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**DRILLING REPORT**  
  
on the  
  
**ASHTON GROUP  
MINERAL CLAIMS**

**NTS 92I/6W & 92I/3W  
KAMLOOPS MINING DIVISION**

**LATITUDE: 50°15' NORTH  
LONGITUDE: 121°24' WEST**

**OWNER: S.E. APCHKRUM**

**OPERATORS: KINGSTON RESOURCES LTD.  
J.M. ASHTON  
S.E. APCHKRUM**

**CONSULTANT: J.D. GRAHAM, P.ENG.**

**AUTHOR: J.M. ASHTON, P.ENG.**

**SUBMITTED: 26 August, 1994**

Prepared by:

808 Exploration Services Ltd.  
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Vancouver, British Columbia  
V6B 2L3

**GEOLOGICAL BRANCH  
ASSESSMENT REPORT**

**23,495**

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Lithochemical Assay Procedures from Eco-Tech Laboratories Ltd. . . . . III

# ASHTON COPPER PROSPECT DRILLING REPORT

## SECTION 1.0 — INTRODUCTION

The first recorded work on the Ashton Prospect was directed by Alfred A. Burgoyne, M.Sc., in October 1969. His work included a single element copper in soils survey which resulted in the delineation of a large area of highly anomalous copper in soils.

Limited follow-up trenching near the anomaly showed shear zone hosted copper mineralization and accompanying skarnification with contained copper minerals. J.W. Antal, P.Geol., conducted a limited geological examination of the trench exposures and concluded in his November 1969 report that the prospect area had the potential for hosting a large low-grade copper deposit. There was no mention of local intrusive activity.

In 1989-90, the Rebecca 1 to 6, inclusive, and Sheryl mineral claims were staked and a Magnetometer and VLF-EM survey was carried out over the area of interest under the direction of J.M. Ashton, P.Eng. The magnetometer survey identified a prominent magnetic anomaly with an amplitude response greater than 3,000 gammas (Nanoteslas) for a strike length of 350 metres (1,500 feet) trending northerly. The location of this anomaly relative to the 1969 copper in soils anomalies was not known at the time, but it was suspected that there was probably a close relationship.

A petrographical study by P. Reid, Ph.D., P.Eng., of GeoTex Consultants Limited of a representative rock sample taken by J.M. Ashton within the area of the magnetic anomaly showed that the rock was a heavily altered fine-grained pyroxene diorite ? with the alteration assemblage consisting of calcite, chlorite, epidote, sphene, pyrrhotite, and hematite. The original rock has been nearly obliterated by alteration facies. The tourmaline, a major part of the alteration assemblage, indicates that hydrothermal solutions causing the alteration contained significant volatiles.

In August 1992, R.E. Gale, Ph.D., P.Eng., examined the prospect and confirmed the skarnification reported by J.W. Antal, and both altered and unaltered diorite reported by J.M. Ashton.

In April 1992, Kingston Resources Ltd. optioned the property from the recorded owner, S.E. Apchkrum, and in June 1993 carried out a geochemical sampling and limited mapping program to confirm the copper in soils anomalies identified by Burgoyne in 1969.

The Kingston work successfully located part of the anomalous area and showed that it was open in at least three directions from the chosen survey area.

The geological mapping confirmed that heavily altered diorite was in association with the copper in soils anomalies and that the diorite which contained moderate to strongly disseminated magnetite was thought to represent apophyses in the form of dikes and plugs associated with the neighbouring Mount Lytton Complex.

Kingston conducted additional geochemical survey work to the west and to the southeast of the anomalous copper in soils area and the results showed a much enlarged anomalous area that appeared to be closed off in those directions yet open to the north because additional work was not conducted in that direction.

Following the plotting of the copper in soils results, an induced polarization survey was conducted over part of the large area of anomalous copper in soils with the focus over the area of the altered diorite.

A significant induced polarization chargeability anomaly of classic character was interpreted to coincide with the high copper geochemistry and altered diorite in the southwest portion of the anomalous area. It was this coincidental anomalous area that was the focus of the Kingston Resources Ltd. percussion drilling program that is the subject of this report.

## SECTION 2.0 — SUMMARY

The Ashton Copper Prospect is comprised of 12 located mineral claims consisting of 53 units.

The claims are located about 10 km east of Lytton, British Columbia, with the claim boundary beginning about 500 metres southeast of the Thompson River where it bends to the west towards Lytton after travelling southerly from Spences Bridge. The geographical coordinates are 50°15' North Latitude with an intercept of 121°24' West Longitude. The National Topographic System Map References are 92I/6W and 92I/3W.

The property is accessible by automobile from the Trans Canada Highway between Lytton and Spences Bridge. There is a good gravel road that leaves the highway at the north end of a curved bridge which passes over the Nicoamen River 10 km east of Lytton. A switchback gravel road south of the bridge passes through the property on its eastern side.

The claims are held by record by S.E. Apchkrum of Vancouver, British Columbia.

The 1993 reverse circulation Percussion Drilling Program was undertaken by Kingston Resources Ltd. whom at the time had the claims under option from S.E. Apchkrum. The drilling program was carried out to test a coincident copper in soils anomaly with a high chargeability induced polarization anomaly within an area of intensely altered diorite.

The program included:

- preparation of drill sites
- the drilling of seven reverse circulation holes totalling 2,675 feet (816 metres)
- drilling supervision and in-situ selection of hole locations as a result of drill hole geological observations
- the analyses of all percussion drill samples taken over 10-foot drilling intervals
- cursory geological logging of cuttings

Subsequent to the drilling, Kingston dropped its option on the claims and S.E. Apchkrum engaged J.M. Ashton, P.Eng., to review and organize results of the drilling and in this regard engaged the professional services of Dr. R.E. Gale, P.Eng., consulting geologist, to log and interpret the drill hole cuttings.

Of the seven holes drilled, four (93-1, 93-2, 93-3 and 93-4) were targeted into the zone of the coincident induced polarization chargeability anomaly and high copper geochemistry and altered diorite and one hole (93-5) was drilled to test a mineralized shear zone and two holes (93-6 and 93-7) were drilled to test the contact area between the diorites and Spences Bridge Volcanics.

Copper assay results from Drill Holes 93-1 to 93-5, inclusive, for a total length of 676.8 metres (2,220 feet) averaged 554 ppm copper. The high copper content of the large volume of rock tested is geostatistically significant.

The highest geochemical assays, their interval and principal host rock of Drill Holes 93-1 to 93-5 included:

Drill Hole	Interval (feet)	Copper (ppm)	Host Lithology
93-1	60	1,183	Leucodiorite and Gabbro with Cpy and Py
93-2	80	1,089	Felsitic Diorite and Gabbro with Cpy and Py
93-3	50	1,003	Limy Diorite with Several Quartz-Py-Cpy Veinlets
94-4	30	1,000	Medium to Coarse Grained Dark Grey Diorite, Calcite-Py-Cpy Veinlets
	20	874	Pink Garnet in Limestone
	20	1,270	White Diorite with Py
93-5	10	940	Diorite Porphyry with Strong Magnetite
	20	668	Limy Diorite with Quartz-Py-Cpy
	20	1,935	Limy Diorite with Moderate Py

Drill Hole 93-6 penetrated 160 feet (48.8 m) of overburden before entering successively Spences Bridge Volcanics and barren diorite. Drill Hole 93-7 drilled from the same set-up was abandoned in overburden.

Drill hole geological logging has identified copper mineralization as disseminations throughout the multiple intrusive phases and in veins or stockworks within the intrusives. Copper assay results confirm that geostatistically significant copper is pervasive. Pervasive alteration in the form of calcite flooding and quartz-carbonate veining was found in all of those drill holes, 93-1 to 93-5 inclusive, located within the altered diorite and intrusive complex where coincidental



induced polarization chargeability and copper in soils geochemical anomalies were most pronounced.

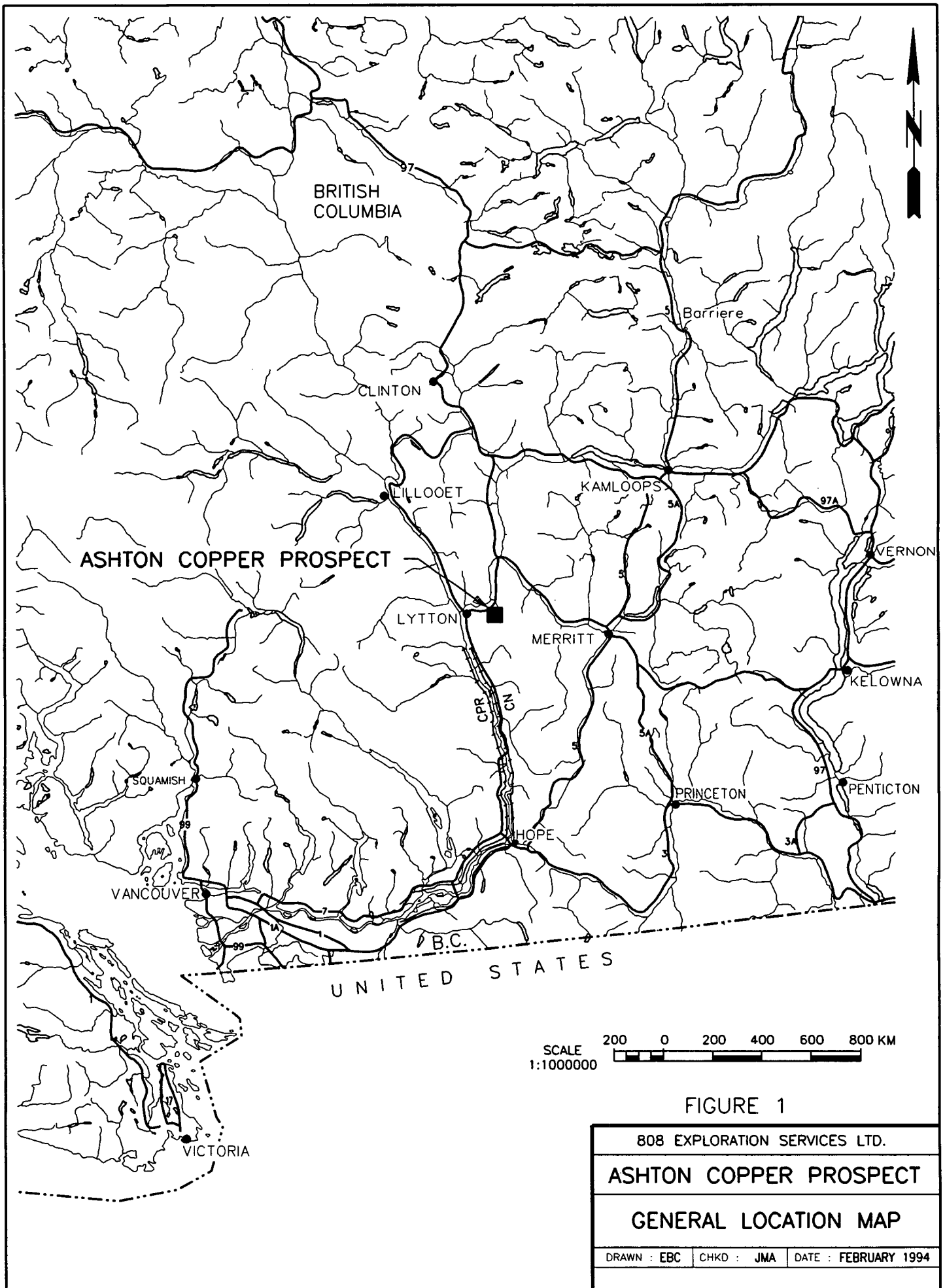
Drill hole geological logging through examination of reverse circulation percussion drill chips under a binocular microscope resulted in the identification of at least three and possibly four types of mineralized intrusive and altered rock: diorite, quartz-diorite, gabbro and felsitic diorite and demonstrates that multiple episodic intrusives penetrated this location forming an altered and mineralized rock network that may represent the uppermost section of a porphyry style mineralizing system of the classic type where the main zone of mineralization may occupy that volume of rock around the margins of a subcropping magma chamber.

### SECTION 3.0 — LOCATION AND ACCESS

The Ashton Group of mineral claims is located approximately 19 km (11.8 miles) south of Spences Bridge, British Columbia. Spences Bridge is located approximately 109 km (118 miles) by air northwest of Vancouver, British Columbia, on Trans Canada Highway 1.

Locally, the northwest corner of the claim group is located about 500 m from the confluence of the Nicoamen River where it enters the Thompson River.

A good all-weather forest service road provides immediate and easy access to the central part of the claims southward from the paved Trans Canada Highway near the confluence of the Nicoamen and Thompson Rivers. Several old logging roads with secondary tree growth cross the property and intersect with the main access road, thereby providing the potential for road access to most every sector of the property through a minimum of rehabilitation. All drill sites were made road-accessible generally through rehabilitation of pre-existing logging roads.

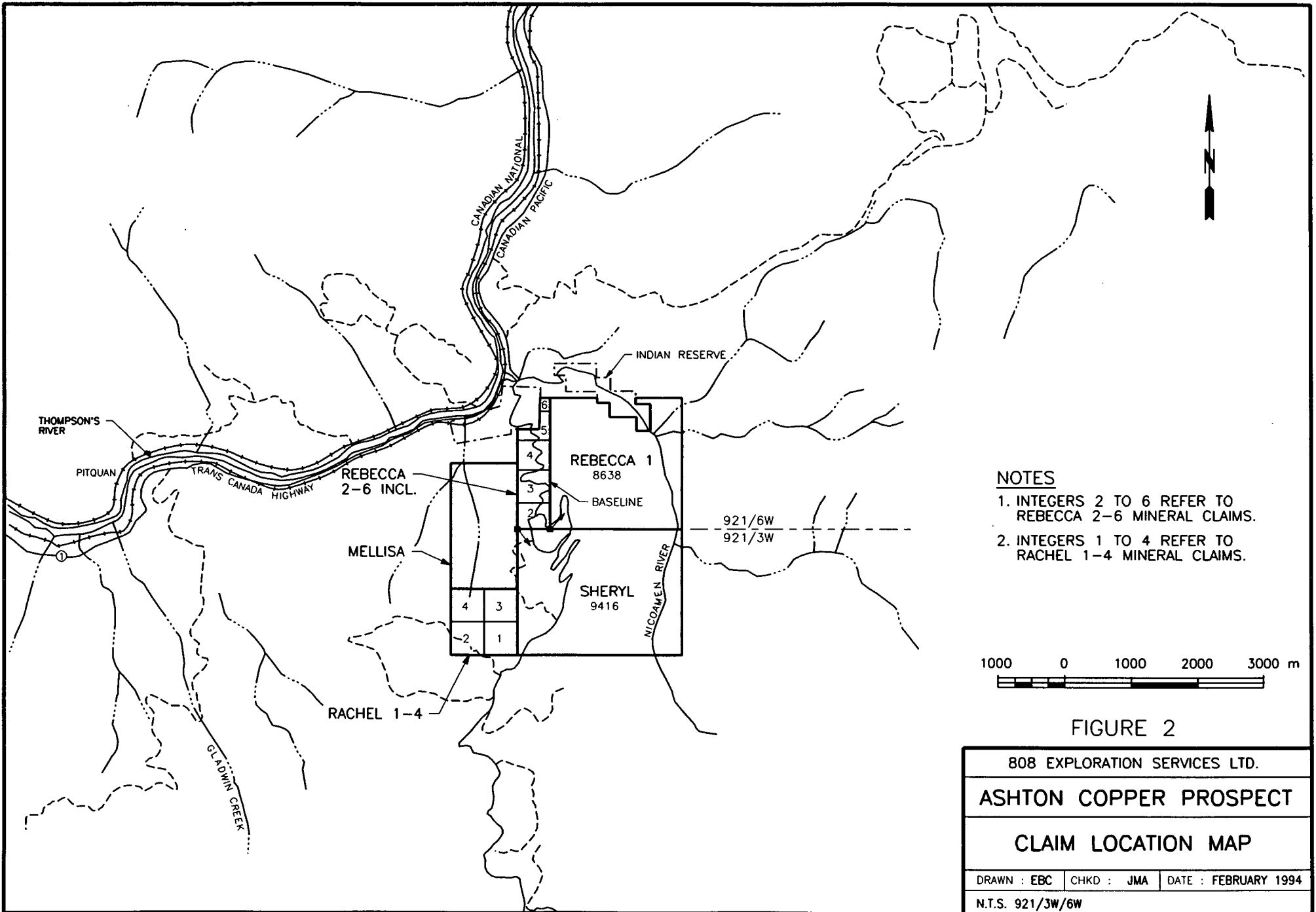


## SECTION 4.0 — PROPERTY AND OWNERSHIP

The Ashton Group is comprised of the following mineral claims with expiry dates shown subject to acceptance of this report:

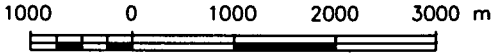
<b>Mineral Claim</b>	<b>Units</b>	<b>Tenure No.</b>	<b>Expiry Date</b>
Rebecca 1	16	218569	21 June 1999
Rebecca 2	1	218570	20 June 1999
Rebecca 3	1	218571	20 June 1999
Rebecca 4	1	218572	20 June 1999
Rebecca 5	1	218573	20 June 1999
Rebecca 6	1	218574	20 June 1999
Sheryl	20	219338	9 June 1999
Rachel 1	1	311562	17 July 1999
Rachel 2	1	311563	17 July 1999
Rachel 3	1	311564	17 July 1999
Rachel 4	1	311565	17 July 1999
Melissa	8	318692	1 July 1999
<b>Total</b>	<b>53</b>		

The mineral claims are held by record in the name of S.E. Apchkrum of Richmond, British Columbia.



**NOTES**

- 1. INTEGERS 2 TO 6 REFER TO REBECCA 2-6 MINERAL CLAIMS.
- 2. INTEGERS 1 TO 4 REFER TO RACHEL 1-4 MINERAL CLAIMS.



**FIGURE 2**

808 EXPLORATION SERVICES LTD.		
ASHTON COPPER PROSPECT		
CLAIM LOCATION MAP		
DRAWN : EBC	CHKD : JMA	DATE : FEBRUARY 1994
N.T.S. 921/3W/6W		

## SECTION 5.0 — PHYSIOGRAPHY AND OUTCROP

The claims cover an area of moderate to steep topographical relief. The central and western part of the claims are traversed by a multiple switchback road that climbs the east side of the Thompson River canyon rising from the canyon bottom at 700 feet (213 m) elevation to a saddle between two peaks at 3,500 feet (213 m) elevation to a saddle between two peaks at 3,500 feet (1,070 m) elevation within a distance of 2 miles (3.2 km). This represents an average mountain slope of 26.5%. Locally the relief is moderate to steep in the area of interest, yet easily accessible by foot from the switchback road.

The area of interest is part of the Cascade Mountains which are separated from the Coast Mountains to the west by the Fraser River. The Thompson River meets the Fraser River at Lytton about 8 miles (13 km) west from the property.

The Cascade Mountains are lower and less rugged than the Coast Mountains and generally consist of rolling and rounded summits, which is the case at the higher elevations on this property.

Southern and western exposures on the property tend to be open areas and easily traversed, whereas northern and eastern slopes are much more heavily wooded. The area of interest on the property is a north-facing slope that has been logged of most of its coniferous growth with new growth represented by denser deciduous trees and in places associated with difficult to traverse underbrush.

Outcrop is generally lacking throughout the area of interest, so trenching is required to access the bedrock for mapping and sampling. Outcrop over the entire property is estimated at about 20%.

Overburden encountered in the drill holes provides an overview of its anticipated range over the area of interest on the property.

