## INTERNATIONAL SKYLINE GOLD CORPORATION

# SUMMARY OF 1995 EXPLORATION WORK ON THE RED BLUFF AREA BRONSON SLOPE PROJECT

FOR EXPLORE B.C.

BY
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GEOLOGICAL SURVEY BRANCH ASSESSMENT REPORT

25,373

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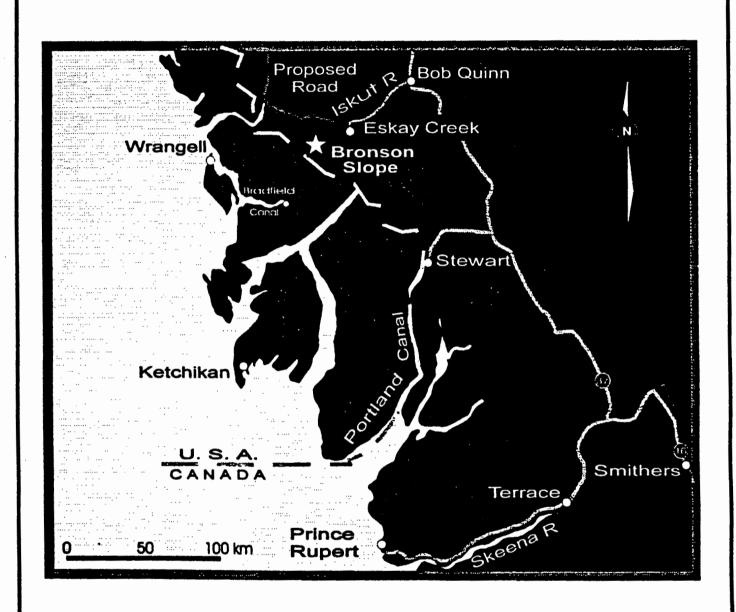
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## 1.0 INTRODUCTION

During the period of April to October 1995 International Skyline Gold Corporation performed a number of exploration programs on its Bronson Slope porphyry gold, copper, silver, molybdenum deposit located in the Iskut River region adjacent to the Johnny Mountain mine of International Skyline and the Snip mine of Cominco (see figure 1). The exploration programs allowed International Skyline to refine its resource estimation to an inferred resource of 90 million tonnes containing 0.749 grams gold/mt, 0.159% copper, 4.17 grams silver/mt and 0.005% molybdenum. The minimum estimated mineable resource contains 56,728,000 tonnes of ore grading 0.545 grams/tonne gold, 2.4 grams/tonne silver, 0.18% copper, and 0.01% molybdenum. The deposit realizes an ultimate strip ratio of 0.29:1 waste to ore.

The exploration programs comprised the following:

- A review of the drill core from the 1994 drilling program to identify potential controls on the distribution of mineralization.
- Surveys were carried out to identify the dip and orientation of previous drill holes.
   Surveys were also completed to accurately establish the location and dip of drilling to be accomplished in the 1995 program.
- A diamond drill program consisting of 7 drill holes totalling more than 10,000 feet in length.
- Using the information generated from the exploration a new resource model was completed.
- As a result of the 1995 exploration program, International Skyline Gold Corporation submitted an Approval Certificate Application as the first step in the Environmental Approval Process to develop the Bronson Slope Deposit.



**LOCATION MAP**BRONSON SLOPE PROJECT

INTERNATIONAL SKYLINE GOLD CORP.

OCTOBER 1995

FIGURE 1



#### 2.0 HISTORY OF WORK

The earliest recorded work on the deposit was by the Iskut Mining Company who performed between 1907 and 1920, surface and minor underground exploration of a number of base and precious metal prospects on the south-west slope of Bronson Creek valley.

The next phase of work for which accurate records are available was done during the period of 1962 to 1965 during which time Cominco Ltd. had an option to develop the ground. Both regional and property scale surface mapping and prospecting were performed. This culminated in 1965 with a pack sack drill program comprising seven holes for a total of 1105 feet of drilling. This program discovered several areas of promising copper and molybdenum mineralization, however the low gold prices prevailing at the time prohibited realization of the potential of the deposit.

During the construction, in 1987, of the Johnny Mountain mine facilities by Skyline Explorations Ltd., several contour lines were soil sampled in the vicinity of the Red Bluff as a preliminary step to performing a comprehensive exploration program to rediscover the object of the early 1900s prospecting and claim staking activity. The soil samples contained, among other metals, extremely high gold values. In 1988, following initial grid soil sampling and prospecting, a total of 1938 meters of diamond drilling was performed in five areas of the Bronson Slope, defined by anomalous gold concentrations in rock and soil samples and by base metal sulphide mineralization. The object of the drilling was to locate high grade concentrations of precious metals similar to the nearby Stonehouse and Twin zone deposits and therefore it was directed at mineralized cross structures. Again, promising low grade concentrations of gold, copper and molybdenum were found but the values encountered were insufficiently high to interest the company in continuing the program.

After a corporate reorganization in 1992, attention was directed to evaluating the low grade potential of the deposit. In 1993, International Skyline Gold Corporation performed an Induced Polarization survey of the deposit and the surrounding alteration zones and completed 872 meters (7 holes) of fence drilling of two cross sections of the deposit. The program was successful in partially delineating a gold, copper porphyry system. In 1994, the company commissioned a computer model and reserve estimate of the deposit using polygonal weighting by levels and preliminary metallurgical studies of composited core samples. The studies confirmed the presence of a significant low grade reserve with very favourable froth flotation recovery characteristics of both gold and copper and were pivotal in giving the company the confidence to progress with exploration of the deposit. The studies were followed by a seven hole drill program totalling 951 meters. The drilling explored undefined zones within the reserve block and untested zones along strike from the deposit. The presence of a high grade zone within the deposit was indicated. Following drilling, detailed surface mapping was performed over the deposit area to try to correlate structural geologic information with observations of the mineralization from core logging.

In addition, the mapping defined the limits of the surface trace of the high grade core of the deposit.

## 3.0 THE 1995 EXPLORATION PROGRAM

#### 3.1 REVIEW OF 1994 DRILL CORE

In April and May of 1994, David Rhys, a consulting geologist, was engaged by International Skyline to review the core from the 1994 diamond drilling program on Bronson Slope (hole numbers S1208-S1216 inclusive). The core was quick logged to identify potential controls on the distribution and mineralization with respect to alteration and vein type, structure and lithology. A core library of type samples was also compiled. Details of the review are contained in Appendix 1.

#### 3.2 SURVEY PROGRAMS

In May 1995, a surveying program was carried out on Bronson Slope to (1) accurately establish the location, dip, and dip direction of diamond drill holes from the previous 1994 diamond drilling program, and (2), to precisely orient and locate drilling for the upcoming 1995 program. Results from the surveys allowed the new resource model to be built with greater precision.

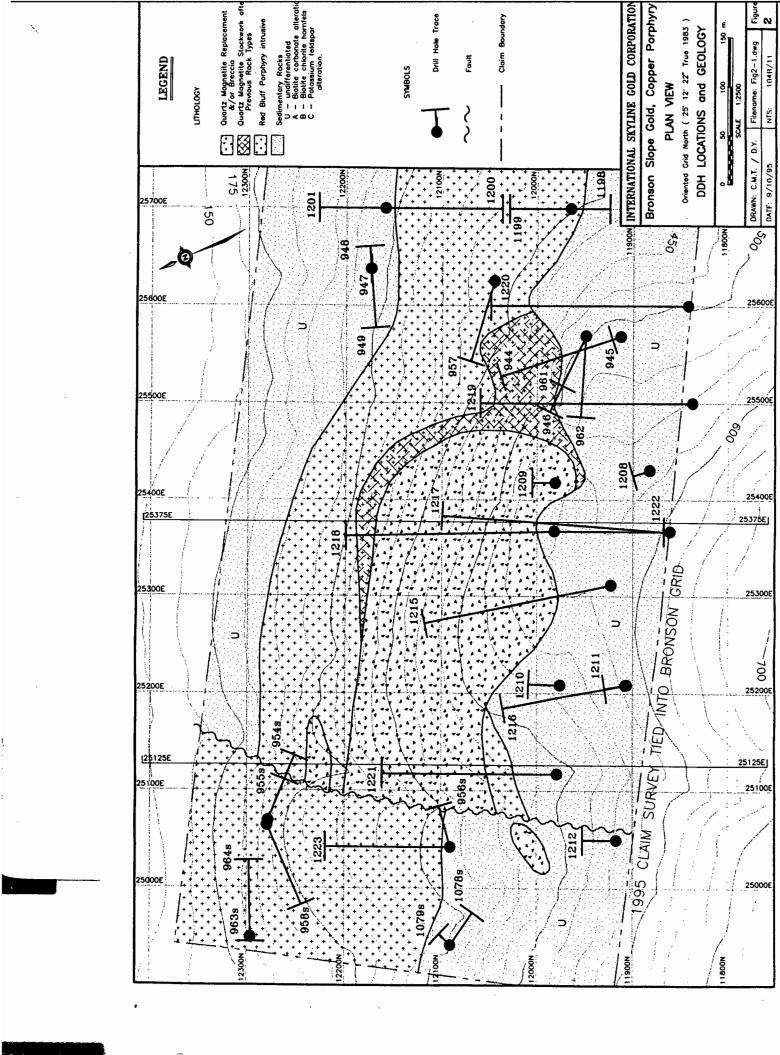
A second survey was performed between July 16 and July 25 1995 by Mathews and Lloyd Professional Land Surveying Ltd. to establish the precise claim boundaries between International Skyline and the Cominco-Snip Joint Venture.

#### 3.3 1995 DIAMOND DRILLING

A diamond drilling program consisting of seven holes and totalling more than 10,000 feet was conducted on Bronson Slope. Supervision was provided by David Yeager (P.Geo. and Chief Geologist, International Skyline Gold) and Cameron Scott. Additional geological services were provided by Lou Straith. Locations of drill holes on the Red Bluff can be seen in figure 2 including those from 1995 (S1217 - S1223, inclusive). Drill logs can be reviewed in Appendix 2.

Cover sheets for the drill logs could not be located, if indeed they exist. Details regarding locations and elevations were included with the drill logs, however, exact dates of the start and conclusion of each hole are not available. It can be assumed that all drilling was concluded prior to July 14, 1995.

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Tables indicating the assay results for each of the 1995 holes are included in Appendix 3.

As of the date of this report, although the drilling results have been fully assessed, no comprehensive analysis or conclusions have been compiled in the form of a geological report. The reader is refereed to the Geology and Project Description sections of International Skyline's Bronson Slope Mine Approval Certificate Application duplicated in Appendix 4. These listed sections were generated using the 1995 drilling results and represent the most recent compilation of geologic data on the Bronson Slope Project.

#### 3.4 COMPUTER MODEL AND RESERVE ESTIMATE

The entire drill hole database was computerized and a reserve estimate calculated using PC-EXPLOR software from Gemcom Services in Vancouver. This work made it possible to identify zones within the deposit that were undefined or incorrectly defined by previous drilling due to insufficient density of data or due to a lack of accurate assay information.

The study was performed by Christopher M. Turek, P.Eng, Chief Engineer, International Skyline Gold Corporation. Reserve polygons based on drill hole assay composites were prepared for 10 meter elevation slices of the deposit. The report is presented in Appendix 5.

#### 4.0 CONCLUSIONS

International Skyline Gold Corporation feels that the exploration program of 1995 has allowed the Bronson Slope Project to advance to the initial mine development phase. Encouraging results from the 1995 exploration program have led to:

- the Company's application for the construction of a spur road extension to the existing Eskay Creek Road which will lead to the Bronson Slope project location;
- an application to the Environmental Assessment Office (included as part of the Bronson Slope Certificate Application) for permission to construct a 20 MW run of river, hydro-electric generation facility on the Iskut River to supply power to the project;
- a geotechnical study by R.C. Dick, P.Eng. (Geotechnical Engineering Consultant), into the proposed Bronson Slope Project Sky Creek tailings impoundment locations and creek diversions;
- a design study for the Bronson Slope pit, including a starter pit;
- a study by Fluor Daniel Wright Ltd. (Vancouver) on various ore pass and crushing options for the Bronson Slope Project;
- a mill facility report on mineral processing options was completed by Rescan Engineering and a mill flowsheet was generated.

The company intends to continue to pursue Provincial environmental approval for the Bronson Slope Project. A 12 hole drilling program is anticipated on Bronson Slope for the 1996 exploration season. A number of environmental and geotechnical studies are anticipated for 1996. The company also intends to update the reserve following the seasons drilling as well as to conduct further metallurgical research on the Bronson ore. The feasibility of recovering and marketing the deposit's magnetite, which constitutes an estimated 11% of the resource, will also be investigated.

Respectfully Submitted,

Sandy Martin, B.A.Sc.

## APPENDIX 1

Report of 1994 Drill Core Review

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May, 1995

#### Memo:

To: D. Yeager, International Skyline Gold Corp.

Re.: Red Bluff porphyry (Bronson Slope Project) - geology, core library and core logging procedures

This memo reports the results of a review of 1994 drill core from the Red Bluff porphyry by the author, with assistance by Al Chapman. The work was completed at the Pamicon camp, located at the north end of the Bronson Creek airstrip, northwestern British Columbia, between April 26 and May 2, 1995. The core from drill holes S1208 to S1216 (inclusive) was examined and quick logged to identify potential controls on the distribution of mineralization with respect to alteration and vein type, structure and lithology. In addition, a core library of type samples was created for future reference.

The reader is referred to Rhys (1995) for a description of the geologic setting and exploration history of the Red Bluff area and to Moore (1994) and Weekes (1994) for a summary of the 1994 exploration program. The observations reported here, however, supersede those made by Rhys (1995) on the alteration, vein types and distribution of mineralization within the Red Bluff porphyry system.

## Geology and mineralization related to the Red Bluff porphyry:

#### Lithologies

The Red Bluff porphyry hydrothermal system is spatially associated with, and overprints a northwest-trending body or series of dykes of an Early Jurassic intrusion. The porphyry intrusion (195±1 Ma), termed the Red Bluff porphyry, is a K-feldspar megacrystic, plagioclase porphyritic intrusion of probable quartz diorite to monzodiorite composition. Subhedral tabular pink K-feldspar phenocrysts generally range in length from 2 to 20 mm, and they are rarely up to 7 cm long. They usually comprise from <1 to 5% of the modal mineralogy. The matrix to the K-feldspar megacrysts consists of medium-grained porphyry containing phenocrysts of albitic plagioclase (1-3 mm, 35-55 volume %), altered amphibole (up to 4%) and quartz. The plagioclase is usually completely altered to aggregates of sericite ± quartz ± K-feldspar. Mafic phenocrysts, probably originally

hornblende from crystal shapes, are commonly altered to magnetite, hematite, pyrite, biotite, and chlorite. Equant, clear to smoky subrounded quartz phenocrysts, 0.2-1.5 mm in diameter, comprise <1 to 4%.

The Red Bluff porphyry intrudes a sequence of biotite altered turbiditic greywacke. siltstone and mudstone that is of probable Triassic age. These rocks are an extension of the thick sequence that hosts the Snip mine. Bedding generally dips moderately to shallowly to the northeast adjacent to the porphyry, and is upright. The 1994 drill holes intersected the greywacke sequence along the southwest side of the porphyry system. Here, the sedimentary rocks are usually foliated and have a slaty to locally phyllitic foliation defined by biotite and sericite. Foliation is commonly spaced. Numerous calcite ± quartz ± pyrite ± chlorite veinlets and stringers are (a) parallel to foliation (predominant) or (b) folded by the foliation. The veinlets commonly occur in densites of >10 per metre. Thin (<2 mm) biotite envelopes and selvages are common on the veinlets, 0.5 to 40 centimetre wide quartz + pyrite + chlorite + chalcopyrite ± sericite ± Fe-carbonate ± biotite veins are developed throughout the greywacke intersect on the southwest side of the porphyry system in 1994. Sericitic shear zones (pale grey) are developed locally and are parallel to the surrounding pervasive foliation. Limited surface mapping in the area southwest of the porphyry suggests that the foliation has a shallow to moderate southwest dip.

On the southwest side of the Red Bluff porphyry within 25 to 50 metres of the quartz-magnetite-hematite stockwork that defines the core of the system, foliation in the sediments generally disappears, magnetite appears (disseminated, in veinlets and in quartz veins), veins become quartz-dominant with sparse calcite and intense K-feldspar alteration is widespread. The rock is commonly pale to dark green, mottled with disseminated blebs of magnetite + hematite. Quartz-magnetite-hematite veins, generally 0.3 to 2 centimetres wide, increase in density and thickness gradually downhole as the quartz-Fe-oxide stockwork is approached. This area of distinctive alteration, termed the "transition zone" in previous drill logs, occurs in the following intervals: \$1208 = 90- approx. 115 metres; \$1210 = top of hole-57 metres; \$1211 = 80-117 metres; \$1212 = 125 metres to end of hole; \$-1215 = 35-80 metres; \$-1216 = 82-125 metres. In these intervals\_quartz veins with magnetite are clearly cut by 0.5 to >50 centimetre wide (apparent thickness) white to pink quartz + pyrite + chalcopyrite + chlorite + biotite + sericite + carbonates veins of the same type described in the preceding paragraph.

## Quartz-Fe-oxide and younger mineralization

The Red Bluff porphyry hydrothermal system is dominated by an intense quartz-magnetite-hematite stockwork that trends northwest along the northern slope of Johnny Mountain. The stockwork overprints and is intimately associated with the Red Bluff porphyry intrusion. Margins of the quartz-magnetite-hematite stockwork are usually discrete. Over intervals of < 5 metres, and commonly < 1 metre, vein abundance increases from 10-25% of the total rock outside the stockwork to >60% (commonly >90%) within

it. The veins form an intense stockwork that usually contains less than 20% interstitial rock. Locally, drill intersections 20 to >100 m long are composed entirely of intersecting to sheeted sets of quartz-magnetite-hematite veins. Individual veins usually range from 0.5 to 10 cm in thickness. Magnetite with subordinate hematite constitutes from 0.5 to 25% of the vein volume, often occurring as multiple 0.1 to 1 mm-wide bands in white quartz. Microscopically, magnetite and hematite commonly occur together in individual grains with undulating irregular boundaries separating the two phases. Magnetite:hematite ratios are usually greater than 3:1. Multiple generations of obliquely cross-cutting quartzmagnetite-hematite veins are common. Vein core axis angles are highly variable in the 1994 drill core, but elsewhere veins are locally sheeted (e.g. Snip 130 portal area - veins dip southwest: Rhys, 1995). Younger veins contain progressively less magnetite and hematite, from 10 to % in the oldest veins to 0.5-5% in the youngest. Overall Fe-oxide content in the stockwork is estimated at between 8 and 15%. Interstitial wallrock within the quartz-magnetite-hematite stockwork is intensely altered to sericite + magnetite + hematite + quartz + K-feldspar + biotite + chlorite. A bright green phyllosilicate (possibly chlorite, biotite or sericite) is locally abundant.

The quartz-magnetite-hematite stockwork is overprinted by quartz + pyrite + chalcopyrite + carbonate veins and alteration equivalent to the veins of similar mineralogy outside the stockwork, and by pyrite and carbonate veins. Grey to pale pink quartz forms 5 centimetre to 3 metre wide patches and veins that typically comprise 10 to 30% of drill intersections in the quartz-magnetite-hematite stockwork. The quartz typically contains 1 to 10% disseminated, blebby and veinlet pyrite + chalcopyrite. Carbonates (?Fecarbonates, and more rarely, calcite), sericite chlorite and green biotite commonly occur with the sulphides. Margins of the quartz-pyrite veins/patches, although locally sharp like quartz-pyrite-chalcopyrite veins outside the stockwork, are typically irregular and gradational with the quartz-magnetite-hematite veins. Over <1 to 5 centimetre widths on the margins of the quartz-pyrite veins/patches, pyrite + chalcopyrite + Fe-carbonate entirely replace the magnetite and hematite, but preserve relict Fe-oxide banding of the adjacent quartz-magnetite-hematite assemblage. Isolated patches of Fe-oxide bearing vein material are commonly preserved within the white/pink quartz and are sulphidised on their margins. These textures suggest that much of the quartz-pyrite may this be an in situ alteration of the quartz-Fe-oxide assemblage, with little introduction of new vein material. The total sulphide content in the quartz-pyrite assemblage (generally approximately 5%), is less than the total Fe-oxide content if the older quartz-magnetite-hematite veins (generally 10%), resulting in a net loss of Fe from the system.

Pyrite + chalcopyrite ± carbonate veinlets and veins frequently cut, but are intimately associated with the quartz-pyrite veins and alteration. They commonly have consistent core axis angles, suggesting that they are sheeted. The veins are typically 0.5 to 4 millimetres wide, but are locally up to 30 centimetres thick. Pyrite + chalcopyrite veins are often spatially related to the quartz-pyrite veins/alteration described above: veinlet densities are usually highest in areas of quartz-pyrite-chalcopyrite veining/alteration, commonly >10 per metre, and drop to usually < 5 per metre in areas of quartz - magnetite - hematite veining that are unaffected by late quartz-pyrite veining/alteration. Pyrite ±

chalcopyrite veins locally have narrow alteration envelopes in which Fe-oxides are sulphidized. White, grey and pink (yellow to brown in old core) ?Fe-carbonate veinlets and stringers are locally abundant and cut the pyrite veins. Progressive mineralogic changes from early pink/white quartz > pyrite - chalcopyrite ± carbonate veins, intermediate pyrite + chalcopyrite ± carbonate veins to late carbonate ± pyrite ± chalcopyrite veins suggest that the veins are part of a single, evolving veining event that terminates in the formation of the late carbonate veinlets.

The quartz-pyrite veins/alteration are locally brecciated. Breccias have variable contacts with the surrounding quartz veins that vary from gradational to sharp. They consist of 25 to 70% angular to subround fragments of quartz-pyrite veins, typically 0.2 to 5 centimetres wide, in a matrix of carbonate (usually calcite) + biotite (black and /or green) + chlorite + sericite + pyrite ± chalcopyrite. Breccia fragments locally contain pyrite veinlets that are truncated at the edges of the fragments. This suggests that brecciation postdates or is late during both the quartz-pyrite and pyrite veining events. The late relative timing and abundance of carbonate in the breccia matrix suggests that brecciation occurred during the late carbonate veining event.

A late set of quart veins that is probably Tertiary in age cuts all of the above rock types and veins. The veins occur throughout the Johnny Mountain area and are flat to shallow southeast dipping, lenticular in shape and commonly occur in en echelon arrays. They are generally widely spaced (<1 per metre usually) and commonly fibrous. In drill core they are difficult to distinguish from veins in the Red Bluff porphyry system.

#### Metal Distribution

Au and Cu grades reflect the distribution of the different vein and alteration types. Areas of quartz-magnetite-hematite veining with sparse or no pyrite-chalcopyrite or quartz-pyrite overprinting typically grade <600 ppm Cu and <0.2 g/t Au (e.g. S1209, 146.5 to 169.2 metres). Highest Cu and Au grades (locally >1,000 ppm Cu and 10 g/t Au) occur in quartz-pyrite-chalcopyrite veins and alteration and in areas of abundant pyrite-chalcopyrite veining both inside the quartz-Fe-oxide stockwork and in adjacent greywacke. Au and Cu grades generally correlate positively and commonly have a linear relationship (Rhys, 1993) suggesting that they were introduced together.\_In greywacke outside of the stockwork, many quartz-pyrite veins with high Cu and Au grades are subparallel to shallowly oblique to the core axis (e.g. S-1210, multiple veins from 26.2 to 41.1 metres), and are thus steeply dipping.

## Geologic summary:

- Quartz-magnetite-hematite veins are the earliest phase of veining in the Red Bluff porphyry system. They form an intense stockwork that is spatially related to the Red Bluff porphyry.

- The quartz-Fe-oxide stockwork and altered sediments on its southwest margin are overprinted by quartz-pyrite +/- chalcopyrite veins/alteration and pyrite + chalcopyrite veinlets that are associated with the highest Au and Cu grades. Where quartz-pyrite assemblages overprint and sulphidize the quartz-Fe-oxide stockwork there is a net loss of Fe from the system. Veins are discrete, with sharp boundaries outside the stockwork in greywacke, but have indistinct alteration boundaries with quartz-Fe-oxide veins within the stockwork.
- The overall sequence from intense early Fe-oxide veining to less intense quartz-pyritechalcopyrite veins and finally to pyrite and carbonate stringers corresponds with a progressive decrease in the total amount and intensity of veining through time.
- A 25 to 50 metre wide zone ("transition zone") of K-feldspar + Fe-oxide alteration in greywacke occurs along the western upper periphery of the quartz-magnetite-hematite stockwork and separates the stockwork from biotitic greywacke to the west. Calcite veinlets, common in the biotitic greywacke, become predominantly quartz veinlets in the transition zone.

## Core Library:

The core library contains representative samples of vein types, alteration and lithologies from holes 1208-1216. The samples, numbered 1 to 70 are listed with the hole numbers and metres they were collected from in Table 1. The samples are ordered in a sequence that represents a typical walk through a drill hole, from altered sediments along the southwest margin of the porphyry system into the core of the quartz-magnetite-hematite stockwork that characterizes the system.

Samples 1-7 are typical of the biotite+pyrite+sericite±calcite altered siltstone adjacent to (SW of) the porphyry system. Note the foliation defined by biotite and muscovite. Calcite±quartz±pyrite±chlorite veinlets are abundant and are commonly foliation parallel or discordant, and folded by the foliation. Narrow biotite envelopes occur on the margins of some calcite and quartz veinlets (samples 1, 5 and 7). Magnetite is absent and K-feldspar stain is variable, but commonly moderate (samples 4 and 5).

Samples 8-19 are from the "transition zone" adjacent to (25-50m from) the quartz Feoxide stockwork. Foliation virtually disappears in this zone, quartz content increases in veins, calcite is no longer a significant vein constituent, and Fe-oxides appear both in quartz veins and disseminated. This area is characterized by intense K-feldspar alteration (samples 15, 17, and 19 are stained) that imparts, with Fe-oxides, a green-grey, mottled texture to the rock. The lack of foliation is probably due to the abundant K-feldspar and the relatively low phyllosilicate content when compared to the previous interval. Fe-oxide content gradually increases as the quartz-magnetite-hematite stockwork is approached. Two main generations of veining are apparent in this zone: early quartz-Fe-oxide veins/veinlets and related Fe-oxide stringers (samples 9-12, 15, 16, 18 and 19) are cut by quartz-pyrite-chalcopyrite veins and veinlets (samples 8-11, 13, 14 and 16). Good

crosscutting relationships are in samples 9 and 11. Note the biotite envelopes on some quartz-pyrite veins (samples 13 and 14) and the common pyrite-chalcopyrite stringers that are completely contained within the quartz-pyrite veins and terminate at the vein boundaries (samples 8-10, and 14). Carbonates occur as stringers in the quartz-pyrite veins (samples 9,13, and 14), as late veinlets that occur outside the quartz veins (sample 10) or more rarely, as irregular veinlets associated with the quartz-Fe-oxide assemblage (sample 17).

Samples 20-34 show vein and alteration styles related to the quartz-magnetite-hematite stockwork. Samples 20-27 are typical examples. Note the abundant laminae of Feoxides, multiple cross-cutting phases of veining, and the general decrease in Fe-oxide content in younger veins. Quartz > pyrite + chalcopyrite and pyrite veinlets cut the Feoxide quartz assemblage (samples 25-27) and Fe-oxides are locally sulphidized in the pyrite vein envelopes (sample 26). Samples 28-34 show the intense alteration of interstitial wallrock in the quartz-magnetite-hematite stockwork. Wallrock is entirely altered to grey-green sericite > magnetite + hematite + chlorite + green biotite + K-feldspar (samples 23, 30-34). K-feldspar is not abundant and is often absent (samples 30, 31, and 34 are stained). A bright green phyllosilicate (samples 28 and 29) predominates locally (possibly sericite, chlorite or green biotite - petrography is needed.) Late carbonate (sample 29) and quartz-pyrite (sample 32) veins cut the quartz-Fe-oxide veins and their alteration assemblage.

Samples 35-42 show quartz-pyrite-chalcopyrite alteration/vein assemblages progressively replacing the textures and mineralogy of quartz-magnetite-hematite veins. Domains of grey, white and pink quartz, here with 5-15% disseminated and veinlet pyrite + chalcopyrite + brown carbonate preserve relict textures of the quartz + magnetite + hematite assemblage on their margins (samples 38-41). Note the net loss of Fe-bearing minerals from the quartz-magnetite-hematite to the quartz-pyrite-chalcopyrite assemblage. Samples 35, 36, and 37 show sulphidization of the Fe-oxides adjacent to pyrite veinlets, again with an overall loss in Fe content. Sample 42 shows complete replacement of the Fe-oxides, with relict textures of the oxide assemblage remaining.

Samples 43-55 show the textural and mineralogical variation in the areas of white/pink quartz-pyrite-chalcopyrite veining. All of these samples come from veins that generally lack discrete boundaries and usually exhibit replacement textures at their margins with the quartz-Fe-oxide assemblage. Pyrite and chalcopyrite are present in all samples; they are disseminated in veinlets or in irregular anastamosing blebs with sericite, carbonates, (samples 43, 44, 46: ?Fe-carbonate and more rarely calcite), chlorite and green biotite. Specular hematite, K-feldspar (sample 51) and a pink carbonate (sample 55) locally occur as coarse blebs in the quartz-pyrite-chalcopyrite veins. Late ?Fe-carbonate (brown to pink when oxidized in air, grey on fresh surfaces: samples 52-54) veinlets locally cut the quartz-pyrite veins. These latter veins may contain chalcopyrite, pyrite, and/or specular hematite (sample 53).

<u>Samples 56-59</u> show breccia textures that occur locally in quartz-pyrite-chalcopyrite veins. The breccias have gradational to sharp boundaries with the surrounding veins, and contain brecciated quartz fragments in a matrix of green biotite, chlorite, sericite, carbonate (generally calcite), pyrite, and chalcopyrite. Sample 57 is exception and has a reddish matrix, possibly coloured by fine-grained hematite and /or Fe-carbonates.

Samples 60-63 are from southeast of the Red Bluff cliffs (holes S1213 and S1214) in intense sericite - pyrite + quartz alteration. K-feldspar content is low (samples 60, 61, and 63 are stained). These samples are from well outside the quartz-magnetite-hematite stockwork.

<u>Samples 64 and 65</u> are of post-mineral mafic dykes that occur locally throughout the area tested by drilling. These are fine-grained, dark grey, commonly magnetic and calcareous. Note the weak foliation developed in sample 65.

<u>Samples 66-70</u> are of K-feldspar megacrystic porphyry, typical of the Red Bluff. Note the pink K-feldspar megacrysts and the complete pale green-grey sericitization of the smaller plagioclase phenocrysts. Chlorite-biotite-Fe-oxide altered mafic phenocrysts have crystal shapes that suggest they are amphiboles. Samples 67, 69 and 70 are from within the quartz-magnetite-hematite stockwork. Sample 69 is stained and has abundant fine-grained K-feldspar in the matrix. Sample 68 is from a Cominco quarry approximately halfway down the Bronson airstrip (NW side). It is of a K-feldspar megacrystic dyke that is typical of Red Bluff type intrusions in the area.

## 1995 core logging sheet:

The 1995 core logging sheet is designed to record the abundance and distribution of predominant vein types, minerals and alteration types in relation to Au and Cu grades The following column headings and sections are indicated:

## 1. Geological Description

From /To: Interval of distinctive lithology, etc.

Description: To include rock type and/or dominant pervasive alteration (e.g. ALT for a highly altered rock of uncertain protolith). The most common lithologies are: (a) K-feldspar megacrystic porphyry; (b) Greywacke and siltstone; (c) Mafic dykes (distinguish foliated from unfoliated, etc.) and (d) alteration. Common pervasive alteration assemblages include: (a) biotite +/- sericite +/- calcite (Snip-type sediments SW of the porphyry system) (b) sericite-pyrite (intense alteration of sediments SE of the porphyry system) (c) K-feldspar +/- Fe-oxides ("Transition zone" adjacent to the quartz-Fe-oxide stockwork in sediments) (d) sericite +/- K-feldspar +/- magnetite +/- ?chlorite (altered wallrock in the quartz-Fe-oxide stockwork). In many highly altered wallrocks within the quartz-Fe-oxide stockwork, only the presence of K-feldspar megacrysts can distinguish between altered porphyry and sedimentary protolith.

## 2. Graphic Log

Provided to allow sketching of contact relationships, angles between structures, etc.

## 3. Structure

From/To: Interval over which the structure(s) is developed

Struct: Type of structure, such as foliation (FLTN), fault (FALT), shear zone (SHR), vein (list predominant mineralogy, e.g. quartz-magnetite = QzMag)

<u>TCA</u>: Angle that the structure makes to the core axis, or predominant angles in the case of multiple structures of the same type (e.g. pyrite veinlets).

<u>%TCA</u>: Percentage of structures of a single type that display a common angle to the core axis (e.g. 60% of pyrite veins are at 50 degrees to the core axis). Two or more orientations may be common in which case a second row could be used.

#### 4. Mineralization:

Columns under mineralization are designed to be recorded with each assay interval so that a direct correlation between assays/analyses and mineralogy and vein types can be made.

Sample #: Number from the tag book (a tag should be stapled into the core box at the beginning of each assay interval.

From/To: Sample interval

Minerals: Contains the following columns:

Py - visual estimate of the total pyrite content in the assay interval Cpy - visual estimate of the total chalcopyrite content in the assay interval FeOx - visual estimate of the total magnetite + hematite content in the

assay interval

Cal - visual estimate of the total calcite content in the assay interval Carb - visual estimate of the total carbonate (excluding calcite) content in

the interval

Blank column - for extra minerals

<u>Veins</u>: Columns are designed to record the number of veins/veinlets in each assay interval and their total cumulate thickness. Pairs of columns for three common vein/alteration types are shown (pyrite veins, quartz-pyrite veins and carbonate veins). The two columns are as follows: # veins is the total number of veins of one type in the assay

interval (e.g. 18 pyrite veinlets); cumulative thickness is the total thickness of veins (thickness of all veins added together) recorded in centimetres. These numbers can later be divided by the thickness of the assay interval to obtain a density of veins per metre and a total % of veins in the interval. Average vein thickness in each interval can be calculated by dividing cumulate thickness by the # veins. For white/pink quartz -pyrite veins/alteration in the quartz-Fe-oxide stockwork which often lack distinct boundaries, measurement of the cumulative thickness is subjective, but important to measure due to the strong influence of these veins/alteration on Au and Cu grades.

One blank column pair under veins is provided. In the quartz-Fe-oxide stockwork, veins are so abundant that it is more practical to measure what is not vein. Thus, I would suggest filling one of these columns with the <u>cumulate thickness of interstitial altered</u> wallrock in each assay interval that is in the stockwork. Other types of veins that could be recorded in these columns are: (a) quartz veins - timing indeterminate (generally in the sediments) (b) calcite veinlets (in the sediments) and (c) breccias and breccia veins.

#### 5. Assays

Au: g/t

Cu: ppm

Ag: ppm

Mo: ppm

One extra column for any new element

## Misused or vague terms in previous core logging

Misused or vague core logging terms that have been commonly used in previous Skyline drill logs include the following:

- (i) "Sheared", "shearing" or "shear" when foliation is meant. Large volumes of rock on Johnny Mountain are foliated but not "sheared". If the foliation is a discrete and definite shear zone (e.g. rapid increase in foliation intensity; oblique and asymmetric fabrics, etc.), it should be named as such (shear zone) with its foliation angle listed under the structure heading. In addition, the vague term "shear" is commonly applied to gouge-filled faults. If gouge is present its thickness should be noted, and any consistent angle of gouge seams to the core axis. I recommend that such a structure (gouge-filled) be described as a "fault" while a discrete, foliated zone be described as a "shear zone" to avoid confusion.
- (ii) The term "flooding" is a vague term that can mean veining or pervasive alteration (e.g. quartz flooding). More definite terminology, such as "intense veining" or "stockwork" could be used to describe veining. Pervasive alteration should be described as such (e.g. pervasive K-feldspar alteration and not K-feldspar flooding).
- (iii) The term "fracture fill" is a cumbersome term that means stringers or veinlets. The latter terms are clearer, and shorter.
- (iv) Andesite/andesitic, dacite/dacitic are commonly used to describe grey to green fine-grained rocks, including dykes, often based on the vague hint of a crystalline matrix or a green tint to the rock. If the rock can not be identified mineralogically (i.e. grains are

clearly visible) a name should be reserved until thin section petrography and/or geochemistry is completed.

(v) Alteration types such as silicification, K-feldspar alteration, sericitization, albitization etc. are commonly assigned to fine grained rocks of varying hardness or colour. For example, hard white or grey altered rocks are commonly called silicified while hard pink altered rocks are commonly called K-feldspar altered. These assignments are usually erroneous. If the alteration mineralogy is too fine-grained to identify while logging core, final identification of alteration type should be made petrographically or by mineral staining (e.g. K-feldspar stain). In addition, if the rock is so altered that protolith is unclear it should be called "altered".

#### References

- Moore, M. (1994): Geologic summary of the Red Bluff area, Bronson Slope project; unpublished company report, International Skyline Gold Corp., 5 pages.
- Rhys, D.A. (1995, in press): The Red Bluff Au-Cu Porphyry System and Related Precious and Base Metal Vein Systems, Northwestern British Columbia; Canadian Institute of Mining and Metallurgy, Special Volume 46.
- Weekes, S. (1994): Summary report on the spring, 1994, diamond drilling program,
  Bronson Creek area; unpublished company report, Pamicon Developments Ltd., for
  International Skyline Gold Corp., 14 pages + drill logs.

Table 1: Samples in the core library:

Sample #	Hole #	Metres
1	S1211	16.9
2	S1211	60.5
3	S1216	50.8
4	S1212	68.0
5	\$1212	55.5
6	\$1212	88.1
7	S1211	46.2
8	\$1211	100.8
9	S1210	44.8
10	S1210	50.0
11	S1210	38.6
12	S1211	112.5
13	S1216	135.0
14	S1211	101.0
15	S1216	119.8
16	S1216	123.0
17a	S1211	91.5
17b	\$1211	91.5
18	S1216	131.8
19	S1216	127.6
20	S1216	198.0
21	S1216	187.0
22	S1211	138.2
23	S1216	191.2
24	S1210	92.0
25	S1215	206.9
26	S1216	204.6
27	S1215	146.7
28	S1215	267.7
29	S1215	152.5
30a	S1211	161.4
30b	\$1211	161.5
31	\$1216	144.8
32	S1216	148.6
33	S1210	109.8
34	S1215	300.6
35	S1215	137.4

	<del></del>	<del></del>
Sample #	Hole #	Metres
36	S1209	101.4
<b>37a</b>	S1215	194.5
37b	S1215	194.6
38	S1216	205.5
39	S1209	105.3
40	S1209	63.3
41	S1209	66.2
42	S1211	139.8
43	S1211	158.3
44	S1210	25,3
45	S1216	137.0
46	S1210	36.0
47	S1216	133.6
48	S1214	19.5
49	S1211	136.7
50	S1216	153.1
51	S1211	98.0
52	S1215	89.7
53	S1211	137.4
54	S1210	67.0
55	S1215	72.1
56	S1209	5.6
57	S1209	45.0
58	S1216	133.2
59	S1211	120.3
60	S1214	61.0
61	S1214	45.4
62	S1213	20.5
63	S1213	20.7
64	\$1215	232.7
65	S1216	253.6
66	S1210	33.9
67	S1208	115.0
68	not core	
69	S1216	197.5
70	\$1216	196.4

## **APPENDIX 2**

1995 Drill Logs

## **HOLE 1217**

11869.07 NORTH

25366.97 EAST

603.53 m ELEVATION

**LENGTH: 423.4 m** 

	,	GEOLOGIC DESCRIPTION					_		SAMPL			Ī	ERAL		•		NERA	YEIN	Ş	 San Bili		T5	,		ASSA	24	
Met RUM		GEOLOGIC DESCRIPTION	8.	FROM	то	STRUCTUR	TCA	%TCA	SAMPL SAMPLE NUMBER	FROM	та	Py	Cpy	/ S <sup>†</sup>	Cal	ا مز	•	YEIN PYRI No. Vein	Cumi	12-PY 10. C	um No.	Cur	No.	Cum	Au	Cu	Ag
0	12 2	Carina	69	-		ļ			NUMBER	<del> </del>	╁	┼─	+	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	-	-	+	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	THE	/ein t	JK V EII	CAR	100	TUTT	$\vdash$		1
		Altered Siltstone : via gla-ser	+	<del> </del>	235	Braccia		///	2251	<del>                                     </del>	14.3	2,01	2	+-	<b>—</b>	1	1	1 1				1	1				
	V3.7	this cost out he as no See	†	19.1	19.2	Fault	600	100%	2252	143	17.4	1.02	2	1		1	1				1	1	1	1			
-		tbi : rock cut by 0.2-0.5cm Calcite vein (leached out to 14 m)	1		23.0	Cak vein	050	10%	2253	17.4	20.9	102	2	1		39	70					. "					
• • •		Cabanyantly rook 200000 to have	1-		7	//	40°	40%	2254	204	29.5	3.0%	7			T											
		undernone intense breezistion				11 Cala · Q11 -	450	70%												3 9	m	<u> </u>	1	<b></b> '	<u> </u>		ļ
		subsequently rock spacers to have undergone intense breceistion cesulting dislocation and fragment.				O) II	200	30%							<u> </u>					_1	<del></del> -	↓	↓	<b>↓</b> '	L	<u> </u>	ļ
		ation of early reins. Fragments range								ļ		<b></b>		ļ	↓	<del> </del>		1		_		<b>↓</b>	<u> </u>	ļ'	L	L	
		From 0.2 - >5.0cm with angular to	L							<u> </u>	ļ	ļ	↓	<u> </u>	↓	<u> </u>		1	_				↓	<u> </u>	<u> </u>	<del></del>	↓
		from 0.2 - >5.0cm with angular to subrounded margins, Matrix of	L					<u> </u>				1	<u> </u>		<u> </u>			$\perp$				<b>↓</b>	↓	<u> </u>		<u> </u>	ļ
		breccia comprises biolite + purite	_	<u> </u>		<u> </u>				ļ	ļ	ļ	<u> </u>	<u> </u>	<u> </u>	<del> </del>		$\bot$		-		↓	↓	<u> </u>	<u> </u>	<b>↓</b>	↓
		Calcile-otz-py:chlorite = biotile veins 0.5-10cm ere later.	L					<u> </u>	<u> </u>		<u> </u>	<u> </u>	↓	<u> </u>	<b>.</b>	↓_						ļ	↓				<b>↓</b>
		veins 0.5-1.0cm ere later.	L							ļ	<u> </u>	1	↓	↓	↓	┦—		1	$\rightarrow$			↓	igaplus	<del>                                     </del>			
		General elongation of bx frags									<u> </u>	<u> </u>	<u> </u>	<b>_</b>	↓_	1_		$\bot$				ļ	—		<b></b>		<b></b>
		at 20°/CA.	_	ļ				<u> </u>		ļ	ļ	↓	↓	ļ	ļ	┿-	-	+	-	_			┼				<del> </del>
	10. 4	011-11-51/1	├-		247 17	Calcite	100	207	2255	22 -	24.0	120			<del> </del>	+	+	1	-		1/3	15en		+	$\vdash$	<del>                                     </del>	<del> </del> -
3.5	14.7	Allered Sillstone : ula chl-bi-ser	╁	23.5	25.7	Veins	60	20%	7722	23.5	76.9	3 70	-	+	+	+-	+	1	_		- 31	1/200	1	<del>                                     </del>	<del></del>		<b>†</b>
		horn felsed? appearance. Segmented calcite veins prominent 0.3-1.0cm.	╂─	22 0	24.3	Weak ale	05	100						1	·	+		1			_	<del> </del> -	1	†			ļ
		Dark green blk colour of rock	✝	13.3	76.7	Calcite Veins Veins Statey clu. Calc-gra-P)	050	<b>†</b>				1	1	1	†	<b>—</b>	1	1 1		/							
		masks any obvious breeciation	t-	<b></b>		<b>†</b>	85"				<b>†</b>	<b>†</b>	†	1-	1	1	1			, \$2	San						
		Fine 105 - Calledon on source	t	<b> </b>	<del>                                     </del>	<b>†</b>	500	<b>†</b>			<del>                                     </del>	1	1	1	1	1	1										
		Fine LOSma subbedied by occurs on reticulate fractures and as	<del> </del>	15.7	25.9	Brecia				†	t	<b>—</b>	1		1	1	1										
		disseminations	╁╌			Broken			<b></b>			1	<del>                                     </del>	1		1		1									
		U 'SÇEDINA CIONS	†	242	2/ 2	Fault	450			<b></b>	·	1	1	<del>                                     </del>	<del>                                     </del>	1	<del>                                     </del>						1				
		Water course at 26 m with 0.4 m	╁╴	20.2	10.3	Favii	77			<u> </u>	<del>                                     </del>	1	†	1	†	1	1	1	$\neg$			T					
		bleached margins - In . Fo carbonales	╁╌	ļ	<del>                                     </del>	<del>                                     </del>	<u> </u>				<del> </del>	·	$t^-$	$\dagger$	†	1	+	1		$\neg$		4	<b>†</b>	1		ļ	
		Diekonest Irarairis sim see caragnates	t	<del> </del> -	<del> </del>	<del> </del>	ļ			<del> </del>	<del> </del>	<del> </del>	<del>† –</del>	+	1	+	<b>†</b>	1 1		$\neg +$	$\top$		<b>†</b>				
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			t	<del> </del>	<del> </del>	<u> </u>				1	<del>                                     </del>	1	<b>†</b>	1	<b>†</b>	+-	+				+	<del> </del>	<del>                                     </del>				<u> </u>
			†		<del>                                     </del>	<del> </del>		·			<del> </del>		1	·	†	1-	†	1	$\dashv$		<b></b> -	1	<b>†</b>				1
60	3/2 8	Altered Siltstone brewiated	1	2/5	31.0	Colcite toda	70"	70%	2256	269	29.3	13%		41%	,	5	2.				$\top$	1					
<b>Z</b> .Z.,	20.00	appearance with Coase bounded	1	24.5	34.8	py-biotile	450	35%	2257	292	32.6	3%	1	41%		50	7.	1			-		1				
		oppearence with frags bounded by somewhat reticulate biotite-pyrite	T	7.0.	1	"	80°	35%	2258	32 %	35, 7	3%		K1%	;	> 5											
		stringers Co. smm - which cut across	1	26.9	29.3	calcile gla	25	1	2250	35.7	38.7	37.	1	K12.		77				5 10	· //	<u> </u>	1				Ī
		segmented coloite = glz veins (early)	†	24.5	2/8	Calcitetala (Carly) py-biolile H Calcifegla py1magn. Yeak slatey Cleavess	ao"	90%	1	, <u>, .</u>	100.1	1"	+	1	1	†	"—	1 1		- 10		1					
		required course - des seins (co. 1)	<del>  -</del>	, , , , , , , , , , , , , , , , , , ,	10.0	1 - CIFAVES	<u> </u>	<u> </u>		1	1	1	<u> </u>	<del> </del>	t	<del> </del>	<del> </del>					1	1	1			1

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	t ·	GEOLOGIC DESCRIPTION	- 2	r		STRUCTUR TYPE	E T	r	SAMPLI	:S	·	MIN	ERAL	S	1	- 51		YEIN PYRI No. Vein	TE	Qz-I	Ру	CARI	6	N- 1		A	Cu	AΩ	Мо
FROM	TO			FROM	ם דו	TYPE	TCA	%TCA	NUMBER	FROM	10	Ру	Сру	Kegy	Cal	Colf		No. Vein	thk	No. Veln	thk	vein	thk	No. Vein	thk	AU	cu	MO	ļ no
16.9	36.8	(cont) - Qtz-cak = chl - py = magn.																											_
	1	veins crosscut biol or stringers												I														<u> </u>	1_
		Magnetite in vein at 29.1 m. A set of late 1 mm atrearb stringers with a carbonate rich	L						<u>.</u>			<u> </u>			<u> </u>					L	L				_				↓_
		A set of late 1mm atrians										L			ļ														ļ
		stringers with a carbonate rich				1	L							<u> </u>	<u> </u>	$\sqcup$					<u> </u>							ļ	↓_
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		Stracture between 314 and	ļ		ļ	L									ļ	ļl		ļ											-
		32.6m				ļ						ļ	<u> </u>		ļ					_		$\vdash$		$\dashv$	-				├
		At 35.5 m 1 cm calcite vein	L		<u> </u>	ļ							ļ	<b> </b>			-				<u> </u>			$\dashv$					$\vdash$
		20°CA with sericite. Bielite 7 py 7 mage	L		<u> </u>	ļ <u> </u>								ļ	_			$\vdash$			ļ—	$\vdash$			-				-
		margins; trep in wall.	L		↓			ļ						ļ				$\vdash$			<u> </u>	-				<u> </u>			├-
		Rock Przga (boudins?) steadily mere sericilis with biolite rpyrik z mass. reticulate margins.			ļ		ļ				· .					<b> </b>		<b>  </b>		-				-+					├-
		sericilis with bioliterpyrik & maan.	L		↓	ļ	<u> </u>	ļ				<b>!</b>	L	ļ				<b> </b>				L							-
		reliculate margins.	L				L						<b> </b>		<u>.                                    </u>	-		$\vdash$								-			├-
		36.0m-3mm biobile pays magn stringer OCA cronulated normal	L			<u> </u>		ļ						L				$\sqcup$			<u> </u>								
		stringer OCA cronulated normal											ļ								<u> </u>	<u> </u>	$\longrightarrow$						⊢
		to cleanage of 75°CA	L				<u> </u>		<u></u>													L_							ļ
												<u> </u>											$\Box$		_				<u> </u>
										<u></u>		<u> </u>											L		_				ļ
			L		$\bot$			<u> </u>				<u> </u>													_				┞
36.8	41.9	Altered Siltstone: slater deovage	ه	36.8	41.0	slaley clv.	75°	80%	2260	38.7	41.0	5%		tr							<u> </u>	5%							ļ
		prominant at 75CA	L	37.8	3	Fault	750		<u> </u>				<u> </u>												_				↓
		Faull at 37.8m-10cm sericity gauge perallel cleavage, Cremlated bonding perallel cleavage, Returnate pyrite> biotite 7 magnetite vein parallel		38.7	38.75	Fault - gla-care	800	100									Sph							ok c	41				_
		perallel cleavage, Crenalated bonding		41.0	91.9	Platinh die-cab-ch	800		2261	A1.0	41.9	12	tr	tr			tr.								2				↓_
		pormal to cleavage. Reticulate purite>																											<u> </u>
		biotite 7 magnetite vein ezrallel																							_				<del> </del>
		crenulations and cleavese, Carbonate-					Ĺ														<u> </u>								ļ_
		crenulations and cleavage. Corbonale- quarts veins segmented and folded																											<u> </u>
		by cleanage, 36.9m 1.0cm pinkal glz-cak.	Γ		T										l														
		v. of 75°CA . A1 - 41.9 pintish at 2 -calc -chl	:5	er.			Ī																		$\perp$				
		vein containing 30% horsts. CatSal	T			1																	]		]				
	1	vein containing 30% horsts, Co+Sph prominent in 3cm pyritic vein al 35%	1			T	1		I																				1
		adjacent to horst at 41.15m (sphalerit					1																						1_
	-	William ) Was a Lat	9-		1	†				<b>†</b>		İ	···		-									1					
	$\vdash$	yellow to orange) HI.85 cp on horst	╁╌		+	<del> </del>	<del>                                     </del>	1	<del>                                     </del>				_	_					-										
	<u></u>	margin	<del> </del>	<u> </u>	<del></del>	<u> </u>										·								<u> </u>					<u> </u>

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	GEOLOGIC DESCRIPTION				TRUCTUR	Ε		SAMPLI	ES		MIN	RAL	<u>s</u>	•	, <b>.</b> . T		PYRI	JE_	Qz-F	<b>y</b>	CARI	B (	Pi 4 8	AZE	AZZA	YYS		<b></b>
FROM T	ra	NO SE	FROM	TO	TRUCTUR	TCA	%TCA	SAMPLE	FROM	TO	Ру	Сру	. eD+	Cal	600		No.	Cum	No.	Cum	No.	Cum	No.	Cum	AZZA Au	Cu	Ag	Мо
41.9	Allered Sillstone: rock becoming	94	41.9	53.4	Cleavage	70.90	()5-0	2262	41.9	448	3%	-	10	5%			VEIII	CITA	V 42 11 1	VIII	VEIII	1	13	15				
7.7	man schistore with development	Н	243	80.35	Fault Calinh	1000		2263	40.0	47.6	3%	10	1r	5%									13	5 cm				
<b>!</b> ! .	A strong Adjustion of BO'CA; servile>		41.9	44.A	(Foliation) Fault cuts foliation pit agreat -th V calcile	700	800	2264	47.8	50.9	3%	tr	to	5%							40	200						
	chlorite; py disseminated and with		41.9	53.4	calcite	20-80	900		1		<del>,</del>			\ <u>\</u>														_
† † •	biolite on rims of bonfinanch rock		•	11	"	10-200	100						1	-														
	fragments. Early calcite = gla veins						1	1	<b>T</b>																	I		
	segmented by cleanage.	<b>-</b>					1				T		1															
	1.3			· · · · ·				1																				
	50.6-50.8 Water course - dissolved				1	1						l ··-							1							I		
	calcile veins												$\overline{}$															
T		T			1			1			Ī			Ī		44												
	51.5 minon fold axis 85°CA		50.9	53.9	iorb			2265	50.9	53.9	5%	lr	to	8%	L.	1.1.					68	40cm	6	15cm				
	51.7 10 - 912-cak-chl at 85° CA-																								<u> </u>	L	<u> </u>	_
	Lr cp, sp with pyrite or maising.										l								L			<b> </b>		L		ļ	ļ	I
	52.6.52.4 15% py at 60°CA prodlet	<u>.                                    </u>									ļ	ļ														ļ	<del> </del>	
ļ	52.6-52.4 15% py at 60°CA prodlet	_				ļ					ļ	ļ	<u> </u>	<u> </u>								$\sqcup$	<u> </u>		ļ		<del> </del>	-
<u> </u>	53.8 sem alz cabile - 4 cp. mo, sp	Щ			ļ								ļ			_	$\vdash$					-			<u> </u>	├	<del> </del>	-
} · · · · ∤	on marsing															٠ ا		<b></b>				<b> </b>	- 1			<del> </del> -		1
<b></b>		Н			distak ±		005	2266			00	<del>, -</del>	<del>  ,                                   </del>	2		50	-			-		-		-			$\vdash$	+
<b>-</b>	53.5-57 Well servilized rock with closes	<u> </u>	53.'7	520	of teins	85'	20%	2266	287	\$ 1.0	1/6	Er	20	10%	-	Er.	$\vdash$				-				<u> </u>		†·	<del> </del>
<del> </del>	Adiation at B5° CA. Much of the	-			-	185	12/0				<del> </del>			-					Н			$\vdash$	$\Box$			<del>                                     </del>		+
<b></b>	fragmontal (boudiness) terture masked					├			<del> </del> -		ł						-		$\vdash$	$\vdash$			$\vdash$			1	<b>†</b>	<b>†</b>
<del></del>	by alteration, Older corporate veins	<b>-</b>				├		<b></b>			╌	<del> </del>							-	$\vdash$		-				<del> </del>	<del>                                     </del>	<del>                                     </del>
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-	seins subparallel or when at an acute angle to CA these are folded	-		<u> </u>	<del> </del>	├	-	<del> </del>	<del> </del>		-								-	$\vdash$		<del>                                     </del>		$\vdash$	<del>                                     </del>	<del> </del>	$\vdash$	+
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<del></del>	generally subported to cleavage.  Contonal in veins from 55.5-56.8	-				<del> </del>	-	<del> </del>			├			-		-	$\vdash$		$\vdash$	H		-	<b>  </b>	-	<del> </del>	├	$\vdash$	+
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-	Continue in veins from 55,5 - 56.8	⊢			+	<del>                                     </del>		<del> </del>			├		<del> </del>				-					$\vdash$	$\overline{}$			<del>                                     </del>		+
<b></b>	leached and causing rock Programment				<del></del>	ł—			<del> </del>		ļ								$\vdash$	-							·	
	selvage 56.9 57.0 pink quart-cabib.	-				+			-		$\vdash$			<del>                                     </del>			$\vdash$		$\vdash$			<del>                                     </del>				<del>                                     </del>	1	
<del> </del>	servage 36.0 37.0 fink quart caviu.					† ·			<del> </del>																	t	<b></b>	t
	chlorite vein - trep, pr, magnetile	$\vdash$			<del> </del>	<u> </u>	<u> </u>				<del>                                     </del>						-						$\overline{}$					1
<b>-</b>	Timming contained lithin remnants.  Icm printin bond at B' CA Pock Scherman	<u> </u>			<del> </del>	<del> </del>		1	<del> </del>		<b>†</b>		<b></b>						1	$\vdash$						† <b>-</b>		<b>†</b>
-	Vimits differentiation of earlier carbonale and	7			<u> </u>	<del> </del>			<del>                                     </del>		$\vdash$		<del>                                     </del>	-			-											
	ymis differentiation of conter Caromate and				t			1	ļ		<u> </u>		<u> </u>						ļ							<u> </u>		1

