GEOLOGICAL REPORT ON THE RAIN PROPERTY

REVELSTOKE MINING DIVISION

 NTS 82M/8E

 51 26N, 118 07'W

 JAN 17 1.37

 Gold Commissioner's One

For

MAJESTIC GOLD CORP. 500 - 885 Dunsmuir Street Street Vancouver, B.C. V6C 1G8

By

Stephen P. Kenwood, P.Geo. January 17, 1997 Addata Statistics Control Editors Add Britshed Statistics (Margarian)

SUMMARY

Majestic Gold Corp. has reached an agreement with Pacific Harbour Resources Inc. whereby Majestic may acquire an interest in the Rain property in the Revelstoke Mining District in southeastern British Columbia. The property is located approximately 60 kilometres north of Revelstoke, B.C. and is comprised of 14 claims totaling 158 units.

The Rain property is underlain by north-northwest trending metasedimentary rocks of the Proterozoic Horsethief Creek and lower Paleozoic Hamill Group, Badshot Formation and Lardeau Group. Three phases of deformation and regional lower greenschist metamorphism have complexly folded and altered these rocks. Lower Lardeau Group metasediments and metavolcanics host several Cu-Pb-Zn massive sulphide deposits in the region, including the 3.5 million tonne Goldstream Mine which is located 20 kilometres northwest of the Rain property. Previous work performed on the property confirmed that a stratigraphic package of rocks found on the Rain property is similar to, if not identical to, that found hosting the Goldstream deposit. Soil geochemistry results from a program done in 1991 strengthens the comparison of the two properties. A similar sized soil anomaly to that at the Rain property was all that was found at the Goldstream deposit, with copper and zinc concentrations being approximately the same.

The 1995-1996 program consisted of the reestablishment and extension of a grid that was originally laid out in 1991. Soil geochemical sampling, VLF-EM geophysics, and limited prospecting and mapping was carried out over half of this new grid. The soil geochemistry results confirmed the presence of the anomaly found in the 1991 program, but failed to significantly expand it to the west, although the anomaly is still open to the north. With a now well confined soil anomaly, it is recommended that this be drill tested, by providing road access to stations higher up the hill from where previous drilling took place.

TABLE OF CONTENTS

Summary	1
Introduction	3
Location, Access, and Physiography	3
Claim Status	5
Regional Geology	6
Regional Economic Setting	7
Property History	11
Property Geology	13
Work Program	14
Discussions and Recommendations	15
Bibliography	17
Appendix 1 - Statement of Costs	18
Appendix 2 - Analytical Results	19
Appendix 3 - Figures:	20
Figure 1 - Location Map	
Figure 2 - Claim Map	
Figure 3 - Regional Geology	
Figure 4 - Property Geology	
Figure 5 - Soil Geochemistry - Copper	
Figure 6 - Soil Geochemistry - Zinc	
Figure 7 - VLF-EM profiles	

.

INTRODUCTION

A work program consisting of the re-establishment and extension of the existing grid and geological mapping was carried carried out on the Rain property between September 10 and November 2, 1995. This report accounts for the period of time between October 17 and November 2 as well as a short program of surveying and prospecting from July 7-16, 1996. The entire program was a Phase one reassessment of an area that displays excellent potential to host copper-zinc mineralization. The grid work and limited mapping/prospecting was followed by grid soil geochemical sampling and VLF EM geophysics of this new grid and will allow a comparison of results from the existing grid. The surface expression and geology of the Rain target is believed to be identical to that found at the nearby Goldstream deposit (McAndless, personal comm., 1996).

The Rain property is comprised of claims owned by Goldstream Mine joint venture partners Goldnev Resources Inc. and Bethlehem Resources Corp. Previous work performed by Bethlehem between 1990 and 1992 resulted in the expenditure of \$168,500 over the three year period. A small mapping and sampling program was carried out on a different portion of the property in 1994. The cost of that program was \$32,000. Pacific Harbour Resources Inc. has an option to earn up to 75% interest in the entire claim group by incurring \$750,000 in exploration expenditures over four years. Majestic Gold Corp. has an option to earn 90% of Pacific Harbour's interest in the Rain property.

LOCATION, ACCESS, AND PHYSIOGRAPHY

The Rain property is located approximately 80 road kilometres north of Revelstoke, British Columbia (Figure 1). It is centered at 51 26' north latitude and 118 07' west longitude on N.T. S. map sheet 82M/8E. The property lies along Downie Creek between Standard Creek and Murder Creek. The property is accessible along Highway 23 north. from Revelstoke, along the Columbia River to the Downie Loop; from here the Downie logging road runs east and passes through the centre of the claims between the 15 and 29 kilometre marks.

The topography is moderate to steep, with elevations ranging between 670 and 2530 metres above sea level. The valley walls are moderate to steep and the ridge tops can be very sharp. Small ice fields occur in the upper reaches of the claims. The property is covered by mature forest for the most part, however some recent clearcutting has cleared some areas in the lower portion of the property. Bedrock exposure is limited to creek beds and steep slopes over most of the property.

The climate consists of warm dry summers and cool wet winters. Temperatures range between -20 to +30 degrees Celsius. Annual precipitation averages approximately one metre, over half of which falls as snow, which translates into an average snowpack of up to six metres. The average field season is from late April to early November. Several creeks drain the centre of the property and sufficient water for all stages of exploration would be available throughout the field season. The Revelstoke Canyon Dam lies 65 kilometres south of the property and the Mica Dam lies 60 kilometres to the north. The power lines from Mica pass five kilometres west of the property.

CLAIM STATUS

The Rain property consists of 14 mineral claims totalling 158 units registered in the Revelstoke Mining Division (Figure 2). The recorded owner of the claims is Bethlehem Resources Corporation (Now called Imperial Metals Corporation). The particulars of the claims are as follows:

CLAIM NAME	RECORD #	UNITS	LOCATION DATE	EXPIRY DATE
RAIN 1	248282	15	Oct. 18, 1989	Oct. 18, 1997
RAIN 3	248284	9	Oct. 18, 1989	Oct. 18,1997
RAIN 4	248285	12	Oct. 18, 1989	Oct. 18,1997
DROP 1	248425	18	Sept. 24, 1990	Sept. 24, 1997
DROP 2	248426	15	Sept. 24, 1990	Sept. 24, 1997
DROP 6	248430	6	Sept. 25, 1990	Sept. 24, 1997
DROP 7	248431	16	Sept. 24, 1990	Sept. 24, 1997
DROP 8	248432	20	Sept. 25, 1990	Sept. 25, 1997
DROP 9	248433	10	Sept. 25, 1990	Sept. 25, 1997
DROP 10	248434	15	Sept. 25, 1990	Sept. 25, 1997
DEER 1	248451	8	Dec. 6, 1990	Dec. 6, 2002
DEER 2	248452	6	Dec. 5, 1990	Dec. 5, 2002
DEER 3	248453	4	Dec. 6, 1990	Dec. 6, 2002
MIT	302917	4	Aug. 8, 1991	Aug. 9, 2003

Pacific Harbour Resources Inc. has an option to earn a 75% interest in the Rain property by incurring exploration expenditures of \$750,000 over four years. Majestic Gold Corp. has optioned 90% of Pacific Harbour's interest in the property. Any legal aspects of claim ownership or of the option deal involving the Rain property are beyond the scope of this report.

REGIONAL GEOLOGY

The geology of the region was first described by Gunning in 1928. Since that time the area has been re-mapped and reclassified by several authors and is yet to be firmly established. The regional work by Logan and Drobe in 1993 provides the most recent interpretation and is summarized below.

The Selkirk Allocthon is a composite terrain comprised of at least four fault bounded tectonic assemblages: The Upper Proterozoic Horsethief Creek Group, the Lower Cambrian Hamill Group, the Cambrian Badshot Formation and the Lower Paleozoic Lardeau Group (Figure 3). Together these units comprise the miogeoclinal wedge of ancestral North America.

The Horsethief Creek Group consists of phyllitic and slaty pelites, interbedded sandstone, conglomerate and minor carbonate rocks. Unconformably overlying these are sandstones and mafic metavolcanic rocks of the Hamill Group. Archaeocyathid bearing limestones of the Badshot Formation conformably overlie the Hamill Group. The Lardeau Group conformably overlies the Hamill Group rocks. Within the study area, the Lardeau Group is composed of at least two distinct formations; the lower Index Formation and the upper Broadview Formation. The Index Formation consists of dark grey and green phyllite, limestone. minor quartzite and, near the top, phyllitic volcanic rocks. Mafic intrusions (altered to tale schist) occur in the uppermost green phyllite unit. Overlying the Index Formation are grey quartz-feldspar grit, foliated micaceous quartzite and phyllite of the Broadview Formation.

The Goldstream slice is comprised of pelitic rocks with interlayered quartzites, grit, carbonates, impure metasandstone and volcanic rocks. These rocks were assigned to the Ordovician to Devonian Lardeau Group by Wheeler (1965). Specific correlations and stratigraphic definition within the slice are made difficult by the following problems; the slice is entirely fault bounded, fossil-bearing strata are absent, repeated deformation has made structure identification difficult and the Lardeau Group closely resembles the Horsethief Creek and Hamil Groups in composition.

The Goldstream slice is believed to be the inverted limb of an early nappe structure developed during phase 1 deformation. Phase 1 deformation resulted in kilometre scale west verging nappes and westerly directed thrust faults. This deformation is believed to be

pre Middle Jurassic. This early structure has been further deformed by map-scale phase 2 folding. Phase 2 folds are tight to isoclinal, overturned to recumbent north, northwest, to west trending with east, northeast or north dips. The Downie Peak, Keystone and Standard antiforms are all phase 2 folds. Phase 2 folding is thought to be synmetamorphic. This phase 2 folding is further deformed by phase 3 folding. Phase 3 folds are east trending open chevron and kink folds that deform S₂ schistosity.

Massive sulphide occurrences in the region are hosted in chloritic schists, sericite schist and dark banded graphitic calcareous phyllite associated with basic volcanism. Stratigraphy that hosts the Standard deposit has been correlated with the Lower Paleozoic Index Formation while lead isotope data from the Goldstream deposit gives a Devonian age (Campbell, 1991).

The area is intruded by several quartz monzonite plutons of Middle Jurassic age that cross the phase 2 deformation.

REGIONAL ECONOMIC SETTING

The Selkirk Allocthon is host to three major types of mineral occurrences; hydrothermal replacement or vein deposits, carbonate hosted lead - zinc deposits and Besshi-type volcanogenic massive sulphide deposits (Figure 3).

Examples of vein type deposits include the Lanark Mine which is located 50 kilometres southeast of the Rain property. Discovered in the 1880's and open until the mid 1920's, this deposit represents one of the first discoveries in the area. Mineralization is described as silver bearing galena in quartz and silicified limestone. The lower workings contained elevated zinc values and one of these workings reportedly contained chalcopyrite with copper values as high as 3.4%.

Other examples of vein deposits include the Snowflake/Woolsey and Waverly/Tangier workings. At the Snowflake working, mineralization occurs in a series of sub-parallel quartz veins hosted by slates. The veins vary from a few centimetres up to six metres wide and contain argentiferous galena, sphalerite, pyrite and minor chalcopyrite. By 1940, the Snowflake property had 609 metres of underground workings and by 1969, the Woolsey had 5940 metres of underground workings on 14 levels and six parallel quartz veins. In 1982, there were reported reserves on the Woolsey property of 590,703 tonnes grading 71.6 grams/tonne silver, 2.66% lead, 1.26% zinc, 1.1% copper, 0.13% tin, and 0.015% tungsten (Minfile).

The mineralization on the Waverly/Tangier property is reported as vein-like orebodies within a limestone or marble unit at or near the contact with schist. At the Waverly deposit, two replacement vein-like orebodies have been developed by over 914 metres of underground workings. Average assays for samples taken from the main oreshoot were 606.7 grams/tonne silver and 5.8% lead (Minfile).

The carbonate hosted massive sulphide deposits in the area are closely related to vein type deposits in some instances and exhalative massive sulphide deposits in others. The correct classification of some deposits in the region is not fully agreed upon even now. Examples of carbonate hosted massive sulphide deposits include the Rift, Keystone, J & L, and KJ showings. The Rift is described as a massive sulphide layer occurring within a calc-silicate unit. The massive sulphide body is exposed for 25 metres along strike and varies in thickness from 0 to 1.4 metres. A sample of the sulphides assayed 29.47% zinc, 6.93% lead, 0.03% copper over 0.8 metres (Minfile).

The Keystone showing is reported as an approximately one metre thick band of massive sulphide replacing limestone. Mineralization consists of pyrrhotite, sphalerite, galena, pyrite, and minor chalcopyrite. A one metre sample assayed 1.0% lead, 0.25% zinc, 0.27% copper, 2.0 grams/tonne gold, and 17.8 grams/tonne silver (Minfile).

The mine was purchased by the Bethlehem Resource Corp. and Goldnev Resources Inc. in 1989 and went back into production in May 1991. Reserves are currently reported at 1.436 million tonnes grading 4.48% copper and 3.03% zinc (Logan and Drobe, 1994).

The Goldstream Mine is a strata-bound copper-zinc deposit consisting of a thin sheet of massive sulphides in dominantly calcareous and graphitic schists of probable early to middle Paleozoic age. A manganiferous, iron-rich chert unit structurally overlies the sulphide layer. Regional structures suggest that the deposit is inverted and, therefore, that the chert horizon, referred to as the garnet zone, is interpreted to have formed as a siliceous exhalite stratigraphically below the massive sulphide deposit.

The massive sulphide layer consists primarily of intermixed pyrrhotite, sphalerite, and chalcopyrite, with numerous subrounded inclusions of quartz, carbonate, and phyllite fragments. The sulphides are locally swirled around the gangue inclusions to produce a durchbewegung fabric (Hoy et al., 1984). a texture common to many deformed and metamorphosed massive sulphide deposits. Contacts with the hanging wall and footwall range from sharp to gradational over a few meters.

Goldstream and other copper-zinc deposits in the Goldstream camp are interpreted to be exhalative massive sulphide deposits that formed in an unstable subsiding basin, near the continental margin. Host rocks include thick accumulations of coarse terrigenous clastics, calcareous shale, and basalt. They are similar to the Besshi-type deposits of Japan.

The ore body at the Goldstream mine averages between 1 and 3 metres in thickness, has a strike length of over 400 metres and extends down dip for over 1,200 metres. The massive sulphide layer is well defined only on its western and southern boundaries, it thins toward the east and one barren hole 300 metres east of the last one to intersect massive sulphides serves as its eastern boundary. The extent that the layer dips north is not as yet definitely defined, it is known to occur at least as far as the Goldstream river where it is 350 metres below the surface. Concentrations of copper, zinc and silver within the massive sulphide layer tend to increase toward the central, thicker part of the layer. The sulphide layer has a pronounced lateral zonation with respect to Zn/(Zn+Cu). Zinc vs. copper ratios tend to increase to the east irrespective of the thickness of the sulphide layer or copper and zinc grades. No vertical zonation is apparent in the massive sulphide layer. This lateral zonation of the massive sulphide layer is an important exploration guideline. Although a massive sulphide body may be uneconomic at one site, this may change as it is tested along strike (or at depth if vertical zonation is present).

PROPERTY HISTORY

Work in the immediate area of the Rain property was first performed by Noranda Exploration Company in 1976. Regional mapping in connection with exploration of the Standard-Keystone area extended to the western boundary of the Rain claims (Wild, 1990). Noranda held portions of the Rain property in the late 1970's. A small copper-tungsten showing immediately north of the confluence of Downie Creek and Sorcerer Creek was examined during this period.

