Geological Report

for the

BAR CLAIM GROUP

CARIBOO MINING DIVISION

NTS: 93A/14W
Latitude 52° 55′N, Longitude 121° 20′W

by

C. C. Downie, P.Geo.
of
Big City Resources Inc.
720-23rd Ave. N.
Cranbrook, BC
V1C-5K5

Date: December 15th 1994

TABLE OF CONTENTS

LIST OF APPENDICES

LIST OF FIGURES

SUMMARY

The **Bar** claims were acquired by staking in March, 1993, and July, 1994 to cover an area in the Cariboo Mining Division. The property is located 25 km southeast of Wells, BC and consists of 26, 2-Post claim units staked to cover ground thought to be prospective with respect to stratabound, base-metal mineralization. Three operators have investigated the general area in the past, and have provided comprehensive data-bases in publicly-accessed information files.

A $65,000 geological and geophysical program was carried out in the summer of 1994 to further evaluate the claims with respect to their potential for hosting large "sedex" (sedimentary-exhalative) deposits. Two separate control grids were established, with 21 line-km placed, and 834 soil samples collected. As well, some 8.0 line-km of UTEM geophysical surveys were completed. 29 rock samples were also taken of representative material from the property. The work program followed work initiated by past operators since 1971, and most recently Toklat Resources in 1993.

The geological/geochemical program was designed to cover stratigraphy of the Hardscrabble Mountain succession, a Palaeozoic sequence of shallow- to deep-water marine sediments which show indications of hosting massive sulphide mineralization. Evidence of this consists of:

(1) a 1000m-long, concordant, silver, lead, zinc and barium soil geochemical anomaly,

(2) coincident geophysical anomalies,

(3) both of the above directly associated with a stratabound barite horizon over 2.0m in width, mappable for over 300m, and apparently occurring some 2.5km along strike,

(4) extremely gossanous material located in at least two places along the trend of the anomaly,

(5) conformable lead-zinc occurrences have been recognised within the same stratigraphic succession less than 500m north of the claim boundary, with grades reported of 7.22% Pb, 5.23% Zn, and .93oz/t Ag over 0.5m., and

(6) the sedimentary sequence underlying the claims is very similar in age, lithology and tectonic setting to those that host world-class "sedex-style" deposits in the Canadian Cordillera, Europe and Australia.

INTRODUCTION

The **Bar** claims were staked on March 12, 1993, and July 22, 1994 to cover ground open to staking in the Cariboo Mining Division. The property is located 25 km southeast of Wells, BC and consists of 26 claim units staked to cover ground thought to be prospective with respect to stratabound, base-metal mineralization. Three operators have investigated the area in the past, and have provided comprehensive data-bases in publicly-accessed information files.

The staking program was designed to cover stratigraphy of the Hardscrabble Mountain succession, a Palaeozoic sequence of shallow- to deep-water marine sediments which have shown strong indications of hosting massive sulphide mineralization. Very high soil geochemical values have been recovered from within the property area in the past, yet insufficient work was carried out in order to fully recognise its geologic potential. Diamond drilling was completed in an area comprising only 400m of strike length, though the geochemical anomaly stretches for approximately 1200m, and the barite horizon, some 2.5 km. Extensive trenching was also carried out in some areas by past operators, but often deep overburden made exposure of bedrock material infrequent, and results inconclusive. Geochemical and geophysical work completed during the 1994 season indicated that prominent faults offset the anomalous horizon, an important feature which may not have been recognised by past operators.

PROPERTY, DESCRIPTION, AND LOCATION

The **Bar** claims are located 25km southeast of Wells, BC. on NTS mapsheet 93A/14W (Fig. 1). They occur within the Cunningham Creek valley, on a gentle grade along the western slope of Roundtop Mountain between elevation 4000 and 6300 ft. Mature spruce and fir cover the entire property area, and outcrop is generally limited to escarpments and creek draws. The claim block consists of 26 contiguous 2-post claim units, which trend north and northeasterly (Fig. 2). Property tenure details are summarized below:

Name	Units	Tag No.	Title No.	Date Acquired	Expiry Date
Bar 1	1	653411M	316623	Mar. 12, 1993	Mar. 12, 2001
Bar 2	1	653412M	316624	Mar. 12, 1993	Mar. 12, 2001
Bar 3	1	653413M	316643	Mar. 12, 1993	Mar. 12, 2001
Bar 4	1	653414M	316644	Mar. 12, 1993	Mar. 12, 2001
Bar 5	1	653415M	316645	Mar. 12, 1993	Mar. 12, 2001
Bar 6	1	653416M	316646	Mar. 12, 1993	Mar. 12, 2001
Bar 7	1	653417M	316647	Mar. 12, 1993	Mar. 12, 2001
Bar 8	1	653418M	316648	Mar. 12, 1993	Mar. 12, 2001
Bar 9	1	653419M	316649	Mar. 12, 1993	Mar. 12, 2001
Bar 10	1	653420M	316650	Mar. 12, 1993	Mar. 12, 2001
Bar 11	1	653421M	316651	Mar. 12, 1993	Mar. 12, 2001
Bar 12	1	653422M	316652	Mar. 12, 1993	Mar. 12, 2001
Bar 13	1	653401M	316653	Mar. 12, 1993	Mar. 12, 2001
Bar 14	1	653402M	316654	Mar. 12, 1993	Mar. 12, 2001
Bar 15	1	653403M	316655	Mar. 12, 1993	Mar. 12, 2001
Bar 16	1	653404M	316659	Mar. 12, 1993	Mar. 12, 2001
Bar 17	1	653405M	316660	Mar. 12, 1993	Mar. 12, 2001
Bar 18	1	653406M	316656	Mar. 12, 1993	Mar. 12, 2001
Bar 19	1	653407M	316657	Mar. 12, 1993	Mar. 12, 2001
Bar 20	1	653408M	316658	Mar. 12, 1993	Mar. 12, 2001
Bar 21	1	653741M	329283	Jul. 22, 1994	Jul. 22, 2001
Bar 22	1	653742M	329285	Jul. 22, 1994	Jul. 22, 2001
Bar 23	1	653744M	329286	Jul. 22, 1994	Jul. 22, 2001
Bar 24	1	653745M	329287	Jul. 22, 1994	Jul. 22, 2001
Bar 25	1	653746M	329288	Jul. 22, 1994	Jul. 22, 2001
Bar 26	1	653747M	329289	Jul. 22, 1994	Jul. 22, 2001
Total:	26 units				

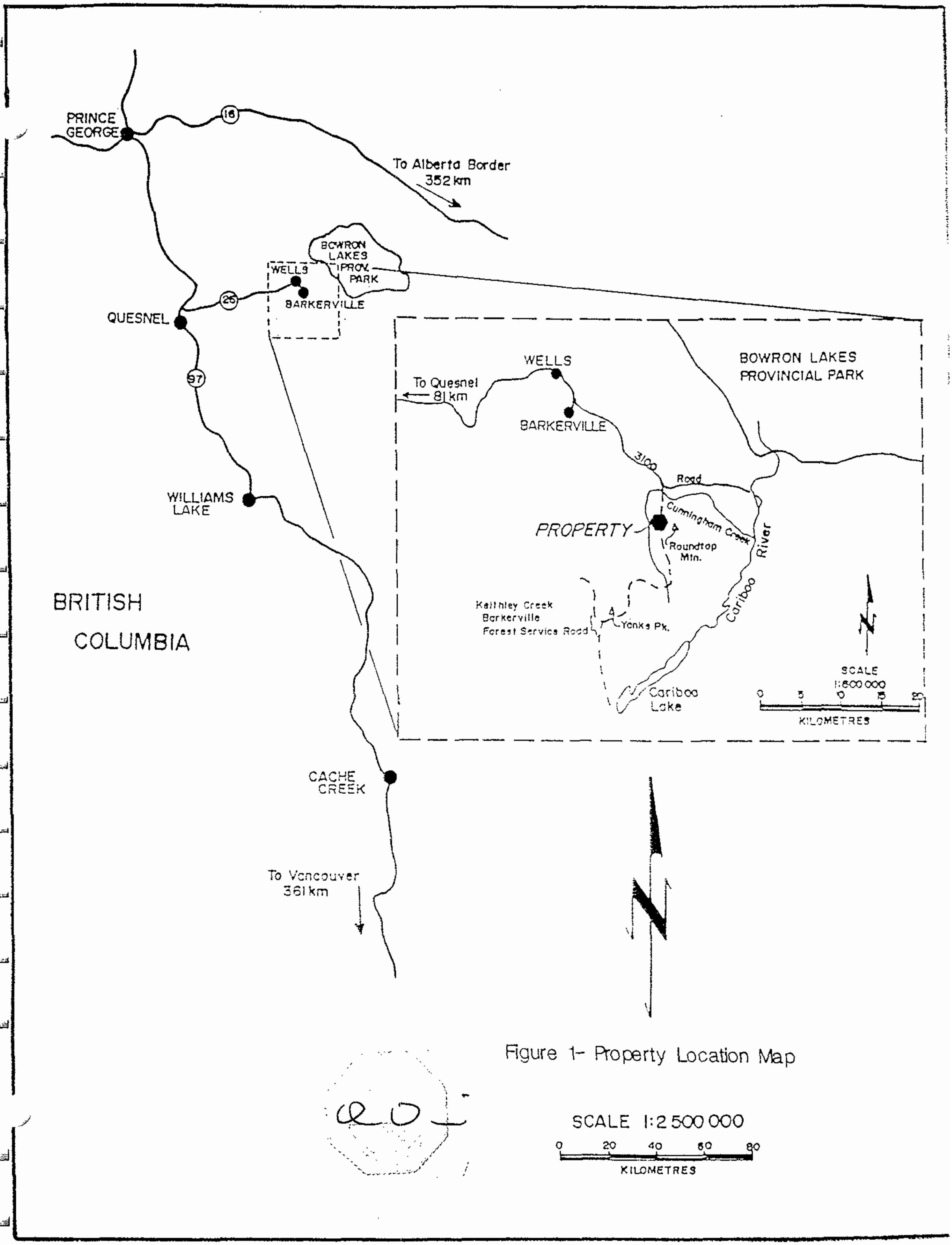
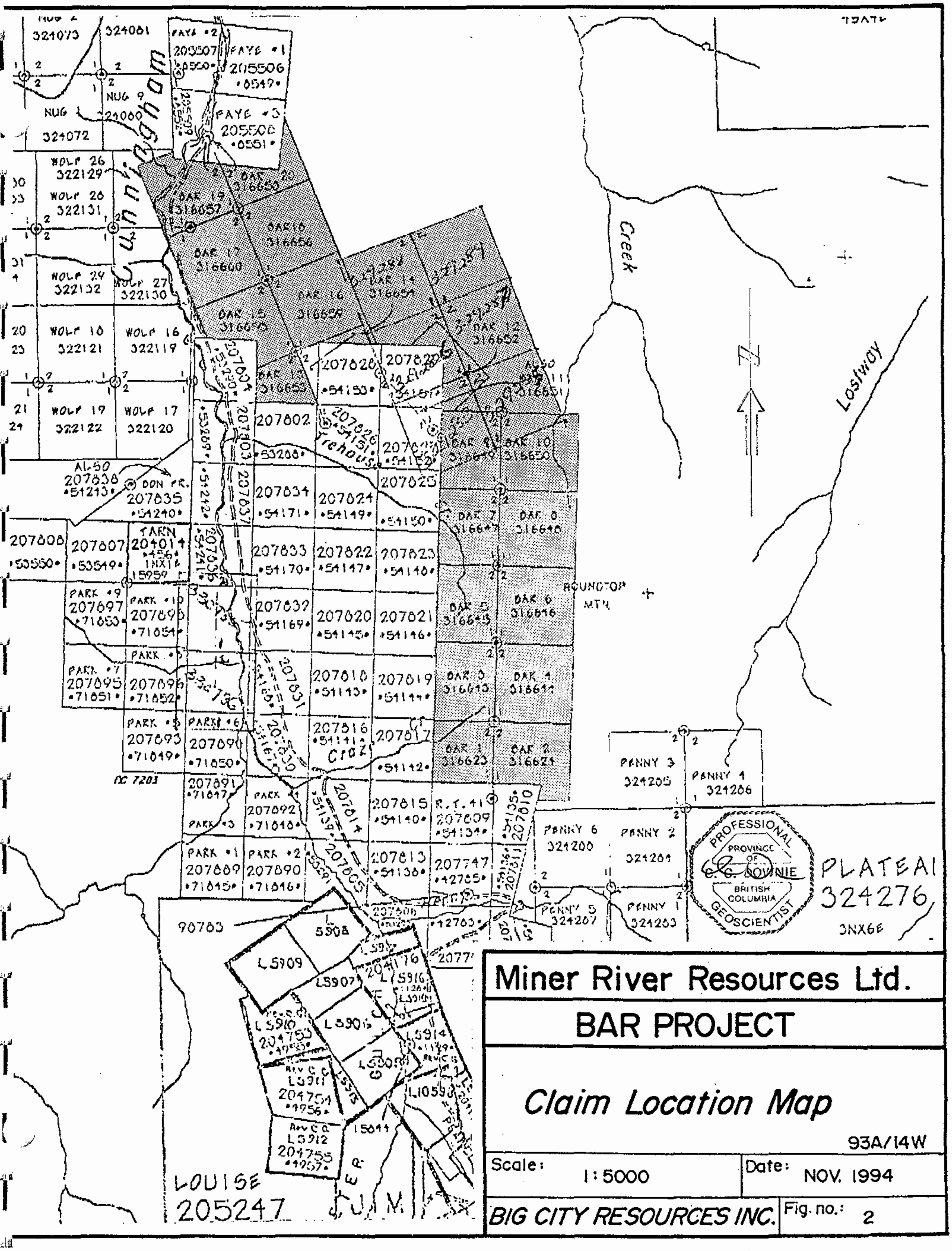


Figure 1- Property Location Map



Miner River Resources Ltd.

BAR PROJECT

Claim Location Map

93A/14W

Scale: 1:5000

Date: NOV. 1994

BIG CITY RESOURCES INC.

Fig. no.: 2

ACCESSIBILITY, CLIMATE AND LOCAL RESOURCES

Access to and within the property area is excellent, provided by forest service roads which are maintained year-round. Logging is presently underway within the Cunningham Creek area. Roads within the property have been constructed by previous operators, and would require very little work to rehabilitate them. The area is subject to moderate precipitation, and is workable from late May to late October.

A local forest company currently has plans to log selected areas of the property in the winter of 1994/95, and as such, a new access road will be built along the east side of Cunningham Creek, at an elevation which will see it transverse much of the property. This road will undoubtedly provide new exposures, and hopefully will benefit the overall geologic interpretation of the property.

Mining has played an important role in the history of the area, and as a result, a well developed infrastructure is located nearby. Three major lode gold producers operated in Wells during the last century, namely the Mosquito Creek, Island Mountain, and Cariboo Gold Quartz Mines. Numerous placer operations have also been in existence nearby, some still working the same creeks which saw activity 130 years ago. A hydroelectric powerline and paved highway are located 15km to the northeast at Barkerville, and the nearest railhead is situated 60km north, along the Yellowhead Highway.
A well developed Forest Service Road network exists to the above services.

HISTORY

The entire Cariboo region has seen a wealth of prospecting activity since 1860, owing primarily to the rich placer gold deposits of the Barkerville area, located some 18km to the northwest of the claims.

Most work in the area was primarily focused on gold, and systematic exploration for base metals was first undertaken in 1971 by Coast Interior Ventures. Their program consisted of detailed drilling of a high-grade silver occurrence off of the present claims, as well as a 4000-sample soil geochemical program which resulted in the discovery of the "X"- Anomaly, along the western boundary of the present **Bar** Claims, and a further 9 discrete soil anomalies in the Cunningham Creek area. A number of anomalies were drilled, but the X-Anomaly remained untested.

Rio Tinto Canadian (Riocanex) optioned the Coast Interior Ventures ground in 1977-1978, and carried out work on all known sedex-style showings in the area, and also located a number more (see Figure 3). Geological work carried out within this program resulted in the recognition of a conformable bedded barite horizon directly overlying the anomaly area, underlining the significant potential for stratabound massive sulphides. Trenching and geophysical work was carried out in the area of the X-Anomaly, followed by approximately 650m of diamond drilling from 4 holes over 400m of strike-length. Trenching failed to locate the source of mineralization, though bedrock was not everywhere exposed along trench floors. Drilling indicated that the anomaly area was complexly folded, and that careful structural interpretation would be necessary to adequately test for mineralization. The best showing worked by Riocanex was at the "A"-Anomaly, and consisted of a conformable galena-sphalerite zone in a siliceous limestone and black shale sequence that assayed 5.98% combined lead-zinc and 2.09 oz/ton silver over 14.5m. It is interesting to note that the geochemical response in soils within the X-Anomaly area on the **Bar** claims, is stronger than that overlying the impressive A-Anomaly mineralization. Riocanex also discovered conformable lead/zinc/silver mineralization in outcrop immediately north of the Bar claim boundary. This occurrence, named the Vic showing, returned values of 7.22% Pb, 5.23% Zn, and .93 oz t Ag over 0.5m.

Loki Gold acquired the ground now overlain by the Bar claims in 1989, as part of a larger property package including 160 units. Their $350,000 work program concentrated on exploration for gold, which occurs in high-grade concentrations within quartz veins at a number of locations along the Cunningham Creek valley. As a result of Lokis' program, a portion of their soil geochemical grid covered the area of the present claims. Though no significant gold geochemical values were returned from this area, a strong coincident silver, lead and zinc soil anomaly was delineated in the area of the X-Anomaly. Interestingly, the strongest zinc values (1235ppm), and highly anomalous silver and lead values were recovered to the south of, and along strike with the area tested by

(1235ppm), and highly anomalous silver and lead values were recovered to the south of, and along strike with the area tested by drilling in 1978 by Riocanex. Also during this program, an extremely rusty ground seep was located within the anomaly area, and appears to have been overlooked by past workers. The value of work completed by Loki in the area of the present Bar claims is approximately $40,000.

In 1993, $6,500 was spent on the property, and consisted of a brief geological program which saw the collection of 94 soil samples, and 2 rock samples. The existing Loki Gold Corp Grid was expanded, and drillholes made by Riocanex in 1977 and 1978 were located and tied-in. The barite in outcrop was also located, and material was examined and sampled by S. Butrenchuk, of Mountain Minerals Ltd.

GEOLOGY

The property covers a section of complexly deformed Upper Proterozoic to Upper Palaeozoic metasediments of the Omineca Tectonic Belt of the Canadian Cordillera. The northwest-southeast trending Pleasant Valley Thrust crosses the claims and separates two tectonically and stratigraphically unique terranes defined by Struik (1988). To the west, the Barkerville Terrane is defined by varieties of grit, quartzite, and pelites with lesser amounts of limestone and volcaniclastic rocks. East of the fault, the Cariboo Terrane comprises Hadrynian to Lower Paleozoic limestone and clastic rocks, and farther to the east, Middle to Upper Paleozoic shales, limestones, and minor basalt.

The rocks of both the Cariboo and Barkerville terannes are structurally complex. According to Struik (1988), they have been affected by at least four episodes of deformation. Generally, the rocks strike to the northwest and dip vertically or steeply to the northeast. Most fold axes plunge gently to the northwest.

The metamorphic grade reaches lower greenschist facies in most of the Cariboo and Barkerville Terrane rocks.

Property Geology

Property geology has been divided by Struik (1982) into five distinct lithologic units, all which strike northwesterly, parallel to claim boundaries, having a consistent 50-60° dip to the northeast.

The youngest unit present within the property is a Tertiary lamprophyre dyke which trends northeasterly, having a vertical dip. Host lithologies are summarized below:

BARKERVILLE TERRANE

Upper Paleozoic

Hardscrabble Mountain succession:

Black siltite and phyllite, grey micaceous quartzite, limestone, minor metatuff?, greywacke, muddy conglomerate

Paleozoic

Bralco succession:

Marble

Downey succession:

Olive and grey micaceous quartzite and phyllite, and

CARIBOO TERRANE

Hadrynian and/or Cambrian

Midas Formation:

Dark siltstone and quartzite, minor shale and argillite

Property Mineralization

Despite the pronounced soil geochemical anomaly present within **Bar** Claim boundaries, very little outcrop mineralization has been discovered. Only two small showings were reported by Riocanex, and were concluded to be related, but not responsible for the extensive geochemical feature. These showings are described below, and their approximate locations shown on Figure 3; following page:

Evening Showing

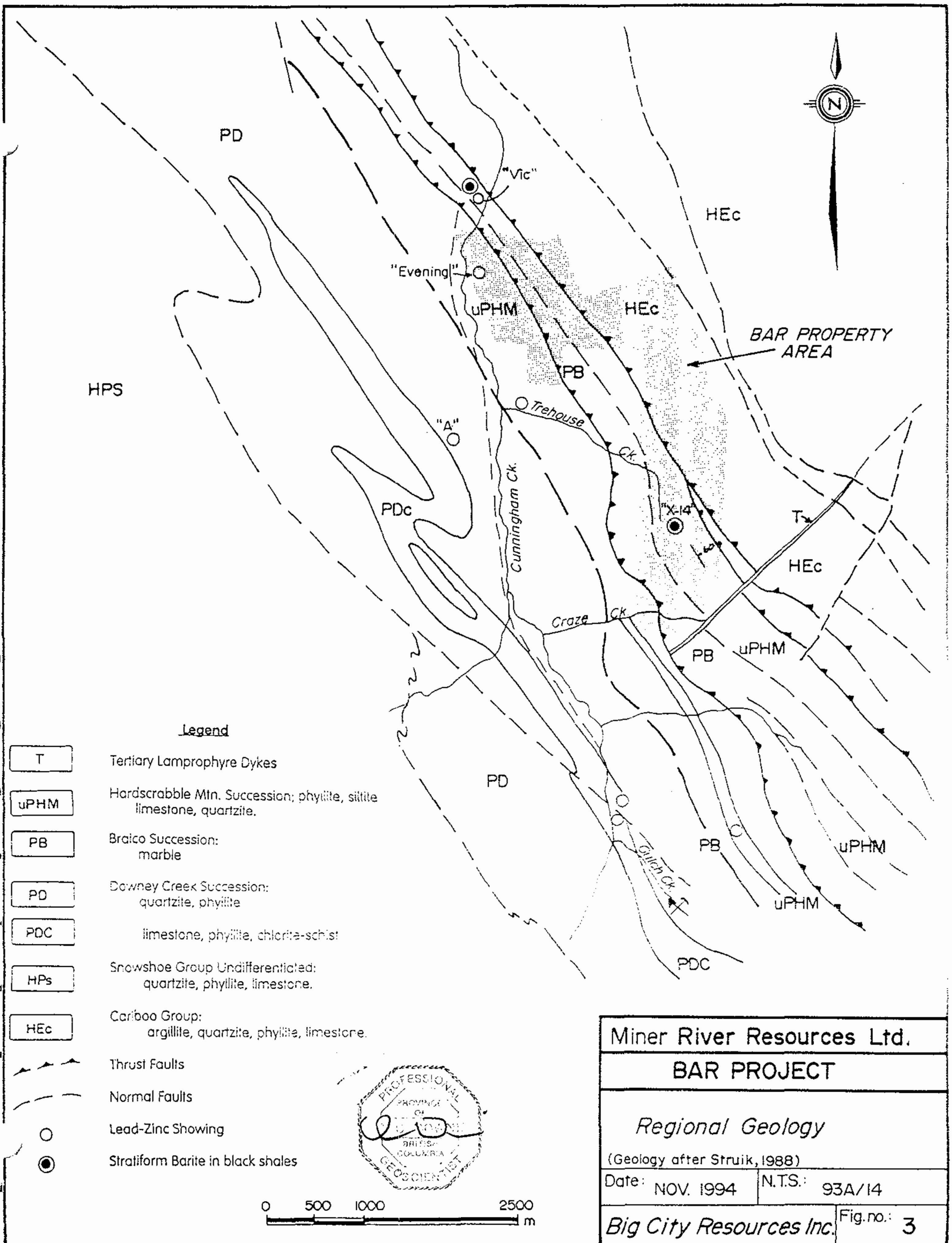
Black cherty shales are host to a conformable sulphide horizon of dark massive sphalerite and galena. A 40cm chip sample taken in 1977 across the mineralization assayed .99% Pb, 3.25% Zn, and .23 oz/t Ag. The showing was originally exposed in a small hand trench from which a sample taken in 1976 assayed 17% Zn. The nature of this sample is unknown. The showing lies along strike with the main Bar geochemical anomaly.

X-14 Showing

Low grade disseminated sphalerite and galena was exposed in 1977 by Riocanex in their 1400 Trench at 3+55W. A grab sample was assayed and found to contain .31% Pb and .70% Zn. Workers at the time suggest that "this mineralization does not explain the occurrence of the extensive X Anomaly, the greater part of which lies uphill from the showing".

Bedded Barite

Parallel to the lead/zinc/silver geochemical anomaly is a bedded barite unit over 2.0m in width. This unit is exposed intermittently on surface for over 300m, and is traced by soil geochemistry for 1300m, with the anomaly open to the north. Whole-rock analysis of this material indicates that it is relatively pure, with a $BaSO_4$ content of 89.59%, and a Specific Gravity of 4.16, making it of acceptable quality for use as a drilling mud product.


PD
"Vic"
HEc
"Evening"
uPHM
HEc
BAR PROPERTY AREA
PB
HPS
Trehouse Ck.
"A"
Cunningham Ck.
PDc
"X-14"
T
HEc
Craze Ck.
PB
uPHM
PD
PB
uPHM
Gulch Ck.
uPHM
PDC
Legend
T Tertiary Lamprophyre Dykes
uPHM Hardscrabble Mtn. Succession: phyllite, siltite limestone, quartzite.
PB Bralco Succession: marble
PD Downey Creek Succession: quartzite, phyllite
PDC limestone, phyllite, chlorite-schist
HPs Snowshoe Group Undifferentiated: quartzite, phyllite, limestone.
HEc Cariboo Group: argillite, quartzite, phyllite, limestone.
Thrust Faults
Normal Faults
Lead-Zinc Showing
Stratiform Barite in black shales
PROFESSIONAL
PROVINCE OF
BRITISH COLUMBIA
GEOSCIENTIST
0 500 1000 2500 m
Miner River Resources Ltd.
BAR PROJECT
Regional Geology
(Geology after Struik, 1988)
Date: NOV. 1994
N.T.S.: 93A/14
Big City Resources Inc.
Fig. no.: 3

1994 PROGRAM

The focus of the $65,000 Summer, 1994 program was to:

(1) extend geochemical coverage initiated by Loki Gold in 1989
(2) locate and tie-in drillholes and trenches constructed by Riocanex in 1977 and 1978
(3) locate and sample the barite occurrences
(4) complete UTEM geophysical coverage of the primary geochemical anomaly.
(5) extend geochemical coverage northward, along strike of the primary anomaly.

A total of 834 soil geochemical samples and 29 rock sample were taken from the property. Sample coverage was designed to extend the existing grid coverage initiated by Loki Gold Corp. in 1989, (the "South Grid"), and to evaluate a new grid area (covered by the "North Grid").

An 8.0 line-km UTEM survey was completed on the South Grid, over the primary soil geochemical anomaly ("X-anomaly"). Work was contracted to SJ Geophysical of Vancouver, the report for which is provided in Appendix V, following this report.

Samples were shipped to Eco-Tech Labs in Kamloops, where they were analyzed by 30 element ICP methods. Eco-Tech's standard procedure for soil sample preparation is provided in Appendix IV, following this report.

Soil samples were taken with a mattock from the B horizon at a depth of about 30 cm.

RESULTS

Geochemistry

South Grid (see Figures 4-7; following)

Results of the 1994 program were extremely encouraging, and clearly warrant extensive follow-up work. Coincident lead-, zinc- and silver-anomalous areas were delineated, and for the most part, indicate mineralization in areas untested by 1977, 1978 RioCanex drilling. The anomalous horizon is some 1000m in length, and its high silver and lead content is confirmed laterally over several separate soil traverses. Coincident with this anomaly is a strong, well-defined barium geochemical anomaly, within which is exposed the bedded barite on surface. The strongest portions of the metals anomaly occur in areas which were not investigated by past Riocanex programs, and must be considered significant exploration targets.

Other encouraging metals anomalies occur at BL 0+00/11+50E and at L2+00S/12+50E, and should see follow-up work done.

Interestingly, poor correlation is made between analytical results returned from both the 1993 program and Loki Golds' 1989 program, and that carried out by Riocanex in 1977. Drillholes completed in 1977 and 1978 by Riocanex generally appear to be located in areas of poor geochemical response, according to 1989 and 1993 data. It is possible that results from the 1977-78 programs were misleading, and caused the location of drillsites to be made in areas of less than optimum potential.

NORTH GRID (see Figures 8-11; following)

A total of 17.6 line-km of survey grid was established in an area of the property located north of Trehouse Creek. The grid was designed to cover any possible extension of geochemically anomalous horizons indicated within the South Grid area.

No linecutting was initiated on this grid, and only hip-chain and compass used for control.

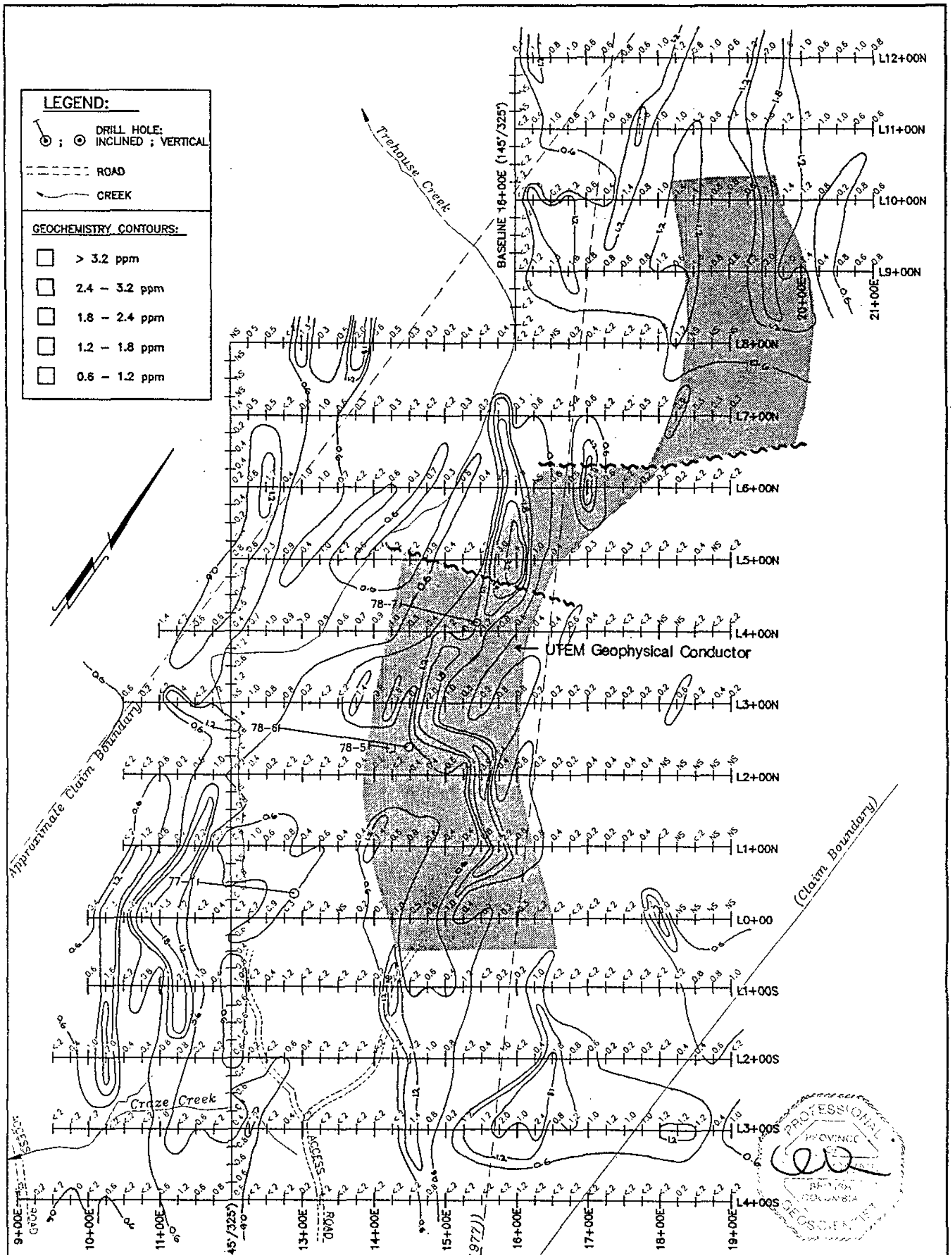
Two strong mineralized trends were indicated in the North Grid area, and occur as parallel, distinct linear features. A strong barite anomaly is indicated over 1200m strike length from L12+00N to L25+00N. Within this anomaly area is found localized silver, lead and zinc enrichment. The strongest response from soils occurs along or near the baseline, from 19+50 to 22+00N.

A strong, continuous silver (with weak zinc and barium) anomaly occurs along the western region of the North Grid, occurring over 1000m, open to the north and south. This anomaly trends off of the present claim area, and forms an obvious staking target.

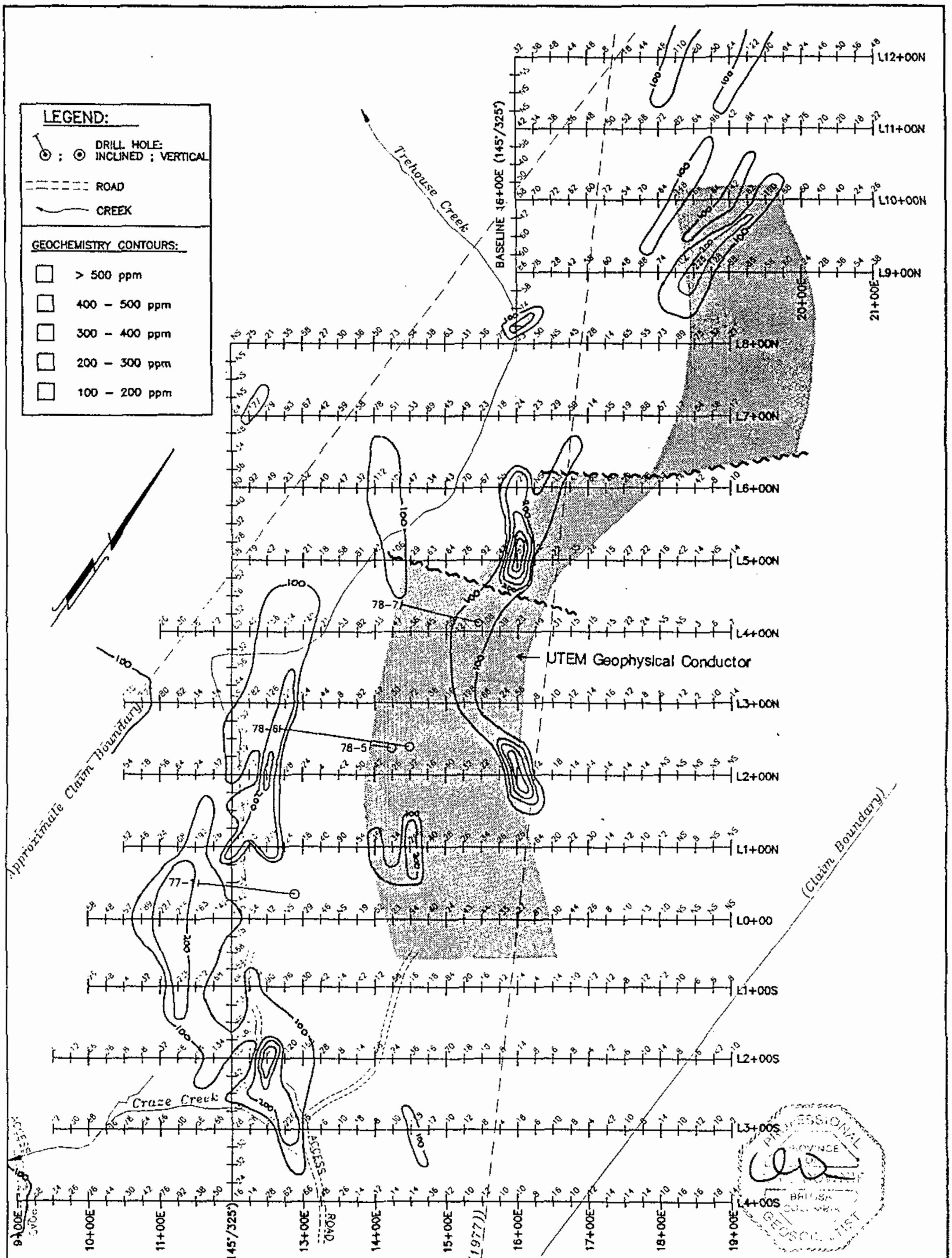
Barite (see Figures 7, 11; following)

The bedded barite occurrence was located at approximately L2N/14+50 E, and was traced intermittently along surface for some 300m. It is exposed over 2.6m in width, representing a true thickness of approximately 2.0m. Tests carried out by Mountain Minerals concluded that the material is suitable as a drilling medium (S. Butrenchuk-personal communication).

Soil sample coverage for barium proved extremely successful in following the underlying barite material, based on its limited exposure on surface. A strong barium anomaly is revealed parallel to stratigraphy within the grid area, and is coincident with known exposures at L2N/14+50E. The anomaly is over 1300m in length, and is open to the south. The anastomosing nature of the anomaly may likely represent either folded or faulted underlying structure, the specifics of which will have to be determined. In either case, it appears as though this unit may prove to be an effective marker for future work programs.



MINER RIVER RESOURCES LIMITED		
BAR PROJECT		
SOUTH GRID SOIL GEOCHEMISTRY Ag IN SOILS		
DATE: NOVEMBER 1994	DRAWN / MAPPED: I. JONES / C. DOWNIE	N.T.S.: 93A / 14
BIG CITY RESOURCES INC.		FIGURE No. 4



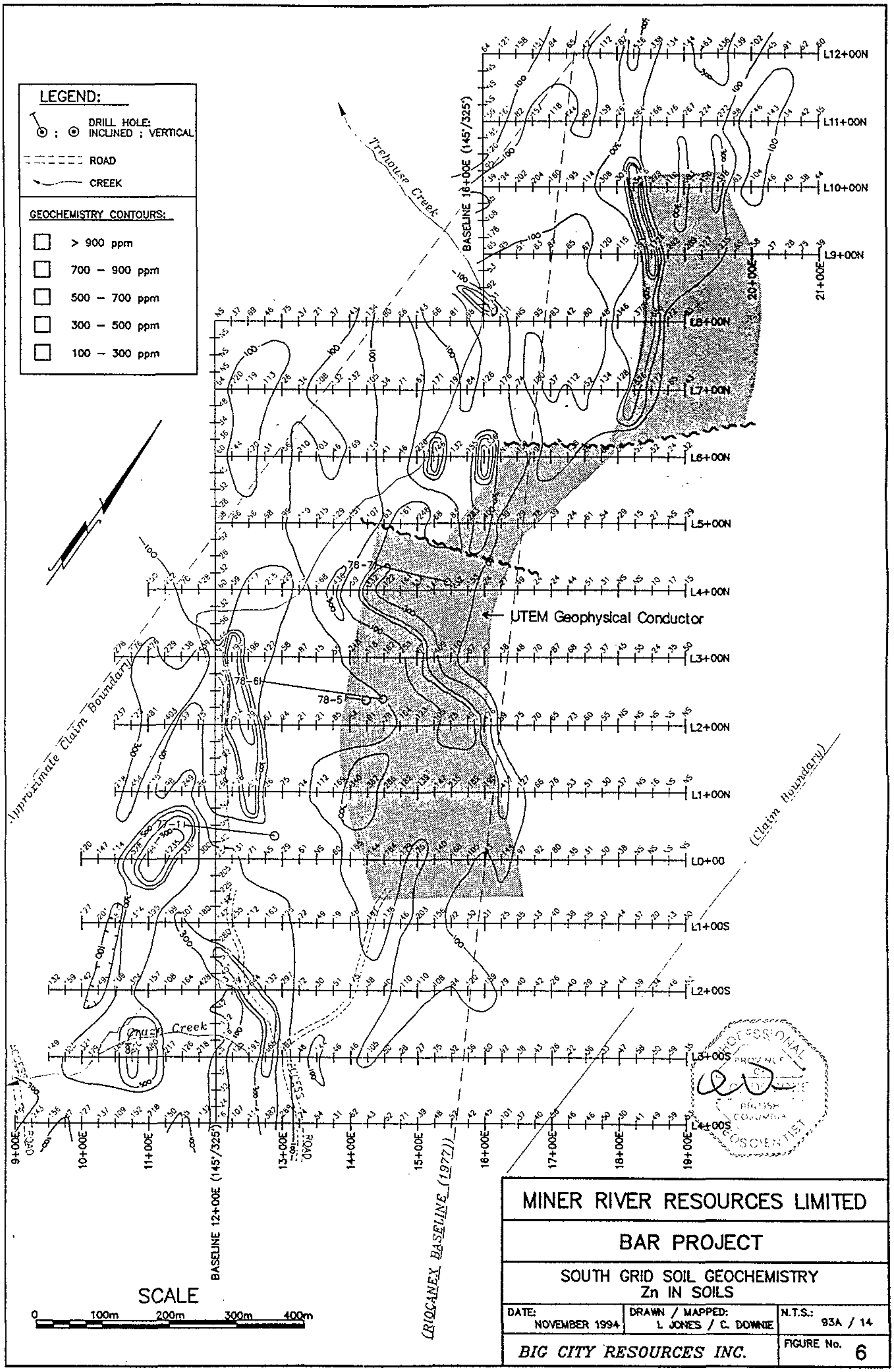
MINER RIVER RESOURCES LIMITED

BAR PROJECT

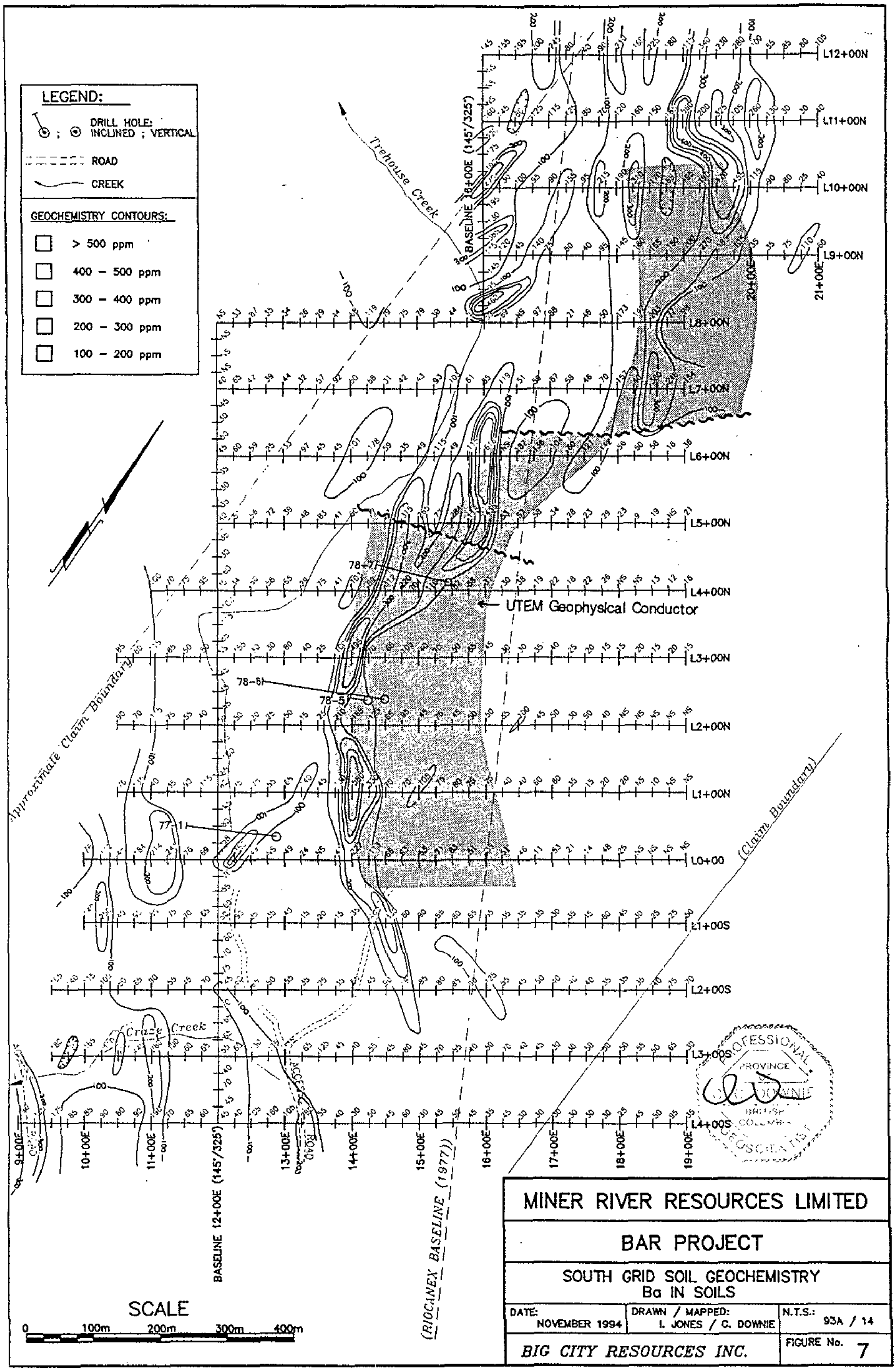
SOUTH GRID SOIL GEOCHEMISTRY
Pb IN SOILS

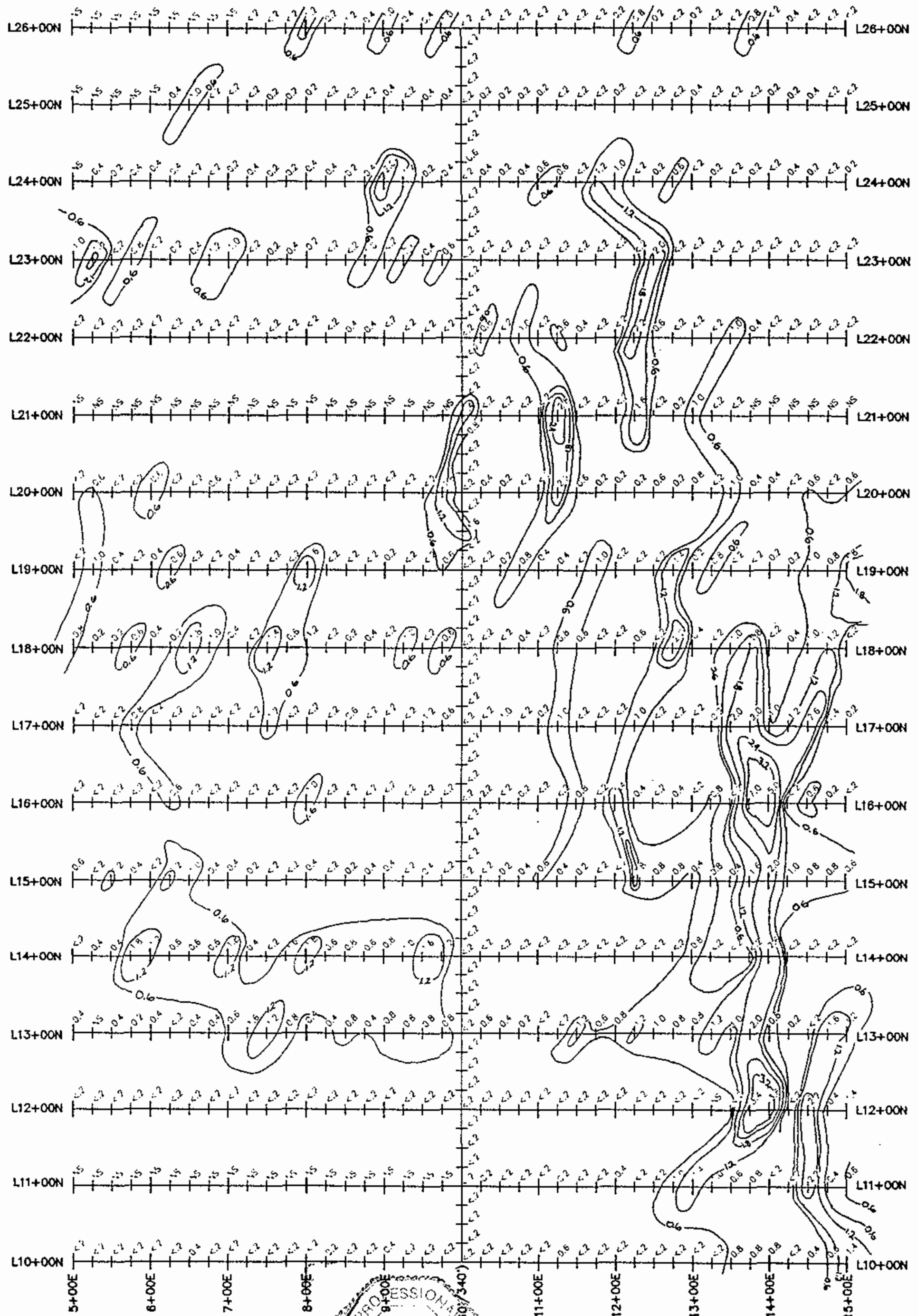
DATE: NOVEMBER 1994 | DRAWN / MAPPED: L. JONES / C. DOWNIE | N.T.S.: 93A / 14

BIG CITY RESOURCES INC. | FIGURE No. 5



LEGEND:
DRILL HOLE: INCLINED ; VERTICAL
ROAD
CREEK
GEOCHEMISTRY CONTOURS:
> 900 ppm
700 – 900 ppm
500 – 700 ppm
300 – 500 ppm
100 – 300 ppm
Trehouse Creek
BASELINE 16+00E (145°/325°)
BASELINE 12+00E (145°/325°)
(RIOCANEX BASELINE (1977))
Approximate Claim Boundary
(Claim Boundary)
UTEM Geophysical Conductor
L12+00N
L11+00N
L10+00N
L9+00N
L8+00N
L7+00N
L6+00N
L5+00N
L4+00N
L3+00N
L2+00N
L1+00N
L0+00
L1+00S
L2+00S
L3+00S
L4+00S
9+00E
10+00E
11+00E
13+00E
14+00E
15+00E
16+00E
17+00E
18+00E
19+00E
20+00E
21+00E
ROAD
Quartz Creek
78-7
78-6
78-5
77-1
SCALE
0 100m 200m 300m 400m
MINER RIVER RESOURCES LIMITED
BAR PROJECT
SOUTH GRID SOIL GEOCHEMISTRY
Zn IN SOILS
DATE: NOVEMBER 1994
DRAWN / MAPPED: L. JONES / C. DOWNIE
N.T.S.: 93A / 14
BIG CITY RESOURCES INC.
FIGURE No. 6


LEGEND:
DRILL HOLE: INCLINED ; VERTICAL
ROAD
CREEK
GEOCHEMISTRY CONTOURS:
> 500 ppm
400 – 500 ppm
300 – 400 ppm
200 – 300 ppm
100 – 200 ppm
Trehouse Creek
Craze Creek
Approximate Claim Boundary
(Claim Boundary)
BASELINE 18+00E (145°/325°)
BASELINE 12+00E (145°/325°)
(RIOCANEX BASELINE (1977))
UTEM Geophysical Conductor
78-7
78-6
78-5
77-1
ACCESS ROAD
L12+00N
L11+00N
L10+00N
L9+00N
L8+00N
L7+00N
L6+00N
L5+00N
L4+00N
L3+00N
L2+00N
L1+00N
L0+00
L1+00S
L2+00S
L3+00S
L4+00S
9+00E
10+00E
11+00E
13+00E
14+00E
15+00E
16+00E
17+00E
18+00E
19+00E
20+00E
21+00E
SCALE
0 100m 200m 300m 400m
MINER RIVER RESOURCES LIMITED
BAR PROJECT
SOUTH GRID SOIL GEOCHEMISTRY
Ba IN SOILS
DATE: NOVEMBER 1994
DRAWN / MAPPED: I. JONES / C. DOWNIE
N.T.S.: 93A / 14
BIG CITY RESOURCES INC.
FIGURE No. 7



GEOCHEMISTRY CONTOURS:

- > 3.2 ppm
- 2.4 – 3.2 ppm
- 1.8 – 2.4 ppm
- 1.2 – 1.8 ppm
- 0.6 – 1.2 ppm

SCALE

0 100m 200m 300m 400m

MINER RIVER RESOURCES LIMITED

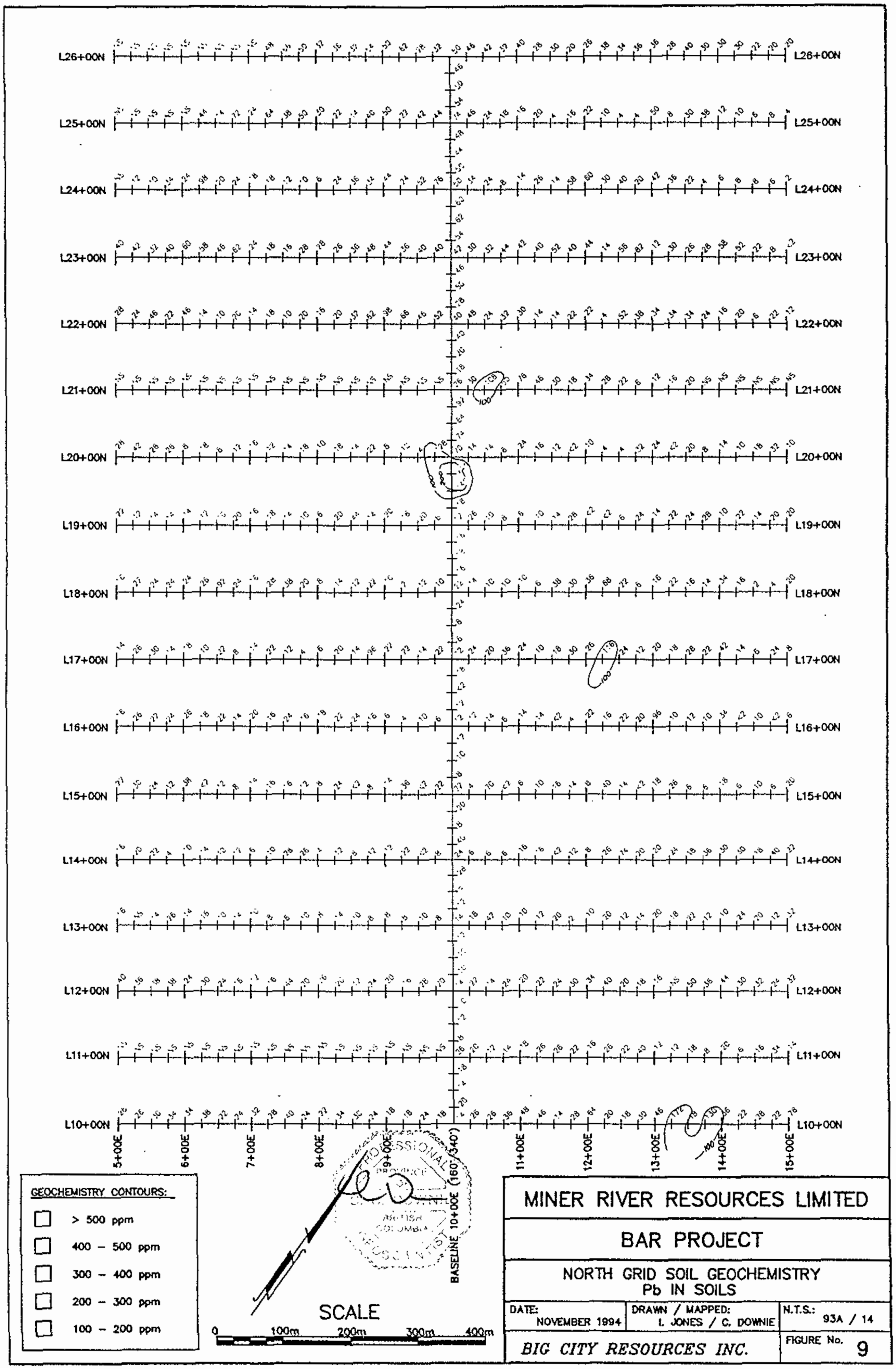
BAR PROJECT

NORTH GRID SOIL GEOCHEMISTRY
Ag IN SOILS

DATE:	DRAWN / MAPPED:	N.T.S.:
NOVEMBER 1994	I. JONES / C. DOWNIE	93A / 14

BIG CITY RESOURCES INC.

FIGURE No. 8



GEOCHEMISTRY CONTOURS:

- > 500 ppm
- 400 – 500 ppm
- 300 – 400 ppm
- 200 – 300 ppm
- 100 – 200 ppm

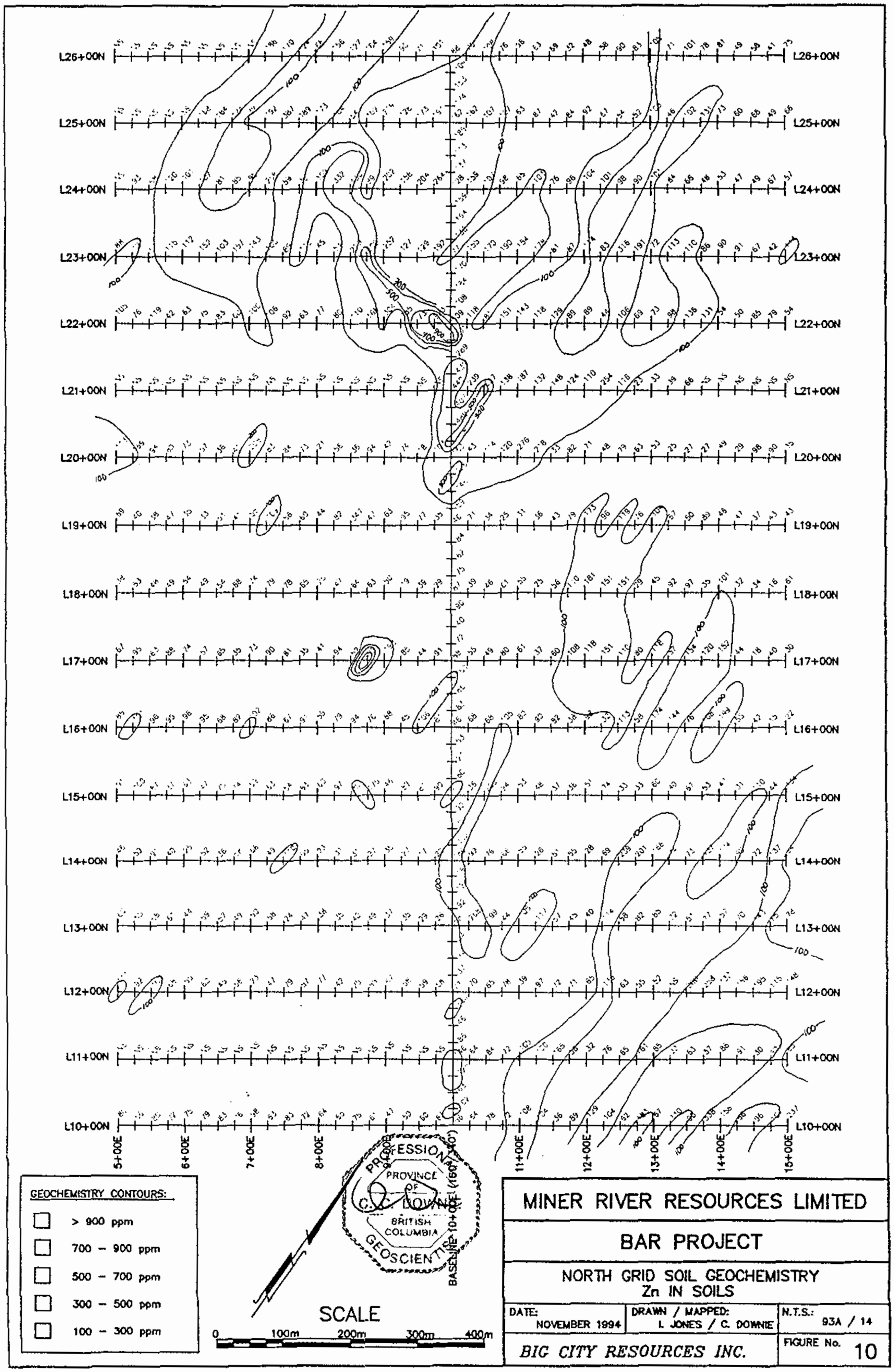
MINER RIVER RESOURCES LIMITED

BAR PROJECT

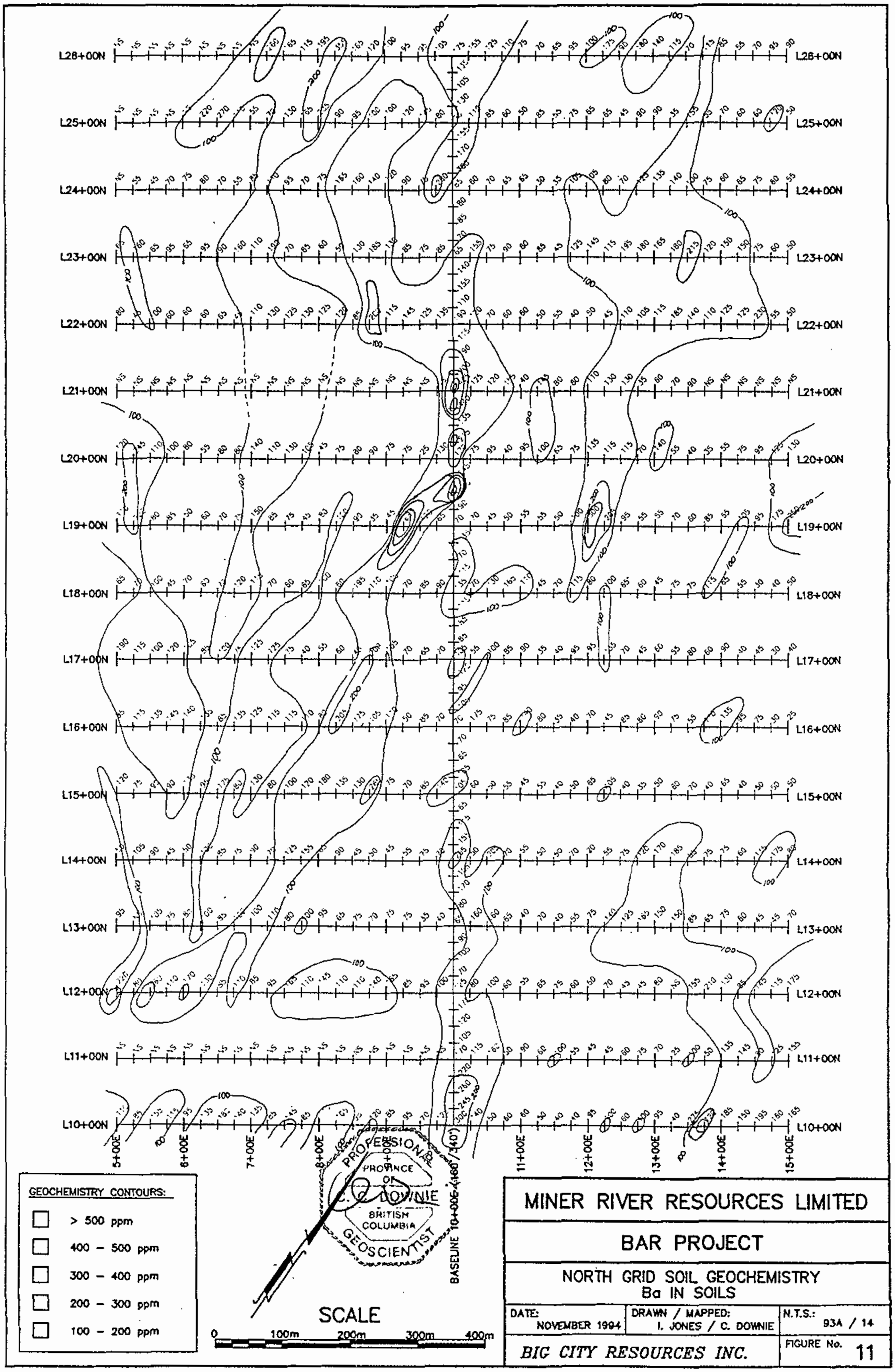
NORTH GRID SOIL GEOCHEMISTRY
Pb IN SOILS

DATE:	DRAWN / MAPPED:	N.T.S.:
NOVEMBER 1994	I. JONES / C. DOWNIE	93A / 14

BIG CITY RESOURCES INC. FIGURE No. 9



L26+00N
L25+00N
L24+00N
L23+00N
L22+00N
L21+00N
L20+00N
L19+00N
L18+00N
L17+00N
L16+00N
L15+00N
L14+00N
L13+00N
L12+00N
L11+00N
L10+00N
5+00E
6+00E
7+00E
8+00E
BASELINE 10+00E
11+00E
12+00E
13+00E
14+00E
15+00E
GEOCHEMISTRY CONTOURS:
> 900 ppm
700 - 900 ppm
500 - 700 ppm
300 - 500 ppm
100 - 300 ppm
SCALE
0
100m
200m
300m
400m
MINER RIVER RESOURCES LIMITED
BAR PROJECT
NORTH GRID SOIL GEOCHEMISTRY
Zn IN SOILS
DATE:
NOVEMBER 1994
DRAWN / MAPPED:
L JONES / C. DOWNIE
N.T.S.:
93A / 14
BIG CITY RESOURCES INC.
FIGURE No. 10



MINER RIVER RESOURCES LIMITED		
BAR PROJECT		
NORTH GRID SOIL GEOCHEMISTRY Ba IN SOILS		
DATE: NOVEMBER 1994	DRAWN / MAPPED: I. JONES / C. DOWNIE	N.T.S.: 93A / 14
BIG CITY RESOURCES INC.		FIGURE No. 11

Geophysics (see appended report by S.J. Geophysics)

Approximately 8 line km of UTEM geophysics was completed on the Bar claims during the 1994 field program. The survey outlined a broad linear zone of high conductivity, open to the north and south, with sharp lateral contacts. The conductive zone is truncated in two areas : Line 500N between 1450 - 1550 E; 625N between 1640 - 1790 E. The linear nature of the anomaly trend and the sharp truncations suggest a conductive bedrock source that is offset by faulting. The shape of the geophysical anomaly mimics the shape of the contoured geochemical data.