Drill Hole	Overburden Depth (feet)
93-1	10 V
93-2	10 (-61°)
93-3	20 V
93-4	10 (-62°)
93-5	30 (-60°)
93-6	135 (-60) Abandoned
93-7	130 V

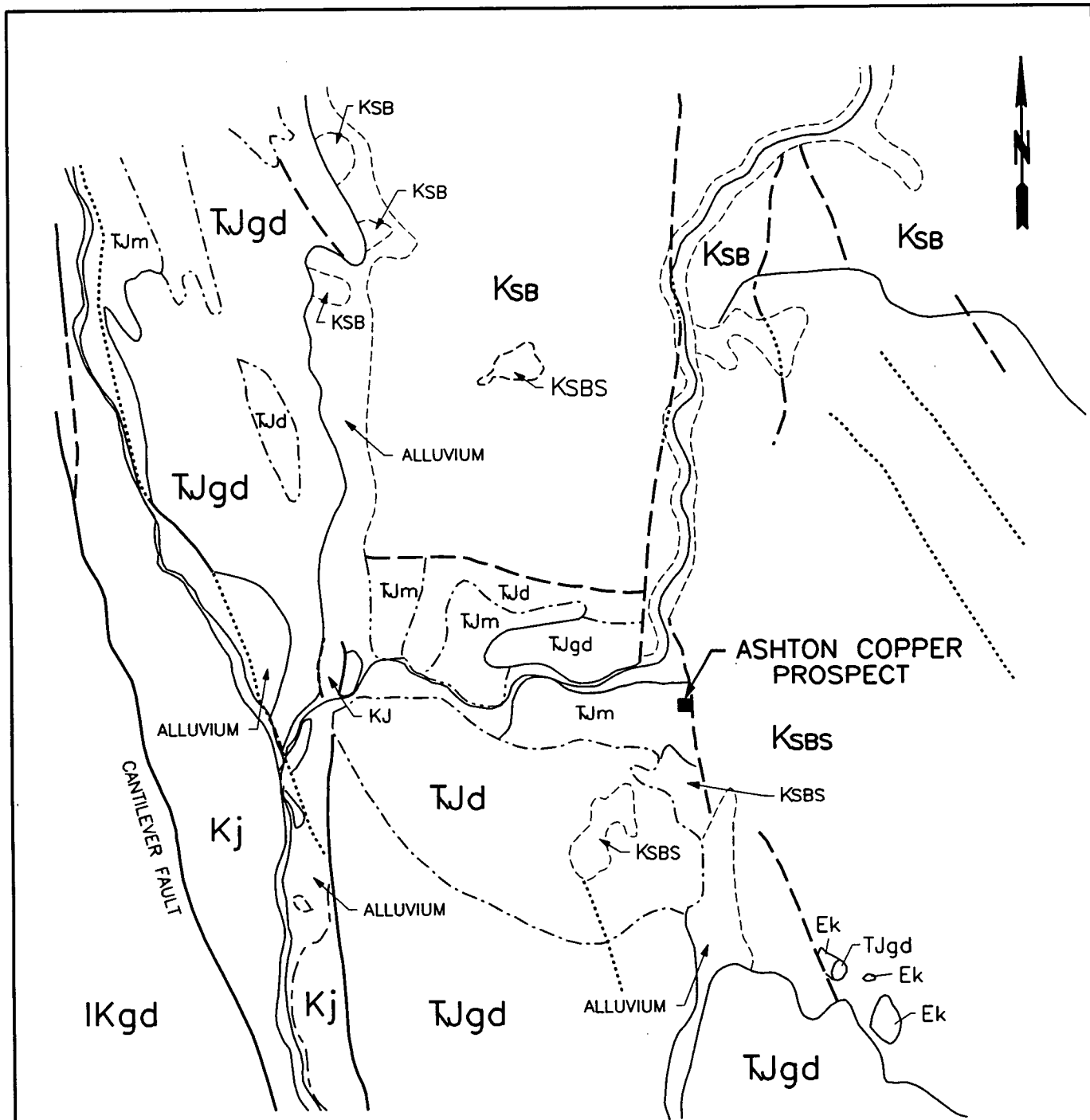
*V = Vertical*

## SECTION 6.0 — REGIONAL GEOLOGY

The regional geology is more recently described in the Geological Survey of Canada *Geology of Hope and Ashcroft Map Areas, British Columbia* by J.W.H. Monger and shown on Map 42-1899, Ashcroft, British Columbia, from which the salient features are shown on Figure 3. As described by S.W. Smith, the property straddles the boundary between the older (Upper Triassic) Mount Lytton Complex on the west part and the younger (Middle and Upper Cretaceous) Spences Bridge Group to the east.

The Mount Lytton Complex has been interpreted by Monger to be part of the roots of the Late Triassic Nicola arc. The complex is fault bounded, on the west by the Fraser River fault system, and on the east by normal faults along the Thompson River. The Mount Lytton Pluton that is part of the complex has been age-dated at 212 +/- 1 Ma (Parrish and Monger, 1992), which is very close to some dates reported from the central Guichon Batholith, which is located about 40 km to the northeast and contains the world-class Highland Valley ore bodies. Parrish and Monger interpret the Mount Lytton and Guichon Creek bodies to be part of the Upper Triassic magmatic arc complex that characterizes Quesnellia terrane, but state that they were probably emplaced at different structural levels, as suggested by their contrasting settings.

The Middle and Upper Cretaceous Spences Bridge Group unconformably overlies and is in fault contact with the older Mount Lytton Complex. In the area of the property, the Spences Bridge Group is relatively unaltered and consists of intermediate, locally felsic and mafic flows and pyroclastics along with sandstone, shale and conglomerate.



**LEGEND**

- FAULT
- INFERRED FAULT

**LATE CRETACEOUS**

IKgd -GRANODIORITE, QUARTZ MONZONITE  
SPENCES BRIDGE GROUP

KsB -FELSIC, MAFIC FLOWS AND SANDSTONE -SHALE  
KsBs -MAFIC VOLCANICS -CONGLOMERATE

**EARLY AND MIDDLE CRETACEOUS**

JACKASS MOUNTAIN GROUP  
KJ SANDSTONE, ARGILLITE, CONGLOMERATE

**TRIASSIC AND/OR JURASSIC**

Tjd -DIORITE, AMPHIBOLITE MT. LYTON COMPLEX  
Tjgd -GRANODIORITE, QUARTZ MONZONITE MT. LYTON BATHOLITH  
Tjm -LAYERED OF ROCK, AMPHIBOLITE, MYLONITE MT. LYTON BATHOLITH

SCALE  
1:200000



**FIGURE 3**

808 EXPLORATION SERVICES LTD.

**ASHTON COPPER PROSPECT**

**REGIONAL GEOLOGY**

DRAWN : EBC    CHKD : JMA    DATE : FEBRUARY 1994

MODIFIED AFTER J.W.H.MONGER    GSC MAP 42-1989



## SECTION 7.0 — PROPERTY GEOLOGY

Geological mapping of the property surface geology is lacking; hence, very little is known of alteration facies and zoning features that would provide helpful information or a prelude to further drilling. The accompanying geological report by Dr. R.E. Gale, Ph.D., found in Appendix I, integral with this report, does provide an excellent summary of subcropping geology alteration and mineralization.

The property appears to be bifurcated by Cretaceous volcanics to the east and Triassic intrusives to the west.

The more recent surface geological information that represents useful information was reported on by S.W. Smith in his 'Assessment Report', *Geological Mapping and Geological Sampling on the Ashton Property* of 20 September 1993.

On the east side of the property, the rocks are reddish coloured andesitic flows and pyroclastics of the Spences Bridge Group. They are relatively unaltered.

The rocks on the west side of the property where the copper in soils geochemistry was found to be significantly anomalous are believed to be part of the Mount Lytton Complex and were cursorily mapped as interbedded limestone and volcanic sediments with intrusive plugs or dykes of fine-grained diorite.

- S. Smith reported that:

The limestone varies from a clean white crystalline variety with a massive appearance to a thinly bedded grey silty variety. The limestone beds were noted to be from 0.5 to 5 m thick. Interbedded with the limestone was fine to medium-grained green volcanic tuff that was much wider in width. The volcanics were commonly limy. Locally these rocks were very strongly altered and fractured, with the strongest alteration seen in the vicinity of the old trenches in the northwestern portion of the Sheryl claims.

The diorite found in surface outcrop obtained by the writer was dark grey to black, was intensely altered and was found to contain significant amounts of disseminated magnetite. A petrographic study of a representative sample was summarized as follows:

The original rock may have been a fine-grained pyroxene ? diorite but this rock has been nearly obliterated by an alteration assemblage of tourmaline-epidote-calcite-chlorite-sphene-pyrite which is cut by a few albite-calcite veinlets.

According to S. Smith, hydrothermal alteration of the volcanics was seen on a wide scale causing bleaching and quartz/carbonate veining within them. Epidote is the most common

alteration mineral. Locally the diorite is so strongly altered that only epidote and magnetite can be seen. Secondary chlorite and calcite are also quite prevalent throughout the complex. The propylitic alteration (epidote, chlorite +/- pyrite) identified in the volcanics and diorite provides surface indication that a significant porphyry style intrusive system underlies the area.

Structurally, the targeted drilling area appears to be proximal to a major north-south fault-shear system.

## SECTION 8.0 — 1993 DRILLING PROGRAM

### General

The reverse circulation percussion drilling program was undertaken to test a coincident induced polarization chargeability anomaly and copper in soils anomaly located within what was identified as a pervasively altered dioritic intrusive complex as a result of the drilling. The program included the drilling of seven holes with a total length of 2,705 feet (824.7 m) and the multi-element analyses of recovered drill cuttings over intervals of 10 feet (3.05 m).

The drilling was conducted between 29 August and 14 September 1993 and the analytical work was carried out between 2 September and about 27 September 1993.

The program was supervised by S.W. Smith, P.Geol. Management and consulting services were provided by Westore Engineering Ltd., Radvak Engineering Ltd. and S.J. Radvak, P.Eng.

Assay results from the drilling were plotted in December 1993 and chip samples from the drilling were geologically logged by Dr. R.E. Gale, P.Eng., in late January 1994.

The assimilation of data and preparation of this report occurred over an extended period between December 1993 and August 1994 by this writer under the auspices of 808 Exploration Services Ltd. on behalf of S.E. Apchkrum.

### Reverse Circulation Percussion Drilling

The reverse circulation drilling was performed by Dateline Contracting Ltd. of Kelowna, British Columbia. Clearing out of old logging roads and preparation of drill sites was performed by Cherma Dozing Ltd.

Drill holes were located in the field by S.W. Smith, P.Geol.

Rock chip samples were recovered from each 10-foot drill rod penetration interval into the subcropping rock and mechanically split into two equal components of which one component was discarded and the other bagged and labelled in large polyethylene sample bags for shipment to the assayer.

Representative samples from each 10-foot interval were systematically selected and placed in plastic sample receptacles, each measuring 5 cm by 2.5 cm by 2.5 cm to provide a record set of drill cuttings for geological mapping purposes including petrographical study.

The bagged samples were shipped in groups by bus to Eco Tech Laboratories Ltd. in Kamloops, British Columbia, for sample preparation and assay by the 30-element ICP technique.

REVERSE CIRCULATION DRILLING STATISTICS							
Item	Hole Identification	Date (1993)		Co-ordinates	Length (feet)	Azimuth	Dip
		Collared	Completed				
1.	RCA 93-1	1 Sept.	2 Sept.	49+60N, 1+10W	500	-	-90°
2.	RCA 93-2	3 Sept.	5 Sept.	49+45N, 2+29W	320	162°	-61°
3.	RCA 93-3	6 Sept.	7 Sept.	48+00N, 0+97E	500	-	-90°
4.	RCA 93-4	7 Sept.	9 Sept.	47+55N, 0+45E	400	270	-62°
5.	RCA 93-5	9 Sept.	11 Sept.	45+70N, 2+70E	500	272°	-60°
6.	RCA 93-6	12 Sept.	13 Sept.	53+00N, 3+45E	135	270°	-60°
7.	RCA 93-7	13 Sept.	14 Sept.	53+00N, 3+45E	350	-	-90°
TOTAL					2,705 feet (824.7 m)		

Drill Holes RCA 93-1 and RCA 93-2 were drilled on the Melissa Claim; Drill Holes RCA 93-3, RCA 93-4 and RCA 93-5 were drilled on the Sheryl Claim; and Drill Holes RCA 93-6 and RCA 93-7 were drilled on the Rebecca 2 Claim.

### Lithochemical Analyses

A total of 249 samples, each representative of a 10-foot percussion drill intercept were prepared and assayed by the ICP (Inductively Coupled Plasma) technique from which 23 elements were determined in parts per million, seven elements determined in percent and one element, Au, determined in parts per billion.

Three copper assays for comparison purposes were made from drill cuttings as follows:

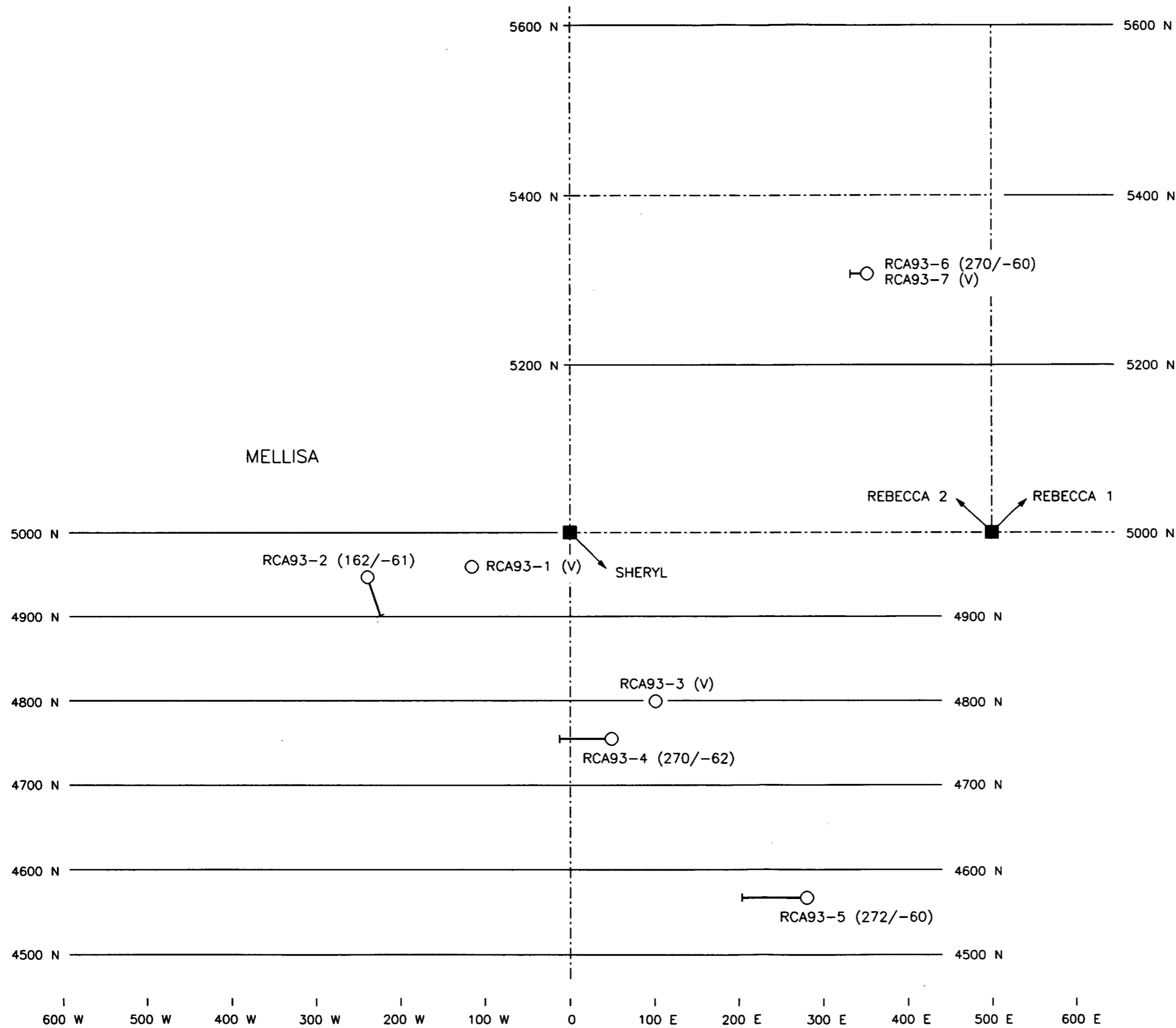
Drill Hole	Interval (feet)	Assay Copper (%)	Assay ICP (ppm)	Difference
93-1	390-400	0.22	1,843	19%
93-2	170-180	0.17	1,501	13%
93-2	210-220	0.18	1,588	13%

In the three cores tested, copper assays were on average 15% higher than the ICP procedure.

Appendix III describes the assay procedures used by Eco-Tech Laboratories Ltd. for analyzing the lithogeochemical samples recovered from the percussion drilling.

## SECTION 9.0 – RESULTS

Geological and geochemical results of the 1993 reverse circulation drilling program are depicted in Figures 4 to 10, inclusive. The geological logs are reported on and summarized in the report by Dr. R.E. Gale, P.Eng., in Appendix I.