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		GEOLOGIC DESCRIPTION	L			TRUCTUR	Ε		SAMPLI	23		MINE	ERAL	2.				PAP	YE-	Qz-F	ΣУ	CARI	B			ASSA	YS		
FROM	TO		169	FROM	Ĺ	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Ру	Сру	KeO+	Cal	Coto		No. Veln	Cum thk	No. Veln	Cum thk	No. Vein	Cum thk	No. Veln	Cum thk	ASSA Au	Cu	Ag	Мо
57.0	61.5	Strom helistin of A: "CA "		970	605	H-	45		2267	570	60.0	370	1-	dr		10%							10%						
		pleaded (1) are Please Ger.													I														
		cents voining segmented and optified																						$oxed{oxed}$					
		cert, voining semanted and optobed.	I											<u> </u>															L
		by where & probincer.													_			L											<b></b>
L J		by which of problemser.  Decesional of contake try man 1912  Namilel I bet Pock has commen						<u> </u>						l															<b>_</b> !
		vamlet All Bock his conson										<u> </u>	L		↓			L					ļ	<b> </b>					<del> </del>
		my lonitized spoor once										,																	ļ !
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			<u> </u>	1- 1		1 12				(		- 77	ļ.,	<del> -,</del>	<del> </del>	1.00						740	. 07						
10.5	61,1.	As Above: Decressional o.s.cm	$\vdash$	(D.5	61.6	W'	70°		2268	60.0	61.6	373	++	100	├	10%					-	140	10 %						<del>                                     </del>
		colo t py mgn of 70°/30°; trace epitte!	-			·				···					-											<del></del> -			<del> </del>
$\vdash$			•				<u> </u>						-	├-			-			$\vdash$		$\vdash$	$\vdash$			-			<del>                                     </del>
		Block, ground &	$\vdash$			<u> </u>									-		7							$\vdash$					
61.6	63.1	Strong schisbeils at BO'CA . Certon	2			Schipperity (alegarity)	80°		2269	61.6	63.1	6%	17.	15%		20%							20%						
		wins radated more Mot. Desmoter				(4)007004)		1	, A. S.				1	T															
		increase in py Robber Combonet com heavil beached - unery Strong chlorite - Common chorite				stickersi	30 mi	4						Г															
		com beaut beached -> vuces												1															
		Strong chlorite - Carbonst chlorite																											1
		setuat: - Cerbonede rains = 0.3 cm																											
		note 50% glz -com/ai minor py 1Ho.													<u> </u>												L		
		Epidok tinda disposed - efter folips	?									<u> </u>		<u> </u>	<u> </u>														
·		apto 50% att com/a more pytho. Epidoh tinda dispossed - ether folsper Most clerves breeks show slickensid	_										L <u>.</u>		ļ														
-		with 30° pilch (SW?) 5" + man polished	<u>.                                    </u>	631	66.1	schools	800		2270	63.1	64.1	5%	170	8%	<u> </u>	20%							20%						<b> </b>
<b>.</b>			_								ļ	ļ		ļ	<u> </u>	<b> </b>													<u> </u>
63.1	(16.	As about Occasional biolih	ļ				ļ					⊢	ļ		<b>├</b>			ļ					_						<b>  </b>
		enhancel dray hold is 2x/cl paillel	_			<b> </b>	ļ						ļ	ļ	ļ	ļ		<u> </u>											
<b>.</b>		Schistocity	-			con loss						.0	-	- 07	<del>                                     </del>	-07		-											<del>                                     </del>
66.1	67.2	As above - core loss due to	-	66.1	7.2	compless fault!	-!-		227/	66.1	69.2	2%	0.57	3%		7%	-												
		-12 st + sec + py co towards	<del>                                     </del>								-	-	-	-	<del>                                     </del>		-	$\vdash$							_				
		and of run. Chlumb decressing	-												t · · ·														
$\vdash$		-tr totoshorih in glz in cp	$\vdash$								-			<del>                                     </del>	<del> </del>														
		IF THE PARTY IN SIE R CP	-			<del></del>									† <i>-</i>														
			$\vdash$		-	<u> </u>				<del> </del>				_	1	$\vdash$		-											
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		GEULOGIC DESCRIPTION				STRUCTUR	 E		SAMPLI	ES		MIN	ERAL					IZATI YEIN		Oz-F		ICAR)	<b>5</b>			AZZA			
FROM	TO		84	FROM	מז	TYPE	TCA	%TCA	SAMPLE SAMPLE NUMBER	FROM	το	Ру	Сру	kest	Cal	Coro		No. Vein	Cum	No. Vein	Cum thk	No. Vein	Cum	No. Veln	Cum thk	AZZA uA	Cu	Ag	Мо
152	D2 1					carb stock	1	1 9		40.0	22.2	20	. =									?	10%				<del> </del>	┼	<u> </u>
01,2	77.5	As shore: lose chlyrich and	$\vdash$			TSOF AY CO	10	40%	7277	69. 2	12.6	4.0	0.5	17.0	-7	10.	$\vdash$	$\vdash$				<u> </u>	10 / W	<del> </del>				<del> </del>	
		slight home hornfolsic proce with whops of broth followed by cole-siz sos =chl py cp	$t^-$			· · · · · · · · · · · · · · · · · · ·		40%	<u> </u>	<b>†</b>			<del>                                     </del>	<b>†</b>															
		by cale-siz sex =chl .px cp	t			<u> </u>		<u> </u>	<u> </u>			<b></b>	<b>†</b>	<del>                                     </del>															
									1																				
73.7	75.3	As shore: rock still belly				Calcula 9tz	70		2273	U3.7	75.3	5%	0.5	5%	-7	10%						7.	10%						
		broken ala-cole voins dominant				calcula 9tz	75°	80%						<u> </u>														ļ	
		broken attack veins dominant veins 0.2 - 0.5 cm often segmental by cleavese. Procy disson cleaves	L.,				350	20%						ļ		$\perp \perp$			<u> </u>									ļ	
<b></b>		by cleavage . Procy diss on cleavage		$\longrightarrow$					<b>!</b>				ļ			$\vdash$												<b></b>	
		phones and = Gtz cole.			-															7. 11					$\rightarrow$		<b> </b>		
~	50.	040 5 0 5 5 7 7		2.5	04 -	8/2			3224	75.3	783	200	0 (1)	170		20				+chl		_			$\dashv$		<del>                                     </del>		<u> </u>
	18.5	All sal : similar to show	-	75.3	75.3	S" fol " Q'acolacki 1 PY EP	45	110				470	0.46	170		3%				21	Bem								<u> </u>
$\vdash$		but more constant server	Н			t PY EP	70"	40				_		-		<del>                                     </del>				$\dashv$	-				$\dashv$				_
		but more cotosjon (gradual change). Hyprofilis spectores. Strudur al deformaly of oris.		78m		3cm colocul	70	00								<del>  </del>													· .
<b>——</b>		Calle based lines in it	┝┈	10m		Str CHICH	15-		ļ	$\vdash$														$\neg$	$\dashv$				
		- Ou-co die and in which acces						<u> </u>	<b></b>					ļ												*			-
		- py-cp dis end in which assoc. in biolite (Kell) and offine bel @ 45"																							二				
		61° @ 45°																											
<u> </u>						gts contact							ļ	<u> </u>							•							ļ	
<b></b>		As 2 bove	_			7	477		2275	78.3	81.4	4%	049	17.	L	12.				20	Bem				<b>-</b> ∔		<u> </u>		
			_				60	50						ļ						_								<b> </b>	
$\vdash$			$\vdash$				85	20	<b>.</b>					Ь—	<u> </u>					_				$\longrightarrow$					
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$\vdash$		A 1 1:11/1/1/ 1/ 1/1:0	-	42.5		10cm	0-1	<del> </del>		0111	au d	47/17	1.00	. 17		- 47				9		± 91						┼	<u> </u>
-		As show . Glightly bleeded . chlorish	-	83.7		myloni lad 5= serichl	85		2276	81.4	84.7	56	1.0.	170	<del> </del>	3%				7	(ocm		3cm						· -
<del>                                     </del>		vom week Sediment deformationstruction	20			closus,		<del> </del>						├		-									$\rightarrow$				
		more epporent - by " little + vein clevery webses 0.5 cm gts ser 15" indicat sebyas testore 45"/60"/70"CA	$\vdash$			Closury	62	<del> </del>		l			ł · · · · ·	<del> </del>					$\dashv$										
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		GEOLOGIC DESCRIPTION				STRUCTUR	Ε		SAMPL	ES		MIN	ERAL	2.			P	YARY	£	Qz-I	Ру	CARI	3			ASSA	YS		
FROM	το	1 Marie - 1 Marie - 1/20 Marie	3,	FROM	τo	TYPE	TCA	%TCA	SAMPLE	FROM	to	Ру	Сру	201	Cal	COLD		No.	Cum	No.	Cur	No.	Cum	No. Veln	Cum	Au	Cu	Ap	Мо
			123	<del> </del>	<del> </del>	<del> </del>	_	<b> </b>	NOMBER	<b>†</b>	1	<del>                                     </del>	_	<u> </u>	$\vdash$	<del>   </del>	一	√ €IU	LIK	vein	ÇNK	A SIU	<b>STIK</b>	v eini	UTIK				
04.4	825	De poore - pr-co in coverel	T	84.4	1000	Shorral' bk	450	<del>                                     </del>	2277	84.9	875	5%	0.8	,	1		$\neg$	2	Con	6	10.		3.0	$\Box$					
	. د د د د ت	diffused bands @ 80 throw folses - blooched near 5= bands.	T	1	100	CP-PY	100°	<b>†</b>	<del> </del>	123.1	1	1		<b>-</b>	1					_			J						
		- bleached near S= bands	1	1	<b>-</b>	Clemin)	500	<b>†</b>			1				1		$\neg$	$\Box$							$\Box$				
				84.11	27.5	C1"	40"			1		<b> </b>	1																
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87.5	90.5	28 shone	1			colc.	70°	65	2278	875	905	2%	0.5	0.						6	27		30						
							0'	15	I	<u> </u>	I	Ι	Ι	I															
							450	20				L	<u> </u>																L
20.5	936												<u> </u>								L								
		24 2 borne.				912 07	70"		2279	30.5	93.6	2.0	1.0	0.1	2					18	22		2.0						
						•/	450	50	L			<u> </u>	<u> </u>																
			L			11	150	20	<u> </u>	L		<u>.</u>		<u> </u>		<u> </u>								$\longrightarrow$					
			L										ļ	ļ	<u> </u>													ļ	
36	96.6	25 2 bons.	_		<u> </u>	Gliry	65	40	2280	93.6	96.6	2.0	0.5	0.1	4		_	_	_	18	25	14	8.5		<b>→</b>				
			_				45	50		<u>                                     </u>	ļ			ļ	ļ			_										<u> </u>	
			L				0	10	<u> </u>	<u> </u>			ļ	ļ	<b> </b>	$\sqcup$	_	_						<u> </u>				ļ	
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			┖					<u> </u>				4		ļ	<b> </b>			_											
N. 6	92.7	As show like heirline all cont		<b> </b>	<u> </u>	ahron	60	60	2281	96.6	99.7	1.5	0.2	1.0	2	+				12	14.5		15						
		± 10° CA	_	<u> </u>	ļ	<u> </u>	45	40	<b>!</b>			—		⊢							<u> </u>	-	$\longrightarrow$		$\dashv$		<del></del>	<del></del>	
		<u> </u>	1			<b>.</b>			-			<u></u>	ļ	<del>  ,                                   </del>				$\rightarrow$		-									
99.7	102.7	As store broken - whine price disseminated end on micro first, often weakly believed	┡		<u> </u>	017:07			2282	99.7	102.1	3.0	0.5	br	15		$\dashv$	<b></b> ⊦		3	1.5	25	10	-					_
		disseminated end on micro fract,	1		ļ	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	45	65	<b></b>	ļ <b>.</b>		ļ	<b>-</b>	<del> </del>	ļ									ı <b></b> +					
		often weskly foliated	↓_		ļ			ļ		<del> </del>				<del> </del>	↓		-	$\rightarrow$			<u> </u>				$\dashv$				
		1	<del> </del>			<del> </del>				ļ	ļ	ļ	<u> </u>	I	<b> </b>	<b>∤</b> ∔				0	10				ł	<b>.</b>			
├─		As show segmented and	├-	<del> </del>	├	Q17 py	40		2283	102.7	1044	30	0.2	tr	5	-		$\rightarrow$		<u> </u>	10	-	2	<del></del>					
		hzirline aslait veining	╀		<del> </del>		40	50	<b> </b>	<del> </del>		<b> </b>	ļ	<b></b> -		<del></del> -								·					
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100		9	╂	ļ	<del> </del>	F1+0/14		<u>.</u>		ļ,;	ļ	1	-	ł,	1.	<del>  -</del>			_	<del></del>				BX Q12	200				
104.4	102.7	Brainful Otz-py vern.	╀	├		FLTIN II.	60-60	<del>' </del>	2284	1044	105.4	18	1.01	C.F.	15_	$\vdash$	$\dashv$				-		-	GIZ.	<del>~</del> ~	1// .	7	ted la	7.
		0.2 - 3cm 919 c1751s 11 holisted	-	<del> </del>	<del> </del>						1		1													///C .	bon a L	vein i	μ. LC
		matrie de chlorite, ser cak py; Mylonitic in particles rathin 120jen.	╁	<del> </del> -	<del> </del>	-		$\vdash$	<del> </del>		<del>                                     </del>	-		<del> </del>			$\dashv$	-+						$\vdash$				-	ļ
100 0		Thyloniac in part, clost not the 12450.	╂	<del> </del>	$\vdash$	<del> </del>		<del> </del>	2245	iner i	402.2			Lr.	-	<del>  -</del>	-+	$\dashv$			2.	5	, ,					<del> </del>	-
105 4		Hornkols: 25 2bour.	+-		<del> </del>	<del> </del>			2285	105.9	101.1	<u> </u>	10.1	Lr.	4	<del>  -</del>	-+	-		<u> </u>	4	-	1.2		$\dashv$				-
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FRUM	та	GEOLOGIC DESCRIPTION	2	FROM		TYPE	TCA	ХТСА	SAMPLE SAMPLE NUMBER	FROM	та	MINI Py	Cpy	2   •0+	Cal	مرم	٠	PYRI No.	Cum	No.	Cum	No.	Cum	No.	Cum	AU	Cu SBX	28,	Мо
$\rightarrow$									Nonzek							_		VEIII	VI IN	V E	CVIK	7 6 11 1	VIIIX	W-1.	Z		i	L	
1074	09.1	alz stockwork: All sed		107.4	109.1	Oto PY4	60	40	2286	107.7	110.2	2	0.2	5	4				18	45				2	1_	45	5-	50	ļ
		probables  109.0 30cm Att py cp Q 60°CA  ser, +5° nehwork variables in gto.				"	40	40																			<u> </u>	$\vdash$	L
		109.0 30cm at pyce @ wacA				•	15	20				L						3	1_								L		<del> </del> _
		ser, +5= network vainlets in gto.				uhl g/z	45																				<b> </b>	<u> </u>	_
		Pink silicite Kapin' latepytop	L			Pytep	80,	85				I		ļ				?	2								<b></b>		-
			ᆫ			ļ.,,	0	15				ļ	ļ												-	a.=			-
		Transition Zone: Positive Kapar	_			atronch	30	20	2287_	110.2	///.5	3	, L.	8	4	41		-	1.5	12	15					25	60	15	
	-	test on groundmess of Interpretable.	-		<u> </u>	+cp	40	50	<b></b>			-	<del>  .  </del>			-	-						-				<u> </u>	$\vdash$	$\vdash$
			$\vdash$		· ·		16	30	<b></b>			<del> </del>								-		-+	-				<del>-</del>		
1115	WA	Alana deiri chan	┢			CH2 V.	25.0	$\vdash$	7288	1115	1/40	2	.,	4	2	-	$\neg$	$\neg$	_		-		$\neg$			5		95	
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//O 2	/22.2	Clark to the	╁		<del> </del>	C (4) +		├	1292	1190	/22 2	60	0.8	8	6	,		_		3	40	<del>                                     </del>	$\vdash$					40	15
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		GEDLAGIC DESCRIPTION			:	STRUCTUR	Έ		SAMPLI	ES		MINE	ERAL	S			. }	PYRI	ΙĘ	Qz-F	У.	[CAR]	₽	I		ASSA	.YS		,
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		Ata Feox Hockwork. Calcite													<u> </u>					L.,			<u> </u>				<del> </del>		4
130.1	/33.2	Ota Feax 40 Protolishing coleta			I	Grapata	45/50	65	2296	130.1	133.2	<b>KI.O</b>	10.1	8	5	4					ļ		ļ			25	ļ	75.	28/2
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1362	139.3	As above: Gla Fear replacement				Cm2 615	±30	60	2298	136.1	137.3	0.7	0.6	10	1	4		2	2				L	3	3		L	80	
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	ļ	bonds 2 guiring & pinkish force. Notwork late Facenb = 20°	T			PY	70,30					[			I												<u> </u>		
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1393	W1.3	As above !	П		1	UGAL PATIN	30-45	an	2299	/39.3	1423	0.5	0.5	7	17	4							Ī			25		75	
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a loter while gtz. Granphyllosilicale 140 - 143

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		on 65° co-ey-man -att chi szle -70° pitch laft (Normal), Pinkish tinge			<del></del>	1.014	85	20	<del> </del>		-	<b> </b> -		-	├	┼	-	├	-	┼	-	<del> </del>	-	-					
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151.5	1545	As Above: cp-py min " meinty on heinlim brackures; 1.0.5cm	$\vdash$		<del>                                     </del>		70	45	12303	121.5	154.3	1.0	0.5	0	<u> </u>	~1		+-	0.5	<del> </del>	<del>                                     </del>	<del> </del>	<del> </del>	-		7 77		•	21.20
		on heirling fractures; 110.5cm	H		<del> </del>	<del> </del> -	· · · · · · · · · · · · · · · · · · ·	20	<del> </del>				<del> </del> -	<del> </del>	$\vdash$	-		<del> </del>		<del> </del>	-	<del> </del>	<del> </del>		<b>-</b>				+-
		cy @ 60°CA			-	CP 84	10		<del> </del>			-			-	+-		├		<del> </del>	-	<del> </del>	<del> </del>						+
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15A5	157.6	As Afore. in wk sex gtz = 11 anv.	Н		<del> </del>	9-12.	- 45	65	2304	154.5	157.6	1.5	0.5	10	12	KI		<u> </u>		-	—	├—				7 23	<del>  </del>	(65)	7/182
		dordoning sti to gray glaverine	$\sqcup$		<b>↓</b>		650						ļ			ļ	<u> </u>	<b>!</b>					ļ	ļ			ļ l		
		cp-py ters 12 concentrating meint	Ц		↓	cp-p71	255-60		ļ	ļ				ـــــ	-	-		ऻ		<del>                                     </del>	ļ			<u> </u>	_		$\vdash \vdash$		
		in att v and all envelopes (45/3.1m)			ļ. <u> </u>		45		<u> </u>	ļ	ļ	ļ		ļ	<del> </del>			<u> </u>		<del> </del>	ļ		ļ	ļ	ļ		ļ J		+-
		- gran at in pool milky white - dillined distribution and again.			<u> </u>		=10	10	1	ļ			<u> </u>	L	ļ			↓		ļ	ļ	ļ	ļ	ļ					<del>- i -</del>
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		-green phylosilicate in protolith's zoof	Ц		ļ		ļ		ļ							<u> </u>		<u> </u>		↓_	↓	ļ	<u> </u>						
	<u> </u>	- green phylosilists in problishs and 75 rain @ 157.0-30 erross gla vas.	H		<del> </del>			<del> </del>	<b>-</b>	ļ	·		ļ		-		-	-	-	<del> </del>		<del> </del> -					<del> </del>		
1526	160.6	gray to mithy at a co-py voillets in and adizent to gla voins				CP-PY	50-6	60	2305	152.6	1606	1.0	0.5	10	2	41		1	0.5							>20		80	1
		in and edizent to gla vains					75	5																					
		- green phylosil, gonerally 25																											
		replacement in proteliths																											
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		GEOLOGIC DESCRIPTION	l				_		} 			I		_		MINI	ERAL	IZAT VEIN	IDN IDN							A22A	ve		
FROM	to	GENERAL DESCRIPTION	<b>8</b> -1		το:	TYPE	E	"YTCA	SAMPLE	ES		MIN	ERAL	.S. I ∧∓	1	1 0	r	PYRI	TE	Qz-P	λ	CAR	B	N		ASSA	10	140	Tw.
r KUM	''		25	FRUM	10	ITPE	ILA	ZICA	SAMPLE NUMBER	FRUM	TU	Py	Сру	KeO.	Lai	Col		No. Veln	thk	vein	thk	No. Veln	thk	Vein	thk	73x	SBX	Â9.7	6.
1001	163 /	C 1 : th tt days a C	H			pyrite Ecp	700	// 2	22.00	1101	//2 D	10	0.2	سر ا	,	,		9	2-							5		75	╀┤
100.0	1020	Grey to milk, white at 2 veins and	<b>t</b> t	-	<del> </del>	E CP	aslen	40	7500	100,0	143.7	16.5	0.2	1/2	<b>+</b>	-		2	2				1 . 1					1.7.7	1
<u> </u>	<u> </u>	PROPERTY OF PROPINED BY OFF	1		-		10/30	70				-	<del> </del>	-	<del>                                     </del>	<del> </del>	-											<u> </u>	+
٠٠.		20020 25 on overs while pyrin	1	<del></del>	1435	MGN	45				·		†	<del> </del>	<del> </del>	ł												1	†-
		timent la servicia a relega			703.3	FEIR	7.7.	<del></del>	· · · · · · · · · · · · · · · · · · ·	<del>                                     </del>		<del> </del>	1	1	$\vdash$	<del>                                     </del>													П
<b>†</b>		clar surfacence la marchine	1		<del> </del>	<del> </del>	<del> </del>							<b>†</b> -	<u> </u>	<del> </del>								1					1 1
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h		all acres of the L.U.	t		<del> </del> -	<u> </u>	<del> </del>	†- <i>-</i>				1	†	†	t	1		1									<b>†</b>	1	1-1
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		replacement of problithe by ofta replacement of problithe by ofta replacement of problithe by ofta replaces as on execut while pyrit veins and veinlet = cp and assoc irregular servites envelopes show preference to more massive sta (ie veins), they also accur cuting across probability whether completely on partially allered.	H		<del> </del>	<del>                                     </del>	1	<u> </u>	<del></del>			<del>                                     </del>	<del> </del>	<del>                                     </del>	<del>                                     </del>							-							1-1
	1	CE aline and a	╂┤		<del> </del>	<del>                                     </del>	<del> </del>	<del> </del>	<del> </del>			<del>                                     </del>	<del>                                     </del>	<del>                                     </del>		<del>                                     </del>													H
<b> </b>	<del> </del>	161.9- Icm Jein grun phylosil i Py C 65° As abon irregular network of him can't men't s= verylots proximal to tollowing dute.	1		<b></b>	<del> </del>	<b>-</b>	<del>                                     </del>	<b></b>			t	$t^-$	T	<del> </del>	1							1				<b></b>		1-1
<b></b>	<b>—</b>	10 45°	$\mathbf{H}$			<u> </u>	<u> </u>	<del>                                     </del>	<b>†</b>			<del>                                     </del>	1	1		<del>                                     </del>						-						<u> </u>	
143.6	1/45.2	as show a incompany as hunt of	1		<del> </del>	Pyrita	65	80	2307	1637	145.2	2.0	0.1	15	1	2		5	.5-							2	·	80	1-1
1		fine can't men + 5= vernlets			<b></b>	Carb, man	80	40		1 - 3.1	140	<u> </u>		1	<del> </del>					一									
	1	presimal to tollowing duke.	1			<del>                                     </del>	45	40	<del></del>	1		İ	1	1	1	1													
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				********			1	1				ļ	1	1	1														Ш
165.2	1667	Fg Grey Green Duke: Chillad HW Bolisted at 450 / conted.	П										1																
	-	HW Relieted at 45° // contest.								1		1		1															Ш
·		10% diss Feax in matric d.	П					Ì																					
		collète sericity +? : Cut by	П										1																
		10% diss Feox in matric & calcilo, sericit +?; Culby Man. Fecerb visilet 40°CA.				1			·	1				1						$\neg$									
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146.7	170.6	Oh Feek Stockwork				Pyril	65		2308	14.7	170.6	20	11.0	15	2	3			0,2									75	Ш
		irregular carb-py-cp tser				Pyrih alz V	75						Γ	Ī														Ĭ	
		violets throughout in concentration										Ī	Ī																
		irregular czob-py-cp + ser veinlets throughout in concontration in 10 cm gta reins 2 + 167.5 and 170.3. Cale + carb pentially lordal											<u> </u>							$\Box$									
		170.3. Cale + carb pentially lorded																											$\sqcup$
	ļ	end co has soft sorty coefings -delcocite?											ļ	ļ	ļ														$\sqcup$
		-delcocite?			ļ								<u> </u>	1	L								L						H
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		GEOLOGIC DESCRIPTION					_					MINE				MINE	RAL	IZAT. YEID	ION	·		1848	 <b>T</b>	1 #1	1 20	 A22A	24.	A9 7.	-
FROM		GENERAL DESCRIPTION	- <del> </del>  8-1		r``	TYPE	E	T	SAMPLI	room.		MINE	KAL	>   `+	المما	اود " ا		PYRI	lt.	WZ-P	'y	LAK	ļ.c	WAR	ZOW	A	loi	140	ı m
RUM	טו		84	FRUM	10	TTPE	ILA	AILA	NUMBER	r KUM	10	РУ	СРУ	(e <sub>Q</sub> )	Lai	COC		Vein	thk	Vein	thk	Veir	the	Vein	thk	IBA	SBL	35 %	G
			$\coprod$				<u></u>		<b></b>	ļ						<b> </b>							<u> </u>	ļ			ļ	-	Н
70.6	<u>L23,L</u>	Dyke: fg % thore, wk FLTN Q 45°CA; HW control 35°; FV 25°-slickonside	┦┤			FLTN	45	ļ	<b></b>		L	<u> </u>										.3_	0.5	<del> </del>			ļ <u>-</u>		$\vdash$
		Q 45°CA; HW control 35°; FV	1			ļ			<b></b>						L							-	-	<b>├</b> ─			ļ	<del> </del>	↤
		25" - slickonside			<u> </u>			ļ <u></u>								ļļ.							ļ	ļ	I		ļ		$\vdash$
			$\downarrow \downarrow$		<u> </u>		ļ								<b> </b>								<b>-</b>	<del> </del>			-		Н
73.1	1259	Guerlz-Feox Stockwork. Groy-white all voining with pervesive Silica = sericite and Feox replacement of protoliths (Inter.) and by ap-pysser = carb micro voinlets; thence by an	$\bot$		ļ	Py Gray Qf z + Man	50	ļ <u>.</u>	2309	173.1	175.9	2.0	0,3	12	ļ	4		1	1	<del> </del>				<b> </b>	<del>  </del>		<b></b>	80	ł
		Gray-white call vaining with	1 1		ļ	Gray Qf &	15/55	50		ļ		ļ			<u> </u>	-							↓	<b>├</b>	ļ			<del> </del>	⊬
		pervasive silica + sericite and			ļ										L	<b> </b>							ļ	<b>↓</b>					
		Fear replacement of protoliths	$\perp$			Carpipy	30-60	50							ļ							_	ļ	↓			ļ	<del> </del>	╀
		(Intr.?) and by cp-py+Ser = carb			L.	<u> </u>	<u> </u>					ļ			l							L	ļ	<del> </del>	<u> </u>		ļ	ļ'	╀
]		micro veinlets; thence by an					<u> </u>								<u> </u>							L	<u> </u>	_			<u> </u>	ļ	L
		irregular network of carb = price	<u> </u>				l															L	ļ	↓	ļ		ļ	ļ	L
		veinlets often appearing to cost					l															<u> </u>						ļ	L
		irregular network of carb = py,co veinletafton appearing to cost co with magnetite? (replecement	4																				<u></u>	L	<u> </u>			L	L
		Where co-present carb veinlets	1																										L
		when cp-py serzcarb veinlets concentrate the development					1																						<u> </u> _
		of soricitic envelope more	1																				Ι						
		consumced Late carb althrims	1																									L	L.
		pronounced. Lake carb althrims	1			1			1	1		1																	
			11							1																		I	L
75.9	1729	As Abore: with wester 5=	T		1	which a	60	75	2310	175.9	1789	21.0	6.1	15		2		1	0.4					22	16		L	>75	
74.		veinletting 177 / cloude 140	$\Box$			1	40	25	7.2.										_				T						
		A5° la a 3 cm year late week!	1-1			Py	60	1	1	1		1										1	1						
		cock camb at = 5000 Vein Charin	1/		1	1	-	<b> </b>	1			1																T	Γ
		at lith a 197 molerally Fact	4-1		<del>                                     </del>		† <del></del> -	†	1	1		1										T	1	1					
		veinletting 177. I elongite vug  2 45° in 0.3cm very late weakly cockcomb at 2-spec very Cocosion portulith - 100% replaced by Feox; 178.3 - 0.4cm py	11		<del>                                     </del>		<del>                                     </del>	<b>†</b>		<u> </u>														1				T	Γ
					<del> </del>	<b>†</b>	<u> </u>	<b>†</b>	t	·					<b></b> -								1	1	<b>†</b>				
705	187	Ds Afore	1		$\vdash$	chiligtz	05-0	/0/2	7211	1209	162.0	1.0	0.2	215	1	4		1	1.0					10	9			775	<b>}</b> 19
.'Q. L	PAU	I I S IV BOV	1-		+-	whitegra	50	90	1 × 2! L	110-1	120.	11.10			<del>                                     </del>	17		<u> </u>	<u> </u>			1	1	1			1		1
			+		$\vdash$	carb ±	0-40	60	<del>                                     </del>			<del>                                     </del>		-	<del>                                     </del>								1	1					Γ
			1		<del> </del>	Cerp -	10-70	100	†· ···	·						1 — †				<del> </del>				1			1	1	1
Q7 A	185	AsAbove	$\top$		<b>†</b> • • • • • • • • • • • • • • • • • • •	P.	40	50	2 712	102 0	105 0	1.0	0.2	15	<del>                                     </del>	3		4	2		_		1	13	8	15		760	6
<i>U</i> ∧.V	70.7.V	183.3 -1840 - stringer 201e	+	<del>                                     </del>	<del> </del>	Gray white	40-0	470	2312	TUDE	ייינים ו	1,.,2	ت را	_رر		-		<u> </u>		1		<b>†</b>	·	1	1	1	<b>†</b>	J	Γ
	$\vdash$	Py-cp some disc" blobs cp	$\top$	-	<del>                                     </del>	while glz	70 d	(100)	<del>                                     </del>	†		<del>                                     </del>	<del> </del>			1								1	1				Γ
	<b></b>	1 1- p some aussigning	+-1	<del> </del> -	<del> </del>	win y's	120.2	100	<b>†</b>			† · ·	† ···		$\vdash$	<del>  </del>		$\vdash$	<del>                                     </del>	1		1		1	1			1	1-
	<u> </u>		$\top$	<del>                                     </del>	<del> </del>	<del>                                     </del>	<del>                                     </del>	<del>                                     </del>	<del>                                     </del>	<del> </del>		t	<del>                                     </del>						<u> </u>					1					Γ
	<u> </u>		1-		<u> </u>	<u> </u>	<u> </u>	1. ::	<u> </u>	<u> 1</u>		1			<u> </u>	<u>t i</u>			<u> </u>	t		t	1	1	1 "	<u> </u>	1	ــــــــــــــــــــــــــــــــــــــ	L

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1	t·	GEOLOGIC DESCRIPTION	P-T_		STRUCTUR	E 1	T	SAMPL	ES 1	ı "	MINE	ERAL	ائد. ا	۱. م	- آمر		YRIT	E_	Qz-F	у	CAR!	B. I C	WAT	017	A	10	م ا	T <sub>M</sub> ,
ROM	το		8 g	ROM TO	STRUCTUR	TCA	ZICA	NUMBER	FRUM	10	Ру	Сру	(e)	Cal	Coca	_\	vo. ∕ein	thk	No. Vein	thk	Vein	thk	Vein	thk	IBY.	Cu Sex	än	60
ar o	100.0	No show the	+		MGW	30"	40	23/3	1010	1000	/10	10.1	20		<del>,</del>	$\dashv$	,	3.5		-	,	,	-	ļ		<del> </del>	75	+
03.0	]	As shore mine py stringer	1		FLIN	550	40	1215	103.0	135.0	ζ1.υ	1011	10		<del></del>	-	1-1	,,,				<del>  ′</del>	<del> </del>		<b></b> -	İ	1	1-
		ornhill lerchart - Grat re alecine	1		Carb.	25/45	1		1	<b>-</b>											<u> </u>							
		company of prolotilles. Minon		1	LSTE Gta Coub Spec	45																						L
		chlorich i py stringers. Late open																				<u> </u>	ļ	ļ	<u> </u>	1		1
		profisilly lorabed - crob replacing, companys of prolatilhs. Mining chlorish in prostringers have open brechause in the spece.			py string	e 53-4	70		ļ							_	_					<u> </u>	ļ	ļ		<del>                                     </del>	(	$\perp$
			$\sqcup$		py sta co	4			ļ						_	$\dashv$							<del> </del>	<del> </del>	10		45	110
7 <b>89</b> 0	1900	As Abore: Combonsh stringers with chil + spec.	H		strmun	30		2314	189.0	190.0	1,0	0.]	20	$\dashv$	3	-	-+					-	/	1		<del>                                     </del>	<del> </del>	+
		WITH CHI + Spot.	╂╌┼╌	<del></del>	Cze brnzte,	40	25-	<del> </del>	<del> </del>							$\dashv$	$\dashv$					<del>                                     </del>		<u> </u>		<b></b>		†-
			╂╌┼╌		Cze bonzu.	45	50	<u> </u>	<u> </u>					$\neg \dagger$	_	$\dashv$		$\dashv$				-	<b>†</b>					T
<b>├</b> ──┤			<del>                                     </del>		<del></del>	73	30	<b></b>	<del> </del>					_	-+	_						<u> </u>						
40.0	150.6	als pyrit voin vita py in			Bendin	30°		23/5	190.0	120.6	12	0.1	1		41.	T	$\neg$		7	60							80	
· ·	75.0	some massing brids with trace			1						1.15	· · · · · · · · · · · · · · · · · · ·																L
		hamilite, Although nobel or ato-py now																					L			<u> </u>	L	↓-
									<u> </u>							$\perp$							_			<b>_</b>	-	╀
10.6		ats Fear Stockwork: As above			CP-PY			23/4	1904	194.2	20	0.5	15		4	_	$\dashv$						8	5		<b> </b>	70	╁-
		Grey gtz running sub parillal	$\sqcup$		Spec.	40	30	ļ	ļ		L		<u> </u>	<del>,  </del>		-	$\dashv$									<b> </b>	<u> </u>	╁
		Gren atz running sub proglat to core le 430 with zone notions	$\bot \bot$			ļ	ļ	<u> </u>	<b></b>													<b> </b>	ļ			<del> </del>		
		& CP-py stringers. Stringers not	$\bot \bot$				ļ		<u> </u>							-	-						├	-			<del></del>	╁
	ļ	d Ep-py stringers Stringers not comband to gtz. Late carb to spec @ 40° and till late crackle fraction	<del> </del>			<del> </del>	ļ	<u></u>	<b></b> -									-					<del> </del>		<del> </del> -	<del> </del>		+-
	<del> </del>	@ 40° 700 Fill late crackle Frater	╅╌┼╴						<del> </del>				$\vdash$					$\dashv$			-		├	-	<u> </u>	<del>                                     </del>		t
		subprealled hoose.	╂┼			<del> </del>	ļ- ·	<b></b>					} <del> </del> -													1	1	†
101 2	1962	A show in a selimina of	+	-	Gren G12	100	<del> </del>	2317	190 3	10/ 7	2.0	ME	10-		4	-+	+				<del> </del>	-	<del> </del>	1	<del> </del>	<u> </u>	80	<b>†</b>
'I'.	(1/2)	artitles cult has aveca continuely	t + t			30	<del>                                     </del>	V31.	1(./7:4	776:3	ענ	V. 3	7.2.		-1-						ļ	<u> </u>	1	†		1		
		As above py cp stimums and petities cut by py-cp corbonale reinlets. Appears to carbonate	1 +		py-cp-	50	40	<b>†</b>	<del> </del>							1												T
		sulphish comented breezes. Chlorich	1		LZFO	45		<del></del>	t							_										<u> </u>		L
		mosent.				200																						ļ
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<u> </u>	197.3	Q12 Breezie: cznbonete-5=			Breceistin	30	60	2318	194.3	197.3	5.0	1.5	3		10						ļ		<del> </del>	ļ		ļ	75	+
	<u> </u>	Comented with sericitic 2110	+		Breceisting Control		<b> </b>	ļ	<del> </del>	ļ	<b> </b>							$\dashv$					+-	$\vdash$	ļ	+		+
	<b> </b>	envelope. S= bonding, commoti	1-10	17.0 197	2 7:11 Ba	30	ļ	ļ	ļ ·				<b>├</b>							<del> </del>		<b></b> -	+					+
		voining and breceistion 30°CA	1		-	<del> </del>	<del> </del>	<b> </b>	<del> </del>	<del> </del>	<del> </del>		<del>                                     </del>			-+	$\rightarrow$			<u> </u>	$\vdash$	-	<del> </del>	1	<del> </del>	+		+
	ļ	GP in 0.5 cm Seams and blehs. Leathing of continuous.	1				1		.1	i	1 .	Į.	i L		_					ļ	į		1			1		1-

Lerihing of cerbonitis.

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		I		Γ													MIN	ERAL									,			
		- 1	GEULUGIC DESCRIPTION			;	STRUCTUR	Ε		SAMPL	ES .		MIN	ERAL	. 2				PAK	ITE.	Qz-	Py	CAR	B	INLL	917	ASSA	YYS		
FRUM	T	0		0	FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Ру	Сру	kes'	Cal	Coro		No. Veln	Cur	No. Vein	Cur	No.	Cu n th	m No. k Velr	Cum	Au 18X	Cu S&r	2612	Mu Gr.4
																					Ĺ.									$\sqcup$
197.3	19	23	Quarta- Fear Stockwork: out	<b>!</b>		ļ	Printets			2319	1973	1993	4	0.6	12	ļ	4	ļ	12	1.0	ļ	ļ	1.	1 -	1				75	
L	<del> </del>		by 5/3 py child co stringers and a notion of lole continues sayous	L.		ļ	ļ	00	40		<del> </del>		Ļ	<del> </del>	↓	↓	╙	<u> </u>	ļ	ļ	<b>├</b>	↓	<del> </del>	↓	+	ļ	<u> </u>	<del> </del>	<del> </del>	
	ļ.,		e notwork of late carbonate, soveral	┖	<u> </u>	Ь	7-43	±10	10				ļ	ļ	ļ	ļ	ļ	ļ		ļ	ļ		↓							
	├-	-	UNSS from looghed carbonshe.				27.6±	£ 45	<del></del>	<b> </b>	—		<del> </del>	-	<del> </del>	<del> </del>	┼	-			-	├	-	-	┼		<u> </u>	<del> </del>		
		‡					<del> </del>	90	30	ł	···		ļ	ļ	<del> </del>	<del> </del>	<del> </del>		ļ		<del> </del> -	ł	<del> </del>						1	11
-	-		Olo Paris de la la	-		<del> </del>	nelwork	50/00	70	22.00	1.00	2-2 /	177	, ,	1	<del> </del>	4	-	В	7	-	2.4	-	+	+		$\vdash$	$\vdash$	80	Π-
1923	10	4./	ata Brecie: 2 bonds of				nelwork.	3945	10	45 70	179.3	102.1	7	,,,	4_	┼─	<del>  4</del>		_0_	/		E.7.	·	·†					100.	- -
		¥	precipled giren glz vein+ glz-ser	$\vdash$	·	-	1215	30-43	173	<del> </del>	<del> </del>		╁─	├-	┼	<del> </del>	<del>                                     </del>	-	$\vdash$		<del>                                     </del>		<del>                                     </del>	+	+-			<b></b>		$\sqcap$
			enveloper essemblese separated	-	0-1	· · ·	CS.pour	74 - 10	130	<b></b>	<del> </del>	<del> </del>		├	╂		<del> </del> -		$\vdash$		<del>                                     </del>		┼─		<del> </del>			<b>—</b> ——		
	╁	-	by 0.4 m loss 2/1 cure. Strong	-	201	1.5cm	Carbonio Carbonio Carbonio En fork	20		<del> </del>	<del> </del>		╂─	├	+	-	-	-	$\vdash$		<del>                                     </del>		$\vdash$	+	+	_		$\vdash$	<b></b>	
			pyrcp = chi, ser as difused bands	-	ļ			├	<del> </del>	<b></b>	<del> </del> -		├	ļ	┼—	<del> </del>	<del> </del>	-	-		-		<del> </del> -	+	<del> </del>					
	╁		and notwork of vanlets and stringer	$\vdash$			<del> </del>			<del>                                     </del>	-	-	╂─	├	┼	<del>                                     </del>	<del> </del>	-	-	<del></del>	-	$\vdash$	<del>                                     </del>	+	+	$\vdash$		<del>                                     </del>		$\Box$
ļ .	ļ	- · ∤	and notwork of vainlets and stringers.  Mid section low 5= strong shl zll a  of parteliths 200.5 strong leaching  of czebonzte from 20 reinlets (vaggy)	٠					· · · ·			1	٠.	1		-								· <del> </del>		1				
	╀	-+	of protoliths 200.5 strong lexchin				<del> </del>	├			<del> </del>		<del> </del>	<del> </del>	┼	<del> </del>	-		-			-	┼	+-	+	-	_	<del> </del>	<b></b>	$\vdash$
	∤		of czobonzte from 20 reintels (vuggy)	-	<u> </u>										<del> </del>	·					<del> </del>		<del> </del>	+	+			<u> </u>		-
	┼-		- Zome may quality es Q12 - py vein?	-	ļ		<del> </del>			<del> </del>	<del> </del>		<del> </del> —	<del> </del>	┼─	+	┼				<del> </del>		+	+	┼	-		<del> </del>	·	<del> </del>
	┨			-	<u> </u>	├	ļ			<b></b>			ł	<del> </del>	<del> </del>	<del> </del>	-		<del> </del>		<del> </del>		<del> </del> -						4	-1
200 1	0~		01	┨		<del> </del> -	EW. MGN	110	<del> </del>			242.3	<del> </del> _	. 3	1	<del>  </del>	1	-	<del>                                     </del>	-	<del> </del>	40	-	+	+	$\vdash$		_	80	+
ן. גשו	10	۶:S	Oto ramissimila to above with				FILTH FILTH PY-17 MGI	43		2321	1021	205.5	ス	0.3	<b></b>		- A-				-/-	40			+					1 1
<u> </u>	+	-+	will rack on HWIF W= 60cm	-	ļ	<del> </del>	Steingers	30	-	<b>}</b>			├	-	┼	₩	┼	-	<del> </del> —		-	├	-	+	+			<del>                                     </del>		$\vdash$
<b></b>	-	-	well rack on HWOFW = 60cm Patches cp + py in middle of vain Chl. in py and in purbliths	-	ļ	-	<del> </del>		<del> </del>	<b></b>	ļ		<b></b>		┼	-			$\vdash$			<del>                                     </del>		+		$\vdash$		-		
<u> </u>	+	$\dashv$	Chl. in py and in phylatiks	$\vdash$		-	<del> </del>			<del> </del>	<del> </del>		├	-	┼─	┼	<del> </del>	$\vdash$	-			$\vdash$	-	+	+	<del>                                     </del>		<del>                                     </del>	<del>                                     </del>	-
2022	124	- //	9ta-FeOx Stockwork; broken con	┨	-	<del> </del>	Q Q+2		7.0	2222	2023	2054	1,5	01	12	<del> </del>	4	-	$\vdash$			<del>                                     </del>	1		+	<del> </del>		<b>†</b>	80	-
103.5	100	2.77	GVI-FEUX SHERWIFF, BIRKETON	Н	<del> </del>				50	1227	XU3.)	403.7	1/.5	0.7	₩^	+	<del>  '-</del>	<del>                                     </del>	<b> </b>	_	<del>                                     </del>	-	$\vdash$	+	+				-	
	+	†	minon py-cp stringers and corb-py stringers. Chi in proteliths.	-	<del> </del>		corbight	00'	1				1	<b>†</b>			†· - ·				<del> </del>		· ·	1	1	- 1		1	, ,	
	+	-†	Strongon, Chi In All William	$\vdash$		-	127	45	<del> </del>		<del>                                     </del>	<del>                                     </del>	$\vdash$	<del> </del>	<del>                                     </del>	<u> </u>	<del> </del>						1	1	<b>†</b>					
	†	†		1			<del> </del>	3.5.	<b>-</b>				ļ · ·		<b>†</b>	†·	1						†	1	1	1 1				
DOK U	20	73	Ola Burning Control				Stemp	30-70		2323	2054	20.7	30	1.5	12	1-	8		<b>—</b>		$\vdash$		1	1	1				90	
7 .ويبر	1~0	٠ <i>٠</i>	Olz Breeciz: Crusted appearant - Notwork of late Czebergli stronger	$\vdash$		<del>                                     </del>	Scember.	70 /	<del> </del>	30.	140267	20.7	1	,	12		T					ļ	†	+	1			1	1	
	+	_	Troposte of 14- 6-20 des) 1- Stranger	$\vdash$			<u>†                                      </u>			<b></b>	<del>                                     </del>		<del>                                     </del>	<del>                                     </del>	<del>                                     </del>															
	1																													
706.3	20	9.4	Ott Breccia: crushed appearance.				Py vein	45	100	2324	206.3	2024	3.0	1.0	1		5		2	4		ļ	ļ	1					85	
			combonate/coloite lerchel; coretite				Propins	45	70				L											1	-					-
	$\Gamma$		tornish on cp \$50% recom, Feat	?			General	40	70														<u> </u>	1						
	Τ				L		1	Ι				I	I	I	1	1	1.													-+

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		CERT GETS DESCRIPTION	T						-						*****	MINI		IZAT		Pin	k					1 400/			m+
Ι.		GEOLOGIC DESCRIPTION	١.,		, :	STRUCTUR	Ę		SAMPLI	ËZ		MIN	FRAL	<b>S</b>	,	1 .1		PYRI	(TE	Qz-I	у	CAR	₿	V/X	COYE	Mass	113	1.	١
FRUM	τυ		84	FRUM	TO	TYPE	TÇA	ХTСА	SAMPLE NUMBER	FRUM	το	Ру	Сру	Kelt	Cal	Coto		No. ∨ein	Cum thk	No. Vein	Cum thk	No. Veln	Cu n thi	M No.' Velr	Cum	Au 1/5/	581	A9,2	Mu Gr G
205.4	212 4	Gla Buccia: Body busher com.	╀		_	Pywin	70.	10B	2325	2024	212.4	7	10	2		5		6	6				+	+	├─	<del> </del> -	+	90	+
	,	on-co es stringer and dissed. Vuggy fredures - combanto lecched?				Stringer	80.	60	2325				0.0	- J.								<u> </u>	1	1_	<u> </u>				
		Fizzdunes - czobonzło lecchal?	<b>-</b>	2/0.8	L	Carb Billad Shear	1 77 25	140																.					$\ \cdot\ $
			$\vdash$	40.0	<u></u>					<del> </del>		<u> </u>												1	<b>1</b>		<u> </u>		$\prod$
2124	215.5	As above: crushed appearant str	L			while of	300	ļ	2326	2124	2/5.5	6	06	10		7							1	4	3		ļ	25	$\coprod$
		Nobrok & czob + py cp stringers	1_		ļ	CP- 07 -	45	30		ļ		ļ.,	ļ <u></u> .		L	ļ	<u> </u>	ļ		ļ	ļ	L	<b>.</b>		<del> </del>	<b> </b>			
		26 45-60', 05". Mind of cu ternisher			ļ	ļ .	40	50				<u> </u>					ļ	L				↓	—	+				<b>—</b>	++
		or with black sody costing Mixad	L		<u>.</u>		05	20				L						<u> </u>		L			↓_	↓	ļ	<b>!</b>	ļ	ļ	<b>↓</b> .
		Notwork of Czob + py cp stringers 26 45-60', 05'. Mont of cy ternister! or with black sody costing. Missal with Questa Frox rock	$\perp$				ļ	-		ļ										-		-	$\vdash$	$\vdash$	-		ļ	-	+
205.5	217.9	Quals - Feex Stockwork : Controllate	1			Spingers	45°	50	2327	215.5	20.7	5	1.0	4		4				1	100							80	
	l	hzirling czob-py-cp stringers			L	Stringers	£ 5"	50	L			l						l				L	ļ	ļ	ļ		ļ. <u>.</u>	1	1
		subproselled to come - open springe					60°				<u> </u>												ـــــ	.↓		L	ļ	<del> </del>	1-1-
		heirlan corb-py-cp stringers subpressed to core - open special 216.3-217.3 Qualque vain with	L																				↓		<u> </u>	ļ	ļ	L	
		CP-py stringer suprelled core - open	Ι																						<u> </u>	L	<u> </u>	<u> </u>	<b>↓</b> ¦_
		cp-py stronger sapprolled core - open and et 60° - blobs of cp; spec hom	$\Box$					ļ												_			ļ			ļ		ļ	
		toy on the perstel fracture,	╀				<del> </del>	-				-			_			_	ļ	-			+-	+-	-		<del> </del>	-	$\vdash$
217.9	218,5	Fault: no come.																					1						
	2014	01. 5. 61 / 1.11	$\vdash$			DYCP	ļ	ļ		2.0.5									├—	ļ			┼			<del> </del> —	<del> </del>	760	
		G17 Feax Shoot work : broken come	-			PT (P	50		2328	Alg.S	141.6	20	0.1	17		8	<u> </u>						+		$\vdash$		┼	160	++
10%	440	hem >> mays.	╁				<del> </del> -	<del> </del> -															+	<del> </del>	<del> </del> -			ł	
22/.6	224.6	As zbum: 15 5 = (pyxxxp) in		221.6	22.9	GH2 V. BX			2329	226	2244	4	0.5	12		5		3	3									60	
		Q12 bx : protolithe replaced by	L			Stringer	40			<u> </u>													1	┶	<u> </u>	<u> </u>	ļ	<b>↓</b>	<u></u>
		Man, chi, carb, Rock Longs to					60		I			L													<u> </u>		ļ		
		Perdone porallol to come.				Prins	30/45		I														_				<u> </u>	<u> </u>	
						Crot Pylp Emyata	25/50	50	I															<u> </u>			ļ		ļ
					ļ	Emyatz	45°																-		_		<del> </del>		<del> </del>
224.6		SILICIFIED QUARTZ IRON	+	224.6	227.0	PINK OFE Py STGR	0	10	2330	2246	227.0	0.6	Tr	10	0	0.1		0	_	15	87	0	-	10	13.5				
		OXIDE BRECCIA as above	T		1	1	30	50	1						_								Τ						
			1		1	1	50	T	1	1	1	1				11			T	T		1		7		I	1		
			†	<b> </b>	<del> </del>	WAY . 072	50		<b></b>			<del>                                     </del>	<b>-</b>				_	<del>                                     </del>		t		1	T	1	1	1			

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		GEOLOGIC DESCRIPTION				ETPLICTUR			SAMPL			L	ERAL	c		MINE	RAL 12			۸. <u>۴</u>	******************		1444		ASSA	AYS	***
ROM	TO		28	FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Сру	KeD+	Cal	Coto	Ņ	o. Cu	ım No. ık Vel	Cur	n No.	Cur n thi	No. Veir	Cum	ASSA Au	Cu	Ag
24.6		(con l'd) SILICIFIED QUARTZ		227.0	230.	PUSTER	50	100	233/	227.0	230.0	0.2	7-	10	0	7		0 -	8	13	0	_	9	12			
		IRON OXIDE BRECCIA	7			598X	20	30													$\Gamma$	L					
Ī						•	50	35														<u> </u>	L			<u> </u>	<u> </u>
							70	35				I					$\perp$				ļ	↓	L	ļ		ļ	
																			_	ļ	ļ	↓_	ļ	ļi	<u> </u>	<u> </u>	<del> </del>
				230.0	233.0	STOR	20	45	2332	2300	233.0	0.6	7-	10	0	0.2		2 -	11	41	0	1-	5	16	<b> </b>	<del></del>	<del> </del>
						~	50	15			<u> </u>	ļ	<u> </u>	ļ						↓	₩	↓	₩	ļ	ļ	<b>├</b>	
					L		70	10			ļ	ļ	ļ							ļ		ļ	ļ		<b>├</b>	<u></u> .	
			$\perp$		L	STEX	50	60		ļ			Ь	<b> </b>						$\vdash$	<del> </del>	+	<del> </del>	-			
					<u> </u>	"	70	10			ļ		ļ <u>.</u>	<b> </b>						<b></b>		↓	<del> </del>	ļ	<u> </u>	ļ	
					<u> </u>		<u> </u>			-			ļ	ļ			-		_			╁	₩	-	<u> </u>	<del> </del>	
			2	235.0	236.0	STEK	20	10	2333	233.0	236.0	0.4	Tr	10	0	0.15		2 -	1	20	0	1-	0	-		<del> </del>	<b></b>
			$\Box$			"	50	10		ļ	<u> </u>		ļ	ļ	L				-	-	-		-	<b> </b>	ļ	<b>├</b>	—
						"	70	80					ļ	ļ						<u> </u>	↓	<del> </del>		ļ		<u> </u>	
		Bull gtz vein included -	-	234.8	235.2	QTZ	20/20			<u> </u>				ļ			_			<b>↓</b>	1	ļ	-	<b> </b>		<b>├</b>	
		shows PQRy replacement at											ļ	ļ					$\bot$		<b>↓</b>		ļ	ļ		<u> </u>	
		margins										L	ļ	<u> </u>					┥	—	↓	<u> </u>	<b> </b>	-	<b></b>		
														L							ļ	ļ		L			
		8238.7m : sport of electron in		736.0	289.0	5762	20	10	2334	236.0	237.0	0.4	Tr	10	0	0.1		<u> </u>	9	40	20	-	0	-			
		1.0mm Cpy STGR at 70° ca in				"	50	80					ļ	ļ						$\perp$	<del> </del>	<b>_</b>	ļ	ļi			
		zone of Pap, replacement				"	70	10		ļ		<u> </u>	ļ	ļ				<u> </u>		—	<del> </del>	-	↓	ļ		—	
						BARZ												-				ļ	l				
			_	37.0	242.0	STOR	50		2535	239.0	2 <b>42.0</b>	0.4	7-	10	0	0.3		<u> </u>	8	12	10	1-	3	4		-	
		@239.7: gradual onsel of non-			ļ	W	70	10	<b></b>				ļ	ļ						<del> </del>	<del> </del>	<del> </del>	ļ			<del></del>	
		replaced country rock frag-				STER	50	35	ļ				ļ	<u> </u>		$\rightarrow$		_		₩	↓		₩	<del> </del> -	<u> </u>	<del></del>	<del></del>
		mente.			ļ	~	70	65		<u></u>				l					_	<b>_</b>	<u> </u>	ļ	ļ	ļ	ļ	ļ	
								<u> </u>		<u> </u>								$\perp$	$\bot$		<u> </u>	ļ	<u> </u>		L	<u> </u>	
		2242.3 - 242.4m : YNLT OTZ CAR P. 90		42.0	245.0	STOR	50	75	2336	242.0	245. o	1.0	T-	10	0	1.3		2 -	1	9	0		0	-		ļ	
		,				"	70	25															<u> </u>				
		,				1																	l				
			7	45.0	248.	FIGE	20	50	2337	245.0	248.0	0.8	To	10	0	0.5	-	2 -	4	/3	0	I-	0	-			
			Ī			"	50	50																			
			1					1	1	1			1									1	Ţ				
		@249.6m: return of total Fe Ox	T,	48.0	251.0	STOK	20	100	2338	248.0	25/. 0	0.4	Tr	10	0	0.3	7	0 -	2	19	0	-	1	1			
		replacement of country	I			STOR WG PY STOR	70	100				1		, ,					1								
-		7	-			2,5	1	1	<del>                                     </del>	1	· · · · ·	t	<del>                                     </del>	1						1	1	1			·		

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		GEOLOGIC DESCRIPTION				TRUCTUR	ε.		SAMPLE	ES.		MINI	RAL	S.		MINE	RAL	ZATI YEIN PYRI	ON S TE	<i>Pi</i> ,	ķ.	[CAR	Ŗ	WI	Cum thk	AZZA	YS		
FROM	TO	0		FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Ру	Сру	KeO+	Cal	Colyo		No. Vein	Cum thk	No. Veln	Cum thk	No. Vein	Cur	No. Ven	Cum thk	Au	Cu	Ag	Мо
27.6		(cont'd) SILICIFIED QUARTZ	$\perp$	25/.0	254.0	596K	20	25	2339	251.0	254.6	0.6	Tr	10	0	0.3		0	-	4	18	0	-	0	-				$\perp$
[		PRONOMIDE BRECCIA				"	50	75													L	<u> </u>		<u> </u>					
			T																		<u>.</u>						· .	L	
			T	254.0	257.0	STER	20	25	2340	254.0	257.0	0.8	Tr	10	0	0.3		0	١	8	28	0	-	3	7			l	
I			T		i	"	50	15																					
			T			STER	50	35 65																					
						~	70	65		I													<u> </u>						
												Γ					I					<u>.</u>	l	l					ļ
			$\mathbf{I}$	257.0	260.0	576 K	50	65	234/	257.0	260.0	3.0	Tr	10	0	0.2		/	4	6	12	0	_	2	4				↓_
			$\mathbf{I}$			••	70	35															<u> </u>	1					
						STER	50	50																<u> </u>					↓
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						Ry STGA	70	100		Ī		<u> </u>					1					<u> </u>	<u></u>	<u> </u>					$\vdash$
																						<u> </u>							
			T	260.0	245.0	Pary	20	65	2342	260.0	263.0	0.4	Tr	10	0	0.2		0	-	3	55	0	-	1	/				
			$\top$				50										$\neg$											l	1.
			1			WQPy	5	100	1	1							<b>1</b>					1							
			+		$\vdash$	7			ļ			1		-			$\neg$					1							
		15/15/10/10/10/10/10/10/10/10/10/10/10/10/10/	+-	2/10	• • • •	Par,	70	100	2343	2/3 0	244.0	06	0.2	10	0	2	_	0	-		19	0	-	3	3/				1-
			+	245.0					-37.5	1.0.0	200.	10.0		<del></del>	-	-	$\dashv$			-	_	1	$\vdash$	<del> </del>					1
			+-	<del> </del>	_	WaPy	70	65	<del> </del>	<del> </del> -	<del> </del>	<del> </del> -			-	$\vdash$							<del> </del>	<del> </del>					1
			+-				10	65	<del> </del>	<del>                                     </del>		<del> </del>		<del>                                     </del>	<del> </del>	$\vdash$						$\vdash$	_	<del>                                     </del>	$\Box$				+-
						Fary	20	10-	2344	2110	290	100		1	_	2 3		0	_	6	97	0	_	8	28				<b>†</b>
			+	262.5	267.0	4.4	50	70	2577	200.0	267.0	0.8	0.2	10	-	0.2		-		۳	-	1	_	1	-			<b></b>	+
		78 · · · · · · · · · · · · · · · · · · ·	-†		<del> </del>		70	15	· · · · · · · ·							1						† <del></del>		†				ļ	1
			+			Wary.	50	25				<del> </del>			_	1-1	-		-				<del> </del>	$\vdash$					1
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			+	2190	272.0	Fary	20	15	2345	2/90	272 0	6	7	10		0,2		0	_	9	60	0	_	2	34				1-
			+	207.0	-/	","	50	60		20/.0	-/2.0	۲۰۰		,	<u> </u>		_	_		_		_		<b>_</b>					
			+		_	"	70	25								1+								†					1
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			Τ														RALI	ZATI	JN.	622	·			5.72	. <del>य</del> ा "1	·			
		GEOLOGIC DESCRIPTION	l		;	STRUCTUR	E		SAMPLE	ES		MINE	RAL	S				PYRIT	Ē.	Oz-F	<u> </u>	CARI		02	A	ASSA	ZYS		
FROM	τo		2	FROM	TO	TYPE	TCA	ХТСА	SAMPLE SAMPLE NUMBER	FROM	τo	Ру	Сру	<b>€</b> 0†	Cal	%,		No. ( Veln 1	Cum	No. Veln	Cum	No. V∉ln	Cum thk	No. V∉ln	Cum	Au	Cu	Ag	Mo
224.6		cont'd) SILICIFIED QUARTY				POP	50	60	2356	302.0	305.0	0.7	Tr	10	0	Tr	I	0 -	_	5	20	0	-	_	2		ļ	┼—	$\vdash$
		IRON ONDE PILLOTA.				"	70	40	I			<b>.</b>															ļ	ļ	
			T	Ī		WQR	50	100				L_																	-
		0.4 m corr/oss; no obvious angle.	Τ	302.7	303.1	FAULT	?				L																	ļ	
		rock after fault is not titolly	Τ															l_										_	↓
			T																									<u> </u>	1
		replaced with quarte	†-	205.0	2000	Pary	50	50	2357	305.0	308.0	0.4	72	10	0	Tr		0	-	4	4	0	1	0	1			l	1_
-			╁	303.0	307.0	7 477		50		555.5		1	<del>'</del>		<u> </u>														
			<del>-</del>		<del> </del>		2	130	ł	<del> </del>		†- ··			ļ					$\vdash$		<del>                                     </del>	_	<b></b>			1	1	1
-		1.0m loss	╀	305.7	306.7	FAULT	ļ:-	-	<del> </del>	+		<del> </del>	-	-	<del></del>	1				_		<del> </del>					<del>                                     </del>	1	_
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			4-	308.0	3//.0	Pary	20		2358	308.0	3/1.0	1.3	0, Z	/_	0	0.2		0		7	0/	-		-			<del> </del>	+	+
L			1			//	50	<u> </u>	ļ	ļ	ļ	ļ		ļ	├—	$\vdash$							<u> </u>		<u> </u>			<del> </del>	+
			1	<u> </u>	L	"	70	30	L	↓		↓_				L				<u> </u>		├	<u> </u>	<u> </u>	├	├	-	┼	+
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			1.	711.0	3/4.0	Fary	20	10	2359	311.0	3/4.0	0.6	Tr	10	0	0.3		0	_	9	22	0	-	0	_				$\perp$
			L			"	50	80	İ			1	ļ <u>.</u>									ļ		ļ		<u> </u>	ļ	<del></del>	
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		3214.9-815.8: pro proposal	$\perp$	74.0	217.0	Pary	50	65	2360	214.0	317.0	1.6	7.	10	Tr	1.3		0	-	6	3	0	-	0	_		<del> </del>	<del> </del>	+
		si citized intermediate dype:		1		"	70	35				1			<u> </u>							<u> </u>		ļ	<u> </u>	<u> </u>	ļ	<b></b>	
		crackled with hem and fracture								<u> </u>		_					_				L		ļ		<u> </u>	ļ	-	<del> </del>	+-
		filling.										l			<u> </u>							<b> </b>	<u> </u>	ļ		ļ	<del> </del>	<del> </del>	-l
			Т	3/7.0	320.0	Par	50	80	2361	317.0	320.0	1.7	Tr	10	0.3	0.3		0	-	12	28	0	_	0	_			↓	┵
			Τ			,,	70	20		1												l							ļ
tt			†-		1		†	† <b>-</b>	1	1	1	1	1	1	1							T	Ī					l	L
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┝┈┈┼╴			十	320.0	1.22.7	"	70	20	2002	10.0	1	10.0		<u> </u>			$\neg$			_		1							T
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322.9 3	24.7	ANDESITE DYKE: medium	+						2363	322.9	324.	7	·			···		$\vdash$			-	<del>                                     </del>	<del> </del>					<del> </del>	-
$\vdash$		green; 4 0.5 mm grain size	+		<del> </del>		<del> </del>	+	<del> </del>			+	<del>                                     </del>		-	$\vdash$		$\vdash$		$\vdash$	-	-	-		_		<del> </del>	+	+
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$\vdash$		@324.7-326.7: quarte de plated on	+	-	$\vdash$		-						-	—	-			1		_	_	<del> </del>	-	0	-		1	+	+
		margin of dy he	1	-	-	POR	20	1	2364	324.7	320.4	p. 5	7	20	10	0.3		0		4	#	0			ļ				+-
		@327.6 -328.0: massive prognette	$\perp$		↓	/-	50	50	ļ	ļ		₩		-	<u> </u>	<del>                                     </del>		$\vdash$						-	-	<u> </u>		+	+
LL		UCZO, LC90 , FOLN 90		<u> </u>	1	,.	70	25	1	1	1	1	ŀ	1		1					<u> </u>	1	1	1	L	l	.1		

