

GEOLOGICAL SURVEY BRANCH ASSESSMENT REPORTS

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CYPRUS CANADA INC. REPORT ON EXPLORATION AND DIAMOND DRILLING ON THE TAURUS PROJECT, LULU NO. 2 CLAIM, LIARD MINING DIVISION, NORTHWESTERN BRITISH COLUMBIA (104P/5) LAT. 59°16'19" N, LONG. 129°42'4"W

Claims owned by Operator

June 1996 Vancouver, B.C. : DOUGLAS BUSAT : CYPRUS CANADA INC.

GEOLOGICAL SURVEY BRANCH ASSESSMENT REPORT

> David Broughton Joseph Dion

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### **INTRODUCTION:**

The Taurus Property consists of 3 groups of mineral claims owned by Cusac Gold Mines Ltd., International Taurus Resources Ltd. and Douglas Busat. Work filed in this assessment report was completed on the Lulu No. 2 claim owned by Douglas Busat.

An I.P. and soils survey was completed over a portion of the Lulu claim in August, 1995. Two NQ diamond drill holes were completed on the claim in early May, 1996.

### LOCATION:

The Taurus Property is located 8 kilometres east of the townsite of Cassiar in northwestern British Columbia (Figure 1). Access to the property is via the paved Cassiar branch of Highway 37 from Watson Lake or Dease Lake.

### HISTORY:

The Cassiar area was first explored for placer gold during 1874 after the gold rush along Dease Lake in 1873. The earliest claims on the Taurus Property still in good standing were staked in 1934 and 1936. These claims and others surrounding them were explored intermittently, with major diamond drilling programs in 1993 and 1994. The Taurus Mine to the northwest of the Lulu No. 2 claim mined 240,000 tons of ore averaging 0.15 oz. Au/ton from 1981 to 1988.

Cyprus Canada Inc. entered into joint venture agreements with International Taurus Resources Inc., Cusac Gold Mines Ltd., and Douglas Busat early in 1995, to explore their ground surrounding the old Taurus Mine.

### CLAIMS

Table 1 contains the mineral claims on which the credit from exploration work is being applied too. The claims were surveyed by BC Land surveyors from the firm Underhill and Underhill using GPS equipment and transits.



Figure 1. Location and index map; diagrams modified from Nelson and Bradford (1993) and Geological Fieldwork (1989).



Mineral Claim	Record Number	Expiry Date After Assessment Credit Has Been Applied
Lulu No. 2	221887	09/24/2006
Bozo	221776	07/10/2006
Mountain Dew	221802	09/18/2006
Carl Fraction	342562	12/06/1998
Perry Fraction	338658	07/22/1998
Whale Fraction	338657	07/22/1998
Larry Fraction	342561	12/05/1998
Matt 1-6	342555-560	12/04/1998

### TABLE 1.

### REGIONAL GEOLOGY

The Taurus Property is located in the Sylvester allochthon which is a flat bottomed synclinorium of thrust stacked slices of Mississippian to Triassic ophiolite and island-arc type rocks, resting upon the miogeoclinal Cassiar Terrane (Nelson and Bradford, 1993). The property is predominantly underlain by flat lying massive and pillowed basalt flows, intercalated with lesser thicknesses of argillite. Ten kilometres west of the property the granite to granodiorite, Cretaceous Cassiar Batholith intruded the sediments of the Cassiar Terrane. Mineralization in the Taurus Property pre-dates the intrusion of the Cassiar Batholith. (Panteleyev and Diakow, 1982).

### LOCAL GEOLOGY

The lithologies of the project area include six main rock units. These include massive basalt and magnetic pillow basalt (often with jasperoidal pillow selvages), which structurally overlie chert, argillaceous chert, argillite and mudstone. These sediments are exposed in structurally disturbed areas with graphitic fault zones and breccias.

### **Rock Descriptions**

Basalt is dark to light green, aphanitic to phaneritic massive (T1) to intensely fractured. This unit is 100 to 250 metres thick, and hosts most of the mineralization occurring in the immediate vicinity of the property. Elsewhere on the Taurus Property this unit has intervals of pillow basalt with spherulitic jasperoidal patches (T1A), but this was not encountered during the current

drilling program. Altered versions of this unit are classified as T2 depending on the degree of the alteration present.

Chert (T7) and Argillaceous chert (T7A) are often faulted and sheared with graphite as fracture coatings, infilling brecciated areas and occurring along slickensided shear planes. Bedding is locally developed, but generally not recognized due to their faulted, broken up nature common along the contact with the overlying basalt.

Argillite (T6) is black, foliated, sheared and often graphitic with very little evidence of the original bedding/banding.

### Structure

Much of the structural interpretation in the area of the Busat property is done from compilation of surface outcrop exposures, geophysical surveys, and information from surrounding properties and deposits. Outcrop is limited on the property to a few exposures along the Snowy Creek and adjoining creeks.

A weak regional foliation trends 000 to 340° and dips steeply south. The Snowy Creek valley represents a prominent topographical feature associated with faulted/brecciated chert trending roughly northwest. A similar faulted and sheared chert unit is spatially associated with gold mineralization further to the west in the 88 Hill area of the Taurus Property. These structures occur at a high angle to mineralized pyritic quartz veins, which have a consistent 070 to 090 trend throughout the property area.

### Alteration

Basalt is pervasively altered to a chloritic +/- calcite +/- epidote or zoisitic? assemblage, suggestive of a lower greenschist metamorphic assemblage (Nelson and Bradford, 1993). In some areas the basalt is strongly ankeritized with local calcite and quartz microveining, this alteration is generally associated with mineralization.

### Mineralization

Mineralization located near the Busat property includes the former Taurus Mine, to the northwest and the producing Cusac mine (formerly Erickson) to the southwest. The Taurus and Cusac mines exploited various lode gold quartz vein systems as high grade mineable structures within Sylvester basalts. Mineralization is associated with strongly altered, bleached basalts injected with pyritized quartz veins. Similar, pyritic quartz vein mineralization occurs locally on

the Lulu No. 2 claim, south of the Snowy Creek chert, where a grab sample ran 2.55 g/t Au.

### DRILL HOLE GEOLOGY

The 1996 exploration program consisted of a total of 259.7 metres of diamond drilling in two NQ holes. The first hole, T96-79, tested for mineralization associated with the northwest trending Snowy Creek chert. The second hole, T96-80, was designed to test an I.P. anomaly presumed to be the contact with argillite to the south of the grid. Refer to Figure 3 for the drill hole locations and geology of the property. Drill logs are in Appendix A.

Selected sections of core were split for assaying by Chemex Labs, Vancouver. The split samples were crushed to 90 percent minus 60 mesh, then a representative 200 to 400 gram split was riffled and pulverized. A one assay ton aliquot was fire assayed with an A.A. finish.

Hole T96-79 was collared on the Lulu claim boundary, at approximately 25+25E, 7+50S, and drilled to the south at minus 45 degrees. It encountered strongly altered and fractured mafic flow (T2) from the start of the hole at 9.75 metres to 26.05 metres. Fractured sections are often brecciated with local gouge and trace pyrite. Weakly altered mafic flow continues to 98.6 metres downhole with some sections strongly fractured and sheared but with little or no quartz and only minor pyrite. The rock is sheared and faulted from 98.6 to 138.15 metres within argillaceous chert (Snowy Creek chert). This is the expression of outcrop further up the valley and consists of cherty rounded clasts in an argillaceous (locally graphitic) matrix. It also contains areas of chloritic, graphitic fault gouge and local trace pyrite. The rest of the hole encountered alternating altered and weakly altered mafic flow which is locally fractured and brecciated but with no significantly mineralized areas. The hole ended at 158.2 metres.

The only assay above background (0.03 g/t Au) from the hole was from a quartz vein at the downhole contact of the argillaceous chert, which returned 0.27 g/t Au over 2.0 metres. Assay results are included with the drill logs.

Hole T96-80 was collared at 12+00 E, 10+00S and drilled to the south at minus 50 degrees. It intersected intercalated faulted graphitic argillite and mafic flow with minor argillaceous chert. The hole collared in faulted graphitic argillite to 52.5 metres with local graphitic clayey gouge. The whole section is broken/blocky with 75 to 90% core recovery and 60 to 70% RQD. Ten metres of altered mafic flow (T2) occurs from 52.5 to 62.8 metres. The rock is light grey green bleached and locally fractured but lacks significant mineralization and quartz veining. The rest of the hole is comprised mainly of argillite with lesser



HOLE NO:	T96-80
LOCATION:	L12+00E, 10+00 S
TARGET:	IP ANOMALY
	T96-80
	OVB ARGILLITE MAFIC FLOW, ALTERED ARGILLITE, FAULT ZONE MAFIC FLOW, ALTERED ARGILLITE, FAULT ZONE MAFIC FLOW, FAULT ZONE MAFIC FLOW, FAULT ZONE MAFIC FLOW, MODERATELY ALTERED ARGILLITE, LECAL MAFIC FLEW EGH 101.5m
	1:1000 SECTION LOOKING

amounts of altered mafic flow and a small amount of chert in faulted brecciated argillite. The hole ended at 101.5 metres in foliated/sheared argillite. The only assay result above background (0.03 g/t Au) was returned from a fault zone at 70 metres which graded 0.07 g/t Au over 2.0 metres.

### GEOPHYSICS AND SOIL SURVEY

In preparation for these surveys approximately 2100 metres of 200 metre spaced lines with 25 metre stations was cut during the summer of 1995.

### GEOPHYSICS

Lloyd Geophysics Ltd. of Vancouver was contracted to conduct I.P. and ground magnetics surveys on the 1995 grid. Their report is in Appendix B.

The I.P. survey was completed using a pole-dipole configuration with a dipole spacing of 50 metres, readings at N=1 through N=6, on 200 metre spaced lines. The magnetics survey was completed at 12.5 metre stations on the same lines. In general, the I.P. survey was successful in defining broad anomalous zones of mineralization and/or argillite, but due to the large spacing was unable to separate zones less than 25 metres wide.

The grid is dominated by the chargeability response associated with two distinct north to northwest trends associated with the Snowy Creek chert body. Low resistivities and high chargeabilities at the south end of the grid are assumed to be related to the underlying argillite to the south. The I.P. survey defines a marked break in the general northwest-southeast trends. This structure was mapped on surface and follows the prominent topographical feature along the Snowy Creek valley.

The magnetic survey is relatively featureless due to the negligible magnetic signature of the majority of the basalts, as well as the sediments. Magnetic highs are presumed to be related to magnetic jasperoidal basalt.

### SOIL SURVEY

Forty soil samples collected during the 1995 summer program were taken from the "B" horizon at 50 metre stations on 200 metre spaced lines. Sample depths ranged up to 0.5 metre. The samples were sent to Chemex Labs, Vancouver, where they were dried, sieved to minus 80 mesh, and fire assayed with an A.A. finish. Results are plotted on Figure 3, and indicate a number of weakly to moderately anomalous responses. The 1996 drilling focussed on the I.P. and geological targets, therefore some of the soil responses remain unexplained.

### CONCLUSIONS AND RECOMMENDATIONS

During 1995-96 an exploration program was carried out on the gridded portion of the Lulu No. 2 claim. This survey included two diamond drill holes, geological mapping, prospecting, soils and geophysics, and failed to outline any new significantly mineralized zones.

Due to a lack of any significant discovery or mineralized zone it is recommended that no further work be carried out at this time.