**LEGEND**

- CLAIM LINE
- GRID LINE

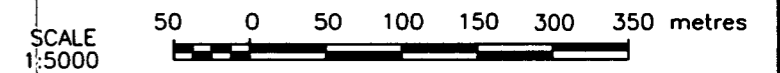
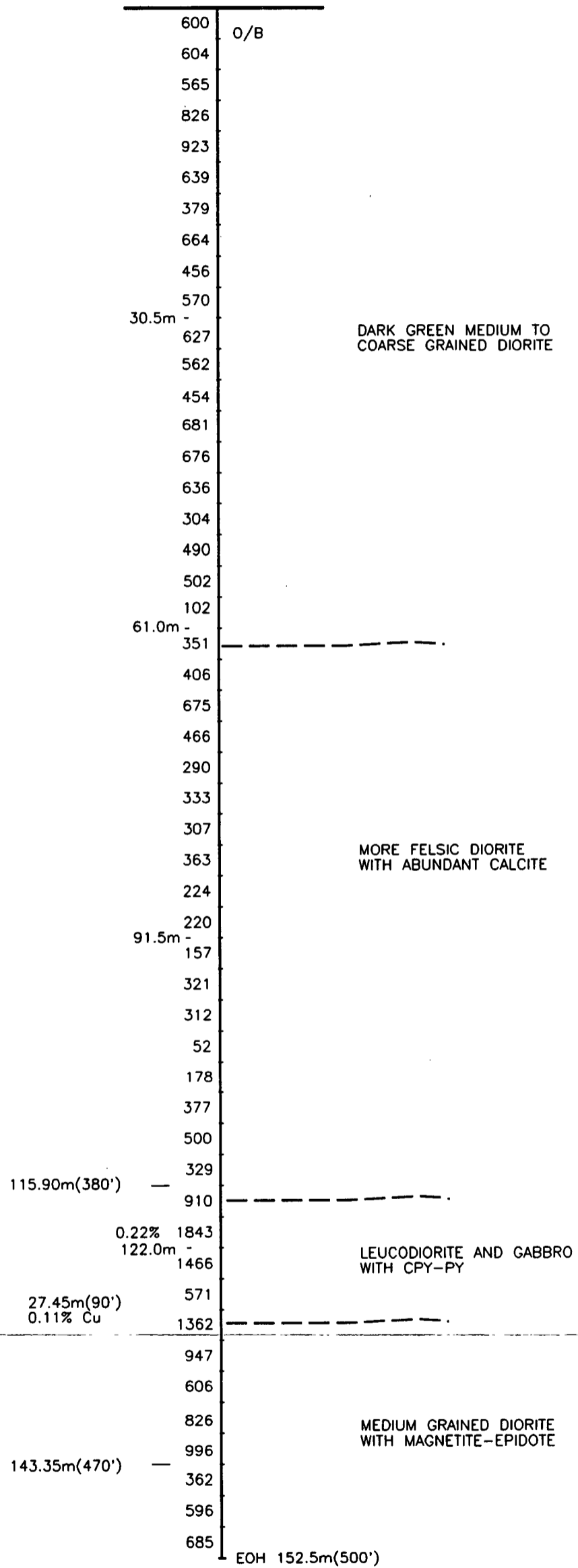


FIGURE 4

808 EXPLORATION SERVICES LTD.			
<b>ASHTON COPPER PROSPECT</b>			
1993 REVERSE CIRCULATION DRILLHOLE & CLAIM LOCATION PLAN			
GEOLOGIST	SS/REG	SCALE	AS SHOWN
DRAWN	EBC	DATE	FEBRUARY 1994
CHECKED	JMA		

RCA 93-1 GRID COORDINATES 49+60N  
(DIP-90°) 1+10W



NOTES

1. AFTER KINGSTON RESOURCES LTD. DECEMBER, 1993.
2. GEOLOGY RELOGGED BY R.E.GALE, Ph D FEBRUARY, 1994.

SCALE 1:500  
5 0 5 10 15 30 35 metres

FIGURE 5

808 EXPLORATION SERVICES LTD.

ASHTON COPPER PROSPECT

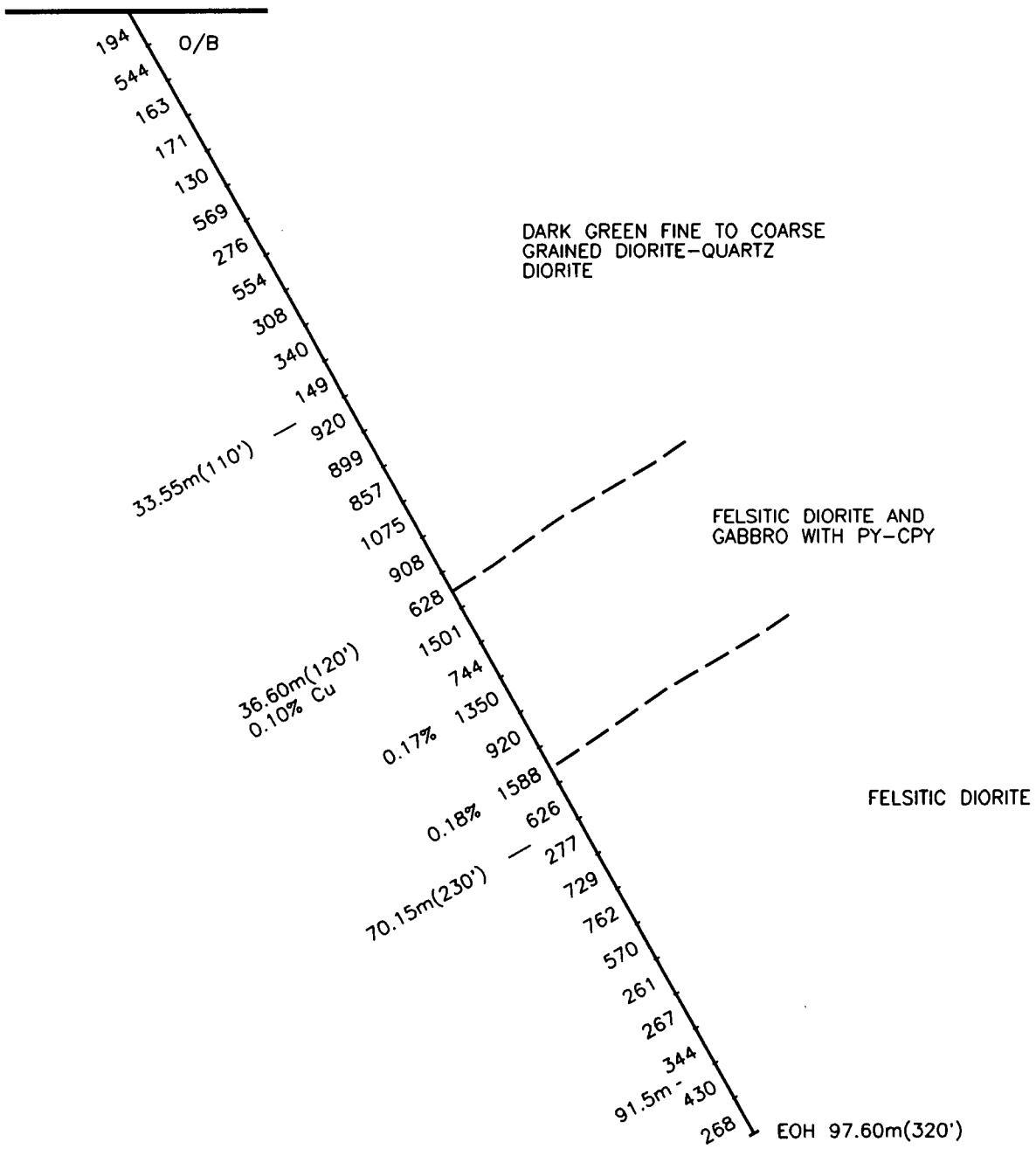
REVERSE CIRCULATION DRILL PROGRAM  
GEOLOGY & COPPER GEOCHEMICAL  
ASSAY RESULTS

HOLE RCA 93-1

GEOLOGIST	REG	SCALE	AS SHOWN
DRAWN	EBC	DATE	DECEMBER 1993
CHECKED	JMA	REVISED	FEBRUARY 1994



RCA 93-2 GRID COORDINATES 49+45N  
 (Az 162°, DIP-61°) 2+29W



**NOTES**

1. AFTER KINGSTON RESOURCES LTD., DECEMBER, 1993.
2. GEOLOGY RELOGGED BY R.E.GALE, Ph D FEBRUARY, 1994.

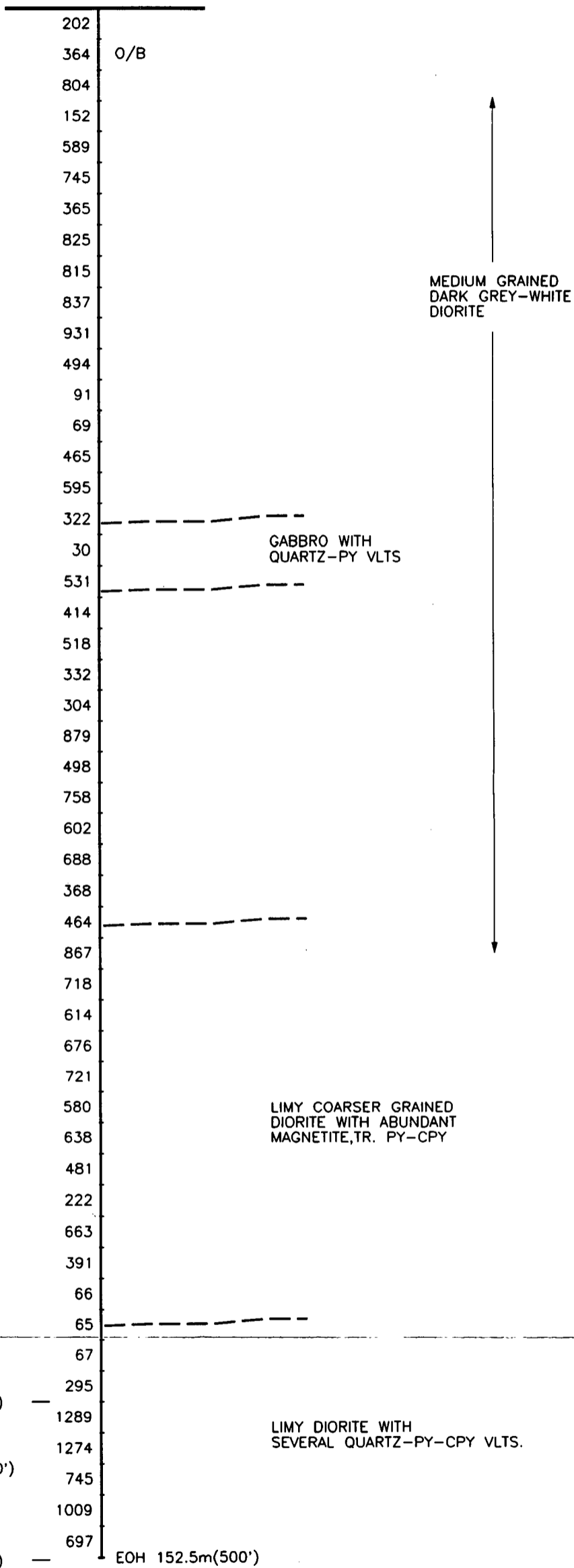


**FIGURE 6**

808 EXPLORATION SERVICES LTD.			
<b>ASHTON COPPER PROSPECT</b>			
REVERSE CIRCULATION DRILL PROGRAM GEOLOGY & COPPER GEOCHEMICAL ASSAY RESULTS			
<b>HOLE RCA 93-2</b>			
DEOLOGIST	REG	SCALE	AS SHOWN
DRAWN	EBC	DATE	DECEMBER 1993
CHECKED	JMA	REVISED	FEBRUARY 1994

ASHTON COPPER PROSPECT  
 HOLE RCA 93-2  
 DECEMBER 1993

RCA 93-3 GRID COORDINATES 48+00N  
(DIP-90°) 0+97E



**NOTES**

1. AFTER KINGSTON RESOURCES LTD. DECEMBER, 1993.
2. GEOLOGY RELOGGED BY R. GALE, Ph D FEBRUARY, 1994.

FIGURE 7

808 EXPLORATION SERVICES LTD.

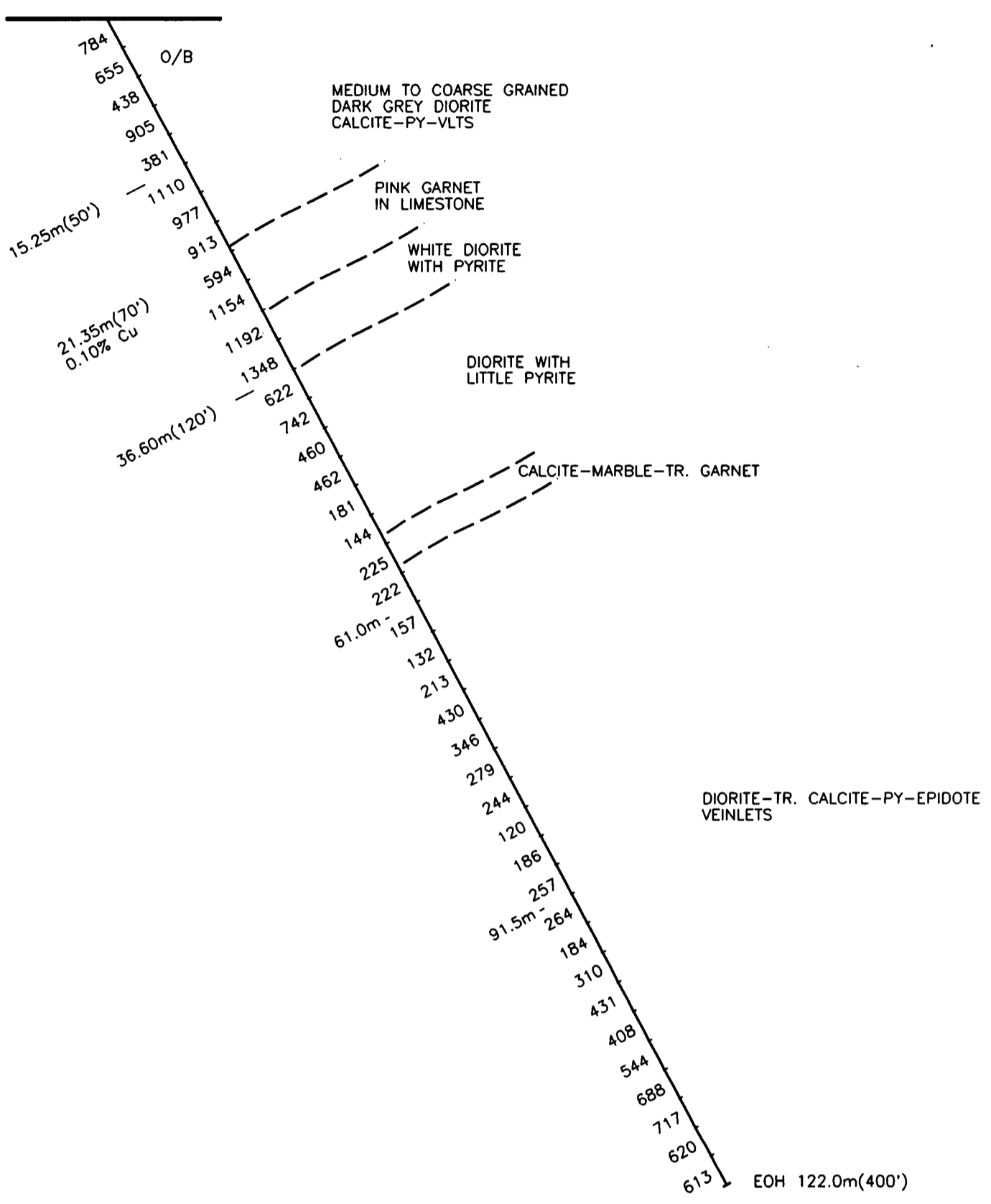
**ASHTON COPPER PROSPECT**

REVERSE CIRCULATION DRILL PROGRAM  
GEOLOGY & COPPER GEOCHEMICAL  
ASSAY RESULTS

HOLE RCA 93-3

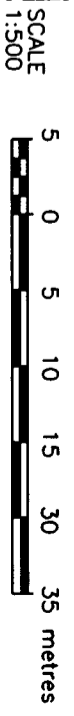
GEOLOGIST	REG	SCALE	AS SHOWN
DRAWN	EBC	DATE	DECEMBER 1993
CHECKED	JMA	REVISED	FEBRUARY 1994

RCA 93-4 GRID COORDINATES 47+55N  
 (Az 270°, DIP-62°) 0+45E



**NOTES**

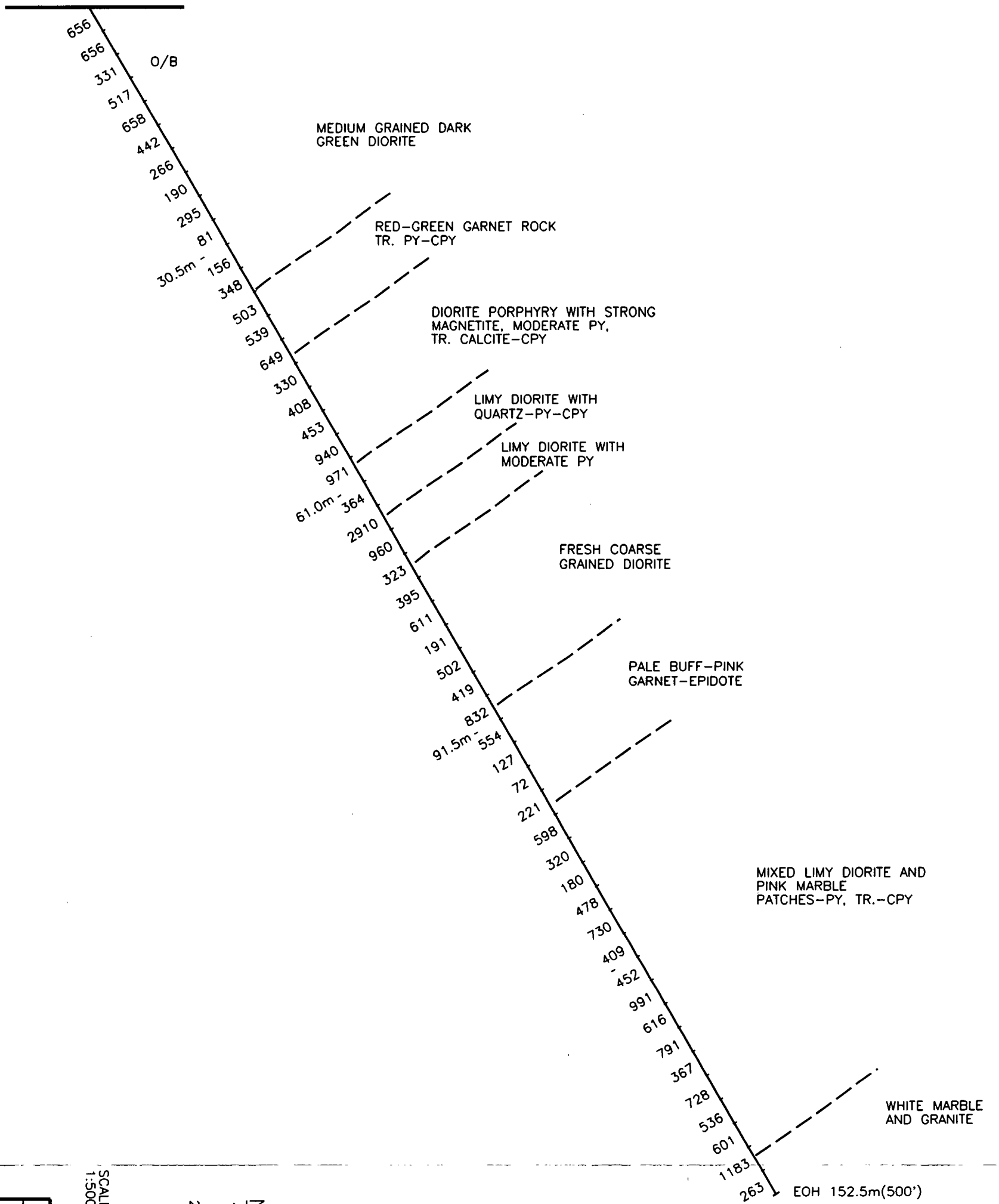
1. AFTER KINGSTON RESOURCES LTD., DECEMBER, 1993.
2. GEOLOGY RELOGGED BY R.E.GALE, Ph D FEBRUARY, 1994.



