GEOLOGICAL, GEOCHEMICAL AND GEOPHYSICAL

REPORT ON THE KING PROPERTY

Northern Vancouver Island, British Columbia

Nanaimo Mining Division

N.T.S. MAP 92L/13E

Lat. 50° 47' Long. 127° 43'

for

Westward Exploration Ltd.
700, 555 West Hastings Street,
Vancouver, B.C.
V6B 4N5

by

D.G.F. Leighton, P. Geo.

December 18, 1995

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KING PROPERTY

SUMMARY AND RECOMMENDATIONS

1. The King Property is a gold prospect on northern Vancouver Island. It consists of thirty six contiguous claims (56 units) controlled by Westward Exploration Ltd. The claims are west of Georgie Lake and southeast of Shushartie River, approximately 20 kilometres northwest of Port Hardy.

2. The Property is underlain almost entirely by Triassic age Karmutsen Formation rocks. This is a thick pile of tholeiitic basalt, homogeneous basic sheet flows, that has been tilted by block faulting but otherwise little altered.

3. Work carried out on the Property after it was identified as an important gold prospect involved geological prospecting, rock chip and geochemical sampling, the most recent of which was completed during the winter of 1993. Notable findings include the discovery of widespread quartz veining and exceptional gold values in soils.

4. A subsequent program which comprised grid controlled geochemical sampling, chip sampling, magnetic/VLF-EM surveys, and geological mapping was completed near the end of the 1995 field season. This helicopter supported effort, which focused on a specific area north of Lake of the Mountains, was completed by a five man team working out of a tent camp.

5. The 1995 work was successful. Specific targets were identified and a staged follow-up program is recommended. In its first phase, this should consist of back-hoe trenching. Trenching can be guided by the results obtained to date: namely; coincident anomalies, geophysical targets, and linear structural elements. Drilling, stage II, would be contingent upon trench sampling results.

6. Such a program will become practical when new logging roads, presently planned and under construction, extend closer to the area of interest. Based on projections, this is likely by the fall of 1996. Costs for the two stages are estimated at $65,000 and $75,000 respectively.

INTRODUCTION

This report describes the results of mapping, geophysical work, geochemical sampling and trenching carried out during the 1995 field season on the King Property, a gold prospect located on northern Vancouver Island. Work was done by Kamaka Resources Ltd. at the request of Mr. John Pallot, President of Westward Exploration Ltd. ("Westward").

The King claim group is controlled by Westward. It was acquired from Consolidated T.C. Resources Ltd. (now Cyclone Capital Corp.) in February, 1993. Westward is earning its 50% interest by spending $200,000 on property development.

The current phase of work was designed to investigate an area containing previously identified gold anomalies. For the program a camp was set up near a small pond northeast of Lake of The Mountains which is referred to as Camp Lake. An old grid, the baseline of which runs E-W through the camp site, was expanded by adding cross lines which were used as the primary ground control.

The program was successful. Identification of concomitant geophysical-geochemical anomalies and strong linear features has served to re-focus attention on specific targets, targets that can now be tested by trenching.

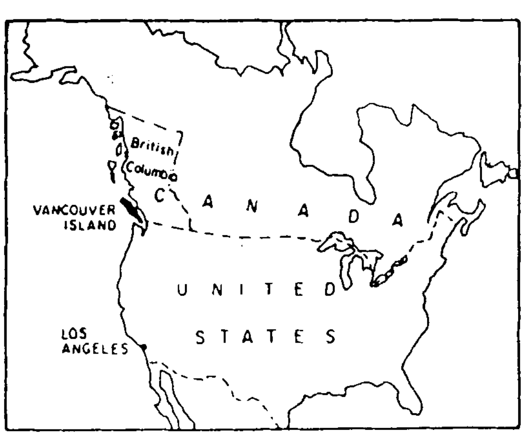
LOCATION, ACCESS AND PHYSIOGRAPHY

The King Property is west of Georgie Lake on northern Vancouver Island. Coordinates are 50° 47' N, 127° 43' W and the applicable topographic map-sheet is 92L/13E.

The eastern edge of the claim block is accessed by a good logging road which runs north from the Port Hardy-Holberg road, approximately 7 km. This road follows the south side of Georgie Lake and enters the Property at the west end of Georgie Lake. It then continues through logged forest land on the eastern portion of the claims and terminates near Shushartie River in the vicinity of the King 25 claim. Much of the eastern sector of the Property has been disrupted by logging activity to the extent that some creeks shown on maps no longer exist.

Access to the western portion of the claim block is by foot, helicopter or float plane into Lake of the Mountains.

Terrain is varied but typical of Vancouver Island; elevations are moderate. The area in the vicinity of Camp Lake, site of the 1995 program, is marshy and plateau like with open forests: cedar and yew predominate. Other parts of the property which haven't been logged support stands of fir and hemlock.



WESTWARD EXPLORATION LTD.

KING PROJECT

NANAIMO MINING DIVISION, B.C.

LOCATION MAP

KAMAKA RESOURCES LTD

SCALE	DATE	FIG.
1: 8,000,000	Feb 1993	1

HISTORY

A 1972 map shows one group of claims west of Lake of the Mountains. It belonged to Imperial Oil but no work was reported and the property lapsed the following year. There is an aeromagnetic anomaly within the area covered by the old claims.

In 1990, Consolidated T.C. Resources Ltd. (now Cyclone Capital Corp.) was active in the region. At that time, the only recorded work in the area was the moss mat sampling by the B.C. Government (1989) and the Government aeromagnetic survey (1962).

Consolidated T.C. Resources carried out a program covering the entire King claim block which consisted of reconnaissance prospecting and panning of several creeks for heavy metals. Some preliminary mapping and sampling was also completed. During April 1991 an attempt was made to clarify geology in the northwestern sector of the block. As well, a prospecting program on ground to the west was continued onto the King claims. This work was hampered by a late snowfall and excess water in the creeks.

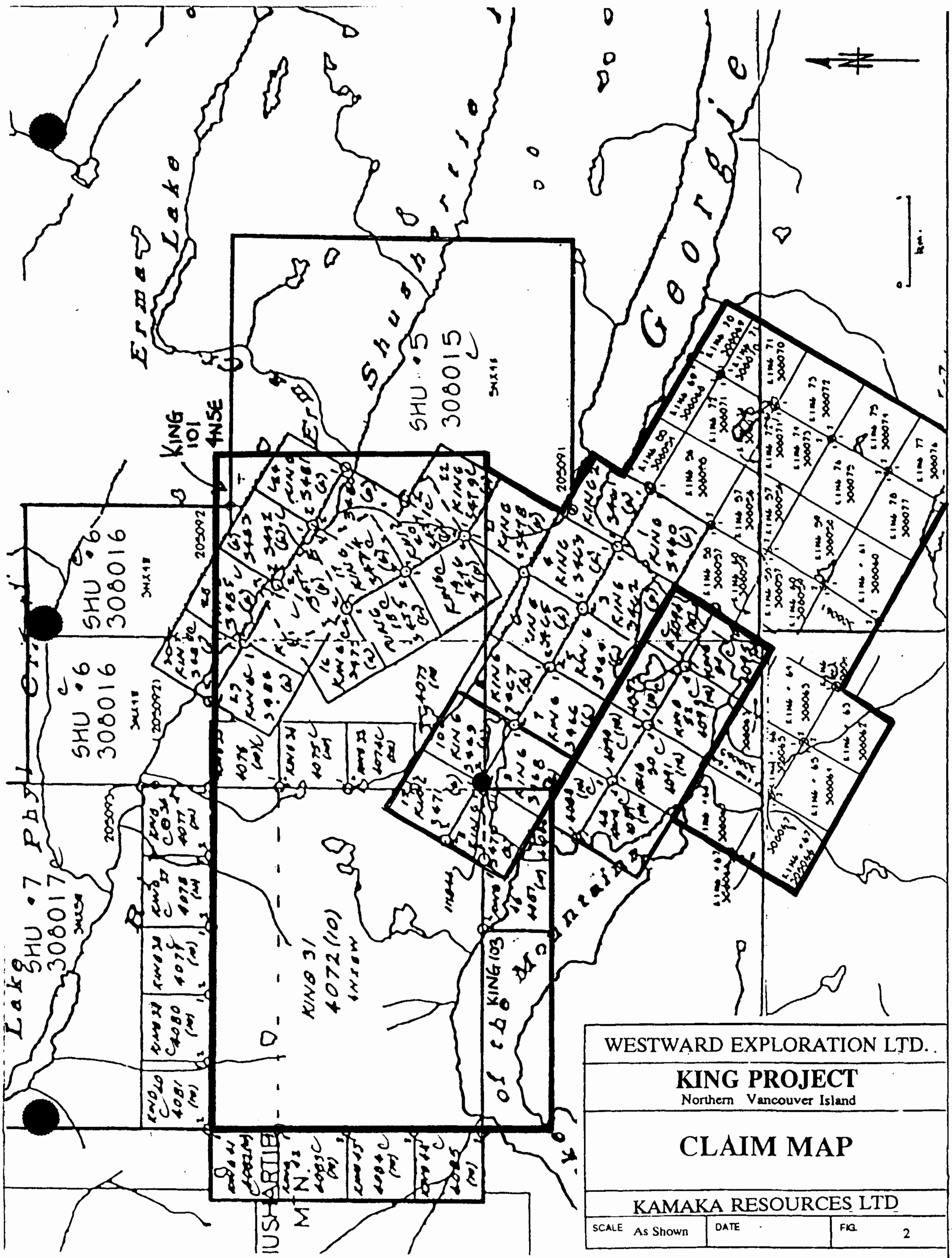
In February 1993, Westward optioned the Property and completed a mapping and detailed soil sampling program. Current work was designed to compliment these surveys.

PROPERTY AND CLAIM STATUS

The King Property is comprised of one contiguous block: 2-post and modified grid claims held by Westward Exploration Ltd. Claims have varying record dates reflecting different staking periods. The following listing provides pertinent data:

Claim	Tenure No.	Units	Expiry	Recorded Owners[1]
King 1-4	230645-48	4	20 Jun. 1997	Daiwan Engineering Ltd.
King 5-11	230649-55	7	21 Jun. 1996	Daiwan Engineering Ltd.
King 12	~~629405~~ 337043	~~7~~ 1	28 Jun. 1996	Daiwan Engineering Ltd.
King 31	231255	20	21 Oct. 1996	Daiwan Engineering Ltd.
King 55-64	308054-63	10	6 Mar. 1995	Daiwan Engineering Ltd.
King 65-68	308064-68	4	7 Mar. 1995	Daiwan Engineering Ltd.
King 69-78	308069-77	10	13 Mar. 1995	Daiwan Engineering Ltd.
King 101/2	111851-52	40	28 Jun. 1996	Daiwan Engineering Ltd.
King 103	341379	20	28 Oct. 1996	P.G. Dasler

[1] The King Property claims are held in trust by Daiwan Engineering and Peter G. Dasler (in trust) for Westward Exploration Ltd. and Consolidated T. C. Resources Ltd.



WESTWARD EXPLORATION LTD.

KING PROJECT
Northern Vancouver Island

CLAIM MAP

KAMAKA RESOURCES LTD

SCALE As Shown	DATE	FIG. 2

REGIONAL GEOLOGY

Vancouver Island north of Holberg and Rupert Inlets is underlain by rocks of the Vancouver Group, a mainly volcanic sequence which ranges from upper Triassic to Lower Jurassic age. These formations are intruded by Jurassic and Tertiary age plutons and disconformably overlain by Cretaceous sedimentary rocks.

Faulting is prevalent in the region. Large-scale block faults with hundreds to thousands of metres of displacement are offset by younger strike-slip faults with displacements up to 750 metres.

The Vancouver Group is described as follows:

- Basal Sediment - Sill Unit: Middle and Upper Triassic Age

The basal sediment-sill unit consists of laminated to graded-bedded black shales and siltstones, silicified and invaded by diabase sills. The entire unit is estimated as 750-900 metres with the sedimentary portion being about 180 metres thick.

- Karmutsen Formation: Upper Triassic Age

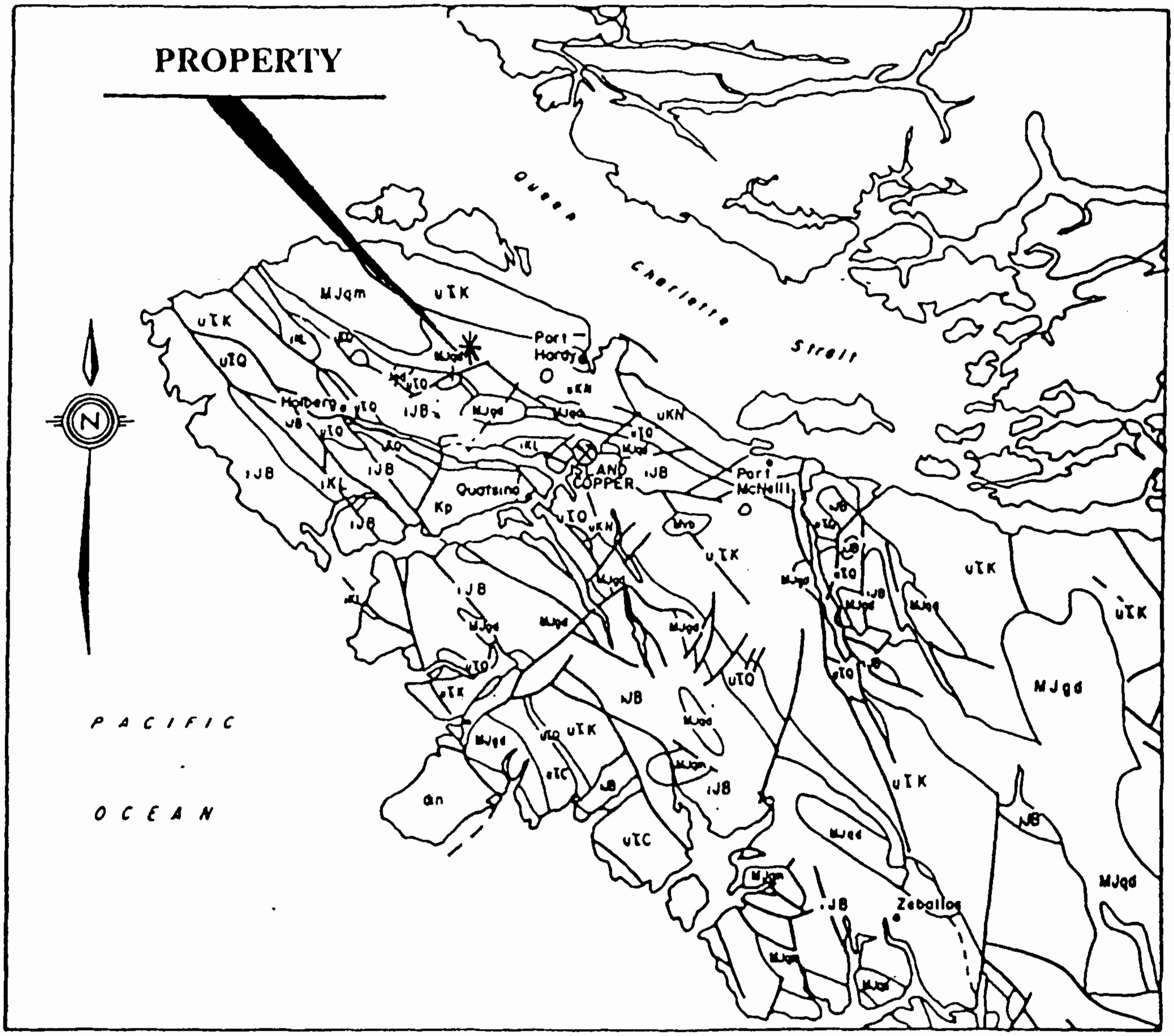
Karmutsen Formation consists of 3,000-6,000 metres of volcanic flows, pyroclastics and minor sediments. It includes three distinct members: a lower pillow lava unit, a middle pillow breccia unit, and an upper lava flow unit. The latter consists of predominantly porphyritic and amygdaloidal basalt flows with individual layers from 1-30 metres thick.

Two bands of limestone occur near the top of the Karmutsen Formation. The distribution of limestone outcrops is erratic however which suggests a series of lenses at the same general stratigraphic horizon rather than one continuous bed.

The lower contact of the Karmutsen Formation has not been observed on the northern part of Vancouver Island. The upper contact with limestone of the Quatsino Formation generally is sharp and easily recognized, although limestone and basalt locally are interbedded over a narrow stratigraphic interval.

Low-grade metamorphism of the Karmutsen has resulted in chloritization and amygdules filled with epidote, carbonate, zeolite, prehnite, chlorite, and quartz.

Basaltic rocks along contacts with intrusive stocks are in many places converted to dark-colored hornblende hornfels. Skarn zones occur sporadically along these contacts, both in the inter-lava limestone and in the basalt.



LEGEND

MIOCENE

- Mvb basalt flows, sills and dykes

UPPER CRETACEOUS, PALEOCENE, EOCENE

- Kp QUEEN CHARLOTTE GROUP: siltstone, shale, greywacke

UPPER CRETACEOUS

- uKN NANAIMO GROUP: sandstone, shale, conglomerate

LOWER CRETACEOUS

- lKL LONGARM; greywacke, conglomerate

JURASSIC

- Jgd granodiorite, quartz diorite

MIDDLE JURASSIC

- MJqm quartz monzonite, granite, monzonite
- MJgd granodiorite
- MJqd quartz diorite

LOWER JURASSIC

- lJB BONANZA; andesite, dacite, rhyolite

UPPER TRIASSIC

- uTQ QUATSINO and PARSON BAY: limestone, argillite
- uTK KARMUTSEN: basalt, pillow lava

SCALE

0 25 50

kilometers

WESTWARD EXPLORATION LTD.		
KING PROJECT Northern Vancouver Island		
REGIONAL GEOLOGY		
KAMAKA RESOURCES LTD		
SCALE As Shown	DATE	FIG. 3

- Quatsino Formation: Upper Triassic Age

The Quatsino Formation ranges from 60-1,000 metres in thickness and consists of limestone with a few thin andesite or basalt flows. It has conformable contacts with both overlying Parson Bay Formation sediments and underlying Karmutsen volcanics. The upper contact with Parson Bay rocks is gradational with limestone grading upward into carbonaceous argillites.

Within the contact metamorphic/metasomatic aureoles adjacent to intrusive stocks, skarn development and silicification of limestone, accompanied by chalcopyrite-magnetite or galena, sphalerite and silver mineralization has been noted.

- Parson Bay Formation: Upper Triassic Age

The Parson Bay Formation consists of between 60-360 metres of argillite, minor limestone, agglomeratic and tuffaceous limestone, tuff, quartzite and minor conglomerate. At both its base and top, the unit exhibits gradational contacts with the Quatsino and Harbledown Formations.

On a regional scale, rocks are unmetamorphosed. Locally, adjacent to intrusive contacts, pyrite-magnetite replacement bands up to one-half inch thick in banded tuffs have been observed.

- Harbledown Formation: Lower Jurassic Age

The Harbledown Formation, about 500 metres thick, consists of a non-volcanic argillite-greywacke sequence separating the Parson Bay from the Bonanza Formation.

- Bonanza Formation: Lower Jurassic Age

The Bonanza Formation is approximately 1,500 metres thick. The lower portion consists of bedded and massive tuffs, intraformational breccias and rare amygdaloidal and porphyritic flows, in the compositional range andesite to basalt. Porphyritic dikes and sills intrude the lower part of the unit. In the upper part of the Bonanza, rhyodacite flows and breccias become more numerous and are interbedded with andesite and basalt flows, tuffs and tuff breccias.

Regional metamorphism within the Bonanza is low grade. Plagioclase commonly is albitized and saussuritized. Chlorite, epidote and laumontite occur within the matrix of volcanic breccias, in veinlets, and in amygdules. Coarse intraformational breccias locally are hematized. Biotite and amphibolite hornfelses occur adjacent to stocks which intrude the Bonanza Volcanics.

Cretaceous Sediments

The Vancouver Group is unconformably overlain by non-marine Cretaceous sediments of the Longarm Formation which are estimated to be about 300 metres thick in the Port Hardy area. These sediments, consisting of conglomerate, sandstone, greywacke, and siltstone and some carbonaceous and impure coal seams, occupy local basins. Early coal mining in the district was from several of these basins.

Intrusive Rocks

Vancouver Group rocks are intruded by a number of Jurassic-aged stocks and batholiths. In the Holberg Inlet area a belt of northwest-trending stocks extend from the east end of Rupert Inlet to the mouth of Stranby River on the north coast of Vancouver Island.

Quartz-feldspar porphyry dikes and irregular bodies occur along the south edge of the belt of stocks. Dikes are characterized by coarse, subhedral quartz and plagioclase phenocrysts set in a pink, fine grained, quartz and feldspar matrix. They are commonly extensively altered and pyritized. At Island Copper Mine, porphyries are enveloped by altered, brecciated, mineralized Bonanza wallrocks. The porphyries, too, are cut by siliceous veins, pyritized, extensively altered, and are mineralized where they have been brecciated. The quartz-feldspar porphyries are thought to be differentiates of middle Jurassic, felsic, intrusive rocks.

Other intrusive rocks of lesser significance include felsic dykes and sills around the margins of some stocks; dikes of andesitic composition, which cut the Karmutsen, Quatsino and Parson Bay formations, and represent feeders for Bonanza volcanism; and Tertiary basalt-dacite dykes intruding Cretaceous sediments.

Structure

The structure of the rocks north of Holberg and Rupert Inlets is that of shallow synclinal folding along a northwesterly fold axis. The steeper southwesterly limbs of the folds have apparently been truncated by faults roughly parallel to the fold axis. Failure of limestone during folding may have influenced the location of some faulting as indicated by proximity of Dawson and Stranby River faults to the Quatsino limestone horizon. Transverse faulting is pronounced and manifested by numerous north and northeasterly trending faults and topographic lineaments.

The northern part of Vancouver Island lies in a block faulted structural setting with post Lower Cretaceous northwesterly trending faults apparently being the major system. This causes repetition and loss of parts of the stratigraphic section, with aggregate movement in a vertical sense in the order of tens to hundreds of metres. The most significant of these fault systems trends west to northwest following Rupert and Holberg inlets. Near the west end of Holberg Inlet this fault splits, with the main branch following Holberg Inlet and the other branch passing through the west side of the Stranby River valley. Another northwesterly to westerly system passes through William Lake and still another, smaller system passes through Nahwitti Lake.

Northeasterly trending faults comprise a subordinate fault system. In some cases, apparent lateral displacement, in the order of a several hundred metres, can be measured on certain horizons. Movement, however, could be entirely vertical with the apparent offset resulting from the regional dip of the beds.

Recent computer modelling of the airborne magnetometer data has facilitated an understanding of the relationship of secondary conjugate sets of northeast and north westerly faults related to the major west-northwest trending breaks. The conjugate fault sets appear to relate directly to the mineralization at the Island Copper, Hushamu, Hep and Red Dog copper/gold deposits.

REGIONAL MINERALIZATION

Several types of mineral occurrences are known on Northern Vancouver Island. These include:

- Skarn deposits: copper-iron and lead-zinc skarns.
- Copper in basic volcanic rocks (Karmutsen Fm.): in amygdules, fractures, small shears and quartz carbonate veins, with no apparent relationship to intrusive activity.
- Veins: with gold and/or base metal sulphides, related to intrusive rocks.
- Porphyry copper deposits: largely in the country rock surrounding or enveloping granitic rocks and their porphyritic phases.

Exploration in the Holberg-Rupert Inlets area during the 1960's focused on the search for copper porphyry deposits. The outstanding result has been the locating and developing the Island Copper Mine. Other areas of porphyry type mineralization, as well as two areas anomalous in gold and one area with massive sulphide mineralization have been identified.

PROPERTY GEOLOGY

The King Property is underlain primarily by Karmutsen Formation rock: medium to dark green massive and basalt flows. Some pyroclastic rocks and metasediments have been reported in the center of the claim block.

The pyroclastics outcrop near the end of a spur road in the north-central part of the claims. Malachite in float was found in road fill about half way up this spur road and traced to outcrop further up the road. Disseminated bornite was located in a amygdaloidal "andesite" (a field term) at a quarry. This unit has a discrete contact with a light green amygdaloidal andesite which has been altered at the contact. Occasional malachite occurs along the contact. Further up the road quartz veinlets cut amygdaloidal andesites. Some of these veinlets contain copper: malachite, chalcopyrite and bornite.

Siliceous alteration was found in outcrops along a creek in the southeast sector of the Property: the creek that drains Lake of the Mountains into Georgie Lake. The rock is a light green color (amygdaloidal andesite) which has been highly fractured and in some areas flooded with silica. Epidote occurs on fractures.

Boulders of quartz containing pyrite, chalcopyrite and bornite, with occasional malachite and azurite, occur along the north shore of Lake of the Mountains. Representative samples assay up to 0.65% Cu, with traces to 300 ppb gold. These boulder trains appear to be mostly in place, indicating a sizeable area of veining.

Northeast of Lake of the Mountains, at the west end of the small linear east-west trending lake (Camp Lake), quartz boulders containing bornite and chalcopyrite assayed 0.22% Cu and 1150 ppb Au. Southeast of Lake of the Mountains, towards Georgie Lake, a number of quartz veins cut an altered andesite tuff unit. One of the larger veins contains disseminated chalcopyrite. Upstream quartz veins have been noted in altered andesitic pyroclastics returning copper values to 1.7% Cu.

The drainages east of Shushartie Mountain contain widely spaced zones of small quartz veins and stringers running up to 0.45% copper and 103 ppb gold. In the north central portion of the area a zone of epidote skarn suggests an intrusive into the metasediments. The metasediment contain traces of arsenopyrite.

Shushartie River was sampled following the discovery of a number of parallel, large quartz veins in shear zones along the river bed. These quartz veins are associated with epidote and calcite mineralization and locally contain chalcopyrite and pyrite. West of the west end of the King 30 claim veining contains traces of chalcopyrite. The June 1990 moss sampling gave values of 590 ppb gold in the river east of this occurrence. Quartz float assaying up to 0.16% Cu in the river bed on the eastern side of the King 24 claim.

Camp Lake Area (1995 program)

The 1995 program focused on a relatively small area (about four square km) in the area directly north and west of Lake of the Mountains. This region was selected owing to its highly anomalous nature as determined by earlier sampling work.

Mapping control was by a combination of grid lines and, in a few cases, by using GPS (Global Positioning System) satellites. Results are summarized on an accompanying map entitled "King Mineral Claims -- General Compilation" (see pocket).

Except for a few diabase dikes, all exposed bedrock in the Camp Lake area consists of upper Karmutsen Formation lava, that is, a sequence of massive basaltic flows averaging about five metres thick. In appearance there is considerable variation within and between outcrops. Textures range from dense massive and fine grained to coarsely vesicular (amygdaloidal). In some spots rock is somewhat porphyritic. Color varies from black to very pale green which in turn reflects vescularity. Rock consisting of 20 or more volume percent gas voids is invariably bleached light green (andesite green!) whereas massive basalt appears black to dark green. Individual flows are typically massive at the base and increasingly amygdaloidal upward. And in fact, there tends to be as much variation within large exposures as there is between different outcrops. Bedding is about 135° ±45° SW.

There are no significant patterns of alteration apart from the widespread and pervasive occurrence of chlorite, epidote and quartz. Quartz occurs (with epidote) filling amygduals and as irregular veinlets (sweats). Chlorite (together with moderate serpendization) is commonly found in association with shearing. In rare instances (i.e., Stn. 3E 2N) rock is metamorphosed to a hornfels and at one location (Stn. 8E 5S) the outcrop has developed a coarse "gabbroic" texture.

Several noteworthy structural elements were observed. There is a general northwesterly fabric to the area which is most clearly perceived on airphotos. This is a reflection of the dominant 135° strike direction, an effect which has been topographical enhanced by glaciation. Small scale shearing observed in outcrop is depicted on the accompanying map.

As well, there are a number of fault zones or lineations with potential mineral deposit implications. These can be seen on the ground, in the geophysical data, and on aerial photographs. In fact, it is the juxtaposition of these projected faults with geochemical anomalies that is considered a key criteria of exploration merit for recommended follow-up work.

There are two (or more) fault directions considered important on the King Property. One trend is northwest-southeast, the other at right angles to this. Features corresponding to the former direction are masked by glacial/bedding trends but still discernible.

In general, most hard-rock gold mineralization occurs in quartz veins and/or in larger fault systems frequently associated with quartz. Since auriferous quartz has been noted on the King Property that criteria is satisfied. But, because exposure is poor (almost non existent in areas where faults are projected to occur) it in not possible to test targets by surveys alone. Targets will now have to be trenched to expose bedrock and facilitate sampling in areas of merit.

GEOCHEMICAL SURVEY

The 1995 sampling program comprised fill-in work in the vicinity of previously identified anomalies located north and northeast of Lake of the Mountains. As well, the quartz vein system at Stn. 3E 2N was trenched and sampled. The areas involved are indicated on the General Compilation Map (see pocket) and referred to as: Zone 2-3, Zone 4, Zone 5 and Main Zone Anomalies.

Sample Collection and Analysis

North-south lines were established using hip chain and compass and marked with stations corresponding to the original system (1993 grid work). Soil samples were collected at a 25 metre spacing on survey lines between 50 and 100 metres apart.

Soil was taken from the "B" horizon using four foot augers with special care taken to maintain uniformity with the earlier sampling. Material was placed in marked Kraft bags for analysis. The samples were shipped to Acme Analytical Laboratories Ltd. at 852 East Hastings Street in Vancouver for drying and analysis by 30 element ICP and 30 gm fire assay for gold. Assay certificates are included in Appendix II, and gold values are posted on figure 5 (see pocket).

Results:

Not counting duplicate check tests, 739 soil samples were collected on the King Property. All returned low base metal values. Gold results are significant. There are a number of isolated highs in excess of 100 ppb (parts per billion) and broad groupings in excess of 15 ppb Au. The average gold value is 5 ppb with a standard deviation of 1.414. For ease of interpretation, values above 10 ppb can be considered as anomalous. Results support the 1993 data.

Several rock chip samples were collected in the course of mapping. One, the 3E 2N "showing", returned anomalous gold and copper values initially but proved disappointing when subsequently trenched. Nevertheless, this occurrence corresponds to a vein-fault system (with altered hanging-foot walls) and may yet prove interesting. Additional work is warranted along strike.

