

Appendix V - X  
Assay Results, Study Reports,  
and  
Project Summary

GEOLOGICAL SURVEY BRANCH  
ASSESSMENT REPORT

24,938 10 of 14

Appendix V

Compiled Assay Results

Greater than 1 gpt Au for the Drill Holes

## APPENDIX V

HOLE	FROM	TO	WIDTH	AVERAGE GRADE
14	19	26.5	7.5	1.05
15	9	10	1	1.87
	12	13	1	4.11
	18	22.7	4.7	2.12
	37	38	1	1.06
	39	42	3	1.44
	73	77	4	7.44
	99	100.5	1.5	1.02
	115.5	117	1.5	8.44
	122.5	123.5	1.0	1.19
16	0.81	2.00	1.19	2.69
	10	11	1	2.42
	14.5	20.5	6	2.79
	35	37	2	2.07
	78	80	2	4.12
	129	132	3	2.07
	144	148.5	4.5	1.32
17	34	36	2	2.52
	40	41	1	1.29
	124.5	126	1.5	1.97
	166.5	168	1.5	1.78
	179	180.5	1.5	2.63
18	5	6	1	2.06
	19	22	3	1.76
	34	35	1	1.01
	100.5	130	29.5	12.53
	149.5	152.5	3	2.97
19	11	13	2	9.12
	16	17	1	2.41
	23	26	3	1.5
	67	68.5	1.5	1.6
	70	71.5	1.5	2.07
	85	86	1	4.06
	141	142	1	1.95
	164	165.5	1.5	1.75
	179	180.5	1.5	1.51
20	30	33	3	2.03
21	16	22	6	2.67
22	12	15	3	3.84
23	0.16	1.17	1.01	1.78
	17	18.5	1.5	1.56
	27.5	29	1.5	28.83
	40	41	1	17.26
	77	78	1	1.35
24	36	37.5	1.5	5.08
	45	46.5	1.5	2.59
	72	73	1	16.30

HOLE	FROM	TO	WIDTH	AVERAGE GRADE
	78	81	3	1.62
	100	101	1	1.97
	102	103	1	1.1
25	37.5	39	1.5	1.11
	53.5	55	1.5	8.87
	81.74	91.66	9.92	9.69
	95	96	1	1.74
26	56.22	57	.78	5.09
27	49	55	6	4.88
	59	60	1	1.56
	62	65	3	2.07
	68	69	1	1.28
	72	73.3	1.3	19.89
	79	81	2	2.22
	104	105	1	1.305
28	88	90.68	2.68	5.56
29	77	78	1	4.32
30	32	33.5	1.5	4.08
	109	110.5	1.5	1.28
	217	218	1	3.12
	358.5	361.5	3	3.95
31	9	10	1	1.68
32	27	29.9	2.9	5.32
33	7	8	1	6.89
	10	11	1	3.75
	25	26	1	1.16
	36	36.5	0.5	2.56
34	24	25	1	6.72
35	7	10	3	4.16
	27	29.87	2.87	4.04
36	32	34.29	2.29	1.85
37	1	2	1	1.48
38	82	83	1	1.08
	97	98	1	1.25
40	36.5	39.5	3.0	2.01
	45	46.95	1.98	4.94
	54.9	55.17	.26	4.86
	69.5	71	1.5	1.24
	83	84	1	5.88
	129.74	130.19	.45	1.78
41	2.5	3.92	1.42	1.38
	25	26	1	13.03
	50.85	58	7.15	4.74
	69	69.55	.58	8.67
	71	74.7	2.7	6.44
	94.7	95.2	0.5	3.82
	96.3	98	1.57	3.9
	110.35	112.3	1.95	3.63
	118	121.5	3.5	4.35

HOLE	FROM	TO	WIDTH	AVERAGE GRADE
	139.32	139.57	0.2	23.66
	162.13	163.5	1.37	5.91
	161.16	167.50	1.34	1.95
42	68	68.45	.45	5.81
	70	71	1	1.14
	111.7	112.02	.32	2.38
43	190.06	206.06	16m	3.41
44	21	22	1	2.75
	63.12	66	2.78	9.23
	83	85	2	1.31
	129	133	4	4.15
	135	137	2	2.10
45	113.5	115	1.5	1.10
46	103	104	1	8.72
50	27	28	1	2.47
51	37	38	1	1.21
52	11	12.5	1.5	1.6
54	12.0	15.0	3	1.83
55	21.5	24.5	3	2.83
56	92	93	1	1.19
	121	122.61	1.61	3.77
	137	140	3	2.23g
	153.5	156	2.5	3.85
57	86	89	3	2.32
	110.9	111.6	0.7	4.02
	152	154	2	1.02
58	19.5	21.0	1.5	4.58
59	19	20.5	1.5	3.32
	63.64	66	2.36	9.86
60	32.5	35.31	2.81	4.82
	69.75	71.22	2.07	1.69
	91.5	92	0.5	1.77
	94	95	1	5.08
61	45.72	46.91	1.19	4.01
	59.82	60.55	0.73	8.80
	73	74	1	2.29
	93	94.5	1.5	1.51
62	62	63	1	2.97
	66.5	68	1.5	11.05
63	48	51	3	5.95
	66.41	66.72	.31	12.98
	74	77	3	2.12
	103	104.5	1.5	1.93
	107.5	112	4.5	3.28
	118	119.5	1.5	1.01
64	70	71	1	4.12
65	46	47	1	1.01
	60	61	1	3.42

HOLE	FROM	TO	WIDTH	AVERAGE GRADE
	69	70	1	1.18
	108.5	111	2.5	2.66
	123.5	124	0.5	30.67
66	78	79.5	1.5	1.63
	96.89	101	4.11	1.76
68	5.5	8.2	2.7	44.32
69	6	8.7	2.7	11.12
71	9.83	10.5	0.73	23.82
72	14.53	15.11	0.58	13.23
	22.46	22.91	0.45	224.4
74	2	3.93	1.93	10.37
75	5.5	6.5	1.0	19.71
76	6.5	8.5	2	9.16
77	9	11.2	2.2	21.91
	13.5	16.07	2.57	7.14
78	17.8	19.5	1.7	12.62
	21.5	22	0.5	12.74
79	14.5	16.5	2	8.34
80	14.93	15.82	0.89	4.36
81	17.75	18.75	1	20.09
82	19.45	20.5	1.05	11.36
83	45.5	46.3	0.8	2.09
84	27	30	3	1.90
	62.5	66	3.5	32.16
85	25	27	2	1.02
	52.5	53	0.5	1.52
	54.5	55	0.5	3.48
	56.50	57.50	1	4.40
	60	62	2	2.03
86	10	11	1	4.2
87	14.87	16.5	1.68	3.38
	19	20	1	1.29
89	17	18	1	2.33
90	40.07	40.50	0.43	1.63
91	2.5	9	6.5	13.2
	11	13	2	5.55
	16.0	18	2	10.89
92	3.5	12.4	8.9	5.18
	18	19	1	1.44
93	7.95	10	2.05	3.68
	13	20.6	7.6	12.14
	21	22	1	2.44
	23	24	1	1.20
	27	28	1	8.7
	30	31	1	1.3
94	50.6	56.16	5.56	1.04
95	90	96	6	8.23
96	23	24	1	3.58
	57	58	1	2.46

HOLE	FROM	TO	WIDTH	AVERAGE GRADE
98	9.45	10.45	1	5.11
	13	14	1	1.02
	93	94	1	1.29
99	10	11	1	2.4
100	17.37	18.65	1.28	5.18
	24	25	1	1.58
	47.95	52	4.05	14.05
	76	78	2	4.03
101	6	8	2	2.79
	10	11	1	1.72
	49	50	1	1.80
	63	64	1	1.62
102	5	6	1	11.94
	9	10	1	1.26
	71.5	72.5	1	1.62
103	8	9	1	1.66
105	10	11	1	5.28
106	16	18	2	2.89
	20	22	2	1.64
	27	28	1	4.14
	31	32	1	1.63
	48	49	1	1.19
107	34	35	1	1.45
	48	49	1	1.19
109	26	30	4	4.115
	34	35	1	3.15
	53	56	3	1.81
	59	60	1	1.38
110	3	13	10	43.82
	19	20	1	3.87
111	7	8	1	1.44
	12	19	7	2.48
	25	25.81	0.81m	1.11
112	22	23	1.0	1.67
113	40.5	41.5	1.0	4.32
	43	44	1.0	1.18
	51	53	2.0	1.34
114	70	72	2	2.97
	77	78	1	1.87
	87.95	89	1.25	1.98
115	19	19.63	0.63	14.22
116	22	23.18	1.18	14.3
118	42	46	4	4.04
	57	59	2	1.25
119	44	45	1	2.28
	62	63	1	1.97
	65	66	1	1.89
	79	80	1	1.06
	89	90	1	4.52

HOLE	FROM	TO	WIDTH	AVERAGE GRADE
122	72	73	1	7.56
	86	86.92	0.92	9.26
	112	113	1	18.03
123	12	13	1	18.86
	40	41	1	7.31
	43	44	1	4.46
	102	104	2	1.52
	113	114	1	1.95
	117.96	119.0	1.04	1.95
124	4	5	1.0	2.22
	9.6	14	4.4	3.11
	22	23	1	4.47
	26	27	1	2.11
	67	68	1	1.68
	71	72	1	1.01
	75	80	5	20.54
125	2	3	1	9.11
	4.88	7.23	2.34	4.49
	6.00	7.23	1.23	2.43
	13	14	1	3.21
	18	20	2	12.93
	25.9	28	2.1	7.34
	74	75	1	1.39
	117.5	119	1.5	1.06
126	3.41	4.39	.98	38.87
	7.9	12	4.1	4.83
	33	35	2	4.49
	54.4	56.59	2.29	8.02
	99	102.6	3.6	5.96
	146	147	1	6.86



Appendix VI  
Petrographic Study Report  
by  
Chris Huggins

# ORE MICROSCOPY OF THE CLONE PROPERTY, NORTHWESTERN B.C.

Geology 428 Research Paper  
by Chris Huggins

## INTRODUCTION:

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The Clone Property is situated on a nunatak on the western margin of the Cambria Icefield, 20 km southwest of Stewart B.C., and is accessible only by helicopter. Samples for this study were collected from August 27 to September 7, 1996 by the author. In total, 6.5 days were spent mapping and collecting samples for meso- and microscopic analysis. The size of the study area is 250m x 600m, on which there is at least 30% snow cover. The area around camp and below was the focus of an extensive drilling and trenching program this year; five of the samples studied for this report are from three different drill holes and two samples are from trenches. The Clone Property is a gold and cobalt prospect; these samples represent the high grade ore found on the property, and are part of a sulphide rich shear system which can be traced for at least 1 km in strike length along the property. The purpose of the paper is to describe and identify opaque mineralogy, and identify gold association within the sample suite.

## *GEOLOGIC SETTING*

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The property is located near the contact between Stikinia, and the Coast Plutonic Complex. The stratigraphy of the property is dominantly of volcanic origin, and is the lithologic equivalent to / or stratigraphic extension of the Betty Creek Formation of the upper Hazelton Group (D. Alldrick, personal communication, Dec. 1996). From southwest to northeast the rock units are; black siltstone with rusty weathering fragments, likely of volcanic origin; to the northwest, the main rock unit is a volcanic breccia, which has gradational contacts with an ash tuff sequence. Clasts within the volcanic breccia are matrix supported and range in size, from 1cm to 5cm. Intruded into the volcanoclastics is a massive hornblende feldspar, locally biotite rich porphyritic unit, which has undergone strong chlorite, sericite and potassic alteration. It is within this area that the sulphide shear system (S-zone) is localized. Most of the samples in this study are from the S-zone. The porphyry is also found further to the northeast along the contact between the volcanoclastic unit, and a strongly hematite altered coarse heterolithic breccia. Hematite staining within the porphyry is locally pervasive; and along fractures. Where the hematite is fracture controlled, pseudo-liesegang rings have formed. At this contact is the H-zone, which is a semi-massive hematite shear zone, which is of variable size, from 20cm to 4m across.

All of the volcanic units on the property have been significantly altered and deformed, such that fragments are aligned towards 315°, which is the dominant foliation direction on the property. The gold is hosted within two main shear zones, the H- and S-zones; with intensity of deformation within the shears is extremely variable, ranging from

brittle fracture to mylonitic textures. Alteration is pervasive potassic and sericitic, and is locally intense. Contacts between individual rock units are near vertical across the sequence.

MESOSCOPIC SAMPLE DESCRIPTION:

*Sample: Tr. #8*

<i>Mineral</i>	<i>modal percentage</i>	<i>description</i>
pyrite	80%	- massive, unequal granular (very fine grained to ~3mm), anhedral grains (from milling?), some colloform banding around grains, rare secondary zoning, highly fractured
arsenopyrite	15%	- massive, unequal granular anhedral crystals, finer grained than pyrite on average, discrete band, microbrecciation
magnetite	2%	- very fine grained, disseminated
chalcopyrite	2%	- fine grained fracture fill in aspy

*Sample: CL96-18-45725*

<i>Mineral</i>	<i>modal percentage</i>	<i>description</i>
pyrite	75%	- semi-massive med. to very fine grained, anhedral grains, microbrecciated
arsenopyrite	17%	- fine to very fine grained, anhedral grains, occurs in bands, and blebs within pyrite, microbrecciated
chalcopyrite	3%	- very fine grained, interstitial fracture fill in aspy > py
magnetite	< 1%	- very fine grained, disseminated
quartz	5%	- quartz vein ~2mm wide, no sulphides in vein, some interstitial space filling in sulphides

*Sample: CL96-18-45726*

<i>Mineral</i>	<i>modal percentage</i>	<i>description</i>
pyrite	50%	- semi-massive, no grain development, microbrecciated
arsenopyrite	30%	- fine to coarse grained, anhedral crystal, as blebs in py, microbrecciated
magnetite	5%	- fine grained fracture fill in sulphides
chalcopyrite	2%	- very fine grained fracture fill, mostly in sulphides
gangue	13%	- quartz > chlorite, veins, and space filling,

*Sample: CL96-25-46456*

<i>Mineral</i>	<i>modal percentage</i>	<i>description</i>
pyrite	65%	- shear bands (~1cm across) of very fine to coarse (~4mm) grained, anhedral crystals, microbrecciated,
arsenopyrite	15%	- bands, and blebs very fine grained, microbrecciated bands are thin relative to py
magnetite	10%	- very fine grained, in bands, and dissem. in sulphides
chalcopyrite	<1%	- disseminated in sulphides
gangue	10%	- chl. > qtz., space filling, in shear/flow zones,

*Sample: CL96-25-50135 @54.50m*

<i>Mineral</i>	<i>modal percentage</i>	<i>description</i>
pyrite	20%	- med. grained, anhedral, microbrecciated
arsenopyrite	15%	- med. grained, anhedral, microbrecciated
magnetite	5%	- dissem. and along fractures
chalcopyrite	35%	- space filling around sulphides, and some wispy veins in gangue with magnetite
gangue	25%	-quartz veins and fracture filling

*Sample: CL96-25-50135 @54.90m*

<i>Mineral</i>	<i>modal percentage</i>	<i>description</i>
pyrite	30%	med. to fine grained breccia, in band
magnetite	40%	very fine grained, fracture and space filling, some massive
chalcopyrite	10%	disseminated fracture fill, in py, and mt.
gangue	20%	mostly quartz, with some chlorite

*THIN SECTION ANALYSIS:*

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Analysis of polished thin section was instrumental in gaining an understanding of the mineral associations and textures because of the fine grained nature of the sulphides.

*GENERAL MINERAL CHARACTERISTICS:*

In all samples studied, there are a number of observations that are consistent throughout the sample suite:

- ⇒ microbrecciation / brittle fracturing of pyrite and arsenopyrite
- ⇒ initial arsenopyrite growth, with pyrite overgrowths common
- ⇒ pyrite and arsenopyrite usually occur in bands of dominantly one mineral or the other, and rarely evenly disseminated throughout
- ⇒ mineral zoning seen only in surface samples, not in core
- ⇒ late chalcopyrite fracture filling within py and aspy grains, and along grain boundaries
- ⇒ amoeboid chalcopyrite blebs within magnetite, and occasionally around sulphides
- ⇒ late magnetite fracture filling along grain boundaries
- ⇒ late gold precipitation
- ⇒ gold in arsenopyrite more often than in pyrite; commonly in contact with chalcopyrite/magnetite
- ⇒ gangue (qtz, chl, cc) often forms radiating growth zones around sulphide grains, and does not show any significant grain rotation

*PARAGENETIC SEQUENCE:*

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## *CONCLUSION*

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From the thin section analysis of these few samples, a number of useful observations have been made regarding the nature of the ore. With respects to gold recovery, it is vital to recognize that the gold is only associated with the sulphides, specifically arsenopyrite and (to a lesser extent) pyrite. The size of the gold grains is also important for milling problems. The size of gold is variable, but fine; from 5 to 20 microns across, but three dimensional size is unknown. It would be interesting to know if the gold grains are separate, or if it forms as elongate micro-veins, but this seems unlikely, as the size and shape of the gold was consistent throughout the sample suite. Other points of interest are the mineral zoning around surface sulphides, and with which phase of mineral growth does the gold associate, is there any elemental difference between the zones, and why is this only seen on surface? Another as of yet unresolved problem is where is the location of cobalt; is it in the pyrite, and if so, which phase? These questions will be addressed and hopefully resolved in the new year for my thesis.

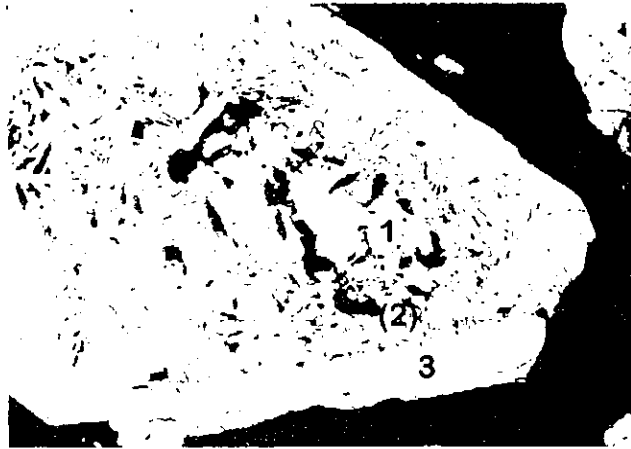


Figure 6a: width of photo 1.25mm



Figure 6b: width of photo 1.25mm

*Sample: Tr. #193*

Figure 6a exhibiting very rare zoning within arsenopyrite. Two and possibly three zones are identifiable. The faint yellow in centre is possibly pyrite. Figure 6b is an excellent example of pressure shadows of quartz, growing from the sides of an arsenopyrite crystal; blue and green are chlorite. The long axis of the growth is parallel with the regional foliation of 315 degrees.



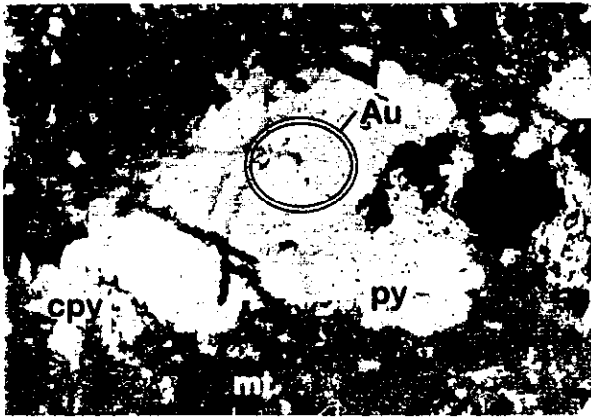


Figure 5a: width of photo 2.5mm

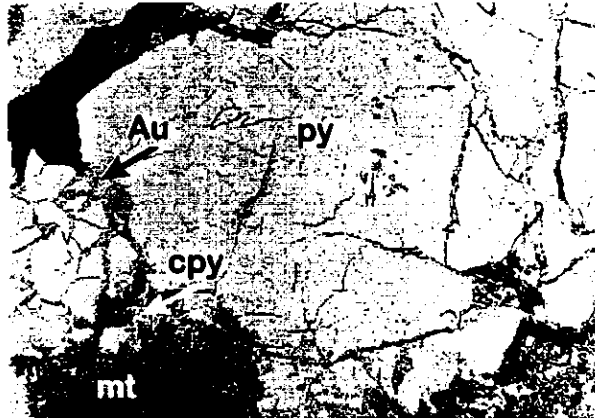


Figure 5b: width of photo 2.5mm



Figure 5c: width of photo 2.5mm

*Sample: CL96-25-50135 @54.90m*

As this sample is an arsenopyrite poor sample, the gold has precipitated in fractures in pyrite grains, and in direct contact with chalcopyrite. As the chalcopyrite surrounds the gold, this would seem to indicate gold precipitation before chalcopyrite; figure 5a,5b. Figure 5c shows amoeboid chalcopyrite within a euhedral magnetite grain, with specular hematite surrounding the magnetite. Some of the specularite has a darker grey colour, which might indicate a replacement of specularite with magnetite. There is also abundant hematite in the gangue.

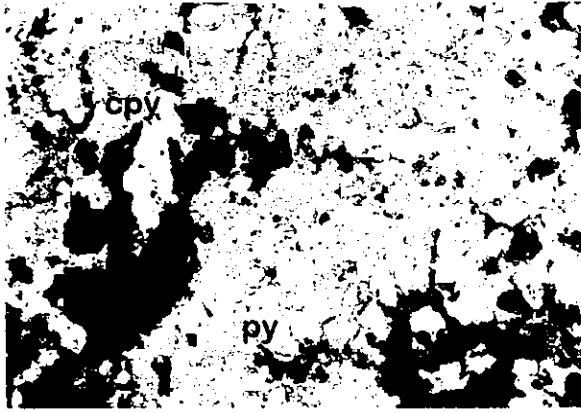


Figure 4a: width of photo 2.5mm



Figure 4b: width of photo 2.5mm

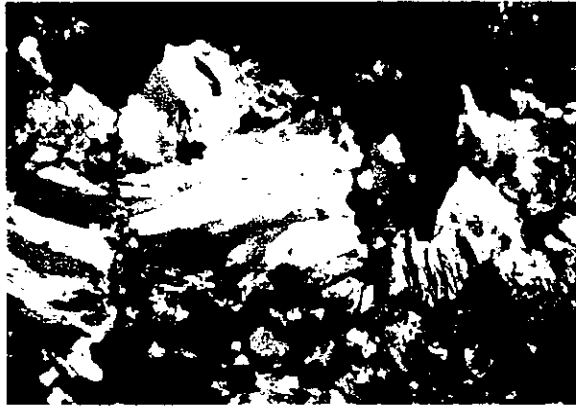


Figure 4c: width of photo 2.5mm

*Sample: CL96-25-50135 @54.50m*

Figure 4a is a unique example showing the dissolution texture of pyrite by chalcopyrite. The chalcopyrite seems to have formed in veins or fractures within pyrite, and replaced pyrite at the contact. Figure 4b, exhibiting late amoeboid chalcopyrite infill at grain boundaries around pyrite and quartz. Figure 4c displays possible strain recovery within ribbon quartz grains.



Figure 3a: width of photo 2.5mm

*Sample: CL96-25-46456*

Figure 3a is an example of the texture of the chlorite 'flowing' around grains, in this case a quartz grain with arsenopyrite replacement.

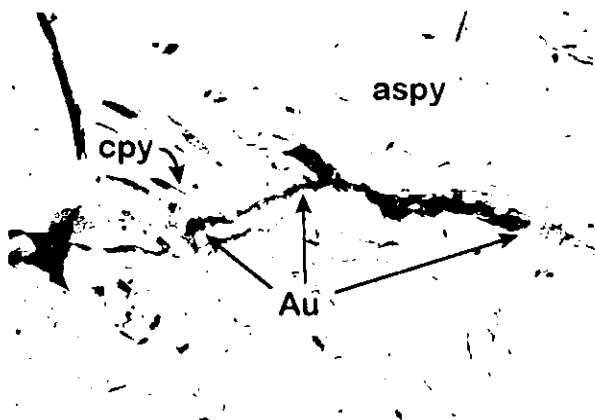


Figure 2a: width of photo 0.625mm

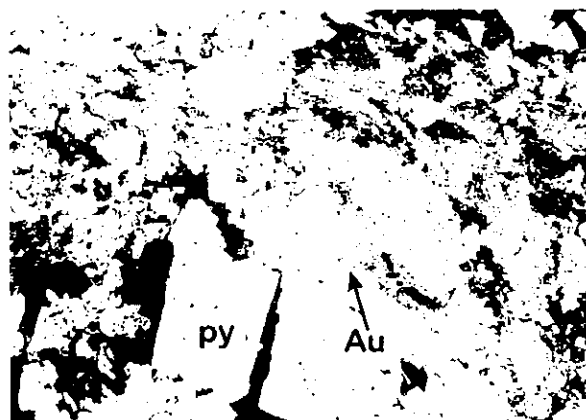


Figure 2b: width of photo 1.25mm

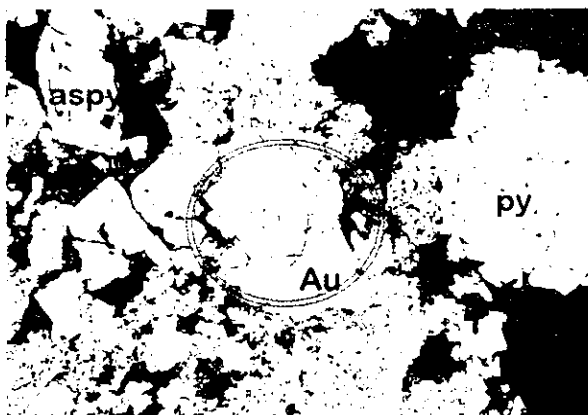


Figure 2c: width of photo 1.25mm

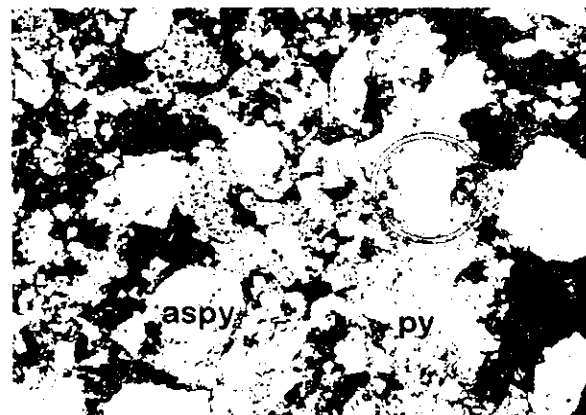


Figure 2d: width of photo 2.5mm

*Sample: CL96-18-45726*

Figure 2a is a good example of the nature of the gold infill, and the variability of the grain sizes (from 5-20 microns). Figure 2b is a rare example of gold within pyrite. As can be seen from the photo, there is no arsenopyrite within the frame; and in the polished section, there was no arsenopyrite in the immediate vicinity. This observation might lead to the conclusion that gold concentrates in arsenopyrite, when pyrite is the dominant sulphide, and in the absence of arsenopyrite, the gold will precipitate in pyrite. Figure 2c shows an arsenopyrite grain with a considerable amount of gold as late mineralization along fractures. Although the gold is usually in contact with chalcopyrite, this photo shows that this is not always the case. The pyrite grains show an aggregate type structure. Figure 2d shows the same grains as in, figure 2c but with half the magnification, giving a better perspective of the brittle fractured arsenopyrite grains, and late fill of magnetite and chalcopyrite.

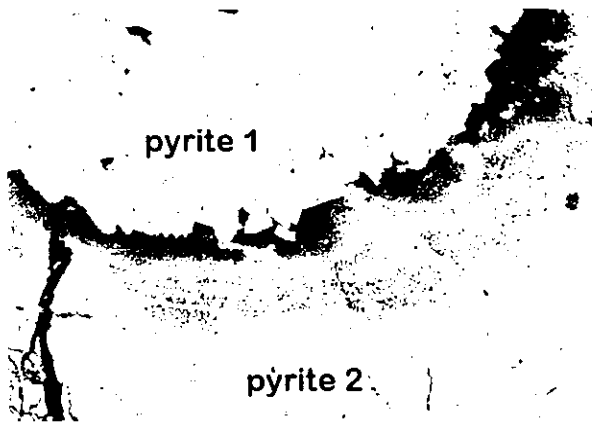


Figure 1a: width of photo 1.25mm

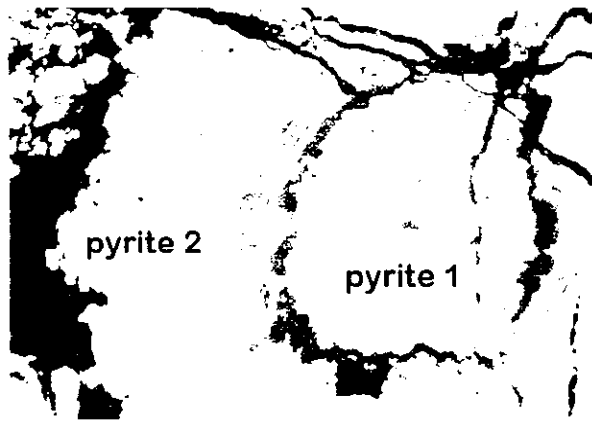


Figure 1b: width of photo 2.5mm



Figure 1c: width of photo 2.5mm

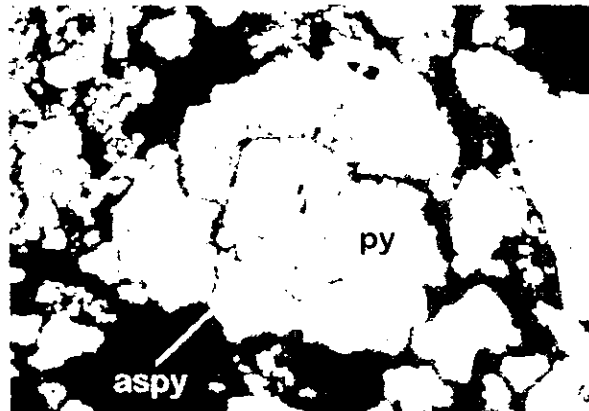
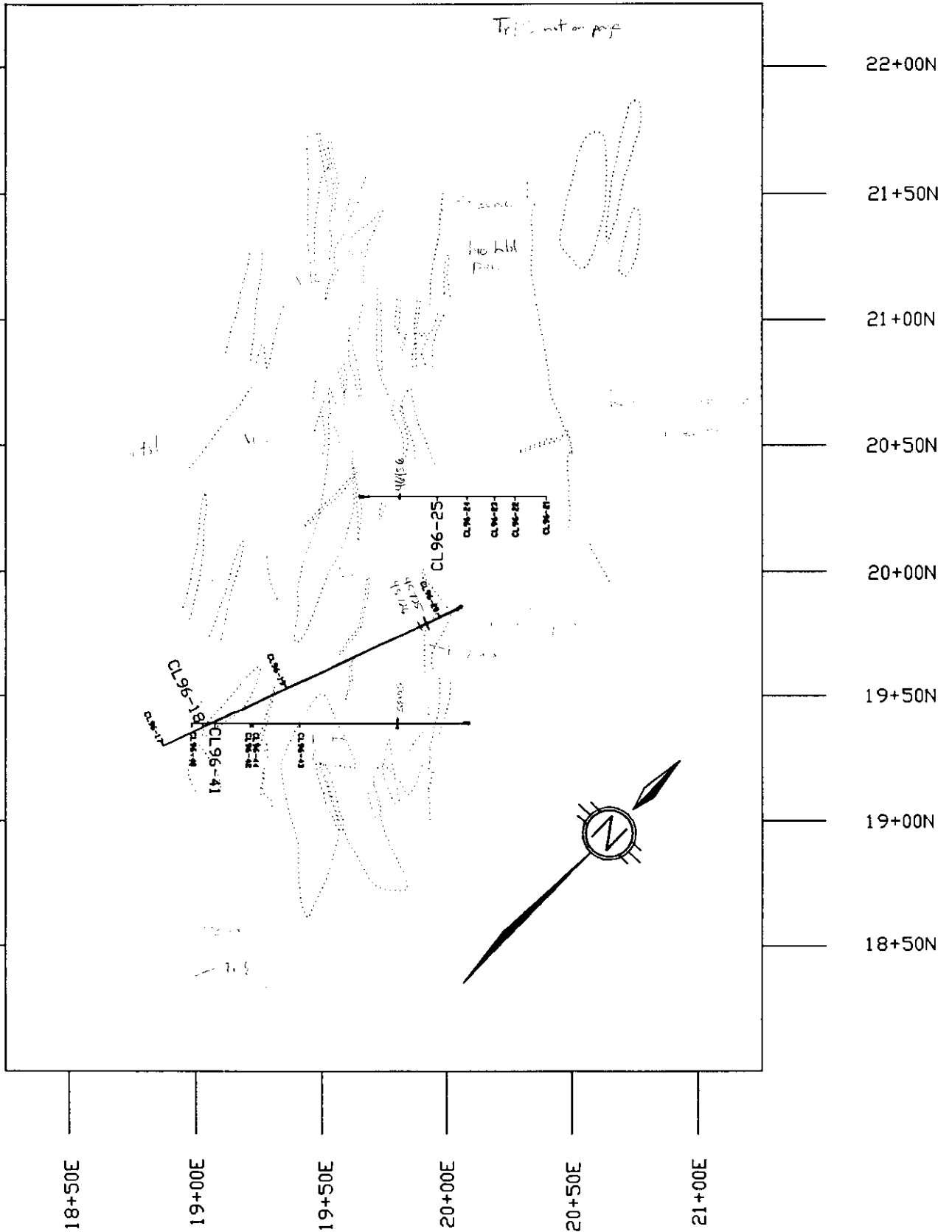


Figure 1d: width of photo 2.5mm

*Sample: Tr. #8*

The photomicrographs from the polished section show the microbrecciated, brittle fracturing of all the sulphides in the study, which is an important feature in the development of gold concentration. It is interesting to note that the surface samples are the only samples which show any zoning around the sulphides. Figure 1a and 1b show an original pyrite nucleus, with irregular colloform banding surrounding the core, and a second growth zone with approximately double the radius of the first pyrite growth. In other places within the thin section, the later phase of pyrite was well developed with euhedral cubes. Figure 1a also shows the nucleus is an aggregate, as the grain boundaries can be seen. Figure 1c shows the microbrecciation of the sulphides, and an unidentified anisotropic mineral. Figure 1c shows a consistently observed relationship of pyrite overgrowths around arsenopyrite grains.

# Diamond Drill Hole and Sample Location Clone Property



Appendix VII

Structural Study Report

by

Ian Harrison

## STRUCTURAL INTERPRETATION OF THE CLONE PROPERTY

by Ian Harrison.

### Introduction:

From the 13th to 16th of September 1996, field work in the immediate vicinity of the Clone Exploration Camp (from 2400N to 1800N local grid) was undertaken to gather information for a structural interpretation of the gold deposit. The deposit consists of mineralized shear zones running parallel to local stratigraphy, which comprise ash lapilli and breccia tuffs, a hornblende-biotite porphyry, and a heterolithic volcanic megabreccia. These three main units dip vertically and strike approximately 132 degrees local azimuth. All azimuths used here relate to the local grid.

### Foliation:

Foliation which the gold bearing shear zones parallel; strikes at 132 degrees on average, with dips within 20 degrees (and mostly within 10 degrees) of vertical. (See stereonet: *Poles to foliation within the H1 and S2A Zones*).

In the H1, S2 and S2A zones foliation is represented by brittle/ductile deformation. These mineralized zones contain ribboned quartz and broken feldspar crystals, deformed wall rock clasts with strain shadows, and other cataclastic to mylonitic textures.

Asymmetric structures are present, but no overall sense of movement could be determined from these features. Sinistral, dextral, reverse and normal movements could be interpreted from different structures.

### Joint and fracture Sets:

There are two major joint sets. They are identifiable as reasonably distinct structures on the stereonet. (See stereonet: *Poles to "Joints"*).

The first is probably better termed as a fracture set. It runs parallel to foliation. The strike is consistent throughout, but dip varies through 180 degrees. (See stereonet: *Poles to faults, veins, and planes with lineations*). This variation in dip may represent several discrete fracture sets striking parallel to one another. However if this is so they could not be differentiated in the field or on the stereonet.

These fractures commonly have mineral lineations on their surfaces. Mineral elongation lineations are especially well developed in calcite and quartz veins, as well as chlorite and epidote veins which lie along the fracture planes. Some of the lineations appear to have developed during crystal growth. Evidence for this is in the form of relatively large, undeformed calcite crystals which have grown with a definite crystal axis alignment in fracture void spaces. Other lineations are striations, usually on joints in chlorite-epidote rich rock.

The lineations are very consistent in orientation and trend at exactly 90 degrees to foliation. (See stereonet: *Lineations*). They plunge from 0-85 degrees, both to the NE (042 degrees) and the SW (222 degrees). Occasionally sense of movement could be determined by steps in the lineations. All indicated reverse movement regardless if the lineations plunged to the NE or SW.

The second joint set cuts foliation at 90 degrees and dips about the vertical. Dykes near trenches 4 and 13 have intruded parallel to these joints. The dykes are relatively undeformed, and only cut by a set of faults running parallel to foliation with dextral and reverse movement along them.

### Faults:

No conclusive results were gained from the orientation and sense of movement on faults seen in the deposit area. The stereonet with *faults, veins, and planes with lineations* shows a possible array of faults striking parallel to foliation (and the fracture set described above). However the senses of movement on these structures were inconsistent with one another.

The faults near trenches 4 and 13 which offset dykes by approximately half a meter, could be related to the major fault which bounds the deposit to the west as they are similarly oriented.



### **Discussion and Conclusions:**

The following is the most likely structural history, given the information above.

Planes of weakness would have developed during initial deformation, which later formed the shear zones. These planes of weakness are parallel to bedding and contacts in the original package of rocks. The H1 zone for example roughly follows the tuff-porphyry contact.

The lineated fracture planes appear to have formed as a response to the stress that created the shear zones. Mineral elongation directions on these fractures indicate a principle compression direction perpendicular to foliation (see schematic sketch). Reverse movement indicators on the lineations are consistent with compression.

Because the lineations are aligned at 90 degrees to the shears, there would have been little or no strike-slip movement (as the rocks are seen now) along the shears. However it is possible there was up-down displacement, as the lineations give no indication of the plunge of the principle compression direction. Indeed the structures within the shears indicate that they were formed by considerable movement along the shears, which would require the principle compression direction to be at an angle from the normal. However, as previously stated, these structures are not indicative of movement in any one direction as one would expect in the case of lateral shearing. Whether it is possible for the cataclastic and mylonitic structures to have been formed by pure flattening with little lateral displacement along the shears is unknown.

It could be argued that the fracture set containing the elongation lineations was active at a different time than the shear zones, and therefore are not indicative of the stresses that formed the shears. However most of the lineations appear to have formed during crystal growth, which only would have occurred at significant temperatures, as would have the ductile deformation within the shear zones. More conclusive evidence that the lineations formed at the same time as the shears is the occurrence of relatively undeformed clasts within the shears with lineated surfaces. These clasts are wrapped by the strongly deformed fabric within the shears. The lineations are similarly oriented to lineations outside the shear zones.

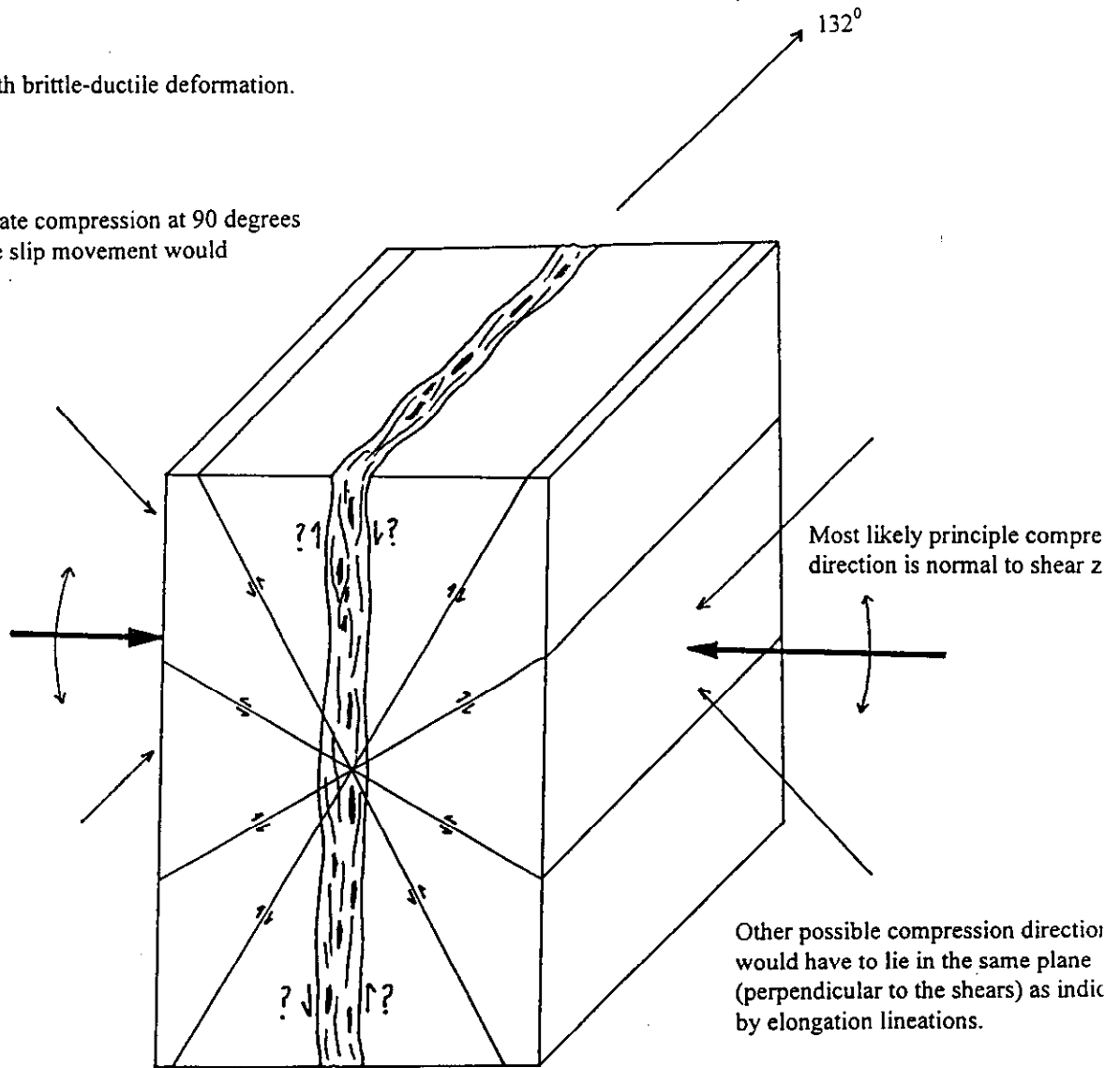
The joints which cut foliation at 90 degrees are interpreted to post date the previous lineated fracture set. They do not seem to have any immediate link with the deformation that formed the shears. The dykes which are aligned parallel to these joints are undeformed except for small offsets on foliation parallel faults. These faults represent the last deformation event, and as mentioned above, could be related to the large fault which bounds the property to the west.

The geometry of the shear zones themselves is difficult to predict from the structural data shown here. The shears are pod like, and pinch and swell as a response to unknown factors. Faults undoubtedly cut the mineralized structures at depth as well as those which have been mapped on surface.

**Schematic Block Diagram showing the most likely Principle Compression Direction.**

Shear zone with brittle-ductile deformation.

Because lineations indicate compression at 90 degrees to the shear zones, strike slip movement would not have occurred.

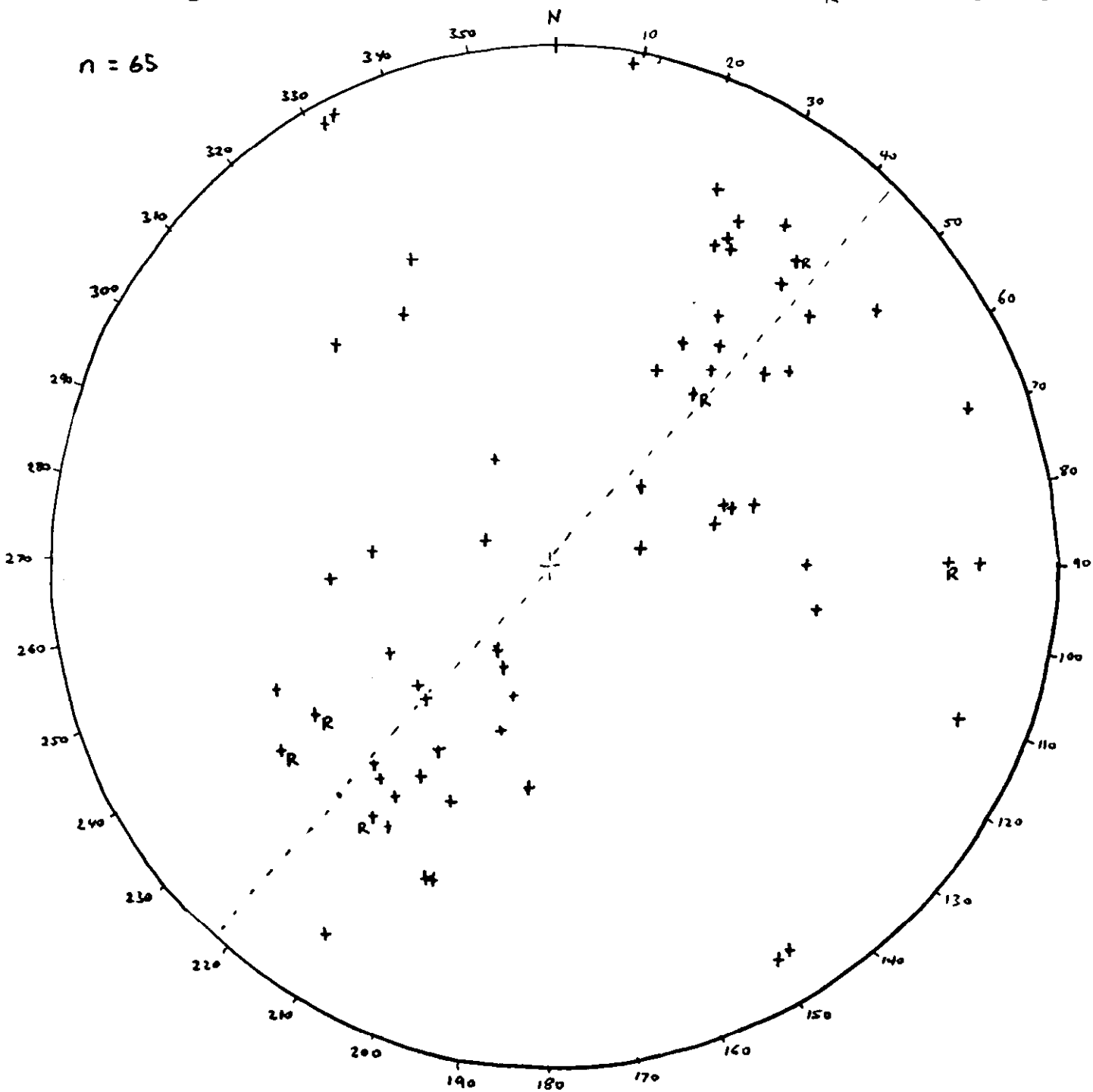


Fractures with mineral elongation lineations on their surfaces. When seen, steps on the lineations indicate reverse movement.

