Report of 1996 Geological, Geochemical, and Geophysical Exploration Work Done on Aftom, Calvin, Dup, Fred, Hags, Hob, Hop, Mojo, Noot, Pmac, and Rags Mineral Claims

Volume 2 of 2 Volumes

Volume 2 for Work on Fred, Pmac, and Noot Claims

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SUB-RECORDER

John Peaks Area, NTS 1048/9 Snippaker Creek Area, NTS 104B/10 Skeena and Liard Mining Divisions British Columbia

by

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GEOLOGICAL SURVEY BRANCH ASSESSMENT REPORT

24,855

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# Introduction

#### Location, Access, and Topography

The Eskay Reconnaissance Area is located in northwestern British Columbia, approximately 70 kilometers north of Stewart and 900 kilometers northwest of Vancouver (Fig. 1). Reference maps are NTS Sheets 104B 9W and 10E.

The area is within the Unuk River watershed. Major drainages include the Unuk River, Coulter Creek, and Storie Creek. All rivers and creeks originate from glacial meltwaters, and reach peak flow conditions in the summer months.

Present access is by helicopter from a camp located along the Eskay Creek Mine road about five kilometers from the mine. The Eskay Creek Mine road extends from the Stewart-Cassier Highway at Bob Quinn Lake to the Eskay Creek Mine.

The region is mountainous with elevations ranging from 250 meters on the Unuk River to approximately 2150 meters at John Peaks. Mountain slopes are moderate to very steep. The treeline occurs at about 1200 meters and at higher elevations, valleys are commonly filled with glaciers. Semi-permanent ice and snow may be encountered on north facing slopes. Snow conditions are extreme in alpine areas while river bottom areas receive little, if any, snow. However, precipitation in the form of rain occurs all year round.

Valley bottoms are densely forested with mature stands of fir, sitka spruce, cedar, hemlock, aspen, alder, and maple. A thick undergrowth of ferns, salmonberry, huckleberry, copperbrush, and devils club is usually present.



# **Property and Program**

#### Claims

The 1996 exploration by Canamera in the Eskay Creek area was done on various Aftom, Dup, Fred, Hags, Hob, Hop, Mojo, Noot, Pmac and Rags claims. The work and dates of work done on individual claims is listed in the Statements of Work in Appendix 3. All of these claims are in the Skenna and Liard Mining Divisions. The claims are privately owned and held in the name of Tagish Resources, Alex H. Briden or Briden/El Cap Gold Mines. All the work was done by Canamera Geological Ltd. The following is a list of claims which were explored or had assessment filed from contiguous claims:

Claim Name	TNR #	NTS	# of Units	Anniversary	Owner
Aftom 1	253140	104 B9\A/	20		Tagish
Aftom 3	253142	104 B0W	12	97/09/09	Tagish
Aftom 4	253143	104 B9\A/	12	97/09/10	Tagish
Aftorn 5	253144	104 B0W	20	97/09/10	Tagish
Aftom 7	253146	104 B0W	16	97/09/16	Tagish
Aftorn 10	253148	104 B0VV	20	97/09/09	Tagish
Aftom 11	253149	104 B9\//	20	97/09/09	Tagish
Aftom 13	253151	104 B9\A/	20	97/09/11	Tagish
Aftom 16	253154	104 B344	20	97/09/18	Tagish
Dup 9	252489	104 B9\M	20	98/02/24	Briden/El Cap
Ered 15	253295	104 B10F	15	00/10/11	Briden H Alex
Hags 5	253254	104 B9\M	15	97/09/30	Briden H Alex
Hob 3	313286	104 B9\M	1	97/09/10	Tanish
Hob 4	313287	104 B9W/	1	97/09/10	Tagish
Hob 8	313291	104 B9W	1	97/09/12	Tagish
Hob 8 5	313292	104 B9W	1	97/09/12	Tagish
Hob 9	313293	104 B9W	1	97/09/12	Tagish
Hob 10	313294	104 B9W	1	97/09/12	Tagish
Hob 11	313295	104 B9W	1	97/09/12	Tagish
Hob 12	313296	104 B9W	1	97/09/12	Tagish
Hob 13	313297	104 B9W	1	97/09/12	Taoish
Hob 14	313298	104 B9W	1	97/09/12	Tagish
Hob 15	313299	104 B9W	1	97/09/12	Tagish
Hob Frac	313301	104 B9W	1	97/09/17	Tagish
Hop 5	313288	104 B9W	1	97/09/10	Tagish
Hop 6	313289	104 B9W	1	97/09/10	Tagish
Hop 7	313290	104 B9W	1	97/09/10	Tagish
Mojo	320729	104 B9W	20	97/08/28	Tagish
Mojo 2	321037	104 B9W	20	97/09/14	Tagish
Noot 1	306723	104 B10E	20	00/11/29	Tagish
Noot 2	306724	104 B10E	20	00/11/29	Tagish
Noot 3	306725	104 B10E	20	97/11/29	Tagish
Noot 4	306726	104 B10E	20	00/11/29	Tagish
Noot 5	306727	104 B9W	20	97/11/25	Tagish
Pmac 1	253176	104 B10E	1	00/09/14	Briden, H. Alex
Pmac 2	253177	104 B10E	1	00/09/14	Briden, H. Alex

Pmac 3	253178	104 B10E	1	00/09/14	Briden, H. Alex
Pmac 4	253179	105 B10E	1	00/09/14	Briden, H. Alex
Pmac 5	253180	106 B10E	1	00/09/14	Briden, H. Alex
Pmac 6	253181	107 B10E	1	00/09/14	Briden, H. Alex
Pmac 7	253182	104 B10E	1	00/09/14	Briden, H. Alex
Pmac 8	253183	108 B10E	1	00/09/14	Briden, H. Alex
Pmac 9	253184	104 B10E	1	00/09/14	Briden, H. Alex
Pmac 10	253185	104 B10E	1	00/09/14	Briden, H. Alex
Rags 1	224392	104 B9W	16	97/09/30	Briden, H. Alex
Rags 2	224393	104 B9W	16	97/09/30	Briden, H. Alex
Rags 3	224394	104 B9W	16	97/09/30	Briden, H. Alex
Rags 4	224395	104 B9W	16	97/09/30	Briden, H. Alex

This volume will detail the work done on the Fred 15, P-mac 1-10, and Noot 1-4 claims. The rest of the claims were covered in the first volume of this report.

#### **Objectives**

The objective of the 1996 exploration program consisted of three parts. First, a structural analysis of the northern Bowser Lake Group claims in order to evaluate the possibility of Hazelton Group rocks extending underneath. Second, a UTEM geophysical program and detailed mapping on the Fred 15 and Pmac claims to follow up on the anomalous gold showings found in 1995. Third, further reconnaissance mapping and sampling within areas of potential Upper Hazelton Group Unit 5 rocks.

#### Scope of Program

During the 1996 field season, Canamera conducted a field program of structural, grid, and reconnaissance mapping, prospecting, soil geochemical sampling, and UTEM geophysics. The structural and reconnaissance mapping was done at 1:5000 while the detailed grid mapping was at 1:1000 scale. Ground control was established with B.C. government air photos, 1 to 5000 metric contour maps, and, in the Fred 15 area, 1:1000 metric contour maps based from 1:10000 orthophotos. Existing grids from previous work and new flagged lines were used for reconnaissance mapping and soil sampling. A new cut and surveyed grid was the basis of the detailed mapping and UTEM program in the Fred 15 area. One new helipad was cut on Aftom 7. No trenching was done.

# **Personnel and Dates**

Geologists Dane Bridge and Greg Burroughs performed mapping and prospecting. Professor Simon Haynes performed the mapping and structural interpretation on the Bowser Lake Group. Assistants Jason Shaw, Ayisha Yeow, Jason Attard, and Jason Gallagher performed soil sampling, and grid flagging. MFH Contracting was used to cut the new grid while Fred Kaiser and Jason Scoffings surveyed it. SJ Geophysics Ltd. performed the UTEM survey. Field work was done between August 11th and September 16th 1996. Information on days worked by specific individuals is included in the cost statements in Appendix 2.

#### **Data Presentation**

# **Distribution of Work Done in 1996**

This report documents the work for a total of eight statements of work (Appendix 3) on seven claim groups and one individual claim. There are a total of eight cost statements (Appendix 2) distributing the work done on these groups and claim. This volume of the report will cover two statements of work and cost statements 7 and 8. The remaining statements of work and cost statements vere covered in volume one.

## **Geologic Mapping**

Structural, grid, and reconnaissance mapping at 1:5000 is presented on six topographic sheets. Detailed mapping, on the Fred grid, at 1:1000 is presented on two topographic sheets.

The geologic and geochemical data and interpretation in this report is organized into sections based on the location within the Eskay work area. Five individual areas had work performed on them. This volume covers the work on project area 5 while project areas 1-4 were covered in volume one.

#### Individual Project Areas

Project Area 1 - Bowser Lake Structural Study (Map sheets 2-7, in volume 1)

Project Area 2 - Aftom 5 (Map sheet 8, in volume 1)

Project Area 3 - Aftom 7 Group (Map sheet 9, in volume 1)

Project Area 4 - Dup 9 Group (Map sheets 10-11, in volume 1)

Project Area 5 - Fred Groups (Map sheets 12-14, in volume 2)

# **Geochemical Sampling**

Soil and rock sampling was done in conjunction with prospecting and mapping. Soil and rock samples are located on the grids or lines where they were collected and are plotted on the

1:5000 topographic sheets. Sample location maps are listed in the list of maps and analytical results are in the appendices.

Soil samples were collected in the B horizon using a mattock and narrow shovel. Samples were collected in high wet strength kraft paper bags and shipped to Chemex Labs Ltd. The grids were sampled on 25 meter centers on 100 meter spaced lines. Reconnaissance soil lines were up to two kilometers long with samples taken every 25 meters. Infill sampling was done on the 1995 Dup 9 grid with new lines every 100 meters between the 2+50m to 7+50m south stations. Minor infill sampling was done, around a single anomalous 1995 sample, on the Fred grid. Results plotted or discussed in this report are in ppb for Au and ppm for all other elements. Nine soil sampling lines were established in 1996 to test the prospective areas, and portions of the 1996 Fred grid were sampled to test the ground yet untested. The individual soil lines and grids are discussed in this report in conjunction with the individual project area where they are located.

Geochemical statistics reported for sampling on the soil grids are threshold, and anomalous. Threshold is mean plus one standard deviation and anomalous is mean plus two standard deviations. Samples with high Mn or Fe contents and indications of adsorption were removed from the sample populations used to calculate statistics.

Rock samples were collected in areas of anomalous pyrite or other sulphide concentrations, or from outcrops with quartz veining or hydrothermal alteration assemblages. Rock sample descriptions are in Appendix 4 and analyses are in Appendix 5.

### Analytical Procedures

Soil and rock samples were processed and analyzed by Chemex Labs Ltd., North Vancouver, British Columbia.

#### Geochemical Gold Analysis

Samples for geochemical Au analysis are catalogued and dried. Soils are prepared by sieving through an 80 mesh screen to obtain a -80 mesh fraction. Rock samples are crushed in two stages to -10 mesh and a 250 gram subsample is pulverized on a ring mill to -140 mesh. The subsample is rolled, homogenized and bagged in a prenumbered bag. The sample is weighed to 10 grams and fused with flux. The bead is digested in aqua regia and analyzed by AA. Over-range samples are re-analyzed using gold assay methods. Appropriate reference materials accompany the samples through the process allowing for quality control. Results are entered and printed along with quality control data (repeats and standards).

# **Multi Element ICP Analysis**

Soil samples are screened to obtain a -80 mesh sample. Rock samples are crushed in two stages to -10 mesh and pulverized on a ring mill to -140 mesh and rolled and homogenized. A 1.0 gram sample is digested with concentrated nitric and aqua regia acids. The aqua regia contains beryllium which acts as an internal standard. The sample is analyzed on a Jarrel Ash ICP unit. Results are collated by computer and printed along with quality control data.

# Gold Assays

Samples are sorted, dried and crushed in a jaw crusher and cone or roll crusher to -10 mesh. The sample is split through a Jones riffle until a 250 gram subsample is achieved. The subsample is pulverized in a ring and puck pulverizer to 95% -140 mesh then rolled and homogenized. Appropriate standards and repeats for quality control accompany the samples and are printed with the sample results.

#### **Base Metal Assays**

Samples are catalogued and dried. Rock samples are crushed in two stages followed by pulverizing a 250 gram subsample. The subsample is rolled, homogenized and bagged in a prenumbered bag. A suitable sample weight is digested with aqua regia. The sample is cooled, bulked up to a suitable volume and analyzed by an AA instrument with a 0.1 ppm detection limit. Appropriate certified reference materials accompany the samples through the process for quality control. Result data is entered along with repeat values.

## **Regional Geology**

#### Introduction and Previous Work

The regional geology of the claim area was established by geologists of the Geological Survey of Canada (Anderson, 1989; Anderson and Thorkelson, 1990) and the British Columbia Geological Survey Branch (Alldrick and Britton, 1988; Alldrick et al., 1989, 1990). Lewis (1992) established a structural framework for the Prout Plateau, which is along the western margin of the claims.

Exploration on the claims has focused on discovering Eskay Creek type deposits. The Eskay Creek deposit and property geology are described by Bartsch (1990a and b), Idzizek et al.(1990), Blackwell (1990), Britton et al. (1990), Ettlinger (1991), Roth and Godwin (1992) and Roth (1993a, 1993b).

The claim area is underlain largely by Jurassic volcanic and sedimentary strata of the Hazelton Group and Bowser Lake Group. A portion of the most eastern Hazelton Group rocks is underlain by an area of Triassic Stuhini Group. Some previously unrecognized intrusive rocks, probably of Jurassic age, form sills or dikes in the Hazelton Group.

### Stuhini Group

The oldest Mesozoic strata in the region are sedimentary and volcaniclastic rocks of the Triassic Stuhini Group. The Stuhini Group consist of a dominantly sedimentary lower division and a dominantly volcanic and volcaniclastic upper division. Most of the sedimentary division comprises undifferentiated fine grained well bedded rocks but coarser conglomerate layers serve as local stratigraphic markers. The volcanic division is locally subdivided into mafic to intermediate tuff and volcanic breccia, mafic porphyritic flows, and felsic flows and flow breccia.

#### Hazelton Group

The Hazelton Group has undergone considerable redefinition since it was defined to encompass Jurassic and Cretaceous volcanic and sedimentary strata of the Skeena River region of central British Columbia. Present usage is restricted to Lower and Middle Jurassic volcanogenic and sedimentary strata in this region (Tipper and Richards, 1976). Hazelton Group rocks are widely distributed within Stikinia, outlining much of the Bowser Basin, and were first described in the Iskut River camp by Schoefield and Hanson (1992). Noting differences from classical Hazelton Group sequences, Grove (1986) established a formational nomenclature for the Iskut River-

Salmon River-Anyox region separate from existing, more regional, definitions. The nomenclature, with subsequent modifications by Anderson and Thorkelson (1989), Alldrick (1991), and Henderson et al.(1992), outlines a five-fold division within the Hazelton Group in the Iskut river camp, comprising the Jack, Unuk River, Betty Creek, Mount Dilworth, and Salmon River formations (Jack and Mount Dilworth formations not formally defined). Difficulties in correlating these units regionally, ambiguous stratigraphic relations at type sections, and apparently contradictory age assignments (Lewis et al. 1992, 1993) have led to inconsistent usage of these formational divisions in the Iskut River area. Lewis (1995) has divided the Hazelton Group into 5 rock-stratigraphic units. These units comprise, from lowest to highest: i) basal, coarse to fine grained, locally fossiliferous siliciclasatic rocks or granitic pebble conglomerate, ii) porphyritic andesitic composition flows, breccias, and related epiclastic rocks, iii) dacitic to rhyolitic flows and tuffs, iv) locally fossiliferous marine sandstone, mudstone, and conglomerate, and v) bimodal subaerial to submarine volcanic rocks and intercalated mudstone.

#### Hazelton Group Stratigraphy

#### Unit 1: Lower Hazelton Group sedimentary strata

Basal Hazelton Group typically consists of locally fossiliferous conglomerate, sandstone, and siltstone which overlie Stuhini Group rocks along a disconformity or angular unconformity. This basal clastic sequence varies from a few tens to a few hundreds of meters in thickness except in the western lskut area (Johnny Mountain section) where it is absent. Unit 1 is best exposed along the Unuk River, where medium to coarse grained, medium to thickly bedded, trough cross-stratified arenitic sandstone is characteristic. Distinctive rounded clast supported granitic and volcanic cobble conglomerate form much of Unit 1 near Sulphurets Creek and are interstratified with the arenitic sandstones. Pelecypod coquinas with a calcareous sandstone matrix are common near the Bruce Glacier section, and are transitional to medium bedded silty limestone. Less common rock types include intermediate welded tuff at Bruce Glacier, and phyllitic turbiditic mudstones near Jack Glacier.

In the southern Iskut River camp near the Salmon Glacier, Alldrick (1991) describes thick siltstone intervals which may be finer grained equivalents to Unit 1 in the north. These siltstones, classified as part of the Unuk River Formation by Alldrick, contain faunal assemblages of similar age to Unit 1 assemblages near Eskay Creek (Anderson, 1993). This correlation implies that lower parts of Alldrick's Unuk River Formation are actually within the Stuhini Group, an assignment consistent with available lithologic and chronologic constraints of the area.

#### Unit 1: Age

Fossil assemblages collected from Unit 1 exposures along the Unuk River indicate a Lower Jurassic age. Well preserved ammonites *Paracalocerous* and *Badouxia Canadensis* occur in the Eskay Creek and Treaty Glacier areas, and are diagnostic of an Upper Hetangian to Lower Sinemurian age. Unconformably underlying Stuhini Group turbiditic siltstone to mudstone in this area contain Upper Norian *Monotis cf. subcircularis* bivalves, providing a maximum age for Unit 1. Upper limits are provided by Upper Pliensbachian ammonite collections from Unit 4 at Eskay Creek and John Peaks (see Unit 4 description).

Isotopic age constraints from bounding units corroborate an Early Jurassic age. Dacitic crystal tuff in the underlying Stuhini Group at John Peaks yields a U-Pb zircon age of 215-220 Ma (V. McNicoll reported in Anderson, 1993), and a granitic clast from Unit 1 in this same section has an age of about 225 Ma. A U-Pb zircon age of  $193 \pm 1$  Ma for Unit 2 flows at Johnny Mountain (M.L. Bevier, pers. comm. to P. Lewis, 1994).

#### Unit 2: Andesitic flows, breccias, and volcaniclastic rocks

Unit 2 andesitic flows, volcanic breccias, and related epiclastic rocks succeed basal Hazelton Group clastic strata in much of the Iskut River area. Lateral thickness variations are pronounced in this unit; coarse volcanic breccias for accumulations up to two kilometers thick; these localized deposits may pinch out completely in distances of less than five kilometers. Unit 2 sharply and conformably overlies Unit 1 in most locations, but near Johnny Mountain it overlies folded Stuhini Group rocks along a sharp angular unconformity.

The thickest and best preserved sections of Unit 2 are at Eskay Creek, Johnny Mountain, Treaty Creek, and Salmon Glacier. In these locations, homblende and plagioclase phyric andesitic to dacitic flows and dark green volcanic breccias are intercalated with lapilli to block tuff, and lesser amounts of epiclastic sandstone and wacke. Volcanic breccias are monolithologic to slightly polylithic, commonly contain vesicular clasts, and have a plagioclase rich volcanic matrix. At Salmon Glacier, two distinct members are differentiable: a lower porphyritic andesitic volcanic breccia to block tuff (Unuk River formation of Alldrick, 1991), separated by plagioclase-homblende-potassium feldspar megacrystic flows or sills from an upper, maroon, well bedded epiclastic conglomerate to sandstone member (Betty Creek Formation of Alldrick, 1991).

#### Unit 2: Age

The age of Unit 2 is constrained by fossil collections from bounding units, and by isotopic age determination of volcanic flows at Johnny Mountain. An older age of Upper Hettangian to Lower Sinemurian is provided by fossil collections from underlying Unit 1 (described above). Strata overlying Unit 2 contain Upper Pliensbachian ammonites at Eskay Creek and near John Peaks (see Unit 4 description), bracketing the age of Unit 2 to Sinemurian or Pliensbachian. U-Pb zircon ages at Johnny Mountain corroborate this timing. Plagioclase phyric dikes cutting Unit 2 have a zircon U-Pb age of 192  $\pm$  3 Ma, while samples of Unit 2 flows yield U-Pb zircon ages of 193  $\pm$  1 Ma. Overlying felsic tuffs provide a further bracketing constraint of 194  $\pm$  3 Ma (M.L.Bevier, pers. comm., to P. Lewis, 1994).

#### Unit 3: Felsic pyroclastic rocks and rhyolite flows

Stratigraphic correlations above Unit 2 have traditionally been more problematic than in older rocks, leading to contradictory and confusing application of existing nomenclature. A common approach to lithologic mapping in the Iskut River area has been to use a felsic pyroclastic unit overlying Unit 2 volcanic rocks as a marker. This method has resulted in inconsistencies in the assigned stratigraphic position and ages of both the datum felsic unit and bounding units, a problem which was partially resolved by the recent recognition that felsic volcanic rock occur at more than one stratigraphic level (Anderson, 1993: Lewis et al., 1993). Still, assigning a particular felsic volcanic succession to one of these two units on the basis of lithological characteristics alone is difficult, making geochronological and biochronologic age control particularly useful.

Present geological constraints indicate that the oldest rocks overlying Unit 2 consist of regionally discontinuous felsic flows and pyroclastic rocks (Unit 3) which are common in the southern and western portion of the Iskut River area (Johnny Mountain), but are thin to nonexistent in the northeast. Twenty kilometers west-northwest of Salmon Glacier near Granduc Mountain, Unit 3 comprises a megaclastic breccia and laterally equivalent lapilli tuff which overlies bedded crystal to dust tuff and volcanic conglomerate. To the north, water lain crystal and ash tuffs just south of John Peaks, and multiple thin cooling units of crystal rich welded lapilli tuff at Treaty Creek are likely equivalents. Possible vent areas for eastern Unit 3 rocks at Brucejack Lake (Sulphurets area) comprise massive, flow banded dacite domes which grade outward into autobreccia and massive, hematitic mud matrix volcanic breccia (Macdonald ref), and potassium feldspar megacrystic flows and welded lapilli tuff which overlie the lower Hazelton andesite-dacite sequence form Unit 3.

#### Unit 3: Age

Numerous new U-Pb ages indicate that the early pulse of felsic volcanism in the Hazelton Group near Iskut River spanned a 5-10 million year period. The oldest age of 194  $\pm$  3 Ma was obtained from flow rocks interlayered with lapilli tuff at Johnny Mountain (M.L. Bevier, pers. comm., to P. Lewis, 1994). This section also has the most felsic rocks included in Unit 3. Zircon extracted from bedded ash tuffs at John Peaks yielded a slightly younger U-Pb age of 190  $\pm$  1 Ma (R. Anderson, pers. comm., to P Lewis, 1994). Several other Unit 3 isotopic ages fall within the 185-188 Ma range. Vent related dacite at Brucejack Lake yield U-Pb ages of 185.6  $\pm$  1.0 Ma and 185.8  $\pm$  1 Ma. Laterally equivalent potassium feldspar megacrystic dacite flows yield overlapping ages of 187.7 + 5.8/-1.5 Ma. Welded tuff at Treaty Creek has an age of 183-185 Ma (R.G. Anderson, pers. comm). In the Granduc Mountain area, the dacite breccia is nearly identical in age to Brucejack samples at 186.6  $\pm$  15.6 Ma.

# Unit 4: Upper sedimentary sequence

Heterogeneous sedimentary strata including sandstone, conglomerate, turbiditic siltstone, and limestone characterize Unit 4. Many of the rock types of Unit 1 are present in Unit 4, but the occurrence of clasts derived from Unit 2 volcanic rocks, and the absence of the distinctive granitic clast conglomerate serve to differentiate the two units. In areas lacking strata of Units 2 and 3, such as near the Bruce Glacier, the division between Units 1 and 4 is difficult to establish and often must be defined on the basis of local stratigraphic characteristics.

Unit 4 varies from a few meters to several hundreds of meters thick. Thickest measured sections are present at Treaty Creek, and at Eskay Creek, while at Johnny Mountain the unit is nonexistent. The most distinctive rock type within Unit 4 consists of rusty brown to tan weathering, bioclastic sandstone and intercalated siltstone or argillite. At Salmon Glacier, this lithology forms a layer 2-3 meter thick, and represents the total thickness of Unit 4. To the north at Treaty Ridge, the bioclastic unit is succeeded by a several hundred meter thick turbiditic mudstone to sandstone section. Bioclastic sandstones are also present in Unit 4 at Eskay Creek and John Peaks, where they are interstratified with siltstone, arenitic sandstone, and heterolithic rounded cobble conglomerate. West of these areas, a thick, grey weathering, medium bedded limestone and siltstone sequence is a probable stratigraphic equivalent to Unit 4.

#### Unit 4: Age

Abundant and diverse fauna within Unit 4 which span Late Pliensbachian to Late Aalenian stages suggest that the unit records a long period of volcanic quiescence (Nadaraju, 1993). Late

Pliensbachian ammonite collections provide age constraints at three locations: at Eskay Creek, bioclastic sandstones contain ammonites *Tiltonicerous* cf. *propinquum* and *Protogrammoceras*; a lithologically similar section at John Peaks and interstatified limestone and siltstone sections to the west at Lyons Creek both yield the Kunae Zone (Upper Pliensbachian) ammonite *Arieticeras* cf *algovianum*; at Treaty Creek the base of Unit 4 is slightly younger where diverse faunal collections from the bioclastic sandstone includes Toarcian belemnites. Higher in this same section, ammonites, *Tmetoceras* cf. *Kirki, Leioceras*, and *Pseudoliocerous* constrain an Upper Aalenian age for turbiditic mudstone and siltstone. Together, these fossil occurrences suggest that Unit 4 sedimentation spans the Upper Pliensbachian, the Toarcian, and most of the Aalenian stages, although no single section includes fauna diagnostic of all three stages. Isotopic ages in the Iskut River area are consistent with a magmatic gap in this time period. Clusters of ages at around 185 Ma and 177 Ma are associated with Unit 3 and Unit 5 volcanism respectively.

#### Unit 5: Bimodal volcanic unit

The upper part of the Hazelton Group in the Iskut River camp comprises dacitic to rhyolitic flows and tuffs, localized interlayered basaltic flows, and intercalated volcaniclastic intervals. Although these different rock types can easily be mapped separately in a property scale, their interfingering nature and lack of continuity dictate that they be grouped into a single unit for regional mapping purposes. This part of the Hazelton Group has attracted the most attention of geologists due to its association with mineralization at Eskay Creek, but at the same time its distribution, internal stratigraphy, and age are poorly understood. Previous workers have mapped felsic volcanic components as a distinct facies of the Salmon River Formation. These assignments become problematic with new work which demonstrates that locally more than one horizon exists, and that mafic volcanic rocks occur both above and below these felsic intervals.

In most locations Unit 5 conformably succeeds Unit 4 sedimentary strata. Condensed sections on the northern part of the McTagg anticlinorium feature disconformable relationships between Unit 5 and Unit 1. Unit 5 felsic volcanic rocks are ubiquitous in the northern Iskut River area. Most sections feature a single layer of felsic strata which vary in thickness from a few tens of meters to a few hundred meters. Lithofacies within the felsic intervals are highly variable both regionally, and vertically in a given section. Deposits proximal to extrusive centers include banded flows, massive domes with carapace breccias, autoclastic megabreccias, and block tuffs. Extrusive centers have been identified at several locations in the Iskut River area, including Eskay Creek, Brucejack Lake, and Bruce Glacier. These felsic extrusive centers are characterized by thick, dome shaped porphyritic centers, grading outward to flow breccias and talus piles. Slightly to densely welded lapilli to ash tuffs characterize more distal equivalents. Reworked tuffs locally form thick epiclastic accumulations, and may fill in paleobasins adjacent to extrusive centers. At

Salmon Glacier, Unit 5 comprises well stratified, variably welded dacitic ash and lapilli tuff which forms the type section of the Mount Dilworth Formation (Alldrick, 1991). Overlying thinly interbedded turbiditic siltstone/argillite and tuff form distinctive black and white striped strata ("pajama beds") at Salmon River, and to a lesser extent, in northern parts of the area. At Troy ridge, this is the only rock type present in Unit 5.

Mafic components of Unit 5 are more localized in their distribution and are missing from much of the Iskut River camp. Generally they occur above the felsic volcanic rocks, but at Treaty Creek thick sections of mafic flows and breccias lie below felsic welded tuffs. Mafic sections are thickest at Mount Shirley and near the mouth of Sulphurets Creek, and form intermediate thicknesses at Eskay Creek and Johnny Mountain. Rocks present include massive flows, pillowed flows, broken pillow breccias, and volcanic breccias. Plagioclase phenocrysts up to two centimeters long are characteristic of the pillowed sequence south of John Peaks. At Treaty Glacier the mafic component grades upward from pillowed and massive flows into broken pillow breccia, and finally, hyaloclastite matrix supporting abundant irregular globular volcanic fragments.

#### Unit 5: Age

Flows across the Unuk River from Eskay Creek, near the Bruce Glacier, yielded an age of 176.2  $\pm$  2.2 Ma. Faunal assemblages from strata underlying Unit 5 are as young as Late Aalenian (Treaty Creek). At Eskay Creek fossil control is available within Unit 5 itself: radiolarians removed from the mineralized "contact" argillite. which occurs between the felsic and mafic volcanic intervals constrain an Aalenian age. Numerous Bajocian fossil collections from sedimentary successions overlying Unit 5 constrain the youngest biostratigraphic age for the unit.

#### **Bowser Lake Group**

The Middle and Upper Jurassic Bowser Lake Group contain the youngest Mesozoic strata in the claim area. In general, the Bowser Lake Group consists of a thick succession of shale and silty mudstones, with local buff sandstone interbeds, lesser amounts of interbedded chert rich conglomerate and conglomerate. It conformably or paraconformably overlies Hazelton Group rocks. In many areas the boundary between Bowser Lake and Hazelton rocks is unclear and is not defined.

Rich faunal collections from Bowser Lake Group turbiditic mudstones in the Prout Plateau define a Bathonian to Callovian age for lowest exposed stratigraphic levels (G. Nadaraju, personal communication to P. Lewis, 1992). Outside of the Iskut River map area, Kimmeridgian faunas are characteristic of higher stratigraphic levels.

Bowser Lake Group strata in the northern part of the claim area consists primarily of highly deformed turbiditic wackes and slates, and subordinate conglomerate and sandstone. These are distinctly different from typical Bowser Lake Group strata and appear to represent a separate subterrane of greenshist facies grade metamorphosed turbidites. New information on this and the Bowser Lake Group comprises much of volume one of this report.

# **Intrusive Rocks**

Anderson (1989, 1993) suggests that Triassic and Jurassic intrusive activity in the Iskut River area can be divided into 5 cycles. He defines four distinct plutonic suites, three of which he relates to cospatial and coeval volcanic suites. Plutonic rocks other than mafic dikes intrude Jurassic Hazelton Group or Bowser Lake Group strata. With the exception of the feldspar porphyry unit at Eskay Creek (U-Pb zircon age of  $186 \pm 2$  Ma, Macdonald et al., 1992; Ghosh, 1992), reliable radiometric ages for plutons are lacking in the area. Undated plutons are assumed, on the basis of intrusive relationships and composition, to be members of the Jurassic Texas Creek or Three Sisters plutonic suites (Anderson and Bevier, 1990), with extrusive equivalents within the Hazelton Group.

## **Project Area 5**

#### **Location and Claims**

Project Area 5 is the Fred grid which is located on Fred 15 and the Pmac claims. It is located on NTS map area 104B/10, approximately 9 kilometers southwest of the Eskay Creek mine. The area lies between 405,000 to 406,000 E and 6,272,000 to 6,274,200 N. The geology was mapped at 1:1000 and is shown on Maps 12 and 13.

#### **Previous Work**

Prospecting, and rock and soil sampling was done in 1989 on Fred 16 and Dup 8 (Hopper, 1989b). The ground was restaked as Fred 15, some of the Pmac claims and Noot 3. A number of areas with very weak sericitic alteration and minor disseminated pyrite were observed. A grab sample, apparently from Pmac 3 assayed 33 grams per tonne Au and 1610 grams per tonne Ag.

A single hole was drilled on the Fred 15 claim on the North Coulter property in 1990 (Verzosa, 1990). However, the drilling was done prior to abandoning and restaking of the claims. Therefore, the position of land staked as Fred 15 changed. The drill hole reported in 1990 is located south of the SIB claim block. It is not on the claim currently called Fred 15, nor is it on any claims reported on in this report.

In 1995, Canamera Geological Ltd. chained and flagged in a grid over the Pmac claims and the western portion of Fred 15. Detailed mapping, soil sampling and prospecting were done on this grid to follow up on an anomalous boulder sample. This resulted in multiple rock samples returning values over 1 gram gold per tonne along with other elevated samples (Bridge and Burroughs, 1995).

#### Grid Cutting

For the 1996 program a new grid was cut and tight chained by MFH Contracting. The grid consists of approximately 17.6 kilometers of cutline including the baseline. The baseline is two kilometers long with crosslines every 100 meters. The azimuth of the baseline is 355°. The stations were located by an in-house survey, and the grid was tied into topographical features. The grid was surveyed to supply the necessary accuracy for proper interpretation of the UTEM geophysical program. A result of the survey is that the grid station labeling does not match the surveyed map coordinates due to the high topographical relief contrast. Therefore, the tight chained 25 meter stations are less than 25 meters in actual horizontal distance.

#### **General Geology**

Area 5 contains a section of Hazelton Group Unit 5 rocks and is very close to the overlying sedimentary rocks of the Bowser Lake Group in the area of Tom Mackay Lake. The structural position of Area 5 is unclear. It is west of the west limb of the gently northeasterly plunging Eskay Creek anticline and west of the strike extension of the Mackay syncline. It contains mainly subhorizontal to gently dipping strata, so may lie along the axis of the Mackay syncline or may be less affected by major isoclinal folding than the region immediately north and northeast. Poorly constrained fold structures are difficult or impossible to map because of a lack of stratigraphic markers, early northeasterly to east-northeasterly faults, west verging thrust faults and later northerly oriented faults.

Area 5 is directly overlain to the north by Bowser Lake Group rocks so mainly contains upper Hazelton Group stratigraphy. Bowser Lake Group rocks occur in the east portion of Area 5 are in fault contact with Hazelton Group rocks. Bartsch (1993b) interprets the area to be upper Hazelton Group and essentially at the same stratigraphic level as the Eskay Creek deposit. However, he interprets the volcanic facies to be polymodal, distal facies rather than proximal vent facies as at Eskay Creek. Sedimentary rocks are shallow marine argillite facies as at Eskay Creek. This is consistent with the mapping by Canamera.

However, it can be very difficult to distinguish proximal facies from distal facies in the Hazelton Group volcanic rocks. Initial literature on the Eskay deposit emphasized rhyolitic breccia and tuffaceous textures (Blackwell, 1990) in the rhyolite at the Eskay deposit, although flow banded clasts were also mentioned (Britton et al., 1990). Only after extensive drilling and more rigorous observations did the emphasis swing to the interpretation of the classical proximal dome facies of Williams and McBirney (1979) which are described as the proximal facies at Eskay by Bartsch (1993b).

#### **Claim Geology**

A general stratigraphic lithology has been determined from the 1995 and 1996 mapping. From younger to older rocks, the sequence is; andesites to basaltic andesites, interbedded rhyolites to dacites, siltstones to mudstones with thin interbedded felsic volcanics, a second group of rhyolites to dacites, and lastly a fine pebble (grits) conglomerate.

The andesites and basaltic andesites occur as massive flows to andesitic breccias. Pillowed flows, pillow breccias and amygdalodial flows also occur. Thin interflow mudstones are common within the mafic to intermediate volcanic rocks.

The upper unit of rhyolites and dacites are massive to intensely fractured or brecciated. These commonly contain monolithic or heterolithic clasts which range from angular to rounded in shape. Flowbanding is seen primarily in the clasts but it is also seen in some of the more massive rhyolite outcrops. They appear to be distal facies rather than flow dome facies which, at the Eskay Creek Mine, has flow banding and autobrecciation. Often the rhyolites lower in this unit appear to be flows which intruded into mudstones. They have bases or margins of rhyolitic fragmental rocks to black matrix rhyolite breccias. Minor areas of rhyolitic and dacitic lapilli tuff occur. These lapilli tuffs are at the base or margins of flows. this indicates that the flows were preceded by lapilli tuffs from plinian or phreatic eruptions as were the flow domes associated with the Eskay Creek deposit. Interflow siltstones and mudstones are a part of this unit, however they are volumetrically small compared to the volcanics.

The siltstone and mudstone unit is composed of monotonous fine grained sediments which are strongly fractured into small friable pieces. This, generally, causes the unit to weather down and makes structural measurements problematic. Interbedded with the sediments are thin rhyolite and dacite flows. The rhyolite, the more common of the two, occurs as black matrix breccias with varying degrees of silica content in the matrix. The dacite flows tend to be more competent than the rhyolites but their thin width causes them to weather the same.

The lower rhyolite and dacite unit also consists of heterolithic and monolithic fragmentals. However, black matrix rhyolites are not seen and interbedded sedimentary rocks are rare compared to the upper unit. Another indication that this unit is different from the upper felsic unit is that the soil geochem over this area shows a lack in the As signature but a possible weak enrichment in Zn.

The lowest unit in the mapping area is a fine pebble conglomerate. This is seen on line 13N and 14N at approximately 5+50E. Topography and geology indicate that that the unit is part of a upthrown fault block but from what depth is unknown.

Intense block faulting and strong weathering of the siltstones does not allow easy correlation within the units or full understanding of the stratigraphy. The first three units appear continuous but the depth from which the last two units were faulted up from and their relation to the upper units is unknown.

The gold mineralization discovered in 1995 is associated with the siltstone/rhyolite unit. All of the anomalous 1995 samples came from rhyolitic boulders or outcrop. The type of rhyolitic flow

varies from massive to fragmental but in all cases they are weathering out as if sourcing from a thinner, easier eroded flows. The differing lithologies would indicate multiple mineralized horizons, all interbedded with the more abundant siltstones/mudstones. This would make the andesite/basaltic andesite unit and the upper felsic volcanic unit, which cover most of the ground from 18N to 22N, hangingwall lithologies with potential mineralization underneath them.

1996 mapping has confirmed shallow dips and erratic strikes. The block faulting has divided the area into smaller packages with most of them displaying different strikes and dips. This may be an indication of local drag folding in response to the faulting or a possible undulating stratigraphy before the faulting. In either case, relatively flat lying stratigraphy is indicated.

#### Geophysics

The focus of the 1996 work on the Fred grid was the completion of a UTEM geophysical program. SJ Geophysics Ltd. was responsible for the collection and interpretation of the data. Their report is presented in appendix 1. Overall, the survey shows weak linear anomalies which appear to correspond well with known and interpreted faults. There is also a deep seated resistivity low but there is no other geological data with which to relate it to so interpretation is vague.

#### Soil Sampling

A total of 330 soil samples were collected on the 1996 Fred grid. The majority (322) of the samples were taken on lines 21 N to 10 N at 25 meter stations. Overall, the samples returned few truly anomalous values, but the statistically anomalous and threshold results produced some general patterns.

Fred Grid	Ag	As	Ва	Bi	Cd	Co	Cu	Мо	Ni	Pb	Sb	Zn
Mean	0.5	5	50	<2	<0.5	11	21	4	14	12	2	90
Standard Deviation	0.6	8	27	<2	<0.5	6	22	2	11	16	<2	51
Threshold	1.1	14	77	2	<0.5	17	44	6	25	28	3	141
Anomalous	1.7	22	104	3	1	23	66	8	36	44	5	191
Range Maximum	5.6	74	160	4	5	42	235	24	62	262	6	462
Minimum	<0.2	<2	10	<2	<0.5	1	<1	<1	<1	<2	<2	32
# of Samples	330	330	330	330	330	330	330	330	330	330	330	330

Gold values are generally under the detection limit (< 5 ppb) but there are four samples with elevated results. These four values are single point anomalies and appear to be erratics. The 950 ppb Au sample is interesting because it occurs within the siltstone/rhyolite unit which

appears to have the highest potential for Au mineralization. However, this sample occurs in a topographic low and is a single point anomaly so it's significance is questionable.