As indicated, there are a number of anomalous areas. Perhaps the most significant is the zone immediately south of and sub-parallel to the base line (north of Camp Lake). High gold values here coincide with a strong VLF-EM anomaly and an airphoto lineament which almost certainly represents a fault system: a target for follow-up work.

CONCLUSIONS

Exploration results on the King Property remain positive and a follow-up program is recommended. This conclusion is based on the cumulative results an integrated program which included: 1) a review of earlier data, 2) grid controlled geological-geochemical surveys, 3) analysis of structural elements based on mapping and photo-interpretation, and, 4) concurrent geophysical surveys.

The principal exploration target on the King Property is structurally controlled gold mineralization -- gold veins. The assumption is that any significant mineralization will be contained within, or be somehow associated with, linear structures. And, since veins, especially quartz veins, tend to be narrow, poorly exposed, and have a low geophysical contrast relative to host lithologies, the only realistic objective at the survey stage is delineation of structure associated with anomalous gold. In that respect, geophysics has been especially helpful. After filtering out false anomalies, a number of linear features can be seen in the data that apparently correspond to through-going faults. Support for this interpretation comes from shearing noted while mapping and corresponding lineations obvious on aerial photographs. For reference see General Compilation Map (figure 4 in pocket) and attachments including a geophysical report (Appendix III).

Three geophysical parameters were measured over target areas on the King Property: the VLF-EM response, Resistivity and Total Magnetic Field. Measurements were taken on 12.5 and 25 metre spacing and a recording base station was used to regulate two field instruments. Linear anomalies seen in the data appear as magnetic lows, resistivity lows and VLF-EM conductors. These features have been plotted on figure 4 along with other related information to facilitate interpretation. The targets correspond to places where linear elements coincide with quartz veining and anomalous gold in soils. Specifically:

1. Gold in vein-quartz was found near station 7W 3S on the north shore of Lake of the Mountains. A prominent northeast trending airphoto linear intersects this point and high geochem values occur in soils at points on this apparent fault.

2. An airphoto lineament, a VLF-EM conductor, and a highly anomalous soil geochem follows a line along the north side of Camp Lake.

3. A quartz vein system characterized by strong foot-wall alteration and high associated geochem values coincide with a southeast trending resistivity low at station 3E 2N.

These are priority targets where future work can be focused. The next step should consist of back-hoe trenching. If successful, showings will then have to be drilled to confirm grade and down-dip continuity. A staged program budget follows.

RECOMMENDED PROGRAM/BUDGET

A staged follow-up program is recommended on the King Property. In the first phase this comprises back-hoe trenching. Contingent upon success a second phase diamond drilling program would follow. Work should be scheduled to take advantage of logging roads which are being extended toward key target areas and will soon provide opportune access for heavy equipment.

The program with estimated costs:

Stage I (Back-hoe trenching: one month, early Fall, 1996?)

Wages, salaries and benefits	$ 11,000	
Accommodation (30 days @ $65/day)	1,950	
Geochemistry and assays	1,500	
Access trails and trenching	35,000	
Vehicle Transportation	1,500	
Office, report preparation, etc.	4,050	
Contingencies	10,000	
Total Stage I		$ 65,000

Stage II (Diamond Drilling: one month, late Fall, 1996?)

Wages, salaries and benefits	$ 12,650	
Drill contract (assume 2,000 ft @ $ 20/ft.)	40,000	
Accommodation	1,950	
Vehicle Transportation	1,500	
Assays (assume 200 @ $18.50)	3,700	
Office, report preparation, etc.	4,200	
Contingencies	11,000	
Total Stage II		75,000
Total Stage I and Stage II		$ 140,000

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(1993) Geochemical Assessment Report on the King Mineral Claims dated February 26, by Peter G. Dasler.

CERTIFICATE OF QUALIFICATIONS

I, Douglas G.F. Leighton, do hereby certify that:

1. I am a consulting geophysicist/geologist with offices at 3806 - 254th Street, Aldergrove, B.C., V4W 2R3.

2. I am a graduate of the University of British Columbia, B.Sc., (1968).

3. I am a registered Professional Geoscientist of the Province of British Columbia.

4. I have practiced my profession continuously since 1968.

5. I personally supervised the exploration program on the King claims described in this report for Westward Exploration Ltd.

6. I have not received, nor do I expect to receive any interest, direct or indirect, in the King Property, in Westward Exploration Ltd., in Consolidated T.C. Resources Ltd. or in the securities of either company.

7. I hereby consent to the publication of this report for purposes of a Prospectus or Statement of Material Facts.

Dated at Aldergrove, British Columbia, this 18th day of December, 1995

Douglas G.F. Leighton, P.Geo.

PROFESSIONAL
PROVINCE OF
D. G. F. LEIGHTON
BRITISH COLUMBIA
GEOSCIENTIST

APPENDIX I

Breakdown of Costs

(For Assessment Purposes)

Westward Explorations Ltd															
King Project	total costs from invoices Dec 10 1995														
Personnel		1-15 Sept	16-30 Sept	1-15 Oct	16-31 Oct	1-15 Nov	16-30Nov		**Totals $**	GST					
P. Dasler P. Geo.		0.8	1.70	0.50	0.50	0.75	0.50		1805.00	126.35					
J Telegus, field assist			8.00	10.00					4950.00	346.50					
S. Salmon, field Assist.			2.00	0.00					550.00	38.50					
R. Riuta, field Assist			4.00	9.00					3575.00	250.25					
Doug Leighton, Snr Geol			8.50	10.00		5.00			8930.00	625.10					
P MacDonald	Field Tech					3.00			825.00	57.75					
									0.00						
Totals Days	63.45		24.20	29.50	0.50	8.75	0.50	0.00	20635.00	1444.45		1444.45			
DISBURSEMENTS															
Date	Item	Gross	NET	GST	Food /Accom	Hotel	Transportation	Supplies	Field Equip Rental	H.Equip/Heli	Contactor	Assays	Offfice	Checks	Disb Fee
15-Sep	Kamaka Inv 950912	21.28	0.00	21.28											
30-Sep	Kamak Inv 950914	1419.59	1022.58	397.01	73.78	229.11	425.01	294.68							153.39
15-Oct	Kamaka Inv 951003	19114.71	16899.29	2215.42	1510.44		1756.70	524.56	140.00	1358.12	11609.47				2304.64
31-Oct	Kamaka Inv 951010	12354.85	11422.07	932.78		112.48		48.22	1050.00	1464.90		8713.44	33.03		1713.31
15-Nov	Kamka Inc 951102	1012.93	865.55	147.38				240.75		616.80			8.00		129.83
30-Nov	Kamaka Inv 951108	2407.31	2092.56	314.75	22.84		290.79	194.39		1517.55			66.99		313.88
		0.00	0.00												
		0.00	0.00												
Totals	Disbursement Totals	36330.67	32302.05	4028.62	1607.06	341.59	2472.50	1302.60	1190.00	4957.37	11609.47	8713.44	108.02	0.00	4615.05
	Check	36330.67	32302.05												
	Disbursement Fees		4615.05			Inv 950912	325.28								
	Labour		20635.00			Inv 950914	6068.98								
	GST		4028.62			Inv 951003	33864.35								
	TOTAL INCL GST		61580.72			Inv 951010	14258.16								
	NET		57552.10			Inv 951102	2252.76								
						Inv 951108	4811.19								
						TOTAL	61580.72								

APPENDIX II

Certificates of Analysis

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Kamaka Resources Ltd. File # 95-4192 Page 1

6074 - 45A Ave, Delta BC V4K 1H7

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L13+50W 1+00N	2	48	<3	28	<.3	12	5	149	11.01	3	6	<2	<2	12	<.2	<2	<2	308	.71	.013	<1	117	.35	5	.90	<3	7.31	.01	<.01	<2	10
L13+50W 0+87.5N	1	29	4	29	<.3	7	3	116	9.21	6	<5	<2	<2	14	<.2	<2	<2	382	.53	.009	<1	56	.16	5	.99	<3	2.28	.01	.01	<2	6
L13+50W 0+75N	2	43	5	52	.3	17	9	357	8.24	4	<5	<2	<2	20	<.2	<2	<2	259	1.20	.019	1	68	.54	7	.98	<3	3.82	.01	.01	<2	8
L13+50W 0+62.5N	2	33	4	49	<.3	11	8	302	5.41	4	<5	<2	<2	19	<.2	<2	<2	248	1.07	.017	1	55	.38	8	.96	3	2.90	.01	<.01	<2	5
L13+50W 0+50N	2	28	7	30	<.3	9	2	119	12.49	2	<5	<2	<2	9	<.2	7	3	581	.25	.007	1	74	.08	4	1.13	<3	1.28	.01	<.01	<2	6
L13+50W 0+37.5N	1	17	6	31	<.3	5	1	96	8.22	3	<5	<2	<2	15	.4	2	<2	436	.87	.007	<1	66	.16	5	1.25	<3	1.46	.01	<.01	<2	6
L13+50W 0+25N	2	23	4	45	<.3	7	49	3575	8.74	3	<5	<2	3	15	<.2	<2	<2	325	1.10	.011	<1	61	.28	10	1.00	<3	2.15	.01	.01	<2	5
L13+50W 0+12.5N	2	68	<3	75	<.3	22	14	339	9.02	8	<5	<2	<2	12	<.2	<2	2	286	1.10	.014	<1	91	.71	7	1.03	<3	4.27	.01	<.01	<2	3
L13+50W 0+00	2	39	4	45	<.3	13	17	377	10.66	6	<5	<2	<2	15	<.2	4	3	331	.93	.017	3	66	.33	10	.73	<3	3.08	.01	<.01	<2	5
L13+50W 0+12.5S	1	36	<3	49	<.3	17	25	1286	6.42	<2	<5	<2	<2	27	<.2	<2	2	201	1.49	.010	2	45	.60	12	.57	<3	2.42	.02	.01	<2	3
L13+50W 0+25S	1	42	<3	34	<.3	15	15	355	7.58	4	<5	<2	<2	25	<.2	2	<2	216	1.33	.006	1	45	.54	13	.64	<3	2.32	.02	<.01	<2	4
L13+50W 0+37.5S	1	46	<3	55	<.3	16	12	334	3.60	4	<5	<2	<2	22	<.2	<2	<2	139	1.17	.024	5	49	.57	13	.46	3	2.86	.02	.01	<2	10
L13+00W 1+00N	2	50	3	66	<.3	18	43	1613	10.56	2	<5	<2	<2	19	<.2	<2	<2	330	.98	.015	1	89	.43	13	.95	<3	3.48	.01	<.01	<2	9
L13+00W 0+87.5N	1	34	3	33	<.3	12	5	222	10.10	2	<5	<2	<2	16	<.2	2	<2	358	.68	.009	<1	74	.27	7	.99	<3	2.29	.01	<.01	<2	5
L13+00W 0+75N	2	30	4	40	<.3	13	8	229	10.74	5	<5	<2	<2	16	<.2	<2	<2	231	.92	.011	1	103	.37	9	.79	<3	3.81	.01	<.01	<2	3
L13+00W 0+62.5N	1	27	4	29	.4	7	3	122	8.55	<2	<5	<2	<2	16	<.2	2	4	411	.58	.012	<1	53	.16	9	1.27	<3	1.57	.01	.01	<2	10
L13+00W 0+50N	1	29	<3	34	.3	10	5	207	9.01	4	<5	<2	<2	19	<.2	4	<2	346	.94	.007	<1	62	.32	7	1.06	<3	2.08	.01	<.01	<2	46
L13+00W 0+37.5N	1	35	3	42	<.3	16	9	242	8.78	6	<5	<2	<2	18	<.2	<2	<2	241	1.03	.010	1	86	.48	7	.74	<3	3.70	.01	<.01	<2	8
L13+00W 0+25N	1	51	<3	47	<.3	18	17	432	7.01	5	<5	<2	<2	27	<.2	3	<2	201	1.53	.011	2	43	.68	14	.62	3	2.45	.02	.01	<2	5
L13+00W 0+12.5N	1	54	3	53	<.3	19	24	633	5.70	2	<5	<2	<2	27	<.2	<2	<2	182	1.56	.018	3	45	.73	13	.54	<3	2.78	.02	<.01	<2	12
L13+00W 0+00	1	29	4	60	<.3	18	10	304	6.41	3	<5	<2	<2	26	<.2	<2	2	247	1.32	.018	<1	49	.69	11	.82	<3	1.97	.02	.01	<2	3
RE L13+00W 0+00	1	29	<3	59	<.3	18	10	298	6.48	4	<5	<2	<2	26	<.2	<2	2	251	1.30	.017	<1	48	.67	11	.82	<3	1.96	.02	.01	<2	6
L13+00W 0+12.5S	1	36	3	42	<.3	14	10	274	8.04	4	<5	<2	<2	26	<.2	<2	<2	253	1.29	.010	<1	57	.46	12	.79	3	2.22	.02	.01	<2	6
L13+00W 0+25S	1	43	7	43	<.3	16	30	868	8.35	4	<5	<2	2	24	<.2	3	2	234	1.32	.017	2	51	.62	13	.63	4	2.46	.02	.02	<2	3
L13+00W 0+37.5S	1	40	<3	40	<.3	15	17	371	8.12	5	<5	<2	<2	24	<.2	2	<2	220	1.20	.008	<1	58	.51	10	.63	<3	2.55	.01	<.01	<2	8
L13+00W 0+50S	1	33	3	80	<.3	24	13	359	4.73	3	<5	<2	<2	26	<.2	<2	<2	131	1.56	.023	3	37	.96	11	.46	3	2.30	.03	.02	<2	4
L12+50W 1+00N	2	43	4	40	.4	9	5	175	12.51	4	5	<2	<2	18	<.2	2	2	357	.85	.018	<1	93	.24	8	1.13	<3	2.87	.01	.01	<2	4
L12+50W 0+87.5N	1	33	<3	31	<.3	8	4	105	10.33	6	<5	<2	<2	12	<.2	<2	<2	326	.61	.011	<1	92	.20	5	.93	<3	3.49	.01	.01	<2	58
L12+50W 0+75N	1	42	<3	55	<.3	16	7	204	7.17	8	<5	<2	<2	18	<.2	3	<2	218	1.09	.016	1	58	.40	9	.71	<3	2.86	.01	<.01	<2	5
L12+50W 0+62.5N	1	41	<3	44	<.3	10	5	147	9.54	3	<5	<2	<2	16	<.2	2	3	294	.85	.015	2	72	.23	8	.88	3	3.28	.01	.01	<2	3
L12+50W 0+50N	1	55	<3	74	<.3	28	18	480	8.38	6	<5	<2	<2	26	<.2	<2	<2	200	1.32	.026	2	68	.92	16	.76	<3	4.11	.02	.02	<2	4
L12+50W 0+37.5N	1	28	3	62	<.3	22	10	286	8.01	3	<5	<2	<2	25	<.2	2	<2	319	1.72	.013	<1	54	.79	12	.95	<3	2.42	.02	.01	<2	3
L12+50W 0+25N	1	43	<3	62	.4	19	30	1121	7.07	3	<5	<2	4	25	<.2	<2	2	224	1.40	.018	3	62	.66	18	.84	3	3.34	.01	<.01	<2	10
L12+50W 0+12.5N	1	40	<3	67	<.3	25	13	340	6.34	4	<5	<2	<2	26	<.2	<2	<2	215	1.39	.019	<1	46	.83	11	.67	3	2.16	.03	.01	<2	3
L12+50W 0+00	1	44	<3	63	.5	20	40	3292	6.32	6	<5	<2	6	24	<.2	<2	<2	183	1.29	.015	4	54	.59	18	.56	<3	3.00	.01	<.01	<2	4
STANDARD C/AU-S	22	61	38	130	6.5	68	30	1044	4.07	43	18	7	40	53	19.0	18	20	57	.51	.094	39	63	.93	189	.08	25	1.88	.06	.14	10	53

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.
- SAMPLE TYPE: SOIL AU* - IGNITED, AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED.
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 11 1995 DATE REPORT MAILED: Oct 24/95 SIGNED BY C. Leong ......D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L12+50W 0+12.5S	1	25	<3	85	<.3	22	22	718	5.70	9	<5	<2	<2	37	<.2	<2	<2	164	1.52	.028	4	45	.78	19	.57	4	2.03	.02	.04	<2	88
L12+50W 0+25S	1	43	<3	46	<.3	18	12	337	10.04	13	<5	<2	<2	25	<.2	<2	<2	251	1.17	.010	<1	77	.55	14	.83	<3	3.22	.01	.01	<2	6
L12+50W 0+37.5S	1	39	<3	50	<.3	18	14	350	9.22	9	<5	<2	<2	27	<.2	<2	<2	272	1.38	.009	1	71	.53	11	.81	<3	3.32	.01	.01	<2	4
L11+50W 1+00N	1	36	<3	34	.3	8	4	149	9.54	10	<5	<2	<2	20	.4	<2	<2	322	.91	.019	1	111	.19	5	.92	<3	4.22	.01	.01	<2	4
L11+50W 0+87.5N	1	26	<3	28	.4	5	3	133	10.80	11	<5	<2	<2	34	<.2	<2	<2	473	.68	.013	<1	87	.12	4	1.13	<3	1.82	.01	.01	<2	3
L11+50W 0+75N	<1	21	<3	43	.3	6	5	196	7.64	10	<5	<2	<2	51	<.2	<2	<2	495	2.08	.009	1	41	.26	4	1.03	<3	2.20	.01	.03	<2	10
L11+50W 0+62.5N	1	35	5	26	.6	5	4	208	15.16	7	<5	<2	<2	17	.2	5	<2	552	.51	.016	<1	76	.10	5	1.18	<3	1.92	.01	.01	<2	7
L11+50W 0+50N	1	40	5	44	.5	11	5	143	12.96	11	<5	<2	<2	19	.4	2	<2	401	.88	.013	<1	80	.26	7	1.17	<3	3.08	.01	.02	<2	2
L11+50W 0+37.5N	<1	33	6	25	.4	6	3	185	12.39	6	<5	<2	<2	14	.4	4	<2	607	.42	.009	<1	49	.12	5	1.31	<3	1.26	.01	.01	<2	7
RE L11+50W 0+37.5N	1	31	7	26	.8	6	4	182	12.61	9	<5	<2	3	14	.2	3	<2	599	.42	.007	<1	50	.12	5	1.27	<3	1.28	.01	.01	<2	9
L11+50W 0+25N	2	28	6	46	.4	8	5	143	12.37	12	<5	<2	2	20	<.2	4	<2	365	.73	.014	<1	79	.20	7	1.04	<3	2.37	.01	.01	<2	2
L11+50W 0+12.5N	2	51	<3	65	<.3	13	28	807	11.64	12	<5	<2	<2	20	<.2	<2	<2	367	.78	.025	2	90	.24	11	.90	<3	3.97	.01	.02	<2	3
L11+50W 0+00	1	22	3	26	.3	3	6	257	9.03	11	<5	<2	<2	15	<.2	6	<2	454	.34	.006	1	46	.07	6	1.12	<3	1.53	.01	.01	<2	4
L11+50W 0+12.5S	<1	27	3	35	.3	10	5	163	8.17	6	<5	<2	<2	18	<.2	4	<2	421	.88	.009	<1	56	.31	6	1.19	<3	2.39	.01	.01	<2	6
L11+50W 0+25S	1	65	5	35	.4	7	3	117	15.49	9	<5	<2	<2	18	.7	<2	<2	513	.64	.015	<1	94	.20	6	1.23	<3	2.88	.01	.01	<2	3
L11+50W 0+37.5S	1	45	<3	40	.6	5	2	76	17.28	10	<5	<2	3	19	.6	4	<2	563	.56	.015	<1	88	.12	6	1.37	<3	2.47	.01	.01	<2	20
L11+50W 0+50S	2	121	<3	36	<.3	10	6	100	10.42	8	<5	<2	2	10	<.2	<2	<2	170	.35	.025	4	101	.17	7	.50	<3	11.02	.01	.01	<2	5
L11+00W 1+00N	<1	26	3	29	.3	7	3	100	12.39	7	<5	<2	<2	15	<.2	4	<2	453	.50	.011	<1	100	.14	6	1.08	<3	2.77	.01	.01	<2	5
L11+00W 0+87.5N	1	43	<3	31	<.3	10	5	212	11.25	6	<5	<2	<2	17	<.2	<2	<2	396	.46	.011	<1	97	.39	6	.80	<3	2.18	.01	.03	<2	7
L11+00W 0+75N	1	68	<3	48	<.3	20	8	186	11.08	9	<5	<2	<2	20	<.2	<2	<2	387	.43	.007	<1	142	.71	10	.79	<3	3.93	.01	.02	<2	6
L11+00W 0+62.5N	1	20	4	32	<.3	8	4	143	8.67	6	<5	<2	<2	18	<.2	3	<2	509	.41	.009	<1	55	.21	7	.89	<3	1.22	.01	.03	<2	4
L11+00W 0+50N	1	34	5	43	<.3	14	5	172	4.60	6	<5	<2	<2	24	<.2	<2	<2	337	1.25	.011	<1	84	.40	9	1.30	<3	3.66	.01	.01	<2	4
L11+00W 0+37.5N	<1	46	3	65	<.3	8	15	1384	8.05	6	<5	<2	2	19	<.2	<2	<2	271	.62	.038	6	73	.22	11	.48	<3	2.94	.01	.02	<2	5
L11+00W 0+25N	1	45	3	58	<.3	9	24	882	14.92	5	<5	<2	4	14	<.2	<2	<2	283	.71	.020	2	112	.37	9	.63	<3	4.67	.01	.02	<2	4
L11+00W 0+12.5N	1	34	6	59	<.3	8	17	548	3.86	6	<5	<2	<2	25	<.2	2	<2	219	.88	.026	4	73	.27	14	.69	3	2.99	.01	.03	<2	81
L11+00W 0+00	<1	35	4	50	.6	4	723	34016	18.20	9	12	3	2	14	<.2	<2	<2	338	.30	.020	2	137	.11	52	.66	<3	3.84	.01	.02	<2	5
L11+00W 0+12.5S	1	22	8	29	<.3	7	8	298	13.14	6	<5	<2	2	12	<.2	2	<2	456	.47	.010	<1	85	.14	5	1.04	<3	2.11	.01	.01	<2	8
L11+00W 0+25S	1	27	10	24	.3	6	3	129	14.54	8	<5	<2	<2	12	<.2	2	<2	544	.37	.010	<1	89	.13	5	1.17	<3	1.74	.01	.01	<2	8
L11+00W 0+37.5S	<1	17	5	23	.4	4	2	143	9.06	3	<5	<2	<2	23	<.2	<2	<2	567	.65	.006	<1	38	.10	4	1.13	<3	1.19	.01	.01	<2	92
L11+00W 0+50S	1	26	<3	46	<.3	11	6	181	10.70	6	<5	<2	<2	28	<.2	<2	<2	535	1.71	.012	<1	53	.35	6	1.12	<3	2.45	.01	<.01	<2	10
L10+50W 1+00N	1	44	<3	28	<.3	7	3	112	12.59	7	<5	<2	<2	11	<.2	<2	<2	337	.47	.020	<1	130	.19	6	.93	<3	5.96	.01	<.01	<2	5
L10+50W 0+87.5N	1	49	3	25	<.3	4	2	86	17.48	3	<5	<2	<2	10	.4	4	<2	507	.25	.009	<1	101	.11	5	1.02	<3	3.03	.01	<.01	<2	8
L10+50W 0+75N	<1	59	3	29	<.3	3	2	78	12.24	5	<5	<2	2	14	<.2	3	<2	456	.35	.011	1	81	.12	5	.88	<3	3.14	.01	<.01	<2	8
L10+50W 0+62.5N	1	35	8	28	<.3	6	3	104	10.58	3	<5	<2	3	14	<.2	<2	<2	342	.49	.010	<1	91	.16	6	.93	<3	3.22	.01	.01	<2	8
L10+50W 0+50N	<1	16	6	38	<.3	2	121	10141	26.68	<2	<5	<2	20	10	<.2	10	<2	220	.27	.020	3	58	.12	64	.32	<3	1.67	.01	.03	<2	4
STANDARD C/AU-S	21	60	37	133	6.8	68	30	1027	4.11	43	15	7	42	55	18.7	16	17	60	.53	.096	42	63	.94	193	.09	26	1.96	.06	.16	11	50

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L10+50W 0+37.5N	<1	24	<3	84	<.3	4	7	360	1.34	<2	<5	<2	<2	6	<.2	<2	<2	46	.18	.029	4	12	.05	5	.05	4	.77	.01	<.01	<2	5
L10+50W 0+25N	1	24	3	25	<.3	7	2	107	13.26	<2	<5	<2	<2	13	.8	<2	<2	571	.50	.015	<1	112	.13	6	1.28	<3	2.77	.01	<.01	<2	6
L10+50W 0+12.5N	1	12	10	26	<.3	6	4	126	6.32	<2	<5	<2	<2	15	.2	3	<2	516	.61	.002	1	53	.23	6	.94	3	1.61	.01	<.01	<2	15
L10+50W 0+00	1	25	5	41	<.3	4	13	356	14.47	3	<5	<2	2	15	.4	<2	<2	575	.45	.009	1	78	.12	8	.88	<3	2.08	.01	.01	<2	6
L10+50W 0+12.5S	2	18	<3	33	<.3	5	51	1038	13.52	4	<5	<2	2	13	.2	5	<2	392	.53	.009	2	89	.17	10	.69	<3	2.55	.01	.01	<2	8
L10+50W 0+25S	1	36	4	33	<.3	7	3	109	9.41	<2	<5	<2	<2	12	.3	<2	<2	476	.62	.007	<1	96	.21	6	1.20	<3	4.26	.01	<.01	<2	8
L10+50W 0+37.5S	1	18	6	39	<.3	2	17	298	11.89	3	<5	<2	<2	13	.3	<2	<2	477	.47	.013	1	41	.09	6	.72	<3	1.22	.01	.02	<2	5
L10+50W 0+50S	1	27	3	31	<.3	5	17	504	14.76	<2	<5	<2	2	10	.4	<2	<2	471	.44	.016	<1	58	.24	6	.78	<3	1.75	.01	.01	<2	5
L10+50W 0+62.5S	1	19	5	36	<.3	3	6	229	10.79	<2	<5	<2	<2	9	.4	3	<2	473	.21	.015	2	40	.07	6	.64	<3	1.32	.01	.02	<2	4
L10+50W 0+75S	1	26	4	26	.3	7	10	226	13.32	2	<5	<2	<2	9	.4	2	<2	716	.33	.004	<1	79	.10	6	1.17	<3	1.40	.01	<.01	<2	4
L10+00W 0+25N TEST A	1	37	3	44	<.3	7	3	105	9.47	2	<5	<2	<2	15	.4	<2	<2	422	.84	.010	<1	89	.23	5	.97	<3	3.66	.01	<.01	<2	5
L10+00W 0+25N TEST B	1	23	5	32	<.3	4	2	96	12.06	3	<5	<2	<2	10	.5	2	<2	508	.41	.013	<1	82	.10	5	1.08	<3	1.95	.01	<.01	<2	9
L10+00W 0+25N TEST C	1	16	<3	38	<.3	10	6	140	8.26	3	<5	<2	<2	14	.2	<2	<2	515	1.99	.010	<1	61	.27	4	.85	<3	2.18	.01	<.01	<2	19
L9+50W 0+75N	1	21	5	32	<.3	7	3	100	13.43	<2	<5	<2	<2	10	.4	2	<2	568	.29	.016	<1	79	.08	4	1.01	<3	1.39	.01	<.01	<2	7
L9+50W 0+62.5N	1	26	<3	24	<.3	6	3	112	13.95	<2	<5	<2	2	7	.5	2	<2	575	.25	.016	<1	71	.13	4	1.00	<3	1.69	.01	.01	<2	11
RE L10+00W 0+25N TEST C	1	17	4	39	<.3	11	6	143	8.15	<2	<5	<2	<2	14	<.2	<2	<2	509	2.07	.011	1	59	.29	4	.85	<3	2.22	.01	<.01	<2	27
L9+50W 0+50N	2	30	5	22	<.3	4	2	76	12.27	5	<5	<2	2	10	.3	<2	<2	518	.37	.009	<1	96	.13	4	.93	<3	3.07	.01	<.01	<2	6
L9+50W 0+37.5N	1	31	<3	20	<.3	6	3	102	13.51	3	<5	<2	<2	13	.3	<2	<2	600	.45	.013	1	98	.12	6	1.05	<3	3.23	.01	<.01	<2	14
L9+50W 0+25N	2	90	<3	34	<.3	14	7	166	7.54	6	<5	<2	<2	14	<.2	<2	<2	269	1.00	.013	2	118	.45	4	.81	3	8.15	.01	<.01	<2	7
L9+50W 0+12.5N	1	52	3	41	<.3	14	8	178	3.66	<2	<5	<2	<2	18	<.2	<2	<2	221	1.27	.011	2	96	.46	7	.77	4	5.60	.01	<.01	<2	7
L9+50W 0+00	<1	4	9	20	<.3	2	<1	53	.70	<2	<5	<2	<2	12	<.2	<2	<2	131	.23	.004	1	26	.04	7	.71	3	.70	.01	<.01	<2	13
L9+50W 0+12.5S	<1	6	8	16	<.3	2	2	105	2.09	<2	<5	<2	<2	13	<.2	2	<2	311	.36	.002	2	31	.08	6	.84	3	.90	.01	.01	<2	10
L9+50W 0+25S	1	81	5	34	.4	8	4	131	12.14	2	<5	2	<2	13	.6	<2	<2	510	.79	.008	<1	93	.24	5	1.29	<3	3.39	.01	<.01	<2	3
L9+50W 0+37.5S	2	83	<3	28	<.3	7	12	211	14.70	4	<5	<2	2	10	<.2	<2	<2	398	.38	.011	<1	93	.15	6	.92	<3	3.71	.01	<.01	<2	3
L9+50W 0+50S	1	32	<3	27	.3	6	3	101	13.55	3	<5	<2	3	13	<.2	<2	<2	516	.54	.012	<1	94	.13	5	1.15	<3	2.32	.01	.01	<2	7
L9+50W 0+62.5S	1	28	4	30	<.3	8	5	125	12.13	<2	<5	<2	<2	16	.5	<2	<2	498	1.30	.010	<1	61	.24	5	.96	<3	2.41	.01	.01	<2	8
L9+50W 0+75S	1	26	5	36	<.3	8	20	1015	7.59	4	<5	<2	<2	13	.2	<2	<2	340	.93	.016	1	44	.31	6	.80	<3	2.08	.01	.02	<2	8
L9+50W 0+87.5S	1	39	<3	32	.4	3	2	92	15.24	2	<5	<2	<2	9	.7	2	<2	566	.26	.013	<1	89	.12	5	1.22	<3	2.34	.01	.01	<2	5
L9+00W 0+75N	1	61	<3	31	<.3	15	7	178	9.01	<2	<5	<2	<2	15	.5	<2	<2	340	.87	.008	1	95	.42	5	.82	<3	4.53	.01	.01	<2	13
L9+00W 0+62.5N	1	16	5	21	.4	3	2	73	10.05	3	<5	<2	<2	8	<.2	4	<2	488	.21	.008	1	50	.07	3	.82	3	1.19	.01	.01	<2	505
L9+00W 0+50N	1	29	<3	25	<.3	4	2	79	10.47	<2	<5	<2	2	10	.2	<2	<2	405	.42	.012	<1	109	.15	5	.91	<3	4.48	.01	.01	<2	9
L9+00W 0+37.5N	1	18	<3	15	.3	3	1	76	9.69	<2	<5	<2	<2	8	<.2	2	<2	475	.22	.005	<1	76	.09	3	.86	<3	1.82	<.01	<.01	<2	6
L9+00W 0+25N	<1	30	4	20	.3	3	1	53	14.29	<2	<5	<2	2	7	.5	3	<2	578	.12	.009	1	64	.06	5	.86	<3	1.72	<.01	.01	<2	30
L9+00W 0+12.5N	1	93	5	39	<.3	8	9	210	13.52	<2	<5	<2	<2	8	.3	<2	<2	546	1.05	.012	<1	78	.35	5	.99	<3	2.90	.01	.03	<2	15
L9+00W 0+00	<1	22	4	19	.6	7	2	104	15.61	<2	<5	<2	3	8	.9	5	<2	771	.12	.010	<1	79	.06	4	1.33	<3	1.00	.01	.01	<2	7
STANDARD C/AU-S	21	58	36	125	6.3	65	32	990	3.93	41	16	7	38	51	18.9	15	16	61	.50	.092	42	58	.90	184	.08	26	1.84	.06	.13	11	45

