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GEOLOGICAL AND GEOCHEMICAL SUMMARY REPORT

ON

THE

BEN ALI GROUP OF CLAIMS

SKEENA MINING DIVISION
STEWART B.C.

NTS 104A4W

LONGITUDE: 129° 55' 00"W
LATITUDE: 56° 01'00"N

For:

PRIME EQUITIES INTERNATIONAL
1100-808 WEST HASTINGS STREET
VANCOUVER, B.C.
V6C 2X4

By:

FILMED

John A. Nicholson, P.Geo.
Nicholson & Associates

GEOLOGICAL BRANCH
ASSESSMENT REPORT

Vancouver, B.C.

March 15, 1995

23,855

SUMMARY

During the month of July 1994, Nicholson and Associates undertook 2 days of mapping, rock and silt sampling on the Ben Ali Group of claims. The property is situated 7 km northeast of Stewart B.C. The property is held under option by Prime Equities International from KRL Resources as part of the larger MM Group. Prime Equities International is earning a 50% interest in the MM group of claims by paying $200,000 cash to KRL over three years; spending a minimum of $1,000,000 on exploration by September 31, 1996, (of which a minimum $225,000 is committed in 1994); and by issuing shares of Prime to KRL at a rate of 25,000 upon approval and 25,000 per year for each of the next three years. KRL is entitled to a net smelter return of up to 3% on the property. (Stock Watch news release, February 8th, 1994)

The MM Group was optioned by Prime Equities International to cover favourable volcanic and sedimentary rocks of the Salmon River and Unuk River Formations which could possibly host precious metal deposits similar to American Barrick's Minerals Red Mountain deposit.

Mapping and sampling on the Ben Ali group confirmed the presence of the Ben Ali vein and confirmed the presence of gold mineralization in the area.

Total expenditures that were spent on the group was $1200.00

TABLE OF CONTENTS

LIST OF FIGURES

INTRODUCTION

During the month of July, Nicholson and Associates undertook a program of geochemical rock sampling on the BenAli Group which is located 7 km northeast of Stewart, B.C.

A total of 5 silt and 14 rock samples were collected from the property. The program was supervised by the author who mapped and collected samples on the property.

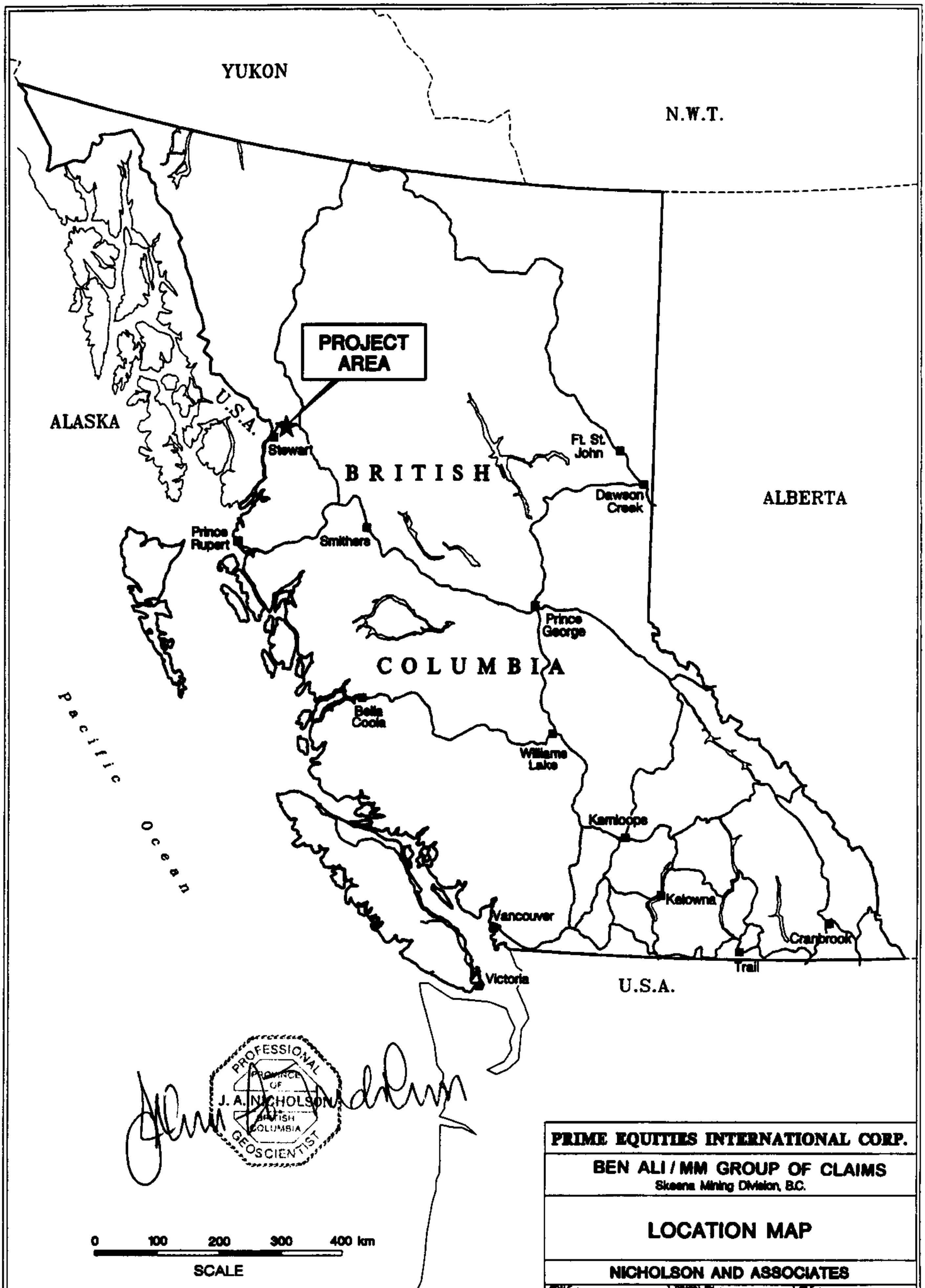
The purpose of the program was to test the property for its bulk tonnage potential outside of the main Ben Ali Vein.

A total of $1,200.00 was spent sampling and mapping the property.

LOCATION AND ACCESS

The Ben Ali group of claims which Prime Equities International holds under option from KRL Resources as part of the MM Group of claims, consists of 3 contiguous mining claims. The claims are situated in the Skeena Mining Division, 7 kms. northeast of Stewart, B.C. (figure 1). The claims occur on map sheet NTS 104A/4W near 56 degrees 01 minutes N latitude and 129 degrees 55 minutes W longitude.

Access to the property is presently gained by driving east of Stewart along highway 7. An old logging road located 500 metres past the Trade West sorting ground on the right hand side of the highway provides for easy access to the base of the claim block. Old trials and cut lines which have been constructed by previous operators provide for easy access throughout the property.



PROFESSIONAL GEOSCIENTIST
PROVINCE OF BRITISH COLUMBIA
J. A. NICHOLSON

PRIME EQUITIES INTERNATIONAL CORP.

BEN ALI / MM GROUP OF CLAIMS
Skeena Mining Division, B.C.

LOCATION MAP

NICHOLSON AND ASSOCIATES

SCALE : 1 : 8,000,000	DRAWN BY : Luminai Drafting Ltd.	FILE : BMMBC.DWG
DATE : DEC 1994	REVISED :	FIGURE : 1

PROPERTY STATUS

Prime Equities International has entered into an agreement with KRL Resources whereby Prime Equities International can earn a 50% interest in the MM Group of claims by spending a minimum of $1,000,000 on exploration by December 31, 1996, of which a minimum of $225,000 is committed in 1994; and by issuing 100,000 shares of Prime to KRL at a rate of 25,000 upon approval and 25,000 shares for each of the next three years. KRL is entitled to a net smelter return at various rates up to 3% on the property. The claim group consists of 3 metric units
(figure 2)

BEN ALI and BITTER CREEK

Claim Name	Tenure#	# of Units	Expiry Date
Sunbeam Fraction	250637	1	Feb 8, 1997*
Ben Ali	251271	1	Jan. 2, 1997
Ben Ali #2	251272	1	Jan. 2, 1997

TOTAL UNITS 3

* after 1994 work assessment has been applied

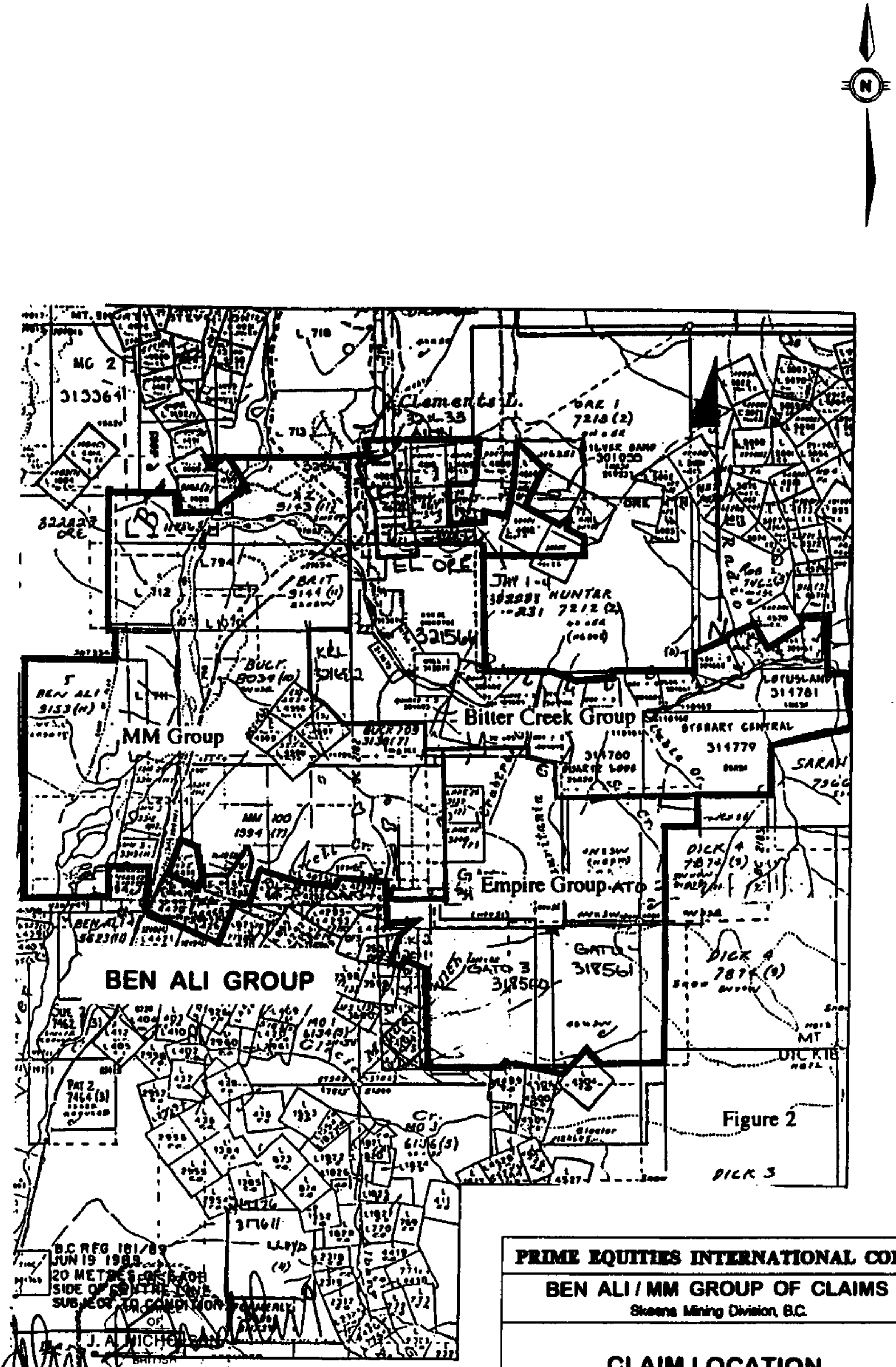


Figure 2

J. A. NICHOLSON

PRIME EQUITIES INTERNATIONAL CORP.

BEN ALI / MM GROUP OF CLAIMS

Skeena Mining Division, B.C.

CLAIM LOCATION

NICHOLSON AND ASSOCIATES

SCALE : AS SHOWN	DRAWN BY :	FILE :
DATE : SEPT 1994	REVISED :	FIGURE : 2

TOPOGRAPHY, VEGETATION and CLIMATE

The topography on the Ben Ali Group varies from a low of 50 metres to a high of 500 metres. The terrain is typical of the Stewart area and consists of tall stands of over mature spruce and hemlock. Underbrush in the form of slide alder, brambles and ferns are very thick making movement slow and difficult.

Water on the property is plentiful in the form of and creeks which run year round.

The climate on the property is typical coastal weather with heavy precipitation year round. Snowfall and snow coverage is variable and is dependant on the elevation. Snowfall on the property averages between 350 and 500 centimetres. As a result access is limited from mid May to mid October.

HISTORY

The Stewart Camp over the past one hundred years has been a major producer of both precious and base metals. The Stewart Camp has had over 50 producing mines which have produced in excess of 2 million ounces of gold, 50 million ounces of silver, and over 100 million pounds of Cu-Pb-Zn between 1910 and 1992. Presently there are two active mines in the area both operating on a limited bases.(figure 3)

Activity in the area first began in the late 1800's when placer miners arrived in the valley and started to operate placer mines on various creeks in the area. Subsequent discoveries on Bitter Creek and Glacier Creek led to the staking and granting of several crown granted claims. Several small "High Grade" mines opened up as a result of this staking, but were short lived due the boom/bust economic cycle of the "Roaring 1920's/1930's Great Depression".

On the Ben Ali Group of mineral claims, which forms the southern portion of the property, extensive work has been undertaken. The Ben Ali Mine has had a reported + 5,000 tons of ore grading 0.6 oz/ton gold which was shipped to the Dunwell mill. (J.W. Young, 1949, BenAli Mine, Portland Canal District, B.C.) The ore was mined from 4 levels of workings which presently are all accessible. Limited work was undertaken on the property after its closure in 1949, when reportedly 3 diamond drill holes were drilled by Hedley Mascot Mines to test the extension of the vein system. One drill hole is reported to have intersected 15 cm. of 5.0 oz/t Au. The property remained dormant until 1979 when the underground workings were reopened and reassessed. No further work was undertaken on the property until 1987-89 by Rose Spit Resources Inc. which undertook extensive soil sampling, mapping, prospecting and geophysically surveys using VLF-Electromagnetic and Magnetometer surveys.

Adjacent to the MM Group, American Barrick is exploring Red Mountain for precious metals. The newly discovered Au-Ag deposit is situated 15 kilometres south-southwest of the Ben Ali group of claims at the headwaters of Bitter Creek. The deposit, which has drill proven reserves of 2.8 million tons, grading 0.37 oz/ton gold, occurs at a sedimentary - volcanic contact which has been intruded by the Early Jurassic Goldslide and Hillside intrusives with related hornblende feldspar porphyry dykes of varying composition. Mineralization consists mainly of semi-massive to massive, medium to coarse grained pyrite and/or stringer which contain varying amounts of chalcopyrite, pyhrrotite and sphalerite. Gold occurrences in the system is zoned and higher values are associated with coarse pyrite and lesser chalcopyrite (1-30 metres wide), which is characterized by adjacent pyrrhotite-sphalerite mineral zones (5-25 metres wide). Current reserves are based on extrapolated diamond drill hole data from the Marc and AV zones which are traced horizontally and vertically for about 600 meters (Smit, H. 1994, personal communication).

Westmin Resources is presently operating their Premier Gold Project from development work on the No. 6 level of the Silbak-Premier deposit as well as Tenajon's SB deposit several km. to the north. The Silbak-Premier has a recorded production in excess of 2 million ounces Au, 40 million ounces Ag, and 100 million pounds of Pb-Zn from about 5 million tons of ore. Production from two distinct breccia and vein stockwork trends, the Main and West zones, came from ore shoots distributed along a combined strike length of 1,600 meters, but 80% of the production was recovered from within 500 meters of the intersection of these two trends. The intersection area contained the widest ore shoots (up to 20 metres) and those with the highest Au-Ag grades (Alldrick, D.J., 1993).

Dunwell Mines, located 1000 metres east Ben Ali workings, produced 10,000 ounces Au, 330,000 ounces Ag, and 5 million pounds Pb-Zn from 50,000 tons of ore. Quartz-calcite breccia fissure veins contain galena, dark-brown sphalerite, pyrite, chalcopyrite, as well as minor tetrahedrite, argentite, and ruby silver. North-northeast trending, moderate to steep west dipping veins are found along the Portland Canal Fissure zone, hosted by Salmon River Fm. argillaceous graphitic siltstone, which unconformably overlie Unuk River Fm. conglomerates and volcanic breccias and are intruded by augite porphyry and cross-cutting hornblende-granodiorite dyke swarms (Grove, E.W., 1971)..