In 1989, Bethlehem Resources Corp. staked the Rain property based on a reevaluation of the Goldstream Mine stratigraphy which suggested that similar host rocks existed at both locations. Initial reconnaissance was performed in 1990, and confirmation of the existence of Paleozoic Lardeau Group rocks lead to further work being recommended. This first program was performed at a cost of \$22,000.

More detailed exploration was focused on the Murder Creek area by Orequest Consultants Ltd. is 1991. This program consisted of the establishment of a grid used for soil geochemistry, magnetometer/VLF-EM survey, prospecting, and geological mapping. Geochemical results from sampling of B horizon yielded two anomalous zones of copperzinc-lead in soils. The most significant of these anomalies exists in the northern portion of the Murder Creek grid where soil results returned values up to 2066 ppm copper and 8992 ppm zinc. The combined copper-zinc anomaly is approximately 400 by 600 metres in size and is centred at 0+00 West and 2+00 South. Values greater than 75 ppm copper and 350 ppm zinc were considered anomalous; within the main portion of the zinc anomaly, 22 of 37 values are greater than 1000 ppm zinc.

A second anomaly, approximately one kilometre south of Murder Creek, yielded results up to 577 ppm copper, 1084 ppm zinc, as well as high manganese. The latter is of significance in that it is also found to be abundant within the garnet zone that encloses the Goldstream deposit. This anomaly is based on only three stations but like the major anomaly to the north, it also remains open to expansion. This program was performed at a cost of \$40,000.

A diamond drilling program was performed in 1992 to test the more significant northern soil anomaly. Results from the five hole, 900 metre program were inconclusive but encouraging. The drilling intersected stratigraphy very similar to that seen at the Goldstream Mine. Although no significant economic results were obtained, several garnet/semi-massive sulphide zones were encountered with up to 30% pyrrhotite and traces of chalcopyrite and sphalerite over 50 cm. Assay results for these zones returned values that do not suitably explain the soil anomaly; copper values ranged from 44 to 573 ppm while zinc values ranged from 54 to 443 ppm. The presence of the garnet zones is however significant because a well defined garnet zone is located structurally above the ore zone at the Goldstream deposit and it is believed that these zones are indicators of similar types of massive sulphide deposits (Cavey, 1992). Further drilling was recommended after analysis of this program and a subsequent bore hole EM survey program. Combined costs of these two programs was \$106,500.

PROPERTY GEOLOGY

The Rain Property is underlain by rocks of the Proterozoic Horsethief CreekGroup, Proterozoic to Lower Paleozoic Hamill Group and Paleozoic Badshot Formation and Lardeau Group.

Structurally these units trend northwest with moderate east to northeast dips.Second phase isoclinal folding and a dominant axial planar foliation are the dominant structural elements. Fold axes plunge gently to the southeast and northeast end of Keystone Peak. East of Downie Creek, plunges are moderate to the northeast, steepening northward toward Downie Peak. Broad, open third phase folds warp the foliation and original layering kink folds and crenulation cleavage are the dominant third phase structures showing near vertical axial planar cleavage and gentle east-west plunges (Wild, 1990).

Chloritic and calcareous metasediments dominate from Downie Creek westward to Standard Creek. These rocks tend to become more chloritic to the south and west, eventually becoming metavolcanic greenstones near Standard Peak. To the north, graphitic dark banded phyllites are more common. These metasediments are overlain to the east by older Badshot Marble and Hamill quartzites indicating the entire section to be overturned.

The Murder Creek area is underlain by graphitic dark banded phyllite, sericite to quartz sericite schist, siliceous silstones and marble. The dark banded phyllite is similar, if not identical, to the enclosing strata of the Goldstream ore body (Campbell, 1991). The unit generally trends north-south with dips ranging from 40 to 65 degrees to the east (Figure 4).

The dark banded phyllite is overlain by sericite to quartz sericitic siliceous schists and siliceous siltstones. Interbedded marble units have been noted within the dark banded phyllite and the sericitic schists.

1995-1996 WORK PROGRAM

Work outlined in this report entailed the re-establishment and western extension of a portion of a grid cut previously by Orequest Consultants in 1991. This was the first phase in an exploration program that included grid soil geochemical sampling, VLF-EM geophysics, property scale prospecting and mapping that was completed by the end of October, 1995.

The area chosen was one which contains a significant copper-zinc soil anomaly, roughly measuring 250 by 400 metres, centered at roughly 2+50 South, 0+00West, and remained open to the west (Figure 4). Early reconnaissance noted that the original grid had either grown in or deteriorated to the point that re-establishment of the grid became necessary. The original baseline was recut, chained, and picketed from 0+00 South to 20+00 South. Crosslines were slashed and flagged to 7+00 West. A tie line was cut, chained, and picketed at 5+00 West as well. Limited prospecting and mapping over this part of the grid yielded very little, as the property has very poor exposure at lower elevations.

Geochemical sampling of B horizon was done at 25 metre stations over the northern half of the grid. A total of 271 samples were collected, from an average depth of about 30 cms. Overburden depth is 1 - 3 metres over much of the grid area. Samples were taken to Acme Laboratories in Vancouver and the complete results are listed in Appendix 2.

ł

Copper results closely matched those of previous work, outlining a main anomaly between 0+00 South to 3+00 South and from 0+00 West to 2+00 West. Values in this area reached as high as 377 ppm (Figure 5). Results to the west, where previous anomalous results were left open, were disappointing; a two station anomaly in the 100 ppm range occurs at 3+50 West. 0+00 and 1+00 South.

Zinc results are similar to copper in that they confirm the results of the 1991 program. Only a portion of the major zinc anomaly east of the 0+00 baseline was sampled, but results confirm its' presence, with results up to 515 ppm (Figure 6). This anomaly, the largest in dimension (200 x 300 metres) is interpreted to have been mobilised to its' present position from an uphill source (personal communication, Wild, 1995).

A very low frequency electromagnetic (VLF-EM) survey was completed over half of the grid, from 0+00 South to 10+00 South. A Sabre VLF unit was used with the Seattle transmitter. The survey outlines a number of anomalies (Figure 7), which most probably define bedrock conductors. The conductors trend south-southeast, with the strongest lying along a ridgetop and trending from 3+25 West, 1+00 South to 2+50 West, 6+00 South. This conductor appears to step to the west between lines 6+00 South and 7+00 South, possibly indicating an east-west fault in that area. A weaker conductor centered at 0+50 West and 3+00 South is probably indicative of a parallel bedrock conductor, perhaps a graphitic horizon within the dark banded phyllite that was intersected in the previous drilling program.

In July of 1996, a crew was sent to Revelstoke to meet with Peter Frew of the Ministry of Forests and with J.D. Green of Revelstoke Community Forest Company (RCFC) to discuss and plan the best location of a drill access road. RCFC was involved in the meetings because they were interested in the timber potential of that particular area and the two groups are planning to share costs of any road construction that is mutually beneficial.

DISCUSSIONS AND RECOMMENDATIONS

Previous work performed on the Rain property has confirmed the presence of a stratigraphic package of rocks similar to those found to be hosting the Goldstream deposit twenty kilometres to the northwest. Diamond drilling failed to intersect economic mineralization but did contribute information that makes the comparison between the two properties to be even more compelling. At Goldstream, a garnet zone is found to be structurally above the ore zone and is believed to be unique to the Goldstream deposit itself (Cavey, 1992). Of the five holes drilled at the Rain property, four intersected multiple garnet/semi-massive sulphide horizons. If the garnet zones are indicators for the presence of massive sulphides in the area then the results of the drilling program at the Rain property provide significant reason to continue exploration of the property.

A combination of soil results, ground magnetometer survey, and surface mapping and prospecting will help determine the contacts between limestone and phyllites. Personal communication with Chris Wild (1995), mine geologist at Goldstream, suggests that the steepness of the hill and dip slope orientation of limestone units provide strong arguments for downhill migration of the soil anomaly. It was suggested that the limestone units could also act as aquifers, providing a conduit for downhill migration of fluids. If this proves to be the case, it is conceivable that previous drilling tested the anomaly area but not the possible uphill source. The Bethlehem Resources geological staff is now convinced that this is indeed the case (McAndless, personal comm., 1996).

It is recommended that a road building program be implemented to provide access for diamond drilling further up the hill to drill the parts of the stratigraphy that remain untested. The road building itself will be instructive, as there is a good possibility that bedrock exposures will be encountered as the road is built, providing more geologic information on a hillside with little or no exposure.

BIBLIOGRAPHY

- Campbell, I. Report of Exploration on Murder Creek Project, Rain Property, for Bethlehem Resources Corp., Orequest Consultants Ltd., October 25, 1991.
- Cavey, G. and Raven, W. Report of Diamond Drilling of Murder Creek Project, Rain Property, for Bethlehem Resources Corp., Orequest Consultants Ltd., October 22, 1992.
- Gunning, H.C. Geology and Mineral Deposits of the Big Bend Map Area, British Columbia. Canada Geol. Survey Preliminary Report, pages 136A-193A. 1928.
- Hoy, T. Geology of the Goldstream Area. B.C. Ministry of Energy, Mines and Petroleum Resources Bulletin 71, 1979.
- Hoy, T., Gibson, G. and Berg, N.W. Copper-Zinc Deposits Associated with Basic Volcanism, Goldstream Area. Southeastern British Columbia; Economic Geology, Vol. 79, pp. 789-814, 1984.
- LeBel, J.L. Report on Bore Hole Electromagnetic Survey, Murder Creek Project, Rain Property for Bethlehem Resources Corp. Orequest Consultants Ltd., December 7, 1992.
- Logan, J.M. and Drobe, J.R., Summary of Activities. North Selkirk Project Goldstream River and Downie Creek Map Areas. Geological Fieldwork 1993,
 British Columbia Ministry of Energy, Mines and Petroleum Resources,
 Paper 1994-1, pages 153-169.
- Reynolds, P. Geological Report on the Brew Property, for OTM International Development Inc., February 15, 1994.
- Wild, C.J. Geological and Geochemical Report on the Rain 1 17 Mineral Claims. Assessment Report, October 18, 1990.
- Wild, C.J. Personal Communication, May, 1995.

APPENDIX 1

STATEMENT OF COSTS

October 17 - November 2, 1995; July 7-16, 1996

1. Field Personnel

.

....

	S.P. Kenwood, P. Geo 17 days @ 400.00 R.W. Husband, P. Geo 10 days @ \$400.00 Field Assistant - 27 days @ \$250.00	6,800.00 4,000.00 6,750.00	
	Field Assistant - 27 days @ \$250.00	0.750.00	17 550 00
2.	Food and Accommodation		17,550.00
	54 man-days @ \$125.00		6,750.00
3.	Transportation truck rental/mileage		2,500.00
	Travel expenses		887.50
4.	Field Supplies		1,000.00
5.	Report		<u>2,000.00</u>

k

30,687.50

•

APPENDIX 2

.

ANALYTICAL RESULTS

•

						<u>Pr</u>	<u>oGr</u>	oup	Ge	OCH <u>010</u> 709 -	qic	<u>a</u>] .	Ltd		Fil	e #	96	-00	34	Pa	ge :	1								
SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Со ррп.	Mn ppm	Fe %	As ppm	U PPM	Au ppm	Th ppm	Sr ppm	Cdi ppm	Sb ppm	Bi ppm	V ppm	Ca X		La ppm		Mg X	Ba ppm	Ti X	B ppm	AL X	Na X	K X	W ppm
)+00s 7+00W	<1	31		122		73		372		9	<5	<2	10		<.2	<2	<2	46	.29	.057	25			117			3.09			<2
+005 6+75W	<1	6	13	21 126	<.3	5	3	56 519	1.25	4	<5 - E	<2	4	3	<.2	<2	<2	27	.02	.012	22	_8	.06	23	.04				.03	<2
)+00s 6+50W)+00s 6+25W	<1 <1	20 20	20 12		<.3 <.3	47 41	29 20	301		6 5	<5 <5	<2 <2	75	14 15	<.2 <.2	<2 <2	<2 <2	37 43		.070 .053	25 19	34 32	.64 .53	68 81	.13 .14		2.66 2.60			<2 <2
)+005 6+00W	<1	16	14	122	<.3	36		232		9	<5	<2	7	8	<.2	3	<2	44	.10	.040	23	35	.69	84	.15				.23	<2
)+00s 5+75W	<1	19	19	116	.5	43	18	383	4.16	10	<5	<2	9	13	.3	<2	<2	40	.45	.053	23	38	.79	99	. 16	ব	3.17	.01	.23	<2
+00s 5+50W	<1	17	84	278	.8	38		504		11	<5	<2	10		1.6	<2	4	42		.054	28		.76	96	- 13		2.82			<2
)+00s 5+25¥)+00s 5+00¥	<1 <1	8 24	153 188		3.3 3.7	9 34		6090 876		9 21	<5 <5	<2 <2	<2 10		11.6	<2	7 11	13 35		.031 .055	2 26		9.11	123 73			.35			<2
)+005 4+75W	<1	24 31	161	489	2.1	35		791		11	<5	<2	8	16	2.3 4.0	<2 <2	8	36	.71	.082	20	37		87	.11 .08		2.38 2.73		.12	<2 <2
)+00s 4+50W	<1	31	39	133	<.3	- 34	21	641	3.29	13	<5	<2	10	23	.9	2	2	19	.47	.070	26	22	.51	35	.05	<3	1.14	.01	. 10	<2
)+00s 4+25₩	1	48	76	167	.6			727		16	<5	<2	8	81	1.1	3	<2			.094	18	26	.86		.07		1.33			<2
RE 0+005 4+25W	1	44	72	149	.7	33		648 700		11	<5	<2	8	79	.9	2	<2			.087	16		.78	54	.07		1.23			<2
)+00\$ 3+75¥	2	26 101	34 40	148 180	.7 .5	43 74		399 1123		12 26	<5 <5	<2 <2	3 7	19 27	.3 1.0	<2 4	<2 <2	55 84		.058 .162	19 24		.91 1.66	109	.08 .11		2.91 4.59			<2 <2
)+00s 3+50W	2	42	27	129	<.3	39	12	1073	3.67	13	<5	<2	2	15	.5	<2	<2	67	.27	.080	20	31	.86	72	.09	ও	2.80	.01	.07	<2
+00s 3+25W	2	38	21	115	<.3	37		878		13	<5	<2	4	15	.6	<2	<2	63		.119	20	35	.87	68	.10				.06	<2
+005 3+00W	2	50		170	<.3	77		620		12	<5	<2	3	17	.4	<2	2		.29	.077	19	36	.79	101	.08		3.09			<2
)+00s 2+75¥)+00s 2+50¥	2	74 37	20 25	143 115	<.3 <.3	70 49		551 362		12 14	<5 <5	<2 <2	5 3	13 14	.3 .2	<2 4	<2 <2	58 58	.24 .28	.069 .072	18 15	38 33	.87 .78	82 75	.10 .09		3.38 3.67		.07 .05	<2 <2
)+00s 2+25₩	2	97	28	158	<.3	94	18	487	4.86	17	<5	<2	8	132	.6	5	<2	61	.32	.088	22	44	1.24	115	.12	<3	3.90	.01	.09	<2
)+00s 2+00W	-	119	23	133	.6	68	17	727	4.82	11	<5	<2	5	59	.8	5 2	<2	52	.78	. 153	16	34	1.13	77	-08	<3	2.39	.04		<2
)+00s 1+75W	6	307	65	403	1.1	262		3830		35	<5	<2		110	2.3	8	3			.144	13		1.57		.07		2.03			<2
)+00S 1+50W)+00S 1+25W	1	36 13	14 14	162 64	<.3 .4	46 15		1090 331		9 3	<5 5	<2 <2	3 3	12 22	.3 .2	<2 <2	<2 <2	40 23		.099 .085	16 7	29 12	.58 .16	102 61	.09 .13		3.41 4.99	.01 .03		<2 <2
)+00s 1+00W	1	37	29	209	<.3	40	12	1766	3 09	5	<5	<2	<2	30	1.0	3	<2	67	77	. 149	15	34	1.01	152	.07	<3	3.12	.01	.06	<2
0+005 0+75W	3	56	39		<.3	53		886		6	<5	<2	5		1.5	3	<2			.170	18	54	1.51	157			4.34			<2
+00s 0+50W	3	44	66	319	.3	59		1152		13	<5	<2	6		1.9	<2	<2		2.37		33		.94	133	.06		3.27			<2
)+00s 0+25W)+00s 0+00W	2	21 66	40 33	333 372	<.3 <.3	32 121		2722 1410		10 10	<5 7	<2 <2	2 9		2.0 2.5	2 2	<2 <2		4.55 1.24		22 21		.38 1.28	203 94	.09 .10		4.34 3.51		.06 .19	<2 <2
+00s 7+00W	<1	23	10	106	<.3	38	17	287	4.01	5	<5	<2	7	10	.2	3	<2	37	.13	.052	23	37	.84	9 1	.13	<3	2.31	.01	.32	<2
+00\$ 6+75W	<1	22	9	109	<.3	46	16	547	4.03	5	<5	<2	9	7	.2	3	<2	38	.08	.033	28	42	.95	93	.16	<3	2.58	.01	.38	<2
+005 6+50W	<1	28	13		<.3	50		253				<2	9	8	.4	6	2			.070	24		.84		- 14		2.89			
+005 6+25W +005 6+00W	<1 <1	25 20	82 46	108 73	.7 .5	46 27	22 14	666 410	5.94 4.11	13 22	<5 <5	<2 <2	7 6	11 15	.8 .6	<2 3	4 <2	25 29	.21 30	.061 .034	24 21	30 24	.71 .52	57	.07 .13		2.61 2.22			
STANDARD C	22	55	42	123	6.1	72	31	965	5.70	43	17	6	57	50	17.7	16	17	58	.54	.091	41	61	.87	170	.07	22	1.77	.06	.13	10
		ICP -	500	GPAM	SAMP	1 = 10	0109	STED	มาาม	3MI 2.	-1-2	401 - 4	NU-12-11	20 81	07. u	FG C	FUP	UNE H	OUR AN	חוכח	11 1170	ס ד ס	10 🖬	UITL		>				
•			LEACH	IS P	ARTIA	L FOR	MN F	E SR	CA P	LA CR	MG B/	A TI	BWA	ND LI	MITED	FOR	NA K	AND A	۲.	. 12 0	10016	U U	10 Fil		- M NICI	••				
											Λ				<u> </u>	<u>י הכן</u>	<u> r</u>	1	Ť											