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L9+00W 0+12.5S	2	54	<3	43	<.3	12	7	151	11.48	4	6	<2	7	14	<.2	<2	<2	302	.81	.012	1	130	.35	5	.83	4	7.13	.01	.01	<2	5
L9+00W 0+25S	2	30	5	43	.4	2	110	3640	25.70	8	12	<2	14	9	<.2	2	<2	653	.20	.022	1	111	.11	13	.62	3	2.53	.01	.02	<2	5
L9+00W 0+37.5S	2	34	4	50	.5	4	73	1941	22.44	2	11	<2	12	14	<.2	2	<2	587	.41	.015	2	98	.14	9	.70	4	3.51	.01	.02	<2	14
L9+00W 0+50S	1	30	<3	33	.6	2	19	560	17.25	<2	7	<2	9	16	<.2	<2	<2	529	.43	.015	<1	78	.11	6	1.04	3	2.16	.01	.01	<2	8
L9+00W 0+62.5S	1	34	4	31	.8	7	3	123	9.50	3	6	<2	5	18	.7	<2	<2	414	.79	.005	<1	78	.23	5	1.29	3	2.97	.01	.01	<2	4
L9+00W 0+75S	1	27	<3	17	.6	3	1	73	11.95	3	5	<2	7	11	<.2	<2	<2	518	.22	.006	<1	62	.07	3	1.12	4	1.33	<.01	<.01	<2	27
L9+00W 0+87.5S	1	40	5	25	.3	7	4	112	10.32	<2	8	<2	6	15	<.2	<2	<2	349	.69	.025	<1	102	.19	4	.88	3	4.42	.01	.01	<2	47
L9+00W 1+00S	<1	5	4	77	<.3	1	2	84	.72	2	<5	<2	<2	21	<.2	<2	<2	23	.32	.030	2	5	.13	7	.05	4	.25	.02	.05	<2	1
L9+00W 1+12.5S	<1	5	3	56	<.3	1	<1	25	.17	<2	<5	<2	<2	16	<.2	<2	<2	5	.29	.024	1	2	.07	5	.01	<3	.08	.01	.03	<2	2
L9+00W 1+25S	1	21	<3	40	.5	8	4	140	8.33	<2	<5	<2	5	13	.3	<2	<2	542	.58	.007	<1	47	.22	5	1.09	5	.96	.01	<.01	<2	7
L9+00W 1+37.5S	1	15	6	39	<.3	12	10	406	7.59	3	<5	<2	2	24	<.2	<2	<2	335	1.37	.011	1	34	.52	9	.60	<3	1.89	.01	.02	<2	5
L9+00W 1+50S	1	23	4	58	<.3	15	43	2164	10.83	4	6	<2	9	24	<.2	<2	<2	334	1.37	.020	2	42	.72	12	.52	4	2.20	.01	.02	<2	4
L8+50W 0+75N	1	30	<3	19	<.3	6	4	141	11.13	2	<5	<2	5	13	<.2	<2	<2	369	.50	.010	1	121	.21	5	.85	3	5.17	.01	<.01	<2	8
L8+50W 0+62.5N	1	24	<3	16	.5	3	2	80	13.58	5	<5	<2	7	12	<.2	<2	<2	590	.32	.007	<1	80	.12	5	1.11	<3	1.82	.01	<.01	<2	8
L8+50W 0+50N	1	35	<3	26	.3	9	5	133	11.57	2	6	<2	5	15	<.2	<2	<2	425	.74	.008	<1	116	.37	5	.98	3	4.85	.01	.01	<2	4
L8+50W 0+37.5N	2	46	<3	14	<.3	6	3	94	6.08	5	<5	<2	3	11	<.2	<2	<2	176	.65	.023	3	111	.22	4	.60	3	9.95	.01	<.01	<2	8
L8+50W 0+25N	1	68	<3	21	<.3	9	5	133	10.75	<2	6	<2	4	15	<.2	<2	<2	300	.84	.014	2	124	.33	5	.86	3	5.84	.01	<.01	<2	8
L8+50W 0+12.5N	1	18	<3	17	.5	5	3	100	10.56	<2	6	<2	7	14	<.2	2	<2	482	.54	.007	<1	91	.22	6	1.06	<3	2.75	.01	.01	<2	7
L8+50W 0+00	1	12	5	11	.3	2	1	84	9.22	3	<5	<2	4	14	<.2	2	<2	528	.29	.005	<1	51	.08	6	.92	3	1.24	.01	<.01	<2	9
L8+50W 0+12.5S	1	32	3	18	<.3	4	3	79	9.27	3	<5	<2	5	12	<.2	<2	<2	378	.43	.015	2	93	.12	4	.91	<3	3.82	.01	<.01	<2	7
L8+50W 0+25S	<1	23	3	22	<.3	12	6	250	3.84	4	<5	<2	<2	68	<.2	<2	<2	443	1.19	.008	1	28	.42	3	.72	<3	1.35	.01	.01	<2	91
L8+50W 0+37.5S	1	19	<3	13	.3	5	3	150	10.67	3	<5	<2	3	8	<.2	3	<2	541	.25	.011	1	58	.12	4	.86	3	.96	.01	.01	<2	18
L8+50W 0+50S	1	29	<3	23	<.3	8	4	121	9.82	2	5	<2	5	14	<.2	<2	<2	336	.61	.020	1	85	.22	8	.82	3	4.22	.01	.02	<2	6
RE L8+50W 0+50S	1	29	5	23	<.3	8	4	119	10.06	<2	6	<2	6	14	<.2	<2	<2	345	.61	.021	<1	87	.22	7	.84	3	4.32	.01	.01	<2	7
L8+50W 0+75S	1	30	<3	19	.6	4	2	86	16.71	3	12	<2	7	11	<.2	3	<2	553	.24	.012	<1	97	.10	5	1.22	<3	2.35	.01	.01	<2	10
L8+50W 0+87.5S	<1	9	6	14	.3	3	2	108	6.95	<2	<5	<2	5	11	<.2	4	<2	634	.23	.004	<1	52	.11	6	1.00	<3	1.13	.01	.01	<2	9
L8+50W 1+00S	2	34	4	27	.4	9	5	231	16.97	8	9	<2	7	18	<.2	2	<2	512	.53	.021	<1	83	.32	7	1.32	3	2.65	.01	.01	<2	5
L8+50W 1+12.5S	1	58	4	25	<.3	5	4	83	12.19	2	<5	<2	4	12	<.2	<2	<2	366	.35	.014	<1	86	.14	7	.92	3	4.17	.01	.01	<2	7
L8+50W 1+25S	1	43	4	25	.4	6	4	116	13.56	4	6	<2	5	14	<.2	2	<2	642	.31	.006	<1	67	.10	6	1.06	<3	1.56	.01	<.01	<2	8
L8+50W 1+37.5S	1	48	<3	41	<.3	15	8	180	9.61	4	<5	<2	3	17	<.2	<2	<2	357	.91	.012	<1	62	.46	8	.82	5	3.04	.02	.01	<2	6
L8+50W 1+50S	<1	6	5	30	<.3	3	1	83	1.98	<2	<5	<2	<2	11	<.2	<2	<2	263	.23	.005	1	17	.08	6	.68	3	.56	.01	.01	<2	9
L7+50W 1+00N	1	30	<3	44	<.3	17	18	544	12.16	<2	<5	<2	6	23	<.2	2	<2	360	1.01	.010	<1	79	.62	12	.97	4	2.86	.01	.01	<2	25
L7+50W 0+87.5N	<1	48	<3	40	<.3	17	15	345	10.11	<2	6	<2	6	18	<.2	<2	<2	282	.88	.015	<1	121	.49	7	.83	<3	5.05	.01	.01	<2	8
L7+50W 0+75N	<1	38	<3	38	<.3	14	8	211	6.81	<2	6	<2	3	25	<.2	<2	<2	335	1.15	.008	2	86	.49	8	.99	<3	4.10	.01	<.01	<2	6
L7+50W 0+62.5N	<1	15	<3	27	<.3	4	3	134	10.74	<2	<5	<2	5	20	<.2	4	<2	322	.64	.007	1	54	.16	6	.70	3	1.54	.01	.01	<2	8
STANDARD C/AU-S	21	60	38	132	7.1	68	30	1054	4.20	37	22	6	40	54	19.7	15	18	65	.52	.096	45	62	.95	190	.09	27	1.95	.06	.15	10	48

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L7+50W 0+50N	1	34	<3	32	<.3	14	7	172	9.91	3	5	<2	<2	18	<.2	<2	<2	303	.89	.009	<1	103	.45	5	.81	<3	4.42	.01	.01	<2	5
L7+50W 0+37.5N	<1	18	<3	46	<.3	13	9	283	8.49	<2	<5	<2	<2	22	<.2	<2	<2	252	1.29	.015	<1	34	.52	7	.52	<3	1.93	.01	.03	<2	7
L7+50W 0+25N	<1	20	4	25	<.3	4	2	92	11.80	3	<5	<2	2	14	<.2	<2	<2	472	.52	.006	<1	61	.18	6	.93	<3	1.78	.01	.01	<2	4
L7+50W 0+12.5N	1	27	4	22	<.3	2	<1	54	12.68	5	7	<2	3	10	<.2	<2	2	536	.22	.003	<1	74	.08	4	1.05	<3	2.34	.01	.01	<2	3
L7+50W 0+00	<1	22	5	41	<.3	13	6	177	11.40	<2	7	<2	<2	18	<.2	<2	<2	398	1.16	.009	<1	67	.47	6	.96	<3	2.30	.01	.02	<2	5
RE L7+50W 0+00	1	21	4	38	<.3	13	6	170	10.89	<2	8	<2	<2	16	<.2	<2	<2	386	1.08	.010	<1	64	.44	6	.94	<3	2.16	.01	.01	<2	7
L7+50W 0+12.5S	1	28	3	17	<.3	6	2	93	12.76	<2	10	<2	<2	12	<.2	<2	<2	418	.43	.010	<1	109	.15	4	.91	<3	3.52	.01	.01	<2	2
L7+50W 0+25S	<1	30	<3	16	<.3	5	2	72	9.90	<2	8	<2	2	14	<.2	<2	<2	424	.45	.003	<1	78	.16	5	.97	<3	3.27	.01	.01	<2	4
L7+50W 0+37.5S	<1	20	<3	30	<.3	11	8	233	9.63	2	8	<2	<2	23	<.2	<2	<2	277	1.17	.013	<1	55	.46	8	.58	<3	2.17	.01	.02	<2	3
L7+50W 0+50S	<1	24	<3	13	<.3	4	1	77	11.98	<2	8	<2	3	13	<.2	<2	<2	525	.33	.003	<1	62	.12	5	1.06	<3	1.53	.01	.02	<2	3
L7+50W 0+62.5S	1	21	<3	41	<.3	21	17	616	8.90	<2	9	<2	2	27	<.2	<2	<2	251	1.60	.012	<1	53	.94	8	.62	<3	2.98	.02	.01	<2	3
L7+50W 0+75S	<1	15	<3	14	<.3	3	2	98	9.39	3	8	<2	<2	14	.4	<2	<2	452	.58	.004	<1	51	.15	5	.92	<3	1.73	.01	<.01	<2	5
STANDARD C/AU-S	20	55	36	124	6.2	63	31	974	3.90	40	21	6	39	51	18.1	15	20	57	.51	.089	39	59	.91	192	.09	30	1.87	.06	.15	9	54

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L7+00E 7+00N	1	18	12	21	<.3	3	2	74	10.41	6	<5	<2	<2	9	<.2	<2	5	341	.19	.006	<1	71	.13	6	.82	<3	2.21	.01	<.01	<2	5
L7+00E 6+87.5N	<1	5	6	17	<.3	3	<1	81	1.65	6	<5	<2	<2	13	.2	<2	2	124	.23	.003	1	25	.09	6	.52	<3	.71	.01	.01	<2	4
L7+00E 6+75N	1	34	5	28	<.3	9	4	113	8.96	3	<5	<2	<2	13	<.2	<2	5	211	.34	.011	<1	92	.25	9	.66	<3	4.90	.01	<.01	<2	5
L7+00E 6+62.5N	1	29	4	26	<.3	4	2	80	8.33	7	<5	<2	<2	12	<.2	<2	4	211	.31	.014	1	88	.16	7	.54	<3	3.89	.01	<.01	<2	3
L7+00E 6+50N	1	36	6	25	<.3	8	3	117	4.67	<2	<5	<2	<2	16	<.2	<2	3	125	.47	.008	2	86	.25	11	.48	<3	3.76	.01	<.01	<2	77
L7+00E 6+37.5N	1	18	7	24	<.3	5	2	82	5.09	3	<5	<2	<2	14	<.2	<2	4	195	.33	.007	1	67	.13	7	.70	<3	3.33	.01	<.01	<2	5
L7+00E 6+25N	1	26	10	17	<.3	4	2	72	8.57	6	<5	<2	<2	9	<.2	<2	3	277	.21	.007	1	71	.11	5	.69	<3	2.59	.01	<.01	<2	3
RE L7+00E 6+25N	1	27	11	18	<.3	3	1	71	9.00	4	<5	<2	<2	9	<.2	<2	3	292	.21	.008	1	76	.11	5	.72	<3	2.75	.01	<.01	<2	3
L7+00E 6+12.5N	1	41	3	28	<.3	15	6	148	8.44	7	<5	<2	<2	14	<.2	<2	<2	178	.45	.008	<1	108	.39	8	.58	<3	5.53	.01	<.01	<2	4
L7+00E 6+00N	1	68	3	31	<.3	16	6	154	7.60	6	5	<2	<2	15	.3	<2	<2	185	.42	.007	<1	113	.41	14	.56	<3	6.21	.01	.01	<2	4
L7+00E 5+87.5N	1	29	4	20	<.3	5	2	86	9.44	5	<5	<2	<2	10	<.2	<2	3	245	.21	.010	<1	108	.16	8	.63	<3	3.97	.01	<.01	<2	3
L7+00E 5+75N	1	67	<3	23	<.3	10	4	101	10.02	2	<5	<2	<2	14	.2	<2	<2	209	.24	.012	<1	149	.26	12	.53	<3	7.79	.01	<.01	<2	2
L7+00E 5+62.5N	1	46	6	33	<.3	13	5	138	5.97	3	<5	<2	<2	14	.2	<2	2	168	.33	.013	1	84	.32	15	.47	<3	4.72	.01	<.01	<2	2
L7+00E 5+50N	1	27	6	35	<.3	9	4	107	9.57	7	<5	<2	<2	12	<.2	<2	2	242	.30	.011	<1	98	.27	11	.74	<3	4.10	.01	<.01	<2	2
L7+00E 5+37.5N	1	51	<3	40	<.3	15	6	160	6.51	7	<5	<2	<2	17	.2	<2	2	170	.45	.009	<1	91	.44	14	.52	<3	4.97	.01	<.01	<2	3
L7+00E 5+25N	1	23	6	28	<.3	8	3	89	2.66	2	<5	<2	<2	15	.4	<2	4	199	.32	.012	1	65	.18	9	.64	<3	2.85	.01	<.01	<2	3
L7+00E 5+12.5N	1	25	7	107	<.3	4	<1	30	.91	3	<5	<2	<2	10	.3	<2	<2	65	.16	.055	5	19	.05	8	.10	3	.82	.02	<.01	<2	3
L7+00E 5+00N	1	58	4	29	<.3	13	5	126	2.67	4	<5	<2	<2	18	<.2	<2	<2	132	.50	.006	2	77	.32	15	.46	3	4.79	.01	<.01	<2	8
L7+00E 4+87.5N	1	41	<3	36	<.3	12	6	144	6.64	<2	<5	<2	<2	15	.2	<2	2	225	.45	.009	2	86	.38	11	.70	<3	5.52	.01	<.01	<2	3
L7+00E 4+75N	1	11	10	22	<.3	5	1	91	2.37	4	<5	<2	<2	16	.2	2	<2	178	.39	.005	1	33	.14	8	.66	<3	1.22	.01	<.01	<2	2
L7+00E 4+62.5N	1	24	10	99	<.3	3	<1	19	1.47	2	<5	<2	<2	10	<.2	<2	<2	44	.08	.044	5	15	.05	13	.10	3	.79	.02	.01	<2	2
L7+00E 4+50N	<1	1	7	7	<.3	<1	<1	124	.41	<2	<5	<2	<2	6	.2	<2	<2	70	.09	.002	2	12	.02	4	.45	3	.25	.01	<.01	<2	8
L7+00E 4+37.5N	1	27	7	30	<.3	8	4	97	7.89	4	<5	<2	<2	14	.3	<2	<2	250	.37	.010	<1	74	.16	8	.73	<3	2.40	.01	<.01	<2	2
L7+00E 4+25N	2	59	7	31	<.3	10	5	99	9.04	9	<5	<2	2	10	.4	2	5	285	.27	.015	2	105	.28	12	.88	<3	5.56	.01	.01	<2	5
L7+00E 4+12.5N	1	18	7	60	<.3	6	1	43	3.25	2	<5	<2	<2	8	<.2	<2	2	85	.13	.050	5	25	.07	10	.09	<3	1.28	.01	.03	<2	2
L7+00E 4+00N	1	11	9	40	<.3	3	<1	27	6.16	2	<5	<2	<2	10	.2	2	2	131	.13	.026	7	29	.05	11	.19	<3	1.36	.01	.03	<2	4
L7+50E 7+00N	1	37	9	21	<.3	8	4	108	8.03	3	<5	<2	<2	13	<.2	<2	<2	222	.29	.014	<1	82	.20	10	.61	<3	4.42	.01	<.01	<2	5
L7+50E 6+87.5N	1	47	4	29	<.3	8	3	79	11.84	5	<5	<2	<2	58	.2	<2	5	370	.15	.014	<1	71	.16	19	.86	<3	3.25	.01	<.01	<2	3
L7+50E 6+75N	1	17	6	21	<.3	4	2	76	7.88	3	<5	<2	<2	12	.4	3	2	297	.29	.006	<1	55	.11	8	.62	<3	1.87	.01	.01	<2	3
L7+50E 6+62.5N	1	17	8	17	<.3	4	1	68	7.79	3	<5	<2	<2	11	<.2	3	3	299	.27	.005	<1	77	.12	6	.62	<3	2.44	.01	<.01	<2	1
L7+50E 6+50N	<1	39	<3	30	<.3	12	5	135	8.70	<2	8	<2	2	15	.2	<2	<2	223	.36	.012	<1	102	.36	11	.67	<3	3.23	.01	.01	<2	2
L7+50E 6+37.5N	<1	28	3	19	<.3	5	2	88	9.98	<2	<5	<2	<2	11	<.2	<2	2	297	.28	.010	<1	107	.14	7	.68	<3	3.46	.01	.01	<2	3
L7+50E 6+25N	<1	21	8	24	<.3	6	3	89	8.78	<2	<5	<2	<2	13	<.2	<2	<2	352	.29	.006	1	73	.22	8	.76	<3	2.35	.01	<.01	<2	2
L7+50E 6+12.5N	1	23	10	26	<.3	7	2	100	5.99	3	<5	<2	2	13	<.2	2	3	190	.26	.009	2	66	.18	9	.52	<3	2.10	.01	<.01	<2	3
L7+50E 6+00N	1	34	7	25	<.3	4	2	61	8.02	<2	<5	<2	2	11	.2	<2	<2	277	.23	.016	<1	51	.12	8	.81	<3	2.14	.01	.01	<2	6
STANDARD C/AU-S	21	59	38	130	6.8	66	33	1041	4.09	40	22	7	41	52	18.9	17	20	57	.51	.093	41	62	.93	188	.09	26	1.90	.06	.15	11	45

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L7+50E 5+87.5N	1	24	7	17	.4	5	1	97	10.17	2	<5	<2	<2	10	.4	4	<2	306	.17	.009	1	75	.12	7	.71	<3	1.91	.01	.01	<2	3
L7+50E 5+75N	1	25	<3	30	<.3	6	2	81	10.86	<2	<5	<2	<2	10	.3	4	<2	297	.18	.009	<1	88	.13	6	.68	<3	2.13	.01	.01	<2	7
L7+50E 5+62.5N	2	28	<3	32	<.3	9	2	124	12.20	2	<5	<2	<2	12	.6	2	<2	285	.24	.011	1	119	.26	10	.72	<3	2.96	.01	.01	<2	4
L7+50E 5+50N	1	5	8	20	<.3	2	<1	66	2.24	<2	<5	<2	<2	15	<.2	<2	<2	144	.21	.005	2	24	.07	9	.56	<3	.87	.01	.01	<2	45
L7+50E 5+37.5N	2	50	5	36	<.3	16	5	163	7.65	6	<5	<2	<2	18	.8	<2	<2	188	.39	.011	2	101	.45	15	.55	<3	4.35	.01	.01	<2	5
L7+50E 5+25N	2	40	3	28	<.3	8	3	116	8.41	6	<5	<2	<2	14	.3	<2	2	227	.33	.010	1	114	.22	10	.66	<3	5.04	.01	.02	<2	4
L7+50E 5+12.5N	2	32	3	26	<.3	9	3	108	10.41	4	<5	<2	<2	12	.5	2	2	273	.29	.014	<1	128	.20	8	.70	<3	5.20	.01	.01	<2	3
L7+50E 5+00N	2	31	6	24	<.3	7	2	110	9.30	3	<5	<2	2	13	.5	5	<2	268	.37	.011	<1	108	.19	8	.72	<3	4.34	.01	.01	<2	4
L7+50E 4+87.5N	1	59	<3	32	<.3	13	4	149	8.14	<2	<5	<2	<2	17	.2	<2	<2	223	.43	.010	<1	106	.35	11	.68	<3	5.39	.01	.03	<2	4
L7+50E 4+75N	2	45	7	46	<.3	6	3	94	8.46	4	<5	<2	<2	15	.2	<2	<2	243	.31	.018	<1	76	.19	12	.71	<3	3.07	.01	.02	<2	5
L7+50E 4+62.5N	3	44	<3	33	<.3	10	4	124	7.83	3	<5	<2	<2	16	.5	<2	<2	232	.53	.008	1	117	.32	8	.69	<3	7.29	.01	.01	<2	4
L7+50E 4+50N	1	23	10	26	.4	5	1	100	5.42	<2	<5	<2	<2	16	.2	3	5	322	.37	.005	<1	59	.17	8	1.08	<3	2.16	.01	.02	<2	28
L7+50E 4+37.5N	2	34	<3	31	<.3	7	3	102	11.29	<2	<5	<2	<2	11	<.2	<2	<2	331	.27	.011	<1	92	.20	10	.83	<3	3.53	.01	.02	<2	5
L7+50E 4+25N	<1	11	6	162	<.3	2	<1	35	.49	2	<5	<2	<2	16	.3	<2	<2	12	.28	.041	2	5	.08	9	.04	3	.24	.03	.03	<2	<1
L7+50E 4+12.5N	<1	22	4	92	<.3	6	2	59	.98	3	<5	<2	<2	17	.3	<2	<2	37	.46	.050	6	11	.11	7	.03	<3	.80	.02	.02	<2	1
L7+50E 4+00N	2	36	<3	26	<.3	9	3	112	10.48	5	<5	<2	<2	13	.3	<2	<2	283	.36	.011	1	128	.25	7	.75	<3	4.99	.01	.01	<2	5
L8+00E 6+25N A	1	26	6	19	<.3	4	1	77	9.22	2	<5	<2	<2	9	<.2	2	<2	334	.15	.010	<1	93	.11	6	.72	<3	2.65	.01	.01	<2	5
L8+00E 6+25N B	1	17	11	20	<.3	2	<1	66	8.65	2	<5	<2	<2	14	<.2	3	<2	326	.17	.007	1	63	.08	5	.71	<3	1.66	.01	.01	<2	3
L8+00E 5+75N A	1	62	<3	26	<.3	11	3	125	9.22	3	<5	<2	<2	12	.2	2	<2	281	.29	.015	<1	111	.29	7	.69	<3	5.84	.01	.04	<2	6
L8+00E 5+75N B	2	38	3	17	<.3	4	1	72	11.74	3	<5	<2	<2	9	<.2	2	3	349	.17	.012	<1	113	.14	7	.85	<3	4.56	.01	.01	<2	4
L8+50E 7+00N	2	38	<3	42	<.3	15	5	148	2.68	2	<5	<2	<2	22	<.2	<2	2	121	.56	.011	5	63	.44	15	.51	<3	5.61	.02	.02	<2	3
L8+50E 6+87.5N	2	35	3	36	<.3	10	4	119	10.93	<2	<5	<2	<2	15	.2	2	<2	300	.32	.010	<1	126	.28	10	.79	<3	5.77	.01	.01	<2	4
L8+50E 6+75N	1	28	9	35	<.3	8	2	101	5.36	<2	<5	<2	<2	16	.2	<2	<2	244	.39	.009	2	61	.24	8	.83	<3	3.24	.01	.01	<2	4
RE L8+50E 6+75N	1	26	6	34	<.3	8	2	100	5.22	2	<5	<2	<2	16	.2	<2	<2	240	.38	.009	2	59	.24	8	.81	<3	3.15	.01	.02	<2	5
L8+50E 6+62.5N	2	25	5	36	<.3	10	4	136	4.73	2	<5	<2	<2	19	.4	<2	3	262	.54	.009	1	85	.36	11	.83	<3	3.73	.01	.01	<2	3
L8+50E 6+50N	2	26	<3	30	<.3	6	1	73	10.37	2	<5	<2	<2	10	<.2	<2	<2	309	.25	.009	<1	120	.17	6	.71	<3	4.61	.01	.01	<2	6
L8+50E 6+37.5N	2	34	<3	32	<.3	8	3	120	9.86	4	<5	<2	<2	14	<.2	<2	<2	237	.51	.011	1	92	.30	8	.72	<3	3.92	.01	.01	<2	3
L8+50E 6+25N	7	20	4	32	<.3	11	4	137	3.86	4	<5	<2	<2	19	<.2	<2	2	235	.65	.006	1	96	.36	11	.81	<3	4.42	.01	.01	<2	5
L8+50E 6+12.5N	2	46	3	36	<.3	8	2	95	5.52	4	<5	<2	<2	9	<.2	<2	2	164	.18	.020	2	86	.11	8	.37	<3	4.67	.01	.01	<2	5
L8+50E 6+00N	1	19	4	33	<.3	4	1	64	6.89	5	<5	<2	<2	11	<.2	2	<2	143	.25	.013	1	66	.15	7	.45	<3	3.66	.01	.02	<2	2
L8+50E 5+87.5N	2	33	3	28	<.3	9	3	107	8.72	<2	<5	<2	2	12	<.2	<2	<2	233	.35	.012	<1	113	.22	7	.68	<3	4.89	.01	.01	<2	14
L8+50E 5+75N	1	22	4	16	<.3	4	1	63	11.09	<2	<5	<2	<2	9	<.2	7	<2	316	.15	.008	1	80	.09	4	.70	<3	1.80	.01	.01	<2	3
L8+50E 5+62.5N	1	30	6	35	<.3	8	2	92	9.03	3	<5	<2	<2	12	<.2	5	<2	232	.26	.012	1	93	.20	9	.65	<3	3.44	.01	.02	<2	2
L8+50E 5+50N	1	17	4	19	<.3	3	<1	63	10.91	<2	<5	<2	<2	11	<.2	8	<2	278	.19	.008	<1	94	.10	5	.71	<3	1.99	.01	.02	<2	3
L8+50E 5+37.5N	1	35	<3	29	<.3	7	2	100	9.61	2	<5	<2	<2	12	<.2	<2	<2	246	.32	.008	<1	133	.22	7	.65	<3	6.21	.01	.02	<2	4
STANDARD C/AU-S	21	61	38	133	6.8	67	31	1057	4.16	38	17	7	42	55	19.9	18	20	59	.53	.097	45	63	.94	195	.09	26	1.97	.06	.16	10	55