**FIGURE 8**

808 EXPLORATION SERVICES LTD.		AS SHOWN	
<b>ASHTON COPPER PROSPECT</b>			
REVERSE CIRCULATION DRILL PROGRAM GEOLOGY & COPPER GEOCHEMICAL ASSAY RESULTS			
HOLE RCA 93-4		AS SHOWN	
GEOLOGIST	REG	SCALE	DATE
DRAWN	EBC		DECEMBER 1993
CHECKED	JMA	REVISED	FEBRUARY 1994

RCA 93-5 GRID COORDINATES 45+70N  
 (Az 272°, DIP-60°) 2+70E



**NOTES**

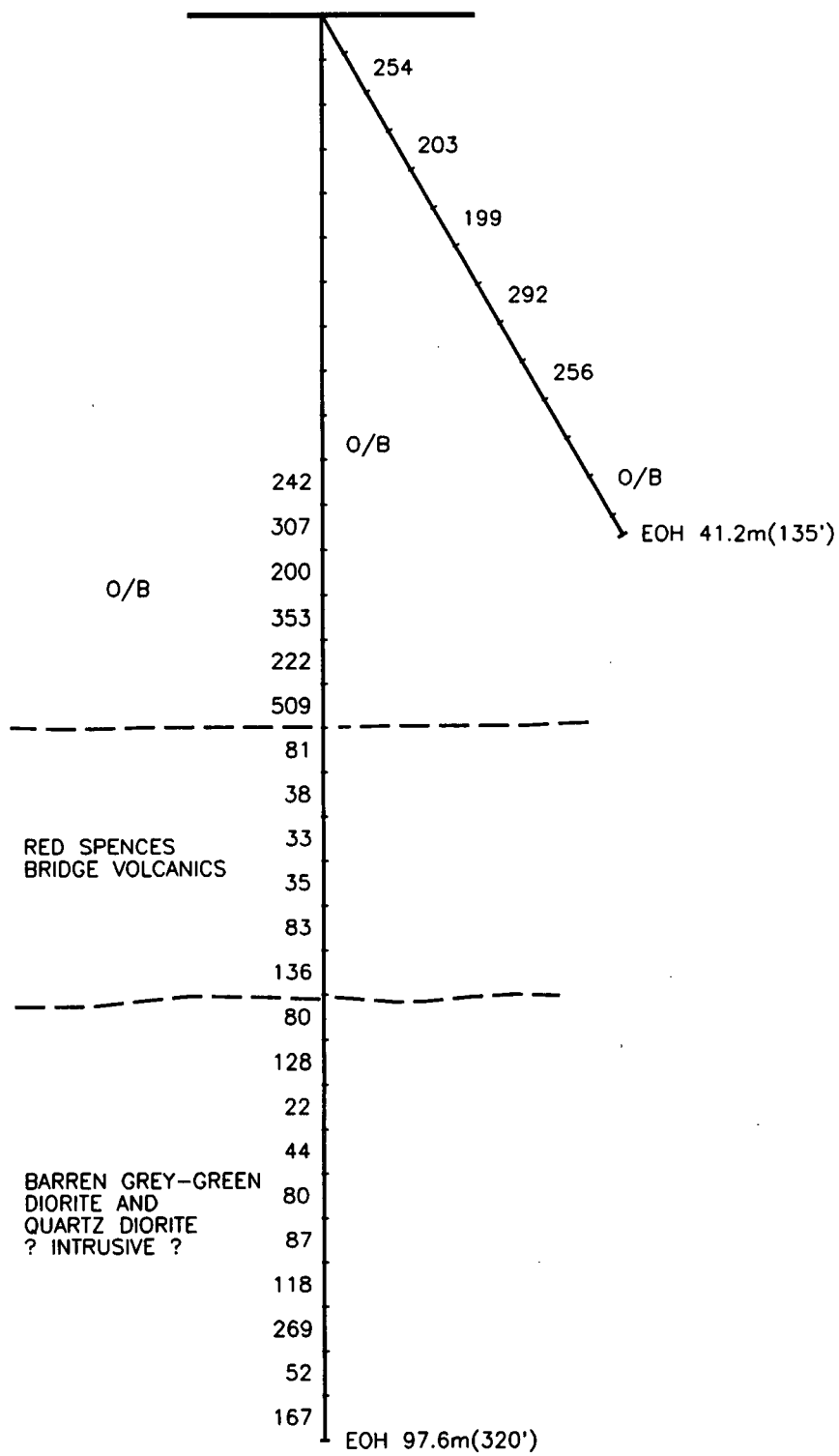
1. AFTER KINGSTON RESOURCES LTD. DECEMBER, 1993.
2. GEOLOGY RELOGGED BY R.E.GALE, Ph D FEBRUARY, 1994.



**FIGURE 9**

808 EXPLORATION SERVICES LTD.			
<b>ASHTON COPPER PROSPECT</b>			
REVERSE CIRCULATION DRILL PROGRAM GEOLOGY & COPPER GEOCHEMICAL ASSAY RESULTS			
<b>HOLE RCA 93-5</b>			
GEOLOGIST	REG	SCALE	AS SHOWN
DRAWN	EBC	DATE	DECEMBER 1993
CHECKED	JMA	REVISED	FEBRUARY 1994

RCA 93-6 & 7      GRID COORDINATES    53+00N  
 (RCA 93-6, Az 270°,DIP-60°)      3+45E  
 (RCA 93-7, DIP-90°)



**NOTES**

1. AFTER KINGSTON RESOURCES LTD. DECEMBER, 1993.
2. GEOLOGY RELOGGED BY R.E.GALE, Ph D FEBRUARY, 1994.

SCALE 1:500  
 5 0 5 10 15 30 35 metres

**FIGURE 10**

808 EXPLORATION SERVICES LTD.

**ASHTON COPPER PROSPECT**

REVERSE CIRCULATION DRILL PROGRAM  
 GEOLOGY & COPPER GEOCHEMICAL  
 ASSAY RESULTS

**HOLE RCA 93-6 & 7**

GEOLOGIST	REG	SCALE	AS SHOWN
DRAWN	EBC	DATE	DECEMBER 1993
CHECKED	JMA	REVISED	FEBRUARY 1994

## SECTION 10.0 — EXPLORATION POTENTIAL

The basic nature of the dioritic intrusive rocks found in the drilling could be indicative of an Afton Style mineralizing event.

Alternatively, J.W. Monger's speculation that the Mount Lytton Complex and the Guichon Batholith were formed from the same subducted section of Oceanic Crust with the Guichon Batholith, a differentiate from the upper part of the upper section of subducted crust and the Mount Lytton Complex representing the lower part of the upper section leads to the interesting speculation that this intrusive event could have concentrated copper minerals from a similarly copper-enriched crustal element in a similar fashion, as it stoped its way towards the surface. The giant world-class Valley Copper Mine is located only 23 miles (37 km) northeasterly from the Ashton Prospect. This mine produces an estimated 1.4 million pounds of copper in concentrate daily.

SECTION 11.0 – COST STATEMENT

Summary

1.	Personnel . . . . .	\$ 11,000.00
2.	Field Expense . . . . .	1,625.55
3.	Room and Board . . . . .	1,020.00
4.	Bulldozing . . . . .	1,502.00
5.	Reverse Circulation Drilling . . . . .	27,756.25
6.	Assaying . . . . .	3,718.00
7.	Drill Hole Logging . . . . .	1,280.00
8.	Data Preparation, Reports and Drawings . . . . .	4,540.00
9.	Report Reproduction and Drawings . . . . .	<u>250.00</u>
	TOTAL	<u>\$ 52,691.80</u>



**Personnel**

1.	Drilling Preparation Scott Smith, P.Geol. 5 days @ \$400	\$ 2,000.00
2.	Drilling Supervision and Drill Hole Sampling and Logging 31 August to 15 September Scott Smith, P.Geol. 16 days @ \$400	6,400.00
3.	Site Inspection 7 September 1993 J.M. Ashton, P.Eng.	500.00
4.	Consulting to 30 September S.J. Radvak, P.Eng.	<u>2,100.00</u>
	SUBTOTAL	<u>11,000.00</u>

**Field Expense**

1.	Vehicle Rental 18 days @ \$65	1,170.00
2.	Gasoline	243.70
3.	Sample Bags, Ties and Miscellaneous	<u>211.85</u>
	SUBTOTAL	1,625.55

**Room and Board**

Scott Smith 17 days @ \$60	1,020.00
-------------------------------	----------

**Bulldozing**

Contractor: Cherma Dozing Ltd.	1,502.00
--------------------------------	----------

**Reverse Circulation Drilling**

Contractor: Dateline Contracting Ltd.	27,756.25
---------------------------------------	-----------



**Assaying**

1.	Eco-Tech Laboratories	3,643.25
2.	Acme Analytical Laboratories	<u>74.75</u>
	SUBTOTAL	3,718.00

**Drill Hole Logging**

	R.E. Gale, Ph.D., P.,Eng. for 808 Exploration Services Ltd.	1,280.00
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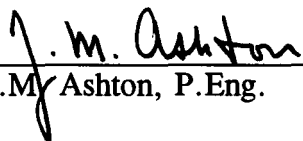
**Data Preparation, Reports and Drawings**

1.	J.M. Ashton, P.Eng. 5 days @ \$500	2,500.00
2.	Plotting and Drafting, CAD Station E.B. Catanpia, C. Tech 24 hours @ \$60	1,440.00
3.	Report Typing, Collation, Drawing Reproduction 20 hours @ \$30	<u>600.00</u>
	SUBTOTAL	<u>4,540.00</u>

SECTION 12.0 — CERTIFICATION OF J.M. ASHTON, P.ENG.

I, J.M. Ashton, of Suite 201 — 518 Beatty Street, Vancouver, British Columbia, hereby certify that:

1. I am a Consulting Electrical Engineer and also a principal in the company, 808 Exploration Services Ltd.
2. I am a graduate of the University of British Columbia with a B.A.Sc. in Electrical Engineering (1966).
3. I am a member in good standing in the Association of Professional Engineers of the Province of British Columbia.
4. I am a member of the Canadian Institute of Mining and Metallurgy.
5. I have practised both as a mineral explorationist and a consulting electrical engineer since 1969.
6. This report was prepared by me. I requested that J. Donald Graham, P.Eng., review the contents herein and certify the same if in concurrence.

  
\_\_\_\_\_  
J.M. Ashton, P.Eng.



Dated this 26th day of August 1994  
VANCOUVER, BRITISH COLUMBIA

**SECTION 13.0 - CERTIFICATION OF J. D. GRAHAM, P. ENG.**

I, J. Donald Graham, of 3962 West 37th Avenue, Vancouver, British Columbia, hereby certify that:

1. I am a graduate of the University of British Columbia with a B. A. Sc. in Geological Engineering (1962).
2. I am a graduate of the University of British Columbia with a B. A. Sc. in Mining Engineering (1964).
3. I am a member of the Canadian Institute of Mining and Metallurgy.
4. I am a registered member in good standing of the Association of Professional Engineers of the Province of British Columbia.
5. I have practised my profession as a Geological and Mining Engineer since graduation to date.
6. I have reviewed the contents of the Drilling Report On The Ashton Group Mineral claims prepared by J. M. Ashton, P. Eng. of 808 Exploration Services Ltd. dated 26 August, 1994. I find the information to be presented in a well organized, professional format. The drill program described has significantly advanced the understanding of the mineral deposit located on the subject claims.

These comments are intended for the internal use of the claim owners and are not to be used in connection with any public financing of work on the subject claims.



J. Donald Graham, P. Eng.

Dated this 26th day of August, 1994

VANCOUVER, BRITISH COLUMBIA

## SECTION 14.0 — REFERENCES

- Antal, J.W., November 25, 1969:  
Geology T Claims. Assessment Report No. 2532.
- Ashton, J.M., August 30, 1990:  
VLF-EM and Magnetic Survey of the Burgoyne Group of Mineral Claims. Assessment Report.
- Burgoyne, A.A., October 31, 1969:  
Copper Geochemical Soil Survey, Mineral Claims T1-T28. Assessment Report No. 2533.
- Gale, R.E., April 21, 1992:  
Summary Report and Recommendations, Ashton Copper Prospect, for Kingston Resources Ltd.
- Gale, R.E., February 4, 1994:  
Logs of Drillhole Cuttings, 1993 Reverse Circulation Drilling, Ashton Copper Prospect (Appendix I).
- Monger, J.W.H., 1989:  
GSC, Geology Map 42-1989 and accompanying notes.
- Monger, J.W.H., June 1993:  
Personal Communication.
- Parrish, R.R. and J.W.H. Monger, 1992:  
New U-Pb dates from southwestern British Columbia; in Radiogenic Age and Isotopic Studies: Report 5, GSC, Paper 91-2, p.87-108.
- Smith, S.W., September 20, 1993:  
Geological Mapping and Geochemical Sampling on the Ashton Property, Assessment Report.

**APPENDIX I**

**Logs and Summary Report  
of Drillhole Cuttings**

**1993 Reverse Circulation Drilling**

**Ashton Copper Prospect**

LOGS OF DRILLHOLE CUTTINGS  
1993 REVERSE CIRCULATION DRILLING  
ASHTON COPPER PROSPECT  
Kamloops M.D. British Columbia

Report for J.M. Ashton, 808 Exploration Services Ltd.  
By R.E. Gale, PhD., P.Eng  
R.E. Gale and Associates Inc.  
February 4, 1994

INTRODUCTION

This report is written at the request of Mr. J.M. Ashton of 808 Exploration Services Ltd.

It is the result of a 2 day binocular microscope study of cuttings collected in a 7 hole reverse circulation drilling program carried out by Kingston Resources Ltd. in September, 1993 on the Ashton copper prospect near Lytton, B.C.

LOGS OF CUTTINGS

(1)Hole No.	Grid Coordinates	Approximate Elevation	Attitude	Total Depth	Significant Intercepts
RC93-1	49+60N 1+10W	2580 Ft.	Vertical	500 Ft.	390-430 Ft 40Ft-0.13% Cu

From	To	Int. Ft.	Description
0	10	10	Overburden
10	210	200	Dark green medium to coarse grained diorite with up to 10% magnetite. Less than 5% epidote and calcite veinlets, rare pyrite, hematite, red garnet and barren quartz veinlets.
210	390	180	Lighter colored, more felsic diorite with abundant calcite in matrix and thin veinlets. More pyrite, up to 2%, traces of chalcopyrite. Less magnetite.
390	430	40	Leucodiorite with more calcite veinlets, pyrite up to 5% and little magnetite. Some quartz-biotite diorite with calcite-quartz veinlets with chalcopyrite. From 410-430 some coarse grained gabbro with pyrite, trace chalcopyrite. The interval from 390 to 430 assayed 0.13% Cu., best grade in the hole.
430	500	70	Dark medium grained diorite with magnetite, some epidote. Bottom of hole.

(2) Hole No.	Grid Coordinates	Approximate Elevation	Attitude	Total Depth	Significant Intercepts
RC 93-2	49+45N 2+29W	2750 Ft.	-61° @ Az. 162°	320 Ft	170-220 50 Ft-0.12%Cu

From	To	Int. Ft.	Description
0	10	10	Overburden
10	170	160	Dark green to grey fine to coarse grained diorite and quartz diorite with 10-15% magnetite and up to 20% quartz. Several zones of greenish white fine grained felsic intrusive with low magnetite. Short sections of red fine grained hematite (or red mica) and epidote with quartz-magnetite veinlets.
170	220	50	Increased amounts of felsitic rock with strong red hematite or red mica coatings on fractures in gabbroic rock sections, 200 to 210 feet, along with magnetite, pyrite, trace chalcopyrite. From 170 - 210 - 40 feet averaged 0.12% Cu., best grade interval in this hole.
220	320	100	Fine to medium grained felsitic intrusive with fairly abundant red hematite or mica and epidote. Bottom of hole.

(3) Hole No.	Grid Coordinates	Approximate Elevation	Attitude	Total Depth	Significant Intercepts
RC 93-3	48+00N 0+97E	2530 Ft.	Vertical	500 Ft.	450-490 40 Ft-0.10%Cu

From	To	Int. Ft.	Description
0	20	20	Overburden
20	300	280	Medium grained dark grey to white diorite with 5-10% magnetite, trace epidote and quartz-calcite veinlets, hematite (red mica) coatings on several fragments. From 150-170, magnetite-rich gabbro with quartz-pyrite in fractures. Calcite increases from 200-300 feet.
300	430	130	Limy, coarser grained dark green diorite with numerous veinlets of calcite. Abundant coarse grained magnetite with traces of pyrite and chalcopyrite.



430 500 70 Similar to above but with several quartz-calcite pyrite-chalcopyrite veinlets. Best grade interval in hole is 450-490, 40 feet grading 0.10% Cu. Bottom of hole-500 feet.

(4)Hole No.	Grid Coordinates	Approximate Elevation	Attitude	Total Depth	Significant Intervals
RC 93-4	47+55N 0+45E	2880 Ft.	-62° @ Az. 270°	400 Ft	90 - 120 30 Ft.-0.12%Cu

From	To	Int.-Ft.	Description
0	10	10	Overburden
10	80	70	Medium to coarse grained dark green diorite with few calcite-pyrite veinlets.
80	100	20	Fine to medium grained pink to red garnet replacing recrystallized limestone. Weak disseminated pyrite and chalcopyrite in marble remnants.
100	120	20	Green to white medium grained diorite with traces of pyrite. The best mineralized intercept in the drillhole is 90-120 feet, 30 feet - 0.12% Cu.
120	180	60	Diorite with little pyrite, some hematite red mica and epidote.
180	190	10	Calcite-marble with traces of yellow garnet replacing marble.
190	400	210	Dark coarse grained to lighter fine grained diorite with traces of calcite veinlets carrying pyrite-epidote. Bottom of hole.

(5)Hole No.	Grid Coordinates	Approximate Elevation	Attitude	Total Depth	Significant Intercepts
RC 93-5	45+70N 2+70E	2530 Ft.	-60° @ Az. 272°	500 Ft	210-220 10 Ft.-0.29%Cu 480-490 10 Ft.-0.12%Cu

From	To	Int.-Ft.	Description
0	30	30	Overburden
30	120	90	Medium grained dark green diorite with up to 10% magnetite, trace pyrite, calcite and epidote. Minor fine grained hematite or

			red mica coatings on magnetite.
120	150	30	Red-green medium grained garnet rock with trace pyrite and chalcopyrite.
150	200	50	Medium grained to coarse grained diorite porphyry with abundant magnetite, moderate pyrite, traces chalcopyrite in calcite veinlets.
200	220	20	Magnetite-poor silicified to highly calcareous diorite with 2% disseminated pyrite-chalcopyrite. Few patches magnetite-pyrite-epidote in thin fractures. Best grade interval in hole here, 10 feet - 0.29% Cu.
220	240	20	Coarse grained diorite with some patches of strong pyrite but little chalcopyrite.
240	300	60	Fresh looking coarse grained diorite.
300	340	40	Pale buff to pink garnet and epidote replacing marble-limestone. Trace pyrite.
340	490	150	Mixed calcite-rich diorite and pink marble with patches of pyrite, trace chalcopyrite. Best mineralization in interval is 480 - 490 feet, 10 feet grading 0.12% Cu.
490	500	10	Mainly white marble with some coarse grained white graphic textured granite or pegmatite. Bottom of hole at 500 feet.

(6) Hole RC 93-6, drilled at same point as RC 93-7, drilled 130 feet of overburden and failed to reach bedrock-was cut off at 130 feet.

(7) Hole No.	Grid Coordinates	Approximate Elevation	Attitude	Total Depth	Significant Intercepts
RC 93-7	53+00N 3+45E	2180 Ft.	Vertical	330 Ft	None

From	To	Int.-Ft.	Description
0	160	160	Overburden
160	220	60	Red-green andesite volcanic - probably Spences Bridge Group.
220	320	100	Barren grey green diorite and quartz diorite, intrusive texture.

COMMENTS ON GEOLOGY FROM LOGS  
-----

- (1) Further drilling should utilize a diamond drill so that the all-important geological relationships between the diorite, gabbro, limestone and skarn can be interpreted properly. The complex structures and contact relationships on the property can only be solved with core drilling with a diamond drill.
- (2) Fragments of the mineralized rocks which I have retained from my study should be impregnated and thin-sectioned to enable positive identification of the rocks which host the mineralization.
- (3) The limy diorite and skarn-marble and their contact areas appear to be the best host rocks for copper mineralization. Further work on the property prior to diamond drilling should include detailed mapping to pin point the contacts on surface between these rocks and the other noted host rocks, gabbro and quartz diorite.
- (4) It is apparent from the occurrence of at least 3 types of mineralized intrusives, diorite, gabbro and quartz diorite, that there are multiple intrusive phases present in the altered and mineralized system on the property. Mineralization occurs both as disseminated zones and as mineralized vein systems, probably along the predominant northerly trend of structures noted in the area. Alteration in the form of calcite flooding and quartz and calcite veining was noted in all of the southernmost holes, RC 93-1 through RC 93-5 and therefore is widespread throughout the latter area.