Prosperity/Porter Idaho Mines produced 2,329,000 ounces of silver from a modest 31,884 tons of ore processed. Production from stopes was generally confined to quartz vein swells and bulges where galena-sphalerite-tetrahedrite-polybasite-native Ag mineralization was concentrated. Oreshoots were generally steeply plunging and appear to be controlled by slight vein flexures (Grove, E.W.,1971).

TABLE 15
MINE PRODUCTION AND ORE RESERVES IN THE STEWART MINING CAMP
(To January 1, 1992)

Property	Minfile No.	Date	Past Production (tonnes)	Reserves (category)	Au g/t	Ag g/t	Pb %	Zn %	Cu %	WO₃ %
EAST GOLD	*104B 033*	*1939-1954*	*44*		*1207.00*	*3 313.00*	*4.00*	*1.30*	*0.07*	
SCOTTIE GOLD	104B 034	1981-1985 1985(U) 1990(U)	197 522	 132 000 (g) 28 992 (m)	16.50 19.20 18.51	16.00 17.00				
SPIDER	104A 010	1925, 1933-1936	22.2		14.20	8 238.00	3.50	3.90		
MARTHA ELLEN	104B 092	1987		1 576 449 (g)	2.26	27.43				
SILVER TIP	104B 043	1915, 1950, 1951, 1957	26		11.80	2 610.00	14.00	19.00		
		1956(U)		816 (g)	4.80	970.30	4.20	6.20		
NORTHSTAR	104B 146	1987		47 078 (g)	4.29	20.57				
S-1	104B 084	1987 1990 1991	 304 000	1 209 709 (g) 800 000 (g)	2.71 2.40 2.20	7.20 10.00 10.00				
CREEK	104B 086	1987		7 529 (g)	2.40	116.23				
BIG MISSOURI	104B 046	1938-1942	768 943		2.37	2.13				
DAGO HILL	104B 045	1934, 1950 1987 1988-1989 1991	14 384 000	 557 141 (g) 150 000 (g)	48.00 2.54 1.20 1.20	3 952.00 38.06 10.00 10.00	0.46		0.12	
PROVINCE	104B 147	1987 1990 1991	 33 300	286 734 (g) 100 000 (g)	2.43 2.46 1.50	12.69 21.88 20.00				
SILVER BUTTE	*104B 150*	1991(U) 1991(U) 1991	 102 539	96 209 (m) 279 387 (g)	9.91 17.31 8.89	65.90 36.69 55.50	*0.67*	3.85	0.32	
INDIAN	104B 031	1925, 1952	12 870		3.40	119.70	4.40	5.50		
SILBAK PREMIER (includes SEBAKWE and B.C. SILVER)	104B 054 104B 153 104B 155	1919-1953, 1959-1968, 1989(O) 1990(O) 1990(U) 1991(O) 1988-1991 1992(U+O)	4 276 714 1 060 593	 6 300 000 (m) 3 388 900 (m) 851 000 (m) 945 000 (m) 4 900 000 (g)	13.00 2.16 2.51 7.50 2.80 2.27 2.00	274.00 80.23 67.73 34.84 41.30 67.00 20.00	0.66	0.20		
RIVERSIDE	104B 073	1925, 1927, 1941-1950	26 437		2.89	102.10	3.90		0.13	0.12
DUNWELL	*103P 052*	*1926-1941*	*45 710*		*6.72*	*224.40*	*1.83*	*2.43*	*0.03*	
UNITED EMPIRE	103P 050	1925 1934, 1936	163		2.10	1 136.70	7.40			
MOLLY B	103P 085	1940, 1941	290		2.36	12.01			0.72	
SILVERADO	103P 088	1927	13			3 662.40				
PROSPERITY/ PORTER IDAHO	103P 089	1922 1924-1932, 1938, 1939, 1947, 1950, 1981	27 268		1.00	2 692.97	5.10	0.03	0.10	
		1989(U)		826 400 (g)		668.50	2.50	2.50		

U = underground
O = open pit

g = geological
m = mineable

NICHOLSON

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BEN ALI / MM GROUP OF CLAIMS
Skeena Mining Division, B.C.

PAST PRODUCTION
STEWART MINING CAMP

NICHOLSON AND ASSOCIATES

SCALE :	DRAWN BY :	FILE : BMMPROD.DWG
DATE : DEC 1994	REVISED :	FIGURE : 3

REGIONAL GEOLOGY

The Ben Ali Group of claims lies within the Stewart Mining camp on the Salmon River map sheet area. The property lies close to the boundary between the Intermontaine Belt and the Coast Plutonic complex of the Canadian Cordillera. The property lies in the southern part of the Stikine Arch, a late Paleozoic to Mesozoic assemblages of volcanic and sedimentary rocks. The Stikine Arch stretches from Anyox to Atlin, and east to Telegraph Creek around the northern edge of the Bowser Basin.(figure 4a/4b Wheeler and McFeely, 1987) reproduces part of the regional geology map. The Ben Ali group of claims is located at the contact between the Unuk River Formation to the west and the Salmon River Formation to the east, both of the Jurassic Hazelton Group. (figure 5) Cutting the formations are the Eocene Bitter Creek granodiorite, Hyder quartz monzonite, and Glacier Creek augite porphyry. As a result of the emplacement of these Eocene stocks and dyke swarms, the Unuk river and Salmon River Formations form a fold/fault complex. The most evident feature of this Eocene fold/fault complex is the Portland Canal Fissure Zone, which attains widths up to 500 metres, strikes northeasterly on the property, and the Portland Canal Dyke Swarms which strikes northwesterly to northerly. (Livegard and Cavey, 1994)

Within the Stikine Arch, Triassic rocks are found only in the Iskut and Unuk River area. Named the Stuhini /Takla Group (Alldrick , 1993) these rocks are dominantly intermediate volcanics and sediments and host several deposits in the area, namely the Snip, Stonehouse, Inel, and Granduc.

Triassic rocks are unconformably to gradationally overlain by the Lower to Middle Jurassic Hazelton Group. Grove (1986) divided the Jurassic Hazelton into four major lithostratigraphic divisions: the Unuk River Formation (Early Jurassic), the Betty Creek and Salmon River Formations (Middle Jurassic), and the Nass Formation (Late Jurassic). Anderson and Thorkelson (1990) do not include the Nass Formation, which includes the Bowser Basin sediments. The Hazelton Group is dominated by island arc volcanics which are the source rocks for much of the Bowser Basin sediments. Anderson and Thorkelson (1990) do recognize a regionally mappable unit (the Mt. Dilworth Formation) between the Betty Creek Formation and the Salmon River Formation.

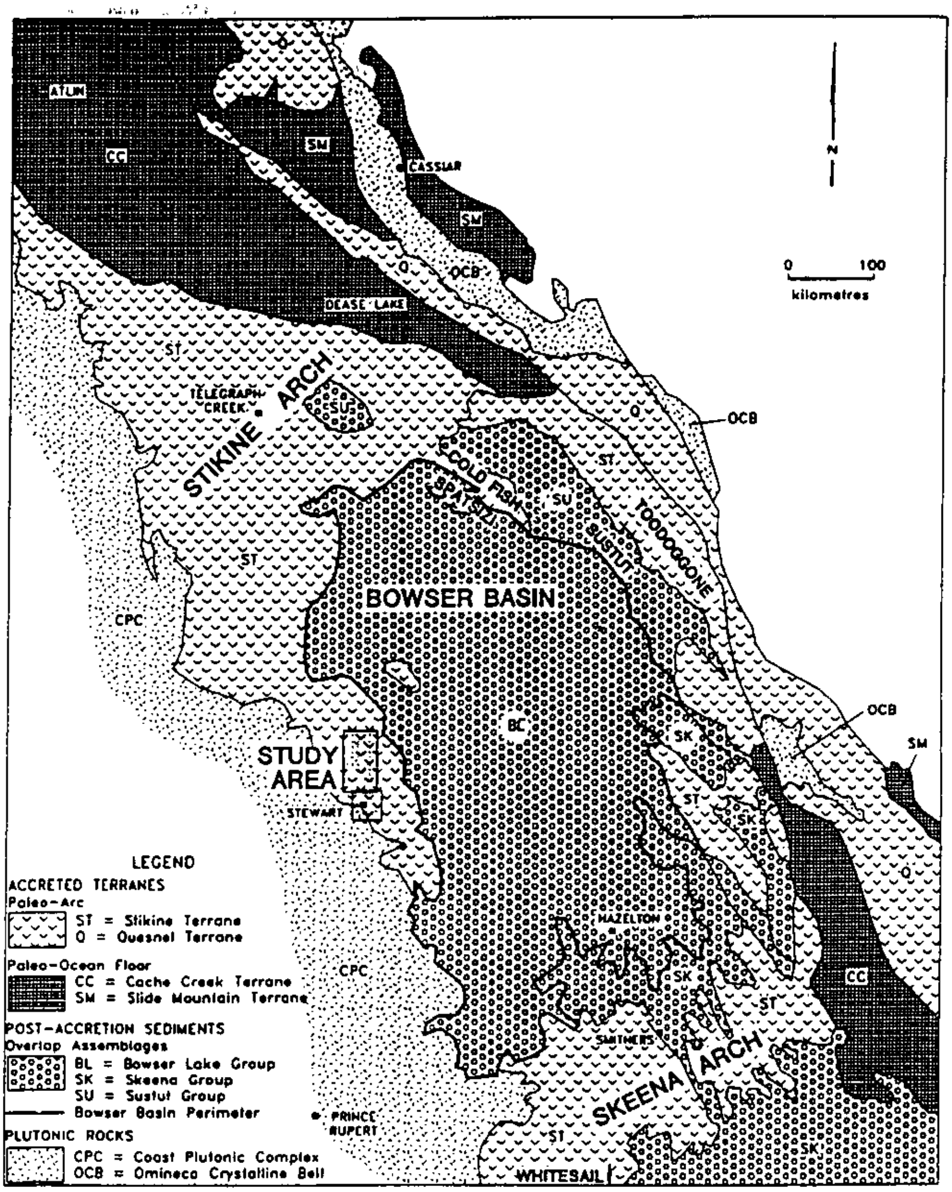

Figure Tectonic elements of northern British Columbia (modified from Wheeler and McFeely, 1987).

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Skeena Mining Division, B.C.

TECTONIC REGIONAL GEOLOGY

NICHOLSON AND ASSOCIATES

SCALE : AS SHOWN	DRAWN BY :	FILE :
DATE : SEPT 1994	REVISED :	FIGURE : 4a

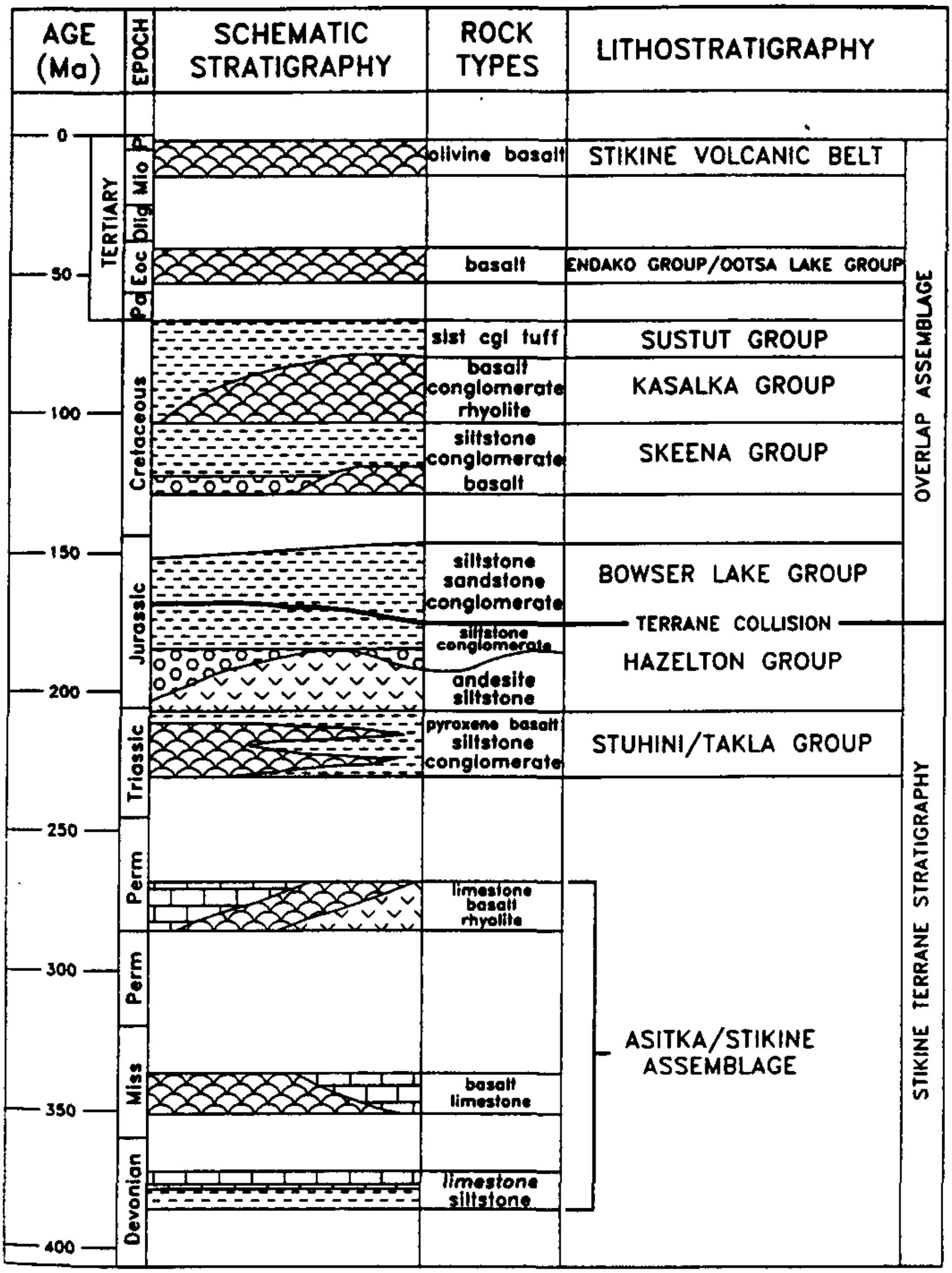

Figure Stratigraphy of Stikinia and younger overlap assemblages.

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Skeena Mining Division, B.C.

REGIONAL KEY

NICHOLSON AND ASSOCIATES

SCALE : AS SHOWN	DRAWN BY :	FILE :
DATE : SEPT 1994	REVISED :	FIGURE : 4b

The Unuk River Formation is characterized by basal pyroclastic flows that are progressively overlain by tuffs, argillites, local andesitic breccia and finally conglomerates with interbedded tuffs, wackes, siltstones and minor carbonate lenses.

The Betty Creek Formation unconformably overlies the Unuk River Formation and is comprised of maroon to green volcanic siltstone, greywacke, conglomerate, breccia, basaltic pillow lavas, andesitic flows and some carbonate lenses.