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L8+50E 5+25N	1	44	3	29	<.3	10	3	116	7.53	9	<5	<2	3	15	.6	<2	<2	213	.32	.008	1	100	.28	11	.57	<3	4.35	.01	.01	<2	6
L8+50E 5+12.5N	1	48	6	37	<.3	17	5	183	7.25	5	<5	<2	2	16	.2	<2	<2	198	.46	.009	<1	116	.45	13	.56	<3	3.82	.01	.02	<2	6
L8+50E 5+00N	1	13	8	20	<.3	3	1	151	8.24	<2	<5	<2	<2	8	.4	<2	3	348	.14	.010	<1	53	.08	4	.68	<3	1.92	.01	.01	<2	4
L8+50E 4+87.5N	<1	4	4	24	<.3	3	<1	88	2.06	<2	<5	<2	<2	14	.2	2	2	125	.22	.004	1	16	.09	8	.39	<3	.65	.01	.01	<2	4
L8+50E 4+75N	1	47	6	30	<.3	14	4	128	7.01	6	<5	<2	2	13	.4	<2	<2	202	.28	.008	<1	99	.29	13	.52	<3	4.72	.01	.01	<2	4
L8+50E 4+62.5N	1	34	<3	26	<.3	16	5	136	6.03	2	<5	<2	<2	15	<.2	<2	<2	309	.37	.008	<1	110	.45	12	.71	<3	3.84	.01	.01	<2	6
L8+50E 4+50N	1	44	4	28	<.3	11	4	122	6.05	6	<5	<2	<2	13	.5	<2	<2	204	.37	.009	<1	76	.28	9	.52	<3	3.79	.01	.01	<2	2
L8+50E 4+37.5N	1	28	<3	18	<.3	4	1	79	10.20	3	<5	<2	<2	11	.8	<2	3	406	.24	.007	<1	90	.15	5	.72	<3	3.01	.01	<.01	<2	3
RE L8+50E 4+37.5N	1	29	<3	19	<.3	4	1	81	10.26	4	<5	<2	<2	11	.5	<2	<2	409	.24	.007	<1	91	.15	5	.73	<3	3.03	.01	.01	<2	4
L8+50E 4+25N	1	24	6	21	<.3	6	2	88	12.56	3	<5	<2	<2	9	.6	<2	<2	418	.21	.009	<1	89	.13	6	.87	<3	2.82	.01	.01	<2	5
L8+50E 4+12.5N	2	60	<3	28	<.3	13	5	113	5.58	8	<5	<2	2	14	.2	<2	2	249	.38	.008	1	125	.30	12	.66	<3	7.56	.01	<.01	<2	5
L8+50E 4+00N	1	30	<3	22	<.3	6	2	83	10.52	8	<5	<2	2	10	.8	<2	<2	274	.25	.011	1	100	.16	5	.64	<3	3.75	.01	<.01	<2	3
L9+00E 7+00N	1	34	3	24	<.3	5	1	71	11.65	6	<5	<2	2	10	.3	5	<2	393	.19	.009	<1	93	.13	7	.85	<3	2.80	.01	.01	<2	50
L9+00E 6+87.5N	1	29	<3	20	<.3	4	1	73	13.16	6	<5	<2	<2	10	.4	2	<2	622	.06	.009	<1	63	.08	6	1.08	<3	1.47	.01	.01	<2	35
L9+00E 6+75N	1	31	5	24	.3	5	1	79	12.12	<2	<5	<2	<2	19	1.5	<2	3	680	.11	.006	<1	61	.15	5	1.45	<3	1.20	.01	.01	<2	9
L9+00E 6+62.5N	<1	4	7	13	<.3	<1	<1	108	.66	<2	<5	<2	2	18	<.2	<2	2	141	.08	.002	<1	24	.02	6	.75	<3	.32	.01	.01	<2	10
L9+00E 6+50N	1	27	4	32	<.3	5	1	75	11.00	3	<5	<2	<2	14	.6	2	<2	497	.23	.005	<1	68	.14	8	1.07	<3	1.74	.01	.01	<2	3
L9+00E 6+37.5N	1	49	5	30	<.3	5	1	84	15.38	5	<5	<2	2	14	.7	<2	3	546	.13	.009	<1	78	.13	8	1.32	<3	2.89	.01	.01	<2	4
L9+00E 6+25N	<1	15	5	183	<.3	5	1	28	.51	<2	<5	<2	<2	16	<.2	<2	<2	17	.23	.052	2	7	.06	10	.04	<3	.58	.02	.02	<2	1
L9+00E 6+12.5N	<1	13	5	204	<.3	4	1	34	.29	<2	<5	<2	<2	13	<.2	<2	<2	7	.21	.065	3	4	.06	9	.02	3	.44	.02	.03	<2	1
L9+00E 6+00N	1	8	5	70	<.3	3	<1	28	2.31	2	<5	<2	<2	20	<.2	<2	<2	67	.29	.034	4	25	.05	11	.12	<3	1.21	.02	.02	<2	1
L9+00E 5+87.5N	1	29	3	35	<.3	18	6	169	5.14	7	<5	<2	<2	31	<.2	<2	3	110	.59	.015	6	47	.47	36	.30	<3	2.91	.02	.01	<2	3
L9+00E 5+75N	1	12	7	15	<.3	3	1	76	9.84	4	<5	<2	<2	11	.3	2	2	350	.18	.004	<1	63	.11	7	.77	<3	1.93	.01	.01	<2	2
L9+00E 5+62.5N	2	29	<3	22	<.3	2	1	27	8.54	5	<5	<2	<2	5	.4	<2	2	254	.05	.022	2	83	.07	4	.55	<3	6.84	.01	.02	<2	4
L9+00E 5+50N	1	62	<3	38	<.3	17	6	185	5.83	5	<5	<2	2	16	.2	<2	<2	180	.44	.008	1	88	.44	13	.52	<3	5.42	.01	.01	<2	3
L9+00E 5+37.5N	1	26	4	22	<.3	5	1	61	12.58	5	<5	<2	<2	8	.4	2	<2	359	.11	.011	<1	104	.10	5	.77	<3	3.21	.01	<.01	<2	2
L9+00E 5+25N	1	34	<3	22	<.3	8	3	175	6.60	5	<5	<2	2	10	.4	<2	4	338	.31	.005	<1	51	.20	4	.59	<3	1.98	.01	.01	<2	5
L9+00E 5+12.5N	1	12	6	16	<.3	2	<1	91	6.63	4	<5	<2	<2	7	.3	4	3	457	.10	.002	<1	30	.06	4	.70	<3	.61	.01	<.01	<2	13
L9+00E 5+00N	2	53	<3	35	<.3	10	4	126	6.52	4	<5	<2	<2	13	<.2	<2	2	192	.39	.008	2	83	.33	10	.60	<3	6.85	.01	.01	<2	5
L9+00E 4+87.5N	2	42	<3	30	<.3	13	5	125	9.07	6	<5	<2	<2	13	.5	<2	<2	246	.29	.012	<1	112	.31	11	.66	<3	5.65	.01	.01	<2	2
L9+00E 4+75N	1	33	<3	22	<.3	8	2	92	7.59	5	<5	<2	2	12	.2	3	<2	247	.20	.010	1	79	.15	8	.57	<3	3.04	.01	.02	<2	3
L9+00E 4+62.5N	1	33	5	24	<.3	7	2	91	10.17	6	<5	<2	2	12	.5	<2	<2	314	.25	.011	<1	99	.18	8	.71	<3	3.59	.01	.01	<2	3
L9+00E 4+50N	1	17	6	22	<.3	4	1	95	5.91	3	<5	<2	<2	15	<.2	2	3	201	.29	.007	1	62	.14	9	.54	<3	2.16	.01	.01	<2	2
L9+00E 4+37.5N	1	53	5	26	<.3	13	4	109	6.77	8	<5	<2	3	12	.6	2	2	195	.25	.012	1	118	.27	12	.53	<3	6.96	.01	.01	<2	2
L9+00E 4+25N	1	41	<3	30	<.3	11	4	146	7.66	6	<5	<2	2	17	.2	<2	3	223	.37	.007	1	113	.39	15	.58	<3	3.38	.01	.01	<2	4
STANDARD C/AU-S	20	58	40	128	7.0	66	32	1023	3.98	40	16	7	40	52	19.6	19	21	59	.51	.093	43	62	.91	185	.08	25	1.89	.06	.15	11	50

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L9+00E 4+12.5N	2	73	<3	34	<.3	22	6	146	3.57	5	<5	<2	<2	17	.3	<2	2	134	.43	.012	2	95	.42	15	.44	3	6.87	.01	.01	<2	4
L9+00E 4+00N	2	39	4	23	<.3	7	2	93	6.00	6	<5	<2	2	13	<.2	<2	<2	163	.32	.008	<1	102	.20	10	.55	<3	5.46	.01	.01	<2	3
L9+50E 7+00N	1	37	6	24	<.3	9	3	131	7.23	4	<5	<2	<2	12	.2	<2	<2	254	.33	.012	<1	96	.16	7	.67	<3	4.09	.01	<.01	<2	5
L9+50E 6+87.5N	2	46	<3	24	<.3	10	4	122	8.99	4	<5	<2	<2	11	<.2	2	<2	236	.41	.010	<1	105	.28	6	.66	<3	5.04	.01	<.01	<2	4
L9+50E 6+75N	2	42	5	25	<.3	7	3	116	9.17	3	<5	<2	<2	11	.2	2	2	244	.29	.011	<1	96	.21	6	.67	<3	3.93	.01	.01	<2	108 *
L9+50E 6+62.5N	1	26	9	20	<.3	3	1	105	15.21	3	<5	<2	<2	6	.2	6	<2	497	.05	.011	<1	90	.07	5	.97	<3	1.73	.01	<.01	<2	6
L9+50E 6+50N	1	70	4	36	<.3	5	1	94	18.08	<2	6	<2	<2	11	<.2	4	<2	558	.15	.016	<1	112	.14	7	1.43	<3	3.64	.01	.01	<2	6
L9+50E 6+37.5N	1	17	6	25	<.3	5	1	79	6.51	3	<5	<2	<2	13	<.2	3	3	291	.26	.005	<1	59	.13	9	.79	<3	1.99	.01	.01	<2	4
L9+50E 6+25N	3	32	5	33	<.3	6	1	63	5.43	4	<5	<2	<2	10	<.2	<2	2	163	.24	.013	4	79	.14	8	.51	<3	7.20	.01	<.01	<2	4
L9+50E 6+12.5N	1	41	6	29	<.3	11	5	126	7.09	7	<5	<2	<2	14	.2	<2	<2	203	.46	.007	<1	78	.28	8	.62	<3	3.71	.01	.01	<2	3
RE L9+50E 6+12.5N	1	43	3	31	<.3	11	5	133	7.54	4	<5	<2	<2	15	.2	2	<2	214	.49	.008	<1	84	.29	8	.66	<3	3.97	.01	.01	<2	12
L9+50E 6+00N	1	22	4	15	<.3	6	2	92	8.55	3	<5	<2	<2	11	<.2	2	<2	256	.30	.009	<1	89	.20	8	.69	<3	3.59	.01	.02	<2	4
L9+50E 5+87.5N	1	27	5	25	<.3	7	3	106	12.69	2	<5	<2	<2	13	<.2	5	<2	293	.34	.013	<1	101	.23	8	.76	<3	3.54	.01	.01	<2	3
L9+50E 5+75N	2	36	4	28	<.3	11	4	112	8.98	11	6	<2	<2	13	.2	<2	<2	215	.34	.008	<1	139	.28	10	.64	<3	6.84	.01	<.01	<2	3
L9+50E 5+62.5N	2	46	6	25	<.3	14	5	300	6.41	4	<5	<2	3	16	<.2	<2	<2	136	.35	.011	1	97	.34	14	.47	<3	6.31	.01	.01	<2	3
L9+50E 5+50N	1	30	5	24	<.3	10	3	128	6.10	3	<5	<2	2	13	<.2	<2	<2	168	.30	.010	<1	84	.25	10	.46	<3	3.95	.01	.01	<2	3
L9+50E 5+37.5N	2	37	6	30	<.3	12	5	152	6.68	4	5	<2	<2	13	<.2	<2	2	199	.47	.014	<1	80	.29	7	.56	<3	4.39	.01	.01	<2	5
L9+50E 5+25N	1	28	6	21	<.3	6	2	81	6.61	5	5	<2	<2	13	<.2	<2	2	227	.35	.009	<1	74	.21	7	.81	<3	3.58	.01	.01	<2	4
L9+50E 5+12.5N	1	18	<3	10	<.3	3	1	66	9.12	<2	<5	<2	<2	9	<.2	5	<2	328	.13	.005	<1	58	.07	5	.67	<3	1.38	.01	.01	<2	4
L9+50E 5+00N	2	28	5	16	<.3	5	2	68	10.45	3	<5	<2	2	8	<.2	<2	<2	300	.15	.010	<1	119	.14	7	.70	<3	5.24	.01	.01	<2	2
L9+50E 4+87.5N	1	17	6	24	<.3	5	2	89	9.25	<2	6	<2	<2	12	<.2	2	<2	308	.21	.005	<1	53	.17	8	.74	<3	1.86	.01	.01	<2	1
L9+50E 4+75N	1	11	4	126	.6	3	<1	32	1.00	2	<5	<2	<2	10	.4	2	<2	33	.18	.044	3	10	.06	7	.07	3	.53	.02	.02	<2	1
L9+50E 4+62.5N	1	28	10	12	<.3	4	1	84	2.71	2	5	<2	3	13	<.2	<2	4	167	.26	.006	2	66	.12	9	.59	<3	2.85	.01	.01	<2	8
L9+50E 4+50N	1	31	7	23	<.3	8	3	104	7.16	4	<5	<2	2	12	.3	2	<2	221	.24	.008	<1	101	.17	11	.58	<3	4.33	.01	<.01	<2	3
L9+50E 4+37.5N	1	16	6	15	.3	7	2	108	5.15	4	5	<2	2	12	<.2	5	<2	179	.32	.007	1	62	.28	7	.50	<3	2.63	.01	.01	<2	1
L9+50E 4+25N	1	30	4	26	<.3	13	5	153	6.13	4	5	<2	3	18	<.2	2	4	163	.41	.010	2	78	.46	13	.56	<3	4.00	.01	.01	<2	2
L9+50E 4+12.5N	2	34	5	19	<.3	8	4	107	11.03	7	<5	<2	<2	10	<.2	3	<2	272	.23	.010	<1	110	.30	8	.73	<3	4.23	.01	.01	<2	5
L9+50E 4+00N	1	17	6	30	.4	9	6	161	5.33	3	<5	<2	<2	21	<.2	2	<2	101	.44	.031	3	30	.26	16	.23	<3	1.84	.03	.03	<2	2
STANDARD C/AU-S	21	58	37	129	6.8	65	33	996	4.02	43	21	7	41	52	18.6	15	20	56	.51	.092	41	59	.91	191	.09	25	1.89	.06	.16	11	47

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

* Subject to reassay check

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L5+00E 4+50S	2	41	<3	21	<.3	12	5	139	5.04	8	<5	<2	<2	18	<.2	<2	2	188	.85	.010	2	84	.31	5	.69	<3	5.86	.01	<.01	<2	6
L5+00E 4+62.5S	2	40	<3	14	<.3	9	4	124	8.58	8	<5	<2	2	16	<.2	<2	<2	298	.58	.006	<1	137	.29	4	.81	<3	6.23	.01	<.01	<2	4
L5+00E 4+75S	2	16	<3	12	<.3	6	2	72	1.95	3	<5	<2	2	16	<.2	<2	<2	204	.49	.010	<1	88	.13	6	.88	<3	3.17	.01	<.01	<2	6
L5+00E 4+87.5S	2	59	<3	28	.3	26	9	212	3.22	7	<5	<2	<2	13	<.2	<2	<2	251	.90	.024	1	131	.65	11	.79	<3	7.89	.01	<.01	<2	4
L5+00E 5+00S	1	53	<3	21	.3	22	6	200	1.63	6	<5	<2	<2	29	<.2	<2	<2	93	1.49	.036	4	24	.54	18	.37	4	1.95	.02	<.01	<2	5
L5+00E 5+12.5S	<1	36	<3	8	<.3	11	<1	57	.60	2	<5	<2	<2	12	<.2	<2	<2	39	.47	.016	4	15	.10	19	.09	<3	1.00	.01	<.01	<2	2
L5+00E 5+25S	1	33	<3	35	<.3	20	9	295	3.07	5	<5	<2	<2	15	<.2	<2	2	113	1.46	.021	<1	36	.88	6	.50	3	1.85	.01	.01	<2	1
L5+00E 5+37.5S	1	27	<3	9	.3	12	<1	44	.63	3	<5	<2	<2	13	.3	2	2	38	.37	.016	2	17	.12	17	.11	<3	.90	.01	<.01	<2	38
L5+00E 5+50S	<1	23	3	9	.4	10	<1	37	.42	2	<5	<2	<2	9	<.2	2	2	45	.20	.016	3	25	.10	14	.17	<3	.91	.01	.01	<2	7
L5+00E 5+62.5S	1	63	<3	8	<.3	15	2	54	.66	4	<5	<2	<2	18	.3	<2	<2	37	.69	.018	3	16	.12	18	.08	<3	.96	.01	<.01	<2	2
L5+00E 5+75S	<1	38	<3	7	<.3	11	<1	72	.46	<2	<5	<2	<2	12	<.2	<2	<2	28	.56	.014	2	12	.11	14	.06	<3	.82	.01	<.01	<2	1
L5+00E 5+87.5S	<1	91	<3	7	<.3	8	<1	39	.38	3	<5	<2	<2	12	<.2	<2	<2	28	.49	.020	6	14	.06	14	.06	<3	1.23	.01	<.01	<2	1
L5+00E 6+00S	1	115	<3	7	<.3	9	<1	16	.27	3	<5	<2	<2	8	<.2	<2	2	29	.21	.035	7	19	.03	14	.05	<3	1.76	.01	<.01	<2	2
RE L5+00E 6+00S	<1	115	3	7	<.3	10	1	15	.27	3	<5	<2	<2	8	<.2	<2	<2	29	.21	.034	7	19	.03	14	.04	<3	1.75	.01	<.01	<2	3
L5+00E 6+12.5S	1	26	<3	15	<.3	12	5	135	2.51	8	<5	<2	3	20	<.2	<2	2	313	.70	.006	<1	91	.37	7	1.01	<3	3.85	.01	<.01	<2	5
L5+00E 6+25S	2	33	<3	16	<.3	12	5	138	5.54	9	<5	<2	2	15	<.2	<2	2	176	.64	.011	<1	110	.35	5	.58	<3	7.33	.01	<.01	<2	2
L5+00E 6+37.5S	2	72	<3	16	<.3	14	5	152	4.01	12	<5	<2	3	16	<.2	<2	3	140	.72	.017	<1	87	.39	5	.48	<3	7.07	.01	<.01	<2	5
L5+00E 6+50S	2	14	<3	8	<.3	6	1	70	8.66	7	<5	<2	2	9	.3	<2	<2	383	.25	.007	<1	108	.12	4	.77	<3	3.43	.01	.01	<2	9
L5+50E 4+50S	2	28	<3	13	<.3	9	3	91	12.28	8	<5	<2	2	12	<.2	<2	2	332	.38	.009	<1	128	.19	5	.89	<3	6.23	.01	<.01	<2	4
L5+50E 4+62.5S	1	18	3	14	<.3	8	3	117	2.21	5	<5	<2	<2	19	<.2	<2	<2	164	.59	.008	<1	62	.23	7	.70	<3	2.40	.01	<.01	<2	7
L5+50E 4+75S	1	21	<3	11	<.3	7	1	73	11.48	8	<5	<2	<2	12	<.2	<2	<2	314	.42	.011	<1	121	.15	4	.74	<3	3.49	.01	<.01	<2	3
L5+50E 4+87.5S	<1	8	<3	7	<.3	3	1	22	.56	<2	<5	<2	<2	12	<.2	<2	<2	11	.34	.022	1	5	.06	5	.02	<3	.41	.01	<.01	<2	1
L5+50E 5+00S	2	31	<3	16	<.3	13	5	152	4.15	9	<5	<2	2	16	<.2	2	3	123	.95	.011	<1	84	.37	4	.52	<3	7.61	.01	<.01	<2	3
L5+50E 5+12.5S	1	27	<3	16	<.3	11	4	145	5.81	9	<5	<2	3	18	.3	<2	2	186	.90	.008	<1	131	.35	5	.57	<3	5.69	.01	<.01	<2	4
L5+50E 5+25S	1	21	<3	9	<.3	4	1	63	11.78	9	<5	<2	<2	11	<.2	<2	2	362	.31	.005	<1	149	.13	4	.89	<3	6.01	.01	<.01	<2	10
L5+50E 5+37.5S	1	28	<3	9	<.3	6	2	69	9.86	7	<5	<2	<2	13	.5	<2	<2	376	.38	.006	<1	143	.14	4	.75	<3	5.84	.01	.01	<2	5
L5+50E 5+50S	1	14	<3	12	<.3	10	4	110	2.12	7	<5	<2	2	17	<.2	<2	<2	240	.74	.007	2	97	.27	4	.69	3	4.34	.01	<.01	<2	4
L5+50E 5+62.5S	1	22	<3	12	<.3	10	3	123	2.53	4	<5	<2	<2	19	<.2	<2	<2	190	.67	.007	1	64	.26	7	.59	<3	3.04	.01	.01	<2	4
L5+50E 5+75S	<1	27	5	9	<.3	13	<1	37	.55	2	<5	<2	<2	11	.2	<2	<2	44	.34	.015	3	18	.11	19	.11	<3	1.07	.01	<.01	<2	2
L5+50E 5+87.5S	1	27	<3	16	<.3	12	5	122	2.53	12	<5	<2	2	13	.2	2	<2	119	.59	.017	1	99	.35	5	.48	3	9.09	.01	.01	<2	5
L5+50E 6+00S	1	22	<3	11	<.3	8	2	88	11.21	6	<5	<2	<2	10	.2	<2	<2	279	.32	.007	<1	131	.22	4	.70	<3	5.64	.01	.01	<2	3
L5+50E 6+12.5S	1	40	5	7	<.3	11	3	99	1.31	8	6	<2	<2	16	<.2	<2	<2	37	.76	.019	4	12	.08	9	.03	<3	.90	.01	.01	<2	2
L5+50E 6+25S	1	147	3	11	<.3	8	1	18	.71	3	<5	<2	<2	10	<.2	<2	<2	29	.26	.031	6	19	.03	8	.05	<3	1.52	.01	<.01	<2	2
L5+50E 6+37.5S	1	54	<3	17	.3	15	6	131	1.86	8	<5	<2	2	18	<.2	2	<2	166	.69	.007	1	70	.34	10	.64	3	5.03	.01	.01	<2	6
L5+50E 6+50S	1	29	<3	16	<.3	10	4	130	9.50	6	<5	<2	2	16	<.2	<2	<2	302	.54	.006	<1	88	.27	5	.89	<3	3.09	.01	<.01	<2	18
STANDARD C/AU-S	20	57	37	124	6.8	68	32	977	3.87	44	18	7	41	50	18.0	15	20	55	.49	.089	40	50	.88	178	.08	25	1.79	.06	.14	11	49

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L6+50E 4+50S	1	44	5	78	.3	6	1	28	1.17	<2	<5	<2	<2	10	<.2	2	3	64	.31	.036	5	26	.09	6	.23	3	1.10	.01	.01	<2	1
L6+50E 4+62.5S	1	37	<3	30	<.3	12	9	155	8.74	8	<5	<2	<2	20	<.2	<2	<2	262	.95	.007	<1	96	.36	5	.89	<3	3.87	.01	<.01	<2	5
RE L6+50E 4+62.5S	1	36	3	30	<.3	12	9	157	8.41	5	<5	<2	2	20	<.2	<2	<2	255	.97	.007	1	94	.37	5	.87	<3	3.92	.01	.01	<2	5
L6+50E 4+75S	1	52	<3	30	<.3	7	6	110	10.79	7	<5	<2	2	14	.2	<2	<2	273	.55	.008	1	123	.26	5	.83	<3	4.81	.01	<.01	<2	3
L6+50E 4+87.5S	1	21	4	21	<.3	5	6	104	11.07	4	<5	<2	<2	15	<.2	<2	<2	407	.45	.009	<1	73	.22	4	1.07	<3	2.15	.01	.01	<2	885 *
L6+50E 5+00S	<1	10	7	24	<.3	4	5	96	10.54	5	<5	<2	2	12	<.2	<2	<2	393	.38	.005	<1	90	.13	4	.97	<3	2.26	.01	.01	<2	3
L6+50E 5+12.5S	<1	41	<3	27	<.3	13	8	146	8.55	6	<5	<2	<2	18	.4	<2	<2	268	.78	.010	<1	123	.28	6	.78	<3	4.86	.01	.01	<2	2
L6+50E 5+25S	1	7	7	23	<.3	3	4	95	2.78	4	<5	<2	<2	21	<.2	<2	<2	276	.55	.003	<1	48	.10	9	1.03	3	1.30	.01	.01	<2	6
L6+50E 5+37.5S	<1	30	<3	21	<.3	6	5	91	12.79	5	<5	<2	<2	14	<.2	<2	<2	385	.52	.008	<1	131	.15	3	1.12	<3	3.73	.01	.01	<2	3
L6+50E 5+50S	1	28	5	31	<.3	7	6	89	12.33	6	5	<2	2	13	.2	<2	<2	304	.38	.015	<1	111	.13	5	.88	<3	4.65	.01	.01	<2	2
L6+50E 5+62.5S	1	34	4	32	<.3	11	7	134	9.90	8	<5	<2	<2	15	<.2	<2	2	269	.59	.019	<1	105	.21	7	.77	<3	3.67	.01	.01	<2	8
L6+50E 5+75S	<1	16	6	23	<.3	7	5	128	12.21	5	<5	<2	2	11	<.2	<2	<2	511	.22	.008	<1	86	.11	5	1.03	<3	1.24	.01	.01	<2	6
L6+50E 5+87.5S	1	33	3	29	<.3	9	7	117	9.33	8	<5	<2	<2	16	<.2	<2	<2	262	.61	.011	<1	118	.23	6	.78	<3	5.30	.01	.01	<2	3
L6+50E 6+00S	<1	9	4	15	<.3	2	2	112	5.17	4	<5	<2	<2	10	<.2	3	<2	328	.21	.006	2	24	.04	4	.64	<3	.69	.01	.02	<2	8
L6+50E 6+12.5S	1	53	<3	32	<.3	9	6	123	9.17	<2	<5	<2	2	13	<.2	<2	2	230	.51	.015	1	103	.26	6	.66	<3	5.46	.01	.01	<2	3
L6+50E 6+25S	<1	19	6	25	<.3	8	5	118	10.51	3	<5	<2	3	14	<.2	<2	<2	495	.24	.008	<1	53	.11	6	1.07	<3	1.22	.01	.01	<2	9
L6+50E 6+37.5S	<1	1	9	22	<.3	2	2	103	2.16	2	<5	<2	<2	19	<.2	<2	<2	167	.26	.003	2	21	.05	6	.72	4	.69	.01	.02	<2	4
L6+50E 6+50S	1	19	5	32	<.3	8	6	125	6.89	3	<5	<2	<2	19	<.2	<2	<2	421	.56	.006	1	58	.29	8	.99	<3	2.52	.01	.02	<2	6
L7+00E 4+50S	1	9	8	24	<.3	5	5	104	3.90	5	<5	<2	<2	21	<.2	<2	<2	259	.69	.007	1	46	.16	7	.85	<3	1.85	.01	.01	<2	11
L7+00E 4+62.5S	1	11	7	51	<.3	10	8	142	4.95	5	<5	<2	<2	20	<.2	<2	<2	242	.86	.014	2	36	.36	11	.80	3	1.74	.01	.03	<2	6
L7+00E 4+75S	<1	6	4	18	<.3	3	4	90	4.24	2	<5	<2	<2	15	<.2	<2	<2	281	.40	.004	<1	29	.11	6	.88	<3	.96	.01	.02	<2	3
L7+00E 4+87.5S	<1	6	7	16	<.3	2	4	85	5.56	4	<5	<2	<2	11	<.2	<2	<2	415	.32	.003	<1	28	.07	5	.99	<3	1.00	.01	.01	<2	6
L7+00E 5+00S	<1	26	4	24	.3	6	5	78	12.65	5	<5	<2	<2	16	.3	<2	<2	491	.48	.008	<1	73	.14	5	1.25	<3	1.97	.01	.01	<2	5
L7+00E 5+12.5S	<1	20	<3	25	<.3	5	5	126	4.81	2	<5	<2	<2	22	<.2	<2	<2	255	.57	.006	1	53	.16	7	.87	<3	1.77	.01	.01	<2	9
L7+00E 5+25S	<1	18	<3	31	<.3	8	6	161	8.89	<2	<5	<2	<2	18	.2	<2	<2	323	.77	.017	<1	95	.21	6	.92	<3	2.37	.01	.01	<2	4
L7+00E 5+37.5S	<1	6	6	34	<.3	9	4	111	2.36	3	<5	<2	<2	16	<.2	2	<2	230	.87	.008	1	44	.22	5	.70	3	1.14	.01	.01	<2	8
L7+00E 5+50S	1	16	8	86	<.3	23	20	349	6.63	7	<5	<2	2	14	<.2	<2	<2	255	1.60	.035	<1	35	1.35	6	.89	4	2.02	.02	.04	<2	3
L7+00E 5+62.5S	1	17	6	25	<.3	4	5	102	13.10	4	<5	<2	2	12	<.2	<2	<2	351	.32	.026	<1	102	.12	7	.93	<3	2.90	.01	.01	<2	3
L7+00E 5+75S	<1	4	9	36	<.3	2	2	168	1.60	3	<5	<2	<2	6	<.2	<2	<2	166	.21	.004	2	40	.11	6	.66	4	.95	.01	.01	<2	9
L7+00E 5+87.5S	<1	21	<3	26	<.3	5	5	89	13.27	7	<5	<2	2	13	<.2	<2	<2	459	.32	.020	<1	109	.10	4	1.06	<3	2.28	.01	.01	<2	5
L7+00E 6+00S	<1	27	4	23	<.3	4	3	90	4.38	4	<5	<2	<2	16	<.2	<2	<2	249	.51	.009	2	41	.11	6	.72	<3	1.66	.01	.01	<2	4
L7+00E 6+12.5S	<1	18	6	16	<.3	3	4	80	11.68	6	<5	<2	2	11	<.2	<2	<2	467	.23	.007	<1	68	.06	3	.99	<3	1.59	.01	.01	<2	9
L7+00E 6+25S	<1	4	6	16	<.3	1	1	74	1.36	<2	<5	<2	<2	12	<.2	<2	<2	162	.19	.007	2	19	.04	5	.58	<3	.64	.01	.02	<2	12
L7+00E 6+37.5S	<1	37	5	21	<.3	6	4	104	10.87	5	<5	<2	2	14	<.2	<2	2	293	.36	.025	4	107	.15	7	.75	<3	3.44	.01	.02	<2	7
L7+00E 6+50S	<1	19	4	15	<.3	3	3	81	11.06	5	<5	<2	<2	11	<.2	2	<2	409	.15	.009	<1	64	.06	4	.82	<3	1.26	.01	.01	<2	3
STANDARD C/AU-S	20	58	38	129	7.1	67	33	1011	4.01	40	19	7	40	52	19.1	18	20	56	.51	.093	42	58	.92	187	.09	26	1.87	.06	.15	10	47