### STATEMENT OF COSTS

### Period of Work August 1- September 11, 1995

Geophysical Surveys Done By:	Lloyd Geophysics Inc. 1007-1166 Alberni Street Vancouver, B.C. V6E 3Z3
I.P. survey (2.1 line km, 2 days @ \$1350)	\$2700.00
Ground Magnetics survey (2.1 line km @ \$130)	\$273.00
Room and Board for Geophysical Crew (2 days x 6 m	en x \$100) \$1200.00
Linecutting (2 men x 3 days @ \$150)	\$900.00
Geophysical Interpretation & Report Writing	\$1211.41
Subtotal	\$6284.41
Geological mapping, David Broughton, Cyprus Canad (2 days x \$250)	a Inc. \$500.00
(address, Site 23, C30, RR#6, Vernon, B.C.) (5 days @ \$125)	\$625.00
Room & board for soil sampler (5 days @ \$100)	\$500.00
Gold assays of soil samples (40 @ \$20) (assays by Chemex Labs, 212 Brooksbank Ave., N. Vancouver, B.C. V7J 2C1)	\$800.00

Subtotal \$2425.00

Period of Work: May 7 - 12, 1996

Diamond Drilling Done By: D.J. Drilling Co. Ltd. 2115 - 129<sup>th</sup> St., S. Surrey, B.C. V4A 8H6 Drill hole Metres Drilling Muds Tests Total T96-79 158.2 \$8443.19 \$240.00 \$150.00 \$8833.69 T96-80 101.5 \$5483.38 \$300.00 \$100.00 \$5883.38 Mobilization \$3900.00 D6 Cat 25hrs @ \$95 \$2375.00 Excavator 5 hrs @ \$125 \$625.00 Core Boxes 40 @ \$9 \$360.00 Subtotal \$21977.07

Core samples assayed for Au g/t 49 samples @ \$20 per sample <u>\$980.00</u> (assays by: Chemex Labs Ltd., 212 Brooksbank Ave., N. Vancouver, B.C. V7J 2C1)

### Camp and Other Costs

Drillers Room & Board (4 men x 6 days @ \$100)	\$2400.00
Fuel for drill, cat and backhoe (6 days x 200 l x \$0.50/ l)	\$600.00
Wages & benefits: Geologist, Joseph Dion, Cyprus Canada Inc, (6 days @ \$200)	\$1200.00
Wages & benefits: Core splitter, Alan McChesney, Cyprus Canada Inc, (6 days @ \$150)	\$900.00
Wages: Cook, Murdena MacDonald, Cyprus Canada Inc, (6 days @ \$150)	\$900.00

Total Cost	\$40616.48
Subtotal	<u>\$8950.00</u>
Map preparation: Draftsman, Zbijniew Wtyrwal, Cyprus Canada Inc. (2 days @ \$175)	\$350.00
Report Writing Costs, David Broughton, Project Geologist , Cyprus Canada Inc., (2 days @ \$250)	\$500.00
Truck rental + gas (6 days @ \$50) (rental from Norcan Rentals, Mile 917.4 Alaska Highway, Whitehorse, Yukon, Y1A 3E5)	\$300.00
Room & Board for Geologist, Geotechnician, Cook (3 x 6 days @ \$100)	\$1800.00

### **REFERENCES:**

- Nelson, J.L and Bradford, J.A., 1993. Geology of the Midway-Cassiar area, Northern British Columbia, MEMPR, Bulletin 83, 94p.
- Panteleyev, A. and Diakow, L.J., 1982. Cassiar gold deposits, McDame map-area (104P/4,5); Geological Fieldwork 1981, MEMPR, Paper 1982-1, p 156-161.

### STATEMENTS OF QUALIFICATIONS

I, Joseph Dion of Cyprus Canada Inc. do hereby certify that:

- 1. I am a contract geologist with Cyprus Canada Inc. and reside at 6303 -315 Southampton Drive S.W., Calgary, Alberta, T2W 2T6.
- 2. I have a BSc from The University of Saskatchewan, in 1987.
- 3. I have been employed as a contract geologist with Cyprus Canada since June, 1995.
- 5. I worked on the Taurus Property as a geologist in May 1996.

Joseph Dion

### STATEMENT OF QUALIFICATIONS

I, David Broughton of Cyprus Canada Inc. do hereby certify that:

- 1. I am a staff project geologist with Cyprus Canada Inc. and reside at 1134 50B Street, Delta, B.C., V4M 2W1.
- 2. I have a Bsc and Msc from The University of Waterloo, Ontario in 1984 and 1987, respectively.
- 3. I have been employed as a geologist with Cyprus Canada since November 1992.
- 5. I have worked on the Taurus Property since January 1995.

David Broughton

## APPENDIX A

## DRILL LOGS, ASSAY CERTIFICATES

Northing: Easting: Elevation: Collar Azi.: Collar Dip: Hole Length Casing: Province: Date Started Completed: Drilled by: Sample Nos: Analytical T Logged By: Assay Summa Purpose:	: Jun, 1996 -750.0 2525.0 1000.0 -1 -45.0 (m): 158.20 PULLED BRITISH COLUMBIA. CANADA I: MAY 8, 1996 MAY 9, 1996 DJ ORILLING 120001-120035 .ab: CHEMEX, VANCOUVER JOSEPH DION Y: TEST SOUTH FLANK OF THE S	CYPRUS CANADA INC. DRILL HOLE RECORD *** Dip Tests *** Depth Azi. Dip 26.2 -45.0 157.0 -46.0	Drill Hole: Northing: Basting: Project: Property: Drill type: Dip/Azi Tes Grid: Core Size:	Page: 1 07 4 T96-79 7+50S 25+25R TAURUS BUSAT I.ONGYFAR 3A t Method: SPERRYSUN 1995 NQ
From To (m) (m)	Geolo	gy Sample	From To Lngth REC ROD FGPY (m) (m) {m} % % %	CGPY QV SG AU 8 8 G/T
.00 9.75 9.75 26.05 26.05 46.70 46.70 52.00 52.00 81.10 81.10 98.60 98.60 138.15 138.15 145.30 145.30 158.20	SUMMARY LOG OVERBURDEN ALTERED MAFIC FLOW STRONGLY BRECC MAFIC FLOW MAFIC FLOW WEAKLY ALTERED ALTERED MAFIC FLOW MODERATELY ALT GRAPHITIC BRECCIATED FAULT ZONE ALTERED MAFIC FLOW MODERATELY ALT MAFIC FLOW BRECCIATED FAULT ZONE	TATED ERED BRECCIATED ERED		

Pres	T'96-7	(continued)	10	E		Itert	(PEG)	BCE	Party	Page	: 2	of 4	(
from (m)	То (m)	Geology	Sample	(m)	(m)	(m)	8 8	8 ROD	FGPY 8	CGPY %	8 8	SG	AU G/T
. 00	9.75	OVERBURDEN									1		
9.75	26.05	ALTERED MAPIC FLOW STRONGLY BRECCIATED Surficial weathering to 12.8 with pervasive/fractur hematite/limonite, Dark brown to light to mediu grey,fine to medium grained,hardness 4,no magnetic,local intense brecciation,sections ar sheared with slickensided shear surfaces,narro clayey/graphitic gouge,the section is moderatel altered from 15.3 to 26.05, bleached/calcite and F											
		(chloritic). Sheared lower contact at 55 deg. 9.75 12.00 STRONG SURFICIAL WEATHERING, INTENSI BRECCIATION QUARTZ/CALCITE INFIL FRACTURES.	120001 120002	9.75 12.00	12.00 14.00	2.25	90 95	25 40	.0 tr	.0 .0	1.0 1.0		<.030 <.030
		<ul> <li>14.30 Slickensided fracture surface at 41</li> <li>degrees to the core axis.</li> <li>15.30 18.00 Weathered fractures hematitie/limonite.</li> <li>16.00 NARROW CALCTE</li> </ul>	5 120003	16.00	18.00	2.00	100	50	tr	.0	.0		<.03
		VEINING,WEATHERED(HEMATITE), BLEACHED. 17.80 Calcite/ankeritic/hematite coated vug. 18.30 Slickensides at 30 degrees to the corr	120005	18.00	20.00	2.00	100	80	tr	.0	1.0		<.03
		axis. 20.00 22.00 BLEACHED BRECCTATED, TRACE DISS. PY. 22.00 24.00 STRONGLY BLEACHED, ANKERITE, CALCITI VEINING.	120006 120007	20.00 22.00	22.00 24.00	2.00 2.00	100 100	80 85	tr tr	.0 .0	2.0 .0		<.030 <.030
-		core axis. Slickensided fracture with graphite at 62 degrees to											
		Che Core 3738. 24.00 26.00 MODERATELY BRECCIATED, BLEACHED, INTERSTITIAL CALCITE 26.00 28.00 WEAK TO MOD. BLEACHING TO WEAKLY ALTEREI	120008	24.00 26.00	26.00 28.00	2.00 2.00	100 100	80 65	tr tr	.0 .0	.0 2.0		<.030
26.05	46.70	Basalt. MAFIC FLOW Light to medium green,fine grained,massive,local breccisted sections,chloritic scattered narrow											
		irregular calcite/quartz-calcite veinlets,weakly blached to 27.6,locally weakly ankeritized, trace local Py. 26.05 Sheared contact at 55 degrees to the											
		core amis. 27.00 2-3 cm calcitic shear at 35 degrees to	×										
		the core axis. 27.60 28.00 Narrow quarts/calcite veinlets at 50 degrees to the core axis,trace vein selvags euhedral Py. 30.80 31.00 Several narrow calcite/chlorite shears											
		at 40 to 55 degrees to the core axis. 33.30 2cm calcite shear at 20 degrees to the core axis. 35.00 2 cm quartz/carb veinlet (barren) at 20											
		degrees to the core axis. 37.00 39.00 SCATTERED NARROW QUARTZ/CARF	120010	37.00	39.00	2.00	100	85	tr	. 0	1.0		<.030
		VEINLETS, TRACE PY. 37.90 38.20 Resciated calcitic/chloritic trace Py. 39.00 41.00 QUARTZ/CALCITE VEINING, QUARTZ VEIN AN 40.50.40.90 Calcite/quartz vein.subparallel corr	120011	39.00	41.00	2.00	100	85	tr	. 0	2.0		<.030
		axis(long),vein is offset by later chlorite/calcite fractures at 60 to 80 degrees to the core axis.											
		41.00 43.00 WEAKLY (CALCITE/ANKERITE), BLEACHED. 41.50 45.40 ALTERED MAFIC FLOW ankeritized/calcite.	120012	41.00	43.00 45.00	2.00	100 100	90 90	.0	.0 .0	1.0 tr		<.030
		contact at 60 degrees to the core axis. 43.70 1-2 cm quartz veinlet, ankeritized vein selvage, barren. 44.40 44.50 Shear, strong calcite/bleaching at 85	120014	45.00	47.00	2.00	100	95	tr	.0	1.0		<.030
		degrees to the core axis.											
46.70	52.00	MAFIC FLOW WEAKLY ALTERED 3-5% Marrow quarts and qts/carb. Veining,local weak to moderate brecciation light green,f.g., massive,brecciated sections with narrow related shearing veining at 15 to 70 degrees to the core ssis non magnetic,trace local Py.					_						
		47.00 49.00 QTZ/CARB VEINING, TRACE LOCAL PY. 49.00 51.00 WEAR CAL ALTERATION, LOCAL BRECCIATION.	120015 120016 120017	47.00 49.00 51.00	49.00 51.00 53.00	2.00 2.00 2.00	100 100 100	75 90 90	tr tr tr	.0 .0 .0	3.0 4.0 2.0		<.030 <.030 <.030
52.00	81.10	MAFIC FLOW MODERATELY ALTERED											
		Fractured, locally bracciated with up to 10% quarts and qtx/carb veining scattered narrow fault zones with narrow sections of clayey gouge, and interstitial clay zones which are friable and crumbly, light greeg green to. Light green, f.g., calcite altered, local moderate bleaching, chloritic trace Py, non magnetic, locally soft, hardness approx.4.						والأحد وإراقي والمتعاومين والمتحارفة والمتحاولة والمتحار			-		
		57.80 Shear/gouge at 30 degrees to the core axis. 59.00 Quartx vein,3cm wide,white to											
		grey, silicified vein selvages, 2-3 diss Py at 25 degrees to the core axis. Slickensided shear at 35 degrees to the core axis. 59.00 61.00 QT% VEIN/2-3% DISS PY.	120018	59.00	61.00	2.00	100	50	1.0	.0	3.0		<.030
		<ul> <li>62.70 63.70 Patchy moderate silicification/quarts veining, irregular calcite veina.</li> <li>66.30 67.90 Fault zons/shear zone, upper contact 35 degrees to the core axis locally</li> </ul>	120020 120021 120022	63.00 65.00 67.00	65.00 67.00 69.00	2.00 2.00 2.00	100 100 100	80 60 70	tr tr tr	.0 .0 .0	.0 3.0 4.0		<.030 <.030 <.030 <.030
		friable/crumbly 66.6 66.9 silicified shear with clay coated shear											

