ARIS SUMMARY SHEET

District Geologist, Kamloops　　　　Off Confidential: 94.12.10

ASSESSMENT REPORT 23340　　　　MINING DIVISION: Kamloops

PROPERTY: Getty North
LOCATION: LAT 50 35 00　　LONG 121 00 00
UTM 10 5605182 641591
NTS 092I11E 092I10W

CAMP: 018 Highland Valley Camp

CLAIM(S): Getty 1-2,Getty 4
OPERATOR(S): Getty Copper Corp.
AUTHOR(S): Gower, S.C.
REPORT YEAR: 1994, 99 Pages
COMMODITIES
SEARCHED FOR: Copper,Molybdenum/Molybdenite,Gold,Silver
KEYWORDS: Guichon Batholith,Supergene breccia,Malachite,Chrysocolla,Tenorite
Jarosite,Native copper,Cuprite,Chalcopyrite,Bornite,Reserves
WORK
DONE: Drilling,Geochemical
DIAD 557.8 m 5 hole(s);HQ
Map(s) - 5; Scale(s) - 1:1000
META 8 sample(s)
SAMP 279 sample(s) ;ME
RELATED
REPORTS: 17974,19858
MINFILE: 092INE038

GOWER,
THOMPSON
& ASSOCIATES LTD.

985 Gatensbury Street
Coquitlam, B.C. Canada
V3J 5J6
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ASSESSMENT REPORT. DRILLING & METALLURGY ON THE GETTY NORTH PROPERTY & SURROUNDING CLAIMS IN AUGUST, 1993

**Consisting of: Getty 1 - 94
and Getty "A" Fractional
Mineral Claims**

Highland Valley Area, B.C.
Kamloops Mining Division
LAT.:50° 35' LONG: 121° 00'
NTS 92 I/11E & 92 I/10W

Prepared for:

**GETTY COPPER CORP.
ROBAK INDUSTRIES LTD.
& JOHN LEPINSKI**
1000 Austin Avenue
Coquitlam, B.C.
V3K 3P3

MARCH 29, 1994

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1.0 STATEMENT OF COSTS

This statement of costs includes work carried out from the period August 17 to December 31, 1993. The work includes diamond drilling, core splitting, core logging, assaying, metallurgical studies and engineering of reports. An air photo and a satellite interpretation of linears are in progress and will constitute a separate statement of costs and report. Of this total, $ 68,400 has been claimed for assessment purposes.

TABLE ONE STATEMENT OF COSTS

Diamond drilling, 1827 feet @ $24.00/foot. Fixed cost HQ core	$ 43,850
Field Personnel	
Core splitting, E. M. Thompson, Aug 17 to Sept 1, 16 days @ $125/day	2,000
Core logging, S.C. Gower, Aug. 17 to Sept 1, 16 days @ $300/day	4,800
Support Cost	
Vehicle rental two trucks @ $150/day for 16 days	2,400
Core storage	1,000
Reclamation costs	1,000
Management costs - Getty Copper	3,000
Support Costs, room and board @ $100/day for 16 days	1,600
Gasoline and consumed materials	945
Generator rental 3 weeks @ $107/week	321
Assaying - Total copper, Oxide copper, molybdenum, silver and gold	7,300
Metallurgy	5,000
Report preparation and drafting	1,500
Geological Mapping & Engineering	500
TOTAL	**$ 75,216**

2.0 SUMMARY

This report describes the drill program and metallurgical study carried out by Getty Copper Corp. in 1993. The data acquired from the drilling and metallurgy indicates that if sufficient reserves can be discovered, the oxide deposit is amenable to extraction by a leaching operation. This plant would treat oxide and some categories of sulphide mineralization. Initial metallurgical testing of the sulphide material indicates that it responds favorably to concentration utilizing flotation methods.

3.0 CONCLUSIONS

The Getty North porphyry copper deposit is a partially developed mineral resource that warrants further exploration. The potential exists to prove up sufficient reserves to provide oxide ore for a heap leach solvent extraction and electro-winning plant. In addition, further drilling may prove up mineable tonnages of sulphide ore that could be concentrated onsite or processed at the nearby Highland Valley Copper operation.

4.0 RECOMMENDATIONS

Further exploration on the Getty North deposit should include geological mapping, geophysics, diamond drilling, assaying of drill core and metallurgical test work. It is recommended that Getty Copper Corp. should option the adjacent Getty South and Getty West deposits. These properties would provide additional exploration targets in the area. This would increase the potential of developing sufficient reserves to justify the construction of production facilities.

5.0 INTRODUCTION

5.1 Terms of Reference

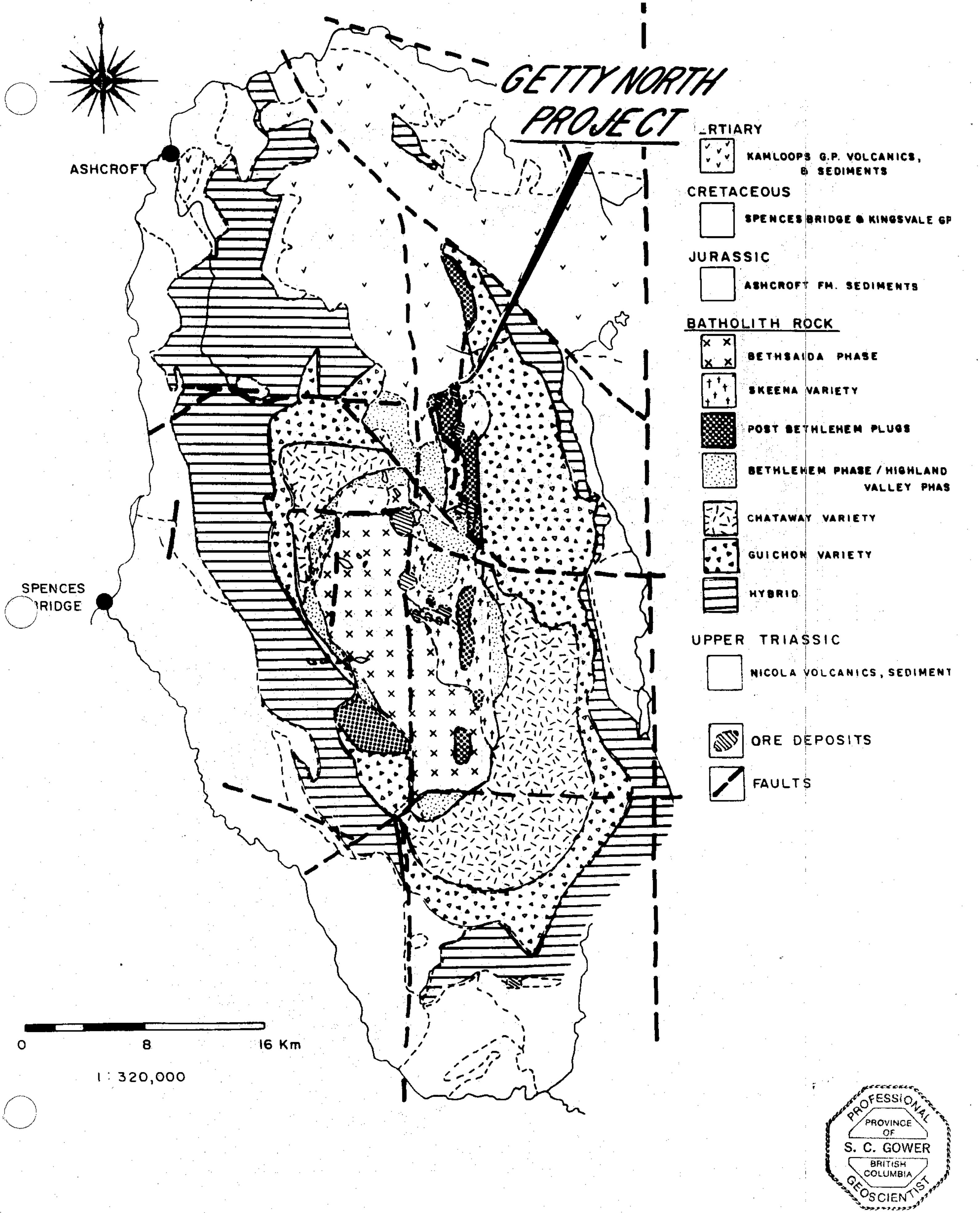
Gower Thompson and Associates Ltd. and Beattie Consulting Ltd. were contracted by Getty Copper Corp. to supervise a drilling and metallurgical program on the Getty North deposit. Data used in this report was generated during the 1993 exploration program or consisted of reports commissioned by Getty Copper Corp. or by prior operators. Data from prior operators was provided by Robak Industries Ltd.

5.2 Location and Access

The Getty North deposit is well situated for ease of access and availability of infrastructure, power and a stable workforce. It is located to the north of the Highland Valley Copper mine. The Getty claims are situated on and around Forge Mountain which exhibits some areas of moderately steep relief on its east flank. The mineral deposit is located between 1525 meters (5000 feet) to 1830 meters (6000 feet).

The deposit is located in the Highland Valley of B.C. at Lat.: 50° 35' Long: 121° 00' in the Kamloops Mining District. The claims are situated about 6 kilometers north of the Bethlehem Copper deposit. The nearest major city is Kamloops, B.C., which is located 72 kilometers to the north east.

Access to the property is via the Bose Lake road that branches off the road to the Bethlehem Mine.



GEOLOGY OF THE GUICHON CREEK BATHOLITH

6.0 CLAIM STATUS

The claims that make up the Getty property have been surveyed; title verified by Land Titles in Victoria and overstaked in the name of Getty Copper Corp. by four post claims to acquire any fractions.

The current Getty Copper Corp. claim consists of the following two post mineral claims:

TABLE TWO:

CLAIM STATUS

Owner: Getty Copper Corp. by purchase from Robak Industries.

Claim Name	Number of Units	Month/Day of Record	Expiry year	Record Number
Getty 1, 2	2	August 6	2003*	221561-562
Getty 3, 4	2	August 6	2003*	221563-564
Getty 5, 6	2	August 16	2003*	221565-566
Getty 7, 8	2	August 16	2003*	221567-568
Getty 9 to 18	10	August 16	2003*	221569-578
Getty 19	1	August 16	2003*	221579
Getty 20	1	August 16	2003*	221580
Getty 21	1	August 16	2003*	221581
Getty 22	1	August 16	2003*	221582
Getty "A" Fr.	1	August 16	2003*	221585

* Pending acceptance of 1993 Assessment Report.

All of the claim posts and tags except for the final tags for Getty 7 and 8 have been examined in the field by staff of Gower Thompson & Associates Ltd. These post and tags were found to be as described on the affidavits and located on the maps. The final post for Getty 7 and 8 appears to have been destroyed by fire related to clear cut logging.

The following claims are part of the exploration agreement between Getty Copper, Robak Industries Ltd. and John Lepinski. These claims are grouped under Getty four and five grouping notices and are contiguous.

Name	Units	Record Date	Expiry	Record Number
Getty 23/24	2	August 16	1996*	221583/221584
Getty 26	8	January 7	1996*	218221
Getty 27-29	3	January 5	1996*	218222-218224
Getty 30	1	January 7	1996*	218225
Getty 31-36	6	January 6	1996*	218226-218231
Getty 37/38	2	January 7	1996*	218232/218233
Getty 39-44	6	May 13	1996*	218430-218435
Getty 45-47	3	May 15	1996*	218436-218438
Getty 48	8	May 17	1996*	218439
Getty 49-52	4	May 16	1996*	218440-218443
Getty 53	1	May 17	1996*	218444
Getty 54	4	May 19	1996*	218445
Getty 55/56	2	May 19	1996*	218446/218447
Getty 57-60	4	May 19	1996*	218448-218451
Getty 61	9	June 6	1997*	218489
Getty 62	9	June 6	1996*	218490
Getty 63-67	5	June 6	1996*	218491-218495
Getty 68-71	4	June 7	1996*	218496-218499
Getty 72-76	5	June 8	1996*	218500-218504
Getty 78/79	2	June 9	1996*	218506/218507
Getty 80/81	2	June 10	1998*	218508/218509
Getty 82/83	2	June 10	1996*	218510/218511
Getty 85-87	3	June 11	1996*	218513-218515
Getty 88-90	3	June 11	1996*	218522-218524
Getty 91/92	2	July 1	1996*	218557/218558
Getty 93	20	June 16	1996*	318212
Getty 94	5	June 17	1996*	318213

* Pending acceptance of assessment report.

7.0 PREVIOUS WORK

The history of the property is fragmented. Unfortunately much of the data generated by prior operators is not a matter of public record.

A brief description of the available history of the Getty North property is as follows:

Year:	Work Performed:
1956 - 1957	Company: Northlodge Copper Mines Geological Mapping, geochemical and magnetic surveys, 1970 feet of bulldozer trenching and 27 diamond drill holes totaling 9,635 feet.(K-1 to K-27).
1957 - 1959	Company: Kennco Explorations (Western) Ltd. Geological Mapping, Geochemical, magnetic and I.P. surveys; 2,170 feet of bulldozer trenching and 2 diamond drill holes totaling 1,115 feet.
1964 - 1965	Company: North Pacific Mines Eight holes totaling 7,688 feet of Diamond Drilling and 17 holes totaling 2,625 of percussion drilling. (DDH 1-65 to 8-65, and P-1 to P-17).
1965	Company: Canex Aerial Explorations Ltd. Soil sampling; 15 diamond drill holes totaling 6500 feet. (DDH 9-65 to 22-65).
1967	Company: Isaac Shulman syndicate. Four diamond drill holes totaling 2,775 feet. (S-30 to S-33)
1968	Company: North Pacific Mines Bulldozer trenching and airborne magnetic survey.
1968 - 1969	Company: Noranda Explorations Ltd. Geological, Geochemical and Geophysical surveys. Seven diamond drill holes totaling 3,140 feet. (DDH 1-69 to 3-69, and 9-69 to 12-69).
1970	Company: North Pacific Mines Twenty-five percussion holes were drilled totaling 3,770 feet. (P1-70 to P18-70 and P20-70 to P26-70)

1971 -1972	Company: Getty Mining Pacific Ltd. I.P. surveys. Sixteen percussion holes were drilled totaling 5,792 feet. Three diamond drill holes were drilled totaling 2,050 feet. (P1-71 to P16-71, DDH 71-1 to 71-3).
1972 - 1973	Company: Quintana Minerals Percussion Drilling.
1974 - 1992	Company: Robak Industries Ltd. Percussion drilling, geological studies, geochemical surveys, bulk sampling, metallurgical studies and engineering reports. Claim staking, water quality and surveying.
1993	Company: Getty Copper Corp. Five diamond drill holes were drilled. Water quality survey. Claim staking and surveying.

8.0 1993 DRILL PROGRAM

Using funds raised by Getty Copper Corp. five HQ diamond drill holes were drilled into the central portion of the Getty North deposit in late August, 1993. The drilling was carried out by J.T. Thomas Diamond Drilling out of Smithers B.C. The drilling was done for a fixed total cost of $ 24/foot. These holes demonstrated that the fragile oxide cap could be recovered by diamond drilling. Core recovery was consistently close to 100% and copper loss was judged to be negligible. In all the drill holes the oxide zone was observed to be jarositic and intensely shattered. Copper mineralization in the zone of oxidation was predominantly malachite and chrysocolla. A zone of enrichment was generally present at the top of the oxide deposit at the paleosurface.

Water for the drill program was taken from Krain Lake. At the end of the program the water level in the lake was drawn down significantly.

The data in the following table provides the geometry of the drilling.

TABLE THREE:

DRILL DATA 1993 PROGRAM BY GETTY COPPER CORP.

HOLE NO.	COORDINATES	DEPTH	DIP	AZIMUTH
93-1	130460 N 118580 E	500 feet (152 meters)	090 degrees	------
93-2	130120 N 118745 E	500 feet (152 meters)	090 degrees	------
93-3	130035 N 118690 E	300 feet (91 meters)	090 degrees	------
93-4	130250 N 118960 E	212 feet (65 meters)	090 degrees	------
93-5	130250 N 118960 E	318 feet (97 meters)	-60 degrees	310 true

Drill hole 93-1 returned rusty colored mud from 50 to 94 feet. It is believed that this may represent an unconformity. The drill head banged into the top of a supergene breccia at 94 feet. The oxide zone was cored from 94 to 500 feet. The zone was well shattered and jarositic. Secondary copper minerals were primarily malachite and chrysocolla, with minor tenorite. This mineralization occurs along jointing and fracture planes, and as dusty infilling in the matrix. Some native copper and cuprite were observed near the bottom of the hole.

The material from 50 to 94 feet requires redrilling using a split tube to recover a sample. It is possible this interval contains ore grade intersections in the poorly consolidated material that could not be cored with the bit and core tube used. It is believed that the hole was terminated close to the oxide interface with the primary zone.

Drill hole 93-2 intersected the oxide zone at 40 feet. No core was recovered from an anticipated high grade intercept from 23 to 40 feet. This intercept had assayed 1.65 % copper in a hole drilled by Canex Placer in 1965. It is believed the bottom of this enriched zone is represented by the supergene breccia encountered at 40 feet (1.03 % copper). The interface between oxide and sulphide zones was marked by the presence of cuprite. The drill hole exited the oxide zone at 210 feet and was still in sulphide material when the hole was stopped at 500 feet.

Drill hole 93-3 cored the oxide zone at 30 feet. The hole intersected a supergene breccia and a copper enriched zone from 30 to 60 feet. Copper content in the zone diminished as the drill hole followed a series of vertical shear zones from 150 to 210 feet. The drill hole exited the oxide zone at 214 feet and encounter a chalcopyrite and bornite mineralization. The hole was terminated at 300 feet due to budgetary considerations.

Drill hole 93-4 triconed through 28 feet of broken oxide material which contained significant secondary copper values. Core was returned at 28 feet and the hole exited the oxide zone at 104 feet. The oxide zone was significantly shallower in this hole than the first 3 holes presumably due to a cross cutting north east trending fault.

Drill hole 93-5 was drilled off the same site at 93-4, but at a dip and azimuth that followed the deposit to depth along a north west trend. This hole encountered a zone of paleosurface enrichment from 29 to 129 feet. This hole encountered the highest grade material drilled during the 1993 program. The drill hole averaged 0.90 % copper over a true thickness of 190 feet.

The split portion of the drill core is stored at the public warehouse on the west side of Kamloops under the name of Getty Copper Corp. The reject portions from assays of the drill core are stored at Eco-Tech Laboratories in Kamloops.

9.1 GETTY NORTH GEOLOGY

1.1 Introduction

The Getty North deposit occurs as a partially drift covered porphyry copper system at least 1000 meters long, 350 meters wide and up to 450 meters deep. Additional drilling is required to delineate the outer boundaries of the mineralization.

The primary sulphide minerals consist of chalcopyrite, bornite and pyrite. These minerals occur as disseminations and fracture fillings within the quartz diorite and breccia zones and near the shattered margins of the mineral zone. A zone of oxidized copper minerals has been formed over the north end of the deposit. This zone is bowl shaped with the deepest portion of the bowl overlying the area of the most intense fracturing.

These primary copper minerals have been oxidized to chrysocolla, malachite, azurite, cuprite and chalcocite within the zone of oxidation.

In plan view, the copper zone appears to be cylindrical with the axis plunging to the southeast. The copper zone appears to be cut and possibly offset by a fault to the northwest. The northeastern boundary is nearly vertical. The nose of the deposit has a steep plunge to the northwest.

The mineralization hosted on the Getty North property consists of a porphyry copper suite of ore and alteration minerals. The ore resource occurs within a northwest trending fracture system typified by porphyry dykes, hydrothermal veins and fracture assemblages. This fracture system is part of a major regional break that also hosts the Bethlehem Copper and the Getty South deposit. A zone of oxidation has been developed on the property that forms a cap of secondary copper minerals at and near surface. Within the oxide zone copper values have been remobilized and concentrated along jointing planes.

The primary ore controls on the Getty property are associated with an elongated stock that intrudes quartz diorite of the Highland Valley phase. This younger intrusive stock appears to possess a cupola shaped projection at its higher levels. The apex of the stock plunges gently away from the topographical high at Getty North to both the northwest and southeast. Fracturing, brecciation, alteration and mineralization are localized in and around the younger stock.

TABLE FIVE:

MINERALOGY OF THE OXIDE ZONE

DDH No.	Footage From	To	Total Copper	Carbonate Copper	Silicate Copper	Copper as Carbonate
93-1	94	235	0.46%	0.34%	0.10%	77%
93-1	235	335	0.28%	0.20%	0.06%	77%
93-1	335	435	0.34	0.28%	0.04%	88%
93-2	40	100	0.44%	0.36%	0.08%	82%
93-2	100	210	0.32%	0.16%	0.08%	67%
93-3	30	60	1.26%	1.08%	0.12%	90%
93-5	29	129	1.04%	0.86%	0.10%	90%
93-5	129	219	0.66%	0.52%	0.06%	90%

9.1.3 Primary Mineralization and Alteration

As expected in a porphyry copper deposit primary sulphide mineralization and silicate alteration form well-defined patterns around the Bethlehem age intrusion. Within the Bethlehem intrusion, and its margins, chalcopyrite and bornite mineralization are the primary copper minerals present. Associated mineralization consists of molybdenite and gold and silver bearing minerals in quartz veins. Adjacent to the chalcopyrite and bornite zone, lower grade chalcopyrite and pyrite fracture fillings occur within the quartz stockworks. The copper content in the chalcopyrite and pyrite zone diminishes toward the outer margins.

The primary sulphide mineralization has been tested to an average depth of 150 meters over a length of 730 meters. Holes deeper than 240 meters have been drilled only in the central portion of the deposit. Most of the deep holes have copper values in the 0.2% to 0.5 % copper range. Assays from the deepest hole indicate that at the center of the porphyry system 0.22 % copper is present 450 meters below the drill collar.