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

* Subject to reassay check

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L7+50E 4+50S	1	25	9	33	<.3	10	4	155	6.28	10	<5	<2	4	30	.5	3	<2	277	.84	.006	1	67	.33	8	.85	<3	2.39	.01	.02	<2	6
RE L7+50E 4+50S	1	27	8	34	<.3	8	4	158	6.49	7	<5	<2	2	31	.6	4	<2	284	.87	.005	<1	66	.33	8	.87	<3	2.46	.01	.01	<2	5
L7+50E 4+62.5S	1	20	9	36	<.3	8	3	116	6.95	10	<5	<2	2	24	<.2	<2	<2	362	.73	.008	1	87	.20	7	.98	<3	3.47	.01	.01	<2	34
L7+50E 4+75S	1	28	4	28	<.3	10	4	172	8.90	8	<5	<2	2	26	<.2	<2	4	282	.77	.015	<1	108	.27	7	.85	<3	3.74	.01	.01	<2	6
L7+50E 4+87.5S	<1	10	4	28	<.3	3	1	92	9.09	9	<5	<2	2	18	<.2	<2	<2	403	.36	.007	<1	43	.10	5	.89	<3	1.42	.01	.01	<2	7
L7+50E 5+00S	1	19	8	19	.3	4	2	99	10.86	7	<5	<2	4	15	<.2	3	<2	370	.33	.013	<1	78	.11	5	.94	<3	2.05	.01	.02	<2	43
L7+50E 5+12.5S	1	45	<3	32	<.3	11	5	162	8.59	<2	<5	<2	3	20	.3	<2	<2	240	.71	.013	1	125	.34	5	.73	<3	6.59	.01	.01	<2	5
L7+50E 5+25S	<1	25	3	42	<.3	5	2	104	9.75	11	<5	<2	3	17	.3	<2	<2	309	.46	.014	<1	102	.15	4	.87	<3	3.11	.01	.02	<2	5
L7+50E 5+37.5S	1	20	5	96	.3	4	<1	30	4.33	3	<5	<2	<2	11	<.2	3	3	104	.14	.040	4	26	.05	8	.29	<3	.97	.02	.03	<2	3
L7+50E 5+50S	2	36	<3	37	<.3	8	4	130	8.98	8	<5	<2	2	19	.2	<2	<2	245	.62	.017	1	121	.25	5	.74	<3	5.10	.01	.01	<2	2
L7+50E 5+62.5S	1	23	9	29	<.3	5	2	81	9.63	8	<5	<2	2	17	<.2	<2	<2	361	.43	.009	<1	108	.15	5	.91	<3	2.13	.01	.01	<2	33
L7+50E 5+75S	1	12	11	23	<.3	3	1	126	9.16	9	<5	<2	2	12	<.2	3	<2	471	.18	.005	<1	53	.10	5	.92	<3	1.14	.01	.01	<2	8
L7+50E 5+87.5S	1	32	6	20	.3	3	1	63	13.47	9	<5	<2	3	11	<.2	<2	<2	448	.21	.009	<1	92	.08	4	.88	<3	1.73	.01	.01	<2	46
L7+50E 6+00S	1	49	6	19	<.3	2	1	75	9.03	3	<5	<2	3	17	<.2	2	<2	360	.41	.004	<1	125	.15	4	.84	<3	3.81	.01	.01	<2	9
L7+50E 6+12.5S	1	44	<3	26	<.3	11	4	129	7.91	<2	<5	<2	3	17	.2	<2	<2	201	.62	.023	1	139	.31	4	.58	<3	6.82	.01	.02	<2	5
L7+50E 6+25S	<1	47	5	23	.3	4	2	115	11.51	5	<5	<2	2	13	<.2	<2	<2	544	.46	.016	<1	63	.15	3	.88	<3	1.52	.01	.01	<2	7
L7+50E 6+37.5S	1	33	8	40	.4	4	2	122	11.18	6	<5	<2	3	22	.7	<2	<2	472	.90	.022	<1	60	.15	6	.97	<3	1.73	.01	.02	<2	7
L7+50E 6+50S	1	87	<3	34	<.3	6	2	78	12.51	2	<5	<2	3	14	<.2	<2	<2	316	.38	.014	<1	123	.18	5	.75	<3	5.69	.01	.01	<2	4
L8+50E 4+50S	<1	17	8	36	.4	10	5	203	5.89	3	<5	<2	<2	22	.3	4	<2	201	.78	.013	1	36	.37	7	.70	<3	1.69	.01	.02	<2	8
L8+50E 4+62.5S	<1	3	7	18	<.3	3	<1	105	.70	3	<5	<2	<2	13	<.2	<2	2	66	.14	.005	2	16	.05	6	.45	3	.46	.01	.01	<2	30
L8+50E 4+75S	1	36	7	36	<.3	6	3	155	10.49	6	<5	<2	2	23	<.2	<2	<2	300	.62	.011	<1	101	.21	7	.88	<3	3.07	.01	.01	<2	5
L8+50E 4+87.5S	1	17	10	22	<.3	2	1	58	12.64	7	<5	<2	3	16	.2	<2	<2	403	.25	.006	<1	79	.10	5	.96	<3	2.81	.01	<.01	<2	5
L8+50E 5+00S	<1	24	6	28	<.3	8	3	126	5.49	<2	<5	<2	3	28	.2	2	<2	268	.91	.011	1	94	.23	9	.88	<3	4.22	.01	.01	<2	8
L8+50E 5+12.5S	<1	13	10	14	<.3	4	2	98	7.03	5	<5	<2	3	17	.2	<2	<2	356	.33	.003	1	52	.16	4	.83	<3	1.48	.01	.02	<2	11
L8+50E 5+25S	1	40	<3	26	<.3	10	4	142	8.91	<2	<5	<2	2	19	<.2	<2	<2	286	.62	.016	1	140	.25	5	.79	<3	5.83	.01	.01	<2	19
L8+50E 5+37.5S	1	19	9	15	<.3	3	2	91	10.89	5	<5	<2	3	10	<.2	<2	<2	396	.17	.009	<1	80	.08	5	.82	<3	1.68	.01	.01	<2	5
L8+50E 5+50S	2	28	4	26	<.3	6	3	97	10.96	6	<5	<2	3	14	<.2	<2	<2	305	.39	.016	2	114	.16	5	.74	<3	6.19	.01	<.01	<2	4
L8+50E 5+62.5S	1	24	4	28	<.3	7	2	109	7.56	6	<5	<2	<2	17	.3	<2	<2	239	.51	.009	<1	116	.21	5	.62	<3	4.24	.01	.01	<2	36
L8+50E 5+75S	1	26	6	29	<.3	8	3	128	5.33	2	<5	<2	<2	20	.2	<2	<2	183	.72	.008	1	95	.29	6	.63	<3	4.38	.01	.01	<2	6
L8+50E 5+87.5S	1	18	7	27	<.3	5	2	80	11.20	8	<5	<2	<2	13	<.2	<2	2	398	.28	.007	<1	90	.10	4	.74	<3	2.01	.01	<.01	<2	3
L8+50E 6+00S	<1	44	<3	28	<.3	9	4	129	8.58	<2	<5	<2	<2	15	<.2	<2	<2	224	.60	.009	1	155	.33	4	.62	<3	6.94	.01	<.01	<2	5
L8+50E 6+12.5S	1	41	6	26	<.3	8	3	98	10.56	<2	<5	<2	3	17	.3	<2	<2	330	.46	.011	<1	137	.21	6	.74	<3	4.91	.01	.01	<2	4
L8+50E 6+25S	<1	4	7	22	<.3	1	<1	43	.58	3	<5	<2	<2	10	.2	<2	<2	71	.05	.004	2	20	.03	5	.43	<3	.55	.01	.02	<2	14
L8+50E 6+37.5S	<1	31	8	15	<.3	2	1	60	11.69	2	<5	<2	2	12	.2	<2	<2	387	.16	.009	<1	109	.08	4	.87	3	2.59	.01	.01	<2	4
L8+50E 6+50S	<1	13	10	15	<.3	3	1	92	7.49	2	<5	<2	<2	13	<.2	2	<2	472	.21	.007	<1	42	.06	4	.86	<3	.78	<.01	.01	<2	6
STANDARD C/AU-S	21	61	36	136	7.4	67	30	1053	4.18	46	17	8	42	55	19.0	19	22	59	.48	.096	44	64	.95	183	.09	27	2.02	.06	.16	10	48

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Kamaka Resources Ltd. File # 95-4191 Page 1

6074 - 45A Ave, Delta BC V4K 1M7

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L0+50W 2+50N	<1	57	8	52	<.3	14	3	131	16.58	4	<5	<2	3	14	.2	<2	<2	448	.22	.011	3	139	.33	14	.97	<3	5.14	<.01	.02	<2	6
L0+50W 2+37.5N	<1	33	5	48	<.3	17	4	171	7.53	5	<5	<2	2	21	.2	<2	<2	222	.85	.009	2	97	.41	11	.76	<3	3.93	.02	.02	2	6
L0+50W 2+25N	1	26	<3	28	<.3	10	<1	159	7.27	3	5	<2	2	18	<.2	2	<2	270	.75	.004	2	102	.27	11	.84	<3	3.38	.01	.02	<2	3
L0+50W 2+12.5N	1	50	9	32	<.3	13	3	153	10.51	8	<5	<2	2	15	.2	<2	<2	253	.69	.012	2	174	.30	14	.78	3	7.31	.01	.01	<2	3
L0+50W 2+00N	<1	33	10	30	<.3	10	2	157	10.30	11	<5	<2	2	16	.3	<2	<2	295	.85	.004	2	111	.32	11	1.05	<3	4.12	.01	.01	<2	1
L0+50W 1+87.5N	<1	32	12	36	<.3	13	2	178	11.22	6	<5	<2	<2	17	.2	2	<2	283	.96	.009	2	123	.39	9	.90	<3	3.44	.02	.02	<2	3
L0+50W 1+75N	<1	38	<3	26	<.3	9	2	166	7.55	<2	<5	<2	2	19	.2	<2	<2	181	.78	.008	3	154	.32	11	.61	<3	5.25	.02	.01	<2	5
L0+50W 1+62.5N	1	45	11	29	<.3	12	3	234	11.16	<2	<5	<2	3	11	.2	<2	<2	238	.65	.016	3	200	.33	14	.76	<3	9.21	.01	.02	<2	4
L0+50W 1+50N	<1	30	10	34	<.3	7	<1	134	13.07	3	6	<2	2	11	.2	<2	<2	315	.57	.014	2	144	.23	6	.88	<3	4.01	.01	.02	<2	2
L0+50W 1+37.5N	<1	19	10	27	<.3	2	<1	117	15.23	6	<5	<2	3	7	.2	2	<2	450	.19	.013	2	101	.07	14	1.04	<3	1.98	.01	.02	<2	4
L0+50W 1+25N	<1	18	16	19	<.3	3	<1	77	14.67	8	<5	<2	3	10	<.2	3	<2	416	.23	.011	2	123	.08	11	1.03	<3	3.42	.01	.02	<2	4
L0+50W 1+12.5N	<1	34	6	29	<.3	7	<1	95	14.63	<2	7	<2	2	10	.2	<2	<2	346	.35	.017	2	169	.15	6	.93	<3	5.29	.01	.02	<2	5
L0+50W 1+00N	1	18	8	30	<.3	7	<1	130	8.33	<2	<5	<2	2	15	.2	<2	<2	251	.54	.015	3	117	.16	12	.77	<3	4.17	.01	.02	<2	6
L0+50W 0+87.5N	<1	57	15	36	<.3	8	1	130	11.45	2	<5	<2	2	14	.3	<2	<2	299	.57	.021	2	120	.18	11	.88	<3	5.52	.01	.02	<2	2
L0+50W 0+75N	<1	59	6	46	<.3	13	4	193	9.68	3	<5	<2	<2	18	.2	<2	5	237	.81	.012	2	124	.35	9	.77	<3	6.12	.02	.02	<2	24
L0+50W 0+62.5N	<1	31	12	28	<.3	8	1	142	12.10	14	<5	<2	3	16	.2	<2	<2	301	.62	.014	2	160	.25	11	.91	<3	4.48	.01	.02	2	5
L0+50W 0+50N	<1	36	7	25	<.3	9	1	163	12.91	7	<5	<2	3	17	.2	<2	<2	283	.85	.007	2	181	.37	9	.91	<3	6.00	.01	.01	<2	3
L0+50W 0+37.5N	<1	21	3	25	<.3	3	<1	98	12.68	2	5	<2	2	11	.2	2	<2	393	.31	.010	1	86	.06	6	1.02	<3	1.80	.01	.01	<2	11
L0+50W 0+25N	<1	68	<3	27	<.3	12	<1	129	11.99	8	<5	<2	2	11	.2	<2	<2	246	.60	.020	2	142	.23	14	.80	<3	6.67	.01	.02	<2	4
RE L0+50W 0+25N	1	69	5	30	<.3	8	1	143	11.71	5	<5	<2	3	12	.2	3	<2	240	.68	.021	2	140	.25	3	.79	3	6.77	.01	.01	<2	4
L0+50W 0+12.5N	<1	12	10	26	<.3	1	<1	84	8.15	<2	<5	<2	<2	12	.2	<2	<2	364	.30	.005	2	53	.07	12	.95	3	1.55	.01	.02	<2	4
L0+50W 0+00	<1	91	<3	27	<.3	4	<1	122	15.94	3	<5	<2	3	13	.2	<2	<2	349	.50	.019	3	140	.20	14	1.01	<3	5.24	.01	.02	<2	3
L0+50W 0+12.5S	<1	31	4	23	<.3	4	<1	399	17.97	3	<5	<2	3	12	.2	<2	<2	477	.21	.016	2	110	.05	11	1.06	<3	2.64	.01	.02	<2	6
L0+50W 0+25S	<1	35	10	31	<.3	7	<1	130	11.87	3	5	<2	2	20	.2	<2	<2	346	.70	.014	2	110	.18	6	1.00	<3	4.32	.01	.01	3	13
L0+50W 0+37.5S	<1	40	4	36	<.3	9	2	138	7.25	<2	<5	<2	2	23	<.2	3	<2	217	.79	.010	4	98	.23	16	.90	3	4.96	.01	.01	<2	7
L0+50W 0+50S	<1	32	9	39	<.3	13	4	198	6.92	<2	<5	<2	<2	27	<.2	2	<2	222	1.20	.007	4	100	.34	11	.94	4	4.32	.02	.01	<2	27
L0+50W 0+62.5S	<1	30	7	38	<.3	10	3	175	6.40	<2	<5	<2	2	21	<.2	2	<2	224	.98	.008	3	107	.36	12	.84	<3	4.88	.01	.01	<2	45
L0+50W 0+75S	<1	37	<3	34	<.3	12	2	153	10.86	<2	<5	<2	2	15	.2	<2	<2	250	.81	.016	2	135	.28	8	.83	<3	5.40	.01	.01	2	4
L0+50W 0+87.5S	1	21	9	68	.3	13	7	227	2.98	2	<5	<2	<2	26	<.2	3	<2	132	.69	.022	3	40	.62	14	.56	<3	2.19	.02	.01	2	6
L0+50W 1+00S	<1	57	10	31	<.3	10	2	187	9.31	<2	5	<2	2	19	.2	<2	<2	235	.92	.011	2	144	.30	6	.81	3	6.22	.01	.01	<2	6
L0+50W 1+12.5S	<1	25	6	21	<.3	7	<1	162	12.98	7	<5	<2	2	7	<.2	<2	2	496	.10	.008	2	75	.05	14	.95	<3	1.20	<.01	.01	<2	4
L0+50W 1+25S	<1	43	3	25	.3	7	<1	114	14.69	3	<5	<2	3	12	.2	<2	<2	403	.43	.018	2	136	.13	8	1.12	<3	4.44	.01	.03	<2	10
L0+50W 1+37.5S	<1	42	6	29	.4	4	<1	104	14.45	2	<5	<2	2	15	<.2	4	<2	550	.37	.008	1	76	.11	3	1.26	<3	1.85	.01	.02	<2	7
L0+50W 1+50S	<1	28	7	21	<.3	4	<1	117	14.72	6	<5	<2	2	14	.2	<2	<2	486	.50	.005	2	122	.15	11	1.00	<3	2.70	.01	.01	<2	2
L0+50W 1+62.5S	<1	26	7	83	<.3	6	1	33	.52	<2	<5	<2	<2	13	<.2	<2	<2	32	.19	.031	3	34	.06	11	.12	<3	1.12	.01	.01	<2	3
STANDARD C/AU-S	20	60	39	131	6.4	67	33	1129	4.24	40	19	6	38	52	17.9	19	18	60	.53	.094	40	61	.94	194	.10	28	2.01	.06	.16	11	54

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.
- SAMPLE TYPE: SOIL AU* - IGNITED, AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED.
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 12 1995 **DATE REPORT MAILED:** Oct 25/95 **SIGNED BY** ....D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L0+50W 1+75S	1	14	7	35	<.3	8	14	622	6.85	<2	9	<2	<2	24	<.2	<2	<2	149	1.24	.007	2	42	.40	5	.49	6	2.22	.02	.01	<2	4
L0+50W 1+87.5S	<1	14	<3	34	<.3	12	7	204	2.55	<2	<5	<2	<2	26	<.2	<2	<2	108	1.21	.013	4	54	.47	9	.50	4	3.22	.01	.01	<2	5
L0+50W 2+00S	<1	7	5	98	.3	1	1	66	1.24	4	<5	<2	<2	13	<.2	<2	<2	11	.49	.028	2	7	.08	9	.04	3	.33	.01	.02	<2	1
L0+50W 2+12.5S	<1	10	5	146	<.3	4	1	125	.50	4	<5	<2	<2	12	<.2	<2	<2	10	.21	.045	2	6	.05	12	.02	3	.41	.01	.03	<2	<1
L0+50W 2+25S	<1	12	7	91	<.3	6	1	33	.15	7	<5	<2	<2	12	<.2	2	<2	5	.16	.021	2	4	.04	9	.01	4	.45	.01	.01	<2	1
L0+50W 2+37.5S	1	48	<3	30	<.3	6	2	148	7.02	4	<5	<2	2	19	<.2	<2	<2	216	.84	.013	4	105	.28	7	.79	5	6.01	.01	.01	<2	4
L0+50W 2+50S	<1	24	7	22	.4	1	<1	94	10.33	<2	9	<2	2	14	.3	<2	<2	331	.39	.012	2	99	.09	7	.84	4	2.93	.01	.01	<2	3
L0+50W 2+62.5S	1	30	4	19	<.3	1	<1	97	12.68	<2	7	<2	2	13	.3	<2	<2	249	.50	.009	1	121	.14	7	.76	3	3.96	.01	.01	<2	52
L0+50W 2+75S	<1	23	7	18	<.3	2	<1	105	11.72	<2	8	<2	2	14	<.2	<2	<2	310	.34	.008	2	102	.11	7	.82	<3	3.13	.01	.01	<2	14
L0+50W 2+87.5S	<1	42	10	30	<.3	8	1	118	7.83	<2	<5	<2	2	11	<.2	<2	<2	171	.55	.016	3	100	.21	9	.62	3	6.38	.01	.01	<2	5
L0+50W 3+00S	1	43	3	29	<.3	8	2	151	7.83	<2	6	<2	2	16	<.2	<2	<2	191	.72	.012	2	96	.24	7	.63	3	4.90	.01	.01	<2	4
L0+50E 2+50N	1	14	15	23	<.3	<1	<1	77	12.76	<2	10	<2	3	12	.2	<2	<2	377	.30	.006	2	88	.07	7	.93	3	1.91	.01	.02	<2	5
L0+50E 2+37.5N	1	25	7	23	<.3	3	<1	109	8.79	<2	<5	<2	<2	15	.2	<2	<2	222	.54	.013	2	94	.15	9	.70	<3	2.97	.01	.01	<2	6
L0+50E 2+25N	1	24	7	22	<.3	4	1	111	5.98	<2	5	<2	<2	18	<.2	<2	<2	210	.54	.004	2	65	.18	10	.73	<3	3.06	.01	.01	<2	4
L0+50E 2+12.5N	1	24	6	21	<.3	2	<1	94	10.96	<2	10	<2	2	13	<.2	<2	<2	292	.44	.008	2	80	.15	10	.70	<3	3.10	.01	.02	<2	4
L0+50E 2+00N	1	48	13	28	<.3	11	5	403	11.78	<2	8	<2	2	17	.3	<2	<2	184	.57	.013	5	87	.23	11	.45	<3	5.36	.01	.02	<2	8
L0+50E 1+87.5N	1	29	8	25	<.3	15	6	174	2.57	4	<5	<2	<2	22	<.2	<2	<2	107	1.02	.007	4	68	.40	7	.57	3	4.39	.01	.01	2	13
L0+50E 1+75N	1	22	5	67	.3	4	1	52	.57	4	5	<2	<2	13	<.2	<2	2	46	.37	.036	8	39	.07	12	.07	<3	1.92	.01	.01	<2	4
L0+50E 1+62.5N	<1	31	7	26	<.3	11	2	160	6.60	<2	<5	<2	<2	17	<.2	<2	<2	169	.91	.009	2	89	.32	11	.63	<3	3.70	.01	.01	<2	4
RE L0+50E 1+12.5N	<1	36	3	28	<.3	7	1	136	9.20	2	<5	<2	2	16	<.2	<2	<2	203	.73	.010	2	120	.27	7	.72	<3	4.94	.01	.01	<2	4
L0+50E 1+50N	<1	13	7	21	<.3	3	<1	97	12.61	<2	5	<2	<2	11	.3	<2	<2	333	.25	.004	2	57	.11	9	.80	<3	1.44	.01	.02	<2	5
L0+50E 1+37.5N	1	19	7	20	<.3	<1	<1	81	15.44	<2	7	<2	2	10	.3	<2	7	323	.26	.005	2	100	.10	9	.78	<3	2.10	.01	.01	<2	4
L0+50E 1+25N	<1	16	12	25	<.3	3	<1	98	8.53	<2	<5	<2	<2	15	<.2	<2	2	280	.50	.007	2	74	.13	9	.79	3	2.21	.01	.02	<2	6
L0+50E 1+12.5N	1	38	3	28	<.3	11	2	137	9.34	<2	7	<2	2	16	<.2	<2	<2	206	.76	.010	2	123	.28	7	.72	<3	5.08	.01	.01	<2	7
L0+50E 1+00N	1	17	9	18	<.3	2	<1	93	8.78	<2	7	<2	2	11	<.2	<2	<2	306	.23	.004	2	57	.10	9	.70	<3	1.65	.01	.02	<2	7
L0+50E 0+87.5N	<1	9	12	21	<.3	2	<1	93	5.57	<2	<5	<2	<2	25	<.2	<2	<2	323	.39	<.001	3	50	.07	9	.80	4	1.67	.01	.01	<2	8
L0+50E 0+75N	<1	12	4	17	<.3	<1	<1	73	12.04	<2	<5	<2	<2	14	.3	<2	<2	441	.30	.003	2	50	.05	7	.89	<3	1.16	<.01	.02	<2	9
L0+50E 0+62.5N	1	34	6	27	.3	6	<1	87	10.81	<2	8	<2	2	16	.2	<2	<2	268	.55	.009	2	88	.14	5	.79	<3	3.78	.01	.01	<2	28
L0+50E 0+50N	<1	46	<3	28	<.3	12	4	147	8.25	<2	<5	<2	2	19	.2	<2	4	134	.96	.011	4	114	.39	11	.64	<3	6.08	.01	.01	<2	4
L0+50E 0+37.5N	1	25	4	25	.3	4	2	103	8.66	<2	6	<2	3	14	<.2	4	<2	214	.49	.018	2	95	.15	5	.68	<3	4.34	.02	.02	2	2
L0+50E 0+25N	<1	25	9	18	<.3	2	<1	57	14.48	<2	6	<2	2	7	<.2	<2	<2	392	.22	.006	1	75	.07	9	.77	<3	2.14	.01	.02	<2	4
L0+50E 0+12.5N	<1	14	5	23	<.3	4	1	70	5.79	<2	<5	<2	2	12	<.2	<2	<2	142	.37	.009	2	37	.10	12	.55	<3	1.80	.01	.02	<2	2
L0+50E 0+00	<1	22	7	25	<.3	4	1	104	7.04	<2	<5	<2	<2	18	.2	<2	<2	210	.62	.007	2	45	.13	11	.74	<3	1.62	.01	.02	<2	8
L0+50E 0+12.5S	<1	78	4	23	<.3	4	<1	91	14.01	<2	9	<2	2	12	.2	<2	<2	308	.32	.012	1	112	.13	7	.80	<3	2.87	.01	.02	<2	4
L0+50E 0+25S	<1	94	8	18	<.3	3	<1	90	13.96	<2	7	<2	2	13	<.2	<2	<2	310	.37	.009	1	121	.12	2	.85	<3	3.01	.01	.01	<2	5
STANDARD C/AU-S	20	58	39	126	6.0	66	31	1029	4.04	38	21	5	36	51	17.5	18	19	54	.52	.090	38	60	.90	180	.09	25	1.93	.06	.15	9	51