There would have been significant "up-down" displacement if the principle compression direction was not normal to foliation.

# ELONGATION LINEATIONS

R = Reverse sense of movement



Homestake Canada Inc.

*Date:* October 16, 1996

*To:* Andrew Kaip

*From:* Chris Huggins

*Re:* Summary of Clone field work and conclusions

The following report is a summary of field work and initial conclusions regarding the Clone property. Several days were spent on the Clone property to continue mapping at 1:500 scale, and collect data for my B.Sc. thesis on the style of deformation, and mineralogy of the area.

In total, 7.5 days were spent mapping and collecting data for the thesis topic. The first 2.5 days were spent in the area previously mapped by A. Kaip, K. Patterson, and R. McLeod, becoming familiar with the property, and making notes on the main shear zones, in particular the H-zone. Samples were collected showing clast alignment, and shearing. The following three days were spent mapping, collecting structural data, and samples in the area to the north of camp. It was in this area that I did original mapping of the property. One day was spent touring around the property with Dani Alldrick and Al Raven.

A total of 28 samples were collected for analysis by polished thin section, including 5 samples of core taken to complement the surface samples. The core samples, and samples from trenches 8 & 193 will be used in my Geology 428 Ore Microscopy course, for which a report on the mineralogy, textures, and possible deposit models will be produced. This data will also be included in my thesis paper.

### *Structure*

There is an dominant trend of the rock units, shears, and cleavage towards 320. The main area of study was the shearing within the H&S-zones, the foliation development, and the alignment of clasts in volcanoclastic and breccia units. The H-zone is strongly hematite and quartz altered, with rare sulphide mineralization and localized disseminated free gold. Within the H-zone, the he and qtz appears to be 'flowing' as in a ductile system, in addition to the presence of brittle features. Deformation in the area was likely a cyclic brittle-ductile event. There is evidence abound for this conclusion: the alignment and elongation of fragments and crystals in the rock units, pervasive foliation, and well developed S&C fabric within the shears indicate a ductile environment. The formation of Reidel shears within shear zones and brecciation of rock units along strike serves as evidence for brittle deformation. The formation of the main structures seen on the property were developed over a long period of time, with pressure and temperature conditions likely in greenschist facies.

It is anticipated that the questions of how this area was deformed will be resolved with polished thin section , SEM and TEM work. Many of the structures noted in the field could not be interpreted with confidence in the absence of thin section analysis. For

example, is the alignment of the clasts due to pure, or simple shear, or is this a combination of all of these processes?

There is some obvious shearing in the S-zone, with development of a cleavage fabric, sub-euhedral recrystallization of py and aspy, and alignment of sulphides in bands and lenticular masses. The S-zone consists primarily of Py, Aspy, and minor Cpy, with very strong pervasive chlorite alteration, with minor magnetite and hematite. The S-zone can be traced for a considerable distance, grading from fine dissemination within volcanic tuffs to massive sulphide veins up to 1m thickness.

As with the H-zone, it is unknown whether or not the textures and mineralogy along strike of the S-zone are correlative, and if the mechanism of deformation can be quantified.

Are the deformation textures for the S-zone seen in Tr 8 correlative to those seen in Tr 193, and in core, and what is the possible origin for the textures seen? Is the mineralogy the same throughout the zone? What is the mechanism of deformation of this zone, and how can it be related to the textures seen in the H-zone? As with the H-zone, these questions will be resolved through thin section study.

### *Deformation History*

1. Cyclic brittle ductile deformation
  - elongation and alignment of clasts towards  $\sim 320^\circ$
  - fluid flow along major conduits (H & S-zone?)
    - H-zone most evidence of flow & pressure solution
    - S-zone shows brittle & ductile flow of sulphides
  - brittle cataclastic features also evident in both zones
  - mostly sinistral shearing, but occasional dextral movement (conjugate shears)
2. Sinistral shears offset oriented towards  $\sim 260^\circ$ 
  - occasional dextral shears
  - shown best in diorite dyke offset in gabbro & H-zone, but pervasive throughout area
  - most readily identified shears, cut entire area of study
  - cataclastic (brittle) movement, R, R', P shear evident
  - sigmoidal tension gashes showing sinistral compression

## Conclusion

The shear system of the Clone property resulted from a long history of brittle and ductile shearing with examples showing both styles of deformation. The overall direction of movement within the primary shear system (320) is sinistral, with some vertical component.

Through detailed polished thin section analysis of strain textures in transparent and opaque minerals, the paragenetic sequence of mineral deposition and deformation history of the property will be resolved.

## Addendum

Initial thin section analysis indicates gold deposition in the last phase of brittle movement along the 320 trend from a sample in Trench 4. Other textures seen in thin section are indicative of brittle and ductile environments; from granoblastic polygonal quartz ('foam structure') to brecciated clasts and quartz grains. In some thin sections, the texture is similar to that of an ultramylonite, and a sample from a brittle shear in the gabbro on the SW side of the property shows almost no deformation of the minerals, and minor calcite fracture fill (possible tension gashes).

Appendix VIII

Summary on Clone Project

by

E.W. Grove



## **E. W. Grove Consultants Ltd.**

4581 Boulderwood Drive, Victoria, British Columbia V8Y 3A5

Telephone (604) 658-2366 · Fax (604) 658-5289

November 3, 1996

Dino Cremonese, P.Eng., President  
TEUTON RESOURCES CORP.  
509 - 675 W. Hastings Street  
VANCOUVER, B.C. V6B 1N2

Dear Dino:

### **RE: CLONE Property**

My geological appraisal of the CLONE H and S zones of mineralization in 1995 was based upon a partial day on the property and partly upon the 1996 report by Walus and Kruchkowski. Because of an unusual snowfall in mid-September I was unable to see more of the property's surface, in particular the stratigraphy mapped during the 1996 season by Homestake and Teuton personnel. I therefore spent my time on the property examining core from 14 of the 1996 drill holes.

Work by the Homestake personnel suggests that the H- and S- mineral zones lie within either mainly hornblende biotite porphyry and mafic volcanic breccia (Andrew Kaip) or a sequence comprising intermediate to mafic volcanics and sediments which have been intruded by several phases of felsic sills and dikes (McLeod).

The mixed sedimentary/volcanic explanation seems best at this time by assuming a southwest to northeast sequence in which altered and strongly deformed black 'argillite' forms the main westerly recognizable Camp unit which has been intersected in a good number of drill holes and is well exposed through the camp area. In surface outcrop this rock has a mottled aspect related to either siderite or ankerite alteration and is marked by contorted foliation. In drill core the argillite is marked by light colored, rotated angular chloritic K-feldspar, and sericitic/quartz lenses which grade into 1 to 15 cm wide finely foliated syenite/K-feldspar laminae to the west. The fragments, lenses and laminae show both flaser structure and extensive recrystallization. Drill hole 96-36 is a good example of the 'argillite' which grades westerly into a semischist/sericite schist of unknown extent. Homestake surface mapping also shows a number of 'gabbro' lenses more or less in the same stratigraphic horizon as the schist/mudstone below camp, but McLeod has suggested this argillite (mudstone) units which also includes intercalated siltstone, sandstone, and intermediate volcanic strata. The mudstone units lies in sharp and near vertical contact with a 75 to 100 meter wide mixed sequence which hosts the gold-cobalt bearing H- and S- zones. The bulk of the 1995 and 1996 core drilling has been

oriented to test this important unit. The Homestake core logging has interpreted this mixed sequence as mainly hornblende, hornblende-biotite, and biotite porphyry, and andesite with variously intercalated hematite and chlorite. This simplified nomenclature has probably been based upon map units in use at Red Mountain. In fact most of the rocks in this unit have been cataclastically deformed and intensely altered and probably include a variety of country rocks and syenite lenses (sills). Most of the country rocks are now represented by massive to mottled dark green and grey cataclasites. Most are very fine grained as a result of intense recrystallization. K-feldspar alteration which is very obvious when etched varies from a few percent to almost 100 percent over large widths both as veins, veinlets, and matrix. The breccia aspect of many of these rocks in core has been strongly accentuated by chlorite, hematite, magnetite, and by later quartz and calcite veining. Deformation features also include a variable to strong irregular foliation which cuts cataclastic foliation, as well as late crushing and faulting.

At this time the amount of fault displacement within and across the zone is uncertain although Kaip has suggested that both the H- and S- zones are fault controlled. Deformation throughout the 'Host' sequence and wall rocks exemplified by cataclasis and mylonitization is certain. As in most cataclasite zones the variable attitude and plunges noted by Kaip can be related very simply to the complex makeup of the system. That is, the finely laminated materials tend to wrap around the less friable elements such as the relatively massive syenite and quartz lenses. Foliation is therefore complex and determined by rock components and does not lend to simplistic structural determinations. Chaotic folds and foliation are typical.

The extent of chlorite alteration in these mineral zone hosts suggest relatively low grade hydrothermal alteration of a mainly basic volcanic country rock including andesitic basalts, and basalts. Relict textures in many of the cores examined showed scattered altered hornblende and augite. In hole 96-64 one segment from 47.5 to 47.8 m has a well developed trachytic texture with augite phenocrysts and could represent the preserved portion of a flow, or sill, but elsewhere in this hole I would describe the K-feldspar rich massive rocks as pseudo-porphyry. The breccia aspect of many of these rocks has been accentuated by fine grained hematite outlining the clasts as well as by K-feldspar. Hematite also comprises a number of substantial widths within the overall Host rock and coexists with variable to substantial amounts of magnetite and chlorite which has led to the general opinion that the hematite represents a mainly early alteration phase.

This Host sequence is in sharp contact to the northeast with a 100 meter thick, possibly wedge shaped, very coarse heterolithic breccia unit which contains some

auriferous hematite clasts and sulfides. This massive unit shows very little deformation and has acted as a large 'horse' within the local sequence which to the northeast again, comprises an assemblage of thinly banded mudstone, siltstone, sandstone, limestone plus intercalated volcanic rocks. McLeod has described these rocks as the basal unit and suggested tops lie to the southwest. I have not seen this sequence and cannot comment on tops but it is similar in makeup to both late Upper Triassic and early Lower Jurassic sequences found throughout the Stewart Complex. Apparently one fossil 'clam' has been found in these rocks, but was not available at the time of my visit.

Of most importance to the project is the gold-cobalt mineralization so far localized within the H- and S- zones. Native gold has been observed as fine specks in fine quartz veinlets in association with vuggy coarse specularite, with pods and lenses of sugary brown biotite, and as specks in late vuggy calcite stockwork veinlets in the H-1 hematite zones. As such, VG has been noted in several trenches and at least eight core holes (Phase 1). Sulfide distribution within the H-1 (pyrite, chalcopyrite, arsenopyrite, pyrrhotite) has not yet been plotted from trenches, core, and rock descriptions and so has been described as erratic. Sulfides seen in the core I examined have like the host materials been deformed by crushing and redistributed.

Gold and cobalt bearing sulfides appear to be found in the S- zones where chlorite rather than hematite predominates. The sulfide minerals include mainly pyrite and arsenopyrite, with lesser chalcopyrite, and pyrrhotite. In all of the core I examined from the S- zones the pyrite and arsenopyrite had been strongly crushed to form lenses and pods within the foliated cataclasites. In Hole 96-18 arsenopyrite-pyrite intersected from about 124.0 to 128.0 meters displays coarse to fine banding at about 40 degrees to the core and indicates the true width of the intersection is less than the intersection. This also suggests that the sulfides originally formed a narrow vein or lens within the now chloritic host. Other core examined (96-41, and -43) showed similar features. McLeod suggested that so far the results indicate that the hematite rich H-1 type gold mineralization will become sulfide rich (S- type?) at depth. This has not yet been demonstrated but demands that detailed cross sections and long sections are required for both the H- and S- zones.

Thus far, based upon mainly visual identifications sulfide minerals include mainly pyrite, arsenopyrite, chalcopyrite, pyrrhotite (rare), and tennantite (?). Oxide minerals include mainly hematite, magnetite, and specularite. Native gold has been identified in several associations, mainly as late stage or transported occurrences. Overall general alteration includes a variety of low grade and retrograde silicates including

biotite(s), sericite, chlorite, calcite, ankerite (siderite?), quartz, and substantial to pervasive K-feldspar. Some hematite and magnetite are alteration products. Late stage quartz stockwork veins and veinlets, as well as calcite veinlets, appear to have been the last significant mineralizing features in both the H- and S- zones.

On the basis of limited visual study I would suggest that the 'host' rock units were intruded at an early stage by mafic syenite as thin sill-like units (K-feldspar intrusives, and K-feldspar/magnetite flows are well documented in the Stewart Complex) as low temperature pre tectonic features. This event was followed by formation of sulfide veins and injection of early stage quartz veins along early fracture systems and accompanied by extensive K-feldspar metasomatism, and chloritization. Hematite/magnetite rich units within the 'Host' sequence, as well as the altered country rock, was cataclastically deformed resulting in the brecciation, boudinage, and redistribution noted today.

Explanation of the 'ore' mineralogy in the H- and S- zones should account for both the simple boudinaged auriferous sulfide lenses, the auriferous quartz lenses and stringers, and the occurrence of hematite/magnetite. Comparison of the new mineral deposit to well studied major producers (models) can provide some insight to genesis.

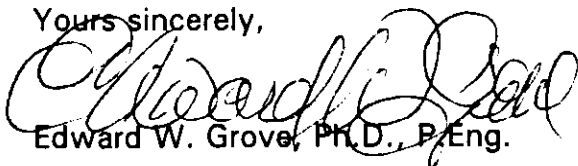
British Columbia's major producer, the Bridge River Camp (>8,000,000 oz. gold), which comprised mainly massive bull quartz veins with ribbon sulfides and free gold does not provide any insight to the Clone deposits. The Rossland Camp (2,800,000 oz. Au) ores were mainly massive to well banded pyrite, pyrrhotite, chalcopyrite veins localized along rock contacts. The copper-gold ores contained less than 10 percent quartz, and carried significant nickel and cobalt (up to 0.56% Co). K-feldspar rich intrusives (pulaskite) were also locally important features. The #3 Silbak Premier Camp (>2,000,000 oz. Au, 50,000,000 Ag) mineralization comprises a 6,000 foot long quartz replacement zone within cataclastically deformed Lower Jurassic country rocks. The ore shoots comprised massive sulfides contained within an extensive quartz rich envelope peripherally marked by wide K-feldspar alteration. Evidence for the general low temperature environment of mineralization in the camp is the presence of andularia/sericite alteration. All of the massive sulfide lenses within the Silbak Premier system have been strongly deformed to produce breccia/banded ore. The bonanza ores found near the present surface extend to depth where they change to lower grade quartz-sulfide shoots. The deposit has been classified as a telethermal or telescoped epithermal deposit. Hematite rich units located above the mineralization were first called the "purple tuff" units and were thought to control sulfide mineralization. Detailed mapping showed these units were part of the country rock sequence. Other thick hematitic strata have been mapped throughout the general area.

The Johnny Mountain gold-silver mineralization found in 1981 produced from 1986 to 1989. Ore consisted of massive to banded pyrite, chalcopyrite, pyrrhotite and lesser amounts of galena, sphalerite, a variety of gold and silver sulfides, and native gold. Quartz and carbonate content was less than 10%. Host rock syenite was fractured and altered by several phases of K-feldspar, biotite, and chlorite before injection of the massive sulfide veins. The sulfides were followed by, and host rocks were further cataclastically deformed and altered by K-feldspar metasomatism. Arsenopyrite was not a significant mineral in the sulfide veins. Vein quartz made up less than 10% of the orebodies. Overall this deposit has some similarities to the Rosslund ores but is marked by repeated cataclasis and K-feldspar metasomatism.

The nearby Snip gold deposit put into production by Cominco in 1993 represents a quartz rich, sulfide bearing, deformed vein system. The primary gold bearing sulfide is arsenopyrite with associated pyrite and pyrrhotite. The country rocks are part of an early Lower Jurassic folded, deformed siltstone sequence which has been almost entirely replaced by K-feldspar with associated chlorite and carbonate. The veins are closely associated with chalcopyrite-pyrite lenses and veins, and a syenite stock (Red Bluff). The McLymont gold deposit located on the north side of the Iskut River near Kennecott Lake has been intensely explored by core drilling and surface trenching. The mineralization consists almost entirely of massive pods of magnetite, hematite (some coarse specularite), pyrite and pyrrhotite, with lesser chalcopyrite, and minor galena and sphalerite. Native gold was found in late quartz veinlets which cut across the main mineralization. The host rocks are part of a Lower Mississippian carbonate-sandstone sequence. The deposit is a simple skarn type marked by extensive retrograde metasomatism. That is, the original skarn silicates have been altered to mainly biotite and chlorite. The overall spatial relationships have been complicated by early stage stratigraphic folding and late faulting.

The Clone mineral deposits show similarities to aspects of several of the above well explored and documented properties but resemble most closely skarn mineralization. I suggest that the Clone deposit is atypical and represents a metasomatized (K-feldspar) highly deformed skarn-like deposit along with early quartz veining.

Yours sincerely,



Edward W. Grove, Ph.D., P.Eng.

Appendix IX  
Magnetometer Readings

TEU1

Line 7+7	5N D	ate	25-Jun-96	#2
POSITIO	FIELD	ERR	DRIFT	TIME DS CULT
1750	50029.2	0.06	6744.3	9:17:39 88
1775	50021.4	0.04	6744.3	9:20:09 88
1800	50014.7	0.04	6744.2	9:21:41 88
1825	50035.2	0.07	6744	9:22:49 88
1850	50023.8	0.04	6743.9	9:23:53 88
1875	50008.7	0.04	6744	9:25:05 88
1900	50027.5	0.04	6744.2	9:26:03 88
1925	50027.2	0.04	6744.2	9:27:17 88
1950	50016	0.03	6744	9:28:11 88
1975	50008.5	0.03	6744	9:29:46 88
2000	50026.5	0.04	6744	9:30:38 88
2025	50029.2	0.04	6744.1	9:31:38 88
2050	50015.7	0.05	6744.1	9:32:45 88
2075	50024.2	0.04	6744.1	9:33:42 88
2100	50053.1	0.04	6744.2	9:34:45 88
2125	50023.5	0.03	6744.3	9:35:42 88
2150	50039.6	0.04	6744.2	9:36:47 88
2175	50030.5	0.04	6744.3	9:37:40 88
2200	50038.3	0.04	6744.4	9:38:42 88
2225	50036.4	0.14	6744.4	9:39:37 88
2250	50033.8	0.11	6744.4	9:40:38 88
2275	50042.2	0.04	6744	9:41:52 88
2300	49998.1	0.04	6743.8	9:42:52 88
2325	50033.5	0.04	6743.7	9:43:47 88
2350	50007.2	0.05	6743.6	9:44:48 88
2375	50027.3	0.04	6743.6	9:45:41 88
2400	50028.1	0.11	6743.5	9:46:43 88
2425	50019.1	0.04	6743.2	9:47:40 88
2450	50006.1	0.04	6743.1	9:48:42 88
2475	50033.1	0.05	6743	9:49:38 88
2500	49996.2	0.04	6742.9	9:50:45 88

Line 8+	00N	Date	25-Jun-96	#33
POSITIO	FIELD	ERR	DRIFT	TIME DS CULT
-2500	50010.9	0.05	6742.8	9:52:06 88
-2475	50033.5	0.05	6742.5	9:56:31 88
-2450	50043.1	0.33	6742.5	9:57:35 88
-2425	50031.8	0.03	6742.4	9:58:34 88
-2400	50031.7	0.06	6742.1	9:59:28 88
-2375	50019.5	0.04	6742.3 1	0:00:25 88
-2350	50025.4	0.05	6742.2 1	0:01:22 88
-2325	50016.2	0.03	6742.2 1	0:02:18 88
-2300	50033.7	0.07	6742.1 1	0:03:13 88
-2275	50029.6	0.04	6741.8 1	0:04:09 88
-2250	50023.1	0.04	6741.8 1	0:05:07 88
-2225	50048.5	0.04	6741.8 1	0:06:03 88
-2200	50023.9	0.05	6741.8 1	0:06:59 88
-2175	50066	0.05	6741.6 1	0:07:55 88
-2150	50028	0.06	6741.5 1	0:08:51 88
-2125	50038.4	0.06	6741.3 1	0:09:56 88

## TEU1

-2100	50004.2	0.04	6741.2 1	0:10:48	88
-2075	50052.2	0.04	6741.1 1	0:11:43	88
-2050	50031.1	0.04	6741.1 1	0:12:40	88
-2025	50037.7	0.04	6740.7 1	0:13:36	88
-2000	50028.6	0.04	6740.3 1	0:14:31	88
-1975	50048.2	0.05	6740.2 1	0:15:30	88
-1950	50025.2	0.06	6739.9 1	0:16:28	88
-1925	50061.5	0.04	6739.5 1	0:17:23	88
-1900	50029	0.04	6739.4 1	0:18:19	88
-1875	50048.2	0.12	6739.1 1	0:19:15	88
-1850	50035.1	0.04	6739.0 1	0:20:13	88
-1825	50047.7	0.25	6738.7 1	0:21:07	88
-1800	50028.7	0.12	6738.7 1	0:22:05	88
-1775	50019.2	0.19	6738.5 1	0:23:00	88
-1750	50043.2	0.15	6738.5 1	0:23:59	88

Line 8+	25N	Date	25-Jun-96	#64	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
1750	50025.1	0.04	6738.4 1	0:24:54	88
1775	50035.4	0.04	6737.7 1	0:27:29	88
1800	50053.1	0.04	6737.3 1	0:28:36	88
1825	50061.5	0.07	6737.0 1	0:29:31	88
1850	50027	0.06	6736.9 1	0:30:31	88
1875	50049.6	0.07	6736.7 1	0:31:25	88
1900	50018.4	0.04	6736.4 1	0:32:29	88
1925	50021.9	0.04	6736.5 1	0:33:25	88
1950	50028.6	0.03	6736.3 1	0:34:28	88
1975	50030.2	0.06	6736.0 1	0:35:24	88
2000	50020.1	0.03	6735.7 1	0:36:26	88
2025	50041.7	0.15	6735.8 1	0:37:21	88
2050	50010.8	0.06	6735.8 1	0:38:25	88
2075	50028.1	0.05	6735.2 1	0:39:21	88
2100	50027.6	0.04	6734.7 1	0:40:23	88
2125	50022.5	0.1	6734.9 1	0:41:18	88
2150	50013.9	0.04	6734.9 1	0:42:24	88
2175	50042.7	0.04	6734.5 1	0:43:21	88
2200	50020.3	0.04	6734.3 1	0:44:25	88
2225	50022.5	0.03	6734.5 1	0:45:22	88
2250	50006.4	0.03	6734.7 1	0:46:25	88
2275	50009.5	0.04	6734.4 1	0:47:22	88
2300	50015.4	0.03	6733.8 1	0:48:26	88
2325	50027.2	0.04	6733.5 1	0:49:38	88
2350	50019.6	0.05	6733.3 1	0:50:37	88
2375	50021.5	0.04	6733.2 1	0:51:40	88
2400	50008.9	0.04	6733.2 1	0:52:38	88
2425	50037.3	0.08	6733.5 1	0:53:44	88
2450	49994.9	0.04	6733.7 1	0:54:42	88
2475	50032.2	0.03	6733.2 1	0:55:37	88
2500	50026.2	0.09	6732.6 1	0:56:46	88

Line 8+5	ON D	ate	25-Jun-96	#95	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2500	50058.4	0.22	6732.5 1	0:57:49	88



TEU1

-2475	50041	0.04	6732.6	1	0:59:30	88
-2450	50038.1	0.04	6732.1	1	1:00:29	88
-2425	50060.9	0.14	6731.5	1	1:01:26	88
-2400	50019.5	0.03	6731.4	1	1:02:22	88
-2375	50041.4	0.08	6731.7	1	1:03:18	88
-2350	50025.2	0.11	6732.0	1	1:04:15	88
-2325	50032.3	0.05	6731.8	1	1:05:11	88
-2300	50039.4	0.04	6731.9	1	1:06:07	88
-2275	50041.2	0.07	6732.2	1	1:07:02	88
-2250	50036.3	0.04	6732.2	1	1:08:00	88
-2225	50030.3	0.07	6731.7	1	1:08:55	88
-2200	50068.4	0.15	6731.3	1	1:09:52	88
-2175	50024.1	0.14	6731.2	1	1:10:56	88
-2150	50027.3	0.03	6731.4	1	1:11:51	88
-2125	50045.4	0.07	6731.5	1	1:12:47	88
-2100	50046.9	0.04	6731.4	1	1:13:43	88
-2075	50045.7	0.04	6731.5	1	1:14:40	88
-2050	50077.4	0.18	6731.5	1	1:15:39	88
-2025	50028.2	0.04	6731.5	1	1:16:34	88
-2000	50034.3	0.04	6731.2	1	1:17:29	88
-1975	50030.9	0.04	6731.0	1	1:18:23	88
-1950	50053.4	0.04	6730.8	1	1:19:20	88
-1925	50033.9	0.03	6730.8	1	1:20:16	88
-1900	50034.2	0.04	6730.7	1	1:21:14	88
-1875	50046.7	0.04	6730.5	1	1:22:10	88
-1850	50037.4	0.03	6730.2	1	1:23:10	88
-1825	50044.2	0.04	6730.2	1	1:24:06	88
-1800	50015.3	0.04	6730.0	1	1:25:05	88
-1775	50047.6	0.05	6729.9	1	1:26:03	88
-1750	50039.6	0.04	6729.8	1	1:27:04	88

Line	8+7	5N	D	ate	25-Jun-96	#126
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1750	50022.9	0.04	6729.9	1	1:28:02	88
1775	50028.5	0.03	6729.6	1	1:32:00	88
1800	50026.6	0.04	6729.6	1	1:33:05	88
1825	50019.5	0.04	6729.4	1	1:34:05	88
1850	50018.8	0.03	6729.1	1	1:35:04	88
1875	50028.9	0.04	6729.0	1	1:36:02	88
1900	50007.8	0.04	6728.9	1	1:37:10	88
1925	50025.5	0.04	6728.9	1	1:38:06	88
1950	50039.5	0.05	6728.8	1	1:39:13	88
1975	50033.2	0.04	6728.8	1	1:40:08	88
2000	50047	0.08	6728.4	1	1:41:12	88
2025	50039.9	0.03	6728.4	1	1:42:12	88
2050	50019.7	0.04	6728.5	1	1:43:13	88
2075	50017.1	0.04	6728.4	1	1:44:10	88
2100	50020.3	0.04	6728.4	1	1:45:14	88
2125	50017.8	0.06	6728.4	1	1:46:22	88
2150	50012.3	0.03	6728.4	1	1:47:27	88
2175	50020.1	0.04	6728.3	1	1:48:25	88
2200	50034	0.05	6728.3	1	1:49:27	88

TEU1

2225	50015.9	0.06	6728.1	1	1:50:23	88
2250	50011.9	0.04	6728.0	1	1:51:28	88
2275	50003.9	0.04	6728.0	1	1:52:24	88
2300	50001.4	0.04	6727.8	1	1:53:28	88
2325	50013	0.04	6727.8	1	1:54:25	88
2350	50021.1	0.04	6727.6	1	1:55:27	88
2375	50021.5	0.03	6727.4	1	1:56:28	88
2400	50010.1	0.04	6727.5	1	1:57:32	88
2425	50020.8	0.04	6727.5	1	1:58:30	88
2450	50009	0.07	6727.5	1	1:59:33	88
2475	50003.1	0.04	6727.4	1	2:00:38	88
2500	50006.1	0.04	6727.4	1	2:01:44	88

Line 9+0	ON D	ate	25-Jun-96		#157	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT	
-2500	50013.3	0.04	6727.4	1	2:02:42	88
-2475	50033	0.04	6727.4	1	2:04:09	88
-2450	50034.4	0.05	6727.4	1	2:05:09	88
-2425	50020.7	0.03	6727.4	1	2:06:06	88
-2400	50010.3	0.04	6727.8	1	2:07:00	88
-2375	50021.3	0.04	6728.1	1	2:07:57	88
-2350	50003.5	0.04	6727.8	1	2:08:51	88
-2325	50023.9	0.04	6727.5	1	2:09:48	88
-2300	50022.4	0.05	6727.4	1	2:10:43	88
-2275	50034.5	0.05	6727.5	1	2:11:49	88
-2250	50036.2	0.05	6727.6	1	2:12:39	88
-2225	50045.2	0.05	6727.8	1	2:13:37	88
-2200	50044.2	0.03	6727.8	1	2:14:34	88
-2175	50035.7	0.05	6727.6	1	2:15:36	88
-2150	50018	0.05	6727.4	1	2:16:29	88
-2125	50051.3	0.04	6727.5	1	2:17:25	88
-2100	50027.1	0.04	6727.8	1	2:18:25	88
-2075	50024.1	0.03	6727.6	1	2:19:22	88
-2050	50032.3	0.06	6727.3	1	2:20:19	88
-2025	50031.1	0.05	6727.8	1	2:21:16	88
-2000	50022.7	0.03	6728.1	1	2:22:12	88
-1975	50026.4	0.04	6728.1	1	2:23:08	88
-1950	50036.3	0.05	6728.2	1	2:24:05	88
-1925	50025.7	0.04	6728.2	1	2:25:06	88
-1900	50019.2	0.04	6728.0	1	2:26:02	88
-1875	50037.5	0.04	6728.1	1	2:27:00	88
-1850	50020.7	0.04	6728.0	1	2:28:00	88
-1825	50040.4	0.03	6728.1	1	2:29:08	88
-1800	50056.1	0.06	6728.1	1	2:29:56	88
-1775	50041.9	0.04	6728.2	1	2:30:52	88
-1750	50036.7	0.05	6728.3	1	2:31:56	88

Line 9+2	5N D	ate	25-Jun-96		#188	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT	
1750	50012.5	0.04	6728.2	1	2:32:56	88
1775	50017.9	0.04	6728.0	1	2:34:17	88
1800	50027	0.04	6728.3	1	2:35:21	88
1825	50019.4	0.04	6728.5	1	2:36:17	88

TEU1

1850	50003.4	0.05	6728.3	1	2:37:22	88
1875	50020.7	0.04	6728.3	1	2:38:19	88
1900	50022.8	0.04	6728.3	1	2:39:25	88
1925	50024.6	0.04	6728.2	1	2:40:23	88
1950	50028.3	0.03	6728.2	1	2:41:30	88
1975	50012.1	0.04	6728.3	1	2:42:27	88
2000	50034.6	0.07	6728.3	1	2:43:33	88
2025	50017.9	0.05	6728.4	1	2:44:31	88
2050	50023.9	0.03	6728.5	1	2:45:38	88
2075	50014.1	0.04	6728.5	1	2:46:34	88
2100	50002.4	0.05	6728.6	1	2:47:40	88
2125	50014	0.03	6728.6	1	2:48:40	88
2150	50009.9	0.05	6728.6	1	2:49:46	88
2175	50006	0.05	6728.7	1	2:50:53	88
2200	50015.2	0.04	6728.7	1	2:51:49	88
2225	50012.9	0.04	6728.7	1	2:52:46	88
2250	50004	0.03	6728.7	1	2:53:49	88
2275	50017.4	0.04	6728.7	1	2:54:49	88
2300	50006.9	0.04	6728.8	1	2:55:53	88
2325	50003.2	0.05	6728.7	1	2:56:51	88
2350	50030.7	0.05	6728.6	1	2:57:59	88
2375	50001.7	0.05	6728.5	1	2:58:55	88
2400	49993.9	0.04	6728.6	1	3:00:01	88
2425	50014.8	0.19	6728.7	1	3:01:03	88
2450	50006.4	0.04	6728.8	1	3:02:06	88
2475	50015.4	0.04	6728.7	1	3:03:08	88
2500	50017	0.03	6728.6	1	3:04:15	88

Line 9+5	ON D	ate	25-Jun-96	#219		
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT	
-2500	49998.3	0.04	6728.9	1	3:05:18	88
-2475	50020	0.04	6728.9	1	3:06:45	88
-2450	50024.4	0.07	6728.8	1	3:07:44	88
-2425	50021.7	0.16	6728.9	1	3:08:41	88
-2400	50010.4	0.04	6728.8	1	3:09:37	88
-2375	50015	0.04	6729.0	1	3:10:32	88
-2350	50009.3	0.06	6729.2	1	3:11:28	88
-2325	50026.1	0.06	6729.0	1	3:12:23	88
-2300	50034.9	0.05	6729.1	1	3:13:17	88
-2275	50030.3	0.03	6729.5	1	3:14:12	88
-2250	50036.6	0.04	6729.7	1	3:15:09	88
-2225	50017.9	0.04	6729.9	1	3:16:06	88
-2200	50023.8	0.06	6730.0	1	3:17:04	88
-2175	50024.2	0.03	6730.0	1	3:17:59	88
-2150	50026.3	0.05	6730.1	1	3:18:56	88
-2125	50031.1	0.04	6730.1	1	3:19:52	88
-2100	50010.5	0.05	6730.0	1	3:20:51	88
-2075	50010.7	0.04	6730.1	1	3:21:47	88
-2050	50024.4	0.04	6730.2	1	3:22:42	88
-2025	50064.8	0.1	6730.1	1	3:23:38	88
-2000	50033	0.05	6730.2	1	3:24:35	88
-1975	50035	0.05	6730.2	1	3:25:29	88

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-1950	50053	0.05	6730.3	1	3:26:29	88
-1925	50015.5	0.1	6730.4	1	3:27:28	88
-1900	50036.1	0.04	6730.6	1	3:28:26	88
-1875	50059.1	0.05	6730.7	1	3:29:23	88
-1850	50038.1	0.1	6731.0	1	3:30:22	88
-1825	50056.2	0.04	6731.3	1	3:31:18	88
-1800	50038.8	0.04	6731.3	1	3:32:21	88
-1775	50045.5	0.04	6731.5	1	3:33:19	88
-1750	50019.3	0.03	6731.6	1	3:34:20	88

Line 9+7	5N	D	ate	25-Jun-96	#250	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1750	50017.8	0.04	6731.8	1	3:35:27	88
1775	50005	0.06	6731.9	1	3:36:55	88
1800	50010.9	0.04	6732.2	1	3:38:00	88
1825	50015.8	0.04	6732.2	1	3:38:57	88
1850	50015.5	0.08	6732.4	1	3:40:02	88
1875	50005.7	0.04	6732.6	1	3:41:00	88
1900	50023.7	0.05	6732.6	1	3:42:11	88
1925	50011.6	0.04	6732.6	1	3:43:12	88
1950	50020.1	0.07	6732.5	1	3:44:19	88
1975	50007.8	0.04	6732.6	1	3:45:17	88
2000	50021.3	0.06	6732.6	1	3:46:25	88
2025	50003.1	0.05	6732.9	1	3:47:25	88
2050	50015.6	0.06	6733.1	1	3:48:36	88
2075	50005.3	0.03	6733.1	1	3:49:35	88
2100	50009.4	0.04	6733.2	1	3:50:47	88
2125	50008.5	0.04	6733.1	1	3:51:52	88
2150	50022.1	0.04	6733.0	1	3:53:05	88
2175	50021.6	0.04	6733.0	1	3:54:03	88
2200	49992.6	0.04	6733.1	1	3:55:09	88
2225	50017.5	0.04	6733.2	1	3:56:16	88
2250	50026.4	0.04	6732.9	1	3:57:11	88
2275	50012.9	0.04	6732.8	1	3:58:10	88
2300	50015.5	0.04	6732.7	1	3:59:14	88
2325	50010.3	0.04	6732.7	1	4:00:13	88
2350	50001	0.04	6732.7	1	4:01:19	88
2375	50002.7	0.05	6732.9	1	4:02:16	88
2400	50006.9	0.04	6732.9	1	4:03:23	88
2425	50013.3	0.06	6732.8	1	4:04:22	88
2450	50005.5	0.04	6732.9	1	4:05:31	88
2475	50009.5	0.05	6733.2	1	4:06:32	88
2500	50004.5	0.04	6733.3	1	4:07:41	88

Line 10+0	0N	D	ate	25-Jun-96	#281	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-2500	50001.6	0.04	6733.4	1	4:08:37	88
-2475	50003.6	0.04	6733.4	1	4:09:56	88
-2450	50011.1	0.04	6733.7	1	4:10:56	88
-2425	50028.5	0.04	6733.9	1	4:11:50	88
-2400	50030.7	0.05	6734.1	1	4:12:47	88
-2375	50008.5	0.04	6734.2	1	4:13:46	88
-2350	50017.4	0.04	6734.2	1	4:14:43	88

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-2325	50014.4	0.04	6734.4	1	4:15:40	88
-2300	50003.4	0.04	6734.6	1	4:16:36	88
-2275	50020.9	0.13	6734.9	1	4:17:30	88
-2250	50028.7	0.03	6735.3	1	4:18:30	88
-2225	50018.7	0.04	6735.5	1	4:19:27	88
-2200	50020.4	0.04	6735.4	1	4:20:29	88
-2175	50013.9	0.04	6735.5	1	4:21:25	88
-2150	50035.1	0.04	6735.6	1	4:22:24	88
-2125	50030	0.03	6735.7	1	4:23:22	88
-2100	50029.3	0.03	6735.9	1	4:24:21	88
-2075	50011.9	0.04	6736.1	1	4:25:18	88
-2050	50025.6	0.04	6736.3	1	4:26:18	88
-2025	50010.3	0.06	6736.5	1	4:27:15	88
-2000	50018.1	0.03	6736.8	1	4:28:14	88
-1975	50030	0.05	6737.1	1	4:29:10	88
-1950	50025.7	0.06	6737.2	1	4:30:09	88
-1925	50044.7	0.04	6737.3	1	4:31:08	88
-1900	50022.3	0.04	6737.5	1	4:32:07	88
-1875	50005.4	0.04	6738.2	1	4:33:07	88
-1850	50024.5	0.04	6738.7	1	4:34:07	88
-1825	50011.7	0.04	6739.4	1	4:35:05	88
-1800	50017	0.03	6740.3	1	4:36:03	88

Line	10+2	5N	D	ate	25-Jun-96	#310
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1800	49996.2	0.04	6741.2	1	4:37:12	88
1825	50017.6	0.04	6742.2	1	4:39:02	88
1850	50035.8	0.03	6742.1	1	4:40:07	88
1875	50001	0.05	6741.4	1	4:41:06	88
1900	50015.2	0.04	6740.7	1	4:42:16	88
1925	50012	0.04	6740.3	1	4:43:20	88
1950	50011	0.04	6740.0	1	4:44:27	88
1975	50007.3	0.04	6739.5	1	4:45:28	88
2000	50021.7	0.03	6739.0	1	4:46:38	88
2025	50022.4	0.04	6738.6	1	4:47:43	88
2050	50007.3	0.04	6737.9	1	4:48:49	88
2075	50015.1	0.05	6737.5	1	4:50:06	88
2100	50023.8	0.03	6737.3	1	4:51:16	88
2125	50006	0.05	6737.2	1	4:52:19	88
2150	50021.2	0.03	6737.1	1	4:53:26	88
2175	50007.9	0.04	6736.8	1	4:54:29	88
2200	50010.8	0.04	6736.7	1	4:55:36	88
2225	50024.8	0.03	6736.9	1	4:56:35	88
2250	50003.3	0.09	6737.4	1	4:57:44	88
2275	50012.3	0.04	6737.7	1	4:58:51	88
2300	50002	0.04	6737.6	1	5:00:00	88
2325	49994.3	0.04	6737.2	1	5:01:03	88
2350	49992.1	0.05	6737.0	1	5:02:11	88
2375	50003.7	0.04	6736.5	1	5:03:11	88
2400	50023.9	0.04	6736.5	1	5:04:21	88
2425	50003.2	0.04	6736.5	1	5:05:21	88
2450	50002.3	0.04	6736.7	1	5:06:30	88

## TEU1

2475	49994.9	0.04	6736.7	1	5:07:29	88
2500	50017.8	0.04	6736.9	1	5:08:41	88
Line 10+5	0N D	ate	25-Jun-96			#339
POSITIO	FIELD	ERR	DRIFT		TIME	DS CULT
-2500	49995.6	0.04	6737.5	1	5:09:48	88
-2475	50014.2	0.06	6738.4	1	5:11:09	88
-2450	50021.4	0.04	6739.0	1	5:12:11	88
-2425	50018.9	0.05	6739.5	1	5:13:09	88
-2400	50050.1	0.04	6739.9	1	5:14:07	88
-2375	50024.8	0.04	6739.7	1	5:15:06	88
-2350	50010	0.04	6739.5	1	5:16:05	88
-2325	50024.4	0.07	6739.3	1	5:17:02	88
-2300	50032.4	0.04	6739.2	1	5:18:02	88
-2275	50031.2	0.05	6739.0	1	5:19:01	88
-2250	50026.5	0.03	6738.7	1	5:19:56	88
-2225	50032.2	0.04	6738.2	1	5:20:52	88
-2200	50025.9	0.04	6737.8	1	5:21:49	88
-2175	50043.8	0.04	6737.6	1	5:22:46	88
-2150	50034.2	0.04	6737.3	1	5:23:43	88
-2125	50022.9	0.03	6737.2	1	5:24:41	88
-2100	50013.3	0.04	6737.2	1	5:25:45	88
-2075	50024.3	0.04	6737.1	1	5:26:43	88
-2050	50012.6	0.06	6736.6	1	5:27:42	88
-2025	50020.5	0.04	6736.2	1	5:28:43	88
-2000	50017.4	0.04	6735.9	1	5:29:39	88
-1975	50029.7	0.08	6735.5	1	5:30:37	88
-1950	50014.6	0.04	6735.0	1	5:31:37	88
-1925	50032.4	0.05	6734.4	1	5:32:34	88
-1900	50057.1	0.25	6733.7	1	5:33:35	88
-1875	50041.4	0.06	6733.2	1	5:34:30	88
-1850	50038.8	0.04	6733.0	1	5:35:31	88
-1825	50012.7	0.04	6733.1	1	5:36:30	88
-1800	50007.5	0.04	6733.2	1	5:37:30	88
Line 10+7	5N D	ate	25-Jun-96			#368
POSITIO	FIELD	ERR	DRIFT		TIME	DS CULT
1800	50006.4	0.04	6733.1	1	5:38:39	88
1825	50016.5	0.03	6733.0	1	5:39:54	88
1850	50002.9	0.04	6732.8	1	5:41:04	88
1875	50004.7	0.04	6732.9	1	5:42:02	88
1900	49997.5	0.04	6733.1	1	5:43:13	88
1925	50017.4	0.03	6733.3	1	5:44:12	88
1950	50019.4	0.05	6733.5	1	5:45:23	88
1975	50012.5	0.04	6733.7	1	5:46:21	88
2000	50019.9	0.05	6733.6	1	5:47:33	88

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## TEU2

Line 10+7	5N	D	ate	28-Jun-96	#1
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
2000	50051	0.05	6739.8	9:14:02	88
2025	50003.5	0.05	6739.9	9:15:56	88
2050	50007.4	0.04	6740.2	9:17:02	88
2075	50004.4	0.04	6740.3	9:18:19	88
2100	50003.9	0.05	6740.1	9:19:39	88
2125	50004.2	0.04	6740.3	9:20:38	88
2150	50009.9	0.05	6740.4	9:21:40	88
2175	49992.1	0.04	6740.7	9:23:04	88
2200	50018.7	0.04	6740.6	9:23:59	88
2225	50007.1	0.04	6740.5	9:24:55	88
2250	50014.1	0.05	6740.6	9:25:58	88
2275	50017.6	0.04	6740.5	9:26:55	88
2300	50000.8	0.04	6740.5	9:27:55	88
2325	49995.5	0.05	6740.4	9:28:57	88
2350	50009.6	0.04	6740.3	9:29:53	88
2375	50013.6	0.05	6740.3	9:30:49	88
2400	50010.3	0.04	6740.3	9:31:52	88
2425	50030.5	0.05	6740.2	9:32:52	88
2450	50028.4	0.04	6740.3	9:33:54	88
2475	50005.6	0.04	6740.2	9:34:53	88
2500	50001.5	0.05	6739.9	9:35:57	88

Line 11+0	ON	D	ate	28-Jun-96	#22
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2500	50012.6	0.04	6739.3	9:41:28	88
-2475	50020.7	0.15	6738.9	9:43:15	88
-2450	50006.9	0.04	6738.7	9:44:18	88
-2425	50029.7	0.04	6738.6	9:45:24	88
-2400	50063.3	1	6738.6	9:46:17	88
-2375	50014.2	0.04	6738.7	9:47:14	88
-2350	50009.8	0.06	6738.5	9:48:11	88
-2325	50018.2	0.07	6738.2	9:49:11	88
-2300	50017.2	0.04	6738.2	9:50:06	88
-2275	50017.5	0.03	6737.9	9:51:02	88
-2250	50017.5	0.04	6737.7	9:51:56	88
-2225	50029.6	0.04	6737.6	9:52:51	88
-2200	50007.6	0.06	6737.6	9:54:18	88
-2175	50017.5	0.04	6737.2	9:55:15	88
-2150	50039.8	0.05	6736.7	9:56:12	88
-2125	50023.6	0.05	6736.3	9:57:10	88
-2100	50026.2	0.04	6736.1	9:58:07	88
-2075	50023.3	0.04	6735.9	9:59:03	88
-2050	50017.1	0.04	6735.9	9:59:59	88
-2025	50021.6	0.19	6735.7 1	0:00:57	88
-2000	50012.4	0.04	6735.6 1	0:01:53	88
-1975	50020.1	0.04	6735.1 1	0:03:00	88
-1950	50017.9	0.04	6735.1 1	0:03:54	88
-1925	50027	0.04	6735.1 1	0:04:49	88
-1900	50006.8	0.04	6735.1 1	0:05:47	88
-1875	50028.7	0.04	6735.0 1	0:06:46	88