9.1.2 Oxidized Zone

A cap of oxidized copper mineralization occurs over the northern portion of the porphyry deposit. The degree of oxidation observed in the 1993 drill core was total and complete. It is believed that native copper makes up the balance of the copper minerals that did not report as oxide in the analytical procedures.

This oxide cap forms a homogenous unit up to 150 meters thick which has been largely preserved from erosion by Early Tertiary Basalt. These basaltic rocks onlap onto the oxide zone in the vicinity of Krain Lake and form the north boundary of the area of interest.

Copper mineralization within the oxide zone consists of malachite, chrysocolla, azurite and cuprite. These minerals occur primarily filling jointing planes, fractures and cavities. It is suspected that trace amounts of chalcocite that occur form a major component of a black, waxy mineral.

The copper bearing portion of the oxide zone is thickest and highest grade over the center of the sulphide zone, and decreases in grade to the northwest. The southern and northwestern edges have been depleted of copper leaving predominantly iron oxides.

TABLE FOUR:

DEGREE OF OXIDATION IN OXIDE ZONE

A study by Beattie Consulting Ltd. of acid soluble copper assays show the following depth below surface and degree of oxidation in each of the five holes drilled in 1993.

HOLE NO.	OXIDATION DEPTH	% OF COPPER AS OXIDE
DDH 93-1	152.5 Meters	84.2% Average
DDH 93-2	64.0 Meters	94.6% Average
DDH 93-3	57.9 Meters	88.6% Average
DDH 93-4	33.3 Meters	97.9% Average
DDH 93-5	72.0 Meters	97.4% Average

A study by Beattie Consulting Ltd. on the mineralogy of the oxide zone based on analytical procedures yielded the following data.

Malachite, azurite and tenorite are expected to be the main carbonate copper minerals. Chrysocolla is the main silicate copper mineral. No chalcocite was identified in any of the samples.

9.1.4 Structure

The copper mineralization at the Getty North deposit is structurally controlled. The highest grades of copper occur in zones occupying areas of high fracture density adjacent to the Bethlehem age intrusion. A strong predominantly post mineral north and northeasterly trending fault system crosses the property. Faulting within the Early Tertiary Kamloops group rocks is restricted almost entirely to down faulted blocks.

10.0 DRILL INDICATED RESERVES

An accurate determination of the tonnage and grade of the Getty North deposit has not been achieved by the drilling to date. The drilling carried out by Getty Copper Corp. and the previous operators have been exploration rather than development drilling. The property requires development drilling to determine the actual reserves present. Based on the available drill data an estimate of current reserves can be calculated using the polygon method to establish areas of influence. Due to the varying quality of data depending on the drill method used, only the drill holes where the values could be assigned a high level of confidence were used in the calculations. These high confidence drill holes were generally diamond drilled by major contractors engaged by North Pacific Mines, Canex-Placer or Getty Mines. Percussion holes drilled by small contractors were not used because of the poor recovery and the uncertain methods of sample collection.

10.1 Oxide Reserve

The revised tonnage and grade figures for the polygons included in the oxide reserve category are summarized as follows:

TABLE SIX:

TONNAGE AND GRADE ESTIMATES - OXIDE ZONE

POLYGON	SURFACE AREA	VERTICAL	TONNES	DEPTH TO ZONE	% COPPER
65-1	3,780 sq M	33.5 M	329,200	16.8 M	0.73
65-2	2,490 sq M	64.0 M	414,300	12.5 M	0.76
65-4	3,360 sq M	58.5 M	511,000	7.0 M	0.55
93-2		51.8 M	452,500	12.2 M	0.48
Revised Polygon			481,800		0.52
65-6	645 sq M	36.0 M	60,300	4.3 M	0.62
93-4		23.5 M	39,400	8.5 M	0.58
Revised Polygon			49,900		0.60
65-11	3,320 sq M	79.3 M	684,300	39.6 M	0.47
65-15	3,550 sq M	48.8 M	450,200	36.6 M	0.45
65-21	2,900 sq M	76.2 M	574,500	6.7 M	0.47
93-1	2,900 sq M	123.8 M	933,450	28.7 M	0.41
Revised Polygon			754,000		0.44
S-30	5,930 sq M	69.0 M	1,064,000	53.7 M	0.60
S-31	8,680 sq M	49.0 M	1,105,800	43.6 M	0.31
S-32	3,060 sq M	82.0 M	652,400	37.8 M	0.66
S-33	8,060 sq M	36.0 M	754,400	88.4 M	0.36

K-3	3,420 sq M	64.0 M	569,000	12.8 M	0.43
K-1	1,770 sq M	47.0 M	216,300	0.0 M	1.08
93-5		72.0 M	331,350	8.0 M	0.90
Revised Polygon			273,800		0.98
K-12	3,250 sq M	73.2 M	618,500	24.4 M	1.02
K-4	8,000 sq M	30.0 M	624,000	24.1 M	0.40

The polygons used in Table 6 are those that are contiguous and have a copper grade greater than 0.30 % copper.

10.2 Sulphide Reserve

The tonnage and grade values for polygons developed to date that form the present drill indicated sulphide reserve are summarized in Table 7.

TABLE SEVEN:

TONNAGE AND GRADE ESTIMATES - SULPHIDE ZONE

POLYGON	AREA(SQ METERS)	VERTICAL	TONNES	% TOTAL COPPER
65-1*	6,195	100 meters	1,672,650	0.50
93-3 intersected		24 meters		0.39
93-4 intersected		32 meters		0.53
65-2	2,490	30 meters	201,700	0.48
		109 meters	732,800	0.21
		243 meters	1,633,700	0.38
65-4	3,360	119 meters	1,079,600	0.54
93-2 drilling intersected		88 meters		0.59
65-15	3,550	50 meters	479,250	0.39
65-21	2,900	90 meters	704,700	0.59
65-8	3,000	103 meters	834,300	0.48
65-3	4,500	158 meters	1,919,700	0.44
65-5	3,250	204 meters	1,790,000	0.52
		50 meters	438,750	0.31
65-7	3,500	137 meters	1,294,650	0.30
K-14	1,480	96 meters	383,600	0.56
	Total			0.50

* Includes oxide polygons 65-6 and K-1

10.21 Low Grade Mineralization

A preliminary pit design on the Getty North deposit was constructed by Canex Placer in 1965. This work indicated that the following tonnage of low grade mineralization would be extracted, if the central portion of the Getty North deposit was mined to a 465 foot (150 meter depth).

TABLE EIGHT:

LOW GRADE MINERALIZATION	
Sulphide Protore	11,000,000 tonnes of 0.27 % Copper
Oxide and Sulphide	21,000,000 tonnes of 0.14 % Copper

The first cleaner concentrate contained 2.37 grams of gold, and 122 grams of silver per tonne of concentrate. A smelter credit would be obtained for both these precious metals. No molybdenum was detected in any of these products so that this element does not appear to occur in this section of the deposit.

13.0 QUALIFICATIONS

I, STEPHEN C. GOWER, of 985 Gatensbury Street, Coquitlam, B.C., V3J 5J6 do hereby certify that:

1. I have been practising as a geologist for a period of approximately 23 years for mining exploration and consulting companies. During this time I have carried out numerous exploration programs on porphyry copper deposits in British Columbia. I have been trained in geochemical, geophysical and geological exploration techniques used in the evaluation of porphyry targets.

2. I obtained a B.Sc. in geology from U.B.C. in 1970 and have completed Master's courses at U.B.C. in property evaluation and exploration.

3. I am a fellow in the Geological Association of Canada and a member of the Association of Professional Engineers and Geoscientists of the Province of British Columbia.

4. I have carried out exploration programs on the Getty North property during the field seasons of 1984, 1986, 1988 and 1990 and supervised the diamond drilling in 1993. This report was written during the period January 15 to March 28, 1994.

5. I, and Gower Thompson & Associates Ltd. hold shares in Getty Copper Corp.

6. I am currently employed as a geologist with Gower Thompson and Associates Ltd.

Stephen C. Gower

B.Sc/F.G.A.C./P.Geo.

PROFESSIONAL
PROVINCE OF
S. C. GOWER
BRITISH COLUMBIA
GEOSCIENTIST

14.0 REFERENCES

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APPENDIX ONE

DRILL LOGS 1993 PROGRAM

GETTY NORTH PROJECT FIELD LOGGING Logging by Stephen Gower, P. Geo.

HOLE NO. 93 - 1

METERS	SAMPLE	Assay % Total Copper	Assay % Oxide Copper	ZONE	Rock Type	Structure	Major mineralization.	NOTES: Dip 090 degrees. HQ core. **Notes: intervals given in feet .**
0-28.7	Overburden						Fragments of chrysocolla.	Drill return reddish. Fragments of volcanics and granitics 84 to 94.
28.7-31.7	120001	0.75	0.65	Oxidized	Guichon	Brecciated	Malachite	Fragments of Guichon averaging about 1 cm. Some malachite in matrix.
								Supergene breccia developed on top of bedrock.
31.7-34.8	120002	0.59	0.57	Oxidized	Guichon	Shattered	Malachite, chrysocolla	Seams of chryocolla and cuprite. Black blebs of tenorite.
34.8-37.8	120003	0.55	0.50	Oxidized	Guichon	Shattered	Malachite, chrysocolla	Rock is more silicious. Feldspar envelopes along fractures.
37.8-40.9	120004	0.53	0.44	Oxidized	Guichon	Shattered	Malachite, chrysocolla	More abundant mafics.
40.9-43.9	120005	0.66	0.69	Oxidized	Guichon	Shear zone	Malachite, chrysocolla	Fault zone crosses perpendicular to core axis.
								Malachite and chrysocolla along fractures and in matrix.
43.9-47.3	120006	0.42	0.38	Oxidized	Guichon	Shattered	Malachite, chrysocolla	Andesitic dyke containing fragments of Guichon crossing core axis.
47.3-50.3	120007	0.45	0.43	Oxidized	Guichon	Shattered	Malachite, chrysocolla	Highly altered granitic rock. Malachite infillings.
50.3-53.4	120008	0.44	0.44	Oxidized	Guichon	Fault Bx.	Malachite, chrysocolla	Jarosite decreasing to 172. Apple green mineral.
53.4-56.4	120009	0.25	0.23	Oxidized	Guichon	Shattered	Malachite, chrysocolla	Mineralization occurs in fractures following core axis.
56.4-59.5	120010	0.28	0.22	Oxidized	Guichon	Shattered	Malachite, chrysocolla	Shattering and quartz sericite alteration increasing.
59.5-62.5	120011	0.50	0.45	Oxidized	Guichon	Shattered	Malachite, chrysocolla	Seams of chrysocolla and apple green mineral crossing core axis
62.5-65.6	120012	0.44	0.39	Oxidized	Guichon	Shattered	Malachite, chrysocolla	Seams of malachite following qtz stringers. Blebs of chrysocolla.
65.6-68.6	120013	0.35	0.30	Oxidized	Guichon	Shattered	Malachite, chrysocolla	Shear zone 216 to 217.
68.6-71.7	120014	0.61	0.58	Oxidized	Guichon	Fault Bx.	Malachite, chrysocolla	Increase of malachite in matrix.
71.7-74.7	120015	0.52	0.50	Oxidized	Guich/Beth	Shattered	Malachite, chrysocolla	Fracture fillings of malachite and chrysocolla. Abundant quartz veinlets.
74.7-77.7	120016	0.40	0.39	Oxidized	Bethlehem	Fault	Malachite	Dyke at 247 - 254. Fault gouge following core axis.
77.7-80.8	120017	0.41	0.42	Oxidized	Bethlehem	Fault	Malachite, chrysocolla	Dyke at 256 to 257. Chrysocolla along fractures. Major fault zone.
80.8-83.8	120018	0.33	0.33	Oxidized	Bethlehem	Fault	Malachite	Some dyke rock. Quartz stringers and gouge.
83.8-86.9	120019	0.41	0.40	Oxidized	Bethlehem	Fault	Malachite, chrysocolla	Local fault breccia at 279.
86.9-89.9	120020	0.25	0.25	Oxidized	Bethlehem	Fault	Malachite	Fault zone. Highly sericitic. Sheared Guichon. Very broken. Low grade.
89.9-93.0	120021	0.26	0.21	Oxidized	Bethlehem	Fault	Malachite	As above.
								Strongly sericitized. Manganese dendrites.
93.0-96.0	120022	0.14	0.13	Oxidized	Bethlehem	Fault	Tenorite	Strong shear zone. Strongly sericitized.
				Oxidized	Bethlehem	Fault	Malachite	Strong shear zone.
96.0-99.0	120023	0.16	0.14	Oxidized	Bethlehem	Fault	Malachite	Strong shear zone.
99.0-102.1	120024	0.16	0.13	Oxidized	Bethlehem	Fault	Azurite	Occasional speck of tenorite. Jarositic. Sometimes vuggy.
102.1-105.2	120025	0.45	0.20	Oxidized	Bethlehem	Fault	Azurite, Malachite	Strong shear zone.
105.2-108.2	120026	0.44	0.17	Oxidized	Bethlehem	Fault	Azurite, tenorite	Strong crush zone.
108.2-111.3	120027	0.30	0.30	Oxidized	Bethlehem	Fault	Chrysocolla, tenorite	Shear zone.
111.3-114.3	120028	0.40	0.39	Oxidized	Beth/Guich	Contact		Contact at 370.
114.3-117.4	120029	0.55	0.50	Oxidized	Guichon	Fractured	Chrysocolla	Mafics recognizable.
117.4-120.4	120030	0.36	0.29	Oxidized	Guichon	Fractured	Chrysocolla, cuprite	Some dendritic tenorite.
120.4-123.5	120031	0.43	0.33	Oxidized	Guichon	Fractured	Chrysocolla, tenorite	Some emerald green mineral associated with quartz veinlets.
123.5-126.5	120032	0.50	0.40	Oxidized	Guichon	Fractured	Chrysocolla, tenorite	Some sooty chalcocite.
126.5-129.6	120033	0.50	0.46	Oxidized	Guichon	Fractured	Chrysocolla, tenorite	Cuprite 418 to 419.
129.6-132.6	120034	0.48	0.36	Oxidized	Guichon	Fractured	Cuprite, native copper	Native copper occurs associated with chrysocolla, cuprite and tenorite.
132.6-135.7	120035	0.34	0.28	Oxidized	Guichon	Fractured	Malachite, native copper	Distinct leafs of native copper.
135.7-138.7	120036	0.28	0.19	Oxidized	Guichon	Fractured	Malachite, native copper	Minor tenorite and cuprite.
138.7-141.8	120037	0.31	0.23	Oxidized	Guichon	Fractured	Malachite, native copper	Minor tenorite.
141.8-144.8	120038	0.35	0.26	Oxidized	Guichon	Fractured	Chrysocolla, cuprite	Minor tenorite
144.8-147.9	120039	0.40	0.20	Oxidized	Guichon	Fractured	Chrysocolla, native copper	Good specimen of native copper selected at 485.
147.9-152.4	120040	0.52	0.10	Oxidized	Guichon	Fractured	Chrysocolla, native copper	Still well oxidized, some cuprite, tenorite. End of Hole.

PROFESSIONAL
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BRITISH COLUMBIA

GOWER THOMPSON

GETTY NORTH PROJECT
HOLE NO. 93 - 2

FIELD LOGGING

G93-2.XLS

Logged by Stephen Gower, P.Geo.

METERS	SAMPLE NO.	ASSAY % Total Copper	ASSAY % Oxide Copper	Zone	Rock Type	Structure	Copper	Notes: Intervals given in feet.
0-12.2	Overburden							Volcanic fragments, clasts of quartz diorite.
12.2-15.2	122051	1.03	1.03	Oxidized	Guichon	Shattered	Mal/chry/ten	Supergene breccia 40 - 41. Enriched in copper to 48.
15.2-18.3	122052	0.54	0.51	Oxidized	Guichon	Shattered	Mal/chry	Some pale blue mineral mixed with the malachite.
18.3-21.3	122053	0.49	0.41	Oxidized	Guichon	Shattered	Mal/chry/ten	Local fault breccia at 69.
21.3-24.4	122054	0.68	0.67	Oxidized	Guichon	Shattered	Mal/chry/ten	Blebs of tenorite replacing sulphides.
24.4-27.4	122055	0.44	0.36	Oxidized	Guichon	Shear zone	Mal/chry	Shear zone 83 -102
27.4-30.5	122056	0.41	0.40	Oxidized	Guichon	Shattered	Malachite	Fault breccia at 90 - 91. Thin aplitic dyke at 91.
30.5-33.5	122057	0.38		Oxidized	Guichon	Shattered	Mal/chry	Jarositic,
33.5-36.6	122058	0.32		Oxidized	Guichon	Shattered	Malachite	Jarositic to 113, Malachite - 117.
36.6-39.6	122059	0.30		Oxidized	Guichon	Shattered	Malachite	Crush zone - 123, Cuprite - 126, hematite
39.6-42.7	122060	0.31		Oxidized	Guichon	Shattered	Mal/azur	Crush zone at 139 to 140.
42.7-45.7	122061	0.35		Oxidized	Guichon	Shattered	Malachite	Vuggy quartz veinlets. Malachite blotches.
45.7-48.8	122062	0.35		Oxidized	Guichon	Shattered	Malachite	Black crosscutting seams more numerous.
48.8-51.8	122063	0.27		Oxidized	Guichon	Shattered	Chrysocolla	Dyke rock at 165 to 169.
51.8-54.9	122064	0.46		Oxidized	Guichon	Shattered	Mal/chry	Dyke 126 - 127. Sericite alteration intensifying.
54.9-57.9	122065	0.59		Oxidized	Guichon	Shattered	Cup/chry/ten	Sericite alteration deminishing. Jarositic.
57.9-61.0	122066	0.38		Oxidized	Guichon	Shattered	Chrysocolla	Highly sheared 198 to 200. Sericitic.
61.4-64.0	122067	0.56		Oxidized	Guichon	Shattered	Cuprite	Oxide boundry - 209. Horizontal cuprite seams.
64.0-67.1	122068	0.32		Primary	Bethlehem	Broken	Cpy/mal	Chill margin at 210. Chloritic.
67.1-70.1	122069	0.50		Primary	Bethlehem	Broken	Cpy/mal	
70.1-73.2	122070	0.61		Primary	Bethlehem	Broken	Chalcopyrite	Chalcopyrite occurs as vertical fracture fillings.
73.2-76.2	122071	0.35		Primary	Bethlehem	Broken	Cpy/bn	Very fine grained sulphides.
76.2-79.3	122072	0.40		Primary	Bethlehem	Broken	Vfg cpy/bn	
79.3-82.3	122073	0.31		Primary	Bethlehem	Broken	Vfg cpy/bn	
82.3-85.4	122074	0.34		Primary	Bethlehem	Broken	Vfg cpy/bn	Shear zone at 276. Quartz stringers 279 to 287.
85.4-88.4	122075	0.47		Primary	Bethlehem	Broken	Fg cpy/bn	Clay gouge at 286. Shattered at 287.
88.4-91.5	122076	0.48		Primary	Bethlehem	Broken	Chalcopyrite	
91.5-94.5	122077	1.20		Primary	Bethlehem	Broken	Cpy/bn	Sulphide filled fractures - 302
95.5-97.6	122078	0.78		Primary	Bethlehem	Broken	Cpy/bn	Sulphide filled fractures - 311. Black seams.
97.6-100.6	122079	0.88		Primary	Bethlehem	Broken	Cpy/bn	Increased mafic content, Vertical black seams.
100.6-103.7	122080	0.75		Primary	Bethlehem	Broken	Fg cpy/bn	Granophyre 336 - 338.
103.7-106.7	122081	0.60		Primary	Bethlehem	Broken	Cpy/ccte	Granular texture, low mafics.
106.7-109.8	122082	0.73		Primary	Bethlehem	Broken	Cpy/ccte	As above to 365.
109.8-112.8	122083	0.77		Primary	Bethlehem	Broken	Cpy/ccte	Shear zone 366 - 380. Vertical stringers.
112.8-115.9	122084	0.73		Primary	Bethlehem	Broken	Chalcopyrite	Vein of cpy perpendicular to core axis.
115.9-118.9	122085	1.41		Primary	Bethlehem	Broken	Cpy/bn	Horizontal seams of sulphides.
118.9-122.0	122086	0.65		Primary	Bethlehem	Broken	Vfg cpy/bn	
122.0-125.0	122087	0.62		Primary	Bethlehem	Broken	Vfg cpy/bn	Quartz vein perpendicular to core axis at 404.
125.0-128.1	122088	0.75		Primary	Bethlehem	Broken	Vfg cpy/bn	Sulphides - dissem and as fracture fillings to 460.
128.1-131.1	122089	0.68		Primary	Bethlehem	Broken	Cpy/bn	Shear zone 435 to 436.
131.1-134.2	122090	0.71		Primary	Bethlehem	Broken	Cpy/bn	
134.2-137.2	122091	0.49		Primary	Bethlehem	Broken	Cpy/bn	
137.2-140.2	122092	0.43		Primary	Bethlehem	Broken	Fg cpy/bn	
140.2-143.3	122093	0.15		Primary	Bethlehem	Broken	Chalcopyrite	Rock more massive.
143.3-146.3	122094	0.45		Primary	Bethlehem	Broken	Cpy/bn	Chill margin, quartz sericite alteration.
146.3-149.4	122095	0.43		Primary	Bethlehem	Broken	Vfg cpy/bn	Back in granular phase at 480.
149.4-152.4	122096	0.24		Primary	Bethlehem	Broken	Vfg cpy/bn	Black seams containing sulphides.

Note: Malachite -Mal. Azurite - azur. Chrysocolla - chry. Tenorite - ten.
Chalcopyrite - cpy. Bornite - bn. Chalcocite - ccte.

PROFESSIONAL
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S. C. GOWER
BRITISH COLUMBIA
GEOSCIENTIST

GETTY NORTH PROJECT
HOLE NO. 93 - 3

FIELD LOGGING

Logging by Stephen Gower, P.Geo.