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L0+50E 0+37.5S	1	70	7	26	.3	10	<1	131	10.69	4	<5	<2	2	15	.2	<2	6	277	.69	.013	2	149	.27	12	.86	<3	5.51	.01	.02	3	19
L0+50E 0+50S	1	48	15	22	<.3	2	<1	106	12.63	<2	<5	<2	<2	13	<.2	<2	<2	340	.45	.010	3	113	.18	7	.90	<3	3.37	.01	.02	<2	11
L0+50E 0+62.5S	1	30	9	24	<.3	6	<1	104	5.74	<2	<5	<2	<2	21	<.2	2	<2	284	.72	.007	4	103	.19	7	1.00	<3	3.47	.01	.01	3	4
L0+50E 0+75S	1	26	17	28	<.3	7	<1	126	10.07	<2	6	<2	2	14	.2	<2	<2	300	.57	.009	3	86	.22	7	.88	<3	2.58	.01	.02	2	3
L0+50E 0+87.5S	1	42	12	33	.6	6	<1	104	15.67	<2	5	<2	2	11	<.2	<2	<2	389	.34	.016	3	121	.18	9	1.02	<3	3.48	.01	.02	2	3
RE L0+50E 1+00S	1	37	3	36	.4	7	<1	111	12.69	<2	6	<2	2	12	<.2	<2	<2	320	.56	.016	3	123	.19	9	.92	<3	5.31	.01	.02	3	8
L0+50E 1+00S	1	39	8	36	.3	4	<1	115	12.55	<2	5	<2	2	13	.2	<2	<2	318	.63	.015	3	125	.20	7	.90	<3	5.51	.01	.02	3	4
L0+50E 1+12.5S	<1	26	12	21	.4	4	<1	88	11.80	<2	5	<2	2	11	.2	<2	<2	333	.31	.008	3	74	.13	6	.89	<3	2.09	.01	.02	2	5
L0+50E 1+25S	<1	18	9	33	.3	13	4	211	7.92	<2	<5	<2	<2	23	.2	<2	<2	243	1.15	.007	3	47	.57	9	.67	3	2.20	.01	.02	2	4
L0+50E 1+37.5S	<1	38	5	56	.4	24	13	353	8.61	<2	<5	<2	<2	24	<.2	<2	<2	287	1.41	.010	4	64	1.12	4	.72	<3	3.65	.01	.01	3	7
L0+50E 1+50S	1	54	8	36	<.3	11	5	272	11.62	<2	<5	<2	2	16	.2	<2	<2	276	.75	.015	2	138	.34	11	.85	<3	5.38	.01	.02	3	4
L0+50E 1+62.5S	1	23	8	21	<.3	4	<1	121	15.22	<2	7	<2	2	8	.2	<2	<2	502	.19	.005	2	66	.05	3	.99	<3	1.68	<.01	.01	2	231*
L0+50E 1+75S	1	28	13	20	<.3	1	<1	96	14.07	<2	<5	<2	2	7	.2	<2	<2	559	.20	.006	2	88	.08	6	1.00	5	1.89	<.01	.01	2	10
L0+50E 1+87.5S	<1	18	9	21	<.3	6	1	104	5.13	<2	<5	<2	<2	14	.2	4	<2	312	.68	.005	3	65	.20	5	.93	<3	2.76	.01	.01	2	4
L0+50E 2+00S	1	31	6	101	<.3	6	1	32	.36	<2	<5	<2	<2	10	<.2	3	4	25	.18	.065	3	21	.05	8	.05	<3	.93	.01	.03	<2	1
L1+50W 2+00N	<1	29	7	22	.5	5	<1	87	11.21	<2	<5	<2	2	9	<.2	3	<2	377	.36	.007	2	119	.15	8	.91	<3	3.42	.01	.02	4	5
L1+50W 1+87.5N	<1	29	8	23	2.2	5	<1	88	12.44	<2	<5	<2	2	11	.2	<2	<2	351	.40	.013	2	126	.11	10	.95	<3	3.73	.01	.01	2	6
L1+50W 1+75N	<1	11	8	18	<.3	2	<1	70	8.75	<2	<5	<2	<2	9	<.2	3	<2	518	.26	.006	2	61	.10	5	.87	<3	1.18	<.01	.02	2	10
L1+50W 1+62.5N	<1	7	12	27	<.3	3	<1	66	1.23	<2	<5	<2	<2	10	<.2	2	2	167	.13	.003	2	24	.03	5	.66	5	.50	.01	.02	2	8
L1+50W 1+50N	<1	58	<3	41	<.3	17	7	262	4.39	2	<5	<2	<2	19	<.2	<2	6	116	1.42	.015	6	68	.69	7	.56	6	4.88	.01	.01	4	8
L1+50W 1+37.5N	<1	41	9	36	.4	6	<1	128	15.75	<2	7	<2	2	11	<.2	<2	<2	461	.39	.007	2	111	.23	7	1.09	<3	3.04	.01	.02	2	3
L1+50W 1+25N	<1	46	5	33	<.3	2	<1	93	18.59	<2	9	<2	2	12	<.2	<2	<2	539	.25	.007	2	125	.11	5	1.17	<3	2.35	.01	.02	2	5
L1+50W 1+12.5N	1	154	4	41	.5	10	3	163	9.96	<2	<5	2	<2	16	.2	2	<2	283	.66	.026	6	140	.40	4	.91	6	8.89	.01	.01	5	9
L1+50W 1+00N	1	25	11	21	<.3	1	<1	57	19.73	<2	6	<2	2	7	.2	<2	<2	611	.09	.007	2	116	.03	7	1.17	<3	1.93	<.01	.02	<2	5
L1+50W 0+87.5N	1	39	9	26	<.3	7	1	130	10.84	<2	<5	<2	2	16	.2	<2	<2	300	.78	.013	3	145	.21	7	.88	3	4.77	.01	.02	3	3
L1+50W 0+75N	1	24	14	19	.3	<1	<1	75	14.35	<2	5	<2	2	10	.2	<2	<2	511	.27	.006	2	96	.07	7	1.24	<3	2.27	.01	.02	3	9
L1+50W 0+62.5N	1	37	9	28	.3	8	2	150	9.92	<2	<5	<2	<2	12	.2	<2	<2	294	.56	.015	3	115	.19	2	.83	<3	5.25	<.01	.01	3	6
L1+50W 0+50N	1	31	11	26	<.3	5	<1	136	12.09	<2	5	<2	2	13	.2	<2	<2	276	.70	.011	2	139	.24	4	.83	<3	4.22	.01	.01	2	4
L1+50W 0+37.5N	<1	21	3	27	<.3	5	<1	113	7.70	<2	<5	<2	<2	15	<.2	2	<2	351	.67	.007	2	63	.19	9	.92	4	2.08	.01	.03	2	9
L1+50W 0+25N	<1	35	8	25	<.3	5	<1	121	12.56	<2	<5	<2	2	12	.2	<2	<2	359	.48	.008	2	128	.19	1	.93	<3	3.17	.01	.03	3	3
L1+50W 0+12.5N	1	59	6	31	.3	8	1	146	10.70	<2	<5	<2	2	14	.2	<2	2	278	.59	.011	2	133	.26	4	.74	<3	4.77	.01	.01	3	6
L1+50W 0+00	<1	22	8	105	<.3	7	2	51	2.34	<2	<5	<2	<2	11	<.2	4	<2	51	.26	.042	3	16	.06	6	.07	3	.83	.01	.02	<2	1
L1+50W 0+12.5N	1	30	4	38	.3	9	2	155	6.30	<2	<5	<2	<2	17	.2	2	<2	288	.59	.006	3	114	.32	6	.85	<3	3.50	.01	.02	4	9
L1+50W 0+25N	1	32	5	34	<.3	8	<1	143	9.56	<2	<5	<2	2	17	.2	<2	2	286	.64	.010	2	124	.21	1	.78	<3	3.42	.01	.01	2	3
L1+50W 0+37.5N	<1	24	7	25	<.3	2	<1	88	11.24	<2	<5	<2	2	12	.2	2	<2	363	.49	.013	2	115	.11	<1	.87	<3	3.62	.01	.01	3	8
STANDARD C/AU-S	21	60	39	128	6.4	65	32	1002	4.06	36	18	7	38	51	18.3	20	22	65	.49	.094	40	60	.89	185	.09	28	1.91	.07	.15	12	46

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

* Subject to reassay check

Kamaka Resources Ltd. FILE # 95-4191

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L1+50W 0+50S	<1	21	4	17	<.3	4	<1	76	12.93	<2	8	<2	2	9	.2	<2	<2	378	.11	.013	3	99	.03	1	.82	4	2.76	.01	.02	<2	6
L1+50W 0+62.5S	<1	36	8	30	<.3	11	4	160	10.78	7	<5	<2	2	18	.2	<2	<2	301	.78	.014	3	120	.24	7	.87	<3	5.25	.01	.02	2	12
L1+50W 0+75S	<1	31	3	26	<.3	7	1	165	11.04	<2	5	<2	2	16	<.2	<2	<2	303	.55	.008	2	90	.19	5	.87	<3	2.50	.01	.02	<2	3
L1+50W 0+87.5S	<1	43	3	38	<.3	8	4	176	9.24	5	<5	<2	2	15	<.2	<2	<2	254	.59	.011	3	88	.29	5	.84	<3	3.15	.01	.02	<2	6
L1+50W 1+00S	<1	4	10	17	<.3	1	1	109	1.16	2	<5	<2	<2	13	<.2	2	2	90	.17	.001	3	32	.04	3	.70	<3	.96	.01	.02	2	20
L1+50W 1+12.5S	<1	26	4	22	.3	4	<1	103	14.83	3	7	<2	2	12	<.2	<2	<2	351	.37	.006	2	111	.12	3	.95	<3	2.62	.01	.01	2	4
L1+50W 1+25S	<1	29	7	33	.4	8	3	164	11.84	<2	6	<2	2	17	<.2	<2	<2	270	.72	.008	2	94	.21	6	.89	<3	2.39	.01	.02	<2	3
L1+50W 1+37.5S	<1	12	3	49	<.3	8	4	209	3.53	<2	<5	<2	<2	19	<.2	<2	<2	107	.77	.017	3	38	.19	6	.53	3	1.25	.02	.03	<2	3
L1+50W 1+50S	<1	23	3	35	<.3	12	4	164	10.62	4	<5	<2	2	16	.2	<2	<2	239	.60	.011	3	94	.26	3	.75	<3	3.49	.01	.02	<2	4
L1+50W 1+62.5S	<1	17	3	40	<.3	8	2	168	10.46	<2	<5	<2	2	20	<.2	2	6	266	.90	.008	3	69	.26	4	.84	<3	2.16	.01	.02	<2	11
L1+50W 1+75S	<1	42	6	41	<.3	12	6	219	9.12	7	<5	<2	2	20	.2	<2	<2	214	1.04	.009	3	126	.52	8	.81	3	3.82	.01	.02	2	4
L1+50W 1+87.5S	<1	14	4	30	<.3	4	<1	104	12.19	3	<5	<2	2	9	.2	<2	<2	369	.27	.006	2	74	.09	4	.89	<3	2.08	.01	.01	<2	6
L1+50W 2+00S	<1	34	4	19	<.3	8	1	110	14.09	5	<5	<2	3	11	.2	3	<2	321	.51	.015	3	145	.19	8	.87	<3	4.38	.01	.02	<2	2
L1+50W 2+12.5S	<1	40	6	33	<.3	11	5	178	8.55	6	<5	<2	2	19	<.2	3	2	238	1.02	.016	3	109	.35	8	.79	4	3.50	.01	.02	<2	6
L1+50W 2+25S	<1	44	13	27	<.3	8	2	133	11.40	3	9	<2	2	14	.2	<2	<2	295	.70	.016	2	159	.26	<1	.92	<3	6.63	.01	.01	2	13
L1+50W 2+37.5S	<1	36	5	22	<.3	5	1	98	14.44	3	7	<2	2	13	.2	<2	<2	357	.45	.010	2	127	.13	2	1.06	<3	2.61	.01	.01	<2	4
L1+50W 2+50S	<1	25	4	32	<.3	9	3	147	10.24	8	<5	<2	<2	17	<.2	3	<2	287	.72	.015	2	87	.22	8	.81	<3	2.60	.01	.02	<2	34
L1+50W 2+62.5S	<1	18	4	26	<.3	6	<1	80	14.17	<2	6	<2	2	11	<.2	<2	<2	466	.27	.005	2	113	.07	9	1.14	<3	2.15	.01	.01	<2	5
RE L1+50W 2+62.5S	<1	22	4	29	<.3	8	1	143	9.83	<2	<5	<2	2	16	<.2	<2	<2	279	.68	.013	2	82	.19	7	.78	<3	2.39	.01	.02	<2	13
L1+50W 2+75S	<1	23	3	19	<.3	5	1	121	10.79	3	<5	<2	2	11	<.2	<2	5	322	.41	.006	2	91	.08	<1	.78	4	2.10	.01	.01	<2	4
L1+50W 2+87.5S	<1	27	9	22	<.3	7	<1	129	13.29	9	<5	<2	2	15	.2	<2	4	318	.62	.008	2	128	.15	7	.88	<3	2.99	.01	.02	<2	14
L1+50W 3+00S	<1	44	9	29	<.3	13	5	177	8.37	7	<5	<2	2	17	.2	4	<2	208	.98	.011	2	114	.29	9	.67	<3	6.43	.01	.01	2	3
L1+50E 2+50N	<1	9	8	20	<.3	2	1	96	9.06	2	<5	<2	<2	14	.2	<2	2	324	.41	.008	2	70	.09	7	.68	4	1.69	.01	.02	2	11
L1+50E 2+37.5N	<1	17	7	27	<.3	11	5	204	7.72	<2	<5	<2	2	20	.3	<2	<2	240	1.13	.004	3	108	.44	5	.77	<3	3.76	.01	.02	2	4
L1+50E 2+25N	<1	14	7	30	<.3	4	<1	101	10.47	2	<5	<2	2	14	<.2	5	<2	304	.57	.010	3	102	.14	8	.77	3	2.85	.01	.02	<2	4
L1+50E 2+12.5N	<1	10	6	35	.3	3	<1	104	11.28	<2	<5	<2	<2	16	<.2	<2	<2	384	.68	.005	2	62	.15	9	.82	<3	1.08	.01	.03	<2	5
L1+50E 2+00N	<1	18	9	22	<.3	3	1	97	12.26	<2	5	<2	2	11	<.2	2	4	359	.37	.014	2	101	.11	6	.92	<3	2.82	.01	.02	<2	16
L1+50E 1+87.5N	<1	27	9	19	<.3	5	1	110	9.76	2	<5	<2	2	15	.2	<2	<2	402	.30	.004	2	87	.15	10	1.14	<3	2.11	.01	.01	<2	6
L1+50E 1+75N	<1	29	10	28	<.3	11	4	145	10.04	3	<5	<2	2	15	.2	<2	<2	217	.78	.012	2	116	.26	10	.73	<3	4.27	.01	.01	<2	3
L1+50E 1+62.5N	<1	36	8	22	<.3	8	<1	106	12.17	7	<5	<2	2	11	.2	<2	2	275	.45	.007	2	161	.18	10	.72	<3	6.23	.01	.01	2	4
L1+50E 1+50N	1	23	6	16	<.3	<1	<1	68	17.12	<2	<5	<2	3	9	<.2	<2	<2	467	.15	.008	2	91	.06	10	.91	<3	2.40	.01	.03	<2	4
L1+50E 1+37.5N	<1	46	5	54	<.3	236	27	194	15.37	<2	<5	<2	2	6	<.2	2	<2	260	.21	.022	1	146	1.87	4	.47	<3	3.68	.04	.04	<2	<1
L1+50E 1+25N	<1	25	7	30	<.3	11	<1	101	16.92	<2	6	<2	2	7	.2	<2	<2	408	.20	.014	2	97	.11	2	.78	<3	1.97	.01	.02	<2	3
L1+50E 1+12.5N	<1	15	3	22	<.3	4	<1	104	10.32	<2	<5	<2	2	8	<.2	2	<2	305	.17	.007	2	60	.05	8	.61	<3	1.45	.01	.01	<2	7
L1+50E 1+00N	<1	28	13	21	<.3	5	2	111	9.35	<2	<5	<2	<2	13	<.2	<2	<2	273	.48	.007	4	97	.15	4	.75	<3	4.05	.01	.01	<2	11
STANDARD C/AU-S	20	59	37	130	6.4	63	32	1105	4.09	43	18	6	35	49	17.4	17	19	59	.52	.095	39	58	.91	171	.09	24	1.91	.06	.16	11	51

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L1+50E 0+87.5N	<1	20	<3	18	.7	4	<1	115	7.22	<2	<5	<2	3	6	<.2	2	<2	461	.08	.003	1	46	.03	10	.96	<3	.69	.01	.01	3	8
RE L1+50E 0+87.5N	1	20	6	22	.4	3	<1	128	7.44	2	<5	<2	<2	7	<.2	2	<2	471	.10	.002	2	48	.03	5	.99	3	.78	.01	.01	3	7
L1+50E 0+75N	<1	11	7	17	<.3	1	<1	63	1.13	5	<5	<2	<2	12	<.2	2	8	103	.22	.002	3	32	.05	12	.68	<3	1.24	.01	.01	2	4
L1+50E 0+62.5N	2	30	3	27	.4	7	<1	126	12.17	4	<5	<2	3	12	.2	<2	<2	295	.56	.011	2	116	.21	12	.90	<3	5.38	.01	.02	2	4
L1+50E 0+50N	<1	17	<3	24	.5	4	<1	93	10.42	<2	<5	<2	2	12	<.2	<2	<2	376	.23	.007	1	66	.07	12	.93	3	1.62	.01	.01	2	4
L1+50E 0+37.5N	1	35	4	24	.3	6	<1	160	10.18	<2	<5	<2	2	14	<.2	<2	<2	309	.65	.013	1	101	.25	9	.88	<3	3.84	.01	.02	<2	4
L1+50E 0+25N	1	35	<3	25	.3	4	<1	134	11.70	<2	<5	<2	3	12	<.2	<2	<2	316	.62	.009	1	146	.23	8	.86	3	5.39	.01	.02	<2	2
L1+50E 0+12.5N	1	36	10	22	.6	4	<1	95	11.89	<2	<5	<2	3	12	.2	5	<2	324	.37	.014	1	120	.12	7	.90	4	4.79	.01	.02	3	1
L1+50E 0+00	1	52	11	30	<.3	12	1	163	9.19	<2	<5	<2	2	13	<.2	4	<2	231	.82	.007	2	152	.34	9	.74	<3	6.84	.01	.01	4	5
L1+50E 0+12.5S	1	62	16	32	<.3	13	3	148	3.84	4	<5	<2	<2	16	<.2	<2	4	169	.77	.012	3	109	.36	9	.62	<3	6.87	.01	.01	<2	4
L1+50E 0+25S	1	29	3	25	.4	<1	<1	95	14.95	<2	<5	<2	2	8	.2	3	<2	513	.29	.007	1	79	.09	9	1.00	<3	1.96	.01	.02	2	2
L1+50E 0+37.5S	1	37	7	39	.5	8	<1	137	10.76	9	<5	<2	2	17	.2	2	<2	345	.75	.007	2	85	.25	12	1.01	4	3.04	.01	.02	2	2
L1+50E 0+50S	1	34	8	26	<.3	4	<1	112	9.42	<2	<5	<2	2	15	<.2	3	3	393	.51	.005	5	101	.15	11	1.15	3	3.33	.01	.01	3	5
L1+50E 0+62.5S	1	40	5	23	<.3	9	1	154	9.90	<2	<5	<2	2	18	<.2	<2	<2	239	.60	.009	2	109	.29	6	.74	<3	3.65	.01	.01	2	5
L1+50E 0+75S	1	33	3	19	.3	3	<1	66	15.95	5	<5	<2	2	9	.2	<2	<2	399	.26	.004	1	150	.08	9	.97	<3	5.01	.01	.01	3	5
L1+50E 0+87.5S	1	50	3	33	<.3	15	3	200	9.72	<2	<5	<2	2	20	.2	<2	<2	249	.98	.006	2	120	.45	6	.86	3	5.44	.01	.01	2	41
L1+50E 1+00S	1	65	6	34	<.3	9	2	137	9.51	<2	<5	<2	2	15	<.2	<2	<2	308	.81	.011	7	80	.26	9	1.16	<3	4.59	.01	.01	<2	6
L1+50E 1+12.5S	2	50	10	26	<.3	10	<1	118	10.47	<2	<5	<2	2	11	<.2	<2	<2	256	.52	.012	2	142	.22	9	.77	3	7.59	.01	.02	2	3
L2+50W 2+00N	1	20	5	8	<.3	3	<1	87	10.10	<2	<5	<2	<2	7	<.2	2	<2	401	.15	.010	1	58	.04	6	.77	<3	1.47	.01	.02	<2	5
L2+50W 1+87.5N	1	54	9	25	<.3	12	4	219	9.20	<2	<5	<2	<2	7	.2	2	<2	260	.58	.009	3	54	.46	6	.47	<3	1.66	.01	.04	<2	3
L2+50W 1+75N	1	61	21	27	<.3	15	3	271	9.15	3	<5	<2	2	13	.2	<2	<2	281	.62	.012	1	144	.39	8	.86	<3	7.52	.01	.02	2	4
L2+50W 1+62.5N	1	49	12	26	.3	11	<1	150	10.20	6	<5	<2	2	12	.2	<2	<2	299	.53	.015	1	146	.26	6	.87	<3	6.51	.01	.01	2	4
L2+50W 1+50N	1	57	3	41	.3	10	<1	135	15.94	4	<5	<2	2	13	<.2	<2	<2	350	.53	.013	1	158	.23	11	.96	<3	4.35	.01	.01	<2	4
L2+50W 1+37.5N	<1	41	3	38	<.3	12	<1	182	12.18	<2	<5	<2	2	15	.2	<2	6	371	.86	.013	1	120	.32	8	.94	<3	4.75	.01	.02	<2	3
L2+50W 1+25N	1	38	11	30	<.3	7	<1	100	12.54	6	<5	<2	2	19	.2	<2	<2	447	.45	.006	1	102	.16	11	1.07	<3	3.12	.01	.02	<2	7
L2+50W 1+12.5N	1	36	9	23	<.3	4	<1	97	14.92	<2	<5	<2	2	11	.2	<2	<2	390	.43	.008	1	144	.11	3	1.07	<3	3.97	.01	.01	<2	7
L2+50W 1+00N	1	29	3	27	<.3	3	<1	86	14.38	<2	<5	<2	2	11	.2	<2	<2	403	.44	.015	1	101	.12	8	1.03	<3	2.59	.01	.01	<2	5
L2+50W 0+87.5N	1	23	8	32	<.3	9	<1	147	8.71	<2	<5	<2	<2	16	.2	<2	<2	282	.86	.016	2	97	.20	8	.86	<3	3.96	.01	.01	2	3
L2+50W 0+75N	1	22	9	20	<.3	<1	<1	90	9.92	<2	<5	<2	<2	11	.2	<2	<2	438	.39	.003	2	85	.08	8	1.10	<3	2.79	.01	.01	2	3
L2+50W 0+62.5N	1	45	5	32	.5	7	<1	147	12.26	3	<5	<2	<2	15	.2	<2	<2	394	.68	.008	1	81	.24	13	1.01	<3	2.49	.01	.01	3	4
L2+50W 0+50N	1	26	6	32	<.3	9	2	187	11.17	6	<5	<2	2	21	<.2	<2	<2	376	1.02	.004	2	88	.40	6	1.10	<3	3.35	.01	.02	<2	13
L2+50W 0+37.5N	1	31	<3	27	<.3	6	<1	112	11.58	<2	<5	<2	2	14	.2	<2	<2	378	.47	.008	2	100	.14	8	1.06	<3	2.84	.01	.02	<2	652
L2+50W 0+25N	1	31	5	27	<.3	4	<1	127	11.91	4	<5	<2	<2	14	.3	2	<2	348	.52	.007	1	112	.15	10	1.00	4	2.84	.01	.01	2	7
L2+50W 0+12.5N	1	38	<3	26	<.3	10	<1	120	11.34	3	<5	<2	2	11	.2	<2	<2	308	.53	.013	1	147	.19	10	.81	<3	6.27	.01	.02	2	4
L2+50W 0+00	<1	20	9	23	.4	2	<1	78	9.56	<2	<5	<2	<2	13	.2	2	<2	380	.38	.006	1	72	.08	8	.95	3	1.62	.01	.02	2	9
STANDARD C/AU-S	20	58	36	124	5.9	66	31	1074	4.06	41	17	6	35	50	17.3	16	15	59	.50	.091	38	61	.87	181	.10	30	1.88	.06	.15	9	50

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L2+50W 0+12.5S	<1	32	16	17	<.3	7	1	117	13.45	3	<5	<2	2	12	<.2	4	2	456	.27	.008	3	81	.08	7	.86	<3	1.94	.01	.01	<2	8
L2+50W 0+25S	1	34	5	28	.3	8	1	125	10.38	6	<5	<2	2	16	.7	2	<2	329	.72	.011	2	112	.22	9	.87	<3	3.89	.01	.01	<2	7
L2+50W 0+37.5S	1	36	<3	28	<.3	8	1	136	11.20	<2	<5	<2	3	17	<.2	<2	<2	333	.77	.012	3	134	.24	7	.92	<3	5.21	.01	.01	<2	3
RE L2+50W 0+37.5S	<1	36	5	27	<.3	8	1	131	11.05	<2	<5	<2	3	17	<.2	<2	6	329	.75	.011	3	132	.23	5	.91	<3	5.06	.02	.01	<2	5
L2+50W 0+50S	1	43	3	33	<.3	10	4	168	8.99	6	<5	<2	2	19	.3	<2	<2	292	.97	.014	3	99	.37	9	.81	<3	4.09	.01	.01	<2	4
L2+50W 0+62.5S	<1	13	13	46	<.3	<1	<1	54	27.19	<2	<5	<2	3	9	<.2	2	11	486	.16	.018	2	32	.05	9	.34	7	.75	.01	.03	<2	2
L2+50W 0+75S	<1	11	15	27	<.3	<1	<1	50	17.54	<2	<5	<2	3	10	<.2	2	9	273	.12	.011	2	31	.03	5	.46	<3	.65	.01	.03	<2	3
L2+50W 0+87.5S	1	53	3	32	<.3	10	3	156	8.85	<2	<5	<2	2	17	<.2	<2	<2	232	.90	.011	3	125	.30	4	.70	<3	5.92	.01	.01	<2	6
L2+50W 1+00S	1	58	6	37	.4	16	5	197	8.09	<2	<5	<2	2	19	.4	<2	<2	244	1.06	.010	6	114	.48	<1	.89	<3	7.08	.02	.01	<2	8
L2+50W 1+12.5S	<1	44	8	37	<.3	6	<1	89	13.70	<2	<5	<2	3	13	.4	<2	7	475	.49	.008	4	139	.15	7	1.33	<3	4.78	.02	.01	<2	3
L2+50W 1+25S	1	39	<3	38	<.3	10	2	139	12.64	2	<5	<2	2	16	.2	<2	4	347	.71	.009	2	109	.28	7	.91	3	3.67	.02	.02	<2	5
L2+50W 1+37.5S	1	64	<3	36	<.3	14	4	144	6.10	<2	<5	<2	2	13	.4	<2	<2	170	.79	.017	4	109	.36	8	.60	4	9.69	.01	.01	<2	6
L2+50W 1+50S	1	60	<3	40	<.3	19	6	207	7.15	6	<5	<2	2	18	.4	<2	<2	179	1.04	.011	3	119	.53	8	.64	3	8.39	.01	.01	<2	5
L2+50W 1+62.5S	<1	28	5	35	<.3	8	3	171	6.07	<2	<5	<2	<2	25	<.2	2	<2	264	.95	.006	3	52	.34	6	.85	<3	2.32	.01	.01	<2	11
L2+50W 1+75S	<1	23	7	21	<.3	4	1	96	5.06	3	<5	<2	2	18	<.2	4	<2	290	.55	.010	3	51	.09	4	.88	<3	2.07	.01	.01	<2	7
L2+50W 1+87.5S	<1	29	5	27	.3	4	2	107	11.36	5	<5	<2	2	19	<.2	<2	<2	327	.64	.007	2	107	.18	6	.86	<3	3.35	.01	.02	<2	7
L2+50W 2+00S	<1	21	8	19	<.3	2	<1	91	11.19	<2	<5	<2	2	14	.3	5	<2	413	.25	.003	2	80	.06	2	1.04	<3	1.40	.02	.02	<2	4
L2+50W 2+12.5S	<1	30	<3	34	<.3	10	4	149	7.48	3	6	<2	2	17	.5	<2	<2	210	.74	.014	3	126	.28	6	.68	<3	6.72	.01	.01	<2	3
L2+50W 2+25S	1	61	10	37	<.3	11	3	206	11.92	5	<5	<2	3	17	<.2	<2	3	267	.98	.008	2	126	.39	6	.87	<3	5.45	.01	.01	<2	3
L2+50W 2+37.5S	<1	34	8	33	.3	9	1	157	11.05	<2	<5	<2	2	19	.3	<2	<2	350	.85	.009	2	97	.25	6	1.00	<3	2.75	.01	.02	<2	4
L2+50W 2+50S	<1	9	9	14	<.3	4	<1	102	1.47	<2	<5	<2	<2	18	<.2	5	<2	127	.45	.001	2	42	.09	8	.91	3	1.03	.02	.01	<2	15
L2+50E 2+50N	<1	28	8	25	<.3	7	1	124	11.21	<2	<5	<2	2	13	.2	<2	<2	407	.55	.005	2	146	.30	6	.87	4	3.23	.02	.01	<2	64
L2+50E 2+37.5N	1	31	12	19	<.3	4	<1	73	12.41	<2	<5	<2	2	7	<.2	2	<2	424	.22	.009	3	82	.05	4	.68	<3	2.27	.01	.02	<2	6
L2+50E 2+25N	<1	24	4	42	<.3	15	5	225	6.44	<2	<5	<2	<2	24	<.2	<2	3	198	1.40	.005	4	96	.59	6	.82	4	3.88	.01	.01	<2	5
L2+50E 2+12.5N	<1	18	16	26	<.3	4	<1	66	14.35	<2	5	<2	3	10	.4	2	9	495	.27	.004	2	103	.09	4	1.13	<3	2.49	.01	.02	<2	8
L2+50E 2+00N	<1	21	<3	32	<.3	11	2	168	8.68	2	7	<2	2	19	<.2	<2	<2	337	1.09	.004	3	97	.44	4	1.13	6	3.79	.01	.02	<2	4
L2+50E 1+87.5N	<1	20	13	17	<.3	1	<1	69	16.85	<2	<5	<2	2	9	<.2	2	5	516	.24	.006	2	120	.12	6	.85	<3	2.33	.01	.02	<2	4
L2+50E 1+75N	<1	33	8	28	<.3	4	<1	90	12.57	<2	<5	<2	2	10	.5	<2	5	353	.41	.011	2	100	.12	3	.71	<3	3.06	.01	.02	<2	5
L2+50E 1+62.5N	<1	34	9	35	<.3	9	2	136	8.48	<2	5	<2	2	15	.2	<2	<2	308	.76	.005	2	109	.34	8	.89	<3	4.67	.01	.01	<2	6
L2+50E 1+50N	1	30	3	19	<.3	3	<1	70	14.76	<2	<5	<2	3	10	<.2	<2	<2	440	.26	.011	2	138	.07	8	.80	3	3.82	.01	.02	<2	2
L2+50E 1+37.5N	<1	17	<3	57	<.3	5	1	27	2.18	<2	8	<2	<2	7	<.2	3	4	39	.20	.030	3	17	.04	6	.07	<3	.83	.01	.01	<2	2
L2+50E 1+25N	<1	47	<3	25	<.3	9	2	112	8.18	7	6	<2	2	11	.5	<2	<2	246	.65	.008	2	139	.26	5	.67	3	7.42	.01	.01	<2	4
L2+50E 1+12.5N	<1	25	9	15	.3	5	<1	86	12.95	<2	5	<2	2	9	.2	<2	<2	431	.32	.002	2	103	.11	5	.85	<3	2.50	.01	.01	<2	27
L2+50E 1+00N	<1	38	10	17	<.3	5	<1	81	11.93	<2	5	<2	3	11	.3	<2	<2	381	.34	.001	3	119	.14	8	.88	4	4.35	.01	.02	<2	4
L2+50E 0+87.5N	1	27	12	21	<.3	5	1	102	13.13	<2	<5	<2	2	11	.5	<2	<2	406	.37	.008	2	126	.13	7	.87	4	3.32	.01	.02	<2	13
STANDARD C/AU-S	21	61	39	132	6.4	64	33	1012	4.05	43	18	7	37	53	18.4	17	22	58	.52	.094	40	63	.92	193	.09	36	1.93	.06	.15	10	56