The arsenic values range from under the detection limit (<2 ppm) to 74 ppm. The anomalous and threshold values are not high enough to indicate mineralization but the concentration of these samples from line 17 to 21 N roughly outline the area of the upper felsic volcanic and the siltstone/rhyolite units which is the main units of interest.

Along the eastern edge of the grid, a trend of anomalous and threshold nickel values are seen. These occur on the eastern side of the major topographic break that runs along the western shore of Pmac and Barb Lakes. The rocks underlying this area are of a different stratigraphic level than the rest of the grid so the nickel values are an indication of the change in geology.

A weak trend of copper is present from 7+00 E, 13+00N to 10+50E, 16+00N. This is along the slope of the major topographic break and may indicate the exposure of, or access to, a different geological unit caused by a structure responsible for the break.

Statistically high zinc values are seen all over the grid, with a concentration on the western side between 16+00N and 19+00N. Again, these values appear to be indicating a change in geology and not mineralization as this area is underlain by dacite/rhyolite volcanic rocks with minor sedimentary rocks, not the felsic volcanic/mudstone/siltstone/epiclastic rocks as occur under the As anomaly.

Eight of the 1996 samples were taken as infill around the 1995 anomalous result of 90 ppb Au. These did not return any significant results so the 1995 sample can be confirmed as an erratic point anomaly.

#### Interpretation and Recommendations

The Fred 15 area has Au-Ag mineralization in massive to brecciated rhyolites. The mineralization occurs in multiple horizons within the siltstone/mudstone dominated unit. The mineralization is exposed in small erosional windows through overlying rhyolite, dacite and andesite flows. The 1996 mapping and prospecting did not indicate any new mineralized horizons within any of the other stratigraphic units so. Thus, for the majority of the claims, the rock unit of highest potential is still buried.

Geophysics did not define a strong conductor within the property. It did outline weak linear anomalies, interpreted as fault structures, and a deep resistivity low which can not be correlated with any other data.

Alteration ranges from absent to very weak silicification. This may indicate that the mineralization is distal to volcanic centers. The absence of gossanous bluffs and altered dacitic rocks, characteristic of the footwall to the favourable horizon, may indicate that favourable stratigraphy occurs lower in the section and has not been removed by erosion.

Soil geochem is useful in indicating general stratigraphy but it has not helped in narrowing the search for mineralization. Evidence from the soil results and geological mapping are used to define a second unit of felsic volcanics.

Stratigraphic drilling is the only step left with which to advance the understanding of the geology of these claims. Multiple holes should be drilled to confirm the stratigraphy, locate the exact position of the mineralized horizons, and locate new mineralized horizons that may be associated with those seen on surface. The examination of unweathered mineralized and footwall rocks would enable assessment for the potential for massive sulphides on these claims.

### Statement of Qualifications

I, Simon J. Haynes, of Box 397, Fonthill, Ontario, LOS 1E0, certify that:

I was commissioned as a consultant geologist by Canamera Geological Ltd., of 540-220 Cambie Street, Vancouver, B.C., to conduct a field geological program on claims described in the accompanying report.

I am a graduate of: Manchester University, Manchester, U.K., with a Bachelor of Science (Honours) in Geology, 1965; Carleton University, Ottawa, Ontario, with a Master of Science in Geology, 1969, and; Queen's University, Kingston, Ontario, with a Doctor of Philosophy in Geology, 1975.

I have practiced my profession continuously since graduation with a B.Sc.

i am a fellow of:

Geological Association of Canada Society of Economic Geologists

#### I am a member of:

Canadian Institute of Mining and Metallurgy Association of Geoscientists of Ontario

I am a recipient of the following professional society awards:

Honour Award, Geological Society of Cuba; Santiago, Cuba, 1994

Honour Award, Hunan Geological Society; Shuikoushan, China, 1988

Certificate of Appreciation, Northwest Mining Association, Spokane, Washington, U.S.A., 1986 Certificate of Appreciation, Philippine Institute of Mining and Metallurgy, Bagulo, Philippines, 1986

This report is based on personal observations, field mapping, photogeology, and thin-section petrography during the period August 12th to August 29th and September 14, 1996.

I have no interest, either direct or indirect, with Tagish Joint Venture, Canamera Geological Ltd., or their partners, nor do I expect to acquire any interests.

I grant permission to Canamera Geological Ltd. to use this report.

October 10, 1996

Simon Haynes, Ph.D.

# Statement of Qualifications

I, Dane A. Bridge, of 16 Massey Place SW, Calgary, Alberta, T2V 2G3, certify that:

I was commissioned as a contract geologist by Canamera Geological Ltd., 540-220 Cambie Street, Vancouver, BC, to conduct a field program on claims held by Tagish Resources and Alex H. Briden, as outlined in the accompanying report.

I am a graduate of the University of Manitoba, Winnipeg, Manitoba, with a Bachelor of Science (Honours) in Geology, 1969, and a Master of Science in Geology, 1972.

I have practiced my profession continuously since graduation.

I am a registered professional geologist in Alberta, APEGGA number 057688, and I am a member of:

Canadian Institute of Mining Geological Association of Canada Society of Economic Geologists

This report is based on personal observations and field mapping during the periods August 25th to August 27th and September 9th to September 14th, 1996.

I have no interest, either direct or indirect, in Tagish Resources or its partners, nor do I expect to acquire any interests.

I grant permission to Tagish Resources and Canamera Geological Ltd. to use this report.

November 20, 1996

Dane Bridge, P. Geol.

Statement of Qualifications

I, Greg R. Burroughs, of 6B-4141 Oak Street, Vancouver, British Columbia, V6H 2N1, certify that:

I was commissioned as a geologist by Canamera Geological Ltd., 540-220 Cambie Street, Vancouver, BC, to conduct a field program on claims held by Tagish Resources and Alex H. Briden, as outlined in the accompanying report.

I am a graduate of the University of Saskatchewan, Saskatoon, Saskatchewan, with a Bachelor of Science (Advanced) in Geology, 1990.

I have practiced my profession continuously since graduation.

This report is based on personal observations and field mapping during the periods August 11 to September 14th, 1995.

I have no interest, either direct or indirect, in Tagish Resources or its partners, nor do I expect to acquire any interests.

I grant permission to Tagish Resources and Canamera Geological Ltd. to use this report.

November 20, 1996

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Greg Burroughs

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Appendix 1

# **UTEM SURVEY**

ON THE

# FRED 15 CREEK PROJECT ISKUT AREA, B.C., SNIPPAKER CREEK

LIARD MINING DIVISION B.C., N.T.S. 104B/10E

FOR

# CANAMERA GEOLOGICAL LTD..

SURVEY BY

SJ GEOPHYSICS LTD.

AND ·

LAMONTAGNE GEOPHYSICS LTD.

November 1996

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REPORT BY Syd Visser S.J.V. Consultants Ltd.

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### **INTRODUCTION**

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A large loop time domain electromagnetic (UTEM-3) survey was completed by SJ Geophysics Ltd. and Lamontagne Geophysics Ltd. for Canamera Geological Ltd. on the Fred 15 Creek Project during the period of September 3 to September 19, 1996. The Fred 15 Creek Project is located approximately 300 Km north of Smithers near Snippaker Creek and the border of the Liard and Skeena M.D., of B.C. (N.T.S. 104B/10e). Access is via highway 37, north of Smithers, to Bob Quinn Lake and then by the private Eskay Creek Mine road to the camp. Access from the camp to the property is via helicopter

The purposes of the survey were to search for flat lying conductive massive sulphides and to aid in the mapping of local geology.

This report is meant to be an addendum to a main property report by Canamera Geological Ltd. which will describe local geology, previous work and provide location maps.

### **DESCRIPTION OF UTEM SYSTEM**

UTEM is an acronym for "University of Toronto ElectroMagnetometer". The system was developed by Dr. Y. Lamontagne (1975) while he was a graduate student of the university.

The following is a short description of the UTEM system used in the field. A paper (A time-domain EM system measuring the step response of the ground) by G.F. West, J.C. Macnae and Y. Lamontagne, giving a more complete description with an overview of interpretations is located in Appendix III.

The field procedure involves laying out a large loop, which can vary in size from less than 100M X 100M to more than 2Km X 2Km, of single strand insulated wire and energizing it with current from a transmitter which is powered by a 2.2 kW motor generator. During a surface survey the lines are generally oriented perpendicular to one side of the loop and surveying can be performed both inside and outside the loop. For a borehole survey the sensor coil is placed down the borehole to measure the axial component of the electromagnetic field from a minimum of 2 separate loops.

The transmitter loop is energized with a precise triangular current waveform at a carefully controlled frequency (30.97 Hz for this survey). The receiver system

includes a sensor coil and backpack portable receiver module, which has a digital recording facility. The time synchronization between transmitter and receiver is achieved through quartz crystal clocks in both units which are accurate to about one second in 50 years.

The receiver sensor coil measures the vertical horizontal, or axial magnetic, component of the electromagnetic field and responds to its time derivative. Since the transmitter current waveform is triangular, the receiver coil will sense a perfect square wave in the absence of geologic conductors. Deviations from a perfect square wave are caused by electrical conductors which may be geologic or cultural in origin. The receiver stacks any pre-set number of cycles in order to increase the signal to noise ratio.

The UTEM receiver gathers and records 10 channels of data at each station occupied. The higher number channels (7-8-9-10) correspond to short time or high frequency while the lower number channels (1-2-3) correspond to long time or low frequency. Poor or weak conductors will respond on channels 10, 9, 8, 7 and 6. Progressively better conductors will give responses on progressively lower number channels as well. For example, massive, highly conducting sulfides or graphite will produce a response on all ten channels.

The Borehole system consists of a normal surface UTEM-3 transmitter and receives along with special receiver coil ( $1 \frac{1}{4}$ " in diameter). The coil is connected to the receiver through a controller and fibre optic cable.

## **FIELD WORK**

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John Ashenhurst (Technologist) and David Reip, (helper from Whitehorse) both with SJ Geophysics Ltd,. and , the equipment were mobilized from Whitehorse by truck on September 3, 1996. John and the equipment returned to Vancouver on September 19, 1996. The survey area was accessed daily by helicopter from accommodations on the Eskay Creek Mine road. The field parameters and local geology were discussed with the Canamera Geologist before commencing the survey and during the survey period.

Approximately 14 Km, using a station spacing of 25m, were surveyed from 1 loop in a period of 9 data collection days 2.5 loop laying days, 1 standby day and 3 mobilization days.

The grid is comprised of cut and surveyed lines in fairly rough terrain, therefore, channel 1 should be accurate if the location of the loop was recorded accurately. The survey data was supplied by the client and applied to produce a topographic map and aid in reduction of the data.

### **DATA PRESENTATION**

The results of the UTEM survey are presented on 42 data sections (Appendix IV) and one compilation map, Plate G1.

Legends for the UTEM data sections are also attached (Appendix II).

In order to reduce the field data, the theoretical primary field of the loop must be computed at each station. The normalization of the data is a follows:

a) For Channel 1:

% Ch.1 anomaly = (Ch.1 - PC)  $X \frac{100}{PT}$ 

Where:

PC is the calculated primary field in the direction of the component from the loop at the occupied station

Ch.1 is the observed amplitude of Channel 1

PT is the calculated total field

b) For remaining channels (n = 2 to 9)

% Ch.n anomaly =  $(Ch.n - Ch.1) \times 100/Ni$ 

where:

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Ch.n is the observed amplitude of Channel n (2 to 9)

- N is Ch1 for Ch1 normalized
- N is PT for primary field normalized
- I is the data station for continuous normalized (each reading normalized by different primary field)
- I is the station below the arrow on the data sections for point normalized (each reading normalized by the same primary field)

Subtracting channel 1 (Ch.1) from the remaining channels eliminates the topographic errors from all the data except channel 1.

If there is a response in channel 1 from a conductor, this value must be added to do a proper conductivity determination from the decay curves. Channel 1 should not be subtracted indiscriminately.

The data from each line is plotted on at least 2 separate sections consisting of a continuous normalized section and a point normalized section. Additional point normalized data sections were produced where more than one conductor is present on the same line. Point normalization data is the absolute secondary field at a "gain setting" related to the normalization point. The data is usually point normalize over the central part of the crossover anomaly to aid in interpretation.

### DISCUSSION

The survey which was conducted inside a large loop was designed to locate flat lying conductors at depth with a size smaller than the loop or with at least one edge within the loop. The loop location was largely determined by the topography. The survey indicated a structure striking across the survey area as shown on the compilation map G1. The rocks appear to be somewhat less resistive on the eastern edge of this structure.

The data indicates there is some deep-seated low resistivity feature. This low resistivity unit which is likely a sedimentary package is located between approximately 300m and 1000m. If it is of interest, it may be possible to do additional processing of this data to determine a more accurate depth to top and depth extent of this feature. The large size of the transmitter loop would make it difficult to locally invert the data.

Geo

## **APPENDIX I**

### STATEMENT OF QUALIFICATIONS

I, Syd J. Visser, of 11762 - 94th Avenue, Delta, British Columbia, hereby certify that,

- 1) I am a graduate from the University of British Columbia, 1981, where I obtained a B.Sc. (Hon.) Degree in Geology and Geophysics.
- 2) I am a graduate from Haileybury School of Mines, 1971.
- 3) I have been engaged in mining exploration since 1968.

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4) I am a professional Geoscientist registered in British Columbia.

Syd J. Visser, B.Sc., P.Geo Geophysicist/Geologist

# **APPENDIX II**

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## Legend

UTEM SYSTEM MEAN DELAY TIME		
Channel Number	Delay Time(msec)	Symbol
1	12.8	1
2	6.4	
3	3.2	2
4	1.6	
5	0.8	Z
6	0.4	$\leq$
7	0.2	7
8	0.1	×
9	0.05	
10	0.025	$\diamond$
Base Frequency = 31 Hz		

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# **APPENDIX III**

A time domain EM system measuring

the step response of the ground

### A time-domain EM system measuring the step response of the ground

G. F. West\*, J. C. Macnae\*‡, and Y. Lamontagne‡

#### ABSTRACT

A wide-band time-domain EM system, known as UTEM, which uses a large fixed transmitter and a moving receiver has been developed and used extensively in a variety of geologic environments. The essential characteristics that distinguish it from other systems are that its system function closely approximates a stepfunction response measurement and that it can measure both electric and magnetic fields. Measurement of step rather than impulse response simplifies interpretation of data amplitudes, and improves the detection of good conductors in the presence of poorer ones. Measurement of electric fields provides information about lateral conductivity contrasts somewhat similar to that obtained by the gradient array resistivity method.

#### INTRODUCTION

This article describes the design of the UTEM system and its development at the Geophysics Laboratory of the University of Toronto by Y. Lamontagne and G. F. West from 1971 to 1979. UTEM is a wideband, time-domain, ground EM system with a step-function system response. It was designed to try to achieve the sensitivity and interpretability necessary to handle problems of deep exploration, conductive environments, and a variety of terrain conditions, in an economically viable manner. As with most EM systems, effective exploration for massive sulfide ores was the principal objective. The method was conceived in 1971, and the first UTEM I instrument was operational in 1972. It was an analog electronic system, and was used in a number of surveys which have been described by Lamontagne (1975). An improved UTEM II which incorporated a digital recording system was then designed and constructed at the University of Toronto with financial aid from a consortium of mining companies. It was first used in 1976. To fall 1980, about 1000 line-km had been surveyed with the system from 144 loops in 35 areas. UTEM III, which is a microprocessor-controlled system with expanded capabilities, is now produced commercially by Lamontagne Geophysics Ltd. Some of the field results obtained using the UTEM II system have been described in Lamontagne et al. (1977, 1980), Macnae (1977, 1980, 1981). Lodha (1977), and Podolsky and Slankis (1979). Data from all three UTEM systems are identical insofar as geophysical characteristics are concerned. The differences affect only data noise levels and operational convenience. Some of the noise rejection features of UTEM III are discussed by Macnae et al. (1984).

#### THE UTEM SYSTEM

#### Design philosophy

UTEM uses a large, fixed, horizontal transmitter loop as its source. The field of the loop is mapped in the quasi-static zone with the receiver system; the vertical component of the magnetic field is always measured, and in some circumstances the horizontal magnetic and electric field components may be measured as well (Figure 1). The size of the transmitter loop depends on the prospecting problem; loops may range from about 2 km  $\times$  1 km in resistive terrain to 300 m  $\times$  300 m in a conductive area. Lines are typically surveyed to a distance of 1.5 to 2 times the loop dimensions.

The large loop transmitter-field mapping receiver configuration was chosen in order to give the system the deepest possible exploration for orebody sized conductors, without sacrificing the ability to resolve shallower structures (depth < 50 m). This dictates a very large transmitter moment, and makes an extended source desirable. The virtue of an extended source is that the coupling between the source and a receiver or the source and a nearby conductive zone is not so many orders of magnitude larger than the coupling to a distant receiver or deep target as is the case with a confined source.



FIG. 1. Schematic layout of a UTEM survey.

Manuscript received by the Editor November 1983; revised manuscript received December 1983. "Geophysics Lab., Dept. of Physics, Univ. of Toronto, Ont., Canada M5S 1A7. ‡Lamontagne Geophysics, 740 Spadina Ave., Toronto, Ont., Canada M5S 2J2. © 1984 Society of Exploration Geophysicists. All rights reserved.



FIG. 2. Transmitted and received UTEM waveforms. Note that the measurement channels are numbered from the latest to the earliest. Sampling is repeated, with due regard to sign, in every half-cycle.

Given a large transmitter and a large Tx-Rx separation, it is inevitable that induction in extensive conductive overburden and in large formational conductors will contribute more to the response than with a small scale system. Also, as the separation becomes larger it becomes increasingly likely that the system will be responding to several nearby conductors at once. However, a fixed transmitter-moving receiver system offers a basis for separating the signal contributions from the various conductors and resolving the geometry of deep-seated conductors. At any time instant, the magnetic field of the current system induced in the ground is a potential field (within the quasistatic zone), and if it is mapped on a profile or over a surface, there is a firm theoretical basis for separating it into parts and estimating the current systems which caused it. When the transmitter and hence the eddy current system move for each observation, it is more difficult to find a theoretical basis for stripping of responses into component parts.

There are negative aspects to using a fixed transmitter method. In addition to the aforementioned enhancement of anomalies due to formational conductors, the transmitter can be positioned badly for induction in small plate-like conductors, and a large good conductor can screen a smaller, shorter time-constant conductor which lies behind it. For these reasons it may be desirable to have survey coverage from more than one transmitter location.

The UTEM II transmitter passes a low-frequency current of precise triangular waveform through the transmitter loop. The magnetic field is sensed with a coil, which responds to the time

**k** 2



FIG. 3. Comparison of transient signals in step and pulse type systems.

derivative of the local magnetic field, so in "free space" a precise square-wave voltage would be induced in the receiver. In the presence of conductors the waveform is substantially distorted. The UTEM receiver measures this distortion by determining amplitudes at 10 delay times (actually, averages over time windows) which are spaced in a binary geometric progression between the waveform transitions. The sample scheme is shown in Figure 2. Note that the UTEM channel numbers are conventionally numbered in reverse order of time. This is because the latest time measurement often serves as a reference to which the other measurements are compared, whereas the number of earlier time measurements which can be made accurately may change if base period or instrument bandwidth is altered. The base frequency of the system is selectable, usually about 30 or 15 Hz (25 or 12.5 Hz in countries with 50 Hz power). A common practice is to set the base frequency (adjustable in 0.1 percent steps) about 0.5 Hz from a subharmonic of the power line in order that power line interference can be detected by slow beating in the data. The base frequency is usually set low enough that all ground response has nearly vanished by the end of the half-cycle. When this is the case, the UTEM system determines the step response of the ground in the time range  $25\mu$ s to 12.8 ms (30 Hz base frequency).

#### Time-domain systems

Time-domain systems have some advantage over frequencydomain systems in that simultaneous measurement is easier to achieve over the whole spectrum and, at the same time, it is possible to check the phase synchronization of the transmitter and receiver time bases. Most time-domain systems employ an on-off type of transmitter current and confine all measurements to the off period, as this automatically separates the secondary from the primary field. However, when a coil is used as a sensor, the time derivative of the signal is observed. Thus, if the transmitter loop is energized with a step current, it is the impulse response of the ground which is observed.

When prospecting for conductive mineral deposits, it is generally more desirable for interpretation purposes to observe the step response than any other time response. The reason for this lies in the characteristics of eddy current decay. For the step time. A small component of response appears to have persisted to Ch I and, for quantitative analysis, it should be remembered that the data reduction process will have caused subtraction of this amount from profiles of Ch 2-Chn. On the early-time channels, the migration of crossover location from one channel to another indicates that the secondary current flow at these times is not fixed in geometry, a characteristic which is indicative of an extensive conductor (here extensive overburden) rather than a localized conductor such as that responsible for the late time crossovers.

Since at any delay time, the secondary field is a potential field, interpretation of geometrically fixed current systems is best performed using absolute secondary fields normalized by the primary field intensity at a single point rather than continuously along the profile. Although only one case presented in this paper has this absolute or "point normalization," recent routine field practice is to point normalize all survey profiles exhibiting discrete anomalies, in order to simplify interpretation.

Horizontal magnetic field measurements may be made by

reorienting the receiver coil. Normalization is done using the vertical primary magnetic field (calculated or vertical Ch 1 measurement). Unfortunately, horizontal field measurements frequently suffer a somewhat higher noise level than vertical fields, due to the predominantly horizontal orientation of sferic interference.

The electric field waveform is, like the voltage from the coil sensor, a square wave if the ground is very resistive. It is distorted in much the same way as the coil signal when the ground is conductive. Electric field observations are usually plotted as  $E_i/E_T^{p}$ —the observed channel voltage between the electrodes divided by the maximum expected late time voltage between electrodes at the observation point in any horizontal direction, i.e.,  $E_T^{p} = (E_x^{p2} + E_y^{p2})^{1/2}$ . "Expected" here refers to the electric field produced by a loop on a laterally uniform, resistive half-space. This normalization facilitates intercomparison of x and y component data. The geologic noise level in electric field data is usually high, so plotting on expanded scales is rarely justified. All channel data are usually plotted on the same axes, as shown in Figure 5.





FIG. 5. Standard presentation of electric field data. The observed component is normalized to the total primary electric field of the transmitter loop.



Fig. 6. Vector plots of late time electric field. (a) Direction information only. (b) Showing direction and intensity of the primary field.

the position of the main current concentrations. However, the UTEM receiver is a coil which is sensitive only to dH/dt, and thus to the rate of change of induced and transmitter loop current. Thus the moving pattern of crossovers is actually indicating outward migration of *changes* in the induced current pattern. Toward the end of each half-cycle, the induced current system at any point in the survey area tends to a constant value, as indicated by the electric field measurements, but this steady current is invisible to the coil receiver.

When interpreting UTEM magnetic field data, it can often be simpler to think of the data in terms of the magnetometer receiver, square-wave transmitter current (MSW) analogy. Because the analogy is exact for a linear process like EM induction, there is no approximation in using it. It is very convenient to think of the field measurements of secondary signal at any delay time as describing the Biot-Savart magnetic field of a changing and decaying (analogous) induced current system. However, when electric field data are being analyzed and compared with magnetic field (dH/dt) data, it is necessary to revert to the true picture of the induced currents (or take a time derivative of the E data) to maintain a consistent relationship. UTEM magnetic field data are usually symbolized as  $H_{xi}^{s}$  (alphabetic subscript = component direction, superscript = p primary, s secondary, T total, numeric subscript = channel number) to accord with the magnetometer analogy; and in most discussions of simple induction, it is the time history of the analogous induced current which is described.

An important feature of layered earth  $H_z^i$  data is the earlytime limit of continuously normalized  $H_{zi}^i/H_z^o$  data. If the ground is sufficiently conductive near the surface, the early-time secondary field data at points remote from the transmitter loop will approach -200 percent; i.e., one finds that the voltage in the receiver coil has had insufficient time to change from the steady value attained at the end of the previous half-cycle (Figure 2). This situation may be pictured in the magnetometersquare wave current analogy as an induced current system forming near the surface of the ground under the transmitter loop such as prevents the total (analogous) magnetic field from entering into the ground anywhere except very close to the transmitter wire. The -200 percent anomaly thus represents response at the inductive limit.

#### Finite thin plate in free space

A convenient modeling method for thin finite plate conductors in free space is the integral equation solution of Annan (1974). Annan computed the best set of polynomial eigenpotentials of order 4, and used these to represent the induced current flow in the plate as a sum of 15 "eigencurrents." The solution for the eigencurrents themselves is quite complicated, but needs only to be done once for a plate of given width to length ratio. After that, any induced current system can be described in terms of 15 coefficients in the eigenpotential summation. The secondary field at a receiver can then be simply computed in terms of these induced eigencurrents. One great advantage of Annan's method is that each eigencurrent has a frequency or time-domain response identical to a simple loop circuit. Thus the solution for a broad frequency range or many time windows is very easy to calculate. Routines for simple, interactive application of Annan's algorithms to a number of EM systems have been programmed by Dyck (Dyck et al., 1980).

Examples of type curves generated with Annan's solution may be found in Lodha (1977) and Lamontagne et al. (1980). Figure 9 shows the results of a set of computed UTEM type curves for the geometry shown in Figure 10. Also shown in Figure 10 is the geometry of the primary magnetic field, which controls the nature of induction in the plate. For the zero din case, the primary field is mostly perpendicular to the plate. The induction in the plate tends to cancel this field at early times. leading to a negative H, anomaly directly over the plate. Positive shoulders on each side show the secondary magnetic field of the "forward (analogous) current" near the front edge of the plate nearest the loop and the "reverse current" near the rear edge. The normalization scheme used in plotting this data is to divide the total secondary field by the calculated primary field at the measuring point. It has the undesirable effect of making asymmetric a secondary anomaly that is symmetric in terms of absolute amplitude by increasing the relative amplitude away from the loop. In fact, the absolute secondary amplitude of the positive shoulder near the loop is usually larger than the one on the side away from the loop. As the dip of the plate is increased, the positive shoulder moves away, and by the time a 30-degree dip is reached the reverse crossover is off the end of the plotted line. From dips of 30 to 135 degrees, the anomaly maintains a basic shape in the form of a simple crossover. The amplitude



FIG. 8. Hz response of a thin horizontal sheet at various depths. The conductivity-thickness of the sheet is 2 S. The front of the transmitter loop is at the origin of coordinates.



SECTION VIEW OF PLATE CONDUCTORS AND PRIMARY MAGNETIC FIELD

GEOMETRY FOR 90° CASE

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FIG. 10. Geometry and dimensions of the models shown in Figure 9. Also shown is the configuration of the primary field in the vicinity of the target conductor.

a resistive half-space is caused by charge on the plate as well as eddy currents flowing in it, and is affected by the earth-air interface. Annan's algorithm does not determine the charge distribution, so analog scale modeling methods were employed to produce type profiles. Figure 11 shows an example for a vertical plate. The longitudinal electric field is greatly reduced over the body at all times (i.e., there is a strong reduction in the late time limit). The dynamic (time-varying) part of the anomaly has the same time variation as the magnetic field but has a different geometrical pattern. The electric field is highly vulnerable to distortion by any conductivity contrast and the intensity of the static, late-limit anomaly over a conductor may therefore be reduced by any stratification between the conductor and the surface.

#### Other simple anomaly shapes

A set of simple schematic models is shown in Figure 12, for each of which the main features of the vertical magnetic field are sketched. The set of sketches was derived from quantitative scale model experiments by Lamontagne (1975). For the simple models illustrated where the host rock is completely nonconducting, the general anomaly shape for one body remains quite constant for the whole time range. The changes in anomaly from one channel to another are mostly in the amplitude and smoothness of the anomalies.



FIG. 11. Scale model UTEM secondary magnetic  $H_x^i$  and total electric  $E_x$  data over a vertical plate conductor.



FIG. 12. The form of continuously normalized UTEM  $H_z^s$  anomalies over some simple shapes. All conductors are in free space.



FIG. 15. Decay plots for the  $H_z^z$  anomalies of Figure 14.



FIG. 16. Decay plots of H<sup>s</sup> anomalies over a thin dike (I) under a conductive overburden and (II) in a conductive half-space.

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#### Host rock effects

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Figure 16 II shows the time variation in response of a 60 S vertical plate located in a half-space. The results were calculated by Lamontagne (1975) by Fourier transformation of the frequency-domain numerical modeling of Lajoie and West (1976). At early times the response is reduced from the free-air response: this corresponds to blanking by the conductive region above the target. At later times the response is enhanced indicating that the regional (analogous) current in the host rock is being gathered into the plate at these times. For poorly conducting host rock, the response at late times is close enough to the free-space response that simple interpretation of the target using a plate in free-space model is valid. For the higher host conductivities (case 4, 5) this is no longer the case.

#### FIELD RESULTS

#### Milton, Ontario

This area was surveyed to demonstrate what data from a conductive, well-stratified earth looks like. The area is one where 650 m of flat-lying Paleozoic sediments overlie the Precambrian basement. The predominant member of the stratigraphy is a uniform and thick sequence of shale. Other beds are mostly resistive calcareous and sandstone formations. The survey area is covered by a mixed forest and marshy streams, with occasional outcrops. The top of the bedrock is a dolomite formation which is everywhere more than 20 m thick. Topographic relief is minor (<10 m), with occasional rough spots near outcrop. Overburden is probably less than 10 m every-



FIG. 18. A profile of  $H_z^s$  data from the north transmitter loop across the Thomas Twp test site. A map of the survey is included (different scale).



FIG. 20. Comparison of  $H_z^a$  data from the south transmitter loop with a free-space plate model. The configuration of the primary field is also shown.

500 µs the response changes to an asymmetric negative anomaly which decays much more slowly than the crossover response. The early-time crossover response is a current gathering or channeling anomaly where the (analogous) anomalous current flows along the length of the zone, while the longer time constant response is a local induction anomaly, where induced currents flow in a vortex within the target conductor.

Figure 19 shows a map of all the late-time profiles. They clearly delineate the edge of the target body. Figure 20 shows how a rectangular plate model can be found which models the observed results from one transmitter loop quite accurately, but which has to be rotated in order to match the results from the other loop. The late-time induced (analogous) current system in the actual conductor appears to be a tightly defined normal current in the front upper (near-loop) edge of the conductor with a more diffuse, return current deep in the rear of the body. A survey with the transmitter loop located on the other side of the body was similarly fitted by a plate dipping away from that loop, indicating the conductor to be a thick zone in which currents can flow in a variety of directions.

Electric fields were measured at the Thomas site. The late time vector map is shown in Figure 21, along with a rough numerical model. The conductive zone shows very clearly, although its edge is ill defined. Figure 22 shows a profile of the longitudinal component of electric field over the body. The field

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intensity is almost constant from channel 6 onward, and the main feature of the response is the aforementioned broad reduction in the field strength over the conductor. It is helpful, when looking at E field profiles, to imagine a plot on the same axes of the negative of the observed channel 1 response. This is the value the field starts from at the half-cycle transition. Even as early as 50 µs (Ch 9), the electric field has made most of its polarity reversal. In fact, between the loop to the target body it has overshot, while from the target body outwards it is changing relatively slowly. The time changes in E are actually very similar to those in H. There are two dominant decay times, a short one corresponding to the overburden and the channeling target response (Ch 8-6) and a long one corresponding to the local induction response (Ch 5-1). Also, these two E-field responses have a different geometrical form corresponding with the different forms of the magnetic anomalies. The scaled up version of the E data in Figure 22 shows the slowly decaying anomaly. Considerable noise is apparent in the data at this magnification.

#### Bedrock conductor beneath overburden

Figure 23 shows the measured secondary  $H_x$  fields at a site in Australia. The slow outward migration of the early-time channels and the -200 percent early-time limit away from the transmitter loop are characteristics of the response of a nearsurface conductive weathered layer. This layer has a total conductance of about 4 S.

Around station 210W a more local superimposed crossover anomaly is evident which is fixed in location. This feature is evident over a great strike length. When the visually estimated overburden response is stripped from the anomaly and the peak-to-peak crossover response is plotted on a decay plot (Figure 26), the characteristics of early time blanking, time delay, and enhancement are clearly displayed. Corresponding to the model data of Figure 16, the early time blanking attenuates the local anomaly as the (analogous) magnetic field has not had time to penetrate the weathered layer. At intermediate times (Ch 5, 4) the response lies above a fitted free-space, half-plane conductor decay curve. This is partly an amplitude enhancement from current gathering and partly due to a small delay in time while the (analogous) magnetic field penetrates the near-surface conductor. It is not clear whether any of the L400S response can be identified as due to local induction. Nevertheless, the plotted induction curve for a half-plane in free space serves as a useful reference and establishes an upper limit on the conductance of the feature (7S in this case).

On two survey lines about 1 km away, the same local feature is observed, but the response has changed to one of longer time constant. As shown in Figure 24, a clear response persists through channels 2 and 1. These data are replotted with "point normalization" on Figure 25 to show the absolute secondary field. Absolute normalization preserves the true anomaly shape, but has the disadvantage of scaling up strongly those anomalies which lie near the transmitter. The stripped peak-to-peak response is plotted in decay form in Figure 26 and clearly shows the difference in time constant at the two locations.

The increase in time constant seen on line 600N is very significant, since little change is seen in the background response and only a lesser change in the blanking time. It indicates that the L600N late-time response is due to local induc-



FIG. 22. Thomas Twp E, data for line 0 from the south transmitter loop. The expanded scale data on the lower axes show that a very weak dynamic E field anomaly is associated with the main  $H_{z}^{z}$  late time response (Ch 5-1).

Natural Sciences and Engineering Research Council of Canada and the University of Toronto. All this assistance is gratefully acknowledged. We also thank an anonymous reviewer for a very careful, helpful review.

#### REFERENCES

Annan, A. P., The equivalent source method for electromagnetic scattering analysis and its geophysical application: Ph.D. thesis, Memo-rial Univ. of Newfoundland.



FIG. 23. H<sup>a</sup> data from New South Wales showing the migrating crossovers of the overburden near the loop and a local anomaly around station 210 W. (Survey frequency 26 Hz.)

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FIG. 24. H<sup>s</sup> data on line 600N 1 km away from the previous figure showing a time decay of the local anomaly lasting to much later times. Remeasurement of the profile at 13 Hz gave virtually identical profiles (shifted one channel) with no visible Ch 1 anomaly.

- Bosschart, R. A., 1964, Analytical interpretation of fixed source electro-magnetic data: Doctoral thesis, Univ. of Delft.
  Dyck, A. V., Bloore, M., and Vallée, M. A., 1980, User manual for programs PLATE and SPHERE: Res. in Appl. Geophys. 14, Geo-bert of Device Using Using a Conceptorl. phys. Lab. Dept. of Physics, Univ. of Toronto.
- Kaufman, A., 1978, Frequency and transient responses of electromagnetic fields created by currents in confined conductors: Geo-
- physics, v. 43, p. 1002-1010. Lajoie, J., and West, G. F., 1976, The electromagnetic response of a conductive inhomogeneity in a layered earth: Geophysics, v. 41, p. 1133-1156.
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FIG. 25. Point normalized  $H_x^s$  from line 600N. The local secondary fields have been normalized to the constant primary field at station 210W and show how stripped peak-to-peak local anomaly amplitude is estimated.

# **APPENDIX IV**

data sections

SJ Geophysics Ltd. / S.J.V. Consultants Ltd. 11762 - 94th Ave., Delta, B.C. Canada tel (604) 582-1100 fax (604) 589-7466 Email syd\_visser@mindlink.net

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Appendix 2

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The following eight cost statements are for the 1996 exploration program. The statements which apply to the work filed in this volume of the report are statements 7 and 8.

# **Cost Statement 1**

The following cost statement is for work done on Aftom 10, 11, 13, and Hags 5. Structural mapping was performed by Simon Haynes, and soil sampling was performed by Ayisha Yeow and Jason Shaw during Aug. 12 to Aug.28, 1996.

Aftom 10,11,13, Hags 5	Amount	Cost
S. Haynes	7 days @ \$700/day	\$4,900.00
Soil Samplers	2 days @ \$250/day	\$500.00
Supervisor	6.6 days @ \$350/day	\$2,310.00
Helicopter	3.5 hrs @ \$750/hr	\$2,625.00
Vehicle	4 days @ \$90/day	\$360.00
Field Consumables	9 days @ \$25/day	\$225.00
Radios	9 days @ \$70/day	\$630.00
Camp Costs	15.6 days @ \$125/day	\$1,950.00
Soil Samples	82 samples @\$25/sample	\$2,050.00
Maps and Reproduction		\$50.00
Reporting	3.5 days @ \$700/day	\$2,450.00
Cad	1 days @ \$200/day	\$200.00
Travel		\$150.00
Freight		\$100.00
	TOTAL	<u>\$18,500.00</u>

Simon Haynes performed structural mapping on the Rags 1-4 and Hob 10-15 on Aug. 12 to Aug. 28, 1996.

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Rags 1-4,Hop 10-15	Amount	Cost			
S. Haynes	4.5 days @ \$700/day	\$3,150.00			
Supervisor	5.3 days @ \$350/day	\$1,855.00			
Helicopter	2.3 hrs @ \$750/hr	\$1,725.00			
Vehicle	2 days @ \$90/day	\$180.00			
Field Consumables	4.5 days @ \$25/day	\$112.50			
Radios	4.5 days @ \$70/day	\$315.00			
Camp Costs	11.5 days @ \$125/day	\$1,437.50			
Maps and Reproduction		\$50.00			
Reporting	3 days @ \$700/day	\$2,100.00			
Cad	1 days @ \$200/day	\$200.00			
Travel		\$150.00			
Freight		\$100.00			
-	TOTAL	<u>\$11,375.50</u>			

# **Cost Statement 3**

Aftom 1, 2, 3, Hob 3, 4, 8, 8.5, 9, Mojo 2 were structurally mapped by Simon Haynes and soil sampled by Ayisha Yeow, Jason Shaw, and Jason Attard during August 12 to 28 1996.

Aftom 1, 2, 3, Hob 3, 4, 8, 8.5, 9, Mojo 2	Amount	Cost
S. Haynes	5.5 days @ \$700/day	\$3,850.00
Soil Samplers	3 days @ \$250/day	\$750.00
Supervisor	6.1 days @ \$350/day	\$2,135.00
Helicopter	3.8 hrs @ \$750/hr	\$2,850.00
Vehicle	3 days @ \$90/day	\$270.00
Field Consumables	8.5 days @ \$25/day	\$212.50
Radios	8.5 days @ \$70/day	\$595.00
Camp Costs	12.6 days @ \$125/day	\$1,575.00
Soil Samples	99 samples @ \$25/sample	\$2,475.00
Maps and Reproduction		\$50.00
Reporting	3.5 days @ \$700/day	\$2,450.00
Cad	1 days @ \$200/day	\$200.00
Travel		\$150.00
Freight		\$100.00
	TOTAL	<u>\$17.662.50</u>

Cost statement for geologic mapping done by Greg Burroughs and Dane Bridge and soil samples taken by Jason Shaw and Ayisha Yeow. Work was performed on Aug. 26, 24,27 1996.

Aftom 5	Amount	Cost			
G. Burroughs	1 days @ \$350/day	\$350.00			
D. Bridge	1 days @ \$450/day	\$450.00			
Soil Samplers	3 days @ \$250/day	\$750.00			
Supervisor	1.8 days @ \$350/day	\$630.00			
Helicopter	2.1 hrs @ \$750/hr	\$1,575.00			
Vehicle	1 days @ \$90/day	\$90.00			
Field Consumables	5 days @ \$25/day	\$125.00			
Radios	5 days @ \$70/day	\$350.00			
Camp Costs	7 days @ \$125/day	\$875.00			
Soil Samples	51 samples @ \$25/sample	\$1,275.00			
Maps and Reproduction		\$50.00			
Reporting	1 days @ \$350/day	\$350.00			
Cad	1 days @ \$200/day	\$200.00			
Travel		\$150.00			
Freight		\$100.00			
	<u>TOTAL</u>	<u>\$7.320.00</u>			

# **Cost Statement 5**

Cost statement for geological mapping done by Greg Burroughs and Dane Bridge and soils sampling done by Jason Gallagher on Aftom 7 and Aftom 16 claims. Work was done Aug. 26, 29, 30, and Sept. 3, 1996.