NOTES: Dip 090 degrees. HQ core.
Notes: Intervals given in feet.

METERS	SAMPLE NO.	Assay % Total Copper	Assay % Oxide Copper	Zone	Rock Type	Structure	Copper	Notes
0-9.2	Overburden							First core 0.5 feet of volcanics then into granitics.
9.2-12.2	122501	1.48	1.46	Oxidized	Guichon	Shattered	Mal/chry/ten/azur	Supergene breccia to 35 feet. Intense malachite.
12.2-15.2	122502	1.45	1.42	Oxidized	Guichon	Shattered	Mal/chry/ten/azur	Sericitized, manganese dendrites.
15.2-18.3	122503	1.70	1.64	Oxidized	Guichon	Shattered	Mal/chry	Crush zone 56.5. Jarositic.
18.3-21.3	122504	0.50	0.46	Oxidized	Guichon	Shattered	Mal/chry/azurite	Crush zones, manganese dendrites.
21.3-24.4	122505	0.49	0.49	Oxidized	Guichon	Shattered	Malachite	Breccia at 80 feet.
24.4-27.4	122506	0.53	0.50	Oxidized	Guichon	Shattered	Mal/chry/ten/azur	Crush zones at 81, 82 feet.
27.4-30.5	122507	0.47	0.44	Oxidized	Guichon	Shattered	Mal/chry/ten/azur	Blue tinge to matrix.
30.5-33.5	122508	0.36	0.32	Oxidized	Guichon	Shattered	Mal/chry	Well shattered, local fault breccia. Silicious.
33.5-36.6	122509	0.43	0.71	Oxidized	Contact	Shattered	Mal/chry/azurite	Chloritic crush zone 118 to 122.
36.6-39.6	122510	0.35	0.29	Oxidized	Bethlehem	Shattered	Mal/chry	Crush zone, sericitic, clay gouge. Dendrites.
39.6-42.7	122511	0.37	0.35	Oxidized	Bethlehem	Shattered	Mal/chry/azurite	Seams of jarosite parallel to core axis.
42.7-45.7	122512	0.43	0.38	Oxidized	Bethlehem	Shattered	Mal/chry/azurite	Crush zone 149 to 150, vertical fractures.
45.7-48.8	122513	0.20	0.20	Oxidized	Bethlehem	Shattered	Malachite	Sericitic, whitish in color. Clumps of jarosite.
48.8-51.8	122514	0.27	0.22	Oxidized	Bethlehem	Shattered	Mal/chry/tenorite	Manganese dendrites, reddish calcite crystals.
51.8-54.9	122515	0.27	0.25	Oxidized	Bethlehem	Shattered	Mal/chry/tenorite	As above.
54.9-57.9	122516	0.25	0.18	Oxidized	Bethlehem	Shattered	Malachite, cuprite	Crush zone at 184 feet. Fault breccia at 189.
57.9-61.0	122517	0.21	0.15	Oxidized	Bethlehem	Shattered	Mal/chry/cuprite	
61.0-64.0	122518	0.31	0.20	Oxidized	Bethlehem	Shattered	Mal/native copper	Native copper at 204, crush zone at 205.
64.0-67.1	122519	0.23	0.10	Contact	Bethlehem	Shattered	Mal/cpy/bornite	Oxide ends at 214. Strongly jarositic.
67.1-70.1	122520	0.35		Primary	Bethlehem	Broken	Vfg cpy/bn	Sulphides disseminated and along fractures.
70.1-73.2	122521	0.33		Primary	Bethlehem	Broken	Fg cpy/bn	Sulphides disseminated and along fractures.
73.2-76.2	122522	0.40		Primary	Bethlehem	Broken	Cpy/bn	Sulphides disseminated and along fractures.
76.2-79.3	122523	0.35		Primary	Bethlehem	Broken	Cpy/bn	Sulphides disseminated and along fractures.
79.3-82.3	122524	0.27		Primary	Bethlehem	Broken	Fg cpy/bn	Sulphides disseminated and along fractures.
82.3-85.4	122525	0.45		Primary	Bethlehem	Broken	Cpy/bn	Coarser mafics, almost Guichon in appearance.
85.4-88.4	122526	0.53		Primary	Bethlehem	Broken	Vfg cpy/bn	Sericitized, fine grained dyke rock, chloritized.
88.4-91.5	122527	0.40		Primary	Bethlehem	Broken	Vfg cpy/bn	As above. More visible sulphides than 280 - 290.

See drill hole 93 - 2 for abbreviations.

PROFESSIONAL
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S. C. GOWER
BRITISH COLUMBIA

GOWER THOMPSON

GETTY NORTH PROJECT
HOLE NO. 93 - 4

FIELD LOGGING

Logging by Stephen Gower, P. Geo.

METERS	SAMPLE NO.	Assay % Total Copper	Assay % Oxide Copper	Zone	Rock Type	Structure	Copper	NOTES: Dip 090 degrees. HQ core.
								Notes: Intervals given in feet.
0-8.5	Overburden							Clay gouge at 29 feet.
8.5-11.6	122551	0.64	0.62	Oxidized	Guichon	Shattered	Mal/azur/chry	Jarositic, manganese dendrites.
11.6-14.6	122552	0.64	0.63	Oxidized	Guichon	Shattered	Mal/azur/chry	Abundant jarosite and manganese dendrites
14.6-17.7	122553	0.56	0.55	Oxidized	Bethlehem	Shattered	Mal/azur/chry	Jarositic, manganese dendrites.
17.7-20.7	122554	0.80	0.79	Oxidized	Bethlehem	Shattered	Mal/azur/chry	Jarositic, blebs of cuprite.
20.7-23.8	122555	0.67	0.65	Oxidized	Bethlehem	Shattered	Mal/azur/chry	Jarositic, manganese dendrites, pinkish.
23.8-26.8	122556	0.46	0.44	Oxidized	Bethlehem	Shattered	Mal/azur/chry	Jarositic, manganese dendrites.
26.8-29.9	122557	0.33	0.32	Oxidized	Bethlehem	Shattered	Mal/azur/chry	Highly jarositic at 90. Cuprite.
29.9-33.0	122558	0.56	0.47	Contact	Bethlehem	Shattered	Mal/cuprite	Cuprite at 100. Contact at 105. Jarositic.
33.0-36.0	122559	0.55	0.07	Primary	Bethlehem	Broken	Fg cpy/bn	Bleached, sericitic.
36.0-39.0	122560	0.55		Primary	Bethlehem	Broken	Fg cpy/bn	Bleached, sericitic.
39.0-42.1	122561	0.58		Primary	Bethlehem	Broken	Fg cpy/bn	As above, sheared dyke, abundant clays.
42.1-45.1	122562	0.58		Primary	Bethlehem	Broken	Vfg cpy/bn	Bleached, sericitic, abundant clays.
45.1-48.2	122563	0.63		Primary	Bethlehem	Broken	Vfg cpy/bn	Sheared dyke, parallel to core axis.
48.2-51.2	122564	0.53		Primary	Bethlehem	Broken	Fg cpy/bn	Sericitic, clay altered
51.2-54.3	122565	0.46		Primary	Bethlehem	Broken	Fg cpy/bn	Sericitic clay altered
54.3-57.3	122566	0.58		Primary	Bethlehem	Broken	Fg cpy/bn	Abundant clay alteration along shears.
57.3-60.4	122567	0.50		Primary	Bethlehem	Broken	Vfg cpy bn	As above.
60.4-64.6	122568	0.30		Primary	Bethlehem	Broken	Fg cpy/bn	Crush zones at 202, 204, 212. Sericitized.

See drill log 93 - 2 for abbreviations.

PROFESSIONAL PROVINCE OF S. C. GOWER BRITISH COLUMBIA GEOSCIENTIST

GOWER THOMPSON

GETTY NORTH PROJECT
HOLE NO. 93 - 5

Field logging.

FIELD LOGGING

Logging by Stephen Gower, P. Geo.

METERS	SAMPLE	Assay % Total Copper	Assay % Oxide Copper	Zone	Rock Type	Structure	Copper	NOTES: Minus 60 degree dip, strike 310 degrees. Hq core.
								Notes: Intervals given in feet.
0-8.8	Overburden							Fragments of volcanics and granitics.
8.8-11.9	122569	0.84	0.84	Oxidized	Guichon	Breccia	Mal/azur/chry	Supergene breccia.
11.9-14.9	122570	1.19	1.19	Oxidized	Guichon	Shattered	Mal/azur/chry	Jarositic, manganese dendrites.
14.9-18.0	122571	1.82	1.82	Oxidized	Guichon	Shattered	Mal/chry	Malachite flooding of matrix, well mineralized.
18.0-21.0	122572	1.53	1.52	Oxidized	Guichon	Shattered	Mal/azur/chry	Patches of jarosite, manganese dendrites.
21.0-24.1	122573	1.08	1.07	Oxidized	Guichon	Shattered	Mal/azur/chry	As above, quartz stringers.
24.1-27.1	122574	0.78	0.76	Oxidized	Guichon	Shattered	Mal/chry	Breccia at 79, jarosite around fragments.
27.1-30.2	122575	0.86	0.85	Oxidized	Guichon	Shattered	Mal/azur/chry	Jarosite, manganese dendrites.
30.2-33.2	122576	0.90	0.89	Oxidized	Contact	Shattered	Mal/chry	Shatter zone at 99. Patches of jarosite.
33.2-36.3	122577	1.05	1.04	Oxidized	Contact	Shattered	Mal/chry	Shear zone 107 to 109. Pinkish overprint.
36.3-39.3	122578	1.08	1.03	Oxidized	Guichon	Sheared	Mal/chry	Shear zone 127 to 128.
39.3-42.4	122579	0.48	0.47	Oxidized	Contact	Shattered	Mal/chry	Dyke at 136. Shear zone. Jarosite increasing.
42.4-45.4	122580	0.78	0.76	Oxidized	Bethlehem	Sheared	Mal/chry	Fault zone at 145. Sericitized, patches jarosite.
45.4-48.5	122581	0.71	0.70	Oxidized	Bethlehem	Sheared	Mal/chry	Jarositic.
48.5-51.5	122582	1.02	1.02	Oxidized	Bethlehem	Shattered	Mal/chry	Jarositic, manganese, sericitized.
51.5-54.6	122583	0.68	0.63	Oxidized	Contact	Shattered	Malachite	Light dusting of malachite to 176.
54.6-57.6	122584	0.80	0.74	Oxidized	Contact	Shattered	Mal/chry/bn	Guichon 176 to 180.5, pervasive orange color.
57.6-60.7	122585	0.48	0.46	Oxidized	Bethlehem	Shattered	Mal/azur/chry	Patches of malachite and azurite.
60.7-63.7	122586	0.50	0.48	Oxidized	Bethlehem	Sheared	Mal/cuprite	Jarositic, sericitic, manganese dendrites.
63.7-66.8	122587	0.63	0.47	Oxidized	Bethlehem	Shattered	Mal/cuprite	Reds oranges and yellows.
66.8-69.8	122588	0.75		Oxidized	Bethlehem	Shattered	Mal/cuprite	Abrupt color change to bluish with gray veins.
69.8-72.9	122589	0.60		Contact	Bethlehem	Shattered	Vfg cpy/bn	Chloritic.
72.9-75.9	122590	0.36		Primary	Bethlehem	Shattered	Vfg cpy/bn	Dark gray, chloritic, well sheared.
75.9-79.0	122591	0.24		Primary	Bethlehem	Shattered	Vfg cpy/bn	Dark gray, chloritic, well sheared.
79.0-82.0	122592	0.20		Primary	Bethlehem	Shattered	Vfg cpy/bn	Dark gray, chloritic, well sheared.
82.0-85.1	122593	0.29		Primary	Bethlehem	Shattered	Vfg cpy	Shear zone at 271.
85.1-88.1	122594	0.73		Primary	Bethlehem	Shattered	Vfg cpy/bn	Shear zone at 284.
88.1-91.2	122595	0.40		Primary	Bethlehem	Shattered	Vfg cpy/bn	Increased mafics at 285.
91.2-94.2	122596	0.45		Primary	Contact	Shattered	Vfg cpy/bn	Guichon at 306 feet. Shatter zone.
94.2-97.0	122597	0.49		Primary	Guichon	Shattered	Vfg cpy/bn	Chalcopyrite increasing.

See drill log 93 - 2 for abbreviations.

PROFESSIONAL
PROVINCE OF
S. C. GOWER
BRITISH COLUMBIA
GEOSCIENTIST

GOWER THOMPSON

APPENDIX TWO

DRILL DATA - GETTY NORTH PROPERTY

DRILL DATA - GETTY NORTH PROPERTY

NOTES:

1) X means Oxidized Granitic Rock. Primary copper minerals are oxidized to secondary minerals.

2) P means primary sulphide zone. No visible oxidation of sulphide minerals.

3) Placer assay is the assay from the nearest diamond drill hole drilled by Placer Development in 1965. For comparison purposes only.

4) Assays from Eco - Tech Labs are reported in % total copper (TTL Cu), and % oxide copper.

5) Samples are divided into approximate 5 foot runs. The samples were generally run separately and averaged using the weight of the sample as a parameter. The average of the A & B samples is reported as the * result.

6) Drill hole 93 - 1, and the top of 93 - 2 were jaw crushed and the A & B samples composited and assayed together. These samples may require reassaying separately utilizing a cone crusher for improved amalgamation.

GETTY COPPER (65-21) Placer Assay Eco - Tech Assay

DDH-93-1 Footage	SAMPLE #	% TTL Cu/Oxide	% TTL Cu	% OXIDE Cu
		Footage always 4 feet less for Placer		
094-104X	120001A Metallic	0.10/0.10	0.75	
	120001B Assay		0.76	0.65 comb
104-114X	120002	0.14/0.09	0.59	0.57
114-124X	120003	0.15/0.12	0.55	0.50
124-134X	120004	0.15/0.16	0.53	0.44
134-144X	120005A Metallic	0.55/0.50	0.66	
	120005B Assay		0.67	0.69 comb
144-155X	120006	0.55/0.40	0.42	0.38
155-165X	120007	0.30/0.30	0.45	0.43
165-175X	120008	0.60/0.45	0.44	0.44
175-185X	120009	0.85/0.86	0.25	0.23
185-195X	120010	0.75/0.65	0.28	0.22
195-205X	120011	0.56/0.50	0.50	0.45
205-215X	120012	0.60/0.56	0.44	0.39
215-225X	120013	0.35	0.35	0.30
225-235X	20014	0.65	0.61	0.58
235-245X	120015	0.40	0.52	0.50
245-255X	120016	0.45	0.40	0.39
255-265X	120017	0.63	0.41	0.42
265-275X	120018	0.75	0.33	0.33
275-285X	120019	0.50	0.41	0.40
285-295X	120020	0.40	0.25	0.25

295-305X	120021A Metallic		0.25	
	120021B Assay	1.05	0.27	0.21 comb
305-315X	120022A Metallic		0.14	
	120022B Assay	0.55	0.15	0.13
315-325X	120023	0.45	0.16	0.14
325-335X	120024	0.70	0.16	0.13
335-345X	120025	0.41	0.45	0.20
345-355X	120026	0.55	0.44	0.17
355-365X	120027	0.55	0.31	0.30
365-375X	120028	0.50	0.40	0.39
375-385X	120029	0.50	0.55	0.50
385-395X	120030	0.51	0.36	0.29
395-405X	120031	0.42	0.43	0.33
405-415X	120032	0.60	0.50	0.40
415-425X	120033	0.65	0.50	0.46
425-435X	120034	0.52	0.48	0.36
435-445X	120035	0.80	0.34	0.28
445-455X	120036	0.50	0.28	0.19
455-465X	120037	0.90	0.31	0.23
465-475X	120038A Metallic		0.35	
	120038B Assay	0.90	0.35	0.26 comb
475-485X	120039A Metallic	0.33		
	120039B Assay	0.65	0.33	0.20 comb
485-500X	120040A Metallic		0.51	
	120040B Assay	0.45	0.53	0.10 comb

DDH-93-2	SAMPLE #	Placer % Total Cu (65-4)	Eco-Tech % Total Cu		Eco-Tech % Oxide Cu
023-030X		1.80			
030-040X		1.50			
040-050X	122051	1.02	1.03		1.03
050-060X	122052	0.47	0.54		0.51
060-070X	122053	0.38	0.49		0.41
070-080X	122054	0.30	0.68		0.67
080-090X	122055	0.40	0.44		0.36
090-100X	122056	0.40	0.41		0.40
100-110X	122057A	0.53	0.37		0.33
	122057B		0.39	**0.38***	0.32
110-120X	122058A	0.60	0.38		0.30
	122058B		0.27	**0.32***	0.20
120-130X	122059A	0.55	0.26		0.16
	122059B		0.34	**0.30***	0.27
130-140X	122060A	0.43	0.29		0.21
	122060B		0.34	**0.31***	0.26
140-150X	122061A	0.37	0.30		0.19
	122061B		0.40	**0.35***	0.35
150-160X	122062A	0.30	0.38		0.31
	122062B		0.32	**0.35***	0.26
160-170X	122063A	0.35	0.26		0.19
	122063B		0.29	**0.27***	0.19
170-180X	122064A	0.28	0.46		0.39
	122064B		0.47	**0.46***	0.25
180-190X	122065A	0.30	0.34		0.16
	122065B		0.84	**0.59***	0.13

*** A & B Weighted Average**

190-200X	122066A	0.33	0.37		0.14
	122066B		0.39	**0.38***	0.11
200-210X	122067A	0.27	0.52		0.12
	122067B		0.59	**0.56***	0.12
210-220P	122068A	0.35	0.43		
	122068B		0.23	**0.32***	
220-230P	122069A	0.43	0.51		
	122069B		0.49	**0.50***	
230-240P	122070A	0.37	0.86		
	122070B		0.35	**0.61***	
240-250P	122071A	0.50	0.38		
	122071B		0.32	**0.35***	
250-260P	122072A	0.43	0.41		
	122072B		0.38	**0.40***	
260-270P	122073A	0.32	0.34		
	122073B		0.27	**0.31***	
270-280P	122074A	0.62	0.28		
	122074B		0.41	**0.34***	
280-290P	122075A	0.45	0.49		
	122075B		0.44	**0.47***	
290-300P	122076A	0.50	0.44		
	122076B		0.52	**0.48***	
300-310P	122077A	0.45	1.75		
	122077B		0.65	**1.20***	
310-320P	122078A	0.60	0.92		
	122078B		0.62	**0.78***	
320-330P	122079A	0.45	0.54		
	122079B		1.09	**0.88***	
330-340P	122080A	0.60	0.74		
	122080B		0.76	**0.75***	
340-350P	122081A	0.50	0.61		
	122081B		0.60	**0.60***	

*** A & B Weighted Average**

350-360P	122082A	0.45	0.67		
	122082B		0.83	**0.73***	
360-370P	122083A	0.38	0.82		0.17
	122083B		0.71	**0.77***	0.08
370-380P	122084A	0.05	0.76		0.06
	122084B		0.68	**0.73***	0.08
380-390P	122085A CPY/BN	0.55	0.65		0.08
	122085B		2.14	**1.41***	0.26
390-400P	122086A	0.40	0.67		0.09
	122086B		0.63	**0.65***	0.08
400-410P	122087A	2.30	0.68		0.10
	122087B		0.56	**0.62***	0.09
410-420P	122088A	0.75	0.74		0.10
	122088B		0.76	**0.75***	0.10
420-430P	122089A	0.60	0.68		0.09
	122089B		0.69	**0.68***	0.10
430-440P	122090A	0.57	0.79		0.11
	122090B		0.61	**0.71***	0.08
440-450P	122091A	1.05	0.47		0.07
	122091B		0.52	**0.49***	0.11
450-460P	122092A	0.47	0.54		0.11
	122092B		0.24	**0.43***	0.02
460-470P	122093A	0.55	0.15		0.0
	122093B		0.15	**0.15***	0.04
470-480P	122094A	0.50	0.49		0.07
	122094B		0.38	**0.45***	0.07
480-490P	122095A	0.50	0.47		0.08
	122095B		0.40	**0.43***	0.07
490-500P	122096A	0.35	0.20		0.02
	122096B		0.27	**0.24***	0.04

*** A & B Weighted Average**

DDH-93-3	SAMPLE #	Placer % Total Cu (65-2)	Eco-Tech % Total Cu		Eco-Tech % Oxide Cu
030-040X	122501A		1.51		1.48
	122501B		1.44	**1.48***	1.43
040-050X	122502A	0.80	1.06		1.00
	122502B		1.86	**1.45***	1.84
050-060X	122503A	0.90	2.26		2.25
	122503B		1.05	**1.70***	1.03
060-070X	122504A	0.93	0.46		0.39
	122504B		0.53	**0.50***	0.53
070-080X	122505A	0.60	0.52		0.51
	122505B		0.46	**0.49***	0.41
080-090X	122506A	0.70	0.57		0.56
	122506B		0.49	**0.53***	0.43
090-100X	122507A	1.30	0.52		0.52
	122507B		0.38	**0.47***	0.36
100-110X	122508A	1.50	0.39		0.35
	122508B		0.38	**0.36***	0.28
110-120X	122509A	1.30	0.40		0.33
	122509B		0.46	**0.43***	0.38
120-130X	122510A	0.86	0.31		0.22
	122510B		0.39	**0.35***	0.35
130-140X	122511A	0.80	0.32		0.31
	122511B		0.41	**0.37***	0.38
140-150X	122512A	0.70	0.47		0.45
	122512B		0.38	**0.43***	0.28
150-160X	122513A	0.70	0.23		0.17
	122513B		0.18	**0.20***	0.14
160-170X	122514A	0.45	0.25		0.20
	122514B		0.29	**0.27***	0.29