EXPLORATION MODEL

Mineralization on the Bar property is similar to that found in the Gataga District of Northeastern British Columbia. The Gataga District hosts at least 22 sedimentary - exhalative type deposits, the largest of which is the Cirque deposit which has a geological reserve in excess of 35 million tons averaging 10% combined Pb/Zn and 47 g/t Ag. Mineralization in the Gataga District is barite-zinc-lead-silver in 19 of the 22 documented deposits. There are also stratiform barite deposits within the district. According to MacIntyre(1992), the Gataga deposits were formed by precipitation of sulfide and sulfate minerals from metalliferous brines that were exhaled along active rift zones. These submarine faults were later reactivated as thrust faults. Mineralization hosting lithologies include cherty to carbonaceous argillite, brecciated dolomite and quartzite, and cherty mudstone. The Gunsteel Formation, which hosts eight important sedimentary-exhalative barite-sulfide deposits, including the Cirque, has a distinctive lithogeochemical signature. Regionally deficient in lead, zinc, copper and silver, the Gunsteel rocks are only enriched in lead and zinc in the immediate footwall of the barite-sulfide deposits. These footwall rocks are also enriched in organic carbon and phosphate. MacIntyre has proposed the underlying Hadrynian Grit unit as a source for the metallic brines.

Mineralization on the Bar Claims indicates the potential for Gataga style barite-zinc-lead-silver deposits. A bedded barite unit 2.0m thick indicates the presence of a paleomarine exhalative system. Exposed intermittently on surface over 300m, the barite horizon has a strong geochemical trace over 1300m. Coincident with the bedded barite horizon is a strong zinc-lead-silver geochemical anomaly.The geochemistry trend shows an anastomosing surface trace which may be related to faulting, possibly related to reactivation along the Pleasant Valley Thrust which cuts the Bar claims to the east. Geochemistry also indicates the presence of elevated phosphate in the soils. The host rocks on the Bar claims are carbonaceous siltites, phyllites, grey micaceous quartzites, siliceous limestones and cherty shales. The Hadrynian Cariboo and Kaza Group rocks include argillites, shales, and greywacke which are potential source rocks for metalliferous brines.

CONCLUSION AND RECOMMENDATIONS

The following conclusions may be drawn from work relating to the Bar property:

The Bar property has indications that it may host a sedimentary-exhalative base metal deposit. A bedded barite horizon 2.0m thick, exposed intermittently on surface over a distance of 300m with a strong soil geochemical trace extending over 1300m, is suggestive of a marine exhalative system. Coincident with the bedded barite horizon is a strong lead-zinc-silver soil geochemical anomaly, also indicative of sedimentary-exhalative style mineralization. 1994 work has located another (possibly continuous) silver-lead-zinc soil anomaly on the North Grid area. The strong linear nature of the geochemical anomalies may be suggestive of underlying stratabound mineralization, or may be related to metal remobilization along re-activated faults. These anomalies could then represent the surface expression of deeper sed-ex mineralization.

Trenching and limited diamond drilling by past operators failed to locate a source for the base metal values in the soils. Trench exposures may have been constrained by overburden thickness. Also the enriched soils may be indications of a sed-ex deposit located beyond the reach of a surface trench. Poor correlation is made between analytical results obtained from the 1994, 1993, and 1989 programs, and that carried out by Riocanex in 1977. Drillholes completed in 1977 and 1978 by Riocanex generally do not appear to be located in areas of optimum geochemical response outlined by 1994, 1993, and 1989 work. The results from the 1977-1978 programs may have been misleading, and the drillsites may not have been in the most favourable locations.

The following field program is recommended to further evaluate sed-ex potential on the Bar claims. A estimated budget for the work is included, following:

1) Land position should be increased by staking north of the BAR 25 and 26 claims and east of the main claim group. This will cover a possible northern extension of a multi-element anomaly located within both the North and South Grid areas.

2) The geochemistry survey should be extended to include any new claims. The new claims should be thoroughly prospected.

3) The North grid area should be prospected, with particular detail in the areas of geochemical soil anomalies.

4) A diamond drilling program of 1000m should be completed to locate the source of the base metal geochemistry anomalies.

5) Contingent on favourable results from Phase 1 drilling, a follow- up drilling program of 6000 feet should be completed.

PROPOSED BUDGET

Phase 1

Personnel	$ 35,000.00
Diamond-Drilling (3000 ft x $35/foot)	105,000.00
Heavy Equipment	20,000.00
Mob/Demob	5,000.00
Analytical	8,000.00
Meals/Grocery	10,000.00
Truck and Equipment Rentals	5,000.00
Fuel (Diesel, Gasoline, Propane)	4,000.00
Supplies	3,000.00
Miscellaneous	6,000.00
Report/Reproduction	4,000.00
Sub-Total:	$205,000.00
10% Contingency:	20,000.00
TOTAL, Phase 1:	**$225,000.00**

Phase 2

Personnel	$ 40,000.00
Diamond-Drilling (6,000ft x $35/foot)	210,000.00
Heavy Equipment	25,000.00
Mob/Demob	5,000.00
Analytical	10,000.00
Meals/Grocery	12,000.00

Truck and Equipment Rentals........................	5,000.00
Fuel (Diesel, Gasoline, Propane)..................	6,000.00
Supplies..	4,000.00
Miscellaneous...................................	5,000.00
Report/Reproduction.............................	3,000.00
Sub-Total:	$325,000.00
10% Contingency:	35,000.00
TOTAL, Phase 2:	**$360,000.00**

REFERENCES

Alldrick, D.J. (1983): The Mosquito Creek Mine, Cariboo Gold Belt; BCDM Geol. Fieldwork 1982, Paper 83-1

Andrew, A., Godwin, C. and Sinclair, Al. (1983): Age and Genesis of Cariboo Gold Mineralization Determined by Isotope Methods (93H); in Geol. Fieldwork 1982, BCDM Paper 1983-1.

BCDM GEM Reports on Coast Interior Ventures work: 1970, p. 207; 1971, p. 136; 1972, p. 333; 1973, p. 295.

Holland, S. (1954): Geology of the Yanks Peak-Roundtop Mountain Area, Cariboo District; BCDM Bull. No. 34.

Humphreys, N (1989): Geological Report on the Cunningham Creek Property, Cariboo Mining Division; private report for Loki Gold Corp.

Kirwin, G.L. (1971): Coast Interior Ventures, Report on Property, Cariboo Mining Division; private report dated 22 Oct. 1971.

MacIntyre, D.G. (1992): Geological Setting and Genesis of Sedimentary Exhalative Barite and Barite-Sulfide Deposits, Gataga District, Northeastern British Columbia; in Exploration and Mining Geology, Vol.1, No.1, pp 1-20;

Matheson, R. (1985): 1985 Field and Assay Report; private report for Clansman Resources, report not dated.

Mitchell, J.M. (1974): Report on the Mineralization of the Main Vein, R.T. Claims, Copper Creek, in the Cariboo Mining Division, BC; private report for Coast Interior Ventures.

Muloin, B.T. (1987): Cunningham Creek Claims; private report for Chaput Logging dated August 1987.

Muloin, B.T. (1988): Cunningham Creek Claims; private report for Chaput Logging dated January 1988.

Robert, F. and Taylor, G. (1989): Structure and Mineralization at the Mosquito Creek Mine, Cariboo District, BC in G.A.C. Cordilleran Section Short Course No. 14, Structural Environments and Gold in the Canadian Cordillera, 18 January, 1989.

Singhai, G.C. (1980): Report on 1-15 Park and Tarn Mineral Claims, Cunningham Creek Area, Cariboo M.D.; private report for Chaput Logging dated 10 January, 1980.

Stewart, J.W. (1970): Report on Examination of Mineral Showings on Nugget and Roundtop Mountains; private report for Coast Interior Ventures dated 26 August, 1970.

Struik, L.C. (1988): The Structural Geology of the Cariboo Gold Mining District, East Central BC; GSC Mem. 421.

Timmins, W.G. (1971): Coast Interior Ventures Ltd., Interim Report on Property, Cariboo Mining Division; private report dated 9 November, 1971.

BCDM ASSESSMENT REPORTS

5609 Park Claim Prospecting Report; R.J. Miller, September 1975.

3521 Coast Interior Ventures, Geochemical Survey; W.G. Timmins; February 1972.

4587 Report on Geophysical Surveys, Barkerville Area, Bon, Park, Roundtop Claims, Coast Interior Ventures; J. Haynes, M. Lewis, June 1973.

6314 Barkerville Project, Description of Sulphide Showings and Geochemistry of Soils; R. Longe for Riocanex Ltd., May 1977.

6545 Barkerville Project, 1977, Cunningham Creek Claims; R. Longe et al., for Riocanex Ltd., October 1977.

7106 Barkerville Project, 1978, Cunningham Creek Claims; R. Longe et at., for Riocanex Ltd., December 1978.

10,270 A Geological and Geochemical Report on Roundtop Mt. Project; P. Hawkins 26 February, 1982.

10,762 Prospecting Report for the Bon 1-4 Mineral Claims; R. Durfield for the Estate of W.E.Thompson, October 1982.

11,193 1982 Exploration Activities at Roundtop Mountain, Cariboo Lake Area; P. Hawkins for Suncor Inc., February 1983.

11,831 Geochemical Report on the Bon 1-4 Mineral Claims; R. Durfield for the Estate of W.E. Thompson, December 1983.

13,085 Geophysical Report on the Bon 1-4 Mineral Claims; R. Durfield for the Estate of W.E. Thompson, October 1984.

13,550 Geochemical Report on the Bou Group of Mineral Claims; R. Durfield for the Estate of W.E.Thompson, March 1985.

13,664 1984 Exploration Activities, Cariboo Gold Project, D. Safton, 1984.

15,552 Geochemical Report on the Bon Mineral Claims; R. Durfield for the estate of W.E. Thompson, December 1986.

16,876 Geochemical Report on the Bon Mineral Claim Group, R. Durfield for the Estate of W.E. Thompson, December 1987.

17,114 1987 Cunningham Creek Property Report; P. Delancey for Imperial Metals, February 1988.

? Termuende, T.J (1990): Geological Report on the Craze Creek (Cunningham) Property, Cariboo Mining Division, on behalf of Loki Gold Corporation, Vancouver, BC.

APPENDIX I

Certificate of Qualification

CERTIFICATE OF QUALIFICATION

I, Charles C. Downie, of 720- 23rd Ave. N. in the City of Cranbrook in the Province of British Columbia do hereby certify that:

1) I am a Professional Geoscientist registered with the Association of Professional Engineers and Geoscientists of British Columbia.

2) I am a 1988 graduate of The University of Alberta with a B.Sc. degree, and have practised my profession as a geologist continuously since graduation in 1988.

3) I have had previous working experience in "Sedex"-type deposit models, including work as underground geologist at Comincos' Sullivan Mine, a world-class sedimentary-exhalative base metal deposit.

3) This report is based on my personal examination of the Bar property.

4) This report is supported by data and observations collected during fieldwork conducted from July 20 - July 24, 1994, in addition to data from past programs dating to 1977.

5) I have no interest, direct or otherwise, in the Bar Claim Group, nor do I anticipate receiving any interest in the Bar Claim group in the future. I do not beneficially own, directly or indirectly, any shares, certificates, or warrants in Miner River Resources Ltd.

Dated this 15th day of December, 1994.

PROFESSIONAL PROVINCE OF C. C. DOWNIE BRITISH COLUMBIA GEOSCIENTIST

C.C. Downie, P.Geo.

APPENDIX II

Statement of Expenditures

Statement of Expenditures

The following expenses were incurred for the purpose of mineral exploration on the **Bar** property, Cariboo Mining Division, British Columbia, between the dates of June 28th and July 25th, 1994:

PERSONNEL		
T. Termuende, P.Geo:	20.0 days x $350/day......	$7,000.00
M. Betker, Assistant:	17.0 days x $225/day......	3,825.00
B. Betker, Assistant:	17.0 days x $200/day......	3,400.00
EQUIPMENT RENTAL		
4WD Vehicles (2):	28.0 days x $50.00/day..........	1,400.00
Mileage:	8820km x $.20/km................	1,764.00
Motorcycle:	1.0 mo. x $1,000/mo.............	1,000.00
Radios (3):	22.0 days x $10.00/day..........	660.00
Chainsaw:	5.0 days x $15.00/day...........	75.00
Camper:	3.0 weeks x $350/week...........	1,050.00
4-Trax ATV:	1.0 mo..........................	1,710.50
ANALYTICAL	....	7,176.71
GEOPHYSICAL SURVEY	....	14,890.98
MATERIALS		
Field Supply:	....	975.00
Fuel:	....	1,502.86
Air Photos:	....	22.06
Reproduction, Maps, Etc	....	451.14
Miscellaneous	....	373.27
SHIPPING	....	72.34
HANDLING CHARGES	....	3,614.11
CONSULTANTS	....	2,109.50
MEALS/ACCOMMODATIONS	....	4,701.38
RECORDING FEES	....	60.00
OFFICE/TELEPHONE	....	200.00
RECLAMATION BOND	....	2,500.00
MISCELLANEOUS	....	373.27
	TOTAL :	**$60,907.12**

Appendix III

Analytical Results

4-Aug-94

ECO-TECH LABORATORIES LTD.
10041 East Trans Canada Highway
KAMLOOPS, B.C.
V2C 2J3

Phone: 604-573-5700
Fax : 604-573-4557

TOKLAT RESOURCES INC. ETK 94-480
2720-17TH STREET SOUTH
CRANBROOK, B.C.
V1C 4H4

ATTENTION: TIM TERMUENDE

29 ROCK samples received July 25, 1994
PROJECT #: NA

Values in ppm unless otherwise reported

Et #.	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
1	BAR94-1	<.2	1.09	<5	750	70	0.82	4	99	17	75	> 15	<10	<.01	1826	<1	0.04	29	4410	8	<5	<20	42	0.02	<10	55	<10	<1	163
2	BAR94-2	<.2	0.12	<5	120	<5	0.03	<1	3	255	7	0.89	<10	0.02	41	18	<.01	7	40	148	<5	<20	2	<.01	<10	2	<10	<1	123
3	BAR94-3	<.2	0.10	5	3310	<5	0.23	<1	5	55	<1	0.23	<10	<.01	13	3	<.01	4	1130	54	<5	<20	127	<.01	<10	4	<10	2	80
4	BAR94-4	<.2	0.07	10	1915	<5	<.01	<1	4	190	4	0.73	<10	<.01	22	16	<.01	12	110	50	<5	<20	7	<.01	<10	32	<10	<1	107
5	BAR94-5	<.2	1.97	<5	925	20	0.59	15	272	36	301	> 15	<10	<.01	4723	3	<.01	445	1600	52	<5	<20	33	<.01	<10	35	<10	25	6804
6	BAR94-6	<.2	0.62	25	515	<5	0.24	4	43	92	237	4.73	<10	<.01	1300	7	0.01	18	2070	18	<5	<20	12	<.01	<10	15	<10	3	185
7	BAR94-7	<.2	0.94	100	585	<5	0.46	5	76	227	150	11.10	<10	<.01	361	15	<.01	345	4400	44	<5	<20	34	<.01	<10	44	<10	13	484
8	BAR94-8	<.2	0.39	30	260	<5	2.66	2	5	220	58	2.52	<10	<.01	85	24	<.01	21	>10000	226	<5	<20	130	<.01	<10	135	<10	15	800
9	BAR94-9	5.6	0.08	105	5620	<5	0.22	12	154	132	266	> 15	<10	<.01	>10000	38	<.01	150	8420	36	<5	<20	33	<.01	<10	26	<10	<1	1220
10	BAR94-10	<.2	<.01	<5	3275	<5	<.01	<1	6	6	<1	0.25	<10	<.01	180	<1	<.01	1	110	<2	<5	<20	38	<.01	<10	1	<10	<1	15
11	BAR94-11	<.2	0.83	5	>10000	<5	0.26	<1	23	39	12	0.58	<10	<.01	78	3	<.01	8	1440	14	<5	<20	150	<.01	<10	16	<10	2	39
12	CDW-1	<.2	> 15	<5	2885	<5	1.12	1	65	238	115	10.80	30	3.98	2495	<1	0.01	127	3420	<2	10	<20	50	0.13	<10	195	<10	13	196
13	CDW-2	<.2	0.13	<5	2950	10	> 15	<1	13	56	<1	5.96	<10	6.61	1814	1	<.01	14	880	16	25	<20	277	<.01	<10	9	<10	6	58
14	CDW-3	<.2	2.60	<5	2230	10	> 15	<1	40	93	43	7.45	20	4.47	1776	<1	<.01	46	2490	38	25	<20	587	<.01	<10	105	<10	8	85
15	CDW-4	<.2	0.05	10	1130	<5	> 15	<1	3	7	<1	0.64	<10	1.82	309	<1	<.01	2	220	<2	30	<20	651	<.01	<10	5	<10	7	25
16	CDW-5	<.2	0.16	5	1315	<5	0.79	<1	6	237	<1	1.14	<10	0.07	334	17	<.01	10	360	10	<5	<20	18	<.01	<10	3	<10	<1	26
17	CDW-6	<.2	0.12	10	1165	<5	0.22	<1	4	265	<1	0.57	<10	0.01	59	19	<.01	6	80	18	<5	<20	5	<.01	<10	2	<10	<1	20
18	CDW-7	<.2	3.38	<5	495	10	0.64	<1	45	583	120	6.08	<10	3.45	697	<1	0.01	233	550	48	<5	<20	16	0.15	<10	106	<10	7	95
19	CDW-8	<.2	1.29	10	1805	<5	0.30	<1	4	162	9	1.33	10	0.07	35	11	0.04	15	5280	24	<5	<20	1533	<.01	<10	27	<10	7	110
20	CDW-9	<.2	1.87	<5	260	<5	0.20	<1	11	95	34	3.51	<10	1.25	48	4	<.01	17	1060	32	10	<20	33	<.01	<10	45	<10	<1	103
21	CDW-10	<.2	0.07	20	235	<5	> 15	<1	2	11	<1	0.65	<10	0.37	267	<1	<.01	3	230	<2	10	<20	702	<.01	<10	4	<10	9	9
22	CDW-11	<.2	<.01	<5	3195	<5	0.84	<1	4	13	<1	0.04	<10	<.01	7	<1	<.01	<1	700	<2	<5	<20	90	<.01	<10	2	<10	<1	2
23	CDW-12	<.2	0.86	10	210	<5	0.14	<1	7	16	6	3.17	10	0.08	436	<1	<.01	11	1350	22	<5	<20	2	<.01	<10	33	<10	<1	41
24	CDW-13	<.2	0.22	135	1950	55	0.48	7	96	25	38	> 15	<10	<.01	1036	<1	<.01	348	9740	54	<5	<20	32	0.01	<10	8	<10	<1	2627
25	CDW-13B	3.2	0.42	55	>10000	<5	0.55	20	864	119	14	> 15	<10	<.01	>10000	223	<.01	656	9630	<2	<5	<20	345	<.01	<10	22	<10	16	2151
26	CDW-14	<.2	0.37	80	1330	20	0.40	3	101	12	47	> 15	<10	<.01	4148	4	<.01	343	6460	106	<5	<20	56	<.01	<10	12	<10	<1	1496
27	CDW-15	<.2	> 15	<5	>10000	<5	0.48	<1	111	121	40	3.58	<10	<.01	1659	7	0.02	46	3370	<2	<5	<20	86	<.01	<10	48	<10	3	146
28	CDW-16	<.2	0.04	<5	3370	<5	0.07	<1	5	5	<1	0.14	<10	<.01	169	<1	<.01	1	350	<2	<5	<20	58	<.01	<10	3	<10	<1	7

Eco-Tech LABORATORIES LTD.

ASSAYING
GEOCHEMISTRY
ANALYTICAL CHEMISTRY
ENVIRONMENTAL TESTING

10041 E. Trans Canada Hwy., R.R. #2, Kamloops, B.C V2C 2J3 Phone (604) 573-5700
Fax (604) 573-4557

CERTIFICATE OF ASSAY ETK 94-480

TOKLAT RESOURCES INC. ETK 94-480
2720-17TH STREET SOUTH
CRANBROOK, B.C.
V1C 4H4

5-Aug-94

ATTENTION: TIM TERMUENDE

29 ROCK samples received July 25,1994
PROJECT #: NA

ET #.	Tag #	Ba (%)
11	BAR94-11	51.90
25	CDW-13B	7.68
27	CDW-15	15.58

XLS/toklat

ECO-TECH LABORATORIES LTD.
Frank J. Pezzotti, A.Sc.T.
B.C. Certified Assayer

8-Aug-94

ECO-TECH LABORATORIES LTD.
10041 East Trans Canada Highway
KAMLOOPS, B.C.
V2C 2J3

Phone: 604-573-5700
Fax : 604-573-4557

TOKLAT RESOURCES INC. ETK 94-481
2720-17TH STREET SOUTH
CRANBROOK, B.C.
V1C 4H4

ATTENTION: TIM TERMUENDE

98 SOIL samples received July 25, 1994
PROJECT #: NA

Values in ppm unless otherwise reported

ET#:	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
1	L7N: 19+ 25 E	2.2	1.55	<5	65	<5	0.08	2	5	21	19	4.20	20	0.17	110	3	<.01	13	1440	42	<5	<20	<1	<.01	<10	48	<10	1	93
2	L7N: 19+ 50 E	1.2	1.80	<5	90	<5	0.11	1	11	40	30	6.66	10	0.36	311	<1	<.01	27	2630	66	<5	<20	1	0.01	<10	44	<10	<1	134
3	L7N: 19+ 75 E	0.2	1.72	5	130	10	0.10	1	11	37	43	5.69	<10	0.30	246	<1	<.01	32	2570	72	<5	<20	8	<.01	<10	52	<10	<1	130
4	L7N: 20+ 00 E	1.6	1.21	<5	55	<5	0.05	1	6	17	20	4.40	30	0.16	142	2	<.01	16	1450	64	<5	<20	<1	<.01	<10	36	<10	2	82
5	L7N: 20+ 25 E	0.6	1.56	<5	75	10	0.11	1	7	24	17	3.91	20	0.26	166	<1	<.01	17	1690	42	<5	<20	4	<.01	<10	35	<10	<1	76
6	L7N: 20+ 50 E	1.8	2.97	<5	70	5	0.72	1	17	26	25	4.18	20	0.41	1624	<1	<.01	32	3900	44	10	<20	63	0.01	<10	32	<10	12	96
7	L7N: 20+ 75 E	0.8	0.69	<5	30	<5	0.29	<1	7	9	9	1.86	<10	0.13	737	<1	<.01	12	1230	16	<5	<20	23	<.01	<10	10	<10	4	48
8	L7N: 21+ 00 E	0.6	1.14	<5	60	<5	0.30	1	19	16	17	4.08	20	0.17	1067	<1	<.01	26	1620	34	<5	<20	36	<.01	<10	18	<10	8	76
9	L9N: 16+ 25 ER	1.2	1.55	<5	120	<5	0.12	1	14	25	18	4.03	20	0.20	890	<1	<.01	18	1660	78	<5	<20	<1	<.01	<10	29	<10	2	95
10	L9N: 16+ 50 ER	1.0	1.31	<5	45	<5	0.05	<1	6	16	13	2.75	30	0.12	177	1	<.01	14	1210	28	<5	<20	<1	<.01	<10	35	<10	2	51
11	L9N: 16+ 75 ER	1.8	1.01	<5	140	<5	0.07	2	7	17	15	2.80	20	0.14	164	3	<.01	22	1860	42	<5	<20	<1	<.01	<10	24	<10	3	83
12	L9N: 17+ 00 ER	0.8	1.31	<5	75	<5	0.04	1	10	29	21	4.84	20	0.24	140	1	<.01	26	1790	58	<5	<20	7	<.01	<10	34	<10	<1	87
13	L9N: 17+ 25 ER	0.8	1.31	<5	50	<5	0.06	1	8	34	15	4.43	20	0.20	94	2	<.01	26	2390	60	<5	<20	<1	<.01	<10	44	<10	<1	65
14	L9N: 17+ 50 ER	0.6	0.79	<5	40	<5	0.04	<1	9	20	20	2.40	30	0.05	64	1	<.01	26	750	48	<5	<20	<1	<.01	<10	37	<10	2	67
15	L9N: 17+ 75 ER	0.8	1.64	5	95	15	0.10	1	15	46	31	6.69	10	0.42	387	<1	<.01	41	3260	88	<5	<20	13	<.01	<10	57	<10	<1	120
16	L9N: 18+ 00 ER	1.2	1.42	5	145	<5	0.14	2	11	40	26	5.53	20	0.39	458	1	<.01	37	3650	74	<5	<20	<1	<.01	<10	51	<10	2	115
17	L9N: 18+ 25 ER	0.6	1.22	15	180	<5	0.14	1	13	21	30	5.04	10	0.13	234	2	<.01	53	2560	102	<5	<20	5	<.01	<10	30	<10	1	193
18	L9N: 18+ 50 ER	1.6	1.26	10	165	<5	0.93	9	27	26	69	5.18	20	0.18	1178	<1	<.01	74	2220	228	<5	<20	40	<.01	<10	23	<10	13	1726
19	L9N: 18+ 75 ER	0.8	1.02	15	150	<5	0.07	1	13	18	35	5.26	20	0.06	362	2	<.01	50	1380	128	<5	<20	3	<.01	<10	30	<10	1	262
20	L9N: 19+ 00 ER	0.6	2.14	15	200	10	0.08	1	19	58	31	5.49	10	0.52	405	<1	<.01	47	1280	88	<5	<20	7	<.01	<10	63	<10	1	289
21	L9N: 19+ 25 ER	1.2	1.90	<5	270	<5	0.04	1	8	26	20	4.43	20	0.41	309	1	<.01	24	1210	86	<5	<20	<1	<.01	<10	41	<10	1	127
22	L9N: 19+ 50 ER	2.0	1.86	<5	185	5	0.17	2	10	30	48	6.47	40	0.41	168	6	<.01	44	3190	58	<5	<20	28	<.01	<10	56	<10	3	235
23	L9N: 19+ 75 ER	1.0	1.41	10	105	<5	0.06	1	6	28	26	5.91	20	0.19	105	4	<.01	18	4270	60	<5	<20	14	<.01	<10	68	<10	<1	65
24	L9N: 20+ 00 ER	1.4	1.14	<5	35	<5	0.03	1	4	23	17	2.71	30	0.19	132	2	<.01	18	800	24	<5	<20	<1	<.01	<10	42	<10	3	58
25	L9N: 20+ 25 ER	0.4	0.93	<5	35	<5	0.03	<1	3	10	9	1.29	30	0.07	64	1	<.01	8	550	28	<5	<20	<1	<.01	<10	22	<10	2	37
26	L9N: 20+ 50 ER	0.8	1.69	<5	75	<5	0.06	<1	2	16	7	1.30	30	0.10	60	1	<.01	6	540	36	5	<20	7	<.01	<10	29	<10	2	28
27	L9N: 20+ 75 ER	0.6	2.66	<5	110	10	0.05	1	15	61	42	7.51	<10	1.05	478	<1	<.01	34	1250	54	<5	<20	<1	0.02	<10	144	<10	<1	75
28	L9N: 21+ 00 ER	0.8	1.51	<5	60	<5	0.03	<1	5	21	11	2.16	30	0.17	105	1	<.01	11	580	38	<5	<20	9	<.01	<10	50	<10	1	39

TOKLAT RESOURCES INC. ETK 94-481

Eco-Tech Laboratories Ltd.

ET#:	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
29	L10N: 16+ 25 ER	1.8	1.91	<5	130	<5	0.55	2	26	28	39	5.54	20	0.34	1606	1	<.01	45	2320	70	<5	<20	27	<.01	<10	31	<10	13	194
30	L10N: 16+ 50 ER	0.2	1.41	<5	100	<5	0.35	1	24	26	35	5.23	20	0.34	785	<1	<.01	42	1440	72	<5	<20	21	<.01	<10	26	<10	7	202
31	L10N. 16+ 75 ER	1.2	1.24	<5	95	<5	0.96	1	19	22	31	4.56	10	0.32	760	<1	<.01	45	1770	62	<5	<20	51	<.01	<10	20	<10	14	204
32	L10N: 17+ 00 ER	0.6	1.24	<5	90	<5	0.16	<1	14	24	24	4.54	20	0.25	341	<1	<.01	32	1470	60	<5	<20	5	<.01	<10	27	<10	3	160
33	L10N: 17+ 25 ER	0.4	1.50	<5	155	<5	0.09	1	18	41	28	5.10	20	0.36	564	1	<.01	41	1280	72	<5	<20	<1	<.01	<10	38	<10	1	195
34	L10N: 17+ 50 ER	1.4	1.17	<5	95	<5	1.12	1	12	26	20	3.52	10	0.28	208	2	<.01	30	1570	54	10	<20	29	<.01	<10	24	<10	7	114
35	L10N: 17+ 75 ER	0.8	1.38	15	215	<5	0.59	2	36	34	52	6.25	<10	0.29	1548	2	<.01	70	2450	70	<5	<20	42	<.01	<10	27	<10	14	308
36	L10N. 18+ 00 ER	1.0	1.53	<5	190	<5	0.10	1	11	40	20	4.03	20	0.31	292	2	<.01	32	1890	64	<5	<20	<1	<.01	<10	45	<10	2	303
37	L10N: 18+ 25 ER	1.4	1.30	<5	310	<5	1.08	15	14	19	66	3.85	10	0.25	932	<1	<.01	54	1260	148	5	<20	41	<.01	<10	24	<10	8	3416
38	L10N: 18+ 50 ER	1.4	2.27	<5	170	10	0.07	2	21	32	67	8.29	<10	0.57	1154	3	<.01	45	1970	66	<5	<20	15	<.01	<10	73	<10	<1	279
39	L10N 18+ 75 ER	0.8	2.92	<5	65	10	0.04	1	10	84	13	6.19	<10	1.37	285	1	<.01	23	750	64	10	<20	<1	0.01	<10	114	<10	<1	110
40	L10N 19+ 00 ER	0.8	2.94	45	195	15	0.06	2	30	246	55	8.10	<10	1.66	1217	<1	<.01	175	1450	142	5	<20	<1	0.01	<10	100	<10	<1	383
41	L10N. 19+ 25 ER	0.6	1.67	<5	190	<5	0.10	1	12	36	33	5.13	20	0.46	437	4	<.01	31	2260	62	<5	<20	9	<.01	<10	39	<10	<1	150
42	L10N: 19+ 50 ER	2.0	1.46	15	470	<5	0.67	4	20	21	84	5.04	20	0.24	968	4	<.01	40	4020	190	<5	<20	26	<.01	<10	36	<10	9	318
43	L10N. 19+ 75 ER	1.4	0.69	15	455	<5	0.16	<1	3	16	26	2.51	30	0.06	58	8	<.01	9	3420	88	<5	<20	157	<.01	<10	46	<10	5	63
44	L10N: 20+ 00 ER	1.2	3.45	10	115	15	0.23	1	17	327	37	7.34	<10	2.35	292	<1	<.01	124	1750	60	<5	<20	<1	0.01	<10	118	<10	<1	104
45	L10N: 20+ 25 ER	0.8	1.19	<5	90	<5	0.05	<1	4	25	14	2.24	20	0.17	124	1	<.01	14	1360	40	<5	<20	1	<.01	<10	29	<10	1	46
46	L10N: 20+ 50 ER	0.2	1.65	<5	80	<5	0.03	<1	5	23	17	3.15	20	0.16	101	<1	<.01	11	900	40	<5	<20	7	<.01	<10	40	<10	<1	40
47	L10N: 20+ 75 ER	0.8	0.73	<5	25	<5	0.03	<1	2	13	17	1.14	20	0.07	46	2	<.01	8	480	24	<5	<20	<1	<.01	<10	24	<10	2	38
48	L10N: 21+ 00 ER	0.6	1.13	<5	40	<5	0.02	<1	6	8	29	1.81	40	0.05	89	2	<.01	13	570	26	<5	<20	<1	<.01	<10	30	<10	2	44
49	L11N: 7+ 75 EN	1.4	1.08	<5	90	<5	2.88	1	8	15	25	2.54	20	0.21	277	3	<.01	30	1710	18	5	<20	111	<.01	<10	18	<10	11	72
50	L11N: 8+ 00 EN	1.0	1.48	<5	95	<5	0.67	1	12	22	23	4.23	20	0.30	460	3	<.01	25	1340	34	<5	<20	30	<.01	<10	30	<10	2	83
51	L11N: 8+ 25 EN	<2	1.27	10	115	10	0.30	<1	13	26	25	4.05	20	0.24	431	2	<.01	28	1280	44	<5	<20	25	<.01	<10	31	<10	2	108
52	L11N. 8+ 50 EN	1.0	0.99	<5	90	<5	0.14	1	9	20	23	3.82	20	0.16	223	5	<.01	27	1780	32	<5	<20	<1	<.01	<10	29	<10	2	93
53	L11N: 8+ 75 EN	0.8	1.61	15	125	5	1.01	2	20	31	29	4.57	20	0.39	695	2	<.01	44	1190	48	5	<20	40	0.01	<10	28	<10	7	167
54	L11N: 9+ 00 EN	1.0	0.54	<5	130	<5	3.61	2	6	9	54	1.16	<10	0.17	433	3	0.02	17	1180	14	10	<20	156	<.01	<10	8	<10	5	126
55	L11N: 9+ 25 EN	0.6	1.58	5	80	10	0.36	1	16	28	21	4.52	20	0.28	303	3	<.01	33	830	44	<5	<20	11	<.01	<10	31	<10	3	132
56	L11N: 9+ 50 EN	0.8	1.62	5	160	10	1.09	1	15	24	25	4.12	20	0.23	411	3	<.01	30	1730	48	<5	<20	55	<.01	<10	29	<10	4	115
57	L11N: 9+ 75 EN	1.4	1.80	<5	85	<5	0.47	1	17	24	23	4.70	30	0.51	509	<1	<.01	39	1270	34	<5	<20	6	<.01	<10	25	<10	5	136
58	L11N. 16+ 25 ER	0.4	1.16	<5	145	<5	1.14	<1	19	21	35	4.47	10	0.38	795	<1	<.01	40	1240	34	<5	<20	42	<.01	<10	19	<10	4	161
59	L11N: 16+ 50 ER	1.0	1.17	<5	80	<5	0.07	<1	9	20	20	3.98	20	0.14	183	1	<.01	23	790	38	<5	<20	<1	<.01	<10	36	<10	1	82
60	L11N: 16+ 75 ER	0.8	1.07	<5	125	<5	1.41	<1	17	20	32	3.62	<10	0.33	843	<1	<.01	33	1250	36	<5	<20	59	<.01	<10	17	<10	5	157
61	L11N: 17+ 00 ER	1.2	1.73	<5	115	5	0.50	1	28	23	21	4.91	10	0.20	669	<1	<.01	25	1140	48	<5	<20	16	<.01	<10	32	<10	6	118
62	L11N: 17+ 25 ER	1.0	1.60	<5	125	5	0.41	1	20	30	35	4.80	20	0.30	1071	<1	<.01	45	1190	50	<5	<20	19	<.01	<10	28	<10	13	144
63	L11N: 17+ 50 ER	0.8	1.22	<5	85	<5	0.05	<1	9	26	19	4.39	20	0.20	185	1	<.01	23	1650	52	<5	<20	6	<.01	<10	33	<10	<1	82
64	L11N: 17+ 75 ER	1.8	1.54	<5	70	<5	0.12	1	16	39	34	6.11	10	0.38	429	2	<.01	49	2950	68	<5	<20	<1	<.01	<10	36	<10	1	159
65	L11N: 18+ 00 ER	1.0	1.36	<5	130	5	0.18	2	17	29	32	4.99	10	0.30	608	2	<.01	44	2110	72	<5	<20	9	<.01	<10	29	<10	2	261
66	L11N: 18+ 25 ER	1.0	1.81	5	160	<5	1.40	3	25	49	72	5.65	<10	0.48	654	3	<.01	64	2380	82	5	<20	68	<.01	<10	34	<10	10	364
67	L11N: 18+ 50 ER	1.2	2.12	10	150	<5	0.06	2	17	54	36	5.97	10	0.54	528	2	<.01	48	1300	64	<5	<20	<1	<.01	<10	49	<10	1	166

TOKLAT RESOURCES INC. ETK 94-481 Eco-Tech Laboratories Ltd.

ET#:	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
68	L11N: 18+ 75 ER	0.8	2.21	25	165	5	0.06	1	28	128	48	6.46	<10	0.87	1245	2	<.01	82	2220	96	<5	<20	3	<.01	<10	77	<10	<1	176
69	L11N: 19+ 00 ER	1.2	> 15	<5	560	5	0.20	4	68	152	63	9.63	<10	2.21	3183	4	<.01	139	2020	<2	10	<20	<1	<.01	<10	120	<10	<1	267
70	L11N: 19+ 25 ER	1.8	1.07	20	200	<5	0.31	2	8	19	48	3.84	20	0.15	239	5	<.01	29	3500	84	<5	<20	10	<.01	<10	44	<10	3	224
71	L11N: 19+ 50 ER	1.8	1.75	40	325	5	0.21	4	23	55	74	6.76	20	0.38	710	12	<.01	67	2630	74	<5	<20	28	<.01	<10	63	<10	2	272
72	L11N: 19+ 75 ER	1.2	0.86	10	105	<5	0.07	1	6	14	45	3.60	20	0.07	135	6	<.01	19	2240	64	<5	<20	10	<.01	<10	30	<10	2	88
73	L11N: 20+ 00 ER	1.2	2.73	20	260	<5	1.00	1	25	198	50	5.65	60	1.46	1137	<1	<.01	97	1710	76	10	<20	81	<.01	<10	71	<10	24	146
74	L11N: 20+ 25 ER	1.0	1.97	<5	130	<5	0.07	2	18	28	60	9.01	20	0.38	335	<1	<.01	38	1960	70	<5	<20	<1	<.01	<10	35	<10	2	143
75	L11N: 20+ 50 ER	1.0	0.89	<5	30	<5	0.06	<1	2	9	15	0.98	20	0.07	32	<1	<.01	6	310	20	<5	<20	<1	<.01	<10	18	<10	2	34
76	L11N: 20+ 75 ER	0.6	0.77	<5	30	<5	0.02	<1	6	4	14	2.40	20	0.03	144	<1	<.01	10	550	18	<5	<20	<1	<.01	<10	19	<10	1	42
77	L11N: 21+ 00 ER	0.6	1.12	<5	40	<5	0.07	<1	3	9	19	1.39	20	0.08	76	<1	<.01	6	700	22	<5	<20	<1	<.01	<10	21	<10	1	35
78	L12N: 61+ 00 E	0.4	1.26	<5	145	5	0.12	<1	7	23	17	3.84	20	0.19	302	<1	<.01	15	1340	32	<5	<20	2	<.01	<10	33	<10	<1	64
79	L12N: 16+ 25 E	1.4	1.68	<5	155	<5	0.84	2	19	29	32	4.70	20	0.38	1027	2	<.01	39	1230	38	10	<20	23	<.01	<10	30	<10	6	121
80	L12N: 16+ 50 E	0.8	1.77	<5	195	<5	0.70	1	19	32	30	4.88	10	0.39	784	1	<.01	38	1090	48	<5	<20	31	<.01	<10	32	<10	4	158
81	L12N. 16+ 75 E	1.0	1.86	<5	200	<5	0.77	1	16	34	26	4.87	10	0.38	753	2	<.01	33	1330	44	<5	<20	25	<.01	<10	37	<10	1	151
82	L12N: 17+ 00 E	0.6	2.00	<5	245	5	0.68	1	8	33	15	4.04	20	0.25	152	2	<.01	21	730	48	<5	<20	25	<.01	<10	50	<10	<1	84
83	L12N: 17+ 25 E	0.6	0.19	<5	80	<5	3.62	1	2	6	46	0.29	<10	0.18	653	1	<.01	19	1060	8	10	<20	117	<.01	<10	2	<10	4	65
84	L12N: 17+ 50 E	0.8	1.02	<5	40	<5	0.08	<1	4	15	8	2.11	30	0.13	99	1	<.01	12	430	18	<5	<20	<1	<.01	<10	27	<10	2	42
85	L12N: 17+ 75 E	0.6	1.49	<5	90	5	0.04	<1	12	30	21	5.68	10	0.24	365	2	<.01	26	1100	44	<5	<20	<1	<.01	<10	31	<10	<1	112
86	L12N: 18+ 00 E	1.0	1.79	<5	210	5	1.03	2	23	34	40	5.38	10	0.45	776	3	<.01	52	1360	48	5	<20	33	<.01	<10	29	<10	6	182
87	L12N: 18+ 25 E	1.2	1.37	5	160	<5	1.50	4	19	29	66	3.97	10	0.36	623	2	<.01	49	1780	110	10	<20	54	<.01	<10	28	<10	9	536
88	L12N: 18+ 50 E	0.8	2.28	20	225	<5	0.76	3	23	55	70	5.55	20	0.68	674	3	<.01	60	1790	80	10	<20	36	<.01	<10	49	<10	6	338
89	L12N: 18+ 75 E	1.0	1.78	<5	180	5	0.34	1	12	47	26	4.48	20	0.54	342	2	<.01	34	1310	50	<5	<20	5	<.01	<10	49	<10	<1	134
90	L12N: 19+ 00 E	0.6	2.26	30	115	<5	0.06	1	17	195	30	5.71	10	0.88	390	1	<.01	78	1680	64	<5	<20	<1	<.01	<10	65	<10	<1	144
91	L12N: 19+ 25 E	1.0	2.52	20	340	5	0.64	6	48	63	67	7.81	20	0.67	3445	2	<.01	82	3490	122	<5	<20	46	0.01	<10	61	<10	10	463
92	L12N: 19+ 50 E	2.0	1.35	15	230	<5	1.73	10	17	37	133	3.38	60	0.32	1703	3	<.01	91	3840	90	5	<20	86	<.01	<10	32	<10	37	336
93	L12N: 19+ 75 E	1.8	0.93	5	280	<5	0.22	2	4	25	25	1.95	20	0.16	68	2	<.01	20	1480	94	<5	<20	12	<.01	<10	16	<10	6	139
94	L12N: 20+ 00 E	1.0	1.21	<5	100	<5	0.05	1	9	17	24	4.28	30	0.11	176	3	<.01	31	1440	74	<5	<20	<1	0.01	<10	36	<10	2	102
95	L12N: 20+ 25 E	0.6	1.57	<5	55	<5	0.03	<1	4	13	11	2.31	20	0.11	72	<1	<.01	11	480	46	<5	<20	<1	0.01	<10	33	<10	2	45
96	L12N: 20+ 50 E	0.6	1.80	5	85	5	0.08	1	8	23	24	4.22	10	0.18	212	<1	<.01	21	1200	50	<5	<20	2	0.01	<10	48	<10	<1	91
97	L12N: 20+ 75 E	1.0	1.15	<5	80	<5	0.13	1	6	15	29	3.22	30	0.08	294	1	<.01	11	650	36	<5	<20	<1	0.01	<10	35	<10	3	62
98	L12N: 21+ 00 E	0.8	1.14	<5	105	<5	0.03	<1	10	12	21	3.53	20	0.11	793	<1	<.01	15	1050	48	<5	<20	<1	<.01	<10	23	<10	<1	60

QC/DATA:		Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
Repeat #:																													
1	L7N: 19+ 25 E	2.0	1.46	<5	75	<5	0.05	1	6	22	17	4.05	20	0.14	120	2	<.01	13	1480	48	<5	<20	<1	<.01	<10	45	<10	<1	88
30	L10N: 16+ 50 ER	1.0	1.42	<5	85	<5	0.62	1	23	25	33	5.21	20	0.34	782	1	<.01	43	1460	68	<5	<20	18	<.01	<10	26	<10	8	204
77	L11N: 21+ 00 ER	0.6	1.08	<5	35	<5	0.06	<1	2	9	15	1.26	20	0.07	73	<1	<.01	6	690	20	<5	<20	<1	<.01	<10	19	<10	1	32
Standard 1993																													
		1.4	2.00	65	175	<5	2.00	2	21	70	88	4.10	<10	0.99	728	<1	0.03	26	700	22	5	<20	65	1.40	<10	86	<10	10	76
		1.4	1.95	65	100	<5	1.99	2	21	74	85	4.20	<10	0.97	718	<1	0.03	26	710	24	20	<20	55	0.12	<10	84	<10	9	82
		1.4	2.13	55	150	5	1.96	2	21	72	81	4.49	<10	0.93	699	<1	0.03	31	720	50	20	<20	55	0.16	<10	89	<10	13	82

ECO-TECH LABORATORIES LTD
Frank J. Pezzotti, A.Sc.T.
B.C. Certified Assayer

XLS/toklat

July 28, 1994

ECO-TECH LABORATORIES LTD.
10041 East Trans Canada Highway
KAMLOOPS, B.C.
V2C 2J3

Phone: 604-573-5700
Fax : 604-573-4557

TOKLAT RESOURCES INC. ETK 94-455
2720-17TH STREET SOUTH
CRANBROOK, B.C.
V1C 4H4

ATTENTION: TIM TERMUENDE

834 samples received July 14,1994
PROJECT #: NA

Values in ppm unless otherwise reported

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
1	L9N: 14+ 00 E	<.2	1.86	35	210	<5	0.23	<1	20	44	43	5.14	<10	0.28	1091	2	0.02	29	2610	28	<5	<20	12	0.01	<10	41	<10	<1	114
2	L9N: 14+ 25 E	<.2	1.80	50	490	<5	0.24	2	29	60	81	6.18	<10	0.35	1503	2	0.03	41	2100	42	<5	<20	17	<.01	<10	48	<10	21	156
3	L9N: 14+ 50 E	<.2	1.44	45	295	<5	1.05	1	25	44	49	5.31	<10	0.31	917	4	0.02	42	2270	58	<5	<20	56	0.01	<10	41	<10	20	204
4	L9N: 14+ 75 E	<.2	1.16	25	180	<5	0.46	<1	12	34	40	4.91	<10	0.17	349	3	0.01	25	1630	44	<5	<20	39	<.01	<10	45	<10	<1	148
5	L9N: 15+ 00 E	<.2	0.89	20	115	<5	0.13	<1	7	33	16	2.98	<10	0.22	120	3	0.03	16	2240	36	<5	<20	23	<.01	<10	42	<10	2	71
6	L9N: 15+ 25 E	<.2	0.94	85	510	<5	0.66	5	49	24	171	7.99	<10	0.16	3211	9	<.01	140	4120	98	<5	<20	80	<.01	<10	39	<10	40	449
7	L9N: 15+ 50 E	1.2	1.39	35	70	<5	0.17	<1	11	43	33	5.77	<10	0.23	365	<1	0.02	38	2710	48	<5	<20	12	<.01	<10	38	<10	<1	117
8	L9N: 15+ 75 E	<.2	1.66	65	85	<5	0.34	1	18	60	50	7.29	<10	0.37	513	<1	0.03	65	3820	16	<5	<20	15	<.01	<10	37	<10	<1	152
9	L9N: 16+ 25 E	0.6	1.52	35	150	<5	0.58	<1	17	50	13	5.50	<10	0.39	672	2	0.03	19	1850	32	<5	<20	33	<.01	<10	40	<10	<1	109
10	L9N: 16+ 50 E	<.2	1.69	35	80	<5	0.43	<1	14	42	12	4.66	<10	0.33	579	2	0.03	13	1560	26	<5	<20	31	<.01	<10	51	<10	<1	72
11	L9N: 16+ 75 E	<.2	1.25	20	65	<5	0.04	<1	8	32	13	4.40	<10	0.23	358	<1	0.03	11	1740	16	<5	<20	7	<.01	<10	51	<10	<1	50
12	L9N: 17+ 00 E	<.2	0.95	25	50	<5	0.14	<1	11	30	15	5.03	<10	0.18	711	2	0.04	16	2230	30	<5	<20	9	<.01	<10	36	<10	<1	58
13	L9N: 17+ 25 E	<.2	1.52	30	45	<5	0.11	<1	11	47	20	5.41	<10	0.34	270	<1	0.02	21	2810	22	<5	<20	10	0.01	<10	51	<10	<1	71
14	L9N: 17+ 50 E	<.2	1.51	60	120	<5	0.17	1	31	45	37	8.37	<10	0.21	1453	3	0.01	49	3140	68	<5	<20	13	<.01	<10	44	<10	<1	276
15	L9N: 17+ 75 E	<.2	1.00	25	240	<5	0.18	<1	15	20	23	3.64	<10	0.11	652	2	0.02	20	1490	54	<5	<20	15	<.01	<10	32	<10	<1	108
16	L9N: 18+ 00 E	2.0	1.02	30	175	<5	0.30	1	33	18	41	5.64	<10	0.08	1843	<1	<.01	30	1790	96	<5	<20	12	<.01	<10	22	<10	<1	181
17	L9N: 18+ 25 E	<.2	1.16	60	165	<5	0.07	2	27	36	31	6.99	<10	0.12	1043	3	<.01	40	3100	48	<5	<20	10	<.01	<10	41	<10	<1	255
18	L9N: 18+ 50 E	2.2	1.74	35	290	<5	0.73	17	59	36	76	4.89	<10	0.22	2528	2	<.01	41	4100	58	<5	<20	42	<.01	<10	30	<10	31	1086
19	L9N: 18+ 75 E	<.2	1.20	25	115	<5	0.16	<1	8	19	39	3.03	<10	0.07	126	5	<.01	19	1630	30	<5	<20	13	<.01	<10	49	<10	<1	193
20	L9N: 19+ 00 E	<.2	2.50	35	115	<5	0.08	1	9	44	21	4.49	<10	0.77	307	1	0.03	12	1310	10	<5	<20	7	<.01	<10	48	<10	<1	71
21	L10N 14+ 00 E	<.2	1.43	35	200	<5	0.12	1	10	46	21	5.32	<10	0.28	271	1	0.02	20	1490	32	<5	<20	18	0.01	<10	45	<10	<1	84
22	L10N 14+ 25 E	<.2	1.51	30	155	<5	0.15	<1	24	41	38	4.81	<10	0.49	872	2	0.04	31	1130	16	<5	<20	16	0.02	<10	35	<10	2	92
23	L10N 14+ 50 E	<.2	0.94	45	140	<5	0.12	1	17	16	55	7.18	<10	0.13	618	2	0.02	51	2710	36	<5	<20	39	<.01	<10	22	<10	<1	151
24	L10N 14+ 75 E	<.2	0.76	70	180	<5	0.23	1	19	24	85	7.37	<10	0.07	660	3	0.01	53	4310	134	<5	<20	66	<.01	<10	36	<10	4	250
25	L10N 15+ 00 E	<.2	0.98	75	235	<5	0.45	3	50	16	120	8.00	<10	0.18	1712	3	<.01	100	3360	126	<5	<20	51	<.01	<10	34	<10	18	535
26	L10N 15+ 25 E	<.2	1.50	65	85	<5	0.15	<1	19	54	34	8.12	<10	0.30	515	2	0.03	46	2980	34	<5	<20	14	<.01	<10	58	<10	<1	154
27	L10N 15+ 50 E	1.6	1.03	65	135	<5	1.56	2	37	38	78	6.06	<10	0.37	2455	2	0.01	71	2650	78	<5	<20	74	<.01	<10	27	<10	10	243
28	L10N 15+ 75 E	<.2	1.23	20	70	<5	0.09	<1	7	40	11	3.46	<10	0.26	171	<1	0.03	12	1800	36	<5	<20	12	<.01	<10	46	<10	<1	49

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
29	L10N 16+ 25 E	1.0	1.95	40	150	10	0.88	1	31	43	53	5.65	<10	0.37	2681	3	0.04	33	3390	36	<5	<20	51	0.01	<10	38	<10	33	165
30	L10N 16+ 50 E	0.2	1.35	15	100	<5	0.22	<1	15	33	26	4.71	<10	0.27	762	<1	0.02	20	1530	18	<5	<20	20	<.01	<10	33	<10	<1	86
31	L10N 16+ 75 E	<.2	1.07	35	110	<5	0.12	<1	16	41	22	5.24	<10	0.21	1051	2	0.03	17	1820	34	<5	<20	15	<.01	<10	50	<10	<1	70
32	L10N 17+ 00 E	<.2	1.24	30	95	<5	0.35	<1	17	30	36	4.88	<10	0.29	444	1	0.01	24	1240	46	<5	<20	29	<.01	<10	29	<10	<1	164
33	L10N 17+ 25 E	<.2	1.48	25	115	<5	0.15	<1	16	40	19	5.01	<10	0.28	477	<1	0.03	21	1490	22	<5	<20	15	<.01	<10	40	<10	3	79
34	L10N 17+ 50 E	1.2	1.54	30	90	<5	1.18	<1	21	33	45	4.29	<10	0.42	1185	2	0.02	29	1880	22	<5	<20	65	<.01	<10	26	<10	45	101
35	L10N 17+ 75 E	<.2	1.72	45	125	<5	0.61	1	31	56	34	6.06	<10	0.42	1262	2	0.02	37	2090	36	<5	<20	24	<.01	<10	44	<10	2	179
36	L10N 18+ 00 E	<.2	1.34	40	175	<5	1.38	2	27	43	41	4.93	<10	0.43	1760	2	<.01	41	2330	68	<5	<20	43	<.01	<10	32	<10	8	400
37	L10N 18+ 25 E	1.0	1.90	40	150	<5	0.45	4	37	50	62	7.65	<10	0.42	1830	<1	<.01	50	3130	52	<5	<20	31	<.01	<10	34	<10	26	515
38	L10N 18+ 50 E	<.2	0.93	50	85	<5	0.09	<1	13	35	23	4.49	<10	0.09	227	4	0.01	35	1870	110	<5	<20	17	<.01	<10	42	<10	<1	182
39	L10N 18+ 75 E	<.2	1.93	85	140	<5	0.25	1	24	78	36	7.03	<10	0.40	752	4	<.01	36	1550	66	<5	<20	16	<.01	<10	50	<10	<1	278
40	L10N 19+ 00 E	<.2	3.37	50	170	<5	0.05	1	19	114	23	8.00	<10	1.14	1144	1	0.02	29	1380	10	<5	<20	7	0.01	<10	158	<10	<1	132
41	L11N 14+ 00 E	<.2	1.68	50	175	<5	0.54	1	34	63	77	6.77	<10	0.47	1271	1	0.02	71	2880	32	<5	<20	41	0.01	<10	39	<10	12	231
42	L11N 14+ 25 E	0.2	1.40	55	175	<5	0.27	1	25	38	69	6.48	<10	0.31	865	3	0.01	54	2780	46	<5	<20	47	<.01	<10	36	<10	<1	213
43	L11N 14+ 50 E	<.2	1.41	70	75	<5	0.16	1	22	52	48	8.71	<10	0.25	721	3	0.02	51.	3890	62	<5	<20	16	<.01	<10	49	<10	<1	219
44	L11N 14+ 75 E	<.2	1.08	70	145	<5	0.49	1	37	35	105	6.98	<10	0.25	2260	2	0.02	75	2130	112	<5	<20	39	<.01	<10	32	<10	13	274
45	L11N 15+ 00 E	1.6	1.90	20	180	<5	0.19	1	25	40	34	5.51	<10	0.36	1132	<1	0.02	25	1640	16	<5	<20	19	<.01	<10	36	<10	4	113
46	L11N 15+ 25 E	<.2	1.75	35	130	<5	0.23	<1	25	51	34	6.06	<10	0.46	1005	2	0.03	31	1710	24	<5	<20	20	<.01	<10	45	<10	7	145
47	L11N 15+ 50 E	<.2	1.15	25	135	<5	0.14	<1	10	32	16	4.52	<10	0.24	409	<1	0.02	13	1960	20	<5	<20	19	<.01	<10	39	<10	<1	69
48	L11N 15+ 75 E	<.2	1.58	35	115	<5	1.04	<1	30	45	33	5.87	<10	0.48	1060	2	0.02	31	1440	30	<5	<20	42	<.01	<10	37	<10	2	154
49	L11N 16+ 25 E	<.2	1.69	35	130	<5	0.52	<1	15	32	31	5.41	<10	0.34	287	1	0.02	20	1130	16	<5	<20	29	<.01	<10	31	<10	<1	93
50	L11N 16+ 50 E	<.2	1.32	20	90	<5	0.06	<1	7	37	14	3.91	<10	0.22	137	1	0.03	10	770	12	<5	<20	9	<.01	<10	48	<10	<1	48
51	L11N 16+ 75 E	<.2	1.55	30	100	5	0.16	<1	13	43	24	4.07	<10	0.44	154	2	0.03	22	950	14	<5	<20	13	<.01	<10	37	<10	<1	77
52	L11N 17+ 00 E	0.2	1.69	15	145	<5	0.99	<1	18	35	24	4.22	<10	0.32	861	<1	<.01	17	1370	12	<5	<20	39	<.01	<10	29	<10	<1	92
53	L11N 17+ 25 E	<.2	1.53	40	70	<5	0.08	<1	12	44	18	4.31	<10	0.29	286	4	0.03	16	930	20	<5	<20	11	<.01	<10	53	<10	<1	62
54	L11N 17+ 50 E	<.2	1.28	30	60	<5	0.11	<1	11	38	22	4.53	<10	0.24	517	1	0.02	20	1850	22	<5	<20	12	<.01	<10	53	<10	<1	73
55	L11N 17+ 75 E	<.2	1.65	55	70	<5	0.24	<1	23	65	30	7.44	<10	0.43	825	4	0.03	28	3300	40	<5	<20	21	0.01	<10	53	<10	<1	101
56	L11N 18+ 00 E	<.2	1.38	30	125	<5	0.07	<1	10	45	22	3.70	<10	0.19	149	2	0.02	21	1840	40	<5	<20	12	<.01	<10	64	<10	<1	66
57	L11N 18+ 25 E	<.2	1.34	50	75	<5	0.22	<1	25	75	38	8.10	<10	0.42	756	3	0.03	42	4120	60	<5	<20	21	<.01	<10	59	<10	<1	164
58	L11N 18+ 50 E	<.2	3.68	90	120	<5	0.08	1	31	117	86	9.01	<10	0.68	1391	11	0.02	42	3580	42	<5	<20	12	0.02	<10	85	<10	<1	249
59	L11N 18+ 75 E	1.2	1.84	40	220	<5	0.10	1	16	44	33	6.54	<10	0.16	649	4	0.01	17	6690	72	<5	<20	64	<.01	<10	48	<10	<1	126
60	L11N 19+ 00 E	<.2	5.01	110	85	<5	0.11	<1	50	653	30	12.10	<10	2.48	3560	4	0.01	113	2710	36	<5	<20	9	0.03	<10	247	<10	<1	283
61	L16N 5+ 00 E	<.2	1.32	30	85	<5	0.57	<1	12	40	18	4.86	<10	0.36	457	3	0.02	17	1080	16	<5	<20	27	0.01	<10	37	<10	<1	85
62	L16N 5+ 25 E	<.2	1.76	45	115	<5	0.29	<1	27	46	35	6.19	<10	0.38	1195	3	0.02	25	1280	26	<5	<20	20	0.01	<10	41	<10	4	101
63	L16N 5+ 50 E	<.2	1.46	40	135	<5	1.70	<1	22	33	32	4.96	<10	0.34	1458	4	0.02	25	1450	22	<5	<20	58	0.01	<10	34	<10	<1	96
64	L16N 5+ 75 E	<.2	1.57	40	145	<5	1.45	<1	25	40	27	5.52	<10	0.42	1584	4	0.02	25	1320	24	<5	<20	50	0.01	<10	33	<10	2	99
65	L16N 6+ 00 E	<.2	1.90	60	140	<5	0.78	<1	28	43	34	6.53	<10	0.35	1877	5	0.03	32	1120	26	<5	<20	31	<.01	<10	40	<10	3	96
66	L16N 6+ 25 E	0.6	2.07	50	135	<5	0.71	<1	25	40	35	6.50	<10	0.35	1158	2	0.02	29	1090	18	<5	<20	30	<.01	<10	30	<10	<1	95
67	L16N 6+ 50 E	<.2	1.35	40	85	<5	0.19	<1	13	40	21	5.35	<10	0.23	437	5	0.03	18	1270	22	<5	<20	11	0.01	<10	51	<10	<1	68

TOKLAT RESOURCES INC. ETK 94-455

ECO-TECH LABORATORIES LTD.