Page 2

ACINE AMALYTICAL																													ACR	E ANALYTICAL
SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni Ppm	Co ppm	Min ppm	Fe X	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P X	La ppm	Cr PPm	Mg X	Ba ppm	Ti %	B ppm	Al X	Na X	K X	W ppm
1+005 5+75W 1+005 5+50W 1+005 5+25W 1+005 5+00W 1+005 4+75W	4 1 4 1 1 1	41 29 19 19 18	142	240 1337 155 200 230	1.1 1.7 .5 1.4 1.1	44 41 42 23 28	17 16 12	1673 1484 311 1068 940	4.96 4.30 4.00	16 26 56 8 10	<5 <5 <5 <5 <5	<2 <2 <2 <2 <2 <2 <2 <2	7 12 7 6 3	31 34 32 13 18	3.6 3.9 1.3 1.8 1.8	<2 5 5 2 2 2	<2 5 <2 3 <2	34 36 37 36 39	.69 .61	.075 .098 .026 .047 .034	33 32 25 20 24	36 43 40 28 30	.91 1.15 .81 .46 .63	89 71 70 63 70	. 11 . 13 . 16 . 16 . 14	ব্য ব্য ব্য	2.22 2.00 2.33 3.06 1.94	.02 .02 .01 .02 .01	.49 .32 .11	<2 <2 <2 <2 <2 <2 <2 <2
1+00s 4+50W 1+00s 4+25W 1+00s 4+00W 1+00s 3+75W 1+00s 3+50W	1 1 2 3 5	11 29 27 40 101	23 34 21 15 21		<.3 <.3 <.3 <.3 <.3	16 40 30 49 78	15 11 14	1146 603 850 1249 1539	3.93 3.87 4.26	<2 14 8 11 14	ৎ ১ ১ ১ ১ ১ ১	<2 <2 <2 <2 <2 <2 <2 <2 <2	<2 4 <2 3 3	10 17 9 29 18	.6 .8 .4 1.0 1.7	<2 3 2 5 2	<2 <2 <2 <2 <2 <2 <2 <2	38 50 58 55 89	.29 .10 .42	.036 .104 .053 .148 .195	19 26 24 18 21	18 36 35 31 45	.28 .85 .65 .65 .52	70 61 65 100 84	.09 .08 .10 .12 .07	ব্য ব্য ব্য	1.08 3.47 3.13 6.21 3.80	.01 .01 .01 .01 .01	.08 .07 .04 .04 .08	୧ ୧ ୧ ୧ ୧ ୧ ୧ ୧
RE 1+00S 3+50W 1+00S 3+25W 1+00S 3+00W 1+00S 2+75W 1+00S 2+50W	7 2 3 2 2	110 29 47 11 50	22 19 19 17 23		<.3 .3 <.3 <.3 <.3	83 36 36 11 38	10 11 5	1661 499 1000 1067 271	3.53 3.86 2.88	14 13 18 5 6		<2 <2 <2 <2 <2 <2 <2 <2	3 3 2 <2 5	19 17 10 7 17	2.1 .8 .7 .7 .5	<2 4 <2 3 <2	<2 <2 <2 2 3	95 44 59 41 49	.27 .12 .05	.206 .062 .097 .084 .132	22 13 18 7 20	49 30 33 14 29	.55 .50 .64 .18 .80	90 103 88 72 59	.07 .14 .08 .13 .05	ব্য ব্য ব্য	4.09 5.35 3.09 2.49 2.65	.01 .02 .01 .02 .01	.08 .08 .06 .03 .07	ବ ବ ବ ବ ବ ବ ବ ବ ବ ବ ବ ବ ବ ବ ବ ବ ବ ବ ବ
1+00s 2+25W 1+00s 2+00W 1+00s 1+75W 1+00s 1+50W 1+00s 1+25W	2 4 3 3 4	29 107 169 44 73	21 39 29 23 16	91 242 182 177 197	<.3 <.3 <.3 .5 <.3	28 61 67 31 52	14 14 10	318 1878 3501 2305 569	4.86 4.69 3.81	5 21 88 <2 7	ৎ ১ ২ ১ ২ ১ ২ ১	<2 <2 <2 <2 <2 <2 <2 <2	<2 2 2 2 2 2 2 2 2	11 23 19 29 34	.5 1.8 1.3 1.4 1.5	2 <2 <2 <2 <2 <2	<2 <2 <2 <2 <2 <2 <2	49 91 66 68 57	.41 .44 .53	.057 .173 .159 .123 .150	15 16 22 11 10	26 40 34 31 28	.60 1.26 .64 .70 .91	83 108 84 105 115	.07 .08 .05 .10 .11	ব্য ব্য ব্য	2.85 3.13 2.11 3.50 4.76	.01 .01 .01 .02 .02	.06 .10 .07 .06 .06	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
1+00s 1+00W 1+00s 0+75W 1+00s 0+50W 1+00s 0+25W 1+00s 0+25W	6 3 2 2 1	96 92 42 20 47	22 45 19 27 22	199 190 111 108 121	.5 .3 <.3 <.3 <.3	49 60 26 21 55	14 9 7	2298 1422 2780 1065 535	4.73 3.73 3.47	13 27 25 4 10	<5 <5 <5 <5 <5	<2 <2 <2 <2 <2 <2	<2 2 2 2 2 2 5	46 20 12 19 16	1.8 1.2 .8 .7	<2 <2 <2 <2 <2 <2	<2 <2 <2 <2 <2 <2 <2	94 54 47 46 47	.33 .14 .37	.189 .115 .108 .073 .070	12 22 13 12 20	38 33 24 26 41	.51 .76 .37 .45 1.06	137 135 82 90 112	.06 .08 .07 .08 .09	ব্য ব্য ব্য	2.96 3.11 2.42 3.13 2.93	.01 .01	.06 .07 .05 .04 .09	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
2+005 7+00W 2+005 6+75W 2+005 6+50W 2+005 6+25W 2+005 6+00W	1 1 <1 1	15 12 17 15 17	14 27 14 27 14	48 28 63 54 63	<.3 .3 <.3 <.3 <.3	22 10 28 25 29	4 11 10	199 116 300 377 388	3.20 4.58 4.49	5 2 7 5	<5 <5 <5 <5 <5	<2 <2 <2 <2 <2 <2	4 2 3 4 <2	6 4 8 8 17	<.2 .2 .3 <.2 .3	<2 <2 <2 <2 <2 <2	<2 <2 <2 <2 <2 <2	18 21 22 24 40	.02 .08 .09	.086 .036 .065 .095 .047	29 26 27 26 23	15 12 34 29 37	.36 .10 .62 .42 .63	43 28 52 44 59	.02 .04 .05 .06 .14	⊲ ⊲ ⊲	1.22 1.18 2.09 1.44 1.85		.07 .05 .11 .07 .26	2 2 2 2 2 2 2 2 2
2+005 5+75W 2+005 5+50W 2+005 5+25W 2+005 5+00W 2+005 4+75W	1 <1 <1 <1 1	18 24 18 21 13	23 51 146 195 76	89 130 295 312 213	<.3 .6 1.2 1.2 2.6	30 35 29 33 20	15 17 15	317 903 935 1211 5812	4.03 4.51 4.17	6 20 5 5 2	১ ১ ১ ১ ১ ১ ১ ১	<2 <2 <2 <2 <2 <2	4 2 6 5 <2	11 17 15 14 14	.2 .7 2.7 2.5 3.9	<2 <2 <2 <2 <2 <2	<2 <2 4 8 6	41 31 36 33 41	.32 .60 .38	.227 .066 .103 .085 .074	25 20 23 27 19	38 39	.53 .71 .72 1.14 .41	49 64 96 57 130	.12 .10 .08 .11 .09	<3 <3 <3	1.88 2.29 4.37 2.50 2.78	.01 .01 .01 .01 .02	.23 .20 .09 .32 .06	<2 <2 <2 <2 <2 <2 <2
STANDARD C	21	54	37	120	5.8	68	30	1041	3.83	38	19	7	37	50	18.3	16	17	58	.49	.091	38	61	.87	175	.08	27	1.84	.06	.14	11

ProGroup Geological Ltd. FILE # 96-0034

Page 3

ACHE ANALYTICAL							···																						ACHE	ANALTTICAL
SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bí	٧	Ca	P	La	Cr	Mg	Ba	Ti	В	AL	Na	ĸ	¥
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	X	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	X	*	ppm	ppm	X	ppm	*	ppm	x	x	X	ppa
2+005 4+50W 2+005 4+25W 2+005 4+00W 2+005 3+75W 2+005 3+50W	1 1 1 1 2	17 22 20 15 24	43 34 18 28 29	198 134 61 114 113	1.6 .8 <.3 .3 .3	31 37 29 25 36	12 10 12	255 775 255 1664 630	2.88 3.41 3.36	18 63 3 6 11	6 8 <5 <5 <5	<2 <2 <2 <2 <2 <2	<2 4 6 2 4	44 33 12 11 17	1.6 3.0 .2 .5 .6	3 3 2 3 4	2 3 3 <2 3	16 21 32 36 58	.72 .11 .11	.075 .062 .024 .050 .075	23 25 29 20 22	21 26 29 24 36	.47 .67 .57 .49 .91	51 71 68 73 63	.06 .07 .10 .08 .09	31 31 31 31 33	.66 .52 .76	.02	.13 .25 .14 .07 .07	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~
2+00\$ 3+25W 2+00\$ 3+00W 2+00\$ 2+75W 2+00\$ 2+50W 2+00\$ 2+25W	2 4 2 4 2	43 26 43 44 15	23 23 22 31 16	166 80 135 147 94	.6 .3 .5 .3 .3	35 24 37 43 28	7 11 15	1828 563 1237 1063 230	3.83 3.30 3.90	13 10 15 15 11	ی ج ج ج	<2 <2 <2 <2 <2 <2 <2	2 2 2 2 3	43 9 30 19 52	1.8 .3 1.0 .4 <.2	3 3 6 8 5	<2 2 2 2 2 2 2 2	46 75 60 94 52	.11 .40 .23	.117 .171 .099 .080 .059	19 17 25 18 17	35 31 35 41 33	.83 .48 .86 1.18 .48	91 61 73 131 85	- 06 - 10 - 08 - 10 - 14	उ 2 उ 1 उ 2 उ 3 उ 1	.64 .67 .50	.01	.07 .04 .06 .05 .13	<2 <2 <2 <2 <2 <2 <2 <2 <2
2+00S 2+00W 2+00S 1+75W RE 2+00S 1+75W 2+00S 1+50W 2+00S 1+25W	7	49 185 170 107 101	41 89 91 59 48	167 187 180 246 319	< 3 .5 6 < 3 3	49 85 83 77 97	13 13 16	453 1561 1455 760 469	6.68 6.35 7.37	13 99 92 25 20	<5 <5 <5 <5 <5	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <	5 4 5 5 6	28 31 29 30 30	.7 .4 .3 .8 1.5	7 4 3 6 7	3 <2 3 <2 2	75 96 91 113 81	.41 .39 .29	.134 .114 .108 .145 .142	21 20 19 20 20	41 38 47	1.18 .63 .61 1.45 1.67	118 156 144 143 126	.11 .09 .09 .12 .11	3 5 3 3 3 3 3 3 3 3	.25 .11 .66	.01 .01	.05 .16 .15 .11 .10	<2 <2 2 <2 <2 <2 <2
2+00S 1+00W 2+00S 0+75W 2+00S 0+50W 2+00S 0+25W 2+00S 0+00W	4 2 2 3 3	63 23 18 30 26	23 20 40 47 77	275 87 134 318 515	.7 .3 .3 .3	72 22 37 54 54	7 10 13	1011 700 717 454 691	2.79 3.36 4.33	15 9 12 15 21	<5 6 <5 <5 <5	<2 <2 <2 <2 <2 <2	3 <2 3 4 5	51 12 16 16 10	1.6 .2 .4 .6 1.1	8 3 5 6 4	2 <2 3 3 <2	66 51 38 53 39	. 13 . 34 . 27	.182 .063 .120 .086 .051	13 11 17 22 22	21 26	1.04 .44 .66 1.11 .77	191 69 170 155 125	.12 .10 .11 .07 .08	<36 <32 <34 <33 <34	.60 .70 .73	.02 .01 .02 .01 .01	.08 .06 .08 .09 .07	<2 <2 <2 <2 <2 <2 <2
3+00s 7+00W 3+00s 6+75W 3+00s 6+50W 3+00s 6+25W 3+00s 6+00W	1 1 2 1 1	13 17 17 18 17	14 35 33 27 22	39 66 71 75 66	<.3 .6 <.3 <.3	13 23 20 28 30	8 9 11	230 556 757 718 415	5.55 4.06 3.90	8 9 10 8 8	<5 <5 <5 <5 <5	<2 <2 <2 <2 <2 <2	<2 6 <2 2 4	6 6 8 7 9	<.2 <.2 .3 .3 <.2	<2 <2 <2 2 3	<2 <2 <2 <2 <2 <2	28 36 26 25 17	.04 .09 .07	.110 .069 .087 .051 .060	21 24 24 26 31	13 32 18 28 23	.11 .39 .30 .49 .58	31 65 56 59 53	.07 .12 .04 .05 .02	<3 <3 1 <3 1 <3 1 <3	.85 .23 .38	.01 .01 .01 .01 .01	.07 .09 .13 .09 .09	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <
3+005 5+75W 3+005 5+50W 3+005 5+25W 3+005 5+00W 3+005 4+75W	1 1 2 2 2	10 19 14 15 33	11 24 22 16 45	25 67 40 32 134	<.3 .5 <.3 <.3	10 27 18 13 37	10 5 5	222 3442 388 218 988	2.93 3.30 2.92	9 135 37 8 11	<5 9 <5 <5 <5	<2 <2 <2 <2 <2 <2 <2 <2 <2	2 <2 <2 2 2 4	8 24 9 4 24	<.2 1.1 <.2 <.2 2.2	<2 2 2 2 2 2 2 2 2	<2 <2 <2 <2 <2 <2	22 26 28 29 23	.54 .15 .04	.131 .163 .043 .150 .103	19 27 22 28 35	10 23 15 14 24	.05 .29 .14 .06 .67	41 125 30 20 119	.07 .04 .07 .08 .04		.42 .78 .60	.01 .02 .02 .02 .02	.05 .08 .06 .05 .25	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$
3+00s 4+50W 3+00s 4+25W 3+00s 4+00W 3+00s 3+75W 3+00s 3+50W	2 1 1 1 1	16 15 15 14 25	28 29 41 28 43	50 47 121 63 146	<.3 <.3 <.3 <.3 <.3	16 22 34 18 32	7	276 548 798 710 971	4.53 3.51 3.30	8 9 8 10		<2 <2 <2 <2 <2 <2 <2	2 <2 3 <2 3	14 6 27 17 12	-2 <.2 .6 .4 .7	<2 <2 <2 <2 <2 <2	2 <2 <2 <2 <2 <2	31 23 21 27 30	.04 .41 .27	.113 .189 .103 .075 .063	27 33 26 23 29	15 20 24 15 32	.14 .27 .55 .20 .81	37 31 147 77 68	.05 .03 .04 .05 .05	<3 2 <3 1	.69 .89 .06 .49 2.02	.01 .01 .02 .01 .01	.08	<2 <2 <2 <2 <2 <2 <2
STANDARD C	23	57	40	132	6.5	77	33	1052	3.97	43	19	8	37	52	19.7	15	21	59	.50	.090	42	62	.95	186	.09	27 1	.92	.06	. 15	10