*** A & B Weighted Average**

170-180X	122515A	0.30	0.29		0.27
	122515B		0.26	**0.27***	0.23
180-190X	122516A cuprite	0.35	0.33		0.27
	122516B		0.16	**0.25***	0.08
190-200X	122517A	0.50	0.20		0.14
	122517B		0.23	**0.21***	0.16
200-210X	122518A native	0.60	0.29		0.15
	122518B		0.33	**0.31***	0.19
210-220XP	122519A	0.70	0.20		0.07
	122519B		0.27	**0.23***	0.10
220-230P	122520A	0.60	0.38		
	122520B		0.32	**0.35***	
230-240P	122521A	0.57	0.37		
	122521B		0.28	**0.33***	
240-250P	122522A	0.45	0.46		
	122522B		0.34	**0.40***	
250-260P	122523A	0.55	0.37		
	122523B		0.33	**0.35***	
260-270P	122524A	0.50	0.29		
	122524B		0.24	**0.27***	
270-280P	122525A	0.45	0.42		
	122525B		0.48	**0.45***	
280-290P	122526A	0.55	0.53		
	122526B		0.53	**0.53***	
290-300P	122527A	0.50	0.43		
	122527B		0.37	**0.40***	

*** A & B Weighted Average**

DDH-93-4	SAMPLE #	Placer % Total Cu (65-6)	Eco-Tech % Total Cu		Eco-Tech % Oxide Cu
014-028X		0.34			
028-038X	122551A		0.64		0.62
	122551B	0.62	0.63	**0.64***	0.62
038-048X	122552A	1.27	0.52		0.51
	122552B		0.80	**0.64***	0.79
048-058X	122553A	0.60	0.50		0.49
	122553B		0.62	**0.56***	0.61
058-068X	122554A	0.66	0.72		0.71
	122554B		0.87	**0.80***	0.88
068-078X	122555A	0.68	0.84		0.82
	122555B		0.47	**0.67***	0.46
078-089X	122556A	0.62	0.48		0.46
	122556B		0.44	**0.46***	0.42
089-098X	122557A	0.34	0.34		0.34
	122557B		0.31	**0.33***	0.30
098-108X/P	122558A	0.54	0.61		0.60
	122558B		0.48	**0.56***	0.27
108-118P	122559A	.81	0.47		0.06
	122559B		0.63	**0.55***	0.08
118-128P	122560A	0.79	0.46		
	122560B		0.67	**0.55***	
128-138P	122561A	1.16	0.51		
	122561B		0.67	**0.58***	
138-148P	122562A	0.90	0.54		
	122562B		0.61	**0.58***	
148-158P	122563A	0.44	0.71		
	122563B		0.53	**0.63***	

*** A & B Weighted Average**

158-168P	122564A	0.40	0.60	
	122564B		0.45	**0.53***
168-178P	122565A	0.50	0.48	
	122565B		0.44	**0.46***
178-188P	122566A	0.46	0.51	
	122566B		0.65	**0.58***
188-198P	122567A	0.58	0.57	
	122567B		0.44	**0.50***
198-212P	122568A	0.54	0.32	
	122568B		0.28	**0.30***

*** A & B Weighted Average**

DDH-93-5	SAMPLE #	Eco-Tech % Total Cu		Eco-Tech % Oxide Cu
Minus 60 degree dip, north west strike, no Placer equivalent				
029-039X	122569A	0.97		0.96
	122569B	0.64	**0.84***	0.69
039-049X	122570A	1.06		1.04
	122570B	1.35	**1.19***	1.33
049-059X	122571A	1.53		1.53
	122571B	2.22	**1.82***	2.19
059-069X	122572A	1.68		1.67
	122572B	1.35	**1.53***	1.34
069-079X	122573A	1.07		1.06
	122573B	1.09	**1.08***	1.07
079-089X	122574A	0.77		0.76
	122574B	0.79	**0.78***	0.77
089-099X	122575A	0.83		0.80
	122575B	0.92	**0.86***	0.92
099-109X	122576A	0.78		0.77
	122576B	1.02	**0.90***	1.00
109-119X	122577A	0.83		0.80
	122577B	1.28	**1.05***	1.27
119-129X	122578A	1.49		1.44
	122578B	0.58	**1.49***	0.54
129-139X	122579A	0.52		0.51
	122579B	0.44	**0.48***	0.42
139-149X	122580A	0.67		0.65
	122580B	0.94	**0.78***	0.91
149-159X	122581A	0.69		0.68
	122581B	0.73	**0.71***	0.71
159-169X	122582A	1.24		1.22
	122582B	0.86	**1.02***	0.88

*** A & B Weighted Average**

169-179X	122583A	0.60		0.59
122583B		0.76	**0.68***	0.68
179-189X	122584A	0.69		0.69
	122584B	0.92	**0.80***	0.88
189-200X	122585A	0.49		0.48
	122585B	0.46	**0.48***	0.44
200-209X	122586A	0.50		0.48
	122586B	0.49	**0.50***	0.48
209-219X	122587A	0.65		0.57
	122587B	0.60	**0.63***	0.36
219-229X	122588A	0.84		
	122588B	0.67	**0.75***	
229-239X/P	122589A	0.69		
	122589B	0.48	**0.60***	
239-249P	122590A	0.52		
	122590B	0.26	**0.36***	
249-259P	122591A	0.24		
	122591B	0.23	**0.24***	
259-269P	122592A	0.20		
	122592B	0.19	**0.20***	
269-279P	122593A	0.29		
	122593B	0.34	**0.29***	
279-289P	122594A	0.60		
	122594B	0.92	**0.73***	
289-299P	122595A	0.46		
	122595B	0.36	**0.40***	
299-309P	122596A	0.40		
	122596B	0.53	**0.45***	
309-318P	122597A	0.50		
	122597B	0.48	**0.49***	

*** A & B Weighted Average**

APPENDIX THREE

CERTIFICATES OF ASSAY - ECO TECH LABS

Eco-Tech LABORATORIES LTD.

ASSAYING
GEOCHEMISTRY
ANALYTICAL CHEMISTRY
ENVIRONMENTAL TESTING

10041 E. Trans Canada Hwy., R.R. 2, Kamloops, B.C. V2C 2J3 Phone (604) 573-5700
Fax (604) 573-4557

OCTOBER 20, 1993

CERTIFICATE OF ANALYSIS ETK 93-336

GETTY COPPER CORPORATION
1000 AUSTIN AVENUE
COQUITLAM, B.C.
V3K 3P3

ATTENTION: MR. JOHN LEPINSKI

SAMPLE IDENTIFICATION: 48 CORE sample received AUGUST 27, 1993

ET#	Description		Au (ppb)
33	- 122520 A	11.75 lbs.	10
35	- 122521 A	12.25 lbs.	10
37	- 122522 A	11.5 lbs.	10
39	- 122523 A	12.5 lbs.	10
41	- 122524 A	11.5 lbs.	10
43	- 122525 A	12.25 lbs.	5
45	- 122526 A	9.5 lbs.	5
47	- 122527 A	11 lbs.	5

NOTE: < = LESS THAN

ECO-TECH LABORATORIES LTD.
FRANK J. PEZZOTTI, A.Sc.T.
B.C. Certified Assayer

SC93/Getty

Eco-Tech LABORATORIES LTD.

ASSAYING
GEOCHEMISTRY
ANALYTICAL CHEMISTRY
ENVIRONMENTAL TESTING

10041 E. Trans Canada Hwy., R.R. #2, Kamloops, B.C. V2C 2J3 Phone (604) 573-5700
Fax (604) 573-4557

SEPTEMBER 28, 1993

CERTIFICATE OF ASSAY ETK 93-336

GETTY COPPER CORPORATION
1000 AUSTIN AVENUE
COQUITLAM, B.C.
V3K 3P3

ATTENTION: MR. JOHN LEPINSKI

SAMPLE IDENTIFICATION: 48 CORE sample received AUGUST 27, 1993

ET#	Description		Ag (g/t)	Ag (oz/t)	Cu Oxide (%)	Cu (%)	Cu% Average Value
1	- 122504 A	9.5 lbs.	.2	.01	.39	.46	.50
2	- 122504 B	9.5 lbs.	.3	.01	.53	.53	
3	- 122505 A	11.25 lbs.	.2	.01	.51	.52	.49
4	- 122505 B	10.25 lbs.	.2	.01	.41	.46	
5	- 122506 A	11.5 lbs.	.1	<.01	.56	.57	.53
6	- 122506 B	10.25 lbs.	.3	.01	.43	.49	
7	- 122507 A	12 lbs.	.2	.01	.52	.52	.47
8	- 122507 B	7.25 lbs.	.1	<.01	.36	.38	
9	- 122508 A	9.25 lbs.	.2	.01	.35	.39	.36
10	- 122508 B	11.25 lbs.	.2	.01	.28	.33	
11	- 122509 A	11 lbs.	.4	.01	.33	.40	.43
12	- 122509 B	10.25 lbs.	.1	<.01	.38	.46	
13	- 122510 A	11.25 lbs.	.1	<.01	.22	.31	.35
14	- 122510 B	9.5 lbs.	.2	.01	.35	.39	
15	- 122511 A	9.75 lbs.	.1	<.01	.31	.32	.37
16	- 122511 B	11.75 lbs.	.1	<.01	.38	.41	
17	- 122512 A	12.75 lbs.	.1	<.01	.45	.47	.43
18	- 122512 B	8.5 lbs.	.3	.01	.28	.38	
19	- 122513 A	10 lbs.	.2	.01	.17	.23	.20
20	- 122513 B	12 lbs.	.1	<.01	.14	.18	
21	- 122514 A	11.25 lbs.	.1	<.01	.20	.25	.27
22	- 122514 B	10.25 lbs.	.1	<.01	.24	.29	
23	- 122515 A	11.5 lbs.	.1	<.01	.27	.29	.27
24	- 122515 B	11.75 lbs.	.1	<.01	.23	.26	
25	- 122516 A	11.5 lbs.	.2	.01	.27	.33	.25
26	- 122516 B	10 lbs.	.2	.01	.08	.16	

FRANK J. PEZZOTTI, A.Sc.T. B.C. Certified Assayer

GETTY COPPER CORPORATION ETK 93-336 SEPTEMBER 28, 1993

ET#	Description		Ag (g/t)	Ag (oz/t)	Mo (%)	Cu Oxide (%)	Cu (%)	Cu% Average Value
27	- 122517 A	13.25 lbs.	.3	.01	-	.1	.20	.21
28	- 122517 B	11.5 lbs.	.4	.01	-	.2	.23	
29	- 122518 A	11 lbs.	.5	.02	-	.2	.29	.31
30	- 122518 B	9 lbs.	.2	.01	-	.2	.33	
31	- 122519 A	11.75 lbs.	.2	.01	-	.1	.20	.23
32	- 122519 B	11.5 lbs.	.3	.01	-	.10	.27	
33	- 122520 A	11.75 lbs.	.6	.02	.003	-	.38	.35
34	- 122520 B	12.5 lbs.	.5	.02	<.001	-	.32	
35	- 122521 A	12.25 lbs.	.7	.02	<.001	-	.37	.33
36	- 122521 B	10.5 lbs.	.5	.02	.001	-	.28	
37	- 122522 A	11.5 lbs.	1.4	.04	<.001	-	.46	.40
38	- 122522 B	13.25 lbs.	.7	.02	<.001	-	.34	
39	- 122523 A	12.5 lbs.	.5	.02	<.001	-	.37	.35
40	- 122523 B	12.5 lbs.	.4	.01	<.001	-	.33	
41	- 122524 A	11.5 lbs.	.3	.01	.003	-	.29	.27
42	- 122524 B	11.5 lbs.	.2	.01	.002	-	.24	
43	- 122525 A	12.25 lbs.	.9	.03	.004	-	.42	.45
44	- 122525 B	11.25 lbs.	1.4	.04	.002	-	.48	
45	- 122526 A	9.5 lbs.	2.1	.06	<.001	-	.53	.53
46	- 122526 B	10.5 lbs.	2.6	.08	.001	-	.53	
47	- 122527 A	11 lbs.	1.2	.04	<.001	-	.43	.40
48	- 122527 B	11.25 lbs.	.1	<.01	.001	-	.37	

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OCTOBER 20, 1993

CERTIFICATE OF ANALYSIS ETK 93-336

GETTY COPPER CORPORATION
1000 AUSTIN AVENUE
COQUITLAM, B.C.
V3K 3P3

ATTENTION: MR. JOHN LEPINSKI

SAMPLE IDENTIFICATION: 48 CORE sample received AUGUST 27, 1993

ET#	Description		Au (ppb)
33	122520 A	11.75 lbs.	10
35	122521 A	12.25 lbs.	10
37	122522 A	11.5 lbs.	10
39	122523 A	12.5 lbs.	10
41	122524 A	11.5 lbs.	10
43	122525 A	12.25 lbs.	5
45	122526 A	9.5 lbs.	5
47	122527 A	11 lbs.	5

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SEPTEMBER 22, 1993

CERTIFICATE OF ASSAY ETK 93-286-A

GETTY COPPER CORPORATION
1000 AUSTIN AVENUE
COQUITLAM, B.C.
V3K 3P3

ATTENTION: MR. JOHN LEPINSKI

SAMPLE IDENTIFICATION: 22 CORE samples received AUGUST 20, 1993

COPPER SCREENS & RESPLIT:
From the jaw crushed material, two replits were taken A + B. On the A pulp a metallic Copper was performed; on the B pulp a total Copper assay was performed.

		SCREEN		CALCULATED VALUE	TOTAL COPPER
ET#	Description	-140	+140		
1 A-	120001 (2x)	.75	.45	.75	-
1 B-	120001 (2x)	-	-	-	.76
5 A-	120005 (2x)	.7	.40	.66	-
5 B-	120005 (2x)	-	-	-	.67
21 A-	120021 (2x)	.25	.13	.25	-
21 B-	120021 (2x)	-	-	-	.27
22 A-	120022 (2x)	.14	6.08	.14	-
22 B-	120022 (2x)	-	-	-	.15

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SEPTEMBER 7, 1993

CERTIFICATE OF ASSAY ETK 93-286

GETTY COPPER CORPORATION
1000 AUSTIN AVENUE
COQUITLAM, B.C.
V3K 3P3

ATTENTION: MR. JOHN LEPINSKI

SAMPLE IDENTIFICATION: 22 CORE sample received AUGUST 20, 1993

ET#	Description	Ag (g/t)	Ag (oz/t)	Cu-Total (%)	Cu Oxide (%)	Mo (%)
1-	120001 (2x)	.4	.01	.76	.65	.002
2-	120002 (2x)	.7	.02	.59	.57	.002
3-	120003 (2x)	.3	.01	.55	.50	.001
4-	120004 (2x)	.4	.01	.53	.44	<.001
5-	120005 (2x)	.4	.01	.78	.69	<.001
6-	120006 (2x)	.3	.01	.42	.38	<.001
7-	120007 (2x)	.1	.00	.45	.43	<.001
8-	120008 (2x)	.2	.01	.44	.44	<.001
9-	120009 (2x)	.3	.01	.25	.23	<.001
10-	120010 (2x)	.3	.01	.28	.22	<.001
11-	120011 (2x)	.2	.01	.5	.45	.001
12-	120012 (2x)	.6	.02	.44	.39	<.001
13-	120013 (2x)	.8	.02	.35	.30	<.001
14-	120014 (2x)	.6	.02	.61	.58	<.001
15-	120015 (2x)	.3	.01	.52	.50	<.001
16-	120016 (2x)	.2	.01	.4	.39	<.001
17-	120017 (2x)	.3	.01	.41	.42	<.001
18-	120018 (2x)	.2	.01	.33	.33	<.001
19-	120019 (2x)	.2	.01	.41	.40	<.001
20-	120020 (2x)	.4	.01	.25	.25	<.001
21-	120021 (2x)	.4	.01	.25	.24	.001
22-	120022 (2x)	.3	.01	.16	.13	<.001

NOTE: < = LESS THAN

cc: Gower Thompson & Assc.Ltd.
Attn: Mr. Stephen Gower

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SEPTEMBER 20, 1993

CERTIFICATE OF ASSAY ETK 93-287

GETTY COPPER CORPORATION
1000 AUSTIN AVENUE
COQUITLAM, B.C.
V3K 3P3

ATTENTION: MR. JOHN LEPINSKI

SAMPLE IDENTIFICATION: 24 CORE sample received AUGUST 23, 1993

ET#	Description	Ag (g/t)	Ag (oz/t)	Cu Oxide (%)	Cu (%)	Mo (%)
1-	120023 (2)	.2	.01	.14	.16	.003
2-	120024 (2)	<.1	<.01	.13	.16	.001
3-	120025 (2)	<.1	<.01	.20	.45	.002
4-	120026 (2)	.2	.01	.17	.44	.001
5-	120027 (2)	<.1	<.01	.31	.30	<.001
6-	120028 (2)	<.1	<.01	.39	.40	.001
7-	120029 (2)	.2	.01	.50	.55	.001
8-	120030 (2)	.2	.01	.29	.36	<.001
9-	120031 (2)	.1	<.01	.33	.43	<.001
10-	120032 (2)	<.1	<.01	.40	.50	<.001
11-	120033 (2)	<.1	<.01	.46	.50	<.001
12-	120034 (2)	.1	<.01	.36	.48	<.001
13-	120035 (2)	<.1	<.01	.28	.34	.001
14-	120036 (2)	<.1	<.01	.19	.28	<.001
15-	120037 (2)	.1	<.01	.23	.31	.001
16-	120038 (2)	.2	.01	.26	.35	.001
17-	120039 (2)	<.1	<.01	.20	.40	<.001
18-	120040 (2)	.1	<.01	.10	.52	.001
19-	122051 (2)	.2	.01	1.03	1.03	.001
20-	122052 (2)	.1	<.01	.51	.54	<.001
21-	122053 (2)	<.1	<.01	.41	.49	<.001
22-	122054 (2)	<.1	<.01	.67	.68	<.001
23-	122055 (2)	<.1	<.01	.36	.44	<.001
24-	122056 (2)	<.1	<.01	.40	.41	.001

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CERTIFICATE OF ASSAY ETK 93-287-A

GETTY COPPER CORPORATION
1000 AUSTIN AVENUE
COQUITLAM, B.C.
V3K 3P3

ATTENTION: MR. JOHN LEPINSKI

SAMPLE IDENTIFICATION: 24 CORE sample received AUGUST 23, 1993

COPPER SCREENS & RESPLIT:
From the jaw crushed material, two replits were taken A + B.
On the A pulp a metallic Copper was performed; on the B pulp
a total Copper assay was performed.

		SCREENED VALUES			UNSCREENED VALUES
		SCREEN		CALCULATED VALUE	TOTAL COPPER
ET#	Description	-140	+140		
5 A-	120027 (2)	.31	.14	.31	-
5 B-	120027 (2)	-	-	-	.33
6 A-	120028 (2)	.4	.15	.40	-
6 B-	120028 (2)	-	-	-	.40
7 A-	120029 (2)	.52	.21	.52	-
7 B-	120029 (2)	-	-	-	.57
8 A-	120030 (2)	.34	.15	.34	-
8 B-	120030 (2)	-	-	-	.30
9 A-	120031 (2)	.41	.28	.41	-
9 B-	120031 (2)	-	-	-	.42
10 A-	120032 (2)	.49	.17	.48	-
10 B-	120032 (2)	-	-	-	.49
11 A-	120033 (2)	.49	.20	.49	-
11 B-	120033 (2)	-	-	-	.53
12 A-	120034 (2)	.46	.23	.46	-
12 B-	120034 (2)	-	-	-	.46
13 A-	120035 (2)	.32	.53	.32	-
13 B-	120035 (2)	-	-	-	.36
14 A-	120036 (2)	.30	.45	.30	-
14 B-	120036 (2)	-	-	-	.30
15 A-	120037 (2)	.36	.37	.36	-
15 B-	120037 (2)	-	-	-	.35

FRANK J. PEZZOTTI, A.Sc.T. B.C. Certified Assayer

GETTY COPPER CORPORATION ETK 93-287-A SEPTEMBER 24, 1993

ET#	Description	SCREENED VALUES: SCREEN -140	SCREENED VALUES: SCREEN +140	SCREENED VALUES: CALCULATED VALUE	UNSCREENED VALUES: TOTAL COPPER
16 A-	120038 (2)	.35	.27	.35	-
16 B-	120038 (2)	-	-	-	.35
17 A-	120039 (2)	.33	.20	.33	-
17 B-	120039 (2)	-	-	-	.33
18 A-	120040 (2)	.52	.31	.51	-
18 B-	120040 (2)	-	-	-	.53

NOTE: < = LESS THAN

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OCTOBER 20, 1993

CERTIFICATE OF ANALYSIS ETK 93-335

GETTY COPPER CORPORATION
1000 AUSTIN AVENUE
COQUITLAM, B.C.
V3K 3P3

ATTENTION: MR. JOHN LEPINSKI

SAMPLE IDENTIFICATION: 52 CORE sample received AUGUST 25, 1993

ET#	Description			Au (ppb)
1	- 122057	A	10 lbs.	5
3	- 122058	A	11 lbs.	20
5	- 122059	A	10.25 lbs.	10
7	- 122060	A	11.5 lbs.	15
9	- 122061	A	10.5 lbs.	5
11	- 122062	A	11 lbs.	5
13	- 122063	A	11.75 lbs.	10
15	- 122064	A	10.25 lbs.	5
17	- 122065	A	11 lbs.	10
19	- 122066	A	12 lbs.	10
21	- 122067	A	10 lbs.	30
23	- 122068	A	10.5 lbs.	25
25	- 122069	A	11.75 lbs.	50
27	- 122070	A	12.75 lbs.	60
29	- 122071	A	12.5 lbs.	20
31	- 122072	A	10.75 lbs.	25
33	- 122073	A	11 lbs.	15
35	- 122074	A	10 lbs.	15
37	- 122075	A	11.75 lbs.	25
39	- 122076	A	11.25 lbs.	10
41	- 122077	A	10 lbs.	65
43	- 122078	A	11.5 lbs.	60
45	- 122079	A	7.5 lbs.	25
47	- 122080	A	14 lbs.	10
49	- 122081	A	13.75 lbs.	30
51	- 122082	A	8.5 lbs.	30