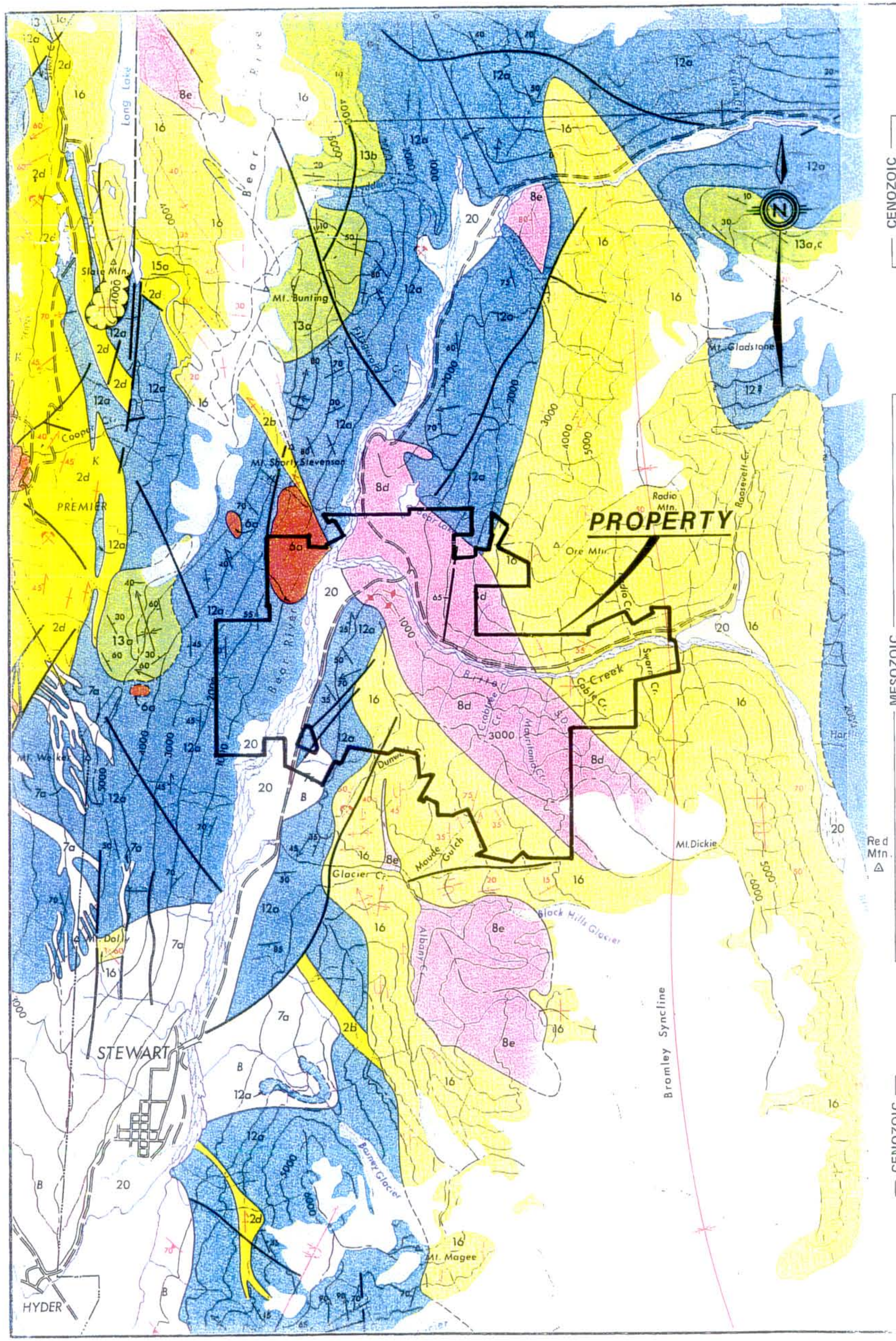
The Mt. Dilworth Formation, recognized in the Iskut-Unuk River region, consists of tuff breccia, felsic tuff, ash tuff, and argillaceous sediments.

The Salmon River Formation conformably to unconformably overlies the Betty Creek Formation and the Mt. Dilworth Formation. It consists of intensely folded, colour banded siltstones and lithic wackes with locally occurring calcarnite and volcanic components.

At the end of the Middle Jurassic the volcanic complex was uplifted and detritus shed from the Stikine Arch into the adjacent Bowser Basin. The Nass Formation outcrops mainly along the western part of the basin and represents primarily deltaic accumulation of material consisting of conglomerate, and calcareous siltstone.

These volcanics and sedimentary sequences were subsequently intruded by Middle Jurassic to Early Tertiary granitoid intrusions associated with the Coast Plutonic Complex. The intrusions can be an important source for localizing mineralization.

Late stage (Quaternary) basaltic volcanism resulted in deposits of columnar basaltic flows, ash and tephra layers, and cinder cones, that are relatively rare in the southern part of the Stikine Arch. Pleistocene and Recent glaciation has eroded and or covered much of this volcanism.



SEDIMENTARY AND VOLCANIC ROCKS

CENOZOIC

QUATERNARY

RECENT

20	UNCONSOLIDATED DEPOSITS; RIVER FLOODPLAIN, ESTUARINE, RIVER CHANNEL AND TERRACES, ALLUVIAL FANS, DELTAS AND BEACHES, OUTWASH, GLACIAL LAKE SEDIMENTS, TILL, PEAT, LANDSLIDES, VOLCANIC ASH, HOTSPRING DEPOSITS
19	BASALT FLOWS (a), CINDERS, ASH (b)

PLEISTOCENE AND RECENT

18	BASALT FLOWS

MESOZOIC

JURASSIC

HAZELTON GROUP

UPPER JURASSIC

NASS FORMATION

17	SILTSTONE, GREYWACKE, SANDSTONE, SOME CALCARENITE, ARGILLITE, CONGLOMERATE, MINOR LIMESTONE, MINOR COAL (INCLUDING EQUIVALENT SHALE, PHYLLITE, AND SCHIST)

MIDDLE JURASSIC

SALMON RIVER FORMATION

16	SILTSTONE, GREYWACKE, SANDSTONE, SOME CALCARENITE, MINOR LIMESTONE, ARGILLITE, CONLOMERATE, LITTORAL DEPOSITS
15	RHYOLITE, RHYOLITE BRECCIA; CRYSTAL AND LITHIC TUFF

BETTY CREEK FORMATION

14	PILLOW LAVA, BROKEN PILLOW BRECCIA (a); ANDESITIC AND BASALTIC FLOWS (b)
13	GREEN, RED, PURPLE, AND BLACK VOLCANIC BRECCIA, CONLOMGERATE, SANDSTONE, AND SILTSTONE (a); CRYSTAL AND LITHIC TUFF (b); SILTSTONE (c); MINOR CHERT AND LIMESTONE [INCLUDES SOME LAVA (+14)] (d)

LOWER JURASSIC

UNUK RIVER FORMATION

12	GREEN, RED, AND PURPLE VOLCANIC BRECCIA, CONGLOMERATE, SANDSTONE, AND SILTSTONE (a); CRYSTAL AND LITHIC TUFF (b); SANDSTONE (c); CONGLOMERATE (d); LIMESTONE (e); CHERT (f); MINOR COAL (g)
11	PILLOW LAVA (a); VOLCANIC FLOWS (b)

TRIASSIC

UPPER TRIASSIC

TAKLA GROUP (?)

10	SILTSTONE, SANDSTONE, CONGLOMERATE (a); VOLCANIC SILTSTONE, SANDSTONE, CONLOMGERATE (b); AND SOME BRECCIA (c); CRYSTAL AND LITHIC TUFF (d); LIMESTONE (e)

PLUTONIC ROCKS

CENOZOIC

OLIGOCENE AND YOUNGER

9	DYKES AND SILLS (SWARMS), DIORITE (a); QUARTZ DIORITE (b); GRANODIORITE (c); BASALT (d)

EOCENE (STOCKS, ETC.) AND OLDER

8	QUARTZ DIORITE (a); GRANODIORITE (b); MONZONITE (c); QUARTZ MONZONITE (d); AUGITE DIORITE (e); FELDSPAR PORPHYRY (f)
7	COAST PLUTONIC COMPLEX: GRANODIORITE (a); QUARTZ DIORITE (b); QUARTZ MONZONITE, SOME GRANITE (c); MIGMATITE – AGMATITE (d)

KILOMETRES

0 1 2 3 4 5

MESOZOIC

JURASSIC

MIDDLE JURASSIC AND YOUNGER ?

6	GRANODIORITE (a); DIORITE (b); SYENODIORITE (c); MONZONITE (d); ALASKITE (e)

LOWER JURASSIC AND YOUNGER ?

5	DIORITE (a); SYENOGABBRO (b); SYENITE (c)

TRIASSIC

UPPER TRIASSIC AND YOUNGER ?

4	DIORITE (a); QUARTZ DIORITE (b); GRANODIORITE (c)

HORNBLENDE PREDOMINANT . . . . H
BIOTITE PREDOMINANT . . . . B

METAMORPHIC ROCKS

JURASSIC

2	HORNFELS (a); PHYLLITE, SEMI-SCHIST, SCHIST (b); GNEISS (c); CATACLASITE, MYLONITE (d); TACTITE (e)

SYMBOLS

ADIT
ANTICLINE (NORMAL, OVERTURNED)
BEDDING (HORIZONTAL, INCLINED, VERTICAL, CONTORTED)
BOUNDARY MONUMENT
CONTOURS (INTERVAL 1,000 FEET) 5000
FAULT (DEFINED, APPROXIMATE)
FAULT (THRUST)
FAULT MOVEMENT (APPARENT)
FOLD AXES, MINERAL LINEATION (HORIZONTAL, INCLINED)
FOSSIL LOCALITY Ⓕ
GEOLOGICAL CONTACT (DEFINED, APPROXIMATE)
GLACIAL STRIAE
GRAVEL, SAND, OR MUD
HEIGHT IN FEET ABOVE MEAN SEA LEVEL •6234'
INTERNATIONAL BOUNDARY
JOINT SYSTEM (INCLINED, VERTICAL)
MARSH
MINING PROPERTY
RIDGE TOP
SCHISTOSITY (INCLINED, VERTICAL)
SYNCLINE (NORMAL, OVERTURNED)
TUNNEL

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BEN ALI / MM GROUP OF CLAIMS
Skeena Mining Division, B.C.

REGIONAL GEOLOGY

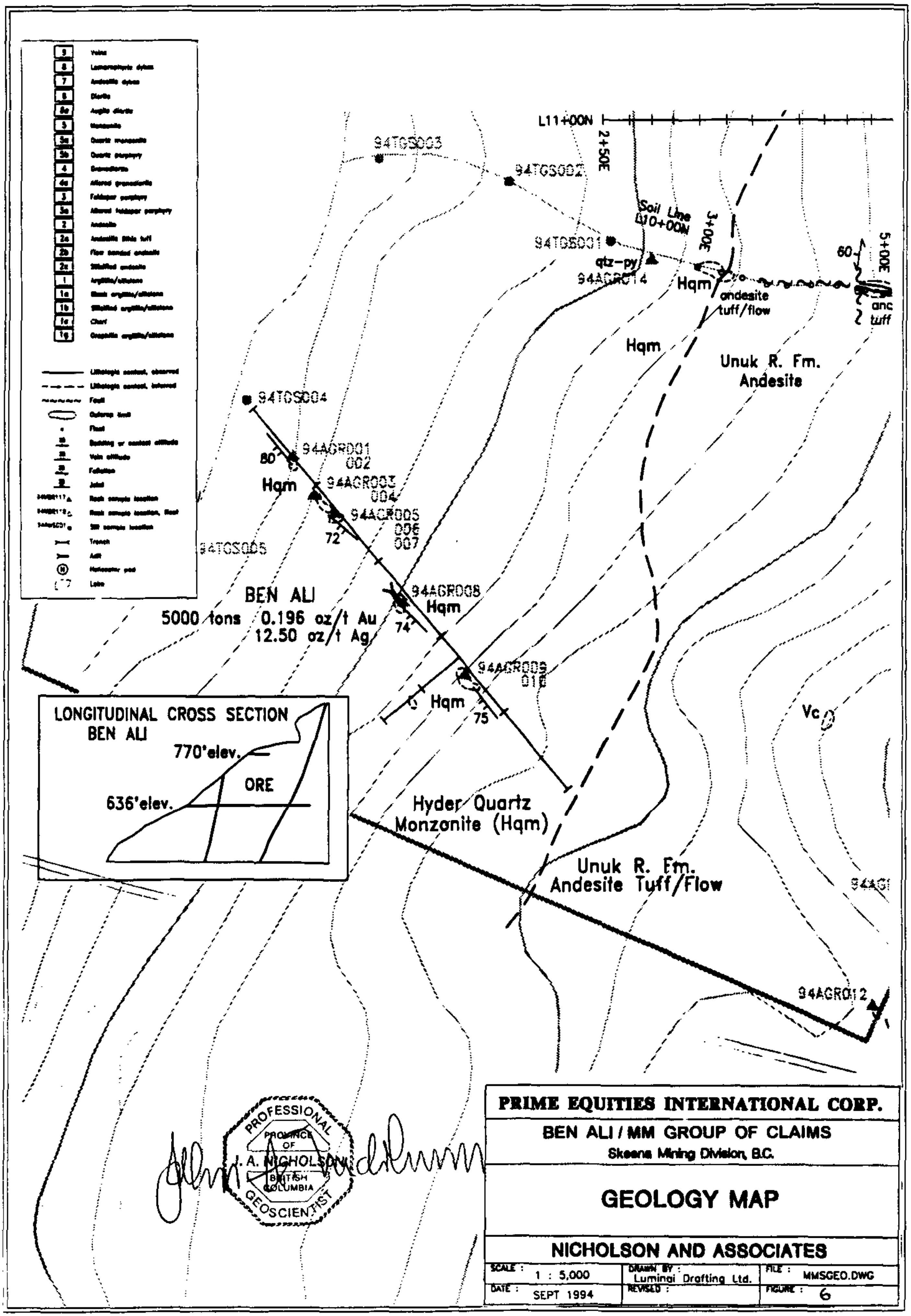
NICHOLSON AND ASSOCIATES

SCALE : AS SHOWN	DRAWN BY :	FILE : BMMREG.DWG
DATE : DEC 1994	REVISED :	FIGURE : 5

PROPERTY GEOLOGY

During the month of July, 2 days were spent on the Ben Ali Group and was mapped on a 1:5000 scale. The property is largely covered by a thick mat of vegetation with moderate to steep topography. Outcroppings are limited to knolls, gullies and ravines.

Lower reaches of the property are covered in alluvium making mapping difficult. Outcroppings observed on the property consisted mainly of Hyder Creek Monzonite and Unuk River Formation Andesite and tuffaceous flows.(figure 6)



PRIME EQUITIES INTERNATIONAL CORP.

BEN ALI / MM GROUP OF CLAIMS

Skeena Mining Division, B.C.

GEOLOGY MAP

NICHOLSON AND ASSOCIATES

SCALE : 1 : 5,000	DRAWN BY : Luminai Drafting Ltd.	FILE : MMSGEO.DWG	
DATE : SEPT 1994	REVISED :	FIGURE : 6	

PROFESSIONAL GEOSCIENTIST
PROVINCE OF BRITISH COLUMBIA
J. A. NICHOLSON

MINERALIZATION

The most evident form of mineralization found on the property is pyrite. Pyrite appears abundant throughout the property.

Pyrite in all instances occurs as fine to medium grained disseminations and also occurs as narrow wispy stringers within both andesitic and sedimentary rock units.

Chalcopyrite occurs primarily as disseminations and as stringers.

Galena and Sphalerite occurs as massive inclusions.

Arsenopyrite is present as medium to coarse grained disseminations, masses and or as streaks in quartz veins.

Tetrahedrite/freibergite is present in most of the quartz veins as irregular blebs and streaks.

Quartz-sulphide mineralization which return elevated Au-Ag values contains trace amounts of electrum.

GEOCHEMICAL SAMPLING RESULTS

During the month of July a total of 5 silt samples and 14 rock samples were collected by crews of Nicholson & Associates.(figure 7)

Silt samples taken were placed into a labelled kraft sample bag. Location sites were marked with pink- glo flagging tape which was marked with black felt pen markers. All samples obtained were later allowed to dry and shipped of dry. Rock samples obtained from the property were all placed into individually labelled plastic sample bags. Sample sites were marked with pink - glo flagging which had corresponding sample numbers marked on the flags.

Silt and rock samples were sent to XRAL Laboratories in Don Mills, Ontario.

All samples were analyzed for 32 element by Induced Coupled Plasma analyser (I.C.P.) with an FA finish for gold. (see Appendix 2 for analysis technique)

Silt samples which were obtained throughout the property returned elevated results.