From To	Geology	Sample	From	To	Ingth	REC	ROD	FGPV	CGPV	07	SC	
(m) (m)	Georogy	58	(m)	(m)	(m)	8	ð	-	8	8		G/
	planes,quart¤ calcite and ankerite,trace Py,ehearing at 40 degrees to the core											
	axis. 67.40 Clayey gouge at 60 degrees to the core axis.											
	71.00 72.00 Bagalt,very weak alteration. 72.00 72.30 FAULT/SHEAR ZONE,narrow clayey gouge and											
	ductile shearing,strong calcite at 60 degrees to the core axis.											
	73.10 Quartz (Shirregular grey/white quartz. fracture,irregular grey/white quartz. 74.30 81.10 Sections intensely fractured/brecciated											
	with interstitial clay and clayey gouge,local healed breccia											
	(quartz/calcite). 74.50 2cm clayey gouge at 30 degrees to the											
	75.00 77.00 QTZ/CARB VEINING, TRACE PY. 75.60 76.00 Strong pervasive calcite	120023	75.00	77.00	2.00	100	70	tr	.0	3.0		٢.
	alteration, irregular quartz calcite vein. Contacts at 30 degrees to the core			1								
	77.00 79.00 SAME AS 120023.	120024	77.00	79.00	2.00	95	75	tr	.0	2.0		٢.
	79.00 81.00 QTZ/CARB. VEINING LOCAL BRECCIATION. 81.00 83.00 CHERTY ARGILITE/FAULT ZONE 82.6-83.3.	120025	79.00 81.00	81.00 83.00	2.00	95 80	65 60	tr tr	.0 .0	2.0		<. <.
31.10 98.6	ALTERED MAFIC FLOW MODERATELY ALTERED BRECCLATED Light grey green,f.g.,moderately altered											
	clay,chlorite,calcite,bleached, local brecciation,faulted sections with clayey gouge,trace											
	B2.60 83.25 Graphitic fault zone,contact at 10 to 15											
	degrees to the core axis Cherty Argillite,tr Py 93.3 93.7 healed											
	94.80 2cm shear,clayey,slickensided at 5 to 10 degrees to the core axis.											
8.60 138.1	Cherty rounded clasts within a argillaceous											
	(graphitic) matrix Sheared argillaceous chert,Dark grey to black,broken,brecciated,graphitic, areas of											
	fault gouge, shearing with slickensides, alteration includes very weak calcite, bleaching, graphite occuring interstitially between chert.lower contact											
	marked by a lom chloritic clayey gouge at 80 degrees to the core axis trace local Py associated with											
	shearing. Pragments (volc.?) are weakly carbonitized,only weakly or non silicified, possibly emission to charty volcanic on surface											
	99.40 101.50 42 % recovery,5 % RQD, broken crumbly							1				
	core, shearing at 25 degrees to the core axis. 101 50 102 70 80% recovery 60% POD broken/friable											
н		•	t	a ;	i i	11	1	1	1	;	1 1	
ł	core,shearing at 60 degrees to the					H	1			1		
	103.30 103.50 Broken/friable core quartz microfractures, fault gouge at 55.											
	108.30 Graphitic,slickensided shear at 5 degrees to the core axis.								. "			
	109.00 111.00 PARGMENTED/SREARED CHERTY GRAPHITIC ARGILLITE.										I 1	
ii ii	109.40 Graphitic slickensided shear plane at	120027	109.00	111.00	2.00	90	70	tr	tr	. 0		٢.
	109.40 Graphitic,slickensided shear plane at 15 degrees to the core axis. 111.00 113.00 SAME AS 120028.	120027	109.00	111.00 113.00	2.00	90 90	70 90	tr tr	tr tr	. 0		<i>د.</i>
	109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis. 111.00 113.00 SAME AS 120028. 115.00 117.00 CRUMELY SECTIONS WITH BROKEN CORE. 115.00 116 70 Broken sheared core core is in places	120027 120028 120029 120030	109.00 111.00 113.00 115.00	111.00 113.00 115.00 117.00	2.00 2.00 2.00 2.00	90 90 75 90	70 90 75 40	tr tr tr	tr .0 .0	0. 0. 0.		<
	109.40 Graphitic,slickensided shear plane at 15 degrees to the core axis. 111.00 113.00 SAME AS 120028. 115.00 117.00 CRUMBLY SECTIONS WITH BROKEN CORE. 116.00 116.70 Broken sheared core,core is in places. 117.50 Slickensided shear plane,1% diss. Py at 50 degrees to the core axis.	120027 120028 120029 120030 120031 120032	109.00 111.00 113.00 115.00 117.00 119.00	111.00 113.00 115.00 117.00 119.00 121.00	2.00 2.00 2.00 2.00 2.00 2.00	90 90 75 90 95 85	70 90 75 40 75 30	tr ttttttt	tr .0 .0 .0	.0. .0 .0 .0		<<<
	109.40       Graphitic,slickensided shear plane at 15 degrees to the core axis.         111.00       113.00       SAME AS 120028.         115.00       117.00       CRUMBLY SECTIONS WITH BROKEN CORE.         116.00       116.70       Broken sheared core,core is in pleces.         117.50       Slickensided shear plane,1% diss. Py at 50 degrees to the core axis.         119.50       122.50       15-20% RQD,75-60% recovery,broken core,crumbly,shearing at 40 degrees to	120027 120028 120029 120030 120031 120032	109.00 111.00 113.00 115.00 117.00 119.00	111.00 113.00 115.00 117.00 119.00 121.00	2.00 2.00 2.00 2.00 2.00 2.00	90 90 75 90 95 85	70 90 75 40 75 30	tr trrtr trr tr	tr .0 .0 .0	. 0 . 0 . 0 . 0 . 0		< . < . < . < .
	<ul> <li>109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis.</li> <li>111.00 113.00 SAME AS 120028.</li> <li>115.00 117.00 CRUMBLY SECTIONS WITH BROKEN CORE.</li> <li>116.00 Broken sheared core, core is in pieces.</li> <li>117.50 Slickensided shear plane, 1% disc. Py at 50 degrees to the core axis.</li> <li>119.50 122.50 15-20% RQD, 75-80% recovery, broken core, crumbly, shearing at 40 degrees to the core axis.</li> <li>123.50 Shearing at 25 degrees to the core axis</li> <li>125.70 Shearing at 25 30 degrees to the core axis</li> </ul>	120027 120028 120029 120030 120031 120032	109.00 111.00 113.00 115.00 117.00 119.00	111.00 113.00 115.00 117.00 119.00 121.00	2.00 2.00 2.00 2.00 2.00	90 90 75 90 95 85	70 90 75 40 75 30	tr trtrr trr tr	tr .0 .0 .0	.0. .0 .0 .0		< . < . < . < .
	<ul> <li>109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis.</li> <li>111.00 113.00 SAME AS 120028.</li> <li>115.00 117.00 CRUMBLY SECTIONS WITH BROKEN CORE.</li> <li>116.00 116.70 Broken sheared core, core is in pleces.</li> <li>117.50 Slickensided shear plane, 1% diss. Py at 50 degrees to the core axis.</li> <li>119.50 122.50 15-20% RQD, 75-80% recovery, broken core, crumbly, shearing at 40 degrees to the core axis.</li> <li>123.50 Shearing at 25 degrees to the core axis is.</li> <li>125.70 25-30% RQD.</li> <li>126.00 126.70 25-30% RQD.</li> </ul>	120027 120028 120029 120030 120031 120032	109.00 111.00 113.00 115.00 117.00 119.00	111.00 113.00 115.00 117.00 119.00 121.00	2.00 2.00 2.00 2.00 2.00	90 90 75 90 95 85	70 90 75 40 75 30	tr trrtr tr	tr .0 .0 .0	.0. .0 .0 .0		<<<<<
	<ul> <li>109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis.</li> <li>111.00 113.00 SAME AS 120028.</li> <li>115.00 117.00 CRUMELY SECTIONS WITH BROKEN CORE.</li> <li>116.00 116.70 Broken sheared core, core is in pieces.</li> <li>117.50 Slickensided shear plane, 1% diss. Py at 50 degrees to the core axis.</li> <li>19.50 122.50 12-20% RQD, 75-60% recovery, broken core, crumbly, shearing at 40 degrees to the core axis.</li> <li>123.50 Shearing at 25 degrees to the core axis 125.70 Shearing at 25 30 degrees to the core axis.</li> <li>126.00 126.70 25-30% RQD.</li> <li>128.30 Shearing at 15 degrees to the core axis 131.00 Shearing at 30 degrees to the core axis 132.60 Quartz filled shear at 35 degrees to</li> </ul>	120027 120028 120029 120030 120031 120032	109.00 111.00 113.00 115.00 117.00 119.00	111.00 113.00 115.00 117.00 119.00 121.00	2.00 2.00 2.00 2.00 2.00	90 90 75 90 95 85	70 90 75 40 75 30	tr trttr tr t t t -	tr -0 .0 .0	.0 .0 .0 .0		< <. <. <.
	<ul> <li>109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis.</li> <li>111.00 113.00 SAME AS 120028.</li> <li>115.00 117.00 CRUMBLY SECTIONS WITH BROKEN CORE.</li> <li>116.00 Broken sheared core, core is in pieces.</li> <li>117.50 Slickensided shear plane, 1% diss. Py at 50 degrees to the core axis.</li> <li>119.50 122.50 15-20% RQ0, 75-60% recovery, broken core, crumbly, shearing at 40 degrees to the core axis.</li> <li>123.50 Shearing at 25 degrees to the core axis axis.</li> <li>126.70 25-30% RQ0.</li> <li>126.30 Shearing at 15 degrees to the core axis 131.00 Shearing at 30 degrees to the core axis 132.60 Quartz filled shear at 35 degrees to the core axis.</li> <li>134.15 136.15 ARGILACEOUS CREPT.</li> </ul>	120027 120028 120029 120030 120031 120032	109.00 111.00 113.00 115.00 117.00 119.00	111.00 113.00 115.00 117.00 121.00	2.00 2.00 2.00 2.00 2.00 2.00	90 90 75 95 85	70 90 75 40 75 30	tr trttttr tr	tr .0 .0 .0	.0 .0 .0 .0		<<
	<ul> <li>109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis.</li> <li>111.00 113.00 SAME AS 120028.</li> <li>115.00 117.00 CRUMBLY SECTIONS WITH BROKEN CORE.</li> <li>115.00 116.70 Broken sheared core, core is in pieces.</li> <li>117.50 Slickensided shear plane, 1% diss. Py at 50 degrees to the core axis.</li> <li>119.50 122.50 15-20% RQD, 75-80% recovery, broken core, crumbly, shearing at 40 degrees to the core axis.</li> <li>123.50 Shearing at 25 degrees to the core axis</li> <li>125.70 Shearing at 25 30 degrees to the core axis</li> <li>126.00 126.70 25-30% RQD.</li> <li>128.30 Shearing at 15 degrees to the core axis</li> <li>133.00 Shearing at 30 degrees to the core axis</li> <li>133.60 Quartz filled shear at 35 degrees to the core axis.</li> <li>134.15 136.15 ARGILLACEOUS CREMT.</li> <li>136.05 138.15 ARGILLACEOUS CREMT.</li> <li>136.15 138.15 9% OTZ 136.5-137.6.90% GRAPHITE</li> </ul>	120027 120028 120029 120030 120031 120032	109.00 111.00 113.00 115.00 115.00 119.00	111.00 115.00 117.00 121.00 121.00	2.00 2.00 2.00 2.00 2.00 2.00	90 90 95 95 85 95	70 90 75 30 85	tr trrttr tr tr tr	tr .00.00 .0	.0 .0 .0 .0 .0		<<<
	<ul> <li>109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis.</li> <li>111.00 113.00 SAME AS 120028.</li> <li>115.00 117.00 CRUMELY SECTIONS WITH BROKEN CORE.</li> <li>116.00 116.70 Broken sheared core, core is in pieces.</li> <li>117.50 Slickensided shear plane, 1% diss. Py at 50 degrees to the core axis.</li> <li>19.50 122.50 15-20% RQD, 75-60% recovery, broken core, crumbly, shearing at 40 degrees to the core axis.</li> <li>123.50 Shearing at 25 degrees to the core axis at 30 degrees to the core axis.</li> <li>125.70 Shearing at 25 degrees to the core axis.</li> <li>126.00 126.70 25-30% RQD.</li> <li>128.30 Shearing at 15 degrees to the core axis 131.00 Shearing at 15 degrees to the core axis the core axis.</li> <li>131.01 Shearing at 15 degrees to the core axis 132.60 Quartz filled shear at 35 degrees to the core axis.</li> <li>134.15 136.15 ARGILLACEOUS CREPT.</li> <li>136.15 138.15 90% QTZ 136.5-137.6,90% GRAPHITE 137.6-138.15.</li> <li>136.50 137.60 90% white fracture quartz with</li> </ul>	120027 120028 120029 120030 120031 120032	109.00 111.00 113.00 115.00 117.00 119.00	111.00 115.00 117.00 121.00 121.00	2.00 2.00 2.00 2.00 2.00 2.00 2.00	90 90 95 85 95	70 90 75 40 75 30 85 75	tr trr trr tr tr tr tr	tr tr	.0 .0 .0 .0 .0		< <. <. <.
	<ul> <li>109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis.</li> <li>111.00 113.00 SAME AS 120028.</li> <li>115.00 117.00 CRUMBLY SECTIONS WITH BROKEN CORE.</li> <li>116.00 Broken sheared core, core is in pieces.</li> <li>117.50 Slickensided shear plane, 1% diss. Py at 50 degrees to the core axis.</li> <li>119.50 122.50 15-20% RQD, 75-80% recovery, broken core, crumbly, shearing at 40 degrees to the core axis.</li> <li>123.50 Shearing at 25 degrees to the core axis axis.</li> <li>126.00 126.70 25-30% RQD.</li> <li>126.30 Shearing at 15 degrees to the core axis 131.00 Shearing at 30 degrees to the core axis 132.60 Quartz filled shear at 35 degrees to the core axis.</li> <li>134.15 136.15 ARGILLACEOUS CHEPT.</li> <li>136.00 Clayey mud filled fracture at 10 degrees to the core axis.</li> <li>136.15 138.15 90% QTZ 136.5-137.6,90% GRAPHITE 137.6-138.15.</li> <li>136.50 137.60 90% white fracture duartz with therstitial graphic/md, 2% Py associated with the fracture infilling contact at 55 degrees to the core axis</li> </ul>	120027 120028 120030 120030 120031 120032	109.00 111.00 113.00 115.00 117.00 119.00	111.00 113.00 115.00 117.00 121.00 121.00	2.00 2.00 2.00 2.00 2.00 2.00 2.00	90 90 75 95 85 95 90	70 90 75 40 75 30 85	tr tr tr tr tr tr tr	tr .0 .0 .0	.0 .0 .0 .0 .0		< <. <. <.
	<ul> <li>109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis.</li> <li>111.00 113.00 SAME AS 120028.</li> <li>115.00 117.00 CRUMBLY SECTIONS WITH BROKEN CORE.</li> <li>115.00 116.70 Broken sheared core, core is in pieces.</li> <li>117.50 Slickensided shear plane, 1% diss. Py at 50 degrees to the core axis.</li> <li>119.50 122.50 15-20% RQD, 75-80% recovery, broken core, crumbly, shearing at 40 degrees to the core axis.</li> <li>123.50 Shearing at 25 degrees to the core axis</li> <li>125.70 Shearing at 25 degrees to the core axis</li> <li>126.00 126.70 25-30% RQD.</li> <li>126.30 Shearing at 15 degrees to the core axis</li> <li>133.00 Shearing at 30 degrees to the core axis</li> <li>133.60 Quartz filled shear at 35 degrees to the core axis.</li> <li>134.15 136.15 ARGILLACEOUS CREMT.</li> <li>136.15 138.15 9% QTZ 136.5-137.6,90% GRAPHITE 137.6-138.15.</li> <li>136.50 137.60 90% white fracture quartz with interstitial graphite/mud, 2% Py associated with the fracture infilling contact at 35 degrees to the core axis.</li> <li>137.60 138.15 95% graphite, broken, leading to the coreaxis.</li> </ul>	120027 120028 120029 120030 120031 120032	109.00 111.00 113.00 117.00 117.00 119.00	111.00 113.00 115.00 117.00 119.00 121.00	2.00 2.00 2.00 2.00 2.00 2.00 2.00	90 90 95 85 95 95	70 90 75 30 85 75	tr trttrt tr tr tr tr tr	tr .0 .0 .0 .0	0. .0 .0 .0 .0		< . < . < . < .