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		GENERAL DESCRIPTION					_					l					RAL 17/	ZNL.	1	int	7575		101	1.6	1224	. 76	
αмΊ	TO	G. OCTORE DESCRIPTION	Ŋ.	FROM	 TO	TYPE	TCA	%TCA	SAMPLE	ES	TO	Py	CDY	S   S <sup>†</sup>	Cal	ζΦ	PY No	RITE Cu	M No.	Cur	No.	Cur	No.	Cum	AZZA uA	Cu	Ag
_			89						NUMBER			,		Ker		Co.	V 9	in th	k Vel &	thk	Veli	thk	Vein	thk	<del></del>	-	1
1.7		(cont &) SILICIFIED QUARTE	-			Pary			2365	328.0	33/.0	1.3	70	10	0	0.3	+-	+/	18	2/	10	<del>  -</del>	10	1			┼—
		IRON OXIDE BRECCIA	1					60			ļ	ļ					-	-		-			<del> </del>			<del>                                     </del>	┼
_		@328.0-328.5 : brenia is	L			<u> </u>		25		<u> </u>						$\vdash$		4_				↓	₩	$\vdash$	<u> </u>		-
		mylonitized & undulating tol'n P 45° - 90°. Strong @ 90° @ LC @ 328.5 - 329.2: cata rlacke bx.				Py	70	100				L					_			↓	ļ	<del> </del>	↓				┦
$\perp$		2 45°- 90°. Strong @ 90° @ LC.						<u> </u>		<u> </u>						<u> </u>				<b>↓</b> _	↓	╙	↓	$\sqcup$			↓_
		@ 328.5 - 329.2 : catarlacke bx.												_								<u> </u>	$\vdash$	1			ļ
		Irags 5 Icm LC 70. @330.9: onset at bull quartz												$\sqcup$					$\perp$	↓_		↓	↓	Ш			<del>-</del>
[	*	@330.9: onset at bull quartz																			ļ	_		1			ļ
		stringers.	L													1			4_	↓	<del> </del>	↓	<del>↓</del>	<b> </b>		ļ	
	-	stringers. Note onset of pyrite strings	c			Py			2366	3310	334.0	2.8	0.4	10	0	0.4	_/	1		16	0	_	8	25	$\vdash$		· <b>}</b> -
						PORy	50	20										-		↓_	<del>  </del>		↓	igspace	—		$\leftarrow$
_						"	70	10		ļ		ļ				$\sqcup \sqcup$			1_	ـــــ	↓	ļ	—	igspace			
			L			Wary	20	25		L	<u> </u>	L							4	_	<del> </del>	<b> </b>	—	$\sqcup$		<u> </u>	₩-
						,, /	50	60	<u> </u>												╙	<u> </u>	↓	ļ!		ļ	1-
						//	70	15	l															$oxed{oxed}$	$ldsymbol{ldsymbol{ldsymbol{eta}}}$		
T			Γ																		1	1				<u></u>	1_
		+ 23 Bull quarte = chl in	T			P	50	100	2367	334.0	337.0	5.2	0.3	10	0	0.2		5	6	2/	0	-	6	9			
$\neg$	-	+ 23 Bull quartz & chl in this sample interval	T			Py	20	15											$\top$								
			1			",	50	50	1			1						$\top$									
7			T			"	70	35	<b></b>	1																	
_			1-	1		WOP	20	<del></del>		·	İ	<b></b>						_	$\top$	1	1		_			1	1
寸			$\vdash$			"	50	65		<b>†</b>	<del> </del>	<del>                                     </del>					$\neg$		_	$\top$		1					
†			1	tt		<del></del>	70	20	<u> </u>	·†		1				1-1				1	1	1	1				
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-†		@338.5 - 339.2: first large sull quarte rein * This samp interval comprises 60% bull gtz.	1	1 1		Py	70	100	2368	337.0	340 0	23	7-	10	0	0.5	12	0.	2 4	12	0	1-	5	12			
7		and quarte year	+-	1		Pary	50	75	2300	757.0	7.7-1.5	P	-	1				1	7		1						
+		Y This sample interval	t			~ /	70		1	1		1		-					1								
_		Companies 60% bull ate	1			War	50	_	1	1																	
_		772.	†			"		50	1	1	<del></del>	1					$\neg$		1	1			1				
_		· · · · · · · · · · · · · · · · · · ·	1	$\vdash$		<del></del> -	1	1				t				1		1	1	1							
		@341.0: Sem mad star & de	T	1		Pary	20	100	2369	240.0	344.0	To	To	15	0	0.2	1	,   -	1	7	0	1-	2	3		1	
		@341.0: Scm. mag. stgr. \$ 45° @ 341.7: 10cm. mag. vn/t \$ 50°				War	20	50	T-°'	7	7.3.5	1	<del>-</del>	<u> </u>	<u> </u>			1.	+-	1			1				T
+		2 342.3: 10 in. mag. vnlt. 4 40°	$\vdash$	<del>                                     </del>		Wary.	50			†				† "		1	_	$\top$	_	+-		1	1				1
_		372.3.70.2.2.7.7.2.7.7.2	╁┈	1		P			2370	7000	2410	7-	7-	10	0	5	1,	1	+,	6	0	1-	0	-			_
-		@345 6: April of	+-			//		50	23/0	349.0	70.0	†′′~	1/5	1		F.'+	<del> -</del>	Ť	+	+=	1	†~-	†	1			1
┪		@345.5: onset of mag, 9tz, py vein; mottled c.g. texture py d.	1			PQPy		100	<del></del>	<del> </del>		╁		$\vdash$		<del>                                     </del>		+-	┪	+	$\vdash$	+	+	1			<del>                                     </del>
-+		wein; moved c.g. lexture py d.	¥5	1.21	2011	LYLY	120	1,00	ļ		ļ		~	1		<b>+</b> +		-	+-		+						1

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			Γ						[							MINER	ALIZA	ION		4.1.1	~.			٠,٠			
	- 1	GEOLOGIC DESCRIPTION	ı		5	TRUCTUR	E		SAMPLI	ES .		MIN	ERAL	2			PYR	NS	10z-	Py	ICAR	B	Oz.	A	ASSA	YS	
FROM	то		8	FROM	TO	TYPE	TCA	%TCA	SAMPLE SAMPLE NUMBER	FROM	TO	Ру	Сру	, a0+	Cal	30	No.	Cum	No.	Cum	No.	Cur	No.	Cum	Au	Cu	Ag
324.7		cont'd) SILICITIED QUARTE	183			Py POPy	50	100	237/	344.0	249 3	37	Tr	45	0	0.2	V EII	6	2	180	Veir	-	0	-			
324:1		PRON DEIDE BRECCIA	$\vdash$	<del>                                     </del>		000	50			778.5	377. 3		-	1	<u> </u>		15	<del> </del>	<del>  _</del> _	7.50	1	$\vdash$					
ł · † -		RIATE DECLIA		<b></b>		rary	50 70	50				· ·				<del>  -</del>		<del> </del>	<del>                                     </del>		<del> </del>	<del> </del>	<del> </del>	$\vdash$			
<del>                                     </del>		@ 347.3: end of neare grained	$\vdash$				10	50	<del></del>			<del> </del>	-			<del>                                     </del>	+	┼─	<del>                                     </del>	<del> </del>	<del>                                     </del>	<del> </del>	-				
<del>-</del>		pressively replaced by prote 347.0	-	<del> </del> -			ļ	<del> </del> -					<del> </del>			<del>                                     </del>		┼	┼		<del> </del>	┼					
<b></b>		messively replaced by pyrite 347.0	┨	<del> </del>		<del> </del>		-					├	-			+	┼	╁		⊢	-		$\vdash$		<u> </u>	
┟		347.3.											·				10	┼	0		0	<del> </del>	0				
<b> </b>		* Note onset of sheeted pink quotiz pyrite yeins in Same. No. 2371. These veins also contain sovered per- curt light green phyllosilicate chlorite sericite? In fractures	-		very	silice	CUE.		2372	549.3	352.0	0.5	70	10	0	P./	10	-	10	<del>-</del>	10	-	10	-			<del></del>
+ +		pyrite yeins in Samp. No. 2371; These	ļ	ļ								ŀ			ļ			ļ	<del>  _</del>	<del> </del> -	0	-	0				·
		Veins also contain soverel per.	_	L	•			<u> </u>	2373	352.0	355.0	0.3	Ir	10	0	0./	0	ļ-	0	<u> </u>	0	1-	10	-		<b> </b>	<del></del>
		cort light green phyllosilicate	L	ļ						ļ		ļ	ļ		ļ			ļ	<u> </u>	<u> </u>	ļ		↓				
		(chlorite sericite?) on fractures				Pary			2374	355.0	350.0	0.Z	1.4	10	0	p./	10	-	7	175	0	-	0	_		<b> </b>	
$oxed{oxed}$		and shears within the quartz				"	50	60	<u> </u>	l		L		L				<u> </u>			<u> </u>						
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						POPY	50	65	2375	358.0	361.0	1.4	Tr	10	0	0.1	0	_	3	12	0	<u> </u>	1	/			
			Γ			"	70	35										Ī	Ī								
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			$\Box$			POPy	50	25	2376	3410	344.0	0.4	70	10	0	0.1	0	1-	4	4	0	-	1	3			
			<b>†</b>			"	70	75	1	-	-			1				1									
			$\vdash$		_	Wary		100										T	1		Г	<b>†</b>					
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		GEOLOGIC DESCRIPTION				CTRUCTUR	_		SAMPL	FS		MINI	r DAI	•				YEI	Ÿ\$	P, 1	*	ir ab	· ·	اس	,, <u>C</u>	ASSA	ZYA		
ROM	το		8.	FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	Tn	Ру	Сру	St	Cal	مرم		No.	Cum	No.	Cum	No.	Cur	No.	Cur	Au	Cu	Ag	
	-		189		-	<del> </del>	┼	<del> </del>	NOMBER	<del> </del>			_	-	-	C	-	∨ ein	TOK	V ein	THE	V RII	TOR	<b>V Q</b>	TOR				1
57./	363	Heyz crystic Dyke: 0.5 x 1.0cm							2378	367.1	368.3		-		-											Ţ			1
		blocky phenocrysts in Eq. sericitis matrix. Phenos (Kapar?) aftering	L											L							_		↓	↓	↓	ļ	<b>↓</b>	—	-
		matrix. Phenos (Ksorr?) altering							L			L									L	L	<b> </b>	<u> </u>	ļ	<u> </u>	ļ	<b>↓</b>	_
		to calcile + sericite 8% disse	Ŀ										<u> </u>				$\Box$					L	ļ	<u> </u>	<u> </u>	<b>!</b> —	<del> </del>	<del> </del>	_
		man + 61% py; folt (messerists, sericite and magnetite whisps)								<u> </u>		ļ <u>.</u>	ļ	<u> </u>					igspace			ļ	ļ		<b>├</b>	ļ	<b>├</b> —-	ļ	_
		scricile and magnetite whisps)						<u> </u>					<u> </u>			ļi							ļ	<b>├</b> ─	_	ļ		<del></del>	_
		15°CA. FW and HW ground.						ļ	ļ <u></u>															ļ ·		<del> </del> -			
UR 3	395.4	Sila Breccia: Brecciated atampo	$\vdash$	368.3	369.0	Detwerk	60%	80%	2451	368.3	369.0	20%	1.0%	10%	0	Łr.		1	0.3cm	0	-	0	-	0	=				_
		effered sectionants cut by several				( ch) + 04	50	20%																	L	<u> </u>		<u> </u>	_
		lzeue a wylam - pink atz veins	Γ		1	1 "	25.	102																l	L .	l			
		lizene gray/gray-pink at 2 veins with welldrudged petwork py-cp			-	Speanler	0.	20%		1													<u> </u>	<u> </u>				<u> </u>	_
		veinlets. Crushed network somerrous																							I			ļ	
		veinlets frushed natural appearance		369.0	370.1	network	25/50	50%	2452	3620	370.1	4%	3%	117	0	10		0	_	/	110	0	_	0		l		<u> </u>	
		but diminishes markedly in serlions	1			"		50%																					
		of zHd Lithis framents.			·	CP-PY.	100	20%		-		T																	
		of 2Hd Lithin fragments.				"		20%																П					
		367.0-3701 P. gray afectornical				Par				1																	Ĺ		
		appearance (network rountels).							]																				
		cp and py on network freedoms \$ 369.2						1																					
		-160 color similar 60° companis																										l	
		- 1cm ca/py reinlet 60° combins tetrahedrite + tr maly = sulphoset								1		<b> </b>																	_
		10017 = 34000																					I	I		L			
		370.1 - 371.5 sil-man altered		370./	371.5	CP-PY	±20°	20%	2453	320.1	371.5	1%	1%	10%	0	Er.		1	L Dem	5	<b>3</b> 7	0	-	0	<u> </u>				_
		WEll rock week notwork highwing				. "	450	50				l	<u> </u>	ļ									<b>.</b>	ļ	L				
		with tozens cpt py. Vellrock all"				"	600	300	L													<u> </u>	L		<u> </u>			ļ	_
		decresses & doubt, comprising series				Papy	20	20	I	I		I													ļ				
		371.0m - 1cm -> 0.1cm GO-PY				"	50	60	I			I													<u> </u>			<u> </u>	_
		+ Celre hodrite? inpy	Γ			"	70	20																<u> </u>	<u> </u>			ļ	
			Τ				1		1																	l		<u> </u>	
		371.5- 373.7 p.grey 9/24.		371.5	373.9	cppy	50-60	70%	2454	371.5	373.9	8%	1.5%	4%	0	10		2	5cm	/	236	0	_	1	4			J	
		network co-og semlets 25 2bore.				"	25"																						_
		CP-PY reins ~ 0.5 cm @ 50°CA				Pary	20	100	1		[																		_
		pyveins 20 20 cA (tr. cp)				War		-	<b>†</b>	1		1												I					
		Diech coding on so exposed on 40°	T			7	1	1	1	1		1											1			T			
	t	The second of the second of the	<del>  -</del>	<b>+</b>	ŧ		· · · · · · · · · · · · · · · · · · ·	<b>†</b>	t			t · ·	ł ·		+	<b></b>		·	<b></b>				t		t	t	†···-	1	•

freitures - Sold, guy black -chelcocite?

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		GEOLOGIC DESCRIPTION			:	TRUCTUR	Ε		SAMPLE	22		MINI	ERAL	2				PAK	TE.	16z-1	Py	CAR	B	Qz	-15	ASSA	27		
FROM	TO		8 89	FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	το	Ру	Сру	Kest	Cal	Coto		No. Veln	Cum thk	No. Vein	Cum	No. Veir	Cur	No. Veir	Cúm thk	ASSA Au	Cu	Ag	Мо
		3739 - 375.4 Silicom Breccia	H	373.9	575.4	Eb.	500/60	507	2455	3785	375.4	8.0	1.0	2	0	Tr		0	-	7	38	0	-	0	-		-	-	-
		Foulled Ful Zone will	1 !	5/2.7	70.7	1	70	40%		-101	7	<u> </u>		1		1		1		1		1	1	1					
		minor area questa ) Franc mainly				Pary	20	15																Ι				I	
		subangular to rounded at some				"	50	70																					$\perp$
		of which are 1 cm bifurished gtz					70	15																					
		minor gray querts) Froms mainly suborquior to rounded at 2 some of which are 1 cm bilurished at 2 man voins. Original matrix elle to chi-ser i py man & cp. Lete breceistion common by celcite veinlet				-																							
		which are leaching to form open from		-		<del>                                     </del>	ļ					-	-	<del> </del>	-	<del>                                     </del>	-		-	<del>                                     </del>	-		$\vdash$	1	<del>                                     </del>	<del> </del>		<del> </del>	_
		Late structural popular probable	1				<del> </del>			ļ——				†		-	-		_	<del> </del>	<del> </del>	<del> </del>		<del> </del>			ļ	1	
		et 374.6m where solo cavilies					<b></b>	1					<b>-</b>														Ī	1	Ī.
	*********	storme 50 /CA ( 3 storme Lozedures)																											<u> </u>
		storms 50 /CA ( 3 storms fractures)																				L	L	<u> </u>					-
		Py-cp on irregular constal freshing					<u> </u>							L	ļ			<b>_</b>	ļ	ļ			<u> </u>	ļ			ļ	<del> </del>	$\vdash$
		will dommant from 50/60° End	$\sqcup$					L		ļ		<u> </u>								-				<del> </del>				<del> </del>	-
		in all motors	$\sqcup$			-	ļ						_			_		<u> </u>			-	_	-	-			ļ	<del> </del>	$\vdash$
			$\vdash$	375.4	378.0	Pary	50	100	2379	375.4	-378.0	0. <del>1</del>	70	10	0	Zr_		0	_	6	30	0	<del>-</del>	ا_				ļ	-
		@375.6: quartz replacement	$\vdash$				<del> </del>									-			-	-	<del>                                     </del>		├──	<del> </del>	-			<del>                                     </del>	$\vdash$
		diminishes; altered fragishow	-																									· · ··	
		probable remnant phenocycls	╂╌┨				<del> </del>					-									-	$\vdash$	-	<del> </del>	-			╁──	-
	···· <del>-</del> - ··	after perphyry intrusive	<b>├</b> ┤			840			2700				 - ـ ـ	0		0.1		0	<u> </u>	3	7.	~		0				· · · · · · · · · · · · · · · · · · ·	
			╂╌┤	5 <i>78</i> .0	38/.0	Pary	50	100	2380	378.0	38/.0	0. 4	72	0	-	0.7	_	0	<del>-</del> -	-3	/3	-		۲			<del></del>	<del> </del>	
			H	201 -	70 / -	Papy	20	2.0	2381	2010	201	10	4 3	10	_	2	$\vdash$	0		1	96	0	_	-	3			·	_
			H	501.0	204.0	"474	50	50	2001	387.0	20 70	/	0.5	/2	-	0.7		-		,	1	-		<u> </u>	-				
						,	70	25				<del>                                     </del>			<b></b>	-								1				1	
						WOPY	50	100																					
			1			, , , , , , , , , , , , , , , , , , ,		,																					
			П	3840	387.0	Pary	50	30	2382	384.0	387.0	0.8	17	10	0	0.4		0	1	7	25	0	-	0	-			ļ	
						*	70	70																				ļ	_
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				387.0	390.0	Pary			2383	387.0	390.0	1.2	Tr	8	Tr	0.4		0	_	5	2/	0	_	1	/3				-
			Н			work		100											ļ	_									
			H	390. O	393.0	POPY	50	_	2384	370.0	393-0	0.5	Tr	10	0	0.2		0	_	6	20	0	-	0	_				₩
							70	35				l		l				L				1	<b>.</b> .	I				<b></b>	ļ

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			Γ						[			•		,		MIN	ERAL	IZAT	ION.		-,								
1		GEOLOGIC DESCRIPTION			:	STRUCTUR	E		SAMPL	ES		MIN	ERAL	2				<b>YFI</b>	IS	IQZ-F	<del></del>	CAR	9	Qz.	Py	ASSA	ZY		
FROM	TO		2	FROM		TYPE	TCA	%TCA	SAMPLE SAMPLE NUMBER	FROM	TO	Ру	Сру	(est	Cal	Coto		No. Veln	Cum	No. Vein	Cum	No. Vein	Cum	No. Veln	Cum	Au	Cu	Ag	Мо
368.3		(cont d) QUARTZ IRON OXIDE	T-	393.0	396.0	Pary		60	2385	5730	396.0	0.5	Tr	10	0	0.3		0	1	5	10	0	_	2	2				
		BRECCIA after PURPHYRY			1	"	70	40															Ī						
1 1			-			Wary		100	1	1		1						[									l		
						,									П												l	L	
1				3960	399.0	Pary	50	85	2386	396.0	399.0	1.3	Tr	10	Tr	0.3		0	_	6	50	0	_	0	—				
			1	7,5,5	77.00	"	70																				L		
										1		1																	<u> </u>
		* In this and the following inter-		399.0	102.0	Py	50	25	2387	377.0	102.0	2.0	0.5	10	0	ブ		4	3	9	68	0	_	/	4			ļ	
		une the late op stars asser			·	"	70	75				I .	I																<u> </u>
		to have replaced the corb.				Papy	50	65																				ļ	ļ
		51976.	$\Box$			"	70	35		1		1	T													L			
					1	WOPY	20	-																					ļ
									I																Ш		<u> </u>	<u> </u>	<u> </u>
		# probable specks of	$\Box$	302.0	405.0	Py	50	65	2388	402.0	\$45.0	1.6	0.6	7	To	0.2		3	2	7	149	0	-	/	14				ļ
		* probable specks of electrum and argentite				1,,	70	35																$oxed{oxed}$				<u> </u>	<del> </del>
		chalcolite in op appregates in				Pary	20	30				<u> </u>	<u> </u>										L					ļ	
		this interval.				/	50	55																igsqcup					↓
			П			"	70	15																igsqcut	$\square$				<del> </del>
			П			WOP	70	100				L											<u> </u>	igsqcup		L_	L		ـــــ
			Г																				<u> </u>						ļ
				\$05.0	408.0	Pary	20	50	2389	405.0	408.0	0.4	Tr	10	0	0.3		0	-	4	39	0	_	/		<u> </u>		<u></u>	<u> </u>
						"	50	50																					
					1	Wary		100		1																			
			T			,			1																				L
<b>—</b>			t⊤	408.0	411.0	POP	50	25	2390	108.0	411.0	0.6	0.3	10	Tr	0.3		0	_	4	14	0	_	/	1				
			T	7	1	Pary	70	75	f	<u> </u>	7.7																		L
			1			War	50		1			ļ	1																
			1							1		1.	$\Box$		$\vdash$														
			1	41.0	414.0	Wary	50	100	2391	41.0	414.0	0.2	7	10	Tr	0.3		0	_	0		0	_	1	2				
			1	,,,		7		1	· · · · · · · · · · · · · · · · · · ·	1																			
		84153 · 415 5 · 012 0 == 11	$t^-$	414.0	4/7.0	Pary	20	20	2392	4/4.0	417.0	5.0	1.6	10	Tr	0.2		0	1	5	77	0	_	3	20				
		filled choop; cataclasis forming	<b>†</b>		7,75	"	50	80		1,,,,,	.,,,,,	1	1.0	<u> </u>						- <del>-</del> -									
		frogreeds ranging low from	t		<b></b>	WOR		65	t · ··			1		1	· · · · · ·		1								1				<u> </u>
		to Icm & Zem ; foliation & roughly			$\vdash$	"	70	35	†						<b></b>														
		CD.	1		$\vdash$		1		<del>                                     </del>	<b>†</b>			†		1														T
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L		GEOLOGIC DESCRIPTION	1		5	STRUCTUR	Ε		SAMPLI	23		MINE	ERAL	S			X	INS RITE	10z-	PV	ICARI	B	WA	- Pu	ASSA	24		
FROM	1		8	FROM	то	TYPE	TCA	%TCA	SAMPLE SAMPLE NUMBER 2393	FROM	το	Ру	Сру	KeD+	Cal	Coro	No Ve	. Cur	No. Veir	Cum	No. Vein	Cum thk	No. Veln	Cum	J	Cu	Ag	Мо
366.3	423.4	QUARTZ IRON OXIDE BRECCIA after porphyry.	$\mathbf{I}^{-}$	417.0	\$20.0	Pary	20	30	2393	417.0	120.0	1.0	0.5	10	Tr	0.4	70	-	11	72	0	_	/	8				
		BRECCIA after porphyry.	Т			11	50	70									$\top$			Π								
		7///	1			WOP	70	100	1							1		1		1								
			$\top$			7									<b></b>		1											
			T	120.0	423.4	Py	10	100	2394	420.0	123.4	1.6	0.2	10	Tr	0.4	1,	//	10	49	0	-		4				
			Т			POR	20	10									1.											<u> </u>
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			1			Wary	50	100				<b>-</b>				11-	-1-		1	1								
		423.4 DOH	1			17											1	1	1									
1			+			<b>†</b>			<b> </b>						T		$\top$											
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			十	<b></b>					<b></b>							<del>                                     </del>	$\top$	+	1	<u> </u>								1
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## **HOLE 1218**

11981.71 NORTH

**25367 EAST** 

581.69 m ELEVATION

**LENGTH: 408.1 m** 

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			Τ					·								MIN	ERAL	IZAT	ION										
		GEOLOGIC DESCRIPTION			5	TRUCTUR	E		SAMPLE	ES		MINE	ERAL	S				PYRI	IS.	Oz-F	٧.	CARI	9			ASSA	.YS		_ ÷.
FROM	TO		8	FROM	τα	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	τα	Ру	Сру	KeD+	Cal	Coto		YEIN PYRI No. Vein	Cum thk	No. Veln	Cum	No. Vein	Cum thk	No. Vein	Cum thk	Au	Cu	Ag .	Мо
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0	3.0	Casing	-			···	·		† · ··	<del> </del> -		1			<del> </del>			-											
3.0	7.0	Aliered Sillsione: la dock green		3.0	7.1	Q(2.07	5-100	80%	2501	3.0	7:0	7.%	0.1	10%	170					13	224								
		chloritized rock. Original tolistion	╙			0 /	35.45		<b></b>	ļ		<del> </del>	↓	<b> </b>	<b>├</b>	├		<b> </b>									<b></b>		
		and cleavage are indistinct Framental	1	ļ	<u> </u>	Craduses	160	60%	<b> </b>	ļ		ļ	ļ	ļ <u>.</u>	<u></u>	ļ	<u> </u>	ļ					ļ						<del> </del>
		(bourinosi) texture of more phyllitic	L			•	450	35%	<u> </u>	ļ		<u> </u>	ļ	ļ.,	<u> </u>	<u> </u>		L					<u> </u>						-
		(loss albord) indistinct Early calcile		ļ		,	5°	5%	<b>1</b>			Ι.	l	ļ	ļ	ļ	ļ	l					ļ				ļ		-
		veins not appearant. Early at 2 scale	L						↓	<u> </u>		ļ		L	<b> </b>	<u> </u>		L					<u> </u>					<del> </del>	-
		of magn segmented by late hairling				<u> </u>			L	ļ		<u> </u>	<u> </u>	ļ	ļ	<u> </u>	ļ	ļ		L.,			ļ						
		fractures, 9.0 m - 1 cm reverse dyphosom	<u>Ł</u>				<u> </u>		ļ		ļ	<u> </u>	<u> </u>	<u> </u>	<u> </u>	ļ			L										-
		of asen glav 25 /CA by I trusture			<u></u>			L	<u> </u>			<u> </u>		<b></b> .	<u> </u>	<u> </u>	<u> </u>						<u> </u>				<b></b>		-
		at 30°CA. Magnetite 7 pg > bist in							<u> </u>	ļ	· .	1	<u> </u>		<u> </u>	L	L						<b> </b>				<b></b> -	<del> </del>	
		rock. 5= in veine 6 3% (py, loca). Magni	·L			I		<u> </u>	<u> </u>		ļ	<u> </u>	<u> </u>	<u> </u>	ļ	<u> </u>	ļ			L								ļ	-
		Price concentrated along yein							<u> </u>	L		<u> </u>		<u> </u>	L	<u> </u>	L	ļ										ــــ	
		boundaries and within wallrook. Prominat branite on broken cure	L	l		<u> </u>	<u> </u>	<u> </u>	<u></u>			ļ	1	<u> </u>	ļ	l	ļ	<b> </b>										ļ	
[			L				<u> </u>		<u> </u>	l		<u> </u>	<u> </u>			FI		<u> </u>										<b>├</b>	-
7.0	10.0	As Above Cp gone, the concented along roin margins, 7.1-8.7	L	8.7	8.75	Fanit Glaipyt Common	300		2502	7.0	10.0	490	0.1	3%	1170	4%	ļ	<u> </u>		22	/.2m								
Ĺ		along roin margins, 7.1-8.7		7.1	10.0	CO. MAAN	450	60	<u></u>	<u> </u>				↓	<u> </u>	<u> </u>	<u> </u>	L_			L							<del> </del>	<del> </del>
		prosoningly yle vein 80% oftologt	•	ĺ	<u> </u>	"	25°	30	<u> </u>	1		I	1	l	<u> </u>			ļ					ļ					ļ	ļ.,
			T									<u> </u>		<u> </u>		1	_		$ldsymbol{ldsymbol{ldsymbol{eta}}}$		L		L		]			<u> </u>	<u> </u>
			Т											I	1	Fe	<u> </u>		Ĺ				<u> </u>			<b></b>		ļ <u> </u>	<u> </u>
10.0	14.1	Maraly gla vein -HW 30'CA (10.3m)	Т	100	12.1	Py-Co-chi	10-10	70	2503	10.0	12.1	5%	0.79	32	417.	2%													<u> </u>
	1	Py-Col-magnetit concentrated al vein	Τ			11	5-10	30									Ī.,						L					$oxed{oxed}$	
		and horst margine assec with chlorite	1	ļ		1	1			1			Ī		1								L					<u> </u>	<u></u>
		Interior of horses replaced with 20% magn.	1			1				1		Г																	_
<b></b>	<del>                                     </del>	Pr+Cp also on a set of veinlets love	<b>3</b>	12.1	10.2	GIZPY "	60-70	50	2504	12.1	14.2	12.	tr	3%	170	41%				40	95cm								
	1	within als veinwill co concontrated	7			1	5-10	25'		1		1																<u> </u>	
	1	at veinlet intersediene. These					35-40	25				1	1		T														L
		Crosscut horsts chlorite-magnetile	T			Py-chl	60	100		1.				1				2	Icm									ļ	
<b></b>			Τ	1	1	1-		1		T		1	1											ah 🗪					$\perp$
14.2		Altered Sillston: by dark, fragmet	1	14.2	16.2	Ot + mign	5-150	60	2505	14.2	16.2	1%	6	5%	170	41%								40	Cam				_
	T	In quartz = magn veins at 15.6	T		Γ	"	450	10		1												L							_
		by quartz = magn veins. at 156 wall rock 60% magnifile	Τ			(ale:50.p	60		T	1		T	T																
<b></b>	1	-	1	<u> </u>	† — —	(46.80.P	70°	30	1			1		1	1		T	Π				15	Icm						
	1		+	<del> </del>	<b>†</b>	- VP	†	1	1	1		1	1	1	1	1						Ī							
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	- 1	GEOLOGIC DESCRIPTION	l		5	TRUCTURE	Ε		SAMPLI	23		MIN	ERAL	2.				<b>AAK</b>	JE 10	ž-P	y [C/	ARI				ASSA	YS		-• -
FROM	រប		8	FROM	TD	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	ΤO	Ру	Сру	Ke0t	Cal	Coto		No. Vein	Cum !	Vo. Zeln	y C/ Cum N thk V	o. ein	Cum	No. Veln	Cum thk	Au	Cu	Ag	Mc
			П																		01	• (		CH ?	- Maga		<u> </u>		$\perp$
16.7	12.2	Altered Sillstone dark gray green; chl/b. 1500 + hornfelsic; criginal fabric oblibrated; Cal by Ota: magn. Vs -pt 10 cm. thomas Ota: cakite chlorite rains followed		16.2	12.2	GH3= Magn.	15-8	65°	2506	16.2	12.2	1%	t.	5%							$\perp \Gamma$	$\Box$		38	76cm				1
		chl/biser+ hornfelsic				4	45.7	10	I																				1
		creamed taken abliterated and bu				,	60-75	25																					
		Olz: man is note 10 (45°) thence	1	1		,				1		T		1	Ī														$\perp$
		Discopile chlorite soin fillowed	✝			of cake.	60'	100				Π		1	Τ							5	8cm					<u> </u>	1_
		by a nedwork of barrier Price cash whi	1-	1		PYSCP CH COLL	10'		1				1	1	1					$\top$							L		$\perp$
		veine Months conventrated alma	1				40°		1	1		Г			1														
		well have former leave ment of hell mil	ļ	<u> </u>		1	850	†		1	i .	1	1	1	1				T										
		and realization hands from some int	1	-					1	1				$\Box$						T							<u> </u>	<u>L</u>	
		veine Magnific concombrated along wall boundaries (represented host ports or preplacing horses from rims into chlorite core.	t-			†	<del> </del> -	<b>†</b>	t	<b>†</b>	† ·- · · · ·	1	1	1	T-														
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19.2			╂╌			an may	0.00	-	12501	12.2	7.7	14/8	1	12/	4	+	_	$\vdash$	-+		<del>-   '</del>	$\dashv$		77	~~				$\top$
			╂─	17.2	21.4	<del>                                     </del>	15"	30		<del> </del>	<del> </del>	<del> </del> -	<del> </del>	<del> </del>		<del> </del>	-	$\vdash$	-		_	$\dashv$						<b>†</b>	1
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21.4	<b> </b>	as above with more inlense	<b>↓</b> _	121.4	24.1	precialed	ļ	<del> </del>	2508	21.4	24.1	1370	150	57		<del></del>		,	UIM					.50	<u> </u>		-	<del> </del>	
		brecciation of 1-2 cm glz maynihl	╄	↓	<u> </u>	<b></b>	<del> </del>	<del> </del>	<b> </b>		ļ	₩.	ļ	┼	┼	-	<u> </u>	<u> </u>				$\dashv$	<b>  </b>				<del>                                     </del>	+	+-
	ļ	bresciation of 1-2 cm glz manihl veins (70% briscielal), attitudes of segments girmlen to room.	┺	ļ	<u> </u>	<del> </del>	↓	<del> </del>	<b>↓</b>		ļ	<del> </del>	<b>↓</b>	╁	<del> </del>	<b>-</b>	ļ		$\vdash$							├─-		+-	+
		segments similar to room.	┖	<u> </u>		ļ	<u> </u>	ļ	ļ		ļ	↓	ـــــ		↓	-	ļ	<u> </u>	-						$\vdash$			┼─	+-
		Nedwork of hairline my cp chl veins	L		<u> </u>		<u> </u>	<u> </u>	<u> </u>	ļ	ļ	ļ	J	- L	ļ		ļ	_				/	L					<del> </del>	+-
		Nedwork of hairline of up chi seins	L										↓	ļ	↓	-	<u> </u>						<b> </b>			<u> </u>		<del></del>	+
		Some atz fra rounted.  Ott seinin, intensifies generally  40 - 45 CA;	_		<u> </u>		<u> </u>	1	<u> </u>			ļ		ļ	1	1	<u> </u>						L		ļ		ļ	<del> </del>	
241		Qtz remin intensifies conseelly		24,1	25.6	PyCP	100	75	2509	24.1	25.6	5%	0.2%	99	úL			5	1000				$\sqcup \sqcup$	6	(Down	<u> </u>	—		-
		(10 -45°CA)				PYCP	60	25		<u> </u>		<b>.</b>	J				L	<u> </u>							ļ		ļ		
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		GEOLOGIC DESCRIPTION	1		,	יםוורדוום	-		SAMPL			LINI	FDAI	2				YĒİ	کا	n	5:7	יר גם ז	5			ASSA	YS		
FROM	70		· •	I COUNT	TD.	TYPE	TCA	ZTCA	SAMPLE	CODM	1 70	D	Con	<b>i</b> ~+	ادما	1 0		YEIN PYRI No. Vein	Cue	WZ-I	Y	No	C	No	Cum	Δ.,	Cu	Ag	Мо
r Kum	-		1	FRUM	טי	1172	ICA	%1CM	NUMBER	FRUM	10	ry	СРУ	(e)	Cat	CoC		Veln	thk	Vein	thk	Vein	thk	Vein	thk	nu	Cu	79	1,
		Altered Broccia , Silva +?	Т																										
25.6	29.3	Tolone a Chiciliation: at laine	T	25.4		PYCP	60-90	30	25/0	25.6	28.3	#7.	0.7	72		1%													$\top$
2.0	<u> </u>	and citization of wall and	T	100.4		<u> </u>	50-60	50	~	27.0	70.0	1.70	-	1.74															1
		Il de la la constant de la constant	1				5-15	20		<del> </del>												-		_					
		Harris alspire progression replacement	$\top$	1					<b></b>			<b>-</b>				<del>  </del>												<del> </del>	1
		ent silvetication of will rock.  Hards display progressive replacements by magnetite which reflect pringed teclure of determined sillstones.  Nelwork of printe-cp hardine	┢					<del></del>	<b></b>	<u> </u>					$\vdash$	<del>                                     </del>								$\vdash$					+
		teriore of deform a sulfstands	+-													<del>   </del>													1
		Nelwork of MINTE-CP handline	╀	-		<del> </del>			<del> </del>			-		$\vdash$	-	<del>  </del>		-		-									+
+		reinless cross cut glamas veins	<del> </del>	<del> </del>				<u></u>	<b>.</b>																-+			···-	-
<del></del> ∔		and silice / meanition replaced horses	┼-						ļ						<u> </u>	<del>                                     </del>				_		_		-				-	+-
		Printe-cp veinless 0.1-0.5 cm with	1											$\square$		ļļ													+
		przins generalle, 62mm Cpis patchy on reintals, other to 0.5cm	┺			L			<b></b> _			L	<u> </u>												$\dashv$		· · ·		+-
		patchy on veinles, often to 0.5cm	L										ļ			$\sqcup$													+
		Lite krzetures at 85 , 15" limonite	L								<u>.</u>					$\Box$													
		costed = adjacant cartonate legal	1																										
		Pink mineral (corbonale? - radocosite)																											
		1-2 greins in late gla at 30°	Т				,		·																				
		2mf 80°	T						2511	28.3	21.A	2%	0.5	12		1%												Ī	
			Т						7711	FB1.2	2,1-7		-	/															T
20.2	21.4	Ac , how	†	1																									
	34.7	- late glz-cak - ser veinlets 1-2 mm	╁╌	-		<del>                                     </del>							<del>                                     </del>	-		$\vdash$	$\neg$			$\vdash$								1	1
		- Tare gra-care - Ser Demiers J-Lmm	╀╌	<del> </del>			<del> </del>	<del>                                     </del>	25-12	3//	2.1.0	.7	. =	1-7		1%	-	-		-		$\vdash$			_			<del>                                     </del>	+
		accor on earlier py-cp network voilets pradominantly at 80.85 CA 20.62 x 3cm lets ball gla viet ASKS CA MI.	╁╴	$\vdash$			<del> </del>	<del></del>	Y2 17	21.4	34.5	2/4	0.3	2 /0	-	/ /*		$\vdash$			$\vdash$		Н						+
		vonlets predominantly at 80.85 (1)	╀	<del></del>		<del></del>		<del></del> -								├─┤													
		29.62 x 3cm late ball at 4 wat ASKS CA. MI.	╀			<del> </del>			ļ			-				$\vdash$				_								<del> </del>	+
		This in turn cut by late freque	<b></b> .	ļ																									- 1
		(weder course) at 035°-lm, mal	Ļ.	1		ļ			<b></b>			<u> </u>				$\sqcup$		-											+
			1_						L									Ш									<b>-</b>		
			L						Ĺ		<u> </u>									L									↓_
31.4	37.5	As above - characterized by angular		34.5	37.5	Ayer	60	800	25/3	345	37.5	3%	0.5	3%		1%		7	7cm						1		·		
		As about - characterised by angular to subnounced agrey silicions from in a matrix of servite-calcile-pit se, magn) with a 35°CA alignment. By-cp network veins later most oflar lie within matrix but also crosscul silicous fragments.	Γ			Lota ata	50'	100			<del></del> -																		
		in a materia of Secrete calcileralt	$\top$																										T
		ce mass with a 35°CA aliment	1-				<u> </u>						T			11												Ī	T
		Proce solvent daine later and alle				1		<b></b>	t		<u> </u>														$\neg$				T
		lie will in male in his also	+	1		<del> </del> -	<b></b>													<b></b>	_							İ	1
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		SUICORES Et 23 monts.	+-	<del> </del>		<del> </del>			·			. 1			_												· · - · · · -		+
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l .		GEULUGIC DESCRIPTION	<u>.</u>			TRUCTUR	E		SAMPLI	E <b>S</b>	_	MIN	RAL	S			h	À L'HU	JE	Qz-	y	<b>ICAR</b>	B	1		AZSA	YS		- <b>.</b> -
FROM	TO		18,	FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Ру	Сру	e0+	Cal	200		No.	Cum	No.	Cum	No.	Cur	No.	Cum	AZZA uA	Cu	Ag	Мо
			189				<del> </del>	-	NUMBER	<del> </del>	├─	-		<del>\</del>		<del>  C</del>	-	Vein	The	∨ ein	thk	Veir	THE	O/2	THE			<del> </del>	+
37.5	110 -	Silical Breezes Ol I A	╁╴	20.5	40.0	Ri-Ca	100	100	21-11	20.5	40.0	0.00	207	107	,	41%	-	A	50	_		<del>                                     </del>	1	978	8m			<u> </u>	+
3,3	74. 2	I deli de su la sericite	<del>†-</del> -	3/.2	70.5	","	45	337	2514	3.7.5	70.3	1.70	476	10.70	1	516		#-	JUCA	٠	2364	4	f	+ 4	0.04			<del> </del>	1-
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		of the structurally deformed sills tones and early seining ie parallel benfing and breciation	T														$\neg$												
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		The network of py op veinlets  15 weakly developed Later  15 some dislocation and rotation  of Fregs. This freetway provided  chemnelways for later carbonst.									·	1																	
		les chains caused Rusther brecedin	厂																										
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		Superimposed on Py-Cp vainlets	$\vdash$			<u> </u>		1	1															-					
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		les I les d' sur con	+-									1				$\vdash$	-					_	<del> </del>						<u> </u>
		branding generally constant from frag to frag at 5-10°CA Occassional late a sem guarde	+-			<del> </del>	<u> </u>	<u> </u>		<del>                                     </del>	-	1			<del>                                     </del>			$\dashv$						1					
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		Vein Culs 211 veins and teatures - 05°CA. 38.4 Conjugate 510 000-Py	1					$\vdash$									$\neg$												
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405	43.6	As shore; with incresse in	<b>†</b>	405	43 (	P4.60	456	,	2515	405	43.6	4%	0.8	6%		1%		3	Scan					17	Ben				
		lale barren gtz veins 0.5 - 20cm	1	-7 7		alers	25	4%		1		[ '-' ']			ļ														
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		GEOLOGIC DESCRIPTION	l		:	STRUCTUR	E		SAMPL	ES		MIN	ERAL	S				ΡΥR	TE	Qz-F	У	CARI	7			ASSA	1YS		
FROM	TO		Š	FROM	מז	STRUCTUR TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	ŤΠ	Ру	Сру	KeD+	Cal	Coto		No. Vein	Cum thk	No. Veln	Cum thk	No. Vein	Cum thk	No. Veln	Cum thk	ASSA	Cu	Ag	M
			Ц			<u> </u>						<u> </u>	<u> </u>		<u> </u>				L					104		<u> </u>	<b>↓</b>	ļ	$\perp$
43.6	46.6	Silicitied Breceis - es etons.		43.6	46.6	network	450	40	25/6	43.6	46.6	37.	0.5	7%		3%		2	ICM					13	Sem		ļ	ļ	-
		magnetite distribution defines					300	40	ļ	<u> </u>					<u> </u>				<u> </u>	ļ	$\sqcup$					<u> </u>		↓	+
		relie fragments. Nelvok py-cp				<b></b>	100		<u></u>			<b> </b>							ļ								ļ	ļ	4
		voialets bensist cut by coop - at - ser				PY-CP.	65.00	100																					$\perp$
		relie fragments Nelwork py-cp verselets person cul by cook-ghaser network verselets of 50° But 15°				Life 912													L										-
		- 12he at 2 - milky white barren					50°	30%					L														<u> </u>	<u> </u>	╀
		,					40	25%																				ļ	$\perp$
							150	25%																	·				$\perp$
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			П							1																			$\perp$
46.6	42.7	As above: energie in no. 2mp	П	46.6	41.7	Py-CP	80	35-0	25/7	46.6	457	6%	0.5%	7%	ر-	3%		16	15cm	2	5600			2/	170				
		size of minh veries - later than	П			•	60	40		F1, R3_R_		1		-															$\Gamma$
		size of pyinh veries - Istor than perpasion silveticition - Pyter uplo gen - occasional pint carponate ni-amon				"	45		1															$\neg$					T
		- accessional pint cartonate alana	4	, .		Let. ata	15.0	10%	1	1			-			1			$\vdash$										1-
		- Glz-py veins more distinct	$\Box$					65%	<del>                                     </del>	<b>†</b>					<b>†</b>														T
		- Immonitatie (Fe coob?) rim on many	I			<b>†</b>	60	10%	t	<b>†</b>					<b></b>														1
		excite and Form reinlets and				ah ey		30%	T																				
		grain aggregation. As store			<b></b>	10.17	60.	30%	1	†		·																	1
		an account or half minute comme				<b>†</b>	80'	40%	<u> </u>																				T
		disserved in ellered little freque																											$\perp$
		anderblebs and seems within					ļ							L_											_		<del></del>	↓	╁
		pyrite veins	Ш																				$\rightarrow$				L	<u> </u>	┸
		, ,																						1	l				1_
49.7	52.7	Pytop vains up to som		49.7	52.7	Py vains	450	85	2518	49.7	52.7	4%	047	8%		2%		6	(3cm					13	Sea				
		30.5 Comjugate icm py veins 65/30					30 '	15%																				l	⊥.
		Net work on reinlete loss interes. 1				Late Oft	40"	10 %																	I				
		60° pr deina der massive and					50°	20%									-												T
		wider then 30 veins forcessive	$\Box$			Gel-glase			1			<b></b>															1		T
		Silicification = seriale persons	$\vdash$			are disease	NT-50	40%	<b>†</b>				-																T
		Wetwork of calcogiz ser seinles	t⊤t			<del>                                     </del>	1,,,,,	100.0	<del> </del>																			·	1
		persists we could appear once.	H			<u> </u>	<u> </u>	<b>†</b>	<del>                                     </del>	<b> </b>								-											1
		50.5' Conjuged set of bete Proclures			<del>                                     </del>	1	<del>                                     </del>	<del> </del>	<b></b>									-											1
		-lim - 55 /35"	H			<del>                                     </del>	<del>                                     </del>	<del> </del>	<del>                                     </del>			-			-				$\vdash$			+							
		-m - va /33	┥			<del> </del>	<del> </del>	<del> </del>	<del> </del>	1		ı ı	ł.		'														

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		GEULOGIC DESCRIPTION	L			STRUCTUR	E		SAMPLE	2		MIN	RAL	S				PYR	JE.	Qz-	<b>3</b> у	CAR	B	Ι		ASSA	ZYS		
FROM	70			FROM	TO	TYPE	TÇA	%TCA	SAMPLE NUMBER	FROM	מז	Ру	Сру	Kept	Cal	Coto		No. Vein	Cum	No. Vein	Cum	No. Vein	Cur	No. Vein	Cum	ASSA Au	Cu	Ag	Мо
																								Lot	atz				
52.7	55.8	Silveihi Breceie 25 1bone.						ļ	2519	52.7	55.8	3%	0.3%	8%		2%								7	700	Ī			
		seem majoration bondomy of 55°CA - majoratile bearing little pelies	<del> </del>		├	<u> </u>		ļ				<b> </b>			ļ	-		ļ					<del> </del>	<del> </del>		<u> </u>	ļ	<u> </u>	-
		- mesnetile bearing little relies	ļ		-	ļ	-						ļ		-				<u>.                                    </u>	<u> </u>			<del> </del>	<del> </del> -	ļ	<b> </b>	<del> </del> -	<del> </del>	<del></del>
		comprise 80% & core, romainder	╀			ļ	ļ	-	ļ			ļ		-						-		<del> </del>	├			-	<del> </del>	<del> </del>	+
-		gla salphid, gta magnetith and pervession silicitization which has	├		<del> </del>	ļ	ļ	·	ļ				ļ <u>.</u>								_					<b></b> -	<del> </del> -	ļ	
		pervession silicitiestion which has	├-		-		<del> </del>	<del> </del> -	ļ			<b> </b>		_	_									-	-	<del></del>		<del> </del>	+
		in pert replaced lithic freqs 25	ļ		ļ:		ļ	ļ	<b>.</b>														ļ	ļ				ł	
		en alteration envelope round	┞			ļ	<del> </del>		<b></b>			ļ		ļ					-			_	<del>                                     </del>					├	+
	ļ	gray gla chammoloways Py cp network win lets intensity and wider	ļ		<u> </u>	<del></del>	↓	ļ												<u> </u>								ļ	<del> </del> -
		reinlots intensity and widen	⊢		<u> </u>	<u> </u>	ļ								ļ														-
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		by segmental gray at 2 vains at 45 1/25° ~ 27. as non fazzy white grows chambic section - plageolese?	├-		<del>                                     </del>	ļ		<u> </u>				<b>-</b>																	-
		45725 ~ 27 asnim Fazzy	-		-	ļ	ļ											i							-				+-
		while grains, chambic section - plagiacize!	⊢		├	1.2292						<b> </b>												_					┼—
		Cl. 1: 1 2	-				1	<u> </u>							-			-						<u> </u>					
55.8	50.4	Silicitian Breizie	-	55.8	58.4	ļ	40	50	2520	55. <b>8</b>	584	2%	0,3	10%		2%						<u>-</u>		7	SSem				-
		Memorile bolish al 55°CA	<b> </b>	<u></u>	ļ			50																<u> </u>					
		Magnetite occurs not only as diss."  and o 3 mm sub posselled binds in				Lete heets						-		$\rightarrow$		$\rightarrow$												<u> </u>	├
		and o. 3 mm sub parallel diands in				him	40	35%																					<del> </del>
		selic lithin fregs but as complete	_				250	652																					<del> </del>
		replacement of fress and as laker			L		<u> </u>																		_				<del> </del>
		Semi m 2950 0.5 - 2.0 (m yeins:				<u> </u>												$\Box$											<u> </u>
504	01.3	Salvertial Breceix.		58.4	61.3	Py-CP	60-70	40%	2521	584	61.3	4%	0.4	5%		?		6	llan										
		59.35 - 20 cm pt2 - 04 co vein					85-90	10%																					l
		59.35 - 20 cm ata-py co vein implaced in finely breceived Silicitist pack (frzgs roundat-1 cm)										1													· · · · I			.,,,, ,,	[
		silicition out (frage counted - 1 cm)		59.1	610	Firefors	15.	35																					
	Цω	Sami massive on rite nalesia mana	1	V-1:1	21.12	(mjugate)	45.	65									$\neg$	$\neg$	-										
		Somi massive pyrite replacing magnet 10cm with at 10°CA. At 60.7 - 2 cm	1		<b>—</b>	1	73	7				<del></del>				-	-												
		Sanimaria Ou at SO.CA (EU)			<b></b>			<b></b>																					-
		saminogin py at 90°CA (FW) Lete hazelving at 15° and 45°	H														-												_
		represented zone establishing	$\vdash$		<u> </u>																								ļ
		TESTELLIZIONE ZONE ESTENISMO Z	$\vdash$		-									-+			$\dashv$	-		-					-				-
		wedercourse which is leaching			1			1					- 1	- 1		- 1	- 1	- 1	- 1	- 1	- 1								1

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		GEULAGIC DESCRIPTION			5	TRUCTUR	Ε		SAMPLI	<b>2</b> 3		MINE	RAL	\$				KAK!	YE.	Qz-F	y.	CAR:	В	1		AZZA	YS		
FROM	το	_	200	FROM	TO	TYPE	TCA	%TCA	SAMPLE	FROM	10	Ру	Сру	Kest.	Cal	Coro		No. Veln	Cum	No. Velo	Cum	No. Vein	Cur	No. Veln	Cum	AZZA .uA	Cu	Ag	Мо
		* Carbonofes.						<u> </u>			<u> </u>				<u> </u>				****										
		stong py-co notwork , was beened stone of the stone of th	1								1	1		<b></b> -	1	T			<u> </u>										
	<u> </u>	Blong price notwork son freing	s				1	1			T			1		Ī.							Ī						$\coprod$
		through to him secondarting																										<u> </u>	
		breceiz texture limenite on																										<u> </u>	
		all late foretures and rugs.  Fraction octoring approves  i. be post lategla vains  0.5cm cp somiet of 20°CA					L											I						<u></u>			<u></u>		
		Fraction achorning appears																					<u> </u>	<u> </u>		L		ļ	
		1. be post 12te at 2 Voins	ļ					1			ļ												ļ <i>.</i>	J					
		0.5cm cp semlet of 20°CA	$\perp$	ļ	ļ	<u> </u>		<u> </u>	L	<u> </u>	<b>↓</b>	<b> </b>		ļ	ļ	↓	ļ	ļ	ļ	ļ			<u> </u>	ļ	$\sqcup$			├	+-
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	(0.1		╂┈			mg 76/2	24-	-	0,50	//2		207		17		170		7	2					├				<del> </del>	╁
<i>G</i> 1.3 .	67.	Sil Bx hithe fires some cal by	-	627	_	101	30'		2522 2523	61.5	65.4	30	2.5	107	<del>                                     </del>	18		9	Zen Zen					<del> </del>			ļ	<del> </del>	╁─
		magnetite Wishick Ser. Beforend	╢			<del>                                     </del>	ļ	<del> </del>	2524	63.4	105.1	13	0.1	10	1-	1/ 4/3 1/ 5/		<del>-</del>	10cm				-	<del> </del>				<del> </del>	+
	ļ	verns treased + there is the free	╁			<del> </del>			1277	1.00	68.2	46	0.5	10.70	کـــــا	<del>"</del>		5	(vem				ļ	ļ					<del> </del>
		vans transed 7 (Him I) in free	+		-				<del>                                     </del>	-	<del> </del>	-		-	-	-							╁	-				<del> </del>	+
	ļ	Granglamer 45 /3000 cul by Span all very co ser Asca End Besociated all ser alberation	╁			ļ					<del> </del>				<del> </del>	-		$\vdash$					<del> </del>	<del> </del>				<del> </del>	-
		Gray 9114 - By Co ser AS CA End	╁					<del> </del>		<del> </del>		1			-	<del> </del>		$\vdash$					-	<del> </del>				<del> </del>	+
	ļ	2550cized glz ser 21terzhon	+		-		<del> </del>	-	ļ	<del> </del>		1			<del> </del>			<del> </del>					<del> </del>						
		onvelope (pervessive). Dissemine tel	╁		<u> </u>			<del> </del>			<del> </del>				├									<u> </u>					<del>                                     </del>
	<b></b>	op. py (KO17) man be associated with the allertion stage.  This in turn cut by py constant at a stage cach at ser 4505° CA. Ry CR of this stage man property and stage of the	1-	ļ <u>.</u>	<del> </del>	<del> </del>		<del> </del>	}		<del> </del>			-															$\dagger$
		T/ 1 1 mg/ 1	╁		-			-		<del> </del>					<del> </del>								<del> </del>						$\vdash$
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		ha, papier explien magnetic, trails	4		<del> </del>	<del> </del>	<del> </del>	<del> </del>	<del></del>		<del> </del>	l		ļ	<del> </del>														
		also displaces graffind stav. Smiles man and si's 45°	+		<del>                                     </del>	<b></b>		<del>                                     </del>	<b></b>	-	<del>                                     </del>	$\vdash$		<del> </del>							-		-	<del>                                     </del>					<del> </del>
		MSn : 47 CA Veins (1951 A1 25 195	1		·	<del> </del>	<del> </del>	<del> </del> -				1	· ,																
	-		f				<del> </del>	<del>                                     </del>	<del> </del>	<del> </del>	<u> </u>				<del>                                     </del>									Bx C	<u>/</u>			·	<del> </del>
191	728	Bre Quirty Vein	+	161	7/ 10	Pyce	200	ROU	2525	633	710	52	0.87	20%	<del> </del>	17%.		12	12cm						200				1
191.1	0.0	1.2 mark 25 to 200	1	<i>"</i>	711.0	7.7	25.20	20%	2525 2526	71.0	74.1	27	1.59	5%		15%		22	4500										
	<del>                                     </del>	committed in Purch and calife	1		<del>                                     </del>	t	l		ŀ	1	†*****	' <sup>2</sup>	* : <1D		t —	1		^	,										1
	<b></b> -	trayments 0.5 to 2.0 cm comontal in Py co and calcite	.1	71.0	74.1	Ouca	15-30	102	<b>1</b>	1																			
	<b></b>	CP OCCUIS 25 0.2 to 05 om blebs	⇈	11.0	<del></del>	Pyrp Cokeyco	05-12	709.	† <u>-</u> -	ļ																			1
		and elissoniastal in some massion py band	1	<b></b>	<b>†</b>	N. P. C.	450	300	<b>†</b>	<b></b>									$\neg$										<u> </u>
	<del>!</del>	Allson 142 and 11. Some and 22. Del Dans	<u> </u>			<u> </u>	7.2	†**/ <u>-</u>	t	ł	t																		<u> </u>