In the area of the Ben Ali showings, creeks returned elevated Cu-Pb-Zn-Ag-Au-As values. These results are listed bellow:

SAMPLE #	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Au ppb	As ppm
TGS 001	64	430	861	1.3	555	934
TGS 003	40	200	636	0.1	132	346
TGS 004	2,160	488	3,500	13.4	1,160	8
TGS 005	76	130	376	0.1	75	160

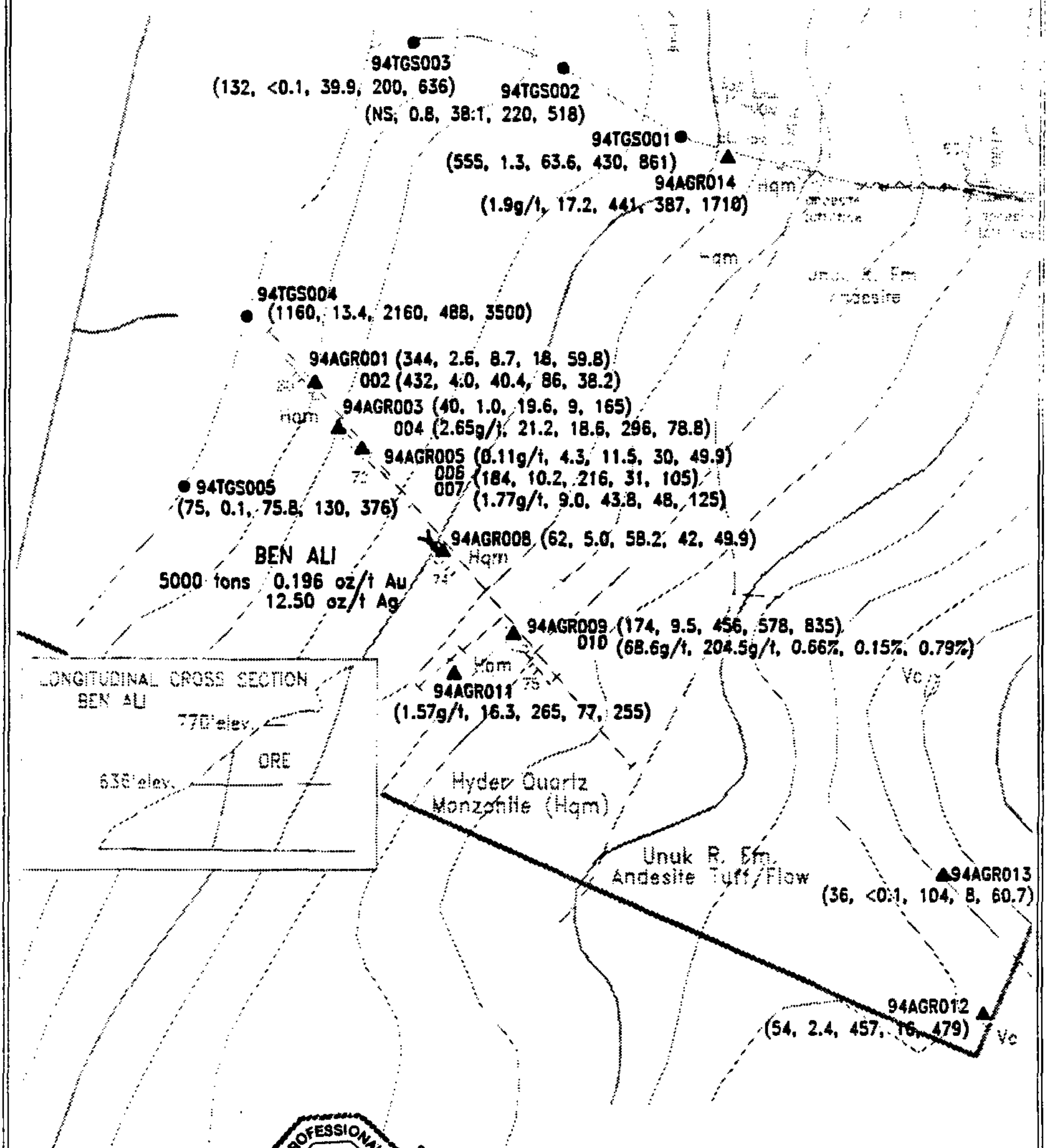
Rock samples which were obtained from the property returned several encouraging results. Several of these areas of interest were in areas of known mineral occurrences on the property which are described as follows: (Appendix 3)

Four levels of underground development consisting of a 96 metre drift (No. 4 level), a collapsed 12 metre adit (No. 3 level), collapsed 25 metre adit (No. 2 level), and a 35 X 20 X 2 metre glory hole, follows a northwest trending, steeply dipping quartz-breccia sulphide vein hosted by a shear zone within the Hyder quartz monzonite. The following samples were obtained from the main vein and adjacent wall rock:

SAMPLE #	WIDTH	Cu ppm	Zn ppm	Pb ppm	Ag ppm	Au ppb	As ppm
AGR 004	48 CM.	19	296	79	21.2	2,380	153
AGR 005	200 CM.	12	30	50	4.3	2,370	17
AGR 007	200 CM.	44	48	125	9.0	1,780	10
AGR 010	GRAB	6,550	1,540	7,760	204.5	76,400	187

A parallel vein located 60 metres southwest of the main vein assayed:

SAMPLE #	WIDTH	Cu ppm	Zn ppm	Pb ppm	Ag ppm	Au ppb	As ppm
AGR 011	25 CM.	265	77	255	16.3	2,450	67
AGR 014	30 CM.	441	387	1,710	17.2	1,910	46



PROFESSIONAL GEOSCIENTIST
PROVINCE OF BRITISH COLUMBIA
J.A. NICHOLSON

PRIME EQUITIES INTERNATIONAL CORP.

BEN ALI / MM GROUP OF CLAIMS

Skeena Mining Division, B.C.

ROCK AND SILT GEOCHEMISTRY SAMPLE MAP

NICHOLSON AND ASSOCIATES

SCALE : 1 : 5,000	DRAWN BY : Luminai Drafting Ltd.	FILE : MMSSAM.DWG
DATE : SEPT 1994	REVISED :	FIGURE : 7

CONCLUSION AND RECOMMENDATIONS

Sampling and mapping undertaken in the vicinity of the Ben Ali vein system appears to have limited the bulk tonnage potential of the vein.

Stream silt samples obtained from the various creeks that drained the Ben Ali vein system, returned elevated values in both gold, silver, copper and arsenic. The samples obtained were taken from streams that cut across the Ben Ali vein. This would account for the elevated numbers that were obtained. Samples taken outside of the drainage pattern elsewhere throughout the property were less than encouraging. This would conclude that the system appears to be limited in size and not as wide spread as had hoped.

The Ben Ali vein system observed on surface appears to be limited in width with the size of the vein ranging from 30 cm. up to 2 metres. Gold values obtained from the vein appear to be relatively consistent in the 2000 - 3000 ppb range with elevated silver and arsenic values. The vein appears to be fissure controlled which would account for the pinching and swelling nature that the vein exhibits. At present the length of the vein is unknown and has not been fully tested.

The surrounding wall rock is relatively unaltered as was seen along the exposed length of the vein.

Therefore, it is being recommended that a MAG - V.L.F. program be undertaken. The program would be orientated to test the strike length of the vein and other related vein fissures which may occur in the vicinity of the Ben Ali vein.

Anticipated cost of this program is $15,000.

PROPOSED PHASE 1 BUDGET

Geophysical Surveys Mag, VLF-EM	$ 8,000
Grid Establishment	$ 3,000
Camp, room and board .	$ 2,000
Consulting, report	$ 2,000
SUBTOTAL	**$15,000**

Contingent on the results of Phase 1, a second phase of trenching and drilling will be recommended.

STATEMENT OF COSTS

Personnel

Andres Kikauka	P.Geol.	2 days @ $300/day	$600.00
Tim Woods		2 days @ $265/day	$530.00
John A. Nicholson	P.Geol.	1 day @ $300/day	$300.00

Equipment Rental

(1) Ford X-tra cab 4 x 4 2 days @ $75/day	$150.00

Assays

5 silt samples @ $20/sample	$100.00
14 rock samples @ $20/sample	$280.00

Room and Board	2 man days @ $35/day	$ 70.00
Field Supplies		$ 25.00
Miscellaneous		$100.00
Report Writing		$300.00
TOTAL EXPENDITURES		**$2,455.00**

Province of British Columbia
Ministry of Energy, Mines and Petroleum Resources
MINERAL RESOURCES DIVISION — TITLES BRANCH

EVENT NO. 3063945
OFFICE USE ONLY

RECEIVED
JAN 3 - 1995
Gold Commissioner's Office
VANCOUVER, B.C.

RECORDING STAMP

Mineral Tenure Act
Sections 25, 26 & 27

STATEMENT OF WORK — CASH PAYMENT

Indicate type of title MINERAL (Mineral or Placer)

Mining Division SKEENA

PLEASE PRINT CLEARLY

I, JOHN A NICHOLSON (Name)
606 675 WEST HASTINGS ST (Address)
VANCOUVER B.C.
682 1845 (Telephone) V6B-1N2 (Postal Code)
Client Number 119688

Agent for DAVID JAVORSKY (Name(s) of all recorded title holders)
1614 675 WEST HASTINGS ST (Address)
VANCOUVER B.C.
(Telephone) V6B 1N2 (Postal Code)
Client Number 113058

STATE THAT: **(NOTE: If only paying cash in lieu or lease rental, turn to reverse and complete columns G to J and Q to T.)**

Work has been done on the SUNBEAM FRACTION, BEN ALI, BEN ALI # 2 Claim(s)

Tenure No.(s) 250637, 251271, 251272

Work was done from JULY 1, , 19 94 , to AUGUST 31 , 19 94 ;

and was done in compliance with Section 50 of the Mineral Tenure Act and

Section 19(3) of the Regulation YES ☒ NO ☐ WORK PERMIT No. SM1-94-0100629O-124

TYPE OF WORK

PHYSICAL: Work such as trenches, open cuts, adits, pits, shafts, reclamation, and construction of roads and trails. Details as required under section 13 of the Regulations, including the map and cost statement must be given on or attached to this statement.

PROSPECTING: Details as required under section 9 of the Regulations must be submitted in a technical report. Prospecting work can only be claimed once by the same owner of the ground, and only during the first three years of ownership.

GEOLOGICAL, GEOPHYSICAL, GEOCHEMICAL, DRILLING: Details must be submitted in a technical report conforming to sections 5 through 8 (as appropriate) of the Regulations.

PORTABLE ASSESSMENT CREDIT (PAC) WITHDRAWAL: A maximum of 30% of the approved value of geological, geophysical, geochemical and/or drilling work on this statement may be withdrawn from the owner's or operator's PAC account and added to the work value on this statement.

Note: Where required, the assessment report must be received within ninety days of the earliest due anniversary date on this statement.

TYPE OF WORK	VALUE OF WORK			
(Specify Physical (include details), Prospecting, Geological, etc.)	Physical	*Prospecting	*Geological, etc.	
GEOLOGICAL			600.00	
GEOCHEMICAL			600.00	
Report to Follow				
TOTALS	A +	B +	C 1200.00	D
PAC WITHDRAWAL — Maximum 30% of Value in Box C Only			E →	E
from account(s) of			TOTAL	F1200.00

*Who was the operator (provided the financing)?
Name PRIME EQUITIES INTL
Address 1100-808 W. HASTINGS ST
VAN B.C. Phone

Transfer amount in Box F to reverse side of form and complete as required.

M29-2024

MTL 112 REV 94/01

F 1200.00 I WISH TO APPLY $ 1200.00 OF THE TOTAL VALUE FROM BOX F AS FOLLOWS:

Columns G through P inclusive MUST BE COMPLETED before work credits can be granted to claims Columns G through J and Q through T inclusive MUST BE COMPLETED before a cash payment or rental payment can be credited Columns not applicable need not be completed.

Cash Payment

	CLAIM IDENTIFICATION				APPLICATION OF WORK CREDIT					
	G	H	I	J	K	L	M	N	O	P
	CLAIM NAME (one claim/lease per line)	TENURE No	No. OF UNITS*	CURRENT EXPIRY DATE	WORK TO BE APPLIED VALUE	WORK TO BE APPLIED YEARS	Recording Fees	PRIOR EXCESS CREDIT BEING USED	NEW EXPIRY DATE	EXCESS CREDIT REMAINING
1	SUNBEAM FRACTION	250637	1	FEB 8 1995	400.00	2	20.00		FEB 8, 1997	
2	BEN ALI	251271	1	JAN 2, 1995	400.00	2	20.00		JAN 2, 1997	
3	BEN ALI #2	251272	1	JAN 2, 1995	400.00	2	20.00		JAN 2, 1997	
4										
5										
6										
7										
8										
9										
10										
11										
12										
13										
14										
15										
16										
17										
18										
19										
					1200.00 TOTAL OF K		60.00 TOTAL OF M			

*2 POST FRACTION REV CROWN GRANT AND PLACER CLAIM ARE 1 UNIT EACH

CASH IN LIEU OF WORK OR LEASE RENTAL

Q	R	S	T
C/L	RECORDING FEE	LEASE RENTAL	NEW EXPIRY DATE
TOTAL OF Q	TOTAL OF R	TOTAL OF S	

NOTICE TO GROUP No ______________ RECORDED ______________

Value of work to be credited to portable assessment credit (PAC) account(s)
(May only be credited from the approved value of Box C not applied to claims.)

		Name	Amount
Name of owner/operator	1		
	2		
	3		

I, the undersigned Applicant, hereby acknowledge and understand that it is an offence to knowingly make a false statement or provide false information under the Mineral Tenure Act I further acknowledge and understand that if the statements made, or information given, in this Statement of Work — Cash Payment are found to be false and the exploration and development has not been performed, as alleged in this Statement of Work — Cash Payment, then the work reported on this statement will be cancelled and the subject mineral claim(s) may as a result, forfeit to and vest back to the Province

Signature of Applicant

REFERENCES

Alldrick, D.J. (1983): Salmon River Project, Stewart, B.C., Geological Fieldwork 1982, B.C. Min.E.M.P.Res., Paper 1983-1, pages 182-195.

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Pritchard, R.A. (1990): DIGHEM III Survey for KRL Res. Corp., Stewart, B.C., Report # 1088.

CERTIFICATE

I, **John A. Nicholson**, do herby certify that:

1. I am a consulting geologist with offices at 606-675 West Hastings Street, Vancouver, British Columbia.

2. I am a graduate of the University of British Columbia with a Bachelor of Science, Geology (Honours).

3. I am a member of the Professional Engineers and Geoscientists of British Columbia, member # 19933.

4. I supervised work carried out on the Ben Ali Group of mineral claims.

5. Data that was used in this report came from field notes and published and unpublished reports.

6. I have no direct or indirect interest in the property or securities in KRL Resources

7. I authorize the use of this report for public financing.

J. A. NICHOLSON

John A. Nicholson, P.Geo

APPENDIX 1

CLAIM RECORDS

```
                           MINERAL TITLES BRANCH (MiDA)                  1994/SEP/22
                           Mineral Tenure Master Report

  Tenure #     : 251272    Old Tenure #: 19   5065    Tenure Sub-Type: claim
  Mining Div.  : SKEENA                               Map #       : 103P13W-E
  Termination  :                   Date:              Tag #       :


URRENT OWNERS
  Client #  Name                                                    % Interest
  113058    JAVORSKY, DAVID                                          100.0000


LAIM DETAILS
  Claim Name   : REFER TO LOT TABLE                   Claim Type : RCG
  Issued       : 1986/JAN/02    Good To: 1995/JAN/02        Area : 1 unit
  Locator      : 999999  MATS CONVERSION


OTS

  District          Lot        Lot Name

      6             4470       BEN ALI NO 2


 ****************************************************************************************
  NOTE:     Mineral Tenure events recorded prior to June 1, 1991                        *
*           are NOT stored on the MiDA system; please refer to manual                   *
            records located in the Gold Commissioner's office.                          *
 ****************************************************************************************

                                  TENURE EVENTS


CLAIM APPLIC.
  Event #   : 2050936     Recorded: 1986/JAN/02     Effective: 1991/JUN/22
  Submitter: 999999  MATS CONVERSION
  Comments : MATS conversion


OTICE TO GROUP
  Event #   : 3041861     Recorded: 1993/SEP/23     Effective: 1993/SEP/23
  Submitter: 113058  JAVORSKY, DAVID
  Comments : N/G BEN ALI MINE


ORK STATEMENT
  Event #   : 3008480     Recorded: 1991/OCT/18     Effective: 1991/OCT/18
  Submitter: 113058  JAVORSKY, DAVID
  Comments :
  Work Start Date : 1991/09/13     Work Stop Date  : 1991/10/10
  Old Good To Date: 1992/01/02     New Good To Date: 1994/01/02
  Work Types:
  PHYSICAL

  Event #   : 3045203     Recorded: 1993/DEC/09     Effective: 1993/DEC/09
  Submitter: 126610  TERRY, MARK A.
  Comments :
  Work Start Date : 1993/10/15     Work Stop Date  : 1993/10/18
```

```
                         MINERAL TITLES BRANCH (MiDA)                    1994/SEP/22
                         Mineral Tenure Master Report

  Tenure #    : 251271    Old Tenure #: 19    5064    Tenure Sub-Type: claim
  Mining Div. : SKEENA                                Map #         : 103P13W-E
  Termination :                    Date:              Tag #         :


CURRENT OWNERS
  Client #  Name                                                      % Interest
  113058    JAVORSKY, DAVID                                            100.0000


CLAIM DETAILS
  Claim Name   : REFER TO LOT TABLE                   Claim Type : RCG
  Issued       : 1986/JAN/02    Good To: 1995/JAN/02        Area : 1 unit
  Locator      : 999999  MATS CONVERSION


LOTS

  District          Lot        Lot Name

      6             4283       BEN ALI


*********************************************************************************
* NOTE:     Mineral Tenure events recorded prior to June 1, 1991               *
*           are NOT stored on the MiDA system; please refer to manual          *
*           records located in the Gold Commissioner's office.                 *
*********************************************************************************

                                  TENURE EVENTS


CLAIM APPLIC.
  Event #  : 2050935     Recorded: 1986/JAN/02     Effective: 1991/JUN/22
  Submitter: 999999  MATS CONVERSION
  Comments : MATS conversion


NOTICE TO GROUP
  Event #  : 3041861     Recorded: 1993/SEP/23     Effective: 1993/SEP/23
  Submitter: 113058  JAVORSKY, DAVID
  Comments : N/G BEN ALI MINE


WORK STATEMENT
  Event #  : 3008480     Recorded: 1991/OCT/18     Effective: 1991/OCT/18
  Submitter: 113058  JAVORSKY, DAVID
  Comments :
  Work Start Date : 1991/09/13     Work Stop Date   : 1991/10/10
  Old Good To Date: 1992/01/02     New Good To Date: 1994/01/02
  Work Types:
  PHYSICAL

  Event #  : 3045203     Recorded: 1993/DEC/09     Effective: 1993/DEC/09
  Submitter: 126610  TERRY, MARK A.
  Comments :
  Work Start Date : 1993/10/15     Work Stop Date   : 1993/10/18
```

```
                           MINERAL TITLES BRANCH (MiDA)                1994/SEP/22
                           Mineral Tenure Master Report

  Tenure #     : 250637    Old Tenure #: 19   1019    Tenure Sub-Type: claim
  Mining Div.  : SKEENA                               Map #       : 104A04W-D
  Termination  :                 Date:                Tag #       :

 CURRENT OWNERS
  Client #  Name                                                  % Interest
  113058    JAVORSKY, DAVID                                        100.0000

 CLAIM DETAILS
  Claim Name   : REFER TO LOT TABLE                   Claim Type : RCG
  Issued       : 1979/FEB/08    Good To: 1995/FEB/08        Area : 1 unit
  Locator      : 999999  MATS CONVERSION

 LOTS

  District          Lot        Lot Name

      6             4469       SUNBEAM FR

 ******************************************************************************
 * NOTE:    Mineral Tenure events recorded prior to June 1, 1991              *
 *          are NOT stored on the MiDA system; please refer to manual         *
 *          records located in the Gold Commissioner's office.                *
 ******************************************************************************

                                  TENURE EVENTS

 CLAIM APPLIC.
  Event #   : 2050301      Recorded: 1979/FEB/08     Effective: 1991/JUN/22
  Submitter: 999999  MATS CONVERSION
  Comments : MATS conversion

 NOTICE TO GROUP
  Event #   : 3041861      Recorded: 1993/SEP/23     Effective: 1993/SEP/23
  Submitter: 113058  JAVORSKY, DAVID
  Comments : N/G BEN ALI MINE

 WORK STATEMENT
  Event #   : 3008480      Recorded: 1991/OCT/18     Effective: 1991/OCT/18
  Submitter: 113058  JAVORSKY, DAVID
  Comments :
  Work Start Date : 1991/09/13     Work Stop Date   : 1991/10/10
  Old Good To Date: 1992/02/08     New Good To Date: 1994/02/08
  Work Types:
  PHYSICAL

  Event #   : 3045203      Recorded: 1993/DEC/09     Effective: 1993/DEC/09
  Submitter: 126610  TERRY, MARK A.
  Comments :
  Work Start Date : 1993/10/15     Work Stop Date   : 1993/10/18
```