A 15 146 7	<ul> <li>109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis.</li> <li>111.00 113.00 SAME AS 120028.</li> <li>115.00 117.00 CRUMELY SECTIONS WITH BROKEN CORE.</li> <li>116.00 Broken sheared core, core is in pieces.</li> <li>117.50 Slickensided shear plane, 1% diss. Py at 50 degrees to the core axis.</li> <li>119.50 122.50 15-20% RQD, 75-60% recovery, broken core, crumbly, shearing at 40 degrees to the core axis.</li> <li>123.50 Shearing at 25 degrees to the core axis</li> <li>125.00 126.70 25-30% RQD.</li> <li>126.00 126.70 25-30% RQD.</li> <li>128.30 Shearing at 15 degrees to the core axis 131.00 Shearing at 10 degrees to the core axis 132.60 Quartz filled shear at 35 degrees to the core axis.</li> <li>134.15 136.15 ARG TLLACEOUS CREMT.</li> <li>136.00 Clayey mud filled fracture at 10 degrees to the core axis.</li> <li>136.50 137.60 30% white fractured quartz with interstitial graphite/mud, 2% Py associated with the fracture infilling contact at 55 degrees to the core axis.</li> <li>137.60 138.15 95% graphite, broken, leading to the contact at 138.15.</li> </ul>	120027 120028 120029 120030 120031 120032	109.00 111.00 113.00 115.00 117.00 119.00	111.00 115.00 117.00 119.00 121.00	2.00 2.00 2.00 2.00 2.00 2.00	90 905 905 95 85 95 95	90 75 30 85 75	tr trrttr trr tr tr tr tr	tr tr .0 .0 .0	.0 .0 .0 .0 .0		< < <. <.
8.15 145.30	<ul> <li>109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis.</li> <li>111.00 113.00 SAME AS 120028.</li> <li>115.00 117.00 CRUMELY SECTIONS WITH BROKEN CORE.</li> <li>116.00 Broken sheared core, core is in pieces.</li> <li>117.50 Slickensided shear plane, 1% diss. Py at 50 degrees to the core axis.</li> <li>119.50 122.50 15-20% RQD, 75-80% recovery, broken core, crumbly, shearing at 40 degrees to the core axis.</li> <li>123.50 Shearing at 25 degrees to the core axis axis.</li> <li>126.00 126.70 25-30% RQD.</li> <li>128.30 Shearing at 15 degrees to the core axis 131.00 Shearing at 30 degrees to the core axis 132.60 Quartz filled shear at 35 degrees to the core axis.</li> <li>134.15 136.15 ANGILLACEOUS CHEPT.</li> <li>136.00 Clayey mud filled fracture at 10 degrees to the core axis.</li> <li>136.15 138.15 90% QTZ 136.5-137.6,90% GRAPHITE 137.6-138.15.</li> <li>136.50 137.60 90% white fracture quartz with interstitial graphite/moid, 2% Py associated with the fracture infilling contact at 55 degrees to the core axis.</li> <li>137.60 138.15 95% graphite, broken, leading to the contact at 138.15.</li> <li>ALTERED MAPIC FLOW MODERATELY ALTERED fight grey buff, f.g. To m.g., massive to brecciated (healed) bleached, calcite along</li> </ul>	120027 120028 120030 120030 120031 120032	109.00 111.00 113.00 117.00 119.00	111.00 113.00 115.00 119.00 121.00	2.00 2.00 2.00 2.00 2.00 2.00 2.00	90 90 95 85 95 95	70 90 75 30 85 75	tr trrttr tr tr tr tr	tr .0 .0 .0 .0	.0 .0 .0 .0 .0		<<<<
8.15 145.30	<ul> <li>109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis.</li> <li>111.00 113.00 SAME AS 120028.</li> <li>115.00 117.00 CRUMBLY SECTIONS WITH BROKEN CORE.</li> <li>115.00 116.70 Broken sheared core, core is in pieces.</li> <li>117.50 Slickensided shear plane, 1% diss. Py at 50 degrees to the core axis.</li> <li>119.50 122.50 15-20% RQD, 75-80% recovery, broken core, crumbly, shearing at 40 degrees to the core axis.</li> <li>123.50 Shearing at 25 degrees to the core axis</li> <li>125.70 Shearing at 25 degrees to the core axis</li> <li>126.00 126.70 25-30% RQD.</li> <li>126.00 126.70 25-30% RQD.</li> <li>126.00 Shearing at 30 degrees to the core axis</li> <li>133.00 Shearing at 30 degrees to the core axis</li> <li>134.15 136.15 ARGILLACEOUS CREMT.</li> <li>136.15 138.15 ARGILLACEOUS CREMT.</li> <li>136.50 137.60 90% white fractured quartz with interstital graphite/mud, 2% Py associated with the fracture infilling contact at 55 degrees to the core axis.</li> <li>137.60 138.15 95% graphite, broken, leading to the contact at 136.15.</li> <li>ALTERED MAPIC FLOW MODERATELY ALTERED Light grey buff, fg. To m.g., massive to brecciated(healed)</li> <li>JHAPTIC FLOW MODERATELY ALTERED Light grey buff, fg. To m.g. Massive to brecciated(healed)</li> <li>JHAPTIC FLOW MODERATELY ALTERED Light Grey Duff, fg. To m.g. Massive to brecciated(healed)</li> <li>JHAPTIC FLOW MODERATELY ALTERED Light Grey Duff, fg. To m.g. Massive to brecciated(healed)</li> <li>JHAPTIC FLOW MODERATELY ALTERED Light Grey Duff, fg. To m.g. Massive to brecciated(healed)</li> <li>JHAPTIC FLOW MODERATELY ALTERED</li> <li>JHAPTIC F</li></ul>	120027 120028 120029 120030 120031 120032 120033 120033 120034	109.00 111.00 113.00 117.00 117.00 119.00 134.15 136.15 138.15	1111.00 113.00 115.00 119.00 121.00 136.15 136.15	2.00 2.00 2.00 2.00 2.00 2.00 2.00 2.00	90 90 95 90 95 85 95 90 95	70 90 75 40 75 30 85 75	tr trr trr tr tr tr tr tr	tr .0 .0 .0 .0	0. 0. 0. 0. 0. 0.		<
8.15 145.30	<ul> <li>109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis.</li> <li>111.00 113.00 SAME AS 120028.</li> <li>115.00 117.00 CRUMELY SECTIONS WITH BROKEN CORE.</li> <li>116.00 I16.70 Broken sheared core, core is in pieces.</li> <li>117.50 Slickensided shear plane, 1% diss. Py at 50 degrees to the core axis.</li> <li>119.50 122.50 15-20% RQD, 75-80% recovery, broken core, crumbly, shearing at 40 degrees to the core axis.</li> <li>123.50 Shearing at 25 degrees to the core axis axis.</li> <li>126.00 126.70 Shearing at 15 degrees to the core axis 131.00 Shearing at 15 degrees to the core axis 131.00 Shearing at 15 degrees to the core axis 132.60 Quartz filled shear at 35 degrees to the core axis.</li> <li>136.15 ARGILLACEOUS CREMT.</li> <li>136.00 Clayey mud filled fracture at 10 degrees to the core axis.</li> <li>136.15 138.15 90% QTZ 136.5-137.6,90% GRAPHITE 137.60 138.15 90% White fracture dquartz with interstitial graphite/mud, 2% Py associated with the fracture infilling contact at 55 degrees to the core axis.</li> <li>137.60 138.15 95% graphite, broken, leading to the contact at 138.15.</li> <li>ALTERED MAPIC FLOW MODERATELY ALTERED fight grey buff, f.g. To m.g., massive to brecciate(healed) bleached, calcite along fractures, weak ankerite, weak silicification, 138.15 140.15 ALTERED</li> <li>144.10 144.20 Shear, marcow irregular quartz, ankerite at 60 degrees to the core axis.</li> </ul>	120027 120028 120029 120030 120031 120032 120033 120033 120034	109.00 111.00 113.00 115.00 119.00 119.00	1111.00 115.00 117.00 117.00 121.00 121.00	2.00 2.00 2.00 2.00 2.00 2.00 2.00 2.00	90 90 75 95 85 95 95 95	70 90 75 40 75 30 85 75	tr trr tr tr tr tr tr tr	tr Fr .0 .0 .0 .0	.0 .0 .0 .0 .0 .0		<
8.15 145.30	<ul> <li>109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis.</li> <li>111.00 113.00 SAME AS 120028.</li> <li>115.00 117.00 CRUMELY SECTIONS WITH BROKEN CORE.</li> <li>116.00 Broken sheared core, core is in pieces.</li> <li>117.50 Slickensided shear plane, 1% diss. Py at 50 degrees to the core axis.</li> <li>119.50 122.50 15-20% RQD, 75-80% recovery, broken core, crumbly, shearing at 40 degrees to the core axis.</li> <li>123.50 Shearing at 25 degrees to the core axis axis.</li> <li>126.00 126.70 25-30% RQD.</li> <li>126.30 Shearing at 15 degrees to the core axis 131.00 Shearing at 30 degrees to the core axis 132.60 Quartz filled shear at 35 degrees to the core axis.</li> <li>134.15 136.15 ANGILLACEOUS CHEPT.</li> <li>136.00 Clayey mud filled fracture at 10 degrees to the core axis.</li> <li>136.15 138.15 90% QTZ 136.5-137.6,90% GRAPHITE 137.6-138.15.</li> <li>136.50 137.60 90% white fracture duartz with interstitial graphite/moid, 2% Py associated with the fracture infilling contact at 55 degrees to the core axis.</li> <li>137.60 138.15 95% graphite, broken, leading to the contact at 138.15.</li> <li>ALTERED MAPIC FLOW MODERATELY ALTERED Light grey buff, f.g. To m.g., massive to brecciated (healed) bleached, calcite along fractures, weak ankerite, weak silicification,.</li> <li>136.15 144.10 144.20 Shear, narrow irregular quartz, ankerite at 60 degrees to the core axis.</li> </ul>	120027 120028 120030 120030 120031 120032 120033 120033 120034	109.00 111.00 113.00 117.00 119.00 134.15 136.15	1111.00 113.00 115.00 117.00 121.00 121.00	2.00 2.00 2.00 2.00 2.00 2.00 2.00 2.00	90 9075995 85 95 90 95	70 90 75 40 75 30 85 75	tr trrttr tr tr tr tr tr	tr tr .0 .0 .0	.0 .0 .0 .0 .0		<<
8.15 145.30 5.30 158.20	<ul> <li>109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis.</li> <li>111.00 113.00 SAME AS 120028.</li> <li>115.00 117.00 CRUMBLY SECTIONS WITH BROKEN CORE.</li> <li>115.00 116.70 Broken sheared core, core is in pieces.</li> <li>117.50 Slickensided shear plane, 1% diss. Py at 50 degrees to the core axis.</li> <li>119.50 122.50 15-20% RQD, 75-80% recovery, broken core, crumbly, shearing at 40 degrees to the core axis.</li> <li>123.50 Shearing at 25 degrees to the core axis</li> <li>125.70 Shearing at 25 degrees to the core axis</li> <li>126.00 126.70 25-30% RQD.</li> <li>126.30 Shearing at 30 degrees to the core axis</li> <li>131.00 Shearing at 30 degrees to the core axis</li> <li>132.60 Quartz filled shear at 35 degrees to the core axis.</li> <li>134.15 136.15 ARGILLACEOUS CREMT.</li> <li>136.15 138.15 90% QT 136.5-137.6,90% GRAPHITE</li> <li>136.50 137.60 90% white fracture quartz with interstitial graphite/mud, 2% Py associated with the fracture infilling contact at 55 degrees to the core axis.</li> <li>137.60 138.15 95% graphite, broken, leading to the contact at 136.15.</li> <li>ALTERED MAPIC FLOW MODERATELY ALTERED fight grey buff, f.g. To m.g. massive to brecciated(healed) bleached, calcite along fractures, weak anterite, weak silicification, 138.15 140.15 ALTERED</li> <li>ALTERED MAPIC FLOW MODERATELY ALTERED flow, BLEACHED, SILICIFIED, WEAK CALCITE.</li> <li>ALTERED MAPIC FLOW MODERATELY ALTERED flow, BLEACHED, SILICIFIED, WEAK CALCITE.</li> <li>ALTERED MAPIC FLOW MODERATELY ALTERED FLOW, BLEACHED, SILICIFIED, WEAK CALCITE.</li> <li>ALTERED MAPIC FLOW MODERATELY ALTERED flow BRECCIATED FAULT ZONE Fractured/brecciated mafic flow, sections of broken core with shearing, local fault gouve. light to</li> </ul>	120027 120028 120030 120030 120031 120033 120033 120034	109.00 111.00 113.00 117.00 117.00 119.00 134.15 136.15 138.15	1111.00 113.00 117.00 119.00 121.00	2.00 2.00 2.00 2.00 2.00 2.00 2.00 2.00	90 9075995 85 95 90 95	70 90 75 40 75 30 85 75	tr trr tr tr tr tr tr tr	tr .0 .0 .0 .0	.0. .0. .0. .0. .0		<
8.15 145.30 5.30 158.20	<ul> <li>109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis.</li> <li>111.00 113.00 SAME AS 120028.</li> <li>115.00 117.00 CRUMBLY SECTIONS WITH BROKEN CORE.</li> <li>115.00 116.70 Broken sheared core, core is in pieces.</li> <li>117.50 Slickensided shear plane, 1% diss. Py at 50 degrees to the core axis.</li> <li>119.50 122.50 15-20% RQD, 75-80% recovery, broken core, crumbly, shearing at 40 degrees to the core axis.</li> <li>123.50 Shearing at 25 degrees to the core axis</li> <li>124.50 Shearing at 25 degrees to the core axis</li> <li>125.70 Shearing at 15 degrees to the core axis</li> <li>126.00 126.70 25-30% RQD.</li> <li>128.30 Shearing at 15 degrees to the core axis</li> <li>133.00 Shearing at 30 degrees to the core axis</li> <li>134.15 136.15 ARGILLACEOUS CREMT.</li> <li>136.51 136.15 ARGILLACEOUS CREMT.</li> <li>136.51 137.60 138.15.</li> <li>136.50 137.60 9% white fractured quartz with interstitial graphite/mud, 2% Py associated with the fracture infilling contact at 136.45.</li> <li>137.60 138.15 95% graphite, broken, leading to the core axis.</li> <li>137.60 138.15 ARGILLACEOUS CREMT.</li> <li>136.51 137.65 138.15.</li> <li>136.50 137.60 9% white fractured quartz with interstitial graphite/mud, 2% Py associated with the fracture infilling contact at 138.15.</li> <li>137.60 138.15 95% graphite, broken, leading to the contact at 138.15.</li> <li>136.15 140.15 ALTERED fight grey buff, f.g. To m.g., massive to brecciated(healed) bleached, calcite along fractures, weak ankerite, weak silicification,</li></ul>	120027 120028 120029 120030 120031 120032 120033 120033 120034	109.00 111.00 113.00 117.00 117.00 119.00	1111.00 115.00 117.00 117.00 121.00 121.00	2.00 2.00 2.00 2.00 2.00 2.00 2.00	90 9075 995 85 95 90 95	70 90 75 40 75 30 85 75	tr trr tr tr tr tr tr tr	tr -0 .0 .0 .0	.0 .0 .0 .0 .0 .0		<<
8.15 145.30 5.30 158.20	<ul> <li>109.40 Graphitic, slickensided shear plane at 15 degrees to the core axis.</li> <li>111.00 113.00 SAME AS 120028.</li> <li>115.00 117.00 CRUMELY SECTIONS WITH BROKEN CORE.</li> <li>116.70 Broken sheared core, core is in pieces.</li> <li>117.50 Slickensided shear plane, 1% diss. Py at 50 degrees to the core axis.</li> <li>123.50 Shearing at 25 degrees to the core axis.</li> <li>125.70 Shearing at 25 degrees to the core axis axis.</li> <li>126.70 E75-30% RQD.</li> <li>128.30 Shearing at 15 degrees to the core axis</li> <li>132.50 Shearing at 15 degrees to the core axis</li> <li>132.60 Quartz filled shear at 35 degrees to the core axis.</li> <li>134.15 136.15 ARGILLACCOUS CHEPT.</li> <li>136.00 Clayey mud filled fracture at 10 degrees to the core axis.</li> <li>136.15 138.15 90% QTZ 136.5-137.6,90% GRAPHITE 137.6-138.15.</li> <li>136.50 137.60 90% white fracture duartz with interstitial graphite/mod, 2% Py associated with the fracture infilling contact at 155 degrees to the core axis.</li> <li>137.60 138.15 95% graphite, broken, leading to the contact at 138.15.</li> <li>ALTERED MAFIC FLOW MODERATELY ALTERED fight grey buff, f.g. To m.g., massive to brecciated(healed) bleached, calcite along fractures, weak ankerite, weak silicification,.</li> <li>138.15 140.15 ALTERED FAULT ZONE Fractured/brecciated mafic flow, sections of broken core with shearing, local fault gouge, light to medium green, f.g., graphite/modiate axis.</li> <li>MAFIC PLOW BRECCIATED FAULT ZONE Fractured/brecciated mafic flow, sections of broken core with shearing, local fault gouge, light to medium green, f.g., graphite/modiate axis.</li> <li>MAFIC PLOW BRECCIATED FAULT ZONE Fractured/brecciated mafic flow, sections of broken core with shearing, local fault gouge, light to degrees to the core axis.</li> </ul>	120027 120028 120029 120030 120031 120032 120033 120033 120033	109.00 111.00 113.00 117.00 119.00 134.15 136.15	1111.00 113.00 115.00 117.00 121.00 121.00	2.00 2.00 2.00 2.00 2.00 2.00 2.00	90 90750 9585 95 90 95	70 90 75 40 75 30 85 75	tr trttr tr tr tr	tr Fr .0 .0 .0	.0 .0 .0 .0 .0		