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SEPTEMBER 27, 1993

CERTIFICATE OF ASSAY ETK 93-335

GETTY COPPER CORPORATION
1000 AUSTIN AVENUE
COQUITLAM, B.C.
V3K 3P3

ATTENTION: MR. JOHN LEPINSKI

SAMPLE IDENTIFICATION: 52 CORE sample received AUGUST 25, 1993

ET#	Description		Ag (g/t)	Ag (oz/t)	Cu (%)	Mo (%)	Cu % Average Value
1	122057 A	10 lbs.	.2	.01	.37	<.001	.38
2	122057 B	9.75 lbs.	.4	.01	.39	<.001	
3	122058 A	11 lbs.	.2	.01	.38	<.001	.32
4	122058 B	11.25 lbs.	.2	.01	.27	.002	
5	122059 A	10.25 lbs.	.2	.01	.26	.001	.30
6	122059 B	11 lbs.	.4	.01	.34	.001	
7	122060 A	11.5 lbs.	.1	<.01	.29	<.001	.31
8	122060 B	11 lbs.	.1	<.01	.34	<.001	
9	122061 A	10.5 lbs.	.1	<.01	.30	.001	.35
10	122061 B	10.5 lbs.	.1	<.01	.40	<.001	
11	122062 A	11 lbs.	.1	<.01	.38	<.001	.35
12	122062 B	11.5 lbs.	.1	<.01	.32	.001	
13	122063 A	11.75 lbs.	.1	<.01	.26	.001	.27
14	122063 B	9 lbs.	.1	<.01	.29	<.001	
15	122064 A	10.25 lbs.	.5	.02	.46	.002	.46
16	122064 B	9.5 lbs.	.7	.02	.47	<.001	
17	122065 A	11 lbs.	.5	.02	.34	<.001	.59
18	122065 B	11 lbs.	.6	.02	.84	.003	
19	122066 A	12 lbs.	.9	.03	.37	<.001	.38
20	122066 B	12.5 lbs.	1.1	.03	.39	<.001	
21	122067 A	10 lbs.	1.3	.04	.52	.002	.56
22	122067 B	12 lbs.	1.0	.03	.59	.002	
23	122068 A	10.5 lbs.	.7	.02	.43	<.001	.32
24	122068 B	13 lbs.	.2	.01	.23	.002	
25	122069 A	11.75 lbs.	.7	.02	.51	.001	.50
26	122069 B	11.75 lbs.	.6	.02	.49	.001	

FRANK J. PEZZOTTI, A.Sc.T. B.C. Certified Assayer

GETTY COPPER CORPORATION ETK 93-335   SEPTEMBER 27, 1993

PAGE 2

ET#	Description		Ag (g/t)	Ag (oz/t)	Cu (%)	Mo (%)	Cu% Average Value
27 -	122070 A	12.75 lbs.	1.6	.05	.86	<.001	.61
28 -	122070 B	12 lbs.	.2	.01	.35	.001	
29 -	122071 A	12.5 lbs.	.2	.01	.38	<.001	.35
30 -	122071 B	10.5 lbs.	.4	.01	.32	<.002	
31 -	122072 A	10.75 lbs.	.6	.02	.41	.001	.40
32 -	122072 B	10.5 lbs.	.4	.01	.38	.002	
33 -	122073 A	11 lbs.	.6	.02	.34	.002	.31
34 -	122073 B	9.5 lbs.	.3	.01	.27	.008	
35 -	122074 A	10 lbs.	.4	.01	.28	<.001	.34
36 -	122074 B	9 lbs.	1.1	.03	.41	<.001	
37 -	122075 A	11.75 lbs.	1.5	.04	.49	<.001	.47
38 -	122075 B	7.5 lbs.	1.8	.05	.44	<.001	
39 -	122076 A	11.25 lbs.	2.2	.06	.44	.590	.48
40 -	122076 B	10.25 lbs.	1.9	.06	.52	.001	
41 -	122077 A	10 lbs.	7.1	.21	1.75	.001	1.20
42 -	122077 B	10 lbs.	2.1	.06	.65	.001	
43 -	122078 A	11.5 lbs.	3.2	.09	.92	.002	.78
44 -	122078 B	10 lbs.	1.7	.05	.62	.001	
45 -	122079 A	7.5 lbs.	1.3	.04	.54	<.001	.88
46 -	122079 B	12.5 lbs.	3.0	.09	1.09	.003	
47 -	122080 A	14 lbs.	2.0	.06	.74	.004	.75
48 -	122080 B	9 lbs.	2.1	.06	.76	.002	
49 -	122081 A	13.75 lbs.	1.6	.05	.61	.001	.60
50 -	122081 B	17.25 lbs.	1.4	.04	.60	.002	
51 -	122082 A	8.5 lbs.	1.9	.06	.67	.007	.73
52 -	122082 B	5.5 lbs.	2.3	.07	.83	.002	

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SEPTEMBER 24, 1993

CERTIFICATE OF ASSAY ETK 93-334

GETTY COPPER CORPORATION
1000 AUSTIN AVENUE
COQUITLAM, B.C.
V3K 3P3

ATTENTION: MR. JOHN LEPINSKI

SAMPLE IDENTIFICATION: 34 CORE sample received AUGUST 26, 1993

ET#	Description	Ag (g/t)	Ag (oz/t)	Cu Oxide (%)	Cu (%)	Mo (%)	Cu% Average Value
1	122083 A 13.5 lbs.	2.5	.07	.17	.82	<.001	.77
2	122083 B 9.5 lbs.	2.2	.06	.08	.71	.004	
3	122084 A 16.5 lbs.	2.0	.06	.06	.76	<.001	.73
4	122084 B 10.5 lbs.	2.2	.06	.08	.68	.002	
5	122085 A 12.5 lbs.	2.2	.06	.08	.65	.001	1.41
6	122085 B 13 lbs.	7.6	.22	.26	2.14	.002	
7	122086 A 10.25 lbs.	2.3	.07	.09	.67	.002	.65
8	122086 B 14.25 lbs.	2.1	.06	.08	.63	.001	
9	122087 A 11.5 lbs.	2.2	.06	.10	.68	<.001	.62
10	122087 B 12 lbs.	1.9	.06	.09	.56	.001	
11	122088 A 12.5 lbs.	2.4	.07	.09	.74	<.001	.75
12	122088 B 13.75 lbs.	2.6	.08	.10	.76	.001	
13	122089 A 12.75 lbs.	2.3	.07	.09	.68	<.001	.68
14	122089 B 10.75 lbs.	2.3	.07	.10	.69	.002	
15	122090 A 11.25 lbs.	3.3	.10	.11	.79	<.001	.71
16	122090 B 9.5 lbs.	2.0	.06	.08	.61	.001	
17	122091 A 12 lbs.	1.7	.05	.07	.47	<.001	.49
18	122091 B 10 lbs.	1.9	.06	.11	.52	.001	
19	122092 A 12 lbs.	2.4	.07	.11	.54	.001	.43
20	122092 B 6.5 lbs.	.2	.01	.02	.24	.001	
21	122093 A 12.5 lbs.	.6	.02	.03	.15	.002	.15
22	122093 B 12.75 lbs.	.6	.02	.04	.15	<.001	
23	122094 A 10.75 lbs.	1.9	.06	.07	.49	<.001	.45
24	122094 B 6.25 lbs.	1.0	.03	.07	.38	.003	
25	122095 A 10.25 lbs.	1.6	.05	.08	.47	<.001	.43
26	122095 B 11.25 lbs.	.9	.03	.07	.40	<.001	
27	122096 A 11 lbs.	.1	<.01	.02	.20	<.001	.24
28	122096 B 12.25 lbs.	.5	.02	.04	.27	<.001	
29	122501 A 11.75 lbs.	<.1	<.01	1.48	1.51	.005	1.48
30	122501 B 7.25 lbs.	.2	.01	1.43	1.44	.004	

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GETTY COPPER CORPORATION SEPTEMBER 24, 1993

ET#	Description	Ag (g/t)	Ag (oz/t)	Cu Oxide (%)	Cu (%)	Mo (%)	Cu% Average Value
31	- 122502 A 11.75 lbs.	.2	.01	1.00	1.06	.002	1.45
32	- 122502 B 11 lbs.	.3	.01	1.84	1.86	.005	
33	- 122503 A 11.5 lbs.	.3	.01	2.25	2.26	.007	1.70
34	- 122503 B 10 lbs.	.5	.02	1.03	1.05	.003	

NOTE: < = LESS THAN

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Fax (604) 573-4557

SEPTEMBER 27, 1993

CERTIFICATE OF ASSAY ETK 93-339

GETTY COPPER CORPORATION
1000 AUSTIN AVENUE
COQUITLAM, B.C.
V3K 3P3

ATTENTION: MR. JOHN LEPINSKI

SAMPLE IDENTIFICATION: 94 CORE sample received AUGUST 31, 1993

ET#	Description	Ag (g/t)	Ag (oz/t)	Cu Oxide (%)	Cu (%)	Mo (%)	Cu % Average Value
1	12551 A 12.5 lbs.	-	-	.62	.64	-	.64
2	12551 B 11.25 lbs.	-	-	.62	.63	-	
3	12552 A 11.75 lbs.	-	-	.51	.52	-	.64
4	12552 B 9.25 lbs.	-	-	.79	.80	-	
5	12553 A 11.75 lbs.	-	-	.49	.50	-	.56
6	12553 B 10.5 lbs.	-	-	.61	.62	-	
7	12554 A 12 lbs.	-	-	.71	.72	-	.80
8	12554 B 12.75 lbs.	-	-	.88	.87	-	
9	12555 A 13 lbs.	-	-	.82	.84	-	.67
10	12555 B 10.5 lbs.	-	-	.46	.47	-	
11	12556 A 11.5 lbs.	-	-	.46	.48	-	.46
12	12556 B 13.5 lbs.	-	-	.42	.44	-	
13	12557 A 10 lbs.	-	-	.34	.34	-	.33
14	12557 B 9.75 lbs.	-	-	.30	.31	-	
15	12558 A 14 lbs.	-	-	.60	.61	-	.56
16	12558 B 9 lbs.	-	-	.27	.48	-	
17	12559 A 11.25 lbs.	-	-	.06	.47	-	.55
18	12559 B 11.5 lbs.	-	-	.08	.63	-	
19	12560 A 13.25 lbs.	.5	.02	-	.46	.006	.55
20	12560 B 10 lbs.	1.0	.03	-	.67	<.001	
21	12561 A 12 lbs.	.4	.01	-	.51	.006	.58
22	12561 B 8.25 lbs.	.8	.02	-	.67	.004	
23	12562 A 10.25 lbs.	.5	.02	-	.54	.008	.58
24	12562 B 11.75 lbs.	.9	.03	-	.61	.012	
25	12563 A 12 lbs.	.7	.02	-	.71	.009	.63
26	12563 B 9 lbs.	.5	.02	-	.53	.007	

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FRANK J. PEZZOTTI, A.Sc.T. B.C. Certified Assayer

GETTY COPPER CORPORATION ETK 93-339 SEPTEMBER 27, 1993

PAGE 2

ET#	Description	Ag (g/t)	Ag (oz/t)	Cu Oxide (%)	Cu (%)	Mo (%)	Cu % Average Value
27	- 12564 A 11.75 lbs.	.5	.02	-	.60	.003	.53
28	- 12564 B 10.5 lbs.	.2	.01	-	.45	.006	
29	- 12565 A 11.25 lbs.	.4	.01	-	.48	.006	.46
30	- 12565 B 10.5 lbs.	.6	.02	-	.44	.022	
31	- 12566 A 11.5 lbs.	.5	.02	-	.51	.017	.58
32	- 12566 B 11.5 lbs.	.5	.02	-	.65	.033	
33	- 12567 A 9.5 lbs.	.4	.01	-	.57	.060	.50
34	- 12567 B 11.5 lbs.	.1	<.01	-	.44	.009	
35	- 12568 A 17.25 lbs.	.1	<.01	-	.32	.003	.30
36	- 12568 B 11 lbs.	.1	<.01	-	.28	.004	
37	- 12569 A 8.5 lbs.	-	-	.96	.97	-	.84
38	- 12569 B 5.5 lbs.	-	-	.69	.64	-	
39	- 12570 A 10.5 lbs.	-	-	1.04	1.06	-	1.19
40	- 12570 B 8.75 lbs.	-	-	1.33	1.35	-	
41	- 12571 A 12 lbs.	-	-	1.53	1.53	-	1.82
42	- 12571 B 8.75 lbs.	-	-	2.19	2.22	-	
43	- 12572 A 12.5 lbs.	-	-	1.67	1.68	-	1.53
44	- 12572 B 10.5 lbs.	-	-	1.34	1.35	-	
45	- 12573 A 12.75 lbs.	-	-	1.06	1.07	-	1.08
46	- 12573 B 10.5 lbs.	-	-	1.07	1.09	-	
47	- 12574 A 14.75 lbs.	-	-	.76	.77	-	.78
48	- 12574 B 12 lbs.	-	-	.77	.79	-	
49	- 12575 A 10.5 lbs.	-	-	.80	.83	-	.86
50	- 12575 B 6 lbs.	-	-	.92	.92	-	
51	- 12576 A 11.75 lbs.	-	-	.77	.78	-	.90
52	- 12576 B 11.75 lbs.	-	-	1.00	1.02	-	
53	- 12577 A 10 lbs.	-	-	.80	.83	-	1.05
54	- 12577 B 9.25 lbs.	-	-	1.27	1.28	-	
55	- 12578 A 9.25 lbs.	-	-	1.44	1.49	-	1.49

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GETTY COPPER CORPORATION ETK 93-339 SEPTEMBER 27, 1993

ET#	Description	Ag (g/t)	Ag (oz/t)	Cu Oxide (%)	Cu (%)	Mo (%)	Cu % Average Value
56	- 12578 B 7.75 lbs.	-	-	.54	.58	-	
57	- 12579 A 8.75 lbs.	-	-	.51	.52	-	.48
58	- 12579 B 8 lbs.	-	-	.42	.44	-	
59	- 12580 A 12.75 lbs.	-	-	.65	.67	-	.78
60	- 12580 B 9 lbs.	-	-	.91	.94	-	
61	- 12581 A 9.5 lbs.	-	-	.68	.69	-	.71
62	- 12581 B 11 lbs.	-	-	.71	.73	-	
63	- 12582 A 9 lbs.	-	-	1.22	1.24	-	1.02
64	- 12582 B 13 lbs.	-	-	.88	.86	-	
65	- 12583 A 14.25 lbs.	-	-	.59	.60	-	.68
66	- 12583 B 12.75 lbs.	-	-	.68	.76	-	
67	- 12584 A 12.75 lbs.	-	-	.69	.69	-	.80
68	- 12584 B 11 lbs.	-	-	.88	.92	-	
69	- 12585 A 13.75 lbs.	-	-	.48	.49	-	.48
70	- 12585 B 10.5 lbs.	-	-	.44	.46	-	
71	- 12586 A 11.5 lbs.	-	-	.48	.50	-	.50
72	- 12586 B 9.75 lbs.	-	-	.48	.49	-	
73	- 12587 A 12.25 lbs.	-	-	.57	.65	-	.63
74	- 12587 B 12.25 lbs.	.3	.01	.36	.60	.003	
75	- 12588 A 11 lbs.	.1	<.01	-	.84	.004	.75
76	- 12588 B 13.25 lbs.	.4	.01	-	.67	.008	
77	- 12589 A 15 lbs.	.1	<.01	-	.69	.025	.60
78	- 12589 B 11 lbs.	.1	<.01	-	.48	.017	
79	- 12590 A 9.5 lbs.	.1	<.01	-	.52	.008	.36
80	- 12590 B 15.75 lbs.	.1	<.01	-	.26	.005	
81	- 12591 A 12.25 lbs.	.1	<.01	-	.24	.006	.24
82	- 12591 B 9.75 lbs.	.1	<.01	-	.23	.005	
83	- 12592 A 14 lbs.	.1	<.01	-	.20	.011	.20
84	- 12592 B 7.75 lbs.	.1	<.01	-	.19	.009	
85	- 12593 A 13.25 lbs.	.1	<.01	-	.29	.008	.29

FRANK J. PEZZOTTI, A.Sc.T. B.C. Certified Assayer

GETTY COPPER CORPORATION ETK 93-339 SEPTEMBER 27, 1993

ET#	Description	Ag (g/t)	Ag (oz/t)	Cu Oxide (%)	Cu (%)	Mo (%)	Cu % Average Value
86	- 12593 B 7.25 lbs.	.2	.01	-	.34	.008	
87	- 12594 A 12.75 lbs.	.2	.01	-	.60	.006	.73
88	- 12594 B 8.25 lbs.	.4	.01	-	.92	.005	
89	- 12595 A 9.5 lbs.	.1	<.01	-	.46	.005	.40
90	- 12595 B 15.75 lbs.	.1	<.01	-	.36	.004	
91	- 12596 A 11.5 lbs.	.1	<.01	-	.40	.006	.45
92	- 12596 B 7.25 lbs.	.1	<.01	-	.53	.007	
93	- 12597 A 12 lbs.	.1	<.01	-	.50	.003	.49
94	- 12597 B 8.5 lbs.	.1	<.01	-	.48	.002	

NOTE: < = LESS THAN

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Fax (604) 573-4557

JANUARY 27, 1994

CERTIFICATE OF ASSAY ETK 93-335

GETTY COPPER CORPORATION
1000 AUSTIN AVENUE
COQUITLAM, B.C.
V3K 3P3

ATTENTION: MR. STEPHEN GOWER

SAMPLE IDENTIFICATION: 52 CORE sample received AUGUST 25, 1993
PHONE REQUEST : JANUARY 24, 1994

ET#	Description		Weight	Cu Oxide (%)
1	122057	A	10 lbs.	.33
2	122057	B	9.75 lbs.	.32
3	122058	A	11 lbs.	.30
4	122058	B	11.25 lbs.	.20
5	122059	A	10.25 lbs.	.16
6	122059	B	11 lbs.	.27
7	122060	A	11.5 lbs.	.21
8	122060	B	11 lbs.	.26
9	122061	A	10.5 lbs.	.19
10	122061	B	10.5 lbs.	.35
11	122062	A	11 lbs.	.31
12	122062	B	11.5 lbs.	.26
13	122063	A	11.75 lbs.	.19
14	122063	B	9 lbs.	.19
15	122064	A	10.25 lbs.	.39
16	122064	B	9.5 lbs.	.25
17	122065	A	11 lbs.	.16
18	122065	B	11 lbs.	.13
19	122066	A	12 lbs.	.14
20	122066	B	12.5 lbs.	.11
21	122067	A	10 lbs.	.12
22	122067	B	12 lbs.	.12

NOTE: < = LESS THAN

Bob Miner

ECO-TECH LABORATORIES LTD.
per FRANK J. PEZZOTTI, A.Sc.T.
B.C. Certified Assayer

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APPENDIX FOUR

BOTTLE ROLL TESTING - BEATTIE CONSULTING LTD.

BOTTLE ROLL TESTING
OF SAMPLES FROM
THE GETTY NORTH DEPOSIT

GETTY COPPER CORP.

JANUARY 1994

BEATTIE CONSULTING LTD.

VANCOUVER, B.C. CANADA

BEATTIE CONSULTING LTD.

2955 WEST 38th AVENUE
VANCOUVER, B.C.
V6N 2X2

TEL.(604) 263 0695
FAX.(604) 263 0695

January 26, 1994

Getty Copper Corp.
1000 Austin Ave.
Coquitlam, B.C. V3K 3P3
Canada

ATTENTION: **Mr. J.B. Lepinski**

Dear John,

Enclosed please find my report on the bottle roll testwork which was recently conducted by Process Research Associates Ltd. on the assay rejects from the 1993 drill program. As you will note in the report, the testwork was very encouraging in that it shows consistency in the metallurgical response of samples representing a cross section of the oxide zone in the Getty Deposit.

I look forward to participation in the futher development of this project and would be pleased to discuss the results of the testwork once you have had an opprtunity to review the report.

Yours truly,
BEATTIE CONSULTING LTD.

Dr. M.J.V. Beattie, P. Eng.

PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
M. J. V. BEATTIE

1.0 SUMMARY

Bottle roll leaching testwork has been conducted on a series of drill core rejects from the Getty North Copper deposit. The tests were conducted on composite samples from surface to a depth of 435 feet which had been crushed to nominally minus 3/4 inch although one sample was predominantly minus 6 mesh. The head grade of the composites varied from 0.28 to 1.32 % Cu. The test results demonstrated the following:

1. The copper extraction from the core samples achieved in a 6 day test varied from 67.5% to 92.0% except for one partially oxidized sample which achieved 43.5%. Comparing these results to those for a previous sample for which both bottle and column tests were conducted suggests that a heap leach extraction of 80% should be achievable for oxide ore from the various areas of the Getty North deposit which were tested. For material which is only partially oxidized, such as the deeper material from hole no. 2 (test L4), bacterial oxidation would be required to achieve this extraction.

   The copper extraction obtained from different sections of the deposit is dependent only on the crush size of the rock and the degree of oxidation. For drill hole no. 1 for instance, the extraction in the six day tests was 67.5 to 71.9 % over the entire 435 feet represented by the composite samples.

2. The acid consumption in the bottle roll tests varied from 11.8 to 17.4 kg/tonne except for one sample which required 23.8 kg/tonne. Although limited data are available to correlate the bottle results to those to be achieved in heap leaching of material from this deposit, it appears that an acid consumption of 25 kg/tonne may be a reasonable expectation based on results to date. Optimization of operating procedures through further testing holds forth the possibility of achieving lower acid consumption.