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L2+50E 0+75N	<1	24	10	23	<.3	1	<1	100	15.46	10	<5	<2	3	7	<.2	<2	4	381	.29	.023	1	165	.12	5	.73	<3	5.74	.01	.02	<2	2
L2+50E 0+62.5N	<1	21	16	19	<.3	<1	<1	56	15.32	7	<5	<2	3	8	<.2	<2	2	432	.18	.008	2	136	.08	3	.81	<3	3.30	.01	.02	<2	4
L2+50E 0+50N	<1	30	13	23	<.3	7	<1	101	11.79	5	<5	<2	2	13	<.2	<2	<2	346	.43	.008	2	147	.18	5	.77	<3	4.82	.01	.02	<2	2
L2+50E 0+37.5N	<1	16	10	18	<.3	<1	<1	107	13.07	11	<5	<2	2	12	<.2	<2	<2	503	.20	.009	2	87	.08	7	.88	<3	1.94	.01	.02	<2	8
L2+50E 0+25N	<1	25	9	25	<.3	3	<1	95	13.07	3	<5	<2	2	11	<.2	<2	<2	397	.34	.016	2	109	.11	5	.84	<3	3.28	.01	.03	<2	4
L2+50E 0+12.5N	<1	22	4	21	<.3	7	1	105	8.92	11	<5	<2	2	14	<.2	<2	<2	266	.47	.009	2	96	.17	7	.70	<3	3.22	.01	.02	<2	16
L2+50E 0+00	<1	6	4	23	<.3	4	1	124	1.89	<2	<5	<2	<2	17	<.2	3	<2	115	.64	.005	2	28	.21	5	.49	4	1.13	<.01	.02	<2	114
L2+50E 0+12.5S	<1	<1	7	15	<.3	2	<1	68	.81	<2	<5	<2	<2	17	.2	3	6	90	.17	.004	2	24	.04	5	.59	<3	.52	.01	.02	<2	9
L2+50E 0+25S	<1	34	10	28	<.3	11	3	159	7.67	3	<5	<2	2	16	<.2	<2	2	238	.72	.008	2	93	.34	2	.68	<3	4.41	.01	.01	<2	4
L2+50E 0+37.5S	<1	36	7	25	<.3	3	<1	86	14.19	13	<5	<2	2	10	<.2	<2	<2	346	.44	.013	2	154	.15	<1	.83	<3	4.40	.01	.01	<2	2
L2+50E 0+50S	<1	41	5	33	<.3	14	4	176	9.79	8	<5	<2	2	17	<.2	<2	<2	282	1.05	.009	2	136	.45	4	.90	<3	5.98	.01	.01	<2	5
L2+50E 0+62.5S	<1	7	6	14	<.3	<1	<1	59	1.61	2	<5	<2	<2	19	<.2	3	4	189	.29	.001	2	39	.04	4	.86	3	.82	.01	.01	<2	21
L2+50E 0+75S	<1	47	10	35	<.3	3	<1	84	12.04	11	<5	<2	2	20	<.2	<2	<2	417	.50	.005	2	102	.16	4	.97	4	2.67	.01	.01	<2	24
L2+50E 0+87.5S	<1	14	7	32	<.3	10	<1	107	12.22	15	<5	<2	2	90	<.2	<2	<2	325	.74	.013	2	111	.15	4	.98	<3	4.02	.01	.01	<2	1
L2+50E 1+00S	<1	60	8	31	<.3	9	<1	113	15.16	6	<5	<2	3	17	<.2	<2	<2	380	.45	.011	2	143	.25	4	.93	<3	6.23	.01	.02	<2	4
L2+50E 1+12.5S	<1	23	7	35	<.3	2	<1	108	8.01	6	<5	<2	<2	49	<.2	<2	<2	371	.87	.003	2	89	.21	6	1.18	<3	2.92	.01	.01	<2	11
L3+50W 1+75N	<1	19	5	39	<.3	3	1	110	6.82	8	<5	<2	2	14	.4	<2	<2	298	.58	.010	3	118	.20	6	.82	<3	4.63	<.01	.01	<2	5
L3+50W 1+62.5N	<1	47	9	32	<.3	7	<1	131	12.34	11	<5	<2	3	12	<.2	<2	<2	335	.65	.013	2	142	.30	6	.87	5	3.98	.01	.01	<2	4
L3+50W 1+50N	<1	45	12	30	<.3	7	<1	112	12.39	8	<5	<2	2	10	.7	<2	<2	317	.48	.023	2	132	.21	4	.79	4	6.08	.01	.02	<2	51
L3+50W 1+37.5N	<1	36	11	30	<.3	3	<1	127	13.36	9	<5	<2	2	12	<.2	<2	<2	407	.74	.021	2	142	.23	4	.93	<3	6.25	.01	.02	<2	5
L3+50W 1+25N	<1	43	6	34	<.3	6	<1	118	11.91	8	<5	<2	2	15	<.2	<2	<2	331	.69	.010	2	114	.20	4	.87	<3	4.13	.01	.02	<2	5
L3+50W 1+12.5N	<1	13	5	20	<.3	1	<1	75	6.90	9	<5	<2	<2	12	<.2	3	2	355	.46	.006	3	62	.08	4	.99	<3	2.02	.01	.02	<2	5
L3+50W 1+00N	<1	4	7	28	<.3	3	<1	87	4.88	<2	<5	<2	<2	17	<.2	2	2	497	.67	<.001	2	49	.11	4	.99	3	1.46	.01	.02	<2	3
RE L3+50W 0+25N	<1	28	7	48	<.3	13	2	241	12.87	13	<5	<2	2	12	<.2	<2	<2	381	1.06	.018	2	83	.61	1	1.05	3	2.72	.02	.02	<2	5
L3+50W 0+87.5N	<1	18	16	30	<.3	2	<1	76	14.26	7	<5	<2	2	12	<.2	<2	<2	588	.40	.008	2	85	.12	4	.94	<3	2.62	.01	.02	<2	5
L3+50W 0+75N	<1	29	7	31	<.3	<1	1	102	10.30	4	<5	<2	<2	9	.3	2	<2	257	.17	.011	2	10	.31	8	.39	<3	2.04	.03	.03	<2	2
L3+50W 0+62.5N	1	9	5	28	<.3	6	<1	96	2.46	<2	<5	<2	<2	15	.4	4	<2	197	.49	.002	3	64	.17	1	.79	3	1.90	.01	.01	<2	12
L3+50W 0+50N	<1	42	6	45	<.3	12	3	172	4.65	4	<5	<2	<2	19	.2	<2	2	228	1.10	.012	3	92	.42	1	.74	5	4.91	.01	.01	<2	6
L3+50W 0+37.5N	<1	35	7	35	<.3	11	4	177	7.90	12	<5	<2	2	21	.3	<2	<2	270	1.25	.012	4	115	.40	1	.85	<3	4.66	.01	.01	<2	6
L3+50W 0+25N	<1	29	7	47	<.3	11	1	222	12.51	15	<5	<2	2	12	<.2	<2	<2	370	1.01	.018	2	82	.57	1	1.03	3	2.62	.02	.02	<2	6
L3+50W 0+12.5N	<1	20	10	25	<.3	1	<1	75	14.29	13	<5	<2	2	9	<.2	<2	<2	512	.26	.004	2	120	.12	<1	1.02	<3	2.63	.01	.01	<2	8
L3+50W 0+00	<1	21	10	32	<.3	1	<1	102	13.24	9	<5	<2	2	11	.2	<2	4	459	.36	.008	2	124	.14	1	.98	3	2.76	.01	.01	<2	5
L3+50W 0+12.5S	<1	22	8	40	<.3	12	1	131	6.57	2	<5	<2	<2	15	.7	<2	<2	274	.62	.011	2	75	.27	1	.74	4	3.11	.02	.03	<2	6
L3+50W 0+25S	<1	30	14	37	<.3	2	<1	97	14.39	10	<5	<2	2	10	.3	<2	<2	438	.51	.011	2	107	.14	1	1.02	6	2.86	.01	.01	<2	15
L3+50W 0+37.5S	<1	5	7	58	<.3	3	<1	65	2.28	<2	<5	<2	<2	9	.2	4	<2	183	.09	.008	3	14	.02	3	.50	4	.25	.01	.02	<2	18
STANDARD C/AU-S	20	57	40	125	6.1	67	32	974	3.98	43	18	6	36	49	17.1	17	19	56	.49	.094	39	59	.89	185	.08	25	1.83	.06	.14	10	54

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L3+50W 0+50S	1	24	15	42	<.3	<1	<1	113	15.66	<2	7	<2	2	16	.4	<2	<2	600	.34	.017	1	112	.09	6	1.23	<3	2.43	.02	.03	<2	4
L3+50W 0+62.5S	1	25	7	25	.3	<1	<1	86	11.33	<2	10	<2	2	12	.4	<2	<2	413	.44	.012	2	113	.12	1	1.21	5	4.30	.01	.01	2	12
L3+50W 0+75S	1	30	4	20	<.3	6	1	99	6.00	<2	6	<2	<2	16	.2	<2	<2	309	.67	.015	4	106	.17	6	.95	<3	4.71	.02	.01	<2	9
L3+50W 0+87.5S	1	27	3	36	<.3	4	2	145	8.36	<2	8	<2	<2	19	<.2	<2	<2	397	.85	.009	2	94	.27	6	1.03	3	4.72	.01	.01	<2	4
L3+50W 1+00S	1	40	9	44	<.3	6	2	115	6.83	<2	5	<2	2	14	<.2	<2	3	254	.64	.022	4	101	.19	8	.87	<3	6.24	.01	.01	<2	4
L3+50W 1+12.5S	1	47	3	44	<.3	4	1	155	8.51	2	9	<2	<2	14	<.2	<2	4	236	.70	.014	2	99	.22	4	.75	<3	5.64	.02	.02	<2	4
L3+50W 1+25S	<1	28	4	21	<.3	<1	<1	87	13.27	4	5	<2	<2	11	.2	3	<2	485	.33	.007	1	92	.07	9	1.15	3	1.94	.01	.02	<2	7
L3+50W 1+37.5S	1	29	<3	48	<.3	14	6	200	4.98	3	<5	<2	<2	21	.2	<2	<2	199	1.13	.014	5	85	.43	9	.84	3	5.57	.01	.01	<2	4
L3+50W 1+50S	1	23	3	36	<.3	6	2	126	9.55	2	<5	<2	2	14	.2	2	<2	253	.70	.009	3	97	.19	4	.86	<3	4.10	.01	.01	<2	4
L3+50W 1+62.5S	<1	23	8	33	<.3	4	<1	112	12.99	2	6	<2	2	12	.2	<2	<2	409	.41	.011	2	81	.17	4	1.13	<3	2.61	.01	.02	<2	2
L3+50W 1+75S	1	12	6	37	<.3	2	3	423	10.11	4	8	<2	<2	21	<.2	<2	3	331	.75	.011	2	38	.18	4	.72	<3	1.67	.01	.03	<2	4
L3+50W 1+87.5S	<1	27	6	44	<.3	5	8	266	12.36	5	<5	<2	2	14	.2	<2	<2	356	.57	.012	2	112	.23	9	.99	4	4.37	.01	.03	<2	2
L3+50W 2+00S	1	45	5	36	<.3	6	3	172	12.45	10	<5	<2	2	15	.2	<2	<2	304	.74	.012	2	123	.35	9	.96	3	4.32	.01	.02	<2	5
L3+50E 2+50N	1	21	4	30	<.3	8	2	122	2.26	<2	<5	<2	<2	19	<.2	<2	4	150	.91	.008	3	79	.24	7	.73	4	4.19	.01	.01	<2	4
L3+50E 2+37.5N	<1	27	3	20	<.3	5	2	125	8.24	2	<5	<2	2	13	<.2	3	<2	243	.48	.008	2	90	.22	7	.71	<3	3.49	.01	.01	<2	3
L3+50E 2+25N	<1	9	8	21	<.3	1	<1	97	13.12	9	<5	<2	<2	10	.4	<2	<2	402	.35	.014	1	89	.11	7	.85	7	1.43	.01	.01	<2	2
L3+50E 2+12.5N	<1	158	15	45	<.3	24	5	239	19.41	<2	9	<2	2	9	.3	<2	2	696	.18	.008	3	192	.49	13	1.35	<3	1.95	.02	.03	<2	4
L3+50E 2+00N	<1	19	6	17	<.3	1	<1	64	13.57	6	<5	<2	2	9	<.2	<2	<2	622	.15	.006	1	148	.07	10	1.28	<3	1.51	.01	.02	<2	5
RE L3+50E 2+00N	1	19	7	18	<.3	1	<1	63	13.48	<2	8	<2	2	9	<.2	<2	<2	623	.14	.005	1	148	.07	8	1.29	<3	1.53	.01	.02	<2	4
L3+50E 1+87.5N	<1	54	9	38	<.3	21	6	166	14.11	9	<5	<2	<2	16	.3	<2	<2	564	.61	.006	3	183	.42	10	.99	5	2.22	.01	.02	<2	13
L3+50E 1+75N	1	21	7	24	<.3	4	<1	103	11.03	6	<5	<2	2	10	<.2	<2	<2	302	.39	.014	1	111	.17	3	.82	<3	3.33	.01	.02	<2	3
L3+50E 1+62.5N	<1	38	3	15	<.3	3	<1	77	7.12	3	9	<2	2	7	<.2	<2	<2	206	.39	.012	2	168	.13	5	.63	<3	8.56	.01	<.01	<2	4
L3+50E 1+50N	1	15	12	17	<.3	<1	<1	86	10.22	8	<5	<2	2	7	.2	3	<2	472	.16	.009	2	61	.05	6	.79	<3	1.63	.01	.02	<2	15
L3+50E 1+37.5N	<1	13	13	19	<.3	<1	<1	80	10.97	4	6	<2	2	8	<.2	<2	<2	638	.17	.007	1	75	.08	8	.84	<3	1.51	.01	.02	<2	8
L3+50E 1+25N	<1	25	6	23	<.3	5	1	125	9.14	<2	6	<2	2	12	.3	<2	<2	330	.40	.016	2	133	.18	9	.76	3	5.72	.01	.01	<2	3
L3+50E 1+12.5N	<1	19	9	14	<.3	2	<1	116	11.11	3	<5	<2	2	10	<.2	2	<2	412	.22	.009	2	93	.05	6	.77	6	2.07	.01	.02	2	16
L3+50E 1+00N	1	9	4	16	<.3	1	<1	86	8.08	<2	<5	<2	<2	12	<.2	3	3	398	.40	.005	2	63	.06	6	.77	5	1.22	.01	.02	<2	6
L3+50E 0+87.5N	<1	9	6	124	<.3	2	1	25	.33	<2	<5	<2	<2	7	<.2	<2	<2	21	.14	.031	4	12	.04	6	.04	3	.63	.02	.01	<2	<1
L3+50E 0+75N	1	27	6	22	<.3	5	<1	104	11.28	<2	<5	<2	2	10	<.2	<2	<2	312	.43	.013	2	129	.18	6	.86	<3	4.74	.01	.02	<2	3
L3+50E 0+62.5N	<1	10	7	16	<.3	1	<1	49	8.12	3	8	<2	<2	9	<.2	3	5	447	.27	.007	2	44	.04	9	.79	4	1.21	.01	.02	<2	6
L3+50E 0+50N	1	14	7	18	<.3	1	<1	81	11.37	7	<5	<2	2	10	<.2	2	<2	369	.37	.015	2	96	.09	9	.82	4	2.98	.01	.02	<2	5
L3+50E 0+37.5N	<1	21	9	19	<.3	<1	<1	99	11.10	<2	<5	<2	2	8	<.2	<2	<2	322	.31	.012	2	86	.07	6	.73	4	3.09	.01	.01	<2	2
L3+50E 0+25N	<1	49	11	15	<.3	<1	<1	66	18.97	8	<5	<2	2	5	<.2	<2	<2	544	.12	.011	1	132	.04	11	1.17	5	2.12	.01	.01	<2	4
L3+50E 0+12.5N	1	22	4	13	<.3	<1	<1	65	12.82	2	<5	<2	2	8	<.2	<2	<2	386	.22	.007	1	80	.07	7	.79	<3	2.28	.01	.02	<2	3
L3+50E 0+00	<1	37	5	19	<.3	3	<1	103	12.03	5	5	<2	<2	33	<.2	<2	3	598	.27	.005	1	70	.10	9	1.56	3	1.41	.01	.01	<2	6
STANDARD C/AU-S	21	60	39	134	6.6	67	32	1026	4.12	42	22	8	38	53	18.6	16	21	58	.53	.095	40	62	.94	188	.09	26	1.99	.06	.16	11	48

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L3+50E 0+12.5S	<1	12	10	28	<.3	2	<1	95	14.13	<2	10	<2	2	26	<.2	<2	<2	650	.28	.007	2	78	.11	1	1.22	<3	1.41	.02	.02	<2	12
L3+50E 0+25S	<1	21	16	25	<.3	2	1	93	14.11	<2	8	<2	2	36	<.2	<2	5	817	.31	.004	2	82	.06	6	1.45	<3	1.87	.01	.02	<2	9
L3+50E 0+37.5S	1	20	13	23	<.3	<1	<1	70	11.14	<2	6	<2	2	8	.7	2	<2	491	.18	.006	3	66	.05	4	.99	<3	2.50	.01	.02	<2	3
L3+50E 0+50S	1	49	<3	44	<.3	19	6	163	4.74	<2	6	<2	<2	18	<.2	<2	5	207	.94	.010	4	101	.39	1	.65	3	6.97	.02	.01	<2	3
L3+50E 0+62.5S	1	12	3	56	<.3	20	13	344	10.58	<2	7	<2	2	16	.4	<2	<2	257	.84	.013	2	64	.83	7	.71	<3	3.49	.02	.05	<2	2
L3+50E 0+75S	<1	39	4	45	<.3	15	8	201	5.23	2	<5	<2	<2	42	<.2	<2	<2	214	1.40	.007	3	76	.60	2	.89	4	4.11	.01	.01	<2	6
L4+50E 2+50N	1	14	11	16	<.3	<1	<1	78	12.10	<2	9	<2	2	7	.2	3	<2	482	.13	.010	2	70	.05	2	.84	<3	1.33	.01	.02	<2	3
L4+50E 2+37.5N	1	25	8	23	<.3	8	1	115	10.57	<2	5	<2	2	11	<.2	<2	<2	283	.38	.013	2	115	.21	2	.75	<3	3.14	.01	.02	<2	2
L4+50E 2+25N	<1	18	8	26	<.3	<1	<1	61	11.21	<2	5	<2	<2	10	.5	<2	<2	453	.24	.010	2	107	.07	7	.99	<3	2.34	.01	.02	<2	3
L4+50E 2+12.5N	<1	28	14	22	<.3	2	<1	64	12.90	2	6	<2	2	8	<.2	4	<2	361	.20	.012	2	84	.07	5	.87	<3	2.13	.01	.02	<2	5
L4+50E 2+00N	<1	37	11	18	<.3	3	2	88	11.43	<2	5	<2	2	10	<.2	<2	<2	341	.36	.009	3	107	.10	5	.78	<3	3.47	.01	.01	<2	92
L4+50E 1+87.5N	<1	28	8	34	<.3	8	1	121	8.67	<2	5	<2	2	14	<.2	<2	5	368	.53	.008	3	106	.29	5	.88	<3	3.98	.01	.02	<2	10
L4+50E 1+75N	<1	10	13	27	<.3	1	<1	119	8.24	<2	<5	<2	<2	8	<.2	3	<2	430	.15	.004	2	46	.05	8	.76	<3	.80	.01	.02	<2	6
L4+50E 1+62.5N	<1	23	6	19	<.3	4	<1	95	12.63	<2	9	<2	2	8	.2	3	2	435	.35	.007	2	112	.17	6	.89	<3	2.62	.01	.02	<2	4
L4+50E 1+50N	<1	9	5	27	<.3	6	1	90	2.06	<2	<5	<2	<2	13	<.2	2	<2	216	.50	.007	3	64	.18	8	.74	4	1.60	.01	.01	<2	5
L4+50E 1+37.5N	<1	25	5	26	<.3	2	<1	95	13.72	4	5	<2	2	9	<.2	<2	3	364	.37	.012	2	139	.12	8	.83	3	3.14	.01	.02	<2	2
L4+50E 1+25N	<1	27	10	33	<.3	7	2	126	13.98	4	5	<2	2	10	.6	<2	2	359	.35	.019	2	123	.17	8	.78	<3	4.31	.01	.04	<2	3
L4+50E 1+12.5N	1	37	5	35	<.3	12	5	158	4.29	5	<5	<2	<2	14	<.2	<2	5	161	.90	.015	6	113	.42	4	.60	4	6.77	.01	.01	<2	6
L4+50E 1+00N	<1	21	11	21	<.3	2	<1	96	13.69	<2	7	<2	2	11	<.2	<2	<2	429	.48	<.001	2	129	.21	6	.95	<3	3.05	<.01	.02	<2	4
L4+50E 0+87.5N	1	18	10	20	<.3	2	<1	79	13.60	<2	5	<2	2	7	<.2	<2	<2	436	.30	.008	2	114	.10	9	.83	<3	1.81	.01	.02	<2	6
L4+50E 0+75N	<1	12	11	62	<.3	9	5	231	2.46	<2	5	<2	<2	11	<.2	2	<2	158	1.20	.027	2	39	.28	2	.45	7	1.33	.03	.05	<2	5
L4+50E 0+62.5N	<1	5	8	18	<.3	1	<1	60	1.54	<2	<5	<2	<2	6	<.2	2	<2	175	.37	.007	2	21	.10	2	.60	3	.57	.01	.02	<2	18
L4+50E 0+50N	1	25	9	26	<.3	4	1	101	8.42	<2	<5	<2	2	11	<.2	<2	<2	265	.50	.012	2	131	.21	2	.80	<3	4.83	.01	.01	<2	5
L4+50E 0+37.5N	<1	24	9	17	<.3	3	1	113	9.38	<2	6	<2	<2	10	<.2	<2	<2	451	.38	.003	2	63	.08	5	1.03	<3	1.43	.01	.01	<2	5
RE L4+50E 0+37.5N	<1	22	10	16	<.3	2	1	103	9.05	<2	6	<2	<2	10	<.2	2	<2	432	.37	.003	2	60	.08	5	.98	<3	1.30	.01	.01	<2	8
L4+50E 0+25N	1	31	4	35	<.3	9	3	134	6.36	<2	<5	<2	<2	12	.3	<2	2	234	.55	.010	6	105	.30	5	.66	<3	5.09	.01	.02	<2	5
L4+50E 0+12.5N	1	12	10	27	<.3	1	2	160	13.49	<2	6	<2	2	10	<.2	<2	<2	559	.39	.005	2	65	.15	5	.83	4	1.48	.01	.02	<2	6
L4+50E 0+00	<1	31	8	20	<.3	2	<1	95	10.18	<2	<5	<2	2	9	<.2	<2	<2	492	.36	.004	2	81	.10	1	.92	<3	2.76	.01	.01	<2	5
L4+50E 0+12.5S	<1	42	7	23	<.3	3	1	120	11.56	<2	7	<2	2	11	<.2	<2	<2	357	.53	.012	2	99	.21	6	.87	3	3.50	.01	.02	<2	4
L4+50E 0+25S	<1	25	11	28	<.3	3	<1	137	10.85	<2	5	<2	<2	6	<.2	<2	<2	461	.47	.013	2	49	.12	1	1.02	<3	1.14	.01	.02	<2	4
L4+50E 0+37.5S	<1	32	9	41	<.3	8	4	136	9.32	<2	6	<2	<2	20	.4	<2	<2	381	.63	.010	2	86	.36	8	.95	3	4.07	.01	.02	<2	2
L4+50E 0+50S	<1	35	6	22	<.3	8	2	107	11.91	<2	5	<2	2	12	.3	<2	<2	341	.36	.013	2	104	.18	2	.76	<3	3.64	.01	.02	<2	3
L4+50E 0+62.5S	<1	22	6	18	<.3	<1	<1	79	13.29	<2	6	<2	2	8	<.2	<2	5	471	.26	.005	1	97	.06	4	.92	3	1.90	.01	.02	<2	2
L4+50E 0+75S	<1	4	9	14	<.3	3	<1	118	1.59	<2	<5	<2	<2	11	<.2	<2	<2	177	.19	.001	2	30	.05	9	.82	4	.67	.01	.02	<2	11
L4+50E 0+87.5S	<1	27	15	21	<.3	3	<1	78	15.18	<2	5	<2	2	8	.3	<2	<2	534	.19	.007	2	74	.07	2	1.01	<3	1.88	.01	.02	<2	5
STANDARD C/AU-S	20	59	41	129	6.2	67	32	991	4.12	42	21	7	37	51	17.9	15	17	57	.52	.095	39	61	.92	185	.09	28	1.94	.06	.15	11	46

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L4+50E 1+00S	<1	28	10	31	<.3	9	4	174	13.52	2	<5	<2	2	13	<.2	<2	<2	437	.30	.006	3	63	.34	5	.87	<3	2.27	.01	.01	<2	7
L4+50E 1+12.5S	<1	11	10	38	<.3	4	2	58	1.15	6	<5	<2	<2	14	<.2	<2	3	86	.27	.013	3	21	.07	10	.53	4	.67	.02	.02	<2	10
L5+50E 2+00N	1	48	3	23	<.3	8	3	124	10.08	3	<5	<2	2	12	.3	<2	<2	270	.41	.009	2	135	.24	8	.68	<3	7.23	.01	<.01	<2	18
L5+50E 1+87.5N	<1	47	<3	23	<.3	9	5	136	6.29	4	<5	<2	2	17	<.2	<2	<2	224	.72	.010	4	84	.31	10	.80	<3	4.42	.01	<.01	<2	7
L5+50E 1+75N	1	21	8	32	<.3	7	4	141	2.08	4	<5	<2	<2	21	<.2	<2	3	169	.60	.009	3	60	.20	15	.83	<3	2.17	.01	.01	<2	6
L5+50E 1+62.5N	<1	8	8	14	<.3	4	2	77	1.04	<2	<5	<2	<2	18	<.2	3	3	109	.36	.011	2	20	.06	8	.45	<3	.69	.01	.01	<2	5
L5+50E 1+50N	<1	20	4	30	.3	7	8	184	14.51	8	<5	<2	2	16	.2	<2	<2	817	2.18	.008	2	89	.27	5	.65	<3	2.84	.01	.02	<2	20
L5+50E 1+37.5N	<1	23	8	25	<.3	5	4	111	8.35	7	<5	<2	2	15	<.2	3	<2	419	.53	.007	2	67	.17	8	.81	<3	1.95	.01	.01	<2	4
L5+50E 1+25N	1	23	<3	40	.3	8	5	168	12.59	7	<5	<2	2	16	.2	<2	<2	321	.49	.013	3	64	.33	15	.58	4	2.46	.01	.03	<2	1
L5+50E 1+12.5N	<1	15	8	21	<.3	<1	2	100	9.05	2	<5	<2	2	14	<.2	<2	<2	559	.48	.009	3	69	.09	3	.75	<3	1.55	.01	.03	<2	7
L5+50E 1+00N	<1	13	14	18	<.3	1	1	87	4.25	3	<5	<2	<2	11	<.2	3	5	345	.20	.005	2	28	.07	8	.63	<3	.71	.01	.01	<2	9
L5+50E 0+87.5N	<1	26	6	29	<.3	4	1	111	11.54	5	<5	<2	2	27	<.2	<2	<2	496	1.08	.006	2	113	.23	10	.97	3	2.03	.01	.02	<2	3
L5+50E 0+75N	<1	31	3	40	<.3	8	3	129	7.52	4	<5	<2	2	13	.2	<2	<2	377	.61	.010	3	89	.30	4	.82	3	3.66	.01	.01	<2	3
L5+50E 0+62.5N	<1	18	12	25	<.3	5	3	92	5.45	5	<5	<2	<2	16	<.2	<2	4	385	.52	.002	2	65	.13	10	1.15	3	1.85	.01	.01	<2	4
L5+50E 0+50N	<1	10	6	15	<.3	3	1	89	3.32	4	<5	<2	<2	16	<.2	3	<2	191	.31	.005	2	32	.09	11	.54	<3	.99	.01	.01	<2	3
L5+50E 0+37.5N	<1	25	4	22	.3	3	4	102	9.44	2	<5	2	2	13	.2	4	<2	371	.41	.006	2	85	.21	6	.79	4	3.29	.01	.01	2	4
L5+50E 0+25N	<1	20	3	24	<.3	4	4	315	6.95	5	<5	<2	2	15	<.2	<2	<2	267	.63	.012	2	79	.16	6	.72	4	2.61	.01	.01	<2	1
L5+50E 0+12.5N	1	66	<3	40	<.3	27	12	360	2.70	4	<5	<2	<2	26	<.2	<2	3	99	1.06	.019	8	58	.88	11	.46	<3	6.01	.02	.01	<2	11
L5+50E 0+00	<1	27	9	19	<.3	4	2	105	7.24	<2	<5	<2	2	14	<.2	2	<2	335	.47	.005	2	79	.17	9	.87	5	2.68	.01	.01	<2	4
L5+50E 0+12.5S	1	61	6	40	<.3	15	6	182	7.22	4	<5	<2	2	18	.2	<2	<2	192	.84	.013	3	99	.36	16	.60	<3	5.57	.01	.01	<2	6
L5+50E 0+25S	<1	38	8	21	<.3	1	<1	85	15.55	<2	<5	<2	2	16	.2	<2	<2	566	.39	.010	2	94	.08	4	1.12	4	1.64	<.01	.01	<2	48
L5+50E 0+37.5S	<1	27	13	24	<.3	2	2	96	9.43	3	<5	<2	2	17	<.2	<2	<2	581	.57	.001	2	78	.15	11	1.22	<3	2.35	.01	.02	<2	6
L5+50E 0+50S	<1	41	<3	25	<.3	8	4	122	8.08	<2	<5	<2	2	14	<.2	<2	<2	314	.78	.011	3	126	.29	9	.87	<3	5.14	.01	.01	<2	3
L5+50E 0+62.5S	<1	9	3	89	<.3	4	1	34	.45	<2	<5	<2	<2	9	<.2	<2	<2	19	.13	.022	1	8	.05	9	.06	<3	.41	.02	.01	<2	<1
RE L5+50E 0+75S	<1	42	10	15	<.3	2	<1	72	15.10	<2	5	<2	2	10	.2	<2	<2	541	.18	.009	2	80	.07	7	1.05	5	2.28	.01	.02	<2	4
L5+50E 0+75S	<1	42	11	16	<.3	1	<1	66	15.86	<2	<5	<2	3	9	.3	<2	<2	561	.17	.009	2	84	.07	5	1.08	3	2.31	.01	.02	<2	3
L5+50E 0+87.5S	<1	9	8	24	<.3	3	1	53	.98	<2	<5	<2	<2	13	<.2	3	<2	93	.10	.011	2	19	.03	9	.57	3	.45	.01	.01	<2	45
L5+50E 1+00S	<1	38	7	30	<.3	9	4	135	9.38	4	7	<2	2	14	.2	<2	<2	305	.82	.010	2	96	.35	9	.86	4	4.25	.01	.01	<2	3
L5+50E 1+12.5S	<1	22	7	13	<.3	1	1	71	9.18	<2	<5	<2	2	10	.2	<2	<2	426	.24	.002	3	75	.07	12	.98	<3	2.63	.01	.01	<2	8
L5+50E 1+25S	<1	36	9	23	<.3	8	1	96	16.53	<2	<5	<2	3	11	<.2	<2	<2	641	.12	.005	1	110	.17	9	1.09	<3	1.78	.01	.02	<2	3
L6+50E 1+00N	1	35	5	23	<.3	10	4	100	3.76	<2	5	<2	<2	13	<.2	<2	<2	199	.42	.009	6	81	.24	9	.69	<3	5.07	.01	.01	<2	6
L6+50E 0+87.5N	<1	19	11	28	<.3	5	3	474	8.61	<2	7	<2	<2	18	<.2	<2	5	512	.40	.010	1	68	.38	10	.88	<3	1.54	.01	.03	<2	5
L6+50E 0+75N	<1	33	<3	21	<.3	4	2	143	11.70	<2	8	<2	2	13	.2	<2	<2	325	.52	.020	1	131	.18	10	.78	4	4.15	.01	.02	<2	1
L6+50E 0+62.5N	<1	28	9	23	<.3	4	1	105	14.09	<2	7	<2	2	15	.2	<2	<2	454	.55	.013	2	144	.09	7	.79	5	3.02	<.01	.01	<2	5
L6+50E 0+50N	<1	19	8	54	<.3	9	5	152	3.82	4	<5	<2	<2	21	<.2	<2	<2	124	.58	.027	2	33	.26	19	.37	3	.72	.02	.04	<2	3
STANDARD C/AU-S	21	62	36	133	6.5	67	33	1037	4.22	43	20	8	39	53	17.8	15	20	60	.53	.096	40	57	.96	196	.09	29	1.99	.06	.15	9	56