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
68	L16N 6+ 75 E	<.2	1.67	30	135	5	0.89	<1	21	41	27	4.72	<10	0.47	1039	2	0.02	25	1050	14	<5	<20	35	<.01	<10	33	<10	1	82
69	L16N 7+ 00 E	<.2	1.66	35	125	<5	0.87	<1	29	57	22	5.69	<10	0.48	1035	2	0.03	26	1270	20	<5	<20	37	0.01	<10	40	<10	6	102
70	L16N 7+ 25 E	<.2	1.42	25	115	<5	1.54	<1	19	44	24	4.00	<10	0.50	782	2	0.02	25	1230	16	<5	<20	50	0.01	<10	31	<10	5	86
71	L16N 7+ 50 E	<.2	1.41	40	115	<5	0.11	<1	13	54	19	5.01	<10	0.27	385	4	0.03	16	900	24	<5	<20	11	0.01	<10	70	<10	<1	67
72	L16N 7+ 75 E	<.2	1.42	35	110	<5	0.19	<1	18	47	30	4.42	<10	0.42	884	2	0.02	27	1120	16	<5	<20	12	0.02	<10	44	<10	<1	91
73	L16N 8+ 00 E	1.0	1.19	30	80	<5	0.28	<1	8	44	11	4.23	<10	0.26	235	3	0.02	11	1530	18	<5	<20	12	0.01	<10	57	<10	<1	55
74	L16N 8+ 25 E	<.2	1.45	35	205	<5	0.20	<1	12	70	16	5.75	<10	0.33	485	4	0.03	17	2110	22	<5	<20	15	0.01	<10	75	<10	<1	79
75	L16N 8+ 50 E	<.2	2.08	45	175	<5	0.21	<1	18	71	25	6.10	<10	0.45	512	5	0.03	25	1040	24	<5	<20	18	0.01	<10	61	<10	<1	94
76	L16N 8+ 75 E	<.2	2.13	30	105	<5	0.12	<1	24	89	21	4.68	<10	0.73	199	2	0.03	30	620	16	<5	<20	9	0.01	<10	51	<10	2	76
77	L16N 9+ 00 E	<.2	3.11	50	110	<5	[illegible]	1	18	99	20	7.18	<10	1.01	328	2	0.03	24	2130	6	<5	<20	7	0.01	<10	113	<10	<1	88
78	L16N 9+ 25 E	<.2	1.73	20	50	<5	0.04	<1	7	30	10	3.64	<10	0.34	157	<1	0.02	11	870	4	<5	<20	6	0.01	<10	45	<10	<1	45
79	L16N 9+ 50 E	<.2	2.16	35	85	<5	0.08	<1	15	52	19	5.15	<10	0.43	499	1	0.02	20	1630	10	<5	<20	7	0.01	<10	48	<10	<1	106
80	L16N 9+ 75 E	<.2	2.35	30	70	<5	0.09	<1	9	58	12	4.81	<10	0.50	271	1	0.02	13	1230	6	<5	<20	8	0.02	<10	54	<10	<1	81
81	L16N 10+ 25 E	2.2	1.38	20	175	<5	0.76	<1	14	41	14	3.79	<10	0.33	1898	1	0.02	14	940	12	5	<20	29	<.01	<10	48	<10	<1	68
82	L16N 10+ 50 E	<.2	1.51	35	75	<5	0.26	<1	16	37	22	4.83	<10	0.41	558	2	0.03	20	1240	14	<5	<20	16	0.02	<10	39	<10	<1	68
83	L16N 10+ 75 E	0.2	2.68	40	85	<5	0.10	<1	18	48	28	5.59	<10	0.57	460	1	0.02	27	1290	6	<5	<20	10	<.01	<10	40	<10	<1	105
84	L16N 11+ 00 E	<.2	1.70	35	140	<5	0.05	<1	13	50	16	4.51	<10	0.34	465	2	0.03	20	1140	14	<5	<20	8	0.01	<10	66	<10	<1	80
85	L16N 11+ 25 E	<.2	1.72	35	80	<5	1.12	<1	20	32	25	4.37	<10	0.47	775	2	0.02	26	1310	14	<5	<20	46	0.01	<10	30	<10	<1	90
86	L16N 11+ 50 E	0.8	0.13	<5	35	<5	6.72	<1	2	6	12	0.25	<10	0.27	931	<1	<.01	6	840	<2	<5	<20	166	<.01	<10	5	<10	2	82
87	L16N 11+ 75 E	<.2	1.49	20	40	<5	0.09	1	6	24	10	3.30	<10	0.29	115	<1	0.01	10	1000	4	<5	<20	8	0.01	<10	32	<10	<1	38
88	L16N 12+ 00 E	1.4	2.12	50	70	<5	0.26	<1	16	60	20	8.24	<10	0.43	387	2	0.03	26	2780	22	<5	<20	15	<.01	<10	52	<10	<1	98
89	L16N 12+ 25 E	0.4	1.42	30	45	<5	0.08	<1	5	38	4	4.77	<10	0.23	164	2	0.03	7	2010	16	<5	<20	8	0.02	<10	85	<10	<1	32
90	L16N 12+ 50 E	<.2	2.00	55	85	<5	0.06	<1	15	80	32	8.14	<10	0.51	659	3	0.03	30	3840	22	<5	<20	12	0.02	<10	86	<10	<1	113
91	L16N 12+ 75 E	0.4	1.19	45	80	<5	0.10	<1	12	43	16	5.19	<10	0.19	401	3	0.03	24	2470	20	<5	<20	12	0.01	<10	72	<10	<1	58
92	L16N 13+ 00 E	<.2	0.51	30	90	<5	0.16	<1	7	15	69	3.52	<10	0.04	116	15	<.01	27	1420	96	<5	<20	39	<.01	<10	150	<10	1	174
93	L16N 13+ 25 E	0.8	3.35	120	75	<5	0.09	1	27	333	40	12.20	<10	1.43	740	5	0.03	69	3360	10	<5	<20	7	0.02	<10	161	<10	<1	144
94	L16N 13+ 50 E	<.2	1.76	70	55	<5	0.07	<1	16	63	36	8.17	<10	0.37	697	4	0.03	29	1530	12	<5	<20	12	0.01	<10	76	<10	<1	76
95	L16N 13+ 75 E	7.0	1.97	35	110	<5	2.38	5	23	58	48	5.11	<10	0.65	3082	3	0.04	39	2510	10	<5	<20	73	0.01	<10	42	<10	49	108
96	L16N 14+ 00 E	5.0	1.97	45	135	<5	1.70	3	27	63	22	4.69	<10	0.45	2567	4	0.01	25	1730	34	<5	<20	66	0.01	<10	87	<10	29	199
97	L16N 14+ 25 E	<.2	1.07	5	95	<5	0.11	<1	5	23	16	3.20	<10	0.17	120	<1	0.02	12	1220	<2	<5	<20	8	<.01	<10	53	<10	<1	55
98	L16N 14+ 50 E	0.6	1.02	25	75	<5	0.04	<1	5	24	8	4.87	<10	0.08	160	1	0.03	7	1420	10	<5	<20	5	0.02	<10	39	<10	<1	42
99	L16N 14+ 75 E	0.2	0.96	<5	30	<5	0.13	<1	2	13	2	0.73	<10	0.06	131	<1	0.01	2	480	<2	<5	<20	4	<.01	<10	22	<10	<1	15
100	L16N 15+ 00 E	<.2	0.71	15	25	<5	0.06	<1	4	13	6	2.39	<10	0.05	149	<1	0.02	5	900	6	<5	<20	4	<.01	<10	41	<10	<1	22
101	L17N 5+ 00 E	<.2	0.91	25	190	<5	0.38	<1	10	26	18	4.43	<10	0.19	731	3	0.02	11	850	14	<5	<20	16	<.01	<10	36	<10	<1	67
102	L17N 5+ 25 E	<.2	1.74	45	115	<5	1.30	<1	29	48	28	6.72	<10	0.33	1577	4	0.02	28	1370	26	<5	<20	39	0.01	<10	46	<10	4	95
103	L17N 5+ 50 E	<.2	1.25	55	100	5	0.10	<1	16	49	18	6.47	<10	0.25	375	6	0.03	18	1100	30	<5	<20	9	0.01	<10	54	<10	<1	63
104	L17N 5+ 75 E	0.8	1.90	30	120	<5	0.99	<1	26	40	44	5.97	<10	0.29	1674	2	0.03	27	1540	14	<5	<20	32	<.01	<10	36	<10	32	88
105	L17N 6+ 00 E	<.2	1.31	40	105	<5	0.54	<1	12	39	12	5.20	<10	0.36	389	3	0.03	14	1240	18	<5	<20	24	0.01	<10	51	<10	<1	74
106	L17N 6+ 25 E	<.2	1.26	20	85	<5	1.11	<1	11	29	11	3.66	<10	0.32	333	2	0.02	11	810	10	<5	<20	42	<.01	<10	35	<10	<1	57

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
107	L17N 6+ 50 E	<.2	1.44	35	100	<5	0.26	<1	18	44	16	5.86	<10	0.33	1085	3	0.03	18	920	22	<5	<20	13	0.01	<10	48	<10	<1	65
108	L17N 6+ 75 E	<.2	1.00	20	75	<5	0.32	<1	6	23	8	3.47	<10	0.17	157	2	0.02	8	700	8	<5	<20	17	<.01	<10	38	<10	<1	35
109	L17N 7+ 00 E	<.2	1.49	25	125	<5	1.73	<1	18	40	12	4.74	<10	0.29	1157	3	0.02	14	1390	14	<5	<20	46	0.01	<10	50	<10	<1	73
110	L17N 7+ 25 E	<.2	1.75	40	125	<5	2.90	<1	20	62	16	4.67	<10	0.32	575	5	0.02	20	1360	22	<5	<20	71	0.02	<10	53	<10	5	90
111	L17N 7+ 50 E	1.2	1.25	25	75	<5	0.37	<1	14	49	15	5.16	<10	0.28	394	<1	0.01	17	730	12	<5	<20	14	0.02	<10	62	<10	<1	81
112	L17N 7+ 75 E	<.2	1.02	5	40	<5	0.05	<1	4	29	6	1.89	<10	0.15	105	<1	0.01	6	490	4	<5	<20	5	0.02	<10	60	<10	<1	35
113	L17N 8+ 00 E	<.2	0.87	15	55	<5	0.09	<1	5	20	9	1.74	<10	0.11	142	1	0.02	8	360	6	<5	<20	7	0.01	<10	50	<10	<1	41
114	L17N 8+ 25 E	<.2	1.20	35	60	<5	0.27	<1	15	46	24	5.23	<10	0.40	415	2	0.02	25	1560	20	<5	<20	14	0.04	<10	64	<10	<1	94
115	L17N 8+ 50 E	0.6	1.15	10	45	<5	0.05	<1	10	22	<1	4.07	<10	0.27	393	<1	0.01	12	1300	14	<5	<20	5	<.01	<10	30	<10	<1	52
116	L17N 8+ 75 E	<.2	1.95	15	200	<5	0.33	5	17	42	8	6.67	<10	0.25	3697	2	<.01	29	1250	96	<5	<20	11	0.01	<10	37	<10	33	821
117	L17N 9+ 00 E	<.2	2.82	30	155	<5	0.36	<1	31	89	11	8.45	<10	0.86	989	<1	<.01	44	1990	22	<5	<20	11	0.01	<10	70	<10	2	193
118	L17N 9+ 25 E	<.2	2.17	15	70	<5	1.05	<1	21	45	<1	5.53	<10	0.49	520	<1	<.01	20	1230	22	<5	<20	40	0.01	<10	44	<10	5	85
119	L17N 9+ 50 E	1.2	0.74	10	65	<5	3.38	1	6	22	<1	1.71	<10	0.20	138	1	0.01	9	720	14	<5	<20	102	<.01	<10	24	<10	3	44
120	L17N 9+ 75 E	0.6	2.72	20	70	<5	0.95	<1	15	62	<1	6.98	<10	0.87	377	<1	<.01	21	750	22	<5	<20	34	<.01	<10	49	<10	<1	91
121	L17N 10+ 25 E	< 2	1.59	10	55	<5	0.12	<1	10	37	<1	5.65	<10	0.52	413	<1	0.02	12	2920	24	<5	<20	8	0.01	<10	40	<10	<1	55
122	L17N 10+ 50 E	1.0	1.41	10	100	<5	0.54	<1	11	31	<1	4.35	<10	0.40	445	<1	0.02	14	1470	20	<5	<20	22	<.01	<10	35	<10	<1	49
123	L17N 10+ 75 E	< 2	1.28	20	85	<5	1.14	1	22	47	20	6.73	<10	0.30	1512	<1	<.01	24	1980	36	<5	<20	43	0.01	<10	46	<10	2	80
124	L17N 11+ 00 E	0.2	1.68	15	90	<5	2.17	<1	26	34	9	4.82	<10	0.35	1073	<1	<.01	18	1830	24	<5	<20	76	0.01	<10	33	<10	6	61
125	L17N 11+ 25 E	1.0	0.32	<5	35	<5	0.12	<1	11	6	7	2.86	<10	0.02	107	<1	0.04	13	410	10	<5	<20	7	<.01	<10	17	<10	1	37
126	L17N 11+ 50 E	<.2	1.33	10	40	<5	0.05	<1	14	30	<1	7.59	<10	0.33	586	<1	<.01	15	2420	18	<5	<20	5	<.01	<10	27	<10	<1	60
127	L17N 11+ 75 E	<.2	0.88	35	95	5	0.54	<1	37	25	6	12.70	<10	0.12	3249	<1	<.01	46	4100	30	<5	<20	15	0.01	<10	31	<10	<1	108
128	L17N 12+ 00 E	<.2	0.77	35	95	10	0.07	<1	25	25	25	9.40	<10	0.07	648	6	<.01	70	3780	26	<5	<20	9	<.01	<10	33	<10	<1	118
129	L17N 12+ 25 E	1.0	0.93	40	135	<5	0.21	1	12	22	53	8.06	<10	0.09	481	15	<.01	21	4920	116	<5	<20	35	<.01	<10	54	<10	4	151
130	L17N 12+ 50 E	<.2	1.84	30	70	<5	0.16	<1	30	58	11	8.17	<10	0.47	1604	2	<.01	26	2330	24	<5	<20	12	0.01	<10	56	<10	<1	110
131	L17N 12+ 75 E	<.2	1.67	30	45	<5	0.06	<1	15	37	7	6.55	<10	0.64	594	2	0.01	26	2070	12	<5	<20	7	0.01	<10	75	<10	<1	80
132	L17N 13+ 00 E	< 2	2.79	50	60	10	0.12	<1	23	118	16	7.60	<10	1.11	731	2	<.01	41	1260	20	<5	<20	10	0.01	<10	73	<10	1	118
133	L17N 13+ 25 E	0.2	1.18	15	55	<5	0.04	<1	9	24	3	4.40	<10	0.33	413	<1	0.02	15	1540	18	<5	<20	6	<.01	<10	34	<10	<1	57
134	L17N 13+ 50 E	2.0	2.16	15	80	<5	1.56	2	28	42	20	5.32	<10	0.98	3061	<1	0.03	28	2340	28	<5	<20	66	0.01	<10	31	<10	28	154
135	L17N 13+ 75 E	2.0	2.16	20	60	<5	1.24	3	26	36	46	5.02	<10	0.77	2532	1	0.06	37	2370	22	<5	<20	61	<.01	<10	25	<10	95	120
136	L17N 14+ 00 E	1.0	1.77	20	90	<5	1.26	2	35	34	25	6.12	<10	0.38	2010	<1	0.02	39	2140	42	<5	<20	74	<.01	<10	29	<10	48	152
137	L17N 14+ 25 E	1.2	0.60	10	40	<5	0.27	<1	8	11	<1	2.56	<10	0.08	245	<1	0.03	11	680	14	<5	<20	9	<.01	<10	29	<10	2	44
138	L17N 14+ 50 E	2.6	1.27	<5	45	<5	0.06	<1	3	8	<1	1.48	<10	0.07	132	<1	0.02	3	720	6	<5	<20	6	<.01	<10	14	<10	1	18
139	L17N 14+ 75 E	0.4	1.52	10	30	<5	0.14	<1	12	21	<1	4.57	<10	0.25	525	<1	0.05	11	2270	24	<5	<20	14	0.01	<10	35	<10	3	40
140	L17N 15+ 00 E	0.2	1.66	5	40	<5	0.04	<1	8	22	<1	4.62	<10	0.21	346	<1	0.02	7	1210	8	<5	<20	6	<.01	<10	28	<10	<1	30
141	L18N 5+ 00 E	0.8	0.84	10	65	<5	0.07	<1	8	23	<1	3.27	<10	0.23	207	<1	0.02	12	1000	16	<5	<20	7	<.01	<10	30	<10	<1	38
142	L18N 5+ 25 E	0.2	1.16	20	70	<5	0.06	<1	12	27	3	4.94	<10	0.27	437	1	0.01	15	890	22	<5	<20	6	<.01	<10	29	<10	<1	53
143	L18N 5+ 50 E	0.2	1.51	15	100	<5	0.08	<1	10	33	<1	5.54	<10	0.47	249	<1	0.01	13	1780	24	<5	<20	8	<.01	<10	29	<10	<1	46
144	L18N 5+ 75 E	0.6	0.86	15	45	<5	0.16	<1	10	22	2	3.87	<10	0.28	409	<1	0.02	14	1190	24	<5	<20	8	<.01	<10	27	<10	<1	49
145	L18N 6+ 00 E	0.4	1.25	10	70	<5	0.16	<1	10	44	<1	4.59	<10	0.52	351	<1	0.01	15	1190	24	<5	<20	8	0.01	<10	40	<10	<1	54

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
146	L18N 6+ 25 E	0.2	1.40	20	60	5	0.07	<1	10	38	<1	4.44	<10	0.49	249	2	0.02	14	1500	26	<5	<20	7	<.01	<10	37	<10	<1	49
147	L18N 6+ 50 E	1.8	1.25	10	70	<5	0.10	<1	8	36	<1	4.15	<10	0.35	311	2	0.01	11	1560	92	<5	<20	9	<.01	<10	34	<10	<1	54
148	L18N 6+ 75 E	1.0	1.92	10	120	<5	1.27	<1	23	57	8	4.71	<10	0.63	1830	1	0.01	22	1230	24	<5	<20	43	0.01	<10	33	<10	10	88
149	L18N 7+ 00 E	0.4	1.94	10	115	<5	1.63	<1	20	53	3	4.81	<10	0.52	1193	<1	0.01	18	1250	16	<5	<20	42	0.01	<10	38	<10	5	74
150	L18N 7+ 25 E	<.2	2.04	15	70	5	0.21	<1	14	113	<1	6.51	<10	1.36	397	<1	<.01	24	3030	28	<5	<20	10	0.02	<10	100	<10	<1	79
151	L18N 7+ 50 E	1.4	0.89	<5	60	<5	0.07	<1	3	18	<1	1.35	<10	0.15	75	<1	0.02	5	470	38	<5	<20	6	<.01	<10	23	<10	1	78
152	L18N 7+ 75 E	0.6	1.17	10	65	<5	0.25	<1	10	27	<1	4.31	<10	0.33	446	<1	0.02	14	1200	20	<5	<20	10	0.01	<10	40	<10	<1	65
153	L18N 8+ 00 E	1.2	0.74	<5	100	<5	0.06	<1	3	13	6	1.42	<10	0.15	95	<1	0.02	5	660	8	<5	<20	7	<.01	<10	20	<10	1	25
154	L18N 8+ 25 E	<.2	1.27	<5	60	<5	0.05	<1	7	23	8	3.36	<10	0.31	352	<1	0.01	9	780	14	<5	<20	7	0.01	<10	30	<10	<1	47
155	L18N 8+ 50 E	0.2	1.01	<5	195	<5	0.18	<1	11	22	12	3.03	<10	0.25	1290	<1	0.01	11	900	12	<5	<20	17	<.01	<10	33	<10	<1	64
156	L18N 8+ 75 E	0.4	1.55	10	110	<5	1.61	<1	17	34	30	3.33	<10	0.42	1504	<1	0.01	21	1320	22	<5	<20	75	0.01	<10	28	<10	10	63
157	L18N 9+ 00 E	<.2	2.19	10	105	<5	1.00	<1	15	39	18	3.53	<10	0.61	418	<1	0.01	17	820	10	<5	<20	54	<.01	<10	38	<10	7	50
158	L18N 9+ 25 E	1.0	0.99	<5	70	<5	0.05	<1	3	13	5	1.27	<10	0.12	86	<1	0.02	5	310	2	<5	<20	6	<.01	<10	29	<10	1	19
159	L18N 9+ 50 E	<.2	1.41	5	85	<5	0.04	<1	9	22	10	3.64	<10	0.39	593	<1	0.02	10	1940	12	<5	<20	8	0.01	<10	29	<10	<1	39
160	L18N 9+ 75 E	0.6	0.98	<5	90	<5	0.02	<1	6	14	9	2.19	<10	0.22	287	<1	0.03	6	490	10	<5	<20	6	0.01	<10	25	<10	1	29
161	L18N 10+ 25 E	<.2	1.41	10	70	<5	0.03	<1	8	23	11	3.52	<10	0.38	191	<1	0.02	11	680	14	<5	<20	7	<.01	<10	27	<10	<1	39
162	L18N 10+ 50 E	<.2	1.39	5	130	<5	0.05	<1	9	22	12	3.10	<10	0.30	388	<1	0.02	10	720	10	<5	<20	9	<.01	<10	29	<10	<1	46
163	L18N 10+ 75 E	0.4	1.67	<5	165	<5	1.07	<1	16	22	17	3.21	<10	0.48	2609	<1	0.02	18	1120	10	<5	<20	56	0.01	<10	21	<10	8	61
164	L18N 11+ 00 E	<.2	1.74	5	110	<5	0.08	<1	9	24	12	3.62	<10	0.39	322	<1	0.01	10	950	10	<5	<20	12	<.01	<10	29	<10	<1	55
165	L18N 11+ 25 E	0.8	1.04	<5	45	<5	0.05	<1	3	13	3	1.45	<10	0.17	64	<1	0.03	4	420	6	<5	<20	7	<.01	<10	25	<10	1	25
166	L18N 11+ 50 E	0.6	1.44	10	70	<5	0.25	<1	8	28	11	3.19	<10	0.34	104	<1	<.01	13	840	38	<5	<20	17	<.01	<10	32	<10	<1	56
167	L18N 11+ 75 E	<.2	0.58	<5	115	<5	0.11	<1	10	7	20	4.10	<10	0.04	193	4	0.01	29	1310	30	<5	<20	13	<.01	<10	17	<10	1	110
168	L18N 12+ 00 E	<.2	0.54	15	80	<5	0.04	<1	13	9	41	4.81	<10	0.03	164	8	0.01	43	1640	36	<5	<20	10	<.01	<10	37	<10	<1	181
169	L18N 12+ 25 E	0.6	0.41	15	100	<5	0.08	<1	14	1	219	4.23	<10	0.03	178	4	<.01	29	1640	68	<5	<20	22	<.01	<10	23	<10	8	151
170	L18N 12+ 50 E	<.2	0.40	10	65	5	0.16	<1	17	4	128	6.95	<10	0.08	736	6	<.01	28	1720	22	<5	<20	14	<.01	<10	63	<10	3	151
171	L18N 12+ 75 E	2.2	0.96	5	60	<5	0.02	<1	4	15	15	1.89	<10	0.17	62	<1	0.01	7	830	6	<5	<20	5	<.01	<10	27	<10	<1	29
172	L18N 13+ 00 E	0.4	0.96	10	45	<5	0.03	<1	7	15	20	3.88	<10	0.17	164	1	0.01	14	1250	16	<5	<20	5	<.01	<10	34	<10	<1	45
173	L18N 13+ 25 E	<.2	0.99	5	75	<5	0.07	<1	9	18	105	4.55	<10	0.19	205	2	0.02	18	1670	22	<5	<20	10	0.01	<10	49	<10	1	92
174	L18N 13+ 50 E	1.0	0.48	5	75	<5	0.18	<1	8	10	144	2.64	<10	0.07	134	<1	0.03	18	680	16	<5	<20	18	<.01	<10	26	<10	4	97
175	L18N 13+ 75 E	1.8	0.58	<5	115	<5	0.10	<1	2	6	73	0.98	<10	0.04	25	<1	0.02	5	480	14	<5	<20	22	<.01	<10	13	<10	2	35
176	L18N 14+ 00 E	<.2	1.58	65	65	<5	[illegible]	<1	25	64	65	7.39	<10	0.57	1225	<1	<.01	57	1940	34	<5	<20	12	<.01	<10	39	<10	<1	101
177	L18N 14+ 25 E	0.4	1.02	10	55	<5	0.05	<1	6	10	20	2.13	<10	0.09	251	<1	0.03	8	890	16	<5	<20	6	<.01	<10	30	<10	2	32
178	L18N 14+ 50 E	1.0	0.78	<5	30	<5	0.14	<1	4	3	66	1.41	<10	0.04	117	<1	0.02	5	490	2	<5	<20	7	<.01	<10	21	<10	1	34
179	L18N 14+ 75 E	1.2	1.05	<5	40	<5	0.02	<1	2	6	10	0.74	<10	0.05	25	<1	0.02	3	400	4	<5	<20	5	<.01	<10	20	<10	2	16
180	L18N 15+ 00 E	<.2	1.16	<5	50	<5	0.03	<1	12	16	73	4.24	<10	0.25	538	<1	0.01	11	1220	20	<5	<20	5	0.03	<10	27	<10	1	61
181	L19N 5+ 00 E	<.2	2.13	15	110	<5	0.54	<1	22	31	27	4.50	<10	0.45	1230	<1	0.01	23	900	22	<5	<20	27	0.01	<10	27	<10	9	69
182	L19N 5+ 25 E	1.0	0.67	<5	220	<5	0.25	<1	8	14	18	1.99	<10	0.15	998	<1	0.02	6	810	12	<5	<20	12	<.01	<10	26	<10	1	40
183	L19N 5+ 50 E	0.4	1.03	<5	80	<5	0.07	<1	7	20	20	3.09	<10	0.25	310	<1	0.01	8	830	14	<5	<20	7	<.01	<10	27	<10	<1	38
184	L19N 5+ 75 E	<.2	1.17	5	85	<5	0.04	<1	9	24	31	4.10	<10	0.26	367	<1	0.01	10	630	14	<5	<20	5	0.01	<10	33	<10	<1	47

TOKLAT RESOURCES INC. ETK 94-455 | ECO-TECH LABORATORIES LTD.

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
185	L19N 6+ 00 E	0.4	0.81	5	50	<5	0.08	<1	7	18	17	2.89	<10	0.25	269	<1	0.01	9	1280	14	<5	<20	6	<.01	<10	26	<10	<1	35
186	L19N 6+ 25 E	0.6	0.65	15	60	<5	0.03	<1	8	19	18	2.86	<10	0.22	195	1	0.01	13	1190	12	<5	<20	4	<.01	<10	23	<10	<1	33
187	L19N 6+ 50 E	<.2	1.09	5	70	<5	0.06	<1	10	25	23	4.54	<10	0.36	295	<1	<.01	15	1810	16	<5	<20	7	<.01	<10	23	<10	<1	51
188	L19N 6+ 75 E	<.2	0.94	10	75	<5	0.11	<1	8	21	19	3.51	<10	0.26	329	<1	0.01	11	1150	20	<5	<20	9	<.01	<10	32	<10	<1	41
189	L19N 7+ 00 E	0.4	1.16	5	150	<5	0.11	<1	9	20	40	3.54	<10	0.33	679	<1	0.02	11	1720	16	<5	<20	10	<.01	<10	25	<10	1	55
190	L19N 7+ 25 E	<.2	1.51	10	85	<5	0.32	<1	15	27	20	4.34	<10	0.48	757	<1	0.01	14	1370	18	<5	<20	16	0.01	<10	29	<10	<1	109
191	L19N 7+ 50 E	<.2	1.46	<5	75	<5	0.20	<1	16	22	50	3.47	<10	0.41	463	<1	0.02	15	890	14	<5	<20	19	0.01	<10	23	<10	6	56
192	L19N 7+ 75 E	<.2	1.11	<5	45	<5	0.54	<1	6	19	136	2.39	<10	0.21	127	1	<.01	7	650	10	<5	<20	29	<.01	<10	19	<10	2	60
193	L19N 8+ 00 E	1.6	0.47	<5	80	<5	2.01	<1	6	10	36	0.98	<10	0.17	545	<1	<.01	7	510	6	<5	<20	91	<.01	<10	8	<10	4	44
194	L19N 8+ 25 E	<.2	1.90	15	100	<5	0.22	<1	18	52	37	4.21	<10	0.85	375	<1	0.01	31	970	20	<5	<20	16	0.01	<10	43	<10	4	82
195	L19N 8+ 50 E	<.2	2.53	20	90	<5	0.12	<1	16	55	36	5.15	<10	0.89	326	<1	<.01	29	840	44	<5	<20	10	<.01	<10	46	<10	<1	347
196	L19N 8+ 75 E	<.2	0.84	5	35	<5	0.09	<1	9	17	45	3.71	<10	0.19	237	<1	0.01	11	1140	14	<5	<20	6	0.03	<10	41	<10	<1	47
197	L19N 9+ 00 E	0.2	0.77	15	45	<5	0.07	<1	9	9	114	3.70	<10	0.09	353	3	<.01	19	1110	20	<5	<20	9	0.01	<10	36	<10	<1	63
198	L19N 9+ 25 E	<.2	1.78	10	680	10	1.07	2	38	21	48	12.50	<10	0.20	4498	<1	<.01	30	3360	16	<5	<20	24	0.02	<10	66	<10	23	95
199	L19N 9+ 50 E	<.2	2.07	35	120	<5	0.32	<1	43	31	33	6.03	<10	0.33	1067	2	0.01	56	1590	20	<5	<20	9	<.01	<10	35	<10	15	77
200	L19N 9+ 75 E	0.6	1.07	<5	65	<5	0.10	<1	10	18	15	2.95	<10	0.19	266	<1	0.02	18	740	6	<5	<20	5	<.01	<10	41	<10	<1	35
201	L19N 10+ 25 E	<.2	1.05	40	70	<5	0.28	<1	24	23	38	6.05	<10	0.26	448	4	<.01	68	2070	26	<5	<20	13	<.01	<10	22	<10	2	71
202	L19N 10+ 50 E	0.2	1.40	10	45	<5	0.03	<1	8	21	12	3.60	<10	0.32	163	<1	0.02	10	1110	10	<5	<20	5	0.01	<10	32	<10	<1	34
203	L19N 10+ 75 E	0.8	0.89	<5	50	<5	0.08	<1	6	13	10	2.10	<10	0.19	264	<1	0.02	7	770	8	<5	<20	7	<.01	<10	23	<10	<1	25
204	L19N 11+ 00 E	0.4	1.30	5	55	<5	0.03	<1	7	17	9	2.78	<10	0.32	147	<1	0.02	7	610	6	<5	<20	5	<.01	<10	25	<10	<1	31
205	L19N 11+ 25 E	0.4	1.33	5	55	<5	0.04	<1	7	20	16	3.11	<10	0.36	208	<1	0.02	8	920	10	<5	<20	6	0.01	<10	30	<10	<1	36
206	L19N 11+ 50 E	<.2	1.60	15	50	<5	0.05	1	8	24	10	4.57	<10	0.38	228	<1	0.01	10	1240	14	<5	<20	7	0.01	<10	34	<10	<1	43
207	L19N 11+ 75 E	1.0	0.49	10	100	<5	0.06	<1	5	3	97	2.93	<10	0.03	546	3	<.01	12	1010	28	<5	<20	11	<.01	<10	17	<10	<1	79
208	L19N 12+ 00 E	<.2	2.59	25	300	<5	0.50	<1	28	<1	20	8.64	<10	0.95	2216	<1	<.01	4	3470	<2	<5	<20	29	<.01	<10	32	<10	3	173
209	L19N 12+ 25 E	<.2	2.87	30	205	5	0.65	1	40	<1	37	9.53	<10	1.05	2173	1	<.01	6	2430	<2	<5	<20	33	<.01	<10	27	<10	9	96
210	L19N 12+ 50 E	<.2	1.50	5	95	5	0.10	<1	47	4	52	10.00	<10	0.65	547	2	<.01	35	3220	6	<5	<20	9	0.01	<10	44	<10	<1	119
211	L19N 12+ 75 E	1.4	1.22	20	55	<5	0.05	<1	12	18	127	4.82	<10	0.19	210	5	<.01	27	2360	24	<5	<20	10	<.01	<10	40	<10	4	76
212	L19N 13+ 00 E	0.2	1.47	15	55	<5	0.07	<1	8	21	23	4.43	<10	0.44	184	1	0.03	21	2800	14	<5	<20	6	<.01	<10	43	<10	2	104
213	L19N 13+ 25 E	0.8	0.97	10	70	<5	0.06	<1	8	14	31	3.61	<10	0.14	116	3	0.02	17	1540	22	<5	<20	11	0.02	<10	53	<10	2	67
214	L19N 13+ 50 E	<.2	1.21	15	60	<5	0.02	<1	7	27	19	5.67	<10	0.12	98	2	<.01	14	2310	24	<5	<20	6	0.02	<10	87	<10	<1	50
215	L19N 13+ 75 E	<.2	0.67	5	85	<5	0.05	<1	11	11	46	4.97	<10	0.10	814	3	<.01	21	2110	28	<5	<20	26	<.01	<10	42	<10	1	89
216	L19N 14+ 00 E	0.2	1.09	<5	65	<5	0.05	<1	8	15	15	3.96	<10	0.15	262	<1	0.01	11	1310	10	<5	<20	8	0.01	<10	34	<10	<1	46
217	L19N 14+ 25 E	0.2	0.91	5	105	<5	0.22	1	9	10	20	3.57	<10	0.14	311	<1	0.03	13	1150	22	<5	<20	16	<.01	<10	23	<10	4	47
218	L19N 14+ 50 E	1.0	0.78	5	95	<5	0.16	<1	9	9	12	2.31	<10	0.10	294	<1	0.03	8	900	14	<5	<20	11	<.01	<10	25	<10	3	37
219	L19N 14+ 75 E	0.8	0.93	<5	175	<5	0.18	<1	10	11	14	2.18	<10	0.13	1213	<1	0.02	7	630	20	<5	<20	11	0.02	<10	31	<10	2	43
220	L19N 15+ 00 E	1.8	1.00	<5	250	<5	0.13	<1	14	10	18	2.03	<10	0.13	3120	<1	<.01	7	820	20	<5	<20	13	0.01	<10	24	<10	5	43
221	L11N 10+ 25 E	0.2	1.08	10	115	<5	0.47	<1	12	18	16	3.75	<10	0.24	521	1	<.01	14	1150	20	<5	<20	22	<.01	<10	26	<10	1	64
222	L11N 10+ 50 E	<.2	1.27	5	160	<5	0.45	<1	13	19	21	3.44	<10	0.35	759	<1	0.02	16	1070	12	<5	<20	22	<.01	<10	21	<10	7	84
223	L11N 10+ 75 E	<.2	1.39	10	50	<5	0.21	<1	13	22	22	4.05	<10	0.46	313	<1	0.02	20	1490	14	<5	<20	15	<.01	<10	21	<10	3	72

TOKLAT RESOURCES INC. ETK 94-455 ECO-TECH LABORATORIES LTD.

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
224	L11N 11+ 00 E	<.2	1.87	20	90	<5	0.15	<1	15	30	21	4.04	<10	0.44	382	<1	0.02	23	1590	18	<5	<20	13	<.01	<10	28	<10	5	105
225	L11N 11+ 25 E	0.2	0.69	15	60	<5	0.06	<1	9	28	19	3.58	<10	0.17	305	<1	0.01	29	2030	26	<5	<20	10	<.01	<10	39	<10	<1	100
226	L11N 11+ 50 E	<.2	1.96	20	100	<5	0.25	<1	20	74	27	5.94	<10	0.46	940	1	<.01	45	2530	26	<5	<20	15	<.01	<10	55	<10	7	165
227	L11N 11+ 75 E	<.2	1.20	30	55	<5	0.03	<1	10	65	16	5.26	<10	0.46	249	<1	0.01	22	2440	22	<5	<20	5	0.02	<10	86	<10	<1	56
228	L11N 12+ 00 E	0.4	1.00	10	45	<5	0.03	<1	7	18	9	3.27	<10	0.15	141	<1	0.02	10	760	16	<5	<20	5	0.01	<10	30	<10	<1	32
229	L11N 12+ 25 E	<.2	0.95	20	45	<5	0.12	<1	14	22	19	5.41	<10	0.10	357	<1	<.01	27	1500	26	<5	<20	7	0.01	<10	38	<10	<1	76
230	L11N 12+ 50 E	<.2	0.63	25	60	5	0.03	<1	13	11	19	4.72	<10	0.05	211	1	0.01	40	1050	22	<5	<20	5	0.01	<10	35	<10	<1	65
231	L11N 12+ 75 E	1.0	0.94	20	75	<5	0.42	1	11	15	13	4.38	<10	0.06	2014	1	<.01	25	1060	40	<5	<20	10	<.01	<10	35	<10	<1	161
232	L11N 13+ 00 E	1.4	0.36	10	70	<5	0.10	<1	8	4	43	2.25	<10	0.03	1610	<1	0.02	17	580	12	<5	<20	7	<.01	<10	20	<10	2	85
233	L11N 13+ 25 E	1.0	0.58	<5	25	<5	<.01	<1	6	2	13	1.72	<10	0.01	73	<1	0.04	6	430	12	<5	<20	3	<.01	<10	18	<10	2	22
234	L11N 13+ 50 E	0.6	1.30	10	100	<5	0.13	<1	12	13	23	3.62	<10	0.12	906	1	0.02	12	1120	18	<5	<20	15	<.01	<10	26	<10	3	63
235	L11N 13+ 75 E	0.8	0.70	5	50	<5	0.25	<1	7	3	18	2.22	<10	0.08	159	<1	0.03	11	390	8	<5	<20	20	<.01	<10	20	<10	1	37
236	L11N 14+ 00 E	<.2	1.39	20	135	<5	0.33	<1	13	22	30	4.38	<10	0.24	271	2	0.01	22	860	20	<5	<20	30	<.01	<10	33	<10	1	88
237	L11N 14+ 25 E	<.2	1.72	25	145	<5	0.04	<1	16	65	28	5.40	<10	0.39	274	1	0.01	38	1730	6	<5	<20	6	0.01	<10	38	<10	<1	91
238	L11N 14+ 50 E	2.2	0.69	5	80	<5	0.05	<1	4	14	7	1.30	<10	0.11	93	1	0.02	7	650	16	<5	<20	12	<.01	<10	23	<10	1	30
239	L11N 14+ 75 E	0.4	1.23	15	125	<5	0.19	<1	11	33	20	3.67	<10	0.30	480	1	<.01	22	1640	34	<5	<20	21	<.01	<10	39	<10	3	207
240	L11N 15+ 00 E	0.6	0.86	10	155	<5	0.11	<1	12	22	27	3.01	<10	0.24	554	<1	0.01	19	1160	14	<5	<20	14	<.01	<10	32	<10	2	65
241	L13N 5+ 00 E	0.4	1.31	10	95	<5	0.19	<1	14	23	23	3.77	<10	0.32	719	1	0.01	20	810	16	<5	<20	18	<.01	<10	24	<10	7	60
242	L13N 5+ 25 E	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
243	L13N 5+ 50 E	0.4	1.48	15	105	<5	0.08	<1	14	22	18	3.51	<10	0.31	704	<1	0.02	16	750	14	<5	<20	9	<.01	<10	26	<10	5	58
244	L13N 5+ 75 E	0.2	1.82	10	75	<5	0.04	<1	12	23	25	3.79	<10	0.22	521	2	<.01	13	740	26	<5	<20	7	0.01	<10	26	<10	1	61
245	L13N 6+ 00 E	0.4	0.78	10	85	<5	0.24	<1	8	15	15	3.23	<10	0.12	318	2	0.01	10	670	14	<5	<20	13	0.01	<10	25	<10	2	44
246	L13N 6+ 25 E	<.2	1.92	20	100	<5	0.24	<1	16	27	17	4.30	<10	0.28	450	1	0.01	15	830	18	<5	<20	15	0.01	<10	30	<10	2	59
247	L13N 6+ 50 E	0.4	1.80	5	85	<5	0.19	<1	12	24	17	4.33	<10	0.26	433	<1	<.01	12	790	10	<5	<20	13	<.01	<10	24	<10	<1	57
248	L13N 6+ 75 E	0.4	1.07	10	100	<5	0.26	<1	9	19	15	3.13	<10	0.26	370	1	0.01	12	1080	14	<5	<20	18	<.01	<10	23	<10	1	49
249	L13N 7+ 00 E	0.6	1.18	10	100	<5	0.55	<1	9	18	15	2.80	<10	0.20	588	2	<.01	10	710	10	<5	<20	38	<.01	<10	22	<10	1	50
250	L13N 7+ 25 E	1.6	1.13	5	110	<5	1.70	<1	11	22	15	2.39	<10	0.19	1155	2	<.01	10	1220	8	<5	<20	80	<.01	<10	19	<10	7	58
251	L13N 7+ 50 E	1.2	0.81	<5	80	<5	0.10	<1	4	12	14	2.15	<10	0.13	132	<1	0.01	5	850	8	<5	<20	14	<.01	<10	20	<10	<1	24
252	L13N 7+ 75 E	0.8	0.84	5	100	<5	0.91	<1	7	15	13	2.40	<10	0.17	582	1	0.01	9	990	10	<5	<20	53	<.01	<10	23	<10	2	47
253	L13N 8+ 00 E	0.4	0.79	<5	95	<5	0.51	<1	7	11	16	2.10	<10	0.15	361	<1	0.01	8	790	8	<5	<20	31	<.01	<10	22	<10	1	38
254	L13N 8+ 25 E	0.4	0.80	5	65	<5	0.06	<1	6	14	17	3.03	<10	0.15	168	<1	0.02	10	860	14	<5	<20	11	<.01	<10	27	<10	<1	35
255	L13N 8+ 50 E	0.8	1.13	10	75	<5	0.10	<1	10	16	14	2.49	<10	0.31	214	1	0.02	12	560	10	<5	<20	13	0.01	<10	23	<10	3	40
256	L13N 8+ 75 E	0.4	1.30	<5	70	<5	0.08	<1	7	23	13	2.97	<10	0.27	150	2	0.01	11	430	8	<5	<20	8	<.01	<10	26	<10	<1	49
257	L13N 9+ 00 E	0.8	0.81	<5	75	<5	0.05	<1	6	13	10	2.35	<10	0.21	162	<1	0.02	9	700	8	<5	<20	9	0.01	<10	23	<10	1	37
258	L13N 9+ 25 E	0.8	0.79	<5	75	<5	0.04	<1	6	16	9	2.43	<10	0.17	258	<1	0.02	8	590	8	<5	<20	7	0.01	<10	28	<10	<1	35
259	L13N 9+ 50 E	0.8	0.66	5	35	<5	0.04	<1	5	13	7	2.20	<10	0.12	110	<1	0.02	7	680	10	<5	<20	6	0.01	<10	26	<10	<1	29
260	L13N 9+ 75 E	0.8	0.86	<5	40	<5	0.05	<1	4	14	6	2.53	<10	0.15	141	<1	0.02	5	980	8	<5	<20	6	0.01	<10	27	<10	<1	26
261	L13N 10+ 25 E	0.6	2.15	15	160	<5	0.41	2	17	46	16	3.82	<10	0.51	387	2	<.01	31	810	18	<5	<20	14	<.01	<10	35	<10	8	268
262	L13N 10+ 50 E	0.4	1.47	20	160	<5	1.78	1	11	19	12	2.53	<10	0.25	1730	6	<.01	19	1150	42	<5	<20	26	<.01	<10	27	<10	9	199

TOKLAT RESOURCES INC. ETK 94-455 | ECO-TECH LABORATORIES LTD.

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
263	L13N 10+ 75 E	0.2	1.61	10	65	<5	0.05	<1	7	29	9	3.90	<10	0.30	138	<1	0.02	10	770	10	<5	<20	7	<.01	<10	41	<10	<1	44
264	L13N 11+ 00 E	<.2	2.04	15	40	<5	0.07	<1	20	92	21	6.37	<10	1.00	420	2	0.01	41	1470	10	<5	<20	5	0.01	<10	92	<10	<1	105
265	L13N 11+ 25 E	<.2	3.44	15	70	<5	0.07	<1	17	124	30	6.28	<10	1.69	326	<1	<.01	35	1450	12	<5	<20	6	<.01	<10	112	<10	<1	117
266	L13N 11+ 50 E	1.2	0.98	10	40	<5	0.02	<1	6	18	19	2.57	<10	0.15	149	4	0.02	12	890	20	<5	<20	8	<.01	<10	50	<10	1	57
267	L13N 11+ 75 E	0.6	1.91	10	55	<5	0.02	<1	7	30	9	2.74	<10	0.65	309	<1	0.01	9	760	2	<5	<20	4	<.01	<10	36	<10	<1	45
268	L13N 12+ 00 E	0.8	0.74	10	75	<5	0.10	<1	7	12	12	2.52	<10	0.10	150	<1	0.02	11	840	10	<5	<20	9	<.01	<10	24	<10	<1	40
269	L13N 12+ 25 E	1.2	1.40	15	140	<5	1.04	1	20	19	25	3.58	<10	0.29	2281	2	<.01	20	2140	20	<5	<20	51	0.01	<10	23	<10	9	114
270	L13N 12+ 50 E	1.0	1.32	10	125	<5	0.82	<1	14	15	22	2.77	<10	0.25	1107	1	0.01	15	1430	12	<5	<20	45	<.01	<10	22	<10	8	58
271	L13N 12+ 75 E	0.8	1.30	10	165	<5	0.74	<1	16	18	17	3.14	<10	0.24	2128	1	0.01	14	1380	14	<5	<20	40	<.01	<10	24	<10	5	62
272	L13N 13+ 00 E	0.8	1.75	15	150	5	0.73	<1	20	21	32	3.68	<10	0.28	2202	1	0.01	21	1970	20	<5	<20	42	<.01	<10	24	<10	17	85
273	L13N 13+ 25 E	1.2	1.90	15	150	<5	0.63	<1	18	21	32	3.70	<10	0.32	457	1	0.01	23	1710	18	<5	<20	40	<.01	<10	24	<10	13	72
274	L13N 13+ 50 E	1.0	0.67	10	85	<5	0.15	<1	6	12	12	2.40	<10	0.09	99	1	0.02	14	1360	22	<5	<20	12	<.01	<10	27	<10	1	51
275	L13N 13+ 75 E	2.0	0.58	<5	65	<5	0.07	<1	7	7	33	3.23	<10	0.06	134	<1	<.01	16	1270	12	<5	<20	7	<.01	<10	18	<10	<1	77
276	L13N 14+ 00 E	0.8	0.56	<5	75	<5	0.10	<1	8	6	26	3.31	<10	0.07	166	1	<.01	14	1120	10	<5	<20	9	<.01	<10	20	<10	<1	57
277	L13N 14+ 25 E	0.2	1.20	15	60	<5	0.10	<1	9	34	24	4.37	<10	0.28	165	1	<.01	22	1840	24	<5	<20	17	<.01	<10	35	<10	1	70
278	L13N 14+ 50 E	<.2	0.78	15	45	<5	0.06	<1	15	16	41	4.58	<10	0.09	590	9	0.03	25	1170	20	<5	<20	9	<.01	<10	26	<10	6	143
279	L13N 14+ 75 E	1.6	2.85	30	45	<5	0.03	<1	8	51	37	8.66	<10	0.98	213	3	0.04	9	1600	12	<5	<20	24	<.01	<10	66	<10	<1	75
280	L13N 15+ 00 E	1.2	1.28	30	70	<5	0.08	<1	9	36	22	6.16	<10	0.21	251	3	0.02	13	3020	32	<5	<20	12	0.01	<10	76	<10	<1	78
281	L14N 5+ 00 E	<.2	0.82	30	50	<5	0.06	<1	9	22	18	6.21	<10	0.13	491	3	0.01	9	670	16	<5	<20	6	<.01	<10	29	<10	<1	46
282	L14N 5+ 25 E	0.4	1.24	20	105	<5	2.07	<1	17	32	20	4.63	<10	0.27	1120	2	0.01	13	1170	20	<5	<20	48	<.01	<10	27	<10	9	59
283	L14N 5+ 50 E	0.4	1.23	15	90	<5	0.80	<1	17	24	24	3.61	<10	0.37	850	2	0.01	21	780	22	<5	<20	37	<.01	<10	23	<10	9	91
284	L14N 5+ 75 E	1.8	0.35	<5	45	<5	2.87	<1	5	5	11	0.94	<10	0.20	838	<1	<.01	6	920	4	<5	<20	112	<.01	<10	4	<10	3	40
285	L14N 6+ 00 E	1.2	0.55	10	50	<5	0.10	<1	5	12	13	2.12	<10	0.11	174	2	0.01	6	390	10	<5	<20	7	<.01	<10	27	<10	<1	25
286	L14N 6+ 25 E	0.6	1.02	15	100	<5	0.08	<1	13	17	25	3.20	<10	0.22	1047	<1	0.01	15	620	14	<5	<20	7	<.01	<10	17	<10	3	52
287	L14N 6+ 50 E	0.6	0.78	10	85	<5	0.11	<1	6	14	14	2.32	<10	0.15	215	<1	0.01	8	550	10	<5	<20	8	<.01	<10	29	<10	<1	36
288	L14N 6+ 75 E	0.6	1.56	15	75	<5	0.14	<1	17	20	29	3.57	<10	0.45	402	<1	0.01	21	600	12	<5	<20	12	<.01	<10	15	<10	3	58
289	L14N 7+ 00 E	1.8	0.56	<5	90	<5	3.34	<1	7	10	25	1.28	<10	0.19	1160	2	<.01	9	980	6	<5	<20	124	<.01	<10	11	<10	5	66
290	L14N 7+ 25 E	0.4	1.24	5	70	<5	0.41	<1	11	21	20	2.86	<10	0.27	363	1	0.01	13	670	10	<5	<20	24	<.01	<10	23	<10	4	49
291	L14N 7+ 50 E	<.2	1.59	15	125	5	0.49	<1	18	43	37	4.09	<10	0.39	664	2	0.02	23	910	28	<5	<20	32	<.01	<10	32	<10	53	110
292	L14N 7+ 75 E	1.6	2.43	25	155	<5	0.59	<1	22	34	41	4.37	<10	0.24	580	2	0.03	26	930	26	<5	<20	35	0.01	<10	33	<10	39	65
293	L14N 8+ 00 E	1.8	0.85	<5	65	<5	0.06	<1	4	10	6	1.43	<10	0.11	185	<1	0.02	5	350	4	<5	<20	8	<.01	<10	21	<10	2	23
294	L14N 8+ 25 E	0.6	0.99	5	90	<5	0.05	<1	6	16	7	2.85	<10	0.21	143	<1	0.02	7	870	12	<5	<20	8	0.01	<10	26	<10	<1	31
295	L14N 8+ 50 E	0.8	0.92	<5	45	<5	0.04	<1	5	15	7	2.92	<10	0.15	209	<1	0.02	7	860	8	<5	<20	7	0.01	<10	24	<10	<1	31
296	L14N 8+ 75 E	0.6	0.81	5	50	<5	0.08	<1	5	16	9	2.80	<10	0.16	134	<1	0.02	7	780	12	<5	<20	8	0.02	<10	28	<10	<1	27
297	L14N 9+ 00 E	0.8	0.76	5	45	<5	0.05	<1	6	15	9	2.48	<10	0.19	255	<1	0.01	9	1040	12	<5	<20	6	0.01	<10	36	<10	<1	35
298	L14N 9+ 25 E	1.0	0.78	5	55	<5	0.05	<1	4	18	5	2.66	<10	0.15	108	<1	0.01	6	1370	22	<5	<20	6	0.02	<10	38	<10	<1	27
299	L14N 9+ 50 E	1.6	0.55	<5	75	<5	0.07	<1	2	6	3	0.86	<10	0.08	358	<1	0.02	3	400	<2	<5	<20	6	<.01	<10	13	<10	<1	17
300	L14N 9+ 75 E	1.2	0.62	<5	70	<5	0.07	<1	3	11	5	1.16	<10	0.13	112	<1	0.02	5	490	8	<5	<20	7	<.01	<10	21	<10	1	20
301	L14N 10+ 25 E	<.2	4.23	20	50	<5	0.14	<1	26	214	16	6.42	<10	2.80	503	<1	0.02	40	1600	6	<5	<20	10	0.05	<10	149	<10	<1	99

TOKLAT RESOURCES INC. ETK 94-455 | ECO-TECH LABORATORIES LTD.

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
302	L14N 10+ 50 E	<.2	3.37	10	205	<5	0.30	<1	34	184	30	6.06	<10	3.41	889	<1	0.02	49	1240	6	<5	<20	16	0.12	<10	199	<10	<1	76
303	L14N 10+ 75 E	<.2	3.01	25	70	10	0.07	<1	25	116	28	5.63	<10	2.05	587	1	0.02	31	1090	6	<5	<20	6	0.02	<10	155	<10	<1	66
304	L14N 11+ 00 E	<.2	1.30	20	55	<5	0.03	<1	13	39	19	4.22	<10	0.37	339	<1	0.01	18	910	16	<5	<20	5	0.01	<10	52	<10	<1	55
305	L14N 11+ 25 E	<.2	0.81	15	50	<5	0.04	<1	4	22	4	2.16	<10	0.20	168	<1	0.02	7	520	16	<5	<20	6	<.01	<10	27	<10	<1	26
306	L14N 11+ 50 E	<.2	2.19	15	50	<5	0.03	<1	6	39	6	2.86	<10	0.91	174	<1	0.02	10	780	<2	<5	<20	4	<.01	<10	29	<10	<1	51
307	L14N 11+ 75 E	<.2	1.63	15	70	<5	0.02	<1	8	26	13	3.79	<10	0.62	350	<1	0.02	12	950	12	<5	<20	5	<.01	<10	29	<10	<1	55
308	L14N 12+ 00 E	<.2	0.31	15	20	<5	0.07	<1	6	6	5	1.33	<10	0.04	161	1	0.04	7	420	8	<5	<20	5	<.01	<10	20	<10	2	28
309	L14N 12+ 25 E	<.2	1.12	25	55	<5	0.14	<1	8	16	19	3.05	<10	0.21	180	2	0.02	16	2040	26	<5	<20	15	<.01	<10	22	<10	1	69
310	L14N 12+ 50 E	<.2	0.80	60	75	<5	0.20	1	11	40	19	4.44	<10	0.19	632	<1	0.02	55	2290	74	<5	<20	16	0.01	<10	30	<10	1	239
311	L14N 12+ 75 E	<.2	1.34	25	120	<5	0.67	2	30	19	50	5.19	<10	0.41	610	2	0.01	55	1630	20	<5	<20	37	<.01	<10	19	<10	6	201
312	L14N 13+ 00 E	0.8	1.56	20	170	<5	1.11	4	20	21	56	2.66	<10	0.42	180	<1	0.02	49	1800	20	<5	<20	54	0.01	<10	21	<10	14	166
313	L14N 13+ 25 E	<.2	1.63	20	185	<5	0.46	<1	8	18	38	4.00	<10	0.29	206	2	0.01	12	1410	24	<5	<20	28	<.01	<10	35	<10	<1	74
314	L14N 13+ 50 E	<.2	0.84	15	85	<5	0.44	<1	4	6	26	3.16	<10	0.14	78	2	<.01	8	1160	18	<5	<20	34	<.01	<10	34	<10	<1	73
315	L14N 13+ 75 E	<.2	1.56	50	75	<5	0.15	<1	17	25	26	7.33	<10	0.30	406	2	0.01	36	3240	36	<5	<20	15	0.01	<10	39	<10	<1	137
316	L14N 14+ 00 E	2.6	0.92	30	75	<5	0.09	1	11	11	170	5.48	<10	0.14	266	4	<.01	30	2400	30	<5	<20	79	<.01	<10	51	<10	4	174
317	L14N 14+ 25 E	<.2	1.14	25	60	<5	0.11	<1	15	25	32	5.39	<10	0.16	580	8	0.03	26	1400	30	<5	<20	15	0.01	<10	84	<10	1	99
318	L14N 14+ 50 E	<.2	1.40	20	115	<5	0.37	<1	9	28	17	3.54	<10	0.36	343	2	0.02	15	960	18	<5	<20	20	<.01	<10	41	<10	<1	72
319	L14N 14+ 75 E	<.2	1.66	45	175	<5	0.33	2	17	44	43	6.71	<10	0.59	468	3	0.02	42	1780	40	<5	<20	18	0.01	<10	50	<10	4	137
320	L14N 15+ 00 E	<.2	1.69	25	80	<5	0.02	<1	9	28	23	6.57	<10	0.31	172	<1	<.01	23	1670	22	<5	<20	5	0.01	<10	35	<10	<1	94
321	L12N 5+ 00 E	<.2	2.35	40	220	<5	0.78	1	22	42	30	5.89	<10	0.36	1927	1	0.03	30	1380	40	<5	<20	16	0.01	<10	40	<10	19	111
322	L12N 5+ 25 E	<.2	1.21	35	80	<5	0.12	<1	18	30	23	5.62	<10	0.31	643	1	0.02	29	1270	36	<5	<20	10	0.01	<10	26	<10	3	92
323	L12N 5+ 50 E	<.2	1.82	40	200	5	0.70	<1	25	36	30	5.12	<10	0.31	1926	1	0.03	31	1550	38	<5	<20	30	0.01	<10	34	<10	30	109
324	L12N 5+ 75 E	<.2	0.87	40	110	<5	0.16	<1	14	29	21	5.73	<10	0.19	494	<1	0.01	21	1060	38	<5	<20	11	0.02	<10	38	<10	<1	68
325	L12N 6+ 00 E	<.2	0.67	30	170	<5	0.08	<1	9	18	14	3.97	<10	0.15	400	<1	0.02	12	950	24	<5	<20	8	0.01	<10	30	<10	<1	55
326	L12N 6+ 25 E	<.2	1.01	35	130	<5	0.09	<1	11	26	16	5.54	<10	0.23	663	<1	0.01	17	2210	30	<5	<20	8	0.01	<10	28	<10	<1	60
327	L12N 6+ 50 E	<.2	0.65	30	85	<5	0.12	<1	7	17	9	3.02	<10	0.15	151	2	0.02	12	1240	24	<5	<20	8	0.01	<10	33	<10	<1	45
328	L12N 6+ 75 E	<.2	0.96	20	110	<5	0.15	<1	9	20	13	4.12	<10	0.18	483	<1	0.02	13	1170	16	<5	<20	9	0.02	<10	27	<10	<1	56
329	L12N 7+ 00 E	<.2	0.69	15	85	<5	0.02	<1	4	12	5	1.91	<10	0.08	81	<1	0.03	5	650	12	<5	<20	5	0.01	<10	25	<10	1	23
330	L12N 7+ 25 E	<.2	1.07	20	95	<5	0.05	<1	7	21	9	3.47	<10	0.24	176	<1	0.02	12	1520	16	<5	<20	7	<.01	<10	30	<10	<1	47
331	L12N 7+ 50 E	<.2	1.49	30	165	<5	0.22	<1	12	28	12	4.94	<10	0.43	392	<1	0.02	19	1630	44	<5	<20	21	0.01	<10	24	<10	<1	79
332	L12N 7+ 75 E	<.2	1.31	25	110	<5	0.11	<1	9	21	16	3.93	<10	0.27	215	<1	0.02	14	1080	20	<5	<20	11	0.01	<10	31	<10	2	57
333	L12N 8+ 00 E	<.2	1.00	25	145	<5	0.17	<1	11	21	71	4.46	<10	0.25	426	<1	0.02	18	1160	26	<5	<20	13	0.01	<10	40	<10	<1	77
334	L12N 8+ 25 E	<.2	1.22	20	110	<5	0.06	<1	6	21	10	2.83	<10	0.22	156	<1	0.02	8	1030	20	<5	<20	8	0.01	<10	30	<10	<1	42
335	L12N 8+ 50 E	<.2	0.93	10	110	<5	0.05	<1	3	11	7	1.65	<10	0.11	128	<1	0.02	3	530	12	<5	<20	8	<.01	<10	24	<10	<1	25
336	L12N 8+ 75 E	<.2	1.30	25	140	<5	0.15	<1	6	26	10	4.17	<10	0.29	162	<1	0.02	11	2250	24	<5	<20	15	0.01	<10	32	<10	<1	55
337	L12N 9+ 00 E	<.2	1.26	20	165	<5	0.03	<1	8	28	12	4.55	<10	0.26	376	<1	0.01	10	1920	20	<5	<20	12	0.01	<10	31	<10	<1	67
338	L12N 9+ 25 E	<.2	1.16	15	85	<5	0.13	1	8	21	9	3.75	<10	0.29	521	<1	0.02	11	1450	16	<5	<20	12	0.01	<10	27	<10	<1	58
339	L12N 9+ 50 E	<.2	0.97	30	95	<5	0.08	<1	8	24	12	4.84	<10	0.20	218	1	0.02	14	1680	28	<5	<20	10	0.02	<10	31	<10	<1	59
340	L12N 9+ 75 E	<.2	0.87	15	100	<5	0.19	<1	8	15	17	4.08	<10	0.12	212	<1	0.03	17	730	20	<5	<20	16	<.01	<10	24	<10	10	58

TOKLAT RESOURCES INC. ETK 94-455 ECO-TECH LABORATORIES LTD.