*R. E. Gale*

R.E. Gale, Phd. P.Eng.  
R.E. Gale and Associates Inc.

February 4, 1994

**APPENDIX II**

**31-Element ICP Assay Results  
from Eco-Tech Laboratories Ltd.**

Reverse Circ drilling

ECO-TECH LABORATORIES LTD.  
 10041 EAST TRANS CANADA HWY.  
 KAMLOOPS, B.C. V2C 2J3  
 PHONE - 604-573-5700  
 FAX - 604-573-4557

KINGSTON RESOURCES ETK 93-346  
 703-1112 W. PENDER  
 VANCOUVER, B.C.  
 V6E 2S1

ATTENTION: SCOTT SMITH

SEPTEMBER 10, 1993

VALUES IN PPM UNLESS OTHERWISE REPORTED

50 PERCUSSION DRILL SAMPLES RECEIVED SEPTEMBER 3, 1993  
 PROJECT #: ASHTON

PAGE 1

ET#	DESCRIPTION	AU (ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
1	- RCA 93 - 1 ( 0 - 10 ' )	-	<.2	4.21	10	4	60	<5	2.70	<1	42	27	600	8.31	.05	<10	1.41	437	<1	.24	28	220	22	15	<20	162	.22	<10	617	<10	9	46
2	- RCA 93 - 1 ( 10 - 20 ' )	5	<.2	4.09	20	4	60	<5	2.59	<1	46	57	604	9.14	.04	<10	1.38	433	<1	.24	28	190	20	20	<20	143	.21	10	696	<10	8	59
3	- RCA 93 - 1 ( 20 - 30 ' )	-	<.2	3.93	20	4	60	<5	2.59	<1	46	40	565	9.55	.03	<10	1.33	408	<1	.22	27	160	20	20	<20	132	.21	<10	731	<10	8	61
4	- RCA 93 - 1 ( 30 - 40 ' )	5	<.2	4.31	15	6	85	<5	3.63	<1	48	10	826	9.48	.04	<10	1.51	585	<1	.18	24	<10	18	10	<20	151	.28	10	862	<10	10	48
5	- RCA 93 - 1 ( 40 - 50 ' )	-	<.2	4.51	20	8	130	<5	3.64	<1	43	8	923	8.38	.04	<10	1.56	611	<1	.17	20	<10	26	20	<20	217	.28	10	657	<10	12	59
6	- RCA 93 - 1 ( 50 - 60 ' )	10	<.2	3.58	15	8	75	<5	2.57	<1	50	27	639	9.82	.05	<10	2.16	674	<1	.07	29	<10	14	15	<20	91	.29	10	794	<10	11	53
7	- RCA 93 - 1 ( 60 - 70 ' )	-	<.2	2.38	15	30	60	<5	2.54	<1	31	28	379	6.04	.06	<10	1.32	440	<1	.04	14	1050	28	15	<20	69	.30	<10	367	<10	21	72
8	- RCA 93 - 1 ( 70 - 80 ' )	10	<.2	3.89	10	12	70	<5	3.71	<1	39	7	664	7.54	.04	<10	1.47	420	<1	.14	18	<10	52	15	<20	163	.21	<10	653	<10	8	51
9	- RCA 93 - 1 ( 80 - 90 ' )	-	<.2	2.98	10	6	55	<5	3.71	<1	36	11	456	7.21	.03	<10	1.27	528	<1	.04	14	610	14	15	<20	69	.31	<10	515	<10	19	52
10	- RCA 93 - 1 ( 90 - 100 ' )	5	<.2	4.19	10	8	70	<5	3.40	<1	43	12	570	8.60	.03	<10	1.41	473	<1	.18	17	70	18	10	<20	174	.24	<10	711	<10	9	45
11	- RCA 93 - 1 ( 100 - 110 ' )	-	<.2	4.25	5	6	60	<5	3.96	<1	45	16	627	8.66	.03	<10	1.72	495	<1	.11	18	10	16	15	<20	116	.22	<10	661	<10	9	46
12	- RCA 93 - 1 ( 110 - 120 ' )	10	<.2	3.97	10	8	55	<5	3.51	<1	41	11	562	7.95	.03	<10	1.49	461	<1	.10	20	50	16	20	<20	119	.21	10	605	<10	8	46
13	- RCA 93 - 1 ( 120 - 130 ' )	-	<.2	3.82	10	28	45	<5	3.57	<1	31	13	454	5.92	.03	<10	1.20	391	<1	.09	15	50	20	10	<20	112	.18	<10	448	<10	8	39
14	- RCA 93 - 1 ( 130 - 140 ' )	5	<.2	4.46	20	12	65	<5	3.93	<1	46	11	681	9.50	.02	<10	1.34	474	<1	.15	20	<10	26	15	<20	141	.29	<10	842	<10	11	50
15	- RCA 93 - 1 ( 140 - 150 ' )	-	<.2	4.29	15	12	65	<5	3.41	<1	48	17	676	10.99	.03	<10	1.16	502	<1	.19	22	<10	18	15	<20	161	.30	10	999	<10	10	48
16	- RCA 93 - 1 ( 150 - 160 ' )	10	<.2	3.93	15	62	45	<5	3.89	<1	43	40	636	8.19	.01	<10	1.32	535	<1	.06	17	<10	18	10	<20	115	.31	<10	696	<10	13	52
17	- RCA 93 - 1 ( 160 - 170 ' )	-	<.2	2.03	10	80	20	<5	4.45	<1	22	55	304	3.17	.01	<10	1.15	458	2	.04	7	360	12	10	<20	90	.22	<10	178	<10	15	33
18	- RCA 93 - 1 ( 170 - 180 ' )	10	<.2	4.18	25	100	40	<5	4.73	<1	37	31	490	7.03	<.01	<10	1.82	696	<1	.03	17	170	18	20	<20	150	.33	<10	534	<10	17	52
19	- RCA 93 - 1 ( 180 - 190 ' )	-	<.2	3.67	20	32	45	<5	4.45	<1	37	15	502	7.26	.02	<10	1.45	458	<1	.09	15	100	20	15	<20	122	.24	<10	534	<10	11	46
20	- RCA 93 - 1 ( 190 - 200 ' )	5	<.2	2.90	5	14	35	<5	2.11	<1	21	7	102	4.75	.02	<10	1.16	321	<1	.06	4	120	18	5	<20	58	.10	<10	160	<10	4	38

1200 69.09

PAGE 2

ET#	DESCRIPTION	AU (ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	HG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
21	RCA 93 - 1 ( 200 - 210')	-	<.2	6.06	55	50	60	<5	5.23	<1	41	13	351	8.42	.02	<10	1.89	608	<1	.07	13	40	32	20	<20	111	.25	<10	391	<10	11	62
22	RCA 93 - 1 ( 210 - 220')	5	<.2	4.67	40	96	40	<5	4.70	<1	22	51	406	3.93	.03	<10	.83	343	1	.08	28	240	26	10	<20	96	.08	<10	127	<10	5	26
23	RCA 93 - 1 ( 220 - 230')	-	<.2	2.79	95	118	25	<5	2.64	<1	31	38	675	5.80	<.01	<10	.90	621	1	.04	38	660	18	15	<20	45	.05	<10	54	<10	3	65
24	RCA 93 - 1 ( 230 - 240')	5	<.2	2.01	85	232	25	<5	5.59	<1	32	89	466	5.75	<.01	<10	1.13	1361	2	.01	67	1120	10	10	<20	47	.06	<10	95	<10	6	185
25	RCA 93 - 1 ( 240 - 250')	-	<.2	2.63	25	142	30	<5	3.54	<1	15	55	290	2.75	.03	<10	.84	510	2	.08	20	310	18	5	<20	58	.09	<10	72	<10	6	84
26	RCA 93 - 1 ( 250 - 260')	5	<.2	4.14	20	148	30	<5	5.69	<1	18	46	333	2.50	.02	<10	1.16	393	2	.05	10	110	26	5	<20	64	.14	<10	114	<10	10	29
27	RCA 93 - 1 ( 260 - 270')	-	<.2	4.60	25	164	25	<5	6.38	<1	17	36	307	2.44	.02	<10	1.26	406	2	.04	9	50	26	10	<20	61	.14	<10	107	<10	10	29
28	RCA 93 - 1 ( 270 - 280')	5	<.2	3.49	10	58	35	<5	4.66	<1	37	31	363	7.61	.01	<10	1.67	575	<1	.05	18	50	18	10	<20	104	.35	<10	375	<10	18	49
29	RCA 93 - 1 ( 280 - 290')	-	<.2	3.94	15	22	55	10	3.63	<1	43	21	224	10.05	.02	<10	1.50	541	<1	.12	20	220	16	10	<20	110	.29	<10	427	<10	12	52
30	RCA 93 - 1 ( 290 - 300')	10	<.2	3.20	10	8	30	<5	5.36	<1	19	66	220	3.29	.03	<10	1.29	405	4	.07	11	110	20	10	<20	93	.18	<10	182	<10	12	39
31	RCA 93 - 1 ( 300 - 310')	-	<.2	2.59	10	6	20	<5	4.10	<1	15	25	157	2.41	.02	<10	1.08	317	1	.04	8	90	18	5	<20	83	.14	<10	112	<10	9	34
32	RCA 93 - 1 ( 310 - 320')	10	<.2	3.26	<5	22	40	<5	4.15	<1	38	20	321	8.04	.01	<10	1.51	513	<1	.04	19	40	14	15	<20	103	.27	<10	596	<10	12	56
33	RCA 93 - 1 ( 320 - 330')	-	<.2	5.60	10	182	55	<5	5.23	<1	38	29	312	8.53	.02	<10	2.23	648	<1	.05	28	300	18	30	<20	117	.10	<10	418	<10	4	71
34	RCA 93 - 1 ( 330 - 340')	5	<.2	6.07	15	20	65	15	4.68	<1	42	62	52	9.89	.02	<10	2.31	820	<1	.06	33	150	20	45	<20	127	.21	<10	387	<10	11	102
35	RCA 93 - 1 ( 340 - 350')	-	<.2	4.92	15	20	45	<5	5.61	<1	30	147	178	6.18	.01	<10	1.62	546	1	.06	45	<10	24	15	<20	148	.21	<10	399	<10	10	43
36	RCA 93 - 1 ( 350 - 360')	70	<.2	5.31	15	248	55	<5	4.99	<1	37	129	377	7.87	.02	<10	1.59	521	<1	.07	57	<10	26	15	<20	154	.27	<10	567	<10	13	49
37	RCA 93 - 1 ( 360 - 370')	-	<.2	3.95	25	138	55	<5	3.39	<1	44	173	500	9.55	.01	<10	1.92	600	<1	.06	81	<10	18	15	<20	118	.32	<10	658	<10	13	64
38	RCA 93 - 1 ( 370 - 380')	15	<.2	2.28	20	100	40	<5	5.21	<1	39	34	329	8.27	<.01	<10	1.59	400	<1	.02	24	<10	10	20	<20	188	.36	<10	498	<10	17	36
39	RCA 93 - 1 ( 380 - 390')	-	<.2	3.15	25	798	25	<5	4.84	<1	24	83	910	2.95	.02	<10	1.31	311	4	.05	26	220	18	10	<20	66	.12	<10	109	<10	10	27
40	RCA 93 - 1 ( 390 - 400')	10	<.2	2.46	55	1086	25	<5	4.17	<1	78	44	1843	5.78	<.01	<10	1.79	415	4	.02	96	270	12	15	<20	67	.09	<10	88	<10	5	37
41	RCA 93 - 1 ( 400 - 410')	-	<.2	2.60	70	330	30	<5	2.54	<1	70	50	1466	8.09	<.01	<10	2.03	602	2	.02	89	130	16	15	<20	63	.14	<10	312	<10	5	60
42	RCA 93 - 1 ( 410 - 420')	5	<.2	3.14	15	26	30	<5	2.82	<1	35	32	571	6.36	.01	<10	1.55	448	<1	.03	30	30	16	15	<20	95	.16	<10	319	<10	8	42
43	RCA 93 - 1 ( 420 - 430')	-	<.2	3.30	50	48	40	<5	3.44	<1	65	43	1362	7.80	.01	<10	2.35	589	3	.05	66	380	18	20	<20	106	.18	<10	366	<10	7	50
44	RCA 93 - 1 ( 430 - 440')	10	<.2	2.73	50	22	20	<5	4.10	<1	47	53	947	4.81	<.01	<10	1.76	471	5	.04	73	250	16	15	<20	56	.11	<10	100	<10	7	32
45	RCA 93 - 1 ( 440 - 450')	-	<.2	3.44	15	78	35	<5	2.87	<1	46	40	606	7.72	.01	<10	2.13	531	<1	.08	42	40	20	20	<20	95	.20	<10	510	<10	8	49

935 109.56

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ET#	DESCRIPTION	AU (ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
46	RCA 93 - 1 ( 450 - 460')	5	<.2	3.36	20	320	40	<5	2.65	<1	46	42	826	7.63	.02	<10	2.33	544	<1	.06	41	<10	16	15	<20	111	.29	<10	516	<10	13	45
47	RCA 93 - 1 ( 460 - 470')	-	<.2	3.88	25	38	45	<5	3.43	<1	45	65	996	6.94	.02	<10	2.06	502	<1	.15	38	<10	20	20	<20	240	.22	<10	458	<10	10	44
48	RCA 93 - 1 ( 470 - 480')	10	<.2	3.47	15	30	30	<5	3.65	<1	33	53	362	5.59	.01	<10	1.80	425	<1	.07	23	<10	20	10	<20	227	.23	<10	398	<10	11	34
49	RCA 93 - 1 ( 480 - 490')	-	<.2	4.30	10	18	60	<5	3.48	<1	25	57	596	4.45	.04	<10	1.03	284	2	.34	20	10	30	10	<20	549	.13	<10	377	<10	7	29
50	RCA 93 - 1 ( 490 - 500')	5	<.2	2.77	10	36	55	<5	2.85	<1	33	41	685	6.35	.03	<10	1.35	391	<1	.11	26	<10	16	15	<20	186	.19	<10	509	<10	10	32

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NOTE: < = LESS THAN

*Frank J. Pezzotta*  
 ECO-TECH LABORATORIES LTD.  
 FRANK J. PEZZOTTA, A.Sc.T.  
 B.C. Certified Assayer

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KINGSTON RESOURCES ETK 93-347  
 703-1112 W. PENDER  
 VANCOUVER, B.C.  
 V6E 2S1

ATTENTION: SCOTT SMITH

SEPTEMBER 14, 1993

VALUES IN PPM UNLESS OTHERWISE REPORTED

76 PERCUSSION DRILL SAMPLES RECEIVED SEPTEMBER 3, 1993  
 PROJECT #: ASHTON

PAGE 1

ET#	DESCRIPTION	AU (ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
1	- RCA 93 - 2 ( 0 - 10 ' )	-	<.2	3.61	15	8	80	<5	3.36	<1	33	80	194	6.44	.09	<10	1.85	703	1	.14	36	620	32	10	<20	143	.26	<10	363	<10	15	60
2	- RCA 93 - 2 ( 10 - 20 ' )	5	<.2	3.90	10	6	70	<5	3.32	<1	41	38	544	8.43	.06	<10	1.60	538	<1	.14	26	210	16	10	<20	112	.30	<10	657	<10	11	50
3	- RCA 93 - 2 ( 20 - 30 ' )	-	<.2	2.96	10	6	45	<5	3.16	<1	21	30	163	5.87	.04	<10	.85	652	<1	.05	7	720	16	5	<20	78	.25	10	149	<10	25	64
4	- RCA 93 - 2 ( 30 - 40 ' )	5	<.2	3.19	10	66	50	<5	3.20	<1	26	23	171	6.17	.06	<10	1.25	758	<1	.08	6	1120	20	10	<20	50	.32	<10	198	<10	30	70
5	- RCA 93 - 2 ( 40 - 50 ' )	-	<.2	4.85	10	142	80	5	3.71	<1	33	73	130	6.67	.03	<10	1.78	564	<1	.30	24	200	22	15	<20	136	.29	<10	381	<10	13	56
6	- RCA 93 - 2 ( 50 - 60 ' )	5	<.2	5.22	10	14	75	<5	4.18	<1	38	56	569	6.90	.04	<10	1.38	417	<1	.37	26	150	28	10	<20	199	.31	<10	576	<10	11	45
7	- RCA 93 - 2 ( 60 - 70 ' )	-	<.2	2.64	<5	8	35	<5	2.24	<1	20	8	276	4.85	.03	<10	.61	324	<1	.13	10	380	14	5	<20	79	.17	<10	321	<10	10	38
8	- RCA 93 - 2 ( 70 - 80 ' )	15	<.2	3.22	5	10	60	<5	3.07	<1	34	19	554	7.19	.07	<10	.73	390	<1	.12	22	780	14	<5	<20	102	.27	<10	609	<10	13	46
9	- RCA 93 - 2 ( 80 - 90 ' )	-	<.2	2.58	5	10	35	<5	3.16	<1	32	21	308	6.39	.03	<10	1.00	454	<1	.05	16	1050	12	5	<20	130	.27	<10	317	<10	19	40
10	- RCA 93 - 2 ( 90 - 100 ' )	10	<.2	3.12	10	12	55	<5	3.19	<1	33	20	340	8.25	.06	<10	.96	589	<1	.08	15	1090	14	5	<20	68	.31	<10	496	<10	22	60
11	- RCA 93 - 2 ( 100 - 110 ' )	-	<.2	3.28	10	10	45	5	4.13	<1	32	17	149	6.49	.07	<10	1.63	718	<1	.04	10	1200	14	10	<20	60	.39	<10	292	<10	26	57
12	- RCA 93 - 2 ( 110 - 120 ' )	5	<.2	4.12	5	10	65	<5	3.72	<1	51	8	920	10.67	.07	<10	1.48	630	<1	.22	35	240	16	15	<20	184	.40	<10	827	<10	15	75
13	- RCA 93 - 2 ( 120 - 130 ' )	-	<.2	3.63	10	8	35	<5	4.21	<1	44	2	899	8.41	.02	<10	1.43	535	<1	.09	25	20	14	10	<20	104	.35	10	703	<10	11	46
14	- RCA 93 - 2 ( 130 - 140 ' )	5	<.2	4.59	5	10	45	<5	4.22	<1	51	8	857	10.33	.01	<10	1.83	613	<1	.07	27	<10	14	10	<20	82	.38	10	946	<10	10	50
15	- RCA 93 - 2 ( 140 - 150 ' )	-	<.2	4.36	5	6	45	<5	4.02	<1	55	9	1075	10.32	.02	<10	2.15	676	<1	.09	28	<10	14	10	<20	101	.37	<10	913	<10	10	46
16	- RCA 93 - 2 ( 150 - 160 ' )	5	<.2	3.75	15	6	45	<5	4.17	<1	46	5	908	8.87	.03	<10	1.70	590	<1	.10	24	<10	14	5	<20	113	.31	10	786	<10	8	43
17	- RCA 93 - 2 ( 160 - 170 ' )	-	<.2	3.47	5	4	25	<5	4.52	<1	33	20	628	5.24	.01	<10	1.82	532	<1	.02	16	70	16	10	<20	145	.25	<10	415	<10	10	35
18	- RCA 93 - 2 ( 170 - 180 ' )	5	<.2	2.91	10	6	140	<5	10.22	<1	38	15	1501	5.82	.01	<10	1.49	3407	2	.01	21	270	8	10	<20	151	.26	10	302	<10	16	40
19	- RCA 93 - 2 ( 180 - 190 ' )	-	<.2	3.68	10	10	50	<5	4.80	<1	47	33	744	8.81	.03	<10	2.09	912	<1	.05	25	20	14	15	<20	109	.34	<10	720	<10	12	54
20	- RCA 93 - 2 ( 190 - 200 ' )	5	<.2	3.66	5	8	45	<5	3.27	<1	60	9	1350	11.96	.02	<10	2.16	708	<1	.05	34	<10	12	10	<20	71	.40	10	1140	<10	9	61