Page 4

1

ACHE ANALYTICAL																														ACHE	ANALYTICAL
SAMPLE#	1		Pb		-			Mn			U					Sb			Ca		La		-			В		Na	ĸ		
	ppm	ppm	ppm	ppm	ppm	ppn	ppm	ppm	X	ppm	ppm	pbu :	ppm	ppm	ppm	bbw b	pipin)	ppm	×X	~ ~	ppn	ppm	*	PPR.	*	ppm	<u>x</u>	*	7	ppm.	
3+00s 3+25W 3+00s 3+00W 3+00s 2+75W 3+00s 2+50W 3+00s 2+25W	1	38 14 20	9 30	85 43	.3 .3 <.3	16 7	7 5 13	1969 1043 742		6 <2 6	<5	<2 <2 <2	<2 <2 <2	43 14	2.9 1.0 1.4	<2 <2 2	2 <2 <2	28 28 58	1.24 1.16 .33	.073 .159 .108 .043 .067	13 9 14	26 14 31	.25 .13 .69	87 36 59	.03 .05 .10		2.13 2.77 1.96	.03 .04 .01	.05 .03 .06	<2 <2 <2	
3+005 2+00W RE 3+005 2+00W 3+005 1+75W 3+005 1+50W 3+005 1+25W	14 2 2	64 33 41		132 168 116	.5 <.3 .3	29 34 33	8 10 11	1325 541 567	3.25	8 5 11	<5 <5	<2 <2 <2	<2 2 <2	24 14 25	1.1 1.2 1.2 1.0 1.1	<2 <2 2	<2 2 2	64 41 50	.26 .20 .39	.093 .094 .092 .089 .116	12 14 15	26 23 29	.80 .65 .88	165 122 121	.07 .10 .06	5 5 5 5	2.40 3.82 3.09	.01 .01 .01	.11 .07 .08	<2 <2 2	
3+005 1+00W 3+005 0+75W 3+005 0+50W 3+005 0+25W 3+005 0+00W	23	48 46	. 30 26	118 133 138	<.3 .3	26 44 34	10 13 10	2164 470 1418	2.28 3.23 4.12 3.99 2.64	5 13 6		<2 <2 <2	2 3	34 31 19		3 <2	<2 2 <2	81 61	.77 .71 .38	.039 .095 .180 .178 .073	17 16 14	27 49 30	.72 1.46 .90	234 200 101	.10 .08 .08	ব ব	3.54 3.14 3.35	.03 .01 .01	.08 .09 .06	<2 2 <2	
4+00S 5+00W 4+00S 4+75W not received 4+00S 4+50W 4+00S 4+25W 4+00S 4+20W	1	17	41 192 27 24	208 70	- 1.0	21 23	8 9	745 517	3.40 3.35 2.89 2.72	- 9 5	<5 - - - - - - - - - - - - -	- <2 <2	3 - ~2 2 2	- 23 11	-	- <2 <2	- 11 <2	- 21 19	.38 .11	.112 .076 .052 .058	21 25	- 19 19	- .37 .34	- 66 59	- .02 .03	- ও ও	- 1.29 1.38	- .01 .01	.10 .09	- ~2 ~2	
4+00s 3+75W 4+00s 3+50W 4+00s 3+25W 4+00s 3+00W 4+00s 2+75W	1 1 2		29	147 88 89		29 26 23	12 10 8	1974 448 342	3.89 3.58 5.85 4.32 3.91	12 7 10	<5	<2 <2 <2		8 30 9 8 7	.6 1.0 .9 .4 .3	2	2 <2 <2	30	.51 .09 .09	.104 .196 .081 .098 .203	27 25 25	27 29 24	.55 .53 .51	77 50 49	.05 .07 .07	<3	3.66 2.50 1.80	.02 .01 .01	.09 .09 .08	\$ \$ \$ \$	
4+00S 2+50W 4+00S 2+25W 4+00S 2+00W 4+00S 1+75W 4+00S 1+50W	1 2 3 2 2	43 51 25	19	208 208 115	.3 .4	57 28	14 9	979 580 751	1.75 4.31 3.97 3.17 3.32	15 8	<5 <5 <5	<2 <2		24 16	.3 1.3 .7 .4 .4	3 5	<2 <2	93 89 46	.80 .36 .25	.025 .189 .110 .071 .051	17 17 16	48 26	.92 1.60 .61	114 169 110	.07	<3 <3	5.69 3.83 3.05	.01 .01 .02	.05 .08 .07	3 ≺2 <2	
4+00S 1+25W 4+00S 1+00W 4+00S 0+75W 4+00S 0+50W 4+00S 0+25W	2 5 1	41 59	15 34 19	182 129 122	<.3 .3 .3	42 44 23	10 13 7	1542 1334 725	3.16 3.76 4.02 2.49 3.87	62 97 8	<5 <5 <5	<2 <2 <2	<2 <2	21 27 8	.6 .7 .5 .6	<2 2 <2	<2 <2 <2	47 76 25	.30 .42 .09	.086 .104 .151 .058 .140	13 21 19	23 33 18	.54 .76 .32	96 90 87	.09 .04 .08	থ থ থ থ	3.19 1.84 3.23	.02 .01 .01	.06 .09 .04	<2 <2 <2	
STANDARD C	21	.54	39	123	6.1	69	30	968	3.71	40	18	7	35	50	18.2	18	19	58	.54	.093	40	57	.89	172	.08	25	1.81	.06	.14	10	





Page 5

ACHE ANALYTIC	CAL																															ACHE MALYTICAL
	SAMPLE#						i Ni n pom		nM pom			U DOM				Cd ppm	Sb					La ppm p		-					Na X		W	
	4+00S 0+00W 5+00S 5+00W 5+00S 4+75W 5+00S 4+50W 5+00S 4+25W	1 1 1	34 19 16	22 29 22	9 5 5	2 < 5 < 6 <	4 47 5 67 5 21 5 33 5 36	21 6 10	632 310 253	4.52 5.63 4.57 4.49 4.73	10 12 7	5 5 <5	<2 <2 <2		15 10 7	.2 <.2 .2	4 3 4	<2 <2 <2	27 40 29	.22 .10 .09	.079 .136 .143 .040 .081	26 21 21	62 23 42	.87 .35 .63	54 72 45	.05 .08 .08	3 3 3 3	3.35 1.72 1.85 1.36	.01 .01 .01 .01	.06 .10 .08 .06	<2 <2 <2 <2 <2 <2	
	5+005 4+00W 5+005 3+75W 5+005 3+50W 5+005 3+25W 5+005 3+00W	<1 1 1	23 9	32 21 32	8	8 < 6 1 <	3 35 3 11	13 6 12	512 508 649	4.07 5.08 2.91 5.03 3.50	13 4	<5 7 <5	<2 <2		11 19 11	.5 .5 .8	2 <2 <2	<2 <2 <2	19 26 34	.11 .40 .19	.116 .058 .043 .064 .112	25 11 18	28 12 23	.65 .14 .37	88 62 59	.01 .08 .08	5 2 2 2 2 2 2	1.87 2.79 3.55	.01 .01 .02	.10 .06 .05	<2 <2 <2	
	5+00S 2+75W 5+00S 2+50W 5+00S 2+25W 5+00S 2+00W RE 5+00S 2+00W	1 2 1	16	17 22 17	2 12 7 11	8 . 3 . 1 <.:	324	9 13 11	828 621 658	3.76 3.12 3.97 3.35 3.46	7 5	<5	<2 <2	2 2	23	.8 .5	3 <2 2	<2 <2 <2	24 43 27	.14 .26 .33	.144 .053 .082 .057 .059	18 13 14	17 24 21	.34 .60 .37	114 116 99	.04 .11 .09	3 3 3 3	2.21 5.22 3.99	.01 .02 .01	.07 .05 .06	<2 <2 <2	
	5+00S 1+75W 5+00S 1+50W 5+00S 1+25W 5+00S 1+00W 5+00S 0+75W	1 1 3	19 27	67 29 24	7 11 7 12 7 12	3 <. 4 <. 4 <.	3 17 3 24 3 31 3 29 3 26	11 12 9	1599 771 338	2-83 3-39 3-44 4-46 3-49	8 6 9		<2 <2 <2	<2 3 <2	24 14	.3 .4 .4 .3 .5	2 3 4	<2 <2 <2	35 38 51	.34 .21 .22	.037 .090 .080 .042 .139	18 20 16	20 26 31	.45 .70 .65	198 92 89	-04 -07 -07	<3 <3 <3	1.62 2.65 2.69	.01 .01 .01	.06 .07 .05	<2 <2 <2	
	5+00S 0+50W 5+00S 0+25W not received 5+00S 0+00W 6+00S 5+00W 6+00S 3+50W	- 3 1	17	31 32	2 7	1 <. 1 <.	4 25 3 29 3 25 3 34	- 13 11	- 781 472	3.62 4.26 5.09 3.60	4 - 11 10 8	- <5	<2 <2 <2 <2	2 - 3 9		-4	- 4 3	- <2 <2	- 40 30	- -08 -22	.077 .040 .114 .071	- 23 24	28 27	.42	70 32	.07 .06	3 <3		.01 .01	.05	- <2 <2	
	6+00S 3+25W 6+00S 3+00W 6+00S 2+75W 6+00S 2+50W 6+00S 2+25W	1 1 <1	23	29 48 27	6 3 11 7 7	6 <. 8 <. 7 .	3 29 3 27 3 33 3 29 3 24	9 16 11	439 1786 849	3.45 4.13 4.24 4.82 3.42	11 14 3	<5	<2 <2 <2	<2 2	20	.3	4 3 2	<2 <2 <2	24 19 24	.33 .33 .09	.093 .110 .125 .117 .054	22 28 17	18 21 26	.32 .52 .50	119 107 61	.04 .02 .10	<3 <3 <3	1.11 1.88 4.72	.01 .01 .01	.08 .08 .10	<2 <2 <2	
	6+00S 2+00W 6+00S 1+75W 6+00S 1+50W 6+00S 1+25W 6+00S 1+00W	2 1 2	19 20	30 22 22	0 11 2 10 2 9	8. 6<.	5 35 3 30 3 28	11 12 9	429 1282 331	3.07 3.55 3.52 3.64 3.93	6 7 3	<5 <5 <5 <5 <5	<2 <2 <2	3 2 2	10 11 11	.6 .7 .8	3 3 2	<2 <2 <2	24 27 26	. 15 . 13 . 17	.080 .101 .069 .060 .062	23 23 16	24 23 23	.53 .50 .42	78 107 78	.04 .06 .08	<3 <3 <3	3.10 3.05 4.37	.01 .01 .01	.07 .06 .05	<2 <2 <2	
	STANDARD C	22	57	38	3 12	8 6.	4 72	32	1057	3.92	41	19	7	37	52	19.3	16	19	57	.50	.088	39	63	.91	183	.08	27	1.88	.06	. 14	11	