## TEU2

-1850	50016	0.04	6734.7	1	0:07:41	88
-1825	50019.5	0.05	6734.5	1	0:08:36	88
-1800	50014.5	0.04	6734.3	1	0:09:31	88
Line 11+2	5N D	ate	28-Jun-96		#51	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1800	49990.4	0.04	6734.2	1	0:10:39	88
1825	50003.1	0.04	6733.9	1	0:12:03	88
1850	50003.9	0.06	6733.9	1	0:13:04	88
1875	50007	0.04	6734.1	1	0:13:59	88
1900	50008.4	0.05	6734.1	1	0:15:03	88
1925	50009.8	0.09	6734.1	1	0:15:59	88
1950	50015.6	0.04	6734.1	1	0:17:02	88
1975	50004.2	0.06	6734.0	1	0:18:06	88
2000	49996.3	0.05	6734.0	1	0:19:11	88
2025	50011.5	0.04	6733.7	1	0:20:09	88
2050	50012.1	0.06	6733.6	1	0:21:15	88
2075	50007.3	0.05	6733.2	1	0:22:12	88
2100	50009.4	0.04	6733.0	1	0:23:15	88
2125	50020	0.04	6732.6	1	0:24:09	88
2150	50001.3	0.04	6732.2	1	0:25:16	88
2175	50008.5	0.04	6732.2	1	0:26:14	88
2200	50021.2	0.04	6731.9	1	0:27:22	88
2225	50013.5	0.04	6731.8	1	0:28:18	88
2250	50005.7	0.07	6731.8	1	0:29:19	88
2275	50003.3	0.05	6731.6	1	0:30:15	88
2300	50002.4	0.08	6731.5	1	0:31:17	88
2325	50011.2	0.05	6731.6	1	0:32:14	88
2350	50004.5	0.07	6731.5	1	0:33:18	88
2375	50006.3	0.06	6731.5	1	0:34:23	88
2400	50010.5	0.04	6731.4	1	0:35:31	88
2425	50025.7	0.04	6731.1	1	0:36:30	88
2450	50006.6	0.16	6730.9	1	0:37:34	88
2475	50010.9	0.04	6730.6	1	0:38:55	88
2500	49996.8	0.05	6730.0	1	0:40:38	88

Line 11+5	0N D	ate	28-Jun-96		#80	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-2500	50008.4	0.06	6729.3	1	0:41:41	88
-2475	49974.1	0.04	6728.9	1	0:43:00	88
-2450	50019.1	0.04	6728.7	1	0:44:53	88
-2425	50017.1	0.15	6728.5	1	0:46:03	88
-2400	50026.5	0.04	6728.2	1	0:47:00	88
-2375	50032.9	0.04	6727.9	1	0:48:09	88
-2350	50004	0.04	6727.7	1	0:49:05	88
-2325	50015.6	0.05	6727.7	1	0:49:59	88
-2300	50006.7	0.04	6727.7	1	0:50:56	88
-2275	50025.9	0.04	6727.8	1	0:51:49	88
-2250	49999.6	0.05	6727.7	1	0:52:44	88
-2225	50024.8	0.97	6727.5	1	0:53:36	88
-2200	50002.3	0.04	6727.4	1	0:54:35	88
-2175	50009.1	0.05	6727.2	1	0:55:28	88
-2150	50008.1	0.06	6726.9	1	0:56:23	88



TEU2

-2125	50019.1	0.04	6726.6	1	0:57:16	88
-2100	50024.5	0.04	6726.6	1	0:58:14	88
-2075	50012.1	0.09	6726.4	1	0:59:06	88
-2050	49991.9	0.08	6726.2	1	1:00:03	88
-2025	50015.7	0.04	6725.8	1	1:00:57	88
-2000	50018.8	0.06	6725.5	1	1:01:52	88
-1975	50021.7	0.12	6725.4	1	1:02:44	88
-1950	50009.9	0.1	6725.2	1	1:03:42	88
-1925	50005.4	0.04	6725.0	1	1:04:38	88
-1900	49996.9	0.07	6725.1	1	1:05:33	88
-1875	50007.8	0.04	6724.9	1	1:06:28	88
-1850	49986.3	0.05	6724.6	1	1:07:23	88
-1825	50000.5	0.04	6724.4	1	1:08:20	88
-1800	49998.8	0.06	6724.2	1	1:09:17	88
Line 11+7	5N D	ate	28-Jun-96			#109
POSITIO	FIELD	ERR	DRIFT	TIME		DS CULT
1800	50001.9	0.04	6724.2	1	1:10:19	88
1825	50009.4	0.04	6724.1	1	1:11:30	88
1850	50002.1	0.05	6723.9	1	1:12:31	88
1875	50001.3	0.04	6723.9	1	1:13:28	88
1900	50008.4	0.05	6723.6	1	1:14:34	88
1925	50002	0.04	6723.4	1	1:15:34	88
1950	50015.8	0.05	6723.6	1	1:16:40	88
1975	49995.9	0.05	6723.7	1	1:17:38	88
2000	50007.2	0.05	6723.7	1	1:18:42	88
2025	49991.6	0.05	6723.7	1	1:19:38	88
2050	50002.1	0.04	6723.2	1	1:20:43	88
2075	50003.7	0.05	6722.9	1	1:21:39	88
2100	50011	0.05	6723.0	1	1:22:39	88
2125	50010	0.06	6723.2	1	1:23:40	88
2150	50003.1	0.05	6723.2	1	1:24:42	88
2175	50011.8	0.04	6723.0	1	1:25:39	88
2200	50008.5	0.05	6722.7	1	1:26:43	88
2225	50017.7	0.08	6722.6	1	1:27:44	88
2250	50003.2	0.04	6722.4	1	1:28:49	88
2275	50008.7	0.04	6722.4	1	1:29:47	88
2300	49998.6	0.05	6722.6	1	1:30:47	88
2325	50006	0.08	6722.7	1	1:31:45	88
2350	49998.2	0.06	6722.8	1	1:32:48	88
2375	50008.9	0.06	6722.9	1	1:33:45	88
2400	49997	0.04	6723.0	1	1:34:47	88
2425	50011.1	0.05	6723.1	1	1:35:44	88
2450	50002.7	0.04	6723.2	1	1:36:51	88
2475	50016.4	0.1	6722.9	1	1:37:49	88
2500	49989.2	0.04	6722.4	1	1:38:59	88
Line 12+0	0N D	ate	28-Jun-96			#138
POSITIO	FIELD	ERR	DRIFT	TIME		DS CULT
-2500	49983.8	0.04	6722.0	1	1:40:01	88
-2475	50014.2	0.09	6721.7	1	1:41:08	88
-2450	49995.9	0.04	6721.3	1	1:42:05	88
-2425	50005.2	0.04	6721.3	1	1:43:02	88

## TEU2

-2400	49999.4	0.04	6721.5	1	1:43:59	88
-2375	50008.7	0.04	6721.6	1	1:44:52	88
-2350	49980.9	0.04	6721.4	1	1:45:47	88
-2325	50007.9	0.04	6721.3	1	1:46:40	88
-2300	49990.3	0.05	6721.4	1	1:47:36	88
-2275	49999.5	0.04	6721.4	1	1:48:36	88
-2250	49994.5	0.04	6721.4	1	1:49:26	88
-2225	50014.2	0.04	6721.5	1	1:50:21	88
-2200	49999	0.04	6721.4	1	1:51:15	88
-2175	50010.8	0.04	6721.3	1	1:52:10	88
-2150	50006.9	0.04	6721.3	1	1:53:07	88
-2125	50010.1	0.06	6721.3	1	1:54:02	88
-2100	49997.6	0.04	6721.2	1	1:54:59	88
-2075	50006	0.04	6721.1	1	1:55:54	88
-2050	50005.1	0.05	6721.3	1	1:56:49	88
-2025	50013.7	0.05	6721.3	1	1:57:44	88
-2000	49991	0.12	6721.2	1	1:58:41	88
-1975	50010.4	0.04	6721.3	1	1:59:37	88
-1950	50024.7	0.04	6721.4	1	2:00:34	88
-1925	50015.4	0.04	6721.4	1	2:01:31	88
-1900	49994.9	0.04	6721.3	1	2:02:31	88
-1875	50010.1	0.04	6721.3	1	2:03:27	88
-1850	49981.8	0.04	6721.2	1	2:04:22	88
-1825	49993.7	0.04	6721.3	1	2:05:18	88
-1800	49986.4	0.04	6721.2	1	2:06:10	88

Line	12+2	5N	D	ate	28-Jun-96	#167
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1800	49989.3	0.04	6721.2	1	2:07:13	88
1825	49992	0.04	6721.1	1	2:08:24	88
1850	49982.8	0.04	6720.9	1	2:09:28	88
1875	50006.3	0.05	6720.6	1	2:10:24	88
1900	50001.9	0.04	6720.4	1	2:11:29	88
1925	50002.1	0.05	6720.3	1	2:12:24	88
1950	49997.8	0.06	6720.3	1	2:13:31	88
1975	49990.3	0.04	6720.2	1	2:14:27	88
2000	49998.3	0.04	6720.0	1	2:15:32	88
2025	49990.1	0.04	6719.9	1	2:16:29	88
2050	50001	0.04	6720.1	1	2:17:35	88
2075	50031.2	0.11	6720.3	1	2:18:35	88
2100	49993.8	0.06	6720.1	1	2:19:38	88
2125	49999.5	0.04	6720.0	1	2:20:32	88
2150	50002.8	0.05	6720.1	1	2:21:38	88
2175	49988.6	0.04	6720.0	1	2:22:36	88
2200	50009.4	0.04	6720.0	1	2:23:39	88
2225	50007.8	0.05	6720.0	1	2:24:42	88
2250	49999.9	0.04	6720.0	1	2:25:37	88
2275	50006.2	0.04	6720.1	1	2:26:33	88
2300	50009	0.08	6720.2	1	2:27:42	88
2325	50003.7	0.04	6720.0	1	2:28:38	88
2350	50089.6	1.5	6720.0	1	2:29:42	88
2375	50011.8	0.04	6720.1	1	2:30:40	88

## TEU2

2400	49992.4	0.06	6720.0	1	2:31:45	88
2425	50009.6	0.05	6719.9	1	2:32:52	88
2450	50006.3	0.07	6719.8	1	2:33:56	88
2475	50000.5	0.04	6719.9	1	2:34:50	88
2500	49998	0.04	6720.3	1	2:35:56	88
Line 12+5	0N D	ate	28-Jun-96			#196
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-2500	49995	0.04	6720.5	1	2:37:00	88
-2475	50004.3	0.04	6721.0	1	2:38:40	88
-2450	50010	0.04	6721.1	1	2:39:29	88
-2425	50024.6	0.04	6721.3	1	2:40:24	88
-2400	49997.4	0.04	6721.6	1	2:41:18	88
-2375	50021.7	0.05	6721.8	1	2:42:12	88
-2350	50003.4	0.05	6721.8	1	2:43:07	88
-2325	50007.6	0.04	6722.1	1	2:44:04	88
-2300	49992.6	0.04	6722.1	1	2:44:56	88
-2275	50009.4	0.05	6722.6	1	2:45:50	88
-2250	50008.2	0.05	6723.6	1	2:46:44	88
-2225	50018.1	0.04	6724.0	1	2:47:41	88
-2200	50001.1	0.05	6723.7	1	2:48:36	88
-2175	50013.7	0.06	6723.4	1	2:49:31	88
-2150	49988.8	0.04	6723.4	1	2:50:26	88
-2125	50002.7	0.04	6723.1	1	2:51:21	88
-2100	49994.6	0.04	6722.8	1	2:52:16	88
-2075	50001.2	0.04	6723.1	1	2:53:10	88
-2050	50007.2	0.07	6722.9	1	2:54:07	88
-2025	50001.7	0.04	6722.9	1	2:55:12	88
-2000	50000.7	0.05	6722.7	1	2:56:08	88
-1975	50007.9	0.04	6722.9	1	2:57:03	88
-1950	50009.8	0.04	6723.0	1	2:58:00	88
-1925	50015.8	0.07	6723.1	1	2:58:55	88
-1900	49985.5	0.04	6723.1	1	2:59:52	88
-1875	50003	0.04	6723.0	1	3:00:48	88
-1850	49992.7	0.04	6723.0	1	3:01:43	88
-1825	49996.3	0.04	6723.0	1	3:02:36	88
-1800	49983.3	0.05	6722.8	1	3:03:32	88
Line 12+7	5N D	ate	28-Jun-96			#225
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1800	49991.4	0.04	6722.8	1	3:04:33	88
1825	49986.1	0.05	6722.9	1	3:05:46	88
1850	49988.3	0.05	6723.0	1	3:06:55	88
1875	49980.5	0.04	6723.1	1	3:07:58	88
1900	49993.1	0.06	6723.1	1	3:09:03	88
1925	49999.2	0.04	6723.1	1	3:09:59	88
1950	49995.5	0.05	6722.9	1	3:11:02	88
1975	49992.7	0.05	6722.8	1	3:11:58	88
2000	49999	0.04	6722.7	1	3:13:02	88
2025	50000.4	0.06	6722.7	1	3:13:59	88
2050	50001.7	0.04	6722.9	1	3:15:03	88
2075	50009.3	0.05	6723.0	1	3:15:57	88
2100	50022	0.06	6723.1	1	3:17:03	88

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2125	50002.8	0.05	6723.4	1	3:18:00	88
2150	49991.1	0.04	6724.0	1	3:19:00	88
2175	50001.6	0.04	6724.2	1	3:19:58	88
2200	50007.2	0.06	6724.4	1	3:21:00	88
2225	49992.6	0.04	6724.7	1	3:22:06	88
2250	50001.7	0.05	6725.0	1	3:23:03	88
2275	50012.6	0.04	6725.3	1	3:24:01	88
2300	49988.1	0.04	6725.5	1	3:25:06	88
2325	50002.8	0.05	6725.4	1	3:26:05	88
2350	50006.5	0.04	6725.5	1	3:27:04	88
2375	49994.9	0.04	6725.7	1	3:28:01	88
2400	50008.6	0.04	6725.6	1	3:29:05	88
2425	49996.1	0.04	6725.7	1	3:30:03	88
2450	50006	0.05	6726.2	1	3:31:05	88
2475	50003.1	0.04	6726.3	1	3:32:03	88
2500	50009.3	0.04	6726.6	1	3:33:07	88

Line 13+0	ON	D	ate	28-Jun-96	#254	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT	
-2500	49994.7	0.04	6726.9	1	3:37:34	88
-2475	50003.8	0.05	6727.1	1	3:38:51	88
-2450	49996.5	0.07	6727.1	1	3:39:46	88
-2425	50006.4	0.05	6727.3	1	3:40:44	88
-2400	49998.1	0.06	6727.4	1	3:41:40	88
-2375	50003.6	0.05	6727.6	1	3:42:35	88
-2350	49990.7	0.15	6728.0	1	3:43:30	88
-2325	50006.4	0.04	6728.2	1	3:44:25	88
-2300	50000.7	0.05	6728.5	1	3:45:22	88
-2275	50006.7	0.04	6728.8	1	3:46:21	88
-2250	49985	0.04	6728.9	1	3:47:17	88
-2225	50005.2	0.04	6729.2	1	3:48:10	88
-2200	49995.1	0.04	6729.5	1	3:49:05	88
-2175	50000.9	0.05	6729.7	1	3:50:02	88
-2150	49988.1	0.04	6729.8	1	3:50:53	88
-2125	49996	0.04	6730.4	1	3:51:46	88
-2100	49983.7	0.04	6730.8	1	3:52:40	88
-2075	50013.2	0.04	6731.0	1	3:53:35	88
-2050	49985.4	0.06	6731.2	1	3:54:30	88
-2025	50012.5	0.05	6731.2	1	3:55:23	88
-2000	49990.2	0.05	6731.3	1	3:56:20	88
-1975	49998.2	0.04	6731.4	1	3:57:17	88
-1950	49989.7	0.15	6731.2	1	3:58:12	88
-1925	49992.1	0.04	6731.0	1	3:59:08	88
-1900	49993.7	0.05	6731.2	1	4:00:03	88
-1875	50001.3	0.04	6731.2	1	4:00:58	88
-1850	49966.5	0.04	6731.2	1	4:01:52	88
-1825	49985.9	0.08	6731.2	1	4:02:46	88
-1800	49982.8	0.05	6731.6	1	4:03:44	88

Line 13+2	5N	D	ate	28-Jun-96	#283	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT	
1800	49978.6	0.04	6732.0	1	4:04:45	88
1825	49969.7	0.05	6731.7	1	4:06:32	88

TEU2

1850	49978.9	0.05	6731.6 1	4:07:40	88
1875	49983.1	0.04	6731.7 1	4:08:37	88
1900	49996.7	0.04	6731.8 1	4:09:42	88
1925	49985.1	0.04	6732.0 1	4:10:40	88
1950	49967.9	0.08	6731.8 1	4:11:46	88
1975	49992.9	0.04	6731.9 1	4:12:46	88
2000	49986.3	0.04	6731.8 1	4:14:00	88

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## TEU3

Line 13+2	5N	D	ate	29-Jun-96	#1
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
2000	50006.3	0.04	6681.2	8:57:49	88
2025	50008.8	0.04	6691.3	9:00:25	88
2050	50028.9	0.04	6690.2	9:03:45	88
2075	50008.5	0.04	6689.1	9:04:54	88
2100	50013.8	0.04	6688.8	9:05:59	88
2125	50021.5	0.04	6687.8	9:08:15	88
2150	50013.4	0.05	6687	9:09:33	88
2175	50018.2	0.04	6686.8	9:10:32	88
2200	50010.7	0.04	6686.1	9:12:24	88
2225	50038.8	0.04	6686	9:13:58	88
2250	50035	0.04	6687.3	9:15:12	88
2275	50018.9	0.05	6693.4	9:16:09	88
2300	50034.7	0.04	6677.1	9:17:15	88
2325	50054.6	0.04	6659.7	9:18:15	88
2350	50029.7	0.04	6684.6	9:21:15	88
2375	50027.9	0.04	6685.1	9:22:10	88
2400	50029.5	0.04	6685.4	9:23:11	88
2425	50042	0.05	6667	9:24:34	88
2450	50040	0.04	6673.3	9:25:32	88
2475	50023.7	0.04	6694.4	9:26:27	88
2500	50033.4	0.04	6689.1	9:27:27	88

Line 13+5	0N	D	ate	29-Jun-96	#22
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2500	50042.2	0.05	6684.8	9:28:26	88
-2475	50026.6	0.04	6694.5	9:29:45	88
-2450	50024	0.03	6693.5	9:30:38	88
-2425	50034.4	0.04	6696.5	9:31:35	88
-2400	50023.7	0.04	6698.6	9:32:23	88
-2375	50025.4	0.04	6696.9	9:33:22	88
-2350	50033.1	0.04	6698.9	9:38:12	88
-2325	50031.7	0.05	6696	9:39:15	88
-2300	50039	0.14	6689.9	9:40:08	88
-2275	50058.8	0.07	6700.7	9:41:01	88
-2250	50015.2	0.06	6697.9	9:41:54	88
-2225	50031.8	0.05	6700.3	9:42:49	88
-2200	50034.3	0.05	6700.1	9:45:45	88
-2175	50060.4	0.04	6660.9	9:46:41	88
-2150	50034	0.05	6674	9:47:35	88
-2125	50029.9	0.04	6698.9	9:48:32	88
-2100	50015	0.05	6698.9	9:49:21	88
-2075	50021.1	0.04	6700	9:50:17	88
-2050	50000.8	0.05	6698.5	9:51:08	88
-2025	50036.1	0.04	6682.7	9:52:04	88
-2000	49999.8	0.12	6699.1	9:52:59	88
-1975	50005.3	0.04	6698.7	9:53:56	88
-1950	50015.8	0.08	6696.5	9:54:46	88
-1925	49992.6	0.04	6697.4	9:55:43	88
-1900	50006.5	0.04	6698.3	9:56:35	88
-1875	49997.8	0.04	6698.5	9:57:35	88

## TEU3

-1850	49985.3	0.09	6698.3	9:58:22	88
-1825	49998	0.05	6698	9:59:17	88
-1800	49971.5	0.04	6699.0 1	0:00:12	88
Line 13+7	5N D	ate	29-Jun-96	#51	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
1800	49975	0.03	6699.3 1	0:01:15	88
1825	49981.2	0.04	6695.9 1	0:02:23	88
1850	49984	0.04	6694.4 1	0:03:30	88
1875	49991.1	0.04	6698.0 1	0:04:29	88
1900	49991.4	0.04	6697.2 1	0:05:33	88
1925	49995.1	0.05	6697.3 1	0:06:41	88
1950	49985.8	0.04	6698.5 1	0:07:38	88
1975	49999.8	0.04	6698.2 1	0:08:45	88
2000	49998.9	0.04	6698.4 1	0:09:39	88
2025	49999.1	0.05	6697.7 1	0:10:51	88
2050	50005.1	0.04	6697.4 1	0:11:44	88
2075	49989.8	0.04	6696.4 1	0:12:49	88
2100	49999	0.04	6697.9 1	0:13:46	88
2125	50004.1	0.06	6697.0 1	0:14:50	88
2150	50001.7	0.04	6697.6 1	0:15:46	88
2175	50003.6	0.04	6690.1 1	0:16:50	88
2200	50002.5	0.04	6694.8 1	0:17:42	88
2225	49994.1	0.04	6698.5 1	0:18:45	88
2250	50002.3	0.15	6696.2 1	0:19:42	88
2275	49998.8	0.05	6696.1 1	0:20:44	88
2300	50004.3	0.16	6696.7 1	0:21:43	88
2325	49989.1	0.04	6696.7 1	0:22:46	88
2350	50003.9	0.07	6696.9 1	0:23:41	88
2375	50007.6	0.04	6698.4 1	0:24:44	88
2400	50005.6	0.04	6697.8 1	0:25:39	88
2425	50016	0.04	6697.2 1	0:26:35	88
2450	50012	0.04	6695.1 1	0:27:36	88
2475	49994.9	0.04	6695.4 1	0:28:32	88
2500	50013.7	0.06	6698.4 1	0:29:33	88

Line 14+0	0N D	ate	29-Jun-96	#81	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2500	50028	0.04	6698.9 1	0:32:42	88
-2475	50027.7	0.04	6699.9 1	0:33:56	88
-2450	50023.9	0.04	6699.2 1	0:34:52	88
-2425	50025.3	0.05	6699.4 1	0:35:50	88
-2400	50016.6	0.04	6700.3 1	0:36:45	88
-2375	50028.8	0.04	6700.6 1	0:37:44	88
-2350	49988.7	0.04	6700.6 1	0:38:36	88
-2325	50016.5	0.04	6700.5 1	0:39:33	88
-2300	50005.6	0.13	6700.3 1	0:40:28	88
-2275	50019	0.04	6700.4 1	0:41:25	88
-2250	49991.4	0.04	6700.2 1	0:42:19	88
-2225	50014.1	0.05	6699.9 1	0:43:25	88
-2200	50004.6	0.04	6699.9 1	0:44:11	88
-2175	50015.1	0.04	6699.8 1	0:45:06	88
-2150	49999.3	0.04	6699.5 1	0:46:03	88

## TEU3

-2125	50004.5	0.04	6698.6	1	0:47:00	88
-2100	50009.9	0.06	6698.9	1	0:47:55	88
-2075	50014.1	0.03	6699.0	1	0:48:52	88
-2050	49989.9	0.04	6698.6	1	0:49:50	88
-2025	50000.7	0.04	6699.1	1	0:50:50	88
-2000	50014.2	0.05	6698.9	1	0:51:41	88
-1975	49993.3	0.03	6699.0	1	0:52:37	88
-1950	49992	0.04	6699.3	1	0:53:31	88
-1925	49998.6	0.04	6698.9	1	0:54:26	88
-1900	49988.2	0.05	6698.6	1	0:55:19	88
-1875	49994.6	0.04	6699.1	1	0:56:13	88
-1850	49989.3	0.06	6698.5	1	0:57:05	88
-1825	49971.3	0.12	6698.3	1	0:58:01	88
-1800	49978.2	0.06	6698.3	1	0:58:54	88

Line 14+2	5N	D	ate	29-Jun-96	#110	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT	
1800	49970.1	0.03	6698.6	1	0:59:56	88
1825	49967.6	0.04	6698.0	1	1:01:06	88
1850	49986.3	0.06	6698.6	1	1:02:13	88
1875	49974.8	0.04	6698.4	1	1:03:24	88
1900	49979.5	0.03	6698.6	1	1:04:30	88
1925	49993.2	0.04	6698.3	1	1:05:29	88
1950	49985.2	0.04	6698.7	1	1:06:33	88
1975	50011.5	0.04	6698.8	1	1:07:35	88
2000	49991.1	0.05	6698.5	1	1:08:37	88
2025	49989.2	0.05	6698.5	1	1:09:33	88
2050	50000.8	0.04	6698.9	1	1:10:40	88
2075	50009.2	0.04	6699.1	1	1:11:36	88
2100	50003.8	0.04	6698.5	1	1:12:53	88
2125	49999	0.04	6698.4	1	1:13:52	88
2150	50006.7	0.03	6698.8	1	1:14:54	88
2175	49995	0.04	6698.4	1	1:15:56	88
2200	49999.4	0.05	6698.8	1	1:16:52	88
2225	49989.4	0.06	6698.5	1	1:17:49	88
2250	50005.8	0.04	6698.4	1	1:18:51	88
2275	49995.8	0.08	6698.5	1	1:19:51	88
2300	49991.9	0.04	6699.0	1	1:20:52	88
2325	49991.4	0.04	6698.6	1	1:21:49	88
2350	50008.1	0.04	6698.4	1	1:22:50	88
2375	49999.7	0.04	6698.6	1	1:23:47	88
2400	50017.9	0.04	6698.7	1	1:24:49	88
2425	49991.7	0.04	6698.2	1	1:25:46	88
2450	50008.4	0.04	6698.0	1	1:26:48	88
2475	50010.5	0.04	6698.1	1	1:27:45	88
2500	50008.7	0.04	6698.1	1	1:28:50	88

Line 14+5	0N	D	ate	29-Jun-96	#139	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT	
-2500	50010	0.04	6698.2	1	1:29:47	88
-2475	50030.5	0.04	6698.8	1	1:30:51	88
-2450	50017	0.04	6698.6	1	1:31:49	88
-2425	50006.5	0.05	6698.4	1	1:32:43	88



-2400	50013.1	0.04	6698.4	1	1:33:40	88
-2375	50027.3	0.04	6698.8	1	1:34:37	88
-2350	50023.6	0.04	6698.9	1	1:35:30	88
-2325	50031	0.05	6698.8	1	1:36:26	88
-2300	50025.2	0.05	6699.2	1	1:37:24	88
-2275	50017	0.04	6699.3	1	1:38:20	88
-2250	50019.8	0.04	6699.1	1	1:39:15	88
-2225	50016.2	0.04	6699.4	1	1:40:10	88
-2200	50017	0.04	6698.8	1	1:41:05	88
-2175	50012.8	0.04	6699.5	1	1:42:00	88
-2150	50015.5	0.04	6699.1	1	1:42:55	88
-2125	50010.8	0.04	6699.4	1	1:43:54	88
-2100	50009.2	0.04	6699.2	1	1:44:48	88
-2075	50014.9	0.04	6699.1	1	1:45:44	88
-2050	50019.8	0.04	6699.0	1	1:46:39	88
-2025	50013.8	0.04	6699.3	1	1:47:33	88
-2000	50004.3	0.05	6699.4	1	1:48:28	88
-1975	49996.5	0.04	6699.2	1	1:49:24	88
-1950	49992.6	0.04	6699.1	1	1:50:15	88
-1925	49994	0.04	6699.3	1	1:51:10	88
-1900	49996.2	0.05	6700.1	1	1:52:03	88
-1875	49989.6	0.04	6700.1	1	1:52:59	88
-1850	49990.1	0.05	6700.0	1	1:53:52	88
-1825	49986	0.04	6700.0	1	1:54:46	88
-1800	49976.9	0.04	6700.1	1	1:55:41	88
Line 14+7	5N D	ate	29-Jun-96			#168
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-1800	50012	0.04	6699.7	1	2:18:58	88
-1825	49985.2	0.06	6699.3	1	2:20:14	88
1850	49991.3	0.04	6699.8	1	2:26:59	88
1875	49979.2	0.04	6699.9	1	2:28:47	88
1900	49974.6	0.04	6699.8	1	2:29:58	88
1925	49977.3	0.04	6699.8	1	2:30:57	88
1950	49989.8	0.04	6700.0	1	2:31:51	88
1975	49996.6	0.04	6700.1	1	2:32:45	88
2000	49992.4	0.08	6699.9	1	2:34:01	88
2025	49988.1	0.04	6699.6	1	2:36:55	88
2050	49999.6	0.07	6699.7	1	2:37:58	88
2075	50001	0.05	6699.3	1	2:38:53	88
2100	50012.2	0.04	6699.5	1	2:39:54	88
2125	49990.7	0.04	6699.7	1	2:40:57	88
2150	50017.3	0.04	6699.3	1	2:41:51	88
2175	49986.5	0.06	6699.4	1	2:42:58	88
2200	50019.3	0.04	6700.0	1	2:43:49	88
2225	50002.4	0.05	6699.7	1	2:44:50	88
2250	50006.6	0.04	6699.8	1	2:45:49	88
2275	50003.4	0.04	6700.3	1	2:46:46	88
2300	50010.2	0.04	6700.3	1	2:47:50	88
2325	50007.5	0.37	6700.3	1	2:48:48	88
2350	50006.3	0.04	6700.8	1	2:49:49	88
2375	49996.9	0.04	6701.0	1	2:50:50	88

## TEU3

2400	50012	0.04	6700.7 1	2:51:48	88
2425	50013.6	0.04	6700.7 1	2:52:45	88
2450	49995.3	0.04	6700.7 1	2:53:43	88
2475	50027.5	0.05	6701.2 1	2:54:38	88
2500	50013.4	0.04	6701.7 1	2:55:42	88
Line 15+0	0N D	ate	29-Jun-96	#203	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2500	50013.6	0.05	6701.7 1	2:56:40	88
-2475	50024.1	0.05	6701.9 1	2:58:02	88
-2450	50026.9	0.05	6702.2 1	2:59:27	88
-2425	50017.9	0.04	6702.4 1	3:00:18	88
-2400	50010.3	0.05	6702.6 1	3:01:15	88
-2375	50017.5	0.04	6701.9 1	3:02:09	88
-2350	50025.1	0.05	6702.3 1	3:03:02	88
-2325	50028.3	0.05	6703.2 1	3:03:58	88
-2300	50011.4	0.04	6703.4 1	3:04:48	88
-2275	50020.9	0.04	6703.1 1	3:05:46	88
-2250	50016	0.06	6703.0 1	3:06:38	88
-2225	50023.2	0.06	6703.6 1	3:07:28	88
-2200	50018.2	0.04	6704.1 1	3:08:22	88
-2175	50038.5	0.13	6703.9 1	3:09:15	88
-2150	50017.8	0.06	6704.3 1	3:10:05	88
-2125	50024.7	0.05	6705.1 1	3:11:00	88
-2100	50032	0.06	6704.4 1	3:11:50	88
-2075	50034.6	0.05	6704.4 1	3:12:42	88
-2050	49987.4	0.04	6705.0 1	3:13:31	88
-2025	50031.8	0.05	6705.5 1	3:14:23	88
-2000	50007.6	0.04	6705.5 1	3:15:12	88
-1975	50003.4	0.04	6705.5 1	3:16:04	88
-1950	50006	0.06	6705.1 1	3:16:54	88
-1925	50027	0.11	6704.9 1	3:17:52	88
-1900	50013.7	0.07	6704.9 1	3:18:39	88
-1875	49983.5	0.04	6705.6 1	3:19:31	88
-1850	50002	0.04	6706.1 1	3:20:25	88
-1825	49976.8	0.05	6706.0 1	3:21:15	88
-1800	50025.8	0.14	6706.0 1	3:22:05	88

Line 15+2	5N D	ate	29-Jun-96	#232	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
1800	49971.6	0.04	6706.3 1	3:23:06	88
1825	49971.3	0.04	6705.9 1	3:24:20	88
1850	49980.6	0.04	6705.6 1	3:25:20	88
1875	49986.2	0.04	6706.2 1	3:26:18	88
1900	50008.9	0.96	6706.7 1	3:27:20	88
1925	49978.7	0.05	6706.0 1	3:28:13	88
1950	49997.5	0.05	6706.5 1	3:29:20	88
1975	49988.3	0.04	6706.8 1	3:30:24	88
2000	49986.9	0.04	6706.4 1	3:31:20	88
2025	50010.6	0.07	6707.0 1	3:32:16	88
2050	50000.7	0.04	6707.1 1	3:33:20	88
2075	50001.7	0.06	6707.3 1	3:34:22	88
2100	50004.1	0.05	6707.9 1	3:35:19	88

2125	50005.4	0.05	6707.6	1	3:36:23	88
2150	49996	0.05	6708.1	1	3:37:16	88
2175	50027.7	0.06	6708.5	1	3:38:19	88
2200	50014.6	0.04	6708.5	1	3:39:10	88
2225	50019.7	0.05	6708.7	1	3:40:09	88
2250	50015.2	0.05	6709.1	1	3:41:58	88
2275	50016.1	0.05	6709.8	1	3:43:02	88
2300	50013.2	0.04	6707.7	1	3:44:13	88
2325	50005.1	0.04	6707.1	1	3:45:16	88
2350	50020.8	0.04	6707.1	1	3:46:14	88
2375	50005.9	0.04	6706.6	1	3:47:29	88
2400	50009.2	0.04	6705.1	1	3:48:22	88
2425	50016.7	0.04	6704.2	1	3:49:23	88
2450	50011.7	0.04	6703.6	1	3:50:19	88
2475	50013.5	0.04	6702.5	1	3:51:22	88
2500	50009	0.04	6701.8	1	3:52:19	88

Line 15+5	ON D	ate	29-Jun-96	#262		
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-2500	50010.4	0.08	6700.9	1	3:53:23	88
-2475	50020.2	0.05	6701.4	1	3:55:33	88
-2450	49996.7	0.05	6701.5	1	3:56:44	88
-2425	50024.4	0.05	6702.4	1	3:57:42	88
-2400	50022.9	0.04	6703.1	1	3:58:33	88
-2375	50022	0.04	6702.6	1	3:59:28	88
-2350	50009.6	0.04	6701.8	1	4:00:23	88
-2325	50025.2	0.05	6701.9	1	4:01:20	88
-2300	50027.8	0.04	6702.1	1	4:02:11	88
-2275	50023	0.04	6703.9	1	4:03:10	88
-2250	50018	0.04	6703.2	1	4:04:00	88
-2225	50035.4	0.05	6705.1	1	4:05:23	88
-2200	50030.2	0.07	6705.5	1	4:06:18	88
-2175	50037.5	0.04	6706.0	1	4:07:16	88
-2150	50037	0.05	6706.6	1	4:08:04	88
-2125	50022.2	0.05	6705.6	1	4:09:02	88
-2100	50010.4	0.05	6706.6	1	4:09:52	88
-2075	50018.9	0.05	6708.3	1	4:10:50	88
-2050	50026.6	0.06	6700.4	1	4:11:36	88
-2025	50029.1	0.05	6703.6	1	4:12:35	88
-2000	50009.9	0.06	6701.1	1	4:13:24	88
-1975	50032.5	0.07	6696.0	1	4:14:22	88
-1950	50016.1	0.05	6711.8	1	4:15:11	88
-1925	50008.4	0.05	6713.6	1	4:16:03	88
-1900	50015.1	0.04	6702.3	1	4:16:57	88
-1875	50031.4	0.04	6682.0	1	4:17:55	88
-1850	49983.3	0.09	6702.7	1	4:18:41	88
-1825	50019.7	0.05	6692.5	1	4:19:34	88
-1800	50014.1	0.04	6693.8	1	4:20:26	88

Line 15+7	5N D	ate	29-Jun-96	#290		
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1800	49981.1	0.04	6716.4	1	4:21:28	88
1825	49982.5	0.04	6714.5	1	4:22:43	88

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1850	50017	0.04	6683.5	1	4:23:45	88
1875	49990.6	0.05	6713.6	1	4:24:56	88
1900	49990.2	0.04	6714.2	1	4:25:51	88
1925	50067.2	0.04	6641.7	1	4:27:00	88
1950	50001.5	0.04	6705.4	1	4:27:52	88
1975	50068.2	0.04	6649.6	1	4:29:01	88
2000	50006.3	0.05	6705.4	1	4:29:51	88
2025	50009.3	0.04	6717.2	1	4:30:49	88
2050	50028.3	0.04	6687.4	1	4:31:52	88
2075	50060	0.04	6662.0	1	4:32:54	88
2100	50028.6	0.04	6693.2	1	4:33:51	88
2125	50044.7	0.04	6696.1	1	4:34:54	88
2150	50017	0.05	6714.0	1	4:35:50	88
2175	50090.3	0.04	6625.3	1	4:36:55	88
2200	50060	0.05	6668.2	1	4:37:44	88
2225	50035.2	0.04	6677.9	1	4:38:43	88
2250	50039.5	0.06	6686.6	1	4:39:40	88
2275	50051	0.04	6677.8	1	4:40:36	88
2300	50055.5	0.59	6668.6	1	4:41:35	88
2325	50032.3	0.06	6689.5	1	4:42:31	88
2350	50009.1	0.04	6711.1	1	4:43:29	88
2375	50008.8	0.04	6715.2	1	4:44:28	88
2400	50020	0.05	6698.5	1	4:45:21	88
2425	50059.2	0.07	6672.9	1	4:46:26	88
2450	50034.4	0.04	6688.8	1	4:47:14	88
2475	50033.3	0.07	6687.5	1	4:48:07	88
2500	50023.7	0.04	6697.1	1	4:49:09	88

Line	16+0	ON	D	ate	29-Jun-96	#319
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-2500	50053.3	0.05	6687.8	1	4:50:31	88
-2475	50093.5	0.04	6646.4	1	4:51:38	88
-2450	50066	0.04	6666.0	1	4:52:33	88
-2425	50058.8	0.05	6682.7	1	4:53:25	88
-2400	50074	0.05	6674.3	1	4:54:17	88
-2375	50011.4	0.04	6719.8	1	4:55:09	88
-2350	50039.1	0.05	6697.2	1	4:56:03	88
-2325	50024.6	0.05	6718.2	1	4:56:55	88
-2300	50034.3	0.05	6719.7	1	4:57:48	88
-2275	50077.4	0.06	6678.2	1	4:58:40	88
-2250	49972.8	0.04	6766.7	1	4:59:33	88
-2225	49972.4	0.06	6775.3	1	5:00:25	88
-2200	50085.3	0.05	6669.0	1	5:01:21	88
-2175	50032.4	0.04	6725.9	1	5:02:16	88
-2150	50017	0.04	6729.5	1	5:03:09	88
-2125	50136.7	0.05	6607.6	1	5:04:01	88
-2100	50100.8	0.04	6642.6	1	5:04:54	88
-2075	49938	0.05	6815.8	1	5:05:45	88
-2050	49892.7	0.04	6853.6	1	5:06:39	88
-2025	50021.9	0.05	6742.3	1	5:07:26	88
-2000	50109	0.04	6629.0	1	5:08:24	88
-1975	50101.3	0.04	6648.0	1	5:09:15	88

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-1950	50092.1	0.04	6622.5	1	5:10:08	88
-1925	50219.3	0.05	6510.8	1	5:11:02	88
-1900	50230.4	0.05	6485.0	1	5:11:53	88
-1875	50179.7	0.05	6534.8	1	5:12:41	88
-1850	50145	0.05	6559.5	1	5:13:35	88
-1825	50162.5	0.04	6560.1	1	5:14:28	88
-1800	50143	0.05	6556.8	1	5:15:18	88

Line 16+2	5N	D	ate	29-Jun-96	#348	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1800	50202.4	0.08	6488.3	1	5:16:17	88
1825	50216.4	0.05	6478.3	1	5:17:25	88
1850	50249.7	0.03	6456.3	1	5:18:25	88
1875	50494.8	0.05	6210.9	1	5:19:17	88
1900	50313.8	0.05	6404.3	1	5:20:23	88
1925	50374.9	0.04	6349.0	1	5:21:22	88
1950	50224.2	0.04	6493.9	1	5:22:21	88
1975	50172.1	0.05	6543.1	1	5:23:29	88
2000	50189	0.05	6540.4	1	5:24:29	88
2025	50212.4	0.04	6511.1	1	5:25:22	88
2050	50402.8	0.05	6323.2	1	5:26:25	88
2075	50501.8	0.04	6228.5	1	5:27:18	88
2100	50287	0.05	6458.0	1	5:28:22	88
2125	50156.9	0.06	6585.1	1	5:29:17	88
2150	50244.4	0.05	6487.3	1	5:30:17	88
2175	50535.8	0.04	6194.7	1	5:31:15	88
2200	50458.2	0.04	6286.0	1	5:32:15	88
2225	50498.8	0.04	6234.2	1	5:33:09	88
2250	50247.7	0.04	6481.8	1	5:34:09	88
2275	50631.8	0.06	6093.5	1	5:35:04	88
2300	50205.8	0.07	6532.7	1	5:36:07	88
2325	50300.3	0.04	6427.6	1	5:37:07	88
2350	50645.9	0.05	6082.4	1	5:38:03	88
2375	50282.9	0.04	6438.0	1	5:38:58	88
2400	50269.2	0.04	6453.2	1	5:40:01	88
2425	50283.7	0.12	6457.3	1	5:40:58	88
2450	50165.5	0.04	6562.6	1	5:41:57	88
2475	50216.3	0.04	6508.2	1	5:42:50	88
2500	50055.6	0.05	6676.0	1	5:43:51	88

Line 16+5	0N	D	ate	29-Jun-96	#377	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-2500	50188.8	0.05	6549.2	1	5:44:55	88
-2475	50473.9	0.04	6272.5	1	5:46:02	88
-2450	50253.8	0.09	6486.9	1	5:46:56	88
-2425	50413.5	0.05	6335.3	1	5:47:46	88
-2400	50315.3	0.04	6432.4	1	5:48:40	88
-2375	50216.9	0.04	6533.4	1	5:49:33	88
-2350	50185.7	0.05	6557.5	1	5:50:26	88
-2325	50186.8	0.04	6561.2	1	5:51:19	88
-2300	50214.8	0.04	6532.8	1	5:52:12	88
-2275	50362.6	0.05	6397.5	1	5:53:13	88
-2250	50317.4	0.05	6424.2	1	5:53:57	88

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-2225	50602.4	0.05	6160.6	1	5:54:48	88
-2200	50582.1	0.04	6163.3	1	5:55:41	88
-2175	50539.8	0.04	6216.4	1	5:56:32	88
-2150	50418.5	0.05	6340.9	1	5:57:24	88
-2125	50342.2	0.05	6431.1	1	5:58:14	88
-2100	50532.3	0.06	6229.4	1	5:59:06	88
-2075	50239.7	0.05	6534.4	1	5:59:56	88
-2050	50489.7	0.04	6283.9	1	6:00:47	88
-2025	50717.6	0.04	6049.2	1	6:01:37	88
-2000	50771	0.05	5969.3	1	6:02:27	88
-1975	50378.9	0.07	6373.7	1	6:08:42	88
-1950	50415.4	0.05	6340.1	1	6:09:30	88
-1925	50399	0.04	6360.9	1	6:10:22	88
-1900	50201.2	0.04	6540.3	1	6:11:12	88
-1875	50065	0.04	6688.1	1	6:12:07	88
-1850	50286.3	0.09	6467.1	1	6:12:54	88
-1825	50429.3	0.04	6308.0	1	6:13:45	88
-1800	50448.1	0.17	6263.0	1	6:14:41	88

Line 16+7	5N D	ate	29-Jun-96	#406
POSITIO	FIELD	ERR	DRIFT	TIME DS CULT
1800	50401.1	0.04	6310.6	1 6:15:38 88
1825	50356.6	0.04	6357.0	1 6:17:06 88
1850	49858.6	0.04	6857.9	1 6:18:02 88
1875	50334.5	0.04	6396.3	1 6:18:57 88
1900	49923.1	0.05	6819.9	1 6:20:04 88
1925	49417.7	0.1	7317.4	1 6:20:59 88
1950	48556.1	0.05	8188.6	1 6:21:56 88
1975	49629.8	0.04	7113.9	1 6:22:49 88
2000	50725.4	0.04	6023.5	1 6:23:48 88

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## TEU4

Line 16+7	5N	D	ate	1-Jul-09	6 #1
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
2000	50022.2	0.03	6734.8	10:46:34	88
2025	50007.4	0.03	6734.4	10:48:01	88
2050	50010	0.05	6734.1	10:49:02	88
2075	50014.9	0.04	6734.1	10:50:07	88
2100	50020.7	0.03	6733.9	10:51:08	88
2125	50019.5	0.04	6734	10:52:05	88
2150	50021	0.04	6733.8	10:53:07	88
2175	50016	0.05	6733.9	10:54:03	88
2200	50010	0.03	6734	10:55:07	88
2225	50006.3	0.03	6734.1	10:56:06	88
2250	50004.8	0.03	6734	10:57:08	88
2275	50003.1	0.04	6733.9	10:58:08	88
2300	49997.4	0.04	6733.8	10:59:09	88
2325	49992.8	0.04	6733.7	11:00:08	88
2350	50000.1	0.04	6733.8	11:01:10	88
2375	50002.2	0.04	6733.4	11:02:09	88
2400	49994.1	0.05	6733.2	11:03:07	88
2425	49990.6	0.05	6732.7	11:04:21	88
2450	50005.5	0.03	6732.3	11:05:21	88
2475	49998.8	0.03	6732.5	11:06:19	88
2500	49997.6	0.09	6732.1	11:07:18	88

Line 17+0	0N	D	ate	1-Jul-09	6 #22
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2500	50002	0.04	6731.9	11:08:24	88
-2475	50022.2	0.03	6731.8	11:09:37	88
-2450	49993.6	0.13	6731.5	11:10:33	88
-2425	50015.4	0.04	6731.5	11:11:30	88
-2400	50023.8	0.04	6731.6	11:12:34	88
-2375	49999.7	0.03	6731.6	11:13:30	88
-2350	50026.7	1	6731.8	11:14:23	88
-2325	50004.2	0.04	6731.7	11:15:18	88
-2300	50009.3	0.04	6731.5	11:16:16	88
-2275	50007.7	0.03	6731.8	11:17:14	88
-2250	50013.9	0.03	6731.7	11:18:06	88
-2225	50019	0.04	6731.5	11:19:03	88
-2200	50024.1	0.11	6731.4	11:19:57	88
-2175	50029.6	0.03	6731.1	11:20:58	88
-2150	50020.3	0.05	6730.7	11:21:50	88
-2125	50028.7	0.03	6730.1	11:22:47	88
-2100	50042.8	0.04	6730.1	11:23:39	88
-2075	50032.6	0.03	6729.6	11:27:12	88
-2050	50018.8	0.04	6729.3	11:28:11	88
-2025	50023.9	0.04	6729.1	11:29:10	88
-2000	50033.7	0.05	6729.5	11:30:03	88
-1975	50044.3	0.04	6729.5	11:31:01	88
-1950	50006.9	0.04	6729.5	11:32:00	88
-1925	50005	0.04	6729.7	11:33:02	88
-1900	49998.6	0.05	6729.9	11:33:58	88
-1875	49996.1	0.04	6730.2	11:35:56	88