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
341	L12N 10+ 25 E	<.2	1.39	25	80	<5	0.19	<1	11	27	14	4.80	<10	0.34	314	<1	0.02	20	970	22	<5	<20	13	0.01	<10	26	<10	1	70
342	L12N 10+ 50 E	<.2	1.73	25	100	<5	0.08	<1	11	25	15	5.08	<10	0.37	275	<1	0.01	19	990	14	<5	<20	10	<.01	<10	21	<10	<1	85
343	L12N 10+ 75 E	<.2	1.93	35	60	<5	0.05	<1	11	27	15	4.90	<10	0.33	171	2	0.01	21	680	24	<5	<20	6	<.01	<10	21	<10	<1	78
344	L12N 11+ 00 E	<.2	0.87	20	55	<5	0.03	<1	5	15	7	3.15	<10	0.13	130	<1	0.02	10	880	20	<5	<20	6	0.02	<10	29	<10	<1	39
345	L12N 11+ 25 E	<.2	1.74	30	65	<5	0.03	<1	12	24	16	5.11	<10	0.38	282	<1	0.02	23	920	22	<5	<20	6	<.01	<10	20	<10	<1	97
346	L12N 11+ 50 E	<.2	1.58	40	75	<5	0.08	<1	12	30	12	5.88	<10	0.25	356	1	0.02	21	1860	24	<5	<20	7	0.01	<10	30	<10	<1	72
347	L12N 11+ 75 E	<.2	1.17	60	60	<5	0.11	<1	11	30	20	5.79	<10	0.24	358	1	0.01	27	2290	30	<5	<20	11	0.02	<10	29	<10	<1	71
348	L12N 12+ 00 E	<.2	1.07	40	50	<5	0.08	<1	9	22	10	5.17	<10	0.16	412	<1	0.01	19	1690	34	<5	<20	7	0.01	<10	33	<10	<1	65
349	L12N 12+ 25 E	<.2	1.36	50	70	<5	0.10	1	15	27	17	5.92	<10	0.24	804	2	0.02	40	1530	40	<5	<20	8	0.01	<10	31	<10	<1	136
350	L12N 12+ 50 E	<.2	0.94	75	45	<5	0.06	<1	12	15	24	6.58	<10	0.19	485	<1	0.02	45	1600	20	<5	<20	8	0.01	<10	22	<10	<1	63
351	L12N 12+ 75 E	<.2	0.82	20	45	<5	0.15	1	8	18	10	3.98	<10	0.19	249	<1	0.02	15	920	18	<5	<20	14	0.01	<10	36	<10	<1	55
352	L12N 13+ 00 E	<.2	1.27	25	80	<5	0.18	1	6	17	8	3.83	<10	0.23	178	1	0.01	10	830	16	<5	<20	16	<.01	<10	23	<10	<1	52
353	L12N 13+ 25 E	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
354	L12N 13+ 50 E	<.2	1.43	50	155	<5	0.58	1	26	30	27	5.70	<10	0.29	1939	3	0.01	46	1640	50	<5	<20	32	0.02	<10	30	<10	20	208
355	L12N 13+ 75 E	3.4	1.14	40	210	<5	1.71	6	17	12	81	3.31	<10	0.13	3058	3	<.01	28	2750	36	<5	<20	58	<.01	<10	13	<10	38	258
356	L12N 14+ 00 E	3.8	2.29	20	130	<5	2.11	4	27	27	90	4.02	<10	0.22	2282	<1	0.05	43	1900	44	<5	<20	64	<.01	<10	16	<10	126	132
357	L12N 14+ 25 E	<.2	1.00	25	85	<5	0.21	1	13	22	56	6.10	<10	0.15	352	2	<.01	26	1310	30	<5	<20	22	0.01	<10	52	<10	2	156
358	L12N 14+ 50 E	2.2	2.06	30	145	<5	1.00	5	33	39	63	5.21	<10	0.38	5329	2	0.01	42	2010	32	<5	<20	49	0.01	<10	37	<10	37	195
359	L12N 14+ 75 E	0.4	1.50	35	115	<5	0.47	2	22	24	44	4.85	<10	0.38	1212	1	0.02	36	970	24	<5	<20	29	0.01	<10	22	<10	17	115
360	L12N 15+ 00 E	1.4	2.23	30	175	<5	0.64	4	26	36	59	5.16	<10	0.46	1923	2	0.04	42	1840	32	<5	<20	39	<.01	<10	35	<10	48	148
361	L10N 5+ 00 E	<.2	1.46	35	110	<5	0.13	<1	19	30	22	5.26	<10	0.29	586	<1	0.01	23	930	26	<5	<20	10	0.01	<10	25	<10	6	80
362	L10N 5+ 25 E	<.2	1.13	30	85	<5	0.11	<1	12	23	16	4.40	<10	0.23	403	1	0.01	16	800	26	<5	<20	9	<.01	<10	25	<10	3	56
363	L10N 5+ 50 E	<.2	1.28	35	155	<5	0.21	<1	13	27	20	5.12	<10	0.29	466	<1	0.01	20	830	30	<5	<20	12	0.01	<10	26	<10	<1	80
364	L10N 5+ 75 E	<.2	1.23	45	115	<5	0.26	<1	16	24	28	5.50	<10	0.18	568	<1	0.01	21	920	34	<5	<20	17	0.01	<10	29	<10	16	72
365	L10N 6+ 00 E	<.2	0.93	70	95	<5	0.09	<1	14	29	18	5.60	<10	0.20	771	1	0.02	19	1080	34	<5	<20	7	0.01	<10	31	<10	2	75
366	L10N 6+ 25 E	<.2	0.99	45	135	5	0.46	<1	17	29	17	4.61	<10	0.26	660	2	0.01	20	1090	38	<5	<20	23	0.02	<10	31	<10	3	79
367	L10N 6+ 50 E	0.4	1.42	15	180	<5	0.73	<1	15	29	29	3.81	<10	0.33	657	<1	0.01	28	1230	22	<5	<20	34	<.01	<10	18	<10	15	83
368	L10N 6+ 75 E	<.2	1.19	25	140	<5	0.51	<1	17	25	26	3.99	<10	0.33	1253	<1	0.01	26	1060	24	<5	<20	26	0.01	<10	20	<10	13	76
369	L10N 7+ 00 E	<.2	1.41	30	135	<5	0.44	<1	18	27	24	4.17	<10	0.33	1184	<1	0.01	25	1170	32	<5	<20	24	0.01	<10	22	<10	11	98
370	L10N 7+ 25 E	<.2	0.66	35	85	<5	0.41	<1	12	23	17	4.62	<10	0.24	431	1	0.01	19	1220	28	<5	<20	19	<.01	<10	24	<10	<1	63
371	L10N 7+ 50 E	<.2	1.24	25	145	<5	0.65	<1	14	24	26	3.72	<10	0.29	895	2	0.01	24	1180	40	<5	<20	39	0.01	<10	21	<10	14	83
372	L10N 7+ 75 E	<.2	1.36	20	85	<5	0.45	<1	17	27	12	4.57	<10	0.48	510	<1	0.02	22	860	24	<5	<20	23	0.01	<10	23	<10	3	72
373	L10N 8+ 00 E	<.2	1.52	25	110	<5	0.79	<1	17	24	22	4.46	<10	0.30	1126	1	0.01	23	1370	22	<5	<20	35	0.01	<10	22	<10	9	64
374	L10N 8+ 25 E	0.2	0.96	30	105	<5	0.50	<1	13	27	19	5.27	<10	0.21	543	2	0.02	21	1440	34	<5	<20	22	<.01	<10	31	<10	5	65
375	L10N 8+ 50 E	<.2	1.38	30	95	<5	0.20	<1	14	29	18	5.48	<10	0.31	533	<1	0.02	22	1210	30	<5	<20	11	0.01	<10	28	<10	5	75
376	L10N 8+ 75 E	<.2	0.81	30	120	<5	0.36	<1	10	20	18	4.18	<10	0.18	344	<1	0.02	19	1310	24	<5	<20	21	<.01	<10	28	<10	4	61
377	L10N 9+ 00 E	0.4	0.61	15	85	<5	0.52	<1	6	14	11	2.81	<10	0.12	295	<1	0.02	11	1010	18	<5	<20	27	<.01	<10	23	<10	1	47
378	L10N 9+ 25 E	<.2	0.69	20	95	<5	0.13	<1	7	15	11	3.15	<10	0.12	251	<1	0.02	13	1150	18	<5	<20	10	<.01	<10	24	<10	1	50
379	L10N 9+ 50 E	<.2	0.82	25	70	<5	0.31	<1	10	20	14	4.51	<10	0.20	383	1	0.02	15	1350	24	<5	<20	18	0.01	<10	25	<10	1	60

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
380	L10N 9+ 75 E	< 2	0.79	20	125	<5	0.62	<1	8	16	14	3.17	<10	0.17	367	3	0.02	14	870	18	<5	<20	35	0.01	<10	23	<10	4	63
381	L10N 10+ 25 E	< 2	0.74	25	140	<5	0.45	<1	12	20	13	3.73	<10	0.16	784	2	0.02	19	670	26	<5	<20	20	0.01	<10	30	<10	2	64
382	L10N 10+ 50 E	< 2	0.86	30	50	<5	0.12	<1	10	24	14	5.09	<10	0.15	232	2	0.02	27	990	26	<5	<20	9	<.01	<10	36	<10	<1	78
383	L10N 10+ 75 E	< 2	0.57	35	60	<5	0.09	<1	11	16	14	4.77	<10	0.14	278	2	0.03	22	1260	36	<5	<20	13	0.02	<10	35	<10	1	72
384	L10N 11+ 00 E	< 2	1.11	45	60	<5	0.15	<1	15	26	26	7.09	<10	0.25	455	2	0.01	30	3240	48	<5	<20	13	<.01	<10	25	<10	1	108
385	L10N 11+ 25 E	0.6	0.81	35	50	<5	0.05	<1	8	28	10	5.11	<10	0.16	142	1	0.02	26	2580	46	<5	<20	9	<.01	<10	39	<10	<1	104
386	L10N 11+ 50 E	< 2	0.78	15	40	<5	0.01	<1	5	16	5	2.36	<10	0.11	75	<1	0.03	10	580	14	<5	<20	4	0.01	<10	31	<10	<1	36
387	L10N 11+ 75 E	< 2	1.05	30	40	<5	0.08	<1	9	31	12	4.58	<10	0.25	160	1	0.02	23	1490	28	<5	<20	8	0.01	<10	41	<10	<1	89
388	L10N 12+ 00 E	< 2	1.43	30	95	<5	0.16	<1	6	22	25	2.84	<10	0.12	179	10	0.02	14	1650	64	<5	<20	9	0.01	<10	49	<10	<1	129
389	L10N 12+ 25 E	< 2	2.00	35	100	<5	0.05	1	13	60	19	7.50	<10	0.63	460	2	<.01	26	1590	20	<5	<20	6	<.01	<10	50	<10	<1	104
390	L10N 12+ 50 E	< 2	1.40	35	60	<5	0.03	<1	8	34	14	6.88	<10	0.53	304	2	<.01	15	1040	18	<5	<20	5	0.01	<10	44	<10	<1	62
391	L10N 12+ 75 E	< 2	3.01	60	100	<5	0.29	<1	32	39	33	8.90	<10	0.23	1024	<1	<.01	54	2680	30	<5	<20	10	0.01	<10	43	<10	5	183
392	L10N 13+ 00 E	< 2	0.36	45	95	<5	0.09	<1	8	12	25	3.01	<10	0.03	340	7	0.02	30	1030	46	<5	<20	26	<.01	<10	42	<10	<1	67
393	L10N 13+ 25 E	< 2	1.02	175	40	<5	0.05	<1	19	42	15	> 15	<10	0.10	1220	2	<.01	85	1660	172	<5	<20	5	0.02	<10	54	<10	<1	110
394	L10N 13+ 50 E	0.8	0.70	45	275	<5	0.45	<1	17	14	15	5.47	<10	0.10	4183	2	<.01	53	1610	18	<5	<20	37	<.01	<10	20	<10	3	90
395	L10N 13+ 75 E	0.8	1.23	105	120	<5	0.87	2	26	23	23	8.42	<10	0.09	2601	3	0.02	95	2710	130	<5	<20	20	<.01	<10	21	<10	33	338
396	L10N 14+ 00 E	0.8	0.86	15	185	<5	1.01	<1	8	7	12	3.01	<10	0.13	1652	1	0.01	13	1020	36	<5	<20	64	<.01	<10	14	<10	31	158
397	L10N 14+ 25 E	< 2	1.06	30	150	<5	0.31	1	12	25	9	3.77	<10	0.15	373	3	0.02	16	820	22	<5	<20	20	<.01	<10	36	<10	2	66
398	L10N 14+ 50 E	0.4	1.68	50	195	<5	0.19	<1	20	35	25	6.08	<10	0.40	450	2	0.02	28	1460	28	<5	<20	16	<.01	<10	32	<10	<1	96
399	L10N 14+ 75 E	0.6	1.89	45	160	<5	0.27	<1	23	146	30	6.94	<10	0.94	851	2	<.01	35	1910	22	<5	<20	18	0.01	<10	74	<10	<1	107
400	L10N 15+ 00 E	1.4	1.41	55	165	<5	0.89	1	28	61	56	6.38	<10	0.31	565	23	<.01	34	2480	78	<5	<20	49	<.01	<10	125	<10	6	237
401	L15N 5+ 00 E	0.6	1.34	35	130	<5	0.70	1	23	32	30	5.32	<10	0.41	1161	2	0.01	21	1250	22	<5	<20	29	<.01	<10	24	<10	4	91
402	L15N 5+ 25 E	< 2	1.12	35	75	<5	1.13	<1	20	39	18	6.06	<10	0.23	997	6	0.01	15	1470	30	<5	<20	37	0.01	<10	40	<10	<1	100
403	L15N 5+ 50 E	1.2	1.44	25	90	<5	0.33	1	28	47	24	5.43	<10	0.51	1484	2	0.01	20	1470	24	<5	<20	18	0.01	<10	35	<10	6	87
404	L15N 5+ 75 E	0.4	1.28	15	90	<5	0.18	<1	8	37	7	4.10	<10	0.39	237	2	0.01	7	950	12	<5	<20	8	<.01	<10	34	<10	<1	37
405	L15N 6+ 00 E	< 2	1.14	55	135	<5	0.09	<1	13	44	9	7.49	<10	0.23	855	6	0.01	9	1230	38	<5	<20	8	0.01	<10	59	<10	<1	63
406	L15N 6+ 25 E	1.2	1.37	5	95	<5	0.08	<1	9	41	13	4.38	<10	0.51	368	<1	<.01	11	780	<2	<5	<20	6	<.01	<10	32	<10	<1	47
407	L15N 6+ 50 E	1.0	1.36	20	175	<5	1.00	<1	20	40	16	4.64	<10	0.39	1695	2	0.02	15	1390	12	<5	<20	31	0.01	<10	39	<10	4	70
408	L15N 6+ 75 E	0.4	0.75	30	80	<5	0.08	<1	7	18	8	3.18	<10	0.19	329	1	0.02	7	1740	8	<5	<20	6	<.01	<10	28	<10	<1	34
409	L15N 7+ 00 E	0.4	1.08	20	130	<5	0.14	<1	8	51	7	4.69	<10	0.31	231	1	0.01	10	2630	14	<5	<20	7	0.01	<10	61	<10	<1	59
410	L15N 7+ 25 E	0.2	1.33	20	80	<5	0.11	<1	10	38	8	3.82	<10	0.37	227	<1	<.01	11	930	16	<5	<20	7	<.01	<10	34	<10	<1	63
411	L15N 7+ 50 E	< 2	1.13	25	100	<5	0.12	<1	11	64	7	4.14	<10	0.37	329	3	0.02	13	690	16	<5	<20	7	0.01	<10	64	<10	<1	54
412	L15N 7+ 75 E	< 2	1.10	25	120	<5	0.07	<1	12	65	10	3.80	<10	0.43	350	3	0.02	16	1100	12	<5	<20	6	0.01	<10	50	<10	<1	63
413	L15N 8+ 00 E	0.4	0.59	10	180	<5	0.55	<1	6	23	5	2.41	<10	0.12	127	1	0.03	6	920	8	<5	<20	23	0.01	<10	36	<10	<1	60
414	L15N 8+ 25 E	< 2	1.04	35	135	5	1.96	<1	16	52	12	4.71	<10	0.33	394	5	0.01	16	1150	24	<5	<20	53	0.01	<10	49	<10	<1	97
415	L15N 8+ 50 E	0.2	0.90	10	130	<5	1.42	<1	9	39	11	3.87	<10	0.27	474	<1	<.01	11	900	<2	<5	<20	48	<.01	<10	30	<10	<1	85
416	L15N 8+ 75 E	0.4	1.69	20	265	<5	1.94	1	16	68	23	4.22	<10	0.47	973	1	<.01	17	1480	8	<5	<20	68	0.01	<10	52	<10	<1	175
417	L15N 9+ 00 E	0.4	1.01	20	75	<5	0.13	<1	7	32	11	2.65	<10	0.26	118	2	0.02	10	770	14	<5	<20	11	<.01	<10	48	<10	<1	46
418	L15N 9+ 25 E	< 2	1.26	30	70	<5	0.19	<1	15	66	18	4.91	<10	0.61	302	3	0.02	23	2110	36	<5	<20	12	0.02	<10	61	<10	<1	89

TOKLAT RESOURCES INC. ETK 94-455 ECO-TECH LABORATORIES LTD.

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
419	L15N 9+ 50 E	0.4	2.04	<5	85	<5	0.09	<1	14	86	18	5.32	<10	1.19	331	<1	<.01	19	1200	<2	<5	<20	6	0.02	<10	62	<10	<1	81
420	L15N 9+ 75 E	<.2	1.67	40	140	<5	0.10	<1	18	70	20	7.68	<10	0.59	895	2	<.01	21	2200	22	<5	<20	8	0.02	<10	66	<10	<1	90
421	L15N 10+ 25 E	<.2	1.03	20	60	<5	0.04	<1	12	48	13	3.20	<10	0.65	245	<1	0.01	12	920	4	<5	<20	4	0.04	<10	87	<10	<1	36
422	L15N 10+ 50 E	0.2	2.42	25	50	<5	0.16	<1	21	115	25	6.01	<10	1.84	535	<1	<.01	24	2020	70	<5	<20	7	0.02	<10	136	<10	<1	200
423	L15N 10+ 75 E	0.4	0.67	10	55	<5	0.09	<1	4	11	2	1.79	<10	0.17	126	<1	0.02	4	480	<2	<5	<20	6	<.01	<10	20	<10	<1	24
424	L15N 11+ 00 E	0.6	1.31	25	45	<5	0.14	<1	13	26	12	4.50	<10	0.42	513	<1	0.01	11	1420	6	<5	<20	7	<.01	<10	22	<10	<1	53
425	L15N 11+ 25 E	0.4	1.67	25	55	<5	0.09	<1	10	32	8	4.63	<10	0.30	424	1	0.02	9	2070	10	<5	<20	5	<.01	<10	32	<10	<1	48
426	L15N 11+ 50 E	0.2	0.90	25	40	<5	0.02	<1	7	19	8	3.27	<10	0.18	140	1	0.02	11	1320	16	<5	<20	4	<.01	<10	32	<10	<1	37
427	L15N 11+ 75 E	<.2	1.04	20	50	<5	0.07	<1	7	18	5	3.25	<10	0.18	188	<1	0.02	10	1610	14	<5	<20	5	0.01	<10	29	<10	<1	36
428	L15N 12+ 00 E	<.2	1.73	25	65	<5	0.04	<1	9	27	8	3.79	<10	0.26	326	1	0.02	9	1140	8	<5	<20	5	0.01	<10	35	<10	<1	51
429	L15N 12+ 25 E	1.8	1.80	30	105	<5	1.02	<1	24	36	18	4.71	<10	0.35	1796	2	0.02	21	1830	40	<5	<20	34	<.01	<10	32	<10	16	74
430	L15N 12+ 50 E	0.8	1.22	25	40	<5	0.04	<1	6	29	5	4.46	<10	0.25	194	1	0.02	7	1880	14	<5	<20	5	<.01	<10	42	<10	<1	33
431	L15N 12+ 75 E	0.8	1.23	15	35	<5	0.05	<1	8	14	9	3.41	<10	0.13	166	<1	0.02	8	1210	<2	<5	<20	4	<.01	<10	29	<10	<1	33
432	L15N 13+ 00 E	0.4	0.90	70	50	<5	0.04	<1	23	26	18	8.37	<10	0.08	1414	2	0.01	34	2440	18	<5	<20	3	0.01	<10	37	<10	<1	60
433	L15N 13+ 25 E	0.8	0.44	35	60	<5	0.10	<1	7	8	28	2.45	<10	0.03	398	4	<.01	12	1010	26	<5	<20	18	<.01	<10	39	<10	<1	40
434	L15N 13+ 50 E	0.4	1.94	35	70	<5	0.12	<1	18	23	22	7.56	<10	0.43	292	2	<.01	16	2970	6	<5	<20	8	<.01	<10	58	<10	<1	67
435	L15N 13+ 75 E	1.6	1.50	35	40	<5	0.05	<1	14	91	31	6.64	<10	0.56	497	2	<.01	26	2020	6	<5	<20	4	0.01	<10	68	<10	<1	53
436	L15N 14+ 00 E	2.0	1.42	25	65	<5	0.04	<1	7	43	15	6.04	<10	0.24	120	5	0.03	8	2350	18	<5	<20	7	0.02	<10	71	<10	<1	47
437	L15N 14+ 25 E	1.0	1.35	30	40	<5	0.01	<1	6	23	15	4.48	<10	0.33	113	2	0.02	7	1660	6	<5	<20	2	<.01	<10	37	<10	<1	31
438	L15N 14+ 50 E	0.8	0.35	30	50	<5	0.09	<1	8	6	67	2.93	<10	0.03	294	5	0.03	19	800	10	<5	<20	8	<.01	<10	58	<10	3	110
439	L15N 14+ 75 E	0.8	0.74	15	50	<5	0.05	<1	10	17	31	3.39	<10	0.08	236	2	0.02	18	880	6	<5	<20	5	<.01	<10	50	<10	1	44
440	L15N 15+ 00 E	0.6	1.49	40	50	<5	0.07	<1	16	24	39	6.81	<10	0.48	417	3	0.02	29	2060	20	<5	<20	6	<.01	<10	41	<10	<1	134
441	L20N 10+ 25 E	0.4	1.31	30	75	<5	0.12	<1	11	36	10	3.64	<10	0.34	270	1	0.02	13	1140	14	<5	<20	5	<.01	<10	46	<10	<1	43
442	L20N 10+ 50 E	0.2	1.35	20	95	<5	0.13	<1	15	50	13	4.59	<10	0.39	600	<1	0.02	19	1200	14	<5	<20	14	0.07	<10	98	<10	<1	114
443	L20N 10+ 75 E	<.2	0.85	15	40	<5	0.08	<1	8	15	7	3.23	<10	0.09	188	<1	0.02	8	660	6	<5	<20	6	<.01	<10	38	<10	<1	120
444	L20N 11+ 00 E	<.2	1.33	40	95	<5	0.05	<1	19	36	20	6.88	<10	0.28	660	1	<.01	19	1580	24	<5	<20	6	0.01	<10	37	<10	<1	276
445	L20N 11+ 25 E	2.2	0.56	20	100	<5	2.06	2	18	12	56	4.83	<10	0.16	1089	4	<.01	27	1240	16	<5	<20	65	<.01	<10	32	<10	<1	218
446	L20N 11+ 50 E	0.6	1.20	15	65	<5	0.03	<1	7	16	20	2.75	<10	0.08	86	3	0.02	8	1020	12	<5	<20	4	<.01	<10	37	<10	<1	33
447	L20N 11+ 75 E	0.2	1.44	25	75	<5	0.08	<1	15	8	43	9.06	<10	0.30	625	2	<.01	12	1920	<2	<5	<20	4	<.01	<10	36	<10	<1	82
448	L20N 12+ 00 E	0.2	2.33	40	135	<5	0.10	<1	22	19	26	10.40	<10	0.40	798	3	0.01	10	1960	10	<5	<20	5	<.01	<10	44	<10	<1	71
449	L20N 12+ 25 E	0.2	1.06	25	115	<5	0.14	<1	9	34	19	3.85	<10	0.21	249	2	0.01	13	830	4	<5	<20	7	<.01	<10	59	<10	<1	48
450	L20N 12+ 50 E	0.6	2.52	55	115	<5	0.29	<1	16	280	14	7.00	<10	1.50	579	2	<.01	33	1200	4	<5	<20	7	0.01	<10	129	<10	<1	79
451	L20N 12+ 75 E	0.2	1.16	25	70	<5	0.03	<1	6	21	11	3.74	<10	0.15	108	2	0.02	9	1400	32	<5	<20	4	<.01	<10	57	<10	<1	63
452	L20N 13+ 00 E	0.8	0.98	20	140	<5	0.10	<1	9	23	23	4.51	<10	0.10	1791	3	0.02	12	2280	24	<5	<20	6	<.01	<10	58	<10	<1	53
453	L20N 13+ 25 E	<.2	0.70	10	55	<5	0.02	<1	4	7	6	1.70	<10	0.04	85	1	0.02	5	680	<2	<5	<20	2	<.01	<10	24	<10	1	25
454	L20N 13+ 50 E	1.0	0.93	25	40	<5	0.02	<1	5	12	4	3.91	<10	0.06	114	<1	0.02	5	1910	20	<5	<20	3	<.01	<10	26	<10	<1	27
455	L20N 13+ 75 E	0.4	0.81	15	35	<5	0.10	<1	5	11	3	1.87	<10	0.10	193	<1	0.02	5	550	8	<5	<20	5	<.01	<10	33	<10	<1	27
456	L20N 14+ 00 E	0.4	1.29	20	55	<5	0.05	<1	9	26	12	4.95	<10	0.21	222	<1	0.02	9	1710	14	<5	<20	6	0.01	<10	41	<10	<1	49
457	L20N 14+ 25 E	<.2	1.27	15	75	<5	0.05	<1	4	11	6	2.06	<10	0.15	140	<1	0.02	5	790	10	<5	<20	10	<.01	<10	27	<10	<1	29

TOKLAT RESOURCES INC. ETK 94-455 | ECO-TECH LABORATORIES LTD.

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
458	L20N 14+ 50 E	0.6	2.39	15	95	<5	0.84	<1	23	31	35	4.51	<10	0.30	1480	<1	0.04	29	2730	18	<5	<20	55	<.01	<10	19	<10	49	98
459	L20N 14+ 75 E	<.2	1.07	20	125	<5	0.23	<1	16	22	19	3.75	<10	0.24	920	<1	0.02	23	1240	32	<5	<20	16	<.01	<10	28	<10	8	90
460	L20N 15+ 00 E	0.6	0.77	<5	130	<5	0.27	<1	4	10	6	1.08	<10	0.13	165	<1	0.02	6	510	10	<5	<20	18	<.01	<10	18	<10	3	35
461	L21N 10+ 25 E	<.2	1.52	20	125	5	0.10	<1	19	33	17	4.35	<10	0.36	384	<1	0.02	31	870	30	<5	<20	10	0.01	<10	36	<10	9	239
462	L21N 10+ 50 E	<.2	1.40	15	120	<5	0.21	4	20	25	20	3.54	<10	0.26	1578	<1	<.01	28	1090	108	<5	<20	24	0.01	<10	27	<10	7	627
463	L21N 10+ 75 E	<.2	0.65	10	155	5	0.35	<1	8	11	30	4.06	<10	0.15	319	2	<.01	13	2220	50	<5	<20	25	<.01	<10	31	<10	<1	138
464	L21N 11+ 00 E	<.2	1.18	25	40	5	0.23	<1	17	24	31	5.17	<10	0.35	488	3	<.01	27	1250	76	<5	<20	18	<.01	<10	27	<10	2	187
465	L21N 11+ 25 E	2.8	1.14	<5	145	<5	2.86	4	15	14	114	3.22	<10	0.25	1121	<1	<.01	44	2290	46	<5	<20	145	<.01	<10	14	<10	10	132
466	L21N 11+ 50 E	<.2	0.66	30	80	<5	0.06	<1	13	20	55	4.32	<10	0.09	318	6	0.02	29	1230	30	<5	<20	10	<.01	<10	45	<10	2	148
467	L21N 11+ 75 E	<.2	2.37	35	80	<5	0.23	<1	14	75	18	7.74	<10	0.89	768	<1	<.01	20	1910	18	<5	<20	16	0.01	<10	96	<10	<1	124
468	L21N 12+ 00 E	<.2	1.84	45	110	<5	0.09	1	24	54	31	10.20	<10	0.48	1146	1	<.01	25	1740	34	<5	<20	8	0.01	<10	57	<10	<1	110
469	L21N 12+ 25 E	1.6	1.13	15	130	<5	0.34	1	36	29	40	4.23	<10	0.23	582	2	0.04	30	1500	28	<5	<20	33	<.01	<10	26	<10	43	254
470	L21N 12+ 50 E	<.2	1.36	45	130	<5	0.20	<1	16	47	14	5.15	<10	0.18	277	1	<.01	37	950	22	<5	<20	18	<.01	<10	35	<10	<1	116
471	L21N 12+ 75 E	0.2	0.85	10	35	<5	0.08	<1	4	5	5	1.11	<10	0.04	149	<1	0.02	5	530	6	<5	<20	4	<.01	<10	16	<10	1	23
472	L21N 13+ 00 E	1.0	0.88	10	60	<5	0.08	<1	6	9	7	2.24	<10	0.04	462	<1	0.02	8	430	12	<5	<20	6	<.01	<10	35	<10	<1	33
473	L21N 13+ 25 E	<.2	1.15	15	70	<5	0.09	<1	5	14	7	2.47	<10	0.11	150	<1	0.02	7	910	16	<5	<20	9	0.01	<10	44	<10	<1	39
474	L21N 13+ 50 E	<.2	1.59	15	90	<5	0.07	<1	9	21	13	5.11	<10	0.25	178	<1	0.02	13	1680	20	<5	<20	8	<.01	<10	39	<10	<1	66
475	L1S: 14+ 75 E	0.6	1.07	10	80	<5	0.09	<1	5	38	13	2.99	<10	0.29	227	<1	0.02	11	1020	18	<5	<20	11	<.01	<10	49	<10	<1	46
476	L1S: 15+ 00 E	0.4	1.95	25	90	<5	0.67	3	31	51	67	4.41	<10	0.57	2805	2	0.05	27	3470	84	<5	<20	40	0.01	<10	39	<10	60	203
477	L1S: 15+ 25 E	1.2	1.88	50	85	<5	1.80	3	33	59	131	4.86	<10	0.63	2995	5	0.04	33	3220	20	<5	<20	68	0.01	<10	48	<10	42	156
478	L1S: 15+ 50 E	<.2	1.43	40	80	<5	0.06	<1	17	83	16	4.58	<10	0.60	1502	3	<.01	21	1220	16	<5	<20	8	0.01	<10	56	<10	<1	92
479	L1S: 15+ 75 E	0.2	0.95	10	65	<5	0.07	<1	4	27	6	1.65	<10	0.22	138	<1	0.02	6	710	12	<5	<20	11	<.01	<10	43	<10	2	30
480	L1S: 16+ 00 E	0.2	0.81	10	55	<5	0.05	<1	4	27	7	2.01	<10	0.15	173	1	0.02	7	1200	14	<5	<20	10	<.01	<10	41	<10	1	31
481	L1S: 16+ 25 E	1.0	0.76	<5	35	<5	0.07	<1	2	22	5	2.15	<10	0.16	106	<1	0.02	4	840	4	<5	<20	10	<.01	<10	31	<10	<1	25
482	L1S: 16+ 50 E	<.2	0.97	15	35	<5	0.05	<1	6	40	7	3.66	<10	0.28	297	<1	0.02	10	1140	14	<5	<20	10	0.01	<10	62	<10	<1	35
483	L1S: 16+ 75 E	<.2	0.85	10	35	<5	0.04	<1	5	28	5	2.74	<10	0.22	266	<1	0.02	7	710	10	<5	<20	8	0.01	<10	45	<10	<1	33
484	L1S: 17+ 00 E	<.2	1.11	10	30	<5	0.06	<1	6	37	7	3.58	<10	0.26	322	<1	0.02	9	760	12	<5	<20	7	0.03	<10	53	<10	<1	40
485	L1S: 17+ 25 E	<.2	1.05	10	35	<5	0.04	<1	5	32	5	4.25	<10	0.18	296	<1	0.01	6	930	12	<5	<20	8	0.01	<10	55	<10	<1	38
486	L1S: 17+ 50 E	<.2	0.77	5	45	<5	0.05	<1	5	28	5	2.47	<10	0.19	432	<1	0.02	6	1040	8	<5	<20	7	0.01	<10	43	<10	<1	35
487	L1S: 17+ 75 E	<.2	0.81	10	60	<5	0.10	<1	9	19	5	2.84	<10	0.20	592	<1	0.01	9	1130	12	<5	<20	11	<.01	<10	30	<10	<1	37
488	L1S: 18+ 00 E	<.2	0.83	10	45	<5	0.09	<1	7	31	5	2.69	<10	0.18	1033	<1	0.01	7	960	12	<5	<20	9	0.03	<10	56	<10	<1	44
489	L1S: 18+ 25 E	<.2	0.91	10	30	<5	0.08	<1	5	32	7	2.87	<10	0.23	194	<1	0.01	7	700	10	<5	<20	8	0.05	<10	53	<10	<1	37
490	L1S: 18+ 50 E	0.8	0.42	<5	25	<5	0.04	<1	2	16	3	1.06	<10	0.05	81	<1	0.02	2	510	6	<5	<20	7	0.01	<10	30	<10	1	20
491	L1S: 18+ 75 E	0.8	0.34	<5	25	<5	0.04	<1	1	11	3	0.47	<10	0.03	56	<1	0.02	1	310	6	<5	<20	7	0.02	<10	17	<10	2	13
492	L1S: 19+ 00 E	1.0	0.44	<5	50	<5	0.03	<1	5	19	6	1.44	<10	0.04	551	<1	0.02	5	430	8	<5	<20	7	0.02	<10	33	<10	1	30
493	L2S: 14+ 25 E	<.2	0.57	15	45	5	0.02	<1	8	10	8	2.92	<10	0.04	205	1	0.02	11	820	24	<5	<20	4	<.01	<10	30	<10	<1	38
494	L2S: 14+ 50 E	1.2	0.76	10	90	<5	0.02	<1	6	24	17	2.02	<10	0.09	146	3	0.01	9	1020	36	<5	<20	16	<.01	<10	37	<10	1	40
495	L2S: 14+ 75 E	1.0	1.49	20	190	<5	0.47	1	23	41	45	4.11	<10	0.47	2339	<1	<.01	26	2650	16	<5	<20	29	<.01	<10	33	<10	22	110
496	L2S: 15+ 00 E	0.8	1.85	45	85	<5	0.66	2	29	111	51	4.69	<10	0.91	1951	2	<.01	47	2670	20	<5	<20	30	0.01	<10	55	<10	18	110

TOKLAT RESOURCES INC. ETK 94-455 ECO-TECH LABORATORIES LTD.

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
497	L2S: 15+ 25 E	<.2	1.32	20	80	<5	0.38	1	24	39	41	3.47	<10	0.47	1356	2	0.01	20	2130	18	<5	<20	25	<.01	<10	36	<10	14	108
498	L2S: 15+ 50 E	0.4	1.49	20	85	<5	0.68	2	21	47	25	3.20	<10	0.51	1417	1	0.01	19	2030	10	<5	<20	32	0.01	<10	40	<10	9	94
499	L2S: 15+ 75 E	1.0	1.58	15	90	<5	0.72	3	16	38	34	2.82	<10	0.54	1261	<1	0.02	17	2120	8	<5	<20	32	0.01	<10	32	<10	18	120
500	L2S: 16+ 00 E	<.2	1.74	15	125	<5	0.33	3	30	44	18	3.87	<10	0.60	2377	3	0.01	21	2280	14	<5	<20	23	<.01	<10	42	<10	7	189
501	L2S: 16+ 25 E	0.4	1.60	20	55	5	0.08	1	28	38	34	2.74	<10	0.37	938	4	0.02	15	1120	8	<5	<20	12	0.02	<10	43	<10	8	79
502	L2S: 16+ 50 E	1.8	1.11	5	45	<5	0.04	<1	6	37	9	2.75	<10	0.32	329	<1	0.01	10	1080	6	<5	<20	12	<.01	<10	42	<10	<1	40
503	L2S: 16+ 75 E	0.8	1.35	10	50	<5	0.04	<1	9	64	12	3.41	<10	0.38	952	<1	0.01	13	1070	8	<5	<20	7	0.02	<10	64	<10	<1	42
504	L2S: 17+ 00 E	0.6	1.19	10	40	<5	0.03	<1	4	36	6	1.91	<10	0.23	236	<1	<.01	6	680	4	<5	<20	6	<.01	<10	40	<10	<1	26
505	L2S: 17+ 25 E	0.2	0.76	10	40	<5	0.05	<1	5	27	6	2.54	<10	0.17	717	<1	0.02	6	1120	12	<5	<20	7	0.01	<10	42	<10	<1	40
506	L2S: 17+ 50 E	0.2	0.76	5	40	<5	0.05	<1	5	28	6	1.90	<10	0.24	483	<1	0.02	7	870	6	<5	<20	6	0.01	<10	37	<10	<1	29
507	L2S: 17+ 75 E	0.2	0.72	10	35	<5	0.05	<1	4	33	6	2.47	<10	0.19	189	<1	0.01	8	880	10	<5	<20	7	0.01	<10	43	<10	<1	34
508	L2S: 18+ 00 E	<.2	1.09	10	35	<5	0.05	<1	14	22	8	2.63	<10	0.24	944	<1	<.01	9	1090	14	<5	<20	8	0.01	<10	32	<10	<1	44
509	L2S: 18+ 25 E	0.4	1.07	10	35	<5	0.05	<1	8	24	8	2.55	<10	0.22	778	<1	<.01	8	1000	8	<5	<20	7	0.02	<10	42	<10	<1	39
510	L2S: 18+ 50 E	0.4	0.80	5	40	<5	0.06	<1	6	19	4	2.59	<10	0.19	678	<1	<.01	6	1060	6	<5	<20	7	0.01	<10	35	<10	<1	34
511	L2S: 18+ 75 E	0.6	0.77	<5	75	<5	0.08	<1	7	16	5	2.80	<10	0.15	1138	<1	<.01	5	1110	<2	<5	<20	10	<.01	<10	30	<10	<1	46
512	L2S: 19+ 00 E	<.2	0.82	10	70	<5	0.10	<1	10	25	8	3.89	<10	0.17	1035	<1	<.01	9	1230	10	<5	<20	11	0.01	<10	43	<10	<1	52
513	L3S: 14+ 25 E	<.2	1.09	30	55	5	0.02	<1	15	50	28	6.61	<10	0.39	259	<1	0.01	27	1020	30	<5	<20	7	0.02	<10	47	<10	<1	105
514	L3S: 14+ 50 E	1.4	0.99	25	45	<5	0.02	<1	6	25	10	4.08	<10	0.14	376	<1	<.01	10	960	108	<5	<20	8	<.01	<10	41	<10	<1	50
515	L3S: 14+ 75 E	0.8	0.80	10	80	<5	0.03	<1	4	25	9	2.10	<10	0.17	117	<1	0.01	8	930	12	<5	<20	8	<.01	<10	34	<10	<1	28
516	L3S: 15+ 00 E	0.2	0.36	<5	45	5	0.06	<1	6	13	6	2.25	<10	0.08	270	<1	<.01	9	560	10	<5	<20	5	<.01	<10	19	<10	2	27
517	L3S: 15+ 25 E	1.2	1.21	40	70	<5	0.13	<1	15	36	14	4.24	<10	0.36	1379	2	<.01	17	1210	12	<5	<20	8	<.01	<10	40	<10	<1	75
518	L3S: 15+ 50 E	1.2	0.89	15	55	<5	0.05	<1	5	28	12	2.63	<10	0.21	187	1	<.01	9	650	8	<5	<20	7	<.01	<10	44	<10	<1	32
519	L3S: 15+ 75 E	2.0	0.81	5	40	<5	0.04	<1	4	26	12	2.72	<10	0.18	196	<1	<.01	8	890	4	<5	<20	5	<.01	<10	32	<10	<1	36
520	L3S: 16+ 00 E	1.0	0.89	30	50	<5	0.04	<1	14	27	17	4.00	<10	0.30	1208	4	0.01	13	920	18	<5	<20	7	0.01	<10	45	<10	<1	60
521	L3S: 16+ 25 E	2.4	1.39	15	70	<5	1.25	1	19	37	21	2.67	<10	0.35	1194	1	<.01	17	1950	6	<5	<20	43	0.01	<10	28	<10	10	92
522	L3S: 16+ 50 E	0.8	0.95	15	40	<5	0.05	<1	8	39	10	3.76	<10	0.27	716	<1	0.01	12	730	10	<5	<20	6	0.02	<10	48	<10	<1	38
523	L3S: 16+ 75 E	1.2	0.84	20	45	<5	0.05	<1	9	34	8	3.49	<10	0.22	1229	<1	<.01	9	830	8	<5	<20	5	0.02	<10	43	<10	<1	43
524	L3S: 17+ 00 E	1.0	0.61	5	30	<5	0.04	<1	5	27	5	1.91	<10	0.18	432	<1	0.01	6	700	4	<5	<20	5	<.01	<10	36	<10	<1	26
525	L3S: 17+ 25 E	1.2	0.55	<5	30	<5	0.04	<1	2	14	4	1.77	<10	0.08	163	<1	0.01	3	550	<2	<5	<20	5	<.01	<10	26	<10	<1	22
526	L3S: 17+ 50 E	1.0	0.71	15	50	<5	0.07	<1	8	22	7	2.68	<10	0.19	781	1	<.01	7	850	10	<5	<20	8	0.02	<10	38	<10	<1	36
527	L3S: 17+ 75 E	1.0	0.67	10	50	<5	0.11	<1	9	13	5	2.18	<10	0.15	721	<1	<.01	5	930	8	<5	<20	12	<.01	<10	26	<10	<1	33
528	L3S: 18+ 00 E	1.2	0.92	10	50	<5	0.32	<1	21	17	7	2.72	<10	0.21	1359	<1	0.02	8	1480	14	<5	<20	24	<.01	<10	30	<10	11	47
529	L3S: 18+ 25 E	1.2	0.85	15	55	<5	0.33	<1	14	21	7	2.85	<10	0.29	1214	<1	<.01	11	1730	10	<5	<20	25	<.01	<10	29	<10	3	58
530	L3S: 18+ 50 E	1.2	1.09	15	50	<5	0.27	<1	15	21	8	2.80	<10	0.26	1319	<1	<.01	12	1700	12	<5	<20	20	<.01	<10	28	<10	17	50
531	L3S: 18+ 75 E	0.4	0.61	15	65	<5	0.28	<1	17	15	9	2.52	<10	0.21	1314	<1	<.01	12	1420	10	<5	<20	23	<.01	<10	19	<10	7	59
532	L3S: 19+ 00 E	1.0	0.65	5	30	<5	0.05	<1	5	17	6	3.02	<10	0.17	422	<1	<.01	6	750	2	<5	<20	5	0.01	<10	24	<10	<1	35
533	L4S: 13+ 75 E	<.2	0.81	20	40	<5	0.03	<1	7	22	10	2.49	<10	0.16	291	<1	0.02	10	790	14	<5	<20	5	0.01	<10	39	<10	<1	31
534	L4S: 14+ 00 E	<.2	1.57	30	30	<5	0.07	<1	12	62	23	4.82	<10	0.51	328	<1	0.01	23	910	12	<5	<20	7	0.03	<10	47	<10	<1	62
535	L4S: 14+ 25 E	<.2	0.95	25	50	<5	0.06	<1	8	47	12	2.88	<10	0.33	476	<1	0.01	15	1010	14	<5	<20	7	0.02	<10	55	<10	<1	43

TOKLAT RESOURCES INC. ETK 94-455

ECO-TECH LABORATORIES LTD.

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
536	L4S: 14+ 50 E	<.2	1.82	35	45	<5	0.03	<1	10	79	12	4.16	<10	0.56	724	1	<.01	17	1280	14	<5	<20	5	0.01	<10	80	<10	<1	52
537	L4S: 14+ 75 E	0.8	1.46	35	60	<5	0.03	<1	14	58	24	3.98	<10	0.41	1119	<1	0.01	23	900	36	<5	<20	7	0.01	<10	63	<10	<1	71
538	L4S: 15+ 00 E	<.2	1.27	25	30	<5	0.04	<1	6	62	12	3.26	<10	0.43	275	<1	0.01	15	1030	12	<5	<20	6	0.01	<10	59	<10	<1	39
539	L4S: 15+ 25 E	<.2	1.37	25	45	<5	0.04	<1	9	67	12	3.32	<10	0.46	944	<1	0.01	16	900	10	<5	<20	6	0.02	<10	61	<10	<1	48
540	L4S: 15+ 50 E	<.2	1.46	30	50	<5	0.04	<1	11	70	16	3.77	<10	0.49	1084	1	0.01	18	960	12	<5	<20	7	0.02	<10	64	<10	<1	52
541	L4S: 15+ 75 E	<.2	1.23	20	45	<5	0.04	<1	6	57	12	3.05	<10	0.36	582	1	0.01	12	990	10	<5	<20	7	0.01	<10	47	<10	<1	42
542	L4S: 16+ 00 E	1.2	1.27	25	35	<5	0.05	<1	7	63	14	3.29	<10	0.37	394	2	0.01	15	1630	10	<5	<20	7	0.02	<10	54	<10	<1	45
543	L4S: 16+ 25 E	<.2	3.17	80	45	<5	0.03	1	30	108	28	7.38	<10	1.32	1867	2	<.01	32	2080	8	<5	<20	4	0.02	<10	101	<10	<1	101
544	L4S: 16+ 50 E	<.2	1.01	20	30	<5	0.04	<1	5	34	10	3.52	<10	0.19	178	<1	0.01	9	1340	16	<5	<20	6	<.01	<10	45	<10	<1	37
545	L4S: 16+ 75 E	<.2	1.03	20	30	<5	0.05	<1	7	34	9	3.49	<10	0.21	526	<1	0.01	9	900	10	<5	<20	6	0.02	<10	45	<10	<1	40
546	L4S: 17+ 00 E	<.2	1.23	20	30	<5	0.04	<1	11	42	14	4.79	<10	0.28	1053	<1	0.01	11	1900	12	<5	<20	6	0.03	<10	49	<10	<1	56
547	L4S: 17+ 25 E	<.2	1.21	25	30	<5	0.05	<1	11	47	13	4.18	<10	0.33	1090	<1	0.02	15	1200	14	<5	<20	6	0.03	<10	52	<10	<1	46
548	L4S: 17+ 50 E	<.2	1.17	25	30	<5	0.04	<1	9	37	10	4.29	<10	0.24	678	<1	0.01	9	950	14	<5	<20	6	0.02	<10	47	<10	<1	46
549	L4S: 17+ 75 E	<.2	1.15	25	30	<5	0.05	<1	12	36	9	4.28	<10	0.28	1390	<1	0.02	11	1390	14	<5	<20	5	0.02	<10	41	<10	<1	50
550	L4S: 18+ 00 E	<.2	0.93	20	25	<5	0.04	<1	5	28	5	2.92	<10	0.19	248	<1	0.02	7	680	10	<5	<20	5	0.01	<10	40	<10	<1	30
551	L4S: 18+ 25 E	0.2	0.93	20	45	<5	0.04	<1	11	30	8	3.65	<10	0.16	2068	<1	0.01	7	1110	16	<5	<20	6	0.01	<10	48	<10	<1	41
552	L4S: 18+ 50 E	<.2	0.98	20	50	<5	0.07	<1	14	34	10	4.15	<10	0.19	2174	<1	0.01	9	1290	16	<5	<20	7	0.02	<10	52	<10	<1	49
553	L4S: 18+ 75 E	<.2	0.88	15	95	<5	0.06	<1	12	29	9	4.19	<10	0.11	3709	<1	<.01	7	1320	18	<5	<20	6	0.01	<10	42	<10	<1	59
554	L4S: 19+ 00 E	<.2	1.03	25	35	<5	0.07	<1	9	37	9	4.03	<10	0.24	611	<1	0.02	9	1090	14	<5	<20	7	0.02	<10	51	<10	<1	53
555	L20N 5+ 00 E	<.2	1.44	30	120	5	0.59	1	20	46	16	4.41	<10	0.39	1367	3	0.02	22	1420	28	<5	<20	25	0.01	<10	36	<10	7	113
556	L20N 5+ 25 E	0.6	1.97	40	245	<5	1.85	2	23	56	39	5.47	<10	0.34	3330	3	0.02	37	1670	42	<5	<20	57	0.01	<10	40	<10	16	169
557	L20N 5+ 50 E	<.2	1.29	40	110	<5	0.18	<1	14	45	14	4.51	<10	0.36	431	3	0.02	19	860	28	<5	<20	10	0.01	<10	39	<10	<1	94
558	L20N 5+ 75 E	<.2	1.07	35	100	<5	0.91	<1	20	41	20	4.39	<10	0.28	872	3	0.02	24	700	26	<5	<20	32	<.01	<10	33	<10	3	80
559	L20N 6+ 00 E	0.6	0.45	10	80	<5	7.20	2	9	18	13	1.45	<10	0.14	341	2	<.01	13	1180	8	<5	<20	173	<.01	<10	12	<10	6	73
560	L20N 6+ 25 E	<.2	1.07	25	55	<5	0.63	2	11	28	9	3.57	<10	0.23	212	2	<.01	10	990	18	<5	<20	30	<.01	<10	34	<10	<1	57
561	L20N 6+ 50 E	<.2	0.96	20	80	<5	0.16	<1	5	22	5	2.35	<10	0.18	98	<1	0.03	7	810	8	<5	<20	12	<.01	<10	35	<10	<1	36
562	L20N 6+ 75 E	0.6	0.77	15	80	<5	0.11	<1	6	24	8	2.29	<10	0.24	189	<1	0.02	9	1080	12	<5	<20	7	0.01	<10	38	<10	<1	41
563	L20N 7+ 00 E	<.2	2.97	40	140	<5	0.13	<1	24	157	24	5.77	<10	1.98	430	<1	<.01	40	1740	16	<5	<20	7	0.03	<10	139	<10	<1	208
564	L20N 7+ 25 E	<.2	1.12	20	110	<5	1.21	<1	12	24	11	2.71	<10	0.31	1284	<1	0.01	13	1040	12	<5	<20	44	0.01	<10	25	<10	<1	83
565	L20N 7+ 50 E	<.2	1.24	20	130	<5	2.04	<1	19	33	14	2.88	<10	0.42	1774	1	0.01	17	1370	14	<5	<20	73	0.02	<10	27	<10	3	84
566	L20N 7+ 75 E	<.2	2.59	30	105	<5	0.19	<1	25	45	26	3.30	<10	0.59	260	<1	0.02	33	1040	18	<5	<20	13	0.01	<10	31	<10	4	73
567	L20N 8+ 00 E	<.2	0.78	15	45	<5	0.04	<1	4	13	5	1.41	<10	0.11	79	<1	0.03	6	460	10	<5	<20	5	0.02	<10	36	<10	<1	21
568	L20N 8+ 25 E	<.2	1.30	35	75	<5	0.05	<1	10	32	14	4.22	<10	0.23	389	<1	0.01	13	1300	18	<5	<20	6	0.03	<10	50	<10	<1	56
569	L20N 8+ 50 E	<.2	0.78	20	80	<5	0.14	<1	6	20	7	2.69	<10	0.16	276	<1	0.02	8	800	14	<5	<20	8	0.03	<10	46	<10	<1	36
570	L20N 8+ 75 E	<.2	1.62	60	90	<5	1.01	1	40	36	24	6.07	<10	0.18	1254	4	0.03	64	2070	22	<5	<20	15	0.01	<10	32	<10	34	94
571	L20N 9+ 00 E	<.2	1.38	25	75	<5	0.16	1	15	24	10	3.31	<10	0.12	130	1	0.02	25	450	8	<5	<20	5	0.01	<10	50	<10	<1	42
572	L20N 9+ 25 E	<.2	1.19	30	75	5	0.10	<1	25	60	28	6.77	<10	0.15	331	<1	0.02	86	1490	10	<5	<20	7	<.01	<10	44	<10	<1	74
573	L20N 9+ 50 E	<.2	0.36	10	25	<5	0.04	<1	6	5	6	2.07	<10	0.02	117	<1	0.05	10	390	4	<5	<20	4	<.01	<10	18	<10	1	18
574	L20N 9+ 75 E	1.8	0.57	30	130	<5	0.37	<1	27	14	11	5.69	<10	0.05	>10000	3	<.01	24	1450	128	<5	<20	23	0.01	<10	29	<10	<1	103

TOKLAT RESOURCES INC. ETK 94-455 ECO-TECH LABORATORIES LTD.

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
575	L22N 5+ 00 E	<.2	1.60	30	80	<5	0.80	<1	18	37	25	4.53	<10	0.52	955	<1	0.01	24	1050	28	<5	<20	29	0.01	<10	27	<10	4	105
576	L22N 5+ 25 E	<.2	1.79	40	45	<5	0.06	<1	14	45	19	5.95	<10	0.69	624	1	0.01	20	1020	24	<5	<20	4	<.01	<10	31	<10	<1	76
577	L22N 5+ 50 E	0 2	2 24	40	100	<5	0 36	<1	29	49	43	5.85	<10	0.67	1504	1	0.02	44	930	46	<5	<20	19	0.01	<10	30	<10	17	119
578	L22N 5+ 75 E	<.2	1.21	15	60	<5	0 03	2	5	30	3	2.23	<10	0.52	144	<1	0.02	6	360	22	<5	<20	4	0.01	<10	29	<10	<1	42
579	L22N 6+ 00 E	< 2	1.69	25	60	<5	0 04	<1	9	37	7	3.95	<10	0.71	313	<1	0.01	11	550	46	<5	<20	4	0.01	<10	46	<10	<1	63
580	L22N 6+ 25 E	< 2	1 89	30	60	<5	0 05	<1	12	40	13	4 79	<10	0 91	700	<1	0.01	14	840	14	<5	<20	4	<.01	<10	37	<10	<1	75
581	L22N 6+ 50 E	< 2	2 49	35	65	<5	0 07	<1	15	48	18	4 86	<10	1.21	470	<1	0.01	22	1230	10	<5	<20	4	<.01	<10	31	<10	<1	83
582	L22N 6+ 75 E	< 2	1 22	50	45	<5	0 26	<1	26	28	53	7 70	<10	0.19	599	<1	0 03	54	1830	20	<5	<20	7	< 01	<10	26	<10	13	60
583	L22N 7+ 00 E	<.2	2.47	40	110	5	0.59	<1	24	41	44	7 25	<10	0.38	1719	<1	0.02	33	1610	14	<5	<20	13	0.01	<10	33	<10	12	100
584	L22N 7+ 25 E	<.2	1.62	40	130	<5	0 65	<1	27	37	21	6 28	<10	0.25	1546	1	<.01	22	1710	18	<5	<20	12	0.01	<10	50	<10	<1	106
585	L22N 7+ 50 E	<.2	2.10	35	125	<5	0 16	<1	20	44	27	5 73	<10	0 44	525	<1	0.02	31	970	10	<5	<20	7	<.01	<10	41	<10	5	92
586	L22N 7+ 75 E	< 2	1 34	35	130	<5	0 57	<1	15	27	15	5 35	<10	0.16	607	2	0.02	17	920	20	<5	<20	18	0.01	<10	42	<10	<1	63
587	L22N 8+ 00 E	< 2	1.81	30	125	<5	0 13	<1	13	37	20	4 85	<10	0 44	258	<1	0 01	26	1030	16	<5	<20	10	<.01	<10	28	<10	<1	77
588	L22N 8+ 25 E	<.2	1.75	40	120	<5	0 13	<1	14	39	22	4.98	<10	0.43	277	1	0.01	27	1010	20	<5	<20	10	<.01	<10	32	<10	<1	80
589	L22N 8+ 50 E	0 4	1 09	45	85	5	0 60	1	30	21	20	6.67	<10	0.12	3558	1	<.01	34	2230	32	<5	<20	14	0.01	<10	31	<10	1	110
590	L22N 8+ 75 E	0 4	0 67	75	200	<5	0 53	1	21	24	19	8.23	<10	0.09	7563	<1	< 01	34	4530	62	<5	<20	15	0.01	<10	32	<10	<1	168
591	L22N 9+ 00 E	< 2	1.37	60	115	<5	0 12	<1	16	34	28	5.83	<10	0.22	584	1	<.01	39	1510	98	<5	<20	10	0.01	<10	37	<10	<1	304
592	L22N 9+ 25 E	< 2	1 12	35	145	<5	0 26	<1	16	25	20	5 19	<10	0.17	744	1	0.01	20	990	66	<5	<20	22	0.01	<10	31	<10	<1	185
593	L22N 9+ 50 E	< 2	1 02	30	125	<5	1 17	4	23	28	63	4 57	<10	0.49	1110	<1	<.01	48	1370	46	<5	<20	57	<.01	<10	21	<10	4	735
594	L22N 9+ 75 E	< 2	0 90	10	135	5	1 23	4	23	24	56	4 28	<10	0.43	987	<1	<.01	72	1270	52	<5	<20	73	<.01	<10	18	<10	3	923
595	L22N 10+ 25 E	0 8	1.20	30	120	<5	1 19	1	18	26	48	3 87	<10	0 26	1146	2	< 01	22	1680	48	<5	<20	66	0 01	<10	27	<10	4	118
596	L22N 10+ 50 E	< 2	1 85	25	70	<5	0 07	<1	9	30	25	3 96	<10	0 25	144	<1	0.01	13	950	24	<5	<20	12	0 01	<10	38	<10	<1	81
597	L22N 10+ 75 E	1 0	1.22	20	60	<5	2 35	2	15	28	67	3 08	<10	0.33	511	<1	<.01	28	1560	32	<5	<20	108	<.01	<10	16	<10	19	151
598	L22N 11+ 00 E	<.2	1 20	30	60	<5	1 08	2	20	22	41	3 85	<10	0.36	575	2	0.01	28	1000	30	<5	<20	60	0.01	<10	20	<10	11	143
599	L22N 11+ 25 E	0 6	1.35	25	50	<5	1 90	3	9	23	60	3 34	<10	0.29	145	<1	0.06	31	1730	14	<5	<20	109	<.01	<10	17	<10	62	118
600	L22N 11+ 50 E	0.4	1.30	25	55	<5	1 35	2	12	23	48	4.41	<10	0.24	340	1	0.06	31	1710	14	<5	<20	90	< 01	<10	19	<10	62	129
601	L22N 11+ 75 E	<.2	0.38	30	40	<5	0.39	<1	10	16	60	3.30	<10	0.07	138	2	0.02	23	960	22	<5	<20	36	<.01	<10	35	<10	<1	89
602	L22N 12+ 00 E	<.2	1.39	30	50	<5	0 87	<1	15	39	26	4 48	<10	0.44	332	1	0.02	30	1050	22	<5	<20	59	< 01	<10	29	<10	11	89
603	L22N 12+ 25 E	2.2	0.68	<5	45	<5	2.94	<1	20	3	59	0 63	<10	0.17	531	<1	0.09	31	1260	4	<5	<20	179	<.01	<10	3	<10	95	44
604	L22N 12+ 50 E	0.6	2.40	40	110	<5	0 31	<1	47	27	117	4 91	<10	0 24	779	<1	0.02	37	2020	52	<5	<20	26	0.02	<10	31	<10	2	106
605	L22N 12+ 75 E	<.2	1 60	25	105	<5	0 13	<1	11	19	51	4 06	<10	0 24	263	<1	0.01	14	1370	38	<5	<20	18	<.01	<10	27	<10	<1	69
606	L22N 13+ 00 E	<.2	0 85	15	115	<5	0 26	<1	6	7	90	1 88	<10	0.08	292	<1	<.01	6	610	34	<5	<20	20	<.01	<10	22	<10	<1	73
607	L22N 13+ 25 E	<.2	1 88	25	185	<5	0 19	<1	13	20	37	3.80	<10	0 31	344	<1	0.01	16	1250	34	<5	<20	22	0.02	<10	30	<10	<1	98
608	L22N 13+ 50 E	1.0	2.45	20	140	<5	0 64	<1	30	19	57	3.47	<10	0.28	1234	<1	0.03	29	1750	34	<5	<20	49	<.01	<10	18	<10	42	136
609	L22N 13+ 75 E	0.4	1.65	15	110	<5	0 87	<1	16	18	56	2.99	<10	0.31	261	<1	0.03	34	1900	24	<5	<20	59	<.01	<10	16	<10	67	131
610	L22N 14+ 00 E	<.2	0.82	10	125	<5	0 13	<1	6	8	36	1.67	<10	0.10	182	<1	0.02	8	630	16	<5	<20	11	0.01	<10	31	<10	<1	54
611	L22N 14+ 25 E	<.2	0 81	20	125	<5	0.13	<1	7	11	27	2.08	<10	0.10	174	1	0.02	9	680	20	<5	<20	11	0.01	<10	41	<10	<1	50
612	L22N 14+ 50 E	<.2	0.94	10	230	<5	0.21	<1	5	6	47	1.54	<10	0.23	942	<1	0.02	5	410	6	<5	<20	12	0.03	<10	31	<10	<1	85
613	L22N 14+ 75 E	<.2	0.75	20	55	<5	0 08	<1	18	15	43	5.05	<10	0.11	787	<1	<.01	22	900	22	<5	<20	10	< 01	<10	31	<10	<1	79

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
614	L22N 15+ 00 E	<.2	1.02	5	50	<5	0.02	<1	7	14	47	2.52	<10	0.08	203	<1	0.02	14	490	12	<5	<20	5	0.02	<10	53	<10	<1	54
615	L23N 10+ 25 E	<.2	1.31	15	155	<5	1.08	3	23	25	76	4.22	<10	0.30	2157	<1	0.02	36	2560	30	<5	<20	69	<.01	<10	27	<10	30	155
616	L23N 10+ 50 E	<.2	1.31	20	75	<5	1.18	2	21	38	35	4.33	<10	0.46	844	<1	0.02	43	1420	32	<5	<20	73	<.01	<10	33	<10	20	170
617	L23N 10+ 75 E	<.2	1.68	30	90	<5	0.60	1	29	58	42	5.78	<10	0.50	1201	<1	0.03	52	1610	44	<5	<20	50	<.01	<10	46	<10	26	190
618	L23N 11+ 00 E	<.2	1.49	20	80	<5	0.25	<1	21	48	37	5.74	<10	0.44	530	<1	0.02	38	1300	42	<5	<20	30	<.01	<10	38	<10	<1	154
619	L23N 11+ 25 E	<.2	1.77	30	85	<5	1.51	1	29	44	48	5.44	<10	0.52	750	<1	0.03	50	1430	40	<5	<20	97	<.01	<10	35	<10	25	178
620	L23N 11+ 50 E	<.2	0.75	25	45	<5	0.14	<1	11	19	38	5.23	<10	0.11	329	<1	0.02	23	940	52	<5	<20	22	0.01	<10	41	<10	<1	81
621	L23N 11+ 75 E	<.2	0.95	10	125	<5	0.11	<1	10	15	23	3.65	<10	0.19	661	<1	0.02	13	740	40	<5	<20	19	0.01	<10	36	<10	<1	87
622	L23N 12+ 00 E	<.2	1.38	25	145	<5	0.11	<1	22	28	34	4.88	<10	0.33	549	<1	0.03	26	800	44	<5	<20	16	0.02	<10	40	<10	10	114
623	L23N 12+ 25 E	<.2	0.52	10	115	<5	4.12	<1	9	14	29	2.26	<10	0.21	314	<1	0.02	22	1290	14	<5	<20	236	<.01	<10	28	<10	23	83
624	L23N 12+ 50 E	2.0	4.94	45	195	<5	1.51	1	36	39	72	4.97	<10	0.32	1145	<1	0.03	111	4190	56	<5	<20	118	0.02	<10	30	<10	139	316
625	L23N 12+ 75 E	<.2	2.40	25	180	<5	0.22	<1	50	33	44	5.24	<10	0.31	1734	<1	0.04	31	2920	82	<5	<20	32	0.01	<10	44	<10	106	191
626	L23N 13+ 00 E	<.2	0.93	15	165	<5	0.24	<1	8	11	30	2.41	<10	0.19	142	<1	0.02	8	680	12	<5	<20	18	0.03	<10	46	<10	<1	72
627	L23N 13+ 25 E	<.2	1.15	15	180	<5	0.16	<1	14	11	22	3.27	<10	0.15	1487	<1	0.01	9	1050	30	<5	<20	16	0.02	<10	48	<10	<1	113
628	L23N 13+ 50 E	<.2	1.72	15	215	<5	0.16	1	14	22	29	4.75	<10	0.16	409	<1	0.03	17	1130	26	<5	<20	28	<.01	<10	41	<10	6	110
629	L23N 13+ 75 E	<.2	1.18	20	120	<5	0.23	1	9	18	29	4.26	<10	0.16	201	<1	0.01	17	890	28	<5	<20	24	0.01	<10	45	<10	<1	86
630	L23N 14+ 00 E	<.2	1.49	20	150	<5	0.10	<1	15	21	30	4.62	<10	0.17	591	<1	0.01	19	960	58	<5	<20	12	0.01	<10	47	<10	<1	90
631	L23N 14+ 25 E	<.2	1.38	20	150	<5	0.10	<1	14	20	25	4.20	<10	0.16	515	<1	0.01	18	900	52	<5	<20	12	0.01	<10	48	<10	<1	91
632	L23N 14+ 50 E	<.2	0.99	20	75	<5	0.05	<1	12	7	33	3.83	<10	0.12	432	<1	0.01	15	1540	22	<5	<20	9	<.01	<10	38	<10	<1	67
633	L23N 14+ 75 E	<.2	1.45	15	60	<5	0.05	<1	6	12	14	2.80	<10	0.25	255	<1	0.02	5	590	8	<5	<20	9	<.01	<10	28	<10	<1	42
634	L23N 15+ 00 E	<.2	3.12	<5	50	<5	0.10	<1	18	38	49	7.77	<10	0.46	302	<1	<.01	24	1310	<2	<5	<20	17	<.01	<10	25	<10	<1	114
635	BL10+00 10+00N	<.2	0.90	5	300	<5	0.62	1	8	9	59	2.42	<10	0.12	347	1	0.02	23	740	14	<5	<20	29	<.01	<10	27	<10	8	56
636	BL10+00 10+25N	<.2	1.69	20	245	<5	1.72	2	20	26	76	3.91	<10	0.27	1687	2	0.02	37	1610	20	<5	<20	72	<.01	<10	25	<10	15	102
637	BL10+00 10+50N	<.2	0.47	10	260	<5	0.23	<1	8	6	24	2.24	<10	0.07	235	<1	0.02	16	600	14	<5	<20	17	<.01	<10	25	<10	<1	63
638	BL10+00 10+75N	<.2	1.43	25	220	<5	0.66	1	19	22	33	3.84	<10	0.36	1300	3	0.02	25	1550	18	<5	<20	44	<.01	<10	30	<10	6	125
639	BL10+00 11+00N	<.2	1.09	15	170	<5	0.76	<1	22	17	36	4.31	<10	0.20	2531	2	0.01	29	1460	26	<5	<20	43	<.01	<10	26	<10	<1	146
640	BL10+00 11+25N	<.2	1.92	15	105	<5	0.06	1	14	23	34	4.36	<10	0.26	450	<1	0.02	20	910	8	<5	<20	10	<.01	<10	32	<10	<1	86
641	BL10+00 11+50N	<.2	0.90	10	120	<5	0.07	<1	6	10	17	2.53	<10	0.17	194	<1	0.02	10	930	12	<5	<20	10	0.01	<10	31	<10	<1	46
642	BL10+00 11+75N	<.2	2.91	25	170	<5	0.12	1	18	33	55	4.96	<10	0.33	979	<1	0.01	40	1280	10	<5	<20	13	0.01	<10	37	<10	<1	149
643	BL10+00 12+00N	<.2	1.28	10	125	<5	0.24	<1	11	17	30	4.91	<10	0.30	478	<1	0.01	18	1310	14	<5	<20	17	0.01	<10	30	<10	<1	77
644	BL10+00 12+25N	<.2	0.79	10	70	<5	0.04	<1	6	9	11	2.49	<10	0.20	139	<1	0.02	8	1050	10	<5	<20	10	0.02	<10	31	<10	<1	37
645	BL10+00 12+50N	<.2	1.00	15	105	<5	[illegible]	1	9	17	22	3.48	<10	0.25	227	<1	0.02	16	690	10	<5	<20	10	0.01	<10	35	<10	<1	72
646	BL10+00 12+75N	<.2	1.24	15	90	<5	0.06	<1	7	25	13	3.85	<10	0.31	152	<1	0.02	13	1030	12	<5	<20	9	0.02	<10	39	<10	<1	54
647	BL10+00 13+00N	<.2	1.29	25	65	<5	[illegible]	1	7	42	13	3.12	<10	0.43	99	2	0.01	20	1070	14	<5	<20	8	0.01	<10	52	<10	<1	58
648	BL10+00 13+25N	<.2	1.30	20	80	<5	0.16	2	12	35	23	4.03	<10	0.41	272	1	<.01	25	1270	12	<5	<20	8	0.01	<10	54	<10	<1	92
649	BL10+00 13+50N	<.2	0.84	20	170	<5	0.92	1	30	23	37	5.32	<10	0.20	1246	<1	<.01	50	1640	8	<5	<20	29	0.02	<10	45	<10	<1	124
650	BL10+00 13+75N	<.2	0.97	15	155	<5	0.34	<1	20	33	32	4.98	<10	0.23	1530	1	<.01	49	1070	28	<5	<20	15	0.01	<10	72	<10	<1	198
651	BL10+00 14+00N	<.2	2.14	35	205	<5	0.08	2	17	66	36	5.70	<10	0.53	359	<1	<.01	44	1110	24	<5	<20	9	<.01	<10	73	<10	<1	186
652	BL10+00 14+25N	<.2	3.05	20	155	<5	0.87	2	17	40	15	4.80	<10	0.22	1524	<1	<.01	26	1930	40	<5	<20	42	0.01	<10	46	<10	4	352