<b>T</b> 96-79	9 (continued)							Pa	ye: 4	of 4	
From To (m) (m)	Geology	Sample	From (m)	¶то (m)	Lngth (m)	REC I	ROD F	GPY CG	PY QV	SG	AU G/T
	marks the contact between F, g and m.g. Flow contact/shear at 50 degrees to the core axis. 149.00 149.20 Intense fracturing/quartz carb. ROD 658 150.00 Lower contact at 75 degrees to the core axis. 152.20 Chloritic fault gouge,crumbly core,interstial chlorite/graphite. 154.50 Shear/fault,calcite/quarts, bound by chloritic gouge at 25 degrees to the core axis. 156.50 157.10 Practured/sheared,graphitic shear planes/brecciated at 50 degrees to the core axis. 157.10 158.20 M.g. Plow. 158.20 END OP HOLE.										

Collar Collar Hole I Casing Provin	ng: tion: r Azi.: r Dip: Length g: nce:	1200.0 1200.0 1800 -50.0 (m): 101.50 PULLED BRITISH COLUMBIA, CANAD	*** D Depth 50.6 100.6	ip Tests Azi. 183 183	-48.5 -49.0				Dri Eas Pro Pro Dri Dip Gri Cor	thing ting: ject: perty 11 ty /Azi d: e Siz	le: : pe: Test Me e:	thod:	T96-80 10+00S 12+00E TAURUS TAURUS I.ONGYE SPERRY 1995 NQ	AR 36 SUN
Date S Comple Drille Sample Analyt Logged Assay Purpoe	Started eted: ed by: e Nos: tical [ d By: Summar se:	I: MAY 11, 1996 MAY 12, 1996 DJ DRTLLING 120036-120048 .ab: CHEMEX, VANCOUVER LOGGED BY JOSEPH DION Y: TEST TP ANOMALY POSSIBL	RELATED TO TH	E ARGILI.	.T <b>T</b> F.									
From (m)	То (m)	Geo	ogy		Sample	From (m)	То (m)	I.ngth (m)	REC	ROD FO	SPY CGP	V QV 8	SG	AL G/T
		SUMMARY LOG												
. 00	28.00	OVERBURDEN						ĥ			i		5	t.
28.00	46.10	GRAPHITIC ARGULUTE FAULT ZONE										14 <b>1</b> 1		
46.10	48.20	ALTERED MAFIC FLOW ARGILLACEOUS	CHERT							ť	2			
48.20	52.50	GRAPHITIC ARGILLITE FAULT ZONE								i i	l			
52.50	62.80	ALTERED MAFIC FLOW												
62.80	68.50	GRAPHITIC ARGILLITE					1							
68.50	79.70	GRAPHITIC ARGILLITE MAFIC FLOW	AULT ZONE											
88.101	101.50	GRAPHITIC ARGILLITE ARGILLACEOUS	CHERT							ľ	i,			
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	T96-80	) (continued)			l		(north)	D.C.T. <sup>JI</sup>	Dee	rage			n
From (m)	Тс) (m)	Geology	Sample	From (m)	То (m)	(m)	REC 8	<u></u> 8 10н	FGPY 8	CGPY *	QV *	SG	AU G/T
.00	28.00	OVERBURDEN											
28.00	46.10	GRAPHITIC ARCILLITE FAULT ZONE Dark grey to hlack,v.f.g. To f.g.,hedded at approximately 20 to 50 deg., locally faulted with sheared/graphitic fault gouge,hroken crumhly sections 75 to 90% core recovery,60 to 70% RQD,.											
		30.00 33.25 Fault zone strongly graphitic/clayey fault gouge,local massive sections minor quartz and quartz/carh veinlets,local bedding preserved at 10 25 degrees to the own put											
		33.25 35.50 Practured locally bedded graphitic argillite. 35.50 39.20 Pault zone faulted/sheared/hrecciated graphitic argillite,clayey gouge occurs at 25 degrees to the core axis											
		interfragment graphitic mud. 37.20 Bedding at 25 degrees to the core axis. 39.10 Lower contact at 30 degrees to the core axis. 39.20 46.10 Paulted/hrecciated											
		argillite,interstitial black graphitic mud, sections of clayey gouge,slickensided graphitic shear planes narrow quartz and qtz/calcite microveinlets.											
46.10	48.20	ALTERED MAFTC FLOW ARGILLACEOUS CHERT Light grey,f.g.,fractured,weakly brecciated,local fault gouge,approx. Upper contact at 20 degrees to the core axis weak local calcite,bleacbed,silicified,hardness 5 non magnetic,.											
		46.90 47.00 Fault gouge contact at 30 degrees to the core axis.											
48,20	52.50	GRAPHITIC ARGILLITE FAULT ZONE Dark grey/black,f.g.,faulted,fragmented,no bedding remains,fragments/ blocks within zone could be silicified T2 or sections of T7,75 to 80% rec_local											
		48.40 48.90 Broken core, interstitial graphitic mun between sil fragments. 49.80 ]cm graphitic gouge at 10 degrees to the							-				
		core axis. 50.00 52.50 Graphitic gouge, white quartz vein. 50.75 52.80 Pault zone massive clayey gouge with	120036	50.00	52.50	2.50	60	40	.0	. 0	20.0		<.030
		narrow quartz veining. 50.75 51.10 Quartz vein,white,upper and lower contact at 30 degrees to the core axis.											
			1					0			1		
52.50	62,80	ALTERED MAPIC FLOW Light, grey green,m.g.,fractured,bleached,weak calcite alteration,minor narrow fault gouge,possible upper contact with fault gouge 52.5 at 35 degrees to the core axis fractured with sections of broken core and 10 to 20% RQD,55-60% recovery. 53 40 1 cm clavev gouge at 55 degrees to the											
		<ul> <li>5.1.40 Core axis.</li> <li>61.35 62.40 Fractured T6, broken core 61.35 to 61.9.</li> <li>61.90 Bedding at 55 degrees to the core axis.</li> </ul>											
62.80	68.50	GRAPHITIC ARGILLITE Dark grey to black,massive to moderately fractured,narrow faulted sections with fault gouge f.g. To m.g.,trace local fracture related Py,weak calcite alteration strongly graphitic,remnants of bedding weak or absent,local m.g. Porphyroblasts (remnant T1),contacts are gradational. 62.80 Lower contact at 40 degrees to the core											
		axis. 62.80 Upper contact at 40 degrees to the core											
		66.00 68.00 Massive argillite,shear from 67.6 to 67.8 66.50 66.70 Fractured,bracciated zone,narrow gouge at 40 degrees to the core axis. 67.60 67.80 Shear with narrow guartz carb. Vening,strongly graphitc.l-2% ov	120037	66.00	68.00	2.00	100	45	.0	.0	1.0		<.030
		shearing at 25 degrees to the core axis. 67.80 68.50 M.g argillite ?.	1.20020	60.00	70.00	2 00	100	5.0	2.0		3.0		< 030
68.50	79.70	68.00 70.00 Pault zone begins at 68.5. GRAPHITIC ARGILLITE MAPIC FLOW PAULT ZONE Dark grey to black,f.g. To m.g.,mixture of f.g. And	120038	68.00	70.00	2.00	100	50	2.0	.0	3.0		(.030
		c.g. Material, local quarts veining, local strongy graphitic clayey/mud gouge, patchy bleaching very weak calcite alt.(narrow qtπ/calcite veinlets and fracture filling trace py. 68.40 68.50 Graphitic clayey gouge 2-3% finely											
		disseminated Py. 68.50 68.60 Trregular white quartz and clayey gouge. 68.60 69.70 Altered/fractured m.g. Tl/T67,contact with the quartz unclear irregular. 69.70 72.10 Fault gouge contact at approximately 50											
		degrees to the core axis. 70.00 72.00 30% clayey gouge,1 10 cm gtz vein.	120039 120040	70.00 72.00	72.00 74.00	2.00 2.00	70 90	30 50	2.0 2.0	.0 .0	20.0 15.0		.070 <.030
		35 degrees to the core axis bull white guartz. 73,90 74.40 Bull white guartz vein contact at 35											
		degrees to the core axis. 74.00 76.00 Rull white quartz to 74.4, fault gouge 75.00 76.00 Rull white quartz to 74.4, fault gouge	120041	74.00	76.00	2.00	90	75	2.0	1.0	25.0		<.030
		degrees to the core axis strongly sheared lower contact.											
1							. 11		. 1				