																					<u> </u>		<b>.</b>			1 7.1		٠.٠٠	
									1			1					ERAL	IZAT Nen	IDN_					٠	1				
		GEULOGIC DESCRIPTION	Ĺ.		S	TRUCTURE	Ε		SAMPLI	ES		MINI	ERAL	\$				PAK	TE.	Oz-P	y [	CARE				AZZA	YS		
FROM	TO		Š,	FROM	TO	TYPE	TCA	%TCA	SAMPLE SAMPLE NUMBER	FROM	מז	Ру	Сру	K . ST	Cal	Coto		No. Velo	Cum	No. Vein	Cum	No. Veln	Cum N	lo. I	Cum	Au	Cu	Ag	Mo
																						$\Box$	$\Box$	$\rightrightarrows$	$\Box$				$\sqsubset$
		Style often filling spaces to 0.50							L	74.1	77.1	L	ļ	1	<u> </u>	<u> </u>	ļ	<u> </u>							<b>.</b>		•		ļ.
		at in ter section			•							<u> </u>												$\rightarrow$				↓	↓_
		72.1-20cm Somi 10735/146 PM								/		l	<u> </u>	<u> </u>		<u> </u>		<u> </u>					$\bot$	$\bot$				ļ	$oldsymbol{\perp}$
		w the co cover letal or								V			I															Ь	_
		Style often filling spaces to 0.5 c at intersection.  72.1 - 20 cm some intesting pro- with a concentration from most boundaries (most of property).  The second of the fire of the second of the s										ļ												$\dashv$	_		<b></b>	<del> </del>	<b>↓</b> _
		72.3. 3cm /2k /imanin.							<u> </u>			<u> </u>				L		<u> </u>					$\rightarrow$	<del></del>				<del></del>	╁-
		917 v. 20°CA							<u> </u>				<u> </u>	<u> </u>	<u> </u>			<u>!</u>							$\dashv$			ļ	↓_
		1 '						<u> </u>	<u> </u>			<u> </u>	<u> </u>					L					$\rightarrow$	_	$\dashv$		<u> </u>	<del> </del>	ــــ
74.1	77.1	Silve Bx marked increase in												L_	<u> </u>	<u> </u>	<u> </u>								_1				ļ
		Feron including 90 replaced lithin							2527	74.1	77.1	190	1/2	9%		41%		6	4cm	2	30							↓	ــــــــــــــــــــــــــــــــــــــ
		Pross, Magnetit banking more													<u> </u>		<u> </u>	<u> </u>	<u> </u>										-
		Silve Bx marked increase in Fe on including go replaced lithin from ss. Magnetith banking more preparented - Subpressed (0) (5-15°) when larger transpossure										<u> </u>			L.								$\dashv$	_	_		L	<del> </del>	$\perp$
		when large trass occur.	L						<u> </u>			<u> </u>	<u> </u>	<b> </b>	<u> </u>	L	ļ	<u> </u>						.	4				ļ
	L		L				<u> </u>					<u> </u>	<u> </u>		<u> </u>	L	ļ	<u> </u>						_			<u> </u>	<del>  </del>	╁
	ļ	GHR mayn = on up to 2cm 6 45°CA	L				L		<u> </u>	<b></b>		<u> </u>	<u> </u>		ļ	ļ	ļ						$\rightarrow$				L	<b></b> -	1_
		- zapears to be conduit for part-	L						<u> </u>	<u>.</u>		<u> </u>	<u> </u>	L	<u> </u>		<u> </u>	<u> </u>		$\sqcup$				$\rightarrow$	_		<u> </u>	<del>  </del>	↓_
	l	souls elbertion magnitude							<u> </u>			L	<u> </u>	L	<u> </u>	ļ	<u>L</u>		L								L	ļ	ļ
		on lithreless, and replacement						<u> </u>	<u> </u>			L	<u> </u>		<u> </u>	L	$ldsymbol{f eta}$	<u> </u>					<del></del> -				<u> </u>	↓	╀
		CHR magn - on up to 2cm 6 45 CA - 2 peros to be conduit for port- sould ellergher in 2 person and brinds with frags. Verns are bidnished gonerally in come some magn 200 at 200 at 100 magn massing at 50° a 70° GHZ 1 py magn End py co voin less 12 ter (± 45° in glz)	L					ļ	<u> </u>			<u> </u>	<u> </u>	ļ	<u> </u>		<u> </u>	ļ					$\dashv$		_			<del> </del>	↓_
		bifries of generally in come your							<u> </u>			<u> </u>	<u> </u>	<u> </u>	<u> </u>		L.,	<u> </u>					$\rightarrow$		_		<u> </u>	<del> </del>	╀
		magn >py Rock or man marins						<u> </u>	<u> </u>			<u> </u>	<u> </u>	ļ	<u> </u>	ļ	ļ	<u> </u>					$\rightarrow$	$\dashv$	_				╀
		at 500 m 700 Q+2 + py , mgn End	乚					<u> </u>	<u> </u>			<u> </u>	<u> </u>	<u> </u>	<u> </u>		ļ	<u> </u>				<b></b> Ì		<del> -</del>	_		<b></b>	<b>↓</b> —	╀
	l <u>.</u>	py cp vointele 12 ter (= 45 in alza)	L_					<u> </u>	<u> </u>			ļ	<u> </u>	<u> </u>		ļ	<u> </u>	<u> </u>										ļ	<b>∤</b> –
			_					ļ	ļ			<u> </u>	<u> </u>	ļ	<u> </u>		<u> </u>		ļ					$\dashv$			<del></del>	—	╀
	ļ	Note: Im rind on Mgn> PY>CP	\$15						<u> </u>			ļ	<u> </u>	ļ	<u> </u>		<u> </u>	<b>12</b>										<del> </del>	↓_
22.1	802	As Almas neglesche pyco Network vein:	là	85		My RI		Ί	2528	27.1	827	0.5%	tr	10 %	-	1%	ļ	<u> </u>	0.5	2	14 cm		$\rightarrow$					——	╁
	<u> </u>	Network vein:	<u> </u>	11		,	65	<u> </u>	<u> </u>			<u> </u>	↓	<u> </u>	<u> </u>		ļ	ļ	ļ					_				<u></u>	<del> </del> _
		Celi t py, mgn. ± 15°, 45°, 85°	<u> </u>	45			85 0	<u> </u>	ļ			1	<u> </u>		<u> </u>	<u> </u>		<u> </u>	ļ					$\perp \!\!\! \perp$				—	↓_
		Remork value:  Cyli top, man t 15° 45° 85°  Formac Pis; 1 , 35° Feedure in  Spec 1-1. ferri.  Men ) by in wantels  Tam & 3cm Massin man vain gramped  and by lek so glav. WK nelwork us	_		·		<b></b>	ļ	<b> </b>	ļ		ļ	ļ	ļ	<b> </b>	<u> </u>		<u> </u>	<u> </u>						_			ļ	<del> </del>
		Spec 1-te frais.	<u></u>					<u> </u>				L	<u> </u>	<u> </u>	<u> </u>	L		,	٠,,,	$\sqcup$			$-\!$	$\dashv$	_			—	ــ
		Man > Py in vaniets	_				05	5	L			L	<u></u>	<b> </b>	1	L		Py Me		$\sqcup$								<b> </b>	<del> </del> _
80.2	83,7	Tem & 3 cm Massin man voin soument				Ry Mantep	60.65	95	2529	802	63.2	0.5%	0.1	6%	<u> </u>	13	<u> </u>	3	3.500					$\dashv$			<u> </u>	<u> </u>	$\vdash$
		and by left 30 atov. WK network is				New man	= 25°	70%		L			<u> </u>	L			L									]		<u> </u>	<u> </u>
		,	L				85°	30%																$\bot$	$\Box$		<u></u>	<u> </u>	$\perp$
						19th corb	10°	60				L							L		[							<u> </u>	<u> </u>
	L	L.					85		<u> </u>						ــــــــــــــــــــــــــــــــــــــ	L	<u> </u>			لتب									

85° 20 45' 20

		GEULOGIC DESCRIPTIUN			•	STRUCTURE			SAMPLE	ES	-	MINE	RAL	<u> </u>				IZATI YUN		Qz-	]	CARB				ASS/	AYS		
FROM	TO			FROM		TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Ру	Сру	KeD+	Cal	COLO		No. Veln	Cum	No. Vein	Cum thk	No. Veln	Cum	No. Veln	Cum thk	AZZA uA	Cu	Ag	Мо
80,2	23.7	830 · Ned CalCaroll in																					$\Box$						
		5/2 x and s/done 1.7 his Prays	$\sqcup$				<b> </b>	ļ	ļ	ļ				ļ										1.1					
$\vdash$	<del> </del>	icm pyman v GOCA	$\square$					ļ		ļ								$\vdash$					Lefe	씠	fred	003)			
02	017	Be con: - bordal man -		<b>e</b> z 2	04.5	1172012	56%	120%	2620	<b>42.7</b>	0/ 1	19	42	102		-	-						-		37		<del> </del>	+	_
D 214	26.	Freqs. Mico + hom network reins		03.2	80.5	1,7.0 tz	25	57/2	23,00	03.2	06.3	1 10	0. 2	100	<u> </u>			<del>                                     </del>						Ť	- 10		<b>†</b>		$\vdash$
<u> </u>	1	suppossed core lin mid on				man L	4-1-0	10/0		<del> </del>		<b> </b>	-	<del>                                     </del>		$\vdash$ $\vdash$													
		5= and mga. Hom prodominant					-	1	1				<b></b>	1															
	L	len Fe Dr.							<u> </u>																		<u> </u>		_
														ļ <u>.</u>													<u></u>	ļ	-
86.3	87,3	As Above:				(2)12 an		ļ	2531	86.3	89.3	1%	0.1	10%				1	1CM		1.0m						┼		
	ļ	Commite: XI , soft edination	-	87.7	88.7	Acribo Network	60	/		ļ		<b>-</b>											$\rightarrow$		$\vdash$		<del> </del> -		
	├	rung red on weitherst fratione	$\square$			Network	35,45	20%		<del> </del>			-	├												<b></b>	<del>                                     </del>		_
	<del> </del>	perullal come . 0.5 cm blebs cp 25 cm	1 1			1	5	10/	<b></b>	<del> </del>			-		-					-						<b> </b>			-
89.3	91.4	Sil- Bx - Bx Alt-pyron. 89.9 91.2 cp-py netword reinles will bloby cp. Limon life conti) rimi on py cp. mgn. Corb on polymetraine-lerchony				912-17	?		2532	893	91.4	3%	1.07	2%		23				1	1.3m								
		cp-py netword reinles will bleby				New COPY	+5°	40%							·					<u> </u>							<u> </u>		_
	↓	cpo kimonil (Fectob) rind on ance					60-75	40%		ļ		L		ļ						L						L	<u> </u>	ļ	<b></b>
	ļ	man Carb on notint rains-leaching						<u> </u>	ļ	ļ						Ш								-1			$\rightarrow$	ļ	
L	l				<u></u>	Lim BK	1 00	<del> </del>		ļ	40			-	ļ							<b></b> /				<u>-5</u>	+		
27.4	924	Sil Bx 91.4-72.0 Lm + pyre?	H	71.4	92.0	LIM BK	45°/1	1	2533	71.4	92.4	1%	0.27	65%	—	3%						-/		8		<del> </del>	₩	-	
<b></b>		jar, neal? replaced proce Freez	-			B~784	30	50		<del> </del>												{-	454	3			V-		
<u> </u>	$\vdash$	A world in breeze - Neter contre				Labold	15	100		<del> </del>		<del> </del>	_	<del> </del>				$\vdash$		_		<b>₩</b>		3	360				
	<del> </del>	As materia in breceix - Neter course? As usual there is a trace of chlorida with man in original sill & Krags		200	eile.	tote fall her	+100	1/00	t	<del> </del>				<del> </del>	<del>  `</del>	11		1	_								<b>—</b>		-
_	† —	A DESTRUCTION STORES	H			1 STONY MED	1210	<del>                                     </del>	<b>†</b>														T			$\Box$			
92.4	25.4	SIX - zecontasted by neethoring				As above			2534	92.4	95.4	270	0,23	6%		270						4							
-	1~~	dealinate man + 5 = on micro	П																										
		frzitores leti creomy-baise min																									L		
		on let height frakting i centle																L_									<b> </b>		
	ļ	hangtill Joseite?) I'm on late.												1	L			$\sqcup$	_							—	├	<u> </u>	
<u> </u>	ļ	hometal/Joseila?) Lom on later Resultance t O'NS" (" Wack and")	Н					<b> </b>	ļ	ļ				<b> </b>													<del> </del>	ļ.——	
<b>-</b>	-	dr ce py on ut notwork freetures	$\vdash$							-			-	_	-	-		-	$\dashv$			-	$\rightarrow$	$\dashv$	-			<b></b>	
	<del> </del>		H			·			<del>-</del> -	<del> </del>					-	$\vdash$	_												
_	<del>                                     </del>	<del> </del>						<del> </del>		<del>                                     </del>				<del> </del>	-							$\neg$		$\neg$					
	<u>†                                    </u>					<u> </u>	<u> </u>	<b>†</b>					· ·	<u> </u>	t	<del></del> -													

		<del>(11)                                   </del>					}(			<b></b> -		<del></del> -			-	MINE	ERAL	IZHT	DN							<b></b>			- <i></i>
		GEOLOGIC DESCRIPTION	l		5	TRUCTUR	Ξ		SAMPLE	ES		MINE	ERAL	S				PYRI	S IE I	Qz-F	5v	ICARE	1			AZZA	ZY		
FROM	τa		0 18	FROM	סד	TYPE	TCA	%ТСА	SAMPLE NUMBER	FROM	τo	Ру	Сру	Kept	Cal	Coco		No. Vein	Cum	No. V <b>e</b> in	Cum	No. Vein	Cum I	No. /ein	Cum thk	Au	Cu	Ag	Мо
																							$\rightarrow$	_					_
94.5	985	As above bearily reathered				26 About			2535	95.4	98.5	0.5	073	8%		5%									_		ļ		
																						L			94		<u> </u>		
						l							L											_					L
985	101.]	Sil Bx is As above but less		98.5	101.1	freelant.	25/55	30"	2536	98.5	101.	19	04%	8%		12					4000			3	22cm		igspace		<u> </u>
		werthered 98m - 40cm gt 2 V		980m	l	Olz py	45						L	<u> </u>										_				ļ	
		in middle (biturested your?) Games		985	/01.1	PYER	600	75"	<u> </u>				Ĺ	<u> </u>															<u> </u>
		in middle (between ted year?) Gament	<b>3</b>										l											·					L .
		why in rollad py closes to o. sem foulful	<u> </u>										<u> </u>																
		No co in massim py; only in Azeron																											L
		heistings and wealth dissominated																											<u></u>
		in cilicitial gones. Butt bringin																											L
		freedomes ent by late Fo On heinline	4																					_	_		<u> </u>		<u> </u>
		1/CA																											ļ
																							(	500	9/2		ļ		_
																											L	L	ļ
[01.]	100.5	Sild By includes . but glz venus		101.	104.5	notwork	45°	40"	2537	101.1	104.5	1.52	1.02	69	<u> </u>	190								8	ð (m				
		recommended by prep-FROX network				"	15	150					L																Ļ
		ven t czrb. NB. Cp in 1-2 mm																L											_
		seems on nedwork front 7 py											l														<u> </u>		<u>.                                    </u>
		1	Γ																										
			П																				Grea	01	2				
1045	107.6	5,18 Bx mainly bx - Qt2 v.	1						I	1		Ī																	
	!	104.5 - 105.5 / hrd Alay 17	T	104.5	107.6	perent	45	35'	2538	104.5	107.6	3%	2,5%	4%		12								0	1.8m			<u> </u>	
	Ī	massive cpapy vein in middle Wie				11121	1650	55"		1			Ī															<u> </u>	L
		Be veine disolon well develope notwork	T																										
		veins with purce Section re by			-	1			1	T			1	T															L
		massive cp=py vein in middle Will Bu veine display well develope notwork veins with py=cp. Section re bx ±30° hairline (crashed but competer	V.)											1															
	1	ann	1	l	Ī					1		I											G	29	7				
107.4	110,6	5/ Bx Bx Qtz V. = 20% horde &		107.6	110.6	Vaintels	150		2539	107.6	1106	3%	1.70	5%		1%									1.3				
		man bould unt mil (25°CA). Cp 25	$\Gamma$			(03-10)	45-50																						
		blobs and seems on network rainless					75.1																	]					
		- numaros 1-3 mm sol cavilis				natura k		40%															-						
		down beeching to coloit- a man constit	_			(1-2)	45	307.		1		L	ļ	ļ		ļ											ļ <u>.</u>		ļ
		liss in selection envoluses	1_				70	30%										ļ						_			<u> </u>	ļ	ļ
		NB - Tr. Nol. Cu 1085 on wirthoutford	•~	ŀ		network	35/55	70%				ļ	ļ ,									ļ							
		- 35" dominant and most preeffered	٠			1475/166	-	157.				·															****	L	-

horning cale v. direction (wk show?)

	<u> </u>																								14021		rel (	
		Г													MIN	ERAL	IZAT	ÎON.						1				
	GEOLOGIC DESCRIPTION	ı		;	STRUCTUR	E		SAMPL	ES		MIN	ERAL	S				PYR	ME_	Qz-	Py	CAR	B	T		ASSA	ZYS		•
FROM TO		8	FROM	סד	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	τo	Ру	Сру	KeS+	Cal	Coto		No. Veln	Cur	No. Veir	Cur	No. Vel	Cur	No. Vein	Cum	ASSA	Cu	Ag	Мо
110.613.1	Sil Bx 29 shows	Г	111.8	1/2.15	GOHOV	45	I	2540	110.6	113.1	4%	0.87		l	l				<u> </u>		1	1	4	(Och		<u> </u>		_
	NB. 0.5-100 mante state				Cont.	40'		1								,					4,5	405	В	1400				
<del></del>	of ep in lote while alov. 5 to Mis	╀	$\vdash$	-	1-4 also.	150	500	+	-		-		-	<del> </del>		<del> </del>	<del>-</del> -	├-	┼	<del> </del>	┼	<del> </del>	$\vdash$			<del>                                     </del>	<del>                                     </del>	┼
<b></b>	Notwork copy to persial	╀	-	┼		850		<del> </del>	· · · · · · · · · · · · · · · · · · ·		<del> </del>				<del> </del>		<del> </del>	<del> </del>	<del> </del> -		<del> </del>	+	<del> </del>	$\vdash$			ļ	-
<b></b>		╁╴	├─	+	<del> </del>	83	50	<del> </del>	<del> </del>		<del>                                     </del>	-			-	-	<del>                                     </del>		-		$\vdash$	-				<b></b>	<del> </del>	-
1131 1155	Sil Bx - strong leaching of	t	S	miles	h eb	ove.	<del>                                     </del>	2541	1/3.1	15.9	Uni	conf	zin	du	17.	_		->										
	carl + Foox + S= . Ruck Bodly	Γ		T					Ī		54	***	10	edi.								<u> </u>	L				ļ	
	broken - mints 21 50 /30' /60 CA	Τ						1				-			,						Ι.		L					
	broken - minty st 5" /30' /60 CA Frult? ) has on weatherd surfaces																						Ι					
	+ thin earthy red bonn encrustation																			<u></u>	_	_	_				<u> </u>	┞
	essec i minute blecks of Nel. Cu.	<u> </u>	<u> </u>	<u> </u>				<u> </u>													ļ	<u> </u>	ļ					ļ
	Fresh bresks on rock free covered minute diss cp. It express									·					L.,						_	lacksquare	<del> </del>				<b> </b>	<u> </u>
	minute dissa cp. It zonous	L		L				<u> </u>													L	<u> </u>	ļ				ļ	ļ
	that most of rock keelum 14/2/201			l				l											_	L	_	$oxed{oxed}$						L
	nestharing of co-py and calcite man																			L		<u> </u>						ļ_
	network Preduces.							1											<u> </u>		<u> </u>					<u> </u>		_
1 1	ł i	Г																						I			L	
118,7 121.5	SI" Bx - well workland - most		4	imi/	or 1 26	me.		2542	1/5.9	118-7	u	nce	rtz	٤, م	lore	Ł	wes	Ha	-	_	-2		GMY	G/Z			<u> </u>	<u> </u>
	notwork Practures leached of																L_						2	2019		ļ	ļ	
1 12 6	carb. 5 - Fear and conted																			<u> </u>	<u></u>						L	_
1   5 3	with izrositic(7)-limonile																				<u>L</u>							_
YO 2 3	+ Cuprite + Eirthy dep red crustinge + Nat. Cm. + mals with Fore is probable water course!																											
14 3 2	+ Net. Cm. + melochite.																			<u> </u>	<u> </u>	lacksquare				L	ļ	┡
61 3 0	Zone is probable water course!																<u> </u>		<u> </u>		<u> </u>					ļ		<b> </b>
-01		L													L.	L.,		L_,			<u> </u>	L	L	<b>.</b>				ļ
115.9 118 7	Sil" Bu - broken come - light							2543	118.7	121.5	1_1	mo	ent	2	du	九	W	27	ers	ns							· ·	<u> </u>
	werthering on firstures - ochre hm.	T									2	<b>L</b> d	15.5°	سكرم	-1	cel	<u> </u>		<u>L.</u>		<u> </u>	<u> </u>				L		
	weethering on freelures - ochre hm. 115.9 - 116.3 Grang Otz V. in lete					Ī	1												L								ļ	ļ
	co-ex 0.3cm veintel: 6. 45°	Τ		1			T													l	L	<u> </u>					<b>.</b>	
	CP-PY 0.3 cm veinleft @ 45° Ground CUM 116.9 - Feath in Grey Ate				]	I	1																					_
	vain a bezeling of network reins																				L							$oxed{oxed}$
	increases is doubt malachite							]																		ļ		<del> </del>
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T +- · · · · · · · · · · · · · · · ·			+		1		+		1	1		1			****	<del></del> -	1		-	7	1	1	1	1		1 .	1	1

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		GEOLOGIC DESCRIPTION				TRUCTUR			SAMPLE	7.5		MINE	RAL	2		۷L	K/N	YEIN PYRY	S S IE I	Oz-F		CARI	,			ASSA	YS		
ROM	το	GENERAL PERIODS	8	FROM		TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	та	Ру	Сру	Kest	Cal	Coto		No. Veln	Cum thk	No. Vein	Cum	No. Veln	Cum	No. Veln	Cum thk	ASSA Au	Cu	Ag	M
		C 1010					7	-	2544	1215	122 8	40	- 4	12			$\dashv$												+
<u>us  </u>	174.8	SIBX. Grangle is will		122.1	122.5	Gregatz	350		1299	141.5	100	7.2	0.4	9 10	-	1	_												1
		network py-cp voinlets 2nd 2cm massafs py cal all by vony thin irrespolar FW at 55°CA Distribution of lots which gts us		1221	1,4.10	AT A VS	7.	<b>†</b>	1	<u> </u>		T		1															Ţ.,
		very thin irregular FW at 55°CA																											1
		Distribution of lots which at 2 us							I															<u> </u>				ļ	4.
$\perp$		nonerally control by bresks between man all this frags. 122.4 - man replaced lithis frag									L	<u> </u>				$\sqcup$					<u> </u>	ļ		<b> </b>					+
		man elfel 11thin Areas.						ļ			Į	1		ļ	L									ļ					1
_		122.4 - Man replaced lithic free	L		<u> </u>		<u> </u>	<u> </u>		<u> </u>		<b> </b>			<b> </b> _		-				<u> </u>		-						+
		endored within whit at a rimmed by Netion Con Trace Nation Con on some late tractures // CA.	Ц		<u> </u>	ļ	↓	ļ	<b></b> _	ļ		ļ			<del> </del> —				-	-				├	├─┤				+
_		by Netion Ca Trace Notice Ca			<b> </b> -		ļ	<b>├</b>				<del> </del>	-			1-1					<u> </u>		-		-			<del> </del>	+
		on some late fractures / CA.					ļ	<del> </del>	<b>{</b>	ļ				<del> </del>															1
-		Trace chi in magn in alled foregs.	$\vdash$			<del> </del>		├	<del> </del>	<del> </del> -		$\vdash$		-	-	┝╌┤								_					†
			-		<del> </del>	<del> </del>	<del> </del>	<del> </del>		<del> </del>						$\vdash$						7	4.	LL.	120				T
-		Si Bx: Chlorit = late	-	122 6	125 9	1.1. 1816	24-0	200	2045	1228	125 3	12	0.1	8%		4%								/3	Ster				T
1.8	123.1	St SX Chippin = 13/6	1	1000	1	CN- 4/2	100	00	A27.2	165,5	1257.T		<u>37</u>	-								90	7 4	120					$\perp$
-+		cook 5 here heirlim natural remote Rock has less pervession stateer atto - vein boundaries and	H			SM, 9/7 Confell	45	80%	<b></b>	1														2	53m				1.
+		adation alle a verie houndaries and				20.01.41	0-5'	20%																					$\perp$
		Who have more district Hen Zugan							1																				1
		lither force more district. Hem Torry in tale remine Sulphide low Colorb (Corbonate) cream colonial.					ļ	1																					1
		Colit (Combant) come and amount	<del>                                     </del>					<b>†</b>																				<u></u>	1
		123.6 Cp in whit giz rimmed by spec.				1	†	1						1															
-		175.0 OP IN AME GIT FIRMING OF SPEC.	1				<del>                                     </del>	1		<del>                                     </del>	<del> </del> -													6~7	a12				I
145	1285	Sild Bx: Lithis Frees contain				Ging at	25"	250	2546	1259	126.9	12	4.	87		6%								23	Gra				1
2.4	158.1	more cerhonole which has not hem made by silice as well as chi. Notwork cale + ch! + hem my cp.  Blebs co in white at a Slight losething of CA! voinleds				1	560	470	,,, , <u>v</u>		1 2.1	1		1										WLL					
		have respect to silie as well as	t			cele chi	40%	1	<b>†</b>	<u> </u>		1												5	Sem				1
$\neg$		ell. Note at cole + all them and	T			ati.	0:5	<u>'</u>						1															1.
		Bloke co in which at Slight leaching	1				30°																				L		1
$\neg \uparrow$		d CAll vainleds					`															<u></u>		<b>.</b>					1
			1										<u></u>										(	Gry	24				+
8.2	13/.8	Sil Bx as above - loy 5"		128.2	1312			l	2547	129.2	131.8	1%	tr	72		5%						L							
		Sil Bx as above - low 50 Late celeite @ 45°CA Brill	L			ļ				-		L		-			·				ļ			6	53				+
		green ser? in calcile in frigs.	L		L			ļ	ļ	ļ		ļ		<b> </b>		$\vdash$		<u> </u>						<del> </del>					+
					<u> </u>	L	L	ļ		<u></u>		ļ								L.,					-				+
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			Ī		-1							 i			-	MINE	RALI	ZATI	ΩŃ									-	
	- 1	GEOLOGIC DESCRIPTION	1		S	TRUCTUR	Ε		SAMPLE	:\$		MINE	RAL:	2			h	3 VAL	È I	Qz-P	у]	CARI		l		ASSA	ivs	:	· .
РМОЯ	то		84	FROM	το	TYPE	TCA	ХТСА	SAMPLE NUMBER	FROM	TO	Ру	Сру	<e<sup>Q†</e<sup>	Cal	Corp		No. Vein	Cum thk	No. Veln	Cum thk	No. Veln	Cum thk	No. Veln	Cum thk	ASSA Au	Cu	Ag	M
1.8/	2.2	Dyke: Bis somer, bolistalason	-	13/.8		HUcaba	30°					$\vdash$			$\dashv$		$\dashv$											<u> </u>	+
		1 To diss All my fimm VK																									ļ	<u> </u>	$\bot$
		1 % dissa x10 my Limon, UK	↓_		Gla	For		ļ	ļ															ļ				<del> </del>	+
		wh specified teature due to	╂┈			(caleita) Cale ser	35	-						-		-  -	$\dashv$			$\dashv$		_		<del>                                     </del>					$^{\dagger}$
• • • • • •	t	being cele see stomes @35°	1	<del> </del>	-	Stomp +1		<u> </u>						$\neg \uparrow$															1
1	1	- 1 0 11 0 - 0 - 1/1 1 1/0W	T			5mb// 11/1/											[											ļ	
		Cot grains amonal of film.	╀		ļ			<del> </del>										-		$\dashv$				-	-			$\vdash$	+
		C 120 CONTROL - 1/4KE	╁╴	132.7	<del> </del>	PVFell	50"				,						寸	_						_					1
		Cot grains augment of film.  May correlate Dyke  6 1705 m 1217 HW: 36'CA  (151, magnetit)	十	132.7		7 4 1251																						I	1
		•						ļ	0.7.0					00		_			_					<u> </u>	_			<del> </del>	+
.7/	350	Sill Box Similar to show except	-					ļ	2548	1327	135.0	4176	tr	0%					124	rka	` <u>c</u>	2							-
+		for brist green society in metrix I Lithin Progs let Grabonst V.	╁		<del>                                     </del>		<del>                                     </del>	<del> </del>									寸	$\neg \uparrow$											1
		on tredung \$ 15° 6																										<del> </del>	4
		consing blocky ground essisted						<u> </u>																├				<del> </del>	
+		Green sericih - egnin ksor i	╂	-		<del></del>		-															-	<del>                                     </del>			<u> </u>		+
+		doniling and - Knick ame ?	,					<del> </del>	i																				_
		francishin 2000 - Krish 2000 ??  or lithu frees are of intrusive origins is appropriate of placerration intrusion																						ļ				<del> </del>	4
		All D D D. D. D.	╄		100 4	Litoret	-	<u> </u>	0.546			,,0	7	09	-		$\dashv$		R.	4-				-			-	┼	4
0 !	138.	What Dx: Biturestal 917 magn	, -	135.0	138./	ant mesh	200	<del> </del>	2549	1350	<i>1.38•.</i> 7.	K1/0	cr.	0%					/~9	7		<u> </u>					† ···	-	-
$\pi$	IJ	Alfal Bx: Bilorcalad off magno obviously coment little transport Man replacement in frags.	1	-	<del>                                     </del>	late colo	30	<del>                                     </del>																			Ī		1
		Notwork 1 lok cale = 5 is 2 loh					55										$\Box$										<u> </u>		4
		event (post bright sert cole?)	$\bot$	ļ	ļ		ļ	ļ																					-
+	-H	133.9 contre of heavily westland	1	ļ	<del> </del>		-	-	<b></b>					$\vdash$				$\dashv$			_			-				<del>                                     </del>	+
-†		Fort? Mil on most frestore.	11		<b> </b>	<del> </del> -	<del> </del>	<del>                                     </del>	<u> </u>																				_
	7		7														$\Box$										ļ	<b>_</b>	
$\perp$			╀	<del> </del>		ļ	ļ		<b> </b>	ļ														ļ				<del> </del>	+
+		NB wwk Ksport -> Ser (bright amon)	-	<u> </u>	<del> </del>			<del> </del>	ļ									-										ļ	_
1		@ 135.2 m					<u> </u>	1																					T
_		· · · · · · · · · · · · · · · · · · ·			<u> </u>				<del></del>												_								

			F				—			<b>—</b>				-		INE	RAL	VĖÌN	NUI 21			-1	_					7.7	<del>, , , , , , , , , , , , , , , , , , , </del>
		GEOLOGIC DESCRIPTION	I		5	TRUCTUR	Ę.	<b>.</b>	SAMPLI	ES		MINE	ERAL	2		ı. ı		PYRI	TE_	Qz-I	Y	CAR	<b>B</b>	ļ		ASS	Cu 3BX	* · S	8
FROM	סז		Ĭ,	FROM	ם ד	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	סזי	Рy	Сру	est	Cal	COLO		No.	Cum	No.	Cur	No.	Cur	No.	Cum	Au IBX	Cu	A9	Mo
-			183		<del>                                     </del>	<del> </del>	_		THOMBER	<del>                                     </del>		_			<del>                                     </del>	<del>                                     </del>	-	V 2	VI III	V &	41.11	1	1	GMY	Qfz	oyeer,			
			╁╴		<del>                                     </del>	<del> </del>	<del>                                     </del>	<del> </del>	<del> </del>	<del> </del>	<del></del>	$\vdash$	<del>                                     </del>		<del> </del>	$\vdash$						†	<del>                                     </del>			2000			
1201	124 0	6 1 d R	╁	120	1200	Gandia	0.0	4450	2550	1201	120 4	252	0.69	09	<del> </del>	2%						†	<del> </del>	7	30cm				1-
1284	121.0	Sild Bx es show but seo/cont	+-	1:0	(375	CAPA ,	35300	2001	12220	1 SEI	(27.5	, J,	2.3%	D.60	<del> </del>	7 '8						†	+-	<del>  '-</del>					
		715- Mar exiden.	╁╌			Lite care	4 + 15	0-7	2550	<del> </del>	<u> </u>	<del> </del> -		†	<del> </del>	1				-		†	<del>                                     </del>				1		
	-		╁	-		Watnerst 5	0,213	200	<del> </del>	<del> </del>		<del>                                     </del>		<del>                                     </del>	<del> </del> -	-						+	<del>                                     </del>	<del>                                     </del>					$\vdash$
1700	1111	Sild By 25 ster - goodered	╁┈		-	<del> </del>			2551	130.8	141.6	1.09	n.1	a7.		8%	$\neg$					<del>                                     </del>	1	1		5	70	25	
4.5-1.5	147.6	all limited to lete along along	T		_	tFe	20.0	50%	10231	1	-	,	1	0.711	1	1				l									
		in the fraction foots	T			7	45°	500	İ	† ·	1	† · · · ·	† ···	1	1	1-1													
<b></b>		corb + 5 + Fe from fractures crestes	$\vdash$			Carb = pry	± 5	1		<b></b>		1										Ι	Ι				<u></u>		
<b></b> -		bother core. We have course 2°Cu	T			1110- 174	± 15		1	1	1	1	<b>†</b>	1-															$\perp$
		I Lon on most frechers	1-	<b></b>	<del> </del>		1	· · · · ·	<del> </del>	1	<b></b>										_								<u>_</u> .
	<del> </del>	Law an Mist Lections	†	<u> </u>		<u> </u>		1	1	<b>†</b>	† · · ·	<u> </u>	1	T															
1411	1047	As Above relatively solid.	+	141.6	144.7	PY-CP15	20"	<u> </u>	2552	141.6	1012	0.5%	61	8%		5%							Ĭ	3	30-		Γ		
77L.V	17.7	masses of see in Lithie foress.	T	7.7.0	1	i	50	<b>†</b>		12.0	1	["	-	1	1											70	15	20	
		723313 4 327	†	1	<u> </u>	CZrbzpyip	0	20	1		1				T							T							1_
			T			<b> </b>	+ 30	50		1	1	1	1		1														
			T			1	70	30	1			1			1														1
	1		T			Quad	46"	100%		1		1			T											l			$\perp$
			T			1,944.7	1		1	1	1		1		1								Τ				L		
1002	146.0	As store: here westoring 145 3 - 146 - fault? In 2°Cu which minordists.	1	144.2	1464		1		2553	144.2	146.4	6.5	(0.1	129	2	5%										5	70	25	
14.7	1	145.3-146 - Fm-H?	1		1	<b>T</b>		1	1	1		1											T	$\Gamma$					
	1	Le 2ºcu pk const mineralization	1		1	1	1	1	1			l	1	1	1													<u> </u>	
		Lm on seut Pred.	T	1456		Broken?			1			Ī			I									1	ļ		ļ		
	1		T						T "		<u> </u>	L		<u> </u>						L	<u></u>	<u> </u>			<u> </u>		-	<u> </u>	1
			Τ			L	I				Ι									L		ļ			ļ				
146.4	149.3	A: 2 bove: with rock comprising				Constal	45	40	2554	147.2	149.3	10.5	10	15%	2	3%						↓	$\perp$	<b>↓</b> ∴	<u> </u>	5	60	35	$\vdash$
		35% ata v. with acrorolly	Γ			1	1.0	40				<u> </u>	ļ	<u> </u>	<u>L</u> .							J			ļ <i>.</i> .	<b>_</b>		ļ	
		diffused boundaries while ther than	Τ			Carb Ser	±15	50%						<u> </u>	$oldsymbol{ol}}}}}}}}}}}}}}}}}$					<u> </u>	_	<del> </del>	↓	┷	<u> </u>	ļ	↓		—
		grey sta. Finer Lithic Rrass	$\Gamma$				60	45		1			ļ		ļ	ļ				L	L	↓		<del> </del>	-		<b>-</b>		ļ
		A: above: with pack compressions 35% glav with generally diffused boundaries, while therethan extra sta. Finer Lithic Rrags 1-2°Cm + Coppile, Cu					0	15	ļ		<u> </u>	<u> </u>	ļ	_	1	<u> </u>				_		$\vdash$	+	+			-		<del> </del>
			1_	ļ	ļ		ļ		<u> </u>	ļ		ļ	ļ.,	ļ								+		+	ļ. —	20	10		+
149.3	152.4	As above - Carhoneth - 5= - Feax	$\perp$			Gray Q12	70		2555	149.3	157.4	1.0	Er	15%	4	58			<u> </u>			-	+	+3	200	10	10	20	-
	. ,	lezihim @ 149.8 (0.5m) ,150.7(3m	)			1	30'	30	<u> </u>	ļ	ļ	ļ		ļ	<del> </del>	L						<del> </del>			ļ		ļ		+
		lezihing @ 149.8 (o.s.m) ,150.7 (3 m leta crushel freilures in ser-cont				while GHz	45 .	80	L			L		<u>.</u>	1			L	_		_	-	1_		<b> </b>	<u> </u>		-	-
	I	+ 5 = Frox. Mgn 25 1cm clots				Csep	45/20	700	1			1								ļ		1							
	<u> </u>	Car on lake Praduct Sandan	Ţ	1		har face					1	<u></u>	<u></u>		1														

Spec on 12te Krzeluns, Secondary . Cu - Nahim, cupile etc. 50 100 bs 0° 30° cp Py Fe 30° 50°

			P		-							<b>1</b>				MINE	ŘÁL	IZA II VÉ ÍN	UN.			-		<b>( .</b>					
		GEOLOGIC DESCRIPTION	ļ.,		,	STRUCTUR	E	·	SAMPL	ES .		MINE	ERAL	S				PYRY	TE.	Qz-P	У	CARB	I	r		ASSA	12	T	1
FROM	TO		84	FROM	TO	TYPE	TCA	%TCA	SAMPL SAMPLE NUMBER	FROM	70	Ру	Сру	Ken	Cal	Colf	_	No. ∨etn	Cum thk	No. Vein	thk!	No. Vein	thk V	ein	thk a/>	Ĩ/3≠	Cu 5.8v	A9 0	Mo
1524	155.1	Sild Bx. crusted appearance				Pobrie			2556	152.9	155.1	2%	0.1	12%		5%								4	300	75	5	20	
		Lithis frozes well replaced by man				"	£ 20°	40	ļ			ļ					_			<b> </b>				_				<del> </del> -	
		Lithis frozz well replaced by man  py-ep-man atomser 2t route CA  strong creb-son petront.																						// /2	Des			ļ	
			L				<u></u>							ļ											4/2			ļ <u>.</u>	-
155.1	156.4	51/ Bx - Zone bounded by	上	155.1	<u> </u>	Old 18?	450		2557	155,1	1564	170	20.1	7%		3%	_			$\sqcup$		$\rightarrow$		8	60cm	?	7	40	<b>⊢</b> -
		Old foults @ 45°CA - herd grey	<u> </u>	155.6				<u> </u>	L	<u></u>				<u> </u>	L									_				ļ	ļ
		green gouge, diss man cut by cerb man veinlets. Mino zom	丄	1564	)	Lexiture	50					L		l				$\sqcup$				_	_	_	_			ļ	
		czob man veinlets. Mino zom	<u> </u>				300	60				L								L								ļ <u></u>	ļ
		1 50°CA py stringers intruded	$\perp$																					$\dashv$				ļ	<u></u>
		do 50°CA py stringers intended by white queels Czebenga later										l	l											_				<b></b> .	1-
		Strong Fear All' of fixs masks origin	_			ļ	ļ	L									_							_				ļ	<del> </del>
			_				ļ			ļ			ļ				_											ļ	₩.
1564	1594	Sila Bx. minor copy von.	↓_			A41-	ļ <u>.</u>																	-				ļ	—
		at + 30°; crob-ger - hom retwork	1_	158.8	<u> </u>	9772	450	ļ	2558	156.4	154.4	2%	0.1	122		2%		4	211					3_1	Sca	7	3	40	ļ
		10/day 1 mm which 8/7 . which 8/2 vacsy	┵			PYCP	25-30		ļ								4			$\vdash$				$\rightarrow$	$\dashv$			<b></b>	-
		-terminated gla Late hedares	<u> </u>		<u> </u>	ļ	ļ	ļ																					
		at 0° 50° Lithe front being	↓		ļ	ļ		<u> </u>	<b></b>								$\dashv$				$\dashv$			$\rightarrow$	$\dashv$			<del> </del>	├
		replaced by hometite, which	┺			ļ		ļ	L	<b></b>											$\rightarrow$							ļ.—	
		guarta generally barron.		155.4	<u> </u>	waterman	7	1	ļ												-			$\rightarrow$				├	-
			1		ļ		ļ	ļ	ļ											-								<del> </del> -	-
		,,,,	1			whitests	ļ	ļ				_	<u> </u>	_						$\vdash$				$\dashv$				- 45	-
159.4	162.5	25 2 bone: Lithis horse 80% replace	<u> </u>			W-1-7-	1 / 0	50%	2559	1554	162.5	2%	0./	15%		ļ		3	1 Cm							7	. i	20 %	
		by Feax (magnetite exply, hometite	4				200	25%								-	_						_	-				ļ	₩
		Late) Mino py-cp = hem 40° cA;	_			ļ <u>.</u>	450	25%				ļ	ļ													J			
		by Fe ox (magnetit errly, hemstit late) Minn py-cp + hem 40°CA; lat carb agec network occasional	_	102.5		ham	25°	ļ	ļ				ļ							<b> </b>		<b></b> -∔						<b></b>	-
		bleb cp. Potelyczob in ser	<u> </u>		<u> </u>	•	4	ļ				<b></b>		L	L					<u> </u>				-,-,					ļ
		, , , , , , , , , , , , , , , , , , , ,	$\perp$				<u> </u>	<u> </u>				L_		L	L_	$\sqcup$	_			$\sqcup$				4	_			<del>  _</del>	<u> </u>
1625	165.5	of hither trass. Bloky segmental	1		L	Whit at	1 7	50%	2560	1625	165.5	2%	0.1	25%	L	ļl.								2 !	360			20%	4
L		of Lithic Frage Bloky Sognanted	1_	ļ		ļ	70°	40	ļ			ļ		L	L	ļļ.	_			<b></b>				$\dashv$	$\dashv$			<b>├</b>	
		which als reining. Polichy py hom top	1_		<b>↓</b>	ļ <u>.</u>	85.	10							ļ					<b> </b>								<b></b>	-
<b></b>		bek crob. venning	1		<u> </u>	Corb	40"	ļ				ļ			L									$\dashv$					-
<b>├</b>			. <b>.</b>		<del> </del>		400	ļ																				<b></b>	· -
$\vdash$			╀		-	intefinal.	= 150	600	ļ				ļ								$\rightarrow$			$\dashv$					-
L			1	L	L	w. 5/// .		1	l	1				l	L	L I	_ l	LL		L l			1		. 1	<u>.</u> . /			

																MIN		IZAT						_		7		1.10	
		GEOLOGIC DESCRIPTION			,	TRUCTUR	F		SAMPL	FS		MIN	ERAL	2				Y&Y!	Ş	10	p.,	וראם	B Cum I thk			ASSA	ZYS		
FROM	та		¥.	FROM	) to `	TYPE	TCA	12TCA	SAMPLE NUMBER	FROM	тп	Pv	Cpy	اه	t cal	%	-	No.	Cum	No.	Cur	No.	Cumi	No.	Cum	Au	Cu	Ag Gi v	Мо
	<u> </u>		189	-			-		NUMBER	-		Ľ		Ke.	+	( <sub>0</sub> )		Veln	thk	Veir	thk	Vein	thk	/ein	thk	791	58,	ai v	_
165.5	1101		╀		-	whih. 3/2	45-57	70	0.77	ne e	,,,,	. 0	200	,	+	12.				<del> </del>	┼	<del> </del>	++	27 3	<i>,,,</i>		<u> </u>	30%	-
(,,,)	1621	occasional pay in white sta . 5 vaniels	╂	165.5	1004	<del> </del>	75- 90		2561	165.5	168.6	206	0.14	20	· <del> </del>	1 (0)				<del> </del>	ł		ł ŀ.	.". P	إست			90%	
		irregater and petchy, 106.2 10cm	+		+	DYIPFIN	400	50	<del> </del>	<del> </del>	<del>                                     </del>	$\vdash$	<del>                                     </del>	$\vdash$	+			-		<del>                                     </del>	<del>                                     </del>	+	+	$\rightarrow$	$\dashv$			<del> </del>	-
		map cele chi v. Q 45°CA	+-		<del> </del>	<u> </u>	600	50	<del> </del>	· · · · · ·			<del> </del>	<del> </del> -	+	<del>  </del>				<del> </del>	<del> </del>	<del> </del>	<del>  - +</del>						-
		THE CHE LAKE, WE 45 CH	╁	-	_	<del> </del>	100	30	<del> </del>	<del> </del>		<del>                                     </del>	<del>                                     </del>	-	+	1-1					<del> </del>	<del> </del>	<del>    ,</del>	Ti.	9/2			<b>†</b>	-
166 6	1916	25 shore: specularly commonly	<del> </del>		<del> </del>	who sh	100	(7)	2542	11,91	121.6	109	101	257	<del>_</del>	100					<del> </del>	<del> </del> -		17				30%	
100.0	77.0	rimmay who da v.	$\vdash$		<b>†</b>	<b>†</b>	,	13.5	~~~	1000	777.0	11.0%	13-11	100		1						<del>                                     </del>	1	7	~				
		Transport of the second	1		1	· · · · · · · · · · · · · · · · · · ·			1			İ .			1_														<u>_</u> .
													ļ									L	$\perp$	_			ļ		
171.6	173.8	25 shove: billy broken and ox.	L		<u> </u>	2 veidels		30	2563	171.6	173.8	2%	0.2	20	<del> </del>	23				ļ	<del>  `</del>	ļ	<del>                                     </del>					20%	
		on Asselwes at acute angles to core.	┖		<u> </u>	"	45	30		ļ		L	ļ	_	ـــــ						<u> </u>	ļ	<del>     </del>	$\dashv$				ļ	<u> </u>
		corbis + Fear leached - waterway	↓_	ļ	ļ	CP · PI Feak	40						ــــ	<u> </u>	<del> </del>	$\vdash$				<u> </u>	<del> </del>	├	$\vdash$	-+			<b></b>		
		Pault?	<b> </b>		ļ	ļ		<u> </u>	ļ	ļ			ļ		<del> </del>						ļ	ļ	—-				<sup>!</sup>		-
			-		ļ		ļ		ļ	ļ			<u> </u>	<u> </u>	—	$\vdash$				-		├	$\vdash$	$\dashv$	$\dashv$				
1210	10/ 1	1	-	ļ		Lik coib	+ 0 00	1.01							<del>,</del>	1%				├-	ļ	<del> </del>				-	<u> </u>		
113.8	176.	25 stare: 2 grangla verne will later	╁	ļ ——		1 py Fark	-10	60%	2564	173,8	176.1	2%	0.5	10%	4-	170				_	0.8		$\vdash$	$\dashv$				40%	
		1 cm py - cp veinlels in each @ 20°CA;	╁			. ,				<del> </del>				<del> </del>	<del> </del>					1/2	0.8 m	<del> </del>	<del>  -</del>		$-\dagger$			40 0	
		minus heirline co or notunt Limonite	⊢		<del> </del>			-	ļ	<del> </del>		<u> </u>			┼	$\vdash$				$\vdash$	├	-		-					
		on scale myled freshors is 2°Cu	<del> </del>		<del> </del>		<del> </del>					<i></i>	ļ. <b></b>		·	<del>  </del>						ļ		My	ah				
12/ 1	1795	25 Those: with several any all Feek	-	1769		0-	100	├	2545	12/ 1	1295	19	229	19	,			, -	1Cm		-	$\vdash$		2/			<u>`</u>	40%	
1761	77.5	vains, wh history on ep. Corb. py- 5%		1767	$\vdash$	P7 947 917	45	60	1545	176.1	1115	1.19.	6,24	137	+	<del>                                     </del>			16 m		<del> </del>	<del>                                     </del>	+-+	<del></del>	<del>'</del> ~			4010	
		ep-hem lesching -> Lim + 2°Cm	╁╌		├	<del> </del>	450	30°	<del> </del>	<del> </del>		-	-		+	$\vdash$	-1			$\vdash$	├─	<del> </del>	$\vdash$	_	一				
		Eponen (proping - 1 pm - 1 CM	╁╌		+	carb. Duce hen	450	1.20	<del> </del>	<del> </del>			<del> </del>		<del> </del>					<del> </del>	<del>                                     </del>	-	1		一				-
				-	<del> </del>	DY CP TRA	600	<del> </del>	<b></b>	<del> </del>		$\vdash$	-	<del> </del>	+		$\dashv$	-			_	1		$\dashv$					
			1-		<del> </del> -		100	ļ		ļ- ···- ·	<b>-</b> -	- 1			<del> </del>						<del> </del>	<del> </del>	† · † .	>00	95				
1795	182.4	Sild Breaze 25 There.			<del>                                     </del>	grengts	15.	20	2566	179.5	,42 0	2%	0.3%	200	7						$\Box$				3.			40%	
	,	west co-py stringer; life netions	1		<del>                                     </del>	7	45.	57)	2700	12.1.7	1.05.1	Y			1	1					<b>†</b>				1				_
	<b></b>	& gla cont chi i pycphem	<del>  -</del>	<del>                                     </del>	<del>                                     </del>	<del> </del>	60.	30	t					<del>                                     </del>	†						$\vdash$			$\neg$					
		The state of the s	T		1	CD-D7	40	†- <u></u> -	İ					<b> </b>	1-							1							
			Т			<u> </u>									1														
182.4	184.0	25 store: Strong network freatures	Г						2567	1824	184.0	5%	1.0	129	2													50%	
		of cp-py, 182.7 - 1cm masina	П			C10-194	60"	570	1		-																		
		CP & 45°CA . Incres is chl.				-4	35.0						1																
		celit expecially in little tregs.	T			~	200	10				l			1						Ī								
	·				1	6029/1	I		<u> </u>	لــــــــــــــــــــــــــــــــــــــ			<u> </u>	1	1						1	1	للتل		· \				

9279/1 250 500

	-		F	Щ		_				Ш				<b>.</b>	_	MINER				-	<b>-</b>					• •		•/	
		GEOLOGIC DESCRIPTION			5	TRUCTURE	F		SAMPLE			MINE	ERAL	S			F	YEIN: YRIT	Ē	Qz-P	y	CARI	3			AZZA	YS		
FROM	TO		ğ.,	FROM	TO	TYPE	TCA	%TCA	SAMPLE	FROM	מז	Ру	Сру	e0+	Cal	Coco	_[	No.	Cum	No.	Cum	No.	Cum	No.	Cum	Au I 3x	Cu SBX	Ag	Мо
<del></del>			89						NUMBER					<u> </u>	$\vdash$		-†	veni.	,, , , , , , , , , , , , , , , , , , ,	V E	CT II	V E 111	- CITIK	GMy	912	F.1.1	22.1	27.12	
184.0	165.3	25 7 bout cale + chl notice able	1			247913	15° V	20%	256B	184.17	185.3	2%	43	12%		2%	十							2				75%	
1.7.		in around 1255 of some Little frage					40"	30%																					
		network com vaintels mod developed	T											Ī	I														
	*	in ground miss of some Lithie frags.  network op my voim lets mod. Leveloped.  N.Cu + brossy asicular min (morcesit on late zente ca. fractions.	(?)																						$\Box$				
		on late zenle'CA. Fractures.													l														
185.3	187.6	24 shore: section doming tel by		1859	187.6	griyatz	20°	•	2569	185.3	187.6	2%	0.37	490		2%	$\perp$	$\perp$						/	1.700			80%	
		scute angle gray gla voin with				CP-PY	60/00	65%					<u> </u>		<u> </u>								L_						
		well dandones nelvort A. CD-Dy-FEOX				Sereptop	20.	80%						<u> </u>	<u> </u>		$\perp$												<b></b>
		well durdened nelvork of cp-py-Fear and ser py-cp yeinleds.	Γ				700	15%					l		L		$\perp$												<sup> </sup>
			1																					w	917				
			Г																			L		9	10/2				
1A2.4	182 6	Sil" Bluccia - occassionel	1						2570	1876	189.9	1%	(0.1	30%	]	1%								1000	4/2 4cm			8%	
	1	of py variable 60° us " where the															$\Box$												
<b> </b>	T	on her world Sagrafail on bounts	1-														$\Box$											L	
		of some white star .	$\Box$								11																		
		0 2000 2100	1												<u> </u>										$\Box$				ļ!
			Γ						2571	189.5	192.9	1%	KO.1	30%		1%							L	343	5/2				
189.9	174.1	As alone: Nest 5 leining chillsen	Γ																					20	6500			8%	<u> </u>
		hom with gray gla deine	Γ									I	L									L		L	4/2				
		7 / /	Г											I								L		5	3cm				
													I									L_	L						
Ţ		·							2572	1929	194.1	K17.	(0.1)	30%			_					<u> </u>						8%	
								L				<u> </u>	<u> </u>				_	$\dashv$											
			T												I														
194.1	199.0	Sild Breceiz 25 show	Τ			Gren Qtz	60°	60%	2573	174.1	196.6	1%	Lo.1	257		3%						ļ	L	Siez				35%	
	1	194,2 to 194.85 - 2 crushed	Γ				150	15%							1		$\perp$						↓	13					<u> </u>
		evenate voins commental with fine	Т					-				Ι	I									ļ		vil					
		stander veins commental with affine standard returnt	I									L												5	8cm				
		& hate ravilate Hino- on-co-hem							l						1							ļ	ļ						
		stringers																					L	Guy					<b></b>
		196.6 to 199.0 soveral gray gtz veins	$\mathbf{I}^{-}$						2574	1966	122.0	3%	1.01	10%	<u>}</u>	3%	_					ļ	L	1_	<u> 1.1 m</u>			60%	
		displey grobs breccistion and sherring	<u>.</u>	1983		Ser shed in 642 of 6 Macob chi 45	165°						_				_										-		<u> </u>
		possibly are 50 " subsequent more mont,				Ma cot chi	650	500						ļ			_					ļ	ļ		L				
		1977 cale chi IS appear to hold rock	1		'												$\perp$	$\perp$				<u> </u>	L						
		Togethar . T. Not. Cu on occass lost feele de	410						I																				!
	Ī				I	1	I	1		1		1	1	1	1					I		1						-	

FROM	ro	GEOLOGIC DESCRIPTION	8.	FROM	TO	TYPE	TCA	%TCA	SAMPLE SAMPLE NUMBER	FROM	το	Py	RAL Cpy	s   o+	Cal	Coto		No.	E_ Cum	No.	Y Cum	No.	Cur	No.	Cum	ASSA	Cu	Ag	Mo
<del></del>			89		<del>                                     </del>		<u> </u>	<del> </del>	NOWBER			<del>  -  </del>		ξ.	_	0	<del> `</del>	/ein	thk	∨ein!	thk	Vein	tnk	Vein	Thk		+	+	+-
20.01		SIP I I I	Н		-	whitest		<del> </del>	0.20-	100 0	2 - 6	07	102	2	. 07		+					$\vdash$	<del>                                     </del>	-	<del> </del>		<del> </del>	+	+
7).0	200.4	Sil Bx boston sulvertheral	┥	199.0	200.9	pyepists		<del> </del>	2575	129.0	100.7	270	20.2	10%	470		-	-+						<del> </del>	<del> </del>		··· ·	·	
		- appear to pave on affinity for	-		ļ	ween lets	900					$\vdash$										-		<u> </u>	-		<del> </del>	<del> </del>	+-
		- appear to have an affinity for	$\vdash$				<del></del>	<del> </del>									-	$\dashv$				<u> </u>		├				·	+
		specularite.			<u> </u>	OTZV 15	<b>!</b>	┞	<b>!</b>			<b> </b>											<u> </u>	<del>  , ,</del>	1		<del> </del>	┼	+-
		diss*.	$\sqcup$		ļ	. 11 012		ļ <u>,</u>	ļ					<u></u>								<b> </b>		Ш	2/2		<del> </del>		
00.9	05.1	Sild 3x - specular hourstile becoming	Ш	700.5	202.4	11.917	450		1373	700,9	202.4	1%	0,27	25%	3%	$\vdash$	_					-		7	90-		ļ. —	├	+
		more prominent giving rock 2				547912	y5-40	500															ļ	9~,			-	1	
		distinction blue grey colour. Lote					700	500																12	12 (4			ļ	—
		distinction blue grey colour. Lots with gla reining increasing Distinct				107.50	30°					L					_	$\rightarrow$							$\sqcup$			ļ	
		Fil at BO'CA displayed by Feax					500																					ļ	$\perp$
I		minerale imperiore a areissic				QTZV 20												[									L	ļ	$\perp$
		minerale improving a greissic															T												$\perp$
		smy alz vein 201 - 201.6 contains zugen alt benefal by Sericite py-ce	П														T										L		
		Rusen at hour ful his consiste ource							1			1					$\neg$	$\neg$											
		bands of 20° Trace Mos, *			$\vdash$												$\neg$	$\neg$	$\neg$										T
		Py-Cp Finel, disseminated will				<u> </u>	<del> </del>			·		1				$\vdash$		$\neg$	$\neg$								T	1	1
		Foox I how fort rock, Co. bonto 25			<del> </del>		<del> </del>					1				-	_							<del>                                     </del>				1	$\top$
			╂─┤		<del> </del>		<del>                                     </del>	<del> </del>				<b> </b>				+						<del> </del>	-	<del> </del>			<b>†</b>	†	
		creamy paletes on freetures			+		-	┼				<del>  </del>	-			-	-+		-				$\vdash$	14	sta		┼──	<del> </del>	+
		Note: 5 slickonsidat in siliceons - sericiti			├	<del> </del>	ļ					207		2.4					-						13cm		<del> </del>	+	+-
		sherr a 201.4		202.4	205.1	9~79/7			2577	202.4	2043	770	0.4	75/0	4%	-	$\dashv$			-				94	13cm			+	+-
		204.5 - 2mm Hos, @ 40° 0			<u> </u>	ukls17	45-0		<u> </u>									-	$\dashv$	-				<b></b> -	-		├	<del>                                     </del>	+
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95.1		SILICIFIED QUARTZ		205.	208.	STER ATZ ME	20	30	2578	204.3	208.1	7-	Tr	10	nil	Tr		0		0		3	0.5	1.1	6.0				
		MAGNETITE BRECCIA					50	35			l													<u> </u>			ļ.,	ļ	$\bot$
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Ι,	_	GEOLOGIC DESCRIPTION	ļ.,	<del>-</del> . <del>-</del> . <del>-</del> . <del>-</del>	r <u>-</u> .	TRUCTUR	E	1	SAMPLE	S		MINE	RAL	\$  +	ادما	ام ا		PYRI	Τ <u>Ε</u>	Qz-l	у ГС	CAR	B   C	02.C	(4)	A336	irs Ini	Ag	Мо
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		SILICIFIED QUARTZ MAGNETITE		2/1.1	214.0	57GP 012-111	50 70	80	2580	211.1	2/4.0	0.1	Tr	8	0	0.5			1.0	1	57.4	0	<u> </u>		1.0		<u> </u>	<b>├</b> ──	<u> </u>
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-		, , , , , , , , , , , , , , , , , , , ,	$\vdash$	214.0	2/7.0	STOR STOR OIZ-Py			258/	2/4.0	217.0	0.3	Tr	10	0	0.3	$\dashv$	-	1.0	8	82	0	<del> </del>	0			<del> </del>	$\vdash$	<del> </del>
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						STGR QTZ-TY	50	100								$\sqcup$		$\longrightarrow$			ļ	Ь	ļ				ļ'	<b></b>	<b>_</b>
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		C 227 - Imm spechem	$\vdash$	216.0	29.0	5760 9-0 5762 072-04	45		2585	26.0	229.0	0.5	1.0	10	0	0.1				2	8	<del>  '-</del>	-	13					
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				232.0	2350	STGE CIZ-PH	50	100	2587	232.0	235.0	0.6	0.3	9	٥	0.1		0		3	68	ļ	<u> </u>	2	9		<b></b>		<b> </b>
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<b> </b>			╂		<u> </u>	POTZP	50	100	<b>.</b>	<del> </del>	<b></b>	<b>.</b>				<del> </del>				-		┼	┼	<del> </del>		}	<b> </b>		<del> </del>
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<b></b>		2mm spec hem + carb	╁┈		<del> </del>	MALE C	30	100	<u>'</u>	<del> </del>	<del> </del>	╁─	<del> </del>	<del> </del>	<del> </del>	┼┤				<del> </del>	<del> </del>	+	<del>                                     </del>	<del>   </del>	-	<del>                                     </del>	<del> </del>	<u> </u>	<del> </del> -
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		GEOLOGIC DESCRIPTION			S	TRUCTUR	Ε		SAMPLE	ES		MINE	ERAL	S				PYRI	SE-1	Qz-P	Ý	CARI	3	West	ام -	ASSA	YS		
FROM	סז		89	FROM	TO	TYPE	TCA	ХТСА	SAMPLE NUMBER	FROM	TO	Ру	Сру	KeO+	Cal	Coto		No. Vein	Cum thk	No. Veln	Cum thk	No. Veln	Cum thk	No. Veln	Cum thk	AZZA	Cu	Ag	Мо
			L	2-2		6404.0			26:00		-	22	0.5	_		<u> </u>	-1	0		-	3	0	_	٥	-				$\vdash$
		S'LICIFIED QUARTZ- MAGNETITE BRECCIA (CONT)	-	238.0	241.0	PQ-P	50	100	2589	23B O	241.0	0.5	U.5		O.	TY				-									_
	,	•				247.6										<b> </b>					36	٥		<del>     </del>	8				<del> </del>
		243.0-244 - FUT 1-3 cm		241	244	STGA PA-P ST&R	50		2590	241.0	244.0	1.2	0.8	1	O	tr		0			26	5			9		-		<del> </del>
	<b></b>		┨			436	50	100		ł	-					<del> </del>													
			$\vdash$	744	247	STER	\$2	100	2591	244.D	2470	0,6	1.0	8	٥	0.3	$\neg$	0	$\neg$	2	43	Ò		2	6				
•			1	MT1		STGR WGP STGR DAD	50	100		<b>6</b> , •			-																
		247.7-247.8-flt 1-3cm	П																										ļ
				247	250	STER	70	50	2592	37.0	250 J	1.4	0.9	6	4~	0.5		2	4	2	44	0		2	n				<del> </del>
		248 small bleb spea hem.					\$0	50																			L		<del> </del>
		+ pyllosilicates 247-250 (green)				STER WAR STER	50	100			·													Ш			L		├—
		(green)				STER	SD	100											_										<b> </b>
																	$\dashv$		_						_		<u> </u>		<del> </del>
		251.5 - 1-2 ma wire Native Cu	Ц	250	283	\$762 \$762 \$762	50		2593	530	233.0	1.0	0.8	5	Ψ×	۵,3		0		3	73	0		4	36.				
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		2.2.2.4.2.1.2.2.2	╀╌	253		OTZ-PY	7.	100	2594	253	761- 4	0.3	0 7	4	0	^ 2			BS	1	120	O	_	0					<b>-</b>
		253.9- STRONG BID	-	252	4>6	CC15- P4	10	190	<u> </u>		2300	19:3	<u></u>		<u> </u>	2.5			23	<del>`</del>	-	-							
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			-	256	259	MAP	50	100	2595	25h	259	2	0.2	6	0	tv		T	50	0		0		3	12				
				638		WW C	J.	100		-50		-	0.0		_										_				
				259	262	STOS PY	70	100	2596	259	262	0.1	0.2	9	tr	0.1		7	2	U		0		2	9				
				22)		ध्रु	50	100	2070				-		<u> </u>	1													
								1		<b>†</b>	1											11		977					
		263.5 . 25cm GREY OTZ - DV UN		262	265	VN 9Y GTZ-PH STEP PWP	So	loo	2597	362	2650	0.2	0,3	6	0.3	0.2				2	110	0			25				
		263.5. 25cm GREY QTZ- PY VID = mad. civil.	1			5165	50																						
		265 chl-mod to struct																						24.5	- 50				ļ
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			<u> </u> _	265	268	aus-bh			2598	د کین2	268,0	1.0	0.3	5	+4	14		٥		2	85	0	WAP	L.J	SO				
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		GEULOGIC DESCRIPTION			_	TRUCTUR	<b></b>	_	SAMPLE	2.3	-	MIN	ERAL	s		MINE	RAL	IZATI YUN	UN S	P.V.F	14 5 v	ICARI		WH!	Y &	ASSA	YS	<b></b>	
FROM	סד		38	FROM	TD	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Ру	Сру	Kellt	Cal	Colo		YLIN PYRI No. Vein	Cum thk	No. Vein	Cum	No. Vein	Cum thk			Au	Cu	Ag	Мо
			╀		-	STOR			200			ļ.,		-	ļ	<del>                                     </del>				_		ļ	L	હ્ય				┼	+
		SILICIFIED QUARTZ - MAENETITE  BZECCIA (CONT)		265	271.0	STOR Pap W SEY 477-94	50 70	100	5 <i>2</i> 30	268.0	271.0	06	0.5	5	+*	*		0		2	140			<u>'</u>	80				
		269.4-270.Z - GREY CRACKLE GTZ-DY	<del> </del>																										
	_	JN ~ 1-2 % DM	✝					$\vdash$	<b></b>	-		$\vdash$		-	-	$\vdash$		1							_			<del>                                     </del>	1
		* - NATTIVE CU @ 270.2	ł					<del> </del>								·						1						1	-
	$\neg$	(PRIMARY) + ON FRACTURE	1					<u> </u>				<del>                                     </del>						1											
	- 1	- wk - mad ser - epi	t –																										I
				271	274	STER POP	70	50	2600	271.0	274.0	8.0	0.5	7	tr	0.1		0		2	50			1	8				
						••	50	50																				<u> </u>	
						STC D. NOP	50	100																				ļ	<b></b>
																												<b>↓</b>	—
		275-277 - MD. SEV-691		274	277	666 668 8768 8768	20 50	loo	2601	27 <b>H</b> .O	277.0	12	03	8	0	0.1		۰		-	2				4			ļ	ļ
			L			wap	50	100									_			$\rightarrow$					_			├	—
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						ACD	50	100	2602	271.0	280.0	0,1	tr	8	tv	0.1	_	0	_	0		0		2	4			↓	
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			<u></u>			Pap	20		2603	280.0	283 o	$\perp$	1.5	8	łr	0.3		0		3	38	0			2				-
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			Ц			NQP	50	100									_								_			<u> </u>	—
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$\rightarrow$			L			Par	50	100	2604	283.0	286.0	1	0.6	9	0.2	ان.ه	_	٥		2	94	0		0	$\dashv$			<u> </u>	—
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	_	288.2-289.5 - BUL GTZ VIJ	$\sqcup$			46A	50		2605	786 U	<b>29</b> 0.0	2	0.9	8	0.2	0.4	_	0			8	0	<b></b> ∤	-	26				<del> </del>
			_			WQP	50	100						L			_												<del> </del>
																				-								<u> </u>	+
	*	QT2-Mt DYKE 60% HT 40% OTZ							2606	290	<u> 291.5</u>	0.2	0.3	13		4		-		-		-							+
		- WELL DISSEMINATED																-			_								-
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									2607	291.5	2940	0,2	TV	9	*	tv		-		-		-1						-	+-
			-						3/-0	204 6	200.0				1			_	-							<del></del> -			
			-						2600	294.0	247.0	0.2	14	10	FV	0.7	$\dashv$	-						_					+
			1_									L						-				<del>  </del>		-, 1					·
		BECOMING HORE ALTERED & SERICITE	$oldsymbol{oldsymbol{oldsymbol{eta}}}$			NQ2	50	100	2609	297.0	300.0	0.1	0.2	9	0.1	0.5	_								2				<del> </del>
		CAL & green phyllosilicatus	<u> </u>														_ 1												ļ