Et #	Tag #		Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
653	BL10+00	14+50N	<.2	0.99	15	115	<5	0.09	<1	11	35	21	3.13	<10	0.50	437	<1	0.01	24	540	8	<5	<20	8	0.02	<10	86	<10	<1	79
654	BL10+00	14+75N	<.2	0.59	30	65	<5	0.07	<1	15	21	40	3.74	<10	0.19	418	2	0.02	25	950	20	<5	<20	7	0.05	<10	93	<10	<1	90
655	BL10+00	15+00N	<.2	1.15	30	105	<5	0.14	<1	15	44	28	4.50	<10	0.49	772	<1	0.01	26	1920	22	<5	<20	11	0.04	<10	82	<10	<1	107
656	BL10+00	15+25N	<.2	1.08	15	105	<5	0.05	<1	7	18	12	3.25	<10	0.26	479	<1	0.01	11	1160	8	<5	<20	8	0.01	<10	31	<10	<1	80
657	BL10+00	15+50N	<.2	0.69	5	65	<5	0.04	<1	2	6	5	1.57	<10	0.08	49	<1	0.02	2	820	10	<5	<20	6	0.01	<10	26	<10	<1	21
658	BL10+00	15+75N	<.2	1.29	15	70	<5	0.66	<1	8	22	15	3.71	<10	0.35	255	<1	0.01	13	1150	12	<5	<20	7	0.01	<10	37	<10	<1	53
659	BL10+00	16+00N	<.2	0.70	10	70	<5	0.12	<1	6	12	11	2.17	<10	0.21	191	<1	0.02	9	860	12	<5	<20	9	0.01	<10	33	<10	<1	46
660	BL10+00	16+25N	<.2	1.59	10	105	<5	0.27	<1	16	26	19	3.47	<10	0.52	665	<1	0.01	19	960	12	<5	<20	17	<.01	<10	32	<10	<1	83
661	BL10+00	16+50N	<.2	2.54	20	95	<5	0.36	<1	11	38	25	3.55	<10	0.81	263	<1	<.01	18	1000	<2	<5	<20	25	0.01	<10	45	<10	<1	86
662	BL10+00	16+75N	<.2	3.09	10	120	<5	0.09	<1	24	45	66	3.70	<10	0.96	662	<1	<.01	53	1250	18	<5	<20	9	<.01	<10	36	<10	<1	160
663	BL10+00	17+00N	<.2	1.64	25	105	<5	0.03	<1	11	37	16	4.67	<10	0.49	566	<1	0.01	17	1860	12	<5	<20	6	<.01	<10	47	<10	<1	88
664	BL10+00	17+25N	<.2	1.55	15	85	<5	0.03	<1	9	22	17	3.52	<10	0.40	646	<1	0.01	13	1410	6	<5	<20	5	<.01	<10	39	<10	<1	72
665	BL10+00	17+50N	<.2	1.05	10	85	<5	0.07	<1	5	10	14	2.59	<10	0.22	109	<1	<.01	9	1390	8	<5	<20	7	<.01	<10	21	<10	<1	40
666	BL10+00	17+75N	<.2	1.11	30	115	<5	0.12	<1	15	42	16	5.33	<10	0.54	509	2	0.02	24	2200	24	<5	<20	13	0.01	<10	48	<10	<1	90
667	BL10+00	18+00N	<.2	1.03	20	135	<5	0.07	<1	13	32	46	5.21	<10	0.36	876	<1	0.02	14	1330	22	<5	<20	8	<.01	<10	44	<10	<1	87
668	BL10+00	18+25N	<.2	1.42	20	115	<5	0.11	<1	10	39	13	5.72	<10	0.45	442	<1	0.02	13	1750	16	<5	<20	9	<.01	<10	50	<10	<1	75
669	BL10+00	18+50N	<.2	0.99	25	70	<5	0.12	<1	8	28	15	4.88	<10	0.29	178	<1	0.02	9	1250	18	<5	<20	8	0.02	<10	55	<10	<1	62
670	BL10+00	18+75N	<.2	1.15	25	135	<5	0.06	<1	12	35	44	4.89	<10	0.45	532	<1	0.02	17	1350	16	<5	<20	7	0.01	<10	45	<10	<1	84
671	BL10+00	19+00N	<.2	0.63	10	70	<5	0.02	<1	4	6	57	1.32	<10	0.12	89	<1	0.02	6	500	12	<5	<20	5	<.01	<10	28	<10	<1	46
672	BL10+00	19+25N	<.2	0.53	15	90	<5	0.07	<1	11	14	36	3.66	<10	0.13	1582	<1	0.02	20	1240	18	<5	<20	7	0.01	<10	37	<10	<1	59
673	BL10+00	19+50N	1.6	1.75	50	620	15	2.88	3	22	26	23	6.40	<10	0.07	>10000	3	0.02	47	2810	140	<5	<20	137	0.02	<10	34	<10	8	146
674	BL10+00	19+75N	<.2	1.40	110	145	<5	1.20	2	33	57	57	8.90	<10	0.16	1215	7	<.01	87	6570	256	<5	<20	43	0.01	<10	69	<10	<1	496
675	BL10+00	20+00N	<.2	1.05	60	170	<5	0.15	<1	34	134	50	8.22	<10	0.39	970	<1	0.01	94	2410	70	<5	<20	9	0.03	<10	113	<10	<1	163
676	BL10+00	20+25N	<.2	1.54	75	215	10	0.35	1	30	80	33	9.03	<10	0.36	1735	<1	<.01	80	2570	74	<5	<20	13	0.01	<10	82	<10	<1	518
677	BL10+00	20+50N	<.2	1.62	45	135	<5	0.27	2	22	53	35	7.71	<10	0.27	1200	<1	<.01	38	3100	64	<5	<20	13	0.02	<10	89	<10	<1	489
678	BL10+00	20+75N	0.8	1.30	40	440	<5	3.16	3	26	29	24	6.09	<10	0.20	>10000	<1	0.01	42	3070	92	<5	<20	158	0.02	<10	38	<10	15	407
679	BL10+00	21+00N	1.4	1.63	20	2465	5	1.74	2	35	58	30	6.04	<10	0.23	>10000	<1	0.01	34	2910	26	<5	<20	104	0.02	<10	63	<10	23	440
680	BL10+00	21+25N	<.2	1.55	25	200	<5	0.45	1	29	42	19	5.99	<10	0.34	1938	<1	0.02	38	1350	18	<5	<20	36	0.01	<10	48	<10	<1	439
681	BL10+00	21+50N	<.2	0.79	60	190	<5	0.26	1	18	28	20	5.85	<10	0.10	468	<1	0.01	55	1520	20	<5	<20	18	<.01	<10	55	<10	<1	289
682	BL10+00	21+75N	<.2	0.61	20	115	<5	1.87	6	29	16	41	4.19	<10	0.28	1415	<1	<.01	55	1550	40	<5	<20	89	<.01	<10	19	<10	7	1001
683	BL10+00	22+00N	<.2	1.29	25	190	<5	1.88	4	23	37	47	4.74	<10	0.44	1110	<1	<.01	47	1490	40	<5	<20	91	<.01	<10	39	<10	8	509
684	BL10+00	22+25N	<.2	1.25	20	110	<5	1.55	1	13	31	31	4.34	<10	0.29	567	<1	0.01	24	1600	28	<5	<20	82	<.01	<10	39	<10	3	108
685	BL10+00	22+50N	<.2	1.43	40	155	<5	2.10	2	28	53	42	4.62	<10	0.57	1178	2	0.02	42	1710	50	<5	<20	105	0.02	<10	48	<10	13	184
686	BL10+00	22+75N	<.2	1.32	25	140	<5	2.15	2	24	40	51	4.10	<10	0.51	1042	<1	0.02	39	1540	46	<5	<20	109	0.01	<10	37	<10	11	170
687	BL10+00	23+00N	<.2	0.38	15	65	<5	0.60	<1	7	15	30	2.73	<10	0.07	192	1	0.02	17	1000	42	<5	<20	48	0.01	<10	43	<10	<1	77
688	BL10+00	23+25N	<.2	1.01	40	70	<5	0.52	1	19	40	31	5.32	<10	0.29	674	2	0.02	29	1780	54	<5	<20	45	0.01	<10	54	<10	2	130
689	BL10+00	23+50N	<.2	1.40	30	85	<5	0.34	1	29	55	37	6.15	<10	0.36	2769	<1	0.02	39	2620	62	<5	<20	30	<.01	<10	54	<10	21	194
690	BL10+00	23+75N	<.2	1.10	95	80	<5	0.44	1	43	78	70	7.37	<10	0.29	2181	2	0.03	72	2850	60	<5	<20	49	0.01	<10	57	<10	28	159
691	BL10+00	24+00N	<.2	0.97	25	85	<5	0.42	1	15	36	36	4.55	<10	0.17	544	1	0.03	27	1650	50	<5	<20	46	<.01	<10	52	<10	18	128

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
692	BL10+00 24+25N	0.6	0.97	30	160	5	1.15	2	18	27	28	4.70	<10	0.21	1694	<1	0.02	25	2250	50	<5	<20	42	<.01	<10	43	<10	<1	137
693	BL10+00 24+50N	<.2	0.75	20	170	<5	0.44	<1	11	25	31	3.82	<10	0.21	590	<1	0.02	19	1970	44	<5	<20	30	<.01	<10	37	<10	<1	113
694	BL10+00 24+75N	<.2	1.37	25	155	<5	1.79	2	23	30	43	4.31	<10	0.32	1227	2	0.02	37	1830	48	<5	<20	107	0.01	<10	36	<10	23	185
695	BL10+00 25+00N	<.2	1.27	40	95	<5	0.13	2	25	45	47	5.35	<10	0.40	1342	2	0.02	45	1270	74	<5	<20	16	<.01	<10	44	<10	<1	162
696	BL10+00 25+25N	<.2	1.36	35	130	<5	0.32	1	22	43	53	6.00	<10	0.37	922	<1	0.02	42	4020	54	<5	<20	27	<.01	<10	45	<10	<1	174
697	BL10+00 25+50N	<.2	1.21	30	105	<5	0.18	<1	21	46	46	5.26	<10	0.49	730	<1	0.02	42	1290	50	<5	<20	20	0.01	<10	42	<10	<1	153
698	BL10+00 25+75N	<.2	1.15	25	135	<5	1.65	<1	19	32	37	4.11	<10	0.39	925	<1	0.02	31	1490	46	<5	<20	103	<.01	<10	36	<10	15	109
699	BL10+00 26+00N	<.2	0.82	25	175	<5	0.26	1	14	29	25	4.81	<10	0.24	704	<1	0.03	24	1730	50	<5	<20	26	0.01	<10	47	<10	<1	88
700	BL16+00 8+25N	<.2	0.47	60	460	<5	0.27	4	53	5	184	8.07	<10	0.07	4384	4	0.02	107	3470	206	<5	<20	97	<.01	<10	23	<10	54	531
701	BL16+00 8+50N	<.2	1.28	30	95	<5	0.08	<1	11	45	33	4.44	<10	0.24	459	1	0.02	25	2060	74	<5	<20	22	<.01	<10	46	<10	<1	92
702	BL16+00 8+75N	<.2	0.90	25	145	<5	0.07	<1	5	21	17	2.72	<10	0.11	144	<1	0.02	14	2170	58	<5	<20	21	<.01	<10	41	<10	<1	53
703	BL16+00 9+00N	<.2	0.97	50	115	<5	0.17	1	15	27	54	6.44	<10	0.15	564	<1	0.01	54	2780	86	<5	<20	20	<.01	<10	28	<10	<1	165
704	BL16+00 9+25N	<.2	0.93	45	385	<5	0.18	1	30	31	64	5.38	<10	0.24	4558	1	0.02	50	2070	90	<5	<20	30	<.01	<10	34	<10	7	178
705	BL16+00 9+50N	<.2	0.83	30	130	<5	0.12	<1	18	37	22	5.55	<10	0.23	1152	<1	0.02	28	2690	60	<5	<20	14	<.01	<10	55	<10	<1	108
706	BL16+00 9+75N	<.2	0.95	25	195	<5	0.16	<1	12	37	20	4.46	<10	0.29	678	<1	0.03	21	2170	42	<5	<20	19	<.01	<10	34	<10	<1	85
707	BL16+00 10+00N	<.2	1.22	30	470	5	0.54	<1	20	58	33	6.30	<10	0.44	849	<1	0.02	35	1960	58	<5	<20	31	<.01	<10	59	<10	<1	139
708	BL16+00 10+25N	<.2	0.70	25	190	<5	0.26	1	11	30	30	3.98	<10	0.20	338	<1	0.03	23	1550	50	<5	<20	21	<.01	<10	40	<10	<1	95
709	BL16+00 10+50N	<.2	1.01	25	175	<5	1.04	<1	17	32	20	4.37	<10	0.38	694	<1	0.02	26	1490	40	<5	<20	68	<.01	<10	30	<10	6	120
710	BL16+00 10+75N	<.2	1.34	30	220	<5	1.01	<1	29	43	29	5.43	<10	0.38	1363	<1	0.02	35	1490	58	<5	<20	55	<.01	<10	44	<10	9	185
711	BL16+00 11+00N	<.2	0.97	25	160	<5	1.65	<1	26	31	23	4.56	<10	0.38	1056	<1	0.01	27	1550	42	<5	<20	71	<.01	<10	26	<10	4	159
712	L26N 7+ 25 E	<.2	1.39	20	260	<5	0.27	1	21	40	37	5.58	<10	0.44	1227	<1	0.01	42	2160	48	<5	<20	25	0.01	<10	50	<10	<1	186
713	L26N 7+ 50 E	<.2	1.49	35	165	<5	0.33	1	20	42	37	5.55	<10	0.38	1057	2	0.02	39	2030	66	<5	<20	28	<.01	<10	42	<10	25	170
714	L26N 7+ 75 E	<.2	0.99	25	115	<5	0.26	1	14	34	28	4.94	<10	0.31	633	2	0.02	33	1730	50	<5	<20	24	0.01	<10	47	<10	<1	124
715	L26N 8+ 00 E	1.2	0.66	20	195	<5	0.11	<1	7	5	15	2.21	<10	0.14	613	2	0.01	10	730	32	<5	<20	10	<.01	<10	28	<10	<1	66
716	L26N 8+ 25 E	0.2	2.15	60	355	5	0.51	1	18	20	34	4.66	<10	0.40	863	4	0.01	28	1840	36	<5	<20	23	<.01	<10	29	<10	<1	156
717	L26N 8+ 50 E	1.2	1.74	35	165	<5	0.15	1	17	16	49	4.12	<10	0.40	685	2	0.01	30	1180	32	<5	<20	15	0.01	<10	28	<10	<1	127
718	L26N 8+ 75 E	0.4	1.63	50	120	<5	0.15	<1	21	32	35	5.06	<10	0.36	1118	2	0.02	34	1810	54	<5	<20	13	<.01	<10	36	<10	2	164
719	L26N 9+ 00 E	1.0	1.66	40	100	<5	0.19	1	19	20	51	4.18	<10	0.35	872	1	0.01	33	1230	50	<5	<20	16	<.01	<10	25	<10	4	159
720	L26N 9+ 25 E	0.4	0.98	50	95	<5	0.18	<1	12	15	21	4.22	<10	0.25	486	2	0.01	20	2590	62	<5	<20	17	<.01	<10	29	<10	<1	90
721	L26N 9+ 50 E	0.4	1.14	20	95	<5	1.04	<1	8	8	39	2.03	<10	0.30	258	<1	0.01	18	850	28	<5	<20	74	<.01	<10	14	<10	4	71
722	L26N 9+ 75 E	1.0	1.21	20	105	<5	0.74	<1	11	8	62	2.81	<10	0.31	297	<1	<.01	20	810	32	<5	<20	56	<.01	<10	14	<10	<1	101
723	L26N 10+ 25 E	<.2	0.80	30	155	<5	0.05	<1	9	8	31	4.33	<10	0.15	408	<1	0.01	19	1030	46	<5	<20	8	<.01	<10	25	<10	<1	76
724	L26N 10+ 50 E	<.2	1.80	55	125	<5	0.30	<1	19	26	35	4.79	<10	0.36	1206	4	0.03	25	1480	42	<5	<20	26	0.01	<10	37	<10	20	108
725	L26N 10+ 75 E	<.2	1.39	35	110	<5	0.51	<1	15	19	23	4.46	<10	0.37	620	<1	0.02	18	1130	32	<5	<20	36	<.01	<10	26	<10	9	76
726	L26N 11+ 00 E	<.2	1.51	40	75	<5	0.26	<1	17	28	20	5.83	<10	0.44	448	1	0.02	21	1100	40	<5	<20	23	<.01	<10	33	<10	1	96
727	L26N 11+ 25 E	<.2	1.50	35	70	<5	0.10	<1	15	18	21	4.48	<10	0.36	495	<1	0.02	14	780	28	<5	<20	12	0.01	<10	29	<10	2	63
728	L26N 11+ 50 E	<.2	1.23	25	65	<5	0.09	<1	19	24	18	4.73	<10	0.44	460	<1	0.02	19	500	30	<5	<20	10	0.01	<10	31	<10	<1	69
729	L26N 11+ 75 E	<.2	0.87	15	95	<5	0.16	<1	4	5	6	1.73	<10	0.15	105	<1	0.02	3	630	20	<5	<20	11	<.01	<10	29	<10	<1	32
730	L26N 12+ 00 E	0.2	0.92	25	100	<5	0.06	<1	7	14	8	4.03	<10	0.25	291	<1	0.02	7	1170	26	<5	<20	7	<.01	<10	39	<10	<1	48

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
731	L26N 12+ 25 E	0.8	0.69	25	175	5	0.17	<1	17	10	17	3.31	<10	0.14	3006	2	0.02	7	980	38	<5	<20	12	<.01	<10	41	<10	<1	58
732	L26N 12+ 50 E	0.2	1.55	40	90	<5	0.26	<1	20	27	39	4.99	<10	0.53	503	<1	0.02	28	1100	34	<5	<20	22	0.03	<10	36	<10	6	90
733	L26N 12+ 75 E	<.2	1.06	35	180	<5	0.12	<1	12	22	72	5.21	<10	0.30	678	<1	0.02	14	1930	36	<5	<20	14	<.01	<10	48	<10	<1	83
734	L26N 13+ 00 E	0.2	1.68	45	140	<5	0.08	<1	17	30	27	5.60	<10	0.48	788	<1	0.02	23	1140	36	<5	<20	10	<.01	<10	34	<10	4	105
735	L26N 13+ 25 E	<.2	1.01	30	115	<5	0.28	<1	13	18	24	4.57	<10	0.32	609	<1	0.03	13	900	28	<5	<20	22	<.01	<10	33	<10	<1	71
736	L26N 13+ 50 E	<.2	1.67	40	70	<5	0.08	<1	15	28	29	6.16	<10	0.38	644	<1	0.02	20	1010	40	<5	<20	14	<.01	<10	37	<10	<1	101
737	L26N 13+ 75 E	0.8	1.43	30	115	<5	0.60	<1	16	20	23	4.87	<10	0.40	820	<1	0.02	16	1310	30	<5	<20	53	<.01	<10	30	<10	2	78
738	L26N 14+ 00 E	<.2	1.55	35	85	5	0.64	<1	18	23	22	4.68	<10	0.49	722	2	0.03	21	970	30	<5	<20	53	0.01	<10	32	<10	10	81
739	L26N 14+ 25 E	0.4	1.19	25	55	<5	0.04	<1	6	11	19	4.94	<10	0.24	216	<1	0.02	7	900	30	<5	<20	7	<.01	<10	29	<10	<1	49
740	L26N 14+ 50 E	<.2	1.70	30	70	<5	0.06	<1	11	17	17	4.14	<10	0.40	446	<1	0.02	10	1010	22	<5	<20	9	<.01	<10	28	<10	<1	58
741	L26N 14+ 75 E	<.2	0.99	15	95	<5	0.20	<1	8	4	14	2.51	<10	0.31	273	<1	0.02	7	560	20	<5	<20	18	<.01	<10	18	<10	<1	41
742	L26N 15+ 00 E	<.2	2.18	40	90	<5	0.10	<1	15	27	22	5.46	<10	0.65	413	<1	0.02	21	1550	20	<5	<20	11	0.01	<10	28	<10	<1	75
743	L23N 5+ 00 E	1.0	1.39	50	65	<5	0.09	<1	20	21	39	4.97	<10	0.38	934	3	0.01	29	830	40	<5	<20	7	<.01	<10	26	<10	<1	88
744	L23N 5+ 25 E	1.8	1.44	35	160	<5	0.72	1	15	19	26	4.44	<10	0.37	3424	1	<.01	19	1330	42	<5	<20	37	<.01	<10	19	<10	<1	121
745	L23N 5+ 50 E	<.2	0.92	30	65	<5	0.17	<1	7	18	12	3.29	<10	0.30	229	2	0.01	10	670	32	<5	<20	9	<.01	<10	33	<10	<1	51
746	L23N 5+ 75 E	0.8	1.55	45	95	<5	0.90	<1	23	23	68	5.22	<10	0.60	985	2	0.01	34	960	40	<5	<20	29	<.01	<10	25	<10	<1	115
747	L23N 6+ 00 E	<.2	1.92	45	65	<5	0.05	<1	15	27	34	6.17	<10	0.50	476	<1	0.01	24	850	60	<5	<20	5	<.01	<10	31	<10	<1	112
748	L23N 6+ 25 E	0.2	2.60	40	95	<5	0.09	<1	15	23	45	4.72	<10	0.57	413	<1	<.01	25	910	58	<5	<20	8	<.01	<10	26	<10	<1	152
749	L23N 6+ 50 E	0.4	2.06	50	90	<5	0.03	<1	10	36	17	7.09	<10	0.47	320	2	<.01	10	800	46	<5	<20	5	0.01	<10	51	<10	<1	103
750	L23N 6+ 75 E	1.2	2.06	35	160	<5	0.95	<1	13	16	49	4.54	<10	0.45	685	1	0.01	24	1040	62	<5	<20	26	<.01	<10	22	<10	<1	157
751	L23N 7+ 00 E	1.0	3.20	75	110	<5	0.25	1	36	32	53	9.05	<10	0.63	716	<1	0.03	42	1830	24	<5	<20	10	<.01	<10	42	<10	<1	143
752	L23N 7+ 25 E	<.2	2.68	55	190	<5	0.41	<1	19	30	23	6.26	<10	0.43	694	<1	<.01	22	1010	18	<5	<20	11	<.01	<10	42	<10	<1	100
753	L23N 7+ 50 E	0.2	2.29	40	70	<5	0.26	<1	17	19	23	5.87	<10	0.33	520	<1	<.01	21	1350	16	<5	<20	8	<.01	<10	32	<10	<1	89
754	L23N 7+ 75 E	0.4	2.15	55	85	<5	0.13	1	18	32	30	7.50	<10	0.41	521	2	<.01	25	1020	28	<5	<20	8	<.01	<10	40	<10	<1	115
755	L23N 8+ 00 E	0.2	0.90	30	60	<5	0.09	<1	9	6	23	4.38	<10	0.16	329	<1	<.01	14	1870	28	<5	<20	6	<.01	<10	22	<10	<1	45
756	L23N 8+ 25 E	<.2	1.25	30	50	<5	0.03	<1	11	10	21	4.81	<10	0.16	561	<1	0.01	14	830	26	<5	<20	5	<.01	<10	27	<10	<1	54
757	L23N 8+ 50 E	<.2	1.00	30	130	<5	1.09	<1	9	7	34	3.52	<10	0.28	303	<1	<.01	12	880	36	<5	<20	59	<.01	<10	19	<10	<1	229
758	L23N 8+ 75 E	1.0	0.95	35	185	<5	1.81	3	16	15	63	4.36	<10	0.31	1206	2	<.01	28	1230	48	<5	<20	83	<.01	<10	25	<10	3	609
759	L23N 9+ 00 E	<.2	1.32	40	130	<5	0.44	2	21	14	174	4.83	<10	0.35	888	1	<.01	37	1150	44	<5	<20	33	<.01	<10	24	<10	<1	252
760	L23N 9+ 25 E	0.6	1.24	30	85	<5	0.60	<1	18	9	36	4.34	<10	0.29	650	<1	<.01	19	1430	36	<5	<20	41	<.01	<10	21	<10	<1	127
761	L23N 9+ 50 E	0.4	1.38	<5	75	<5	0.23	2	14	24	70	4.84	10	0.21	387	1	<.01	28	1190	40	<5	<20	13	<.01	<10	29	<10	9	129
762	L23N 9+ 75 E	0.6	1.90	<5	85	5	0.23	2	30	33	43	5.86	<10	0.34	1393	<1	<.01	41	1710	40	<5	<20	16	0.01	<10	29	<10	8	192
763	L24N 5+ 00 E	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
764	L24N 5+ 25 E	0.4	1.92	5	55	10	0.22	<1	15	29	<1	5.16	<10	0.92	724	<1	<.01	24	950	12	<5	<20	8	<.01	<10	26	<10	<1	93
765	L24N 5+ 50 E	0.2	1.02	10	45	<5	0.07	<1	9	18	<1	4.31	<10	0.35	261	<1	<.01	16	750	10	<5	<20	<1	<.01	<10	23	<10	<1	58
766	L24N 5+ 75 E	0.4	1.91	5	70	<5	0.24	1	31	28	52	6.23	30	0.85	1351	<1	<.01	58	960	34	<5	<20	8	<.01	<10	22	<10	11	120
767	L24N 6+ 00 E	0.4	1.75	5	75	<5	0.15	<1	23	26	31	4.95	20	0.75	1191	<1	<.01	41	910	24	<5	<20	7	<.01	<10	21	<10	7	101
768	L24N 6+ 25 E	0.4	1.80	<5	80	<5	0.16	<1	23	24	40	5.58	30	0.72	665	<1	<.01	49	970	98	<5	<20	5	<.01	<10	22	<10	9	107
769	L24N 6+ 50 E	<.2	1.11	<5	70	5	0.06	<1	11	18	1	5.16	<10	0.28	304	<1	<.01	22	1150	20	<5	<20	<1	<.01	<10	23	<10	<1	81

TOKLAT RESOURCES INC. ETK 94-455 | ECO-TECH LABORATORIES LTD.

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
770	L24N 6+ 75 E	<.2	1.26	<5	55	<5	0.11	<1	10	18	<1	4.69	<10	0.31	223	<1	<.01	24	840	24	<5	<20	2	<.01	<10	21	<10	<1	85
771	L24N 7+ 00 E	0.2	1.50	<5	85	<5	0.07	<1	8	21	<1	4.05	<10	0.19	302	<1	<.01	11	630	18	<5	<20	<1	<.01	<10	35	<10	<1	95
772	L24N 7+ 25 E	0.4	1.88	<5	110	10	0.70	2	23	29	8	7.77	20	0.54	1447	<1	<.01	41	2360	18	<5	<20	11	0.01	<10	38	<10	8	258
773	L24N 7+ 50 E	0.2	1.81	10	95	10	0.40	1	24	27	12	7.40	20	0.34	705	<1	<.01	55	1170	12	<5	<20	3	<.01	<10	33	<10	9	89
774	L24N 7+ 75 E	0.2	1.56	<5	70	10	0.15	<1	26	24	7	7.82	30	0.23	934	<1	<.01	38	1180	10	<5	<20	1	<.01	<10	30	<10	9	75
775	L24N 8+ 00 E	0.4	1.42	<5	75	5	0.19	<1	15	21	<1	4.69	<10	0.19	783	<1	<.01	23	1480	6	<5	<20	<1	<.01	<10	26	<10	2	109
776	L24N 8+ 25 E	0.4	1.54	<5	165	5	0.54	1	20	21	7	4.99	10	0.39	705	<1	<.01	46	1090	24	<5	<20	24	<.01	<10	21	<10	6	332
777	L24N 8+ 50 E	0.2	1.39	5	160	<5	0.74	3	22	25	30	5.20	<10	0.34	1122	<1	<.01	56	1310	36	<5	<20	45	<.01	<10	24	<10	6	430
778	L24N 8+ 75 E	0.4	1.25	<5	140	<5	0.14	<1	10	19	<1	5.26	<10	0.17	290	<1	<.01	18	1620	34	<5	<20	3	<.01	<10	28	<10	<1	89
779	L24N 9+ 00 E	2.0	1.08	20	120	<5	2.61	5	12	3	228	2.30	<10	0.32	967	<1	0.01	35	1820	44	<5	<20	132	<.01	<10	11	<10	22	202
780	L24N 9+ 25 E	1.2	0.20	<5	90	<5	4.44	1	5	<1	44	0.70	<10	0.25	1440	2	<.01	5	1370	24	<5	<20	189	<.01	<10	2	<10	3	158
781	L24N 9+ 50 E	0.2	1.90	<5	75	5	0.09	1	30	40	47	6.32	40	0.35	1224	<1	<.01	50	2210	52	<5	<20	12	0.01	<10	34	<10	23	204
782	L24N 9+ 75 E	0.4	1.73	10	280	5	0.56	2	35	67	60	7.32	10	0.76	1523	7	<.01	98	1930	76	<5	<20	30	0.03	<10	47	<10	10	264
783	L24N 10+ 25 E	0.4	1.53	<5	60	5	0.27	2	21	31	30	5.62	10	0.31	854	<1	<.01	46	1320	34	<5	<20	18	0.01	<10	33	<10	7	159
784	L24N 10+ 50 E	0.2	1.00	<5	70	<5	0.59	1	13	23	29	4.62	20	0.12	330	<1	<.01	33	1120	24	<5	<20	40	0.01	<10	33	<10	8	107
785	L24N 10+ 75 E	0.4	0.90	<5	65	<5	2.70	1	8	10	11	1.93	30	0.23	515	<1	<.01	37	1430	8	<5	<20	155	<.01	<10	11	<10	23	98
786	L24N 11+ 00 E	0.6	0.75	<5	65	<5	1.34	2	7	10	26	2.28	20	0.05	158	<1	<.01	46	970	14	<5	<20	77	<.01	<10	17	<10	13	65
787	L24N 11+ 25 E	0.6	0.28	<5	30	<5	1.22	<1	4	<1	59	0.70	<10	0.14	89	<1	<.01	1	1200	26	<5	<20	80	<.01	<10	6	<10	6	103
788	L24N 11+ 50 E	<.2	0.72	<5	35	<5	0.45	<1	10	26	15	4.14	10	0.16	225	<1	<.01	25	1180	14	<5	<20	28	0.02	<10	42	<10	1	76
789	L24N 11+ 75 E	1.2	1.55	<5	105	<5	0.52	<1	9	18	37	3.24	20	0.20	168	<1	<.01	30	1530	58	<5	<20	43	0.02	<10	18	<10	22	96
790	L24N 12+ 00 E	1.0	1.68	<5	105	<5	0.44	<1	10	22	24	3.65	20	0.25	207	<1	<.01	32	1500	60	<5	<20	40	0.02	<10	22	<10	19	104
791	L24N 12+ 25 E	<.2	1.08	<5	80	<5	0.14	<1	10	17	21	4.07	<10	0.20	161	<1	<.01	22	760	30	<5	<20	18	<.01	<10	23	<10	1	101
792	L24N 12+ 50 E	0.2	1.23	<5	70	5	0.15	<1	10	19	11	4.69	10	0.20	151	<1	<.01	24	910	40	<5	<20	14	<.01	<10	22	<10	3	98
793	L24N 12+ 75 E	0.6	0.99	<5	125	<5	2.99	<1	66	6	15	1.21	70	0.21	794	<1	<.01	20	1690	20	<5	<20	175	<.01	<10	5	<10	38	90
794	L24N 13+ 00 E	<.2	1.00	<5	135	<5	0.83	<1	21	15	21	4.14	10	0.11	1505	<1	<.01	30	1310	42	<5	<20	48	0.01	<10	29	<10	8	101
795	L24N 13+ 25 E	0.2	1.54	<5	140	5	0.91	<1	28	13	4	3.54	<10	0.24	874	<1	<.01	16	990	36	<5	<20	55	0.02	<10	26	<10	7	84
796	L24N 13+ 50 E	<.2	1.67	<5	100	5	0.08	<1	9	19	<1	4.24	10	0.26	232	<1	<.01	15	1040	22	<5	<20	6	<.01	<10	28	<10	<1	66
797	L24N 13+ 75 E	0.2	1.06	<5	75	5	0.51	<1	7	14	<1	2.99	20	0.26	134	<1	<.01	12	790	4	<5	<20	48	<.01	<10	22	<10	1	48
798	L24N 14+ 00 E	<.2	0.83	5	60	<5	0.05	<1	7	13	<1	2.96	20	0.12	187	<1	<.01	12	640	6	<5	<20	2	0.02	<10	34	<10	1	53
799	L24N 14+ 25 E	0.4	1.28	<5	65	<5	0.07	<1	9	17	4	3.83	20	0.18	239	<1	<.01	15	820	8	<5	<20	4	<.01	<10	24	<10	4	47
800	L24N 14+ 50 E	0.2	1.10	<5	75	5	0.05	<1	8	15	<1	4.28	10	0.17	319	<1	<.01	13	780	8	<5	<20	1	<.01	<10	27	<10	<1	49
801	L24N 14+ 75 E	<.2	2.09	<5	60	<5	0.03	<1	12	21	<1	5.36	10	0.34	275	<1	<.01	18	1100	6	<5	<20	<1	<.01	<10	23	<10	<1	67
802	L24N 15+ 00 E	0.2	1.42	<5	55	<5	0.01	<1	11	18	<1	4.22	10	0.25	553	<1	<.01	14	770	2	<5	<20	2	<.01	<10	29	<10	<1	57
803	L25N 6+ 25 E	0.4	1.42	<5	220	10	0.70	1	18	21	3	7.97	<10	0.33	3080	<1	<.01	23	2090	44	<5	<20	16	0.01	<10	32	<10	1	168
804	L25N 6+ 50 E	1.0	1.09	<5	270	10	2.94	2	17	16	5	8.84	<10	0.33	5633	<1	<.01	37	2050	14	<5	<20	32	0.01	<10	24	<10	9	184
805	L25N 6+ 75 E	<.2	2.00	<5	110	10	0.27	<1	15	24	<1	5.51	<10	0.23	704	<1	<.01	26	900	72	<5	<20	10	<.01	<10	26	<10	2	124
806	L25N 7+ 00 E	<.2	0.79	<5	55	<5	0.11	<1	4	12	<1	2.86	<10	0.08	115	<1	<.01	6	470	24	<5	<20	4	<.01	<10	37	<10	<1	39
807	L25N 7+ 25 E	<.2	0.90	<5	70	5	0.57	<1	15	17	<1	4.75	<10	0.13	710	<1	<.01	18	1350	64	<5	<20	17	<.01	<10	29	<10	<1	192
808	L25N 7+ 50 E	0.2	1.31	<5	130	<5	0.47	1	21	21	14	5.35	10	0.31	715	<1	<.01	46	1220	38	<5	<20	26	<.01	<10	21	<10	7	387

Et #	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
809	L25N 7+ 75 E	0.2	1.39	<5	165	<5	0.58	2	22	23	26	5.78	10	0.34	984	<1	<.01	58	1230	50	<5	<20	22	0.01	<10	24	<10	9	189
810	L25N 8+ 00 E	0.2	1.03	<5	235	<5	1.27	2	17	19	39	3.80	<10	0.34	590	<1	<.01	52	1300	30	<5	<20	79	<.01	<10	17	<10	9	173
811	L25N 8+ 25 E	<.2	1.03	5	90	5	0.12	<1	10	17	2	4.10	<10	0.14	210	<1	<.01	26	630	22	<5	<20	11	<.01	<10	29	<10	<1	104
812	L25N 8+ 50 E	<.2	0.75	<5	95	<5	0.04	3	7	11	<1	2.37	20	0.09	141	<1	<.01	20	590	14	<5	<20	10	<.01	<10	21	<10	<1	54
813	L25N 8+ 75 E	<.2	1.04	5	100	10	0.06	1	13	23	5	5.49	<10	0.23	361	<1	<.01	32	2200	40	<5	<20	12	0.01	<10	30	<10	<1	102
814	L25N 9+ 00 E	0.4	1.35	10	100	<5	0.24	2	26	26	32	6.08	10	0.32	819	1	<.01	59	1430	50	<5	<20	17	<.01	<10	25	<10	8	219
815	L25N 9+ 25 E	<.2	1.17	<5	120	<5	0.46	<1	13	21	2	3.97	10	0.37	305	<1	<.01	34	780	22	<5	<20	25	0.01	<10	21	<10	2	128
816	L25N 9+ 50 E	0.4	1.74	<5	145	5	0.44	2	23	32	29	5.26	20	0.35	1034	<1	<.01	49	1310	42	<5	<20	36	0.01	<10	30	<10	16	173
817	L25N 9+ 75 E	0.4	1.84	<5	80	<5	0.24	2	23	30	42	5.92	20	0.26	834	<1	<.01	51	1450	44	<5	<20	19	0.01	<10	30	<10	20	191
818	L25N 10+ 25 E	0.2	1.61	10	110	<5	0.30	<1	23	33	24	5.59	20	0.41	1096	<1	<.01	49	1930	46	<5	<20	29	0.01	<10	30	<10	10	162
819	L25N 10+ 50 E	0.2	1.25	<5	85	<5	0.64	1	16	23	19	4.69	10	0.28	577	<1	<.01	38	900	24	<5	<20	42	0.01	<10	26	<10	10	107
820	L25N 10+ 75 E	0.2	0.95	5	60	10	0.84	<1	12	20	11	4.24	<10	0.23	252	<1	<.01	28	730	18	<5	<20	59	<.01	<10	25	<10	4	107
821	L25N 11+ 00 E	0.2	1.32	<5	50	<5	0.81	<1	10	20	7	3.01	20	0.24	175	<1	<.01	26	1160	16	<5	<20	65	<.01	<10	20	<10	22	63
822	L25N 11+ 25 E	<.2	1.57	<5	85	<5	0.49	<1	16	24	4	4.54	20	0.33	595	<1	<.01	28	1190	20	<5	<20	35	0.01	<10	28	<10	8	87
823	L25N 11+ 50 E	<.2	0.74	<5	55	<5	0.15	<1	6	14	<1	3.00	10	0.09	121	<1	<.01	14	1210	4	<5	<20	11	<.01	<10	29	<10	<1	42
824	L25N 11+ 75 E	<.2	1.55	<5	75	5	0.25	<1	16	21	5	4.22	20	0.31	586	<1	<.01	32	890	16	<5	<20	17	0.01	<10	26	<10	8	84
825	L25N 12+ 00 E	0.2	1.48	<5	65	<5	0.22	<1	14	20	38	4.00	<10	0.29	369	<1	<.01	22	1030	22	<5	<20	12	<.01	<10	24	<10	5	92
826	L25N 12+ 25 E	<.2	1.73	<5	65	<5	0.07	<1	11	21	6	5.03	<10	0.31	208	<1	<.01	20	630	10	<5	<20	4	0.01	<10	24	<10	<1	67
827	L25N 12+ 50 E	<.2	0.82	<5	45	<5	0.04	<1	6	13	<1	2.44	20	0.12	168	<1	<.01	11	640	4	<5	<20	1	<.01	<10	23	<10	1	54
828	L25N 12+ 75 E	<.2	1.07	<5	90	<5	<.01	<1	6	13	<1	2.89	20	0.20	318	<1	<.01	10	920	4	<5	<20	<1	<.01	<10	21	<10	<1	52
829	L25N 13+ 00 E	0.4	1.88	<5	90	<5	0.02	<1	12	25	12	5.55	<10	0.21	357	<1	<.01	22	2260	50	<5	<20	2	0.01	<10	32	<10	<1	105
830	L25N 13+ 25 E	<.2	0.60	<5	35	<5	0.06	<1	6	10	<1	2.34	20	0.04	133	<1	<.01	13	890	8	<5	<20	6	<.01	<10	22	<10	1	46
831	L25N 13+ 50 E	<.2	1.36	<5	155	<5	0.08	<1	17	21	9	4.95	<10	0.20	478	<1	<.01	27	1190	30	<5	<20	11	<.01	<10	27	<10	3	102
832	L25N 13+ 75 E	<.2	1.62	5	55	5	0.06	<1	20	32	12	6.29	<10	0.34	726	<1	<.01	40	1260	38	<5	<20	2	<.01	<10	30	<10	2	131
833	L25N 14+ 00 E	0.2	1.70	<5	70	5	0.69	<1	16	20	2	4.16	20	0.38	702	<1	<.01	25	1040	12	<5	<20	50	<.01	<10	24	<10	10	73
834	L25N 14+ 25 E	0.2	1.59	<5	60	<5	0.35	<1	13	18	6	3.71	30	0.27	354	<1	<.01	25	910	10	<5	<20	32	<.01	<10	20	<10	16	60
835	L25N 14+ 50 E	0.4	1.74	<5	60	10	0.25	<1	18	21	7	4.41	30	0.40	508	<1	<.01	33	750	6	<5	<20	18	<.01	<10	24	<10	13	68
836	L25N 14+ 75 E	<.2	1.37	<5	120	5	0.16	<1	9	19	<1	5.05	<10	0.24	158	<1	<.01	16	540	8	<5	<20	8	0.01	<10	33	<10	<1	49
837	L25N 15+ 00 E	<.2	1.79	<5	50	5	0.25	<1	17	23	1	4.64	20	0.54	503	<1	<.01	25	710	4	<5	<20	15	0.01	<10	25	<10	4	66

QC DATA:		Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
Repeat:																													
1	L9N: 14+ 00 E	<.2	1.88	40	225	<5	0.26	<1	21	46	43	5.23	<10	0.30	1110	1	0.02	30	2630	28	<5	<20	14	0.01	<10	44	<10	<1	125
39	L10N 18+ 75 E	<.2	2.01	75	130	<5	0.24	<1	22	73	38	7.00	<10	0.38	756	<1	<.01	32	1530	60	<5	<20	16	<.01	<10	39	<10	<1	265
77	L16N 9+ 00 E	<.2	3.06	50	115	<5	0.10	<1	20	107	18	7.71	<10	1.01	340	2	0.03	25	2160	8	<5	<20	8	0.02	<10	117	<10	<1	91
115	L17N 8+ 50 E	0.6	1.18	10	45	<5	0.06	<1	10	23	<1	4.13	<10	0.30	394	<1	0.02	12	1240	16	<5	<20	5	0.01	<10	32	<10	<1	55
153	L18N 8+ 00 E	1.2	0.76	<5	100	<5	0.06	<1	3	12	6	1.43	<10	0.15	98	<1	0.02	4	650	6	<5	<20	7	<.01	<10	20	<10	1	26
191	L19N 7+ 50 E	0.2	1.47	5	75	<5	0.17	<1	15	20	48	3.16	<10	0.38	440	<1	0.01	15	840	12	<5	<20	18	0.01	<10	22	<10	5	54
229	L11N 12+ 25 E	<.2	0.97	20	50	<5	0.11	<1	13	20	20	5.21	<10	0.09	336	<1	<.01	25	1450	24	<5	<20	7	0.01	<10	36	<10	<1	73
267	L13N 11+ 75 E	0.8	1.85	10	50	<5	0.02	<1	7	27	9	2.60	<10	0.60	280	<1	0.01	8	720	2	<5	<20	4	<.01	<10	33	<10	<1	42
305	L14N 11+ 25 E	<.2	0.76	15	50	<5	0.04	<1	4	23	4	2.20	<10	0.19	163	<1	0.02	7	490	14	<5	<20	7	<.01	<10	28	<10	<1	26
343	L12N 10+ 75 E	0.2	1.94	30	60	<5	0.06	1	12	31	15	5.00	<10	0.36	187	1	0.02	24	720	26	<5	<20	7	<.01	<10	22	<10	<1	85
381	L10N 10+ 25 E	0.6	0.69	20	130	<5	0.42	<1	12	18	12	3.56	<10	0.16	763	1	0.02	18	650	24	<5	<20	18	<.01	<10	29	<10	<1	60
419	L15N 9+ 50 E	0.4	2.10	10	95	<5	0.10	<1	16	92	20	5.40	<10	1.36	342	1	0.01	22	1240	6	<5	<20	7	0.03	<10	64	<10	<1	85
457	L20N 14+ 25 E	<.2	1.27	10	80	<5	0.06	<1	5	13	7	2.46	<10	0.16	155	<1	0.02	5	790	12	<5	<20	11	0.01	<10	32	<10	<1	30
495	L2S: 14+ 75 E	1.0	1.41	30	195	<5	0.48	<1	19	29	39	4.16	<10	0.40	2295	2	<.01	23	2435	16	<5	<20	22	<.01	<10	30	<10	15	97
533	L4S: 13+ 75 E	<.2	0.77	20	40	<5	0.04	<1	7	23	9	2.52	<10	0.15	312	<1	0.02	9	780	16	<5	<20	5	0.01	<10	39	<10	<1	32
571	L20N 9+ 00 E	<.2	1.40	25	65	<5	0.16	<1	14	22	11	3.16	<10	0.13	95	1	0.01	22	430	6	<5	<20	4	0.01	<10	48	<10	<1	39
609	L22N 13+ 75 E	0.4	1.72	15	115	<5	0.85	<1	12	16	59	3.05	<10	0.29	248	<1	0.03	33	1830	22	<5	<20	61	<.01	<10	14	<10	66	128
647	BL10+00 13+00N	<.2	1.20	25	70	<5	0.06	<1	8	44	13	3.16	<10	0.47	101	2	0.01	24	1120	20	<5	<20	9	<.01	<10	56	<10	<1	60
685	BL10+00 22+50N	0.2	1.57	45	150	<5	2.00	2	26	51	45	4.58	<10	0.54	1096	3	0.02	39	1690	48	<5	<20	101	0.01	<10	46	<10	12	178
723	L26N 10+ 25 E	<.2	0.76	35	150	<5	0.03	<1	10	8	30	4.11	<10	0.14	380	2	0.01	17	990	48	<5	<20	8	<.01	<10	26	<10	<1	69
761	L23N 9+ 50 E	0.4	1.41	<5	80	<5	0.23	2	13	25	77	4.87	10	0.21	387	1	<.01	28	1200	38	<5	<20	14	<.01	<10	30	<10	10	126
799	L24N 14+ 25 E	0.4	1.26	<5	60	<5	0.07	<1	9	16	3	3.85	20	0.17	240	<1	<.01	16	800	10	<5	<20	3	<.01	<10	23	<10	4	46
837	L25N 15+ 00 E	<.2	1.77	<5	55	5	0.24	<1	17	22	<1	4.60	20	0.53	495	<1	<.01	25	690	4	<5	<20	18	0.01	<10	25	<10	5	65

TOKLAT RESOURCES INC. ETK 94-455 ECO-TECH LABORATORIES LTD.

QC DATA:	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
Standard 1991																												
	1.2	1.86	75	155	<5	1.93	<1	27	72	83	4.03	<10	1.13	720	<1	0.01	22	720	10	<5	<20	64	0.11	<10	83	<10	3	76
	1.2	1.93	70	155	<5	1.94	<1	22	72	80	4.08	<10	1.14	730	<1	0.01	21	720	16	<5	<20	60	0.10	<10	82	<10	6	79
	1.2	1.86	70	160	<5	1.93	<1	27	74	83	3.89	<10	1.09	736	<1	0.01	23	730	18	<5	<20	60	0.11	<10	84	<10	2	78
	1.2	1.90	60	140	<5	2.01	<1	23	74	77	4.54	0.46	1.00	730	<1	<.01	18	730	16	<5	<20	53	0.12	<10	86	<10	9	70
	1.4	1.86	65	150	<5	1.73	<1	17	68	74	3.60	<10	0.96	687	<1	<.01	20	650	18	<5	<20	58	0.11	<10	78	<10	8	70
	1.2	1.78	60	155	<5	1.75	<1	17	66	74	3.40	<10	0.96	705	<1	<.01	19	670	20	<5	<20	55	0.09	<10	78	<10	7	68
	1.2	1.88	65	150	<5	1.85	<1	18	67	76	3.80	<10	1.02	749	<1	<.01	18	720	18	<5	<20	58	0.10	<10	83	<10	8	64
	1.2	1.71	60	145	<5	1.80	<1	18	66	75	3.80	<10	0.93	680	<1	<.01	20	680	16	<5	<20	63	0.09	<10	78	<10	6	70
	1.0	1.79	65	150	<5	1.80	<1	17	64	76	3.89	<10	0.90	691	<1	<.01	16	680	18	<5	<20	55	0.12	<10	76	<10	5	69
	1.0	1.80	70	155	<5	1.99	<1	18	70	77	4.36	<10	0.94	736	<1	<.01	18	690	20	<5	<20	55	0.13	<10	82	<10	6	72
	1.2	1.71	65	145	<5	1.82	<1	20	67	76	3.89	<10	0.95	748	<1	<.01	20	670	22	<5	<20	46	0.09	<10	78	<10	5	72
	1.6	1.88	60	155	<5	1.99	<1	19	74	74	3.41	<10	1.00	780	<1	<.01	18	730	12	<5	<20	60	0.12	<10	88	<10	6	62
	1.2	1.89	65	160	<5	1.90	<1	22	72	78	4.33	<10	0.96	720	<1	<.01	23	780	18	<5	<20	55	0.10	<10	87	<10	6	72
	1.4	2.00	75	150	<5	2.09	<1	20	42	82	3.96	<10	0.96	730	<1	<.01	20	760	18	<5	<20	58	0.11	<10	83	<10	4	76
	1.2	1.92	60	160	<5	1.86	<1	20	65	84	3.92	<10	0.99	680	<1	<.01	19	680	18	<5	<20	57	0.11	<10	81	<10	7	75
	1.2	1.89	75	174	<5	2.06	<1	21	68	84	3.79	<10	0.95	734	<1	<.01	21	750	18	<5	<20	64	0.12	<10	84	<10	6	71
	1.0	1.98	70	165	<5	2.05	1	23	64	89	3.86	<10	0.99	998	<1	<.01	22	800	16	<5	<20	57	0.11	<10	80	<10	2	77
	1.0	2.02	75	170	<5	2.08	<1	20	69	82	3.76	<10	0.95	720	<1	<.01	21	730	22	<5	<20	66	0.11	<10	83	<10	6	73
	1.2	1.97	65	155	<5	1.45	<1	16	85	86	3.86	<10	1.00	700	<1	<.01	21	690	18	<5	<20	59	0.10	<10	77	<10	6	73
	1.2	2.02	65	165	<5	1.76	1	20	62	75	4.11	<10	0.97	700	<1	<.01	24	708	18	5	<20	56	0.11	<10	79	<10	8	74
	1.2	2.04	65	165	<5	1.77	1	20	63	75	4.11	<10	1.02	711	<1	<.01	23	690	16	<5	<20	55	0.10	<10	80	<10	6	73
	1.2	1.91	65	165	5	1.82	2	20	63	76	4.03	<10	0.94	724	<1	<.01	24	650	18	5	<20	55	0.12	<10	80	<10	8	74

***No Sample**

ECO-TECH LABORATORIES LTD.
Frank J. Pezzotti, A.Sc.T.
B.C. Certified Assayer

Appendix IV

Analytical Procedures

ECO-TECH LABORATORIES LTD.

ASSAYING
GEOCHEMISTRY
ANALYTICAL CHEMISTRY
ENVIRONMENTAL TESTING

10041 E. Trans Canada Hwy., R.R. #2, Kamloops, B.C. V2C 2J3 Phone (604) 573-5700
Fax (604) 573-4557

METHODOLOGY

a) Gold - Geochemical — Fire Assay - A.A.

A 10.000 gram sample is fire assayed by conventional fire assay procedures. The resulting bead is dissolved in 3ml aqua regia and is analyzed for gold by Atomic Absorption.

Minimum Reportable Concentration: 5 (pbb)

b) 30 Element ICP — Aqua Regia Digestion

A one gram sample* is digested with a 6ml mixture of HCL, HNO_3, H_2O in a ratio of 3:2:1. The digestion is carried out at 95°C for two hours. The digested sample is made up to 20ml with distilled water and analyzed by ICP.

Minimum Reportable Concentration:

a) Aqua Regia Digestion

Ag	0.2 ppm	Cu	1 ppm	Pb	2 ppm
Al*	0.01%	Fe*	0.01%	Sb	5 ppm
As	5 ppm	K*	0.01%	Sn	20 ppm
B*	2 ppm	La	10 ppm	Sr*	1 ppm
Ba*	5 ppm	Mg*	0.01%	Ti*	0.01%
Bi	5 ppm	Mn*	1 ppm	U*	10 ppm
Ca*	0.01%	Mo	1 ppm	V	1 ppm
Cd	1 ppm	Na*	0.01%	W*	10 ppm
Co	1 ppm	Ni	1 ppm	Y	1 ppm
Cr*	1 ppm	P*	10 ppm	Zn	1 ppm

Dissolution of elements marked by an asterisk may not be complete.
* 2 gram sample can be used at no extra charge

Copper Assay

A 2g sample is digested in a 200ml phosphoric flask with HNO_3, HCl. The digestion is carried out on a hot plate for 2 hours. The sample is bulked up with distilled water and analysed for copper by Atomic Absorbtion. The minimum reportable concentration is <0.01%.

Eco-Tech LABORATORIES LTD.

ASSAYING
GEOCHEMISTRY
ANALYTICAL CHEMISTRY
ENVIRONMENTAL TESTING

10041 E. Trans Canada Hwy., R.R. #2, Kamloops, B.C. V2C 2J3 Phone (604) 573-5700
Fax (604) 573-4557

Quality control

a) Sample Preparation

Random Duplicate samples are split from each shipment and introduced in each suite of samples sent to the laboratory for analysis. No less than one sample in forty is re-split. Each sample is assigned a unique lab number and barcode to be read by the barcode reader at the weigh station. A second person checks the lab number assignment for accuracy.

b) Weighing Stations

Each balance is calibrated twice during each shift using N.B.S. referenced weights. Samples are identified prior to weighing by use of a barcode reader. The sample identification, sample weight and analysis required is automatically captured by computer.

c) Fire Lab

Separate fusion pots are used for Assay, Rock Geochem and Soil Geochem. The pots are catalogued and are not reused until the assay is completed. Pots which were used for samples containing high or anomalous gold values are discarded at the end of each day. All flux mixtures are tested for purity before use.

d) Analysis

Samples are analyzed from test tube racks containing forty test tubes. Each rack will contain thirty-seven samples, (one of which may be a blind duplicate re-split form the bucking facility), one blank, one soil standard and one duplicate sample. Approximately 25 Can Met and several in-house standards are routinely used by our laboratory. As a minimum, a full 10% of all samples analyzed are quality control samples. In addition to the quality control analyses, check analyses are routinely performed to verify data for anomalous samples.

Eco-Tech LABORATORIES LTD.

ASSAYING
GEOCHEMISTRY
ANALYTICAL CHEMISTRY
ENVIRONMENTAL TESTING

10041 E. Trans Canada Hwy., R.R. #2, Kamloops, B.C. V2C 2J3 Phone (604) 573-5700
Fax (604) 573-4557

The samples are analyzed in the following order:

Test Tube	Contents
#40	Soil Standard (CanMet or In-House) to verify instrument calibration and sample digestion.
#1	Reagent Blank to check for reagent contamination and instrument zero.
#2 to #38	Analysis of samples.
#39	Sample Duplicate.
#40	Soil Standard and Recalibration.

Quality Control Data Assessment

Each element analyzed in the soil standards has an individual statistical plot of standard deviation for the analysis. Upper and lower warning limits are set at ±2 standard deviations. The analysis is considered to be out of control and is stopped when the value exceeds ±3 standards deviations. If the nature of the problem cannot be determined, the entire block of samples is re-analyzed. The results for duplicate and blind duplicate pairs must fall within our tolerance limits for precision of geochemical analysis as outlined below:

Average Value	Precision
1 to 2 times detection limit	± 100%
3 to 4 " "	± 60%
5 to 6 " "	± 40%
7 to 10 " "	± 25%
11 to 100 " "	± 15%
> 100 " "	± 10%

Appendix V

UTEM Survey on the Bar River Claim Group
by S.J Geophysics Ltd
Author: S.J. Visser, P.Geo.

UTEM SURVEY

ON THE

BAR RIVER CLAIM GROUP

CARIBOO MINING DIVISION B.C., N.T.S. 93 A/14

FOR

MINER RIVER RESOURCES LTD.

SURVEY BY

SJ GEOPHYSICS LTD.

AND

LAMONTAGNE GEOPHYSICS LTD.

October 1994

REPORT BY
Syd Visser
SJ Geophysics Ltd.

TABLE OF CONTENTS

SJ Geophysics Ltd. 11762 - 94th Ave., Delta, B.C. Canada tel (604) 582-1100 fax (604) 589-7466

INTRODUCTION

Instrument

A large loop time domain electromagnetic (UTEM-3) survey was completed by SJ Geophysics Ltd. and Lamontagne Geophysics Ltd., for Miner River Resources Ltd. on the Bar River Claim Group during the period of July 1-8 and July 17-23, 1994. The Bar River Claim Group is located near Wells B.C., in the Cariboo M.D., of B.C. (N.T.S. 93 A/14).

The purpose of the survey was to search for massive sulphides, and to aid in the mapping of local geology.

DESCRIPTION OF UTEM SYSTEM

UTEM is an acronym for "University of Toronto ElectroMagnetometer". The system was developed by Dr. Y. Lamontagne (1975) while he was a graduate student of that University.

The following is a short description of the UTEM system used in the field. A paper (A time-domain EM system measuring the step response of the ground) by G.F. West, J.C. Macnae and Y. Lamontagne, giving a more complete description with an overview of interpretations is located in Appendix III.

The field procedure consists of first laying out a large loop, which can vary in size from less than 100M X 100M to more than 2Km X 2Km, of single strand insulated wire and energizing it with current from a transmitter which is powered by a 2.2 kW motor generator. During a surface survey the lines are generally oriented perpendicular to one side of the loop and surveying can be performed both inside and outside the loop. For Borehole survey the sensor coil is placed down the borehole measuring the axial component of the electromagnetic field from a minimum of 2 separate loops.

The transmitter loop is energized with a precise triangular current waveform at a carefully controlled frequency (30.97 Hz for this survey). The receiver system includes a sensor coil and backpack portable receiver module which has a digital recording facility. The time synchronization between transmitter and receiver is achieved through quartz crystal clocks in both units which are accurate to about one second in 50 years.

The receiver sensor coil measures the vertical horizontal, or axial magnetic component of the electromagnetic field and responds to its time derivative. Since the transmitter current waveform is triangular, the receiver coil will sense a perfect square wave in the absence of geologic conductors. Deviations from a perfect square wave are caused by electrical conductors which may be geologic or cultural in origin. The receiver stacks any pre-set number of cycles in order to increase the signal to noise ratio.

The UTEM receiver gathers and records 10 channels of data at each station occupied. The higher number channels (7-8-9-10) correspond to short time or high frequency while the lower number channels (1-2-3) correspond to long time or low frequency. Therefore, poor or weak conductors will respond on channels 10, 9, 8, 7 and 6. Progressively better conductors will give responses on progressively lower number channels as well. For example, massive, highly conducting sulfides or graphite will produce a response on all ten channels.

The Borehole system consists of a normal surface UTEM-3 transmitter and receives along with special receiver coil (1 1/4" in diameter). The coil is connected to the receiver trough a controller and fibre optic cable.

FIELD WORK

Rolf Krowinkel, geophysicist with SJ Geophysics Ltd., and the equipment were mobilized from Vancouver by truck on July 1, 1994. The initial work on the Bar River Claim Group was completed between July 1 and 8, 1994 with helpers supplied by the client. Rolf was joined by Neil Visser and the survey was extended from July 17 and 23, 1994. The survey area was accessed daily by truck and all terrain vehicle from Wells. The field parameters and local geology were discussed with geologist Tim Tourmunde, Toklat, before commencing the survey and during the survey period.

Approximately 8 Km (including overlap) using a station spacing of 25m were surveyed from 2 loops in a period of 6 production days 4 loop laying days 3 mobilization days and 2 down days.

The grid is comprised of flagged lines in rough terrain therefore channel 1 data cannot be guaranteed to be accurate. Slopes were recorded during the survey to produce a topographic map and aid in reduction of the data. The loop lines were not flagged therefore the loop locations were estimated as close as possible. The long daily commute to the survey grid and poor access to parts of the grid and rough lines slowed the survey considerably.

SJ Geophysics Ltd. 11762 - 94th Ave., Delta, B.C. Canada tel (604) 582-1100 fax (604) 589-7466

DATA PRESENTATION

The results of the 1994 UTEM survey are presented on 12 data sections (Appendix IV) and one compilation map, Plate G1.

Legends for the UTEM data sections are also attached (Appendix II).

In order to reduce the field data, the theoretical primary field of the loop must be computed at each station. The normalization of the data is a follows:

a) For Channel 1:

% Ch.1 anomaly = (Ch.1 - PC) X 100//PT/

Where:

PC is the calculated primary field in the direction of the component from the loop at the occupied station

Ch.1 is the observed amplitude of Channel 1

PT is the calculated total field

b) For remaining channels (n = 2 to 9)

% Ch.n anomaly = (Ch.n - Ch.1) X 100/Ni

where:

Ch.n is the observed amplitude of Channel n (2 to 9)

N is Ch1 for Ch1 normalized

N is PT for primary field normalized

I is the data station for continuous normalized (each reading normalized by different primary field)

I is the station below the arrow on the data sections for point normalized (each reading normalized by the same primary field)

Subtracting channel 1 (Ch.1) from the remaining channels eliminates the topographic errors from all the data except channel 1.

If there is a response in channel 1 from a conductor then this value must be added to do a proper conductivity determination from the decay curves. Therefore channel 1 should not be subtracted indiscriminately.

The data from each line is plotted on at least 2 separate sections consisting of a continues normalized section and a point normalized section. Additional point normalized data sections were produced where more than one conductor is present on the same line. Point normalization data is the absolute secondary field at a "gain setting" related to the normalization point. The data is usually point normalize over the central part of the crossover anomaly to aid in interpretation.

DISCUSSION

The compilation of the UTEM data is shown on the UTEM compilation map Plate 1. The survey indicted a good conductive package of rocks which are likely graphitic argillites or bedded sulphydes striking across the survey grid from the southern end at line 0 to the northern end at line 100N. The conductive zone is approximately 200m wide and is continuos, except for the breaks near line 500N and 600N, along the length of the survey grid. Because of the strong late time (channel 1) response due to this extensive conductive package it is difficult to locate any zones of higher conductivity although the conductivity does not appear to be homogeneous along the complete strike length.

On the southern part of the survey area from line 0 to 400N, the conductive zone appears to be very conductive on both the western and eastern edge with possibly a somewhat resistive zone(s) in the central part. The conductive zone likely consists of a number of interbedded conductive and non-conductive layers. Both the western and eastern edges of the conductive zone are very distinct in this area.

In the central part of the survey grid between lines 500N and 600N the conductivity appears to be weak on the western edge and very strong on the eastern edge of the conductive zone. The conductive zone is narrower in this region.

The extension of the conductive zone north of line 600N is approximately the same width as the southern part. The conductivity on this part of the zone appears to be concentrated on the western edge of the zone.

Current channeling in all of these conductive zones make it very difficult to do any quantitative interpretation. The contacts of these zones appear to be very near surface (25m or less) therefore can likely be located with trenching or shallow drilling.

There are a number of very weak anomalies on the remainder of the grid. These are located mainly in the north western part of the survey grid and appear to be related to contact zones. There is also likely a conductive unit located under the loops.

The remaining interesting feature shown on the compilation map is the narrow high resistivity zone located at 1450E on line 600N.

RECOMMENDATIONS

It is recommended to closely correlate the geophysics to any geological and geochemical information to determine the possible potential of the conductive zone. If more detailed geophysics is required it is recommended a carefully chained grid on cut lines to aid in the correction the late time response. A lower base frequency should also be considered to get more information at later time and therefore possibly discriminate between the conductive lithology and strong conductors due to sulphyde mineralization. A loop located from the east side could aid in the interpretation of the eastern side of the conductive zone.

The edges of the conductive zones are near surface and can likely be located by trenching or shallow drilling. The conductive zone appear to consists of a number of interbedded conductive layers which extend to depth. Therefore a deeper hole to intersect the full width of the conductive zone may be of more interest. The location of the drill hole should be influenced by the geochemical results.

CONCLUSION

A strongly conductive zone with a width of approximately 200m strikes across the length of the survey grid. The signature of the zone varies somewhat along strike with the southern part of the zone being very conductive on both the eastern and western edges with possibly interbedded conductive zones, the central part being conductive on the eastern edge and the northern zone conductive on the western edge. A number of weak anomalies located in the north western part of the grid are likely contacts. A small high resistivity zone is located in the central part of the survey area.

All of the conductive units are near surface and can likely be investigated by trenching or shallow drilling. The data should be closely correlated to the local geology and geochemical results to determine the best location to test this conductive zone by drilling or trenching.

Syd Visser, P.Geo

Geophysicist

SJ Geophysics Ltd.

APPENDIX I

STATEMENT OF QUALIFICATIONS

I, Syd J. Visser, of 11762 - 94th Avenue, Delta, British Columbia, hereby certify that,

1) I am a graduate from the University of British Columbia, 1981, where I obtained a B.Sc. (Hon.) Degree in Geology and Geophysics.
2) I am a graduate from Haileybury School of Mines, 1971.
3) I have been engaged in mining exploration since 1968.
4) I am a professional Geoscientist registered in British Columbia.

PROFESSIONAL PROVINCE OF S. J. VISSER BRITISH COLUMBIA GEOSCIENTIST

Syd J. Visser, B.Sc., P.Geo
Geophysicist

APPENDIX II

Legend

UTEM SYSTEM MEAN DELAY TIME

Channel Number	Delay Time(msec)	Symbol
1	12.8	|
2	6.4	╲
3	3.2	╱
4	1.6	□
5	0.8	⋝
6	0.4	∡
7	0.2	⊅
8	0.1	×
9	0.05	△
10	0.025	◇

Base Frequency = 31 Hz

APPENDIX III

A time domain EM system measuring the step response of the ground

GEOPHYSICS, VOL. 49, NO. 7 (JULY 1984); P. 1010-1026, 26 FIGS.

A time-domain EM system measuring the step response of the ground

G. F. West*, J. C. Macnae*‡, and Y. Lamontagne‡

ABSTRACT

A wide-band time-domain EM system, known as UTEM, which uses a large fixed transmitter and a moving receiver has been developed and used extensively in a variety of geologic environments. The essential characteristics that distinguish it from other systems are that its system function closely approximates a step-function response measurement and that it can measure both electric and magnetic fields. Measurement of step rather than impulse response simplifies interpretation of data amplitudes, and improves the detection of good conductors in the presence of poorer ones. Measurement of electric fields provides information about lateral conductivity contrasts somewhat similar to that obtained by the gradient array resistivity method.

INTRODUCTION

This article describes the design of the UTEM system and its development at the Geophysics Laboratory of the University of Toronto by Y. Lamontagne and G. F. West from 1971 to 1979. UTEM is a wideband, time-domain, ground EM system with a step-function system response. It was designed to try to achieve the sensitivity and interpretability necessary to handle problems of deep exploration, conductive environments, and a variety of terrain conditions, in an economically viable manner. As with most EM systems, effective exploration for massive sulfide ores was the principal objective. The method was conceived in 1971, and the first UTEM I instrument was operational in 1972. It was an analog electronic system, and was used in a number of surveys which have been described by Lamontagne (1975). An improved UTEM II which incorporated a digital recording system was then designed and constructed at the University of Toronto with financial aid from a consortium of mining companies. It was first used in 1976. To fall 1980, about 1000 line-km had been surveyed with the system from 144 loops in 35 areas. UTEM III, which is a microprocessor-controlled system with expanded capabilities, is now produced commercially by Lamontagne Geophysics Ltd. Some of the field results obtained using the UTEM II system have been described in Lamontagne et al. (1977, 1980), Macnae (1977, 1980, 1981), Lodha (1977), and Podolsky and Slankis (1979). Data from all three UTEM systems are identical insofar as geophysical characteristics are concerned. The differences affect only data noise levels and operational convenience. Some of the noise rejection features of UTEM III are discussed by Macnae et al. (1984).