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-1850	50002.1	0.04	6730.2	11:36:51	88
-1825	49990.5	0.03	6729.8	11:38:54	88
-1800	49943.9	0.05	6729.4	11:40:00	88
-1775	49974.2	0.03	6729	11:41:02	88
-1750	49960.8	0.04	6728.4	11:42:12	88
-1725	49900.7	0.03	6728	11:43:14	88
-1700	49880	0.05	6727.7	11:44:19	88
Line 17+2	5N D	ate	1-Jul-09	6 #56	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
1700	49875.3	0.04	6725.8	11:54:01	88
1725	49886.9	0.04	6718.3	12:24:55	88
1750	49914.7	0.03	6718.2	12:25:53	88
1775	49931.8	0.04	6717.6	12:26:47	88
1800	49972.9	0.04	6717	12:28:03	88
1825	49962.2	0.05	6717.3	12:29:01	88
1850	49990	0.11	6717.6	12:30:01	88
1875	49975	0.03	6717.8	12:30:59	88
1900	49997.8	0.03	6718.1	12:32:00	88
1925	49988.3	0.04	6718.6	12:32:57	88
1950	50009.4	0.04	6718.5	12:33:57	88
1975	50009.4	0.04	6719.2	12:34:54	88
2000	50008.3	0.04	6719.5	12:35:55	88
2025	50008.3	0.04	6720	12:36:52	88
2050	50017.1	0.04	6719.7	12:37:53	88
2075	50009.2	0.04	6719.7	12:38:59	88
2100	50013.5	0.11	6719.9	12:39:54	88
2125	50020	0.03	6720.4	12:41:04	88
2150	50016	0.04	6720.6	12:42:05	88
2175	50007.8	0.04	6720.6	12:43:07	88
2200	50003.4	0.03	6720.8	12:44:05	88
2225	50000.2	0.05	6721	12:45:03	88
2250	49993.4	0.04	6720.9	12:46:06	88
2275	49989.7	0.04	6720.8	12:47:07	88
2300	49984.1	0.04	6721.3	12:48:27	88
2325	49986.8	0.03	6721.3	12:49:22	88
2350	49979.2	0.1	6721.5	12:50:30	88
2375	49986.9	0.03	6721.4	12:51:23	88
2400	49982.3	0.06	6721.6	12:52:42	88
2425	49981.6	0.07	6721.7	12:53:34	88
2450	49973.4	0.04	6722.1	12:55:20	88
2475	49989.7	0.03	6721.9	12:56:13	88
2500	49996.8	0.04	6722.2	12:57:14	88
Line 17+5	0N D	ate	1-Jul-09	6 #89	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2500	50008.9	0.05	6722.1	12:58:25	88
-2475	50010.6	0.04	6722.2	12:59:37	88
-2450	49992.4	0.06	6722.6	13:00:35	88
-2425	49998	0.03	6722.6	13:01:36	88
-2400	49998.5	0.18	6722.5	13:02:32	88
-2375	49988.4	0.04	6722.7	13:03:26	88
-2350	49993.9	0.04	6723	13:04:24	88



## TEU4

-2325	50004.3	0.04	6723.4	13:05:30	88
-2300	50002.1	0.04	6723.2	13:06:22	88
-2275	50002	0.04	6723.4	13:07:14	88
-2250	49997.7	0.03	6723.8	13:08:08	88
-2225	49998.2	0.04	6723.9	13:09:02	88
-2200	50016.3	0.04	6724.1	13:09:55	88
-2175	50013.8	0.03	6724.6	13:10:51	88
-2150	49998.8	0.04	6724.7	13:11:45	88
-2125	50024	0.03	6725.1	13:12:39	88
-2100	50026.8	0.03	6725.4	13:13:31	88
-2075	50030.7	0.03	6725.9	13:14:42	88
-2050	50024.5	0.09	6726.2	13:15:35	88
-2025	50023.3	0.04	6726.1	13:16:30	88
-2000	50022.8	0.09	6726.2	13:17:21	88
-1975	50030.9	0.04	6726.9	13:18:13	88
-1950	50021.6	0.03	6726.7	13:19:34	88
-1925	50017.2	0.03	6728.1	13:23:02	88
-1900	49993.7	0.11	6727.8	13:23:58	88
-1875	49994.5	0.04	6728.2	13:25:05	88
-1850	49946.4	0.1	6727.9	13:25:58	88
-1825	49959.8	0.04	6728.7	13:27:24	88
-1800	49962	0.03	6728.9	13:28:30	88
-1775	49936.6	0.04	6729.2	13:29:29	88
-1750	49934.7	0.29	6730.3	13:30:40	88
-1725	49932.7	0.38	6730.4	13:32:32	88
-1700	49839.5	0.05	6735.4	13:39:31	88
Line 17+7	5N D	ate	1-Jul-09	6 #122	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
1700	49837.6	0.04	6736.2	13:55:06	88
1725	49849.2	0.04	6738.1	13:59:55	88
1750	49859.9	0.04	6741.1	14:04:16	88
1775	49899.2	0.06	6741.3	14:06:12	88
1800	49916.4	0.04	6739	14:17:06	88
1825	49916.1	0.04	6739.4	14:17:58	88
1850	49916.7	0.03	6739.9	14:18:40	88
1875	49939	0.04	6740.2	14:19:34	88
1900	49986.5	0.04	6741.8	14:22:28	88
1925	49985.1	0.05	6742.8	14:23:28	88
1950	49986	0.05	6743.1	14:24:32	88
1975	50018	0.04	6742.8	14:25:40	88
2000	50030.3	0.04	6743.6	14:27:13	88
2025	50020.7	0.03	6743	14:28:14	88
2050	50005.2	0.04	6743.2	14:29:18	88
2075	50009.8	0.03	6742.6	14:30:14	88
2100	50009.6	0.03	6743.2	14:31:23	88
2125	50015.7	0.04	6741.7	14:32:52	88
2150	50007.9	0.04	6741.4	14:33:55	88
2175	50005.4	0.04	6741.3	14:35:54	88
2200	49998.8	0.04	6741.2	14:37:29	88
2225	50000.4	0.04	6741.6	14:38:34	88
2250	49981.4	0.03	6741.7	14:39:53	88

## TEU4

2275	49988.7	0.04	6742	14:41:02	88
2300	49973.2	0.04	6741.5	14:42:04	88
2325	49976	0.03	6741.7	14:43:03	88
2350	49974.1	0.03	6741.8	14:44:04	88
2375	49977.6	0.03	6742.5	14:45:03	88
2400	49980.4	0.07	6741.9	14:46:06	88
2425	49976.9	0.03	6742.4	14:47:04	88
2450	49982.3	0.03	6743.2	14:49:09	88
2475	49978.9	0.03	6744	14:50:06	88
2500	49984.8	0.08	6744.5	14:51:05	88

Line 18+0	ON D	ate	1-Jul-09	6 #155	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2500	49982.3	0.07	6744.5	14:52:23	88
-2475	49992.5	0.04	6745.2	14:53:28	88
-2450	49998.2	0.04	6745.8	14:54:24	88
-2425	49987.4	0.05	6746	14:55:28	88
-2400	49979.4	0.04	6746.4	14:56:50	88
-2375	49980.5	0.04	6746.2	14:57:48	88
-2350	49985.3	0.03	6745.6	14:59:44	88
-2325	49989.3	0.04	6745.5	15:00:35	88
-2300	49979.2	0.04	6745.2	15:01:38	88
-2275	49977.2	0.03	6745	15:02:30	88
-2250	49987.5	0.04	6745.3	15:03:40	88
-2225	49993.6	0.03	6745.2	15:04:41	88
-2200	50005.3	0.03	6745.1	15:05:43	88
-2175	50000	0.03	6745.3	15:06:59	88
-2150	50009.5	0.07	6745.5	15:07:58	88
-2125	50020.4	0.05	6745.7	15:08:56	88
-2100	50021.1	0.03	6746.2	15:10:49	88
-2075	50023.4	0.04	6746.2	15:11:41	88
-2050	50012.9	0.03	6745.6	15:12:40	88
-2025	50030.2	0.03	6745.4	15:13:33	88
-2000	50036.8	0.04	6745.6	15:18:38	88

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TEU5

Line 18+0 ON D		ate	3-Jul-96		#8
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2000	50082.4	0.07	6730.6	8:48:02	88
-1975	49977.8	0.05	6731.3	8:49:15	88
-1950	49960	0.04	6731.8	8:50:18	88
-1925	50141	0.04	6732.5	8:53:13	88
-1900	50043.3	0.05	6732.7	8:54:20	88
-1875	50007.5	0.05	6732.9	8:55:21	88
-1850	49979.3	0.04	6733.1	8:56:13	88
-1825	49962.4	0.04	6733.5	8:57:13	88
-1800	49925.5	0.04	6733.8	8:58:13	88
-1775	49889.6	0.04	6733.9	8:59:28	88
-1750	49879.5	0.04	6734.5	9:01:53	88
-1725	49880.1	0.04	6735.6	9:05:45	88
-1700	49844.8	0.04	6736	9:08:32	88

Line 18+2 5N D		ate	3-Jul-96		#21
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
1700	49813	0.04	6736.7	9:13:15	88
1725	49847.6	0.04	6737.3	9:16:41	88
1750	49859.3	0.04	6737.9	9:18:58	88
1775	49887.6	0.04	6738.4	9:23:16	88
1800	49912.9	0.05	6738.7	9:25:10	88
1825	49927.5	0.04	6738.7	9:28:02	88
1850	49967.4	0.05	6738.7	9:29:10	88
1875	49976.3	0.04	6738.6	9:30:19	88
1900	50062.7	0.04	6738.5	9:31:57	88
1925	50179.9	0.04	6738.1	9:36:45	88
1950	50003.2	0.06	6737.8	9:38:27	88
1975	49989.8	0.05	6737.4	9:40:21	88
2000	50033.4	0.07	6737.4	9:42:08	88
2025	50034.6	0.05	6737.4	9:43:32	88
2050	50080.5	0.08	6737.3	9:44:32	88
2075	50016.6	0.04	6737.3	9:47:12	88
2100	50010.3	0.04	6737	9:48:22	88
2125	50002.8	0.04	6736.9	9:49:28	88
2150	50005.7	0.04	6736.6	9:50:35	88
2175	49998.3	0.04	6736.4	9:51:49	88
2200	49990.4	0.04	6736	9:52:58	88
2225	50001.6	0.04	6735.8	9:53:53	88
2250	49980	0.05	6735.6	9:55:00	88
2275	49995	0.04	6735.6	9:55:56	88
2300	49986.8	0.04	6735.5	9:57:03	88
2325	49973.6	0.05	6735.5	9:58:00	88
2350	49973.2	0.04	6735.5	9:59:50	88
2375	49972.3	0.04	6735.4 1	0:00:53	88
2400	49981.6	0.04	6735.5 1	0:01:59	88
2425	49980.2	0.09	6735.6 1	0:02:57	88
2450	49983	0.04	6735.7 1	0:03:59	88
2475	49989.1	0.04	6735.8 1	0:04:57	88
2500	49984.6	0.04	6736.0 1	0:06:01	88

Line 18+5 ON D ate 3-Jul-96 #54

## TEU5

POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-2500	50012.6	0.04	6735.9 1	0:06:59	88	
-2475	50008.4	0.04	6735.4 1	0:08:05	88	
-2450	50018.2	0.04	6735.2 1	0:09:06	88	
-2425	49998.7	0.07	6735.2 1	0:10:15	88	
-2400	49980.9	0.08	6735.4 1	0:11:07	88	
-2375	50001.7	0.04	6735.6 1	0:12:09	88	
-2350	49988.7	0.04	6735.6 1	0:13:08	88	
-2325	50002.1	0.04	6735.5 1	0:15:04	88	
-2300	49990.4	0.05	6735.2 1	0:15:56	88	
-2275	49982.8	0.04	6735.1 1	0:16:51	88	
-2250	49993.3	0.04	6735.0 1	0:17:52	88	
-2225	50002.2	0.04	6735.0 1	0:18:44	88	
-2200	50005.9	0.04	6734.7 1	0:19:39	88	
-2175	50007.3	0.05	6734.3 1	0:20:40	88	
-2150	50014.1	0.04	6734.1 1	0:21:35	88	
-2125	50021.6	0.04	6734.1 1	0:22:28	88	
-2100	50002	0.07	6733.9 1	0:23:26	88	
-2075	50020.3	0.04	6734.2 1	0:25:32	88	
-2050	50025.8	0.03	6734.4 1	0:27:24	88	
-2025	50012.6	0.04	6734.3 1	0:28:40	88	
-2000	49962.1	0.12	6734.2 1	0:29:54	88	TRENCH-84
-1825	49934.8	0.04	6733.1 1	0:46:36	88	
-1800	49895.5	0.04	6732.6 1	0:47:43	88	
Line 18+7 5N D ate 3-Jul-96 #79						
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1800	49908	0.04	6732.0 1	0:53:05	88	
1825	49902.9	0.04	6733.2 1	0:56:29	88	
1850	49943.1	0.04	6733.3 1	0:57:49	88	
1875	49978.7	0.04	6733.6 1	0:59:44	88	
1900	50086.5	0.04	6730.9 1	1:13:38	88	
1925	50012.8	0.05	6731.0 1	1:15:22	88	
1950	49970.6	0.04	6730.7 1	1:17:11	88	
1975	50149.9	0.06	6730.5 1	1:18:55	88	
2000	49903.5	0.07	6730.2 1	1:19:54	88	DDH96 #1 SITE
2025	49983	0.04	6729.0 1	1:23:05	88	
2050	50003.7	0.04	6729.7 1	1:25:15	88	
2075	50031	0.03	6729.9 1	1:26:22	88	
2100	49996.6	0.05	6729.7 1	1:27:40	88	
2125	49986.4	0.03	6729.1 1	1:29:11	88	
2150	49983.9	0.04	6728.6 1	1:30:13	88	
2175	49986.3	0.03	6728.4 1	1:31:12	88	
2200	49974.8	0.04	6728.7 1	1:32:15	88	
2225	49972.2	0.04	6728.8 1	1:33:18	88	
2250	49972.3	0.04	6728.8 1	1:34:25	88	
2275	49970.4	0.04	6728.8 1	1:35:22	88	
2300	49988.7	0.03	6728.5 1	1:36:29	88	
2325	49975.8	0.04	6728.0 1	1:37:25	88	
2350	49972.9	0.04	6727.7 1	1:38:30	88	
2375	49977.2	0.04	6727.6 1	1:39:26	88	
2400	49993	0.06	6727.4 1	1:40:30	88	

TEU5

	2425	49980.4	0.04	6727.3	1	1:41:28	88
	2450	49981.9	0.04	6726.9	1	1:42:31	88
	2475	49979.6	0.05	6726.8	1	1:43:31	88
	2500	49983.8	0.04	6726.9	1	1:44:33	88
Line 19+0	ON	D	ate	3-Jul-96		#108	
	POSITIO	FIELD	ERR	DRIFT		TIME	DS CULT
	-2500	49983.9	0.04	6727.2	1	1:45:36	88
	-2475	49988.2	0.05	6727.6	1	1:46:50	88
	-2450	49989.5	0.03	6728.1	1	1:47:50	88
	-2425	49999.8	0.19	6728.3	1	1:48:48	88
	-2400	49987.2	0.09	6728.2	1	1:49:45	88
	-2375	49983.2	0.04	6728.0	1	1:50:44	88
	-2350	49992.1	0.03	6727.8	1	1:51:43	88
	-2325	49989.4	0.03	6727.7	1	1:52:38	88
	-2300	49993.5	0.03	6727.7	1	1:53:34	88
	-2275	49992	0.03	6727.9	1	1:54:31	88
	-2250	49997.4	0.04	6728.0	1	1:55:28	88
	-2225	49995.3	0.04	6728.1	1	1:56:24	88
	-2200	49997.2	0.04	6728.1	1	1:57:20	88
	-2175	50007.5	0.05	6728.1	1	1:58:16	88
	-2150	50003.9	0.04	6728.1	1	1:59:14	88
	-2125	50002.6	0.36	6728.0	1	2:00:14	88
	-2100	49993.2	0.03	6728.0	1	2:01:42	88
	-2075	50021	0.04	6728.2	1	2:06:01	88
	-2050	50010.1	0.04	6728.4	1	2:07:22	88
	-2025	49985.5	0.05	6729.0	1	2:08:40	88
	-2000	49827.6	0.05	6728.8	1	2:10:52	88
	-1975	51542	0.3	6728.3	1	2:13:47	88
	-1950	50007.8	0.06	6729.0	1	2:19:41	88
	-1925	50006.9	0.04	6728.5	1	2:29:12	88
	-1900	50037.6	0.08	6727.4	1	2:31:41	88
Line 19+2	5N	D	ate	3-Jul-96		#133	
	POSITIO	FIELD	ERR	DRIFT		TIME	DS CULT
	1900	49960.3	0.04	6725.8	1	2:42:23	88
	1925	49982.7	0.04	6726.4	1	2:44:24	88
	1950	50048.2	0.04	6726.6	1	2:45:43	88
	1975	50786.9	0.05	6726.5	1	2:47:19	88 TRENCH 49
	2000	49963.7	0.05	6726.4	1	2:50:52	88 DDH96 #2 SITE
	2025	49929.8	0.04	6727.1	1	2:53:28	88
	2050	49985.3	0.04	6727.7	1	2:55:52	88
	2075	50002	0.04	6727.2	1	2:58:49	88
	2100	50009.1	0.04	6726.9	1	3:00:00	88
	2125	50014.4	0.03	6727.1	1	3:04:44	88
	2150	50008	0.04	6727.4	1	3:05:36	88
	2175	49985.4	0.04	6727.5	1	3:07:04	88
	2200	49988.9	0.03	6727.5	1	3:08:01	88
	2225	49983.9	0.04	6727.5	1	3:08:58	88
	2250	49981.9	0.03	6727.8	1	3:09:54	88
	2275	49967.7	0.04	6727.8	1	3:10:50	88
	2300	49975.4	0.04	6727.7	1	3:11:49	88
	2325	49984.7	0.04	6727.7	1	3:12:46	88

## TEU5

2350	49971.9	0.04	6727.3	1	3:13:55	88
2375	49981.1	0.03	6727.4	1	3:14:52	88
2400	49968.4	0.04	6727.5	1	3:15:50	88
2425	49980.3	0.04	6727.5	1	3:16:46	88
2450	49974.3	0.04	6727.2	1	3:17:47	88
2475	49985.4	0.04	6727.1	1	3:18:42	88
2500	49979.4	0.03	6727.2	1	3:19:43	88
Line 19+5	0N D	ate	3-Jul-96			#158
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-2500	49985.7	0.04	6727.1	1	3:20:48	88
-2475	49980.5	0.04	6727.1	1	3:22:13	88
-2450	49986.8	0.04	6727.1	1	3:23:14	88
-2425	49987	0.04	6726.8	1	3:24:10	88
-2400	49995.2	0.04	6726.5	1	3:25:08	88
-2375	49992.2	0.04	6726.1	1	3:26:04	88
-2350	49984	0.04	6725.9	1	3:27:02	88
-2325	49982.5	0.04	6726.2	1	3:28:00	88
-2300	49994.4	0.04	6726.3	1	3:28:58	88
-2275	49989.3	0.04	6726.3	1	3:29:54	88
-2250	49990.5	0.04	6726.3	1	3:30:57	88
-2225	50002.5	0.05	6726.0	1	3:31:55	88
-2200	49988.9	0.03	6725.5	1	3:32:55	88
-2175	49989.2	0.04	6725.4	1	3:33:56	88
-2150	50036.9	0.03	6724.9	1	3:34:56	88
-2125	50014.4	0.04	6724.3	1	3:36:01	88
-2100	50044.1	0.04	6725.7	1	3:39:50	88
-2075	50026.1	0.04	6724.3	1	3:47:31	88
-2050	50020.9	0.04	6722.8	1	3:52:35	88
-2025	49970.6	0.57	6724.1	1	3:54:44	88
-2000	49999.6	0.03	6724.3	1	3:56:16	88 TRENCH-43?
-1975	50180.9	0.04	6723.0	1	4:02:30	88
-1950	50010.4	0.05	6722.9	1	4:05:05	88
-1925	50009.4	0.04	6723.0	1	4:06:36	88
-1900	49997.7	0.03	6723.4	1	4:08:42	88
Line 19+7	5N D	ate	3-Jul-96			#184
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1900	49983.6	0.04	6726.0	1	4:12:26	88
1925	49996.9	0.04	6726.2	1	4:15:32	88
1950	50035.1	0.04	6725.9	1	4:16:38	88
1975	50345.7	0.03	6725.9	1	4:18:04	88
2000	50009.6	0.05	6726.4	1	4:19:16	88
2025	49954	0.04	6727.0	1	4:23:39	88
2050	49999.3	0.05	6727.3	1	4:24:32	88
2075	50023.4	0.04	6727.1	1	4:25:28	88
2100	50040.4	0.06	6726.9	1	4:27:09	88
2125	50024.7	0.05	6727.6	1	4:28:41	88
2150	49986.5	0.06	6727.9	1	4:29:44	88
2175	49984.2	0.04	6727.7	1	4:30:35	88
2200	49983.4	0.04	6727.4	1	4:31:27	88
2225	49980	0.04	6727.6	1	4:32:22	88
2250	49983.9	0.04	6727.6	1	4:33:22	88

TEU5

2275	49978.2	0.04	6727.5	1	4:34:17	88
2300	49974.2	0.03	6727.6	1	4:35:14	88
2325	49985.4	0.04	6727.2	1	4:36:11	88
2350	49973.7	0.04	6727.6	1	4:37:10	88
2375	49978.7	0.03	6727.1	1	4:38:04	88
2400	49993.1	0.04	6726.9	1	4:39:00	88
2425	49987.6	0.04	6726.8	1	4:39:54	88
2450	49977.5	0.04	6726.0	1	4:40:51	88
2475	49980.8	0.04	6725.6	1	4:41:45	88
2500	49978.9	0.04	6725.0	1	4:42:44	88

Line	20+0	ON	D	ate	3-Jul-96	#209
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-2500	49999.2	0.04	6725.0	1	4:43:41	88
-2475	49992.8	0.04	6726.7	1	4:45:22	88
-2450	49980.7	0.04	6728.3	1	4:46:32	88
-2425	50001.7	0.04	6729.2	1	4:47:31	88
-2400	49995.7	0.05	6729.8	1	4:48:31	88
-2375	49988.3	0.04	6730.2	1	4:49:32	88
-2350	49987.1	0.03	6730.1	1	4:50:30	88
-2325	49983.2	0.04	6729.8	1	4:51:29	88
-2300	49992.1	0.03	6729.7	1	4:52:32	88
-2275	49992.9	0.03	6729.7	1	4:53:34	88
-2250	49990.7	0.03	6729.7	1	4:54:34	88
-2225	50014.5	0.04	6729.4	1	4:55:37	88
-2200	49987.9	0.04	6729.3	1	4:56:38	88
-2175	49989.2	0.04	6729.8	1	4:57:48	88
-2150	50036.1	0.04	6730.3	1	4:59:04	88
-2125	50053.9	0.04	6730.4	1	5:00:45	88
-2100	50095.6	0.04	6729.5	1	5:05:12	88
-2075	50021.1	0.04	6730.6	1	5:11:22	88
-2050	50033.2	0.06	6730.4	1	5:13:45	88
-2025	49981.5	0.03	6730.2	1	5:17:27	88
-2000	50055	0.05	6730.1	1	5:18:36	88
-1975	50208.6	0.04	6730.6	1	5:19:58	88
-1950	50050.9	0.04	6731.3	1	5:20:55	88
-1925	50033.9	0.03	6731.5	1	5:21:55	88
-1900	50017.5	0.04	6731.3	1	5:22:57	88

Line	20+2	5N	D	ate	3-Jul-96	#234
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1900	50009.5	0.04	6731.7	1	5:29:11	88
1925	50024.9	0.04	6732.6	1	5:30:46	88
1950	50147.7	0.04	6732.7	1	5:32:24	88
1975	49913.5	0.05	6732.8	1	5:33:40	88 DDH96 #3 SITE & DRILL
2000	49991.8	0.04	6736.0	1	5:52:40	88

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## TEU6

Line 16+0	ON D	ate	6-Jul-96	#1
POSITIO	FIELD	ERR	DRIFT	TIME DS CULT
1700	49959.2	0.04	6723.9	8:55:12 88
1725	49975	0.04	6724.3	8:57:01 88
1750	49976.9	0.04	6724.7	8:57:49 88
1775	49993.4	0.04	6724.8	8:58:35 88
1800	49981.4	0.04	6724.9	8:59:26 88
1825	49990.9	0.04	6725.1	9:00:18 88
1850	49991.1	0.06	6725.2	9:01:18 88
1875	49998	0.04	6725.4	9:02:12 88
1900	49999.8	0.04	6725.5	9:03:09 88
1925	49998.2	0.04	6725.5	9:04:03 88
1950	50001.7	0.04	6725.9	9:05:03 88
1975	50007.8	0.04	6725.8	9:06:02 88
2000	50010.5	0.04	6725.8	9:06:55 88
2025	50022.1	0.04	6726	9:07:48 88
2050	50022.9	0.04	6726.2	9:08:50 88
2075	50024.6	0.04	6726.3	9:09:40 88
2100	50026.9	0.04	6726.5	9:10:43 88
2125	50017	0.04	6726.6	9:11:42 88
2150	50029.5	0.04	6726.8	9:12:36 88
2175	50027.2	0.03	6727	9:13:28 88
2200	50024.6	0.04	6726.9	9:14:27 88
2225	50013.7	0.04	6727	9:15:18 88
2250	50024.7	0.04	6727.5	9:16:17 88
2275	50006.7	0.04	6727.8	9:17:10 88
2300	50015.8	0.04	6727.8	9:18:07 88
2325	50010.9	0.04	6727.7	9:18:59 88
2350	50016.8	0.04	6727.9	9:19:58 88
2375	50013.1	0.04	6727.9	9:20:47 88
2400	50025.9	0.03	6728.1	9:21:46 88
2425	50008.8	0.03	6728.2	9:22:36 88
2450	50013.5	0.05	6728.2	9:23:35 88
2475	50018.1	0.03	6728.2	9:24:25 88
2500	50027.9	0.03	6728.1	9:25:28 88

Line 16+2	5N D	ate	6-Jul-96	#34
POSITIO	FIELD	ERR	DRIFT	TIME DS CULT
-2500	50019.8	0.04	6728.2	9:29:20 88
-2475	50021.1	0.03	6728.3	9:30:41 88
-2450	50017.2	0.04	6728.4	9:31:28 88
-2425	50030.5	0.04	6728.3	9:32:16 88
-2400	50020.9	0.04	6728.1	9:33:05 88
-2375	50026.7	0.04	6728	9:33:53 88
-2350	50021.6	0.03	6728	9:34:42 88
-2325	50021.2	0.04	6727.9	9:35:32 88
-2300	50030	0.04	6727.7	9:36:20 88
-2275	50022.4	0.04	6727.6	9:37:08 88
-2250	50026.4	0.03	6727.6	9:37:56 88
-2225	50030.8	0.04	6727.7	9:38:45 88
-2200	50032.6	0.03	6727.5	9:39:35 88
-2175	50032.4	0.03	6727.5	9:40:23 88



## TEU6

-2150	50042.2	0.04	6727.7	9:41:11	88
-2125	50035.2	0.03	6727.8	9:41:57	88
-2100	50032.6	0.03	6727.9	9:42:41	88
-2075	50032.5	0.04	6727.7	9:43:29	88
-2050	50034.7	0.04	6727.3	9:44:15	88
-2025	50033.3	0.03	6727.2	9:45:01	88
-2000	50025.9	0.04	6727.6	9:45:51	88
-1975	50020.6	0.04	6727.4	9:47:05	88
-1950	50016.6	0.05	6727.4	9:47:55	88
-1925	50021	0.04	6727.3	9:48:44	88
-1900	50016.8	0.04	6727.3	9:49:30	88
-1875	50005.4	0.03	6727.4	9:50:18	88
-1850	49980.2	0.08	6727.2	9:51:12	88
-1825	50006.4	0.04	6727.4	9:51:58	88
-1800	49967.6	0.04	6727.2	9:52:48	88
-1775	49985	0.03	6727.4	9:53:40	88
-1750	49984.4	0.04	6727.6	9:54:30	88
-1725	49974.9	0.04	6727.7	9:55:16	88
-1700	49968.4	0.04	6727.8	9:56:09	88
Line 16+5	0N D	ate	6-Jul-96	#67	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
1700	49947.2	0.04	6727.5	9:57:49	88
1725	49949.2	0.04	6727.5	9:58:59	88
1750	49962.4	0.04	6727.1	9:59:46	88
1775	49970.2	0.04	6727.0 1	0:00:32	88
1800	49985.2	0.04	6726.8 1	0:02:03	88
1825	49995	0.03	6726.6 1	0:02:58	88
1850	49986.6	0.04	6726.5 1	0:03:57	88
1875	50004.7	0.05	6726.4 1	0:04:48	88
1900	49999	0.04	6726.6 1	0:05:48	88
1925	50009.8	0.04	6726.7 1	0:06:43	88
1950	50008.7	0.04	6726.9 1	0:07:39	88
1975	50010	0.04	6726.9 1	0:08:32	88
2000	50019	0.04	6726.7 1	0:09:31	88
2025	50014.8	0.04	6726.9 1	0:10:23	88
2050	50026.1	0.04	6726.6 1	0:11:21	88
2075	50026.1	0.03	6726.2 1	0:12:13	88
2100	50027.6	0.04	6725.9 1	0:13:08	88
2125	50026.4	0.03	6725.9 1	0:13:59	88
2150	50026.3	0.04	6725.8 1	0:14:54	88
2175	50021.1	0.04	6725.5 1	0:15:47	88
2200	50009.8	0.04	6725.4 1	0:16:43	88
2225	50019.5	0.04	6725.1 1	0:17:35	88
2250	50010.2	0.03	6724.7 1	0:18:27	88
2275	50006	0.04	6724.8 1	0:19:18	88
2300	50013.3	0.05	6724.7 1	0:20:11	88
2325	50010.3	0.03	6724.6 1	0:21:02	88
2350	50003.1	0.04	6724.5 1	0:21:56	88
2375	50005.4	0.04	6724.4 1	0:22:46	88
2400	50001.9	0.05	6724.5 1	0:23:39	88
2425	50007.6	0.03	6724.4 1	0:24:31	88

## TEU6

2450	50001.5	0.04	6724.5	1	0:25:25	88
2475	50010.9	0.04	6724.7	1	0:26:14	88
2500	50003.8	0.03	6724.9	1	0:27:08	88
Line 16+7	5N D	ate	6-Jul-96		#100	
POSITIO	FIELD	ERR	DRIFT		TIME	DS CULT
-2500	50016.2	0.06	6724.7	1	0:28:06	88
-2475	50016.4	0.03	6724.7	1	0:30:11	88
-2450	50013.8	0.04	6725.1	1	0:31:03	88
-2425	50012.2	0.04	6724.9	1	0:31:58	88
-2400	50011.6	0.04	6725.0	1	0:32:44	88
-2375	50015.9	0.03	6725.1	1	0:33:33	88
-2350	50005.5	0.05	6725.0	1	0:34:21	88
-2325	50013.6	0.05	6725.1	1	0:35:09	88
-2300	50009.5	0.04	6725.1	1	0:35:57	88
-2275	50017.1	0.04	6725.0	1	0:36:44	88
-2250	49998.9	0.03	6724.9	1	0:37:32	88
-2225	50025.1	0.04	6724.8	1	0:38:27	88
-2200	50027.2	0.04	6724.5	1	0:39:11	88
-2175	50034.5	0.03	6724.3	1	0:40:05	88
-2150	50034.7	0.03	6724.3	1	0:40:49	88
-2125	50035.4	0.03	6724.4	1	0:41:36	88
-2100	50033.5	0.03	6724.5	1	0:42:25	88
-2075	50037.8	0.03	6724.3	1	0:43:13	88
-2050	50024	0.13	6724.3	1	0:44:03	88
-2025	50034.4	0.04	6724.2	1	0:44:53	88
-2000	50025.4	0.04	6723.9	1	0:45:40	88
-1975	50027.4	0.04	6723.7	1	0:46:31	88
-1950	50012.8	0.04	6723.8	1	0:47:19	88
-1925	50018	0.03	6723.9	1	0:48:08	88
-1900	49997.8	0.05	6723.8	1	0:48:55	88
-1875	50015.1	0.04	6723.5	1	0:49:41	88
-1850	49981.1	0.06	6723.4	1	0:50:31	88
-1825	50004.2	0.04	6723.4	1	0:51:35	88
-1800	49977.4	0.17	6723.4	1	0:52:27	88
-1775	49990.6	0.04	6723.2	1	0:53:20	88
-1750	49972.6	0.03	6723.1	1	0:54:11	88
-1725	49954.9	0.03	6723.0	1	0:54:59	88
-1700	49930.4	0.04	6723.0	1	0:55:45	88
Line 19+0	0N D	ate	6-Jul-96		#133	
POSITIO	FIELD	ERR	DRIFT		TIME	DS CULT
1825	49917.9	0.04	6721.6	1	1:18:37	88
1850	49926.3	0.03	6721.4	1	1:19:56	88
1875	49947.9	0.04	6721.3	1	1:20:59	88
Line 19+2	5N D	ate	6-Jul-96		#136	
POSITIO	FIELD	ERR	DRIFT		TIME	DS CULT
-1875	49987.1	0.05	6720.8	1	1:23:34	88
-1850	49926.2	0.04	6720.5	1	1:24:42	88
-1825	49906.8	0.04	6720.3	1	1:25:35	88
Line 19+5	0N D	ate	6-Jul-96		#139	
POSITIO	FIELD	ERR	DRIFT		TIME	DS CULT
1825	49908	0.04	6720.0	1	1:28:08	88

## TEU6

1850	49934	0.06	6720.0	1	1:29:06	88
1875	49941.3	0.04	6719.9	1	1:30:24	88
Line 19+7	5N D	ate	6-Jul-96		#142	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-1875	49995.6	0.25	6719.5	1	1:32:14	88
-1850	49973.1	0.09	6719.0	1	1:34:39	88
Line 20+0	0N D	ate	6-Jul-96		#144	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1850	49949.2	0.04	6719.0	1	1:37:08	88
1875	50018.3	0.04	6719.0	1	1:38:44	88
Line 20+2	5N D	ate	6-Jul-96		#146	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-1875	49989	0.05	6718.3	1	1:41:44	88
-1850	49980	0.04	6718.0	1	1:43:09	88
Line 20+5	0N D	ate	6-Jul-96		#148	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1850	49962.3	0.03	6717.2	1	1:46:30	88
Line 20+7	5N D	ate	6-Jul-96		#149	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-1850	49940.5	0.04	6716.7	1	1:50:01	88
Line 18+5	0N D	ate	6-Jul-96		#151	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1850	49940.9	0.04	6707.9	1	3:08:44	88
1875	49963.4	0.04	6707.8	1	3:11:26	88
1900	50002.4	0.04	6707.5	1	3:13:46	88
1925	50094.9	0.04	6706.9	1	3:17:33	88
1950	50086.6	0.05	6706.5	1	3:19:07	88
1975	50063	0.04	6706.8	1	3:20:26	88 LOWER TEMP HELO PAD
2000	49989.7	0.08	6706.0	1	3:21:30	88 TRENCH 84
Line 20+2	5N D	ate	6-Jul-96		#158	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
2000	49993	0.04	6707.1	1	3:41:10	88
2025	49997.3	0.09	6708.2	1	3:42:42	88
2050	50027.6	0.07	6709.0	1	3:43:44	88
2075	50068.1	0.04	6709.1	1	3:47:42	88
2100	50061.5	0.04	6709.4	1	3:49:10	88
2125	50052.2	0.04	6709.9	1	3:50:14	88
2150	50006.3	0.04	6706.2	1	3:53:25	88
2175	49997.2	0.03	6708.0	1	3:54:46	88
2200	49993.1	0.04	6709.8	1	3:55:39	88
2225	49999.2	0.03	6709.7	1	3:56:29	88
2250	49994.1	0.04	6708.6	1	3:57:16	88
2275	49996.5	0.04	6705.2	1	3:58:04	88
2300	49991.7	0.04	6709.3	1	3:58:57	88
2325	49993.9	0.04	6710.2	1	3:59:44	88
2350	49990	0.03	6710.6	1	4:00:35	88
2375	49987	0.03	6711.1	1	4:01:23	88
2400	49987.7	0.03	6711.7	1	4:02:14	88
2425	49997.7	0.04	6711.5	1	4:03:03	88
2450	49996.1	0.03	6706.2	1	4:03:58	88
2475	49995.5	0.03	6711.6	1	4:05:11	88

TEU6

Line	POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
2500	49994.6		0.06	6712.0 1	4:05:53	88	
Line 20+5 0N D ate 6-Jul-96 #179							
-2500	50003.2		0.03	6711.7 1	4:06:52	88	
-2475	50035.1		0.03	6674.6 1	4:07:50	88	
-2450	49995.6		0.05	6702.1 1	4:08:46	88	
-2425	49996.9		0.03	6712.8 1	4:09:37	88	
-2400	49984.2		0.05	6712.9 1	4:10:31	88	
-2375	49993.5		0.04	6712.9 1	4:11:22	88	
-2350	49988.2		0.05	6712.8 1	4:12:18	88	
-2325	50002.8		0.04	6713.3 1	4:13:12	88	
-2300	50009.9		0.04	6712.3 1	4:14:03	88	
-2275	50009.2		0.04	6707.0 1	4:14:53	88	
-2250	50006.9		0.03	6692.2 1	4:15:54	88	
-2225	50003		0.04	6708.6 1	4:16:47	88	
-2200	49991.3		0.04	6714.4 1	4:17:57	88	
-2175	50019.8		0.04	6714.2 1	4:19:00	88	
-2150	50022.8		0.04	6714.7 1	4:20:06	88	
-2125	50113		0.03	6716.0 1	4:23:47	88	
-2100	50157.3		0.04	6715.1 1	4:25:31	88	
-2075	50050.1		0.03	6717.4 1	4:27:16	88	
-2050	50040.4		0.07	6717.4 1	4:28:42	88	
-2025	50067.9		0.04	6717.6 1	4:29:50	88	
-2000	50062.2		0.06	6719.0 1	4:35:54	88	7M E DDH95 SITE
-1975	50127.1		0.04	6713.1 1	4:40:01	88	
-1950	50465.4		0.03	6710.8 1	4:41:33	88	
-1925	50305		0.04	6709.2 1	4:42:45	88	MAIN HELO PAD
-1900	49966.4		0.04	6709.9 1	4:45:40	88	
-1875	49930.4		0.04	6712.7 1	4:47:08	88	
Line 20+7 5N D ate 6-Jul-96 #205							
1875	49970.3		0.04	6716.1 1	4:49:28	88	
1900	49893.6		0.15	6717.0 1	4:50:37	88	WEATHERHAVEN
1925	49804.1		0.07	6721.1 1	4:54:10	88	S E CORNER DRY
1950	50068.6		0.04	6722.6 1	4:55:16	88	
1975	50035.1		0.14	6722.7 1	4:56:33	88	
2000	49992.2		0.03	6722.4 1	4:57:25	88	
2025	50020.9		0.04	6722.6 1	4:58:10	88	
2050	50055		0.05	6722.4 1	4:59:16	88	
2075	50039.8		0.04	6722.4 1	5:00:05	88	
2100	50076		0.04	6722.2 1	5:00:52	88	
2125	50005.7		0.04	6722.2 1	5:01:46	88	
2150	50022.8		0.08	6721.9 1	5:02:41	88	
2175	49995.1		0.03	6721.6 1	5:03:29	88	
2200	49989.7		0.03	6721.4 1	5:04:19	88	
2225	49988.8		0.04	6721.4 1	5:05:09	88	
2250	49988		0.03	6721.8 1	5:06:00	88	
2275	50002.2		0.04	6721.3 1	5:06:46	88	
2300	49999		0.03	6721.7 1	5:08:23	88	
2325	49989.6		0.03	6722.3 1	5:09:13	88	
2350	49993.9		0.04	6722.1 1	5:10:03	88	

TEU6

Line	21+0	ON	D	ate	6-Jul-96	#231
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
2375	49995.1	0.04	6722.0	1	5:10:54	88
2400	50019.1	0.94	6722.4	1	5:11:46	88
2425	50003.9	0.04	6722.7	1	5:12:33	88
2450	49995.6	0.03	6723.0	1	5:13:26	88
2475	49985.6	0.03	6723.5	1	5:14:16	88
2500	50004.4	0.04	6724.1	1	5:15:11	88
-2500	49999	0.04	6724.0	1	5:16:08	88
-2475	50007.9	0.04	6724.5	1	5:17:15	88
-2450	50000.9	0.04	6724.7	1	5:18:07	88
-2425	50007.1	0.04	6724.5	1	5:19:06	88
-2400	50004	0.04	6724.7	1	5:19:59	88
-2375	50000.8	0.03	6725.2	1	5:20:50	88
-2350	49996.4	0.03	6725.7	1	5:21:49	88
-2325	50001.1	0.04	6725.9	1	5:22:43	88
-2300	49990	0.03	6726.2	1	5:23:40	88
-2275	50003.4	0.04	6726.2	1	5:24:38	88
-2250	50003.4	0.05	6726.1	1	5:25:40	88
-2225	50008	0.04	6726.2	1	5:26:37	88
-2200	49995.6	0.04	6726.2	1	5:27:39	88
-2175	50024.2	0.03	6726.0	1	5:28:40	88
-2150	50037	0.03	6726.0	1	5:29:43	88
-2125	50070.4	0.04	6725.9	1	5:30:54	88
-2100	50078.7	0.04	6726.0	1	5:32:16	88
-2075	50048.1	0.03	6726.6	1	5:37:12	88

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Line 21+0	ON	D	ate	6-Jul-96	#	1
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-2050	56765.2	0.04	0	8:29:26	88	
-2025	56757.7	0.03	0	8:31:03	88	DDH96 #4 SITE
-2000	56732.1	0.05	0	8:33:11	88	
-1975	56844.1	0.06	0	8:34:36	88	3M W BA SE STATION
-1950	56790	0.05	0	8:38:47	88	
-1925	56644	0.04	0	8:40:07	88	KITCHEN
-1900	56617.6	0.04	0	8:54:42	88	
-1875	56701.3	0.03	0	8:55:35	88	
-1850	56694.1	0.04	0	8:58:07	88	

Line 21+2	5N	D	ate	6-Jul-96	#1	0
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1850	56693.5	0.04	0	9:00:45	88	
1875	56696.6	0.05	0	9:02:18	88	
1900	56679.9	0.04	0	9:03:13	88	
1925	56643.9	0.04	0	9:04:13	88	TENTS
1950	56748.4	0.04	0	9:05:17	88	TRENCH #?
1975	56830.9	0.08	0	9:06:43	88	OUT HOU SE
2000	56767.2	0.16	0	9:09:01	88	
2025	56771	0.04	0	9:09:56	88	
2050	56751.3	0.05	0	9:11:51	88	
2075	56723.6	0.04	0	9:15:51	88	
2100	56740.6	0.04	0	9:20:20	88	
2125	56758.9	0.04	0	9:21:10	88	
2150	56760	0.06	0	9:22:03	88	
2175	56732.9	0.04	0	9:22:50	88	
2200	56712.5	0.04	0	9:23:39	88	
2225	56703	0.03	0	9:24:26	88	
2250	56708.6	0.04	0	9:25:10	88	
2275	56719.3	0.03	0	9:25:56	88	
2300	56710.5	0.03	0	9:26:40	88	
2325	56717.2	0.03	0	9:27:49	88	
2350	56709.5	0.03	0	9:28:41	88	
2375	56705.5	0.03	0	9:29:27	88	
2400	56705.1	0.03	0	9:30:16	88	
2425	56708.7	0.04	0	9:31:00	88	
2450	56709.3	0.03	0	9:31:46	88	
2475	56708.7	0.03	0	9:32:32	88	
2500	56703.6	0.03	0	9:33:20	88	

Line 21+5	ON	D	ate	6-Jul-96	#3	7
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-2500	56721.4	0.03	0	9:34:11	88	
-2475	56714.1	0.03	0	9:35:06	88	
-2450	56704	0.04	0	9:36:01	88	
-2425	56708	0.03	0	9:36:48	88	
-2400	56706	0.04	0	9:37:42	88	
-2375	56715.3	0.03	0	9:38:40	88	
-2350	56707.9	0.04	0	9:39:34	88	
-2325	56705.4	0.03	0	9:40:31	88	
-2300	56705.5	0.04	0	9:41:29	88	

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-2275	56708.3	0.03	0	9:42:23	88	
-2250	56700.8	0.03	0	9:43:17	88	
-2225	56712.7	0.03	0	9:44:10	88	
-2200	56715.5	0.03	0	9:45:09	88	
-2175	56742.8	0.04	0	9:46:04	88	
-2150	56753.5	0.04	0	9:47:07	88	
-2125	56745.8	0.03	0	9:48:10	88	
-2100	56725.2	0.05	0	9:49:23	88	
-2075	56724.2	0.04	0	9:52:13	88	
-2050	56746.6	0.04	0	9:54:19	88	
-2025	56754.4	0.04	0	9:55:37	88	
-2000	56737.2	0.04	0	9:56:44	88	
-1975	56794.2	0.04	0	9:58:14	88	
-1950	56682.8	0.05	0	9:59:16	88	OFFICE & GENSET
-1925	56648	0.04 0.0 1		0:02:47	88	CORE SH ACK
-1900	56711.7	0.04 0.0 1		0:04:01	88	
-1875	56722.8	0.03 0.0 1		0:04:52	88	
-1850	56736	0.03 0.0 1		0:05:45	88	
-1825	56754.5	0.04 0.0 1		0:06:43	88	
Line 21+7	5N D	ate	6-Jul-96	#6	5	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1800	56777.6	0.05 0.0 1		0:11:04	88	
1825	56706.7	0.03 0.0 1		0:14:37	88	
1850	56714.3	0.03 0.0 1		0:15:39	88	
1875	56710.4	0.03 0.0 1		0:16:31	88	
1900	56703.4	0.03 0.0 1		0:17:22	88	
1925	56667.9	0.31 0.0 1		0:18:16	88	
1950	56589.7	0.04 0.0 1		0:22:38	88	
1975	56812.9	0.03 0.0 1		0:23:35	88	
2000	56759.3	0.06 0.0 1		0:24:26	88	
2025	56783.5	0.03 0.0 1		0:25:15	88	
2050	56783.5	0.04 0.0 1		0:26:07	88	
2075	56765.1	0.03 0.0 1		0:27:53	88	
2100	56782.2	0.03 0.0 1		0:29:13	88	
2125	56763.5	0.03 0.0 1		0:30:16	88	
2150	56745.5	0.03 0.0 1		0:31:12	88	
2175	56763	0.03 0.0 1		0:32:00	88	
2200	56722.8	0.04 0.0 1		0:32:46	88	
2225	56716.8	0.03 0.0 1		0:33:34	88	
2250	56749.9	0.03 0.0 1		0:34:19	88	
2275	56753.7	0.03 0.0 1		0:35:07	88	
2300	56725.1	0.04 0.0 1		0:35:52	88	
2325	56726.2	0.04 0.0 1		0:36:41	88	
2350	56734.5	0.03 0.0 1		0:37:28	88	
2375	56733.6	0.04 0.0 1		0:38:13	88	
2400	56741.2	0.03 0.0 1		0:38:59	88	
2425	56739.5	0.04 0.0 1		0:39:45	88	
2450	56737.7	0.04 0.0 1		0:40:33	88	
2475	56734.4	0.04 0.0 1		0:41:21	88	
2500	56730.9	0.03 0.0 1		0:42:10	88	
Line 22+0	0N D	ate	6-Jul-96	#9	4	

POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-2500	56729.9	0.04	0.0 1	0:43:09		88
-2475	56736.3	0.03	0.0 1	0:44:07		88
-2450	56727.2	0.05	0.0 1	0:45:06		88
-2425	56730.8	0.05	0.0 1	0:45:54		88
-2400	56748.5	0.03	0.0 1	0:46:52		88
-2375	56694.4	0.04	0.0 1	0:47:48		88
-2350	56740.1	0.03	0.0 1	0:49:48		88
-2325	56741.7	0.04	0.0 1	0:50:48		88
-2300	56751.6	0.03	0.0 1	0:51:49		88
-2275	56744.2	0.04	0.0 1	0:52:51		88
-2250	56726.9	0.04	0.0 1	0:53:56		88
-2225	56739.9	0.03	0.0 1	0:55:06		88
-2200	56735.3	0.04	0.0 1	0:55:56		88
-2175	56762.9	0.04	0.0 1	0:57:49		88
-2150	56756.5	0.03	0.0 1	0:58:43		88
-2125	56759.2	0.04	0.0 1	0:59:43		88
-2100	56768.1	0.04	0.0 1	1:00:53		88
-2075	56730.8	0.04	0.0 1	1:02:51		88
-2050	56755.6	0.04	0.0 1	1:03:57		88
-2025	56757.7	0.04	0.0 1	1:05:12		88
-2000	56729.7	0.08	0.0 1	1:06:41		88
-1975	56746.7	0.03	0.0 1	1:07:50		88
-1950	56735.7	0.03	0.0 1	1:09:05		88
-1925	56723.5	0.03	0.0 1	1:09:55		88
-1900	56724.4	0.04	0.0 1	1:10:58		88
-1875	56725.6	0.03	0.0 1	1:11:54		88
-1850	56727.5	0.04	0.0 1	1:12:51		88
-1825	56742.4	0.04	0.0 1	1:13:56		88
-1800	56747.1	0.04	0.0 1	1:15:12		88

Line 22+2 5N D ate 6-Jul-96 #12 3

POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1800	56749.8	0.03	0.0 1	1:16:40		88
1825	56715.3	0.03	0.0 1	1:17:47		88
1850	56725.5	0.04	0.0 1	1:18:36		88
1875	56722.7	0.03	0.0 1	1:19:25		88
1900	56723.4	0.03	0.0 1	1:20:13		88
1925	56711.3	0.04	0.0 1	1:20:59		88
1950	56727.6	0.03	0.0 1	1:21:45		88
1975	56749.7	0.04	0.0 1	2:45:27		88
2000	56743.7	0.04	0.0 1	2:46:16		88
2025	56755.7	0.05	0.0 1	2:47:12		88
2050	56774.4	0.04	0.0 1	2:48:33		88
2075	56750.9	0.04	0.0 1	2:49:33		88
2100	56717.6	0.03	0.0 1	2:50:16		88
2125	56719.3	0.03	0.0 1	2:51:09		88
2150	56723.2	0.03	0.0 1	2:51:57		88
2175	56725.4	0.04	0.0 1	2:52:45		88
2200	56720	0.03	0.0 1	2:53:33		88
2225	56718.8	0.04	0.0 1	2:54:23		88
2250	56725.4	0.06	0.0 1	2:55:09		88



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2275	56740.9	0.03	0.0	1	2:55:59	88	
2300	56717.3	0.06	0.0	1	2:56:48	88	
2325	56724.6	0.04	0.0	1	2:57:36	88	
2350	56739.5	0.04	0.0	1	2:58:28	88	
2375	56716.8	0.03	0.0	1	2:59:15	88	
2400	56736.2	0.04	0.0	1	3:00:01	88	
2425	56725.2	0.04	0.0	1	3:00:46	88	
2450	56740.1	0.04	0.0	1	3:01:33	88	
2475	56726.1	0.04	0.0	1	3:02:21	88	
2500	56721.1	0.03	0.0	1	3:03:08	88	
Line 22+5	ON D	ate	6-Jul-96		#15		2
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT	
-2500	56721.2	0.05	0.0	1	3:04:04	88	
-2475	56725.6	0.04	0.0	1	3:05:07	88	
-2450	56720.8	0.05	0.0	1	3:06:04	88	
-2425	56723.9	0.04	0.0	1	3:07:01	88	
-2400	56715.1	0.04	0.0	1	3:07:55	88	
-2375	56711.7	0.03	0.0	1	3:08:46	88	
-2350	56712.4	0.04	0.0	1	3:09:42	88	
-2325	56719.7	0.03	0.0	1	3:10:33	88	
-2300	56708.9	0.04	0.0	1	3:11:36	88	
-2275	56704.3	0.05	0.0	1	3:12:32	88	
-2250	56707.6	0.03	0.0	1	3:13:38	88	
-2225	56708.7	0.03	0.0	1	3:14:34	88	
-2200	56709	0.04	0.0	1	3:15:41	88	
-2175	56707	0.04	0.0	1	3:16:48	88	
-2150	56714.7	0.04	0.0	1	3:17:49	88	
-2125	56711.7	0.03	0.0	1	3:18:58	88	
-2100	56721.8	0.03	0.0	1	3:20:01	88	
-2075	56725.8	0.04	0.0	1	3:21:14	88	
-2050	56741.8	0.04	0.0	1	3:22:19	88	
-2025	56737.3	0.04	0.0	1	3:23:31	88	
-2000	56751.3	0.05	0.0	1	3:24:42	88	
-1975	56768.4	0.03	0.0	1	3:25:56	88	
-1950	56732.1	0.04	0.0	1	3:27:19	88	
-1925	56695.7	0.03	0.0	1	3:28:14	88	
-1900	56716	0.04	0.0	1	3:29:25	88	
-1875	56738.8	0.04	0.0	1	3:30:34	88	
-1850	56714	0.04	0.0	1	3:31:40	88	
-1825	56726.2	0.03	0.0	1	3:32:57	88	
-1800	56735.1	0.08	0.0	1	3:34:23	88	
Line 22+7	5N D	ate	6-Jul-96		#18		1
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT	
1800	56730.1	0.03	0.0	1	3:37:44	88	
1825	56707.7	0.04	0.0	1	3:40:59	88	
1850	56699.3	0.03	0.0	1	3:43:18	88	
1875	56692.9	0.04	0.0	1	3:44:13	88	
1900	56705.1	0.03	0.0	1	3:45:03	88	
1925	56673.9	0.03	0.0	1	3:45:55	88	
1950	56722	0.03	0.0	1	3:46:50	88	
1975	56732.3	0.04	0.0	1	3:48:02	88	

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2000	56731	0.05 0.0 1	3:49:04	88
2025	56742.2	0.05 0.0 1	3:50:05	88
2050	56747.9	0.03 0.0 1	3:51:12	88
2075	56718.9	0.03 0.0 1	3:52:11	88
2100	56724.9	0.03 0.0 1	3:53:05	88
2125	56713.3	0.03 0.0 1	3:54:02	88
2150	56707.1	0.03 0.0 1	3:54:51	88
2175	56699.5	0.04 0.0 1	3:55:42	88
2200	56700.5	0.05 0.0 1	3:56:33	88
2225	56703.2	0.03 0.0 1	3:57:23	88
2250	56704.6	0.04 0.0 1	3:58:16	88
2275	56704.6	0.04 0.0 1	3:59:05	88
2300	56706.9	0.03 0.0 1	3:59:55	88
2325	56707.2	0.04 0.0 1	4:00:43	88
2350	56712.5	0.03 0.0 1	4:01:32	88
2375	56708.6	0.04 0.0 1	4:02:21	88
2400	56717.1	0.04	0	

## TEU8

Line	23+2	5N	D	ate	10-Jul-96	#1
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
2000	49980.7	0.1	6743.5	9:09:31	88	
2025	50015.4	0.04	6743.4	9:10:56	88	
2050	50000	0.09	6743.3	9:11:39	88	
2075	49994.4	0.05	6743.5	9:12:22	88	
2100	49998.7	0.04	6744	9:13:08	88	
2125	49968.5	0.04	6743.2	9:13:52	88	
2150	49986.1	0.04	6742.9	9:14:34	88	
2175	49979.3	0.04	6743	9:15:15	88	
2200	49975.7	0.04	6743.7	9:16:00	88	
2225	49972.9	0.04	6743	9:16:45	88	
2250	49965.6	0.05	6742.7	9:17:27	88	
2275	49992.4	0.06	6742.6	9:18:09	88	
2300	49979.5	0.06	6743.1	9:18:50	88	
2325	49975	0.04	6742.8	9:19:32	88	
2350	49975.8	0.04	6742.5	9:20:18	88	
2375	49971	0.04	6743	9:21:04	88	
2400	50003.2	0.09	6742.3	9:21:46	88	
2425	49983	0.04	6742	9:22:31	88	
2450	49974.3	0.04	6742.2	9:23:17	88	
2475	49996.3	0.06	6742.6	9:24:14	88	
2500	49995.5	0.04	6742.4	9:24:46	88	

Line	22+5	0N	D	ate	10-Jul-96	#22
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
2500	50001.9	0.05	6742.5	9:26:10	88	

Line	22+7	5N	D	ate	10-Jul-96	#23
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
2500	49986	0.04	6742.2	9:27:53	88	

Line	23+0	0N	D	ate	10-Jul-96	#24
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
2500	49989.2	0.06	6742.2	9:29:04	88	

Line	23+5	0N	D	ate	10-Jul-96	#25
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-2500	49978.1	0.06	6741.3	9:35:04	88	
-2475	49982.9	0.04	6741	9:36:41	88	
-2450	49986.4	0.04	6740.9	9:37:42	88	
-2425	49984.1	0.04	6740.9	9:38:31	88	
-2400	49981.1	0.04	6741	9:39:34	88	
-2375	49972.7	0.04	6741	9:40:30	88	
-2350	49974.3	0.04	6740.7	9:41:26	88	
-2325	49975.7	0.04	6740.6	9:42:21	88	
-2300	49975.3	0.04	6740.6	9:43:23	88	
-2275	49972.1	0.04	6740.8	9:44:14	88	
-2250	49975.2	0.04	6740.6	9:45:13	88	
-2225	49969.8	0.04	6740.2	9:46:12	88	
-2200	49972.2	0.04	6740.1	9:47:06	88	
-2175	49981.8	0.04	6740.2	9:48:09	88	
-2150	49981.2	0.04	6739.9	9:49:10	88	
-2125	49984.3	0.04	6739.8	9:50:42	88	
-2100	50002.6	0.04	6739.5	9:51:48	88	

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-2075	49993.9	0.04	6739.5	9:52:57	88
-2050	50010.7	0.08	6739.4	9:54:29	88
-2025	50001.1	0.04	6739.6	9:56:08	88
-2000	50010.5	0.05	6739.5	9:57:19	88
-1975	50001.6	0.04	6739.4 1	0:00:04	88
-1950	50016.5	0.04	6738.8 1	0:02:42	88
-1925	49978.7	0.05	6738.8 1	0:03:52	88
-1900	49977.7	0.03	6738.6 1	0:05:18	88
-1875	50011.9	0.93	6738.7 1	0:08:14	88
-1850	49988.6	0.04	6738.3 1	0:10:19	88
-1825	49979.2	0.04	6738.5 1	0:11:01	88
-1800	49971.2	0.04	6738.5 1	0:11:41	88

Line 23+7	5N D	ate	10-Jul-96	#54	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
1800	49979	0.04	6738.5 1	0:13:37	88
1825	49981.3	0.04	6738.4 1	0:14:40	88
1850	49982.8	0.04	6738.4 1	0:15:34	88
1875	49983.7	0.04	6738.3 1	0:16:41	88
1900	49987	0.05	6738.4 1	0:18:18	88
1925	49992.9	0.04	6738.1 1	0:19:00	88
1950	50000.7	0.05	6738.0 1	0:20:13	88
1975	50025.6	0.04	6738.0 1	0:21:22	88
2000	49989.5	0.06	6738.2 1	0:22:10	88
2025	50002	0.05	6738.1 1	0:22:57	88
2050	50008.6	0.05	6737.9 1	0:24:52	88
2075	49991	0.04	6737.8 1	0:25:36	88
2100	49991.2	0.04	6737.9 1	0:26:19	88
2125	49973.1	0.04	6737.9 1	0:27:05	88
2150	49994.7	0.05	6737.9 1	0:27:46	88
2175	49980.1	0.04	6737.8 1	0:28:29	88
2200	49977.3	0.03	6737.6 1	0:29:12	88
2225	49966.8	0.04	6737.6 1	0:29:56	88
2250	49971.2	0.04	6737.8 1	0:30:43	88
2275	49986.7	0.04	6737.7 1	0:31:31	88
2300	49988.2	0.04	6737.5 1	0:32:16	88
2325	49970.6	0.04	6737.5 1	0:32:59	88
2350	49987.1	0.04	6737.8 1	0:33:48	88
2375	49965.9	0.04	6737.9 1	0:34:44	88
2400	49979.8	0.04	6737.8 1	0:35:44	88
2425	50002.3	0.04	6737.8 1	0:36:30	88
2450	50005.4	0.05	6737.8 1	0:37:20	88
2475	49995.6	0.05	6737.8 1	0:38:10	88
2500	50006.6	0.03	6737.8 1	0:38:59	88

Line 24+0	0N D	ate	10-Jul-96	#83	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2500	50003.2	0.03	6738.1 1	0:44:45	88
-2475	50003.2	0.04	6737.9 1	0:46:37	88
-2450	50000.8	0.03	6738.0 1	0:47:49	88
-2425	49990.4	0.04	6737.9 1	0:48:47	88
-2400	49980.8	0.11	6737.8 1	0:49:50	88
-2375	50001.3	0.04	6737.7 1	0:50:45	88

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-2350	49987.2	0.04	6737.7	1	0:51:49	88
-2325	49983.1	0.04	6737.8	1	0:53:04	88
-2300	49991.3	0.06	6737.8	1	0:54:03	88
-2275	49989.2	0.66	6738.5	1	0:56:23	88
-2250	49987.6	0.04	6738.3	1	0:57:14	88
-2225	49983.3	0.03	6738.2	1	0:58:01	88
-2200	49976.7	0.04	6737.9	1	0:59:10	88
-2175	49972.7	0.04	6737.8	1	1:00:15	88
-2150	49983.5	0.03	6737.9	1	1:01:40	88
-2125	49973.7	0.03	6737.8	1	1:03:11	88
-2100	49971.9	0.04	6737.6	1	1:04:25	88
-2075	50004.4	0.04	6737.8	1	1:06:19	88
-2050	50001.6	0.03	6738.0	1	1:07:35	88
-2025	50013.5	0.03	6737.8	1	1:11:07	88

Line 24+2	5N	D	ate	10-Jul-96	#103	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT	
2025	50121.9	0.04	6737.7	1	1:16:29	88
2050	50017.4	0.04	6737.6	1	1:17:56	88
2075	49972.7	0.04	6737.2	1	1:18:39	88
2100	49989	0.06	6737.1	1	1:19:37	88
2125	49983	0.04	6737.2	1	1:20:24	88
2150	49976.3	0.04	6736.9	1	1:21:08	88
2175	49977.2	0.04	6737.0	1	1:21:52	88
2200	49999.1	0.05	6736.6	1	1:22:39	88
2225	49998.5	0.04	6736.3	1	1:23:23	88
2250	49965.1	0.04	6736.4	1	1:24:08	88
2275	49986.9	0.03	6736.4	1	1:24:50	88
2300	49979.4	0.03	6736.2	1	1:25:35	88
2325	49979.4	0.04	6736.1	1	1:26:16	88
2350	49979.5	0.04	6735.8	1	1:27:01	88
2375	49982.6	0.04	6736.5	1	1:27:44	88
2400	49999.7	0.04	6736.6	1	1:28:28	88
2425	49983.7	0.04	6736.1	1	1:29:10	88
2450	49999.1	0.04	6735.7	1	1:29:57	88
2475	49994.7	0.04	6735.8	1	1:30:39	88
2500	49991.5	0.11	6735.7	1	1:31:28	88

Line 24+5	0N	D	ate	10-Jul-96	#123	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT	
-2500	49991.6	0.04	6735.2	1	1:32:19	88
-2475	49983.9	0.04	6735.2	1	1:34:28	88
-2450	49987.3	0.07	6734.9	1	1:35:22	88
-2425	49989.9	0.05	6734.5	1	1:36:12	88
-2400	49981.9	0.04	6734.7	1	1:37:12	88
-2375	49978	0.04	6734.6	1	1:38:04	88
-2350	49970.5	0.04	6734.2	1	1:39:02	88
-2325	49973.1	0.03	6734.0	1	1:39:57	88
-2300	49967.6	0.06	6733.9	1	1:40:54	88
-2275	49976.1	0.04	6733.4	1	1:42:07	88
-2250	49974.9	0.04	6733.5	1	1:43:07	88
-2225	49970.9	0.04	6734.0	1	1:44:05	88
-2200	49975	0.04	6734.1	1	1:45:18	88

## TEU8

-2175	49965	0.04	6733.2	1	1:48:03	88
-2150	49972.4	0.04	6732.8	1	1:49:08	88
-2125	49978.9	0.04	6732.7	1	1:50:25	88
-2100	49973.2	0.04	6732.3	1	1:51:43	88
-2075	49965.3	0.04	6731.7	1	1:52:55	88
-2050	50011.7	0.04	6731.4	1	1:54:35	88
-2025	50016.6	0.04	6731.2	1	1:57:28	88

Line 24+7	5N	D	ate	10-Jul-96	#143	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
2025	49993.2	0.04	6730.8	1	1:58:26	88
2050	49988.5	0.04	6730.8	1	1:59:23	88
2075	49972.5	0.04	6730.6	1	2:00:08	88
2100	49961.6	0.04	6730.7	1	2:00:57	88
2125	49971.7	0.04	6730.5	1	2:01:45	88
2150	49963	0.04	6730.5	1	2:02:26	88
2175	49962.6	0.04	6730.9	1	2:03:13	88
2200	49965.6	0.04	6730.8	1	2:04:02	88
2225	49959.6	0.04	6730.5	1	2:04:40	88
2250	49974.5	0.04	6730.3	1	2:05:25	88
2275	49967	0.04	6730.3	1	2:06:09	88
2300	49962	0.03	6730.3	1	2:06:56	88
2325	49958	0.05	6730.0	1	2:07:46	88
2350	49966.1	0.04	6730.0	1	2:08:32	88
2375	49967.1	0.04	6730.0	1	2:09:14	88
2400	49980.7	0.04	6729.6	1	2:10:02	88
2425	49978.1	0.04	6729.4	1	2:11:12	88
2450	49989.8	0.04	6729.4	1	2:12:04	88
2475	49990.7	0.04	6729.5	1	2:12:47	88
2500	49988.7	0.04	6729.5	1	2:13:35	88

Line 25+0	0N	D	ate	10-Jul-96	#163	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-2500	50011.3	0.04	6729.0	1	2:27:56	88
-2475	49999.7	0.04	6729.1	1	2:28:59	88
-2450	49988	0.03	6728.8	1	2:29:41	88
-2425	50000.9	0.04	6728.6	1	2:30:33	88
-2400	49993.2	0.04	6728.5	1	2:31:31	88
-2375	49988.9	0.04	6728.3	1	2:32:23	88
-2350	49987.2	0.04	6728.2	1	2:33:22	88
-2325	49972.6	0.04	6728.5	1	2:34:20	88
-2300	49971.6	0.04	6728.9	1	2:35:33	88
-2275	49970.7	0.04	6728.8	1	2:37:24	88
-2250	49970.5	0.03	6729.0	1	2:38:28	88
-2225	49977.8	0.04	6728.2	1	2:39:53	88
-2200	49970.3	0.04	6728.0	1	2:40:51	88
-2175	49969.7	0.04	6727.0	1	2:42:10	88
-2150	49974.1	0.04	6726.9	1	2:43:11	88
-2125	49966.4	0.04	6726.0	1	2:44:46	88
-2100	49976.3	0.04	6725.1	1	2:46:31	88
-2075	49982.1	0.04	6723.9	1	2:48:04	88
-2050	49993.4	0.04	6724.0	1	2:49:43	88
-2025	49975.7	0.04	6724.7	1	2:51:24	88

Line 25+2	5N	D	ate	10-Jul-96	#184
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
2025	49999.9	0.08	6725.9 1	2:57:49	88
2050	49974.8	0.04	6725.8 1	2:58:42	88
2075	49974.5	0.04	6725.6 1	2:59:38	88
2100	49956.1	0.04	6725.5 1	3:00:28	88
2125	49964.4	0.04	6725.6 1	3:01:17	88
2150	49968.1	0.04	6725.4 1	3:02:38	88
2175	49975.7	0.04	6725.4 1	3:03:24	88
2200	49974.1	0.04	6725.2 1	3:04:04	88
2225	49972.8	0.04	6725.4 1	3:04:48	88
2250	49970.2	0.04	6725.6 1	3:05:33	88
2275	49972.5	0.04	6725.7 1	3:06:19	88
2300	49969.9	0.04	6725.7 1	3:07:08	88
2325	49975.4	0.04	6725.7 1	3:07:54	88
2350	49983.6	0.04	6725.5 1	3:08:42	88
2375	49995.5	0.04	6725.4 1	3:09:23	88
2400	49986.5	0.04	6725.5 1	3:10:12	88
2425	49987.4	0.04	6725.5 1	3:10:59	88
2450	50003.9	0.04	6725.4 1	3:12:46	88
2475	50000.8	0.04	6724.9 1	3:14:41	88
2500	49993	0.03	6724.5 1	3:16:38	88

Line 25+5	0N	D	ate	10-Jul-96	#205
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2500	50018.2	0.04	6723.5 1	3:19:47	88
-2475	49994.2	0.04	6723.2 1	3:21:35	88
-2450	50009	0.04	6722.8 1	3:23:29	88
-2425	50018.3	0.04	6722.6 1	3:24:34	88
-2400	49983.2	0.04	6722.3 1	3:25:27	88
-2375	49984	0.04	6722.0 1	3:26:31	88
-2350	50019.2	0.05	6721.9 1	3:27:37	88
-2325	49987.4	0.04	6721.7 1	3:30:46	88
-2300	49987.8	0.04	6721.8 1	3:31:57	88
-2275	49972.8	0.04	6721.7 1	3:33:18	88
-2250	49976.9	0.04	6721.8 1	3:34:22	88
-2225	49968.5	0.04	6721.8 1	3:35:28	88
-2200	49976.2	0.04	6722.1 1	3:36:58	88
-2175	49962.7	0.04	6722.1 1	3:38:34	88
-2150	49972	0.04	6722.2 1	3:40:03	88
-2125	49969.9	0.04	6722.3 1	3:41:30	88
-2100	49980.5	0.04	6722.0 1	3:44:12	88
-2075	49987	0.04	6721.9 1	3:46:07	88
-2050	50021.3	0.03	6722.0 1	3:49:22	88
-2025	50004.2	0.04	6721.9 1	3:50:44	88

Line 24+0	0N	D	ate	10-Jul-96	#225
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2000	50047.4	0.05	6721.9 1	3:56:13	88

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## TEU9

Line 24+0 ON D			ate		11-Jul-96		#1
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT	
-2000	50027.8	0.04	6728.6	8:50:11	88		
-1975	50003.8	0.04	6728.7	8:52:35	88		
-1950	49990.9	0.04	6728.9	8:54:13	88		
-1925	50020.7	0.03	6729	8:55:30	88		
-1900	49976.7	0.05	6729.2	8:56:42	88		
-1875	49976.9	0.04	6729.3	8:57:44	88		
-1850	49982.7	0.08	6729.4	8:59:11	88		
-1825	49966	0.03	6729.6	9:00:25	88		
-1800	49959.8	0.03	6729.8	9:01:22	88		
-1775	49971.6	0.03	6730	9:02:27	88		
-1750	49968	0.04	6730.2	9:03:39	88		

Line 24+2 5N D			ate		11-Jul-96		#12
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT	
1750	49981.8	0.03	6730.2	9:05:13	88		
1775	49975.4	0.04	6730.3	9:06:23	88		
1800	49980.9	0.03	6730.3	9:07:10	88		
1825	49988.8	0.04	6730.6	9:08:03	88		
1850	49987.9	0.04	6730.9	9:09:07	88		
1875	49992.6	0.04	6731.4	9:10:12	88		
1900	49982.5	0.03	6731.9	9:11:20	88		
1925	50005.4	0.03	6732.1	9:12:17	88		
1950	49986.9	0.03	6732.2	9:13:17	88		
1975	49996.6	0.03	6732.1	9:14:21	88		
2000	50023.8	0.03	6731.7	9:15:19	88		

Line 24+5 ON D			ate		11-Jul-96		#23
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT	
-2000	50011.6	0.03	6731.1	9:16:28	88		
-1975	50002.5	0.04	6730.7	9:17:40	88		
-1950	49993.5	0.04	6730.7	9:19:06	88		
-1925	49995.7	0.04	6731.5	9:20:13	88		
-1900	49991.3	0.04	6732.1	9:21:34	88		
-1875	49987.8	0.04	6732.4	9:22:42	88		
-1850	50000.8	0.04	6732.4	9:23:52	88		
-1825	50004.8	0.05	6732.5	9:25:20	88		
-1800	49988.6	0.03	6732.4	9:26:18	88		
-1775	49983.4	0.04	6732.3	9:27:11	88		
-1750	49962.1	0.04	6732.3	9:28:24	88		
-1725	50005.8	0.04	6732.4	9:30:13	88		
-1700	50009.8	0.06	6732.5	9:31:24	88		

Line 24+7 5N D			ate		11-Jul-96		#36
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT	
1700	49991.2	0.04	6732.6	9:33:09	88		
1725	49976.4	0.04	6732.8	9:34:14	88		
1750	49982.5	0.04	6732.8	9:35:09	88		
1775	49987.4	0.03	6733.1	9:36:05	88		
1800	49995.3	0.04	6733.4	9:37:05	88		
1825	49986	0.03	6733.5	9:38:10	88		
1850	50001.8	0.05	6733.5	9:40:17	88		
1875	49988	0.04	6733.4	9:41:23	88		



## TEU9

1900	49984.7	0.03	6733.1	9:42:22	88
1925	49975.6	0.04	6732.9	9:44:04	88
1950	49996	0.04	6733.4	9:45:29	88
1975	50005	0.03	6733.7	9:46:54	88
2000	50003	0.04	6734	9:48:11	88

Line 25+0 0N D ate 11-Jul-96 #51					
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2000	49999.2	0.04	6734	9:49:22	88
-1975	49998.9	0.03	6734	9:51:17	88
-1950	50002.8	0.04	6733.8	9:52:45	88
-1925	50004.6	0.09	6733.8	9:55:21	88
-1900	49997.6	0.1	6734	9:56:41	88
-1875	49996.8	0.04	6733.8	9:59:19	88
-1850	50003.6	0.04	6733.4 1	0:01:06	88
-1825	49995.2	0.04	6732.8 1	0:10:39	88
-1800	49988.3	0.04	6732.6 1	0:11:25	88
-1775	50006.5	0.04	6732.6 1	0:12:40	88
-1750	49989.4	0.04	6732.6 1	0:13:56	88
-1725	49999.8	0.04	6732.3 1	0:15:11	88
-1700	50027	0.05	6732.0 1	0:16:25	88

Line 25+2 5N D ate 11-Jul-96 #62					
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
1700	50044	0.04	6731.8 1	0:17:27	88
1725	50011.6	0.03	6731.4 1	0:21:16	88
1750	50006	0.03	6730.6 1	0:24:11	88
1775	50017.1	0.04	6730.5 1	0:26:19	88
1800	49984.7	0.04	6729.1 1	0:32:26	88
1825	50007.3	0.03	6729.0 1	0:33:26	88
1850	50004.3	0.05	6728.8 1	0:34:50	88
1875	50007	0.04	6728.6 1	0:35:58	88
1900	50001	0.04	6728.4 1	0:37:01	88
1925	49992.7	0.04	6728.0 1	0:38:34	88
1950	50002.1	0.04	6727.9 1	0:39:35	88
1975	50005.3	0.04	6727.7 1	0:40:30	88
2000	50002.1	0.05	6727.5 1	0:41:29	88

Line 25+5 0N D ate 11-Jul-96 #75					
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2000	50048	0.04	6727.1 1	0:43:36	88

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## TEU10

Line -30+	25N	Date	22-Jul	96 #1	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
1800	50083.2	0.04	6739.9	9:33:25	88
1825	50085.8	0.04	6739.8	9:34:17	88
1850	50086.8	0.04	6739.7	9:35:26	88
1875	50074.6	0.04	6739.5	9:36:16	88
1900	50066.9	0.04	6739.5	9:37:00	88
1925	50063.5	0.04	6739.4	9:38:13	88
1950	50076.8	0.04	6739.4	9:39:18	88
1975	50072.3	0.04	6739.3	9:40:59	88
2000	50014.2	0.04	6738.5	9:53:31	88
2025	50064.2	0.03	6738.4	9:54:34	88
2050	50048.8	0.04	6738.4	9:55:28	88
2075	50047.7	0.04	6738.4	9:57:17	88
2100	50049.6	0.04	6738.2	9:58:47	88
2125	50056.2	0.04	6738.1	9:59:56	88
2150	50056.7	0.03	6738.1	10:00:45	88
2175	50046.9	0.04	6738.1	10:01:36	88
2200	50037.5	0.04	6738.1	10:02:29	88
2225	50052	0.03	6738.1	10:03:13	88
2250	50071.4	0.03	6737.8	10:05:02	88
2275	50058.2	0.04	6737.8	10:05:42	88
2300	50050.1	0.04	6737.7	10:06:29	88
2325	50037.5	0.03	6737.4	10:07:53	88
2350	50052.6	0.04	6737.4	10:09:22	88
2375	50057.5	0.03	6737.3	10:10:04	88
2400	50040	0.06	6737.5	10:10:49	88
2425	50042.8	0.04	6737.5	10:11:34	88
2450	50056.3	0.03	6737.3	10:12:19	88
2475	50047.1	0.03	6737.2	10:13:22	88
2500	50054.5	0.04	6737.3	10:14:32	88

Line -30+	00N	Date	22-Jul	96 #30	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2500	50069.5	0.05	6736.7	10:16:09	88
-2475	50071.5	0.04	6736.5	10:17:26	88
-2450	50075.9	0.03	6736.4	10:18:02	88
-2425	50080.9	0.04	6736.5	10:18:46	88
-2400	50045	0.04	6736.2	10:20:02	88
-2375	50048.2	0.03	6736	10:20:53	88
-2350	50055.3	0.05	6735.9	10:21:36	88
-2325	50044.2	0.04	6736	10:22:21	88
-2300	50043.9	0.03	6736.2	10:23:15	88
-2275	50044.4	0.04	6736.5	10:24:23	88
-2250	50050.4	0.05	6736.2	10:25:35	88
-2225	50039.1	0.04	6735.9	10:26:51	88
-2200	50044.4	0.04	6735.6	10:28:03	88
-2175	50057.3	0.04	6735.4	10:29:34	88
-2150	50052.5	0.04	6735.6	10:30:49	88
-2125	50041.4	0.04	6735.3	10:33:20	88
-2100	50059.4	0.03	6734.8	10:35:58	88
-2075	50049.3	0.04	6734.5	10:37:54	88

TEU10

-2050	50048	0.04	6734.5	10:39:31	88
-2025	50064.8	0.03	6734.5	10:40:32	88
-2000	50066.9	0.04	6734.5	10:42:04	88
-1975	50078	0.03	6734.5	10:42:54	88
-1950	50137.5	0.81	6734.2	10:44:13	58
-1925	50100.5	0.04	6734.1	10:45:08	88
-1900	50101.8	0.04	6734.2	10:46:01	88
-1875	50075.2	0.03	6734.2	10:46:48	88
-1850	50072.2	0.04	6734.1	10:47:33	88

Line -29+	75N	Date	22-Jul	96 #57	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
1850	50069.3	0.03	6734	10:51:16	88
1875	50062.8	0.03	6734.3	10:52:25	88
1900	50069.6	0.03	6734.2	10:53:15	88
1925	50075.8	0.04	6734.8	10:54:01	88
1950	50094.7	0.04	6734.3	10:54:47	88
1975	50191.4	0.04	6734.1	10:55:32	88
2000	50048.6	0.03	6734.2	10:56:32	88
2025	50042.2	0.05	6734.2	10:57:38	88
2050	50048.1	0.03	6734.2	10:59:26	88
2075	50061	0.04	6734.2	11:00:59	88
2100	50045	0.03	6734.3	11:02:15	88
2125	50047.6	0.04	6734.3	11:03:11	88
2150	50043	0.03	6734.7	11:04:06	88
2175	50048.6	0.04	6734.6	11:06:15	88
2200	50045.8	0.04	6734.7	11:07:07	88
2225	50038.1	0.04	6734.4	11:08:03	88
2250	50037.1	0.04	6734	11:09:02	88
2275	50038.1	0.04	6734	11:09:49	88
2300	50048.6	0.04	6734.1	11:10:27	88
2325	50041.7	0.04	6733.9	11:11:15	88
2350	50036.6	0.03	6733.5	11:12:03	88
2375	50041.8	0.04	6733.5	11:12:50	88
2400	50038.1	0.04	6733.3	11:13:35	88
2425	50038.1	0.03	6732.5	11:15:22	88
2450	50060	0.03	6732.3	11:16:42	88
2475	50046.7	0.04	6731.9	11:18:14	88
2500	50053.5	0.03	6731.3	11:19:54	88

Line -29+	50N	Date	22-Jul	96 #84	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2500	50061.2	0.03	6728.7	11:33:49	88
-2475	50074.4	0.03	6728.5	11:34:58	88
-2450	50074.4	0.03	6728.4	11:35:52	88
-2425	50067.2	0.03	6728.1	11:37:04	88
-2400	50057.4	0.03	6727.9	11:39:01	88
-2375	50044.7	0.03	6727.9	11:39:45	88
-2350	50050.5	0.05	6727.8	11:40:30	88
-2325	50050.2	0.04	6727.6	11:41:25	88
-2300	50046.2	0.04	6727.4	11:42:09	88
-2275	50030.6	0.03	6727.2	11:43:24	88
-2250	50047.8	0.22	6726.2	11:47:04	48

TEU10

-2225	50027.5	0.03	6725.8	11:49:39	88
-2200	50057.7	0.04	6725.9	11:51:03	88
-2175	50055.4	0.03	6725.7	11:52:50	88
-2150	50054	0.04	6725.6	11:55:43	88
-2125	50044.2	0.03	6725.5	11:58:03	88
-2100	50074.3	0.05	6725.4	11:59:57	88
-2075	50050.5	0.04	6725.7	12:01:33	88
-2050	50063.7	0.04	6724.6	12:02:52	88
-2025	50059.8	0.04	6724.4	12:03:34	88
-2000	50061.1	0.04	6725.2	12:04:37	88
-1975	50094.5	0.04	6726.1	12:05:33	88
-1950	50070.5	0.03	6726.3	12:07:03	88
-1925	50065.5	0.04	6725.6	12:08:17	88
-1900	50068.9	0.03	6724.8	12:09:36	88
-1875	50076.5	0.04	6724.5	12:10:28	88
-1850	50094.3	0.04	6723.9	12:11:33	88
-1825	50081.6	0.03	6723.3	12:12:25	88
-1800	50086.4	0.04	6722.9	12:13:12	88

Line -29+	25N	Date	22-Jul	96 #113	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
1800	50071.2	0.05	6722.5	12:14:02	88
1825	50061.6	0.04	6721.1	12:16:32	88
1850	50075.7	0.04	6720.2	12:17:30	88
1875	50078.2	0.03	6719.1	12:18:47	88
1900	50082.8	0.05	6719.2	12:20:24	88
1925	50059.6	0.03	6719	12:21:24	88
1950	50056.4	0.04	6719.5	12:26:01	88
1975	50046.2	0.04	6719.6	12:27:34	88
2000	50127.3	0.03	6718.9	12:29:27	88
2025	50022.8	0.04	6718.4	12:30:59	88
2050	50031.4	0.03	6717.9	12:32:24	88
2075	50033.8	0.04	6717.1	12:34:39	88
2100	50040.2	0.03	6716.6	12:36:14	88
2125	50000.7	0.23	6716.5	12:37:10	88
2150	50049.9	0.03	6716.6	12:38:21	88
2175	50028.1	0.03	6716.3	12:40:29	88
2200	50002.4	0.03	6716.3	12:42:01	88
2225	50037.3	0.03	6716.5	12:43:22	88
2250	50030.5	0.03	6716.7	12:44:43	88
2275	50024.2	0.03	6717.1	12:46:09	88
2300	50018.8	0.04	6717.3	12:47:08	88
2325	50031.3	0.03	6717.8	12:48:09	88
2350	50032.1	0.03	6718.3	12:48:59	88
2375	50027.4	0.04	6718.4	12:49:50	88
2400	50028.2	0.03	6718.7	12:50:35	88
2425	50031.9	0.04	6719.1	12:51:43	88
2450	50043.7	0.03	6719.4	12:52:41	88
2475	50032	0.04	6719.7	12:53:24	88
2500	50030	0.04	6719.1	12:54:30	88

Line -29+	00N	Date	22-Jul	96 #141	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT

TEU10

-2500	50055.2	0.04	6720.2	12:55:53	88
-2475	50043.2	0.03	6720.3	12:56:41	88
-2450	50048.1	0.04	6720.4	12:57:23	88
-2425	50037.6	0.03	6720.5	12:58:07	88
-2400	50048.1	0.03	6720.8	12:58:54	88
-2375	50045.8	0.03	6720.9	12:59:37	88
-2350	50027.7	0.03	6720.8	13:00:32	88
-2325	50046.1	0.03	6721.2	13:06:03	88
-2300	50064.6	0.07	6721.4	13:07:05	88
-2275	50046.6	0.05	6721.8	13:08:05	88
-2250	50012.2	0.04	6722.4	13:12:27	88
-2225	50019.5	0.03	6722.4	13:15:46	88
-2200	50035.8	0.04	6723.2	13:19:32	88
-2175	50029	0.03	6724.6	13:22:18	88
-2150	50031.5	0.03	6724.7	13:23:22	88
-2125	50019.7	0.04	6724.7	13:25:46	88
-2100	50027.5	0.03	6725.1	13:30:00	88
-2075	50039.7	0.04	6725.2	13:31:51	88
-2050	50022.8	0.06	6725.3	13:32:59	88
-2025	50035.2	0.03	6725.3	13:34:17	88
-2000	50022.4	0.03	6725.2	13:35:38	88
-1975	50039.7	0.03	6725	13:39:52	88
-1950	50045.5	0.07	6724.7	13:41:03	88
-1925	50048.6	0.03	6724.5	13:42:18	88
-1900	50059.4	0.04	6724.2	13:46:39	88
-1875	50070.4	0.03	6724.6	13:48:56	88
-1850	50105.7	0.03	6724.5	13:50:39	88
-1825	50109.7	0.03	6724.2	13:52:21	88
-1800	50067.2	0.08	6724.3	13:53:19	88
Line -28+	75N	Date	22-Jul	96 #170	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
1800	50061.4	0.04	6724.4	13:54:10	88
1825	50054.7	0.04	6724.9	13:56:36	88
1850	50048.3	0.04	6725.3	13:58:10	88
1875	50047.8	0.04	6724.8	14:17:11	88
1900	50040.6	0.03	6724.9	14:18:12	88
1925	50043.4	0.04	6724.7	14:19:59	88
1950	50039	0.04	6724.8	14:20:53	88
1975	50041.6	0.03	6724.8	14:21:53	88
2000	50032.7	0.05	6725.2	14:23:08	88
2025	50030.8	0.03	6725.2	14:23:52	88
2050	50027.3	0.03	6725	14:24:45	88
2075	50017.8	0.04	6724.9	14:25:33	88
2100	50021	0.05	6724.9	14:27:06	88
2125	50025.3	0.04	6725	14:28:27	88
2150	50018.9	0.04	6725	14:29:19	88
2175	50023	0.04	6725	14:30:29	88
2200	50027.4	0.03	6725.4	14:31:31	88
2225	50034.2	0.04	6725.7	14:33:11	88
2250	50019.7	0.04	6726	14:34:09	88
2275	50005.1	0.03	6726.4	14:35:57	88

TEU10

2300	50009.2	0.04	6726.5	14:36:42	88
2325	50016.9	0.03	6726.4	14:37:37	88
2350	50025	0.03	6726.5	14:38:30	88
2375	50012.1	0.04	6726.5	14:39:31	88
2400	50011.1	0.05	6726.3	14:40:09	88
2425	50012	0.04	6726.3	14:40:57	88
2450	50013.2	0.03	6726	14:41:52	88
2475	50014.6	0.03	6725.9	14:42:42	88
2500	50008.4	0.04	6725.9	14:43:42	88
Line -28+	50N	Date	22-Jul	96 #199	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2500	50029.4	0.03	6725.8	14:44:28	88
-2475	50033.6	0.03	6725.7	14:45:14	88
-2450	50024.8	0.04	6725.7	14:45:59	88
-2425	50030.8	0.03	6725.9	14:46:42	88
-2400	50027.8	0.03	6726	14:47:27	88
-2375	50029.9	0.03	6726.1	14:48:04	88
-2350	50027.8	0.03	6726.2	14:48:56	88
-2325	50016	0.04	6726.6	14:49:47	88
-2300	50014.4	0.03	6726.8	14:50:34	88
-2275	50008.8	0.03	6727.4	14:53:17	88
-2250	50006.4	0.04	6727.8	14:54:54	88
-2225	50009.2	0.03	6728.2	14:56:32	88
-2200	50011.9	0.03	6728.7	14:57:39	88
-2175	50010.4	0.03	6729.1	14:59:22	88
-2150	50012.2	0.03	6729.7	15:01:21	88
-2125	50021.9	0.03	6730.1	15:03:30	88
-2100	50014.2	0.04	6730.5	15:06:49	88
-2075	50024.5	0.04	6731	15:11:10	88
-2050	50040.5	0.04	6731.2	15:12:15	88
-2025	50036.8	0.03	6731.6	15:13:10	88
-2000	50040	0.03	6731.9	15:14:16	88
-1975	50030.9	0.03	6732	15:15:17	88
-1950	50047.6	0.03	6732	15:16:17	88
-1925	50042.7	0.04	6732.2	15:17:24	88
-1900	50034.4	0.04	6732.1	15:18:25	88
-1875	50059.8	0.03	6732	15:19:26	88
-1850	50046.5	0.04	6732.3	15:20:28	88
-1825	50070.7	0.03	6732.8	15:21:36	88
-1800	50062.4	0.03	6733.1	15:22:29	88
Line -28+	25N	Date	22-Jul	96 #228	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
1800	50062.1	0.03	6733.6	15:24:13	88
1825	50045.8	0.03	6733.9	15:25:06	88
1850	50041.5	0.03	6734.4	15:26:52	88
1875	50036.9	0.04	6734.6	15:27:37	88
1900	50041.2	0.04	6734.7	15:28:45	88

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## TEU11

Line -28+	25N	Date	23-Jul	96 #1	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
1875	50035.8	0.09	6727.6	11:59:03	88
1900	50033.3	0.03	6727.2	12:05:05	88
1925	50036.2	0.03	6726.9	12:06:29	88
1950	50030.2	0.03	6726.5	12:07:20	88
1975	50019.9	0.03	6726.1	12:08:08	88
2000	50033	0.03	6725.8	12:08:59	88
2025	50040	0.03	6725.5	12:10:02	88
2050	50035.7	0.04	6725.1	12:10:48	88
2075	50019.4	0.04	6724.7	12:11:31	88
2100	50007.8	0.03	6724.4	12:12:48	88
2125	50011.5	0.04	6724.2	12:13:40	88
2150	50013.7	0.03	6724.2	12:16:55	88
2175	49998.6	0.04	6724.4	12:18:15	88
2200	50013.4	0.03	6724.4	12:19:12	88
2225	50006.2	0.03	6724.4	12:19:55	88
2250	50015.3	0.04	6724.1	12:21:02	88
2275	50011	0.05	6724.2	12:22:55	88
2300	50003.8	0.03	6724.2	12:23:29	88
2325	50002.4	0.04	6724	12:24:37	88
2350	50002.9	0.04	6724.1	12:25:36	88
2375	50005.3	0.04	6724.2	12:26:29	88
2400	50009.1	0.03	6724.1	12:27:31	88
2425	50019.8	0.03	6724	12:28:38	88
2450	50019	0.04	6724	12:29:27	88
2475	50015.5	0.03	6723.8	12:30:40	88
2500	50013.9	0.03	6723.9	12:31:52	88

Line -28+	00N	Date	23-Jul	96 #27	
POSITIO	FIELD	ERR	DRIFT	TIME	DS CULT
-2500	50024.7	0.03	6724.1	12:32:47	88
-2475	50033.6	0.03	6724.3	12:33:54	88
-2450	50020.2	0.03	6724.8	12:35:28	88
-2425	50016.6	0.03	6725.1	12:36:30	88
-2400	50011.5	0.03	6725.2	12:37:22	88
-2375	50008.8	0.04	6725.4	12:38:23	88
-2350	50009.3	0.03	6725.8	12:39:54	88
-2325	49998.5	0.03	6726.9	12:41:20	88
-2300	50002.1	0.04	6727.4	12:42:38	88
-2275	49998	0.05	6727.5	12:43:38	88
-2250	49992.1	0.04	6727.1	12:45:40	88
-2225	50008.4	0.03	6727.1	12:46:51	88
-2200	50023.2	0.03	6727	12:48:19	88
-2175	50006.2	0.04	6727	12:50:06	88
-2150	50009.8	0.09			