APPENDIX 2

ASSAY TECHNIQUES

XRAL
XRAL Laboratories
A Division of SGS Canada Inc.

Acid Extraction, determination by ICP Spectroscopy - 36 elements

Description:

A quarter gram sample is digested with 2 ml of nitric acid for one half hour in a water bath, then 1 ml of hydrochloric acid is added and the digestion continues for another 2 hours. Test tubes are shaken at regular intervals.

In house standards and previously analysed samples are run to monitor proper digestion procedures. Synthetic standards are used to calibrate the instrument.

Limitations:

The nitric aqua regia extraction will not completely extract difficultly soluble elements such as Ba,Cr,Sb,Sn,Ta,W,V and Zr. The multi-acid extraction (Method code 80-1) will ensure better extraction, though some refractory minerals may remain incompletely attacked. Volatile elements such as As may be lost from solution in the multi-acid attack.

Elements:

Al	0.01%	Fe	0.01%	Na	0.01%
Sb	5ppm	Pb	2ppm	Sr	.5ppm
As	5ppm	Li	1ppm	Ag	.1ppm
Ba	1ppm	Mg	.01%	Sn	10ppm
Be	.5ppm	Mn	.01%	Ti	.01%
Bi	3ppm	Mo	1ppm	W	10ppm
Cd	1ppm	Ni	1ppm	V	2ppm
Ca	.01%	P	.01%	Y	.1ppm
Cr	1ppm	K	.01%	Zr	.5ppm
Co	1ppm	Sc	.5ppm	Zn	.5ppm
Cu	.5ppm				

Prepared by	Approved by	Date

Issue 1
Rev. 0
December 19/91
Part
Page 1

XRAL **X-Ray Assay Laboratories**
A Division of SGS Supervision Services Inc.

X-Ray Fluorescence Spectrometry - 27 Elements - Pressed Pellet

Description:

At least 5 g of sample is required for the analysis of one or all of the above elements. A pellet is loaded into the holder of the automatic sample changer of a Philips PW1400 wavelength dispersive x-ray spectrometer. The 40 mm diameter sample pellets are loaded six to a tray with a total of 10 trays.

Elements are run in an inert nitrogen atmosphere employing a rhodium tube which also serves as an internal standard for some elements. For different combinations of requested elements various standard reference materials are inserted with these samples to verify calibration. Calibration is programmed into the instrument and inter-element corrections are applied to necessary analyte elements. Commonly requested element combinations are programmed to be determined individually or in groups.

Limitations:

This procedure is not suitable for mineralized materials. The presence of percentage levels of any element except the usual major rock constituents will have a adverse effect on the calibration.

The maximum concentration reported by these procedures is generally 5000 ppm. Analysis for elements with concentrations higher than 5000 ppm should be analysed by one of our assay procedures. The assay procedure involves a potassium pyrosulfate fusion of the sample followed by the preparation of a pressed disk. The pyrosulfate fusion produces a very homogeneous sample material with a uniform grain size. The fusion also saturates any matrix impact from the sample with the overwhelming matrix of the pyrosulfate flux itself thus allowing for synthetic standard calibrations. Internal standards are also used for assay grade analysis. This procedure is essential to produce the accuracy and precision requirements needed for assay grade analysis.

Elements:

Sb	3 ppm	Pb	2 ppm	Tl	5 ppm
As	3 ppm	Mo	2 ppm	Th	2 ppm
Ba	20 ppm	Nb	2 ppm	Sn	5 ppm
Bi	3 ppm	Ni	2 ppm	Ti	5 ppm
Cl	50 ppm	Rb	2 ppm	W	5 ppm
Co	2 ppm	Sc	3 ppm	U	2 ppm
Cu	2 ppm	Sr	2 ppm	Y	2 ppm
Ga	3 ppm	S	50 ppm	Zr	3 ppm
Fe	3 ppm	TA	5 ppm	Zn	2 ppm

Prepared by Approved by Date

Geochemical Gold , Platinum and Palladium by Lead Fire Assay
Assay Gold, Platinum, Palladium and Silver by Lead Fire Assay

Our quality control includes the following procedures:

1. The cleaner sample which was crushed before the samples is analysed along with the samples.

2. A standard reference sample doped with cobalt and copper is run with each tray. The position of this standard is varied systematically from one tray to the next. This serves as a check to identify each batch through to the final cupellation and as a monitor of the final measurement of gold content.

3. Every tenth sample is run in duplicate. The second run is made at a different time from the first.

4. anomalous samples are repeated.

The routine involves weighing of a 15 or 30 gram aliquot of sample on a top loader electronic balance to_+_ 0.01 grams tolerance. This is added to a assay crucible which has been pre-charged with 100-200 grams of flux. A fixed amount of reducing agent is then added to ensure production of a 30-50 gram lead button during fusion. Finally for gold assays five milligrams of silver is added and the sample and flux are mixed together.

The fusion is carried out at an average temperature of about 1000 degrees celsius for about 1 hour. Melts are poured and when the slag has cooled the lead buttons are recovered, deslagged, and placed in preheated cupels in the cupellation furnace. Cupellation takes about 1 hour and is carried out at about 960 degrees celsius. The silver bead recovered after cupellation can be treated in several ways to determine the gold content as indicated below.

1. Plasma spectrometry: Requires digestion of the bead with aqua regia followed by measurement of the gold content in the solution. Platinum and palladium may also be determined on this solution (XRAL Group 02-1).

2. Neutron activation analysis: This requires only an irradiation of the bead followed by measurement of the gold content by gamma spectrometry. It is normally used for the analysis of gold only.

3. For high grade samples the gold can be parted from the silver and weighed as per the classical technique.

Atomic absorption is seldom used as the sensitivity is not quite adequate for the low levels required for geochemical applications.

Silver analyses follow the same path as gold samples except that the final measurement is always gravimetric and no silver is added to the pot.

Elements:

Au to 1 ppb detection limit

Prepared by	Approved by	Date

APPENDIX 3

ASSAY SAMPLE RESULTS

ROCK SAMPLE DESCRIPTION RECORD

			Location: Stewart			Operator:		
Sample No.	Location	Description	Analytical Results					
			Au	Ag	Pb	Zn	Cu	As
	BEN ALI CK.		ppb/g/t	ppm	ppm/%	ppm/%	ppm/%	ppm
94AGR001	0+60E 0+00S	180 cm chp channel, qtz. monzonite wall rock 5% frac. fill py.	344	2.6	18	59.8	8.7	14
94AGR002	0+60E 0+00S	40 cm. chip channel, NW trending qtz. vein, 20% py 1-5 mm. blebs.	432	4.0	86	38.2	40.4	30
94AGR003	1+08E 0+07S	180 cm, chip channel, qtz. monzonite wall rock, 5% frac. fill py.	40	1.0	9	165	19.6	4
94AG004	1+30E 0+09S	48 cm. chip channel, NW trending qtz. vein, 20% py 1-6 mm. blebs.	2380	21.2	296	78.8	18.6	153
94AGR005	1+30E 0+09S	200 cm. chip channel, qtz. monzonite wall rock, 3% frac. fill py. several 0.5-3.0 cm. qtz. veins along fractures.	3470 .11 g/t	4.3	30	49.9	11.5	17
94AGR006	1+30E 0+09S	28 cm. chip channel, WNW trending qtz. vein, 20% py.	184	10.2	31	105	216	20
94AGR007	1+30E 0+09S	200 cm chip channel, qtz. monzonite wall rock, 3% frac. fill py.	1780 1.77 g/t	9.0	48	125	43.8	10

ROCK SAMPLE DESCRIPTION RECORD

			Location: Stewart			Operator:		
Sample No.	**Location**	**Description**	**Analytical Results**					
			Au	**Ag**	**Pb**	**Zn**	**Cu**	**As**
	BEN ALI CK.		**ppb/g/t**	**ppm**	**ppm/%**	**ppm/%**	**ppm/%**	**ppm**
94AGR008	2+39E 0+04S	65 cm chip channel, NW trending qtz. vein, 8% py. at portal No. 4 level	62	5.0	42	49.9	58.2	9
94AGR009	3+40E 0+08S	180 cm. chip channel, qtz. monzonite wallrock, 5% py.	174	9.5	578	835	456	22
94AGR010	3+40E 0+08S	GRAB, NW trending qtz. vein from glory hole stope 25% py 3% sp 1% cp.	76400 68.6 g/t	46.9 204.5	1540 .15%	7760 .79%	6550 .66%	187
94AGR011	3+25E 0+68S	25 cm. chip channel 8% py. in qtz. monzonite	2450 1.57 g/t	16.3	77	255	265	67
94AGR012	Shagri-La grid L6+50E 2+OOS	35 cm. chip channel, bleached felsic rock, 1% py. trace cp. mal barite	54	2.4	16	479	457	22
94AGR013	L7+00E 1+20S	12 cm.chip channel, altered volcanics 1-3 cm. qtz. veinlets, 5% pyo. trace cp. 3% chlorite.	36	< .1	8	60.7	104	11
94AGR014	I1+00E 2+50N	30 cm. chip channel, Altered qtz. monzonite, 5% chlorite, 8% py. 8% qtz. as veins.	1910 1.9 g/t	17.2	387	1710	441	46

10924.A

SAMPLE	AU-1AT PPB FADCP 1	AU-1AT G/MT FA 0.03	BE PPM ICP 0.5	NA % ICP 0.01	MG % ICP 0.01	AL % ICP 0.01	P % ICP 0.01	K % ICP 0.01	CA % ICP 0.01	SC PPM ICP 0.5
94AGR001	344	--	1.0	.04	.22	.58	.04	.24	.08	<.5
94AGR002	432	--	.9	.04	.05	.22	.01	.16	.02	<.5
GR003	40	--	1.0	.05	.42	.96	.07	.35	.17	1.0
AGR004	2380	2.65	1.5	.03	<.01	.13	<.01	.14	<.01	<.5
94AGR005	2370	.11	1.1	.04	.24	.83	.05	.33	.13	<.5
94AGR006	184	--	1.0	.04	.32	.98	.05	.33	.18	<.5
94AGR007	1780	1.77	.9	.05	.34	.85	.05	.29	.12	.6
94AGR008	62	--	.5	.04	.03	.21	<.01	.18	.03	<.5
94AGR009	174	--	1.2	.04	.40	.96	.06	.34	.15	.9
94AGR010	76400	68.6	2.6	.03	<.01	.11	<.01	.12	<.01	<.5
94AGR011	2450	1.57	1.5	.03	.25	.76	.04	.35	.08	<.5
94AGR012	54	--	.6	.09	.12	.34	.06	.02	.70	.6
94AGR013	36	--	1.7	.32	.47	3.61	.06	.48	2.14	2.7
94AGR014	1910	1.90	1.4	.04	.25	.75	.05	.33	.29	<.5
94ABR001	299	--	1.5	.04	.84	.87	.06	.17	.15	<.5
94ABR002	155	--	2.8	.06	1.89	2.47	.20	.44	.61	[illegible]
94ABR003	2820	2.59	8.4	.03	.11	.21	.01	.06	.02	<.5
94ABR004	2350	2.32	4.1	.04	.50	.67	.05	.20	.11	<.5
94ABR005	2100	2.17	6.3	.04	.17	.33	.03	.11	.07	<.5
94AHR001	2430	2.25	1.8	.04	.50	.64	.03	.07	.06	2.2
94AHR002	1610	1.84	4.9	.03	.14	.30	.04	.10	.27	<.5
94AHR003	5530	4.76	5.4	.03	.17	.38	.05	.14	.24	<.5
94AHR004	322	--	1.8	.03	.36	.63	.07	.25	1.15	1.0
94AHR005	875	--	3.7	.03	.13	.46	.13	.25	.31	<.5
94AHR006	252	--	1.8	.03	.46	.90	.12	[illegible]	.48	1.5
94JHR036A	12	--	1.9	.06	1.64	2.01	.10	.11	.65	5.4
94JHR037A	36	--	1.9	.06	2.41	2.36	.14	.10	1.22	5.5
94JHR038A	9	--	1.8	.05	1.18	1.51	.12	.19	1.42	7.4
94JHR039A	4	--	1.2	.05	1.50	1.74	.07	.06	.31	3.5
94JHR040A	3	--	1.8	.05	1.60	2.34	.12	.21	.63	5.9
94JHR041A	346	--	2.9	.03	1.97	2.19	.15	.26	2.50	6.2
94JHR042A	3	--	2.1	.06	1.43	2.44	.12	.07	.50	6.6
94JHR043A	7980	6.97	7.1	.03	.38	.37	<.01	.03	.39	<.5
94JHR044A	5640	5.11	3.3	.04	.66	.94	.09	.16	.58	1.4
94JBR084	26	--	1.7	.05	1.63	1.81	.12	.05	.25	4.7
94BDR087	12	--	1.6	.40	.39	3.29	.05	.24	2.12	1.7
BDR090	8	--	1.5	.20	.44	1.42	.08	.18	.91	1.0
DR091	5	--	.7	.14	.12	.72	.03	.06	2.85	<.5
94BDR093	4	--	1.0	.13	.17	.88	.05	.04	1.24	<.5
94BDR094	4	--	<.5	.04	.02	.20	<.01	.02	.68	<.5
94BDR095	<1	--	1.4	.43	1.21	3.25	.09	.73	1.47	4.0
94BDR097	31	--	1.5	.22	.79	1.65	.08	.25	.82	7.2
94BDR098	2	--	1.4	.33	.59	2.46	.07	.33	1.45	3.1
94BDR099	36	--	.6	.03	.07	.19	.01	.10	.60	<.5
94BDR100	8	--	1.8	.06	1.33	1.55	.15	.09	.24	3.7
94BDR101	12	--	1.7	.05	1.26	1.36	.11	.06	.31	7.5
94BDR102	50	--	2.9	.04	2.63	2.81	.12	.12	.22	9.9
94BDR103	92	--	2.2	.04	.82	1.42	.12	.26	1.23	[illegible]
94BDR104	48	--	5.3	.04	2.16	2.42	.16	.07	19	8.3
94BDR106	640	--	3.1	.04	3.21	3.75	.17	.07	[illegible]	15.7
94BTR003	22	--	1.0	.05	.84	1.27	.08	.20	1.68	1.0
94BTR005	11	--	1.1	.04	1.27	.54	.20	.39	3.47	3.4
94BTR007	33	--	1.6	.04	1.23	1.93	.16	.28	1.26	2.4
94BTR008	2	--	2.4	.05	1.52	2.08	.20	.38	3.99	7.4
94BTR010	2	--	.7	.06	.76	.57	.17	.41	3.76	5.1
94BTR022	<1	--	2.3	.07	3.52	4.39	.09	.06	.55	4.0
94BTR023	4	--	1.3	.05	1.36	1.65	.21	.43	1.52	3.4
94BTR024	<1	--	1.8	.04	2.98	3.59	.09	.06	.45	2.5
94BTR025	165	--	2.7	.23	3.24	5.70	.08	2.78	1.46	27.9
94BTR026	30	--	1.9	.22	2.31	4.09	.08	1.97	[illegible]	13.2
94BTR030	14	--	.9	.09	.83	1.41	.09	.86	[illegible]	4.2
94BTR033	14	--	.9	.21	.43	1.42	.02	.25	[illegible]	1.8
94HDR122	486	--	.9	.04	.02	.14	.02	.16	.03	.7
94HDR123	4980	4.74	4.1	.05	.01	.06	<.01	.05	.02	<.5
94AGR015	521	--	1.8	.04	.12	.35	.03	.20	.09	<.5
94AGR016	47000	64.4	3.9	.04	<.01	.04	<.01	.06	.02	<.5
94AGR017	2480	1.97	2.0	.04	<.01	.07	<.01	.09	<.01	<.5
94BDR023	16	--	1.1	.25	.98	2.89	.14	.87	1.40	5.7
94BDR024	4	--	1.6	.04	.30	.54	.08	.30	2.58	3.8
94BDR025	4	--	.5	.07	.01	.13	<.01	.07	.09	<.5
94BDR026	<1	--	<.5	.08	.02	.12	<.01	.05	.05	<.5
BDR027	<1	--	.5	.06	.02	.14	<.01	.06	.04	<.5
4BDR028	9	--	.5	.08	.12	.35	.10	.03	1.01	<.5
94BDR036	79	--	2.4	.09	.37	.82	.06	.28	.66	.9
94BDR037	6	--	.8	.05	1.50	.29	.13	.11	9.87	1.9
94BDR038	10	--	1.7	.04	.67	1.10	.10	.13	.33	1.8
94BDR039	17	--	1.1	.04	.56	.30	.13	.22	.47	1.2
94BDR040	16	--	1.9	.04	3.15	3.56	.12	.11	4.35	6.6
94BDR041	35	--	1.4	.04	1.65	1.53	.10	.12	4.78	4.4
94BDR042	24	--	1.1	.04	1.39	.94	.12	.12	4.92	[illegible]

