

SUB-RECORDER
RECEIVED #
MAY 30 1994
M.R. # \$
VANCOUVER, B.C.

**GEOLOGICAL, GEOCHEMICAL, GEOPHYSICAL
AND PHYSICAL
ASSESSMENT REPORT
ON THE
JOH, DARB, CROYDON, MARIPOSITE & KLIYUL
PROPERTIES**

LATITUDE: 56°30'N LONGITUDE: 126°08'W

FEBRUARY 1994

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

23,379

PART 1 OF 3

**Author: D.G.Gill, P. Geo. (Project Geologist)
Owner : Hemlo Gold Mines Inc.
Operator: Noranda Exploration Company, Limited
(No Personal Liability)**

FILMED

TABLE OF CONTENTS

| | <u>PAGE</u> |
|--|-------------|
| 1.0 INTRODUCTION..... | 1 |
| 1.1 Location and Access..... | 1 |
| 1.2 Topography and Physiography..... | 1 |
| 1.3 History..... | 3 |
| 1.4 Claims..... | 6 |
| 1.5 Economic Potential..... | 8 |
| 1.6 Survey Control..... | 17 |
| 1.7 Sampling..... | 17 |
| | |
| 2.0 GEOLOGY..... | 19 |
| 2.1 Regional..... | 19 |
| 2.2 Detailed..... | 19 |
| 2.3 Main & Moraine Grids..... | 19 |
| 2.4 Mineralization..... | 22 |
| 2.4.1 Skarn Mineralization..... | 22 |
| 2.4.2 Porphyry Style Mineralization..... | 24 |
| 2.4.3 Quartz Vein Mineralization..... | 25 |
| 2.4.4 Shear Related Mineralization..... | 25 |
| 2.5 Darb Lake Grid..... | 26 |
| | |
| 3.0 TEST PITTING..... | 28 |
| | |
| 4.0 SOIL GEOCHEMISTRY..... | 30 |
| 4.1 Gold..... | 30 |
| 4.2 Copper..... | 31 |
| | |
| 5.0 GEOPHYSICS..... | 33 |
| | |
| 6.0 CONCLUSIONS..... | 35 |

REFERENCES

APPENDICES

| | | |
|--------------|---|---|
| APPENDIX I | : | Laboratory Analytical Techniques |
| APPENDIX II | : | Soil Geochemical Results |
| APPENDIX III | : | Rock Geochemical Descriptions/Assay Sheets |
| APPENDIX IV | : | Pit Rock/Soil Descriptions/Assay Sheets |
| APPENDIX V | : | Combined Helicopter-Borne Magnetic, Electromagnetic, Radiometric and VLF-EM Survey Report |
| APPENDIX VI | : | Statement of Costs |
| APPENDIX VII | : | Statement of Qualifications |

DRAWINGS

SCALE

| | | |
|---------------------|---|-------------|
| 1. | Location Map..... | 1:2,000,000 |
| 2-9. | Claim Group Location Maps..... | 1:50,000 |
| 10. | Regional Geology..... | 1:50,000 |
| 11. | Kliyul Main Grid Geology..... | 1:5,000 |
| 12. | Darb Lake Grid Geology..... | 1:5,000 |
| 13. | Pit Locations..... | 1:5,000 |
| 14a. | Kliyul Main Grid - Test Pit Locations/Rocks..... | 1:5,000 |
| 14b. | Kliyul Main Grid - Test Pit Locations/Soils..... | 1:5,000 |
| 15. | Project Area Gold Soil Geochem (North Half)..... | 1:10,000 |
| 16. | Project Area Gold Soil Geochem (South Half)..... | 1:10,000 |
| 17. | Project Area Copper Soil Geochem (North Half).... | 1:10,000 |
| 18. | Project Area Copper Soil Geochem (South Half).... | 1:10,000 |
| 19. | Kliyul Main Area Gold Soil Geochem..... | 1:5,000 |
| 20. | Kliyul Main Area Copper Soil Geochem..... | 1:5,000 |
| 21. | Darb Lake Gold Soil Geochem..... | 1:5,000 |
| 22. | Darb Lake Copper Soil Geochem..... | 1:5,000 |
| 23 _{a,b} . | Kliyul Main & Moraine Grids Ground Mag..... | 1:5,000 |
| 24. | Airborne Base Map and Claim Locations..... | 1:20,000 |
| 25. | Airborne Flight Path..... | 1:20,000 |
| 26. | Airborne Interpretation..... | 1:20,000 |
| 27. | Airborne Total Field Magnetics..... | 1:20,000 |
| 28. | Airborne Vertical Magnetic Gradient..... | 1:20,000 |
| 29. | Airborne Apparent Resistivity (935 Hz Coaxial)... | 1:20,000 |
| 30. | Airborne Apparent Resistivity (800 Hz Coplanar).. | 1:20,000 |
| 31. | Airborne Apparent Resistivity (4600 Hz Coaxial).. | 1:20,000 |
| 32. | Airborne Apparent Resistivity (4175 Hz Coplanar). | 1:20,000 |
| 33. | Airborne Apparent Resistivity (32 Khz Coplanar).. | 1:20,000 |
| 34. | Airborne Total Field VLF-EM..... | 1:20,000 |
| 35. | Airborne Uranium Count Radiometrics..... | 1:20,000 |
| 36. | Airborne Thorium Count Radiometrics..... | 1:20,000 |
| 37. | Airborne Potassium Count Radiometrics..... | 1:20,000 |
| 38. | Airborne Total Count Radiometrics..... | 1:20,000 |
| 39. | Airborne Weight Percent Magnetite..... | 1:20,000 |

1.0 INTRODUCTION

During the period between July 4 and October 7, 1993 Noranda Exploration Company, Ltd. conducted prospecting, soil and rock geochemistry, mapping, test pitting and ground geophysics (mag) on the Joh, Darb, Croydon, Mariposite and Kliyul claim blocks. A helicopter-borne magnetic, electromagnetic, radiometric and VLF-EM survey was also completed over the survey area between July 20 to 22, 1993 by Geonex Aerodat Inc.

The focus of the exploration programme described in this report was to delineate further favorable stratigraphy and intrusive activity associated with the main Kliyul property skarn zone and to generate a stratigraphic model or section of the known mineralized horizons which would be useful in future regional mapping programmes throughout the claim blocks.

This report not only describes the work conducted by Noranda during the 1993 field programme but also incorporates historic data (gained through government assessment reports) to link all surveys together in an effort to define further possible Cu-Au skarn occurrences.

1.1 Location and Access

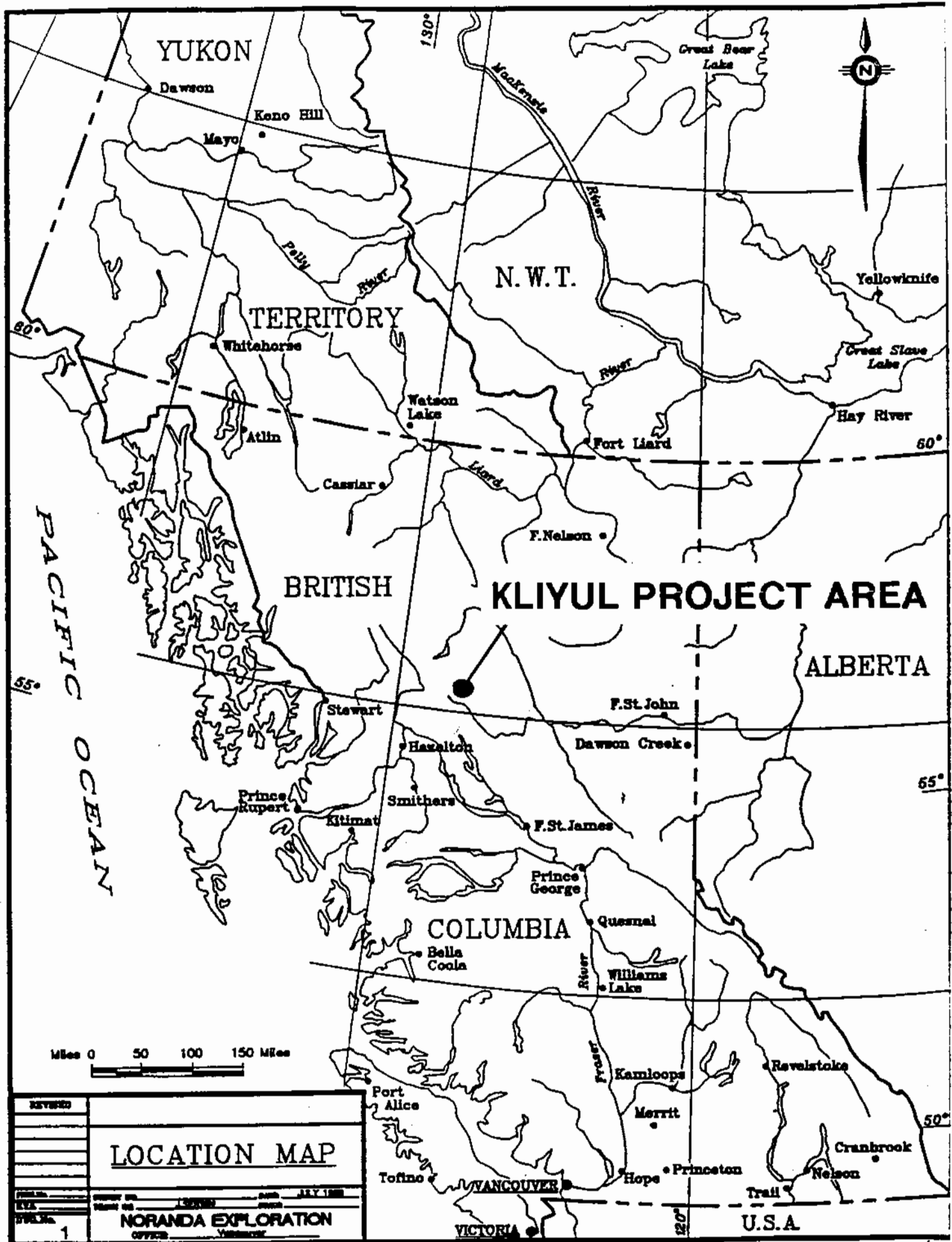
The Kliyul project area is located approximately 200 kms north-northeast of Smithers, B.C. on NTS Mapsheets 94D/8 and 9 in the Omineca Mining Division.

Camp mobilization was achieved by helicopter based at both the Osilinka Logging Camp and Suskeena Lodge (see Drawing #1).

1.2 Topography and Physiography

The Kliyul project area is situated within the Osilinka Ranges and is located directly east of Goldway and Dortatelle Peaks. The claim groupings stretch from Johanson Lake in the north to the upper portions of Kliyul Creek in the south. Most of the area is above treeline with elevations ranging from 3805 to 7480 feet. The project area is drained by Darb Creek in the north, Goldway and Dortatelle creeks to the west, Kliyul Creek in the south and the headwaters of Lay Creek to the north and east.

Slopes of +45° occur along east-west and dominantly north-northwest trending ridges although the central portion of the area (Kliyul claim block) consists of a gently sloping, wide marshy valley floor.



1.3 History

Below is a brief outline of documented work performed in the project area in chronological order.

- 1949: Preliminary work on auriferous quartz veins conducted by Goldway Peak Mines Ltd. in the Goldway Peak area.
- 1970-1972: The Kliyul property was staked and geochemically and geophysically surveyed by Kennco Explorations. These surveys delineated a 2.5 km x 1.0 km I.P. chargeability anomaly and coincident (yet smaller) copper soil geochemical and magnetic anomalies.
- 1971-1972: Geological, geochemical and geophysical (magnetics) surveys were conducted by El Paso Mining and Milling Co. who discovered skarn zones along the sheared contact between ultramafics and volcanics on lower Kliyul Creek.
- 1973: Kliyul property optioned to Sumac Mines Ltd. who drilled 3 x-ray holes (no results available).
- 1973: San Jacinto Explorations Ltd. performed soil surveying near the gold/quartz veins on Goldway Peak.
- 1974: Sumac Mines drilled 6 'BQ' holes on the Kliyul property to test the West and East Zone copper soil anomalies and 5 'BQ' holes into the magnetic high. The latter drill holes intersected magnetite - copper - gold mineralization within a well fractured, sericite, chlorite, epidote, carbonate, quartz, pyrite skarn hosted by calcareous andesite tuffs and agglomerates and lesser dioritic units. A reserve of 2.5 million tons of 0.3% Cu and 0.03 opt Au was returned from this skarn zone.
- 1974-1975: BP Minerals Ltd. completed geological, geochemical and geophysical (mag/JEM) over the Bap mineral claims which overly intensely sheared, clay-sericite altered feldspar porphyry volcanics/intrusives and auriferous quartz veins.
- 1976: Maxmin (EM) surveying completed over the Bap claims by BP Minerals Ltd.

- 1981: Geological and geochemical surveying was completed by Dupont of Canada on the AS 1 claim near Goldway Creek.
- 1981: Kennco and Vital Pacific drilled 4 NQ holes (1978 feet) into the central skarn zone on the Kliyul property; all in a southerly direction.
- 1982: A trace element study was performed by BP Minerals on previously collected samples from the Bap claims.
- 1982: Further geochemistry was completed in the Goldway Peak area by Dermot Fahey and by Laramie Mining Corporation.
- 1983: A preparatory study to determine road access to Goldway Peak was undertaken by Laramie Mining Corporation.
- 1984: BP Minerals relogged and sampled portions of available core and conducted geological mapping and geochemical sampling on the Kliyul property.
- 1984: Laramie Mining Corporation conducted mapping, geophysics (VLF) and sampling/assaying of their Goldway Peak property.
- 1984: Mapping and geochemistry was completed in the lower Kliyul Creek area by BP Resources , Canada, Ltd.
- 1984: After obtaining the KC 1 & 2 mineral claims and conducting preliminary sampling and prospecting, Golden Rule Resources Ltd. completed further geological, geochemical and geophysical (magnetics) surveys.
- 1985: Geological and geochemical surveying in the Goldway Peak area by BP Resources, Canada, Ltd. delineated auriferous quartz veins and fractures within quartz-carbonate-pyrite altered zones.
- 1985: Further geological, geochemical and geophysical work (magnetics, VLF) was performed by Golden Rule Resources Ltd. on the KC 1 & 2 claims.
- 1985-1986: Prospecting, mapping, trenching and sampling of the auriferous quartz veins in the Goldway Peak area continued with Laramie as the operator.

- 1986: Soil surveying was performed by Lemming Mining Resources for BP Resources on the Bap claims.
- Ritz Resources Ltd. for Goldnev Rule Resources Ltd. performed further geological, geochemical and geophysical (magnetics, VLF) work on the KC 1 & 2 claims.
- 1990: Placer Dome conducted linecutting, magnetometer and VLF-EM surveying, soil and rock sampling and prospecting on the Kliyul property in order to delineate magnetic anomalies similar to the known skarn zone, possible porphyry style mineralization and/or mineralized structures parallel to the large glacial valley.
- 1992: Noranda Exploration Company, Ltd. conducted 1:5,000 geological mapping on the Kliyul property, concentrating on alteration assemblages as well as rock and minor soil sampling.
- 1993: Noranda completed a 6 hole, 560 meter reverse circulation drill programme on the Kliyul main skarn zone. Results were encouraging enough to pursue options on surrounding properties which host similar stratigraphy, intrusives and mineralization.

1.4 Claims

The claims which comprise the Joh, Darb, Croydon, Mariposite and Kliyul properties are listed below by groupings with corresponding owners, expiry dates, tenure numbers and property names.

| GROUP | CLAIM | TITLE | UNITS | EXPIRY DATE | OWNER | PROPERTY |
|-------|--------|--------|-------|---------------|------------------|------------|
| KLI | KLI 1 | 245065 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 2 | 245066 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 3 | 245067 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 4 | 245068 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 5 | 245069 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 6 | 245070 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 7 | 245071 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 8 | 245072 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 9 | 245073 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 10 | 245074 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 11 | 245075 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 12 | 245076 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 13 | 245077 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 14 | 245078 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 15 | 245079 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 16 | 245080 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 17 | 245081 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 18 | 245082 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 19 | 245083 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 20 | 245084 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 21 | 245155 | 1 | Sep. 11, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 25 | 245156 | 1 | Sep. 11, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 26 | 245157 | 1 | Sep. 11, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 27 | 245158 | 1 | Sep. 11, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 28 | 245159 | 1 | Sep. 11, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 39 | 245382 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 40 | 245383 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 41 | 245384 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 42 | 245385 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 43 | 245386 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 44 | 245387 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 45 | 245388 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 46 | 245389 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 47 | 245390 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 48 | 245391 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 49 | 245392 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | KLI 50 | 245393 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | UTA 4 | 245777 | 1 | Aug. 29, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | UTA 6 | 245778 | 1 | Aug. 29, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | UTA 8 | 245779 | 1 | Aug. 29, 2004 | Hemlo Gold Mines | Kliyul |
| KLI | YUL 7 | 319492 | 1 | Jul. 15, 2000 | Hemlo Gold Mines | Mariposite |
| KLI | YUL 8 | 319493 | 1 | Jul. 15, 2000 | Hemlo Gold Mines | Mariposite |
| KLI | YUL 9 | 319494 | 1 | Jul. 15, 2000 | Hemlo Gold Mines | Mariposite |
| KLI | YUL 10 | 319495 | 1 | Jul. 15, 2000 | Hemlo Gold Mines | Mariposite |
| KLI | YUL 11 | 319496 | 1 | Jul. 15, 2000 | Hemlo Gold Mines | Mariposite |

| GROUP | CLAIM | TITLE | UNITS | EXPIRY DATE | OWNER | PROPERTY |
|---------|--------|--------|-------|---------------|-------------------|------------|
| KLI | YUL 12 | 319497 | 1 | Jul. 20, 2000 | Hemlo Gold Mines | Mariposite |
| KLI | YUL 13 | 319498 | 1 | Jul. 20, 2000 | Hemlo Gold Mines | Mariposite |
| KLI | DARB 2 | 316541 | 1 | Mar. 10, 2000 | Hemlo Gold Mines | Mariposite |
| CRO | JO 7 | 242399 | 15 | Jul. 12, 1995 | Golden Rule Res. | DARB |
| CRO | JO 8 | 242400 | 20 | Jul. 12, 1995 | Golden Rule Res. | DARB |
| CRO | CRO 2 | 242402 | 20 | Jul. 11, 1995 | Golden Rule Res. | DARB |
| CRO | CRO 3 | 242403 | 20 | Jul. 11, 1995 | Golden Rule Res. | DARB |
| CRO | CRO 4 | 242404 | 20 | Jul. 11, 1995 | Golden Rule Res. | DARB |
| CRO | YUL 3 | 318890 | 1 | Jul. 6, 1995 | Hemlo Gold Mines | Mariposite |
| CRO | YUL 4 | 318891 | 1 | Jul. 6, 1995 | Hemlo Gold Mines | Mariposite |
| CRO | YUL 5 | 318892 | 1 | Jul. 6, 1995 | Hemlo Gold Mines | Mariposite |
| CRO | YUL 6 | 318893 | 1 | Jul. 6, 1995 | Hemlo Gold Mines | Mariposite |
| Goldway | DARB 1 | 316540 | 1 | Mar. 10, 1996 | Hemlo Gold Mines | Mariposite |
| Goldway | DORT 1 | 316536 | 20 | Mar. 10, 1996 | Hemlo Gold Mines | Mariposite |
| Goldway | DORT 2 | 316537 | 20 | Mar. 10, 1996 | Hemlo Gold Mines | Mariposite |
| Goldway | DORT 3 | 316538 | 20 | Mar. 10, 1996 | Hemlo Gold Mines | Mariposite |
| Goldway | DORT 4 | 316539 | 12 | Mar. 10, 1996 | Hemlo Gold Mines | Mariposite |
| JO | KLI 12 | 245076 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JO | KLI 14 | 245078 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JO | KLI 15 | 245079 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JO | KLI 39 | 245382 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| JO | KLI 40 | 245383 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| JO | KLI 43 | 245386 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| JO | KLI 44 | 245387 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| JO | KLI 45 | 245388 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| JO | KLI 46 | 245389 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| JO | JO 4 | 242396 | 20 | Jul. 13, 1996 | Golden Rule Res. | DARB |
| JO | JO 5 | 242397 | 20 | Jul. 13, 1995 | Golden Rule Res. | DARB |
| JO | JO 6 | 242398 | 18 | Jul. 12, 1996 | Golden Rule Res. | DARB |
| JO | YUL 1 | 318888 | 1 | Jul. 6, 2000 | Hemlo Gold Mines | Mariposite |
| JO | YUL 2 | 318889 | 1 | Jul. 6, 2000 | Hemlo Gold Mines | Mariposite |
| CROYDON | KC 1 | 238258 | 20 | Apr. 8, 1998 | Golden Rule Res. | Croydon |
| CROYDON | KC 2 | 238259 | 20 | Apr. 8, 1998 | Golden Rule Res. | Croydon |
| CROYDON | CRO 1 | 242401 | 18 | Jul. 14, 1995 | Golden Rule Res. | Croydon |
| CROYDON | CRO 5 | 242405 | 6 | Jul. 14, 1995 | Golden Rule Res. | Croydon |
| CROYDON | YUL 14 | 319639 | 18 | Jul. 31, 1995 | Hemlo Gold Mines | Mariposite |
| CROYDON | YUL 15 | 319640 | 16 | Jul. 31, 1995 | Hemlo Gold Mines | Mariposite |
| KLI-UTA | KLI 1 | 245065 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI-UTA | KLI 3 | 245067 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| KLI-UTA | KLI 48 | 245391 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| KLI-UTA | KLI 49 | 245392 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| KLI-UTA | KLI 50 | 245393 | 1 | Jul. 12, 2004 | Hemlo Gold Mines | Kliyul |
| KLI-UTA | UTA 6 | 245778 | 1 | Aug. 29, 2004 | Hemlo Gold Mines | Kliyul |
| KLI-UTA | UTA 8 | 245779 | 1 | Aug. 29, 2004 | Hemlo Gold Mines | Kliyul |
| KLI-UTA | JOH 3 | 242521 | 20 | Aug. 1, 1996 | Major General Res | JOH |
| KLI-UTA | JOH 5 | 242523 | 20 | Aug. 1, 1996 | Major General Res | JOH |
| KLI-UTA | JOH 6 | 242524 | 20 | Aug. 1, 1996 | Major General Res | JOH |

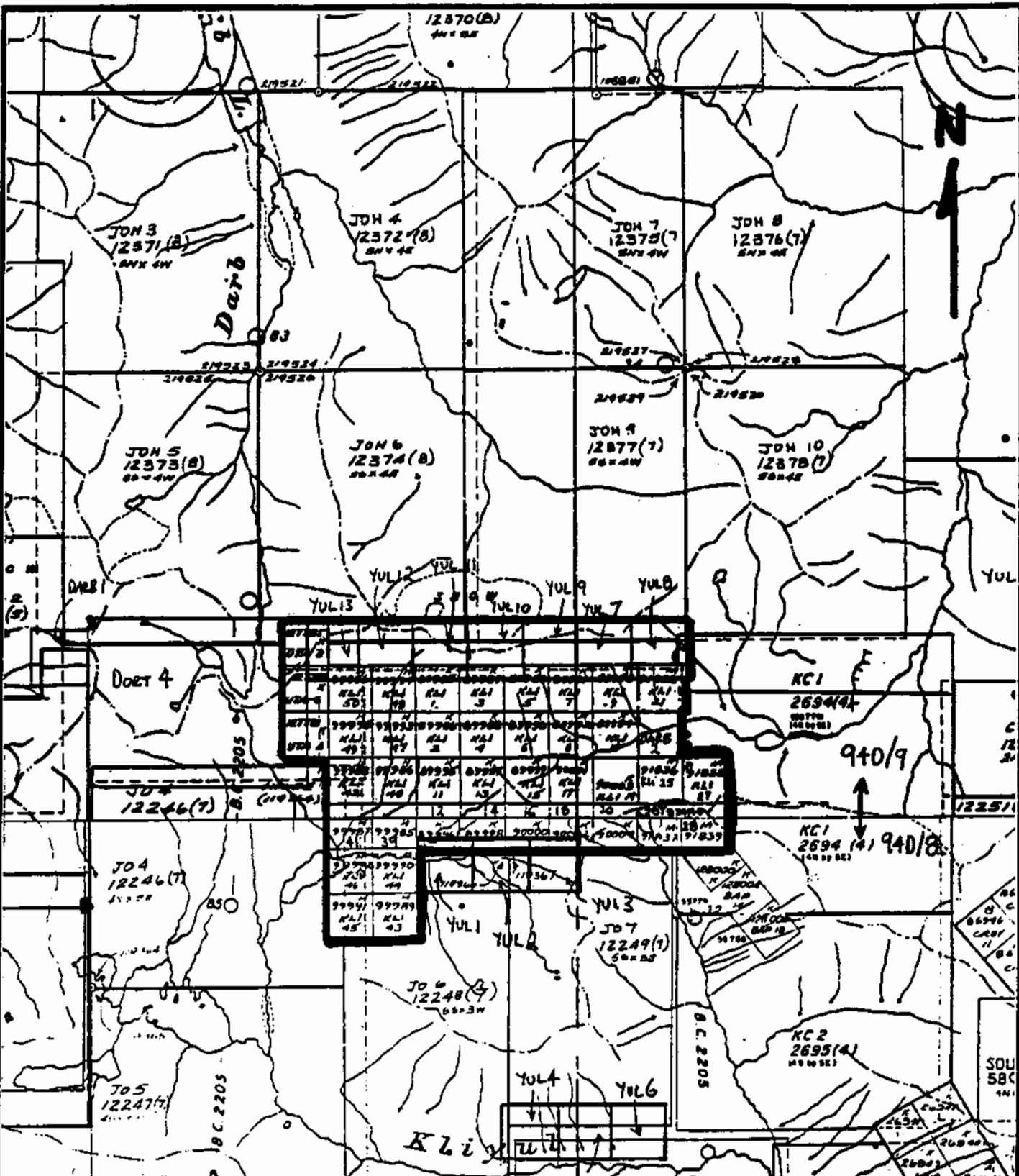
| GROUP | CLAIM | TITLE | UNITS | EXPIRY DATE | OWNER | PROPERTY |
|-------|--------|--------|-------|---------------|-------------------|------------|
| JOH 1 | KLI 5 | 245069 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 1 | KLI 6 | 245070 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 1 | KLI 8 | 245072 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 1 | KLI 10 | 245074 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 1 | KLI 17 | 245081 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 1 | KLI 19 | 245083 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 1 | KLI 20 | 245084 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 1 | KLI 25 | 245156 | 1 | Sep. 11, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 1 | KLI 26 | 245157 | 1 | Sep. 11, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 1 | KLI 27 | 245158 | 1 | Sep. 11, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 1 | DARB 2 | 316541 | 1 | Mar. 10, 2000 | Hemlo Gold Mines | Mariposite |
| JOH 1 | JOH 1 | 242519 | 20 | Aug. 1, 1996 | Major General Res | JOH |
| JOH 1 | JOH 4 | 242522 | 20 | Aug. 1, 1997 | Major General Res | JOH |
| JOH 1 | JOH 9 | 242527 | 20 | Jul. 31, 1997 | Major General Res | JOH |
| JOH 1 | YUL 9 | 319494 | 1 | Jul. 15, 2000 | Hemlo Gold Mines | Mariposite |
| JOH 2 | KLI 5 | 245069 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 2 | KLI 6 | 245070 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 2 | KLI 8 | 245072 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 2 | KLI 10 | 245074 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 2 | KLI 17 | 245081 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 2 | KLI 19 | 245083 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 2 | KLI 20 | 245084 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 2 | KLI 25 | 245156 | 1 | Sep. 11, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 2 | KLI 26 | 245157 | 1 | Sep. 11, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 2 | KLI 27 | 245158 | 1 | Sep. 11, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 2 | KLI 9 | 245073 | 1 | Aug. 10, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 2 | KLI 21 | 245155 | 1 | Sep. 11, 2004 | Hemlo Gold Mines | Kliyul |
| JOH 2 | DARB 2 | 316541 | 1 | Mar. 10, 2000 | Hemlo Gold Mines | Mariposite |
| JOH 2 | YUL 8 | 319493 | 1 | Jul. 15, 2000 | Hemlo Gold Mines | Mariposite |
| JOH 2 | JOH 10 | 242528 | 20 | Jul. 31, 1997 | Major General Res | JOH |
| JOH 2 | JOH 8 | 242526 | 20 | Jul. 31, 1996 | Major General Res | JOH |
| JOH 2 | JOH 7 | 242525 | 20 | Jul. 31, 1997 | Major General Res | JOH |
| JOH 2 | JOH 2 | 242520 | 20 | Aug. 1, 1997 | Major General Res | JOH |
| * | BAP 10 | 245780 | 1 | Aug. 13, 1998 | Trinity Control | Croydon |
| * | BAP 14 | 245781 | 1 | Aug. 13, 1998 | Trinity Control | Croydon |
| * | BAP 18 | 245782 | 1 | Aug. 13, 1998 | Trinity Control | Croydon |
| * | JOH 11 | 242606 | 20 | Aug. 21, 1995 | Major General Res | JOH |
| * | JOH 12 | 242607 | 20 | Aug. 21, 1995 | Major General Res | JOH |
| * | JOH 13 | 242608 | 18 | Aug. 21, 1995 | Major General Res | JOH |

* Claims which are part of the property but were not grouped and to which no assessment is being applied.

Please refer to the Statement of Exploration forms at the beginning of this report for further clarification of assessment and work performed on each claim. Following are a series of maps showing the claim groupings involved.

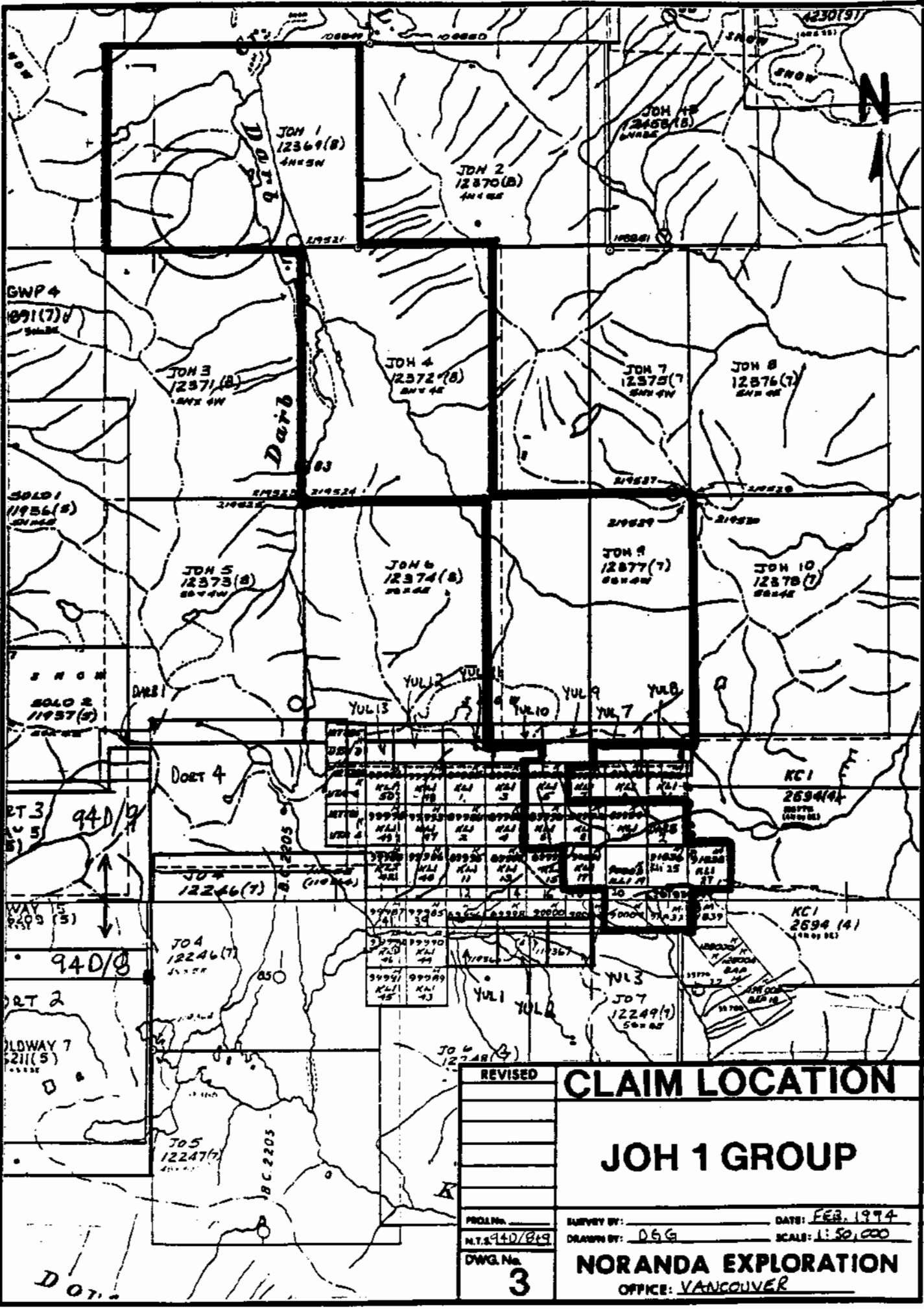
1.5 Economic Potential

The Kliyul project area is considered to be ideal for hosting high grade Cu-Fe-Au skarn deposits and/or bulk tonnage Au-Cu deposits for the following reasons.



| | | |
|------------------------|----------------------------|------------------------|
| REVISED | CLAIM LOCATION | |
| | KLI GROUP | |
| PROJ. No. | SURVEY BY: <u>D.G.G.</u> | DATE: <u>FEB. 1974</u> |
| N.T.S. <u>1:50,000</u> | DRAWN BY: <u>D.G.G.</u> | SCALE: <u>1:50,000</u> |
| DWG. No. | NORANDA EXPLORATION | |
| 2 | OFFICE: <u>VANCOUVER</u> | |

AMCAL 11807

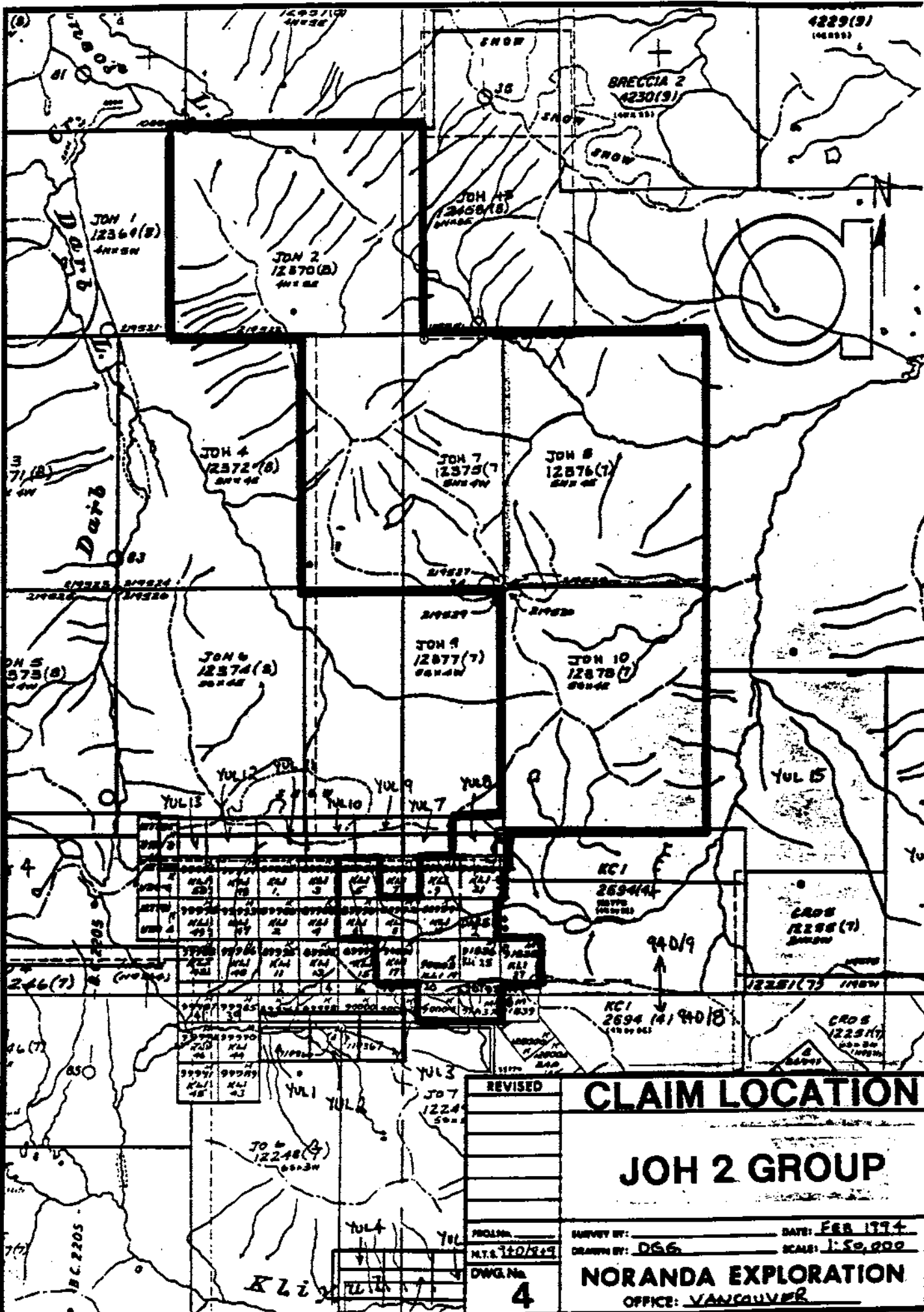


CLAIM LOCATION

JOH 1 GROUP

REVISED _____
 PROJ. No. _____ SURVEY BY: _____ DATE: FEB. 1974
 N.T.S. 940/819 DRAWN BY: D.S.G. SCALE: 1:50,000
 DWG. No. **3** NORANDA EXPLORATION
 OFFICE: VANCOUVER

VANCAL 11827



| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|-----|
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|-----|

REVISD

CLAIM LOCATION

JOH 2 GROUP

PROGRAM: _____ SURVEY BY: _____ DATE: FEB 1974

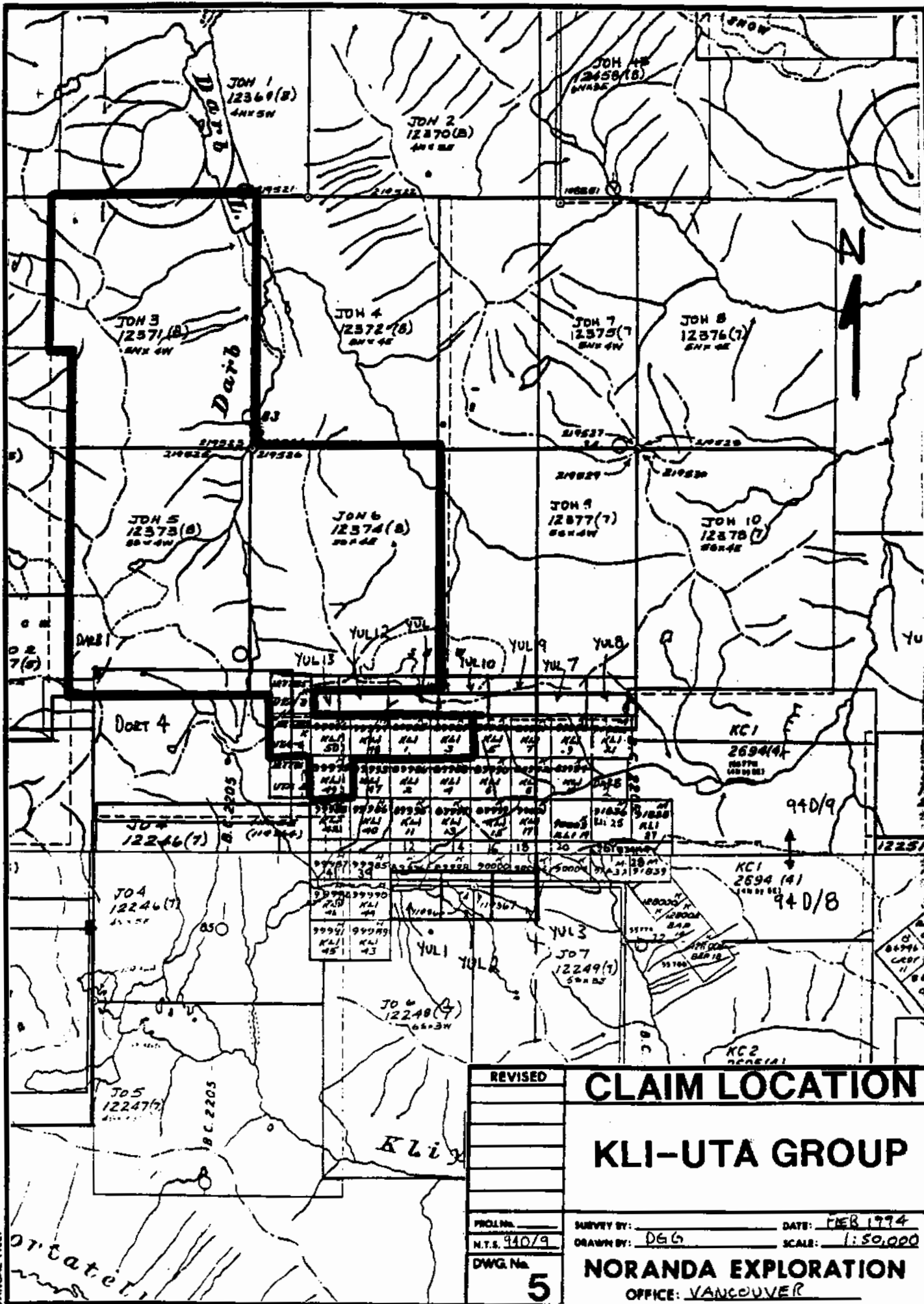
N.T.S. 1:20,000 DRAWN BY: DSG SCALE: 1:50,000

DWG. No. **4**

NORANDA EXPLORATION

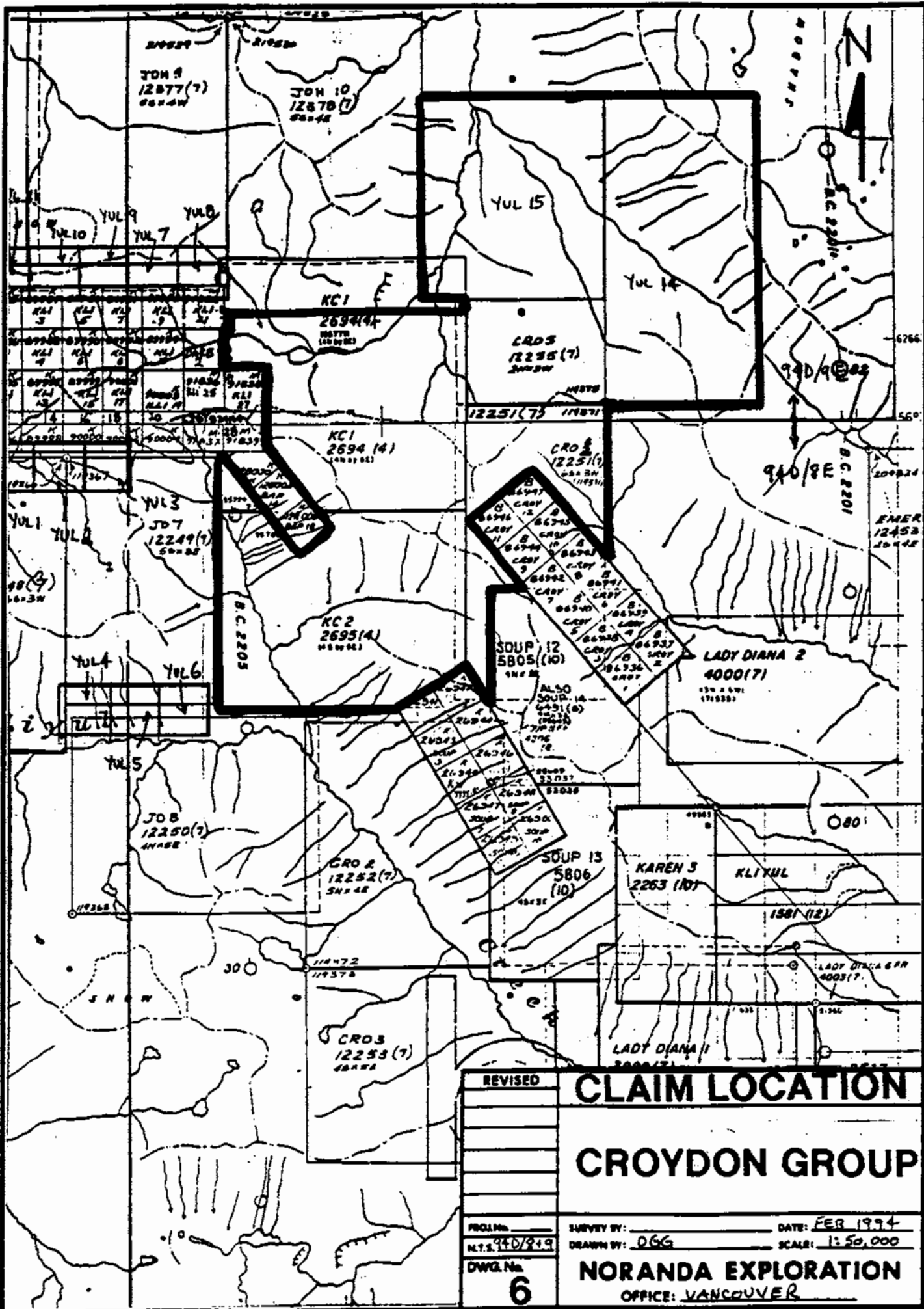
OFFICE: VANCOUVER

MINERAL 11087

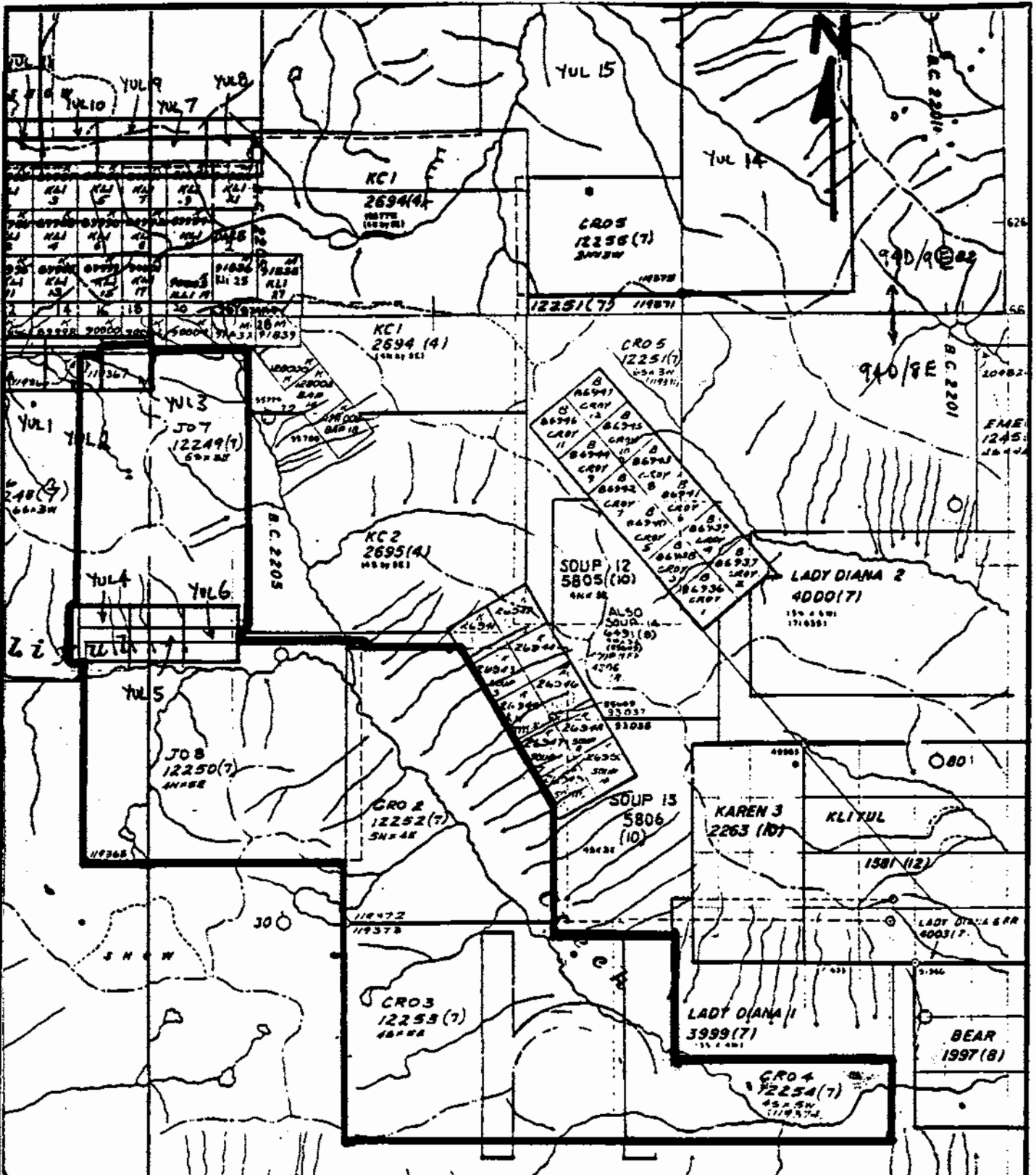


| | | |
|--------------|----------------------------|-----------------|
| REVISED | CLAIM LOCATION | |
| | KLI-UTA GROUP | |
| PROJ. No. | SURVEY BY: | DATE: FEB 1974 |
| N.T.S. 940/9 | DRAWN BY: DGL | SCALE: 1:50,000 |
| DWG. No. | NORANDA EXPLORATION | |
| 5 | OFFICE: VANCOUVER | |

VANCAL 11827

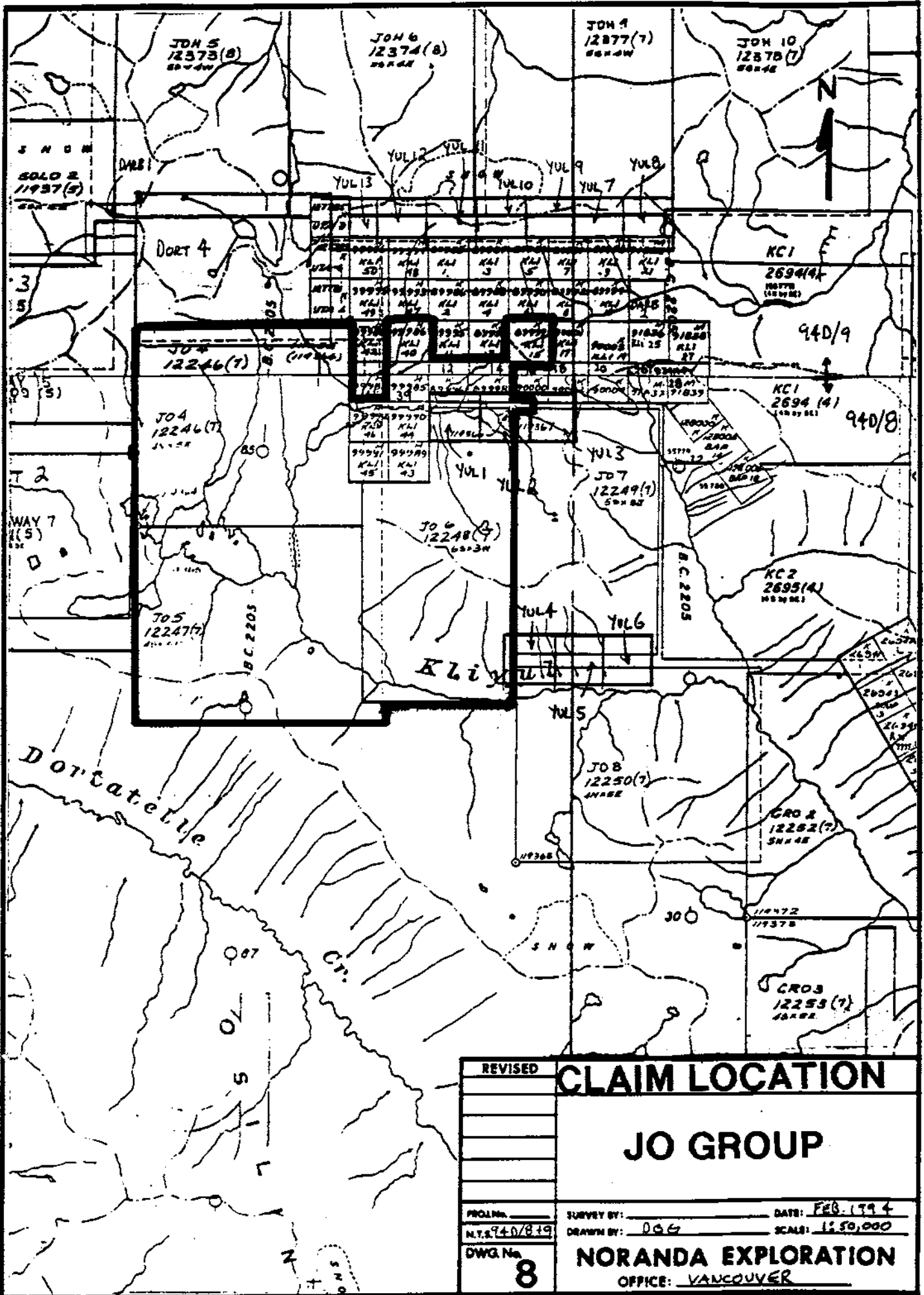


VANCOUVER 11827



| | | |
|-------------------|----------------------------|-----------------|
| REVISED | CLAIM LOCATION | |
| | CRO GROUP | |
| PROJ. No. _____ | SURVEY BY: _____ | DATE: FEB 1994 |
| N.T.S. 747/B | DRAWN BY: DGG | SCALE: 1:50,000 |
| DWG. No. 7 | NORANDA EXPLORATION | |
| | OFFICE: VANCOUVER | |

VANCAL 11927



| | | |
|-------------------|----------------------------|-----------------|
| REVISED | CLAIM LOCATION | |
| | JO GROUP | |
| PROJ. No. _____ | SURVEY BY: _____ | DATE: FEB. 1994 |
| N.T.S. 740/819 | DRAWN BY: DGG | SCALE: 1:50,000 |
| DWG. No. 8 | NORANDA EXPLORATION | |
| | OFFICE: VANCOUVER | |

ANCAL 11827



94D/9W

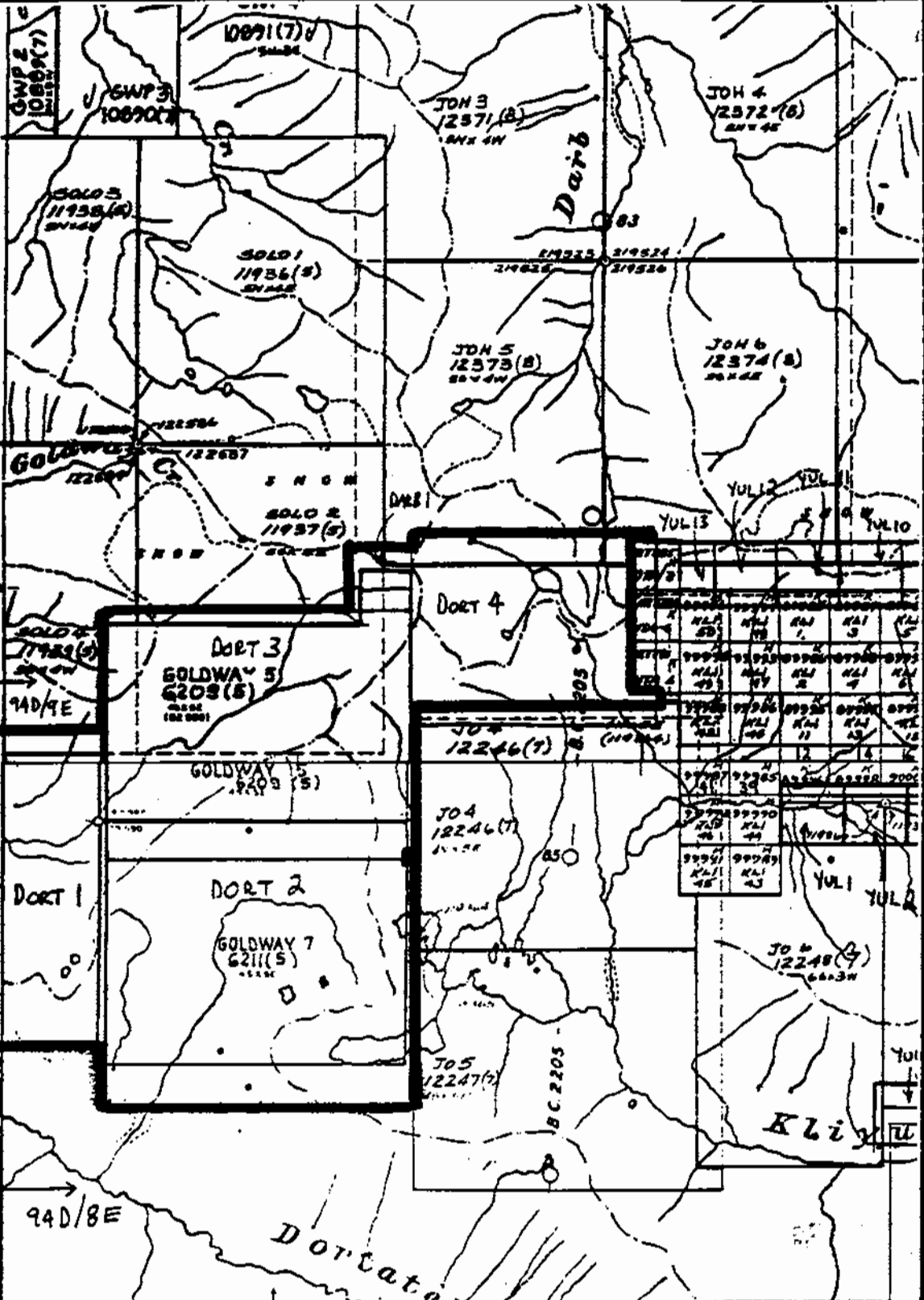
94D/9E

ON
M 94D/8E
B.C. 2206

94D/8W

94D/8E

(FOR PLACER SEE P 94D/8E)



| | | |
|----------------|----------------------------|-----------------|
| REVISED | CLAIM LOCATION | |
| | GOLDWAY GROUP | |
| PROJ. No. | SURVEY BY: | DATE: FEB 1994 |
| M.T.S. 74D/8E9 | DRAWN BY: DGG | SCALE: 1:50,000 |
| DWG. No. | NORANDA EXPLORATION | |
| 9 | OFFICE: VANCOUVER | |

1. Favorable stratigraphy (Takla volcanics) and related intrusive complexes (monzonites-diorites) which form the northern part of the Hogem Batholith, a large hydrothermal cell associated with known porphyry Cu deposits (Mt. Milligan).
2. Known Cu-Fe-Au skarn occurrences exist on the property(ies) within the same calcareous stratigraphic horizon which remains under-explored.
3. The positioning between the Cu rich porphyry systems to the south and Au-Cu rich porphyry and epithermal deposits to the north (Kemess/Cheni) may suggest a more Au rich zonation as one moves northward from the Hogem Batholith.

1.6 Survey Control

The surveying of the flagged and picketed grid lines was conducted with the aid of a compass and metric hipchain. A Geographical Positioning System unit was also used to better locate the baseline established by Placer Dome in 1990 which was used by Noranda for control of the Main grid. Other reconnaissance style grids (i.e. Recce, Darb Lake and Moraine grids) were labeled with reference to arbitrarily picked coordinates or the large grid covering the Joh property established by Reliance Geological in 1992.

1.7 Sampling

Soil sampling was conducted along metrically chained lines with samples taken every 50-100 meters apart to the depth of 20-40 cm with the aid of a shovel or mattock. Soils were collected in brown Kraft envelopes for drying, storage and shipping purposes and sent to Noranda Exploration Laboratory at Unit #1, 7550 - 76th Street, Delta, B.C. (as were all other samples).

Rock samples were collected as grabs or chips across certain widths whenever representative, altered and/or mineralized formations were encountered.

Test pits were initially dug at 50 meter intervals along 200 meter spaced lines and later tightened to 100 m spaced lines where warranted. Composite samples of mineralized/altered bedrock were collected from the bottom of the pits whereas soils were collected at different depths and/or at the bottom of the pits if bedrock was not encountered. Numbering of the test pit samples used an alpha numeric system denoting the property, the pit number and the depth in meters from where the sample was collected as shown below.

KLP-33-3.5
(Kliyul Pit - number - depth in meters)

Please refer to Appendix I for the laboratory analytical techniques and Appendix III and IV for sample assay values and descriptions where applicable.

A total of 433 soils, 107 rocks, 160 pit soils and 216 pit rocks and their accompanying analytical charges are being applied for assessment.

2.0 GEOLOGY

2.1 Regional

The Kliyul property is situated within the Intermontane Belt which is comprised of Upper Triassic to Lower Jurassic island arc volcanics, volcanoclastics and minor sediments of the Takla Group which hosts such Cu-Au porphyry deposits as Mt. Milligan and Kemess. The dominantly volcanic package in the Kliyul Creek area has been intruded by Jura-Cretaceous aged diorites, monzonites and syenites associated with the Hogem Batholith.

Prominent structural features in the area include NW, E-W, N-S and NNE-SSW trending fault systems. At Kliyul the first two systems seem to be closely related to mineralization.

2.2 Detailed

Geological surveying of the Kliyul project area was conducted at 1:5,000 scale on the Main (Drawing 11) and Darb Lake (Drawing 12) grids using flagged, metrically chained grid lines and topographic bases for control. The resulting map (Drawing 11) for the Kliyul property is a combination of Noranda's 1992 and 1993 mapping and shows rock types, rock sample locations, test pit locations and drill sites.

2.3 Main & Moraine Grids

Mapping has confirmed that the survey area is underlain by a late Triassic aged volcano-sedimentary succession of Takla Group rocks intruded by Triassic-Jurassic aged gabbro/pyroxenites, listwanites, monzonites and diorites and Cretaceous aged quartz monzonites/diorites.

The southeast section of the property is dominated by massive feldspar +/- augite phyric andesitic tuffs and flows (Unit 1) which are intercalated with beds of fine grained laminated, white to grey limestones and agglomerates with a limy matrix containing large clasts (up to 30-40 cms) of limestone and volcanic derived material (Unit 3). Pyritic, dark grey, finely laminated sediments (sandstones, argillites, Unit 4) stratigraphically overlie the section of impure limestones. Locally the sedimentary pile also contains sections of graphitic mudstones and shales (Unit 5). Bedding and foliation orientations suggest that the volcano-sedimentary package in this area of the grid strikes northwest and dips moderately northeast.

DARB LAKE



LAY CK.

2

KLIYUL CLAIMS

2

4

2

KLIYUL CK.

4

SOUP CLAIMS

4

3

DORATELLE CK.

2

3

2

LEGEND

INTRUSIVES



DIORITE, MONZONITE, SYENITE



ULTRAMAFIC ROCKS (PYROXENITE)

TAKLA VOLCANICS (UP. TRIASSIC)



ANDESITES



SEDIMENTS (ss, arg. lst.)

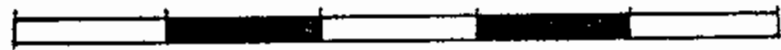
10



REGIONAL GEOLOGY

KLIYUL CREEK AREA

0 1 2 3 4 5 KMS



★ OCCURRENCES

SCALE 1:50,000

Unconformably overlying the above mentioned stratigraphy in the far southeast portion of the map area are flat lying, massive dark green augite porphyry flows and tuffs which are typically magnetic and well epidotized. Brecciation of this unit (#6) is thought to be related to faulting and late cross-cutting dykes.

Similar stratigraphy is evidenced in the north-central portion of the grid area where the rocks are folded in a shallow syncline with an east-west axial trace. The southern limb strikes east-west with shallow dips to the north. Local north-south strikes, easterly dips within the sediments on this limb of the fold are due to moderate intrafolding. The northern limb of the syncline exhibits moderately steep dips to the southeast which are exposed on the north facing slopes of an east-west trending ridge underlain by augite porphyry flows.

In the west-central portion of the grid the predominantly volcanic rich sequence of undifferentiated andesitic tuffs and flows is observed with a basic east-west trending orientation and intercalated with a pervasively epidotized fragmental andesite which exhibits predominantly angular felsic intrusives clasts (Unit 2). Further west the stratigraphy begins to strike north-south with moderate to shallow east dips observed in the sedimentary package.

It is postulated that the sedimentary sequences within the Takla Group observed in the gridded area represent one distinct stratigraphic horizon. However, it is unclear whether the sequence of argillites/limestones to the south and west of the large northwest-southeast trending fault (marked by listwanite outcroppings) is connected below surface to the similar sedimentary package in the northern portion of the survey area by gentle, east-west trending folds or if the large east-west trending fault marked by the headwaters of west Kliyul Creek and Lay Creek and by patches of ferrocrete (or another unobserved fault to the north of the baseline) has caused vertical displacement between the two major sedimentary occurrences.

Intrusive rocks observed during the mapping programme consist of listwanites (Unit 8), gabbro/pyroxenites (Unit 9), altered monzonite/diorite (Unit 10), melanocratic diorites (Unit 11 including microdiorite dykes), leucocratic diorites (Unit 12), quartz monzonites (Unit 13) and fine to medium grained feldspar porphyry dykes (Unit 14).

The predominant trend of intrusive occurrences on the grid appears southeast to northwest. In the southeast portion a gabbro/pyroxenite intrusive occurs along a sheared/faulted contact between the sedimentary-volcanic package to the south and highly altered and foliated monzonite/diorite to the north. This ultramafic intrusive grades or alters to listwanite and continues northwest for 2500 meters before disappearing under glacial drift cover of the West Kliyul Creek valley and is again exposed in the far northwest portion of the map area. It is not known if the listwanite dyke crosscuts the east-west trending fault along the baseline or if the listwanite and altered monzonite/diorite intrusives have been left laterally displaced for approximately 1.5 kms in an east-west direction.

The most visually striking intrusive in the survey area consists of an intensely sheared, bleached, pyritic (5-10%), strongly to moderately sericite-quartz-clay altered and gossaned sheeted dyke complex ranging in composition from feldspar porphyritic diorite to feldspar +/- quartz porphyritic monzonite. This intrusive complex also strikes northwest and exists near Divide Lake through to the main skarn mineralization and area of drilling and test pitting. Other occurrences of Unit 10 can be observed as plugs/dykes on lines 2600E & 2800E/2500N and in the northwest corner of the grid along line 800E.

Field observations of contact relationships suggest that the next phase of intrusion consists of the massive, medium to coarsely crystalline, melanocratic diorite which outcrops as a plug on the east side of the headwaters of East Kliyul Creek between lines 4000E & 4800E, on line 3200E, 1800N, intruding the altered feldspar porphyritic monzonite/diorite, on lines 1000E & 1200E, 2400N, on the southwest portions of the Moraine grid and to the far east-central part of the grid on lines 5600-6000E/2400N. This unit stands out as a strong magnetic anomaly on the airborne vertical magnetic gradient map due to finely disseminated magnetite. The unit appears relatively fresh and uniform and averages 40% mafics (hornblende), 50% plagioclase and minor potassium feldspar. It is believed that this intrusive phase is responsible for the subsequent altering of the feldspar porphyry monzonite/diorite and introduction of the Fe-Cu-Au skarn mineralization.

Other smaller dykes and plugs of medium grained, leucocratic diorite and felsic, feldspar porphyry dykes occur throughout the property while to the northwest and northeast corners of the grid exist larger, younger, fresh looking quartz monzonites of probable Cretaceous age.

2.4 Mineralization

To date four styles of mineralization including skarn, intrusive hosted porphyry, quartz veining and shear zone related have been recognized through the 1993 mapping and testpitting programmes.

2.4.1 Skarn Mineralization

Mineralization on the Kliyul property is manifested as finely disseminated, stringer type and clasts of magnetite and chalcopyrite hosted in chlorite-epidote-carbonate altered andesites and calcareous sediments (limy agglomerates). Although only one outcrop (excluding the test pitting) of the skarn is exposed it is believed that the volcanic-sedimentary sequence is dipping approximately 20° to the south/southwest through drilling information.

Results from a composite grab sample (185-E) taken across the exposed skarnified outcrop (2800E/2020N) in 1992 returned values of 1.4 gpt Au/15.0 m.

Results of the best values obtained from test pit rock samples are shown below (excluding quartz vein samples). These 15 samples outline a rough west-northwest trend which conforms to the trend of the sericite-clay altered and sheared feldspar porphyry monzonite and the subsequent medium grained melanocratic diorite (thought to be the source of the main skarn mineralization). Results of the test pit soil and rock sampling are shown on Drawing 14a and b. Also, refer to Appendix IV for testpit locations and rock descriptions.

| TEST PIT | LOCATION EAST NORTH | Cu (ppm) | Au (ppm) |
|----------|------------------------|-------------|-------------|
| KLP-152 | 2700 1940 | 2393 | - |
| KLP-153 | 2700 1965 | 8948 | 2700 |
| KLP-16 | 2800 1950 | 1926 | 1700 |
| KLP-20 | 2800 1740 | 1228 | - |
| KLP-176 | 2850 1800 | 1105 | - |
| KLP-226 | 2850 1750 | 1491 | - |
| KLP-144 | 2900 1850 | 2017 | - |
| KLP-147 | 2900 1700 | 1695 | - |
| KLP-24 | 3000 1750 | 15000 | 1200 |
| KLP-124 | 3100 1850 | 2990 | 410 |
| KLP-121 | 3100 1700 | 1110 | - |
| KLP-96 | 3500 1800 | 1453 | 500 |
| KLP-91 | 3700 1500 | - | 580 |
| KLP-141 | 2900 2010 | 2463 | - |
| KLP-26 | 3000 1850 | 1504 | - |

Other skarn mineralization found to date includes the area centered on lines 3300 and 3400E, 2150N where values returned up to 420 ppb Au and 1321 ppm Cu in pits 52 and 112; skarn float (382-L) at 3290E/2240N which returned 3728 ppm Cu, 810 ppb Au; 2925E/2650N, an area of skarnified magnetite rich volcanic tuff which ran 1200 ppb Au (394E) located near the volcanic-sedimentary sequence in the north-central portion of the grid; 1465E/2850N where pyrite-magnetite-epidote skarn exists in an andesitic host near the contact with the overlying augite porphyry with results of 2750 ppm Cu, 990 ppb Au.

The most significant mineralized skarn occurrence (excluding the main Kliyul zone) is centered on Line 2600E/3050N and is known as the Pacific Sugar Zone. Here melanocratic diorite intrudes the calcareous sediment-volcanic package near the top of the ridge in the north-central portion of the grid. Anomalous results on the weight percent magnetite and vertical magnetic gradient airborne maps are centered on this area and perhaps reflect a magnetite rich skarn zone covered by magnetic augite porphyry flows. This area remains the most prospective mineralized area found to date in the area. Best results returned from this zone are listed below.

| SAMPLE | TYPE | WIDTH | Cu (ppm) | Au (ppb) |
|--------|-------|-------|----------|----------|
| 378-Q | Chip | 1.5 m | 6014 | 1000 |
| 379-R | Float | - | 13000 | 4400 |
| 379-S | Float | - | 794 | 4600 |
| 391-L | Grab | - | 6381 | 1200 |
| 379-I | Float | - | 9804 | 2000 |
| 1679-M | Float | - | 8064 | 10,600 |
| 1679-Q | Float | - | 13000 | 1730 |
| 1679-U | Float | - | 8304 | 4100 |
| 1679-W | Float | - | 13000 | 880 |

Most of the sampling of this occurrence was done from talus slopes below the outcroppings of mineralized skarn as steep bluffs and cliffs hampered a proper sampling program of the in-situ mineralization. Mineralization consists locally of massive magnetite with up to 20% coarse grained pyrite and up to 5% interstitial and disseminated chalcopyrite in melanocratic diorite hosts. The mineralization is also associated with quartz stringers and carbonitization. Chalcopyrite also occurs without magnetite within quartz and is also finely disseminated within the host skarn. Skarn mineralogy consists of medium to fine grained pyroxene, actinolite with strong epidotization and minor garnet. Azurite/malachite staining is common.

Well developed sulfide banding was observed within silicified, mineralized limestone exoskarn boulders. The style and composition of exoskarn mineralization is similar to that of the endoskarn.

2.4.2 Porphyry Style Mineralization

Several large gossanous areas occur throughout the map area and can be attributed to pyrite and silica, sericite and a combination of quartz-sericite-pyrite altered zones ranging in intensity from weak to intense and may represent different alteration zones associated with a series of smaller (or one large) porphyry hydrothermal cell(s). All gossanous zones appear to be related to large structural breaks (and corresponding alignment of intrusive rocks) which are delineated by the presence of incised gulleys, alignment of creeks and lakes, patches of ferrocrete and large dykes or dyke complexes. The main trends of these zones are east-west, north-south and east-southeast to west-northwest.

The largest of these altered zones is the quartz-sericite-kaolinite-pyrite (up to 15%) zone located in the southeast corner of the survey area which extends to the southeast onto the Bap mineral claims (Golden Rule Resources Ltd.). This area is predominantly underlain by foliated feldspar porphyry monzonite and andesitic tuffs and a large number of radiating micro-diorite dykes and precious to base metal rich quartz veins. Although minor copper mineralization (malachite, chalcopyrite) was observed in the area of the Bap claims the test pitting program between lines 2700E and 4200E south of baseline 2000N returned up to 1.2 gpt Au, and 1.5% Cu in pit KLP-24-1.5 with average geochemical results ranging from 200 to 400 ppb Au and less than 0.2% Cu.

To the north of the Lay Creek fault the highly sericite-clay-pyrite altered zone is exposed in the northwest corner of the grid where it begins to trend northerly.

The widespread alteration and occurrence of radiating dykes and quartz veins associated with the feldspar porphyry monzonite/diorite intrusive complex coupled with the low grade copper mineralization may represent the surface manifestation of a larger, buried intrusive body which may contain higher grade porphyry mineralization.

2.4.3 Quartz Vein Mineralization

Several quartz veins were exposed by historic trenching and the current test pitting programs. Quartz veins located between lines 4200E and 4000E, in the vicinity of the baseline (2000N), are less than 2.0 meters wide white bull quartz with traces of pyrite near sheared wallrock/vein contacts. These are generally barren with gold values less than 1.0 gram per tonne.

The most significant auriferous quartz veins in the survey area include those at the "Ginger B" Showing which are emplaced along northwest, north-south and east-west shears and fracture zones with up to 2.0 meter widths and an exposed strike length of approximately 200 meters. Wall rock of the veins is strongly pyritized and often carbonatized.

A grab sample of semi-massive pyrite adjacent to the Ginger quartz vein returned 25.0 gpt Au and 32.0 gpt Ag. Two 2.0 meter chip samples of oxidized pyritic andesite including 30-50 percent quartz returned 13.0, 3.8 gpt Au and 15.2, 5.2 gpt Ag respectively. Grab samples (Noranda 1992) of quartz vein exposed in old pits in the vicinity of the "Ginger B" showing returned gold values to 20.6 gpt Au. (See the area of test pits 173-175).

2.4.4 Shear Related Mineralization

A showing centered at 5760E/2410N is hosted by fine to medium grained diorite outcropping on the south bank of Lay Creek. The diorite is strongly propylitized and frequently sheared with 153°/90 oriented quartz-chlorite-carbonate veins and chalcopyrite impregnations and disseminations. Malachite/azurite fracture coatings are also common. The west end of the showing is marked by subcrop of pyritic gossan with no copper mineralization. Twelve 2.0 meter chip samples and one grab sample were collected from this area. Copper values ranged from 85 ppm to 3583 ppm with the best gold value being 440 ppb.

2.5 Darb Lake Grid

The Darb Lake Grid is underlain by a NW striking, moderately (30-50 deg) southwest dipping sequence of augite-feldspar porphyry andesite (Unit 7) to trachyandesite flows, tuffs (Unit 1) and fragmentals (Unit 2). Interbedded within the volcanics is a green-gray, fine grained, millimeter to centimeter bedded argillite to siltstone member (Unit 4) with dark gray shale (Unit 5) and rare limestone bands (Unit 3). Within the northern half of the grid (named the Camp Creek Basin), the volcanics/sediments are intruded by a medium to coarse grained diorite to gabbro stock (Unit 11) and related sills and dykes. These sills and dykes continue south of the stock, as N-S to NE-SW trending bodies of diorite to feldspar porphyry monzonite, intruding mainly sediments, and causing a hornfels aureole surrounding the intrusives. An ultra-mafic pyroxenite body (Units 9a and 9b) intrudes all in the northwest part of the grid.

Structure

The entire package displays 170-190 degree shears and faults with conjugate fault/shear splays trending NW-SE and ENE-WSW. Shears are particularly evident along the east contact of the Camp Ck Diorite with the sediments. Dips on either side of the main mountain ridge suggest a synclinal closure although the position of the axial plane has not been located.

Mineralization/Alteration

The sediments and the fine grained volcanics have been hornfelsed to varying degrees when in contact with the Camp Ck Diorite and its associated intrusives. Maximum alteration is calc-silicate facies. Where the sediments are slightly limy a pyroxene skarn containing pyrrhotite, pyrite +/- magnetite and chalcopryite is developed in small (1-5 m), discontinuous pods.

Most of the hornfelsed rock contains 1-15% py +/- po which produces a prominent gossan zone. Several of these gossans are found within the Darb Lake Grid. Quartz, chlorite, epidote, magnetite, and carbonate (retrograde?) veins with a trace to 0.5% chalcopryite are locally developed in the calc-silicate hornfelses. The Camp Ck Diorite often shows stockwork quartz-chlorite +/- epidote, and pyrite veining. Rarely found within these stockwork zones is trace to 2% chalcopryite +/- magnetite or bornite. None of these mineralized zones show any size extent. The Camp Ck Diorite is generally propylitically altered.

Magnetite-quartz veins up to 15 cm wide were also noted at several localities in locally pyritic volcanic tuffs above the diorite. Several rusty zones are due to the weathering of mafic to ultramafic rock.

Considerable difficulty was experienced with magnetic compass deflection in the center part of the grid although the dominantly augite-porphry andesite scree found there is not particularly magnetic. A hidden magnetic body is thus theorized of probable ultramafic affinity.

Of the 47 rocks collected on the Darb Lake grid only 6 returned values of over 500 ppb Au and /or greater than 1000 ppm Cu of which 3 were taken from small (up to 10 cm wide) quartz, chlorite, pyrite, magnetite veins. Of more interest are samples taken from quartz-pyrite stockworks within diorite (726-P) which ran 1315 ppm Cu and 920 ppb Au and another taken from a shear zone between calc-silicate altered volcanics-sediments and the diorite stock which returned 3462 ppm Cu and 440 ppb Au (727-A).

3.0 TEST PITTING (See Drawings 13, 14a, 14b)

The objective of the test pitting programme was to outline the surface or near surface extent of the skarn mineralization of the Kliyul main zone, to aid in the mapping of the local geology commonly buried in 4-10 meters of glacial drift in the valley floor and to explain other Cu-Au soil geochemical and magnetic anomalies previously untested. Besides the mineralization, alteration and geology attention was placed on delineating main structures which intersect in the vicinity of the Kliyul main zone and which may play an important role in localizing mineralization.

The main highlights of the 1993 test pitting programme are revealed below.

1. Mineralized bedrock and subcrop similar to the Kliyul main skarn zone was uncovered in an area measuring 400 x 350 centered on line 2800E/1900N and remains open to the southwest.
2. A new zone of skarn mineralization with magnetite, traces of disseminated chalcopyrite and malachite in altered diorite/chloritic andesite was uncovered in pits 112, 113, 50 and 101 centered on line 3350E/2150N.
3. Both of the skarn zones mentioned above correlate well with high magnetic susceptibility readings taken over the Kliyul Main grid.
4. A large zone (350 x 200) of ferrocrete located immediately southeast of the newly discovered skarn zone may in fact mark more mineralization at depth.
5. Test pitting of the center and northwest portions of the grid has identified moderate to intensely altered and sheared feldspar porphyry monzonites which have been in turn intruded by melanocratic, (+/- magnetite rich) diorites. The altered monzonitic intrusive carries elevated values of copper and gold and may reflect a larger mineralized porphyry cell which is in part structurally controlled.
6. Although rock geochemistry returned sporadic results from the test pitting (see Geology section) the basic WNW trend of the Main zone was defined. Also, the values from rocks taken at the newly discovered skarn showing and in part along the altered feldspar porphyry monzonite trace were anomalous.

7. Contouring (500 ppm Cu, 100 ppb Au) of the soils taken from the pits at the Main Kliyul zone reveals the same WNW trend beginning in the northwest with the skarn zone and trailing off to the southeast along the altered monzonite trace. Of interest is the >1000 ppm Cu/>200 ppb Au zone which is located between lines 2900E and 3250E/1900N which has not yet been drill tested.

4.0 SOIL GEOCHEMISTRY

The soil geochemical programme conducted over the Kliyul area essentially focused on airborne magnetic anomalies, favorable stratigraphy known to host skarn mineralization, monzodioritic intrusives, east-west structures which bisect the Kliyul property and areas of widely spaced anomalous geochemistry requiring infill sampling.

A detailed compilation of all historic soil geochem data as well as Noranda's sampling is shown on Figures 15, 16, 17 and 18. For the purpose of this report only the gold and copper values are illustrated and have been contoured at the 100 ppb and 300 ppm contour intervals respectively. Refer to Appendix II for ICP results with corresponding line and station co-ordinates.

4.1 Gold

Three main >100 ppb Au zones exist on the northern half of the mapsheet and all are situated within the Joh claims. The first is centered on lines 14200N through 12800N at approximately 11500E. This anomalous zone averages about 100 to 300 meters in width and strikes for 1900 meters in a northwest direction. Two smaller gold zones occur to the south and east of the first area and occur along a northeast trending ridge at approximately the same elevation ranges as the original northwest trending zone suggesting a flat lying source to the gold and a possible connection between the zones that is not readily apparent on initial inspection of the data. These zones both occur within Takla volcanics proximal to Cretaceous quartz monzonite stock and Jurassic aged diorites.

Further to the southeast on lines 11600N through 11000N at approximately 13200E lies a cluster of four other >100 ppb Au zones which may represent a single zone due to their proximity. As was the case in the zone mentioned above, these anomalies also occur at the 1700-1900 m elevation range supporting the idea of a relatively flat lying host rock.

Underlying geology is reported to be both Takla volcanics intruded by Cretaceous quartz monzonites as suggested by regional government mapping.

Smaller zones of geochemically anomalous gold also occur on the Darb Lake grid on lines 8800E, 8900E and 9000E which are underlain by limy sections of the Takla Group intruded by melanocratic diorites.

Referring to the southern mapsheet a large, circular, >100 ppb Au zone has been delineated wrapping around the east-west trending ridge which separates the Joh claims from the Kliyul property. (This anomaly is also depicted on Drawing 19 at 1:5,000 scale for comparison with the detailed geological interpretation). The halo effect created by this anomaly around a topographical high also suggests a flat lying host for gold mineralization in this area which is supported by geological mapping that reveals shallow dipping skarnified units just below the capping augite porphyry unit observed at the top of the east-west trending ridge.

Of interest is the relatively small area of anomalous gold geochemistry associated with the main Kliyul skarn zone located at line 2700E, 1900N. The lack of strong geochem in this area is likely due to a 4-10 m deep cover of glacial till covering the bottom of the valley at the headwaters of Lay and Kliyul creeks.

To the southeast of the above mentioned valley (which likely represents a large structural break and change in the main geological trend) the gold geochemistry follows a distinct northwest-southeast trend which reflects the trend of the multiphase intrusive complex, structural fabric and bedding orientation of the Soup skarn zones. The gold in soil zones here are open-ended in each of the areas gridded and most likely continue between these previously surveyed areas along the east banks of East Kliyul Creek.

4.2 Copper

Copper soil geochemical anomalies contoured at 300 ppm are illustrated on Drawings 17 and 18 at 1:10,000 scale and Drawings 20 and 22 at 1:5,000 for comparison with the detailed geological map.

Referring to the northern section of the map a large northwest trending 400-1200 meters wide, 4400 m long, open-ended copper soil anomaly is evident on the Joh claims mainly on the western side of the pronounced ridge dividing Darb and Lay creeks.

This large anomaly appears more contiguous and essentially covers the clusters of anomalous gold geochem seen in the area further supporting the idea of a large single host rather than several disjointed, smaller occurrences.

Copper geochem seen on the Darb Lake grid basically mimics the elevated gold occurrences associated with dioritic plugs intruding limy sections of the Takla Group.

Although not as widespread as the gold the anomalous copper values to the north and northeast and to the immediate west of the east-west trending ridge indicate a leakage from a mineralized zone situated beneath the augite porphyry caprock that cover the topographic highs in the area. This idea is also supported by the existence of in-situ skarn mineralization directly beneath the augite porphyry on the north side of the large east-west trending ridge (see Drawing 11.

Copper geochemical values in the vicinity of the main Kliyul skarn zones are, as in the case of the gold, less widespread and subdued due to the effect of overburden in the valley. On both the copper and gold maps the anomalous zones plot to the east of the known mineralization due to glacial transport from west to east.

Anomalous copper soil geochemistry to the south of the large east-west structural break (located in the Lay and Kliyul Creek valley) is evident only over the Soup claims as no copper geochem values were obtained from the gridded area immediately east of the headwaters of East Kliyul Creek. The anomaly over the Soup claims trends northwest-southeast and is open along strike and to the east. Values in this vicinity are obviously due in part to the documented skarn zones located just east of the baseline but anomalous results have also been returned uphill of the known mineralization with no obvious source as yet determined.

No anomalous values of either copper or gold were returned from the surveyed areas to the south of the main Kliyul property grid or from the area covered from the 800N baseline.

5.0 GEOPHYSICS

From October 20, 1993 to November 7, 1993 ground magnetic readings were collected on the Kliyul Creek, Joh and Croydon Creek claims. The work was contracted to Peter E. Walcott and Associates Ltd. and performed by Garry MacMillan, P. Charlie and M. Schulze (Noranda employee) using EDA OMNI & Magnetometers.

Three grids were surveyed and named the Kliyul Main Grid, Morraine Grid (Joh Property) and Recce Grid (Croydon Creek Property). Of the 60 line kilometers of readings proposed 59.43 were collected. Only a very small portion of the Morraine Grid was left unsurveyed due to equipment trouble and rough topography.

The work on the Main Grid provided infill lines to compliment the surveys performed in the early 80's by Placer Dome and by Kennco before them. Readings were collected every 12.5 m. The Kliyul Skarn zone now has effective 100 m line separation coverage. Repeat stations were collected on some of the Placer Dome lines and all three surveys leveled to the 1993 Norex base station.

In all 48.80 line kilometers of coverage were obtained (31 lines). Base line stations and end of line stations were located of the Trimble Ensign GPS unit. The accuracy, of the Ensign, when compared to NTS topographic features is ± 30 m.

On the Morraine Grid 9.23 line kilometers were surveyed (10 lines) and on the Recce Grid 1.40 line kilometers (3 lines). The plots included in this report were produced with Geosoft softwares.

INTERPRETATION

The Kliyul Skarn Zone (L2600E to L3200E and 1600N to 2100N) is well delineated by a strong magnetic signature of up to 500 nT above background. This magnetic high correlates with an increase in magnetite in the skarn mineralization. This Main Zone is truncated on its north side by a regional E-W break. Southwest trending Listwanite dykes, Gabbros and Pyroxenites, abutting the south side of the Main Kliyul Skarn Zone also exhibit intense magnetic signatures. Immediately to the northeast of the Main Skarn Zone lies a second area of skarn mineralization characterized by several localized magnetic highs. The magnetic response displayed by the Main Zone indicates a shallow dip to the southwest.

North of the Kliyul Main Zone and coincident with a topographic high ridge a further area of intense magnetization is seen. The bulk of the lithologies mapped on this ridge are of the Takla Group. A good correlation is observed between intense magnetic highs and augite porphyry.

Discrete anomalies can also be identified where altered monzonite/diorite, undivided flows/tuffs and clastic metasediments have been mapped. Anomalous gold geochemistry shows a good coincidence with areas of intense magnetic highs. North of the ridge on, the Moraine Grid, two distinct magnetic zones have been identified. The southernmost shows an excellent correlation with melanocratic diorite. Little is known of the northernmost magnetic trend. This area should receive thorough geological mapping and complete soil coverage. The magnetic highs mapped by the three lines of the Recce Grid appear to be caused by melanocratic diorite and augite porphyry.

RECOMMENDATIONS

Ground magnetic surveys work well in defining the skarn mineralization as well as the intrusive rocks. The only available IP/Resistivity was collected by Kennco on east-west lines, separated by 800 feet, over the Kliyul Main Zone. Although not the ideal direction the IP/Resistivity does tend to map the skarn mineralization.

Ground magnetic coverage should be extended to connect the Moraine and Recce Grids to the Main Grid. In areas with coincident magnetic highs and anomalous geochemistry IP/Resistivity surveys should be performed. The aeromagnetic survey has identified several other magnetic highs. They should receive reconnaissance ground magnetic surveys as well as soil sampling and geological mapping.

6.0 CONCLUSIONS

The geological, geochemical, geophysical and trenching programmes conducted on the Kliyul area in 1993 combined with historically data compilation have led to the following conclusions.

1. Mapping has revealed that the stratigraphy of the project area includes a relatively flat lying sediment/limestone horizon which acts as host to the skarn mineralization and occurs directly beneath an unconformable augite porphyry flow/flow breccia unit.
2. Geochemical surveying and compilation of historic geochemical results has revealed 3 large coincident Cu-Au zones associated with Jura-Cretaceous aged diorites/monzonites within Takla Group rocks. These anomalous zones are also coincident with both vertical gradient magnetics and weight percent magnetite highs returned from the helicopter-borne magnetic, electromagnetic, radiometric and VLF-EM survey.
3. Trenching of the Kliyul property has revealed near surface skarn mineralization in the area of drilling on the Kliyul claims and to the east in an area of high magnetic susceptibility previously untested. Trenching results have also confirmed the northwest-southeast trend to the altered monzonite and subsequent diorite intrusions in the vicinity of the skarn zone and that some of the mineralization within the intrusives may be in part porphyry related.
4. Ground geophysical surveying has revealed an open-ended, high magnetic susceptibility anomaly to the north of the east-west trending ridge separating the Joh & Kliyul properties in the vicinity of known skarn mineralization.

Further follow-up work in the form of detailed mapping, sampling and ground magnetic surveying over the areas containing the 3 large Cu-Au soil enriched areas is highly recommended. Particular attention should be placed on stratigraphy during the mapping programme.

A diamond drilling programme is recommended to further delineate the Kliyul Main skarn zone to the southwest and in the area of newly discovered skarn mineralization centered at line 3400E, 2150N. Additional drilling of the other prospective zones should be considered when the remaining Stage II exploration work has been completed.

REFERENCES

1. Assessment Report #675: Geology of the Soup Claims, K.C. McTaggart, 1965.
2. Assessment Report #5562: Mineralogical Study of Soup Claims, A.J. Sinclair, 1975.
3. Assessment Report #5985: Ground Magnetics, Soup Claims, A.J. Sinclair, 1976.
4. Assessment Report #6410: Geochemical Survey, Soup Claims, B.P. Minerals, 1977.
5. Assessment Report #7033: Litho geochemistry, Soup Claims, A.J. Sinclair, 1978.
6. Assessment Report #9485: Geochemistry, Soup Claims, Vital Resources, 1981.
7. Assessment Report #10,743: Geochem, Geophysics, Geology, Soup Claims, Noranda Exploration, 1982.
8. Assessment Report #13,315: Geology, Geochem, Soup Claims, B.P. Minerals, 1984.
9. Assessment Report #15,201: Magnetometer, Rock Sampling, Soup Claims, C.M. Rebagliati, 1986.
10. Summary Report on the Soup Claims, Rebagliati Geological Consulting Ltd. for Athlone Resources Ltd., 1988.
11. Summary Report on the Soup Claims (Drilling), Rebagliati Geological Consulting Ltd. for Athlone Resources Ltd., 1989.
12. Exploration Report on the Soup Property, Teck Explorations Ltd., 1991.

13. Assessment Report #2818: Magnetometer Survey on the Kli Claims, Kennco, 1970.
14. Assessment Report #3312: Soil and Silt Survey, Kli Claims, Kennco, 1971.
15. Assessment Report #3313: Geophysical Survey, Kli Claims, Kennco, 1971.
16. Compilation Report on the Kliyul Property, R.W. Stevenson, 1973.
17. Assessment Report #5211: Drilling Report, Kli Claims, Sumac Mines Ltd. 1974.
18. Report on the Diamond Drilling on Kli Claims, Koji Hashimoto, 1975.
19. Assessment Report #9464: Drilling on the Klisum Group, Kennco & Vital Resources, 1981.
20. Assessment Report #13,258: Geology, Geochem on the Kli Claims, B.P. Minerals, 1984.
21. Geochemical, Geophysical and Prospecting Report on the KLI Claims, S. Price, G. Linden, R. Cannon, P. Eng., G. Ditson for Placer Dome, November, 1990.
22. Assessment Report #15,313: Geological Report on Mapping, Sampling & Bulk Sampling on the Gold Group claims, Laramie Mining Corporation, Gerhard von Rosen, P.Eng., November, 1986.
23. Assessment Report #13,697: Geological and Geochemical Report on the Goldway 1-8 Claims of B.P. Resources Canada Ltd., R.E. Meyers and H.Q. Smit, March 1985.

24. Geologic Setting and Sampling of Vein Systems on the Solo Group Mineral Claims for Jetta Resources Ltd., by T.A. Richards, June, 1991.
25. Assessment Report #10,809: Geochemical Report on the Good, Prospects, Much, Pro, Fit and Dar Mineral Claims, G.E.A. von Rosen, P.Eng., 1982.
26. Assessment Report #15,538: Geological, Geochemical and Geophysical Report on the KC 1 & 2 Claims, Peter A. Christopher, Ph.D., P.Eng., October, 1986.
27. Assessment Report #14,416: Geological, Geophysical & Geochemical Report on the KC 1 & 2 Claims, Donald B. Cross, 1985.
28. Assessment Report #15,182: Soil Geochemistry on the Bap 10, 14, 18 Mineral Claims, C.M. Rebagliati, P.Eng., 1986.
29. Assessment Report #13,460: Geological, Geochemical Report on the Goldway 9 Claim Group, D.R. Heberlein, 1984.

APPENDIX I
LABORATORY ANALYTICAL TECHNIQUES

ANALYTICAL METHOD DESCRIPTIONS FOR GEOCHEMICAL ASSESSMENT REPORTS

The methods listed are presently applied to analyse geological materials by the Noranda Geochemical Laboratory at Vancouver.

Preparation of Samples:

Sediments and soils are dried at approximately 80°C and sieved with a 80 mesh nylon screen. The -80 mesh (0.18 mm) fraction is used for geochemical analysis.

Rock specimens are pulverized to -120 mesh (0.13 mm). Heavy mineral fractions (panned samples * from constant volume), are analysed in its entirety, when it is to be determined for gold without further sample preparation.

Analysis of Samples:

Decomposition of a 0.200 g sample is done with concentrated perchloric and nitric acid (3:1), digested for 5 hours at reflux temperature. Pulps of rock or core are weighed out at 0.4 g and chemical quantities are doubled relative to the above noted method for digestion.

The concentrations of Ag, Cd, Co, Cu, Fe, Mn, Mo, Ni, Pb, V and Zn can be determined directly from the digest (dissolution) with a conventional atomic absorption spectrometric procedure. A Varian-Techtron, Model AA-5 or Model AA-475 is used to measure elemental concentrations.

Elements Requiring Specific Decomposition Method:

Antimony - Sb: 0.2 g sample is attacked with 3.3 ml of 6% tartaric acid, 1.5 ml conc. hydrochloric acid and 0.5 ml of conc. nitric acid, then heated in a water bath for 3 hours at 95°C. Sb is determined directly from the dissolution with an AA-475 equipped with electrodeless discharge lamp (EDL).

Arsenic - As: 0.2 - 0.3 g sample is digested with 1.5 ml of perchloric 70% and 0.5 ml of conc. nitric acid. A Varian AA-475 equipped with an As-EDL is used to measure arsenic content in the digest.

Barium - Ba: 0.1 g sample digested overnight with conc. perchloric, nitric and hydrofluoric acid; Potassium chloride added to prevent ionization. Atomic absorption using a nitrous oxide-acetylene flame determines Ba from the aqueous solution.

Bismuth - Bi: 0.2 - 0.3 g is digested with 2.0 ml of perchloric 70% and 1.0 ml of conc. nitric acid. Bismuth is determined directly from the digest with an AA-475 complete with EDL.

Gold - Au: 10.0 g sample is digested with aqua regia (1 part nitric and 3 parts hydrochloric acid). Gold is extracted with MIBK from the aqueous solution. AA is used to determine Au.

Magnesium - Mg: 0.05 - 0.10 g sample is digested with 4 ml perchloric/nitric acid (3:1). An aliquot is taken to reduce the concentration to within the range of atomic absorption. The AA-475 with the use of a nitrous oxide flame determines Mg from the aqueous solution.

Tungsten - W: 1.0 g sample sintered with a carbonate flux and thereafter leached with water. The leachate is treated with potassium thiocyanate. The yellow tungsten thiocyanate is extracted into tri-n-butyl phosphate. This permits colourimetric comparison with standards to measure tungsten concentration.

Uranium - U: An aliquot from a perchloric-nitric decomposition, usually from the multi-element digestion, is buffered. The aqueous solution is exposed to laser light, and the luminescence of the uranyl ion is quantitatively measured on the UA-3 (Scintrex).

N.B.: If additional elemental determinations are required on panned samples, state this at the time of sample submission. Requests after gold determinations would be futile.