2.0 INTRODUCTION

Preliminary metallurgical testwork on a bulk surface sample from the Getty Copper deposit was conducted by Bacon, Donaldson & Associates (BDA) in 1989. This testwork demonstrated by means of bottle roll and column testwork that the oxidized surface mineralization in this deposit is amenable to copper extraction by means of acidic heap leaching.

During 1993, a drill program was conducted by Getty Copper in order to confirm the presence of both oxide and sulphide copper mineralization and to provide samples for additional metallurgical testwork. The present report summarizes the results of bottle roll testwork conducted on crushed drill core from the 1993 program. All testwork was conducted by Process Research Associates Ltd. of Vancouver, in consultation with M. J. V. Beattie, P.Eng.

3.0 DISCUSSION

3.1 Sample description

A total of eight bottle roll tests were conducted by Process Research. The details of the individual assay rejects used to prepare the composites used for testing are included in Appendix A. The make-up of the composites is summarized in Table 3.1.

Table 3.1
Make-up of Composite Samples

TEST NO.	COMPOSITE	HOLE No.	FOOTAGE From	FOOTAGE To
L1	A	1993-1	94	235
L2	B	1993-1	235	335
L3	C	1993-1	335	435
L4	E	1993-2	100	210
L5	D	1993-2	40	100
L6	F	1993-3	30	60
L7	G	1993-5	29	129
L8	H	1993-5	129	219

The drill core had been crushed by Eco Tech Laboratories of Kamloops, B. C. All the samples had been crushed to at least minus 3/4 inch but showed considerable variation in their size distribution, being 77% to 87% passing 3/8 inch. Composite G, which was used for test L7, had been inadvertently crushed to minus 6 mesh. The size distribution of each composite following the leaching is included with the test details in Appendix B.

3.2 Procedure

A standardized bottle roll procedure was used for all the tests. The test was initiated by combining 2 kilograms of the composite sample with an equivalent weight of solution containing 15 g/L H_2SO_4 in a large bottle. The bottle was placed on rollers and was periodically (once per hour) rotated to allow fresh solution to contact the rock. After set time intervals the sample was filtered and the pregnant leach solution was replaced with fresh acid solution. After 144 hours (6 days) of leaching, the solids were filtered, washed and analyzed for residual copper.

The pregnant solution from each leach cycle was analyzed for copper and residual free acid as well as pH, and solution potential.

3.3 Results

The detailed results for each test are included in Appendix B. The results are summarized in Table 3.2

Table 3.2
Results of bottle roll testwork

TEST NO.	COMP	% Oxdn.	Cu Extn. %	NET ACID kg/tonne	FEED Cu %	RESIDUE % -3/8"
L1	A	86.0	67.5	15.9	0.43	77.3
L2	B	89.3	71.9	23.8	0.28	87.0
L3	C	88.2	67.8	13.6	0.34	81.8
L4	E	64.5	43.5	17.4	0.31	83.4
L5	D	87.5	72.6	14.2	0.48	83.8
L6	F	96.2	85.4	14.2	1.32	86.4
L7	G	96.1	92.0	16.6	1.02	100
L8	H	89.8	78.4	11.8	0.59	86.2

The progression of copper leaching with time is summarized in Figures 3.1 and 3.2. The results for L1 through L3 are very similar, consistent with the similar copper content and degree of oxidation for these samples. Test L4 shows a slower extraction rate which can be explained by the fact that this composite is only 65% oxidized.

GETTY COPPER BOTTLE ROLL TESTS

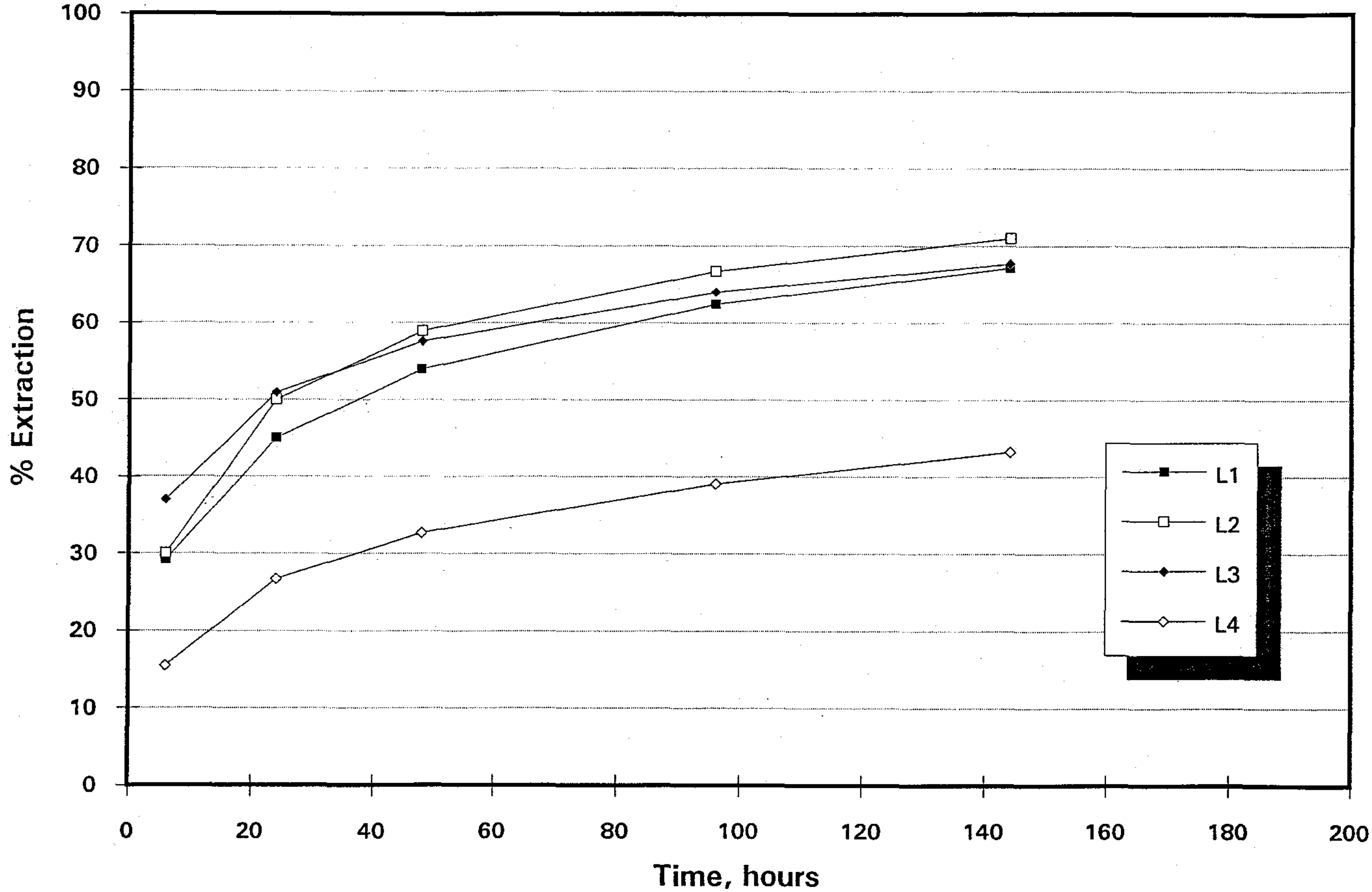


Figure 3.1

GETTY COPPER BOTTLE ROLL TESTS

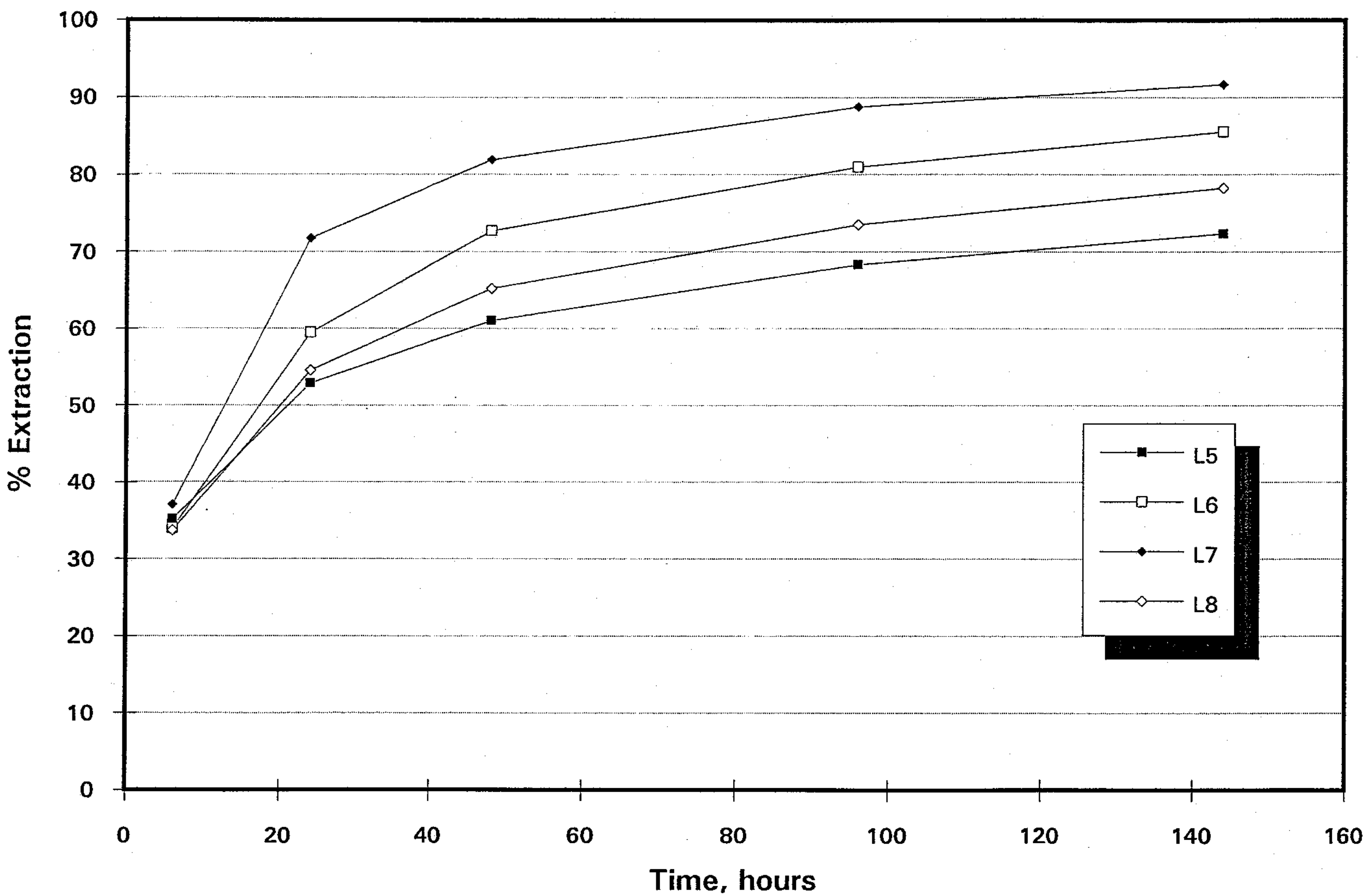
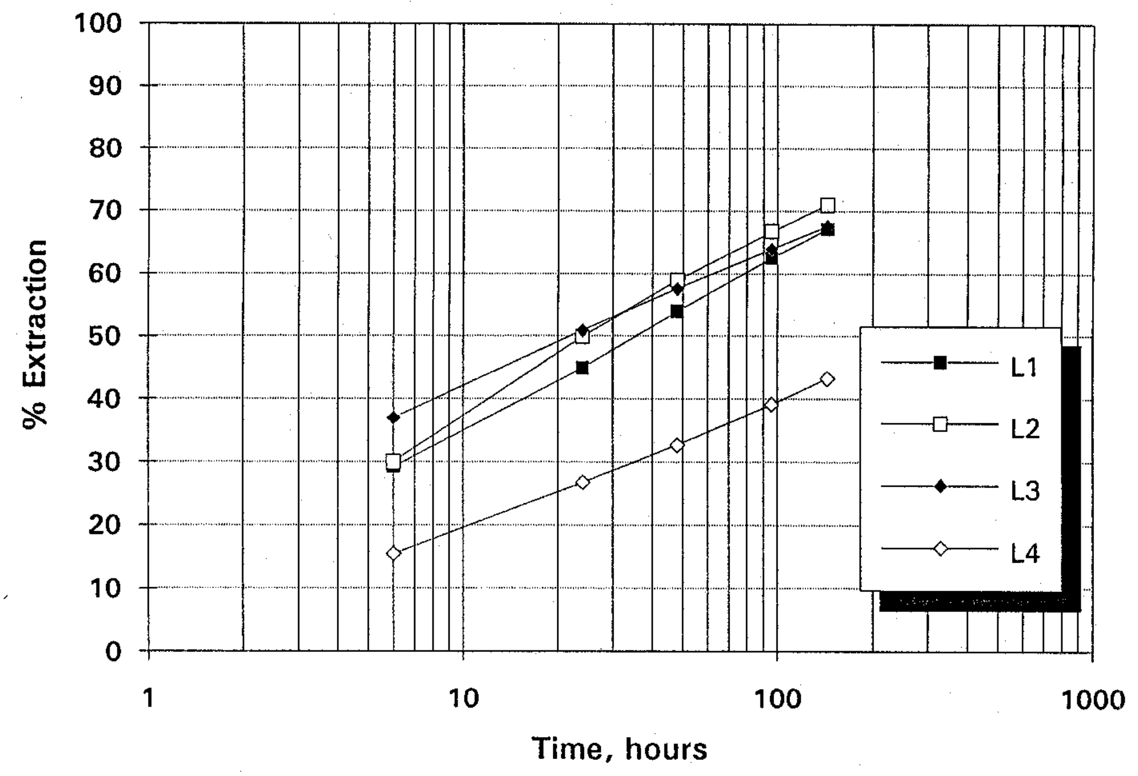


Figure 3.2

The results in Figure 3.2 are also consistent with the varying composition and size of the samples used for each test. L6 and L7 had the highest feed assays of 1.32 and 1.02 % Cu respectively and demonstrated the highest leach rates. Test L7 had a very fine size distribution compared to the other samples and consequently exhibited the highest leaching rate of all the tests and had a copper extraction of greater than 90% after 144 hours.

For the purpose of comparison, the bulk surface sample tested by BDA achieved copper extractions of 76 to 79% over a 120 hour (5 day) leach period with a feed assay of 1.80% copper which was essentially 100% in oxide form. Subsequent column testing of this material crushed to minus 3/4 inch resulted in a copper extraction of 80% after 66 days of leaching. The present drill core rejects have comparable bottle roll results to that of the bulk surface sample. The semi-log plots for the current testwork of copper extraction as a function of log-time included as figure 3 indicate that, with the exception of composite E, the samples should all achieve a copper extraction of at least 80% with extended leaching.

The acid consumption in the present tests ranged from 11.7 to 17.4 kg/tonne with the exception of test L2 (Composite B) which had an anomalously high consumption of 23.8 kg/tonne. Considering the longer duration of the present tests compared to the BDA tests the acid consumptions are comparable to the 9.7 to 12.5 kg/tonne experienced in the previous testwork. The subsequent column testwork on the surface composite conducted by BDA consumed 25.8 kg/tonne. It appears that similar consumptions can be anticipated for all the present samples except composite B which may show a higher consumption. It should be noted that the BDA column was preliminary in nature and that by optimizing the acid addition strategy and including solvent extraction in the test, the potential exists to decrease the acid requirement.


100
90
80
70
60
50
40
30
20
10
0
% Extraction
1
10
100
1000
Time, hours
L1
L2
L3
L4

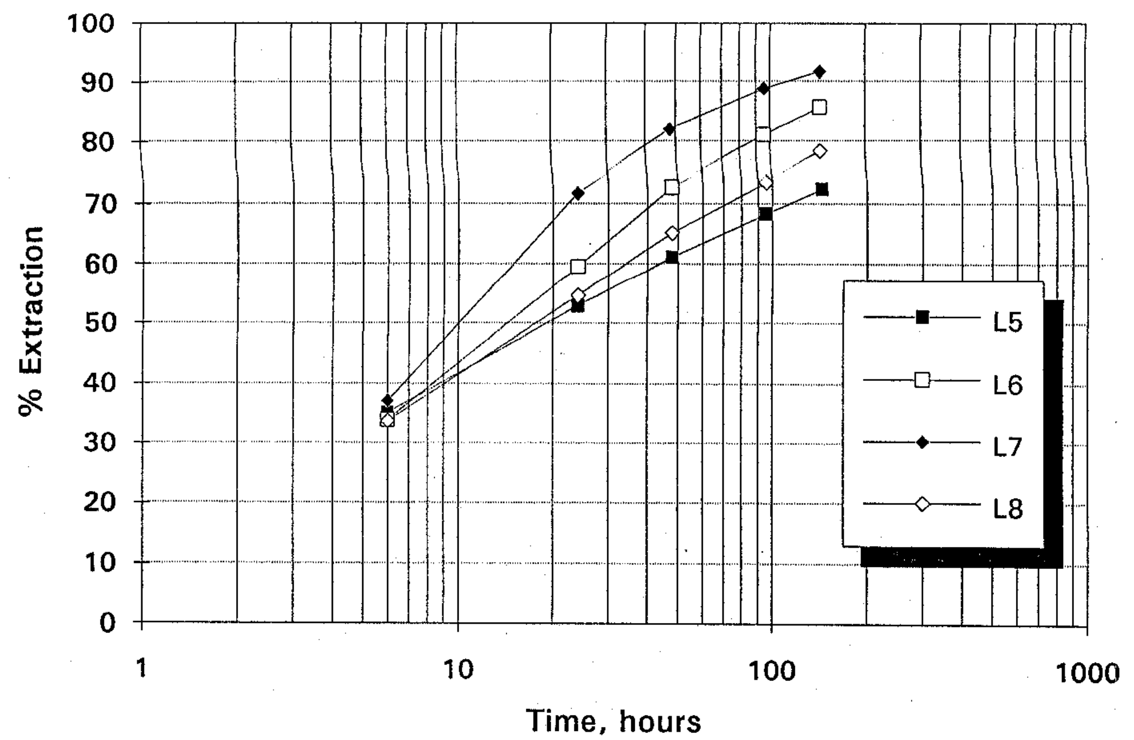

100
90
80
70
60
50
40
30
20
10
0
% Extraction
1
10
100
1000
Time, hours
L5
L6
L7
L8

Figure 3.3

Appendix A

Sample details

COMPOSITE A

Sample	Weight,,g
120001	2827.3
120002	3307.8
120003	3223.7
120004	2483.3
120005	3182.9
120006	3544.6
120007	2977.7
120008	2305.6
120009	2097.3
120010	2472.1
120011	2718.8
120012	2442.1
120013	2054.7
120014	2744.5

COMPOSITE B

Sample	Weight, g
120015	2331.5
120016	2721.9
120017	2296.3
120018	2318.3
120019	1805.1
120020	2462.5
120021	2283.8
120022	2472.8
120023	2714.9
120024	2214.3

COMPOSITE C

Sample	Weight,g
120025	2676.4
120026	3077.9
120027	2197.0
120028	2241.4
120029	3146.8
120030	3738.2
120031	3279.4
120032	3541.7
120033	2511.3
120034	3266.6

COMPOSITE D

Sample	Weight, g
122051	2748.5
122052	2921.4
122053	3217.2
122054	2674.0
122055	3340.5
122056	3100.4

COMPOSITE E

Sample	Weight, g
122057	1515.6
	1223.0
122058	1248.3
	1485.0
122059	1282.7
	1507.3
122060	1459.6
	1919.6
122061	1446.6
	1273.7
122062	1562.8
	1520.9
122063	1247.0
	1584.5
122064	1643.5
	1307.9
122065	1461.0
	1807.8
122066	1522.9
	1463.6
122067	1531.1
	1676.5

COMPOSITE F

Sample	Weight,g
122501	1534.5
	957.4
122502	1776.5
	1594.8
122503	1521.6
	1149.0

COMPOSITE G

Sample	Weight, g
122569	1055.8
	746.9
122570	1556.5
	1032.7
122571	1541.9
	1133.2
122572	1333.5
	1363.6
122573	1659.3
	1505.5
122574	1912.7
	1565.4
122575	1190.1
	686.7
122576	1391.9
	1452.7
122577	935.2
	1021.0
122578	1265.5
	1582.5

COMPOSITE H

Sample	Weight,g
122579	1130.6
	835.1
122580	1623.8
	1012.5
122581	1265.6
	1402.4
122582	1399.5
122583	1617.1
	1720.7
122584	1775.4
	1350.2
122585	1525.4
	1207.2
122586	1271.5
	1151.2
122587	1310.1
	2111.9

Appendix B

Testwork details

BOTTLE ROLL SULPHURIC ACID LEACHING OF GETTY OXIDE ORES

File No: 93 - 061
Test No: L1
Sample Description: Composite A

Date: 6-Dec-93

TEST CONDITIONS:

Solids:	2000 g
H2O:	2000 g
% Solids:	50%
Solution Strength:	15 g/l H2SO4
Test Duration:	144 hours

TEST DESCRIPTION:

-solids and acid solution combined in large bottle
-bottles placed on rollers
-each day, acid solution decanted and replaced with fresh solution
-decanted solution analyzed for Cu, free acid, and pH
-test ended after 144 hours
-solids washed and wash solutions analyzed
-final solids assayed for TOTAL COPPER, OXIDE COPPER

TEST RESULTS:

Solution Analyses:

TIME hrs	PLS (ml)	COPPER (g/l)	COPPER (g)	ORP mV	pH	H2SO4 (g/l)	H2SO4 (g)
6	1857	1.26	2.34	465	1.36	8.78	16.30
24	1973	0.77	1.52	449	1.15	10.48	20.68
48	1971	0.41	0.81	445	1.16	11.94	23.53
96	1974	0.38	0.74	438	1.15	10.97	21.65
144	2008	0.21	0.43	437	1.48	11.79	23.67
wash	863	0.02	0.02				
	TOTAL		5.86				105.84