Aftom 7,16	Amount	Cost			
G. Burroughs	1 days @ \$350/day	\$350.00			
D. Bridge	1 days @ \$450/day	\$450.00			
Soil Samplers	2 days @ \$250/day	\$500.00			
Pad Building	1 days @ \$500/day	\$500.00			
Supervisor	2.8 days @ \$350/day	\$980.00			
Helicopter	2 hrs @ \$750/hr	\$1,500.00			
Vehicle	2 days @ \$90/day	\$180.00			
Field Consumables	5 days @ \$25/day	\$125.00			
Radios	5 days @ \$70/day	\$350.00			
Camp Costs	5 days @ \$125/day	\$625.00			
Soil Samples	52 sample @ \$25/sample	\$1,300.00			
Maps and Reproduction		\$50.00			
Reporting	1 days @ \$250/day	\$350.00			
Cad	1 days @ \$200/day	\$200.00			
Travel		\$150.00			
Freight		\$100.00			
	TOTAL	<u>\$7.710.00</u>			

Cost statement for geologic mapping by Greg Burroughs and soil sampling by Jason Attard was performed on the Dup 9 group. Work was done during Aug. 13 to Aug. 22.

Dup 9, Noot 5	Amount	Cost
G. Burroughs	5.5 days @ \$350/day	\$1,925.00
Soil Samplers	3.5 days @ \$250/day	\$875.00
Supervisor	3.5 days @ \$350/day	\$1,225.00
Helicopter	3.1 hrs @ \$750/hr	\$2,325.00
Vehicle	1 days @ \$90/day	\$90.00
Field Consumables	9 days @ \$25/day	\$225.00
Radios	9 days @ \$70/day	\$630.00
Camp Costs	9 days @ \$125/day	\$1,125.00
Soil Samples	111 samples @ \$25/sample	\$2,775.00
Maps and Reproduction		\$50.00
Reporting	1 days @ \$350/day	\$350.00
Cad	1 days @ \$200/day	\$200.00
Travel		\$150.00
Freight		\$100.00
-	TOTAL	\$12.045.00

Cost statement for Fred 15 group. Geological mapping by Greg Burroughs and Dane Bridge, soil sampling done by Jason Gallagher, surveying of the cut grid was done by Fred Kaiser and Jason Scoffings, Line cutting by M.F.H. Contracting, UTEM geophysics by SJ Geophysics Ltd. All work done during Aug 11-Sept 16.

Fred 15, PMAC 1-10	Amount	Cost		
G. Burroughs	18 days @ \$350/day	\$6,300.00		
D. Bridge	4 days @ \$450/day	\$2,000.00		
Soil Sampler	9 days @ \$250/day	\$2,250.00		
Supervisor	9 days @ \$350/day	\$3,150.00		
Geophysics (2)	7 days @ \$1850/day	\$12,950.00		
Geophysics Mob\De		\$2,500.00		
Linecutting (2)	23 days @ \$525/day	\$12,075.00		
Surveyors (2)	18 days @ \$600/day	\$10,800.00		
Helicopter	31.7 hrs @ \$750/hr	\$23,775.00		
Vehicle	10 days @ \$90/day	\$900.00		
Field Consumables	136 days @ \$25/day	\$3,400.00		
Radios	136 days @ \$70/day	\$9,520.00		
Camp Costs	136 days @ \$125/day	\$17,000.00		
Soil Samples	290 samples @ \$25/sample	\$7,250.00		
Maps and Reproduction		\$50.00		
Reporting	15 days @ \$350/day	\$5,250.00		
Cad	3 days @ \$200/day	\$600.00		
Travel		\$150.00		
Freight		\$100.00		
·	TOTAL	\$120.020.00		

# **Cost Statement 8**

Cost statement for the PMAC group. UTEM Geophysics was done by SJ Geophysics Ltd. from Sept. 15 to Sept. 17, 1996.

Fred 15, PMAC 1- 10 , Noot 3	Amount	Cost
Supervisor	3 days @ \$350/day	\$1,050.00
Geophysics (2)	3 days @ \$1850/day	\$5,550.00
Helicopter	3.6 hrs @ \$750/hr	\$2,700.00
Vehicle	1 days @ \$90/day	\$90.00
Radios	6 days @ \$70/day	\$420.00
Camp Costs	9 days @ \$125/day	\$1,125.00
	TOTAL	<u>\$12.185.00</u>

Appendix 4

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# Eskay Rock Samples

09-Dec	-96	inpics			
Numbe	r Claim Nam	Grid N	Grìd E	Rockname	Comments
56811	DUP 9	3+60 N	0+05 E	Epiclastic	Sample of epiclastic in area with soil anomalies.
56812	DUP 9	2+95 N	0+40 W	Siltstone	Possible sub-crop of fine grained silts with vf dissem. py and others.
56813	DUP 9	2+50 N	0+20 W	Aphyric felsic rock	Felsic volcanic with a high amount of dark sed. fragments
56814	DUP 9	0+10 S	3+95 W	Mud/siltstone	Black-grey mud-silt from fold nose. Weak fracturing and minor qtz veinlets
56815	DUP 9	4+95 S	2+85 W	Rhyolite	Accumulated from 3 massive rhyolite boulders. VFG pyrite in minor clots and fracture filling.
56816	DUP 9	4+95 S	2+85 W	Rhyolite	Multiple massive rhyolite boulders with vfg py. One boulder appears strained with py along fractures.
56810	FRED 15	13+92 N	[ 8+02 E	Fragmental felsic volcanic	
56817	FRED 15	18+07 N	I 9+62 E	Dacite/ Rhyolite	Black/ grey matrix dacite/rhyolite bx with up to 5% py mostly constrained to matrix
56818	FRED 15	21+43 N	I 6+55 E	Siltstone	Siltstone layer in andesite flows.
56819	FRED 15	20+83 N	1 7+00 E	Rhyolite	Gossanous boulder of probable rhyolite. Strong fracturing with 5% sulphides.
56820	FRED 15	22+72 N	13+00 E	Rhyolite	Resample in area of 3517. Black matrix rhyolite.
56821	FRED 15	22+72 N	13+00 E	Mud/siltstone	Mud/ siltstone in contact with 56820. Also contains 2-3% vfg py.
56822	FRED 15	20+62 N	I 8+05 E	Dacite	Boulders of brecciated amygdaloidal dacite. All from source in the hill. Posibly some large boulder altered with 2-3% fg py. Zoning in larger clasts seen.
56823	FRED 15	8+10 N	20+78 E	Felsic breccia	Rhyolite frag. in slightly darker groundmass. Few exotic clasts. 2-5% fg py.
56824	FRED 15	19+60 N	1 8+45 E	Rhyolite	Outcrop of black rhyolite with minor light clasts. 1-5% py. Some is vfg.
56825	FRED 15	19+02 N	1 8+56 E	Rhyolite	Rhyolite fragments with up to 15% py in matrix.

Number	r Claim Nam	Grid N Grid E	Rockname	Comments
56826	FRED 15	19+50 N 9+65 E	Felsic breccia	Heterolithic Dac/Rhy Bx. Clasts and matrix vary with trace to 10% py.
56827	FRED 15	15+06 N 6+79 E	Rhyolite	Sample of Rhyolite frag that appears sheared (?) with qtz and sericite (?) and 2-5% py along fractures.

Appendix 5

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# Chemex Labs Ltd.

Analytical Chemists \* Geochemists \* Registered Assayers 212 Brooksbank Ave., North Vancouver

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218 To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9 Page Number :1-A Total Pages :1 Certificate Date: 26-SEP-96 Invoice No. :19632283 P.O. Number :8029 Account :KBOA

Project : FD6CA0052 Comments: ATTN:DAVID BRIDGE

										CE	RTIFI	CATE	OF A	NAL	<u>(SIS</u>		9632	283		
SAMPLE	PREP CODE	Au-AA ppb	Ag pp <b>n</b>	Al %	As ppm	Ba pp <b>s</b>	Be ppm	Bi ppm	Ca	Cd ppm	Co ppm	Cr ppm	Cu ppm	Fe %	Ga ppm	Hg ppm	К %	La ppm	Hg %	Mn ppm
6810 6811 6812 6813 6814	205 226 205 226 205 226 205 226 205 226 205 226 205 226	<pre></pre>	< 0.2 < 0.2 0.2 < 0.2 < 0.2 1.0	1.92 1.85 1.04 0.89 1.17	10 6 28 6 22	110 220 100 60 160	< 0.5 0.5 0.5 < 0.5 < 0.5	<pre> &lt; 2 &lt; 2</pre>	5.62 0.01 0.10 < 0.01 0.06	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	17 < 1 4 < 1 7	36 40 97 117 96	72 1 11 1 45	5.10 1.02 2.95 1.16 4.39	< 10 < 10 < 10 < 10 < 10 < 10	<pre>&lt; 1 &lt; 1</pre>	0.18 0.29 0.19 0.09 0.13	<pre>&lt; 10</pre>	1.58 1.28 0.56 0.59 0.30	1375 35 125 50 505
6815 6816 6817 6818 6819	205 226 205 226 205 226 205 226 205 226 205 226	<pre></pre>	< 0.2 < 0.2 < 0.2 < 0.2 < 0.2 < 0.2 < 0.2	0.27 0.22 1.71 3.90 1.91	26 24 12 8 12	90 120 60 1810 70	< 0.5 < 0.5 0.5 1.0 < 0.5	<pre> &lt; 2 &lt; 2</pre>	0.22 0.13 0.47 2.99 1.29	< 0.5 < 0.5 < 0.5 2.5 < 0.5	4 3 9 27 16	98 104 61 75 27	4 4 17 33 4	2.57 2.28 9.80 6.53 8.22	< 10 < 10 < 10 < 10 10 < 10	<pre>&lt; 1 &lt; 1 &lt; 1 &lt; 1 &lt; 1 &lt; 1 &lt; 1</pre>	0.15 0.13 0.29 1.10 0.19	10 10 20 40 10	0.01 0.01 0.60 3.05 0.50	240 125 260 1015 770
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 212 Brooksbank Ave.,
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 V6B 2M9

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 V7J 2C1
 Project :
 FD6CA0052

 PHONE: 604-984-0221
 FAX: 604-984-0218
 Comments:
 ATTN:DAVID BRIDGE

										CE	RTIF	CATE	OF A	NALY	SIS	A9632283
SAMPLE	PREP CODE	Mo ppm	Na %	Ni ppm	Ppm P	Pb ppm	Sb ppm	Sc ppm	Sr ppm	Ti %	T1 ppm	U ppm	V ppm	W	Zn ppm	
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56815 56816 56817 56818 56819	205 226 205 226 205 226 205 226 205 226 205 226	1 1 19 2 3	0.05 0.06 0.05 0.17 0.04	4 3 14 60 < 1	480 340 3290 2340 1570	12 10 26 6 10	6 12 4 2 2	1 1 8 10 11	13 < 11 < 33 < 299 8	0.01 0.01 0.01 0.10 0.21	<pre>&lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10</pre>	5 4 129 157 115	<pre>&lt; 10 &lt; 10</pre>	34 50 82 156 112	
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North Vancouver

212 Brooksbank Ave.,

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Project : FD6CA0052 Comments: ATTN:DAVE BRIDGE

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										CE	RTIFIC	CATE	OF A	NAL	/SIS	4	<b>\9632</b>	221		
SAMPLE	PREP CODE	Au-AA ppb	Ag ppm	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cd ppm	Co ppm	Cr ppm	Cu ppm	Fe %	Ga pp <b>a</b>	Hg ppm	X %	La ppm	Mg %	Mn ppm
6822 6823 6824 6825 6826	205 226 205 226 205 226 205 226 205 226 205 226	<pre></pre>	< 0.2 0.2 < 0.2 0.2 < 0.2 < 0.2	2.17 0.51 2.37 2.87 3.33	6 18 30 20 6	250 140 80 140 120	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	<pre>&lt; 2 &lt; 2</pre>	4.88 1.92 0.64 0.49 6.10	2.0 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	21 13 15 17 30	53 69 85 71 181	33 51 60 48 72	5.76 3.70 7.02 6.54 4.87	< 10 < 10 < 10 10 10	<pre>&lt; 1 &lt; 1</pre>	0.14 0.21 0.20 0.09 0.07	30 < 10 < 10 < 10 < 10 < 10	1.55 0.59 1.27 1.96 3.39	840 735 260 410 810
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Analytical Chemists \* Geochemists \* Registered Assayers

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Project : FD6CA0052 Comments: ATTN:DAVE BRIDGE Page Number :1-B Total Pages :1 Certificate Date: 24-SEP-96 Invoice No. :19632221 P.O. Number :8023 Account :KBOA

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PRI	EP DE	Мо ррш	Na %	Ni PPB	P ppm	Pb pp <b>n</b>	Sb ppm	Sc ppm	Sr pp <b>a</b>	Ti %	Tl ppm	n Bða	V ppm	W W	Zn ppm	
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	PE CO 205 205 205 205	PREP CODE 205 226 205 226 205 226 205 226	PREP CODE         Mo ppm           205         226         < 1	PREP CODE         Mo         Na           205         226         < 1	PREP CODE         Mo         Na         Ni           205         226         < 1	PREP CODE         HO         Na         Ni         P           205         226         < 1	PREP CODE         Mo         Na         Ni         P         Pb           205         226         < 1	PEEP         Mo         Na         Ni         P         Pb         Sb           205         226         (1)         0.04         30         4170         38         6           205         226         8         0.04         9         1290         26         2           205         226         8         0.05         22         3120         14         4           205         226         6         0.06         22         1930         4         6           205         226         <1	PREP CODE         Mo         Na         Ni         P         Pb         Sb         Sc           205         226         < 1	PBEP CODE         No         Na         Ni         P         Pb         Sb         Sc         Sr           205         226         < 1	PREP CODE         Mo         Na         Ni         P         Pb         Sb         Sc         Sr         Ti           205         226         (1)         0.04         30         4170         38         6         5         240 (-0.01)           205         226         8         0.04         9         1290         26         2         4         7         39 (-0.01)           205         226         8         0.06         22         1200         26         2         4         7         39 (-0.01)           205         226         6         0.06         22         1330         4         6         8         37 (-0.01)           205         226         (1)         0.04         139         960         8         2         19         205 (-0.01)	PBEP CODE         No         Na         Ni         P         Pb         Sb         Sc         Sr         Ti         Ti           205         226          1         0.04         30         4170         38         6         5         240         0.01         <10	PREP CODE         Mo         Na         Ni         P         Pb         Sb         Sc         Sz         Ti         Tl         U           205         226         (1)         0.04         30         4170         38         6         5         240 (-0.01         (10) </td <td>PREP CODE         No         Na         Ni         P         Pb         Sb         Sc         Sr         Ti         Ti         U         V           205         226         &lt;1</td> 0.04         30         4170         38         6         5         240         0.01         (10         (10         10         30           205         226         8         0.04         9         1290         26         2         4         179         0.01         (10         (10         10         30           205         226         6         0.065         32         1124         4         7         79         0.01         (10         (10         10         130           205         226         <1	PREP CODE         No         Na         Ni         P         Pb         Sb         Sc         Sr         Ti         Ti         U         V           205         226         <1	PREP CODE         Mo         Na         Ni         P         Pb         Sb         Sc         Sz         Ti         Ti         U         V         M           205         226         (1         0.04         30         4170         38         6         5         240 (0.01         (10         119 (10)         (10)         100         (10)         119 (10)         (10)         119 (10)         (10)	PEEP CODE         Mo         Na         Hi         P         Pb         Sb         Sc         Sr         Ti         Tl         U         V         M         Za           205         226         < 1

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Project : Comments: FD6CA0052 Page Number :1-A Total Pages :1 Certificate Date: 06-OCT-96 Invoice No. : 19633566 P.O. Number :8026 Account :KBOA

					. <u></u>		<u> </u>			CE	RTIFI	CATE	OF /	ANAL	YSIS	/	A9633	566	
SAMPLE	PREP CODE	Au-AA ppb	Ag pp <b>m</b>	Al S	As ppm	Ba P <b>PM</b>	Be ppm	Bi ppm	Ca	Cđ ppm	Co ppm	Cr pp=	Cu ppm	Fe L	Ga ppm	Hg ppm	K S	La pp <b>n</b>	Ng ¥
6827	205 226	600	< 0.2	0.23	6	80	< 0.5	< 2	5.97	< 0.5	8	95	19	3.34	< 10	< 1	0,14	< 10	0.35
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						-						-		CERTIE	CATION	14	ait	Bi	Ale

To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9

Project : FD6CA0052 Comments:

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Page Number :1-B Total Pages :1 Certificate Date: 06-OCT-96 Invoice No. : 19633566 P.O. Number :8026 Account :KBOA

										CE	RTIF	CATE	OF /	ANAL	/SIS	A9633566	
SAMPLE	PREP CODE	Мо ррш	Na L	Ni PPM	P ppm	Pb ppm	Sb ppm	Sc ppm	Sr ppm	Ti <b>X</b>	Tl pp <b>z</b>	U PP <b>m</b>	V ppm	W P <b>p</b> m	Zn pp=		
56827	205 226	5	0.01	21	670	6	2	2	547	< 0.01	< 10	< 10	9	< 10	16		
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A second																	
	<u> </u>															H. J.R. 20.	



# **Chemex Labs Ltd.**

Analytical Chemists \* Geochemists \* Registered Assayers 212 Brooksbank Ave North Vancouver

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218



# **Chemex Labs Ltd.**

Analytical Chemists \* Geochemists \* Registered Assayers 212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218

#### To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9

#### Comments:

CER	RTIFIC	CATE	A9633566			ANALYTICAL P	ROCEDURES	5	
KBOA) - CAN/ Project: FC P.O. # : 80	IAMER/ D6CA0	A GEOLOGICAL L 1052		CHEMEX CODE	NUMBER SAMPLES	DESCRIPTION	METHOD		upper Limit
Samples sub bis report	bmitte t was	ed to our lab f printed on 6	in Vancouver, BC. -OCT-96.	17 2118 2119 2120 2121 2122 2122 2123		Au ppb Ag ppm: 32 element, soil & rock Al %: 32 element, soil & rock As ppm: 32 element, soil & rock Ba ppm: 32 element, soil & rock Be ppm: 32 element, soil & rock Bi ppm: 32 element, soil & rock	AAS ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES	5 0.2 0.01 2 10 0.5 2	10000 100.0 15.00 10000 100.0 100.0 100.0
S	SAMF	PLE PREPA	RATION	2124		Cd ppm: 32 element, soil & rock	ICP-AES ICP-AES	0.5	100.0
CHEMEX NUN CODE SAM	MBER		DESCRIPTION	2127 2128 2150 2130 2131	1 1 1 1 1	Cr ppm: 32 element, soil & rock Cu ppm: 32 element, soil & rock Fe %: 32 element, soil & rock Ga ppm: 32 element, soil & rock Hg ppm: 32 element, soil & rock	ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES	1 1 0.01 10 1	10000 10000 15.00 10000 10000
205 226 3202 229	1 1 1	Geochem ring 0-3 Kg crush Rock - save e ICP - AQ Dige	to approx 150 mesh and split intire reject istion charge	2132 2151 2134 2135 2136 2137 2138 2139 2140 2141 2142 2143		K %: 32 element, soil & rock La ppm: 32 element, soil & rock Mg %: 32 element, soil & rock Mn ppm: 32 element, soil & rock Mo ppm: 32 element, soil & rock Na %: 32 element, soil & rock Ni ppm: 32 element, soil & rock P ppm: 32 element, soil & rock Pb ppm: 32 element, soil & rock Sb ppm: 32 element, soil & rock Sc ppm: 32 element, soil & rock Sr ppm: 32 element, soil & rock Sr ppm: 32 element, soil & rock	ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES	0.01 10 0.01 5 1 0.01 10 2 2 1 1 0.01	10.00 10000 15.00 10000 5.00 10000 10000 10000 10000 10000
NOTE 1: The 32 elements trace metal Elements for ligestion 1: Sa, Be, Ca,	ment I als i or wh is pos	CP package is n soil and ich the nitri sibly incomple Ga, K, La, Mg,	suitable for rock samples. lc-aqua regia ete are; Al, , Na, Sr, Ti,	2145 2146 2147 2148 2149		TI ppm: 32 element, soil & rock U ppm: 32 element, soil & rock V ppm: 32 element, soil & rock W ppm: 32 element, soil & rock Zn ppm: 32 element, soil & rock	ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES	10 10 1 10 2	10000 10000 10000 10000 10000

A9633566



Analytical Chemists \* Geochemists \* Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218

To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9

CERTIFICATION:

Project : FD6CA0052 Comments:

Page Number :1-A Total Pages :1 Certificate Date: 06-OCT-96 Invoice No. : 19633566 P.O. Number :8026 :KBOA Account

											CE	RTIF	CATE	OF A	NAL	YSIS		A9633	566		
SAMPLE	PR CO	EP DE	Au-AA ppb	Ag ppm	Al %	As ppm	Ba ppm	Be pp∎	Bi ppm	Ca %	Cđ ppm	Co pp∎	Cr ppm	Cu ppm	Fe %	Ga pp <b>m</b>	Hg ppm	K L	La pp#	Mg	Mn ppm
56827	205	226	600	< 0.2	0.23	5	80	< 0.5	< 2	5.97	< 0.5	8	95	19	3.34	< 10	< 1	0.14	< 10	0.35	985
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# **Chemex Labs Ltd.**

Analytical Chemists \* Geochemists \* Registered Assavers 212 Brooksbank Ave., North Vancouver

British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218

To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V68 2M9

Project : FD6CA0052 Comments:

Page Number : 1-B Total Pages : 1 Certificate Date: 06-OCT-96 Invoice No. : 19633566 P.O. Number : 8026 Account :KBOA

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SAMPLE	PI CO	EP DE	Mo ppm	Na %	Ni PPm	P ppm	Pb ppm	Sb PP <b>n</b>	Sc pp <b>n</b>	Sr ppm	Ti %	Tl ppm	U PP <b>m</b>	V ppm	W ppm	Zn ppm	
56827	205	226	5 5	0.01	21	670	6	2	2	547 <	0.01	< 10	< 10	9	< 10	16	
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															CERTIFIC	ATION:	Hart Brechler

CERTIFICATION:\_



### **Chemex Labs Ltd.**

Analytical Chemists \* Geochemists \* Registered Assayers 212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218

#### To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9

Comments:

С	ERTIFI	CATE	A9633567			ANALYTICAL P	ROCEDURES	6	
KBOA) - ( Project:	CANAMER FD6CA(	A GEOLOGICAL 0052	LTD.	CHEMEX CODE	NUMBER	DESCRIPTION	METHOD		Upper Limit
amples his rej	submitte	ed to our lab printed on (	in Vancouver, BC. 6-OCT-96.	17 2118 2119 2120 2121 2122 2123	330 330 330 330 330 330 330 330	Au ppb Ag ppm: 32 element, soil & rock Al %: 32 element, soil & rock As ppm: 32 element, soil & rock Ba ppm: 32 element, soil & rock Be ppm: 32 element, soil & rock Bi ppm: 32 element, soil & rock	AAS ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES ICP-AES	5 0.2 0.01 2 10 0.5 2	10000 100.0 15.00 10000 10000 100.0 10000
	SAM	PLE PREPA	RATION	2124 2125 2126	330 330 330	Ca %: 32 element, soil & rock Cd ppm: 32 element, soil & rock Co ppm: 32 element, soil & rock	ICP-AES ICP-AES ICP-AES	0.01 0.5 1	15.00 100.0 10000
201 202 229	NUMBER SAMPLES 330 330 330	Dry, sieve f save reject ICP - AQ Dig	DESCRIPTION to -80 mesh gestion charge	2127 2128 2150 2130 2131 2132 2151 2134 2135 2136 2137 2138 2139 2140 2141 2142 2143 2144 2145 2146	330 330 330 330 330 330 330 330 330 330	Cr ppm: 32 element, soil & rock Cu ppm: 32 element, soil & rock Fe %: 32 element, soil & rock Ga ppm: 32 element, soil & rock Hg ppm: 32 element, soil & rock K %: 32 element, soil & rock Ma ppm: 32 element, soil & rock Mn ppm: 32 element, soil & rock Mo ppm: 32 element, soil & rock Na %: 32 element, soil & rock Na %: 32 element, soil & rock Na %: 32 element, soil & rock Ppm: 32 element, soil & rock Ppm: 32 element, soil & rock Sb ppm: 32 element, soil & rock Sb ppm: 32 element, soil & rock Sc ppm: 32 element, soil & rock Sr ppm: 32 element, soil & rock Ti %: 32 element, soil & rock Ti ppm: 32 element, soil & rock Ti ppm: 32 element, soil & rock Sc ppm: 32 element, soil & rock	ICP-AES ICP-AES	1 1 0.01 10 1 0.01 10 0.01 1 10 2 2 1 10 2 1 10 2 1 10 10 10 10 10 10 10 10 10	$     \begin{array}{r}       10000 \\     $
he 32 of race 1 lement: igestic a, Be, 1, W.	element metals s for wi on is por Ca, Cr,	ICP package i in soil and hich the nit saibly incomp Ga, K, La, M	s suitable for rock samples. ric-aqua regia lete are: Al, g, Na, Sr, Ti,	2148 2149	330 330	W ppm: 32 element, soil & rock Zn ppm: 32 element, soil & rock	ICP-AES ICP-AES	10 2	10000

A9633567



Analytical Chemists \* Geochemists \* Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218 To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9 Page Number :1-A Total Pages :9 Certificate Date: 06-OCT-96 Invoice No. :19633567 P.O. Number :8026 Account :KBOA

Project : FD6CA0052 Comments:

										CE	RTIF	CATE	OF A	NAL	<b>YSIS</b>		19633	567		
SAMPLE	PREP CODE	Au-AA ppb	Ag ppm	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cd ppm	Co ppm	Cr ppm	Cu pp=	Fe %	Ga ppm	Hg ppm	K %	La ppm	Mg %	Mn ppm
F15-L10 05+50 F15-L10 05+75 F15-L10 06+00 F15-L10 06+25 F15-L10 06+50	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.8 0.8 0.6 < 0.2 1.2	4.23 4.04 4.23 3.58 5.61	8 < 2 < 2 < 2 < 2 < 2 < 2	50 60 30 40 10	1.0 2.0 0.5 0.5 1.5	<pre>&lt; 2 &lt; 2 4 &lt; 2 &lt; 4 &lt; 2 &lt; 2 &lt; 2</pre>	0.07 0.10 0.15 0.07 0.06	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	16 22 4 7 6	28 37 27 35 20	19 40 12 10 3	5.66 5.95 5.05 5.86 6.27	20 10 30 30 30	<pre>&lt; 1 &lt; 1</pre>	0.05 0.07 0.05 0.06 0.04	20 50 10 20 30	0.37 0.52 0.35 0.32 0.10	1060 2180 215 500 690
F15-L10 06+75 F15-L10 07+00 F15-L10 07+25 F15-L10 07+75 F15-L10 08+00	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	<pre>&lt; 0.2 0.6 &lt; 0.2 &lt; 0.2 0.2</pre>	4.39 4.62 1.54 2.88 3.03	<pre> &lt; 2 &lt; 2 16 18 &lt; 2 </pre>	20 30 80 70 60	0.5 1.0 0.5 1.0 0.5	2 < 2 < 2 < 2 < 2 < 2 < 2	0.09 0.07 0.08 0.22 0.03	<pre>&lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5</pre>	13 8 12 24 20	29 27 14 8 12	12 10 26 36 25	7.33 6.78 4.79 5.04 6.95	40 40 < 10 10 10	<pre>&lt; 1 &lt; 1</pre>	0.06 0.04 0.10 0.13 0.10	10 20 < 10 20 10	0.28 0.29 0.23 0.82 0.26	985 635 395 1315 2560
F15-L10 08+25 F15-L10 08+50 F15-L10 08+75 F15-L10 09+25 F15-L10 09+50	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.2 < 0.2 < 0.2 < 0.2 < 0.2 0.2	3.22 3.66 5.33 5.23 3.95	<pre>&lt; 2 &lt; 2</pre>	50 20 50 30 10	0.5 0.5 0.5 1.0 0.5	<pre> &lt; 2 &lt; 2 &lt; 4 &lt; 2 &lt; 4 &lt; 2 2 </pre>	0.13 0.11 0.44 0.11 0.08	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	21 6 10 10 4	22 27 22 29 27	20 9 19 14 5	5.02 6.45 6.62 6.38 7.14	10 30 20 30 30	< 1 < 1 < 1 < 1 < 1 < 1	0.08 0.04 0.11 0.04 0.04	< 10 10 < 10 20 30	0.38 0.27 0.78 0.23 0.16	1755 390 305 365 270
P15-L10 09+75 P15-L10 10+00 P15-L10 10+25 F15-L10 10+50 F15-L10 10+75	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5</pre>	0.4 < 0.2 < 0.2 0.2 0.2	3.86 5.16 4.14 4.17 3.75	6 < 2 < 2 < 2 < 2 < 2 < 2	30 30 20 20 20	0.5 1.0 1.0 1.0 0.5	<pre> &lt; 2 &lt; 2</pre>	0.08 0.18 0.05 0.09 0.08	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	7 6 8 8 4	30 25 22 20 30	16 11 9 9 17	6.00 6.76 6.57 7.05 6.22	30 30 30 30 40	<pre>&lt; 1 &lt; 1</pre>	0.07 0.06 0.06 0.06 0.06	10 20 30 20 10	0.33 0.31 0.13 0.21 0.25	580 500 565 620 145
F15-L10 11+00 F15-L10 11+50 F15-L10 12+00 F15-L10 12+25 F15-L10 12+50	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.2 0.6 0.2 0.4 < 0.2	3.76 5.05 4.82 3.89 4.79	<pre> &lt; 2 &lt; 2</pre>	50 30 50 10 40	0.5 1.5 2.0 1.0 2.0	<pre></pre>	0.04 0.11 0.30 0.07 0.06	<pre>&lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5</pre>	12 8 6 5 9	46 29 29 28 22	14 10 15 9 23	5.70 6.31 6.03 7.89 6.21	20 30 20 40 30	<pre>&lt; 1 &lt; 1</pre>	0.03 0.05 0.08 0.03 0.07	10 20 40 20 30	0.50 0.23 0.57 0.14 0.23	910 360 285 435 955
P15-L10 12+75 P15-L10 13+00 P15-L11 05+75 P15-L11 07+00 P15-L11 08+00	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 </pre>	0.2 < 0.2 0.4 0.2 < 0.2	3.74 3.32 4.52 4.06 4.07	< 2 < 2 < 2 < 2 < 2 < 2 < 2	60 20 10 40 50	0.5 0.5 1.0 0.5 0.5	<pre>&lt; 2 &lt; 2</pre>	0.23 0.11 0.04 0.21 0.15	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	20 9 4 7 12	33 32 20 17 32	23 11 < 1 8 13	4.75 7.43 7.16 5.07 5.28	10 30 40 10 10	<pre>&lt; 1 &lt; 1</pre>	0.09 0.06 0.06 0.04 0.06	< 10 10 30 10 10	0.70 0.38 0.10 0.32 0.42	1060 500 530 260 480
F15-L11 08+25 F15-L11 08+50 F15-L11 08+75 F15-L11 09+00 F15-L11 09+25	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 </pre>	< 0.2 1.0 0.2 < 0.2 < 0.2	4.35 4.90 5.01 5.24 3.90	<pre>&lt; 2 &lt; 2</pre>	40 20 30 40 50	0.5 1.0 1.0 2.0 1.0	4 2 2 4 < 2	0.18 0.13 0.08 0.15 0.14	<pre>&lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5</pre>	10 6 5 12 15	25 25 29 34 30	21 11 13 23 21	7.05 6.72 6.95 6.46 5.99	20 30 30 30 20	<pre>&lt; 1 &lt; 1</pre>	0.08 0.05 0.04 0.05 0.07	10 30 20 40 10	0.52 0.29 0.19 0.33 0.47	745 275 370 625 760
F15-L11 09+50 F15-L11 09+75 F15-L11 10+00 F15-L11 10+75 F15-L11 11+00	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.2 < 0.2 < 0.2 0.6 < 0.2	3.64 5.02 2.28 5.27 4.35	< 2 < 2 22 < 2 < 2 < 2 < 2	60 60 80 20 50	1.5 0.5 2.0 1.5 0.5	< 2 < 2 < 2 < 2 < 2 4	0.11 0.33 0.01 0.06 0.32	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	11 12 15 4 9	30 23 7 35 30	23 19 30 6 22	4.88 6.26 5.57 7.60 6.18	10 10 < 10 40 10	< 1 < 1 < 1 < 1 < 1 < 1	0.07 0.10 0.08 0.04 0.11	10 10 20 30 < 10	0.55 0.61 0.06 0.14 0.71	570 485 1395 370 345

tart Broklen CERTIFICATION:\_



Analytical Chemists \* Geochemists \* Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218 To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9

Page Number :1-B Total Pages :9 Certificate Date: 06-OCT-96 Invoice No. : 19633567 P.O. Number : 8026 Account :KBOA

Project : FD6CA0052 Comments:

										CE	RTIFI	CATE	OF A	NALY	'SIS	A9633567
SAMPLE	PREP CODE	Мо ррш	N	a Ni k ppm	p ppm	Pb ppm	Sb ppm	Sc ppm	Sr ppm	Ti %	Tl ppm	U PPm	V ppm	W ppm	Zn ppm	
P15-L10 05+50 P15-L10 05+75 P15-L10 06+00 P15-L10 06+25 P15-L10 06+50	201 202 201 202 201 202 201 202 201 202 201 202	6 4 3 4 6	< 0.0 0.0 0.0 0.0	L 12 L 18 L 4 L 13 B 5	1020 1230 740 770 980	18 14 12 12 12	2 4 4 2 4	6 10 7 5 4	9 12 13 9 7	0.30 0.28 0.51 0.27 0.18	<pre>&lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10</pre>	88 102 108 69 34	< 10 < 10 < 10 < 10 < 10 < 10	132 104 38 54 72	
F15-L10 06+75 F15-L10 07+00 F15-L10 07+25 F15-L10 07+75 F15-L10 08+00	201 202 201 202 201 202 201 202 201 202 201 202	7 5 2 5 3	0.0 0.0 < 0.0 0.0 < 0.0	2 5 L 15 L 11 L 7 L 5	790 730 1220 1310 1670	12 14 6 12 16	2 2 2 2 2 2 2	7 4 5 7 4	9 8 13 6	0.40 0.23 0.01 0.07 0.04	< 10 < 10 < 10 < 10 < 10 < 10	< 10 < 10 < 10 < 10 < 10 < 10	89 62 32 61 47	< 10 < 10 < 10 < 10 < 10 < 10	62 74 92 102 94	
F15-L10 08+25 F15-L10 08+50 F15-L10 08+75 F15-L10 09+25 F15-L10 09+50	201 202 201 202 201 202 201 202 201 202 201 202	3 4 2 5 6	0.0 < 0.0 0.1 0.0 0.0	L 9 L 5 L 9 L 5 L 2	1000 720 1390 890 660	2 10 < 2 10 6	2 < 2 2 4 2	6 6 16 8 5	14 13 44 12 10	0.24 0.45 0.76 0.39 0.33	<pre>&lt; 10 &lt; 10</pre>	< 10 < 10 < 10 < 10 < 10 < 10	84 115 147 89 78	< 10 < 10 < 10 < 10 < 10 < 10	72 40 48 64 42	
F15-L10 09+75 F15-L10 10+00 F15-L10 10+25 F15-L10 10+50 F15-L10 10+75	201 202 201 202 201 202 201 202 201 202 201 202	6 4 6 6 4	0.0	2 11 4 4 2 3 4 5 3 6	1390 950 720 640 1210	12 2 14 12 14	<pre></pre>	6 9 5 5 7	8 18 7 10 9	0.25 0.44 0.29 0.30 0.37	<pre>&lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10</pre>	67 81 58 53 98	< 10 < 10 < 10 < 10 < 10 < 10	80 50 50 62 48	
F15-L10 11+00 F15-L10 11+50 F15-L10 12+00 F15-L10 12+25 F15-L10 12+50	201 202 201 202 201 202 201 202 201 202 201 202	4 5 5 7 6	< 0.0 0.0 0.0 < 0.0	L 27 3 7 7 14 L 4 3 26	660 830 960 730 1000	8 8 4 12 14	2 2 4 2 2	5 6 9 5 5	9 12 27 9 10	0.20 0.33 0.58 0.34 0.28	<pre>&lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10</pre>	74 78 111 84 56	< 10 < 10 < 10 < 10 < 10 < 10	78 62 66 52 122	
F15-L10 12+75 F15-L10 13+00 F15-L11 05+75 F15-L11 07+00 F15-L11 08+00	201 202 201 202 201 202 201 202 201 202 201 202	2 5 7 3 3	0.0	6 25 3 10 4 1 1 6 1 13	1100 640 860 860 930	10 10 16 8 8	4 2 2 2 2	6 6 4 5 7	25 13 5 21 16	0.21 0.37 0.24 0.42 0.29	<pre>&lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10</pre>	< 10 < 10 < 10 < 10 < 10 < 10	77 92 48 104 91	< 10 < 10 < 10 < 10 < 10 < 10	84 52 66 60 62	
F15-L11 08+25 F15-L11 08+50 F15-L11 08+75 F15-L11 09+00 F15-L11 09+25	201 202 201 202 201 202 201 202 201 202 201 202	4 5 5 3	0.0 0.0 0.0 0.0	12 3 4 1 5 3 10 3 15	1190 760 860 1030 1120	8 14 10 12 10	4 2 4 2 2	10 8 6 8 8	19 14 10 16 17	0.47 0.46 0.35 0.45 0.41	<pre>&lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10</pre>	103 90 86 99 98	< 10 < 10 < 10 < 10 < 10 < 10	80 52 52 82 72	
F15-L11 09+50 F15-L11 09+75 F15-L11 10+00 F15-L11 10+75 F15-L11 10+75 F15-L11 11+00	201 202 201 202 201 202 201 202 201 202 201 202	3 2 4 6 3	0.0 0.0 < 0.0 0.0	L 25 B 8 L 8 2 4 9 14	1290 1240 1030 810 1340	10 4 12 12 2	2 2 2 2 2 2	7 11 7 6 11	13 34 5 8 34	0.25 0.64 0.01 0.30 0.56	< 10 < 10 < 10 < 10 < 10 < 10	< 10 < 10 < 10 < 10 < 10 < 10	73 132 23 67 127	< 10 < 10 < 10 < 10 < 10 < 10	114 58 98 60 66	•
	<u></u>													ERTIFIC	ATION:	HartBuchler



Analytical Chemists \* Geochemists \* Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218 To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9

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Page Number :2-A Total Pages :9 Certificate Date: 06-OCT-96 Invoice No. :19633567 P.O. Number :8026 Account :KBOA

Project : FD6CA0052 Comments:

												JAIE	UF A	NALT	313	<i></i>	19033	507		
SAMPLE	PREP CODE	Au-AA ppb	Ag ppm	A1 %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cd pp∎	Со ррт	Cr ppm	Cu ppm	Fe %	Ga pp <b>m</b>	Hg ppm	K 8	La ppm	Mg	Mn ppm
P15-L11 11+25 P15-L11 11+50 P15-L11 11+75 P15-L11 12+00 P15-L11 12+25	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.8 1.0 < 0.2 0.6 0.2	4.54 4.55 3.58 4.77 3.55	<pre>&lt; 2 &lt; 2 </pre>	50 10 80 10 10	0.5 1.0 0.5 1.0 1.0	<pre>&lt; 2 &lt; 2 &lt; 2 &lt; 4 &lt; 2</pre>	0.25 0.09 0.13 0.05 0.05	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	15 6 15 3 9	30 24 37 18 22	18 6 28 5 13	5.38 7.26 4.72 6.43 6.47	10 30 10 30 30	<pre>&lt; 1 &lt; 1</pre>	0.08 0.05 0.09 0.06 0.10	10 20 10 30 30	0.58 0.18 0.63 0.09 0.20	835 555 745 385 1580
F15-L11 12+50 F15-L11 12+75 F15-L11 13+00 F15-L12 04+50 F15-L12 04+75	201 202 201 202 201 202 201 202 201 202 201 202	<pre></pre>	< 0.2 < 0.2 < 0.2 < 0.2 0.2 1.4	3.49 3.52 4.15 4.08 4.40	<pre>&lt; 2 &lt; 2</pre>	50 60 30 20 20	0.5 0.5 0.5 0.5 0.5	<pre>&lt; 2     4     &lt; 2     &lt; 2     &lt; 2     &lt; 2 &lt; 2</pre>	0.16 0.42 0.16 0.09 0.11	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	16 17 6 6 6	45 32 30 36 25	20 13 10 13 12	5.68 7.21 6.08 6.69 6.50	20 30 30 30 30 30	<pre> &lt; 1 &lt; 1</pre>	0.07 0.12 0.05 0.05 0.05	10 10 10 30 30	0.73 0.73 0.38 0.27 0.29	850 1635 455 300 470
F15-L12       05+00         F15-L12       05+25         F15-L12       05+50         F15-L12       05+75         F15-L12       06+00	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5</pre>	0.4 < 0.2 0.8 1.4 1.4	4.25 3.32 2.85 5.24 3.59	<pre>&lt; 2     6     &lt; 2     &lt; 2     &lt; 2     &lt; 2     &lt; 2</pre>	40 40 20 10 20	0.5 0.5 < 0.5 1.5 0.5	<pre></pre>	0.22 0.05 0.11 0.04 0.05	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	B 6 2 8	28 30 31 15 23	16 17 12 5 12	6.32 7.14 7.82 6.09 6.66	20 10 30 30 30	<pre>&lt; 1 &lt; 1</pre>	0.08 0.03 0.06 0.04 0.08	10 < 10 10 20 20	0.56 0.28 0.37 0.09 0.22	635 260 360 485 1190
F15-L12 06+25 F15-L12 06+50 F15-L12 06+75 F15-L12 07+00 F15-L12 07+25	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	2.2 0.8 1.2 0.2 1.0	4.24 3.98 4.49 3.85 3.35	<pre></pre>	40 60 50 20 70	0.5 0.5 1.0 0.5 0.5	<pre> &lt; 2 &lt; 2 &lt; 2 &lt; 4 &lt; 4 &lt; 2 &lt; 4 </pre>	0.16 0.23 0.05 0.06 0.15	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	16 12 16 3 7	25 26 34 27 26	15 19 27 8 14	6.44 5.16 5.79 7.36 4.72	30 10 20 30 10	<pre>&lt; 1 &lt; 1</pre>	0.06 0.07 0.07 0.06 0.06	20 10 20 30 10	0.42 0.45 0.33 0.23 0.40	1570 900 1735 185 370
P15-L12       08+75         P15-L12       09+00         P15-L12       09+25         P15-L12       09+50         P15-L12       09+75	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.2 0.2 < 0.2 0.2 0.2 0.2	3.26 4.17 4.00 4.20 5.19	<pre> &lt; 2 &lt; 2 &lt; 2 &lt; 2 10 &lt; 2 </pre>	40 40 50 40 10	<pre>&lt; 0.5 0.5 0.5 1.0 1.5</pre>	< 2 < 2 < 2 2 < 2 < 2	0.15 0.08 0.09 0.12 0.03	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	8 13 9 8 4	38 41 48 34 23	26 23 18 21 9	6.18 6.17 4.62 5.56 6.32	10 30 10 20 30	<pre>&lt; 1 &lt; 1</pre>	0.08 0.08 0.07 0.08 0.05	10 20 10 20 30	0.59 0.42 0.54 0.41 0.15	380 835 425 925 400
F15-L12 10+00 F15-L12 10+25 F15-L12 10+50 F15-L12 10+75 F15-L12 10+75 F15-L12 11+25	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5</pre>	0.8 < 0.2 0.2 0.8 < 0.2	3.63 1.83 4.73 1.84 4.45	2 14 8 12 < 2	70 80 30 80 20	0.5 0.5 2.0 0.5 0.5	<pre>&lt; 2 &lt; 2</pre>	0.06 0.06 0.04 0.09 0.10	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	5 10 5 16 5	20 7 16 8 35	19 34 < 1 37 16	5.23 6.03 5.07 5.09 6.68	10 < 10 20 < 10 30	<pre>&lt; 1 &lt; 1</pre>	0.05 0.07 0.07 0.09 0.05	10 < 10 30 < 10 20	0.11 0.04 0.16 0.13 0.30	400 760 355 1000 255
F15-L12 11+50 F15-L12 11+75 F15-L12 12+00 F15-L12 12+25 F15-L12 12+50	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	< 0.2 0.2 < 0.2 0.2 0.2 0.2	5.45 3.26 3.22 4.51 4.48	<pre> &lt; 2 &lt; 2</pre>	60 50 60 20 40	1.0 0.5 1.0 0.5 2.5	4 < 2 < 2 2 < 2	0.40 0.06 0.12 0.12 0.10	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	15 19 24 7 3	24 57 38 29 15	26 21 32 11 12	6.19 6.34 4.81 5.96 4.62	10 20 10 20 30	<pre>&lt; 1 &lt; 1</pre>	0.12 0.08 0.09 0.05 0.05	10 10 10 20 40	0.70 0.81 0.65 0.27 0.14	615 1585 1580 520 215
F15-L12 12+75 F15-L12 13+00 F15-L13 04+50 F15-L13 04+75 F15-L13 05+00	201 202 201 202 201 202 201 202 201 202 201 202	<pre></pre>	0.2 0.2 0.2 0.6 < 0.2	4.14 3.66 4.35 2.85 3.47	<pre></pre>	100 20 30 40 30	2.0 0.5 1.0 0.5 < 0.5	2 < 2 4 < 2 < 2 < 2	0.54 0.04 0.21 0.03 0.05	3.0 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	11 6 5 6 5	27 31 20 45 49	12 15 9 15 18	5.68 6.07 6.02 7.15 6.01	10 30 30 30 10	<pre>&lt; 1 &lt; 1</pre>	0.05 0.06 0.07 0.03 0.03	30 20 40 10 10	0.60 0.41 0.53 0.45 0.34	575 530 240 310 185
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CERTIFICATION: Hart Brokler



Analytical Chemists \* Geochemists \* Registered Assayers 212 Brooksbank Ave., North Vancouver

212 Brooksbank Ave.,North VancouverBritish Columbia, CanadaV7J 2C1PHONE: 604-984-0221FAX: 604-984-0218

To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9 Page Number :2-B Total Pages :9 Certificate Date: 06-OCT-96 Invoice No. :19633567 P.O. Number :8026 Account :KBOA

Project : FD6CA0052 Comments:

											CE	RTIFI	CATE	OF A	NALY	'SIS	A9633567
SAMPLE	PREP CODE	;	Мо рра	Na %	Ni ppm	pp#	Pb pp <b>n</b>	Sb ppm	Sc ppm	Sr ppm	Ti %	Tl ppm	U ₽₽∎	V ppm	W PP=	Zn ppm	
F15-L11 11+25 F15-L11 11+50 F15-L11 11+75 F15-L11 12+00 F15-L11 12+25	201 2 201 2 201 2 201 2 201 2 201 2	02 02 02 02 02	3 6 3 5 7	0.03 0.04 0.03 0.04 0.05	13 4 29 4 14	1090 930 1190 910 810	4 10 8 10 14	2 < 2 2 < 2 2 2 2	8 4 9 5 5	25 11 17 7 6	0.45 0.29 0.28 0.19 0.23	<pre>&lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10</pre>	115 60 89 33 43	< 10 < 10 < 10 < 10 < 10 < 10	66 56 96 64 98	
F15-L11 12+50 F15-L11 12+75 F15-L11 13+00 F15-L12 04+50 F15-L12 04+75	201 2 201 2 201 2 201 2 201 2 201 2	02 02 02 02 02 02	4 3 4 5 6	0.03 0.19 0.04 0.01 0.03	50 14 10 8 6	1030 780 770 850 700	10 10 10 6 8	2 < 2 2 < 2 2 2	5 7 5 7 5	20 51 18 10 11	0.26 0.33 0.35 0.33 0.40	<pre>&lt; 10 &lt; 10</pre>	< 10 < 10 < 10 < 10 < 10 < 10	75 109 83 75 88	< 10 < 10 < 10 < 10 < 10 < 10	134 74 52 44 60	
F15-L12       05+00         F15-L12       05+25         F15-L12       05+50         F15-L12       05+75         F15-L12       06+00	201 2 201 2 201 2 201 2 201 2 201 2	02 02 02 02 02	4 2 6 7 6	0.04 (0.01 0.01 0.03 0.03	10 8 7 1 8	940 680 630 760 890	6 14 10 16 14	4 2 2 2 2	8 5 6 4 4	21 9 13 5 8	0.53 0.10 0.39 0.21 0.25	<pre>&lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10</pre>	115 128 108 40 60	<pre>&lt; 10 &lt; 10</pre>	62 60 56 62 94	
F15-L12       06+25         F15-L12       06+50         F15-L12       06+75         F15-L12       07+00         F15-L12       07+25	201 2 201 2 201 2 201 2 201 2 201 2	02 02 02 02 02	6 3 5 7 3	0.04 0.01 0.01 0.01 0.02	8 11 22 5 12	1000 2910 1080 780 1030	10 6 14 12 12	4 2 2 2 2	6 6 6 4	17 21 9 8 19	0.42 0.35 0.17 0.34 0.28	< 10 < 10 < 10 < 10 < 10 < 10	<pre>&lt; 10 &lt; 10</pre>	104 126 55 75 94	<pre>&lt; 10 &lt; 10</pre>	76 102 140 48 80	
F15-L12       08+75         F15-L12       09+00         F15-L12       09+25         F15-L12       09+50         F15-L12       09+75	201 2 201 2 201 2 201 2 201 2 201 2	02 02 02 02 02 02	3 5 3 4 5	0.01 0.01 0.01 0.01 0.01	21 24 25 17 7	1390 1080 860 1430 980	10 14 6 12 8	2 2 2 2 2 4	8 6 7 4	17 9 12 15 6	0.37 0.26 0.25 0.28 0.19	< 10 < 10 < 10 < 10 < 10 < 10	<pre>&lt; 10 &lt; 10</pre>	110 69 71 84 39	<pre>&lt; 10 &lt; 10</pre>	82 96 64 100 56	
F15-L12       10+00         F15-L12       10+25         F15-L12       10+50         F15-L12       10+75         F15-L12       11+25	201 2 201 2 201 2 201 2 201 2 201 2	02 02 02 02 02	4 4 5 1 6	0.01 (0.01 0.04 (0.01 0.03	3 4 8 9 9	1190 3190 470 1850 1210	8 12 10 10 10	2 2 < 2 < 2 4	4 4 3 4 6	8 7 6 9 11	0.13 0.01 0.12 0.01 0.36	< 10 < 10 < 10 < 10 < 10 < 10	<pre>&lt; 10 &lt; 10</pre>	53 25 22 31 89	<pre>&lt; 10 &lt; 10</pre>	62 116 82 112 66	
F15-L12       11+50         F15-L12       11+75         F15-L12       12+00         F15-L12       12+25         F15-L12       12+50	201 2 201 2 201 2 201 2 201 2 201 2	02 02 02 02 02 02	2 3 3 5 3	0.10 < 0.01 0.01 0.02 0.05	10 45 43 7 12	1280 970 1280 950 630	< 2 10 14 10 10	2 2 2 < 2 < 2 < 2	12 5 6 5 5	41 11 17 12 13	0.71 0.18 0.20 0.33 0.19	< 10 < 10 < 10 < 10 < 10 < 10	<pre>&lt; 10 &lt; 10</pre>	136 66 60 74 29	< 10 < 10 < 10 < 10 < 10 < 10	80 90 164 52 78	
F15-L12 12+75 F15-L12 13+00 F15-L13 04+50 F15-L13 04+75 F15-L13 05+00	201 2 201 2 201 2 201 2 201 2 201 2	02 02 02 02 02	4 6 4 4	0.03 0.01 0.04 < 0.01 < 0.01	41 21 7 22 17	980 750 910 480 640	2 12 4 12 8	2 2 2 2 2 2	7 4 8 5 4	53 7 18 8 10	0.61 0.14 0.59 0.21 0.12	< 10 < 10 < 10 < 10 < 10 < 10	< 10 < 10 < 10 < 10 < 10 < 10 < 10	112 40 107 102 74	< 10 < 10 < 10 < 10 < 10 < 10	246 68 50 66 56	

CERTIFICATION:

Ho & Bichles



Analytical Chemists \* Geochemists \* Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218 To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9 Page Number :3-A Total Pages :9 Certificate Date: 06-OCT-96 Invoice No. :19633567 P.O. Number :8026 Account :KBOA

Project : FD6CA0052 Comments:

											C	ERTIF	ICAT	EOF	ANAL	YSIS		A963	3567		
SAMPLE	PRI COI	EP DE	Au-AA ppb	Ag ppm	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cd PP <b>m</b>	Co ppm	Cr ppm	Cu ppm	Fe %	Ga ppm	Hg ppm	K %	La ppm	Mg %	Mn ppm
F15-L13 05+25 F15-L13 05+50 F15-L13 05+75 F15-L13 06+00 F15-L13 06+25	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.4 < 0.2 0.6 < 0.2 0.2	4.02 4.47 3.31 3.91 3.72	<pre></pre>	20 20 50 50 70	0.5 0.5 ( 0.5 0.5 0.5	< 2 4 2 < 2 < 2	0.09 0.15 0.17 0.08 0.19	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	13 13 11 6 22	29 28 42 39 35	17 16 14 15 21	7.25 6.04 5.66 5.77 5.22	30 30 20 10 10	<pre>&lt; 1 &lt; 1</pre>	0.07 0.06 0.07 0.03 0.07	20 20 < 10 10 10	0.24 0.32 0.52 0.24 0.67	1160 805 615 525 2810
F15-L13 06+50 F15-L13 06+75 F15-L13 07+00 F15-L13 07+50 F15-L13 07+75	201 201 201 201 201 201	202 202 202 202 202 202	<pre></pre>	0.2 0.2 1.0 1.2 < 0.2	4.15 4.35 2.58 2.57 4.01	<pre></pre>	30 40 90 90 50	0.5 1.0 0.5 0.5 0.5	<pre></pre>	0.14 0.14 0.06 0.16 0.27	< 0.5 < 0.5 0.5 < 0.5 < 0.5	11 12 14 11 14	27 32 37 30 23	13 24 44 16 10	5.56 6.11 5.76 5.70 5.78	20 20 10 10	<pre>&lt; 1 &lt; 1</pre>	0.07 0.07 0.07 0.06 0.06	10 10 < 10 10 10	0.45 0.45 0.46 0.47 0.53	675 775 645 970 785
F15-L13 08+00 F15-L13 08+25 F15-L13 08+50 F15-L13 08+75 F15-L13 09+00	201    	202   	<pre></pre>	0.2 NotRcd NotRcd NotRcd NotRcd	2.47 NotEcd NotEcd NotEcd NotEcd	26 NotRcd NotRcd NotRcd NotRcd	80 NotRcd NotRcd NotRcd NotRcd	< 0.5 NotRcd NotRcd NotRcd NotRcd	<pre>&lt; 2 NotRcd NotRcd NotRcd NotRcd NotRcd</pre>	0.05 NotRcđ NotRcđ NotRcđ NotRcd	<pre>&lt; 0.5 NotRcd NotRcd NotRcd NotRcd NotRcd</pre>	9 NotRcd NotRcd NotRcd NotRcd	26 NotRcd NotRcd NotRcd NotRcd	54 NotRcđ NotRcđ NotRcđ NotRcđ	8.02 NotRcd NotRcd NotRcd NotRcd	10 NotRcd NotRcd NotRcd NotRcd	<pre>&lt; 1 NotRcd NotRcd NotRcd NotRcd NotRcd</pre>	0.06 NotRcd NotRcd NotRcd NotRcd	< 10 NotRcd NotRcd NotRcd NotRcd	0.15 NotRcd NotRcd NotRcd NotRcd	260 NotRcd NotRcd NotRcd NotRcd
F15-L13 09+25 F15-L13 09+50 F15-L13 09+75 F15-L13 10+00 F15-L13 10+25	  201	  202	NotRcd NotRcd NotRcd NotRcd < 5	NotRcd NotRcd NotRcd NotRcd 0.2	NotRcd NotRcd NotRcd NotRcd 1.63	NotRcd NotRcd NotRcd NotRcd 34	NotRcd NotRcd NotRcd NotRcd 70	NotRcd NotRcd NotRcd NotRcd 0.5	NotRcd NotRcd NotRcd NotRcd < 2	NotRcd NotRcd NotRcd NotRcd 0.01	NotRcd NotRcd NotRcd NotRcd < 0.5	NotRcd NotRcd NotRcd NotRcd 16	NotRcd NotRcd NotRcd NotRcd 7	NotRed NotRed NotRed NotRed 29	NotRcd NotRcd NotRcd NotRcd 5.62	NotRcd NotRcd NotRcd NotRcd ( 10	NotRcd NotRcd NotRcd NotRcd < 1	NotRcd NotRcd NotRcd NotRcd 0.08	NotEcd NotEcd NotEcd NotEcd ( 10	NotRcd NotRcd NotRcd NotRcd 0.05	NotRcd NotRcd NotRcd NotRcd 475
F15-L13 10+50 F15-L13 10+75 F15-L13 11+00 F15-L13 11+25 F15-L13 11+50	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	< 0.2 0.2 0.2 1.2 0.6	4.72 3.34 2.62 4.36 4.36	<pre>&lt; 2 &lt; 2 16 &lt; 2 &lt; 2 &lt; 4 2</pre>	40 60 90 40 30	0.5 0.5 1.5 0.5 0.5	<pre></pre>	0.25 0.03 0.11 0.12 0.13	<pre>&lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5</pre>	7 17 11 12 6	22 24 33 33 34	16 14 32 36 15	5.37 6.03 4.50 5.56 6.67	10 10 20 30	<pre>   { 1         &lt; 1         &lt; 1         &lt; 1</pre>	0.07 0.06 0.08 0.08 0.06	10 10 10 10 30	0.48 0.32 0.43 0.43 0.38	270 3520 385 1060 335
F15-L13 11+75 F15-L13 12+00 F15-L13 12+25 F15-L13 12+50 F15-L13 12+75	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5</pre>	1.6 1.0 < 0.2 0.2 0.2	5.70 4.99 4.37 3.02 4.89	<pre> &lt; 2 &lt; 2</pre>	20 40 70 40 70	1.5 0.5 1.0 < 0.5 2.5	<pre></pre>	0.05 0.29 0.16 0.04 0.18	<pre>&lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5</pre>	4 10 16 7 8	27 31 51 63 44	10 13 27 16 19	6.28 7.85 4.69 7.31 6.23	30 30 10 20 30	<pre>&lt; 1 &lt; 1</pre>	0.05 0.06 0.05 0.08	30 10 10 < 10 30	0.13 0.63 0.58 0.69 0.53	315 435 860 370 325
F15-L13 13+00 F15-L14 05+25 F15-L14 05+50 F15-L14 05+75 F15-L14 06+00	201 201 201 201 201 201	202 202 202 202 202 202	<pre></pre>	0.2 < 0.2 0.2 < 0.2 < 0.2 < 0.2	4.12 3.64 4.78 4.25 4.91	<pre>&lt; 2 &lt; 2</pre>	40 30 20 30 40	1.5 0.5 1.5 0.5 < 0.5	4 < 2 < 2 2 4	0.23 0.06 0.06 0.18 0.40	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	6 7 7 6 8	32 37 26 36 26	6 15 13 35 19	5.54 6.22 6.50 5.25 7.61	20 30 20 10	<pre>&lt; 1 &lt; 1</pre>	0.04 0.05 0.05 0.06 0.11	10 20 30 10 < 10	0.51 0.27 0.17 0.52 0.80	185 355 375 255 265
F15-L14 06+25 F15-L14 06+50 F15-L14 06+75 F15-L14 06+75 F15-L14 07+00 F15-L14 07+25	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.6 < 0.2 0.2 0.8 0.6	3.84 4.70 4.68 5.37 4.36	<pre>&lt; 2 &lt; 2</pre>	120 160 40 30 40	0.5 0.5 1.5 0.5 0.5	< 2 < 2 < 2 4 < 2	0.11 0.15 0.08 0.14 0.05	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5	21 21 15 19 7	34 30 28 28 36	20 35 14 19 20	5.80 6.45 6.12 6.52 5.89	10 10 30 20 10	<pre>&lt; 1 &lt; 1 &lt; 1 &lt; 1 &lt; 1 &lt; 1 &lt; 1</pre>	0.03 0.04 0.04 0.05 0.05	20 10 20 40 10	0.71 0.82 0.25 0.35 0.34	1045 1435 1345 1255 520

CERTIFICATION:\_\_

HartBuchler



Analytical Chemists \* Geochemists \* Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218 To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9

CERTIFICATE OF ANALYSIS

Page Number : 3-B Total Pages :9 Certificate Date: 06-OCT-96 Invoice No. : 19633567 P.O. Number :8026 Account :KBOA

10633567

Project : FD6CA0052 Comments:

																A3000001
SAMPLE	PREP CODE	Mo ppm	Na %	Ni ppa	P mege	Pb ppm	Sb ppm	Sc ppm	Sr ppm	Ti %	Tl PPm	U ppm	V ppm	W ppm	Zn ppm	
F15-L13 05+25 F15-L13 05+50 F15-L13 05+75 F15-L13 06+00 F15-L13 06+25	201 20 201 20 201 20 201 20 201 20 201 20	2 5 2 4 2 3 2 3 2 3 2 2	0.03 0.05 0.05 < 0.01 0.01	5 5 14 10 17	1050 1060 1120 1260 1760	12 8 12 8 16	2 2 2 4 2 2 2	6 7 4 6	11 16 21 11 19	0.38 0.42 0.38 0.30 0.29	< 10 < 10 < 10 < 10 < 10 < 10	< 10 < 10 < 10 < 10 < 10	88 96 125 111 121	<pre>&lt; 10 &lt; 10</pre>	68 58 84 54 122	
F15-L13 06+50 F15-L13 06+75 F15-L13 07+00 F15-L13 07+50 F15-L13 07+75	201 20 201 20 201 20 201 20 201 20 201 20	2 4 2 4 2 4 2 3 2 3	0.04 0.03 0.01 0.01 0.03	12 13 21 15 9	1260 1200 1390 1750 1330	8 10 8 6 4	<pre></pre>	6 9 3 3 6	15 15 9 18 26	0.33 0.34 0.04 0.26 0.46	<pre>&lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10</pre>	82 102 94 114 133	<pre>&lt; 10 &lt; 10</pre>	72 104 158 86 66	
F15-L13 08+00 F15-L13 08+25 F15-L13 08+50 F15-L13 08+75 F15-L13 09+00	201 20   	2 4 NotRcd NotRcd NotRcd NotRcd	< 0.01 NotRcd NotRcd NotRcd NotRcd	32 NotRcd NotRcd NotRcd NotRcd	1070 NotRcd NotRcd NotRcd NotRcd	14 NotRcd NotRcd NotRcd NotRcd	6 NotRcd NotRcd NotRcd NotRcd	5 NotRcd NotRcd NotRcd NotRcd	12 NotRcd NotRcd NotRcd NotRcd	0.02 NotRcd NotRcd NotRcd NotRcd	<pre>&lt; 10 NotRcd NotRcd NotRcd NotRcd NotRcd</pre>	<pre>&lt; 10 NotRcd NotRcd NotRcd NotRcd NotRcd</pre>	93 NotRcd NotRcd NotRcd NotRcd	<pre>&lt; 10 NotRcd NotRcd NotRcd NotRcd NotRcd</pre>	82 NotRcd NotRcd NotRcd NotRcd	
F15-L13 09+25 F15-L13 09+50 F15-L13 09+75 F15-L13 10+00 F15-L13 10+25	   201 20	NotRcd NotRcd NotRcd NotRcd 2 1	NotRcd NotRcd NotRcd NotRcd ( 0.01	NotRcd NotRcd NotRcd NotRcd 14	NotRcd NotRcd NotRcd NotRcd 1350	NotRcd NotRcd NotRcd NotRcd 26	NotRcd NotRcd NotRcd NotRcd 6	NotRcd NotRcd NotRcd NotRcd 5	NotRcd NotRcd NotRcd NotRcd 4	NotRcd NotRcd NotRcd NotRcd < 0.01	NotRcd NotRcd NotRcd NotRcd ( 10	NotRcd NotRcd NotRcd NotRcd < 10	NotRcd NotRcd NotRcd NotRcd 24	NotRcd NotRcd NotRcd NotRcd < 10	NotRcd NotRcd NotRcd NotRcd 82	
F15-L13 10+50 F15-L13 10+75 F15-L13 11+00 F15-L13 11+25 F15-L13 11+50	201 20 201 20 201 20 201 20 201 20 201 20	2 2 2 5 2 3 2 6 2 4	0.05 < 0.01 0.01 0.02 0.01	6 12 29 23 11	1310 810 930 1910 950	6 10 12 10 10	2 2 2 2 2 2 4 2	9 4 5 9 8	24 7 14 13 14	0.54 0.13 0.05 0.33 0.48	< 10 < 10 < 10 < 10 < 10 < 10	< 10 < 10 < 10 < 10 < 10 < 10	127 51 45 88 103	< 10 < 10 < 10 < 10 < 10 < 10	58 74 134 180 72	
F15-L13 11+75 F15-L13 12+00 F15-L13 12+25 F15-L13 12+50 F15-L13 12+75	201 20 201 20 201 20 201 20 201 20 201 20	2 6 2 3 2 2 2 3 2 3 2 1	0.03 0.06 0.01 < 0.01 < 0.01	6 15 26 41 32	870 1020 1150 640 1320	14 6 10 8 8	2 2 2 2 2 2	5 8 7 3 7	7 29 15 8 18	0.24 0.49 0.21 0.13 0.32	< 10 < 10 < 10 < 10 < 10 < 10	<pre>&lt; 10 &lt; 10</pre>	46 106 79 80 94	< 10 < 10 < 10 < 10 < 10 < 10	60 56 84 60 98	
F15-L13 13+00 F15-L14 05+25 F15-L14 05+50 F15-L14 05+75 F15-L14 06+00	201 20 201 20 201 20 201 20 201 20 201 20	2 3 2 4 2 5 2 3 2 1	0.01 < 0.01 0.01 0.01 0.10	9 11 6 11 9	940 770 910 1220 1510	8 16 12 14 2	< 2 2 4 2 4	7 6 5 8 13	25 8 7 16 38	0.64 0.34 0.27 0.43 0.79	<pre>&lt; 10 &lt; 10</pre>	< 10 < 10 < 10 < 10 < 10 < 10	120 97 63 120 163	<pre>&lt; 10 &lt; 10</pre>	42 70 68 70 56	
F15-L14 06+25 F15-L14 06+50 F15-L14 06+75 F15-L14 06+75 F15-L14 07+00 F15-L14 07+25	201 20 201 20 201 20 201 20 201 20 201 20	2 3 2 3 2 5 2 6 2 5	< 0.01 0.01 0.01 0.01 < 0.01	15 12 11 11 19	1470 1570 1180 1440 1550	12 6 12 10 12	2 2 4 2 < 2	4 6 4 8 4	13 17 10 17 8	0.21 0.18 0.28 0.40 0.12	< 10 < 10 < 10 < 10 < 10 < 10	< 10 < 10 < 10 < 10 < 10 < 10	140 159 81 98 80	< 10 < 10 < 10 < 10 < 10 < 10	96 108 122 168 120	
														CERTIE		Sant Buchler

CERTIFICATION:\_



Analytical Chemists \* Geochemists \* Registered Assayers

212 Brooksbank Ave.,North VancouverBritish Columbia, CanadaV7J 2C1PHONE: 604-984-0221FAX: 604-984-0218

To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9 Page Number :4-A Total Pages :9 Certificate Date: 06-OCT-96 Invoice No. :19633567 P.O. Number :8026 Account :KBOA

Project : FD6CA0052 Comments:

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										CE	RTIFI	CATE	OF A	NAL	/SIS		9633	567		
SAMPLE	PREP CODE	Au-AA ppb	Ag PP <b>a</b>	Al %	As ppm	Ba pp <b>n</b>	Be ppm	Bi PP <b>m</b>	Ca %	Cđ ppm	Co ppm	Cr ppz	Cu pp <b>n</b>	Fe %	Ga ppm	Hg ppm	K %	La ppm	Mg %	Mn ppm
F15-L14 07+50 F15-L14 07+75 F15-L14 08+00 F15-L14 08+25 F15-L14 08+50	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	< 0.2 < 0.2 < 0.2 < 0.2 0.2 0.2	5.33 3.99 4.53 2.67 2.58	<pre>&lt; 2 &lt; 2 &lt; 2 &lt; 2 2 20</pre>	30 30 30 50 90	1.5 < 0.5 0.5 0.5 0.5	<pre>&lt; 2 &lt; 2</pre>	0.07 0.20 0.17 0.09 0.14	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	7 10 12 22 19	29 28 26 21 15	12 18 18 46 62	6.07 5.71 6.58 6.32 5.41	20 10 20 10 < 10	<pre>&lt; 1 &lt; 1</pre>	0.05 0.07 0.05 0.06 0.08	20 < 10 10 10 10	0.21 0.58 0.49 0.34 0.27	305 555 660 1690 1260
F15-L14 08+75 F15-L14 09+00 F15-L14 11+75 F15-L14 12+00 F15-L14 12+25	201 202 201 202 201 202 201 202 201 202 201 202	<pre></pre>	< 0.2 < 0.2 0.6 0.6 < 0.2	3.99 4.36 5.26 3.38 4.11	<pre>&lt; 2 &lt; 2</pre>	40 40 30 40 70	<pre>&lt; 0.5 &lt; 0.5 1.0 0.5 0.5</pre>	<pre> &lt; 2 &lt; 2</pre>	0.22 0.30 0.05 0.06 0.08	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	10 7 4 11 9	28 34 33 44 60	24 21 13 21 16	6.38 5.90 5.47 4.95 5.05	10 10 20 10 10	<pre>&lt; 1 &lt; 1</pre>	0.08 0.08 0.05 0.06 0.08	10 < 10 20 10 10	0.63 0.61 0.33 0.73 0.66	425 240 250 525 450
P15-L14       12+50         P15-L14       12+75         P15-L15       04+75         P15-L15       05+00         P15-L15       05+25	201 202 201 202 201 202 201 202 201 202 201 202	<pre></pre>	< 0.2 < 0.2 1.2 3.0 0.2	4.66 5.04 3.66 3.82 4.50	< 2 < 2 74 20 60	40 50 50 70 50	0.5 0.5 < 0.5 1.0 0.5	<pre>&lt; 2 &lt; 2</pre>	0.20 0.27 0.08 0.93 0.28	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	4 9 9 19 15	32 34 27 43 27	15 35 27 140 14	4.09 6.29 7.95 5.45 5.93	20 20 20 10 10	< 1 < 1 < 1 < 1 < 1 < 1	0.06 0.07 0.03 0.13 0.05	20 < 10 < 10 < 10 10 < 10	0.37 0.85 0.51 0.46 0.59	155 355 905 4090 1315
F15-L15 05+50 F15-L15 06+00 F15-L15 06+25 F15-L15 06+50 F15-L15 06+75	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.2 < 0.2 < 0.2 < 0.2 < 0.2 0.2	2.58 4.87 4.91 3.67 4.28	18 < 2 < 2 6 < 2	50 30 40 70 10	<pre>&lt; 0.5 0.5 &lt; 0.5 &lt; 0.5 0.5 0.5</pre>	<pre>&lt; 2 &lt; 2</pre>	0.03 0.28 0.31 0.05 0.11	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	5 6 10 5	31 27 23 15 21	19 12 14 57 4	7.08 5.31 5.83 5.03 6.33	20 10 10 < 10 30	<pre>&lt; 1 &lt; 1</pre>	0.06 0.06 0.07 0.07 0.06	10 10 10 10 30	0.20 0.63 0.60 0.10 0.32	385 185 205 580 420
F15-L15 07+00 F15-L15 07+25 F15-L15 07+50 F15-L15 07+75 F15-L15 08+00	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.2 0.6 0.4 < 0.2 1.8	5.41 6.87 5.31 5.31 4.64	< 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2	40 20 30 50 40	1.0 2.0 0.5 1.0 0.5	<pre>&lt; 2 &lt; 2</pre>	0.27 0.07 0.25 0.27 0.15	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	13 6 17 12 7	36 16 39 31 27	24 < 1 21 17 14	6.52 6.16 6.85 6.73 5.57	20 30 20 20 10	<pre>&lt; 1 &lt; 1</pre>	0.08 0.05 0.06 0.05 0.04	10 30 10 10 10	0.53 0.13 0.59 0.63 0.40	685 625 995 490 325
F15-L15 08+25 F15-L15 08+50 F15-L15 08+75 F15-L15 09+00 F15-L15 09+25	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 10</pre>	0.8 0.6 1.6 0.4 < 0.2	4.06 5.82 3.52 3.07 3.40	<pre>&lt; 2 &lt; 2 &lt; 2 &lt; 2 &lt; 2 &lt; 2 &lt; 14</pre>	90 40 60 70 60	0.5 1.5 0.5 0.5 1.5	<pre>&lt; 2 &lt; 2</pre>	0.08 0.11 0.08 0.09 0.15	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	11 7 17 13 32	40 23 35 27 20	29 16 42 235 213	6.36 5.91 6.35 5.93 6.87	10 30 10 10 10	<pre>&lt; 1 &lt; 1</pre>	0.07 0.06 0.08 0.09 0.08	10 40 10 < 10 10	0.50 0.23 0.34 0.62 1.24	645 405 1135 1185 2170
F15-L15 09+50 F15-L15 09+75 F15-L15 10+00 F15-L15 10+25 F15-L15 10+50	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	( 0.2 0.2 0.2 0.8 0.8	4.68 4.43 3.38 2.71 2.86	<pre></pre>	60 50 50 100 130	0.5 0.5 0.5 < 0.5 < 0.5 0.5	<pre></pre>	0.12 0.05 0.06 0.14 0.06	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	7 11 14 10 8	37 34 39 30 13	23 25 23 14 32	6.22 5.78 4.76 5.99 4.09	10 20 10 10 < 10	<pre>&lt; 1 &lt; 1</pre>	0.03 0.06 0.07 0.08 0.08	10 20 10 < 10 < 10	0.31 0.27 0.59 0.40 0.13	310 1050 1130 750 685
F15-L15 10+75 F15-L15 11+00 F15-L15 11+25 F15-L15 11+50 F15-L15 11+75	201 202 201 202 201 202 201 202 201 202 201 202	<pre>&lt; 5 &lt; 5 </pre>	2.4 1.6 1.6 1.2 1.4	5.26 4.36 4.76 4.24 3.43	< 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2	40 20 30 70 60	1.5 0.5 1.0 0.5 0.5	<pre>&lt; 2 &lt; 2</pre>	0.10 0.08 0.13 0.23 0.17	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	7 5 8 21 14	30 29 16 23 26	11 12 9 25 20	6.39 6.58 6.03 5.59 5.11	30 30 20 10 10	< 1 < 1 < 1 < 1 < 1 < 1 < 1	0.05 0.06 0.05 0.07 0.06	20 20 10 10 < 10	0.14 0.18 0.26 0.72 0.52	565 600 405 1555 1140

CERTIFICATION: StartBuchler



Analytical Chemists \* Geochemists \* Registered Assayers

212 Brooksbank Ave. North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218 To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9

Page Number :4-B Total Pages :9 Certificate Date: 06-OCT-96 Invoice No. : 19633567 P.O. Number :8026 :KBOA Account

Project : FD6CA0052 Comments:

										CE	RTIF	CATE	OF A	NALY	SIS	A9633567
SAMPLE	PREP CODE	Мо ррш	Na %	Ni ppm	ppm P	Pb pp <b>n</b>	Sb ppm	Sc ppm	Sr ppm	Ti %	T1 ppm	U PPm	V ppm	W PPm	Zn ppm	
F15-L14 07+50 F15-L14 07+75 F15-L14 08+00 F15-L14 08+25 F15-L14 08+50	201 202 201 202 201 202 201 202 201 202 201 202	5 3 4 5 4	0.01 0.03 0.02 0.01 0.03	8 16 11 13 20	1200 1120 910 1690 1780	12 6 6 10 12	2 2 2 2 4		9 20 19 11 17	0.32 0.40 0.45 0.12 0.08	<pre>&lt; 10 &lt; 10</pre>	< 10 < 10 < 10 < 10 < 10 < 10	77 107 108 102 72	< 10 < 10 < 10 < 10 < 10 < 10	84 78 64 118 124	
F15-L14 08+75 F15-L14 09+00 F15-L14 11+75 F15-L14 12+00 F15-L14 12+25	201 202 201 202 201 202 201 202 201 202 201 202	4 3 4 3 3	0.05 0.06 (0.01 (0.01 (0.01	16 12 21 42 38	1290 1240 1000 620 980	8 4 6 8 10	2 2 2 4 2	10 10 4 3 4	23 30 8 12 12	0.46 0.49 0.11 0.13 0.11	<pre>&lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10</pre>	120 124 37 61 61	<pre>&lt; 10 &lt; 10</pre>	112 68 60 84 82	
P15-L14       12+50         F15-L14       12+75         £15-L15       04+75         F15-L15       05+00         F15-L15       05+25	201 202 201 202 201 202 201 202 201 202 201 202	2 2 4 6 2	0.03 0.05 (0.01 0.04 0.03	16 24 4 34 10	1100 1390 1560 4150 1400	4 6 30 40 12	2 2 4 6 6	8 12 4 9 5	23 29 15 35 28	0.56 0.65 0.23 0.12 0.46	<pre>&lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10</pre>	108 132 172 105 121	<pre>&lt; 10 &lt; 10</pre>	66 74 40 164 78	
F15-L15 05+50 F15-L15 06+00 F15-L15 06+25 F15-L15 06+50 F15-L15 06+75	201 202 201 202 201 202 201 202 201 202 201 202	5 2 1 5 6	<pre>&lt; 0.01 0.04 0.06 0.01 0.02</pre>	12 8 7 8 10	1050 1100 1120 680 760	24 < 2 2 18 10	2 2 6 2 2	2 10 8 5 5	8 24 28 7 10	0.20 0.72 0.66 0.04 0.35	<pre>&lt; 10 &lt; 10</pre>	< 10 < 10 < 10 < 10 < 10 < 10	139 132 121 37 67	<pre>&lt; 10 &lt; 10</pre>	82 38 38 94 68	
P15-L15 07+00 P15-L15 07+25 P15-L15 07+50 P15-L15 07+75 P15-L15 08+00	201 202 201 202 201 202 201 202 201 202 201 202	4 6 4 2 5	0.05 0.04 0.04 0.04 0.01	10 6 10 9 11	1200 930 1220 1070 1140	8 10 6 4 4	2 2 4 2 2	10 4 9 9 5	26 8 24 27 16	0.54 0.17 0.57 0.54 0.36	<pre>&lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10</pre>	131 25 143 147 155	<pre>&lt; 10 &lt; 10</pre>	74 64 84 74 82	
F15-L15       08+25         F15-L15       08+50         F15-L15       08+75         F15-L15       09+00         F15-L15       09+25	201 202 201 202 201 202 201 202 201 202 201 202	6 5 5 6 6	0.01 0.02 0.01 0.01 ( 0.01	19 7 11 15 14	1360 1500 1170 2300 2200	16 10 12 18 26	2 2 2 4 4	4 5 4 5 12	14 13 12 10 13	0.14 0.27 0.24 0.03 0.01	<pre>&lt; 10 &lt; 10</pre>	< 10 < 10 < 10 < 10 < 10 < 10	125 56 132 110 130	<pre>&lt; 10 &lt; 10</pre>	150 82 80 118 104	
F15-L15 09+50 F15-L15 09+75 F15-L15 10+00 F15-L15 10+25 F15-L15 10+50	201 202 201 202 201 202 201 202 201 202 201 202	4 4 3 4 3	< 0.01 0.01 < 0.01 0.04 0.01	14 16 35 16 6	1330 910 1460 960 1100	8 14 10 8 6	<pre></pre>	4 4 3 5	10 9 10 20 9	0.24 0.18 0.20 0.17 < 0.01	<pre>&lt; 10 &lt; 10</pre>	< 10 < 10 < 10 < 10 < 10 < 10	84 58 65 82 44	<pre>&lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10</pre>	52 98 98 62 98	
F15-L15 10+75 F15-L15 11+00 F15-L15 11+25 F15-L15 11+25 F15-L15 11+50 F15-L15 11+75	201 202 201 202 201 202 201 202 201 202 201 202	5 6 4 3 2	0.01 0.04 0.05 0.05 0.03	6 7 5 12 16	1220 1000 840 1610 1070	10 12 8 6 4	2 2 2 2 2 4 2	5 4 5 8 4	12 11 14 23 17	0.32 0.33 0.36 0.49 0.33	<pre>&lt; 10 &lt; 10</pre>	< 10 < 10 < 10 < 10 < 10 < 10	74 71 70 126 101	<pre>&lt; 10 &lt; 10</pre>	84 74 54 100 78	
<u> </u>											<del></del> .			CERTIFIC		Sart Bichler