LOWEST VALUES REPORTED IN PPM:

| | | | |
|----------|---------|---------|-----------|
| Ag - 0.2 | Mn - 20 | Zn - 1 | Au - 0.01 |
| Cd - 0.2 | Mo - 1 | Sb - 1 | W - 2 |
| Co - 1 | Ni - 1 | As - 1 | U - 0.1 |
| Cu - 1 | Pb - 1 | Ba - 10 | |
| Fe - 100 | V - 10 | Bi - 1 | |

APPENDIX II
SOIL GEOCHEMICAL RESULTS

NORANDA DELTA LABORATORY

Geochemical Analysis

Project Name & No.: KLIYUL - 148
 Material: 5 Silts, 402 Soils, 1 Moss & 29 Rx
 Remarks: * Sample screened @ -35 MESH (0.5 mm)

Geol.: T.W.
 Sheet: 1 of 10

Date received: JULY 16
 Date completed: JULY 26

LAB CODE: 9307-023

* Organic, & Humus, S Sulphide
 Au - 10.0 g sample digested with aqua-regia and determined by A.A. (D.L. 5 PPB)
 ICP - 0.2 g sample digested with 3 ml HClO₄/HNO₃ (4:1) at 203 °C for 4 hours diluted to 10 ml with water. Leeman PS3000 ICP determined elemental contents.
 N.B. The major oxide elements and Ba, Be, Ce, La, Li, Oa are rarely dissolved completely from geological materials with this acid dissolution method.

| T.T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Be ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm |
|----------|------------|--------|--------|------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|-------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|
| 3 | 200E-000S | 60 | 0.2 | 4.89 | 9 | 214 | 0.4 | 5 | 1.38 | 0.3 | 40 | 17 | 33 | 123 | 5.14 | 0.30 | 11 | 24 | 1.88 | 641 | 1 | 0.07 | 31 | 0.10 | 2 | 69 | 0.30 | 190 | 87 |
| 4 | 50 | 15 | 0.2 | 4.71 | 6 | 229 | 0.4 | 5 | 1.71 | 0.3 | 39 | 16 | 31 | 78 | 4.86 | 0.33 | 10 | 22 | 1.89 | 754 | 1 | 0.08 | 28 | 0.10 | 2 | 76 | 0.31 | 190 | 97 |
| 5 | 100 | 5 | 0.2 | 3.30 | 6 | 93 | 0.3 | 5 | 2.35 | 0.3 | 42 | 8 | 44 | 22 | 3.44 | 0.20 | 10 | 9 | 1.44 | 551 | 1 | 0.14 | 25 | 0.13 | 2 | 78 | 0.37 | 142 | 52 |
| 6 | 150 | 25 | 0.2 | 3.23 | 40 | 222 | 0.4 | 15 | 0.98 | 1.9 | 40 | 25 | 37 | 136 | 10.63 | 0.25 | 12 | 17 | 1.26 | 652 | 32 | 0.06 | 37 | 0.07 | 4 | 49 | 0.21 | 161 | 81 |
| 7 | 200E-200S | 45 | 0.2 | 4.30 | 8 | 200 | 0.4 | 5 | 1.17 | 0.2 | 40 | 14 | 36 | 143 | 4.43 | 0.30 | 11 | 21 | 1.45 | 481 | 2 | 0.06 | 28 | 0.11 | 2 | 62 | 0.29 | 167 | 102 |
| 8 | 200E-250S | 5 | 0.2 | 3.33 | 11 | 258 | 0.3 | 5 | 1.72 | 0.4 | 39 | 15 | 66 | 92 | 4.07 | 0.34 | 9 | 11 | 1.97 | 525 | 1 | 0.12 | 39 | 0.14 | 2 | 25 | 0.34 | 131 | 64 |
| 9 | 300 | 25 | 0.2 | 4.58 | 12 | 210 | 0.3 | 5 | 2.19 | 0.6 | 41 | 17 | 25 | 89 | 4.62 | 0.33 | 10 | 15 | 1.73 | 855 | 1 | 0.09 | 24 | 0.09 | 2 | 97 | 0.29 | 177 | 77 |
| 10 | 350 | 5 | 0.2 | 3.89 | 13 | 135 | 0.3 | 5 | 1.95 | 0.5 | 39 | 11 | 24 | 42 | 3.96 | 0.24 | 9 | 12 | 1.47 | 631 | 1 | 0.10 | 18 | 0.11 | 2 | 69 | 0.28 | 159 | 79 |
| 11 | 400 | 10 | 0.2 | 4.20 | 13 | 157 | 0.3 | 5 | 2.46 | 0.4 | 38 | 15 | 31 | 57 | 4.19 | 0.25 | 10 | 14 | 1.69 | 671 | 1 | 0.09 | 25 | 0.08 | 2 | 113 | 0.29 | 174 | 69 |
| 12 | 200E-450S | 5 | 0.2 | 4.09 | 13 | 159 | 0.3 | 5 | 2.20 | 0.6 | 40 | 18 | 25 | 92 | 4.57 | 0.25 | 10 | 16 | 1.97 | 643 | 1 | 0.12 | 26 | 0.10 | 2 | 119 | 0.34 | 185 | 71 |
| 13 | 200E-500S | 5 | 0.2 | 4.37 | 10 | 111 | 0.3 | 5 | 2.64 | 0.6 | 40 | 16 | 24 | 50 | 4.47 | 0.17 | 10 | 13 | 1.84 | 662 | 1 | 0.14 | 24 | 0.09 | 2 | 89 | 0.34 | 178 | 70 |
| 14 | 550 | 5 | 0.2 | 2.90 | 14 | 153 | 0.2 | 5 | 1.62 | 0.6 | 37 | 14 | 21 | 55 | 4.11 | 0.24 | 9 | 10 | 1.61 | 614 | 1 | 0.15 | 19 | 0.15 | 2 | 45 | 0.29 | 154 | 65 |
| 15 | 600 | 5 | 0.2 | 3.40 | 12 | 112 | 0.3 | 5 | 2.47 | 0.6 | 40 | 18 | 16 | 57 | 4.47 | 0.16 | 10 | 16 | 1.86 | 746 | 2 | 0.16 | 20 | 0.16 | 2 | 58 | 0.33 | 155 | 109 |
| 16 | 650 | 10 | 0.2 | 3.72 | 13 | 249 | 0.3 | 5 | 1.31 | 0.5 | 41 | 11 | 38 | 27 | 3.85 | 0.44 | 11 | 14 | 1.37 | 537 | 1 | 0.08 | 23 | 0.13 | 4 | 72 | 0.29 | 171 | 82 |
| 17 | 200E-700S | 110 | 0.2 | 4.48 | 18 | 245 | 0.4 | 5 | 1.65 | 0.8 | 43 | 19 | 33 | 100 | 4.73 | 0.37 | 11 | 18 | 1.88 | 713 | 1 | 0.10 | 33 | 0.10 | 4 | 77 | 0.27 | 185 | 87 |
| 18 | 200E-750S | 5 | 0.2 | 4.14 | 14 | 220 | 0.3 | 5 | 2.64 | 0.7 | 41 | 16 | 20 | 41 | 4.49 | 0.28 | 10 | 13 | 1.85 | 705 | 1 | 0.14 | 20 | 0.13 | 2 | 101 | 0.30 | 179 | 72 |
| 19 | 800 | 5 | 0.2 | 3.52 | 15 | 76 | 0.3 | 5 | 2.22 | 0.7 | 36 | 23 | 35 | 120 | 4.67 | 0.47 | 10 | 18 | 2.07 | 794 | 1 | 0.08 | 35 | 0.12 | 4 | 221 | 0.32 | 190 | 80 |
| 20 | 850 | 5 | 0.2 | 3.99 | 16 | 152 | 0.4 | 6 | 2.58 | 0.7 | 38 | 16 | 25 | 76 | 4.42 | 0.22 | 11 | 15 | 1.81 | 680 | 1 | 0.13 | 20 | 0.12 | 3 | 95 | 0.30 | 180 | 83 |
| 21 | 900 | 5 | 0.2 | 4.45 | 10 | 150 | 0.3 | 5 | 3.00 | 0.6 | 41 | 20 | 27 | 82 | 5.18 | 0.19 | 12 | 19 | 1.78 | 802 | 1 | 0.12 | 24 | 0.12 | 2 | 114 | 0.42 | 189 | 100 |
| 22 | 200E-950S | 5 | 0.2 | 5.31 | 7 | 316 | 0.4 | 5 | 2.55 | 0.6 | 40 | 23 | 29 | 107 | 5.70 | 0.51 | 11 | 21 | 2.53 | 1125 | 1 | 0.12 | 33 | 0.12 | 2 | 120 | 0.30 | 217 | 91 |
| 23 | 200E-1000S | 5 | 0.2 | 5.04 | 11 | 211 | 0.4 | 5 | 3.42 | 0.7 | 39 | 22 | 32 | 115 | 5.41 | 0.28 | 12 | 17 | 2.16 | 965 | 1 | 0.14 | 34 | 0.12 | 2 | 139 | 0.40 | 203 | 91 |
| 24 | 1050 | 10 | 0.2 | 4.97 | 11 | 162 | 0.9 | 5 | 3.29 | 0.8 | 55 | 22 | 38 | 114 | 5.89 | 0.22 | 16 | 23 | 1.94 | 1156 | 1 | 0.13 | 40 | 0.15 | 2 | 138 | 0.47 | 211 | 132 |
| 25 | 1100 | 5 | 0.2 | 5.19 | 9 | 200 | 0.4 | 5 | 4.11 | 0.6 | 36 | 24 | 18 | 90 | 5.65 | 0.24 | 11 | 17 | 1.84 | 973 | 1 | 0.08 | 29 | 0.13 | 2 | 178 | 0.44 | 231 | 90 |
| 26 | 1150 | 5 | 0.2 | 4.94 | 8 | 124 | 0.4 | 5 | 4.17 | 0.6 | 37 | 20 | 16 | 73 | 5.39 | 0.20 | 11 | 15 | 1.69 | 877 | 1 | 0.10 | 27 | 0.11 | 2 | 177 | 0.46 | 227 | 89 |
| 27 | 200E-1200S | 5 | 0.2 | 4.31 | 9 | 175 | 0.3 | 5 | 3.51 | 0.5 | 38 | 18 | 15 | 48 | 5.11 | 0.16 | 10 | 13 | 1.30 | 1153 | 1 | 0.08 | 21 | 0.19 | 2 | 149 | 0.52 | 235 | 84 |
| 28 | 200E-1250S | 5 | 0.2 | 5.14 | 13 | 176 | 0.4 | 5 | 4.18 | 0.8 | 38 | 23 | 39 | 100 | 5.66 | 0.28 | 11 | 20 | 1.87 | 1219 | 1 | 0.11 | 46 | 0.13 | 2 | 185 | 0.51 | 224 | 97 |
| 29 | 1300 | 5 | 0.2 | 3.57 | 13 | 137 | 0.2 | 5 | 3.35 | 0.6 | 39 | 12 | 41 | 21 | 3.91 | 0.21 | 11 | 8 | 1.29 | 550 | 1 | 0.09 | 28 | 0.13 | 2 | 137 | 0.49 | 186 | 58 |
| 30 | 1350 | 5 | 0.2 | 4.19 | 14 | 114 | 0.4 | 5 | 2.39 | 0.5 | 48 | 17 | 16 | 52 | 5.13 | 0.20 | 13 | 15 | 1.50 | 999 | 1 | 0.09 | 15 | 0.22 | 4 | 88 | 0.42 | 179 | 97 |
| 31 | 1400 | 5 | 0.2 | 3.61 | 6 | 177 | 0.3 | 5 | 2.25 | 1.0 | 36 | 20 | 39 | 69 | 4.86 | 0.25 | 10 | 15 | 1.95 | 803 | 1 | 0.14 | 30 | 0.20 | 2 | 75 | 0.31 | 166 | 103 |
| 32 | 200E-1450S | 5 | 0.2 | 4.31 | 2 | 159 | 0.5 | 5 | 2.07 | 0.3 | 39 | 17 | 33 | 71 | 4.84 | 0.22 | 11 | 16 | 2.09 | 750 | 1 | 0.14 | 32 | 0.17 | 2 | 69 | 0.31 | 158 | 77 |
| 33 | 200E-1500S | 30 | 0.2 | 4.77 | 2 | 157 | 0.5 | 5 | 2.41 | 0.2 | 41 | 17 | 29 | 79 | 5.08 | 0.27 | 11 | 15 | 1.99 | 782 | 1 | 0.16 | 28 | 0.15 | 2 | 94 | 0.34 | 174 | 87 |
| 34 | 200E-1550S | 10 | 0.2 | 8.17 | 2 | 38 | 1.0 | 5 | 6.66 | 0.2 | 22 | 21 | 8 | 210 | 3.52 | 0.14 | 4 | 8 | 1.03 | 571 | 1 | 0.06 | 17 | 0.11 | 2 | 226 | 0.16 | 115 | 47 |
| 35 | 200E-50N | 10 | 0.2 | 5.02 | 2 | 398 | 0.4 | 5 | 1.63 | 0.2 | 42 | 18 | 40 | 293 | 5.18 | 0.28 | 11 | 15 | 1.50 | 583 | 2 | 0.10 | 31 | 0.13 | 2 | 58 | 0.41 | 148 | 85 |
| 36 | 100 | 10 | 0.2 | 3.85 | 2 | 220 | 0.3 | 5 | 1.93 | 0.2 | 36 | 8 | 31 | 97 | 4.73 | 0.41 | 8 | 16 | 1.58 | 582 | 2 | 0.10 | 20 | 0.15 | 2 | 70 | 0.39 | 160 | 78 |
| 37 | 200E-150N | 15 | 0.2 | 4.43 | 4 | 231 | 0.4 | 5 | 1.69 | 0.3 | 41 | 27 | 28 | 69 | 5.02 | 0.29 | 10 | 20 | 1.60 | 2312 | 11 | 0.08 | 24 | 0.18 | 2 | 73 | 0.27 | 176 | 93 |

OAR

06/28 GP

| T.T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Bc ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Tl % | V ppm | Zn ppm | 0307-023 Pg. 2 of 10 |
|----------|------------|--------|--------|------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|-------------------------|
| 38 | 200E-200N | 25 | 0.2 | 4.98 | 13 | 184 | 0.4 | 5 | 1.38 | 0.3 | 38 | 15 | 45 | 61 | 4.80 | 0.25 | 9 | 20 | 1.70 | 622 | 2 | 0.06 | 34 | 0.09 | 2 | 67 | 0.28 | 176 | 82 | |
| 39 | 250 | 35 | 0.2 | 4.94 | 2 | 203 | 0.4 | 5 | 1.34 | 0.2 | 39 | 13 | 32 | 70 | 4.75 | 0.31 | 10 | 17 | 1.68 | 646 | 1 | 0.07 | 25 | 0.12 | 2 | 67 | 0.27 | 169 | 83 | |
| 40 | 300 | 20 | 0.2 | 4.73 | 6 | 188 | 0.3 | 5 | 1.57 | 0.2 | 38 | 13 | 40 | 50 | 4.64 | 0.31 | 9 | 15 | 1.55 | 613 | 1 | 0.07 | 25 | 0.11 | 2 | 80 | 0.26 | 180 | 73 | |
| 41 | 350 | 40 | 0.2 | 4.58 | 15 | 240 | 0.3 | 5 | 1.15 | 0.5 | 37 | 17 | 44 | 75 | 4.80 | 0.35 | 12 | 19 | 1.62 | 666 | 1 | 0.05 | 32 | 0.09 | 2 | 76 | 0.24 | 193 | 73 | |
| 42 | 200E-400N | 80 | 0.2 | 3.86 | 8 | 206 | 0.3 | 5 | 1.47 | 0.4 | 39 | 15 | 43 | 86 | 4.43 | 0.31 | 11 | 16 | 1.56 | 534 | 1 | 0.06 | 30 | 0.09 | 2 | 82 | 0.24 | 177 | 70 | |
| 43 | 200E-450N | 15 | 0.2 | 4.44 | 8 | 199 | 0.4 | 5 | 1.62 | 0.5 | 41 | 15 | 38 | 60 | 4.96 | 0.25 | 12 | 20 | 1.88 | 608 | 1 | 0.06 | 28 | 0.13 | 2 | 85 | 0.32 | 194 | 80 | |
| 44 | 500 | 30 | 0.2 | 4.83 | 10 | 206 | 0.4 | 5 | 1.31 | 0.5 | 40 | 20 | 43 | 107 | 5.52 | 0.30 | 12 | 23 | 2.48 | 698 | 1 | 0.05 | 44 | 0.11 | 2 | 71 | 0.32 | 217 | 89 | |
| 45 | 550 | 10 | 0.2 | 3.27 | 9 | 230 | 0.3 | 5 | 1.72 | 0.4 | 45 | 13 | 20 | 74 | 4.06 | 0.24 | 12 | 27 | 1.69 | 615 | 2 | 0.08 | 24 | 0.09 | 2 | 90 | 0.34 | 173 | 85 | |
| 46 | 600 | 85 | 0.2 | 5.00 | 5 | 260 | 0.3 | 5 | 2.34 | 0.6 | 40 | 18 | 32 | 109 | 5.08 | 0.32 | 10 | 18 | 2.03 | 878 | 1 | 0.10 | 35 | 0.09 | 5 | 96 | 0.30 | 188 | 87 | |
| 47 | 200E-650N | 50 | 0.2 | 4.62 | 9 | 189 | 0.3 | 5 | 1.50 | 0.5 | 40 | 18 | 47 | 98 | 4.88 | 0.27 | 10 | 18 | 2.15 | 639 | 1 | 0.06 | 42 | 0.09 | 2 | 86 | 0.27 | 205 | 79 | |
| 48 | 200E-700N | 35 | 0.2 | 4.98 | 15 | 202 | 0.4 | 5 | 1.49 | 0.7 | 42 | 24 | 51 | 114 | 5.47 | 0.30 | 12 | 19 | 2.37 | 859 | 1 | 0.06 | 51 | 0.08 | 3 | 87 | 0.28 | 219 | 83 | |
| 51 | 750 | 130 | 0.2 | 4.06 | 15 | 225 | 0.4 | 5 | 1.04 | 0.4 | 37 | 15 | 48 | 50 | 5.52 | 0.36 | 11 | 18 | 1.37 | 528 | 1 | 0.06 | 30 | 0.11 | 5 | 65 | 0.23 | 181 | 74 | |
| 52 | 850 | 25 | 0.2 | 3.56 | 6 | 114 | 0.2 | 5 | 2.24 | 0.3 | 36 | 10 | 142 | 67 | 4.07 | 0.17 | 7 | 11 | 0.95 | 390 | 1 | 0.05 | 68 | 0.08 | 2 | 89 | 0.34 | 120 | 53 | |
| 53 | 900 | 165 | 0.2 | 4.59 | 13 | 221 | 0.4 | 5 | 1.35 | 0.4 | 41 | 17 | 29 | 88 | 5.30 | 0.35 | 11 | 19 | 1.58 | 759 | 1 | 0.09 | 23 | 0.10 | 2 | 62 | 0.27 | 175 | 74 | |
| 54 | 200E-950N | 10 | 0.2 | 4.10 | 9 | 191 | 0.3 | 5 | 1.20 | 0.5 | 39 | 11 | 30 | 30 | 4.46 | 0.32 | 10 | 15 | 1.17 | 464 | 1 | 0.06 | 17 | 0.12 | 3 | 70 | 0.28 | 179 | 58 | |
| 55 | 200E-1000N | 20 | 0.2 | 4.46 | 6 | 234 | 0.4 | 5 | 1.18 | 0.4 | 37 | 13 | 28 | 44 | 5.24 | 0.36 | 10 | 15 | 1.21 | 580 | 1 | 0.06 | 19 | 0.18 | 2 | 64 | 0.27 | 169 | 67 | |
| 56 | 1050 | 10 | 0.2 | 4.86 | 8 | 241 | 0.3 | 5 | 1.96 | 0.2 | 41 | 13 | 26 | 68 | 5.32 | 0.25 | 9 | 14 | 1.58 | 634 | 1 | 0.08 | 21 | 0.15 | 2 | 99 | 0.32 | 191 | 60 | |
| 57 | 1100 | 20 | 0.2 | 4.44 | 9 | 208 | 0.3 | 5 | 1.71 | 0.4 | 40 | 12 | 39 | 53 | 5.02 | 0.25 | 10 | 13 | 1.40 | 528 | 1 | 0.08 | 19 | 0.13 | 2 | 79 | 0.30 | 179 | 58 | |
| 58 | 1150 | 5 | 0.2 | 4.15 | 5 | 121 | 0.4 | 5 | 1.54 | 0.4 | 47 | 11 | 140 | 47 | 3.86 | 0.26 | 14 | 14 | 1.87 | 477 | 1 | 0.12 | 66 | 0.22 | 2 | 51 | 0.26 | 114 | 53 | |
| 59 | 200E-1200N | 15 | 0.2 | 4.48 | 8 | 318 | 0.3 | 5 | 1.70 | 0.3 | 36 | 8 | 28 | 36 | 3.86 | 0.33 | 9 | 11 | 1.17 | 516 | 1 | 0.06 | 19 | 0.20 | 2 | 99 | 0.28 | 139 | 50 | |
| 60 | 200E-1250N | 40 | 0.2 | 3.50 | 10 | 195 | 0.3 | 5 | 0.48 | 0.4 | 25 | 9 | 32 | 42 | 3.67 | 0.29 | 8 | 17 | 0.94 | 779 | 1 | 0.04 | 15 | 0.17 | 3 | 37 | 0.19 | 132 | 72 | |
| 61 | 1300 | 50 | 0.2 | 5.14 | 22 | 366 | 0.4 | 5 | 0.69 | 0.3 | 35 | 27 | 35 | 88 | 5.90 | 0.47 | 12 | 28 | 1.58 | 1205 | 1 | 0.07 | 31 | 0.10 | 5 | 57 | 0.19 | 191 | 100 | |
| 62 | 1350 | 35 | 0.2 | 4.56 | 11 | 300 | 0.4 | 5 | 0.58 | 0.2 | 32 | 15 | 31 | 51 | 5.71 | 0.39 | 10 | 22 | 1.32 | 1086 | 1 | 0.06 | 22 | 0.14 | 4 | 46 | 0.21 | 182 | 88 | |
| 63 | 1400 | 5 | 0.2 | 3.90 | 2 | 161 | 0.3 | 5 | 0.59 | 0.2 | 30 | 8 | 41 | 37 | 3.74 | 0.26 | 9 | 17 | 1.40 | 445 | 1 | 0.05 | 21 | 0.13 | 2 | 31 | 0.27 | 165 | 66 | |
| 64 | 200E-1450N | 5 | 0.2 | 3.70 | 2 | 299 | 0.2 | 5 | 1.49 | 0.2 | 38 | 5 | 5 | 40 | 3.63 | 0.40 | 9 | 10 | 1.01 | 586 | 1 | 0.02 | 5 | 0.13 | 2 | 77 | 0.33 | 142 | 47 | |
| 65 | 200E-1500N | 5 | 0.2 | 3.83 | 2 | 124 | 0.4 | 5 | 0.83 | 0.2 | 36 | 4 | 20 | 37 | 2.12 | 0.22 | 10 | 9 | 0.57 | 243 | 1 | 0.06 | 9 | 0.24 | 3 | 44 | 0.18 | 74 | 35 | |
| 66 | 400E-2500N | 10 | 0.2 | 4.96 | 4 | 211 | 0.3 | 5 | 1.76 | 0.3 | 43 | 15 | 23 | 73 | 5.08 | 0.31 | 11 | 16 | 1.69 | 885 | 1 | 0.10 | 20 | 0.11 | 2 | 74 | 0.25 | 162 | 99 | |
| 67 | 2550 | 5 | 0.2 | 5.70 | 10 | 288 | 0.4 | 5 | 1.73 | 0.5 | 43 | 22 | 31 | 213 | 5.56 | 0.41 | 11 | 20 | 2.29 | 1169 | 1 | 0.10 | 40 | 0.11 | 2 | 75 | 0.29 | 183 | 126 | |
| 68 | 2600 | 5 | 0.2 | 4.29 | 8 | 97 | 0.4 | 5 | 0.82 | 0.3 | 39 | 12 | 43 | 51 | 4.29 | 0.25 | 11 | 13 | 1.27 | 822 | 1 | 0.06 | 20 | 0.17 | 2 | 45 | 0.28 | 178 | 76 | |
| 69 | 400E-2650N | 5 | 0.2 | 0.61 | 15 | 83 | 0.3 | 5 | 3.46 | 0.7 | 24 | 3 | 18 | 88 | 0.34 | 0.11 | 5 | 4 | 0.17 | 307 | 1 | 0.02 | 12 | 0.16 | 2 | 62 | 0.02 | 29 | 53 | |
| 70 | 400E-2700N | 5 | 0.2 | 6.01 | 18 | 207 | 0.6 | 5 | 1.13 | 0.5 | 33 | 17 | 42 | 180 | 4.48 | 1.04 | 11 | 17 | 1.57 | 1393 | 1 | 0.05 | 34 | 0.23 | 6 | 45 | 0.32 | 234 | 106 | |
| 71 | 2750 | 5 | 0.2 | 5.38 | 7 | 144 | 0.4 | 5 | 1.25 | 0.4 | 38 | 28 | 49 | 253 | 5.83 | 0.23 | 11 | 20 | 2.40 | 1167 | 1 | 0.07 | 41 | 0.13 | 2 | 62 | 0.28 | 192 | 95 | |
| 72 | 2850 | 5 | 0.2 | 3.35 | 2 | 29 | 0.4 | 5 | 0.62 | 0.4 | 26 | 43 | 20 | 175 | 6.00 | 0.07 | 7 | 7 | 0.88 | 1846 | 4 | 0.03 | 35 | 0.17 | 5 | 30 | 0.24 | 130 | 80 | |
| 73 | 400E-2900N | 10 | 0.2 | 2.94 | 27 | 163 | 0.3 | 5 | 1.80 | 0.5 | 35 | 13 | 27 | 123 | 2.83 | 0.41 | 7 | 10 | 0.98 | 330 | 1 | 0.05 | 26 | 0.21 | 2 | 112 | 0.12 | 83 | 74 | |
| 74 | 600W-100N | 5 | 0.2 | 4.36 | 2 | 182 | 0.4 | 5 | 1.26 | 0.2 | 39 | 18 | 38 | 118 | 5.58 | 0.20 | 11 | 26 | 2.04 | 582 | 1 | 0.07 | 29 | 0.13 | 2 | 53 | 0.30 | 243 | 85 | |
| 75 | 600W-150N | 20 | 0.2 | 4.53 | 3 | 222 | 0.4 | 5 | 1.17 | 0.2 | 38 | 16 | 44 | 89 | 5.04 | 0.30 | 12 | 24 | 1.69 | 562 | 2 | 0.05 | 30 | 0.13 | 2 | 62 | 0.25 | 192 | 81 | |
| 76 | 194 | 6500 | 0.2 | 4.30 | 5 | 224 | 0.3 | 5 | 1.56 | 0.2 | 40 | 19 | 51 | 63 | 5.15 | 0.35 | 11 | 20 | 2.14 | 784 | 1 | 0.06 | 37 | 0.06 | 2 | 88 | 0.23 | 202 | 89 | |
| 77 | 200 | 30 | 0.2 | 4.49 | 10 | 259 | 0.4 | 5 | 1.05 | 0.3 | 35 | 18 | 38 | 79 | 5.16 | 0.38 | 11 | 22 | 1.86 | 827 | 1 | 0.06 | 35 | 0.07 | 2 | 62 | 0.24 | 183 | 93 | |
| 78 | 250 | 10 | 0.2 | 4.45 | 10 | 172 | 0.3 | 5 | 1.59 | 0.2 | 39 | 18 | 54 | 92 | 5.05 | 0.22 | 11 | 19 | 2.21 | 593 | 1 | 0.04 | 42 | 0.07 | 2 | 94 | 0.30 | 199 | 81 | |
| 79 | 600W-300N | 55 | 0.2 | 4.78 | 12 | 243 | 0.5 | 5 | 1.04 | 0.2 | 39 | 17 | 48 | 81 | 5.25 | 0.36 | 11 | 18 | 1.66 | 634 | 1 | 0.05 | 34 | 0.10 | 2 | 66 | 0.23 | 190 | 83 | |
| 80 | 600W-350N | 20 | 0.2 | 4.55 | 11 | 225 | 0.4 | 5 | 1.29 | 0.3 | 40 | 19 | 61 | 97 | 4.90 | 0.36 | 11 | 18 | 1.82 | 713 | 1 | 0.06 | 38 | 0.08 | 2 | 76 | 0.24 | 195 | 77 | |
| 81 | 400 | 15 | 0.2 | 4.64 | 4 | 149 | 0.5 | 5 | 0.85 | 0.3 | 54 | 14 | 57 | 69 | 4.71 | 0.26 | 20 | 20 | 1.23 | 495 | 1 | 0.05 | 28 | 0.18 | 3 | 54 | 0.25 | 150 | 78 | |
| 82 | 450 | 30 | 0.2 | 4.18 | 2 | 218 | 0.3 | 5 | 0.65 | 0.2 | 31 | 13 | 71 | 40 | 4.75 | 0.37 | 10 | 15 | 1.54 | 1209 | 1 | 0.04 | 32 | 0.14 | 2 | 51 | 0.26 | 201 | 80 | |
| 83 | 500 | 180 | 0.2 | 4.91 | 10 | 187 | 0.4 | 5 | 0.89 | 0.2 | 34 | 19 | 60 | 69 | 5.55 | 0.26 | 10 | 21 | 1.75 | 908 | 1 | 0.04 | 35 | 0.12 | 2 | 59 | 0.28 | 203 | 80 | |
| 84 | 600W-550N | 25 | 0.2 | 4.16 | 8 | 188 | 0.4 | 5 | 0.71 | 0.2 | 34 | 10 | 47 | 36 | 4.63 | 0.26 | 10 | 15 | 1.17 | 509 | 1 | 0.04 | 19 | 0.18 | 2 | 56 | 0.25 | 202 | 65 | |

DARB

DARB

DARB

| T.T. No. | SAMPLE No. | Au | Ag | Al | As | Ba | Bc | Bi | Cu | Cl | Ce | Co | Cr | Cs | Fe | K | La | Li | Mg | Mn | Mo | Na | Ni | P | Pb | Sr | Ti | V | Zn | 9307-023 | |
|----------|------------|------|-----|------|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|------|------|-----|-----|------|------|-----|------|----|------|-----|-----|------|-----|-----|----------|------|
| | | ppb | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm |
| 85 | 600W-600N | 5 | 0.2 | 4.47 | 5 | 216 | 0.4 | 5 | 0.70 | 0.4 | 33 | 14 | 64 | 51 | 4.85 | 0.32 | 9 | 17 | 1.58 | 631 | 1 | 0.04 | 30 | 0.16 | 2 | 52 | 0.26 | 186 | 73 | | |
| 86 | 650 | 440 | 0.2 | 3.91 | 4 | 193 | 0.3 | 5 | 0.72 | 0.2 | 33 | 10 | 41 | 38 | 4.55 | 0.30 | 10 | 17 | 1.20 | 635 | 1 | 0.05 | 18 | 0.16 | 2 | 55 | 0.23 | 182 | 69 | | DARB |
| 87 | 700 | 30 | 0.2 | 4.34 | 8 | 217 | 0.4 | 5 | 1.00 | 0.2 | 36 | 16 | 46 | 85 | 4.82 | 0.31 | 9 | 19 | 1.44 | 1026 | 1 | 0.05 | 30 | 0.13 | 2 | 65 | 0.22 | 177 | 79 | | |
| 88 | 750 | 530 | 0.2 | 4.20 | 8 | 221 | 0.4 | 5 | 0.89 | 0.2 | 36 | 13 | 45 | 60 | 4.58 | 0.34 | 10 | 18 | 1.32 | 521 | 1 | 0.06 | 24 | 0.13 | 2 | 58 | 0.23 | 178 | 71 | | |
| 89 | 600W-850N | 15 | 0.2 | 3.49 | 6 | 120 | 0.5 | 5 | 0.82 | 0.3 | 32 | 17 | 39 | 60 | 5.22 | 0.13 | 9 | 30 | 1.98 | 1341 | 1 | 0.09 | 25 | 0.13 | 2 | 21 | 0.33 | 208 | 89 | | |
| 90 | 600W-900N | 15 | 0.2 | 4.05 | 5 | 74 | 0.4 | 5 | 0.46 | 0.3 | 22 | 16 | 23 | 68 | 4.95 | 0.11 | 6 | 31 | 2.13 | 961 | 1 | 0.06 | 24 | 0.14 | 2 | 14 | 0.24 | 189 | 72 | | |
| 91 | 950 | 25 | 0.2 | 4.11 | 4 | 158 | 0.5 | 5 | 0.72 | 0.4 | 31 | 17 | 51 | 80 | 5.16 | 0.18 | 10 | 30 | 1.86 | 817 | 1 | 0.04 | 27 | 0.15 | 2 | 42 | 0.25 | 197 | 95 | | |
| 92 | 1000 | 20 | 0.2 | 4.55 | 5 | 273 | 0.4 | 5 | 1.15 | 0.4 | 37 | 21 | 36 | 123 | 5.50 | 0.36 | 10 | 33 | 2.06 | 964 | 1 | 0.09 | 32 | 0.08 | 2 | 52 | 0.24 | 197 | 93 | | |
| 93 | 1050 | 35 | 0.2 | 3.99 | 7 | 186 | 0.3 | 5 | 0.63 | 0.4 | 30 | 14 | 39 | 48 | 5.03 | 0.32 | 8 | 21 | 1.38 | 1242 | 1 | 0.05 | 20 | 0.17 | 2 | 42 | 0.22 | 176 | 99 | | |
| 94 | 600W-1100N | 10 | 0.2 | 3.48 | 4 | 179 | 0.2 | 5 | 0.71 | 0.2 | 30 | 9 | 37 | 32 | 3.74 | 0.26 | 8 | 14 | 1.00 | 591 | 1 | 0.05 | 15 | 0.19 | 2 | 38 | 0.26 | 150 | 63 | | |
| 95 | 600W-1150N | 10 | 0.2 | 4.25 | 2 | 169 | 0.3 | 5 | 1.17 | 0.4 | 37 | 16 | 16 | 69 | 5.69 | 0.44 | 9 | 29 | 1.74 | 817 | 1 | 0.10 | 13 | 0.10 | 2 | 28 | 0.34 | 182 | 96 | | |
| 96 | 1200 | 25 | 0.2 | 3.95 | 8 | 156 | 0.3 | 5 | 0.56 | 0.5 | 31 | 16 | 20 | 79 | 5.69 | 0.33 | 9 | 33 | 1.85 | 858 | 1 | 0.06 | 14 | 0.10 | 2 | 17 | 0.29 | 167 | 105 | | |
| 97 | 1250 | 45 | 0.2 | 5.28 | 3 | 200 | 0.4 | 5 | 0.54 | 0.5 | 35 | 18 | 36 | 94 | 5.80 | 0.42 | 12 | 32 | 2.27 | 1015 | 1 | 0.09 | 32 | 0.12 | 2 | 20 | 0.28 | 206 | 114 | | |
| 98 | 1300 | 25 | 0.2 | 5.10 | 6 | 247 | 0.4 | 5 | 0.89 | 0.3 | 36 | 19 | 32 | 95 | 5.96 | 0.47 | 11 | 34 | 2.29 | 1442 | 1 | 0.10 | 34 | 0.12 | 2 | 30 | 0.27 | 198 | 125 | | |
| 101 | 600W-1350N | 120 | 0.2 | 5.09 | 18 | 257 | 0.3 | 5 | 1.06 | 0.3 | 41 | 24 | 26 | 103 | 6.40 | 0.47 | 14 | 37 | 2.05 | 1727 | 1 | 0.22 | 32 | 0.10 | 2 | 46 | 0.22 | 179 | 98 | | |
| 102 | 600W-1400N | 25 | 0.2 | 4.46 | 2 | 221 | 0.3 | 5 | 0.55 | 0.2 | 31 | 20 | 37 | 90 | 5.34 | 0.47 | 10 | 29 | 2.24 | 1182 | 1 | 0.06 | 33 | 0.09 | 2 | 25 | 0.19 | 177 | 103 | | |
| 103 | 1450 | 35 | 0.2 | 4.68 | 2 | 276 | 0.3 | 5 | 0.77 | 0.2 | 37 | 22 | 40 | 99 | 5.83 | 0.54 | 11 | 28 | 2.14 | 1440 | 1 | 0.11 | 38 | 0.09 | 2 | 29 | 0.21 | 195 | 107 | | |
| 104 | 600W-1482N | 40 | 0.2 | 4.66 | 2 | 260 | 0.3 | 5 | 0.96 | 0.2 | 40 | 21 | 39 | 92 | 5.79 | 0.57 | 12 | 28 | 2.01 | 1327 | 1 | 0.14 | 41 | 0.09 | 2 | 39 | 0.24 | 185 | 100 | | |
| 105 | 600E-850N | 45 | 0.2 | 4.26 | 5 | 219 | 0.4 | 5 | 1.40 | 0.2 | 41 | 16 | 39 | 40 | 5.30 | 0.31 | 11 | 22 | 1.48 | 526 | 2 | 0.06 | 24 | 0.12 | 2 | 78 | 0.26 | 199 | 77 | | |
| 106 | 600E-900N | 100 | 0.2 | 4.86 | 2 | 126 | 0.5 | 5 | 1.74 | 0.2 | 41 | 16 | 25 | 153 | 4.69 | 0.20 | 10 | 19 | 1.44 | 673 | 1 | 0.07 | 19 | 0.12 | 2 | 84 | 0.28 | 154 | 76 | | DARB |
| 107 | 600E-950N | 105 | 0.2 | 3.85 | 4 | 182 | 0.4 | 5 | 1.35 | 0.2 | 38 | 15 | 32 | 98 | 5.46 | 0.26 | 9 | 16 | 1.37 | 739 | 2 | 0.07 | 20 | 0.16 | 2 | 67 | 0.30 | 185 | 78 | | |
| 108 | 1000 | 20 | 0.2 | 4.19 | 2 | 168 | 0.3 | 5 | 1.56 | 0.2 | 41 | 9 | 40 | 33 | 4.09 | 0.26 | 10 | 15 | 1.31 | 544 | 1 | 0.07 | 25 | 0.15 | 2 | 81 | 0.32 | 157 | 72 | | |
| 109 | 1050 | 130 | 0.2 | 4.03 | 3 | 234 | 0.5 | 5 | 1.50 | 0.2 | 45 | 11 | 37 | 39 | 4.64 | 0.34 | 12 | 19 | 1.30 | 497 | 2 | 0.07 | 21 | 0.13 | 2 | 77 | 0.25 | 152 | 80 | | |
| 110 | 1100 | 25 | 0.2 | 5.38 | 2 | 183 | 0.5 | 5 | 1.87 | 0.2 | 44 | 18 | 39 | 81 | 5.11 | 0.32 | 10 | 18 | 1.81 | 823 | 1 | 0.09 | 29 | 0.10 | 2 | 95 | 0.28 | 165 | 91 | | |
| 111 | 600E-1150N | 80 | 0.2 | 4.14 | 16 | 224 | 0.4 | 5 | 1.62 | 0.6 | 50 | 18 | 34 | 127 | 5.42 | 0.30 | 15 | 24 | 1.44 | 599 | 1 | 0.07 | 26 | 0.11 | 4 | 84 | 0.24 | 171 | 99 | | |
| 112 | 600E-1200N | 160 | 0.2 | 4.62 | 15 | 279 | 0.4 | 5 | 0.83 | 0.4 | 39 | 19 | 32 | 76 | 5.04 | 0.36 | 11 | 22 | 1.40 | 1006 | 1 | 0.07 | 25 | 0.10 | 3 | 56 | 0.17 | 161 | 86 | | |
| 113 | 1250 | 160 | 0.2 | 4.34 | 11 | 278 | 0.4 | 5 | 0.76 | 0.2 | 38 | 14 | 38 | 50 | 4.81 | 0.39 | 11 | 21 | 1.32 | 526 | 1 | 0.07 | 23 | 0.11 | 4 | 57 | 0.17 | 173 | 75 | | |
| 114 | 1300 | 75 | 0.2 | 4.12 | 12 | 269 | 0.4 | 5 | 0.80 | 0.4 | 39 | 13 | 38 | 40 | 4.58 | 0.38 | 11 | 19 | 1.22 | 619 | 1 | 0.06 | 21 | 0.12 | 5 | 58 | 0.19 | 170 | 67 | | |
| 115 | 1350 | 50 | 0.2 | 4.70 | 10 | 193 | 0.4 | 5 | 1.25 | 0.3 | 43 | 13 | 35 | 88 | 4.93 | 0.27 | 12 | 18 | 1.45 | 637 | 1 | 0.06 | 23 | 0.19 | 4 | 90 | 0.26 | 175 | 85 | | |
| 116 | 600E-1400N | 70 | 0.2 | 4.44 | 12 | 259 | 0.4 | 5 | 1.13 | 0.5 | 43 | 21 | 37 | 108 | 5.14 | 0.36 | 12 | 18 | 1.44 | 1197 | 1 | 0.07 | 26 | 0.13 | 2 | 75 | 0.24 | 177 | 87 | | |
| 117 | 600E-1450N | 40 | 0.2 | 4.79 | 7 | 316 | 0.4 | 5 | 0.87 | 0.4 | 39 | 14 | 48 | 59 | 4.89 | 0.47 | 12 | 23 | 1.53 | 505 | 1 | 0.07 | 28 | 0.11 | 4 | 60 | 0.20 | 187 | 88 | | |
| 118 | 1500 | 35 | 0.2 | 4.85 | 7 | 268 | 0.4 | 5 | 0.79 | 0.4 | 34 | 13 | 40 | 61 | 4.81 | 0.39 | 11 | 20 | 1.33 | 822 | 2 | 0.06 | 23 | 0.15 | 5 | 50 | 0.22 | 169 | 98 | | |
| 119 | 1550 | 20 | 0.2 | 4.62 | 5 | 164 | 0.4 | 5 | 0.55 | 0.3 | 32 | 9 | 32 | 51 | 3.99 | 0.24 | 10 | 14 | 0.84 | 854 | 1 | 0.05 | 13 | 0.18 | 6 | 33 | 0.21 | 129 | 64 | | |
| 120 | 1600 | 35 | 0.2 | 5.35 | 9 | 274 | 0.5 | 5 | 0.80 | 0.6 | 32 | 20 | 35 | 104 | 5.18 | 0.34 | 11 | 23 | 1.62 | 1057 | 1 | 0.05 | 30 | 0.12 | 9 | 46 | 0.22 | 170 | 87 | | |
| 121 | 600E-1650N | 1630 | 0.2 | 4.38 | 6 | 202 | 0.3 | 5 | 0.64 | 0.4 | 33 | 11 | 35 | 50 | 4.37 | 0.24 | 10 | 16 | 0.94 | 978 | 2 | 0.04 | 15 | 0.19 | 2 | 41 | 0.23 | 143 | 74 | | |
| 122 | 600E-1700N | 20 | 0.2 | 4.88 | 5 | 273 | 0.4 | 5 | 0.82 | 0.2 | 33 | 17 | 30 | 79 | 5.27 | 0.29 | 9 | 24 | 1.57 | 1266 | 1 | 0.06 | 24 | 0.16 | 2 | 47 | 0.26 | 185 | 91 | | |
| 123 | 1750 | 40 | 0.2 | 4.83 | 7 | 312 | 0.4 | 5 | 0.76 | 0.2 | 34 | 19 | 33 | 81 | 5.58 | 0.40 | 10 | 25 | 1.73 | 1297 | 1 | 0.06 | 27 | 0.13 | 2 | 50 | 0.24 | 199 | 97 | | |
| 124 | 1800 | 100 | 0.2 | 4.49 | 16 | 394 | 0.4 | 5 | 0.76 | 0.2 | 31 | 19 | 37 | 82 | 5.42 | 0.57 | 9 | 24 | 1.80 | 874 | 1 | 0.08 | 31 | 0.08 | 2 | 46 | 0.14 | 196 | 95 | | |
| 125 | 1850 | 15 | 0.2 | 5.92 | 2 | 243 | 0.4 | 5 | 1.07 | 0.2 | 38 | 15 | 42 | 83 | 5.44 | 0.34 | 9 | 19 | 1.47 | 777 | 1 | 0.06 | 24 | 0.18 | 2 | 63 | 0.27 | 168 | 103 | | 100% |
| 126 | 600E-1900N | 150 | 0.2 | 5.21 | 2 | 219 | 0.5 | 5 | 0.85 | 0.2 | 43 | 12 | 43 | 52 | 5.15 | 0.37 | 13 | 21 | 1.52 | 624 | 1 | 0.08 | 25 | 0.14 | 2 | 48 | 0.26 | 158 | 96 | | |
| 127 | 600E-1950N | 130 | 0.2 | 4.71 | 19 | 447 | 0.5 | 5 | 0.65 | 0.2 | 34 | 22 | 45 | 93 | 5.91 | 0.53 | 10 | 23 | 1.70 | 919 | 1 | 0.07 | 34 | 0.09 | 5 | 52 | 0.17 | 201 | 103 | | |
| 128 | 2000 | 40 | 0.2 | 4.76 | 2 | 206 | 0.4 | 5 | 1.47 | 0.3 | 46 | 18 | 31 | 82 | 4.88 | 0.41 | 12 | 21 | 1.83 | 838 | 1 | 0.09 | 28 | 0.10 | 2 | 61 | 0.22 | 161 | 98 | | |
| 129 | 2050 | 20 | 0.2 | 4.69 | 2 | 164 | 0.5 | 5 | 1.14 | 0.2 | 39 | 12 | 37 | 54 | 4.37 | 0.27 | 10 | 15 | 1.21 | 621 | 1 | 0.07 | 18 | 0.14 | 2 | 54 | 0.27 | 146 | 69 | | |
| 130 | 2100 | 10 | 0.2 | 5.09 | 2 | 157 | 0.3 | 5 | 1.07 | 0.2 | 37 | 11 | 34 | 58 | 4.36 | 0.22 | 8 | 14 | 1.25 | 645 | 1 | 0.06 | 18 | 0.14 | 2 | 46 | 0.22 | 130 | 76 | | |
| 131 | 600E-2150N | 20 | 0.2 | 5.13 | 2 | 208 | 0.4 | 5 | 1.31 | 0.3 | 44 | 15 | 40 | 73 | 5.02 | 0.36 | 12 | 21 | 1.62 | 760 | 2 | 0.09 | 25 | 0.11 | 2 | 68 | 0.26 | 162 | 103 | | |

| T.T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Be ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm | 6307-023 Pg. 4 of 10 |
|----------|-------------|--------|--------|------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|----------------------|
| 132 | 600E-2200N | 40 | 0.2 | 5.57 | 2 | 271 | 0.5 | 5 | 1.32 | 0.2 | 48 | 20 | 37 | 171 | 5.29 | 0.46 | 13 | 22 | 1.83 | 927 | 2 | 0.11 | 35 | 0.09 | 2 | 73 | 0.22 | 165 | 111 | |
| 133 | 2250 | 25 | 0.2 | 5.21 | 2 | 235 | 0.4 | 5 | 1.20 | 0.2 | 43 | 11 | 39 | 117 | 4.59 | 0.49 | 12 | 19 | 1.41 | 608 | 2 | 0.11 | 29 | 0.15 | 2 | 78 | 0.24 | 153 | 92 | DARB |
| 134 | 2300 | 155 | 0.2 | 6.50 | 6 | 453 | 0.6 | 5 | 0.78 | 0.4 | 40 | 36 | 14 | 747 | 8.56 | 0.86 | 13 | 24 | 1.66 | 2109 | 17 | 0.32 | 25 | 0.16 | 7 | 105 | 0.10 | 154 | 179 | |
| 135 | 2350 | 140 | 0.2 | 6.34 | 10 | 471 | 0.5 | 7 | 0.71 | 0.7 | 42 | 52 | 16 | 714 | 8.56 | 0.87 | 14 | 25 | 1.68 | 2869 | 15 | 0.31 | 34 | 0.16 | 9 | 98 | 0.10 | 153 | 196 | |
| 136 | 600E-2400N | 105 | 0.2 | 5.33 | 5 | 401 | 0.7 | 5 | 0.71 | 0.9 | 40 | 43 | 106 | 490 | 7.06 | 0.75 | 14 | 33 | 2.93 | 2223 | 5 | 0.29 | 154 | 0.17 | 2 | 88 | 0.09 | 130 | 164 | |
| 137 | 600E-2450N | 10 | 0.2 | 4.69 | 15 | 173 | 0.4 | 5 | 1.36 | 0.3 | 39 | 14 | 54 | 54 | 4.68 | 0.17 | 9 | 13 | 1.08 | 1776 | 1 | 0.04 | 24 | 0.21 | 2 | 75 | 0.34 | 158 | 82 | |
| 138 | 600E-2500N | 10 | 0.2 | 5.47 | 7 | 148 | 0.4 | 5 | 1.32 | 0.2 | 43 | 20 | 62 | 77 | 5.96 | 0.31 | 11 | 16 | 1.84 | 1184 | 1 | 0.06 | 37 | 0.20 | 2 | 100 | 0.39 | 184 | 112 | |
| 139 | 800N-200E | 25 | 0.2 | 3.96 | 3 | 263 | 0.3 | 5 | 2.40 | 0.3 | 38 | 26 | 62 | 472 | 5.77 | 0.33 | 8 | 23 | 2.13 | 851 | 6 | 0.06 | 49 | 0.09 | 2 | 86 | 0.45 | 237 | 102 | DARB |
| 140 | 600E | 30 | 0.2 | 4.38 | 8 | 209 | 0.5 | 5 | 1.48 | 0.2 | 43 | 20 | 51 | 110 | 5.15 | 0.31 | 11 | 17 | 1.44 | 794 | 1 | 0.06 | 30 | 0.15 | 2 | 81 | 0.24 | 173 | 68 | |
| 141 | 800N-200W | 30 | 0.2 | 4.34 | 2 | 199 | 0.8 | 5 | 0.69 | 0.2 | 45 | 12 | 27 | 79 | 5.44 | 0.27 | 19 | 30 | 1.53 | 618 | 1 | 0.06 | 17 | 0.14 | 3 | 36 | 0.29 | 202 | 76 | |
| 142 | 800N-600W | 25 | 0.2 | 5.25 | 21 | 167 | 0.5 | 5 | 0.88 | 0.2 | 35 | 17 | 43 | 83 | 5.56 | 0.22 | 10 | 23 | 1.47 | 683 | 1 | 0.04 | 28 | 0.11 | 2 | 57 | 0.24 | 171 | 80 | |
| 143 | 1000 | 20 | 0.2 | 4.71 | 2 | 286 | 0.3 | 5 | 0.92 | 0.3 | 34 | 18 | 24 | 102 | 5.49 | 0.38 | 9 | 41 | 2.24 | 1430 | 1 | 0.06 | 25 | 0.10 | 2 | 39 | 0.25 | 175 | 129 | |
| 144 | 1400 | 15 | 0.2 | 4.37 | 2 | 214 | 0.5 | 5 | 0.70 | 0.2 | 36 | 15 | 41 | 61 | 5.20 | 0.25 | 12 | 29 | 1.64 | 511 | 1 | 0.04 | 26 | 0.12 | 2 | 47 | 0.28 | 195 | 100 | DARB |
| 145 | 1800 | 25 | 0.2 | 4.36 | 4 | 414 | 0.4 | 5 | 1.36 | 0.2 | 39 | 16 | 45 | 65 | 5.24 | 0.47 | 11 | 31 | 1.65 | 675 | 1 | 0.06 | 29 | 0.17 | 2 | 63 | 0.24 | 197 | 130 | |
| 146 | 800N-2200W | 240 | 0.6 | 4.87 | 8 | 549 | 0.5 | 7 | 0.55 | 0.2 | 35 | 19 | 37 | 117 | 6.19 | 0.72 | 12 | 31 | 1.42 | 852 | 1 | 0.07 | 30 | 0.15 | 5 | 57 | 0.17 | 230 | 101 | |
| 147 | 800N-2400W | 170 | 0.8 | 4.41 | 24 | 670 | 0.8 | 5 | 0.29 | 0.3 | 32 | 23 | 52 | 119 | 6.11 | 0.76 | 11 | 23 | 1.13 | 1167 | 1 | 0.08 | 38 | 0.10 | 9 | 47 | 0.13 | 224 | 109 | |
| 148 | 800N-2500W | 70 | 0.2 | 2.99 | 25 | 472 | 1.4 | 6 | 0.22 | 0.4 | 30 | 20 | 34 | 83 | 5.89 | 0.48 | 11 | 12 | 0.47 | 2105 | 1 | 0.05 | 21 | 0.14 | 10 | 86 | 0.08 | 156 | 115 | |
| 151 | 1400E-50S | 5 | 0.2 | 4.89 | 3 | 113 | 0.4 | 5 | 1.65 | 0.3 | 35 | 25 | 35 | 140 | 6.23 | 0.19 | 9 | 20 | 2.76 | 1117 | 1 | 0.03 | 38 | 0.11 | 2 | 51 | 0.48 | 254 | 125 | DARB |
| 152 | 100 | 5 | 0.2 | 4.89 | 12 | 108 | 0.4 | 5 | 1.95 | 0.3 | 41 | 25 | 60 | 210 | 5.43 | 0.18 | 10 | 18 | 2.38 | 1394 | 1 | 0.03 | 49 | 0.13 | 2 | 76 | 0.39 | 195 | 97 | |
| 153 | 1400E-150S | 5 | 0.2 | 4.89 | 2 | 110 | 0.3 | 5 | 2.38 | 0.2 | 38 | 19 | 41 | 55 | 5.25 | 0.16 | 10 | 14 | 1.89 | 1689 | 1 | 0.03 | 29 | 0.20 | 2 | 110 | 0.46 | 210 | 90 | |
| 154 | 1400E-200S | 5 | 0.2 | 5.80 | 2 | 81 | 0.3 | 5 | 2.25 | 0.2 | 30 | 32 | 183 | 148 | 6.03 | 0.09 | 6 | 18 | 2.65 | 1586 | 1 | 0.03 | 96 | 0.15 | 2 | 67 | 0.49 | 208 | 117 | |
| 155 | 250 | 20 | 0.2 | 6.67 | 2 | 116 | 0.4 | 5 | 2.42 | 0.3 | 34 | 33 | 131 | 188 | 6.29 | 0.19 | 8 | 18 | 3.40 | 1576 | 1 | 0.03 | 105 | 0.10 | 2 | 87 | 0.48 | 211 | 106 | |
| 156 | 300 | 15 | 0.2 | 5.27 | 2 | 110 | 0.5 | 5 | 2.45 | 0.2 | 39 | 17 | 66 | 108 | 5.31 | 0.20 | 10 | 16 | 1.89 | 897 | 1 | 0.04 | 43 | 0.18 | 2 | 91 | 0.41 | 191 | 93 | |
| 157 | 350 | 5 | 0.2 | 5.61 | 2 | 171 | 0.4 | 5 | 1.90 | 0.2 | 41 | 21 | 43 | 91 | 5.06 | 0.27 | 10 | 15 | 1.90 | 919 | 1 | 0.05 | 40 | 0.10 | 2 | 99 | 0.36 | 177 | 83 | |
| 158 | 1400E-400S | 5 | 0.2 | 5.51 | 11 | 122 | 0.4 | 5 | 2.61 | 0.2 | 41 | 18 | 50 | 79 | 4.97 | 0.23 | 9 | 15 | 1.92 | 806 | 1 | 0.04 | 41 | 0.10 | 2 | 99 | 0.37 | 176 | 101 | |
| 159 | 1400E-450S | 20 | 0.2 | 4.87 | 35 | 120 | 0.5 | 5 | 2.35 | 0.2 | 40 | 16 | 47 | 72 | 4.68 | 0.23 | 10 | 15 | 1.67 | 914 | 1 | 0.04 | 33 | 0.20 | 2 | 86 | 0.33 | 166 | 108 | |
| 160 | 500 | 5 | 0.2 | 4.83 | 14 | 152 | 0.4 | 5 | 2.17 | 0.2 | 40 | 15 | 49 | 75 | 4.78 | 0.25 | 9 | 15 | 1.64 | 830 | 1 | 0.04 | 36 | 0.16 | 2 | 91 | 0.33 | 169 | 80 | |
| 161 | 550 | 5 | 0.2 | 4.62 | 77 | 118 | 0.5 | 5 | 2.57 | 0.4 | 44 | 13 | 39 | 73 | 4.49 | 0.22 | 9 | 14 | 1.09 | 596 | 1 | 0.04 | 24 | 0.16 | 2 | 98 | 0.31 | 138 | 91 | |
| 162 | 600 | 5 | 0.2 | 5.81 | 37 | 69 | 0.4 | 5 | 2.75 | 0.4 | 37 | 20 | 63 | 78 | 6.14 | 0.10 | 8 | 14 | 1.80 | 1155 | 2 | 0.03 | 55 | 0.13 | 2 | 99 | 0.41 | 145 | 121 | |
| 163 | 1400E-650S | 5 | 0.2 | 4.71 | 3 | 82 | 0.4 | 5 | 2.17 | 0.7 | 40 | 58 | 22 | 103 | 7.63 | 0.09 | 9 | 8 | 0.67 | 1816 | 4 | 0.03 | 45 | 0.24 | 2 | 76 | 0.31 | 126 | 147 | |
| 164 | 1400E-700S | 10 | 0.2 | 5.36 | 7 | 146 | 0.3 | 5 | 2.51 | 0.4 | 40 | 15 | 29 | 91 | 5.34 | 0.23 | 10 | 13 | 1.43 | 804 | 2 | 0.04 | 35 | 0.13 | 2 | 115 | 0.38 | 174 | 113 | |
| 165 | 750 | 5 | 0.2 | 4.69 | 23 | 138 | 0.3 | 5 | 2.15 | 0.7 | 39 | 23 | 38 | 79 | 4.68 | 0.25 | 9 | 12 | 1.59 | 1381 | 2 | 0.05 | 28 | 0.15 | 2 | 112 | 0.23 | 158 | 106 | |
| 166 | 800 | 5 | 0.4 | 5.43 | 16 | 119 | 0.3 | 5 | 1.34 | 0.6 | 35 | 20 | 42 | 97 | 5.65 | 0.18 | 7 | 13 | 1.54 | 829 | 1 | 0.07 | 29 | 0.14 | 2 | 108 | 0.24 | 176 | 96 | |
| 167 | 850 | 5 | 0.2 | 5.34 | 3 | 107 | 0.3 | 5 | 1.59 | 0.3 | 40 | 10 | 36 | 34 | 4.28 | 0.19 | 9 | 13 | 1.35 | 663 | 1 | 0.06 | 20 | 0.12 | 2 | 100 | 0.36 | 181 | 84 | |
| 168 | 1400E-900S | 5 | 0.2 | 5.75 | 26 | 136 | 0.3 | 5 | 1.74 | 0.5 | 39 | 25 | 39 | 139 | 5.69 | 0.29 | 10 | 16 | 2.10 | 1098 | 1 | 0.06 | 42 | 0.09 | 2 | 132 | 0.23 | 192 | 104 | |
| 169 | 1400E-950S | 5 | 0.2 | 5.79 | 10 | 131 | 0.3 | 5 | 1.82 | 0.3 | 39 | 15 | 37 | 73 | 4.97 | 0.27 | 9 | 15 | 1.89 | 623 | 1 | 0.07 | 30 | 0.12 | 2 | 119 | 0.25 | 179 | 94 | |
| 170 | 1000 | 5 | 0.2 | 5.58 | 2 | 95 | 0.2 | 5 | 2.47 | 0.3 | 42 | 12 | 31 | 53 | 5.11 | 0.19 | 9 | 11 | 1.47 | 641 | 1 | 0.06 | 21 | 0.07 | 2 | 107 | 0.44 | 238 | 71 | |
| 171 | 1050 | 10 | 0.2 | 4.69 | 2 | 90 | 0.3 | 5 | 2.73 | 0.2 | 38 | 6 | 27 | 19 | 4.16 | 0.17 | 9 | 9 | 0.96 | 492 | 1 | 0.04 | 14 | 0.10 | 2 | 118 | 0.67 | 287 | 52 | |
| 172 | 1100 | 5 | 0.2 | 5.77 | 2 | 88 | 0.4 | 5 | 2.58 | 0.2 | 40 | 19 | 34 | 56 | 4.93 | 0.15 | 10 | 13 | 1.72 | 960 | 1 | 0.06 | 27 | 0.08 | 2 | 103 | 0.40 | 199 | 74 | |
| 173 | 1400E-1150S | 5 | 0.2 | 5.69 | 2 | 81 | 0.3 | 5 | 2.60 | 0.2 | 37 | 19 | 32 | 102 | 5.50 | 0.13 | 8 | 12 | 2.05 | 920 | 1 | 0.06 | 30 | 0.08 | 2 | 98 | 0.45 | 220 | 75 | |
| 174 | 1400E-000N | 5 | 0.2 | 5.11 | 2 | 124 | 0.4 | 5 | 1.48 | 0.2 | 41 | 18 | 34 | 100 | 5.99 | 0.19 | 10 | 17 | 1.89 | 871 | 2 | 0.05 | 36 | 0.14 | 2 | 62 | 0.47 | 201 | 99 | DARB |
| 175 | 50 | 5 | 0.2 | 5.57 | 2 | 83 | 0.3 | 5 | 1.88 | 0.2 | 36 | 28 | 155 | 104 | 6.03 | 0.11 | 9 | 20 | 3.06 | 1084 | 1 | 0.04 | 117 | 0.12 | 2 | 81 | 0.46 | 219 | 107 | |
| 176 | 100 | 5 | 0.2 | 4.88 | 4 | 104 | 0.4 | 5 | 2.06 | 0.3 | 54 | 20 | 81 | 109 | 5.11 | 0.15 | 18 | 18 | 2.67 | 824 | 1 | 0.04 | 64 | 0.16 | 2 | 114 | 0.42 | 176 | 99 | |
| 177 | 150 | 5 | 0.2 | 5.76 | 2 | 166 | 0.4 | 5 | 1.97 | 0.2 | 44 | 22 | 41 | 119 | 5.72 | 0.29 | 11 | 18 | 2.24 | 1104 | 1 | 0.06 | 43 | 0.14 | 2 | 110 | 0.42 | 205 | 106 | |
| 178 | 1400E-200N | 5 | 0.2 | 5.75 | 2 | 194 | 0.4 | 5 | 1.71 | 0.2 | 36 | 22 | 58 | 110 | 5.72 | 0.30 | 9 | 16 | 2.38 | 1197 | 1 | 0.05 | 56 | 0.15 | 2 | 102 | 0.40 | 197 | 91 | |

| T.T. No. | SAMPLE No. | Au | Ag | Al | As | Ba | Be | Bi | Ca | Cd | Ce | Co | Cr | Cu | Fe | K | La | Li | Mg | Mn | Mo | Na | Ni | P | Pb | Sr | Tl | V | Zn | 0307-023 | | |
|----------|-------------|-----|-----|------|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|------|------|----|-----|------|------|-----|------|----|------|----|-----|------|-----|-----|----------|-----|-----|
| | | ppb | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | ppm | % | ppm | % | ppm | ppm | % | ppm | ppm | ppm | ppm |
| 179 | 1400E-250N | 5 | 0.2 | 5.92 | 2 | 204 | 0.3 | 5 | 1.32 | 0.2 | 34 | 15 | 45 | 78 | 5.62 | 0.32 | 9 | 13 | 1.77 | 752 | 1 | 0.06 | 31 | 0.13 | 2 | 79 | 0.34 | 179 | 88 | DARB | | |
| 180 | 300 | 5 | 0.2 | 5.40 | 3 | 201 | 0.4 | 5 | 1.86 | 0.2 | 39 | 18 | 33 | 87 | 5.22 | 0.36 | 11 | 15 | 1.84 | 925 | 1 | 0.07 | 31 | 0.12 | 2 | 106 | 0.35 | 188 | 93 | DARB | | |
| 181 | 350 | 5 | 0.2 | 5.14 | 2 | 197 | 0.3 | 5 | 1.61 | 0.2 | 40 | 19 | 42 | 72 | 5.18 | 0.32 | 11 | 17 | 1.98 | 1004 | 1 | 0.06 | 35 | 0.13 | 2 | 95 | 0.36 | 186 | 96 | DARB | | |
| 182 | 400 | 5 | 0.2 | 4.42 | 2 | 168 | 0.3 | 5 | 1.50 | 0.2 | 40 | 12 | 40 | 50 | 4.71 | 0.25 | 10 | 17 | 1.75 | 716 | 1 | 0.04 | 29 | 0.11 | 2 | 71 | 0.40 | 184 | 80 | DARB | | |
| 183 | 1400E-450N | 10 | 0.2 | 4.86 | 2 | 154 | 0.3 | 5 | 2.02 | 0.2 | 40 | 12 | 29 | 46 | 4.87 | 0.24 | 9 | 14 | 1.80 | 642 | 1 | 0.05 | 22 | 0.12 | 2 | 104 | 0.44 | 210 | 75 | | | |
| 184 | 1400E-500N | 5 | 0.2 | 6.83 | 2 | 233 | 0.4 | 5 | 2.99 | 0.2 | 37 | 31 | 70 | 242 | 6.25 | 0.20 | 8 | 22 | 3.30 | 1860 | 1 | 0.03 | 56 | 0.14 | 2 | 202 | 0.53 | 269 | 122 | | | |
| 185 | 550 | 10 | 0.2 | 6.03 | 2 | 102 | 0.4 | 5 | 1.32 | 0.2 | 35 | 26 | 90 | 105 | 6.08 | 0.15 | 8 | 23 | 3.17 | 969 | 1 | 0.04 | 62 | 0.10 | 2 | 58 | 0.48 | 231 | 84 | | | |
| 186 | 600 | 5 | 0.2 | 5.29 | 11 | 284 | 0.9 | 5 | 1.41 | 0.2 | 46 | 9 | 56 | 126 | 4.09 | 0.39 | 11 | 21 | 1.00 | 497 | 1 | 0.05 | 26 | 0.21 | 3 | 99 | 0.37 | 136 | 118 | | | |
| 187 | 650 | 5 | 0.2 | 4.22 | 2 | 117 | 0.7 | 5 | 0.62 | 0.2 | 44 | 7 | 33 | 42 | 4.03 | 0.18 | 15 | 14 | 0.66 | 415 | 2 | 0.08 | 13 | 0.13 | 4 | 44 | 0.26 | 110 | 73 | | | |
| 188 | 1400E-700N | 5 | 0.2 | 5.23 | 2 | 112 | 0.3 | 5 | 2.16 | 0.2 | 37 | 11 | 29 | 47 | 4.56 | 0.16 | 9 | 13 | 1.75 | 655 | 2 | 0.04 | 21 | 0.13 | 2 | 95 | 0.46 | 217 | 74 | KLI | | |
| 189 | 1400E-750N | 5 | 0.2 | 5.82 | 2 | 93 | 0.4 | 5 | 2.08 | 0.4 | 37 | 20 | 45 | 85 | 5.58 | 0.14 | 10 | 18 | 2.36 | 1071 | 1 | 0.03 | 32 | 0.16 | 2 | 89 | 0.50 | 262 | 89 | | | |
| 190 | 800 | 50 | 0.2 | 5.12 | 2 | 219 | 0.4 | 5 | 1.97 | 0.2 | 36 | 21 | 38 | 95 | 5.48 | 0.31 | 10 | 17 | 2.06 | 1088 | 1 | 0.08 | 32 | 0.12 | 2 | 102 | 0.33 | 202 | 95 | | | |
| 191 | 850 | 5 | 0.2 | 4.44 | 2 | 153 | 0.3 | 5 | 1.61 | 0.3 | 39 | 17 | 48 | 100 | 4.90 | 0.20 | 11 | 18 | 1.91 | 727 | 1 | 0.05 | 25 | 0.11 | 2 | 69 | 0.36 | 197 | 82 | | | |
| 192 | 900 | 75 | 0.2 | 4.45 | 6 | 142 | 0.4 | 5 | 1.61 | 0.3 | 43 | 15 | 37 | 56 | 4.40 | 0.23 | 12 | 17 | 1.62 | 561 | 1 | 0.07 | 29 | 0.10 | 2 | 89 | 0.26 | 168 | 86 | | | |
| 193 | 1400E-950N | 15 | 0.2 | 4.03 | 5 | 183 | 0.3 | 5 | 1.55 | 0.3 | 40 | 12 | 35 | 33 | 4.33 | 0.32 | 11 | 15 | 1.39 | 727 | 1 | 0.07 | 22 | 0.14 | 3 | 74 | 0.26 | 163 | 103 | | | |
| 194 | 1400E-1000N | 35 | 0.2 | 4.53 | 2 | 143 | 0.4 | 5 | 1.55 | 0.2 | 41 | 16 | 31 | 68 | 4.85 | 0.23 | 11 | 17 | 1.91 | 637 | 1 | 0.09 | 28 | 0.11 | 2 | 72 | 0.30 | 165 | 94 | | | |
| 195 | 1050 | 20 | 0.2 | 4.74 | 13 | 161 | 0.4 | 5 | 1.93 | 0.3 | 41 | 16 | 35 | 138 | 4.60 | 0.29 | 10 | 15 | 1.96 | 783 | 1 | 0.07 | 37 | 0.11 | 2 | 100 | 0.29 | 166 | 147 | | | |
| 196 | 1100 | 60 | 0.2 | 4.81 | 8 | 176 | 0.4 | 5 | 2.02 | 0.4 | 48 | 19 | 29 | 99 | 4.84 | 0.35 | 11 | 14 | 1.81 | 899 | 1 | 0.08 | 33 | 0.10 | 2 | 99 | 0.28 | 170 | 99 | | | |
| 197 | 1150 | 25 | 0.2 | 4.37 | 5 | 175 | 0.3 | 5 | 1.53 | 0.3 | 43 | 9 | 32 | 41 | 3.78 | 0.30 | 11 | 13 | 1.22 | 493 | 1 | 0.06 | 17 | 0.14 | 4 | 89 | 0.27 | 153 | 71 | | | |
| 198 | 1400E-1200N | 65 | 0.2 | 3.93 | 7 | 218 | 0.4 | 5 | 1.20 | 0.3 | 40 | 13 | 38 | 43 | 4.61 | 0.35 | 11 | 15 | 1.32 | 507 | 1 | 0.06 | 24 | 0.12 | 4 | 72 | 0.23 | 173 | 72 | | | |
| 201 | 1400E-1250N | 30 | 0.2 | 4.24 | 3 | 195 | 0.4 | 5 | 1.19 | 0.2 | 42 | 13 | 44 | 60 | 4.26 | 0.29 | 12 | 15 | 1.29 | 451 | 1 | 0.06 | 22 | 0.13 | 4 | 71 | 0.24 | 156 | 67 | | | |
| 202 | 1300 | 20 | 0.2 | 4.83 | 2 | 151 | 0.4 | 5 | 1.32 | 0.2 | 36 | 12 | 50 | 60 | 4.21 | 0.25 | 9 | 16 | 1.47 | 521 | 1 | 0.05 | 27 | 0.13 | 2 | 69 | 0.28 | 160 | 74 | | | |
| 203 | 1400E-1350N | 40 | 0.2 | 5.24 | 2 | 174 | 0.3 | 5 | 1.39 | 0.3 | 37 | 11 | 46 | 68 | 4.75 | 0.35 | 9 | 14 | 1.42 | 579 | 2 | 0.07 | 26 | 0.14 | 2 | 79 | 0.27 | 159 | 82 | | | |
| 204 | 1400W-100S | 45 | 0.2 | 5.12 | 9 | 247 | 0.4 | 5 | 1.16 | 0.3 | 38 | 16 | 27 | 67 | 5.09 | 0.33 | 10 | 19 | 1.52 | 785 | 1 | 0.06 | 23 | 0.10 | 2 | 60 | 0.27 | 170 | 82 | | | |
| 205 | 1400W-150S | 30 | 0.2 | 4.48 | 21 | 204 | 0.3 | 5 | 1.49 | 0.3 | 40 | 20 | 34 | 97 | 5.00 | 0.30 | 11 | 16 | 1.62 | 972 | 1 | 0.06 | 32 | 0.09 | 2 | 80 | 0.24 | 180 | 78 | DARB | | |
| 206 | 1400W-200S | 15 | 0.2 | 4.98 | 6 | 198 | 0.3 | 5 | 1.15 | 0.3 | 38 | 13 | 34 | 52 | 5.37 | 0.33 | 10 | 24 | 1.55 | 599 | 1 | 0.05 | 23 | 0.12 | 2 | 64 | 0.26 | 206 | 96 | | | |
| 207 | 250 | 10 | 0.2 | 5.05 | 5 | 231 | 0.4 | 5 | 1.68 | 0.2 | 41 | 16 | 32 | 91 | 4.54 | 0.31 | 10 | 16 | 1.51 | 733 | 1 | 0.07 | 27 | 0.11 | 2 | 78 | 0.23 | 164 | 78 | | | |
| 208 | 300 | 15 | 0.2 | 4.88 | 3 | 174 | 0.4 | 5 | 1.53 | 0.3 | 42 | 13 | 27 | 67 | 5.02 | 0.27 | 10 | 21 | 1.46 | 647 | 2 | 0.07 | 22 | 0.09 | 4 | 82 | 0.30 | 172 | 78 | | | |
| 209 | 350 | 50 | 0.2 | 4.78 | 2 | 256 | 0.5 | 5 | 1.89 | 0.3 | 45 | 12 | 28 | 60 | 4.56 | 0.27 | 10 | 16 | 1.34 | 632 | 1 | 0.07 | 24 | 0.10 | 2 | 87 | 0.31 | 159 | 74 | | | |
| 210 | 1400W-400S | 15 | 0.2 | 6.23 | 28 | 669 | 0.4 | 5 | 0.80 | 0.6 | 35 | 24 | 70 | 154 | 5.94 | 0.55 | 11 | 27 | 2.38 | 872 | 1 | 0.16 | 56 | 0.08 | 3 | 41 | 0.28 | 275 | 124 | | | |
| 211 | 1400W-450S | 5 | 0.4 | 5.26 | 2 | 555 | 0.3 | 5 | 0.96 | 0.4 | 36 | 23 | 57 | 94 | 5.60 | 0.56 | 12 | 42 | 2.64 | 1198 | 1 | 0.17 | 40 | 0.06 | 2 | 74 | 0.28 | 254 | 86 | | | |
| 212 | 500 | 20 | 0.2 | 4.82 | 2 | 196 | 0.3 | 5 | 1.75 | 0.2 | 41 | 12 | 32 | 49 | 4.56 | 0.28 | 11 | 13 | 1.46 | 684 | 1 | 0.07 | 18 | 0.10 | 2 | 83 | 0.31 | 168 | 69 | | | |
| 213 | 550 | 10 | 0.2 | 4.54 | 5 | 158 | 0.3 | 5 | 1.07 | 0.2 | 37 | 20 | 54 | 108 | 5.09 | 0.17 | 10 | 24 | 1.87 | 769 | 2 | 0.05 | 38 | 0.09 | 2 | 44 | 0.27 | 238 | 85 | | | |
| 214 | 600 | 10 | 0.2 | 4.77 | 2 | 173 | 0.3 | 5 | 1.01 | 0.2 | 36 | 9 | 37 | 45 | 4.69 | 0.14 | 10 | 24 | 1.24 | 476 | 1 | 0.05 | 18 | 0.10 | 2 | 49 | 0.29 | 168 | 63 | | | |
| 215 | 1400W-650S | 45 | 0.4 | 4.20 | 2 | 708 | 0.3 | 5 | 0.87 | 0.4 | 40 | 31 | 57 | 253 | 6.64 | 0.48 | 14 | 37 | 2.74 | 1927 | 1 | 0.05 | 61 | 0.07 | 2 | 27 | 0.35 | 289 | 112 | | | |
| 216 | 1400W-700S | 10 | 0.2 | 4.37 | 2 | 139 | 0.3 | 5 | 2.75 | 0.2 | 43 | 16 | 30 | 57 | 4.55 | 0.14 | 10 | 13 | 1.81 | 703 | 1 | 0.14 | 25 | 0.07 | 2 | 84 | 0.29 | 175 | 61 | | | |
| 217 | 750 | 10 | 0.2 | 4.76 | 2 | 127 | 0.3 | 5 | 2.46 | 0.2 | 42 | 12 | 31 | 28 | 4.64 | 0.20 | 10 | 13 | 1.64 | 630 | 1 | 0.10 | 22 | 0.08 | 2 | 99 | 0.32 | 181 | 66 | | | |
| 218 | 800 | 5 | 0.2 | 4.95 | 2 | 122 | 0.3 | 5 | 2.28 | 0.2 | 42 | 15 | 35 | 51 | 4.63 | 0.19 | 10 | 14 | 1.76 | 723 | 1 | 0.11 | 26 | 0.10 | 2 | 80 | 0.32 | 176 | 71 | | | |
| 219 | 850 | 5 | 0.2 | 4.27 | 2 | 131 | 0.3 | 5 | 2.39 | 0.2 | 45 | 15 | 31 | 38 | 4.84 | 0.17 | 11 | 20 | 1.30 | 683 | 1 | 0.11 | 25 | 0.10 | 2 | 81 | 0.33 | 180 | 93 | | | |
| 220 | 1400W-900S | 10 | 0.2 | 4.38 | 2 | 140 | 0.3 | 5 | 2.01 | 0.2 | 42 | 15 | 40 | 44 | 5.04 | 0.20 | 10 | 17 | 1.78 | 757 | 1 | 0.10 | 26 | 0.10 | 2 | 64 | 0.31 | 193 | 73 | | | |
| 221 | 1400W-50N | 15 | 0.2 | 4.50 | 5 | 208 | 0.5 | 5 | 1.02 | 0.2 | 43 | 17 | 52 | 71 | 5.15 | 0.26 | 12 | 25 | 1.78 | 644 | 1 | 0.05 | 32 | 0.09 | 2 | 64 | 0.27 | 190 | 77 | DARB | | |
| 222 | 100 | 80 | 0.2 | 4.86 | 6 | 190 | 0.4 | 5 | 1.15 | 0.2 | 36 | 20 | 44 | 80 | 4.98 | 0.28 | 10 | 18 | 1.59 | 817 | 1 | 0.05 | 31 | 0.10 | 2 | 73 | 0.25 | 186 | 74 | | | |
| 223 | 200 | 590 | 0.2 | 4.60 | 4 | 248 | 0.4 | 5 | 1.24 | 0.2 | 35 | 15 | 54 | 65 | 5.55 | 0.21 | 10 | 23 | 1.69 | 562 | 1 | 0.04 | 33 | 0.12 | 2 | 73 | 0.29 | 197 | 78 | | | |
| 224 | 250 | 30 | 0.6 | 4.66 | 3 | 520 | 0.7 | 5 | 0.84 | 0.2 | 43 | 21 | 55 | 184 | 7.37 | 0.52 | 17 | 27 | 0.95 | 1386 | 3 | 0.03 | 30 | 0.24 | 3 | 34 | 0.20 | 234 | 105 | | | |
| 225 | 1400W-300N | 10 | 0.2 | 4.32 | 2 | 178 | 0.2 | 5 | 2.10 | 0.2 | 43 | 18 | 40 | 53 | 5.66 | 0.19 | 12 | 32 | 2.50 | 822 | 1 | 0.14 | 34 | 0.10 | 2 | 56 | 0.37 | 252 | 80 | | | |

| T.T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Be ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Nb % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm | 8307-023 Pg. 8 of 10 |
|----------|-------------|--------|--------|------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|----------------------|
| 226 | 1400W-350N | 30 | 0.2 | 4.79 | 2 | 224 | 0.3 | 5 | 0.22 | 0.2 | 25 | 11 | 37 | 135 | 5.79 | 0.28 | 9 | 30 | 1.93 | 747 | 1 | 0.04 | 23 | 0.10 | 2 | 16 | 0.29 | 281 | 109 | |
| 227 | 400 | 25 | 0.2 | 4.69 | 37 | 171 | 0.4 | 5 | 0.88 | 0.3 | 37 | 26 | 46 | 95 | 5.95 | 0.24 | 10 | 26 | 1.91 | 1167 | 2 | 0.04 | 34 | 0.12 | 3 | 54 | 0.28 | 210 | 91 | |
| 228 | 450 | 15 | 0.2 | 4.34 | 4 | 313 | 0.4 | 5 | 0.89 | 0.2 | 41 | 16 | 48 | 40 | 5.70 | 0.33 | 12 | 20 | 1.81 | 794 | 1 | 0.05 | 35 | 0.09 | 3 | 59 | 0.28 | 245 | 86 | |
| 229 | 500 | 45 | 0.2 | 4.13 | 2 | 216 | 0.3 | 5 | 0.88 | 0.2 | 37 | 8 | 43 | 31 | 3.76 | 0.33 | 10 | 16 | 1.19 | 351 | 1 | 0.05 | 19 | 0.16 | 3 | 61 | 0.26 | 169 | 54 | |
| 230 | 1400W-550N | 35 | 0.2 | 4.84 | 4 | 220 | 0.4 | 5 | 1.29 | 0.2 | 37 | 24 | 48 | 116 | 5.94 | 0.33 | 11 | 26 | 2.27 | 1240 | 1 | 0.08 | 47 | 0.10 | 2 | 64 | 0.24 | 210 | 86 | |
| 231 | 1400W-600N | 50 | 0.2 | 4.63 | 13 | 268 | 0.4 | 5 | 0.98 | 0.3 | 40 | 23 | 51 | 118 | 5.47 | 0.39 | 13 | 24 | 1.87 | 943 | 1 | 0.06 | 39 | 0.09 | 5 | 64 | 0.25 | 204 | 84 | |
| 232 | 650 | 40 | 0.2 | 4.58 | 9 | 256 | 0.5 | 5 | 0.81 | 0.2 | 41 | 20 | 48 | 92 | 5.51 | 0.40 | 12 | 25 | 1.83 | 1116 | 1 | 0.06 | 42 | 0.12 | 2 | 52 | 0.24 | 198 | 98 | |
| 233 | 1400W-700N | 35 | 0.2 | 4.55 | 7 | 261 | 0.5 | 5 | 0.95 | 0.2 | 39 | 16 | 45 | 55 | 4.95 | 0.41 | 11 | 20 | 1.61 | 606 | 1 | 0.06 | 33 | 0.10 | 4 | 64 | 0.23 | 181 | 81 | |
| 234 | 1700E-200S | 5 | 0.2 | 4.70 | 2 | 66 | 0.2 | 5 | 3.26 | 0.5 | 43 | 19 | 12 | 72 | 5.46 | 0.10 | 11 | 11 | 1.80 | 1275 | 1 | 0.03 | 18 | 0.10 | 2 | 219 | 0.37 | 173 | 105 | |
| 235 | 1700E-250S | 10 | 0.2 | 5.37 | 9 | 223 | 0.4 | 5 | 2.19 | 0.4 | 47 | 25 | 19 | 126 | 5.60 | 0.41 | 13 | 14 | 1.73 | 1600 | 1 | 0.05 | 22 | 0.13 | 2 | 153 | 0.30 | 155 | 109 | |
| 236 | 1700E-350S | 5 | 0.2 | 5.21 | 17 | 114 | 0.3 | 5 | 3.42 | 0.3 | 44 | 19 | 21 | 89 | 5.29 | 0.20 | 11 | 13 | 1.68 | 1099 | 1 | 0.03 | 22 | 0.09 | 2 | 222 | 0.34 | 194 | 80 | |
| 237 | 400 | 10 | 0.2 | 4.72 | 14 | 160 | 0.3 | 5 | 2.63 | 0.5 | 44 | 23 | 36 | 122 | 5.24 | 0.27 | 12 | 14 | 2.01 | 1367 | 1 | 0.04 | 32 | 0.16 | 2 | 157 | 0.30 | 170 | 115 | |
| 238 | 450 | 5 | 0.2 | 5.52 | 12 | 110 | 0.3 | 5 | 2.34 | 0.3 | 46 | 20 | 40 | 101 | 5.14 | 0.19 | 11 | 15 | 1.91 | 977 | 1 | 0.04 | 36 | 0.10 | 2 | 173 | 0.31 | 197 | 83 | |
| 239 | 500 | 15 | 0.2 | 4.96 | 26 | 288 | 0.3 | 7 | 1.45 | 0.9 | 46 | 34 | 39 | 191 | 7.20 | 0.48 | 14 | 15 | 1.85 | 1590 | 6 | 0.05 | 61 | 0.13 | 4 | 136 | 0.37 | 223 | 155 | |
| 240 | 1700E-550S | 10 | 0.2 | 3.40 | 39 | 71 | 0.2 | 9 | 2.05 | 0.6 | 45 | 45 | 24 | 149 | 8.66 | 0.13 | 10 | 11 | 1.35 | 1762 | 4 | 0.03 | 31 | 0.13 | 2 | 57 | 0.40 | 188 | 124 | |
| 241 | 1700E-650S | 15 | 0.2 | 5.12 | 2 | 170 | 0.3 | 5 | 2.13 | 0.4 | 43 | 48 | 61 | 134 | 7.13 | 0.31 | 11 | 13 | 1.57 | 2710 | 2 | 0.04 | 105 | 0.18 | 2 | 81 | 0.33 | 180 | 116 | |
| 242 | 700 | 5 | 0.2 | 5.74 | 8 | 168 | 0.5 | 5 | 2.17 | 0.2 | 43 | 22 | 47 | 107 | 5.96 | 0.24 | 10 | 13 | 1.71 | 1330 | 1 | 0.04 | 40 | 0.16 | 2 | 119 | 0.41 | 182 | 100 | |
| 243 | 750 | 5 | 0.2 | 4.83 | 8 | 306 | 0.4 | 5 | 1.96 | 0.4 | 43 | 47 | 59 | 112 | 7.30 | 0.47 | 11 | 9 | 1.02 | 2519 | 6 | 0.03 | 52 | 0.17 | 2 | 109 | 0.38 | 152 | 143 | |
| 244 | 800 | 5 | 0.2 | 4.97 | 2 | 252 | 0.4 | 5 | 1.28 | 0.2 | 43 | 28 | 19 | 106 | 8.05 | 0.42 | 11 | 14 | 1.19 | 1653 | 7 | 0.05 | 24 | 0.17 | 2 | 127 | 0.43 | 143 | 118 | |
| 245 | 1700E-850S | 5 | 0.2 | 5.12 | 21 | 69 | 0.2 | 5 | 2.11 | 0.7 | 39 | 67 | 63 | 173 | 9.96 | 0.07 | 9 | 14 | 2.65 | 1843 | 4 | 0.03 | 127 | 0.15 | 2 | 107 | 0.43 | 248 | 91 | |
| 246 | 1700E-900S | 5 | 0.2 | 6.43 | 2 | 160 | 0.3 | 5 | 1.59 | 0.2 | 37 | 15 | 43 | 61 | 5.47 | 0.16 | 8 | 12 | 1.52 | 672 | 2 | 0.04 | 39 | 0.13 | 2 | 113 | 0.32 | 156 | 76 | |
| 247 | 950 | 5 | 0.2 | 3.92 | 5 | 189 | 0.3 | 5 | 1.82 | 0.2 | 44 | 16 | 27 | 55 | 5.06 | 0.22 | 13 | 17 | 1.81 | 1028 | 2 | 0.04 | 23 | 0.13 | 2 | 102 | 0.40 | 170 | 110 | |
| 248 | 1700E-1000S | 5 | 0.2 | 5.08 | 2 | 99 | 0.3 | 5 | 2.13 | 0.2 | 41 | 26 | 19 | 107 | 5.70 | 0.10 | 8 | 14 | 1.56 | 1334 | 1 | 0.04 | 24 | 0.14 | 2 | 148 | 0.46 | 196 | 92 | |
| 251 | 2200W-50S | 25 | 0.2 | 4.59 | 15 | 270 | 0.4 | 5 | 1.37 | 0.2 | 43 | 19 | 43 | 108 | 5.11 | 0.40 | 13 | 21 | 1.95 | 768 | 1 | 0.06 | 38 | 0.07 | 2 | 87 | 0.24 | 199 | 83 | |
| 252 | 2200W-100S | 30 | 0.2 | 5.01 | 6 | 262 | 0.4 | 5 | 1.79 | 0.2 | 43 | 19 | 39 | 106 | 5.49 | 0.35 | 12 | 20 | 2.24 | 800 | 1 | 0.07 | 39 | 0.09 | 2 | 106 | 0.28 | 219 | 93 | |
| 253 | 2200W-150S | 170 | 0.6 | 4.58 | 2 | 219 | 0.5 | 5 | 1.53 | 0.2 | 47 | 21 | 26 | 123 | 6.42 | 0.32 | 12 | 28 | 1.78 | 966 | 1 | 0.06 | 25 | 0.11 | 2 | 64 | 0.37 | 238 | 106 | |
| 254 | 200 | 20 | 0.2 | 5.42 | 2 | 278 | 0.4 | 5 | 1.66 | 0.2 | 40 | 22 | 27 | 94 | 5.67 | 0.34 | 10 | 19 | 1.65 | 901 | 1 | 0.09 | 27 | 0.10 | 2 | 72 | 0.27 | 170 | 87 | |
| 255 | 300 | 40 | 0.2 | 4.51 | 2 | 247 | 0.4 | 5 | 2.05 | 0.2 | 47 | 16 | 25 | 79 | 5.10 | 0.34 | 12 | 21 | 1.59 | 940 | 1 | 0.08 | 25 | 0.11 | 2 | 93 | 0.30 | 161 | 85 | |
| 256 | 350 | 95 | 0.2 | 4.76 | 2 | 199 | 0.5 | 5 | 0.59 | 0.2 | 31 | 45 | 206 | 104 | 8.57 | 0.26 | 9 | 21 | 1.45 | 1377 | 1 | 0.04 | 78 | 0.13 | 2 | 21 | 0.17 | 235 | 105 | |
| 257 | 2200W-400S | 40 | 0.2 | 4.56 | 2 | 237 | 0.2 | 5 | 0.65 | 0.2 | 29 | 22 | 23 | 63 | 5.89 | 0.16 | 9 | 32 | 1.78 | 869 | 1 | 0.13 | 18 | 0.13 | 2 | 26 | 0.29 | 186 | 89 | |
| 258 | 2200W-450S | 10 | 0.2 | 5.25 | 2 | 447 | 0.3 | 5 | 0.62 | 0.2 | 36 | 12 | 5 | 37 | 5.43 | 0.60 | 11 | 31 | 1.65 | 787 | 1 | 0.17 | 4 | 0.07 | 2 | 29 | 0.32 | 173 | 75 | |
| 259 | 500 | 55 | 0.2 | 3.81 | 2 | 513 | 0.5 | 5 | 0.28 | 0.2 | 20 | 23 | 16 | 43 | 6.27 | 0.40 | 8 | 25 | 1.64 | 818 | 1 | 0.04 | 14 | 0.07 | 2 | 14 | 0.33 | 181 | 93 | |
| 260 | 550 | 10 | 0.2 | 4.06 | 2 | 269 | 0.2 | 5 | 0.76 | 0.2 | 25 | 21 | 16 | 52 | 5.33 | 0.29 | 7 | 43 | 1.96 | 772 | 1 | 0.10 | 16 | 0.06 | 2 | 23 | 0.30 | 168 | 77 | |
| 261 | 650 | 20 | 0.2 | 4.64 | 5 | 227 | 0.3 | 5 | 1.87 | 0.2 | 40 | 17 | 26 | 70 | 5.00 | 0.27 | 10 | 19 | 1.64 | 843 | 1 | 0.07 | 19 | 0.09 | 2 | 84 | 0.29 | 173 | 77 | |
| 262 | 2200W-700S | 35 | 0.2 | 4.80 | 2 | 276 | 0.3 | 5 | 2.33 | 0.2 | 39 | 17 | 22 | 90 | 4.89 | 0.41 | 9 | 13 | 1.78 | 974 | 1 | 0.09 | 21 | 0.08 | 2 | 104 | 0.29 | 176 | 71 | |
| 263 | 2200W-750S | 20 | 0.2 | 2.94 | 2 | 186 | 0.2 | 5 | 0.19 | 0.2 | 21 | 20 | 19 | 49 | 5.00 | 0.14 | 6 | 17 | 1.06 | 678 | 1 | 0.05 | 13 | 0.06 | 2 | 7 | 0.25 | 152 | 49 | |
| 264 | 800 | 35 | 0.2 | 4.16 | 9 | 197 | 0.3 | 5 | 2.06 | 0.2 | 40 | 11 | 25 | 46 | 4.60 | 0.24 | 9 | 19 | 1.51 | 651 | 1 | 0.08 | 16 | 0.10 | 2 | 79 | 0.31 | 166 | 74 | |
| 265 | 850 | 15 | 0.2 | 4.31 | 2 | 194 | 0.3 | 5 | 1.70 | 0.2 | 38 | 11 | 26 | 40 | 4.62 | 0.25 | 9 | 15 | 1.47 | 656 | 1 | 0.08 | 18 | 0.11 | 2 | 75 | 0.30 | 167 | 75 | |
| 266 | 900 | 10 | 0.2 | 4.51 | 2 | 184 | 0.3 | 5 | 2.22 | 0.3 | 37 | 15 | 27 | 65 | 4.69 | 0.25 | 8 | 16 | 1.83 | 781 | 1 | 0.09 | 23 | 0.07 | 2 | 90 | 0.30 | 178 | 75 | |
| 267 | 2200W-950S | 10 | 0.2 | 4.56 | 4 | 181 | 0.3 | 5 | 2.36 | 0.2 | 42 | 18 | 30 | 66 | 4.91 | 0.26 | 9 | 18 | 1.85 | 920 | 1 | 0.10 | 36 | 0.08 | 2 | 92 | 0.30 | 177 | 84 | |
| 268 | 2200W-1000S | 20 | 0.2 | 3.82 | 2 | 335 | 0.3 | 5 | 0.98 | 0.2 | 34 | 17 | 20 | 54 | 5.50 | 0.23 | 9 | 24 | 1.36 | 1304 | 1 | 0.06 | 13 | 0.16 | 2 | 29 | 0.29 | 179 | 97 | |
| 269 | 1050 | 10 | 0.2 | 4.75 | 9 | 183 | 0.3 | 5 | 2.60 | 0.2 | 36 | 18 | 35 | 84 | 5.01 | 0.25 | 9 | 17 | 2.01 | 875 | 1 | 0.12 | 31 | 0.08 | 2 | 90 | 0.31 | 192 | 69 | |
| 270 | 1100 | 20 | 0.8 | 5.74 | 2 | 891 | 0.5 | 5 | 0.46 | 0.2 | 34 | 43 | 177 | 187 | 8.34 | 0.31 | 16 | 45 | 3.43 | 1610 | 1 | 0.03 | 103 | 0.12 | 2 | 27 | 0.23 | 404 | 121 | |
| 271 | 1200 | 10 | 0.2 | 3.43 | 7 | 314 | 0.3 | 5 | 0.62 | 0.4 | 33 | 31 | 22 | 314 | 6.39 | 0.35 | 13 | 29 | 1.79 | 1125 | 1 | 0.02 | 23 | 0.08 | 2 | 16 | 0.29 | 287 | 93 | |
| 272 | 2200W-1250S | 5 | 0.2 | 4.58 | 7 | 182 | 0.3 | 5 | 1.67 | 0.2 | 41 | 12 | 40 | 64 | 4.72 | 0.31 | 11 | 18 | 1.52 | 584 | 1 | 0.08 | 24 | 0.13 | 2 | 71 | 0.29 | 193 | 69 | |

DART

DART

DART

| T.T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Be ppm | Bi ppm | Cu % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm | 9307-023 Pg. 7 of 10 |
|----------|-------------|--------|--------|------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|----------------------|
| 273 | 2200W-1300S | 55 | 0.2 | 3.89 | 3 | 191 | 0.6 | 5 | 0.61 | 0.3 | 28 | 22 | 28 | 94 | 6.21 | 0.12 | 10 | 26 | 2.08 | 1037 | 1 | 0.03 | 21 | 0.12 | 2 | 39 | 0.33 | 295 | 96 | |
| 274 | 1350 | 5 | 0.2 | 4.27 | 4 | 603 | 0.8 | 5 | 0.56 | 0.2 | 27 | 19 | 9 | 120 | 5.70 | 0.32 | 9 | 29 | 1.94 | 1066 | 1 | 0.03 | 13 | 0.13 | 2 | 55 | 0.40 | 232 | 90 | |
| 275 | 1400 | 5 | 0.2 | 4.37 | 2 | 308 | 0.3 | 5 | 1.44 | 0.2 | 38 | 17 | 27 | 51 | 5.24 | 0.23 | 10 | 25 | 1.94 | 1063 | 1 | 0.07 | 20 | 0.12 | 2 | 58 | 0.31 | 198 | 104 | |
| 276 | 1450 | 5 | 0.2 | 4.30 | 2 | 159 | 0.3 | 5 | 1.97 | 0.2 | 43 | 11 | 29 | 42 | 4.38 | 0.20 | 11 | 15 | 1.39 | 574 | 1 | 0.11 | 16 | 0.12 | 2 | 76 | 0.37 | 176 | 58 | |
| 277 | 2200W-1500S | 5 | 0.2 | 5.35 | 2 | 223 | 0.3 | 5 | 0.36 | 0.2 | 28 | 22 | 26 | 61 | 6.20 | 0.27 | 10 | 38 | 3.65 | 688 | 1 | 0.02 | 30 | 0.10 | 2 | 13 | 0.43 | 279 | 89 | |
| 278 | 2200W-000N | 25 | 0.2 | 4.90 | 10 | 234 | 0.4 | 5 | 1.35 | 0.2 | 43 | 20 | 38 | 92 | 5.10 | 0.33 | 11 | 19 | 1.79 | 740 | 1 | 0.06 | 35 | 0.10 | 2 | 82 | 0.24 | 194 | 84 | |
| 279 | 50 | 75 | 0.2 | 4.58 | 6 | 256 | 0.4 | 5 | 1.29 | 0.3 | 41 | 18 | 42 | 105 | 5.51 | 0.30 | 12 | 26 | 1.90 | 1294 | 1 | 0.05 | 35 | 0.12 | 2 | 77 | 0.26 | 198 | 112 | |
| 280 | 100 | 5 | 0.2 | 3.98 | 4 | 192 | 0.3 | 5 | 1.72 | 0.2 | 42 | 16 | 32 | 43 | 4.75 | 0.28 | 11 | 20 | 1.95 | 777 | 1 | 0.06 | 29 | 0.05 | 2 | 106 | 0.21 | 191 | 79 | |
| 281 | 250 | 50 | 0.2 | 4.65 | 11 | 290 | 0.3 | 5 | 1.07 | 0.2 | 37 | 22 | 48 | 127 | 5.52 | 0.38 | 12 | 30 | 1.95 | 885 | 2 | 0.06 | 43 | 0.08 | 2 | 59 | 0.22 | 193 | 104 | |
| 282 | 2200W-300N | 60 | 0.4 | 4.36 | 6 | 283 | 0.3 | 5 | 1.16 | 0.2 | 35 | 17 | 41 | 107 | 5.38 | 0.32 | 10 | 27 | 1.93 | 621 | 1 | 0.06 | 38 | 0.07 | 2 | 62 | 0.23 | 188 | 88 | |
| 283 | 2200W-350N | 45 | 0.2 | 4.02 | 7 | 275 | 0.3 | 5 | 1.16 | 0.2 | 36 | 18 | 45 | 98 | 5.08 | 0.30 | 10 | 25 | 1.79 | 850 | 2 | 0.06 | 37 | 0.09 | 2 | 58 | 0.21 | 176 | 94 | |
| 284 | 400 | 35 | 0.4 | 4.16 | 8 | 292 | 0.3 | 5 | 1.20 | 0.2 | 37 | 18 | 52 | 88 | 5.09 | 0.31 | 10 | 26 | 1.66 | 716 | 1 | 0.05 | 35 | 0.12 | 2 | 65 | 0.23 | 183 | 95 | |
| 285 | 450 | 50 | 0.2 | 4.04 | 4 | 284 | 0.4 | 5 | 0.90 | 0.2 | 32 | 15 | 59 | 72 | 4.93 | 0.35 | 9 | 20 | 1.66 | 609 | 1 | 0.04 | 37 | 0.13 | 2 | 60 | 0.22 | 187 | 92 | |
| 286 | 500 | 40 | 0.2 | 3.89 | 8 | 258 | 0.3 | 5 | 1.24 | 0.2 | 36 | 17 | 42 | 98 | 4.94 | 0.27 | 10 | 27 | 1.75 | 740 | 1 | 0.06 | 33 | 0.07 | 2 | 63 | 0.21 | 176 | 87 | |
| 287 | 2200W-550N | 145 | 0.2 | 3.54 | 11 | 322 | 0.4 | 5 | 0.99 | 0.2 | 35 | 16 | 46 | 92 | 5.03 | 0.40 | 10 | 21 | 1.58 | 963 | 2 | 0.05 | 35 | 0.07 | 4 | 59 | 0.19 | 166 | 82 | |
| 288 | 2200W-600N | 30 | 0.4 | 3.80 | 10 | 291 | 0.3 | 5 | 1.12 | 0.2 | 37 | 14 | 48 | 62 | 4.64 | 0.36 | 10 | 22 | 1.51 | 592 | 2 | 0.05 | 27 | 0.09 | 3 | 65 | 0.20 | 169 | 102 | |
| 289 | 650 | 125 | 0.6 | 3.46 | 30 | 396 | 0.4 | 5 | 0.92 | 0.2 | 37 | 22 | 51 | 124 | 5.54 | 0.52 | 11 | 24 | 1.34 | 1108 | 2 | 0.06 | 33 | 0.11 | 4 | 64 | 0.12 | 171 | 103 | |
| 290 | 700 | 35 | 0.2 | 3.27 | 12 | 354 | 0.3 | 5 | 0.42 | 0.3 | 29 | 22 | 44 | 72 | 4.85 | 0.47 | 8 | 18 | 0.91 | 2475 | 2 | 0.04 | 19 | 0.20 | 5 | 44 | 0.11 | 173 | 82 | |
| 291 | 750 | 10 | 0.2 | 4.35 | 3 | 252 | 0.4 | 5 | 1.34 | 0.2 | 36 | 21 | 33 | 96 | 5.03 | 0.33 | 11 | 29 | 2.15 | 952 | 1 | 0.07 | 31 | 0.06 | 2 | 74 | 0.21 | 201 | 74 | |
| 292 | 2200W-850N | 130 | 0.4 | 4.55 | 16 | 469 | 0.5 | 5 | 0.68 | 0.2 | 33 | 18 | 42 | 123 | 6.23 | 0.62 | 13 | 29 | 1.52 | 564 | 1 | 0.06 | 31 | 0.13 | 3 | 68 | 0.14 | 215 | 103 | |
| 293 | 2200W-900N | 85 | 0.2 | 4.30 | 14 | 440 | 0.4 | 5 | 0.53 | 0.2 | 32 | 19 | 35 | 127 | 5.83 | 0.53 | 12 | 28 | 1.52 | 873 | 1 | 0.05 | 31 | 0.10 | 2 | 55 | 0.14 | 203 | 101 | |
| 294 | 950 | 130 | 0.2 | 4.24 | 18 | 409 | 0.4 | 5 | 0.42 | 0.2 | 32 | 22 | 39 | 134 | 5.95 | 0.52 | 12 | 28 | 1.59 | 1052 | 1 | 0.05 | 34 | 0.10 | 2 | 53 | 0.15 | 202 | 101 | |
| 295 | 1000 | 190 | 0.8 | 3.69 | 28 | 446 | 0.5 | 5 | 0.47 | 0.3 | 32 | 25 | 50 | 130 | 6.10 | 0.47 | 12 | 24 | 1.34 | 1139 | 1 | 0.05 | 40 | 0.11 | 3 | 46 | 0.12 | 192 | 107 | |
| 296 | 1050 | 210 | 1.0 | 3.56 | 35 | 497 | 0.5 | 5 | 0.42 | 0.4 | 34 | 27 | 49 | 152 | 6.53 | 0.60 | 14 | 23 | 1.09 | 1645 | 1 | 0.06 | 43 | 0.11 | 3 | 43 | 0.10 | 177 | 115 | |
| 297 | 2200W-1100N | 400 | 0.2 | 3.33 | 31 | 519 | 0.4 | 5 | 0.43 | 0.2 | 34 | 35 | 45 | 142 | 6.44 | 0.43 | 12 | 24 | 1.27 | 1458 | 1 | 0.05 | 44 | 0.07 | 2 | 48 | 0.11 | 172 | 108 | |
| 298 | 2950N-4300E | 470 | 0.2 | 4.45 | 8 | 331 | 0.4 | 5 | 1.55 | 0.2 | 42 | 23 | 47 | 183 | 4.92 | 0.36 | 11 | 16 | 1.67 | 1120 | 1 | 0.08 | 29 | 0.14 | 4 | 144 | 0.30 | 167 | 87 | |
| 3 | 4350 | 175 | 0.2 | 5.32 | 13 | 317 | 0.4 | 5 | 1.96 | 0.3 | 37 | 27 | 45 | 164 | 5.48 | 0.40 | 12 | 19 | 2.05 | 1122 | 1 | 0.11 | 33 | 0.16 | 4 | 164 | 0.35 | 192 | 101 | |
| 4 | 4400 | 110 | 0.2 | 5.25 | 13 | 311 | 0.5 | 5 | 2.23 | 0.3 | 40 | 37 | 46 | 276 | 5.75 | 0.46 | 13 | 21 | 2.42 | 1337 | 1 | 0.12 | 37 | 0.12 | 3 | 215 | 0.33 | 201 | 95 | |
| 5 | 4450 | 65 | 0.2 | 6.06 | 2 | 513 | 0.5 | 5 | 1.49 | 0.3 | 41 | 25 | 39 | 130 | 5.04 | 0.78 | 14 | 17 | 1.72 | 1245 | 1 | 0.10 | 27 | 0.12 | 6 | 150 | 0.24 | 161 | 98 | |
| 6 | 2950N-4550E | 30 | 0.2 | 4.24 | 2 | 296 | 0.3 | 5 | 1.41 | 0.2 | 39 | 5 | 21 | 20 | 3.00 | 0.69 | 13 | 10 | 0.90 | 552 | 1 | 0.06 | 8 | 0.11 | 10 | 91 | 0.38 | 160 | 63 | |
| 7 | 2950N-4600E | 20 | 0.2 | 5.10 | 2 | 289 | 0.5 | 5 | 1.38 | 0.3 | 36 | 25 | 29 | 114 | 5.36 | 0.83 | 11 | 23 | 2.38 | 1077 | 1 | 0.06 | 27 | 0.10 | 4 | 107 | 0.30 | 220 | 90 | |
| 8 | 4700 | 590 | 0.2 | 5.24 | 6 | 1290 | 0.7 | 6 | 1.18 | 0.5 | 46 | 22 | 27 | 64 | 5.72 | 0.92 | 17 | 19 | 1.32 | 1834 | 1 | 0.06 | 20 | 0.17 | 27 | 91 | 0.27 | 182 | 132 | |
| 9 | 4750 | 30 | 0.2 | 3.21 | 2 | 329 | 0.3 | 5 | 0.71 | 0.2 | 30 | 4 | 25 | 18 | 1.95 | 0.49 | 10 | 7 | 0.45 | 269 | 1 | 0.05 | 7 | 0.13 | 7 | 59 | 0.20 | 106 | 40 | |
| 10 | 4800 | 10 | 0.2 | 4.70 | 7 | 146 | 0.5 | 5 | 0.69 | 0.4 | 30 | 15 | 42 | 47 | 4.23 | 0.31 | 10 | 15 | 0.96 | 592 | 1 | 0.03 | 17 | 0.22 | 2 | 33 | 0.29 | 143 | 111 | |
| 11 | 2950N-4850E | 40 | 0.2 | 5.03 | 11 | 289 | 0.6 | 5 | 1.35 | 0.2 | 42 | 21 | 57 | 71 | 4.54 | 0.41 | 19 | 20 | 1.16 | 686 | 1 | 0.06 | 23 | 0.14 | 4 | 99 | 0.28 | 148 | 81 | |
| 12 | 2950N-4900E | 10 | 0.2 | 5.13 | 6 | 182 | 0.6 | 5 | 0.82 | 0.2 | 43 | 11 | 32 | 56 | 4.75 | 0.27 | 17 | 13 | 0.95 | 675 | 1 | 0.07 | 16 | 0.16 | 2 | 58 | 0.28 | 117 | 80 | |
| 13 | 4950 | 65 | 0.2 | 4.46 | 4 | 239 | 0.4 | 5 | 1.55 | 0.2 | 40 | 13 | 49 | 58 | 4.31 | 0.50 | 15 | 14 | 1.17 | 606 | 1 | 0.07 | 18 | 0.16 | 3 | 112 | 0.28 | 143 | 84 | |
| 14 | 5050 | 50 | 0.2 | 4.09 | 2 | 243 | 0.4 | 5 | 1.86 | 0.2 | 36 | 14 | 33 | 67 | 4.40 | 0.41 | 11 | 14 | 1.35 | 764 | 1 | 0.06 | 20 | 0.16 | 2 | 108 | 0.27 | 143 | 112 | |
| 15 | 5100 | 1900 | 0.2 | 5.45 | 2 | 130 | 0.5 | 5 | 1.55 | 0.2 | 38 | 12 | 53 | 66 | 4.55 | 0.23 | 13 | 13 | 1.08 | 531 | 1 | 0.05 | 23 | 0.16 | 5 | 110 | 0.32 | 147 | 68 | |
| 16 | 2950N-5150E | 20 | 0.2 | 4.03 | 6 | 212 | 0.3 | 5 | 1.87 | 0.3 | 37 | 23 | 27 | 113 | 5.04 | 0.46 | 13 | 15 | 2.02 | 1051 | 1 | 0.06 | 30 | 0.09 | 4 | 136 | 0.30 | 190 | 91 | |
| 17 | 2950N-5200E | 35 | 0.2 | 5.42 | 5 | 306 | 0.5 | 5 | 1.72 | 0.2 | 40 | 25 | 39 | 170 | 5.21 | 0.50 | 13 | 17 | 2.00 | 1028 | 1 | 0.09 | 31 | 0.13 | 3 | 115 | 0.32 | 183 | 97 | |
| 18 | 5250 | 80 | 0.2 | 5.35 | 16 | 288 | 0.5 | 11 | 1.36 | 0.3 | 43 | 51 | 26 | 400 | 9.90 | 0.96 | 16 | 14 | 2.09 | 3186 | 12 | 0.06 | 37 | 0.13 | 8 | 83 | 0.23 | 428 | 148 | |
| 19 | 5300 | 30 | 0.2 | 5.25 | 5 | 268 | 0.5 | 5 | 1.75 | 0.2 | 41 | 19 | 38 | 109 | 5.27 | 0.45 | 13 | 16 | 1.68 | 868 | 1 | 0.08 | 25 | 0.16 | 5 | 113 | 0.33 | 192 | 96 | |
| 20 | 5350 | 55 | 0.2 | 5.44 | 10 | 313 | 0.5 | 5 | 1.74 | 0.2 | 41 | 25 | 41 | 153 | 5.31 | 0.48 | 15 | 17 | 1.72 | 1273 | 1 | 0.08 | 27 | 0.19 | 6 | 124 | 0.29 | 170 | 116 | |
| 21 | 2950N-5450E | 30 | 0.2 | 4.83 | 15 | 218 | 0.5 | 6 | 1.34 | 0.3 | 38 | 20 | 49 | 66 | 4.70 | 0.33 | 18 | 19 | 1.09 | 568 | 1 | 0.05 | 21 | 0.15 | 4 | 96 | 0.30 | 167 | 71 | |