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10.00         10.00 <td< th=""><th>From (m)</th><th>То (m)</th><th>Geology</th><th>Sample</th><th>From (m)</th><th>То (m)</th><th>Lngth (m)</th><th>REC %</th><th>ROD 8</th><th>FGPY %</th><th>CGPY %</th><th>QV %</th><th>SG</th><th>AU G/T</th></td<>	From (m)	То (m)	Geology	Sample	From (m)	То (m)	Lngth (m)	REC %	ROD 8	FGPY %	CGPY %	QV %	SG	AU G/T
10. 10. 10. 10. 10. 10. 10. 10. 10. 10.			76.00 78.00 Intense shearing,graphite,tr <sup>p</sup> y. 77.40 Shearing at 20 degrees to the core axis.	120042	76.00	78.00	2.00	80	0	2.0	tr	5.0		<.030
79,70         84.10         ATTREED MORE FLAG MORE ALL ANTERD Watch (1) or 100 more (1) more (1) more (1) more watch (1) or 100 more (1) more (1) more (1) more watch (1) or 100 more (1) more (1) more (1) watch (1) more (1)			78.00 80.00 Intense shearing,hleached T2 from 79.7 to 80.	120043	78.00	80.00	2.00	90	55	2.0	1.0	. 0		<.0.30
79.70         Shearing at X degrees to Discore afis.         100044         0.00 </td <td>79.70</td> <td>88.10</td> <td>ALTERED MAFIC FLOW MODERATELY ALTERED Light grey green to dark grey black,f.g. To m.g.,strongly fractured,locally sheared,locally weakly silicified and bleached,local graphitic shear planes possibly medium to coarse grained mafic flow or f.g. Intrusive,trace Py mixture of c.g. And f.g. Graphitic material,fracturing at 50 70 degrees to the core axis.</td> <td></td>	79.70	88.10	ALTERED MAFIC FLOW MODERATELY ALTERED Light grey green to dark grey black,f.g. To m.g.,strongly fractured,locally sheared,locally weakly silicified and bleached,local graphitic shear planes possibly medium to coarse grained mafic flow or f.g. Intrusive,trace Py mixture of c.g. And f.g. Graphitic material,fracturing at 50 70 degrees to the core axis.											
Int 0         30         degrees to the over a dis         100027         80.00         2.00         90         20         150			79.70 Shearing at 35 degrees to the core axis.	120044 120045 120046	80.00 82.00 84.00	82.00 84.00 86.00	2.00 2.00 2.00	80 90 95	50 25 65	1.0 tr tr	.0 .0 .0	5.0 1.0 2.0		<.030 <.030 <.030
An. 10         101.00         100.00         20.00         20         10         0			30 degrees to the core axis. 86.00 88.00 MODERATELY ALTERED ALTERED MAPIC FLOW	120047	86.00	88.00	2.00	90	20	tr	. 0	. 0		<.030
Duck jew to block a. to m. g. With mostros Derem it core and to man g. With mostros porphyritic 72 and 75. Bis 56 88.70 core and 75. Bis 56 88.70 core and 75. Bis 50 88.70 core and 75. Bis 50 24 core and 75. Bis 50	88.10	101.50	intense fracturing. Graphitic Argillite Argillaceous Chert	120048	88.00	90.00	2.00	80	70	.0	.0	.0		<.030
Re.50 At 70 Quarts version, soil white contacts 30.20 At 20 Aug at 5 degrees to the cortacts 31.50 The cortacts 32.50 Explore the cortacts 37.50 2 do goot wite contacts 30.30 Busing subpractile to 5 day. The cortact 30.30 Busing subpracting			Dark grey black, f.g. To m.g. With coarse blocks/fragments within the sheared argillite at 20 degrees to the core axis mix of greenish grey porphyritic T2 and T6.											
			<ul> <li>88.50 88.70 Quartz vein, massive, bull white contact at 40 degrees to the core axis.</li> <li>90.20 Shearing at 53 degrees to the core axis.</li> <li>94.50 Shearing at 5 degrees to the core axis.</li> <li>96.60 4 cm white quartz vein at 50 degrees to the core axis.</li> <li>97.90 2 cm quartz veinlet, bull white, at 35 degrees to the core axis.</li> </ul>											
			98.30 Shearing subparallel to 5 deg. The core axis. 101.50 END OF HOLE.											
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										(				



Analytical Chemists \* Geochemists \* Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218 To: CYPRUS CANADA INC.

322 WATER ST. VANCOUVER, BC V6B 1B6

Page Number :1 Total Pages :2 Certificate Date: 31-MAY-96 Invoice No. :19619159 P.O. Number : Account :MVM

JUN U U 1930

Project : TAURUS Comments: ATTN: JOE DION CC: DAVID BROUGHTON

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CERTIFICATION:\_

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# Chemex Labs Ltd.