1125 79.87



PAGE 2

ET#	DESCRIPTION	AU (ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
21	RCA 93 - 2 ( 200 - 210' )	-	<.2	4.25	5	8	45	<5	3.92	<1	55	17	920	11.12	.01	<10	1.93	635	<1	.11	29	<10	12	10	<20	117	.40	20	1027	<10	11	55
22	RCA 93 - 2 ( 210 - 220' )	5	<.2	4.24	5	14	55	<5	3.13	<1	62	9	1588	12.64	.02	<10	1.78	516	<1	.23	39	<10	12	15	<20	177	.38	10	1224	<10	8	53
23	RCA 93 - 2 ( 220 - 230' )	-	<.2	5.51	10	90	55	<5	4.31	<1	46	49	626	9.52	.02	<10	1.56	564	<1	.36	29	<10	26	10	<20	296	.37	<10	825	<10	10	59
24	RCA 93 - 2 ( 230 - 240' )	5	<.2	4.38	10	10	45	<5	3.40	3	34	34	277	6.89	.02	<10	1.30	445	<1	.22	20	<10	20	5	<20	173	.23	<10	511	<10	6	56
25	RCA 93 - 2 ( 240 - 250' )	-	<.2	4.69	15	10	60	<5	4.05	<1	42	24	729	8.53	.03	<10	1.62	598	<1	.19	23	<10	18	5	<20	155	.33	<10	722	<10	9	54
26	RCA 93 - 2 ( 250 - 260' )	5	<.2	3.38	10	8	45	<5	4.31	<1	37	12	762	7.39	.03	<10	1.43	631	<1	.12	22	30	12	10	<20	146	.29	<10	626	<10	9	44
27	RCA 93 - 2 ( 260 - 270' )	-	<.2	3.64	15	6	60	<5	4.15	<1	44	35	570	7.98	.04	<10	2.05	792	<1	.07	21	120	12	15	<20	125	.40	10	600	<10	15	52
28	RCA 93 - 2 ( 270 - 280' )	5	<.2	2.70	10	8	35	<5	2.99	<1	26	33	261	4.87	.04	<10	1.41	644	<1	.06	12	420	14	5	<20	120	.24	<10	290	<10	11	42
29	RCA 93 - 2 ( 280 - 290' )	-	<.2	3.08	10	4	45	<5	3.24	<1	35	32	267	5.45	.04	<10	2.27	733	<1	.04	19	390	16	10	<20	156	.29	10	313	<10	13	59
30	RCA 93 - 2 ( 290 - 300' )	5	<.2	3.61	15	8	40	<5	3.83	<1	37	18	344	6.12	.02	<10	1.94	678	<1	.05	18	440	16	10	<20	183	.32	<10	389	<10	17	48
31	RCA 93 - 2 ( 300 - 310' )	-	<.2	4.59	10	16	50	<5	4.26	<1	39	137	430	6.91	.03	<10	1.96	674	<1	.18	30	100	20	10	<20	193	.29	<10	504	<10	11	47
32	RCA 93 - 2 ( 310 - 320' )	190	<.2	3.78	5	52	45	<5	3.66	<1	29	153	268	4.83	.03	<10	1.57	473	<1	.12	21	220	22	<5	<20	155	.24	<10	313	<10	11	35
33	RCA 93 - 3 ( 0 - 10' )	-	<.2	3.10	10	4	55	<5	3.66	<1	31	36	202	6.05	.07	<10	1.96	684	<1	.14	24	580	14	10	<20	118	.16	<10	327	<10	11	51
34	RCA 93 - 3 ( 10 - 20' )	5	<.2	2.71	10	4	45	<5	3.19	<1	34	38	364	6.03	.05	<10	1.75	609	<1	.10	24	680	14	10	<20	129	.18	<10	320	<10	11	47
35	RCA 93 - 3 ( 20 - 30' )	-	<.2	2.86	10	4	45	<5	2.18	<1	58	22	804	12.33	.03	<10	1.90	548	<1	.03	37	<10	8	5	<20	83	.35	20	1193	<10	10	57
36	RCA 93 - 3 ( 30 - 40' )	5	<.2	2.92	10	4	35	<5	5.23	<1	19	25	152	5.09	.08	<10	1.22	488	<1	.02	10	570	14	10	<20	47	.03	<10	213	<10	14	47
37	RCA 93 - 3 ( 40 - 50' )	-	<.2	3.58	10	6	45	<5	6.92	<1	37	5	589	7.83	.05	<10	2.07	864	<1	.08	25	<10	10	10	<20	84	.08	<10	594	<10	4	56
38	RCA 93 - 3 ( 50 - 60' )	15	<.2	3.80	30	4	55	<5	5.48	<1	44	4	745	8.53	.06	<10	2.83	1008	<1	.04	26	<10	12	10	<20	84	.19	10	682	<10	9	60
39	RCA 93 - 3 ( 60 - 70' )	-	<.2	2.36	75	4	50	<5	4.24	<1	30	37	365	5.92	.04	<10	1.49	582	<1	.03	13	500	10	10	<20	71	.18	<10	283	<10	20	35
40	RCA 93 - 3 ( 70 - 80' )	60	<.2	3.05	185	4	50	<5	2.70	<1	54	17	825	9.26	.04	<10	2.06	509	<1	.05	19	10	10	10	<20	86	.28	<10	707	<10	8	52
41	RCA 93 - 3 ( 80 - 90' )	-	<.2	1.97	40	4	35	<5	2.16	<1	59	27	815	9.27	.02	<10	1.66	478	<1	.03	27	<10	6	<5	<20	69	.30	10	747	<10	9	47
42	RCA 93 - 3 ( 90 - 100' )	5	<.2	1.49	25	4	35	<5	2.19	<1	57	33	837	10.66	.02	<10	1.28	398	<1	.02	27	<10	2	5	<20	58	.31	10	865	<10	7	45
43	RCA 93 - 3 ( 100 - 110' )	-	<.2	2.11	30	6	35	<5	2.89	<1	49	40	931	10.27	.01	<10	1.78	600	<1	.02	27	120	6	10	<20	69	.30	<10	758	<10	9	56
44	RCA 93 - 3 ( 110 - 120' )	5	<.2	2.39	70	8	40	<5	6.44	<1	40	11	494	8.14	.03	<10	1.67	757	<1	.02	16	40	6	10	<20	77	.21	<10	611	<10	8	47
45	RCA 93 - 3 ( 120 - 130' )	-	<.2	1.82	30	10	35	<5	12.59	<1	23	15	91	5.19	.07	<10	1.04	772	<1	<.01	5	170	4	45	<20	117	.10	<10	176	<10	12	39

CA  
93-2: 45.25

93-3: 59.87

BA  
93-2: 580

93-3: 560

ET#	DESCRIPTION	AU (ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
46	RCA 93 - 3 ( 130 - 140')	5	<.2	1.42	10	6	20	<5	>15	<1	7	6	69	1.35	.03	<10	.88	354	<1	<.01	3	<10	2	10	<20	221	.02	<10	3	<10	4	17
47	RCA 93 - 3 ( 140 - 150')	-	<.2	2.28	20	16	20	<5	10.40	<1	27	26	465	4.34	<.01	<10	1.86	503	<1	.01	9	140	8	10	<20	106	.20	<10	181	<10	12	61
48	RCA 93 - 3 ( 150 - 160')	5	<.2	2.67	10	8	45	<5	2.67	<1	53	14	595	10.31	.03	<10	1.61	582	<1	.07	18	20	10	5	<20	74	.30	10	852	<10	7	47
49	RCA 93 - 3 ( 160 - 170')	-	<.2	3.36	20	6	45	<5	3.09	<1	47	11	322	9.68	.03	<10	1.98	555	<1	.10	10	<10	10	10	<20	122	.25	<10	796	<10	5	44
50	RCA 93 - 3 ( 170 - 180')	5	<.2	3.69	10	6	55	5	3.72	<1	21	35	30	3.78	.02	<10	2.30	490	<1	.21	14	<10	20	15	<20	147	.11	<10	176	<10	3	23
51	RCA 93 - 3 ( 180 - 190')	-	<.2	4.35	10	4	50	<5	3.19	<1	51	12	531	8.87	.02	<10	3.17	695	<1	.21	13	<10	16	15	<20	104	.17	<10	608	<10	4	38
52	RCA 93 - 3 ( 190 - 200')	5	<.2	3.98	10	4	40	<5	4.31	<1	45	14	414	8.71	.03	<10	3.35	706	<1	.13	14	<10	12	15	<20	87	.18	<10	590	<10	5	37
53	RCA 93 - 3 ( 200 - 210')	-	<.2	2.97	30	6	40	<5	7.19	<1	41	15	518	7.99	.03	<10	2.23	964	<1	.06	18	30	8	15	<20	83	.07	<10	580	<10	4	42
54	RCA 93 - 3 ( 210 - 220')	5	<.2	2.20	20	8	30	<5	8.75	<1	30	13	332	6.03	.03	<10	2.17	938	<1	.01	11	140	4	15	<20	92	.03	<10	350	<10	4	49
55	RCA 93 - 3 ( 220 - 230')	-	<.2	2.36	15	6	35	<5	7.36	<1	31	8	304	6.36	.02	<10	1.91	860	<1	<.01	13	240	6	15	<20	72	.01	<10	342	<10	5	45
56	RCA 93 - 3 ( 230 - 240')	5	<.2	3.85	25	6	90	<5	5.58	<1	55	17	879	10.23	.04	<10	2.40	875	<1	.09	33	180	10	10	<20	86	<.01	<10	702	<10	<1	66
57	RCA 93 - 3 ( 240 - 250')	-	<.2	2.77	5	6	60	<5	4.10	<1	31	22	498	6.47	.03	<10	2.13	787	<1	.08	18	180	12	10	<20	63	.05	<10	427	<10	3	42
58	RCA 93 - 3 ( 250 - 260')	10	<.2	3.34	10	6	45	<5	5.76	<1	39	24	758	7.89	.03	<10	2.28	885	<1	.10	20	70	10	10	<20	91	.06	10	624	<10	3	48
59	RCA 93 - 3 ( 260 - 270')	-	<.2	3.70	10	4	40	<5	5.55	<1	36	11	602	7.29	.02	<10	2.08	704	<1	.18	15	80	14	10	<20	119	.07	<10	569	<10	4	43
60	RCA 93 - 3 ( 270 - 280')	5	<.2	4.10	10	6	40	<5	5.21	<1	45	25	688	8.62	.04	<10	3.62	789	<1	.09	16	20	12	15	<20	90	.14	<10	678	<10	6	46
61	RCA 93 - 3 ( 280 - 290')	-	<.2	2.60	10	4	30	<5	2.67	<1	28	32	368	5.87	.03	<10	1.79	637	<1	.07	12	240	12	10	<20	57	.13	<10	425	<10	6	39
62	RCA 93 - 3 ( 290 - 300')	5	<.2	2.68	10	8	30	<5	3.42	<1	33	26	484	6.79	.03	<10	1.73	702	<1	.08	12	190	12	10	<20	63	.16	<10	498	<10	7	42
63	RCA 93 - 3 ( 300 - 310')	-	<.2	3.08	10	12	45	<5	3.67	<1	46	13	867	9.42	.03	<10	1.86	613	<1	.12	22	10	12	10	<20	110	.25	<10	871	<10	7	40
64	RCA 93 - 3 ( 310 - 320')	165	<.2	3.73	10	8	45	<5	3.88	<1	41	10	718	8.14	.03	<10	1.70	543	<1	.22	16	30	16	10	<20	184	.22	<10	708	<10	6	39
65	RCA 93 - 3 ( 320 - 330')	-	<.2	3.96	15	14	40	<5	4.05	<1	36	9	614	7.15	.02	<10	1.60	472	<1	.18	17	50	18	10	<20	234	.19	<10	607	<10	6	37
66	RCA 93 - 3 ( 330 - 340')	5	<.2	4.39	15	26	45	<5	3.83	<1	41	14	676	9.05	.02	<10	1.39	458	<1	.32	24	<10	18	5	<20	333	.23	<10	788	<10	5	38
67	RCA 93 - 3 ( 340 - 350')	-	<.2	4.33	10	28	50	<5	3.28	<1	39	18	721	8.80	.02	<10	1.17	372	<1	.36	21	<10	18	5	<20	308	.22	<10	820	<10	4	34
68	RCA 93 - 3 ( 350 - 360')	5	<.2	3.81	10	10	45	<5	3.64	<1	39	13	580	8.25	.03	<10	1.53	533	<1	.27	17	20	16	10	<20	218	.23	<10	754	<10	6	41
69	RCA 93 - 3 ( 360 - 370')	-	<.2	2.88	10	6	35	<5	4.92	<1	41	9	638	7.96	.02	<10	2.10	620	<1	.09	18	<10	10	10	<20	80	.22	<10	677	<10	7	42
70	RCA 93 - 3 ( 370 - 380')	5	<.2	3.26	10	8	35	<5	4.60	<1	44	26	481	8.08	.01	<10	2.33	772	<1	.13	21	10	12	10	<20	90	.16	<10	574	<10	7	43

1055 129.84

PAGE 4

ET#	DESCRIPTION	AU (ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
71	RCA 93 - 3 ( 380 - 390')	-	<.2	3.24	10	4	35	<5	4.05	<1	29	12	222	6.37	.02	<10	2.58	704	<1	.15	9	90	14	15	<20	82	.05	<10	348	<10	2	42
72	RCA 93 - 3 ( 390 - 400')	5	<.2	3.16	10	6	40	<5	4.51	<1	44	19	663	8.98	.03	<10	2.07	720	<1	.14	17	100	10	10	<20	121	.24	<10	707	<10	9	52
73	RCA 93 - 3 ( 400 - 410')	-	<.2	2.94	10	6	35	<5	3.98	<1	39	15	391	7.99	.03	<10	1.83	653	<1	.13	13	50	12	15	<20	135	.26	<10	600	<10	10	52
74	RCA 93 - 3 ( 410 - 420')	10	<.2	3.22	10	6	35	<5	3.66	<1	26	12	66	5.87	.03	<10	1.91	755	<1	.21	7	60	14	10	<20	108	.17	<10	300	<10	7	49
75	RCA 93 - 3 ( 420 - 430')	-	<.2	3.86	5	6	40	5	2.75	<1	26	10	65	5.81	.03	<10	1.84	618	<1	.33	7	70	22	10	<20	149	.17	<10	322	<10	5	42
76	RCA 93 - 3 ( 430 - 440')	10	<.2	5.53	15	6	55	10	5.93	<1	35	45	67	7.73	.04	<10	1.93	679	<1	.49	19	<10	20	10	<20	209	.16	<10	509	<10	6	40

240 24.88

QC/DATA:

Repeat #:

30	RCA 93 - 2 ( 290 - 300')	<.2	3.42	15	10	35	<5	3.64	<1	36	17	327	5.85	.02	<10	1.84	646	<1	.05	17	410	16	10	<20	174	.30	<10	371	<10	16	46
70	RCA 93 - 3 ( 370 - 380')	<.2	3.22	15	8	35	<5	4.55	<1	43	25	476	7.99	.02	<10	2.31	761	<1	.13	20	10	12	10	<20	88	.15	<10	566	<10	7	44

STANDARD 1991:		.6	1.99	60	6	150	<5	1.81	<1	20	67	88	3.96	.39	<10	1.03	713	<1	.02	24	620	32	10	<20	65	.12	<10	91	<10	10	93
STANDARD 1991:		1.0	2.00	65	4	155	<5	1.78	<1	21	68	83	3.96	.39	<10	1.08	723	<1	.02	24	630	24	10	<20	63	.12	<10	86	<10	10	68

SC93/KAMISC

*Frank J. Pezzotti*  
 ECO-TECH LABORATORIES LTD.  
 FRANK J. PEZZOTTI, A.Sc.T.  
 B.C. Certified Assayer

ECO-TECH LABORATORIES LTD.  
 10041 EAST TRANS CANADA HWY.  
 KAMLOOPS, B.C. V2C 2J3  
 PHONE - 604-573-5700  
 FAX - 604-573-4557

FEED DOCUMENT THIS DIRECTION  
**IMPORTANT FAX MESSAGE**

TO: *Scott Smith*  
 COMPANY: *Kingston Resources*  
 FROM: *Kingston Resources*  
 NO OF PAGES: *3*  
 RE: *Perforation*

KINGSTON RESOURCES BTK 93-355  
 703-1112 W. PENDEB  
 VANCOUVER, B.C.  
 V6B 2S1

ATTENTION: SCOTT SMITH

61 PERCUSSION DRILL SAMPLES RECEIVED SEPTEMBER 10, 1993

SEPTEMBER 17, 1993

VALUES IN PPM UNLESS OTHERWISE REPORTED

PAGE 1

HT#	DESCRIPTION	AD(ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Z	ZN
1	- RCA 93 - 3 ( 440 - 450')	-	<.2	3.37	80	4	35	<5	2.50	<1	22	17	295	4.50	.02	<10	1.78	378	<1	.18	12	20	<2	15	<20	252	.14	<10	357	<10	8	27
2	- RCA 93 - 3 ( 450 - 460')	5	<.2	3.19	50	8	35	<5	2.93	<1	34	2	1289	6.81	.01	<10	2.68	434	<1	.11	14	<10	<2	20	<20	124	.13	<10	617	<10	6	36
3	- RCA 93 - 3 ( 460 - 470')	-	<.2	3.26	10	6	35	<5	2.05	<1	35	3	1274	6.66	.01	<10	3.11	390	<1	.09	14	<10	<2	15	<20	100	.14	<10	638	<10	6	32
4	- RCA 93 - 3 ( 470 - 480')	<5	<.2	3.25	15	8	30	<5	4.77	<1	27	4	745	5.59	.03	<10	2.20	585	<1	.03	12	<10	<2	15	<20	115	.02	<10	449	<10	2	36
5	- RCA 93 - 3 ( 480 - 490')	-	<.2	3.67	10	6	35	<5	3.31	<1	30	4	1009	6.45	.02	<10	2.02	509	<1	.18	14	<10	<2	15	<20	139	.08	<10	600	<10	3	34
6	- RCA 93 - 3 ( 490 - 500')	5	<.2	3.14	15	8	30	<5	3.32	<1	28	3	697	5.92	.02	<10	1.80	486	<1	.11	14	<10	<2	15	<20	128	.07	<10	531	<10	4	35
7	- RCA 93 - 4 ( 0 - 10')	-	<.2	3.39	10	6	30	<5	1.79	<1	28	18	784	6.14	.02	<10	1.41	249	1	.15	14	<10	<2	15	<20	190	.17	<10	554	<10	7	29
8	- RCA 93 - 4 ( 10 - 20')	15	<.2	3.74	15	8	35	<5	1.58	<1	32	4	655	6.58	.02	<10	1.60	242	<1	.24	12	<10	<2	15	<20	245	.18	<10	624	<10	7	29
9	- RCA 93 - 4 ( 20 - 30')	-	<.2	3.35	15	6	25	<5	2.00	<1	26	16	438	4.81	.01	<10	1.63	264	<1	.06	10	380	<2	10	<20	109	.19	<10	344	<10	11	23
10	- RCA 93 - 4 ( 30 - 40')	10	<.2	3.17	20	10	30	<5	1.61	<1	28	4	905	6.41	.02	<10	1.49	290	<1	.10	14	<10	<2	15	<20	92	.21	<10	669	<10	9	30
11	- RCA 93 - 4 ( 40 - 50')	-	<.2	2.35	15	4	20	<5	1.09	<1	18	4	381	3.96	.01	<10	1.01	171	<1	.14	10	<10	<2	10	<20	120	.09	<10	344	<10	3	22
12	- RCA 93 - 4 ( 50 - 60')	5	<.2	3.85	15	8	40	<5	1.73	<1	34	2	1110	7.81	.02	<10	1.34	253	<1	.28	17	<10	<2	15	<20	258	.24	<10	830	<10	9	32
13	- RCA 93 - 4 ( 60 - 70')	-	<.2	2.89	20	6	30	<5	1.29	<1	26	4	977	5.70	.02	<10	1.21	198	<1	.18	14	<10	<2	10	<20	129	.15	<10	559	<10	5	30
14	- RCA 93 - 4 ( 70 - 80')	<5	<.2	4.19	15	8	40	<5	1.76	<1	32	8	913	6.55	.04	<10	1.58	259	<1	.28	18	<10	<2	15	<20	186	.17	<10	601	<10	6	31
15	- RCA 93 - 4 ( 80 - 90')	-	<.2	2.55	15	6	20	<5	3.13	<1	27	11	594	4.40	.01	<10	1.31	393	<1	.07	16	30	<2	10	<20	107	.23	<10	406	<10	12	87
16	- RCA 93 - 4 ( 90 - 100')	<5	<.2	2.35	15	104	20	<5	5.48	<1	33	14	1054	3.76	<.01	<10	1.06	355	<1	.02	15	60	<2	15	<20	147	.12	<10	206	<10	7	40
17	- RCA 93 - 4 ( 100 - 110')	-	<.2	3.79	20	12	35	<5	1.99	<1	35	3	1192	6.93	.02	<10	1.90	359	<1	.15	25	<10	<2	15	<20	202	.28	<10	655	<10	12	40
18	- RCA 93 - 4 ( 110 - 120')	<5	<.2	3.25	15	10	25	<5	2.04	<1	30	6	1348	5.38	.01	<10	1.75	316	<1	.02	24	<10	<2	20	<20	186	.23	<10	483	<10	11	35
19	- RCA 93 - 4 ( 120 - 130')	-	<.2	3.07	15	8	25	<5	1.21	<1	23	16	622	5.06	.01	<10	1.55	261	<1	.20	19	<10	<2	15	<20	181	.13	<10	295	<10	5	30
20	- RCA 93 - 4 ( 130 - 140')	5	<.2	3.03	15	6	25	<5	1.66	<1	22	8	742	4.12	.01	<10	1.67	240	<1	.13	18	<10	<2	15	<20	160	.10	<10	244	<10	4	30