122

Joh

| T.T. No. | SAMPLE No. | Au | Ag | Al | As | Ba | Be | Bi | Cd | Ce | Co | Cr | Cu | Fe | K | La | Li | Mg | Mn | Mo | Na | Ni | P | Pb | Sr | Tl | V | Zn | 9307-023 | |
|----------|-------------|------|-----|------|-----|------|-----|-----|------|-----|-----|-----|-----|-----|------|------|-----|-----|------|------|-----|------|-----|------|-----|-----|------|-----|----------|-----|
| | | ppb | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | ppm | % | ppm | % | ppm | ppm | % | ppm | ppm | ppm |
| 22 | 2950N-5500E | 10 | 0.2 | 4.69 | 13 | 165 | 0.4 | 5 | 1.14 | 0.3 | 36 | 12 | 35 | 58 | 4.64 | 0.34 | 14 | 12 | 0.98 | 599 | 1 | 0.06 | 16 | 0.15 | 5 | 81 | 0.32 | 157 | 67 | |
| 23 | 5550 | 40 | 0.2 | 5.79 | 7 | 182 | 0.4 | 5 | 2.52 | 0.3 | 34 | 21 | 27 | 113 | 5.96 | 0.36 | 11 | 18 | 2.23 | 636 | 1 | 0.05 | 25 | 0.12 | 3 | 163 | 0.47 | 247 | 67 | |
| 24 | 5600 | 10 | 0.2 | 4.35 | 5 | 155 | 0.3 | 5 | 1.43 | 0.2 | 33 | 10 | 31 | 50 | 3.83 | 0.30 | 11 | 10 | 1.12 | 476 | 1 | 0.05 | 17 | 0.16 | 4 | 105 | 0.37 | 157 | 61 | |
| 25 | 5650 | 15 | 0.2 | 3.83 | 14 | 179 | 0.4 | 5 | 1.17 | 0.4 | 32 | 13 | 31 | 75 | 5.62 | 0.30 | 11 | 13 | 1.32 | 542 | 3 | 0.06 | 23 | 0.20 | 6 | 81 | 0.38 | 195 | 87 | |
| 26 | 2950N-5700E | 60 | 0.2 | 3.80 | 13 | 145 | 0.4 | 5 | 1.31 | 0.2 | 34 | 11 | 33 | 51 | 3.48 | 0.29 | 12 | 9 | 0.78 | 352 | 1 | 0.04 | 11 | 0.19 | 3 | 141 | 0.35 | 161 | 43 | |
| 27 | 2950N-5750E | 50 | 0.2 | 4.56 | 17 | 216 | 0.3 | 7 | 1.66 | 0.5 | 35 | 17 | 24 | 131 | 4.91 | 0.25 | 11 | 11 | 1.26 | 643 | 1 | 0.06 | 16 | 0.22 | 4 | 120 | 0.32 | 173 | 61 | |
| 28 | 5800 | 65 | 0.2 | 4.10 | 13 | 208 | 0.4 | 5 | 1.40 | 0.2 | 34 | 12 | 35 | 78 | 4.25 | 0.31 | 11 | 10 | 0.97 | 455 | 1 | 0.05 | 16 | 0.20 | 6 | 106 | 0.30 | 156 | 53 | |
| 29 | 5850 | 100 | 0.4 | 5.12 | 25 | 277 | 0.4 | 12 | 2.46 | 0.4 | 39 | 52 | 29 | 659 | 6.76 | 0.44 | 14 | 14 | 2.14 | 1163 | 7 | 0.08 | 34 | 0.13 | 22 | 203 | 0.38 | 249 | 82 | |
| 30 | 5900 | 55 | 0.2 | 5.09 | 18 | 290 | 0.4 | 11 | 2.00 | 0.3 | 40 | 42 | 26 | 510 | 6.39 | 0.48 | 13 | 16 | 2.25 | 1261 | 4 | 0.07 | 30 | 0.14 | 17 | 162 | 0.39 | 244 | 88 | |
| 31 | 2950N-5950E | 20 | 0.2 | 4.95 | 2 | 235 | 0.5 | 5 | 2.06 | 0.5 | 40 | 37 | 29 | 342 | 5.96 | 0.39 | 17 | 21 | 1.97 | 1213 | 4 | 0.07 | 25 | 0.17 | 4 | 161 | 0.41 | 242 | 96 | |
| 32 | 2950N-6100E | 15 | 0.2 | 3.10 | 2 | 256 | 0.2 | 5 | 1.69 | 0.2 | 31 | 2 | 16 | 11 | 2.37 | 0.43 | 9 | 5 | 0.34 | 233 | 1 | 0.05 | 5 | 0.09 | 2 | 154 | 0.55 | 176 | 27 | |
| 33 | 6150 | 10 | 0.2 | 3.27 | 2 | 171 | 0.3 | 5 | 1.35 | 0.2 | 31 | 8 | 16 | 24 | 3.74 | 0.33 | 11 | 8 | 0.84 | 401 | 2 | 0.04 | 8 | 0.12 | 2 | 119 | 0.41 | 177 | 48 | |
| 34 | 2950E-6200N | 10 | 0.2 | 3.82 | 2 | 202 | 0.3 | 5 | 1.71 | 0.2 | 33 | 8 | 20 | 30 | 4.48 | 0.40 | 11 | 10 | 0.90 | 410 | 1 | 0.06 | 11 | 0.11 | 2 | 127 | 0.44 | 221 | 44 | |
| 35 | 4650E-1950N | 210 | 0.6 | 4.06 | 2 | 363 | 0.4 | 5 | 1.34 | 0.4 | 33 | 25 | 31 | 151 | 5.93 | 0.64 | 12 | 15 | 2.26 | 1773 | 1 | 0.04 | 21 | 0.11 | 6 | 101 | 0.28 | 201 | 101 | |
| 36 | 4650E-2000N | 170 | 0.2 | 3.95 | 2 | 333 | 0.4 | 5 | 1.34 | 0.2 | 31 | 23 | 26 | 121 | 5.50 | 0.61 | 11 | 15 | 2.26 | 1689 | 1 | 0.04 | 22 | 0.11 | 4 | 97 | 0.28 | 192 | 99 | |
| 37 | 4650E-2050N | 175 | 0.6 | 4.52 | 2 | 420 | 0.5 | 5 | 1.53 | 0.3 | 34 | 27 | 36 | 192 | 5.75 | 0.59 | 12 | 17 | 2.59 | 2724 | 2 | 0.04 | 29 | 0.12 | 8 | 89 | 0.28 | 200 | 117 | |
| 38 | 2200 | 145 | 0.2 | 4.95 | 4 | 468 | 0.5 | 5 | 1.65 | 0.4 | 37 | 24 | 23 | 181 | 5.55 | 0.72 | 13 | 17 | 2.08 | 2131 | 1 | 0.07 | 25 | 0.12 | 14 | 110 | 0.25 | 178 | 141 | |
| 39 | 2250 | 140 | 0.2 | 5.75 | 2 | 464 | 0.5 | 5 | 1.32 | 0.4 | 33 | 25 | 25 | 184 | 6.05 | 0.85 | 12 | 17 | 1.89 | 1771 | 1 | 0.07 | 20 | 0.16 | 26 | 94 | 0.25 | 176 | 155 | |
| 40 | 2300 | 70 | 0.2 | 5.37 | 2 | 331 | 0.5 | 5 | 1.37 | 0.2 | 34 | 20 | 27 | 491 | 4.85 | 0.57 | 12 | 15 | 1.46 | 792 | 3 | 0.08 | 19 | 0.15 | 12 | 94 | 0.23 | 140 | 136 | |
| 41 | 4650E-2350N | 15 | 0.2 | 4.82 | 5 | 395 | 0.5 | 5 | 1.39 | 0.2 | 42 | 17 | 36 | 95 | 5.79 | 0.60 | 18 | 21 | 1.21 | 741 | 4 | 0.07 | 18 | 0.18 | 51 | 107 | 0.33 | 184 | 113 | |
| 42 | 4650E-2400N | 55 | 0.2 | 5.11 | 12 | 331 | 0.5 | 5 | 1.78 | 0.2 | 37 | 23 | 35 | 101 | 5.36 | 0.57 | 13 | 21 | 1.90 | 1758 | 1 | 0.08 | 27 | 0.17 | 7 | 135 | 0.31 | 188 | 139 | |
| 43 | 2450 | 20 | 0.2 | 4.18 | 2 | 316 | 0.3 | 5 | 1.40 | 0.2 | 32 | 15 | 30 | 49 | 4.63 | 0.57 | 11 | 14 | 1.39 | 1374 | 1 | 0.07 | 18 | 0.17 | 3 | 104 | 0.29 | 173 | 89 | |
| 44 | 2500 | 35 | 0.2 | 4.49 | 2 | 436 | 0.5 | 5 | 2.16 | 0.2 | 38 | 19 | 40 | 91 | 4.97 | 0.44 | 14 | 16 | 1.69 | 866 | 1 | 0.09 | 24 | 0.11 | 3 | 157 | 0.29 | 176 | 84 | |
| 45 | 2550 | 15 | 0.2 | 3.34 | 3 | 444 | 0.4 | 5 | 1.50 | 0.2 | 33 | 9 | 31 | 33 | 3.15 | 0.35 | 11 | 13 | 1.01 | 498 | 1 | 0.13 | 17 | 0.25 | 3 | 97 | 0.25 | 109 | 69 | |
| 46 | 4650E-2600N | 15 | 0.2 | 3.35 | 2 | 438 | 0.3 | 5 | 2.08 | 0.2 | 38 | 9 | 43 | 10 | 3.23 | 0.39 | 13 | 10 | 1.10 | 513 | 1 | 0.05 | 19 | 0.10 | 4 | 142 | 0.37 | 137 | 54 | |
| 47 | 4650E-2650N | 5 | 0.2 | 2.71 | 2 | 112 | 0.2 | 5 | 0.82 | 0.2 | 27 | 6 | 15 | 10 | 2.70 | 0.21 | 9 | 7 | 1.01 | 477 | 1 | 0.04 | 6 | 0.11 | 2 | 39 | 0.31 | 104 | 63 | |
| 48 | 2700 | 1400 | 0.2 | 3.51 | 2 | 226 | 0.4 | 5 | 0.98 | 0.2 | 39 | 8 | 29 | 28 | 4.65 | 0.35 | 15 | 11 | 0.87 | 614 | 1 | 0.07 | 11 | 0.16 | 5 | 69 | 0.37 | 143 | 86 | |
| 51 | 2750 | 20 | 0.2 | 3.67 | 5 | 407 | 0.4 | 5 | 1.43 | 0.4 | 37 | 21 | 35 | 56 | 4.36 | 0.42 | 17 | 19 | 1.23 | 1321 | 2 | 0.06 | 19 | 0.23 | 2 | 93 | 0.30 | 155 | 103 | |
| 52 | 2800 | 50 | 0.2 | 4.33 | 4 | 246 | 0.6 | 5 | 1.27 | 0.2 | 33 | 14 | 35 | 62 | 4.34 | 0.34 | 11 | 14 | 1.11 | 718 | 1 | 0.05 | 19 | 0.18 | 7 | 83 | 0.25 | 131 | 75 | |
| 53 | 4650E-2850N | 5 | 0.2 | 5.48 | 4 | 505 | 0.7 | 5 | 1.14 | 0.2 | 35 | 17 | 41 | 95 | 4.92 | 0.53 | 15 | 22 | 1.65 | 1038 | 1 | 0.06 | 26 | 0.30 | 5 | 89 | 0.29 | 173 | 121 | |
| 54 | 4650E-2900N | 15 | 0.2 | 5.67 | 2 | 497 | 0.3 | 5 | 1.58 | 0.2 | 35 | 14 | 27 | 64 | 5.07 | 0.68 | 12 | 13 | 1.17 | 976 | 1 | 0.08 | 15 | 0.17 | 8 | 119 | 0.26 | 169 | 91 | |
| 55 | 4650E-2950N | 75 | 0.2 | 4.40 | 2 | 351 | 0.3 | 5 | 1.21 | 0.2 | 36 | 9 | 26 | 39 | 3.81 | 0.60 | 13 | 10 | 0.95 | 934 | 1 | 0.07 | 13 | 0.18 | 6 | 100 | 0.28 | 155 | 66 | |
| 56 | 5000E-1850N | 80 | 0.6 | 6.29 | 2 | 682 | 0.7 | 6 | 1.35 | 0.3 | 39 | 28 | 32 | 226 | 5.90 | 0.99 | 15 | 21 | 2.46 | 3587 | 1 | 0.06 | 37 | 0.13 | 11 | 145 | 0.23 | 181 | 113 | |
| 57 | 1950 | 110 | 0.2 | 5.73 | 3 | 514 | 0.5 | 5 | 2.10 | 0.4 | 39 | 28 | 22 | 244 | 5.49 | 0.86 | 13 | 18 | 2.09 | 2285 | 1 | 0.08 | 30 | 0.12 | 11 | 169 | 0.26 | 177 | 122 | |
| 58 | 5000E-2000N | 250 | 0.2 | 5.61 | 4 | 483 | 0.6 | 5 | 1.76 | 0.3 | 40 | 27 | 35 | 192 | 5.59 | 0.84 | 13 | 18 | 2.04 | 1941 | 1 | 0.07 | 35 | 0.13 | 15 | 141 | 0.26 | 176 | 135 | |
| 59 | 5000E-2050N | 80 | 0.2 | 5.45 | 5 | 543 | 0.6 | 7 | 1.97 | 0.4 | 40 | 32 | 65 | 199 | 5.83 | 0.72 | 14 | 19 | 2.36 | 3181 | 1 | 0.06 | 77 | 0.13 | 10 | 176 | 0.26 | 188 | 118 | |
| 60 | 2350 | 810 | 0.6 | 4.60 | 8 | 618 | 0.4 | 9 | 1.49 | 0.2 | 36 | 15 | 27 | 182 | 6.88 | 0.82 | 12 | 12 | 1.38 | 768 | 3 | 0.09 | 14 | 0.16 | 87 | 130 | 0.25 | 149 | 107 | |
| 61 | 2400 | 70 | 0.2 | 5.22 | 4 | 595 | 0.5 | 5 | 1.70 | 0.2 | 44 | 22 | 40 | 127 | 5.37 | 0.50 | 20 | 25 | 1.67 | 893 | 1 | 0.08 | 24 | 0.15 | 17 | 133 | 0.31 | 182 | 115 | |
| 62 | 2450 | 60 | 0.2 | 5.94 | 2 | 1847 | 0.7 | 5 | 1.38 | 0.2 | 47 | 26 | 24 | 107 | 5.57 | 1.05 | 19 | 18 | 1.67 | 1459 | 1 | 0.08 | 24 | 0.17 | 11 | 127 | 0.26 | 163 | 107 | |
| 63 | 5000E-2500N | 45 | 0.2 | 6.28 | 2 | 791 | 0.5 | 5 | 1.54 | 0.2 | 42 | 15 | 28 | 81 | 5.18 | 0.78 | 15 | 18 | 1.66 | 790 | 1 | 0.09 | 20 | 0.11 | 7 | 123 | 0.26 | 166 | 98 | |
| 64 | 5000E-2550N | 25 | 0.2 | 5.70 | 2 | 274 | 0.5 | 5 | 1.27 | 0.2 | 35 | 17 | 37 | 94 | 6.36 | 0.46 | 12 | 18 | 1.18 | 1076 | 1 | 0.06 | 22 | 0.18 | 3 | 82 | 0.26 | 153 | 104 | |
| 65 | 2600 | 110 | 0.2 | 5.83 | 2 | 245 | 0.5 | 5 | 2.01 | 0.2 | 40 | 15 | 39 | 58 | 5.13 | 0.39 | 14 | 13 | 1.26 | 652 | 1 | 0.08 | 17 | 0.16 | 3 | 129 | 0.32 | 170 | 74 | |
| 66 | 2650 | 60 | 0.2 | 4.85 | 21 | 235 | 0.8 | 5 | 2.33 | 0.2 | 51 | 24 | 47 | 282 | 5.66 | 0.44 | 18 | 22 | 1.34 | 1060 | 4 | 0.11 | 24 | 0.21 | 3 | 130 | 0.30 | 177 | 105 | |
| 67 | 2700 | 60 | 0.2 | 5.24 | 5 | 230 | 0.5 | 5 | 2.07 | 0.2 | 39 | 18 | 52 | 108 | 5.80 | 0.35 | 13 | 16 | 1.49 | 718 | 3 | 0.08 | 21 | 0.16 | 2 | 118 | 0.35 | 183 | 108 | |
| 68 | 5000E-2750N | 35 | 0.2 | 5.77 | 2 | 175 | 0.4 | 5 | 1.44 | 0.2 | 37 | 14 | 44 | 57 | 5.27 | 0.32 | 12 | 12 | 1.27 | 703 | 1 | 0.07 | 18 | 0.16 | 3 | 89 | 0.32 | 168 | 84 | |

Soh

Coy

Coy

| T.T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Bc ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm | 6207-023 Pg. 9 of 10 |
|----------|-------------|--------|--------|------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|----------------------|
| 69 | 5000E-2800N | 20 | 0.8 | 5.14 | 2 | 174 | 0.4 | 5 | 0.95 | 0.2 | 29 | 10 | 33 | 60 | 4.86 | 0.22 | 10 | 11 | 0.92 | 442 | 1 | 0.04 | 15 | 0.19 | 2 | 62 | 0.25 | 135 | 69 | |
| 70 | 2850 | 25 | 0.2 | 5.01 | 2 | 169 | 0.4 | 5 | 1.00 | 0.2 | 35 | 22 | 51 | 97 | 6.07 | 0.33 | 12 | 17 | 2.84 | 742 | 1 | 0.05 | 32 | 0.12 | 2 | 62 | 0.42 | 251 | 82 | |
| 71 | 2900 | 110 | 0.2 | 5.37 | 4 | 294 | 0.5 | 6 | 1.88 | 0.2 | 44 | 25 | 63 | 94 | 5.50 | 0.51 | 21 | 22 | 1.56 | 912 | 1 | 0.08 | 30 | 0.15 | 3 | 139 | 0.33 | 186 | 103 | |
| 72 | 5000E-2950N | 40 | 0.2 | 5.35 | 2 | 284 | 0.5 | 5 | 1.55 | 0.2 | 35 | 18 | 41 | 112 | 5.08 | 0.43 | 13 | 15 | 1.41 | 872 | 1 | 0.07 | 22 | 0.14 | 2 | 106 | 0.28 | 155 | 95 | |
| 73 | 5400E-2000N | 15 | 0.2 | 5.48 | 2 | 182 | 0.4 | 5 | 2.34 | 0.2 | 34 | 39 | 24 | 295 | 6.83 | 0.37 | 12 | 21 | 3.22 | 1345 | 1 | 0.13 | 46 | 0.12 | 2 | 165 | 0.34 | 218 | 121 | |
| 74 | 5400E-2100N | 40 | 0.2 | 6.03 | 8 | 260 | 0.5 | 5 | 2.35 | 0.2 | 36 | 38 | 30 | 421 | 6.45 | 0.48 | 14 | 18 | 2.27 | 1259 | 1 | 0.13 | 49 | 0.14 | 9 | 144 | 0.40 | 212 | 143 | |
| 75 | 2150 | 40 | 0.2 | 5.77 | 10 | 274 | 0.5 | 5 | 2.00 | 0.2 | 37 | 40 | 30 | 380 | 6.61 | 0.50 | 14 | 18 | 2.26 | 1378 | 1 | 0.12 | 46 | 0.17 | 10 | 142 | 0.36 | 209 | 138 | |
| 76 | 2200 | 25 | 0.2 | 5.29 | 70 | 222 | 0.4 | 8 | 1.75 | 0.2 | 40 | 50 | 22 | 206 | 8.06 | 0.33 | 15 | 17 | 2.02 | 2109 | 42 | 0.08 | 29 | 0.12 | 8 | 116 | 0.39 | 250 | 102 | |
| 77 | 2250 | 55 | 0.2 | 4.49 | 9 | 276 | 0.3 | 5 | 2.27 | 0.2 | 40 | 22 | 21 | 160 | 4.81 | 0.51 | 15 | 12 | 1.36 | 801 | 2 | 0.08 | 20 | 0.10 | 4 | 152 | 0.26 | 159 | 92 | |
| 78 | 5400E-2300N | 90 | 0.2 | 4.95 | 2 | 307 | 0.5 | 5 | 1.45 | 0.2 | 38 | 15 | 33 | 179 | 5.42 | 0.53 | 14 | 14 | 1.29 | 801 | 9 | 0.07 | 22 | 0.16 | 29 | 107 | 0.29 | 148 | 104 | |
| 79 | 5400E-2350N | 60 | 0.2 | 5.58 | 446 | 218 | 0.4 | 6 | 2.14 | 0.2 | 36 | 29 | 22 | 245 | 5.92 | 0.33 | 13 | 10 | 1.05 | 851 | 2 | 0.05 | 19 | 0.17 | 2 | 154 | 0.27 | 158 | 60 | |
| 80 | 2400 | 40 | 0.2 | 4.56 | 12 | 239 | 0.5 | 5 | 2.14 | 0.2 | 41 | 23 | 36 | 154 | 5.04 | 0.45 | 14 | 13 | 1.39 | 1124 | 2 | 0.08 | 23 | 0.17 | 3 | 132 | 0.29 | 156 | 97 | |
| 81 | 2450 | 30 | 0.2 | 4.95 | 5 | 188 | 0.5 | 5 | 1.47 | 0.2 | 43 | 23 | 49 | 112 | 4.30 | 0.32 | 20 | 19 | 0.99 | 697 | 1 | 0.06 | 21 | 0.18 | 3 | 94 | 0.27 | 137 | 78 | |
| 82 | 2500 | 60 | 0.2 | 6.06 | 2 | 313 | 0.4 | 5 | 2.05 | 0.2 | 40 | 22 | 36 | 146 | 5.36 | 0.51 | 13 | 14 | 1.44 | 857 | 1 | 0.07 | 23 | 0.14 | 5 | 144 | 0.27 | 160 | 77 | |
| 83 | 5400E-2550N | 50 | 0.2 | 5.73 | 4 | 445 | 0.4 | 5 | 2.10 | 0.2 | 42 | 30 | 25 | 245 | 5.94 | 0.75 | 15 | 17 | 1.87 | 1219 | 1 | 0.11 | 29 | 0.12 | 8 | 136 | 0.31 | 192 | 120 | |
| 84 | 5400E-2600N | 55 | 0.2 | 5.39 | 2 | 418 | 0.5 | 5 | 2.26 | 0.2 | 43 | 30 | 37 | 189 | 5.78 | 0.75 | 15 | 15 | 1.69 | 1154 | 1 | 0.09 | 25 | 0.12 | 6 | 167 | 0.29 | 183 | 97 | |
| 85 | 2650 | 45 | 0.2 | 6.50 | 2 | 237 | 0.6 | 5 | 1.63 | 0.2 | 40 | 25 | 42 | 128 | 5.51 | 0.35 | 15 | 15 | 1.58 | 1264 | 1 | 0.08 | 24 | 0.20 | 4 | 95 | 0.28 | 156 | 102 | |
| 86 | 2700 | 10 | 0.2 | 4.55 | 2 | 196 | 0.4 | 5 | 1.39 | 0.2 | 38 | 10 | 38 | 37 | 4.28 | 0.35 | 13 | 12 | 1.12 | 699 | 1 | 0.06 | 19 | 0.19 | 2 | 93 | 0.32 | 144 | 75 | |
| 87 | 2750 | 40 | 0.2 | 5.66 | 2 | 166 | 0.4 | 5 | 1.18 | 0.2 | 35 | 13 | 27 | 68 | 5.13 | 0.28 | 11 | 10 | 0.95 | 469 | 1 | 0.06 | 15 | 0.17 | 5 | 72 | 0.23 | 134 | 71 | |
| 88 | 5400E-2800N | 30 | 0.2 | 4.77 | 2 | 218 | 0.4 | 5 | 1.40 | 0.2 | 37 | 16 | 24 | 68 | 4.92 | 0.39 | 12 | 13 | 1.22 | 1648 | 1 | 0.06 | 17 | 0.20 | 5 | 100 | 0.31 | 167 | 84 | |
| 89 | 5400E-2850N | 65 | 0.2 | 5.11 | 2 | 291 | 0.5 | 5 | 1.53 | 0.2 | 37 | 18 | 37 | 129 | 4.67 | 0.42 | 12 | 14 | 1.35 | 921 | 1 | 0.07 | 21 | 0.14 | 6 | 108 | 0.27 | 150 | 81 | |
| 90 | 2900 | 130 | 0.2 | 5.31 | 3 | 252 | 0.5 | 7 | 1.87 | 0.2 | 41 | 23 | 56 | 172 | 6.17 | 0.43 | 14 | 15 | 1.51 | 959 | 2 | 0.07 | 24 | 0.22 | 5 | 124 | 0.32 | 187 | 101 | |
| 91 | 5400E-2950N | 10 | 0.2 | 4.16 | 2 | 179 | 0.5 | 5 | 1.54 | 0.2 | 37 | 11 | 68 | 39 | 4.01 | 0.29 | 14 | 13 | 1.15 | 650 | 1 | 0.05 | 31 | 0.13 | 3 | 119 | 0.35 | 159 | 65 | |
| 92 | 5800E-2150N | 40 | 0.2 | 5.60 | 7 | 261 | 0.6 | 5 | 1.73 | 0.2 | 39 | 68 | 30 | 707 | 7.40 | 0.43 | 14 | 20 | 2.26 | 1529 | 6 | 0.07 | 47 | 0.11 | 8 | 137 | 0.35 | 217 | 104 | |
| 93 | 5800E-2200N | 45 | 0.2 | 6.08 | 2 | 288 | 0.5 | 5 | 1.31 | 0.2 | 32 | 50 | 27 | 794 | 7.18 | 0.46 | 12 | 19 | 2.69 | 1305 | 3 | 0.05 | 33 | 0.13 | 2 | 136 | 0.36 | 229 | 85 | |
| 94 | 5800E-2250N | 30 | 0.6 | 6.29 | 2 | 324 | 0.6 | 5 | 1.51 | 0.2 | 34 | 36 | 33 | 852 | 7.12 | 0.48 | 13 | 21 | 2.84 | 963 | 5 | 0.07 | 48 | 0.17 | 3 | 151 | 0.32 | 208 | 114 | |
| 95 | 2300 | 5 | 0.2 | 6.55 | 2 | 249 | 0.4 | 5 | 3.76 | 0.2 | 31 | 23 | 55 | 104 | 4.91 | 0.22 | 11 | 10 | 2.35 | 899 | 1 | 0.13 | 66 | 0.11 | 2 | 556 | 0.40 | 164 | 72 | |
| 96 | 2350 | 25 | 0.2 | 4.89 | 2 | 343 | 0.3 | 5 | 1.92 | 0.2 | 35 | 11 | 19 | 71 | 4.27 | 0.40 | 12 | 9 | 0.98 | 619 | 1 | 0.08 | 14 | 0.16 | 3 | 204 | 0.32 | 159 | 67 | |
| 97 | 2400 | 60 | 0.4 | 5.20 | 2 | 332 | 0.4 | 5 | 2.79 | 0.2 | 44 | 46 | 17 | 1008 | 7.41 | 0.61 | 16 | 16 | 2.13 | 1215 | 7 | 0.07 | 27 | 0.17 | 4 | 218 | 0.45 | 233 | 87 | |
| 98 | 5800E-2450N | 50 | 0.4 | 4.98 | 2 | 234 | 0.3 | 5 | 3.06 | 0.2 | 38 | 52 | 20 | 752 | 6.55 | 0.43 | 13 | 12 | 1.61 | 916 | 4 | 0.09 | 27 | 0.13 | 2 | 194 | 0.35 | 210 | 72 | |
| 101 | 5800E-2500N | 20 | 0.2 | 5.65 | 2 | 147 | 0.5 | 5 | 1.80 | 0.2 | 34 | 21 | 24 | 423 | 5.78 | 0.23 | 12 | 10 | 0.99 | 544 | 3 | 0.06 | 16 | 0.18 | 3 | 106 | 0.26 | 169 | 55 | |
| 102 | 2550 | 15 | 0.2 | 4.66 | 3 | 159 | 0.4 | 5 | 1.66 | 0.2 | 42 | 13 | 19 | 275 | 4.50 | 0.31 | 16 | 12 | 1.17 | 543 | 2 | 0.09 | 17 | 0.19 | 2 | 100 | 0.31 | 151 | 65 | |
| 103 | 2600 | 35 | 0.2 | 4.70 | 6 | 207 | 0.3 | 5 | 1.82 | 0.2 | 41 | 15 | 26 | 113 | 4.94 | 0.38 | 14 | 12 | 1.34 | 689 | 1 | 0.09 | 19 | 0.17 | 4 | 116 | 0.33 | 169 | 73 | |
| 104 | 2650 | 25 | 0.2 | 4.62 | 3 | 193 | 0.5 | 5 | 1.88 | 0.2 | 37 | 28 | 31 | 532 | 5.54 | 0.31 | 13 | 23 | 2.43 | 922 | 1 | 0.07 | 50 | 0.18 | 2 | 82 | 0.40 | 216 | 94 | |
| 105 | 5800E-2700N | 30 | 0.2 | 5.19 | 2 | 300 | 0.4 | 7 | 1.98 | 0.2 | 42 | 24 | 24 | 203 | 6.35 | 0.53 | 15 | 18 | 2.15 | 930 | 1 | 0.07 | 24 | 0.12 | 3 | 140 | 0.40 | 228 | 89 | |
| 106 | 5800E-2750N | 20 | 0.2 | 4.81 | 2 | 258 | 0.4 | 5 | 1.87 | 0.2 | 42 | 22 | 17 | 142 | 5.57 | 0.50 | 15 | 17 | 2.11 | 1032 | 1 | 0.06 | 20 | 0.17 | 3 | 148 | 0.44 | 253 | 72 | |
| 107 | 2800 | 30 | 0.2 | 4.92 | 5 | 425 | 0.4 | 10 | 1.78 | 0.2 | 45 | 30 | 16 | 307 | 6.77 | 0.77 | 17 | 17 | 2.65 | 1327 | 1 | 0.05 | 22 | 0.16 | 3 | 144 | 0.46 | 257 | 97 | |
| 108 | 2850 | 330 | 1.0 | 4.29 | 12 | 169 | 0.3 | 14 | 2.29 | 0.2 | 40 | 29 | 19 | 808 | 8.46 | 0.24 | 13 | 9 | 1.20 | 857 | 75 | 0.04 | 21 | 0.23 | 16 | 217 | 0.32 | 209 | 58 | |
| 109 | 5800E-2900N | 55 | 0.2 | 4.55 | 6 | 254 | 0.4 | 6 | 1.71 | 0.2 | 40 | 27 | 25 | 340 | 5.16 | 0.38 | 14 | 15 | 1.63 | 846 | 4 | 0.06 | 28 | 0.16 | 6 | 139 | 0.33 | 184 | 84 | |
| 110 | 6200E-2000N | 70 | 0.4 | 4.54 | 6 | 160 | 0.4 | 7 | 2.12 | 0.4 | 43 | 41 | 44 | 402 | 6.32 | 0.27 | 14 | 15 | 2.40 | 1519 | 1 | 0.05 | 39 | 0.12 | 10 | 161 | 0.39 | 232 | 101 | |
| 111 | 6200E-2050N | 35 | 0.2 | 4.37 | 2 | 235 | 0.5 | 5 | 1.88 | 0.2 | 39 | 21 | 51 | 155 | 5.03 | 0.37 | 15 | 15 | 1.51 | 741 | 1 | 0.06 | 26 | 0.11 | 3 | 159 | 0.34 | 191 | 79 | |
| 112 | 2100 | 10 | 0.2 | 5.44 | 2 | 179 | 0.5 | 5 | 2.06 | 0.3 | 35 | 41 | 34 | 524 | 6.76 | 0.27 | 12 | 21 | 3.20 | 1384 | 1 | 0.09 | 47 | 0.13 | 22 | 177 | 0.36 | 226 | 178 | |
| 113 | 2150 | 75 | 0.2 | 3.58 | 2 | 237 | 0.3 | 5 | 1.10 | 0.2 | 32 | 20 | 24 | 139 | 4.86 | 0.42 | 11 | 11 | 1.37 | 761 | 2 | 0.04 | 14 | 0.14 | 2 | 75 | 0.35 | 227 | 66 | |
| 114 | 2200 | 25 | 0.2 | 4.27 | 2 | 237 | 0.3 | 5 | 1.36 | 0.2 | 40 | 5 | 30 | 31 | 3.32 | 0.48 | 13 | 11 | 0.85 | 312 | 2 | 0.05 | 11 | 0.15 | 6 | 123 | 0.43 | 189 | 46 | |
| 115 | 6200E-2250N | 5 | 0.2 | 4.05 | 2 | 218 | 0.2 | 5 | 1.99 | 0.2 | 41 | 9 | 30 | 25 | 3.73 | 0.40 | 13 | 9 | 1.36 | 436 | 8 | 0.06 | 32 | 0.10 | 5 | 153 | 0.53 | 213 | 46 | |

Cray
↓
Cray

Cray

Cray

| SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Be ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Tl % | V ppm | Zn ppm | 8307-023 Pg. 10 of 10 |
|-------------|--------|--------|------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|--------------------------|
| 6200E-2300N | 5 | 0.2 | 4.55 | 2 | 534 | 0.4 | 5 | 1.78 | 0.2 | 46 | 6 | 16 | 16 | 3.61 | 0.65 | 15 | 9 | 0.94 | 472 | 1 | 0.05 | 8 | 0.10 | 7 | 301 | 0.55 | 191 | 52 | |
| 2350 | 10 | 0.2 | 4.83 | 2 | 276 | 0.4 | 5 | 2.38 | 0.3 | 43 | 14 | 30 | 67 | 5.04 | 0.40 | 14 | 19 | 1.58 | 1061 | 4 | 0.08 | 21 | 0.16 | 3 | 135 | 0.38 | 196 | 142 | |
| 2400 | 10 | 0.2 | 4.23 | 2 | 187 | 0.2 | 5 | 2.73 | 0.2 | 42 | 9 | 19 | 13 | 3.59 | 0.41 | 13 | 8 | 1.05 | 412 | 1 | 0.08 | 12 | 0.08 | 4 | 158 | 0.50 | 205 | 38 | |
| 2450 | 20 | 0.2 | 4.92 | 2 | 243 | 0.3 | 5 | 2.39 | 0.2 | 42 | 27 | 37 | 176 | 6.35 | 0.33 | 14 | 16 | 2.40 | 1007 | 3 | 0.08 | 34 | 0.11 | 7 | 181 | 0.45 | 262 | 90 | |
| 6200E-2500N | 5 | 0.2 | 4.47 | 2 | 200 | 0.9 | 6 | 1.28 | 0.3 | 41 | 20 | 32 | 462 | 4.46 | 0.34 | 21 | 19 | 1.35 | 1675 | 13 | 0.06 | 19 | 0.32 | 5 | 74 | 0.28 | 163 | 94 | |
| 6200E-2550N | 160 | 0.2 | 4.46 | 2 | 297 | 0.4 | 5 | 1.08 | 0.2 | 38 | 14 | 26 | 39 | 5.12 | 0.55 | 15 | 11 | 1.23 | 701 | 2 | 0.06 | 12 | 0.11 | 4 | 90 | 0.38 | 253 | 67 | |
| 2600 | 40 | 0.2 | 4.18 | 2 | 212 | 0.2 | 5 | 2.27 | 0.2 | 39 | 5 | 22 | 11 | 3.07 | 0.41 | 11 | 7 | 0.81 | 412 | 1 | 0.05 | 9 | 0.07 | 6 | 152 | 0.55 | 220 | 31 | |
| 2650 | 40 | 0.2 | 4.83 | 2 | 326 | 0.5 | 5 | 1.50 | 0.2 | 38 | 14 | 21 | 104 | 5.09 | 0.46 | 12 | 16 | 1.80 | 747 | 1 | 0.05 | 15 | 0.19 | 2 | 123 | 0.38 | 203 | 83 | |
| 2700 | 500 | 0.2 | 4.41 | 2 | 450 | 0.4 | 5 | 0.57 | 0.2 | 32 | 14 | 16 | 18 | 6.41 | 0.86 | 14 | 11 | 1.64 | 902 | 1 | 0.04 | 11 | 0.12 | 8 | 48 | 0.35 | 297 | 65 | |
| 6200E-2750N | 10 | 0.2 | 4.55 | 2 | 333 | 0.4 | 5 | 1.14 | 0.2 | 36 | 18 | 13 | 203 | 7.88 | 0.64 | 13 | 17 | 2.62 | 1172 | 1 | 0.03 | 17 | 0.23 | 2 | 78 | 0.59 | 307 | 89 | |
| 6200E-2800N | 15 | 0.2 | 4.32 | 2 | 151 | 0.3 | 5 | 1.17 | 0.2 | 31 | 11 | 21 | 168 | 5.19 | 0.25 | 9 | 8 | 0.97 | 487 | 1 | 0.04 | 11 | 0.14 | 2 | 94 | 0.28 | 166 | 50 | |
| 2900 | 60 | 0.2 | 2.95 | 2 | 203 | 0.4 | 5 | 1.22 | 0.4 | 35 | 39 | 16 | 363 | 3.39 | 0.30 | 12 | 9 | 0.89 | 2823 | 14 | 0.04 | 14 | 0.28 | 3 | 80 | 0.25 | 119 | 74 | |
| 6200E-2950N | 10 | 0.2 | 3.91 | 2 | 190 | 0.3 | 5 | 1.84 | 0.2 | 39 | 13 | 15 | 152 | 3.96 | 0.38 | 12 | 12 | 1.27 | 482 | 10 | 0.05 | 12 | 0.12 | 2 | 140 | 0.43 | 177 | 60 | |

IGNORE

NORANDA DELTA LABORATORY

Geochemical Analysis

Project Name & No.: KLIYUL - 148

Geol.: T.W.

Date received: JULY 26

LAB CODE: 9307-031

Material: 268 Soils

Sheet: 1 of 7

Date completed: AUG. 04

Remarks: * Sample screened @ -35 MBSH (0.5 mm)

□ Organic, & Humus, & Sulfide

Au - 10.0 g sample digested with aqua-regia and determined by A.A. (D.L. 5 PPB)

ICP - 0.2 g sample digested with 3 ml HClO₄/HNO₃ (4:1) at 203 °C for 4 hours diluted to 10 ml with water. Leeman PS3000 ICP determined elemental contents.

N.B. The major oxide elements and Ba, Be, Ce, La, Li, Ga are rarely dissolved completely from geological materials with this acid dissolution method.

| SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Be ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm |
|-------------|--------|--------|------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|
| 1400W-850N | 10 | 0.2 | 4.77 | 2 | 264 | 0.3 | 5 | 1.20 | 0.2 | 37 | 17 | 31 | 68 | 5.77 | 0.27 | 11 | 35 | 1.85 | 748 | 1 | 0.06 | 24 | 0.14 | 2 | 54 | 0.34 | 252 | 105 |
| 1400W-900N | 30 | 0.2 | 5.54 | 6 | 375 | 0.3 | 5 | 1.40 | 0.2 | 40 | 22 | 21 | 118 | 5.81 | 0.81 | 11 | 46 | 2.08 | 1115 | 1 | 0.16 | 24 | 0.08 | 2 | 56 | 0.30 | 206 | 116 |
| 950 | 10 | 0.2 | 4.79 | 6 | 191 | 0.4 | 5 | 0.93 | 0.2 | 38 | 18 | 33 | 81 | 5.63 | 0.24 | 12 | 41 | 1.97 | 742 | 1 | 0.07 | 26 | 0.15 | 2 | 40 | 0.28 | 213 | 107 |
| 1000 | 15 | 0.2 | 3.80 | 10 | 242 | 0.4 | 5 | 0.78 | 0.2 | 34 | 13 | 43 | 46 | 4.66 | 0.34 | 10 | 19 | 1.20 | 877 | 1 | 0.06 | 20 | 0.17 | 2 | 50 | 0.21 | 183 | 77 |
| 1400W-1050N | 40 | 0.2 | 4.78 | 15 | 334 | 0.5 | 5 | 0.68 | 0.2 | 35 | 15 | 36 | 61 | 5.29 | 0.40 | 11 | 25 | 1.29 | 703 | 1 | 0.07 | 21 | 0.15 | 5 | 54 | 0.21 | 190 | 101 |
| 1400W-1100N | 70 | 0.2 | 4.56 | 27 | 321 | 0.5 | 5 | 0.84 | 0.2 | 33 | 19 | 46 | 76 | 5.58 | 0.33 | 11 | 27 | 1.42 | 833 | 2 | 0.05 | 27 | 0.19 | 6 | 51 | 0.23 | 204 | 98 |
| 1150 | 170 | 0.2 | 3.74 | 20 | 412 | 0.4 | 5 | 0.66 | 0.2 | 29 | 18 | 67 | 58 | 5.33 | 0.38 | 11 | 20 | 1.36 | 1842 | 1 | 0.06 | 28 | 0.21 | 6 | 51 | 0.20 | 226 | 105 |
| 1200 | 35 | 0.2 | 4.34 | 19 | 298 | 0.5 | 5 | 0.67 | 0.2 | 33 | 22 | 43 | 93 | 5.50 | 0.40 | 12 | 27 | 1.90 | 1333 | 1 | 0.06 | 32 | 0.13 | 2 | 47 | 0.24 | 209 | 118 |
| 1250 | 5 | 0.2 | 5.24 | 4 | 462 | 0.4 | 5 | 1.47 | 0.2 | 38 | 14 | 6 | 42 | 4.85 | 1.22 | 11 | 27 | 1.22 | 3527 | 1 | 0.13 | 5 | 0.14 | 2 | 46 | 0.24 | 108 | 97 |
| 1400W-1300N | 10 | 0.2 | 5.07 | 4 | 317 | 0.3 | 5 | 1.02 | 0.2 | 38 | 22 | 31 | 113 | 6.05 | 0.42 | 13 | 34 | 2.30 | 1521 | 1 | 0.06 | 28 | 0.12 | 2 | 63 | 0.30 | 228 | 110 |
| 1400W-1350N | 10 | 0.2 | 7.37 | 6 | 579 | 0.5 | 5 | 1.03 | 0.2 | 40 | 25 | 20 | 118 | 6.76 | 0.81 | 13 | 45 | 2.88 | 1803 | 1 | 0.08 | 33 | 0.15 | 2 | 48 | 0.31 | 232 | 129 |
| 1400 | 5 | 0.2 | 5.44 | 3 | 178 | 0.4 | 5 | 0.91 | 0.2 | 36 | 22 | 36 | 98 | 5.82 | 0.28 | 11 | 33 | 2.29 | 1324 | 1 | 0.08 | 29 | 0.16 | 2 | 50 | 0.29 | 229 | 109 |
| 1450 | 10 | 0.2 | 4.24 | 2 | 156 | 0.3 | 5 | 1.57 | 0.2 | 37 | 13 | 24 | 42 | 5.00 | 0.18 | 10 | 21 | 1.59 | 906 | 1 | 0.06 | 15 | 0.16 | 2 | 56 | 0.26 | 157 | 100 |
| 1500 | 20 | 0.2 | 5.23 | 4 | 214 | 0.4 | 5 | 1.38 | 0.2 | 41 | 24 | 41 | 108 | 5.89 | 0.32 | 12 | 32 | 2.56 | 1109 | 1 | 0.08 | 37 | 0.13 | 2 | 58 | 0.28 | 226 | 97 |
| 1400W-1550N | 5 | 0.2 | 5.37 | 2 | 204 | 0.4 | 5 | 1.36 | 0.2 | 41 | 25 | 41 | 112 | 5.75 | 0.34 | 12 | 31 | 2.43 | 1262 | 1 | 0.08 | 34 | 0.13 | 2 | 54 | 0.27 | 219 | 94 |
| 1400W-1600N | 5 | 0.2 | 4.19 | 5 | 279 | 0.2 | 5 | 1.45 | 0.3 | 40 | 26 | 23 | 212 | 6.19 | 0.24 | 12 | 26 | 2.27 | 1448 | 1 | 0.13 | 27 | 0.10 | 2 | 33 | 0.32 | 241 | 107 |
| 1650 | 5 | 0.2 | 5.28 | 3 | 217 | 0.4 | 5 | 1.37 | 0.2 | 41 | 24 | 40 | 116 | 5.67 | 0.41 | 13 | 27 | 2.47 | 1032 | 1 | 0.09 | 33 | 0.13 | 2 | 45 | 0.25 | 193 | 105 |
| 1700 | 65 | 0.2 | 4.94 | 2 | 213 | 0.4 | 5 | 1.02 | 0.3 | 42 | 22 | 41 | 117 | 5.31 | 0.40 | 14 | 24 | 2.09 | 1180 | 1 | 0.09 | 32 | 0.12 | 2 | 36 | 0.23 | 180 | 90 |
| 1750 | 5 | 0.2 | 5.10 | 6 | 214 | 0.7 | 5 | 0.77 | 0.3 | 43 | 23 | 32 | 99 | 5.61 | 0.40 | 15 | 28 | 2.01 | 1231 | 1 | 0.07 | 26 | 0.14 | 2 | 30 | 0.28 | 179 | 105 |
| 1400W-1800N | 10 | 0.2 | 4.30 | 51 | 216 | 0.2 | 5 | 0.72 | 0.3 | 36 | 23 | 28 | 107 | 6.07 | 0.29 | 12 | 19 | 1.77 | 1182 | 5 | 0.05 | 26 | 0.12 | 2 | 36 | 0.34 | 285 | 181 |
| 1400W-1850N | 5 | 0.2 | 4.43 | 5 | 185 | 0.2 | 5 | 0.33 | 0.3 | 30 | 20 | 18 | 95 | 6.16 | 0.35 | 11 | 23 | 1.87 | 1459 | 1 | 0.05 | 14 | 0.12 | 2 | 13 | 0.29 | 170 | 149 |
| 1900 | 30 | 0.2 | 3.81 | 6 | 338 | 0.2 | 5 | 0.52 | 0.2 | 31 | 11 | 13 | 47 | 4.37 | 0.50 | 10 | 21 | 1.14 | 1100 | 1 | 0.04 | 10 | 0.10 | 2 | 24 | 0.21 | 90 | 109 |
| 1950 | 25 | 0.2 | 4.42 | 8 | 438 | 0.2 | 5 | 1.06 | 0.4 | 36 | 21 | 23 | 131 | 5.89 | 0.54 | 10 | 27 | 2.16 | 1558 | 1 | 0.07 | 24 | 0.10 | 2 | 36 | 0.28 | 152 | 118 |
| 2000 | 10 | 0.2 | 5.30 | 11 | 215 | 0.7 | 5 | 0.62 | 0.5 | 53 | 23 | 76 | 118 | 6.07 | 0.51 | 22 | 25 | 1.74 | 1349 | 1 | 0.07 | 58 | 0.20 | 32 | 43 | 0.26 | 153 | 189 |
| 1400W-2050N | 10 | 0.2 | 5.33 | 7 | 289 | 0.7 | 5 | 1.36 | 0.2 | 49 | 23 | 25 | 124 | 6.34 | 0.50 | 18 | 28 | 2.17 | 1191 | 1 | 0.10 | 23 | 0.16 | 2 | 59 | 0.32 | 204 | 133 |
| 1400W-2100N | 10 | 0.2 | 5.23 | 7 | 357 | 0.4 | 5 | 1.60 | 0.2 | 44 | 23 | 27 | 152 | 6.42 | 0.60 | 15 | 29 | 2.20 | 1374 | 1 | 0.09 | 26 | 0.11 | 2 | 64 | 0.30 | 198 | 144 |
| 1450W-2100N | 10 | 0.2 | 6.86 | 9 | 437 | 0.5 | 5 | 0.66 | 0.3 | 31 | 27 | 52 | 199 | 6.87 | 1.10 | 16 | 36 | 2.51 | 1535 | 1 | 0.05 | 39 | 0.14 | 2 | 30 | 0.19 | 260 | 112 |
| 1500W-2150N | 10 | 0.2 | 6.57 | 7 | 192 | 0.4 | 5 | 1.88 | 0.2 | 35 | 35 | 70 | 139 | 6.40 | 0.28 | 13 | 39 | 3.88 | 1501 | 1 | 0.06 | 90 | 0.12 | 2 | 88 | 0.35 | 238 | 113 |
| 2200 | 15 | 0.2 | 5.98 | 9 | 324 | 0.6 | 5 | 1.00 | 0.4 | 44 | 27 | 42 | 230 | 6.11 | 0.62 | 18 | 44 | 2.32 | 2047 | 1 | 0.06 | 37 | 0.15 | 3 | 44 | 0.22 | 244 | 113 |
| 1500W-2250N | 5 | 0.2 | 4.80 | 3 | 302 | 0.4 | 5 | 0.68 | 0.2 | 31 | 31 | 89 | 156 | 6.51 | 0.20 | 12 | 35 | 2.94 | 1734 | 1 | 0.04 | 48 | 0.17 | 2 | 37 | 0.24 | 282 | 102 |
| 1500W-2300N | 5 | 0.2 | 6.02 | 3 | 216 | 0.3 | 5 | 1.63 | 0.3 | 36 | 34 | 55 | 114 | 6.58 | 0.41 | 12 | 49 | 3.70 | 1233 | 1 | 0.04 | 59 | 0.08 | 2 | 75 | 0.29 | 276 | 100 |
| 2350 | 10 | 0.2 | 4.68 | 11 | 475 | 1.5 | 5 | 1.11 | 0.2 | 70 | 21 | 30 | 135 | 5.84 | 0.58 | 30 | 41 | 1.80 | 1533 | 1 | 0.09 | 27 | 0.09 | 2 | 47 | 0.24 | 181 | 142 |
| 2400 | 15 | 0.2 | 5.44 | 7 | 244 | 0.4 | 5 | 0.79 | 0.2 | 37 | 29 | 60 | 160 | 6.14 | 0.51 | 13 | 36 | 2.56 | 1469 | 1 | 0.06 | 46 | 0.12 | 2 | 41 | 0.23 | 224 | 127 |
| 2450 | 10 | 0.2 | 6.15 | 4 | 462 | 0.3 | 5 | 1.05 | 0.2 | 33 | 33 | 52 | 146 | 6.76 | 0.28 | 11 | 56 | 3.33 | 1294 | 1 | 0.04 | 46 | 0.12 | 7 | 39 | 0.37 | 297 | 109 |
| 1500W-2500N | 10 | 0.2 | 5.08 | 10 | 396 | 0.3 | 5 | 0.98 | 0.4 | 32 | 28 | 74 | 121 | 5.96 | 0.42 | 11 | 47 | 2.88 | 1721 | 1 | 0.05 | 51 | 0.10 | 2 | 47 | 0.25 | 201 | 109 |

12/08 GP

| SAMPLE No. | As | Ag | Al | As | Ba | Be | Bi | Cu | Cd | Cr | Co | Cr | Cu | Fe | K | La | Li | Mg | Mn | Mo | Na | Ni | P | Pb | Sr | Ti | V | Zn | 6307-003 |
|-------------|-----|-----|------|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|-------|------|-----|-----|------|------|-----|------|-----|------|-----|-----|------|-----|-----|----------|
| | ppb | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | ppm | % | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm |
| 1500W-2550N | 30 | 0.2 | 6.68 | 7 | 407 | 0.5 | 5 | 0.79 | 0.3 | 38 | 35 | 47 | 260 | 6.61 | 0.72 | 14 | 49 | 3.14 | 2142 | 1 | 0.05 | 47 | 0.11 | 2 | 33 | 0.18 | 271 | 105 | |
| 2600 | 25 | 0.2 | 6.03 | 3 | 313 | 0.4 | 5 | 0.62 | 0.2 | 34 | 30 | 83 | 105 | 6.24 | 0.47 | 14 | 49 | 3.63 | 1022 | 1 | 0.04 | 66 | 0.10 | 2 | 29 | 0.26 | 258 | 103 | |
| 2650 | 10 | 0.2 | 5.66 | 6 | 284 | 0.4 | 5 | 0.79 | 0.3 | 35 | 31 | 61 | 183 | 6.34 | 0.46 | 13 | 49 | 3.53 | 1246 | 1 | 0.04 | 57 | 0.09 | 2 | 37 | 0.27 | 273 | 101 | |
| 2750 | 30 | 0.2 | 5.65 | 10 | 469 | 0.7 | 5 | 0.87 | 0.3 | 39 | 28 | 48 | 129 | 6.55 | 0.76 | 15 | 43 | 2.56 | 1666 | 1 | 0.07 | 50 | 0.11 | 9 | 39 | 0.24 | 243 | 119 | |
| 1500W-2800N | 70 | 0.2 | 4.58 | 10 | 397 | 0.3 | 5 | 0.86 | 0.2 | 33 | 28 | 46 | 120 | 5.93 | 0.48 | 12 | 35 | 2.29 | 1233 | 1 | 0.06 | 45 | 0.08 | 2 | 48 | 0.22 | 227 | 97 | |
| 1500W-2850N | 75 | 0.2 | 4.84 | 16 | 420 | 0.4 | 5 | 0.57 | 0.2 | 33 | 26 | 41 | 126 | 5.89 | 0.53 | 13 | 31 | 2.01 | 1206 | 1 | 0.05 | 40 | 0.07 | 5 | 35 | 0.21 | 210 | 107 | |
| 2900 | 25 | 0.2 | 5.80 | 24 | 638 | 0.9 | 5 | 0.33 | 0.2 | 37 | 26 | 60 | 42 | 4.99 | 1.46 | 16 | 27 | 1.57 | 1576 | 1 | 0.09 | 91 | 0.08 | 15 | 18 | 0.09 | 108 | 105 | |
| 2950 | 15 | 0.2 | 4.03 | 6 | 553 | 0.3 | 5 | 0.61 | 0.2 | 34 | 17 | 23 | 101 | 5.10 | 0.50 | 12 | 37 | 1.67 | 1294 | 1 | 0.04 | 22 | 0.08 | 2 | 64 | 0.25 | 177 | 92 | |
| 1500W-3000N | 25 | 0.2 | 4.47 | 3 | 497 | 0.3 | 5 | 1.01 | 0.2 | 38 | 25 | 28 | 141 | 5.88 | 0.62 | 13 | 45 | 2.37 | 1257 | 1 | 0.08 | 32 | 0.08 | 2 | 47 | 0.29 | 261 | 93 | |
| 1550W-3025N | 55 | 0.2 | 4.65 | 17 | 632 | 0.4 | 5 | 0.55 | 0.2 | 32 | 33 | 71 | 152 | 6.39 | 0.64 | 13 | 33 | 1.96 | 1365 | 1 | 0.06 | 58 | 0.10 | 6 | 22 | 0.19 | 236 | 117 | |
| 2100N-1500W | 5 | 0.2 | 6.83 | 2 | 273 | 0.3 | 5 | 0.08 | 0.2 | 19 | 28 | 18 | 92 | 6.15 | 0.57 | 7 | 47 | 2.90 | 1488 | 1 | 0.35 | 22 | 0.07 | 2 | 50 | 0.07 | 261 | 80 | |
| 1550 | 5 | 0.2 | 6.06 | 3 | 396 | 0.5 | 5 | 0.98 | 0.2 | 39 | 31 | 51 | 306 | 6.79 | 0.54 | 15 | 39 | 2.88 | 1648 | 1 | 0.06 | 44 | 0.13 | 2 | 33 | 0.28 | 298 | 118 | |
| 1600 | 5 | 0.2 | 6.40 | 2 | 601 | 0.6 | 5 | 0.32 | 0.2 | 30 | 40 | 139 | 166 | 7.42 | 0.78 | 13 | 80 | 3.19 | 2346 | 1 | 0.05 | 111 | 0.11 | 2 | 16 | 0.07 | 296 | 111 | |
| 1650 | 5 | 0.2 | 7.94 | 2 | 241 | 0.5 | 5 | 0.44 | 0.2 | 37 | 40 | 32 | 186 | 8.45 | 0.59 | 14 | 48 | 1.03 | 1694 | 1 | 0.05 | 58 | 0.10 | 2 | 63 | 0.12 | 375 | 111 | |
| 2100N-1700W | 10 | 0.2 | 5.72 | 2 | 194 | 0.3 | 5 | 1.42 | 0.2 | 36 | 31 | 46 | 216 | 6.63 | 0.15 | 11 | 37 | 3.10 | 1352 | 1 | 0.06 | 47 | 0.14 | 2 | 91 | 0.29 | 263 | 122 | |
| 2100N-1750W | 140 | 0.4 | 3.22 | 31 | 647 | 0.3 | 5 | 0.26 | 0.2 | 29 | 22 | 30 | 114 | 5.41 | 0.69 | 11 | 19 | 1.11 | 1281 | 1 | 0.06 | 23 | 0.08 | 2 | 16 | 0.15 | 205 | 88 | |
| 1800 | 15 | 0.2 | 4.16 | 11 | 250 | 0.2 | 5 | 1.05 | 0.3 | 35 | 27 | 35 | 192 | 5.74 | 0.14 | 11 | 27 | 2.33 | 1560 | 1 | 0.03 | 36 | 0.09 | 2 | 132 | 0.27 | 242 | 103 | |
| 1850 | 435 | 1.4 | 3.78 | 46 | 908 | 0.3 | 5 | 0.63 | 0.7 | 37 | 52 | 94 | 273 | 7.74 | 0.57 | 14 | 26 | 1.48 | 1523 | 2 | 0.10 | 80 | 0.09 | 10 | 35 | 0.21 | 252 | 135 | |
| 1900 | 340 | 1.4 | 4.08 | 20 | 582 | 0.4 | 5 | 0.65 | 0.5 | 36 | 36 | 73 | 190 | 7.62 | 0.77 | 13 | 23 | 1.54 | 1027 | 4 | 0.11 | 64 | 0.09 | 4 | 29 | 0.24 | 301 | 146 | |
| 2100N-1950W | 175 | 1.4 | 4.26 | 13 | 636 | 0.4 | 5 | 0.92 | 0.4 | 34 | 42 | 66 | 214 | 8.03 | 0.77 | 13 | 22 | 1.56 | 1430 | 1 | 0.19 | 68 | 0.09 | 3 | 37 | 0.26 | 259 | 139 | |
| 2100N-2050W | 240 | 0.2 | 5.44 | 7 | 653 | 0.4 | 5 | 0.70 | 0.2 | 29 | 33 | 39 | 196 | 7.17 | 0.77 | 13 | 28 | 2.11 | 1583 | 1 | 0.07 | 46 | 0.09 | 2 | 38 | 0.20 | 227 | 105 | |
| 2100 | 80 | 0.2 | 5.04 | 11 | 306 | 0.4 | 5 | 1.26 | 0.2 | 37 | 27 | 52 | 106 | 5.39 | 0.38 | 13 | 23 | 2.17 | 1179 | 1 | 0.08 | 47 | 0.08 | 2 | 64 | 0.21 | 188 | 82 | |
| 2150 | 40 | 0.2 | 5.30 | 10 | 329 | 0.3 | 5 | 0.97 | 0.2 | 35 | 29 | 37 | 115 | 6.39 | 0.44 | 13 | 32 | 2.39 | 1170 | 1 | 0.08 | 42 | 0.08 | 2 | 54 | 0.26 | 223 | 110 | |
| 2200 | 25 | 0.2 | 4.85 | 10 | 246 | 0.4 | 5 | 0.52 | 0.2 | 29 | 19 | 41 | 66 | 5.25 | 0.34 | 10 | 26 | 1.64 | 1034 | 1 | 0.04 | 28 | 0.13 | 2 | 37 | 0.21 | 200 | 95 | |
| 2100N-2300W | 215 | 0.4 | 4.46 | 25 | 566 | 0.7 | 5 | 0.40 | 0.3 | 31 | 30 | 57 | 130 | 6.96 | 0.81 | 13 | 25 | 1.51 | 1253 | 1 | 0.05 | 52 | 0.10 | 41 | 31 | 0.22 | 229 | 149 | |
| 2100N-2350W | 95 | 0.4 | 4.38 | 25 | 562 | 0.7 | 5 | 0.31 | 0.5 | 32 | 22 | 49 | 101 | 6.46 | 0.86 | 13 | 21 | 1.21 | 815 | 1 | 0.05 | 40 | 0.10 | 41 | 22 | 0.23 | 193 | 152 | |
| 2400 | 60 | 0.2 | 4.43 | 17 | 468 | 0.8 | 5 | 0.28 | 0.2 | 30 | 14 | 60 | 69 | 5.57 | 0.61 | 12 | 22 | 1.08 | 608 | 1 | 0.05 | 30 | 0.14 | 21 | 25 | 0.22 | 207 | 140 | |
| 2450 | 75 | 0.2 | 4.17 | 13 | 487 | 0.7 | 5 | 0.35 | 0.3 | 32 | 19 | 48 | 83 | 6.44 | 0.69 | 14 | 24 | 1.30 | 798 | 1 | 0.05 | 31 | 0.15 | 33 | 27 | 0.25 | 205 | 160 | |
| 2500 | 160 | 1.6 | 4.76 | 35 | 674 | 1.1 | 5 | 0.73 | 0.7 | 39 | 27 | 58 | 104 | 7.00 | 0.90 | 15 | 26 | 1.61 | 1674 | 3 | 0.06 | 51 | 0.13 | 84 | 37 | 0.25 | 200 | 216 | |
| 2100N-2550W | 35 | 0.2 | 4.62 | 18 | 436 | 0.3 | 5 | 0.86 | 0.3 | 31 | 29 | 44 | 120 | 5.76 | 0.53 | 12 | 30 | 2.12 | 1412 | 1 | 0.06 | 41 | 0.08 | 4 | 49 | 0.18 | 222 | 91 | |
| 2100N-2600W | 140 | 1.8 | 3.98 | 31 | 544 | 0.9 | 5 | 0.52 | 0.9 | 33 | 28 | 77 | 112 | 6.71 | 0.75 | 14 | 23 | 1.56 | 1532 | 2 | 0.05 | 59 | 0.12 | 102 | 27 | 0.25 | 194 | 198 | |
| 2600N-700E | 80 | 0.4 | 5.26 | 2 | 363 | 1.1 | 5 | 0.80 | 0.2 | 35 | 40 | 174 | 790 | 6.23 | 0.88 | 14 | 36 | 2.99 | 1235 | 4 | 0.27 | 209 | 0.16 | 2 | 81 | 0.08 | 136 | 113 | |
| 750 | 95 | 0.2 | 4.67 | 3 | 299 | 1.1 | 5 | 0.89 | 0.2 | 34 | 54 | 289 | 910 | 6.62 | 0.77 | 13 | 34 | 3.81 | 1376 | 4 | 0.19 | 305 | 0.18 | 2 | 101 | 0.08 | 133 | 96 | |
| 800 | 15 | 0.2 | 3.45 | 6 | 491 | 1.2 | 5 | 2.83 | 0.3 | 33 | 42 | 319 | 170 | 5.15 | 0.68 | 11 | 33 | 6.20 | 1065 | 1 | 0.07 | 419 | 0.17 | 2 | 89 | 0.11 | 65 | 77 | |
| 2600N-850E | 185 | 0.2 | 6.31 | 20 | 512 | 0.5 | 5 | 0.18 | 0.2 | 25 | 44 | 7 | 72 | 10.03 | 1.55 | 10 | 18 | 1.09 | 1538 | 14 | 0.26 | 11 | 0.17 | 2 | 42 | 0.05 | 129 | 122 | |
| 2600N-900E | 30 | 0.2 | 7.97 | 2 | 575 | 0.4 | 5 | 0.12 | 0.2 | 24 | 7 | 4 | 53 | 3.19 | 1.40 | 10 | 29 | 1.24 | 292 | 2 | 0.74 | 4 | 0.07 | 2 | 98 | 0.06 | 173 | 67 | |
| 950 | 145 | 0.2 | 7.23 | 32 | 490 | 0.5 | 5 | 0.27 | 1.0 | 34 | 57 | 11 | 275 | 8.30 | 1.01 | 11 | 31 | 1.54 | 3310 | 21 | 0.37 | 18 | 0.20 | 17 | 77 | 0.06 | 177 | 266 | |
| 1000 | 100 | 0.2 | 6.63 | 5 | 483 | 0.7 | 5 | 0.65 | 0.4 | 37 | 43 | 26 | 219 | 7.16 | 0.86 | 13 | 24 | 1.42 | 3294 | 16 | 0.19 | 38 | 0.23 | 15 | 71 | 0.15 | 165 | 210 | |
| 1050 | 90 | 0.4 | 6.41 | 2 | 451 | 0.6 | 5 | 1.37 | 0.2 | 38 | 40 | 19 | 246 | 6.09 | 0.82 | 11 | 21 | 1.66 | 2932 | 13 | 0.10 | 27 | 0.13 | 24 | 153 | 0.20 | 158 | 164 | |
| 2600N-1100E | 215 | 0.8 | 5.79 | 3 | 327 | 0.4 | 5 | 0.98 | 0.2 | 36 | 54 | 9 | 296 | 6.58 | 0.94 | 10 | 14 | 1.52 | 1744 | 17 | 0.06 | 14 | 0.13 | 7 | 63 | 0.20 | 163 | 146 | |
| 2600N-1150E | 10 | 0.2 | 5.28 | 2 | 180 | 0.3 | 5 | 0.44 | 0.2 | 30 | 10 | 23 | 66 | 7.80 | 0.42 | 11 | 10 | 1.71 | 627 | 13 | 0.04 | 10 | 0.17 | 2 | 49 | 0.21 | 185 | 78 | |
| 1200 | 75 | 0.2 | 4.52 | 10 | 179 | 0.4 | 5 | 1.16 | 0.2 | 35 | 16 | 20 | 142 | 7.88 | 0.49 | 11 | 13 | 1.55 | 718 | 6 | 0.05 | 11 | 0.15 | 2 | 95 | 0.25 | 183 | 107 | |
| 1250 | 100 | 0.2 | 5.14 | 2 | 283 | 0.3 | 5 | 0.91 | 0.2 | 35 | 25 | 13 | 126 | 7.63 | 0.74 | 11 | 13 | 1.67 | 1273 | 17 | 0.05 | 12 | 0.14 | 2 | 101 | 0.29 | 194 | 103 | |
| 1300 | 30 | 0.2 | 5.39 | 2 | 486 | 0.5 | 5 | 0.76 | 0.2 | 36 | 18 | 13 | 84 | 6.11 | 0.65 | 13 | 21 | 1.65 | 993 | 24 | 0.06 | 10 | 0.16 | 2 | 60 | 0.30 | 173 | 103 | |
| 2600N-1350E | 30 | 0.2 | 4.33 | 2 | 185 | 0.2 | 5 | 0.98 | 0.2 | 34 | 12 | 11 | 107 | 6.11 | 0.43 | 9 | 11 | 1.52 | 775 | 9 | 0.04 | 7 | 0.17 | 2 | 74 | 0.33 | 182 | 72 | |

Det

K10

| SAMPLE No. | Am ppb | Ag ppm | Al % | As ppm | Ba ppm | Be ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm | 8307-003 Pg. 3 of 7 |
|-------------|-----------|-----------|---------|-----------|-----------|-----------|-----------|---------|-----------|-----------|-----------|-----------|-----------|---------|--------|-----------|-----------|---------|-----------|-----------|---------|-----------|--------|-----------|-----------|---------|----------|-----------|------------------------|
| 2600N-1400E | 150 | 0.2 | 3.29 | 5 | 225 | 0.2 | 5 | 0.51 | 0.2 | 25 | 7 | 8 | 87 | 6.35 | 0.75 | 7 | 10 | 1.73 | 806 | 1 | 0.03 | 5 | 0.10 | 2 | 27 | 0.33 | 177 | 74 | 11 |
| 1450 | 105 | 0.2 | 5.98 | 2 | 699 | 0.6 | 5 | 0.88 | 0.2 | 43 | 33 | 18 | 188 | 5.97 | 1.00 | 16 | 19 | 1.63 | 1716 | 22 | 0.07 | 21 | 0.16 | 12 | 81 | 0.23 | 152 | 136 | |
| 1500 | 90 | 0.4 | 3.95 | 5 | 384 | 0.2 | 5 | 0.98 | 0.2 | 34 | 17 | 10 | 92 | 7.21 | 0.87 | 9 | 11 | 1.67 | 905 | 4 | 0.09 | 8 | 0.12 | 2 | 66 | 0.32 | 174 | 75 | |
| 1550 | 195 | 0.2 | 4.77 | 6 | 304 | 0.3 | 5 | 1.54 | 0.2 | 35 | 20 | 11 | 174 | 7.96 | 0.63 | 11 | 11 | 1.56 | 1036 | 5 | 0.07 | 9 | 0.15 | 2 | 118 | 0.29 | 167 | 85 | |
| 2600N-1600E | 105 | 0.2 | 5.21 | 3 | 342 | 0.3 | 5 | 1.23 | 0.2 | 33 | 15 | 15 | 194 | 5.78 | 0.50 | 11 | 12 | 1.49 | 869 | 3 | 0.06 | 10 | 0.13 | 2 | 68 | 0.26 | 157 | 114 | |
| 2600N-1650E | 75 | 0.2 | 5.53 | 7 | 324 | 0.4 | 5 | 1.17 | 0.3 | 29 | 27 | 15 | 293 | 5.33 | 0.58 | 10 | 20 | 2.40 | 1335 | 1 | 0.05 | 18 | 0.13 | 2 | 62 | 0.29 | 178 | 155 | |
| 1700 | 75 | 0.6 | 5.99 | 2 | 261 | 0.5 | 5 | 2.61 | 0.2 | 41 | 24 | 12 | 370 | 5.15 | 0.39 | 12 | 11 | 1.00 | 986 | 7 | 0.05 | 10 | 0.16 | 2 | 306 | 0.22 | 141 | 68 | |
| 1750 | 750 | 1.4 | 3.60 | 5 | 357 | 0.3 | 5 | 0.73 | 0.2 | 36 | 32 | 10 | 176 | 5.09 | 0.33 | 13 | 11 | 1.25 | 2184 | 6 | 0.06 | 10 | 0.12 | 9 | 156 | 0.16 | 101 | 68 | |
| 1800 | 80 | 0.4 | 4.40 | 2 | 418 | 0.3 | 5 | 1.02 | 0.2 | 34 | 16 | 13 | 121 | 5.21 | 0.55 | 10 | 11 | 1.38 | 1043 | 9 | 0.05 | 9 | 0.13 | 2 | 76 | 0.29 | 148 | 84 | |
| 2600N-1900E | 135 | 0.2 | 4.19 | 2 | 509 | 0.2 | 5 | 0.55 | 0.2 | 29 | 9 | 8 | 22 | 6.08 | 1.16 | 10 | 13 | 1.91 | 927 | 3 | 0.05 | 6 | 0.10 | 2 | 132 | 0.34 | 192 | 80 | |
| 2600N-2000E | 45 | 0.2 | 4.31 | 4 | 454 | 0.2 | 5 | 0.98 | 0.2 | 36 | 11 | 10 | 139 | 7.41 | 0.58 | 11 | 12 | 1.67 | 796 | 1 | 0.05 | 11 | 0.18 | 2 | 165 | 0.25 | 171 | 79 | |
| 2050 | 90 | 0.2 | 6.84 | 2 | 445 | 0.5 | 5 | 0.63 | 0.2 | 27 | 23 | 15 | 255 | 4.80 | 0.55 | 9 | 19 | 2.04 | 1768 | 1 | 0.05 | 15 | 0.17 | 2 | 75 | 0.23 | 145 | 125 | |
| 2100 | 570 | 0.6 | 4.90 | 6 | 425 | 0.4 | 5 | 1.76 | 0.2 | 42 | 30 | 44 | 264 | 5.83 | 0.74 | 12 | 18 | 1.74 | 1979 | 1 | 0.06 | 21 | 0.13 | 2 | 176 | 0.25 | 167 | 143 | |
| 2350 | 55 | 0.2 | 6.04 | 9 | 389 | 0.5 | 5 | 1.79 | 0.2 | 41 | 36 | 27 | 189 | 5.59 | 0.74 | 13 | 21 | 2.26 | 1782 | 1 | 0.06 | 49 | 0.15 | 2 | 155 | 0.28 | 150 | 133 | |
| 2600N-2500E | 40 | 0.2 | 5.92 | 4 | 475 | 0.6 | 5 | 0.93 | 0.2 | 28 | 29 | 43 | 203 | 5.09 | 0.53 | 11 | 21 | 2.34 | 1403 | 1 | 0.04 | 43 | 0.17 | 2 | 98 | 0.23 | 143 | 119 | |
| 2600N-2550E | 70 | 0.2 | 5.74 | 2 | 374 | 0.4 | 5 | 1.31 | 0.2 | 36 | 43 | 33 | 145 | 4.78 | 0.39 | 11 | 13 | 1.14 | 1063 | 1 | 0.05 | 34 | 0.15 | 2 | 184 | 0.20 | 122 | 87 | |
| 2600 | 30 | 0.2 | 6.17 | 2 | 456 | 0.5 | 5 | 0.88 | 0.2 | 35 | 20 | 28 | 144 | 5.12 | 0.53 | 12 | 15 | 1.21 | 825 | 2 | 0.10 | 24 | 0.23 | 2 | 132 | 0.18 | 113 | 79 | |
| 2650 | 45 | 0.2 | 5.88 | 2 | 500 | 0.5 | 5 | 1.16 | 0.2 | 41 | 22 | 27 | 172 | 5.92 | 0.65 | 14 | 17 | 1.28 | 986 | 1 | 0.12 | 22 | 0.19 | 3 | 123 | 0.22 | 139 | 87 | |
| 2600N-2700E | 50 | 0.4 | 6.40 | 3 | 520 | 0.5 | 5 | 1.25 | 0.2 | 38 | 24 | 35 | 157 | 5.87 | 0.64 | 12 | 20 | 1.26 | 861 | 1 | 0.17 | 21 | 0.20 | 3 | 144 | 0.18 | 152 | 80 | |
| 2600E-3250N | 50 | 0.4 | 5.34 | 5 | 231 | 0.4 | 5 | 2.52 | 0.2 | 38 | 40 | 24 | 302 | 5.87 | 0.54 | 11 | 19 | 2.20 | 1539 | 1 | 0.08 | 26 | 0.12 | 2 | 191 | 0.34 | 171 | 110 | 26 |
| 2600E-3300N | 100 | 0.2 | 4.98 | 12 | 193 | 0.4 | 5 | 2.79 | 0.2 | 36 | 40 | 28 | 315 | 6.10 | 0.49 | 11 | 18 | 2.15 | 1434 | 1 | 0.10 | 28 | 0.12 | 2 | 207 | 0.36 | 183 | 106 | |
| 3400 | 80 | 0.2 | 4.28 | 9 | 230 | 0.3 | 5 | 3.16 | 0.2 | 35 | 35 | 22 | 357 | 6.11 | 0.49 | 12 | 16 | 2.11 | 1264 | 1 | 0.16 | 27 | 0.11 | 2 | 191 | 0.38 | 188 | 121 | |
| 3500 | 360 | 0.6 | 4.27 | 14 | 174 | 0.3 | 5 | 3.66 | 0.2 | 32 | 34 | 26 | 387 | 6.47 | 0.42 | 11 | 14 | 1.88 | 1327 | 1 | 0.16 | 25 | 0.11 | 2 | 170 | 0.36 | 174 | 87 | |
| 2600E-3550N | 160 | 0.8 | 4.69 | 12 | 224 | 0.4 | 5 | 2.62 | 0.2 | 35 | 42 | 23 | 296 | 5.97 | 0.48 | 12 | 17 | 2.06 | 1174 | 1 | 0.11 | 26 | 0.11 | 2 | 195 | 0.35 | 166 | 89 | |
| 2700N-2700E | 5 | 0.2 | 4.56 | 5 | 152 | 0.6 | 5 | 2.41 | 0.3 | 40 | 22 | 72 | 48 | 3.96 | 0.30 | 13 | 22 | 2.36 | 1033 | 1 | 0.03 | 47 | 0.10 | 2 | 157 | 0.26 | 113 | 131 | 11 |
| 2700N-2800E | 10 | 0.2 | 6.29 | 2 | 275 | 0.7 | 5 | 3.46 | 0.2 | 32 | 12 | 13 | 78 | 2.96 | 0.63 | 9 | 14 | 1.27 | 924 | 1 | 0.03 | 16 | 0.13 | 2 | 235 | 0.19 | 117 | 61 | |
| 2850 | 40 | 0.2 | 4.51 | 4 | 256 | 0.5 | 5 | 1.45 | 0.2 | 39 | 16 | 42 | 113 | 4.39 | 0.30 | 11 | 15 | 1.49 | 881 | 1 | 0.05 | 26 | 0.20 | 2 | 118 | 0.28 | 135 | 87 | |
| 2900 | 30 | 0.4 | 4.80 | 50 | 301 | 0.6 | 5 | 1.74 | 0.5 | 48 | 28 | 55 | 185 | 5.16 | 0.50 | 16 | 18 | 1.68 | 1426 | 1 | 0.10 | 37 | 0.16 | 3 | 164 | 0.31 | 159 | 134 | |
| 2950 | 55 | 0.2 | 5.49 | 25 | 459 | 0.7 | 5 | 1.32 | 0.6 | 52 | 35 | 48 | 448 | 5.66 | 0.78 | 19 | 23 | 2.25 | 2957 | 1 | 0.06 | 42 | 0.16 | 12 | 114 | 0.30 | 177 | 138 | |
| 2700N-3000E | 35 | 0.2 | 5.43 | 5 | 238 | 0.6 | 5 | 1.83 | 0.2 | 39 | 22 | 62 | 174 | 5.09 | 0.40 | 12 | 19 | 2.05 | 1094 | 1 | 0.05 | 35 | 0.15 | 2 | 152 | 0.32 | 157 | 96 | |
| 2700N-3050E | 10 | 0.2 | 2.27 | 16 | 178 | 0.5 | 5 | 15.56 | 0.2 | 9 | 29 | 26 | 103 | 2.56 | 0.22 | 4 | 13 | 1.09 | 3292 | 2 | 0.09 | 22 | 0.09 | 2 | 133 | 0.16 | 151 | 68 | |
| 3150 | 95 | 1.0 | 5.50 | 104 | 489 | 0.6 | 5 | 1.55 | 2.5 | 46 | 66 | 50 | 213 | 4.91 | 0.93 | 18 | 20 | 1.68 | 1364 | 4 | 0.08 | 98 | 0.26 | 75 | 118 | 0.30 | 368 | 285 | |
| 3200 | 330 | 1.0 | 5.46 | 85 | 270 | 0.7 | 5 | 1.69 | 0.9 | 50 | 37 | 43 | 479 | 5.74 | 0.60 | 17 | 22 | 2.08 | 2150 | 1 | 0.05 | 38 | 0.17 | 66 | 144 | 0.31 | 182 | 162 | |
| 3250 | 35 | 0.4 | 5.17 | 20 | 256 | 0.9 | 5 | 1.48 | 0.5 | 56 | 20 | 44 | 181 | 4.91 | 0.50 | 20 | 22 | 1.80 | 1243 | 1 | 0.07 | 32 | 0.20 | 15 | 115 | 0.30 | 172 | 135 | |
| 2700N-3300E | 20 | 0.2 | 5.23 | 13 | 258 | 0.8 | 5 | 1.52 | 0.4 | 39 | 20 | 46 | 109 | 4.67 | 0.54 | 13 | 19 | 1.50 | 1528 | 1 | 0.04 | 28 | 0.28 | 16 | 130 | 0.30 | 163 | 113 | |
| 2700N-3350E | 90 | 0.4 | 5.29 | 14 | 249 | 0.6 | 5 | 2.31 | 0.4 | 43 | 21 | 47 | 207 | 5.03 | 0.58 | 14 | 18 | 1.79 | 1231 | 1 | 0.11 | 35 | 0.17 | 7 | 176 | 0.34 | 183 | 134 | |
| 3400 | 100 | 0.6 | 5.85 | 19 | 335 | 0.7 | 5 | 1.37 | 0.7 | 40 | 24 | 44 | 230 | 5.39 | 0.64 | 13 | 20 | 1.82 | 1981 | 1 | 0.05 | 36 | 0.21 | 6 | 106 | 0.33 | 175 | 184 | |
| 3450 | 75 | 0.2 | 5.86 | 3 | 302 | 0.7 | 5 | 1.79 | 0.2 | 41 | 26 | 45 | 313 | 5.79 | 0.71 | 12 | 22 | 2.29 | 1469 | 1 | 0.06 | 41 | 0.16 | 2 | 123 | 0.34 | 176 | 121 | |
| 3500 | 25 | 0.2 | 5.90 | 2 | 405 | 0.5 | 5 | 0.75 | 0.2 | 37 | 15 | 28 | 96 | 6.39 | 0.61 | 12 | 13 | 0.87 | 734 | 1 | 0.17 | 16 | 0.22 | 2 | 88 | 0.16 | 111 | 70 | |
| 2700N-3550E | 250 | 0.8 | 5.90 | 29 | 332 | 0.6 | 5 | 2.03 | 0.5 | 42 | 25 | 29 | 202 | 5.65 | 0.55 | 15 | 17 | 1.72 | 1238 | 1 | 0.14 | 31 | 0.17 | 4 | 208 | 0.36 | 179 | 134 | |
| 2700N-3600E | 45 | 0.2 | 5.88 | 23 | 266 | 0.6 | 5 | 1.23 | 0.6 | 35 | 22 | 39 | 115 | 5.14 | 0.58 | 13 | 23 | 1.79 | 1615 | 1 | 0.07 | 30 | 0.27 | 9 | 99 | 0.38 | 212 | 122 | |
| 3650 | 45 | 0.2 | 5.30 | 14 | 396 | 0.5 | 5 | 1.31 | 0.2 | 36 | 19 | 45 | 106 | 5.62 | 0.71 | 13 | 17 | 1.49 | 1000 | 1 | 0.06 | 25 | 0.22 | 3 | 105 | 0.25 | 157 | 77 | |
| 3700 | 30 | 0.2 | 5.01 | 16 | 312 | 0.6 | 5 | 1.57 | 0.4 | 35 | 26 | 37 | 136 | 4.97 | 0.53 | 11 | 15 | 1.37 | 1377 | 1 | 0.06 | 27 | 0.24 | 6 | 110 | 0.27 | 134 | 106 | |
| 3750 | 70 | 0.2 | 5.45 | 13 | 323 | 0.7 | 5 | 1.73 | 0.2 | 40 | 27 | 49 | 220 | 5.30 | 0.73 | 15 | 18 | 1.82 | 1549 | 1 | 0.06 | 33 | 0.17 | 7 | 130 | 0.27 | 154 | 128 | |
| 2700N-3850E | 60 | 0.2 | 5.01 | 11 | 321 | 0.7 | 5 | 1.54 | 0.2 | 39 | 25 | 43 | 165 | 4.70 | 0.43 | 12 | 18 | 1.79 | 1116 | 1 | 0.08 | 32 | 0.16 | 2 | 165 | 0.27 | 142 | 96 | |

| SAMPLE No. | Am ppb | Ag ppm | Al % | As ppm | Ba ppm | Be ppm | Bi ppm | Ca % | Cl ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm | 8307-003 Pg. 6 of 7 |
|-------------|-----------|-----------|---------|-----------|-----------|-----------|-----------|---------|-----------|-----------|-----------|-----------|-----------|---------|--------|-----------|-----------|---------|-----------|-----------|---------|-----------|--------|-----------|-----------|---------|----------|-----------|------------------------|
| 3200N-4650E | 30 | 0.2 | 3.66 | 3 | 168 | 0.3 | 5 | 0.68 | 0.2 | 25 | 6 | 28 | 37 | 2.99 | 0.23 | 9 | 7 | 0.61 | 284 | 1 | 0.05 | 9 | 0.20 | 2 | 53 | 0.27 | 108 | 39 | |
| 4700 | 30 | 0.2 | 5.18 | 2 | 575 | 0.5 | 5 | 1.10 | 0.2 | 39 | 19 | 34 | 139 | 4.93 | 0.59 | 17 | 20 | 1.66 | 1088 | 1 | 0.07 | 21 | 0.20 | 4 | 159 | 0.33 | 185 | 86 | |
| 4750 | 65 | 0.4 | 4.59 | 4 | 284 | 0.7 | 5 | 2.12 | 0.3 | 40 | 28 | 37 | 99 | 5.96 | 0.22 | 12 | 17 | 1.56 | 1943 | 1 | 0.06 | 20 | 0.29 | 2 | 233 | 0.40 | 229 | 91 | |
| 4800 | 130 | 0.4 | 4.15 | 4 | 214 | 0.4 | 5 | 1.42 | 0.2 | 38 | 16 | 44 | 112 | 4.52 | 0.35 | 12 | 18 | 1.27 | 833 | 1 | 0.06 | 22 | 0.18 | 2 | 135 | 0.29 | 158 | 126 | |
| 3200N-4900E | 20 | 0.4 | 4.11 | 3 | 233 | 0.4 | 5 | 2.50 | 0.2 | 42 | 15 | 11 | 77 | 3.97 | 0.40 | 12 | 11 | 1.13 | 1062 | 1 | 0.05 | 11 | 0.13 | 2 | 267 | 0.28 | 145 | 73 | |
| 3200N-4950E | 350 | 0.4 | 4.13 | 4 | 246 | 0.4 | 5 | 1.44 | 0.3 | 42 | 29 | 25 | 197 | 5.20 | 0.45 | 13 | 16 | 1.76 | 1798 | 8 | 0.06 | 24 | 0.15 | 6 | 147 | 0.27 | 192 | 112 | |
| 5000 | 10 | 0.6 | 5.39 | 2 | 149 | 0.4 | 5 | 2.60 | 0.2 | 43 | 35 | 12 | 279 | 6.40 | 0.17 | 11 | 7 | 0.68 | 1126 | 1 | 0.08 | 12 | 0.22 | 2 | 357 | 0.20 | 113 | 76 | |
| 3200N-5200E | 5 | 0.2 | 4.70 | 3 | 285 | 0.4 | 5 | 1.71 | 0.2 | 33 | 30 | 41 | 383 | 6.41 | 0.47 | 11 | 13 | 3.28 | 1484 | 1 | 0.04 | 45 | 0.13 | 2 | 126 | 0.48 | 287 | 98 | |
| 3300N-3400E | 390 | 0.6 | 5.12 | 3 | 247 | 0.4 | 5 | 2.64 | 0.2 | 34 | 74 | 65 | 326 | 6.56 | 0.30 | 12 | 20 | 2.91 | 1424 | 1 | 0.09 | 55 | 0.11 | 2 | 296 | 0.29 | 196 | 100 | |
| 3300N-3650E | 150 | 1.0 | 5.78 | 2 | 453 | 0.7 | 5 | 1.70 | 0.2 | 54 | 45 | 32 | 824 | 5.64 | 0.60 | 23 | 25 | 2.02 | 884 | 1 | 0.07 | 34 | 0.17 | 15 | 292 | 0.30 | 165 | 121 | |
| 3300N-4400E | 50 | 0.2 | 4.28 | 2 | 636 | 0.7 | 5 | 0.80 | 0.2 | 50 | 11 | 15 | 44 | 3.65 | 0.59 | 21 | 15 | 0.98 | 767 | 1 | 0.05 | 12 | 0.17 | 9 | 111 | 0.23 | 103 | 73 | |
| 4400 DUPT | 70 | 0.2 | 5.03 | 2 | 329 | 0.7 | 5 | 1.06 | 0.2 | 40 | 25 | 42 | 191 | 5.26 | 0.88 | 18 | 20 | 1.95 | 1302 | 1 | 0.07 | 24 | 0.15 | 3 | 103 | 0.20 | 179 | 85 | |
| 4450 | 220 | 0.2 | 5.07 | 5 | 333 | 0.6 | 5 | 1.71 | 0.2 | 39 | 27 | 51 | 134 | 4.50 | 0.27 | 12 | 15 | 1.36 | 1052 | 1 | 0.08 | 24 | 0.16 | 2 | 142 | 0.25 | 151 | 86 | |
| 4550 | 55 | 0.2 | 3.22 | 2 | 233 | 0.4 | 5 | 0.67 | 0.2 | 28 | 5 | 24 | 33 | 2.08 | 0.43 | 9 | 6 | 0.44 | 303 | 1 | 0.04 | 8 | 0.22 | 2 | 71 | 0.18 | 76 | 63 | |
| 3300N-4600E | 45 | 0.2 | 4.20 | 2 | 284 | 0.3 | 5 | 0.88 | 0.2 | 32 | 8 | 32 | 33 | 2.83 | 0.29 | 10 | 9 | 0.71 | 412 | 1 | 0.05 | 12 | 0.20 | 2 | 78 | 0.23 | 100 | 56 | |
| 3350N-550E | 15 | 0.2 | 6.04 | 32 | 199 | 0.4 | 5 | 2.42 | 0.2 | 37 | 48 | 36 | 240 | 6.39 | 0.30 | 10 | 21 | 2.28 | 1203 | 1 | 0.07 | 77 | 0.10 | 2 | 129 | 0.35 | 205 | 125 | |
| 600 | 30 | 0.2 | 6.27 | 11 | 239 | 0.6 | 5 | 1.98 | 0.2 | 38 | 28 | 59 | 215 | 5.82 | 0.64 | 11 | 25 | 2.00 | 1169 | 2 | 0.09 | 59 | 0.14 | 2 | 152 | 0.24 | 177 | 105 | |
| 650 | 25 | 0.2 | 6.29 | 8 | 235 | 0.6 | 5 | 2.12 | 0.2 | 36 | 28 | 39 | 168 | 5.36 | 0.63 | 11 | 21 | 1.78 | 1366 | 1 | 0.10 | 48 | 0.14 | 2 | 141 | 0.22 | 170 | 110 | |
| 700 | 70 | 0.6 | 7.91 | 20 | 327 | 0.6 | 5 | 1.93 | 0.5 | 35 | 56 | 11 | 449 | 6.09 | 0.99 | 11 | 23 | 2.12 | 1331 | 4 | 0.11 | 35 | 0.11 | 2 | 99 | 0.21 | 170 | 141 | |
| 3350N-750E | 220 | 0.4 | 5.92 | 6 | 373 | 0.5 | 5 | 0.18 | 0.2 | 25 | 13 | 20 | 486 | 5.76 | 1.22 | 12 | 28 | 0.97 | 432 | 28 | 0.21 | 17 | 0.15 | 5 | 38 | 0.08 | 155 | 74 | |
| 3350N-950E | 210 | 0.2 | 5.36 | 2 | 383 | 0.6 | 5 | 2.17 | 0.2 | 38 | 32 | 18 | 313 | 5.59 | 0.64 | 12 | 21 | 1.83 | 1162 | 1 | 0.10 | 24 | 0.12 | 2 | 146 | 0.26 | 160 | 92 | |
| 1000 | 30 | 0.4 | 5.80 | 2 | 442 | 0.5 | 5 | 2.18 | 0.2 | 37 | 34 | 15 | 235 | 5.58 | 0.68 | 11 | 20 | 1.96 | 1279 | 1 | 0.09 | 25 | 0.12 | 2 | 145 | 0.26 | 163 | 97 | |
| 1050 | 20 | 0.2 | 5.52 | 2 | 323 | 0.4 | 5 | 1.89 | 0.2 | 37 | 66 | 11 | 414 | 5.90 | 0.65 | 11 | 17 | 1.81 | 1548 | 1 | 0.07 | 20 | 0.12 | 2 | 135 | 0.27 | 162 | 91 | |
| 2450 | 880 | 1.0 | 3.97 | 13 | 237 | 0.5 | 5 | 4.31 | 0.2 | 37 | 124 | 28 | 1750 | 8.54 | 0.43 | 14 | 11 | 1.15 | 1932 | 10 | 0.07 | 46 | 0.22 | 2 | 167 | 0.27 | 151 | 109 | |
| 3350N-2500E | 320 | 0.8 | 3.96 | 7 | 209 | 0.4 | 5 | 4.86 | 0.2 | 36 | 61 | 34 | 784 | 8.38 | 0.49 | 12 | 12 | 1.36 | 1291 | 6 | 0.09 | 41 | 0.14 | 2 | 175 | 0.29 | 188 | 84 | |
| 3350N-2550E | 1120 | 1.0 | 4.14 | 2 | 246 | 0.4 | 5 | 2.80 | 0.2 | 35 | 33 | 49 | 272 | 5.70 | 0.65 | 11 | 14 | 1.78 | 1009 | 2 | 0.09 | 27 | 0.12 | 2 | 206 | 0.32 | 161 | 65 | |
| 2600 | 120 | 0.2 | 4.18 | 10 | 214 | 0.3 | 5 | 3.00 | 0.2 | 32 | 34 | 19 | 327 | 5.96 | 0.49 | 10 | 15 | 1.91 | 1178 | 1 | 0.13 | 27 | 0.11 | 2 | 205 | 0.36 | 179 | 87 | |
| 2650 | 60 | 0.4 | 4.80 | 2 | 214 | 0.4 | 5 | 2.77 | 0.2 | 31 | 46 | 18 | 306 | 6.13 | 0.51 | 10 | 16 | 2.13 | 1122 | 1 | 0.12 | 22 | 0.11 | 2 | 213 | 0.35 | 172 | 83 | |
| 2650 DUPT | 90 | 0.2 | 4.72 | 3 | 233 | 0.3 | 5 | 3.17 | 0.2 | 28 | 31 | 28 | 206 | 5.74 | 0.63 | 10 | 17 | 2.31 | 1149 | 1 | 0.16 | 31 | 0.10 | 2 | 191 | 0.38 | 175 | 80 | |
| 3350N-2700E | 30 | 0.2 | 4.51 | 2 | 216 | 0.4 | 5 | 2.57 | 0.2 | 33 | 37 | 17 | 171 | 5.85 | 0.53 | 13 | 15 | 1.90 | 1026 | 1 | 0.11 | 18 | 0.11 | 2 | 222 | 0.34 | 164 | 84 | |
| 3350N-2750E | 110 | 0.4 | 4.40 | 4 | 141 | 0.5 | 5 | 3.03 | 0.2 | 35 | 48 | 20 | 361 | 6.85 | 0.34 | 11 | 14 | 1.82 | 983 | 1 | 0.13 | 21 | 0.11 | 2 | 223 | 0.40 | 206 | 63 | |
| 2800 | 225 | 0.2 | 4.72 | 3 | 162 | 0.3 | 5 | 2.55 | 0.2 | 35 | 63 | 19 | 287 | 7.07 | 0.49 | 9 | 17 | 1.99 | 1014 | 1 | 0.08 | 24 | 0.11 | 2 | 201 | 0.37 | 200 | 64 | |
| 2850 | 160 | 0.2 | 5.91 | 2 | 120 | 0.4 | 5 | 2.87 | 0.2 | 35 | 66 | 31 | 244 | 6.83 | 0.44 | 10 | 19 | 2.57 | 1063 | 1 | 0.08 | 42 | 0.12 | 2 | 206 | 0.31 | 197 | 61 | |
| 3000 | 200 | 0.4 | 5.88 | 2 | 176 | 0.5 | 5 | 2.41 | 0.2 | 36 | 61 | 20 | 656 | 7.04 | 0.38 | 11 | 21 | 2.46 | 1079 | 1 | 0.08 | 32 | 0.15 | 2 | 199 | 0.34 | 199 | 65 | |
| 3350N-3050E | 40 | 0.2 | 6.39 | 2 | 84 | 0.5 | 5 | 3.43 | 0.2 | 32 | 88 | 15 | 623 | 6.71 | 0.25 | 10 | 21 | 2.28 | 896 | 1 | 0.08 | 34 | 0.11 | 2 | 223 | 0.36 | 182 | 58 | |
| 3350N-3100E | 100 | 0.2 | 5.73 | 2 | 307 | 0.4 | 5 | 3.20 | 0.2 | 34 | 30 | 13 | 313 | 5.46 | 0.25 | 10 | 16 | 2.06 | 730 | 1 | 0.10 | 19 | 0.11 | 2 | 223 | 0.40 | 181 | 53 | |
| 3150 | 930 | 0.8 | 5.24 | 2 | 174 | 0.4 | 5 | 2.95 | 0.2 | 36 | 41 | 23 | 382 | 6.03 | 0.36 | 10 | 18 | 2.33 | 890 | 1 | 0.10 | 25 | 0.10 | 6 | 250 | 0.37 | 210 | 62 | |
| 3200 | 230 | 0.6 | 4.59 | 2 | 189 | 0.5 | 5 | 2.83 | 0.2 | 42 | 39 | 21 | 345 | 5.47 | 0.38 | 13 | 17 | 1.92 | 864 | 1 | 0.10 | 22 | 0.11 | 2 | 283 | 0.32 | 167 | 63 | |
| 3250 | 390 | 0.6 | 4.72 | 2 | 327 | 0.4 | 5 | 2.36 | 0.2 | 41 | 47 | 24 | 806 | 5.72 | 0.57 | 12 | 17 | 2.09 | 1096 | 1 | 0.08 | 23 | 0.10 | 2 | 200 | 0.29 | 180 | 61 | |
| 3350N-3300E | 180 | 0.2 | 4.13 | 2 | 128 | 0.4 | 5 | 2.59 | 0.2 | 45 | 26 | 11 | 256 | 5.57 | 0.40 | 12 | 17 | 1.68 | 830 | 1 | 0.07 | 9 | 0.16 | 2 | 213 | 0.38 | 182 | 56 | |
| 3350N-3350E | 150 | 0.2 | 4.31 | 7 | 185 | 0.5 | 5 | 2.77 | 0.2 | 43 | 41 | 24 | 268 | 5.95 | 0.35 | 14 | 18 | 1.88 | 901 | 1 | 0.09 | 20 | 0.12 | 2 | 208 | 0.35 | 200 | 62 | |
| 3400 | 190 | 0.2 | 4.85 | 5 | 241 | 0.5 | 5 | 2.25 | 0.2 | 39 | 76 | 61 | 309 | 6.21 | 0.34 | 12 | 21 | 2.85 | 1555 | 1 | 0.08 | 53 | 0.10 | 2 | 254 | 0.26 | 180 | 93 | |
| 3450 | 30 | 0.2 | 5.32 | 2 | 372 | 0.6 | 5 | 3.04 | 0.2 | 43 | 22 | 11 | 159 | 3.86 | 0.53 | 14 | 15 | 1.65 | 680 | 1 | 0.08 | 16 | 0.10 | 2 | 251 | 0.22 | 125 | 62 | |
| 3500 | 50 | 0.2 | 4.39 | 5 | 253 | 0.5 | 5 | 2.26 | 0.2 | 54 | 32 | 15 | 247 | 4.56 | 0.50 | 19 | 15 | 1.42 | 895 | 1 | 0.06 | 17 | 0.12 | 32 | 341 | 0.24 | 137 | 90 | |
| 3350N-3600E | 250 | 0.4 | 5.62 | 7 | 499 | 1.0 | 5 | 2.01 | 0.2 | 70 | 35 | 20 | 244 | 4.97 | 0.81 | 31 | 32 | 1.97 | 1080 | 1 | 0.05 | 25 | 0.13 | 18 | 388 | 0.33 | 151 | 103 | |

| SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Bc ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm | 9307-003 Pg. 6 of 7 |
|-------------|--------|--------|------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|-------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|---------------------|
| 3350N-3650E | 20 | 0.2 | 2.48 | 3 | 226 | 0.4 | 5 | 0.90 | 0.2 | 41 | 11 | 13 | 30 | 2.78 | 0.41 | 13 | 13 | 0.90 | 802 | 1 | 0.05 | 11 | 0.07 | 2 | 121 | 0.20 | 84 | 62 | |
| 3400E-3250N | 230 | 0.2 | 5.07 | 11 | 268 | 0.5 | 5 | 2.46 | 0.2 | 40 | 80 | 63 | 318 | 6.48 | 0.33 | 13 | 21 | 2.86 | 1491 | 1 | 0.09 | 53 | 0.10 | 2 | 279 | 0.26 | 188 | 97 | |
| 3450N-2450E | 1130 | 1.2 | 3.89 | 18 | 333 | 0.5 | 5 | 1.92 | 0.2 | 45 | 122 | 28 | 1364 | 12.75 | 0.59 | 22 | 12 | 1.22 | 1094 | 21 | 0.06 | 33 | 0.19 | 2 | 132 | 0.28 | 176 | 75 | |
| 3550N-2450E | 140 | 0.2 | 5.28 | 6 | 397 | 0.8 | 5 | 2.59 | 0.2 | 43 | 374 | 20 | 859 | 7.28 | 0.53 | 17 | 21 | 1.81 | 2115 | 2 | 0.06 | 48 | 0.15 | 2 | 169 | 0.26 | 152 | 84 | |
| 3550N-2500E | 670 | 0.8 | 4.22 | 14 | 278 | 0.5 | 5 | 2.71 | 0.4 | 41 | 99 | 49 | 1388 | 8.79 | 0.54 | 17 | 14 | 1.55 | 1778 | 9 | 0.07 | 47 | 0.18 | 5 | 141 | 0.28 | 164 | 107 | |
| 3550N-2550E | 130 | 0.2 | 3.88 | 6 | 235 | 0.5 | 5 | 2.77 | 0.2 | 40 | 27 | 32 | 228 | 5.36 | 0.62 | 13 | 16 | 1.83 | 1013 | 2 | 0.11 | 24 | 0.12 | 2 | 156 | 0.33 | 171 | 70 | |
| 2700 | 130 | 0.2 | 4.30 | 2 | 160 | 0.3 | 5 | 2.98 | 0.2 | 34 | 47 | 22 | 446 | 6.50 | 0.43 | 10 | 15 | 2.00 | 1038 | 1 | 0.14 | 22 | 0.10 | 2 | 210 | 0.40 | 202 | 61 | |
| 2750 | 320 | 0.6 | 5.31 | 2 | 138 | 0.4 | 5 | 2.89 | 0.2 | 36 | 49 | 22 | 250 | 6.65 | 0.48 | 11 | 18 | 2.17 | 1121 | 1 | 0.08 | 28 | 0.11 | 5 | 213 | 0.34 | 209 | 79 | |
| 3550N-2850E | 130 | 0.2 | 5.04 | 2 | 234 | 0.4 | 5 | 1.65 | 0.2 | 40 | 54 | 20 | 869 | 7.75 | 0.42 | 12 | 18 | 1.88 | 844 | 4 | 0.06 | 24 | 0.19 | 2 | 241 | 0.33 | 179 | 55 | |
| 4450N-4350E | 25 | 0.2 | 4.30 | 2 | 811 | 0.4 | 5 | 1.70 | 0.2 | 35 | 23 | 25 | 166 | 4.38 | 0.22 | 9 | 14 | 2.00 | 832 | 1 | 0.08 | 27 | 0.20 | 2 | 205 | 0.30 | 124 | 78 | |
| 4450N-4400E | 10 | 0.4 | 2.74 | 2 | 183 | 0.3 | 5 | 1.19 | 0.2 | 26 | 28 | 20 | 182 | 4.39 | 0.21 | 7 | 11 | 1.49 | 816 | 1 | 0.09 | 15 | 0.15 | 2 | 48 | 0.36 | 141 | 82 | |
| 4450 | 15 | 0.6 | 2.41 | 2 | 131 | 0.2 | 5 | 0.79 | 0.2 | 25 | 9 | 23 | 66 | 3.31 | 0.24 | 8 | 6 | 0.83 | 347 | 1 | 0.06 | 11 | 0.13 | 2 | 57 | 0.40 | 126 | 43 | |
| 4500 | 75 | 0.2 | 3.15 | 2 | 228 | 0.4 | 5 | 1.38 | 0.2 | 43 | 13 | 23 | 77 | 4.18 | 0.30 | 16 | 11 | 1.12 | 602 | 1 | 0.08 | 15 | 0.14 | 2 | 142 | 0.29 | 121 | 73 | |
| 4550 | 90 | 0.2 | 5.91 | 2 | 171 | 0.6 | 5 | 2.90 | 0.2 | 33 | 73 | 62 | 233 | 7.56 | 0.24 | 12 | 18 | 2.64 | 1383 | 1 | 0.07 | 79 | 0.16 | 2 | 366 | 0.36 | 209 | 111 | |
| 4450N-4600E | 160 | 0.4 | 5.61 | 2 | 120 | 0.5 | 5 | 3.56 | 0.2 | 28 | 53 | 57 | 187 | 8.17 | 0.13 | 10 | 12 | 1.99 | 865 | 1 | 0.08 | 69 | 0.19 | 2 | 471 | 0.35 | 215 | 79 | |
| 4450N-4650E | 110 | 0.2 | 5.52 | 2 | 88 | 0.8 | 5 | 4.65 | 0.2 | 28 | 81 | 72 | 172 | 6.84 | 0.11 | 9 | 11 | 1.72 | 1014 | 1 | 0.07 | 72 | 0.12 | 2 | 646 | 0.30 | 215 | 77 | |
| 4450N-4750E | 10 | 0.2 | 6.74 | 2 | 280 | 0.6 | 5 | 1.56 | 0.2 | 36 | 50 | 62 | 526 | 7.82 | 0.28 | 13 | 33 | 4.72 | 2371 | 2 | 0.03 | 67 | 0.12 | 2 | 131 | 0.40 | 257 | 97 | |
| 4600N-4400E | 45 | 0.2 | 4.67 | 2 | 455 | 0.4 | 5 | 2.90 | 0.2 | 31 | 37 | 29 | 192 | 5.65 | 0.28 | 9 | 14 | 2.17 | 1084 | 1 | 0.11 | 28 | 0.16 | 6 | 235 | 0.30 | 171 | 86 | |
| 4450 | 150 | 0.2 | 4.00 | 2 | 154 | 0.5 | 5 | 3.07 | 0.2 | 33 | 57 | 51 | 231 | 6.66 | 0.18 | 10 | 9 | 1.77 | 1803 | 7 | 0.10 | 36 | 0.12 | 2 | 335 | 0.33 | 167 | 64 | |
| 4600N-4500E | 30 | 0.2 | 5.71 | 2 | 81 | 0.6 | 5 | 3.71 | 0.2 | 27 | 71 | 49 | 396 | 6.70 | 0.13 | 8 | 18 | 3.29 | 1430 | 1 | 0.10 | 84 | 0.13 | 2 | 385 | 0.38 | 196 | 87 | |
| 4600N-4550E | 150 | 0.2 | 5.38 | 2 | 103 | 0.6 | 5 | 3.81 | 0.2 | 30 | 38 | 29 | 162 | 6.58 | 0.16 | 10 | 15 | 2.64 | 2075 | 2 | 0.06 | 36 | 0.10 | 2 | 451 | 0.42 | 233 | 74 | |
| 4600N-4600E | 145 | 0.2 | 5.32 | 2 | 94 | 0.6 | 5 | 4.31 | 0.2 | 27 | 41 | 31 | 162 | 6.63 | 0.14 | 9 | 14 | 2.57 | 2407 | 2 | 0.08 | 36 | 0.09 | 2 | 430 | 0.40 | 233 | 78 | |
| 4650E-3000N | 35 | 0.2 | 4.63 | 2 | 355 | 0.3 | 5 | 1.32 | 0.2 | 33 | 9 | 31 | 40 | 4.43 | 0.53 | 10 | 11 | 1.15 | 726 | 1 | 0.07 | 16 | 0.16 | 2 | 109 | 0.30 | 152 | 87 | |
| 3050 | 85 | 0.2 | 4.85 | 6 | 299 | 0.7 | 5 | 1.50 | 0.2 | 42 | 20 | 43 | 138 | 4.78 | 0.47 | 15 | 18 | 1.60 | 993 | 1 | 0.07 | 29 | 0.17 | 2 | 106 | 0.30 | 158 | 99 | |
| 4650E-3100N | 65 | 0.2 | 5.53 | 9 | 361 | 0.5 | 5 | 1.58 | 0.2 | 43 | 21 | 59 | 122 | 5.43 | 0.54 | 15 | 16 | 1.56 | 952 | 1 | 0.09 | 29 | 0.19 | 2 | 134 | 0.29 | 155 | 101 | |
| 4650E-3150N | 60 | 0.2 | 4.53 | 4 | 469 | 0.5 | 5 | 1.28 | 0.2 | 42 | 15 | 36 | 91 | 4.38 | 0.47 | 14 | 14 | 1.39 | 825 | 1 | 0.07 | 22 | 0.14 | 2 | 102 | 0.26 | 141 | 81 | |
| 3250 | 80 | 0.2 | 5.52 | 105 | 573 | 0.6 | 5 | 1.73 | 0.2 | 43 | 27 | 52 | 136 | 5.81 | 0.62 | 15 | 18 | 1.83 | 1133 | 1 | 0.10 | 37 | 0.16 | 2 | 148 | 0.27 | 156 | 98 | |
| 3350 | 35 | 0.2 | 2.94 | 3 | 311 | 0.5 | 5 | 1.09 | 0.2 | 42 | 17 | 19 | 73 | 3.28 | 0.30 | 13 | 11 | 0.76 | 1303 | 1 | 0.05 | 9 | 0.22 | 2 | 334 | 0.20 | 99 | 67 | |
| 3400 | 30 | 0.2 | 4.63 | 3 | 444 | 1.2 | 5 | 0.81 | 0.2 | 61 | 52 | 26 | 622 | 5.25 | 0.52 | 31 | 24 | 1.09 | 1780 | 3 | 0.05 | 37 | 0.20 | 2 | 126 | 0.21 | 117 | 102 | |
| 4650E-3500N | 20 | 0.2 | 3.31 | 4 | 380 | 0.9 | 5 | 1.38 | 0.2 | 41 | 11 | 21 | 46 | 3.26 | 0.40 | 16 | 11 | 0.66 | 1471 | 2 | 0.05 | 10 | 0.48 | 8 | 323 | 0.22 | 105 | 69 | |
| 4650E-3550N | 20 | 0.2 | 3.72 | 8 | 234 | 1.5 | 5 | 0.55 | 0.2 | 72 | 7 | 24 | 33 | 4.29 | 0.30 | 37 | 14 | 0.55 | 461 | 1 | 0.13 | 12 | 0.14 | 6 | 108 | 0.25 | 78 | 97 | |
| 3600 | 30 | 0.2 | 3.97 | 3 | 387 | 0.8 | 5 | 0.95 | 0.2 | 38 | 13 | 29 | 57 | 4.19 | 0.55 | 15 | 14 | 1.01 | 1250 | 1 | 0.05 | 15 | 0.22 | 5 | 153 | 0.27 | 135 | 80 | |
| 3650 | 10 | 0.2 | 5.17 | 4 | 682 | 1.0 | 5 | 0.95 | 0.2 | 60 | 16 | 26 | 90 | 4.59 | 0.93 | 31 | 19 | 1.57 | 1818 | 1 | 0.05 | 21 | 0.19 | 11 | 389 | 0.26 | 141 | 120 | |
| 3700 | 10 | 0.2 | 4.49 | 4 | 248 | 0.9 | 5 | 0.88 | 0.2 | 58 | 10 | 29 | 44 | 3.69 | 0.44 | 27 | 15 | 0.80 | 524 | 1 | 0.07 | 15 | 0.22 | 4 | 175 | 0.22 | 111 | 84 | |
| 4650E-3750N | 10 | 0.2 | 2.76 | 2 | 388 | 0.2 | 5 | 0.59 | 0.2 | 21 | 11 | 5 | 162 | 5.51 | 0.61 | 7 | 9 | 1.75 | 596 | 1 | 0.03 | 4 | 0.17 | 2 | 302 | 0.41 | 200 | 63 | |
| 4650E-3800N | 15 | 0.2 | 3.64 | 4 | 305 | 0.4 | 5 | 1.55 | 0.2 | 41 | 13 | 27 | 124 | 4.38 | 0.46 | 13 | 12 | 1.37 | 627 | 1 | 0.10 | 19 | 0.16 | 2 | 174 | 0.32 | 145 | 73 | |
| 3850 | 260 | 0.2 | 5.80 | 2 | 503 | 1.4 | 5 | 1.29 | 0.2 | 44 | 83 | 25 | 1609 | 7.67 | 0.45 | 15 | 25 | 1.91 | 1611 | 2 | 0.05 | 29 | 0.19 | 6 | 564 | 0.33 | 203 | 78 | |
| 3900 | 35 | 0.2 | 4.51 | 2 | 859 | 0.8 | 5 | 1.16 | 0.2 | 63 | 15 | 23 | 116 | 4.40 | 0.62 | 27 | 21 | 1.21 | 932 | 1 | 0.07 | 19 | 0.15 | 10 | 213 | 0.28 | 131 | 96 | |
| 3950 | 10 | 0.2 | 4.40 | 2 | 241 | 0.4 | 5 | 2.26 | 0.2 | 40 | 16 | 25 | 126 | 4.98 | 0.49 | 13 | 15 | 1.65 | 662 | 1 | 0.12 | 21 | 0.15 | 2 | 159 | 0.35 | 172 | 87 | |
| 4650E-4000N | 10 | 0.2 | 4.68 | 2 | 160 | 0.4 | 5 | 3.22 | 0.2 | 37 | 24 | 18 | 283 | 5.58 | 0.27 | 12 | 11 | 1.50 | 613 | 1 | 0.11 | 17 | 0.18 | 2 | 240 | 0.41 | 201 | 60 | |
| 4650E-4050N | 10 | 0.2 | 4.68 | 2 | 207 | 0.3 | 5 | 2.53 | 0.2 | 33 | 21 | 25 | 272 | 5.07 | 0.25 | 10 | 11 | 1.72 | 582 | 2 | 0.10 | 22 | 0.16 | 2 | 190 | 0.40 | 158 | 59 | |
| 4100 | 10 | 0.2 | 4.44 | 2 | 252 | 0.5 | 5 | 2.73 | 0.2 | 40 | 18 | 26 | 140 | 4.67 | 0.36 | 14 | 12 | 1.60 | 653 | 1 | 0.11 | 20 | 0.14 | 2 | 288 | 0.36 | 162 | 71 | |
| 4150 | 95 | 0.2 | 5.08 | 3 | 286 | 0.6 | 5 | 3.21 | 0.2 | 37 | 37 | 28 | 258 | 5.22 | 0.30 | 13 | 12 | 1.58 | 783 | 1 | 0.10 | 27 | 0.14 | 2 | 433 | 0.32 | 171 | 72 | |
| 4200 | 15 | 0.2 | 6.36 | 2 | 302 | 1.0 | 5 | 1.44 | 0.2 | 51 | 57 | 26 | 705 | 7.48 | 0.80 | 19 | 21 | 2.81 | 2168 | 1 | 0.06 | 31 | 0.14 | 7 | 176 | 0.39 | 361 | 97 | |
| 4650E-4250N | 30 | 0.6 | 5.30 | 2 | 351 | 0.5 | 5 | 3.34 | 0.2 | 37 | 62 | 27 | 383 | 5.99 | 0.27 | 10 | 13 | 1.95 | 1119 | 1 | 0.13 | 32 | 0.13 | 2 | 360 | 0.35 | 184 | 134 | |

| SAMPLE No. | Au | Ag | Al | As | Ba | Be | Bi | Ca | Cd | Ce | Co | Cr | Cu | Fe | K | La | Li | Mg | Mn | Mo | Na | Ni | P | Pb | Sr | Ti | V | Zn | 9307-003 Pg. 7 of 7 |
|-------------|-----|-----|------|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|------|------|-----|-----|------|------|-----|------|-----|------|-----|-----|------|-----|-----|------------------------|
| | ppb | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | ppm | % | ppm | % | ppm | ppm | % | ppm | ppm | |
| 4650E-4600N | 15 | 0.2 | 6.19 | 2 | 61 | 0.7 | 5 | 3.41 | 0.2 | 34 | 41 | 45 | 193 | 7.61 | 0.16 | 10 | 28 | 4.17 | 1398 | 1 | 0.05 | 47 | 0.09 | 2 | 430 | 0.51 | 285 | 106 | |
| 4700E-4300N | 15 | 0.2 | 4.46 | 4 | 155 | 0.4 | 5 | 3.28 | 0.2 | 32 | 33 | 25 | 307 | 5.38 | 0.24 | 10 | 11 | 1.66 | 781 | 1 | 0.10 | 31 | 0.14 | 2 | 399 | 0.32 | 176 | 72 | |
| 4350 | 60 | 0.4 | 5.51 | 2 | 124 | 0.6 | 5 | 5.11 | 0.2 | 20 | 76 | 24 | 726 | 7.42 | 0.18 | 9 | 10 | 1.69 | 1059 | 1 | 0.09 | 41 | 0.11 | 2 | 610 | 0.34 | 209 | 65 | |
| 4400 | 40 | 0.2 | 6.01 | 2 | 116 | 0.6 | 5 | 3.92 | 0.2 | 27 | 38 | 32 | 487 | 7.65 | 0.27 | 11 | 18 | 2.85 | 1262 | 1 | 0.05 | 38 | 0.12 | 2 | 472 | 0.35 | 231 | 84 | |
| 4700E-4450N | 35 | 0.2 | 4.94 | 2 | 60 | 0.5 | 5 | 4.20 | 0.2 | 24 | 35 | 49 | 193 | 6.35 | 0.10 | 9 | 12 | 2.37 | 887 | 1 | 0.07 | 53 | 0.10 | 2 | 529 | 0.29 | 205 | 76 | |
| 4700E-4500N | 30 | 0.2 | 6.10 | 2 | 84 | 0.8 | 5 | 5.15 | 0.2 | 15 | 62 | 53 | 696 | 5.67 | 0.12 | 7 | 11 | 2.14 | 1056 | 1 | 0.10 | 65 | 0.11 | 2 | 567 | 0.30 | 192 | 69 | |
| 4550 | 5 | 0.2 | 5.46 | 2 | 128 | 0.6 | 5 | 2.58 | 0.2 | 27 | 36 | 51 | 123 | 6.32 | 0.42 | 11 | 31 | 3.44 | 1405 | 1 | 0.04 | 37 | 0.11 | 2 | 149 | 0.42 | 228 | 95 | |
| 4700E-4600N | 5 | 0.2 | 6.40 | 2 | 158 | 0.6 | 5 | 1.80 | 0.2 | 26 | 32 | 37 | 181 | 6.37 | 0.76 | 10 | 28 | 3.26 | 1577 | 1 | 0.03 | 35 | 0.09 | 2 | 107 | 0.56 | 276 | 96 | |
| 4800N-4250E | 5 | 0.2 | 4.90 | 2 | 478 | 0.8 | 5 | 1.62 | 0.2 | 40 | 20 | 27 | 111 | 4.43 | 0.44 | 15 | 20 | 1.90 | 809 | 1 | 0.09 | 22 | 0.14 | 2 | 139 | 0.28 | 136 | 76 | |
| 4800N-4300E | 10 | 0.4 | 3.84 | 2 | 256 | 0.4 | 5 | 1.17 | 0.2 | 30 | 18 | 27 | 245 | 4.12 | 0.26 | 10 | 13 | 1.41 | 625 | 4 | 0.07 | 20 | 0.20 | 2 | 120 | 0.29 | 126 | 74 | |
| 4800N-4350E | 10 | 0.4 | 4.03 | 2 | 387 | 0.3 | 5 | 1.96 | 0.2 | 35 | 31 | 24 | 365 | 6.01 | 0.41 | 11 | 12 | 1.90 | 712 | 6 | 0.09 | 23 | 0.14 | 2 | 202 | 0.36 | 171 | 69 | |
| 4800N-4450E | 20 | 0.2 | 4.45 | 2 | 211 | 0.3 | 5 | 2.88 | 0.2 | 31 | 47 | 26 | 443 | 6.91 | 0.25 | 9 | 9 | 1.77 | 863 | 17 | 0.11 | 24 | 0.14 | 2 | 251 | 0.39 | 188 | 68 | |