## TEU12

Line -21+	00N	Date	25-Jul	96	#1	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-1900	49860.8	0.04	6744.2	9:16:47	88	
-1875	49959.3	0.04	6743.7	9:18:24	88	
-1850	49943.5	0.04	6743.5	9:20:04	88	
-1825	49963.5	0.04	6743.6	9:22:21	88	
-1800	49990	0.04	6743.7	9:24:57	88	
-1775	49972.2	0.03	6743.7	9:28:28	88	
-1750	49995.9	0.03	6743.6	9:29:19	88	
-1725	50027.1	0.04	6743.7	9:30:17	88	
-1700	49983.1	0.04	6743.9	9:31:29	88	
-1675	49983.8	0.04	6743.8	9:32:50	88	
-1650	49989.1	0.03	6743.7	9:33:48	88	
-1625	49990.8	0.04	6743.7	9:34:52	88	
-1600	50024.8	0.04	6743.2	9:37:04	88	
-1575	50132.3	0.04	6742.5	9:40:22	88	
-1550	49927.9	0.04	6742	9:42:35	88	
-1525	49906.7	0.04	6741.8	9:43:28	88	
-1500	49894.8	0.06	6741.6	9:44:35	88	
Line -20+	75N	Date	25-Jul	96 #	18	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1500	49904.7	0.04	6740.8	9:48:05	88	
1525	49904.8	0.04	6741.2	9:49:24	88	
1550	49910.2	0.04	6741.2	9:50:32	88	
1575	49931.7	0.04	6741.2	9:51:36	88	
1600	49942.5	0.04	6741.3	9:52:39	88	
1625	49976.7	0.04	6741.1	9:54:05	88	
1650	50000.1	0.04	6740.7	9:55:15	88	
1675	49982.3	0.03	6740.5	9:56:37	88	
1700	49999.7	0.03	6740.3	9:57:53	88	
1725	49957.9	0.04	6739.8	9:58:55	88	
1750	49996.5	0.03	6739.6	10:00:17	88	
1775	49983	0.04	6739.5	10:01:51	88	
1800	49972.5	0.04	6739.9	10:02:41	88	
1825	49962.6	0.03	6740.2	10:03:29	88	
Line -20+	50N	Date	25-Jul	96 #	32	
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-1825	49970.8	0.03	6740.4	10:04:29	88	
-1800	49967	0.04	6740.7	10:05:27	88	
-1775	49977.2	0.04	6741	10:06:39	88	
-1750	49976.7	0.04	6741.1	10:07:29	88	
-1725	49995.9	0.04	6741.1	10:08:19	88	
-1700	49996	0.02	6740.7	10:09:37	88	
-1675	50003.2	0.04	6740.6	10:10:31	88	
-1650	50022.1	0.03	6740.4	10:11:38	88	
-1625	49993.6	0.04	6740.2	10:12:31	88	
-1600	49954.8	0.05	6740.1	10:13:41	88	
-1575	49948.5	0.04	6740	10:14:30	88	
-1550	49942.4	0.05	6739.9	10:15:14	88	
-1525	49958.5	0.3	6739.2	10:17:25	68	
-1500	49954.9	0.04	6738.7	10:18:15	88	



Line -20+	25N	Date	25-Jul	96 #	46
POSITIO	FIELD	ERR	DRIFT	TIME	DS
					CULT
1500	49983.3	0.03	6738.3	10:19:22	88
1525	49979	0.04	6738.1	10:20:22	88
1550	49981.4	0.03	6737.9	10:21:27	88
1575	50001.2	0.04	6737.5	10:22:41	88
1600	50005.9	0.04	6737.3	10:24:00	88
1625	50039.2	0.04	6737.1	10:25:22	88
1650	50021.2	0.05	6736.2	10:27:09	88
1675	50011.2	0.06	6735.6	10:28:26	88
1700	50049.5	0.04	6735	10:29:39	88
1725	50029	0.04	6734.4	10:30:44	88
1750	50010.8	0.03	6734	10:31:42	88
1775	50021.1	0.03	6734.1	10:32:41	88
1800	50071	0.44	6735.1	10:34:26	48
1825	49970.7	0.04	6735.7	10:35:29	88

Line -20+	00N	Date	25-Jul	96 #	60
POSITIO	FIELD	ERR	DRIFT	TIME	DS
					CULT
-1825	49980.6	0.03	6736.1	10:44:05	88
-1800	49976.6	0.03	6735	10:46:03	88
-1775	49980.9	0.03	6734.5	10:47:21	88
-1750	49972	0.04	6732.7	10:53:28	88
-1725	50029.5	0.03	6732.9	10:54:23	88
-1700	50033.5	0.05	6732.9	10:55:14	88
-1675	50052.5	0.03	6732.8	10:56:05	88
-1650	50020.2	0.04	6732.7	10:56:54	88
-1625	50085.6	0.04	6732.9	10:58:00	88
-1600	50060.1	0.04	6732.4	11:02:25	88
-1575	50109.3	0.03	6732.7	11:03:30	88
-1550	50033.9	0.03	6732.4	11:05:00	88
-1525	50092.8	0.03	6732.4	11:05:57	88
-1500	50164.5	0.03	6732	11:06:54	88

Line -19+	75N	Date	25-Jul	96 #	74
POSITIO	FIELD	ERR	DRIFT	TIME	DS
					CULT
1500	50363.6	0.03	6731.8	11:08:33	88
1525	50224.7	0.04	6731.1	11:10:58	88
1550	50123.4	0.04	6731	11:11:59	88
1575	50100.6	0.03	6730.8	11:12:59	88
1600	50115.2	0.04	6730.3	11:14:27	88
1625	50016.4	0.03	6730.1	11:15:15	88
1650	50009.2	0.03	6729.8	11:16:12	88
1675	49959.2	0.04	6729.5	11:17:08	88
1700	49979.5	0.04	6729.4	11:17:57	88
1725	50100	0.04	6729.3	11:18:52	88
1750	50005.3	0.04	6729	11:19:42	88
1775	50047.6	0.04	6728.9	11:20:41	88
1800	49968.3	0.03	6728.8	11:21:47	88
1825	49957.2	0.03	6728.5	11:22:56	88

Line -19+	50N	Date	25-Jul	96 #	88
POSITIO	FIELD	ERR	DRIFT	TIME	DS
					CULT
-1800	50098.3	0.04	6728.5	11:24:33	88

TEU12

-1775	50052.7	0.05	6728.2	11:26:56	88
-1750	49991.5	0.03	6727.6	11:28:19	88
-1725	49996.9	0.03	6727.4	11:29:43	88
-1700	49989.5	0.04	6727.5	11:31:08	88
-1675	49973.2	0.04	6727.3	11:32:02	88
-1650	50002.5	0.03	6727.2	11:32:50	88
-1625	50067.2	0.03	6727.1	11:33:50	88
-1600	50189.5	0.03	6726.7	11:35:19	88
-1575	50089.6	0.04	6726.4	11:36:26	88
-1550	50107.6	0.04	6726.2	11:37:20	88
-1525	50125.6	0.03	6726	11:38:22	88
-1500	51231.7	0.05	6725.9	11:40:35	88

Line -19+	25N	Date	25-Jul	96 #1		1
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
1500	50590.7	0.04	6725.3	11:43:01	88	
1525	50094.9	0.05	6725.1	11:44:05	88	
1550	50091.6	0.04	6725.2	11:45:06	88	
1575	50151.7	0.03	6724.9	11:46:05	88	
1600	49926.3	0.04	6724.5	11:47:27	88	
1625	49877	0.04	6724.7	11:48:22	88	
1650	49971	0.04	6724.3	11:50:23	88	
1675	49959.1	0.05	6724.2	11:51:17	88	
1700	49959.8	0.09	6724.1	11:52:16	88	
1725	49927.2	0.04	6723.7	11:54:56	88	
1750	49915.8	0.05	6723.7	11:56:10	88	
1775	49936.5	0.03	6723.9	11:57:12	88	
1800	49913.8	0.04	6724	11:58:13	88	

Line -19+	00N	Date	25-Jul	96 #1		14
POSITIO	FIELD	ERR	DRIFT	TIME	DS	CULT
-1800	49938.4	0.03	6723.9	12:00:49	88	
-1775	49961.8	0.04	6724	12:02:13	88	
-1750						

Appendix X  
Downhole IP Report

LOGISTICAL REPORT  
DOWNHOLE INDUCED POLARIZATION SURVEY

CLONE PROJECT  
STEWART AREA, BRITISH COLUMBIA

on behalf of

TEUTON RESOURCES CORP.  
509 - 675 West Hastings Street  
Vancouver, B.C. V6B 1N2

Field work completed: September 21-30, 1996

by

Alan Scott, Geophysicist  
SCOTT GEOPHYSICS LTD.  
4013 West 14th Avenue  
Vancouver, B.C. V6R 2X3

October 2, 1996

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	page
1 Introduction	1
2 Survey coverage and data presentation	1
3 Personnel	2
4 Instrumentation	2
5 Discussion of Results	2
6 Recommendations	5

### Appendix

Statement of Qualifications	rear of report
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### Maps and Materials included in body of report

Chargeability/normalized primary voltage logs - ddh CL96-19	map pocket 1
Chargeability/normalized primary voltage logs - ddh CL96-25	map pocket 1
Chargeability/normalized primary voltage logs - ddh CL96-29	map pocket 1
Chargeability/normalized primary voltage logs - ddh CL96-30	map pocket 1
Chargeability/normalized primary voltage logs - ddh CL96-43	map pocket 1
Final edited data listings	map pocket 2
One (1) floppy disk with all survey data	map pocket 3

### Accompanying Maps

(vellum originals, three blackline copies of each)

Chargeability/normalized primary voltage logs - ddh CL96-19	map roll
Chargeability/normalized primary voltage logs - ddh CL96-25	map roll
Chargeability/normalized primary voltage logs - ddh CL96-29	map roll
Chargeability/normalized primary voltage logs - ddh CL96-30	map roll
Chargeability/normalized primary voltage logs - ddh CL96-43	map roll

## 1. INTRODUCTION

Downhole induced polarization surveys (DHIP surveys) were performed at the Clone Project, Stewart Area, B.C., within the period September 21-30, 1996. The survey was conducted by Scott Geophysics Ltd. on behalf of Teuton Resources Corp.

An axial gradient array was used for the directional DHIP survey. The current electrode sources were located at the surface and the axial gradient measurements were taken within the boreholes at an "a" spacing of 20 metres and at a data interval of 5 m.

This report describes the instrumentation and procedures, presents the results of the survey, and gives a brief discussion of those results.

## 2. SURVEY COVERAGE AND DATA PRESENTATION

Five boreholes were surveyed at the Clone Project, namely CL96-19, 25, 29, 30, and 43. The following table summarizes the location of the surface electrodes and depth of survey for each borehole. A common remote electrode, which was located some 1200 metres north of the survey area, was used for all the borehole logs.

ddh	True Azimuth	Grid Azimuth	Inclination (from horiz.)	Current source locations (w.r.t. Grid Azimuth)	Depth Surveyed
CL96-19	220	265	-65	100N, 100E, 100S, 100W	15-165 m
CL96-25	65	110	-80	100N, 100E, 100S, 100W	15-165 m
CL96-29	245	290	-75	100N, 100E, 100S, 100W	15-165 m
CL96-30	65	110	-70	100N, 100E, 100S 200N, 200E, 200S	15-270 m 15-270 m
CL96-43	245	290	-75	100N, 100E, 100S, 100W	15-215 m

Ideally, each hole would have been surveyed with sources at both 100 and 200 m in all four directions, but topography restricted access to those locations noted above.

The results are presented as profiles of the chargeability (IP), in units of mV/Volt and of the normalized primary voltage (Vp), in units of mV/Amp. The latter can be considered a proxy for the resistivity. It is the primary voltage measured when the current is on per amp of transmitted current. Resistivities have not been computed at this time since this will require detailed consideration of the surface topography.

The profiles for each borehole are located in map pocket 1 at the rear of this report. They have been plotted at a depth scale of 1:1000. The profile scales are 10 mV/V per cm for the IP and 200 mV/Amp per cm for the normalized Vp. The legends give additional details on the form of presentation for each of the plots.

Map pocket 2 contains a listing of the final edited data. The data disk in map pocket 3 has ASCII format files for each of these edited listings. It also contains the raw survey data (\DAT) and SURFER format plot files for each of the plots accompanying this report (\PLOTS).

### 3. PERSONNEL

Jim Hawkins, Geophysicist, was the party chief on the survey on behalf of Scott Geophysics Ltd. Ed Kruchkowski, Geologist, was the representative on site on behalf of Teuton Resources Corp.

### 4. INSTRUMENTATION

A Scintrex IPR12 receiver and IRIS VIP3000 (3.0 kw) transmitter along with a downhole IP system custom built to Scott Geophysics specifications were used for the DHIP survey. Readings were taken in the time domain using a 2 second current pulse (0.125 Hz). The chargeability plotted on the accompanying logs is for the interval 690-1050 msec after shutoff.

### 4. DISCUSSION OF RESULTS

The discussion of results in this report gives a preliminary assessment of the survey. It is intended to draw attention to the main chargeability (IP) highs detected on the survey, in case they are of interest to the present drilling program. Additional interpretation, including calculation of the apparent resistivities and correlation to the geological logs, is recommended prior to the next drilling stage.

In general, the interpretation is based on the fact that the IP response will be stronger for a current electrode that is located on the same side as the chargeable body than for the current electrode located on the opposite side. This general rule, however, is subject to two main constraints. Firstly, the dip of the body w.r.t. the borehole axis and the surface will effect the response, and secondly, the primary field will be near zero at critical geometric points. Such critical points occur where a line from that point within the borehole to the relevant current electrode is approximately normal to the borehole axis. The resulting very low primary voltages can lead to unreliable IP measurements. In addition, the critical points may be offset somewhat from that geometric location, depending on resistivity variations within the geoelectric section and surface topography.

To avoid misinterpretation due to dipping bodies, and to ensure there will be an independent current source at any critical depth point, it is better to have at least two separate current sources in each direction. The terrain rendered this impractical for the present survey.

The following discussion of the results, therefore, only treats those IP responses which appear to be very well defined and are not likely to be associated with critical geometric points.

DDH CL96-19:

A strong IP high was detected at the top of the surveyed portion of CL96-19. It is interpreted to indicate a near surface source extending preferentially to the west of the borehole axis, which would be up and to the west, since the borehole was drilled to the grid west.

The negative normalized Vp response at about 50m on the S log is probably located near a critical geometric point.

A broad, moderate IP high was detected at a depth of some 100m on the current west log for ddh CL96-19, with only background or weak IP response on the other directional logs. It is interpreted to indicate the presence of a target at that depth to the west of hole CL96-19.

A broad weak IP high was detected at about 140m depth. The response is slightly higher on the S and E logs versus the N and W logs, suggesting a weakly chargeable zone which extends preferentially to the S and E.

It suggests the presence of a weak chargeable zone, but no preferred direction is indicated.

DDH CL96-25:

The negative normalized Vp responses at about 25m on the S log, and at about 55m and 70m on the E logs, are probably related to a critical geometric point.

A broad, moderate IP high was detected at a depth of some 130m on all the directional logs in ddh CL96-25. The amplitude is somewhat higher on the E versus the W log, and slightly higher on the N versus the S log. This suggests that a target lies, or extends preferentially, at about that depth to the east, and perhaps to the north, of CL96-25.

DDH CL96-29:

The negative normalized Vp response at about 50m on the S log is probably located near a critical geometric point. Further evaluation is required before offering an opinion on whether the IP high on the S log immediately below that is related to a critical point or indicates a source to the S.

A broad, moderate IP high was detected at a depth of some 85m on all the directional logs in ddh CL96-29. The amplitude differences for the N versus S and E versus W logs are not large, and further evaluation is required before inferring a preferred direction.

A weak IP high was detected at a depth of some 140m on the W and N logs, with only background response on the E and S logs. This suggests that a target lies at that depth to the NW of CL96-29.



DDH CL96-30:

The negative normalized Vp response in the vicinity of 50m depth is probably located near the critical geometric point for the 100m current electrodes.

A moderate IP high was detected at about 90m in CL96-30 on the 200S and 200E logs and at about 100m on the 100S and 100E logs. This suggests a target lies at about that depth to the S and E. This response may, however, be associated with a critical point for the 200m electrodes, as suggested by the negative normalized Vp at about 100m on the S and E logs.

A narrow, strong IP high was detected at a depth of some 150 m on the 200E log. It gives a weak response on the 100E log and a broad, weak response on the 100S and 200S logs. It is interpreted as indicating a source which extends preferentially to the S and E.

A strong IP high was detected at a depth of some 210m on the 200E log. It gives a weak response on the 100E log and only background response on the N and S logs. This suggests a target lies at that depth to the E of CL96-30, most probably dipping upwards towards the 200m E electrode. West logs were not obtained in CL96-30 due to the presence of a canyon.

DDH CL96-43:

A strong IP high was detected on the W log at the top of the surveyed portion of CL96-43. It is interpreted to indicate a near surface source extending preferentially to the W of the borehole.

The negative normalized Vp response at about 50m on the S and W logs are probably located near a critical geometric point.

A broad, moderate IP high was detected at a depth of some 110m on the W and N logs for CL96-43, with broad, weak IP highs at 130m on the S and E logs. It is interpreted to indicate the presence of a target at that depth that extends preferentially to the W and N of CL96-43.

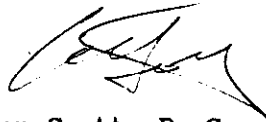
A broad, weak IP high was detected at a depth of some 195m on all logs. It is interpreted to represent a weakly chargeable zone with no preferred direction.

5. RECOMMENDATIONS

A preliminary evaluation of the results of the downhole IP survey at the Clone Project has suggested preferred directions for several targets, as described in the preceding Discussion of Results. Correlation of these suggested targets to the geological logs is required before any specific target could be recommended for additional drilling.

Subject to that geological evaluation, and the results of any additional drilling, a detailed interpretation of these results, including calculation of the apparent resistivities, is recommended.

Respectfully Submitted,

A handwritten signature in black ink, appearing to read 'Alan Scott', written in a cursive style.

Alan Scott, P. Geos.

Statement of Qualifications

for

Alan Scott, Geophysicist

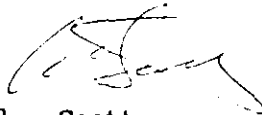
of

4013 West 14th Avenue  
Vancouver, B.C. V6R 2X3

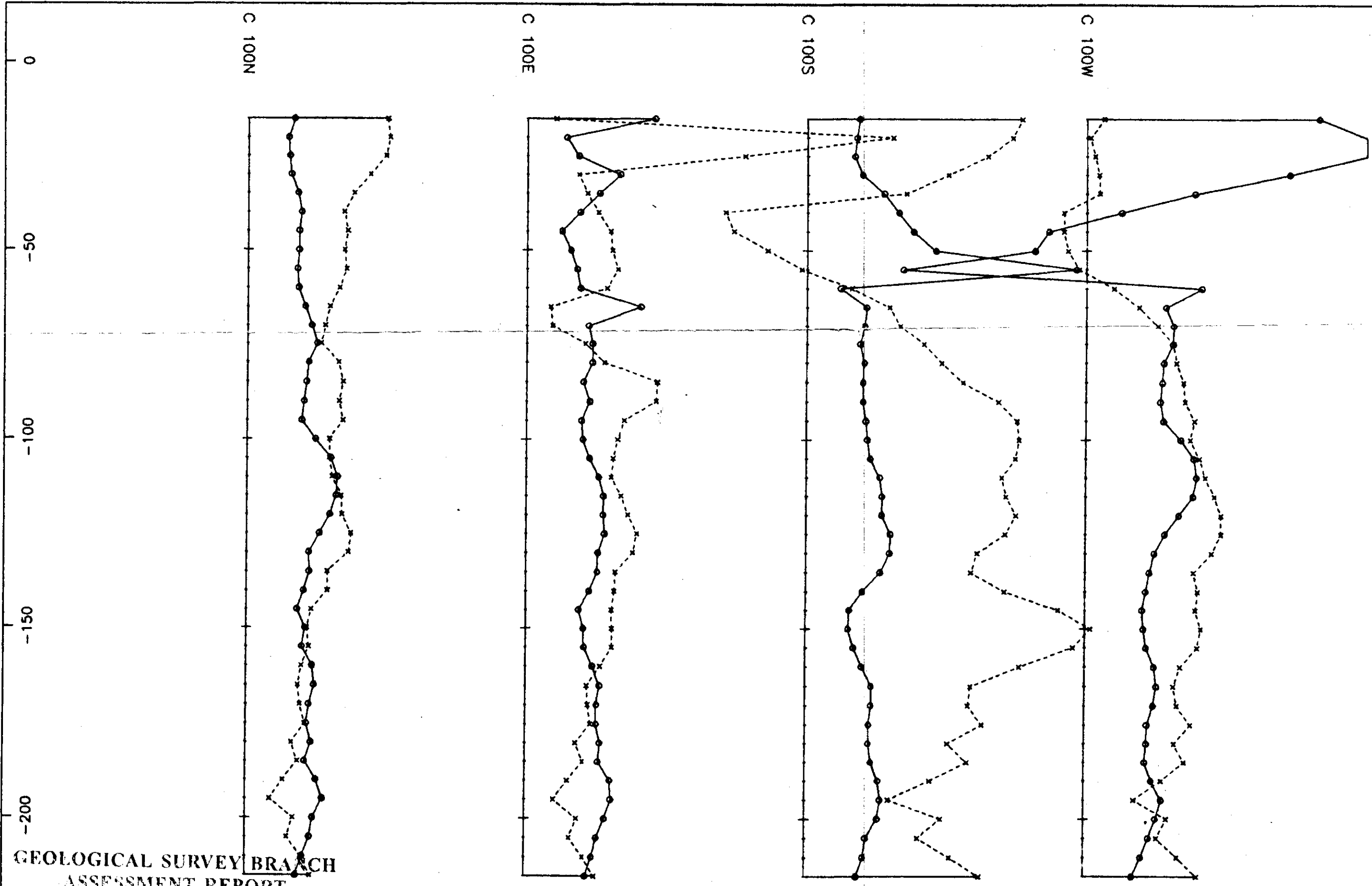
I, Alan Scott, hereby certify the following statements regarding my qualifications, and my involvement in the program of work described in this report.

1. The work was performed by individuals sufficiently trained and qualified for its performance.
2. I have no material interest in the property under consideration in this report, nor in the company on whose behalf the work was performed.
3. I graduated from the University of British Columbia with a Bachelor of Science degree (Geophysics) in 1970, and with a Master of Business Administration degree in 1982.
4. I am a member of the Association of Professional Engineers and Geoscientists of the Province of British Columbia.
5. I have been practicing my profession as a Geophysicist in the field of Mineral Exploration since 1970.

Respectfully submitted,



Alan Scott



CL96-43 Az 245, Dip -75, Depth 223m

Directional Array:  
 receiver Scintrex IPR12  
 pulse time 2 seconds  
 Mx window 690-1050 msecs

transmitter array Iris VIP 3000 (3kw)  
 axial gradient  
 a spacing 20 meters  
 C2 (for current) > 1200 m North

C1 (Grid coordinate w.r.t. collar):  
 Log #1 C1 100N  
 Log #2 C1 100E  
 Log #3 C1 100S  
 Log #4 C1 100W

Grid North 315 degrees

o—o chargeability  
 scale 10 mV/V /cm

x - x normalized VP  
 scale 200 mV/amp /cm.

positive to right of graph

chargeability values truncated at 75 mV/V

0 20 40 60 80  
 M E T E R S

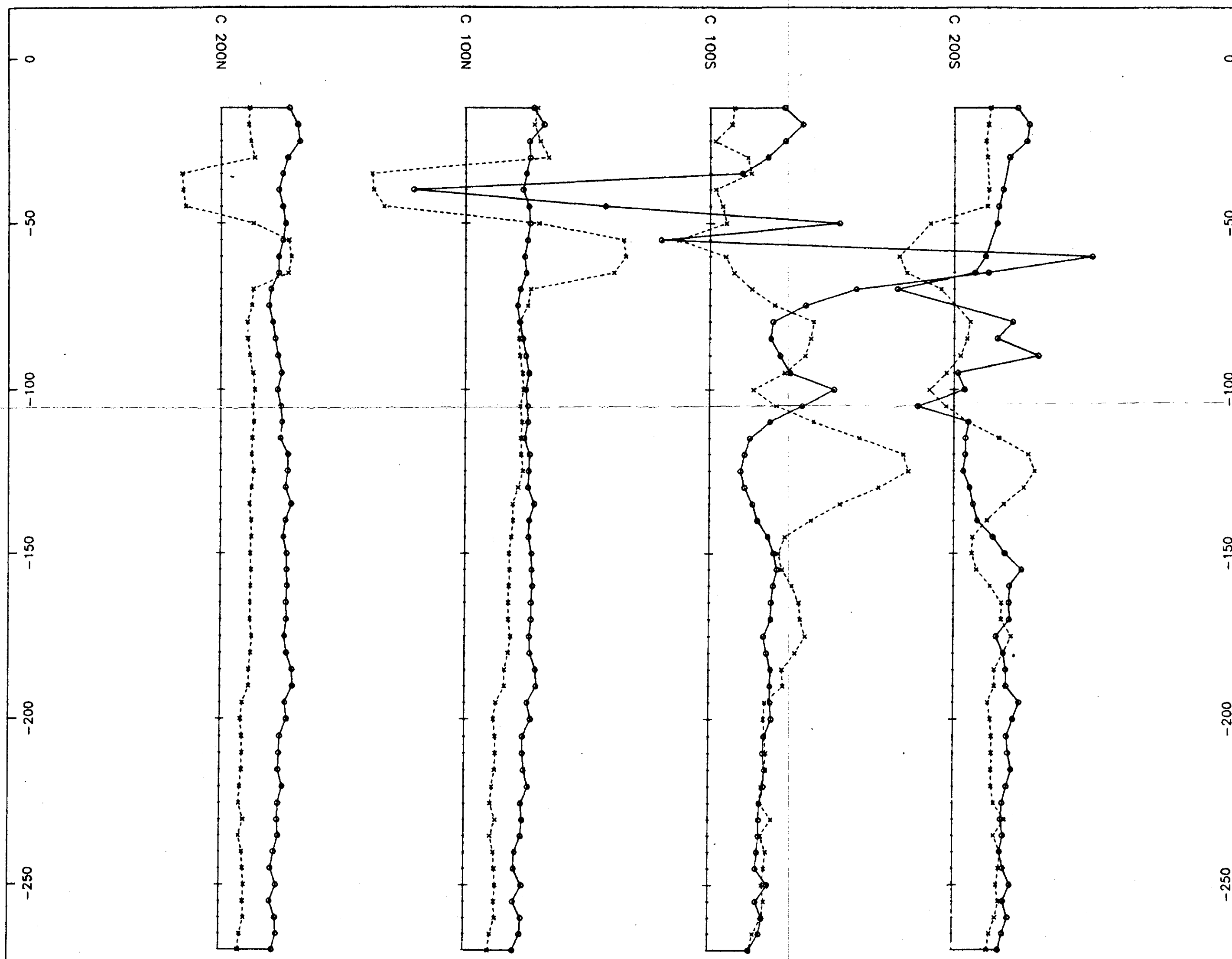
TEUTON RESOURCES CORP.

CLONE PROJECT  
 STEWART AREA, B.C.  
 DOWNHOLE IP SURVEY  
 DDH CL96-43

DRAWN BY: arw DATE: Oct/96  
 SCOTT GEOPHYSICS LTD.

GEOLOGICAL SURVEY BRANCH  
 ASSESSMENT REPORT

24938 10 of 14  
 ①



CL96-30 Az 65, Dip -70, Depth 280m

Directional Array:  
 receiver Scintrex IPR12  
 pulse time 2 seconds  
 Mx window 690-1050 msecs

transmitter Iris VIP 3000 (3kw)  
 array axial gradient  
 a spacing 20 meters  
 C2 (far current) > 1200 m North

C1 (Grid coordinate w.r.t. collar):

Log #1	C1	200N
Log #2	C1	100N
Log #3	C1	100S
Log #4	C1	200S

Grid North 315 degrees

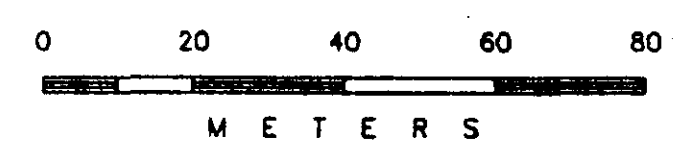
o---o scale chargeability  
 10 mV/V /cm

x---x scale normalized VP  
 200 mV/amp /cm

positive to right of graph

GEOLOGICAL SURVEY BRANCH  
 ASSESSMENT REPORT

24,938 (2)

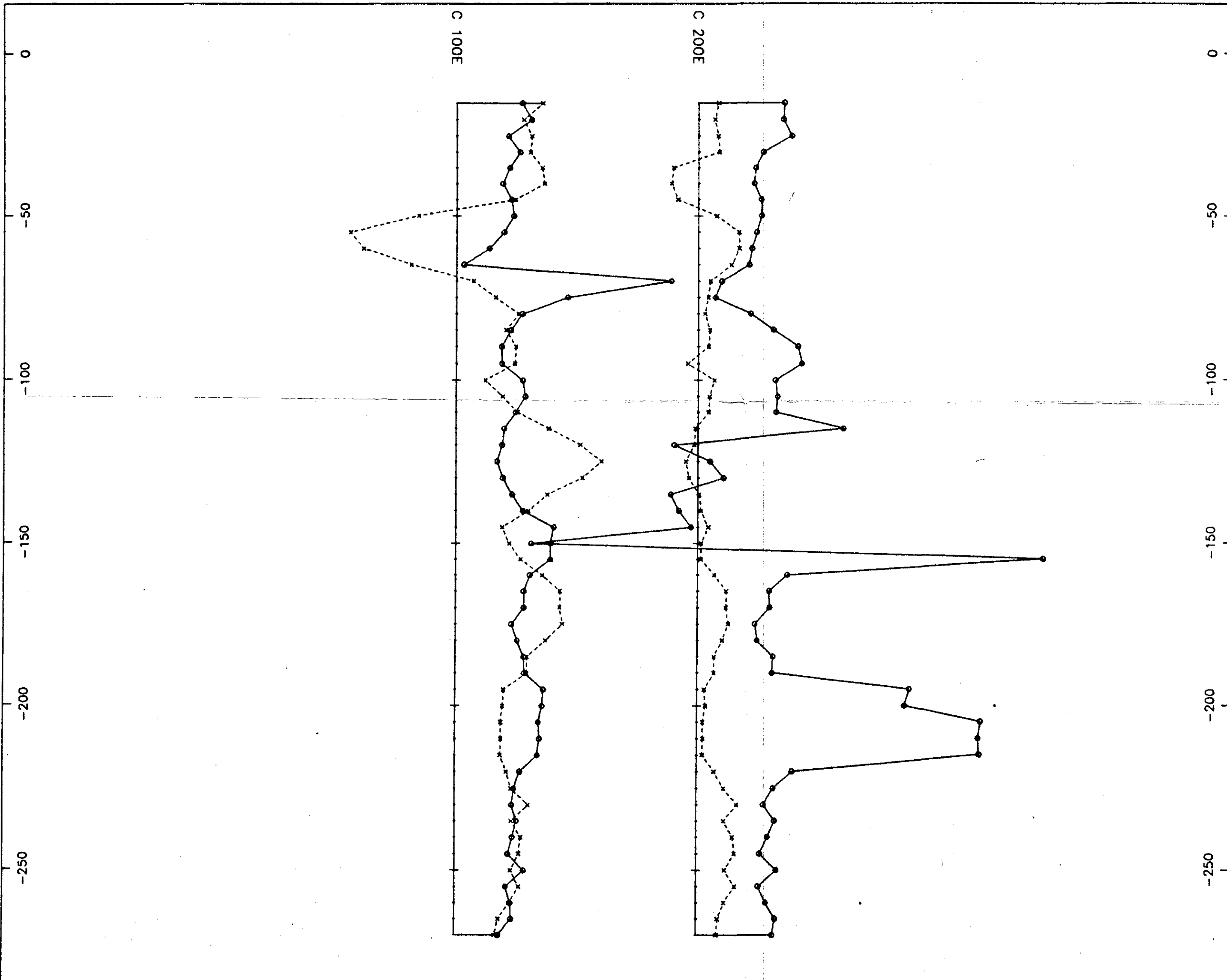


TEUTON RESOURCES CORP.

CLONE PROJECT  
 STEWART AREA, B.C.  
 DOWNHOLE IP SURVEY  
 DDH CL96-30

Current Electrodes North and South

DRAWN BY: arw	DATE: Oct/96
SCOTT GEOPHYSICS LTD.	



CL96-30 Az 65, Dip -70, Depth 280m

Directional Array:  
 receiver Scintrex IPR12  
 pulse time 2 seconds  
 Mx window 690-1050 msec

transmitter Iris VIP-3000 (3kw)  
 array axial gradient  
 a spacing 20 meters  
 C2 (far current) > 1200 m North

C1 (Grid coordinate w.r.t. cellar):  
 Log #1 C1 100E  
 Log #2 C1 200E

Grid North 315 degrees

o---o chargeability  
 scale 10 mV/V /cm

x - x normalized VP  
 scale 200 mV/amp /cm

positive to right of graph

**GEOLOGICAL SURVEY BRANCH  
 ASSESSMENT REPORT**

**24,938** <sup>(3)</sup>

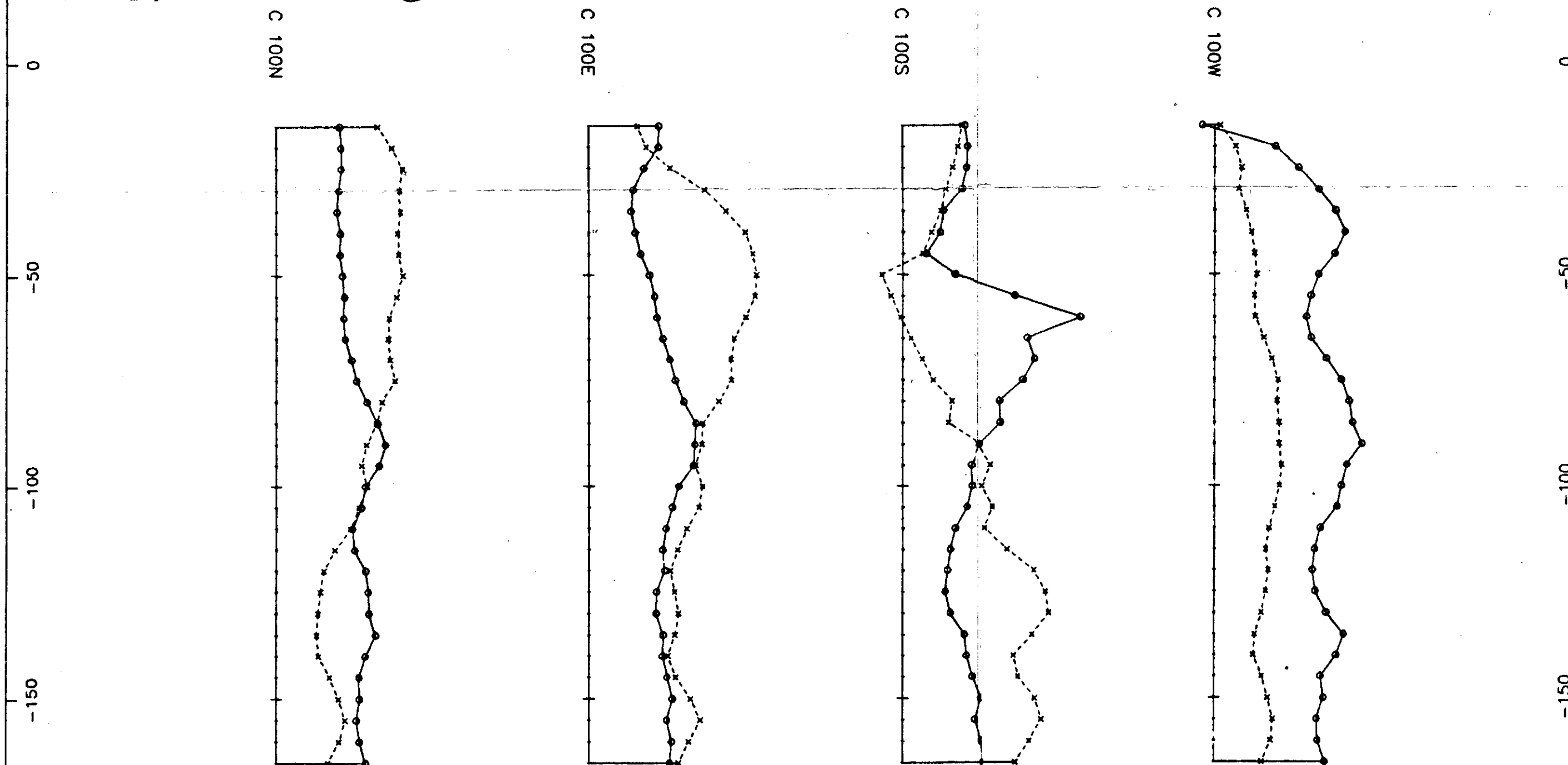
0 20 40 60 80  
 M E T E R S

TEUTON RESOURCES CORP.

CLONE PROJECT  
 STEWART AREA, B.C.  
 DOWNHOLE IP SURVEY  
 DDH CL96-30  
 Current Electrodes East

DRAWN BY: arw DATE: Oct/96  
 SCOTT GEOPHYSICS LTD.

24,938 (4)



CL96-29 Az 245, Dip -75, Depth 179 m

Directional Array:

receiver Scintrex IPR12  
pulse time 2 seconds  
Mx window 690-1050 msec

transmitter Iris VIP 3000 (3kw)  
array axial gradient  
a spacing 20 meters  
C2 (far current) > 1200 m North

C1 (Grid coordinate w.r.t. collar):

Log #1 C1 100N  
Log #2 C1 100E  
Log #3 C1 100S  
Log #4 C1 100W

Grid North 315 degrees

o---o chargeability  
scale 10 mV/V /cm  
x - x normalized VP  
scale 200 mV/amp /cm  
positive to right of graph



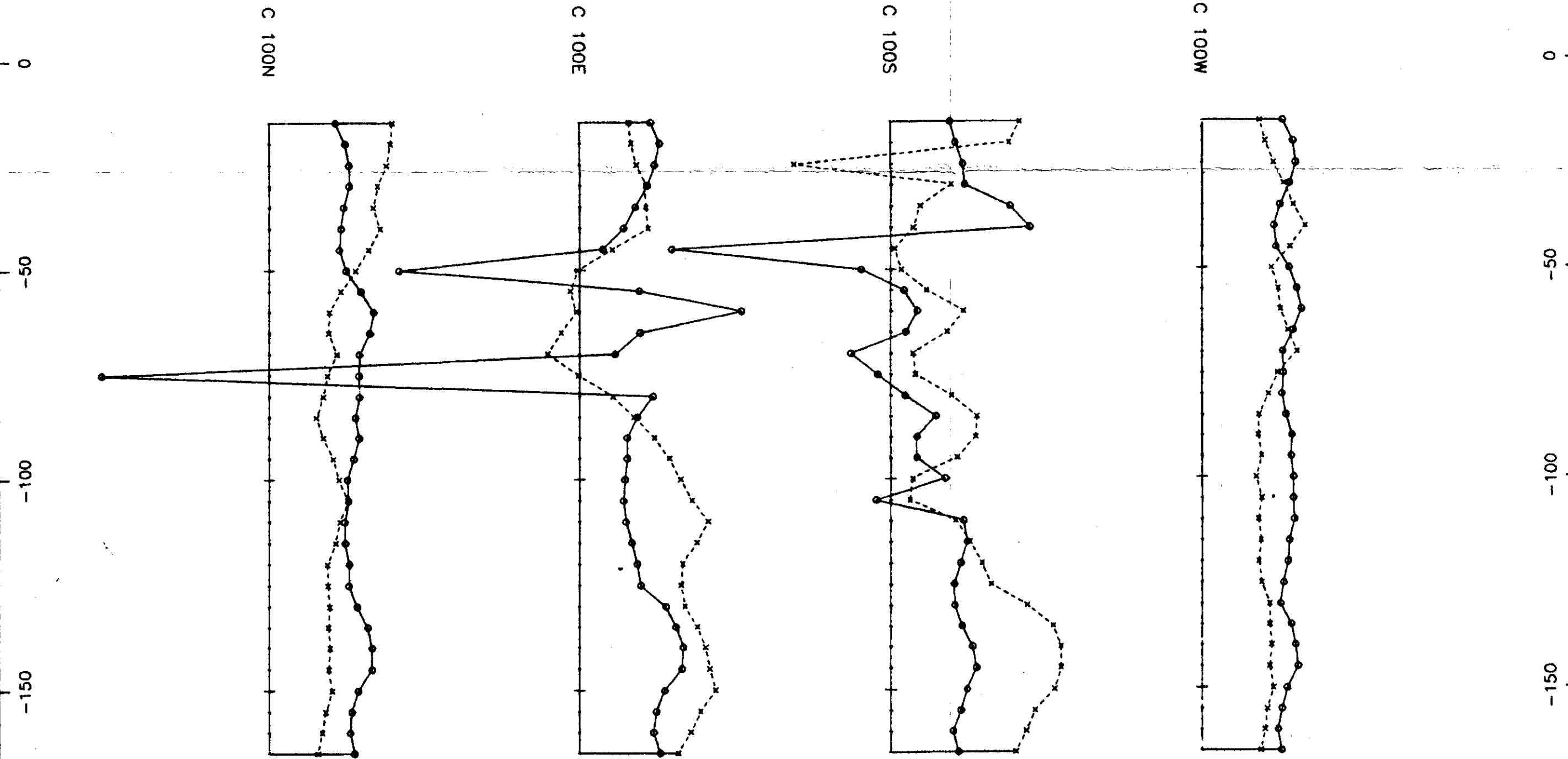
TEUTON RESOURCES CORP.

CLONE PROJECT  
STEWART AREA, B.C.  
DOWNHOLE IP SURVEY  
DDH CL96-29

DRAWN BY: arw DATE: Oct/96

SCOTT GEOPHYSICS LTD.

24,938 (5)



CL96-25 Az 65, Dip -80, Depth 177m

Directional Array:  
receiver Scintrex IPR12  
pulse time 2 seconds  
Mx window 690-1050 msec

transmitter Iris VIP 3000 (3kw)  
array axial gradient  
a spacing 20 meters  
C2 (far current) > 1200 m North

C1 (Grid coordinate w.r.t. collar):

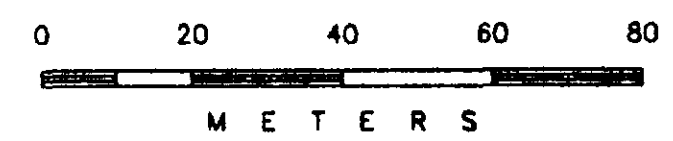
Log #1	C1	100N
Log #2	C1	100E
Log #3	C1	100S
Log #4	C1	100W

Grid North 315 degrees

o---o chargeability  
scale 10 mV/V /cm

x - x normalized VP  
scale 200 mV/amp /cm

positive to right of graph



TEUTON RESOURCES CORP.

CLONE PROJECT  
STEWART AREA, B.C.  
DOWNHOLE IP SURVEY  
DDH CL96-25

DRAWN BY: arw DATE: Oct/96

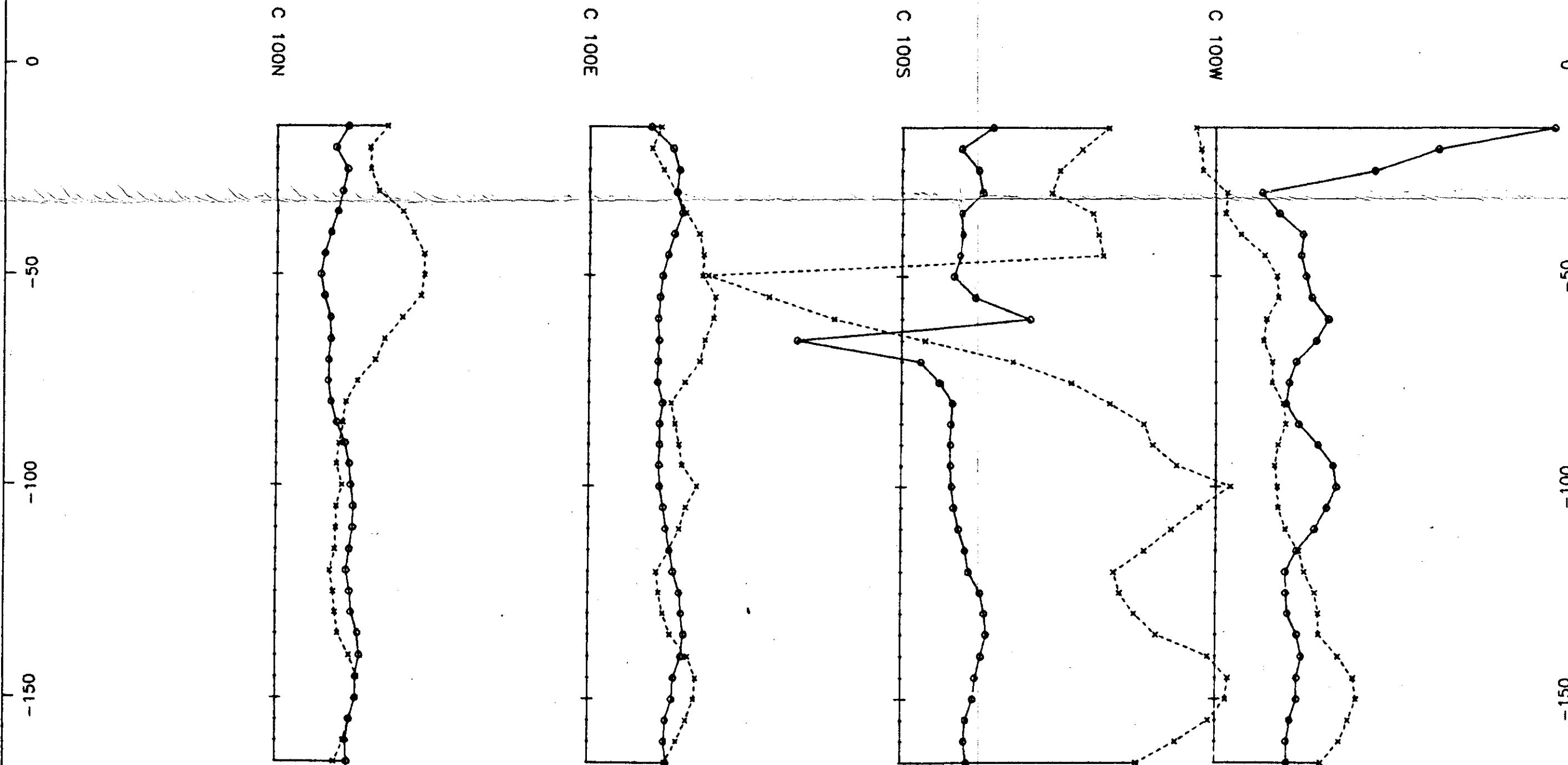
SCOTT GEOPHYSICS LTD.