		CERL DETE DESCRIPTION														МІМ	EKAL.	IZAT VEIN	1111V 21	Piel	ار			W141	Z	ASSA		_	
FRUM	i to	GEOLOGIC DESCRIPTION	<b> </b>	FULIM	TO	TRUCTUR	E Tira	ZTCA	SAMPL	EDITH	Tn	MIN	ERAL	S	Cal	[ ] <sub>0</sub>	1	PYRI No.	Cum	No.	Cur	ICAR	Cur	With Q2- No. Vein	Cum	Au	Cu	Ao	Мо
, Kun			89	7 8017		1172		7107	NUMBER	1 2011	, , ,	ļ', <b>'</b>	СРУ	ke~	-	Cor		Vein	thk	Vein	thk	Vein	the	Vein	thk		-	<u> </u>	+
		SILICIFIED WARTZ - FE OX	1									ļ.,	<u> </u>	<del> </del>	-	-		<del> </del>	<u> </u>	<del>  . −</del>		<del> </del>	<del> </del>	0			<del>├</del>		+-
		REPLACEMENT BROCKIA (CONT)	$\bot$			RUP	52	100	2610	3∞.0	303.0	0.3	0.3	1.1.	0.5	0.8		<u> </u>			20	10	-				<del> </del> -	<del> </del>	
			-			GREY VA		<del> </del>	2		2-1	-	1.0	100	0.3	1.		_	22	$\vdash$		-	$\vdash$	GREY			$\vdash$		+-
	· ·	202 2 205 4 650 4 650 4 1	1-1			COUS. DA			2611	303.0	206 0	18.0	1.0	4.0	0.2	1.0	-	4	21	├		╁─╴	<del> </del>	┼┷╌	170				<del>- </del>
		303.7 - 305.4 - GREY QTZ VN	╂┤			TY YN	70	52		<del> </del>	-	╂	├		-	-	<del>                                     </del>		-		_	┼─	<del> </del>	<del> </del>	-		<del> </del>	-	+
		- CRACKIE	1			<del></del>	50	75		ļ ·			ļ	<del> </del>	<del> </del>	<del> </del>		<del>  -</del>		-	-	-	<del> </del>	+-				-	<del> </del> -
		305.4 fit? - Cole Broken to 2 cm	╂┤			<del> </del>		┼	<del></del>	<del> </del>		├	<del>├</del>	├	<del> </del>	+	-	-		├-	-	<del> </del>	+	┼			<del>                                     </del>	<del>                                     </del>	+
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306	325	CORE IS INTENSIA AUT. TO SER.	H		<del> </del>		-	-	2612	306.0	3090	٦,	L.	40	0.2	04	-	0		-		+_	$\vdash$	-					1
	يب	CHL = 310 GREEN PHILLD SILLCAMES	1		<del> </del>		ļ	<del> </del> -	2012	1008.0	20,0	. <u></u>	-3×-	7.0	10.0	10.7		<del>                                     </del>		<del> </del>		<del>                                     </del>	1	1				1	
	<del></del>	LITTLE OF NO REPLACEMENT	H		<b></b>				<b>†</b>	<del>                                     </del>	_	1	1		1	1	<b>-</b>					<b>—</b>	<del>                                     </del>						1
		-CORE 300KEN P 307.1-508	1		<b></b>							†	1		ļ	1	<b> </b>	l		<b> </b>			1						
		C 308.8	П																										1
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		· CON'E Brown @ 309-309.8m				PWP	50	100	2613	309.0	312.0	0.6	0.5	7_	0.2	03		-		2	22	ļ <u>-</u>	ļ	-					-
			$\sqcup$					<b></b>		ļ		L_		<u> </u>	L			<u> </u>		Ь		ļ	<u> </u>	<del>                                     </del>	_			├	┼—
			$\sqcup$		ļ	be is	50	100	2614	3120	3150	1.0	3.0	3_	0.3	10		-		1	23	-	<del> </del> -	1	2		ļ <u>-</u>	ļ	ļ
		- Cosé blace 6 312	+			2000	50	100		ļ		<b> </b>			-	<del> </del>		<u> </u>		<del> </del>	<u> </u>	₩-	<del> </del>					<del> </del>	
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			H			404 Nr	50	(00)	2615	315.0	218.0	10	0.4	2	0.2	0.6	<u> </u>	2	8	4	42	-		-				├	<del> </del>
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			H			42		<del>                                     </del>	2000	-		<u></u>		-	-			-				<u> </u>		1				<del> </del>	
			H		-	PY	20	100	2616	3180	321.0	11	0.2	4	0.2	0.3			2	-		<del>                                     </del>			<b>—</b> ∤			<del> </del>	+
			H			<u> </u>	<del> </del> —		2617	321.0	2140	0/-	24	2	1.0	0.6	$\vdash$	-				-	<del>                                     </del>	-					+
			H		-				2617	361.0	324.0	10.6	0.7	-	.77	0.6		-						-					
		# NATINE CL @ 324.5 - 326.5	H			PY VA	50	100	2618	324.0	322.0	25	1.5	5	0.3	5.3		1	18	7	98	_		-					<b>—</b>
		n 10 - 1 nm blebs				POP	50	100	20,0	327.0	327.0		,~		· · · · · -			2	10		70		† · · · ·	† · · ·					-
-			H				<del></del>	1.50		<b></b>		-		-										+	_				<b>†</b>
333		MODERATELY ALTERS Q-M	$\dagger$					†	2619	327.0	330 D	0.7	0.2	4	0.1	0.2		-		-		-	†	1-1					1
		- magnetite decreasing down									,,,,,,,	-	_	1	-														
		hole, by decreasing	$T^{\dagger}$					İ	2620	330.0	333 0	0.2	tv	3	0.1	0.4		_		-		_	-	-					1
		Sx decreasing	H					<b></b>		1				-	<u> </u>										$\neg$				
	*	- Mative Cu on Practures (0x10)						†	2621	333.0	336.0	0.2	tv	2	0.3	0.4		-		/		-		_					1
		CAVE @ 334 ~ 10 cm									-														$\neg$				
			L							t														11					1

		GEOLOGIC DESCRIPTION				TOUCTUD.			SAMPL			Luvu	ERAL			MIN	ERAL	IZAT	ION S	Pin				WH:	7 d	224	244	<b></b>	
FROM	TO	CIOUKID	88	FROM	TO	TYPE	TCA	итса	SAMPLE NUMBER	FROM	то	Py	Сру	, eQ+	Cal	COLO		No.	Cum	No.	Cum	No.	Cum	No.	Cum	AZ ZA Au	Cu	Ag	Mo
		ALTERED, INTRIXIVE +	1		<del>                                     </del>	<del></del>		<del>                                     </del>	, worder			<b></b>	1.	1	<del> </del>	Υ	<del>                                     </del>	Veni	CITIC	V 6111	CIIK	V E 111	-	V E 117	VIJK.		1		
		ALTERED QUARTZ HACNETITE	T	<del> </del>	<del> </del>	<u> </u>	<del>                                     </del>		2622	336 0	359.0	0.2	+4	1	0.3	0.6	<del>                                     </del>	-		-		-	<u> </u>	_		<u> </u>	<b>†</b>	1	<del>                                     </del>
		- mud sex	1	İ	<del>                                     </del>	<b>†</b>	<u> </u>	İ	1				1 .	1		╁▔	1	<b>†</b>											<b>†</b>
		- str Chi	$t^-$		<del> </del>	POP	50	100	2623	3390	¥2.	0.3	0.3	3	0.1	0.3	$\vdash$	-		2	85	-		-					T
			十	<del> </del>		1-1-81		1.00	1	J. L.S.	-				·	1	<del>                                     </del>	<del>                                     </del>					<b></b>	04	•		<b>—</b>	1	1-
		* native Cu on oxidized fractures	†		<del> </del>	DEVAP	50	100	2624	342.0	345.0	06	0.3	17	0.1	0.3		-		-		-	$\vdash$		IZ7				
		Thirtee Co. St. Oxide Co. Tilde Co. Co.	T		_		30	100		(6)		-,3	1	† <u>-</u>	1	<u></u>	1	1							EV			1	
344	368	PREDOMINATELY ALT INTRUSIVE	1		<u> </u>	PQP	50	100	2625	345.4	340.0	٥.٠	0.6	1	0.1	0.2	1	-	_	1	60	_		T	80				
	420	- mob ser	1	<u> </u>	<b>†</b>	497	50	100	1		-:0:-	1		1	1		†	1	1										<u> </u>
		- MOD CHL	†-			77.		-		<b>†</b>		1																	
		- pyllosilicates (green)	十	<del> </del> -	1	<u> </u>	1	†	2626	348.0	351.0	0.1	+~	3	tr	0.5		-		-		-		-					
			1		1	1	1		1				1.																
		e351 - hem.				PY VNU	50	100	2627	351.0	354.0	1.7	0.3	3	tr	0.3		2	8	1	40	-		_					
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		CORE BROKES 346-354	T			Pap	50	600	2628	354.0	357.0	0.8	0.3	2	*	0.1		1	2	-	130	_	Ĺ	-					<u> </u>
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			T			PIVNE	50	100	2630	360.0	3630	0.5	0.3	6	0.1	0.3		11	4	5	110								I
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			Т				\$0	SO							1														
			T						1	1			1																
363		HEGACRYSTIC K SPAR POPPHYRY	1	ļ		Py unit	70	100	2631	363.0	3460	0.5	0.2	5	0.1	0.2		ľ	4	4	21	-		~					
		- CLEARLY DEFINED	1			Pap	70	60	1 22 7	1		"	1	1	1			1											
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			T							1		Ī		1	Ī	T													
			Τ			PQP	70	75	2632	366.0	3490	0.1	0.1	6	0.1	0.2		-		12	35	1		1					
			T		1	T	50	25					T	Ī	1	1													
			T						1				1																
			Т			PQ?	70	30	2633	369.0	3720	0.2	02	5	0.1	0.5		1	2	15	86	2	١	-					
			T				90	25																					
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			土		<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>			<u> </u>	<u> </u>		1		<b>1</b>											

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		GEOLOGIC DESCRIPTION	Ļ.,		, <u>.</u>	STRUCTUR	E		SAMPL	ĘS	,	MIN	RAL	S			,	PAK	YE .	Qz-I	Y	CAR	9	T	T	AZZA	247	1	T
FROM	ם ז		24	FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	מד	Ру	Сру	Kest	Cal	COLO		No. Vein	Cum	No. Vein	Cum	No. Vein	Cur	No.	thk	AZZA Au	Cu	Ag	Мо
		(cont)			T							l									l								
		K SPAR MEGACRYSTIC PORPHYRY				POP	70	70	2634	372.0	375 3	0.5	0.3	5	0.1	0.3		1	0.5	13	55	-		1.					
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	ļ		$\bot$		ļ	707	OF		2635	375.0	378 0	0.5	0.3	5	0.1	03		4	Z	9	25	<u> </u>	<del> </del> —	-	$\vdash$		├	├	├
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			$\perp$	<u> </u>	₩		<u> </u>	-	<del>  </del>	-		<del>ا</del> ـــا	ļ.,	_				_		1		-		+-		├──	├─		$\vdash$
391.4	396.6	HYLOWITE SHEAR ZONE	1	ļ	ļ	POP	70	100	2641	391 4	394.1	0.6	14	1_	1	1.0		-		<del>  '</del> -	6				<del> </del>	<del> </del>	<del> </del> -	ļ	
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		ALTERED PORPHYRY DUARTE	+			<del> </del>	<del> </del>		2642	374.1	376.6	0.6	14	. 10	1	1.0			-			<del>  -</del>	··· ·	+	1 - 1				
=	ОН	FE . ON REPLACEMENTS	+			+	<del> </del>	-	2643	DGL 1	400	100	1	=	0.1	05	<del>                                     </del>	_	-	-		-	-	+-			_	<b></b>	<u> </u>
	·	- REMNANT K SPAR FRAGMENTS	-		<del> </del>		- i · · · · · ·		_ حبري	- 12.6	1	70.0	"	.3		10.3				<del> </del>		1	ļ		j				<u> </u>
-m		THE STATE OF THE PERSON OF THE	-						2644		44.	٠.		-	1	0.0	227.1			12.11		-		1-					
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ł			GEOLOGIC DESCRIPTION			:	STRUCTUR	Ξ		SAMPLI	E <b>S</b>		MIN	ERAL	S				PAP.	IE-	IQZ-I	- Y	CARI	3	¥7-	Py	ASSA	YS		
FROM	TO	1		24	FROM	TO	TYPE	TCA	XTCA	NOMBER	FROM	TO	Ру	Сру	K.0+	Cal	Coto	Мο	No. Veln	Cum thk	No. Vein	Cum	No. Vein	Cum (	lo. 'ein	Cum	Au	Cu	Ag	Мо
2	2'.	2	CASING.							2468	i			1												_				
		+	NO BLUCK AT START				<u> </u>			2469	24.1	27.1	4.0	74	4	0.2	0.8	+											<u> </u>	
21.2	21.6	0	RUBBLE - Runded 2 cm							2470	27.1	30.1	5.0	ħ	6	0.1	0												-	
		1	pieces. Very exid.	L			Dy star	SD	100	2471	30.1	33.1	5.0	0,1	5	+1	0.2		2	5										
21.6		+	- U to med. grey.	$\vdash$		<del>                                     </del>	<u> </u>				<u> </u>							_												
		$\perp$	- LITTLE TO NO K-SPAR STAIN - Magnetile 10-20%	F			Pustar	ടാ	100	2472	33 -1	36.1	6.0	N	6	74	0.2		1	4		_							-	
		1	- purite 10% (very pole-silver - ukagy - oxidized FeO on	1		-				2473	26.1	30.1	6.0	te	6	4	<b>k</b>											-	-	-
		#	calcute remnants.				<u> </u>			07.13	367.	37.1	_		_	<u> </u>									_					<b>—</b>
		#	- Lin's of no Coy 2 supt go, late remiet . + 24.1-24.	1					<u> </u>	2474	39.1	42.1	₩	ir	2	*	2.5													<del> </del>
		$\pm$	Q-C usinglet + in pyride valt	t													<u> </u>		_											1
		1	- Core broken to 16 111	$\perp$						2475	42 1	45.1	<b>*</b>	+4	Ľ	14	4.0													-
		7	Du Stringers & 31.0 4cm	+		-				2476	45.1	48.)	+	₩	2	tr	3.0													
		7	py Stringers & 31.0 4 cm + 2 blebs Cp - 33.1 4 cm 35.1 4 cm	F								ļ		-						_	-	<u> </u>								
		-	2 chlarite Nebs @ 36.3	1		-			-	2477	48.1	<u>রা.।</u>	+4	tr	3	+	5,0				-	-							-	+
		#	•	#		<b>†</b>			ļ. <u>.</u>	24 78	(1)	64 \	120		, ,	1	20						-							
		ı	- grun mica as bleb a 51.7	#						29 /8	51.1	<del>4</del> .1		10.8	10	177	-											ļ		-
1		- }	- core bleached 4 gray to white	$\pm$													-											<u> </u>	-	
51.3	56.	4	PY - CARB SHEAR ZONE u 75% py 25% CARB	$\pm$	<u> </u>					2479	54.1	57.1	15.	11.0	10	tr	15											<u> </u>		-
	+-	-	- very rotten - Crumbly - CPU present but sporty.	+					-	-		-	-	-	-	$\vdash$	$\vdash$	-												+

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								-									RAL	LVC ti	N					- PV	<u> </u>				
		GEULOGIC DESCRIPTION	1		S	TRUCTUR	E		SAMPLE	23		MINE	RAL	5				PYR	YE_	Qz-F	y	CAR		OTZ.	P <sub>1</sub>	AZZA	24		
FRON	τo		34	FROM	TO	TYPE	TCA	%TCA	SAMPLE SAMPLE NUMBER	FROM	מד	Ру	Сру	KeOt	Cal	Colo	Мо	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Veln	Cum thk	Au	Cu	Ag	Мо
		ALTERED HOENFELS (CON'T)							2480	57.1	60.1	30	1.0	10	-	6	*					<u> </u>		_	$\exists$				-
			╁				<u> </u>			ļ		ļ			ļ			_		-				$\dashv$					┼
	*	57.4:58.3 - Py vein with ~ 1% cpy + 0.01:	+				├		2481	60.1	L9 1	, .		-,		-		-						+					<del> </del> ·
<del></del> +		40c	╁╌				<del> </del>		2701	00.7	03 1	3.0	Ψ.	6	-	3	_		-			$\vdash$			$\dashv$				<del>                                     </del>
		Plus	+				<del> </del>			<del> </del>		-			_	1								$\neg$					1
		From 60.1 -					<del>                                     </del>		2482	63.1	66.1	1.0	0.3	6	-	3													
		rugs fulled until vellow - rusty brown carbonate.	-																										ــــ
		rustul brown carbonate.																					1						<del> </del>
			$\perp$		<u> </u>			ļ	2483	66.1	69.1	0.3	0.2	9	-	3				$\vdash \vdash$									┼
	*	- core body broken 60.2-63.1	↓_				ļ			ļ				L		1		<u> </u>											<del> </del>
		- core recovery ~ 50%	╁			ļ	<del> </del>		2/2/	10.			43	10	-	1,		-				-	-+	-+	-			-	+-
			╄			·	<b>├</b>		2404	69.1	13.1	1.0	0.5	10	Tr.	1.0									-				<b>-</b>
		G/05 = 2 Con 550, 500	╁╴				<del> </del>			<del> </del>		-	-		-			<del>                                     </del>		$\vdash$				$\dashv$	$\dashv$				
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		green mica @ 4500 TCA.	T				t			1																			
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	*	CORE BADLY BROKEN 75.1.795	Τ						2486	75.1	79.5	1.2	0.4	10	tr	0.6													<u> </u>
		- COIL TECOVERY & 40%																<u> </u>						_	_				<u> </u>
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77.5	81.1	MAFIC DYKE	$\perp$				L		2487	79 5	811	1.3	+	-	-	-		L											-
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	•	COLE BROKEN 96-114	┖					↓	2494	99.4	102.4	15	0.4	9	#	4				<u> </u>	<u> </u>	<u> </u>		<u> </u>					<del> </del>
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		- moderate chlorite alteration	+		ļ	10. P4	8	15	2903	126.8	129 8	10	0.6	19	0.3	0.1	+		<del>                                     </del>	4	20	$\vdash$		<del> </del>		<u> </u>	<u> </u>	<u> </u>	1
		- weak spirite & birthe					20	25					ļ			I						<u> </u>					<u> </u>		I
		- K SPAC Activation is intense	╂┤			Pa. Pu	75	45	2904	129.8	183.0	12	05	-	101	0,	-	┢	├	4	24	$\vdash$	-	├	-			$\vdash$	+
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			+			Po-Py	75 SD	25	290 <b>5</b>	152.7	135.9	1.0	10.1	1.0	10.4	170	<del>  '</del> '-	╁┈		, p	100	<del> </del>	-		-		<u> </u>	<u> </u>	t
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			H			PQPy	75	100	2906	1359	139.0	1.3	0.4	10	0.1	0.1	0.02	-	-	2	14	<del> </del>	-	-	_		├	├	+
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	+	healed Q.C shear zone @ 147.9	$\sqcup$			PQ. Py	75	15	2909	145.1	148.1	1.4	1.3	9	0.3	1.6	0.06	<b> </b>		9	125	<u> </u>		_				<del>                                     </del>	╀
		4cm & 2-5% Cpu + 0.5% MO?	╂┤			<b></b>	30	35 50				$\vdash$	<del> </del>	-	+-	┢	-	├─	<u> </u>					-		<del>                                     </del>	-	-	t
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						PQ-P4	40	100	2911	151-2	154.2	1.3	1.2	10	0.4	1.3	-			3	93								
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-	┼	- strong Biotite along margins	1-1		+	Pip- Py	2	+	2914	/60 3	163.4	1.1	2.4	12	+	1	-	<del>                                     </del>	<del> </del>	2	2	$\vdash$			<del>                                     </del>			$\vdash$	<del>                                     </del>
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<u> </u>	<b>└</b>	1745 - 1749 - Shear Zone	₩		ـ	py show	45		2918	172.5	173.6	3.8	0.7	10	0.1	0.2	0.65	1-	40	13	10							<del> </del>	<del> </del>
	↓	- 60% py	+		ļ	PO: 14	75	70	<b> </b>	-		<del> </del>	⊢		┼—	╁	<del>                                     </del>	<del> </del>	├	├—	├		$\vdash$		-		-	<del> </del>	╁─
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<u> </u>			1-1		+	Pa-Py	75	70	2919	175.6	1/86	11.	10.7	7	10,2	0.8	+	┼		1,3	37		-					<b></b>	1
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LC 45

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1   at downhole and ("40-45")	ļ		- pyrite has some banding					ļ <u>.</u>	<u></u>	ļ							ļ							ļ				ļ!		. <del> </del>
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Coaling on the moly.	ļ		coating on the mony.							<b> </b>													ļ	ļ						
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- also biotite & chlorite (mod.)	ļ		also biotite & chicrite [mod]	_														·					<u> </u>	1						

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1		GEOLOGIC DESCRIPTION			S	TRUCTUR	Ε		SAMPLI	ES		MINE	ERAL	S				PAK	TE_	Qz-I	Ру	[CAR]	9	L OT	2 - R/	ASSA	YS		
FROM	TO	1	ğ , f	ROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Ру	Сру	, Q <sup>†</sup>	Cal	2,00		No.	Cur	No.	Cur	No.	Cum	No.	Cum	A22A Au	Cu	Ag	Мо
<b></b>			19					<b>├</b> ─	NUMBER	1			<u> </u>	K-	├	C.		Veln	thk	Vein	the	Vein	thk	Vein	thk				-
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199.55	10.		-			WQ. P4	20	100	2929	177.S	ထား	5.0	27	<del> </del>	ļ <u> </u>	+		ļ	<u> </u>	<del> </del>	}	<del> </del>	<del> </del> -	12	-		<del> </del>		<del> </del>
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1		- hemodite Saining around pyrite - Biecciated from 202.4 -	-			<del> </del>		-	2930	202.0	200.	5.0	0.5		<u> </u>	0.2				-		-		├					├──
		- siecciated from 202.4 -				-		ļ	<u> </u>	ļ			<b>.</b>	<b>.</b>	-	$\vdash$		<b>!</b> —	ļ	ļ				├		-			₩-
$\vdash$		205.7				ļ		<u> </u>		<b>!</b>		<u> </u>	<u> </u>	<b></b>	<b> </b>	$\vdash$		ļ		Ь	ļ	$\vdash$	<u> </u>	<b> </b>		<u> </u>			<del>                                     </del>
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		- "It brown carbonate bands	$\perp$					ļ	<u> </u>	ļ		L	ļ	<u> </u>		1				<u> </u>		<b>—</b>		<u> </u>					├
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		- little or no magnetite											L		<u> </u>					<u> </u>	L	<u> </u>		<u> </u>	<b> </b>				
		* 4						<u></u>							<u> </u>			L		<u> </u>	<u> </u>	<u> </u>	ļ	l			<u> </u>		
		C 203.0 - Bull QTZ VEIN - 30 cm						<u> </u>						<u> </u>	<u> </u>							<u> </u>	L		L		ļ		<u> </u>
		-2048 - broken core						Ĭ						l	İ									l					
		· 205 · 5 - 205 · 6 - "							I	1										l									
		contact between sedements +					ļ															Γ							
		OTZ - Fe Dy Replacement Buccia				1																							
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205.7	$\neg$	DT2 - FOD PEDIACEUEST	+			Pa-Py	70	40	2931	205.7	201.7	4	26	10	-	OA				13	37	$\vdash$		1					
		DTZ - FEO. REPLACEMENT BRECCIA. / K-SPAR	-			14-14	40	40	- 1-1	-3			0.0	-	1	1		<b>-</b>		<del>  '-</del>	-/								
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		- K-sear crystals to 1cm	+			Pu stra	70	30	2936	208 /	611.1	1.0	0.8	111	0,1	JU, -			-	10	-	<del>                                     </del>		<del>                                     </del>	-		<del>                                     </del>		<b> </b>
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		- culorite - moderate to strong	_			ļ	ļ	ļ	ļ						<b> </b>			ļ		-	ļ <u>.</u>	├	-				<u> </u>		
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						Rustar	70	45	2933	2117	214.7	3.3	0.5	16	0.2	+r		<u> 3</u>	5	14	58		L	L				<u> </u>	
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		GEOLOGIC DESCRIPTION										<b></b>	-		_	MIN	ERAL	IZAT VEIN	IUN_ S	_				<u>نن</u>	76	A22A	- (	B	
FROM	TO		og F	ROM	TO	TYPE	TCA	ХТСА	SAMPLE NUMBER	FROM	то	Py	Cpy	KeQ+	Cal	Corp		No. Veln	Cun thk	No. Vetn	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	AZZA	Cu	Ag	Мо
		K-SPAR MEGACRYSTIC PORPHYRY / QTZ-FEOX REPLACEMENT BRECCIA	$\vdash \vdash$	-		<b></b>		<del> </del>		<del> </del>		╁			<del>  -</del>	-	<u> </u>		-				_						
		PORPHYRY / QTZ- Fe Ox				RQ-Py	70	150	2934	214.7	2165	8.0	0.4	18	-	-				5	18								
		REPLACEMENT BRECCIA	П									1			П														
		(CON'T)				1	1			1		1	1			1													L.
									2935	216.5	218.	0,6	0.4	1	0.6	1.0												L	
		# 216.5-218.3 - 90% QUARTZ VEIN	$\Box$			1				1		1	1																
						Po-Py	70	30	2936	5.812	221.3	0.7	0.6	ıß	0.3	0.2				10	60								
		- core is oxidized (1454) on					70	30				1																	
		- core is oxidized (custy) on procture surfaces.					20	40																				I	
																												L	
						Pa-Py	70 40	55 40	2937	221.3	224.3	0.6	0,4	16	0.1	0,1				13	72			!					
			$\perp$			1				ļ	<u> </u>	L_			<u> </u>						<u> </u>	$\sqcup$	<u> </u>	$\sqcup$	┌┤			-	
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			$\vdash$			10.P4	90	30	2939	227.4	230.5	0.3	0.4	14	0.2	10.1			<u> </u>	14	No.	$\vdash$		$\vdash$	<b> </b>		-	-	┼─
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			$\vdash$			Po.Py	85	40	2940	230.5	273.5	0.6	1.4	12	0.3	0.4	0,02	1-		13	76	<del>                                     </del>		┟─┤			<del>                                     </del>	-	┼
			⊣			<u> </u>	70	20	<b></b>	├		├				<del> </del>	-	<b>├</b> ─┤		-			<b> </b>					├	┼─-
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Ĺ		GEOLOGIC DESCRIPTION				ST	RUCTUR	Ε		SAMPL	ES 23		MIN	ERAL	2				PAK	NE.	Qz-	Py	[CAR]	В		-14	AZSA	YS		<b></b>
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<b></b>		QUARTZ - FEOZ REPLACEMENT	╆		+	T	20.0.	85	30	2943	204	242 6	1.3	04	10	101	1		╁	┼─	10	123	<del>                                     </del>	<del> </del>	<del>                                     </del>	$\vdash$		-		<del>                                     </del>
t : t		Briecas (CONT)	+-			+	D.Py	70	40		-27.0	2-2-0	1::-	7:7	ļ <u></u>	10.,	†- <u></u>	<del> </del>	<del> </del>	+	1	1			<del> </del>				† <b>-</b> -	1-
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		Called PQ-Py have				+		40	30		İ		<b>-</b>	1		1			<u> </u>											
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		are not true veins in				1				i			· ·		İ				Ĭ									<u></u>		
		this section.				17	3- P4	85	60	2945	245.7	2487	2.5	1.0	ь	44	14	+			11	170		Ĺ					1	_
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		+ 251.9-254.9 - 2 QTZ- Py uns	T			T P	Pa- Ry	70	10	1947	251 9	2549	4.0	0.5	2	0.2	<u>a1</u>	tr	2	4	7	181								
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FROM	TO	·	88	FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Ру	Сру	Kell	Cal	Color		No. Veln	Cum thk	No. Veln	thk \	No. √ein	Cum N	vo. /ein	thk	Au	Cu	Ag	Мо
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		WARTZ-FED, REPLACEMENT				Ry	75	Sb	2952	267.5	270.1	4.6	0.6	7_	0.3	0.5		2	5	3	200			<b></b> ⊦				-	
<u> </u>		BRECCIA / SHEETED				<u>'</u>	50	ક્ર																				<b>├</b>	<b></b>
		GUARTZ - PN VEINS,				PQ. Pu	70	75		]									L			$\rightarrow$						ļ	ļ
		(COUT)				)	45	25							<u> </u>							_	$\rightarrow$					↓	<u> </u>
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		267.0-270.1 - 90% QTZ- QU	Π			20-84	70	40	2953	270.1	273.1	1.8	0.3	10	0,1	+4				8	121	$\rightarrow$	$\rightarrow$					<del> </del>	
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			$\top$				20	30										l											
	-	90% of counineralization	1			Pu stur	10	100									`	Γ											
		is in stringers, micro-	+			134		<u> </u>									• •												<u></u>
<b></b>	1	tractieres . 10% dissemine	W.			Pa.Py	70	10	2956	279.7	262.2	3.0	0,6	14	40	h				12	111								
	†		+-			9	45	45	15,50			<b>†</b>		1				1											Ι.
	†··		-†			<b></b>	20	45	†	ļ		t			† <del></del>			†		1								I	Ι
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<b>—</b>	<b>†</b>	4 782.2-7834 - OTZ-PA-COU	1			We-Py	70	100	2957	287.2	285.3	2.5	1.4	9	0.2	0.2			<b>-</b>	7	173			(	8				
-	<u> </u>	+ 282.2-2834 - OTZ-Py-Cpu VEIN	1			PO-P4	70	20								'													
<b>.</b>	† ` ` `	- 1.5 - 2% Cpy m	1-			13.4	70	70	1	' '		1		ļ		1			1										
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FROM	το		S <sub>e</sub>	FROM	τo	TYPE	TCA	%ТСА	SAMPLE SAMPLE NUMBER	FROM	ΤΟ	Ру	Сру	KeQ+	Cal	Coro	Нο	No. Vein	Cum	No. Vein	Cur	No. Veln	Cum	No. Vein	CUM	Au	Cu	Ag	Мо
		OVARTZ - FED, REPLACEMENT							2960	291.4	294.4	3.6	0,4	14	tr	0.1				8	54								-
		BRECCIA / K-SPAR MEGA- CRYSTIC POEPHYPY	$\vdash$			Wapy	70	100	2961	2944	292.5	1.8	0.7	14	₩	0.4	$\vdash$	┢		10	80	$\vdash$	-	1	7			<del>                                     </del>	<del> </del> -
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		- OTZ-FEQ replacement gradually fades to 95% porphyry.																											_
<b></b>		faces to 45% porphyry.	H			<b> </b>	<del> </del>	<del>                                     </del>		<del> </del>	ļ	<del>                                     </del>			<del> </del>		$\vdash$	$t^-$	$\vdash$	-									
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2999	300.5	- QTZ - Py - Cpy - MO VEIN				<u> ೪೬</u>	45°	ļ	2963	399.9	30.5	100	80	!	1.2	2.5	1.0	ļ		<u> </u>	<del> </del>	<b></b> .		ļ			ļ	<del> </del>	
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-	ļ	- QTZ - Py - Cpy - MO VEIN - 5cm py e UC - 2cm bland of cpy - 1cm bleb C My @ LC	H			<del> </del>	<u> </u>	<del> </del>	ļ	ļ	<b> </b>				ļ			<del> </del>				<del> </del> -							
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L		GEULUGIC DESCRIPTION				STRUCTUR	E		SAMPL	ES		MIN	ERAL	2.				PYR	YE.	Qz-l	Ру	CARI	1	23.5	·N	ASSA	YS		•
FROM	TO		8.	FROM	Ta	TYPE	TCA	%TCA	SAMPL SAMPLE NUMBER	FROM	TO	Ру	Сру	est	Cai	640	Mo	No.	Cum	No.	Cum	No.	Cum	No.	Cum	Au	Cu	Ag	Mo
$\vdash$			183		_	+	+-	+-	NUMBER	<del> </del>	-	<del>                                     </del>	-	<u> </u>	┼	<u> </u>	<del>  ``</del>	\ 6 IV	THE	Vein	THE	vein	UNK	vein	UNK				$\vdash$
$\vdash$		K-SPAR MEGACRYSTIC			$\vdash$	PQ-14	70	120	2945	3034	30h.h	10	0.3	4	0.2	tr	+~			8	53		-						
<b>!</b>		PORPHIRY / SHEETED			<del>                                     </del>	+	45	57)	2965	1-70	~	1	1	<del>  `</del>	1	-	<u> </u>			<u> </u>		1		-					-
		QTZ-PY VEINS	1		1		<del>                                     </del>	1				<del>                                     </del>																	
1					<del> </del>	Pu. Ty	45	100	3966	306.6	309.0	1.5	0.5	6	tr	h	tr			3	ळ			·					
		- Chlorite mod. to strong.				1			1																				
		(especially in ore-py Jewlots)										Ŀ																	
		' ' '				Q-C	20	100	2967	309.0	311.7	3.2	0.4	11.	tr	۲٧.	4			6	દ્ધ		2						
		309.0.311.7 - 3 QZ-Py VENB - mod. Chl., green			<u> </u>	PO.Py	70	30		ļ		<u> </u>		Ь—	<b> </b>	<u> </u>	<u> </u>				L			$\rightarrow$					<u> </u>
		- mod. Chl. green	Ш		<u> </u>		45	70				L	ļ	ļ	igspace	ļ		L		_	<u> </u>		$\rightarrow$						
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		LC 450			-	x-C	50	100	2968	3117	315.4	3.5	0.4	12	10.6	0.5	1			ь	43	1	7						├
			<u> </u>		ļ	Po-Py	50	100	<b> </b>	ļ	<u> </u>		<del> </del>	-	├	<u> </u>	<u> </u>							$\rightarrow$	$\dashv$				
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		321.5 - 321.8 - QTZ - py Vein			<del> </del> -	PY SEV	70	75	197.7.1	2010	300		•	1'	0.0		1.	- <i>T</i>			1-1			· · · - † ·					
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		324.3 - 325.4 - HAFIC DIKE	Н				<u> </u>	<b>†</b>				T			1														
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		GEOLOGIC DESCRIPTION	ı			STRUCTUR	E		SAMPL	ES		MIN	ERAL	S	<b>.</b>		•	PAK	(IE	Qz-I	У.	CARI	3	ãz	Py	ASSA	YS		<b></b>
FROM	TO		ě.	FROM	TO	TYPE	TCA	XTCA	SAMBLE	FROM	TC)	Ру	Cpy	. Ot	Cal	COLA	MO	No.	Cum	No.	Cum	No.	Cum	No.	Cúm	Au	Cu	Ao	Me
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		K-SPAR HEGACRYSTIC	$\vdash$		<del> </del>	Pa. Pu	70	10	2973	3254	327.3	1.1	0.8	5	tr	tr	0.02	1		5	44								
· <del> </del>		PORPHYRY (CONT)	$\vdash$		<del> </del>	1.4.4	50	60	† <b>-</b>	1000		T	1	1	1														
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		325.4-325.7 - BLECCIA 3CAL E	T		1	<b></b>				1	<u> </u>		†	1		T													
		contact with duke	✝		$\vdash$	Pa.Py	70	50	2974	327.3	330.3	3.0	0.8	10	0,2	0.4	0.03	1		8	57								1_
		- good cp mineralization	1			1	50	45	1	1		1			1												<u></u>	<u> </u>	$\perp$
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						70-Py	70	10	2975	330.3	333 3	3.5	0.4	10	0.1	0.2	-			7	32						L		_
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		333.3-336+- Py seinler n 75%				Py volt	70	100	2976	333.3	3464	5.0	0.6	12	tr	to	tv	4	20	5	79					ļ			1_
		py )25% Q1Z				Pa-Py		50				<u> </u>		<u> </u>	<u> </u>	<u> </u>		oxdot	_	<u> </u>						<u> </u>	ļ	↓	╀
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			_	ļ	<b></b>	10.Py	70	60	2977	336.4	339.4	3.0	0.5	10	1~	110	0.03	<b>├</b>		4	62								-
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	<u> </u>	GEOLOGIC DESCRIPTION				STRUCTUR	<b>■</b> E		SAMPL	ES		MINI	ERAL	s		MIN	ERAL	YEI PYRI	ICIN IS	ioz-f	<b>-</b>	CARB	W.	117E	ASS	2YA		·
FROM	TO		24	FRO	м то	STRUCTUR	TCA	ХТСА	SAMPLE NUMBER	FROM	TO	Ру	Сру	Kelit	Cal	Coto	Mo	No. Veln	Cum thk	No. Vein	Cum thk	No. Vein	Cum No thk Ve	Cur	Au	Cu	Ag	Мо
		K. SPAR MEGACRYSTIC	H			Po-P4	70	15	2982	351.4	354.5	1.6	0.5	12	0.1	tr	tr			9	100			_				
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		<1 mm Value MAGNETITE. QTZ	H			<b></b>		<b>†</b>	3010	434.7	4277	-	tr	5	0.2	+~	1					<u> </u>							
	1	WELLERS / low To other count of	┪			<del> </del>	<del> </del>		1	<del>, , , ,</del>	1361	†	+	+ -	1			<del>                                     </del>	-			<del> </del>		t					
		colate laddering by	H				<u> </u>	<del> </del>	1	<del> </del>		<b>†</b>	†	_	<b> </b>	_	<del> </del>	t					<b>-</b>						
		Carry tableing	ŧ.			<u> </u>	<u> </u>		<u> </u>	<u> </u>		<u> </u>	· · · · ·	<u> </u>	<u> </u>			<u> </u>	$\vdash =$										

FLT e 437.0 - 437.8 / - BLOKEN CORE - STEONE CHLORISE

	GEOLOGIC DESCRIPTION				STRUCTUR	-		SAMPI			MINE	DAI	<u> </u>	-			YEIN	\$	0,-5		CAPT	11	WIT	7	ASSA	YS		
ROM TO		89	FROM		TYPE	TCA	ХТСА	SAMPLE NUMBER	FROM	מד	Ру	Сру	4e0+	Cal	Coto		YEIN PYR No. Vein	Cum	No. Vein	Cum	No. Vein	Cum thk	No. Veln	Cum thk	Au	Cu	Ag	۱
		$\perp$		<u> </u>				<b>!</b>			-																-	+
	QUARTZ - FEO. REPLACEMENT	╀-		<del> </del>	20.0	3-		25	437.7	4407	5.7		10	0.4	54				4	3.5						<del> </del>		+
	Breccia (CON'T)	╁		├	PO-Ry	20	1100	3011	731.[	440./	0.4	0.6	10	0.4	0.4				4	30				$\neg$		<b></b>	<del>                                     </del>	+
	- chlorite alteration is strong	╁	-	<del>                                     </del>	<u> </u>	-	<del>                                     </del>	<del> </del>	···-								-					-				<del> </del>	1	+
	A STORY	T			Bx/shea.	UC	45	3012	440.7	443.7	2.5	5.0	4	۵,2	-			_					2	6				I
	- biolite " is modifo					بد	7																				<u> </u>	4
	Strong (stringers)	$\perp$			WW Py	45 25	30									_												+
03/441/	Notes a Second Learning Tools	╁	<del>                                     </del>	ļ		25	70		-			-				-					$\vdash$					-	<del> </del>	+
0, / 441.5	HEALED BEECCIA/SHEAR ZONE	╁	<del> </del>	<del> </del> -	<del>                                     </del>	<del> </del>	┼		<del> </del> -		$\vdash$		-			$\dashv$							-			<b>-</b>		+
	· HIGHLY SILICEOUS, AK GIRDA	$\top$	<u> </u>																								Ī	Ţ
	(chlorite?) matrix with 5%									7														_				+
_	Jy. Rounded & angular atz	$\perp$			ļ	ļ	ļ								_	_				_								+
ام مون	of tracments with "laddered"	╁	├—		<del> </del>	<u> </u>	ļ	<b>_</b>				<u> </u>			$\vdash$	$\dashv$			-	_							<del>                                     </del>	+
	calcate strucers	╁		<del> </del>	Po. Py	42	70	3013	4437	441	1	0.3	10	0.2					4	G2			3	7				+
	- very hard (R6)	+			PW- P4	20	80	5013	44.5/	440 0	0.5	0.,	10	U, L	0.,				-	10			~				<u> </u>	†
	<del> </del>	╁╌	<del> </del>	├	WW- Py	45	100		<del> </del>						-													†
	· · · · · · · · · · · · · · · · · · ·	╁╴		$\vdash$	124.19	7.3	1,00	<u> </u>				_																T
_	<u> </u>	+-		<b> </b>	<del>                                     </del>	<del>                                     </del>	$\vdash$	<b></b>																				Ι
	4 purite is diffuse viinlets	+			PQ. P4	40	50	3014	4468	449.9	1.5	0.3	14	0.2	0.1	4	2	3	7	60								$\perp$
	1' = 75% public) @ 90° TCA				,	20	50																					4
	Y' CLITTING Pa-Py voinlets. Not	·L							<u> </u>																			+
	true veins or structures.	1	<u> </u>				-		ļ			ļ	<u> </u>		$\vdash$	_	<del></del>					_						+
	Miles No. 0 442 Co. H.	+	ļ	┼—		<del> </del>	<del> </del>		<del> </del>		-						-				-						<del>                                     </del>	+
	K trace Up @ 447.5 as then <1 mm Stringer in PR- By stringer	+	-	<del> </del>	-	<del> </del>	-	<del> </del>	╁──			-				-			_				_					+
	- I was 2 lawren on 14-14 3 march	+	<del> </del>	<del> </del>	<del>                                     </del>	<del> </del>			<b>†</b>																			Ī
	+ 448.9 5 cm 2010 of	1	<b></b>	1				1																				I
	COU (n 22/0) in diss				न्धि-पि	40	\$	3015	4499	4529	2.1	03	15	0.2	+4				5	46								4
	+ bleb.	L			,	20	So																			L		4
		1		<u> </u>	<u> </u>	<u> </u>	ļ	ECH	<u> </u>												$\vdash$	_				-		+
452	9 EOH	+-				ļ			├	ļ	<u> </u>							_									-	+
1		1	<del> </del>			-	ļ	-	<del> </del>																	-	-	+

## **HOLE 1220**

11842.89 NORTH

25600.05 EAST

**496.781 m ELEVATION** 

LENGTH: 369.1 m

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	l		Г					_				<u> </u>						IZATI VETN						M 111.	TE			-	. —
FROM		GEOLOGIC DESCRIPTION		I	rS	TRUCTUR	E !	l	SAMPL	E2	1:	MIN	ERAL	. Z		ام ا		PAK	YE_	Oz-	Py	CAR	B	az.	Ň.	ASSA Au	YS	T:	1.5
, KOK	70		1	FROM	10	TYPE	TCA	%TCA	SAMPLE NUMBER	FRUM	TO	Ру	Сру	K.0.	Cal	Coch		No. Vein	Cum thk	No. Vein	Cur	No. Vein	Cum thk	No. Veln	Cum	AU	Cu	Ag	Мо
-	20.1		<u></u>																	L								L	
10	25.6	CASING	ł		<del> </del>	80. Py	. 50 .	100	2747	25.6	28.6	1.0	0.9	1.3	2.0	1.2		<b> </b>		1.	100								
25.6	45.0	ALTERED SILTSTONE / WACKE	1-		<del>                                     </del>			<b></b>		<del>                                     </del>		$\vdash$		<del>                                     </del>	<del> </del>					╁	_			Η					
		TRANSITION ZONE	† "						274B	286	31.8	1.2	0.5	2.0	15	12										,			
										Ī				Ĭ										ļ ļ					
		- HEAVY K-SPAR ALTERATION								- 6	24.0	2 -	2					-			-		$\vdash$						
<b>}</b> <del> </del>		CORE BROKEN WITH RUSTY	ļ						2749	31.8	34.8	2.2	0, 6	2.2	2.6	1.0		1				<del> </del>							_
1		STAINING ON FRACTURE SURFICES	$\vdash$									<del>  -</del>	-	<del>                                     </del>	<del>                                     </del>			$\vdash$			_	$\vdash \dashv$			_				
		- Co mineralization pridiminate			-				2750	34.8	37. R	09	0.9	3.0	2.1	14	_												
		disservinated				<b></b>				7	3,1.0		-																
											·																		
		- numerous calcula vivis .							2751	37.8	41.1	3.1	0.7	2.3	1.1	0.6								L_	_				
		(asperally leached our)																		<u></u>									
		are present C 50° TCA				PQ- Py	ಉ	100	2752	41_1	44.1	1.0	0.8	/	1.3	1.1				1	17								-
			L									L		<u> </u>		$\sqcup$		$\sqcup$										<b></b>	· ·
		- mmor chl alteration + ser.	↓_								4.	١.,	<del> </del>	ļ		,													
	$\dashv$	ov a 202 Ovid 100	$\vdash$						2753	44.1	47,1	1.8	1.2	1.2	0.7	7.8				-					-				
1		26.3-27.3 - Oxidized QTZ py	-						ļ			<del> </del> —		<del> </del>	-	$\vdash$				-	-				-				-
<del>     </del>		VEW.	$\vdash$						2754	421	So.l	0 0	0.5	1	0 <	0.7	-	$\vdash$			_	-						·	
45	1.0	LESS INTENSE KSAR ALTER.							C DT	7.1.1		۰۰۰	1	_ع_ا	23							t ·†							
	···· /	- WACKE DK GREY	H							<del> </del>			_																
		- Brecciped - transments 0.1 -							2755	50.1	53.1	0.8	0.1	3	0.2	1.0													
		2 cm. subjounded.																				<u> </u>			_			<b></b>	
		silerous.											L	L	_			$\vdash$				<b> </b>							
		- mor former carcile yourse	4_		<u> </u>				2756	23.1	55. B	2.0	0.2	3	0.2	0.8								ļ <del>ļ</del>			<b>!</b>	ļ	
$\vdash$		- consent decreases down	<u> </u>			ļ		L				<u> </u>		<b> </b>	ļ	-		$\sqcup$											
-		hole.	<b>!</b>		ļ	ļ				100		L-,	1	٠, ٠				<b> </b>											
			-			ļ			2757	£5.8	588	11.6	0.2	3	0.8	0.5	_	<b>├</b> ─┤		-	-			-	-				-
$\vdash$		58.6-70.7 Cure badly broken				ļ			·	·		ł	ļ							-		-							
$\vdash$		1-5 cm sharp contacts			-				2758	(2)	1.10	14	02	-	01	04		╂╾┼		-	-		-	$\vdash$					
$\vdash$		· carb. staving or fracture	4-	<del> </del> -					2130	35.Y	01. 3	11:3	0.3	4	9./	47				-		1							
		Suraces. Little crine	╁					-	<del></del>	<del> </del>					-							$\vdash$							
		OLIV.	<u>+-</u>		<del> </del>	<u> </u>				· · ·			1	<u>.</u>							<u></u>								

		GEULOGIC DESCRIPTION	'		-	STRUCTUR	ξ		SAMPLE	S		MINE	ERAL	S				Y LIN	EI	nz-P	ý	ÇARD		02:	Pu	ASSA	YS		,
M	τn		8	FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	10	Ру	Сру	4.0°	Cal	Coco	Мо	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Veln	Cum	Au	Cu	AQ	Мс
3 3	82.5	ALTERED GPEYWACKE							·759	61.8	64.8	0.6	0.8	5	į,s	1.0													
+		- resdicate to vicinate KSFO1	$\perp$						2760	4.8	67.8	0.6	0,6	4	0.6	1.)	+4												1
+		- inggy ex-calcure veinlets - Tr HO a 65.4	- -		-			<u> </u>	3=.	120	20.7	2.4	0.5		00	00				_									<del> -</del>
+		- 14 NO 16 02.4	+	ļ		112.2			1		70.7													1	15				
‡		12.5 - Cpy increasing manule	1		<u> </u>	no. by	50	100	2762	7.0	73.7	1.1	0.6	4	0,6	0, 3													+
-		Also some superache	+	-		<del> </del>		<u> </u>	2763	73.7	76.6	0,8	1.7	5	0,2	0.4				_									F
-		2-7- Car Ox levelles	+			-		<u> </u>	2764	76.6	79.6	0.5	0.7	5	0.7	0.3		$\dashv$	$\dashv$	1									-
_		borrite chalcocite	1	<b>—</b>	-	א אייים	50	- 100	2765	79.6	80.S	30	0,4	7	2.2	1.4		1	"	1 6	90								$\perp$
F		JILLING CONTRACTOR	1		1	The state														$\dashv$									$\vdash$
-		BE GEEN - BACK	<u> </u>	-				-	2766	છે <	82.5	0,8	0.9	ø	2.0	1.0				-									
		82.5-62.5- angillic shops	1	-	-			-	2767	87.5	85.5	2.5	1.2	4	2.0	22				-									F
_		30res with 3% CDU	1	ļ	1	<del> </del>		ļ						-															F
F		704	1											_															F
-			#	<u> </u>	-				2768	85.5	8C.5	1.0	0.8	3	70	1.4													-
-			1	<u> </u>			_		2769	58.5	90.6	0 6	1.0	Z	10	0.7			$\dashv$	1									F
-			#		1			-										_											F
			1						2770	90.6	93.6	0.7	0.7	2	0.8	υ.9		$\dashv$											F
+				<del> </del>			ļ	<b></b>	ļ	L									_			-							<u> †</u>

													(							1					-				
ĺ			Т													MINE		IZAT.			***					7			
1		GEOLOGIC DESCRIPTION	1		S	TRUCTUR	Ε		SAMPLE	2.3		MINE	ERAL	S				PAP!	ŶΕ.	Qz-F	7 · ·	CARI	B	I		ASSA	YS		
FROM	TO		8_	FROM	TO	TYPE	TCA	XTCA	SAMPLE	FROM	TO	Ру	Сру	O+	Cal	8	1	No.	Cun	No.	Cum	No.	Cum	No.	Cum	Au	Cu	<b>AQ</b>	Мо
<b></b>			ᆵ				_	ļ	NUMBER	<del> </del>		-	-	K-	$\vdash$	100		Vein	thk	Vein	thk	Vein	thk	∨ en	The				<del></del>
3			╀		<u> </u>	ļ		<u> </u>	ļ		├	<u> </u>										$\vdash$		├					-
À 5	119.0	K-spar altered Greywacks	-						2771	03.	ļ	ابتا		· <u>-</u>	~									<del> </del>			ļ		_
	-		╀						2771	73.6	46.6	0.6	1.4	3	0.6	0.0						_	<del> </del>	<del>                                     </del>					
		- whense k-spar booking - curk sill body bloven	-						<u> </u>	· ·		-			<del> </del>	-						-	<del>                                     </del>	<del>                                     </del>					<del></del>
		2 - 10 cm	+			····			2772	Oh h	90 L	0.9	1.5	4	0.3	0.5						_							
		- Cov contert up to 3% e	╁╌		<del> </del>	<del> </del>		<del> </del>	- 1, 2	70.0	772.0	·-·-	-											T					
$\vdash$		96.6	✝								<del> </del>			<b>—</b>		$\Box$								1					
		- minor Coicité vemlets	+-		<del> </del>	<del>                                     </del>		<del> </del>	2773	99.6	102.6	1.2	0.9	4	0.4	0.8								1					
	-	(< 1 cm) mostly dissoived	†-		<del>  .</del>		_	1	<i></i>	17.5		<u> </u>		<u> </u>	<u> </u>														
		TE TOM MOSTLY ALSSO VED	╁╴	<del> </del>	<del>                                     </del>			<del> </del> -	t					<del> </del>	†	†		1				1		<b>†</b>					I
<b></b>		- unggy.  minet off py virialis  (sleadury broken	+				<del>                                     </del>		2774	107.6	105.6	1.4	1.4	4	02	DZ			$\vdash$					1					
		K landy on land gen	╁╴		<del> </del> -	<del> </del>	<del> </del>		1	,,,,,,	-	<u> </u>	İ	<del>- `</del> -	2.0	15.5		t						<b>†</b>					
		- cu 90% diss. 10% in	+	<del>                                     </del>	<del> </del>	<del>                                     </del>		<del>                                     </del>	<del> </del>	<del> </del>	<u> </u>	-	1								Ì								
		one of delias actions	+	<del> </del>	<del> </del>		<del> </del>		2775	105	1077	12	1.8	2	0.4	0.3					$\overline{}$			1					
<b>-</b>		9+2- in devides of stringers	┿	-	<del> </del>		<del>                                     </del>		61.12	100.00	101.1	<u> </u>	1	-	-	1													
			╁┈			<del></del>	<del> </del>	<del> </del>		·			<del> </del> -	t	†	<del>  -  </del>						1		†					1
	-		╁	<b>-</b>	<del> </del>	PQ. PA	4=	25	2776	107.7	110.7	10	1.5	4	0.1	0.4				2	74	$\vdash$		<b></b>					
			╁╴	<del> </del> -	<del> </del>	1 4 5	0-10	24	-1-10	1	1	1	-	<del></del> -	1			1				1		1					
$\vdash$			+		<del>                                     </del>	<del>                                     </del>	0-10			<del> </del>	<del>                                     </del>	<del>                                     </del>	<b>-</b>	<b>—</b> —	<u> </u>			$t^-$				1							
$\vdash$			+	<del></del>	<del> </del>	PQ . Py	70	30	2777	110.7	113.7	1.5	1.4	3	1.2	0.8				10	24								
$\vdash$			╁	<del> </del>	<del> </del>	1,4.14	50	20	- ,	1.0.1	<del>                                     </del>	1		1	<u> </u>			I				1							
<b></b>	-		+		<del>                                     </del>	<u> </u>		50		<del></del>		t	<del> </del>	t									<u> </u>						
<b></b>			+	1		4.12.1	100.00	-	1		1	<del>                                     </del>		<u> </u>	1			i –											1
		4 113.7 -1167 - TAIC ON FONCTURES	+-		<del> </del>	PQ. Pu	مه	100	2778	113.7	116.7	14	1.2	4	0.4	10		1	<b></b>	1	16	1	1	1	1		, , ,		
		10-15 TCA	+-		<del>                                     </del>	(-50%	-	1.00	1 - 1 - 1 - 1	1		<del>                                     </del>		† '	1	1													
_	<del>                                     </del>	10-13 , 05	+	<del>                                     </del>		PY	t	†	<del>                                     </del>	<b>†</b>		<b>—</b>	<b>1</b>		T			1			_								
	<del>                                     </del>		+	<del>                                     </del>		<del>                                     </del>	<del> </del>	<del>                                     </del>		<del> </del>	1	$\vdash$		-	$t^-$			1				1							
	*	119 - X-spax alteration is	+	$\vdash$	<del>                                     </del>	Pa-Pu	70.80	20	2779	114.7	1107	1.3	1.0	3	2./	1.6		1	<u> </u>	5	76	<u> </u>	1	1	1				
		auminished ( u 25%) Cpy	+	<del> </del>	<del> </del>	rairy	20	20	15.1.	1,0.	1	† <del>``</del>	†' <del>'</del>	-	† <del></del>	1				_	<u> </u>	1			1				
	<del>                                     </del>	ralus recreasing as well	+	<del> </del>	<del>                                     </del>	<b>+-</b> :	20	50	<del> </del>	<del> </del>	<del> </del>	t	<del> </del>	<b>†</b>	T	<b></b>		1					1	1	1				1
-		ATMIN CHANGE OF MICH.	+		<del> </del>	<del>                                     </del>	10	10	<del></del>	<del>                                     </del>		<del>                                     </del>	<del>                                     </del>	<u> </u>	1	$\vdash$		t —		<b></b>		1		1					T .
	<del> </del> -	- chl & bio & sev weak	+-	<del> </del>		<del>                                     </del>	۱ <u>.'۷</u>	Į. <u>'</u>	·	<b>†</b>		t :	1	t				t	_			1	†·	1			!		1 :
-		to mederate	+	<b></b>	<del> </del>	R-Pu	70	40	2780	119.7	122.5	08	0.9	2	1.4	1.0		<del>                                     </del>		5	67	1		†	1				
	<del> </del>	to moneigie	+-	<del> </del>		+.A.TA	50	40	1 20	1.1.7.1.	+ ''	1		-=-	1	1		1-	t —		1	$\vdash$	1	1	T			l	
	-		+-	<del>                                     </del>	<del> </del>	<del> </del>	10-20		<del> </del>		<del> </del>	1		<del> </del>	+			<del>                                     </del>				<b>†</b>	<del>                                     </del>	1					
			<u> </u>			<u> </u>	100	1 20	ł ———				<u> </u>		<u> </u>	· <del> </del> · · · · - ·		<u> </u>						+	<u> </u>		<u> </u>		<u> </u>