NORANDA DELTA LABORATORY

Geochemical Analysis

Project Name & No.: KLIYUL (DARB LK.) - 148
 Material: 187 Soils & 52 Rx
 Remarks: * Sample screened @ -35 MESH (0.5 mm)
 ■ Organic, & Humus, S Sulfide

Geol.: R.W.
 Sheet: 1 of 6

Date received: JULY 28
 Date completed: AUG. 06

LAB CODE: 9308-001

Au - 10.0 g sample digested with aqua-regia and determined by A.A. (D.L. 5 PPB)
 ICP - 0.2 g sample digested with 3 ml HClO₄/HNO₃ (4:1) at 203 °C for 4 hours diluted to 10 ml with water. Looman PS3000 ICP determined elemental contents.
 N.B. The major oxide elements and Ba, Be, Ce, La, Li, Ga are rarely dissolved completely from geological materials with this acid dissolution method.

| T.T. No. | SAMPLE No. | Au | Ag | Al | As | Ba | Be | Bi | Ca | Cd | Ce | Co | Cr | Cu | Fe | K | La | Li | Mg | Mn | Mo | Na | Ni | P | Pb | Sr | Ti | V | Zn |
|----------|-------------|-----|-----|------|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|------|------|-----|-----|------|------|-----|------|----|------|-----|-----|------|-----|-----|
| | | ppb | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | ppm | ppm | % | ppm | ppm | % | ppm | ppm | |
| 3 | 1000W-300N | 5 | 0.8 | 4.84 | 16 | 234 | 0.3 | 5 | 0.86 | 0.6 | 30 | 24 | 26 | 89 | 6.27 | 0.32 | 12 | 33 | 2.66 | 826 | 1 | 0.05 | 29 | 0.11 | 3 | 37 | 0.39 | 273 | 116 |
| 4 | 350 | 10 | 0.4 | 4.52 | 15 | 227 | 0.4 | 5 | 0.96 | 0.3 | 30 | 26 | 41 | 103 | 5.40 | 0.29 | 11 | 28 | 1.84 | 1342 | 1 | 0.04 | 33 | 0.21 | 4 | 63 | 0.28 | 188 | 104 |
| 5 | 400 | 40 | 0.4 | 4.96 | 11 | 238 | 0.4 | 5 | 1.05 | 0.5 | 32 | 21 | 30 | 108 | 5.81 | 0.32 | 11 | 34 | 2.28 | 857 | 1 | 0.06 | 32 | 0.12 | 5 | 67 | 0.30 | 204 | 120 |
| 6 | 450 | 10 | 0.2 | 4.25 | 16 | 277 | 0.3 | 5 | 1.04 | 0.6 | 32 | 18 | 54 | 63 | 6.19 | 0.30 | 11 | 17 | 1.71 | 760 | 1 | 0.05 | 34 | 0.13 | 8 | 70 | 0.31 | 245 | 79 |
| 7 | 1000W-500N | 20 | 0.2 | 4.72 | 16 | 290 | 0.4 | 5 | 1.32 | 0.7 | 34 | 25 | 39 | 93 | 5.70 | 0.47 | 12 | 27 | 2.04 | 1098 | 1 | 0.07 | 36 | 0.08 | 6 | 73 | 0.28 | 199 | 94 |
| 8 | 1000W-600N | 45 | 0.6 | 3.94 | 21 | 204 | 0.3 | 5 | 0.90 | 0.5 | 29 | 16 | 48 | 59 | 4.97 | 0.27 | 10 | 18 | 1.64 | 606 | 1 | 0.04 | 29 | 0.17 | 5 | 68 | 0.29 | 201 | 78 |
| 9 | 650 | 10 | 0.4 | 4.30 | 14 | 261 | 0.4 | 5 | 0.93 | 0.8 | 31 | 20 | 51 | 59 | 5.26 | 0.37 | 11 | 24 | 1.82 | 1333 | 1 | 0.05 | 33 | 0.16 | 7 | 60 | 0.26 | 202 | 97 |
| 10 | 700 | 30 | 0.2 | 4.30 | 13 | 215 | 0.4 | 5 | 0.84 | 0.8 | 31 | 21 | 46 | 53 | 5.66 | 0.30 | 12 | 23 | 1.66 | 1751 | 1 | 0.05 | 28 | 0.23 | 9 | 58 | 0.27 | 204 | 107 |
| 11 | 750 | 5 | 0.2 | 3.55 | 2 | 599 | 0.3 | 5 | 0.21 | 0.3 | 21 | 7 | 9 | 18 | 2.60 | 0.81 | 10 | 11 | 0.44 | 1228 | 1 | 0.05 | 6 | 0.21 | 2 | 26 | 0.21 | 91 | 57 |
| 12 | 1000W-800N | 10 | 0.2 | 4.65 | 7 | 285 | 0.3 | 5 | 1.14 | 0.8 | 34 | 24 | 31 | 97 | 5.78 | 0.45 | 12 | 41 | 2.28 | 1244 | 1 | 0.11 | 29 | 0.10 | 5 | 52 | 0.31 | 210 | 138 |
| 13 | 1000W-850N | 5 | 0.2 | 4.10 | 6 | 223 | 0.4 | 5 | 0.79 | 0.6 | 31 | 17 | 33 | 46 | 5.26 | 0.29 | 11 | 35 | 1.78 | 1152 | 1 | 0.05 | 23 | 0.22 | 6 | 50 | 0.28 | 195 | 169 |
| 14 | 900 | 5 | 0.2 | 4.11 | 4 | 208 | 0.3 | 5 | 0.66 | 0.8 | 30 | 14 | 32 | 52 | 4.96 | 0.30 | 11 | 28 | 1.67 | 770 | 1 | 0.05 | 22 | 0.17 | 4 | 38 | 0.27 | 187 | 108 |
| 15 | 950 | 5 | 0.2 | 3.59 | 5 | 136 | 0.2 | 5 | 0.68 | 0.7 | 28 | 17 | 16 | 42 | 4.53 | 0.11 | 10 | 34 | 1.50 | 697 | 1 | 0.04 | 13 | 0.10 | 2 | 59 | 0.26 | 161 | 88 |
| 16 | 1000 | 40 | 0.2 | 4.88 | 17 | 221 | 0.7 | 5 | 0.88 | 0.8 | 34 | 18 | 37 | 64 | 5.42 | 0.29 | 12 | 32 | 1.67 | 648 | 1 | 0.07 | 28 | 0.11 | 8 | 61 | 0.24 | 193 | 97 |
| 17 | 1000W-1050N | 110 | 0.2 | 5.67 | 7 | 232 | 0.4 | 5 | 0.39 | 0.9 | 33 | 23 | 30 | 91 | 5.60 | 0.41 | 11 | 37 | 1.90 | 1394 | 1 | 0.05 | 31 | 0.10 | 3 | 21 | 0.27 | 179 | 99 |
| 18 | 1000W-1100N | 55 | 0.2 | 4.45 | 10 | 284 | 0.2 | 5 | 0.50 | 0.9 | 27 | 20 | 19 | 80 | 5.56 | 0.46 | 11 | 37 | 1.93 | 1051 | 1 | 0.07 | 24 | 0.06 | 4 | 23 | 0.30 | 167 | 96 |
| 19 | 1150 | 5 | 0.2 | 4.44 | 9 | 247 | 0.3 | 5 | 0.77 | 0.8 | 31 | 19 | 24 | 94 | 5.22 | 0.30 | 11 | 39 | 2.16 | 1205 | 1 | 0.06 | 25 | 0.10 | 5 | 43 | 0.27 | 168 | 126 |
| 20 | 1200 | 5 | 0.4 | 4.67 | 9 | 290 | 0.3 | 5 | 1.10 | 1.0 | 32 | 22 | 25 | 103 | 5.42 | 0.43 | 11 | 40 | 2.27 | 1453 | 1 | 0.10 | 26 | 0.10 | 6 | 51 | 0.27 | 187 | 130 |
| 21 | 1250 | 10 | 0.6 | 5.31 | 6 | 270 | 0.4 | 5 | 0.77 | 0.5 | 29 | 21 | 23 | 123 | 5.82 | 0.30 | 13 | 50 | 2.43 | 1052 | 1 | 0.05 | 26 | 0.10 | 2 | 44 | 0.29 | 181 | 143 |
| 22 | 1000W-1300N | 50 | 0.2 | 5.71 | 7 | 278 | 0.3 | 5 | 0.60 | 0.3 | 25 | 18 | 23 | 102 | 6.08 | 0.41 | 9 | 45 | 2.20 | 1657 | 1 | 0.12 | 19 | 0.12 | 2 | 27 | 0.33 | 174 | 124 |
| 23 | 1000W-1350N | 15 | 0.2 | 4.19 | 3 | 194 | 0.2 | 5 | 0.81 | 0.4 | 29 | 18 | 17 | 140 | 5.73 | 0.30 | 11 | 38 | 2.12 | 1071 | 1 | 0.05 | 20 | 0.10 | 2 | 42 | 0.32 | 201 | 92 |
| 24 | 1400 | 20 | 0.2 | 4.66 | 4 | 282 | 0.2 | 5 | 1.08 | 0.3 | 28 | 12 | 10 | 54 | 4.91 | 0.50 | 9 | 38 | 1.59 | 878 | 1 | 0.09 | 9 | 0.11 | 2 | 50 | 0.27 | 125 | 124 |
| 25 | 1450 | 15 | 0.2 | 4.20 | 5 | 363 | 0.2 | 5 | 0.70 | 1.7 | 31 | 30 | 24 | 254 | 6.50 | 0.41 | 13 | 44 | 3.20 | 1454 | 1 | 0.06 | 37 | 0.09 | 2 | 20 | 0.37 | 320 | 300 |
| 26 | 1500 | 10 | 0.2 | 4.21 | 3 | 148 | 0.3 | 5 | 1.05 | 0.6 | 40 | 20 | 33 | 121 | 5.53 | 0.23 | 15 | 36 | 2.14 | 926 | 1 | 0.07 | 30 | 0.16 | 4 | 109 | 0.32 | 237 | 105 |
| 27 | 1000W-1550N | 10 | 0.2 | 3.63 | 6 | 271 | 0.2 | 5 | 0.93 | 0.9 | 39 | 21 | 26 | 103 | 5.61 | 0.38 | 16 | 30 | 2.27 | 1582 | 1 | 0.06 | 29 | 0.11 | 5 | 80 | 0.29 | 228 | 123 |
| 28 | 1000W-1600N | 20 | 0.2 | 5.17 | 10 | 376 | 0.3 | 5 | 0.95 | 0.7 | 31 | 25 | 33 | 127 | 5.85 | 0.58 | 11 | 46 | 2.89 | 1310 | 1 | 0.06 | 34 | 0.10 | 3 | 45 | 0.24 | 188 | 161 |
| 29 | 1650 | 15 | 0.2 | 4.50 | 6 | 305 | 0.3 | 5 | 1.12 | 1.1 | 34 | 25 | 40 | 111 | 5.94 | 0.53 | 12 | 39 | 2.59 | 1425 | 1 | 0.07 | 35 | 0.09 | 4 | 52 | 0.26 | 205 | 138 |
| 30 | 1800 | 20 | 0.2 | 4.61 | 8 | 349 | 0.3 | 5 | 1.29 | 0.9 | 34 | 21 | 17 | 93 | 5.23 | 0.64 | 11 | 34 | 2.05 | 2577 | 1 | 0.05 | 18 | 0.09 | 3 | 74 | 0.25 | 148 | 126 |
| 31 | 1950 | 20 | 0.2 | 4.46 | 11 | 257 | 0.4 | 5 | 1.84 | 1.0 | 39 | 28 | 32 | 119 | 6.51 | 0.41 | 15 | 36 | 2.44 | 1139 | 1 | 0.09 | 29 | 0.09 | 8 | 125 | 0.32 | 258 | 105 |
| 32 | 1000W-2000N | 5 | 0.2 | 4.70 | 2 | 368 | 0.3 | 5 | 1.61 | 0.7 | 38 | 23 | 20 | 122 | 5.69 | 0.49 | 14 | 33 | 2.35 | 1178 | 1 | 0.07 | 25 | 0.09 | 2 | 148 | 0.32 | 211 | 118 |
| 33 | 1000W-2100N | 5 | 0.2 | 4.91 | 7 | 281 | 0.5 | 5 | 1.65 | 0.6 | 45 | 21 | 27 | 126 | 5.56 | 0.52 | 19 | 29 | 2.15 | 1067 | 1 | 0.08 | 29 | 0.09 | 6 | 142 | 0.32 | 213 | 126 |
| 34 | 2150 | 60 | 0.2 | 4.62 | 2 | 476 | 0.3 | 5 | 1.03 | 0.7 | 38 | 20 | 22 | 101 | 5.56 | 0.59 | 15 | 28 | 2.07 | 1085 | 1 | 0.09 | 23 | 0.08 | 2 | 87 | 0.31 | 186 | 128 |
| 35 | 2250 | 5 | 0.2 | 4.93 | 11 | 560 | 0.4 | 5 | 1.67 | 0.8 | 43 | 25 | 31 | 145 | 5.79 | 0.49 | 17 | 26 | 2.62 | 1168 | 1 | 0.09 | 38 | 0.09 | 7 | 106 | 0.30 | 209 | 141 |
| 36 | 2300 | 5 | 0.2 | 5.40 | 12 | 570 | 0.4 | 5 | 1.90 | 0.8 | 42 | 31 | 36 | 153 | 6.12 | 0.47 | 16 | 24 | 2.54 | 1240 | 1 | 0.12 | 49 | 0.09 | 7 | 97 | 0.32 | 220 | 159 |
| 37 | 1000W-2400N | 5 | 0.2 | 5.33 | 13 | 315 | 0.4 | 5 | 2.14 | 0.8 | 41 | 26 | 28 | 153 | 5.97 | 0.45 | 15 | 25 | 2.41 | 1235 | 1 | 0.13 | 33 | 0.10 | 6 | 98 | 0.31 | 183 | 121 |

13/08 GP

| T.T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Bc ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm | 8308-001 |
|----------|--------------|--------|--------|------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|----------|
| 38 | 1000W-2450N | 20 | 0.2 | 5.11 | 5 | 433 | 0.3 | 5 | 1.30 | 1.0 | 43 | 21 | 30 | 113 | 5.49 | 0.54 | 16 | 23 | 1.85 | 1401 | 1 | 0.06 | 29 | 0.09 | 10 | 120 | 0.29 | 173 | 130 | |
| 39 | 3000E-100S | 5 | 0.2 | 4.84 | 15 | 259 | 0.5 | 5 | 3.30 | 0.9 | 35 | 19 | 24 | 79 | 5.05 | 0.56 | 14 | 16 | 1.97 | 1661 | 1 | 0.05 | 21 | 0.24 | 20 | 165 | 0.34 | 137 | 124 | |
| 40 | 150 | 5 | 0.2 | 6.10 | 26 | 277 | 0.5 | 5 | 1.69 | 0.8 | 45 | 23 | 30 | 74 | 5.95 | 0.53 | 14 | 17 | 1.84 | 1272 | 1 | 0.06 | 22 | 0.16 | 8 | 169 | 0.39 | 161 | 102 | |
| 41 | 250 | 5 | 0.2 | 5.37 | 12 | 256 | 0.6 | 5 | 1.71 | 0.5 | 42 | 22 | 28 | 97 | 5.18 | 0.53 | 17 | 20 | 1.61 | 955 | 1 | 0.08 | 24 | 0.15 | 4 | 189 | 0.34 | 158 | 125 | |
| 42 | 3000E-350S | 5 | 0.2 | 6.44 | 11 | 293 | 0.5 | 5 | 1.70 | 0.4 | 40 | 43 | 15 | 140 | 5.66 | 0.48 | 14 | 17 | 1.96 | 1486 | 1 | 0.07 | 18 | 0.12 | 2 | 182 | 0.26 | 154 | 100 | |
| 43 | 3000E-500S | 5 | 0.2 | 7.31 | 65 | 576 | 0.6 | 5 | 1.70 | 0.5 | 35 | 58 | 74 | 125 | 5.95 | 0.95 | 12 | 25 | 3.63 | 1656 | 1 | 0.06 | 100 | 0.11 | 2 | 311 | 0.44 | 240 | 95 | |
| 44 | 550 | 5 | 0.2 | 6.05 | 10 | 275 | 0.4 | 5 | 2.13 | 0.5 | 37 | 26 | 23 | 109 | 5.61 | 0.49 | 14 | 17 | 1.86 | 835 | 1 | 0.13 | 29 | 0.13 | 2 | 287 | 0.28 | 210 | 116 | |
| 45 | 600 | 5 | 0.2 | 5.24 | 15 | 268 | 0.4 | 5 | 2.40 | 0.6 | 39 | 30 | 22 | 108 | 5.46 | 0.43 | 14 | 15 | 1.69 | 1091 | 1 | 0.07 | 27 | 0.11 | 4 | 329 | 0.31 | 177 | 100 | |
| 46 | 650 | 5 | 0.2 | 6.77 | 13 | 256 | 0.4 | 5 | 1.13 | 0.9 | 35 | 26 | 17 | 84 | 5.73 | 0.53 | 13 | 17 | 2.02 | 1072 | 1 | 0.22 | 25 | 0.12 | 2 | 139 | 0.13 | 186 | 119 | |
| 47 | 3000E-700S | 5 | 0.2 | 6.28 | 16 | 363 | 0.4 | 5 | 2.44 | 0.6 | 39 | 25 | 19 | 84 | 5.32 | 0.63 | 16 | 15 | 1.82 | 1135 | 2 | 0.08 | 26 | 0.13 | 2 | 511 | 0.33 | 216 | 113 | |
| 48 | 3000E-750S | 30 | 0.2 | 6.14 | 18 | 317 | 0.4 | 5 | 2.55 | 1.0 | 35 | 29 | 18 | 95 | 5.62 | 0.55 | 14 | 13 | 1.93 | 1259 | 1 | 0.09 | 25 | 0.12 | 2 | 385 | 0.34 | 197 | 117 | |
| 51 | 3000E-50N | 5 | 0.2 | 5.80 | 9 | 271 | 0.7 | 5 | 1.56 | 0.6 | 44 | 21 | 31 | 94 | 5.37 | 0.40 | 17 | 17 | 1.65 | 988 | 1 | 0.06 | 23 | 0.13 | 2 | 165 | 0.35 | 149 | 89 | |
| 52 | 100 | 5 | 0.2 | 6.24 | 9 | 156 | 0.4 | 5 | 3.63 | 0.5 | 29 | 26 | 21 | 117 | 5.34 | 0.18 | 14 | 12 | 1.50 | 1473 | 1 | 0.04 | 39 | 0.12 | 2 | 349 | 0.37 | 238 | 85 | |
| 53 | 150 | 5 | 0.2 | 5.44 | 7 | 163 | 0.4 | 5 | 2.02 | 0.4 | 35 | 15 | 31 | 49 | 5.17 | 0.22 | 13 | 12 | 1.46 | 588 | 1 | 0.05 | 19 | 0.20 | 2 | 264 | 0.47 | 209 | 82 | |
| 54 | 3000E-200N | 5 | 1.2 | 5.46 | 10 | 198 | 0.3 | 5 | 3.02 | 1.3 | 33 | 78 | 18 | 271 | 9.81 | 0.30 | 14 | 11 | 1.85 | 2677 | 1 | 0.03 | 53 | 0.15 | 11 | 428 | 0.42 | 246 | 113 | |
| 55 | 3000E-250N | 5 | 0.2 | 6.51 | 14 | 258 | 0.5 | 5 | 2.44 | 0.8 | 37 | 32 | 29 | 89 | 6.24 | 0.34 | 13 | 16 | 2.17 | 1216 | 1 | 0.06 | 37 | 0.16 | 2 | 299 | 0.41 | 217 | 119 | |
| 56 | 300 | 5 | 0.2 | 6.02 | 13 | 249 | 0.4 | 5 | 1.91 | 0.7 | 38 | 25 | 30 | 63 | 5.96 | 0.40 | 13 | 18 | 2.22 | 1097 | 1 | 0.06 | 26 | 0.18 | 2 | 242 | 0.44 | 202 | 132 | |
| 57 | 350 | 5 | 0.2 | 5.30 | 9 | 201 | 0.4 | 5 | 2.63 | 1.0 | 33 | 30 | 39 | 121 | 6.12 | 0.35 | 14 | 20 | 2.38 | 1065 | 1 | 0.05 | 37 | 0.14 | 5 | 416 | 0.40 | 223 | 91 | |
| 58 | 400 | 5 | 0.2 | 5.96 | 18 | 225 | 0.4 | 5 | 2.08 | 1.0 | 34 | 38 | 43 | 131 | 6.60 | 0.30 | 12 | 20 | 2.70 | 1313 | 1 | 0.05 | 30 | 0.12 | 3 | 358 | 0.40 | 221 | 102 | |
| 59 | 3000E-450N | 5 | 0.2 | 5.27 | 17 | 258 | 0.3 | 5 | 2.61 | 0.9 | 32 | 27 | 30 | 112 | 5.59 | 0.34 | 12 | 16 | 2.20 | 993 | 1 | 0.05 | 37 | 0.12 | 4 | 292 | 0.35 | 194 | 107 | |
| 60 | 3000E-500N | 5 | 0.2 | 5.19 | 12 | 173 | 0.4 | 5 | 2.11 | 0.7 | 33 | 26 | 32 | 53 | 5.28 | 0.23 | 11 | 14 | 1.88 | 1426 | 1 | 0.04 | 21 | 0.24 | 4 | 254 | 0.47 | 174 | 102 | |
| 61 | 550 | 5 | 0.2 | 5.25 | 2 | 162 | 0.4 | 5 | 2.29 | 0.3 | 27 | 16 | 36 | 42 | 4.87 | 0.24 | 11 | 14 | 1.66 | 738 | 1 | 0.05 | 21 | 0.16 | 2 | 190 | 0.42 | 185 | 78 | |
| 62 | 600 | 5 | 0.4 | 4.95 | 2 | 172 | 0.3 | 5 | 1.92 | 0.3 | 29 | 15 | 38 | 36 | 4.70 | 0.30 | 9 | 13 | 1.58 | 800 | 1 | 0.05 | 22 | 0.18 | 2 | 201 | 0.45 | 192 | 74 | |
| 63 | 650 | 5 | 0.2 | 5.58 | 2 | 217 | 0.4 | 5 | 2.28 | 0.3 | 31 | 24 | 33 | 100 | 5.68 | 0.33 | 11 | 20 | 2.06 | 1149 | 1 | 0.07 | 31 | 0.13 | 2 | 158 | 0.38 | 212 | 98 | |
| 64 | 3000E-700N | 10 | 0.2 | 4.83 | 2 | 226 | 0.3 | 5 | 1.69 | 0.3 | 31 | 19 | 28 | 52 | 5.46 | 0.32 | 11 | 23 | 1.94 | 839 | 1 | 0.06 | 25 | 0.11 | 2 | 104 | 0.36 | 211 | 97 | |
| 65 | 3000E-750N | 370 | 0.2 | 5.05 | 2 | 138 | 0.3 | 5 | 1.56 | 0.3 | 32 | 17 | 34 | 26 | 5.59 | 0.27 | 10 | 24 | 1.74 | 762 | 1 | 0.06 | 20 | 0.13 | 2 | 111 | 0.39 | 226 | 97 | |
| 66 | 800 | 5 | 0.2 | 5.99 | 4 | 184 | 0.4 | 5 | 2.39 | 0.4 | 31 | 27 | 26 | 69 | 5.77 | 0.37 | 11 | 17 | 1.85 | 1411 | 1 | 0.05 | 30 | 0.16 | 2 | 224 | 0.38 | 192 | 94 | |
| 67 | 850 | 5 | 0.2 | 5.63 | 2 | 269 | 0.3 | 5 | 2.41 | 0.3 | 31 | 16 | 26 | 63 | 5.29 | 0.45 | 10 | 14 | 1.55 | 868 | 1 | 0.07 | 25 | 0.12 | 2 | 162 | 0.39 | 196 | 91 | |
| 68 | 900 | 35 | 0.2 | 5.45 | 4 | 167 | 0.5 | 5 | 2.64 | 0.4 | 34 | 19 | 27 | 68 | 5.09 | 0.30 | 13 | 15 | 1.71 | 927 | 1 | 0.06 | 25 | 0.16 | 2 | 202 | 0.39 | 189 | 106 | |
| 69 | 3000E-950N | 5 | 0.2 | 5.15 | 4 | 170 | 0.3 | 5 | 2.50 | 0.3 | 30 | 17 | 32 | 54 | 4.61 | 0.30 | 10 | 13 | 1.74 | 798 | 1 | 0.05 | 27 | 0.12 | 2 | 228 | 0.35 | 181 | 73 | |
| 70 | 3000E-1000N | 5 | 0.4 | 5.18 | 2 | 167 | 0.3 | 5 | 2.73 | 0.3 | 31 | 19 | 27 | 60 | 4.92 | 0.31 | 11 | 13 | 1.69 | 887 | 1 | 0.07 | 26 | 0.11 | 4 | 174 | 0.36 | 196 | 83 | |
| 71 | 1050 | 10 | 0.2 | 4.72 | 9 | 215 | 0.4 | 5 | 2.75 | 0.7 | 34 | 19 | 30 | 77 | 4.72 | 0.36 | 14 | 13 | 1.49 | 816 | 1 | 0.07 | 23 | 0.09 | 2 | 161 | 0.30 | 194 | 70 | |
| 72 | 1100 | 30 | 0.2 | 4.81 | 7 | 188 | 0.3 | 5 | 2.74 | 0.3 | 34 | 19 | 33 | 71 | 4.69 | 0.34 | 12 | 12 | 1.53 | 841 | 1 | 0.07 | 24 | 0.09 | 2 | 170 | 0.32 | 188 | 70 | |
| 73 | 1150 | 35 | 0.2 | 5.38 | 17 | 207 | 0.6 | 5 | 2.43 | 0.4 | 39 | 15 | 36 | 108 | 4.82 | 0.36 | 16 | 17 | 1.59 | 771 | 1 | 0.07 | 26 | 0.24 | 2 | 127 | 0.30 | 172 | 98 | |
| 74 | 3000E-1200N | 10 | 0.2 | 5.13 | 4 | 146 | 0.3 | 5 | 2.13 | 0.3 | 36 | 10 | 34 | 31 | 4.46 | 0.26 | 12 | 12 | 1.23 | 563 | 1 | 0.06 | 18 | 0.12 | 3 | 126 | 0.41 | 181 | 69 | |
| 75 | 3000E-1250N | 10 | 0.2 | 5.57 | 4 | 201 | 0.4 | 5 | 1.83 | 0.5 | 40 | 20 | 36 | 89 | 5.77 | 0.37 | 15 | 20 | 1.85 | 830 | 1 | 0.07 | 28 | 0.14 | 4 | 122 | 0.36 | 228 | 106 | |
| 76 | 8400E-10400N | 180 | 0.4 | 5.92 | 18 | 232 | 0.4 | 5 | 2.28 | 0.8 | 39 | 32 | 38 | 227 | 6.19 | 0.48 | 16 | 37 | 3.11 | 1363 | 1 | 0.15 | 68 | 0.11 | 32 | 79 | 0.30 | 227 | 123 | |
| 77 | 10500 | 35 | 0.4 | 5.91 | 13 | 203 | 0.4 | 5 | 2.28 | 0.7 | 40 | 32 | 42 | 193 | 6.35 | 0.30 | 15 | 29 | 3.03 | 1220 | 1 | 0.15 | 53 | 0.14 | 19 | 89 | 0.35 | 227 | 123 | |
| 78 | 10600 | 430 | 0.2 | 5.46 | 16 | 126 | 0.4 | 5 | 2.59 | 0.8 | 43 | 28 | 41 | 151 | 5.88 | 0.25 | 16 | 25 | 2.80 | 1081 | 1 | 0.16 | 48 | 0.11 | 9 | 79 | 0.32 | 223 | 104 | |
| 79 | 8400E-10700N | 55 | 0.2 | 5.44 | 12 | 133 | 0.3 | 5 | 2.63 | 0.8 | 37 | 30 | 36 | 143 | 6.11 | 0.27 | 14 | 24 | 2.96 | 1103 | 1 | 0.16 | 45 | 0.12 | 7 | 106 | 0.33 | 232 | 104 | |
| 80 | 8400E-10800N | 35 | 0.4 | 6.55 | 13 | 301 | 0.4 | 5 | 2.20 | 1.2 | 39 | 33 | 33 | 238 | 6.63 | 0.56 | 15 | 31 | 3.23 | 1504 | 1 | 0.14 | 49 | 0.12 | 41 | 113 | 0.31 | 243 | 157 | |
| 81 | 10900 | 45 | 0.2 | 5.33 | 10 | 196 | 0.4 | 5 | 1.69 | 0.7 | 36 | 31 | 45 | 140 | 6.10 | 0.32 | 14 | 25 | 2.92 | 1234 | 1 | 0.11 | 40 | 0.08 | 12 | 85 | 0.23 | 224 | 97 | |
| 82 | 11000 | 85 | 0.2 | 5.03 | 8 | 232 | 0.2 | 5 | 1.35 | 0.3 | 34 | 27 | 20 | 161 | 6.05 | 0.34 | 13 | 28 | 2.80 | 1061 | 1 | 0.14 | 32 | 0.09 | 9 | 38 | 0.38 | 223 | 102 | |
| 83 | 11100 | 30 | 0.2 | 4.92 | 3 | 186 | 0.3 | 5 | 2.13 | 0.7 | 32 | 23 | 39 | 87 | 5.61 | 0.24 | 12 | 22 | 2.66 | 1037 | 1 | 0.15 | 39 | 0.11 | 10 | 61 | 0.30 | 196 | 98 | |
| 84 | 8400E-11200N | 25 | 0.2 | 5.75 | 4 | 209 | 0.3 | 5 | 1.51 | 0.3 | 35 | 28 | 29 | 189 | 6.19 | 0.28 | 13 | 32 | 3.22 | 953 | 1 | 0.12 | 47 | 0.12 | 8 | 48 | 0.36 | 220 | 110 | |

| T.T. No. | SAMPLE No. | As ppb | Ag ppm | Al % | As ppm | Ba ppm | Be ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm | score-001 ppm |
|----------|--------------|-----------|-----------|---------|-----------|-----------|-----------|-----------|---------|-----------|-----------|-----------|-----------|-----------|---------|--------|-----------|-----------|---------|-----------|-----------|---------|-----------|--------|-----------|-----------|---------|----------|-----------|------------------|
| 85 | 8400E-11300N | 25 | 0.4 | 5.53 | 7 | 210 | 0.4 | 5 | 1.76 | 0.3 | 41 | 26 | 30 | 211 | 5.76 | 0.28 | 15 | 28 | 2.93 | 1030 | 1 | 0.12 | 44 | 0.12 | 5 | 67 | 0.32 | 212 | 113 | |
| 86 | 11400 | 20 | 0.2 | 4.99 | 4 | 180 | 0.3 | 5 | 2.05 | 0.4 | 35 | 23 | 35 | 109 | 5.45 | 0.24 | 13 | 19 | 2.49 | 908 | 1 | 0.14 | 35 | 0.12 | 2 | 97 | 0.29 | 196 | 89 | |
| 87 | 11500 | 25 | 0.4 | 5.74 | 6 | 248 | 0.3 | 5 | 1.96 | 0.6 | 31 | 29 | 27 | 180 | 5.86 | 0.20 | 10 | 31 | 3.24 | 941 | 1 | 0.12 | 43 | 0.10 | 10 | 81 | 0.32 | 201 | 105 | |
| 88 | 11600 | 160 | 0.4 | 4.13 | 2 | 322 | 0.3 | 5 | 1.01 | 0.4 | 33 | 17 | 23 | 52 | 4.73 | 0.31 | 12 | 16 | 1.91 | 925 | 1 | 0.10 | 22 | 0.16 | 9 | 83 | 0.25 | 160 | 91 | |
| 89 | 8400E-11700N | 130 | 0.2 | 4.43 | 33 | 290 | 0.3 | 5 | 1.21 | 0.3 | 37 | 20 | 20 | 34 | 5.94 | 0.45 | 12 | 29 | 2.58 | 1211 | 1 | 0.13 | 26 | 0.12 | 4 | 32 | 0.41 | 207 | 86 | |
| 90 | 8400E-13200N | 15 | 0.2 | 4.78 | 5 | 164 | 0.3 | 5 | 2.24 | 0.6 | 33 | 28 | 21 | 186 | 5.95 | 0.21 | 12 | 15 | 2.19 | 989 | 1 | 0.16 | 27 | 0.11 | 3 | 73 | 0.36 | 192 | 83 | |
| 91 | 13300 | 30 | 0.4 | 4.49 | 8 | 145 | 0.4 | 5 | 1.85 | 0.4 | 33 | 22 | 25 | 159 | 5.82 | 0.26 | 12 | 14 | 1.74 | 741 | 3 | 0.12 | 20 | 0.13 | 3 | 68 | 0.32 | 172 | 75 | |
| 92 | 13400 | 50 | 0.2 | 4.88 | 2 | 89 | 0.3 | 5 | 1.43 | 0.2 | 28 | 12 | 32 | 64 | 5.51 | 0.11 | 9 | 10 | 1.35 | 517 | 1 | 0.09 | 19 | 0.11 | 2 | 57 | 0.31 | 182 | 57 | |
| 93 | 13500 | 60 | 0.4 | 4.54 | 2 | 125 | 0.3 | 5 | 2.00 | 0.2 | 31 | 18 | 24 | 108 | 5.40 | 0.17 | 10 | 11 | 1.66 | 899 | 1 | 0.13 | 21 | 0.11 | 2 | 81 | 0.31 | 182 | 70 | |
| 94 | 8400E-13600N | 30 | 0.2 | 4.09 | 2 | 214 | 0.3 | 5 | 1.68 | 0.2 | 30 | 22 | 16 | 331 | 5.60 | 0.23 | 10 | 14 | 1.74 | 918 | 1 | 0.10 | 21 | 0.15 | 2 | 74 | 0.31 | 183 | 95 | |
| 95 | 8400E-13700N | 40 | 0.2 | 4.53 | 3 | 313 | 0.3 | 5 | 1.71 | 0.3 | 34 | 29 | 15 | 240 | 5.67 | 0.47 | 12 | 15 | 1.77 | 1059 | 3 | 0.11 | 28 | 0.09 | 2 | 102 | 0.31 | 196 | 116 | |
| 96 | 13800 | 20 | 0.4 | 4.25 | 4 | 178 | 0.3 | 5 | 1.38 | 0.2 | 29 | 16 | 15 | 152 | 4.45 | 0.18 | 9 | 10 | 1.08 | 711 | 4 | 0.08 | 17 | 0.15 | 2 | 77 | 0.27 | 135 | 75 | |
| 97 | 13900 | 20 | 0.2 | 4.38 | 8 | 249 | 0.4 | 5 | 1.97 | 0.3 | 37 | 39 | 16 | 228 | 5.71 | 0.26 | 14 | 14 | 1.61 | 1313 | 5 | 0.10 | 33 | 0.10 | 2 | 124 | 0.33 | 221 | 124 | |
| 98 | 14000 | 170 | 0.2 | 5.57 | 2 | 152 | 0.3 | 5 | 1.19 | 0.2 | 29 | 14 | 19 | 114 | 4.46 | 0.23 | 9 | 9 | 1.13 | 778 | 2 | 0.07 | 14 | 0.16 | 2 | 54 | 0.25 | 130 | 81 | |
| 101 | 8400E-14100N | 10 | 0.2 | 4.02 | 5 | 181 | 0.5 | 5 | 1.13 | 0.3 | 34 | 16 | 24 | 107 | 3.98 | 0.20 | 14 | 12 | 0.92 | 858 | 2 | 0.07 | 14 | 0.22 | 2 | 69 | 0.26 | 132 | 66 | |
| 102 | 8400E-14200N | 30 | 0.2 | 4.61 | 6 | 267 | 0.3 | 5 | 1.99 | 0.2 | 37 | 22 | 20 | 218 | 6.38 | 0.31 | 14 | 12 | 1.82 | 936 | 6 | 0.12 | 20 | 0.11 | 2 | 107 | 0.37 | 212 | 86 | |
| 103 | 14300 | 15 | 0.2 | 4.77 | 2 | 237 | 0.3 | 5 | 2.02 | 0.3 | 33 | 17 | 22 | 154 | 5.11 | 0.25 | 12 | 11 | 1.59 | 861 | 1 | 0.12 | 18 | 0.21 | 2 | 115 | 0.33 | 194 | 77 | |
| 104 | 14400 | 150 | 0.2 | 7.51 | 2 | 369 | 0.4 | 5 | 2.82 | 0.4 | 28 | 40 | 31 | 258 | 7.67 | 0.32 | 11 | 26 | 4.49 | 1226 | 1 | 0.22 | 49 | 0.08 | 2 | 175 | 0.46 | 377 | 90 | |
| 105 | 14500 | 20 | 0.2 | 6.07 | 2 | 189 | 0.3 | 5 | 2.70 | 0.2 | 30 | 22 | 26 | 193 | 6.22 | 0.14 | 11 | 15 | 2.33 | 713 | 1 | 0.18 | 26 | 0.10 | 2 | 133 | 0.38 | 244 | 76 | |
| 106 | 8400E-14600N | 10 | 0.2 | 4.47 | 6 | 126 | 0.3 | 5 | 3.83 | 0.7 | 21 | 47 | 22 | 89 | 8.93 | 0.15 | 10 | 12 | 3.23 | 1091 | 1 | 0.27 | 40 | 0.09 | 4 | 142 | 0.54 | 416 | 94 | |
| 107 | 8400E-14700N | 30 | 0.2 | 4.33 | 2 | 174 | 0.3 | 5 | 3.31 | 0.8 | 25 | 37 | 36 | 91 | 7.67 | 0.20 | 10 | 14 | 3.03 | 1142 | 1 | 0.27 | 40 | 0.10 | 15 | 118 | 0.50 | 371 | 85 | |
| 108 | 14800 | 10 | 0.2 | 4.44 | 8 | 115 | 0.3 | 5 | 3.39 | 0.3 | 25 | 29 | 52 | 162 | 5.94 | 0.17 | 10 | 14 | 2.79 | 775 | 1 | 0.26 | 43 | 0.13 | 2 | 127 | 0.37 | 242 | 76 | |
| 109 | 8400E-14900N | 10 | 0.2 | 3.79 | 14 | 89 | 0.3 | 5 | 3.30 | 0.3 | 25 | 33 | 84 | 106 | 6.56 | 0.15 | 10 | 12 | 3.03 | 800 | 1 | 0.29 | 63 | 0.10 | 2 | 112 | 0.38 | 276 | 67 | |
| 110 | 8500E-13200N | 15 | 0.2 | 4.78 | 3 | 186 | 0.3 | 5 | 1.38 | 0.4 | 37 | 26 | 17 | 251 | 6.05 | 0.33 | 13 | 14 | 1.71 | 922 | 1 | 0.10 | 15 | 0.13 | 2 | 47 | 0.35 | 184 | 84 | |
| 111 | 8600E-13700N | 100 | 0.2 | 4.66 | 7 | 151 | 0.4 | 5 | 2.47 | 0.3 | 32 | 38 | 27 | 517 | 6.32 | 0.26 | 13 | 20 | 2.06 | 965 | 6 | 0.18 | 30 | 0.08 | 2 | 92 | 0.32 | 209 | 95 | |
| 112 | 8600E-13800N | 140 | 0.6 | 5.25 | 4 | 245 | 0.3 | 5 | 2.31 | 0.3 | 30 | 28 | 15 | 305 | 7.31 | 0.40 | 11 | 13 | 1.98 | 793 | 2 | 0.11 | 20 | 0.11 | 2 | 129 | 0.37 | 224 | 78 | |
| 113 | 13900 | 85 | 0.4 | 7.10 | 2 | 107 | 0.3 | 5 | 2.20 | 0.2 | 28 | 21 | 16 | 303 | 7.05 | 0.15 | 9 | 12 | 1.74 | 637 | 2 | 0.12 | 16 | 0.11 | 2 | 82 | 0.31 | 217 | 72 | |
| 114 | 14000 | 45 | 0.2 | 4.79 | 2 | 199 | 0.3 | 5 | 1.95 | 0.2 | 31 | 21 | 16 | 225 | 5.54 | 0.18 | 10 | 11 | 1.65 | 677 | 3 | 0.12 | 15 | 0.09 | 2 | 96 | 0.29 | 150 | 68 | |
| 115 | 14100 | 15 | 0.2 | 5.01 | 2 | 149 | 0.3 | 5 | 1.49 | 0.2 | 29 | 10 | 16 | 164 | 4.75 | 0.09 | 9 | 9 | 0.98 | 456 | 2 | 0.07 | 11 | 0.11 | 2 | 72 | 0.23 | 117 | 52 | |
| 116 | 8600E-14200N | 20 | 0.2 | 5.18 | 2 | 227 | 0.3 | 5 | 1.50 | 0.3 | 32 | 9 | 12 | 161 | 5.71 | 0.30 | 11 | 10 | 1.53 | 631 | 2 | 0.07 | 10 | 0.12 | 2 | 88 | 0.28 | 126 | 55 | |
| 117 | 8600E-14300N | 20 | 0.2 | 5.57 | 2 | 115 | 0.4 | 5 | 1.19 | 0.2 | 35 | 14 | 21 | 103 | 4.53 | 0.17 | 12 | 10 | 1.10 | 641 | 1 | 0.10 | 15 | 0.12 | 2 | 55 | 0.24 | 130 | 75 | |
| 118 | 14400 | 15 | 0.4 | 4.28 | 2 | 147 | 0.3 | 5 | 1.72 | 0.2 | 33 | 8 | 19 | 100 | 5.59 | 0.13 | 10 | 7 | 1.17 | 554 | 6 | 0.11 | 13 | 0.13 | 2 | 73 | 0.36 | 224 | 67 | |
| 119 | 14500 | 200 | 0.2 | 3.64 | 2 | 585 | 0.2 | 5 | 1.52 | 0.4 | 33 | 40 | 12 | 342 | 6.68 | 0.36 | 11 | 10 | 1.70 | 1024 | 11 | 0.09 | 16 | 0.09 | 2 | 135 | 0.32 | 171 | 76 | |
| 120 | 8600E-14600N | 50 | 0.2 | 5.46 | 2 | 172 | 0.4 | 5 | 2.41 | 0.3 | 32 | 33 | 24 | 265 | 6.18 | 0.17 | 12 | 14 | 2.13 | 1167 | 1 | 0.20 | 25 | 0.14 | 2 | 116 | 0.37 | 245 | 77 | |
| 121 | 8800E-11000N | 15 | 0.4 | 3.30 | 7 | 313 | 0.3 | 5 | 1.35 | 0.7 | 38 | 8 | 15 | 174 | 5.89 | 0.45 | 15 | 11 | 1.51 | 706 | 2 | 0.07 | 9 | 0.12 | 3 | 61 | 0.28 | 111 | 64 | |
| 122 | 8800E-11100N | 30 | 0.2 | 5.29 | 9 | 191 | 0.4 | 5 | 1.45 | 0.3 | 35 | 24 | 34 | 241 | 5.40 | 0.21 | 12 | 24 | 2.17 | 1161 | 1 | 0.10 | 31 | 0.14 | 7 | 80 | 0.27 | 185 | 83 | |
| 123 | 11200 | 35 | 0.2 | 5.01 | 7 | 173 | 0.3 | 5 | 1.97 | 0.3 | 37 | 22 | 34 | 128 | 5.20 | 0.27 | 14 | 20 | 2.25 | 1064 | 1 | 0.13 | 32 | 0.14 | 5 | 93 | 0.27 | 186 | 85 | |
| 124 | 11300 | 45 | 0.2 | 5.51 | 3 | 330 | 0.4 | 5 | 1.46 | 0.8 | 38 | 43 | 26 | 347 | 6.48 | 0.52 | 15 | 25 | 2.55 | 1281 | 1 | 0.10 | 39 | 0.12 | 13 | 76 | 0.31 | 187 | 103 | |
| 125 | 11400 | 35 | 0.2 | 5.97 | 9 | 247 | 0.4 | 5 | 2.69 | 0.3 | 31 | 26 | 23 | 164 | 5.54 | 0.37 | 13 | 26 | 2.77 | 1048 | 1 | 0.16 | 38 | 0.09 | 3 | 150 | 0.32 | 202 | 89 | |
| 126 | 8800E-11500N | 210 | 0.2 | 5.54 | 10 | 333 | 0.3 | 5 | 2.09 | 0.3 | 35 | 26 | 18 | 131 | 6.12 | 0.49 | 13 | 26 | 2.61 | 1232 | 1 | 0.17 | 27 | 0.09 | 10 | 104 | 0.32 | 214 | 108 | |
| 127 | 8800E-11600N | 80 | 0.2 | 5.35 | 7 | 307 | 0.3 | 5 | 2.52 | 0.6 | 33 | 25 | 20 | 126 | 5.59 | 0.41 | 13 | 24 | 2.61 | 1190 | 1 | 0.15 | 31 | 0.08 | 16 | 114 | 0.26 | 187 | 98 | |
| 128 | 11700 | 115 | 0.2 | 5.65 | 5 | 223 | 0.4 | 5 | 1.80 | 0.4 | 39 | 31 | 30 | 196 | 5.46 | 0.36 | 15 | 19 | 2.01 | 1004 | 1 | 0.12 | 29 | 0.13 | 5 | 104 | 0.25 | 173 | 84 | |
| 129 | 11800 | 110 | 0.2 | 5.89 | 17 | 304 | 0.3 | 5 | 0.98 | 0.2 | 32 | 18 | 19 | 140 | 5.33 | 0.54 | 11 | 16 | 1.36 | 746 | 1 | 0.15 | 15 | 0.20 | 2 | 143 | 0.14 | 166 | 59 | |
| 130 | 11900 | 75 | 0.4 | 6.18 | 19 | 227 | 0.5 | 5 | 2.35 | 0.4 | 35 | 41 | 22 | 343 | 5.92 | 0.35 | 13 | 20 | 2.05 | 1296 | 1 | 0.10 | 32 | 0.18 | 4 | 166 | 0.26 | 163 | 87 | |
| 131 | 8800E-12000N | 125 | 0.2 | 5.80 | 2 | 167 | 0.4 | 5 | 2.54 | 0.3 | 30 | 27 | 24 | 123 | 5.33 | 0.26 | 13 | 16 | 2.01 | 1176 | 1 | 0.11 | 23 | 0.13 | 2 | 119 | 0.30 | 187 | 70 | |

| T.T. No. | SAMPLE No. | As | Ag | Al | Ar | Ba | Be | Bi | Cu | Cd | Ce | Co | Cr | Cu | Fe | K | La | Li | Mg | Mn | Mo | Na | Ni | P | Pb | Sr | Ti | V | Zn | 8008-001 |
|----------|--------------|-----|-----|------|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|-------|------|-----|-----|------|------|-----|------|----|------|-----|-----|------|-----|-----|----------|
| | | ppb | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | ppm | % | % | ppm | ppm | % | ppm | ppm | ppm | ppm |
| 132 | 8800E-12200N | 80 | 0.4 | 5.00 | 2 | 188 | 0.3 | 5 | 2.53 | 0.2 | 29 | 51 | 18 | 307 | 7.99 | 0.23 | 10 | 15 | 2.14 | 1036 | 21 | 0.13 | 22 | 0.13 | 3 | 234 | 0.30 | 187 | 66 | |
| 133 | 12300 | 20 | 0.2 | 5.24 | 2 | 244 | 0.3 | 5 | 2.18 | 0.3 | 28 | 33 | 22 | 219 | 5.67 | 0.35 | 10 | 26 | 2.90 | 1058 | 1 | 0.13 | 37 | 0.09 | 2 | 105 | 0.31 | 180 | 94 | |
| 134 | 12400 | 30 | 0.2 | 5.56 | 2 | 224 | 0.4 | 5 | 1.44 | 0.5 | 29 | 31 | 26 | 376 | 5.48 | 0.27 | 9 | 21 | 2.50 | 895 | 1 | 0.08 | 34 | 0.14 | 2 | 70 | 0.30 | 164 | 78 | |
| 135 | 12600 | 130 | 0.2 | 5.91 | 2 | 160 | 0.3 | 5 | 3.54 | 0.2 | 22 | 36 | 12 | 298 | 5.64 | 0.26 | 9 | 16 | 2.40 | 917 | 1 | 0.14 | 23 | 0.08 | 2 | 185 | 0.32 | 202 | 66 | |
| 136 | 8800E-12700N | 110 | 0.2 | 4.79 | 2 | 222 | 0.3 | 5 | 2.23 | 0.3 | 30 | 30 | 17 | 252 | 5.63 | 0.39 | 11 | 16 | 2.39 | 924 | 2 | 0.12 | 25 | 0.09 | 2 | 122 | 0.31 | 183 | 70 | |
| 137 | 8800E-12800N | 45 | 0.2 | 4.78 | 2 | 215 | 0.3 | 5 | 2.15 | 0.2 | 31 | 30 | 20 | 234 | 5.75 | 0.31 | 11 | 17 | 2.40 | 890 | 2 | 0.13 | 28 | 0.08 | 2 | 99 | 0.31 | 196 | 71 | |
| 138 | 12900 | 10 | 0.2 | 3.88 | 3 | 154 | 0.3 | 5 | 1.18 | 0.2 | 29 | 15 | 20 | 171 | 3.87 | 0.17 | 9 | 10 | 1.15 | 487 | 2 | 0.08 | 15 | 0.18 | 2 | 72 | 0.22 | 107 | 61 | |
| 139 | 13000 | 70 | 0.2 | 4.81 | 4 | 196 | 0.3 | 5 | 2.71 | 0.3 | 30 | 29 | 15 | 259 | 6.16 | 0.39 | 11 | 13 | 1.84 | 1220 | 1 | 0.13 | 18 | 0.10 | 2 | 164 | 0.29 | 188 | 78 | |
| 140 | 13100 | 10 | 0.2 | 4.92 | 2 | 156 | 0.3 | 5 | 3.03 | 0.3 | 27 | 25 | 21 | 145 | 5.74 | 0.18 | 11 | 12 | 2.01 | 852 | 2 | 0.14 | 21 | 0.09 | 2 | 130 | 0.32 | 197 | 70 | |
| 141 | 8800E-13200N | 15 | 0.2 | 5.93 | 2 | 126 | 0.4 | 5 | 2.05 | 0.2 | 30 | 17 | 26 | 101 | 5.53 | 0.13 | 11 | 10 | 1.28 | 608 | 3 | 0.10 | 15 | 0.12 | 2 | 92 | 0.26 | 160 | 52 | |
| 142 | 8800E-13300N | 5 | 0.2 | 5.88 | 2 | 88 | 0.3 | 5 | 1.92 | 0.2 | 28 | 15 | 22 | 90 | 5.20 | 0.12 | 10 | 10 | 1.46 | 624 | 1 | 0.10 | 15 | 0.11 | 2 | 68 | 0.27 | 160 | 64 | |
| 143 | 13400 | 35 | 0.2 | 5.17 | 2 | 144 | 0.4 | 5 | 2.85 | 0.2 | 28 | 24 | 24 | 160 | 5.51 | 0.25 | 11 | 16 | 2.03 | 900 | 3 | 0.13 | 22 | 0.11 | 2 | 111 | 0.32 | 188 | 83 | |
| 144 | 13500 | 40 | 0.2 | 5.10 | 2 | 100 | 0.4 | 5 | 2.13 | 0.3 | 33 | 37 | 23 | 321 | 5.79 | 0.16 | 12 | 16 | 1.67 | 711 | 4 | 0.13 | 21 | 0.14 | 2 | 65 | 0.31 | 175 | 98 | |
| 145 | 13600 | 10 | 0.2 | 4.01 | 2 | 79 | 0.2 | 5 | 1.86 | 0.2 | 32 | 10 | 20 | 43 | 4.86 | 0.15 | 11 | 8 | 1.29 | 586 | 1 | 0.12 | 13 | 0.08 | 2 | 61 | 0.32 | 174 | 61 | |
| 146 | 8800E-13700N | 10 | 0.2 | 4.25 | 2 | 93 | 0.3 | 5 | 2.33 | 0.2 | 36 | 38 | 20 | 131 | 5.51 | 0.19 | 14 | 16 | 1.63 | 1133 | 11 | 0.13 | 17 | 0.10 | 2 | 87 | 0.38 | 196 | 101 | |
| 147 | 8900E-12000N | 110 | 0.2 | 5.44 | 2 | 175 | 0.5 | 5 | 2.32 | 0.2 | 40 | 20 | 30 | 305 | 5.34 | 0.28 | 16 | 23 | 2.21 | 774 | 1 | 0.15 | 34 | 0.15 | 2 | 108 | 0.30 | 183 | 78 | |
| 148 | 12100 | 35 | 0.2 | 5.52 | 2 | 236 | 0.4 | 5 | 1.92 | 0.2 | 36 | 21 | 26 | 139 | 5.11 | 0.41 | 13 | 17 | 1.96 | 852 | 1 | 0.11 | 25 | 0.15 | 2 | 117 | 0.29 | 180 | 77 | |
| 151 | 12200 | 40 | 0.2 | 6.10 | 2 | 283 | 0.6 | 5 | 2.04 | 0.4 | 42 | 45 | 41 | 372 | 6.70 | 0.54 | 17 | 22 | 2.66 | 1903 | 1 | 0.10 | 39 | 0.14 | 2 | 134 | 0.27 | 225 | 88 | |
| 152 | 12300 | 20 | 0.2 | 5.07 | 2 | 111 | 0.4 | 5 | 2.96 | 0.2 | 32 | 27 | 35 | 263 | 5.78 | 0.25 | 13 | 17 | 2.38 | 895 | 2 | 0.16 | 32 | 0.07 | 2 | 124 | 0.32 | 207 | 72 | |
| 153 | 8900E-12400N | 35 | 0.2 | 5.04 | 2 | 219 | 0.4 | 5 | 2.81 | 0.2 | 34 | 38 | 31 | 258 | 6.39 | 0.34 | 12 | 14 | 2.22 | 1082 | 1 | 0.15 | 33 | 0.09 | 2 | 138 | 0.30 | 184 | 69 | |
| 154 | 8900E-12500N | 30 | 0.2 | 5.34 | 2 | 176 | 0.3 | 5 | 2.63 | 0.2 | 33 | 27 | 26 | 166 | 5.86 | 0.18 | 12 | 13 | 2.14 | 826 | 1 | 0.16 | 28 | 0.12 | 2 | 101 | 0.35 | 184 | 69 | |
| 155 | 12600 | 110 | 0.2 | 5.11 | 2 | 199 | 0.3 | 5 | 2.53 | 0.2 | 31 | 23 | 19 | 235 | 5.28 | 0.24 | 11 | 16 | 2.26 | 722 | 1 | 0.13 | 22 | 0.10 | 2 | 122 | 0.33 | 184 | 72 | |
| 156 | 12700 | 35 | 0.2 | 4.57 | 2 | 308 | 0.3 | 5 | 1.90 | 0.2 | 32 | 41 | 18 | 322 | 5.54 | 0.34 | 11 | 15 | 1.93 | 1004 | 4 | 0.11 | 19 | 0.11 | 2 | 112 | 0.29 | 161 | 74 | |
| 157 | 12800 | 20 | 0.2 | 5.64 | 2 | 146 | 0.3 | 5 | 2.72 | 0.2 | 32 | 23 | 22 | 130 | 5.38 | 0.20 | 12 | 13 | 2.00 | 875 | 1 | 0.13 | 22 | 0.11 | 2 | 121 | 0.31 | 176 | 64 | |
| 158 | 8900E-12900N | 20 | 0.2 | 6.93 | 2 | 216 | 0.5 | 5 | 3.05 | 0.2 | 31 | 32 | 25 | 240 | 6.20 | 0.39 | 12 | 23 | 2.52 | 1090 | 1 | 0.18 | 28 | 0.10 | 2 | 137 | 0.36 | 220 | 76 | |
| 159 | 8900E-13000N | 35 | 0.2 | 5.82 | 2 | 233 | 0.3 | 5 | 1.73 | 0.2 | 34 | 19 | 28 | 150 | 5.44 | 0.30 | 11 | 14 | 1.51 | 817 | 2 | 0.09 | 19 | 0.17 | 2 | 110 | 0.29 | 174 | 67 | |
| 160 | 13100 | 40 | 0.2 | 4.95 | 2 | 122 | 0.3 | 5 | 3.08 | 0.3 | 30 | 26 | 27 | 182 | 5.60 | 0.19 | 11 | 14 | 2.16 | 868 | 2 | 0.15 | 24 | 0.08 | 2 | 122 | 0.33 | 192 | 69 | |
| 161 | 13200 | 35 | 0.2 | 4.59 | 2 | 107 | 0.2 | 5 | 2.46 | 0.2 | 29 | 16 | 20 | 79 | 5.21 | 0.14 | 10 | 9 | 1.52 | 717 | 1 | 0.12 | 16 | 0.13 | 2 | 103 | 0.33 | 180 | 56 | |
| 162 | 13300 | 45 | 0.2 | 5.74 | 2 | 125 | 0.3 | 5 | 2.51 | 0.2 | 29 | 22 | 15 | 248 | 6.97 | 0.15 | 10 | 10 | 1.49 | 757 | 11 | 0.10 | 13 | 0.11 | 2 | 91 | 0.27 | 156 | 65 | |
| 163 | 8900E-13400N | 780 | 0.2 | 2.93 | 2 | 52 | 0.2 | 5 | 1.87 | 0.2 | 31 | 5 | 19 | 57 | 3.94 | 0.10 | 10 | 4 | 0.57 | 363 | 4 | 0.06 | 8 | 0.10 | 2 | 110 | 0.37 | 185 | 37 | |
| 164 | 8900E-13500N | 15 | 0.2 | 3.95 | 2 | 163 | 0.2 | 5 | 2.55 | 0.2 | 31 | 8 | 19 | 78 | 7.70 | 0.26 | 11 | 8 | 1.43 | 774 | 3 | 0.12 | 13 | 0.15 | 3 | 106 | 0.40 | 212 | 79 | |
| 165 | 13610 | 10 | 0.2 | 6.17 | 2 | 83 | 0.3 | 5 | 1.99 | 0.2 | 30 | 11 | 13 | 96 | 5.98 | 0.09 | 9 | 10 | 1.51 | 667 | 3 | 0.13 | 10 | 0.08 | 2 | 52 | 0.32 | 176 | 61 | |
| 166 | 13700 | 15 | 0.2 | 5.73 | 2 | 103 | 0.3 | 5 | 2.10 | 0.2 | 31 | 13 | 21 | 65 | 5.42 | 0.13 | 10 | 8 | 1.26 | 645 | 1 | 0.10 | 14 | 0.10 | 2 | 88 | 0.29 | 165 | 68 | |
| 167 | 13800 | 15 | 0.2 | 4.51 | 2 | 63 | 0.2 | 5 | 1.80 | 0.2 | 29 | 8 | 22 | 41 | 6.02 | 0.13 | 9 | 9 | 1.38 | 528 | 1 | 0.09 | 12 | 0.09 | 2 | 68 | 0.40 | 230 | 64 | |
| 168 | 8900E-13900N | 45 | 0.4 | 6.18 | 2 | 90 | 0.3 | 5 | 2.25 | 0.2 | 30 | 15 | 22 | 82 | 5.86 | 0.12 | 10 | 10 | 1.30 | 582 | 1 | 0.10 | 15 | 0.10 | 2 | 119 | 0.31 | 184 | 64 | |
| 169 | 8900E-14000N | 180 | 1.0 | 4.61 | 136 | 24 | 0.5 | 10 | 3.60 | 0.2 | 30 | 76 | 26 | 880 | 11.28 | 0.05 | 17 | 7 | 0.68 | 1074 | 37 | 0.03 | 36 | 0.16 | 22 | 270 | 0.18 | 627 | 83 | |
| 170 | 9000E-11000N | 20 | 0.2 | 4.71 | 2 | 149 | 0.3 | 5 | 1.85 | 0.2 | 33 | 19 | 27 | 142 | 5.42 | 0.24 | 11 | 14 | 1.81 | 762 | 1 | 0.12 | 19 | 0.12 | 2 | 61 | 0.27 | 161 | 69 | |
| 171 | 11100 | 50 | 0.2 | 3.64 | 2 | 393 | 0.3 | 5 | 1.55 | 0.2 | 41 | 7 | 8 | 121 | 4.97 | 0.44 | 15 | 11 | 1.20 | 511 | 5 | 0.07 | 7 | 0.14 | 2 | 66 | 0.34 | 115 | 45 | |
| 172 | 11200 | 15 | 0.2 | 5.50 | 2 | 154 | 0.3 | 5 | 1.75 | 0.2 | 35 | 20 | 37 | 138 | 5.51 | 0.25 | 13 | 18 | 2.03 | 702 | 1 | 0.12 | 28 | 0.11 | 2 | 72 | 0.27 | 202 | 77 | |
| 173 | 9000E-11300N | 25 | 0.2 | 6.54 | 2 | 149 | 0.4 | 5 | 2.06 | 0.2 | 32 | 27 | 25 | 167 | 5.83 | 0.28 | 11 | 20 | 2.50 | 802 | 1 | 0.19 | 31 | 0.12 | 2 | 95 | 0.29 | 232 | 88 | |
| 174 | 9000E-11400N | 65 | 0.2 | 5.10 | 2 | 184 | 0.3 | 5 | 1.93 | 0.2 | 35 | 22 | 34 | 134 | 5.27 | 0.24 | 12 | 17 | 2.12 | 1025 | 1 | 0.12 | 28 | 0.14 | 4 | 86 | 0.27 | 180 | 83 | |
| 175 | 11500 | 70 | 0.2 | 4.84 | 2 | 186 | 0.3 | 5 | 1.52 | 0.2 | 34 | 18 | 31 | 110 | 4.65 | 0.30 | 11 | 18 | 1.84 | 908 | 1 | 0.10 | 26 | 0.16 | 4 | 76 | 0.25 | 164 | 90 | |
| 176 | 11600 | 190 | 0.2 | 5.27 | 5 | 206 | 0.3 | 5 | 1.87 | 0.2 | 36 | 23 | 37 | 115 | 5.43 | 0.29 | 12 | 21 | 2.42 | 845 | 1 | 0.12 | 36 | 0.10 | 6 | 88 | 0.28 | 191 | 92 | |
| 177 | 11700 | 140 | 0.2 | 5.34 | 4 | 189 | 0.3 | 5 | 2.01 | 0.2 | 37 | 23 | 38 | 109 | 5.51 | 0.19 | 12 | 20 | 2.31 | 765 | 1 | 0.12 | 34 | 0.09 | 6 | 94 | 0.30 | 187 | 81 | |
| 178 | 9000E-11800N | 260 | 0.2 | 4.87 | 4 | 187 | 0.3 | 5 | 2.10 | 0.3 | 35 | 24 | 31 | 143 | 5.40 | 0.25 | 12 | 18 | 2.23 | 937 | 1 | 0.13 | 32 | 0.11 | 2 | 87 | 0.30 | 187 | 80 | |

| T.T. No. | SAMPLE No. | As ppb | Ag ppm | Al % | Ar ppm | Ba ppm | Bc ppm | Bi ppm | Ca % | Cl ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm | 900E-001 Pg. 8 of 8 |
|----------|--------------|-----------|-----------|---------|-----------|-----------|-----------|-----------|---------|-----------|-----------|-----------|-----------|-----------|---------|--------|-----------|-----------|---------|-----------|-----------|---------|-----------|--------|-----------|-----------|---------|----------|-----------|------------------------|
| 179 | 9000E-11900N | 70 | 0.2 | 5.07 | 2 | 167 | 0.3 | 5 | 2.63 | 0.3 | 33 | 27 | 23 | 127 | 5.88 | 0.31 | 11 | 13 | 2.22 | 1073 | 1 | 0.14 | 25 | 0.09 | 2 | 141 | 0.30 | 197 | 73 | |
| 180 | 12000 | 30 | 0.2 | 5.33 | 2 | 156 | 0.4 | 5 | 2.06 | 0.3 | 35 | 23 | 26 | 118 | 5.06 | 0.21 | 11 | 12 | 1.70 | 765 | 1 | 0.10 | 21 | 0.10 | 2 | 98 | 0.24 | 164 | 69 | |
| 181 | 12100 | 15 | 0.2 | 3.99 | 2 | 171 | 0.3 | 5 | 1.84 | 0.3 | 33 | 19 | 23 | 126 | 5.14 | 0.29 | 12 | 12 | 1.83 | 792 | 2 | 0.14 | 19 | 0.11 | 2 | 81 | 0.35 | 179 | 73 | |
| 182 | 12200 | 10 | 0.2 | 5.52 | 2 | 202 | 0.3 | 5 | 2.50 | 0.2 | 33 | 23 | 24 | 142 | 6.17 | 0.27 | 12 | 15 | 2.05 | 853 | 4 | 0.15 | 26 | 0.12 | 2 | 112 | 0.36 | 209 | 81 | |
| 183 | 9000E-12300N | 15 | 0.2 | 4.57 | 2 | 171 | 0.3 | 5 | 2.37 | 0.2 | 33 | 17 | 18 | 151 | 5.57 | 0.24 | 12 | 12 | 1.80 | 733 | 1 | 0.15 | 20 | 0.13 | 2 | 116 | 0.38 | 206 | 73 | |
| 184 | 9000E-12400N | 10 | 0.2 | 5.00 | 2 | 169 | 0.3 | 5 | 2.29 | 0.2 | 33 | 18 | 28 | 86 | 5.65 | 0.17 | 11 | 12 | 1.84 | 1065 | 1 | 0.13 | 25 | 0.12 | 2 | 105 | 0.35 | 188 | 67 | |
| 185 | 12500 | 5 | 0.2 | 7.10 | 2 | 113 | 0.4 | 5 | 1.90 | 0.2 | 29 | 13 | 29 | 77 | 4.59 | 0.10 | 9 | 8 | 1.16 | 502 | 1 | 0.08 | 17 | 0.13 | 2 | 62 | 0.24 | 130 | 53 | |
| 186 | 12600 | 10 | 0.4 | 5.18 | 2 | 129 | 0.4 | 5 | 2.64 | 0.2 | 31 | 25 | 21 | 135 | 5.68 | 0.20 | 11 | 17 | 1.81 | 651 | 4 | 0.14 | 25 | 0.16 | 2 | 92 | 0.33 | 165 | 76 | |
| 187 | 12700 | 75 | 0.2 | 5.23 | 2 | 252 | 0.3 | 5 | 2.40 | 0.2 | 32 | 30 | 20 | 253 | 6.02 | 0.36 | 11 | 18 | 2.53 | 931 | 2 | 0.14 | 25 | 0.09 | 2 | 139 | 0.34 | 197 | 71 | |
| 188 | 9000E-12800N | 15 | 0.2 | 4.93 | 2 | 206 | 0.3 | 5 | 2.33 | 0.2 | 32 | 17 | 20 | 171 | 5.59 | 0.25 | 11 | 11 | 1.86 | 782 | 1 | 0.13 | 20 | 0.10 | 2 | 96 | 0.33 | 179 | 73 | |
| 189 | 9000E-12900N | 10 | 0.2 | 5.16 | 2 | 196 | 0.3 | 5 | 2.97 | 0.2 | 30 | 21 | 25 | 151 | 5.92 | 0.27 | 12 | 12 | 2.08 | 849 | 1 | 0.14 | 23 | 0.10 | 2 | 128 | 0.35 | 208 | 75 | |
| 190 | 13000 | 35 | 0.2 | 4.83 | 2 | 231 | 0.3 | 5 | 2.58 | 0.2 | 31 | 20 | 24 | 140 | 5.82 | 0.30 | 12 | 11 | 1.93 | 959 | 2 | 0.14 | 23 | 0.10 | 2 | 100 | 0.32 | 192 | 96 | |
| 191 | 13100 | 60 | 0.2 | 5.17 | 2 | 173 | 0.4 | 5 | 2.78 | 0.2 | 32 | 18 | 23 | 147 | 5.63 | 0.26 | 15 | 13 | 1.74 | 861 | 2 | 0.12 | 20 | 0.12 | 2 | 131 | 0.35 | 195 | 85 | |
| 192 | 9000E-13200N | 10 | 0.2 | 4.34 | 2 | 253 | 0.2 | 5 | 2.36 | 0.2 | 32 | 10 | 20 | 90 | 5.10 | 0.34 | 14 | 8 | 1.51 | 832 | 6 | 0.09 | 11 | 0.10 | 2 | 156 | 0.35 | 227 | 73 | |

| F. No. | SAMPLE No. | ELEMENTS | | | | | | | | | | | | | | | | | | | | | | | | | | | | Zn | 6009-006 |
|-------------|------------|----------|------|----|------|-----|-----|------|-----|-----|-----|-----|-----|------|------|-----|----|------|------|-----|------|-----|------|-----|-----|------|-----|-----|--|----|----------|
| | | Au | Ag | Al | As | Ba | Be | Bi | Cd | Ce | Co | Cr | Cu | Fe | K | La | Li | Mg | Mn | Mo | Na | Ni | P | Pb | Sr | Ti | V | Zn | | | |
| | | ppb | ppm | % | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | ppm | ppm | % | ppm | ppm | ppm | % | ppm | ppm | ppm | | | |
| 2500W-3350N | 370 | 0.6 | 3.55 | 14 | 183 | 0.4 | 5 | 4.45 | 0.4 | 43 | 62 | 51 | 740 | 8.09 | 0.47 | 14 | 13 | 1.36 | 1331 | 5 | 0.08 | 45 | 0.13 | 4 | 172 | 0.25 | 173 | 78 | | | |
| E 3400 | 510 | 1.6 | 3.42 | 14 | 190 | 0.4 | 5 | 4.04 | 0.5 | 44 | 56 | 46 | 858 | 8.31 | 0.50 | 15 | 12 | 1.24 | 1185 | 6 | 0.07 | 36 | 0.13 | 7 | 160 | 0.26 | 155 | 81 | | | |
| E 3450 | 630 | 1.0 | 3.39 | 17 | 181 | 0.4 | 5 | 4.10 | 0.5 | 45 | 54 | 49 | 767 | 8.31 | 0.50 | 16 | 11 | 1.17 | 1145 | 5 | 0.07 | 36 | 0.13 | 6 | 166 | 0.27 | 156 | 75 | | | |
| 2500W-3500N | 340 | 1.0 | 4.28 | 17 | 254 | 0.5 | 5 | 3.79 | 0.8 | 41 | 59 | 52 | 857 | 6.16 | 0.67 | 11 | 16 | 1.90 | 2062 | 6 | 0.06 | 50 | 0.13 | 59 | 148 | 0.25 | 160 | 158 | | | |
| 2900E-3150N | 350 | 0.4 | 6.31 | 11 | 154 | 0.5 | 5 | 3.51 | 0.3 | 42 | 47 | 13 | 497 | 6.30 | 0.41 | 11 | 24 | 2.41 | 1687 | 1 | 0.04 | 23 | 0.10 | 20 | 240 | 0.32 | 207 | 88 | | | |
| 2900E-3200N | 250 | 0.4 | 6.03 | 10 | 113 | 0.4 | 5 | 3.73 | 0.2 | 43 | 45 | 10 | 172 | 6.83 | 0.46 | 12 | 17 | 1.83 | 1084 | 1 | 0.06 | 22 | 0.13 | 2 | 225 | 0.40 | 216 | 52 | | | |
| 3250 | 310 | 0.4 | 5.80 | 16 | 114 | 0.4 | 5 | 3.82 | 0.4 | 42 | 52 | 13 | 232 | 6.52 | 0.38 | 11 | 17 | 1.99 | 1152 | 1 | 0.07 | 24 | 0.12 | 2 | 278 | 0.38 | 207 | 59 | | | |
| 3300 | 70 | 0.2 | 4.98 | 11 | 79 | 0.4 | 5 | 3.20 | 0.2 | 42 | 60 | 41 | 217 | 6.33 | 0.36 | 11 | 17 | 2.53 | 1016 | 1 | 0.10 | 54 | 0.11 | 2 | 215 | 0.31 | 185 | 56 | | | |
| 3350 | 270 | 0.2 | 4.30 | 11 | 96 | 0.3 | 5 | 3.02 | 0.3 | 44 | 50 | 53 | 280 | 6.29 | 0.33 | 12 | 16 | 2.67 | 874 | 1 | 0.13 | 65 | 0.11 | 2 | 255 | 0.31 | 181 | 66 | | | |
| 2900E-3400N | 130 | 0.2 | 4.14 | 11 | 168 | 0.3 | 5 | 2.88 | 0.2 | 46 | 43 | 33 | 408 | 5.57 | 0.40 | 11 | 14 | 1.97 | 806 | 1 | 0.15 | 31 | 0.10 | 2 | 306 | 0.30 | 168 | 57 | | | |
| 2900E-3450N | 160 | 0.4 | 4.76 | 13 | 259 | 0.4 | 5 | 1.47 | 0.2 | 48 | 39 | 28 | 714 | 6.36 | 0.41 | 15 | 18 | 1.80 | 756 | 2 | 0.08 | 33 | 0.19 | 6 | 173 | 0.28 | 165 | 70 | | | |
| 2900E-3500N | 150 | 0.2 | 4.37 | 9 | 260 | 0.3 | 5 | 1.42 | 0.2 | 40 | 43 | 20 | 934 | 6.42 | 0.51 | 12 | 14 | 1.76 | 844 | 1 | 0.05 | 20 | 0.12 | 2 | 181 | 0.30 | 202 | 50 | | | |
| 4400E-1750N | 230 | 1.6 | 5.80 | 15 | 573 | 0.5 | 5 | 1.64 | 0.7 | 50 | 39 | 11 | 345 | 7.64 | 0.94 | 15 | 15 | 1.27 | 2826 | 3 | 0.08 | 12 | 0.21 | 27 | 252 | 0.25 | 191 | 196 | | | |
| 1800 | 110 | 0.8 | 5.75 | 16 | 709 | 0.5 | 5 | 0.75 | 0.6 | 43 | 21 | 13 | 167 | 7.63 | 1.35 | 16 | 14 | 1.30 | 2104 | 4 | 0.11 | 15 | 0.22 | 38 | 132 | 0.21 | 173 | 238 | | | |
| 4400E-1850N | 85 | 1.4 | 5.85 | 20 | 701 | 0.5 | 5 | 1.19 | 1.3 | 48 | 26 | 11 | 167 | 6.81 | 1.22 | 15 | 16 | 1.59 | 2425 | 3 | 0.09 | 16 | 0.17 | 70 | 155 | 0.23 | 172 | 259 | | | |
| 4400E-1900N | 100 | 1.0 | 5.76 | 22 | 697 | 0.5 | 5 | 1.21 | 1.1 | 47 | 24 | 11 | 163 | 6.67 | 1.25 | 15 | 16 | 1.66 | 2200 | 4 | 0.09 | 16 | 0.16 | 66 | 155 | 0.23 | 178 | 251 | | | |
| 1950 | 140 | 0.8 | 5.40 | 21 | 350 | 0.4 | 5 | 1.60 | 1.5 | 50 | 25 | 22 | 134 | 6.30 | 0.96 | 16 | 18 | 1.85 | 2150 | 4 | 0.07 | 20 | 0.13 | 49 | 144 | 0.27 | 185 | 266 | | | |
| 2050 | 70 | 0.4 | 6.16 | 20 | 594 | 0.5 | 5 | 1.42 | 0.7 | 49 | 23 | 18 | 175 | 6.61 | 1.02 | 15 | 20 | 2.05 | 1983 | 4 | 0.08 | 22 | 0.16 | 45 | 114 | 0.28 | 194 | 278 | | | |
| 2100 | 100 | 0.2 | 6.43 | 26 | 589 | 0.6 | 5 | 0.96 | 0.7 | 40 | 25 | 15 | 190 | 6.25 | 1.14 | 12 | 19 | 2.04 | 2869 | 4 | 0.08 | 21 | 0.18 | 39 | 78 | 0.24 | 185 | 263 | | | |
| 4400E-2150N | 15 | 0.2 | 5.35 | 21 | 335 | 0.3 | 5 | 1.95 | 0.3 | 50 | 16 | 19 | 64 | 5.31 | 0.64 | 13 | 14 | 1.50 | 1270 | 1 | 0.07 | 15 | 0.11 | 10 | 214 | 0.27 | 187 | 97 | | | |
| 4400E-2200N | 80 | 0.2 | 5.08 | 22 | 369 | 0.3 | 5 | 1.89 | 0.5 | 52 | 17 | 19 | 107 | 5.47 | 0.65 | 14 | 14 | 1.39 | 1164 | 2 | 0.08 | 17 | 0.16 | 12 | 154 | 0.27 | 167 | 112 | | | |
| 2250 | 120 | 0.4 | 6.59 | 9 | 633 | 0.5 | 5 | 1.14 | 0.8 | 38 | 23 | 25 | 208 | 6.49 | 1.19 | 12 | 20 | 2.00 | 2126 | 4 | 0.08 | 21 | 0.17 | 53 | 102 | 0.26 | 183 | 301 | | | |
| 2300 | 160 | 0.4 | 4.61 | 12 | 278 | 0.3 | 5 | 1.89 | 0.5 | 46 | 22 | 31 | 200 | 5.97 | 0.56 | 12 | 13 | 1.38 | 1268 | 2 | 0.06 | 16 | 0.14 | 11 | 135 | 0.25 | 166 | 117 | | | |
| 2350 | 75 | 0.2 | 4.45 | 5 | 207 | 0.3 | 5 | 1.19 | 0.2 | 40 | 6 | 29 | 48 | 5.73 | 0.36 | 11 | 9 | 1.00 | 660 | 2 | 0.05 | 10 | 0.18 | 15 | 82 | 0.32 | 158 | 78 | | | |
| 4400E-2400N | 270 | 0.8 | 5.21 | 15 | 265 | 0.6 | 5 | 1.60 | 0.7 | 47 | 35 | 92 | 292 | 6.13 | 0.48 | 13 | 18 | 2.26 | 2465 | 2 | 0.07 | 48 | 0.21 | 19 | 88 | 0.22 | 159 | 179 | | | |
| 4400E-2450N | 50 | 0.4 | 4.94 | 7 | 201 | 0.3 | 5 | 1.48 | 0.4 | 44 | 9 | 47 | 29 | 3.78 | 0.41 | 11 | 10 | 1.04 | 548 | 1 | 0.06 | 18 | 0.19 | 5 | 100 | 0.36 | 144 | 73 | | | |
| 2500 | 5 | 0.6 | 4.76 | 12 | 203 | 0.4 | 5 | 1.49 | 0.5 | 44 | 14 | 44 | 60 | 4.73 | 0.41 | 12 | 12 | 1.23 | 1129 | 2 | 0.06 | 18 | 0.20 | 3 | 103 | 0.34 | 157 | 91 | | | |
| 2550 | 110 | 0.2 | 4.49 | 63 | 173 | 0.5 | 5 | 1.46 | 0.4 | 47 | 17 | 32 | 62 | 5.06 | 0.34 | 14 | 19 | 1.69 | 1177 | 2 | 0.07 | 19 | 0.16 | 3 | 79 | 0.32 | 179 | 121 | | | |
| 2600 | 30 | 0.2 | 4.43 | 22 | 187 | 0.3 | 5 | 1.60 | 0.4 | 44 | 12 | 37 | 78 | 4.09 | 0.34 | 11 | 11 | 1.17 | 646 | 1 | 0.07 | 19 | 0.19 | 2 | 102 | 0.26 | 134 | 85 | | | |
| 4400E-2650N | 270 | 0.2 | 4.81 | 69 | 247 | 0.7 | 5 | 1.65 | 0.2 | 47 | 19 | 41 | 109 | 4.93 | 0.45 | 12 | 19 | 1.62 | 1417 | 2 | 0.07 | 29 | 0.26 | 6 | 108 | 0.28 | 173 | 127 | | | |
| 4400E-2700N | 110 | 0.2 | 5.31 | 23 | 406 | 0.6 | 5 | 1.58 | 0.5 | 48 | 25 | 49 | 180 | 5.14 | 0.54 | 13 | 18 | 2.04 | 1546 | 1 | 0.09 | 40 | 0.15 | 8 | 179 | 0.27 | 165 | 102 | | | |
| 2750 | 60 | 0.2 | 5.00 | 16 | 321 | 0.7 | 5 | 1.45 | 0.2 | 42 | 22 | 57 | 154 | 4.90 | 0.46 | 12 | 18 | 1.78 | 1314 | 1 | 0.08 | 37 | 0.15 | 4 | 158 | 0.26 | 157 | 104 | | | |
| 2800 | 200 | 0.2 | 4.95 | 8 | 550 | 0.5 | 5 | 1.96 | 0.2 | 47 | 26 | 45 | 212 | 5.32 | 0.54 | 13 | 19 | 2.20 | 1482 | 1 | 0.11 | 37 | 0.12 | 5 | 230 | 0.30 | 177 | 99 | | | |
| 2850 | 320 | 1.0 | 5.55 | 9 | 926 | 0.6 | 5 | 1.53 | 0.4 | 51 | 24 | 38 | 220 | 5.54 | 0.74 | 15 | 20 | 2.15 | 1906 | 1 | 0.09 | 32 | 0.15 | 6 | 206 | 0.26 | 174 | 102 | | | |
| 4400E-2900N | 110 | 0.2 | 4.45 | 15 | 292 | 0.4 | 5 | 2.19 | 0.3 | 48 | 27 | 56 | 200 | 5.29 | 0.44 | 13 | 17 | 2.26 | 1263 | 1 | 0.12 | 42 | 0.12 | 3 | 190 | 0.33 | 176 | 96 | | | |
| 4400E-2950N | 35 | 0.2 | 4.99 | 12 | 354 | 0.4 | 5 | 1.84 | 0.4 | 46 | 28 | 53 | 191 | 5.34 | 0.46 | 12 | 17 | 1.92 | 1474 | 1 | 0.09 | 33 | 0.16 | 5 | 171 | 0.33 | 184 | 101 | | | |
| 3000 | 30 | 0.2 | 4.95 | 13 | 402 | 0.5 | 5 | 1.67 | 0.3 | 46 | 22 | 42 | 129 | 4.94 | 0.45 | 13 | 17 | 1.61 | 1538 | 1 | 0.08 | 29 | 0.20 | 10 | 167 | 0.32 | 176 | 102 | | | |
| 3050 | 25 | 0.2 | 4.95 | 7 | 370 | 0.5 | 5 | 1.50 | 0.4 | 52 | 28 | 29 | 246 | 4.49 | 0.49 | 15 | 23 | 1.91 | 1249 | 1 | 0.08 | 25 | 0.16 | 7 | 337 | 0.29 | 167 | 93 | | | |
| 4400E-3150N | 170 | 0.6 | 6.32 | 8 | 1330 | 3.1 | 5 | 0.41 | 0.2 | 62 | 19 | 10 | 54 | 7.08 | 2.07 | 30 | 18 | 0.90 | 2294 | 1 | 0.07 | 20 | 0.18 | 17 | 37 | 0.08 | 125 | 190 | | | |
| 5600E-2150N | 10 | 0.2 | 4.70 | 10 | 180 | 0.3 | 5 | 1.01 | 0.2 | 37 | 11 | 36 | 79 | 4.48 | 0.28 | 9 | 10 | 0.95 | 606 | 2 | 0.05 | 18 | 0.20 | 6 | 76 | 0.26 | 127 | 80 | | | |
| 5600E-2200N | 25 | 0.2 | 4.78 | 18 | 235 | 0.3 | 5 | 2.41 | 0.3 | 47 | 25 | 36 | 189 | 5.30 | 0.34 | 12 | 14 | 1.90 | 895 | 2 | 0.09 | 31 | 0.12 | 4 | 179 | 0.35 | 184 | 99 | | | |
| 2250 | 20 | 0.2 | 4.79 | 9 | 362 | 0.3 | 5 | 2.06 | 0.3 | 42 | 16 | 28 | 105 | 4.52 | 0.45 | 12 | 12 | 1.43 | 939 | 1 | 0.08 | 21 | 0.14 | 3 | 239 | 0.28 | 160 | 87 | | | |
| 2300 | 10 | 0.2 | 4.00 | 7 | 211 | 0.3 | 5 | 1.78 | 0.3 | 42 | 18 | 23 | 146 | 3.86 | 0.33 | 11 | 9 | 1.17 | 917 | 1 | 0.08 | 18 | 0.14 | 2 | 127 | 0.25 | 137 | 76 | | | |
| 2350 | 70 | 0.2 | 5.21 | 11 | 218 | 0.3 | 5 | 2.16 | 0.3 | 45 | 19 | 25 | 205 | 5.05 | 0.35 | 13 | 12 | 1.49 | 781 | 2 | 0.09 | 22 | 0.15 | 2 | 134 | 0.33 | 172 | 78 | | | |
| 5600E-2400N | 40 | 0.2 | 5.22 | 14 | 281 | 0.3 | 5 | 2.43 | 0.3 | 49 | 28 | 22 | 388 | 5.54 | 0.48 | 14 | 13 | 1.76 | 1011 | 2 | 0.10 | 25 | 0.15 | 5 | 181 | 0.33 | 190 | 90 | | | |

Sch
↓

ELI
Crcy

Sch
↓

Crcy
↓

| SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Bc ppm | Bi ppm | Ca % | Cl ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm | 9306-005 Pa. 3 of 7 |
|---------------|--------|--------|------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|---------------------|
| 5600E-2450N | 35 | 0.2 | 5.16 | 13 | 232 | 0.3 | 5 | 2.46 | 0.2 | 49 | 13 | 23 | 389 | 5.79 | 0.39 | 13 | 11 | 1.41 | 738 | 3 | 0.08 | 18 | 0.15 | 2 | 166 | 0.36 | 187 | 74 | Croy |
| 2500 | 20 | 1.0 | 2.55 | 2 | 164 | 0.2 | 5 | 1.31 | 0.2 | 38 | 3 | 21 | 30 | 1.88 | 0.31 | 10 | 4 | 0.27 | 240 | 1 | 0.04 | 6 | 0.19 | 4 | 110 | 0.23 | 93 | 31 | |
| 2550 | 10 | 0.2 | 4.69 | 7 | 201 | 0.3 | 5 | 2.91 | 0.2 | 47 | 19 | 16 | 163 | 5.02 | 0.45 | 14 | 13 | 1.77 | 879 | 1 | 0.10 | 24 | 0.12 | 6 | 171 | 0.34 | 195 | 80 | |
| 2600 | 200 | 0.2 | 3.91 | 8 | 177 | 0.2 | 5 | 1.96 | 0.2 | 46 | 10 | 27 | 33 | 4.26 | 0.36 | 13 | 8 | 0.99 | 517 | 1 | 0.08 | 15 | 0.11 | 5 | 130 | 0.39 | 188 | 58 | |
| 5600E-2650N | 10 | 0.6 | 2.67 | 3 | 117 | 0.2 | 5 | 1.72 | 0.2 | 43 | 3 | 19 | 28 | 2.87 | 0.23 | 11 | 5 | 0.68 | 333 | 1 | 0.06 | 9 | 0.17 | 3 | 89 | 0.45 | 172 | 35 | |
| 5600E-2700N | 20 | 0.2 | 6.27 | 20 | 115 | 0.4 | 5 | 0.71 | 0.3 | 29 | 10 | 28 | 60 | 3.74 | 0.16 | 8 | 8 | 0.70 | 560 | 1 | 0.04 | 13 | 0.23 | 3 | 43 | 0.16 | 94 | 71 | |
| 2750 | 60 | 0.2 | 3.73 | 2 | 194 | 0.2 | 5 | 1.63 | 0.2 | 42 | 7 | 34 | 25 | 3.66 | 0.40 | 11 | 8 | 0.71 | 552 | 1 | 0.06 | 11 | 0.14 | 2 | 138 | 0.42 | 184 | 56 | |
| 2800 | 260 | 0.2 | 4.08 | 2 | 211 | 0.3 | 5 | 1.88 | 0.2 | 45 | 9 | 32 | 73 | 4.09 | 0.41 | 12 | 9 | 1.04 | 560 | 1 | 0.06 | 14 | 0.20 | 2 | 145 | 0.38 | 156 | 66 | |
| 2850 | 10 | 0.2 | 4.16 | 2 | 149 | 0.3 | 5 | 1.12 | 0.2 | 36 | 6 | 34 | 64 | 3.64 | 0.31 | 9 | 8 | 0.76 | 456 | 1 | 0.04 | 13 | 0.17 | 2 | 89 | 0.32 | 129 | 53 | |
| 5600E-2900N | 20 | 0.2 | 3.41 | 3 | 210 | 0.3 | 5 | 1.45 | 0.2 | 40 | 9 | 33 | 43 | 3.85 | 0.40 | 10 | 8 | 0.91 | 604 | 1 | 0.05 | 17 | 0.23 | 2 | 113 | 0.30 | 142 | 59 | |
| 5600E-2950N | 20 | 0.2 | 4.10 | 2 | 244 | 0.4 | 5 | 1.30 | 0.2 | 40 | 13 | 23 | 78 | 4.77 | 0.47 | 10 | 11 | 1.27 | 732 | 2 | 0.05 | 16 | 0.18 | 7 | 108 | 0.31 | 169 | 84 | |
| 3000 | 15 | 0.4 | 4.45 | 6 | 243 | 0.3 | 5 | 1.43 | 0.2 | 41 | 14 | 24 | 95 | 4.88 | 0.39 | 10 | 12 | 1.47 | 773 | 2 | 0.06 | 19 | 0.15 | 2 | 116 | 0.30 | 163 | 95 | Sch |
| 3050 | 35 | 0.2 | 4.86 | 5 | 342 | 0.3 | 5 | 1.44 | 0.3 | 42 | 9 | 36 | 62 | 4.70 | 0.52 | 11 | 10 | 1.06 | 706 | 1 | 0.08 | 16 | 0.17 | 4 | 129 | 0.31 | 190 | 76 | |
| 3100 | 5 | 0.2 | 3.70 | 6 | 347 | 0.3 | 5 | 1.66 | 0.2 | 41 | 21 | 35 | 89 | 5.63 | 0.31 | 10 | 12 | 1.88 | 1134 | 1 | 0.06 | 23 | 0.22 | 3 | 130 | 0.36 | 232 | 106 | |
| 5600E-3150N | 1200 | 0.2 | 3.95 | 2 | 247 | 0.3 | 5 | 1.52 | 0.8 | 37 | 13 | 36 | 62 | 5.15 | 0.29 | 10 | 13 | 1.36 | 1076 | 1 | 0.05 | 18 | 0.27 | 2 | 103 | 0.39 | 171 | 123 | |
| 6000E-2000N | 20 | 0.2 | 5.77 | 3 | 309 | 0.5 | 5 | 1.51 | 0.2 | 42 | 36 | 43 | 334 | 7.15 | 0.41 | 13 | 21 | 3.05 | 1649 | 2 | 0.06 | 55 | 0.13 | 7 | 139 | 0.40 | 230 | 130 | Croy |
| 2050 A | 10 | 0.2 | 1.80 | 2 | 173 | 0.2 | 5 | 1.46 | 0.4 | 33 | 6 | 20 | 30 | 1.91 | 0.27 | 7 | 4 | 0.37 | 447 | 1 | 0.04 | 8 | 0.17 | 3 | 103 | 0.24 | 107 | 74 | |
| 2100 | 40 | 0.2 | 5.75 | 15 | 319 | 0.5 | 5 | 1.92 | 0.4 | 49 | 37 | 33 | 421 | 6.26 | 0.63 | 14 | 21 | 2.19 | 1276 | 2 | 0.09 | 52 | 0.13 | 9 | 145 | 0.35 | 200 | 132 | |
| 2150 | 15 | 0.2 | 5.95 | 10 | 319 | 0.5 | 5 | 1.78 | 0.7 | 40 | 60 | 34 | 694 | 7.90 | 0.40 | 12 | 22 | 3.30 | 1526 | 6 | 0.07 | 66 | 0.14 | 10 | 184 | 0.32 | 204 | 123 | |
| 6000E-2200N | 20 | 0.2 | 5.11 | 10 | 279 | 0.5 | 5 | 1.70 | 0.4 | 42 | 43 | 32 | 554 | 6.65 | 0.43 | 11 | 17 | 2.08 | 2298 | 12 | 0.07 | 40 | 0.20 | 12 | 138 | 0.30 | 187 | 116 | |
| 6000E-2250N | 5 | 0.2 | 2.80 | 2 | 121 | 0.2 | 5 | 1.04 | 0.4 | 30 | 8 | 144 | 50 | 2.79 | 0.31 | 8 | 9 | 1.41 | 302 | 1 | 0.04 | 84 | 0.18 | 2 | 102 | 0.32 | 121 | 47 | |
| 2300 | 5 | 0.2 | 4.01 | 3 | 103 | 0.2 | 5 | 2.11 | 0.4 | 44 | 13 | 32 | 125 | 5.35 | 0.22 | 10 | 8 | 1.45 | 527 | 2 | 0.08 | 21 | 0.11 | 2 | 131 | 0.52 | 233 | 49 | |
| 2350 | 15 | 0.2 | 4.50 | 5 | 228 | 0.4 | 5 | 2.33 | 0.6 | 50 | 21 | 29 | 441 | 4.93 | 0.40 | 15 | 14 | 1.42 | 875 | 8 | 0.07 | 23 | 0.15 | 6 | 163 | 0.37 | 176 | 80 | |
| 2400 | 20 | 1.6 | 4.64 | 8 | 246 | 0.5 | 5 | 1.95 | 0.9 | 48 | 20 | 25 | 444 | 4.36 | 0.46 | 15 | 15 | 1.40 | 656 | 5 | 0.07 | 28 | 0.14 | 7 | 143 | 0.36 | 165 | 94 | |
| 6000E-2450N | 15 | 0.2 | 4.25 | 3 | 176 | 0.2 | 5 | 1.67 | 0.2 | 42 | 9 | 30 | 56 | 4.68 | 0.31 | 12 | 10 | 1.08 | 632 | 1 | 0.06 | 14 | 0.17 | 2 | 140 | 0.43 | 183 | 55 | |
| 6000E-2500N | 250 | 0.2 | 3.58 | 2 | 178 | 0.2 | 5 | 1.61 | 0.4 | 43 | 6 | 21 | 25 | 4.26 | 0.36 | 11 | 7 | 0.82 | 411 | 2 | 0.05 | 10 | 0.15 | 2 | 146 | 0.47 | 185 | 44 | |
| 2550 | 90 | 0.2 | 3.34 | 2 | 267 | 0.2 | 5 | 1.14 | 0.2 | 41 | 18 | 20 | 69 | 5.38 | 0.47 | 11 | 8 | 0.89 | 1484 | 10 | 0.05 | 11 | 0.19 | 9 | 121 | 0.40 | 236 | 76 | |
| 2600 | 15 | 0.2 | 4.34 | 8 | 190 | 0.5 | 5 | 1.83 | 0.2 | 49 | 15 | 25 | 249 | 4.96 | 0.36 | 16 | 18 | 1.44 | 900 | 6 | 0.07 | 19 | 0.29 | 2 | 124 | 0.33 | 172 | 87 | |
| 2650 | 5 | 0.2 | 3.32 | 2 | 136 | 0.2 | 5 | 2.15 | 0.2 | 46 | 5 | 22 | 27 | 3.82 | 0.30 | 12 | 7 | 0.86 | 417 | 3 | 0.07 | 12 | 0.14 | 2 | 147 | 0.44 | 173 | 47 | |
| 6000E-2700N | 15 | 0.2 | 4.30 | 6 | 309 | 0.4 | 5 | 1.99 | 0.5 | 51 | 22 | 17 | 163 | 5.86 | 0.58 | 15 | 17 | 2.32 | 1124 | 2 | 0.06 | 20 | 0.18 | 2 | 159 | 0.46 | 241 | 91 | |
| 6000E-2750N | 5 | 0.2 | 3.52 | 2 | 182 | 0.2 | 5 | 2.00 | 0.4 | 47 | 8 | 17 | 32 | 3.69 | 0.30 | 12 | 8 | 1.18 | 402 | 2 | 0.06 | 13 | 0.10 | 4 | 182 | 0.56 | 204 | 45 | |
| 2800 | 5 | 0.2 | 4.38 | 5 | 213 | 0.3 | 5 | 1.67 | 0.5 | 49 | 13 | 20 | 121 | 5.14 | 0.36 | 13 | 15 | 1.39 | 1281 | 9 | 0.04 | 16 | 0.18 | 4 | 163 | 0.54 | 244 | 84 | |
| 3000 | 30 | 0.2 | 2.61 | 2 | 194 | 0.2 | 5 | 1.94 | 0.4 | 46 | 2 | 19 | 18 | 1.81 | 0.31 | 11 | 5 | 0.32 | 248 | 4 | 0.05 | 6 | 0.10 | 8 | 132 | 0.37 | 125 | 33 | |
| 3050 | 15 | 0.2 | 4.40 | 7 | 176 | 0.3 | 5 | 1.67 | 0.7 | 44 | 11 | 44 | 59 | 5.47 | 0.33 | 12 | 12 | 1.23 | 528 | 2 | 0.06 | 21 | 0.12 | 4 | 123 | 0.37 | 181 | 63 | Sch |
| 6000E-3100N | 15 | 0.2 | 2.41 | 2 | 157 | 0.2 | 5 | 0.96 | 0.2 | 30 | 7 | 29 | 71 | 2.69 | 0.25 | 8 | 6 | 0.65 | 318 | 1 | 0.05 | 11 | 0.19 | 2 | 99 | 0.22 | 109 | 42 | |
| 6000E-3150N | 15 | 0.2 | 6.02 | 8 | 309 | 0.5 | 5 | 1.16 | 0.4 | 38 | 35 | 43 | 200 | 6.63 | 0.44 | 12 | 21 | 2.69 | 1541 | 1 | 0.06 | 36 | 0.18 | 14 | 103 | 0.35 | 212 | 144 | |
| 3200 | 150 | 0.2 | 3.75 | 2 | 227 | 0.3 | 5 | 1.19 | 0.2 | 35 | 21 | 36 | 134 | 5.07 | 0.38 | 10 | 11 | 1.54 | 1775 | 1 | 0.05 | 21 | 0.22 | 3 | 115 | 0.33 | 184 | 81 | |
| 3250 | 60 | 0.4 | 5.21 | 8 | 304 | 0.4 | 5 | 2.07 | 0.2 | 47 | 31 | 39 | 537 | 7.07 | 0.49 | 13 | 15 | 2.05 | 1389 | 3 | 0.07 | 31 | 0.15 | 2 | 164 | 0.36 | 217 | 104 | |
| 6000E-3300N | 30 | 0.2 | 5.14 | 3 | 274 | 0.4 | 5 | 1.86 | 0.2 | 46 | 29 | 43 | 240 | 6.26 | 0.36 | 12 | 15 | 2.16 | 1582 | 2 | 0.06 | 28 | 0.15 | 8 | 159 | 0.38 | 223 | 110 | |
| 10000E-10000N | 5 | 0.2 | 5.54 | 9 | 316 | 0.3 | 5 | 1.77 | 0.7 | 44 | 19 | 50 | 76 | 5.90 | 0.40 | 12 | 18 | 1.72 | 957 | 2 | 0.06 | 33 | 0.11 | 2 | 210 | 0.40 | 225 | 98 | Croy |
| 10000E-10050N | 5 | 0.6 | 5.40 | 7 | 285 | 0.4 | 5 | 1.95 | 0.6 | 44 | 26 | 68 | 68 | 6.17 | 0.30 | 12 | 17 | 1.73 | 2168 | 2 | 0.05 | 35 | 0.16 | 2 | 232 | 0.48 | 241 | 115 | |
| 10100 | 5 | 0.4 | 5.39 | 3 | 224 | 0.2 | 5 | 2.68 | 0.2 | 46 | 7 | 23 | 36 | 4.54 | 0.38 | 12 | 7 | 0.74 | 492 | 2 | 0.04 | 14 | 0.10 | 2 | 250 | 0.45 | 243 | 71 | |
| 10150 | 5 | 0.2 | 5.15 | 4 | 148 | 0.3 | 5 | 1.90 | 0.2 | 42 | 12 | 38 | 40 | 6.55 | 0.28 | 10 | 13 | 1.36 | 584 | 1 | 0.04 | 26 | 0.08 | 2 | 160 | 0.58 | 276 | 77 | |
| 10200 | 5 | 0.4 | 6.56 | 9 | 253 | 0.6 | 5 | 1.67 | 0.2 | 46 | 23 | 81 | 82 | 7.13 | 0.54 | 16 | 35 | 2.15 | 1159 | 2 | 0.04 | 57 | 0.12 | 3 | 154 | 0.33 | 275 | 112 | |
| 10000E-10250N | 5 | 0.2 | 5.37 | 6 | 213 | 0.3 | 5 | 1.91 | 0.2 | 43 | 10 | 46 | 43 | 5.50 | 0.30 | 12 | 15 | 1.18 | 578 | 1 | 0.05 | 22 | 0.12 | 2 | 184 | 0.42 | 209 | 79 | |

APPENDIX III

ROCK GEOCHEMICAL DESCRIPTIONS/ASSAY SHEETS

NORANDA DELTA LABORATORY

Geochemical Analysis

Project Name & No.: **KLJUL - 148**

Material: **59 Rx**

Remarks: * Sample screened @ -35 MESH (0.5 mm)

□ Organic, & Humus, & Sulfide

Geol.: T.W.
Sheet: 1 of 2

Date received: SEP. 17
Date completed: OCT. 05

LAB CODE: 9309-033

Au - 10.0 g sample digested with aqua-regia and determined by A.A. (D.L. 5 PPB)

ICP - 0.2 g sample digested with 3 ml HClO₄/HNO₃ (4:1) at 203 °C for 4 hours diluted to 10 ml with water. Leeman PS3000 ICP determined elemental contents.