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L6+50E 0+37.5N	<1	32	<3	89	<.3	7	1	21	.43	4	<5	<2	<2	8	.2	<2	<2	28	.25	.052	7	31	.03	12	.03	<3	2.23	.01	.01	<2	3
L6+50E 0+25N	<1	33	6	38	<.3	14	7	199	6.74	<2	<5	<2	<2	20	<.2	<2	<2	193	1.09	.010	5	127	.60	9	.80	<3	5.32	.01	.01	<2	4
L6+50E 0+12.5N	<1	39	8	33	<.3	13	6	192	3.72	<2	<5	<2	<2	18	<.2	<2	<2	121	.93	.016	4	81	.49	11	.55	4	4.39	.01	.02	<2	4
L6+50E 0+00	<1	19	13	14	<.3	1	<1	101	6.91	3	<5	<2	<2	14	<.2	3	<2	401	.27	.004	2	51	.07	9	.83	3	1.00	<.01	.02	<2	4
L6+50E 0+12.5S	<1	20	8	25	<.3	4	3	130	5.99	<2	6	<2	<2	14	<.2	<2	<2	333	.82	.005	2	87	.30	5	.86	<3	2.51	.01	.02	<2	18
L6+50E 0+25S	<1	9	9	15	<.3	2	1	63	.96	<2	6	<2	<2	12	<.2	4	<2	113	.21	.004	2	45	.05	7	.78	3	.86	.01	.02	<2	6
L6+50E 0+37.5S	<1	9	8	16	<.3	3	<1	78	3.80	3	5	<2	<2	10	<.2	3	<2	299	.28	.003	3	40	.06	9	.81	<3	.72	<.01	.02	<2	11
L6+50E 0+50S	<1	46	5	26	<.3	10	3	140	9.35	<2	8	<2	2	10	.5	<2	<2	254	.70	.014	2	167	.33	5	.72	3	7.87	.01	.01	<2	3
L6+50E 0+62.5S	1	39	<3	30	<.3	8	4	150	4.27	2	5	<2	<2	13	<.2	<2	<2	125	.92	.016	4	150	.37	2	.51	<3	9.52	.01	.01	<2	2
L6+50E 0+75S	<1	13	<3	131	<.3	6	1	78	.46	<2	<5	<2	<2	9	.2	2	<2	19	.21	.026	1	11	.06	9	.05	4	.58	.05	.01	<2	1
L6+50E 0+87.5S	<1	21	8	23	<.3	2	2	107	12.31	<2	9	<2	2	8	<.2	2	<2	365	.39	.008	1	124	.17	5	.85	<3	3.05	.01	.02	<2	2
L6+50E 1+00S	<1	7	10	15	<.3	4	1	78	1.42	3	5	<2	<2	11	.4	4	4	158	.28	.003	1	31	.06	11	.73	<3	.65	.01	.01	<2	7
L6+50E 1+12.5S	<1	23	6	14	<.3	<1	<1	46	19.20	<2	6	<2	2	6	<.2	<2	<2	480	.15	.007	1	102	.04	4	.80	<3	2.30	<.01	.03	<2	5
L6+50E 1+25S	<1	24	11	13	<.3	<1	<1	93	13.14	<2	6	<2	2	5	<.2	<2	<2	534	.13	.004	1	86	.04	9	.96	<3	1.35	<.01	.01	<2	34
L7+00E 0+50N	<1	29	4	16	<.3	1	<1	85	16.77	<2	12	<2	2	11	<.2	<2	<2	478	.51	.006	2	117	.18	7	.96	<3	2.53	.01	.01	<2	3
L7+00E 0+37.5N	1	6	4	57	<.3	6	1	42	.73	<2	<5	<2	<2	16	.4	2	<2	22	.31	.023	1	8	.10	7	.05	<3	.24	.02	.01	<2	1
L7+00E 0+25N	<1	16	4	25	.3	1	6	175	16.11	4	9	<2	3	41	<.2	<2	<2	826	1.96	.008	3	226	.31	9	1.16	<3	4.66	.01	.02	<2	15
L7+00E 0+12.5N	<1	45	7	21	<.3	6	3	91	4.43	<2	<5	<2	<2	20	.3	<2	<2	206	.56	.010	6	86	.14	9	.67	<3	4.41	.01	.02	<2	5
L7+00E 0+00	<1	15	10	9	<.3	<1	<1	32	19.71	<2	12	<2	2	6	.2	2	<2	711	.09	.007	2	119	.03	7	.70	<3	2.05	<.01	.02	<2	3
RE L7+00E 0+00	1	14	14	9	<.3	<1	<1	31	19.54	<2	7	<2	3	6	.3	<2	2	713	.09	.008	2	117	.03	5	.70	<3	2.01	<.01	.02	<2	2
L7+00E 0+12.5S	<1	57	5	24	<.3	14	7	198	4.45	<2	<5	<2	<2	19	.4	2	<2	158	1.05	.013	3	78	.54	9	.49	6	3.99	.01	.01	<2	4
L7+00E 0+25S	<1	19	12	10	.3	<1	<1	85	12.28	<2	6	<2	2	8	<.2	3	<2	452	.13	.005	3	101	.05	9	.82	<3	1.97	<.01	.01	<2	3
L7+00E 0+37.5S	<1	17	8	9	<.3	<1	<1	80	9.55	<2	7	<2	<2	9	<.2	4	<2	410	.11	.004	2	71	.03	11	.84	<3	.82	<.01	.02	<2	4
L7+00E 0+50S	<1	32	8	13	<.3	2	1	98	8.98	<2	6	<2	2	12	.2	<2	<2	256	.45	.004	2	137	.17	9	.73	3	3.89	.01	.01	<2	2
L7+00E 0+62.5S	<1	47	6	41	<.3	77	11	120	8.73	2	7	<2	<2	13	<.2	<2	<2	286	.58	.014	4	168	.42	9	.76	<3	5.55	.01	.01	2	2
L7+00E 0+75S	<1	27	<3	20	<.3	7	3	134	11.04	<2	13	<2	2	13	.6	<2	<2	318	.77	.008	2	110	.27	7	.95	6	3.80	.01	.01	<2	1
L7+00E 0+87.5S	<1	28	10	21	<.3	1	<1	80	14.77	<2	11	<2	2	9	<.2	<2	<2	406	.41	.009	2	146	.15	7	.89	<3	5.01	.01	.01	<2	2
L7+00E 1+00S	<1	21	16	18	<.3	4	1	98	9.11	2	8	<2	<2	14	.2	2	<2	384	.61	.005	3	87	.18	11	.97	3	2.93	.01	.02	<2	2
L7+00E 1+12.5S	<1	10	11	12	<.3	2	<1	88	8.54	<2	8	<2	<2	12	<.2	2	<2	270	.34	.006	2	66	.07	7	.61	<3	1.43	.01	.01	<2	2
L7+00E 1+25S	<1	22	5	11	<.3	4	1	97	7.34	3	<5	<2	<2	13	.3	3	<2	318	.52	.007	3	64	.17	7	.74	<3	2.53	.01	.03	<2	4
STANDARD C/AU-S	20	60	40	129	6.2	69	31	1005	4.27	37	19	6	37	51	18.4	16	22	60	.51	.091	39	63	.91	183	.10	26	1.91	.06	.15	11	55

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

APPENDIX III

Geophysical Survey Report

PACIFIC Geophysical Limited

4508 WEST 13TH AVENUE, VANCOUVER, B.C. V6R 2V4

TEL. 604-222-2125
FAX. 604-222-2141

MEMO

To: Peter Dasler, Kamaka Resources Ltd.

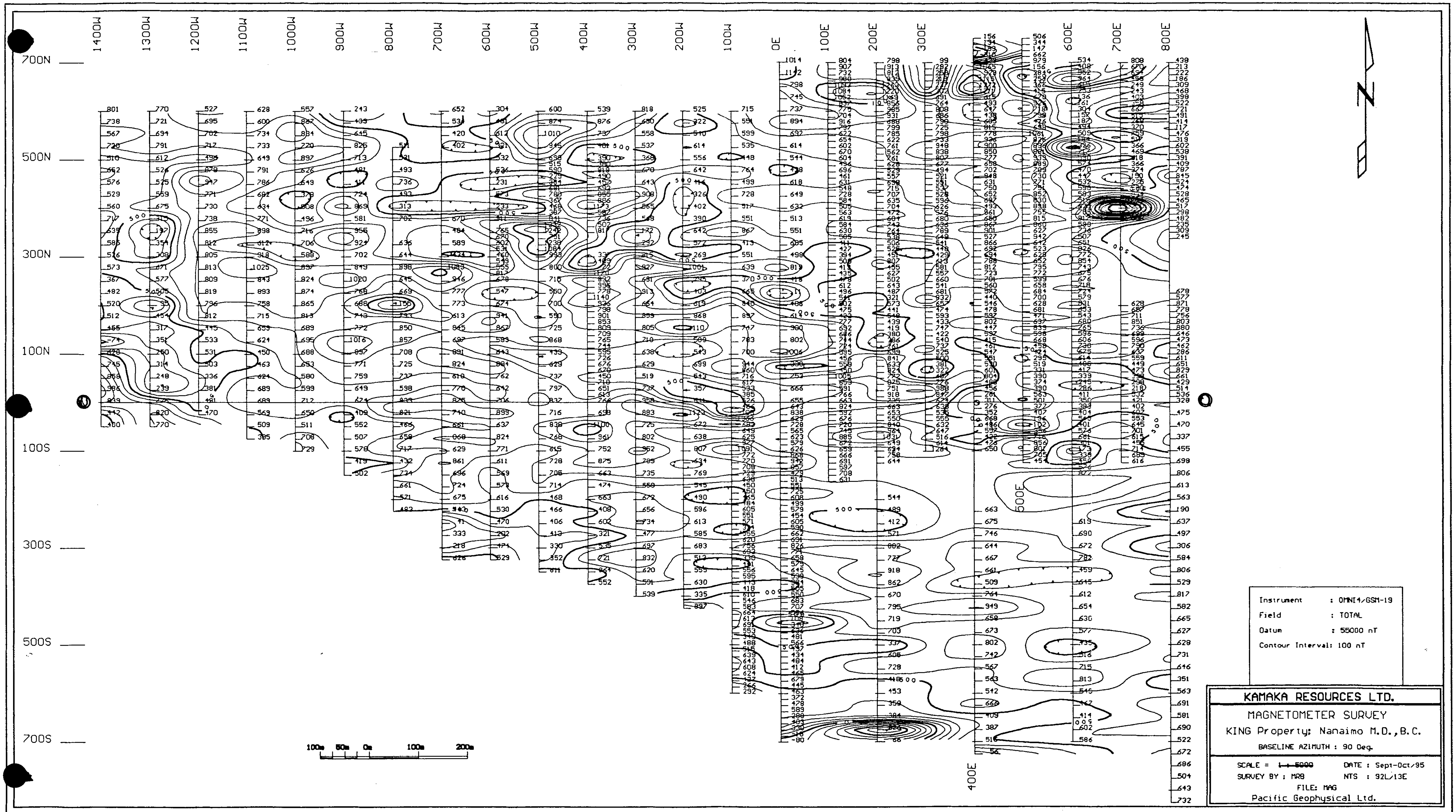
Re: KING Property Geophysical Surveys

A program of total field magnetic surveying , and VLF electro-magnetic surveying, and VLF resistivity surveying has been carried out by Pacific Geophysical Ltd. on the King Property, Nanaimo Mining Division, British Columbia, on behalf of Kamaka Resources Ltd.

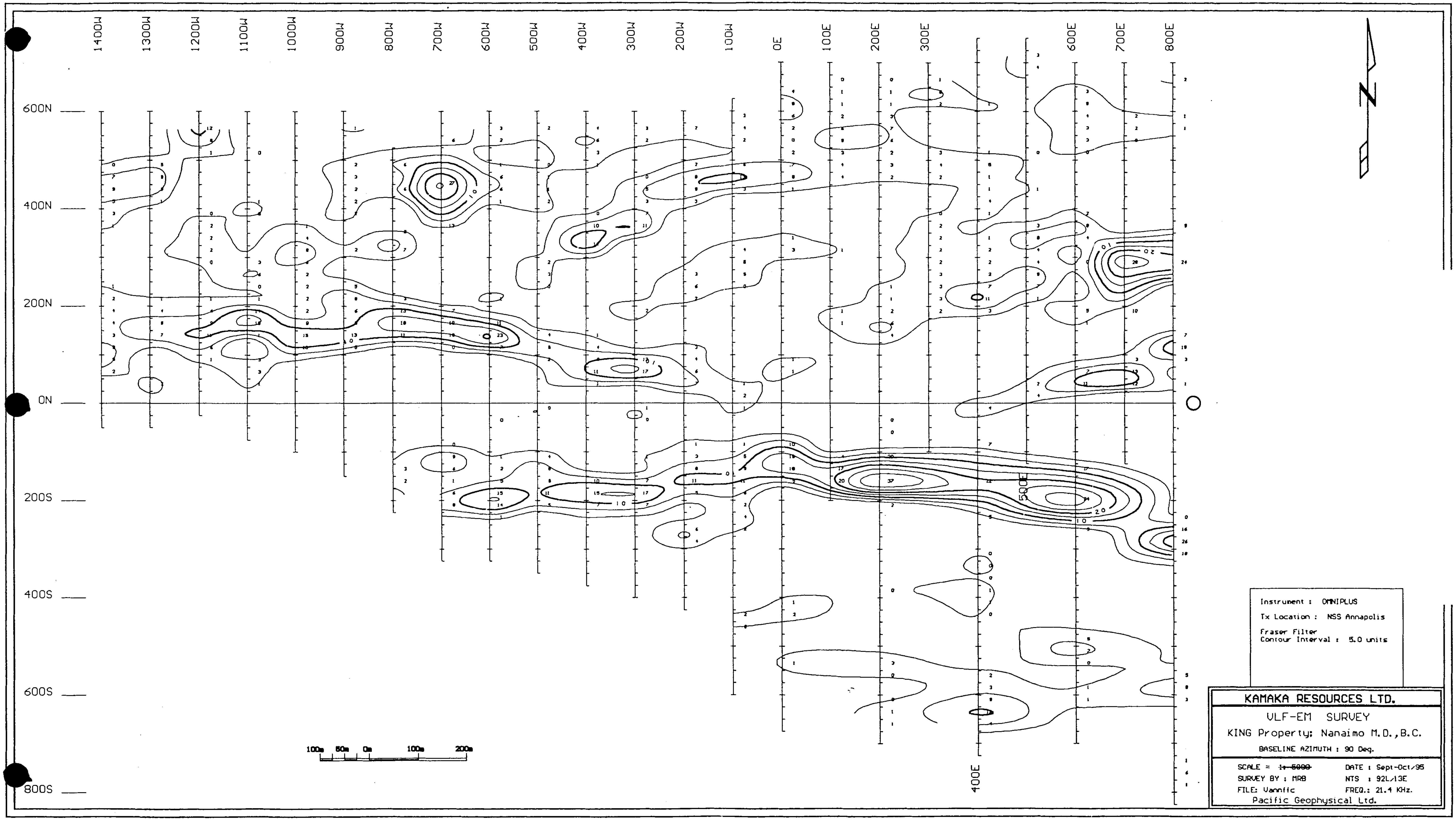
A two person geophysical crew consisting of M. Beaupre, senior geophysical technician, and B. Page, junior geophysical technician, mobilized to the property on Sept. 29, 1995, and demobilized on October 9-10, 1995. During the period Sept. 30, 1995 to October 8, 1995 the crew utilized an EDA Model OmniPlus Magnetometer/VLF-EM/Resistivity unit to survey most of the geophysical grid using the magnetic and VLF-EM techniques. A Gem Systems Model GSM-19 total field magnetometer was also employed during this phase of the program. An EDA Model PPM375 recording magnetic base station was used to correct all magnetic data for the effects of diurnal changes.

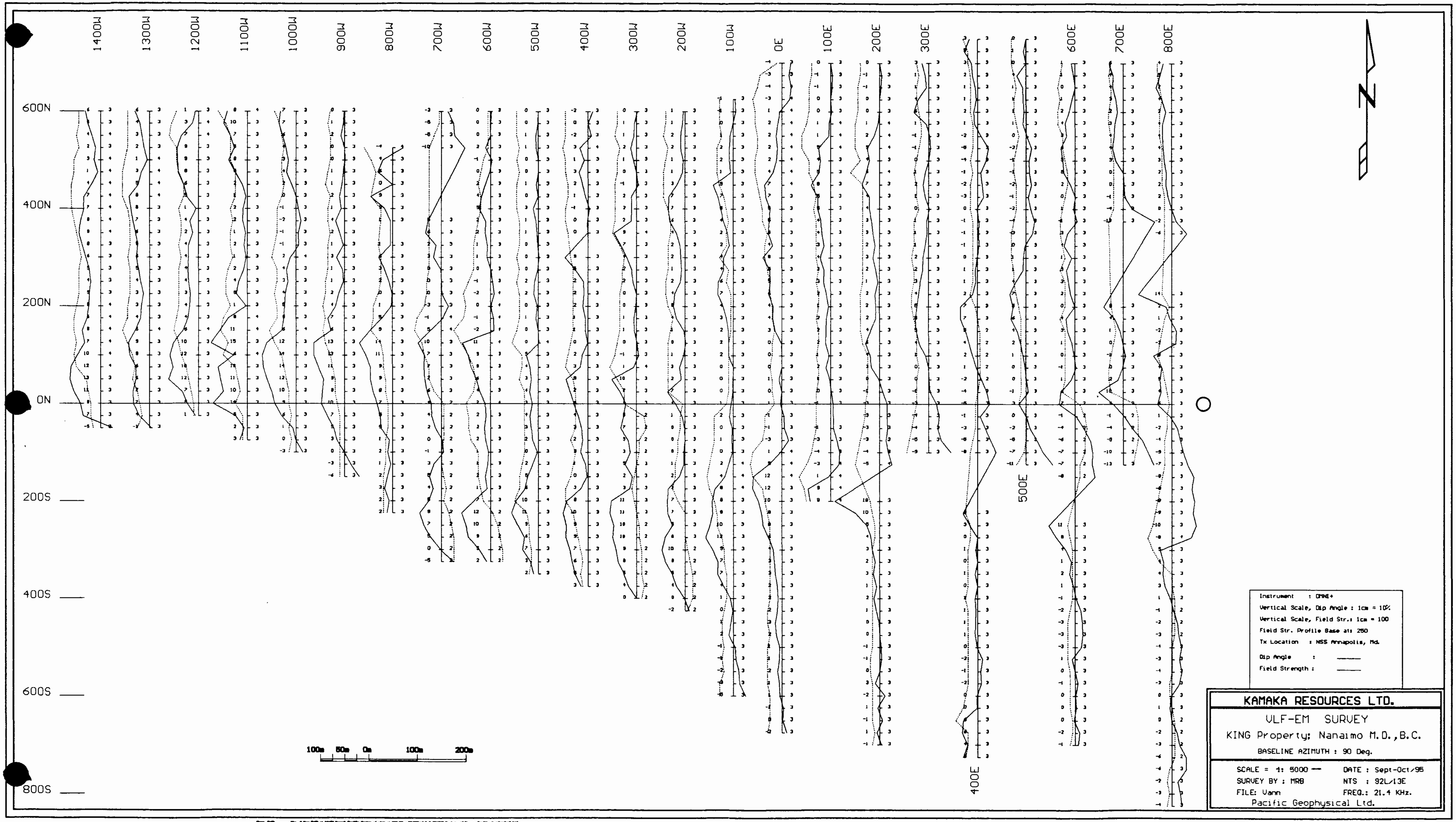
The VLF-EM work primarily used the transmitting station located in Annapolis, Maryland, however, various parts of the geophysical grid were also measured using the transmitters positioned near Cutler, Maine, and on the Island of Hawaii. Dip angle and field strength parameters were recorded in all cases. A small region in the central portion of the grid was surveyed using the VLF resistivity method, employing the transmitter located near Seattle, Washington. In this case, Cagniard resistivities in units of ohm-metres were obtained by measuring the electric field induced across a 20 metre earth electrode separation, together with the horizontal magnetic field measured perpendicular to the line joining the observation point and the transmitter station. Phase shift between the electric and magnetic signals was also measured in degrees.

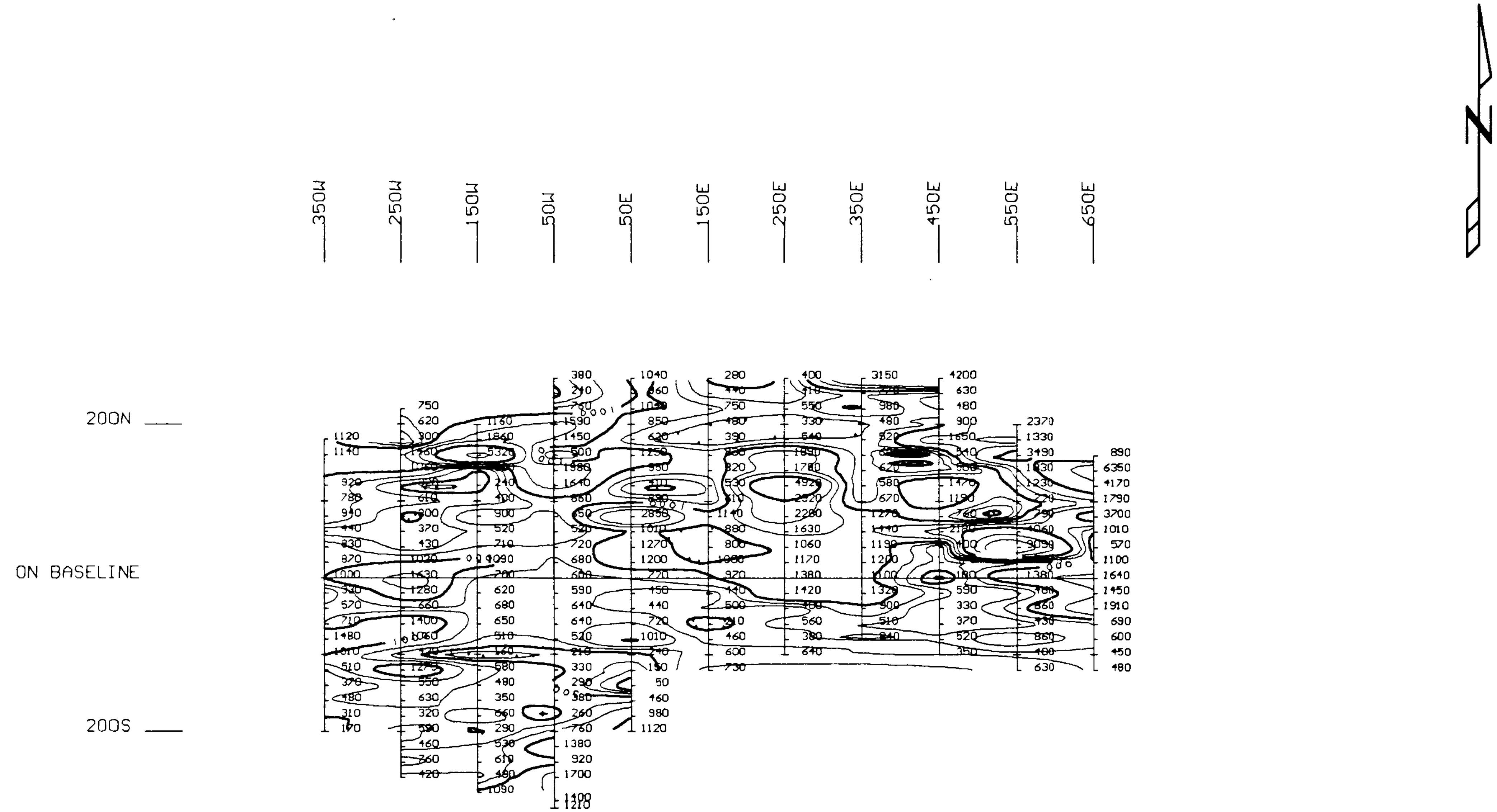
Paul A. Cartwright, P.Geo.



KAMAKA RESOURCES LTD.
MAGNETOMETER SURVEY
KING Property: Nanaimo M.D., B.C.
BASELINE AZIMUTH : 90 Deg.
SCALE = 1 : 5000
DATE : Sept-Oct/95
SURVEY BY : MRB
NTS : 92L/13E
FILE: MAG
Pacific Geophysical Ltd.
Instrument : OMNI4/GSM-19
Field : TOTAL
Datum : 55000 nT
Contour Interval: 100 nT
1400W 1300W 1200W 1100W 1000W 900W 800W 700W 600W 500W 400W 300W 200W 100W 0E 100E 200E 300E 600E 700E 800E
700N 500N 300N 100N 100S 300S 500S 700S
500E
400E
100m 50m 0m 100m 200m


1400W
1300W
1200W
1100W
1000W
900W
800W
700W
600W
500W
400W
300W
200W
100W
0E
100E
200E
300E
400E
500E
600E
700E
800E
600N
400N
200N
0N
200S
400S
600S
800S
100m 50m 0m 100m 200m
Instrument : OMNIPLUS
Tx Location : NSS Annapolis
Fraser Filter
Contour Interval : 5.0 units
KAMAKA RESOURCES LTD.
VLF-EM SURVEY
KING Property: Nanaimo M.D., B.C.
BASELINE AZIMUTH : 90 Deg.
SCALE = ~~1: 5000~~
DATE : Sept-Oct/95
SURVEY BY : MRB
NTS : 92L/13E
FILE: Vannffc
FREQ.: 21.4 KHz.
Pacific Geophysical Ltd.


1400W
1300W
1200W
1100W
1000W
900W
800W
700W
600W
500W
400W
300W
200W
100W
0E
100E
200E
300E
400E
500E
600E
700E
800E
600N
400N
200N
0N
200S
400S
600S
800S
100m 50m 0m 100m 200m
Instrument : OMNI+
Vertical Scale, Dip Angle : 1cm = 10%
Vertical Scale, Field Str.: 1cm = 100
Field Str. Profile Base at: 250
Tx Location : NSS Annapolis, Md.
Dip Angle :
Field Strength :
KAMAKA RESOURCES LTD.
VLF-EM SURVEY
KING Property: Nanaimo M.D., B.C.
BASELINE AZIMUTH : 90 Deg.
SCALE = 1: 5000
SURVEY BY : MRB
FILE: Vann
DATE : Sept-Oct/95
NTS : 92L/13E
FREQ.: 21.4 KHz.
Pacific Geophysical Ltd.



100m 50m 0m 100m 200m

Instrument : OMNIPLUS

Tx Location : NLK Seattle

Contour Interval :
70,100,150,200,300,500 ohm

KAMAKA RESOURCES LTD.

ULF RESISTIVITY SURVEY

KING Property; Nanaimo M.D., B.C.

BASELINE AZIMUTH : 90 Deg.

SCALE = ~~1:5000~~	DATE : Sept-Oct/95
SURVEY BY : MRB	NTS : 92L/13E
FILE: MKNGRES	FREQ.: 24.8 KHz.

Pacific Geophysical Ltd.


GEOLOGICAL BRANCH
ASSESSMENT REPORT
24,283
SCALE
0 40 80 120 160
Metres
WESTWARD EXPLORATION LTD.
KING MINERAL CLAIMS
SOIL GEOCHEMISTRY
GOLD (ppb)
KAMAKA RESOURCES LTD.
Scale : 1 : 2,000
Date : DEC. 1995
CAMP LAKE
LAKE OF THE MOUNTAINS


ZONE 4 ANOMALY
MAIN ZONE ANOMALY
ZONE 2-3 ANOMALIES
ZONE 5 ANOMALY
CAMP LAKE
LAKE OF THE MOUNTAINS
Camp Site
sampled on quartz vein
no outcrop
BASELINE
KING 31
KING 103
KING 11
KING 12
KING 9
KING 10
KING 7
KING 8
DB
1400 W
1200 W
1000 W
800 W
600 W
400 W
200 W
0
200 E
400 E
600 E
800 E
1000 E
600 N
400 N
200 N
200 S
400 S
600 S
LEGEND
GEOLOGY
Triassic KARMUTSEN Formation (black to green, massive to porphyritic ± amygdaloidal units)
Diabase Dyke (massive – fine to medium grained)
Bedding attitude (dip indicated)
Structural attitude (faulting and/or shearing)
Airphoto lineament (photos; BC 79144 No. 156–158)
Outcrop area (shearing indicated)
Geological contact
Vein Quartz (Auriferous)
GEOPHYSICS
VLF-EM Anomaly
Magnetic Anomaly (low)
Resistivity (low)
SSESSMENT REPOR
24,283
SCALE
0 40 80 120 160
Metres
WESTWARD EXPLORATION LTD.
KING MINERAL CLAIMS
GENERAL COMPILATION
KAMAKA RESOURCES LTD.
Scale : 1 : 2,000
Fig : 4
Date : DEC. 1995