Analytical Chemists \* Geochemists \* Registered Assayers 212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218

To: CYPRUS CANADA INC.

322 WATER ST. VANCOUVER, BC V6B 1B6

Page Number :2 Total Pages :2 Certificate Date: 31-MAY-96 Invoice No. : 19619159 P.O. Number : :MVM Account

Project : TAURUS Comments: ATTN: JOE DION CC: DAVID BROUGHTON

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CERTIFICATION:

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212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218



Comments: ATTN: DAVID BROUGHTON

A9531142

CERTIFICATE A9531142 ANALYTICAL PROCEDURES (MVM) - CYPRUS CANADA INC. DETECTION LIMIT CHEMEX NUMBER UPPER CODE SAMPLES DESCRIPTION LIMIT METHOD Project: TAURUS P.O. # : 983 197 Au ppb: Fuse 30 g sample የእ-እእይ 5 10000 Samples submitted to our lab in Vancouver, BC. 1000 0 Au check analysis 1 10000 This report was printed on 18-OCT-95. 1995 SOIL ASSAYS SAMPLE PREPARATION Υ. CHEMEX CODE NUMBER DESCRIPTION 199 Dry, sieve to -80 mesh 201 202 199 save reject NOTE Code 1000 is used for repeat gold analyses It shows typical sample variability due to coarse gold effects. Each value is correct for its particular subsample.

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Analytical Chemists \* Geochemists \* Registered Assayers

212 Brooksbank Ave.,North VancouverBritish Columbia, CanadaV7J 2C1PHONE: 604-984-0221FAX: 604-984-0218

o: CYPRUS CANADA INC.

322 WATER ST. VANCOUVER, BC V6B 1B6

Comments: ATTN: DAVID BROUGHTON

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CERTIFICATE A9531144 ANALYTICAL PROCEDURES (MVM) - CYPRUS CANADA INC. CHEMEX NUMBER DETECTION UPPER CODE SAMPLES METHOD DESCRIPTION IMIT LIMIT Project: P.O. # : TAURUS 983 212 Au ppb: Fuse 30 g sample FA-AAS 5 10000 Samples submitted to our lab in Vancouver, BC. 1000 0 Au check analysis 1 10000 This report was printed on 19-OCT-95. SAMPLE PREPARATION 1995 SOIL ASSAYS CHEMEX NUMBER SAMPLES DESCRIPTION 201 212 Dry, sieve to -80 mesh 202 212 save reject NOTE Code 1000 is used for repeat gold analyses It shows typical sample variability due to coarse gold effects. Each value is correct for its particular subsample.





Analytical Chemists \* Geochemists \* Registered Assayers 212 Brooksbank Ave., North Vancouver

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 British Columbia, Canada
 V7J 2C1

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 FAX: 604-984-0218



o: CYPRUS CANADA INC.

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Analytical Chemists \* Geochemists \* Registered Assayers 212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218

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## **APPENDIX B**

## **GEOPHYSICAL REPORT**

# **CYPRUS CANADA INC.**

A GEOPHYSICAL ASSESSMENT REPORT **ON AN INDUCED POLARIZATION AND GROUND MAGNETOMETER SURVEY ON THE TAURUS PROPERTY** CASSIAR, BRITISH COLUMBIA

> LIARD MINING DIVISION LATITUDE 59°20' NORTH LONGITUDE 129 • 47' WEST NTS 104P/5

> > BY

### LLOYD GEOPHYSICS INC.

S. John A. Cornock, B.Sc. and John Lloyd, M.Sc., P.Eng.

**JANUARY, 1996** 

**VOLUME 1 OF 2** 



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### **1.0 INTRODUCTION**

During the periods of March 18 to April 30, 1995 and August 15 to September 11, 1995, Lloyd Geophysics Inc. conducted Induced Polarization (IP) and ground magnetic surveys on the Taurus property near Cassiar, British Columbia, for Cyprus Canada Inc.

The purpose of the surveys was to locate zones of sulphide mineralization associated with goldbearing quartz veins.

### 2.0 PROPERTY LOCATION AND ACCESS

The Taurus property is located in northwest British Columbia approximately 130 kilometres north of Dease Lake, B.C. and about 5 kilometres from the former town of Cassiar, B.C. (Figure 1). It lies within the Liard Mining Division, NTS 104P/5 at coordinates 59°20' north latitude and 129°47' west longitude.

Access to the property is by truck north along Highway 37 to the junction at Jade City and then west for approximately 10 kilometres along the road to Cassiar.

### **3.0 PROPERTY STATUS AND CLAIM HOLDINGS**

The area covered by the geophysical surveys is comprised of the following claims as provided by Cyprus Canada Inc.:

Claim Name	Record Number	No. of Hectares
ADD 1-4	1268-1271	30.819
MISS DAISY 1-2	331105-331106	3.37
HOPEFULL 1-4	524	86.10
PANDA	885	?
MMIFR	1744	1.006
HIGHGRADE	929	3.52
HILLSIDE	928	10.20
ALTA 3	804	500





ALTA 4	131	297
ELAN 2	1171	476
EL 1 FR	1700	6.11
MARK I-IV	339214-339217	31.84
TOR 2	332630	0.159
WINGGOLD 1-2	6743-6744	37.2
TOD 7-8	57648-57649	26.35
ROY FR	5213	3.57
THRUSH	7329	15.6
PERRY FR	635656	19.1
BOZO 16	621	25.0
MOUNTAIN DEW	718	404
RICHVEIN	510	?
hanna 9	554	?
COOT 1-4	956-959	80.9
VAL 11-14	54915-54918	?
ROY 1-4	55511-55514	10.855
PORTAL 1-2	1045-1046	262.7
ATLAS 1-11	69566-69576	117.845
COPCO 1-6	5213-5218	50.73
MACK 1-4	515-518-	66.71

### 4.0 GEOLOGY

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The region is underlain by sediments and volcanics of the Carboniferous-Permian Sylvester Group. Low angle thrust faults and normal east-west striking faults are the dominant structural features.

Locally, ankeritic volcanic rocks contain pyrite and auriferous quartz veins. The veins dip

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steeply to the south and have extensive wall rock alteration zones of pyrite and ankerite. The veins vary from a few inches to a few feet in width. The enveloping alteration zone may be from 10 to several 10's of feet wide.

In 1993, the recognition of low grade gold occurring in basaltic rocks has led to a new approach to exploration. There are now 2 types of targets viz. quartz veins and open pit bulk tonnage low grade gold in basalts.

### 5.0 INSTRUMENT SPECIFICATIONS

#### 5.1 Induced Polarization Survey

The equipment used was a time domain measuring system consisting of a Wagner Leland/Onan motor generator set and a Mark II transmitter manufactured by Huntec Limited, Toronto, Canada and a 6 channel IP-6 receiver manufactured by BRGM Instruments, Orleans, France. The Wagner Leland/Onan motor generator supplies in excess of 7.5 kilowatts of 3 phase power to the ground at 400 hertz via the Mark II transmitter.

The transmitter was operated with a cycle time of 8 seconds and the duty cycle ratio: [(time on)/(time on + time off)] was 0.5 seconds. This means the cycling sequence of the transmitter was 2 seconds current "on" and 2 seconds current "off" with consecutive pulses reversed in polarity.

The IP-6 receiver can read up to 6 dipoles simultaneously. It is microprocessor controlled, featuring automatic calibration, gain setting, SP cancellation and fault diagnosis. То accommodate a wide range of geological conditions, the delay time, the window widths and hence the total integration time is programmable via the keypad. Measurements are calculated automatically every 2 to 4 seconds from the averaged waveform which is accumulated in memory.

The window widths of the IP-6 receiver can be programmed arithmetically or logarithmically. For this particular survey the instrument was programmed arithmetically into 10 equal window

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widths or channels,  $Ch_0$ ,  $Ch_1$ ,  $Ch_2$ ,  $Ch_3$ ,  $Ch_4$ ,  $Ch_5$ ,  $Ch_6$ ,  $Ch_7$ ,  $Ch_8$ ,  $Ch_9$  (see Figure 2). These may be recorded individually and summed up automatically to obtain the total chargeability. Similarly, the resistivity ( $\rho_a$ ) in ohm-metres is also calculated automatically.

The instrument parameters chosen for this survey were as follows:

Cycle Time  $(T_c) = 8$  seconds

Ratio (<u>Time On</u>) = 1:1 (Time Off)

**Duty Cycle Ratio** 

 $\frac{\text{(Time On)}}{\text{(Time On)} + \text{(Time Off)}} = 0.5$ 

Delay Time  $(T_D) = 120$  milliseconds

Window Width  $(t_p) = 90$  milliseconds

Total Integration Time = 900 milliseconds

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### 5.2 Ground Magnetometer Survey

The magnetometer equipment used was the Omni proton precession magnetometer system consisting of 2 Omni Plus magnometers manufactured by EDA Instruments Inc., Toronto, Canada.

The system is completely software/microprocessor controlled and measures and stores in memory the total field component of the earth's magnetic field.

The instrument also identifies and stores in memory the location and time of each measurement and computes the statistical error of the reading and stores the decay and strength of the signal being measured.

Throughout each survey day, a similar base station magnetometer measures and stores in memory the daily fluctuations of the earth's magnetic field. At the end of each survey day the field data is merged with the base station data and diurnal corrections are automatically applied to the field data.

### **6.0 SURVEY SPECIFICATIONS**

6.1 Induced Polarization Survey

The configuration of the pole-dipole array used for the survey is shown below:

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x = 50 metres n = 1,2,3,4,5 and 6

The dipole length (x) is the distance between  $P_1$  and  $P_2$  and mainly determines the sensitivity of The electrode separation (nx) is the distance between  $C_1$  and  $P_1$  and mainly the array. determines the depth of penetration of the array.

On the Taurus property the Induced Polarization survey was carried out with the current electrode, C<sub>1</sub>, south of the potential measuring dipole P<sub>1</sub>P<sub>2</sub>. Here the survey lines were 200 metres apart and measurements were taken for x = 50 metres and n = 1,2,3,4,5 and 6.

### 6.2 Ground Magnetometer Survey

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The ground magnetic data was collected on lines 200 metres apart using a station interval of 12.5 metres.

### 7.0 DATA PROCESSING

The IP and magnetic data collected was processed in the field at the end of each survey day using a portable 486 computer and a Fujitsu printer.

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The IP pseudo-sections were plotted out in the field and contoured using in-house software based on the mathematical solution known as kriging.

In our Vancouver office, the data was transferred to mylar and colour plots produced using a Hewlett-Packard DesignJet 650C plotter.

### **8.0 DATA PRESENTATION**

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The data obtained from the surveys described in this report is presented on 31 pseudo-sections and 16 contour plan maps as outlined below:

Pseudo-Section	s (Scale 1:5000)		
Line No	Dwg No	Line No	<u>Dwg No</u>
3400W	95365-01	200W	95365-17
3200W	95365-02	0	95365-18
3000W	95365-03	200E	95365-19
2800W	95365-04	400E	95365-20
2600W	95365-05	600E	95365-21
2400W	95365-06	800E	95365-22
2200W	95365-07	1000E	95365-23
2000W	95365-08	1200E	95365-24
1800W	95365-09	1400E	95365-25
1600W	95365-10	1600E	95365-26
1400W	95365-11	1800E	95365-27
1200W	95365-12	2000E	95365-28
1000W	95365-13	2200E	95365-29
800W	95365-14	2400E	95365-30
600W	95365-15	BL0	95365-31
400W	95365-16		



#### Plan Maps (Scale 1:5000)

**I**]

Chargeability	21 Point Triangular Filter	95365-32
Resistivity	21 Point Triangular Filter	95365-33
Total Field Ma	agnetic Profiles	95365-34
Total Field Ma	agnetic Contours	95365-35

Chargeability N=	1 95365-36	Chargeability	N=4	95365-42
Resistivity N=	1 95365-37	Resistivity	N=4	95365-43
Chargeability N=2	2 95365-38	Chargeability	N=5	95365-44
Resistivity N=2	2 95365-39	Resistivity	N=5	95365-45
Chargeability N=	3 95365-40	Chargeability	N=6	95365-46
Resistivity N=:	3 95365-41	Resistivity	N=6	95365-47

### 9.0 DISCUSSION OF RESULTS

An IP response depends largely on the following factors:

- 1. The volume content of sulphide minerals
- 2. The number of pore paths that are blocked by sulphide grains
- 3. The number of sulphide faces that are available for polarization
- The absolute size and shape of the sulphide grains and the relationship of their size and 4. shape to the size and shape of the available pore paths
- 5. The electrode array employed
- 6. The width, depth, thickness and strike length of the mineralized body and its location relative to the array
- 7. The resistivity contrast between the mineralized body and the unmineralized host rock

The sulphide content of the underlying rocks is one of the critical factors that we would like to determine from the field measurements. Experience has shown that this is both difficult and unreliable because of the large number of variables, described above, which contribute to an IP response. The problem is further complicated by the fact that rocks containing magnetite,

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graphite, clay minerals and variably altered rocks produce IP responses of varying amplitudes.