N.B. The major oxide elements and Ba, Be, Ce, La, Li, Ga are rarely dissolved completely from geological materials with this acid dissolution method.

| T. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Bc ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Tl % | V ppm | Zn ppm |
|----|------------|--------|--------|------|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------|-------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|
| 6 | 389 - A | 20 | 0.2 | 5.12 | 2 | 232 | 0.2 | 7 | 0.89 | 0.2 | 36 | 16 | 21 | 161 | 5.28 | 0.70 | 9 | 15 | 2.68 | 728 | 1 | 0.25 | 8 | 0.05 | 3 | 69 | 0.30 | 196 | 204 |
| 7 | B | 530 | 0.4 | 3.23 | 16 | 189 | 0.3 | 5 | 1.04 | 0.2 | 45 | 17 | 85 | 389 | 22.65 | 1.00 | 9 | 5 | 0.56 | 439 | 1 | 0.04 | 15 | 0.10 | 14 | 80 | 0.19 | 184 | 56 |
| 8 | C | 10 | 0.2 | 6.77 | 2 | 51 | 0.3 | 8 | 5.92 | 0.2 | 77 | 37 | 18 | 288 | 6.15 | 0.08 | 12 | 15 | 2.42 | 1359 | 1 | 0.08 | 13 | 0.09 | 3 | 373 | 0.38 | 233 | 127 |
| 1 | D | 5 | 0.2 | 1.74 | 2 | 456 | 0.8 | 5 | 0.40 | 0.3 | 28 | 14 | 57 | 27 | 4.04 | 0.52 | 11 | 18 | 0.96 | 806 | 1 | 0.09 | 26 | 0.18 | 2 | 27 | 0.04 | 188 | 96 |
| 2 | F | 320 | 0.2 | 0.06 | 2 | 4 | 0.2 | 5 | 0.01 | 0.2 | 5 | 1 | 341 | 24 | 1.21 | 0.01 | 1 | 1 | 0.01 | 27 | 469 | 0.01 | 2 | 0.01 | 2 | 1 | 0.01 | 4 | 3 |
| 3 | G | 5 | 0.2 | 4.31 | 2 | 1252 | 0.4 | 5 | 1.39 | 0.2 | 71 | 9 | 35 | 40 | 4.31 | 1.59 | 23 | 8 | 1.05 | 863 | 1 | 0.08 | 7 | 0.15 | 2 | 209 | 0.21 | 118 | 67 |
| 4 | H | 20 | 0.2 | 2.51 | 2 | 213 | 0.2 | 5 | 1.44 | 0.2 | 45 | 23 | 41 | 90 | 6.25 | 0.81 | 8 | 10 | 1.63 | 727 | 1 | 0.14 | 10 | 0.07 | 2 | 44 | 0.30 | 174 | 56 |
| 5 | I | 310 | 0.2 | 4.39 | 18 | 597 | 0.2 | 5 | 0.89 | 0.2 | 28 | 24 | 38 | 346 | 6.66 | 1.60 | 5 | 6 | 0.65 | 454 | 2 | 0.06 | 9 | 0.05 | 14 | 14 | 0.17 | 149 | 52 |
| 6 | J | 990 | 4.8 | 1.08 | 52 | 11 | 0.2 | 5 | 0.32 | 0.2 | 28 | 72 | 95 | 2750 | 17.54 | 0.05 | 11 | 2 | 0.49 | 460 | 1 | 0.01 | 10 | 0.04 | 2 | 4 | 0.02 | 33 | 74 |
| 8 | K | 6700 | 14.4 | 0.11 | 2 | 2 | 0.2 | 5 | 0.01 | 0.2 | 5 | 5 | 384 | 329 | 5.80 | 0.01 | 1 | 1 | 0.01 | 37 | 29 | 0.01 | 4 | 0.01 | 2 | 1 | 0.01 | 5 | 6 |
| 9 | L | 30 | 9.2 | 4.04 | 2 | 268 | 0.2 | 5 | 2.43 | 0.2 | 55 | 8 | 39 | 116 | 4.42 | 0.85 | 10 | 10 | 1.41 | 761 | 1 | 0.10 | 6 | 0.07 | 2 | 122 | 0.24 | 112 | 55 |
| 0 | M | 5700 | 0.2 | 0.42 | 2 | 30 | 0.2 | 5 | 0.05 | 0.2 | 7 | 10 | 238 | 2145 | 7.84 | 0.10 | 2 | 1 | 0.22 | 115 | 1 | 0.05 | 5 | 0.02 | 15 | 3 | 0.05 | 56 | 16 |
| 1 | N | 5 | 0.2 | 5.64 | 2 | 664 | 0.2 | 5 | 0.90 | 0.2 | 42 | 14 | 27 | 53 | 5.98 | 2.07 | 12 | 12 | 1.10 | 811 | 1 | 0.10 | 5 | 0.11 | 11 | 113 | 0.25 | 188 | 98 |
| 2 | O | 5 | 0.2 | 3.80 | 2 | 161 | 0.2 | 5 | 3.01 | 0.2 | 62 | 12 | 23 | 9 | 4.16 | 0.86 | 12 | 11 | 1.34 | 954 | 1 | 0.10 | 7 | 0.07 | 2 | 95 | 0.26 | 153 | 55 |
| 3 | P | 40 | 0.2 | 3.35 | 2 | 81 | 0.2 | 5 | 5.50 | 0.2 | 70 | 8 | 24 | 80 | 4.19 | 0.56 | 9 | 7 | 0.61 | 1513 | 1 | 0.13 | 6 | 0.08 | 2 | 123 | 0.35 | 179 | 52 |
| 4 | Q | 2000 | 8.8 | 1.68 | 4 | 94 | 0.2 | 7 | 4.44 | 0.2 | 70 | 439 | 27 | 11000 | 10.55 | 0.21 | 13 | 6 | 0.36 | 979 | 6 | 0.02 | 16 | 0.06 | 4 | 117 | 0.07 | 67 | 36 |
| 5 | R | 10 | 0.2 | 5.81 | 2 | 500 | 0.2 | 5 | 1.32 | 0.2 | 47 | 11 | 31 | 88 | 5.84 | 1.89 | 11 | 11 | 1.65 | 1488 | 1 | 0.10 | 13 | 0.06 | 21 | 62 | 0.38 | 228 | 186 |
| 6 | S | 5 | 0.2 | 3.40 | 2 | 576 | 0.3 | 5 | 2.06 | 0.2 | 82 | 8 | 24 | 31 | 2.57 | 1.08 | 28 | 11 | 0.87 | 499 | 1 | 0.11 | 9 | 0.09 | 8 | 70 | 0.14 | 69 | 62 |
| 7 | T | 8300 | 8.0 | 1.82 | 2 | 519 | 0.2 | 5 | 0.03 | 0.2 | 16 | 4 | 204 | 250 | 14.09 | 0.81 | 6 | 2 | 0.17 | 258 | 5 | 0.04 | 3 | 0.08 | 11 | 5 | 0.06 | 106 | 203 |
| 8 | U | 20 | 0.2 | 2.54 | 2 | 398 | 0.3 | 5 | 0.16 | 0.2 | 22 | 6 | 131 | 56 | 2.76 | 0.59 | 8 | 15 | 0.55 | 150 | 1 | 0.08 | 5 | 0.07 | 130 | 17 | 0.01 | 55 | 131 |
| 9 | V | 50 | 0.2 | 4.77 | 2 | 1031 | 0.6 | 8 | 0.37 | 0.2 | 46 | 35 | 36 | 13000 | 4.13 | 1.32 | 16 | 12 | 1.49 | 933 | 1 | 0.11 | 9 | 0.11 | 3 | 24 | 0.05 | 124 | 199 |
| 0 | 389 - W | 40 | 0.8 | 3.75 | 2 | 850 | 0.3 | 5 | 0.87 | 0.2 | 44 | 13 | 30 | 2907 | 3.34 | 0.87 | 11 | 10 | 0.98 | 825 | 1 | 0.14 | 9 | 0.07 | 2 | 86 | 0.06 | 90 | 135 |
| 1 | 390 - A | 5 | 0.2 | 2.43 | 2 | 749 | 1.5 | 5 | 1.80 | 0.3 | 46 | 8 | 22 | 46 | 2.45 | 1.38 | 11 | 6 | 0.60 | 597 | 1 | 0.09 | 12 | 0.12 | 2 | 104 | 0.03 | 135 | 45 |
| 2 | B | 5 | 0.2 | 5.19 | 2 | 160 | 0.2 | 5 | 3.10 | 0.2 | 54 | 25 | 14 | 52 | 6.53 | 0.33 | 7 | 20 | 2.26 | 1084 | 1 | 0.11 | 11 | 0.06 | 2 | 372 | 0.40 | 179 | 82 |
| 3 | C | 5 | 0.2 | 2.03 | 10 | 22 | 0.3 | 5 | 17.47 | 0.2 | 51 | 12 | 21 | 51 | 2.73 | 0.08 | 1 | 9 | 0.79 | 754 | 2 | 0.13 | 11 | 0.10 | 2 | 386 | 0.27 | 94 | 36 |
| 4 | O | 5 | 0.2 | 5.15 | 2 | 108 | 0.2 | 5 | 4.53 | 0.2 | 59 | 21 | 37 | 42 | 4.93 | 0.31 | 7 | 9 | 0.97 | 464 | 1 | 0.30 | 21 | 0.07 | 2 | 255 | 0.49 | 112 | 44 |
| 5 | E | 5 | 0.2 | 1.96 | 2 | 327 | 1.0 | 5 | 2.28 | 0.2 | 56 | 15 | 52 | 186 | 4.11 | 0.67 | 13 | 21 | 1.56 | 643 | 1 | 0.12 | 34 | 0.17 | 9 | 104 | 0.05 | 183 | 61 |
| 6 | G | 5 | 0.2 | 6.65 | 2 | 13 | 0.2 | 5 | 8.09 | 0.2 | 65 | 20 | 16 | 89 | 4.64 | 0.04 | 5 | 10 | 1.28 | 783 | 1 | 0.07 | 12 | 0.06 | 2 | 174 | 0.33 | 177 | 48 |
| 7 | H | 5 | 0.2 | 1.74 | 40 | 19 | 0.6 | 5 | 7.64 | 0.2 | 74 | 24 | 33 | 566 | 23.55 | 0.04 | 10 | 5 | 0.50 | 2531 | 4 | 0.03 | 55 | 0.10 | 17 | 41 | 0.07 | 59 | 118 |
| 8 | I | 5 | 0.2 | 5.43 | 2 | 507 | 0.3 | 5 | 3.65 | 0.2 | 58 | 27 | 21 | 201 | 5.77 | 0.74 | 10 | 36 | 2.07 | 1424 | 1 | 0.38 | 13 | 0.08 | 2 | 118 | 0.09 | 177 | 123 |
| 9 | J | 5 | 0.2 | 3.58 | 2 | 70 | 0.2 | 5 | 2.39 | 0.2 | 50 | 23 | 43 | 28 | 6.79 | 0.45 | 8 | 8 | 1.28 | 422 | 1 | 0.31 | 12 | 0.04 | 2 | 89 | 0.26 | 172 | 27 |
| 0 | K | 5 | 0.2 | 7.25 | 2 | 195 | 0.3 | 5 | 4.67 | 0.2 | 62 | 18 | 35 | 124 | 4.93 | 0.97 | 10 | 18 | 1.78 | 1020 | 1 | 0.37 | 11 | 0.10 | 5 | 69 | 0.31 | 146 | 83 |
| 1 | L | 5 | 0.2 | 2.48 | 2 | 232 | 0.2 | 5 | 0.33 | 0.2 | 26 | 17 | 69 | 16 | 5.96 | 0.70 | 10 | 11 | 1.63 | 370 | 1 | 0.12 | 9 | 0.07 | 2 | 21 | 0.12 | 166 | 43 |
| 2 | M | 5 | 0.2 | 1.40 | 2 | 74 | 0.2 | 5 | 0.47 | 0.2 | 29 | 13 | 58 | 14 | 6.08 | 0.29 | 9 | 6 | 1.55 | 240 | 1 | 0.18 | 6 | 0.06 | 2 | 20 | 0.17 | 154 | 57 |
| 3 | 390 - N | 40 | 0.2 | 5.63 | 2 | 600 | 0.2 | 5 | 0.92 | 0.4 | 43 | 4 | 44 | 109 | 3.52 | 1.40 | 13 | 14 | 1.76 | 637 | 1 | 0.17 | 12 | 0.08 | 9 | 126 | 0.16 | 124 | 212 |

D6/10 June off

| T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Bc ppm | Bi ppm | Ca % | Cl ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm | 3300-033 Pg. 2 of 2 |
|--------|------------|--------|--------|------|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------|------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|------------------------|
| 4 | 390 - O | 5 | 0.2 | 5.93 | 2 | 419 | 0.3 | 5 | 1.39 | 0.2 | 44 | 15 | 52 | 29 | 4.88 | 0.90 | 10 | 21 | 1.60 | 633 | 1 | 0.48 | 10 | 0.18 | 3 | 181 | 0.09 | 143 | 61 | |
| 5 | P | 5 | 0.2 | 2.66 | 2 | 282 | 0.4 | 5 | 2.06 | 0.2 | 60 | 16 | 114 | 29 | 3.81 | 0.14 | 14 | 9 | 2.40 | 692 | 3 | 0.26 | 56 | 0.11 | 6 | 185 | 0.27 | 136 | 69 | |
| 6 | Q | 5 | 0.2 | 4.98 | 2 | 637 | 0.3 | 5 | 3.12 | 0.2 | 68 | 14 | 28 | 50 | 5.27 | 0.92 | 13 | 11 | 1.08 | 929 | 1 | 0.16 | 8 | 0.11 | 2 | 224 | 0.27 | 155 | 79 | |
| 7 | R | 5 | 0.4 | 2.61 | 2 | 305 | 0.2 | 5 | 0.65 | 0.2 | 36 | 14 | 47 | 33 | 5.64 | 0.44 | 11 | 13 | 1.28 | 400 | 1 | 0.12 | 7 | 0.12 | 2 | 60 | 0.17 | 149 | 81 | |
| 8 | S | 5 | 0.2 | 3.25 | 6 | 320 | 0.3 | 5 | 2.98 | 0.2 | 67 | 14 | 100 | 64 | 5.24 | 0.61 | 14 | 11 | 1.38 | 644 | 1 | 0.16 | 34 | 0.14 | 3 | 206 | 0.30 | 115 | 68 | |
| 9 | T | 5 | 0.2 | 3.39 | 2 | 168 | 0.2 | 5 | 2.47 | 0.2 | 55 | 16 | 31 | 139 | 4.91 | 0.58 | 10 | 11 | 1.37 | 871 | 1 | 0.22 | 8 | 0.07 | 2 | 97 | 0.31 | 159 | 68 | |
| 0 | U | 5 | 0.2 | 2.68 | 4 | 270 | 0.3 | 5 | 2.39 | 0.2 | 83 | 10 | 62 | 36 | 3.77 | 0.80 | 22 | 13 | 1.22 | 841 | 1 | 0.09 | 26 | 0.11 | 7 | 192 | 0.31 | 106 | 67 | |
| 1 | V | 10 | 0.2 | 4.59 | 2 | 423 | 0.3 | 7 | 2.44 | 0.5 | 58 | 10 | 23 | 59 | 3.27 | 1.05 | 11 | 11 | 1.15 | 923 | 1 | 0.09 | 8 | 0.12 | 2 | 227 | 0.23 | 139 | 54 | |
| 2 | 390 - W | 5 | 0.2 | 6.78 | 2 | 768 | 0.3 | 6 | 0.42 | 0.2 | 31 | 12 | 27 | 45 | 3.53 | 1.52 | 9 | 26 | 0.72 | 156 | 1 | 0.53 | 10 | 0.10 | 2 | 108 | 0.06 | 143 | 19 | |
| 3 | 392 - A | 5 | 0.2 | 4.32 | 8 | 1289 | 1.0 | 5 | 3.29 | 0.9 | 75 | 35 | 122 | 30 | 5.86 | 2.50 | 18 | 57 | 4.72 | 801 | 1 | 0.19 | 171 | 0.35 | 6 | 493 | 0.35 | 209 | 69 | |
| 4 | B | 5 | 0.2 | 2.39 | 7 | 183 | 1.0 | 5 | 1.69 | 0.5 | 59 | 16 | 105 | 63 | 4.04 | 1.48 | 15 | 30 | 1.92 | 566 | 1 | 0.16 | 64 | 0.28 | 4 | 285 | 0.27 | 189 | 53 | |
| 5 | C | 5 | 0.2 | 2.35 | 7 | 223 | 0.7 | 5 | 2.11 | 0.2 | 65 | 13 | 35 | 113 | 4.25 | 0.95 | 15 | 20 | 1.15 | 582 | 1 | 0.09 | 24 | 0.22 | 4 | 465 | 0.28 | 191 | 58 | |
| 6 | D | 5 | 0.2 | 0.16 | 2 | 16 | 0.2 | 5 | 0.08 | 0.2 | 9 | 3 | 325 | 46 | 0.91 | 0.08 | 2 | 2 | 0.13 | 237 | 1 | 0.03 | 6 | 0.02 | 2 | 6 | 0.02 | 27 | 7 | |
| 7 | E | 5 | 0.2 | 6.60 | 2 | 318 | 0.2 | 8 | 3.44 | 0.2 | 71 | 16 | 14 | 92 | 7.65 | 0.62 | 12 | 14 | 2.02 | 420 | 1 | 0.17 | 10 | 0.08 | 4 | 437 | 0.56 | 198 | 83 | |
| 8 | F | 5 | 0.2 | 6.65 | 5 | 61 | 0.2 | 10 | 5.67 | 0.4 | 74 | 25 | 22 | 59 | 5.76 | 0.11 | 9 | 12 | 1.89 | 1024 | 1 | 0.16 | 15 | 0.07 | 6 | 202 | 0.34 | 149 | 74 | |
| 11 | G | 5 | 0.2 | 6.21 | 4 | 75 | 0.2 | 8 | 4.36 | 0.2 | 65 | 30 | 33 | 50 | 6.97 | 0.14 | 11 | 22 | 2.65 | 1119 | 1 | 0.07 | 17 | 0.06 | 2 | 299 | 0.42 | 242 | 84 | |
| 12 | H | 5 | 0.2 | 4.10 | 5 | 9 | 0.3 | 5 | 16.16 | 0.2 | 65 | 12 | 20 | 40 | 2.88 | 0.04 | 2 | 9 | 0.73 | 815 | 1 | 0.05 | 12 | 0.06 | 2 | 608 | 0.24 | 132 | 31 | |
| 13 | I | 5 | 0.2 | 2.52 | 2 | 15 | 0.2 | 5 | 1.83 | 0.2 | 56 | 16 | 37 | 97 | 5.56 | 0.05 | 12 | 9 | 1.65 | 767 | 1 | 0.15 | 11 | 0.08 | 2 | 76 | 0.58 | 155 | 76 | |
| 14 | 392 - J | 5 | 0.2 | 3.64 | 6 | 182 | 0.3 | 5 | 12.01 | 0.2 | 73 | 21 | 31 | 45 | 4.09 | 0.41 | 4 | 11 | 1.21 | 1705 | 1 | 0.21 | 15 | 0.06 | 2 | 234 | 0.45 | 154 | 56 | |
| 15 | 393 - A | 90 | 0.2 | 4.69 | 2 | 554 | 0.2 | 5 | 0.39 | 0.2 | 32 | 3 | 32 | 152 | 2.06 | 1.55 | 11 | 13 | 1.07 | 368 | 5 | 0.13 | 3 | 0.09 | 2 | 23 | 0.15 | 97 | 168 | |
| 16 | B | 110 | 0.8 | 1.83 | 2 | 276 | 0.2 | 5 | 0.06 | 0.2 | 11 | 4 | 176 | 239 | 2.02 | 0.68 | 5 | 3 | 0.20 | 109 | 116 | 0.09 | 3 | 0.04 | 2 | 4 | 0.03 | 69 | 48 | |
| 17 | 393 - C | 460 | 0.2 | 0.73 | 2 | 114 | 0.2 | 5 | 0.02 | 0.2 | 8 | 4 | 217 | 32 | 2.00 | 0.33 | 4 | 1 | 0.04 | 71 | 1447 | 0.04 | 2 | 0.02 | 2 | 3 | 0.01 | 26 | 12 | |

NORANDA DELTA LABORATORY

Geochemical Analysis

Project Name & No.: **KLIVUL - 148**
 Material: **25 Rx**
 Remarks: * Sample analyzed @ -35 MESH (0.5 mm)
 # Organic, & Humus, & Sulfide

Geol.: T.W.
 Sheet: 1 of 1

Date received: OCT. 14
 Date completed: OCT. 26

LAB CODE: 9310-015

Au - 10.0 g sample digested with aqua-regia and determined by A.A. (D.L. 5 PPB)

ICP - 0.2 g sample digested with 3 ml HClO₄/HNO₃ (4:1) at 203 °C for 4 hours diluted to 10 ml with water. Leeman PB3000 ICP determined elemental contents.
 M.B. The major oxide elements and Ba, Be, Ce, La, Li, Ga are rarely dissolved completely from geological materials with this acid dissolution method.

| T.T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Be ppm | Bi ppm | Ca % | Cl ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm |
|----------|-------------|--------|--------|------|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------|-------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|
| 31 | 393 - D | 150 | 0.2 | 3.93 | 13 | 25 | 0.3 | 5 | 7.92 | 0.2 | 63 | 22 | 34 | 304 | 5.69 | 0.05 | 11 | 12 | 1.33 | 1904 | 1 | 0.09 | 20 | 0.09 | 2 | 269 | 0.46 | 197 | 110 |
| 32 | E | 280 | 0.4 | 0.46 | 41 | 18 | 0.4 | 5 | 23.36 | 0.2 | 20 | 201 | 29 | 459 | 5.69 | 0.08 | 1 | 7 | 0.28 | 8432 | 10 | 0.03 | 316 | 0.03 | 2 | 158 | 0.01 | 70 | 29 |
| 33 | F | 100 | 0.4 | 5.03 | 33 | 20 | 0.4 | 5 | 8.80 | 0.2 | 64 | 21 | 39 | 351 | 7.85 | 0.07 | 14 | 11 | 1.29 | 2478 | 1 | 0.10 | 38 | 0.14 | 2 | 240 | 0.36 | 204 | 85 |
| 34 | G | 5 | 0.2 | 3.97 | 8 | 30 | 0.2 | 5 | 3.67 | 0.2 | 56 | 9 | 30 | 48 | 5.17 | 0.28 | 11 | 9 | 0.94 | 696 | 2 | 0.08 | 4 | 0.14 | 2 | 173 | 0.22 | 107 | 43 |
| 35 | H | 30 | 0.2 | 2.73 | 7 | 97 | 0.2 | 5 | 2.25 | 0.2 | 47 | 20 | 31 | 16 | 4.56 | 0.56 | 9 | 7 | 0.93 | 602 | 1 | 0.12 | 6 | 0.12 | 2 | 101 | 0.30 | 131 | 32 |
| 36 | I | 100 | 0.2 | 6.48 | 12 | 271 | 0.3 | 5 | 3.80 | 0.2 | 52 | 16 | 13 | 86 | 6.67 | 0.47 | 9 | 11 | 1.85 | 1221 | 1 | 0.06 | 6 | 0.10 | 2 | 180 | 0.36 | 136 | 90 |
| 37 | J | 30 | 0.2 | 6.24 | 15 | 28 | 0.3 | 5 | 5.70 | 0.2 | 63 | 14 | 21 | 74 | 6.06 | 0.07 | 12 | 12 | 1.77 | 1286 | 1 | 0.07 | 9 | 0.10 | 2 | 312 | 0.42 | 177 | 90 |
| 38 | K | 53000 | 10.8 | 0.26 | 2 | 21 | 0.2 | 6 | 0.04 | 0.2 | 6 | 1 | 294 | 206 | 2.73 | 0.10 | 2 | 1 | 0.03 | 96 | 3 | 0.01 | 3 | 0.01 | 2 | 2 | 0.01 | 12 | 11 |
| 39 | L | 140 | 2.8 | 4.50 | 7 | 387 | 0.9 | 5 | 1.69 | 0.2 | 45 | 10 | 60 | 193 | 2.74 | 2.04 | 11 | 4 | 0.72 | 286 | 32 | 0.11 | 6 | 0.08 | 4 | 30 | 0.03 | 95 | 30 |
| 40 | M | 5 | 0.2 | 3.81 | 27 | 246 | 0.3 | 5 | 5.93 | 1.9 | 62 | 24 | 118 | 114 | 5.15 | 0.58 | 12 | 33 | 2.10 | 921 | 3 | 0.07 | 44 | 0.07 | 2 | 205 | 0.06 | 286 | 135 |
| 41 | N | 620 | 0.2 | 2.26 | 14 | 1019 | 0.3 | 5 | 3.60 | 0.2 | 48 | 10 | 147 | 35 | 2.98 | 0.64 | 9 | 11 | 0.46 | 702 | 1 | 0.13 | 7 | 0.04 | 2 | 75 | 0.08 | 98 | 33 |
| 42 | O | 20 | 0.2 | 4.02 | 10 | 619 | 0.4 | 5 | 5.53 | 0.2 | 60 | 22 | 65 | 86 | 4.88 | 1.33 | 12 | 13 | 1.94 | 890 | 1 | 0.15 | 34 | 0.06 | 2 | 108 | 0.09 | 178 | 63 |
| 43 | P | 5 | 0.4 | 5.79 | 10 | 1372 | 0.4 | 5 | 5.43 | 0.2 | 63 | 21 | 26 | 101 | 5.45 | 2.33 | 13 | 17 | 1.11 | 897 | 1 | 0.13 | 22 | 0.10 | 2 | 70 | 0.27 | 223 | 72 |
| 44 | Q | 30 | 1.6 | 1.06 | 6 | 727 | 0.5 | 5 | 2.84 | 0.7 | 53 | 10 | 178 | 218 | 2.13 | 0.49 | 9 | 6 | 0.81 | 505 | 1 | 0.06 | 20 | 0.08 | 14 | 109 | 0.03 | 117 | 51 |
| 45 | R | 100 | 0.8 | 2.68 | 7 | 945 | 0.8 | 5 | 3.63 | 0.3 | 61 | 17 | 102 | 84 | 4.46 | 1.19 | 11 | 8 | 0.92 | 833 | 1 | 0.10 | 20 | 0.05 | 2 | 177 | 0.07 | 178 | 47 |
| 46 | S | 5 | 0.4 | 4.06 | 131 | 567 | 0.5 | 5 | 3.57 | 2.0 | 64 | 28 | 82 | 125 | 6.62 | 0.78 | 14 | 29 | 2.39 | 956 | 19 | 0.18 | 55 | 0.08 | 4 | 65 | 0.06 | 498 | 216 |
| 47 | T | 20 | 0.2 | 6.66 | 20 | 289 | 0.4 | 5 | 3.28 | 0.6 | 64 | 7 | 35 | 74 | 6.25 | 0.93 | 15 | 16 | 2.74 | 1463 | 1 | 0.08 | 18 | 0.07 | 6 | 181 | 0.31 | 191 | 116 |
| 48 | U | 5 | 0.2 | 7.35 | 24 | 151 | 0.3 | 5 | 4.96 | 0.5 | 67 | 15 | 15 | 86 | 5.25 | 1.06 | 13 | 11 | 2.26 | 1087 | 1 | 0.05 | 9 | 0.08 | 2 | 161 | 0.30 | 198 | 78 |
| 51 | V | 5 | 0.2 | 4.99 | 24 | 385 | 0.8 | 5 | 3.06 | 0.2 | 57 | 21 | 50 | 23 | 5.26 | 2.00 | 15 | 17 | 1.40 | 841 | 1 | 0.06 | 35 | 0.19 | 2 | 74 | 0.07 | 108 | 114 |
| 52 | 393 - W | 130 | 0.4 | 4.93 | 13 | 195 | 0.5 | 5 | 3.83 | 0.2 | 49 | 39 | 21 | 398 | 10.27 | 0.30 | 13 | 19 | 2.52 | 1062 | 1 | 0.33 | 11 | 0.10 | 2 | 136 | 0.28 | 182 | 95 |
| 53 | 394 - A | 300 | 0.2 | 4.16 | 6 | 105 | 0.3 | 5 | 3.57 | 0.2 | 54 | 17 | 54 | 97 | 4.68 | 0.24 | 11 | 10 | 1.20 | 594 | 1 | 0.41 | 23 | 0.08 | 2 | 158 | 0.42 | 130 | 80 |
| 54 | B | 5 | 0.2 | 2.28 | 11 | 290 | 0.2 | 5 | 1.49 | 0.2 | 48 | 14 | 63 | 108 | 4.72 | 0.48 | 13 | 13 | 1.74 | 603 | 1 | 0.19 | 28 | 0.08 | 2 | 48 | 0.35 | 179 | 104 |
| 55 | C | 30 | 0.2 | 2.66 | 10 | 315 | 0.2 | 5 | 0.49 | 0.2 | 28 | 24 | 44 | 11 | 8.40 | 1.05 | 7 | 9 | 0.87 | 322 | 1 | 0.10 | 2 | 0.14 | 2 | 17 | 0.17 | 158 | 39 |
| 56 | D | 30 | 0.2 | 8.73 | 2 | 1755 | 0.3 | 5 | 0.19 | 0.2 | 28 | 1 | 106 | 34 | 3.54 | 3.59 | 10 | 2 | 0.09 | 23 | 1 | 0.28 | 5 | 0.12 | 2 | 87 | 0.08 | 404 | 11 |
| 57 | E | 1200 | 0.2 | 1.29 | 3 | 197 | 0.2 | 5 | 0.03 | 0.2 | 12 | 1 | 181 | 32 | 8.62 | 0.42 | 5 | 4 | 0.11 | 89 | 1 | 0.06 | 3 | 0.03 | 2 | 15 | 0.10 | 67 | 17 |
| 58 | 394 - E rpt | - | 0.4 | 1.28 | 4 | 195 | 0.2 | 5 | 0.03 | 0.2 | 14 | 1 | 188 | 32 | 8.77 | 0.42 | 6 | 4 | 0.11 | 93 | 1 | 0.06 | 4 | 0.04 | 2 | 15 | 0.11 | 67 | 18 |

27/10 - done ff

Norex - Delta
RT. NO. 9309-033
59 RX

PROJECT NO. 148 PROPERTY KL1406

N.T.S. 94D/08

GRID REFERENCE _____

DATE Sept 17

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | CO-ORDINATES | SAMPLER |
|----------|---|---------|---------|--------|--|------------------------------|---------|
| | | | | Au | Cu | | |
| A | Bleached, pyritic monzonite porphyry, 3-5% P ₂ O ₅ | Gnub | | | | 1075N 4420E | TW |
| B | Monzonite? Ser. sheared bleached gossen clay | Gnub | | | | 925N 4475E | Crop |
| C | Med gr. microdiorite w/ epi + tr mul schl | Gnub | massive | | | 725N 4735E | Crop |
| D | Carbonized diorite H ₂ O mt; limonite | Gnub | | | | 675N 4600E | Crop |
| E | Bleached Pyritic + chl diorite. ^{bluish} ser ~7% P ₂ O ₅ | Gnub | | | | 2025N 1625E | LI |
| F | Bull gte (in trend) 235°/080° w/ shaly hem or sulverge. w/ 1m wide gnub | | | | | 2190N 1545E | LI |
| G | fine grained felsic dyke in fragmental host rock, epi P ₂ O ₅ 3% | Gnub | | | | 2575N 1490E | LI |
| H | DK-green andesite (biotite - chl) w/ epi + P ₂ O ₅ 5% | Gnub | | | Half | 2675N 1625E | LI |
| J | Irregular shaped py-mt-epi stream. sieved locally | Gnub | | | | 2850N 1465E | Down |
| I | Sieve pick sediment (ultra ^{clastic}) pyritic schl by epi hornblende | | | | | 2850N 1465E | mount |
| K | QV with pyrite in (0.7m) wide in 2m wide stream/fault | Gnub | | | | 2165N 1410E | LI |
| L | Sheared diorite w/ massive pylic blebs + gte - epi | Gnub | | | | 2165N 1415E | LI |
| M | Sulphidized monzonite - blorp / dia, bleached goss 5-7% P ₂ O ₅ | Gnub | | | In diss + 5% P ₂ O ₅ | 2100N 1365E | LI |
| N | Diorite. Bleached Ser. Kaol w/ky sheared, goss m ^o P ₂ O ₅ sweet 2-3 diss. w/ky sief locally < 10% P ₂ O ₅ | Gnub | | | | 2320N 17800E | LI |
| P | Calc-silicate hornfels + garnet. mt + epi, filled fines | Gnub | | | | 2450N 1800E | LI |
| Q | Fl-physis thud, epi filled flocs + w/ky sief, intense bio | Gnub | | | | 2670N 1800E | LI |
| R | Sheared, bleached andesite Rusky, epi + 2-3% P ₂ O ₅ | Gnub | | | | 4600E 1800E 1440N | ? |
| B | Diorite?/FP. sheared goss, Ser clay - chl | Gnub | | | | 1350N 4610E | LI |
| S | sheared diorite. carb + epi - cc in fines | Frane | Gnub | | | 7100N 4941E | Crop |
| T | Sheared fin thud in sulverge, QV irregular, goss on sulverge - 1/2 of 30 + chrysic - in ker. | | | | | 9475N 4800E | Crop |
| U | Bleached chl diorite, w/ky sief, no S = | Gnub | | | | 6425N 4800E | Crop |
| V | sheared chloritic diorite, w/ky sief in fine coating + diss | Cooling | | | Med 1.0m chip | 7400N 4720E | Crop |
| W | Fels-physis di/mow w/ky sief; diss + fine ending | Med | gnub | | 2.0m chip | 7400N 4720E | Crop |

Norex Delta

PROJECT NO. 184 148 PROPERTY Klyne

N.T.S. 440/8

T. NO. _____

GRID REFERENCE _____

DATE Sept 25/93

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | | CO-ORDINATES | | SAMPLER |
|----------|--|-----------------|-------|--------|--|---------------------------|-------------------------|-------|---------|
| | | | | | | | | | |
| A | Fe-Carb felsic Intrusive - light brown | grab | | | | 3925E | 950N | MLP | |
| B | Laminated Chert. Silt. Arg. carbonate matrix | grab | | | | 3725E 3425E | 750N 765N | BARB | |
| B | Intrusive Porphyry (Fel/Dic) in mag. rock on road | grab | | | | 3925E | 700N | BARB | |
| D | Felsic/Diorite Dyke 10% clissom py | grab | | | | 3725E | 765N | LAID | |
| E | Diorite Kspar Fe Carb Alt. magnetite | grab | | | | 4000E | 1100N | CIC-1 | |
| F | Horstels Intr. Dyke - section 1 No sample | grab | | | | 8900E | 1875N | | |
| G | Alt Diorite Serpentine Shear calcite veins rusty top | grab | | | | 800E | 2360N | Kli | |
| H | Magnetite / Epidote Banded Skarn? | grab | | | | 800E | 2500N | Kli | |
| I | Py Cpy clissom Diorite - calcite and feldspar | grab | | | | 800E | 2590N | Kli | |
| J | Horstels Intr. Dyke - clissom s py stringer | grab | | | | 1000E | 2800N | Kli | |
| K | Large talus boulder hornfels clissom py | grab | | | | 1200E | 2220N | Kli | |
| L | Felsic, Int. plagiocl. 20% clissom py | grab | | | | 1200E | 2880N | Kli | |
| M | hornfels meta-sediments clissom py | grab | | | | 1200E | 2600N | Kli | |
| N | Altered Deeply weathered Fel Int. clissom py, ser. siliceous | grab | | | | 2575E | 2005N | Kli | |
| O | Py bdr. black sil. w/ mag. feldspar fine py | grab | | | | 2600E | 2510N | Kli | |
| P | Intrusive fine granite in chert | grab | | | | 2600E | 2490N | Kli | |
| Q | Feldspar Porphyry weak epidote | grab | | | | 2535E | 2650N | Kli | |
| R | Felsic Porphyry 10-15% fine clissom py | grab | | | | 2600E | 2650N | Kli | |
| S | Dark Diorite in mag. dyke | grab | | | | 2600E | 2900N | Bar 7 | |
| T | Intrusive Py Int. sulphides | grab | | | | 2800E | 2990N | Joh | |
| U | Feldspar Porphyry tr py | grab | | | | 2800E | 2975N | Joh | |
| V | Course granular Feldspar porphyry py | grab | | | | 2800E | 2600N | Kli | |
| W | Pyrite Hala. Felsic Int. fine py | grab | | | | 2800E | 2500N | Kli | |

2715

LAB Norex - Delta
CERT. NO. 9309-034

PROJECT NO. 183+184 PROPERTY Golden R. / Jo

N.T.S. 948/8E

GRID REFERENCE _____

DATE Sept 25, 93

24 RX

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | CO-ORDINATES | | SAMPLER |
|----------|--|----------------|-----------|--------|--|--------------|--------|---------|
| | | | | | | | | |
| A | Diorite Blenched goss, chl: bx | Gmb | | | | 675N | 4725E | Geo/In |
| B | Blenched dio blenched - porph, wtkly sil, chl | Gmb | gas frs | | | 680N | 4725E | Geo/In |
| C | Monzonite feldspar porphyry chl, mal | diss | mal fracs | | | 650N | 4715E | Geo/In |
| D | wtkly Blenched dio tr of mal stains, mal stain, chl | Gmb | | | | 635N | 4710E | Geo/In |
| E | Gossanous microdiorite, fracs (N-E), hem + mal stain | ln chip | | | | 3115N | 2510E | Sch |
| F | Dark bio-diorite, with epi + mal + azurite stain | Gmb | | | | 3115N | 2520E | " |
| G | A4 lens microdiorite fracs | Gmb | | | | 3105N | 2525E | " |
| H | Dark bio-diorite w mt, py, epi, mal stains in fr | Gmb | | | | 3100 | 2520E | " |
| I | Epidiot - Garnet - mal skarn in Py + tr epi oxidized | Gmb | | | | 183 | 1.0 | |
| J | Massive Alt, mal conhd fracs: diss py, epy local | Gmb | | | | | | |
| K | Py - Cpy - mt epi - diorite | Gmb | | | | | | |
| L | Py - epy - mal Epi - Diorite - Highly altered | Gmb | | | | | | |
| M | Massive MnO - py frambooidal: epid | Gmb | | | | | | |
| N | Laminated met-sediment w fr py diss | Gmb | | | | | | |
| O | Altered country rock: met sed blenched py | Gmb | | | | 3115N | 2635E | |
| P | shered, bx, carbonated fragmental, py in gen vol | bx Gmb | | | | 3115N | 2625E | |
| Q | Microdiorite w 5% diss py: porphy > 10% Py in fracs | bx wtkly, mtic | | | | 3200N | 2700E | |
| R | Felsic dyke, w 3-5% Py | Gmb | | | | 3200N | 2760E | |
| S | Fragmental in host (Fel) xenolith? epi goss dip to SE ~ 5% Py w tight sherd cc | | | | | 3200N | 2800NE | |
| U | Fragmental, w py impregnation 3-5%, epi chl in host | | | | | 3200N | 2860NE | |
| T | Basaltic flow massive, usually 5-7% Py, chl | Gmb | | | | 3200N | 2850N | |
| V | Monzonitic blenched diorite w 1% epy epi + mt | Talus | | | | 3450N | 2700E | |
| W | Banded mt - epi + garnet w tr epy + mal stain | Talus | | | | 3550N | 2475E | |

Proj # 183
Proj. 184
9309-034
RX

LAB Norex - Delta

NORANDA EXPLORATION COMPANY, LIMITED

0393

Now - Field

PROJECT NO. 148 PROPERTY R414ULN.T.S. 740/56

CERT. NO. _____

GRID REFERENCE _____

DATE Sept 26

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | CO-ORDINATES | | SAMPLER |
|----------|---|------|-------|--------|----------------------|--------------|-------|---------|
| | | | | | | | | |
| A | Bleached, glass diorite, sheared locally to P ₂ | | Grub | | | 1620N | 3580E | Kli / |
| B | Subvolcanic Bull qtz, hematite stained goss in sub mags | | Grub | | | 1620N | 3575E | " / |
| C | over two meter wide qv (305/048's) hem to P ₂ | | Grub | | | 1625N | 3520E | " / |
| D | Hornfelsic andesite w/ ep+bio, fac. calcic P ₂ | | Grub | | | 2975N | 2750E | Sch / |
| E | Epi-mt skarn in limy layered sed, ash fall, apf | | Grub | | | 2975N | 2665E | " / |
| F | Qtz-carb veins in sheared andesite py-cpy-epi | | Grub | | | 2925N | 2560E | " / |
| G | Intermediate dyke pyritic 2-3% Bleached goss | | Grub | | | 3025N | 2875E | " / |
| H | Bleached andesite microdiorite, glass >5% Pel type | | Grub | | | 3100N | 3000E | " / |
| I | sheared light green lithic andesitic tuff, pyritic | | Grub | | | 2865N | 680E | Kli / |
| J | Intermediate Vol lithic tuff chd w/ sil flow? | | Grub | | | 2980N | 685E | Kli / |
| K | sheared intrusive, ser-hem + kaolin vuggy qtz vein (streak) | | Grub | | 70% qtz | 3195N | 800E | Sch / |
| L | Sheared felsic intrusive in stockwork - qtz and stained | | Grub | | old bench waste dump | 3225N | 775E | Sch / |
| M | silicified sst, qz veins, hematite, 3% py | | Grub | | | 1035N | 2400W | Doc / |
| N | qtz-carb stockwork in wtkly silf + carb fr sed | | Grub | | X 5% qtz-carb | 1125N | 2340W | " / |
| O | F.g. sst w/ qtz stringers, weakly calcareous, qz-carb veins, 3% py | | Grub | | | 1075N | 2400W | " / |
| P | sheared wtkly silf + carbonized sed (sst) | | | | | 1307N | 2400W | " / |
| Q | Qtz-carb stringers and streaks, wk hem staining; tr P ₂ | | | | in lab? lpl: tuff | 1350N | 2155W | " / |
| R | Qtz-carb str-zone in wtkly fr sed adjacent to fault/fnc zone | | | | | 1350N | 2105W | " / |
| S | fr laminated sed (sst) w/ 3-5% py impregnation, wk carb alt. | | | | float | 1350N | 1975W | " / |
| T | Bleached, sheared wtkly silf-diorite 3-5% P ₂ | | Grub | | | 590N | 4790E | Croy / |
| U | ditto | | | | | 540N | 4840E | " / |
| V | Alt-and. wtkly calcareous, wtkly impregnated, 2% qtz, local qz flooding | | Grub | | | 2710N | 3600E | Kli / |
| W | F.g. sediment, 5% mgd/ff py, rusty W.S. | | Grub | | | 2800N | 4300E | Croy / |

LAB _____

PROJECT NO. 148 PROPERTY Kliyul

N.T.S. _____

CERT. NO. _____

GRID REFERENCE _____

DATE _____

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | CO-ORDINATES | | SAMPLER |
|----------|---|------|--------|--------|--|--------------|-------|---------|
| | | | | | | | | |
| A | Fg seed, slightly skarnified, 1-4% v/g/ff Py | | Gravel | | | 3180E | 2720N | Kli ✓ |
| B | Sediment, rusty WS, 5-15% v/g/ff Py | | Gravel | | | 3170E | 2775N | Line ✓ |
| C | Alt volc, 20-30% mgd Py, 13-18% Hch, rusty WS | | Gravel | | | 3200E | 2910N | " ✓ |
| D | Silic. volc, weakly magnetite, tr. sulf., massive P | | Gravel | | | 2925E | 2650N | Kli ✓ |
| E | Skarnified volc tuff, magnetite rich, 3% fg sulf. | | Gravel | | | 2925E | 2650N | " ✓ |
| F | | | | | | | | |
| G | | | | | | | | |
| H | | | | | | | | |
| I | | | | | | | | |
| J | | | | | | | | |
| K | | | | | | | | |
| L | | | | | | | | |
| M | | | | | | | | |
| N | | | | | | | | |
| O | | | | | | | | |
| P | | | | | | | | |
| Q | | | | | | | | |
| R | | | | | | | | |
| S | | | | | | | | |
| T | | | | | | | | |
| U | | | | | | | | |
| V | | | | | | | | |
| W | | | | | | | | |

VOID

NORANDA DELTA LABORATORY

Geochemical Analysis

Project Name & No.: KLIYUL - 148

Geol.: T.W.

Date received: AUG. 27

LAB CODE: 9309-006

Material: 173 Rx

Sheet: 1 of 5

Date completed: SEP. 20

Remarks: * Sample screened @ -35 MESH (0.5 mm)

† Organic, & Humus, S Sulphide

Au - 10.0 g sample digested with aqua-regia and determined by A.A. (D.L. 5 PPB)

ICP - 0.2 g sample digested with 3 ml HClO₄/HNO₃ (4:1) at 203 °C for 4 hours diluted to 10 ml with water. Leeman PS3000 ICP determined elemental contents.

N.B. The major oxide elements and Ba, Be, Ce, La, Li, Ga are rarely dissolved completely from geological materials with this acid dissolution method.

| T.T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Be ppm | Bi ppm | Cs % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm |
|----------|------------|--------|--------|------|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------|-------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|
| 12 | 383 - A | 30 | 0.2 | 7.24 | 102 | 593 | 2.8 | 5 | 0.81 | 1.0 | 154 | 19 | 13 | 44 | 7.01 | 2.28 | 64 | 39 | 0.67 | 1990 | 2 | 0.10 | 23 | 0.17 | 92 | 98 | 0.30 | 150 | 307 |
| 13 | B | 20 | 0.2 | 4.80 | 2 | 481 | 0.2 | 5 | 1.47 | 0.2 | 48 | 14 | 42 | 40 | 5.16 | 0.71 | 11 | 11 | 1.63 | 723 | 1 | 0.10 | 22 | 0.07 | 3 | 242 | 0.20 | 171 | 63 |
| 14 | C | 10 | 0.2 | 4.97 | 5 | 555 | 0.3 | 5 | 3.90 | 0.4 | 65 | 14 | 14 | 23 | 4.46 | 0.93 | 12 | 10 | 0.95 | 1322 | 1 | 0.09 | 7 | 0.10 | 5 | 242 | 0.32 | 120 | 63 |
| 15 | D | 5 | 0.2 | 3.87 | 10 | 333 | 0.2 | 5 | 1.86 | 0.6 | 51 | 12 | 13 | 39 | 3.79 | 0.73 | 10 | 12 | 1.39 | 1130 | 1 | 0.13 | 7 | 0.09 | 2 | 155 | 0.27 | 164 | 70 |
| 16 | E | 5 | 0.2 | 4.38 | 7 | 520 | 0.2 | 5 | 1.18 | 0.2 | 43 | 13 | 17 | 28 | 4.11 | 0.75 | 9 | 13 | 1.73 | 466 | 8 | 0.23 | 6 | 0.08 | 4 | 107 | 0.16 | 133 | 37 |
| 17 | F | 10 | 0.2 | 7.39 | 3 | 1837 | 0.2 | 5 | 0.77 | 0.2 | 32 | 19 | 10 | 12 | 5.48 | 2.82 | 7 | 11 | 1.12 | 486 | 1 | 0.19 | 7 | 0.10 | 2 | 31 | 0.27 | 188 | 54 |
| 18 | G | 30 | 0.2 | 2.63 | 9 | 428 | 0.2 | 5 | 1.63 | 0.6 | 51 | 14 | 25 | 31 | 5.12 | 0.81 | 10 | 9 | 1.07 | 950 | 1 | 0.11 | 5 | 0.08 | 2 | 67 | 0.35 | 153 | 69 |
| 19 | H | 5 | 0.2 | 8.08 | 2 | 1086 | 0.4 | 5 | 0.58 | 0.8 | 35 | 17 | 6 | 32 | 4.80 | 3.48 | 10 | 9 | 1.10 | 700 | 1 | 0.06 | 6 | 0.09 | 5 | 16 | 0.23 | 166 | 82 |
| 20 | M | 90 | 0.2 | 3.41 | 18 | 131 | 0.2 | 5 | 2.64 | 0.3 | 58 | 21 | 20 | 11 | 4.70 | 0.53 | 12 | 9 | 1.24 | 1038 | 2 | 0.09 | 7 | 0.08 | 4 | 99 | 0.29 | 149 | 49 |
| 21 | S | 5 | 0.2 | 5.17 | 15 | 1620 | 0.3 | 5 | 0.76 | 0.4 | 39 | 12 | 27 | 10 | 4.51 | 2.01 | 11 | 11 | 1.17 | 509 | 5 | 0.10 | 6 | 0.09 | 2 | 25 | 0.26 | 158 | 33 |
| 22 | 383 - U | 25000 | 32.0 | 2.11 | 5 | 178 | 0.2 | 5 | 1.01 | 0.3 | 40 | 38 | 58 | 20 | 15.66 | 0.65 | 10 | 3 | 0.31 | 424 | 3 | 0.06 | 5 | 0.06 | 2 | 38 | 0.11 | 96 | 18 |
| 24 | 386 - A | 40 | 4.8 | 8.42 | 17 | 10 | 0.4 | 5 | 10.12 | 13.8 | 101 | 33 | 48 | 2228 | 8.60 | 0.03 | 17 | 7 | 0.56 | 894 | 1 | 0.03 | 37 | 0.12 | 5 | 570 | 0.42 | 314 | 1215 |
| 25 | B | 5 | 0.2 | 7.17 | 17 | 33 | 0.4 | 5 | 9.47 | 0.2 | 82 | 10 | 35 | 23 | 8.45 | 0.06 | 9 | 7 | 1.18 | 1235 | 1 | 0.06 | 24 | 0.10 | 3 | 487 | 0.44 | 245 | 52 |
| 26 | C | 5 | 0.2 | 1.48 | 2 | 2035 | 0.8 | 5 | 0.64 | 0.3 | 34 | 5 | 27 | 138 | 1.99 | 0.70 | 9 | 5 | 0.23 | 530 | 1 | 0.12 | 8 | 0.05 | 2 | 83 | 0.04 | 79 | 24 |
| 27 | D | 5 | 0.8 | 0.65 | 3 | 726 | 1.1 | 5 | 0.09 | 0.2 | 12 | 3 | 156 | 52 | 1.23 | 0.30 | 3 | 3 | 0.07 | 191 | 44 | 0.06 | 5 | 0.04 | 27 | 27 | 0.02 | 40 | 14 |
| 28 | E | 5 | 0.2 | 5.67 | 15 | 66 | 0.2 | 5 | 3.57 | 1.1 | 69 | 24 | 18 | 51 | 7.05 | 0.16 | 12 | 21 | 3.04 | 1036 | 1 | 0.18 | 11 | 0.11 | 5 | 160 | 0.82 | 263 | 101 |
| 29 | F | 5 | 0.4 | 7.21 | 4 | 161 | 0.4 | 5 | 0.54 | 0.7 | 36 | 5 | 16 | 83 | 6.18 | 0.54 | 12 | 43 | 2.45 | 550 | 2 | 0.76 | 7 | 0.10 | 5 | 182 | 0.05 | 195 | 65 |
| 30 | G | 5 | 0.2 | 3.48 | 15 | 264 | 0.2 | 5 | 1.81 | 0.8 | 65 | 3 | 26 | 25 | 2.82 | 0.40 | 15 | 10 | 1.58 | 375 | 1 | 0.14 | 9 | 0.08 | 2 | 155 | 0.25 | 138 | 37 |
| 31 | H | 5 | 0.2 | 2.72 | 10 | 72 | 0.3 | 5 | 3.72 | 0.3 | 55 | 5 | 41 | 11 | 1.39 | 0.11 | 10 | 14 | 1.19 | 457 | 2 | 0.09 | 12 | 0.08 | 4 | 138 | 0.24 | 97 | 23 |
| 32 | I | 5 | 0.2 | 6.44 | 10 | 92 | 0.3 | 5 | 7.18 | 0.2 | 67 | 20 | 77 | 20 | 6.77 | 0.09 | 8 | 8 | 1.12 | 848 | 1 | 0.06 | 29 | 0.09 | 2 | 328 | 0.40 | 229 | 36 |
| 33 | J | 5 | 0.2 | 3.92 | 2 | 782 | 0.2 | 5 | 2.55 | 0.2 | 54 | 7 | 42 | 12 | 2.53 | 0.50 | 10 | 9 | 0.80 | 738 | 3 | 0.12 | 9 | 0.07 | 2 | 238 | 0.09 | 72 | 43 |
| 34 | K | 5 | 0.2 | 4.08 | 9 | 35 | 0.2 | 5 | 3.70 | 0.2 | 60 | 11 | 29 | 153 | 4.93 | 0.07 | 12 | 9 | 1.53 | 549 | 4 | 0.12 | 23 | 0.09 | 2 | 207 | 0.34 | 117 | 28 |
| 35 | L | 5 | 0.2 | 4.07 | 14 | 333 | 0.2 | 5 | 3.90 | 0.5 | 62 | 44 | 33 | 264 | 6.49 | 0.72 | 12 | 14 | 1.97 | 776 | 2 | 0.16 | 21 | 0.10 | 6 | 175 | 0.53 | 247 | 52 |
| 36 | M | 20 | 0.2 | 4.97 | 7 | 77 | 0.3 | 5 | 3.99 | 0.2 | 60 | 36 | 27 | 65 | 5.97 | 0.56 | 10 | 16 | 1.73 | 771 | 1 | 0.11 | 17 | 0.11 | 28 | 249 | 0.45 | 222 | 82 |
| 37 | N | 50 | 0.2 | 3.98 | 10 | 73 | 0.2 | 5 | 3.11 | 0.5 | 60 | 7 | 21 | 32 | 6.39 | 0.39 | 11 | 13 | 1.65 | 721 | 2 | 0.15 | 11 | 0.10 | 17 | 181 | 0.55 | 206 | 77 |
| 38 | O | 190 | 0.2 | 1.34 | 13 | 48 | 0.2 | 5 | 4.02 | 0.2 | 53 | 25 | 69 | 56 | 4.00 | 0.13 | 8 | 6 | 0.89 | 1190 | 2 | 0.14 | 14 | 0.08 | 4 | 80 | 0.26 | 109 | 30 |
| 39 | P | 5 | 0.2 | 4.02 | 13 | 77 | 0.4 | 5 | 4.15 | 0.5 | 64 | 23 | 16 | 167 | 7.03 | 0.47 | 12 | 13 | 2.63 | 1254 | 1 | 0.28 | 16 | 0.16 | 3 | 227 | 0.61 | 305 | 71 |
| 40 | Q | 40 | 0.4 | 3.44 | 7 | 93 | 0.3 | 5 | 3.97 | 0.2 | 64 | 52 | 49 | 1048 | 5.04 | 0.45 | 12 | 9 | 0.79 | 700 | 6 | 0.10 | 18 | 0.17 | 5 | 189 | 0.37 | 149 | 45 |
| 41 | R | 5 | 0.2 | 2.48 | 13 | 47 | 0.3 | 5 | 4.18 | 0.2 | 64 | 21 | 55 | 300 | 2.26 | 0.28 | 11 | 6 | 0.45 | 579 | 2 | 0.10 | 13 | 0.15 | 3 | 142 | 0.36 | 122 | 20 |
| 42 | S | 80 | 0.2 | 3.47 | 11 | 190 | 0.3 | 5 | 1.94 | 0.5 | 57 | 51 | 53 | 685 | 4.91 | 1.20 | 13 | 14 | 1.47 | 593 | 2 | 0.09 | 24 | 0.15 | 3 | 97 | 0.24 | 157 | 48 |
| 43 | 386 - T | 5 | 0.2 | 4.70 | 11 | 117 | 0.4 | 5 | 4.84 | 0.3 | 77 | 36 | 35 | 281 | 5.17 | 0.60 | 15 | 10 | 1.32 | 724 | 1 | 0.14 | 21 | 0.13 | 2 | 340 | 0.26 | 136 | 44 |
| 44 | 387 - A | 5 | 0.2 | 5.28 | 5 | 280 | 0.2 | 5 | 3.01 | 0.6 | 68 | 26 | 10 | 61 | 6.92 | 0.49 | 15 | 22 | 2.07 | 1291 | 1 | 0.11 | 5 | 0.12 | 7 | 154 | 0.31 | 227 | 101 |
| 45 | B | 5 | 0.2 | 5.10 | 9 | 284 | 0.3 | 5 | 4.10 | 0.6 | 65 | 23 | 13 | 58 | 6.72 | 0.33 | 13 | 17 | 2.43 | 1254 | 1 | 0.14 | 5 | 0.09 | 4 | 202 | 0.40 | 262 | 86 |
| 46 | C | 5 | 0.2 | 3.53 | 12 | 95 | 0.3 | 5 | 3.13 | 0.8 | 63 | 27 | 39 | 94 | 6.40 | 0.35 | 12 | 18 | 2.96 | 848 | 1 | 0.23 | 28 | 0.10 | 2 | 81 | 0.40 | 240 | 54 |
| 47 | 387 - D | 20 | 0.2 | 2.74 | 14 | 133 | 0.3 | 5 | 2.81 | 1.3 | 62 | 28 | 62 | 141 | 5.65 | 0.28 | 13 | 10 | 2.70 | 836 | 2 | 0.23 | 30 | 0.10 | 5 | 58 | 0.35 | 190 | 54 |

21/09 Vanc ff

| F.T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Bc ppm | Bl ppm | Ca % | Od ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Tl % | V ppm | Zn ppm | 3308-008 Pa. 2 of 5 |
|----------|-------------|-----------|-----------|---------|-----------|-----------|-----------|-----------|---------|-----------|-----------|-----------|-----------|-----------|---------|--------|-----------|-----------|---------|-----------|-----------|---------|-----------|--------|-----------|-----------|---------|----------|-----------|------------------------|
| 18 | 387-E | 5 | 0.2 | 6.13 | 5 | 1028 | 0.3 | 5 | 2.91 | 0.7 | 68 | 18 | 8 | 55 | 5.66 | 1.81 | 16 | 25 | 1.69 | 1005 | 1 | 0.09 | 9 | 0.11 | 3 | 107 | 0.08 | 173 | 93 | |
| 51 | 4720E-5870N | 5 | 0.2 | 5.22 | 16 | 11 | 0.4 | 5 | 5.40 | 0.2 | 73 | 18 | 36 | 4146 | 5.94 | 0.05 | 14 | 12 | 1.86 | 716 | 1 | 0.08 | 23 | 0.10 | 3 | 362 | 0.52 | 273 | 41 | |

IB Norex-Delta BrkPROJECT NO. 148 PROPERTY KLIYUL

N.T.S. _____

ERT. NO. _____

GRID REFERENCE _____

DATE _____

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | | CO-ORDINATES | | SAMPLER |
|----------|--|------|-----------------|--------|--|--|--------------|---------------------------|---------|
| | | | | | | | | | |
| A | Brecciated Andesite, Blomhed. Pyrite 3-5% | Rx | Grabs | | | | 2690E | 2550N | KLI ✓ |
| B | fine grained andesite fr Py imp. dyke/sill? | | Grabs | | | | 2500E | 2550N | KLI ✓ |
| C | Hornfelsed andesite with cc + epi on face | | Grabs | | | | 2400E | 2837N | DORT ✓ |
| D | Qtz-epi str. zone narrow discont. fines (cm) | | composite grabs | | | | 2200E | 2600N | KLI ✓ |
| E | Fractured pyritic Blomhed Andesite del ser | | Grabs | | | | 2200E | 2500N | KLI ✓ |
| F | Silicified Andesite w fr py diss. shered | | Grabs | | | | 2000E | 2675N | KLI ✓ |
| G | fine grained andesite; pyritic; wk sil. + epi. 3-5% Py | | Grabs | | | | 2000E | 2700N | KLI ✓ |
| H | Carbonized, shered andesite | | Grabs | | | | 2000E | 2665N | KLI ✓ |
| M | wk silf + epi, fractured Andesite w fr Py diss | | Grabs | | | | 26900N | 2000E | |
| S | Silicified, fractured andesite w fr Py $\leq 5\%$ grab | | | | | | 2725N | 1800E (near 255 app. 500) | |
| U | Some massive sulphide Py adjacent to Gv (182-7) | | Grabs | | | | | | |

adjacent to veins

GINGER B.
ZONE AREA

IB _____

PROJECT NO. _____

PROPERTY Golden Rule

N.T.S. _____

ERT. NO. _____

GRID REFERENCE Recee Grid

DATE Aug. 21/93

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | CO-ORDINATES | | SAMPLER Tm/LE |
|----------|--|------|-------------------|--------|--|---------------|---------|------------------|
| | | | | | | | | |
| A | Strongly epidotized int(?), chloritic, Mc, 2% fg Py | o/c | grab | | | 100+15E | 102+50N | Cray |
| B | Chloritic aug. porph, rare dPy, very magnetic, some epidote | | | | | 100+00E | 101+90N | |
| C | Qz-carb alt int, no V.S. | | | | | 100+00E | 104+50N | |
| D | Qz-carb alt int. w streak qz veins (mm-3.5cm) No V.S. | | | | | 99+90E | 104+50N | |
| E | Bleached sediment, 2% ch. magnetite, local 5% fg dPy | | | | | 99+95E | 109+50N | |
| F | Int./aug porph, weakly siliceous, limonitic, trace pyrite sulfides | | | | | 101+00E | 103+65N | |
| G | Alt. qz monz, trace sulfides, limonitic V.S. | | | | | 100+85E | 102+20N | |
| H | Altered intrusive, no sulfides | | | | | 100+25E | 102+40N | |
| I | Aug porph/int, very wk mag, trace to local 5% fg dPy | o/c | grab | | | 100+15E | 102+50N | |
| J | Wkly altered silty, propylitic alted (epi) Qtz-monz zone | | grab | | | 100+50E | 102+40N | |
| K | chloritic Augite Porphy 5% of Py | | grab | | | 100+70E | 102+35N | |
| L | Hornfelsed augite pyritic and/or epi, tr-2% fg locally etc | | grab | | | L-2900E | 3190N | Soft ✓ |
| M | gossan. epidotized augite porphyry Py Fe | | 2m composite chip | | | L-2900E | 3185N | |
| N | gossan. pyritic Augite porphyry | | | | | 2915E | 3185N | ✓ |
| O | brecc. w siliceous, epi, chl Py + Po, magnetic etc | | | | | MAJOR 2900E | 3150N | |
| P | strongly epidotized and/or epi, locally sheared | | grab | | | GENERAL 2900E | 35+25N | ✓ |
| Q | micro-dio, fine, epi tr Py mal total BMS | | | | | 2500E | 3170N | |
| R | dk green microdio w diss mal + Azu + traces | | | | | 2510E | 3115N | |
| S | Hornfelsic rock. weakly silty, augite pyritic and/or epi | | grab | | | 2505E | 3115N | Py + Po, Azu-mal |
| T | pyritic gossan, rare wk mal stain; 1% diss Py + epi | | grab | | | 2490E | 3115N | ✓ |
| U | | | | | | | | |
| V | | | | | | | | |
| W | | | | | | | | |

VOID

Norex-Delta B.V.

NORANDA EXPLORATION COMPANY, LIMITED

0383

Yellow

PROJECT NO. 148 PROPERTY KLIYUH

N.T.S.

NO. _____

GRID REFERENCE _____

DATE _____

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | | CO-ORDINATES | | SAMPLER |
|----------|--|------|-----------|--------|--|--|--------------|--------------------------|---------|
| | | | | | | | | | |
| A | Brecciated andesite, bleached. Pyrite 3-5% | Rx | Grabs | | | | 2690E | 2550N | KLI ✓ |
| B | fine grained andesite, fr. Py. imp. dyke fill? | | Grabs | | | | 2500E | 2550N | KLI ✓ |
| C | Hornfelsed andesite with cc + epi on face | | Grabs | | | | 2400E | 2837N | DORT ✓ |
| D | Qtz-epi str. zone, narrow discont. fines (cm) | | Composite | | | | 2200E | 2600N | KLI ✓ |
| E | Fractured pyritic bleached andesite, del. ser. | | Grabs | | | | 2200E | 2500N | KLI ✓ |
| F | Silicified andesite w/ fn py. diss. stream | | Grabs | | | | 2000E | 2675N | KLI ✓ |
| G | fine grained andesite; pyritic, wk sil. 1.5% 3-5% Py | | Grabs | | | | 2000E | 2700N | KLI ✓ |
| H | Carbonized, sheared andesite | | Grabs | | | | 2000E | 2665N | KLI ✓ |
| M | wk silf + epi, fractured andesite w/ fn Py diss | | Grabs | | | | 26700N | 2000E | |
| S | Silicified, fractured andesite w/ fn Py < 5% pyrite | | Grabs | | | | 2725N | 1800E (near 255 226 Snd) | |
| U | Some massive sulphide Py adjacent to G4 (182-7) | | Grabs | | | | | | |

adjacent to veins

GINGER B
ZONE AREA

NORANDA DELTA LABORATORY

Geochemical Analysis

Project Name & No.: KLIYR. - 148

Geol.: T.W.

Date received: AUG. 05

LAB CODE: 9308-008

Material: 26 Rx

Sheet: 1 of 1

Date completed: AUG. 26

Remarks: * Sample screened @ -35 MESH (0.5 mm)

□ Organic, & Humus, S Sulfide

Au - 10.0 g sample digested with aqua-regia and determined by A.A. (D.L. 5 PPB)

ICP - 0.2 g sample digested with 3 ml HClO₄/HNO₃ (4:1) at 203 °C for 4 hours diluted to 10 ml with water. Leeman PS3000 ICP determined elemental contents.

N.B. The major oxide elements and Ba, Be, Ce, La, Li, Ga are rarely dissolved completely from geological materials with this acid dissolution method.

| T.T. SAMPLE No. | Au | Ag | Al | As | Ba | Be | Bi | Ca | Cd | Ce | Co | Cr | Cu | Fe | K | La | Li | Mg | Mn | Mo | Na | Ni | P | Pb | Sr | Ti | V | Zn |
|-----------------|-----|-----|----|-----|-----|-----|-----|----|-----|-----|-----|-----|-----|----|---|-----|-----|----|-----|-----|----|-----|---|-----|-----|----|-----|-----|
| No. | ppb | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | ppm | % | ppm | % | ppm | ppm | % | ppm | ppm |

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|----|---------|-----|-----|------|----|-----|-----|---|------|-----|----|----|----|-----|-------|------|----|----|------|-----|----|------|---|------|---|-----|------|-----|----|
| 97 | 381 - A | 20 | 0.2 | 3.38 | 11 | 260 | 0.2 | 5 | 2.44 | 0.2 | 52 | 17 | 30 | 211 | 6.40 | 0.85 | 9 | 10 | 2.01 | 946 | 6 | 0.28 | 5 | 0.08 | 2 | 74 | 0.36 | 177 | 83 |
| 98 | 381 - B | 180 | 2.4 | 3.45 | 22 | 56 | 0.2 | 5 | 3.72 | 0.2 | 65 | 2 | 59 | 299 | 12.38 | 0.21 | 15 | 5 | 0.43 | 670 | 22 | 0.04 | 1 | 0.05 | 2 | 154 | 0.10 | 104 | 57 |

20/8/68

| No. | Au | | Ag | | Al | | As | | Ba | | Be | | Bi | | Ca | | Cd | | Ce | | Co | | Cr | | Cu | | Fe | | K | | La | | Li | | Mg | | Mn | | Mo | | Na | | Ni | | P | | Pb | | Sr | | Ti | | V | | Zn | |
|-----|-----|-----|----|-----|-----|-----|-----|---|-----|-----|-----|-----|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|-----|----|-----|-----|---|-----|-----|----|-----|-----|---|-----|-----|-----|-----|----|--|----|--|----|--|---|--|----|--|
| | ppb | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | % | ppm | ppm | % | ppm | ppm | % | ppm | ppm | ppm | ppm | | | | | | | | | | |

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|----|---------|-----------|------|------|------|----|------|-----|---|------|-----|----|----|-----|------|------|------|----|----|------|------|----|------|----|------|------|-----|------|-----|------|
| 93 | 381 - C | Flow | 200 | 24.4 | 5.93 | 12 | 711 | 0.3 | 5 | 2.84 | 6.6 | 55 | 19 | 19 | 4863 | 4.69 | 2.22 | 7 | 10 | 0.61 | 649 | 5 | 0.10 | 9 | 0.08 | 4513 | 67 | 0.30 | 177 | 1059 |
| 94 | D | | 10 | 0.4 | 1.89 | 2 | 66 | 0.9 | 5 | 0.04 | 0.5 | 15 | 1 | 78 | 33 | 0.56 | 0.81 | 4 | 2 | 0.09 | 221 | 5 | 0.12 | 2 | 0.01 | 51 | 4 | 0.02 | 10 | 75 |
| 95 | E | | 40 | 0.2 | 4.40 | 2 | 713 | 0.2 | 5 | 0.87 | 0.2 | 35 | 7 | 22 | 70 | 5.83 | 0.64 | 9 | 17 | 2.46 | 594 | 3 | 0.10 | 5 | 0.08 | 2 | 92 | 0.37 | 215 | 303 |
| 96 | 381 - N | CV | 3100 | 36.4 | 0.44 | 2 | 2112 | 0.2 | 5 | 0.09 | 0.2 | 11 | 7 | 181 | 535 | 2.34 | 0.16 | 2 | 3 | 0.14 | 241 | 10 | 0.02 | 27 | 0.01 | 76 | 39 | 0.01 | 16 | 20 |
| 97 | 382 - F | 376/48005 | 5 | 0.2 | 6.08 | 2 | 298 | 0.3 | 5 | 3.06 | 0.2 | 64 | 4 | 9 | 44 | 5.38 | 0.83 | 12 | 11 | 1.92 | 1096 | 2 | 0.16 | 3 | 0.08 | 2 | 207 | 0.37 | 202 | 106 |
| 98 | H | | 130 | 0.2 | 2.86 | 2 | 776 | 0.2 | 5 | 0.47 | 0.2 | 33 | 4 | 18 | 41 | 4.41 | 1.18 | 10 | 7 | 0.80 | 630 | 46 | 0.11 | 3 | 0.09 | 16 | 34 | 0.22 | 88 | 94 |
| 99 | K | | 5 | 0.2 | 1.51 | 2 | 13 | 0.2 | 5 | 0.22 | 0.2 | 29 | 1 | 84 | 65 | 8.67 | 0.03 | 11 | 16 | 0.36 | 206 | 3 | 0.03 | 1 | 0.04 | 2 | 14 | 0.06 | 84 | 35 |
| 00 | 382 - L | Flow | 810 | 10.0 | 4.05 | 2 | 257 | 0.4 | 5 | 3.50 | 0.2 | 63 | 16 | 104 | 3728 | 4.89 | 0.70 | 11 | 12 | 1.82 | 917 | 5 | 0.15 | 39 | 0.15 | 4 | 189 | 0.34 | 112 | 105 |

32256/224023

3 NOREX-DELTA 66

PROJECT NO. 148 PROPERTY KLIYUL

N.T.S. 748/2

IT. NO. _____

GRID REFERENCE _____

DATE August 4, 77

SAMPLE REPORT

| AMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | | CO-ORDINATES | | SAMPLER |
|---------|--|-------|------------|--------|--|--|--------------|-------|---------|
| | | | | | | | | | |
| A | Subangular and Block, py + po | Flot | | | | | 3200E | 2150N | Kli |
| B | Subangular semi-massive po + py, garnet | Flot | | | | | 3700E | 2150N | " |
| C | Quartz (Vein) boulder train. No visible S ² | Flot? | Subangular | | | | 3400E | 2130N | " |
| D | Carbonated andrite with white top + ga impregnation | Flot | | | | | 4200E | 2090N | Coy |
| E | Massive cubic andrite or 3-5% chl | Rock | Grnd | | | | 3760E | 2010N | Kli |

N 1200m from subangular Qv. mass. 1cm stain train to an in mass. 4000E / 2150N Q't. boulder train port.

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-----|-----|-----|-----|------|---|-----|-----|---|------|-----|----|----|----|-----|------|------|----|----|------|-----|---|------|---|------|----|----|------|-----|-----|
| 120 | 0.3 | 170 | 0.4 | 3.88 | 2 | 568 | 0.4 | 5 | 0.71 | 0.3 | 26 | 4 | 25 | 251 | 4.91 | 1.70 | 16 | 34 | 2.49 | 806 | 5 | 0.11 | 7 | 0.09 | 48 | 60 | 0.18 | 138 | 270 |
| 133 | 3.0 | 20 | 0.2 | 5.19 | 2 | 813 | 0.3 | 5 | 0.89 | 0.3 | 28 | 12 | 12 | 86 | 5.06 | 2.06 | 10 | 19 | 2.19 | 646 | 2 | 0.09 | 6 | 0.12 | 7 | 96 | 0.25 | 171 | 147 |

IB _____

PROJECT NO. 148 PROPERTY KLIYUL

N.T.S. 948

ERT. NO. _____

GRID REFERENCE _____

DATE _____

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | | CO-ORDINATES | SAMPLER |
|----------|---|-------------|-------|--------|--|--|--------------|--------------------------------|
| | | | | | | | | |
| F | Goss ser solust / altered monzonite Py + Pb with matic Fe | | | | | | | |
| H | Very qtz with tr of cubic py | | | | | | | |
| I | Big boulders of massive Gv boulders in main CK, in situ? | Tr Py | | | | | L-3500G/210N | Kli |
| J | Angular boulder of soft dark in qtz sweets in CK | tr Py Float | | | | | 3610E/210W | Kli |
| K | Magnetite-epidote skarn float in CK, strong magnetite | | | | | | 3190E/2270N | Kli |
| L | Hornblende chl. and silite w tr magnetite + talc-like siliceous | Float | | | | | | Area of frequent min float Kli |

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|----|---------|------|----|-----|------|---|-----|-----|---|------|-----|----|----|----|----|------|------|----|----|------|-----|---|------|---|------|---|----|------|-----|-----|
| 31 | KLP 133 | -3.0 | 20 | 0.2 | 5.19 | 2 | 813 | 0.3 | 5 | 0.89 | 0.3 | 28 | 12 | 12 | 86 | 5.06 | 2.06 | 10 | 19 | 2.19 | 646 | 2 | 0.09 | 6 | 0.12 | 7 | 96 | 0.25 | 171 | 147 |
|----|---------|------|----|-----|------|---|-----|-----|---|------|-----|----|----|----|----|------|------|----|----|------|-----|---|------|---|------|---|----|------|-----|-----|

27-29 GP

NORANDA DELTA LABORATORY

Geochemical Analysis

Project Name & No.: KLIYUL - 148

Geol.: T.W.

Date received: JULY 26

LAB CODE: 9307-031

Material: 67 Rx

Sheet: 1 of 2

Date completed: AUG. 04

Remarks: * Sample screened @ -35 MESH (0.5 mm)

□ Organic, & Humus, 5 SoKide

Au - 10.0 g sample digested with aqua-regia and determined by A.A. (D.L. 5 PPB)

ICP - 0.2 g sample digested with 3 ml HClO₄/HNO₃ (4:1) at 203 °C for 4 hours diluted to 10 ml with water. Luemm PS3000 ICP determined elemental contents.

N.B. The major oxide elements and Ba, Be, Ce, La, Li, Ga are rarely dissolved completely from geological materials with this acid dissolution method.

| T.T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Bc ppm | Bi ppm | Ca % | Cl ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm |
|----------|------------|--------|--------|------|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------|-------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|
| 156 | 378-A | 20 | 1.2 | 5.67 | 2 | 141 | 0.3 | 5 | 6.07 | 0.2 | 52 | 20 | 45 | 511 | 7.30 | 0.34 | 10 | 7 | 1.18 | 728 | 3 | 0.12 | 26 | 0.10 | 5 | 387 | 0.40 | 215 | 110 |
| 157 | B | 5 | 0.4 | 4.17 | 2 | 1051 | 0.2 | 5 | 0.51 | 0.2 | 20 | 6 | 35 | 30 | 3.64 | 1.63 | 6 | 9 | 0.92 | 244 | 2 | 0.11 | 7 | 0.05 | 2 | 59 | 0.19 | 128 | 50 |
| 158 | C | 5 | 0.2 | 3.57 | 9 | 746 | 0.2 | 5 | 1.02 | 0.2 | 32 | 16 | 49 | 36 | 5.52 | 1.26 | 10 | 13 | 1.63 | 905 | 3 | 0.21 | 7 | 0.08 | 2 | 64 | 0.32 | 183 | 75 |
| 159 | D | 280 | 0.4 | 3.20 | 14 | 1701 | 11.7 | 5 | 0.05 | 0.2 | 14 | 6 | 117 | 12 | 2.31 | 1.47 | 8 | 1 | 0.11 | 100 | 16 | 0.05 | 10 | 0.03 | 2 | 85 | 0.04 | 55 | 26 |
| 160 | E | 180 | 0.8 | 3.71 | 19 | 783 | 2.2 | 5 | 0.74 | 0.2 | 29 | 11 | 139 | 11 | 3.23 | 1.75 | 10 | 2 | 0.25 | 403 | 22 | 0.05 | 11 | 0.04 | 2 | 34 | 0.05 | 67 | 30 |
| 161 | F | 5 | 0.2 | 3.57 | 2 | 1338 | 1.0 | 5 | 2.87 | 0.2 | 58 | 8 | 81 | 24 | 3.06 | 1.53 | 21 | 4 | 0.62 | 689 | 4 | 0.15 | 10 | 0.08 | 2 | 95 | 0.04 | 80 | 43 |
| 162 | G | 30 | 0.2 | 4.96 | 4 | 453 | 0.9 | 5 | 4.37 | 0.2 | 49 | 20 | 77 | 71 | 6.68 | 1.13 | 14 | 36 | 3.08 | 895 | 1 | 0.22 | 34 | 0.09 | 3 | 134 | 0.08 | 258 | 121 |
| 163 | H | 5 | 0.2 | 3.07 | 2 | 957 | 0.8 | 5 | 1.79 | 0.2 | 56 | 7 | 85 | 9 | 2.91 | 1.22 | 20 | 8 | 0.31 | 510 | 4 | 0.12 | 10 | 0.08 | 2 | 46 | 0.05 | 68 | 45 |
| 164 | I | 20 | 0.4 | 4.40 | 10 | 176 | 0.4 | 5 | 3.32 | 0.2 | 46 | 36 | 112 | 259 | 5.79 | 0.65 | 12 | 17 | 3.17 | 1117 | 1 | 0.23 | 57 | 0.11 | 3 | 181 | 0.38 | 195 | 80 |
| 165 | J | 10 | 0.2 | 3.55 | 2 | 56 | 0.2 | 5 | 2.45 | 0.2 | 46 | 15 | 78 | 29 | 4.84 | 0.50 | 13 | 13 | 1.63 | 550 | 1 | 0.10 | 26 | 0.11 | 2 | 165 | 0.44 | 157 | 57 |
| 166 | K | 50 | 0.4 | 2.17 | 5 | 147 | 0.2 | 5 | 1.82 | 0.2 | 46 | 41 | 57 | 90 | 7.51 | 0.58 | 11 | 10 | 1.23 | 567 | 2 | 0.15 | 29 | 0.07 | 4 | 108 | 0.46 | 183 | 43 |
| 167 | L | 70 | 0.4 | 3.12 | 5 | 76 | 0.2 | 5 | 2.65 | 0.2 | 47 | 40 | 63 | 24 | 5.46 | 0.69 | 11 | 12 | 1.32 | 444 | 1 | 0.15 | 28 | 0.10 | 2 | 110 | 0.31 | 121 | 33 |
| 168 | M | 60 | 1.2 | 3.37 | 19 | 12 | 0.3 | 5 | 5.38 | 0.2 | 61 | 34 | 52 | 497 | 22.26 | 0.09 | 21 | 4 | 0.50 | 1510 | 3 | 0.07 | 25 | 0.10 | 32 | 117 | 0.13 | 105 | 58 |
| 170 | N | 30 | 0.4 | 3.24 | 19 | 13 | 0.3 | 5 | 7.64 | 0.2 | 57 | 17 | 58 | 228 | 21.19 | 0.06 | 14 | 5 | 0.47 | 2259 | 2 | 0.06 | 18 | 0.15 | 29 | 61 | 0.20 | 120 | 57 |
| 172 | O | 10 | 0.4 | 2.60 | 14 | 6 | 0.3 | 5 | 13.69 | 0.2 | 40 | 11 | 92 | 161 | 13.64 | 0.04 | 6 | 5 | 0.17 | 4245 | 4 | 0.04 | 9 | 0.09 | 18 | 42 | 0.07 | 80 | 27 |
| 173 | P | 5 | 0.4 | 2.50 | 14 | 42 | 0.3 | 5 | 12.28 | 0.2 | 45 | 11 | 74 | 169 | 10.75 | 0.17 | 11 | 7 | 0.45 | 3864 | 2 | 0.10 | 8 | 0.10 | 11 | 59 | 0.15 | 98 | 30 |
| 174 | Q | 1000 | 3.2 | 1.96 | 36 | 11 | 0.6 | 5 | 3.83 | 0.2 | 55 | 142 | 70 | 4014 | 17.92 | 0.11 | 23 | 6 | 0.63 | 1380 | 4 | 0.03 | 49 | 0.06 | 27 | 60 | 0.01 | 90 | 76 |
| 176 | R | 60 | 0.2 | 4.61 | 2 | 149 | 0.4 | 5 | 4.42 | 0.2 | 51 | 26 | 35 | 693 | 5.15 | 0.81 | 14 | 11 | 1.10 | 829 | 1 | 0.11 | 21 | 0.14 | 3 | 203 | 0.35 | 133 | 32 |
| 177 | S | 60 | 0.4 | 3.60 | 2 | 131 | 0.3 | 5 | 3.42 | 0.2 | 52 | 44 | 64 | 719 | 5.08 | 0.65 | 15 | 8 | 0.91 | 563 | 2 | 0.13 | 22 | 0.13 | 3 | 210 | 0.38 | 132 | 28 |
| 178 | T | 150 | 0.8 | 2.32 | 2 | 94 | 0.2 | 5 | 2.22 | 0.2 | 46 | 28 | 63 | 573 | 4.29 | 0.55 | 12 | 9 | 0.94 | 476 | 4 | 0.14 | 20 | 0.17 | 3 | 119 | 0.35 | 130 | 27 |
| 179 | U S | 100 | 1.6 | 4.33 | 7 | 8 | 0.4 | 5 | 8.25 | 0.2 | 49 | 68 | 53 | 1412 | 16.15 | 0.05 | 9 | 4 | 0.22 | 2213 | 2 | 0.04 | 17 | 0.09 | 19 | 174 | 0.07 | 185 | 42 |
| 181 | V | 120 | 0.8 | 4.14 | 19 | 38 | 0.6 | 5 | 6.91 | 0.2 | 56 | 13 | 58 | 339 | 19.13 | 0.13 | 17 | 9 | 0.21 | 1607 | 4 | 0.04 | 11 | 0.08 | 23 | 170 | 0.15 | 112 | 53 |
| 182 | W | 140 | 2.8 | 2.87 | 13 | 3 | 0.4 | 5 | 9.64 | 0.2 | 46 | 167 | 67 | 985 | 13.46 | 0.04 | 8 | 4 | 0.14 | 2245 | 1 | 0.03 | 28 | 0.05 | 12 | 99 | 0.03 | 92 | 35 |
| 184 | 379-A | 5 | 0.2 | 3.56 | 2 | 625 | 0.6 | 5 | 0.21 | 0.2 | 45 | 61 | 66 | 12000 | 3.35 | 1.02 | 24 | 12 | 0.39 | 1838 | 4 | 0.24 | 16 | 0.09 | 3 | 38 | 0.05 | 94 | 287 |
| 185 | B | 60 | 0.8 | 7.18 | 2 | 504 | 0.4 | 5 | 0.05 | 0.2 | 21 | 12 | 23 | 1798 | 6.68 | 1.40 | 13 | 44 | 1.56 | 402 | 11 | 0.49 | 11 | 0.11 | 2 | 57 | 0.08 | 191 | 180 |
| 186 | C | 80 | 0.8 | 7.42 | 2 | 482 | 0.4 | 5 | 0.04 | 0.2 | 19 | 6 | 23 | 334 | 6.71 | 1.28 | 11 | 47 | 1.43 | 146 | 11 | 0.61 | 10 | 0.11 | 3 | 71 | 0.07 | 181 | 173 |
| 187 | D | 160 | 0.8 | 6.77 | 2 | 298 | 0.4 | 5 | 2.27 | 0.2 | 51 | 2 | 21 | 147 | 5.95 | 0.79 | 14 | 46 | 1.88 | 697 | 2 | 0.29 | 6 | 0.10 | 8 | 230 | 0.30 | 161 | 188 |
| 188 | E | 110 | 1.2 | 8.76 | 2 | 805 | 0.4 | 5 | 0.08 | 0.2 | 32 | 7 | 19 | 402 | 5.51 | 2.91 | 16 | 38 | 1.22 | 294 | 2 | 0.36 | 6 | 0.10 | 2 | 52 | 0.07 | 129 | 88 |
| 189 | F | 40 | 0.8 | 6.23 | 2 | 218 | 0.3 | 5 | 4.35 | 0.2 | 52 | 10 | 49 | 553 | 6.77 | 0.75 | 13 | 10 | 1.03 | 515 | 5 | 0.48 | 10 | 0.11 | 2 | 145 | 0.45 | 174 | 41 |
| 190 | G | 5 | 0.4 | 2.63 | 6 | 56 | 0.2 | 5 | 2.69 | 0.4 | 46 | 25 | 99 | 182 | 5.83 | 0.42 | 12 | 12 | 1.84 | 906 | 9 | 0.17 | 41 | 0.08 | 6 | 113 | 0.46 | 181 | 65 |
| 191 | H | 10 | 0.2 | 1.60 | 10 | 268 | 0.5 | 5 | 0.20 | 0.4 | 36 | 11 | 149 | 7324 | 1.32 | 0.60 | 26 | 8 | 0.35 | 283 | 8 | 0.12 | 9 | 0.04 | 6 | 20 | 0.09 | 41 | 108 |
| 192 | I | 5 | 0.4 | 4.21 | 2 | 197 | 0.3 | 5 | 3.48 | 0.5 | 42 | 26 | 80 | 1939 | 5.85 | 0.56 | 10 | 14 | 2.39 | 743 | 1 | 0.32 | 31 | 0.09 | 3 | 150 | 0.43 | 211 | 58 |
| 193 | J | 2000 | 8.8 | 4.37 | 4 | 170 | 0.3 | 5 | 2.52 | 1.2 | 51 | 79 | 28 | 9804 | 7.84 | 0.61 | 16 | 22 | 1.89 | 670 | 202 | 0.09 | 33 | 0.19 | 19 | 404 | 0.22 | 153 | 88 |
| 194 | K | 130 | 0.8 | 2.28 | 2 | 202 | 0.2 | 5 | 0.46 | 0.3 | 21 | 14 | 48 | 790 | 5.63 | 0.76 | 8 | 18 | 1.92 | 314 | 2 | 0.11 | 8 | 0.12 | 2 | 16 | 0.34 | 227 | 27 |
| 195 | 379-L | 610 | 3.6 | 5.17 | 2 | 309 | 0.3 | 5 | 3.29 | 0.4 | 41 | 9 | 46 | 3991 | 5.77 | 1.16 | 10 | 21 | 1.49 | 1230 | 8 | 0.07 | 12 | 0.08 | 2 | 120 | 0.38 | 167 | 70 |

| T.T. No. | SAMPLE No. | An ppb | Ag ppm | Al % | As ppm | Ba ppm | Bc ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cs ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | |
|----------|------------|--------|--------|------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|-------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|-----|
| 196 | 379 - M | 60 | 0.4 | 3.50 | 2 | 400 | 0.2 | 5 | 3.16 | 0.6 | 44 | 50 | 59 | 276 | 7.89 | 0.78 | 11 | 16 | 3.02 | 1081 | 1 | 0.25 | 30 | 0.08 | 2 | 94 | 0.49 | 218 | 80 |
| 197 | N | 430 | 5.2 | 4.20 | 3 | 107 | 0.3 | 5 | 2.22 | 0.9 | 39 | 25 | 85 | 3306 | 7.86 | 0.63 | 11 | 29 | 3.38 | 1377 | 3 | 0.07 | 29 | 0.08 | 8 | 37 | 0.08 | 255 | 128 |
| 198 | O | 200 | 0.4 | 2.63 | 8 | 42 | 0.2 | 5 | 2.06 | 0.2 | 37 | 17 | 75 | 118 | 6.54 | 0.19 | 8 | 8 | 2.11 | 513 | 1 | 0.15 | 36 | 0.07 | 2 | 113 | 0.47 | 191 | 42 |
| 201 | P | 5 | 0.2 | 3.50 | 10 | 90 | 0.7 | 5 | 3.03 | 0.5 | 73 | 16 | 42 | 132 | 4.45 | 0.15 | 27 | 16 | 1.46 | 921 | 1 | 0.16 | 11 | 0.15 | 4 | 648 | 0.41 | 160 | 81 |
| 202 | Q | 5 | 1.2 | 6.12 | 7 | 32 | 0.7 | 5 | 6.10 | 0.2 | 73 | 19 | 66 | 320 | 23.74 | 0.08 | 27 | 12 | 1.16 | 1374 | 5 | 0.06 | 34 | 0.12 | 32 | 374 | 0.24 | 181 | 72 |
| 204 | R | 4400 | 10.4 | 4.47 | 5 | 8 | 0.6 | 5 | 7.56 | 0.2 | 60 | 26 | 163 | 13000 | 13.03 | 0.03 | 18 | 4 | 0.18 | 614 | 6 | 0.03 | 51 | 0.59 | 11 | 267 | 0.24 | 264 | 66 |
| 205 | S | 4600 | 4.8 | 1.97 | 19 | 42 | 1.2 | 5 | 4.92 | 0.2 | 55 | 19 | 74 | 794 | 27.18 | 0.12 | 18 | 9 | 0.85 | 1074 | 80 | 0.06 | 91 | 0.15 | 49 | 67 | 0.07 | 721 | 70 |
| 206 | T | 150 | 1.2 | 1.99 | 2 | 123 | 0.2 | 5 | 3.35 | 0.2 | 55 | 39 | 77 | 642 | 3.04 | 0.35 | 14 | 6 | 0.38 | 545 | 6 | 0.09 | 14 | 0.15 | 2 | 127 | 0.32 | 108 | 21 |
| 207 | U | 90 | 0.4 | 4.14 | 2 | 254 | 0.4 | 5 | 3.14 | 0.2 | 48 | 26 | 111 | 366 | 5.32 | 0.83 | 14 | 14 | 2.05 | 1008 | 1 | 0.29 | 50 | 0.15 | 2 | 339 | 0.36 | 123 | 75 |
| 208 | V | 10 | 0.2 | 0.10 | 2 | 6 | 0.2 | 5 | 0.04 | 0.2 | 5 | 2 | 364 | 36 | 1.45 | 0.01 | 1 | 1 | 0.08 | 47 | 15 | 0.03 | 5 | 0.01 | 2 | 3 | 0.02 | 24 | 4 |
| 209 | 379 - W | 10 | 0.4 | 4.26 | 2 | 165 | 0.2 | 5 | 3.83 | 0.2 | 42 | 20 | 44 | 214 | 7.22 | 0.42 | 10 | 10 | 2.50 | 1486 | 1 | 0.21 | 21 | 0.09 | 2 | 107 | 0.55 | 300 | 102 |
| 210 | 380 - A | 30 | 0.8 | 2.83 | 3 | 117 | 0.2 | 5 | 2.69 | 0.2 | 41 | 36 | 58 | 348 | 4.20 | 0.52 | 9 | 7 | 0.45 | 251 | 10 | 0.12 | 23 | 0.10 | 2 | 206 | 0.38 | 109 | 25 |
| 211 | B | 140 | 1.2 | 3.29 | 13 | 92 | 0.3 | 5 | 1.08 | 0.5 | 37 | 29 | 59 | 437 | 5.97 | 0.54 | 15 | 22 | 2.43 | 481 | 4 | 0.09 | 19 | 0.13 | 5 | 104 | 0.30 | 175 | 41 |
| 212 | C | 20 | 0.8 | 3.09 | 8 | 226 | 0.2 | 5 | 1.66 | 0.2 | 36 | 20 | 24 | 146 | 6.79 | 0.97 | 10 | 16 | 2.45 | 727 | 1 | 0.16 | 7 | 0.13 | 2 | 39 | 0.53 | 294 | 48 |
| 213 | D | 5 | 0.4 | 4.67 | 2 | 232 | 0.6 | 5 | 4.05 | 0.2 | 58 | 10 | 42 | 30 | 3.97 | 0.68 | 20 | 9 | 1.16 | 823 | 3 | 0.11 | 17 | 0.12 | 4 | 633 | 0.24 | 103 | 71 |
| 214 | E | 20 | 1.2 | 2.96 | 9 | 66 | 0.2 | 5 | 2.77 | 0.2 | 41 | 31 | 121 | 28 | 5.16 | 0.39 | 10 | 9 | 2.14 | 552 | 2 | 0.14 | 55 | 0.09 | 2 | 136 | 0.35 | 151 | 45 |
| 215 | F | 2300 | 4.0 | 2.96 | 54 | 793 | 0.7 | 5 | 0.29 | 0.2 | 23 | 5 | 117 | 12 | 2.87 | 1.39 | 10 | 2 | 0.14 | 170 | 10 | 0.05 | 7 | 0.04 | 722 | 23 | 0.04 | 57 | 115 |
| 216 | G | 440 | 6.4 | 2.59 | 7 | 238 | 0.2 | 5 | 3.08 | 0.3 | 43 | 23 | 56 | 3853 | 5.42 | 0.57 | 11 | 14 | 2.05 | 746 | 5 | 0.08 | 24 | 0.09 | 12 | 90 | 0.27 | 208 | 63 |
| 217 | H | 5 | 0.8 | 3.56 | 6 | 419 | 0.3 | 5 | 2.61 | 0.2 | 43 | 17 | 49 | 143 | 4.45 | 1.05 | 11 | 15 | 2.13 | 620 | 17 | 0.09 | 22 | 0.11 | 2 | 122 | 0.41 | 220 | 36 |
| 218 | I | 5 | 0.8 | 4.30 | 3 | 293 | 0.3 | 5 | 3.79 | 0.2 | 51 | 19 | 30 | 411 | 5.05 | 0.72 | 15 | 13 | 1.54 | 598 | 91 | 0.09 | 11 | 0.14 | 2 | 329 | 0.41 | 195 | 33 |
| 219 | J | 5 | 1.2 | 4.50 | 4 | 374 | 0.3 | 5 | 3.75 | 0.2 | 54 | 22 | 27 | 555 | 5.06 | 0.96 | 16 | 13 | 1.61 | 606 | 9 | 0.08 | 11 | 0.14 | 5 | 317 | 0.40 | 198 | 32 |
| 220 | K | 5 | 1.2 | 4.17 | 2 | 408 | 0.3 | 5 | 3.45 | 0.2 | 52 | 15 | 29 | 546 | 4.50 | 0.95 | 15 | 12 | 1.42 | 499 | 3 | 0.09 | 10 | 0.13 | 2 | 309 | 0.40 | 176 | 27 |
| 221 | L | 40 | 2.4 | 3.68 | 12 | 281 | 0.5 | 5 | 3.04 | 0.4 | 48 | 60 | 143 | 1603 | 7.15 | 0.58 | 17 | 27 | 3.25 | 856 | 26 | 0.07 | 58 | 0.09 | 5 | 63 | 0.36 | 251 | 79 |
| 222 | M | 5 | 0.8 | 4.23 | 2 | 166 | 0.3 | 5 | 3.27 | 0.2 | 46 | 40 | 119 | 1106 | 7.12 | 0.39 | 13 | 21 | 4.05 | 978 | 8 | 0.09 | 59 | 0.09 | 2 | 131 | 0.49 | 282 | 51 |
| 223 | N | 5 | 1.2 | 4.38 | 2 | 171 | 0.3 | 5 | 3.61 | 0.2 | 46 | 39 | 118 | 1142 | 6.59 | 0.39 | 12 | 20 | 3.80 | 964 | 4 | 0.08 | 61 | 0.08 | 3 | 215 | 0.47 | 267 | 47 |
| 224 | O | 160 | 0.8 | 0.69 | 8 | 177 | 0.3 | 5 | 5.06 | 0.2 | 42 | 10 | 165 | 85 | 2.71 | 0.29 | 7 | 4 | 0.51 | 779 | 10 | 0.07 | 13 | 0.04 | 5 | 141 | 0.03 | 66 | 47 |
| 225 | P | 130 | 2.0 | 1.80 | 11 | 403 | 0.6 | 5 | 5.55 | 0.2 | 43 | 38 | 31 | 442 | 6.16 | 0.82 | 8 | 6 | 1.25 | 1032 | 5 | 0.09 | 18 | 0.09 | 9 | 201 | 0.10 | 97 | 64 |
| 226 | Q | 20 | 0.2 | 3.79 | 3 | 201 | 0.3 | 5 | 3.68 | 0.2 | 45 | 41 | 131 | 1199 | 6.64 | 0.42 | 12 | 19 | 3.34 | 924 | 11 | 0.08 | 54 | 0.08 | 2 | 168 | 0.43 | 250 | 46 |
| 227 | R | 5 | 0.2 | 4.15 | 7 | 178 | 0.3 | 5 | 4.07 | 0.2 | 44 | 39 | 107 | 1272 | 5.96 | 0.41 | 11 | 17 | 3.24 | 848 | 15 | 0.10 | 54 | 0.08 | 2 | 195 | 0.45 | 251 | 42 |
| 228 | S | 5 | 0.8 | 4.04 | 3 | 154 | 0.3 | 5 | 3.54 | 0.2 | 43 | 39 | 128 | 1070 | 6.82 | 0.41 | 12 | 22 | 3.85 | 919 | 5 | 0.08 | 57 | 0.08 | 2 | 115 | 0.48 | 283 | 50 |
| 229 | T | 5 | 0.2 | 3.71 | 2 | 117 | 0.2 | 5 | 3.37 | 0.2 | 41 | 20 | 109 | 193 | 5.52 | 0.40 | 11 | 12 | 2.03 | 539 | 4 | 0.10 | 43 | 0.08 | 2 | 189 | 0.43 | 206 | 37 |
| 230 | 380 - U | 10 | 0.8 | 2.83 | 2 | 85 | 0.2 | 5 | 2.69 | 0.2 | 40 | 21 | 138 | 287 | 6.64 | 0.35 | 10 | 8 | 1.14 | 318 | 19 | 0.07 | 40 | 0.07 | 2 | 188 | 0.36 | 160 | 27 |

LAB _____

PROJECT NO. 148 PROPERTY KLIYUL

CERT. NO. _____

GRID REFERENCE _____

67 Ra

SAMPLE REPORT

9307

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | | CO-ORDINA | | |
|----------|---|-------|---------|--------|--|--|-----------|-------|---------|
| | | | | | | | | | |
| A | Silicified volc, 10% fgd Py, local ep. alt. | | | | | | L-5800E | 2850 | TWC |
| B | Pyritic andosite (bleached 5% Py Pr) | gnab | | | | | L-26N | 2150E | ✓ " 30" |
| C | Pyritic andosite, wkly silt + ser ~ 10% Py | gnab | | | | | L-2600N | 2000E | " 30" |
| D | Qtz - carb vein, irregular in shape carb 200' int-in fm | gnab | | | | | 3160N | 4250E | 30' W / |
| E | Qtz - carb - py vein sub androp | gnab | | | | | " | " | 30' W / |
| F | Altered granite - carb to Py - fractured volat | gnab | | | | | " | " | 30' W / |
| G | Qtz - carb veins + serents | gnab | | | | | 3160N | 4220E | 30' W / |
| H | Weakly carb andosite - (along fractures) chf | gnab | | | | | 3120N | 4210E | 30' W / |
| I | Gossanous, andosite, py, wk silt | gnab | | | | | L-3300N | 3620E | 30' W / |
| J | wkly Sericitic silt andosite - fractured | gnab | | | | | 3325N | 3600E | 30' W / |
| K | Andosite with wkly pyritic inlets + diss Py + silic | Talus | | | | | 3350N | 2690E | 30' W / |
| L | Brecciated/fragmental andosite ~ 15% Py + silt | Talus | | | | | 3420N | 2768E | 30' W / |
| M | Magnetite - epidote + horn ^{bl} skarn | chip | 2m chip | | | | | | " |
| N | Magnetite - epidote + calc - silicite " | chip | 2m chip | | | | | | " |
| O | " " " " " | chip | 1.0m | | | | | | " |
| P | Calc - sil epi wk magnetite " | chip | 1.5m | | | | | | " |
| Q | massive magnetite - pyrite + epi + malachite | chip | 1.5m | | | | | | " |
| R | " " " " " + malachite " | chip | 2.0m | | | | | | " |
| S | " " " " " + malachite " | chip | 2.0m | | | | | | " |
| T | Calc - silicite skarn / hornbls to q silic | chip | 1.0m | | | | | | " |
| U | Massive magnetite pyrite epi - rpl skarn | gnab | | | | | | | " |
| V | Epi - chl - magnetite, pyrite skarn | chip | 1.0m | | | | | | " |
| W | magnetite - pyrite - epidote - mass skarn | chip | 2.0m | | | | | | " |

NEW SKARN SHOWING

For location

centered @ L-265E/3350N

Exposed dimension

11m wide and 25m long

LAB _____

PROJECT NO. 148 PROPERTY kliyul

CERT. NO. _____

GRID REFERENCE _____

DATE _____

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | CO-ORDINATES | | |
|----------|---|----------|---------|--------|----|--------------|-------|------|
| | | | | Cu | Au | | | |
| A | And tuff (?) Mc on surface, no vis. sulf., ^{poorly developed} siliceous flooding | o/c | Grabr | Cu | Au | 2660N | 785E | ✓ LE |
| B | 2 Similar to "A" but some surfaces show | o/c | 2m chip | Cu | Au | 2660N | 790E | ✓ K |
| C | Slickensides | o/c | 2m chip | Cu | Au | 2660N | 790E | ✓ K |
| D | Sheared slightly chl. volc. tuff, 2% Py, rusty W.S. | o/c | Grabr | Cu | Au | 2760N | 800E | ✓ K |
| E | Sheared chloritic, sericitic volc., 3%-5% mgd Py | o/c | Grabr | Cu | Au | 3000N | 750E | ✓ K |
| F | Silicified tuff, ep-3% Py alt., Py also in frac | o/c | Grabr | Cu | Au | 3300N | 1050E | ✓ K |
| G | Hornfelsed volc., 1-2% diss Py, Py in frac., rusty WS | Grabr/oc | Grabr | Cu | Au | 4200N | 4500E | ✓ K |
| H | Int., no visible sulfides, malachite on surface | Talus | | Cu | Au | 3350N | 3580E | ✓ K |
| I | Augite porphyritic volc., malachite rare f.g.d. Py | Talus | | Cu | Au | 3550N | 3400E | ✓ K |
| J | Alt. volc w stringer carb/silica vein. Malachite, trace Py | Talus | | Cu | Au | 3550N | 3650E | ✓ K |
| K | Silicified aug. porph. volc., 3% mgd Py | o/c | Grabr | Cu | Au | 3150N | 3876E | ✓ K |
| L | Qz vein (10cm) in calcareous and ^{vein hosts trace Py} magnetic, malachite | Talus | | Cu | Au | 3112N | 3585E | ✓ K |
| M | Volc, trace dissem f.g. Py, Py on fractures, permineralized | Talus | | Cu | Au | 3110N | 3600E | ✓ K |
| N | Volc, poorly dev. silica flooding, magnetic, malach, ep, Py | Talus | | Cu | Au | 3105N | 3590E | ✓ K |
| O | Volc., 4-5% mgd. Py and Py in frac., rusty WS | o/c | Grabr | { | { | 4700E | 4430N | " |
| P | Epithermal feldspar porphyry dyke | o/c | Grabr | { | { | 4700E | 4360N | " |
| Q | Magnetite skarn, qz veining, minor diss Py | Talus | | Cu | Au | 3350N | 2487E | ✓ K |
| R | Volc(?) magnetic, minor silica flooding, 7% mgd Py | Talus | | { | { | 3350N | 2483E | ✓ K |
| S | Magnetite skarn, epidote, silica, 3% fgd Py, rare malach. | Talus | | { | { | 3350N | 2483E | ✓ K |
| T | Silicified banded tuff, rare epidote, minor Mc, trace Py | Talus | | Cu | Au | 3350N | 2450E | ✓ K |
| U | Andesite w ep-calc stringers, 2% mgd diss Py, Az malachite fractures | Talus | | Cu | Au | 3350N | 2400E | ✓ K |
| V | Qz vein in aug. porph. volc., no visible sulfides, rusty WS | Talus | | " | " | 3200N | 5175E | ✓ K |
| W | Aug. porph. volc., epidote alteration, 2%-3% fgd Py, minor qz veins | Talus | | " | " | 3175N | 5900E | ✓ K |

AB _____

PROJECT NO. 148 PROPERTY KLIYUL

N.T.S. 94D/8E

SERT. NO. _____

GRID REFERENCE _____

DATE JULY/93

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | CO-ORDINATES | | SAMPLER | |
|----------|---|-------|-------|-----------------------------------|--|--------------|-------|---------|------|
| | | | | | | | | | |
| A | Ep. alt. volc. br, 5% Py arsenic w ep, local contact. | | | | | L-2610E | 3950N | Joh TUB | |
| B | Andesite 3-5% S(P ₂) epi. web veinlets | Talus | | | | 3400N | 2750E | Sch V | |
| C | Andesite mass 2-3% P ₂ | Grubs | | | | 3400N | 2800E | Sch V | |
| D | Mud. sp. in massive syenite / 100% chl | Grubs | | | | L-47E | 4450N | Sch | |
| E | Gossan 3-5% P ₂ epi | Talus | | | | 4625E | 4450N | Jeh I | |
| F | Carb. sp. (SiO ₂) rounded sub angular | chip | 1.0m | | | 4740E | 2950N | Cray V | |
| G | Alt. chl - carb - epy vein show zone | chip | 1.0m | same as 316-11 | | L-5800E | 2412N | Cray | |
| H | Propylitized diorite 5 to epy + py intense | chip | 2.0m | | | | | | Cray |
| I | | | | } showing L-5800E - 5770E / 2415N | | | | | |
| J | | | | | | | | | |
| K | | | | | | | | | |
| L | sheared, cherted, carb. mud to epy + py diorite | chip | 2m | | | | | | |
| M | " " mal + epy | " | 2m | | | | | | |
| N | " " " " | " | 2m | | | | | | |
| O | Diabase - carb. alt. Irregular veins discontinuous | Grubs | | | | L-2100N | 2030E | Kli | |
| P | Silicified carbonated seds? w to py | " | | | | | | Kli | |
| Q | Same as N | | 2m | } showing L-5800E - 5770E / 2415N | | | | Cray | |
| R | same as Q | | 2m | | | | | | Cray |
| S | sheared diorite w mal chert veins py chl - epi | | 2m | | | | | | Cray |
| T | 2. breccia matrix and veins py - epy - vein, has mal | | 2m | | | | | Cray | |
| U | Gossan pylic | Grubs | | | | | | Cray | |
| V | | | | | | | | | |
| W | | | | | | | | | |

VOID

Total = 21 Sample

NORANDA DELTA LABORATORY

Geochemical Analysis

Project Name & No.: GOLDEN R. JO - 183/184

Geol.: T.W.