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SAMPLE	AU-1AT PPB FADCP 1	AU-1AT G/MT FA 0.03	BE PPM ICP 0.5	NA % ICP 0.01	MG % ICP 0.01	AL % ICP 0.01	P % ICP 0.01	K % ICP 0.01	CA % ICP 0.01	SC PPM ICP 0.5
94JBR083	5	--	1.7	.08	1.83	1.84	.06	.34	.58	6.8
94JHR085	29	--	2.0	.05	1.89	1.96	.17	.08	.48	9.6
HR086	12	--	1.1	.05	2.64	2.66	.26	.07	.95	8.8
HR087		--	1.8	.07	2.12	1.87	.17	.28	6.51	12.4
94JHR088	22	--	1.4	.06	.96	1.41	.08	.20	2.26	2.8
94JHR089	36	--	1.0	.05	.73	1.03	.05	.18	4.34	2.2
94JHR090	5	--	<.5	.06	.10	.14	<.01	.04	.02	<.5
94HDR109	5	--	.9	.08	1.83	1.91	.10	.11	.19	3.2
94HDR110	<1	--	1.3	.07	3.59	3.38	.18	.04	4.78	23.3
94HDR111	102	--	.6	.03	.34	.57	.08	.18	.16	1.3
94HDR112	12	--	.8	.08	.69	1.16	.27	.19	.50	2.5
94HDR113	3	--	.9	.08	1.57	1.73	.18	.08	.73	3.9
94HDR114	<1	--	.9	.07	1.56	1.78	.09	.17	1.23	2.8
94HDR115	10	--	1.0	.07	2.26	2.21	.17	.10	3.81	13.5
94HDR116	4	--	.9	.09	1.28	1.74	.18	.07	.90	3.3
94HDR117	8	--	.7	.09	1.23	1.58	.09	.05	.70	1.6
94HDR120	2	--	.8	.09	1.50	1.57	.15	.09	1.30	2.1
94HDR121	6	--	<.5	.07	.49	.64	.04	.14	.07	.7
D 94AGR001	211	--	<.5	.04	.23	.59	.04	.25	.09	.7
94AGR013	41	--	1.3	.37	.52	3.98	.06	.52	2.40	3.2
94AHR006	278	--	1.0	.03	.45	.87	.11	.26	.49	2.0
94BDR090	10	--	.9	.22	.48	1.56	.08	.19	1.02	1.4
D 94BDR102	--	--	1.6	.03	2.52	2.60	.12	.11	.21	9.1
D 94BDR104	50	--	--	--	--	--	--	--	--	--
94BTR025	--	--	1.7	.23	3.43	5.86	.08	2.81	1.52	27.6
94BTR030	37	--	--	--	--	--	--	--	--	--
94BDR026	--	--	<.5	.06	.02	.13	<.01	.05	.05	.9
D 94BDR028	9	--	--	--	--	--	--	--	--	--
94BDR045	--	--	.6	.03	1.00	1.29	.08	.11	.32	1.7
94BDR047	29	--	--	--	--	--	--	--	--	--
94BDR055	--	--	.6	.03	.79	.98	.09	.10	2.68	1.5
D 94BDR059	20	--	--	--	--	--	--	--	--	--
D 94BDR069	--	--	3.1	.05	.25	.17	.02	.13	.92	<.5
94BDR073	15	--	--	--	--	--	--	--	--	--
94BDR082	--	--	2.3	.27	.88	2.40	.08	.84	2.76	7.1
94BDR086	28	--	--	--	--	--	--	--	--	--
D 94JBR053	--	--	1.3	.06	1.35	.87	.10	.31	4.08	8.8
BR057	18	--	--	--	--	--	--	--	--	--
BR063	--	--	1.5	.10	2.10	2.70	.12	.34	.93	16.8
94JBR069	84	--	--	--	--	--	--	--	--	--
D 94JBR076	--	--	.8	.17	1.28	1.98	.07	.11	1.27	7.5
D 94ABR006	51	--	--	--	--	--	--	--	--	--
94JHR086	--	--	1.1	.04	2.56	2.57	.26	.07	.88	8.2
94HDR110	2	--	--	--	--	--	--	--	--	--
94HDR116	--	--	.8	.09	1.27	1.69	.17	.07	.82	3.0

SAMPLE	TI % ICP 0.01	V PPM ICP 2	CR PPM ICP 1	MN PPM ICP 2.00	FE % ICP 0.01	CO PPM ICP 1	NI PPM ICP 1	CU % XRF 0.01	CU PPM ICP 0.5	ZN % XRF 0.01
94AGR001	.01	17	85	256	2.05	6	5	--	8.7	--
94AGR002	<.01	5	154	79.0	1.59	10	14	--	40.4	--
94AGR003	.02	24	71	781	1.79	9	<1	--	19.6	--
94AGR004	<.01	5	139	41.0	4.24	17	<1	--	18.6	--
94AGR005	.02	16	69	443	2.38	11	<1	--	11.5	--
94AGR006	<.01	21	85	610	2.53	11	1	--	216	--
94AGR007	.02	22	60	586	2.15	7	<1	--	43.8	--
94AGR008	<.01	4	129	62.0	.71	6	<1	--	58.2	--
94AGR009	.01	24	62	921	2.72	10	<1	--	456	--
94AGR010	<.01	7	109	41.0	8.73	18	<1	.66	6550	.79
94AGR011	<.01	13	70	390	3.85	7	<1	--	265	--
94AGR012	.05	13	68	125	.82	15	1	--	457	--
94AGR013	.07	120	22	224	3.38	23	<1	--	104	--
94AGR014	<.01	13	69	516	3.87	11	<1	--	441	.17
94ABR001	.02	19	63	308	3.46	15	24	--	197	1.36
94ABR002	.07	131	136	749	7.90	18	45	--	463	1.08
94ABR003	<.01	29	26	63.0	33.7	34	55	--	708	--
94ABR004	.02	30	73	201	15.2	46	27	--	415	.24
94ABR005	<.01	27	65	147	23.9	63	32	.07	1130	.43
94AHR001	<.01	30	131	425	5.82	7	15	--	562	1.64
94AHR002	<.01	24	59	187	18.5	13	2	--	150	6.07
94AHR003	<.01	23	53	151	20.9	141	34	--	45.3	.10
AHR004	<.01	33	73	504	4.60	12	10	--	48.0	--
94AHR005	<.01	19	49	104	12.0	17	16	--	49.1	.30
94AHR006	<.01	24	62	221	4.38	11	16	--	77.5	.15
94JHR036A	.09	109	104	739	4.25	19	37	--	63.0	--
94JHR037A	.08	165	114	773	4.36	24	45	--	57.8	--
94JHR038A	<.01	68	31	1720	4.48	25	12	--	86.3	--
94JHR039A	.11	86	104	704	3.50	13	22	--	32.3	--
94JHR040A	<.01	87	55	1960	4.57	16	25	--	51.9	.10

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SAMPLE	TI % ICP 0.01	V PPM ICP 2	CR PPM ICP 1	MN PPM ICP 2.00	FE % ICP 0.01	CO PPM ICP 1	NI PPM ICP 1	CU % XRF 0.01	CU PPM ICP 0.5	ZN % XRF 0.01
94BDR055	<.01	22	33	1070	3.41	11	84	--	60.5	--
94BDR059	--	--	--	--	--	--	--	--	--	--
D 94BDR069	<.01	15	30	614	22.9	80	10	--	2090	--
DR073	--	--	--	--	--	--	--	--	--	--
DR082	.09	683	80	793	12.0	80	273	--	436	--
94BDR086	--	--	--	--	--	--	--	--	--	--
D 94JBR053	<.01	60	30	463	4.84	22	33	--	411	--
94JBR057	--	--	--	--	--	--	--	--	--	--
94JBR063	.16	197	72	612	9.02	30	51	--	570	--
94JBR069	--	--	--	--	--	--	--	--	--	--
94JBR076	.29	146	58	439	4.75	21	54	--	240	--
D 94ABR006	--	--	--	--	--	--	--	--	--	--
94JHR086	.10	211	114	651	6.07	17	20	--	167	--
94HDR110	--	--	--	--	--	--	--	--	--	--
94HDR116	.05	82	59	492	3.30	11	10	--	46.8	--

SAMPLE	ZN PPM ICP 0.5	AS PPM ICP 3	SR PPM ICP 0.5	Y PPM ICP 0.1	ZR PPM ICP 0.5	MO PPM ICP 1	AG G/MT FA 3.0	AG PPM ICP 0.1	CD PPM ICP 1	SN PPM ICP 10
94AGR001	59.8	14	6.9	1.8	<.5	5	--	2.6	<1	<10
94AGR002	38.2	30	1.2	1.3	<.5	7	--	4.0	<1	<10
94AGR003	165	4	9.8	3.7	<.5	5	--	1.0	<1	<10
94AGR004	78.8	153	.9	1.2	<.5	37	--	21.2	<1	<10
94AGR005	49.9	17	5.3	2.4	<.5	15	--	4.3	<1	<10
94AGR006	105	20	7.7	3.7	<.5	5	--	10.2	<1	<10
94AGR007	125	10	7.5	2.9	<.5	3	--	9.0	<1	<10
94AGR008	49.9	9	1.0	1.5	<.5	2	--	5.0	<1	<10
94AGR009	835	22	3.8	4.0	<.5	7	--	9.5	1	<10
94AGR010	7760	187	<.5	1.1	<.5	2	204.5	46.9	85	<10
94AGR011	255	67	1.9	1.4	<.5	1	--	16.3	<1	<10
94AGR012	479	22	7.5	7.5	<.5	4	--	2.4	5	<10
94AGR013	60.7	11	294	5.4	<.5	2	--	<.1	<1	<10
94AGR014	1710	46	6.2	3.3	<.5	15	--	17.2	12	<10
94ABR001	13200	282	3.4	5.5	<.5	3	--	23.4	340	<10
94ABR002	10700	256	20.8	7.2	<.5	3	--	27.8	256	<10
94ABR003	429	175000	<.5	1.5	<.5	<1	252.5	37.4	<1	<10
ABR004	2430	76600	3.9	2.5	<.5	5	239.1	33.8	43	<10
BR005	4380	4210	2.0	2.8	<.5	<1	215.7	66.9	121	<10
AHR001	14900	2710	3.3	1.5	<.5	8	47.8	30.8	364	<10
94AHR002	63600	23700	17.0	3.0	<.5	1	149.2	51.8	1470	<10
94AHR003	1260	249000	12.1	2.8	<.5	<1	37.2	51.5	19	<10
94AHR004	747	1510	51.9	5.1	<.5	5	--	8.3	16	<10
94AHR005	2730	1600	17.5	4.7	<.5	1	--	26.3	53	<10
94AHR006	1670	1020	25.4	4.4	<.5	3	--	14.9	36	<10
94JHR036A	144	78	17.8	7.8	<.5	4	--	2.4	<1	<10
94JHR037A	80.8	52	19.5	6.8	<.5	5	--	1.0	<1	<10
94JHR038A	249	84	56.7	9.4	<.5	4	--	1.6	<1	<10
94JHR039A	48.1	39	11.1	5.2	<.5	3	--	1.9	<1	<10
94JHR040A	1080	32	29.1	6.9	<.5	3	--	1.5	6	<10
94JHR041A	10600	10900	95.5	7.7	<.5	2	--	17.9	342	<10
94JHR042A	5260	101	17.9	5.6	<.5	7	--	4.5	51	<10
94JHR043A	7720	36600	8.9	2.8	<.5	<1	284.4	83.8	239	<10
94JHR044A	11600	31200	28.1	5.1	<.5	<1	316.0	54.2	353	<10
94JBR084	232	277	7.6	8.2	<.5	2	--	3.5	<1	<10
94BDR087	60.7	47	104	4.4	<.5	1	--	1.2	<1	<10
94BDR090	36.6	88	69.6	5.0	<.5	18	--	<.1	<1	<10
94BDR091	144	44	71.6	4.0	<.5	5	--	1.7	<1	<10
94BDR093	36.1	17	29.4	4.8	<.5	7	--	1.6	<1	<10
94BDR094	12.7	16	4.8	2.8	<.5	17	--	.9	<1	<10
94BDR095	42.9	9	139	5.4	<.5	5	--	.9	<1	<10
94BDR097	90.2	21	68.3	5.6	<.5	5	--	2.9	<1	<10
94BDR098	26.5	11	115	5.2	<.5	2	--	.6	<1	<10
94BDR099	11.6	43	20.1	1.7	<.5	10	--	.2	<1	<10
94BDR100	50.0	7	10.7	9.2	<.5	11	--	.7	<1	<10
94BDR101	50.1	50	9.7	10.8	<.5	8	--	2.3	<1	<10
94BDR102	47.7	37	10.3	4.7	<.5	7	--	2.6	<1	<10
94BDR103	69.2	51	77.3	5.1	<.5	10	--	4.0	<1	<10
94BDR104	30.7	65	7.8	6.9	<.5	3	--	3.5	<1	<10
94BDR106	42700	320	22.7	7.1	<.5	7	85.6	30.5	304	<10
94BTR003	209	15	40.0	4.2	<.5	2	--	2.5	<1	<10
94BTR005	349	12	142	7.6	<.5	2	--	1.3	<1	<10
BTR007	54700	234	29.7	5.3	<.5	3	--	10.9	540	<10
BTR008	383	16	98.3	8.1	<.5	<1	--	1.9	<1	<10
94BTR010	1210	152	89.7	8.6	<.5	2	--	2.0	13	<10
94BTR022	190	18	15.1	11.3	<.5	2	--	.3	<1	<10
94BTR023	104	<3	27.5	4.9	<.5	<1	--	<.1	<1	<10
94BTR024	99.8	10	12.6	11.3	<.5	<1	--	.3	<1	<10
94BTR025	2600	62	44.4	8.6	<.5	4	--	1.5	41	<10
[illegible]	[illegible]	[illegible]	61.6	[illegible]	<.5	[illegible]	--	[illegible]	[illegible]	[illegible]