CERTIFICATION:

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#### Chemex Labs Ltd. Analytical Chemists \* Geochemists \* Registered Assayers

British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218

North Vancouver

212 Brooksbank Ave.,

To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9

Page Number :5-A Total Pages :9 Certificate Date: 06-OCT-96 Invoice No. : 19633567 P.O. Number :8026 :KBOA Account

Project : Comments: FD6CA0052

											CE	RTIFI	CATE	OF A	NAL	<u>YSIS</u>	/	A9633	567		
SAMPLE	PRE COD	P E	Au-AA ppb	Ag ppm	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cd pp∎	Co pp <del>a</del>	Cr ppm	Cu ppm	Fe %	Ga ppm	Edd Hd	K %	La ppm	Mg %	Mn ppm
F15-L15 12+25 F15-L15 12+50 F15-L15 12+75 F15-L15 13+25 F15-L15 13+50	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 65 &lt; 5 &lt; 5 &lt; 5</pre>	0.6 0.2 0.4 0.2 1.4	4.76 3.29 3.37 3.81 2.87	<pre>&lt; 2 14 16 &lt; 2 &lt; 2 &lt; 2</pre>	30 80 70 40 40	1.0 0.5 1.5 0.5 < 0.5	<pre>&lt; 2 &lt; 2</pre>	0.05 0.11 0.11 0.20 0.05	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	20 11 20 4 10	31 34 23 22 22	12 24 39 9 15	6.78 7.76 5.56 5.26 5.07	30 10 10 10 10	<pre>&lt; 1 &lt; 1</pre>	0.06 0.09 0.08 0.04 0.07	30 < 10 10 10 < 10	0.19 0.39 0.77 0.27 0.35	2000 575 1855 120 830
F15-L15 14+00 F15-L15 14+25 F15-L15 14+50 F15-L16 05+25 F15-L16 05+50	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	< 0.2 < 0.2 0.2 1.0 < 0.2	4.41 3.77 3.21 4.26 4.51	<pre></pre>	50 80 40 50 30	0.5 1.0 0.5 0.5 1.0	<pre>&lt; 2 &lt; 2</pre>	0.21 0.04 0.14 0.09 0.10	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	8 22 12 10 16	25 47 22 41 36	12 42 15 42 23	4,95 5.67 4.90 6.87 7.44	10 10 10 20 30	<pre>&lt; 1 &lt; 1</pre>	0.05 0.08 0.08 0.04 0.05	<pre>&lt; 10     20     &lt; 10     10     10     30</pre>	0.52 0.81 0.41 0.41 0.26	340 1665 535 760 1910
F15-L16 06+00 F15-L16 06+25 F15-L16 06+50 F15-L16 06+75 F15-L16 07+00	201 201 201 201 201 201	202 202 202 202 202 202	< 5 < 5 < 5 < 5 < 5 < 5	0.2 < 0.2 < 0.2 < 0.2 0.2 0.2	4.24 2.73 4.22 4.38 4.47	<pre></pre>	20 50 70 20 30	0.5 < 0.5 0.5 0.5 0.5	<pre>&lt; 2 &lt; 2</pre>	0.20 0.08 0.08 0.16 0.24	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	6 6 15 8 8	23 33 78 38 27	12 14 16 21 25	6.56 7.31 6.52 7.49 7.02	30 30 10 30 20	<pre>&lt; 1 &lt; 1</pre>	0.06 0.04 0.04 0.05 0.06	20 10 < 10 20 20	0.40 0.29 0.49 0.39 0.77	310 670 1770 430 380
F15-L16 07+25 F15-L16 07+50 F15-L16 07+75 F15-L16 08+00 F15-L16 08+50	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.2 0.2 < 0.2 0.2 < 0.2 < 0.2	5.05 5.17 3.99 4.68 4.14	<pre></pre>	10 70 60 40 50	1.0 1.0 0.5 1.5 0.5	<pre>&lt; 2 &lt; 2</pre>	0.10 0.42 0.11 0.12 0.23	<pre>&lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5 &lt; 0.5</pre>	11 16 21 18 17	34 24 30 26 24	15 29 19 9 16	7.30 6.84 6.25 6.08 6.03	30 10 10 20 20	<pre>&lt; 1 &lt; 1</pre>	0.05 0.10 0.06 0.05 0.07	30 10 10 40 10	0.18 0.85 0.41 0.27 0.61	685 550 1405 1925 1380
F15-L16 08+75 F15-L16 09+00 F15-L16 09+50 F15-L16 09+75 F15-L16 10+00	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	< 0.2 0.2 1.4 2.0 0.4	5.04 3.23 3.22 2.91 4.22	<pre></pre>	30 70 30 90 100	0.5 0.5 < 0.5 0.5 0.5 0.5	<pre>&lt; 2 &lt; 2</pre>	0.29 0.08 0.12 0.12 0.27	< 0.5 < 0.5 < 0.5 0.5 0.5 0.5	15 19 5 7 10	24 36 25 17 27	16 17 9 28 19	6.38 5.45 7.72 4.60 5.29	10 10 30 < 10 10	<pre>&lt; 1 &lt; 1</pre>	0.06 0.05 0.05 0.06 0.06	10 10 10 < 10 10	0.79 0.44 0.30 0.29 0.48	800 1250 255 515 490
F15-L16 10+25 F15-L16 10+50 F15-L16 10+75 F15-L16 11+00 F15-L16 11+25	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.2 < 0.2 0.6 0.8 0.8	4.14 2.75 4.33 4.39 2.91	<pre></pre>	40 130 30 10 50	0.5 0.5 0.5 0.5 < 0.5 < 0.5	<pre> &lt; 2 &lt; 2</pre>	0.07 0.10 0.08 0.03 0.20	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	9 21 8 3 7	39 12 34 23 22	12 48 17 13 13	5.74 7.00 7.40 7.24 5.28	10 < 10 30 30 10	<pre>&lt; 1 &lt; 1</pre>	0.04 0.12 0.06 0.05 0.05	10 10 40 30 < 10	0.40 0.11 0.19 0.08 0.43	535 1415 545 260 400
F15-L16 11+50 F15-L16 11+75 F15-L16 12+25 F15-L16 12+50 F15-L16 13+00	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	1.2 1.0 0.6 < 0.2 < 0.2	2.76 3.96 4.78 4.56 4.10	14 < 2 < 2 < 2 < 2 < 2 < 2	70 40 10 50 40	<pre>&lt; 0.5 0.5 0.5 0.5 1.5</pre>	<pre> &lt; 2 &lt; 2</pre>	0.04 0.09 0.06 0.28 0.17	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	5 15 3 7 10	15 36 30 24 30	22 19 6 16 14	6.11 6.17 6.95 4.93 6.02	< 10 20 30 10 30	<pre>&lt; 1 &lt; 1</pre>	0.07 0.06 0.03 0.04 0.06	<pre>&lt; 10     10     20     10     50</pre>	0.08 0.38 0.17 0.52 0.54	375 895 295 270 535
F15-L16 13+50 F15-L16 13+75 F15-L16 14+00 F15-L17 05+00 F15-L17 05+25	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 </pre>	0.2 0.2 < 0.2 0.4 0.2	5.36 5.03 5.71 4.32 5.03	<pre>&lt; 2 &lt; 2</pre>	30 40 50 30 60	2.0 2.5 1.5 0.5 2.0	<pre>&lt; 2 &lt; 2</pre>	0.15 0.39 0.55 0.20 0.19	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 1.0	4 8 7 14 5	21 22 24 22 19	5 13 14 16 12	5.15 6.36 6.11 6.70 6.03	30 10 20 20 30	<pre>&lt; 1 &lt; 1</pre>	0.04 0.05 0.06 0.04 0.04	40 30 10 < 10 40	0.11 0.78 0.74 0.58 0.13	145 225 225 815 405
	<b>L</b>										· · · · ·						R	Jan	12	SI	en.

CERTIFICATION:

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Analytical Chemists \* Geochemists \* Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218 To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9

Page Number :5-B Total Pages :9 Certificate Date: 06-OCT-96 Invoice No. : 19633567 P.O. Number :8026 Account :KBOA

Project : FD6CA0052 Comments:

										CE	RTIFI	CATE	OF A	NALY	<b>SIS</b>	A9633567
SAMPLE	PREP CODE	Мо ррш	Na %	Ni ppm	P PPm	Pb ppm	Sb ppm	Sc ppm	Sr ppm	Ti %	Tl ppm	U PP <b>a</b>	V PP <b>n</b>	W PPm	Zn ppm	
P15-L15 12+25 P15-L15 12+50 P15-L15 12+75 P15-L15 13+25 P15-L15 13+50	201 202 201 202 201 202 201 202 201 202 201 202	5 4 < 5 1 2 <	0.02 0.01 0.01 0.01 0.01	8 16 16 7 8	930 1460 2040 1100 1130	14 24 104 8 8	2 { 2 2 2 2	4 3 5 6 2	9 14 11 23 8	0.29 0.07 0.09 0.55 0.08	<pre>&lt; 10 &lt; 10</pre>	< 10 < 10 < 10 < 10 < 10 < 10	71 97 77 116 72	<pre>&lt; 10 &lt; 10</pre>	96 74 158 40 64	
F15-L15 14+00 F15-L15 14+25 F15-L15 14+50 F15-L16 05+25 F15-L16 05+50	201 202 201 202 201 202 201 202 201 202 201 202	2 3 3 6 < 10	0.03 0.01 0.03 0.01 0.01	10 53 10 19 7	1010 780 940 1140 1120	2 16 8 42 14	2 4 < 2 4 2	5 6 5 6 8	19 10 15 11 13	0.33 0.06 0.20 0.18 0.38	< 10 < 10 < 10 < 10 < 10 < 10	< 10 < 10 < 10 < 10 < 10 < 10 < 10	100 50 87 107 112	< 10 < 10 < 10 < 10 < 10 < 10	64 172 76 134 94	
F15-L16 06+00 F15-L16 06+25 F15-L16 06+50 F15-L16 06+75 F15-L16 07+00	201 202 201 202 201 202 201 202 201 202 201 202	5 4 < 3 < 4 3	0.06 0.01 0.01 0.02 0.06	5 11 27 6 10	800 620 850 860 830	10 14 14 12 6	2 2 2 < 2 2	7 4 9 9	19 12 12 16 24	0.43 0.47 0.32 0.51 0.47	< 10 < 10 < 10 < 10 < 10 < 10	<pre>&lt; 10 &lt; 10</pre>	87 144 131 124 122	<pre>&lt; 10 &lt; 10</pre>	48 62 92 50 44	
P15-L16 07+25 P15-L16 07+50 P15-L16 07+75 P15-L16 08+00 P15-L16 08+50	201 202 201 202 201 202 201 202 201 202 201 202	6 3 4 5 5	0.04 0.10 0.01 0.01 0.04	5 14 11 12 11	1110 1450 1250 1630 1030	12 6 10 14 8	2 4 2 2 4	6 12 7 5 5	10 43 13 14 25	0.35 0.72 0.28 0.24 0.44	<pre>&lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10</pre>	88 138 125 74 126	<pre>&lt; 10 &lt; 10</pre>	84 128 118 120 80	
F15-L16 08+75 F15-L16 09+00 F15-L16 09+50 F15-L16 09+75 F15-L16 10+00	201 202 201 202 201 202 201 202 201 202 201 202	4 5 < 7 8 4	0.05 0.01 0.03 0.01 0.03	11 23 4 11 12	1170 1490 630 1600 1430	2 14 14 8 6	2 2 2 2 2 2	8 3 5 4 8	28 11 12 15 25	0.57 0.08 0.36 0.19 0.40	<pre>&lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10</pre>	139 90 109 84 116	<pre>&lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10</pre>	68 182 60 154 112	
F15-L16 10+25 F15-L16 10+50 F15-L16 10+75 F15-L16 11+00 F15-L16 11+25	201 202 201 202 201 202 201 202 201 202 201 202	4 1 5 6 3	0.01 0.01 0.03 0.01 0.02	24 11 7 < 1 7	910 1840 930 990 1240	12 18 12 14 6	2 2 < 2 2 2 2	4 7 7 5 3	9 11 4 10 6 20	0.18 ( 0.01 0.36 0.34 0.46	<pre>&lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10</pre>	54 39 91 63 127	< 10 < 10 < 10 < 10 < 10 < 10	82 122 128 76 54	
F15-L16 11+50 F15-L16 11+75 F15-L16 12+25 F15-L16 12+50 F15-L16 13+00	201 202 201 202 201 202 201 202 201 202 201 202 201 202	6 < 4 5 1 4	0.01 0.02 0.01 0.04 0.04	13 13 7 9 10	1370 980 750 990 930	2 12 12 ( 2 10	2 2 2 2 6	3 6 5 6 8	6 12 7 24 16	0.02 0.27 0.16 0.49 0.53	<pre>&lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10</pre>	40 86 35 113 112	<pre>&lt; 10 &lt; 10</pre>	124 80 40 58 52	
P15-L16 13+50 P15-L16 13+75 P15-L16 14+00 P15-L17 05+00 P15-L17 05+25	201 202 201 202 201 202 201 202 201 202 201 202	12 3 3 2 6	0.01 0.06 0.06 0.04 0.03	10 9 10 9 5	720 960 990 1150 730	16 < 2 2 8 12	2 2 6 2 6	5 9 10 7 <b>4</b>	17 35 48 22 15	0.27 0.69 0.60 0.53 0.21	<pre>&lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10</pre>	39 131 111 165 48	< 10 < 10 < 10 < 10 < 10 < 10	96 46 48 48 108	

**CERTIFICATION:** 

tart Brokler



Analytical Chemists \* Geochemists \* Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218 To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9 Page Number :6-A Total Pages :9 Certificate Date: 06-OCT-96 Invoice No. : 19633567 P.O. Number :8026 Account :KBOA

Project : FD6CA0052 Comments:

m											C	ERTIF	ICAT	EOF	ANAL	YSIS		A9633	3567		
SAMPLE	PRI COI	ep De	Au-AA ppb	Ag ppm	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cć pp	i Co ppm	Cr ppm	Cu ppm	Fe %	Ga ppm	Hg Ngg	К %	La ppm	Mg %	Mn ppm
F15-L17 05+50 F15-L17 05+75 F15-L17 06+00 F15-L17 06+25 F15-L17 06+50 F15-L17 06+50	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.6 0.6 0.2 0.2 < 0.2	4.04 2.00 4.22 4.08 5.28	2 26 < 2 < 2 < 2 < 2	80 60 10 10 90	1.5 0.5 0.5 1.0 1.5	<pre>&lt; 2 &lt; 2</pre>	0.32 0.02 0.07 0.06 0.35	< 0.5 < 0.5 < 0.5 < 0.5	5 21 5 17 5 2 5 1 5 1 7 5 17	26 20 35 9 28	27 87 19 4 31	6.73 5.36 9.87 5.48 6.49	10 < 10 40 20 20	<pre>&lt; 1 &lt; 1</pre>	0.08 0.05 0.04 0.08 0.10	30 10 20 30 20	0.49 0.38 0.17 0.08 0.73	2040 2110 350 385 970
F15-L17 06+75 F15-L17 07+00 F15-L17 07+25 F15-L17 07+50 F15-L17 07+75	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.2 0.2 < 0.2 0.2 < 0.2 < 0.2	5.11 5.35 5.41 3.87 3.66	< 2 < 2 < 2 < 2 < 2 < 2	10 40 40 50 10	0.5 0.5 < 0.5 0.5 0.5	<pre> &lt; 2 &lt; 2</pre>	0.04 0.33 0.36 0.13 0.10	< 0.5 < 0.5 < 0.5 < 0.5	5 7 5 8 5 7 5 8 5 8	15 27 26 31 23	12 19 19 22 11	5.65 6.69 6.04 4.76 8.08	20 20 10 20 30	<pre>&lt; 1 &lt; 1</pre>	0.05 0.07 0.06 0.09 0.08	20 10 10 10 20	0.06 0.63 0.78 0.42 0.24	1220 315 225 505 705
F15-L17 08+00 F15-L17 08+25 F15-L17 08+50 F15-L17 08+75 F15-L17 09+00	201 201 201 201 201 201	202 202 202 202 202 202	<pre></pre>	0.4 3.4 0.2 0.2 < 0.2	5.24 4.22 4.33 2.68 2.22	< 2 8 < 2 16 12	30 40 40 50 110	1.5 2.0 1.0 0.5 0.5	<pre></pre>	0.15 0.05 0.08 0.04 0.07	< 0.5 < 0.5 < 0.5 < 0.5	5 5 5 6 5 13 5 17 5 23	18 31 24 20 17	31 23 19 57 117	6.33 5.27 6.20 7.29 6.28	20 20 20 10 < 10	<pre></pre>	0.09 0.06 0.05 0.08 0.11	10 30 20 10 20	0.29 0.36 0.31 0.19 0.25	275 260 1445 1510 1735
F15-L17 09+25 F15-L17 09+50 F15-L17 09+75 F15-L17 10+00 F15-L17 10+75	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.2 < 0.2 0.8 1.4 0.8	2.28 3.51 3.27 3.03 4.98	18 < 2 2 4 < 2	90 60 100 80 80	0.5 1.5 0.5 0.5 0.5	<pre></pre>	0.10 0.24 0.09 0.06 0.35	< 0. < 0. < 0. < 0.	5 15 5 12 5 11 5 11 5 10	12 37 27 23 23	66 28 19 26 27	4.90 5.18 7.90 5.97 6.14	< 10 10 10 10 10	<pre></pre>	0.09 0.07 0.05 0.09 0.11	10 30 30 10 < 10	0.13 0.85 0.26 0.25 0.67	1025 605 855 655 650
F15-L17 11+00 F15-L17 11+50 F15-L17 11+75 F15-L17 11+75 F15-L17 12+00 F15-L17 12+25	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.8 5.6 0.2 < 0.2 < 0.2	5.04 4.94 4.20 1.28 3.13	<pre>&lt; 2 &lt; 2</pre>	50 120 40 80 120	0.5 2.0 < 0.5 0.5 < 0.5	<pre>&lt; 2 &lt; 2</pre>	0.25 0.16 0.34 0.07 0.08	< 0. 4. < 0. < 0. < 0.	5 5 5 30 5 7 5 6 5 8	27 33 24 33	21 63 15 9 25	6.02 5.34 6.37 3.93 5.81	10 10 ( 10 ( 10 ( 10	<pre>&lt; 1 &lt; 1</pre>	0.09 0.07 0.09 0.12 0.10	10 30 < 10 30 < 10	0.54 0.52 0.64 0.08 0.23	230 2220 340 1820 390
F15-L17 12+50 F15-L17 12+75 F15-L17 13+00 F15-L17 13+25 F15-L17 13+50	201 201 201 201 201	202 202 202 202 202	<pre></pre>	< 0.2 0.4 0.2 < 0.2 NotRcd	4.64 3.03 5.07 4.51 NotRcd	<pre>     &lt; 2     NotRcd </pre>	60 60 40 40 NotRcd	0.5 < 0.5 0.5 2.5 NotRed	<pre></pre>	0.09 0.20 0.24 0.08 NotRcd	< 0.5 < 0.5 < 0.5 < 0.5 NotRcd	5 5 5 4 5 5 5 5 1 NotRcd	53 30 29 21 NotRcd	18 13 13 16 NotRcd	5.21 4.57 5.58 5.15 NotRcd	10 10 20 20 NotRcd	<pre></pre>	0.04 0.05 0.05 0.06 NotRcd	10 10 10 40 NotRcd	0.37 0.42 0.49 0.21 NotEcd	245 140 230 580 NotEcd
F15-L17 13+75 F15-18+00N05+25E F15-18+00N05+50E F15-18+00N05+75E F15-18+00N06+00E	201 201 201 201 201 201	202 202 202 202 202 202	<pre></pre>	<pre>&lt; 0.2 2.8 2.6 0.8 1.0</pre>	3.97 2.18 2.24 3.15 3.85	<pre> &lt; 2 38 10 &lt; 2 4</pre>	40 90 130 80 50	0.5 0.5 0.5 0.5 0.5	<pre></pre>	0.10 0.43 0.11 0.18 0.07	< 0. < 0. < 0. < 0. < 0.	5 6 5 15 5 20 5 20 5 20 5 15	48 91 12 25 31	16 71 28 14 21	5.71 4.60 6.29 6.43 6.25	20 < 10 < 10 20 20	<pre></pre>	0.05 0.17 0.05 0.07 0.06	10 10 10 10	0.58 0.24 0.42 0.42 0.45	320 2810 4900 3160 1445
F15-18+00N06+25E F15-18+00N06+50E F15-18+00N06+75E F15-18+00N07+00E F15-18+00N07+25E	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	1.6 0.6 1.2 0.4 0.8	4.96 4.65 4.79 4.21 4.93	<pre>&lt; 2 &lt; 2</pre>	20 10 120 90 50	1.0 1.0 1.5 1.5 3.5	<pre></pre>	0.05 0.06 0.07 0.16 0.07	< 0.5 < 0.5 1.5 0.5	5 10 5 6 5 12 5 8 5 13	23 17 23 36 18	20 7 20 22 17	6.72 6.86 7.47 5.20 6.20	30 30 20 10 30	<pre>&lt; 1 &lt; 1</pre>	0.06 0.07 0.06 0.06 0.07	30 30 30 30 70	0.20 0.13 0.22 0.50 0.21	825 935 4440 360 1340

CERTIFICATION:

tart Bichler



Analytical Chemists \* Geochemists \* Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218

To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9

Page Number :6-B Total Pages :9 Certificate Date: 06-OCT-96 Invoice No. : 19633567 P.O. Number : 8026 Account : KBOA

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Project : Comments: FD6CA0052

											CE	RTIF	CATE		NAL	(SIS	A9633567
SAMPLE	PR COI	EP DE	Mo pp <b>n</b>	Na %	Ni PPm	P ppm	Pb ppm	Sb ppm	Sc ppm	Sr ppm	Ti %	Tl ppm	U Ppa	V PP <b>n</b>	M Bbm	Zn ppm	
F15-L17 05+50 F15-L17 05+75	201 201	202 202	8 7	0.01	16 21	2330 1410	20 20	4	7 9	27 5	0.22	< 10 < 10	< 10 < 10	114 130	< 10 < 10	168 124	
F15-L17 06+00 F15-L17 06+25	201 201	202 202	6 7	< 0.01 0.06	4	1000 490	12 14	6 2	63	10 6	0.36	< 10 < 10	< 10 < 10	95 19	< 10 < 10	60 78	
F15-L17 06+30	201	202		0.05	25	710		2		36	0.65	( 10	< 10	130	( 10	84	<u></u>
F15-L17 07+00	201	202	3	0.07	9	1050	6	4	10	31 30	0.62	< 10 < 10	< 10 < 10	125 127	< 10 < 10	54 38	
F15-L17 07+50 F15-L17 07+75	201 201	202 202	4	0.03	14 3	1600 870	16 14	2	5 5	15 11	0.32	< 10 < 10	< 10 < 10	89 77	< 10 < 10	96 64	
F15-L17 08+00	201	202	5	0.06	7	1060	10	6	8	16	0.42	< 10	< 10	74	< 10	94	
F15-L17 08+25 F15-L17 08+50	201 201	202	5	0.03	22 10	1130 990	16	4	6 5	11	0.21	< 10 < 10	< 10	60 72	< 10	148 86	
F15-L17 09+00	201	202	2	< 0.01	18	1720	28	4	5	8 9	0.09	< 10	< 10	47	< 10	126	
F15-L17 09+25 F15-L17 09+50	201 201	202 202	4	0.01	7 49	1400 1290	12 10	2	2	12 22	0.04 0.31	< 10 < 10	< 10 < 10	61 77	< 10 < 10	62 176	
F15-L17 09+75 F15-L17 10+00	201 201	202 202	6 3	0.01 0.01	13 13	2180 940	22 12	6 6	4 3	14 9	0.05	< 10 < 10	< 10 < 10	112 76	< 10 < 10	96 90	
P15-L17 10+75	201	202	5	0.08		1720	6	4	12		0.61	< 10	< 10	133	< 10	112	
F15-L17 11+00 F15-L17 11+50	201	202	7	0.01	58	1630	12	6	9 7	18	0.23	< 10	< 10	76	< 10	462	
F15-L17 12+00 F15-L17 12+25	201 201	202	< 1 < 1	0.01	3	960 1340	44	2 4	, 1 6	7	< 0.01 0.01	< 10 < 10 < 10	< 10 < 10 < 10	13 86	< 10 < 10	66 62	
F15-L17 12+50	201	202	2	< 0.01	19	780	8	2	5	14	0.34	< 10	< 10 < 10	100	< 10	50 36	······
F15-L17 13+00 F15-L17 13+25	201	202	3	0.04	8	1020	4	2	7	24	0.57	< 10 < 10	< 10 < 10	113	< 10 < 10	42 88	
F15-L17 13+50			NotRed	NotRed	NotRcd	NotRed	NotRcd 1	NotRed 1	NotRcd N	otRcd	NotRcd	NotRed	NotRcd 1	NotRed	NotRed 1	NotRed	
F15-L17 13+75 F15-18+00N05+25E	201 201	202 202	3 9	0.01 0.01	31 60	1060 4900	8 56	4	5 1	12 18	0.25 0.03	< 10 < 10	< 10 < 10	79 99	< 10 < 10	62 130	
F15-18+00N05+50E F15-18+00N05+75E	201 201	202 202	7	0.01	19 10	1260 1200	32 16	62	6	12 22	0.06	< 10 < 10	< 10 < 10	99 121	< 10 < 10	58 106	
F15-18+00N06+00E	201	202	6	< 0.01	25	1320	18	2	3		0.16	< 10	< 10		< 10	188	
E15-18+00N06+25E E15-18+00N06+50E	201	202		0.05	2	600	16	2	4	7	0.26	< 10	< 10	49	< 10	70	
F15-18+00N07+00E F15-18+00N07+00E F15-18+00N07+25E	201 201	202 202 202	75	0.01	33	960 1170	12	2	6 5	19 11	0.15	< 10 < 10 < 10	< 10 < 10 < 10	72 45	< 10 < 10	418 136	
														(	CERTIFIC	CATION:	tart Bichler

CERTIFICATION:

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#### Chemex Labs Ltd.

Analytical Chemists \* Geochemists \* Registered Assayers

212 Brooksbank Ave.,North VancouverBritish Columbia, CanadaV7J 2C1PHONE: 604-984-0221FAX: 604-984-0218

To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9

FD6CA0052

Page Number :7-A Total Pages :9 Certificate Date: 06-OCT-96 Invoice No. :19633567 P.O. Number :8026 Account :KBOA

CERTIFICATE OF ANALYSIS A9633567 PREP Au-AA Ag Al As Ba Be Bi Ca Cđ Co Cr Cu Fe Ga K Mg Ηq La Mn SAMPLE CODE ppb ppm 8 ppm ppm ppa ppm Ł ppm Ł 8 ppm ppm ppm ppm ppm 8 ppm ppm F15-18+00N07+50E 201 202 < 5 0.4 4.95 2 50 1.5 0.28 < 2 < 0.5 16 27 23 6.29 20 2 0.10 20 0.56 645 F15-18+00N07+75E 201 202 F15-18+00N08+25E 201 202 < 5 1.8 5.14 16 30 0.05 2.0 < 2 < 0.5 15 19 6.01 20 13 < 1 0.07 40 0.23 1340 < 5 0.8 5.20 16 30 < 2 0.14 2.0 < 0.5 5 25 27 5.39 20 < 1 30 375 0.06 0.17 F15-18+00N08+50E 201 202 < 5 1.0 0.2 4.92 (2 50 < 2 0.24 < 0.5 11 33 24 6.55 20 < 1 0.06 10 490 0.44 F15-18+00N08+75E 201 202 < 5 0.2 4.51 4 40 0.5 < 2 0.28 < 0.5 10 31 28 5.09 10 < 1 10 380 0.07 0.63 F15-18+00N09+00E 201 202 0.2 < 5 2.70 24 90 0.5 < 2 0.03 < 0.5 17 44 51 8.30 10 < 1 0.06 < 10 0.17 640 F15-18+00N09+25E 201 202 < 5 0.8 3.93 8 30 0.5 < 2 0.05 < 0.5 38 15 7.84 30 0.05 20 385 5 3 0.30 F15-18+00N09+50E 201 202 < 5 0.6 2.39 < 2 40 0.5 ۲ < 2 0.06 < 0.5 5 39 14 6.15 20 0.08 10 0.42 285 4 F15-18+00N09+75E 201 202 < 5 < 0.2 5.03 70 1.5 < 2 0.39 < 0.5 10 < 1 4 22 24 16 6.02 0.11 20 0.64 760 F15-18+00N10+00E 201 202 < 5 24 1.2 3.33 80 0.5 < 2 0.04 < 0.5 20 30 36 5.14 < 10 < 1 675 0.09 10 0.38 F15-18+00N10+50E 201 202 < 5 0.2 4.26 < 2 70 0.5 < 2 0.13 < 0.5 12 26 15 4.79 10 < 1 0.07 10 0.38 390 F15-18+00N10+75E 201 202 < 5 1.2 4.64 14 10 1.0 < 2 0.05 < 0.5 6 13 10 5.13 20 < 1 0.07 20 0.10 1015 F15-18+00N11+00E 201 202 < 5 0.2 4.35 6 60 3.0 < 2 0.05 < 0.5 15 32 26 5.46 10 < 1 0.06 30 0.50 925 F15-18+00N11+50E 201 202 30 < 0.2 2.87 160 1.5 8 < 2 0.10 < 0.5 20 35 49 4.47 < 10 < 1 0.11 20 0.82 1110 F15-18+00N11+75E 201 202 < 5 < 0.2 3.26 12 60 0.5 < 2 0.08 < 0.5 15 38 17 4.90 10 2 0.05 0.51 790 10 F15-18+00N12+00E 201 202 < 5 0.6 4.49 0.5 0.05 530 4 20 < 2 < 0.5 7 29 15 6.82 30 2 0.05 30 0.23 F15-18+00N12+25E 201 202 < 0.5 < 5 0.2 5.10 < 2 50 0.5 < 2 0.32 25 17 6.23 10 < 1 0.08 10 0.57 230 10 F15-18+00N12+50E 201 202 < 5 < 0.2 4.87 4 40 0.5 < 2 0.32 < 0.5 14 47 19 7.00 10 3 0.08 30 0.72 475 F15-18+00N13+00E 201 202 < 5 < 0.2 4.27 4 40 1.0 < 2 0.11 < 0.5 14 33 20 5.58 10 < 1 0.07 20 0.57 670 F15-18+00N13+25E 201 202 < 5 1.2 5.53 10 10 1.0 < 2 0.04 < 0.5 5 10 6.10 30 < 1 0.05 30 0.06 855 6 F15-18+00N13+50E 201 202 < 5 < 0.2 3.59 12 < 0.5 30 0.5 < 2 0.05 11 50 17 6.47 10 < 1 0.05 10 0.61 625 F15-18+00N14+00E 201 202 < 5 < 0.2 4.05 50 < 2 0.21 0.5 4 1.0 23 43 26 5.60 10 < 1 0.08 10 0.85 1345 F15-18+00N14+25E 201 202 < 5 < 0.2 3.82 < 2 40 0.5 < 2 0.24 < 0.5 15 31 5.58 10 < 1 < 10 985 18 0.07 0.66 F15-19+00N05+25E 201 202 < 5 < 0.2 50 4.32 < 2 0.5 2 0.19 0.5 27 27 18 6.82 20 < 1 0.06 20 0.50 1155 F15-19+00N05+50E 201 202 < 5 0.8 4.13 8 10 0.5 < 2 0.06 < 0.5 1 25 12 7.49 40 1 0.03 20 0.06 170 F15-19+00N05+75E 201 202 < 5 0.8 4.55 14 30 0.10 < 0.5 26 12 5.75 255 0.5 < 2 7 20 1 0.05 30 0.25 F15-19+00N06+00E 201 202 < 5 0.2 3.68 0.21 80 2 1025 6 2.5 2.0 15 28 21 5.13 10 < 1 0.07 50 0.51 F15-19+00N06+25E 201 202 33 < 5 0.4 2.65 6 80 < 2 0.23 < 0.5 23 25 1340 0.5 5.33 10 3 0.05 40 0.89 ۲ F15-19+00N07+00E 201 202 < 5 4.73 0.6 4.05 < 2 60 1.5 < 2 0.21 < 0.5 11 21 13 10 0.05 420 < 1 40 0.36 F15-19+00N07+25E 201 202 < 5 0.8 4.03 20 30 1.5 2 0.05 < 0.5 4 17 5 5.23 20 < 1 0.09 50 0.16 485 F15-19+00N07+50E 201 202 < 5 0.2 4.79 < 2 50 0.5 2 0.31 < 0.5 9 30 13 6.60 10 3 0.08 10 0.59 275 F15-19+00N08+00E 201 202 < 5 < 0.2 4.04 30 1.0 < 2 0.10 < 0.5 31 11 6.81 30 0.05 40 0.25 325 4 3 < 1 F15-19+00N08+50E 201 202 < 5 0.2 4.66 12 30 1.5 < 2 0.12 < 0.5 10 30 11 5.94 30 1 0.05 30 0.23 675 F15-19+00N08+75E 201 202 < 5 1.4 4.16 10 < 0.5 30 1.0 < 2 0.12 9 39 23 5.33 20 < 1 0.05 10 0.38 370 F15-19+00N09+25E 201 202 < 5 < 0.2 4.59 2 90 < 0.5 10 1.0 < 2 0.50 25 27 15 6.22 3 0.11 10 0.80 640 F15-19+00N09+50E 201 202 < 5 1.0 4.43 20 30 2.0 < 2 0.09 < 0.5 9 27 15 5.55 20 5 0.06 30 0.26 340 F15-19+00N09+75E 201 202 < 5 0.8 4.90 20 40 1.5 < 2 0.06 < 0.5 B 20 8 5.60 20 1 0.06 30 0.22 750 F15-19+00N10+25E 201 202 < 5 5.11 0.6 4 30 0.5 < 2 0.06 < 0.5 7 27 14 6.53 20 < 1 0.06 20 0.29 610 F15-19+00N10+75E 201 202 5 0.4 3.75 10 80 0.5 < 2 0.17 < 0.5 26 34 20 5.92 < 10 1 0.11 10 1.86 1115 F15-19+00N11+00E 201 202 < 2 < 5 0.8 5.46 40 1.0 < 2 0.24 < 0.5 20 23 17 6.85 20 < 1 0.06 30 0.48 1220

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Page Number :7-B Total Pages :9 Certificate Date: 06-OCT-96 Invoice No. : 19633567 P.O. Number :8026 Account :KBOA

FD6CA0052 Project : Comments:

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SAMPLE	PREP CODE	,	Mo ppm	Na %	Ni ppm	P ppm	Pb P <b>pm</b>	Sb ppm	Sc ppm	Sr ppm	Ti %	Tl ppm	U PP <b>n</b>	V ppm	W ppa	Zn ppm	
F15-18+00N07+50E F15-18+00N07+75E F15-18+00N08+25E F15-18+00N08+50E F15-18+00N08+75E	201 2 201 2 201 2 201 2 201 2 201 2	202 202 202 202 202 202	4 7 5 3 2	0.08 0.04 0.05 0.04 0.04	11 11 8 6 10	1310 790 1010 1200 1260	8 12 10 10 4	<pre>&lt; 2 &lt; 2</pre>	8 5 7 8 8	22 2 12 20 21	0.47 0.23 0.21 0.53 0.56	< 10 < 10 < 10 < 10 < 10 < 10	10 10 < 10 10 10	111 42 42 131 123	< 10 < 10 < 10 < 10 < 10 < 10	84 90 70 62 50	
P15-18+00N09+00E P15-18+00N09+25E P15-18+00N09+50E F15-18+00N09+75E F15-18+00N10+00E	201 2 201 2 201 2 201 2 201 2 201 2	202 202 202 202 202 202	6 4 5 5 1 4 4	<pre>( 0.01 0.01 ( 0.01 0.12 ( 0.01</pre>	62 16 18 10 23	1450 770 820 1050 1070	10 8 14 4 14	<pre>&lt; 2 &lt; 2</pre>	5 4 4 10 4	4 3 6 35 5	0.03 0.19 0.41 0.64 0.03	<pre>&lt; 10 &lt; 10</pre>	< 10 < 10 < 10 10 < 10	75 51 106 123 47	< 10 < 10 < 10 < 10 < 10 < 10	210 76 86 78 110	
F15-18+00N10+50E F15-18+00N10+75E F15-18+00N11+00E F15-18+00N11+50E F15-18+00N11+75E	201 2 201 2 201 2 201 2 201 2 201 2	202 202 202 202 202 202	2 6 5 1 4	0.01 0.06 0.01 0.02 < 0.01	8 4 29 33 32	790 530 1020 1400 1020	10 8 14 24 10	<pre>&lt; 2 &lt; 2</pre>	7 3 7 5 3	10 1 4 9 7	0.29 0.14 0.19 0.03 0.14	< 10 < 10 < 10 < 10 < 10 < 10	<pre>&lt; 10 &lt; 10</pre>	101 14 54 55 60	<pre>&lt; 10 &lt; 10</pre>	66 78 106 124 106	
F15-18+00N12+00E F15-18+00N12+25E F15-18+00N12+50E F15-18+00N12+50E F15-18+00N13+00E F15-18+00N13+25E	201 2 201 2 201 2 201 2 201 2 201 2	202 202 202 202 202 202 202	4 2 3 3 8	0.01 0.04 0.04 0.04 0.04 0.05	8 11 14 22 1	1010 1250 1180 1050 390	10 < 2 6 16 14	<pre>&lt; 2 &lt; 2</pre>	5 11 8 7 3	3 27 20 11 < 1	0.37 0.71 0.72 0.39 0.16	<pre>&lt; 10 &lt; 10</pre>	< 10 10 10 10 < 10	75 132 145 82 15	< 10 < 10 < 10 < 10 < 10 < 10	66 110 50 90 60	
F15-18+00N13+50E F15-18+00N14+00E F15-18+00N14+25E F15-19+00N05+25E F15-19+00N05+50E	201 2 201 2 201 2 201 2 201 2	202 202 202 202 202 202	3 3 3 9 5	<pre>&lt; 0.01 0.03 0.03 0.02 &lt; 0.01</pre>	37 29 12 8 < 1	1040 1200 1330 940 850	10 6 4 8 10	<pre>&lt; 2 &lt; 2</pre>	4 10 5 11 4	5 17 18 15 3	0.15 0.41 0.46 0.57 0.25	<pre>&lt; 10 &lt; 10</pre>	< 10 < 10 10 10 < 10	63 106 126 124 62	< 10 < 10 < 10 < 10 < 10 < 10	60 96 64 76 32	
F15-19+00N05+75E F15-19+00N06+00E F15-19+00N06+25E F15-19+00N06+25E F15-19+00N07+00E F15-19+00N07+25E	201 2 201 2 201 2 201 2 201 2	202 202 202 202 202 202	4 3 7 3 4	0.01 0.03 ( 0.01 0.02 0.06	6 19 21 9 9	780 2190 2340 1700 680	10 12 14 8 10	<pre>&lt; 2 &lt; 2</pre>	6 5 5 4 4	6 16 10 16 2	0.36 0.23 0.08 0.39 0.14	<pre>&lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10</pre>	75 83 93 116 22	< 10 < 10 < 10 < 10 < 10 < 10	48 216 160 60 94	
F15-19+00N07+50E F15-19+00N08+00E F15-19+00N08+50E F15-19+00N08+75E F15-19+00N09+25E	201 201 201 201 201 201	202 202 202 202 202 202	1 4 5 4 1	0.07 0.03 0.02 0.02 0.15	11 5 6 19 19	1030 1090 830 1290 900	6 2 10 10 4	<pre></pre>	9 7 5 6 10	27 7 7 7 47	0.58 0.42 0.38 0.31 0.59	<pre>&lt; 10 &lt; 10</pre>	10 < 10 < 10 < 10 < 10 10	119 100 82 78 119	<pre>&lt; 10 &lt; 10&lt;</pre>	58 54 58 116 90	
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SAMPLE	PRI COI	ep De	Au-AA ppb	Ag ppm	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca چ	Cd ppi	i Co ppr	o Cr u ppm	Cu ppm	Fe %	Ga ppm	Hg ppm	K %	La ppm	Mg %	Mn ppm
F15-19+00N11+25E F15-19+00N11+50E F15-19+00N11+75E F15-20+00N05+50E F15-20+00N06+00E	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	< 0.2 < 0.2 < 0.2 1.0 0.6	2.52 3.86 3.43 3.44 4.98	16 6 20 16	90 50 60 100 50	1.5 0.5 0.5 0.5 1.5	<pre>&lt; 2 &lt; 2</pre>	0.15 0.08 0.13 0.07 0.15	< 0. < 0. < 0. < 0. < 0.	5 16 5 7 5 10 5 10	5 25 7 28 9 47 7 37 9 24	22 12 22 19 14	4.71 6.26 6.21 5.66 6.44	<pre>&lt; 10     10     10     10     20</pre>	3 < 1 < 1 < 1 < 1	0.10 0.03 0.08 0.06 0.07	20 10 10 30 30	0.74 0.29 0.77 0.38 0.40	995 245 370 485 520
F15-20+00N06+50E F15-20+00N06+75E F15-20+00N07+00E F15-20+00N07+25E F15-20+00N07+50E	201 201 201 201 201 201	202 202 202 202 202 202	<pre></pre>	< 0.2 0.8 0.2 0.4 1.2	5.42 5.13 4.27 4.45 4.48	< 2 8 2 4 4	70 10 40 60 50	1.0 1.5 1.5 1.5 2.5	<pre> &lt; 2 &lt; 2</pre>	0.52 0.05 0.05 0.29 0.04	< 0. < 0. < 0. 0.	5 20 5 4 5 7 5 11 5 10	26 15 29 21 21	13 3 6 8 15	5.97 6.03 6.19 5.57 5.52	10 20 20 10 20	<pre> &lt; 1 &lt; 1 &lt; 1 &lt; 1 2 &lt; 1</pre>	0.11 0.04 0.05 0.05 0.09	20 30 30 10 30	0.71 0.07 0.30 0.58 0.35	635 545 650 545 1055
F15-20+00N07+75E F15-20+00N08+00E F15-20+00N08+25E F15-20+00N08+50E F15-20+00N08+75E	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5</pre>	0.2 < 0.2 0.2 < 0.2 < 0.2 0.6	4.42 3.95 4.70 4.36 4.35	2 16 16 4 8	40 40 60 40 30	0.5 1.5 1.5 1.0 0.5	2 < 2 < 2 < 2 < 2 < 2	0.16 0.09 0.22 0.16 0.10	< 0. < 0. < 0. < 0.	5 9 5 17 5 17 5 9	37 29 33 40 39	17 17 28 13 18	6.00 5.69 5.78 6.30 7.15	10 10 10 20 30	<pre>&lt; 1 &lt; 1 3 &lt; 1 &lt; 1 &lt; 1 &lt; 1</pre>	0.05 0.07 0.08 0.03 0.05	10 30 20 10 20	0.53 0.44 0.54 0.35 0.40	230 460 560 420 340
F15-20+00N09+00E F15-20+00N09+25E F15-20+00N09+50E F15-20+00N09+50E F15-20+00N09+75E F15-20+00N10+00E	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.8 2.0 0.2 0.2 0.2	2.47 4.54 3.61 4.83 3.56	24 6 4 8 < 2	70 30 90 60 30	1.0 1.5 0.5 0.5 0.5	<pre>     &lt; 2     &lt; 2     &lt;         2</pre>	0.16 0.04 0.15 0.19 0.10	0. < 0. < 0. < 0.	5 26 5 10 5 16 5 11 5 11	5 20 20 5 32 42 42	31 8 24 18 16	5.73 6.03 4.57 6.24 7.48	< 10 30 < 10 10 30	< 1 < 1 < 1 < 1 1	0.07 0.06 0.10 0.06 0.06	40 30 10 10 10	0.25 0.16 0.43 0.55 0.39	1745 710 555 470 600
F15-20+00N10+25E F15-20+00N10+50E F15-20+00N10+75E F15-20+00N11+00E F15-20+00N11+50E	201 201  201 201	202 202  202 202	<pre></pre>	0.4 < 0.2 NotRcd 0.2 0.6	4.12 4.98 NotRcd 3.80 2.94	6 16 NotRcd 8 14	30 60 NotRcd 30 80	0.5 1.5 NotRcd 0.5 1.5	<pre></pre>	0.14 0.27 NotRcd 0.10 0.07	< 0. < 0. NotRc 0. < 0.	5 9 5 14 1 NotRcd 5 9 5 39	27 24 NotRed 29 30	13 23 NotRcd 15 21	6.23 6.98 NotRcd 6.40 8.82	20 10 NotRcd 20 < 10	<pre> &lt; 1 &lt; 1 NotRcd &lt; 1 </pre> <pre> </pre>	0.05 0.09 NotRcd 0.07 0.08	10 10 NotRcd 10 20	0.42 0.67 NotRcd 0.37 1.29	460 430 NotRcd 460 2540
F15-20+00N11+75E F15-20+00N12+00E F15-20+00N12+25E F15-21+00N05+50E F15-21+00N05+75E	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.2 < 0.2 0.2 < 0.2 0.2	4.05 3.13 4.11 3.57 3.34	16 12 6 8 14	30 50 90 60 110	0.5 0.5 0.5 0.5 1.5	<pre>&lt; 2 &lt; 2</pre>	0.04 0.05 0.19 0.26 0.22	< 0.1 < 0.1 < 0.1 < 0.1 2.1	5 9 5 20 5 13 5 19 5 9	40 56 24 33 25	15 22 15 16 9	6.96 4.71 4.39 5.45 4.42	10 < 10 10 10 10	< 1 1 3 < 1 4	0.04 0.05 0.06 0.05 0.06	10 10 10 30 20	0.41 0.86 0.46 0.85 0.35	385 1110 560 940 305
F15-21+00N06+50E F15-21+00N06+75E P15-21+00N07+00E F15-21+00N07+25E F15-21+00N07+50E	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.2 < 0.2 0.2 < 0.2 < 0.2 1.0	5.45 4.16 4.60 5.33 4.64	<pre> &lt; 2 14 &lt; 2 6 14 </pre>	70 50 40 100 20	2.0 1.0 1.0 1.5 1.0	<pre></pre>	0.40 0.16 0.24 0.56 0.06	< 0. < 0. < 0. < 0. < 0.	5 12 5 13 5 11 5 18 5 3	24 29 28 28 29 10 16	19 13 19 25 3	5,99 6.04 6.63 6.06 5.86	10 20 10 10 30	<pre>&lt; 1 &lt; 1 &lt; 1 &lt; 1 &lt; 1 &lt; 1 &lt; 3</pre>	0.08 0.07 0.08 0.17 0.06	30 30 10 20 40	0.61 0.38 0.58 0.84 0.11	325 425 260 535 410
F15-21+00N07+75E F15-21+00N08+25E F15-21+00N08+50E F15-21+00N08+50E F15-21+00N08+75E F15-21+00N09+00E	201 201 201 201 201 201	202 202 202 202 202 202	<pre></pre>	0.8 0.2 < 0.2 0.2 0.2 0.6	5.23 4.63 3.69 3.37 1.55	12 6 14 8 22	30 40 50 60 60	0.5 0.5 1.0 1.5 1.0	<pre> &lt; 2 &lt; 2</pre>	0.13 0.24 0.19 0.12 0.04	< 0.1 < 0.1 < 0.1 < 0.1	5 5 5 13 5 42 5 17 5 24	24 30 23 21 5	9 21 72 26 122	7.36 7.18 8.00 6.40 6.72	30 20 10 10 < 10	5 3 2 < 1 < 1	0.04 0.08 0.05 0.08 0.11	30 10 10 20 10	0.23 0.56 1.40 0.40 0.14	305 515 2400 1325 2640
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SAMPLE	PRI COI	EP DE	Mo ppm	Na %	Ni ppm	P ppm	Pb ppm	Sb ppm	Sc ppm	Sr ppm	Ti %	Tl ppm	U negg	V ppm	W ppma	Zn ppm	
F15-19+00N11+25E F15-19+00N11+50E F15-19+00N11+75E F15-20+00N05+50E F15-20+00N06+00E	201 201 201 201 201 201	202 202 202 202 202 202	3 3 1 8 4	0.03 < 0.01 0.04 < 0.01 0.04	33 10 38 16 10	1280 590 610 1530 1060	12 6 4 14 10	<pre> &lt; 2 &lt; 2</pre>	7 5 6 3 9	12 8 16 7 12	0.19 0.30 0.20 0.10 0.46	< 10 < 10 < 10 < 10 < 10 < 10	< 10 < 10 < 10 < 10 < 10 10	60 104 83 98 88	< 10 < 10 < 10 < 10 < 10 < 10	150 46 78 254 76	
F15-20+00N06+50E F15-20+00N06+75E F15-20+00N07+00E F15-20+00N07+25E F15-20+00N07+50E	201 201 201 201 201 201	202 202 202 202 202 202	1 6 4 2 6	0.15 0.03 0.01 0.03 0.04	9 3 10 10 25	1070 710 760 1120 620	<pre></pre>	<pre></pre>	9 3 5 4 4	46 3 23 2	0.70 0.16 0.30 0.59 0.13	< 10 < 10 < 10 < 10 < 10 < 10	10 < 10 < 10 10 < 10	130 27 78 132 23	< 10 < 10 < 10 < 10 < 10 < 10	48 44 90 62 174	
F15-20+00N07+75E F15-20+00N08+00E F15-20+00N08+25E F15-20+00N08+50E F15-20+00N08+75E	201 201 201 201 201 201	202 202 202 202 202 202	3 5 4 3 5	0.02 0.03 0.06 < 0.01 0.01	16 19 17 8 9	1010 970 1180 1040 890	<pre></pre>	<pre></pre>	9 5 10 7 8	12 8 18 12 6	0.48 0.28 0.49 0.53 0.48	< 10 < 10 < 10 < 10 < 10 < 10	< 10 < 10 < 10 < 10 < 10 10	111 64 102 123 108	< 10 < 10 < 10 < 10 < 10 < 10	68 100 102 46 58	
F15-20+00N09+00E F15-20+00N09+25E F15-20+00N09+50E F15-20+00N09+75E F15-20+00N10+00E	201 201 201 201 201 201	202 202 202 202 202 202	7 5 3 1 4	0.01 0.03 0.03 0.02 0.01	30 7 20 22 11	3320 810 910 1090 870	24 10 10 2 6	<pre></pre>	7 3 8 7 6	11 3 12 16 7	0.06 0.21 0.20 0.42 0.41	< 10 < 10 < 10 < 10 < 10 < 10	< 10 < 10 < 10 < 10 < 10	53 46 90 112 113	< 10 < 10 < 10 < 10 < 10 < 10	242 76 88 92 68	
F15-20+00N10+25E F15-20+00N10+50E F15-20+00N10+75E F15-20+00N11+00E F15-20+00N11+50E	201 201  201 201	202 202 202 202 202	3 L NotRcđ 4 3	0.01 0.04 NotRcd 0.01 0.01	5 14 NotRcd 7 41	880 1430 NotRcd 1060 2760	6 6 NotRcd 12 262	< 2 < 2 NotRcd < 2 < 2	7 13 NotRcd 7 9	9 20 NotRcđ 7 5	0.51 0.79 NotRcd 0.48 0.11	< 10 < 10 NotRcd < 10 < 10	10 10 NotRcd 10 < 10	115 139 NotRcd 1 101 69	< 10 < 10 NotRcd < 10 < 10	46 136 NotRcd 56 106	
F15-20+00N11+75E F15-20+00N12+00E F15-20+00N12+25E F15-21+00N05+50E F15-21+00N05+75E	201 201 201 201 201	202 202 202 202 202 202	4 3 1 3 5	< 0.01 < 0.01 0.02 0.01 < 0.01	22 55 13 14 20	670 900 1070 2080 1270	6 12 4 8 12	<pre> &lt; 2 &lt; 2</pre>	4 6 4 6 2	3 5 14 16 17	0.18 0.14 0.28 0.20 0.05	< 10 < 10 < 10 < 10 < 10 < 10	< 10 < 10 < 10 < 10 < 10	62 59 95 145 53	< 10 < 10 < 10 < 10 < 10 < 10	72 120 70 124 306	
F15-21+00N06+50E F15-21+00N06+75E F15-21+00N07+00E F15-21+00N07+25E F15-21+00N07+50E	201 201 201 201 201	202 202 202 202 202 202	< 1 3 2 < 1 6	0.09 0.02 0.05 0.18 0.04	10 9 14 16 1	1190 920 1230 1320 440	<pre></pre>	<pre>&lt; 2 &lt; 2</pre>	12 6 10 12 3	33 13 18 53 2	0.82 0.45 0.59 0.75 0.20	< 10 < 10 < 10 < 10 < 10 < 10	10 < 10 < 10 10 < 10	131 99 114 137 25	< 10 < 10 < 10 < 10 < 10 < 10	72 66 78 100 62	
F15-21+00N07+75E F15-21+00N08+25E F15-21+00N08+50E F15-21+00N08+75E F15-21+00N09+00E	201 201 201 201 201	202 202 202 202 202 202	3 4 10 1 1	0.01 0.05 < 0.01 0.03 < 0.01	4 9 11 11 7	950 870 2830 1580 1950	16 8 18 14 38	<pre>&lt; 2 &lt; 2</pre>	6 11 9 11 12	9 19 10 10 3	0.36 0.61 0.04 0.24 0.05	< 10 < 10 < 10 < 10 < 10 < 10	<pre>&lt; 10     10 &lt; 10 &lt; 10 &lt; 10 &lt; 10</pre>	69 152 184 81 37	< 10 < 10 < 10 < 10 < 10 < 10	36 62 84 110 88	_

CERTIFICATION:

tart Brichler

12.4

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## **Chemex Labs Ltd.**

Analytical Chemists \* Geochemists \* Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218

To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9

Page Number :9-A Total Pages :9 Certificate Date: 06-OCT-96 Invoice No. : 19633567 P.O. Number :8026 Account :KBOA

Project : FD6CA0052 Comments:

SAUTZ         PEEP         Au-AA         Ag         Al         PAS         PB         PPB         PPB </th <th></th> <th>CE</th> <th>RTIFI</th> <th>CATE</th> <th>OF A</th> <th>NAL</th> <th>(SIS</th> <th></th> <th>19633</th> <th>567</th> <th></th> <th></th>												CE	RTIFI	CATE	OF A	NAL	(SIS		19633	567		
p1:2-100000+057       p1:2 - 100000+057       p1:2	SAMPLE	PR CO	EP DE	Au-AA ppb	Ag pp <b>m</b>	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cđ ppm	Co ppm	Cr ppm	Cu ppm	Fe %	Ga ppm	Hg PP#	K %	La ppm	Mg %	Mn ppm
P13-21-00010-752 201 202 (5 0.8 4.47 4 50 1.0 2 0.14 (0.5 11 47 17 7.58 20 1 0.06 20 0.54 440 P13-21-00011-252 201 20 5.40 20 (1 0.06 20 0.54 440 P13-21-00011-252 201 20 5.40 20 (1 0.07 20 0.23 1520 P13-21-00011-752 201 20 (5 0.8 4.57 14 70 1.5 (2 0.08 (0.5 12 20 12 5.49 20 (1 0.07 20 0.23 1520 P13-21-00011-752 201 20 (5 0.2 4.01 2 40 2.5 (2 0.09 (0.5 9 21 12 5.19 20 (1 0.09 60 0.20 650 P13-21-00011-752 201 20 (5 0.2 4.01 2 40 2.5 (2 0.09 (0.5 9 21 12 5.19 20 (1 0.09 60 0.20 650 P13-21-00011-752 201 20 (5 0.2 4.01 2 40 2.5 (2 0.09 (0.5 9 21 12 5.19 10 (1 0.09 10 0.96 60 0.20 650 P13-21-00011-752 201 20 (5 0.2 1.69 10 0.5 (2 0.09 (0.5 9 21 12 5.19 10 (1 0.09 10 0.96 10 0.20 145 150 153 118 20 20 (5 0.2 1.69 10 0.5 (2 0.09 (0.5 9 13 1 12 5.57 10 (1 0.09 10 0.30 146 555 115 5138 201 202 (5 0.2 1.69 145 145 10 0.5 (2 0.09 (0.5 9 31 1 16 5.57 10 (1 0.09 10 0.36 145 155 5318 201 202 (5 0.2 3.57 19 7 0 0.5 (2 0.09 (0.5 9 31 1 17 4.40 10 (1 0.08 10 0.56 120 145 135 118 201 202 (5 0.2 3.52 19 7 0 0.5 (2 0.01 (0.5 15 9 31 1 17 4.40 10 (1 0.08 10 0.56 920 115 53188 201 202 (5 0.2 3.52 19 7 0 0.5 (2 0.01 (0.5 15 117 6 4.49 10 (1 0.08 10 0.56 920 115 53188 201 202 (5 0.2 3.52 19 7 0 0.5 (2 0.01 (0.5 15 117 6 4.49 10 (1 0.08 10 0.56 920 115 53188 201 202 (5 0.2 3.52 19 7 0 0.5 (2 0.01 (0.5 15 15 15 19 6 (10 3 0.07 10 0.54 146 110 0.55 12 15 9.08 (10 3 0.07 10 0.54 146 15 53188 201 202 (5 0.2 3.53 14 10 0.55 (2 0.01 (0.5 15 15 15 15 16 0.18 (10 3 0.06 10 0.56 920 115 53188 201 202 (5 0.4 2.78 (2 70 0.5 (2 0.01 (0.5 10 33 16 6.00 10 (1 0.06 10 0.59 710 15 53188 201 202 (5 0.4 2.78 (2 70 0.5 (2 0.01 (0.5 10 33 16 6.00 10 (1 0.06 (1 0.06 10 0.59 710 115 53188 201 202 (5 0.4 2.78 (2 70 0.5 (2 0.01 (0.5 10 33 16 6.00 10 (1 0.06 (1 0 0.50 710 115 15 117 15 15 15 15 15 15 15 15 15 15 15 15 15	F15-21+00N09+25E F15-21+00N09+50E F15-21+00N10+00E F15-21+00N10+00E F15-21+00N10+25E F15-21+00N10+50E	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	0.4 2.0 0.4 1.2 0.2	3.78 4.88 3.92 4.93 1.68	6 6 16 14 22	90 40 30 20 140	0.5 1.0 2.0 2.0 1.0	<pre>&lt; 2 &lt; 2</pre>	0.13 0.12 0.06 0.03 0.80	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 3.5	17 18 3 3 18	44 32 12 11 24	23 25 8 9 26	5.67 6.77 5.53 5.62 6.19	10 20 20 30 < 10	1 < 1 < 1 < 1 < 1	0.07 0.06 0.09 0.06 0.11	10 20 30 30 60	0.51 0.34 0.16 0.10 0.53	1300 1075 280 275 1360
215 - 21-0081 2-008       201       205       (5       (0.2)       3.83       16       50       0.5       2       0.19       (0.5)       16       31       26       5.55       10       (1       0.06       10       0.5       1215         215 - 518081 2-255       201       202       (5       0.2       3.76       16       90       0.5       (2       0.09       0.5       9       53       16       5.36       10       (1       0.08       10       0.5       15       515       518       5.36       10       (1       0.04       10       0.5       15       515       518       513       18       512       51       18       51       10       0.10       0.5       12       201       00       (1       0.06       10       0.5       12       10       10       0.5       12       10       10       0.5       12       10       10       0.5       10       10       0.5       10       10       0.5       15       15       13       18       10       10       0.5       16       52       35       9.08       (10       0.5       10       10       10       10	F15-21+00N10+75E F15-21+00N11+00E F15-21+00N11+25E F15-21+00N11+25E F15-21+00N11+50E F15-21+00N11+75E	201 201 201 201 201 201	202 202 202 202 202 202	<pre></pre>	0.8 0.2 0.6 0.8 0.2	4.47 4.64 4.57 4.03 4.01	4 6 14 4 2	50 50 70 20 40	1.0 1.5 1.5 0.5 2.5	2 < 2 < 2 2 < 2 < 2 < 2	0.14 0.17 0.08 0.12 0.09	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	11 13 12 6 9	47 28 20 19 21	17 20 12 7 12	7.58 5.80 5.49 6.93 5.17	20 20 20 30 20	1 < 1 < 1 4 < 1	0.05 0.06 0.07 0.07 0.09	20 20 30 20 60	0.54 0.44 0.23 0.27 0.20	840 660 1520 455 600
211       202       < 5	F15-21+00N12+00E F15-21+00N12+25E F15 5318A F15 5318B F15 5318B F15 5318C	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5</pre>	< 0.2 0.2 0.2 0.2 < 0.2 < 0.2	3.83 3.70 2.86 3.47 3.52	18 16 24 16 29	50 80 50 110 70	0.5 0.5 0.5 0.5 0.5	2 < 2 < 2 2 2 < 2	0.19 0.03 0.09 0.07 0.01	< 0.5 0.5 < 0.5 < 0.5 < 0.5 < 0.5	18 9 8 9 16	31 52 13 31 52	26 15 8 17 35	5.56 8.37 5.36 4.40 9.08	10 30 10 10 < 10	<pre>&lt; 1 1 &lt; 1 &lt; 1 &lt; 1 3</pre>	0.08 0.03 0.04 0.08 0.07	10 10 10 10 10	0.69 0.36 0.16 0.54 0.44	1210 345 1030 920 560
	F15 5318D F15 5318E F15 5318F F15 5318G F15 5318H	201 201 201 201 201 201	202 202 202 202 202 202	<pre>&lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5 &lt; 5</pre>	< 0.2 0.2 0.2 0.8 0.4	4.98 3.94 3.93 5.36 2.78	< 2 4 12 10 < 2	60 70 90 30 70	1.0 0.5 0.5 1.5 0.5	<pre> &lt; 2 &lt; 2</pre>	0.31 0.13 0.05 0.04 0.13	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	15 9 15 8 10	17 28 55 17 33	8 13 35 7 16	4.93 4.89 6.18 5.05 6.00	10 10 < 10 20 10	<pre>&lt; 1 &lt; 1 3 &lt; 1 &lt; 1 &lt; 1 &lt; 1 &lt; 1 &lt; 1</pre>	0.05 0.06 0.06 0.05 0.05	10 10 10 20 < 10	0.50 0.44 0.54 0.10 0.50	745 460 605 980 710
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### **Chemex Labs Ltd.**

Analytical Chemists \* Geochemists \* Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218

To: CANAMERA GEOLOGICAL LTD. ATTN: DAVID AWRAM 220 CAMBIE ST., SUITE 650 VANCOUVER, BC V6B 2M9

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Page Number :9-B Total Pages :9 Certificate Date: 06-0CT-96 Invoice No. : 19633567 P.O. Number : 8026 Account :KBOA

Project : FD6CA0052 Comments:

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										CERTIFICATE OF ANALYSIS					A9633567	
SAMPLE	PREP CODE	Мо ррш	Na %	Ni ppm	P PP <b>m</b>	Pb pp∎	Sb ppm	Sc ppm	Sr ppm	Ti %	Tl ppm	U ppm	V ppm	W PP <b>a</b>	Zn pp <b>n</b>	
15-21+00N09+25E 15-21+00N09+50E 15-21+00N10+00E 15-21+00N10+25E 15-21+00N10+50E	201 202 201 202 201 202 201 202 201 202 201 202	2 5 4 8 24	0.03 0.02 0.06 0.05 0.01	22 13 6 6 41	1460 910 470 470 4950	10 10 8 8 20	<pre>&lt; 2 &lt; 2</pre>	4 7 4 4 7	14 10 5 < 1 39	0.18 0.36 0.22 0.14 0.03	< 10 < 10 < 10 < 10 < 10 < 10	< 10 < 10 < 10 < 10 < 10 < 10	104 88 32 14 81	<pre>&lt; 10 &lt; 10</pre>	136 142 94 80 352	
715-21+00N10+75E 715-21+00N11+00E 715-21+00N11+25E 715-21+00N11+50E 715-21+00N11+75E	201 202 201 202 201 202 201 202 201 202 201 202	3 3 4 7 4	0.02 0.03 0.03 0.05 0.05	18 14 7 4 13	1470 970 970 500 720	10 8 10 10 12	<pre></pre>	9 8 5 5 5	12 14 6 9 6	0.34 0.42 0.22 0.37 0.16	<pre>&lt; 10 &lt; 10</pre>	<pre>&lt; 10 &lt; 10</pre>	103 94 51 59 32	<pre>&lt; 10 &lt; 10</pre>	66 86 92 64 116	
15-21+00N12+00E 15-21+00N12+25E 15 5318A 15 5318B 15 5318C	201 202 201 202 201 202 201 202 201 202 201 202	2 4 5 3 3	0.04 < 0.01 < 0.01 < 0.01 < 0.01 < 0.01	25 22 5 13 41	1530 440 880 870 1140	10 8 18 28 14	<pre> &lt; 2 &lt; 2</pre>	8 7 3 3 6	15 5 7 7 3	0.38 0.10 0.14 0.11 0.02	< 10 < 10 < 10 < 10 < 10 < 10	< 10 < 10 < 10 < 10 < 10 < 10	103 92 64 84 70	<pre>&lt; 10 &lt; 10</pre>	112 70 54 76 104	
15 5318D 15 5318E 15 5318F 15 5318F 15 5318G 715 5318H	201 202 201 202 201 202 201 202 201 202 201 202	<pre></pre>	0.04 0.01 < 0.01 0.03 < 0.01	7 7 34 5 22	1200 960 1110 570 1180	< 2 12 6 4 2	<pre> &lt; 2 &lt; 2</pre>	6 6 3 3	21 10 5 1 9	0.53 0.26 0.01 0.18 0.17	<pre>&lt; 10 &lt; 10</pre>	< 10 < 10 < 10 < 10 < 10 < 10	114 100 84 27 118	<pre>&lt; 10 &lt; 10</pre>	72 58 94 80 88	
														CERTIFIC		Hart Bichler





\DRAWINGS\BC-PROJ\FRDN-GEO



#### LEGEND

	CLAIM BOUNDARY
45 50	BEDDING
30 967	CLEAVAGE
75-	TOPS
ł	FOLD AXIS
060	FOLIATION
	FAULT
+	STATION LOCATIONS (FROM SURVEY DATA. STATION NAMES REPRESENT IDEALIZED GRID)
$\bigcirc$	OUTCROP
$\bigcirc$	BOULDERS
ZELTON GROUP	
mud	-MUDSTONE
silt	-SILTSTONE
SS	-SANDSTONE
cong	-CONGLOMERATE
epic	EPICLASTIC
rhy	-RHYOLITE
dac	DACITE
and	-ANDESITE
bx	-BRECCIA
mag	-MAGNETIC
porph	-PORPHYRITIC
blk	-BLACK
amyg	-AMYGDALOIDAL
frag	-FRAGMENTAL
hetero	-HETEROLITHIC
mono	MONOLITHIC



1:1,000NTS: 104BDATE:NOV.1996ED BY:FILE: FRED-N.DWGMAP NO.: 12CANAMERA GEOLOGICAL LTD



HAZELTON GROUP

751





STATION NAMES REPRESENT IDEALIZED GRID)