GEOLOGICAL SURVEY BRANCH

ASSESSMENT REPORT

24,938 (6)



CL96-19 Az 220, Dip -65, Depth 181m

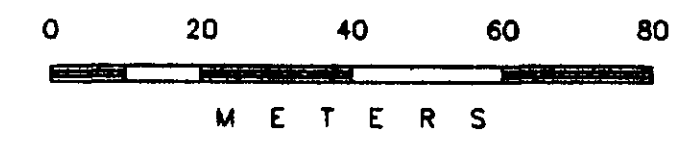
Directional Array:  
 receiver Scintrex IPR12  
 pulse time 2 seconds  
 Mx window 690-1050 msec

transmitter Iris VIP 3000 (3kw)  
 array axial gradient  
 a spacing 20 meters  
 C2 (for current) > 1200 m North

C1 (Grid coordinate w.r.t. collar):  
 Log #1 C1 100N  
 Log #2 C1 100E  
 Log #3 C1 100S  
 Log #4 C1 100W

Grid North 315 degrees

o—o scale chargeability  
 10 mV/V /cm  
 x - x scale normalized Vp  
 200 mV/amp /cm  
 positive to right of graph



TEUTON RESOURCES CORP.

CLONE PROJECT  
 STEWART AREA, B.C.  
 DOWNHOLE IP SURVEY  
 DDH CL96-19

DRAWN BY: arw DATE: Oct/96

SCOTT GEOPHYSICS LTD.

\$\$\$DATA\$\$ 12 -1 8 -2000 1 Sept/96  
 Array:P Trav dir:S Current:T Num Sep:3 A Spc:20,20,20 Eff.Sep:1,2,3  
 TEUTON RESOURCES CORP. - CLONE PROJECT, STEWART, B.C.  
 DDH9619 - Az 222, Dip -65, Depth 177 m

DOWNHOLE IP SURVEY  
 vertical gradient array, C2 @ 1200N; C1 @ 100N, 100E, 100S, 100W  
 Mx chargeability for the interval 690-1050 msec after shutoff  
 Normalized VP = VP / current x 1000

NOTE: Grid North 315 Degrees

LIN	STN	SEP	XGD	YGD	VP	SP	Mx	NVP	Mi	TAU	FIT			
3	3	3	2	2	1	1	1	1	1	1	1			
(T62,2A8,A3,T1,3F8.0,F5.0,3F6.0,2F7.0)														
75.0	-15.0	530.13	-11	17.1	530	374048.000	2.70	100N	15N	1				
75.0	-20.0	447.09	26	14.2	447	242128.000	1.13	100N	20N	1				
75.0	-25.0	450.77	32	17.0	451	250 32.000	0.96	100N	25N	1				
75.0	-30.0	491.39	42	15.8	491	240 16.000	3.73	100N	30N	1				
75.0	-35.0	604.83	24	14.5	605	211 16.000	0.83	100N	35N	1				
75.0	-40.0	656.04	-6	12.9	656	184 4.000	0.37	100N	40N	1				
75.0	-45.0	706.46	-6	11.4	706	165 2.000	0.29	100N	45N	1				
75.0	-50.0	707.95	5	10.5	708	155 2.000	0.69	100N	50N	1				
75.0	-55.0	691.60	0	11.4	692	165 2.000	0.24	100N	55N	1				
75.0	-60.0	605.03	13	12.9	605	185 2.000	0.55	100N	60N	1				
75.0	-65.0	518.70	-0	13.0	519	186 2.000	0.48	100N	65N	1				
75.0	-70.0	474.63	-1	12.5	475	179 2.000	0.72	100N	70N	1				
75.0	-75.0	388.81	94	12.4	389	179 4.000	0.51	100N	75N	1				
75.0	-80.0	334.70	-6	13.1	335	187 4.000	0.57	100N	80N	1				
75.0	-85.0	320.98	3	14.5	321	207 4.000	0.81	100N	85N	1				
75.0	-90.0	302.93	7	16.6	303	230 4.000	0.50	100N	90N	1				
75.0	-95.0	289.98	-87	17.6	290	244 4.000	0.42	100N	95N	1				
75.0	-100.0	317.15	2	17.9	317	250 8.000	0.55	100N	100N	1				
75.0	-105.0	290.09	-0	18.5	290	254 2.000	0.70	100N	105N	1				
75.0	-110.0	286.77	-2	18.4	287	252 4.000	0.57	100N	110N	1				
75.0	-115.0	283.54	-3	17.7	284	245 4.000	0.81	100N	115N	1				
75.0	-120.0	261.32	1	17.0	261	237 2.000	0.43	100N	120N	1				
75.0	-125.0	277.28	7	17.8	277	246 4.000	0.70	100N	125N	1				
75.0	-130.0	285.74	28	18.2	286	251 2.000	0.68	100N	130N	1				
75.0	-135.0	298.51	17	19.7	299	268 2.000	0.89	100N	135N	1				
75.0	-140.0	354.89	7	20.2	355	275 2.000	0.63	100N	140N	1				
75.0	-145.0	390.56	-2	19.3	391	265 2.000	0.68	100N	145N	1				
75.0	-150.0	386.17	-14	19.2	386	267 1.000	0.70	100N	150N	1				
75.0	-155.0	354.87	96	17.8	355	250 1.000	0.51	100N	155N	1				
75.0	-160.0	329.12	11	16.9	329	240 1.000	0.49	100N	160N	1				
75.0	-165.0	284.38	-2	17.3	284	244 1.000	0.75	100N	165N	1				
150.0	-15.0	171.02	-16	14.7	342	100 0.000	29.37	100E	15N	1				
150.0	-20.0	148.72	26	20.0	297	406048.000	4.27	100E	20N	1				
150.0	-25.0	176.94	32	21.5	354	321 64.000	3.20	100E	25N	1				
150.0	-30.0	208.00	43	20.9	416	315 64.000	3.82	100E	30N	1				
150.0	-35.0	230.13	29	22.1	460	346128.000	0.86	100E	35N	1				
150.0	-40.0	262.63	-7	20.3	525	292 32.000	0.49	100E	40N	1				
150.0	-45.0	273.05	-6	18.8	546	265 16.000	0.30	100E	45N	1				
150.0	-50.0	270.17	3	17.5	540	243 8.000	0.33	100E	50N	1				
150.0	-55.0	301.92	1	16.9	604	237 8.000	0.19	100E	55N	1				
150.0	-60.0	297.72	13	16.5	595	232 8.000	0.26	100E	60N	1				
150.0	-65.0	277.04	-1	16.7	554	232 4.000	0.55	100E	65N	1				
150.0	-70.0	264.98	-1	16.5	530	230 4.000	0.31	100E	70N	1				
150.0	-75.0	230.06	94	16.4	460	228 4.000	0.30	100E	75N	1				
150.0	-80.0	196.88	-7	17.6	394	246 8.000	0.53	100E	80N	1				
150.0	-85.0	206.67	3	16.9	413	235 4.000	0.39	100E	85N	1				
150.0	-90.0	215.67	7	16.9	431	235 4.000	0.20	100E	90N	1				
150.0	-95.0	223.00	-87	16.8	446	235 4.000	0.63	100E	95N	1				
150.0	-100.0	258.89	1	16.9	518	234 4.000	0.42	100E	100N	1				
150.0	-105.0	232.66	-1	17.8	465	246 4.000	0.27	100E	105N	1				
150.0	-110.0	216.61	-3	18.4	433	255 8.000	0.55	100E	110N	1				
150.0	-115.0	192.66	-3	19.4	385	268 8.000	0.48	100E	115N	1				
150.0	-120.0	163.22	2	20.3	326	274 4.000	0.26	100E	120N	1				

150.0	-125.0	168.45	7	21.8	337	294	8.000	0.20	100E	125N	1
150.0	-130.0	178.59	27	22.3	357	300	8.000	0.42	100E	130N	1
150.0	-135.0	196.99	18	22.9	394	305	8.000	0.30	100E	135N	1
150.0	-140.0	238.27	8	22.3	477	297	4.000	0.38	100E	140N	1
150.0	-145.0	257.37	-2	20.5	515	278	4.000	0.44	100E	145N	1
150.0	-150.0	253.22	-14	20.1	506	272	2.000	0.66	100E	150N	1
150.0	-155.0	234.91	96	18.6	470	255	2.000	0.47	100E	155N	1
150.0	-160.0	212.74	12	18.2	425	252	2.000	0.29	100E	160N	1
150.0	-165.0	185.13	-1	18.8	370	258	2.000	0.48	100E	165N	1
225.0	-15.0	495.31	-18	22.1	991	351	0.125	1.31	100S	15N	1
225.0	-20.0	432.39	26	14.5	865	207	2.000	0.81	100S	20N	1
225.0	-25.0	379.45	33	18.7	759	257	4.000	1.62	100S	25N	1
225.0	-30.0	361.10	42	19.7	722	260	4.000	3.14	100S	30N	1
225.0	-35.0	458.01	32	14.4	916	202	4.000	1.39	100S	35N	1
225.0	-40.0	471.24	-7	14.7	942	213	1.000	0.86	100S	40N	1
225.0	-45.0	481.66	-6	14.0	963	210	0.500	1.17	100S	45N	1
225.0	-50.0	-466.00	3	12.5	-932	190	0.500	0.94	100S	50N	1
225.0	-55.0	-319.55	1	17.8	-639	246	4.000	0.39	100S	55N	1
225.0	-60.0	-162.47	14	30.9	-325	390	2.000	0.80	100S	60N	1
225.0	-65.0	56.05	-1	-25.1	112	-33	2.000	0.95	100S	65N	1
225.0	-70.0	268.09	-0	4.5	536	70	2.000	0.56	100S	70N	1
225.0	-75.0	406.01	94	9.1	812	142	16.000	0.88	100S	75N	1
225.0	-80.0	497.29	-7	12.3	995	177	4.000	0.64	100S	80N	1
225.0	-85.0	578.14	3	11.9	1156	175	8.000	0.24	100S	85N	1
225.0	-90.0	600.61	6	11.8	1201	173	8.000	0.26	100S	90N	1
225.0	-95.0	657.48	-86	11.8	1315	186	32.000	0.63	100S	95N	1
225.0	-100.0	785.26	0	12.1	1571	177	8.000	0.42	100S	100N	1
225.0	-105.0	712.47	-0	12.6	1425	183	8.000	0.49	100S	105N	1
225.0	-110.0	644.49	-2	13.8	1289	199	8.000	0.34	100S	110N	1
225.0	-115.0	579.54	-3	15.4	1159	218	8.000	0.41	100S	115N	1
225.0	-120.0	507.35	2	16.3	1015	235	16.000	0.44	100S	120N	1
225.0	-125.0	521.46	8	19.1	1043	269	16.000	0.56	100S	125N	1
225.0	-130.0	556.21	28	20.1	1112	281	16.000	0.58	100S	130N	1
225.0	-135.0	608.77	19	20.5	1218	278	8.000	0.52	100S	135N	1
225.0	-140.0	732.44	8	19.3	1465	264	8.000	0.44	100S	140N	1
225.0	-145.0	780.93	-1	17.8	1562	246	4.000	0.42	100S	145N	1
225.0	-150.0	774.77	-13	17.3	1550	240	4.000	0.29	100S	150N	1
225.0	-155.0	734.78	96	15.6	1470	220	4.000	0.41	100S	155N	1
225.0	-160.0	656.11	13	15.2	1312	213	4.000	0.44	100S	160N	1
225.0	-165.0	562.36	0	15.8	1125	223	2.000	0.75	100S	165N	1
300.0	-15.0	-18.16	-22	81.2	-91	508	0.000	31.21	100W	15N	1
300.0	-20.0	-13.36	27	53.6	-67	312	0.000	12.02	100W	20N	1
300.0	-25.0	-12.06	34	38.2	-60	249	0.000	20.09	100W	35N	1
300.0	-30.0	11.38	43	11.2	57	0	0.000	0.00	100W	30N	1
300.0	-35.0	9.83	34	15.3	49	0	0.000	0.00	100W	35N	1
300.0	-40.0	23.96	-7	21.0	120	0	0.000	0.00	100W	40N	1
300.0	-45.0	47.02	-5	20.5	235	386048.000	19.18	100W	45N	1	
300.0	-50.0	58.87	2	21.7	294	432048.000	2.91	100W	50N	1	
300.0	-55.0	60.11	2	23.1	301	422024.000	1.75	100W	55N	1	
300.0	-60.0	48.55	14	27.0	243	413256.000	1.55	100W	60N	1	
300.0	-65.0	45.87	-1	24.2	229	407512.000	1.07	100W	65N	1	
300.0	-70.0	54.27	-0	19.4	271	309128.000	0.56	100W	70N	1	
300.0	-75.0	54.05	93	17.7	270	288128.000	0.61	100W	75N	1	
300.0	-80.0	65.15	-8	16.9	326	252 32.000	0.28	100W	80N	1	
300.0	-85.0	67.40	2	20.0	337	288 32.000	0.22	100W	85N	1	
300.0	-90.0	59.97	6	24.6	300	340 32.000	0.47	100W	90N	1	
300.0	-95.0	56.37	-86	28.2	282	375 32.000	0.41	100W	95N	1	
300.0	-100.0	59.20	-0	29.0	296	384 32.000	0.42	100W	100N	1	
300.0	-105.0	60.15	-1	26.6	301	360 32.000	0.42	100W	105N	1	
300.0	-110.0	66.95	-3	23.7	335	320 16.000	0.53	100W	110N	1	
300.0	-115.0	80.17	-3	19.5	401	267 8.000	0.44	100W	115N	1	
300.0	-120.0	85.32	2	16.8	427	233 4.000	0.31	100W	120N	1	
300.0	-125.0	95.32	5	16.9	477	234 4.000	0.57	100W	125N	1	
300.0	-130.0	98.99	27	17.4	495	241 4.000	0.71	100W	130N	1	
300.0	-135.0	99.55	18	19.7	498	268 4.000	0.68	100W	135N	1	

300.0	-145.0	132.77	1	19.7	664	268	2.000	0.86	100W	145N	1
300.0	-150.0	135.53	-14	19.7	678	268	2.000	0.42	100W	150N	1
300.0	-155.0	127.92	95	18.1	640	251	2.000	0.52	100W	155N	1
300.0	-160.0	119.54	13	17.2	598	241	2.000	0.71	100W	160N	1
300.0	-165.0	102.45	1	17.3	512	245	1.000	0.68	100W	165N	1

MEMORIAL SERVICE BRANCH  
MEMORIAL REPORT

24,938

Array:G Trav dir:S Current:T Num Sep:3 A Spc:20,20,20 Eff.Sep:1,2,3

TEUTON RESOURCES CORP. - CLONE PROJECT, STEWART, B.C.

CL96-25 : Az 065, Dip -80, Depth 177 m

DOWNHOLE IP SURVEY

vertical gradient array, C2 @ 1200N; C1 @ 100N, 100E, 100S, 100W

Mx chargeability for the interval 690-1050 msec after shutoff

Normalized VP = mV / amp (VP / current x 1000)

NOTE: Grid North 315 Degrees

LIN	STN	SEP	XGD	YGD	VP	SP	Mx	NVP	Mi	TAU	FIT		
3	3	3	2	2	1	1	1	1	1	1	1		
(T62,2A8,A3,T1,3F8.0,F5.0,3F6.0,2F7.0)													
75.0	-15.0	444.95	-4	15.9	593	230	4.000	2.33	100N	-15	1		
75.0	-20.0	408.66	0	18.3	584	252	2.000	1.08	100N	-20	1		
75.0	-25.0	395.95	-4	19.2	566	261	4.000	1.04	100N	-25	1		
75.0	-30.0	365.68	14	19.2	522	269	16.000	1.02	100N	-30	1		
75.0	-35.0	374.83	9	17.9	500	246	4.000	0.59	100N	-35	1		
75.0	-40.0	375.20	8	17.3	536	240	4.000	0.52	100N	-40	1		
75.0	-45.0	335.19	9	16.9	479	235	4.000	1.35	100N	-45	1		
75.0	-50.0	312.21	-11	18.5	416	252	4.000	0.69	100N	-50	1		
75.0	-55.0	259.40	2	22.1	346	297	8.000	0.39	100N	-55	1		
75.0	-60.0	216.16	11	25.1	288	327	8.000	0.66	100N	-60	1		
75.0	-65.0	229.10	-5	24.2	286	323	16.000	0.68	100N	-65	1		
75.0	-70.0	243.88	-3	21.7	325	291	8.000	0.65	100N	-70	1		
75.0	-75.0	210.05	1	21.6	280	290	8.000	0.47	100N	-75	1		
75.0	-80.0	194.91	170	21.7	260	291	8.000	0.49	100N	-80	1		
75.0	-85.0	181.47	111	20.8	227	282	8.000	0.26	100N	-85	1		
75.0	-90.0	195.89	-7	21.6	261	290	8.000	0.34	100N	-90	1		
75.0	-95.0	230.47	-7	20.4	307	277	8.000	0.28	100N	-95	1		
75.0	-100.0	252.45	-185	18.8	337	260	8.000	0.42	100N	-100	1		
75.0	-105.0	303.02	-126	19.1	379	269	16.000	0.61	100N	-105	1		
75.0	-110.0	272.43	30	18.2	341	252	8.000	0.29	100N	-110	1		
75.0	-115.0	254.81	45	18.3	319	254	8.000	0.26	100N	-115	1		
75.0	-120.0	210.96	16	19.3	281	265	8.000	0.15	100N	-120	1		
75.0	-125.0	212.35	215	19.2	283	264	8.000	0.22	100N	-125	1		
75.0	-130.0	233.31	-19	21.2	292	285	8.000	0.48	100N	-130	1		
75.0	-135.0	229.05	-39	23.8	286	314	8.000	0.47	100N	-135	1		
75.0	-140.0	219.52	-7	24.8	293	324	8.000	0.50	100N	-140	1		
75.0	-145.0	215.48	-214	24.8	287	332	16.000	0.49	100N	-145	1		
75.0	-150.0	241.73	-5	21.5	302	295	16.000	0.54	100N	-150	1		
75.0	-155.0	218.63	-3	20.0	273	273	8.000	0.29	100N	-155	1		
75.0	-160.0	192.37	2	19.6	256	267	4.000	0.35	100N	-160	1		
75.0	-165.0	176.15	-1	20.6	235	279	4.000	0.44	100N	-165	1		
150.0	-15.0	235.76	-3	17.1	236	251	0.500	2.19	100E	-15	1		
150.0	-20.0	247.40	-1	19.2	247	277	0.500	1.61	100E	-20	1		
150.0	-25.0	273.83	-5	18.0	274	281	0.250	1.58	100E	-25	1		
150.0	-30.0	314.92	13	16.2	315	251	0.250	1.04	100E	-30	1		
150.0	-35.0	317.62	8	13.3	318	201	0.500	0.88	100E	-35	1		
150.0	-40.0	328.67	9	10.5	329	169	0.250	1.04	100E	-40	1		
150.0	-45.0	155.71	12	5.5	156	347	0.000	3.93	100E	-45	1		
150.0	-50.0	-8.68	-4	-43.7	-9	-570	48.000	27.72	100E	-50	1		
150.0	-55.0	-46.39	3	14.3	-46	341	0.007	1.42	100E	-55	1		
150.0	-60.0	-16.15	11	38.9	-16	665	0.031	1.45	100E	-60	1		
150.0	-65.0	-88.91	-5	14.5	-89	240	0.125	0.87	100E	-65	1		
150.0	-70.0	-152.75	-3	8.5	-153	147	0.125	0.32	100E	-70	1		
150.0	-75.0	-5.97	-1	-115.3	-6	-870	48.000	2.93	100E	-75	1		
150.0	-80.0	160.66	172	17.6	161	245	8.000	0.73	100E	-80	1		
150.0	-85.0	261.88	111	13.8	262	197	4.000	1.10	100E	-85	1		
150.0	-90.0	358.91	-6	11.4	359	165	2.000	0.90	100E	-90	1		
150.0	-95.0	430.50	-5	11.4	431	165	2.000	0.94	100E	-95	1		
150.0	-100.0	485.27	-187	10.8	485	158	2.000	0.83	100E	-100	1		
150.0	-105.0	540.35	-126	10.5	540	153	2.000	0.93	100E	-105	1		
150.0	-110.0	617.51	30	11.1	618	161	2.000	0.81	100E	-110	1		
150.0	-115.0	562.52	46	12.5	563	180	2.000	0.82	100E	-115	1		
150.0	-120.0	495.29	16	13.8	495	197	4.000	0.81	100E	-120	1		

150.0	-125.0	488.40	210	14.7	488	209	4.000	0.74	100E	-125	1
150.0	-130.0	506.13	-20	20.8	506	279	4.000	1.05	100E	-130	1
150.0	-135.0	566.48	-38	23.2	566	309	8.000	1.03	100E	-135	1
150.0	-140.0	605.57	-6	24.9	606	328	8.000	0.86	100E	-140	1
150.0	-145.0	626.21	-211	24.6	626	324	8.000	0.81	100E	-145	1
150.0	-150.0	655.24	-5	20.5	655	277	4.000	0.45	100E	-150	1
150.0	-155.0	582.56	-3	18.5	583	255	2.000	0.53	100E	-155	1
150.0	-160.0	534.74	2	17.8	535	253	1.000	0.78	100E	-160	1
150.0	-165.0	475.14	-1	19.5	475	274	1.000	0.85	100E	-165	1
225.0	-15.0	124.76	-3	14.3	624	482	0.000	4.95	100S	-15	1
225.0	-20.0	114.52	-2	15.7	573	282	0.062	3.78	100S	-20	1
225.0	-25.0	-93.32	-6	17.5	-467	116	0.000	13.48	100S	-25	1
225.0	-30.0	57.57	12	17.9	288	350	0.031	11.06	100S	-30	1
225.0	-35.0	27.80	9	28.9	139	417	0.250	3.80	100S	-35	1
225.0	-40.0	21.08	10	33.7	105	435	1.000	2.46	100S	-40	1
225.0	-45.0	3.47	15	-52.9	17	-26	0.000	75.16	100S	-45	1
225.0	-50.0	9.95	-0	-7.2	50	-59	0.000	22.15	100S	-50	1
225.0	-55.0	34.36	3	3.1	172	86048.000		15.23	100S	-55	1
225.0	-60.0	70.49	11	6.3	352	98	8.000	0.44	100S	-60	1
225.0	-65.0	54.29	-4	3.5	271	55	2.000	2.08	100S	-65	1
225.0	-70.0	20.99	-3	-9.7	105	-15	0.250	1.74	100S	-70	1
225.0	-75.0	23.63	-1	-3.2	118	-23	0.000	7.69	100S	-75	1
225.0	-80.0	58.57	173	3.4	293	91048.000		13.59	100S	-80	1
225.0	-85.0	83.34	111	10.8	417	206256.000		0.76	100S	-85	1
225.0	-90.0	82.28	-6	6.2	411	128256.000		0.41	100S	-90	1
225.0	-95.0	63.90	-5	6.2	320	170048.000		0.47	100S	-95	1
225.0	-100.0	20.73	-187	13.1	104	295048.000		7.85	100S	-100	1
225.0	-105.0	18.07	-126	-3.6	90	-27	0.000	27.52	100S	-105	1
225.0	-110.0	62.67	31	17.6	313	305256.000		0.38	100S	-110	1
225.0	-115.0	76.66	46	18.5	383	270	32.000	0.43	100S	-115	1
225.0	-120.0	88.26	16	16.9	441	242	16.000	0.39	100S	-120	1
225.0	-125.0	97.27	214	15.3	486	217	8.000	0.68	100S	-125	1
225.0	-130.0	132.37	-20	15.4	662	216	4.000	0.96	100S	-130	1
225.0	-135.0	157.04	-38	17.2	785	239	4.000	0.91	100S	-135	1
225.0	-140.0	164.43	-6	19.8	822	267	4.000	0.96	100S	-140	1
225.0	-145.0	164.54	-211	20.7	823	282	8.000	0.88	100S	-145	1
225.0	-150.0	158.38	-5	18.5	792	254	4.000	0.46	100S	-150	1
225.0	-155.0	139.75	-3	16.9	699	235	4.000	0.74	100S	-155	1
225.0	-160.0	131.45	0	15.0	657	216	1.000	0.53	100S	-160	1
225.0	-165.0	121.04	-2	16.3	605	232	1.000	0.67	100S	-165	1
300.0	-15.0	280.09	-2	19.6	280	269	8.000	1.16	100W	-15	1
300.0	-20.0	307.90	-2	22.1	308	295	2.000	0.53	100W	-20	1
300.0	-25.0	347.25	-7	22.7	347	301	4.000	1.04	100W	-25	1
300.0	-30.0	276.92	10	21.2	396	286	4.000	0.99	100W	-30	1
300.0	-35.0	442.21	8	18.9	442	259	2.000	0.46	100W	-35	1
300.0	-40.0	499.35	10	17.4	499	243	2.000	0.60	100W	-40	1
300.0	-45.0	426.39	17	17.9	426	246	2.000	0.77	100W	-45	1
300.0	-50.0	336.29	1	21.1	336	283	2.000	0.66	100W	-50	1
300.0	-55.0	369.29	4	22.9	369	304	4.000	0.54	100W	-55	1
300.0	-60.0	380.09	10	24.0	380	315	4.000	0.27	100W	-60	1
300.0	-65.0	415.81	-5	22.0	416	294	4.000	0.23	100W	-65	1
300.0	-70.0	459.42	-2	19.5	459	265	4.000	0.44	100W	-70	1
300.0	-75.0	364.63	-1	19.6	365	267	4.000	0.59	100W	-75	1
300.0	-80.0	320.61	173	19.3	321	266	8.000	0.81	100W	-80	1
300.0	-85.0	274.25	111	20.2	274	276	8.000	0.76	100W	-85	1
300.0	-90.0	270.40	-6	21.7	270	293	8.000	0.68	100W	-90	1
300.0	-95.0	287.02	-4	21.5	287	291	8.000	0.84	100W	-95	1
300.0	-100.0	260.91	-188	22.1	261	297	8.000	0.68	100W	-100	1
300.0	-105.0	287.77	-126	22.0	288	296	8.000	0.52	100W	-105	1
300.0	-110.0	270.68	31	22.3	271	305	16.000	0.68	100W	-110	1
300.0	-115.0	283.84	46	21.1	284	286	8.000	0.64	100W	-115	1
300.0	-120.0	273.32	16	20.8	273	281	8.000	0.52	100W	-120	1
300.0	-125.0	287.94	214	19.7	288	270	8.000	0.60	100W	-125	1
300.0	-130.0	327.78	-20	19.0	328	259	4.000	0.59	100W	-130	1
300.0	-135.0	327.50	-38	21.6	328	289	4.000	0.66	100W	-135	1
300.0	-140.0	336.69	-6	22.6	337	302	8.000	0.37	100W	-140	1

300.0	-145.0	327.84	-211	23.2	328	309	8.000	0.65	100W	-145	1
300.0	-150.0	345.33	-5	20.6	345	279	8.000	0.34	100W	-150	1
300.0	-155.0	317.21	-3	19.4	317	267	8.000	0.74	100W	-155	1
300.0	-160.0	304.74	0	18.4	305	252	4.000	0.32	100W	-160	1
300.0	-165.0	285.56	-3	19.2	286	262	2.000	0.65	100W	-165	1

GEOLOGICAL SURVEY BRANCH  
ASSESSMENT REPORT

24,938

\$\$DATA\$\$ 12 -1 8 -2000 1 Sept/96  
 Array:G Trav dir:S Current:T Num Sep:3 A Spc:20,20,20 Eff.Sep:1,2,3  
 TEUTON RESOURCES CORP. - CLONE PROJECT, STEWART, B.C.  
 CL96-29 : Az 245, Dip -75, Depth 179 m

DOWNHOLE IP SURVEY  
 vertical gradient array, C2 @ 1200N; C1 @ 100N, 100E, 100S, 100W  
 Mx chargeability for the interval 690-1050 msec after shutoff  
 Normalized VP = mV / amp (VP / current x 1000)

NOTE: Grid North 315 Degrees

LIN	STN	SEP	XGD	YGD	VP	SP	Mx	NVP	Mi	TAU	FIT			
3	3	3	2	2	1	1	1	1	1	1	1			
(T62,2A8,A3,T1,3F8.0,F5.0,3F6.0,2F7.0)														
75.0	-15.0	243.46	-13	15.1	487	212	4.000	0.59	100N	15N	1			
75.0	-20.0	277.16	-16	15.5	554	217	4.000	0.45	100N	20N	1			
75.0	-25.0	303.18	-13	15.5	606	218	4.000	0.27	100N	25N	1			
75.0	-30.0	294.86	8	14.9	590	211	4.000	0.34	100N	30N	1			
75.0	-35.0	297.64	6	14.5	595	205	4.000	0.38	100N	35N	1			
75.0	-40.0	291.74	5	15.3	583	215	4.000	0.61	100N	40N	1			
75.0	-45.0	293.43	14	15.2	587	214	4.000	0.10	100N	45N	1			
75.0	-50.0	303.62	16	15.8	607	221	4.000	0.32	100N	50N	1			
75.0	-55.0	288.05	21	16.3	576	235	16.000	0.65	100N	55N	1			
75.0	-60.0	270.39	15	16.1	541	224	4.000	0.61	100N	60N	1			
75.0	-65.0	269.05	2	16.5	538	233	8.000	0.55	100N	65N	1			
75.0	-70.0	273.03	-19	18.0	546	250	8.000	0.51	100N	70N	1			
75.0	-75.0	284.64	-22	19.2	569	269	16.000	0.51	100N	75N	1			
75.0	-80.0	252.87	-7	21.7	506	290	8.000	0.56	100N	80N	1			
75.0	-85.0	240.71	-18	24.3	481	325	16.000	0.18	100N	85N	1			
75.0	-90.0	216.31	2	26.1	433	355	32.000	0.47	100N	90N	1			
75.0	-95.0	204.32	17	24.6	409	353	64.000	0.61	100N	95N	1			
75.0	-100.0	218.17	-4	21.3	436	287	8.000	0.46	100N	100N	1			
75.0	-105.0	198.05	4	20.4	396	278	8.000	0.27	100N	105N	1			
75.0	-110.0	178.70	2	18.2	357	253	8.000	0.08	100N	110N	1			
75.0	-115.0	140.44	-4	18.7	281	255	4.000	0.48	100N	115N	1			
75.0	-120.0	112.91	-12	21.4	226	296	16.000	0.47	100N	120N	1			
75.0	-125.0	83.44	-2	22.0	209	292	4.000	1.09	100N	125N	1			
75.0	-130.0	100.16	-8	22.2	200	297	8.000	0.54	100N	130N	1			
75.0	-135.0	95.80	-7	23.8	192	314	8.000	0.27	100N	135N	1			
75.0	-140.0	100.56	-8	21.3	201	294	16.000	0.28	100N	140N	1			
75.0	-145.0	102.15	6	19.8	255	268	4.000	0.37	100N	145N	1			
75.0	-150.0	148.50	-1	19.9	297	278	16.000	0.45	100N	150N	1			
75.0	-155.0	165.37	6	19.2	331	265	8.000	0.50	100N	155N	1			
75.0	-160.0	149.40	2	19.9	299	272	8.000	0.47	100N	160N	1			
75.0	-165.0	98.38	-10	21.4	246	288	2.000	0.55	100N	165N	1			
150.0	-15.0	116.30	-14	16.8	233	234	2.000	0.88	100E	15N	1			
150.0	-20.0	137.69	-15	16.7	275	233	2.000	0.77	100E	20N	1			
150.0	-25.0	194.73	-13	13.2	389	190	2.000	0.64	100E	25N	1			
150.0	-30.0	276.68	8	10.6	553	157	1.000	0.90	100E	30N	1			
150.0	-35.0	327.72	6	10.1	655	155	0.500	0.69	100E	35N	1			
150.0	-40.0	374.09	6	11.1	748	165	1.000	0.77	100E	40N	1			
150.0	-45.0	391.35	14	12.4	783	180	2.000	0.84	100E	45N	1			
150.0	-50.0	401.01	16	14.5	802	206	2.000	0.68	100E	50N	1			
150.0	-55.0	397.00	21	15.7	794	220	2.000	0.77	100E	55N	1			
150.0	-60.0	374.96	16	16.3	750	228	4.000	0.88	100E	60N	1			
150.0	-65.0	347.39	4	17.7	695	245	4.000	0.66	100E	65N	1			
150.0	-70.0	338.85	-17	19.4	678	265	4.000	0.85	100E	70N	1			
150.0	-75.0	340.62	-21	20.7	681	279	4.000	0.73	100E	75N	1			
150.0	-80.0	310.36	-5	22.7	621	305	8.000	0.87	100E	80N	1			
150.0	-85.0	272.70	-18	25.6	545	334	8.000	0.60	100E	85N	1			
150.0	-90.0	270.22	3	25.3	540	330	8.000	0.71	100E	90N	1			
150.0	-95.0	255.50	17	25.0	511	326	8.000	0.66	100E	95N	1			
150.0	-100.0	271.35	-3	21.5	543	291	8.000	0.91	100E	100N	1			
150.0	-105.0	262.77	5	20.0	526	271	4.000	0.70	100E	105N	1			
150.0	-110.0	234.40	2	18.4	469	254	4.000	0.82	100E	110N	1			
150.0	-115.0	211.99	-5	17.6	424	243	2.000	1.02	100E	115N	1			



150.0	-125.0	246.15	-2	16.1	410	226	4.000	0.53	100E	125N	1
150.0	-130.0	214.42	-8	16.1	429	226	2.000	0.94	100E	130N	1
150.0	-135.0	205.80	-8	17.8	412	246	2.000	0.69	100E	135N	1
150.0	-140.0	188.36	-8	17.6	377	243	2.000	0.88	100E	140N	1
150.0	-145.0	249.61	5	18.7	416	255	4.000	0.35	100E	145N	1
150.0	-150.0	242.62	-0	20.0	485	272	4.000	0.62	100E	150N	1
150.0	-155.0	266.59	6	18.6	533	257	2.000	0.55	100E	155N	1
150.0	-160.0	238.74	2	19.8	477	271	2.000	0.43	100E	160N	1
150.0	-165.0	257.44	-10	19.3	429	265	2.000	0.27	100E	165N	1
225.0	-15.0	142.62	-14	15.0	285	217	1.000	0.97	100S	15N	1
225.0	-20.0	133.28	-15	15.7	267	225	1.000	0.82	100S	20N	1
225.0	-25.0	120.90	-13	15.4	242	221	1.000	0.99	100S	25N	1
225.0	-30.0	102.10	8	14.2	204	212	0.500	1.00	100S	30N	1
225.0	-35.0	90.26	7	9.7	181	195	0.031	0.76	100S	35N	1
225.0	-40.0	67.30	6	8.9	135	180	0.031	0.42	100S	40N	1
225.0	-45.0	47.46	14	5.6	95	379	0.000	4.68	100S	45N	1
225.0	-50.0	-50.93	17	12.6	-102	246	0.031	0.88	100S	50N	1
225.0	-55.0	-28.92	21	27.4	-58	374	0.500	0.72	100S	55N	1
225.0	-60.0	-5.58	16	43.0	-11	241	0.000	3.98	100S	60N	1
225.0	-65.0	18.58	5	30.4	37	511048	0.000	6.67	100S	65N	1
225.0	-70.0	45.06	-16	32.1	90	424	64.000	0.43	100S	70N	1
225.0	-75.0	71.47	-21	29.4	143	386	32.000	0.53	100S	75N	1
225.0	-80.0	117.52	-5	23.7	235	320	16.000	0.82	100S	80N	1
225.0	-85.0	108.64	-18	23.9	217	323	16.000	0.74	100S	85N	1
225.0	-90.0	185.99	3	19.0	372	261	8.000	0.57	100S	90N	1
225.0	-95.0	214.88	17	16.5	430	229	4.000	0.75	100S	95N	1
225.0	-100.0	196.10	-4	16.6	392	230	4.000	0.84	100S	100N	1
225.0	-105.0	220.18	5	15.4	440	217	4.000	0.71	100S	105N	1
225.0	-110.0	202.05	2	12.6	404	182	4.000	0.46	100S	110N	1
225.0	-115.0	256.60	-5	11.4	513	166	4.000	0.48	100S	115N	1
225.0	-120.0	321.24	-13	10.7	642	156	2.000	0.57	100S	120N	1
225.0	-125.0	348.29	-2	10.1	697	148	2.000	0.54	100S	125N	1
225.0	-130.0	355.77	-9	11.4	712	168	1.000	0.70	100S	130N	1
225.0	-135.0	317.29	-8	14.8	635	210	2.000	0.71	100S	135N	1
225.0	-140.0	272.26	-8	15.3	545	216	2.000	0.63	100S	140N	1
225.0	-145.0	283.48	6	16.7	567	234	4.000	0.83	100S	145N	1
225.0	-150.0	323.79	-1	18.7	648	256	4.000	0.57	100S	150N	1
225.0	-155.0	340.22	6	17.3	680	241	2.000	0.42	100S	155N	1
225.0	-160.0	310.41	3	18.9	621	259	2.000	0.40	100S	160N	1
225.0	-165.0	277.60	-10	19.4	555	266	2.000	0.59	100S	165N	1
300.0	-15.0	28.41	-13	-2.9	28	0	0.000	0.00	100W	15N	1
300.0	-20.0	102.64	-15	14.7	103	286	0.031	0.46	100W	20N	1
300.0	-25.0	131.34	-13	20.2	131	303	0.250	0.67	100W	25N	1
300.0	-30.0	116.74	8	25.0	117	349	0.500	0.31	100W	30N	1
300.0	-35.0	151.69	7	29.1	152	381	1.000	0.35	100W	35N	1
300.0	-40.0	177.15	5	31.3	177	403	1.000	0.53	100W	40N	1
300.0	-45.0	193.10	15	28.9	193	379	1.000	0.33	100W	45N	1
300.0	-50.0	202.58	16	25.0	203	347	0.500	0.31	100W	50N	1
300.0	-55.0	191.44	21	23.2	191	327	0.500	0.36	100W	55N	1
300.0	-60.0	194.55	16	22.1	195	313	0.500	0.27	100W	60N	1
300.0	-65.0	237.34	5	23.2	237	317	1.000	0.47	100W	65N	1
300.0	-70.0	275.96	-16	26.8	276	355	1.000	0.61	100W	70N	1
300.0	-75.0	307.33	-21	30.4	307	385	2.000	0.54	100W	75N	1
300.0	-80.0	300.80	-5	32.3	301	402	2.000	0.72	100W	80N	1
300.0	-85.0	310.65	-19	33.1	311	407	4.000	0.55	100W	85N	1
300.0	-90.0	311.26	3	35.3	311	426	4.000	0.59	100W	90N	1
300.0	-95.0	322.32	16	31.7	322	394	4.000	0.52	100W	95N	1
300.0	-100.0	311.50	-4	30.4	312	384	2.000	0.60	100W	100N	1
300.0	-105.0	289.62	4	29.4	290	375	2.000	0.43	100W	105N	1
300.0	-110.0	263.06	3	25.4	263	334	2.000	0.57	100W	110N	1
300.0	-115.0	246.96	-6	24.0	247	318	2.000	0.56	100W	115N	1
300.0	-120.0	258.70	-14	23.5	259	311	2.000	0.82	100W	120N	1
300.0	-125.0	247.66	-2	24.2	248	318	4.000	0.73	100W	125N	1
300.0	-130.0	227.23	-8	26.8	227	347	2.000	0.85	100W	130N	1
300.0	-135.0	193.95	-9	31.0	194	387	4.000	0.52	100W	135N	1
300.0	-140.0	186.73	-8	29.2	187	368	4.000	0.60	100W	140N	1

300.0	-150.0	257.06	1	26.2	257	341	8.000	0.56	100W	150N	1
300.0	-155.0	282.33	6	24.6	282	321	4.000	0.43	100W	155N	1
300.0	-160.0	271.59	2	24.8	272	322	4.000	0.50	100W	160N	1
300.0	-165.0	230.15	-9	26.5	230	343	4.000	0.48	100W	165N	1

GEOLOGICAL SURVEY BRANCH  
ASSESSMENT REPORT

24,938

\$\$DATASS 12 -1 9 -2000 1 1 Sept/96  
 Array:G Trav dir:S Current:T Num Sep:3 A Spc:20,20,20 Eff.Sep:1,2,3  
 TEUTON RESOURCES CORP. - CLONE PROJECT, STEWART, B.C.  
 CL96-30 : Az 065, Dip -70, Depth 362 m (Blocked at 282 m)  
 DOWNHOLE IP SURVEY

vertical gradient array, C2 @ 1200N; C1 @ 100N, 100E, 100S,  
 200N, 200E, 200S, no western electrodes

Mx chargeability for the interval 690-1050 msec after shutoff

Normalized VP = mV / amp (VP / current x 1000)

NOTE: Grid North 315 Degrees

LIN	STN	SEP	XGD	YGD	VP	SP	Mx	NVP	Mi	TAU	FIT		
3	3	3	2	2	1	1	1	1	1	1	1		
(T62,2A8,A3,T1,3F8.0,F5.0,3F6.0,2F7.0)													
75.0	-15.0	106.65	23	20.3	533	320	0.125	3.24	100E	-15	1		
75.0	-20.0	82.92	3	23.2	415	313	8.000	4.45	100E	-20	1		
75.0	-25.0	93.17	2	16.0	466	271	0.062	5.30	100E	-25	1		
75.0	-30.0	91.05	-0	19.6	455	268	8.000	0.42	100E	-30	1		
75.0	-35.0	132.60	-43	16.4	530	232	8.000	0.80	100E	-35	1		
75.0	-40.0	108.70	-11	14.2	544	205	8.000	1.05	100E	-40	1		
75.0	-45.0	72.47	-0	17.0	362	245	16.000	1.43	100E	-45	1		
75.0	-50.0	-71.02	4	17.6	-236	246	8.000	1.85	100E	-50	1		
75.0	-55.0	-165.10	5	14.6	-660	207	4.000	1.45	100E	-55	1		
75.0	-60.0	-115.81	15	10.1	-579	149	4.000	1.40	100E	-60	1		
75.0	-65.0	-56.24	-3	2.2	-281	37	16.000	8.67	100E	-65	1		
75.0	-70.0	31.33	-0	66.6	104	660	4.000	0.64	100E	-70	1		
75.0	-75.0	60.19	1	34.5	241	421	8.000	0.59	100E	-75	1		
75.0	-80.0	77.21	5	20.4	386	276	4.000	0.67	100E	-80	1		
75.0	-85.0	61.41	9	16.9	307	236	8.000	0.49	100E	-85	1		
75.0	-90.0	110.40	1	14.0	368	213	32.000	0.53	100E	-90	1		
75.0	-95.0	108.52	16	14.1	362	256	256.000	0.72	100E	-95	1		
75.0	-100.0	53.80	57	20.6	179	416	048.000	2.05	100E	-100	1		
75.0	-105.0	85.95	5	21.4	287	401	024.000	0.28	100E	-105	1		
75.0	-110.0	113.88	10	18.4	380	381	048.000	4.23	100E	-110	1		
75.0	-115.0	172.69	-10	14.9	576	218	16.000	0.92	100E	-115	1		
75.0	-120.0	231.03	-53	14.2	770	203	8.000	1.26	100E	-120	1		
75.0	-125.0	270.67	-10	12.7	902	184	2.000	1.50	100E	-125	1		
75.0	-130.0	235.55	-7	14.5	785	216	0.500	2.14	100E	-130	1		
75.0	-135.0	170.37	2	17.4	568	242	8.000	0.68	100E	-135	1		
75.0	-140.0	135.00	4	20.8	450	280	4.000	0.73	100E	-140	1		
75.0	-145.0	86.24	6	30.4	287	379	4.000	0.64	100E	-145	1		
75.0	-150.0	99.55	7	29.4	332	375	2.000	0.52	100E	-150	1		
75.0	-155.0	121.04	9	29.3	403	385	1.000	1.05	100E	-155	1		
75.0	-160.0	161.03	11	23.0	537	305	2.000	1.03	100E	-160	1		
75.0	-165.0	193.89	9	21.1	646	284	2.000	0.71	100E	-165	1		
75.0	-170.0	193.55	11	21.1	645	285	2.000	0.51	100E	-170	1		
75.0	-175.0	199.07	1	17.3	664	269	64.000	2.03	100E	-175	1		
75.0	-180.0	167.53	6	19.1	558	262	2.000	0.41	100E	-180	1		
75.0	-185.0	133.21	-9	21.2	444	286	8.000	0.32	100E	-185	1		
75.0	-190.0	133.24	-7	21.4	444	290	2.000	1.10	100E	-190	1		
75.0	-195.0	89.79	12	27.4	299	398	0.250	3.74	100E	-195	1		
75.0	-200.0	87.52	-12	27.0	292	346	8.000	1.58	100E	-200	1		
75.0	-205.0	84.71	71	25.9	282	350	32.000	1.20	100E	-205	1		
75.0	-210.0	84.93	85	26.2	283	344	2.000	1.17	100E	-210	1		
75.0	-215.0	83.57	55	25.6	279	473	0.031	4.35	100E	-215	1		
75.0	-220.0	95.89	-3	20.2	320	469	0.007	6.86	100E	-220	1		
75.0	-225.0	122.57	-64	18.3	350	257	1.000	2.63	100E	-225	1		
75.0	-230.0	159.80	-14	17.7	457	341	0.031	3.85	100E	-230	1		
75.0	-235.0	106.01	-52	19.2	353	269	16.000	1.60	100E	-235	1		
75.0	-240.0	123.21	-1	17.9	411	275	64.000	5.74	100E	-240	1		
75.0	-245.0	140.16	-4	16.6	400	233	8.000	3.07	100E	-245	1		
75.0	-250.0	121.80	-22	21.5	348	133	0.000	4.04	100E	-250	1		
75.0	-255.0	120.31	-4	15.9	401	228	1.000	0.39	100E	-255	1		
75.0	-260.0	102.13	-6	17.3	340	333	0.031	4.99	100E	-260	1		
75.0	-265.0	95.20	4	17.6	272	270	0.250	3.06	100E	-265	1		
75.0	-270.0	87.40	4	12.5	250	0	0.000	0.00	100E	-270	1		