Page 6

1

SMPELE# No. Cu. Pb Zn Ag Ni Co. Mn. Fe Ag U Au Th Sr. Cd Sb Ni V Ca. P La Cr. Mg Ba Ti B At Ma K. V Gen gam																										_						WE ANALYTICAL	I
6+005 0+05 0+05 0+07 17 16 34 98 0.8 3 2.9 1,9 0.67 17 16 34 98 0.8 3 2.0 1,9 0.67 17 16 34 98 0.65 3 2.2 2.3 3.0 1.0 1.5 3.2 2.2 3.0 1.0 1.5 3.2 2.2 3.0 1.0 1.5 3.2 2.2 3.0 1.0 3.0 3.0 1.0 3.2 2.2 3.0 1.0 3.0 3.0 1.0 3.0 3.0 1.0 3.0 3.0 1.0 3.0 3.0 1.0 3.0 3.0 1.0 3.0 3.0 1.0 1.0 3.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 1.0 1.0 1.0	SAMPLE#	1				-																											
6+005 0+05 0+05 0+07 17 16 34 98 0.8 3 2.9 1,9 0.67 17 16 34 98 0.8 3 2.0 1,9 0.67 17 16 34 98 0.65 3 2.2 2.3 3.0 1.0 1.5 3.2 2.2 3.0 1.0 1.5 3.2 2.2 3.0 1.0 1.5 3.2 2.2 3.0 1.0 3.0 3.0 1.0 3.2 2.2 3.0 1.0 3.0 3.0 1.0 3.0 3.0 1.0 3.0 3.0 1.0 3.0 3.0 1.0 3.0 3.0 1.0 3.0 3.0 1.0 1.0 3.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 3.0 1.0 1.0 1.0 1.0		<u> </u>		~ .		-						-	_					-															7
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$																		2	28	.03	.036	19	18	.19	46	.05	<3	1.42	-01	.03	2		
4+005 $4+004$ 2 19 48 88 23 11 77 72 77 72 77 72 77 72 77 72 77 72 77 72 77 72 77 72 77 72 77 72 77 72 77																																	1
7+005 5+004 1 1 1 1 1 1 2 4 6 3 20 10 387 3.26 5 4 2 2 3 13 105 106 2 2 1 1 1 2 2 1 1 1 1 2 2 1 10 337 1 1 2 2 2 1 10 2 2 1 10 2 2 10 2 <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>																																	
7+005 4+75W not received 7+005 4+75W not received 7+7005 4+75W																																	
7+005 4-500 1 12 2 2 2 9 0.6 0.6 0.1 13 1.6 34 0.1 $< < < < < < < < < < < < < < < < < < < $	7+00S 5+00W	1	14	24	66	<.3	20	10	387	3.26	5	<5	<2	<2	8	<.2	<2	3	13	.05	.047	24	15	.42	46	.01	<3	1.28	.01	.08	<2		
7+005 4-500 1 1 2 2 2 9 0.6 0.66 31 13 .6 34 .01 < < 2 7+005 4+250 1 16 25 60 .03 23 16 7 $< 6 26 2 $	7+00s 4+754 pot received	Ι.	-		-		-			-	_	-	-	_	_	_	_	_		_	_	_	_	-		_	_	_	_	_	_		
7+005 4+25U 1 22 48 16 23 23 24 25 24 28 6 6 2 2 22 22 12 12 13 10 $\overline{2}$ 7+005 3+50µ 1 15 15 53 33 55 23 16 4 5 22 22 22 22 12 13 12 13 12 10 13 12 13 12 10 13 12 10 05 33 12 14 20 13 12 13 12 14 10 13 12 14 10 13 12 14 20 13 10 13 12 14 20 13 10 13 12 14 20 10 10 2 2 2 2 2 2 14 10 15 15 13 10 11 15 15 10 10 2 10 10 11 10 2 2 2 11 10		1-1	18	25	40	. 7	22	41	150	7 77	7	~5	~2	4	11	2	2	~ 2	0	<u>64</u>	0/0	71	17	14	71		-7	1 11.		^•			
7+005 4+0004 1 16 25 62 23 22		1												_																			1
7+005 3+75W 1 15 53 2 9 237 3.16 4 <5 <2 2 6 <.2 2 6 <.2 2 6 <.2 2 6 <.2 2 6 <.2 2 6 <.2 2 2 6 <.2 2 2 0 1 3 120 33 9 33 13 30 4.2 4 4 5 <2 6 15 .2 5 2 2 2 0 10 0 0 2 2 2 10 0 7 0 0 0 2 <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>																																	
7+0053+5041203395 < 3 3611300 4.24 9 < 5 < 2 615 $. 3$ 5 < 2 27 22 $.058$ 26 30 $.73$ 106.05 < 3 3.20 .01.09 < 2 7+0053+55W1203395<<									277	3.02	ç	5	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	~~	19	<. <u>.</u>	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	~~	21	. 27	.042	22	14	.25	20	.05	<3	1.32	.02	.00	<2		
RE 7+005 3+50u 1 20 33 95 < 3 36 11 74.24 8 62 6 15 25 12 055 63 32.22 010 05 33.22 010 05 33.22 010 05 33.22 010 05 33.22 010 05 33.22 010 05 33.22 010 05 33.22 010 05 33.22 010 05 33.22 010 05 33.22 100 05 33.22 100 05 33.22 100 05 33.22 100 05 33.22 100 05 33.22 100 05 33.22 100 05 33.22 100 05 33.22 100 05 33.22 100 05 33.22 100 05 33.22 100 05 33.22 100 05 33.22 100 05 33.22 100 05 33.22 100 05 05 05 02 100 </td <td>/+005 3+/3W</td> <td></td> <td>15</td> <td>12</td> <td>22</td> <td>د.></td> <td>25</td> <td>y</td> <td>231</td> <td>3.10</td> <td>4</td> <td>\$</td> <td><2</td> <td>2</td> <td>Ð</td> <td><.2</td> <td><2</td> <td>4</td> <td>18</td> <td>.04</td> <td>.051</td> <td>51</td> <td>22</td> <td>.42</td> <td>70</td> <td>.01</td> <td><5</td> <td>1.26</td> <td>.01</td> <td>.07</td> <td><2</td> <td></td> <td></td>	/+005 3+/3W		15	12	22	د.>	25	y	231	3.10	4	\$	<2	2	Ð	<.2	<2	4	18	.04	.051	51	22	.42	70	.01	<5	1.26	.01	.07	<2		
RE 7+005 3+504 1 207 4,24 8 6 < 2 6 15 2 5 2 2 2 0.5 3 2 0.1 0.5 2 2 2 0.5 0.5 3 2 0.1 0.5 2 2 2 2 0.5 103 2 <th2< th=""> 10 <th< td=""><td>7+00s 3+50W</td><td>1</td><td>20</td><td>33</td><td>95</td><td><.3</td><td>36</td><td>11</td><td>308</td><td>4.24</td><td>9</td><td><5</td><td><2</td><td>6</td><td>15</td><td>.3</td><td>5</td><td><2</td><td>27</td><td>.22</td><td>-058</td><td>26</td><td>30</td><td>.73</td><td>106</td><td>.05</td><td>3</td><td>3.20</td><td>.01</td><td>.09</td><td><?</td><td></td><td></td></td></th<></th2<>	7+00s 3+50W	1	20	33	95	<.3	36	11	308	4.24	9	<5	<2	6	15	.3	5	<2	27	.22	-058	26	30	.73	106	.05	3	3.20	.01	.09	</td <td></td> <td></td>		
7+005 $3+25W$ 2 34 317 71 7508 $5-26$ 618 72 42 42 45 107 22 82 25 83 107 22 82 427 12 242 427 1207 242 478 81 65 33 336 101 62 22 24 272 22 24 533 336 101 62 22 24 21 272 22 833 633 332 11623 44 45 42 24	RE 7+00S 3+50W	1	20																														
7+00S 2+75W 1 1 19 108 3 27 11 627 4.19 6 5 2 2 11 107 2 2 11 107 2 2 11 107 2 2 11 107 2 2 11 107 2 2 11 107 2 2 11 10 2 2 11 10 2 2 11 10 2 2 11 10 2 2 11 10 2 2 11 10 2 2 11 10 2 2 11 10 2 2 11 10 2 2 11 10 2 2 11 10 2 2 11 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 100 100 100 100 100 100 100 100 100 100 10 100 100 100																																	
7+005 2+75W 2 18 34 133 <.3 27 11 $627 4.19$ 6 $55 < 62$ 2 11 .6 $c2$ $c2$ $c15$ $c115$ $c16$ $c25$ $c25$ $c27$ $c27$ $c25$ $c25$ $c25$ $c27$																																	
7+005 2+504 1 1 6 27 95 < 3 21 10 1263 3.44 4 45 42 2 24 2.6 .077 19 17 .40 62 .03 < 3 2.15 .01 .06 < 2 7+005 2+254 1 1 12 32 74 55 75 < 2 2 15 .17 .05 67 .02 < 3 1.36 .01 .06 < 2 .25 .86 .095 31 .26 .98 .34 .04 < 3 .55 .02 .09 .23 .136 .01 .06 < 2 .25 .26 .20 .05 .23 .11 .16 .25 .02 .09 .25 .25 .20 .075 .23 .25 .07 .15 .04 .33 .36 .04 .33 .26 .11 .23 .24 .25 .26 .20 .25 .27 .20 .25 .25 .27 .21 .26 .2																																	
$7+005 2+25 \mu$ 1 2 3 3 7 4 4 2 2 2 2 2 2 5 17 051 28 17 50 67 0.2 3 1.55 0.1 0.6 < 2 7+005 1+005 1+75 \mu 1 18 68 5 3 2 5 7 -7 -2 2 2 5 60 10 0.6 < 2 2 3 2 11		-						•••			-			-				-										3.30					
7+005 2+25W 1 1 21 32 7 8< 3 27 5 < 2 </td <td>7+00s 2+50W</td> <td>1</td> <td>16</td> <td>27</td> <td>93</td> <td><.3</td> <td>21</td> <td>10</td> <td>1263</td> <td>3.44</td> <td>4</td> <td><5</td> <td><2</td> <td><2</td> <td>11</td> <td>.4</td> <td><2</td> <td><2</td> <td>24</td> <td>.24</td> <td>.077</td> <td>19</td> <td>17</td> <td>.40</td> <td>62</td> <td>.03</td> <td><3</td> <td>2.15</td> <td>.01</td> <td>.06</td> <td><2</td> <td></td> <td>1</td>	7+00s 2+50W	1	16	27	93	<.3	21	10	1263	3.44	4	<5	<2	<2	11	.4	<2	<2	24	.24	.077	19	17	.40	62	.03	<3	2.15	.01	.06	<2		1
7+005232555555775557775225855777 <td>7+00s 2+25W</td> <td>1</td> <td>21</td> <td>32</td> <td>78</td> <td><.3</td> <td>27</td> <td>12</td> <td>531</td> <td>3.39</td> <td></td>	7+00s 2+25W	1	21	32	78	<.3	27	12	531	3.39																							
7+00s 1+75W 1 1 18 36 85 < 2 2 13 < 2 3 < 2 < 2 < 2 < 4 8 < 4 < 3 < 3 < 2 < 3 < 2 < 2 < 3 < 2 < 3 < 2 < 2 < 3 < 2 < 2 < 3 < 2 < 3 < 2 < 3 < 2 < 3 < 2 < 3 < 2 < 3 < 2 < 3 < 2 < 3 < 2 < 3 < 2 < 3 < 2 < 3 < 2 < 3 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 <td>7+00s 2+00W</td> <td>2</td> <td>32</td> <td>54</td> <td>130</td> <td>.9</td> <td>48</td> <td>15</td> <td>979</td> <td></td>	7+00s 2+00W	2	32	54	130	.9	48	15	979																								
7+00s $1+50w$ 2 21 26 95 $s.3$ 28 13 920 3.77 7 $s.5$ 22 21 4.6 5 3 27 20 0.75 23 25 $.70$ 115 $.04$ $s.2$ 2.56 $.01$ $.08$ < 2 $7+00s$ $1+00w$ 1 15 29 65 < $.3$ 27 $.20$ $.27$ 22 22 28 117 700 $s.3$ 11 $.04$ $s.3$ 10.8 $.27$ <																																	
7+00s 1+25W1183185 $s.3$ 2411 702 3.97 5 $s.5$ $s.2$ $s.2$ $s.2$ $s.2$ $s.2$ $s.3$ $s.6$ $s.50$ 24 21 $.46$ 70 $.02$ $s.3$ 1.68 $.01$ $.05$ $s.2$ $7+00s$ $0+75W$ 115 29 65 $s.3$ 10 7 323 3.18 5 $s.5$ $s.2$ 22 21 18 11 $.043$ 18 17 $.39$ 46 $.03$ $s.31$ 10.8 $s.2$ $7+00s$ $0+75W$ 1 17 40 75 $s.3$ 20 9 3.08 5 $s.2$ 22 22 24 16 042 20 18 42 58 0.5 $s.3$ 1.08 0.01 $.08$ $s.2$ $7+00s$ $0+75W$ 2 22 64 152 20 3 $s.5$ $s.2$ $s.2$ 22 21 1.68 0.01 0.01 0.5 $s.2$ $7+00s$ $0+20W$ 2 22 64 152 2.9 3 $s.5$ $s.2$ $s.2$ 22 28 0.64 0.32 21 13 22 65 $s.2$ 22 22 24 15 16 100 1.05 $s.2$ $7+00s$ $0+00W$ 113 31 68 $s.33$ 2.74 5 $s.2$ $s.2$ 22 22 28 0.64 0.32 21	7+00S 1+50W	2																															
7+005 1+00W1152965 < 3 1973233.185 < 5 < 2 211 $.2$ < 2 218 $.11$ $.043$ 1817 $.39$ 46 $.03$ < 3 1.08 < 01 $.08$ < 2 $7+005$ 0+56W222646159.42206 3.90 3 < 5 < 2 < 2 2 2 2 1.6 $.02$ 20 18 $.42$ 58 $.05$ < 3 1.86 $.02$ $.07$ < 2 $7+005$ 0+56W22 26 61 159 $.42$ 2.7 2 22 22 21 1.6 $.092$ 22 21 $.49$ 137 $.05$ < 3 1.86 $.01$ $.09$ < 2 $7+005$ 0+00W113 31 68 < 3 15 8 853 2.74 5 < 5 < 2 < 2 2 20 16 155 27 24 $.69$ 0.4 < 3 1.00 01 $.05$ < 2 $8+005$ $5+00W$ 115 19 42 < < 3 15 11 1391 3.45 2 < 2 2 28 0.4 0.32 21 13 24 69 0.4 < 3 1.00 01 05 < 2 $8+005$ $4+50W$ 1 14 36 87 < $.3$ 15 11 1391																															_		
$7+005 0+75W$ 11174075 \cdot 320913083.085 \cdot 5 \cdot 2 \cdot 212 \cdot 2 \cdot 2 \cdot 2 \cdot 2 \cdot 1 \cdot 1 \cdot 4 \cdot 2 \cdot 1 \cdot 2								11	702	3.97	5	<5	<2	<2	9																		
7+00S 7+00S 0+25W2 2 2 22 2 2 2 22 2 2 2 2 22 2 2 2 2 2 2 2 22 	7+005 1+00W	1	15	29	65	<.3	19	7	323	3.18	5	<5	<2	2	11																		
7+00S 7+00S 0+25W2 2 	7+00s 0+75W	1	17	40	75	<.3	20	9	1308	3.08	5	<5	<2	<2	12	.2	<2	2	24	.16	.042	20	18	.42	58	.05	<3	1.86	.02	.07	<2		
$7+00S 0+00W$ 11331 $68 < .3$ 158 $853 2.74$ 5 $< 5 < 2$ $< 2 < 2$ $< 2 < 2 < 2$ $< 28 \cdot 04 \cdot 0.32$ $< 21 \cdot 13$ $.24 \cdot 69 \cdot 0.4$ $< 3 \cdot 1.00 \cdot 01 \cdot 0.5$ < 2 $8+00S 5+00W$ 11519 $42 < .3$ 14 $6 \cdot 212 \cdot 2.93$ $3 \cdot 5 < 2 \cdot 2$ $8 \cdot .2 \cdot 2 \cdot 2$ $21 \cdot 5 \cdot 0.7 \cdot 0.40 \cdot 31 \cdot 11$ $11 \cdot 18 \cdot 39 \cdot 0.2 < 3 \cdot .94 \cdot 0.1 \cdot 0.8 < 2$ $8+00S 4+75W$ 11436 & 87 \cdot .3 \cdot 15 \cdot 11 \cdot 1391 \cdot 3.45 \cdot 2 \cdot 5 < 2 \cdot 2	7+00s 0+50W	2	26	46	159	.4	27	12	2096	3.90	3	<5	<2	<2	22																		1
8+005 +00W11519 $42 < .3$ 146 $212 2.93$ 3 $< 5 < 2$ 28 $< 2 < 2$ 215 $.07$ $.040$ 3111 $.18$ 39 $.02$ < 3 $.94$ $.01$ $.08$ < 2 $8+005 4+75W$ 11436 $87 < .3$ 15111391 3.45 $2 < 5$ < 2 2 2 3 22 $.47$ $.135$ 1415 $.16$ 119 $.11$ < 3 5.77 $.01$ $.05$ < 2 $8+005 4+50W$ 113 29 $67 < .3$ 16 9 382 4.01 3 < 5 < 2 2 25 $.18$ $.051$ 21 17 $.27$ 86 $.05$ < 3 1.97 $.01$ $.07$ < 2 $8+005 4+25W$ 1 23 $.49$ $157 < .3$ $.32$ 15 1114 4.36 10 < 5 < 2 < 2 27 $.36$ $.075$ 19 23 $.38$ 107 $.07$ < 3 $.3.61$ $.01$ $.04$ < 2 $8+005$ $4+00W$ 1 23 49 $157 < .3$ 32 15 1114 4.36 10 < 5 < 2 5 26 $.5$ 3 < 2 27 $.36$ $.03$ < 3 3.73 $.01$ $.07$ < 3 $.61$ $.01$ $.08$ < 2 $.27.36.03.33.73.01.07< 3.36$	7+00s 0+25W	2	25	46	126	<.3	28	13	1422	4.27	4	<5	<2	<2	14	.3	<2	2	29	.16	.155	27	24	.55	91	.04	<3	2.15	.01	.09	<2		
8+005 +00W11519 $42 < .3$ 146 $212 2.93$ 3 $< 5 < 2$ 28 $< 2 < 2$ 215 $.07$ $.040$ 3111 $.18$ 39 $.02$ < 3 $.94$ $.01$ $.08$ < 2 $8+005 4+75W$ 11436 $87 < .3$ 1511 1391 3.45 $2 < 5$ < 2 2 2 3 $2 < 47$ $.135$ 1415 $.16$ 119 $.11$ < 3 5.77 $.01$ $.05$ < 2 $8+005 4+50W$ 113 29 $67 < .3$ 169 382 4.01 3 < 5 < 2 2 2 2 2 2 5.77 $.01$ $.05$ < 2 $8+005 4+25W$ 216 9 382 4.01 3 < 5 < 2 2 2 2 2 2 3 3.81 07 $.07$ < 3 3.61 $.01$ $.07$ < 2 $8+005 4+25W$ 1 23 49 157 $<.3$ 32 15 1114 4.36 10 < 5 < 2 5 26 $.5$ 3 < 2 20 $.75$ $.118$ 28 23 $.54$ 68 $.03$ < 3 3.73 $.01$ $.07$ < 2 $8+005$ $3+50W$ 2 23 36 10 < 5 < 2 5 26 $.5$ 3 < 2 20 $.75$ $.118$ 28 23 $.54$ <td>7.000 0.001</td> <td></td> <td>47</td> <td>74</td> <td></td> <td>. 7</td> <td>45</td> <td></td> <td>957</td> <td>~ ~/</td> <td>-</td> <td></td> <td>-2</td> <td></td> <td>-</td> <td>2</td> <td>- 2</td> <td></td> <td></td> <td>~ /</td> <td>070</td> <td>-</td> <td>47</td> <td>21</td> <td></td> <td>~</td> <td></td> <td></td> <td>~</td> <td></td> <td></td> <td></td> <td></td>	7.000 0.001		47	74		. 7	45		957	~ ~ /	-		-2		-	2	- 2			~ /	070	-	47	21		~			~				
8+005 4+75W111436 $87 < .3$ 151113913.452 $< 5 < 2$ 223.63322.47.1351415.16119.11 $< 3 5.77$.01.05 < 2 $8+005 4+55W$ 1132967 < 3 169382 4.01 3 $< 5 < 2$ 2222218.0512117.2786.05 < 3 1.97.01.07 < 2 $8+005 4+25W$ 2176191 < 3 2413987 6.36 6 $< 5 < 2$ < 2 227.36.0751923.38107.07 < 3 3.61.01.04 < 2 $8+005 3+75W$ 22336109 < 3 231410654.609 $< 5 < 2$ < 2 26.553 < 2 20.75.1182823.5468.03 < 3 .73.01.07 < 2 $8+005 3+75W$ 22336109 < 3 231410654.609 $< 5 < 2$ < 2 26.553 < 2 20.75.1182823.5468.03 < 3 .73.01.07 < 2 $8+005 3+50W$ 22336109 < 3 311410353.774 $< 5 < 2$ 917.3<																																	
8+005 4+50W11329 $67 < .3$ 169 $382 4.01$ 3 $< 5 < 2$ 212 $< 2 < 2$ 225 $.18$ $.051$ 21 17 $.27$ 86 $.05$ < 3 1.97 $.01$ $.07$ < 2 $8+005 4+25W$ 217 $.13$ 29 $67 < .3$ $.32$ 13 987 6.36 6 $< 5 < 2$ < 2 21 18 22 27 $.36$ $.075$ 19 23 $.38$ 107 $.07$ < 3 3.61 $.01$ $.04$ < 2 $8+005 4+00W$ 1 23 49 $157 < .3$ 32 15 1114 4.36 10 < 5 < 2 5 26 $.5$ 3 < 2 20 $.75$ $.118$ 28 23 $.54$ 68 $.03$ < 3 3.73 $.01$ $.07$ < 2 $8+005$ $3+75W$ 2 23 36 10 < 5 < 2 5 26 $.5$ 3 < 2 20 $.75$ $.118$ 28 23 $.54$ 68 $.03$ < 3 3.73 $.01$ $.07$ < 2 $8+005$ $3+75W$ 2 23 36 10 < 3 23 14 1065 4.60 9 < 2 < 2 21 13 9.07 < 3 2.97 $.01$ $.07$ < 2 $8+005$ $3+25W$ 2 22 41 107 < 3 36 14 389																																	
$8+005 4+25W$ 2176191 \cdot .324139876.366 < 5 < 2 < 2 18 $.8$ 2 < 2 27 $.36$ $.075$ 19 23 $.38$ 107 $.07$ < 3 3.61 $.01$ $.04$ < 2 $8+005$ $4+00W$ 1 23 49 157 $<.3$ 32 15 1114 4.36 10 < 5 < 2 < 5 26 $.5$ 3 < 2 20 $.75$ $.118$ 28 23 $.54$ 68 $.03$ < 3 3.73 $.01$ $.07$ < 2 $8+005$ $3+75W$ 2 23 36 109 $<.3$ 23 14 1065 4.60 9 < 5 < 2 < 2 26 $.64$ $.114$ 21 20 $.53$ 93 $.07$ < 3 2.97 $.01$ $.07$ < 2 $8+005$ $3+55W$ 2 22 41 107 $<.3$ 36 14 389 3.87 4 < 5 < 2 9 17 $.3$ 2 < 21 139 $.084$ 26 25 $.72$ 118 $.02$ < 3 2.497 $.01$ $.08$ < 2 $8+005$ $3+00W$ 2 20 28 100 $<.3$ 31 14 1035 3.77 < 5 < 2 2 $27.32.08123.75118.02< 32.97.01.0$																																	
8+00s 4+00w 1 23 49 157 <.3																<.2	<2	2	25	.18	.051	21	17	.27	86	.05	<3	1.9/	.01	.07	<2		1
8+00s 3+75W 2 23 36 109 < .3	8+005 4+25W	2	17	61	91	<.5	24	13	987	6.36	6	<5	<2	<2	18	.8	2	<2	27	.36	.075	19	23	.38	107	.07	<3	3.61	.01	.04	<2		
8+00s 3+75W 2 23 36 109 < .3	8+00\$ 4+00W	1	23	49	157	<.3	32	15	1114	4.36	10	<5	<2	5	26	.5	3	<2	20	.75	.118	28	23	.54	68	.03	<3	3.73	.01	-07	<2		
8+00s 3+50W 2 22 41 107 .3 36 14 389 3.87 4 <5		2																															
8+00s 3+25W 2 20 28 100 <.3																																	
8+00\$ 3+00\$ 1 20 30 125 3 29 12 526 3.57 3 -5 -2 2 15 .4 -2 -2 27 .32 .081 22 23 .73 115 .07 <3																																	
8+00s 2+75W 2 19 55 106 .3 26 8 303 3.38 6 <5 <2 3 16 .2 <2 <2 25 .39 .073 18 19 .49 98 .11 <3 4.48 .02 .06 <2																																	
STANDARD C 23 60 41 135 6.6 70 32 1069 3.99 43 18 7 38 55 17.9 17 21 60 .54 .090 40 57 .96 188 .09 25 1.97 .06 .15 11								8	303	3.38	6	<5	<2	3	16	.2	<2	<2	25	.39	.073	18	19	.49	98	.11	<3	4.48	.02	.06	<2		
	STANDARD C	23	60	41	135	6.6	70	- 52	1069	3.99	43	18	7	38	55	17.9	17	21	60	.54	.090	40	57	.96	188	.09	25	1.97	.06	.15	11		