THE UTEM SYSTEM

Design philosophy

UTEM uses a large, fixed, horizontal transmitter loop as its source. The field of the loop is mapped in the quasi-static zone with the receiver system; the vertical component of the magnetic field is always measured, and in some circumstances the horizontal magnetic and electric field components may be measured as well (Figure 1). The size of the transmitter loop depends on the prospecting problem; loops may range from about 2 km × 1 km in resistive terrain to 300 m × 300 m in a conductive area. Lines are typically surveyed to a distance of 1.5 to 2 times the loop dimensions.

The large loop transmitter-field mapping receiver configuration was chosen in order to give the system the deepest possible exploration for orebody sized conductors, without sacrificing the ability to resolve shallower structures (depth < 50 m). This dictates a very large transmitter moment, and makes an extended source desirable. The virtue of an extended source is that the coupling between the source and a receiver or the source and a nearby conductive zone is not so many orders of magnitude larger than the coupling to a distant receiver or deep target as is the case with a confined source.

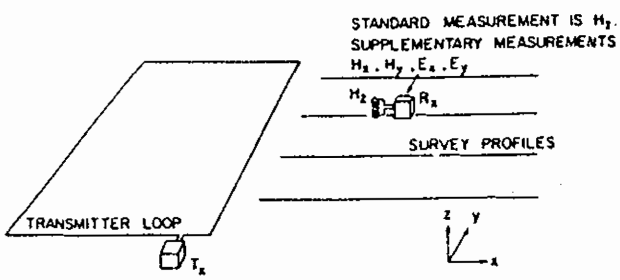


FIG. 1. Schematic layout of a UTEM survey.

Manuscript received by the Editor November 1983; revised manuscript received December 1983.
*Geophysics Lab., Dept. of Physics, Univ. of Toronto, Ont., Canada M5S 1A7.
‡Lamontagne Geophysics, 740 Spadina Ave., Toronto, Ont., Canada M5S 2J2.

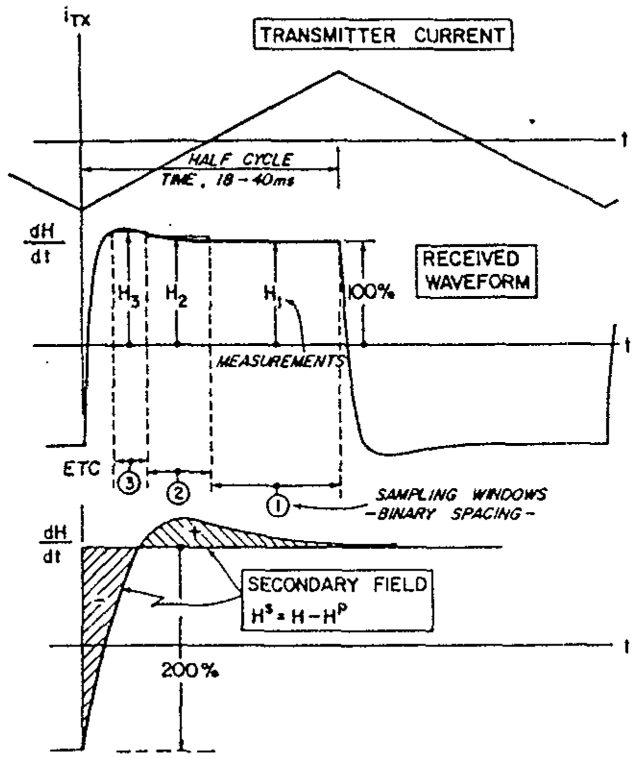


FIG. 2. Transmitted and received UTEM waveforms. Note that the measurement channels are numbered from the latest to the earliest. Sampling is repeated, with due regard to sign, in every *half-cycle.*

Given a large transmitter and a large *Tx-Rx* separation, it is inevitable that induction in extensive conductive overburden and in large formational conductors will contribute more to the response than with a small scale system. Also, as the separation becomes larger it becomes increasingly likely that the system will be responding to several nearby conductors at once. However, a fixed transmitter-moving receiver system offers a basis for separating the signal contributions from the various conductors and resolving the geometry of deep-seated conductors. At any time instant, the magnetic field of the current system induced in the ground is a potential field (within the quasi-static zone), and if it is mapped on a profile or over a surface, there is a firm theoretical basis for separating it into parts and estimating the current systems which caused it. When the transmitter and hence the eddy current system move for each observation, it is more difficult to find a theoretical basis for stripping of responses into component parts.

There are negative aspects to using a fixed transmitter method. In addition to the aforementioned enhancement of anomalies due to formational conductors, the transmitter can be positioned badly for induction in small plate-like conductors, and a large good conductor can screen a smaller, shorter time-constant conductor which lies behind it. For these reasons it may be desirable to have survey coverage from more than one transmitter location.

The UTEM II transmitter passes a low-frequency current of precise triangular waveform through the transmitter loop. The magnetic field is sensed with a coil, which responds to the time derivative of the local magnetic field, so in "free space" a precise square-wave voltage would be induced in the receiver. In the presence of conductors the waveform is substantially distorted. The UTEM receiver measures this distortion by determining amplitudes at 10 delay times (actually, averages over time windows) which are spaced in a binary geometric progression between the waveform transitions. The sample scheme is shown in Figure 2. Note that the UTEM channel numbers are conventionally numbered in reverse order of time. This is because the latest time measurement often serves as a reference to which the other measurements are compared, whereas the number of earlier time measurements which can be made accurately may change if base period or instrument bandwidth is altered. The base frequency of the system is selectable, usually about 30 or 15 Hz (25 or 12.5 Hz in countries with 50 Hz power). A common practice is to set the base frequency (adjustable in 0.1 percent steps) about 0.5 Hz from a subharmonic of the power line in order that power line interference can be detected by slow beating in the data. The base frequency is usually set low enough that all ground response has nearly vanished by the end of the half-cycle. When this is the case, the UTEM system determines the step response of the ground in the time range 25μs to 12.8 ms (30 Hz base frequency).

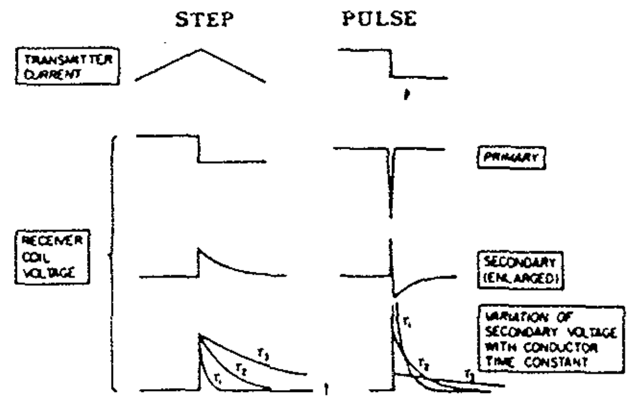


FIG. 3. Comparison of transient signals in step and pulse type systems.

Time-domain systems

Time-domain systems have some advantage over frequency-domain systems in that simultaneous measurement is easier to achieve over the whole spectrum and, at the same time, it is possible to check the phase synchronization of the transmitter and receiver time bases. Most time-domain systems employ an on-off type of transmitter current and confine all measurements to the off period, as this automatically separates the secondary from the primary field. However, when a coil is used as a sensor, the time derivative of the signal is observed. Thus, if the transmitter loop is energized with a step current, it is the impulse response of the ground which is observed.

When prospecting for conductive mineral deposits, it is generally more desirable for interpretation purposes to observe the step response than any other time response. The reason for this lies in the characteristics of eddy current decay. For the step

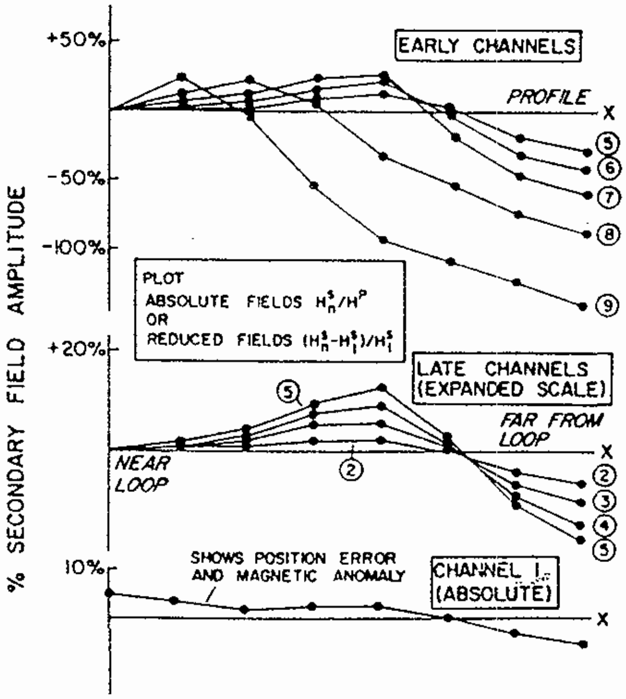


FIG. 4. Standard presentation of UTEM vertical component magnetic field data.

response, the early-time limit of response is identical to the frequency-domain inductive limit, and for a simple conductor in free space this is a function of geometry alone. For the impulse response, the early time limit is scaled from the step response limit by the inverse of the transient decay time constant (Figure 3). Thus, the decay rate must first be determined in order to interpret amplitude information in terms of geometry. This may present little difficulty in simple cases, but when complex or overlapping responses are observed it can be a serious problem. Also, even in the case of the step response, overburden anomalies which generally are of short time constant have early time amplitudes which are very much larger than the anomalies of target conductors with long time constant. Any further amplification caused by measuring the impulse rather than step response is clearly undesirable.

Although a system with a step response is usually desirable for interpretation purposes, the UTEM system is only one implementation of such a system. In fact a system using a magnetometer receiver with a square-wave transmitter instead of an induction coil (referred to as MSW system in the following sections) would have an identical system response. The foregoing rationale of the interpretational advantages of step response does not consider the other important factors which enter the design of actual systems such as signal-to-noise (S/N) efficiency and transmitter-sensor design constraints which in fact guide the choice of the actual transmitter waveform and sensor used. This is a complex topic discussed by Lamontagne et al. (1980). For example, the UTEM III system actually uses a modified triangular transmitter waveform and deconvolution in the receiver to improve its S/N performance but has a system response identical to the UTEM I and UTEM II systems (Macnae et al., 1984), i.e., a square-wave response. Thus the UTEM I/II systems, the conceptual MSW system, and the UTEM III system all make identical measurements although they excite the ground differently. To avoid any confusion, discussions in this paper of actual induced current waveforms in the ground will be limited to the UTEM system with a purely triangular waveform and to the MSW system.

The sampling scheme of Figure 2 was chosen so that virtually all measuring time is utilized and time scaling of the measurements is permitted. In the frequency domain, inductive responses may be characterized by dimensionless parameters of the form

$$\theta_f = \sigma\mu\omega L^2,$$

which demonstrates that scale changes of conductivity, frequency or (length)^2 are equivalent to one another. The analogous parameter for the time domain is

$$\theta_t = \sigma\mu L^2/t.$$

In interpreting frequency-domain data, it is common to compare observed frequency response data with dimensionless model response data. This is convenient because it avoids the necessity of rescaling the model data for all frequencies and physical scale lengths that might be encountered in the field cases. The same sort of scaling is possible with time-domain data, but only if the system function of the apparatus is a pure discontinuity response. If this is not the case, for instance when the apparatus has a characteristic ramp shut-off time, model response curves cannot be rescaled in time to match field data as this would imply rescaling the shut-off time to a value different from that used by the apparatus.

To ensure that time scaling can readily be applied to data that have been sampled and averaged over a time window, it is also necessary that the window widths be proportional to time after the discontinuity. UTEM has such sampling. It should be noted that time scaling may only be applied to UTEM anomalous responses which are short enough so as to have vanished in the interval between the two successive transitions of the step which form the square wave.

Data presentation

Because the field intensity falls off rapidly with increasing distance from the transmitter loop, it is often desirable to normalize the secondary field observations in some manner. One suitable normalizing factor is the primary vertical magnetic field signal (H_z^p). If the positions of the transmitter loop and the receiver are known reasonably accurately, a calculated value of H_z^p may be employed. If the ground response vanishes by late time, the channel 1 measurement is a direct measure of H_z^p. Normal survey data plotting practice encompasses both procedures.

Figure 4 is an example of a standard plot of UTEM secondary vertical magnetic field data (H_z^s). Channel 1 is plotted as secondary field (Ch 1-H_z^p)/H_z^p (where H_z^p is the calculated primary field) and all other channels are normalized to Ch 1 [(Ch n-Ch 1)/Ch 1] to correct for any position error in calculation of H^p and also to remove the effect of induced magnetic anomalies (for further details see Lamontagne, 1975). The late channels on the example plot show a crossover type of anomaly, indicative of a concentration of (changing) induced current, as will be discussed. The amplitude variation with channel number indicates that these induced currents are decaying with time. A small component of response appears to have persisted to Ch 1 and, for quantitative analysis, it should be remembered that the data reduction process will have caused subtraction of this amount from profiles of Ch 2-Ch*n*. On the early-time channels, the migration of crossover location from one channel to another indicates that the secondary current flow at these times is not fixed in geometry, a characteristic which is indicative of an extensive conductor (here extensive overburden) rather than a localized conductor such as that responsible for the late time crossovers.

Since at any delay time, the secondary field is a potential field, interpretation of geometrically fixed current systems is best performed using absolute secondary fields normalized by the primary field intensity at a single point rather than continuously along the profile. Although only one case presented in this paper has this absolute or "point normalization," recent routine field practice is to point normalize all survey profiles exhibiting discrete anomalies, in order to simplify interpretation.

Horizontal magnetic field measurements may be made by reorienting the receiver coil. Normalization is done using the vertical primary magnetic field (calculated or vertical Ch 1 measurement). Unfortunately, horizontal field measurements frequently suffer a somewhat higher noise level than vertical fields, due to the predominantly horizontal orientation of sferic interference.

The electric field waveform is, like the voltage from the coil sensor, a square wave if the ground is very resistive. It is distorted in much the same way as the coil signal when the ground is conductive. Electric field observations are usually plotted as E_i/E_T^p—the observed channel voltage between the electrodes divided by the maximum expected late time voltage between electrodes at the observation point in any horizontal direction, i.e., $E_T^p = (E_x^{p2} + E_y^{p2})^{1/2}$. "Expected" here refers to the electric field produced by a loop on a laterally uniform, resistive half-space. This normalization facilitates intercomparison of *x* and *y* component data. The geologic noise level in electric field data is usually high, so plotting on expanded scales is rarely justified. All channel data are usually plotted on the same axes, as shown in Figure 5.

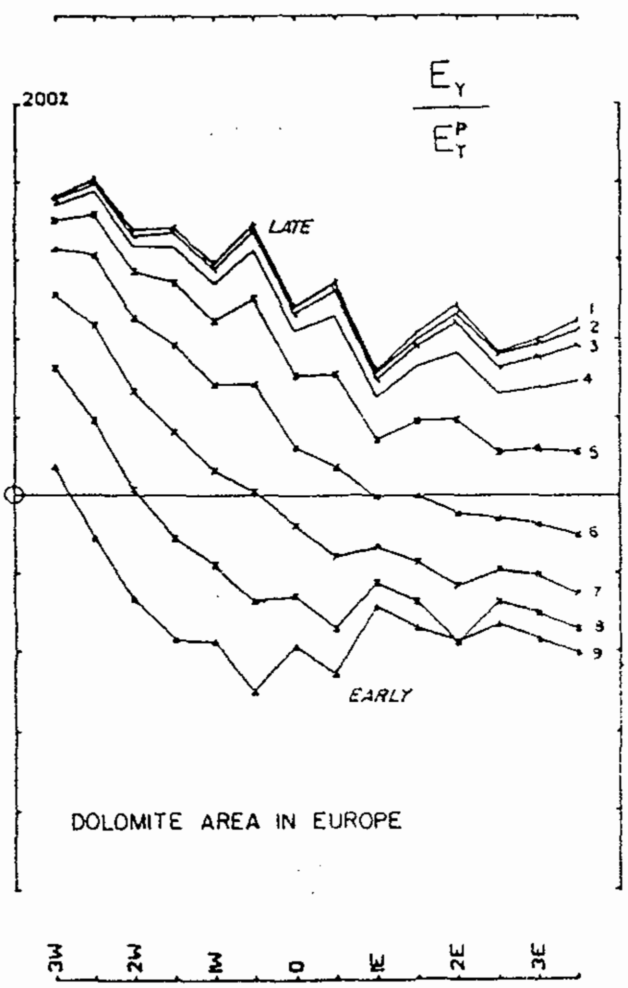


FIG. 5. Standard presentation of electric field data. The observed component is normalized to the total primary electric field of the transmitter loop.

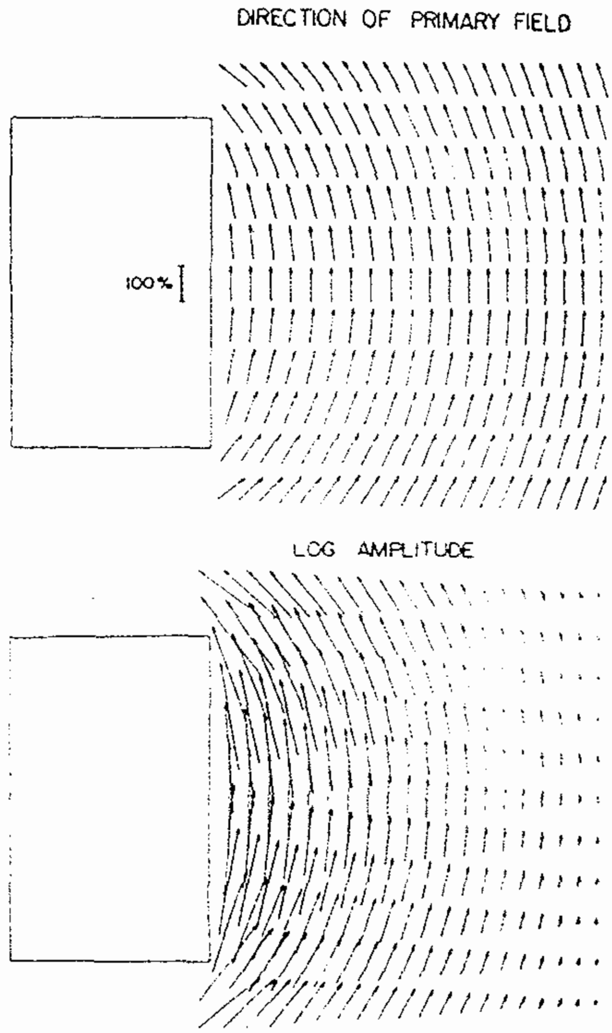


FIG. 6. Vector plots of late time electric field. (a) Direction information only. (b) Showing direction and intensity of the primary field.

The reference state for electric field data is usually described as a "laterally uniform, resistive half-space," rather than free space. By resistive is meant a case where all inductive transients have died out. The free-space electric field of a horizontal loop is horizontal, so introduction of a resistive half-space does not affect the field. However, for any other orientation of the transmitter loop or the earth-air interface, the free-space electric field will be directed across the interface and a strong distortion of the field will occur. Since the conductivity of air is virtually zero, the earth-air interface almost always has a high conductivity ratio, even if the earth is resistive in terms of induction. The charge which arises on the interface essentially doubles the vertical component of the E field in the air near the boundaries and annuls the vertical component in the ground. Thus the E field in the ground is (almost always) virtually horizontal. The nomenclature for the reference state serves to remind one that the earth-air interface has an important role in the physics of

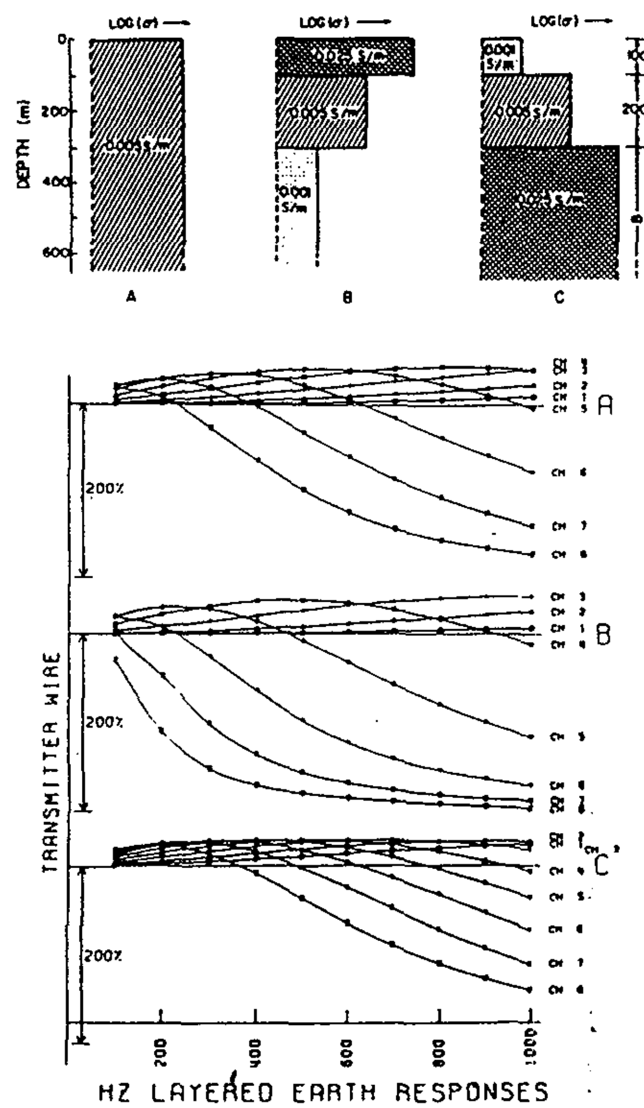


FIG. 7. UTEM layered earth response.

the electric field and is always assumed to be present, but no lateral inhomogeneity or induction is permitted in the reference model.

The electric field of a heterogeneous, conductive earth does normally become constant at late time, as the EM transients vanish. At the same time, the rate of change of magnetic field becomes constant. However, the observed late-time E limit is usually found to be different from the free-space or uniform resistive half-space value, due to lateral inhomogeneity of the earth's conductivity structure. The late-time electric field around a loop greatly resembles what might be seen in a gradient resistivity survey. The field weaves about, deflected around the more resistive areas and through the more conductive ones. A vector display of the late-time E field is an interesting reflection of the *relative* conductivity of various parts of the ground. It is impractical to plot the unnormalized E vectors, since the true field intensity falls off rapidly with increasing distance from the loop. The lengths of the plotted vectors are therefore proportioned to the normalized field of the loop, as for profile plots. Vector plots of the free-space field of a loop are shown in Figure 6. Examples of field data are given in the following section.

Errors caused by the presence of EM noise or by poor geometrical control are discussed for the magnetic (H) field case in Lamontagne (1975). For the electric (E) case, details of the measurement and sources of error are discussed in appendix G of Macnae (1981). As in the dc resistivity method, topographic features can seriously distort local electric fields, and local conductivity contrasts such as overburden patches and minor lithological changes can have quite large effects on the amplitude of measured E fields.

INTERPRETATION

We shall describe briefly the responses from a number of simple geologic models and how these can be identified and interpreted.

Layered earth responses

The problem of EM induction in a layered earth is very well treated in the literature, particularly for frequency-domain systems (e.g., Wait, 1962). Time-domain cases have also been studied for some specific problems, for example the infinite thin sheet was solved by Maxwell (1891) and the half-space response is discussed by Nabighian (1979). A general, layered earth solution for UTEM geometry and waveforms was given in Lamontagne (1975). Figure 7 shows three examples of computed responses for different layer conductivities. Figure 8 shows three examples of a thin layer at different depths. There are several common characteristics of layered earth responses. The shapes of the anomalous profiles are generally similar, becoming broader at later times. The migration of crossovers with time, with positive lobes toward the loop and negative lobes away from the loop, seems to indicate that the induced current system is migrating away from the loop. This is the type of behavior described by Nabighian (1979) as an expanding smoke ring.

If the UTEM system employed a magnetometer as receiver and a square current waveform in the transmitter, the smoke ring analogy would be exact, as the crossovers would indicate the position of the main current concentrations. However, the UTEM receiver is a coil which is sensitive only to dH/dt, and thus to the rate of change of induced and transmitter loop current. Thus the moving pattern of crossovers is actually indicating outward migration of *changes* in the induced current pattern. Toward the end of each half-cycle, the induced current system at any point in the survey area tends to a constant value, as indicated by the electric field measurements, but this steady current is invisible to the coil receiver.

When interpreting UTEM magnetic field data, it can often be simpler to think of the data in terms of the magnetometer receiver, square-wave transmitter current (MSW) analogy. Because the analogy is *exact* for a linear process like EM induction, there is no approximation in using it. It is very convenient to think of the field measurements of secondary signal at any delay time as describing the Biot-Savart magnetic field of a changing and decaying (analogous) induced current system. However, when electric field data are being analyzed and compared with magnetic field (dH/dt) data, it is necessary to revert to the true picture of the induced currents (or take a time derivative of the E data) to maintain a consistent relationship. UTEM magnetic field data are usually symbolized as H^s_{zi} (alphabetic subscript = component direction, superscript = p primary, s secondary, T total, numeric subscript = channel number) to accord with the magnetometer analogy; and in most discussions of simple induction, it is the time history of the *analogous* induced current which is described.

An important feature of layered earth H^s_z data is the early-time limit of continuously normalized H^s_{zi}/H^p_z data. If the ground is sufficiently conductive near the surface, the early-time secondary field data at points remote from the transmitter loop will approach -200 percent; i.e., one finds that the voltage in the receiver coil has had insufficient time to change from the steady value attained at the end of the previous half-cycle (Figure 2). This situation may be pictured in the magnetometer-square wave current analogy as an induced current system forming near the surface of the ground under the transmitter loop such as prevents the total (analogous) magnetic field from entering into the ground anywhere except very close to the transmitter wire. The -200 percent anomaly thus represents response at the inductive limit.

Finite thin plate in free space

A convenient modeling method for thin finite plate conductors in free space is the integral equation solution of Annan (1974). Annan computed the best set of polynomial eigenpotentials of order 4, and used these to represent the induced current flow in the plate as a sum of 15 "eigencurrents." The solution for the eigencurrents themselves is quite complicated, but needs only to be done once for a plate of given width to length ratio. After that, any induced current system can be described in terms of 15 coefficients in the eigenpotential summation. The secondary field at a receiver can then be simply computed in terms of these induced eigencurrents. One great advantage of Annan's method is that each eigencurrent has a frequency or time-domain response identical to a simple loop circuit. Thus the solution for a broad frequency range or many time windows is very easy to calculate. Routines for simple, interactive application of Annan's algorithms to a number of EM systems have been programmed by Dyck (Dyck et al., 1980).

Examples of type curves generated with Annan's solution may be found in Lodha (1977) and Lamontagne et al. (1980). Figure 9 shows the results of a set of computed UTEM type curves for the geometry shown in Figure 10. Also shown in Figure 10 is the geometry of the primary magnetic field, which controls the nature of induction in the plate. For the zero dip case, the primary field is mostly perpendicular to the plate. The induction in the plate tends to cancel this field at early times, leading to a negative H_z anomaly directly over the plate. Positive shoulders on each side show the secondary magnetic field of the "forward (analogous) current" near the front edge of the plate nearest the loop and the "reverse current" near the rear edge. The normalization scheme used in plotting this data is to divide the total secondary field by the calculated primary field at the measuring point. It has the undesirable effect of making asymmetric a secondary anomaly that is symmetric in terms of absolute amplitude by increasing the relative amplitude away from the loop. In fact, the absolute secondary amplitude of the positive shoulder near the loop is usually larger than the one on the side away from the loop. As the dip of the plate is increased, the positive shoulder moves away, and by the time a 30-degree dip is reached the reverse crossover is off the end of the plotted line. From dips of 30 to 135 degrees, the anomaly maintains a basic shape in the form of a simple crossover. The amplitude

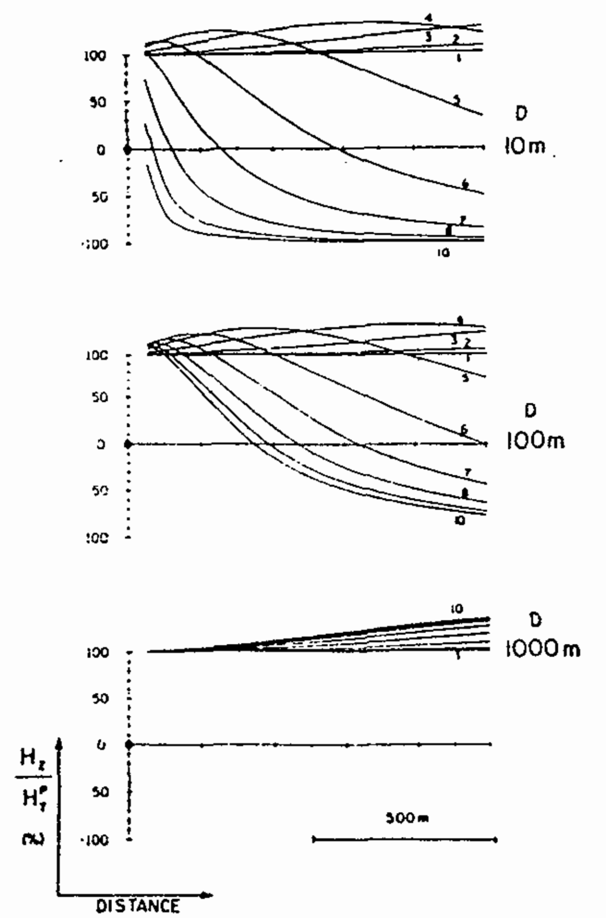


FIG. 8. Hz response of a thin horizontal sheet at various depths. The conductivity-thickness of the sheet is 2 S. The front of the transmitter loop is at the origin of coordinates.

does vary somewhat, however, being controlled by the primary field component normal to the plate which becomes a smaller and smaller fraction of the total field as the plate rotates from 30 to 150 degrees (Figure 10). The case at a dip of 150 degrees shows a very interesting behavior. The primary field can be seen to be *down* in the upper half of the plate and *up* in the lower half. The result of this is that the anomaly changes location and amplitude dramatically. For a very small plate, an anomaly could conceivably disappear completely. This phenomenon has been discussed by Bosschart (1964) for the Turam method. For a large planar conductor, however, an anomaly is always present since a curving primary field must cut it somewhere, except in the special case when a vertical conductor is located directly under the center of a horizontal transmitting loop. The 165-degree dip case of Figure 9 shows a clear reverse crossover on the edge of the conductor far from the loop. The normal crossover is very small, due in part to the reduced induction at the near edge as shown in Figure 10, and also the large primary field used as a divisor for normalization.

The electric field anomaly generated by a plate conductor in

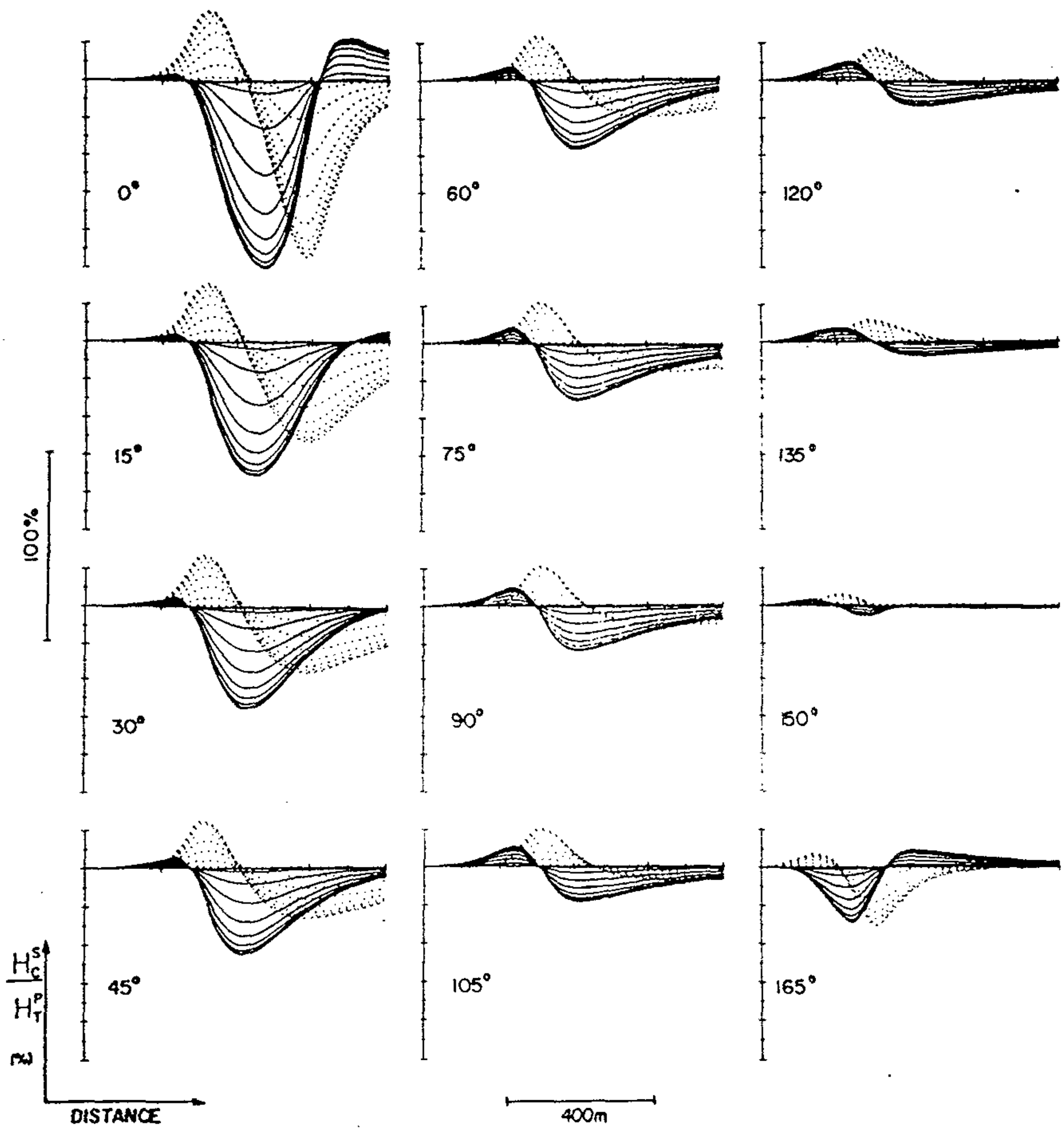


FIG. 9. UTEM H_z (solid) and H_x (dotted) profiles over a dipping plate (continuous normalization). (Geometry shown in Figure 10.)

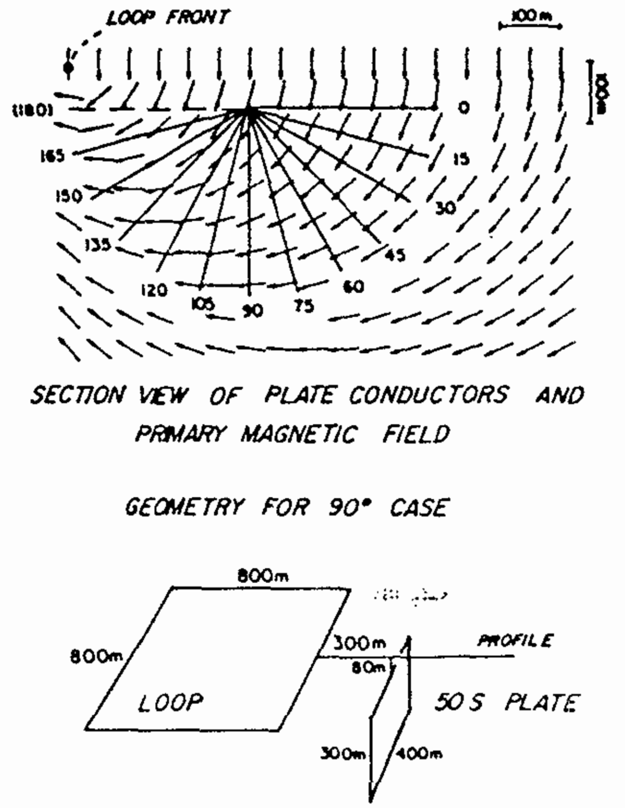


FIG. 10. Geometry and dimensions of the models shown in Figure 9. Also shown is the configuration of the primary field in the vicinity of the target conductor.

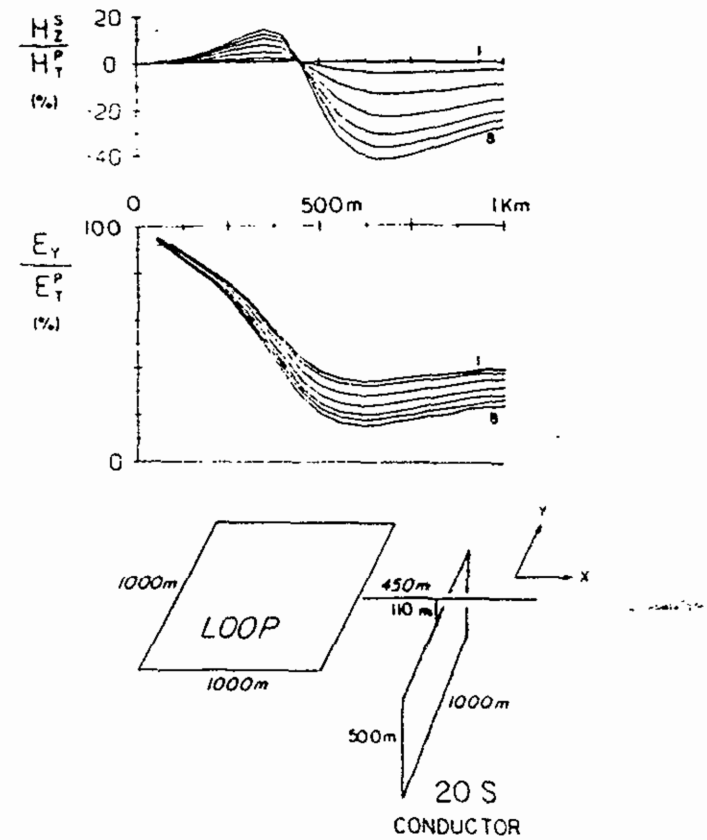


FIG. 11. Scale model UTEM secondary magnetic H_z^s and total electric E_y data over a vertical plate conductor.

a resistive half-space is caused by charge on the plate as well as eddy currents flowing in it, and is affected by the earth-air interface. Annan's algorithm does not determine the charge distribution, so analog scale modeling methods were employed to produce type profiles. Figure 11 shows an example for a vertical plate. The longitudinal electric field is greatly reduced over the body at all times (i.e., there is a strong reduction in the late time limit). The dynamic (time-varying) part of the anomaly has the same time variation as the magnetic field but has a different geometrical pattern. The electric field is highly vulnerable to distortion by any conductivity contrast and the intensity of the static, late-limit anomaly over a conductor may therefore be reduced by any stratification between the conductor and the surface.

Other simple anomaly shapes

A set of simple schematic models is shown in Figure 12, for each of which the main features of the vertical magnetic field are sketched. The set of sketches was derived from quantitative scale model experiments by Lamontagne (1975). For the simple models illustrated where the host rock is completely nonconducting, the general anomaly shape for one body remains quite constant for the whole time range. The changes in anomaly from one channel to another are mostly in the amplitude and smoothness of the anomalies.

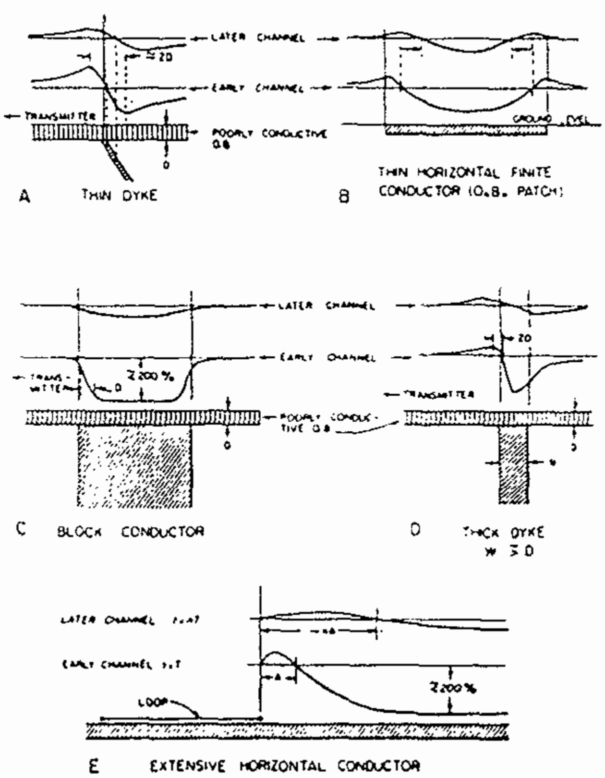


FIG. 12. The form of continuously normalized UTEM H_z^s anomalies over some simple shapes. All conductors are in free space.

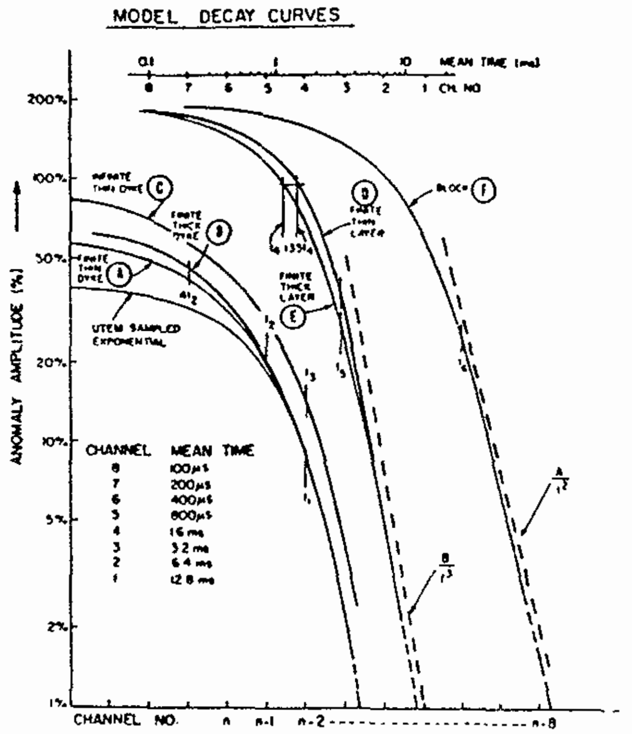


FIG. 13. The amplitude decay curves for the simple models of Figure 12. Mean sampling times are given for a base frequency of 30 Hz. The curve *UTEM sampled exponential* is a calculated function included for comparison. Lamontagne (1975) gives simple approximation formulas for interpreting target conductance from reference times $t_1, \ldots, t_6$ determined by translational curve matching.

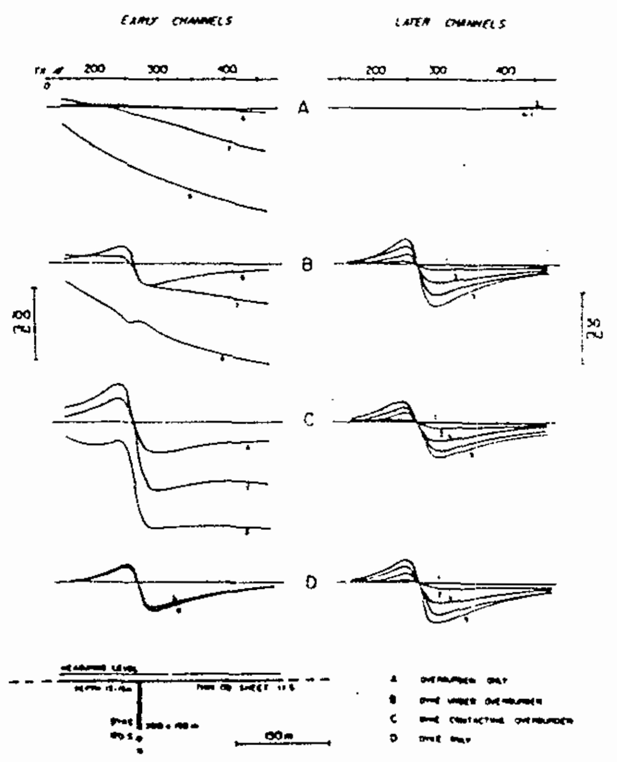


FIG. 14. Scale model UTEM H_z^s profiles over a conductive thin dike with overburden present.

Thin dike.—A conductive, steeply dipping body gives an H_z crossover shape similar to the plate model just discussed. The point where the anomaly changes sign indicates approximately the top edge of the conductor. The anomalies at later times tend to be broader and shifted slightly downdip from those at early times. The inductive decay rate of the anomalies will be discussed in a following section.

Surface horizontal finite conductor.—A thin horizontal conductor of limited dimensions (not extending under the loop) produces an anomaly consisting of a low over its central area, with large positive shoulders near its edge. The shoulders become rounded at later times and migrate towards the center of the conductor. Note that the thin horizontal plate shown in Figure 9 has a fairly deep location and thus the inward migration of the crossover points is less evident, although present.

Shallow block conductor.—This type of conductor produces a negative anomaly over its top having an amplitude of close to 200 percent at early times. An important characteristic of a block-like conductor is the absence of large positive flanking anomalies. The amplitude of the positive shoulders is less than 1/10 of the central negative, in contrast to the thin horizontal layer where the shoulders have amplitudes of order half the central negative. The sharpness of the crossovers at early time can be used as an indication of depth of burial. This type of anomaly is called a top anomaly and is due to a horizontal current pattern flowing around the top of the block.

Thick dike.—As might be expected, this is an intermediate case between a block and a thin dike where the width of a tabular body is of the same order as its depth of burial. In such cases the response is a combination of crossover and top anomaly due to vertical and horizontal current patterns, the top anomaly being more evident on the early-time channels and the crossover anomaly on later-time channels. The difference in decay rates results from the different scales of induced current flows, the top anomaly being controlled by the width of the dike, and the crossover by the depth extent.

Extensive horizontal conductors.—All the models with restricted lateral extent give rise to localized anomalies which simply change amplitude with time (approximately). The response of a very large conductor such as that shown in Figure 12e is included for comparison. In this case, the induced currents are not confined and they migrate horizontally with time.

Time response of simple free-space models.—Figure 13 shows *example decay plots of log anomaly amplitude versus log time* (channel number). The responses shown in Figure 13 are the UTEM sampled step responses that are only strictly valid for interpretation of actual field data when the observed anomalous response has effectively vanished at late times. Time scaling by lateral translation of the graphs is permitted for these cases, as previously discussed. The applicability of these time decays to interpretation is discussed by Lamontagne (1975), including the use of characteristic parameters to estimate conductance. A significant point to note is that simple induction in finite bodies eventually exhibits exponential decay at late time, whereas induction in infinite features takes the form of an inverse power law (Kaufman, 1978). Therefore, for models D, E, and F, the very late portion of the decay should ultimately show an exponential behavior if measured with sufficient sensitivity.

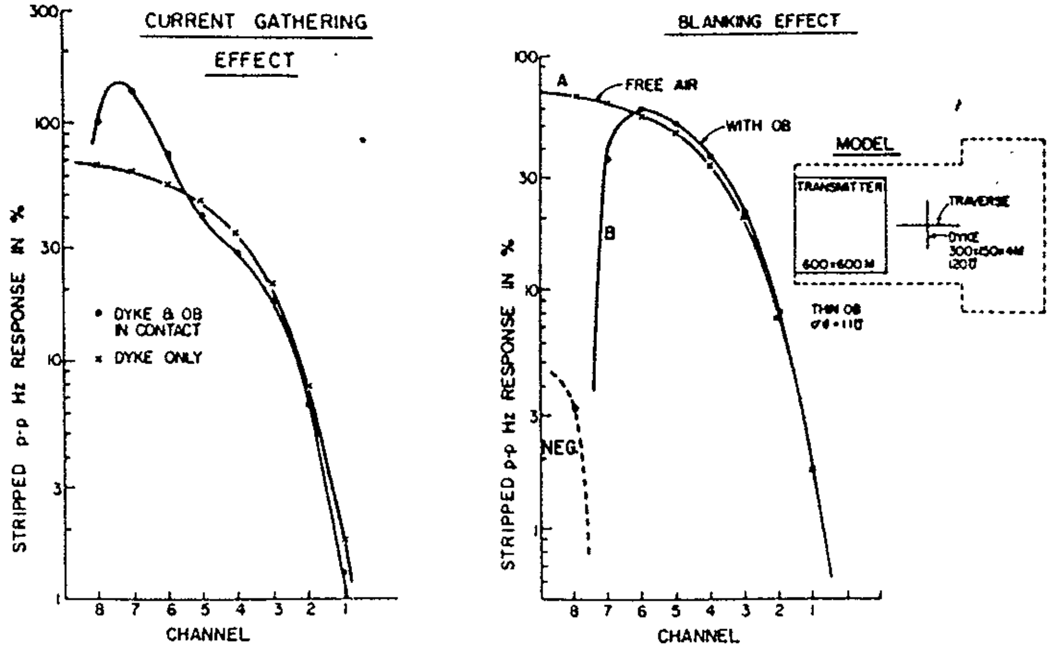


FIG. 15. Decay plots for the H_z^s anomalies of Figure 14.

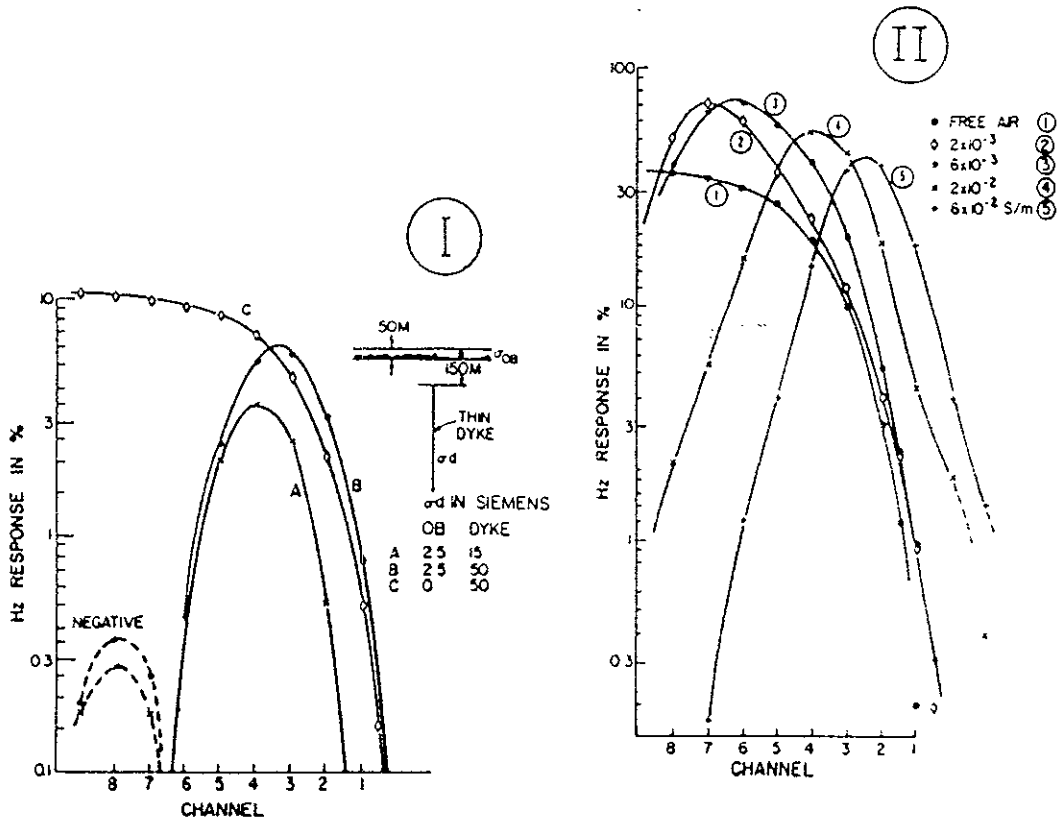


FIG. 16. Decay plots of H_z^s anomalies over a thin dike (I) under a conductive overburden and (II) in a conductive half-space.

Overburden effects

We will restrict the discussion of overburden and host-rock effects to the case of a simple vertical finite dike conductive target, which was studied by Lamontagne (1975) using a scale model. Conductive overburden cover can modify the responses of underlying conductors in two main ways. Let us consider a dike target whose response in free space is given in Figure 14d. If overburden is now placed over this target conductor, the resultant response (Figure 14b) is not just the sum of the overburden and dike response. At early times it can be seen that there is very little response from the dike. This is because the magnetic field (MSW analogy) has not yet penetrated the overburden, and it leads to the name "overburden blanking" for this characteristic. At later times (Ch 6-1), when we can see from Figure 14a that the field has completely penetrated the overburden layer, the dike and overburden response (14b) is virtually indistinguishable from that of the dike alone (14d). The time decay pattern of the peak-to-peak amplitude of the crossover is plotted in Figure 15. It clearly shows the blanking effect of the overburden at early times (right-hand figure). The minute negative response at earliest time is present only when the overburden extends under the loop, and appears to result from the complicated way in which the field first reaches the hidden target.

A second effect occurs when the dike is in conductive contact with the overburden. The results are quite different from those where the dike was not in contact (Figure 14c). In this case, regionally induced (analogous) current flow in the overburden has been "gathered" or "channeled" into the dike which is of higher conductivity. This accounts for the large-amplitude crossover anomalies at early times. Because the conductance of the dike greatly exceeds that of the overburden, the amount of current gathering is virtually independent of the dike's depth extent. The gathering effect at early times of just a "line conductor" remaining attached to the overburden after most of the dike was removed was found to be over 80 percent of that of the complete dike. At later times, when the (analogous) current flow in the overburden has migrated away (i.e., the real overburden current is no longer time-varying), the response is again almost identical to that of the dike alone. The time decay of the response is plotted on Figure 15, and in addition to the enhancement at early times a slight attenuation of the response at intermediate times can be seen.

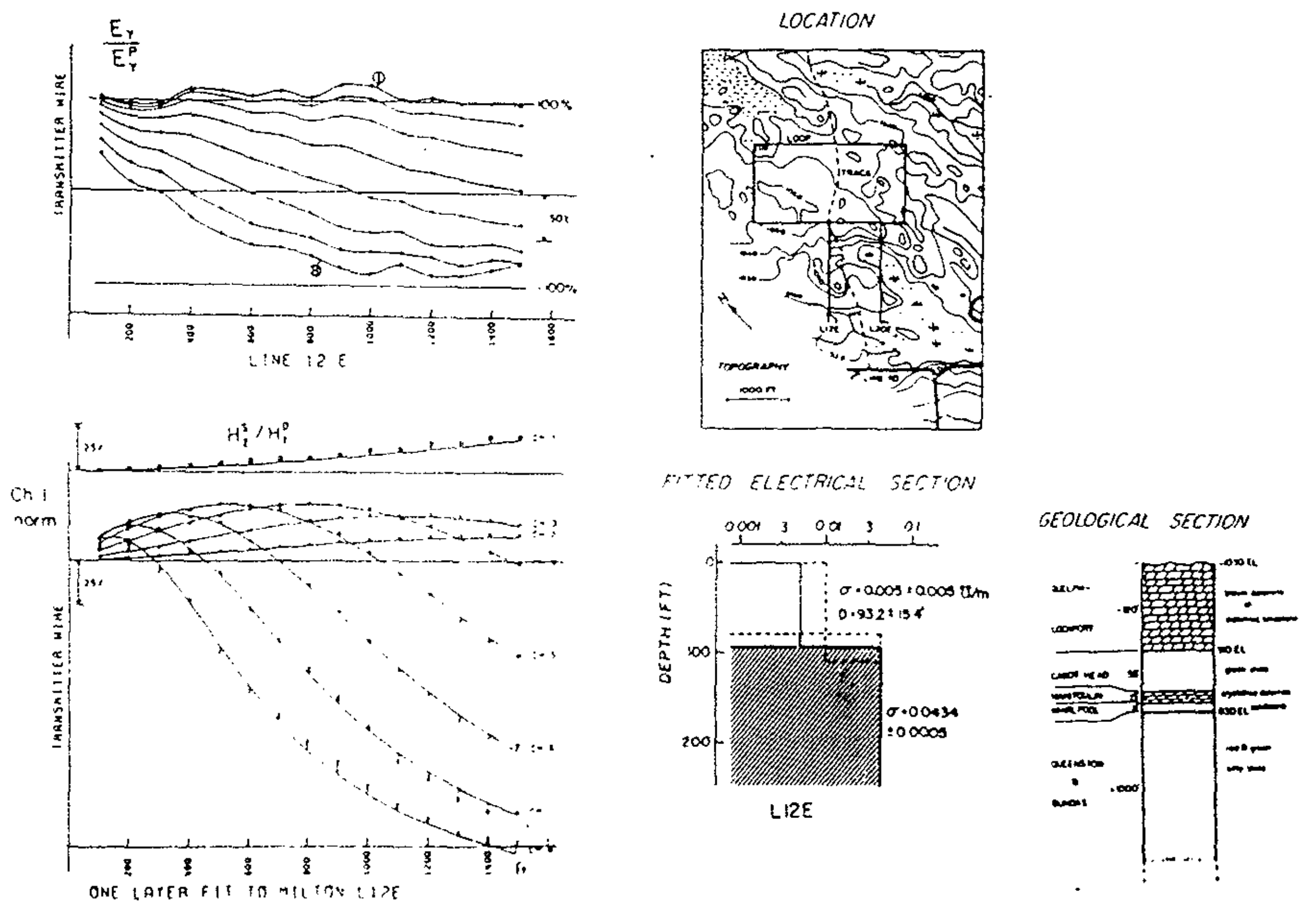


FIG. 17. Field example of E_y and H_z^s data from a well-stratified earth. The electrical section was obtained from inversion of the H_z^s data. The curves on the H_z^s graph are the theoretical model; the points are the field data. The bottom axis is at -150 percent. The geologic section is from nearby gas drilling exploration.

Host rock effects

Figure 16 II shows the time variation in response of a 60 S vertical plate located in a half-space. The results were calculated by Lamontagne (1975) by Fourier transformation of the frequency-domain numerical modeling of Lajoie and West (1976). At early times the response is reduced from the free-air response: this corresponds to blanking by the conductive region above the target. At later times the response is enhanced indicating that the regional (analogous) current in the host rock is being gathered into the plate at these times. For poorly conducting host rock, the response at late times is close enough to the free-space response that simple interpretation of the target using a plate in free-space model is valid. For the higher host conductivities (case 4, 5) this is no longer the case.

FIELD RESULTS

Milton, Ontario

This area was surveyed to demonstrate what data from a conductive, well-stratified earth looks like. The area is one where 650 m of flat-lying Paleozoic sediments overlie the Precambrian basement. The predominant member of the stratigraphy is a uniform and thick sequence of shale. Other beds are mostly resistive calcareous and sandstone formations. The survey area is covered by a mixed forest and marshy streams, with occasional outcrops. The top of the bedrock is a dolomite formation which is everywhere more than 20 m thick. Topographic relief is minor (<10 m), with occasional rough spots near outcrop. Overburden is probably less than 10 m every-

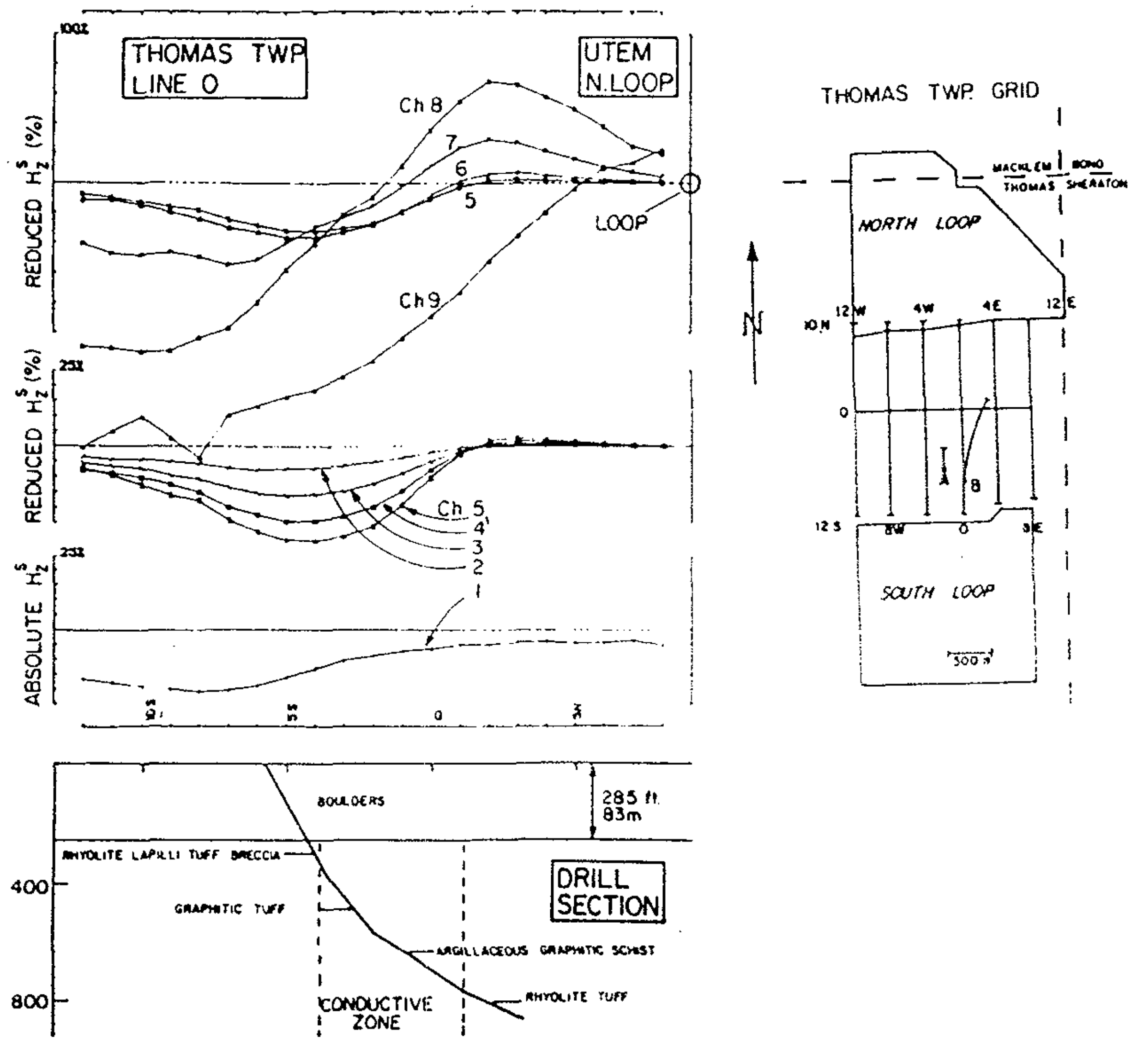


FIG. 18. A profile of H_z^s data from the north transmitter loop across the Thomas Twp test site. A map of the survey is included (different scale).

where and much less on average. It is mostly humus or thin glacial soil. Surface water is fresh, and likely quite resistive (> 100 Ωm). Figure 17 shows some of the data with a layer and half-space model fitted to it by iterative minimization of squared error. Also shown is a stratigraphic section from a well a few kilometers distant. The dolomite layer is too resistive for its conductivity to be determined by data whose earliest time sample is at 100 μs. (The survey was done with UTEM I.) At first glance, the data look just like that for any conductive earth, as the early-time data at the end of profiles have the usual strong negative anomaly, and there is a regular outward progression of crossovers as time progresses (decreasing channel number). However, the resistive surface layer does reveal itself in the limited approach of the early time curves to −200 percent anomaly. The convergence of E_y at late time to 100 percent of the primary field confirms the excellent lateral homogeneity of the site.

Thomas Township, Northern Ontario

This site has become an interesting test range for electrical methods, and a new grid has been cut and named the Nighthawk Lake geophysical test range. It is a graphitic zone that has many of the geometrical and electrical characteristics of a massive sulfide body. It is covered by 83 m of only moderately conductive overburden. It was found originally by airborne EM and has been intersected by two boreholes.

A UTEM II survey with 30 Hz base frequency was carried out on 6 lines of length 2200 ft and spacing 400 ft using transmitter loops to the north and south of the grid. Figure 18 shows a profile across the middle of the conductive zone.