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		GEULOGIC DESCRIPTION				TRUCTUR	E		SAMPLE	2.		MINE	RAL	2				<b>AAA</b> B	1	Qz-P	Y	<u>[CARI</u>	9	42	Py	ASSA	24		<b>,</b> -
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		- Phyllocylicates prosent m	Ц			<u>'</u>	27	30	ļ	1	ļ			ļ			<u> </u>	<b></b>			-	-	├	₩	-	<b></b>	├	├	<del></del>
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			Ш		ļ	Pu. Py	70	Su	2808	202.7	204.9	2.4	0.8	6	1.8	0.8	tr	<u> </u>		3	127	<b>├</b>	₩	<del> </del>	├	<u> </u>	├		+
		- Veins 70.25 m ch 2-4%	Ш			•	Ω	20		ļ		ļ	ļ	ļ	<u> </u>		<u> </u>	<u> </u>	<u> </u>		<b> </b>	↓	┼—	<del>↓</del>	<del> </del>	<b> </b>		├	<del></del>
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			Ц			PD- P4	70	40	2809	204.9	207.0	4.2	0.2	8	76	1.0		<u> </u>		7	10		<del> </del>		<b> </b>	<b> </b>	<del> </del>	<del>-</del>	┼
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		K span alteration still intense	$\sqcup$		<u> </u>	Pa. C.	70	50	2812	211.0	214:0	3.6	0.6	16	0.3	11-1	0.02	1—		-		<del> </del>	-	-	-		<del> </del>	<del> </del>	<del>                                     </del>
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١.	ı	GEOLOGIC DESCRIPTION	L.			TRUCTUR	Ε		SAMPLE	S		MINE	RAL	<b>S</b>	,			PAKI	Έ,	Qz-I	Y	CAR		यः	P4	A27A	75	т	r.::
FROM	TO		89	FROM	TO	TYPE	TCA	XTCA	SAMPLE	FRUM	TO	Ру	Сру	K.04	Cal	Cock	Mo	No. Vein	Cum	No. Velo	thk	No. Vein	thk	No. Veln	thk	Au	Cu	A <sub>Q</sub>	Mu
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			╁			70. Py	70	50	2817	227.0	230.1	0.8	0.4	1	1.2	0.8	17	┼	-	В	113	$\vdash$						1	<del>  -  </del>
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		- no sulphide ninevalization	+	<del>                                     </del>	<u> </u>	<del>  ~</del>	_لع	1	<b>†</b>			1	t	1	<u> </u>	T													
		- no sulphide ninevalization 30% Buy GTZ				Dir Py	70	60	2822	239.5	242,3	9.9	0.7	12	0.9	1.1	$\prod$		30	14	96						L	<del> </del>	-
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2468	2411	Pyrite Vain - badly brusian.	1		-		20	10	ļ	—		<b> </b>		-	-		_		_		_							+	
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		KSPAR MEGACCISTIC POFFING (WIN'T)							2823	242.3	244.7	1.3	0.6	1	0.3	0.6	+												
242 3	744 7	ANK DUARTE VEIN	-			1JC	60																						
44.3		6238.4 - 1cm Cpy in carb.				لـ د	65										$\Box$							ļ					
		blub.	╁			DQ-14	70	45	28Z4	244.7	247.8	20	0.3	9	1.6	0.8	+	$\vdash$		10	3→	<u> </u>							
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			╀╌			اله جدور	6:	(M)	2825	247.8	263.8	25	0.6	7	2.0	0.6		-,	4	4	6							<del>                                     </del>	<del> </del>
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		alteration.	1_			PO. Py	70	80	2826	2528	2540	ن.3	03	4	5.0	20				12	90			├	-			ļ	
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			十	<u> </u>		wc	70	30	2827	254.0	257.2	2.0	1.0	4	1.0	2.8	+(	2	2	5	19	3	5	<b>-</b>				<del>                                     </del>	
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			╄		ļ	PQ. Ty	70	58	Z828	257.0	200.1	0.3	0,7	3	0.4	0.4	<u>+r</u>			10	36	-	3	2	-				<del>                                     </del>
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			1	<u> </u>	<del>                                     </del>	Pa-Ri	70	50	2829	260.1	263.1	5	0.3	5	0.4	0.6	+1			9	29							<u> </u>	<b> </b>
						]	50	25															<u> </u>	1	ļ	<u> </u>	L	<u> </u>	<b>  </b>
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		GEOLOGIC DESCRIPTION				TRUCTUR	F		SAMPI	7.7		MINE	PAI 1	2				X21	15.	10 1	5. ·	ICAP1	В.	1 05	* TE	ASSA	YS		
DH	10		84	FROM	τo	TRUCTUR	TCA	XTCA	NUMBER	FROM	τo	Ру	Сру	<b>60</b> †	Cal	رهرها	Mo	No. Vein	Cum	No. Vein	Cum thk	No. Velo	Cur	No.	Cum	Au T	Cu	Ag	1
																							<u></u>	↓				<u> </u>	4
	- 1	ROSPAR MEGACRYSTIC ROSPHYRY (COUT)		-		Por Cy	70	100	2830	263.1	500·1	15	0.6	6	רָס	3.0	+4			6	30	1	4	<u> </u>					
7	2691	Mt - Carb BLECCIA ZONE + QTZ																						1					-
7-1	267.4								2831	266.1	269.1	6.0	0.5	20	0.5	90	₩							↓					4
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4		- intense K-Spar flooding			ļ		ļ		1832	2691	272.1	1.5	02	7	44	02	*	ļ					-	┼	-		<del></del>	<del></del>	4
			-				<u> </u>		2833	222.	2750	1			1,							-;-	4	· <del> </del>					~
$\dashv$		269 1 - from 269.1 on.				carb	50	100	2133	2 (2.)	213.1	U. 7	**	-	7,4	0.8	_		_	-		<u>'</u>	<del>                                     </del>	+-	<del>  -</del>	_			٦
		absense of arz-py	-			<del> </del>			2834	226.1	2751	24	1	2	1,	A 2	_	-	-	-			-	+	-	<b> </b>	· · · ·		
-		· stringers ventlets Tuelins · very law diss Cpy				<del> </del>	<del> </del>		2037	213.1	2 10	9.7	''	-		9.4	Ť	-	_	<u> </u>	-	_	-	_					_
		only.		<del> </del>	<del>                                     </del>		<del> </del>		2835	2761	2813	06	۵.2	z	20	10	2.02							1	<del> </del>	<b></b> -			-
7						<u> </u>	<del>                                     </del>																						
_		274.0 - 4 cm carbonals	1		1	<u> </u>		<b></b>	2836	185	284.)	0.6	0.3	4	0.5	12	-							1					
		star with 1cm bleb																											-
		of thorspar.							2837	2841	287 1	0.6	0.1	7	0.1	0.2	-			_	L			$\perp$			ļ	<del> </del>	
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$\dashv$		276.0 - 2899 Core Ducoining	-		<del> </del>	700	20	100	2838	257.1	790.	0,6	,	-	٥.٢	1.0	-		<del> </del>	1	1			$\vdash$	-		<del> </del>		H
		less competent, Core	┢			Por	20	100	2835	20.1	701	امدا	2	10	0.1	03				-	100								1
		(15 Fubble (<5 cm)	╌	<del>                                     </del>		7 001	30	100	2 837	270 /	2.7,1	97	,			<b>5</b> ,	-		-	<del>  '-</del>	100	$\vdash$	$\vdash$	<del>                                     </del>	<del>                                     </del>				┪
-		262.7. 284.6	+			0.C	90	100	2840	2931	296.1	1,4	0.1	,,	w	2.0			-		<del> </del>	Ī	5	1					
-		2848-2845	H	<del> </del> -	<del>                                     </del>	1.0.12	10	-	100	100	- 10 .												-	_					٦
-		787.0-2571	<del> </del>		<del> </del>	Py VNU	an	ton	::84)	206.1	2.44.1	7	0.1	9	0.2	2.0		2	15	1	7	ï	3	1					
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		291.7 - 292.7 PINK GTZ - PY VN	1				1		1														Π						
		- core breezen to ser	1			Py Unit	45	100	2842	299.1	1.50	8	+	5	1.3	3.0		1	20			1	4	_					$\Box$
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		3171-305.5 SHEAR ZONE			ļ	wary	8	100	2.845	3-62 1	393.6	2.(	4	6	0.7	2.5			-				-	1	20		1		
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		foliation 60-65° TCA				Su o	70	100	28-4	303.6	3067	0.0	~	15	*	2.3			<u> </u>			-		13	12	· .	İ		
	-	WHITE QTZ New 160 303.4.3096 305.5-306.2- KPAR By	1	<del> </del>	<del> </del>	الآها- هم	1/0	130	<del> </del>	-	-	-	_					1-	-	_	_	-	<del>                                     </del>	+	1-	<del>                                     </del>	-	<b>—</b>	-
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		GEOLOGIC DESCRIPTION	1			TOUCTUD	_		SAMPLI			MINE	DAL		,		Į.	YEIN	Ş,	nt		- 		1 443	·II	ASSA	YS		-
FROM	TO		8	FROM	70	TRUCTUR	TCA	ХТСА	SAMPLE NUMBER	FROM	TO	Ру	Сру	•0+	Cal	Coto	f	No.	Cum	No.	Cum	No.	Cum	No. Vein	Cur	Au		Ag	Мо
		KENAR HEGACONSTIC ROPHYA	183			<del> </del>			NONDER											V 4 11.	VIVI	V (, n.							$\perp$
$\neg$		(حمالا)																									ļ		$\perp$
264	1605	DUARTZ - Py YEIN	$\perp$			UC	20		2845	3064	307.1	0.8	+7	_	1.0	0.3	_	_											╀
		1	$\perp$			LC	50	<b> </b>				-					$\dashv$						-					-	+
			+		·	Pa-Ry	20	20	2846	307.1	310.1	30	+1	-	0.4	DA	-+	-	-	2	24	2	12	<del>                                     </del>					1
	-					10-14	20	80	4070	30		5.0					_			-			_						
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						B ig	70	20	2847	310.1	313.1	1.5	1	10	0.8	44	_	_	_	7	28								╁
			$\perp$				80	60				_										ļ	-	-			<del> </del>		+-
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			+-	-		<del> </del>	-	10		-		$\vdash$			-	<del>}</del>		-				-	-				-		+
			+			Po. Py	70	70	2248	313.1	316.1	1.0	tr	13	1.0	m	-	-	_	11	38								
			+			10.14	50	30	16.04.0	3.3.1	3.4.	-			,		_	$\neg$	_	•									
			+				<u> </u>	130	<del>                                     </del>	<del> </del>																			
			1			Pu Stig	85	100	2849	316 .1	319.1	0.5	47	6	0.5	3.0		1	1	5	17	2	5						
						Py strq	80	SD															L						╀-
							40	Q										_									ļ		+
						Da. Py	80	80	ļ	ļ					_		$\dashv$	$\dashv$				<u> </u>	<u> </u>	-				-	+-
			+				30	20			ļ	-			<del> </del>							-	├	1		<del></del>	-	-	+-
			+	-		Pa-P4	70	50	2850	319.1	722.1	15	w	3	0.3	18	_			4	22		-						+
			+-		-	14:14	45	30	2030	13.1.	,,,,,	163		-	-	1.5	一	_		<u> </u>	-		1						
			+			<u> </u>	30	20		1			_																$\perp$
	+	Fus = 3199 1 cm gouge.	+	319		FLT	80	1		1																			╄
	4	FUE 321.3 1 cm doute.	T	321.3		FLT	80															L	ļ					ļ	┧
												L_			<u> </u>			_			_	_	-	-			<b>├</b>	—	+
			1			PO-PY	60	-	2851	322.1	325 !	0.3	4	5	0.6	0.3	_			7	27	<del> </del> -	<del> </del>	ļ			ļ	ļ	+-
			$\bot$	ļ		<b></b>	40	<del> </del>	<del> </del>	<del>                                     </del>	├	↓			-		-				-	├	┼		-		+	<del> </del>	+
		· · · · · · · · · · · · · · · · · · ·	+		<del></del>	00.0	<del>  -</del> -	+	2852	325.1	270-	10.0			07	04				2	16	<del>  -  </del>	+-	<del> </del>			<del> </del> -	1	+
			+	-		90-Py	70	90	15825	262.1	728.)	0.3	77	3	10.7	0.0		-		-	10	-	1	-				-	+
	*	FLT @ 32+95-3250 D.Oca	+	324.45	ציג	fur	50	120	<del> </del>	<b>†</b>	<del> </del> -	<del> </del>			<del> </del>			-				<del>                                     </del>	$T^{-}$	†			1	<b></b>	1
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	1	GEOLOGIC DESCRIPTION	ı									MINE						YEIN	S			TEXE	B	1.3 <del>1</del>	·**	ASSA	YS		
FROM		GEOLOGIC DESCRIPTION		FROM		TRUCTUR	L   764	T	SAMPLE		70				C 01	<u>اه.</u> آ		YEIN PYRI No. Velo	Cue	NO.	Cum	NO	Cur	NO.	C	Au	Cu	Aq	Мо
FRUM	ıu		189	FRUM	-	ITPE	ICA	ZICA	SAMPLE NUMBER	r Kum		ry	СРУ	رفي	Cui	Col		Vein	thk	Vein	thk	Vel	the	Vein	thk				-
																		$\sqcup$				_	↓	↓	Ш				—
		KSPAR HELACTYSTIC RAPHYRY									L <u>.</u>											<u> </u>	-	↓					<del> </del>
		(SON'T)	Г			Py	70	100	2853	328.7	33/.1	5	0.2	17	0.8	1.2		2	3	4	28	L	↓_	1_					_
328.7	369.1	HORNFELS SILTSTONE	Г			10 Py	70	60												L						<u> </u>			ļ
	COU	- MODERATE TO INTENSE K-SPAR.	Г			1	45	40														L	<u> </u>						
		- MODERATE TO INTENSE K-SPAR.	T																				<u> </u>						<del> </del> _
			Π	331.1	332.4	Q12 VN	80'		2854	331.1	333.0	3	0.1	10	1.2	0.1				1	3								—
		- approx 30% mt alteration																				L	1_	↓_					<u> </u>
		für the first 2 metres	Ī			Ī																							$\perp$
		gradually lives int down	Π			FD-P4	70	50	2855	333.0	3360	1.4	0.3	16	0.7	0.1				5	প্ৰ	<u> </u>	<u> </u>		L				1
		tile to a 10%	Π			1	Su	15														丄	<u> </u>						
			Π				น	35				Ι										<u> </u>	_	↓					<del>↓</del>
		- numerous gtz-struccis (1-20)	1															Ш				1	↓_	<del> </del>					-
		at various angles	Π			Pa. Cy	70	35	282	336.0	339.0	30	0.2	11	0.8	0.3		Ш		11	77	ــــــــــــــــــــــــــــــــــــــ	↓_	↓	1_				<b></b>
		(approx 50/metre.)	$\Box$				50	50								L				L		↓_	1	↓					—
		7	Г				ಬ	25								1						↓	↓		1				<del> </del>
		331.1-332.4 PINK QTZ . PY VEIN																		L		↓	<del> </del>	↓					<del> </del> -
		- INDISTINCT CONTACTS	Γ			10-14	70	60	2857	3350	342.0	2.5	U. 1	8	1.2	0.4				11	77	ļ	1_	1_					<del> </del>
			Γ				23	30				<u>L</u>										$\vdash$	<del> </del>						<del>-</del>
		_	Г				70	10							Ī.,	1. 1						1	1	1	ļ.,	,			1
		- Chloure · muderate	1	1	1	1	1	1	I	]							l	1	l	l		1	L	<u> </u>				L	_
			T	1		OC.	15	100	2858	342.0	345.	1.8	0.1	9	1.2	0.6				12	150	1	3	<u></u>	L				<b></b>
			†	1	$\vdash$	F12. P4	70	30			1	1																	
			T		1	1	90	30				Г										1		T			L	<u> </u>	
			1	1	<u> </u>		1					1	ļ		1			1				T							
			T		<u> </u>	Py	45	100	2859	345.0	348.0	2.0	0.3	10	6.2	0.2		1	1	9	18								
			T	1		116- Q	70	Su	1			1	1	<b>†</b>															
			†-	<b>†</b>		1 3	50	50			1	1-		1								1		1					
			T		<del>                                     </del>	<b>†</b>	1 30	155	<b>†</b>	1	<del> </del>	<b>†</b>		<u> </u>	1	1						1		1			1		
			✝	$\vdash$	<del>                                     </del>	P4	45	100	2860	3480	3<20	1.9	40	11	0.3	0.4		3	2	12	74	-		1					Ι.
			1	†	<u> </u>	w Py	70	50	†	- y - y -	1	Γ΄.	1	†''-	T	T'		T					L	L					
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			1-			1	1		1				Ľ.		Ľ.									L					-
	*	352.4-354.0 PINK 072-F4	T			710. Py	45	100	2861	352 0	344.	110	tr	5	1.4	0.6				3	160	2	1_	<b>_</b>	L.				4
		VEIN				1		1		T	T	Ī .	I																—
			T			1						Π												1					1
			土			1	1		t	<u> </u>	1	1	<u> </u>	1	1	1						L	1						

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		GEDLOGIC DESCRIPTION			S	TRUCTUR	Ε		SAMPLE	22		MINE	RAL	S				YEIN	וב דו פועי	Oz-P	 Y	CAR	В	I		ASSA	YS		
RUM	70		3	FROM	TO	TYPE	TCA	%1CA	SAMPLE SAMPLE SAMPLE SEMUN	FROM	το	Ру	Сру	K. O.	Cal	Coro		No. Vein	Cum thk	No. Vein	Cum	No. Vein	Cur	No. Vein	Cum thk	ASSA	Cu	A <sub>O</sub>	Мо
			╁			Pix Py	70	30	5865	354	357.0	19	4+		0.6	0.2	-		_	7	63	_	-				<del>                                     </del>		<del>                                     </del>
		MONTER SILTSTONE	1			- 3	70 45 20	20 50					-						_			-	-	<u> </u>					
		- 50% GTZ Yeining	上																$\exists$		50								
			+			Pw. Py	70 50	88	2813	357 0	3(1)0	1.2	0.2	٤	٥.9	1.6				8	78								
			1			16.74	90		2864	21.00	21.0	43	4.		1.2	0.4	_	_		5	170	_			-				-
			上		·	75.114	70	10 40	7.004	500.0	307.0			•							.,,								
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			1			26.0			701.5				-			20				,	27								├
			-			RURY	70	75 80	2845	3610	366.0	1.2	*		0.7	04				ن	22_								
			Ŧ				20	25							_				_	_				-					
	36F1	EOH	1			DO.Py	70	30 30	2846	346.0	391	1.3	4	7	0.3	02				3	93								<u> </u>
						•	50 20	40																					
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## **HOLE 1221**

11978.53 NORTH

25117.19 EAST

490.304 m ELEVATION

**LENGTH: 312.1 m** 

			ı													MIN	IERAL	IZAT	ION									
		GEOLOGIC DESCRIPTION	L		:	STRUCTUR	E		SAMPL	ES		MIN	ERAL	.2.				PYR	NS TE 1	02-1	} <u>k</u>	CAR	B	W#	-H-	AZZA	YS	
FROM	το		1	FROM	70	TYPE	TCA	%TCA	SAMPLE SAMPLE NUMBER	FROM	TO	Ру	Сру	K. 67	Cal	Coty	K	No. Veln	Cum	No. Veln	Cum	No. Ver	Cur	No. Veln	Cun	Au	Cu	49
0	9.1	CASING				Pa-Ry	50	100	2646	9.1	13.0	0.4	0.3	2	0.2	0.4	No	-		3	59	-	-	-	2			-
			Ш			v.G. Py	30	100																				
9.1	!3.0		L					ļ	<u> </u>			<b>.</b>	١.	١		l		l					ļ	<u> </u>				
		- 1: ultiple pulk qualty-py	Ц			<u> </u>			ļ			_	L	↓	<u> </u>		_	<u> </u>										Ь.
	<del>  </del>	· reliable print qualty-py	H				-		<del> </del>			ļ		<del> </del>	<del> </del>	<del>-</del>		<del> </del>					-		-			-
13.0	160	K SPAR ALTERED GOEYWACKE				PQ-74	70	40	7647	13.0	16.0	0.6	0.1	3	0.2	0.6	YES	E		5	29	-		2	4			
		· mor chl -bio			Ĺ		50	60		<u> </u>		1		<u> </u>			L						<u> </u>	Ĺ				
						WG-P4	70	100														_						
16.C	ر.22	GREYWACKE WAY KSPAC	Н			PG-P4	70	50	2648	16.0	19.0	0.3	0.3	2	0.4	1.2		-		4	24	3	2	4	13			-
		ALTERATION					50	50		1 -				-		-		_				_	-					
		- Mod to strong Chi + Bio				WQ-Py	70	100				1		1				_					_					
						Q-C	70	100				L	Ŀ	<u> </u>	<u> </u>	<u> </u>	ļ											İ
								<u> </u>	L	ļ				<u>L</u> .										L				
	_					Pa-py	50	85	2649	19.0	22.0	1.0	0.2	3	0.4	08	Ves	-		6	38	~		4	3			
			Н				20	15	ļ	<b></b> -		ļ	<u> </u>	<u> </u>	ļ	L	<b>↓</b>	L_	<u> </u>				L	ļ				l
			Н			4.0	70	100		<del> </del>		├—		-	-	-	-	-							$\dashv$			
30	24.0	LT. GREY INTEUSE K SPAR				P4- P4	70	10	2650	22.0	24.0	1.2	6.3	4	2.6	1.5	YES	-		10	55	-		1	2			
		ALTERED GREINACKE					50	70						$\Gamma$														
							80	20				L		<u> </u>									L					
						Wa-Py	70	100			·						_	_										
24.0	26.9	GREYWACKE - LESS ALTERES	Н			PQ-124	70	5	2651	24.0	26.9	0.4	0.4	<del>  , -</del>	0.4	06	YES	-		5	55	-	-	,	2			
							50	10				I			·													
							20	85																				
						W4-14	70	100				<u> </u>			l													
	II	27.1 - 27.4 - CAVE																										
		- rubbly arz	Ц			PQ-P4	70	5	2652	26.9	30.6	10	0.2	3	0.3	1.2	Yes	-		9	100	_		-				
						<del> </del>	20	90			, .																	
			H				20	5_	<b></b>	-		1		-	-	-	-	_	$\vdash$				-	-				
			П		-									_	<u> </u>													
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	<b>T</b>	GEOLOGIC DESCRIPTION	L-			TRUCTUR	Ε	· · · · · · · ·	SAMPL	E2	<b>.</b>	MIN	ERAL	<u>.</u> S		·• •	ÞΫ	RITE	Oz-	Py	CAR	В			ASSA			
FROM	TO		89	FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	το	Ру	Сру	4.01	Cal	Colo	No Ve	. Cui	No.	Cum	No. Velt	Cun thk	No. Vein	Cum thk	Au	Cu	<b>A0</b>	⊥'
30.6	34.5	TRANSITION ZONE				70-P4	70	40	2653	30.6	34,3	0.6	0.2	7	0.3	0.6		$\pm$	6	ట	Ē		-				$\perp$	+
			Ш			,	50	55			<u> </u>	l	<u></u>	Ĺ														1
		K SPAC ALTERED INTRUSINE					20	5					I	l				$\perp$										].
		+ SULICIFIED GUARTZ - MAGNETITE																										$\perp$
		REPLICEMENT BRECCIA													1				_									$\Box$
34.3	37.4	MOSTLY K SPAF ALTERED	H			PO-P4	70	5	2654	24.3	37.4	0.8	0.4	6	0.4	1.4	<u></u>	+	10	100	1	2	-	$\vdash$			+	+
		GREYWACKE & MINDE				1	50	5	1	1		Ī	İ	1.2-	1	1			† '''	1	1	1						1
		ALTER'S INTRUSIVE					20	90							1				<b>T</b>									$\top$
						<b>Ψ-C</b>	70	100		1				匚				$\perp$										1.
314	4.5	SILICIFIED QUARTZ - MAGNETITE	$\vdash$			Re-Pe	70	70	7.655	37.4	41.5	1.2	0.5	8	0.5	1.2	-+-	+-	8	85	3	5	-				-	+-
		FEPLACEMENT BRECOM					95	50											1	-	<u> </u>						_	+
							20	35				Ì	1	1	1	<b> </b>		1	1			1					1-	1
		- mod ser chl + bro acr.				Q-C	10	100		ļ																		1
415	43.6	tirely Gleywhale	-			Pa. Py	50	100	2656	41.5	43.6	0.4	0.3	2	0.5	0.6		+	1	10	-		1	3			-	+
						NQ. Py	70	100																				1
43.6	55.4	ALTERED MEGACRISTIC KSDAR	+			70- P4	20	60	2657	43.6	44.6	1.0	0.5	g	0.3	0.2		+-	7	50		-	-					-
		PORTHYRY					20	40																				+
		- mod ser bio chl alt	$\vdash$									-	<u> </u>	├	-	$\vdash$		+-	-	_		$\vdash$	-				-	+
		919.	1			İ						·		1	1-	1		1	1								†	+
						PG. P4	50	100	2658	46.6	49.6	0.5	0.3	6	0.2	1.4	Ξ.		9	100	-		-					1
						0. 2.		75	2659			-	21	-	1.0	10		+	+-	-			_				├	+
			+	-		14-14	50 20	25	2634	44.6	52.0	0.6	0.6	R	0.5	1.0	<del> -</del>	+-	4	76		.	-					-
	-		-	-			20	-65				-	-		-	-		+	┼─					$\dashv$			-	+
						PO- Py	50	25	2660	52.6	55.6	1.5	0.4	9	0.2	1.6	-	1	6	95	1	2	-					1
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Hole No. 1221 Pg. 3 of

									-			ſ				MINE	RAL	IZATI VEIN	NO. 21					. 101	1				
· <del></del>		GEOLOGIC DESCRIPTION	<b>.</b>			TRUCTUR	Ē		SAMPLI	<u>S</u>		MINE	RAL	5	,			PYRI	E	QZ-P	Υ	CARE		DZ.	P	AZZA	142	,	┰.
FROM	TO		100	FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Ру	Сру	( of	Cal	Coco		No. Veln	Cum thk	No. Vein	Cun thk	No. Ven	Cun thk	No. Vein	thk	AZZA Au	Cu	<b>A</b> 0	Mc
55.6		SIUCIFICO QUARTE - MAGNETITE	H	-		wa-ay	50	25 75	2661	55.6	586	2.0	0.7	11	0.2	0.6		-						6	100		<del>                                     </del>		+
		REPLACEMENT BEECE A	П				ಬ	K										$\Box$	_										F
		57.3 - 57.4 - CAVE				WG. FY	70	50	2662	28.6	61.6	1.8	0,8	ક	0,4	12		-		-		-		5	51				L
			H				50	50								<b>├</b> ─-									-			-	+
						NO - P4	Ju		2:43	61.60	64.6	0.6	0.4	8	0,2	0,4		=				-		6	45				
			H			\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	50	70				$\vdash$							-						-		-	-	+
						42.R			264	64.6	676	0.6	0.5	6	1.0	0.5		=				-		4	68				1
		- mad zer Cht pio alteration	H				20	3u 50	<u> </u>		<del>-</del>	-													$\dashv$		-	-	+
- 1		- mad zer Chl bio alteration phillosoliculos (crun)					Ī	T	2665	176	70.6		a	-	0.3									8					
						WO-RY	70 50	20	7662	01.6	10.4	0.0	0.6		0.2	<u> </u>								•					+
-			╂┤		_	wa. Ry	70	40	2666	70.6	73.6	0.8	0.4	5	0.2	1.2		-		-		-		12	108		<del> </del>	_	+
			$\square$			1	50 20	50																			<u> </u>		F
																													‡
			H			war Ry	70	10	2467	73.6	76.6	7.	0,4	8	0.7	1.0		-	_	-		-		6	112		-		-
			1-1				70	30																					
		76.6 - While Oz - Py upinlets				170-P4	70	10	2648	76.6	79.6	2.2	08	ط	0.2	1.0		三		2	29	-		-					_
		docreasing + pink - Oz	$\dashv$			<b>'</b>	20	30	<b></b>									$\vdash$							-		<del> </del>	-	+
								L	57.70													- ::					ļ	<u> </u>	1
		- Cp micreasing down hole	H			Po- Py	70	50	2669	79.6	82.6	7.5	5.6	<i>8</i>	0.1	0.5		-		2	100	-		. !	.17.		-		
	Ж	82 - 83.2 · 90% pink 077 VN	$\square$			NQ-Ry	20	100	2670	826	RL.	٦,	2.6	10	0.)	0.2				3	185	•							F
		2 ~ 2-3% cpu	$\Box$			Pa - Ry	20	100	20,0	32.4		3.3		,,,						,	·w								+
			H		-	<del> '</del>	_	-				-			-				_								-		+

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Hole No. 1221 Pg. 4 of 1.

			<del>,</del>																						note	NO.12	21 Pc	). <del>4 0</del>	
1																MINE	RAL	IZATI	IDN					414	.e.	T			
		GEOLOGIC DESCRIPTION	i			TRUCTUR	Ε.		SAMPLI	Ę\$		MIN	ERAL	S				PYRI	ÎE_	Oz-I	Py	CAR	B	197	·Pu	ASSA	.YS		_
FROM	TO			FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Ру	Сру	ای	Cal	20		No.	Cum	No.	Cum	No.	Cu	No.	Ĉ.	Au	Cu	Ag	H.
$\vdash$			183		<del>                                     </del>			-	NUMBER			_	-	-	-	3		Vein	thk	Veh	thk	Vein	The	Ven	thk		├──		+
<b></b>			H		┼	0-	-			05.4	001	-	-	-				$\vdash$			10		├	-	-	<b></b>	├──	——	+
1 1		SILICIFIED 012 - FE CRIDE	<b> </b>		<del> </del>	90- PH	50	100	2671	85.6	60.6	3.0	2.4	8	0.2	0.7		-		4	48	-	┼	ļ <u>-</u>					4 -
		EEPLICEMENT 3x	$\sqcup$		↓	ļ		<u> </u>		ļ					-	-		-			-		<b>├</b> —	-	<b>-</b>		<b>├</b> ──		—
L		- numerous pink 0:2- by			<u> </u>	PG. DY	70		2672	88.6	916	2.5	1.8	9	0.2	0.3		-	_	2	62		ــــ	-					↓_
		un's + veinlets			<u> </u>		8	50							L.									_					$\perp$
									I			l	l	l	1	Ll												L	1_
	*	26.6-89.2 DWR GTZ-DY UN				Ma. PA	2	100	2473	91.6	94.5	1.3	0.5	11	0.2	0.5		-		-		-		2	12				
		₹ ~ 3% cpy			1																			I					
	Ł	46.4-97.6 -OZ VN	П			WQ-PY	50	100	2674	94.5	976	1.0	0.6	6	0.2	1.4								17	120				
		- CORE BROKEN TO ZEM	$\sqcap$			1		1		1																			
			П																										
-			$\Box$			Wa-Py	20	100	2675	97.6	100.6	10.0	0.7	8	0.4	20		7	30	2	24	3	3	3	70				
	-	99 5 . 99 X = MISSING DA 110			<del>                                     </del>	Pa-Py	50	100		///	10014	1.5.1	-	-		1					-	_							<b>†</b>
h		99.5.99.8 - MASSIVE Dy verifiet	╂╌┼		<del> </del>			100						ł	1-	<del>  </del>								<b>†</b>	†i		·		1
			╂╌┧		<del> </del>	py unla	30					_	<del> </del>	-	-			<b>├</b> ─┤	-		_		+	-	-		<del> </del>		+
1			₩		+	Q-C		75	<del> </del>	<del> </del> -		ļ	├	├	├	<del>  </del>		┞╼┥			-		$\leftarrow$			<del> </del>	<del> </del>		+
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			$\sqcup$		<del></del>			<u> </u>	<u> </u>	<b></b>		L	<b></b>		<u> </u>								↓_	<u> </u>	L	L	<b>1</b>		1
					1	WQ-DY	70	100	2676	100.6	1036	377	0.3	9	0.2	1.2		2	3				↓_	4	27		<u> </u>		$\perp$
						PI	70	So				L			<u> </u>									İ		L			
			П			1	50	50																					
					1		-					1																	
	-					PQ-QU	50	100	2677	1036	106.7	3.4	0.3	11	0.2	15		2	7	1	4		1	4	147				1
	*	1059-106.7 NOZ-PY VEIN	1-1		_	WQ-PA		100	= 0 1,7				1	$\vdash$	1	-							$\vdash$						_
		1000	1-1		_		50	100	<u> </u>	<del> </del>		<del> </del>	1	1	†	$\vdash$						_	1	Τ-					$\top$
			1		<del></del>	74		1.00		1			<del>                                     </del>			$\Box$							$\vdash$	1					_
106.7		QUART 2 - MAGNETITE CTKWOCK	<b>†</b> †		<del> </del>	<del></del>			2678	1067	109.7	112	0.6	io	102	170		-		-		† -	†-	† ···-	<del> </del>		1		1
1.50		SOURCE STREET,			+			<del> </del>	0010	1	1911	1		<u> </u>	1						<del>                                     </del>	_	_	†					+
		- very little replacement.	1		<del>                                     </del>	<del> </del>			<del> </del>	<del> </del>		<b> </b> -	†		†··	1-1					<del> </del>	<b> </b> -	<b>†</b>	† ·-	ļ	·	ļ		1
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h			╂─┼		+	P4 U(+	50	75	2679	1097	112 5	1,4	0.2	a	2	17.		4	10			<del>-</del>	3	ļ · -	<b> </b>				ł
-			┥		+	ואן טוף	_		3019	,5,1	112.3	4.7	10.2	<u> </u>	0.2	1.0		+	10		-	<del>  '-</del>	+3	-			-		+
-			-		<del> </del>		20	25		<del> </del> -						ļ		-					+-	ļ					1
			⊢		1	9.0	50	100	<b>!</b>	<u> </u>				<u> </u>	-	$\sqcup$		$\sqcup$				_	-	1_					1
							L			L		1			1							L_		l					
	*	117.5-113.0 8% PU UN				חיום	70	100	2680	115.2	115.5	100	0.5	8	0.6	2.2		2	61										
			П			1.1							[											T					T
			1:::1		1			t		1			1		<u> </u>						<u> </u>		1 .	1		1	1		

	ſ'	GEOLOGIC DESCRIPTION		T=-=-		STRUCTUR	Ε	rain i	SAMPL SAMPLE NUMBER	ES .	r::_:	MIN	ERAL	.s			ERAL	IZAT YEN	ION S	Qz-I		[CAR	3					9. 5 of
FROM	10	-	189	FROM	10	TYPE	TCA	ZTCA	NUMBER	FROM	TO	Py	Сру	Keg	Cal	Cock	_	No. Vein	thk	No. Vein	thk	No. Ven	thk	No. Vein	thk	~	Cu	<b>^</b> 0
		QUARTZ-MAGNETITE STOCKUDAL	-						2681	115.5	118.5	1.3	0.5	9	0.1	2.0	-	=		-		-		-				
									2682	118 5	121.5	1.0	ა.5	11	0.2	1.4		=		1		=		Ξ				
		- muchar Chl, bic alteration	+			Pq-Py	50	100	2683	121.5	124.5	0.8	0.1	ю	0.1	2.0		=		. 1	7	=	_	=				
						AQ. Py	70 50	25	2684	124 - 5	127.6	0.3	0.2	9	0.2	1.5		٠.		3	38	-		-				
			-			Pa-Py	30	100	2685	127.6	130.6	1.0	0.8	9	+	0.8		=		2	35	_		-				
			1			PU-DY	50	lou	2686	130.6	133.6	0.6	0.4	10	10	az		Ē		1	ಬ	-		-				
			1			RD. Py	70	100	2637	133.6	136.4	10	0.2	11	0.1	0.1		=		1	21	=		_				
	+	white quartz vein - very little Minercolization < 170 mt, sar +				W. Ry	70	ы	2688	36.4	139.7	0.1	0.7	10	0.1	0.6		-		-		=		1	હ્ય			
		chi < 0.2% altration.	1																									
						Po. Ry py unit			2689	139.7	144.1	3.0	0.5	15	0.1	10		1	5	2	26							
144.1	1526	ANDESITE DYKE	-		عں	DYKE	L		2690	1,44	148,3		_		_													
			1		LC		50	1		1			<u> </u>	·														
	_₩.	C 149.1 FLT 1 cm gouge	╁			FLY	50	20	2691	1483	152.6				-			-		-		5	2	1				
		- 5 - 1 cm Carb STGES (rom 150.5 - 152.6	E				50	80																				
152.6	162.8	QUARTZ - MAG. STOCK WORK (CON'T)	+			1		100	2692	1526	155 0	0.6	0,1	12	+/	0.8		2	1	-		•		•				
		- magnetite centent uncreases aither dire	F			PO. PM	50	100	2693	155.6		Π						`		2	31	•		•				
			F			Dy stra	<b>5</b> 0	100	2694	150.6	161.7	3	0.5	15	10	0.3		I	2			-		3	44			
			1			t 17	1			<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>						• • • •					

Hole No. 1221 Pg. 6 of 10

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	Ì	GEOLOGIC DESCRIPTION				STRUCTUR	E		SAMPLI	E <b>S</b>		MIN	ERAL	S				PYF	S	loz-F	5 ·	ICAR	B	95	61	AZZA	24		
FROM	TO		3	FROM	TO	TYPE	TCA	%TCA	3 JAMAZ R 3 B MUN	FROM	TO	Ру	Сру	KeO+	Cal	Coro		Na. Veln	Cum	No. Veln	Cur	No. Vet	Cum	No. Vein	Cum thk	Au	Cu	40	Mc
		stockwork aradially ledes to										Π															ļ		Ţ.
	ا		ļ		ļ	Py which	40	Ю	21095	16.7	164.7	4.0	0.6	16	0.3	2.0			3			<del> </del>							-
102.0	191.4	SILICIFIED QUARTZ - FE ONIDE REPLACEMENT BRECCIA	$\vdash$		╁	wo. Ry	50	100	2696	14.7	1477	0.4	0.3	11	1	12				-		$\vdash$	╁─	2	3ა		<del> </del>	<del>                                     </del>	╁
		REPLACEMENT SKOOTA	<b>†</b>		<del> </del>	- rd	20	100	- 70		10 1:1	73.9		-:	<u>''</u>	اعورار							<del> </del> -	-	-~				_
		- mod ser + chl + bio				By unlt	20	100	2697	167.7	170.7	2.8	0.2	12	0.3	2.0		٤	6										
		ateration				'		ļ	1,00					ļ		-							<u> </u>				ļ	<del> </del>	╀
.		Fost advantage							2698	7.07	1737	33	0.1	9	D.Z	1.2						· ·					· ··-		
		- pullosciccotos arundant	┨			200	50	100	2699	173.7	176.7	5.0	0.2	10	0.3	1.5		T	40		_	1	3					1	1
		1 (24 42 11)	1		<b></b> -	17 Jn	50	100	<u> </u>	11131	1	-	1	1.0															
	*	175.2-175.6- Vugay QTZ-Py	7								Ī																	<del> </del>	$\perp$
		vein with 50% crz			ļ			ļ	2700	176.7	1800	1.5	0.2	8	tr	1.2						<u> </u>	-					₩	┿
		25% py + 75 % spec hematale (weaccystic	7			<del></del>										-			•				<del> </del>						ł
		+ 1cm	1	ļ	ļ	py stig	50	100	2701	1800	183.1	1.2	0.5	10	0.2	1.5		-	5	-		-						<del> </del>	╁
			<u> </u>			<del> </del>	<u> </u>	<del> </del> -	2702	183.1	185.2	2.2	04	ID	04	1.5				_		-						<del>                                     </del>	-
		biolite + sovieite	<b>₩</b>	-		<del> </del>		<del>                                     </del>													_		<del>                                     </del>						T
						a-c	70	100)	2703	185.2	188.2	1.8	0.3	11	0.5	1.5		L	5			I	3						Ľ
		- chlorite alteration becoming	$\Box$			pustav	70	100		ļ													<u> </u>				<u> </u>		ļ.
		Strong u 1740 - 178.0 m	<b> </b>		ļ	1,1,,				100.3	1017		2.		_							ļ.,	2				<u> </u>	<del></del>	╀
			-			9.0	70	100	2704	188.2	191.2	1:3	0.6	12	0.4	1.5							-						-
1914	194.1	758 fine Otz-Pu Vein + 25%	T					1	2705	191 2	194.1	2.3	0.6	8	0.8	1.7													
		silicans de Feor redocument																					L						Ļ
		Breeze	L		<u> </u>	<u> </u>		<del> </del>		ļ								_						_	_		<del>  -</del>		1
		3 /	1			<del> </del>		<del> </del>			102.0	<del> </del>	-	-	-		_	4	<u></u>			-	1		-		-	├	╀
194.1	197.5	PINE QUARTE - PU YEW	-		<del> </del>	Py unu	70 SD	2 <b>5</b>	2706	194.2	M/.S	7	103	2.	0.4	2.3		4	10			-	4			<b></b>		· · · · · -	┧
		Distributed Name Assess	╁╌		-	ac	\$0	100			<del> </del>	<del> </del>	-		-	-	_	-			-	-	-	$\vdash$			-	<del>                                     </del>	┢
		- Dy stringers (m/m) every 0.50m 0 45-50° à u 370 cp in stgr.	╁╌		<del>                                     </del>	4.0	30	1.00	<del> </del>	<del> </del>	<del> </del> -	ļ					-				$\vdash$	-	†	† · · · · ·					1
		~ 2-5% COID in stringers.	†-		1	1		<del>                                     </del>		<b> </b>		<del>                                     </del>	<b>†</b>																
1975		SILICIFIED QUARTZ- FE OX				NO-184	20	100	2707	147.5	500	110	0.5	7	0.1	0.6							ļ	1	20				
		REPLICEMENT BRECEIA	1	<u> </u>	<u> </u>	,		<del> </del>			<del> </del>	<u> </u>	-	-	-	-		_		$\vdash$	_	<u> </u>		<u> </u>				<del> </del>	$\vdash$
	L	(con 4)	ļ		·					1			1							ļ	,	<b> </b>	1						1

Hole No. 1221 Pg. 7 of 1

		GEOLOGIC DESCRIPTION							SAMPL			l	ERAL	_		MINE	RALIZA	NOI			1045		w	<u>√</u> . •€	1224		
FROM	το .	GEDELOIC DESCRIPTION	8	FROM	TO	TYPE	TCA	ZTCA	SAMPLE NUMBER	FROM	το	Py	Cpy	201	Cal	20	No.	Cur	No.	Cur	No.	Cum	No.	Cur	AZZA	Cu	Ag
-			49			<del> </del>		-	NUMBER	-		+-	-	-	╁	100	Veh	i the	(Veli	The	Ven	The	Vein	thk	-	<del>                                     </del>	<del> </del>
197.5		SILICIFIED QUARTZ - TE OX				P 4- P4	50	100	2708	200.5	203.5	10	06	7	0.2	0.6	3	200	1								
		REPLACEMENT BLOCKIA (CONT)				1							L														
						py Star	50	100	2709	203.5	206.3	0.5	0.4	9	0.2	1.4			1	2							
	*	Pruk 972 - Py YEINS with							<u> </u>		<u></u>	_	1	ــــــ	↓_	$\perp$		<u> </u>	_		↓	<u> </u>				1	
						ļ				ļ		ļ	<del> </del>	<b> </b>	↓	$\vdash$		↓_	$\vdash$	ļ	↓	<u> </u>			L		
		196.6-197.5 ~ 10% py < 1%C. 201.3-203.4 - 5% mt < 1%	L			ļ		<del> </del>		<del> </del>	2.43	<del>  _</del>	1_	<del> </del>	100	12		┼	↓_	<b>├</b> —	+-					├	
		201.3 - 203,4 - 5% mt < 1%	ļ			ļ		<del> </del>	2710	206.3	504.7	1.0	0.3	110	0 2	0.5	_	┼	<b>├</b> ─	-					<u> </u>	├	<u> </u>
		200 7 200 7 7 200 0 1000				<b>├</b> ──			<del> </del>	<del> </del>		-	+	-	┼─	+-+	+	+-	+-	-	<del> </del>	┼	-	-	-	<del> </del>	
		209.7-210.7 - 2%-Cu 10% py	-			Pa.Pa	50	-	2711	Zc9.3	212 3	00	22	0.0	0.2	1.0	<del>- -</del>	97	+-	$\vdash$	<del> </del>		-		<del>                                     </del>	<del> </del>	$\vdash$
$\vdash$						14.14	35	٠.۵	2/11	W1.3	22.0			4.0	10.0	1.2	<del>-   '</del> -	17/	+	_	<del> </del>	1	_	-	<u> </u>	<del>                                     </del>	
		WHITE GREY QTZ - PV VEIN				<del> </del>		<del> </del>	2712	212.3	2136	/ 2	0.2	11.0	0.1	0.6		1			1	1				<b>†</b>	
-		111170117 0112 14 1612				1			-	1	2100	111		1	1				1		$\vdash$						
	*	213217.7 - CRACKUE TEXTURE				VEIN	LE 50		2713	2136	217.	2.2	0.1	6	0.3	2.2		T	1		t						
		- unggy from 217.5-217.7					-					1										1					
		- fut? 6 20° & 1 cm gauge		216.6	24.7	fu	20°		2714	217.7	219.9	20	06	10	0.3	2.1			·								
																			T								
	*	29.9-221.9 - WHITE /GREY GTZ- PY				VEIN	WE 70		2715	219.9	Z21.9	3.0	0.4	3	0.2	2.0			L								
		VEIN											_								1	1	_			<u></u>	<b></b>
		u 10% of QTZ-Ht				HMA		100	2716	221.9	2249	4	0.3	11	0.1	2.0	3	18	_		ــــــــــــــــــــــــــــــــــــــ		3	98	<b>_</b>	<del></del>	
			L			wa- Py	\$	100	l			ļ	1	<u></u>	↓	$\sqcup$		↓	↓_	ļ	<del> </del>	ļ	ļ	ļ	<u> </u>	↓	ļ
			$\vdash$			<b> </b>		-		l		-	-	-	<del> </del>	- I		-	<del> </del>	<del> </del>	—	↓	_	-	<del> </del>		
			$\vdash$			Wo.R	30	100	2717	224.9	2279	10.5	0.2	14	0.1	0.6		┼	-	<del> </del>	╁—	┼—	-!-	24		<del> </del>	
			-			1 2	_	100	27.0	227.9	2208	1/2	03	100	0.2	10	+	+	+-	-	┼─	+	1	30	<del></del>	-	
-			-			wo-Re	20_	100	2718	417	اللايم	1.0	23	10	1	1	-	<del> </del>	+	├─	<del> -</del> -		<del> -</del> '-	30		<del> </del>	-
			-			<del> </del>		<del> </del>	2719	230.9	7379	7.2	0.3	10	0.2	1.0	_	-	+	$\vdash$	+-	+	-	-	-	_	
			-			t		1		1.75	- :2.	1	10,5	1	1	1		1	<del>                                     </del>		<b>†</b>	1		1	1		'
		e 234 - 2373 green mca							2720	2339	2369	1.2	0.2	7	0.1	1.4				1							
		offeration very strong							1	1		ľ	1		]							1			_		
								I						Γ.										Ι			
	4	137.3 - 238.6 - white 9tz - py				wa Pu	30	100	2721	2369	237.7	1.2	0.3	10	01	00							1	130			
		Vein @ 30° UC				1										$\prod$											
		- 2 - 1 mm blebs cog																							1		
		and the second of the second of the second of			,											1	Ι.										
		I				1		Ь		1		ــــــــــــــــــــــــــــــــــــــ		٠	<u> </u>			1		<u> </u>	┸	ļ					

												ı					ERAL	IZATI	ÖN.	516				۹۵	lite	·····		
		GEOLOGIC DESCRIPTION	<u>.</u>			STRUCTUR	Ē	<b>.</b>	SAMPLI	Ę\$		MIN	ERAL	<u>S</u>	<b>,</b>	<b>,</b> .,		PYRY	È	Oz-F	Y	CAR		QZ.	Ry	ASSA	YYS.	
ROM	TO		84	FROM	ΤŒ	TYPE	TCA	%TCA	SAMPLE SAMPLE NUMBER	FROM	TO	Ру	Сру	Kellt	Cal	Coto		No. Veln	Cum thk	No. Vein	Cum	No. Veln	Cum thk	No. Veln	Clar thk	ASSA	Cu	40
73.8		SILICIFIED QUARTZ - FE OXIDE	Н		-	Ga.Py	50	100	2734	273.8	276.8	0.6	+5	6	0.3	0.6		-		_	30	-		-	$\vdash$	-	<del> </del>	<del> </del>
		REPLACEMENT BRECCIA/	П			1		1	1			<u> </u>																
		MEGACRYSTIC PORPHYRY																										
										1		1	1															
		- magacinative porphyry																										
		to green pullosilicates + cul								1					1													
_	-	the green pyllosiliestes + coll + sovici's.				Ī																						
		- Silica Contril n 30-40%		·		69.P4	50	(M)	Z735	276.8	279.7	0.6	0.2	6	0.4	0.6				1	<b>3</b> 0							
$\dashv$		in viens + verilets as quast?				,						_	-														<u> </u>	_
$\exists$		- magnitute . 5-8% as				<b></b>																						
-		replacement of intrusive.	H				<b> </b>		2736	279.7	282.7	0.6	0.1	8	0.2	0.8	-		$\dashv$					_	$\vdash$	-	-	$\vdash$
7		276 -							122																$\Box$			
		- 90% MEGACRYSTIC PLASIOCUES					i					T	1											90	- 64			1
		PORPHYRY INTRUSION				GO-Py	50	100	2737	282.7	285.7	0.3	+~	7	0.1	0.8				,	73				ಖ			
		10% Q2 - ME PEPLACE MEU				Par Tu	•0	IW		1		1				1							1					1
$\neg$		With numerous aren to	П			1																		40-	P			
		-inc cuests - DU VRIES un FO	П			Gu-Ru	82	100	2738	285.7	288,4	0.6	0.3	9	0.1	0.6								7	68			1
		- me querts - py veins up to 3 metres while !	П			1																						
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		- Chalcopyi'e prisint				Pa. 74	50	ıω	2730	288.4	7914	0.8	0.2	11	fr	OA				1	50							
		ricistly as dissuminations bur				,																						
_		214 cres in while quality of	<b>1</b>		L																							
_		Timers in magnitude.	Ш			PO. Py				291.4	Z945	12	te	9	10	0.6		$\rightarrow$	_	3	38							<u> </u>
		,					<b>برج</b>	75.									.,						- }	-			-	
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		STATE OLSO OVERSUL S	<b>t</b> t			D4	70	100	2741	394.5	297.0	10	6.7	8	0.2	6.2		1	5	2	140			- †			1	
_		stabled also present is	П			18 P4	50	100				1		-					-	-	1			_				1
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4		+ 12 LOTS up 10 co can	┦					-					ļ				_		_			_	_		$\square$			1
_		+ 12,2015 ND 10 FO CHA.						İ		1		1			i l	1	ı		- 1					- 1	. !	1		

Hole No/221 Pg. 10 of 1

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		GEOLOGIC DESCRIPTION				STRUCTUR			CAMBI	re		L	EDAL					YÉÜ	S			 X Pres		<u> </u>	nE	A22A			
ROM	TO		ğ,,	FROM	TO	TYPE	TCA	%TCA	SAMPL SAMPLE NUMBER	FROM	TD	Py	Сру	201	Cal	0,0	<u> </u>	No.	S TE 0: Cum N thk V	- P	Cum N	O.	Cum	No.	ĊJ.	Au	Cu	40	H
			183			-	<del> </del>		INUMBER	<del>                                     </del>		$\vdash$	_	N-	_	<u> </u>	-	Vein	THE	PIO 3	nkiv	Ein	TOK	<b>∨ein</b>	ThK		<del> </del>	-	+
		MEGACRYSTIC PORPHYRY/	1				1	1	2742	247.0	298.7	6	0.3	6	0.1	0.3				1	ىد								1
		SILICIFIED GUANTZ . Fe OXIDE				1	1	Ī																					Γ
		LE PLICEMENT LEELCIA																											Ι
		(cour)																											l
		4						<u></u>					Ι	I			L			$\perp$									1
970	297 C	PINE QUACTS - PU VEIN				UC	70						I																L
		~ 6% Du	Г			LC	_		1								l			Ι								L	I.
		a 0.5% diss. Co	Γ				Ī	1	i		Ĭ .	I	T -		I														I
		<u> </u>	Г																	$\top$	$\top$								Γ
6.7	301.8	PANK GUARTZ - PY VEIN (CRACKLE)	t	1		UC	20	1	2743	2987	301.8	2.0	0.3	1.5	0.1	0.4				1	110								1
	3011.0	- munor Me < 2%	T				24.50		-1.4	1		1						1		1	$\neg$			$\overline{}$					T
		2° 0 PU	1				<del> </del> -	<b>†</b>	1		·	1				1				$\top$		$\neg$							1
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0, C	312.1	PRECOMINATE & STUCIFIED OCAMZ	<u> </u>			<del>                                     </del>	<del> </del>	<del> </del>	2744	3018	30 € 0	0.6	03	1,;	U.1	2.2	-			$\top$	_							<del> </del>	1
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		MAJOCITY OF PIUS QUARTZ - Py	<b>-</b>	-		<del> </del>	<del> </del>	1	<del> </del>	<b>†</b>		t	† <del></del>	<del> </del>	<del> </del>			1-		+	-	$\neg$					<del> </del>	<del> </del>	†
		vemiete @ 20° TCA Mt	╁	<del> </del>		UC	70	<del> </del>	2745	Y65 (	34.9.1	0.5	0.3	12	0.2	04	$\vdash$	1		١,	30	$\dashv$	$\vdash$		Н		$\vdash$	_	+
	·	Content viciosed in 12%	<b>†</b>			LC	20.9	1	-172	1-0			† <u>-</u>	ļ <u> </u>	1		-	1		-	<del>~</del> +	_	l					†	1
_		Control Williams	H			_~_	- 1	<del>                                     </del>		<del>                                     </del>		1		<del>                                     </del>	1					+	$\top$	_	$\Box$			_	<b>†</b>	$\vdash$	T
	•	306.8-308.1 - 60% Grey GTZ-10				-	<del>                                     </del>	†	t	<del> </del>			†	$\vdash$	<del> </del>					7	$\neg$	_	-						†
_		Ucin 11 0.3 % COY	1	_		<del> </del>	<del>                                     </del>	<del>                                     </del>	<b>†</b>	<del>                                     </del>	ļ —	1	$t^{-}$		<u> </u>			$\Box$	_	$\top$	_	$\neg$					$\vdash$		t
	_	~ 6% nt	† ·			<del> </del>	<del> </del>	1	İ	1		-	1	†	<u> </u>	1				+	-1-	1		1	-		1	<u> </u>	1
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Hole No./222 Pg. / of &

													_			MINE		IZAT			-,					,			
		GEOLOGIC DESCRIPTION			5	TRUCTUR	Ε		SAMPL	ES		MIN	ERAL	S				<b>YFI</b>	IS TE 1	0z-P	VC I	CARI	3			ASSA	ZY		
FROM	TO		F F	ROM		TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Ру	Сру	K-0+	Cal	Coto		No. Vein	Cum thk	No. Vein	Cum	No. Vein	Cum	No. Vein	Cum	Au	Cu	Ag	H
0.0	4.5	CASING																											I
4.5	5.5	RUBBLE : Contains come segment	$\Gamma$						2395	4.5	55	L																	
		and rounded fragments of																							$\square$	<u> </u>		<u> </u>	⅃.
		very weathered forafels and																											I
		pink quarte- pyrite.  MAFIC DYKE i med green with																											T
5.5	7.7	MAFIC DYKE i med green with							2376	5.5	7.7																		T
		dork green to black birtike spots \$200; weatly soricitie; HOPATELS (KSPAR TRANSITION)												ĺ													1		I
		= 2mm; weath soricitic:				10	50		[																				T
2.7		HOPNELS (KSPAR TRANSITION)		7.7	11.0	PORK	10	15	2397	7.7	11.0	0.6	0.3	2	10	7-		0	-	19	57	0	_						1
		- Nork over				PORA	50	55																					T
		- very fine grained sillstone				"	75	30																					1
		- weak argillic odour to																											T
		breath test		11.0	140	Paryc	10	30	2398	11.0	14.0	0.8	0.4	2	0.3	0.4		0	-	10	44	/	/						T
		- positive kapper stoins &				,,	50	50															-		$\neg$				1
		- positive tspar stoins &				"	75																		$\neg$				T
		· angular "ceachle" to as	$\vdash$																	$\neg$									T
		- angular "crackly" type		40	17.0	Paryc	10	10	2379	11.0	17.0	D. 2	0.1	1	1.2	1.2		0	-	8	15	7	7						T
	<del>                                     </del>	Assume	- 1	7.5	77	,,,	50	10		7.3																			T
	_	73327.	1			"	75	50		†															_ 1				
	-		1			Carb	10	15		1		_	-	_	_									$\sqcap$					T
	<del> </del>	<u> </u>	1			"	50	10		<b></b>						1													1
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		Que = . assibir K		/7.0	20.0	PAP.	10	25	2400	170	20.0	0/	2 3	3	01	24			_	12	23	4	3	$\vdash$				$\vdash$	+
		C19.5: positive Kapon test	<del>                                     </del>	7.0	20.0	Paric	50	50	27-5	17.0	20.0	9.0	د. ح		2.7	P. 7	-	-		<u></u>			ي			<b></b>	<del> </del>	<del> </del>	+
	<del>                                     </del>		$\vdash$			<del>                                     </del>	75			+		$\vdash$		<del> </del>	-	<del>                                     </del>		H		-				$\vdash$			-	<del>                                     </del>	+
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	_		-	20.0	28.0	Paryc	120	7.	2/01		23.0	1		-	4.3		_		_	10	50	_	7			<b></b>		<del> </del>	+
			1-+-	10.0	23.0	"	50	60	2701	20.0	23.0	0.7	0.6	<b></b>	0.2	0.2		2	-	-	~~	<u></u>	= .						1
			$\vdash$		<del></del>	,,	75	20	<del></del>	<del>                                     </del>		-	_	-		1		-		-	$\rightarrow$						<del> </del>	<del>                                     </del>	+
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	<del>                                     </del>	2 242 million Kenny Lill	<del>   </del>			Po B	-	<del></del>	2402	28.0	34.0		-	-	0.2	2 3				13	19	_		<del> </del> -			<del>                                     </del>	┼	+
		2 24.7 are position Kapar loil	<del>∣−</del> ∤	3.0	28.0	POPY	30	125	2702	23.0	20.0	2	و.ب	<b></b>	2			-		/3	7/	-	3				<del> </del> -	-	+
	-		╂╌┼╴			<del></del>	1/3	73	<del> </del>	-		-		├	$\vdash$	$\vdash$		$\vdash$			• •				$\vdash$		<del> </del>	┼─	+
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	-		<del>                                     </del>	6.0	27.0	" "			2703		27.0	<del> ``</del>	10, 3	1	10./	F'. /				-	OZ		7	<del>   </del>		-	<del> </del>	+	+
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Hole No./22219.2 of