•

ProGroup Geological Ltd. FILE # 96-0034



Page 7

ACRE ANALITICAL																														AMALTEICAL
SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	٧	Ca	Р	La	Cr	Mg	Ba	Ti	В	AL	Na	ĸ	W
	ppm	ppin	ppm	ppm	ppm	ppm	ppm	ppm		ppm	ppm	ppm	ppm	ррп		ppm		ppm	X	x	ppm	ppm		ppm	*		*	x	X	ppm
	••	<u></u>					••				••																			
8+00s 2+50W	2	24	33		<.3	25	9	859	3.38	5	<5	<2	<2	14	.5	<2	<2	34	.28		14	18	.39	88	.06	<32.		.02	.04	<2
8+00s 2+25W	1	21	29	81	<.3	29	10	445	2.98	5	<5	<2	5	14	.2	<2	<2	16	.19	.083	24	20	.53	83	.02	- ৫ 1.	.61	.01	.09	<2
8+00S 2+00W	2	23	34	76	<.3	24	9	619	3.96	10	<5	<2	2	8	.3	2	<2	27	.09	.041	22	21	.39	52	.04	<3 1.	.42	.01	.05	2
8+00s 1+75W	1	19	31	60	<.3	27	10	383	3.22	5	<5	<2	4	13	<.2	<2	<2	18	.15	.056	26	24	.49	45	.03	31.	.22	.01	.06	<2
8+00s 1+50W	1	16	33	115	<.3	27	11	1189	3.54	7	<5	<2	2	10	.5	<2	<2	22	.14	.072	23	22	.44	86	.04	્ય ર	.01	.01	.04	<2
8+00s 1+25W	1	15	28	88	<.3	22	9	648	3.93	5	<5	<2	3	14	.5	<2	<2	23	.28	.111	16	22	.32	76	.08	-34.	.35	.01	.06	<2
8+005 1+00W	1	14	43	132	<.3	33	13	1218	4.14	5	<5	<2	4	17	.6	<2	<2	23		.150	22	26	.47	93	.04	-उ ३.	.50	.01	.06	<2
8+005 0+75W	1	19	43		.5	20		3301		6	<5	<2	<2	12	.5	<2	<2	24		.049	17	16	.23	81	.05	<3 2	.10	.01	.05	<2
8+00\$ 0+50W	1	15	29		<.3	18		844		4	<5	<2	ž	11	.3	<2	<2			.047	20		.27	102	.10	<3 2				<2
8+005 0+25W	1	27		117		38		734		12	<5	<2	6	22	.3	<2	<2			.080	33		.64	105	.03	31				<2
0.003 0.234	•	L (•••		50		134	5.70				Ŷ						•••								•••	•••	• • •	-
8+005 0+00W	1	11	21	74	<.3	15	7	665	2.87	2	<5	<2	2	9	.3	<2	<2	30	.10	.042	17	15	.23	111	.07	<3 2	.71	.02	.04	<2
9+005 7+00W	i	22		114				748		6	<5	<2	9	22	.5	<2	<2		.97		26	33	.70	139	.07	33		.02		3
9+00s 6+75W	9	56	41			113		1214		29	<5	<2	11	18	1.6	<2	<2			.156	51		.83	113	.05	33		.01		~2
9+003 6+50W	2					47		634		11	<5	<2	11	23	.4	<2	3			.093	43		.78	111		<3 2				~2
9+005 6+25W	3	30	25	95	<.3			915		12	<5	<2	8	65	.9	6	<2			.098	32		2.18	73	.02	32		.01		~
94003 0423W	2	20	2	95	`. 」	42	15	915	5.02	12	0	12	o	60	.,	0	×4	44		.070	32	51	2.10		.04	01	. 10	-01	• •	~
9+00\$ 6+00W	1	12	22	59	<.3	18	0	490	7 76	4	<5	<2	4	14	.4	2	<2	26	.66	053	17	18	.30	62	.05	<32	10	.01	05	<2
9+005 5+75W	2	16	25		<.3	24		575		2	<5	<2	2	12	.4	<2	<2		.19		21	18	.38	139	.07	33			.06	<2
		16		112		35		539		11	<5	<2	4	16	.5	<2	<2			.085	29	24	.57		.08	33		.01	.07	<2
9+005 5+50W	1																				29	23	.58	120	.07	<33		.01		<2
RE 9+005 5+50W	1	17	31		<.3	34		562		6	<5	<2	5	16	.5	<2	<2													<2
9+00S 5+25W	4	38	22	115	<.5	66	18	500	3.90	11	<5	<2	(13	.3	2	<2	دد	. 17	.049	37	30	-89	77	.03	<3 2	.02	.01	-00	×2
9+00s 5+00W	4	18	21	104	. 7	27	0	519	7 25	6	<5	<2	3	10	.2	<2	<2	27	.13	05/	26	21	.40	103	.09	<34	10	.01	.06	<2
9+005 5+00W	1	20		150				1199		9	<5	<2	2	23	.8	<2	<2			.172	18	19	.39		.06	33				<2
	2					26										<2	<2			.160	24	23	•	132				.02		<2
9+005 4+50W	1	18		173		30		1589		10	<5	<2	3	20	.7								.25		.16					~2
9+005 4+25W	1	17		129	<.3	17		388		9	<5	<2	3	18	.3	<2	<2			.217		13						.02		
9+005 4+00W	2	15	51	106	د.>	23	10	1431	5.59	14	<5	<2	2	19	.3	<2	<2	27	.69	. 130	17	16	.37	120	.09	<35	.47	.02	-05	<2
0.000 7. 7.	-		74	4//		70	47	1205	7 03	13	-5	<2	,	16	4	<2	<2	26	47	.093	27	24	11	109	.03	17 7	17	.01	07	<2
9+005 3+75W	2	18		164		38		1205		12	<5		43	10	.6	3	<2				29	19		109	.03			.01	.07	<2
9+005 3+50W	1	20	28		<.3	27		791		10	<5	<2	د 7	17	.2					.073				116	.05			.01		<2
9+005 3+25W	2	21		169		40		573		13	<5	<2			.3	<2	<2			.083	27									<2
9+005 3+00W	3	31	39		.4	50		1954		13	<5	<2	7	41	.6	<2	<2			.106	34			213	.03			.02		
9+005 2+75W	2	14	25	96	<.3	25	8	349	که.د	9	<5	<2	3	9	<.2	<2	<2	21	.17	.042	21	21	.48	76	.06	<3 2	.00	.01	.05	<2
9+00s 2+50W	4	22	/7	0/	<.3	33	1/	622	7 75	11	~5	~2	4	22	.2	,	~2	20	77	.089	30	23	.60	76	.04	.7.2	22	.02	08	<2
	1	22	43								<5 <5	<2	4	22 8		4	<2 3	20		.032	26	19	.32		.04					~2
9+005 2+25W	1	14	30		<.3	23		217		8		<2		-	<.2		-	_										.01		
9+005 2+00W	2	31	34	109		43		450		13	<5	<2	5	17		<2	<2			.068	27	26	.81		.04					
9+005 1+75W	1	18	20		<.3	29		314		9	<5	<2	2	9	<-2	3	<2			.053	25	25	.56		.03			.01	.06	2
9+00s 1+50W	2	11	12	31	<.3	12	4	121	2.19	5	<5	<2	<2	4	<.2	2	<2	28	.02	.022	26	12	.10	22	.03	ذ>	.11	.01	.04	2
	-		<i>.</i> -	404		-	70		7 0/			-			47 /	47	10			007		12	-	4.04	07	26.4		04	•/	44
STANDARD C	22	57	43	126	6.3	71	- 52	1035	5.94	41	17		- 57	50	17.6	17	19	60	.50	.087	45	62	.90	181	.07	20 1	.88	.06	. 14	11