2836

ETH	DESCRIPTION	AU(ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CE	CU	FE(%)	K(%)	LA	MG(%)	MO	NO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	Zn	V	W	Y	ZN
21	RCA 93 - 4 ( 140 - 150')	< .2	3.71	20	4	25	<5	1.42	<1	22	41	460	4.10	.01	<10	1.25	186	<1	.31	24	<10	<2	10	<20	239	.07	<10	364	<10	1	22	
22	RCA 93 - 4 ( 150 - 160')	5 <.2	6.28	15	8	35	<5	2.41	<1	24	193	462	4.42	.01	<10	1.95	263	<1	.42	31	<10	<2	20	<20	345	.09	<10	372	<10	4	23	
23	RCA 93 - 4 ( 160 - 170')	< .2	4.43	15	4	20	<5	1.82	<1	9	103	171	1.51	<.01	<10	.93	134	<1	.54	12	10	<2	5	<20	377	.01	<10	67	<10	<1	31	
24	RCA 93 - 4 ( 170 - 180')	<5 <.2	3.59	10	6	25	<5	1.47	<1	10	88	144	1.69	.01	<10	1.02	145	<1	.36	11	<10	<2	15	<20	248	.02	<10	79	<10	1	12	
25	RCA 93 - 4 ( 180 - 190')	< .2	2.44	15	4	30	<5	1.24	<1	9	43	225	1.42	<.01	<10	.74	116	<1	.10	8	<10	<2	5	<20	113	.04	<10	115	<10	2	10	
26	RCA 93 - 4 ( 190 - 200')	<5 <.2	3.52	10	8	15	<5	1.86	<1	13	84	222	2.10	.01	<10	1.12	181	<1	.10	9	10	<2	10	<20	131	.09	<10	151	<10	5	15	
27	RCA 93 - 4 ( 200 - 210')	< .2	4.34	15	14	40	<5	1.88	<1	27	53	157	6.85	.02	<10	1.44	278	<1	.31	20	<10	<2	10	<20	273	.16	<10	420	<10	5	28	
28	RCA 93 - 4 ( 210 - 220')	<5 <.2	1.94	10	8	35	5	1.47	<1	26	28	132	6.38	.01	<10	2.13	340	<1	.14	16	<10	<2	15	<20	97	.14	<10	224	<10	5	35	
29	RCA 93 - 4 ( 220 - 230')	< .2	3.36	15	4	20	<5	1.40	<1	12	37	213	2.37	.02	<10	.93	132	<1	.35	11	<10	<2	10	<20	308	.04	<10	149	<10	1	14	
30	RCA 93 - 4 ( 230 - 240')	40 <.2	3.31	10	4	20	<5	1.40	<1	12	40	430	2.11	.02	<10	.69	117	<1	.35	10	<10	<2	5	<20	260	.04	<10	145	<10	1	13	
31	RCA 93 - 4 ( 240 - 250')	< .2	3.01	15	8	20	<5	1.12	<1	20	7	346	3.08	<.01	<10	1.07	140	<1	.33	6	<10	<2	10	<20	244	.06	<10	214	<10	2	19	
32	RCA 93 - 4 ( 250 - 260')	5 <.2	4.09	10	6	35	<5	1.54	<1	29	<1	279	4.96	.01	<10	1.57	223	<1	.39	6	<10	<2	10	<20	282	.13	<10	364	<10	4	29	
33	RCA 93 - 4 ( 260 - 270')	< .2	4.94	10	8	45	<5	2.11	<1	30	15	244	5.53	.03	<10	1.86	382	<1	.48	12	240	<2	15	<20	371	.25	<10	401	<10	13	43	
34	RCA 93 - 4 ( 270 - 280')	5 <.2	2.53	10	60	20	<5	1.75	<1	12	28	120	2.51	.02	10	1.43	333	<1	.06	13	590	<2	10	<20	79	.13	<10	126	<10	11	25	
35	RCA 93 - 4 ( 280 - 290')	< .2	3.30	15	238	25	<5	1.31	<1	29	<1	186	5.00	.01	<10	1.56	220	<1	.19	7	<10	<2	10	<20	159	.11	<10	399	<10	3	30	
36	RCA 93 - 4 ( 290 - 300')	5 <.2	3.77	10	150	30	<5	1.52	<1	28	2	257	5.22	.01	<10	1.55	215	<1	.27	10	<10	<2	15	<20	225	.11	<10	418	<10	3	27	
37	RCA 93 - 4 ( 300 - 310')	< .2	3.59	20	18	35	<5	2.52	3	45	1	264	7.90	.01	<10	1.63	454	<1	.11	19	10	<2	20	<20	103	.23	<10	518	<10	9	63	
38	RCA 93 - 4 ( 310 - 320')	5 <.2	4.33	15	12	75	<5	2.86	<1	39	3	184	7.66	.02	<10	1.36	396	<1	.29	14	40	<2	15	<20	201	.20	<10	502	<10	8	55	
39	RCA 93 - 4 ( 320 - 330')	< .2	3.85	10	42	35	<5	3.61	<1	33	5	310	6.44	.01	<10	1.23	359	<1	.16	12	20	<2	10	<20	167	.22	<10	447	<10	10	45	
40	RCA 93 - 4 ( 330 - 340')	5 <.2	4.08	15	22	35	<5	3.17	<1	35	6	431	6.95	.02	<10	1.08	350	<1	.23	17	50	<2	15	<20	206	.23	<10	486	<10	10	52	
41	RCA 93 - 4 ( 340 - 350')	< .2	3.62	20	12	30	<5	3.20	<1	36	4	408	6.74	.02	<10	1.27	392	<1	.09	16	40	<2	20	<20	109	.25	<10	466	<10	11	54	
42	RCA 93 - 4 ( 350 - 360')	5 <.2	3.76	15	12	40	<5	3.19	<1	42	7	544	9.40	.02	<10	1.12	425	<1	.14	20	<10	<2	15	<20	143	.30	<10	746	<10	11	55	
43	RCA 93 - 4 ( 360 - 370')	< .2	4.00	30	12	45	<5	3.00	<1	49	<1	688	9.72	.01	<10	1.57	453	<1	.13	23	<10	<2	25	<20	153	.37	<10	768	<10	14	68	
44	RCA 93 - 4 ( 370 - 380')	<5 <.2	3.51	15	12	40	<5	2.77	<1	44	3	717	9.12	.02	<10	1.33	405	<1	.13	20	<10	<2	10	<20	135	.33	<10	741	<10	13	56	
45	RCA 93 - 4 ( 380 - 390')	< .2	4.71	5	10	50	<5	3.52	<1	42	4	620	10.58	.03	<10	1.12	379	1	.32	21	<10	<2	10	<20	212	.25	<10	831	<10	8	51	

53.56

9.10.10.13 17.119

FROM ECO-TECH KAMLOOPS

ETA	DESCRIPTION	AR(ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MV	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
46	RCA 93 - 4 ( 390 - 400 )	10	<.2	4.02	20	8	40	<5	3.78	<1	44	13	613	10.35	.02	<10	1.35	473	<1	.10	21	<10	<2	15	<20	93	.30	<10	828	<10	11	60
47	RCA 93 - 5 ( 0 - 10 )	-	<.2	2.47	25	6	35	<5	3.21	<1	44	7	656	8.29	.07	<10	1.69	684	<1	.02	17	220	<2	20	<20	139	.28	<10	479	<10	14	65
48	RCA 93 - 5 ( 10 - 20 )	<5	<.2	3.71	35	8	45	<5	2.27	<1	56	3	656	11.83	.03	<10	1.94	649	2	.03	17	20	<2	25	<20	138	.40	<10	798	<10	17	68
49	RCA 93 - 5 ( 20 - 30 )	-	<.2	2.31	35	8	30	<5	1.64	1	68	5	331	8.91	.01	<10	1.51	432	1	.02	15	<10	<2	20	<20	211	.34	<10	425	<10	16	48
50	RCA 93 - 5 ( 30 - 40 )	5	<.2	2.58	20	6	30	<5	2.67	<1	39	6	511	8.02	.03	<10	1.32	463	<1	.06	9	110	<2	15	<20	110	.25	<10	504	<10	11	43
51	RCA 93 - 5 ( 40 - 50 )	-	<.2	2.25	10	6	30	<5	2.43	<1	36	5	658	8.42	.07	<10	1.43	462	<1	.04	11	10	<2	15	<20	118	.29	<10	561	<10	13	44
52	RCA 93 - 5 ( 50 - 60 )	<5	<.2	2.53	5	6	35	<5	3.29	<1	31	5	442	8.31	.04	<10	1.24	516	<1	.07	9	40	<2	20	<20	104	.25	<10	536	<10	11	46
53	RCA 93 - 5 ( 60 - 70 )	-	<.2	2.50	25	8	30	<5	2.81	<1	49	28	266	8.17	.01	<10	1.52	526	1	.02	15	260	<2	20	<20	125	.19	<10	234	<10	12	50
54	RCA 93 - 5 ( 70 - 80 )	5	<.2	2.80	5	8	40	<5	3.01	<1	47	45	190	8.65	.04	<10	1.46	534	<1	.02	31	80	<2	15	<20	164	.17	<10	246	<10	14	43
55	RCA 93 - 5 ( 80 - 90 )	-	<.2	2.08	5	6	45	<5	2.73	<1	45	10	295	12.90	.02	<10	1.37	556	<1	.03	21	<10	<2	15	<20	93	.27	<10	811	<10	11	57
56	RCA 93 - 5 ( 90 - 100 )	<5	<.2	2.12	5	8	30	5	3.26	<1	28	4	81	7.84	.03	<10	1.04	417	<1	.06	6	70	<2	15	<20	100	.27	<10	494	<10	13	37
57	RCA 93 - 5 ( 100 - 110 )	-	<.2	2.19	10	6	30	<5	3.66	<1	33	8	156	7.59	.03	<10	1.25	477	<1	.03	9	190	<2	15	<20	101	.21	<10	430	<10	11	36
58	RCA 93 - 5 ( 110 - 120 )	<5	<.2	2.03	15	6	35	<5	2.36	<1	40	6	348	10.65	.02	<10	1.28	531	<1	.04	12	70	<2	15	<20	86	.25	<10	707	<10	10	45
59	RCA 93 - 5 ( 120 - 130 )	-	<.2	1.90	20	12	20	<5	4.27	<1	83	9	503	5.65	<.01	<10	1.56	442	1	.01	22	180	<2	25	<20	70	.29	<10	271	<10	20	32
60	RCA 93 - 5 ( 130 - 140 )	<5	<.2	1.60	315	8	40	<5	1.55	3	111	10	539	11.82	.01	<10	1.10	281	3	.03	25	140	<2	28	<20	88	.26	<10	369	<10	11	31
61	RCA 93 - 5 ( 140 - 150 )	-	<.2	1.44	15	12	30	<5	1.30	<1	68	4	649	11.32	.01	<10	1.40	283	3	.03	26	90	<2	15	<20	77	.24	<10	250	<10	11	28

40.46

QC/DATA:

Repeat #:

35	RCA 93 - 4 ( 280 - 290 )	<.2	3.38	15	248	25	<5	1.34	<1	29	<1	189	4.98	.01	<10	1.61	218	<1	.20	8	<10	<2	15	<20	164	.10	<10	391	<10	3	31
60	RCA 93 - 4 ( 130 - 140 )	<.2	1.66	320	10	40	<5	1.61	2	110	11	550	12.10	.01	<10	1.15	289	3	.03	25	140	<2	20	<20	94	.28	<10	377	<10	12	32

STANDARD 1991:	1.2	1.91	65	12	90	<5	1.08	<1	12	41	86	2.54	.43	<10	1.05	476	<1	.02	16	470	12	15	<20	82	.08	<10	66	<10	8	71
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NOTE: < = LESS THAN  
> = GREATER THAN

SC93/KINGSTON

*Frank J. Pizzotti*  
 ECO-TECH LABORATORIES LTD.  
 FRANK J. PIZZOTTI, A.Sc.T.  
 B.C. Certified Assayer

9.17.1993 17:20  
 FROM ECO-TECH KANLOOPS

ECO-TECH LABORATORIES LTD.  
 10041 EAST TRANS CANADA HWY.  
 KAMLOOPS, B.C. V2C 2J3  
 PHONE - 604-573-5700  
 FAX - 604-573-4557

FEED DOCUMENT THIS DIRECTION  
**IMPORTANT FAX MESSAGE**  
 TO *SCOTT SMITH*  
 COMPANY *Kingson*  
 FAX NO. *604-573-8132*  
 FROM *Alber*  
 NO. OF PAGES *3*  
 RE *ASHTON*  
*Alber*

KINGSTON RESOURCES EYA 93-367  
 703-1112 W. PRINCE  
 VANCOUVER, B.C.  
 V6E 2S1

ATTENTION: SCOTT SMITH

62 PERCUSSION DRILL SAMPLES RECEIVED SEPTEMBER 15, 1993  
 PROJECT #: ASHTON

SEPTEMBER 24, 1993

VALUES IN PPM UNLESS OTHERWISE REPORTED

PAGE 1

BT#	DESCRIPTION	AD (ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	I(%)	LA	MG(%)	NM	NO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZH
1	- RCA 93 - 5 ( 150 - 160')	-	<.2	1.91	20	6	25	<5	1.70	<1	41	35	330	6.61	.02	<10	1.15	357	2	.06	10	20	<2	15	<20	121	.24	<10	435	<10	12	29
2	- RCA 93 - 5 ( 160 - 170')	<5	<.2	1.71	5	8	25	<5	1.49	<1	40	17	408	7.27	.02	<10	1.28	350	<1	.05	8	<10	<2	15	<20	109	.18	<10	519	<10	7	35
3	- RCA 93 - 5 ( 170 - 180')	-	<.2	2.08	10	4	25	<5	1.25	<1	46	22	453	8.00	.01	<10	1.79	423	<1	.04	15	10	<2	20	<20	72	.19	<10	549	<10	7	38
4	- RCA 93 - 5 ( 180 - 190')	<5	<.2	1.66	20	6	25	<5	3.20	<1	92	20	940	9.02	<.01	<10	2.34	469	<1	.02	33	880	<2	30	<20	51	.12	<10	230	<10	6	106
5	- RCA 93 - 5 ( 190 - 200')	-	<.2	1.81	30	4	25	<5	2.28	<1	83	27	971	7.85	.01	<10	3.05	391	<1	.03	25	1450	<2	25	<20	33	.08	<10	130	<10	6	44
6	- RCA 93 - 5 ( 200 - 210')	<5	<.2	1.95	5	4	20	<5	2.80	<1	82	16	364	6.22	.01	<10	2.54	424	<1	.02	17	100	<2	20	<20	45	.12	<10	206	<10	6	33
7	- RCA 93 - 5 ( 210 - 220')	-	<.2	1.28	20	4	30	<5	5.43	<1	170	80	2910	8.35	.01	<10	1.26	466	1	.01	43	10	<2	20	<20	72	.06	<10	164	<10	2	23
8	- RCA 93 - 5 ( 220 - 230')	<5	<.2	1.67	20	6	20	<5	5.39	<1	58	13	960	5.90	.01	<10	1.52	540	<1	.02	18	100	<2	20	<20	78	.05	<10	229	<10	3	31
9	- RCA 93 - 5 ( 230 - 240')	-	<.2	2.18	20	6	35	<5	6.07	<1	48	10	323	7.01	.02	<10	1.32	709	1	.03	11	20	<2	20	<20	92	.05	<10	410	<10	5	38
10	- RCA 93 - 5 ( 240 - 250')	<5	<.2	2.76	5	6	35	<5	5.39	<1	48	10	395	8.18	.04	<10	1.63	750	<1	.03	14	<10	<2	25	<20	95	.07	<10	555	<10	3	43
11	- RCA 93 - 5 ( 250 - 260')	-	<.2	3.00	10	8	30	<5	3.15	<1	60	19	611	11.21	<.01	<10	3.02	617	<1	.02	20	<10	2	45	<20	55	.19	10	871	<10	8	53
12	- RCA 93 - 5 ( 260 - 270')	<5	<.2	2.43	10	6	25	5	3.64	<1	45	17	191	6.09	.04	<10	1.73	440	<1	.01	10	30	<2	10	<20	71	.24	<10	364	<10	12	29
13	- RCA 93 - 5 ( 270 - 280')	-	<.2	2.82	10	8	30	<5	6.12	<1	45	12	502	8.65	.03	<10	1.30	714	<1	.03	14	<10	<2	10	<20	93	.08	<10	608	<10	4	47
14	- RCA 93 - 5 ( 280 - 290')	<5	<.2	2.64	5	6	30	<5	5.02	<1	40	7	419	8.14	.04	<10	1.31	652	<1	.05	13	10	<2	25	<20	113	.11	<10	565	<10	5	45
15	- RCA 93 - 5 ( 290 - 300')	-	<.2	2.52	10	6	35	<5	4.64	<1	51	11	832	9.51	.01	<10	1.98	736	<1	.05	19	20	<2	25	<20	85	.17	<10	692	<10	8	69
16	- RCA 93 - 5 ( 300 - 310')	<5	<.2	2.35	10	6	35	<5	5.70	<1	50	6	554	9.31	.03	<10	1.64	736	<1	.04	16	50	<2	25	<20	86	.11	<10	699	<10	6	53
17	- RCA 93 - 5 ( 310 - 320')	-	<.2	1.38	5	4	10	<5	7.55	<1	18	15	127	3.46	.01	<10	.98	702	1	<.01	5	90	<2	10	<20	71	.08	<10	173	<10	8	24
18	- RCA 93 - 5 ( 320 - 330')	<5	<.2	1.05	15	4	10	5	6.74	<1	12	12	72	2.05	<.01	<10	1.01	564	<1	<.01	3	250	<2	20	<20	52	.07	<10	80	<10	7	20
19	- RCA 93 - 5 ( 330 - 340')	-	<.2	1.73	15	6	45	<5	7.95	<1	31	23	221	4.73	.01	<10	1.61	767	1	.01	7	720	<2	25	<20	77	.12	<10	228	<10	9	42
20	- RCA 93 - 5 ( 340 - 350')	<5	<.2	2.69	25	6	45	<5	5.67	<1	61	9	598	10.00	.01	<10	2.71	1002	1	.01	17	30	<2	30	<20	81	.19	<10	613	<10	10	82
21	- RCA 93 - 5 ( 350 - 360')	-	<.2	1.87	20	6	30	<5	4.92	<1	32	10	320	5.70	.02	<10	1.65	834	<1	.01	9	80	<2	15	<20	79	.07	<10	364	<10	6	51
22	- RCA 93 - 5 ( 360 - 370')	<5	<.2	1.97	20	6	25	<5	9.52	<1	27	10	180	5.59	.02	<10	1.50	983	1	<.01	14	480	<2	20	<20	116	.02	<10	260	<10	5	58
23	- RCA 93 - 5 ( 370 - 380')	-	<.2	2.39	20	6	30	<5	6.58	<1	39	9	478	8.12	.02	<10	1.62	788	<1	.02	17	<10	<2	20	<20	103	.08	<10	743	<10	5	55
24	- RCA 93 - 5 ( 380 - 390')	<5	<.2	2.23	15	6	30	<5	4.60	<1	38	10	730	7.95	.02	<10	1.90	778	1	.06	18	130	<2	25	<20	88	.12	<10	644	<10	7	52
25	- RCA 93 - 5 ( 390 - 400')	-	<.2	1.90	30	4	25	<5	5.06	<1	31	32	409	5.05	.02	<10	1.98	674	1	.03	14	40	<2	20	<20	77	.08	<10	301	<10	12	37