Ore Mtn

Deadwood Zone

Ore Mtn Shear

BEN ALI

SAMPLE	ZN PPM ICP 0.5	AS PPM ICP 3	SR PPM ICP 0.5	Y PPM ICP 0.1	ZR PPM ICP 0.5	MO PPM ICP 1	AG G/MT FA 3.0	AG PPM ICP 0.1	CD PPM ICP 1	SN PPM ICP 10
94JBR065	53.6	105	18.6	10.0	<.5	4	--	.4	<1	<10
94JBR066	98.0	14900	33.7	7.6	<.5	<1	--	4.5	<1	<10
JBR067	69.9	3580	10.5	6.8	<.5	<1	--	4.3	<1	<10
JBR068	46.2	234	10.0	8.6	1.1	3	--	1.5	<1	<10
94JBR069	37.7	1880	12.9	7.6	<.5	<1	--	1.4	<1	<10
94JBR070	49.6	848	12.7	8.2	<.5	6	--	.9	<1	<10
94JBR071	64.9	100	11.0	7.9	.7	3	--	.1	<1	<10
94JBR072	51.4	74	15.4	7.8	<.5	3	--	<.1	<1	<10
94JBR074	67.6	137	14.9	10.0	1.1	2	--	.9	<1	<10
94JBR075	23.8	39	22.0	6.5	1.4	2	--	<.1	<1	<10
94JBR076	32.1	35	23.1	9.5	5.9	3	--	.3	<1	<10
94JBR077	30.8	67	23.2	8.9	2.6	1	--	.7	<1	<10
94JBR079	36.7	693	388	19.8	<.5	4	--	2.1	<1	<10
94JBR080	103	511	473	11.0	<.5	1	--	3.2	<1	<10
94JBR081	61.2	8	26.0	11.7	<.5	4	--	.9	<1	<10
94JBR082	51.8	162	88.8	6.3	<.5	11	--	1.4	<1	<10
94ABR006	232	162	120	4.9	<.5	6	--	9.4	3	<10
94BDR060	281	57	30.6	12.7	3.7	30	--	4.1	<1	<10
94JBR044	65.2	37	76.6	10.1	<.5	5	--	.4	<1	<10
94JBR073	28.6	76	30.8	8.8	5.6	2	--	.3	<1	<10
94JBR083	86.0	7	10.6	12.2	.9	1	--	.4	<1	<10
94JHR085	104	74	15.8	11.4	<.5	18	--	2.1	<1	<10
94JHR086	125	11	29.1	6.0	2.2	<1	--	.6	4	<10
94JHR087	692	132	283	15.1	<.5	9	--	3.0	12	<10
94JHR088	179	80	124	6.3	<.5	8	--	1.3	4	<10
94JHR089	116	266	181	6.7	<.5	4	--	1.8	3	<10
94JHR090	5.6	24	1.8	.3	<.5	5	--	.2	<1	<10
94HDR109	43.5	29	7.3	3.4	<.5	7	--	.4	2	<10
94HDR110	299	5	107	7.0	<.5	1	--	.5	6	<10
94HDR111	44.7	81	8.2	1.9	.6	20	--	.8	1	<10
94HDR112	32.7	27	16.6	8.7	.9	4	--	.5	1	<10
94HDR113	48.2	<3	20.7	10.0	.9	3	--	.2	3	<10
94HDR114	65.2	<3	45.0	7.5	<.5	<1	--	.3	3	<10
94HDR115	55.3	12	109	6.8	1.5	<1	--	.1	3	<10
94HDR116	40.4	<3	36.7	4.7	2.4	1	--	.2	2	<10
94HDR117	24.5	10	17.8	3.7	2.3	2	--	.2	2	<10
HDR120	91.9	5	34.7	7.5	.6	2	--	.9	3	<10
IDR121	23.7	26	2.5	1.5	<.5	<1	--	.3	<1	<10
94AGR001	73.3	11	7.3	.9	<.5	5	--	2.7	2	<10
94AGR013	68.4	9	321	4.5	<.5	<1	--	.7	3	<10
D 94AHR006	1650	986	25.6	3.1	<.5	<1	--	13.9	41	<10
94BDR090	41.0	94	76.2	4.5	<.5	17	--	.7	2	<10
94BDR102	52.4	40	9.9	3.7	<.5	4	--	3.9	4	<10
94BDR104	--	--	--	--	--	--	--	--	--	--
D 94BTR025	2620	45	46.4	6.9	<.5	2	--	.8	53	<10
D 94BTR030	--	--	--	--	--	--	--	--	--	--
94BDR026	39.7	43	2.9	7.0	4.2	4	--	.1	<1	<10
94BDR028	--	--	--	--	--	--	--	--	--	--
94BDR045	65.4	28	11.6	4.8	<.5	3	--	1.5	2	<10
D 94BDR047	--	--	--	--	--	--	--	--	--	--
D 94BDR055	67.5	25	31.9	5.9	<.5	5	--	1.3	2	<10
94BDR059	--	--	--	--	--	--	--	--	--	--
94BDR069	89.2	226000	64.2	2.2	<.5	1	--	69.4	14	<10
D 94BDR073	--	--	--	--	--	--	--	--	--	--
D 94BDR082	28.9	229	51.9	10.3	.5	108	--	.4	5	<10
94BDR086	--	--	--	--	--	--	--	--	--	--
94JBR053	47.4	105	147	6.5	<.5	<1	--	.9	3	<10
94JBR057	--	--	--	--	--	--	--	--	--	--
D 94JBR063	86.0	363	22.7	8.6	1.3	<1	--	1.4	5	<10
D 94JBR069	--	--	--	--	--	--	--	--	--	--
94JBR076	33.7	44	23.5	8.1	4.9	<1	--	.2	3	<10
94ABR006	--	--	--	--	--	--	--	--	--	--
D 94JHR086	118	16	27.8	5.7	1.8	<1	--	.6	4	<10
D 94HDR110	--	--	--	--	--	--	--	--	--	--
94HDR116	39.7	5	33.6	4.3	1.6	1	--	.1	2	<10

SAMPLE	SB PPM ICP 5	BA PPM ICP 1	LA PPM ICP 0.5	W PPM ICP 10	PB % XRF 0.01	PB PPM ICP 2	BI PPM ICP 3
94AGR001	<5	80	4.2	<10	--	18	<3
AGR002	<5	30	<.5	<10	--	86	<3
4AGR003	<5	101	11.7	<10	--	9	<3
94AGR004	<5	55	<.5	<10	--	296	132
94AGR005	<5	47	6.5	<10	--	30	<3
94AGR006	<5	52	4.6	<10	--	31	9
94AGR007	<5	67	4.6	<10	--	48	25
94AGR008	<5	27	<.5	<10	--	42	<3
94AGR009	<5	75	7.1	<10	--	578	9
94AGR010	<5	18	<.5	<10	.15	1540	72

BEN ALI

X-RAY ASSAY LABORATORIES 09-Aug-94 REPORT ----- WORKORDER 19204 PAGE 1

SAMPLE	AU-1AT PPB FADCP 1	BE PPM ICP 0.5	NA % ICP 0.01	MG % ICP 0.01	AL % ICP 0.01	P % ICP 0.01	K % ICP 0.01	CA % ICP 0.01	SC PPM ICP 0.5	TI % ICP 0.01
BDS 080	<1	1.1	.04	.99	1.57	.11	.39	.55	3.3	.11
94 BDS 089	9	1.1	.04	1.00	1.54	.12	.41	.57	3.5	.11
94 BDS 092	11	1.2	.04	1.25	1.92	.14	.50	.74	4.5	.14
94 BDS 096	16	1.6	.04	1.19	2.17	.12	.47	.81	4.6	.12
94 BDS 105	117	2.3	.02	1.67	2.25	.13	.10	.29	7.9	.01
94 BDS 107	35	2.1	.02	1.81	2.32	.15	.10	.39	8.9	.04
94 BDS 108	8	1.4	.02	.83	1.26	.08	.14	.37	2.7	.02
94 BDS 118	15	1.9	.02	1.28	2.15	.12	.13	.65	4.9	<.01
94 BDS 119	20	3.3	.02	1.26	3.73	.12	.05	1.30	15.6	.03
94 BTS 01	28	2.0	.04	.98	1.69	.14	.10	1.42	3.8	.02
94 BTS 02	30	2.1	.04	.94	1.68	.15	.10	1.70	3.9	.02
94 BTS 04	26	1.9	.04	1.00	1.60	.11	.10	1.99	3.0	.02
94 BTS 06	33	1.9	.04	.97	1.66	.13	.10	1.41	3.4	.02
94 BTS 09	33	2.0	.04	.97	1.69	.12	.10	1.70	3.6	.02
94 BTS 011	8	1.6	.03	1.06	1.38	.10	.10	.61	2.7	.02
94 BTS 012	25	1.5	.02	.88	1.14	.12	.05	1.38	2.7	<.01
94 BTS 013	55	1.6	.02	.96	1.37	.13	.06	1.43	4.1	<.01
94 BTS 014	14	1.3	.03	.96	1.37	.10	.08	1.31	2.5	.01
94 BTS 015	18	1.4	.01	.98	1.18	.14	.05	1.88	2.5	<.01
94 BTS 016	14	1.3	.02	.88	1.02	.13	.04	2.04	2.1	<.01
94 BTS 018	23	1.5	.02	.90	1.07	.14	.05	2.02	2.5	<.01
94 BTS 019	17	1.2	.02	.79	.90	.13	.03	1.60	1.7	<.01
94 BTS 020	20	1.5	.02	.83	.84	.13	.04	1.42	2.7	<.01
94 BTS 021	27	2.0	.02	1.01	1.23	.16	.06	1.55	3.2	<.01
94 BTS 027	12	1.5	.12	1.41	2.37	.14	.28	1.34	6.7	.08
94 BTS 028	6	1.7	.13	1.48	2.60	.15	.29	1.59	6.8	.08
94 BTS 029	26	1.8	.13	1.49	2.55	.15	.28	1.59	7.2	.08
94 BTS 031	16	1.5	.11	1.23	2.12	.12	.26	1.67	5.7	.07
94 BTS 032	12	1.2	.08	1.15	1.88	.13	.33	1.02	5.4	.13
94 BTS 038	33	1.7	.03	.93	1.68	.09	.21	.78	5.2	.03
94 BTS 039	13	1.4	.03	.52	1.78	.15	.17	1.62	2.1	.01
94 BTS 040	17	1.9	.03	.79	2.11	.14	.12	1.03	3.3	.02
94 BTS 041	30	1.3	.03	.69	1.45	.12	.09	1.02	3.8	.01
94 BTS 042	15	1.3	.03	1.07	1.91	.11	.22	.70	5.7	.03
BTS 043	33	1.7	.05	1.21	2.35	.10	.20	.84	6.1	.06
4 BTS 044	34	1.7	.05	1.04	1.89	.09	.22	.71	4.9	.03
94 BTS 045	6	1.0	.03	.62	1.03	.09	.16	.71	2.7	.09
94 BTS 046	19	1.5	.03	.33	1.22	.07	.10	1.12	1.1	.02
94 BTS 047	9	1.4	.03	.98	1.40	.08	.10	.35	2.5	.02
94 BTS 048	7	1.1	.03	.22	.84	.03	.07	.37	.8	.02
94 BTS 049	4	1.5	.02	.22	.93	.04	.12	.32	1.2	<.01
94 BTS 050	21	1.6	.03	.95	1.50	.10	.15	.40	5.1	.01
94 ABS 001	32	2.2	.04	2.08	2.90	.14	.32	.61	13.1	.06
94 ABS 002	12	1.3	.02	.77	1.66	.08	.14	.15	3.8	.04
94 ABS 003	15	1.3	.02	.57	1.56	.07	.11	.17	2.6	.02
94 ABS 004	31	1.6	.04	1.28	2.02	.12	.19	.47	7.0	.03
94 ABS 005	19	1.6	.03	1.21	1.83	.11	.16	.45	6.1	.03
94 TGS 001	555	1.4	.04	.93	1.72	.10	.14	.66	3.3	.04
94 TGS 002	NSS	1.2	.04	.82	1.61	.10	.14	.63	2.5	.04
94 TGS 003	132	1.1	.03	.74	1.67	.09	.14	.64	2.3	.04
94 TGS 004	1160	2.2	.02	.25	3.34	.06	.06	.38	1.7	.05
94 TGS 005	75	1.4	.03	1.17	1.81	.11	.11	.49	3.7	.04
L10+00N 3+00E	605	1.6	.03	.44	1.81	.07	.19	.52	2.0	.02
L10+00N 3+25E	61	2.5	.03	.58	3.30	.13	.08	.76	3.7	.03
L10+00N 3+50E	482	2.2	.03	.70	2.54	.13	.10	.83	3.7	.02
L10+00N 3+75E	292	2.2	.02	.47	2.75	.07	.05	.12	3.1	.07
L10+00N 4+00E	174	2.3	.02	.57	4.26	.05	.07	.61	4.9	.09
L10+00N 4+25E	133	3.9	.04	.59	4.76	.12	.15	1.51	5.5	.09
L10+00N 4+50E	14	2.0	.02	.19	3.44	.06	.04	.19	2.0	.02
L10+00N 4+75E	11	2.3	.02	.06	2.86	.02	.02	<.01	.5	.12
L10+00N 5+00E	14	<.5	.02	.01	.30	.01	.03	.03	<.5	<.01
L10+00N 5+25E	14	1.9	.02	.10	2.14	.03	.02	.03	1.0	.06
L10+00N 5+50E	10	2.4	.03	.63	2.28	.10	.07	1.20	3.0	.02
L10+00N 5+75E	126	1.7	.03	.41	1.97	.06	.08	.33	3.3	.03
L10+00N 6+00E	21	1.5	.03	.05	2.67	.04	.02	.85	1.7	.03
L10+00N 6+25E	63	2.5	.03	.50	3.21	.07	.04	.86	4.9	.09
L10+00N 6+50E	5	1.5	.01	.10	3.84	.04	.02	.05	2.8	.05
L10+00N 6+75E	11	<.5	.02	.10	.79	.04	.05	.33	.7	.03
L10+00N 7+00E	5	1.2	.03	.25	2.38	.03	.02	.10	.9	.22
L10+00N 7+25E	17	4.2	.02	.11	6.44	.06	.04	2.47	4.5	.02
L10+00N 7+50E	851	2.0	.01	.81	2.01	.11	.05	.40	2.9	.02
L10+00N 7+75E	196	1.7	.03	.49	2.77	.04	.07	.04	2.2	<.01
L10+00N 8+00E	79	2.4	.03	.81	2.41	.09	.14	.53	4.4	.02
L10+00N 8+25E	175	2.9	.04	.72	3.48	.13	.05	.85	4.7	.03
L10+00N 8+50E	82	1.9	.03	.50	2.43	.06	.04	.16	2.7	.03
L10+00N 8+75E	108	2.2	.03	.42	3.29	.05	.06	1.22	3.5	.04
L10+00N 9+00E	11	1.6	.04	.91	3.56	.04	.05	.13	9.5	.26
L10+00N 9+25E	161	1.9	.04	.82	2.36	.14	.10	1.14	3.5	.03
L10+00N 9+50E	16	1.4	07	.40	1.91	.12	03	1.11	1.3	.01