•

ProGroup Geological Ltd. FILE # 96-0034



٦

ACHE ANALTTICAL				·	<u> </u>																								ACHE	ANAL TTICAL
SAMPLE#	Mo	Cu	Pb	Zn	Ag	Nī	Co	Mn	Fe	As	ບ	Au	Th	Sr	Cd	Sb	Bi	v	Ca	Р	La	Cr	Mg	Ba	Ti	B	AL	Na	ĸ	W
	ppm	ppn	ppm	ppm	ppm	ppm	ppm	ppm	X	ppm	ppm	ppm	ppm	ррп	ppm	ppm	ppm	ppm	*	X	ppm	pom	*	ppm	X	ppm	X	X	X	ppm
				<u> </u>			<u></u>						,,			••														
9+00s 1+25W	2	12	29	53	<.3	14	7	551	3.43	4	<5	<2	<2	6	.2	3	<2	29	.05	.059	19	16	.23	27	.07	<3	1.59	.01	.07	<2
9+00\$ 1+00W	1	29	34	76	<.3	31	12	740	2.98	9	<5	<2	5	38	.4	3	<2	17	1.81	.089	28	16	1.20	60	.04	ব্য	1.25	.02	.11	<2
9+00s 0+75W	1	24	50	107	<.3	38	14	844	3.98	7	<5	<2	5	15	.5	2	<2	28	.25	.095	26	31	.74	93	.06	ব ়	3.91	.02	.07	<2
9+00s 0+50W	1	22	43	128	<.3	38	15	1205	3.70	9	<5	<2	6	20	.8	<2	<2	26	.34	.107	33	33	.81	86	.07	্য :	3.18	.02	,29	<2
RE 9+00S 0+50W	1	23	48	134	<.3	41	16	1257	3.85	9	<5	<2	7	21	.6	4	<2	28		.112	35	34	.84	91	.07	্ৰ :	3.32	-02	.31	2
9+00s 0+25W	2	14	29	110	<.3	22	10	680	2.91	7	<5	<2	3	8	.3	<2	<2	23	.09	.049	26	15	.35	68	.06	্ৰ :	3.52	.01	.06	2
9+00\$ 0+00W	2	23	34	81	<.3	24	11	709		4	<5	<2	<2	26	.3	<2	<2	22	.68	.056	25	20	.41	80	.04	ব্য :	2.94	-01	.07	<2
10+00S 7+00W	1	19	28	72	<.3	28	9	443	3.09	5	<5	<2	7	18	.3	<2	<2	23	.92	.051	27	17	.40	107	-08	্ৰ :	3.19	-02	.07	<2
10+00s 6+75W	1	20	31	132	<.3	23	9	862	3.27	2	<5	<2	4	19	.7	<2	<2	30	.95	.153	23	18	.31	113	.06	্ৰ :	3.86	.02	.06	<2
10+00\$ 6+50W	2	21	38	80	<.3	36	13	746	3.46	3	<5	<2	7	34	.6	<2	<2	23	1.90	.102	47	22	.62	79	.04	ও	2.89	.02	.08	<2
	_									_	-	_				_	_									_				-
10+00s 6+25W	1	22	37	117	<.3	38	12	556	3.73	10	<5	<2	10	52	.3	<2	<2	23	.85	.086	43	18	.46	72	.03	3	1.71	.01	.07	<2
10+005 6+00W	1	21	38	124	<.3	43	· 13	627	4.34	10	<5	<2	10	57	.8	2	<2		1.45		33	26	.50	138	.03		3.50	.01	.09	2
10+00S 5+75W	<1	16	35	94	<.3	34	10	702	3.81	2	<5	<2	9	13	.7	<2	<2	29		.062	25	22	.47	162	.09		5.21	.02	.07	<2
10+00\$ 5+50W	2	35	43	114	<.3	40	14	682	4.08	11	<5	<2	4	15	.7	3	<2	23		.111	31	23	.67	126	.01		2.71	.01	.11	2
10+00s 5+25V	1	12	18	63	<.3	18		685		3	<5	<2	<2	14	<.2	<2	2	25		.032	23	18	.43	113	.02		1.44	.01	.08	<2
	·	•=			••		•			-	-	-	-			-	-		• • •							-		•••		-
10+00\$ 5+00W	1	19	35	159	<.3	36	12	1087	3.67	5	<5	<2	4	18	.7	<2	<2	26	.52	.108	30	23	.57	140	.03	3	2.25	.01	.12	<2
10+00s 4+75W	1	13	25	125	<.3	21		1113		2	<5	<2	<2	14	.4	<2	2	25		.060	21	15	.34	117	.06		2.94	.01	.07	<2
10+00\$ 4+50W	1	22	28	65	<.3	28	11	764		4	<5	<2	6	22	.3	<2	<2	17		.095	36	16	.58	78	.02		1.28	.01	.13	<2
10+00s 4+25W	Ż	17	37	86	<.3	27		728		6	<5	<2	2	10	3	<2	<2	25		.065	27	19	.47	108	.04		2.89	.01	.09	<2
10+005 4+00W	<1	16	36	108	.3	24		1841		2	<5	<2	2	21	.9	<2	<2	23		.110	27	17	.39	107	.06		4.44	.02	.07	<2
							-			_	-	_	_			_	_									_				-
10+00s 3+75₩	2	14	32	79	<.3	23	10	1012	3.18	5	<5	<2	2	26	.3	<2	<2	25	.76	.086	21	16	.38	93	.05	<3	3.11	.01	.07	<2
10+005 3+50W	2	16	38	57	<.3	15	8	901	4.37	<2	<5	<2	3	8	.6	<2	<2	25		.090	20	20	.22	80	.06	<3	4.19	.01	.05	<2
10+00s 3+25W	2	18	35	51	<.3	16	7	938		8	<5	<2	2	10	.6	<2	<2	24		.163	20	16	.17	53	.05		1.96	-01	.03	<2
10+005 3+00V	1	18	39	70	<.3	23	13	959		4	<5	<2	4	8	.5	<2	<2	24		.098	26	25	.36	67	.04		4.04	.01	.05	<2
10+00S 2+75W	1	24	29	73	<.3	37	13	693		4	<5	<2	5	12	.4	<2	<2	32	.16	.088	25	40	.91	54	.10		2.86	.01	.13	<2
		- ·								-	-	-	•	•=	•••	-										-				-
10+00s 2+50W	<1	16	23	68	<.3	19	10	687	3.02	6	<5	<2	2	13	.2	<2	<2	18	.09	.043	24	15	.44	73	.03	<3	1.31	.01	.12	<2
10+00s 2+25W	1	12	26	56	<.3	17		619		3	<5	<2	2	19	< 2	<2	<2	14	.31	.047	25	13	47	81	.03		1.40	.01	.10	<2
10+005 2+00W	2	16	25	93	<.3	21		2017		7	<5	<2	<2	9	.4	<2	2	22	.11	.056	26	18	.37	57	.03		2.07	.01	.06	<2
10+00s 1+75W	1	20	41	74	<.3	30		511		8	<5	<2	6	19	.3	2	<2	20		.078	31	22	.60	72	.04		1.90	.02	.09	<2
10+00s 1+50W	1	15	39	82	<.3	28		417		10	<5	<2	ž	11	.3	<2	<2	21	.15	.085	24	20	.51	58	.04	-	2.62	.01	.07	<2
	1 .										-		-		•-		-		••••		- ·				•••	•				-
10+00s 1+25¥	2	42	44	161	<.3	44	16	830	4.13	9	<5	<2	8	12	.5	2	<2	22	. 19	.081	30	24	.79	90	.02	<3	2.87	.01	.11	<2
10+005 1+00W	2	21	105	122	<.3	26	• -	1057		5	<5	<2	<2	15	.5	<2	<2	26		.073	21	18	.36	56	.05		3.13	.01	.06	<2
10+00s 0+75V	1	21	52	131	<.3	28		1135		9	<5	<2	2	36	.6	<2	2		1.16		24	21	.74	95	.03		1.78	.03	.08	<2
10+00s 0+50W	1	25	41	151	<.3	27		1846		7	<5	<2	<2	28	.9	<2	<2	27		. 125	23	25	.50	109	.06		3.34	.02	.06	<2
10+005 0+25W	Ż	27	40	95	.3	35	13	767		12	<5	<2	4	26	.7	<2	<2	18	.68	.088	31	20	.64	69	.04		1.79	.02	.09	<2
,0.000 0.20M	-	- 1	-10			~~		, 0,				~	-	20	• 1	- [~	10	.00			20		,		~			,	-
10+005 0+00W	1	22	31	118	<.3	30	12	1134	3,19	11	<5	<2	3	24	.7	<2	<2	18	_61	.056	30	16	.53	85	.04	<3	1.57	.01	.07	<2
STANDARD C	22	55		125		68		1056		38	14	7	37		17.6	18	16			.095	42			176	.07		1.88		.14	10
												•																	• • •	

APPENDIX 3

FIGURES

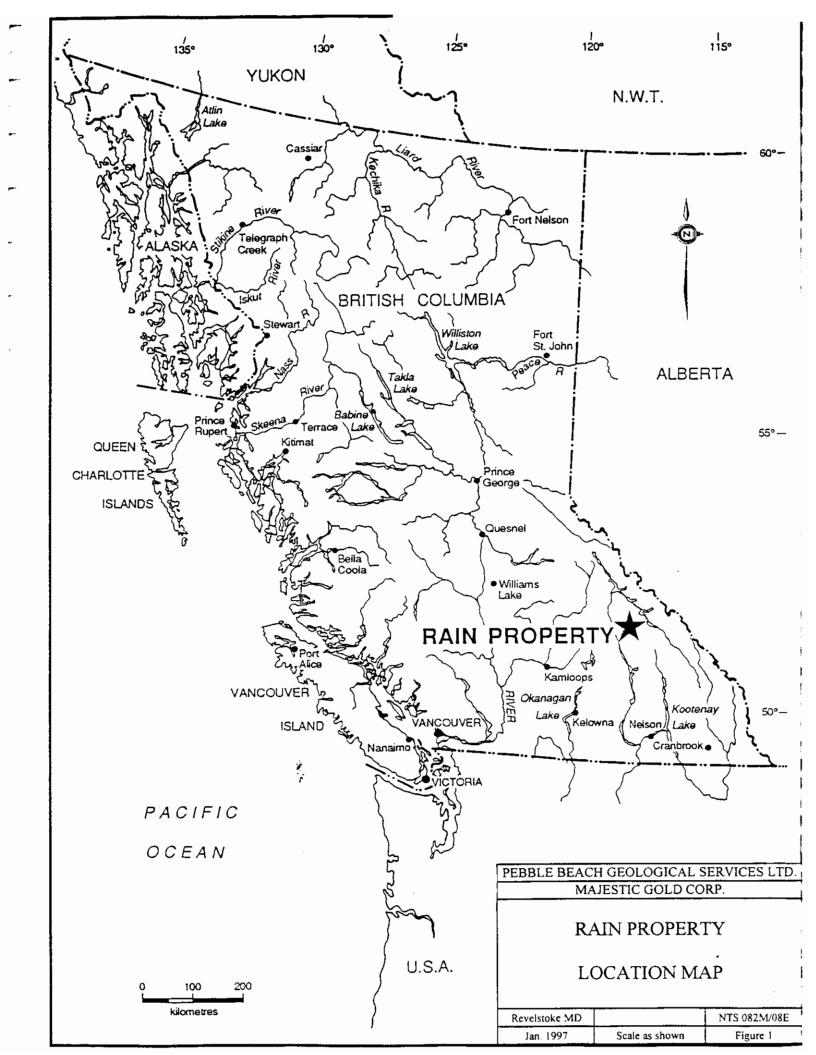
•

.