FOLD AXIS

FOLIATION









	<5	0.6	2	50	2	<0.5	11	14	3	14	12	2	84	_L18
113 - 06+00	<5	<0.2	4	50	2	<0.5	6	15	3	10	8	4	54	L18
113 - 06+25	<5	0.2	\$	70	2	<0.5	22	21	2	17	16	2	122	L19
113 - 06+50	ও	0.2	2	30	>2	<0.5	11	13	4	12	8	2	72	L19 -
113 - 06+75	<5	0.2	6	40	4	<0.5	12	24	4	13	10	2	104	L19 ·
L13 ~ 07+00	<5	1.0	8	90	2	0.5	14	44	4	21	8	Z	158	L19
L13 - 07+50	<5	1.2	2	90	0	<0.5	11	16	3	15	6	2	86	L19 ·
L13 - 07+75	5	<0.2	0	50	0	<0.5	14	10	3	9	4	2	66	L19 -
L13 - 05+00	3	0.2	26	80	a	(0.5	9	54	4	.12	14	6	82	L19 -
113 - 10+25	Å	0.2	- <del>1</del>		0	05	18	20	1 1	14	24			L19
113 - 10150		0.2	5	40		10.0	7	14						L19
113 10175		0.2	Y A			10.5		10	<u></u>			2	<u>⊢ ~</u>	119
L13 - 10+75	(3)	0.2	4	60		<0.5	1/	14	<u> </u>	12	10	<u> </u>	/4	110
L13 - 11+00		0.2	16	90	2	<0.5	11	52	3	29	12	2	134	119
L13 - 11+25	<5	1.2	4	40	<u>a</u>	<0.5	12	36	6	23	10	2	160	110
L13 - 11+50	4	0.6	2	30	2	<0.5	6	15	4	11	10	<2	72	
L13 - 11+75	<5	1.6	থ	20	2	<0.5	4	10	6	6	14	2	<b>60</b>	
L13 - 12+00	<5	1	2	40	2	<0.5	10	13	3	15	6	2	56	L19 -
L13 - 12+25	<5	<0.2	2	70	[ <b>a</b>	0.5	16	27	2	26	10	2	64	L19 ·
L13 - 12+50	<5	D.2	4	40	2	<0.5	7	tB	3	41	8	2	60	L19 ·
L13 - 12+75	<5	0.2	A	70	2	<0.5	8	19	1	32	8	2	96	E19 -
L13 - 13+00	3	0.2	ß	40	4	<0.5	6	6	3	9	. 8	2	42	L19 ·
L14 - 05+25	<5	<0.2	4	30	2	<0.5	7	15	4	11	. 16	2	70	L19 -
L14 - 05+50	<5	0.2	0	20	2	<0.5	7	13	5	6	12	4	58	L20 ·
L14 - 05+75	<5	<0.2	4	30	2	<0.5	6	35	3	11	14	2	70	L20
L14 - 06+00	<5	<1.2	a	40	4	<0.5	8	19	1	9	7	4	56	L20 ·
114 - 06+25	6	0.6		120	à	<0.5	21	20	3	15	12	2	96	120
114 - 06+50	6	0.2	0	180	0	(0.5	21		3	12		2	100	120
114 - 06+75	- A	0.9		40	0	(05	15	14	5	11	19		122	120
114 - 07+00		0.2				(0.5	10	10	- <u>.</u>		10		148	120
114 07+26		0.0	Y T			(0.)	7	20			10	2	100	120
L14 - 0/+25	<3	0.0	4	40	<u>u</u>	<0.5		20		. 19	12	~	120	120
L14 - 07+50	4	<0.2	2	30		<0.5		12		8	12	2	84	120
L14 - 0/+/5	<3	<0.2	2	30	2	<0.5	10	18	3	15	6	2	78	120
L14 - 05+00	3	<0.2	4	30	2	<0.5	12	18	4	11	6	2	64	120
L14 - 08+25	<5	0.2	2	50	2	<0.5	22	46	5	13	10	2	118	
L14 - 06+50	<5	0.2	_ 20	90	2	<0.5	19	62	4	_20	12	4	124	120
L14 - 08+75	<5	<0.2	<2	40	2	<0.5	10	24	4	16	8	2	112	
L14 - 09+00	4	<0.2	4	40	2	<0.5	7	21	3	12	4	2	68	
L14 - 11+75	<5	0.6	Ą	30	2	<0.5	. 4	13	4	21	8	2	60	
L14 - 12+00	<5	0.6	ß	40	2	<0.5	11	21	3	42	8	4	B4	120 -
L14 - 12+25	ব	<0.2	ß	70	2	<0.5	9	16	3	38	10	2	82	L20 ·
L14 - 12+50	<5	<0.2	0	40	2	<0.5	4	15	2	18	4	2	66	L20 -
L14 - 12+75	4	<0.2	4	50	2	<0.5	8	35	2	24	8	2	74	120
L15 - 04+75	<5	1.2	74	50	2	<0.5	8	27	4	4	30	4	40	120 -
L15 ~ 05+00	55	3	20	70	2	<0.5	19	140	8	34	40	8	164	120 -
L15 - 05+25	<5	0.2	60	50	2	<0.5	15	14	2	10	12	6	78	120.
L15 - 05+50	<5	0.2	18	50	2	<0.5	5	19	5	12	24	2	82	<u>L21</u>
L15 - 08+00	4	<0.2	4	30	2	<0.5	8	12	2	<u> </u>	4	2	38	121 -
115 - 06+25	<5	<0.2	4	40	2	0.5	8	14	1	7	1	8	38	121
L15 - 06+50	4	<0.2	6	70	2	<0.5	10	57	5	8	18	2	94	121
L15 - 08+75	ত	0.2	a	10	2	<0.5	5	4	6	10	10	2	68	121
L15 - 07+00	ব্র	0.2	0	40	2	<0.5	13	24	4	10	8	2	74	1.21
115 - 07+25	6	0.6	0	20	0	<0.5	6	<1	6	A	10		84	121
115 - 07+50		0.0	2		0	(0.5	17	21		10		-	84	121
115 - 07475	- a	0.1				(0.5	12	17					74	121
115 - 08+00		1.0	4			0.5	7	14				1		1.21
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115 - 00130	<u></u>	0.0	4	+0	4	(0.5		- 10		1	10			121
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$\begin{array}{r} 15 - 09+25 \\ 115 - 09+50 \\ 115 - 09+50 \\ 115 - 10+00 \\ 115 - 10+25 \\ 115 - 10+25 \\ 115 - 10+73 \\ 115 - 11+25 \\ 115 - 11+25 \\ 115 - 11+25 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 12+75 \\ 115 - 12+75 \\ 115 - 13+25 \\ 115 - 14+00 \\ 115 - 14+25 \\ 115 - 14+2$	12 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.2         0.2           0.2         0.2           0.2         0.2           0.3         2.4           1.6         1.2           1.4         0.6           0.2         0.4           0.2         0.2           0.3         0.2           0.4         0.2           1.4         0.6           0.2         0.2           0.4         0.2           0.4         0.2           0.2         0.2	3 - 8 8 8 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	70         60           60         50           50         50           100         40           20         30           70         60           30         80           70         40           40         50           50         80           70         40           40         50           80         80	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	<ul> <li>ල3</li> <li>ල3</li> <li>ල3</li> <li>ල3</li> <li>ල3</li> <li>ල3</li> <li>ල3</li> <li>ල3</li> <li>ල4</li> <li>ල4</li> <li>ල4</li> <li>ල4</li> <li>ල4</li> <li>g4</li> <l< td=""><td>13 32 7 11 14 10 7 5 8 21 14 20 11 14 20 11 20 11 20 4 10 8 22 12</td><td></td><td>5 6 4 3 5 6 4 3 2 5 4 5 1 2 2 3 3</td><td>11           15           14           16           355           18           6           7           5           12           16           8           18           19           15           7           7           8           10           53           10</td><td>12 15 26 5 14 10 10 12 8 6 4 14 24 104 8 8 2 16 8</td><td>2 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2</td><td>302           800           1118           104           52           98           99           98           99           98           99           98           99           99           99           99           99           99           99           99           99           99           99           90           91</td><td></td></l<></ul>	13 32 7 11 14 10 7 5 8 21 14 20 11 14 20 11 20 11 20 4 10 8 22 12		5 6 4 3 5 6 4 3 2 5 4 5 1 2 2 3 3	11           15           14           16           355           18           6           7           5           12           16           8           18           19           15           7           7           8           10           53           10	12 15 26 5 14 10 10 12 8 6 4 14 24 104 8 8 2 16 8	2 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	302           800           1118           104           52           98           99           98           99           98           99           98           99           99           99           99           99           99           99           99           99           99           99           90           91	
$\begin{array}{c} 115 - 09+25 \\ 115 - 09+50 \\ 115 - 09+50 \\ 115 - 10+00 \\ 115 - 10+25 \\ 115 - 10+25 \\ 115 - 10+73 \\ 115 - 11+25 \\ 115 - 11+25 \\ 115 - 11+75 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 12+75 \\ 115 - 12+75 \\ 115 - 13+25 \\ 115 - 13+25 \\ 115 - 14+25 \\ 115 - 14+50 \\ 115 - 08+25 \\ 115 - 08+$	10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	c.0.2         c.0.2           c0.2         c0.2           c0.2         c0.2           c0.3         c2.4           1.6         1.2           1.4         c.6           c.2         1.4           c.4         c.2           1.4         c.2	5 A • A A A 4 A A A A A A A A A A A A A A	70         60           60         50           50         50           100         40           20         30           70         60           30         70           60         50           50         50           50         50           80         70           80         50           50         50           50         50	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ලව	13           32           7           11           14           10           7           5           8           21           14           20           11           20           4           10           8           22           12           10		5 6 4 4 3 5 6 4 5 1 2 2 3 3 *	11           15           14           16           35           16           7           5           12           16           8           16           7           8           10           53           10           10	12 15 26 8 14 10 12 8 6 4 14 10 12 8 6 4 14 10 12 8 8 14 10 12 8 8 14 10 10 12 8 8 14 10 10 10 10 12 15 16 16 10 10 10 12 10 10 12 16 16 16 16 10 10 10 12 16 16 16 16 16 16 16 16 16 16		80 80 118 104 52 98 98 62 84 74 54 100 78 96 74 158 40 64 64 64 64 172 78 114	
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$\begin{array}{r} 15 - 09+25 \\ 115 - 09+50 \\ 115 - 09+50 \\ 115 - 10+00 \\ 115 - 10+25 \\ 115 - 10+75 \\ 115 - 11+75 \\ 115 - 11+25 \\ 115 - 11+75 \\ 115 - 11+75 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 13+50 \\ 115 - 13+50 \\ 115 - 14+00 \\ 115 - 14+25 \\ 115 - 14+50 \\ 115 - 14+50 \\ 115 - 14+50 \\ 116 - 05+25 \\ 116 - 05+50 \\ 116 - 05+50 \\ 116 - 05+50 \\ 116 - 05+50 \\ 116 - 05+50 \\ 116 - 05+50 \\ 116 - 05+50 \\ 116 - 05+50 \\ 116 - 05+50 \\ 116 - 05+50 \\ 116 - 05+50 \\ 115 - 05+5$	10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	$\begin{array}{c} 0.2 \\ 0.2 \\ 0.2 \\ 0.2 \\ 0.2 \\ 0.2 \\ 0.3 \\ 0.4 \\ 0.2 \\ 1.6 \\ 1.2 \\ 1.6 \\ 1.2 \\ 1.4 \\ 0.6 \\ 0.2 \\ 0.4 \\ 0.2 \\ 1.4 \\ 0.2 \\ 1.4 \\ 0.2 \\ 0.2 \\ 1.0 \\ 0.2 \\$		70         60           60         50           50         50           100         40           20         30           70         60           30         80           70         60           30         80           70         60           30         80           70         40           40         50           80         40           50         30           30         30		ප් ප් ප් ප් ප් ප් ප් ප් ප් ප් ප් ප් ප් ප	13 32 7 11 14 10 7 5 8 21 14 20 11 20 4 10 8 22 12 10 18 8 22 12		5 8 4 4 3 4 5 6 4 3 2 5 4 5 1 2 2 3 5 1 1 2 2 3 5 6 1 1 2 2 3 5 6 1 1 1 2 2 3 5 6 1 1 1 1 1 1 1 1 1 1 1 1 1	11           15           14           16           35           16           7           18           18           18           19           7	12 15 26 8 14 10 8 14 10 12 8 6 4 14 14 24 104 8 8 2 16 8 14 10 12 8 8 14 10 12 15 14 10 10 12 15 14 10 10 12 15 14 10 10 12 12 14 10 10 12 12 14 10 10 12 14 10 10 12 12 14 10 12 12 14 10 12 14 10 12 12 14 10 12 14 10 10 12 12 14 10 10 12 14 14 10 10 12 14 14 10 12 14 14 10 12 14 14 10 12 14 14 10 10 12 14 14 10 10 12 14 14 10 10 12 14 14 10 10 12 14 14 10 10 12 14 14 14 16 16 16 16 16 17 16 16 16 16 16 16 16 16 16 16		80         80           118         104           52         84           74         54           100         76           74         158           40         64           64         64           134         94	
$\begin{array}{r} 15 - 09+25 \\ 115 - 09+50 \\ 115 - 09+50 \\ 115 - 10+00 \\ 115 - 10+25 \\ 115 - 10+75 \\ 115 - 11+25 \\ 115 - 11+25 \\ 115 - 11+25 \\ 115 - 11+75 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 13+50 \\ 115 - 13+50 \\ 115 - 14+00 \\ 115 - 14+25 \\ 115 - 14+50 \\ 115 - 14+50 \\ 116 - 05+25 \\ 116 - 05+50 \\ 116 - 05+5$	12 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	c.2           c0.2           c0.4           c0.2		70         60           60         50           50         50           100         40           20         30           70         60           30         80           70         60           50         50           80         70           40         40           50         50           80         40           50         30           20         30           20         30	x a a a a a a a a a a a a a a a a a a a	03           03	13       32       7       11       14       10       7       5       8       21       14       20       11       20       4       10       8       22       12       10       18       6		5 6 4 4 3 5 6 4 5 1 2 2 3 5 1 2 2 3 5 10 5 10 5 1	11           15           14           16           35           16           6           7           5           12           16           8           16           18           7           8           10           53           10           19           7           5	12 15 26 8 14 10 8 10 12 8 6 4 14 24 104 8 8 2 16 8 4 14 104 10 12 12 12 13 14 10 10 12 12 12 13 14 10 10 12 12 12 12 12 12 14 10 12 12 12 12 12 12 12 14 10 12 12 12 12 12 12 12 12 14 10 12 12 12 12 12 12 12 12 12 12		80         80           118         104           52         98           98         62           84         74           54         100           78         96           74         158           40         64           64         64           134         94           98         64	
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$\begin{array}{c} 115 - 09+25 \\ 115 - 09+50 \\ 115 - 09+50 \\ 115 - 10+00 \\ 115 - 10+25 \\ 115 - 10+75 \\ 115 - 10+75 \\ 115 - 11+25 \\ 115 - 11+25 \\ 115 - 11+75 \\ 115 - 12+75 \\ 115 - 12+75 \\ 115 - 12+75 \\ 115 - 12+75 \\ 115 - 13+25 \\ 115 - 13+25 \\ 115 - 13+25 \\ 115 - 13+25 \\ 115 - 14+00 \\ 115 - 14+25 \\ 115 - 14+50 \\ 115 - 14+50 \\ 116 - 05+25 \\ 116 - 05+50 \\ 116 - 06+25 \\ 116 - 06+$	10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.2         0.2           0.2         0.2           0.2         0.2           0.2         0.2           0.8         2.4           1.8         1.8           1.8         1.6           0.2         0.2           0.3         0.2           0.4         0.6           0.2         0.2           1.4         0.6           0.2         0.2           0.2         0.2           0.2         0.2           0.2         0.2           0.2         0.2           0.2         0.2           0.2         0.2           0.2         0.2           0.2         0.2	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	70           60           50           50           50           100           40           20           30           70           60           330           80           70           60           330           80           70           40           50           50           30           20           50           50           50           50           50           70	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	03           03	13       32       7       11       14       10       7       5       8       21       14       20       11       20       4       10       8       22       12       10       18       6       5		5 6 4 4 3 4 5 6 4 3 2 5 4 5 1 2 2 3 6 10 5 4 3 5 10 5 4 3 5 5 6 10 5 5 5 6 10 5 5 5 5 6 5 5 5 5 5 5 5 5 5 5 5 5 5	11           15           14           16           35           16           8           16           18           19           7           5           10           19           7           5           11           27	12 15 26 8 14 10 12 8 4 14 10 12 8 8 4 14 104 8 8 2 16 8 14 10 12 12 13 14 10 10 12 12 13 14 10 10 12 12 14 10 10 12 12 14 10 10 12 12 14 10 10 12 12 14 10 10 12 12 14 10 10 12 12 14 10 10 12 12 14 10 10 12 14 10 10 12 12 14 10 10 12 14 10 10 12 14 10 10 12 12 14 10 10 10 12 12 14 10 10 10 10 10 10 10 10 10 10	2 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	30           80           118           104           52           98           98           62           84           74           54           100           78           96           94           64           64           64           64           64           64           64           64           62           92           92	
$\begin{array}{rrrr} 15 & - & 09+25 \\ 115 & - & 09+50 \\ 115 & - & 09+50 \\ 115 & - & 10+00 \\ 115 & - & 10+25 \\ 115 & - & 10+75 \\ 115 & - & 10+75 \\ 115 & - & 11+25 \\ 115 & - & 11+25 \\ 115 & - & 11+75 \\ 115 & - & 12+25 \\ 115 & - & 12+75 \\ 115$	12 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	c.1.2         c0.2         c0.2         c0.2         c0.2         c0.2         c0.3         2.4         1.8         1.6         1.2         1.4         c.6         c.2         1.4         c.4         c.2         c.2         1.4         c0.2         c0.2 <t< td=""><td>0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0</td><td>70           60           50           50           50           50           50           50           50           70           80           70           80           70           80           70           80           70           80           70           40           40           50           50           50           70           20</td><td>0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0</td><td>03           03</td><td>13         32         7         11         14         10         7         5         8         21         14         20         11         20         4         10         8         22         12         10         18         6         15         5         5</td><td></td><td>5 6 4 4 3 5 6 4 3 2 5 4 5 1 2 2 3 3 6 10 5 4 3 4 5 6 10 5 4 5 6 10 5 6 10 10 10 10 10 10 10 10 10 10</td><td>11           15           14           16           33           16           18           19           7           5           10           33           10           19           7           5           11           27           6</td><td>12 15 26 5 14 10 10 10 12 8 6 4 14 24 104 8 8 2 16 8 4 14 10 12 12 12 13 10 10 12 12 14 10 10 10 12 12 14 10 10 10 12 12 14 10 10 12 14 10 10 12 12 14 10 10 12 14 10 10 12 12 14 14 10 10 12 12 14 14 10 10 12 14 14 10 10 12 12 14 14 14 14 10 10 12 14 14 14 14 14 14 14 14 14 14</td><td>2 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2</td><td>300           800           1118           104           52           98           98           62           54           74           54           100           78           965           74           54           100           78           965           74           54           100           78           965           74           54           100           78           965           74           54           158           40           64           64           62           92           50</td><td></td></t<>	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	70           60           50           50           50           50           50           50           50           70           80           70           80           70           80           70           80           70           80           70           40           40           50           50           50           70           20	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	03           03	13         32         7         11         14         10         7         5         8         21         14         20         11         20         4         10         8         22         12         10         18         6         15         5         5		5 6 4 4 3 5 6 4 3 2 5 4 5 1 2 2 3 3 6 10 5 4 3 4 5 6 10 5 4 5 6 10 5 6 10 10 10 10 10 10 10 10 10 10	11           15           14           16           33           16           18           19           7           5           10           33           10           19           7           5           11           27           6	12 15 26 5 14 10 10 10 12 8 6 4 14 24 104 8 8 2 16 8 4 14 10 12 12 12 13 10 10 12 12 14 10 10 10 12 12 14 10 10 10 12 12 14 10 10 12 14 10 10 12 12 14 10 10 12 14 10 10 12 12 14 14 10 10 12 12 14 14 10 10 12 14 14 10 10 12 12 14 14 14 14 10 10 12 14 14 14 14 14 14 14 14 14 14	2 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	300           800           1118           104           52           98           98           62           54           74           54           100           78           965           74           54           100           78           965           74           54           100           78           965           74           54           100           78           965           74           54           158           40           64           64           62           92           50	
$\begin{array}{c} 115 - 09+25 \\ 115 - 09+50 \\ 115 - 09+50 \\ 115 - 10+00 \\ 115 - 10+25 \\ 115 - 10+73 \\ 115 - 11+25 \\ 115 - 11+25 \\ 115 - 11+25 \\ 115 - 11+75 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 13+25 \\ 115 - 13+25 \\ 115 - 14+20 \\ 115 - 14+25 \\ 115 - 14+$	12 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	c.2         c0.2          c0.2	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	70           60           50           50           50           50           50           50           50           50           50           50           50           50           30           70           60           30           80           70           40           40           50           50           50           50           50           50           70           20           30	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	03           03	13         32         7         11         14         10         7         5         8         21         14         20         4         10         8         22         12         10         18         6         15         8         8		5       6       4       3       4       5       6       4       3       2       5       4       5       1       2       3       6       10       5       4       3       6       10       5       4       3	11         15         14         16         35         16         7         5         12         16         16         17         8         10         19         7         5         11         27         8         10	12 15 26 5 14 10 10 12 8 6 4 14 10 12 8 6 4 14 14 10 12 8 8 4 14 10 12 8 8 14 10 10 12 8 8 14 10 10 12 10 12 12 15 14 10 10 12 15 16 10 10 12 16 16 10 12 16 16 10 12 16 16 16 16 16 16 16 16 16 16	2 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	300           118           104           52           98           94           94           98           92           50           44	
$\begin{array}{r} 15 & - & 09+25 \\ 115 & - & 09+50 \\ 115 & - & 10+00 \\ 115 & - & 10+25 \\ 115 & - & 10+75 \\ 115 & - & 10+75 \\ 115 & - & 11+75 \\ 115 & - & 11+75 \\ 115 & - & 11+75 \\ 115 & - & 11+75 \\ 115 & - & 12+25 \\ 115 & - & 12+25 \\ 115 & - & 12+25 \\ 115 & - & 12+75 \\ 115 & - & 12+75 \\ 115 & - & 12+75 \\ 115 & - & 12+75 \\ 115 & - & 11+75 \\ 115 & - & 11+25 \\ 115 & - & 11+25 \\ 115 & - & 11+25 \\ 115 & - & 11+25 \\ 115 & - & 11+25 \\ 115 & - & 11+25 \\ 115 & - & 11+25 \\ 115 & - & 11+25 \\ 115 & - & 11+25 \\ 115 & - & 11+25 \\ 115 & - & 11+25 \\ 115 & - & 11+25 \\ 115 & - & 11+25 \\ 115 & - & 11+25 \\ 115 & - & 05+25 \\ 116 & - & 06+25 \\ 116 & - & 06+25 \\ 116 & - & 06+25 \\ 116 & - & 06+25 \\ 116 & - & 06+75 \\ 116 & - & 07+00 \\ 116 & - & 07+25 \\ \end{array}$	12 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	c.2         c0.2         c0.2 <tr< td=""><td>2 2 2 2 2 2 2 2 3 3 4 5 2 3 4 5 2 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5</td><td>70           60           50           50           50           50           30           70           60           30           70           60           30           70           60           30           80           70           60           30           80           70           60           50           50           50           50           50           50           50           50           50           50           50           50           50           50           70           20           30           10</td><td>0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0</td><td>03           03</td><td>13         32         7         11         14         10         7         5         8         21         14         20         11         20         4         10         8         22         12         10         18         6         5         8         11</td><td></td><td>5 6 4 4 3 4 5 6 4 3 2 5 4 5 1 2 2 3 5 1 2 2 3 5 4 5 1 2 2 5 4 5 4 5 6 4 5 6 4 5 6 6 6 7 7 7 7 7 7 7 7 7 7 7 7 7</td><td>11         15         14         16         35         18         6         7         5         12         16         8         10         33         10         13         10         13         10         5         11         27         6         10         5         11         27         5         10         5         11         27         5         10         5</td><td>12 15 26 8 14 10 12 8 6 4 14 10 12 8 8 4 14 104 8 8 2 16 8 2 16 14 10 12 8 8 14 10 10 12 12 16 14 10 10 12 12 16 14 10 10 12 12 16 14 10 10 12 12 16 14 10 10 12 16 14 10 10 12 16 14 10 10 12 16 14 10 10 12 16 16 16 16 16 16 16 16 16 16</td><td>2 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2</td><td>30           80           118           104           52           98           94           94           94           94           94           84</td><td></td></tr<>	2 2 2 2 2 2 2 2 3 3 4 5 2 3 4 5 2 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	70           60           50           50           50           50           30           70           60           30           70           60           30           70           60           30           80           70           60           30           80           70           60           50           50           50           50           50           50           50           50           50           50           50           50           50           50           70           20           30           10	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	03           03	13         32         7         11         14         10         7         5         8         21         14         20         11         20         4         10         8         22         12         10         18         6         5         8         11		5 6 4 4 3 4 5 6 4 3 2 5 4 5 1 2 2 3 5 1 2 2 3 5 4 5 1 2 2 5 4 5 4 5 6 4 5 6 4 5 6 6 6 7 7 7 7 7 7 7 7 7 7 7 7 7	11         15         14         16         35         18         6         7         5         12         16         8         10         33         10         13         10         13         10         5         11         27         6         10         5         11         27         5         10         5         11         27         5         10         5	12 15 26 8 14 10 12 8 6 4 14 10 12 8 8 4 14 104 8 8 2 16 8 2 16 14 10 12 8 8 14 10 10 12 12 16 14 10 10 12 12 16 14 10 10 12 12 16 14 10 10 12 12 16 14 10 10 12 16 14 10 10 12 16 14 10 10 12 16 14 10 10 12 16 16 16 16 16 16 16 16 16 16	2 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	30           80           118           104           52           98           94           94           94           94           94           84	
$\begin{array}{r} 15 - 09+25 \\ 115 - 09+50 \\ 115 - 10+00 \\ 115 - 10+25 \\ 115 - 10+75 \\ 115 - 10+75 \\ 115 - 11+75 \\ 115 - 11+75 \\ 115 - 11+75 \\ 115 - 11+75 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 12+25 \\ 115 - 13+25 \\ 115 - 13+25 \\ 115 - 14+00 \\ 115 - 14+25 \\ 115 - 14+25 \\ 115 - 14+25 \\ 115 - 14+25 \\ 115 - 14+25 \\ 115 - 08+00 \\ 116 - 08+55 \\ 116 - 08+55 \\ 116 - 08+55 \\ 116 - 08+55 \\ 116 - 07+25 \\ 116 - 07+25 \\ 116 - 07+50 \\ \end{array}$	12 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	c.2           c0.2	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	70           60           50           50           50           50           50           50           50           50           30           70           60           30           80           70           60           30           80           70           60           30           80           70           60           50           70           20           30           20           30           20           30           20           50           70           20           30           10           70	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	03           03	13         32         7         11         14         10         7         5         8         21         14         20         11         20         4         10         8         22         12         10         18         6         8         115         5         8         11         16		5 6 4 4 3 4 5 6 4 3 2 5 4 5 1 2 2 3 3 6 10 5 4 3 4 3 5 6 10 5 4 3 5 6 10 5 6 10 10 10 10 10 10 10 10 10 10	11           15           14           16           35           18           6           7           5           12           16           8           16           7           5           12           16           8           10           53           10           13           7           5           11           27           6           10           5           11           27           6           10           5           11	12 15 26 8 14 10 10 12 8 6 4 14 10 12 8 8 24 104 8 8 2 16 8 2 16 14 10 12 8 8 14 10 10 12 10 10 10 12 10 10 10 10 10 10 10 10 10 10		80           80           118           104           52           98           98           62           84           74           54           100           78           96           74           158           40           64           64           64           64           64           64           64           64           64           64           64           64           64           62           92           50           44           128	