At 50 μs (Ch 9), the regionally induced (analogous) current is only 500 ft from the loop. The field has not penetrated the overburden at the target site. From 100 μs to about 500 μs (Ch 8-6), a crossover response is observed over the target. At about

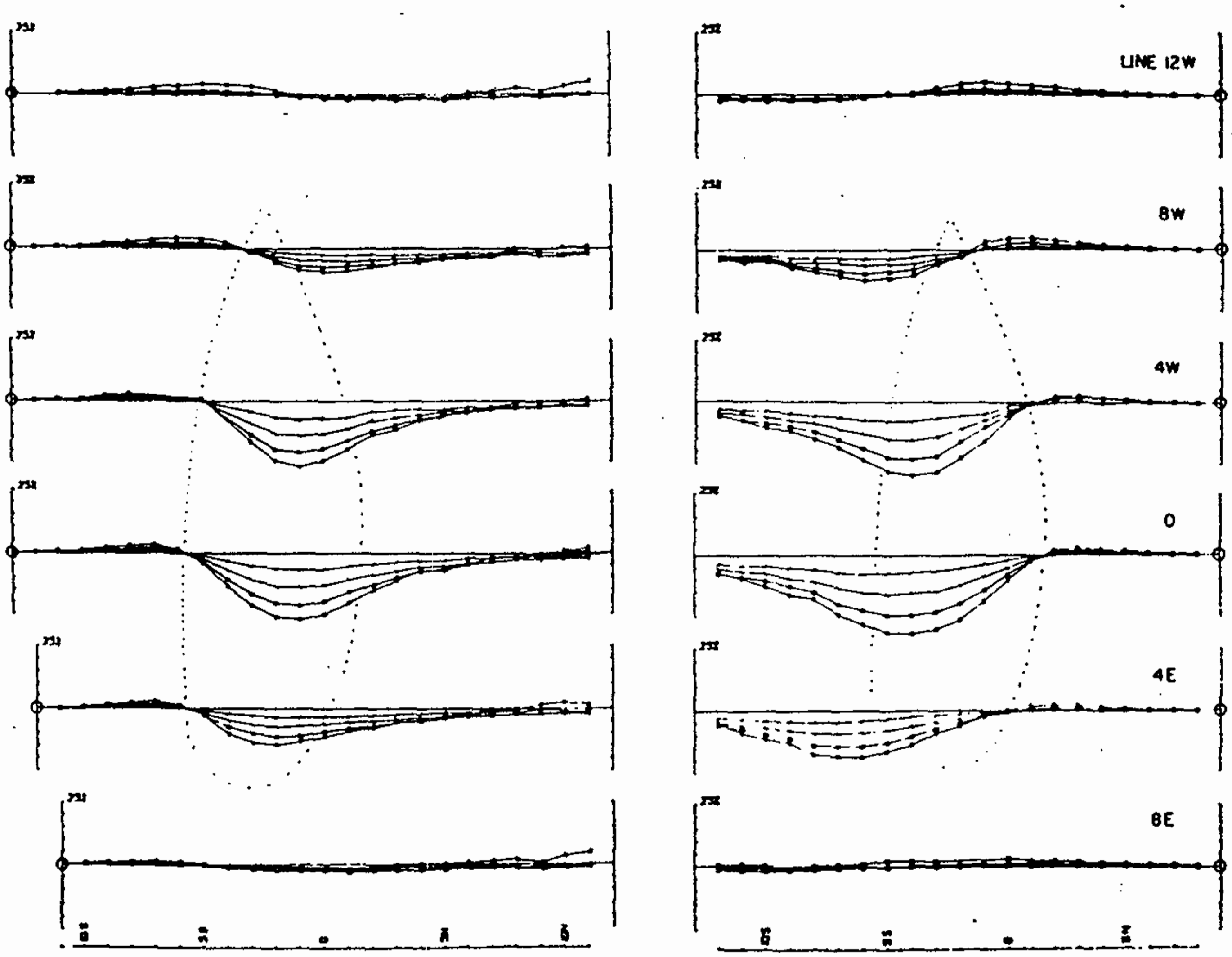


FIG. 19. Later time H_z' profiles (Ch 5-2) outline the perimeter of the conductor.

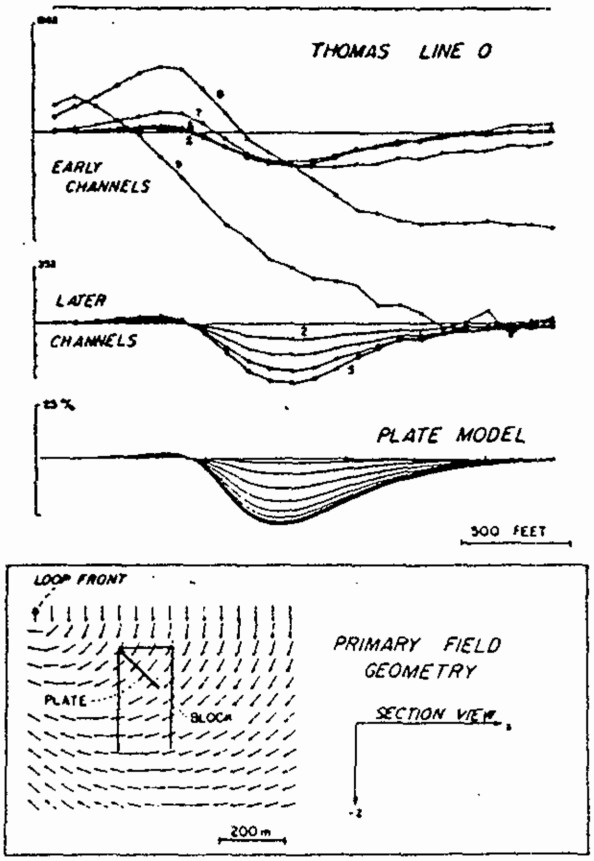


FIG. 20. Comparison of H_z^s data from the south transmitter loop with a free-space plate model. The configuration of the primary field is also shown.

500 μs the response changes to an asymmetric negative anomaly which decays much more slowly than the crossover response. The early-time crossover response is a current gathering or channeling anomaly where the (analogous) anomalous current flows along the length of the zone, while the longer time constant response is a local induction anomaly, where induced currents flow in a vortex within the target conductor.

Figure 19 shows a map of all the late-time profiles. They clearly delineate the edge of the target body. Figure 20 shows how a rectangular plate model can be found which models the observed results from one transmitter loop quite accurately, but which has to be rotated in order to match the results from the other loop. The late-time induced (analogous) current system in the actual conductor appears to be a tightly defined normal current in the front upper (near-loop) edge of the conductor with a more diffuse, return current deep in the rear of the body. A survey with the transmitter loop located on the other side of the body was similarly fitted by a plate dipping away from that loop, indicating the conductor to be a thick zone in which currents can flow in a variety of directions.

Electric fields were measured at the Thomas site. The late time vector map is shown in Figure 21, along with a rough numerical model. The conductive zone shows very clearly, although its edge is ill defined. Figure 22 shows a profile of the longitudinal component of electric field over the body. The field intensity is almost constant from channel 6 onward, and the main feature of the response is the aforementioned broad reduction in the field strength over the conductor. It is helpful, when looking at E field profiles, to imagine a plot on the same axes of the negative of the observed channel 1 response. This is the value the field starts from at the half-cycle transition. Even as early as 50 μs (Ch 9), the electric field has made most of its polarity reversal. In fact, between the loop to the target body it has overshot, while from the target body outwards it is changing relatively slowly. The time changes in E are actually very similar to those in H. There are two dominant decay times, a short one corresponding to the overburden and the channeling target response (Ch 8-6) and a long one corresponding to the local induction response (Ch 5-1). Also, these two E-field responses have a different geometrical form corresponding with the different forms of the magnetic anomalies. The scaled up version of the E data in Figure 22 shows the slowly decaying anomaly. Considerable noise is apparent in the data at this magnification.

Bedrock conductor beneath overburden

Figure 23 shows the measured secondary H_z fields at a site in Australia. The slow outward migration of the early-time channels and the −200 percent early-time limit away from the transmitter loop are characteristics of the response of a near-surface conductive weathered layer. This layer has a total conductance of about 4 S.

Around station 210W a more local superimposed crossover anomaly is evident which is fixed in location. This feature is evident over a great strike length. When the visually estimated overburden response is stripped from the anomaly and the peak-to-peak crossover response is plotted on a decay plot (Figure 26), the characteristics of early time blanking, time delay, and enhancement are clearly displayed. Corresponding to the model data of Figure 16, the early time blanking attenuates the local anomaly as the (analogous) magnetic field has not had time to penetrate the weathered layer. At intermediate times (Ch 5, 4) the response lies above a fitted free-space, half-plane conductor decay curve. This is partly an amplitude enhancement from current gathering and partly due to a small delay in time while the (analogous) magnetic field penetrates the near-surface conductor. It is not clear whether any of the L400S response can be identified as due to local induction. Nevertheless, the plotted induction curve for a half-plane in free space serves as a useful reference and establishes an upper limit on the conductance of the feature (7S in this case).

On two survey lines about 1 km away, the same local feature is observed, but the response has changed to one of longer time constant. As shown in Figure 24, a clear response persists through channels 2 and 1. These data are replotted with "point normalization" on Figure 25 to show the absolute secondary field. Absolute normalization preserves the true anomaly shape, but has the disadvantage of scaling up strongly those anomalies which lie near the transmitter. The stripped peak-to-peak response is plotted in decay form in Figure 26 and clearly shows the difference in time constant at the two locations.

The increase in time constant seen on line 600N is very significant, since little change is seen in the background response and only a lesser change in the blanking time. It indicates that the L600N late-time response is due to local induc-

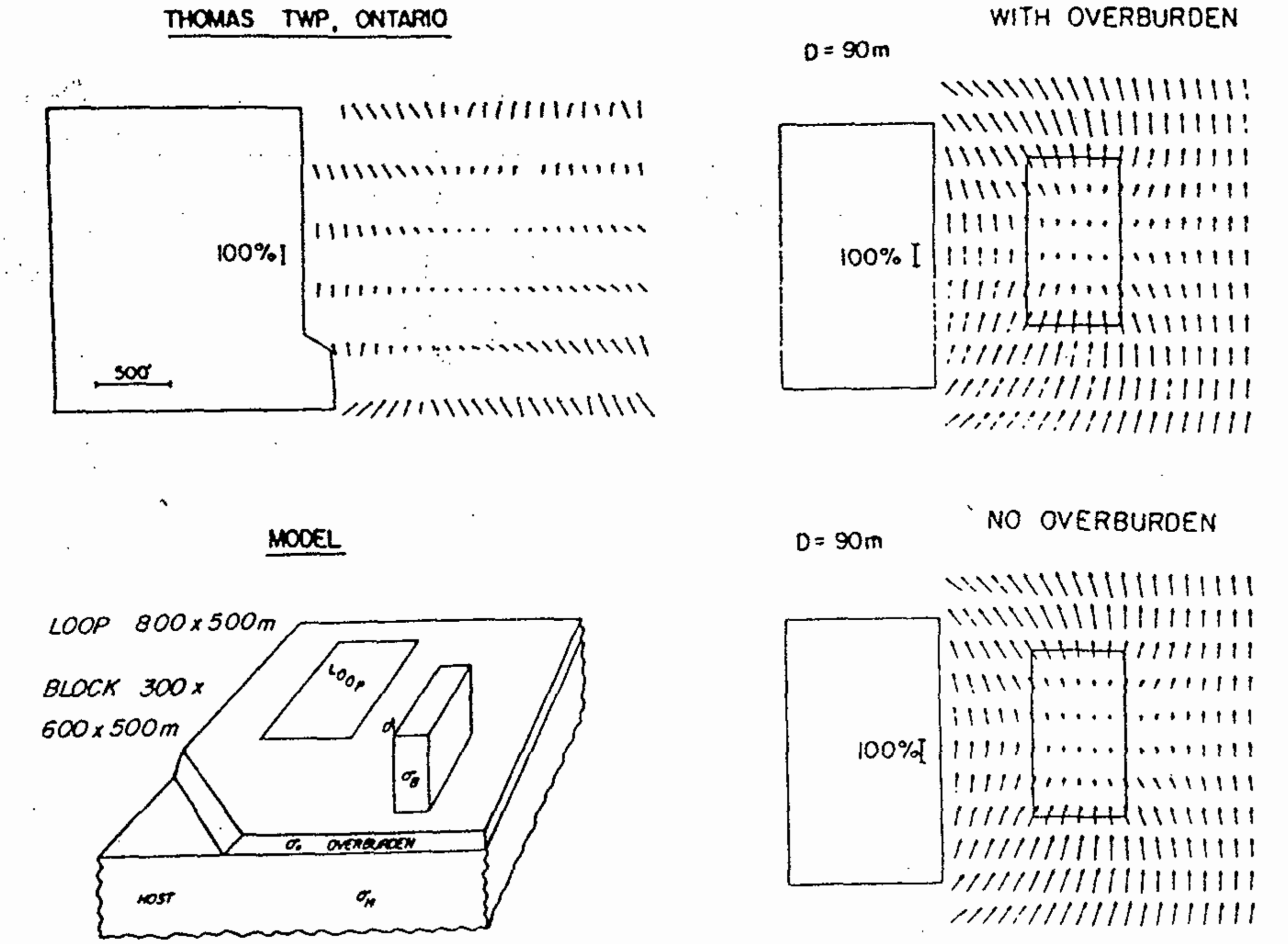


FIG. 21. Vector map of the late-time E field at Thomas Twp. A block model is included for comparison. The example is for a case where $\sigma_B \gg \sigma_O \gg \sigma_H \gg \sigma_{AIR}$.

tion. Model fitting of the decay, taking into account the limited strike extent of the long time constant response, leads to an interpretation of this feature as a local thickening of the half-plane conductor. The local conductance needed to produce the longer time constant is 120 S in contrast to the 7 S maximum of the rest of the bedrock conductor.

Drilling indicated that the extensive conductor was a 50 m thick calc-silicate zone containing both carbonates and sulfide lenses within a talc-sericite host. The locally more conductive part consisted chiefly of nearly massive noneconomic sulfides.

CONCLUSIONS

Experience with UTEM demonstrates that a wideband, time-domain EM system which measures the step response of the ground is electronically feasible and practical. Considerable field and modeling experience has shown that it is simple to use the amplitude information from such a system to aid significantly in interpretation. In our opinion the step response has a significant advantage over the impulse response for detection and interpretation of good conductors in the presence of poorer ones. Electric field data measured with the system can provide independent information about lateral conductivity contrasts and may be a useful aid in interpretation.

ACKNOWLEDGMENTS

Development of the UTEM system and its interpretational capability was funded from a number of sources. UTEM I was developed with support from the National Research Council of Canada. UTEM II instrumentation was supported by UMEX Ltd., Texasgulf Inc., and Cominco Ltd., with interpretational studies funded by a consortium of companies consisting of Aquitaine, Asarco, Cominco, Geoterrex, Gulf Minerals, Inco, Newmont, Noranda, Phelps Dodge, Selco, Shell Canada Resources, Texasgulf, and Umex. Graduate students, Y. Lamontagne, G. Lodha, J. Macnae, and M. Vallée, who worked on the project received stipendary and computing support from the

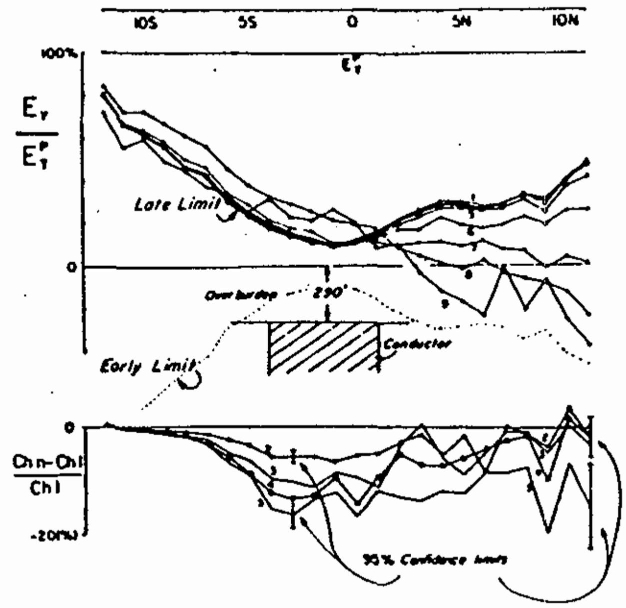


FIG. 22. Thomas Twp E_y data for line 0 from the south transmitter loop. The expanded scale data on the lower axes show that a very weak dynamic E field anomaly is associated with the main H_z^s late time response (Ch 5-1).

Natural Sciences and Engineering Research Council of Canada and the University of Toronto. All this assistance is gratefully acknowledged. We also thank an anonymous reviewer for a very careful, helpful review.

REFERENCES

Annan, A. P., The equivalent source method for electromagnetic scattering analysis and its geophysical application: Ph.D. thesis, Memorial Univ. of Newfoundland.

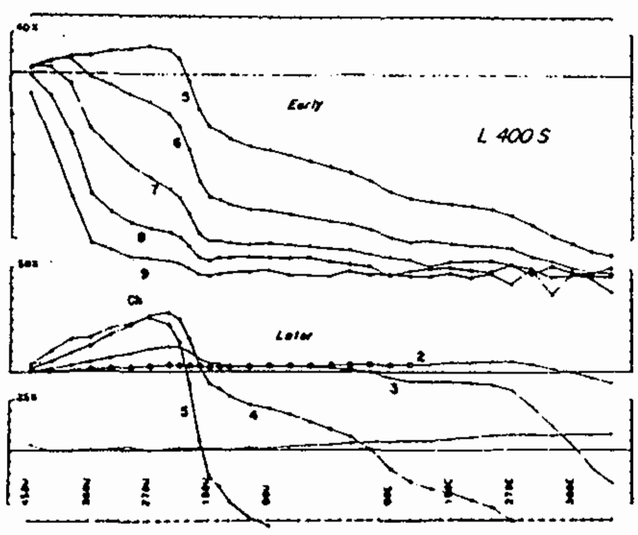


FIG. 23. H_z^s data from New South Wales showing the migrating crossovers of the overburden near the loop and a local anomaly around station 210 W. (Survey frequency 26 Hz.)

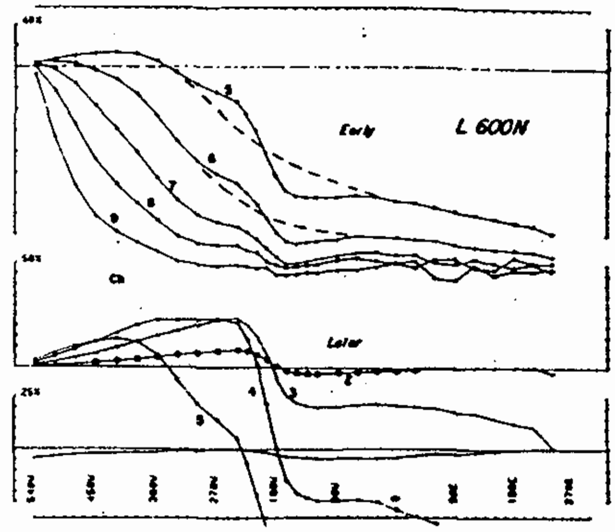


FIG. 24. H_z^s data on line 600N 1 km away from the previous figure showing a time decay of the local anomaly lasting to much later times. Remeasurement of the profile at 13 Hz gave virtually identical profiles (shifted one channel) with no visible Ch 1 anomaly.

Bosschart, R. A., 1964, Analytical interpretation of fixed source electromagnetic data: Doctoral thesis, Univ. of Delft.

Dyck, A. V., Bloore, M., and Vallée, M. A., 1980, User manual for programs PLATE and SPHERE: Res. in Appl. Geophys. 14, Geophys. Lab. Dept. of Physics, Univ. of Toronto.

Kaufman, A., 1978, Frequency and transient responses of electromagnetic fields created by currents in confined conductors: Geophysics, v. 43, p. 1002–1010.

Lajoie, J., and West, G. F., 1976, The electromagnetic response of a conductive inhomogeneity in a layered earth: Geophysics, v. 41, p. 1133–1156.

Lamontagne, Y., 1975, Applications of wide-band, time domain EM

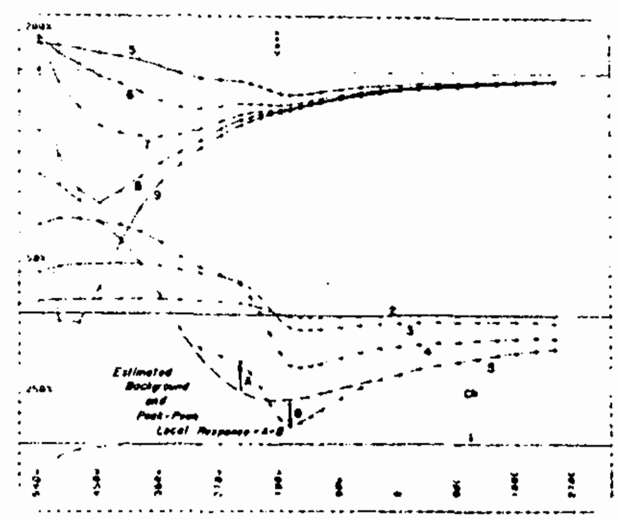


FIG. 25. Point normalized H_z^s from line 600N. The local secondary fields have been normalized to the constant primary field at station 210W and show how stripped peak-to-peak local anomaly amplitude is estimated.

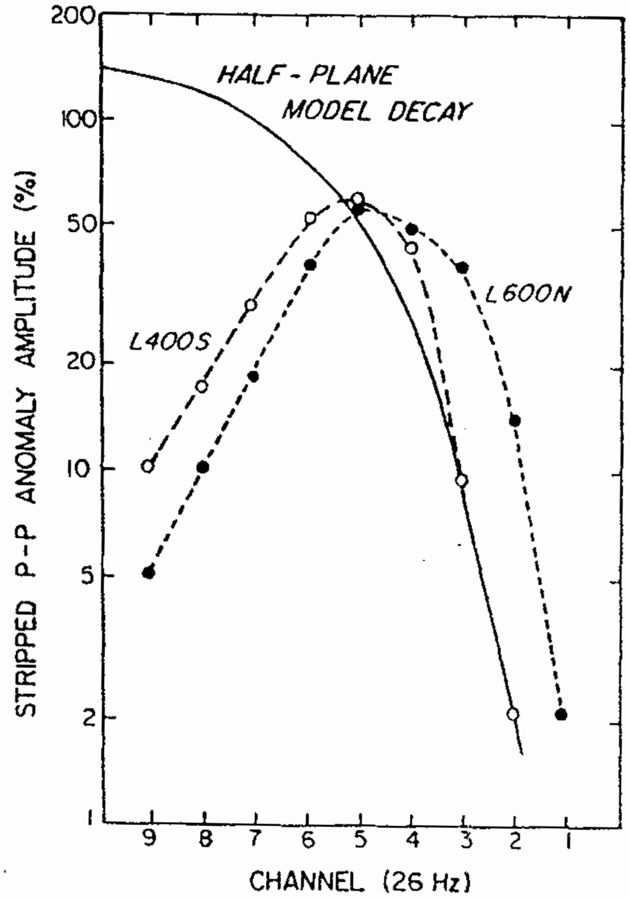


FIG. 26. Amplitude decay plot of stripped anomaly on lines 400S and 600N of the New South Wales survey.

measurements in mineral exploration: Ph.D. thesis, Univ. of Toronto; available as Res. in Appl. Geophys. 7, Geophys. Lab., Univ. of Toronto.

Lamontagne, Y., Lodha, G. L., Macnae, J. C., and West, G. F., 1977, Towards a deep penetration EM system: Paper presented at 79th annual meeting of the Can. Inst. of Min. and Metall., Ottawa, April; published in Bull. Austral. Soc. Expl. Geophys., v. 9, 1978.

——— 1980, UTEM, "Wideband Time-domain EM Project 1976–8, Reports 1-5"; Res. in Appl. Geophys. 11, Geophys. Lab., Dept. of Physics, Univ. of Toronto.

Lodha, G. L., 1977, Time domain and multifrequency electromagnetic responses in mineral prospecting: Ph.D. thesis, Univ. of Toronto; available as Res. in Appl. Geophys. 8, Geophys. Lab., Dept. of Physics, Univ. of Toronto.

Macnae, J. C., 1977, The response of UTEM to a poorly conducting mineralized environment: M.Sc. thesis, Univ. of Toronto.

——— 1980, The Cavendish test site: a UTEM survey plus a compilation of other ground geophysical data: Res. in Appl. Geophys. 12, Geophys. Lab., Dept. of Physics, Univ. of Toronto.

——— 1981, Geophysical prospecting with electrical fields from an inductive source: Ph.D. thesis, Dept. of Physics, Univ. of Toronto, 279 p.; available as Res. in Appl. Geophys., 18, Geophys. Lab., Univ. of Toronto.

Macnae, J. C., Lamontagne, Y., and West, G. F., 1984, Noise processing techniques for time-domain E.M. systems: Geophysics, v. 49, this issue, p. 934–948.

Maxwell, J. C., 1891, A treatise on electricity and magnetism: London, Clarendon Press, v. 2, 500 p.

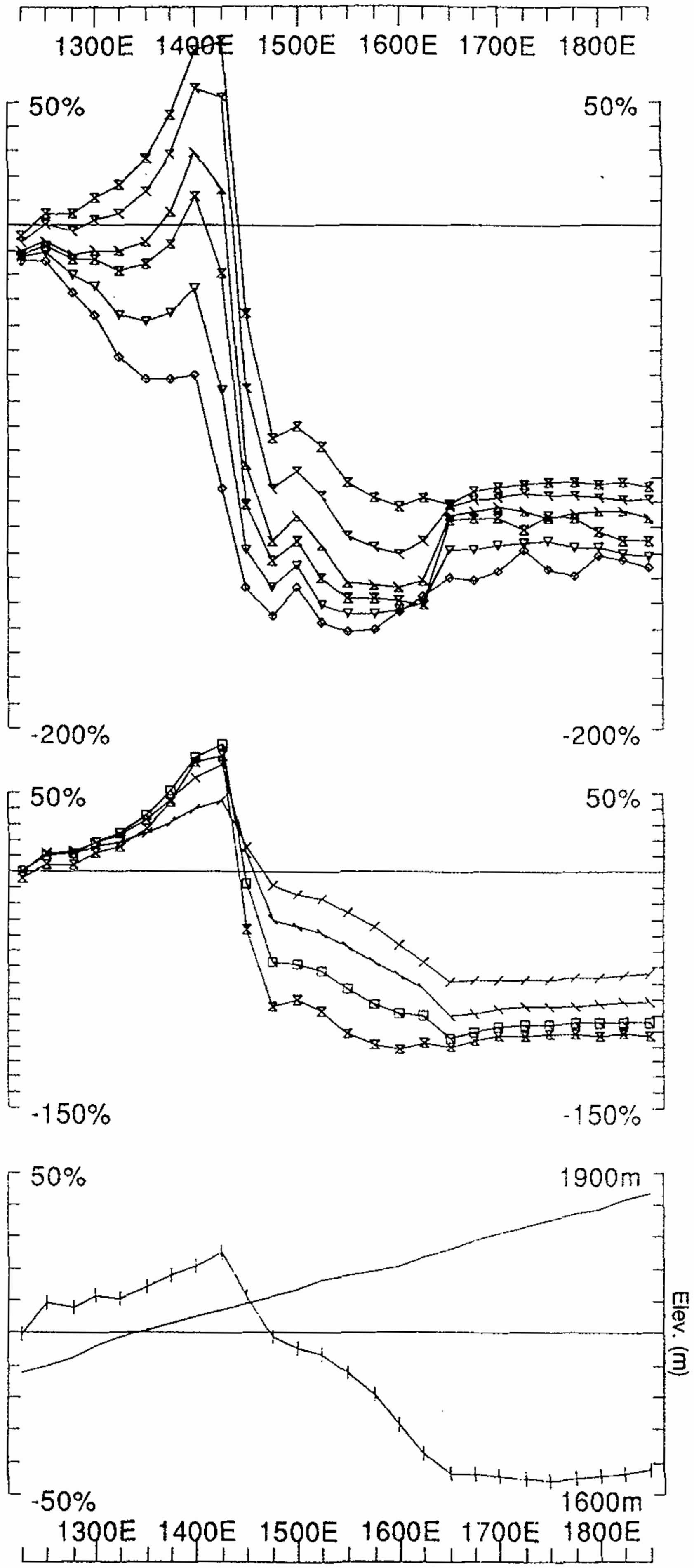
Nabighian, M. N., 1979, Quasi-static transient response of a conducting half-space—An approximate representation: Geophysics, v. 44, p. 1700–1705.

Podolsky, G., and Slankis, J., 1979, Izok Lake deposit, Northwest Territories, Canada. A geophysical case history: *in* Geophysics and Geochemistry in the search for metallic ores: P. J. Hood, ed., Econ. Geol. rep. 31, Geol. Survey of Canada.

Wait, J. R., 1962, Electromagnetic waves in stratified media: New York, MacMillan Co.

APPENDIX IV

data sections



UTEM Survey at: BAR CLAIM GROUP
For: MINER RIVER RESOURCES LTD.

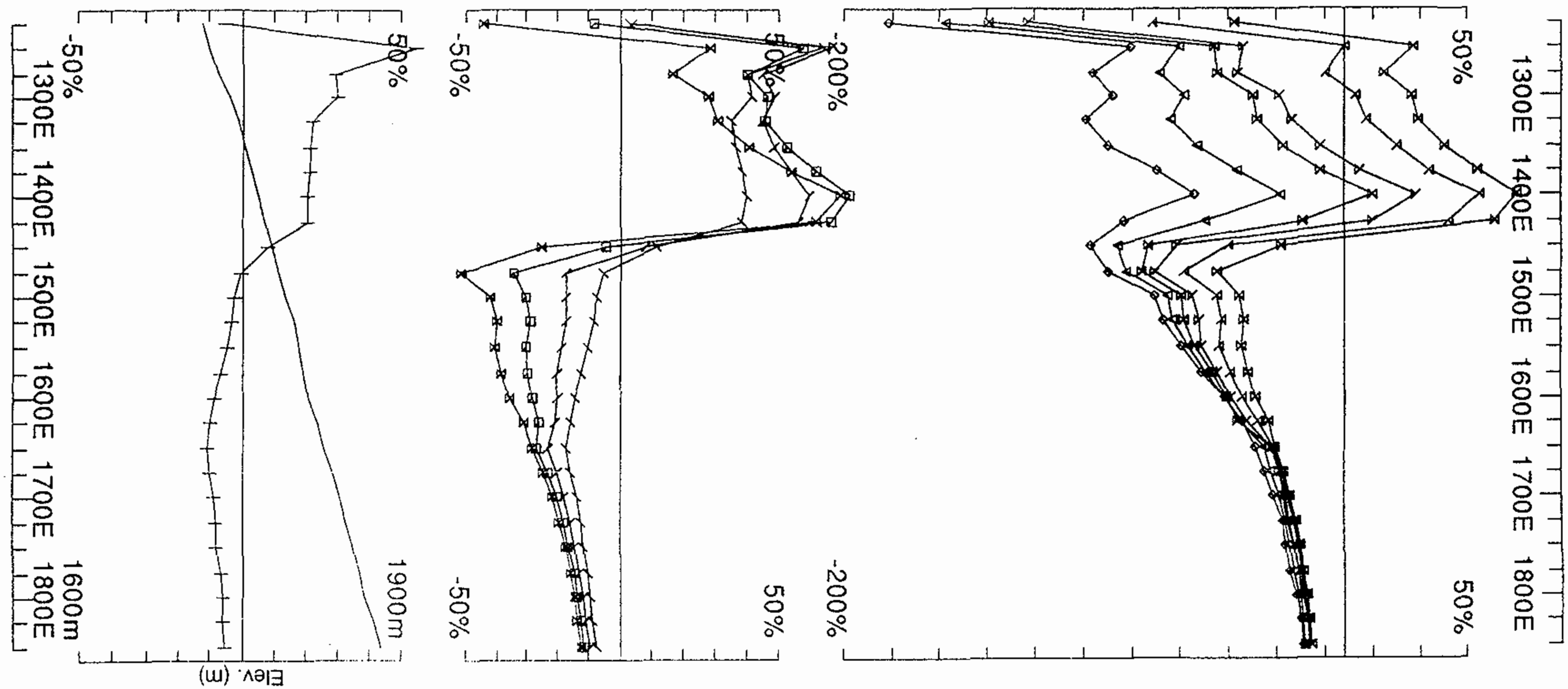
SJ GEOPHYSICS LTD.

Job 9417

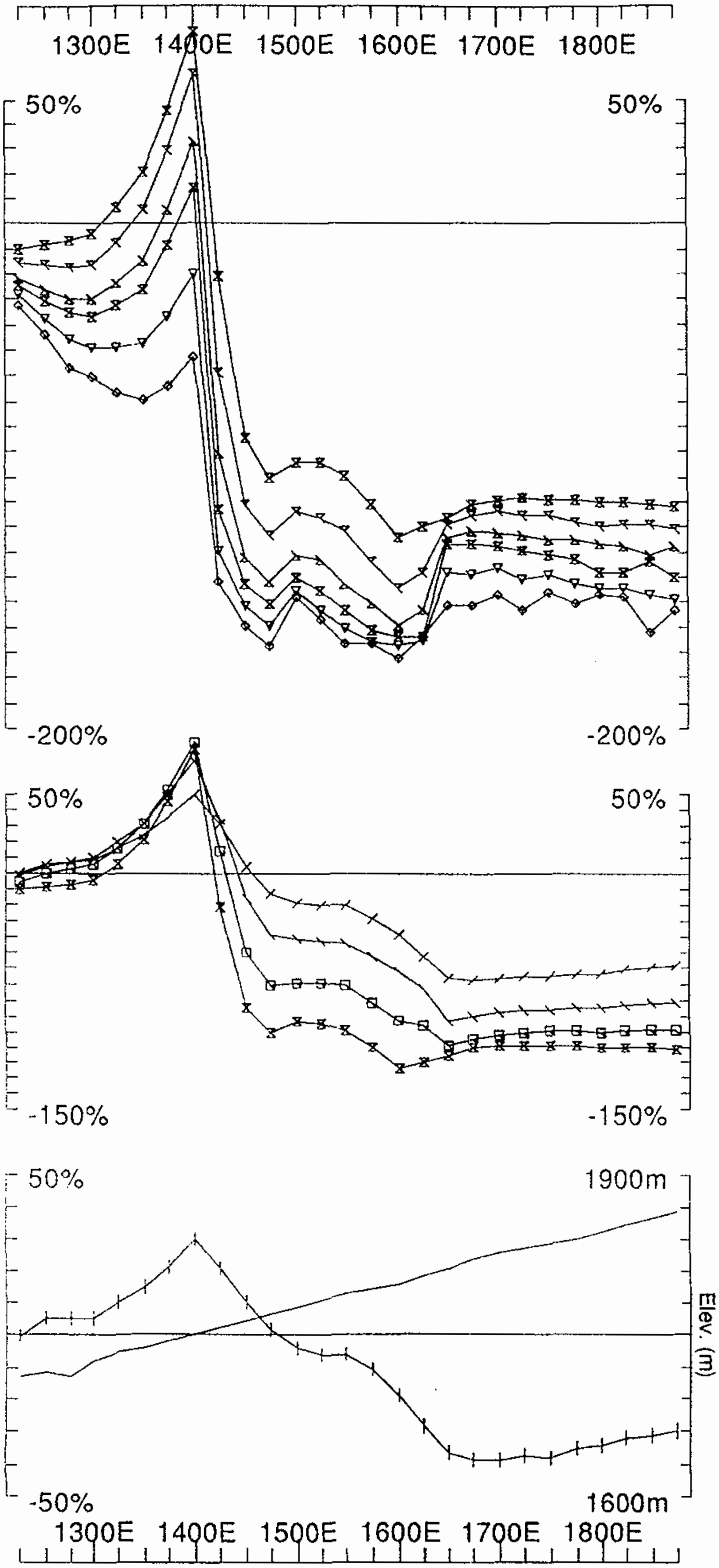
Surveyed : 19/7/94
Reduced : 20/8/94
Plotted : 23/8/94

Secondary, (Chn - Hpc)/|Hp|
Contin. Norm at depth of 0 m
Base Freq. 30.974 Hz

Loop: 2
Line: 0 N
Compt: Hz



Loop: 2	Secondary, (Chn - Hpc)/|Hp|	UTEM Survey at: BAR CLAIM GROUP
Line: 0 N	Point Norm.at stn 1400	For: MINER RIVER RESOURCES LTD.
Compt: Hz	Base Freq. 30.974 Hz	SJ GEOPHYSICS LTD. Job 9417 Surveyed : 19/7/94 Reduced : 20/8/94 Plotted : 23/8/94



UTEM Survey at: BAR CLAIM GROUP

For: MINER RIVER RESOURCES LTD.

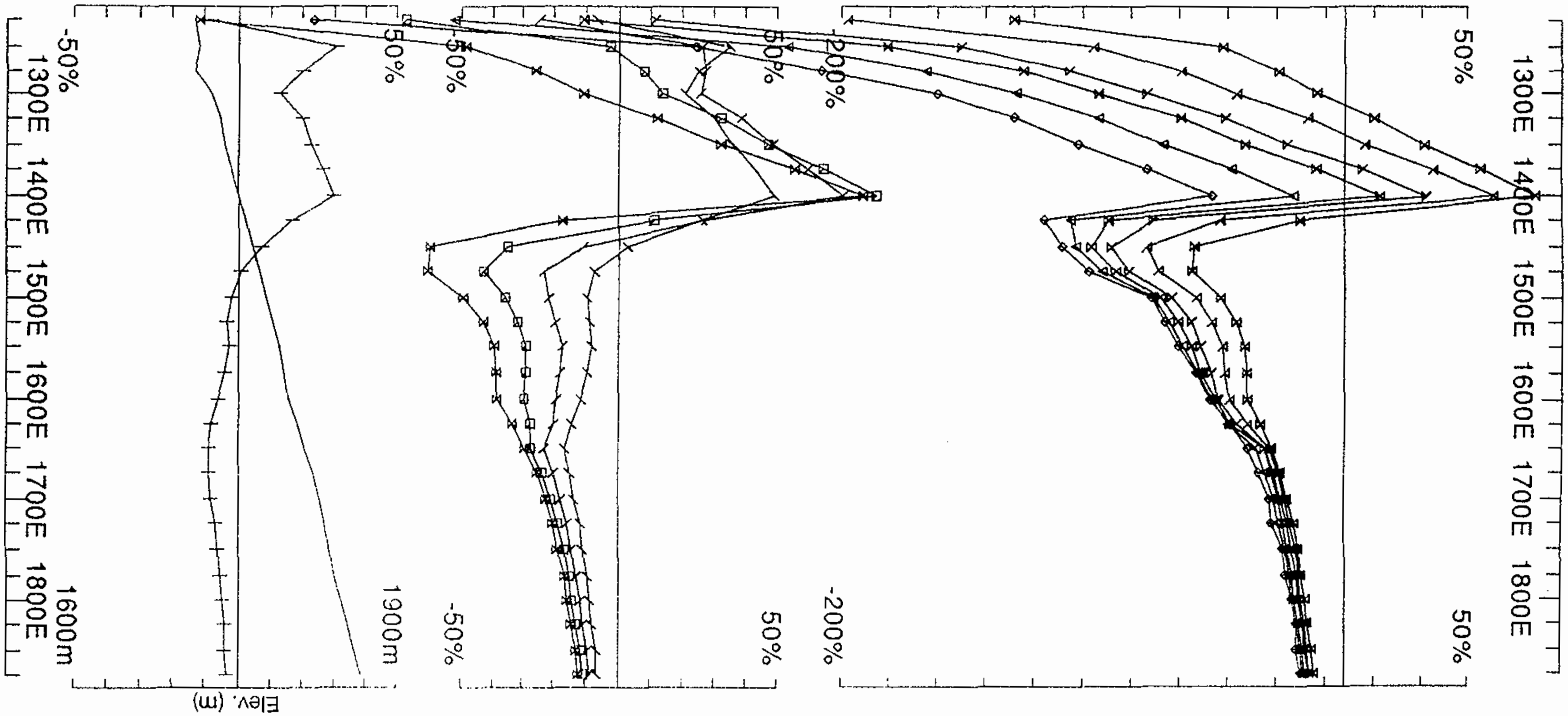
SJ GEOPHYSICS LTD.

Job 9417

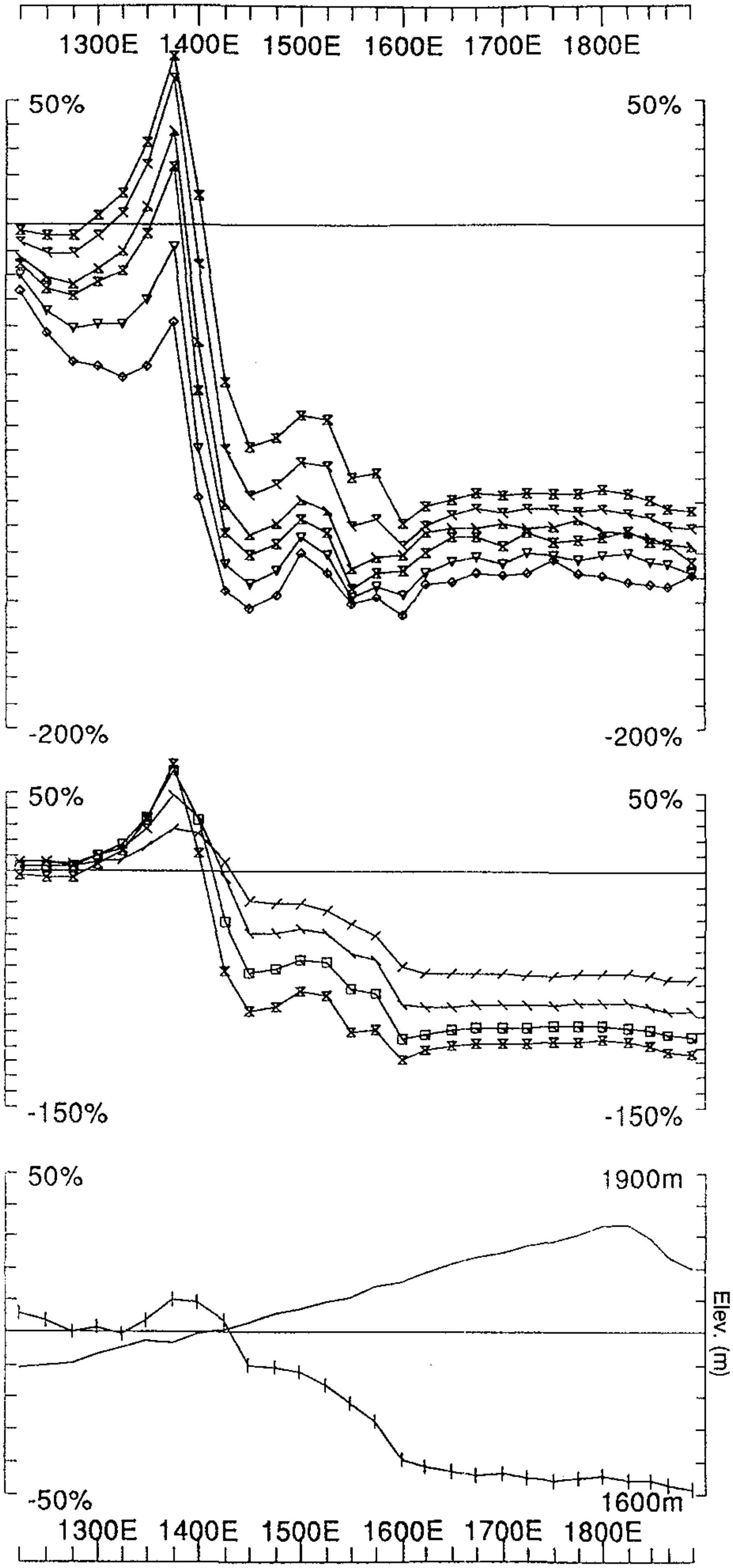
Surveyed : 3/7/94
Reduced : 20/8/94
Plotted : 23/8/94

Loop: 1
Line: 1 N
Compt: Hz

Secondary, (Chn - Hpc)/|Hp|
Contin. Norm at depth of 0 m
Base Freq. 30.974 Hz



Loop: 1	Secondary, (Chn - Hpc)/|Hp|	UTEM Survey at: BAR CLAIM GROUP
Line: 1 N	Point Norm.at stn 1400	For: MINER RIVER RESOURCES LTD.
Compt: Hz	Base Freq. 30.974 Hz	SJ GEOPHYSICS LTD. Job 9417 Surveyed : 3/7/94 Reduced : 20/8/94 Plotted : 23/8/94



Loop: 2
Line: 2 N
Compt: Hz

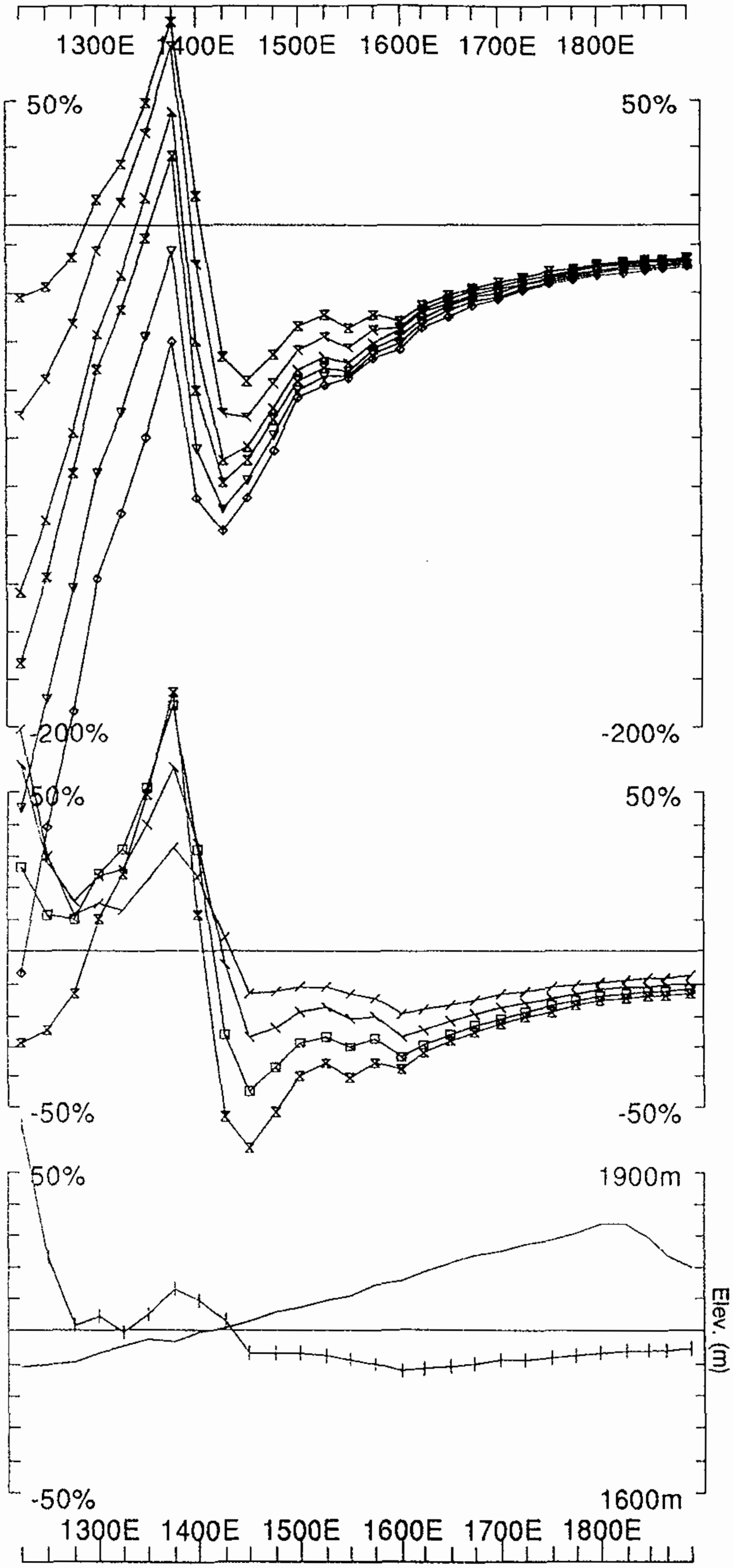
Secondary, (Chn - Hpc)/|Hp|
Contin. Norm at depth of 0 m
Base Freq. 30.974 Hz

UTEM Survey at: BAR CLAIM GROUP
For: MINER RIVER RESOURCES LTD.

SJ GEOPHYSICS LTD.

Job 9417

Surveyed : 19/7/94
Reduced : 20/8/94
Plotted : 23/8/94



Loop: 2
Line: 2 N
Compt: Hz

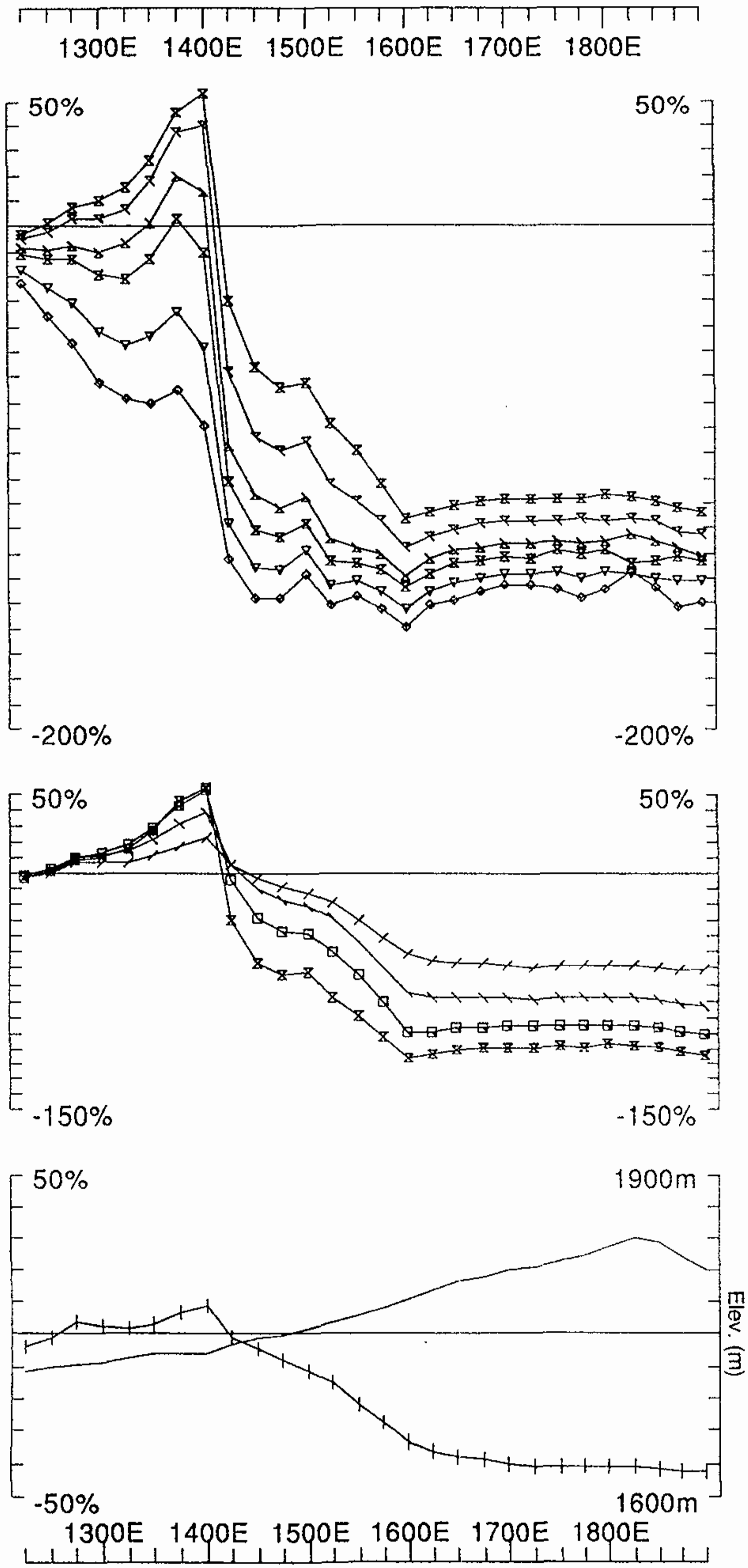
Secondary, (Chn - Hpc)/|Hp|
Point Norm.at stn 1400
Base Freq. 30.974 Hz

UTEM Survey at: BAR CLAIM GROUP
For: MINER RIVER RESOURCES LTD.

SJ GEOPHYSICS LTD.

Job 9417

Surveyed : 19/7/94
Reduced : 20/8/94
Plotted : 23/8/94



Loop: 2
Line: 3 N
Compt: Hz

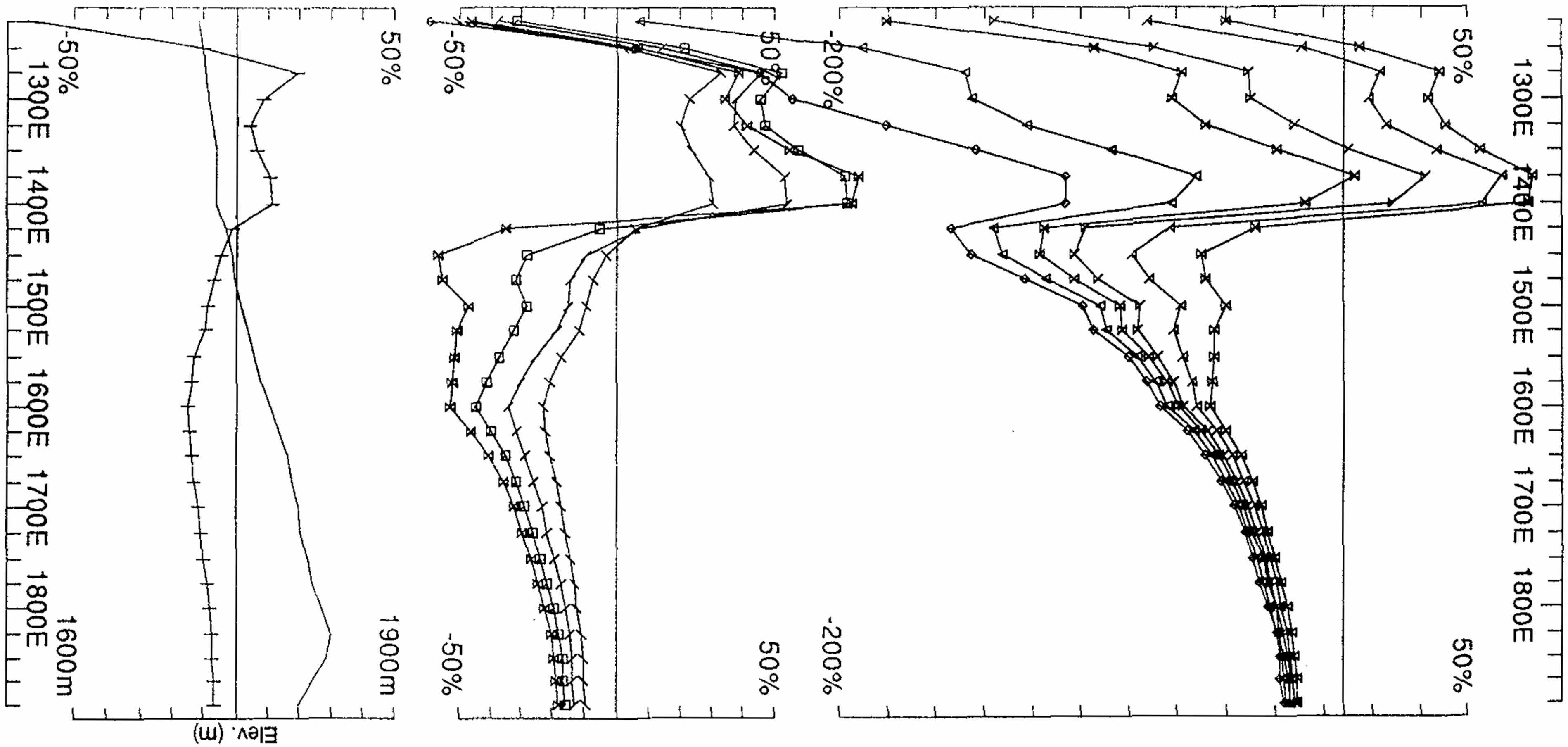
Secondary, (Chn - Hpc)/|Hp|
Contin. Norm at depth of 0 m
Base Freq. 30.974 Hz

UTEM Survey at: BAR CLAIM GROUP
For: MINER RIVER RESOURCES LTD.

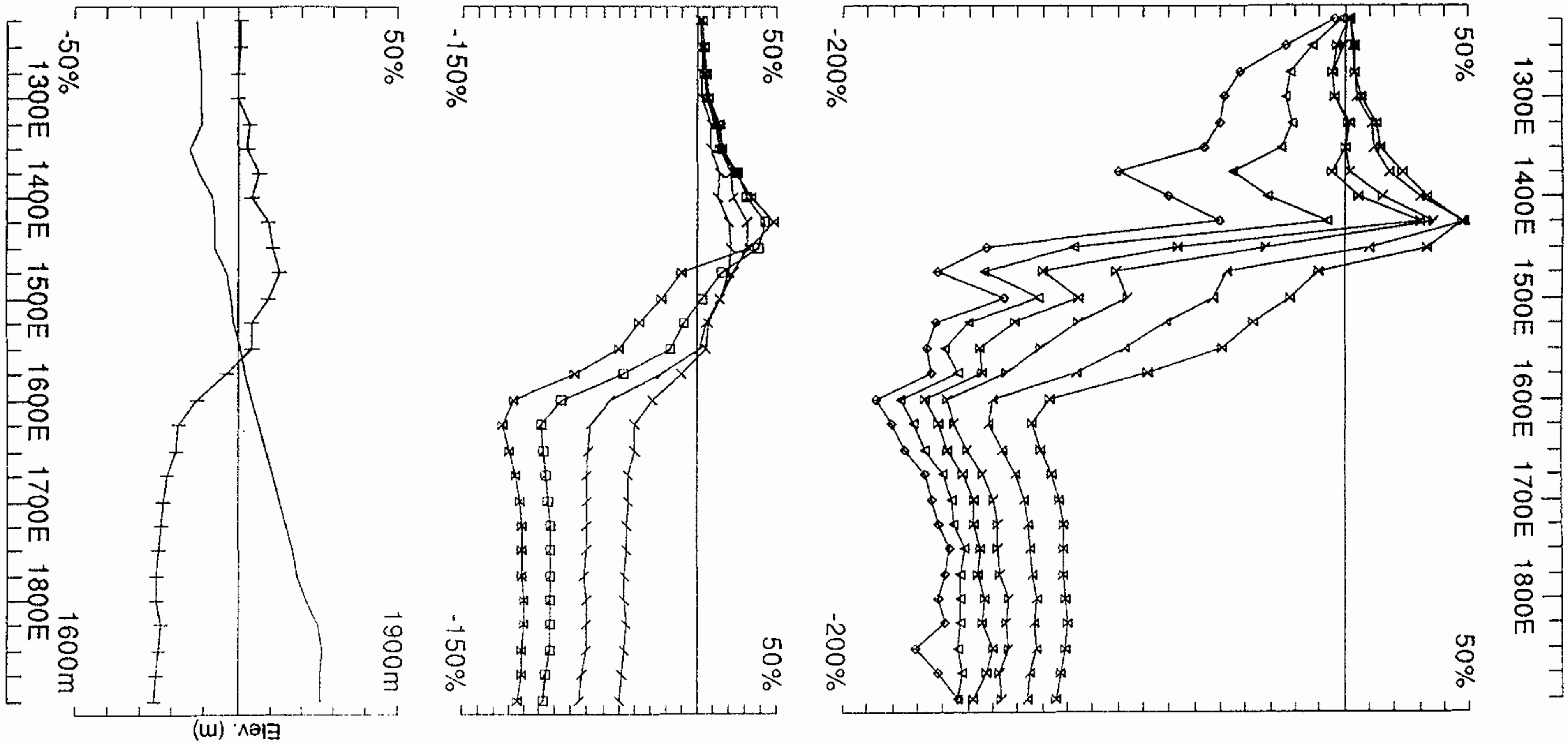
SJ GEOPHYSICS LTD.

Job 9417

Surveyed : 19/7/94
Reduced : 20/8/94
Plotted : 23/8/94



Loop: 2	Secondary, (Chn - Hpc)/|Hp|	UTEM Survey at: BAR CLAIM GROUP
Line: 3 N	Point Norm.at stn 1450	For: MINER RIVER RESOURCES LTD.
Compt: Hz	Base Freq. 30.974 Hz	SJ GEOPHYSICS LTD. Job 9417 Surveyed : 19/7/94 Reduced : 20/8/94 Plotted : 23/8/94



Loop: 1
Line: 4 N
Compt: Hz

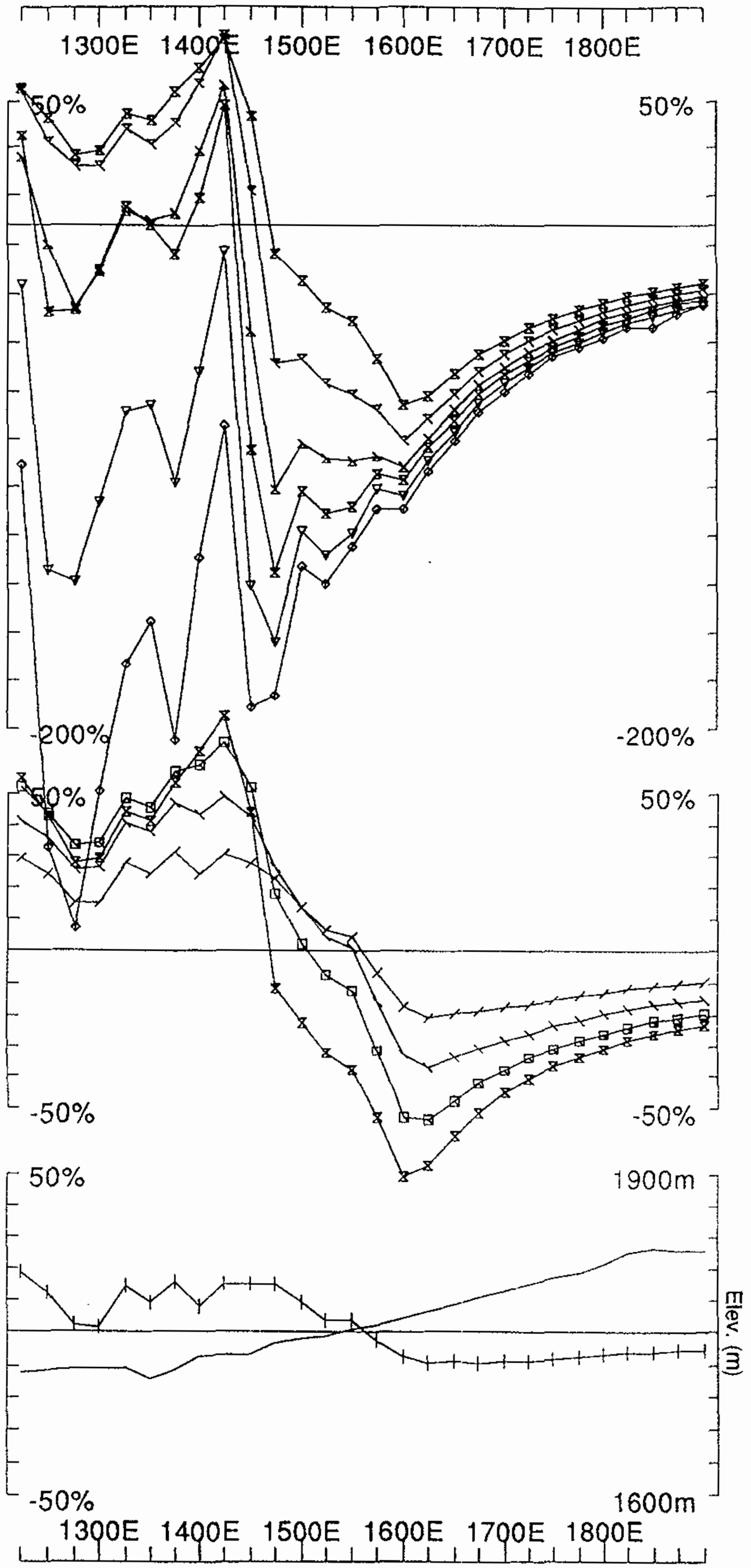
Secondary, (Chn - Hpc)/|Hp|
Contin. Norm at depth of 0 m
Base Freq. 30.974 Hz

UTEM Survey at: BAR CLAIM GROUP
For: MINER RIVER RESOURCES LTD.

SJ GEOPHYSICS LTD.