Solids Analyses:

TIME	SAMPLE SIZE (g)	TOTAL COPPER (%)	TOTAL COPPER (g)	OXIDE COPPER (%)	OXIDE COPPER (g)	IRON (%)	IRON (g)
144	1859	0.152	2.83	0.086	1.60		0.00
	TOTAL		2.83		1.60		0.00

CALCULATIONS:

TIME	COPPER EXTRACTION INDV. %	COPPER EXTRACTION CUM. %			ACID CONSUMPTION INDV. kg/tonne	ACID CONSUMPTION CUM. kg/tonne	NET Acid Kg/tonne
6	29.25%	29.25%			6.22	6.22	4.41
24	15.76%	45.00%			4.08	10.30	7.32
48	8.99%	54.00%			3.00	13.29	9.69
96	8.52%	62.52%			3.99	17.28	13.10
144	4.74%	67.25%			3.16	20.44	15.93
						20.44	15.93
wash	0.22%	67.47%				20.44	15.92
	TOTAL	67.47%				20.44	

HEAD GRADE:

	TOTAL COPPER	OXIDE COPPER	IRON
ASSAY HEAD			
CALCULATED HEAD	0.43%	0.37%	

BOTTLE ROLL SULPHURIC ACID LEACHING OF GETTY OXIDE ORES

File No: 93 - 061
Test No: L2
Sample Description: Composite B

Date: Dec.6,1993

TEST CONDITIONS:

Solids:	2000 g
H2O:	2000 g
% Solids:	50%
Solution Strength:	15 g/l H2SO4
Test Duration:	144 hours

TEST DESCRIPTION:

-solids and acid solution combined in large bottle
-bottles placed on rollers
-each day, acid solution decanted and replaced with fresh solution
-decanted solution analyzed for Cu, free acid, and pH
-test ended after 144 hours
-solids washed and wash solutions analyzed
-final solids assayed for TOTAL COPPER, OXIDE COPPER

TEST RESULTS:

Solution Analyses:

TIME hrs	PLS (ml)	COPPER (g/l)	COPPER (g)	ORP mV	pH	H2SO4 (g/l)	H2SO4 (g)
6	1906	0.82	1.56	452	1.47	4.89	9.32
24	1899	0.61	1.16	457	1.17	8.53	16.20
48	1921	0.31	0.59	450	1.11	11.17	21.46
96	1977	0.22	0.44	439	1.13	10.72	21.19
144	1983	0.12	0.25	434	1.42	11.79	23.38
wash	998	0.06	0.06				
	TOTAL		4.06				91.55

Solids Analyses:

TIME	SAMPLE SIZE (g)	TOTAL COPPER (%)	TOTAL COPPER (g)	OXIDE COPPER (%)	OXIDE COPPER (g)	IRON (%)	IRON (g)
144	1845.1	0.086	1.59	0.046	0.85		0.00
	TOTAL		1.59		0.85		0.00

CALCULATIONS:

TIME	COPPER EXTRACTION INDV. %	COPPER EXTRACTION CUM. %			ACID CONSUMPTION INDV. kg/tonne	ACID CONSUMPTION CUM. kg/tonne	NET Acid Kg/tonne
6	29.66%	29.66%			10.11	10.11	8.90
24	19.93%	49.59%			5.99	16.10	14.01
48	9.68%	59.26%			3.50	19.61	17.05
96	7.46%	66.73%			4.13	23.74	20.84
144	4.26%	70.98%			3.16	26.90	23.81
						26.90	23.81
wash	0.92%	71.90%			0.00	26.90	23.76
	TOTAL	71.90%				26.90	

HEAD GRADE:

	TOTAL COPPER	OXIDE COPPER	IRON
ASSAY HEAD			
CALCULATED HEAD	0.28%	0.25%	

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BOTTLE ROLL SULPHURIC ACID LEACHING OF GETTY OXIDE ORES

File No: 93 - 061
Test No: L3
Sample Description: Composite C

Date: Dec. 6, 1993

TEST CONDITIONS:

Solids:	2000 g
H2O:	2000 g
% Solids:	50%
Solution Strength:	15 g/l H2SO4
Test Duration:	144 hours

TEST DESCRIPTION:

- -solids and acid solution combined in large bottle
- -bottles placed on rollers
- -each day, acid solution decanted and replaced with fresh solution
- -decanted solution analyzed for Cu, free acid, and pH
- -test ended after 144 hours
- -solids washed and wash solutions analyzed
- -final solids assayed for TOTAL COPPER, OXIDE COPPER

TEST RESULTS:

Solution Analyses:

TIME hrs	PLS (ml)	COPPER (g/l)	COPPER (g)	ORP mV	pH	H2SO4 (g/l)	H2SO4 (g)
6	1926	1.24	2.39	409	1.17	8.88	17.10
24	1929	0.53	1.02	431	1.16	11.60	22.38
48	1973	0.25	0.49	441	1.08	12.44	24.54
96	1983	0.22	0.44	443	1.11	11.89	23.58
144	1986	0.13	0.25	439	1.38	12.60	25.02
wash	1000	0.02	0.02				
	TOTAL		4.60				112.62

Solids Analyses:

TIME	SAMPLE SIZE (g)	TOTAL COPPER (%)	TOTAL COPPER (g)	OXIDE COPPER (%)	OXIDE COPPER (g)	IRON (%)	IRON (g)
144	1880.1	0.116	2.18	0.074	1.39		0.00
	TOTAL		2.18		1.39		0.00

CALCULATIONS:

TIME	COPPER EXTRACTION INDV. %	COPPER EXTRACTION CUM. %			ACID CONSUMPTION INDV. kg/tonne	ACID CONSUMPTION CUM. Kg/tonne	NET Acid Kg/tonne
6	37.00%	37.00%			6.12	6.12	4.28
24	13.90%	50.90%			3.17	9.29	6.66
48	6.73%	57.63%			2.44	11.73	8.73
96	6.38%	64.02%			3.08	14.81	11.46
144	3.70%	67.71%			2.37	17.18	13.64
						17.18	13.64
wash	0.14%	67.85%				17.18	13.63
	TOTAL	67.85%				17.18	

HEAD GRADE:

	TOTAL COPPER	OXIDE COPPER	IRON
ASSAY HEAD			
CALCULATED HEAD	0.34%	0.30%	

BOTTLE ROLL SULPHURIC ACID LEACHING OF GETTY OXIDE ORES

File No: 93 - 061
Test No: L4
Sample Description: Composite E

Date: Dec. 6, 1993

TEST CONDITIONS:

Solids:	2000 g
H2O:	2000 g
% Solids:	50%
Solution Strength:	15 g/l H2SO4
Test Duration:	144 hours

TEST DESCRIPTION:

- -solids and acid solution combined in large bottle
- -bottles placed on rollers
- -each day, acid solution decanted and replaced with fresh solution
- -decanted solution analyzed for Cu, free acid, and pH
- -test ended after 144 hours
- -solids washed and wash solutions analyzed
- -final solids assayed for TOTAL COPPER, OXIDE COPPER

TEST RESULTS:

Solution Analyses:

TIME hrs	PLS (ml)	COPPER (g/l)	COPPER (g)	ORP mV	pH	H2SO4 (g/l)	H2SO4 (g)
6	1885	0.47	0.89	416	1.16	7.94	14.97
24	1886	0.36	0.68	412	1.11	10.96	20.67
48	1923	0.22	0.42	417	1.07	12.25	23.56
96	1939	0.21	0.40	417	1.08	11.45	22.20
144	1953	0.14	0.27	416	1.35	12.05	23.53
wash	1235	0.02	0.02				
	TOTAL		2.68				104.93

Solids Analyses:

TIME	SAMPLE SIZE (g)	TOTAL COPPER (%)	TOTAL COPPER (g)	OXIDE COPPER (%)	OXIDE COPPER (g)	IRON (%)	IRON (g)
144	1890.4	0.184	3.48	0.072	1.36		0.00
	TOTAL		3.48		1.36		0.00

CALCULATIONS:

TIME	COPPER EXTRACTION INDV. %	COPPER EXTRACTION CUM. %			ACID CONSUMPTION INDV. kg/tonne	ACID CONSUMPTION CUM. kg/tonne	NET Acid Kg/tonne
6	15.47%	15.47%			7.06	7.06	6.38
24	10.81%	26.28%			3.63	10.69	9.49
48	6.38%	32.66%			2.52	13.21	11.68
96	6.49%	39.14%			3.44	16.66	14.81
144	4.18%	43.32%			2.84	19.50	17.45
						19.50	17.45
wash	0.17%	43.49%				19.50	17.43
	TOTAL	43.49%				19.50	

HEAD GRADE:

	TOTAL COPPER	OXIDE COPPER	IRON
ASSAY HEAD			
CALCULATED HEAD	0.31%	0.20%	

BOTTLE ROLL SULPHURIC ACID LEACHING OF GETTY OXIDE ORES

File No: 93 - 061
Test No: L5
Sample Description: Composite D

Date: Jan. 4, 1994

TEST CONDITIONS:

Solids:	2000 g
H2O:	2000 g
% Solids:	50%
Solution Strength:	15 g/l H2SO4
Test Duration:	144 hours

TEST DESCRIPTION:

- solids and acid solution combined in large bottle
- bottles placed on rollers
- each day, acid solution decanted and replaced with fresh solution
- decanted solution analyzed for Cu, free acid, and pH
- test ended after 144 hours
- solids washed and wash solutions analyzed
- final solids assayed for TOTAL COPPER, OXIDE COPPER

TEST RESULTS:

Solution Analyses:

TIME	PLS	COPPER		ORP	pH	H2SO4	
hrs	(ml)	(g/l)	(g)	mV		(g/l)	(g)
6	1885	1.70	3.20	459	1.34	7.17	13.52
24	1893	0.95	1.80	462	1.21	10.51	19.90
48	1895	0.44	0.83	461	1.58	12.15	23.02
96	1938	0.37	0.72	449	1.21	12.57	24.36
144	1906	0.21	0.40	449	1.06	12.09	23.04
wash	1786	0.02	0.03				
	TOTAL		6.99				103.84

Solids Analyses:

TIME	SAMPLE SIZE	TOTAL COPPER		OXIDE COPPER		IRON	
	(g)	(%)	(g)	(%)	(g)	(%)	(g)
144	1860	0.142	2.64	0.08	1.49		0.00
	TOTAL		2.64		1.49		0.00

CALCULATIONS:

TIME	COPPER EXTRACTION				ACID CONSUMPTION		NET
	INDV. %	CUM. %			INDV. kg/tonne	CUM. kg/tonne	Acid Kg/tonne
6	35.19%	35.19%			7.83	7.83	5.36
24	17.73%	52.92%			4.04	11.87	8.01
48	8.16%	61.08%			2.61	14.48	9.98
96	7.24%	68.33%			2.28	16.76	11.70
144	4.09%	72.42%			2.83	19.59	14.23
						19.59	14.23
wash	0.14%	72.57%				19.59	14.20
	TOTAL	72.57%				19.59	

HEAD GRADE:

	TOTAL COPPER	OXIDE COPPER	IRON
ASSAY HEAD			
CALCULATED HEAD	0.48%	0.42%	

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BOTTLE ROLL SULPHURIC ACID LEACHING OF GETTY OXIDE ORES

File No: 93 - 061
Test No: L6
Sample Description: Composite F

Date: Jan. 4, 1994

TEST CONDITIONS:

Solids:	2000 g
H2O:	2000 g
% Solids:	50%
Solution Strength:	15 g/l H2SO4
Test Duration:	144 hours

TEST DESCRIPTION:

- solids and acid solution combined in large bottle
- bottles placed on rollers
- each day, acid solution decanted and replaced with fresh solution
- decanted solution analyzed for Cu, free acid, and pH
- test ended after 144 hours
- solids washed and wash solutions analyzed
- final solids assayed for TOTAL COPPER, OXIDE COPPER

TEST RESULTS:

Solution Analyses:

TIME	PLS	COPPER		ORP	pH	H2SO4	
hrs	(ml)	(g/l)	(g)	mV		(g/l)	(g)
6	1876	4.50	8.44	484	1.67	3.87	7.26
24	1935	3.62	7.00	493	1.37	6.61	12.79
48	1725	1.88	3.24	481	1.74	9.59	16.54
96	1805	1.36	2.45	478	1.23	9.80	17.69
144	1749	0.73	1.28	472	1.06	11.28	19.73
							0.00
wash	1578	0.09	0.14				0.00
	TOTAL		22.56				74.01

Solids Analyses:

TIME	SAMPLE SIZE	TOTAL COPPER		OXIDE COPPER		IRON	
	(g)	(%)	(g)	(%)	(g)	(%)	(g)
144	1870	0.206	3.85	0.154	2.88		0.00
	TOTAL		3.85		2.88		0.00

CALCULATIONS:

TIME	COPPER EXTRACTION INDV. %	COPPER EXTRACTION CUM. %			ACID CONSUMPTION INDV. kg/tonne	ACID CONSUMPTION CUM. kg/tonne	NET Acid Kg/tonne
6	34.03%	34.03%			11.13	11.13	4.62
24	25.49%	59.51%			7.70	18.83	6.91
48	13.17%	72.69%			5.14	23.97	9.55
96	8.34%	81.03%			4.46	28.42	12.11
144	4.56%	85.59%			3.21	31.64	14.34
						31.64	14.34
wash	-0.17%	85.41%				31.64	14.23
	TOTAL	85.41%				31.64	

HEAD GRADE:

	TOTAL COPPER	OXIDE COPPER	IRON
ASSAY HEAD			
CALCULATED HEAD	1.32%	1.27%	

BOTTLE ROLL SULPHURIC ACID LEACHING OF GETTY OXIDE ORES

File No: 93 - 061
Test No: L7
Sample Description: Composite G

Date:
Jan. 4, 1994

TEST CONDITIONS:

Solids: 2000 g
H_2O: 2000 g
% Solids: 50%
Solution Strength: 15 g/l H_2SO_4
Test Duration: 144 hours

TEST DESCRIPTION:

-solids and acid solution combined in large bottle
-bottles placed on rollers
-each day, acid solution decanted and replaced with fresh solution
-decanted solution analyzed for Cu, free acid, and pH
-test ended after 144 hours
-solids washed and wash solutions analyzed
-final solids assayed for TOTAL COPPER, OXIDE COPPER

TEST RESULTS:

Solution Analyses:

TIME	PLS	COPPER		ORP	pH	H2SO4	
hrs	(ml)	(g/l)	(g)	mV		(g/l)	(g)
6	1855	3.80	7.05	446	1.50	3.08	5.71
24	1817	3.80	6.90	453	1.40	5.24	9.52
48	2020	1.42	2.87	473	1.52	10.25	20.71
96	2046	0.68	1.39	470	1.28	11.35	23.22
144	2034	0.29	0.59	472	1.06	12.34	25.10
							0.00
wash	1400	0.04	0.06				0.00
	TOTAL		18.86				84.26

Solids Analyses:

TIME	SAMPLE SIZE	TOTAL COPPER		OXIDE COPPER		IRON	
	(g)	(%)	(g)	(%)	(g)	(%)	(g)
144	1852.3	0.088	1.63	0.042	0.78		0.00
	TOTAL		1.63		0.78		0.00

CALCULATIONS:

TIME	COPPER EXTRACTION				ACID CONSUMPTION		NET
	INDV. %	CUM. %			INDV. kg/tonne	CUM. kg/tonne	Acid Kg/tonne
6	37.13%	37.13%			11.92	11.92	6.48
24	34.62%	71.75%			8.90	20.82	10.05
48	10.19%	81.94%			3.86	24.67	11.69
96	6.83%	88.77%			3.70	28.37	14.32
144	2.94%	91.71%			2.74	31.11	16.61
						31.11	16.61
wash	0.34%	92.05%				31.11	16.56
	TOTAL	92.05%				31.11	

HEAD GRADE:

	TOTAL COPPER	OXIDE COPPER	IRON
ASSAY HEAD			
CALCULATED HEAD	1.02%	0.98%	

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BOTTLE ROLL SULPHURIC ACID LEACHING OF GETTY OXIDE ORES

File No: 93 - 061 Date: Jan. 4, 1994
Test No: L8
Sample Description: Composite H

TEST CONDITIONS:

Solids:	2000 g
H2O:	2000 g
% Solids:	50%
Solution Strength:	15 g/l H2SO4
Test Duration:	144 hours

TEST DESCRIPTION:

- -solids and acid solution combined in large bottle
- -bottles placed on rollers
- -each day, acid solution decanted and replaced with fresh solution
- -decanted solution analyzed for Cu, free acid, and pH
- -test ended after 144 hours
- -solids washed and wash solutions analyzed
- -final solids assayed for TOTAL COPPER, OXIDE COPPER

TEST RESULTS:

Solution Analyses:

TIME hrs	PLS (ml)	COPPER (g/l)	COPPER (g)	ORP mV	pH	H2SO4 (g/l)	H2SO4 (g)
6	1771	2.00	3.54	448	1.35	7.34	13.00
24	1791	1.47	2.63	449	1.29	9.77	17.50
48	1885	0.78	1.47	455	1.56	11.87	22.37
96	1698	0.59	1.00	448	1.33	11.93	20.26
144	1893	0.32	0.61	455	1.05	13.10	24.80
							0.00
wash	1476	0.03	0.04				0.00
	TOTAL		9.30				97.93

Solids Analyses:

TIME	SAMPLE SIZE (g)	TOTAL COPPER (%)	TOTAL COPPER (g)	OXIDE COPPER (%)	OXIDE COPPER (g)	IRON (%)	IRON (g)
144	1884	0.136	2.56	0.072	1.36		0.00
	TOTAL		2.56		1.36		0.00

CALCULATIONS:

TIME	COPPER EXTRACTION INDV. %	COPPER EXTRACTION CUM. %			ACID CONSUMPTION INDV. kg/tonne	ACID CONSUMPTION CUM. kg/tonne	NET Acid Kg/tonne
6	33.71%	33.71%			7.66	7.66	4.93
24	20.91%	54.62%			4.35	12.01	7.25
48	10.62%	65.24%			2.58	14.60	8.70
96	8.26%	73.51%			2.89	17.49	10.82
144	4.80%	78.30%			1.44	18.92	11.78
						18.92	11.78
wash	0.09%	78.39%				18.92	11.75
	TOTAL	78.39%				18.92	

HEAD GRADE:

	TOTAL COPPER	OXIDE COPPER	IRON
ASSAY HEAD			
CALCULATED HEAD	0.59%	0.53%	

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SIZE DISTRIBUTION

SAMPLE NO : 93-061 L1
Leach tails

Size Fraction (Tylor mesh)	Individual Percentage Retained	Cumulative Percentage Passing
1/2"	5.4	94.6
3/8"	17.3	77.3
6	55.6	21.6
10	7.7	13.9
20	5.6	8.3
35	2.6	5.7
48	1.0	4.7
Undersize	4.7	

SIZE DISTRIBUTION

SAMPLE NO : 93-061 L2
Leach tails

Size Fraction (Tylor mesh)	Individual Percentage Retained	Cumulative Percentage Passing
1/2"	1.2	98.8
3/8"	11.8	87.0
6	52.2	34.8
10	11.2	23.7
20	10.0	13.7
35	5.0	8.7
48	1.8	6.8
Undersize	6.8	

SIZE DISTRIBUTION

SAMPLE NO : 93-061 L3
Leach tails

Size Fraction (Tylor mesh)	Individual Percentage Retained	Cumulative Percentage Passing
1/2"	4.0	96.0
3/8"	14.2	81.8
6	51.6	30.2
10	10.7	19.5
20	8.8	10.6
35	3.8	6.8
48	1.4	5.5
Undersize	5.5	

SIZE DISTRIBUTION

SAMPLE NO : 93-061 L4
Leach tails

Size Fraction (Tylor mesh)	Individual Percentage Retained	Cumulative Percentage Passing
1/2"	1.0	99.0
3/8"	15.6	83.4
6	49.6	33.8
10	10.3	23.5
20	9.4	14.2
35	4.8	9.3
48	1.8	7.5
Undersize	7.5	

SIZE DISTRIBUTION

SAMPLE NO: 93-061 L5
Residue

Size Fraction (Tyler mesh)	Individual Percentage Retained	Cumulative Percentage Passing
1/2"	2.5	97.5
3/8"	13.6	83.8
6	52.8	31.1
10	11.9	19.1
20	6.6	12.5
35	4.2	8.3
48	1.6	6.7
Undersize	6.7	

SIZE DISTRIBUTION

SAMPLE NO: 93-061 L6
Residue

Size Fraction (Tyler mesh)	Individual Percentage Retained	Cumulative Percentage Passing
1/2"	1.9	98.1
3/8"	11.7	86.4
6	39.5	46.9
10	18.6	28.3
20	10.6	17.8
35	6.1	11.7
48	2.2	9.4
Undersize	9.4	