121.86

HT	DESCRIPTION	AD (ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SE	SR	TI(%)	U	V	W	Y	ZN
26	RCA 93 - 5 ( 400 - 410' )	<5	<.2	2.32	70	6	25	<5	3.10	<1	40	30	452	6.79	.01	<10	2.29	622	2	.08	17	40	2	25	<20	63	.12	<10	459	<10	13	43
27	RCA 93 - 5 ( 410 - 420' )	-	<.2	2.93	25	6	45	<5	2.71	<1	56	21	991	9.93	.04	<10	2.49	730	<1	.08	26	<10	<2	40	<20	74	.16	<10	527	<10	8	64
28	RCA 93 - 5 ( 420 - 430' )	<5	<.2	2.54	25	6	40	<5	3.21	<1	46	21	616	8.62	.03	<10	2.02	598	<1	.07	24	80	<2	25	<20	70	.18	<10	621	<10	11	64
29	RCA 93 - 5 ( 430 - 440' )	-	<.2	2.62	40	8	20	<5	4.12	<1	45	43	791	6.16	<.01	<10	3.00	557	8	.01	46	320	2	30	<20	49	.09	<10	138	<10	8	69
30	RCA 93 - 5 ( 440 - 450' )	<5	<.2	1.89	40	6	20	<5	5.01	<1	34	19	367	5.56	.03	<10	1.96	523	2	.02	25	370	<2	15	<20	76	.11	<10	226	<10	8	60
31	RCA 93 - 5 ( 450 - 460' )	-	<.2	2.35	40	8	30	<5	9.08	<1	45	25	728	6.35	.05	<10	1.45	828	1	.02	33	100	<2	15	<20	112	.04	<10	257	<10	7	50
32	RCA 93 - 5 ( 460 - 470' )	<5	<.2	2.31	30	6	40	<5	2.54	<1	39	33	536	7.80	.04	<10	1.18	439	1	.09	21	60	<2	25	<20	83	.18	<10	595	<10	9	50
33	RCA 93 - 5 ( 470 - 480' )	-	<.2	2.28	80	84	30	<5	2.45	<1	35	72	601	6.22	.03	<10	1.02	362	2	.07	30	160	2	10	<20	94	.16	<10	389	<10	9	37
34	RCA 93 - 5 ( 480 - 490' )	<5	<.2	2.59	85	94	25	<5	3.09	<1	45	46	1183	4.87	.02	<10	1.22	381	2	.04	57	150	2	15	<20	90	.12	<10	162	<10	9	48
35	RCA 93 - 5 ( 490 - 500' )	-	<.2	2.68	25	74	25	<5	3.64	<1	22	44	263	3.67	.02	<10	.93	330	2	.04	18	80	4	15	<20	99	.13	<10	188	<10	10	30
36	RCA 93 - 6 ( 10 - 20' )	<5	<.2	2.68	20	10	40	5	38.99	<1	57	28	254	7.46	.03	<10	1.62	595	1	.10	24	440	6	25	<20	115	.18	<10	453	<10	13	64
37	RCA 93 - 6 ( 30 - 40' )	-	<.2	2.96	15	10	60	15	3.24	<1	40	43	203	7.27	.06	<10	1.81	693	2	.12	28	630	6	30	<20	165	.20	<10	420	<10	15	77
38	RCA 93 - 6 ( 50 - 60' )	<5	<.2	2.31	25	6	45	5	2.75	<1	31	35	199	6.68	.04	<10	1.48	638	1	.08	20	560	4	20	<20	110	.18	<10	403	<10	15	69
39	RCA 93 - 6 ( 70 - 80' )	-	<.2	2.00	30	6	30	<5	3.49	<1	31	27	292	6.03	.02	<10	1.31	589	<1	.04	18	320	<2	15	<20	118	.23	<10	400	<10	16	85
40	RCA 93 - 6 ( 90 - 100' )	<5	<.2	1.96	35	8	25	<5	2.47	<1	30	44	256	5.87	.02	<10	1.20	656	2	.04	16	550	2	15	<20	97	.19	<10	344	<10	14	137
41	RCA 93 - 7 ( 100 - 110' )	-	<.2	2.24	45	8	35	<5	3.11	<1	30	35	242	5.35	.04	<10	1.37	776	2	.06	18	560	4	20	<20	119	.20	<10	261	<10	16	175
42	RCA 93 - 7 ( 110 - 120' )	<5	<.2	2.33	30	8	35	<5	2.98	<1	33	29	307	6.25	.03	<10	1.37	632	2	.05	14	440	4	20	<20	113	.21	<10	368	<10	15	111
43	RCA 93 - 7 ( 120 - 130' )	-	<.2	1.83	40	6	25	<5	5.05	<1	25	31	200	4.94	.03	<10	1.11	749	1	.04	12	470	2	15	<20	120	.19	<10	289	<10	15	83
44	RCA 93 - 7 ( 130 - 140' )	<5	<.2	1.99	35	6	25	<5	3.42	<1	30	48	353	5.24	.02	<10	1.35	627	1	.03	18	390	<2	20	<20	108	.21	<10	303	<10	15	95
45	RCA 93 - 7 ( 140 - 150' )	-	<.2	1.91	60	8	25	<5	4.53	<1	25	35	222	4.20	.03	<10	1.18	712	2	.04	14	550	8	15	<20	117	.18	<10	209	<10	16	115
46	RCA 93 - 7 ( 150 - 160' )	<5	<.2	2.29	30	8	35	<5	2.36	<1	41	58	509	6.27	.03	<10	1.44	620	2	.04	23	440	2	20	<20	133	.30	<10	378	<10	22	93
47	RCA 93 - 7 ( 160 - 170' )	-	<.2	2.07	15	8	75	<5	2.26	<1	20	48	81	3.88	.10	10	1.45	678	<1	.13	32	1040	<2	15	<20	214	.16	<10	114	<10	18	55
48	RCA 93 - 7 ( 170 - 180' )	<5	<.2	2.07	5	8	70	10	1.77	<1	18	60	38	3.28	.08	10	1.33	540	1	.24	36	1090	2	20	<20	195	.17	<10	98	<10	19	48
49	RCA 93 - 7 ( 180 - 190' )	-	<.2	1.86	5	6	50	10	1.90	<1	20	75	33	3.57	.11	10	1.63	572	3	.16	47	1240	2	15	<20	148	.15	<10	92	<10	19	50
50	RCA 93 - 7 ( 190 - 200' )	<5	<.2	2.02	10	6	60	15	1.77	<1	21	56	35	3.77	.09	10	1.77	557	<1	.18	45	1350	2	15	<20	224	.17	<10	106	<10	20	55

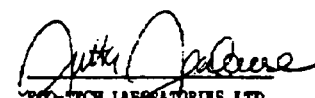
9.24.1993 10:48

FROM ECO-TECH KAMLOOPS



ST#	DESCRIPTION	AD (ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PE	SB	SN	SR	TI(%)	U	V	W	Y	ZN
51	RCA 93 - 7 ( 200 - 210')	-	<.2	2.32	20	8	75	5	2.56	<1	21	60	83	4.24	.09	<10	1.42	660	2	.12	27	920	2	15	<20	211	.14	<10	150	<10	16	53
52	RCA 93 - 7 ( 210 - 220')	<5	<.2	3.18	5	8	140	<5	3.37	<1	19	46	136	3.51	.09	<10	1.48	523	1	.05	17	290	<2	15	<20	166	.08	<10	134	<10	7	34
53	RCA 93 - 7 ( 220 - 230')	-	<.2	1.81	5	2	85	<5	1.46	<1	8	35	80	1.32	.05	<10	.54	197	<1	.02	5	180	<2	5	<20	101	.03	<10	38	<10	3	13
54	RCA 93 - 7 ( 230 - 240')	<5	<.2	2.91	5	6	40	15	3.51	<1	30	26	128	6.43	.04	<10	1.91	1081	<1	.02	5	680	<2	15	<20	99	.29	<10	284	<10	29	41
55	RCA 93 - 7 ( 240 - 250')	-	<.2	1.04	10	4	35	5	2.41	<1	7	62	22	2.44	.05	<10	.52	618	3	.03	3	530	<2	10	<20	41	.09	<10	13	<10	22	36
56	RCA 93 - 7 ( 250 - 260')	<5	<.2	1.55	5	6	25	5	1.94	<1	13	53	44	3.84	.11	<10	.83	821	2	.03	5	600	<2	15	<20	37	.10	<10	73	<10	25	54
57	RCA 93 - 7 ( 260 - 270')	-	<.2	2.24	5	6	85	10	2.50	<1	20	40	80	5.51	.09	<10	1.28	1106	2	.03	6	720	<2	15	<20	41	.14	<10	204	<10	30	80
58	RCA 93 - 7 ( 270 - 280')	<5	<.2	1.82	15	6	65	<5	2.05	<1	19	33	87	5.05	.09	<10	1.06	914	1	.02	5	380	<2	15	<20	29	.13	<10	215	<10	25	45
59	RCA 93 - 7 ( 280 - 290')	-	<.2	2.15	10	6	50	5	2.72	<1	22	36	118	5.11	.05	<10	1.43	972	1	.02	7	700	<2	15	<20	40	.16	<10	193	<10	28	75
60	RCA 93 - 7 ( 290 - 300')	<5	<.2	2.40	5	6	65	5	3.65	<1	36	17	269	7.90	.09	<10	1.89	1050	<1	.02	12	450	<2	25	<20	54	.23	<10	444	<10	21	66
61	RCA 93 - 7 ( 300 - 310')	-	<.2	1.98	25	6	35	5	2.43	<1	17	29	52	4.74	.05	<10	1.19	974	1	.02	3	760	<2	20	<20	32	.11	<10	130	<10	30	67
62	RCA 93 - 7 ( 310 - 320')	<5	<.2	2.61	20	4	45	<5	2.24	<1	27	60	167	5.55	.07	<10	2.14	897	<1	.01	23	380	<2	15	<20	35	.07	<10	207	<10	9	58
QC/DATA																																
39	RCA 93 - 6 ( 40 - 50')		<.2	2.02	10	8	30	5	3.54	<1	32	28	295	6.14	.83	<10	1.30	596	1	.04	20	340	<2	30	<20	114	.23	<10	406	<10	16	87
STANDARD 1991:																																
			1.2	2.16	65	6	145	5	2.05	<1	24	76	86	4.58	.46	<10	1.14	838	<1	.02	31	780	20	20	<20	73	.13	<10	98	<10	14	72

SC93/KINGSTON

  
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 B.C. Certified Assayer

9.24.1993 10:51

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ANALYTICAL CHEMISTRY  
ENVIRONMENTAL TESTING

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Fax (604) 573-4557

SEPTEMBER 14, 1993

**CERTIFICATE OF ASSAY ETK 93-347**

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KINGSTON RESOURCES  
703-1112 W. PENDER STREET  
VANCOUVER, B.C.  
V6E 2S1

ATTENTION: SCOTT SMITH

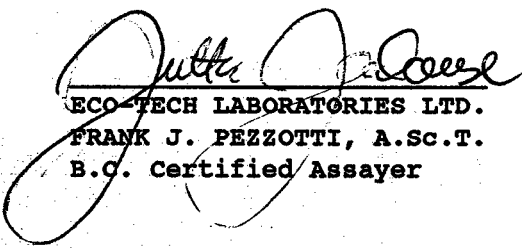
-----

SAMPLE IDENTIFICATION: 76 PRECUSSION DRILL samples received SEPTEMBER 3, 1993  
----- PROJECT #: ASHTON

ET#	Description	Cu (%)
18-	RCA 93 - 2 ( 170 - 180' )	.17
22-	RCA 93 - 2 ( 210 - 220' )	.18

NOTE: < = LESS THAN

SC93/KMISC

  
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B.C. Certified Assayer

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Fax (604) 573-4557

SEPTEMBER 10, 1993

CERTIFICATE OF ASSAY ETK 93-346  
=====

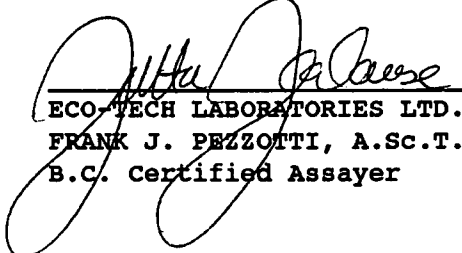
KINGSTON RESOURCES  
703-1112 W. PENDER STREET  
VANCOUVER, B.C.  
V6E 2S1

ATTENTION: SCOTT SMITH  
-----

SAMPLE IDENTIFICATION: 50 ROCK samples received SEPTEMBER 3, 1993  
----- PROJECT #: ASHTON

ET#	Description	Cu (%)
40-	RCA 93 - 1 ( 390 - 400')	.22

SC93/KAMISC

  
\_\_\_\_\_  
ECO-TECH LABORATORIES LTD.  
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**APPENDIX III**

**Lithogeochemical Assay Procedures  
from Eco-Tech Laboratories Ltd.**



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**METHODOLOGY**

a) Gold - Geochemical

Fire Assay - A.A.

A 10.000 gram sample is fire assayed by conventional fire assay procedures. The resulting bead is dissolved in 3ml aqua regia and is analyzed for gold by Atomic Absorption.

Minimum Reportable Concentration: 5 (pbb)

b) 30 Element ICP

Aqua Regia Digestion

A one gram sample\* is digested with a 6ml mixture of HCL, HNO<sub>3</sub>, H<sub>2</sub>O in a ratio of 3:2:1. The digestion is carried out at 95°C for two hours. The digested sample is made up to 20ml with distilled water and analyzed by ICP.

Minimum Reportable Concentration:

a) Aqua Regia Digestion

Ag	0.2 ppm	Cu	1 ppm	Pb	2 ppm
Al*	0.01%	Fe*	0.01%	Sb	5 ppm
As	5 ppm	K*	0.01%	Sn	20 ppm
B*	2 ppm	La	10 ppm	Sr*	1 ppm
Ba*	5 ppm	Mg*	0.01%	Ti*	0.01%
Bi	5 ppm	Mn*	1 ppm	U*	10 ppm
Ca*	0.01%	Mo	1 ppm	V	1 ppm
Cd	1 ppm	Na*	0.01%	W*	10 ppm
Co	1 ppm	Ni	1 ppm	Y	1 ppm
Cr*	1 ppm	P*	10 ppm	Zn	1 ppm

Dissolution of elements marked by an asterisk may not be complete.  
 \* 2 gram sample can be used at no extra charge

Copper Assay

A 2g sample is digested in a 200ml phosphoric flask with HNO<sub>3</sub>, HCl. The digestion is carried out on a hot plate for 2 hours. The sample is bulked up with distilled water and analysed for copper by Atomic Absorption. The minimum reportable concentration is <0.01%.



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## Quality control

### a) Sample Preparation

Random Duplicate samples are split from each shipment and introduced in each suite of samples sent to the laboratory for analysis. No less than one sample in forty is re-split. Each sample is assigned a unique lab number and barcode to be read by the barcode reader at the weigh station. A second person checks the lab number assignment for accuracy.

### b) Weighing Stations

Each balance is calibrated twice during each shift using N.B.S. referenced weights. Samples are identified prior to weighing by use of a barcode reader. The sample identification, sample weight and analysis required is automatically captured by computer.

### c) Fire Lab

Separate fusion pots are used for Assay, Rock Geochem and Soil Geochem. The pots are catalogued and are not reused until the assay is completed. Pots which were used for samples containing high or anomalous gold values are discarded at the end of each day. All flux mixtures are tested for purity before use.

### d) Analysis

Samples are analyzed from test tube racks containing forty test tubes. Each rack will contain thirty-seven samples, (one of which may be a blind duplicate re-split from the bucking facility), one blank, one soil standard and one duplicate sample. Approximately 25 Can Met and several in-house standards are routinely used by our laboratory. As a minimum, a full 10% of all samples analyzed are quality control samples. In addition to the quality control analyses, check analyses are routinely performed to verify data for anomalous samples.



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The samples are analyzed in the following order:

<u>Test Tube</u>	<u>Contents</u>
#40	Soil Standard (CanMet or In-House) to verify instrument calibration and sample digestion.
#1	Reagent Blank to check for reagent contamination and instrument zero.
#2 to #38	Analysis of samples.
#39	Sample Duplicate.
#40	Soil Standard and Recalibration.

Quality Control Data Assessment

Each element analyzed in the soil standards has an individual statistical plot of standard deviation for the analysis. Upper and lower warning limits are set at  $\pm 2$  standard deviations. The analysis is considered to be out of control and is stopped when the value exceeds  $\pm 3$  standards deviations. If the nature of the problem cannot be determined, the entire block of samples is re-analyzed. The results for duplicate and blind duplicate pairs must fall within our tolerance limits for precision of geochemical analysis as outlined below:

<u>Average Value</u>	<u>Precision</u>
1 to 2 times detection limit	$\pm$ 100%
3 to 4 "	$\pm$ 60%
5 to 6 "	$\pm$ 40%
7 to 10 "	$\pm$ 25%
11 to 100 "	$\pm$ 15%
> 100 "	$\pm$ 10%