150.0	-20.0	69.66	7	26.3	100	354	0.500	3.39	200E	-20	1
150.0	-25.0	84.22	6	28.9	120	0	0.000	0.00	200E	-25	1
150.0	-30.0	89.14	1	20.1	127	281	1.000	0.55	200E	-30	1
150.0	-35.0	-92.50	-42	17.7	-154	252	1.000	0.93	200E	-35	1
150.0	-40.0	-99.56	-8	17.2	-166	240	2.000	0.71	200E	-40	1
150.0	-45.0	-89.38	-0	19.5	-128	266	4.000	0.85	200E	-45	1
150.0	-50.0	100.40	4	19.6	112	265	4.000	0.76	200E	-50	1
150.0	-55.0	149.74	2	18.1	250	251	2.000	0.96	200E	-55	1
150.0	-60.0	151.57	9	16.6	253	231	2.000	0.96	200E	-60	1
150.0	-65.0	141.84	-3	15.8	203	223	8.000	0.32	200E	-65	1
150.0	-70.0	66.07	-1	7.1	73	117	0.250	2.10	200E	-70	1
150.0	-75.0	35.37	0	5.2	59	145048.000		2.20	200E	-75	1
150.0	-80.0	23.26	1	16.3	39	231	8.000	0.64	200E	-80	1
150.0	-85.0	49.37	9	23.4	71	347	0.250	1.81	200E	-85	1
150.0	-90.0	55.72	1	31.0	62	386	8.000	0.49	200E	-90	1
150.0	-95.0	-56.77	16	32.2	-63	404	16.000	0.91	200E	-95	1
150.0	-100.0	89.24	57	24.0	99	317	8.000	0.64	200E	-100	1
150.0	-105.0	62.47	5	24.7	69	335	1.000	0.67	200E	-105	1
150.0	-110.0	57.50	10	24.2	64	382	0.125	1.47	200E	-110	1
150.0	-115.0	-13.23	-10	45.2	-15	249	0.000	1.08	200E	-115	1
150.0	-120.0	-21.44	-53	-7.3	-24	-51	0.000	40.30	200E	-120	1
150.0	-125.0	-67.11	-9	3.7	-75	0	0.000	0.00	200E	-125	1
150.0	-130.0	-50.37	-7	7.9	-56	194048.000		19.79	200E	-130	1
150.0	-135.0	5.98	2	-8.4	7	-86	0.000	64.94	200E	-135	1
150.0	-140.0	17.14	5	-5.8	19	0	0.000	0.00	200E	-140	1
150.0	-145.0	56.30	6	-2.1	63	-62048.000		13.86	200E	-145	1
150.0	-150.0	17.97	7	-51.6	20	-70	0.125	1.24	200E	-150	1
150.0	-155.0	17.17	10	107.2	19	106	0.250	0.60	200E	-155	1
150.0	-160.0	90.88	11	27.8	101	357	8.000	1.25	200E	-160	1
150.0	-165.0	157.99	9	22.3	176	298	8.000	0.87	200E	-165	1
150.0	-170.0	157.79	10	22.4	175	300	8.000	0.65	200E	-170	1
150.0	-175.0	169.93	0	17.8	189	245	4.000	1.74	200E	-175	1
150.0	-180.0	135.14	5	18.5	150	256	8.000	0.43	200E	-180	1
150.0	-185.0	91.99	-9	23.5	102	326	32.000	0.33	200E	-185	1
150.0	-190.0	92.23	-7	23.3	102	307	4.000	1.31	200E	-190	1
150.0	-195.0	38.28	14	66.0	43	650	32.000	1.23	200E	-195	1
150.0	-200.0	45.96	-11	64.5	51	648	64.000	1.05	200E	-200	1
150.0	-205.0	30.91	71	88.0	34	754	64.000	0.74	200E	-205	1
150.0	-210.0	31.22	86	87.3	35	761	8.000	0.87	200E	-210	1
150.0	-215.0	33.23	55	87.6	33	889	0.500	1.68	200E	-215	1
150.0	-220.0	107.46	-3	29.7	107	425	0.250	1.59	200E	-220	1
150.0	-225.0	149.28	-64	23.8	166	314	4.000	0.67	200E	-225	1
150.0	-230.0	247.98	-13	20.8	248	281	2.000	1.19	200E	-230	1
150.0	-235.0	168.46	-53	24.3	168	324	16.000	0.53	200E	-235	1
150.0	-240.0	221.87	-1	22.1	222	311	32.000	0.90	200E	-240	1
150.0	-245.0	210.72	-4	19.7	234	267	4.000	0.38	200E	-245	1
150.0	-250.0	172.95	-23	24.9	173	347	0.500	1.13	200E	-250	1
150.0	-255.0	234.70	-3	19.3	235	264	2.000	0.39	200E	-255	1
150.0	-260.0	169.82	-6	21.6	170	294	2.000	1.12	200E	-260	1
150.0	-265.0	118.61	6	24.5	132	324	8.000	0.52	200E	-265	1
150.0	-270.0	124.79	-4	23.7	125	429024.000		3.27	200E	-270	1

\$\$DATA\$\$ 12 -1 9 -2000 1 Sept/96  
 Array:G Trav dir:S Current:T Num Sep:3 A Spc:20,20,20 Eff.Sep:1,2,3  
 TEUTON RESOURCES CORP. - CLONE PROJECT, STEWART, B.C.  
 CL96-30 : Az 065, Dip -70, Depth 362 m (Blocked at 282 m)

DOWNHOLE IP SURVEY

vertical gradient array, C2 @ 1200N; C1 @ 100N, 100E, 100S,  
 200N, 200E, 200S, no western electrodes

Mx chargeability for the interval 690-1050 msec after shutoff

Normalized VP = mV / amp (VP / current x 1000)

NOTE: Grid North 315 Degrees

LIN	STN	SEP	XGD	YGD	VP	SP	Mx	NVP	Mi	TAU	FIT		
3	3	3	2	2	1	1	1	1	1	1	1		
(T62,2A8,A3,T1,3F8.0,F5.0,3F6.0,2F7.0)													
75.0	-15.0	175.08	23	21.0	175	279	2.000	1.68	200N	15N	1		
75.0	-20.0	169.21	7	23.5	169	312	2.000	0.39	200N	20N	1		
75.0	-25.0	182.74	6	24.1	183	4115	12.000	4.06	200N	25N	1		
75.0	-30.0	206.74	1	20.5	207	277	4.000	0.69	200N	30N	1		
75.0	-35.0	-238.57	-42	18.9	-239	279	2.000	0.82	200N	35N	1		
75.0	-40.0	-233.71	-9	17.7	-234	245	4.000	0.59	200N	40N	1		
75.0	-45.0	-217.09	-1	18.9	-217	259	4.000	0.46	200N	45N	1		
75.0	-50.0	197.68	4	19.8	198	268	4.000	0.57	200N	50N	1		
75.0	-55.0	415.47	2	19.0	415	260	4.000	0.81	200N	55N	1		
75.0	-60.0	431.28	10	17.7	431	245	4.000	0.70	200N	60N	1		
75.0	-65.0	412.93	-4	17.7	413	245	4.000	0.46	200N	65N	1		
75.0	-70.0	198.89	-1	15.3	199	215	2.000	0.59	200N	70N	1		
75.0	-75.0	188.55	-0	14.7	189	208	4.000	0.37	200N	75N	1		
75.0	-80.0	161.56	1	15.9	162	223	4.000	0.63	200N	80N	1		
75.0	-85.0	164.70	8	16.7	165	232	2.000	0.94	200N	85N	1		
75.0	-90.0	177.46	1	17.5	177	242	4.000	0.75	200N	90N	1		
75.0	-95.0	197.58	16	18.6	198	254	4.000	0.97	200N	95N	1		
75.0	-100.0	209.92	57	17.4	210	241	4.000	0.72	200N	100N	1		
75.0	-105.0	198.04	4	18.4	198	252	4.000	0.74	200N	105N	1		
75.0	-110.0	204.04	10	18.8	204	257	4.000	0.92	200N	110N	1		
75.0	-115.0	194.93	-10	18.3	195	250	4.000	0.54	200N	115N	1		
75.0	-120.0	191.27	-54	20.7	191	279	4.000	1.08	200N	120N	1		
75.0	-125.0	201.71	-10	20.6	202	277	4.000	0.44	200N	125N	1		
75.0	-130.0	190.86	-7	20.0	191	270	4.000	0.54	200N	130N	1		
75.0	-135.0	178.24	1	21.7	178	290	4.000	0.48	200N	135N	1		
75.0	-140.0	189.60	4	20.0	190	272	8.000	0.40	200N	140N	1		
75.0	-145.0	189.46	5	19.3	189	263	4.000	0.50	200N	145N	1		
75.0	-150.0	184.34	6	20.4	184	276	4.000	0.52	200N	150N	1		
75.0	-155.0	189.87	10	20.4	190	276	2.000	1.03	200N	155N	1		
75.0	-160.0	185.50	11	20.5	186	277	2.000	0.91	200N	160N	1		
75.0	-165.0	183.30	9	20.2	183	274	4.000	0.64	200N	165N	1		
75.0	-170.0	183.00	10	20.3	183	276	4.000	0.75	200N	170N	1		
75.0	-175.0	194.19	1	19.7	194	284	0.500	1.33	200N	175N	1		
75.0	-180.0	186.74	5	20.4	187	276	4.000	0.27	200N	180N	1		
75.0	-185.0	174.80	-9	22.1	175	295	4.000	0.71	200N	185N	1		
75.0	-190.0	174.55	-7	22.2	175	297	2.000	0.89	200N	190N	1		
75.0	-195.0	137.61	13	20.0	138	289	32.000	0.58	200N	195N	1		
75.0	-200.0	126.92	-12	20.5	127	278	4.000	1.17	200N	200N	1		
75.0	-205.0	137.49	71	18.4	137	253	4.000	1.13	200N	205N	1		
75.0	-210.0	137.73	85	18.2	138	253	2.000	1.60	200N	210N	1		
75.0	-215.0	135.93	55	18.0	136	277	0.250	4.15	200N	215N	1		
75.0	-220.0	125.78	-3	19.3	126	313	0.125	4.68	200N	220N	1		
75.0	-225.0	120.04	-64	18.0	120	249	2.000	1.31	200N	225N	1		
75.0	-230.0	146.52	-12	17.8	147	272	0.250	3.29	200N	230N	1		
75.0	-235.0	121.36	-53	18.1	121	250	8.000	1.41	200N	235N	1		
75.0	-240.0	140.32	-1	16.8	140	262	64.000	3.75	200N	240N	1		
75.0	-245.0	146.01	-4	15.8	146	223	4.000	0.96	200N	245N	1		
75.0	-250.0	152.17	-23	17.5	152	257	0.500	1.48	200N	250N	1		
75.0	-255.0	146.75	-3	15.6	147	223	1.000	0.63	200N	255N	1		
75.0	-260.0	152.27	-6	17.3	152	282	0.125	2.97	200N	260N	1		
75.0	-265.0	128.93	5	17.6	129	248	1.000	1.49	200N	265N	1		

150.0	-15.0	440.07	22	20.9	440	284	2.000	0.78	100N	15N	1
150.0	-20.0	421.04	2	24.0	421	313	2.000	1.43	100N	20N	1
150.0	-25.0	456.84	0	19.6	457	274	1.000	2.95	100N	25N	1
150.0	-30.0	507.62	-1	19.8	508	272	2.000	0.84	100N	30N	1
150.0	-35.0	-575.27	-43	18.6	-575	258	2.000	0.90	100N	35N	1
150.0	-40.0	-564.71	-13	17.6	-565	245	2.000	0.63	100N	40N	1
150.0	-45.0	-501.82	-1	19.4	-502	265	2.000	0.67	100N	45N	1
150.0	-50.0	448.58	5	19.8	449	269	2.000	0.86	100N	50N	1
150.0	-55.0	968.75	9	19.0	969	262	2.000	0.80	100N	55N	1
150.0	-60.0	982.05	18	18.1	982	251	2.000	0.74	100N	60N	1
150.0	-65.0	911.56	-4	18.6	912	256	2.000	0.60	100N	65N	1
150.0	-70.0	400.16	0	16.8	400	235	2.000	0.67	100N	70N	1
150.0	-75.0	382.47	1	16.0	382	224	2.000	0.42	100N	75N	1
150.0	-80.0	332.34	6	16.7	332	233	2.000	0.52	100N	80N	1
150.0	-85.0	327.63	7	17.6	328	244	2.000	1.04	100N	85N	1
150.0	-90.0	334.66	1	18.6	335	255	2.000	0.91	100N	90N	1
150.0	-95.0	352.18	16	19.6	352	267	4.000	0.88	100N	95N	1
150.0	-100.0	357.35	57	18.6	357	255	4.000	0.71	100N	100N	1
150.0	-105.0	337.10	5	19.2	337	262	4.000	1.06	100N	105N	1
150.0	-110.0	350.11	10	19.3	350	264	2.000	1.13	100N	110N	1
150.0	-115.0	341.85	-10	18.2	342	250	4.000	0.45	100N	115N	1
150.0	-120.0	343.62	-53	19.9	344	272	2.000	0.99	100N	120N	1
150.0	-125.0	356.22	-11	19.6	356	266	4.000	0.31	100N	125N	1
150.0	-130.0	326.95	-7	19.4	327	267	8.000	0.48	100N	130N	1
150.0	-135.0	292.96	1	21.3	293	287	4.000	0.59	100N	135N	1
150.0	-140.0	295.04	4	19.8	295	270	8.000	0.40	100N	140N	1
150.0	-145.0	283.93	6	19.6	284	266	4.000	0.46	100N	145N	1
150.0	-150.0	270.53	7	20.5	271	277	4.000	0.52	100N	150N	1
150.0	-155.0	276.33	9	20.6	276	279	2.000	0.95	100N	155N	1
150.0	-160.0	270.38	11	20.8	270	282	2.000	0.88	100N	160N	1
150.0	-165.0	267.27	9	20.4	267	277	4.000	0.74	100N	165N	1
150.0	-170.0	267.31	12	20.4	267	276	2.000	0.82	100N	170N	1
150.0	-175.0	281.78	1	19.9	282	302	0.250	2.36	100N	175N	1
150.0	-180.0	267.22	6	20.1	267	271	4.000	0.44	100N	180N	1
150.0	-185.0	246.33	-9	21.8	246	294	2.000	0.79	100N	185N	1
150.0	-190.0	246.46	-6	22.0	246	295	2.000	0.85	100N	190N	1
150.0	-195.0	193.52	12	19.3	194	326256	6.000	2.42	100N	195N	1
150.0	-200.0	178.00	-13	20.4	178	283	1.000	1.35	100N	200N	1
150.0	-205.0	190.44	71	17.9	190	253	1.000	1.30	100N	205N	1
150.0	-210.0	191.15	84	17.9	191	252	1.000	1.26	100N	210N	1
150.0	-215.0	188.93	57	18.3	189	278	0.250	2.58	100N	215N	1
150.0	-220.0	170.43	-2	19.7	170	298	0.250	2.25	100N	220N	1
150.0	-225.0	159.93	-66	17.5	160	247	1.000	1.32	100N	225N	1
150.0	-230.0	193.74	-14	17.9	194	273	0.250	2.18	100N	230N	1
150.0	-235.0	161.47	-53	17.5	161	244	8.000	0.42	100N	235N	1
150.0	-240.0	183.90	-1	15.7	184	227	16.000	1.58	100N	240N	1
150.0	-245.0	187.66	-4	15.4	188	217	4.000	0.57	100N	245N	1
150.0	-250.0	194.72	-22	17.8	195	252	1.000	0.80	100N	250N	1
150.0	-255.0	188.40	-4	15.2	188	218	1.000	0.51	100N	255N	1
150.0	-260.0	193.38	-7	17.7	193	271	0.250	1.62	100N	260N	1
150.0	-265.0	163.91	3	17.3	164	246	1.000	0.83	100N	265N	1
150.0	-270.0	150.64	-4	15.2	151	220	16.000	1.06	100N	270N	1
225.0	-15.0	72.91	22	22.9	146	457	0.015	2.80	100S	15N	1
225.0	-20.0	65.43	3	28.5	131	439	0.250	10.13	100S	20N	1
225.0	-25.0	14.32	4	23.1	29	922048	0.000	15.66	100S	25N	1
225.0	-30.0	114.68	0	17.7	229	251	16.000	2.38	100S	30N	1
225.0	-35.0	99.88	-42	9.8	250	151	16.000	3.86	100S	35N	1
225.0	-40.0	16.21	-9	-91.0	32	-10	0.125	2.52	100S	40N	1
225.0	-45.0	37.59	0	-32.1	75	-45	0.250	2.66	100S	45N	1
225.0	-50.0	58.85	4	39.8	98	507	0.500	1.22	100S	50N	1
225.0	-55.0	-75.85	3	-14.9	-190	-21	0.500	3.89	100S	55N	1
225.0	-60.0	46.93	11	117.3	94	902	4.000	1.03	100S	60N	1
225.0	-65.0	73.00	-4	85.5	146	749	8.000	0.99	100S	65N	1
225.0	-70.0	153.17	-1	44.9	255	506	8.000	0.34	100S	70N	1
225.0	-75.0	158.70	0	29.4	397	371	4.000	0.50	100S	75N	1
225.0	-80.0	319.01	2	19.4	638	266	8.000	0.42	100S	80N	1

150.0	-20.0	421.04	2	24.0	421	313	2.000	1.43	100N	20N	1
150.0	-25.0	456.84	0	19.6	457	274	1.000	2.95	100N	25N	1
150.0	-30.0	507.62	-1	19.8	508	272	2.000	0.84	100N	30N	1
150.0	-35.0	-575.27	-43	18.6	-575	258	2.000	0.90	100N	35N	1
150.0	-40.0	-564.71	-13	17.6	-565	245	2.000	0.63	100N	40N	1
150.0	-45.0	-501.82	-1	19.4	-502	265	2.000	0.67	100N	45N	1
150.0	-50.0	448.58	5	19.8	449	269	2.000	0.86	100N	50N	1
150.0	-55.0	968.75	9	19.0	969	262	2.000	0.80	100N	55N	1
150.0	-60.0	982.05	18	18.1	982	251	2.000	0.74	100N	60N	1
150.0	-65.0	911.56	-4	18.6	912	256	2.000	0.60	100N	65N	1
150.0	-70.0	400.16	0	16.8	400	235	2.000	0.67	100N	70N	1
150.0	-75.0	382.47	1	16.0	382	224	2.000	0.42	100N	75N	1
150.0	-80.0	332.34	6	16.7	332	233	2.000	0.52	100N	80N	1
150.0	-85.0	327.63	7	17.6	328	244	2.000	1.04	100N	85N	1
150.0	-90.0	334.66	1	18.6	335	255	2.000	0.91	100N	90N	1
150.0	-95.0	352.18	16	19.6	352	267	4.000	0.88	100N	95N	1
150.0	-100.0	357.35	57	18.6	357	255	4.000	0.71	100N	100N	1
150.0	-105.0	337.10	5	19.2	337	262	4.000	1.06	100N	105N	1
150.0	-110.0	350.11	10	19.3	350	264	2.000	1.13	100N	110N	1
150.0	-115.0	341.85	-10	18.2	342	250	4.000	0.45	100N	115N	1
150.0	-120.0	343.62	-53	19.9	344	272	2.000	0.99	100N	120N	1
150.0	-125.0	356.22	-11	19.6	356	266	4.000	0.31	100N	125N	1
150.0	-130.0	326.95	-7	19.4	327	267	8.000	0.48	100N	130N	1
150.0	-135.0	292.96	1	21.3	293	287	4.000	0.59	100N	135N	1
150.0	-140.0	295.04	4	19.8	295	270	8.000	0.40	100N	140N	1
150.0	-145.0	283.93	6	19.6	284	266	4.000	0.46	100N	145N	1
150.0	-150.0	270.53	7	20.5	271	277	4.000	0.52	100N	150N	1
150.0	-155.0	276.33	9	20.6	276	279	2.000	0.95	100N	155N	1
150.0	-160.0	270.38	11	20.8	270	282	2.000	0.88	100N	160N	1
150.0	-165.0	267.27	9	20.4	267	277	4.000	0.74	100N	165N	1
150.0	-170.0	267.31	12	20.4	267	276	2.000	0.82	100N	170N	1
150.0	-175.0	281.78	1	19.9	282	302	0.250	2.36	100N	175N	1
150.0	-180.0	267.22	6	20.1	267	271	4.000	0.44	100N	180N	1
150.0	-185.0	246.33	-9	21.8	246	294	2.000	0.79	100N	185N	1
150.0	-190.0	246.46	-6	22.0	246	295	2.000	0.85	100N	190N	1
150.0	-195.0	193.52	12	19.3	194	326256	56.000	2.42	100N	195N	1
150.0	-200.0	178.00	-13	20.4	178	283	1.000	1.35	100N	200N	1
150.0	-205.0	190.44	71	17.9	190	253	1.000	1.30	100N	205N	1
150.0	-210.0	191.15	84	17.9	191	252	1.000	1.26	100N	210N	1
150.0	-215.0	188.93	57	18.3	189	278	0.250	2.58	100N	215N	1
150.0	-220.0	170.43	-2	19.7	170	298	0.250	2.25	100N	220N	1
150.0	-225.0	159.93	-66	17.5	160	247	1.000	1.32	100N	225N	1
150.0	-230.0	193.74	-14	17.9	194	273	0.250	2.18	100N	230N	1
150.0	-235.0	161.47	-53	17.5	161	244	8.000	0.42	100N	235N	1
150.0	-240.0	183.90	-1	15.7	184	227	16.000	1.58	100N	240N	1
150.0	-245.0	187.66	-4	15.4	188	217	4.000	0.57	100N	245N	1
150.0	-250.0	194.72	-22	17.8	195	252	1.000	0.80	100N	250N	1
150.0	-255.0	188.40	-4	15.2	188	218	1.000	0.51	100N	255N	1
150.0	-260.0	193.38	-7	17.7	193	271	0.250	1.62	100N	260N	1
150.0	-265.0	163.91	3	17.3	164	246	1.000	0.83	100N	265N	1
150.0	-270.0	150.64	-4	15.2	151	220	16.000	1.06	100N	270N	1
225.0	-15.0	72.91	22	22.9	146	457	0.015	2.80	100S	15N	1
225.0	-20.0	65.43	3	28.5	131	439	0.250	10.13	100S	20N	1
225.0	-25.0	14.32	4	23.1	29	922048	0.000	15.66	100S	25N	1
225.0	-30.0	114.68	0	17.7	229	251	16.000	2.38	100S	30N	1
225.0	-35.0	99.88	-42	9.8	250	151	16.000	3.86	100S	35N	1
225.0	-40.0	16.21	-9	-91.0	32	-10	0.125	2.52	100S	40N	1
225.0	-45.0	37.59	0	-32.1	75	-45	0.250	2.66	100S	45N	1
225.0	-50.0	58.85	4	39.8	98	507	0.500	1.22	100S	50N	1
225.0	-55.0	-75.85	3	-14.9	-190	-21	0.500	3.89	100S	55N	1
225.0	-60.0	46.93	11	117.3	94	902	4.000	1.03	100S	60N	1
225.0	-65.0	73.00	-4	85.5	146	749	8.000	0.99	100S	65N	1
225.0	-70.0	153.17	-1	44.9	255	506	8.000	0.34	100S	70N	1
225.0	-75.0	158.70	0	29.4	397	371	4.000	0.50	100S	75N	1
225.0	-80.0	319.01	2	19.4	638	266	8.000	0.43	100S	80N	1

225.0	-85.0	309.69	8	18.7	619	264	16.000	0.70	100S	85N	1
225.0	-90.0	351.01	1	21.6	585	287	4.000	0.68	100S	90N	1
225.0	-95.0	277.49	16	24.7	462	329	16.000	0.29	100S	95N	1
225.0	-100.0	159.34	57	38.2	266	476	64.000	0.24	100S	100N	1
225.0	-105.0	246.32	5	28.4	411	391	64.000	0.53	100S	105N	1
225.0	-110.0	383.08	10	18.5	638	255	8.000	0.62	100S	110N	1
225.0	-115.0	552.03	-10	12.3	920	178	2.000	0.72	100S	115N	1
225.0	-120.0	714.89	-53	10.7	1191	165	0.500	0.92	100S	120N	1
225.0	-125.0	731.84	-9	9.5	1220	153	0.250	0.80	100S	125N	1
225.0	-130.0	623.13	-7	10.7	1039	164	0.500	0.55	100S	130N	1
225.0	-135.0	480.70	2	13.2	801	193	1.000	0.64	100S	135N	1
225.0	-140.0	374.32	4	14.6	624	207	4.000	0.29	100S	140N	1
225.0	-145.0	278.24	6	18.0	464	248	4.000	0.44	100S	145N	1
225.0	-150.0	255.00	7	19.8	425	269	2.000	0.86	100S	150N	1
225.0	-155.0	313.05	10	20.8	447	282	4.000	0.70	100S	155N	1
225.0	-160.0	304.63	11	19.7	508	268	2.000	0.44	100S	160N	1
225.0	-165.0	385.56	8	19.1	551	260	4.000	0.12	100S	165N	1
225.0	-170.0	392.00	11	19.0	560	260	4.000	0.22	100S	170N	1
225.0	-175.0	413.52	1	16.7	591	239	1.000	1.03	100S	175N	1
225.0	-180.0	317.85	5	17.6	530	244	4.000	0.60	100S	180N	1
225.0	-185.0	314.96	-9	19.0	450	259	4.000	0.18	100S	185N	1
225.0	-190.0	320.17	-7	18.8	457	258	4.000	0.32	100S	190N	1
225.0	-195.0	241.47	13	18.9	345	287	64.000	0.90	100S	195N	1
225.0	-200.0	201.86	-12	19.3	336	264	2.000	0.78	100S	200N	1
225.0	-205.0	241.16	71	17.0	345	237	2.000	0.49	100S	205N	1
225.0	-210.0	246.00	85	16.7	351	234	2.000	0.64	100S	210N	1
225.0	-215.0	243.74	55	17.2	348	244	1.000	0.47	100S	215N	1
225.0	-220.0	194.36	-3	16.9	324	278	0.125	1.01	100S	220N	1
225.0	-225.0	220.72	-64	15.6	315	221	2.000	0.69	100S	225N	1
225.0	-230.0	270.86	-14	15.5	387	223	1.000	0.65	100S	230N	1
225.0	-235.0	222.86	-52	15.4	318	217	4.000	0.21	100S	235N	1
225.0	-240.0	211.95	-1	14.9	353	217	16.000	0.43	100S	240N	1
225.0	-245.0	239.53	-3	14.5	342	205	2.000	0.32	100S	245N	1
225.0	-250.0	231.21	-22	18.1	330	263	0.500	0.57	100S	250N	1
225.0	-255.0	239.62	-3	14.5	342	207	2.000	0.63	100S	255N	1
225.0	-260.0	194.58	-6	16.4	324	269	0.125	0.98	100S	260N	1
225.0	-265.0	191.79	5	15.5	274	219	2.000	0.35	100S	265N	1
225.0	-270.0	175.93	-4	12.5	251	194	32.000	1.05	100S	270N	1
300.0	-15.0	223.98	23	19.5	224	143	0.000	22.68	200S	15N	1
300.0	-20.0	209.47	6	23.0	209	144	0.000	7.51	200S	20N	1
300.0	-25.0	195.13	7	22.3	195	450	0.015	9.20	200S	25N	1
300.0	-30.0	203.37	1	17.0	203	456	0.003	3.31	200S	30N	1
300.0	-40.0	63.47	-8	15.1	212	995	0.000	6.39	200S	40N	1
300.0	-45.0	60.85	-0	13.7	203	638	0.000	0.38	200S	45N	1
300.0	-50.0	-72.41	4	13.2	-145	288	0.015	4.84	200S	50N	1
300.0	-60.0	-101.67	8	9.6	-339	692	0.000	13.15	200S	60N	1
300.0	-65.0	-86.98	-3	6.4	-290	469	0.000	15.85	200S	65N	1
300.0	-70.0	-40.08	-1	-17.5	-80	-360	48.000	6.34	200S	70N	1
300.0	-80.0	30.27	1	18.1	101	312	256.000	1.23	200S	80N	1
300.0	-85.0	23.61	9	13.3	79	2990	48.000	6.20	200S	85N	1
300.0	-90.0	20.16	1	25.9	40	100	0.000	26.97	200S	90N	1
300.0	-95.0	-22.32	16	1.2	-45	0	0.000	0.00	200S	95N	1
300.0	-100.0	-74.55	57	3.2	-149	267	0.000	29.38	200S	100N	1
300.0	-105.0	-23.39	4	-11.1	-47	0	0.000	0.00	200S	105N	1
300.0	-110.0	42.59	10	4.5	85	0	0.000	0.00	200S	110N	1
300.0	-115.0	138.82	-10	3.6	278	59	8.000	1.16	200S	115N	1
300.0	-120.0	228.64	-54	3.5	457	55	4.000	1.21	200S	120N	1
300.0	-125.0	248.22	-9	2.9	496	194	0.000	0.57	200S	125N	1
300.0	-130.0	214.87	-7	4.9	430	330	0.000	2.82	200S	130N	1
300.0	-135.0	154.84	2	6.0	310	90	4.000	1.38	200S	135N	1
300.0	-140.0	102.55	5	7.3	205	112	1.000	0.51	200S	140N	1
300.0	-145.0	57.80	6	12.1	116	226	256.000	2.07	200S	145N	1
300.0	-150.0	56.60	7	15.8	113	229	16.000	0.64	200S	150N	1
300.0	-155.0	71.18	9	20.9	142	284	8.000	0.71	200S	155N	1
300.0	-160.0	112.51	11	17.2	225	3700	48.000	4.54	200S	160N	1



300.0	-170.0	147.28	9	17.2	295	247	16.000	0.60	200S	170N	1
300.0	-175.0	178.15	-0	13.2	356	288048.000	13.61		200S	175N	1
300.0	-180.0	153.70	4	15.4	307	218	4.000	1.19	200S	180N	1
300.0	-185.0	127.42	-9	16.2	255	330024.000	1.99		200S	185N	1
300.0	-190.0	127.49	-7	16.3	255	245	32.000	0.74	200S	190N	1
300.0	-195.0	106.37	14	20.3	213	387	0.031	3.10	200S	195N	1
300.0	-200.0	114.33	-12	18.4	229	383048.000	5.69		200S	200N	1
300.0	-205.0	118.91	71	16.5	238	360048.000	2.24		200S	205N	1
300.0	-210.0	118.87	86	16.9	238	236	4.000	0.58	200S	210N	1
300.0	-215.0	94.22	56	17.9	236	381048.000	8.22		200S	215N	1
300.0	-220.0	119.16	-3	16.5	238	272128.000	5.86		200S	220N	1
300.0	-225.0	126.38	-63	15.3	253	219	8.000	1.25	200S	225N	1
300.0	-230.0	160.55	-14	14.8	321	207	4.000	0.67	200S	230N	1
300.0	-235.0	102.15	-53	15.5	255	242	0.250	3.22	200S	235N	1
300.0	-240.0	146.39	-1	14.6	293	228	0.250	2.97	200S	240N	1
300.0	-245.0	142.62	-4	15.5	285	239	0.250	1.56	200S	245N	1
300.0	-250.0	135.00	-23	17.6	270	244	2.000	0.27	200S	250N	1
300.0	-255.0	113.59	-2	15.6	284	232	0.500	1.41	200S	255N	1
300.0	-260.0	132.13	-5	17.0	264	235	4.000	2.34	200S	260N	1
300.0	-265.0	114.37	5	15.4	229	215	4.000	0.86	200S	265N	1
300.0	-270.0	106.53	-3	14.1	213	205	1.000	0.48	200S	270N	1

GEOLOGICAL SURVEY BRANCH  
 DEPARTMENT OF MINES

24,938

\$\$DATA\$\$ 12 -1 8 -2000 1 Sept/96  
 Array:P Trav dir:S Current:T Num Sep:3 A Spc:20,20,20 Eff.Sep:1,2,3  
 TEUTON RESOURCES CORP. - CLONE PROJECT, STEWART, B.C.  
 DDH9643 - Az , Dip - , Depth 227 m  
 DOWNHOLE IP SURVEY  
 vertical gradient array, C2 @ 1200N; C1 @ 100N, 100E, 100S, 100W  
 Mx chargeability for the interval 690-1050 msec after shutoff  
 Normalized VP = VP / current x 1000

NOTE: Grid North 315 Degrees

LIN	STN	SEP	XGD	YGD	VP	SP	Mx	NVP	Mi	TAU	FIT			
	3	3	3	2	2	1	1	1	1	1	1			
(T62,2A8,A3,T1,3F8.0,F5.0,3F6.0,2F7.0)														
75.0			-15.0		598.70		13	12.4	748	268048.000	22.69	100N	15N	1
75.0			-20.0		607.02		-2	10.8	759	264048.000	10.29	100N	20N	1
75.0			-25.0		591.22		-16	11.1	739	268048.000	4.77	100N	25N	1
75.0			-30.0		523.25		-14	11.5	654	236512.000	2.91	100N	30N	1
75.0			-35.0		454.94		-6	13.4	569	216 64.000	2.33	100N	35N	1
75.0			-40.0		411.77		12	14.3	515	219 32.000	1.02	100N	40N	1
75.0			-45.0		427.92		20	13.7	535	202 16.000	1.03	100N	45N	1
75.0			-50.0		413.96		18	13.7	517	203 16.000	0.97	100N	50N	1
75.0			-55.0		422.71		19	13.3	528	198 16.000	0.67	100N	55N	1
75.0			-60.0		393.17		20	13.6	491	194 2.000	0.71	100N	60N	1
75.0			-65.0		351.65		8	15.4	440	217 4.000	0.52	100N	65N	1
75.0			-70.0		332.76		9	17.2	416	244 1.000	1.79	100N	70N	1
75.0			-75.0		316.38		18	18.6	395	271 0.500	1.77	100N	75N	1
75.0			-80.0		390.36		-10	16.4	488	246 32.000	1.09	100N	80N	1
75.0			-85.0		408.52		-9	15.8	511	229 16.000	0.82	100N	85N	1
75.0			-90.0		393.97		-14	15.2	492	240 64.000	1.70	100N	90N	1
75.0			-95.0		409.07		-19	14.6	511	247128.000	2.27	100N	95N	1
75.0			-100.0		353.22		23	18.3	442	252 8.000	0.43	100N	100N	1
75.0			-105.0		351.82		10	22.5	440	299 8.000	0.56	100N	105N	1
75.0			-110.0		365.05		23	24.2	456	324 16.000	0.40	100N	110N	1
75.0			-115.0		403.77		21	23.9	505	317 8.000	0.23	100N	115N	1
75.0			-120.0		406.59		-4	22.2	508	302 2.000	0.91	100N	120N	1
75.0			-125.0		446.06		-10	19.5	558	266 2.000	0.46	100N	125N	1
75.0			-130.0		435.68		7	16.7	545	233 2.000	0.28	100N	130N	1
75.0			-135.0		345.95		-16	16.8	432	234 2.000	0.40	100N	135N	1
75.0			-140.0		345.65		-5	15.3	432	237 64.000	1.44	100N	140N	1
75.0			-145.0		278.00		5	13.6	348	201 16.000	1.06	100N	145N	1
75.0			-150.0		260.42		-16	15.7	326	224 8.000	0.52	100N	150N	1
75.0			-155.0		269.03		26	14.9	336	210 4.000	0.57	100N	155N	1
75.0			-160.0		237.41		-4	17.7	297	245 4.000	0.77	100N	160N	1
75.0			-165.0		222.80		-2	18.2	279	250 2.000	0.73	100N	165N	1
75.0			-170.0		232.08		-16	16.9	290	234 4.000	0.44	100N	170N	1
75.0			-175.0		253.95		-1	16.3	317	227 2.000	0.64	100N	175N	1
75.0			-180.0		197.48		118	17.5	247	246 8.000	0.85	100N	180N	1
75.0			-185.0		224.37		216	15.8	280	223 4.000	0.74	100N	185N	1
75.0			-190.0		161.34		81	18.9	202	260 2.000	1.41	100N	190N	1
75.0			-195.0		107.47		216	20.7	134	289 16.000	0.77	100N	195N	1
75.0			-200.0		205.26		-82	18.1	257	247 4.000	1.07	100N	200N	1
75.0			-205.0		180.02		-200	17.3	225	236 4.000	1.02	100N	205N	1
75.0			-210.0		239.53		-61	15.3	299	215 2.000	1.15	100N	210N	1
75.0			-215.0		280.09		-216	13.6	350	195 2.000	0.64	100N	215N	1
150.0			-15.0		122.34		14	34.1	153	0 0.000	0.00	100E	15N	1
150.0			-20.0		1568.69		-6	10.5	1961	100 0.000	32.40	100E	20N	1
150.0			-25.0		932.53		-16	13.7	1166	306048.000	14.20	100E	25N	1
150.0			-30.0		219.83		-16	24.8	275	409512.000	3.56	100E	30N	1
150.0			-35.0		257.13		-5	19.3	321	308128.000	2.43	100E	35N	1
150.0			-40.0		303.61		13	14.1	380	202 8.000	0.67	100E	40N	1
150.0			-45.0		357.18		21	9.3	446	139 1.000	1.17	100E	45N	1
150.0			-50.0		365.23		21	11.7	457	187 0.250	3.08	100E	50N	1
150.0			-55.0		388.48		19	13.4	486	192 4.000	0.37	100E	55N	1
150.0			-60.0		343.56		19	14.3	429	207 1.000	1.20	100E	60N	1
150.0			-65.0		101.29		9	30.5	127	384 32.000	4.69	100E	65N	1

150.0	-80.0	333.01	-8	17.6	416	245	8.000	0.76	100E	80N	1
150.0	-85.0	559.98	-9	15.2	700	227	0.500	2.46	100E	85N	1
150.0	-90.0	555.48	-8	16.9	694	233	4.000	0.39	100E	90N	1
150.0	-95.0	419.07	-17	14.7	524	235	64.000	2.48	100E	95N	1
150.0	-100.0	390.15	24	15.1	488	213	4.000	0.34	100E	100N	1
150.0	-105.0	372.47	10	16.9	466	234	4.000	0.61	100E	105N	1
150.0	-110.0	364.93	26	19.4	456	268	8.000	0.48	100E	110N	1
150.0	-115.0	406.72	20	20.7	508	277	4.000	0.67	100E	115N	1
150.0	-120.0	435.55	-5	20.6	544	280	2.000	0.95	100E	120N	1
150.0	-125.0	475.38	-8	21.0	594	290	1.000	1.06	100E	125N	1
150.0	-130.0	457.19	13	19.3	571	263	2.000	0.63	100E	130N	1
150.0	-135.0	383.89	-16	19.1	480	262	2.000	0.61	100E	135N	1
150.0	-140.0	378.66	-5	16.9	473	238	8.000	0.43	100E	140N	1
150.0	-145.0	367.21	3	14.1	459	204	8.000	0.56	100E	145N	1
150.0	-150.0	369.28	-22	15.4	462	216	2.000	0.66	100E	150N	1
150.0	-155.0	370.57	25	15.6	463	220	2.000	0.58	100E	155N	1
150.0	-160.0	320.08	-3	17.9	400	248	2.000	0.92	100E	160N	1
150.0	-165.0	264.19	-2	19.9	330	271	2.000	1.00	100E	165N	1
150.0	-170.0	267.71	-16	19.1	335	261	4.000	0.48	100E	170N	1
150.0	-175.0	280.36	1	19.1	350	262	2.000	0.73	100E	175N	1
150.0	-180.0	216.98	121	20.1	271	273	2.000	0.52	100E	180N	1
150.0	-185.0	246.87	214	19.7	309	268	4.000	0.86	100E	185N	1
150.0	-190.0	183.00	80	22.9	229	309	1.000	1.28	100E	190N	1
150.0	-195.0	124.18	215	23.2	155	309	4.000	0.74	100E	195N	1
150.0	-200.0	223.77	-86	21.5	280	290	8.000	0.78	100E	200N	1
150.0	-205.0	193.14	-200	19.4	241	267	4.000	1.27	100E	205N	1
150.0	-210.0	251.12	-62	18.1	314	250	2.000	1.00	100E	210N	1
150.0	-215.0	301.54	-214	16.5	377	231	2.000	0.40	100E	215N	1
225.0	-15.0	807.29	16	13.9	1153	335	0.007	3.96	100S	15N	1
225.0	-20.0	771.27	1	13.2	1102	230	0.062	3.59	100S	20N	1
225.0	-25.0	581.79	-17	12.7	970	214	0.125	2.14	100S	25N	1
225.0	-30.0	531.12	-17	14.8	759	221	0.500	1.36	100S	30N	1
225.0	-35.0	373.72	-4	20.7	534	295	0.500	1.64	100S	35N	1
225.0	-40.0	-306.90	12	24.7	-439	323	4.000	0.40	100S	40N	1
225.0	-45.0	-275.80	21	28.6	-394	366	2.000	0.70	100S	45N	1
225.0	-50.0	-127.01	21	34.7	-212	458	0.500	2.46	100S	50N	1
225.0	-55.0	-20.21	19	72.3	-29	118	0.015	2.50	100S	55N	1
225.0	-60.0	168.52	18	9.1	241	226	048.000	4.72	100S	60N	1
225.0	-65.0	312.32	6	16.1	446	231	16.000	0.38	100S	65N	1
225.0	-70.0	302.17	5	15.6	504	218	4.000	1.44	100S	70N	1
225.0	-75.0	441.90	14	14.3	631	203	2.000	1.10	100S	75N	1
225.0	-80.0	510.49	-6	15.5	729	234	32.000	1.56	100S	80N	1
225.0	-85.0	588.84	-6	15.2	841	222	16.000	1.12	100S	85N	1
225.0	-90.0	618.87	-8	15.2	1031	216	8.000	0.63	100S	90N	1
225.0	-95.0	792.26	-15	16.0	1132	240	32.000	1.07	100S	95N	1
225.0	-100.0	799.98	23	16.4	1143	237	16.000	0.22	100S	100N	1
225.0	-105.0	786.58	12	17.2	1124	246	16.000	0.15	100S	105N	1
225.0	-110.0	735.46	23	19.9	1051	278	16.000	0.15	100S	110N	1
225.0	-115.0	644.83	22	20.5	1075	279	8.000	0.56	100S	115N	1
225.0	-120.0	789.31	-8	20.4	1128	276	8.000	0.67	100S	120N	1
225.0	-125.0	750.74	-7	22.8	1072	304	8.000	0.71	100S	125N	1
225.0	-130.0	644.63	-1	22.6	921	301	8.000	0.48	100S	130N	1
225.0	-135.0	532.74	-14	20.1	888	270	4.000	0.69	100S	135N	1
225.0	-140.0	748.26	-6	15.2	1069	223	16.000	0.73	100S	140N	1
225.0	-145.0	950.94	5	11.7	1358	173	8.000	0.49	100S	145N	1
225.0	-150.0	1071.24	-8	11.4	1530	169	8.000	0.62	100S	150N	1
225.0	-155.0	863.12	26	12.9	1439	186	4.000	0.48	100S	155N	1
225.0	-160.0	805.05	-3	15.1	1150	215	8.000	0.23	100S	160N	1
225.0	-165.0	622.53	-3	17.8	889	247	8.000	0.37	100S	165N	1
225.0	-170.0	613.21	-15	17.8	876	244	4.000	0.44	100S	170N	1
225.0	-175.0	713.16	1	17.2	951	241	8.000	0.50	100S	175N	1
225.0	-180.0	538.32	126	17.1	769	240	4.000	0.83	100S	180N	1
225.0	-185.0	611.20	212	17.8	873	244	4.000	0.62	100S	185N	1
225.0	-190.0	474.16	81	19.9	677	270	4.000	0.45	100S	190N	1

215.0	-210.0	547.36	-62	13.7	782	221	4.000	0.67	100S	205N	1
225.0	-215.0	705.84	-212	13.9	941	197	4.000	0.54	100S	210N	1
300.0	-15.0	36.70	17	62.2	92	352	0.000	14.76	100W	215N	1
300.0	-20.0	8.54	11	264.9	21	781	0.000	30.19	100W	15N	1
300.0	-25.0	17.58	-20	117.5	44	527	0.000	15.88	100W	20N	1
300.0	-30.0	26.38	-16	54.3	66	724	0.125	1.70	100W	25N	1
300.0	-35.0	27.88	-6	29.0	70	181	0.000	8.65	100W	30N	1
300.0	-40.0	-48.88	12	9.3	-122	661	0.000	14.84	100W	35N	1
300.0	-45.0	-48.23	22	-10.1	-121	0	0.000	0.00	100W	40N	1
300.0	-50.0	-39.29	22	-13.8	-98	0	0.000	0.00	100W	45N	1
300.0	-55.0	-15.07	20	-49.0	-38	-10	0.000	39.00	100W	50N	1
300.0	-60.0	58.66	16	30.9	147	4755	12.000	0.88	100W	55N	1
300.0	-65.0	112.82	6	21.3	282	285	4.000	1.49	100W	60N	1
300.0	-70.0	153.44	5	23.4	384	308	4.000	2.10	100W	65N	1
300.0	-75.0	186.42	12	23.2	466	325	0.500	2.85	100W	70N	1
300.0	-80.0	193.45	-5	20.8	484	310	64.000	1.10	100W	75N	1
300.0	-85.0	208.39	-5	20.4	521	291	32.000	1.17	100W	80N	1
300.0	-90.0	212.09	-7	19.9	530	288	32.000	1.29	100W	85N	1
300.0	-95.0	232.84	-13	20.8	582	3261	128.000	2.45	100W	90N	1
300.0	-100.0	223.71	24	25.4	559	333	8.000	0.71	100W	95N	1
300.0	-105.0	243.08	12	28.9	608	367	8.000	0.47	100W	100N	1
300.0	-110.0	256.03	23	29.6	640	372	4.000	0.94	100W	105N	1
300.0	-115.0	275.25	21	28.7	688	363	4.000	0.78	100W	110N	1
300.0	-120.0	289.44	-8	24.9	724	328	2.000	1.63	100W	115N	1
300.0	-125.0	289.47	-5	21.2	724	301	0.500	2.08	100W	120N	1
300.0	-130.0	270.21	0	18.5	676	256	2.000	1.23	100W	125N	1
300.0	-135.0	231.87	-15	17.1	580	242	1.000	1.22	100W	130N	1
300.0	-140.0	240.83	-3	16.2	602	234	16.000	1.11	100W	135N	1
300.0	-145.0	236.37	1	15.3	591	224	16.000	1.50	100W	140N	1
300.0	-150.0	247.89	-9	15.7	620	223	8.000	0.81	100W	145N	1
300.0	-155.0	240.50	24	16.4	601	231	8.000	0.68	100W	150N	1
300.0	-160.0	204.62	-3	18.6	512	256	2.000	0.89	100W	155N	1
300.0	-165.0	189.77	-1	19.2	474	264	2.000	0.75	100W	160N	1
300.0	-170.0	197.47	-16	18.4	494	253	2.000	0.60	100W	165N	1
300.0	-175.0	227.04	4	16.8	568	236	2.000	0.86	100W	170N	1
300.0	-180.0	192.78	127	16.7	482	245	0.500	1.09	100W	175N	1
300.0	-185.0	213.94	212	16.3	535	236	1.000	1.69	100W	180N	1
300.0	-190.0	165.80	81	18.1	415	255	1.000	1.43	100W	185N	1
300.0	-195.0	107.53	203	20.8	269	283	1.000	1.79	100W	190N	1
300.0	-200.0	177.61	-96	19.3	444	263	4.000	0.73	100W	195N	1
300.0	-205.0	156.90	-199	17.4	392	237	4.000	1.05	100W	200N	1
300.0	-210.0	200.85	-63	15.4	502	218	2.000	0.67	100W	205N	1
300.0	-215.0	243.09	-208	13.0	608	191	1.000	1.14	100W	210N	1
									100W	215N	1

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