SIZE DISTRIBUTION

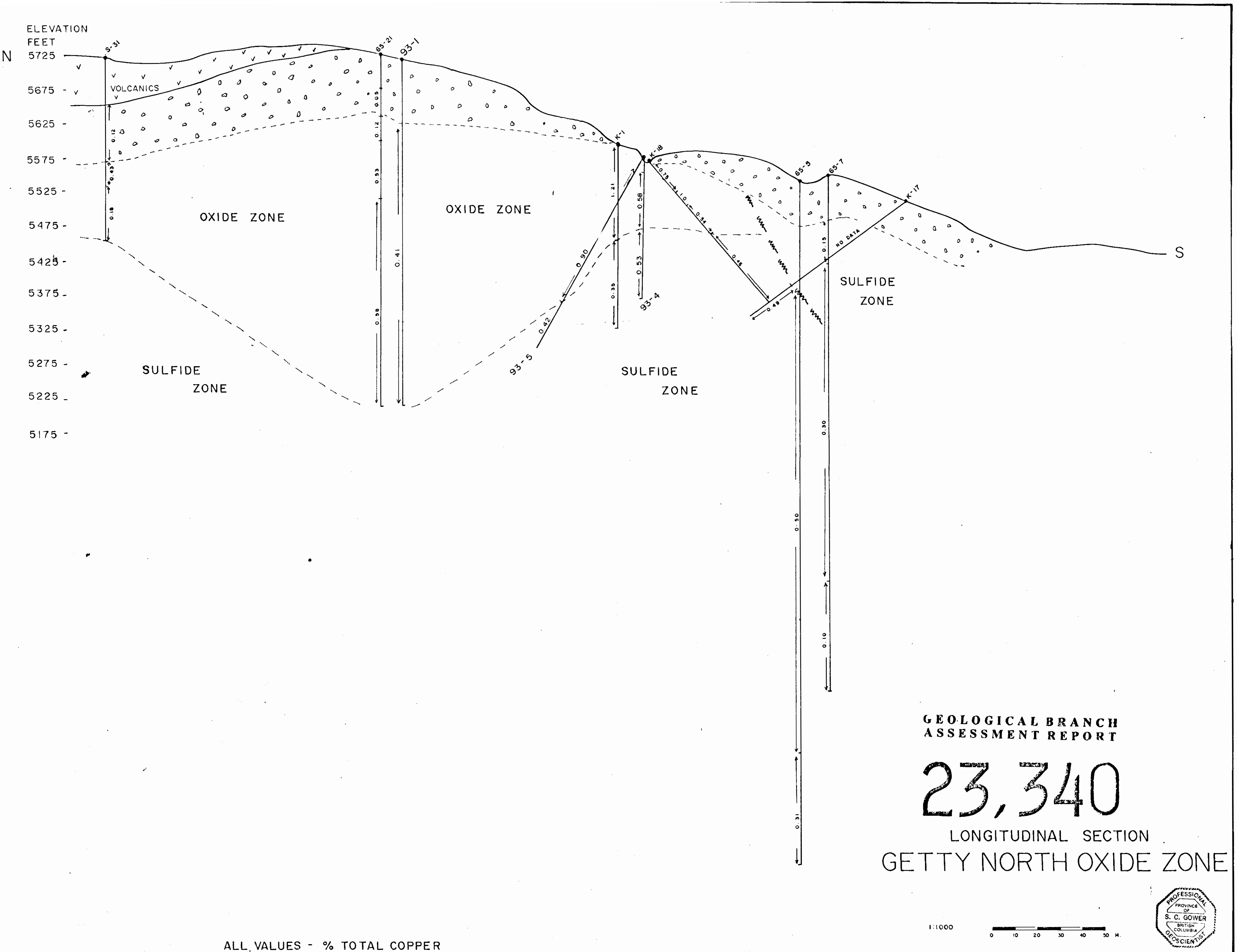
SAMPLE NO: 93-061 L7
Residue

Size Fraction (Tyler mesh)	Individual Percentage Retained	Cumulative Percentage Passing
10	40.4	59.6
20	30.1	29.4
35	10.5	18.9
48	3.8	15.1
60	1.7	13.4
100	3.9	9.5
Undersize	9.5	

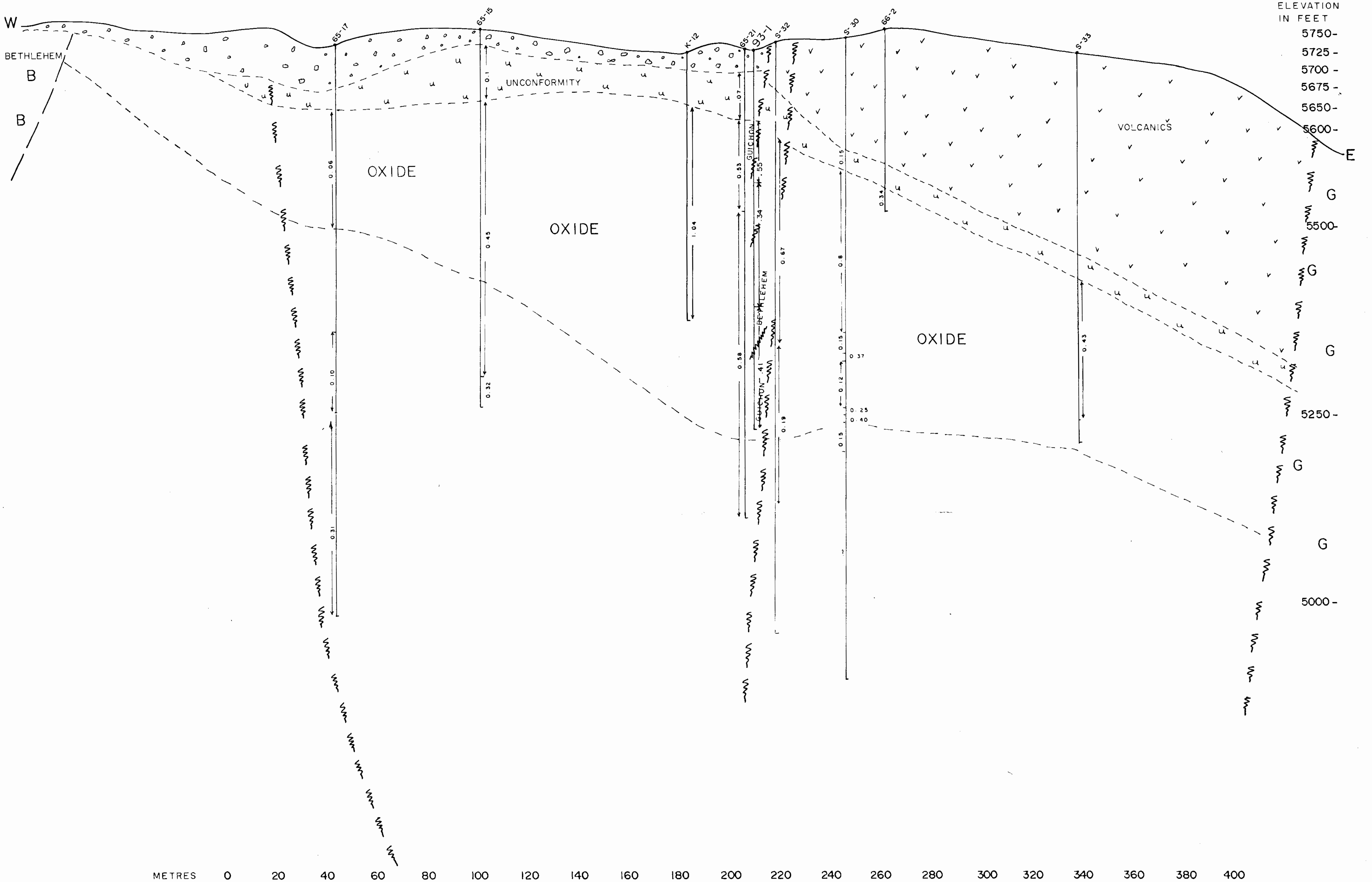
SIZE DISTRIBUTION

SAMPLE NO: 93-061 L8
Residue

Size Fraction (Tyler mesh)	Individual Percentage Retained	Cumulative Percentage Passing
1/2"	2.5	97.5
3/8"	11.3	86.2
6	45.2	41.0
10	13.1	28.0
20	8.6	19.4
35	5.7	13.7
48	2.3	11.3
Undersize	11.3	



ELEVATION
FEET
N
5725
5675
5625
5575
5525
5475
5425
5375
5325
5275
5225
5175
S-31
65-21
93-1
K-1
K-18
65-5
65-7
K-17
93-4
93-5
VOLCANICS
OXIDE ZONE
OXIDE ZONE
SULFIDE ZONE
SULFIDE ZONE
SULFIDE ZONE
NO DATA
S
0.12
0.43
0.18
0.05
0.12
0.53
0.41
0.58
1.21
0.58
0.53
0.35
0.90
0.42
0.73
1.10
0.54
0.46
0.49
0.15
0.30
0.10
0.50
0.31
GEOLOGICAL BRANCH
ASSESSMENT REPORT
23,340
LONGITUDINAL SECTION
GETTY NORTH OXIDE ZONE
1:1000
0
10
20
30
40
50 M.
PROFESSIONAL
PROVINCE OF
S. C. GOWER
BRITISH COLUMBIA
GEOSCIENTIST
ALL VALUES - % TOTAL COPPER



GEOLOGICAL BRANCH ASSESSMENT REPORT

23,340

CROSS SECTION 106 SE

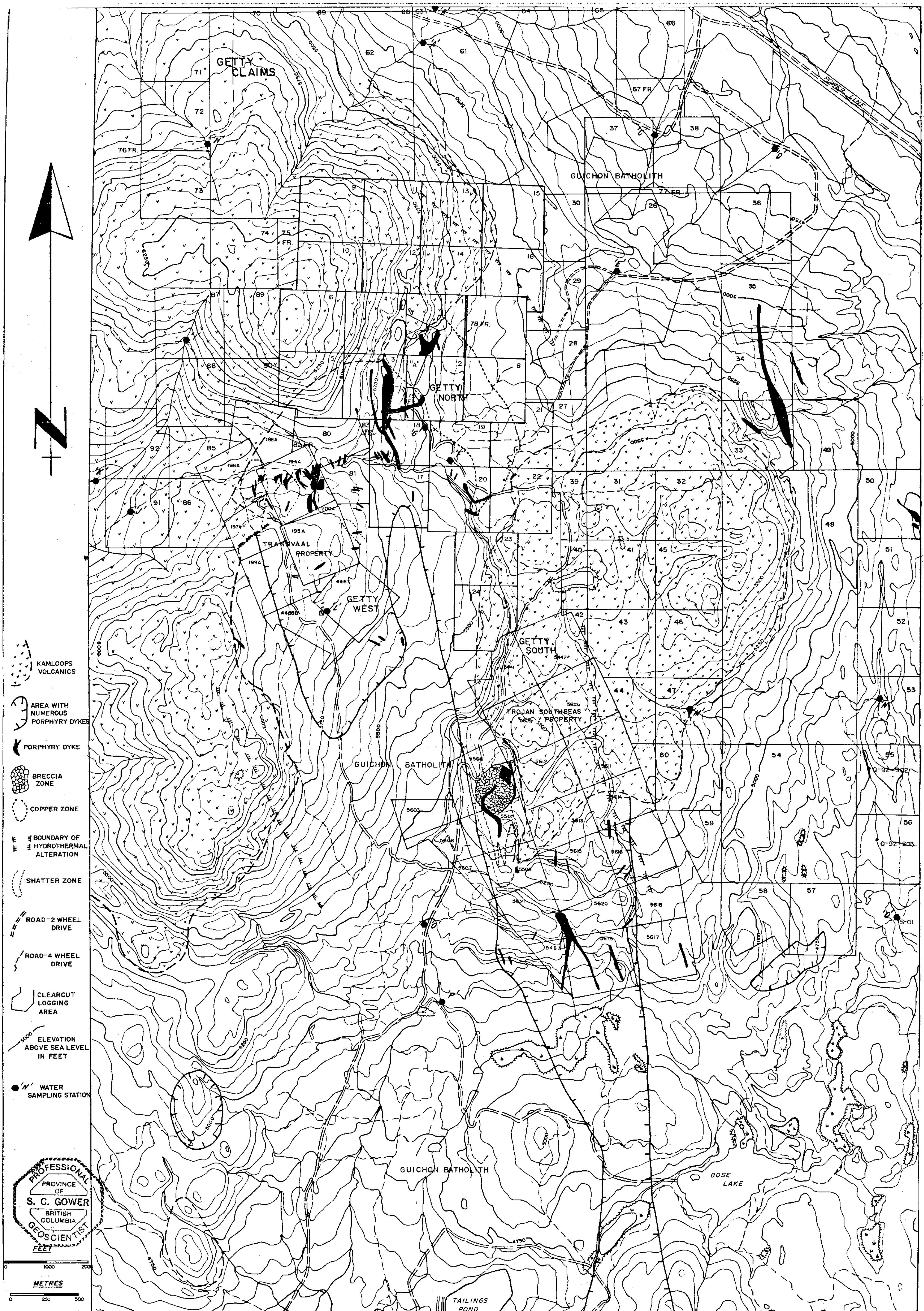
GETTY NORTH PROJECT

0 10 20 30 40 50 M.

1:1000

PROFESSIONAL PROVINCE OF S. C. GOWER BRITISH COLUMBIA GEOSCIENTIST

ALL VALUES - % TOTAL COPPER



ROBAK INDUSTRIES LTD.

NORTH HIGHLAND VALLEY
KRAIN GETTY PROPERTY

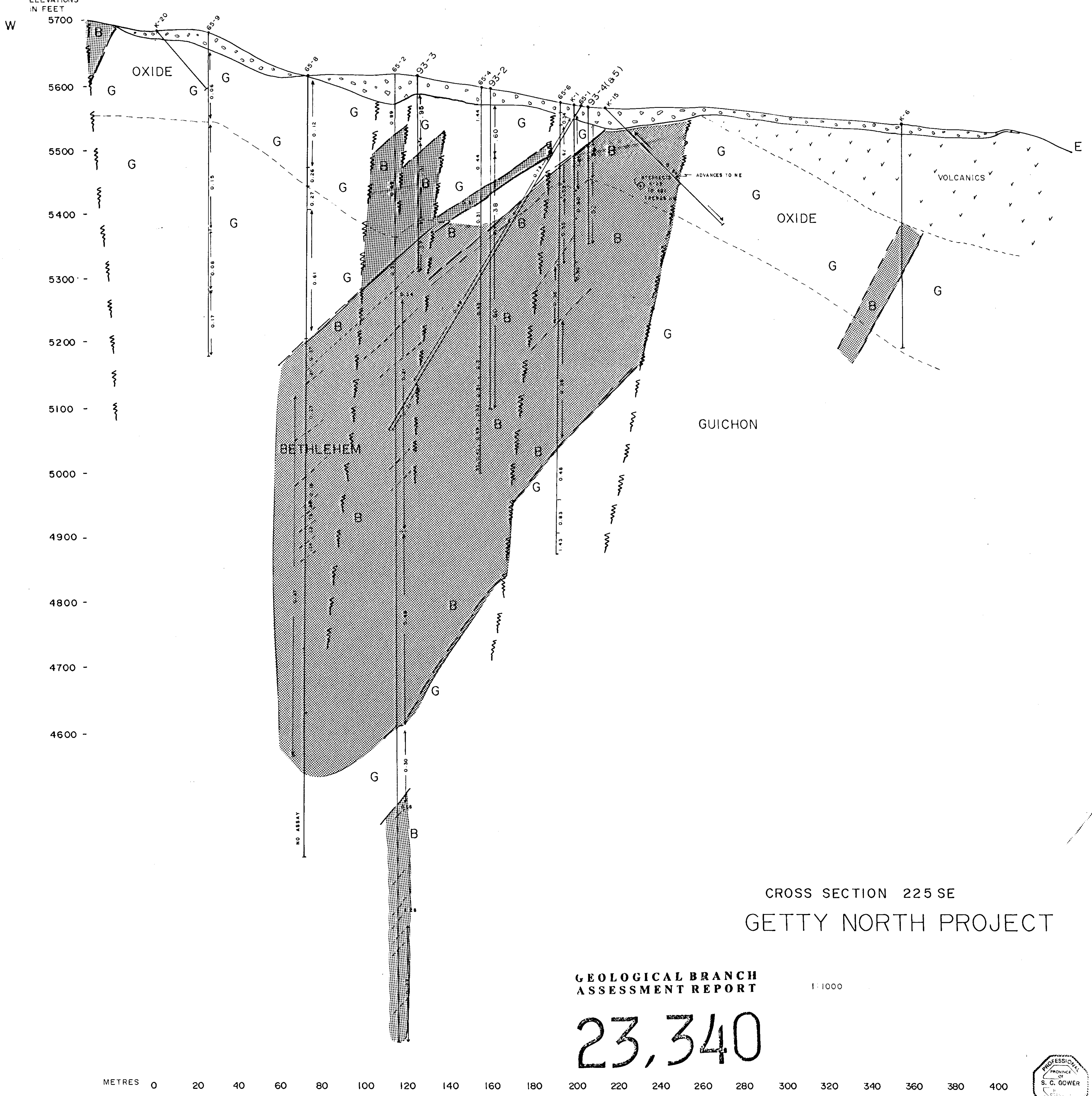
GENERAL GEOLOGY, MINERAL ZONES, CLAIMS ROADS, TOPOGRAPHY, CREEKS & CLEARCUT

DRAWN BY: E. THOMPSON, S. GOWER — DATE: JUNE, 1990. Aug 27/92

FIG.: 4 — SCALE: 1:25,000

GOWER, THOMPSON & ASSOCIATES LIMITED

ALL CLAIM BOUNDARYS APPROX.



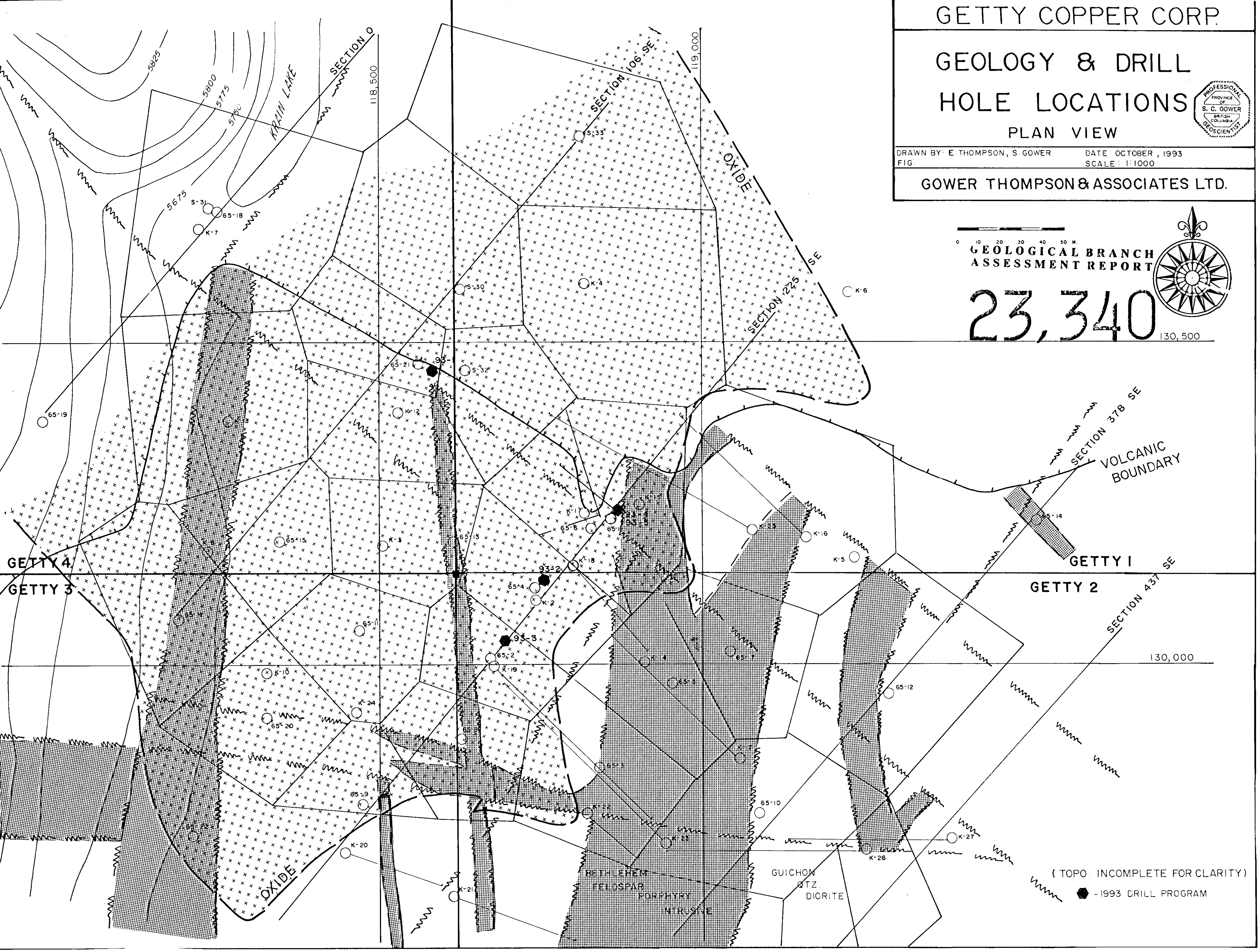
CROSS SECTION 225 SE

GETTY NORTH PROJECT

GEOLOGICAL BRANCH
ASSESSMENT REPORT

23,340

ALL VALUES - % TOTAL COPPER


GETTY COPPER CORP.
GEOLOGY & DRILL HOLE LOCATIONS
PLAN VIEW
DRAWN BY: E. THOMPSON, S. GOWER
FIG.
DATE: OCTOBER, 1993
SCALE: 1:1000
GOWER THOMPSON & ASSOCIATES LTD.
PROFESSIONAL
PROVINCE OF
S. C. GOWER
BRITISH COLUMBIA
GEOSCIENTIST
GEOLOGICAL BRANCH
ASSESSMENT REPORT
23,340
SECTION 0
SECTION 106 SE
SECTION 225 SE
SECTION 378 SE
SECTION 437 SE
118,500
119,000
130,500
130,000
KRAIN LAKE
OXIDE
VOLCANIC BOUNDARY
GETTY 4
GETTY 3
GETTY 1
GETTY 2
BETHLEHEM FELDSPAR PORPHYRY INTRUSIVE
GUICHON QTZ. DIORITE
(TOPO. INCOMPLETE FOR CLARITY)
-1993 DRILL PROGRAM