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	CEST DETO. RESCRIPTION									•	Γ				MIN	ERAL	IZAT:	NO.	Pi	~			4	ाद-	, —		
	 GEOLOGIC DESCRIPTION	-			STRUCTURE	E	· r	SAMPLI	ES.		MIN	ERAL	S	·			PYRY	TE_	Óz-	PyC	CAR	В	Wh.	71	AZZA		
FROM		1851	FROM		TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Ру	Сру	KeOT	Cal	Coto		No. Vein	Cun	No.	Cur	No.	Cur	No.	Cur	Au	Cu	40
7.7	Konl'd) HORNIELS- (Kspar. trans)		29.0	32.0	Par, Cor	20	10	2404	29.0	32.0	0.6	0.3	7	0.5	0.5		0	_	10	17	0	-					
	C29.9m : positive Kaper Test.	$\Box$			<i>"</i>	50																					
I						75																					
																			·								
	# Keony op stors in POP, Car @ \$ 50,50 20	$oxed{oxed}$	32.0	35.0	PORCO	20	35	2405	32.0	35.0	0.6	1.1	7	0.5	0.5		0	_	6	8	0	_					
	C * 50 50 20		'		,,	50	30																				
	834.8 m: positive Kepar feet				"	75	35																				
												Ī															
			35.0	38.0	Papycar			2406	35.0	38.0	0.4	0.4	7	1.2	1.2		0	-	6	19	0	-					
					<i>"</i>	50									[]							Γ	Ι				
			38.0	41.0	MDPy Cor	20	20	2407	38.0	41.0	1.2	0.5	7	0.4	0.4		0	-	9	3.3	0	_	3	20			
	838.2 m: specks of Moss in				"	50	45																				
	0.2 m Pate, px, cpx volt 450°				**	75	35																				
	7 11111				Wary	50	65			,																	
	`				"	75																					
																	$\Box$		Pa	R							
			41.0	4.0	Par	20	15	2408	41.0	140	10	0.1	5	0.5	10.5		0		_	100	10	-	0	-			
					"	50	55		1				-		-		$\overline{}$		_	-	-	_	_				1
						15	30	<del></del>					$\vdash$							$\vdash$		_		-	_		+
	 P43.2-46.6m: 1.4m lost come	$\vdash$				<del></del>	+	İ	<del>                                     </del>		<b>-</b>	<del> </del>			<del>                                     </del>								1			<b>—</b>	<del> </del>
			110	17.0	FORY	ZO	35	2409	44.0	47.0	1.5	0.1	1	0.2	0.2		0	-	3	102	10	-	1	2			1
		1	7.7	7	"	50		· • · · · · · · · · · · · · · · · · · ·	1.5-1.		· · · ·				1						-		+-	-			1
		1			WORY	75		+							1								1				1
		1			- y	<del></del>	1									<b> </b>					<b>†</b>	1	1	1			1
			47.0	50.0	POPY	20	10	2410	17.0	50.0	0.6	0.3	7	0.3	0.7		0	1-1	5	71	0	1-	0	-			
	249.9 m i positive Kapan test				***	50																					
					"	75	+	+																			
		+-				<u> </u>		<del> </del>	-			-		<b></b>		-		<b>—</b>		1	<b>†</b>	1	1	<b>+</b>		1	1
		+-+	520	53.0	POPy	20	50	2411	50.0	53.0	/3	2.6	7	0.7	11.4		0	1_1	7	35	10	-	0	1_	<del></del>	<del> </del>	+-
		+	327.62	32.2	"	50			1		11.5	0.0			1-1		1		-	-	<del> </del>	+	+	+	-	+	+
		+-			<del> </del>	130	130	<del> </del>	<del> </del>	-	-	$\vdash$		-	+	<del>  </del>	<del> </del> -	$\vdash$	<del>                                     </del>	$\vdash$	+	+-	+-	+	<del> </del>	+	+-
		1-1	53.0	54.0	POPY	30	+	2412	Ga	E/ 5	00			17	20	J	0		4	31	0	<del> </del>	0				+
	ess. 6 m. positive Asper fest	+	33.0	.38.0	1,014	7			33.0	26.0	0,0	0.7	-	7.5	12.60		۳		-	3/	1-	+-	ائ	+	-	+	+
	 33.6 m. pasitive Asper Jest	+-			<del> </del>	75	15			/				~	ļJ	<b>  </b>	<del> </del>	-	<del></del>	<del> </del>	+-	<del> </del> -	+	·		ļ ·-	+
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		GEOLOGIC DESCRIPTION	1			TRUCTUR	Ε		SAMPLE	23		MIN	ERAL	2				<b>YYRY</b>		Oz-P	Ý	CAR	8	र्वे	- 75	122A	YS	
ROM	TO		1221	FROM		TYPE	TCA	%TCA	SAMPLE NUMBER									No. Vein	Cun thk	No. Vetn	Cun	No. Ven	Cur	No. Ven	Cun	<b>A</b> u	Cu	40
7.7		(cont'd) HORNFELS (KSpar. trons.)	$\prod$	56.0	59.0	Par			2413	56.0	59.0	1.4	0.3	2	70	0.6		0	-	12	10	0	-	1	/			
		,	$\perp$			,,,	50	50				L	l						_					<u> </u>			<u> </u>	<del></del>
			$\bot \bot$				75	15				<u> </u>		<u>.                                    </u>	<u> </u>		_		_	$\longrightarrow$		<u> </u>	_	<b>└</b>		L	<b>↓</b>	—
			$\sqcup$			Wary	50	100									_							<b>!</b>				<del> </del>
_			$\sqcup$				<u> </u>	<u> </u>				<u> </u>			L	$\longrightarrow$	_					_	<u> </u>	1_			<del></del>	↓
_			1	59.0	62.0	Pary			2414	57.0	62.0	1.1	0.1		0.2	0.6		0	_	7	65	0	1-	0	_			↓
_			$\sqcup$			-	50	55				ļ						_	_				ــــ	↓			↓	—
_			$\bot$				ļ	ļ				ļ	ļ		ļ			-				ļ	<u> </u>	<del> </del>		<b> </b>	-	↓
_			1-4	2.0	65.0	POR	20		2415	62.0	15.0	0.6	0.9	7	0.4	0.8	_	0	_	3	33	0	-	/_	2		-	<del> </del>
_			₩			"	50	+	<del></del>				<u></u>		L			_	_				<u> </u>	ــــ			<b>↓</b>	↓
$\dashv$			$\downarrow \downarrow$			WORY	75	100								$\sqcup$	_		_					<del>                                     </del>			<del></del>	<del> </del>
_			11				ļ	1		-		_			L	-		_	_			_		_			-	-
_			╂┵┼	15.0	48.0	POPY			2416	650	68.0	<i>1.</i> 3	0.9	3	0.2	0.6		0	-	5	140	0	-	0	_		<del></del>	├
_			1-1		_		50	10				ļ	<b> </b>	<u></u>	<u> </u>		$\dashv$	-+						<del> </del>	<u> </u>		├	┼
-			╂╌┼				-	-	21.0	10				_				_				_	-	<del>  _</del>			-	├
-+			₩	68.0	7/.0	Par	T		2417	68.0	77.0	6.0	3.0	3	0.1	0.6		0	-	6	46	0	-	0	-		<del> </del>	├
$\dashv$		269.0m: produce kapon test	╂╌┼				75	15	<u> </u>			<u> </u>				-	$\dashv$	-	-	-				├	$\vdash$		<del> </del>	┼
+			╂╌┼			60.0	-	<del> </del> _	2410	2.						-	-	<del>_</del>	_			_	_	-				<del> </del>
+			╂┼	71.0	74.0	FOR		_	2418	11.0	74.0	0.8	0.4		0.2	0.7	-	4	-	10	57	0	-	-				-
		ellon: abrupt change from	╂┵				50								-	-		-	-			<del> </del>		-	$\vdash$		<del></del>	<del> </del>
-+		e71.8 m: abrupt change from  Alepyocht zopy veins uphole to  Alepyomegropy wins downhole	╂╌┼			1 12 2	75		<del> </del>			-					-+	-	-			-	-	-			<del> </del>	<del>                                     </del>
+		912 py mag + cpy veins down holo	┨╼┼			WORY	/5	100	<b></b>						-	-		<del></del>	$\dashv$			-		┼─			<del> </del>	┼
-		inch hiera lighter grow.	╂╼┼			-	-		2/19			14	2 7		-		$\dashv$	0	_	12	• 7	_	_	0	-		├─	<del> </del>
-+		e 74.8m: positive Kisper fost	╂╌┼	74.0	77.0	Papy			2419	74.0	77.0	1.4	0.7	10	7-	0.1		9	-	12	72	-	-	10			-	┼
-+		@76.5 m: 1cm blobs op in POPs	╂╌┼				50 75					<del> </del>			-		-		$\dashv$					$\vdash$				┼──
-+		7-20	╂╌┼				/3	10	<del> </del>									-					<del> </del>	<del> </del>			<del>                                     </del>	<del>                                     </del>
$\dashv$			╂┼┼			000	<del>                                     </del>	-	2400		-	-	-		-			-	-	4	77			<del> </del>	-	<u> </u>	-	<del>                                     </del>
-+		<b>8 8 8 8 8</b>	╂╌┼	77.0	80,0	Pary	50		2420	17.0	80.0	0.6	0. 5	10	0. 2	/	-+		-	7	.>2	<del> </del> -		<b> </b>			·	
-+		e 79.0m: positive kopen tost	╉╌┼			<u> </u>	30	75					-		-	-		-	-	-	—-			├	-			<del> </del>
$\dashv$			+	AD. 0	83.0	FOP	20	50	2421	80.0	83.0	2.0	100	10	_	7	-	-		7	66	-		,	2			
$\dashv$		CRO.7m: Ism hand so in was.	1 1		33.3	","	50					<del></del>	1	_	-		_			-				† <del>-</del>				
$\dashv$		C80.7m: Icm bard op in Was.	1			"	75	<u>+</u>				T					_							1				
_		FBI. Ton : province espen tost	11			WQP.	+	100								$\vdash$	- 1											$\Box$
$\dashv$			++			<del>4</del> /7	1	1		<del> </del>		†			<b></b>		-							<b>†</b>	<b></b>		<b>†</b>	<b>†</b>
-			++				-	<del>                                     </del>	!			<del>                                     </del>	<del> </del>		<del>                                     </del>	$\vdash$		-+	_			<del>                                     </del>	1	1	<del>                                     </del>	-	1	1

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Hole No. 1/222 Pg. 4 of

								Υ							MIN	ERALI	7ATI	ΠN							110.72		g. <b>4</b> o
		GEOLOGIC DESCRIPTION			STRUCTUR			SAMPL			L	ERAL							Pini	£			uh	3	AZZA	75	
FROM	TO		FRI	M TO			%TCA	SAMPLE NUMBER		TO	Py	Сру	20	Cal	corp		No.	Cum	No.	Cum	No.	Cur	No.	Cum	Au		Ag
7.7		(contid) HORNES (Score forms)	63	.0 84.	Pary			2422									V E 111			55		3716	VER	1110			
		(contid) HORNFELS (topay frame)	1	200	,,	50			-			1	1	1	1		_	$\neg$	-	-							
			1		"	75		<b>+</b>			t	1-															
											1																
		@68.6m: /cm. cp band in POR	86	0 89.0	Pape	20	20	2423	88.0	87.0	1.4	0.7	8	-	0.5				5	60							
		¥ 20°			"	50																					
		289.0m: reasonares of chlin Ola										1	1														
		green color le cocks	89.	0 92.0	POR	20	35	2424	87.0	92.0	1.5	0.3	8	-	0.5				6	27							
		areen colmer le rocks				50	_				1						_										
		@ 90.0 m: specks of Mose in Otaly					1																				
		ml. gr vein	92.	0 95.0	POPY	20	15	2425	92.0	95.0	1.7	0.4	7	-	0.1				12	92			1	//			
			1		-	50			<u> </u>	/			<u> </u>		1		$\neg$	_	-				-				
					-	75	-			<u> </u>	1	1		-	1		$\neg \uparrow$	_				_	_				
				1	Waly	20		1				_	1					_			_						
		@96.8m: sports Mo Szin FORy #200		+	1000	-	1,50				<del>                                     </del>	-	-	<del>                                     </del>	1			_	_		$\overline{}$						
		9915 - 2 - 1 - 1 - POP X2	91	0 980	POR	20	25	2426	250	28.0	2.4	14	7	01	0.1		$\neg$		0	51		_	_				
		*97.5m: 2cm band up in Pap, 420		70.0	POR	50		2750	/2.0	,,,,,	2.1	· /	1	-			-†	-+'				_					
		E 17.6 m. postilize xsper jest	-	<del>-  </del>	<del> </del>	-	12				$\vdash$	<del>                                     </del>	_		1-	-	_	_				_					
			28	0 1011	FQPy	20	25	2427	98.0	101.0	1.3	0.1	7	0.1	0.1			-1,	8	63							
			1/2	- 1227.	7 47	50	50	-7-	/			-	1				$\neg$	-1									
		I			"	75	-										_	_									
				<del>-  </del>		1		<u> </u>			_			_			_	_		$\neg$		_					
		@108.1m: positive Asper fost	101	0 100.0	POP	50	RO	2428	1010	1040	0.7	01	1	0.8	J. R				5	32		_					
		Committee Asper Just	1000	707.0	"	75		2720	107.0	707.0		J.,	-	-	- 6		_			-		<u> </u>					
			<del></del>		<del> </del> -	1-1-					_			1	1		$\neg \dagger$	-+	$\neg$								
		@ 104.8m. rock changes to lighter	124	0 1071	POP.	20	15	2429	1040	1070	10	0.2	1	0.1	0.1				,,	125			2	2			
			107	707.0	Pary	50			707.0	,0,0	7.0		-	1			$\neg \uparrow$	- †	4	-			-	-			
		gray rolow; protolith likely	-			15					_	-		<del> </del>		_	$\neg \uparrow$	_	_		-						
		TEMIL WATER	-		WOP	20	50							†			$\neg$	_	-1	_							
		<del></del>		+	100,9	75	-				<del> </del>	_	_	<del>                                     </del>		-	-+			_		-		-			
			-	+	+	<del>  '-</del>	130	<del> </del>	<b></b>						-			-	-				-				
			-	1	000	2.	1	2420			-	-	-	-					,	_		-	-	-			
			107.1	100.0	FOR	20	100	2430	107.0	108.0	1.0	0.2	-	-	0. /	-	-+		~	20	_						<del> </del>
		2108.8-110.8m: FALT: 0.5 cm gouse	105	0 ///.0	WAF	20	40	2431	108.0	111.0	7.0	3.0	5	-	0.4		+	+	6	121			3	91			
		\$ 108.8-110.8m: FALT: 0.5 cm gouge		1	Wary	50	30	1						1	1					-							
		9007- 25'-35' 1ca.			"	75	_	1				1	1	1			_	_	-			1	1				
		V-27- 23 22 77-				1,3	<u> </u>	<u>t — — </u>			<u> </u>	1	1	1	<u> </u>							<u> </u>					Ŀ

Hole No. /222 Pg. 5 of 3

		T	_						T			—	—			MIN	- CDA	174	TON			—		-	- 1102	۰ <i>/2</i> 22 ۹	<u>8.5</u>	<del></del>
		CEUTOCIC BESCRIPTION		*			_		<u> </u>			T				MIN	LKAL	LIZAT	NZ	P	nt.		u	14:5	1			
		GEOLOGIC DESCRIPTION	+	T		STRUCTUR	E	T	SAMPLE	_S	T	MIN	ERAL	<u>.S</u>	a	T	т	PYR	TE	Qz-P	Ý CA	₹8	- 10	2-5	AS	ZYYZ	1.	٦.
FROM	TO					TYPE		%TCA	SAMPLE NUMBER	FROM	TO	Ру	Сру	4.0	Cal	Core		No. Veli	Cur	No.	Py CAR Cum No. thk Vei	n t	hk V	in tr	<b>11</b> ~	Cu	۸۰	Mo
7.7		(contid.) MORNFELS (KSpor. froms.)	$\perp$	108.0	111.0	Pary	20			'												$\perp$						$\perp$
		/	1	<u> </u>		, ,	50	65			ļ					<u> </u>						$\perp$						$\perp$
			<del> </del>	<b>_</b>				<b></b>	<u> </u>	<b>↓</b> '	<b></b>	<del> </del>	<del></del>	<del> </del>	<b></b>	1	<b>—</b>	1		$\bot$	+	4	_	+				
		" 111.8 - 113.1m: FALT; 0.5cm	<u>-</u> '	111.0	113.1	POP	50	50	2432	111.0	113.1	40	1.2	5	-	0.4	ļ	<del>                                     </del>	<u> </u>	14	31		12	39	4			
		gouge seam 45°	<del> </del>	<del> </del>	_	<del></del>	1			<del> </del> '	<del> </del>	₩.	-	<del> </del>	$\vdash$	+		<del> </del>	<del>                                     </del>	+	-	+	-	+	+-	+	+	+
			+	<del></del>	-	WOPY	20	100		<b></b>	·			-	$\vdash$		-	1		+	-	+		+	+-		+	
			+	102/	116.0	Par	50	45	2433	118.1	115.0	10	0.1	14	-	0.6	-	+-	$\vdash$	3	60	+		+	+-	+	+	+
		0114.7m: positive Aspor test	+	112.1	75.	Pary "	75					//				1						7-		+	1		1	7
	<u></u>	177.7m. 177.00 - 1.00	+			<b>†</b>	1	<b>—</b>	<b>†</b>	<b>—</b>						1						+			1			+
		e 116.4 m; and of light coloured	+	115.0	110.0	Pary	20	65	2434	115.0	118.0	0.8	0.2	7	Tr	0.3				3	10	1			1			1
		harnfels (felsic wache); ansat of	1	,,,,,,	f		50	35		,												+						
		dork green partels (sittators)																				I			1_			T
	NB	W Now well of pyrile relime to		118.0	121.0	Par	20	75	2435	118.0	121.0	2.0	0.3	5	=	0.3		1	3	4	7	T	T	T				T
		results in higher porcentage		,		- '	50															I						I
						Py		100														I						].
											'							$\Box$				1			L			1
				121.0	124.0	Pary	20	30	2436	121.0	124.0	1.1	0.3	5	Tr	0.3		'	'	12	53	1						
			<u></u> '	Ĺ'		"	50	10		igsquare	<b></b> '	<u> </u>				igsquare		<u> </u>	<u> </u>	$\sqcup$		1				$\perp$		_
			1_'	<b></b> '			1	<u> </u>	L	4/	<b></b> '	<u> </u>		<u> </u>	<u></u>		-		<b></b> '	لب		1		$\perp$	1_			-
		<u></u>	1	124.0	127.0	POPY	50	100	2437	124.d	127.0	1. Z	0.3	5	0.3	0.5	-	<b>↓</b> '	<b> </b> '	7	35	+		+	-		-	+
		<b>1</b>	╁_′	<b></b> '	1	-	<del></del>	<u></u> '	L	1	<b></b>	ļ- ;	ļ'	<del>-</del>	-	+		<b> </b> '	—′	+	-		-+-	+	+-		-	
		<u> </u>	4-	127.0	130.0	Pary			2438	127.0	1300	1.0	0.2	5	0.3	0.1	-	<del> </del> '	<del>                                     </del>	+	27	+	+	+-	+-		+-	+
			+-	<del></del> '	-		50	75	<del></del>		<del></del>	<del>                                     </del>	-		<del> </del>		-	1-	<del>-</del> -	1	-	+	+	+	+		+	+
		<b>4</b>	+	<del></del> '	+	000	+	<del>  '</del>	1	1	+'	H.,	+	+	+		-	<del> </del> '	₩'	+	3	+		+-	+-	-	+-	+
		1	₩	130.0	155.0	Pary	50	100	2457	130.0	153.0	1.5	0.3	15	0.5	0.7	-	<del> </del> '	<del> </del> '	1/	-	+	-+-	+	+		+	+
		<b>4</b>	+-	<del> </del>	1	200	+	+	- 14	122	1 79/	<del>  _</del>	1	+=	<del>  ,</del>	+	-	1-	<del>                                     </del>	12	18	+	+	+-	+-		+	+
		<u> </u>	+-	(33.0)	136.0	PAR	50		2440	155.0	136.0	0.7	0.2	-	0.2	10	-	<b>├</b> ─	<del>                                     </del>	1	<del>/*</del>	+	-+-	+	+-	+-	-	+-
			+-	<del></del>	-	-	30	ردو	<del> </del>	<del> </del>	<del></del>	-	<del> </del>	-	<del> </del>		<del></del>	╀	<b>├</b> ─	1		+	+	+	+	+-	+-	+
			+	1.71	1.00	PAR.	10	+-	2/41	12/1	t	1,,		+=		+	-	₩	<b>├</b> ─-'	1	45	+	+-	+-	+-			
			+	136.0	137.0	POR	50		2441	136.0	137.0	1.4	0.0	1	7.	+	-	<b>├</b> ─	igcup	1	45	+	+	+	+		+	+
			+	-	<del> </del>	<u> </u>	30	-301			······ /	!	'		·			╁	$\vdash \vdash$	1		+		-	+-		+-	
-			+	1290	1.00	rory	20	1,5	2442	120	1.42	<del>] , , '</del>	24	+_	12/			₩	$\vdash$	4	1	+	+	+	+-		+-	+
-			+-	77:0	726.0	VOLY	50	75		137.4	17.2.07	1	O. T.	3	0.,	-	-	<del> </del> -	<del> </del>	1	#/	+	-+	-	-			+
			+-		<del></del>		130	1-/21	<del> </del>	1	<b></b> -	<del> </del> '	<del>                                     </del>	<del> </del>	<del></del> '		<del></del>	1	$\vdash$	-		+	-	+	+-	<del></del>	-	+
	/		1	<b>/</b> '	1			·		1 !	1 .	. '	1 '		'				<b>!</b> '	1					1			1.

		<u> </u>	1						Ι							MIN	ERAL	IZAT	IUN								222 19	. 6
		GEOLOGIC DESCRIPTION	1		S	TRUCTUR	ε		SAMPL	23		MIN	ERAL	S				XE IN	S-10	Pi^	<u> </u>	TEAD	<b>n</b>	100	.5	AZZA	24	
FROM	TO		ğ	FROM	TO	TYPE	TCA	%TCA	SAMPLE SAMPLE NUMBER	FROM	TO	Ру	Сру	60t	Cal	Coto		No.	Cun	No.	Cum	No.	Cur	No.	Cur	AZZA	Cu	40
7.7		(cont'd) HORNIELS (KSpar trons.)		142.0	145.0	POPy	20	65	2443	142.0	145.0	1.3	1.0	5	0.1	-				3	33							
			Γ			. /	75	35																				
			Γ					1	1			1																
			ऻऻ			Para	75	60	2444	145.0	1.18.0	1.3	0.9	6	0.1	0.2				12	145			1				
		#145.5 m: speck Mosa		<u> </u>		1	Sv	20		i			1															
		1						20	1			1		1				11						1				
			Г						†	† <del></del>		t		<del>                                     </del>				T	$\neg$				<del>                                     </del>	$t^-$				
			✝			W-C	20	114	2445	148.D	157.0	0.6	0.6	9	0.6	0.3				12	67	I	2					
			<u> </u>			PUR	75	10	1			i	ļ·	1	1	_				-			† <u> </u>	ļ				
			Г			1	30	40				1											1	<b>†</b>				
							20	50							1	l I												
						0. C	75	50	2446	15.0	154.0	1.5	1.0	9	0.7	1.0				11	75	2	2					
							20	SO																				
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							20	40	L			<u> </u>	ļ					$\sqcup$		_		L.		<u> </u>				
			Ц				<u></u>	ļ <u>.</u>	L			<u> </u>	<u> </u>		<u> </u>		L					<u> </u>			Ш			
						o.c	50		2447	154.0	157.0	0.6	0.8	13	0.2	1.0	+			10	20	+	4					
						Pa-R	75	30						<u> </u>														
						7	Su	So				İ			<u> </u>								<u> </u>	<u> </u>				
							20	50														L	L_					
$\perp \perp$							Ĺ																L	<u> </u>				
. ]						P074	75	10	2448	157.0	160	0.8	0.6	4	OA	10				6	60		L	L_				
							45	60							<u> </u>													
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$\perp$																				_				<u> </u>				
						90	50	50	2449	<b>60.0</b>	163.0	09	09	N	0.5	1.5				11	49	3	6	l				
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Hole No. 1222 Pg. 7 of &

			Т													MIN	ERAL	IZAT	ION									9. 7 0	
		GEOLOGIC DESCRIPTION			:	STRUCTUR	Ε		SAMPLE	<b>S</b>		HIN	ERAL	\$				YFI	15	10z-		CAR	3	T		ASS	AYS		
FROM	TO		84	FROM	TO		TCA	%TCA	SAMPLE NUMBER	FROM	TO	Ру	Сру	KeD!	Cal	Coto		YEIN PYR No. Vein	Cum	No. Velo	Cum	No. Veln	Cur thk	No. Vein	Cum thk	Au.		Ag	Мо
			Ц		ļ								_	_	<u> </u>						L							ļ	
4.7	172	HORNFELS (SILTSTONE) TONISMON	_		<del> </del>	0.C	35	50	2450	13.0	166.0	0.5	OA	6	0.6	2.5		L	ļ	10	3/	3	5	<u> </u>		L	<u> </u>	<u> </u>	_
			_		ļ	A	20	50			L	ļ	<b></b>	↓	<u> </u>	<u> </u>		L		<u> </u>	<u> </u>	<u> </u>		L_				↓	1_
		- MODERATE TO INTENSE KEPAR			<u> </u>	Pa. Py	75	20				L		ļ	<del> </del>						L_			L			ļ	<u>ا</u> ــــــــــــــــــــــــــــــــــــ	1_
		- HEAVY MAGNETITE REPLACEMENT			<u> </u>		50	SD	<b></b>							L.		L						<u> </u>			ļ	ļ	_
		DOWN HOLE FROM 172.00			↓		20	20	L	L						L		_			L						<u> </u>	ļ	1
			Ш			ļ	5	10	<u> </u>						↓	$\sqcup$										<u> </u>	ļ	1	_
		& MORE JUMP IN SAIPLE #8	Ш		ļ			L	*			,			ļ	-		<b>.</b>		Ļ_					L		ļ	Ļ	-
			Ш		<b> </b>	Q.C	35	100	2457	1660	169.0	0.4	7.0	7_	0.4	15		1	2	9	72	1	1	<u> </u>			-	↓	ļ
			Ш		<u>.</u>	Py 10.24	45	100					ļ		-												<u> </u>	<b></b>	1
172	199	MAGNETITE K. STAC	Ы		<del>  </del>	101.Ry	50	30				ļ	<u> </u>		↓					L	L			ļ			ļ		-
		HOWELS PETCHCENTAT.	$\vdash$			<b></b>	w	70				<b> </b>	L		-										ļ			<del> </del> -	-
						A .							-	<u> </u>	<del>  _</del>		<u> </u>	-	<u> </u>				<u> </u>		_				-
		U1 UP 70 20%			<u> </u>	Pw. ly	135	30	2458	164.0	1720	14	0.5	10	0.8	1.(	ļ		ļ	14	68	<u> </u>		ļ				<del> </del>	-
		OTZ VEINING TECHINATELY				<u> </u>	50	20	<b> </b>			<b>!</b> —	<u> </u>	├		<del> </del>	-	_	<u> </u>		<u> </u>	-		<b>├</b>	-			<del> </del>	-
		C 40' - 50' TCA ( = 15-40%	_				20	20	<b></b>			ļ <u> </u>	ļ	<b>!</b>				<b> </b>	ļ		ļ	<u> </u>	-					<del> </del>	<b>.</b>
		OTZ . Py VEINS , VEING 15 & STE . INER			ļ							ļ		<del> </del>	1_					_	_		ļ	ļ	<u> </u>		<del> </del>		<del> </del>
			Ц		ļ	20.82	50	4	2459	172.0	175.0	1.6	0.6	18	0.2	0.1		<b>!</b>	ļ	7	જ	_	<u> </u>	<b>├</b>	_	<b> </b>	<b>}</b>	—	<b>↓</b> _
			Ш				20	40				ļ	ļ	₩	↓	$\vdash$			-	<u> </u>	<b> </b>			<b>├</b>	_	<u> </u>	<del>  </del>	ļ	$\vdash$
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			-		—	· 0 - 1 1.	2.	20	2480	175.0	1780	0.8	1.2	17	0.2	0.1				12	63			<u> </u>			-	<del> </del>	
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			$\vdash$			<del> </del>	20	05				_		⊢	├			-	<del> </del>	-	<u> </u>	<del> </del>	-	-		├	├	<del>}</del>	-
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			Н			1000	42.20	100	24.61	. 76.0	1810	0.6	1.6	1.0	10.1	0.1			<del> </del>	-	17	_			-	_	<del>                                     </del>	-	+
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			$\vdash$		_	10.19	מכיבו	100	1461	191.0	174.0	3.3	1.6	14	10.5	0.2	-	-		-	36						<del> </del>		<del> </del>
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	<b>t</b>	185-186.2 - PINK QTZ-PY VEIN UC 45°	$\vdash$		+	1:0.14	7 <b>\$</b>	90	-40	107.0	1 07.0	1.6	J.,,	1.5	10.1	10,1	-		-	<del>-</del>	170						<del> </del> -	<del> </del>	+-
		LC 45 <sup>3</sup>	$\vdash$		+	-	42	70					-		-	-		$\vdash$	_	<del>                                     </del>		-			$\vdash$	-	<del> </del>	-	-
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		GEOLOGIC DESCRIPTION	L			TRUCTUR	<u> </u>		SAMPLE	2		MIN	RAL	2				PYRI	È	Qz-	У	CAR	9			ASSA			
ROM	TO		89	FROM	70	TYPE	TCA	%TCA	SAMPLE SAMPLE NUMBER	FROM	TO	Ру	Сру	( e O+	Cal	Coco		YEIN PYR! No. Vein	Cun thk	No. Vein	Cur thk	No. Vein	Cur	No. Vein	Cum thk	Au	Cu	40	Mo
72	199	HAGNETITE - QTZ KSTAR	╀╌					-	ļ			-	-	_	_		-		-			_	-	-			·	-	+
		HOONFELS (SILTSTONE)	1			Pa. Py	15	50	2465	1900	1930	06	1.0	15	1.8	0.3	-			4	8	-	-						+
		REPLACEMENT (CON'T					50	50																					1_
			$\vdash$			Po.Cy	50	100	246	193.0	196 ·C	1.8	0.4	15	0.5	ا.ن				/1	43	_	_						+
		199. EOH + NOTE : 6000				The Py	50	60	24.7	101	***			13	43	2.1				8	20	_	_					-	+
		199. EOH + NOTE : 6005	╁			Mar Vy	20	40	2067	196	147.0	0.6	1.5.	11	6.5	0.1		-		В	20	├	<del>  -</del>	<del> </del>			<del>                                     </del>	<del> </del> -	
<del></del>		cu mineralization av	<del> </del>					<del>                                     </del>	<b></b>		$\vdash$	-	-	_	-	$\vdash$	_	$\vdash$	_			<del> </del>	<del>                                     </del>	1			<del>                                     </del>	<del>                                     </del>	+-
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# **HOLE 1223**

**12090 NORTH** 

**25042 EAST** 

397 m ELEVATION

LENGTH: 264 m

															MINE	RALI	ZAT	ION									
		GEOLOGIC DESCRIPTION		:	STRUCTUR	Ε		SAMPL	ES		MIN	ERAL	2			Į.	(FII)	15	Oz-F	· ·	CARE		W4	. • •	ASSA	ZY	
ROM	TO		FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Ру	Сру	Ke0+	Cal	Corp		No. /ein	Cun	No. Vein	Cun	No. Vein	Cum	No. Vein	Cun	A22A W	Cu	
٥	7.9	CASING.				-	-	3016	0	7.9	-				$\dashv$	-	-		1	40						-	+
																											1
		-10cm black HAFIC DYKE																									T
		with 2-5 mm DTZ frag.	-	-					<u> </u>	<u> </u>						$\dashv$											7
1.9	13.2	QUARTZ - SERICITE - RYRITE			PO-Py	45	100	397	7.9	11.0	3,8	tr	1	1	0.8				1	Ь							1
		8.8 -9.4 - QUARTZ JEIN																									
			<del>                                     </del>	ļ	PW.Py	70	52	3018	11.0	14.3	3.6	0.3	3	~	0.2	_	_		2	6							┛
3.2	H.2	ALTERO SEDIMENTS	<del>                                     </del>	<u> </u>	<del> '</del>	45	Ω				ļ										-			-			
.2		MEGACRYSTIC PORPHYRY	++-	<del>                                     </del>	Pary	50	20	3019.	14.0	17.1	1.5	₩	8	0.2	0.2	-	-		4	30						<del>                                     </del>	-
		Tipoventy;			1	10	80	1.1.																			
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			<b> </b>	ļ	Papy	70	80	2020	17.1	19.0	09	0.3	1	0.3	0.1				8	14							
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_				<del> </del>	PO.P.	70	100	3021	19.0	22.0	0.9	0.1	6	+5	<del> </del>	-	-		,	12	$\dashv$	-		_		_	_
		# @19.0 fl+. sand+ growel.			fur	85				-	<u> </u>		Ť			_										<del> </del>	-
		# P 23 2 - 24.2 - f(+' core			Pa-Py	70	100	3022	22.0	24.4	0.5	4	6	+	+				2	24							
_		badly core		<del> </del>	· · · · · ·											_				_							_
$\dashv$		+ 25.8 - flt ? e po TCA	<del>                                     </del>		>^ A	11	100	3-0-0	24.4	274		-	6		-				5	-		-					_
$\dashv$		# 15.8 - PCF E 10 TEA	<del>                                     </del>		Pa-Ry	45	no	3013	24.4	21.7	0.4	1	ط	m	*	$\dashv$	-		3	13							_
,1	29.0	FLT. 4 80 cm gauge + sonal.			PQ- P4	30	Gor	3024	27.4	304	0,8	٥.4	5	6.2	+r				2	69							_
		LC @ 30° TCA			1																						
		- some sta degreets			Py VAIT	30	20	3025	30.4	33.8	6.0	05	2	02	0.6	tr	6	17									
_	-20	1 / 1	1		<del>  '</del>	70	30		<del>  </del>		_			$\vdash$		_	-					_					_
4	33.8	F QUARTZ VEN	<del>                                     </del>	<del> </del>	Pa.M	70	100	3026	22 Q	2/ 4		2	0	0.4					4	-1						ļ	-
$\dashv$		- VUGGY IN SPOTS - OVING STAINS (PUSTY) ON	<del>    -   -   -   -   -   -   -   -   -  </del>	-	14.14	w	100	200	27 0	76.4	دم	0.2	<b>D</b>	0.7	~	$\dashv$	-		-	مرد		-		-,-		-	_
$\dashv$		tratures	<del>   </del>	1	Pa-Pu	49	So	3027	36.4	39.4	0.4	+	8	0.0	0.1				5	80		$\dashv$	8	8-			-
		tractures			Pa-Py									,		$\dashv$				-	-			<u> </u>			_
_					Wa-Ry	45	100				ļ						_		_								
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	GEOLOGIC DESCRIPTION	V T			STRUCTUR	E 1	T	SAMPL	E <b>S</b>	r	MIN	ERAL	2		ı		PYR	TE.	Qz-	Ру	CAR	9	<u> 02</u>	-14	ASSA	142	<b>.</b>
סד		89	FROM	סד	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Ру	Сру	KeD	Cal	Cock	Mo	No. Vein	thk	No. Ven	Cur	No. Vein	thk	No. Vein	Cun	<b>A</b> u	Cu	^0
	K-SPAC MEGACRYSTIC	H			<del> </del>	-	<del> </del>	2028	39.4	42 A	0.7	0.1	8	0.3	0.3	-	<del> </del>	-	-	-	_					┼──	╁
	PORPHYRY (CON'T)									,-	L																T
	41.4 - 41.8 - FLT UC 40"	1			Po-12	70	10	3029	42.4	45.6	0.6	05	7	0.4	0.2	-	<del> </del>		3	111						ļ	ļ.,
	Very brotion, some				1,2-1	45	90					1															1.
	• •	H			Pa-Pu	45	100	3030	45.6	49.0	1.0	c. 3	a	0.1	H	<del> </del>	-		6	27						<del> </del>	+
15.4	QUARTZ VEIN UC 450	Н			1	-			<u> </u>		L		Ľ	1	<u> </u>	· ·											$\perp$
0.3	MARIC DYKE - di OKLY /Hack	H			LYKE	<u>ت</u>	70	8031	49.0	50.3				+	-		-	_		-			<u>a</u> -	Caus			
					Q-CALE	70	100	3032	50.3	52.2	0.1	fr	8	1.0	-	-							g	15			L
	- various narrow a-c	╀			· ·	4.0	·	7023	(2.2	CA (		Λ2	4	25	-	-	_		•	200							╀
	Slumers < 1 cm .C/S		_					2033	52.		0.6	0.2	0	0.5	-	-			4	15							
	50.3-522 - strong sericle ALT.				,																						
2.9	DUALTZ VEIN	H	$\dashv$				100	3034	54.5	58.0	6.0	0.3	2	1.7	1.4		2	24				-		$\dashv$			$\vdash$
																											L
84	GUART Z VEIN	+	$\dashv$		12.14	70		3035	28.0	ζο.ς	3.0	0.2	9_	0.3	0.]				2	71		-		$-\dagger$			
05	QUARTZ FEDY REPLACEMENT				a-a			7	112																		T
$\dashv$	BRECCIA / MEGACTISTIC HOTTHIR)				12-14	10	50	3076	60.5	62.5	4.5	*	2	0.4	-				3	رع							├
73																											
	- It green, equique ular	+						3037	62.5	U.1	1.0	~	4	0.3	_						-			_			
	pyrite ( 61.2 m.																									-	
2.1	biotite rich limit - med -	$\vdash$	$\dashv$					3038	66.1	69.!	' D	tr	6	0.4	-	_			-				$\dashv$				-
	- teldspa': ~ 0.5 - 1.0 cm.	<b>. </b> .						303 <del>9</del>	69.1	72.1	1.2	4	5	0.4	-		-										
	~ 1.0 cm & 70 + 45° TCA																					_	+	$\dashv$			
-		-																								· 	_
5	2.9 80	41.4 - 41.8 - FLT UC 40  Very brotion Some  QUILLE Mn STain  5.4 QUARTZ VEIN UC 45  DISTRICT BSU?  - Various Pariow 4-C  STUNGERS < 1 CM. 670  50.3 - 522 - STUNG SEVICIA ALT.  2.9 QUARTZ VEIN  BU QUARTZ VEIN  O'S QUARTZ FEOX RETLACEMENT  BRECCIA / MEGACUTTIC HOTHIR)  75 ANDESITE OTZ VEIN  - It green, equiquendan  June granned. I Som bleb  Pyrite 6 61.2 m.	PORPHYBY (CON'T)  41.4 - 41.8 - FLT UC 40  Very brotion 5000  GUAGE Mn STain  5.4 QUARTZ VEIN UC 45  DIOTITE BSU?  - Various nation 4-C  Strungers < 1 cm. C70  50.3 - 522 - Strung Stricts ALT  2.9 QUARTZ VEIN  BU GUARTZ VEIN  STRUCTIA / MEGACETTIC (DOSMITE)  The grained 1. I sem bleb  Pyrite C 61.2 m  CIE GICY PLANOCYYSTS 21  18(45pa): M 0.5 - 110 cm.	PORPHYBY (CON'T)  41.4 - 41.8 - FLT UC 40  Very brotion 5000  Guige Mn Stain  S.4 QUARTZ VEIN UC 45  DIOTITE BSU?  - Various nariow 4-C  Strungers < 1 cm. C70  50.3 - 522 - Strung Spricte ALT.  2.9 QUARTZ VEIN  BU GUARTZ VEIN  DISTRECIA / MEGACETTIC (DOTHIP)  The grained 1. I sem bleb  Pyrite C 61.2 m  CIE Gray Plenocrysts 5-  18(45pd): M 0.5 - 1:0 cm.	PORPHYRY (CON'T)  41.4 - 41.8 - FLT UC 40  Very brotion Some  QUEST Mn Stain  5.4 QUARTZ VEIN UC 45  DIMETE BSU?  - Diotite BSU?  - Various nation U-C  Slivencys < ICM . 270  50.3 - 522 - Strong Spricts Act  2.9 QUARTZ VEIN  BU QUARTZ VEIN  - It green . Equipionals  I'me grained . I Som bleb  Pyrite C 61.2 m.  10 Gigy Phenocrysts Signed  10 Gigy Phenocrysts Signed  10 Gigy Phenocrysts Signed  10 Gigy Phenocrysts Signed  10 Gigy Phenocrysts Signed  10 Gigy Phenocrysts Signed  10 Gigy Phenocrysts Signed  10 Gigy Phenocrysts Signed  10 Gigy Phenocrysts Signed  10 Gigy Phenocrysts Signed  10 Gigy Phenocrysts Signed  10 Gigy Phenocrysts Signed  11 Giggy Phenocrysts Signed  12 Gigy Phenocrysts Signed  12 Gigy Phenocrysts Signed  13 Gigy Phenocrysts Signed  14 Giggy Phenocrysts Signed  15 Gigy Phenocrysts Signed  16 Gigy Phenocrysts Signed  17 Gigy Phenocrysts Signed  18 Gigy Phenocry Signed  18 Gigy Phenocrysts Signed  18 Gigy Phenocrysts Signed	PORPHYRY (CON'T)  41.4 - 41.8 - FLT UC 40  Very brotion some  QUEST MO STOWN  S.4 QUARTZ VGIN UC 45  DYKE - die grey black  - biotite BSU?  - various nariow 4-C  Strucces < 1cm. @70  DO: Py  DO: Py  DO: - STOWN SERVICITE ALT  PY VN  2.9 QUARTZ VEIN  DS QUARTZ FEOX REPLACEMENT  BREICHA / MEBACFISTIC BERNING  THE GROWN CONSTRUCT  ANDEST TE 'OTZ VEIN  - It grown countrimbar  Line growned. I som bleb  pyrite to 61.2 m  Lin biotite rich (Limit - med -  Cle grey Phenocrysts of  1eldspot; m o.s - 10 cm.	PORPHYRY (CON'T)  41.4 - 41.8 - FLT UC 40  Very brotien, some  Quide Mn stain  PR-Py 45  45.4 QUARTZ VEIN UC 45  TYRE  TYRE  TO  MAFIC DYKE - di QVLY/black  - biotite BSU?  - Varieth Namew 41-C  Structus Com. C70  PO. Py 20  PO. Py 20  PO. Py 20  PO. Py 20  PO. Py 20  PO. Py 20  PO. Py 20  PO. Py 20  AS  QUARTZ VEIN  PR. Py 45  PO. Py 45	PORPHYRY (CON'T)  41.4 - 41.8 - FLT UC 40  Very brotien some  45 90  QUARTZ VEIN UC 45  DYKE LL 70  DYKE LL 70  WAFIC DYKE - dix grey black  - biotite BSU?  Q-CALE 70 100  - Various namew 4-C  Struccis < 1 cm. 270  DO: PY NN 30 100  2.9 QUARTZ VEIN  BE QUARTZ VEIN  PR. Py 45  DOS QUARTZ VEIN  PR. Py 45  DOS QUARTZ VEIN  BRECCIA / MEGACETOTIC BETHIRY  THE GREY ASSOCIATION ASSO	PORPHYRY (CON'T)  41.4 - 41.8 - FLT UC 40"  Very brotien some  QUESTE Mn STain  5.4 QUARTZ VEIN UC 45"  DIOTITE BSU!  Solitie BSU!  Solitie BSU!  Solitie BSU!  Solitie BSU!  Solitie BSU!  Solitie BSU!  Solitie BSU!  Solitie BSU!  Solitie BSU!  Solitie BSU!  Solitie BSU!  Solitie BSU!  Solitie BSU!  Solitie BSU!  G-CALE 70 100 3032  TYRE LL 70 8031  TYRE LL 70 8	POSCHYRY (CON'T)  41.4 - 41.8 - FLT UC 40  Very brolian some  Quite Mn stain  PR-PY 45 100 3030 45.6  49.0  QUARTZ VE, N UC 45  Diotite BSU?  Soly-522 - String Sericial Alt  PYNN 30 100 3034 54.5  Recala / Mebacrimic Barner  BE QUARTZ VE IN  PROPY 45  PROPY 45  POST 45  POST 100 3031 49.0  TO 100 3032 50.3  PROPY 20°  PROPY 20°  PROPY 20°  PROPY 20°  PROPY 20°  PROPY 20°  PROPY 45  P	PORPHYRY (CONT)  41.4 - 41.8 - FLT UC 40  Very broticn some  QUELL Mn stain  S.4 QUARTZ VEIN UC 45  DYNE LL 70 3030 45.6 49.0  TYNE LL 70 3031 49.0 50.3  D.3 MARIC DYNE - dic group black  - biolite BSU?  Q-CALE 70 100 303Z 50.3 52.2  - Varigha namew 4-C  3/Varcus < 1 Cm. C70  DYN DO 303Z 50.3 52.7 64.5  DO 303Z 50.3 52.7 64.5  PA DYN 30 100 303Z 50.3 52.7 64.5  PA DYN 30 100 303Z 50.3 52.7 64.5  PA DYN 30 100 303Z 50.3 52.7 64.5  PA DYN 30 100 303Z 50.3 52.7 64.5  PA DYN 30 100 303Z 50.3 52.7 64.5  PA DYN 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.0 60.5 60.5  PA PY N 30 100 303Z 50.3 50.0 60.5  PA PY N 30 100 303Z 50.3 50.0 60.5  PA PY N 30 100 303Z 50.3 50.0 60.5  PA PY N 30 100 303Z 50.3 50.0 60.5  PA PY N 30 100 303Z 50.3 50.0 60.5  PA PY N 30 100 303Z 50.3 50.3 50.0 60.5  PA PY N 30 100 303Z 50.3 50.3 50.3 50.0 60.5  PA PY N 30 100 303Z 50.3 50.3 50.3 50.3 50.3 50.3 50.3 50.3	PORPHYRY (CONT)  41.4 - 41.8 - FLT UC 40  Very broticn, some  QUEST MA STRIM  S.4 QUARTZ VEIN UC 45  DISTITUTE BSU?  DISTITUTE	PORPHYRY (CONT)  41.4 - 41.8 - FLT UC 40  Very brotion some  QUILLE MA STRUM  5.4 QUARTZ VEIN UC 45  DYKE - di gruy/black  - biolite 750?  - variet nature 9-C  Struccus < 1 cm. C70  D3 522 - Strung Sericla Alt.  PROPHY 20  BU QUARTZ VEIN  PROPHY 45 100 3030 45.6 49.0 1.0 C.3  TYKE LL 70 3031 49.0 50.3  TYKE LL 70 3031 49.0 50.3  TO 30 MARIC DYKE - di gruy/black  - biolite 750?  - variet nature 9-C  Struccus < 1 cm. C70  DROPHY 20  DROPHY 20  DROPHY 20  DROPHY 20  BU QUARTZ VEIN  PROPHY 45 50 3035 58.0 CC.5 1.0 0.2  PROPHY 45 50 3035 58.0 CC.5 1.0 0.2  DS QUARTZ FEO, REPLACEMENT  BREUCIA / MELACTYMIC HOTHYRY  THORY 10 CD 3036 605 CZ 5 4.5 H  THORY 10 CD 3037 605 CZ 5 4.5 H  THORY 10 CD 3038 66.1 69.1 D H  LID DIOTITE TICK (LIMIT - med -  CIE GROW PLENOCYUSYS C:  HELDEDOCYUSY C:  HELDEDOCYUSY C:  HELDEDOCYUSY C:  HELDEDOCYUSY C:  HELDEDOCYUSY C:  HELDEDOCYUSY C:  HELDEDOCYUSY C:  HELDEDOCYUSY C:  HELDEDOCYUSY C:  HELDEDOCYUSY	POPPHY BY (CON'T)  41.4 - 41.8 - FLT UC 40  Very brotion some  QUILLE Mn STRIM  5.4 QUARTZ VEIN UC 45  DIMARIC DYKE - di grey /black  - biolite 3507  - verith nation y-C  So3 - 522 - String Sericia Alt  PAPPY 20  BU QUARTZ VEIN  PAPPY 20  SO3 - 532 - String Sericia Alt  PAPPY 20  QUARTZ VEIN  PAPPY 20  SO3 - 522 - String Sericia Alt  PAPPY 20  SO3 - 522 - String Sericia Alt  PAPPY 20  SO3 - 522 - String Sericia Alt  PAPPY 20  SO3 - 522 - String Sericia Alt  PAPPY 20  SO3 - 522 - String Sericia Alt  PAPPY 20  SO3 - 522 - String Sericia Alt  PAPPY 20  SO3 - 522 - String Sericia Alt  PAPPY 20  SO3 - 522 - String Sericia Alt  PAPPY 20  SO3 - 522 - String Sericia Alt  PAPPY 20  SO3 - 522 - String Sericia Alt  PAPPY 20  SO3 - 522 - String Sericia Alt  PAPPY 20  SO3 - 522 - String Sericia Alt  PAPPY 20  SO3 - 522 - String Sericia Alt  PAPPY 20  SO3 - 522 - String Sericia Alt  PAPPY 20  SO3 - 523 - SER Co. S. S. S. S. S. S. S. S. S. S. S. S. S.	POSPHYEY (CON'T)  41.4 - 41.8 - FLT UC 40"  Very broticn, some  QUILLE MA STRIM  \$45 90  QUILLE MA STRIM  \$45 90  \$45 90  QUILLE MA STRIM  \$45 90  \$46 8031 49.0 50.3  \$46 90	POEPHY & (CON'T)  41.4 - 41.8 - FLT UC 40  Very brotion, some  45 90  QUARTE VEIN UC 45  TYKE LE 70 8031 49.0 50.3  Vary brotion some  45 90  Set QUARTE VEIN UC 45  TYKE LE 70 8031 49.0 50.3  Varies BSU?  - boilte BSU?  Q-CALE 70 100 3032 50.3 52.2 0.1 tr 8 100  Varies Nation 4.0  Sirvinces < 1 cm	PORPHYRY (CON'T)  41.4 - 41.8 - FLT UC 40"  Very brotion toma  QUARTE VEIN UC 45"  DAMARC DYKE - di Gray Hack  - biolite 350?  Varion Jones 45"  DAMARC TO 100 3030 45.6 49.0 1.0 c. 3 9 0.1 H  TYKE 12 70 3031 49.0 50.3	POSCHYRY (CON'T)  41.4 - 41.8 - FLT UC 40  Very brotion 50m0  GURDE Mn STRUM  45 90  GURDE Mn STRUM  12-Py 45 100 3030 45.6 49.0 1.0 C.3 9 0.1 HT  14 QUARTZ VEIN UC 45  DO MAFIC DYKE - di GYKU/Black  - biolite BSO?  - Varieta namew 40-C  STRUCCIS C 1 CM. C 70  DO: Py 20  SO.3 - 52 2 - STRUCK SKINGLA ALT  PY VN 30 100 3034 54.5 58.0 6.0 0.3 2 1.7 L.4 2  29 QUARTZ VEIN  DO GTZ VN 45  BE QUARTZ VEIN  PROPRIED  TO GO 3032 58.0 (C.5 3.0 0.2 9 0.3 0.1)  TO GUARTZ FEOZ REPLACEMENT  BRECCIA / MEGACITIMIC HERMINS  THE CH 10 CD 3076 605 (2.5 4.5 HZ 2.0.4 - 1)  TO STRUCCIS C GIZ VEIN  - It green C GIZ VEIN  DOST IN THE SO	POCPHYRY (CONT)  41.4 - 41.8 - FLT UC 40°  Very brotion, some  QUELLE MA STAIN  12-Py 45 100 3030 45.6 49.0 1.0 C.3 9 0.1 H  44 QUAKTZ VEIJU UC 45°  154 QUAKTZ VEIJU UC 45°  154 QUAKTZ VEIJU UC 45°  154 QUAKTZ VEIJU UC 45°  154 QUAKTZ VEIJU UC 45°  154 QUAKTZ VEIJU UC 45°  154 QUAKTZ VEIJU UC 45°  155 Q-CALE 70 100 3032 50.3 52.7 0.1 H 60 10	POCPHRY (CONT)  41.4 - 41.8 - FLT UC 40°  PO-PY 70 10 3029 42.4 45.60.605 7 0.402 3  Very broticn, 50m0  QUINCE Mn stain  P2-PY 45 100 3030 45.6 49.0 1.0 C.3 9 0.1 11 6  44 QUAKTZ VEIN UC 45°  TYKE L. 70 3031 49.0 50.3  D3 MARC DYKE - dic gruy Mack  - biolite 350 1	POCPHYRY (CON'T)  41.4 - 41.8 - FLT UC 40  PO-PH 45 100 3030 45.4 45.60.60.5 7 0.40.2 3 111  Nery brotion some  Quartz Venu UC 45  DYNE 12 70 8031 49.0 50.3	POCRY BY (CON'T)  41.4 - 41.8 - FLT UC 40"  Nery brotion some  Quality M Stain  Pa-Py 45 100 3030 85.6 49.0 1.0 C. 3 9 0.1 10 6 27  Ext QUARTZ VENU UC 45"  TYKE 12 76 3031 49.0 50.3	POCPUYEY (CONT)  41.4 - 41.8 - FLT UC 40"  Very brothen Soma  Quide Mn stain  Pa-Py 45 100 3030 45.6 49.0 1.0 6.3 9 0.1 hr 6 27  54 QUARTZ VEIN UC 45"  TYKE 12 76 3031 49.0 50.3	Pocryal (Cont)  41.4 - 41.8 - FLT UC 40  Pocry brother boma  45 90  Quide Mn Stain  Pocry 15 100 3030 45.6 49.0 1.0 6.3 9 0.1 m 6 27  Ext QUARTE VEIN UC 45  De Py 45 100 3030 45.6 49.0 1.0 6.3 9 0.1 m 6 27  De Py 45 100 3031 49.0 50.3	POCONY BY (COUT)  41.4 - 41.8 - FLT UC 40  Very brother sema  QUARTE VERY  DEPTH 45 100 3030 45.6 49.0 1.0 7.3 9 0.1 17 6 27  TYRE UL 70 3031 49.0 50.3	Poconyey (cont)  41.4 - 41.8 - FLT UC 40  Poly 10 10 3029 424 45.00.05 7 0.002 3 111  Very brotion some  Quille Mn Stain  Poly 45 100 3030 45.6 49.0 1.0 6.3 9 0.1 14  6.4 QUARTZ VE.I UC 45  TYVE LE 70 3031 49.0 50.3	Postphysy (con't)  41.4 - 41.8 - FLT UC 40"  Very brotten semo  guille Mn stain  18- Py +5 100 3030 85.6 49.0 1.0 C.3 9 0.1 Hr 6 27  54 QUARTZ VE.N UC 45"  19- Py +5 100 3030 85.6 49.0 1.0 C.3 9 0.1 Hr 6 27  10.3 MARC PYKE - dic gray /black  - brotte B50 9  - Cane To 100 3032 50.3 52.7 0.1 Hr 6 10 8 15  - Varien Annum 4-C  Structus <   Can

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		GEOLOGIC DESCRIPTION	L		s	TRUCTUR	Ε		SAMPL	23		MIN	ERAL	2				YEI	YS_	10z-	Pv	ICAP	B	W.	- Pu	ASSA	NYS	
ROM	TO		Š	FROM	TO	TYPE	TCA	%TCA	SAMPLE SAMPLE NUMBER	FROM	TO	Ру	Сру	K & O+	Cal	Coto	М	No. Vein	Cun	No. Ven	Cur	No. Ver	Cu	No.	Cur	Au.	Cu	4
			_	-			L					l	<u> </u>	1	l													
		K-SPAR MEGACRYSTIC PORAHVRY	_			12- Py	45		52oE	106.6	109.6	2.1	0.4	7	0.2	0.4	*			6	114	<u> </u>	2	<u> </u>	L_	ļ		
-		(cont)	$\vdash$			Marry	40	100				<del> </del> —	<u> </u>	<u> </u>		-					<u> </u>	_	1_	↓_	<u> </u>		L	$\perp$
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				<b>├</b> }		Pa-Py	40	100	3054	42.0	1,20	10.5.	10.	_ف	+7	N				4	54	-		<del></del>	<del> </del>		<del> </del> -	+-
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9.011	3	- mettled green with chlority							~340	1120 17	161.3	7.0	3.0	<del>                                     </del>	-	-	$\vdash$			-			-	+	<del> </del>		-	+-
-		4 green mica	$\vdash$			Pa-Pu	40	50	3057	1216	124 (	1.0	0.1	12	30	4		-		8	24	-	-	+-		<del> </del>	-	+
+		- 119.7-120.0 - 80% chlorite	Н			- '4	20	80	12	(21:3		† <del>``</del>		1.0	"	15		$\dashv$		13	LT	-	-	+	-		-	+-
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		- Cou - +5%		<b>-</b>		0.0	45	100	3058	1243	1275	OA	0.2	16	0.2	1				7	34	1	3	<del>                                     </del>	-	-	-	+
		- Cpy - +5% 254 bleb in Jug e119.6	-			700 Py		100	<u> </u>			٠.٠		•••							77	<del>- '-</del>	٦_	<u> </u>				<del> </del>
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	I					PO-Cy			3062	136.5	139.5	1.2	0.1	13	tr	*				5	41							1
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Hole No. 1223 Pg. 5 of

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												·				MIN	ERAL							1.30				
		GEOLOGIC DESCRIPTION			S	TRUCTUR			SAMPLE				ERAL					YEN	15-	Qz-	Py	CAR	В	QZ.	Ã.	A22A	24/	
FROM	TO		8	FROM	TO	TYPE	TCA	ХТСА	SAMPLE NUMBER	FROM	TO				Cal	Coto		No. Vein	Cum	No. Vetr	Cur	No. Vein	Cun thk	Na. Vein	Cun	Au.		40
													_					Ļ			<u> </u>							
		K-SPAR MEGACOISTIC PORPHYRY				Pa-Py	45	100	3064	142.5	45.0	2.2	0.2	12	+	ħ		1	2	4	35	↓		1	2		<u> </u>	
		(cen't)			_	ww-Py	45				ļ	_	ļ	_						<u> </u>	1	ļ						
		SHEETED 072 - Py VEINS.	$\sqcup$			1 34 /	40	60				_			<u> </u>		$\sqcup$			_	1	<del> </del>		80				
<b> </b>		J	$\vdash$			we	70-90	loD	3065	145.0	147.2	1.0	0.3	10	12	+				2	45	<b> </b>	$\sqcup$	6	22		ļ	<b> </b>
1/22		0.007.3 /5.1						-	2		4:25 -			-	-						-	ļ	$\vdash \dashv$					1
147.7	1250	QUARTZ VEIN - 95% OTZ-P4,	-						306	147.2	120.5	0.6	0.1	3	0.1	0.4	$\vdash$		_		<u> </u>	$\vdash$						
							<del> </del>		3267	1802	182 -	00		2	Δ.	0 -				_	<del> </del>	<del> </del>	<b>├</b>					
$\vdash$		- Spec. hem @ 150.9							ן טעב	130 6	137.2	10.8	0.1	-	0.7	2.5		-		-		-						
			$\vdash$		<u> </u>	PU-RI	11	100	3068	167 -	17.1 "	10		4	-	1.0	<b> </b>			<u> </u>	1,5				$\vdash$			
1	16	6 Mars 15 M	$\vdash$			100-19	#5	100	2008	153.2	P)6.0	<u> </u>	10.7	17_	pr	1.0			-	1	43	-	$\vdash \vdash$					
156	120.9	CWARTZ UEIN with massive by.	-			<u> </u>	-		2.70			-	1-	·-	1		-	-	_	ļ	-	-	$\vdash$					
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11.20	ILS. Z	MASSINE PURITE VEIN	$\vdash$			<del>                                     </del>			3074	167.9	169.3	<u> </u>		-	<del> </del>	-	H	7	40	-	+-	-					<del>                                     </del>	<del>                                     </del>
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171.8	174 3	QUACTZ VEN - 95% OTZ	-			1054	45	ler.	30.7	174 3	177.3	1.0	0.2	7	0.7	4-	$\vdash$			4	64	<del>                                     </del>						
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Hole No. | 223 Pg. 6 of