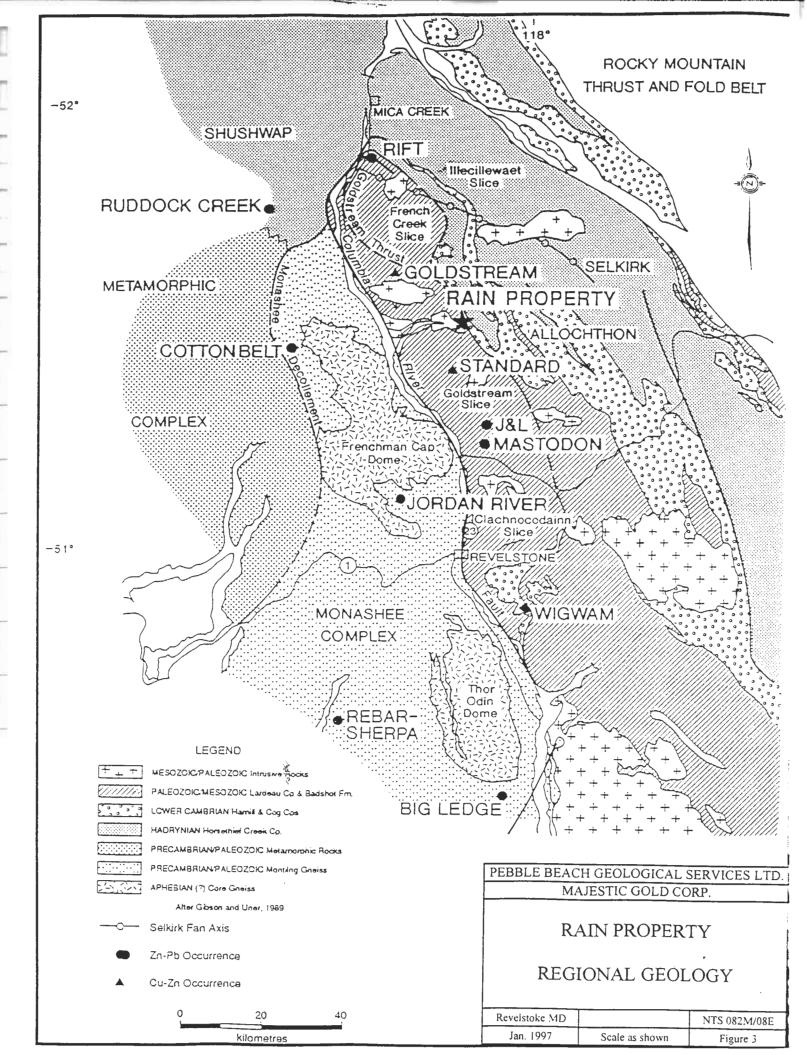
-

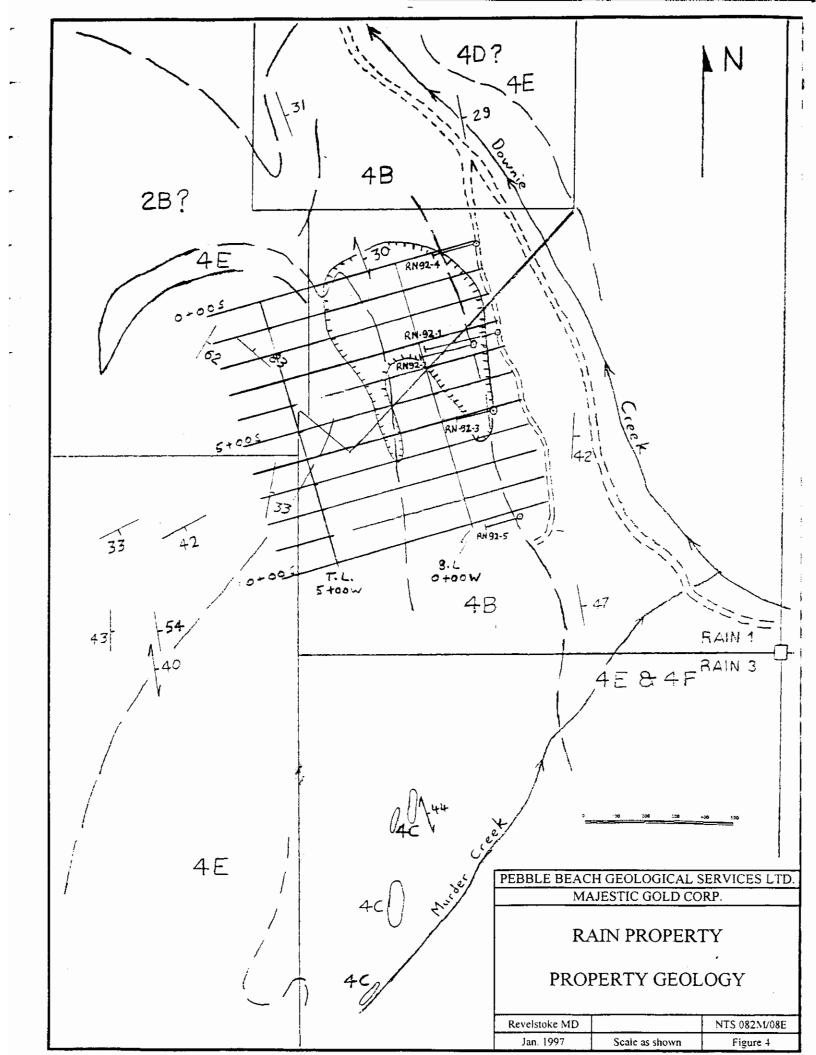
.

-



DROP 10 DROP 10 DROP 10 DROP 10 DROP 10 DROP 10 DROP 10 DROP 1 DROP 1 DROP 1 DROP 1 DROP 1 DROP 1 DROP 1 DROP 1 DROP 2 DROP 3 DROP 2 DROP 3 DROP 2 DROP 4 DROP 1 DROP 2 DROP 4 DROP 4 DROP 4 DROP 4 DROP 4 DROP 4 DROP 4 DROP 5 DROP 7 W ¹⁰ DROP 2 DROP 4 DROP 4 DRO		EFIELD	ICEFTELD SERVICES LTD.
0 <u>2000</u> 4000 metres	MA	H GEOLOGICAL S AJESTIC GOLD CC AIN PROPER CLAIM MAP	rp. ΓΥ
	Revelstoke MD Jan. 1997	Scale: 1 : 50,000	NTS 082M/08E Figure 2





GEOLOGY LEGEND for Figure 4

Lardeau Group - Paleozoic

- 4 F Quartz- Chlorite Sericite Schist, minor Marble, Quartzite
- 4 E Marble
- 4D Sulphide Layer
- 4C "Garnet Zone" cherty and graphitic schist
- 4 B Quartz Graphite Biotite Schist, strongly calcareous
- 4 A Talc Schist

Badshot Formation - Paleozoic

- 3 B Marble
- 3 A Calc Schist

Hamill Group

- 2 B Quartzite
- 2 A Quartz Biotite Muscovite Schist, Quartzite

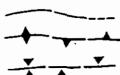
Horsethief Creek - Proterozoic

- 1 B Dolomite, Micaceous Quartzite, Chlorite Schist
- 1 A Marble
- Intrusive Rocks Cretaceous
 - Traverse Station

Attitude of Bedding (S0), Primary Foliation (S2), and Crenulation Cleavage (S3)

Geological Contact - defined, assumed, interred

Direction/Plunge of Minor Fold Axis (F2 and F3) and Lineations (L2 and L3); vergence as viewed down plunge.



Major Antiform - defined, assumed

Major Synform - defined, assumed

www.Fault-defined, assumed

14

٨

Gossan

 \bigcirc

G,

Extent of Outcrop

Mineral Occurrence

- Legal Corner Post, location from claim map
- 2 Post Claimpost

======= Logging Road

Claim Boundary

		7+001	Ĩ		6+0 	011			5+	901	A		4+	+001	W		3	+00	₩		2	+00	W		1	+00	W			B/L 	
24003 91 1 <td< th=""><th>0+005</th><th>31</th><th>6 20</th><th>20</th><th>16</th><th>19</th><th>117</th><th></th><th></th><th>42</th><th>31</th><th>31</th><th>48</th><th>52</th><th>101</th><th>42</th><th>38</th><th>50</th><th>74</th><th>37</th><th>- 6</th><th>119</th><th>. 307</th><th>36</th><th>13</th><th>37</th><th>56</th><th>44</th><th>21</th><th>66</th><th> </th></td<>	0+005	31	6 20	20	16	19	117			42	31	31	48	52	101	42	38	50	74	37	- 6	119	. 307	36	13	37	56	44	21	66	
34003 1 <td>1+005</td> <td>53</td> <td>22</td> <td><mark>9</mark> ੰ ਦ</td> <td>20</td> <td>41</td> <td>29</td> <td></td> <td>61</td> <td></td> <td>18</td> <td>11</td> <td>29</td> <td>27</td> <td>40</td> <td></td> <td>29</td> <td>47</td> <td>11</td> <td>50</td> <td>29</td> <td>107</td> <td>169</td> <td>44</td> <td>73</td> <td>96</td> <td>92</td> <td>42</td> <td>20</td> <td>47</td> <td> </td>	1+005	53	22	<mark>9</mark> ੰ ਦ	20	41	29		61		18	11	29	27	40		29	47	11	50	29	107	169	44	73	96	92	42	20	47	
34003 $\frac{1}{2}$		15	12	1	17	18	24	₩ 0 2 +	10	12	13	17	, 22	20	15	24	43	26	43	44	. 15	49	185	107	101	63	53	18	30	26	
44003 $\frac{1}{2}$ $\frac{1}{2}$ $\frac{9}{2}$ $\frac{1}{2}$ $\frac{9}{2}$ $\frac{1}{2}$ $\frac{9}{2}$ $\frac{9}{2}$ $\frac{1}{2}$ $\frac{9}{2}$ $\frac{9}{2}$ $\frac{1}{2}$ $\frac{9}{2}$ $\frac{9}{2}$ $\frac{1}{2}$ $\frac{9}{2}$	3+005	.13	17	1	21	10	61		14	c1 •	33	16	15	15	14	25	113	38	14	20	<u>б</u>	64	33	41	42	18	22	48	46	14	
64003 1 <td>4+00S</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>18</td> <td></td> <td>17</td> <td>16</td> <td>20</td> <td>15</td> <td>25</td> <td>17</td> <td>14</td> <td>11</td> <td>2</td> <td>43</td> <td>12</td> <td>25</td> <td>33</td> <td>28</td> <td>41</td> <td>59</td> <td>21</td> <td>46</td> <td>84</td> <td> </td>	4 +00S									18		17	16	20	15	25	17	14	11	2	43	12	25	33	28	41	59	21	46	84	
7+005 7 8 8 9 <td>5+008</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1</td> <td>1 34</td> <td>19</td> <td>16</td> <td>21</td> <td>17</td> <td>23</td> <td>о,</td> <td>15</td> <td>34</td> <td>20</td> <td>. 15</td> <td>32</td> <td>16</td> <td>14</td> <td>61</td> <td>27</td> <td>19</td> <td>23</td> <td>19</td> <td></td> <td>20</td> <td> </td>	5+008								1	1 34	19	16	21	17	23	о ,	15	34	20	. 15	32	16	14	61	27	19	23	19		20	
	6+00S																		•	•			• .	•	- -				• ·		
										•					•••		-•		•			•-	•	• .		•	•		•		
.		2	56	27	30	16	10	16		•					•		•		•							•		•			-
			•	-			-		·	,	·		·	·	-		-		-		·		-		-	•	-		•		

	H GEOLOGICAL S JESTIC GOLD CO				
RAIN PROPERTY					
SOIL GEOCHEMISTRY - COPPER					
Revelstoke MD		NTS 082M/08E			
Jan. 1997	Scale: 1 : 25,000	Figure 5			

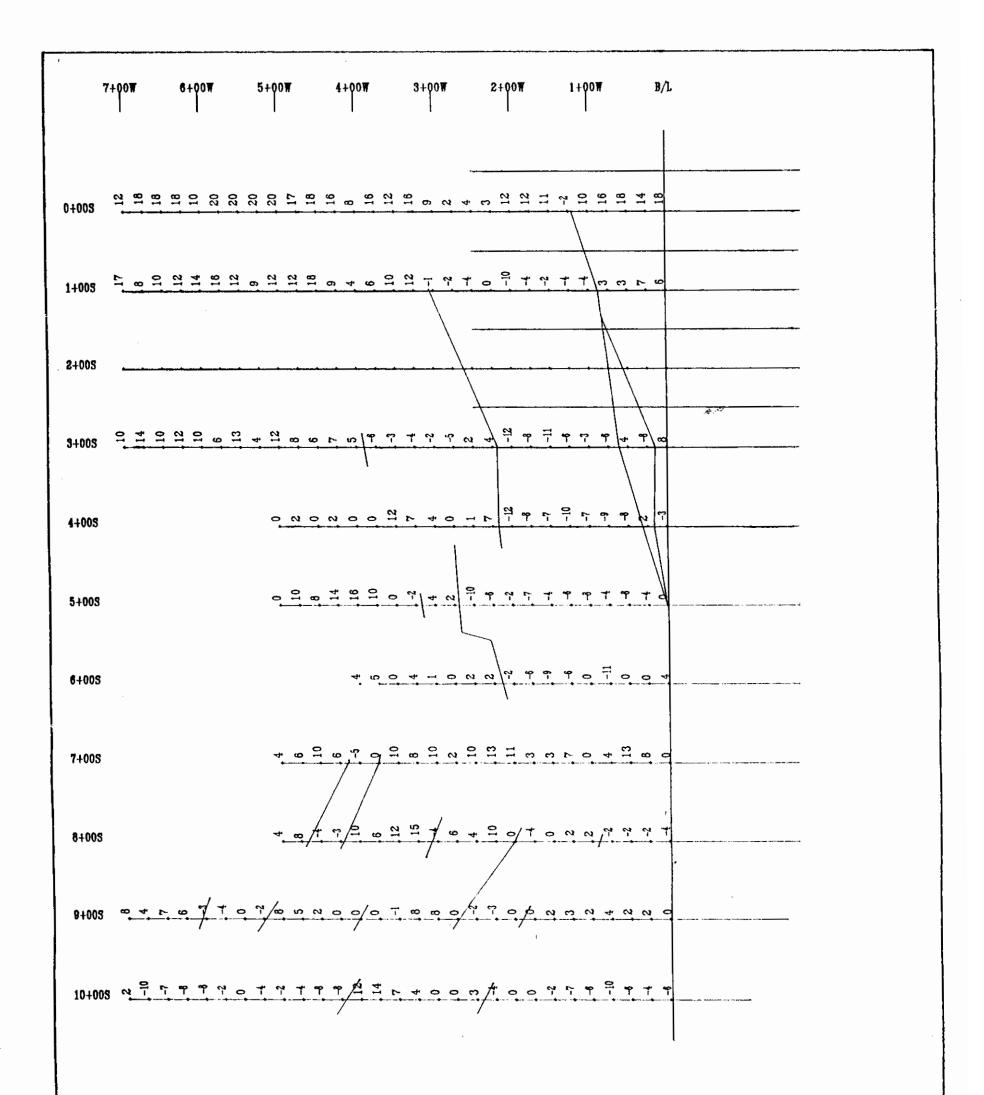
	7+00	¥		6+0	011		5	+00	Ħ		4+	00₩	,		3+	00₩			2+(po w		1	+00'	W		B,	/L
0+003	, 122	21	104	122	116	278	343	305	489	133	167	180	001	115	021	67 T	211	- 15	133	<u>50</u>	162	- <u>5</u>	209	223	319	372	2
1+005	106	109	10%	73	240	1337	155	200	230	86	111	22	*	507	211	011	60 06		24.2	182	177	197	199	20/		121	
2+005	48	28	54	63	89	061	595	312	213	81	134	101	114	115	100	00	001 271	14.		187	246	319	275	87	\$ (318	V CTC
3+005	139	66	71	99	25	67	40	32	134	50	47	121	63	140	50	CD .	43	13.	100	168	911	140	55	118-	133	138	
4+005								، 65		208	02	12	63	147	80	68	10	134	902	115	77	108	182	129	122	171	136
5+00S								, 92	55	56	80	130	1 88	46	81	143	68 t	108	123	65	113	124	124	11	129	Z	91
6+005								, 71				=		177	174	66	118	<u>.</u>	145	118	106	195	91	41	82	125	88
7+005								, 66		60	118	62	23	95	137	108	133	6	18	130 85	95	85	65	. 75	159	126	68
8+003								.42	87	67	16	157	109	101	100	125	106	103	81	50 80	115	88	132	126	80	1117	. 74
9 +005	.114	252	501	95 5 5	34 84	112	115	104	150	173	129	106	164	105	169	500	96	86	62	109	31	53	176	107	128	110	81
10+00	s 22	132	80	117	94	114	63	159	125	65	86	108	64	57	51	20	13	68	56	93	82	161	122	131	151	95	118

PEBBLE BEACH GEOLOGICAL SERVICES L						
MA	RP.					
	AIN PROPERT					
Revelstoke MD		NTS 082M/08E				
Jan. 1997	Scale: 1 : 25,000	Figure 6				

•

.

`



	H GEOLOGICAL S JESTIC GOLD CO	· · · · · · · · · · · · · · · · · · ·		
RAIN PROPERTY VLF - EM PROFILES				
Revelstoke MD		NTS 082M/08E		
Jan. 1997	Scale: 1 : 25,000	Figure 7		

•

I.