Date received: SEP. 25

LAB CODE: 9309-034

Material: 23 rx +1

Sheet: 1 of 1

Date completed: OCT. 05

Remarks: * Sample screened @ -35 MESH (0.5 mm)

** Organic, A Humus, S Sulfide

Au - 10.0 g sample digested with aqua-regia and determined by A.A. (D.L. 5 PPB)

ICP - 0.2 g sample digested with 3 ml HClO₄/HNO₃ (4:1) at 203 °C for 4 hours diluted to 10 ml with water. Leeman FS3000 ICP determined elemental contents.

N.B. The major oxide elements and Ba, Be, Ce, La, Li, Ga are rarely dissolved completely from geological materials with this acid dissolution method.

| T.T. No. | SAMPLE No. | As | Ag | Al | Ar | Ba | Be | Bi | Ca | Cd | Ce | Co | Cr | Cu | Fe | K | La | Li | Mg | Mn | Mo | Na | Ni | P | Pb | Sr | Tl | V | Zn |
|----------|----------------|------|------|------|-----|-----|-----|-----|-------|-----|-----|-----|-----|-------|-------|------|-----|-----|------|------|-----|------|-----|------|-----|-----|------|-----|-----|
| | | ppb | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm |
| 119 | 391 - A | 80 | 0.2 | 6.41 | 2 | 414 | 0.2 | 5 | 2.31 | 0.3 | 56 | 9 | 27 | 590 | 7.99 | 0.76 | 10 | 21 | 3.30 | 1444 | 1 | 0.07 | 12 | 0.06 | 4 | 127 | 0.54 | 387 | 181 |
| 120 | B | 80 | 1.6 | 4.04 | 2 | 574 | 0.3 | 5 | 0.84 | 0.2 | 40 | 8 | 31 | 203 | 3.76 | 0.77 | 9 | 12 | 0.96 | 578 | 1 | 0.16 | 6 | 0.08 | 2 | 115 | 0.04 | 81 | 172 |
| 121 | C | 1400 | 0.2 | 3.69 | 2 | 951 | 0.4 | 5 | 1.34 | 0.8 | 48 | 11 | 32 | 2911 | 2.63 | 0.91 | 13 | 11 | 0.85 | 1310 | 1 | 0.12 | 10 | 0.06 | 6 | 93 | 0.04 | 68 | 261 |
| 122 | D | 10 | 0.2 | 5.77 | 2 | 467 | 0.4 | 5 | 3.15 | 0.2 | 70 | 14 | 20 | 316 | 4.46 | 0.79 | 13 | 17 | 1.30 | 1165 | 1 | 0.14 | 10 | 0.09 | 2 | 239 | 0.07 | 99 | 106 |
| 123 | E | 90 | 0.2 | 3.16 | 2 | 156 | 0.3 | 5 | 2.37 | 0.2 | 64 | 53 | 52 | 495 | 6.17 | 1.00 | 11 | 14 | 1.32 | 772 | 4 | 0.09 | 21 | 0.17 | 3 | 91 | 0.35 | 149 | 50 |
| 124 | F | 70 | 0.2 | 2.59 | 7 | 88 | 0.3 | 5 | 2.73 | 0.2 | 64 | 43 | 48 | 672 | 3.25 | 0.58 | 12 | 9 | 0.76 | 820 | 1 | 0.10 | 18 | 0.16 | 2 | 96 | 0.34 | 123 | 35 |
| 125 | G | 230 | 0.2 | 4.12 | 3 | 79 | 0.4 | 5 | 4.43 | 0.2 | 74 | 46 | 29 | 278 | 6.23 | 0.52 | 15 | 8 | 0.58 | 735 | 2 | 0.09 | 21 | 0.17 | 2 | 304 | 0.34 | 115 | 24 |
| 126 | H | 1030 | 2.4 | 4.18 | 2 | 534 | 0.2 | 8 | 2.07 | 0.4 | 69 | 31 | 25 | 3830 | 8.98 | 1.68 | 19 | 23 | 2.27 | 1036 | 1 | 0.08 | 13 | 0.15 | 2 | 117 | 0.36 | 211 | 74 |
| 127 | I | 1030 | 4.4 | 2.31 | 29 | 8 | 0.4 | 5 | 9.62 | 0.2 | 103 | 50 | 48 | 3244 | 14.30 | 0.05 | 31 | 4 | 0.25 | 2321 | 3 | 0.04 | 28 | 0.09 | 5 | 99 | 0.13 | 121 | 42 |
| 128 | J | 55 | 0.2 | 0.81 | 36 | 55 | 0.6 | 5 | 1.81 | 4.5 | 84 | 34 | 38 | 264 | 31.35 | 0.10 | 25 | 3 | 0.36 | 868 | 5 | 0.04 | 39 | 0.12 | 44 | 31 | 0.04 | 237 | 70 |
| 130 | K | 640 | 1.2 | 1.00 | 132 | 7 | 0.3 | 5 | 13.56 | 0.2 | 78 | 45 | 54 | 1453 | 16.51 | 0.04 | 6 | 5 | 0.11 | 3763 | 4 | 0.03 | 9 | 0.08 | 6 | 31 | 0.02 | 50 | 25 |
| 131 | L | 1200 | 2.8 | 0.81 | 92 | 9 | 0.4 | 5 | 14.67 | 0.2 | 61 | 56 | 61 | 6361 | 15.31 | 0.03 | 5 | 6 | 0.10 | 3904 | 4 | 0.03 | 10 | 0.08 | 3 | 15 | 0.01 | 44 | 31 |
| 132 | M | 1010 | 0.8 | 1.06 | 39 | 30 | 0.7 | 5 | 1.27 | 1.7 | 132 | 244 | 54 | 511 | 30.95 | 0.10 | 82 | 3 | 0.31 | 534 | 23 | 0.03 | 71 | 0.11 | 45 | 35 | 0.04 | 210 | 61 |
| 134 | N | 5 | 0.2 | 2.03 | 3 | 289 | 0.2 | 5 | 2.39 | 0.2 | 57 | 17 | 117 | 167 | 4.51 | 0.50 | 14 | 10 | 1.02 | 579 | 2 | 0.11 | 37 | 0.07 | 2 | 62 | 0.28 | 126 | 49 |
| 135 | O | 40 | 0.2 | 4.73 | 4 | 470 | 0.3 | 5 | 3.80 | 0.2 | 60 | 30 | 14 | 181 | 4.64 | 1.36 | 10 | 19 | 1.28 | 907 | 1 | 0.11 | 8 | 0.13 | 2 | 114 | 0.25 | 135 | 33 |
| 136 | P | 50 | 0.2 | 4.88 | 2 | 266 | 0.4 | 5 | 3.75 | 0.3 | 61 | 37 | 23 | 391 | 5.51 | 1.17 | 12 | 16 | 1.59 | 586 | 1 | 0.11 | 25 | 0.10 | 2 | 141 | 0.37 | 173 | 48 |
| 137 | Q | 5 | 0.2 | 3.93 | 2 | 676 | 0.2 | 5 | 1.78 | 0.2 | 53 | 25 | 21 | 102 | 6.96 | 1.66 | 11 | 21 | 2.83 | 903 | 1 | 0.24 | 22 | 0.09 | 2 | 91 | 0.48 | 238 | 74 |
| 138 | R | 210 | 0.2 | 4.46 | 2 | 188 | 0.2 | 8 | 2.55 | 0.2 | 55 | 56 | 20 | 90 | 6.41 | 1.07 | 9 | 13 | 1.36 | 527 | 1 | 0.10 | 6 | 0.12 | 2 | 142 | 0.29 | 161 | 37 |
| 139 | S | 150 | 0.2 | 2.77 | 16 | 65 | 0.2 | 5 | 2.09 | 0.2 | 49 | 47 | 55 | 78 | 6.52 | 0.41 | 9 | 16 | 2.19 | 825 | 1 | 0.13 | 25 | 0.08 | 2 | 83 | 0.33 | 165 | 55 |
| 140 | T | 70 | 0.2 | 2.52 | 3 | 49 | 0.2 | 5 | 2.06 | 0.2 | 56 | 64 | 63 | 27 | 6.24 | 0.57 | 12 | 11 | 1.39 | 530 | 1 | 0.12 | 24 | 0.09 | 2 | 83 | 0.26 | 149 | 36 |
| 141 | U | 40 | 0.2 | 1.70 | 4 | 88 | 0.2 | 5 | 1.30 | 0.2 | 41 | 39 | 52 | 29 | 4.91 | 0.52 | 9 | 12 | 1.05 | 369 | 2 | 0.08 | 16 | 0.07 | 2 | 47 | 0.28 | 118 | 28 |
| 142 | V _B | 3600 | 15.6 | 2.30 | 4 | 59 | 0.2 | 13 | 4.46 | 0.5 | 70 | 705 | 38 | 14000 | 7.98 | 0.16 | 20 | 3 | 0.33 | 1019 | 4 | 0.02 | 25 | 0.05 | 5 | 168 | 0.01 | 54 | 39 |
| 143 | 391 - W | 1500 | 2.4 | 2.34 | 22 | 31 | 0.7 | 5 | 4.12 | 0.4 | 77 | 16 | 150 | 3207 | 24.70 | 0.10 | 19 | 4 | 0.43 | 1159 | 7 | 0.06 | 59 | 0.22 | 20 | 125 | 0.12 | 190 | 75 |
| 145 | unmarked | 840 | 1.2 | 0.77 | 180 | 3 | 0.3 | 5 | 14.29 | 0.2 | 68 | 62 | 63 | 5311 | 16.87 | 0.03 | 4 | 3 | 0.09 | 4423 | 4 | 0.03 | 12 | 0.10 | 4 | 17 | 0.01 | 41 | 31 |

06/06 Vanc aff

RE

| T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Bc ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe ppm | K ppm | La ppm | Li ppm | Mg ppm | Mn ppm | Mo ppm | Na ppm | Ni ppm | P ppm | Pb ppm | Sr ppm | Ti ppm | V ppm | Zn ppm | 0307-023 |
|--------|------------|--------|--------|------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------|--------|--------|-------|--------|--------|--------|-------|--------|----------|
| 29 | 376 - A | 80 | 1.2 | 3.97 | 17 | 1913 | 0.3 | 34 | 0.45 | 0.2 | 30 | 48 | 55 | 591 | 6.43 | 1.77 | 9 | 8 | 0.75 | 249 | 8 | 0.05 | 12 | 0.12 | 2 | 140 | 0.43 | 177 | 60 | |
| 30 | B s | 50 | 0.4 | 5.49 | 11 | 2407 | 0.4 | 8 | 0.62 | 0.4 | 39 | 45 | 49 | 631 | 6.17 | 2.36 | 10 | 12 | 1.21 | 350 | 4 | 0.06 | 15 | 0.07 | 5 | 35 | 0.26 | 215 | 122 | |
| 31 | C | 130 | 6.4 | 1.34 | 4 | 185 | 0.2 | 13 | 3.31 | 0.5 | 49 | 42 | 110 | 7532 | 4.21 | 0.23 | 14 | 11 | 0.98 | 485 | 238 | 0.07 | 29 | 0.07 | 2 | 59 | 0.14 | 119 | 39 | |
| 32 | D | 10 | 0.2 | 3.66 | 2 | 129 | 0.2 | 6 | 0.86 | 0.4 | 23 | 9 | 83 | 141 | 3.93 | 0.14 | 11 | 21 | 3.03 | 1098 | 6 | 0.16 | 20 | 0.09 | 2 | 63 | 0.21 | 138 | 153 | |
| 33 | E | 10 | 0.2 | 3.60 | 7 | 36 | 0.2 | 5 | 4.25 | 0.2 | 51 | 38 | 39 | 710 | 6.20 | 0.24 | 12 | 4 | 0.16 | 456 | 7 | 0.10 | 15 | 0.13 | 2 | 190 | 0.26 | 96 | 42 | |
| 34 | F | 10 | 0.4 | 5.44 | 2 | 129 | 0.3 | 6 | 5.28 | 0.2 | 61 | 20 | 32 | 401 | 6.54 | 0.39 | 13 | 9 | 1.16 | 555 | 3 | 0.10 | 16 | 0.10 | 2 | 268 | 0.43 | 264 | 32 | |
| 35 | G | 20 | 0.2 | 4.49 | 2 | 261 | 0.2 | 5 | 3.84 | 0.2 | 54 | 18 | 29 | 596 | 4.17 | 0.56 | 12 | 7 | 0.74 | 288 | 5 | 0.11 | 7 | 0.12 | 2 | 246 | 0.29 | 146 | 31 | |
| 36 | H | 5500 | 26.0 | 0.62 | 7 | 32 | 0.2 | 13 | 1.20 | 0.8 | 24 | 18 | 216 | 14000 | 4.02 | 0.09 | 6 | 5 | 0.55 | 314 | 20 | 0.06 | 12 | 0.03 | 2 | 15 | 0.06 | 59 | 24 | |
| 37 | I | 20 | 0.2 | 3.55 | 2 | 128 | 0.2 | 5 | 3.49 | 0.2 | 47 | 19 | 39 | 232 | 5.77 | 0.38 | 12 | 10 | 1.84 | 566 | 2 | 0.18 | 23 | 0.12 | 2 | 134 | 0.46 | 222 | 36 | |
| 38 | J | 5 | 0.2 | 3.16 | 5 | 11 | 0.2 | 5 | 4.02 | 0.2 | 46 | 37 | 42 | 433 | 4.98 | 0.12 | 9 | 4 | 0.45 | 440 | 2 | 0.13 | 28 | 0.09 | 2 | 97 | 0.41 | 182 | 24 | |
| 39 | K | 20 | 0.2 | 0.60 | 3 | 19 | 0.2 | 5 | 0.91 | 0.2 | 22 | 11 | 181 | 200 | 2.19 | 0.04 | 11 | 1 | 0.09 | 255 | 8 | 0.11 | 29 | 0.06 | 2 | 41 | 0.22 | 56 | 9 | |
| 40 | L | 10 | 0.2 | 4.00 | 38 | 125 | 0.2 | 7 | 2.59 | 0.3 | 34 | 32 | 103 | 145 | 6.67 | 0.12 | 12 | 49 | 2.95 | 926 | 4 | 0.11 | 56 | 0.06 | 2 | 85 | 0.03 | 334 | 138 | |
| 41 | M | 10 | 0.4 | 4.49 | 13 | 75 | 0.4 | 12 | 4.39 | 0.4 | 61 | 31 | 108 | 161 | 6.62 | 0.39 | 18 | 42 | 2.53 | 1083 | 3 | 0.33 | 48 | 0.07 | 2 | 66 | 0.11 | 264 | 86 | |
| 42 | N | 60 | 0.2 | 1.77 | 23 | 869 | 0.5 | 7 | 3.67 | 0.3 | 54 | 19 | 107 | 40 | 4.67 | 0.78 | 12 | 17 | 1.27 | 847 | 5 | 0.11 | 22 | 0.05 | 2 | 97 | 0.19 | 160 | 67 | |
| 43 | O | 190 | 0.4 | 5.73 | 2 | 1266 | 0.4 | 7 | 1.89 | 0.6 | 43 | 11 | 18 | 78 | 3.54 | 2.44 | 13 | 22 | 0.79 | 627 | 1 | 0.16 | 7 | 0.08 | 4 | 44 | 0.10 | 119 | 65 | |
| 44 | P | 10 | 0.2 | 4.40 | 63 | 1407 | 1.7 | 10 | 6.02 | 0.2 | 70 | 24 | 67 | 47 | 4.68 | 1.76 | 13 | 11 | 2.37 | 1019 | 5 | 0.16 | 41 | 0.07 | 2 | 183 | 0.07 | 186 | 39 | |
| 45 | Q | 100 | 0.2 | 2.33 | 2 | 202 | 0.2 | 5 | 0.12 | 0.2 | 17 | 10 | 45 | 103 | 5.33 | 0.47 | 9 | 12 | 0.98 | 223 | 2 | 0.13 | 4 | 0.07 | 2 | 8 | 0.08 | 43 | 74 | |
| 46 | R | 5 | 0.2 | 4.59 | 5 | 88 | 0.2 | 11 | 2.55 | 0.2 | 48 | 27 | 109 | 64 | 6.14 | 0.15 | 13 | 15 | 2.29 | 1035 | 4 | 0.09 | 56 | 0.07 | 2 | 77 | 0.49 | 219 | 97 | |
| 47 | S | 5 | 0.2 | 3.50 | 10 | 395 | 0.2 | 5 | 1.45 | 0.2 | 41 | 17 | 51 | 75 | 6.20 | 0.50 | 12 | 15 | 1.66 | 722 | 5 | 0.09 | 11 | 0.08 | 2 | 68 | 0.57 | 179 | 95 | |
| 48 | T | 5 | 0.2 | 6.21 | 2 | 813 | 0.2 | 7 | 1.54 | 0.2 | 41 | 15 | 27 | 47 | 6.91 | 0.94 | 13 | 21 | 3.07 | 1286 | 4 | 0.08 | 12 | 0.09 | 2 | 52 | 0.57 | 201 | 118 | |
| 51 | U | 5 | 0.2 | 5.45 | 11 | 24 | 0.5 | 5 | 3.30 | 0.2 | 49 | 23 | 32 | 58 | 6.11 | 0.05 | 14 | 18 | 2.70 | 1387 | 2 | 0.07 | 22 | 0.09 | 2 | 95 | 0.41 | 159 | 109 | |
| 52 | V | 5 | 0.2 | 4.67 | 2 | 145 | 0.2 | 7 | 2.82 | 0.2 | 43 | 42 | 204 | 97 | 5.12 | 0.23 | 10 | 10 | 1.85 | 851 | 3 | 0.07 | 103 | 0.05 | 2 | 82 | 0.45 | 236 | 71 | |
| 53 | 376 - W | 5 | 0.2 | 4.73 | 2 | 884 | 0.3 | 8 | 4.15 | 0.2 | 55 | 22 | 25 | 86 | 5.35 | 1.77 | 14 | 18 | 1.86 | 1005 | 1 | 0.18 | 16 | 0.08 | 2 | 72 | 0.15 | 214 | 97 | |
| 54 | 377 - A | 40 | 0.2 | 2.46 | 45 | 1317 | 0.8 | 7 | 6.48 | 0.2 | 70 | 19 | 81 | 81 | 4.16 | 0.67 | 13 | 15 | 1.46 | 775 | 3 | 0.25 | 28 | 0.05 | 3 | 666 | 0.06 | 156 | 73 | |
| 55 | B | 30 | 0.2 | 3.67 | 7 | 168 | 0.2 | 9 | 2.36 | 0.7 | 53 | 13 | 34 | 91 | 4.82 | 0.29 | 13 | 11 | 1.27 | 636 | 8 | 0.11 | 11 | 0.08 | 3 | 135 | 0.42 | 173 | 157 | |
| 56 | C | 5 | 0.2 | 3.14 | 21 | 36 | 0.2 | 6 | 2.15 | 0.2 | 49 | 9 | 75 | 138 | 4.58 | 0.11 | 12 | 13 | 1.30 | 547 | 13 | 0.09 | 13 | 0.07 | 3 | 92 | 0.37 | 164 | 71 | |
| 57 | D | 5 | 0.2 | 5.31 | 4 | 41 | 0.2 | 11 | 3.53 | 0.6 | 55 | 13 | 36 | 82 | 5.03 | 0.11 | 14 | 15 | 1.59 | 847 | 8 | 0.10 | 9 | 0.07 | 7 | 111 | 0.49 | 190 | 93 | |
| 158 | E | 5 | 0.2 | 4.10 | 3 | 5 | 0.2 | 9 | 3.18 | 0.2 | 56 | 11 | 16 | 56 | 6.22 | 0.03 | 12 | 9 | 1.66 | 992 | 10 | 0.10 | 3 | 0.09 | 19 | 61 | 0.64 | 212 | 126 | |
| 159 | 377 - F | 5 | 0.2 | 4.22 | 2 | 78 | 0.2 | 12 | 2.17 | 0.3 | 44 | 17 | 24 | 57 | 5.89 | 0.20 | 13 | 15 | 2.00 | 897 | 4 | 0.09 | 7 | 0.08 | 2 | 86 | 0.35 | 130 | 152 | |

IB _____

PROJECT NO. 148

PROPERTY KLIYUL

N.T.S. 945/8E

ERT. NO. _____

GRID REFERENCE _____

KLIYUL-GRID Extn. East & West

DATE July, 1993

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | | CO-ORDINATES | | SAMPLER |
|----------|---|-----------------|-------|--------|----|-----|--------------|-------|---------|
| | | | | | As | +Au | | | |
| A | OT2-PY veining, sugary in chloritic And | Talus | | | | | 86-2000N | 6040E | Cray |
| B | Stockwork of Py in chloritic And host to A | " | | | | | " | " | Cray |
| C | Monzonite 10-15% S ²⁺ Py + Cp7, Mal | Flint | | | | | 2160N | 6200E | " |
| D | Coarse andesite flows w/ bleached 3-5% P. | Talus | | | | | 2950N | 6000E | Soh |
| E | chloritic andesite, mass 5% Py, goss in weathered grab | | | | | | 2900N | 5825E | Cray |
| F | Argite phytic. And w/ sil 3-4% Py grab | | | | | | 2850N | 5800E | Cray |
| G | Monzonite med gr, bleached gran. musc. chloritic | And sub outcrop | | | | | 2825N | 5800E | Cray |
| H | OT2-chl - Py veining w/ cpy impregnation 1-3% P7 | Py grab | | | | | 2415N | 5800E | Cray |
| I | Aphanitic Andesite, chl w/ epi in flow to Py | grab | | | | | 2200N | 5800E | Cray |
| J | And xl tuft chl 5% Py ± P ₆ 1-3% | grab | | | | | 5090E | 1850N | Cray |
| K | goss andesite silty, bleached + silf | grab | | | | | | | ? |
| L | Monzofelsic and/csd w/ streaks of Py to cpy qtz-carb sweets | Talus | | | | | 2200W | 1000N | DORT |
| M | Same as L w qtz-carb sweets/flooding of Py | grab | | | | | 2200W | 1120N | |
| N | qtz-carb Py veining in monzofelsic host | Talus | | | | | 2200W | 1100N | |
| O | And tuft? strongly altered oxidized R _x oxide Py | Talus | | | | | 2700W | 1060N | |
| P | Carbonated And diss Py to Nickel carb | grab | | | | | 2200W | 755N | |
| Q | goss, bleached And, later oxide Py to sil | grab | | | | | L-2200W | 1010N | |
| R | med gr argite - fl phytic and chl 5-7% Py | grab | | | | | L-1400E | 660S | DARB |
| S | ditto | grab | | | | | L-1400E | 700S | |
| T | ditto | grab | | | | | L-1400E | 675S | |
| U | Same as T - chloritic and, less sulphides | grab | | | | | L-1400E | 600S | |
| V | ditto | grab | | | | | L-1700E | 650S | |
| W | carbonated andesite, Py | Talus | | | | | 2200W | 1010N | DORT |

| T. | SAMPLE No. | As ppb | Ag ppm | Al % | Ar ppm | Ba ppm | Bc ppm | Bi ppm | Ca % | Cl ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | NG ppm | P % | Pb ppm | Sc ppm | Ti % | V ppm | Zn ppm | 0000-000 ppm | | | | | | |
|----|------------|-----------|-----------|---------|-----------|-----------|-----------|-----------|---------|-----------|-----------|-----------|-----------|-----------|---------|--------|-----------|-----------|---------|-----------|-----------|---------|-----------|--------|-----------|-----------|---------|----------|-----------|-----------------|--|--|--|--|--|--|
| 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 7 | 388 - A | 5 | 0.2 | 5.11 | 11 | 100 | 0.3 | 5 | 4.44 | 0.2 | 73 | 18 | 138 | 90 | 5.76 | 0.40 | 13 | 9 | 1.78 | 816 | 1 | 0.24 | 29 | 0.10 | 2 | 184 | 0.46 | 224 | 62 | | | | | | | |
| 8 | B | 5 | 0.4 | 4.35 | 5 | 369 | 0.3 | 5 | 3.30 | 0.4 | 73 | 16 | 22 | 9 | 4.53 | 0.59 | 16 | 12 | 1.44 | 673 | 1 | 0.10 | 12 | 0.12 | 3 | 349 | 0.32 | 155 | 33 | | | | | | | |
| 1 | C | 5 | 0.2 | 4.30 | 13 | 404 | 0.4 | 5 | 2.43 | 0.3 | 63 | 18 | 35 | 14 | 5.02 | 0.71 | 15 | 15 | 1.63 | 707 | 1 | 0.09 | 14 | 0.12 | 2 | 246 | 0.32 | 186 | 42 | | | | | | | |
| 2 | D | 5 | 0.2 | 5.12 | 6 | 297 | 0.3 | 5 | 4.20 | 0.2 | 66 | 11 | 22 | 156 | 4.97 | 0.75 | 11 | 11 | 1.63 | 583 | 1 | 0.13 | 15 | 0.10 | 2 | 227 | 0.42 | 240 | 33 | | | | | | | |
| 3 | 388 - E | 5 | 0.2 | 3.41 | 6 | 609 | 0.3 | 5 | 2.00 | 0.2 | 99 | 11 | 21 | 15 | 5.16 | 1.10 | 14 | 11 | 1.67 | 821 | 1 | 0.11 | 10 | 0.13 | 2 | 64 | 0.38 | 219 | 30 | | | | | | | |
| 4 | 387 - F | 5 | 0.2 | 5.13 | 16 | 223 | 0.3 | 5 | 4.98 | 0.2 | 75 | 25 | 24 | 83 | 7.15 | 0.46 | 12 | 8 | 2.32 | 1203 | 2 | 0.35 | 16 | 0.10 | 2 | 185 | 0.99 | 298 | 62 | | | | | | | |
| 5 | G | 5 | 0.2 | 5.35 | 7 | 677 | 0.3 | 5 | 4.32 | 0.3 | 72 | 21 | 26 | 84 | 5.62 | 0.35 | 12 | 11 | 2.31 | 820 | 1 | 0.23 | 24 | 0.11 | 2 | 193 | 0.51 | 243 | 51 | | | | | | | |
| 6 | 387 - H | 5 | 0.2 | 5.45 | 12 | 56 | 0.2 | 5 | 4.59 | 0.3 | 78 | 12 | 20 | 125 | 6.02 | 0.36 | 13 | 11 | 1.68 | 489 | 1 | 0.09 | 23 | 0.11 | 2 | 240 | 0.61 | 246 | 28 | | | | | | | |

| T.T. No. | SAMPLE No. | Au dob | Ag nom | Al % | As ppm | Ba ppm | Be ppm | Bi ppm | Ca % | Cl ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm | 3008-001 Pg. 8 of 8 |
|----------|------------|-----------|-----------|---------|-----------|-----------|-----------|-----------|---------|-----------|-----------|-----------|-----------|-----------|---------|--------|-----------|-----------|---------|-----------|-----------|---------|-----------|--------|-----------|-----------|---------|----------|-----------|------------------------|
| 193 | 726 - A rx | 30 | 0.2 | 4.70 | 2 | 271 | 0.2 | 5 | 3.06 | 0.8 | 46 | 33 | 40 | 226 | 9.05 | 0.63 | 13 | 12 | 1.66 | 1251 | 9 | 0.34 | 8 | 0.09 | 27 | 88 | 0.47 | 147 | 244 | |
| 194 | B | 5 | 0.2 | 3.19 | 4 | 39 | 0.2 | 5 | 2.64 | 0.7 | 48 | 25 | 46 | 40 | 7.56 | 0.15 | 14 | 11 | 2.56 | 793 | 3 | 0.22 | 31 | 0.09 | 32 | 89 | 0.32 | 211 | 287 | |
| 195 | C | 5 | 0.2 | 3.91 | 4 | 173 | 0.2 | 5 | 4.78 | 0.2 | 53 | 19 | 68 | 152 | 5.70 | 0.17 | 15 | 6 | 1.09 | 636 | 19 | 0.16 | 24 | 0.08 | 12 | 197 | 0.32 | 171 | 104 | |
| 196 | D | 90 | 0.4 | 7.62 | 2 | 16 | 0.4 | 5 | 8.30 | 0.2 | 54 | 72 | 34 | 181 | 9.20 | 0.06 | 12 | 13 | 1.57 | 819 | 177 | 0.16 | 46 | 0.07 | 20 | 503 | 0.28 | 425 | 74 | |
| 197 | E | 5 | 0.2 | 6.03 | 2 | 265 | 0.3 | 5 | 4.51 | 0.2 | 47 | 29 | 22 | 106 | 7.15 | 0.55 | 12 | 17 | 2.40 | 824 | 6 | 0.44 | 11 | 0.07 | 12 | 226 | 0.50 | 257 | 75 | |
| 198 | F | 20 | 0.2 | 3.80 | 5 | 30 | 0.3 | 5 | 4.72 | 0.2 | 50 | 7 | 33 | 72 | 5.91 | 0.11 | 14 | 7 | 1.16 | 789 | 19 | 0.17 | 8 | 0.08 | 14 | 241 | 0.32 | 284 | 72 | |
| 201 | G | 5 | 0.2 | 3.25 | 8 | 143 | 0.4 | 5 | 3.96 | 0.5 | 59 | 16 | 82 | 35 | 4.14 | 0.20 | 25 | 9 | 0.71 | 519 | 10 | 0.10 | 22 | 0.06 | 9 | 174 | 0.28 | 352 | 45 | |
| 202 | H | 5 | 0.2 | 4.50 | 4 | 206 | 0.2 | 5 | 3.95 | 0.2 | 43 | 17 | 30 | 38 | 6.45 | 0.50 | 11 | 11 | 1.90 | 785 | 2 | 0.16 | 12 | 0.07 | 11 | 183 | 0.28 | 165 | 79 | |
| 203 | I | 5 | 0.2 | 4.26 | 2 | 1148 | 0.2 | 5 | 0.49 | 0.2 | 25 | 11 | 30 | 167 | 8.96 | 1.60 | 10 | 12 | 1.90 | 1022 | 2 | 0.06 | 7 | 0.08 | 8 | 21 | 0.29 | 169 | 99 | |
| 204 | J | 5 | 0.2 | 4.78 | 2 | 17 | 0.6 | 5 | 6.43 | 0.2 | 54 | 15 | 49 | 60 | 4.69 | 0.05 | 13 | 8 | 0.79 | 749 | 4 | 0.09 | 19 | 0.06 | 9 | 220 | 0.25 | 155 | 48 | |
| 205 | K | 5 | 0.2 | 4.27 | 2 | 134 | 0.2 | 5 | 3.63 | 0.2 | 45 | 12 | 57 | 39 | 7.05 | 0.21 | 10 | 17 | 2.11 | 1109 | 5 | 0.40 | 12 | 0.06 | 7 | 76 | 0.47 | 230 | 80 | |
| 206 | L | 600 | 0.4 | 0.08 | 64 | 4 | 0.2 | 5 | 0.07 | 0.2 | 5 | 2 | 273 | 24 | 1.15 | 0.01 | 1 | 1 | 0.04 | 96 | 7 | 0.01 | 5 | 0.01 | 15 | 2 | 0.01 | 8 | 22 | |
| 207 | M | 30 | 0.2 | 4.20 | 7 | 56 | 0.2 | 5 | 1.39 | 0.2 | 33 | 19 | 65 | 213 | 12.64 | 0.10 | 9 | 16 | 1.73 | 1566 | 4 | 0.05 | 11 | 0.05 | 10 | 37 | 0.18 | 104 | 101 | |
| 208 | N | 160 | 0.4 | 0.24 | 23 | 8 | 0.2 | 5 | 0.08 | 0.2 | 9 | 63 | 212 | 80 | 13.24 | 0.04 | 4 | 1 | 0.12 | 133 | 6 | 0.01 | 17 | 0.02 | 10 | 1 | 0.02 | 32 | 24 | |
| 209 | O | 30 | 1.2 | 3.59 | 321 | 48 | 0.2 | 5 | 2.52 | 0.2 | 53 | 30 | 44 | 1147 | 6.00 | 0.24 | 14 | 8 | 1.36 | 588 | 4 | 0.09 | 8 | 0.08 | 4 | 80 | 0.25 | 133 | 57 | |
| 210 | P | 920 | 1.6 | 5.32 | 5 | 105 | 0.3 | 5 | 3.79 | 0.2 | 40 | 16 | 70 | 1315 | 8.41 | 0.23 | 9 | 12 | 2.13 | 1191 | 3 | 0.50 | 11 | 0.06 | 2 | 73 | 0.38 | 230 | 73 | |
| 211 | Q | 4000 | 14.0 | 5.78 | 31 | 63 | 0.4 | 5 | 4.93 | 1.4 | 52 | 175 | 88 | 15000 | 13.05 | 0.20 | 16 | 15 | 3.53 | 1330 | 7 | 0.27 | 54 | 0.07 | 11 | 60 | 0.30 | 205 | 168 | |
| 213 | R | 30 | 0.4 | 5.33 | 2 | 52 | 0.3 | 5 | 5.70 | 0.2 | 60 | 27 | 39 | 494 | 6.62 | 0.14 | 18 | 10 | 1.47 | 822 | 6 | 0.19 | 15 | 0.10 | 2 | 313 | 0.48 | 198 | 83 | |
| 214 | S | 140 | 0.2 | 6.41 | 229 | 25 | 0.3 | 5 | 6.65 | 0.2 | 56 | 31 | 33 | 416 | 10.65 | 0.08 | 13 | 10 | 1.47 | 718 | 19 | 0.14 | 14 | 0.08 | 4 | 371 | 0.32 | 258 | 55 | |
| 215 | T | 140 | 0.2 | 7.87 | 11 | 12 | 0.5 | 5 | 8.83 | 0.2 | 60 | 32 | 23 | 148 | 10.91 | 0.05 | 12 | 8 | 1.48 | 1546 | 2 | 0.09 | 29 | 0.10 | 5 | 758 | 0.26 | 225 | 89 | |
| 216 | U | 10 | 0.4 | 4.80 | 5 | 36 | 0.3 | 5 | 6.44 | 0.2 | 56 | 16 | 42 | 40 | 6.00 | 0.09 | 14 | 4 | 0.58 | 667 | 11 | 0.11 | 14 | 0.10 | 2 | 385 | 0.31 | 279 | 33 | |
| 217 | V | 20 | 0.2 | 2.85 | 4 | 41 | 0.2 | 5 | 2.49 | 0.3 | 42 | 54 | 94 | 230 | 9.34 | 0.14 | 11 | 9 | 1.85 | 760 | 8 | 0.23 | 23 | 0.06 | 5 | 85 | 0.22 | 163 | 51 | |
| 218 | 726 - W | 10 | 0.2 | 2.35 | 2 | 155 | 0.2 | 5 | 0.70 | 0.2 | 32 | 30 | 108 | 1031 | 7.73 | 0.36 | 12 | 10 | 1.09 | 392 | 7 | 0.09 | 4 | 0.05 | 2 | 75 | 0.14 | 45 | 30 | |
| 219 | 727 - A | 440 | 10.8 | 5.55 | 13 | 11 | 0.2 | 5 | 4.61 | 0.4 | 54 | 18 | 34 | 2462 | 8.46 | 0.07 | 15 | 10 | 2.11 | 1110 | 17 | 0.15 | 10 | 0.11 | 2 | 263 | 0.46 | 193 | 109 | |
| 220 | B | 10 | 0.2 | 2.90 | 6 | 19 | 0.2 | 5 | 2.75 | 0.2 | 40 | 13 | 64 | 108 | 5.39 | 0.08 | 7 | 4 | 1.46 | 897 | 20 | 0.21 | 12 | 0.04 | 2 | 86 | 0.40 | 168 | 56 | |
| 221 | C | 80 | 1.2 | 4.20 | 9 | 39 | 0.4 | 5 | 4.52 | 0.2 | 51 | 25 | 50 | 160 | 7.67 | 0.10 | 16 | 12 | 2.46 | 1144 | 6 | 0.29 | 18 | 0.07 | 4 | 149 | 0.44 | 196 | 70 | |
| 222 | D | 140 | 0.2 | 5.99 | 2 | 70 | 0.3 | 5 | 8.75 | 0.2 | 48 | 32 | 20 | 57 | 6.61 | 0.28 | 9 | 7 | 0.85 | 1022 | 6 | 0.07 | 7 | 0.06 | 2 | 338 | 0.36 | 274 | 33 | |
| 223 | E | 160 | 1.2 | 2.72 | 14 | 158 | 0.2 | 5 | 0.93 | 0.6 | 30 | 342 | 94 | 766 | 17.63 | 0.31 | 10 | 10 | 1.28 | 697 | 7 | 0.03 | 115 | 0.07 | 14 | 57 | 0.09 | 134 | 88 | |
| 225 | F | 20 | 0.2 | 5.43 | 2 | 37 | 0.3 | 5 | 5.24 | 0.2 | 51 | 10 | 38 | 192 | 7.04 | 0.12 | 13 | 8 | 1.37 | 960 | 3 | 0.12 | 14 | 0.09 | 2 | 273 | 0.31 | 209 | 59 | |
| 226 | G | 150 | 0.4 | 5.43 | 2 | 77 | 0.2 | 5 | 2.00 | 0.4 | 40 | 47 | 44 | 189 | 15.04 | 0.20 | 11 | 9 | 2.55 | 1498 | 4 | 0.16 | 12 | 0.07 | 7 | 96 | 0.34 | 129 | 94 | |
| 227 | 727 - H rx | 240 | 9.6 | 0.31 | 62 | 7 | 0.2 | 5 | 0.04 | 0.2 | 5 | 31 | 291 | 715 | 4.44 | 0.03 | 2 | 1 | 0.20 | 91 | 12 | 0.02 | 7 | 0.02 | 2 | 2 | 0.02 | 27 | 15 | |

| P.T. No. | SAMPLE No. | As | Ag | Al | Am | Ba | Be | Bi | Ca | Cl | Ce | Co | Cr | Cu | Fe | K | La | Li | Mg | Mn | Mo | Na | Ni | P | Pb | Sr | Tl | V | Zn | 3000-001 | |
|----------|------------|-----|-----|------|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|------|------|----|-----|------|------|-----|------|----|------|----|-----|------|-----|-----|----------|-----|
| | | ppb | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | ppm | % | ppm | % | ppm | ppm | % | ppm | ppm | ppm |
| 228 | 727 - J rx | 20 | 0.4 | 3.46 | 9 | 106 | 0.2 | 5 | 4.02 | 0.2 | 46 | 12 | 84 | 66 | 5.96 | 0.23 | 16 | 4 | 1.13 | 890 | 11 | 0.16 | 23 | 0.08 | 2 | 192 | 0.29 | 271 | 57 | | |
| 229 | J | 110 | 0.8 | 5.76 | 4 | 17 | 0.3 | 5 | 5.92 | 0.2 | 56 | 34 | 56 | 230 | 8.07 | 0.09 | 14 | 9 | 1.10 | 1109 | 6 | 0.14 | 7 | 0.09 | 2 | 263 | 0.35 | 209 | 51 | | |
| 230 | K | 20 | 0.2 | 2.12 | 2 | 123 | 0.2 | 5 | 0.89 | 0.2 | 26 | 8 | 114 | 94 | 4.16 | 0.29 | 7 | 7 | 0.71 | 302 | 80 | 0.13 | 4 | 0.05 | 2 | 91 | 0.18 | 44 | 22 | | |
| 231 | L | 10 | 0.2 | 5.51 | 9 | 80 | 0.4 | 5 | 2.71 | 0.7 | 49 | 24 | 31 | 203 | 6.90 | 0.42 | 15 | 25 | 2.27 | 766 | 22 | 0.16 | 12 | 0.06 | 4 | 163 | 0.22 | 128 | 50 | | |
| 232 | M | 20 | 0.2 | 2.16 | 6 | 442 | 0.2 | 5 | 1.83 | 0.5 | 42 | 11 | 34 | 74 | 5.58 | 0.62 | 12 | 10 | 1.69 | 732 | 3 | 0.23 | 9 | 0.07 | 5 | 47 | 0.36 | 207 | 65 | | |
| 233 | N | 20 | 0.4 | 3.38 | 7 | 237 | 0.2 | 5 | 4.16 | 0.2 | 57 | 15 | 71 | 106 | 5.21 | 0.33 | 17 | 6 | 0.85 | 668 | 13 | 0.13 | 23 | 0.11 | 7 | 286 | 0.34 | 451 | 49 | | |
| 234 | O | 10 | 0.2 | 1.62 | 5 | 15 | 0.2 | 5 | 2.00 | 0.2 | 51 | 9 | 60 | 44 | 5.97 | 0.07 | 17 | 5 | 1.12 | 925 | 8 | 0.24 | 16 | 0.10 | 6 | 84 | 0.44 | 254 | 58 | | |
| 235 | P | 5 | 0.2 | 4.57 | 2 | 95 | 0.3 | 5 | 2.69 | 0.2 | 50 | 15 | 50 | 37 | 5.57 | 0.42 | 13 | 11 | 1.44 | 822 | 3 | 0.25 | 9 | 0.09 | 3 | 116 | 0.29 | 122 | 40 | | |
| 236 | Q | 5 | 0.4 | 3.31 | 2 | 225 | 0.2 | 5 | 1.02 | 0.2 | 39 | 11 | 95 | 29 | 5.72 | 0.71 | 10 | 9 | 1.07 | 547 | 18 | 0.20 | 8 | 0.08 | 2 | 49 | 0.11 | 59 | 24 | | |
| 237 | R | 20 | 0.2 | 4.07 | 3 | 54 | 0.2 | 5 | 3.59 | 0.2 | 49 | 13 | 38 | 175 | 7.16 | 0.17 | 12 | 10 | 2.02 | 1142 | 17 | 0.32 | 9 | 0.10 | 2 | 79 | 0.55 | 185 | 68 | | |
| 238 | T | 10 | 0.2 | 3.60 | 18 | 135 | 0.2 | 5 | 3.52 | 0.3 | 51 | 28 | 43 | 157 | 8.89 | 0.36 | 14 | 13 | 2.59 | 1201 | 2 | 0.29 | 30 | 0.08 | 8 | 44 | 0.43 | 170 | 98 | | |
| 239 | U | 220 | 0.8 | 4.87 | 6 | 20 | 0.3 | 5 | 6.14 | 0.2 | 56 | 21 | 37 | 214 | 7.66 | 0.10 | 11 | 7 | 1.60 | 1107 | 2 | 0.18 | 18 | 0.14 | 2 | 189 | 0.45 | 185 | 50 | | |
| 240 | V | 70 | 1.2 | 5.51 | 24 | 10 | 0.3 | 5 | 6.01 | 0.2 | 56 | 30 | 59 | 139 | 7.80 | 0.04 | 12 | 7 | 0.87 | 792 | 3 | 0.05 | 18 | 0.06 | 3 | 362 | 0.17 | 151 | 50 | | |
| 241 | 727 - W | 40 | 0.4 | 2.27 | 67 | 14 | 0.3 | 5 | 1.04 | 0.4 | 36 | 47 | 64 | 85 | 8.83 | 0.02 | 13 | 12 | 1.76 | 683 | 12 | 0.10 | 14 | 0.05 | 8 | 48 | 0.38 | 103 | 66 | | |
| 242 | 728 - A | 10 | 0.2 | 2.82 | 5 | 75 | 0.2 | 5 | 2.40 | 0.2 | 47 | 17 | 49 | 134 | 5.64 | 0.17 | 13 | 13 | 1.74 | 847 | 3 | 0.20 | 13 | 0.07 | 2 | 137 | 0.36 | 213 | 68 | | |
| 243 | B | 5 | 0.2 | 2.92 | 2 | 284 | 0.2 | 5 | 0.31 | 0.2 | 22 | 6 | 76 | 16 | 5.25 | 0.72 | 9 | 7 | 1.02 | 574 | 35 | 0.08 | 4 | 0.05 | 2 | 32 | 0.06 | 42 | 25 | | |
| 244 | C | 5 | 0.4 | 4.95 | 3 | 950 | 0.2 | 5 | 1.90 | 0.2 | 40 | 16 | 26 | 81 | 6.06 | 1.13 | 9 | 24 | 1.28 | 721 | 2 | 0.13 | 6 | 0.06 | 2 | 110 | 0.54 | 202 | 50 | | |
| 245 | D | 5 | 1.2 | 2.76 | 9 | 300 | 0.2 | 5 | 3.20 | 0.3 | 52 | 21 | 53 | 212 | 5.94 | 0.67 | 15 | 30 | 2.25 | 904 | 1 | 0.10 | 23 | 0.07 | 5 | 67 | 0.32 | 283 | 75 | | |
| 246 | E | 5 | 0.2 | 6.22 | 2 | 411 | 0.2 | 5 | 0.51 | 0.2 | 26 | 3 | 61 | 24 | 5.95 | 1.31 | 10 | 24 | 4.58 | 476 | 1 | 0.06 | 6 | 0.08 | 2 | 83 | 0.57 | 180 | 58 | | |
| 247 | 728 - F rx | 5 | 0.2 | 6.21 | 2 | 93 | 0.5 | 5 | 9.99 | 0.2 | 59 | 14 | 33 | 22 | 4.94 | 0.15 | 12 | 10 | 1.20 | 1181 | 2 | 0.03 | 10 | 0.11 | 2 | 456 | 0.43 | 110 | 65 | | |

NORANDA EXPLORATION COMPANY, LIMITED

0726

White - Office
Yellow - Field

LAB NOREX

PROJECT NO. _____ PROPERTY KLIYUL (DARB LAKE)

N.T.S. 94D/9

CERT. NO. _____

GRID REFERENCE DARB LK GRID

DATE JULY 19/95

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | | CO-ORDINATES | | SAMPLE |
|----------|---|-------|-------|--------|--|--|--------------|--------|--------|
| | | | | | | | | | |
| A | Mass varicose feld. porphy And-7 Dior 3-5% py. | o/c | | | | | 8800E | 13100N | TW |
| B | Fgm And + chl-qtz-carb veins in clear 5-10% py | o/c | | | | | 8800E | 12900N | TW |
| C | heavy pyritic hfs lufs + calc-sil alt + mag veins | o/c | | | | | 8870E | 12675N | TW |
| D | Pyrite rich (10-15%) - feld porph And. | Float | | | | | 8750E | 12500N | TW |
| E | calc-sil hfs to shaly skinned and 5-10% py, po | o/c | | | | | 8810E | 12200N | TW |
| F | F.G. green (arg/mst) Tr-1% Py | o/c | | | | | 9000E | 13100N | RGW |
| G | " " " " (talus) | Float | | | | | 9000E | 12925N | RGW |
| H | HORNIFIED Volc. breccia to fg. ANDs 1-2% Py | o/c | | | | | 8975E | 12590N | RGW |
| I | calc-silicate alt. (skinned) arg/mst Tr-1% Py | o/c | | | | | 8970E | 12590N | RGW |
| J | " " " " " " " " | o/c | | | | | 9025E | 12575N | RGW |
| K | Intense gabbro with 1% Py on fractures | Float | | | | | 9010E | 11235N | RGW |
| L | Qtz vein ~ 1.5m thick, slightly rusty | o/c | | | | | 8775E | 10990N | RGW |
| M | Fg. gabbro 1% py. | Float | | | | | 8800E | 11520N | RGW |
| N | Diorite skinned zone 1.5m wide with 5cm py band | Float | | | | | 8775E | 11765N | RGW |
| O | Diorite skinned 1x2m pod. minor malachite py | o/c | | | | | 8775E | 11775N | RGW |
| P | Dior - Qtz-py stock veined 5-10% py + MAG. | o/c | | | | | 8545E | 13190N | TW |
| Q | Dior 6-10cm Qtz-chl-py-py-bor-mag vein | o/c | | | | | 8535E | 13195N | TW |
| R | Sulph rich bi-st calc-sil hfs, 10-15% py, po | Float | | | | | 8390E | 13650N | TW |
| S | pyritic calc-sil hfs? argillite ± px skinned py, po | o/c | | | | | 8360E | 13760N | TW |
| T | ditto | o/c | | | | | 8350E | 14210N | TW |
| U | ditto 10-15% py, po | o/c! | | | | | 8860E | 14600N | TW |
| V | chl-epid-qtz retrograde vein 15-20% py, po | Float | | | | | 8500E | 14380N | TW |
| W | ditto + px skinned | | | | | | 8530E | 14300N | TW |

NORANDA EXPLORATION COMPANY, LIMITED

0727

White - Office

Yellow - Field

LAB _____

PROJECT NO. _____ PROPERTY Kiyul (DARB LAKE)

N.T.S. 94D/9

CERT. NO. _____

GRID REFERENCE DARB LK GRID

DATE JULY 19

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | | CO-ORDINATES | | |
|----------|---|-------|-------|--------|--|--------|--------------|----|--|
| | | | | | | | | | |
| A | Mixed sheared calc-sil hls argl + Dms 5-10% py, po | o/c | | | | 89390E | 12355N | 7 | |
| B | Rusty calc-sil hls - shnd argl + feld pyph dyke | o/c | | | | 8910E | 12830N | 7 | |
| C | Endoskeletal feld. porph dyke 10-15% py | float | | | | 8900E | 12590N | 7E | |
| D | calc-sil hls - px shnd luvng argl 5-10% py | o/c | | | | 8920E | 12440N | 7E | |
| E | hls argl + qtz-chl-py-po - may shsk vns | o/c | | | | 8950E | 12270N | 7E | |
| F | green pl calc-sil to px shnd + qtz-csb - Mal, cap, iron | o/c | | | | 8920E | 12140N | 7E | |
| G | Shsk of qtz - mag - py vns in feld porph And. | o/c | | | | 8700E | 11150N | 7E | |
| H | pyhic mm-crystal qtz green argl 5-10% py | float | | | | 8400E | 10450N | 7E | |
| I | hls pyhic argillite, dms in vns | o/c | | | | 8900E | 13485N | 7E | |
| J | Diorite / Gabbro 1% Py minor qty - cont magnetite | FLINT | | | | 8575E | 13820N | RG | |
| K | Fig Diorite / Gabbro qty + 1% Py | FLINT | | | | 8610E | 14215N | | |
| L | Diorite, coarse grained 1% Py, Pb | FLINT | | | | 8590E | 14290N | | |
| M | Homophred fg. arg. minor Py | o/c | | | | 8590E | 14470N | " | |
| N | | o/c | | | | 8620E | 14440N | " | |
| O | Homophred sediment with Py, Pb + minor qty | o/c | | | | 8520E | 14220N | " | |
| P | | o/c | | | | 8530E | 14190N | " | |
| Q | Diorite with qtz + magnetite, Tel-ben alt. | o/c | | | | 8510E | 13990N | " | |
| R | Dior - qtz-epid-chl-py shsk vns 5-10% py | o/c | | | | 8800E | 13650N | TW | |
| S | ~ ~ ~ ~ ~ | | | | | | | | |
| T | Shnd Dior → And + hls scs, shsk qtz py vns | o/c | | | | 8750E | 13270N | TW | |
| U | Dior - mod py-chl-qtz vns | o/c | | | | 8925E | 13775N | TW | |
| V | deto vns in shnd Dior | o/c | | | | 8950E | 13820N | TW | |
| W | Qtz-py vns in calc-sil → px shnd scs | o/c | | | | 8940E | 13900N | TW | |

AB _____

PROJECT NO. _____ PROPERTY KLIUYL (DARR LAKE)

N.T.S. 940/A

CERT. NO. _____

GRID REFERENCE DARR LK GRID AREA B; MAIN GRID E →

DATE 20/11/93

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | CO-ORDINATES | | SAMPLER |
|----------|---|-------|-------|--------|--|--------------|-------|---------|
| | | | | | | | | |
| A | Mass py-76 m or less. Dike dyke | 0/c | | | | 9000E | 1400N | TW |
| B | py. calc. into calc. dike | float | | | | 8875E | 1400N | TW |
| C | py. calc. (shaly) with calc. in volcaniclastic sed. | 0/c | | | | 1000W | 1360N | TW |
| D | qtz-feld. to md. calc. with calc. to py | 0/c | | | | 2100W | 1450N | TW |
| E | Fs porphyry underlain, rusty py zone | 0/c | | | | 3000E | 1175N | R6W |
| F | Sandy lat., banded dk brn + red, much py | 0/c | | | | 3000E | 200N | R6W |
| G | | | | | | | | |
| H | | | | | | | | |
| I | | | | | | | | |
| J | | | | | | | | |
| K | | | | | | | | |
| L | | | | | | | | |
| M | | | | | | | | |
| N | | | | | | | | |
| O | | | | | | | | |
| P | | | | | | | | |
| Q | | | | | | | | |
| R | | | | | | | | |
| S | | | | | | | | |
| T | | | | | | | | |
| U | | | | | | | | |
| V | | | | | | | | |
| W | | | | | | | | |

MAIN GRID

NORANDA DELTA LABORATORY

Geochemical Analysis

K11

Project Name & No.: KLIYUL - 148

Geol.: C.S.

Date received: NOV. 01

LAB CODE: 9311-010

Material: 11 Rx

Sheet: 1 of 1

Date completed: NOV. 10

Remarks: * Sample screened @ -35 MESH (0.5 mm)

** Organic, & Humus, S Sulfide

As - 10.0 g sample digested with aqua-regia and determined by A.A. (D.L. 5 PPB)

ICP - 0.2 g sample digested with 3 ml HClO₄/HNO₃ (4:1) at 203 °C for 4 hours diluted to 10 ml with water. Lasmann PS3000 ICP determined elemental contents.

N.B. The major oxide elements and Ba, Be, Ce, La, Li, Ga are rarely dissolved completely from geological materials with this acid dissolution method.

| Sl. No. | SAMPLE No. | As | Ag | Al | Ar | Ba | Be | Bi | Ca | Cd | Ce | Co | Cr | Cu | Fe | K | La | Li | Mg | Mn | Mo | Na | Ni | P | Pb | Sr | Ti | V | Zn |
|---------|------------|------|-----|------|-----|------|-----|-----|------|-----|-----|-----|-----|-------|-------|------|-----|------|------|------|------|------|------|------|-----|------|------|-----|-----|
| | | ppb | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | ppm | % | ppm | % | ppm | ppm | % | ppm | ppm |
| 3 | 1678 - A | 10 | 0.2 | 3.91 | 5 | 260 | 0.2 | 5 | 1.55 | 0.2 | 54 | 9 | 28 | 86 | 3.25 | 0.69 | 13 | 8 | 1.79 | 560 | 1 | 0.15 | 6 | 0.06 | 2 | 86 | 0.25 | 147 | 91 |
| 4 | B | 5 | 0.2 | 3.70 | 2 | 376 | 0.4 | 5 | 2.25 | 0.2 | 76 | 10 | 23 | 4.42 | 0.48 | 19 | 9 | 0.99 | 787 | 1 | 0.10 | 6 | 0.15 | 2 | 399 | 0.26 | 107 | 93 | |
| 5 | C | 20 | 0.2 | 3.76 | 8 | 18 | 0.5 | 20 | 5.60 | 1.3 | 64 | 34 | 36 | 19.99 | 0.04 | 16 | 14 | 1.03 | 4006 | 1 | 0.03 | 24 | 0.10 | 2 | 91 | 0.10 | 89 | 179 | |
| 7 | D | 40 | 0.2 | 3.53 | 14 | 18 | 0.4 | 14 | 8.96 | 2.8 | 59 | 7 | 24 | 716 | 13.68 | 0.03 | 9 | 6 | 0.59 | 2475 | 2 | 0.03 | 22 | 0.10 | 2 | 147 | 0.15 | 96 | 423 |
| 3 | E | 80 | 1.2 | 2.50 | 19 | 11 | 0.4 | 5 | 8.88 | 0.2 | 56 | 15 | 31 | 1573 | 15.51 | 0.04 | 8 | 7 | 0.57 | 3477 | 2 | 0.03 | 12 | 0.08 | 2 | 56 | 0.07 | 61 | 108 |
| 1 | F | 5 | 0.2 | 5.97 | 2 | 247 | 0.6 | 5 | 1.94 | 0.5 | 63 | 18 | 29 | 996 | 2.92 | 0.65 | 16 | 22 | 1.29 | 1049 | 1 | 0.42 | 11 | 0.09 | 2 | 200 | 0.03 | 113 | 55 |
| 2 | G | 5 | 0.2 | 5.11 | 2 | 230 | 0.2 | 5 | 4.07 | 0.2 | 71 | 8 | 40 | 41 | 3.26 | 0.49 | 10 | 6 | 0.29 | 324 | 1 | 0.10 | 6 | 0.08 | 2 | 643 | 0.22 | 92 | 37 |
| 3 | H | 5 | 0.2 | 5.97 | 2 | 47 | 0.3 | 5 | 5.71 | 0.2 | 84 | 10 | 20 | 28 | 4.84 | 0.13 | 12 | 10 | 1.13 | 999 | 1 | 0.08 | 5 | 0.14 | 2 | 190 | 0.38 | 136 | 69 |
| 1 | 1678 - I | 5 | 0.2 | 0.62 | 4 | 1003 | 0.3 | 7 | 2.31 | 0.2 | 54 | 11 | 41 | 132 | 2.93 | 0.26 | 10 | 5 | 0.98 | 478 | 2 | 0.14 | 28 | 0.13 | 2 | 115 | 0.03 | 81 | 27 |
| 5 | 1679 - A | 1740 | 5.6 | 0.49 | 2 | 90 | 0.2 | 5 | 0.11 | 0.2 | 11 | 2 | 196 | 299 | 2.53 | 0.19 | 3 | 2 | 0.07 | 59 | 354 | 0.06 | 3 | 0.03 | 2 | 15 | 0.04 | 15 | 11 |
| 6 | 1679 - B | 30 | 0.2 | 7.99 | 2 | 950 | 0.4 | 5 | 0.10 | 0.2 | 20 | 1 | 8 | 29 | 2.64 | 2.05 | 5 | 12 | 0.27 | 98 | 5 | 0.73 | 3 | 0.05 | 10 | 110 | 0.06 | 119 | 46 |

15/10 VINC fl

NORANDA DELTA LABORATORY

Geochemical Analysis

Project Name & No.: KLJYUL - 148
 Material: 22 Rx
 Remarks: * Sample screened @ -35 MBSH (0.5 mm)
 † Organic, ‡ Humus, § SuWids

Geol.: C.S.
 Sheet: 1 of 1

Date received: NOV. 08
 Date completed: NOV. 16

LAB CODE: 9311-019

Au - 10.0 g sample digested with aqua-regia and determined by A.A. (D.L. 5 PPB)
 ICP - 0.2 g sample digested with 3 ml HClO₄/HNO₃ (4:1) at 203 °C for 4 hours diluted to 10 ml with water. Leeman PS3000 ICP determined elemental contents.
 N.B. The major oxide elements and Ba, Be, Ce, La, Li, Ga are rarely dissolved completely from geological materials with this acid dissolution method.

| T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Be ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm |
|--------|------------|--------|--------|------|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------|-------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|
| | 1679 - C | 450 | 13.2 | 2.63 | 27 | 115 | 0.3 | 5 | 0.29 | 1.0 | 19 | 32 | 136 | 5572 | 4.65 | 1.02 | 4 | 8 | 0.35 | 272 | 9 | 0.09 | 13 | 0.05 | 2 | 5 | 0.02 | 61 | 68 |
| | D | 40 | 2.4 | 0.35 | 47 | 16 | 0.2 | 5 | 0.49 | 0.2 | 23 | 4 | 476 | 964 | 1.01 | 0.18 | 3 | 2 | 0.06 | 139 | 4 | 0.01 | 8 | 0.01 | 10 | 6 | 0.01 | 18 | 10 |
| | E | 20 | 2.8 | 4.57 | 4 | 23 | 0.4 | 5 | 6.93 | 0.2 | 93 | 13 | 43 | 5102 | 4.99 | 0.09 | 9 | 11 | 0.97 | 922 | 11 | 0.17 | 16 | 0.08 | 2 | 510 | 0.34 | 189 | 50 |
| | F | 100 | 2.8 | 5.56 | 10 | 287 | 0.6 | 5 | 8.50 | 0.5 | 95 | 27 | 26 | 4895 | 6.66 | 0.72 | 10 | 30 | 1.94 | 1300 | 4 | 0.06 | 25 | 0.08 | 4 | 377 | 0.33 | 247 | 98 |
| | G | 150 | 8.4 | 3.11 | 11 | 14 | 0.7 | 5 | 7.41 | 0.2 | 93 | 14 | 43 | 14000 | 6.83 | 0.06 | 10 | 10 | 0.47 | 1997 | 18 | 0.09 | 15 | 0.10 | 2 | 227 | 0.22 | 251 | 62 |
| 0 | H | 450 | 2.8 | 2.03 | 14 | 7 | 0.6 | 5 | 2.62 | 0.5 | 64 | 204 | 40 | 3241 | 27.74 | 0.05 | 16 | 4 | 0.22 | 695 | 5 | 0.03 | 34 | 0.10 | 8 | 76 | 0.04 | 135 | 67 |
| 1 | I s | 280 | 2.8 | 3.29 | 11 | 14 | 0.5 | 5 | 5.00 | 0.2 | 71 | 121 | 52 | 2961 | 14.93 | 0.07 | 16 | 7 | 0.35 | 1228 | 1 | 0.05 | 21 | 0.06 | 2 | 136 | 0.02 | 83 | 51 |
| 3 | J s | 510 | 0.4 | 0.62 | 19 | 70 | 0.7 | 5 | 0.46 | 0.2 | 21 | 463 | 51 | 1178 | 33.45 | 0.12 | 12 | 2 | 0.33 | 370 | 17 | 0.03 | 185 | 0.08 | 9 | 9 | 0.02 | 120 | 56 |
| 5 | K | 5 | 0.2 | 0.19 | 24 | 15 | 0.6 | 5 | 1.19 | 0.4 | 40 | 16 | 33 | 52 | 36.88 | 0.07 | 14 | 3 | 0.07 | 508 | 7 | 0.02 | 52 | 0.11 | 20 | 5 | 0.01 | 201 | 59 |
| 7 | L | 680 | 3.2 | 7.19 | 3 | 14 | 0.4 | 5 | 11.51 | 0.2 | 88 | 17 | 6 | 4534 | 7.52 | 0.05 | 9 | 6 | 0.18 | 1465 | 35 | 0.04 | 11 | 0.14 | 2 | 345 | 0.27 | 144 | 48 |
| 8 | M s | 10600 | 8.8 | 1.68 | 54 | 4 | 0.4 | 5 | 15.27 | 0.2 | 68 | 149 | 56 | 8064 | 15.20 | 0.04 | 4 | 6 | 0.09 | 3693 | 77 | 0.04 | 33 | 0.14 | 2 | 62 | 0.02 | 74 | 72 |
| 0 | N | 1300 | 4.0 | 7.40 | 2 | 9 | 0.3 | 5 | 9.47 | 0.2 | 94 | 145 | 27 | 3542 | 8.10 | 0.05 | 16 | 7 | 0.81 | 1178 | 5 | 0.04 | 23 | 0.09 | 2 | 273 | 0.04 | 105 | 34 |
| 1 | O | 130 | 0.8 | 3.32 | 5 | 20 | 0.6 | 5 | 4.74 | 0.2 | 74 | 116 | 52 | 1625 | 26.28 | 0.08 | 19 | 7 | 0.22 | 929 | 24 | 0.04 | 33 | 0.11 | 2 | 134 | 0.09 | 157 | 57 |
| 3 | P | 1200 | 4.0 | 2.09 | 9 | 9 | 0.8 | 5 | 3.32 | 0.3 | 63 | 38 | 60 | 4609 | 31.77 | 0.05 | 16 | 3 | 0.18 | 899 | 44 | 0.04 | 30 | 0.12 | 11 | 113 | 0.10 | 174 | 100 |
| 5 | Q | 1730 | 6.4 | 0.20 | 22 | 11 | 0.9 | 5 | 6.58 | 0.2 | 74 | 21 | 45 | 13000 | 30.07 | 0.04 | 12 | 4 | 0.15 | 894 | 9 | 0.03 | 47 | 0.09 | 3 | 23 | 0.01 | 177 | 78 |
| 7 | R | 170 | 1.2 | 3.31 | 11 | 2672 | 0.5 | 5 | 8.99 | 0.2 | 89 | 22 | 115 | 742 | 5.00 | 1.66 | 9 | 8 | 1.85 | 2040 | 4 | 0.05 | 31 | 0.08 | 2 | 208 | 0.05 | 137 | 93 |
| 8 | S | 850 | 1.2 | 1.21 | 23 | 41 | 0.7 | 5 | 1.59 | 0.3 | 167 | 424 | 55 | 1397 | 34.33 | 0.08 | 108 | 3 | 0.16 | 469 | 15 | 0.03 | 45 | 0.10 | 22 | 50 | 0.04 | 130 | 56 |
| 0 | T s | 570 | 5.2 | 1.31 | 9 | 4 | 0.7 | 5 | 3.05 | 0.2 | 57 | 1093 | 61 | 7104 | 17.29 | 0.04 | 10 | 4 | 0.21 | 678 | 171 | 0.03 | 36 | 0.06 | 2 | 51 | 0.01 | 85 | 84 |
| 1 | U | 4100 | 8.0 | 1.95 | 17 | 19 | 1.1 | 5 | 3.09 | 0.2 | 74 | 60 | 36 | 8304 | 30.66 | 0.05 | 29 | 5 | 0.15 | 708 | 36 | 0.03 | 43 | 0.13 | 10 | 89 | 0.13 | 211 | 86 |
| 3 | V | 870 | 9.2 | 4.34 | 6 | 22 | 0.4 | 5 | 12.34 | 0.2 | 67 | 61 | 29 | 8216 | 12.51 | 0.04 | 7 | 5 | 0.18 | 1834 | 38 | 0.04 | 11 | 0.11 | 2 | 181 | 0.18 | 172 | 73 |
| 5 | 1679 - W | 880 | 1.2 | 0.29 | 26 | 20 | 0.6 | 5 | 0.85 | 1.9 | 34 | 29 | 33 | 13000 | 35.55 | 0.04 | 16 | 2 | 0.14 | 1052 | 33 | 0.02 | 58 | 0.11 | 25 | 7 | 0.01 | 181 | 78 |
| 7 | 1680 - A | 20 | 0.8 | 1.05 | 17 | 21 | 0.5 | 5 | 4.44 | 0.2 | 59 | 24 | 60 | 1646 | 28.02 | 0.09 | 13 | 4 | 0.16 | 765 | 4 | 0.03 | 30 | 0.10 | 5 | 51 | 0.05 | 94 | 52 |

17/11 done off

IB NORX

PROJECT NO. 148 PROPERTY Sligul

N.T.S. _____

ERT. NO. _____

GRID REFERENCE W. Grid Extension

DATE Oct 24/93

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | CO-ORDINATES | | SAMPLER |
|----------|---|-----------|----------|------------|------------|--------------|--------|------------|
| | | | | 30 element | 10 Fe + Au | | | |
| A | Sil. maf volcanic, 2-3 ³ Pg, weak sugary texture | Composite | grabs | | | 8+40E | 24+00N | C. Scholte |
| B | porphyritic maf. flow, wk sheared, mod azurite | | | | | 8+40E | 24+50N | ✓ |
| C | (Magnetite-bearing skarn, wk sil, tr Cpy. | | | | | 8+60E | 25+60N | ✓ |
| D | mod. mal, wk azurite, up to 10% mag; +2-3 ³ | | | | | " | " | ✓ |
| E | Qz stringers forming mod. stockwork | | | | | " | " | ✓ |
| F | (talus) weak sil. por. flow; wk arg alt local (skarn?) | | | | | 8+40E | 25+50N | ✓/✓ |
| G | Sil. volc (basalt?) - pass skarn, 2-3 ³ Pg + Po | Grab | | | | 37+0E | 9+45N | ✓/✓ |
| H | Sil. volc, local skarn, mod. dev Qz stnork, 2-3 ³ Pg | | | | | 348SE | 5+72N | ✓/✓ |
| I | Sil. weak exoskarn in lap. tuff. 5 ³ Qz-km stnork | | carb alt | | | 3200E | 12+25N | ✓/✓ |
| J | / | | | | | | | |
| K | | | | | | | | |
| L | | | | | | | | |
| M | | | | | | | | |
| N | | | | | | | | |
| O | | | | | | | | |
| P | | | | | | | | |
| Q | | | | | | | | |
| R | | | | | | | | |
| S | | | | | | | | |
| T | | | | | | | | |
| U | | | | | | | | |
| V | | | | | | | | |
| W | | | | | | | | |

AB ADOREX

PROJECT NO. 148

PROPERTY KSIIYUL

N.T.S.

ERT. NO. _____

GRID REFERENCE

MAIN GRID / Moraine Grid

DATE Oct 29/93

SAMPLE REPORT

| SAMPLE # | DESCRIPTION | TYPE | WIDTH | ASSAYS | | | CO-ORDINATES | | SAMPLER | |
|----------|---|-----------|---------------|----------|--------|-----|--------------|---------|--------------|-----|
| | | | | 30 elem. | I.C.P. | +Au | | | | |
| A | Prox. float: Q. Vein + sil. volc - grey-white, 5% B, tr Cpy, mal | Grab | - | | | | L 21+00E | 23+00 N | C.S. Schuler | |
| B | sil. volc (+ sil?) - strong sil; strong lim, mod ser. | " | - | | | | L 21+00E | 24+35 N | ↓ ✓ | |
| C | Talus: Q.V., fract, 1-2% Cpy, tr P ₂ , mod. malachite | " | | | | | L 35+00E | 14+88 N | ↓ ✓ | |
| D | Prox talus: Q.V., weak foliated, Cpy, tr P ₂ , al. foliation | " | | | | | L 34+50E | 15+20 N | ↓ ✓ | |
| E | Sil. lapilli tuff, Qz stringers, 1-2% Cpy, mod mal. | " | | | | | L 34+00E | 15+40 N | ↓ ✓ | |
| F | Weak skarn dev. in mat. volc: Q. stringers, tr Cpy | " | | | | | L 34+10E | 15+35 N | ↓ ✓ | |
| G | Mafic. Jolehnic skarn, some epid, qtz, dev. tr Cpy | Grab | | | | | L 34+00E | 15+40 N | ↓ ✓ | |
| H | Mag bearing skarn: 50% Mag, 10-15% P ₂ , tr 2% Cpy, mal. | Grab | PACIFIC SKARN | | | | MORaine | E 4935E | 10000 N | ↓ ✓ |
| I | Mag bearing skarn: 20% P ₂ , tr 2% Cpy, mal. | Grab | | GRID | | | | 10000 E | 98735 N | ↓ ✓ |
| J | Magnetite skarn (50% mag), tr Cpy, 7-8% mag | Grab | | | | | | 10000 E | 10100 N | ↓ ✓ |
| K | Almost pure magnetite, tr P ₂ , Cpy | Grab | | | | | | 10000 E | 10021 N | ↓ ✓ |
| L | Mag bearing skarn: 30% disc, + free rel Cpy, 5% mag | " | | | | | | 10000 E | 10060 N | ↓ ✓ |
| M | Similar to L (diff. boulder), 4-5% mag, 3% Cpy | " | | | | | | " | " | ↓ ✓ |
| N | Skarn, 1-2% Magnetite, 1-2% Cpy, 7-8% P ₂ | Comp Grab | | | | | | 10008 E | 10075 N | ↓ ✓ |
| O | Skarn, 10-15% Mag, al. fract + interstitial, 2% Cpy | Comp Grab | | | | | | 10012 E | 10100 N | ↓ ✓ |
| P | Magnetite bear. skarn (20% Mag) 4% Cpy, al. sil. | Grab | | | | | | 9830E | 9860N | ↓ ✓ |
| Q | Skarn, 25% Mag, 5% Cpy, al. silica stringers | " | | | | | | 9870E | 9925 N | ↓ ✓ |
| R | Skarn - carbonate + Qz str comprise 30% = 1% Cpy, P ₂ | " | | | | | 10095E | 10200 N | ↓ ✓ | |
| S | Skarn, 85% Mag; 7-8% P ₂ , locally 2% Cpy | Comp Grab | | | | | 10048E | 10200 N | ↓ ✓ | |
| T | Skarn, 60% Mag, 15% P ₂ , 5% Cpy, al. Qz | Grab | | | | | 9820E | 9800N | ↓ ✓ | |
| U | Skarn, 50-60% Mag, 1-2% Cpy, strong Az + Mal. | " | | | | | 9865E | 10030 N | ↓ ✓ | |
| V | Skarn, green, 2% Mag, 2% Cpy, + strong mal/az pr. | Comp Grab | | | | | 10125E | 10090 N | ↓ ✓ | |
| W | Skarn, >60% Mag, 1-2% Cpy, strong az/malachite | Grab | | | | | " | " | ↓ ✓ | |

APPENDIX IV

PIT ROCK/SOIL DESCRIPTIONS/ASSAY SHEETS

KLIYUL PROPERTY - PIT & TRENCH SAMPLE DESCRIPTIONS
**B = SOILS
C = ROCKS & CHIPS**

| PIT #/ SAMPLE # | LOCATION EAST NORTH | TYPE | WIDTH (Metres) | DEPTH Metres | DESCRIPTION |
|----------------------------|--------------------------------|-------------|---------------------------|-------------------------|--|
| KLP 001 | 2600 | 1750 | B | 2.5 | |
| KLP 001 | 2600 | 1750 | C | 4.0 | Feldspar phyrlic andesite/diorite. Pyrite on fractures. |
| KLP 002 | 2600 | 1800 | B | 1.0 | |
| KLP 002 | 2600 | 1800 | B | 2.5 | |
| KLP 002 | 2600 | 1800 | C | 3.5 | Gravels of feldspar phyrlic andesite composition. |
| KLP 003 | 2600 | 1850 | B | 2.0 | |
| KLP 003 | 2600 | 1850 | B | 3.0 | |
| KLP 003 | 2600 | 1850 | B | 4.0 | |
| KLP 003 | 2600 | 1850 | C | 4.0 | |
| KLP 004 | 2600 | 1900 | B | 2.0 | |
| KLP 004 | 2600 | 1900 | B | 4.0 | |
| KLP 005 | 2600 | 1950 | B | 1.5 | |
| KLP 005 | 2600 | 1950 | B | 3.5 | |
| KLP 006 | 2600 | 2000 | B | 1.0 | |
| KLP 006 | 2600 | 2000 | C | 2.5 | Bleached andesite. Clay, sericite alteration. Trace pyrite. |
| KLP 007 | 2600 | 2040 | B | 1.5 | |
| KLP 007 | 2600 | 2040 | C | 2.5 | Silicified, sericitic, pyritic, bleached andesite with disseminations and blebs of 5-10% pyrite. |
| KLP 008 | 2600 | 2100 | B | 2.0 | |
| KLP 008 | 2600 | 2100 | B | 5.0 | |
| KLP 009 | 2600 | 2150 | B | 2.0 | |
| KLP 009 | 2600 | 2150 | B | 4.25 | |
| KLP 010 | 2600 | 2200 | B | 1.0 | |
| KLP 010 | 2600 | 2200 | B | 5.0 | |
| KLP 010 | 2600 | 2200 | C | 5.0 | Pyritic, feldspar phyrlic andesite with epidote-quartz-pyrite. Disseminated pyrite. |
| KLP 011 | 2800 | 2200 | B | 1.5 | |
| KLP 011 | 2800 | 2200 | B | 5.0 | |
| KLP 012 | 2800 | 2150 | B | 1.5 | |
| KLP 012 | 2800 | 2150 | B | 3.5 | |
| KLP 013 | 2800 | 2100 | B | 2.0 | |
| KLP 013 | 2800 | 2100 | B | 3.0 | |
| KLP 014 | 2800 | 2045 | C | 1.5 | Sericite, clay altered, bleached andesite. Weakly magnetic. |
| KLP 015 | 2800 | 2000 | C | 4.5 | Mineralized andesite/fine grained diorite. Stockwork of rusty fractures. Magnetic. |
| KLP 016 | 2800 | 1950 | B | 2.0 | |
| KLP 016 | 2800 | 1950 | C | 3.3 | Dark, hematitic andesite. Weakly silicified. Epidote-quartz veinlets. Trace cpy. |
| KLP 017 | 2800 | 1900 | B | 2.0 | |
| KLP 017 | 2800 | 1900 | B | 3.3 | |
| KLP 018 | 2800 | 1860 | B | 2.0 | |
| KLP 018 | 2800 | 1860 | B | 4.7 | |
| KLP 019 | 2800 | 1770 | B | 2.0 | |
| KLP 019 | 2800 | 1770 | B | 3.5 | |
| KLP 020 | 2800 | 1740 | B | 2.0 | |
| KLP 020 | 2800 | 1740 | B | 4.5 | |
| KLP 020 | 2800 | 1740 | C | 5.3 | Ferrocresc/gossanous, clay altered, magnetic bleached rock. |
| KLP 021 | 2800 | 1700 | B | 2.0 | |
| KLP 021 | 2800 | 1700 | B | 4.5 | |
| KLP 021 | 2800 | 1700 | C | 5.5 | Weakly carbonatized andesitic tuff. |
| KLP 022 | 2800 | 1650 | B | 2.0 | |
| KLP 022 | 2800 | 1650 | B | 5.2 | |
| KLP 023 | 3000 | 1700 | B | 2.0 | |
| KLP 023 | 3000 | 1700 | B | 5.5 | |
| KLP 023 | 3000 | 1700 | C | 5.7 | Epidotized & silicified angular boulders? Minor malachite on fractures. |
| KLP 024 | 3000 | 1750 | C | 1.5 | Clay, sericite altered felsic intrusive and andesite (bleached). |
| KLP 024 | 3000 | 1750 | C | 1.8 | Very clay-rich (altered), malachite stained rocks. |
| KLP 025 | 3000 | 1800 | C | 2.0 | Highly fractured, clay altered, soft rock. |

KLIYUL PROPERTY - PIT & TRENCH SAMPLE DESCRIPTIONS
B = SOILS
C = ROCKS & CHIPS

| PIT #/ SAMPLE # | LOCATION EAST NORTH | TYPE | WIDTH (Metres) | DEPTH Metres | DESCRIPTION |
|--------------------|------------------------|------|-------------------|-----------------|---|
| KLP 025 | 3000 1800 | C | | 2.5 | Clay altered andesite/intrusive. 1% malachite. |
| KLP 025 | 3000 1800 | C | | 3.0 | Loose rock at bottom of trench. Hematitic & clay altered. Trace malachite. |
| KLP 026 | 3000 1850 | B | | 2.0 | |
| KLP 026 | 3000 1850 | C | | 5.0 | Light green, clay fault gouge. Trace pyrite. |
| KLP 027 | 3000 1900 | B | | 2.0 | |
| KLP 027 | 3000 1900 | B | | 3.0 | |
| KLP 028 | 3000 1950 | B | | 2.0 | |
| KLP 028 | 3000 1950 | B | | 5.5 | |
| KLP 028 | 3000 1950 | C | | 5.6 | Weakly carbonatized, chloritic andesite. Trace pyrite. |
| KLP 029 | 3000 2000 | B | | 2.0 | |
| KLP 029 | 3000 2000 | B | | 6.0 | |
| KLP 030 | 3000 2030 | B | | 3.0 | |
| KLP 030 | 3000 2030 | C | | 4.5 | Ferrocorte and intensely bleached, argillically altered andesite. |
| KLP 031 | 3000 2070 | C | | 1.5 | Quartz vein (090/40S) & quartz stockwork in sericite-pyrite schist. |
| KLP 031 | 3000 2070 | C | | 2.0 | Sericite-pyrite schist (090/50N). Gossanous & clay rich. |
| KLP 032 | 3000 2100 | B | | 2.0 | |
| KLP 032 | 3000 2100 | B | | 3.8 | |
| KLP 032 | 3000 2100 | C | | 4.0 | Feldspar phytic andesite. Epidote on fractures. Trace pyrite. |
| KLP 033 | 3000 2150 | B | | 2.0 | |
| KLP 033 | 3000 2150 | B | | 3.5 | |
| KLP 033 | 3000 2150 | C | | 3.7 | Pyritic andesite. Angular talus blocks. |
| KLP 034 | 3000 2200 | B | | 2.0 | |
| KLP 034 | 3000 2200 | B | | 5.2 | |
| KLP 035 | 3200 2200 | B | | 2.0 | |
| KLP 035 | 3200 2200 | C | | 2.8 | Bleached, sericite, clay, gossaned andesite. Talus? |
| KLP 036 | 3200 2150 | B | | 2.0 | |
| KLP 036 | 3200 2150 | C | | 3.2 | Chert/quartzite. Trace pyrite. |
| KLP 037 | 3200 2100 | C | | 1.5 | Sheared, bleached, sericite-clay altered rock. Remnant pyrite crystals. |
| KLP 038 | 3200 2065 | C | | 1.5 | Gossanous, chloritic, pyritic andesite. |
| KLP 039 | 3200 2000 | B | | 2.0 | |
| KLP 039 | 3200 2000 | B | | 3.0 | |
| KLP 040 | 3200 1950 | B | | 2.0 | |
| KLP 040 | 3200 1950 | B | | 3.4 | |
| KLP 040 | 3200 1950 | C | | 2.0 | Greenish-grey andesite crystal tuff. Subcrop. |
| KLP 041 | 3200 1900 | B | | 2.0 | |
| KLP 041 | 3200 1900 | B | | 5.3 | |
| KLP 041 | 3200 1900 | C | | 5.5 | Weakly silicified andesite. Trace pyrite. Bedrock/talus? |
| KLP 042 | 3200 1840 | B | | 2.0 | |
| KLP 042 | 3200 1840 | B | | 4.5 | |
| KLP 042 | 3200 1840 | C | | 5.5 | |
| KLP 043 | 3200 1800 | B | | 2.0 | |
| KLP 043 | 3200 1800 | C | | 3.0 | Manganese stained microdiorite dyke/sill. Quartz stockwork & veins. Tr malachite, cpy on frags. |
| KLP 044 | 3200 1760 | B | | 2.0 | |
| KLP 044 | 3200 1760 | B | | 6.0 | |
| KLP 044 | 3200 1760 | C | | 6.0 | Boulders of manganese stained, weakly magnetic dyke rock. |
| KLP 045 | 3200 1720 | B | | 1.0 | |
| KLP 045 | 3200 1720 | C | | 1.0 | Boulders of sericite/pyrite schist. Bedded & disseminated pyrite. |
| KLP 046 | 3200 1660 | B | | 2.0 | |
| KLP 046 | 3200 1660 | B | | 5.0 | |
| KLP 046 | 3200 1660 | C | | 6.5 | Angular blocks of sericite, chlorite, pyrite schist. Hematite coated. Trace malachite. |
| KLP 047 | 3400 1970 | B | | 1.0 | |
| KLP 047 | 3400 1970 | C | | - | |
| KLP 048 | 3400 2050 | B | | 2.0 | |
| KLP 049 | 3300 2055 | C | | 2.0 | Pyritic, bleached, well fractured andesite. 5-7% pyrite. |
| KLP 050 | 3300 2070 | C | | 1.5 | Chloritic andesite. Weathered feldspars. Fine grained magnetite & trace pyrite. |

KLIYUL PROPERTY - PIT & TRENCH SAMPLE DESCRIPTIONS
**B = SOILS
C = ROCKS & CHIPS**

| PIT #/ SAMPLE # | LOCATION | | TYPE | WIDTH (Metres) | DEPTH (Metres) | DESCRIPTION |
|--------------------|----------|-------|------|-------------------|-------------------|---|
| | EAST | NORTH | | | | |
| KLP 051 | 3390 | 2095 | B | | 2.0 | |
| KLP 051 | 3390 | 2095 | B | | 3.0 | |
| KLP 051 | 3390 | 2095 | C | | 3.3 | Bleached, weathered, clay, sericite, pyrite altered andesite. |
| KLP 052 | 3400 | 2150 | B | | 2.0 | |
| KLP 052 | 3400 | 2150 | B | | 4.0 | |
| KLP 052 | 3400 | 2150 | C | | 4.2 | Ferrocrite; weathered andesite (magnetic). |
| KLP 053 | 3400 | 2200 | B | | 2.0 | |
| KLP 053 | 3400 | 2200 | B | | 3.0 | |
| KLP 054 | 3400 | 2250 | B | | 2.0 | |
| KLP 054 | 3400 | 2250 | B | | 3.6 | |
| KLP 054 | 3400 | 2250 | C | | 3.8 | Foliated, chloritic andesite. Rare quartz-carbonate veinlets & pyrite. |
| KLP 055 | 3600 | 2250 | B | | 2.0 | |
| KLP 055 | 3600 | 2250 | B | | 4.0 | |
| KLP 055 | 3600 | 2250 | C | | 4.6 | Massive pyritic, chloritic andesite. Minor epidote on fractures. Weakly silicified. 5-10% py. |
| KLP 056 | 3580 | 2180 | B | | 2.0 | |
| KLP 056 | 3580 | 2180 | B | | 3.5 | |
| KLP 057 | 3610 | 2140 | C | | 1.8 | Massive pyritic, chloritic andesite with epidote +/- pyrite on fractures. |
| KLP 058 | 3575 | 2100 | B | | 1.0 | |
| KLP 058 | 3575 | 2100 | B | | 1.5 | |
| KLP 058 | 3575 | 2100 | C | | 2.5 | Fault gouge. Epidote, carbonate & pyrite. |
| KLP 059 | 3600 | 2050 | B | | 2.0 | |
| KLP 060 | 3600 | 2000 | B | | 2.0 | |
| KLP 060 | 3600 | 2000 | C | | 3.0 | |
| KLP 061 | 3800 | 2000 | C | | 0.3 | Massive, fractured, blocky andesite with epidote veinlets & veined/disseminated pyrite. |
| KLP 062 | 3800 | 2050 | C | | 0.3 | As above. 1-2% pyrite. |
| KLP 063 | 3800 | 2100 | C | | 1.0 | Highly fractured, bleached, rusty andesite. |
| KLP 064 | 3800 | 2150 | B | | 2.0 | |
| KLP 064 | 3800 | 2150 | C | | 3.0 | Andesite with blabs & disseminations of pyrite & arsenopyrite? |
| KLP 065 | 3800 | 2260 | B | | 2.0 | |
| KLP 065 | 3800 | 2260 | C | | 3.0 | |
| KLP 066 | 3785 | 2300 | B | | 1.5 | |
| KLP 066 | 3785 | 2300 | C | | 1.8 | Strongly epidotized (blabs & veinlets) andesite. Hornfelsed & weak carbonate alteration. |
| KLP 067 | 4000 | 2395 | B | | 2.5 | |
| KLP 068 | 4200 | 2440 | C | | 0.5 | Same as KLP-66-1.8. Trace pyrite. |
| KLP 069 | 4200 | 2300 | B | | 2.0 | |
| KLP 069 | 4200 | 2300 | C | | 2.5 | Massive, dark green andesite with epidote filled fractures. |
| KLP 070 | 4200 | 2245 | B | | 2.0 | |
| KLP 070 | 4200 | 2245 | B | | 3.5 | |
| KLP 070 | 4200 | 2245 | C | | 3.6 | Dark green, massive andesite. |
| KLP 071 | 4200 | 2200 | B | | 2.0 | |
| KLP 071 | 4200 | 2200 | B | | 3.5 | |
| KLP 072 | 4200 | 2100 | B | | 1.5 | |
| KLP 072 | 4200 | 2100 | B | | 2.5 | |
| KLP 072 | 4200 | 2100 | C | | 2.8 | Quartz vein material in hornfelsed andesite with cpy on fractures. |
| KLP 073 | 4000 | 2000 | B | | 2.0 | |
| KLP 073 | 4000 | 2000 | C | | 2.6 | Chloritized, epidotized blocky andesite subcrop. Trace -2% pyrite. |
| KLP 074 | 4000 | 2050 | B | | 2.0 | |
| KLP 074 | 4000 | 2050 | B | | 4.5 | |
| KLP 074 | 4000 | 2050 | C | | 4.6 | Massive dioritic sill/dyke. Hornfelsed & epidote altered feldspars. |
| KLP 075 | 4000 | 2110 | B | | 2.0 | |
| KLP 075 | 4000 | 2110 | C | | 3.0 | Chloritic, well fractured andesite, weakly carbonatized with cubic pyrite. |
| KLP 076 | 4000 | 2150 | C | | 0.7 | Massive, hematite stained quartz vein with trace py, cpy in carbonatized andesite. |
| KLP 076 | 4000 | 2150 | C | | 0.7 | Pyritic, silicified, calcareous, epidotized, fractured andesite. Trace - 3% pyrite. |
| KLP 077 | 4000 | 2200 | B | | 2.0 | |
| KLP 077 | 4000 | 2200 | C | | 2.8 | Subcrop of silicified, epidotized andesite with trace pyrite. |

KLIYUL PROPERTY - PIT & TRENCH SAMPLE DESCRIPTIONS
**B = SOILS
C = ROCKS & CHIPS**

| PIT #/ SAMPLE # | LOCATION | | TYPE | WIDTH (Metres) | DEPTH (Metres) | DESCRIPTION |
|--------------------|----------|-------|------|-------------------|-------------------|--|
| | EAST | NORTH | | | | |
| KLP 078 | 3900 | 2200 | B | | 2.0 | |
| KLP 078 | 3900 | 2200 | C | | 4.2 | Subcrop of carbonatized andesitic blocks with silica rich fractures. 2-3% pyrite. |
| KLP 079 (381-O) | 3900 | 2140 | C | 0.5 | | Clay rich fault gouge (green-grey) plus unaltered andesite. |
| KLP 079 (381-P) | 3900 | 2140 | C | 0.75 | | Gossaned, clay altered, well fractured volcanic adjacent to bull quartz vein. |
| KLP 079 (381-Q) | 3900 | 2140 | C | 1.0 | | Highly crushed quartz vein material. Weak manganese, hematite staining. |
| KLP 079 (381-R) | 3900 | 2140 | C | 1.0 | | Same as KLP-79 (381-P). |
| KLP 079 (381-S) | 3900 | 2140 | C | 1.5 | | Well fractured, green-grey fault gouge. |
| KLP 079 (381-T) | 3900 | 2140 | C | 2.0 | | Gossanous andesite. Trace epidote. |
| KLP 080 | 3900 | 2100 | C | | 0.6 | Dark green, chloritic andesite with rusty fractures. |
| KLP 081 | 3900 | 2050 | B | | 2.0 | |
| KLP 081 | 3900 | 2050 | C | | 4.0 | Angular boulders of chloritic andesite. Trace pyrite & epidote on fractures. |
| KLP 082 | 3900 | 2000 | B | | 2.0 | |
| KLP 082 | 3900 | 2000 | C | | 3.6 | Massive, dark green, hornfelsed andesite. Epidote & 1-2% pyrite on fractures. |
| KLP 083 (381-U) | 3900 | 1970 | C | 0.6 | | Fine grained, dark green, chloritic andesite. Well fractured. |
| KLP 083 (381-V) | 3900 | 1970 | C | 1.4 | | Manganese - iron stained fault gouge with quartz-carbonate stringers. |
| KLP 083 (381-W) | 3900 | 1970 | C | 1.2 | | Hematite stained massive quartz vein. Trace pyrite. |
| KLP 083 (382-A) | 3900 | 1970 | C | 1.4 | | Highly fractured, chloritic andesite. Trace - 2% pyrite. |
| KLP 083 (382-B) | 3900 | 1970 | C | 1.2 | | Intensely fractured, chloritic, manganese stained andesite. |
| KLP 083 (382-C) | 3900 | 1970 | C | 1.0 | | Intensely fractured, chloritic andesite. |
| KLP 083 (382-D) | 3900 | 1970 | C | 1.0 | | Massive quartz-carbonate vein. Hematite, manganese, pyrite. |
| KLP 083 (382-E) | 3900 | 1970 | C | 1.6 | | Manganese stained, dark green, chloritic andesite. Moderate - well fractured. |
| KLP 084 (381-F) | 4000 | 1950 | C | 0.5 | | Highly fractured andesite, manganese stained. Fault gouge present. |
| KLP 084 (381-G) | 4000 | 1950 | C | 1.0 | | Highly fractured andesite. Bleached, gossanous, minor quartz. |
| KLP 084 (381-H) | 4000 | 1950 | C | 1.0 | | Hematite, manganese stained massive quartz vein. Trace sulfides. |
| KLP 084 (381-I) | 4000 | 1950 | C | 2.0 | | Hematite, manganese stained massive bull quartz vein material. |
| KLP 084 (381-J) | 4000 | 1950 | C | 1.0 | | Siliceous, pyritic, foliated andesite. Disseminated & veined pyrite (parallel to foliation). |
| KLP 084 (381-K) | 4000 | 1950 | C | 1.0 | | Manganese, clay rich fault gouge with minor quartz vein material. |
| KLP 084 (381-L) | 4000 | 1950 | C | 0.7 | | Manganese stained, fractured (clay coated) andesite. |
| KLP 084 (381-M) | 4000 | 1950 | C | 0.5 | | Chloritic andesite. Minor quartz healed breccia. Manganese stained. |
| KLP 085 | 3700 | 2000 | B | | 2.0 | |
| KLP 086 | 3700 | 1900 | B | | 1.0 | |
| KLP 086 | 3700 | 1900 | C | | 1.5 | Bleached pyrite andesite/altered intrusive. |
| KLP 087 | 3700 | 1800 | B | | 2.0 | |
| KLP 087 | 3700 | 1800 | B | | 3.5 | |
| KLP 088 | 3700 | 1700 | B | | 2.0 | |
| KLP 088 | 3700 | 1700 | C | | 1.8 | Bleached, gossaned, altered intrusive/monzonite. 2-3% pyrite. |
| KLP 089 | 3700 | 1600 | C | | 2.0 | Bleached, gossaned, altered intrusive/monzonite. 2-3% pyrite. |
| KLP 090 | 3700 | 1550 | B | | 2.5 | |
| KLP 090 | 3700 | 1550 | C | | 4.1 | Sericite, clay, altered monzonite. Gossanous. |
| KLP 091 | 3700 | 1500 | C | | - | Sericite, clay, altered monzonite. Gossanous. |
| KLP 092 | 3500 | 1600 | C | | 1.5 | Pyritic, gossaned altered monzonite. Moderate-well fractured. |
| KLP 093 | 3500 | 1650 | B | | 2.0 | |
| KLP 093 | 3500 | 1650 | C | | 3.0 | Altered monzonite with trace pyrite. Epidote/pyrite seams observed. |
| KLP 094 | 3500 | 1700 | C | | 1.5 | Gossanous monzonite with sericite/hematite stained fractures. |
| KLP 095 | 3500 | 1750 | C | | 3.2 | Chloritic feldspar porphyry dyke. Chlorite, sericite on fractures. Trace malachite. |
| KLP 096 | 3500 | 1800 | B | | 2.0 | |
| KLP 096 | 3500 | 1800 | C | | 2.5 | Fractured intrusive (monzonite)/andesite. Clay, sericite on fractures. Trace py +/- cpy. |
| KLP 097 | 3500 | 1850 | B | | 2.0 | |
| KLP 097 | 3500 | 1850 | C | | 2.5 | Same as KLP-95-3.2. |
| KLP 098 | 3500 | 1900 | B | | 2.0 | |
| KLP 099 | 3525 | 1950 | C | | 3.0 | Fine grained, locally silicified andesite rubble. Locally pyritic to 3%. Epidote noted. |
| KLP 100 | 3500 | 2000 | B | | 2.0 | |
| KLP 101 | 3500 | 2120 | C | | 2.0 | Chloritic, epidotized dark green andesite. Trace magnetite. |
| KLP 102 | 3500 | 2150 | B | | 2.0 | |
| KLP 102 | 3500 | 2150 | B | | 3.5 | |

KLIYUL PROPERTY - PIT & TRENCH SAMPLE DESCRIPTIONS
B = SOILS
C = ROCKS & CHIPS

| PIT #/ SAMPLE # | LOCATION | | TYPE | WIDTH (Metres) | DEPTH (Metres) | DESCRIPTION |
|--------------------|----------|-------|------|-------------------|-------------------|--|
| | EAST | NORTH | | | | |
| KLP 103 | 3500 | 2200 | B | | 2.0 | |
| KLP 103 | 3500 | 2200 | B | | 3.0 | |
| KLP 104 | 3500 | 2250 | B | | 2.5 | |
| KLP 105 | 3500 | 2300 | B | | 2.5 | |
| KLP 105 | 3500 | 2300 | C | | 3.0 | Angular rubble of dark green, massive andesite with epidote, chlorite & quartz-carbonate weavtr. |
| KLP 106 | 3700 | 2300 | C | | 1.5 | Dark green, hornfelsed andesite. Strong epidotization of feldspar phenocrysts. |
| KLP 107 | 3700 | 2250 | B | | 1.5 | |
| KLP 107 | 3700 | 2250 | C | | 1.5 | Chloritic andesite with epidote-carbonate on fractures. Trace - 2% pyrite locally. |
| KLP 108 | 3700 | 2200 | B | | 2.0 | |
| KLP 108 | 3700 | 2200 | C | | 2.5 | Angular boulders of epidotized andesite. |
| KLP 109 | 3700 | 2150 | B | | 1.5 | |
| KLP 110 | 3650 | 2080 | C | | 2.0 | Angular boulders? of epidotized andesite. Weakly bleached. |
| KLP 111 | 3300 | 2250 | B | | 3.0 | |
| KLP 111 | 3300 | 2250 | C | | 6.0 | Highly altered pyritic andesite/intrusive? |
| KLP 112 | 3300 | 2200 | C | | 1.5 | Mineralized, dark green andesite with abundant magnetite, trace py, malachite. |
| KLP 113 | 3300 | 2150 | B | | 2.0 | |
| KLP 113 | 3300 | 2150 | C | | 2.5 | Chloritic andesite with magnetite-epidote skarning. Trace malachite. |
| KLP 114 | 3300 | 2100 | B | | 2.0 | |
| KLP 115 | 3300 | 1950 | B | | 3.5 | |
| KLP 115 | 3300 | 1950 | C | | 0.3 | Clay, sericite altered monzonite. Well fractured. 5-7% pyrite locally. |
| KLP 116 | 3300 | 1900 | C | | 1.5 | Strong clay altered, grey, bleached monzonite. |
| KLP 117 | 3300 | 1850 | B | | 2.0 | |
| KLP 117 | 3300 | 1850 | B | | 4.0 | |
| KLP 118 | 3300 | 1800 | C | | 2.0 | Hematite stained massive quartz material. Trace pyrite. |
| KLP 118 | 3300 | 1800 | C | | 5.5 | Chloritic diorite/monzonite with epidote on fractures, trace pyrite, weakly magnetic. |
| KLP 119 | 3300 | 1750 | B | | 1.5 | |
| KLP 119 | 3300 | 1750 | C | | 5.6 | Weakly silicified, epidotized monzonite with fine grained pyrite and minor manganese. |
| KLP 120 | 3300 | 1700 | C | | 5.0 | Weakly silicified, epidotized monzonite with fine grained pyrite and minor manganese. |
| KLP 121 | 3100 | 1700 | B | | 2.0 | |
| KLP 121 | 3100 | 1700 | B | | 6.0 | |
| KLP 121 | 3100 | 1700 | C | | 5.0 | Quartz-carbonate-pyrite stockwork in altered monzonite/andesite. |
| KLP 122 | 3100 | 1750 | B | | 2.0 | |
| KLP 122 | 3100 | 1750 | C | | 5.0 | Epidote-pyrite stockwork in altered intrusive/chloritic andesite. |
| KLP 122 | 3100 | 1750 | C | | 6.5 | Chloritic, propylitized, massive monzonite/diorite. |
| KLP 123 | 3100 | 1800 | B | | 2.0 | |
| KLP 123 | 3100 | 1800 | B | | 3.0 | |
| KLP 123 | 3100 | 1800 | C | | 5.0 | Malachite stained, moderate epidotization of monzonite/diorite. |
| KLP 124 | 3100 | 1850 | B | | 2.5 | |
| KLP 124 | 3100 | 1850 | B | | 5.5 | |
| KLP 124 | 3100 | 1850 | C | | 5.6 | Malachite, azurite (trace) on mineralized andesite/alterred monzonite gravels. |
| KLP 125 | 3100 | 1900 | B | | 2.0 | |
| KLP 125 | 3100 | 1900 | B | | 3.0 | |
| KLP 126 | 3085 | 1950 | B | | 2.0 | |
| KLP 126 | 3085 | 1950 | B | | 3.0 | |
| KLP 127 | 3100 | 2010 | C | | 1.5 | Bleached andesite/monzonite with chlorite, epidote, magnetite. |
| KLP 128 | 3100 | 2080 | C | | 0.3 | Bleached, pyritic andesite. Sericitic, gossanous 3-5% py. |
| KLP 129 | 3100 | 2120 | B | | 2.0 | |
| KLP 130 | 3100 | 2170 | B | | 2.0 | |
| KLP 130 | 3100 | 2170 | B | | 3.8 | |
| KLP 131 | 3100 | 2215 | B | | 2.5 | |
| KLP 132 | 3100 | 2250 | B | | 4.0 | |
| KLP 132 | 3100 | 2250 | B | | ? | |
| KLP 133 | 3135 | 2215 | C | | 3.0 | Same as KLP-128. Clay altered. |
| KLP 134 | 3200 | 2215 | C | | 3.0 | Same as KLP-128. Clay altered. 5-7% pyrite. |
| KLP 135 | 3100 | 2300 | B | | 5.0 | |