A detailed study has been made of the pseudo-sections which accompany this report. These pseudo-sections are not sections of the electrical properties of the sub-surface strata and cannot be treated as such when determining the depth, width and thickness of a zone which produces an anomalous pattern. The anomalies are classified into 4 groups: definite, probable, and possible anomalies and anomalies which have a deeper source. These latter anomalies are mostly related to deeper overburden cover.

This classification is based partly on the relative amplitudes of the chargeability and to a lesser degree on the resistivity response. In addition the overall anomaly pattern and the degree to which this pattern may be correlated from line to line is of equal importance.

An analysis of the IP/Resistivity data has, first of all, shown that a strong correlation exists between the chargeability and resistivity data. With the exception of a few small, localized zones, areas which exhibit increased chargeability closely coincide with resistivity lows. This is an interesting feature as it can greatly facilitate the mapping of the lithologies and structures.

A feature which stands out strongly is a northwest-southeast trending linear which has a high chargeability response with a coincident resistivity low. This linear has been interpreted as a fault which extends from the northwest corner of the grid to an area around 200W/600S (Fig.3). This fault essentially divides the grid into a northern half characterized by chargeability lowsresistivity highs and a southern half which, for the most part, contains chargeability highsresistivity lows.

The high chargeability-low resistivity values in the southwest part of the grid, which extend across the southern boundary of the property, are indicative of argillaceous sediments. However, it is encouraging that 3 drill holes in this area (T95-12, T95-15 and T95-16) discovered gold mineralization within basalts situated immediately above the argillites. These 3 drill holes are located in an area where the resistivities are not at their lowest but are grading into a higher

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resistive area to the east. Where the resistivities are greater than about 150 ohm-metres, it appears likely that these are areas in which the gold-bearing basaltic rocks overlie the argillaceous sediments and are therefore good targets. As for the chargeability, there is no discernable difference between the data collected in areas known to contain basaltic rocks and those which do not. The chargeability values remain quite high in the 30 to 35 millisecond range over the basalts and the argillites. This is most likely due to the underlying argillites "overprinting" the basaltic response resulting in an overall chargeability high. The magnetic data provides no helpful clues either as the argillites exhibit a consistently low response while the basalts are known to have variable magnetic responses depending on the degree of alteration and/or variation in mineral composition.

The previously mentioned resistivity high to the east is a circular feature which is centered around 1000W/1000S and is approximately 2 kilometres in diameter. The resistivities vary locally within this feature from 500 to 2500 ohm-metres probably due to an increase or decrease in overburden thickness. Bisecting this circular resistivity high is another interpreted fault which strikes approximately 45° and extends off the grid area to the southwest and northeast (Fig. 3). This fault trends along the west flank of a series of chargeability anomalies and cuts off the northwest-southeast fault at 200W/600S and possibly offsets it to the northeast.

Three holes (T95-10, T95-11 and T95-17) which were drilled into a chargeability anomaly in this circular resistivity anomaly again found gold-bearing basalts. Based on the resistivity, there is evidence to suggest that the gold-bearing basalts found here and those discussed earlier in the southwest area of the grid are continuous but under deeper overburden.

Further to the east, the IP data depicts a number of chargeability highs that flank zones which have a high magnetic response. The strongest of these chargeability anomalies is centered at 1000E/400S and contains values up to 35 milliseconds. Another anomaly is located to the south of this one at around 900S between lines 1600E and 2200E. Here, the chargeabilities are slightly lower and are believed to represent more of the same basalts that overlie the argillites which, from the IP/Resistivity data lie directly to the south.





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f this one at around 900S between lines 1600E and 2200E. Here, the chargeabilities are slightly lower and are believed to represent more of the same basalts that overlie the argillites which. from the IP/Resistivity data lie directly to the south.

Another area of interest is in the northeast corner of the grid where there are a number of narrow, closely spaced and strong magnetic highs within a strong magnetic low. The high resistivities associated with this area are indicative of a quartz vein system similar to those found in the Taurus Mine and elsewhere on the property. This area is also geophysically similar to the area around 400N between lines 600E and 1200E and an area close to the baseline from lines 200W to 800W. This latter area has previously been drilled and produced encouraging results.

Finally, the high chargeability-low resistivity zone located in the northwest corner of the grid is thought to again represent argillites. The adjacent magnetic high appears to locate more basalts which have not had their magnetic minerals altered. It is not certain whether or not the degree of alteration in the basalts is related in any way to the occurence of gold. A couple of drill holes in this magnetic high may answer this question.

### **10.0 CONCLUSIONS AND RECOMMENDATIONS**

The IP/Resisitvity and ground magnetic surveys described in this report have depicted a number of zones and trends which are believed to represent good gold-bearing targets worthy of further exploration by drilling. The resistivity data in particular worked well in mapping the location of the basalts.

Two large faults have been interpreted to exist on the property and are shown on the included map (Figure 3).

A total of 4375 metres of drilling in 49 holes has been recommended to test the geophysical targets. These holes are listed below in order from west to east, not in order of priority.

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Hole #	Line	<b>Station</b>	Angle	Depth(m)
1	3400W	1250N	-90	75
2	3400W	1050N	-90	75
3	3200W	850N	-90	75
4	3200W	1050N	-90	75
5	3200W	1250N	-90	75
6	3000W	1050N	-90	75
7	2400W	750S	-90	75
8	2400W	950S	-90	75
9	2400W	1150S	-90	75
10	2000W	550S	-90	75
11	2000W	750S	-90	75
12	2000W	950S	-90	75
13	2000W	1150S	-90	75
14	2000W	1350S	-90	75
15	1600W	700S	-90	75
16	1600W	900S	-90	75
17	1600W	1100S	-90	75
18	600E	550N	-45/000	100
19	600E	200S	-45/000	100
20	600E	450S	-45/000	100
21	600E	650S	-45/000	100
22	800E	400N	-45/000	100
23	800E	300N	-45/000	100
24	800E	0	-45/000	100
25	800E	200S	-45/000	100
26	800E	400S	-45/000	100
27	800E	600S	-45/000	100
28	1000E	300N	-45/000	100
29	1000E	200N	-45/000	100

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30	1000E	0	-45/000	100
31	1000E	200S	-45/000	100
32	1000E	400S	-45/000	100
33	1000E	600S	-45/000	100
34	1200E	500N	-45/000	100
35	1200E	200S	-45/000	100
36	1200E	400S	-45/000	100
37	1200E	600S	-45/000	100
38	1600E	150N	-45/000	100
39	1600E	0	-45/000	100
40	1600E	850S	-90	75
41	1800E	850S	-90	75
42	2000E	200N	-45/000	100
43	2000E	100N	-45/000	100
44	2000E	850S	-90	75
45	2200E	200N	-45/000	100
46	2200E	850S	-90	75
47	2400E	200N	-45/000	100
48	2400E	300N	-45/000	100
49	2400E	400N	-45/000	100

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The completion of these 49 holes will depend on the success of the initial 10 or 12 holes.

Respectfully submitted,

LLOYD GEOPHYSICS INC.

Hornich U

S. John A. Cornock, B.Sc. Project Geophysicist

InMark

John Lloyd, M.Sc., P.Eng. Senior Geophysicist

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### APPENDIX A

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### PERSONNEL EMPLOYED ON SURVEY

Name	<u>Occupation</u>	Address	Dates Worked
J. Lloyd	Geophysicist	#455-409 Granville Street Vancouver, B.C. V6C 1T2	Jan 09/96
J. Cornock	Geophysicist	#455-409 Granville Street Vancouver, B.C. V6C 1T2	April 11-21/95 Aug 15-31/95 Jan 4,5,8/96
F. Dziuba	Geophysicist	#455-409 Granville Street Vancouver, B.C. V6C 1T2	Mar 18 - Apr 30/95 Aug 21-29/95
A. Lloyd	Geophysical Technician	#455-409 Granville Street Vancouver, B.C. V6C 1T2	Aug 15 - Sept 11/95
C. Bilquist	Geophysical Technician	#455-409 Granville Street Vancouver, B.C. V6C 1T2	Aug 15 - Sept 11/95
B. Westerber	rg Geophysical Technician	#445-409 Granville Street Vancouver, B.C. V6C 1T2	Mar 18 - Apr 30/95
S. Garrett	Geophysical Technician	#455-409 Granville Street Vancouver, B.C. V6C 1T2	Aug 15 - Sept11/95
M. Cordiez	Helper	#455-409 Granville Street Vancouver, B.C. V6C 1T2	Mar 18 - Apr 30/95
A. Savard	Helper	#455-409 Granville Street Vancouver, B.C. V6C 1T2	Mar 18 - Apr 30/95
D. Dennis	Helper	#455-409 Granville Street Vancouver, B.C.V6C 1T2	Mar 18 - Apr 30/95



### APPENDIX B

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### **COST OF SURVEY AND REPORTING**

Lloyd Geophysics Inc. contracted the mobilization/demobilization and the data acquisition on a per diem basis. Truck charges, living and travelling expenses, data processing, computer plotting, map reproduction and interpretation and report writing were additional costs. The breakdown of these costs is as follows:

Mobilization/Demobilization and Data Acquisition	ıd	\$ 91870.78
Truck		8645.71
Living and Travelling		2153.21
Data Processing and Computer	5200.20	
Consumables		9034.65
Interpretation and Report Writing		1875.00
	Subtotal	\$ 118716.55
	G.S.T.	8310.15
	Total Cost:	\$ 127026.70



### APPENDIX C

### **CERTIFICATION OF AUTHORS**

I. John Lloyd, of #455 - 409 Granville Street, in the City of Vancouver, in the Province of British Columbia, do hereby certify that:

- I graduated from the University of Liverpool, England in 1960 with a B.Sc. in Physics 1. and Geology, Geophysics Option.
- 2. I obtained the diploma of the Imperial College of Science, Technology and Medicine(D.I.C.), in Applied Geophysics from the Royal School of Mines, London University in 1961.
- I obtained the degree of M.Sc. in Geophysics from the Royal School of Mines, London 3. University in 1962.
- 4. I am a member in good standing of the Association of Professional Engineers in the Province of British Columbia, the Society of Exploration Geophysicists of America, the European Association of Exploration Geophysicists and the Canadian Institute of Mining and Metallurgy.
- 5. I have been practising my profession for over thirty years.

Vancouver, B.C.

Lioyd Geophysics

I, John A. Cornock, of #455 - 409 Granville Street, in the City of Vancouver, in the Province of British Columbia, do hereby certify that:

- I graduated from the University of British Columbia in 1986 with a B.Sc. in Geology and 1. a minor in Geophysics.
- 2. I am a member in good standing of the Society of Exploration Geophysicists of America, British Columbia Geophysical Society, British Columbia and Yukon Chamber of Mines and the Northwest Mining Association.
- I have practiced my profession continuously since 1987. 3.

Vancouver, B.C.

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