Job 9417

Surveyed : 4/7/94
Reduced : 20/8/94
Plotted : 23/8/94



Loop: 1
Line: 4 N
Compt: Hz

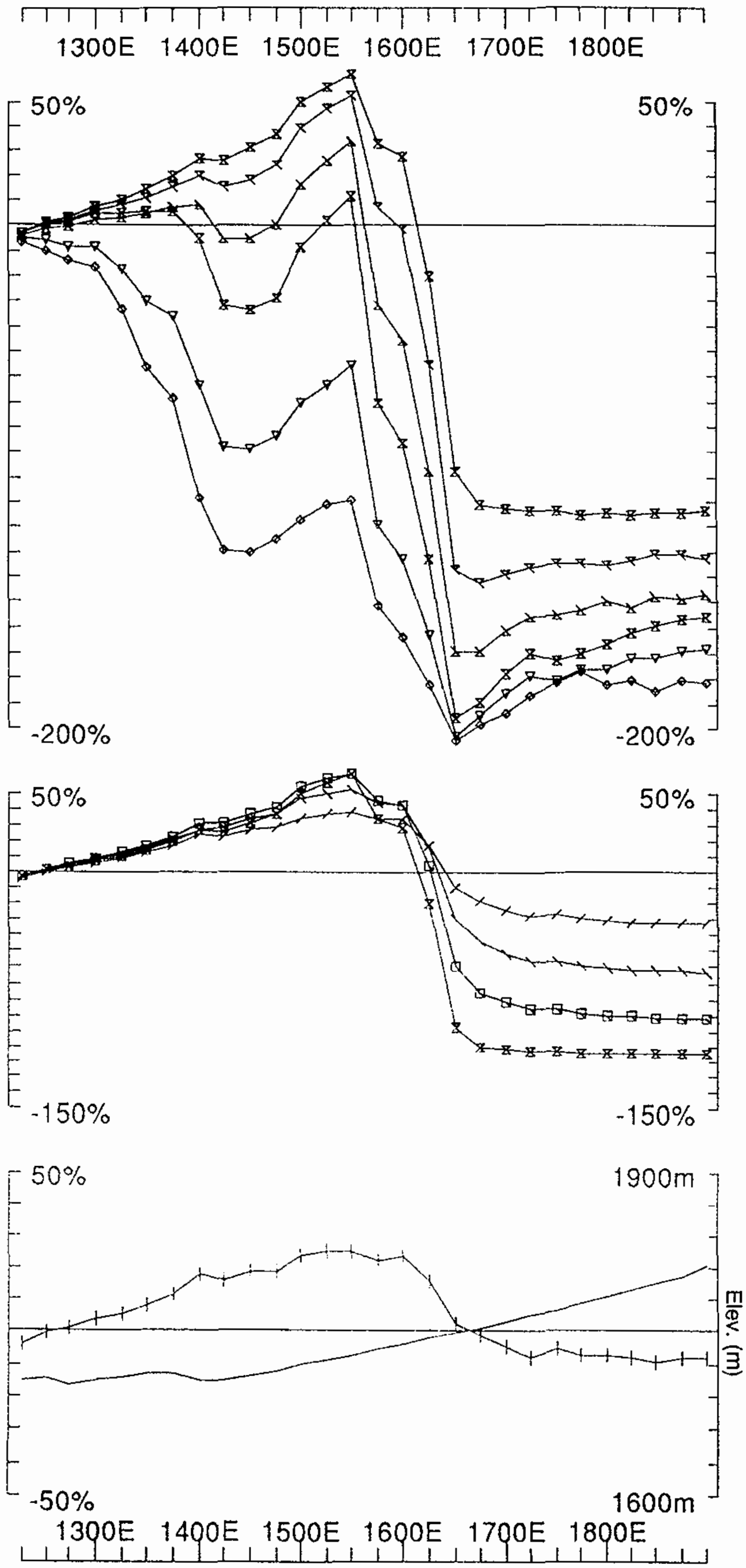
Secondary, (Chn - Hpc)/|Hp|
Point Norm.at stn 1500
Base Freq. 30.974 Hz

UTEM Survey at: BAR CLAIM GROUP
For: MINER RIVER RESOURCES LTD.

SJ GEOPHYSICS LTD.

Job 9417

Surveyed : 4/7/94
Reduced : 20/8/94
Plotted : 23/8/94



Loop: 1
Line: 5 N
Compt: Hz

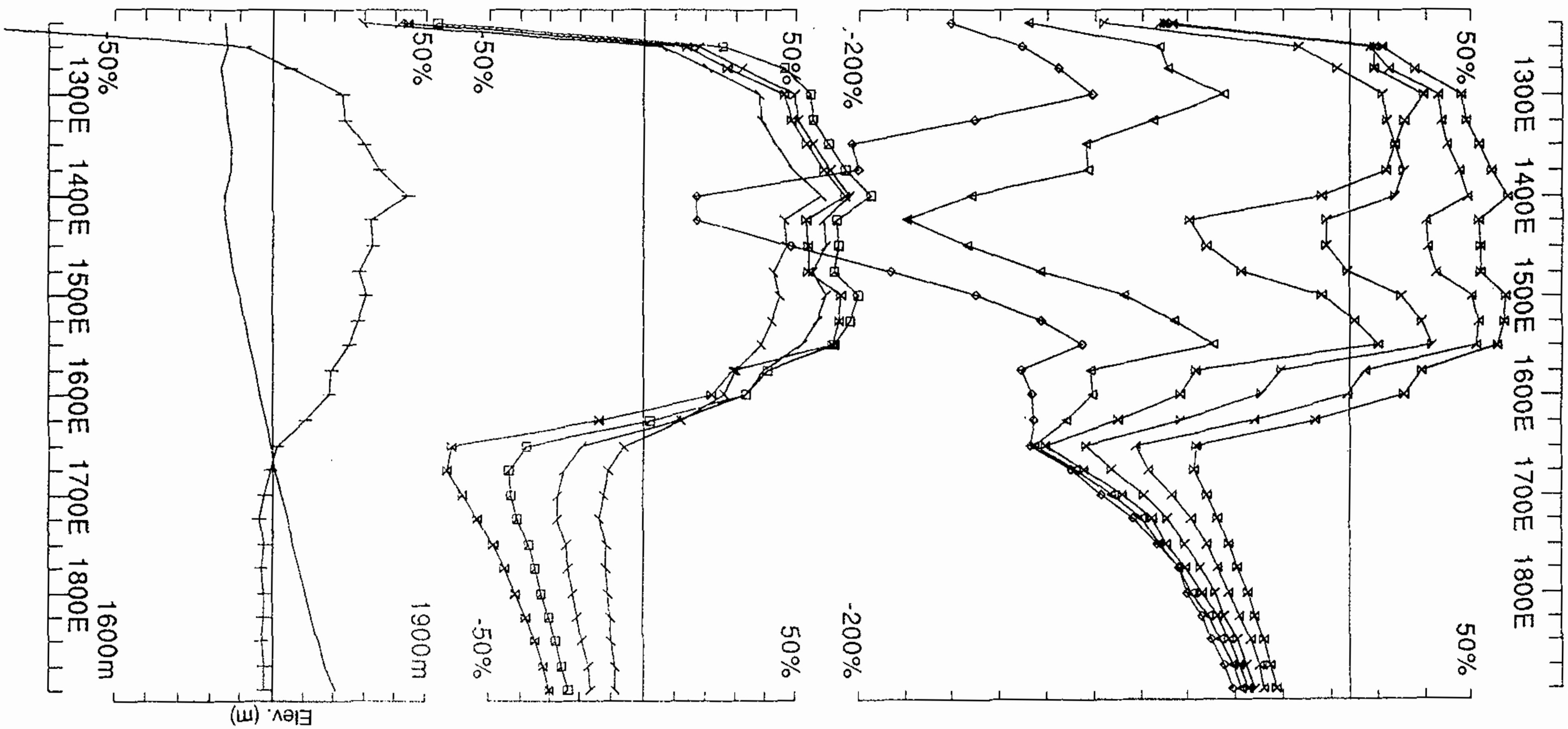
Secondary, (Chn - Hpc)/|Hp|
Contin. Norm at depth of 0 m
Base Freq. 30.974 Hz

UTEM Survey at: BAR CLAIM GROUP
For: MINER RIVER RESOURCES LTD.

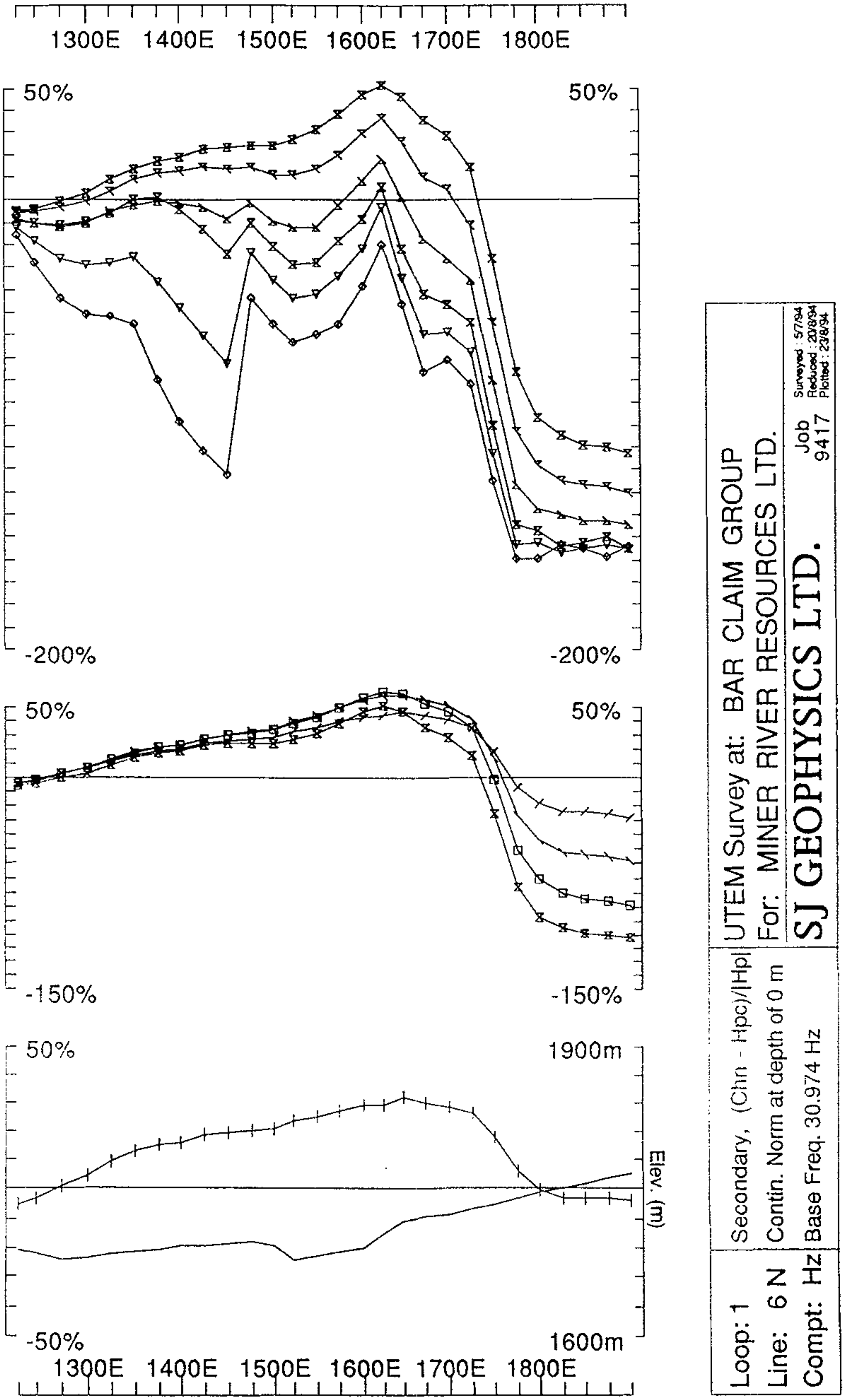
SJ GEOPHYSICS LTD.

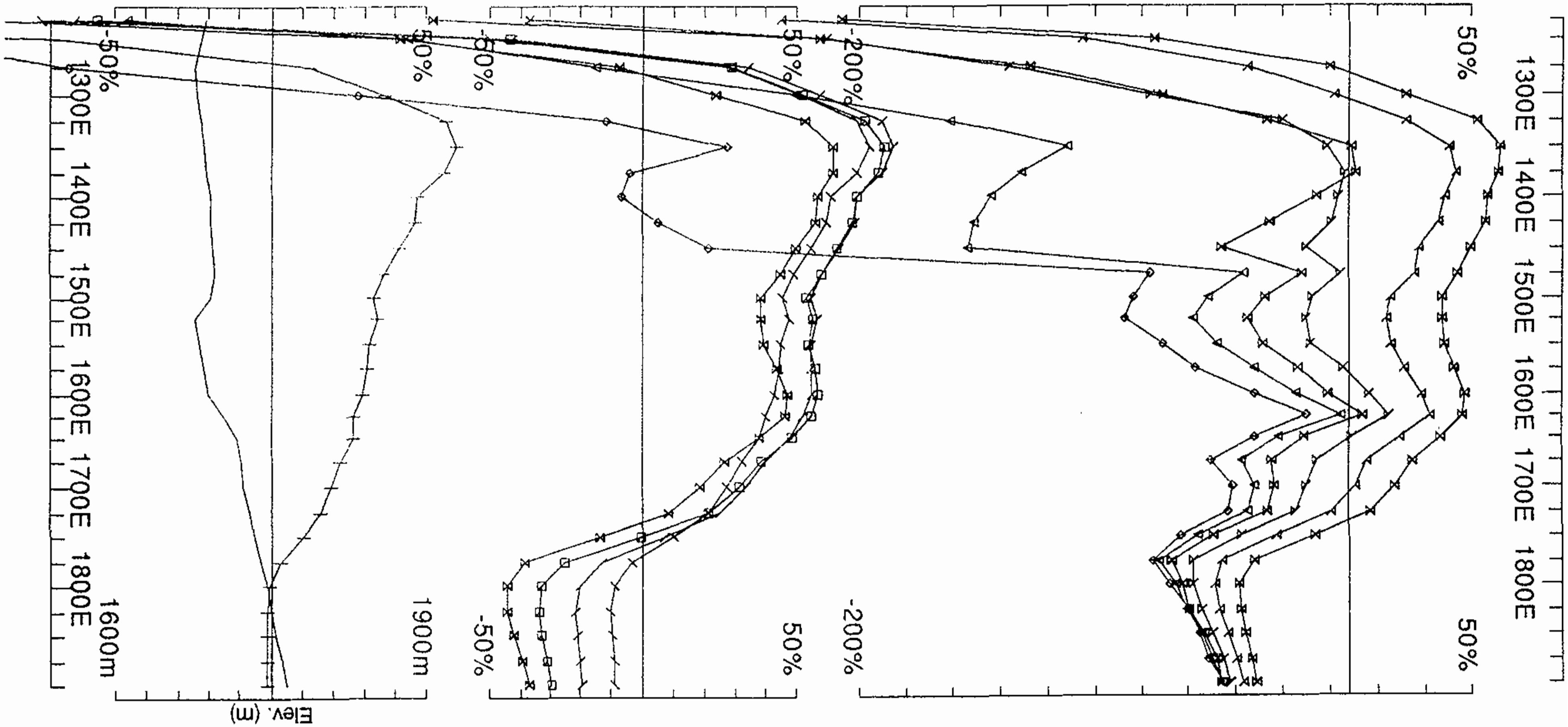
Job 9417

Surveyed : 4/7/94
Reduced : 20/8/94
Plotted : 23/8/94

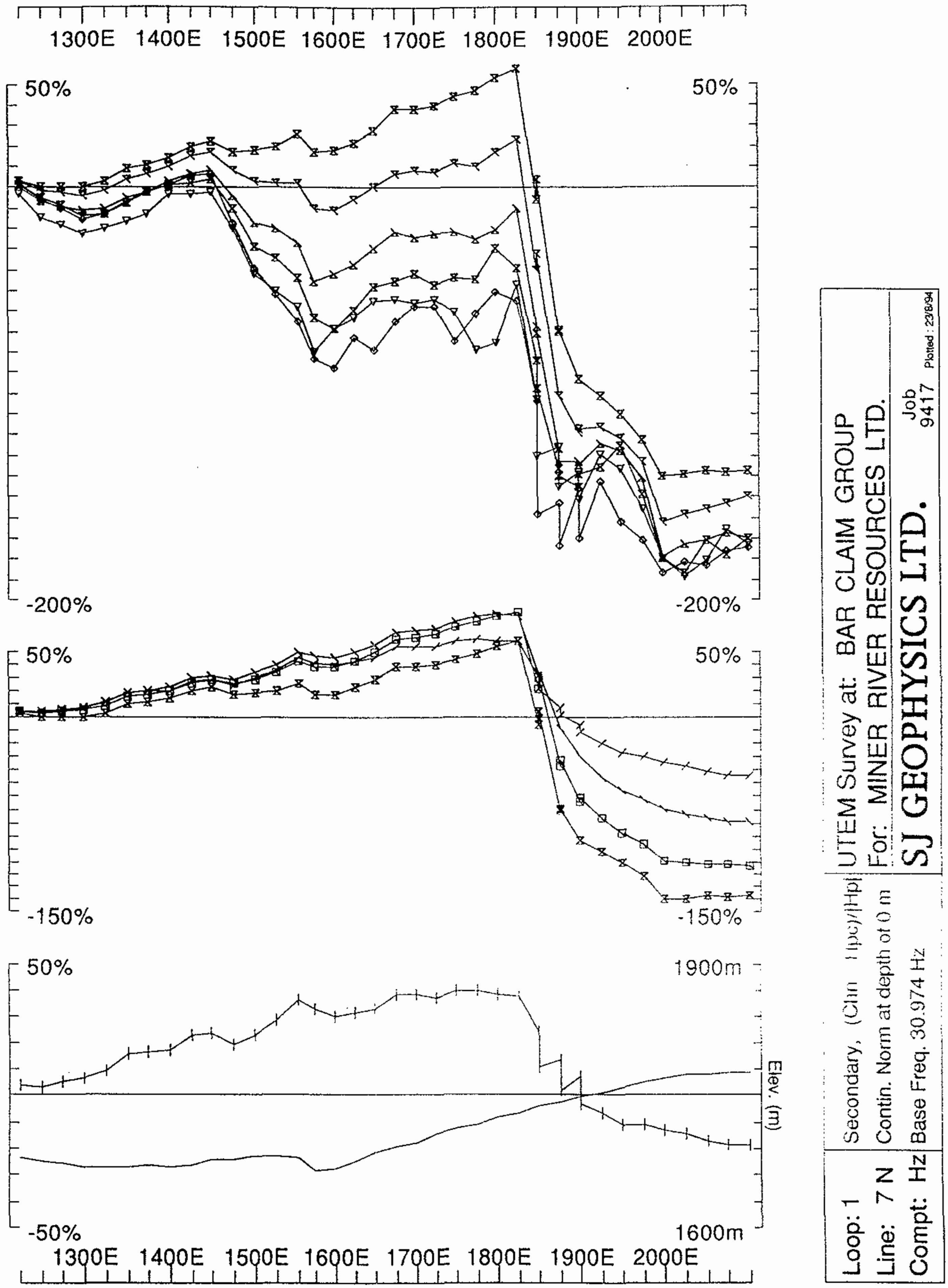


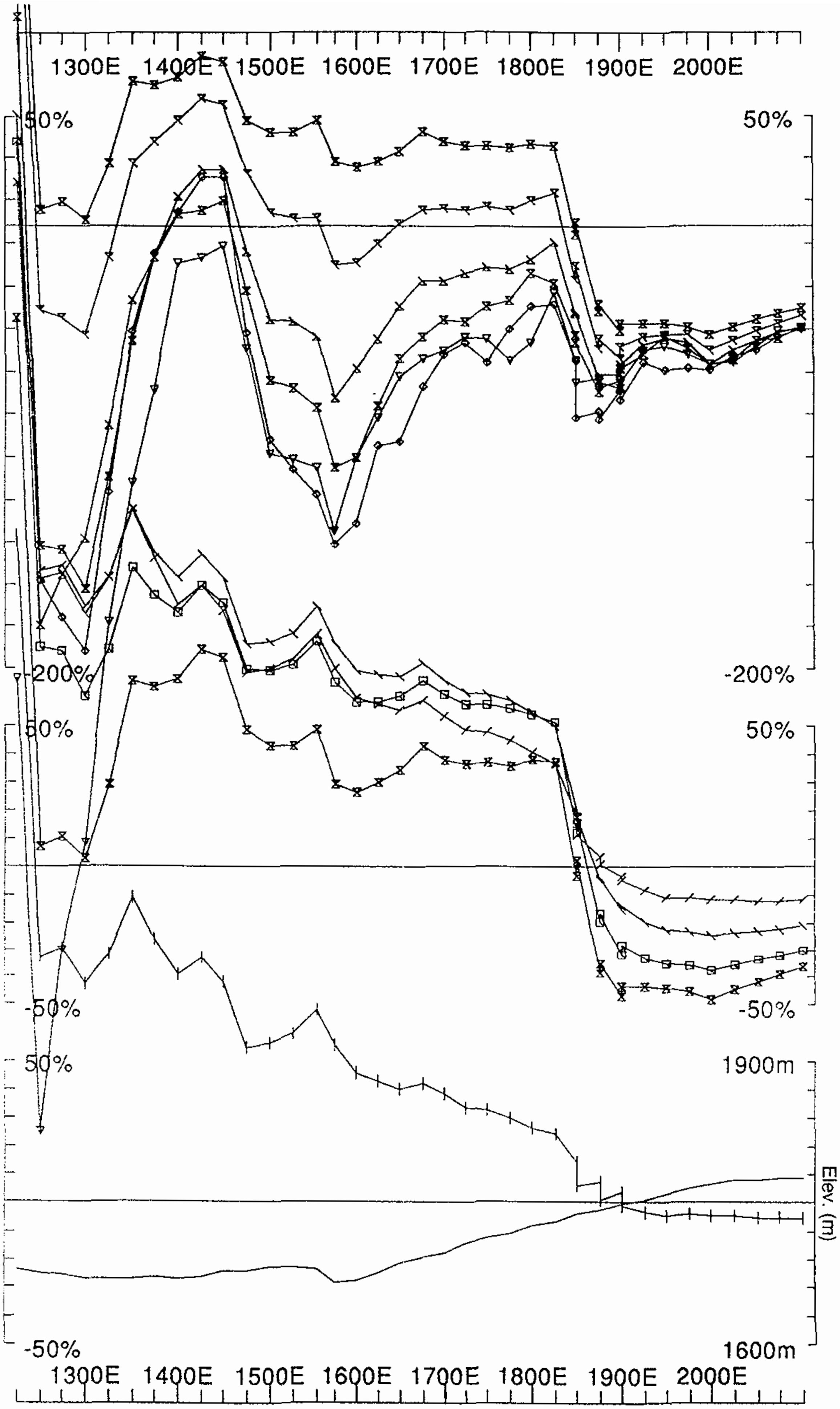
Loop: 1	Secondary, (Chn Hpc)/|Hp|	UTEM Survey at: BAR CLAIM GROUP
Line: 5 N	Point Norm.at stn 1550	For: MINER RIVER RESOURCES LTD.
Compt: Hz	Base Freq. 30.974 Hz	SJ GEOPHYSICS LTD. Job 9417 Surveyed : 4/7/94 Reduced : 20/8/94 Plotted : 23/8/94


1300E 1400E 1500E 1600E 1700E 1800E
50%
50%
-200%
-200%
50%
50%
-150%
-150%
50%
1900m
Elev. (m)
-50%
1600m
UTEM Survey at: BAR CLAIM GROUP
For: MINER RIVER RESOURCES LTD.
SJ GEOPHYSICS LTD.
Job 9417
Surveyed : 5/7/94
Reduced : 20/8/94
Plotted : 23/8/94
Secondary, (Chn - Hpc)/|Hp|
Contin. Norm at depth of 0 m
Base Freq. 30.974 Hz
Loop: 1
Line: 6 N
Compt: Hz



Loop: 1	Secondary, (Chn - Hpc)/|Hp|	UTEM Survey at: BAR CLAIM GROUP
Line: 6 N	Point Norm.at stn 1600	For: MINER RIVER RESOURCES LTD.
Compt: Hz	Base Freq. 30.974 Hz	SJ GEOPHYSICS LTD. Job 9417 Surveyed : 5/7/94 Reduced : 20/8/94 Plotted : 23/8/94


1300E 1400E 1500E 1600E 1700E 1800E 1900E 2000E
50%
50%
-200%
-200%
50%
50%
-150%
-150%
50%
1900m
Elev. (m)
-50%
1600m
1300E 1400E 1500E 1600E 1700E 1800E 1900E 2000E
UTEM Survey at: BAR CLAIM GROUP
For: MINER RIVER RESOURCES LTD.
SJ GEOPHYSICS LTD.
Job 9417
Plotted : 23/8/94
Loop: 1
Line: 7 N
Compt: Hz
Contin. Norm at depth of 0 m
Base Freq. 30.974 Hz



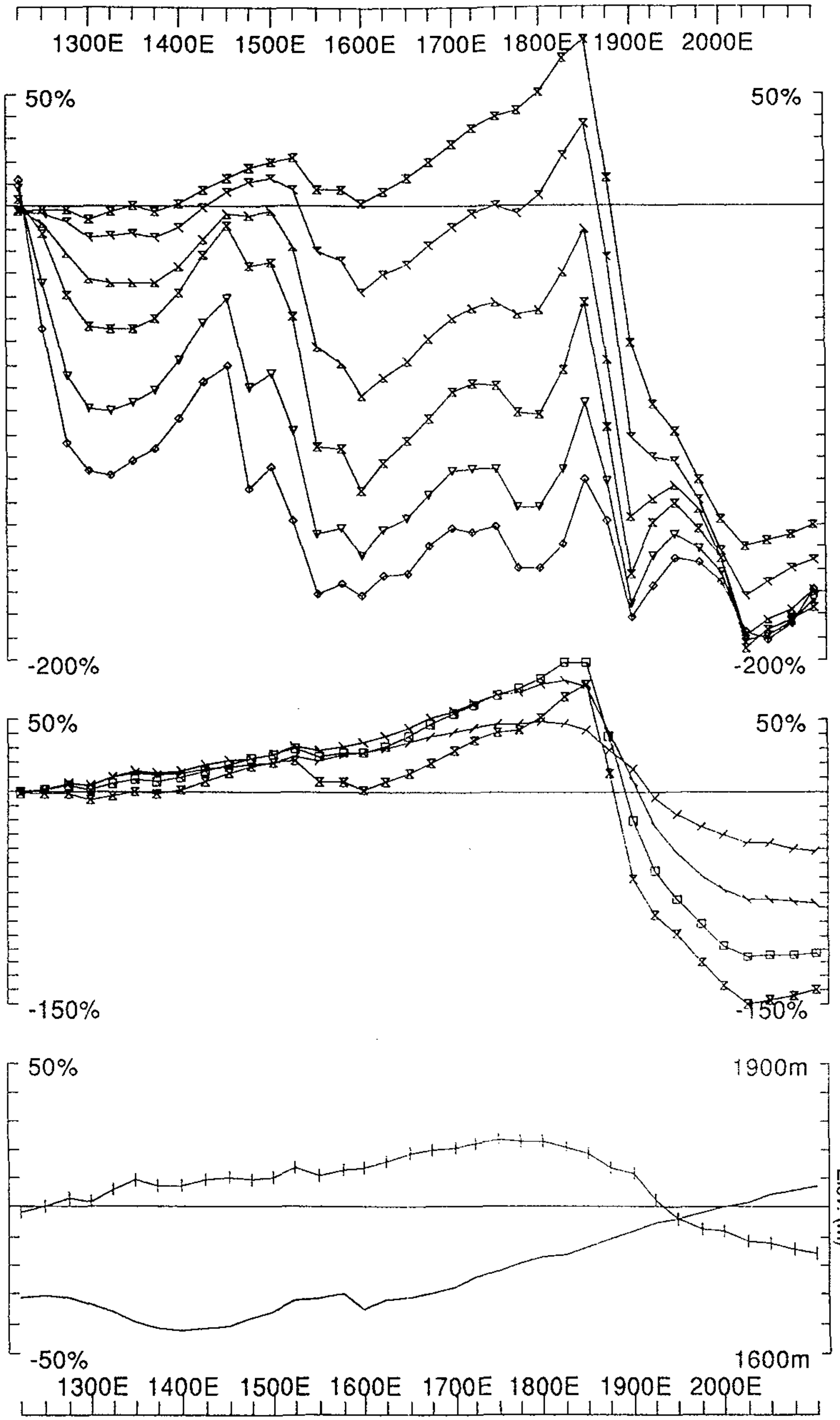
UTEM Survey at: BAR CLAIM GROUP
For: MINER RIVER RESOURCES LTD.

SJ GEOPHYSICS LTD.

Job 9417 Plotted: 23/8/94

Secondary, (Chn - Hpc)/|Hp|
Point Norm.at stn 1700
Base Freq. 30.974 Hz

Loop: 1
Line: 7 N
Compt: Hz



UTEM Survey at: BAR CLAIM GROUP
For: MINER RIVER RESOURCES LTD.

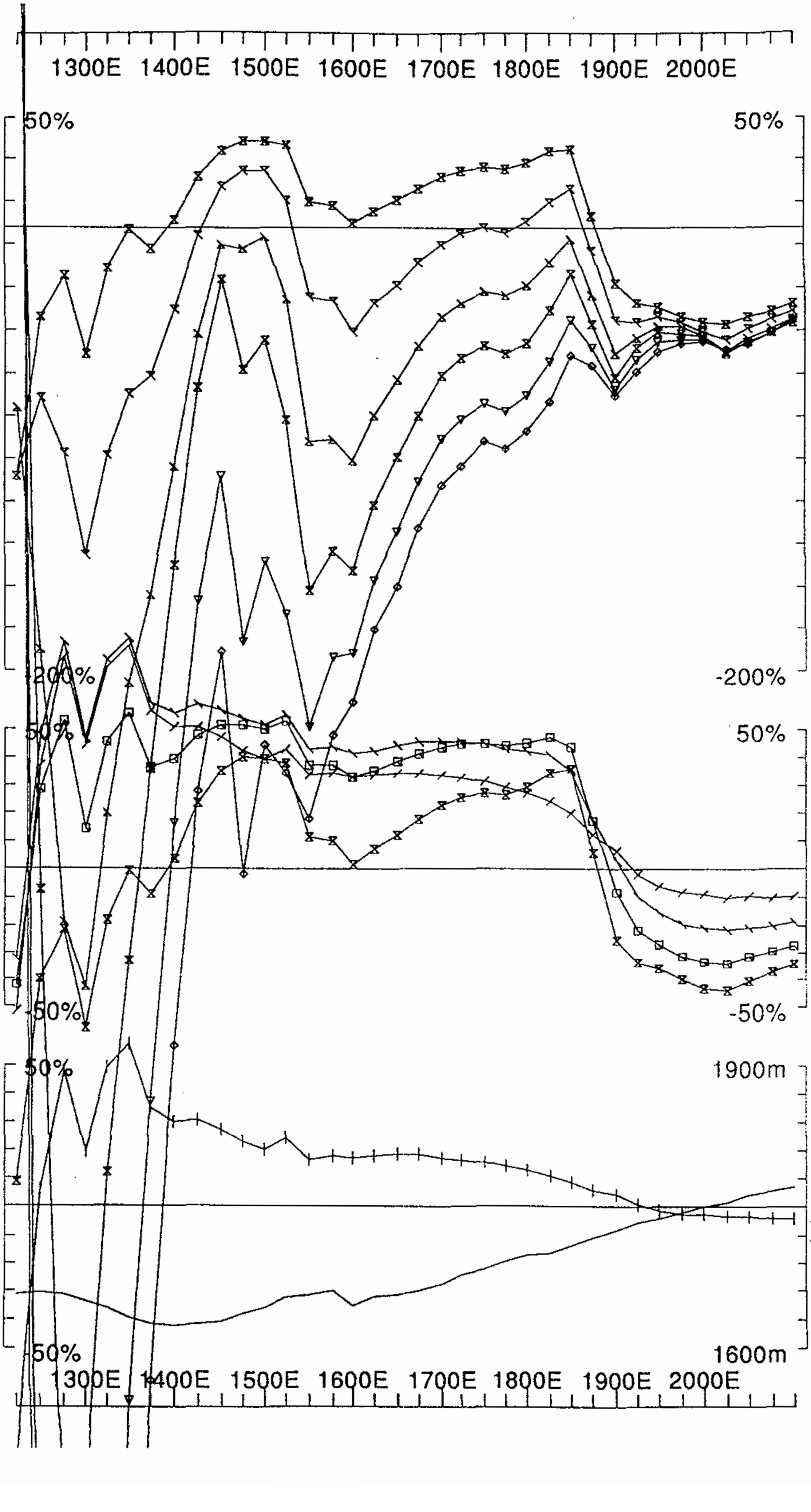
SJ GEOPHYSICS LTD.

Job 9417

Surveyed: 20/7/94
Reduced: 20/8/94
Plotted: 23/8/94

Loop: 2
Line: 8 N
Compt: Hz

Secondary, (Chn - Hpc)/|Hp|
Contin. Norm at depth of 0 m
Base Freq. 30.974 Hz



UTEM Survey at: BAR CLAIM GROUP
For: MINER RIVER RESOURCES LTD.

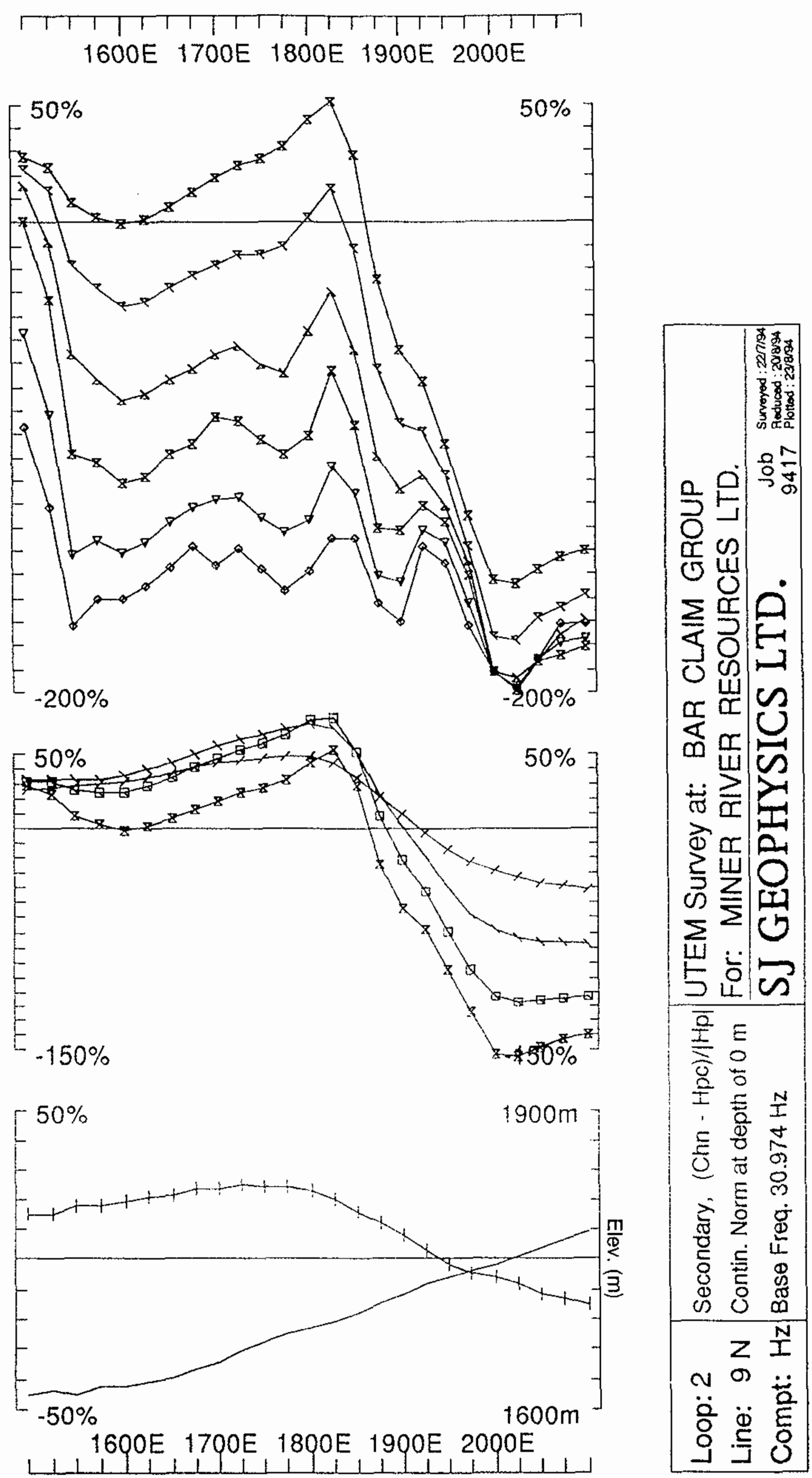
SJ GEOPHYSICS LTD.

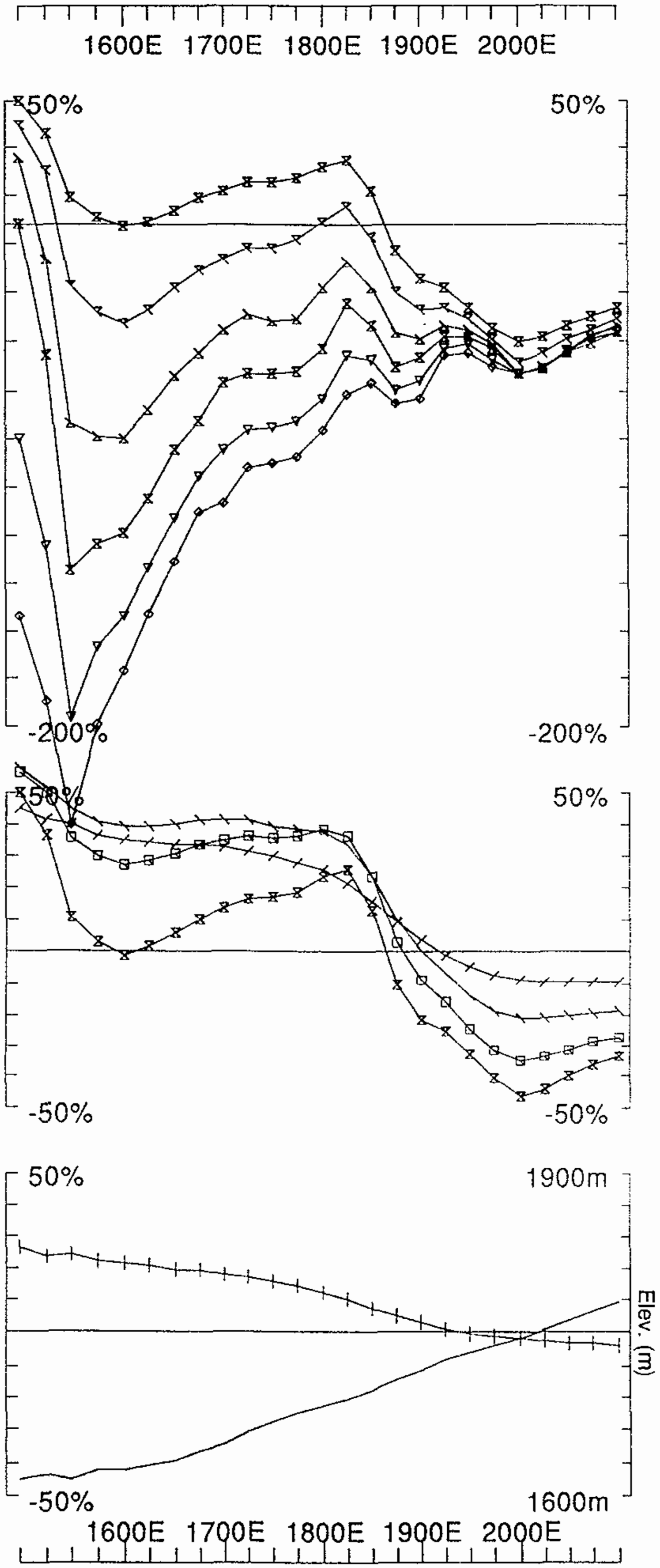
Job 9417

Surveyed : 20/7/94
Reduced : 20/8/94
Plotted : 23/8/94

Loop: 2
Line: 8 N
Compt: Hz

Secondary, (Chn - Hpc)/|Hp|
Point Norm.at stn 1650
Base Freq. 30.974 Hz


1600E 1700E 1800E 1900E 2000E
50%
50%
-200%
-200%
50%
50%
-150%
-150%
50%
1900m
Elev. (m)
-50%
1600m
1600E 1700E 1800E 1900E 2000E
Loop: 2
Line: 9 N
Compt: Hz
Secondary, (Chn - Hpc)/|Hp|
Contin. Norm at depth of 0 m
Base Freq. 30.974 Hz
UTEM Survey at: BAR CLAIM GROUP
For: MINER RIVER RESOURCES LTD.
SJ GEOPHYSICS LTD.
Job 9417
Surveyed: 22/7/94
Reduced: 20/8/94
Plotted: 23/8/94



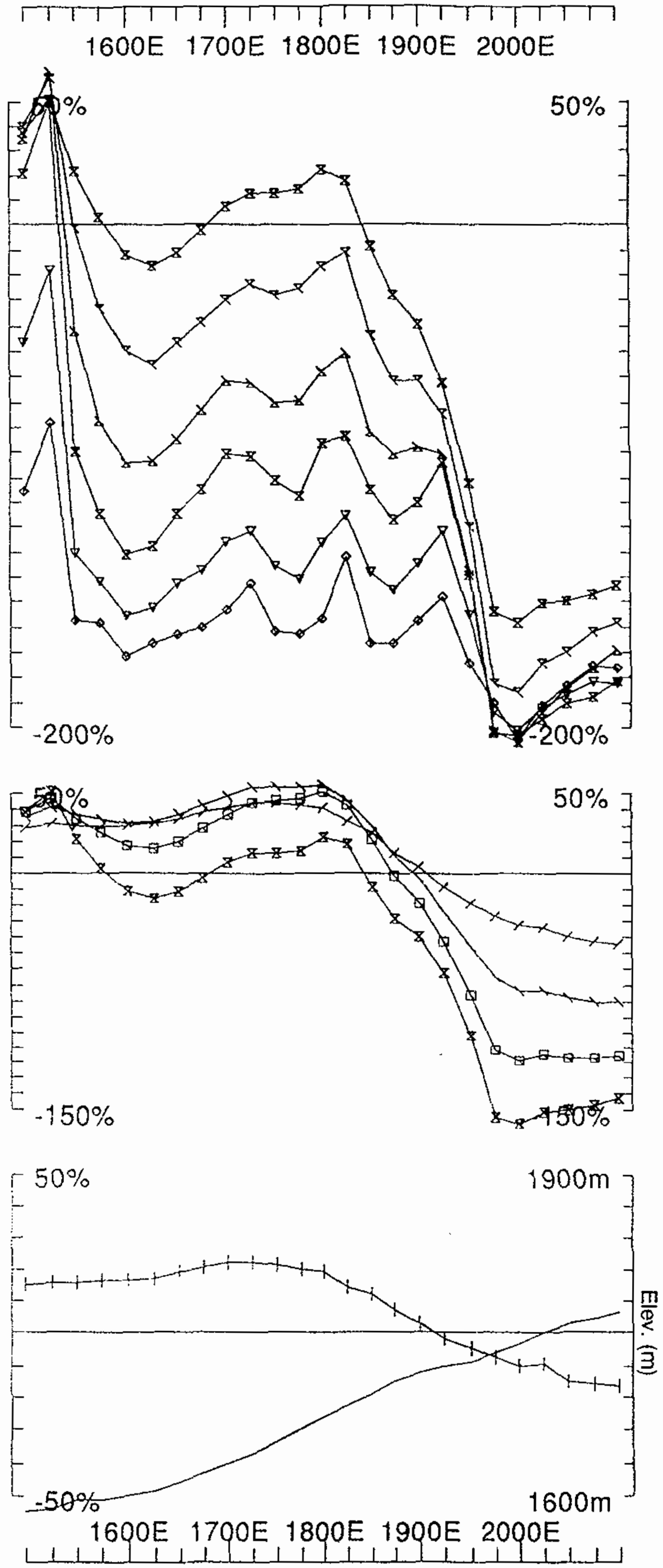
UTEM Survey at: BAR CLAIM GROUP
For: MINER RIVER RESOURCES LTD.
SJ GEOPHYSICS LTD.

Job 9417

Surveyed : 22/7/94
Reduced : 20/8/94
Plotted : 23/8/94

Loop: 2
Line: 9 N
Compt: Hz

Secondary, (Chn Hpc)/|Hp|
Point Norm.at stn 1625
Base Freq. 30.974 Hz



UTEM Survey at: BAR CLAIM GROUP
For: MINER RIVER RESOURCES LTD.

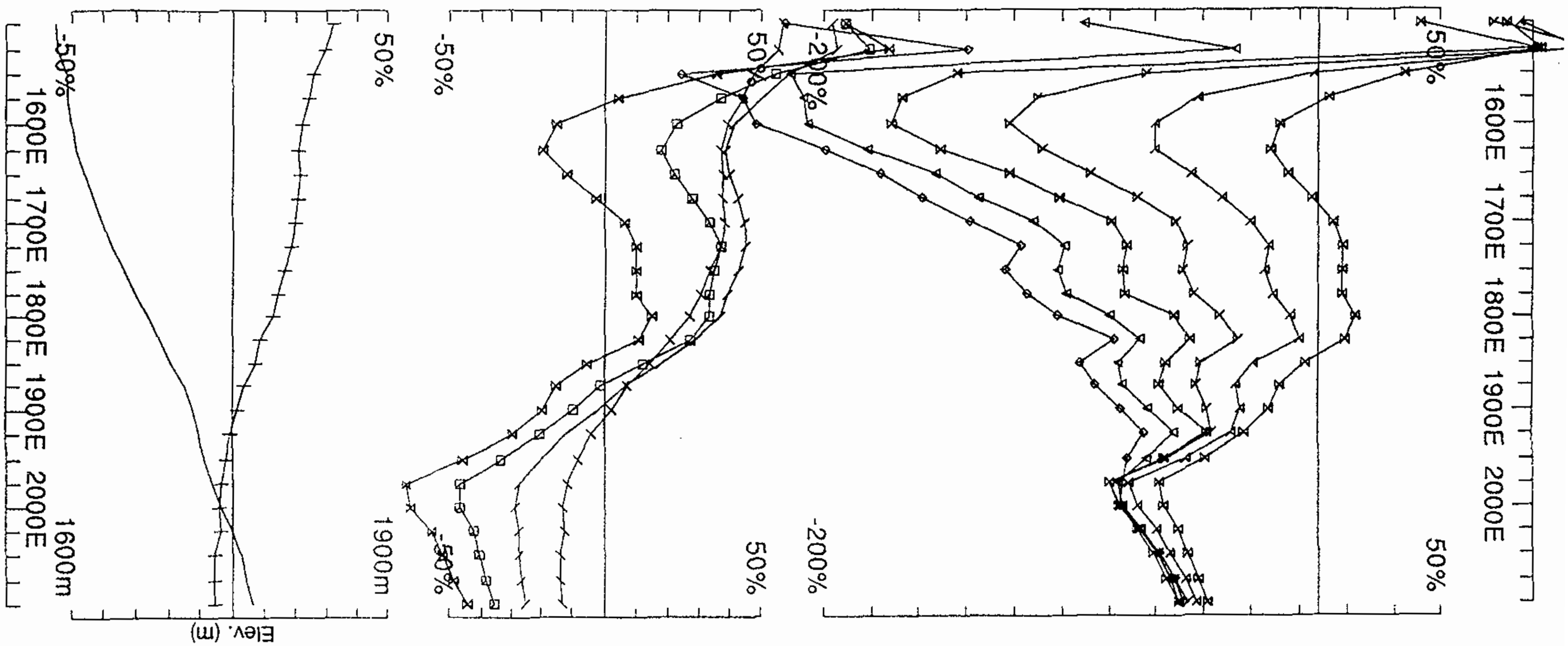
SJ GEOPHYSICS LTD.

Job 9417

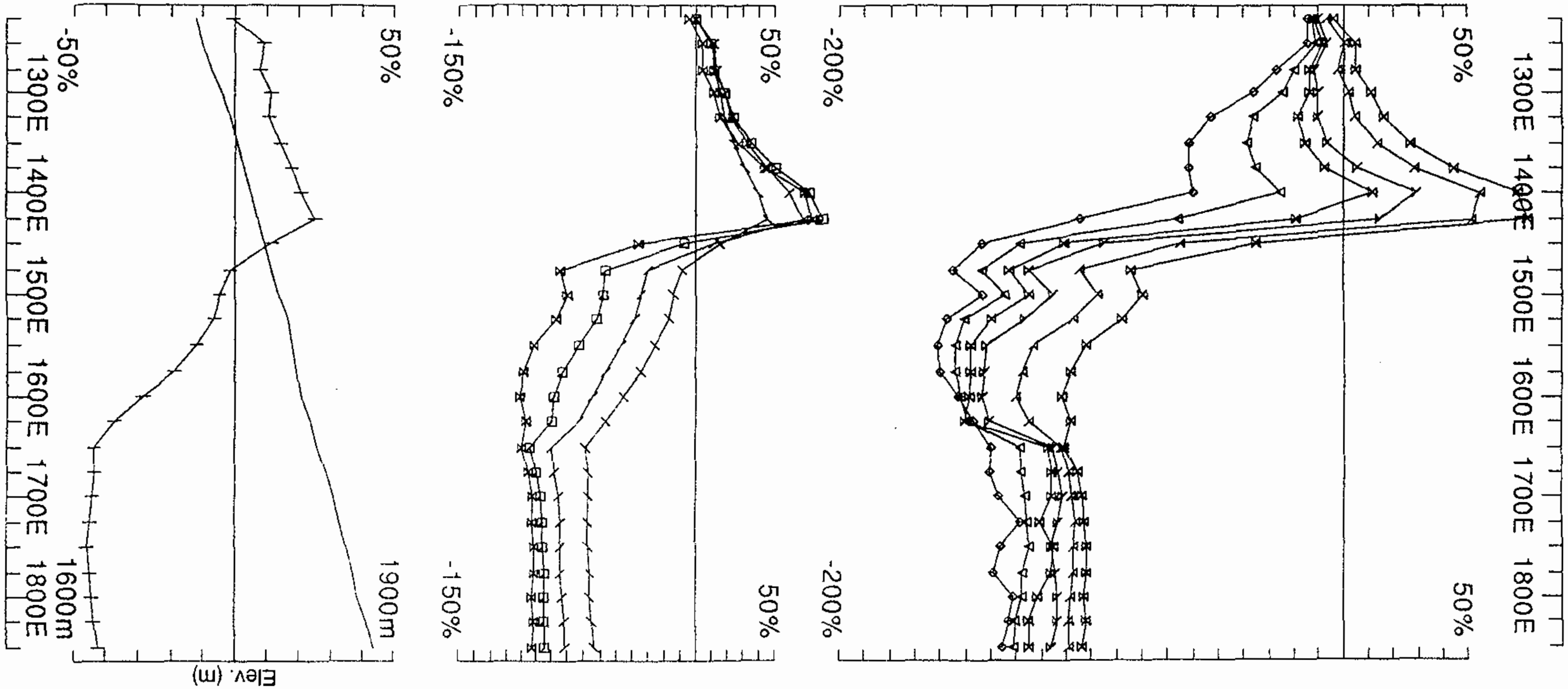
Surveyed : 22/7/94
Reduced : 20/8/94
Plotted : 23/8/94

Secondary, (Chn - Hpc)/|Hp|
Contin. Norm at depth of 0 m
Base Freq. 30.974 Hz

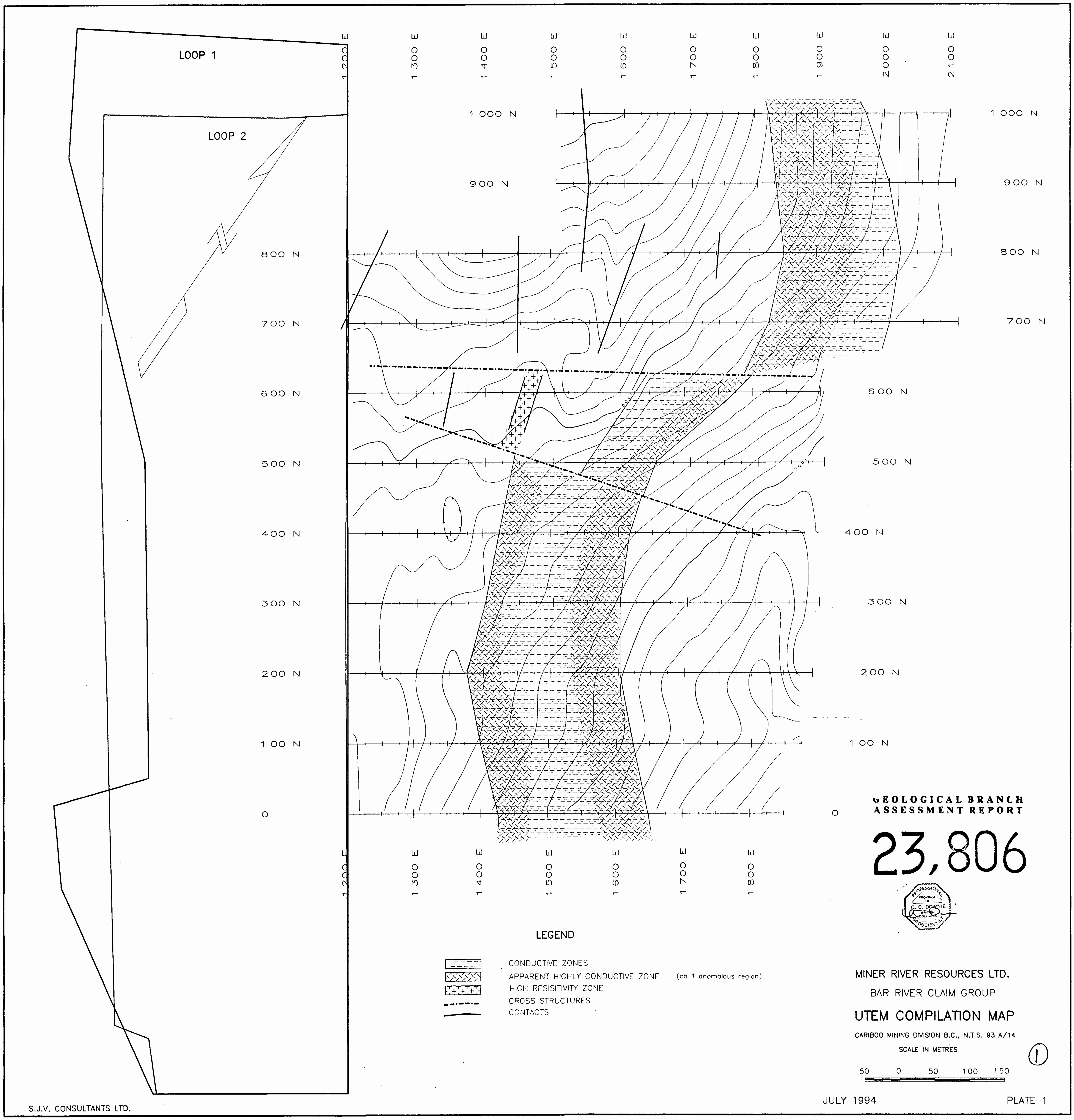
Loop: 2
Line: 10 N
Compt: Hz



Loop: 2 Line: 10 N Compt: Hz	Secondary, (Chn - Hpc)/|Hp| Point Norm.at stn 1675 Base Freq. 30.974 Hz	UTEM Survey at: BAR CLAIM GROUP For: MINER RIVER RESOURCES LTD. SJ GEOPHYSICS LTD. Job 9417 Surveyed : 22/7/94 Reduced : 20/8/94 Plotted : 23/8/94



Loop: 2	Secondary, (Chn - Hpc)/|Hp|	UTEM Survey at: BAR CLAIM GROUP
Line: 0 N	Contin. Norm at depth of 0 m	For: MINER RIVER RESOURCES LTD.
Compt: Hz	Base Freq. 30.974 Hz	SJ GEOPHYSICS LTD. Job 9417 Surveyed : 19/7/94 Reduced : 20/8/94 Plotted : 23/8/94


LOOP 1
LOOP 2
1 200 E
1 300 E
1 400 E
1 500 E
1 600 E
1 700 E
1 800 E
1 900 E
2 000 E
2 100 E
1 000 N
900 N
800 N
700 N
600 N
500 N
400 N
300 N
200 N
100 N
0
GEOLOGICAL BRANCH
ASSESSMENT REPORT
23,806
LEGEND
CONDUCTIVE ZONES
APPARENT HIGHLY CONDUCTIVE ZONE (ch 1 anomalous region)
HIGH RESISITIVITY ZONE
CROSS STRUCTURES
CONTACTS
MINER RIVER RESOURCES LTD.
BAR RIVER CLAIM GROUP
UTEM COMPILATION MAP
CARIBOO MINING DIVISION B.C., N.T.S. 93 A/14
SCALE IN METRES
50 0 50 100 150
JULY 1994
PLATE 1
S.J.V. CONSULTANTS LTD.

● STREAM-SEDIMENT SAMPLES

	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
SS 006	.4	.74	45	<2	240	<5	.80	1	29	37	64	4.18	.04	10	.44	900	1	.05	112	2020	66	5	<20	50	.01	40	27	10	12	384
SS 007	.4	.81	40	<2	285	<5	1.47	2	38	37	71	4.97	.03	10	.48	1091	2	.05	131	2080	66	5	<20	63	.01	50	31	10	13	448
SS 008	.8	.74	40	<2	265	<5	.87	2	40	44	71	5.42	.03	10	.54	1275	2	.04	148	2250	62	10	<20	47	.01	40	34	10	13	575
SS 009	.4	.92	40	<2	285	<5	1.19	1	41	46	89	5.31	.04	10	.52	1414	2	.04	173	2590	62	15	<20	57	.01	30	35	10	16	679
SS 010	.6	.86	45	<2	295	<5	.62	2	38	46	79	5.05	.04	10	.47	1170	5	.04	170	2490	74	10	<20	45	.01	30	36	10	15	553
SS 011	.6	.82	45	<2	310	<5	1.29	2	41	31	92	5.54	.03	10	.38	1184	3	.04	166	2720	54	15	<20	55	.01	40	29	10	15	846
SS 012	.8	.78	35	<2	250	<5	1.27	3	30	29	73	4.59	.03	10	.35	1016	1	.04	147	2490	46	10	<20	52	.01	20	29	20	15	896
SS 013	1.2	.99	25	<2	275	<5	1.54	3	34	51	87	5.35	.04	20	.68	1256	10	.04	204	3490	44	20	<20	67	.01	50	38	20	18	1278
SS 014	1.2	.64	45	<2	295	<5	1.36	5	47	40	108	5.33	.02	10	.37	1189	4	.04	275	4280	74	10	<20	94	<.01	70	23	30	20	1453
SS 015	2.0	.51	95	<2	370	<5	1.74	8	46	22	77	7.40	.02	10	.12	1260	5	.05	451	5810	86	10	<20	86	<.01	40	19	60	18	2837

▲ LITHOGEOCHEMICAL SAMPLES

Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
BAR94-1	<.2	1.09	<5	750	70	0.82	4	99	17	75	>15	<10	<.01	1826	<1	0.04	29	4410	8	<5	<20	42	0.02	<10	55	<10	<1	163
BAR94-2	<.2	0.12	<5	120	<5	0.03	<1	3	255	7	0.89	<10	0.02	41	18	<.01	7	40	148	<5	<20	2	<.01	<10	2	<10	<1	123
BAR94-3	<.2	0.10	5	3310	<5	0.23	<1	5	55	<1	0.23	<10	<.01	13	3	<.01	4	1130	54	<5	<20	127	<.01	<10	4	<10	2	80
BAR94-4	<.2	0.07	10	1915	<5	<.01	<1	4	190	4	0.73	<10	<.01	22	16	<.01	12	110	50	<5	<20	7	<.01	<10	32	<10	<1	107
BAR94-5	<.2	1.97	<5	925	20	0.59	15	272	36	301	>15	<10	<.01	4723	3	<.01	445	1800	52	<5	<20	33	<.01	<10	35	<10	25	6804
BAR94-6	<.2	0.62	25	515	<5	0.24	4	43	92	237	4.73	<10	<.01	1300	7	0.01	18	2070	18	<5	<20	12	<.01	<10	15	<10	3	185
BAR94-7	<.2	0.94	100	585	<5	0.46	5	76	227	150	11.10	<10	<.01	361	15	<.01	345	4400	44	<5	<20	34	<.01	<10	44	<10	13	484
BAR94-8	<.2	0.39	30	260	<5	2.66	2	5	220	58	2.52	<10	<.01	85	24	<.01	21	>10000	226	<5	<20	130	<.01	<10	135	<10	15	800
BAR94-9	5.6	0.08	105	5620	<5	0.22	12	154	132	266	>15	<10	<.01	>10000	38	<.01	150	8420	36	<5	<20	33	<.01	<10	26	<10	<1	1220
BAR94-10	<.2	<.01	<5	3275	<5	<.01	<1	6	6	<1	0.25	<10	<.01	180	<1	<.01	1	110	<2	<5	<20	38	<.01	<10	1	<10	<1	15
BAR94-11	<.2	0.83	5	>10000	<5	0.26	<1	23	39	12	0.58	<10	<.01	76	3	<.01	8	1440	14	<5	<20	150	<.01	<10	16	<10	2	39
CDW-1	<.2	>15	<5	2885	<5	1.12	1	65	238	115	10.80	30	3.98	2495	<1	0.01	127	3420	<2	10	<20	50	0.13	<10	195	<10	13	196
CDW-2	<.2	0.13	<5	2950	10	>15	<1	13	56	<1	5.96	<10	6.61	1814	1	<.01	14	880	16	25	<20	277	<.01	<10	9	<10	6	58
CDW-3	<.2	2.60	<5	2230	10	>15	<1	40	93	43	7.45	20	4.47	1776	<1	<.01	46	2490	38	25	<20	587	<.01	<10	105	<10	8	85
CDW-4	<.2	0.05	10	1130	<5	>15	<1	3	7	<1	0.64	<10	1.82	309	<1	<.01	2	220	<2	30	<20	651	<.01	<10	5	<10	7	25
CDW-5	<.2	0.16	5	1315	<5	0.79	<1	6	237	<1	1.14	<10	0.07	334	17	<.01	10	360	10	<5	<20	18	<.01	<10	3	<10	<1	26
CDW-6	<.2	0.12	10	1165	<5	0.22	<1	4	265	<1	0.57	<10	0.01	59	19	<.01	6	80	18	<5	<20	5	<.01	<10	2	<10	<1	20
CDW-7	<.2	3.38	<5	495	10	0.64	<1	45	583	120	6.08	<10	3.45	697	<1	0.01	233	550	48	<5	<20	16	0.15	<10	106	<10	7	95
CDW-8	<.2	1.29	10	1805	<5	0.30	<1	4	162	9	1.33	10	0.07	35	11	0.04	15	5280	24	<5	<20	1533	<.01	<10	27	<10	7	110
CDW-9	<.2	1.87	<5	260	<5	0.20	<1	11	95	34	3.51	<10	1.25	48	4	<.01	17	1060	32	10	<20	33	<.01	<10	45	<10	<1	103
CDW-10	<.2	0.07	20	235	<5	>15	<1	2	11	<1	0.65	<10	0.37	267	<1	<.01	3	230	<2	10	<20	702	<.01	<10	4	<10	9	9
CDW-11	<.2	<.01	<5	3195	<5	0.84	<1	4	13	<1	[illegible]	<10	<.01	7	<1	<.01	<1	700	<2	<5	<20	90	<.01	<10	2	<10	<1	2
CDW-12	<.2	0.86	10	210	<5	0.14	<1	7	16	6	3.17	10	0.08	436	<1	<.01	11	1350	22	<5	<20	2	<.01	<10	33	<10	<1	41
CDW-13	<.2	0.22	135	1950	55	0.48	7	96	25	38	>15	<10	<.01	1036	<1	<.01	348	9740	54	<5	<20	32	0.01	<10	8	<10	<1	2627
CDW-13B	3.2	0.42	55	>10000	<5	0.55	20	864	119	14	>15	<10	<.01	>10000	223	<.01	656	9630	<2	<5	<20	345	<.01	<10	22	<10	16	2151
CDW-14	<.2	0.37	80	1330	20	0.40	3	101	12	47	>15	<10	<.01	4148	4	<.01	343	6460	106	<5	<20	56	<.01	<10	12	<10	<1	[illegible]
CDW-15	<.2	>15	<5	>10000	<5	0.48	<1	111	121	40	3.58	<10	<.01	1659	7	0.02	46	3370	<2	<5	<20	86	<.01	<10	48	<10	3	143
CDW-16	<.2	0.04	<5	3370	<5	0.07	<1	5	5	<1	0.14	<10	<.01	169	<1	<.01	1	350	<2	<5	<20	58	<.01	<10	3	<10	<1	7

MINER RIVER RESOURCES LTD.			
BAR PROJECT			
Location Map ②			
Scale: 1:5000	Date: NOV. 1994	N.T.S.: 93A/14	
BIG CITY RESOURCES INC.			Map no.: 1