KLIYUL PROPERTY - PIT & TRENCH SAMPLE DESCRIPTIONS
**B = SOILS
C = ROCKS & CHIPS**

| PIT #/ SAMPLE # | LOCATION | | TYPE | WIDTH (Metres) | DEPTH (Metres) | DESCRIPTION |
|--------------------|----------|-------|------|-------------------|-------------------|---|
| | EAST | NORTH | | | | |
| KLP 136 | 3000 | 2250 | B | | 2.0 | |
| KLP 137 | 2900 | 2250 | B | | 2.5 | |
| KLP 138 | 2900 | 2150 | B | | 2.5 | |
| KLP 139 | 2900 | 2100 | B | | 3.0 | |
| KLP 140 (382-M) | 2890 | 2050 | C | 1.0 | | Altered andesite/diorite/monzonite with magnetite, epidote, chlorite. |
| KLP 140 (382-N) | 2890 | 2050 | C | 1.0 | | Bleached, gossanous fracture zone with magnetite, epidote, sericite. |
| KLP 140 (382-O) | 2890 | 2050 | C | 1.0 | | Altered andesite/diorite with magnetite, epidote, chlorite. |
| KLP 140 (382-P) | 2890 | 2050 | C | 1.0 | | Gossanous fracture zone with epidote, chlorite. |
| KLP 140 (382-Q) | 2890 | 2050 | C | 1.0 | | Altered andesite/diorite. Magnetite-epidote-chlorite. |
| KLP 141 (382-R) | 2900 | 2010 | C | 1.0 | | Fault gouge. Magnetite, epidote, chlorite. |
| KLP 141 (382-S) | 2900 | 2010 | C | 1.0 | | Chlorite, clay, epidote, magnetite altered zone. |
| KLP 141 (382-T) | 2900 | 2010 | C | 1.0 | | Gossan with malachite, chlorite, manganese. |
| KLP 141 (382-U) | 2900 | 2010 | C | 1.0 | | Fault brecciated carbonatized sediments/fine grained, chloritic andesites. |
| KLP 142 | 2900 | 1950 | B | | 2.5 | |
| KLP 142 | 2900 | 1950 | C | | 5.5 | Epidote, magnetite, hematite altered volcanic/intrusive. |
| KLP 143 | 2900 | 1900 | B | | 4.5 | |
| KLP 143 | 2900 | 1900 | C | | 4.6 | Angular gravel of magnetite, chlorite altered material. |
| KLP 144 | 2900 | 1850 | C | | 2.0 | Highly fractured zone of hematite, chlorite, malachite, magnetite mineralization. |
| KLP 145 | 2900 | 1800 | C | | 2.5 | Altered monzonite. Bleached, sericite, clay, magnetite. |
| KLP 146 | 2900 | 1780 | C | | 4.7 | Mineralized magnetite, sericite, clay altered gravels. |
| KLP 147 | 2900 | 1700 | C | | 4.0 | Fault zone. Manganese stained diorite. Malachite on fractures. |
| KLP 147 | 2900 | 1700 | C | | 5.7 | Chloritic diorite/gabbro? Fresh (no mineralization). |
| KLP 148 | 2900 | 1650 | B | | 5.0 | |
| KLP 149 | 2700 | 1750 | B | | 3.0 | |
| KLP 149 | 2700 | 1750 | C | | 6.0 | Propylitized andesite boulders with chalcopyrite & magnetite. |
| KLP 149 | 2700 | 1750 | C | | 6.5 | Mafic dyke rock. Weakly magnetic, strongly epidotized on fractures. |
| KLP 150 | 2700 | 1800 | B | | 2.0 | |
| KLP 150 | 2700 | 1800 | B | | 4.0 | |
| KLP 150 | 2700 | 1800 | C | | 4.5 | Angular, mineralized gravels. Chlorite, magnetite, epidote. |
| KLP 151 | 2700 | 1860 | B | | 3.5 | |
| KLP 152 | 2700 | 1940 | B | | 2.4 | |
| KLP 152 | 2700 | 1940 | C | | 2.5 | Chloritized andesite/diorite with pyrite, epidote, trace malachite, chalcopyrite. |
| KLP 153 | 2700 | 1965 | B | | 2.0 | |
| KLP 153 | 2700 | 1965 | B | | 3.5 | |
| KLP 153 | 2700 | 1965 | C | | 3.4 | Massive hornfelsed andesite. 25% manganese, locally 2-3% cpy. |
| KLP 154 | 2700 | 2010 | C | | 1.0 | Propylitized, fractured andesite with minor manganese, epidote. |
| KLP 155 | 2700 | 2050 | C | | 0.3 | Argillic, sericitic, chloritic, manganese altered volcanic/intrusive? |
| KLP 156 | 2700 | 2095 | C | | 5.8 | Intense sericite, clay altered rock. Bleached. Mariposite? |
| KLP 157 | 2715 | 2150 | B | | 3.0 | |
| KLP 158 | 2690 | 2200 | B | | 2.5 | |
| KLP 159 | 2700 | 2250 | B | | 3.0 | |
| KLP 160 | 2700 | 2300 | B | | 6.0 | |
| KLP 161 | 2700 | 2350 | B | | 4.0 | |
| KLP 162 | 2700 | 2400 | B | | 2.0 | |
| KLP 163 | 2700 | 2450 | B | | 4.0 | |
| KLP 164 | 2700 | 2500 | B | | 3.0 | |
| KLP 165 | 2400 | 2550 | C | | 1.5 | Fine grained, grey-green andesite sill/dyke? Weakly magnetic. |
| KLP 166 | 2400 | 2600 | C | | 1.0 | Fine grained, grey-green andesite with pyritic fractures & weakly magnetic. |
| KLP 167 | 2400 | 2650 | B | | 7.0 | |
| KLP 168 | 2000 | 2600 | C | | 0.5 | Pyritic augite porphyry. |
| KLP 169 | 2000 | 2500 | C | | 1.0 | Fractured augite porphyry; manganese, calcite coatings. Weakly magnetic. |
| KLP 170 | 1720 | 2450 | C | | 0.5 | Massive, fractured augite, feldspar, hornblende porphyry. |
| KLP 171 | 1720 | 2550 | C | | 0.5 | As above. Epidotized. 3-5% pyrite. |
| KLP 172 | 1720 | 2600 | C | | 0.3 | Pyritic andesite. Epidote. Trace pyrite. |
| KLP 173 (383-I) | 1720 | 2650 | C | 2.0 | | Highly fractured zone (fault) with quartz stringers and minor magnetite. |

KLIYUL PROPERTY - PIT & TRENCH SAMPLE DESCRIPTIONS

 B = SOILS
 C = ROCKS & CHIPS

| PIT #/ SAMPLE # | LOCATION | | TYPE | WIDTH (Metres) | DEPTH Metres) | DESCRIPTION |
|--------------------|----------|-------|------|-------------------|------------------|--|
| | EAST | NORTH | | | | |
| KLP 173 (383-J) | 1720 | 2650 | C | 2.0 | | Highly fractured zone (fault) with quartz stringers and minor magnetite. |
| KLP 173 (383-K) | 1720 | 2650 | C | 2.0 | | Highly fractured zone (fault) with quartz stringers and minor magnetite. |
| KLP 173 (383-L) | 1720 | 2650 | C | 2.0 | | |
| KLP 174 (383-M) | 1720 | 2700 | C | 2.0 | | Gossanous, clay altered, fractured, manganese stained rock. |
| KLP 174 (383-O) | 1720 | 2700 | C | 2.0 | | Gossanous, clay altered, fractured, manganese stained rock. |
| KLP 174 (383-P) | 1720 | 2700 | C | 2.0 | | Gossanous volcanic? with quartz, pyrite veins & cpy. |
| KLP 174 (383-Q) | 1720 | 2700 | C | 2.0 | | Quartz (30%) flooded andesite. |
| KLP 174 (383-R) | 1720 | 2700 | C | 2.0 | | Clay, manganese, carbonate altered andesite/fault gouge. |
| KLP 175 (383-T) | 1720 | 2750 | C | ? | | Fault gouge described above. |
| KLP 176 | 2850 | 1800 | C | | 4.0 | Weathered volcanic? Chlorite & magnetite altered. |
| KLP 177 (383-V) | 1710 | 2810 | C | 0.7 | | Massive quartz-carbonate vein with pyrite. |
| KLP 177 (383-W) | 1710 | 2810 | C | | | Silicified, carbonatized andesite adjacent to veins in above sample. |
| KLP 177 (384-A) | 1710 | 2810 | | | | Missing sample? |
| KLP 178 | 1200 | 2700 | C | | 2.0 | Green, grey, locally epidotized, hornfelsic andesite. |
| KLP 179 | 1200 | 2675 | C | | 1.0 | Fine grained, gossanous, chloritic, pyrite andesite. Sheared. |
| KLP 180 | 1200 | 2650 | C | | 1.5 | Bleached, gossanous, pyritic andesite. Weak silicification & sericite. 3-5% pyrite. |
| KLP 181 | 1200 | 2600 | C | | 2.5 | Gossanous, fine grained, andesite with pyrite filled fractures. |
| KLP 182 | 1200 | 2550 | C | | 0.5 | Massive augite porphyry. Trace pyrite. |
| KLP 183 | 1200 | 2500 | C | | 0.5 | Massive augite porphyry. Trace pyrite. |
| KLP 184 | 1200 | 2450 | C | | 1.5 | Altered microdiorite. Locally fractured. |
| KLP 185 | 1200 | 2400 | C | | 1.0 | Chloritic, sericitic, weakly silicified andesite. 10% pyrite. |
| KLP 186 | 1200 | 2350 | C | | 3.0 | Altered augite porphyry/diorite. Trace - 2% pyrite. Rusty & bleached. |
| KLP 187 | 1200 | 2300 | C | | 2.5 | Massive, dark green, chloritic andesite. 3-5% pyrite. |
| KLP 188 | 1200 | 2250 | C | | 1.5 | As above with pyrite stringers. Rusty. |
| KLP 189 | 1200 | 2200 | C | | 5.5 | Bleached augite porphyritic andesite. 2-3% pyrite. |
| KLP 190 | 1000 | 2300 | C | | 6.0 | Argillically altered, gossanous, hornfelsic andesite. |
| KLP 191 | 1000 | 2350 | C | | 3.5 | Bleached, gossanous andesite. 2-3% pyrite & minor sericite. |
| KLP 192 | 1000 | 2400 | C | | 2.0 | Soft, bleached, clay, sericite, pyrite altered, oxidized volcanic/intrusive? |
| KLP 193 | 1000 | 2450 | C | | 1.0 | Sericite, pyrite, gossanous volcanic/intrusive. Locally to 20% fine grained disseminated pyrite. |
| KLP 194 | 1000 | 2500 | C | | 1.5 | Sheared carbonate, chlorite altered microdiorite. |
| KLP 195 | 1000 | 2550 | C | | 1.0 | Chlorite, epidote altered diorite (fine grained) with manganese fractures and trace - 3% sulfides. |
| KLP 196 | 1000 | 2600 | C | | 1.5 | Carbonatized andesite with limonitic fault zone. |
| KLP 197 | 1000 | 2650 | C | | 5.5 | Hornfelsic andesite. Siliceous, trace epidote. |
| KLP 198 | 1000 | 2700 | C | | 4.0 | Hornfelsic andesite. Weakly calcareous. |
| KLP 199 | 1000 | 2750 | B | | 3.0 | |
| KLP 200 | 775 | 2950 | C | | 2.0 | Strongly sheared carbonate, sericite, pyrite schist. Clay altered. |
| KLP 201 | 775 | 2950 | C | | 2.0 | Strongly sheared carbonate, sericite, pyrite schist. Clay altered. |
| KLP 202 | 775 | 2900 | C | | 2.0 | Strongly sheared carbonate, sericite, pyrite schist. Clay altered. |
| KLP 203 | 775 | 2850 | B | | 3.0 | |
| KLP 204 | 775 | 2800 | C | | 1.0 | Gossanous sericite, pyrite, schist. |
| KLP 205 | 775 | 2750 | C | | 2.0 | Sericite, carbonate, pyrite altered andesite. |
| KLP 206 | 775 | 2700 | C | | 2.0 | Bleached, gossanous, sericite, hematite +/- pyrite, limonite, carbonate altered volcanic. |
| KLP 207 | 775 | 2650 | C | | 5.0 | Malachite/azurite stained, magnetic, gossanous volcanic/intrusive? |
| KLP 208 | 775 | 2650 | C | | 1.0 | Malachite/azurite stained, magnetic, gossanous volcanic/intrusive? |
| KLP 209 | 775 | 2600 | C | | 0.5 | Well sheared, oxidized, clay, manganese altered gossanous volcanic/intrusive? |
| KLP 210 | 775 | 2550 | C | | ? | Green clay, manganese, quartz flooded fault gouge. |
| KLP 211 | 775 | 2500 | B | | 2.5 | |
| KLP 211 | 775 | 2500 | C | | 0.5 | Carbonatized, gossanous andesite. Locally to 15% fine grained, pyrite. |
| KLP 212 | 775 | 2450 | C | | 1.5 | Mylonitic fault zone with quartz-carbonate boudins. Talc. |
| KLP 213 | 1600 | 2000 | C | | 1.0 | Massive, chloritic andesite/diorite. Local, weak manganese, pyrite, epidote flooding. |
| KLP 214 | 1800 | 1600 | C | | 2.5 | Quartz-hornblende felsic intrusive (quartz monzonite)? |
| KLP 215 | 1800 | 1550 | B | | 2.0 | |
| KLP 215 | 1800 | 1550 | C | | 2.5 | Brown, black graphitic shale. Trace pyrite +/- malachite. |
| KLP 216 | 1800 | 1500 | C | | 4.0 | Graphitic shale. |
| KLP 217 | 1800 | 1450 | C | | 4.0 | Graphitic shale. |

KLIYUL PROPERTY - PIT & TRENCH SAMPLE DESCRIPTIONS
**B = SOILS
C = ROCKS & CHIPS**

| PIT #/ SAMPLE # | LOCATION EAST NORTH | TYPE | WIDTH (Metres) | DEPTH (Metres) | DESCRIPTION |
|--------------------|------------------------|------|-------------------|-------------------|--|
| KLP 218 | 1800 1400 | C | | 5.5 | Graphitic shale. Trace pyrite. |
| KLP 219 | 1800 1350 | C | | 4.0 | Tuffaceous sediment (sandstone) with quartz stringers. |
| KLP 220 | 2000 1300 | C | | 4.0 | Tuffaceous sediment. Weakly silicified. Trace - 3% pyrite. Quartz stringers with trace py, cpy. |
| KLP 221 | 2000 1350 | C | | 3.5 | Graphitic shale, bleached, with pyrite seams. |
| KLP 222 | 2000 1400 | B | | 6.0 | |
| KLP 223 | 2000 1450 | B | | 6.0 | |
| KLP 224 | 2000 1500 | C | | 3.5 | Tuffaceous sediment. Weak silicification, local epidote, 3-5% pyrite. |
| KLP 225 | 2850 1770 | C | | 4.5 | Bleached sericitic, pyritic andesite/alterd intrusive. |
| KLP 226 | 2850 1750 | C | | 2.5 | Sericitic intrusive/andesite with minor malachite stained fractures. |
| KLP 227 | 2850 1720 | C | | 5.0 | Sericitic intrusive/andesite with minor malachite stained fractures. |
| KLP 228 | 3050 1700 | C | | 7.0 | Quartz monzonite? Chloritic. Trace, disseminated pyrite. |
| KLP 229 | 3050 1750 | C | | 5.0 | Pervasive propylitic alteration of monzonite. 5-7% pyrite. |
| KLP 230 | 3050 1800 | C | | 5.0 | Chloritic, epidotized altered monzonite/andesite. |
| KLP 231 | 3990 1635 | C | | 1.5 | F.g. quartz-feldspar porphyry. Sheared, chloritic. 15-20% disseminated & fracture filled py. |
| KLP 232 | 4035 1610 | C | | 2.5 | F.g. quartz-feldspar porphyry. Strongly sheared. 5% disseminated & fracture filled pyrite. |
| KLP 233 | 4040 1550 | B | | 5.5 | |
| KLP 234 | 4040 1500 | C | | 2.0 | Fine grained, quartz-feldspar porphyry. Sheared & vary weathered. 10-15% disseminated pyrite. |
| KLP 235 | 4040 1450 | C | | 2.5 | As above. 2% disseminated pyrite. |
| KLP 236 | 4040 1400 | C | | 2.5 | As above. 2% disseminated pyrite. |
| KLP 237 | 4040 1350 | C | | 1.5 | Fine grained, quartz-feldspar porphyry. Well sheared, sericitic. 1% disseminated pyrite. |
| KLP 238 | 4040 1300 | C | | 1.5 | Fine grained, quartz-feldspar porphyry. Fractured & weathered. <1% pyrite. |
| KLP 239 | 4020 1250 | C | | 5.5 | Fine grained, quartz-feldspar porphyry. Fractured & weathered. <1% pyrite. |
| KLP 240 | 4010 1200 | C | | 4.0 | Quartz-feldspar porphyry. Weakly sheared. Minor sericite. 1% disseminated pyrite. |
| KLP 240 | 4010 1200 | C | | 4.2 | Quartz-feldspar porphyry. Strongly sheared & intense sericite. 5-10% disseminated pyrite. |
| KLP 241 | 4010 1150 | C | | 1.0 | Quartz-feldspar porphyry. Weak shearing, <1% disseminated pyrite. Malachite on fractures. |
| KLP 242 | 4010 1125 | C | | 1.0 | Fine-grained quartz-feldspar porphyry. Sheared with 10-20% disseminated & fracture filled pyrite. |
| KLP 243 | 4010 1100 | C | | 1.5 | Medium-f.g. quartz-feldspar porphyry. Weak sericitic alteration. 5% disseminated py, tr malachite. |
| KLP 244 | 4010 1050 | C | | 3.0 | Gabbro with talc. Magnetic. |
| KLP 245 | 4060 1075 | C | | 1.0 | Medium-fine grained quartz-feldspar porphyry. 2-5% fine grained, disseminated pyrite. |
| KLP 246 | 4060 1125 | C | | 1.1 | Coarse grained quartz-feldspar porphyry. Silicified & sheared. 20% dissem. & fracture filled py. |
| KLP 247 | 4100 1175 | B | | 2.5 | |
| KLP 247 | 4100 1175 | B | | 6.0 | |
| KLP 248 | 4100 1225 | B | | 4.5 | |
| KLP 248 | 4100 1225 | B | | 6.5 | |
| KLP 249 | 4175 1275 | C | | 1.5 | Quartz-feldspar porphyry. Bleached, sheared, sericitic. 10-15% disseminated pyrite. |
| KLP 250 | 4175 1325 | C | | 1.0 | Well sheared, sericitic quartz-feldspar porphyry; bleached. Trace pyrite. |
| KLP 251 | 4175 1375 | B | | 3.0 | |
| KLP 252 | 4200 1425 | B | | 5.5 | |
| KLP 253 | 4220 700 | C | | 4.0 | Sheared, fine grained, quartz-feldspar porphyry. |
| KLP 254 | 4230 700 | C | | 4.5 | Sheared, fine grained, quartz-feldspar porphyry. 20-25% disseminated pyrite. |
| KLP 255 | 4255 700 | B | | 5.5 | |
| KLP 256 | 4280 700 | B | | 5.0 | |
| KLP 257 | 4305 700 | B | | 5.0 | |
| KLP 258 | 4200 2050 | C | | 4.5 | Chloritic quartz-feldspar porphyry. Trace pyrite. |
| KLP 259 | 4200 2000 | C | | 1.5 | Quartz-feldspar +/- augite porphyry. Chloritic, epidotized. <1% pyrite. |
| KLP 260 | 4200 1950 | C | | 4.0 | Chloritic quartz-feldspar porphyry. Trace pyrite. |
| KLP 261 | 4200 1900 | C | | 3.0 | As above. <1% pyrite. |
| KLP 262 | 4200 1850 | C | | 4.5 | Qtz-feldspar porphyry/silicified tuff. Chloritic, hematitic. 15-20% fine-medium grained, diss. py. |
| KLP 263 | 5600 2200 | B | | 6.5 | |
| KLP 264 | 5600 2250 | B | | 6.0 | |
| KLP 265 | 5600 2300 | C | | 3.0 | Quartz-feldspar-augite porphyry. Minor epidote. 2% pyrite. |
| KLP 266 | 5600 2390 | C | | 3.5 | Quartz-feldspar +/- augite porphyry. Diorite? Magnetic. |
| KLP 267 | 5600 2460 | C | | 2.5 | Quartz-feldspar porphyry +/- augite/hornblende. Minor epidote. Traces pyrite. |
| KLP 268 | 5600 2500 | C | | 4.5 | Quartz-feldspar-augite porphyry. Locally magnetic. 2% pyrite in fractures. |
| KLP 269 | 5600 2535 | C | | 0.5 | Quartz-feldspar porphyry +/- augite. Trace pyrite. |

KLIYUL PROPERTY - PIT & TRENCH SAMPLE DESCRIPTIONS
B = SOILS
C = ROCKS & CHIPS

| PIT #/ SAMPLE # | LOCATION EAST NORTH | TYPE | WIDTH (Metres) | DEPTH Metres) | DESCRIPTION |
|--------------------|------------------------|------|-------------------|------------------|--|
| KLP 270 | 5585 2610 | C | | 4.0 | Quartz-feldspar porphyry. Very dark green - black. Trace pyrite. |
| KLP 271 | 5600 2650 | C | | 5.5 | Qtz-feldspar porphyry +/- coarse augite phenocrysts. Dark green-black. <1% fine grained, diss. py. |
| KLP 272 | 5600 2700 | C | | 5.0 | Fine grained, quartz-feldspar-augite porphyry. Epidote surrounds phenocrysts. Magnetic. Tr py. |
| KLP 273 | 5645 2770 | B | | 6.0 | |
| KLP 274 | 5600 2800 | C | | 5.0 | Quartz-feldspar porphyry. Minor epidote; +/- coarse grained augite phenocrysts. Magnetic. Tr py. |
| KLP 275 | 5600 2850 | C | | 2.0 | Coarse grained porphyry. Chloritic. 2-5% pyrite. |
| KLP 276 | 5600 2900 | C | | 1.0 | C.g. porphyry. Moderate epidote rimming qtz-feldspar phenocrysts 5-10% f.g. diss. py. Float. |
| KLP 276 | 5600 2900 | C | | 7.0 | Fine grained quartz-feldspar porphyry +/- augite. Weakly magnetic. 1-2% fracture filled pyrite. |
| KLP 276 | 5600 2900 | C | | 7.0 | Diorite. Minor epidote associated with secondary quartz. Magnetic. Trace pyrite. |
| KLP 277 | 5600 2950 | C | | 6.0 | Volcanic tuff, weakly brecciated, quartz sweets +/- carbonate. Minor magnetite. <1% pyrite. |
| KLP 278 | 5600 3000 | C | | 3.5 | |
| KLP 279 | 5800 2600 | C | | 5.5 | |
| KLP 280 | 5800 2545 | C | | 3.5 | Diorite. Minor epidote associated with quartz. Magnetic. Trace pyrite. |
| KLP 281 | 5800 2500 | C | | 1.0 | Quartz (porphyry) diorite. Black-dark green. Magnetic, 1% pyrite. Quartz & epidote. |
| KLP 282 | 5820 2450 | C | | 1.5 | Quartz-feldspar porphyry. Quartz sweets & epidote. Magnetic. 1-2% disseminated pyrite. |
| KLP 283 | 6000 2645 | C | | 2.5 | Diorite. 5% coarse grained pyrite. |
| KLP 284 | 6000 2500 | C | | 4.5 | Diorite. Minor epidote/quartz sweets. Very magnetic. <1% pyrite. |
| KLP 285 | 6000 2460 | C | | 2.0 | Sheared diorite, chloritic. Trace pyrite. |
| KLP 286 | 6000 2400 | C | | 4.0 | ? |
| KLP 287 | 6000 2350 | C | | 2.5 | ? |
| KLP 288 | 6000 2300 | C | | 1.5 | ? |

| I.T. No. | SAMPLE No. | 3008-033 | | | | | | | | | | | | | | | | | | | | | | | | | | | | Pg. 2 of 2 |
|----------|--------------------------------|----------|------|----|------|-----|-----|------|-----|-----|-----|-----|------|------|------|----|-----|------|------|-----|------|-----|------|-----|-----|------|-----|------|-----|------------|
| | | As | Ag | Al | Ar | Ba | Be | Bi | Ca | Cd | Ce | Co | Cr | Cu | Fe | K | La | Li | Mg | Mn | Mo | Na | Ni | P | Pb | Sr | Ti | V | Zn | |
| | | ppb | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | ppm | % | ppm | % | ppm | ppm | % | ppm | ppm | |
| 282 | KLP 134 - 3.0 ^h x 5 | 0.2 | 4.72 | 2 | 585 | 0.3 | 5 | 0.81 | 0.2 | 28 | 15 | 9 | 49 | 5.56 | 1.09 | 9 | 17 | 1.99 | 726 | 1 | 0.12 | 4 | 0.10 | 2 | 137 | 0.20 | 129 | 89 | | |
| 283 | KLP140 382 - M1.0-60 | 0.2 | 5.57 | 2 | 628 | 0.3 | 5 | 2.13 | 0.2 | 49 | 13 | 10 | 213 | 5.27 | 1.40 | 11 | 14 | 1.77 | 596 | 2 | 0.09 | 8 | 0.10 | 8 | 176 | 0.25 | 145 | 250 | | |
| 284 | KLP140 382 - N1.0-190 | 0.4 | 6.30 | 2 | 1130 | 0.4 | 5 | 1.14 | 0.2 | 35 | 9 | 15 | 547 | 5.75 | 2.34 | 10 | 12 | 1.46 | 550 | 6 | 0.08 | 9 | 0.09 | 7 | 113 | 0.28 | 137 | 208 | | |
| 285 | KLP140 382 - O1.0-60 | 0.4 | 6.15 | 2 | 782 | 0.4 | 5 | 1.51 | 0.2 | 45 | 11 | 13 | 186 | 4.65 | 2.16 | 13 | 14 | 1.73 | 435 | 2 | 0.09 | 11 | 0.11 | 8 | 124 | 0.26 | 110 | 168 | | |
| 286 | KLP140 382 - P1.0-620 | 0.2 | 6.59 | 2 | 951 | 0.4 | 5 | 0.51 | 0.2 | 26 | 10 | 11 | 463 | 4.71 | 2.87 | 10 | 13 | 1.19 | 493 | 7 | 0.07 | 8 | 0.10 | 10 | 54 | 0.23 | 128 | 152 | | |
| 287 | KLP140 382 - Q1.0-100 | 0.2 | 5.45 | 2 | 924 | 0.3 | 5 | 1.46 | 0.2 | 45 | 9 | 22 | 263 | 4.37 | 2.00 | 11 | 14 | 1.39 | 362 | 4 | 0.10 | 12 | 0.09 | 27 | 114 | 0.22 | 110 | 179 | | |
| 288 | KLP141 382 - R1.0-60 | 0.2 | 5.17 | 2 | 693 | 0.3 | 5 | 0.20 | 0.3 | 20 | 12 | 24 | 119 | 5.41 | 1.85 | 9 | 21 | 2.24 | 337 | 5 | 0.07 | 16 | 0.09 | 109 | 14 | 0.14 | 148 | 366 | | |
| 289 | KLP141 382 - S1.0-180 | 4.0 | 5.52 | 2 | 322 | 0.7 | 5 | 0.55 | 1.6 | 23 | 24 | 293 | 215 | 5.81 | 1.74 | 9 | 23 | 2.79 | 343 | 5 | 0.04 | 105 | 0.11 | 253 | 27 | 0.07 | 220 | 650 | | |
| 290 | KLP141 382 - T1.0-130 | 1.2 | 4.43 | 4 | 254 | 0.9 | 5 | 1.91 | 5.9 | 43 | 47 | 304 | 1659 | 6.15 | 1.54 | 10 | 19 | 2.67 | 1323 | 6 | 0.04 | 121 | 0.14 | 179 | 23 | 0.05 | 181 | 1088 | | |
| 291 | KLP141 382 - U1.0-50 | 0.2 | 6.12 | 2 | 422 | 1.2 | 5 | 0.79 | 3.1 | 29 | 48 | 147 | 2443 | 6.26 | 2.31 | 9 | 20 | 2.29 | 614 | 6 | 0.05 | 93 | 0.13 | 116 | 19 | 0.08 | 200 | 1085 | | |
| 292 | KLP 142 - 5.5 80 | 0.2 | 4.47 | 2 | 610 | 0.2 | 5 | 1.04 | 0.2 | 36 | 13 | 13 | 450 | 9.86 | 1.54 | 8 | 18 | 1.63 | 835 | 2 | 0.09 | 4 | 0.09 | 2 | 81 | 0.32 | 183 | 300 | | |

K116

↓

K115

4

9

T. No. SAMPLE No. Au ppb Ag ppm Al % As ppm Ba ppm Be ppm Bi ppm Ca % Cd ppm Ce ppm Co ppm Cr ppm Cu ppm Fe % K % La ppm Li ppm Mg % Mn ppm Mo ppm Na % Ni ppm P % Pb ppm Sr ppm Ti % V ppm Zn ppm 9308-005 Pg. 4 of 7

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-----|--------|----------|-----|-----|------|----|-----|-----|---|------|-----|----|----|----|------|------|------|----|----|------|------|----|------|----|------|---|-----|------|-----|-----|
| 170 | KLP 37 | 2.0 SOIL | 140 | 0.6 | 4.73 | 9 | 437 | 0.3 | 5 | 1.80 | 0.2 | 48 | 28 | 23 | 758 | 7.47 | 0.81 | 14 | 17 | 1.45 | 869 | 4 | 0.10 | 19 | 0.14 | 9 | 141 | 0.28 | 173 | 130 |
| 171 | KLP 38 | 3.0 SOIL | 90 | 0.2 | 4.33 | 9 | 319 | 0.3 | 5 | 2.05 | 0.2 | 48 | 36 | 24 | 1003 | 6.53 | 0.70 | 14 | 14 | 1.28 | 982 | 4 | 0.09 | 19 | 0.10 | 8 | 140 | 0.22 | 160 | 154 |
| 172 | KLP 39 | 2.0 SOIL | 220 | 2.0 | 4.62 | 15 | 415 | 0.3 | 5 | 1.43 | 0.2 | 43 | 21 | 19 | 899 | 8.61 | 0.89 | 14 | 14 | 1.50 | 824 | 15 | 0.11 | 18 | 0.17 | 8 | 126 | 0.30 | 179 | 111 |
| 173 | KLP 40 | 3.4 SOIL | 180 | 1.2 | 4.65 | 10 | 317 | 0.3 | 5 | 1.21 | 0.2 | 49 | 42 | 13 | 1066 | 7.15 | 0.95 | 17 | 14 | 1.47 | 1027 | 17 | 0.08 | 14 | 0.15 | 5 | 106 | 0.23 | 157 | 74 |
| 174 | KLP 41 | 2.0 SOIL | 200 | 0.4 | 4.60 | 17 | 294 | 0.3 | 5 | 1.49 | 0.4 | 46 | 31 | 19 | 1112 | 7.82 | 0.68 | 14 | 14 | 1.37 | 917 | 3 | 0.12 | 20 | 0.14 | 2 | 112 | 0.19 | 168 | 99 |
| 175 | KLP 42 | 5.3 SOIL | 110 | 0.2 | 4.71 | 12 | 316 | 0.3 | 5 | 1.48 | 0.2 | 46 | 25 | 17 | 951 | 6.64 | 0.78 | 13 | 14 | 1.48 | 844 | 6 | 0.09 | 17 | 0.13 | 4 | 114 | 0.22 | 165 | 82 |
| 176 | KLP 43 | 2.0 SOIL | 40 | 0.2 | 4.82 | 9 | 255 | 0.3 | 5 | 1.85 | 0.2 | 49 | 19 | 20 | 436 | 5.49 | 0.56 | 13 | 14 | 1.41 | 961 | 1 | 0.10 | 20 | 0.12 | 2 | 121 | 0.24 | 165 | 85 |
| 177 | KLP 42 | 4.5 SOIL | 120 | 0.4 | 4.54 | 8 | 286 | 0.5 | 5 | 1.48 | 0.4 | 55 | 51 | 13 | 2699 | 5.73 | 0.80 | 17 | 15 | 1.38 | 2721 | 11 | 0.08 | 15 | 0.14 | 8 | 132 | 0.14 | 135 | 125 |
| 178 | KLP 43 | 2.0 SOIL | 350 | 0.6 | 4.31 | 8 | 371 | 0.4 | 5 | 1.36 | 0.4 | 48 | 32 | 21 | 1357 | 7.21 | 0.81 | 15 | 15 | 1.38 | 1697 | 11 | 0.11 | 20 | 0.11 | 4 | 94 | 0.17 | 146 | 198 |

KLP 17

| T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Bc ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm | 3000-000 ppm |
|--------|--------------------|--------|--------|------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|--------------|
| 3 | KLP 139 - 3.0 SOIL | 90 | 0.2 | 4.73 | 2 | 553 | 0.3 | 5 | 1.81 | 0.2 | 47 | 12 | 30 | 173 | 5.37 | 0.72 | 14 | 12 | 1.64 | 739 | 2 | 0.06 | 18 | 0.11 | 23 | 171 | 0.24 | 161 | 111 | K116 |
| 4 | 142 - 2.5 SOIL | 95 | 0.2 | 4.97 | 10 | 382 | 0.3 | 5 | 1.70 | 0.2 | 47 | 15 | 29 | 442 | 6.32 | 0.76 | 14 | 12 | 1.31 | 788 | 3 | 0.11 | 15 | 0.14 | 5 | 129 | 0.23 | 166 | 103 | K115 |
| 5 | 143 - 4.5 SOIL | 100 | 0.2 | 4.64 | 7 | 298 | 0.3 | 5 | 2.23 | 0.3 | 50 | 39 | 35 | 1864 | 6.50 | 0.58 | 13 | 14 | 1.53 | 1109 | 3 | 0.10 | 21 | 0.12 | 3 | 143 | 0.28 | 180 | 378 | K115 |
| 6 | 148 - 5.0 SOIL | 40 | 0.2 | 4.67 | 8 | 266 | 0.3 | 5 | 2.19 | 0.2 | 50 | 26 | 36 | 225 | 5.92 | 0.47 | 13 | 17 | 1.69 | 1360 | 2 | 0.17 | 27 | 0.09 | 2 | 135 | 0.24 | 183 | 94 | K115 |
| 7 | KLP 149 - 3.0 SOIL | 700 | 0.2 | 5.46 | 4 | 301 | 0.4 | 5 | 1.76 | 0.2 | 56 | 36 | 15 | 2059 | 7.96 | 0.85 | 17 | 15 | 1.72 | 990 | 5 | 0.10 | 21 | 0.16 | 2 | 158 | 0.21 | 187 | 108 | K115 |
| 8 | KLP 150 - 2.0 SOIL | 400 | 0.2 | 5.32 | 5 | 312 | 0.4 | 5 | 2.03 | 0.2 | 51 | 24 | 19 | 563 | 6.46 | 0.62 | 14 | 14 | 1.54 | 878 | 4 | 0.11 | 18 | 0.13 | 2 | 146 | 0.24 | 176 | 102 | K115 |
| 9 | 150 - 4.0 SOIL | 190 | 0.2 | 5.75 | 9 | 279 | 0.5 | 5 | 1.69 | 0.2 | 51 | 57 | 16 | 1022 | 7.40 | 0.76 | 14 | 14 | 1.39 | 1204 | 7 | 0.17 | 17 | 0.14 | 2 | 129 | 0.17 | 172 | 108 | K115 |
| 0 | 151 - 3.5 SOIL | 230 | 0.2 | 5.02 | 6 | 263 | 0.3 | 5 | 2.37 | 0.3 | 52 | 55 | 36 | 373 | 6.45 | 0.55 | 14 | 14 | 1.45 | 1446 | 4 | 0.11 | 21 | 0.12 | 2 | 150 | 0.25 | 177 | 164 | K115 |
| 1 | 152 - 2.5 SOIL | 120 | 0.6 | 4.79 | 8 | 307 | 0.3 | 5 | 1.33 | 0.2 | 44 | 18 | 26 | 2393 | 7.83 | 0.81 | 14 | 12 | 1.37 | 905 | 5 | 0.14 | 17 | 0.14 | 7 | 134 | 0.32 | 170 | 110 | K115 |
| 2 | KLP 153 - 2.0 SOIL | 45 | 0.2 | 4.93 | 6 | 388 | 0.3 | 5 | 1.35 | 0.2 | 46 | 7 | 19 | 148 | 6.82 | 1.19 | 14 | 10 | 1.19 | 531 | 5 | 0.11 | 14 | 0.12 | 5 | 165 | 0.28 | 171 | 77 | K115 |
| 3 | KLP 153 - 3.5 SOIL | 110 | 0.2 | 4.92 | 11 | 375 | 0.3 | 5 | 1.91 | 0.2 | 51 | 11 | 26 | 478 | 6.57 | 0.77 | 15 | 12 | 1.40 | 727 | 2 | 0.10 | 17 | 0.12 | 6 | 155 | 0.26 | 171 | 104 | K116 |
| 4 | 157 - 3.0 SOIL | 40 | 0.2 | 5.60 | 2 | 494 | 0.4 | 5 | 1.81 | 0.2 | 50 | 22 | 29 | 137 | 5.56 | 0.79 | 14 | 16 | 1.62 | 1184 | 2 | 0.11 | 22 | 0.12 | 7 | 158 | 0.24 | 162 | 98 | K116 |
| 5 | 158 - 2.5 SOIL | 60 | 0.2 | 5.50 | 3 | 487 | 0.4 | 5 | 1.83 | 0.2 | 50 | 20 | 27 | 157 | 5.72 | 0.79 | 14 | 16 | 1.80 | 1102 | 2 | 0.11 | 22 | 0.12 | 7 | 162 | 0.25 | 162 | 101 | K116 |
| 6 | 159 SOIL | 65 | 0.2 | 5.31 | 11 | 355 | 0.4 | 5 | 2.47 | 0.2 | 52 | 34 | 29 | 201 | 6.33 | 0.70 | 14 | 16 | 1.68 | 1457 | 3 | 0.11 | 31 | 0.12 | 2 | 169 | 0.27 | 170 | 114 | K116 |
| 7 | KLP 160 - 6.0 SOIL | 30 | 0.2 | 5.80 | 13 | 461 | 0.4 | 5 | 1.72 | 0.2 | 54 | 37 | 29 | 201 | 5.90 | 0.64 | 17 | 18 | 2.11 | 1517 | 2 | 0.08 | 23 | 0.12 | 9 | 176 | 0.25 | 158 | 111 | K116 |
| 8 | KLP 161 - 4.0 SOIL | 40 | 0.2 | 6.55 | 2 | 618 | 0.4 | 5 | 1.64 | 0.2 | 49 | 32 | 27 | 147 | 5.80 | 0.95 | 14 | 18 | 1.69 | 1236 | 1 | 0.16 | 25 | 0.14 | 5 | 186 | 0.22 | 160 | 23 | K115 |
| 9 | 162 - 2.0 SOIL | 35 | 0.2 | 6.62 | 3 | 729 | 0.4 | 5 | 1.31 | 0.2 | 44 | 19 | 21 | 137 | 5.57 | 1.03 | 13 | 19 | 1.48 | 877 | 1 | 0.20 | 19 | 0.15 | 7 | 166 | 0.21 | 155 | 76 | K115 |
| 0 | 163 - 4.0 SOIL | 35 | 0.2 | 6.11 | 3 | 598 | 0.4 | 5 | 1.72 | 0.2 | 50 | 26 | 43 | 158 | 5.75 | 0.88 | 14 | 18 | 1.74 | 1133 | 1 | 0.12 | 29 | 0.14 | 2 | 167 | 0.23 | 153 | 90 | K115 |
| 1 | 164 - 3.0 SOIL | 30 | 0.2 | 5.61 | 2 | 556 | 0.4 | 5 | 1.88 | 0.2 | 48 | 27 | 40 | 135 | 5.58 | 0.89 | 13 | 16 | 1.70 | 1028 | 1 | 0.10 | 31 | 0.14 | 2 | 164 | 0.26 | 161 | 84 | K115 |
| 2 | KLP 167 - 1.0 SOIL | 95 | 0.2 | 4.83 | 13 | 439 | 0.4 | 5 | 2.35 | 0.7 | 54 | 23 | 88 | 165 | 5.58 | 0.79 | 16 | 17 | 2.02 | 1556 | 2 | 0.08 | 55 | 0.19 | 11 | 187 | 0.31 | 194 | 171 | K113 |
| 3 | KLP 211 - 2.5 SOIL | 170 | 0.2 | 7.05 | 2 | 576 | 0.6 | 5 | 0.34 | 0.2 | 36 | 35 | 7 | 1162 | 5.90 | 1.51 | 22 | 16 | 1.29 | 1707 | 29 | 0.37 | 13 | 0.15 | 2 | 83 | 0.07 | 140 | 119 | K114 |
| 4 | KLP 215 - 2.0 SOIL | 30 | 0.2 | 5.38 | 7 | 340 | 0.4 | 5 | 2.04 | 0.2 | 48 | 28 | 22 | 187 | 6.41 | 0.55 | 13 | 14 | 1.60 | 1270 | 3 | 0.08 | 34 | 0.12 | 2 | 152 | 0.29 | 167 | 140 | K114 |

| T.T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Be ppm | Bi ppm | Cu % | Cl ppm | Cr ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm | 3308-008 Pg. 6 of 8 |
|----------|----------------|--------|--------|------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|---------------------|
| 190 | KLP 228-7.0 Rx | 5 | 0.2 | 4.00 | 2 | 818 | 0.6 | 5 | 2.26 | 0.3 | 80 | 8 | 24 | 36 | 4.27 | 1.02 | 20 | 10 | 1.00 | 1023 | 1 | 0.08 | 7 | 0.15 | 3 | 547 | 0.32 | 111 | 88 | KL-17 |
| 191 | 229-5.0 Rx | 5 | 0.8 | 4.75 | 7 | 502 | 0.4 | 5 | 2.12 | 0.8 | 66 | 12 | 23 | 101 | 3.62 | 1.14 | 18 | 14 | 1.25 | 809 | 1 | 0.11 | 8 | 0.10 | 2 | 128 | 0.26 | 112 | 72 | |
| 192 | KLP 230-5.0 Rx | 50 | 0.2 | 5.51 | 5 | 235 | 0.3 | 5 | 1.47 | 0.2 | 54 | 21 | 10 | 296 | 6.41 | 0.94 | 14 | 25 | 1.60 | 1016 | 1 | 0.10 | 6 | 0.09 | 2 | 108 | 0.11 | 182 | 97 | ↓ |

NORANDA DELTA LABORATORY

Geochemical Analysis

Project Name & No.: KLIYUL - 148
 Material: 14 Soils & 60 Rx
 Remarks: * Sample screened @ -35 MESH (0.5 mm)
 † Organic, ‡ Humus, § Sulfide

Geol.: JNSB
 Sheet: 1 of 1

Date received: SEP. 07
 Date completed: SEP. 16

LAB CODE: 9309-009

Au - 10.0 g sample digested with aqua-regia and determined by A.A. (D.L. 5 PPB)
 ICP - 0.2 g sample digested with 3 ml HClO₄/HNO₃ (4:1) at 203 °C for 4 hours diluted to 10 ml with water. Leeman PS3000 ICP determined elemental contents.
 N.B. The major oxide elements and Ba, Be, Ce, La, Li, Ga are rarely dissolved completely from geological materials with this acid dissolution method.

| T.T. No. | SAMPLE No. | Au ppb | Ag ppm | Al % | As ppm | Ba ppm | Be ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Nb % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm |
|----------|-----------------------|--------|--------|------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|-------|------|--------|--------|------|--------|--------|------|--------|------|--------|--------|------|-------|--------|
| 3 | Soils KLP 233 - 5.5 B | 80 | 0.2 | 4.75 | 9 | 444 | 0.4 | 5 | 1.11 | 0.2 | 41 | 166 | 24 | 151 | 14.00 | 0.77 | 14 | 18 | 1.08 | 2644 | 1 | 0.10 | 27 | 0.24 | 4 | 128 | 0.16 | 120 | 201 |
| 4 | 247 - 2.5 B | 75 | 0.2 | 6.45 | 14 | 516 | 0.4 | 5 | 1.16 | 0.2 | 42 | 26 | 19 | 203 | 7.92 | 0.94 | 13 | 17 | 1.62 | 1036 | 2 | 0.16 | 15 | 0.19 | 3 | 122 | 0.27 | 162 | 105 |
| 5 | 247 - 6.0 A | 80 | 0.4 | 6.01 | 12 | 621 | 0.4 | 5 | 2.92 | 0.4 | 47 | 25 | 11 | 199 | 4.72 | 1.22 | 13 | 20 | 1.81 | 1072 | 2 | 0.23 | 16 | 0.08 | 12 | 134 | 0.12 | 132 | 128 |
| 6 | 248 - 4.5 B | 70 | 0.2 | 6.05 | 17 | 537 | 0.4 | 5 | 1.28 | 0.2 | 44 | 10 | 22 | 95 | 7.60 | 1.07 | 12 | 15 | 1.77 | 727 | 2 | 0.14 | 16 | 0.16 | 9 | 126 | 0.30 | 185 | 95 |
| 7 | KLP 248 - 6.5 A | 65 | 0.2 | 6.25 | 12 | 638 | 0.5 | 5 | 1.49 | 0.2 | 50 | 30 | 13 | 220 | 4.51 | 1.14 | 14 | 19 | 1.82 | 650 | 2 | 0.21 | 22 | 0.09 | 6 | 129 | 0.14 | 123 | 128 |
| 8 | KLP 251 - 3.0 B | 120 | 0.2 | 7.18 | 17 | 765 | 0.6 | 5 | 0.13 | 0.2 | 30 | 26 | 6 | 250 | 9.46 | 1.93 | 16 | 13 | 0.99 | 1278 | 3 | 0.17 | 10 | 0.23 | 11 | 73 | 0.09 | 141 | 380 |
| 9 | 252 - 5.5 B | 190 | 0.4 | 7.41 | 20 | 890 | 0.6 | 5 | 0.14 | 0.5 | 32 | 28 | 10 | 226 | 9.66 | 2.00 | 17 | 15 | 1.16 | 1391 | 3 | 0.20 | 15 | 0.25 | 21 | 77 | 0.12 | 149 | 303 |
| 10 | 255 - 5.5 B | 50 | 0.2 | 7.15 | 16 | 639 | 0.4 | 5 | 0.27 | 0.2 | 24 | 5 | 11 | 183 | 11.42 | 2.01 | 11 | 11 | 1.41 | 513 | 4 | 0.23 | 8 | 0.15 | 5 | 73 | 0.17 | 199 | 125 |
| 11 | 256 - 5.0 B | 150 | 0.4 | 6.87 | 28 | 493 | 0.4 | 5 | 0.45 | 0.8 | 31 | 12 | 12 | 123 | 8.81 | 1.42 | 12 | 12 | 1.03 | 600 | 7 | 0.22 | 11 | 0.26 | 14 | 87 | 0.18 | 179 | 123 |
| 12 | KLP 257 - 5.0 B | 100 | 0.2 | 6.99 | 28 | 654 | 0.4 | 5 | 0.28 | 0.3 | 29 | 6 | 8 | 84 | 8.10 | 1.78 | 12 | 11 | 1.09 | 420 | 5 | 0.27 | 9 | 0.22 | 12 | 89 | 0.13 | 180 | 111 |
| 13 | 263 - 6.5 A | 35 | 0.2 | 4.18 | 24 | 220 | 0.3 | 5 | 4.06 | 0.5 | 52 | 20 | 24 | 169 | 4.86 | 0.42 | 14 | 13 | 1.70 | 934 | 1 | 0.11 | 26 | 0.10 | 8 | 222 | 0.32 | 177 | 83 |
| 14 | 264 - 5.0 | 20 | 0.2 | 5.26 | 23 | 288 | 0.3 | 5 | 3.64 | 0.8 | 51 | 27 | 15 | 256 | 5.49 | 0.52 | 12 | 15 | 2.05 | 951 | 1 | 0.13 | 27 | 0.11 | 9 | 325 | 0.36 | 195 | 103 |
| 15 | 273 - 6.0 | 15 | 0.2 | 4.41 | 21 | 284 | 0.4 | 5 | 2.64 | 0.7 | 56 | 26 | 20 | 173 | 6.04 | 0.69 | 15 | 17 | 2.75 | 994 | 1 | 0.06 | 27 | 0.13 | 6 | 198 | 0.44 | 259 | 67 |
| 16 | KLP 278 - 3.5 | 60 | 0.2 | 5.12 | 25 | 326 | 0.4 | 5 | 2.41 | 0.9 | 53 | 41 | 23 | 368 | 6.24 | 0.55 | 13 | 15 | 2.20 | 1272 | 1 | 0.10 | 32 | 0.12 | 9 | 189 | 0.33 | 201 | 98 |

KLI 26
 207
 207
 207
 207
 DAR B
 KLI 26
 KLI 26
 KLI
 KLI
 KLI
 KLI
 KLI
 KLI

279 - missing.

21/09 Yavic off

| T. | SAMPLE No. | As ppb | Ag ppm | Al % | Ar ppm | Ba ppm | Bc ppm | Bi ppm | Ca % | Cd ppm | Ce ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | La ppm | Li ppm | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Sr ppm | Ti % | V ppm | Zn ppm | 6008-000 Pg. 2 of 2 |
|----|---------------|-----------|-----------|---------|-----------|-----------|-----------|-----------|---------|-----------|-----------|-----------|-----------|-----------|---------|--------|-----------|-----------|---------|-----------|-----------|---------|-----------|--------|-----------|-----------|---------|----------|-----------|------------------------|
| | 276-7.0 B | 5 | 0.4 | 3.67 | 7 | 692 | 0.3 | 5 | 2.49 | 0.2 | 72 | 11 | 33 | 33 | 3.41 | 1.18 | 16 | 8 | 1.18 | 619 | 2 | 0.10 | 12 | 0.09 | 2 | 293 | 0.23 | 129 | 35 | KCl |
| | 277-6.0 " | 5 | 0.2 | 4.02 | 17 | 206 | 0.4 | 5 | 7.89 | 0.2 | 89 | 18 | 17 | 20 | 5.30 | 0.88 | 16 | 19 | 2.24 | 2057 | 1 | 0.07 | 14 | 0.08 | 2 | 104 | 0.28 | 208 | 68 | " |
| | 279-5.5 R | 20 | 0.2 | 4.44 | 4 | 448 | 0.3 | 5 | 3.07 | 0.3 | 68 | 18 | 32 | 96 | 5.13 | 0.73 | 15 | 14 | 1.73 | 998 | 1 | 0.14 | 20 | 0.09 | 6 | 158 | 0.30 | 171 | 80 | " |
| | 280-3.5 " | 5 | 0.2 | 4.68 | 4 | 420 | 0.3 | 5 | 3.70 | 0.2 | 73 | 14 | 20 | 19 | 4.63 | 0.91 | 14 | 10 | 1.23 | 873 | 1 | 0.11 | 12 | 0.12 | 2 | 350 | 0.32 | 164 | 38 | " |
| | 281-1.0 " | 5 | 0.2 | 3.85 | 2 | 248 | 0.3 | 5 | 4.02 | 0.2 | 67 | 20 | 66 | 88 | 5.30 | 0.52 | 11 | 8 | 2.02 | 723 | 1 | 0.22 | 27 | 0.09 | 2 | 170 | 0.36 | 202 | 38 | ↓ |
| | 282-1.5 " | 5 | 0.2 | 4.10 | 4 | 236 | 0.3 | 5 | 3.97 | 0.2 | 73 | 16 | 39 | 42 | 4.83 | 0.53 | 13 | 9 | 1.87 | 676 | 1 | 0.18 | 20 | 0.09 | 3 | 220 | 0.39 | 195 | 31 | KCl |
| | 283-2.5 " | 5 | 0.2 | 3.30 | 7 | 1040 | 0.4 | 5 | 3.81 | 0.2 | 75 | 10 | 15 | 8 | 3.33 | 1.79 | 15 | 11 | 0.94 | 981 | 1 | 0.12 | 11 | 0.13 | 4 | 42 | 0.20 | 178 | 31 | " |
| | 284-4.5 " | 5 | 0.2 | 4.83 | 2 | 683 | 0.3 | 5 | 1.66 | 0.3 | 63 | 11 | 13 | 12 | 4.36 | 1.68 | 15 | 11 | 1.40 | 705 | 1 | 0.09 | 9 | 0.12 | 3 | 153 | 0.31 | 165 | 43 | " |
| | 285-2.0 " | 5 | 0.2 | 3.36 | 13 | 189 | 0.5 | 5 | 2.20 | 0.6 | 83 | 18 | 60 | 47 | 4.94 | 0.33 | 22 | 14 | 2.48 | 947 | 1 | 0.10 | 60 | 0.14 | 6 | 385 | 0.37 | 155 | 77 | " |
| | 286-4.0 " | 5 | 0.2 | 3.37 | 9 | 305 | 0.3 | 5 | 3.18 | 0.2 | 73 | 17 | 53 | 38 | 4.62 | 0.83 | 14 | 9 | 1.77 | 633 | 1 | 0.15 | 27 | 0.09 | 3 | 227 | 0.34 | 167 | 36 | " |
| | 287-2.5 " | 5 | 0.2 | 4.15 | 14 | 290 | 0.3 | 5 | 4.14 | 0.6 | 76 | 15 | 42 | 18 | 4.77 | 0.52 | 13 | 9 | 1.59 | 707 | 1 | 0.14 | 18 | 0.09 | 5 | 265 | 0.37 | 210 | 38 | KCl |
| | KLP 288-1.5 " | 5 | 0.2 | 4.21 | 8 | 189 | 0.3 | 5 | 4.33 | 0.2 | 71 | 23 | 64 | 102 | 5.54 | 0.47 | 14 | 10 | 2.15 | 874 | 1 | 0.19 | 28 | 0.09 | 2 | 185 | 0.42 | 216 | 48 | ↓ |
| | KLM 239-5.5 " | 5 | 0.2 | 4.93 | 2 | 1080 | 0.5 | 5 | 2.56 | 0.2 | 79 | 9 | 16 | 41 | 4.25 | 1.09 | 20 | 11 | 1.13 | 880 | 1 | 0.11 | 6 | 0.12 | 2 | 213 | 0.28 | 111 | 92 | KCl, 26 |
| | 240-4.3 " | 5 | 0.2 | 5.58 | 2 | 508 | 0.4 | 5 | 0.23 | 0.2 | 32 | 2 | 15 | 110 | 4.90 | 1.35 | 12 | 14 | 1.53 | 294 | 1 | 0.32 | 4 | 0.09 | 2 | 89 | 0.07 | 114 | 54 | 307 |
| | 240-4.0 " | 5 | 0.2 | 4.18 | 9 | 399 | 0.3 | 5 | 3.05 | 0.3 | 68 | 10 | 26 | 19 | 3.06 | 0.47 | 11 | 8 | 1.16 | 1413 | 1 | 0.11 | 10 | 0.07 | 2 | 180 | 0.20 | 105 | 181 | " |
| | 241 | 5 | 0.2 | 4.31 | 3 | 1720 | 0.7 | 5 | 2.04 | 0.4 | 82 | 12 | 30 | 288 | 4.09 | 1.01 | 22 | 9 | 1.64 | 727 | 1 | 0.09 | 9 | 0.11 | 4 | 341 | 0.46 | 124 | 86 | 307 |
| | KLM 242-1.0 | 450 | 0.2 | 5.95 | 10 | 773 | 0.3 | 5 | 3.24 | 0.2 | 68 | 8 | 14 | 192 | 6.37 | 1.05 | 13 | 10 | 1.80 | 1085 | 2 | 0.09 | 6 | 0.09 | 3 | 156 | 0.33 | 169 | 91 | 307 |

| F. SAMPLE | | As | Ag | Al | Ar | Ba | Bc | Bl | Ca | Cd | Ce | Co | Cr | Cu | Fe | K | La | Li | Mg | Mn | Mo | Na | Ni | P | Pb | Sr | Ti | V | Zn | 8308-008 | |
|-----------|----|------|------|-----|------|-----|-----|-----|----|------|-----|-----|-----|-----|------|------|------|-----|----|------|------|----|------|----|------|-----|-----|------|-----|----------|--------|
| No. | | ppb | ppm | % | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | ppm | % | ppm | % | ppm | ppm | % | ppm | ppm | ppm | ppm |
| KLP | 22 | -5.2 | 55 | 0.2 | 4.13 | 7 | 263 | 0.3 | 5 | 3.05 | 0.2 | 23 | 23 | 29 | 132 | 4.78 | 0.48 | 10 | 16 | 1.54 | 857 | 1 | 0.10 | 24 | 0.08 | 2 | 149 | 0.24 | 172 | 90 | cli 15 |
| soil | 23 | -2.0 | 15 | 0.2 | 4.34 | 5 | 257 | 0.3 | 5 | 2.21 | 0.2 | 28 | 22 | 29 | 143 | 4.85 | 0.44 | 10 | 16 | 1.68 | 964 | 1 | 0.10 | 24 | 0.09 | 2 | 127 | 0.26 | 174 | 82 | |
| | 23 | -5.5 | 310 | 0.2 | 4.82 | 2 | 476 | 0.5 | 5 | 1.29 | 1.0 | 34 | 34 | 18 | 808 | 6.06 | 0.99 | 12 | 15 | 1.32 | 2087 | 5 | 0.13 | 22 | 0.12 | 2 | 97 | 0.14 | 143 | 237 | |
| | 26 | -2.0 | 260 | 1.6 | 4.26 | 11 | 217 | 0.4 | 5 | 1.80 | 0.2 | 35 | 46 | 23 | 6611 | 6.44 | 0.56 | 14 | 15 | 1.39 | 1055 | 6 | 0.07 | 17 | 0.11 | 5 | 130 | 0.20 | 156 | 96 | |
| | 27 | -2.0 | 100 | 0.8 | 4.61 | 5 | 387 | 0.3 | 5 | 1.50 | 0.2 | 32 | 19 | 19 | 421 | 6.23 | 0.78 | 11 | 16 | 1.53 | 661 | 6 | 0.08 | 16 | 0.12 | 7 | 126 | 0.25 | 159 | 212 | |
| | 27 | -3.0 | 160 | 0.2 | 4.38 | 7 | 336 | 0.3 | 5 | 1.51 | 0.2 | 31 | 25 | 21 | 698 | 6.14 | 0.70 | 11 | 15 | 1.41 | 633 | 5 | 0.09 | 15 | 0.11 | 4 | 119 | 0.22 | 154 | 210 | |
| | 28 | -2.0 | 80 | 0.6 | 4.29 | 3 | 307 | 0.3 | 5 | 1.93 | 0.2 | 31 | 21 | 23 | 587 | 5.58 | 0.66 | 11 | 12 | 1.31 | 723 | 3 | 0.08 | 15 | 0.12 | 2 | 134 | 0.22 | 160 | 113 | |
| | 28 | -5.5 | 120 | 0.8 | 4.51 | 11 | 360 | 0.3 | 5 | 1.56 | 0.7 | 32 | 37 | 18 | 2025 | 6.83 | 0.84 | 12 | 14 | 1.33 | 982 | 5 | 0.09 | 19 | 0.12 | 6 | 114 | 0.20 | 156 | 208 | |
| | 29 | -2.0 | 1630 | 0.6 | 4.68 | 3 | 336 | 0.3 | 5 | 1.80 | 0.2 | 31 | 22 | 26 | 670 | 5.53 | 0.61 | 11 | 14 | 1.44 | 895 | 3 | 0.09 | 17 | 0.11 | 5 | 135 | 0.23 | 157 | 124 | cli 6 |
| | 29 | -6.0 | 85 | 0.2 | 4.64 | 2 | 350 | 0.3 | 5 | 1.95 | 0.2 | 30 | 23 | 20 | 459 | 5.51 | 0.69 | 11 | 13 | 1.41 | 792 | 3 | 0.09 | 15 | 0.10 | 10 | 148 | 0.24 | 162 | 134 | |
| | 30 | -3.0 | 200 | 0.8 | 4.39 | 9 | 383 | 0.3 | 5 | 1.88 | 0.2 | 29 | 18 | 23 | 391 | 6.78 | 0.71 | 12 | 14 | 1.45 | 736 | 3 | 0.10 | 16 | 0.12 | 8 | 154 | 0.27 | 176 | 154 | |
| | 32 | -2.0 | 100 | 0.2 | 4.54 | 2 | 359 | 0.3 | 5 | 2.16 | 0.2 | 35 | 20 | 27 | 461 | 5.57 | 0.65 | 13 | 13 | 1.31 | 766 | 3 | 0.08 | 17 | 0.11 | 6 | 171 | 0.24 | 166 | 104 | |
| | 32 | -3.8 | 100 | 0.6 | 4.54 | 2 | 489 | 0.3 | 5 | 2.00 | 0.2 | 33 | 19 | 28 | 473 | 6.59 | 0.77 | 13 | 13 | 1.35 | 832 | 5 | 0.08 | 15 | 0.14 | 13 | 187 | 0.25 | 163 | 113 | |
| | 33 | -2.0 | 85 | 0.4 | 4.66 | 2 | 435 | 0.3 | 5 | 2.15 | 0.2 | 33 | 13 | 33 | 290 | 5.26 | 0.75 | 13 | 13 | 1.76 | 643 | 3 | 0.07 | 20 | 0.10 | 48 | 218 | 0.26 | 176 | 170 | |
| | 33 | -3.5 | 65 | 0.8 | 6.02 | 2 | 892 | 0.4 | 5 | 1.36 | 0.2 | 32 | 16 | 17 | 347 | 5.01 | 1.72 | 12 | 14 | 1.52 | 484 | 5 | 0.09 | 14 | 0.09 | 92 | 146 | 0.36 | 166 | 145 | |
| | 34 | -2.0 | 70 | 0.4 | 4.78 | 2 | 335 | 0.4 | 5 | 2.25 | 0.2 | 30 | 28 | 32 | 543 | 6.30 | 0.63 | 12 | 16 | 2.03 | 893 | 3 | 0.07 | 24 | 0.13 | 6 | 165 | 0.30 | 196 | 165 | |
| | 34 | -5.2 | 130 | 0.6 | 4.97 | 2 | 275 | 0.4 | 5 | 2.85 | 0.2 | 29 | 27 | 37 | 540 | 5.85 | 0.61 | 12 | 17 | 2.46 | 1098 | 3 | 0.07 | 33 | 0.16 | 5 | 207 | 0.33 | 214 | 208 | |
| | 35 | -2.0 | 65 | 1.0 | 5.11 | 2 | 646 | 0.3 | 5 | 1.41 | 0.2 | 32 | 6 | 11 | 104 | 7.03 | 1.26 | 13 | 16 | 1.62 | 620 | 15 | 0.18 | 6 | 0.15 | 58 | 263 | 0.32 | 164 | 132 | cli 8 |
| KLP | 36 | -2.0 | 85 | 0.6 | 4.66 | 2 | 370 | 0.3 | 5 | 2.10 | 0.2 | 30 | 21 | 28 | 274 | 5.59 | 0.64 | 11 | 13 | 1.41 | 779 | 3 | 0.09 | 16 | 0.10 | 10 | 159 | 0.24 | 165 | 104 | |

APPENDIX V

COMBINED HELICOPTER-BORNE
MAGNETIC, ELECTROMAGNETIC, RADIOMETRIC
AND VLF-EM SURVEY REPORT

**REPORT ON A
COMBINED HELICOPTER-BORNE
MAGNETIC, ELECTROMAGNETIC
RADIOMETRIC AND VLF-EM SURVEY
OMENICA AREA
PROVINCE OF BRITISH COLUMBIA
NTS 94 D/8,9**

FOR

**NORANDA EXPLORATION COMPANY, LIMITED
SUITE 100, 1285 WEST PENDER STREET
VANCOUVER, BRITISH COLUMBIA
V6E 4B1**

BY

**GEONEX AERODAT INC.
3883 NASHUA DRIVE
MISSISSAUGA, ONTARIO
L4V 1R3
PHONE: 416 - 671-2446**

September 24, 1993



**R. W. Woolham, P. Eng.
Consulting Geophysicist**

J9358

TABLE OF CONTENTS

| | |
|--|---------------------------------------|
| 1. INTRODUCTION | 1 |
| 2. SURVEY AREA | 1 |
| 3. SURVEY PROCEDURES | 2 |
| 4. DELIVERABLES | 2 |
| 5. AIRCRAFT AND EQUIPMENT | 4 |
| 5.1 Aircraft | 4 |
| 5.2 Electromagnetic System | 4 |
| 5.3 VLF-EM System | 4 |
| 5.4 Magnetometer | 5 |
| 5.5 Gamma-Ray Spectrometer | 5 |
| 5.6 Ancillary Systems | 6 |
| 6. DATA PROCESSING AND PRESENTATION | 8 |
| 6.1 Base Map | 8 |
| 6.2 Flight Path Map | 9 |
| 6.3 Electromagnetic Survey Data | 10 |
| 6.4 Total Field Magnetics | 10 |
| 6.5 Vertical Magnetic Gradient | 11 |
| 6.6 Weight Percent Magnetite | 11 |
| 6.7 Apparent Resistivity | 11 |
| 6.8 VLF-EM | 11 |
| 6.9 Radiometric Data | 12 |
| 7. INTERPRETATION | 12 |
| 7.1 Area Geology | 12 |
| 7.2 Magnetic Interpretation | 13 |
| 7.3 Magnetic Survey Results and Conclusions | 13 |
| 7.4 Electromagnetic Anomaly Selection/Interpretation | 14 |
| 7.5 VLF Electromagnetic Survey | 15 |
| 7.6 Electromagnetic Survey Results and Conclusions | 15 |
| 7.7 Radiometric Interpretation | 17 |
| 7.8 Radiometric Survey Results and Conclusions | 18 |
| 8. RECOMMENDATIONS | 19 |
| | |
| APPENDIX I | - General Interpretive Considerations |
| APPENDIX II | - Anomaly Listings |
| APPENDIX III | - Certificate of Qualifications |
| APPENDIX IV | - Personnel |

LIST OF MAPS

The survey area is presented in a two sets of numbered maps, South Sheet; J9358-1 and North Sheet; J9358-2, in the following format:

BLACK LINE MAPS: (Scale 1:20,000)

| Map No. | Description |
|---------|---|
| 1. | BASE MAP; screened topographic base map plus survey area boundary, and UTM grid. |
| 2. | FLIGHT PATH MAP; photo-combination of the base map with flight lines, fiducials and EM anomaly symbols. |
| 3. | COMPILATION / INTERPRETATION MAP; with base map, flight path map and EM anomaly symbols with interpretation . |
| 4. | TOTAL FIELD MAGNETIC CONTOURS; with base map and flight lines. |
| 5. | VERTICAL MAGNETIC GRADIENT CONTOURS; with base map and flight lines. |
| 6. | WEIGHT PERCENT MAGNETITE; with base map and flight lines. |
| 7A. | APPARENT RESISTIVITY CONTOURS; apparent resistivity calculated for the coplanar 850 Hz data, with base map and flight lines. |
| 7B. | APPARENT RESISTIVITY CONTOURS; apparent resistivity calculated for the coaxial 935 Hz data, with base map and flight lines. |
| 7C. | APPARENT RESISTIVITY CONTOURS; apparent resistivity calculated for the coplanar 4,175 Hz data, with base map and flight lines. |
| 7D. | APPARENT RESISTIVITY CONTOURS; apparent resistivity calculated for the coaxial 4,600 Hz data, with base map and flight lines. |
| 7E. | APPARENT RESISTIVITY CONTOURS; apparent resistivity calculated for the coplanar 33,000 Hz data, with base map and flight lines. |
| 8. | VLF-EM TOTAL FIELD CONTOURS; with base map and flight lines. |

COLOUR MAPS: (Scale 1:20,000)

MAGNETIC

1. TOTAL FIELD MAGNETICS; with superimposed contours, flight lines and EM anomaly symbols.
2. VERTICAL MAGNETIC GRADIENT; with superimposed contours, flight lines and EM anomaly symbols.
3. WEIGHT PERCENT MAGNETITE; with base map and flight lines.

RESISTIVITY

- 4A. APPARENT RESISTIVITY; calculated for the coplanar 850 Hz data with superimposed contours, flight lines and EM anomaly symbols.
- 4B. APPARENT RESISTIVITY; calculated for the coaxial 935 Hz data with superimposed contours, flight lines and EM anomaly symbols.
- 4C. APPARENT RESISTIVITY; calculated for the coplanar 4,175 Hz data with superimposed contours, flight lines and EM anomaly symbols.
- 4D. APPARENT RESISTIVITY; calculated for the coaxial 4,600 Hz data with superimposed contours, flight lines and EM anomaly symbols.
- 4E. APPARENT RESISTIVITY; calculated for the coplanar 33,000 Hz data with superimposed contours, flight lines and EM anomaly symbols.

ELECTROMAGNETIC

5. VLF-EM TOTAL FIELD; with superimposed contours, flight lines, and EM anomaly symbols.
- 6A. HEM OFFSET PROFILES; coplanar 850 Hz and coaxial 935 Hz data with flight lines and EM anomaly symbols.
- 6B. HEM OFFSET PROFILES; coplanar 4,175 Hz and coaxial 4,600 Hz data with flight lines and EM anomaly symbols.
- 6C. HEM OFFSET PROFILES; coplanar 33,000 Hz data with flight lines and EM anomaly symbols.

RADIOMETRIC

- 7A. **URANIUM COUNT** with superimposed contours and flight lines.
- 7B. **THORIUM COUNT** with superimposed contours and flight lines.
- 7C. **POTASSIUM COUNT** with superimposed contours and flight lines.
- 7D. **TOTAL COUNT** with superimposed contours and flight lines.

SHADOW DERIVATIVE: (Scale 1:20,000)

- 8. **TOTAL FIELD MAGNETICS SHADOW MAP; one or more of:**
 - (A) parallel to the flight lines
 - (B) perpendicular to the flight lines
 - (C) at 45° or 135° to the flight lines

**REPORT ON A
COMBINED HELICOPTER-BORNE
MAGNETIC, ELECTROMAGNETIC
RADIOMETRIC AND VLF-EM SURVEY
ONEMICA AREA
PROVINCE OF BRITISH COLUMBIA**

1. INTRODUCTION

This report describes an airborne geophysical survey carried out on behalf of Noranda Exploration Company, Limited by Geonex Aerodat Inc. under a contract dated June 21, 1993. Principal geophysical sensors included a five frequency electromagnetic system, a high sensitivity cesium vapour magnetometer, a radiometric system and a two frequency VLF-EM system. Ancillary equipment included a colour video tracking camera, a radar altimeter, a power line monitor and a base station magnetometer.

The survey was carried out over about 90 square kilometres located approximately 195 km. north-northeast of Smithers. Total survey coverage was approximately 350 line kilometres. The flight line spacing was 250 m. The Geonex Aerodat Job Number is J9358.

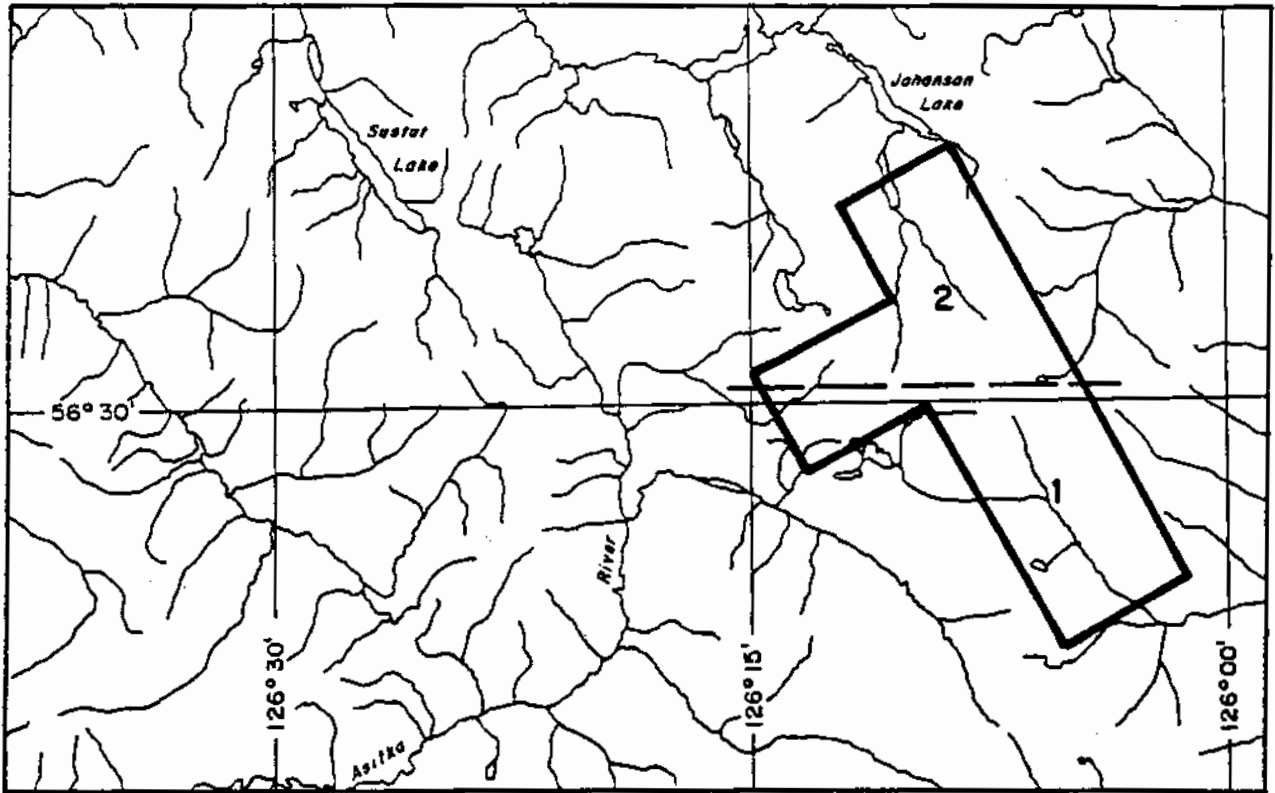
This report describes the survey, the data processing, data presentation and interpretation of the geophysical results. Electromagnetic anomalies have been identified and appear on selected map products as EM anomaly symbols with interpreted source characteristics. Conductive areas of interest are indicated on an interpretation map with designation number or letter. Prominent structural features interpreted from the magnetic results are also indicated. Recommendations concerning areas with favourable geophysical characteristics are made with reference to this compilation/interpretation map.

2. SURVEY AREA

The survey area is located in the Onemica area of northern British Columbia about 230 km. east-northeast of Stewart and 195 km. north-northeast of Smithers just 30 km. south-southeast of Fleet Peak Mountain. Topography is shown on the 1:50,000 scale NTS map sheets 94 D/8 and D/9. Local relief is very rugged. Elevations range from 1,200 to over 2,100 metres above mean sea level.

The survey area is shown in the attached index map which includes local topography and latitude - longitude coordinates. This index map also appears on all black line map products. The flight line direction is north 60° east. Line spacing is 250 metres.

SURVEY AREA



3. SURVEY PROCEDURES

The survey was flown in the period from July 20 to 22, 1993. Principal personnel are listed in Appendix IV. A total of six survey flights were required to complete the project.

The aircraft ground speed was maintained at approximately 60 knots (30 metres per second). The nominal EM sensor height was 30 metres (100 feet), consistent with the safety of the aircraft and crew.

A global positioning system (GPS) consisting of a Trimble TANS GPS receiver plus the Polycorder data logger was used for navigation and flight line control. Differential GPS data is processed in the field on a PC using software supplied by Trimble. One system is installed in the survey helicopter. This involves mounting the receiver antenna on the tail boom. A second system was used as the base station.

The UTM coordinates of survey area corners were taken from the published NTS maps. These coordinates are used to program the navigation system. A test flight was used to confirm that area coverage would be as required.

Thereafter the traverse lines are flown under the guidance of the navigation system. The operator also enters manual fiducials over prominent topographic features as seen on a topographic map. Survey lines which show excessive deviation were re-flown.

The magnetic tie lines were flown using visual navigation in areas of low topographic and magnetic relief. Aircraft position was taken from the navigation system.

Calibration lines are flown at the start, middle (if required) and end of every survey flight. These lines are flown outside of ground effects to record electromagnetic zero levels.

4. DELIVERABLES

The results of the survey are presented in a report plus maps. The report is presented in four copies. White print copies of all black line maps are folded and bound with the report. The colour maps are delivered in four copies. The shadow maps are delivered in two copies. The colour and shadow maps are rolled and delivered in map tube(s).

The black line maps show topography, UTM grid co-ordinates and the survey boundary. A full list of all map types is given at the beginning of this report. A summary is given following:

MAP NO. DESCRIPTION

BLACK LINE

- 1 Base Map
- 2 Flight Path Map
- 3 Compilation/Interpretation Map
- 4 Total Field Magnetic Contours
- 5 Vertical Magnetic Gradient Contours
- 6 Weight Percent Magnetite
- 7A Apparent Resistivity Contours - 850 Hz
- 7B Apparent Resistivity Contours - 935 Hz
- 7C Apparent Resistivity Contours - 4,175 Hz
- 7D Apparent Resistivity Contours - 4,600 Hz
- 7E Apparent Resistivity Contours - 33,000 Hz
- 8 VLF-EM Total Field Contours

COLOUR

- 1 Total Field Magnetics
- 2 Vertical Magnetic Gradient
- 3 Weight Percent Magnetite
- 4A Apparent Resistivity Contours - 850 Hz
- 4B Apparent Resistivity Contours - 935 Hz
- 4C Apparent Resistivity Contours - 4,175 Hz
- 4D Apparent Resistivity Contours - 4,600 Hz
- 4E Apparent Resistivity Contours - 33,000 Hz
- 5 VLF-EM Total Field
- 6A HEM Offset Profiles - 850 Hz and 935 Hz
- 6B HEM Offset Profiles - 4,175 Hz and 4,600 Hz
- 6C HEM Offset Profiles - 33,000 Hz
- 7A Uranium Count Radiometric
- 7B Thorium Count Radiometric
- 7C Potassium Count Radiometric
- 7D Total Count Radiometric
- 8 Total Field Magnetic Shadow

The processed digital data is organized on 9 track archive tape. Both the profile and the gridded data are saved on tape. A full description of the archive tape(s) is delivered with the tape(s).

All gridded data are also provided on diskettes suitable for displaying on IBM compatible 286 or 386 microcomputers using the Aerodat AXIS (Aerodat Extended Imaging System) or RTI (Real Time Imaging) software package.

All analog records, base station magnetometer records, flight path video tape and original map cronaflexes are delivered with the final presentation.

5. AIRCRAFT AND EQUIPMENT

5.1 Aircraft

A ASTAR helicopter, (C-FXHS), piloted by L. Stanley , owned and operated by Executive Helicopters Ltd, was used for the survey. G. Bissonnete of Geonex Aerodat acted as navigator and equipment operator. Installation of the geophysical and ancillary equipment was carried out by Geonex Aerodat. The survey aircraft was flown at a mean terrain clearance of 60 metres (200 feet).

5.2 Electromagnetic System

The electromagnetic system was an Aerodat 5 frequency system. Two vertical coaxial coil pairs were operated at 935 Hz and 4,600 Hz and three horizontal coplanar coil pairs at 850 Hz 4,175 Hz and 33 kHz. The transmitter-receiver separation was 7 metres. Inphase and quadrature signals were measured simultaneously for the 6 frequencies with a time constant of 0.1 seconds. The HEM bird was towed 30 metres (100 feet) below the helicopter.

5.3 VLF-EM System

The VLF-EM System was a Herz Totem 2A. This instrument measures the total field and vertical quadrature components of two selected frequencies. The sensor was towed in a bird 10 metres below the helicopter.

VLF transmitters are designated "Line" and "Ortho". The line station is that which is in a direction from the survey area which is ideally normal to the flight line direction. This is the VLF station most often used because of optimal coupling with near vertical conductors running perpendicular to the flight line direction . The ortho station is ideally 90 degrees in azimuth away from the line station.

The transmitters used were:

NAA, Cutler, Maine broadcasting at 24.0 kHz. (ortho)

NLK, Jim Creek, Washington broadcasting at 24.8 kHz. (line)

NSS, Annapolis, Maryland broadcasting at 21.4 kHz. (ortho)

Periodic shutdown of the VLF stations for maintenance occurs on a rotating basis. As a result, for the particular flight days for this survey, two different sets of stations were used for the survey as listed following:

| FLIGHT NO. | LINE STATION | ORTHO STATION | LINES SURVEYED |
|------------|--------------|---------------|-------------------|
| 1 | NLK (24.8) | NSS (21.4) | 22 -30 |
| 2 to 6 | NLK (24.8) | NAA (24.0) | 1 to 21, 31 to 65 |

5.4 Magnetometer

The magnetometer employed was a Scintrex H8 cesium, optically pumped magnetometer sensor. The sensitivity of this instrument is 0.001 nanoTesla at a 0.2 second sampling rate. The sensor was towed in a bird 15 metres (50 feet) below the helicopter (45 metres (150 feet) above the ground).

5.5 Gamma-Ray Spectrometer

An Exploranium GR-256 spectrometer coupled to 512 cubic inches of crystal sensor was used to record four channels of radiometric data. Spectrum stabilization is based on the 662 KeV peak from Cesium sources planted on the crystals.

The four channels recorded and their energy windows were as follows:

| Channel | Window |
|------------------|------------------|
| Total Count (TC) | 0.40 to 2.80 MeV |
| Potassium (K) | 1.37 to 1.57 MeV |
| Uranium (U) | 1.66 to 1.86 MeV |
| Thorium (Th) | 2.41 to 2.81 MeV |

The four channels of radiometric data were recorded at a 1 second update rate (counts per second - cps). Digital recording resolution is 1 cps.

5.6 Ancillary Systems

Base Station Magnetometer

An IFG-2 proton precession magnetometer was operated at the base of operations (Suskeena Lodge) to record diurnal variations of the earth's magnetic field. The clock of the base station was synchronized with that of the airborne system to facilitate later correlation. Recording resolution was 1 nT. The update rate was 4 seconds.

External magnetic field variations were recorded on a 3" wide paper chart and in digital form. The analog record shows the magnetic field trace plotted on a grid. Each division of the grid (0.25") is equivalent to 1 minute (chart speed) or 5 nT (vertical sensitivity). The date, time and current total field magnetic value are printed every 10 minutes.

Radar Altimeter

A King KRA-10 radar altimeter was used to record terrain clearance. The output from the instrument is a linear function of altitude. The radar altimeter is checked after installation using a line marked off at intervals of 50 feet. A heavy weight is tied onto one end of the line. The helicopter moves up over the weight and the operator notes the radar altimeter reading at the 100, 150, 200 and 250 foot marks.

Tracking Camera

A Panasonic colour video camera was used to record flight path on VHS video tape. The camera was operated in continuous mode. The flight number, 24 hour clock time (to .01 second), and manual fiducial number are encoded on the video tape.

Global Positioning System (GPS)

The Global Positioning System is a U.S. Department of Defense program which will provide world-wide, 24 hour, all weather position determination capability. GPS consists of three segments:

- a constellation of satellites
- ground stations which control the satellites
- a receiver

The receiver takes in coded data from satellites in view and there after works out the range to each satellite. The coded data must therefore include the instantaneous position of the satellite relative to some agreed earth-fixed coordinate system.

The final satellite constellation will consist of 24 satellites with a proportion of the satellites acting as standby spares.

Analog Recorder

A RMS dot matrix recorder was used to display the data during the survey. Record contents are as follows:

| Label | Contents | Scale |
|-------|---|---------------|
| MAGF | Total Field Magnetics, Fine | 2.5 nT/mm |
| MAGC | Total Field Magnetics, Course | 25 nT/mm |
| VLT | VLF-EM, Total Field, Line Station | 2.5% / mm |
| VLQ | VLF-EM, Vert. Quadrature, Line Station | 2.5% / mm |
| VOT | VLF-EM, Total Field, Ortho Station | 2.5% / mm |
| VOQ | VLF-EM, Vert. Quadrature, Ortho Station | 2.5% / mm |
| CXI1 | 935 Hz, Coaxial, Inphase | 2.5 ppm/mm |
| CXQ1 | 935 Hz, Coaxial, Quadrature | 2.5 ppm/mm |
| CXI2 | 4,600 Hz, Coaxial, Inphase | 2.5 ppm/mm |
| CXQ2 | 4,600 Hz, Coaxial, Quadrature | 2.5 ppm/mm |
| CPI1 | 850 Hz, Coplanar, Inphase | 5 ppm/mm |
| CPQ1 | 850 Hz, Coplanar, Quadrature | 5 ppm/mm |
| CPI2 | 4,175 Hz, Coplanar, Inphase | 10 ppm/mm |
| CPQ2 | 4,175 Hz, Coplanar, Quadrature | 10 ppm/mm |
| CPI3 | 33,000 Hz, Coplanar, Inphase | 20 ppm/mm |
| CPQ3 | 33,000 Hz, Coplanar, Quadrature | 20 ppm/mm |
| TF | Radiometric - Total Field | 10 counts/mm |
| K | Radiometric - Potassium | 5 counts/mm |
| U | Radiometric - Uranium | 2.5 counts/mm |
| T | Radiometric - Thorium | 2.5 counts/mm |
| RALT | Radar Altimeter | 10ft/mm |
| PWRL | 60 Hz Power Line Monitor | - |

Data is recorded with positive - up, negative - down. This does not apply to the VLF data as seen on the analog records which is inverted.

The analog zero of the radar altimeter is 5 cm from the top of the analog record. A helicopter terrain clearance of 60 m (200 feet) should therefore be seen some 3 cm from the top of the analog record.

Chart speed is 2 mm/second. The 24 hour clock time is printed every 20 seconds. The total magnetic field value is printed every 30 seconds. The ranges from the radar navigation system are printed every minute.

Vertical lines crossing the record are operator activated manual fiducial markers. The start of any survey line is identified by two closely spaced manual fiducials. The end of any survey line is identified by three closely spaced manual fiducials. Manual fiducials are numbered in order. Every tenth manual fiducial is indicated by its number, printed at the bottom of the record.

Calibration sequences are located at the start and end of each flight and at intermediate times where needed.

Digital Recorder

A DGR-33 data system recorded the digital survey data on magnetic media. Contents and update rates were as follows:

| DATA TYPE | RECORDING INTERVAL | RECORDING RESOLUTION |
|--------------------------|--------------------|----------------------|
| Magnetometer | 0.2 s | 0.001 nT |
| VLF-EM (4 Channels) | 0.2 s | 0.03% |
| HEM (8 Channels) | 0.1 s | |
| coaxial | | 0.03 ppm |
| coplanar-850 Hz/4,175 Hz | | 0.06 ppm |
| coplanar -33 kHz | | 0.125 ppm |
| Radiometric | 0.2 s | 1 cps |
| Position (2 Channels) | 0.2 s | 0.1 m |
| Altimeter | 0.2 s | 0.05 m |
| Power Line Monitor | 0.2 s | - |
| Manual Fiducial | | |
| Clock Time | | |

6. DATA PROCESSING AND PRESENTATION

6.1 Base Map

The base map is taken from a photographic enlargement of the NTS topographic maps. A UTM reference grid (grid lines usually every kilometre) and the survey area boundary were added. After registration of the flight path to the topographic base map, topographic detail and the survey boundary are digitized. This digital image of the base map is used as the base for the colour and shadow maps.

6.2 Flight Path Map

Global Positioning System

The GPS receiver takes in coded data from satellites in view and there after works out the range to each satellite. The coded data must therefore include the instantaneous position of the satellite relative to some agreed earth-fixed coordinate system.

A further calculation using ranges to a number of satellites gives the position of the receiver in that coordinate system (eg. UTM, lat/long.). The elevation of the receiver is given with respect to a model ellipsoidal earth.

Normally the receiver must see 4 satellites for a full positional determination (3 space coordinates and time). If the elevation is know in advance, only 3 satellites are needed. These are termed 3D and 2D solutions.

The position of the receiver is updated every second. The accuracy of any 1 second position determination is described by the Circular Error Probability (CEP). 95% of all position determinations will fall with a circle of a certain radius. If the horizontal position accuracy is 25 m CEP for example, 95% of all trials will fall within a circle of 25 m radius centred on the mean. The system may be degraded for civilian use and the autonomous accuracy is then 100 m CEP. This situation is called selective availability (SA). Much of this error (due to principally to satellite position/time errors and atmospheric delays) can be removed using two GPS receivers operating simultaneously. One receiver acting as the base station, is located at a known position. The second remote receiver is in the unknown position. Differential corrections determined for the base station may then be applied to the remote station. Differential positions are accurate to 5 m CEP (for a one second sample). Averaging will reduce this error further.

Flight Path

The flight path is drawn using linear interpolation between x,y positions from the navigation system. These positions are updated every second (or about 1.5.0 mm at a scale of 1:20,000). These positions are expressed as UTM eastings (x) and UTM northings (y).

Occasional dropouts occur when the optimum number of satellites are not available for the GPS to make accurate positional determinations. Interpolation is used to cover short flight path gaps. The navigator's flight path and/or the flight path recovered from the video tape may be stitched in to cover larger gaps. Such gaps may be recognized by the distinct straight line character of the flight path.

The manual fiducials are shown as a small circle and labelled by fiducial number. The 24 hour clock time is shown as a small square, plotted every 30 seconds. Small tick marks are plotted every 2 seconds. Larger tick marks are plotted every 10 seconds. The line and flight numbers are given at the start and end of each survey line.

The flight path map is merged with the base map by matching UTM coordinates from the base maps and the flight path record. The match is confirmed by checking the position of prominent topographic features as recorded by manual fiducial marks or as seen on the flight path video record.

6.3 Electromagnetic Survey Data

The electromagnetic data were recorded digitally at a sample rate of 10 per second with a time constant of 0.1 seconds. A two stage digital filtering process was carried out to reject major spheric events and to reduce system noise.

Local spheric activity can produce sharp, large amplitude events that cannot be removed by conventional filtering procedures. Smoothing or stacking will reduce their amplitude but leave a broader residual response that can be confused with geological phenomena. To avoid this possibility, a computer algorithm searches out and rejects the major spheric events. The signal to noise ratio was further enhanced by the application of a low pass digital filter. This filter has zero phase shift which prevents any lag or peak displacement from occurring, and it suppresses only variations with a wavelength less than about 0.25 seconds. This low effective time constant gives minimal profile distortion.

Following the filtering process, a base level correction was made using EM zero levels determined during high altitude calibration sequences. The correction applied is a linear function of time that ensures the corrected amplitude of the various inphase and quadrature components is zero when no conductive or permeable source is present. The filtered and levelled data were used in the determination of apparent resistivity (see below).

6.4 Total Field Magnetics

The aeromagnetic data were corrected for diurnal variations by adjustment with the recorded base station magnetic values. No corrections for regional variations were applied. The corrected profile data were interpolated on to a regular grid using an Akima spline technique. The grid provided the basis for threading the presented contours. The minimum contour interval is 5 nT. A grid cell size of 25 m was used.

6.5 Vertical Magnetic Gradient

The vertical magnetic gradient was calculated from the gridded total field magnetic data. The calculation is based on a 17×17 point convolution in the space domain. The results are contoured using a minimum contour interval of 0.1 nT/m. Grid cell sizes are the same as those used in processing the total field data.

6.6 Weight Percent Magnetite

The apparent weight percent magnetite has been calculated from the 4,175 Hz inphase electromagnetic response. The algorithm is based on the electromagnetic response to a non-conducting, magnetically polarizable half-space. The calculation involves a correction to a sensor elevation of 30 m followed by a conversion to weight percent. The elevation correction is based on the exponential fall-off of response amplitude with height. Data collected with a sensor terrain clearance less than 20 m is ignored. As a rule of thumb, a negative inphase response of 1 ppm in either coaxial channel will work out to a percent magnetite by weight of about 0.2%.

The results will be misleading if the source is a near-vertical dyke or intrusion. In such cases, the calculated weight percent magnetite may be too little by a factor of 10 or more.

The calculated apparent percent magnetite data were interpolated on a square grid (25 m grid cell size). The grid provided the basis for threading the presented contours. The minimum contour interval is 1%.

6.7 Apparent Resistivity

The apparent resistivity is calculated by assuming a 200 metre thick conductive layer over resistive bedrock. The computer determines the resistivity that would be consistent with the sensor elevation and recorded inphase and quadrature response amplitudes at the selected frequency. The apparent resistivity profile data was re-interpolated onto a regular grid at a 25 metres true scale interval using an Akima spline technique and contoured using logarithmically arranged contour intervals. The minimum contour interval is 0.1 log(ohm.m).

The highest measurable resistivity is approximately equal to the transmitter frequency. The lower limit on apparent resistivity is rarely reached.

6.8 VLF-EM

The VLF Total Field data from the Line Station is levelled such that a response of less than 0% is seen in non-anomalous regions. The corrected profile data are interpolated onto a regular grid using an Akima spline technique. The grid provided the basis for threading the presented contours. The minimum contour interval is 2%. Grid cell size is 25 m.

6.9 Radiometric Data

The four channels of radiometric data are subject to a four stage data correction process.

The stages are

- low pass filter (seven point Hanning)
- background removal
- terrain clearance correction
- compton stripping correction

The Compton stripping factors used were

| | |
|-------|-------------------|
| alpha | 0.277 (Th into U) |
| beta | 0.436 (Th into K) |
| gamma | 0.77 (U into K) |
| a | 0.07 (U into Th) |
| b | 0.00 (K into Th) |
| g | 0.008 (K into U) |

where alpha, beta and gamma are the forward stripping coefficients and a, b, g are the backward stripping coefficients. These coefficients are taken in part from the sample checks done at the start of each flight.

The altitude attenuation coefficients used were 0.0072 (TC), 0.0085 (K), 0.0082 (U) and 0.0067 (Th). The units are metres⁻¹. These coefficients are taken from GSC publications for similar radiometric systems. Radiometric data were corrected to a mean terrain clearance of 60 m.

The corrected data were interpolated on a square grid (cell size 25m) using an Akima spline technique. The grids provided the basis for threading the presented contours. The minimum contour intervals are 25 cps (TC), 2 cps (K), 1 cps (U) and 1 cps (Th).

7. INTERPRETATION

7.1 Area Geology

The regional geology comprises Triassic and possibly Jurassic age intermediate to mafic volcanic tuffs, agglomerates and lavas enveloping narrow limestone and argillite formations. Minor metasediments and metavolcanics are also present. The whole area is intruded by felsic igneous rocks. The volcanics and associated rocks dip easterly to southerly between 15° to 45°.

7.2 Magnetic Interpretation

The total field magnetic responses reflect major changes in the magnetite content of the underlying rock units. The amplitude of the magnetic responses relative to the regional background help to assist in identifying specific magnetic and non-magnetic units related to, for example, mafic flows or tuffs, mafic to ultramafic intrusives, felsic intrusives, felsic volcanics and/or sediments etc. Obviously, several geological sources can produce the same magnetic response. These ambiguities can be reduced considerably if basic geological information on the area is available to the geophysical interpreter.

In addition to amplitude variations, magnetic patterns related to the geometry of the particular rock unit also help in determining the probable source of the magnetic response. For instance, long narrow magnetic linears usually reflect mafic tuff or flow horizons while semi-circular features with complex magnetic amplitudes may be produced by local plug-like intrusive sources such as pegmatites, carbonatites or kimberlites.

The calculated vertical magnetic gradient assists considerably in mapping weaker magnetic linears that are partially masked by nearby higher amplitude magnetic features. The broad zones of higher magnetic amplitude, however, are severely attenuated in the vertical magnetic gradient results. These higher amplitude zones reflect rock units having magnetic susceptibility signatures. For this reason both the total and gradient magnetic data sets must be evaluated.

Theoretically the zero contour of the magnetic gradient map marks the contacts or limits of large magnetic sources. This applies to wide sources, greater than 50 metres, having simple slab geometries and shallow depth. (See discussion in Appendix I) Thus the gradient map also aids in the more accurate delineation of contacts between differing magnetic rock units.

The cross cutting structures shown on the interpretation map are based on interruptions and discontinuities in the magnetic trends. Generally, sharp folding of magnetic units will produce a magnetic pattern indistinguishable from a fault break. Thus these structures have been designated as fold/fault features.

7.3 Magnetic Survey Results and Conclusions

To facilitate the following discussion of the magnetic results it is suggested that the interpretation map be compared with the total field and vertical gradient magnetic colour contour maps either as overlays or side by side.

The magnetic background is interpreted to be approximately 57,950 nanoTesla (nT). Amplitudes range from about 2,500 nT above background to 350 nT below background. The magnetic anomaly patterns are very complex with rapidly changing amplitudes. Generally, the trend directions of the magnetic units are north-northwest to northwest. The higher amplitude anomalies, greater than 300 nT above background, are indicated on the interpretation map as shaded areas. Almost all of these areas are coincident with topographic highs which are mapped as intermediate volcanics. The best example is seen in the extreme southeast corner of the survey area where there is a four kilometre long northeast striking anomaly greater than 2,000 nT above background. This anomaly reflects a very high magnetite content which produces striking negative in-phase responses on the electromagnetic channels. It is coincident with one of the highest ridges in the area. It could reflect a siliceous iron formation or iron-rich skarn unit rather than a mafic volcanic unit.

Other lower amplitude magnetic trends associated with the higher amplitude areas are designated on the interpretation map as solid lines. These sinuous and intermittent narrow anomalies are more likely to be related to mafic tuffs and flows which are ubiquitous to the area. Northeast striking cross-cutting fold/fault structures have been located on the interpretation map to explain some of the magnetic anomaly displacements and interruptions.

A most obvious north-south striking fault or contact structure is evident in the north central half of the survey block. This structure flanks the west side of a narrow below background magnetic zone that encompasses a complex conductive horizon. Such a signature is typical of a graphitic argillite formation. These designated negative or below background magnetic areas generally flank the east and west sides of the central core of magnetic activity trending through the central north part of the main survey block. In the south half of the block there are three such horizons. They sometimes contain local conductive zones and low amplitude weak magnetic linears which are shown as dashed lines. Sedimentary or felsic volcanic rocks with intercalated narrow mafic tuff or flow horizons may underlay these low amplitude magnetic zones. In areas where there is little conductive activity, such as the south central part of the south survey block and along the east side of the survey boundary, these low amplitude magnetic areas may be mapping felsic intrusive rocks.

7.4 Electromagnetic Anomaly Selection/Interpretation

Usually two sets of stacked colour coded profile maps of one coaxial and one coplanar inphase and quadrature responses are used to select conductive anomalies of interest. Selection of anomalies is based on conductivity as indicated by the inphase to quadrature ratios of the 4,600 Hz coaxial data, anomaly shape, and anomaly profile characteristics relative to coaxial and corresponding coplanar responses.(see discussion and figure in Appendix I)

It is difficult to differentiate between responses associated with the edge effects of flat lying conductors and actual poor conductivity bedrock conductors on the edge of or overlain by flat lying conductors. Poor conductivity bedrock conductors having low dips will also exhibit responses that may be interpreted as surficial overburden conductors. In such cases, where the source of the conductive response appears to be ambiguous, the anomaly is still selected for plotting. In some situations the conductive response has line to line continuity and some magnetic association thus providing possible evidence that the response is related to an actual bedrock source.

The calculation of the depth to the conductive source and its conductivity is based on the 4,600 Hz data using a thin vertical sheet model. The amplitude of the inphase and quadrature responses are used for the calculations which are automatically determined by computer. These data are listed in Appendix II and the depth and conductivity values are shown with each plotted anomaly. Further detailed discussion and illustration of the determination of these values is contained in Appendix I.

The selected anomalies are automatically categorized according to their conductivity and amplitude. The calculation of the conductivity of low amplitude anomalies can be very inaccurate. Therefore, anomalies having amplitudes below a certain level and/or low conductivity value are given a zero rating with the category increasing for increasing conductivity values that are statistically reliable.

7.5 VLF Electromagnetic Survey

This high frequency type of survey, utilizing fixed government communication transmitter stations, tends to detect long strike length and/or surficial poor conductivity sources such as swamps, creeks and rivers. Conductors that are optimum coupled with the primary field will usually predominate over those with other strike directions. In some instances anomalies will be produced by variations in topographic relief.

This appears to be the case for this survey where many of the VLF anomalies that are not coincident with the helicopter EM system conductors are associated with topographic highs. There are some interesting exceptions in the extreme south central part of the survey area. Here, portions of the magnetic linears and areas have a coincident VLF response. These anomalies are on the flanks of topographic highs and can not be explained by topography. Note, also, the spatial relationship of the VLF anomalous and non-anomalous areas to the fault structures that are interpreted exclusively from the magnetic results. The correlations give added credibility to the interpreted fault structures.

7.6 Electromagnetic Survey Results and Conclusions

There are many conductive intercepts scattered haphazardly throughout the survey block. Where line to line continuity of a particular set of conductor intercepts is evident, however, they have been grouped together and designated with a number as previously explained.

Many of the anomalies have poor conductivity and broad multiple peaks without the usual crisp sharp profile peaks associated with vertical conductors. This is to be expected as the source rocks are known to have low dips from 15 to 45 degrees. Nevertheless, some of the designated conductive responses may be produced by conductive overburden.

In addition to the conductive responses, there are very strong negative in-phase responses related to high amplitude magnetic areas. Most of these negative anomalies have no quadrature response and can be attributed solely to high susceptibility material within iron rich rocks. Those anomalies having a quadrature response have been designated as they suggest some conductive material is also present.

The anomaly groupings have been numbered ascending, generally, from southeast to northwest with a total of 25 conductive trends or areas being designated. Anomalies 1, 3 and 4 are conductive/susceptibility responses within three different magnetic environments. Anomaly 1 is flanked by a short magnetic zone on the west and the contact of a low amplitude magnetic area on the east. Anomaly 3 is within the low amplitude area and anomaly 4 is coincident with the extremely high amplitude magnetic zone described previously. The source of these anomalies may be sulphides. They would be a good starting point in the assessment of the importance of these types of responses elsewhere in the survey area.

Anomalies 2, 5A, 5B, 6A, possibly 6B, 8, 19, 21A, 21B and 21C are within the central low amplitude magnetic zone thought to be related to sediments or felsic rocks. They are possibly produced by weakly graphitic/pyritic argillite formations. Anomalies 5A and 6A are long broad anomalous areas which flank interpreted northeast trending fault structures. They may be associated with the fault and/or a fold structure as the strike of the formations are known to be quite variable.

Anomalies 7, 11, 14, 15, 16 and 17 are isolated conductors within areas of low magnetic relief. They are in the same category as the just previously mentioned anomalies. Selective investigation of these anomalies is warranted as they are in a slightly different geophysical environment compared to the other anomalies.

Of more interest, because of their magnetic associations, are anomalies 9, 10, 11, 12, 13, 18, and 20 which are clustered in the west central part of the survey block. Anomaly 12 is a long formational conductive complex while anomalies 9 and 10 cover several short complex conductive areas which may be related to fold structures. With the exception of anomaly 13, a one line response, the conductors lack an exact magnetic correlation and their relationship to the magnetic linears in the area may be only fortuitous. The magnetic and conductive responses in this area may be actually mapping intercalated mafic volcanics and slightly conductive sediments. Anomaly 13 appears to be closely associated with an intrusive magnetic plug-like source. This semi-circular magnetic anomaly especially stands out on the vertical magnetic gradient map.

The remaining conductors, 22, 23, 24 and 25 are isolated features of possible interest. Anomaly 22 is partially coincident with a magnetic linear. Anomalies 23 and 24 are probably related to the same source which has been faulted as indicated on the interpretation map.

7.7 Radiometric Interpretation

The ability to detect natural occurring radiation, whether on the ground or from an airborne platform, depends on a number of factors listed as follows:

Count Time

Measurements or count rate statistics are more reliable the longer the detector is in position over a particular location. Therefore in airborne surveying, traverse speed is an important factor in detecting radiation sources. For this reason STOL aircraft and helicopters are a favoured platform for radiometric surveys.

Detector size

The detector crystal volume and thickness determine the sensitivity of the radiometric system to radiation. For accurate measurement and differentiation of higher energy levels of radiation, a large crystal volume is a pre-requisite.

Distance from Source (Altitude)

The attenuation or absorption of radiation in air, although not a significant factor in ground surveys, is a factor in airborne surveys. Normalization of the radiation amplitude data for altitude variations of the aircraft during the survey is necessary. The attenuation is not significant for large areal sources of radiation but is quite severe for localized point sources.

Overburden Cover

Radiation can be completely masked by one foot of rock or three feet of unconsolidated overburden.

Source Geometry

A large exposed outcrop of slightly radioactive material, such as granite which usually has a high potassium count, will be easily detectable from the air. A small outcrop of highly radioactive material, containing an appreciable amount of pitchblende for instance, may not be detectable unless the sensor passes directly over the outcrop and/or is quite close to it.

Source Characteristics

The type and percentage concentration of radioactive minerals present in the rock will determine radiation amplitudes and therefore the ability of the sensor to measure the radiation.

The above factors must be taken into consideration when evaluating and interpreting radiometric surveys. Variations in radiation amplitudes may only be a factor of overburden cover. As a result, an outcrop map of the survey area is very useful for initial evaluation of radioactive element concentrations.

Shales and felsic intrusives tend to have high potassium and thorium levels. Mafic intrusives, sandstone and especially limestone have concentrations of one half to one tenth of the highest levels. Specific intrusives types, such as pegmatites, can have levels of potassium, uranium and thorium, in the order of three to four times the amounts normally present. Uranium ore can contain concentrations of radioactive minerals one to four orders of magnitude greater than normally encountered.

Thus, interpretation of the source of radioactive anomalies, even when the uranium, thorium and potassium thresholds are separated, can be difficult and ambiguous. In some geological environments, specific rock units have higher or lower uranium/thorium, uranium/potassium, or thorium/potassium ratios. Additional diagnostic information is sometimes available when such ratio maps are generated and compared to known geological parameters.

7.8 Radiometric Survey Results and Conclusions

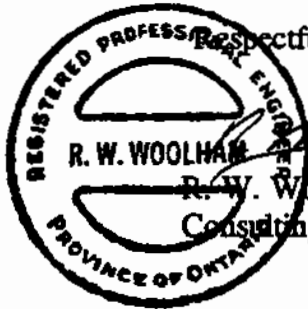
The radiometric responses for this area are not very anomalous. Most of the responses appear to be mapping geological units. A broad zone of potassium channel responses covers the east half of the survey block. The zone comprises elevated potassium channel levels with individual bull's eye anomalies scattered throughout. The west boundary of the zone is marked by Darb Lake and Darb Creek on the north sheet and by Kliyul Creek on the south sheet. This zone of high potassium probably reflects felsic volcanics and intrusives.

There is very little thorium or uranium channel responses except in the extreme south east corner of the south sheet. Here a local area of slightly elevated levels are present probably marking a specific geological unit.

8. RECOMMENDATIONS

Local geological information or the ore target model for the survey area was not available to the author although regional geological information was obtained from Geological Survey maps. It is assumed that the main commodity sought is gold as the area contains several gold occurrences. Possible alteration areas and fault structures are usually the primary host environments for hydrothermally related gold mineralization. Thus, the interpreted fault structure zones that cross local conductive areas are recommended for initial investigation. Many of the anomalies fall into this category with the more interesting ones being 1, 2, 3, 5, 6, 7, 16, 17, 18, 20, 23, 24 and 25. Other anomalies with magnetic associations may also be important targets. Conductors 4, 13, 18 and 20 are of this type.

There are no highly anomalous radiometric responses of note. There are, however, local bull's eye potassium anomalies within the eastern elevated potassium zone as well as a local elevated uranium and thorium anomaly in the southeast corner of the area that warrant investigation. These anomalies may reflect local areas of alteration.

Respectfully submitted,

R. W. Woolham, P.Eng.
Consulting Geophysicist

for

GEONEX AERODAT INC.

J9358

September 24, 1993

APPENDIX I

GENERAL INTERPRETIVE CONSIDERATIONS

GENERAL INTERPRETIVE CONSIDERATIONS

Electromagnetic

The Aerodat six frequency system utilized two different transmitter-receiver coil geometries. The traditional coaxial coil configuration is operated at three widely separated frequencies. The horizontal coplanar coil configuration is similarly operated at three different frequencies where at least one pair is approximately aligned with one of the coaxial frequencies.