52

BEN ALI

X-RAY ASSAY LABORAug-94 REPORT ----- WORKORDER 19204 PAGE 4

SAMPLE	CR PPM ICP 1	MN PPM ICP 2.00	FE % ICP 0.01	CO PPM ICP 1	NI PPM ICP 1	CU PPM ICP 0.5	ZN PPM ICP 0.5	AS PPM ICP 3	SR PPM ICP 0.5
94 BTS 047	33	549	2.80	9	18	48.8	193	12	21.9
94 BTS 048	28	589	1.29	5	5	59.0	75.1	6	23.9
94 BTS 049	16	1330	1.56	4	<1	20.7	43.3	6	20.9
94 BTS 050	39	1570	4.09	17	20	88.2	219	169	25.7
94 ABS 001	89	2150	5.37	29	40	106	191	79	46.6
94 ABS 002	26	1210	3.44	16	15	56.5	112	28	9.8
94 ABS 003	19	1470	3.12	16	9	49.1	83.5	17	16.9
94 ABS 004	51	1510	4.04	18	25	82.2	171	53	30.3
94 ABS 005	48	1210	3.64	14	21	69.4	145	45	31.5
94 TGS 001	36	1270	3.50	14	28	63.9	861	834	44.2
94 TGS 002	40	1260	3.06	13	20	38.1	518	409	36.1
94 TGS 003	32	1220	2.72	11	22	39.9	630	346	42.2
94 TGS 004	10	3170	4.05	22	<1	2160	3500	6	23.2
94 TGS 005	45	1960	3.73	18	20	75.8	376	160	26.5
L10+00N 3+00E	20	1420	3.62	75	2	239	1530	49	25.9
L10+00N 3+25E	27	3140	3.40	57	24	68.1	748	435	48.6
L10+00N 3+50E	26	4280	5.16	33	45	160	1710	1280	40.8
L10+00N 3+75E	31	736	5.38	10	10	46.1	201	521	10.8
L10+00N 4+00E	26	530	6.20	8	<1	40.0	200	262	27.3
L10+00N 4+25E	7	3600	7.47	81	7	148	571	127	80.2
L10+00N 4+50E	8	543	2.55	9	2	18.6	95.5	17	9.0
L10+00N 4+75E	12	53.0	6.45	2	<1	16.4	29.3	13	.8
L10+00N 5+00E	<1	13.0	.23	<1	<1	2.1	5.1	<3	1.9
L10+00N 5+25E	16	86.0	6.84	3	<1	23.3	61.1	93	3.1
L10+00N 5+50E	23	2330	6.50	19	9	33.9	116	83	44.3
L10+00N 5+75E	22	398	3.83	10	9	48.7	266	308	26.6
L10+00N 6+00E	8	182	3.04	6	1	10.4	136	18	29.9
L10+00N 6+25E	23	564	6.67	9	8	30.1	253	410	49.6
L10+00N 6+50E	14	135	4.21	3	2	11.3	32.4	18	2.7
L10+00N 6+75E	1	153	.59	<1	<1	1.1	11.8	5	20.8
L10+00N 7+00E	17	117	3.16	3	<1	1.1	20.9	<3	27.4
L10+00N 7+25E	12	1200	3.71	44	17	35.4	147	93	93.5
L10+00N 7+50E	22	933	4.51	10	6	38.6	175	931	41.0
L10+00N 7+75E	11	1360	5.22	9	<1	37.6	363	52	2.3
L10+00N 8+00E	31	2070	6.43	22	13	82.5	259	446	26.0
L10+00N 8+25E	44	2340	5.80	40	45	101	630	698	47.3
L10+00N 8+50E	41	271	5.48	7	7	47.2	135	477	16.0
L10+00N 8+75E	37	278	6.01	8	18	57.8	260	317	48.0
L10+00N 9+00E	33	218	4.87	6	3	18.8	45.9	251	8.1
L10+00N 9+25E	36	2970	4.92	28	59	107	1090	800	69.5
L10+00N 9+50E	19	2070	4.32	23	122	118	204	39	54.5
L10+00N 9+75E	43	2730	4.84	23	63	150	2420	1640	45.3
L10+00N 10+00E	37	4370	7.67	46	168	306	1360	375	67.6
L27+00S 17+50W	9	89.0	1.27	5	5	28.2	29.3	8	2.5
L27+00S 17&75W	28	171	6.02	5	5	23.8	43.7	19	2.3
L27+00S 18+00W	28	680	5.83	9	8	43.2	81.0	59	1.9
L27+00S 18+25W	54	447	5.46	10	11	42.1	46.9	47	8.5
L27+00S 18+50W	25	926	3.60	12	4	41.2	37.3	17	3.0
L27+00S 18+75W	22	427	5.15	4	2	24.3	24.2	21	3.0
L27+00S 19+00W	8	54.0	.83	3	<1	8.2	11.4	10	2.1
L27+00S 19+25W	23	430	3.74	6	5	26.5	23.5	10	6.2
L27+00S 19+50W	74	430	6.84	11	20	72.7	60.5	172	8.3
L27+00S 19&75W	45	2460	6.60	24	12	162	1560	350	7.4
L27+00S 20+25W	165	23900	3.44	108	343	192	1590	22	43.9
L27+00S 20+50W	20	609	4.51	7	8	22.8	53.7	16	3.0
L27+00S 20+75W	38	481	4.73	12	13	42.7	129	48	2.2
L27+00S 21+00W	34	635	4.60	12	23	57.4	42.0	35	5.7
L27+00S 21+25W	35	267	4.51	8	6	51.7	50.2	17	7.2
L27+00S 21+50W	34	150	3.86	9	11	62.3	32.3	84	7.0
L27+00S 21+75W	25	365	4.03	11	6	45.9	38.7	14	3.4
L27+00S 22+00W	45	342	6.67	10	5	61.4	61.2	388	5.9
L27+00S 22+25W	85	629	8.29	28	10	112	51.3	78	7.6
L27+00S 22+50W	27	81.0	3.66	9	7	46.0	41.7	12	10.0
L28+00S 17+50W	39	1570	6.81	16	9	43.7	66.3	22	3.7
L28+00S 17+75W	28	353	7.60	7	6	38.9	46.6	34	1.6
L28+00S 18+00W	20	208	5.79	5	2	28.1	23.5	27	2.2
L28+00S 18+25W	33	368	5.20	8	18	38.3	58.4	23	2.1
L28+00S 18+50W	26	1010	5.[illegible]0	8	<1	17.1	21.4	13	3.3
L28+0[illegible] [illegible]+75W	31	218	3.26	5	11	21.1	26.1	16	6.2
L28+[illegible] [illegible]+00W	13	53.0	1.37	4	3	12.0	15.3	19	3.1
L28+00S 19+25W	27	486	4.75	9	8	58.9	85.0	41	7.0
L26+00S 19+50W	72	2080	4.45	37	28	104	215	69	6.8
L28+00S 19+75W	46	2240	5.80	16	7	55.6	61.8	32	2.9
L28+00S 20+25W	7	91.0	1.36	6	2	14.4	22.3	24	2.4
L28+00S 20+50W	22	4900	1.11	10	135	112	815	9	115
L28+00S 20+75W	42	17400	3.75	20	470	313	3180	19	41.4
L28+00S 21+00W	29	185	4.20	5	12	29.2	41.0	34	3.7
L28+00S 2+25W	16	261	2.81	5	8	23.1	132	98	5.0
L28+00S 21+50W	52	179	1.99	6	6	10.3	17.4	<3	10.2
L28+00S 21+75W	8	69.0	1.10	4	<1	21.5	52.9	15	8.8

BEN ALI

SAMPLE	PB PPM ICP 2	BI PPM ICP 3
94 BTS 047	16	<3
[illegible] BTS 048	9	<3
94 BTS 049	9	<3
94 BTS 050	58	<3
94 ABS 001	43	<3
94 ABS 002	30	<3
94 ABS 003	21	<3
94 ABS 004	31	<3
94 ABS 005	25	<3
94 TGS 001	430	<3
94 TGS 002	220	<3
94 TGS 003	200	<3
94 TGS 004	488	<3
94 TGS 006	130	<3
L10+00N 3+00E	746	6
L10+00N 3+25E	341	<3
L10+00N 3+50E	817	<3
L10+00N 3+75E	149	<3
L10+00N 4+00E	54	<3
L10+00N 4+25E	114	<3
L10+00N 4+50E	59	<3
L10+00N 4+75E	12	<3
L10+00N 5+00E	4	<3
L10+00N 5+25E	27	<3
L10+00N 5+50E	30	<3
L10+00N 5+75E	227	<3
L10+00N 6+00E	12	<3
L10+00N 6+25E	152	<3
L10+00N 6+50E	<2	<3
L10+00N 6+75E	14	<3
L10+00N 7+00E	11	<3
L10+00N 7+25E	126	<3
L10+00N 7+50E	213	<3
L10+00N 7+75E	386	<3
L10+00N 8+00E	215	<3
0+00N 8+25E	539	<3
0+00N 8+50E	176	4
L10+00N 8+75E	133	4
L10+00N 9+00E	34	5
L10+00N 9+25E	664	<3
L10+00N 9+50E	55	<3
L10+00N 9+75E	1440	<3
L10+00N 10+00E	463	<3
L27+00S 17+50W	6	<3
L27+00S 17&75W	30	<3
L27+00S 18+00W	59	<3
L27+00S 18+25W	37	<3
L27+00S 18+50W	17	<3
L27+00S 18+75W	30	<3
L27+00S 19+00W	<2	<3
L27+00S 19+25W	23	<3
L27+00S 19+50W	46	9
L27+00S 19&75W	3570	<3
L27+00S 20+25W	48	<3
L27+00S 20+50W	16	4
L27+00S 20+75W	62	<3
L27+00S 21+00W	20	<3
L27+00S 21+25W	8	5
L27+00S 21+50W	12	<3
L27+00S 21+75W	16	<3
L27+00S 22+00W	24	6
L27+00S 22+25W	90	11
L27+00S 22+50W	20	<3
L28+00S 17+50W	38	<3
L28+00S 17+75W	34	<3
L28+00S 18+00W	16	5
L28+00S 18+25W	20	<3
L28+00S 18+50W	19	<3
L28+00S 18+75W	22	<3
L28+00S 19+00W	21	<3
8+00S 19+25W	34	<3
8+00S 19+50W	88	<3
L28+00S 19+75W	29	<3
L28+00S 20+25W	10	<3
L28+00S 20+50W	14	<3
L28+00S 20+75W	30	<3
L28+00S 21+00W	28	<3
L28+00S 2+25W	23	<3
L28+00S 21+50W	9	<3
L28+00S 21+75W	18	<3

14

BEN ALI

SAMPLE	Y PPM ICP 0.1	ZR PPM ICP 0.5	MO PPM ICP 1	AG PPM ICP 0.1	CD PPM ICP 1	SN PPM ICP 10	SB PPM ICP 5	BA PPM ICP 1	LA PPM ICP 0.5	W PPM ICP 10
94 BDS 088	3.3	<.5	<1	<.1	<1	<10	<5	125	5.7	<10
94 BDS 089	3.5	<.5	3	.7	<1	<10	<5	124	6.3	<10
94 BDS 092	3.7	<.5	3	<.1	<1	<10	<5	131	6.5	<10
94 BDS 096	5.1	<.5	2	.1	<1	<10	<5	144	8.8	<10
94 BDS 105	8.5	<.5	7	1.4	<1	<10	<5	77	8.5	<10
94 BDS 107	7.6	<.5	3	<.1	<1	<10	<5	66	8.7	<10
94 BDS 108	4.8	<.5	2	<.1	<1	<10	<5	72	10.2	<10
94 BDS 118	12.5	<.5	8	<.1	3	<10	<5	61	12.0	<10
94 BDS 119	38.2	<.5	8	.4	3	<10	<5	61	21.3	<10
94 BTS 01	12.2	<.5	4	.9	<1	<10	<5	166	7.0	<10
94 BTS 02	13.4	<.5	6	1.5	<1	<10	<5	174	8.3	<10
94 BTS 04	9.3	<.5	7	<.1	<1	<10	<5	141	5.7	<10
94 BTS 06	11.8	<.5	3	1.1	<1	<10	<5	150	6.3	<10
94 BTS 09	12.3	<.5	4	1.1	<1	<10	<5	167	6.5	<10
94 BTS 011	9.1	<.5	6	.6	<1	<10	<5	55	7.8	<10
94 BTS 012	10.2	<.5	13	1.1	3	<10	<5	90	4.8	<10
94 BTS 013	13.5	<.5	14	.9	4	<10	6	108	9.1	<10
94 BTS 014	7.9	<.5	5	<.1	<1	<10	<5	101	6.1	<10
94 BTS 015	10.6	<.5	11	<.1	4	<10	<5	84	6.0	<10
94 BTS 016	9.6	<.5	12	.2	4	<10	<5	77	5.4	<10
94 BTS 018	10.7	<.5	13	1.2	5	<10	<5	93	5.7	<10
94 BTS 019	9.3	<.5	10	.3	3	<10	<5	72	2.8	<10
94 BTS 020	12.3	<.5	28	1.3	6	<10	<5	102	5.6	<10
94 BTS 021	15.4	<.5	25	2.6	10	<10	8	78	11.5	<10
94 BTS 027	6.4	<.5	6	<.1	3	<10	<5	135	4.2	<10
94 BTS 028	7.5	<.5	7	1.1	3	<10	<5	139	4.7	<10
94 BTS 029	7.3	<.5	5	.2	3	<10	<5	142	4.3	<10
94 BTS 031	5.9	<.5	5	<.1	1	<10	<5	121	3.2	<10
94 BTS 032	5.1	<.5	1	<.1	<1	<10	<5	117	6.1	<10
94 BTS 038	9.8	<.5	9	.1	<1	<10	<5	104	5.6	<10
94 BTS 039	11.7	<.5	14	.7	<1	<10	<5	108	7.8	<10
94 BTS 040	17.0	<.5	11	.7	10	<10	<5	111	17.6	<10
94 BTS 041	8.6	<.5	9	.9	2	<10	<5	152	6.6	<10
94 BTS 042	7.3	<.5	4	<.1	<1	<10	<5	96	6.8	<10
94 BTS 043	7.1	<.5	2	<.1	1	<10	<5	113	6.4	<10
94 BTS 044	5.7	<.5	3	<.1	<1	<10	<5	88	6.8	<10
94 BTS 045	3.7	<.5	2	<.1	<1	<10	<5	72	7.6	<10
94 BTS 046	7.0	<.5	4	<.1	<1	<10	<5	77	13.3	<10
94 BTS 047	5.9	<.5	4	<.1	<1	<10	<5	69	6.6	<10
94 BTS 048	6.0	<.5	6	.4	<1	<10	<5	61	8.0	<10
94 BTS 049	7.8	<.5	15	<.1	<1	<10	<5	93	13.3	<10
94 BTS 050	6.6	<.5	6	<.1	<1	<10	<5	97	8.2	<10
94 ABS 001	7.8	<.5	2	.2	<1	<10	<5	120	6.4	<10
94 ABS 002	4.6	<.5	2	<.1	<1	<10	<5	87	6.7	<10
94 ABS 003	5.1	<.5	<1	<.1	<1	<10	<5	124	9.0	<10
94 ABS 004	6.3	<.5	<1	<.1	<1	<10	<5	99	8.6	<10
94 ABS 005	5.4	<.5	6	.7	<1	<10	<5	90	7.7	<10
94 TGS 001	6.1	<.5	6	1.3	5	<10	<5	233	7.1	<10
94 TGS 002	5.7	<.5	4	.8	1	<10	<5	107	7.2	<10
94 TGS 003	5.1	<.5	4	<.1	3	<10	<5	175	6.3	<10
94 TGS 004	5.6	<.5	21	13.4	57	<10	<5	120	10.1	<10
94 TGS 005	6.5	<.5	6	.1	1	<10	7	131	8.1	<10
L10+00N 3+00E	6.0	<.5	20	10.6	10	<10	<5	94	7.6	<10
L10+00N 3+25E	13.8	<.5	4	1.6	6	<10	<5	250	11.9	<10
L10+00N 3+50E	13.3	<.5	14	3.6	13	<10	<5	143	11.8	<10
L10+00N 3+75E	4.6	<.5	12	.6	<1	<10	<5	67	6.3	<10
L10+00N 4+00E	4.8	5.8	15	.3	<1	<10	<5	53	5.3	<10
L10+00N 4+25E	16.0	<.5	19	1.3	<1	<10	<5	211	10.9	<10
L10+00N 4+50E	8.4	2.5	2	.7	<1	<10	<5	83	8.9	<10
L10+00N 4+75E	1.4	4.7	30	<.1	<1	<10	<5	41	7.2	<10
L10+00N 5+00E	.6	<.5	<1	<.1	<1	<10	<5	10	3.8	<10
L10+00N 5+25E	2.3	<.5	9	.6	<1	<10	<5	36	6.9	<10
L10+00N 5+50E	7.0	<.5	14	1.0	<1	<10	<5	477	7.7	<10
L10+00N 5+75E	6.6	<.5	9	1.5	<1	<10	<5	98	9.6	<10
L10+00N 6+00E	4.5	<.5	5	<.1	<1	<10	<5	227	5.7	<10
L10+00N 6+25E	7.3	<.5	6	<.1	<1	<10	<5	115	6.9	<10
L10+00N 6+50E	1.1	7.5	<1	<.1	<1	<10	<5	61	7.1	<10
L10+00N 6+75E	.8	<.5	2	<.1	<1	<10	<5	26	3.5	<10
L10+00N 7+00E	1.0	<.5	<1	<.1	<1	<10	<5	53	3.0	<10
L10+00N 7+25E	17.8	<.5	<1	<.1	1	<10	<5	140	12.6	<10
L10+00N 7+50E	3.5	<.5	8	<.1	<1	<10	<5	80	10.1	<10
L10+00N 7+75E	5.8	.9	21	2.3	<1	<10	8	70	17.6	<10
L10+00N 8+00E	16.8	<.5	11	2.9	<1	<10	11	73	15.5	<10
L10+00N 8+25E	10.4	<.5	13	5.4	<1	<10	10	68	10.0	<10
L10+00N 8+50E	4.6	<.5	17	2.4	<1	<10	11	55	6.8	<10
L10+00N 8+75E	6.3	<.5	12	2.9	<1	<10	10	64	8.0	<10
L10+00N 9+00E	4.2	<.5	7	1.5	<1	<10	9	49	2.9	<10
L10+00N 9+25E	9.9	<.5	11	4.5	7	<10	11	118	9.4	<10
L10+00N 9+50E	9.8	<.5	3	1.7	<1	<10	7	13	1.7	<10
L10+00N 9+75E	10.4	<.5	12	6.7	23	<10	13	129	11.4	<10

BEN ALI