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LIG - 14400		<b>KU</b> 2	•	50	2	0.5	23	26	3	20	5	<u> </u>	96
L18 - 14+25		<0.2	2	40	2	<0.5	15	18	3	12	4	2	64
L19 - 05+25	<5	<0.2	2	50	_2	0.5	27	18	9	8	8	2	76
L19 - 05+50	<5	8.0	8	10	2	<0.5	1	12	5	<1	10	2	32
L19 - 05+75	<5	0.8	14		2	<0.5	7	12	4	6	10	<3	48
L19 - 06+00	<5	0.2	6	80	2	2.0	15	21	3	19	12	2	216
L19 - 06+25	<5	0.4	6	80	2	<0.5	23	25	1	21	14	2	160
L19 - 07+00	<5	0.6	4	50	2	<0.5	11	13	3	9	8	2	80
L19 - 07+25	<5	0.8	20	30	2	<0.5	4	5	4	9	10	2	94
L19 - 07+50	ব	0.2	4	50	2	<0.5	9	13	1	11	6	2	58
L19 - 05+00	<5	<0.2	4	30	0	<0.5	3	11	4	5	2	0	54
L19 - 08+50	6	02	12	30	0	(05	10	11	5		10		58
119 - 08475		14	10	- <del></del>		705		21				4	
119 - 00175					4					- 10			
L19 - 09+23		cu.z	2		4	<0.5	20	15	1	19	4	4	90
L19 - 09450		1.0	20		a	<0.5	9	15	. 8	11	12	3	90
L19 - 09+75	<5	0.8	20	40	2	<0.5	8	8	. 6	13	10	<2	96
L19 - 10+25	<5	0.6	4	30	2	<0.5	7	14	5	16	12	2	78
L19 - 10+75	<5	0.4	10	80	Q	<0.5	26	20	<1	32	18	2	96
L19 - 11+00	<5	0.8	0	40	4	<0.5	20	17	1	7	10	2	64
L19 - 11+25	<5	<0.2	16	90	2	<0.5	16	22	3	33	12	4	150
L19 - 11+50	<5	<0.2	6	50	2	<0.5	7	12	3	10	6	2	46
L19 - 11+75	<5	<0.2	24	60	a	<0.5	10	22	1	38	i i	0	78
120 - 05+50	6	10	16	100	0	(05	7	10	- <u>-</u> R	16	14		254
120 - 06400	15	1.00	20	50	4	10.5	<u>-</u>			10	14	<u> </u>	204
100 - 00100		0.0		30	4	<0.5	10	14	•	10	10	a	/6
LOU - VO+30	- 52	SV-4	4	/0	. 4	<0.5	- 20	<u> </u>		. 8.	4	3	- 48
120 - 96+75	<u></u>	<u> </u>	5	10	2	<0.5	4	3_	6	3	12	2	
120 - 07+00	- <5	92	2	- 40	2	<0.5	1	6.	+	10	12	4	_ 90
L20 - 07+25	<5	0.4	4	50	8	0.5			2	10	2	2	<b>42</b>
L20 - 07+50	<5	12	4	50	2	<0.5	10	15	6	25	12	2	. 174
120 - 07+75	<5	0.2	2	40	2	<0.5	9	17	3	15	4	a	58
L20 - 08+00	4	<0.2	.16	40	2	<0.5	. 9	178	5	19	10	2	100
120 - 05+25	<5	0.2	16	60	2	<0.5	17	28	4	17	12	0	102
120 - 08+50	<5	<0.2	4	40	0	<0.5	9	13	3	8	6	a	46
120 - 08+75	<5	0.6	8	30	0	<0.5	9	18	5	9		0	54
120 - 09+00	<5	0.8	24	70	0	0.5	26	31	7	30	24		242
120 - 00+25		20		30			10	<u> </u>			49		- 476
120 - 00160		40		8	~	(0.5	- 10			~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	10	-4	
		0.2	•		2	<0.5	16			20	10	4	
L20 - 09+75	<5	0.2	8		0	<0.5	11	18		22	2	4	92
10+00	<5	0.2	_ <2	30	<2	_ <0.5			4		6	4	66
L20 - 10+25	<5	0.4	6		2	<0.5	9	13	3	5	6	2	46
L20 - 10+50	<5	0.2	16	50	2	<0.5	14	23	. 1	14	6	<2	136
L20 - 11+00	<5	0.2	88	30	2	<0.5	9	15	4	7	12	2	56
L20 - 11+50	950	0.6	14	80	Ø	<b>(05</b>	39	21	3	41	262	4	106
L20 - 11+75	<5	0.2	16	30	Ø	<0.5	9	15	4	22	6	2	72
120 - 12+25	4	0.2		90	0	(05	13	15	1				
121 - 05+50		(02		80	~	/05	10	10	1	14			124
		0.0		110	<u> </u>				3			<u> </u>	
	-9	<u>uz</u>	14		4	25	- 8	<b>9</b>		20	12	<u> </u>	305
L21 - 06+50	<u>a</u>	<0.2	_ 2_	70	9	<u>&lt;0.5</u>	_ 12 .		_ <l< td=""><td>. 10</td><td><u> </u></td><td>4</td><td>72</td></l<>	. 10	<u> </u>	4	72
<u>121 - 06+75</u>	<b></b>	<u>_0.8</u>	14.	- 50	2		_13_	13	3		. 12	4	66_
121 - 07+00			~	40	2	<0,5	11	12	2	_ 14	2	2	
	ব	0.2	<u> </u>									_	100
121 - 07+25	্র ত	0.2	6	1 <b>00</b>	2	<0.5	18	25_	<1	16	8	4	100
L21 - 07+25 L21 - 07+50	র র র	0.2	6 14	100 20	2		18 3	<u>25</u>	<u>&lt;1</u>	_1 <u>6</u> 1	8 12	2	62
L21 - 07+25 L21 - 07+50 L21 - 07+75	0 0 0 0	0.2 0.4 1.2 0.2	6 14 12	100 20 30	0 0 0 0	্ণয় ্থ্য ্থ্য	18 5	<u>25</u> 39	<1 6 3	1 4	8 12 15	4 4 4	<u>62</u> 35
$\begin{array}{r} 121 - 07+25 \\ 121 - 07+50 \\ 121 - 07+75 \\ 121 - 06+25 \end{array}$	0 0 0 0 0 0 0	0.2 0.4 1.2 0.2 (0.2	6 14 12 6	100 20 30 40	A A A A	୍ ପ୍ ସ୍ଥ ପ୍ର ପ୍ର ପ୍ର	18 	<u>25</u> 3 <u>9</u> 21	<1 6 3 4	16 1 9	8 12 15 8	8 8 8	62 36 62
$\begin{array}{r} 121 & -07+25 \\ 121 & -07+50 \\ 121 & -07+75 \\ 121 & -08+25 \\ 121 & -08+50 \\ \end{array}$	ୟ ସ ସ ପ ପ 10	0.2 0.4 1.2 0.2 0.2 0.2 0.2	6 14 12 6 14	100 20 30 40 50	0 0 0 0 0	୍ୟ୍ୟ ୍ୟୁ ୍ୟୁ ୍ୟୁ ୍ୟୁ ୍ୟୁ ୍ୟୁ	18 3 5 13 42	25 3 9 21 72	<1 6 3 4 10	16 1 4 9 11	8 12 16 8 18	8 8 8 8	62 36 62 84
$\begin{array}{r} 121 & - & 07+25 \\ 121 & - & 07+50 \\ 121 & - & 07+75 \\ 121 & - & 08+25 \\ 121 & - & 08+50 \\ 121 & - & 08+75 \\ 121 & - & 08+75 \\ \end{array}$	ଷ ଷ ଷ ପ ପ 10	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	6 14 12 6 14 8	100 20 30 40 50 60	0 0 0 0 0 0 0	୍ଟ୍ର ୍ଟ୍ର ୍ଟ୍ର ୍ଟ୍ର ୍ଟ୍ର ୍ଟ୍ର ୍ଟ୍ର	18 3 5 13 42 17	25 3 9 21 72 28	<1 6 3 4 10 1	18 1 9 11 11	8 12 15 8 18	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	62 55 62 84
$\begin{array}{r} 121 - 07+25 \\ 121 - 07+25 \\ 121 - 07+50 \\ 121 - 07+75 \\ 121 - 08+25 \\ 121 - 08+50 \\ 121 - 08+75 \\ 121 - 08+75 \\ 121 - 09+00 \\ \end{array}$	8 8 8 8 8 8 8 8 9 8 8 9 8 9 8 9 8 9 8 9	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	6 14 12 6 14 8 72	100 20 30 40 50 60 60	0 0 0 0 0 0 0 0 0	୍ଷ୍ୟ ୍ଷ୍ୟ ୍ଷ୍ୟ ୍ଷ୍ୟ ୍ଷ୍ୟ ୍ଷ୍ୟ ୍ଷ୍ୟ ୍ଷ୍ୟ	18 3 5 13 42 17 24	25 3 9 21 72 28 122	<1 6 3 4 10 1	16 1 4 9 11 11 7	8 12 16 8 18 14	3 8 8 8 8 8	62 36 62 84 110
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21 - 07+25 121 - 07+25 121 - 07+50 121 - 08+25 121 - 08+50 121 - 08+75 121 - 09+00 121 - 09+25 121 - 09+25 121 - 09+50 121 - 09+50	00000000000000000000000000000000000000	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.4 2.0	8 14 12 6 14 8 22 6 6	100 20 30 40 50 80 80 80 80 80 80 80	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	දය දය දය දය දය දය දය දය දය දය දය	18 3 5 13 42 17 24 17 18	25 3 9 21 72 28 122 23 23 25	<1 6 3 4 10 1 1 2 5	16 1 9 11 11 7 22 13	8 12 16 8 18 14 36 10		62 36 62 84 110 88 136 142
21 - 07+25 121 - 07+25 121 - 07+50 121 - 08+25 121 - 08+50 121 - 08+50 121 - 08+75 121 - 09+00 121 - 09+25 121 - 09+50 121 - 10+00	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0	6 14 12 6 14 8 22 6 6 6 18	100 20 30 40 50 80 80 80 80 90 40 30	1 A A A A A A A A A A A	ද ද ද ද ද ද ද ද ද ද ද ද ද ද ද ද ද ද ද	18 3 5 13 42 17 24 17 18 3	25 3 9 21 72 28 122 23 25 8 6	<1 6 3 4 10 1 1 2 5 4	16 1 9 11 11 7 22 13 6	8 12 16 8 18 14 36 10 10 10	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	100 62 36 62 84 110 88 136 138 142 94
$\begin{array}{c} 21 - 07 + 25 \\ 121 - 07 + 25 \\ 121 - 07 + 50 \\ 121 - 08 + 50 \\ 121 - 08 + 50 \\ 121 - 08 + 50 \\ 121 - 08 + 75 \\ 121 - 08 + 75 \\ 121 - 09 + 25 \\ 121 - 09 + 25 \\ 121 - 09 + 50 \\ 121 - 10 + 00 \\ 121 - 10 + 00 \\ 121 - 10 + 25 \\ 121 - 10$	ଷ ଷ ଷ ଷ ଷ ଷ ଷ ଷ ଷ ଷ ଷ ଷ ଷ ଷ ଷ ଷ ଷ ଷ ଷ	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.4 2.0 0.4 1.2	6 14 12 6 14 8 22 6 6 6 18 14	100 20 30 40 50 80 80 80 90 40 30 20		<ul> <li>ද්‍t</li> <li>ද</li> <li< td=""><td>18 3 5 13 42 17 24 17 18 3 3 3</td><td>25 3 9 21 72 28 122 23 25 8 9 9</td><td>&lt;1 6 3 4 10 1 1 2 5 5 8 8</td><td>16 1 4 9 11 11 7 22 13 6 6</td><td>8 12 16 8 18 18 14 38 10 10 10 8 8 8</td><td>8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8</td><td>100 62 36 62 84 110 88 136 142 94 80</td></li<></ul>	18 3 5 13 42 17 24 17 18 3 3 3	25 3 9 21 72 28 122 23 25 8 9 9	<1 6 3 4 10 1 1 2 5 5 8 8	16 1 4 9 11 11 7 22 13 6 6	8 12 16 8 18 18 14 38 10 10 10 8 8 8	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	100 62 36 62 84 110 88 136 142 94 80
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$\begin{array}{c} 21 & - & 07 + 25 \\ 121 & - & 07 + 25 \\ 121 & - & 07 + 50 \\ 121 & - & 07 + 75 \\ 121 & - & 08 + 50 \\ 121 & - & 08 + 50 \\ 121 & - & 08 + 75 \\ 121 & - & 09 + 00 \\ 121 & - & 09 + 25 \\ 121 & - & 09 + 50 \\ 121 & - & 10 + 00 \\ 121 & - & 10 + 25 \\ 121 & - & 10 + 50 \\ 121 & - & 10 + 75 \\ $	ଷ ପ ପ ପ ପ ପ ପ ପ ପ ପ ପ ପ ପ ପ ପ ପ ପ ପ ପ ପ	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.4 0.4 1.2 0.4 1.2 0.8	6 14 12 6 14 8 22 6 6 6 18 14 22 4	100 20 30 40 50 60 80 80 90 40 30 20 140 50	~ a a a a a a a a a a a a	ê cê	18         3         5         13         42         17         24         17         18         3         3         16         11         11         11         11         12         12         12         13         13         16         11         11         12         12         13         14         15         16         11         11         12         12         13         14         15         14         15         16         11         11         12	25 3 9 21 72 28 122 23 25 8 9 25 8 9 26 17	<1 6 3 4 10 1 1 2 5 5 4 8 24 3	16 1 4 9 11 11 7 7 22 13 6 6 41 18	\$           12           16           8           18           14           36           10           10           8           20           10	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	100 62 38 62 84 110 88 136 142 94 80 552 66
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	&     &       & <td>0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.4 2.0 0.4 1.2 0.2 0.4 1.2 0.2 0.8 0.2 0.6</td> <td>3         14           12         6           14         12           6         16           14         22           6         6           10         14           22         4           5         14</td> <td>100 20 30 40 50 60 80 90 30 20 140 50 50 70</td> <td>00~00000000000000000000000000000000000</td> <td>ê ê ê ê ê ê ê ê ê ê ê ê</td> <td>18       3       5       13       42       17       24       17       18       3       18       11       12</td> <td>25 3 9 21 72 28 122 23 25 8 9 25 8 9 25 17 20 12</td> <td>&lt;1 6 3 4 10 1 1 2 5 4 8 8 24 3 3 3 4</td> <td>16 1 4 9 11 11 7 22 13 6 6 6 41 18 18 14 7</td> <td>8           12           16           8           18           14           38           10           10           8           8           20           10           8           10           10           8           10           10           10           10           10</td> <td>0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0</td> <td>100 62 36 62 84 110 88 136 136 142 94 80 3552 86 86 86 86 86</td>	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.4 2.0 0.4 1.2 0.2 0.4 1.2 0.2 0.8 0.2 0.6	3         14           12         6           14         12           6         16           14         22           6         6           10         14           22         4           5         14	100 20 30 40 50 60 80 90 30 20 140 50 50 70	00~00000000000000000000000000000000000	ê ê ê ê ê ê ê ê ê ê ê ê	18       3       5       13       42       17       24       17       18       3       18       11       12	25 3 9 21 72 28 122 23 25 8 9 25 8 9 25 17 20 12	<1 6 3 4 10 1 1 2 5 4 8 8 24 3 3 3 4	16 1 4 9 11 11 7 22 13 6 6 6 41 18 18 14 7	8           12           16           8           18           14           38           10           10           8           8           20           10           8           10           10           8           10           10           10           10           10	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	100 62 36 62 84 110 88 136 136 142 94 80 3552 86 86 86 86 86
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0         0	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.4 2.0 0.4 2.0 0.4 1.2 0.2 0.4 0.4 2.0 0.4 0.4 2.0 0.4 0.4 2.0 0.4 0.4 2.0 0.4 0.4 0.4 0.2 0.4 0.2 0.2 0.4 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	3         14           12         6           14         12           6         14           8         22           6         6           18         14           22         6           6         16           14         22           5         14           4         2	100 20 30 40 50 60 60 60 60 40 30 20 140 50 50 70 70 20 40	a ~ a a ~ a a a a a a a a a a a a a	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	18       3       5       13       42       17       24       17       18       3       16       11       12       6       9	25 3 9 21 72 26 122 23 25 8 9 9 25 17 20 12 7 12	<1 6 3 4 10 1 1 2 5 4 8 8 24 3 3 4 7 4	16 1 4 9 11. 11. 7 22. 13. 6 6 41. 18. 14. 7, 4. 13. 14. 7, 4. 13. 14. 7, 14. 18. 19. 19. 11. 11. 11. 11. 11. 11	8 12 16 8 18 14 36 10 10 8 8 20 10 8 10 10 10 10	a a a a a a a a a a a a a a a a a a a	100 62 36 62 84 110 88 136 142 94 80 352 86 85 85 92 84 118
$\begin{array}{c} 21 - 07 + 25 \\ 121 - 07 + 25 \\ 121 - 07 + 50 \\ 121 - 08 + 50 \\ 121 - 08 + 50 \\ 121 - 08 + 50 \\ 121 - 08 + 50 \\ 121 - 08 + 75 \\ 121 - 09 + 25 \\ 121 - 09 + 50 \\ 121 - 10 + 25 \\ 121 - 10 + 25 \\ 121 - 10 + 50 \\ 121 - 10 + 50 \\ 121 - 11 + 50 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 12 + 60 \\ \end{array}$	0     0       0     0       0     0       0     0       0     0       0     0       0     0       0     0       0     0       0     0       0     0       0     0       0     0       0     0       0     0       0     0       0     0       0     0       0     0       0     0	0.2 0.4 1.2 0.2 0.2 0.2 0.4 0.4 2.0 0.4 1.2 0.2 0.4 1.2 0.2 0.8 0.2 0.8 0.2 0.8 0.2 0.8 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	2 14 12 6 14 14 8 22 6 6 18 14 22 4 5 14 14 22 18	100 20 30 40 50 60 60 60 60 60 40 40 30 20 140 50 50 50 70 20 20 20 50 50 50 50 50 50 50 50 50 50 50 50 50	~ a ~ a a a a a a a a a a a a a	ê ê ê ê ê ê ê ê ê ê ê ê ê ê ê	18           .3           5           13           42           17           24           17           18           .3           18           .11           1.3           1.2           6           9           16	25 3 9 21 72 26 122 23 25 8 9 9 26 17 20 12 7 12 7 12 25	<1 6 3 4 10 1 1 1 2 5 4 4 8 8 24 3 3 4 7 7 4 2	16           1           4           9           11           11           7           22           13           6           6           61           18           14           7           4           13           25	8 12 16 8 18 14 36 10 10 8 8 20 10 8 8 10 10 10 10 10	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	100 62 36 62 84 110 88 136 142 94 80 352 86 86 86 86 92 64 116 112
$\begin{array}{c} 21 - 07 + 25 \\ 121 - 07 + 50 \\ 121 - 07 + 50 \\ 121 - 08 + 50 \\ 121 - 08 + 50 \\ 121 - 08 + 50 \\ 121 - 08 + 75 \\ 121 - 08 + 75 \\ 121 - 09 + 25 \\ 121 - 09 + 25 \\ 121 - 09 + 50 \\ 121 - 10 + 25 \\ 121 - 10 + 25 \\ 121 - 10 + 75 \\ 121 - 11 + 00 \\ 121 - 11 + 25 \\ 121 - 11 + 50 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 12 + 00 \\ 121 - 12 + 25 \\ 121 - 12$	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	0,2 0,4 1,2 0,2 0,2 0,2 0,2 0,4 1,2 0,4 1,2 0,4 1,2 0,4 1,2 0,4 1,2 0,4 0,4 1,2 0,4 0,4 0,4 0,4 0,4 0,4 0,4 0,4 0,4 0,2 0,4 0,2 0,2 0,4 0,4 0,2 0,2 0,4 0,2 0,2 0,4 0,2 0,2 0,2 0,4 0,2 0,2 0,4 0,2 0,2 0,2 0,4 0,4 0,2 0,2 0,4 0,4 0,4 0,4 0,4 0,4 0,4 0,4 0,4 0,4	2 14 14 14 14 14 8 22 6 6 16 14 22 4 5 14 14 22 4 14 14 22 14 14 14 12 14 14 14 14 14 14 14 14 14 14	100 20 30 40 50 60 60 90 40 30 20 20 140 50 50 70 20 20 20 40 50 50 50 80	0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	ය යි. සි. සි. සි. සි. සී. සී. සී. සී. සී. සී. සී. සී. සී. සී	18           3           5           13           42           17           24           17           18           11           13           12           6           9           16           9	25 3 9 21 72 28 122 23 25 8 9 9 25 17 20 12 7 7 12 26 15	<1 6 3 4 10 1 1 2 5 4 8 8 8 8 24 3 3 3 4 7 7 4 2 4	16           1           4           9           11           11           7           22           13           6           6           41           18           14           7           4           13           25           22	8           12           16           8           18           14           36           10           10           8           20           10           8           10           10           10           10           10           10           10           10           10           10           10           10	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	100 62 36 62 84 110 88 138 142 94 80 3352 86 86 86 88 92 64 116 112 70
$\begin{array}{c} 21 - 07 + 25 \\ 121 - 07 + 50 \\ 121 - 07 + 50 \\ 121 - 08 + 50 \\ 121 - 08 + 50 \\ 121 - 08 + 50 \\ 121 - 08 + 50 \\ 121 - 08 + 75 \\ 121 - 09 + 50 \\ 121 - 09 + 50 \\ 121 - 09 + 50 \\ 121 - 10 + 25 \\ 121 - 10 + 25 \\ 121 - 10 + 50 \\ 121 - 11 + 50 \\ 121 - 11 + 50 \\ 121 - 11 + 50 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 11 + 75 \\ 121 - 12 + 00 \\ 121 - 12 + 25 \\ 55810 \\ \end{array}$	0         0	0,2 0,4 1,2 0,2 0,2 0,2 0,4 2,0 0,4 2,0 0,4 1,2 0,4 1,2 0,4 1,2 0,5 0,2 0,2 0,2 0,2 0,2 0,2 0,2 0,2 0,2 0,2	22 6 6 14 8 22 6 6 6 18 14 22 6 6 18 14 22 4 4 5 14 22 4 14 21 14 14 22 10 16 10 -	100 20 30 40 50 60 60 90 40 30 20 140 50 50 70 20 40 50 80 110	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ê e ê ê ê ê ê ê ê ê ê ê ê ê ê ê ê ê ê ê	18           3           13           42           17           24           17           18           3           18           11           13           12           6           9           18           9           18           9           17	25 3 9 21 72 28 122 23 25 8 9 25 8 9 26 17 20 12 7 7 12 25 5 72	<1 6 3 4 10 1 1 2 5 4 8 8 24 3 3 4 7 7 4 4 2 4 4 1	16           1           4           9           11           11           7           22           13           6           6           41           18           14           7           4           13           25           22           14	8           12           16           8           18           14           36           10           10           8           20           10           8           10           10           10           10           10           10           10           10           10           10           10           10           10           6	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	100 62 36 62 84 110 88 138 142 94 80 552 86 85 92 86 92 86 116 112 70 65
1         07+25           121         07+25           121         07+75           121         08+25           121         08+50           121         08+50           121         08+50           121         08+50           121         08+50           121         09+00           121         09+25           121         09+25           121         09+25           121         19+00           121         10+75           121         10+75           121         11+25           121         11+25           121         11+75           121         11+25           121         11+50           121         11+75           121         11+75           121         12+50           121         12+55           56810         56811	0         0	0,2 0,4 1,2 0,2 0,2 0,2 0,4 2,0 0,4 2,0 0,4 2,0 0,4 1,2 0,4 2,0 0,4 1,2 0,4 2,0 0,4 2,0 0,4 2,0 0,4 2,0 0,4 2,0 0,4 0,4 0,2 0,4 0,4 0,2 0,2 0,4 0,4 0,2 0,2 0,4 0,4 0,2 0,2 0,2 0,4 0,4 0,4 0,2 0,2 0,2 0,4 0,4 0,4 0,4 0,4 0,4 0,4 0,4 0,4 0,4	3         6           14         12           12         6           14         8           22         6           6         16           14         2           4         6           18         10-           6         6	100 20 30 40 50 60 60 90 40 30 20 140 50 50 70 20 40 50 50 50 50 70 20 20 20 20 20 20 20 20 20 20 20 20 20	2 2 2 ~ 2 ~ 2 ~ 2 ~ 2 ~ 2 ~ 2 ~ 2 ~ 2 ~	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	18       3       5       13       42       17       24       17       18       3       16       11       13       12       6       9       16       17	25 3 9 21 72 28 122 23 25 8 9 25 8 9 25 8 9 25 17 20 12 7 12 7 12 7 12 5 15 72	<1 6 3 4 10 1 1 2 5 4 8 24 3 3 4 7 4 7 4 4 1 8	16       1       4       9       11       11       7       6       61       18       14       7       4       13       25       22       14       1	8           12           16           8           14           36           10           10           8           20           10           8           10           10           8           10           10           8           10           10           10           10           10           10           10           10           10           10           10           10           10		100 62 36 62 84 110 88 138 138 142 94 80 3552 86 85 92 84 118 112 70 66 50
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1         -07+25           121         -07+25           121         -07+75           121         -08+25           121         -08+50           121         -08+75           121         -08+75           121         -08+75           121         -09+00           121         -09+50           121         -10+50           121         -10+50           121         -10+75           121         -11+75           121         -11+75           121         -11+25           56810         -56811           56811         -56812	0         0	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.4 1.2 0.6 0.4 1.2 0.6 0.4 1.2 0.6 0.4 1.2 0.6 0.4 1.2 0.6 0.4 1.2 0.4 0.4 0.4 0.4 0.4 0.2 0.2 0.4 0.4 0.2 0.2 0.4 0.2 0.2 0.2 0.4 0.4 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.4 0.4 0.2 0.2 0.2 0.2 0.2 0.2 0.4 0.4 0.2 0.2 0.2 0.4 0.4 0.2 0.2 0.2 0.2 0.4 0.4 0.4 0.4 0.4 0.2 0.2 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	14           12           6           14           12           6           14           22           6           6           16           14           2           14           2           13           14           2           18           10-           6           23	100 20 30 40 50 60 60 60 60 70 30 20 140 50 50 70 20 70 20 20 110 200 110 200	3 2 2 2 4 2 4 2 2 2 2 2 2 2 2 2 2 2 2 2	2 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	18       3       5       13       42       17       24       17       18       3       18       11       13       12       6       9       16       9       17          10       11       12       6       9       16       9       17       <1	25 3 9 21 72 28 122 23 25 8 9 25 25 8 9 25 17 20 12 7 7 12 25 15 72 11 11	<1 6 3 4 10 1 1 2 5 5 4 8 24 3 3 3 4 7 4 24 3 3 4 4 7 4 1 6 6 4 4	16       1       4       9       11       11       11       7       6       6       41       18       14       7       4       13       25       22       14       1       7       4       13       25       22       14       1       7       .	8           12           16           8           14           36           10           10           8           20           10           8           20           10           8           10           10           8           10           110           12		100 62 36 62 84 110 86 135 142 94 80 3552 86 86 86 92 64 116 112 70 68 20 74 20
21         -07+25           121         -07+25           121         -07+75           121         -08+25           121         -08+50           121         -08+50           121         -08+50           121         -08+50           121         -08+50           121         -09+25           121         -09+50           121         -10+25           121         -10+75           121         -10+75           121         -11+75           121         -11+75           121         -11+75           121         -12+25           56810         56811           56813         56813	0         0	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.2 0.4 1.2 0.5 0.4 2.0 0.4 1.2 0.2 0.4 1.2 0.2 0.4 0.4 2.0 0.4 1.2 0.2 0.4 0.4 2.0 0.4 0.4 0.2 0.2 0.4 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	3         14           12         6           14         12           6         16           18         14           22         4           5         14           4         2           18         10-           6         28           8         28	100 20 30 40 50 60 60 90 40 30 20 140 50 50 70 20 20 20 100 50 50 50 20 20 100 100	x a a a a a a a a a a a a a a a a a a a	e e e e e e e e e e e e e e e e e e e	$   \begin{array}{c}     18 \\     3 \\     5 \\     13 \\     42 \\     17 \\     24 \\     17 \\     18 \\     3 \\     3 \\     18 \\     11 \\     12 \\     6 \\     9 \\     16 \\     9 \\     17 \\     12 \\     6 \\     9 \\     17 \\     <1 \\     4 \\     <1 \\     <1 \\     4 \\     <1 \\     7 \\   \end{array} $	25           3           9           21           72           26           122           23           25           8           9           25           17           20           12           7           12           7           12           7           12           26           15           72           1           11           1	<1 6 3 4 10 1 1 2 5 5 4 8 8 24 3 3 4 7 7 4 2 4 1 6 6 4 1	16       1       4       9       11       11       7       6       6       41       18       18       14       7       4       13       25       22       14       7       13       25       22       14       1       7       1	8         12         16         8         14         36         10         10         8         20         10         8         10         10         8         10         10         8         6         15         30         12	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	100           62           36           62           84           110           88           136           142           94           80           352           86           86           86           110           88           138           142           94           80           352           86           85           86           70           66           20           74           28
1         -07+25           121         -07+75           121         -07+75           121         -08+25           121         -08+50           121         -08+50           121         -08+50           121         -08+50           121         -08+75           121         -09+25           121         -09+50           121         -10+00           121         -10+75           121         -10+50           121         -11+75           121         -11+75           121         -11+75           121         -12+25           56810         -56811           56813         -56813           56814         -50413	0         0	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	2           14           12           6           14           8           22           6           6           18           14           2           6           18           10-           6           28           6           28           6           27	100 20 30 40 50 60 60 90 40 30 20 140 50 50 70 20 70 20 70 20 100 60 100 60 100		e e e e e e e e e e e e e e e e e e e	18       .3       13       42       17       24       17       18       3       18       11       13       16       9       17       18       9       17       18       9       17       4       <1	25 3 9 21 72 25 122 23 25 8 9 9 25 12 7 20 12 7 12 25 15 72 11 11 11 11 1 1 45	<1 6 3 4 10 1 1 2 5 4 8 8 24 3 3 4 7 7 4 2 4 1 6 6 4 1 8 5	16       1       4       9       11       11       7       13       6       61       18       14       7       4       13       25       22       14       7       1       1       7       1       8	8           12           16           8           14           36           10           10           8           20           10           8           10           10           8           10           10           8           10           10           8           6           18           30           12           14		100 62 36 62 84 110 88 136 142 94 80 3552 88 80 3552 88 80 92 84 116 112 70 88 20 74 28 82 20
1         -07+25           121         -07+75           121         -07+75           121         -08+25           121         -08+50           121         -08+50           121         -08+75           121         -08+75           121         -08+75           121         -09+25           121         -09+50           121         -10+00           121         -10+75           121         -10+75           121         -11+25           121         -11+75           121         -11+75           121         -12+25           56810         -56811           56813         -56814           56814         -56814	0     0 <td>0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.4 1.2 0.4 1.2 0.4 1.2 0.4 0.4 1.2 0.2 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2</td> <td>22           6           14           12           6           14           8           22           6           16           14           2           6           16           14           2           6           16           18           10-           6           228           6           223</td> <td>100 20 30 40 50 60 60 90 40 30 20 20 20 140 50 50 50 50 50 50 70 20 20 110 20 0 60 100 60 100 60</td> <td>C C C C C C C C C C C C C C C C C C C</td> <td>2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2</td> <td>18       3       13       42       17       24       17       18       3       18       11       13       16       9       16       9       17       &lt;1</td> 4       <1	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.4 1.2 0.4 1.2 0.4 1.2 0.4 0.4 1.2 0.2 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	22           6           14           12           6           14           8           22           6           16           14           2           6           16           14           2           6           16           18           10-           6           228           6           223	100 20 30 40 50 60 60 90 40 30 20 20 20 140 50 50 50 50 50 50 70 20 20 110 20 0 60 100 60 100 60	C C C C C C C C C C C C C C C C C C C	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	18       3       13       42       17       24       17       18       3       18       11       13       16       9       16       9       17       <1	25       3       9       21       72       26       122       23       25       8       9       26       17       20       12       7       12       7       12       7       12       7       15       72       1       11       1       4	<1 6 3 4 10 1 1 2 5 4 8 8 24 3 3 4 7 7 4 2 4 1 6 6 1 8 1	16       1       4       9       11       11       7       6       6       6       6       13       6       6       13       22       14       7       13       25       22       14       1       7       1       8       4	8         12         16         8         10         10         8         20         10         10         8         10         10         10         8         10         10         10         10         10         10         10         10         10         10         10         10         10         110         12         14         12         14         12		100 62 36 62 84 110 88 138 142 94 80 3352 86 86 88 92 64 116 112 70 66 20 74 28 82 34
1         -07+25           121         -07+75           121         -07+75           121         -08+25           121         -08+25           121         -08+75           121         -08+75           121         -08+75           121         -08+75           121         -09+00           121         -09+50           121         -10+25           121         -10+25           121         -10+75           121         -11+25           121         -11+25           121         -11+75           121         -12+00           121         -12+25           56810         -56811           56813         -56814           56814         -56815           56816	0     0       0     0	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 0.4 0.4 0.2 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	3         3	100 20 30 40 50 60 90 40 30 20 20 140 50 50 50 70 20 20 40 50 50 50 70 20 20 110 20 80 110 200 100 100 100	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Ê Ê Ê Ê Ê Ê Ê Ê Ê Ê Ê Ê Ê Ê Ê Ê Ê Ê Ê	18       3       13       42       17       24       17       18       11       13       16       9       16       9       17       16       9       17       14       17       4       3	25       3       9       21       72       28       122       25       8       9       25       8       9       28       17       20       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       4       4	<1 6 3 4 10 1 1 2 5 4 8 24 3 3 4 7 7 4 2 4 1 6 6 4 1 1 8 1 1	16       1       4       9       11       11       7       6       6       41       18       14       7       4       13       25       22       14       7       4       13       25       22       14       7       1       8       4       3	8         12         16         8         10         10         8         20         10         8         20         10         8         10         10         8         10         10         10         10         10         10         10         10         10         10         10         10         110         12         14         12         10	Q     Q <td>100 62 36 62 84 110 88 138 142 94 80 552 66 86 86 86 86 86 92 86 116 112 70 66 20 74 28 20 74 28 20 34 50</td>	100 62 36 62 84 110 88 138 142 94 80 552 66 86 86 86 86 86 92 86 116 112 70 66 20 74 28 20 74 28 20 34 50
1         -07+25           121         -07+75           121         -07+75           121         -08+25           121         -08+25           121         -08+75           121         -08+75           121         -08+75           121         -09+00           121         -09+25           121         -09+25           121         -09+50           121         -10+25           121         -10+75           121         -10+75           121         -11+25           121         -11+75           121         -11+75           121         -11+75           121         -12+25           56810         56811           56813         -56813           56814         -56816           56816         -56817	0     0 <td>0,2 0,4 1,2 0,2 0,2 0,2 0,2 0,4 2,0 0,4 2,0 0,4 2,0 0,4 1,2 0,4 2,0 0,4 1,2 0,2 0,4 0,4 2,0 0,4 2,0 0,4 2,0 0,4 2,0 0,4 0,4 0,4 0,2 0,4 0,4 0,2 0,4 0,4 0,2 0,4 0,4 0,2 0,4 0,4 0,2 0,4 0,4 0,4 0,4 0,4 0,4 0,4 0,4 0,4 0,4</td> <td>3         3</td> <td>100 20 30 40 50 60 90 30 20 140 50 50 50 70 20 40 50 50 70 20 20 100 60 180 90 120 60</td> <td>2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2</td> <td>ê ê ê ê ê ê ê ê ê ê ê ê ê ê ê ê ê ê ê</td> <td>18       3       5       13       42       17       24       17       18       3       18       11       13       12       6       9       16       17       18       3       12       6       9       16       9       17       &lt;1</td> 7       4       3       9	0,2 0,4 1,2 0,2 0,2 0,2 0,2 0,4 2,0 0,4 2,0 0,4 2,0 0,4 1,2 0,4 2,0 0,4 1,2 0,2 0,4 0,4 2,0 0,4 2,0 0,4 2,0 0,4 2,0 0,4 0,4 0,4 0,2 0,4 0,4 0,2 0,4 0,4 0,2 0,4 0,4 0,2 0,4 0,4 0,2 0,4 0,4 0,4 0,4 0,4 0,4 0,4 0,4 0,4 0,4	3         3	100 20 30 40 50 60 90 30 20 140 50 50 50 70 20 40 50 50 70 20 20 100 60 180 90 120 60	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	ê ê ê ê ê ê ê ê ê ê ê ê ê ê ê ê ê ê ê	18       3       5       13       42       17       24       17       18       3       18       11       13       12       6       9       16       17       18       3       12       6       9       16       9       17       <1	25           3           9           21           72           28           122           23           25           8           9           28           17           20           12           7           12           7           12           7           12           7           12           7           12           7           12           7           12           7           12           74           15           72           1           1           45           4           4           17	<1 6 3 4 10 1 2 5 4 8 24 3 3 3 4 7 4 2 4 7 4 1 6 6 4 1 1 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	16       1       4       9       11       11       7       6       41       18       14       7       4       13       25       22       14       7       1       8       4       3       14	8           12           16           8           18           14           36           10           10           8           8           10           10           8           10           10           8           10           10           10           10           10           10           10           10           10           10           10           110           12           14           12           10           28		100 62 36 62 84 110 88 138 138 142 94 80 352 65 86 86 86 92 86 86 92 84 116 112 70 66 20 74 28 82 34 50 82 34
121         -07+25           121         -07+25           121         -07+75           121         -08+25           121         -08+25           121         -08+75           121         -08+75           121         -09+00           121         -09+25           121         -09+50           121         -10+25           121         -10+50           121         -10+75           121         -11+75           121         -11+75           121         -11+75           121         -11+25           56810         -56811           56811         -56812           56813         -56814           56814         -56816           56817         -56818	0     0       0 <td>0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.4 2.0 0.4 2.0 0.4 1.2 0.4 1.2 0.4 0.4 1.2 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4</td> <td>14           12           6           14           12           6           16           18           10-           6           18           10-           6           22           23           24           12           8</td> <td>100 20 30 40 50 60 90 40 30 30 20 140 50 50 70 20 20 40 50 50 50 70 20 20 100 100 100 100 100 100 100 100</td> <td>A A A A A A A A A A A A A A A A A A A</td> <td>ම වි වි</td> <td>18       3       13       42       17       24       17       18       3       18       11       13       12       6       9       16       9       17       &lt;1</td> 7       4       3       9       27	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.4 2.0 0.4 2.0 0.4 1.2 0.4 1.2 0.4 0.4 1.2 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	14           12           6           14           12           6           16           18           10-           6           18           10-           6           22           23           24           12           8	100 20 30 40 50 60 90 40 30 30 20 140 50 50 70 20 20 40 50 50 50 70 20 20 100 100 100 100 100 100 100 100	A A A A A A A A A A A A A A A A A A A	ම වි	18       3       13       42       17       24       17       18       3       18       11       13       12       6       9       16       9       17       <1	25       3       9       21       72       28       122       23       25       8       9       26       17       20       12       7       12       7       12       7       12       7       12       7       12       4       4       4       17       33	<1 6 3 4 10 1 2 5 4 8 24 3 3 3 4 7 4 2 4 1 1 6 6 6 1 1 1 1 9 2	16         1         4         9         11         11         11         13         6         41         18         14         7         4         13         25         22         14         1         7         1         8         4         3         14         60	8           12           16           8           18           14           36           10           10           8           20           10           8           20           10           8           20           10           8           20           10           8           10           10           10           10           10           10           10           10           10           110           12           14           12           10           28           6		100           62           36           62           84           110           88           138           142           94           80           352           85           92           84           118           112           70           85           20           74           28           82           34           50           82           156
121         -07+25           121         -07+25           121         -07+75           121         -08+25           121         -08+50           121         -08+50           121         -08+50           121         -08+75           121         -09+00           121         -09+50           121         -10+00           121         -10+75           121         -10+75           121         -11+75           121         -11+75           121         -11+75           121         -11+25           56810         56811           56813         56813           56814         56815           56816         56818           56818         56818	0         0	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.4 2.0 0.4 2.0 0.4 1.2 0.2 0.4 1.2 0.2 0.4 1.2 0.2 0.4 0.4 1.2 0.4 0.4 2.0 0.4 0.4 2.0 0.4 0.4 0.4 0.2 0.4 0.4 0.2 0.4 0.4 0.4 0.2 0.2 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	14           12         6           14         12           14         12           14         12           14         12           16         16           18         12           10-         6           28         22           28         22           10-         6           10-         6           12         8           12         8	100 20 30 40 50 60 90 40 30 30 20 140 50 50 50 70 20 70 20 40 50 50 50 70 20 100 100 100 100 100 100 100 100 100	A A A A A A A A A A A A A A A A A A A	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	$\begin{array}{c} 18 \\ 3 \\ 5 \\ 13 \\ 42 \\ 17 \\ 24 \\ 17 \\ 18 \\ 3 \\ 3 \\ 16 \\ 11 \\ 13 \\ 12 \\ 6 \\ 9 \\ 16 \\ 9 \\ 17 \\ <1 \\ 4 \\ <1 \\ 7 \\ 4 \\ 3 \\ 9 \\ 27 \\ 16 \\ \end{array}$	25       3       9       21       72       28       122       23       25       8       9       26       17       20       12       7       12       7       12       25       15       72       15       72       1       11       1       4       4       4       4       4	<1 6 3 4 10 1 2 5 5 4 8 24 3 3 3 4 7 4 24 3 3 3 4 7 4 1 6 6 1 1 1 8 6 1 1 1 9 2 3 3	16       1       4       9       11       11       11       7       6       6       41       13       6       6       41       13       25       22       14       1       7       1       8       4       3       14       60       <1	8         12         16         8         14         36         10         10         8         20         10         8         20         10         8         20         10         8         20         10         8         20         10         8         6         18         30         12         14         12         10         26         6         10		100           62           36           62           84           110           86           138           142           94           80           352           66           85           92           64           116           112           70           88           20           74           28           82           34           50           82           156           112
121         -07+25           121         -07+25           121         -07+75           121         -08+50           121         -08+50           121         -08+50           121         -08+50           121         -08+50           121         -08+75           121         -09+25           121         -09+50           121         -10+75           121         -10+75           121         -10+75           121         -11+75           121         -11+75           121         -11+75           121         -11+75           121         -11+75           121         -11+25           56810         56811           56811         56813           56812         56813           56814         56815           56818         56818           56819         56820	0         0	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.4 1.2 0.2 0.4 1.2 0.2 0.4 1.2 0.2 0.4 1.2 0.2 0.4 1.2 0.2 0.4 1.2 0.2 0.4 0.4 0.4 0.4 0.2 0.2 0.4 0.4 0.2 0.4 0.4 0.2 0.2 0.4 0.4 0.2 0.2 0.4 0.4 0.4 0.2 0.2 0.4 0.4 0.2 0.2 0.4 0.4 0.4 0.4 0.2 0.2 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	14           12           6           14           8           22           6           6           18           10-           6           28           6           28           6           22           4           5           10-           6           28           10-           6           28           12           80	100 20 30 40 50 60 90 40 30 20 20 140 50 50 50 70 20 20 40 50 50 50 70 20 100 100 100 100 120 100 120 100 120 380	a a a a a a a a a a a a a a a a a a a	88888888888888888888888888888888888888	$\begin{array}{c} 18 \\ 3 \\ 5 \\ 13 \\ 42 \\ 17 \\ 24 \\ 17 \\ 24 \\ 17 \\ 18 \\ 3 \\ 3 \\ 16 \\ 11 \\ 12 \\ 6 \\ 9 \\ 16 \\ 11 \\ 12 \\ 6 \\ 9 \\ 17 \\ <1 \\ 4 \\ <1 \\ 7 \\ <1 \\ 4 \\ <1 \\ 7 \\ 7 \\ 4 \\ 3 \\ 9 \\ 27 \\ 16 \\ 4 \\ \end{array}$	25       3       9       21       72       28       122       23       25       8       9       25       17       20       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       33       4       17       33       4       13	<1 6 3 4 10 1 2 5 5 4 8 24 3 3 3 4 7 7 4 2 4 3 3 4 1 1 6 6 1 1 1 1 9 2 3 4	16       1       4       9       11       11       7       6       6       6       41       13       25       22       14       1       7       1       7       1       8       4       3       14       60       <1	8           12           16           8           14           36           10           10           8           20           10           8           10           10           8           6           15           30           12           14           10           26           6           10           14	Q     Q     Q       Q     Q       Q <td>100           62           36           62           84           110           88           136           142           94           80           352           86           85           86           87           88           80           352           86           85           86           86           92           84           1112           70           86           20           74           28           82           34           500           82           112           114</td>	100           62           36           62           84           110           88           136           142           94           80           352           86           85           86           87           88           80           352           86           85           86           86           92           84           1112           70           86           20           74           28           82           34           500           82           112           114
121         -07+25           121         -07+75           121         -07+75           121         -08+25           121         -08+50           121         -08+50           121         -08+50           121         -08+75           121         -09+60           121         -09+50           121         -09+50           121         -10+00           121         -10+75           121         -10+75           121         -11+75           121         -11+75           121         -11+75           121         -12+25           56810         -56811           56811         -56813           56813         -56814           56816         -56818           56818         -56818           56819         -56820           56821         -56821	0     0 <td>0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.2 0.4 1.2 0.2 0.4 1.2 0.2 0.4 0.4 1.2 0.2 0.4 0.4 0.4 0.4 0.4 0.4 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2</td> <td>14           12           6           14           8           22           6           16           14           2           6           16           14           2           6           18           10-           6           225           6           225           6           225           6           226           12           12           185           12           185</td> <td>100 20 30 40 50 60 60 90 40 30 20 40 50 50 70 20 70 20 70 20 40 50 50 70 20 100 60 110 100 60 110 70 380 1170</td> <td>0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0</td> <td>88888888888888888888888888888888888888</td> <td><math display="block">\begin{array}{c} 18 \\ 3 \\ 5 \\ 13 \\ 42 \\ 17 \\ 24 \\ 17 \\ 18 \\ 3 \\ 16 \\ 13 \\ 16 \\ 13 \\ 16 \\ 11 \\ 12 \\ 6 \\ 9 \\ 16 \\ 11 \\ 12 \\ 6 \\ 9 \\ 17 \\ 16 \\ 4 \\ 17 \\ 17 \\ 16 \\ 4 \\ 5 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 </math></td> <td>25           3           9           21           72           26           122           23           25           8           9           26           17           20           12           7           12           7           12           7           12           26           15           72           1           11           4           4           4           15           26</td> <td>&lt;1 6 3 4 10 1 1 2 5 4 8 24 3 3 4 7 7 4 2 4 1 6 6 4 1 1 1 1 9 2 3 4 7 7</td> <td>16         1         4         9         11         11         7         6         6         41         18         18         14         7         13         25         22         14         1         7         1         8         4         5         14         60         &lt;1</td> 9         1'2	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.2 0.4 1.2 0.2 0.4 1.2 0.2 0.4 0.4 1.2 0.2 0.4 0.4 0.4 0.4 0.4 0.4 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	14           12           6           14           8           22           6           16           14           2           6           16           14           2           6           18           10-           6           225           6           225           6           225           6           226           12           12           185           12           185	100 20 30 40 50 60 60 90 40 30 20 40 50 50 70 20 70 20 70 20 40 50 50 70 20 100 60 110 100 60 110 70 380 1170	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	88888888888888888888888888888888888888	$\begin{array}{c} 18 \\ 3 \\ 5 \\ 13 \\ 42 \\ 17 \\ 24 \\ 17 \\ 18 \\ 3 \\ 16 \\ 13 \\ 16 \\ 13 \\ 16 \\ 11 \\ 12 \\ 6 \\ 9 \\ 16 \\ 11 \\ 12 \\ 6 \\ 9 \\ 17 \\ 16 \\ 4 \\ 17 \\ 17 \\ 16 \\ 4 \\ 5 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 $	25           3           9           21           72           26           122           23           25           8           9           26           17           20           12           7           12           7           12           7           12           26           15           72           1           11           4           4           4           15           26	<1 6 3 4 10 1 1 2 5 4 8 24 3 3 4 7 7 4 2 4 1 6 6 4 1 1 1 1 9 2 3 4 7 7	16         1         4         9         11         11         7         6         6         41         18         18         14         7         13         25         22         14         1         7         1         8         4         5         14         60         <1	8           12           16           8           14           36           10           10           8           20           10           8           10           10           8           10           10           8           10           10           10           10           10           10           10           10           10           10           10           20           110           12           14           12           10           26           6           10           14           32	Q     Q       Q       Q <t< td=""><td>100           62           36           62           84           110           88           136           142           94           80           352           68           89           94           80           352           68           89           92           64           1112           112           74           28           82           34           50           82           112           114           134</td></t<>	100           62           36           62           84           110           88           136           142           94           80           352           68           89           94           80           352           68           89           92           64           1112           112           74           28           82           34           50           82           112           114           134
21         - 07+25           121         - 07+75           121         - 07+75           121         - 08+25           121         - 08+25           121         - 08+75           121         - 08+75           121         - 08+75           121         - 08+75           121         - 09+25           121         - 09+50           121         - 10+25           121         - 10+75           121         - 10+75           121         - 11+75           121         - 11+75           121         - 11+75           121         - 11+75           121         - 11+75           121         - 11+75           121         - 11+75           121         - 11+75           121         - 12+25           56810         - 56811           56813         - 56813           56814         - 56815           56815         - 56816           56820         - 56820           56821         - 56821           56821         - 56821	0       0	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.4 1.2 0.2 0.4 1.2 0.2 0.4 1.2 0.2 0.4 0.4 1.2 0.2 0.4 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	14           12           6           14           8           22           6           16           14           2           6           16           14           2           6           13           14           2           6           12           6           22           6           22           6           22           6           22           6           22           6           22           6           22           8           12           8           12           8           12           8           12           8           6           6	100 20 30 40 50 60 60 90 40 30 20 20 140 50 50 50 50 50 70 20 40 50 50 50 50 70 20 100 60 100 60 100 100 60 100 100 70 380 1170 2250	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	$\begin{array}{c} 18 \\ 3 \\ 5 \\ 13 \\ 42 \\ 17 \\ 24 \\ 17 \\ 18 \\ 3 \\ 3 \\ 18 \\ 11 \\ 13 \\ 12 \\ 6 \\ 9 \\ 11 \\ 13 \\ 12 \\ 6 \\ 9 \\ 17 \\ <1 \\ 4 \\ <1 \\ 7 \\ <1 \\ 4 \\ <1 \\ 7 \\ 4 \\ 3 \\ 9 \\ 27 \\ 16 \\ 4 \\ 5 \\ 21 \\ \end{array}$	25       3       9       21       72       28       122       25       8       9       25       8       9       26       17       20       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       11       1       4       4       4       15       26       33	<1 6 3 4 10 1 1 2 5 4 8 24 3 3 4 7 4 7 4 1 6 4 1 1 1 1 1 2 3 3 4 7 4 1 1 1 1 1 1 1 1 1 1 1 1 1	16         1         4         9         11         11         7         13         6         6         41         18         14         7         1         13         25         22         14         1         7         1         8         4         50         (1         9         1'2         30	8         12         16         8         10         10         8         20         10         8         20         10         10         8         10         10         8         10         10         10         10         10         10         10         10         10         110         26         6         10         11         12         14         32         335	Q     Q       Q       Q <t< td=""><td>100           62           36           62           84           110           88           138           142           94           80           352           85           86           87           92           64           116           112           70           68           82           34           50           82           112           114           134           700</td></t<>	100           62           36           62           84           110           88           138           142           94           80           352           85           86           87           92           64           116           112           70           68           82           34           50           82           112           114           134           700
1         -07+25           121         -07+75           121         -07+75           121         -08+25           121         -08+25           121         -08+75           121         -08+75           121         -08+75           121         -08+75           121         -08+75           121         -09+25           121         -09+50           121         -10+75           121         -10+75           121         -10+75           121         -11+25           121         -11+75           121         -11+75           121         -11+75           121         -11+75           121         -12+25           56810         -56811           56811         -56812           56813         -56814           56814         -56818           56820         -56821           56821         -56822           56823         -56823	0         0	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.4 2.0 0.4 2.0 0.4 1.2 0.2 0.4 0.4 1.2 0.2 0.4 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	14           12           6           14           8           22           6           16           14           2           6           13           14           2           6           13           14           2           6           13           14           2           6           13           10-           6           28           6           22           6           22           6           22           6           22           6           228           6           12           6           12           6           12           6           12           6           12           6           18	100 20 30 40 50 60 60 90 40 30 20 20 140 50 50 50 50 70 20 20 40 50 50 50 70 20 20 110 50 50 50 70 20 20 110 50 50 50 50 70 20 20 110 50 50 50 50 50 50 50 60 60 60 60 60 60 60 60 60 60 60 60 60	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	පී පී පී පී පී පී පී පී පී පී පී පී පී ප	$\begin{array}{c} 18 \\ 3 \\ 5 \\ 13 \\ 42 \\ 17 \\ 24 \\ 17 \\ 18 \\ 3 \\ 3 \\ 3 \\ 18 \\ 11 \\ 13 \\ 12 \\ 6 \\ 9 \\ 17 \\ 16 \\ 9 \\ 17 \\ <1 \\ 4 \\ <1 \\ 7 \\ 4 \\ 3 \\ 9 \\ 27 \\ 16 \\ 4 \\ 5 \\ 5 \\ 21 \\ 13 \\ \end{array}$	25       3       9       21       72       28       122       25       8       9       25       8       9       28       17       20       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       13       26       33       51	<1 6 3 4 10 1 2 5 4 8 24 3 3 4 7 7 4 2 4 7 7 4 1 6 6 1 1 1 8 1 1 9 2 3 4 7 7 7 5 5 8 8 1 1 8 8 1 1 1 1 1 1 1 1 1 1 1 1	16         1         4         9         11         11         13         6         6         41         18         14         7         4         13         25         22         14         7         1         8         4         3         14         60         <1	8         12         16         8         16         10         110         12         14         12         10         26         6         10         28         6         10         28         6         10         33         33         33         36	Q     Q       Q       Q <t< td=""><td>100           62           36           62           84           110           88           138           142           94           80           552           86           82           84           110           88           112           70           65           82           34           50           82           112           114           134           700           78</td></t<>	100           62           36           62           84           110           88           138           142           94           80           552           86           82           84           110           88           112           70           65           82           34           50           82           112           114           134           700           78
1         -07+25           121         -07+75           121         -07+75           121         -08+25           121         -08+25           121         -08+75           121         -08+75           121         -08+75           121         -08+75           121         -09+00           121         -09+25           121         -09+50           121         -10+75           121         -10+75           121         -11+25           121         -11+75           121         -11+75           121         -11+75           121         -11+25           56810         -56811           56811         -56812           56813         -56813           56814         -56815           56816         -56817           56820         -56821           56821         -56822           56823         -56823	0         0	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.2 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 0.4 2.0 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0	3         6           14         12           14         12           14         12           6         16           14         22           6         6           16         10-           10         6           28         8           22         8           12         8           12         8           12         8           12         8           188         18           188         18           10         10	100 20 30 40 50 60 90 40 30 20 140 50 50 50 70 20 40 50 50 70 20 40 50 50 100 60 180 90 100 60 1810 70 380 120 120 60 70 50 50 50 70 70 20 70 70 20 70 70 20 70 70 70 20 70 70 70 70 70 70 70 70 70 70 70 70 70	3 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		$\begin{array}{c} 18 \\ 3 \\ 5 \\ 13 \\ 42 \\ 17 \\ 24 \\ 17 \\ 24 \\ 17 \\ 18 \\ 3 \\ 3 \\ 16 \\ 11 \\ 13 \\ 12 \\ 6 \\ 9 \\ 16 \\ 17 \\ 16 \\ 9 \\ 17 \\ 16 \\ 4 \\ 5 \\ 21 \\ 16 \\ 4 \\ 5 \\ 21 \\ 13 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 1$	25       3       9       21       72       28       122       23       25       8       9       25       17       20       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       73       13       4       15       28       33       51	<1 6 3 4 10 1 1 2 5 4 8 24 3 3 3 4 7 4 7 4 4 1 1 6 6 4 1 1 1 9 2 3 4 4 7 7 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	16         1         4         9         11         11         11         13         6         41         18         14         7         4         13         22         14         7         1         8         4         5         14         60         <1	8         12         16         8         18         14         36         10         10         8         20         10         8         20         10         8         20         10         8         20         10         8         10         10         10         10         10         10         110         12         14         12         10         26         6         10         14         32         38         26         14	Q     Q     Q       Q     Q       Q <td>100           62           36           62           84           110           88           138           142           94           80           352           86           85           92           84           111           112           70           85           34           50           82           34           50           82           34           700           778           94</td>	100           62           36           62           84           110           88           138           142           94           80           352           86           85           92           84           111           112           70           85           34           50           82           34           50           82           34           700           778           94
21         -07+25           121         -07+25           121         -07+75           121         -08+25           121         -08+50           121         -08+75           121         -08+75           121         -08+75           121         -09+00           121         -09+50           121         -10+50           121         -10+50           121         -10+75           121         -11+75           121         -11+75           121         -11+75           121         -11+75           121         -11+75           121         -11+75           121         -11+25           56810         56811           56811         56812           56812         56813           56814         56816           56818         56820           56821         56823           56823         56823           56824         56825	0         0	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	3         3	100 20 30 40 50 60 90 40 30 30 30 20 140 50 50 70 20 40 50 50 70 20 40 50 50 70 20 40 50 50 70 70 20 40 50 50 70 70 20 20 140 50 50 70 70 70 20 70 140 50 50 70 70 20 70 70 20 70 70 20 70 70 20 70 70 20 70 70 20 70 70 20 70 70 20 70 70 20 70 70 70 20 70 70 70 20 70 70 70 20 70 70 70 20 70 70 70 70 70 70 70 70 70 70 70 70 70	3 a a a a a a a a a a a a a a a a a a a	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	$\begin{array}{c} 18 \\ 3 \\ 5 \\ 13 \\ 42 \\ 17 \\ 24 \\ 17 \\ 18 \\ 3 \\ 3 \\ 16 \\ 11 \\ 13 \\ 12 \\ 6 \\ 9 \\ 16 \\ 9 \\ 17 \\ <1 \\ 6 \\ 9 \\ 17 \\ <1 \\ 6 \\ 9 \\ 17 \\ <1 \\ 6 \\ 9 \\ 17 \\ <1 \\ 6 \\ 9 \\ 17 \\ <1 \\ 6 \\ 9 \\ 17 \\ <1 \\ 6 \\ 9 \\ 17 \\ <1 \\ 6 \\ 9 \\ 17 \\ <1 \\ 6 \\ 9 \\ 17 \\ <1 \\ 6 \\ 9 \\ 17 \\ <1 \\ 15 \\ 17 \\ 15 \\ 17 \end{array}$	25       3       9       21       72       28       122       23       25       8       9       26       17       20       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       7       12       26       15       72       1       11       1       4       4       15       26       33       51       60	<1 6 3 4 10 1 1 2 5 4 8 24 3 3 3 4 7 4 2 4 1 1 6 6 1 1 1 9 2 3 4 7 7 4 2 4 1 1 9 2 3 4 7 7 4 5 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	16         1         4         9         11         11         11         13         6         41         13         22         14         17         1         8         4         3         14         60         <1	8         12         16         8         18         10         10         8         20         10         8         20         10         10         8         20         10         8         20         10         10         10         10         10         10         10         10         10         10         10         10         10         110         28         6         10         14         32         38         28         28         28         28         28         28         28         28         28         28         28         28         28         28         29         28      <	Q     Q       Q <td>100           62           36           62           84           110           88           138           142           94           80           352           85           86           92           84           118           112           70           82           34           50           82           34           50           82           34           700           78           94</td>	100           62           36           62           84           110           88           138           142           94           80           352           85           86           92           84           118           112           70           82           34           50           82           34           50           82           34           700           78           94
121         -07+25           121         -07+25           121         -07+75           121         -08+25           121         -08+50           121         -08+50           121         -08+50           121         -08+75           121         -08+75           121         -09+25           121         -09+50           121         -10+75           121         -10+75           121         -10+75           121         -11+75           121         -11+75           121         -11+75           121         -11+75           121         -11+75           121         -11+75           121         -11+75           121         -12+25           56810         -56811           56813         -56813           56814         -56815           56815         -56818           56820         -56821           56821         -56823           56824         -56824           56825         -56824	0         0	0.2 0.4 1.2 0.2 0.4 1.2 0.2 0.2 0.2 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	3         3           14         12           14         12           14         14           18         22           6         6           18         14           2         4           5         16           14         2           18         10-           6         28           8         22           28         12           8         12           8         12           8         12           8         12           8         20	100 20 30 40 50 60 60 70 20 140 50 50 70 20 70 20 70 20 70 20 70 20 100 100 100 100 100 100 100 100 100	x a a a a a a a a a a a a a a a a a a a	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	$\begin{array}{c} 18 \\ 3 \\ 5 \\ 13 \\ 42 \\ 17 \\ 24 \\ 17 \\ 24 \\ 17 \\ 18 \\ 3 \\ 3 \\ 16 \\ 11 \\ 13 \\ 12 \\ 6 \\ 9 \\ 16 \\ 11 \\ 13 \\ 12 \\ 6 \\ 9 \\ 17 \\ <1 \\ 4 \\ 4 \\ 4 \\ 5 \\ 27 \\ 16 \\ 4 \\ 5 \\ 21 \\ 13 \\ 15 \\ 17 \\ 7 \\ 16 \\ 13 \\ 15 \\ 17 \\ 7 \\ 16 \\ 13 \\ 15 \\ 17 \\ 7 \\ 16 \\ 13 \\ 15 \\ 17 \\ 7 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 $	25       3       9       21       72       23       25       8       9       25       8       9       26       17       20       12       7       12       7       12       7       12       7       12       25       33       15       77       11       1       4       4       15       26       33       51       60       44       33       51       60		16         1         4         9         11         11         11         13         6         6         41         13         22         14         1         7         4         13         25         22         14         1         8         4         3         14         60         <1	8         12         16         8         14         36         10         10         8         20         10         8         20         10         8         20         10         8         20         10         8         20         10         10         10         8         6         10         12         10         26         6         10         25         14         32         38         26         14         4	Q     Q       Q <td>100           62           36           62           84           110           88           136           142           94           80           352           86           86           87           80           352           86           85           86           86           86           86           86           86           86           86           86           87           82           34           50           82           34           700           76           94           80           76           94</td>	100           62           36           62           84           110           88           136           142           94           80           352           86           86           87           80           352           86           85           86           86           86           86           86           86           86           86           86           87           82           34           50           82           34           700           76           94           80           76           94
121         -07+25           121         -07+75           121         -07+75           121         -08+50           121         -08+50           121         -08+50           121         -08+50           121         -08+50           121         -08+50           121         -09+25           121         -09+50           121         -10+00           121         -10+50           121         -10+50           121         -11+75           121         -11+75           121         -11+75           121         -11+75           121         -12+25           56810         56811           56811         56812           56813         56814           56814         56815           56815         56818           56821         56822           56823         56824           56824         56825	0       0	0.2 0.4 1.2 0.2 0.2 0.2 0.2 0.2 0.2 0.4 1.2 0.2 0.4 0.4 1.2 0.2 0.4 0.4 1.2 0.2 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	14           12           6           14           8           22           6           18           10-           6           28           8           22           6           18           10-           6           28           8           22           8           12           8           12           8           18           300           20           6	100 20 30 40 50 60 90 40 30 20 40 30 20 40 50 50 70 20 20 40 50 50 50 70 20 10 10 10 10 10 10 10 10 10 10 10 10 10		<ul> <li>3</li> <li>3</li> <li>3</li> <li>3</li> <li>3</li> <li>4</li> <li>4</li> <li>5</li> <li>5</li></ul>	$\begin{array}{c} 18 \\ 3 \\ 5 \\ 13 \\ 42 \\ 17 \\ 24 \\ 17 \\ 24 \\ 17 \\ 18 \\ 3 \\ 3 \\ 16 \\ 11 \\ 12 \\ 6 \\ 9 \\ 17 \\ 12 \\ 6 \\ 9 \\ 17 \\ 12 \\ 6 \\ 9 \\ 17 \\ 16 \\ 4 \\ 17 \\ 7 \\ 16 \\ 4 \\ 5 \\ 21 \\ 13 \\ 15 \\ 17 \\ 30 \\ 27 \\ 16 \\ 13 \\ 15 \\ 17 \\ 30 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10$	23       3       9       21       72       28       122       23       25       8       9       25       17       20       12       7       12       7       12       7       12       7       12       7       12       26       15       72       1       11       1       4       17       33       33       51       60       48       72	<1 6 3 4 10 1 2 5 4 8 24 3 3 4 7 4 2 4 1 6 4 1 1 6 1 1 1 2 3 3 4 4 7 7 4 8 8 6 5 1 1 1 1 1 1 1 1 1 1 1 1 1	16         1         4         9         11         11         13         6         6         41         13         25         22         14         1         7         4         13         25         22         14         60         <1	8         12         16         8         14         36         10         10         8         20         10         10         8         10         10         8         30         10         10         10         10         10         10         10         10         10         10         10         10         10         26         6         110         28         6         10         11         12         110         28         6         114         32         338         26         14         4         5	Q     Q       Q <td>100           62           36           62           84           110           88           136           142           94           80           352           88           94           80           352           88           94           80           352           88           96           97           88           20           74           28           34           500           82           34           500           76           94           80           58</td>	100           62           36           62           84           110           88           136           142           94           80           352           88           94           80           352           88           94           80           352           88           96           97           88           20           74           28           34           500           82           34           500           76           94           80           58