The electromagnetic response measured by the helicopter system is a function of the "electrical" and "geometrical" properties of the conductor. The "electrical" property of a conductor is determined largely by its electrical conductivity, magnetic susceptibility and its size and shape; the "geometrical" property of the response is largely a function of the conductor's shape and orientation with respect to the measuring transmitter and receiver.

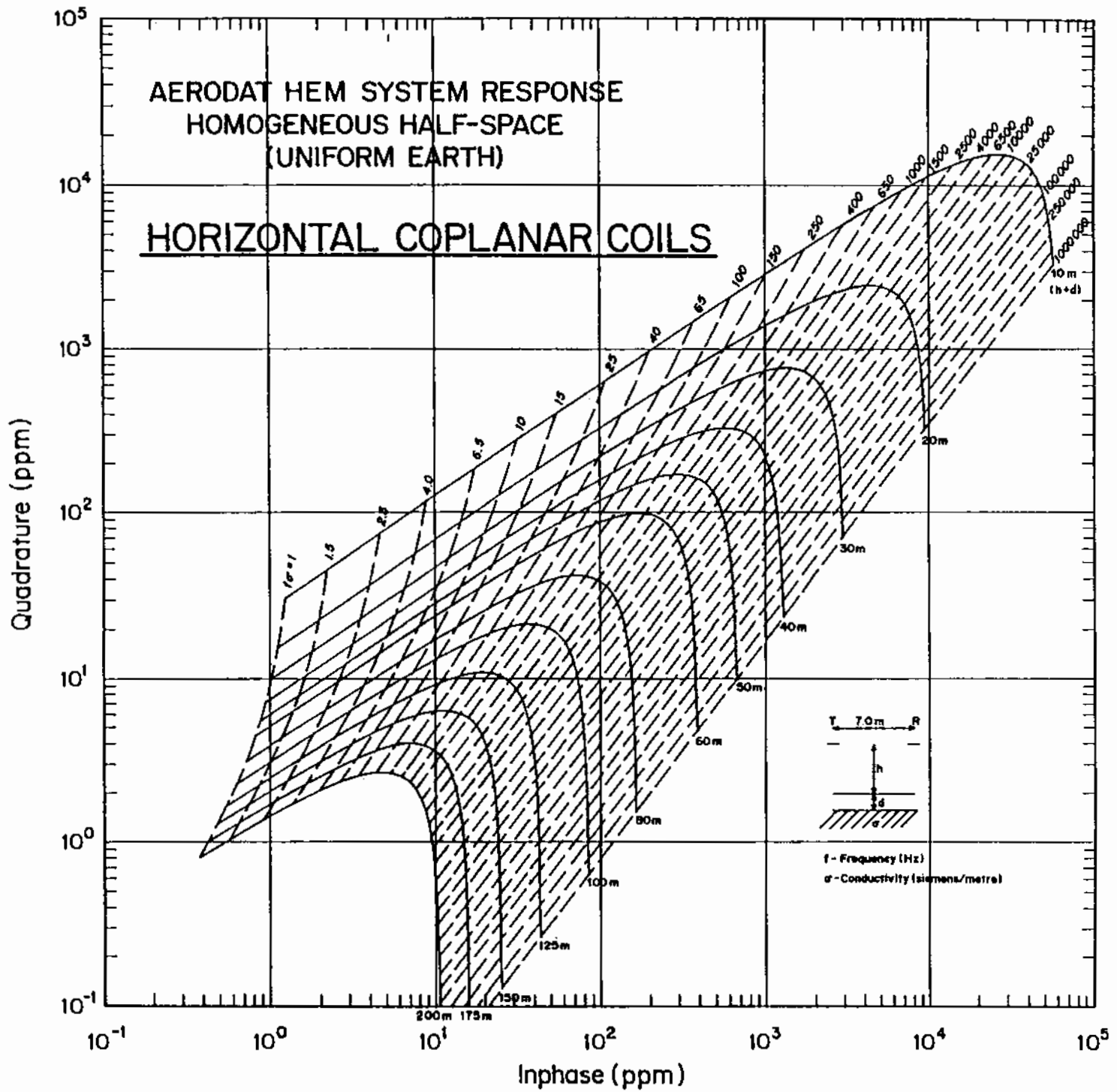
Electrical Considerations

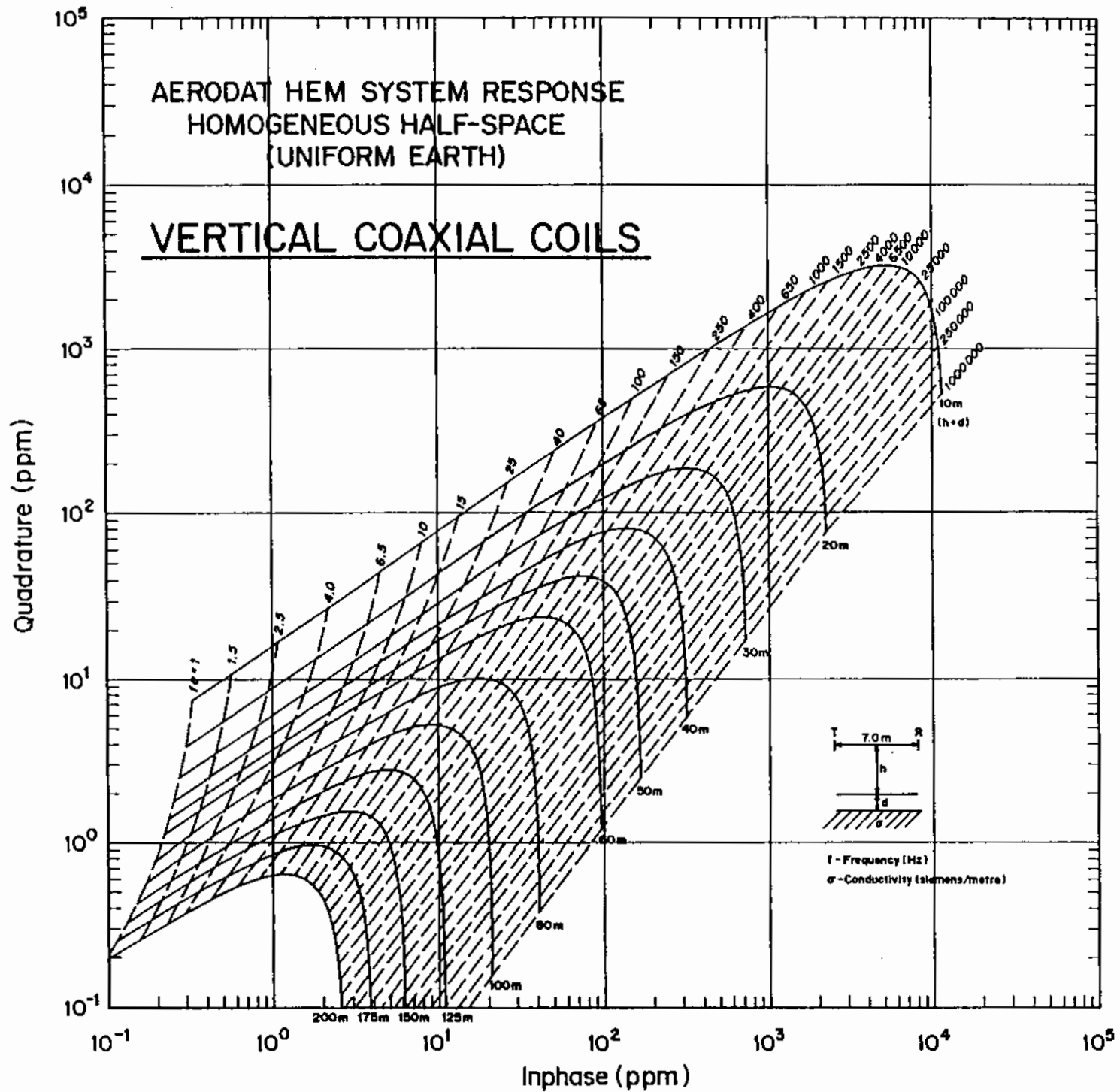
For a given conductive body the measure of its conductivity or conductance is closely related to the measured phase shift between the received and transmitted electromagnetic field. A small phase shift indicates a relatively high conductance, a large phase shift lower conductance. A small phase shift results in a large inphase to quadrature ratio and a large phase shift a low ratio. This relationship is shown quantitatively for a non-magnetic vertical half-plane and half space models on the accompanying phasor diagrams. Other physical models will show the same trend but different quantitative relationships.

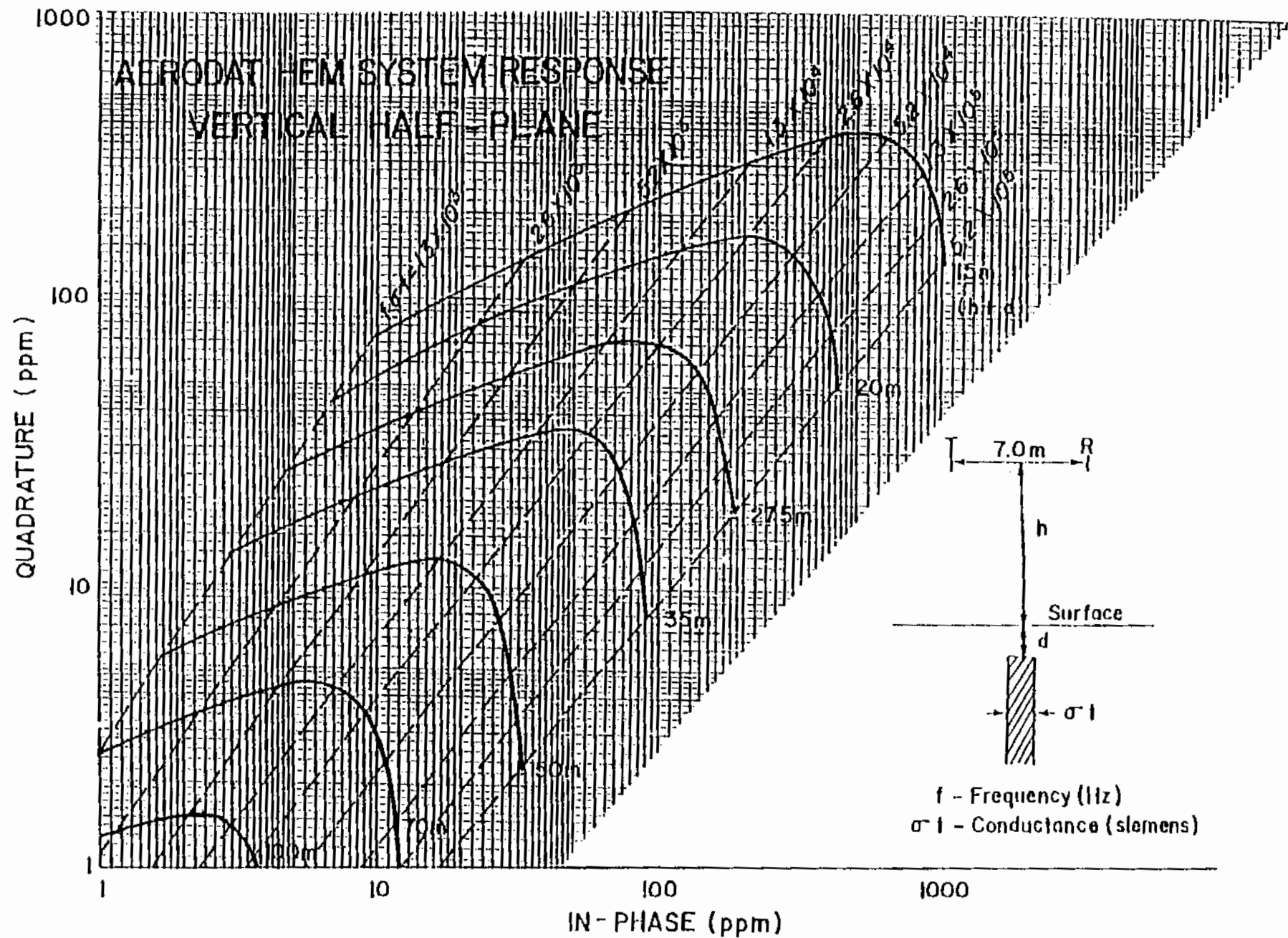
The phasor diagram for the vertical half-plane model, as presented, is for the coaxial coil configuration with the amplitudes in parts per million (ppm) of the primary field as measured at the response peak over the conductor. To assist the interpretation of the survey results the computer is used to identify the apparent conductance and depth at selected anomalies. The results of this calculation are presented in anomaly listings included in the survey report and the conductance and inphase amplitude are presented in symbolized form on the map presentation.

The conductance estimate is most reliable when anomaly amplitudes are large and background resistivities are high. Where the anomaly is of low amplitude and background resistivities are low, the conductance estimates are much less reliable. In such situations, the conductance estimate is often quite low regardless of the true nature of the conductor. This is due to the elevated background response levels in the quadrature channel. In an extreme case, the conductance estimate should be discounted and should not prejudice target selection.

The conductance and depth values as presented are correct only as far as the model approximates the real geological situation. The actual geological source may be of limited length, have significant dip, may be strongly magnetic. Its conductivity and thickness may vary with depth







and/or strike and adjacent bodies and overburden may have modified the response. In general the conductance estimate is less affected by these limitations than is the depth estimate, but both should be considered as relative rather than absolute guides to the anomaly's properties.

Conductance in mhos is the reciprocal of resistance in ohms and in the case of narrow slab-like bodies is the product of electrical conductivity and thickness.

The higher ranges of conductance, greater than 2-4 mhos, indicate that a significant fraction of the electrical conduction is electronic rather than electrolytic in nature. Materials that conduct electronically are limited to certain metallic sulphides and to graphite. High conductance anomalies, roughly 10 mhos or greater, are generally limited to massive sulphides or graphites.

Sulphide minerals, with the exception of such ore minerals as sphalerite, cinnabar and stibnite, are good conductors. Sulphides may occur in a disseminated manner that inhibits electrical conduction through the rock mass. In this case the apparent conductance can seriously underrate the quality of the conductor in geological terms. In a similar sense the relatively non-conducting sulphide minerals noted above may be present in significant concentrations in association with minor conductive sulphides, and the electromagnetic response will only relate to the minor associated mineralization. Indicated conductance is also of little direct significance for the identification of gold mineralization. Although gold is highly conductive, it would not be expected to exist in sufficient quantity to create a recognizable anomaly. Minor accessory sulphide mineralization may however provide a useful indirect indication.

In summary, the estimated conductance of a conductor can provide a relatively positive identification of significant sulphide or graphite mineralization. A moderate to low conductance value does not rule out the possibility of significant economic mineralization.

Geometrical Considerations

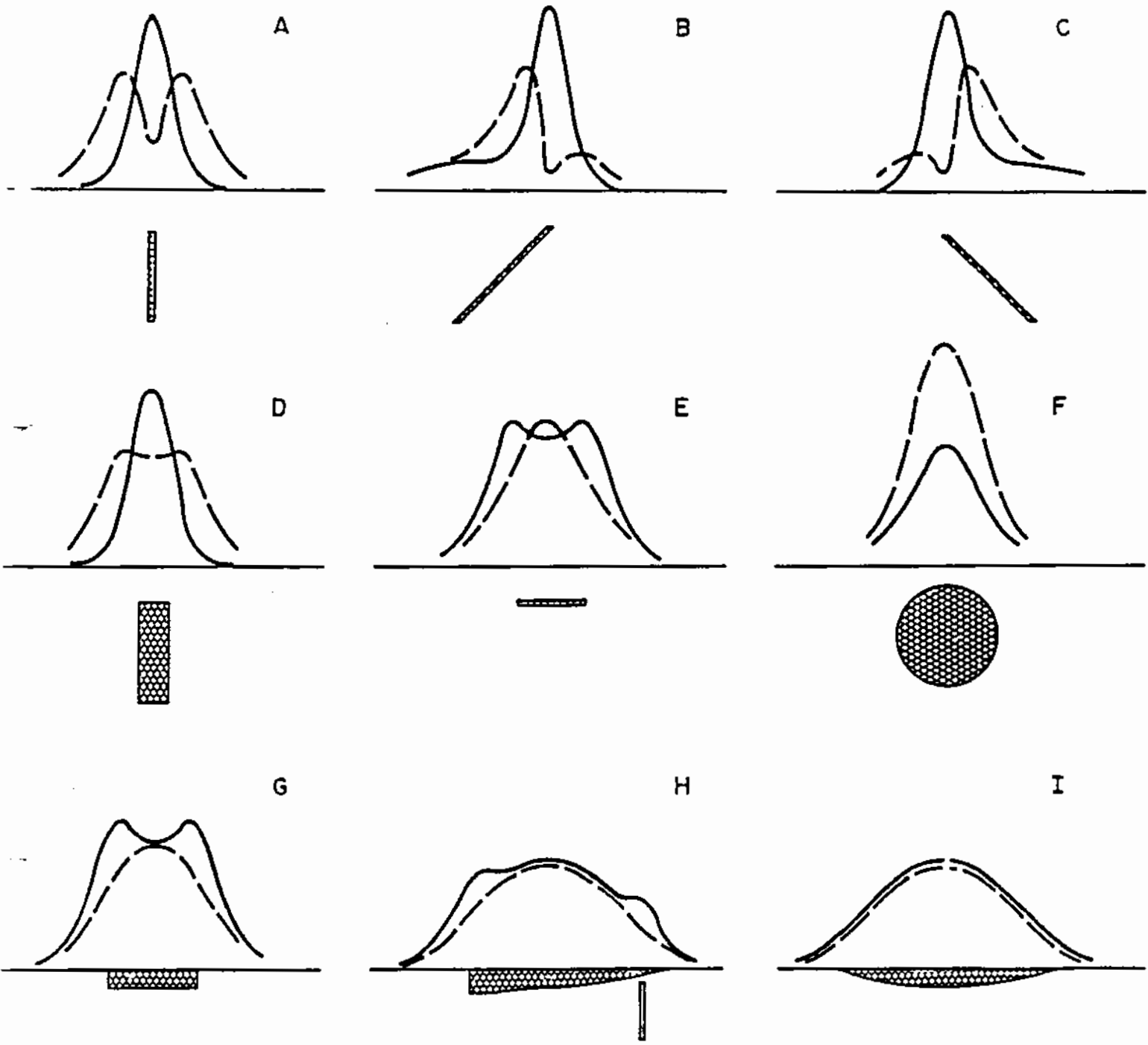
Geometrical information about the geologic conductor can often be interpreted from the profile shape of the anomaly. The change in shape is primarily related to the change in inductive coupling among the transmitter, the target, and the receiver. The accompanying figure shows a selection of HEM response profile shapes from nine idealized targets. Response profiles are labelled A through I. These labels are used in the discussion which follows.

In the case of a thin, steeply dipping, sheet-like conductor, the coaxial coil pair will yield a near symmetric peak over the conductor. On the other hand, the coplanar coil pair will pass through a null couple relationship and yield a minimum over the conductor, flanked by positive side lobes (Profile A). As the dip of the conductor decrease from vertical, the coaxial anomaly shape changes only slightly, but in the case of the coplanar coil pair the side lobe on the down dip side strengthens relative to that on the up dip side (Profiles B and C).

As the thickness of the conductor increases, induced current flow across the thickness of the

HEM RESPONSE PROFILE SHAPE AS AN INDICATOR OF CONDUCTOR GEOMETRY

——— COAXIAL vertical scale 1 ppm/unit
 - - - COPLANAR vertical scale 4 ppm/unit



conductor becomes relatively significant and complete null coupling with the coplanar coils is no longer possible (Profile D). As a result, the apparent minimum of the coplanar response over the conductor diminishes with increasing thickness, and in the limiting case of a fully 3 dimensional body or a horizontal layer or half-space, the minimum disappears completely.

A horizontal conducting layer such as a horizontal thin sheet or overburden will produce a response in the coaxial and coplanar coils that is a function of altitude (and conductivity if not uniform). The profile shape will be similar in both coil configurations with an amplitude ratio (coplanar:coaxial) of about 4:1* (Profiles E and G).

In the case of a spherical conductor, the induced currents are confined to the volume of the sphere, but not relatively restricted to any arbitrary plane as in the case of a sheet-like form. The response of the coplanar coil pair directly over the sphere may be up to 8* times greater than that of the coaxial pair (Profile F).

In summary, a steeply dipping, sheet-like conductor will display a decrease in the coplanar response coincident with the peak of the coaxial response. The relative strength of this coplanar null is related inversely to the thickness of the conductor. A pronounced null indicates a relatively thin conductor. The dip of such a conductor can be inferred from the relative amplitudes of the side-lobes.

Massive conductors that could be approximated by a conducting sphere will display a simple single peak profile form on both coaxial and coplanar coils, with a ratio between the coplanar to coaxial response amplitudes as high as 8*.

Overburden anomalies often produce broad poorly defined anomaly profiles (Profile I). In most cases, the response of the coplanar coils closely follows that of the coaxial coils with a relative amplitude ration of 4*.

Occasionally, if the edge of an overburden zone is sharply defined with some significant depth extent, an edge effect will occur in the coaxial coils. In the case of a horizontal conductive ring or ribbon, the coaxial response will consist of two peaks, one over each edge; whereas the coplanar coil will yield a single peak (Profile H).

* It should be noted at this point that Aerodat's definition of the measured ppm unit is related to the primary field sensed in the receiving coil without normalization to the maximum coupled (coaxial configuration). If such normalization were applied to the Aerodat units, the amplitude of the coplanar coil pair would be halved.

Magnetics

The Total Field Magnetic Map shows contours of the total magnetic field, uncorrected for regional variation. Whether an EM anomaly with a magnetic correlation is more likely to be

caused by a sulphide deposit than one without depends on the type of mineralization. An apparent coincidence between an EM and a magnetic anomaly may be caused by a conductor which is also magnetic, or by a conductor which lies in close proximity to a magnetic body. The majority of conductors which are also magnetic are sulphides containing pyrrhoute and/or magnetite. Conductive and magnetic bodies in close association can be, and often are, graphite and magnetite. It is often very difficult to distinguish between these cases. If the conductor is also magnetic, it will usually produce an EM anomaly whose general pattern resembles that of the magnetics. Depending on the magnetic permeability of the conducting body, the amplitude of the inphase EM anomaly will be weakened, and if the conductivity is also weak, the inphase EM anomaly may even be reversed in sign.

The interpretation of contoured aeromagnetic data is a subject on its own involving an array of methods and attitudes. The interpretation of source characteristics for example from total field results is often based on some numerical modelling scheme. The vertical gradient data is more legible in some aspects however and useful inferences about source characteristics can often be read off the contoured VG map.

The zero contour lines in contoured VG data are often sited as a good approximation to the outline of the top of the magnetic source. This only applies to wide (relative to depth of burial) near vertical sources at high magnetic latitudes. It will give an incorrect interpretation in most other cases.

Theoretical profiles of total field and vertical gradient anomalies from tabular sources at a variety of magnetic inclinations are shown in the attached figure. Sources are 10, 50 and 200 m wide. The source-sensor separation is 50 m. The thin line is the total field profile. The thick line is the vertical gradient profile.

The following comments about source geometry apply to contoured vertical gradient data for magnetic inclinations of 70 to 80°.

Outline

Where the VG anomaly has a single sharp peak, the source may be a thin near-vertical tabular source. It may be represented as a magnetic axis or as a tabular source of measurable width - the choice is one of geological preference.

Where the VG anomaly has a broad, flat or inclined top, the source may be a thick tabular source. It may be represented as a thick body where the width is taken from the zero contour lines if the body dips to magnetic north. If the source appears to be dipping to the south (i.e. the VG anomaly is asymmetric), the zero contours are less reliable indicators of outline. The southern most zero contour line should be ignored and the outline taken from the northern zero contour line and the extent of the anomaly peak width.

Dip

A symmetrical vertical gradient response is produced by a body dipping to magnetic north. An asymmetrical response is produced by a body which is vertical or dipping to the south. For southern dips, the southern most zero contour line may be several hundred meters south of the source.

Depth of Burial

The source-sensor separation is about equal to half of the distance between the zero contour lines for thin near-vertical sources. The estimated depth of burial for such sources is this separation minus 50 m. If a variety of VG anomaly widths are seen in an area, use the narrowest width seen to estimate local depths.

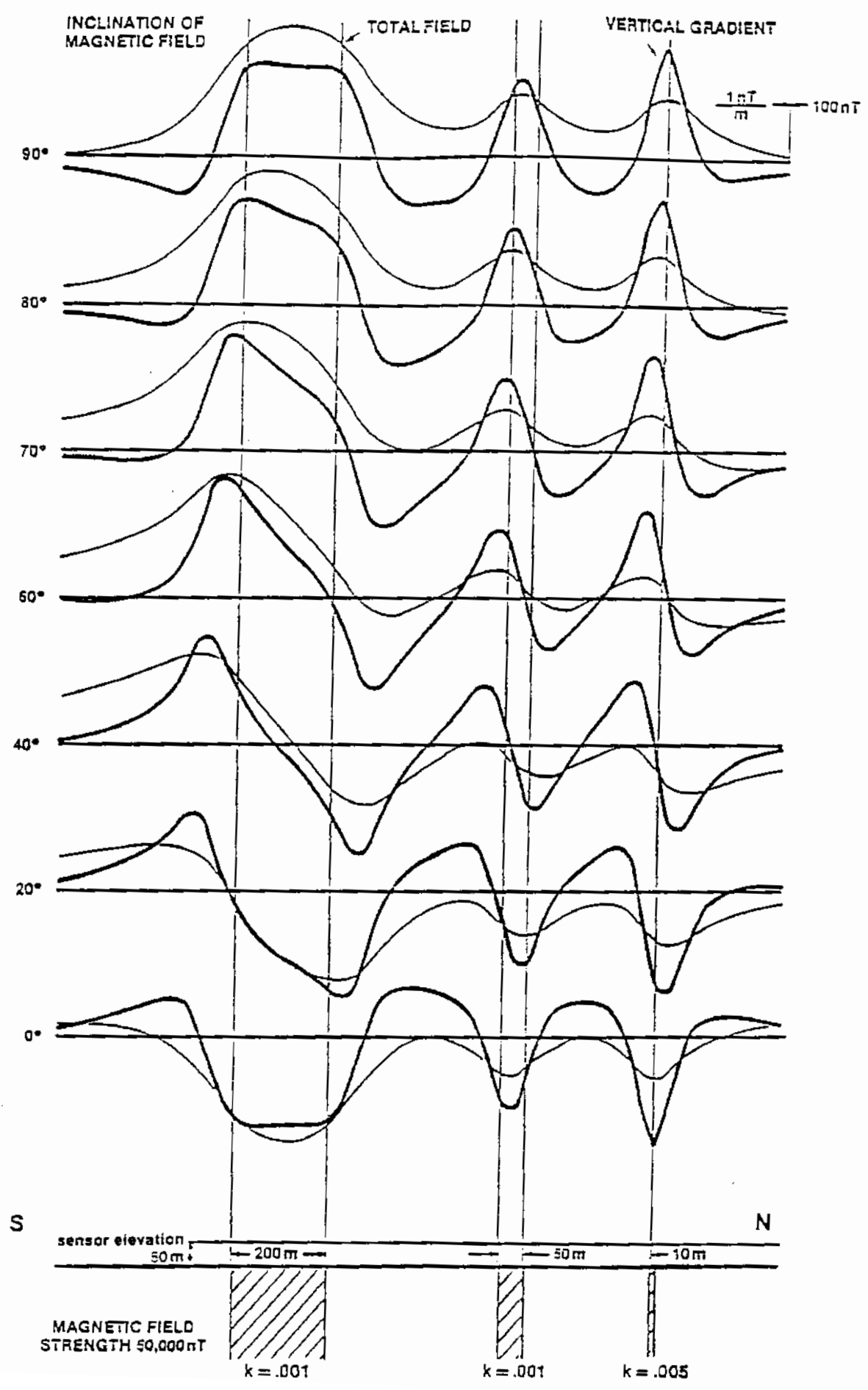
VLF Electromagnetics

The VLF-EM method employs the radiation from powerful military radio transmitters as the primary signals. The magnetic field associated with the primary field is locally horizontal and normal to a line pointing at the transmitter.

The Herz Totem uses three coils in the X, Y, Z configuration to measure the total field and vertical quadrature component from two VLF stations. These stations are designated Line and Ortho. The line station is ideally in a direction from the survey area at right angles to the flight line direction. Conductors normal to the flight line direction point at the line station and are therefore optimally coupled to VLF magnetic fields and in the best situation to gather secondary VLF currents. The ortho station is ideally 90 degrees in azimuth from the line station.

The relatively high frequency of VLF (15-25) kHz provides high response factors for bodies of low conductance. Relatively "disconnected" sulphide ores have been found to produce measurable VLF signals. For the same reason, poor conductors such as sheared contacts, breccia zones, narrow faults, alteration zones and porous flow tops normally produce VLF anomalies. The method can therefore be used effectively for geological mapping. The only relative disadvantage of the method lies in its sensitivity to conductive overburden. In conductive ground to depth of exploration is severely limited.

The effect of strike direction is important in the sense of the relation of the conductor axis relative to the energizing electromagnetic field. A conductor aligned along a radius drawn from a transmitting station will be in a maximum coupled orientation and thereby produce a stronger response than a similar conductor at a different strike angle. Theoretically, it would be possible for a conductor, oriented tangentially to the transmitter to produce no signal. The most obvious effect of the strike angle consideration is that conductors favourably oriented with respect to the transmitter location and also near perpendicular to the flight direction are most clearly rendered and usually dominate the map presentation.



The total field anomaly is an indicator of the existence and position of a conductor. The response will be a maximum over the conductor, without any special filtering, and strongly favour the upper edge of the conductor even in the case of a relatively shallow dip.

Conversely a negative total field anomaly is often seen over local resistivity highs. This is because the VLF field produces electrical currents which flow towards (or away from) the transmitter. These currents are gathered into a conductor and are taken from resistive bodies. The VLF system sees the currents gathered into the conductor as a total field high. It sees the relative absence of secondary currents in the resistor as a total field low.

As noted, VLF anomaly trends show a strong bias towards the VLF transmitter. Structure which is normal to this direction may have no associated VLF anomaly but may be seen as a break or interruption in VLF anomalies. If these structures are of particular interest, maps of the ortho station data may be worthwhile.

Conductive overburden will obscure VLF responses from bedrock sources and may produce low amplitude, broad anomalies which reflect variations in the resistivity of thickness of the overburden.

Extreme topographic relief will produce VLF anomalies which may bear no relationship to variations in electrical conductivity. Deep gullies which are too narrow to have been surveyed at a uniform sensor height often show up as VLF total field lows. Sharp ridges show up as total field highs.

The vertical quadrature component over steeply dipping sheet-like conductor will be a cross-over type response with the cross-over closely associated with the upper edge of the conductor.

The response is a cross-over type due to the fact that it is the vertical rather than total field quadrature component that is measured. The response shape is due largely to geometrical rather than conductivity considerations and the distance between the maximum and minimum on either side of the cross-over is related to target depth. For a given target geometry, the larger this distance the greater the depth.

The vertical quadrature component is rarely presented. Experience has shown the total field to be more sensitive to bedrock conductors and less affected by variations in conductive overburden.

APPENDIX II
ANOMALY LISTINGS

NORANDA EXPLORATION COMPANY LTD. (OMENICA AREA, BRITISH COLUMBIA)

| FLIGHT | LINE | ANOMALY | CATEGORY | AMPLITUDE (PPM) | | CONDUCTOR | | BIRD | | |
|--------|-------|---------|----------|-----------------|-------|-------------------|---------------|----------------|----------|-----------|
| | | | | INPHASE | QUAD. | CTP DEPTH MHOS | DEPTH MTRS | HEIGHT MTRS | | |
| 3 | 10010 | A | 0 | -12.5 | 6.0 | 0.0 | 0 | 22 | 674503.4 | 6273156.0 |
| 3 | 10010 | B | 0 | 2.9 | 45.0 | 0.0 | 0 | 23 | 673421.8 | 6272508.0 |
| 3 | 10010 | C | 0 | -2.0 | 14.0 | 0.0 | 0 | 26 | 673312.8 | 6272440.5 |
| 3 | 10021 | A | 0 | -4.5 | 5.8 | 0.0 | 0 | 28 | 672766.8 | 6271828.0 |
| 3 | 10021 | B | 0 | -4.6 | 11.7 | 0.0 | 0 | 31 | 672959.1 | 6271950.0 |
| 3 | 10021 | C | 0 | 3.8 | 21.8 | 0.0 | 0 | 32 | 673357.6 | 6272239.0 |
| 3 | 10021 | D | 0 | 3.5 | 21.1 | 0.0 | 0 | 30 | 673425.6 | 6272280.0 |
| 3 | 10021 | E | 0 | -8.2 | 6.8 | 0.0 | 0 | 25 | 673590.5 | 6272381.0 |
| 3 | 10030 | A | 0 | 1.0 | 9.6 | 0.0 | 0 | 42 | 673587.6 | 6272086.5 |
| 3 | 10030 | B | 0 | 2.9 | 12.9 | 0.0 | 0 | 42 | 673532.3 | 6272052.0 |
| 3 | 10030 | C | 0 | 3.6 | 11.4 | 0.1 | 0 | 44 | 673458.0 | 6272004.0 |
| 3 | 10040 | A | 0 | -48.1 | 4.8 | 0.0 | 0 | 24 | 672429.6 | 6271110.0 |
| 3 | 10040 | B | 0 | -124.5 | 10.7 | 0.0 | 0 | 21 | 672501.6 | 6271162.0 |
| 3 | 10040 | C | 0 | 6.9 | 28.2 | 0.1 | 0 | 34 | 673506.5 | 6271708.5 |
| 3 | 10040 | D | 0 | 6.7 | 34.6 | 0.0 | 0 | 28 | 673623.5 | 6271778.5 |
| 3 | 10040 | E | 0 | 4.4 | 33.6 | 0.0 | 0 | 26 | 673669.8 | 6271807.5 |
| 3 | 10040 | F | 0 | 1.5 | 33.7 | 0.0 | 0 | 25 | 673721.4 | 6271840.5 |
| 3 | 10050 | A | 0 | -23.2 | 3.0 | 0.0 | 0 | 35 | 675076.0 | 6272393.0 |
| 3 | 10050 | B | 0 | -1.3 | 13.4 | 0.0 | 0 | 38 | 673760.6 | 6271683.0 |
| 3 | 10050 | C | 0 | 3.6 | 16.7 | 0.0 | 0 | 41 | 673660.0 | 6271620.5 |
| 3 | 10050 | D | 0 | 3.7 | 9.5 | 0.1 | 0 | 51 | 673553.3 | 6271554.0 |
| 3 | 10060 | A | 0 | 4.9 | 12.7 | 0.1 | 0 | 45 | 673628.6 | 6271240.5 |
| 3 | 10060 | B | 0 | 0.8 | 12.6 | 0.0 | 0 | 35 | 673752.4 | 6271313.0 |
| 3 | 10060 | C | 0 | -0.5 | 14.6 | 0.0 | 0 | 31 | 673835.2 | 6271359.5 |
| 3 | 10060 | D | 0 | -63.4 | 4.3 | 0.0 | 0 | 8 | 675181.9 | 6272167.5 |
| 3 | 10071 | A | 0 | -0.9 | 7.3 | 0.0 | 0 | 40 | 673810.3 | 6271034.5 |
| 3 | 10071 | B | 0 | 1.1 | 12.3 | 0.0 | 0 | 40 | 673704.4 | 6270973.0 |
| 3 | 10080 | A | 0 | 1.4 | 5.4 | 0.0 | 0 | 64 | 673765.3 | 6270679.0 |
| 3 | 10080 | B | 0 | -1.9 | 6.9 | 0.0 | 0 | 34 | 673919.6 | 6270783.5 |
| 3 | 10080 | C | 0 | -3.7 | 6.7 | 0.0 | 0 | 29 | 674005.8 | 6270844.0 |
| 3 | 10080 | D | 0 | -8.7 | 4.8 | 0.0 | 0 | 25 | 674119.1 | 6270924.0 |
| 3 | 10081 | A | 0 | -4.4 | 5.3 | 0.0 | 0 | 33 | 675985.4 | 6272054.0 |
| 3 | 10081 | B | 0 | -2.8 | 12.9 | 0.0 | 0 | 29 | 676039.4 | 6272089.5 |
| 3 | 10090 | A | 0 | 6.0 | 21.5 | 0.1 | 0 | 35 | 673786.8 | 6270446.0 |
| 3 | 10090 | B | 0 | 3.0 | 13.8 | 0.0 | 0 | 33 | 673695.3 | 6270389.0 |

Estimated depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or overburden effects.

NORANDA EXPLORATION COMPANY LTD. (OMENICA AREA, BRITISH COLUMBIA)

| FLIGHT | LINE | ANOMALY | CATEGORY | AMPLITUDE (PPM) | | CONDUCTOR | | BIRD | HEIGHT | |
|--------|-------|---------|----------|-----------------|-------|-----------|-------|------|----------|-----------|
| | | | | INPHASE | QUAD. | CTP | DEPTH | | | |
| | | | | | | MHOS | MTRS | | | |
| 3 | 10100 | A | 0 | -3.0 | 6.8 | 0.0 | 0 | 36 | 673612.3 | 6270043.5 |
| 3 | 10100 | B | 0 | 1.5 | 8.3 | 0.0 | 0 | 44 | 673712.7 | 6270097.5 |
| 3 | 10100 | C | 0 | 4.0 | 13.7 | 0.1 | 0 | 49 | 673831.2 | 6270162.0 |
| 3 | 10111 | A | 0 | -3.8 | 5.1 | 0.0 | 0 | 33 | 674117.6 | 6270037.5 |
| 3 | 10111 | B | 0 | 2.8 | 20.8 | 0.0 | 0 | 31 | 673907.8 | 6269922.5 |
| 3 | 10111 | C | 0 | 0.7 | 10.1 | 0.0 | 0 | 35 | 673793.5 | 6269858.0 |
| 3 | 10120 | A | 0 | 2.6 | 8.1 | 0.1 | 0 | 43 | 673952.0 | 6269680.0 |
| 3 | 10120 | B | 0 | 2.4 | 5.0 | 0.1 | 15 | 43 | 674206.5 | 6269848.5 |
| 3 | 10130 | A | 0 | -0.8 | 6.1 | 0.0 | 0 | 29 | 674785.9 | 6269880.5 |
| 3 | 10130 | B | 0 | -0.8 | 6.4 | 0.0 | 0 | 24 | 674742.4 | 6269853.5 |
| 3 | 10130 | C | 0 | -0.9 | 6.4 | 0.0 | 0 | 16 | 674693.5 | 6269824.5 |
| 3 | 10130 | D | 0 | -3.7 | 40.5 | 0.0 | 0 | 16 | 674252.1 | 6269567.0 |
| 3 | 10130 | E | 0 | 2.3 | 14.5 | 0.0 | 0 | 31 | 673965.4 | 6269377.0 |
| 3 | 10130 | F | 0 | 0.3 | 6.7 | 0.0 | 0 | 38 | 673831.9 | 6269285.5 |
| 3 | 10141 | A | 0 | 0.7 | 7.5 | 0.0 | 0 | 48 | 673821.1 | 6269060.0 |
| 3 | 10141 | B | 0 | 3.8 | 19.0 | 0.0 | 0 | 30 | 674005.7 | 6269159.0 |
| 3 | 10141 | C | 0 | 2.0 | 12.0 | 0.0 | 0 | 33 | 674123.6 | 6269222.0 |
| 3 | 10141 | D | 0 | 1.9 | 7.9 | 0.0 | 5 | 35 | 674195.8 | 6269262.5 |
| 3 | 10141 | E | 0 | 1.4 | 9.5 | 0.0 | 4 | 28 | 674291.9 | 6269319.0 |
| 3 | 10141 | F | 0 | -1.4 | 5.7 | 0.0 | 0 | 35 | 675066.1 | 6269776.5 |
| 3 | 10150 | A | 0 | -11.5 | 5.1 | 0.0 | 0 | 23 | 676797.5 | 6270465.5 |
| 3 | 10150 | B | 0 | 1.1 | 15.2 | 0.0 | 0 | 28 | 674188.3 | 6268948.0 |
| 3 | 10150 | C | 0 | 3.5 | 17.9 | 0.0 | 0 | 32 | 674004.2 | 6268837.0 |
| 3 | 10150 | D | 0 | 1.8 | 13.3 | 0.0 | 0 | 28 | 673798.1 | 6268712.5 |
| 2 | 10160 | A | 0 | -35.4 | 4.8 | 0.0 | 0 | 17 | 677056.9 | 6270395.5 |
| 2 | 10160 | B | 0 | -2.5 | 16.2 | 0.0 | 0 | 24 | 674187.9 | 6268677.0 |
| 2 | 10160 | C | 0 | 4.1 | 16.4 | 0.0 | 0 | 36 | 674050.2 | 6268596.5 |
| 2 | 10160 | D | 0 | 2.0 | 5.0 | 0.1 | 13 | 42 | 673867.6 | 6268493.5 |
| 2 | 10160 | E | 0 | -41.2 | 4.0 | 0.0 | 0 | 11 | 671195.9 | 6266868.5 |
| 2 | 10160 | F | 0 | 0.0 | 11.9 | 0.0 | 0 | 38 | 669895.7 | 6266078.0 |
| 2 | 10160 | G | 0 | -4.3 | 19.2 | 0.0 | 0 | 17 | 669824.3 | 6266024.0 |
| 2 | 10170 | A | 0 | 0.1 | 6.7 | 0.0 | 0 | 32 | 669980.9 | 6265791.5 |
| 2 | 10170 | B | 0 | 1.6 | 6.7 | 0.0 | 10 | 32 | 670096.0 | 6265868.0 |
| 2 | 10170 | D | 0 | 1.0 | 10.0 | 0.0 | 0 | 41 | 673871.4 | 6268180.5 |
| 2 | 10170 | E | 0 | 0.7 | 9.0 | 0.0 | 0 | 26 | 673955.3 | 6268230.0 |
| 2 | 10170 | C | 0 | -8.9 | 6.3 | 0.0 | 0 | 7 | 670326.3 | 6266042.0 |
| 2 | 10170 | F | 0 | 1.6 | 17.1 | 0.0 | 0 | 31 | 674069.3 | 6268297.5 |

Estimated depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or overburden effects.

NORANDA EXPLORATION COMPANY LTD. (OMENICA AREA, BRITISH COLUMBIA)

| FLIGHT | LINE | ANOMALY | CATEGORY | AMPLITUDE (PPM) | | CONDUCTOR | | BIRD | HEIGHT | | |
|--------|-------|---------|----------|-----------------|-------|-----------|-------|------|----------|-----------|--|
| | | | | INPHASE | QUAD. | CTP | DEPTH | | | | |
| 2 | 10170 | G | 0 | -14.4 | 4.4 | 0.0 | 0 | 22 | 675661.0 | 6269249.0 | |
| 2 | 10180 | A | 0 | -6.1 | 20.2 | 0.0 | 0 | 24 | 674161.6 | 6268046.0 | |
| 2 | 10180 | B | 0 | 2.4 | 9.2 | 0.0 | 0 | 41 | 674077.6 | 6268009.0 | |
| 2 | 10180 | C | 0 | 1.9 | 16.5 | 0.0 | 0 | 29 | 673921.1 | 6267932.5 | |
| 2 | 10180 | D | 0 | 0.3 | 7.6 | 0.0 | 0 | 54 | 671712.6 | 6266587.5 | |
| 2 | 10180 | E | 0 | 0.0 | 11.4 | 0.0 | 0 | 31 | 671425.3 | 6266407.5 | |
| 2 | 10180 | F | 0 | -0.6 | 11.1 | 0.0 | 0 | 34 | 671346.4 | 6266357.5 | |
| 2 | 10190 | A | 0 | -0.6 | 25.0 | 0.0 | 0 | 19 | 673973.2 | 6267683.0 | |
| 2 | 10190 | B | 0 | 10.8 | 23.1 | 0.3 | 1 | 32 | 674159.2 | 6267756.0 | |
| 2 | 10190 | C | 0 | 3.0 | 9.6 | 0.1 | 2 | 38 | 674250.4 | 6267817.5 | |
| 2 | 10200 | A | 0 | -2.2 | 7.2 | 0.0 | 0 | 38 | 677357.2 | 6269402.5 | |
| 2 | 10200 | B | 0 | 3.0 | 9.7 | 0.1 | 0 | 44 | 674304.6 | 6267560.5 | |
| 2 | 10200 | C | 0 | 8.5 | 22.2 | 0.2 | 0 | 53 | 674196.6 | 6267504.5 | |
| 2 | 10200 | D | 0 | 6.3 | 11.9 | 0.3 | 2 | 41 | 674012.6 | 6267400.0 | |
| 2 | 10200 | E | 0 | -4.0 | 9.3 | 0.0 | 0 | 18 | 671572.4 | 6265902.0 | |
| 2 | 10200 | F | 0 | -0.3 | 12.4 | 0.0 | 0 | 24 | 671425.8 | 6265820.5 | |
| 2 | 10200 | G | 0 | -1.7 | 24.1 | 0.0 | 0 | 24 | 671292.4 | 6265741.5 | |
| 2 | 10200 | H | 0 | -2.4 | 11.7 | 0.0 | 0 | 23 | 671042.8 | 6265591.0 | |
| 2 | 10210 | A | 0 | -1.9 | 39.8 | 0.0 | 0 | 23 | 673502.6 | 6266779.5 | |
| 2 | 10210 | B | 0 | 3.0 | 31.4 | 0.0 | 0 | 25 | 673981.0 | 6267133.5 | |
| 2 | 10210 | C | 0 | 4.8 | 21.4 | 0.0 | 0 | 29 | 674048.4 | 6267175.5 | |
| 2 | 10210 | D | 0 | 6.3 | 13.3 | 0.2 | 4 | 37 | 674167.6 | 6267243.0 | |
| 2 | 10210 | E | 0 | 4.2 | 11.5 | 0.1 | 0 | 41 | 674343.5 | 6267343.0 | |
| 2 | 10210 | F | 0 | -2.7 | 3.6 | 0.0 | 0 | 39 | 676753.8 | 6268740.0 | |
| 2 | 10210 | G | 0 | -0.8 | 3.4 | 0.0 | 0 | 51 | 677491.8 | 6269174.5 | |
| 2 | 10210 | H | 0 | -24.4 | 7.4 | 0.0 | 0 | 8 | 677788.1 | 6269336.0 | |
| 2 | 10210 | J | 0 | -32.9 | 9.7 | 0.0 | 0 | 13 | 677853.3 | 6269368.5 | |
| 1 | 10220 | A | 0 | -0.7 | 4.4 | 0.0 | 0 | 37 | 676974.4 | 6268626.5 | |
| 1 | 10220 | B | 0 | -1.0 | 5.1 | 0.0 | 0 | 37 | 676937.0 | 6268605.0 | |
| 1 | 10220 | C | 0 | 4.1 | 52.7 | 0.0 | 0 | 20 | 674410.0 | 6267006.0 | |
| 1 | 10220 | D | 0 | 16.8 | 39.1 | 0.4 | 0 | 37 | 674220.8 | 6266904.0 | |
| 1 | 10220 | E | 0 | -94.4 | 7.7 | 0.0 | 0 | 15 | 672837.8 | 6266101.5 | |
| 1 | 10220 | F | 0 | -54.8 | 6.6 | 0.0 | 0 | 20 | 672718.0 | 6266026.5 | |
| 1 | 10220 | G | 0 | -7.1 | 5.3 | 0.0 | 0 | 17 | 670902.3 | 6264921.0 | |
| 1 | 10230 | A | 0 | 0.0 | 5.8 | 0.0 | 0 | 42 | 673958.0 | 6266458.0 | |
| 1 | 10230 | B | 0 | 0.9 | 3.8 | 0.0 | 0 | 55 | 674126.4 | 6266584.5 | |
| 1 | 10230 | C | 0 | 3.2 | 5.3 | 0.2 | 0 | 63 | 674255.4 | 6266681.0 | |
| 1 | 10230 | D | 0 | -70.6 | 5.9 | 0.0 | 0 | 17 | 675071.8 | 6267157.5 | |
| 1 | 10230 | E | 0 | -94.5 | 10.2 | 0.0 | 0 | 22 | 677939.7 | 6268878.5 | |

Estimated depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or overburden effects.

NORANDA EXPLORATION COMPANY LTD. (OMENICA AREA, BRITISH COLUMBIA)

| FLIGHT | LINE | ANOMALY | CATEGORY | AMPLITUDE (PPM) | | CONDUCTOR | | BIRD | | |
|--------|-------|---------|----------|-----------------|-------|-------------------|---------------|----------------|----------|-----------|
| | | | | INPHASE | QUAD. | CTP DEPTH MHOS | DEPTH MTRS | HEIGHT MTRS | | |
| 1 | 10240 | A | 0 | 4.7 | 23.3 | 0.0 | 1 | 25 | 674532.9 | 6266566.0 |
| 1 | 10240 | B | 0 | 7.8 | 24.8 | 0.1 | 0 | 40 | 674457.0 | 6266522.5 |
| 1 | 10240 | C | 0 | 6.9 | 10.2 | 0.5 | 6 | 43 | 674348.5 | 6266456.0 |
| 1 | 10240 | D | 0 | 13.6 | 34.6 | 0.3 | 0 | 32 | 674187.6 | 6266359.0 |
| 1 | 10240 | E | 0 | 22.5 | 51.0 | 0.4 | 0 | 33 | 674137.4 | 6266328.5 |
| 1 | 10240 | F | 0 | 5.5 | 21.0 | 0.1 | 0 | 31 | 673930.5 | 6266197.0 |
| 1 | 10240 | G | 0 | 1.1 | 6.2 | 0.0 | 0 | 49 | 671242.5 | 6264616.5 |
| 1 | 10240 | H | 0 | 1.7 | 9.2 | 0.0 | 0 | 39 | 671112.1 | 6264521.5 |
| 1 | 10240 | J | 0 | -0.4 | 9.3 | 0.0 | 0 | 27 | 670753.8 | 6264267.0 |
| 1 | 10250 | A | 0 | -36.4 | 6.9 | 0.0 | 0 | 18 | 672925.8 | 6265330.0 |
| 1 | 10250 | B | 0 | -1.5 | 5.0 | 0.0 | 0 | 29 | 673170.1 | 6265481.5 |
| 1 | 10250 | C | 0 | 6.3 | 19.7 | 0.1 | 0 | 36 | 674005.1 | 6266003.0 |
| 1 | 10250 | D | 0 | 2.4 | 10.9 | 0.0 | 0 | 37 | 674080.9 | 6266042.0 |
| 1 | 10250 | E | 0 | 2.1 | 7.4 | 0.0 | 8 | 35 | 674248.1 | 6266127.5 |
| 1 | 10250 | F | 0 | 2.5 | 8.5 | 0.0 | 6 | 35 | 674314.8 | 6266162.0 |
| 1 | 10250 | G | 0 | 7.3 | 20.9 | 0.2 | 0 | 33 | 674528.3 | 6266273.0 |
| 1 | 10250 | H | 0 | 5.9 | 16.8 | 0.1 | 0 | 34 | 674649.9 | 6266341.0 |
| 1 | 10250 | J | 0 | 3.5 | 10.7 | 0.1 | 6 | 33 | 674720.3 | 6266383.5 |
| 1 | 10250 | K | 0 | -2.0 | 6.7 | 0.0 | 0 | 25 | 675035.3 | 6266574.5 |
| 1 | 10251 | A | 0 | -13.1 | 26.4 | 0.0 | 0 | 29 | 678287.9 | 6268456.0 |
| 1 | 10260 | A | 0 | -26.5 | 7.2 | 0.0 | 0 | 15 | 676759.6 | 6267277.0 |
| 1 | 10260 | B | 0 | -6.3 | 7.5 | 0.0 | 0 | 31 | 676654.0 | 6267207.5 |
| 1 | 10260 | C | 0 | -4.5 | 3.9 | 0.0 | 0 | 28 | 676498.5 | 6267108.5 |
| 1 | 10260 | D | 0 | 3.8 | 8.0 | 0.2 | 0 | 49 | 674827.8 | 6266127.5 |
| 1 | 10260 | E | 0 | 1.4 | 6.6 | 0.0 | 0 | 49 | 674712.3 | 6266054.0 |
| 1 | 10260 | F | 0 | 1.3 | 11.0 | 0.0 | 0 | 35 | 674554.0 | 6265953.0 |
| 1 | 10260 | G | 0 | 3.4 | 9.3 | 0.1 | 8 | 35 | 674049.1 | 6265607.0 |
| 1 | 10260 | H | 0 | -1.3 | 7.0 | 0.0 | 0 | 33 | 671506.4 | 6264153.0 |
| 1 | 10260 | J | 0 | 0.6 | 10.4 | 0.0 | 0 | 29 | 671348.8 | 6264051.0 |
| 1 | 10260 | K | 0 | -0.1 | 12.1 | 0.0 | 0 | 25 | 670999.2 | 6263866.5 |
| 1 | 10270 | A | 0 | 0.5 | 6.0 | 0.0 | 0 | 31 | 671642.3 | 6263928.5 |
| 1 | 10270 | B | 0 | -0.5 | 6.8 | 0.0 | 0 | 33 | 673941.4 | 6265300.0 |
| 1 | 10270 | C | 0 | -1.1 | 14.2 | 0.0 | 0 | 31 | 674682.1 | 6265778.0 |
| 1 | 10270 | D | 0 | 3.1 | 8.7 | 0.1 | 4 | 40 | 674961.2 | 6265945.0 |
| 1 | 10271 | A | 0 | -44.9 | 5.1 | 0.0 | 0 | 11 | 677747.7 | 6267524.5 |
| 1 | 10271 | B | 0 | -41.0 | 4.7 | 0.0 | 0 | 19 | 677849.4 | 6267584.5 |
| 1 | 10280 | A | 0 | 6.4 | 11.6 | 0.3 | 0 | 48 | 675167.5 | 6265770.5 |
| 1 | 10280 | B | 0 | 4.4 | 7.7 | 0.3 | 2 | 50 | 675045.4 | 6265694.5 |

Estimated depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or overburden effects.

NORANDA EXPLORATION COMPANY LTD. (OMENICA AREA, BRITISH COLUMBIA)

| FLIGHT | LINE | ANOMALY | CATEGORY | AMPLITUDE (PPM) | | CONDUCTOR | | BIRD | | |
|--------|-------|---------|----------|-----------------|-------|-----------|------------|-------------|----------|-----------|
| | | | | INPHASE | QUAD. | CTP MHOS | DEPTH MTRS | HEIGHT MTRS | | |
| 1 | 10280 | C | 0 | 1.3 | 9.3 | 0.0 | 5 | 27 | 674224.7 | 6265186.0 |
| 1 | 10280 | D | 0 | 2.3 | 10.9 | 0.0 | 9 | 25 | 674113.4 | 6265118.0 |
| 1 | 10280 | E | 0 | 0.9 | 6.9 | 0.0 | 2 | 32 | 673976.2 | 6265035.5 |
| 1 | 10290 | A | 0 | -0.7 | 8.2 | 0.0 | 0 | 34 | 672671.4 | 6263938.5 |
| 1 | 10290 | B | 0 | -7.5 | 6.3 | 0.0 | 0 | 26 | 672882.5 | 6264061.5 |
| 1 | 10290 | C | 0 | -5.6 | 6.2 | 0.0 | 0 | 32 | 672962.7 | 6264109.0 |
| 1 | 10290 | D | 0 | 0.2 | 6.8 | 0.0 | 0 | 36 | 674026.9 | 6264770.5 |
| 1 | 10290 | E | 0 | 1.8 | 15.4 | 0.0 | 0 | 36 | 674279.1 | 6264930.0 |
| 1 | 10290 | F | 0 | 0.6 | 9.9 | 0.0 | 0 | 41 | 674419.3 | 6265015.0 |
| 1 | 10290 | G | 0 | 21.8 | 30.1 | 0.8 | 0 | 37 | 675316.3 | 6265554.0 |
| 1 | 10290 | H | 1 | 24.1 | 31.2 | 1.0 | 0 | 40 | 675409.8 | 6265610.0 |
| 1 | 10290 | J | 0 | 19.3 | 29.0 | 0.7 | 0 | 40 | 675480.1 | 6265652.0 |
| 1 | 10290 | K | 0 | 2.3 | 12.9 | 0.0 | 0 | 35 | 675993.3 | 6265940.5 |
| 1 | 10290 | M | 0 | -13.0 | 3.0 | 0.0 | 0 | 29 | 677727.3 | 6266985.0 |
| 1 | 10290 | N | 0 | -14.8 | 5.4 | 0.0 | 0 | 30 | 677901.4 | 6267093.5 |
| 1 | 10300 | A | 0 | 0.0 | 5.1 | 0.0 | 0 | 30 | 678374.2 | 6267070.5 |
| 1 | 10300 | B | 0 | 2.4 | 7.1 | 0.1 | 13 | 33 | 677211.8 | 6266392.0 |
| 1 | 10300 | C | 0 | 3.7 | 12.2 | 0.1 | 3 | 34 | 676799.9 | 6266161.5 |
| 1 | 10300 | D | 0 | -14.6 | 16.0 | 0.0 | 0 | 34 | 676416.6 | 6265946.5 |
| 1 | 10300 | E | 0 | -14.2 | 17.4 | 0.0 | 0 | 37 | 676313.4 | 6265885.5 |
| 1 | 10300 | F | 0 | 14.5 | 23.9 | 0.5 | 0 | 40 | 675693.1 | 6265496.5 |
| 1 | 10300 | G | 0 | 13.5 | 27.6 | 0.4 | 0 | 35 | 675601.3 | 6265439.0 |
| 1 | 10300 | H | 0 | 2.2 | 13.4 | 0.0 | 0 | 32 | 674716.2 | 6264919.5 |
| 1 | 10300 | J | 0 | 4.3 | 20.4 | 0.0 | 0 | 28 | 674608.1 | 6264853.0 |
| 1 | 10300 | K | 0 | 6.6 | 28.7 | 0.1 | 0 | 27 | 674499.4 | 6264787.0 |
| 1 | 10300 | M | 0 | 3.3 | 14.0 | 0.0 | 4 | 28 | 674406.3 | 6264730.0 |
| 1 | 10300 | N | 0 | 2.1 | 6.9 | 0.0 | 12 | 33 | 674187.4 | 6264593.5 |
| 1 | 10300 | O | 0 | 2.3 | 9.2 | 0.0 | 5 | 33 | 674120.5 | 6264549.5 |
| 2 | 10310 | A | 0 | 0.0 | 5.5 | 0.0 | 0 | 29 | 678400.4 | 6266804.5 |
| 2 | 10310 | B | 0 | 4.3 | 25.0 | 0.0 | 0 | 29 | 677194.9 | 6266069.0 |
| 2 | 10310 | C | 0 | 4.9 | 29.0 | 0.0 | 0 | 29 | 677109.1 | 6266018.0 |
| 2 | 10310 | D | 0 | 6.4 | 28.5 | 0.1 | 0 | 27 | 676991.6 | 6265949.5 |
| 2 | 10310 | E | 0 | 2.6 | 8.4 | 0.0 | 2 | 40 | 675960.6 | 6265386.0 |
| 2 | 10310 | F | 0 | 10.2 | 16.2 | 0.5 | 1 | 40 | 675861.4 | 6265330.0 |
| 2 | 10310 | G | 0 | 10.2 | 15.6 | 0.5 | 0 | 42 | 675785.0 | 6265285.5 |
| 2 | 10320 | A | 0 | 5.6 | 10.5 | 0.3 | 10 | 36 | 675986.5 | 6265075.5 |
| 2 | 10320 | B | 0 | 10.2 | 17.4 | 0.4 | 5 | 34 | 676062.1 | 6265118.5 |
| 2 | 10320 | C | 1 | 30.5 | 38.8 | 1.1 | 0 | 31 | 676186.3 | 6265190.0 |
| 2 | 10320 | D | 0 | 21.8 | 29.4 | 0.9 | 3 | 31 | 676249.6 | 6265227.0 |
| 2 | 10320 | E | 0 | 3.0 | 15.2 | 0.0 | 0 | 31 | 676369.6 | 6265299.0 |
| 2 | 10320 | F | 0 | 7.2 | 25.7 | 0.1 | 0 | 30 | 676426.6 | 6265334.0 |

Estimated depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or overburden effects.

NORANDA EXPLORATION COMPANY LTD. (OMENICA AREA, BRITISH COLUMBIA)

| FLIGHT | LINE | ANOMALY | CATEGORY | AMPLITUDE (PPM) | | CONDUCTOR | | BIRD | HEIGHT | |
|--------|-------|---------|----------|-----------------|-------|-----------|------|------|----------|-----------|
| | | | | INPHASE | QUAD. | CTP DEPTH | MTRS | | | |
| 2 | 10320 | G | 0 | 3.9 | 12.4 | 0.1 | 0 | 44 | 677312.6 | 6265855.0 |
| 2 | 10320 | H | 0 | -0.7 | 8.3 | 0.0 | 0 | 35 | 678355.2 | 6266437.0 |
| 2 | 10330 | A | 0 | -3.0 | 7.6 | 0.0 | 0 | 28 | 678460.3 | 6266294.0 |
| 2 | 10330 | B | 0 | -3.4 | 5.5 | 0.0 | 0 | 37 | 678376.6 | 6266245.5 |
| 2 | 10330 | C | 0 | -0.3 | 12.3 | 0.0 | 0 | 27 | 677777.5 | 6265881.5 |
| 2 | 10330 | D | 0 | -4.0 | 16.2 | 0.0 | 0 | 18 | 677666.8 | 6265809.5 |
| 2 | 10330 | E | 0 | 5.6 | 52.9 | 0.0 | 0 | 24 | 677425.3 | 6265652.0 |
| 2 | 10330 | F | 0 | 5.6 | 19.3 | 0.1 | 0 | 44 | 676625.4 | 6265194.0 |
| 2 | 10330 | G | 1 | 37.1 | 37.0 | 1.6 | 1 | 32 | 676392.0 | 6265047.0 |
| 2 | 10330 | H | 0 | 18.6 | 35.8 | 0.5 | 0 | 37 | 676065.1 | 6264835.5 |
| 2 | 10330 | J | 0 | 26.2 | 48.8 | 0.6 | 0 | 36 | 675986.3 | 6264784.5 |
| 2 | 10330 | K | 0 | 17.9 | 46.5 | 0.3 | 0 | 32 | 675918.3 | 6264740.0 |
| 2 | 10330 | M | 0 | 17.9 | 56.8 | 0.2 | 0 | 27 | 675838.9 | 6264687.5 |
| 2 | 10330 | N | 0 | 16.4 | 39.0 | 0.3 | 0 | 28 | 675793.6 | 6264658.0 |
| 2 | 10330 | O | 0 | -2.1 | 13.6 | 0.0 | 0 | 24 | 675512.8 | 6264479.0 |
| 2 | 10330 | P | 0 | -0.7 | 17.5 | 0.0 | 0 | 25 | 675442.1 | 6264436.5 |
| 2 | 10340 | A | 0 | 5.1 | 17.5 | 0.1 | 0 | 46 | 675572.9 | 6264264.5 |
| 2 | 10340 | B | 0 | 1.5 | 24.2 | 0.0 | 0 | 36 | 675640.7 | 6264307.5 |
| 2 | 10340 | C | 0 | 1.1 | 12.7 | 0.0 | 0 | 36 | 675703.9 | 6264346.5 |
| 2 | 10340 | D | 0 | 5.6 | 12.4 | 0.2 | 3 | 38 | 675828.8 | 6264423.0 |
| 2 | 10340 | E | 0 | 8.3 | 17.6 | 0.3 | 0 | 37 | 675981.3 | 6264512.0 |
| 2 | 10340 | F | 0 | 6.8 | 15.3 | 0.2 | 1 | 37 | 676060.4 | 6264557.5 |
| 2 | 10340 | G | 0 | 5.6 | 18.5 | 0.1 | 0 | 32 | 676456.6 | 6264783.5 |
| 2 | 10340 | H | 1 | 22.0 | 25.3 | 1.1 | 1 | 36 | 676688.0 | 6264931.5 |
| 2 | 10340 | J | 0 | 7.2 | 14.3 | 0.3 | 1 | 39 | 676814.7 | 6265019.0 |
| 2 | 10340 | K | 0 | 3.0 | 12.3 | 0.0 | 0 | 61 | 677524.7 | 6265434.0 |
| 2 | 10340 | M | 0 | 2.2 | 23.6 | 0.0 | 0 | 21 | 677876.8 | 6265632.5 |
| 2 | 10351 | A | 0 | -57.9 | 13.4 | 0.0 | 0 | 11 | 678166.7 | 6265554.5 |
| 2 | 10351 | B | 0 | 2.3 | 14.1 | 0.0 | 0 | 48 | 677662.1 | 6265237.0 |
| 2 | 10351 | C | 1 | 14.3 | 14.7 | 1.1 | 4 | 41 | 677115.9 | 6264832.0 |
| 2 | 10351 | D | 0 | 16.1 | 20.3 | 0.8 | 6 | 33 | 677041.1 | 6264786.0 |
| 2 | 10351 | E | 0 | 3.2 | 9.5 | 0.1 | 11 | 30 | 676660.4 | 6264552.0 |
| 2 | 10351 | F | 0 | 3.2 | 14.6 | 0.0 | 5 | 26 | 676344.4 | 6264377.0 |
| 2 | 10351 | G | 0 | 1.9 | 11.6 | 0.0 | 3 | 28 | 675985.4 | 6264185.0 |
| 2 | 10351 | H | 0 | 7.4 | 19.4 | 0.2 | 0 | 42 | 675703.3 | 6264014.5 |
| 2 | 10351 | J | 0 | 8.8 | 19.0 | 0.3 | 0 | 37 | 675627.5 | 6263967.0 |
| 2 | 10360 | A | 0 | 1.1 | 12.3 | 0.0 | 0 | 40 | 676335.5 | 6264132.5 |
| 2 | 10360 | B | 0 | 2.6 | 11.9 | 0.0 | 0 | 49 | 676478.6 | 6264211.0 |
| 2 | 10362 | A | 0 | 0.9 | 3.7 | 0.0 | 18 | 35 | 678276.1 | 6265289.0 |
| 2 | 10362 | B | 0 | 0.4 | 3.6 | 0.0 | 11 | 30 | 678317.9 | 6265310.0 |

Estimated depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or overburden effects.

NORANDA EXPLORATION COMPANY LTD. (OMENICA AREA, BRITISH COLUMBIA)

| FLIGHT | LINE | ANOMALY | CATEGORY | AMPLITUDE (PPM) | | CONDUCTOR | | BIRD | | | |
|--------|-------|---------|----------|-----------------|-------|-----------|-------|--------|----------|-----------|--|
| | | | | INPHASE | QUAD. | CTP | DEPTH | HEIGHT | HEIGHT | | |
| | | | | | | MHOS | MTRS | MTRS | | | |
| 2 | 10372 | A | 0 | -15.9 | 4.1 | 0.0 | 0 | 20 | 678807.3 | 6265205.0 | |
| 2 | 10373 | A | 0 | 7.6 | 7.8 | 0.8 | 10 | 47 | 677089.1 | 6264265.0 | |
| 2 | 10374 | A | 0 | 0.3 | 12.6 | 0.0 | 0 | 37 | 676965.0 | 6264150.0 | |
| 2 | 10374 | B | 0 | 0.0 | 9.9 | 0.0 | 0 | 23 | 676828.0 | 6264069.5 | |
| 2 | 10374 | C | 0 | 2.2 | 20.3 | 0.0 | 0 | 36 | 676674.9 | 6263986.5 | |
| 2 | 10374 | D | 0 | 3.6 | 19.8 | 0.0 | 0 | 36 | 676622.1 | 6263958.0 | |
| 2 | 10374 | E | 1 | 29.2 | 31.5 | 1.3 | 0 | 50 | 676069.8 | 6263659.5 | |
| 4 | 10400 | A | 0 | 1.8 | 12.5 | 0.0 | 7 | 22 | 676743.1 | 6263221.0 | |
| 4 | 10400 | B | 1 | 5.3 | 2.8 | 1.9 | 0 | 116 | 677471.1 | 6263656.5 | |
| 4 | 10400 | C | 0 | 3.7 | 5.1 | 0.4 | 8 | 55 | 677720.4 | 6263768.5 | |
| 6 | 10410 | A | 0 | 4.6 | 23.5 | 0.0 | 2 | 23 | 677901.4 | 6263590.0 | |
| 6 | 10410 | B | 0 | 4.4 | 11.4 | 0.1 | 18 | 22 | 677815.1 | 6263549.0 | |
| 6 | 10410 | C | 0 | 3.9 | 12.1 | 0.1 | 21 | 17 | 677570.4 | 6263397.5 | |
| 6 | 10410 | D | 0 | 6.4 | 14.5 | 0.2 | 5 | 34 | 676990.4 | 6263090.0 | |
| 6 | 10410 | E | 0 | 4.2 | 10.0 | 0.2 | 12 | 31 | 676869.3 | 6263015.5 | |
| 6 | 10410 | F | 0 | 5.3 | 10.1 | 0.3 | 0 | 47 | 676766.9 | 6262944.5 | |
| 6 | 10420 | A | 0 | 1.0 | 10.2 | 0.0 | 0 | 37 | 676603.2 | 6262489.0 | |
| 6 | 10420 | B | 0 | 0.7 | 10.0 | 0.0 | 0 | 29 | 676681.9 | 6262530.0 | |
| 6 | 10420 | C | 0 | 1.6 | 16.9 | 0.0 | 0 | 29 | 676840.8 | 6262618.0 | |
| 6 | 10420 | D | 0 | 2.2 | 13.6 | 0.0 | 0 | 40 | 676916.7 | 6262665.5 | |
| 6 | 10420 | E | 0 | 9.7 | 26.7 | 0.2 | 0 | 42 | 677081.4 | 6262781.5 | |
| 6 | 10420 | F | 0 | 7.8 | 17.4 | 0.3 | 3 | 33 | 677173.6 | 6262849.0 | |
| 6 | 10420 | G | 0 | 4.9 | 15.2 | 0.1 | 0 | 53 | 677254.9 | 6262905.5 | |
| 6 | 10420 | H | 0 | 1.3 | 15.8 | 0.0 | 0 | 29 | 677336.8 | 6262956.5 | |
| 6 | 10420 | J | 0 | 3.4 | 10.9 | 0.1 | 16 | 23 | 677545.7 | 6263072.5 | |
| 6 | 10420 | K | 0 | -7.8 | 14.2 | 0.0 | 0 | 28 | 677891.6 | 6263284.0 | |
| 6 | 10420 | M | 0 | -9.7 | 12.5 | 0.0 | 0 | 28 | 677930.1 | 6263304.0 | |
| 6 | 10420 | N | 0 | 0.0 | 12.5 | 0.0 | 0 | 29 | 678121.3 | 6263405.5 | |
| 4 | 10431 | A | 0 | -14.4 | 3.9 | 0.0 | 0 | 20 | 680588.7 | 6264597.5 | |
| 4 | 10440 | A | 0 | 9.8 | 18.4 | 0.4 | 4 | 33 | 676745.9 | 6262041.5 | |
| 4 | 10440 | B | 0 | 11.1 | 21.7 | 0.4 | 2 | 33 | 676853.2 | 6262100.0 | |
| 4 | 10440 | C | 0 | 0.3 | 4.1 | 0.0 | 0 | 43 | 677966.5 | 6262763.5 | |
| 4 | 10440 | D | 0 | -0.2 | 6.0 | 0.0 | 0 | 33 | 678090.1 | 6262841.0 | |
| 4 | 10452 | A | 0 | 1.9 | 8.1 | 0.0 | 5 | 34 | 678071.1 | 6262539.0 | |
| 4 | 10452 | B | 0 | 3.4 | 15.3 | 0.0 | 2 | 29 | 678005.8 | 6262500.5 | |
| 4 | 10452 | C | 0 | 3.7 | 10.3 | 0.1 | 16 | 25 | 677909.3 | 6262444.5 | |

Estimated depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or overburden effects.

NORANDA EXPLORATION COMPANY LTD. (OMENICA AREA, BRITISH COLUMBIA)

| FLIGHT | LINE | ANOMALY | CATEGORY | AMPLITUDE (PPM) | | CONDUCTOR | | BIRD | | |
|--------|-------|---------|----------|-----------------|-------|-----------|--------|------|----------|-----------|
| | | | | INPHASE | QUAD. | CTP DEPTH | HEIGHT | MHOS | MTRS | MTRS |
| 4 | 10452 | D | 0 | 1.7 | 11.0 | 0.0 | 9 | 22 | 677692.4 | 6262309.0 |
| 4 | 10452 | E | 0 | 21.6 | 42.1 | 0.5 | 0 | 39 | 677123.6 | 6261935.0 |
| 4 | 10452 | F | 0 | 16.1 | 27.5 | 0.5 | 0 | 42 | 677055.8 | 6261897.0 |
| 4 | 10452 | G | 0 | 11.6 | 20.6 | 0.4 | 0 | 39 | 676964.3 | 6261848.0 |
| 4 | 10460 | A | 0 | 6.0 | 7.9 | 0.5 | 0 | 63 | 677103.4 | 6261685.0 |
| 4 | 10460 | B | 0 | 5.2 | 10.8 | 0.2 | 0 | 63 | 677236.0 | 6261761.5 |
| 5 | 10472 | A | 0 | 3.0 | 9.4 | 0.1 | 15 | 26 | 677697.8 | 6261705.5 |
| 5 | 10472 | B | 0 | 5.2 | 18.3 | 0.1 | 0 | 32 | 677596.4 | 6261636.0 |
| 5 | 10472 | C | 0 | 5.4 | 24.9 | 0.0 | 1 | 24 | 677452.6 | 6261543.5 |
| 5 | 10472 | D | 0 | 5.2 | 29.5 | 0.0 | 0 | 26 | 677365.1 | 6261490.0 |
| 5 | 10472 | E | 0 | 4.7 | 20.9 | 0.0 | 0 | 27 | 677260.1 | 6261427.5 |
| 5 | 10472 | F | 0 | 4.6 | 9.7 | 0.2 | 2 | 43 | 677139.7 | 6261356.5 |
| 5 | 10530 | A | 0 | -849.6 | 8.7 | 0.0 | 0 | 6 | 681477.2 | 6262232.5 |
| 5 | 10530 | B | 0 | -493.3 | 6.1 | 0.0 | 0 | 17 | 681439.9 | 6262202.0 |
| 5 | 10530 | C | 0 | -156.1 | 2.9 | 0.0 | 0 | 38 | 681381.4 | 6262157.0 |
| 5 | 10530 | D | 0 | 2.2 | 6.1 | 0.1 | 11 | 39 | 679404.9 | 6261023.5 |
| 5 | 10530 | E | 0 | 1.4 | 7.7 | 0.0 | 9 | 28 | 678794.6 | 6260642.5 |
| 5 | 10530 | F | 0 | 1.4 | 8.1 | 0.0 | 1 | 35 | 678667.6 | 6260577.5 |
| 5 | 10530 | G | 0 | 1.1 | 6.8 | 0.0 | 4 | 33 | 678584.8 | 6260535.5 |
| 5 | 10540 | A | 0 | 14.2 | 54.6 | 0.1 | 0 | 37 | 678817.1 | 6260345.5 |
| 5 | 10540 | B | 0 | -2.6 | 8.8 | 0.0 | 0 | 22 | 679140.9 | 6260570.0 |
| 5 | 10540 | C | 0 | -1.9 | 8.9 | 0.0 | 0 | 23 | 679272.1 | 6260659.5 |
| 5 | 10540 | D | 0 | -1.4 | 11.0 | 0.0 | 0 | 28 | 679423.0 | 6260744.0 |
| 5 | 10540 | E | 0 | -0.4 | 8.0 | 0.0 | 0 | 35 | 679622.1 | 6260850.0 |
| 5 | 10540 | F | 0 | -0.1 | 14.7 | 0.0 | 0 | 22 | 680674.5 | 6261452.0 |
| 6 | 10550 | A | 0 | -9.2 | 4.8 | 0.0 | 0 | 35 | 680862.8 | 6261316.5 |
| 6 | 10550 | B | 0 | 5.6 | 19.1 | 0.1 | 13 | 18 | 679100.0 | 6260218.0 |
| 6 | 10550 | C | 0 | 8.6 | 26.5 | 0.2 | 7 | 21 | 679043.5 | 6260177.0 |
| 6 | 10550 | D | 0 | 5.5 | 24.1 | 0.0 | 9 | 17 | 678987.0 | 6260136.5 |
| 6 | 10560 | A | 0 | 0.0 | 8.4 | 0.0 | 0 | 35 | 679139.6 | 6259956.5 |
| 6 | 10570 | A | 0 | -305.4 | 12.2 | 0.0 | 0 | 18 | 681967.6 | 6261360.5 |
| 6 | 10570 | B | 0 | 1.7 | 7.8 | 0.0 | 5 | 34 | 679374.8 | 6259839.5 |
| 6 | 10570 | C | 0 | 1.7 | 7.2 | 0.0 | 4 | 37 | 679182.5 | 6259725.5 |
| 6 | 10580 | A | 0 | 0.3 | 7.2 | 0.0 | 0 | 47 | 679892.8 | 6259833.0 |
| 6 | 10581 | A | 0 | -59.7 | 4.4 | 0.0 | 0 | 12 | 682036.0 | 6261108.0 |
| 6 | 10590 | A | 0 | -2.3 | 6.8 | 0.0 | 0 | 38 | 680820.6 | 6260135.5 |

Estimated depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or overburden effects.

NORANDA EXPLORATION COMPANY LTD. (OMENICA AREA, BRITISH COLUMBIA)

| FLIGHT | LINE | ANOMALY | CATEGORY | AMPLITUDE (PPM) | | CONDUCTOR | | BIRD | | |
|--------|-------|---------|----------|-----------------|-------|-----------|--------|------|----------|-----------|
| | | | | INPHASE | QUAD. | CTP DEPTH | HEIGHT | MHOS | MTRS | MTRS |
| 6 | 10590 | B | 0 | 0.0 | 9.7 | 0.0 | 0 | 47 | 680668.4 | 6260037.5 |
| 6 | 10590 | C | 0 | -3.4 | 8.1 | 0.0 | 0 | 41 | 680606.1 | 6259999.5 |
| 6 | 10590 | D | 0 | -2.8 | 5.8 | 0.0 | 0 | 44 | 680505.3 | 6259940.0 |
| 6 | 10600 | A | 0 | -0.2 | 4.7 | 0.0 | 0 | 34 | 679534.8 | 6259069.0 |
| 6 | 10600 | B | 0 | -7.2 | 4.4 | 0.0 | 0 | 46 | 680485.6 | 6259605.0 |
| 6 | 10611 | A | 0 | 0.0 | 5.4 | 0.0 | 0 | 43 | 681212.4 | 6259693.5 |
| 6 | 10611 | B | 0 | -3.0 | 7.4 | 0.0 | 0 | 41 | 680941.1 | 6259563.5 |
| 6 | 10621 | A | 0 | -1.0 | 3.4 | 0.0 | 0 | 50 | 681265.1 | 6259490.5 |
| 6 | 10630 | A | 0 | -3.9 | 9.2 | 0.0 | 0 | 45 | 681387.4 | 6259283.5 |
| 6 | 10630 | B | 0 | -3.4 | 7.4 | 0.0 | 0 | 40 | 681134.9 | 6259129.0 |
| 6 | 10651 | A | 0 | 0.7 | 5.1 | 0.0 | 0 | 54 | 681677.3 | 6258783.5 |
| 6 | 10652 | A | 0 | 0.6 | 6.2 | 0.0 | 0 | 46 | 681675.7 | 6259128.5 |
| 6 | 10652 | B | 0 | -0.4 | 6.2 | 0.0 | 0 | 33 | 681895.3 | 6259269.5 |

Estimated depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or overburden effects.

APPENDIX III

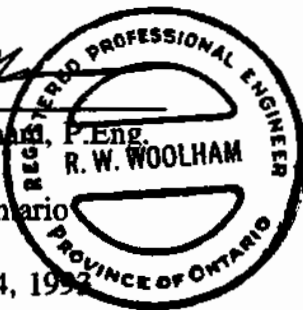
CERTIFICATE OF QUALIFICATION

I, Roderick W. Woolham of the town of Pickering, Province of Ontario, do hereby certify that:-

1. I am a geophysicist and reside at 1463 Fieldlight Blvd., Pickering, Ontario, L1V 2S3
2. I graduated from the University of Toronto in 1961 with a degree of Bachelor of Applied Science, Engineering Physics, Geophysics Option. I have been practising my profession since graduation.
3. I am a member in good standing of the following organizations: The Association of Professional Engineers of the Province of Ontario (Mining Branch); Society of Exploration Geophysicists; South African Geophysical Association.
4. I have not received, nor do I expect to receive, any interest, directly or indirectly, in the properties or securities of Noranda Exploration Company, Ltd. or any affiliate.
5. The statements contained in this report and the conclusions reached are based upon evaluation and review of maps and information supplied by Geonex Aerodat.
6. I consent to the use of this report in submissions for assessment credits or similar regulatory requirements.


R. W. Woolham, P.Eng.
Pickering, Ontario

September 24, 1992



APPENDIX IV

PERSONNEL

FIELD

| | |
|--------------------|----------------------------|
| Flown | July 20 to 21, 1993 |
| Pilot(s) | L. Stanley |
| Operator(s) | G. Bissonnette |

OFFICE

| | |
|-------------------|--|
| Processing | Pierre Marchand George McDonald |
| Report | R. W. Woolham |

APPENDIX VI
STATEMENT OF COSTS

NORANDA EXPLORATION COMPANY, LIMITED
STATEMENT OF COSTS

PROJECT: KLIYUL AREA (KLI GROUP)

DATE: FEBRUARY, 1994

TYPE OF REPORT: GEOPHYSICS

- a) Wages:
No. of Mandays : 11 mandays
Rate per Manday: \$212.50/manday
Dates From : October 19 - November 7, 1993
Total Wages : 11 x \$212.50 \$ 2,337.50
- b) Food & Accommodations:
No. of Mandays : 51 mandays
Rate per Manday: \$18.00/manday
Dates From : October 19 - November 7, 1993
Total Costs : 51 x \$18.00 \$ 918.00
- c) Transportation:
No. of Mandays : 51 mandays
Rate per Manday: \$14.95/manday
Dates From : October 19 - November 7, 1993
Total Costs : 51 x \$14.95 \$ 762.47
- d) Instrument Rental:
Type of Instrument:
No. of Mandays :
Rate per Manday:
Dates From :
Total Costs :
- Type of Instrument:
No. of Mandays :
Rate per Manday:
Dates From :
Total Costs :

e) Analysis:
(See attached schedule)

f) Cost of preparation of Report: \$ 940.00
Author : 2 mandays x \$270.00 = \$540.00
Drafting: 1 manday x \$220.00 = \$220.00
Typing : 1 manday x \$180.00 = \$180.00

g) Other:

Contractor:

Pacific Western Helicopters
6.25 hours x \$725.00/hour (including fuel) \$ 4,531.25

Peter E. Walcott and Associates
10.5 mandays @ \$250.00/manday \$ 2,625.00
10.5 mandays @ \$350.00/manday \$ 3,675.00

TOTAL COST \$15,789.22

h) Unit Costs for Linecutting:
No. of Mandays: 11 mandays
No. of Units : 27.1 line kms
Unit Costs : \$143.17/line km
Total Cost : 27.1 x \$143.17 \$ 3,880.03

i) Unit Costs for Mag:
No. of Mandays: 40 mandays
No. of Units : 27.1 line km
Unit Costs : \$439.45/line km
Total Cost : 27.1 x \$439.45 \$11,909.19

GRAND TOTAL \$15,789.22

NORANDA EXPLORATION COMPANY, LIMITED
STATEMENT OF COSTS

PROJECT: KLIYUL (JOH 1 AND JOH 2 GROUPS)

DATE: FEBRUARY 6, 1994

TYPE OF REPORT: PHYSICAL/GEOCHEMICAL

- a) Wages:
No. of Mandays : 20 mandays
Rate per Manday: \$270.00/manday
Dates From : July 31 - August 21, 1993
Total Wages : 20 x \$270.00 \$ 5,400.00
- b) Food & Accommodations:
No. of Mandays : 40 mandays
Rate per Manday: \$30.37/manday
Dates From : July 31 - August 21, 1993
Total Costs : 40 x \$30.37 \$ 1,214.80
- c) Transportation:
No. of Mandays : 40 mandays
Rate per Manday: \$30.97/manday
Dates From : July 31 - August 21, 1993
Total Costs : 40 x \$30.97 \$ 1,238.80
- d) Instrument Rental:
Type of Instrument:
No. of Mandays :
Rate per Manday:
Dates From :
Total Costs :
- Type of Instrument:
No. of Mandays :
Rate per Manday:
Dates From :
Total Costs :

| | | |
|----|---|--------------------|
| e) | Analysis: 234 samples @ \$13.80/sample (See attached schedule) | \$ 3,229.20 |
| f) | Cost of preparation of Report: Author : 2 mandays x \$270.00 = \$540.00 Drafting: 1 manday x \$220.00 = \$220.00 Typing : 1 manday x \$180.00 = \$180.00 | \$ 940.00 |
| g) | Other: Contractor: Pacific Western Helicopters 6.1 hours @ \$725.00/hour (including fuel) | \$ 4,422.50 |
| | Belham Ltd. 134 pits 172 hours @ \$148.00/hour | \$25,456.00 |
| | TOTAL COST | \$41,631.30 |
| h) | Unit Costs for Geochem: No. of Mandays: 20 mandays No. of Units : 234 samples Unit Costs : \$53.00/sample Total Cost : 234 x \$50.00 | \$12,402.25 |
| i) | Unit Costs for Trenching: No. of Units : 172 hours Unit Costs : \$169.94/hour Total Cost : 172 x \$169.94 | \$29,229.05 |
| | GRAND TOTAL | \$41,631.30 |

NORANDA EXPLORATION COMPANY, LIMITED
(CORDILLERA DIVISION)

DETAILS OF ANALYSES COSTS

PROJECT: KLIYUL (JOH 1 AND JOH 2 GROUPS)

| <u>ELEMENT</u> | <u>NO. OF DETERMINATIONS</u> | <u>COST PER DETERMINATION</u> | <u>TOTAL COSTS</u> |
|-------------------------------------|------------------------------|-------------------------------|--------------------|
| ICP (30 Element) + Geochem Au | 108 Soils (Pits) | \$13.80 | \$1,490.40 |
| | 126 Rocks (Pits) | \$13.80 | <u>\$1,738.80</u> |
| | | | \$3,229.20 |

NORANDA EXPLORATION COMPANY, LIMITED
STATEMENT OF COSTS

PROJECT: KLIYUL (KLI-UTA GROUP) DATE: FEBRUARY 6, 1994

TYPE OF REPORT: GEOLOGICAL, GEOCHEMICAL, PHYSICAL

a) Wages:
No. of Mandays : 11 mandays
Rate per Manday: \$285.00/manday
Dates From : August 14 - October 8, 1993
Total Wages : 11 x \$285.00 \$ 3,135.00

b) Food & Accommodations:
No. of Mandays : 16 mandays
Rate per Manday: \$30.37/manday
Dates From : August 14 - October 8, 1993
Total Costs : 16 x \$30.37 \$ 485.92

c) Transportation:
No. of Mandays : 16 mandays
Rate per Manday: \$30.97/manday
Dates From : August 14 - October 8, 1993
Total Costs : 16 x \$30.97 \$ 495.52

d) Instrument Rental:
Type of Instrument:
No. of Mandays :
Rate per Manday:
Dates From :
Total Costs :

Type of Instrument:
No. of Mandays :
Rate per Manday:
Dates From :
Total Costs :

| | | |
|----|--|--------------------|
| e) | Analysis: 47 rocks @ \$13.80/sample (See attached schedule) | \$ 648.60 |
| f) | Cost of preparation of Report: Author : 2 mandays x \$270.00/manday = \$540.00 Drafting: 1 manday x \$220.00/manday = \$220.00 Typing : 1 manday x \$180.00/manday = \$180.00 | \$ 940.00 |
| g) | Other: Contractor: Pacific Western Helicopters 1.7 hours x \$725.00/hour (including fuel) | \$ 1,232.50 |
| | Belham Ltd. 25.8 hours x \$148.00/hour (20 pits) | \$ 3,818.40 |
| | TOTAL COST | \$10,755.94 |
| h) | Unit Costs for Trenching: No. of Mandays: 5 mandays No. of Units : 25.8 hours Unit Costs : \$171.83/hour Total Cost : 25.8 x \$171.83 | \$ 4,433.23 |
| i) | Unit Costs for Geology: No. of Mandays: 8 mandays No. of Units : 8 mandays Unit Costs : \$482.12/manday Total Cost : 8 x \$482.12 | \$ 3,856.97 |
| j) | Unit Costs for Geochemistry: No. of Mandays: 3 mandays No. of Units : 47 samples Unit Costs : \$52.46/sample Total Cost : 47 x \$52.46 | \$ 2,465.74 |
| | GRAND TOTAL | \$10,755.94 |

NORANDA EXPLORATION COMPANY, LIMITED
(CORDILLERA DIVISION)

DETAILS OF ANALYSES COSTS

PROJECT: KLIYUL (KLI-UTA GROUP)

| <u>ELEMENT</u> | <u>NO. OF DETERMINATIONS</u> | <u>COST PER DETERMINATION</u> | <u>TOTAL COSTS</u> |
|-------------------------------------|------------------------------|-------------------------------|--------------------|
| ICP (30 Element) + Geochem Au | 17 Rocks (Pits) | \$13.80 | \$234.60 |
| | 30 Rocks (Recce) | \$13.80 | <u>\$414.00</u> |
| | | | \$648.60 |

NORANDA EXPLORATION COMPANY, LIMITED
STATEMENT OF COSTS

PROJECT: KLIYUL (CROYDON GROUP) DATE: FEBRUARY 4, 1994
TYPE OF REPORT: GEOLOGICAL, GEOCHEMICAL, GEOPHYSICAL & PHYSICAL

- a) Wages:
No. of Mandays : 31 mandays
Rate per Manday: \$233.26/manday
Dates From : July 20 - November 7, 1993
Total Wages : 31 x \$233.26 \$ 7,231.06
- b) Food & Accommodations:
No. of Mandays : 33 mandays
Rate per Manday: \$30.37/manday
Dates From : July 20 - November 7, 1993
Total Costs : 33 x \$30.37 \$ 1,002.21
- c) Transportation:
No. of Mandays : 33 mandays
Rate per Manday: \$30.97/manday
Dates From : July 20 - November 7, 1993
Total Costs : 33 x \$30.97 \$ 1,022.01
- d) Instrument Rental:
Type of Instrument:
No. of Mandays :
Rate per Manday:
Dates From :
Total Costs :
- Type of Instrument:
No. of Mandays :
Rate per Manday:
Dates From :
Total Costs :
- e) Analysis: 195 soils, 65 rocks @ \$13.80 \$ 3,588.00
(See attached schedule)
- f) Cost of preparation of Report: \$ 900.00
Author : 2 mandays x \$250/day= \$500.00
Drafting: 1 manday x \$220/day = \$220.00
Typing : 1 manday x \$180/day = \$180.00

| | | | |
|----|--|--|--------------------|
| g) | Other: | | |
| | Contractor: | | |
| | Peter E. Walcott & Associates: | | |
| | 2 mandays @ \$350.00 & \$250.00 per | | \$ 600.00 |
| | Pacific Western Helicopters: | | |
| | \$725/hour including fuel x 5.7 hours | | \$ 4,132.50 |
| | Belham Ltd: | | |
| | 34 pits; \$148.00/hr x 44 hrs including mob/demob | | \$ 6,512.00 |
| | Geonex Aerodat Ltd: | | |
| | 35.65 km/415 x \$35,150.00 | | \$ 3,019.51 |
| | TOTAL COST | | \$28,007.29 |
| h) | Unit Costs for Geophysics (Mag) | | |
| | No. of Mandays: 3 mandays | | |
| | No. of Units : 3 km | | |
| | Unit Costs : \$464.32/km | | |
| | Total Cost : 3 x \$464.32 | | \$ 1,392.96 |
| i) | Unit Costs for Geophysics (Airborne) | | |
| | No. of Line Km: 35.65 line km | | |
| | Unit Costs : \$84.70/km | | |
| | Total Cost : 35.65 x \$84.70 | | \$ 3,019.51 |
| j) | Unit Costs for Geology (including pit mapping) | | |
| | No. of Mandays: 13 mandays | | |
| | Unit Costs : \$486.85/manday | | |
| | Total Costs : 13 x \$486.85 | | \$ 6,329.05 |
| k) | Unit Costs for Geochem | | |
| | No of Units : 260 samples | | |
| | Unit Costs : \$32.00/sample | | |
| | Total Cost : 260 x \$32.00 | | \$ 8,319.52 |
| l) | Unit Costs for Trenching | | |
| | No of Units : 44 hours (34 pits) | | |
| | Unit Costs : \$148.00/hour | | |
| | Total Cost : 44 x \$148.00 | | \$ 6,512.00 |
| m) | Unit Costs for Linecutting | | |
| | No. of Units : 15.5 line km | | |
| | Unit Cost : \$157.05/line km | | |
| | Total Cost : 15.5 x \$157.05 | | \$ 2,434.25 |
| | GRAND TOTAL | | \$28,007.29 |

NORANDA EXPLORATION COMPANY, LIMITED
(CORDILLERA DIVISION)

DETAILS OF ANALYSES COSTS

PROJECT: KLIYUL (CROYDON GROUP)

| <u>ELEMENT</u> | <u>NO. OF DETERMINATIONS</u> | <u>COST PER DETERMINATION</u> | <u>TOTAL COSTS</u> |
|--------------------------------------|------------------------------|-------------------------------|--------------------|
| ICP (30 Elements) + Geochem Au | 180 Soils | \$13.80 | \$2,484.00 |
| ICP (30 Elements) + Geochem Au | 38 Rocks | \$13.80 | \$ 524.40 |
| ICP (30 Elements) + Geochem Au | 15 Test Pit Soils | \$13.80 | \$ 207.00 |
| | 27 Test Pit Rocks | \$13.80 | <u>\$ 372.60</u> |
| | | | \$3,588.00 |

NORANDA EXPLORATION COMPANY, LIMITED
STATEMENT OF COSTS

PROJECT: KLIYUL (CRO GROUP)

DATE: FEBRUARY 4, 1994

TYPE OF REPORT: GEOLOGICAL, GEOCHEMICAL, GEOPHYSICAL & PHYSICAL

- a) Wages:
No. of Mandays : 12 mandays
Rate per Manday: \$274.92/manday
Dates From : July 20 - November 7, 1993
Total Wages : 12 x \$274.92 \$ 3,299.00
- b) Food & Accommodations:
No. of Mandays : 13 mandays
Rate per Manday: \$30.37/manday
Dates From : July 20 - November 7, 1993
Total Costs : 13 x \$30.37 \$ 394.81
- c) Transportation:
No. of Mandays : 13 mandays
Rate per Manday: \$30.97/manday
Dates From : July 20 - November 7, 1993
Total Costs : 13 x \$30.97 \$ 402.61
- d) Instrument Rental:
Type of Instrument:
No. of Mandays :
Rate per Manday:
Dates From :
Total Costs :
- Type of Instrument:
No. of Mandays :
Rate per Manday:
Dates From :
Total Costs :
- e) Analysis: 25 rocks, 36 soils \$ 841.80
(See attached schedule)
- f) Cost of preparation of Report: \$ 1,160.00
Author : 2 mandays x \$270.00/mday = \$540.00
Drafting: 2 mandays x \$220.00/mday = \$440.00
Typing : 1 manday x \$180.00/mday = \$180.00

g) Other:

Contractors:

Geonex Aerodat Ltd.

\$106.24/415 line km x \$35,150 \$ 8,998.40

Pacific Western Helicopters

2 hours @ \$725.00/hour (including fuel) \$ 1,450.00

Belham Ltd.

11 pits

\$148.00/hour x 14.2 hours \$ 2,101.60

TOTAL COST \$18,648.22

h) Unit Costs for Linecutting:

No. of Mandays: 3 mandays

No. of Units : 9.8 line km

Unit Costs : \$169.52/line km

Total Cost : 9.8 x \$169.52 \$ 1,661.27

i) Unit Costs for Trenching:

No. of Mandays: 1½ mandays

No. of Units : 14.2 hours

Unit Costs : \$148.00/hour

Total Cost : 14.2 x \$148.00 \$ 2,101.60

j) Unit Costs for Mag:

No. of Mandays: 3 mandays

No. of Units : 8.525 line km

Unit Costs : \$202.97/line km

Total Cost : 8.525 x \$202.97 \$ 1,730.35

k) Unit Costs for Airborne:

No. of Units : 106 line km

Unit Costs : \$84.70/line km

Total Cost : \$35,150 x 106.24/415 (total AB flown) \$ 8,998.40

l) Unit Costs for Geology:

No. of Mandays: 4 mandays

No. of Units : 4

Unit Costs : \$515.43/manday

Total Cost : 4 x \$515.43 \$ 2,061.73

m) Unit Costs for Geochem:

No. of Mandays: 2 mandays

No. of Units : 61 samples

Unit Costs : \$34.34/sample

Total Cost : 61 x \$34.34 \$ 2,094.87

GRAND TOTAL \$18,648.22

NORANDA EXPLORATION COMPANY, LIMITED
(CORDILLERA DIVISION)

DETAILS OF ANALYSES COSTS

PROJECT: KLIYUL (CRO GROUP)

| <u>ELEMENT</u> | <u>NO. OF DETERMINATIONS</u> | <u>COST PER DETERMINATION</u> | <u>TOTAL COSTS</u> |
|-------------------------------------|-------------------------------------|--------------------------------------|---------------------------|
| ICP (30 Element) + Geochem Au | 10 Pit Rocks | \$13.80 | \$138.00 |
| ICP (30 Element) + Geochem Au | 4 Pit Soils | \$13.80 | \$ 55.20 |
| ICP (30 Element) + Geochem Au | 32 Recce Soils | \$13.80 | \$441.60 |
| ICP (30 Element) + Geochem Au | 15 Recce Rocks | \$13.80 | <u>\$207.00</u> |
| | | | \$841.80 |

NORANDA EXPLORATION COMPANY, LIMITED
STATEMENT OF COSTS

PROJECT: KLIYUL (JO GROUP)

DATE: FEBRUARY 6, 1994

TYPE OF REPORT: GEOCHEMICAL, GEOPHYSICAL, PHYSICAL & GEOLOGICAL

- a) Wages:
No. of Mandays : 9 mandays
Rate per Manday: \$283.33/manday
Dates From : July 13 - August 21, 1993
Total Wages : 9 x \$283.33 \$ 2,550.00
- b) Food & Accommodations:
No. of Mandays : 14 mandays
Rate per Manday: \$30.37/manday
Dates From : July 13 - August 21, 1993
Total Costs : 14 x \$30.37 \$ 425.18
- c) Transportation:
No. of Mandays : 14 mandays
Rate per Manday: \$30.97/manday
Dates From : July 13 - August 21, 1993
Total Costs : 14 x \$30.97 \$ 433.58
- d) Instrument Rental:
Type of Instrument:
No. of Mandays :
Rate per Manday:
Dates From :
Total Costs :
- Type of Instrument:
No. of Mandays :
Rate per Manday:
Dates From :
Total Costs :
- e) Analysis: \$ 1,642.20
(See attached schedule)
- f) Cost of preparation of Report: \$ 940.00
Author : 2 mandays x \$270.00 = \$540.00
Drafting: 1 manday x \$220.00 = \$220.00
Typing : 1 manday x \$180.00 = \$180.00

| | | | |
|----|--|--------------------|--------------------|
| g) | Other: | | |
| | Contractors: | | |
| | Pacific Western Helicopters | | |
| | 2.1 hours x \$725.00/hour (including fuel) | | \$ 1,522.50 |
| | Geonex Aerodat Ltd.: (Airborne) | | |
| | 27.4 km/415 km x \$35,150 | | \$ 2,320.75 |
| | Belham Ltd.: (Trenching - 40 pits) | | |
| | 51.5 hours x \$148.00/hour | | \$ 7,622.00 |
| | | TOTAL COST | \$17,356.21 |
| h) | Units Costs for Geochem: | | |
| | No. of Mandays: 6 mandays | | |
| | No. of Units : 119 samples | | |
| | Unit Costs : \$39.01 | | |
| | Total Cost : 119 x \$39.01 | | \$ 4,641.76 |
| i) | Unit Costs for Geology: | | |
| | No. of Mandays: 4 mandays | | |
| | No. of Units : 4 mandays | | |
| | Unit Costs : \$504.69 | | |
| | Total Cost : 4 x \$504.69 | | \$ 2,018.77 |
| j) | Unit Costs for Geophysics (Airborne): | | |
| | No. of Units : 27.4 line km | | |
| | Unit Costs : \$84.70/km | | |
| | Total Cost : 27.4 x \$84.70 | | \$ 2,320.75 |
| k) | Unit Costs for Trenching (40 pits): | | |
| | No. of Mandays: 4 mandays | | |
| | No. of Units : 51.5 hours | | |
| | Unit Costs : \$162.62/hour | | |
| | Total Cost : 51.5 x \$162.62 | | \$ 8,374.93 |
| | | GRAND TOTAL | \$17,356.21 |

NORANDA EXPLORATION COMPANY, LIMITED
(CORDILLERA DIVISION)

DETAILS OF ANALYSES COSTS

PROJECT: KLIYUL (JO GROUP)

| <u>ELEMENT</u> | <u>NO. OF DETERMINATIONS</u> | <u>COST PER DETERMINATION</u> | <u>TOTAL COSTS</u> |
|-------------------------------------|------------------------------|-------------------------------|--------------------|
| ICP (30 Element) + Geochem Au | 33 Soils (Pits) | \$13.80 | \$ 455.40 |
| | 36 Rocks (Pits) | \$13.80 | \$ 496.80 |
| | 43 Soils (Recce) | \$13.80 | \$ 593.40 |
| | 7 Rocks (Recce) | \$13.80 | <u>\$ 96.60</u> |
| | | | \$1,642.20 |

NORANDA EXPLORATION COMPANY, LIMITED
STATEMENT OF COSTS

PROJECT: KLIYUL (GOLDWAY GROUP) DATE: FEBRUARY 4, 1994

TYPE OF REPORT: GEOCHEMICAL/GEOPHYSICAL

- a) Wages:
No. of Mandays : 14 mandays
Rate per Manday: \$250.42/manday
Dates From : July 9 - October 4, 1993
Total Wages : 14 x \$250.42 \$ 3,505.88
- b) Food & Accommodations:
No. of Mandays : 14 mandays
Rate per Manday: \$30.37/manday
Dates From : July 9 - October 4, 1993
Total Costs : 14 x \$30.37 \$ 425.18
- c) Transportation:
No. of Mandays : 14 mandays
Rate per Manday: \$30.97/manday
Dates From : July 9 - October 4, 1993
Total Costs : 14 x \$30.97 \$ 433.58
- d) Instrument Rental:
Type of Instrument:
No. of Mandays :
Rate per Manday:
Dates From :
Total Costs :
- Type of Instrument:
No. of Mandays :
Rate per Manday:
Dates From :
Total Costs :

| | | |
|----|--|--------------------|
| e) | Analysis: 178 soils and 17 rocks @ 13.80/sample (See attached schedule) | \$ 2,691.00 |
| f) | Cost of preparation of Report: Author : 2 mandays @ \$270.00/manday = \$540.00 Drafting: 1 manday @ \$220.00/manday = \$220.00 Typing : 1 manday @ \$180.00/manday = \$180.00 | \$ 940.00 |
| g) | Other: Contractor: Geonex Aerodat Ltd. 40.2 line km x \$35,150.00 415 line km (total) | \$ 3,404.89 |
| | Pacific Western Helicopters \$725.00/hour (including fuel) x 2.1 hours | \$ 1,522.50 |
| | TOTAL COST | \$12,923.03 |
| h) | Unit Costs for Geochem: No. of Mandays: 7 mandays No. of Units : 195 samples Unit Costs : \$31.31/sample Total Cost : 195 x \$31.31 | \$ 6,104.57 |
| i) | Unit Costs for Airborne: No. of Units : 40.2 line km Unit Costs : \$84.68/line km Total Cost : 40.2 x \$84.68 | \$ 3,404.03 |
| j) | Unit Costs for Linecutting: No. of Mandays: 7 mandays No. of Units : 14.25 line km Unit Costs : \$239.61/line km Total Cost : 14.25 x \$239.61 | \$ 3,414.43 |
| | GRAND TOTAL | \$12,923.03 |

NORANDA EXPLORATION COMPANY, LIMITED
(CORDILLERA DIVISION)

DETAILS OF ANALYSES COSTS

PROJECT: KLIYUL (GOLDWAY GROUP)

| <u>ELEMENT</u> | <u>NO. OF DETERMINATIONS</u> | <u>COST PER DETERMINATION</u> | <u>TOTAL COSTS</u> |
|-------------------------------------|-------------------------------------|--------------------------------------|---------------------------|
| ICP (30 Element) + Geochem Au | 178 Soils | \$13.80 | \$2,456.40 |
| ICP (30 Element) + Geochem Au | 17 Rocks | \$13.80 | <u>\$ 234.60</u> |
| | | | \$2,691.00 |

APPENDIX VII
STATEMENT OF QUALIFICATIONS

STATEMENT OF QUALIFICATIONS

I, D. Graham Gill of the City of Vancouver, Province of British Columbia, hereby certify that:


I am a geologist residing at 5442 - 7th Avenue, Delta, B.C.

I have graduated from the University of British Columbia in 1983 with a BSc in geology.

I have worked in mineral exploration since 1979.

I have been a temporary employee with Noranda Exploration Company, Limited since May, 1983 and a permanent employee since November, 1987.

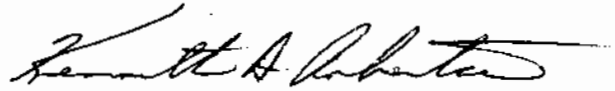
I am a member in good standing of the Professional Engineers & Geoscientists of British Columbia.


D. Graham Gill, P. Geo.

STATEMENT OF QUALIFICATIONS

I, Kenneth A. Robertson, of the City of Delta, Province of British Columbia, hereby certify that:

1. I am a Professional Geophysicist residing at 7540 Garfield Drive, Delta, B.C. V4C 7L4.
2. I have graduated from the University of Toronto in 1977 with an H.B.Sc. in Geology and Physics.
3. I have worked in mineral exploration since 1975.
4. I have been a permanent employee of Noranda Exploration Company, Limited since February 1984.
5. I am a member in good standing of the Professional Engineers and Geoscientists of British Columbia.



Kenneth A. Robertson, P. Geo.