									Υ							MINE	RALIZ	ATIF	384						note	NO.1	23 6	9.6
		GEOLOGIC DESCRIPTION				·	-					J.,,,,	-n.			WINE	.KWE14	EINS	Jr4					.0.	ITE			
FROM	TO.	GENERAL MEDICAL TIMA	Ř.	EDUM	10	TYPE	TCA	VICA	SAMPLE	E00*	70	HIN	ERAL	. <u>Z</u>	TC	1ol	P	YRIT	E	z-P	<u>x</u>	CAR)	_	0	- 64	AZZA	72	
KUN	10		19	r KUM	15	11172	ILA	AICA	NUMBER	r KUM	10	Py	СРУ	Ke <sub>O</sub>	Lat	Coch	(`	ein t	hk \	en	thk	No. Vein	thk	No. Vein	thk	Au	Cu	40
		QUARTZ-FED REPLACEMENT BRECCIA	$\vdash$			Purky	70	20	3080	183.4	1864	40	0.3	И	1	1	-	+	-	3	40							-
···	-	SHEETED QUARTZ VEINS					40	60	1	-		1		1	<del>''</del>	†		_	+	1	<del>"</del>				$\vdash$			<del> </del>
							20	20					$\Box$						1	_		_						
						Pa-Py	40	100	3081	864	1894	2.6	0.1	13	4	+		1		4	50							
1930		QUACIZ - MAG STOCKWORK				Pary	40	100	3082	189.4	193.2	12.0	0.8	8	ħ	h	1	<b>-</b> 3	3 4	1	72	_			$\vdash$			-
			_			Py.		100			<u> </u>	┞	ļ	_					4									_
		THE COCE IS MORE	-					-	3083	193.Z	196 2	3.0	0.3	7	0.2	0.1	-+	+	$\dashv$	+	-			-				<del> </del>
		SILICEOUS TO 90% OTZ.																										
								ļ	5054	196.Z	199.2	3.0	0.2	10	<b>a3</b>	01	$\Box$	$\perp$			$\Box$							
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						WQ Py	40	100	3085	199.2	2017	12.4	0.1	0	0.2	0.1		+	+	-	-			2	7			<b>—</b>
				<del>                                     </del>		ac	90	134	3086	202.2	205.7	20	ne	4	0.2	1	-	-+-	+		$\dashv$	-	2		-			ļ
		•	-				-אדן	1	200		203.2	1	1.0	-	-12	J.	_	+		-+	$-\dagger$	`-	_					<del> </del>
		spec. hem with O-C stringers				QC.	90	100	3087	205.2	208.2	2.2	٩٢	Ю	0.2	0.8		+	+	7	-	5	10					
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						NO-Py	70		3028	208.2	211 2	1.8	tr	10	0.1	0.1								6	8			1
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			<u></u>								<u> </u>	L		<u> </u>		$\sqcup$		$\perp$	$\perp$			_						
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213,6 2	141	MASSIVE PURITE VEIN - 80% PH	_					1	3090	213.6	21+1	<u> </u>	_	1			-	+	_	+	-				$\vdash$			+
		- 15% 002				Rules			1			1								_								
		- 2-3% QQ3				MQ.	45	100	3091	214.1	2172	1.2	+1	12	0.3	0.1				$\Box$				6	20			Ī
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						<b>®</b>	3"	100	3-93	2202	223.2	1.9	0.2	11	0:2	0.6		1	$\downarrow$	$\rightrightarrows$	二	1	3					1.
-		strong chi				BULUZ	75	100	3094	223.2	226.2	18	0.2	14	0.1	0.1	$\dashv$	+	+	+	$\dashv$	-	-	7	14			-
<u> </u>		,	_				•						[			1 1						_	_		I			
						Borr 02	1)	18	اداسد	136.2	K4.5	1.0	12	115	14	M	l.,				1			6	12			

Hole No. 1223

			T-													MINE	DA.	7 A T	1401						HOLE	Novi	25 '	
		GEOLOGIC DESCRIPTION	1		_		_		<b></b>		··· •· · ·					HINE	KAL I	VEIN	Ž						4100	1,		
FROM	то	GENERAL DESCRIPTION	┢	Tconul.	TO	TYPE	TCA	IVTCA	SAMPLI	ES	70	HIN	ERAL	.S	16.	1 6		PYRI	TE	0z-	Py	CAF	₹8	<u>د</u>	7 7	ASSA	112	
r KUR	יי		139	FROM	טי	ITPE	ICA	AILA	SAMPLE NUMBER	FRUM	10	Py	СРУ	K.	Lai	Coco	ŀ	No. ∕ein	thk	NO. Velt	th	NO.	n thi	Ve	n thk	~	Lu	
		(700)										$\Box$													.l			
		OTZ . MAENETITE STUCKWOLK				Bul	45	100	3096	22A S	232 2	, 5	03	14	0.2	0.2								5	10			
																					Ι	<u> </u>		T	I		Γ	
									3297	2322	Z35.2	1.2	0.2	16	0.1	0.1	I				П	T			$I^{-}$			
																								T			$\Box$	
						wa Pu	70	75	3058	235.2	38.	1.0	1	15	0,3	0.1								13	41			
						11	20	25															T	T				
		·	Г														$\neg \neg$					1		1			$\Box$	
			Γ						3099	238.2	241.2	11.5	H	16	4	1						1	1					
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	Ī					74	45	IOD	3100	341.2	24.2	6.	tr	17	tu	tu		7	10									
			Г			<del>                                     </del>		-	K	T	[										_		1	1				
		NOTE NEW SAMPLE *	1						2867	24.2	247.7	1.3	W	14	tv	10	_				1	1	1	_	1-	1		
			Г						<u> </u>			1		1							1	1	1	$\top$				
			1	$\vdash$		Pu	50	100	58982	247.2	250.2	2.1	W	13	tr	tv		7	1			1			†			
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251.2	251.6	FLT. BADY ECONEN COLE	T						2869	250.2	253 2	1.8	tr	12	1.0	03						_			1			
-			Г																			1	_	1				
			┢	1		QTZ VN	30	100	2870	253.2	256.2	30	tr	10	0.5	0.5	$\neg$	2	4			1	1	1	80			
		253.1 - QTZ +CALCITE XTIALS IN	Г			24	30	100		-	, ,	1		1.5			$\neg$					1	<del> </del>	1	1			-
		NUG. ALSO BROWN CALCITE	5		-	<del></del>											_				1	1	1	$\vdash$				
			۲	1		WO. Py	30	100	2871	256.7	259.2	3.0	h	13	1.0	0.3	<u> </u>	_				1	1-	7	14		$\Box$	
		255.2 - 256.0 - BULL QTZ VEIN				1								"							1	_			1			
		with 2cm purite on							2872	259 2	264.0	0.5	tv	14	tv	+5								1				
		WITH ZEM purite ON EACH CENTROT.																				_	1					
																						1						
		290.4 - GTZ CALLITE AS ABOVE																				1	1	† <del></del>				
																		$\neg$		_		1		1				
		Chlorite ALT'N IS MOTERATE.															_					1	+	t	1			
																1	_	_			_	1	†	<b>—</b>	$\vdash$			
	264	EOH	_	1												1	<del>-</del> †	-				$\vdash$	-	†-··-	<del>  </del>			
			Н	<del>                                     </del>								<b>—</b>	_				$\dashv$	-+				-	+	+-	╁─┤		-	
				<del>                                     </del>													-	-				-	-	+	$\vdash$			
			-	<del>                                     </del>		<del> </del>				-				-	-	+	-	-	-		-	+-	+	-	┯			
			$\vdash$	-		<b></b>										-	$\dashv$	-+			-	+		-	+			· · · ·
			-	<del>  -</del>											-			-			-	-	+	-	$\vdash$		-	
				<u> </u>																			1	1				

# APPENDIX 3

1995 Drill Assay Tables

<b>DDH 1217</b>	ASSAY TA	BLE									
From	То	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
12.2	14.3	2251	2.1	0.05	0.8	288	22	0.105	1.68	604.8	46.2
14.3	17.4	2252	3.1	0.07	1.0	281	24	0.217	3.1	871.1	74.4
17.4	20.4	2253	3.0	0.04	1.0	264	18	0.12	3	792	54
20.4	23.5	2254	3.1	0.04	0.9	290	18	0.124	2.79	899	55.8
23.5	26.9	2255	3.4	0.06	1.0	408	35	0.204	3.4	1387.2	119
26.9	29.3	2256	2.4	0.05	0.9	309	65	0.12	2.16	741.6	156
29.3	32.6	2257	3.3	0.06	1.1	348	19	0.198	3.63	1148.4	62.7
32.6		2258	3.1	0.05	1.4	440	58	0.155	4.34	1364	179.8
35.7	38.7	2259	3.0	0.15	2.2	390	22	0.45	6.6	1170	66
38.7	41.0	2260	2.3	0.05	1.4	341	43	0.115	3.22	784.3	98.9
41.0	4	2261	0.9	0.12	2.6	413	24	0.108	2.34	371.7	21.6
41.9		2262	2.9	0.06	1.6	387	30	0.174	4.64	1122.3	87
44.8		2263	3.0	0.06	1.7	385	42	0.18	5.1	1155	126
47.8		2264	3.1	0.15	1.8	775	55	0.485	5.58	2402.5	170.5
50.9		2265	3.0	0.28	3.3	1190	85	0.84	9.9	3570	255
53.9		2266	3.1	0.23	3.8	972	120	0.713	11.78	3013.2	372
57.0		2267	3.0	0.08	0.8	402	190	0.24	2.4	1206	570
60.0	61.6	2268	1.6	0.05	0.6	412	102	0.08	0.96	659.2	163.2
61.6	63.1	2269	1.5	0.26	2.7	2360	182	0.39	4.05	3540	273
63.1	66.1	2270	3.0	0.44	2.4	3590	118	1.32	7.2	10770	354
66.1		2271	3.1	0.32	2.2	2190	124	0.992	6.82	6789	384.4
69.2		2272	3.0	0.34	3.0	2570	80	1.02	9	7710	240
72.2		2273	3.1	0.65	3.8	4180	128	2.015	11.78	12958	396.8
75.3		2274	3.0	0.73	4.0	3450	40	2.19	12	10350	120
78.3		2275	3.1	0.95	6.2	5800	40	2.945	19.22	17980	124
81.4		2276	3.0	0.88	6.9	4260	33	2.64	20.7	12780	99
84.4		2277	3.1	0.93	10.9	5710	42	2.883	33.79	17701	130.2
87.5		2278	3.0	0.58	2.7	3290	13	1.74	8.1	9870	39
90.5		2279	3.1	0.60	2.2	2520	5	1.86	6.82	7812	15.5
93.6		2280	3.0	0.42	2.2	2430	73	1.26		7290	219
96.6		2281	3.1	0.33	2.0	1550	8	1.023	6.2	4805	24.8
99.7		2282	3.0	0.19	1.8	2470	50	0.57	5.4	7410	150
102.7		2283		0.50	1.4			0.85		4216	
104.4		2284 2285	1.0		2.2	1440		0.63			
105.4 107.7		2285	2.3 2.5	0.32 0.35	1.0 1.2	1420 1245	6 8	0.736 0.875			13.8
110.2		2287	1.3	0.51	1.6	1919		0.663		3112.5 2494.7	20 14.3
111.5		2288	2.5	0.31	1.0			0.625			22.5
114.0		2289		0.42	1.6	2800	10	0.023		4760	

119.9   122.2   2292   2.3   0.78   2.1   3000   10   1.794   4.83   6900   23   122.2   124.0   2293   1.8   0.33   0.8   1700   10   0.594   1.08   3000   18   124.0   127.1   2294   3.1   0.36   0.8   1000   10   1.116   1.86   3100   31   127.1   130.1   2295   3.0   1.50   1.8   1000   10   4.5   4.8   3000   30   130.1   133.2   2296   3.1   0.36   1.4   1300   10   1.116   4.34   4030   31   133.2   136.2   2297   3.0   0.62   2.4   3600   10   1.86   7.2   10800   30   136.2   139.3   2298   3.1   0.76   2.3   2290   10   2.356   7.13   8990   31   139.3   142.3   2299   3.0   0.33   0.8   1000   10   0.99   2.4   3000   30   142.3   145.4   2300   3.1   1.60   2.0   2100   10   4.96   6.2   6510   31   145.4   148.4   2301   3.0   0.18   0.7   800   10   0.54   2.1   2400   30   145.4   148.4   2301   3.0   0.18   0.7   800   10   0.54   2.1   2400   30   151.5   154.5   2303   3.0   0.22   1.0   1000   10   0.66   3   3000   30   151.5   154.5   2303   3.0   0.22   1.0   1000   10   0.66   3   3000   30   151.5   154.5   2303   3.0   0.22   1.0   1000   10   0.66   3   3000   30   157.6   160.6   2305   3.0   0.22   1.0   600   10   0.558   3.1   2480   31   163.7   2306   3.1   0.18   1.0   800   10   0.558   3.1   2480   31   163.7   165.2   2307   1.5   0.13   0.5   400   10   0.95   0.75   600   166.7   170.6   2308   3.9   0.35   2.0   2400   10   1.365   7.8   9360   35   170.6   173.1   99999   2.5   0.00   0.0   0   0   0   0   0   0	From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
119.9   122.2   2292   2.3   0.78   2.1   3000   10   1.794   4.83   6900   23   122.2   124.0   2293   1.8   0.33   0.8   1700   10   0.594   1.08   3060   18   124.0   127.1   2294   3.1   0.36   0.8   1000   10   1.116   1.86   3100   31   127.1   130.1   2295   3.0   1.50   1.8   1000   10   4.5   4.8   3000   30   130.1   133.2   2296   3.1   0.36   1.4   1300   10   1.116   4.34   4030   31   133.2   136.2   2297   3.0   0.62   2.4   3600   10   1.166   7.2   10800   30   138.2   139.3   2298   3.1   0.76   2.3   2900   10   2.356   7.13   8990   31   139.3   142.3   2299   3.0   0.33   0.8   1000   10   0.99   2.4   3000   30   142.3   145.4   2300   3.1   1.60   2.0   2100   10   0.99   2.4   3000   30   142.3   145.4   2301   3.0   0.18   0.7   800   10   0.54   2.1   2400   30   145.4   146.4   2301   3.0   0.18   0.7   800   10   0.54   2.1   2400   30   154.5   157.6   2302   3.1   0.30   0.8   1000   20   0.93   2.48   3100   6.2   151.5   154.5   2303   3.0   0.22   1.0   1000   10   0.66   3   3000   30   154.5   157.6   2304   3.1   0.33   1.8   800   10   1.023   4.96   2480   31   157.6   160.6   2305   3.0   0.22   1.0   600   10   0.558   3.1   2480   31   156.7   165.2   2307   1.5   0.13   0.5   400   10   0.95   0.75   600   156.7   166.6   163.7   2306   3.1   0.18   1.0   800   10   0.558   3.1   2480   31   166.7   170.6   2308   3.9   0.35   2.0   2400   10   1.365   7.8   9360   38   170.6   173.1   175.9   2309   2.8   2.10   3.2   3400   20   5.88   8.96   9520   56   175.9   175.9   2310   3.0   0.37   1.5   1800   10   0.66   3   8.00   10   0.75   600   175.1   175.9   2309   2.8   2.10   3.2   3400   20   5.88   8.96   9520   56   175.9   175.9   2310   3.0   0.37   1.5   1800   10   0.66   3   1800   30   170.6   173.1   175.9   2309   2.8   2.10   3.2   3400   20   5.88   8.96   9520   56   175.9   175.9   2310   3.0   0.37   1.5   1800   10   0.14   4.5   5400   30   180.0   190.0   2314   2.0   0.18   1.0   200   10   0.36   2.7   1800   2.1   190.0   190.0   2314   2.0	115.7	117.9	2290	2.2	0.78	1.8	3800	10	1.672	3.96	8360	22
122.2   124.0   2293   1.8   0.33   0.6   1700   10   0.594   1.08   3060   18   124.0   127.1   2294   3.1   0.36   0.6   1000   10   1.116   1.86   3100   31   127.1   130.1   2295   3.0   1.50   1.8   1000   10   4.5   4.8   3000   30   130.1   133.2   2296   3.1   0.36   1.4   1300   10   1.116   4.34   4030   31   133.2   136.2   2297   3.0   0.62   2.4   3800   10   1.86   7.2   10800   30   136.2   139.3   2298   3.1   0.76   2.3   2900   10   2.356   7.13   8990   31   139.3   142.3   2299   3.0   0.33   0.8   1000   10   0.99   2.4   3000   30   142.3   145.4   2300   3.1   1.60   2.0   2100   10   4.96   6.2   6510   31   145.4   2300   3.1   1.60   2.0   2100   10   4.96   6.2   6510   31   145.4   148.4   2301   3.0   0.18   0.7   800   10   0.54   2.1   2400   30   144.4   151.5   2302   3.1   0.30   0.8   1000   20   0.93   2.48   3100   6.2   151.5   154.5   2303   3.0   0.22   1.0   1000   10   0.66   3   3000   30   154.5   157.6   2304   3.1   0.33   1.6   800   10   1.023   4.96   2480   31   157.6   160.6   2305   3.0   0.22   1.0   600   10   0.66   3   1800   30   160.6   163.7   2306   3.1   0.18   1.0   800   10   0.555   3.1   2480   31   163.7   165.2   2307   1.5   0.13   0.5   400   10   0.195   0.75   600   15   166.7   99999   1.5   0.00   0.0   0   0   0   0   0   0	117.9	119.9	2291	2.0	0.56	1.2	2200	10	1.12	2.4	4400	20
122.2   124.0   2293   1.8   0.33   0.8   1700   10   0.594   1.08   3060   18   124.0   127.1   2294   3.1   0.36   0.8   1000   10   1.116   1.88   3100   31   127.1   130.1   2295   3.0   1.50   1.8   1000   10   4.5   4.8   3000   30   130.1   133.2   2296   3.1   0.36   1.4   1300   10   1.116   4.34   4030   31   133.2   136.2   2297   3.0   0.62   2.4   3600   10   1.86   7.2   10800   30   136.2   139.3   2298   3.1   0.76   2.3   2900   10   2.356   7.13   8990   31   139.3   142.3   2299   3.0   0.33   0.8   1000   10   0.99   2.4   3000   30   142.3   145.4   2300   3.1   1.60   2.0   2100   10   4.96   6.2   6510   31   145.4   144.4   2301   3.0   0.18   0.7   800   10   0.54   2.1   2400   30   144.4   151.5   2302   3.1   0.30   0.8   1000   20   0.93   2.48   3100   6.2   151.5   154.5   2303   3.0   0.22   1.0   1000   10   0.66   3   3000   30   154.5   157.6   2304   3.1   0.33   1.8   800   10   1.023   4.96   2480   31   157.6   160.6   2305   3.0   0.22   1.0   600   10   0.66   3   1800   30   160.6   163.7   2306   3.1   0.18   1.0   800   10   0.555   3.1   2480   31   163.7   165.2   2307   1.5   0.13   0.5   400   10   0.195   0.75   600   156.6   163.7   2306   3.1   0.30   0.30   0.00   0.0	119.9	122.2	2292	2.3	0.78	2.1	3000	10	1.794	4.83	6900	23
124.0   127.1   2294   3.1   0.36   0.6   1000   10   1.116   1.86   3100   31     127.1   130.1   2295   3.0   1.50   1.6   1000   10   4.5   4.8   3000   30     130.1   133.2   2296   3.1   0.36   1.4   1300   10   1.116   4.34   4030   31     133.2   136.2   2297   3.0   0.62   2.4   3800   10   1.86   7.2   10800   30     136.2   139.3   2298   3.1   0.76   2.3   2900   10   2.355   7.13   8990   31     139.3   142.3   2299   3.0   0.33   0.8   1000   10   0.99   2.4   3000   30     142.3   145.4   2300   3.1   1.60   2.0   2100   10   4.96   6.2   6510   31     145.4   148.4   2301   3.0   0.18   0.7   800   10   0.54   2.1   2400   30     144.5   148.4   2301   3.0   0.18   0.7   800   10   0.54   2.1   2400   30     145.5   154.5   2302   3.1   0.30   0.8   1000   20   0.93   2.48   3100   62     151.5   154.5   2302   3.1   0.33   1.6   800   10   0.66   3   3000   30     154.5   157.6   2304   3.1   0.33   1.6   800   10   0.66   3   1800   30     156.6   163.7   2306   3.1   0.18   1.0   800   10   0.558   3.1   2480   31     163.7   165.2   2307   1.5   0.13   0.5   400   10   0.558   3.1   2480   31     163.7   165.2   2307   1.5   0.13   0.5   400   10   0.558   3.1   2480   31     170.6   173.1   99999   2.5   0.00   0.0   0   0   0   0   0   0     166.7   170.6   2308   3.9   0.35   2.0   2400   10   1.365   7.8   9360   33     170.6   173.1   99999   2.5   0.00   0.0   0   0   0   0   0   0     168.7   170.8   2301   3.0   0.24   0.8   800   10   0.72   2.4   2400   30     173.1   175.9   2309   2.8   2.10   3.2   3400   20   5.88   8.96   9520   56     175.9   178.9   2310   3.0   0.24   0.8   800   10   0.72   2.4   2400   30     176.0   176.1   177.3   177.3   177.5	122.2	124.0	2293	1.8	0.33	0.6	1700	10	0.594	1.08	3060	18
127.1   130.1   2295   3.0   1.50   1.6   1000   10   4.5   4.8   3000   30   30   130.1   133.2   2296   3.1   0.36   1.4   1300   10   1.116   4.34   4030   31   133.2   136.2   2297   3.0   0.62   2.4   3600   10   1.86   7.2   10800   30   136.2   139.3   2298   3.1   0.76   2.3   2290   10   2.356   7.13   8990   31   139.3   142.3   2299   3.0   0.33   0.8   1000   10   0.99   2.4   3000   30   30   31   42.3   2299   3.0   0.33   0.8   1000   10   0.99   2.4   3000   30   31   42.3   45.4   2301   3.0   0.18   0.7   800   10   0.54   2.1   2400   30   31   45.4   2301   3.0   0.18   0.7   800   10   0.54   2.1   2400   30   31   48.4   151.5   2302   3.1   0.30   0.8   1000   20   0.93   2.48   3100   62   3151.5   154.5   2303   3.0   0.22   1.0   1000   10   0.66   3   3000   30   31   35.4   157.6   160.6   2305   3.0   0.22   1.0   600   10   0.66   3   1800   31   3157.6   160.6   2305   3.0   0.22   1.0   600   10   0.66   3   1800   30   3160.6   163.7   2306   3.1   0.18   1.0   800   10   0.558   3.1   2480   31   163.7   165.2   2307   1.5   0.13   0.5   400   10   0.195   0.75   600   15   165.2   166.7   99999   1.5   0.00   0.0   0   0   0   0   0   0		127.1	2294	3.1	0.36	0.6	1000	10				
130.1   133.2   2296   3.1   0.36   1.4   1300   10   1.116   4.34   4030   31   133.2   136.2   2297   3.0   0.62   2.4   3600   10   1.86   7.2   10800   30   136.2   139.3   2298   3.1   0.76   2.3   2900   10   2.356   7.13   8990   31   139.3   142.3   2299   3.0   0.33   0.8   1000   10   0.99   2.4   3000   30   142.3   145.4   2300   3.1   1.60   2.0   2100   10   0.99   2.4   3000   30   142.3   145.4   2300   3.1   1.60   2.0   2100   10   0.99   2.4   3000   30   142.3   145.4   2301   3.0   0.18   0.7   800   10   0.54   2.1   2400   30   148.4   151.5   2302   3.1   0.30   0.8   1000   20   0.93   2.48   3100   62   151.5   154.5   2303   3.0   0.22   1.0   1000   10   0.66   3   3000   30   30   154.5   157.6   2304   3.1   0.33   1.6   800   10   1.023   4.96   2480   31   157.6   160.6   2305   3.0   0.22   1.0   6000   10   0.66   3   1800   30   160.6   163.7   2306   3.1   0.18   1.0   800   10   0.558   3.1   2480   31   163.7   165.2   2307   1.5   0.13   0.5   400   10   0.195   0.75   600   15   165.2   166.7   99999   1.5   0.00   0.0   0   0   0   0   0   0	127.1	130.1	2295	3.0	1.50	1.6	1000	10	4.5		3000	30
136.2				3.1	0.36		1300	10	1.116			31
139.3	133.2	136.2	2297	3.0	0.62	2.4	3600	10	1.86	7.2	10800	30
142.3         145.4         2300         3.1         1.60         2.0         2100         10         4.96         6.2         6510         31           145.4         148.4         2301         3.0         0.18         0.7         800         10         0.54         2.1         2400         30           148.4         151.5         2302         3.1         0.30         0.8         1000         20         0.93         2.48         3100         62           151.5         154.5         2303         3.0         0.22         1.0         1000         10         0.68         3         3000         30           155.5         157.6         2304         3.1         0.33         1.6         800         10         1.023         4.96         2480         31           157.6         160.6         2305         3.0         0.22         1.0         600         10         0.558         3.1         2480         31           160.7         160.6         163.7         2306         3.1         0.13         0.5         400         10         0.195         0.75         600         15           165.7         166.7         1799999 </td <td>136.2</td> <td>139.3</td> <td>2298</td> <td>3.1</td> <td>0.76</td> <td>2.3</td> <td>2900</td> <td>10</td> <td>2.356</td> <td>7.13</td> <td>8990</td> <td>31</td>	136.2	139.3	2298	3.1	0.76	2.3	2900	10	2.356	7.13	8990	31
145.4         148.4         2301         3.0         0.18         0.7         800         10         0.54         2.1         2400         30           148.4         151.5         2302         3.1         0.30         0.8         1000         20         0.93         2.48         3100         62           151.5         155.6         2304         3.1         0.33         1.6         800         10         1.023         4.96         2480         31           157.6         160.6         2305         3.0         0.22         1.0         600         10         0.66         3         1800         30           160.6         163.7         2306         3.1         0.18         1.0         800         10         0.558         3.1         2480         31           163.7         165.2         2307         1.5         0.13         0.5         400         10         0.195         0.75         600         15           165.2         166.7         99999         1.5         0.00         0.0         0         0         0         0         0         0         0         0         0         0         0         0	139.3	142.3	2299	3.0	0.33	0.8	1000	10	0.99	2.4	3000	30
148.4         151.5         2302         3.1         0.30         0.8         1000         20         0.93         2.48         3100         62           151.5         154.5         2303         3.0         0.22         1.0         1000         10         0.66         3         3000         30           154.5         157.6         2304         3.1         0.33         1.6         800         10         1.023         4.96         2480         31           157.6         160.6         2305         3.0         0.22         1.0         600         10         0.66         3         1800         30           160.6         163.7         2306         3.1         0.18         1.0         800         10         0.558         3.1         2480         31           165.7         165.2         2307         1.5         0.13         0.5         400         10         0.958         3.1         2480         31           166.7         170.6         2308         3.9         0.35         2.0         2400         10         1.365         7.8         9360         39           170.6         173.1         99999         2.5	142.3	145.4	2300	3.1	1.60	2.0	2100	10	4.96	6.2	6510	31
151.5	145.4	148.4				0.7						30
157.6	148.4	151.5		3.1		. 0.8				2.48		62
157.6	151.5	154.5	2303	3.0		1.0						30
160.6		157.6								4.96		31
163.7         165.2         2307         1.5         0.13         0.5         400         10         0.195         0.75         600         15           165.2         166.7         99999         1.5         0.00         0.0         <	157.6	160.6		3.0	0.22	1.0						30
165.2	160.6	163.7	2306	3.1	0.18	1.0	800				2480	
166.7         170.6         2308         3.9         0.35         2.0         2400         10         1.365         7.8         9360         39           170.6         173.1         199999         2.5         0.00         0.0         0	163.7	165.2	2307	1.5	0.13	0.5	400	10	0.195	0.75	600	15
170.6         173.1         99999         2.5         0.00         0.0         0	165.2	166.7	99999	1.5	0.00	0.0	0	0	0	0	. 0	0
173.1         175.9         2309         2.8         2.10         3.2         3400         20         5.88         8.96         9520         56           175.9         178.9         2310         3.0         0.24         0.8         800         10         0.72         2.4         2400         30           178.9         182.0         2311         3.1         0.31         1.6         1400         10         0.961         4.96         4340         31           182.0         185.0         2312         3.0         0.37         1.5         1800         10         1.11         4.5         5400         30           185.0         188.0         2313         3.0         0.21         0.9         600         10         0.63         2.7         1800         30           188.0         190.0         2314         2.0         0.18         1.0         200         10         0.63         2.7         1800         30           190.0         190.6         2315         0.6         1.40         16.8         900         10         0.84         10.08         540         6           190.0         190.6         2315         0.6	166.7	170.6	2308	3.9	0.35	2.0	2400	10	1.365	7.8	9360	39
175.9         178.9         2310         3.0         0.24         0.8         800         10         0.72         2.4         2400         30           178.9         182.0         2311         3.1         0.31         1.6         1400         10         0.961         4.96         4340         31           182.0         185.0         2312         3.0         0.37         1.5         1800         10         1.11         4.5         5400         30           185.0         188.0         2313         3.0         0.21         0.9         600         10         0.63         2.7         1800         30           188.0         190.0         2314         2.0         0.18         1.0         200         10         0.63         2.7         1800         30           190.0         190.6         2315         0.6         1.40         16.8         900         10         0.84         10.08         540         6           190.0         194.2         2316         3.6         0.33         2.0         1600         10         1.188         7.2         5760         36           194.2         196.3         2317         2.1	170.6	173.1	99999	2.5	0.00	0.0	0	0	0	0	0	0
178.9         182.0         2311         3.1         0.31         1.6         1400         10         0.961         4.96         4340         31           182.0         185.0         2312         3.0         0.37         1.5         1800         10         1.11         4.5         5400         30           185.0         188.0         2313         3.0         0.21         0.9         600         10         0.63         2.7         1800         30           188.0         190.0         2314         2.0         0.18         1.0         200         10         0.36         2         400         20           190.0         190.6         2315         0.6         1.40         16.8         900         10         0.84         10.08         540         6           190.6         194.2         2316         3.6         0.33         2.0         1600         10         1.188         7.2         5760         36           194.2         196.3         2317         2.1         1.42         4.8         3000         10         2.982         10.08         6300         21           196.3         197.3         2318         1.0	173.1	175.9	2309	2.8	2.10	3.2	3400	20	5.88	8.96	9520	56
178.9         182.0         2311         3.1         0.31         1.6         1400         10         0.961         4.96         4340         31           182.0         185.0         2312         3.0         0.37         1.5         1800         10         1.11         4.5         5400         30           185.0         188.0         2313         3.0         0.21         0.9         600         10         0.63         2.7         1800         30           188.0         190.0         2314         2.0         0.18         1.0         200         10         0.36         2         400         20           190.0         190.6         2315         0.6         1.40         16.8         900         10         0.84         10.08         540         6           190.6         194.2         2316         3.6         0.33         2.0         1600         10         1.188         7.2         5760         36           194.2         196.3         2317         2.1         1.42         4.8         3000         10         2.982         10.08         6300         21           196.3         197.3         2318         1.0	175.9	178.9	2310	3.0	0.24	0.8	800	10	0.72	2.4	2400	30
185.0         188.0         2313         3.0         0.21         0.9         600         10         0.63         2.7         1800         30           188.0         190.0         2314         2.0         0.18         1.0         200         10         0.36         2         400         20           190.0         190.6         2315         0.6         1.40         16.8         900         10         0.84         10.08         540         6           190.6         194.2         2316         3.6         0.33         2.0         1600         10         1.188         7.2         5760         36           194.2         196.3         2317         2.1         1.42         4.8         3000         10         2.982         10.08         6300         21           196.3         197.3         2318         1.0         0.70         13.8         11000         10         0.7         13.8         11000         10         17         13.8         11000         10         1.86         12         7200         20         199.3         202.1         2320         2.8         2.50         18.0         7600         10         7         50.4	178.9	182.0	2311	3.1	0.31	1.6	1400		0.961	4.96	4340	31
188.0         190.0         2314         2.0         0.18         1.0         200         10         0.36         2         400         20           190.0         190.6         2315         0.6         1.40         16.8         900         10         0.84         10.08         540         6           190.6         194.2         2316         3.6         0.33         2.0         1600         10         1.188         7.2         5760         36           194.2         196.3         2317         2.1         1.42         4.8         3000         10         2.982         10.08         6300         21           196.3         197.3         2318         1.0         0.70         13.8         11000         10         0.7         13.8         11000         10         10         0.7         13.8         11000         10         1.86         12         7200         20         199.3         202.1         2320         2.8         2.50         18.0         7600         10         1.86         12         7200         20         20         20         20         20         20         20         20         20         20         20	182.0	185.0		3.0								30
190.6       194.2       2316       3.6       0.33       2.0       1600       10       1.188       7.2       5760       36         194.2       196.3       2317       2.1       1.42       4.8       3000       10       2.982       10.08       6300       21         196.3       197.3       2318       1.0       0.70       13.8       11000       10       0.7       13.8       11000       10         197.3       199.3       2319       2.0       0.93       6.0       3600       10       1.86       12       7200       20         199.3       202.1       2320       2.8       2.50       18.0       7600       10       7       50.4       21280       28         202.1       203.3       2321       1.2       1.58       10.4       8200       10       1.896       12.48       9840       12         203.3       205.4       2322       2.1       0.58       2.8       2200       30       1.218       5.88       4620       63         205.4       206.3       2323       0.9       1.09       5.8       3600       80       0.981       5.22       3240       72 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>30</td>												30
190.6       194.2       2316       3.6       0.33       2.0       1600       10       1.188       7.2       5760       36         194.2       196.3       2317       2.1       1.42       4.8       3000       10       2.982       10.08       6300       21         196.3       197.3       2318       1.0       0.70       13.8       11000       10       0.7       13.8       11000       10         197.3       199.3       2319       2.0       0.93       6.0       3600       10       1.86       12       7200       20         199.3       202.1       2320       2.8       2.50       18.0       7600       10       7       50.4       21280       28         202.1       203.3       2321       1.2       1.58       10.4       8200       10       1.896       12.48       9840       12         203.3       205.4       2322       2.1       0.58       2.8       2200       30       1.218       5.88       4620       63         205.4       206.3       2323       0.9       1.09       5.8       3600       80       0.981       5.22       3240       72 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>20</td>												20
194.2         196.3         2317         2.1         1.42         4.8         3000         10         2.982         10.08         6300         21           196.3         197.3         2318         1.0         0.70         13.8         11000         10         0.7         13.8         11000         10           197.3         199.3         2319         2.0         0.93         6.0         3600         10         1.86         12         7200         20           199.3         202.1         2320         2.8         2.50         18.0         7600         10         7         50.4         21280         28           202.1         203.3         2321         1.2         1.58         10.4         8200         10         1.896         12.48         9840         12           203.3         205.4         2322         2.1         0.58         2.8         2200         30         1.218         5.88         4620         63           205.4         206.3         2323         0.9         1.09         5.8         3600         80         0.981         5.22         3240         72           206.3         209.4         2324												
196.3       197.3       2318       1.0       0.70       13.8       11000       10       0.7       13.8       11000       10         197.3       199.3       2319       2.0       0.93       6.0       3600       10       1.86       12       7200       20         199.3       202.1       2320       2.8       2.50       18.0       7600       10       7       50.4       21280       28         202.1       203.3       2321       1.2       1.58       10.4       8200       10       1.896       12.48       9840       12         203.3       205.4       2322       2.1       0.58       2.8       2200       30       1.218       5.88       4620       63         205.4       206.3       2323       0.9       1.09       5.8       3600       80       0.981       5.22       3240       72         206.3       209.4       2324       3.1       1.40       12.8       5200       120       4.34       39.68       16120       372         209.4       212.4       2325       3.0       1.05       8.0       2600       140       3.15       24       7800       420<												36
197.3         199.3         2319         2.0         0.93         6.0         3600         10         1.86         12         7200         20           199.3         202.1         2320         2.8         2.50         18.0         7600         10         7         50.4         21280         28           202.1         203.3         2321         1.2         1.58         10.4         8200         10         1.896         12.48         9840         12           203.3         205.4         2322         2.1         0.58         2.8         2200         30         1.218         5.88         4620         63           205.4         206.3         2323         0.9         1.09         5.8         3600         80         0.981         5.22         3240         72           206.3         209.4         2324         3.1         1.40         12.8         5200         120         4.34         39.68         16120         372           209.4         212.4         2325         3.0         1.05         8.0         2600         140         3.15         24         7800         420           212.4         215.5         2326												
203.3     205.4     2322     2.1     0.58     2.8     2200     30     1.218     5.88     4620     63       205.4     206.3     2323     0.9     1.09     5.8     3600     80     0.981     5.22     3240     72       206.3     209.4     2324     3.1     1.40     12.8     5200     120     4.34     39.68     16120     372       209.4     212.4     2325     3.0     1.05     8.0     2600     140     3.15     24     7800     420       212.4     215.5     2326     3.1     0.51     1.8     1900     60     1.581     5.58     5890     186												10
203.3     205.4     2322     2.1     0.58     2.8     2200     30     1.218     5.88     4620     63       205.4     206.3     2323     0.9     1.09     5.8     3600     80     0.981     5.22     3240     72       206.3     209.4     2324     3.1     1.40     12.8     5200     120     4.34     39.68     16120     372       209.4     212.4     2325     3.0     1.05     8.0     2600     140     3.15     24     7800     420       212.4     215.5     2326     3.1     0.51     1.8     1900     60     1.581     5.58     5890     186												20
203.3     205.4     2322     2.1     0.58     2.8     2200     30     1.218     5.88     4620     63       205.4     206.3     2323     0.9     1.09     5.8     3600     80     0.981     5.22     3240     72       206.3     209.4     2324     3.1     1.40     12.8     5200     120     4.34     39.68     16120     372       209.4     212.4     2325     3.0     1.05     8.0     2600     140     3.15     24     7800     420       212.4     215.5     2326     3.1     0.51     1.8     1900     60     1.581     5.58     5890     186												28
205.4         206.3         2323         0.9         1.09         5.8         3600         80         0.981         5.22         3240         72           206.3         209.4         2324         3.1         1.40         12.8         5200         120         4.34         39.68         16120         372           209.4         212.4         2325         3.0         1.05         8.0         2600         140         3.15         24         7800         420           212.4         215.5         2326         3.1         0.51         1.8         1900         60         1.581         5.58         5890         186												
206.3     209.4     2324     3.1     1.40     12.8     5200     120     4.34     39.68     16120     372       209.4     212.4     2325     3.0     1.05     8.0     2600     140     3.15     24     7800     420       212.4     215.5     2326     3.1     0.51     1.8     1900     60     1.581     5.58     5890     186												72
209.4     212.4     2325     3.0     1.05     8.0     2600     140     3.15     24     7800     420       212.4     215.5     2326     3.1     0.51     1.8     1900     60     1.581     5.58     5890     186												372
212.4 215.5 2326 3.1 0.51 1.8 1900 60 1.581 5.58 5890 186												
1 215.5  217.9  2327  2.4  1.48  3.8  3800  50  3.552  9.12  9120  120	215.5			2.4	1.48							

Mo(w*a)	Cu(w*a)	Ag (w°a)	Au (w*a)	Mo ppm	Cu ppm	Ag ppm	Au ppm	Width m	Number	To	From
0	0	0	0	0	0	0.0	0.00	0.6	99999	218.5	217.9
62	2480	4.34	0.62	20	800	1.4	0.20	3.1	2328	221.6	218.5
42	2100	8.4	0.99	14	700	2.8	0.33	3.0	2329	224.6	221.6
21.6	1200	3.84	0.432	9	500	1.6	0.18	2.4	2330	227.0	224.6
27	900	1.2	0.21	9	300	0.4	0.07	3.0	2331	230.0	227.0
30	2400	3.6	0.51	10	800	1.2	0.17	3.0	2332	233.0	230.0
21 51	2400	4.8	0.66	7	800	1.6	0.22	3.0	2333	236.0	233.0
51	4500	6	0.96	17	1500	2.0	0.32	3.0	2334	239.0	236.0
36	1800	2.4	0.9	12	600	0.8	0.30	3.0	2335	242.0	239.0
66	2100	3	0.39	22	700	1.0	0.13	3.0	2336	242.0	242.0
69	1800	2.4	0.48	23	600	0.8	0.16	3.0	2337	248.0	242.0
114	900	1.2	0.24	38	300	0.4	0.08	3.0	2338	251.0	248.0
114	1500	1.8	0.33	38	500	0.6	0.11	3.0	2339	254.0	251.0
36	2400	1.8	0.3	12	800	0.6	0.10	3.0	2340	257.0	254.0
90	2400	4.5	0.93	30	800	1.5	0.31	3.0	2341	260.0	257.0
42	1200	1.5	0.33	14	400	0.5	0.11	3.0	2342	263.0	260.0
75	2400	3	0.51	25	800	1.0	0.17	3.0	2343	266.0	263.0
54	4800	5.4	0.96	18	1600	1.8	0.32	3.0	2344	269.0	268.0
96	3000	3	1.26	32	1000	1.0	0.42	3.0	2345	272.0	269.0
	3000	2.4	0.66	14	1000	0.8	0.22	3.0	2346	275.0	272.0
	3300	4.2	0.87	23	1100	1.4	0.29	3.0	2347	278.0	275.0
		1.8	0.99	16	600	0.6	0.33	3.0	2348	281.0	278.0
				22	800	0.9	0.18	3.0	2349	284.0	281.0
		1.8		14	400	0.6	0.07	3.0	2350	287.0	284.0
				34	300	0.4	0.08	3.0	2351	290.0	287.0
				27	1000	1.4	0.43	3.0	2352	293.0	290.0
				66	800	1.2	0.18	3.0	2353	296.0	293.0
				26	1000	1.0	0.23	3.0	2354	299.0	296.0
	<u> </u>			16	400	0.6	0.05	3.0	2355	302.0	299.0
				28	600	1.0	0.17	3.0	2356	305.0	302.0
				16 14	600 1200	1.0	0.15	3.0	2357	308.0	305.0
				15	1100	1.6	0.30	3.0	2358	311.0	308.0
				L	600	1.2 0.7	0.31	3.0	2359	314.0	311.0
			+				0.09		2360	317.0	314.0
										320.0	317.0
			<del></del>							322.9 324.7	320.0 322.9
										328.0	324.7
<del></del>										331.0	328.0
							L	T-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1		334.0	331.0

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
334.0	337.0	2367	3.0	0.22	1.8	800	30	0.66	5.4	2400	90
337.0	340.0	2368	3.0	0.10	0.4	200	9	0.3	1.2	600	27
340.0	343.0	2369	3.0	0.08	0.3	400	38	0.24	0.9	1200	114
343.0	346.0	2370	3.0	0.05	0.4	200	14	0.15	1.2	600	42
346.0	349.3	2371	3.3	0.29	1.9	100	52	0.957	6.27	330	171.6
349.3	352.0	2372	2.7	0.08	0.6	300	4	0.216	1.62	810	10.8
352.0	355.0	2373	3.0	0.06	0.2	200	5	0.18	0.6	600	15
355.0	358.0	2374	3.0	1.34	5.2	4400	12	4.02	15.6	13200	36
358.0	361.0	2375	3.0	0.17	1.0	600	10	0.51	3	1800	30
361.0	364.0	2376	3.0	0.27	1.0	700	14	0.81	3	2100	42
364.0	367.1	2377	3.1	0.15	1.0	500	6	0.465	3.1	1550	18.6
367.1	368.3	2378	1.2	0.20	0.6	500	26	0.24	0.72	600	31.2
368.3	369.0	2451	0.7	0.38	3.4	3000	30	0.266	2.38	2100	21
369.0	370.1	2452	1.1	4.20	8.6	12500	52	4.62	9.46	13750	57.2
370.1	371.5	2453	1.4	1.11	6.2	7200	140	1.554	8.68	10080	196
371.5	373.9	2454	2.4	2.50	10.3	12200	122	6	24.72	29280	292.8 75
373.9		2455	1.5	0.98	4.8	5000	50		7.2		15.6
375.4	378.0	2379	2.6	0.22	0.8	400	6	0.572	2.08		18
378.0		2380	3.0	0.22	0.8	400	6		2.4	1200 4500	144
381.0		2381	3.0	0.44	1.2	1500	48		3.6 1.2	1500	30
384.0		2382	3.0	0.14	0.4	500	10				24
387.0			3.0	0.39		400	8		0.6	<del></del>	36
390.0			3.0	0.15		200					30
393.0	396.0	2385		0.13		600			1.2 1.2		90
396.0						600	<del></del>				
399.0	402.0	2387	3.0								
402.0	405.0										
405.0	408.0						<u> </u>				
408.0	411.0										
411.0							L				
414.0											
417.0											
420.0	423.4	2394	3.4	0.24	1.6	2400	18	0.816	5.44	0 100	01.2

From	То	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
12.2 m - 61.6 m											
Total (w*a)			49.4	4.61	76.6	23262	2678				
Mean				0.09	1.6	471	54				
61.6 m - 145.4 ı	n										·
Total (w*a)			83.8	50.02	221.6	221342	2997				
Mean				0.60	2.6	2641	36				
145.4 m - 190.6	m										
Total (w*a)			45.2	16.43	62.8	49620	471				
Mean				0.36	1.4	1098	10				
190.6 m - 217.9	m				-						
Total (w*a)			27.3	30.45	195.4	108170	1360				
Mean				1.12	7.2	3962	50				
217.9 m - 368.3	m										
Total (w*a)			150.4	32.88	168.5	115910	3143				
Mean				0.22	1.1	771	21				
368.3 m - 375.4	m										
Total (w*a)			7.1	13.91	52.4	62710	642				
Mean				1.96	7.4	8832	90				
375.4 m - 399.0	m										
Total (w*a)			23.6	5.49	15.3	13640	388				
Mean				0.23	0.6	578	16				
399.0 m - 423.4	m										
Total (w*a)			24.4	9.97	36.0	59160	388				
Mean				0.41	1.5	2425	16				
12.2 m - 423.4	m						1		/ <del>-</del>		
Total (w*a)			411.2	163.76	828.6	653814	12066				
Mean				0.40	2.0	1590					

<b>DDH 1218</b>	ASSAY TA	BLE									
From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
3.0	7.0	2501	4.0	1.18	4.5	3360	19	4.72	18	13440	76
7.0	10.0	2502	3.0	0.76	4.9	3410	32	2.28	14.7	10230	96
10.0	12.1	2503	2.1	1.68	7.4	3690	15	3.528	15.54	7749	31.5
12.1	14.2	2504	2.1	0.34	1.9	1050	23	0.714	3.99	2205	48.3
14.2	16.2	2505	2.0	0.24	2.2	1260	14	0.48	4.4	2520	28
16.2	19.2	2506	3.0	0.23	2.4	1150	14	0.69	7.2	3450	42
19.2	21.4	2507	2.2	0.32	2.5	1890	8	0.704	5.5	4158	17.6
21.4	24.1	2508	2.7	0.89	5.1	1720	20	2.403	13.77	4644	54
24.1	25.6	2509	1.5	0.78	20.2	2250	48	1.17	30.3	3375	72
25.6	28.3	2510	2.7	0.63	3.4	1960	21	1.701	9.18	5292	56.7
28.3	31.4	2511	3.1	0.62	3.6	2660	54	1.922	11.16	8246	167.4
31.4	34.5	2512	3.1	0.61	3.3	1560	26	1.891	10.23	4836	80.6
34.5	37.5	2513	3.0	0.98	5.6	2220	76	2.94	16.8	6660	228
37.5		2514	3.0	1.05	3.6	1680	94	3.15	10.8	5040	282
40.5	43.6	2515	3.1	1.04	4.6	2280	218	3.224	14.26	7068	675.8
43.6	46.6	2516	3.0	0.35	2.8	1560	16	1.05	8.4	4680	48
46.6	49.7	2517	3.1	1.36	3.7	950	40	4.216		2945	124
49.7	52.7	2518	3.0	1.40	3.4	1450	130	4.2			390
52.7	55.8	2519	3.1	0.51	3.3	1810	65	1,581			201.5
55.8	58.4	2520	2.6	0.28	2.4	1920	27	0.728			70.2
58.4	61.3	2521	2.9	0.59	5.4	1430	38	1.711	15.66		110.2
61.3		2522	2.1	0.25	1.8	1730	9				18.9
63.4		2523	1.7	0.26	1.3	1690		0.442			28.9
65.1	68.3	2524	3.2	0.44	3.8	2680		1.408			70.4
68.3	71.0	2525	2.7	0.99	6.9	4500		2.673			72.9
71.0	74.1	2526	3.1	0.69	11.4	4820					37.2
74.1		2527	3.0	0.51	2.5	2290					96
77.1		2528	3.1	0.33	1.2	1640					49.6
80.2		2529	3.0	0.83							66
83.2		2530		0.29							24.8
86.3			3.0	1.58							168
89.3		2532		1.24							100.8
91.4											38
92.4		2534	3.0								
95.4				0.52							
98.											<u> </u>
101.	1 104.5		<u> </u>								1
104.	5 107.6										
107.0	8 110.6	2539	3.0	0.60	4.1	3000	136	1.8	12.3	9000	400

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
110.6	113.1	2540	2.5	0.91	4.5	4360	10	2.275	11.25	10900	25
113.1	115.9	2541	2.8	0.28	1.0	2070	18	0.784	2.8	5796	50.4
115.9	118.7	2542	2.8	0.87	4.5	1580	38	2.436	12.6	4424	106.4
118.7	121.5	2543	2.8	0.30	1.0	2450	44	0.84	2.8	6860	123.2
121.5	122.8	2544	1.3	0.60	4.6	8120	104	0.78	5.98	10556	135.2
122.8	125.9	2545	3.1	0.58	1.4	1640	30	1.798	4.34	5084	93
125.9	128.9	2546	3.0	0.87	4.5	3270	16	2.61	13.5	9810	48
128.9	131.8	2547	2.9	0.35	2.5	1950	12	1.015	7.25	5655	34.8
131.8	132.7	99999	0.9	0.00	0.0	0	0	0	0	0	0
132.7	135.0	2548	2.3	0.23	0.6	930	12	0.529	1.38	2139	27.6
135.0	138.1	2549	3.1	0.15	0.5	545	8	0.465	1.55	1689.5	24.8
138.1	139.8	2550	1.7	0.71	3.8	3500	12	1.207	6.46	5950	20.4
139.8	141.6	2551	1.8	0.54	2.7	2520	11	0.972	4.86	4536	19.8
141.6	144.2	2552	2.6	0.68	2.8	2630	16	1.768	7.28	6838	41.6
144.2	146.4	2553	2.2	0.35	1.6	1670	6	0.77	3.52	3674	13.2
146.4	149.3	2554	2.9	0.13	1.0	620	9	0.377	2.9	1798	26.1
149.3	152.4	2555	3.1	0.10	0.8	575	11	0.31	2.48	1782.5	34.1
152.4	155.1	2556	2.7	0.34	2.0	920	13	0.918	5.4	2484	35.1
155.1	156.4	2557	1.3	0.29	2.6	1330	10	0.377	3.38	1729	13
156.4	159.4	2558	3.0	0.29	2.6	1170	14	0.87	7.8	3510	42
159.4	162.5	2559	3.1	0.39	4.0	1940	12	1.209	12.4	6014	37.2
162.5	165.5	2560	3.0	0.11	1.2	455	14	0.33	3.6	1365	42
165.5	168.6	2561	3.1	0.08	1.2	422	7	0.248	3.72	1308.2	21.7
168.6	171.6	2562	3.0	0.09	0.8	418	10		2.4	1254	30
171.6	173.8	2563	2.2	0.27	1.8	1106	9		3.96	2433.2	19.8
173.8	176.1	2564	2.3	1.71	10.6	6700	22		1	15410	50.6
176.1	179.5	2565	3.4	0.29	3.4	1820	10			6188	34
179.5	182.4	2566		0.28	2.9	1540				4466	26.1
182.4	184.0	2567		1.56	10.4	8000				12800	14.4
184.0				1.67	7.5	6800					10.4
185.3	187.6			2.40	10.5	9100					
187.6	189.9	<u></u>		0.44	2.9	2300				5290	
189.9		2571	3.0	0.54	1.2	910			+		
192.9		2572		0.33	1.4	1310	<del></del>		<del></del>	<del></del>	<del></del>
194.1											
196.6				0.77	5.4						
199.0				0.18	1.5						
200.9				0.19	0.6				<del></del>		
202.4				0.25	1.9						
204.3	208.1	2578	3.8	0.24	1.4	1200	200	0.912	5.32	4560	760

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From	То	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w°a)	Cu(w*a)	Mo(w*a)
208.1	211.1	2579	3.0	0.26	1.8	1100	12	0.78	5.4	3300	36
211.1	214.0	2580	2.9	0.40	2.4	2500	24	1.16	6.96	7250	69.6
214.0	217.0	2581	3.0	0.51	2.0	3000	14	1.53	6	9000	42
217.0	220.0	2582	3.0	0.36	1.1	1000	9	1.08	3.3	3000	27
220.0	223.0	2583	3.0	0.25	1.2	800	9	0.75	3.6	2400	27
223.0	226.0	2584	3.0	0.42	3.8	3800	14	1.26	11.4	11400	42
226.0	229.0	2585	3.0	0.30	2.0	2000	12	0.9	6	6000	36
229.0	232.0	2586	3.0	0.58	2.6	3000	12	1.74	7.8	9000	36
232.0	235.0	2587	3.0	0.11	1.1	1000	12	0.33	3.3	3000	36
235.0	238.0	2588	3.0	0.27	1.8	1400	12	0.81	5.4	4200	36
238.0	241.0	2589	3.0	0.43	2.2	1400	6	1.29	6.6	4200	18
241.0	244.0	2590	3.0	0.32	25.0	1800	68	0.96	75	5400	204
244.0	247.0	2591	3.0	0.30	6.8	3600	8	0.9	20.4	10800	24
247.0	250.0	2592	3.0	0.16	3.6	2400	6	0.48	10.8	7200	18
250.0	253.0	2593	3.0	0.25	1.4	2000	38	0.75	4.2	6000	114
253.0	256.0	2594	3.0	0.35	4.5	2000	20	1.05	13.5	6000	60
256.0	259.0	2595	3.0	0.38	9.0	1900	12	1.14	27	5700	36
259.0	262.0	2596	3.0	0.29	2.4	900	6	0.87	7.2	2700	18
262.0	265.0	2597	3.0	0.20	2.6	2400	18	0.6	7.8	7200	54
265.0	268.0	2598	3.0	0.42	3.8	2200	10	1.26	11.4	6600	30
268.0	271.0	2599	3.0	0.26	2.4	1600	10	0.78	7.2	4800	30
271.0	274.0	2600	3.0	0.16	2.2	1400	6	0.48	6.6	4200	18
274.0	277.0	2601	3.0	0.19	1.4	600	5	0.57	4.2	1800	15
277.0	280.0	2602	3.0	0.25	1.8	1000	11	0.75	5.4	3000	33
280.0	283.0	2603	3.0	0.45	3.4	2000	9	1.35	10.2	6000	27
283.0	286.0	2604	3.0	0.31	2.2	1500	6	0.93	6.6	4500	18
286.0	290.0	2605	4.0	0.24	2.5	1000	18	0.96	10	4000	72
290.0	291.5	2606	1.5	0.12	1.6	1200	12	0.18	2.4	1800	18
291.5	294.0	2607	2.5	0.07	1.2	800	6	0.175	3		15
294.0	297.0	2608	3.0	0.14	1.4	1000	6	0.42	4.2	3000	18
297.0	300.0	2609	3.0	0.11	1.4	1200	5	0.33	4.2	3600	15
300.0	303.0	2610	3.0	0.14	1.8	800	10	0.42	5.4	2400	30
303.0	306.0	2611	3.0	0.74	12.0	3500	16	2.22	36	10500	48
306.0	309.0	2612	3.0		2.4						
309.0	312.0	2613	3.0	0.56	3.0		8	1.68	9	<del>1</del>	
312.0	315.0	2614	3.0	0.70	6.0		12		18	<del></del>	L
315.0	318.0	2615	3.0	0.38	2.6		10	1.14	7.8		
318.0	321.0	2616	3.0	0.23	2.1	1500	10	0.69	6.3		<u> </u>
321.0	324.0	2617	3.0	0.33	3.2			0.99			
324.0	327.0	2618	3.0	0.32	9.6	3600	14	0.96	28.8	10800	42

From	То	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
327.0	330.0	2619	3.0	0.15	1.0	1200	110	0.45	3	3600	330
330.0	333.0	2620	3.0	0.22	0.4	900	8	0.66	1.2	2700	24
333.0	336.0	2621	3.0	0.08	3.2	1400	12	0.24	9.6	4200	36
336.0	339.0	2622	3.0	0.06	1.4	900	10	0.18	4.2	2700	30
339.0	342.0	2623	3.0	0.23	1.0	2800	16	0.69	3	8400	48
342.0	345.0	2624	3.0	0.20	1.4	4000	30	0.6	4.2	12000	90
345.0	348.0	2625	3.0	0.33	1.6	1000	26	0.99	4.8	3000	78
348.0	351.0	2626	3.0	0.12	0.9	600	12	0.36	2.7	1800	36
351.0	354.0	2627	3.0	0.16	2.0	1400	14	0.48	6	4200	42
354.0	357.0	2628	3.0	0.17	1.1	800	34	0.51	3.3	2400	102
357.0	360.0	2629	3.0	0.15	0.6	1000	9	0.45	1.8	3000	27
360.0	363.0		3.0	0.40	0.9	1800	7	1.2	2.7	5400	21
363.0	366.0		3.0	0.22	0.8	1200	8	0.66	2.4	3600	24
366.0	369.0	2632	3.0	0.08	0.3	400	10	0.24	0.9	1200	30
369.0	372.0	2633	3.0	0.05	0.2	600	18	0.15	0.6		54
372.0	375.0	2634	3.0	0.09	1.2		9	0.27			27
375.0		2635	3.0	0.15	0.4		15	0.45			45
378.0	381.0	2636	3.0	0.07	0.3		6	0.21	0.9		18
381.0		2637	3.0		0.6		11	0.24	L	1800	33
384.0	387.0	2638	3.0	0.12	0.4		18				54
387.0	390.0	2639	3.0	0.25	0.3		6		<u> </u>		18
390.0	391.4	2640	1.4	0.09	0.2			<u> </u>	<del></del>		
391.4	394.1	2641	2.7	0.13	0.8					<del>• · · · · · · · · · · · · · · · · · · ·</del>	16.2
394.1	396.6	2642			0.4					1500	15
396.6	400.0		3.4	0.05	0.3						20.4
400.0			4.0		0.3						32
404.0	408.1	2645	4.1	0.01	0.2	300	8	0.041	0.82	1230	32.8

From	То	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
3.0 m - 131.8	m										
Total (w*a)			128.8	94.87	513.9	342195	5193				
Mean				0.74	4.0	2657	40				
131.8 m - 173	.8 m										
Total (w*a)			42.0	11.21	73.1	48504	448				
Mean				0.27	1.7	1155	11				
173.8 m - 199	).0 m										
Total (w*a)			25.2	21.54	123.3	90711	260				
Mean				0.85	4.9	3600	10				
199.0 m - 366	i.0 m										
Total (w*a)			167.0	46.70	496.7	290948	3299				
Mean				0.28	3.0	1742	20				
366.0 m - 408	3.1 m										
Total (w*a)			42.1	3.64	17.6	23750	412				
Mean				0.09	0.4	564	10				
3.0 m - 366.0	m										
Total (w*a)			363.0	174.32	1207.1	772358	9199				
Mean				0.48	3.3	2128	25				
3.0 m - 408.1	m										
Total (w*a)			405.1	177.96	1224.7	796108	9612				
Mean				0.44	3.0	1965	24				

11-4-4-3										ASSAY TA	
Mo(w*a)	Cu(w*a)	Ag (w*a)	Au (w*a)	Mo ppm	Cu ppm	Ag ppm	Au ppm	Width m	Number	To	From
96	2280	21	0.51	32	760	7.0	0.17	3.0	2469	27.1	24.1
174	2544	7.2	0.39	58	848	2.4	0.13	3.0	2470	30.1	27,1
144	3780	16.8	0.81	48	1260	5.6	0.27	3.0	2471	33.1	30.1
90	2400	4.8	0.45	30	800	1.6	0.15	3.0	2472	36.1	33.1
600	6840	5.4	0.72	200	2280	1.8	0.24	3.0	2473	39.1	36.1
270	2190	3	0.33	90	730	1.0	0.11	3.0	2474	42.1	39.1
204	2040	2.4	0.21	68	680	0.8	0.07	3.0	2475	45.1	42.1
354	2430	1.8	0.27	118	810	0.6	0.09	3.0	2476	48.1	45.1
426	2004	1.5	0.24	142	668	0.5	0.08	3.0	2477	51.1	48.1
222	15180	11.1	1.35	74	5060	3.7	0.45	3.0	2478	54.1	51.1
366	10380	19.2	1.5	122	3460	6.4	0.50	3.0	2479	57.1	54.1
426	10650	16.8	1.95	142	3550	5.6	0.65	3.0	2480	60.1	57.1
366	4440	7.2	0.93	122	1480	2.4	0.31	3.0	2481	63.1	60.1
372	4320	4.2	0.54	124	1440	1.4	0.18	3.0	2482	66.1	63.1
270	3450	3	0.45	90	1150	1.0	0.15	3.0	2483	69.1	66.1
294	5580	4.2	0.72	98	1860	1.4	0.24	3.0	2484	72.1	69.1
390	4830	4.8	0.66	130	1610	1.6	0.22	3.0	2485	75.1	72.1
408	9960	10.8	1.98	136	3320	3.6	0.66	3.0	2486	78.1	75.1
36	510	2.4	0.18	12	170	0.8	0.06	3.0	2487	81.1	73.1 78.1
336	9300	6	1.74	112	3100	2.0		3.0	2488	84.1	81.1
204	5430		1.08	68	1810				2489	87.1	84.1
792	5700		1.44	264	1900				2490	90.1	87.1
160	4928		1.216	50	1540			3.2	2491	93.3	90.1
210	15900	15	3.3	70	5300	5.0	1.10		2492		93.3
74	17670		2.852	240	5700		0.92		2493	99.4	96.3
225	4950		1.23	75	1650	2.6			2494	102.4	99.4
241	6138			80	1980		0.52		2495		102.4
180	6690		1.14	60	2230						105.5
279	4774		0.713	90	1540		0.23		2497		108.5
300	9150		1.47	100	3050				2498	114.6	111.6
							0.54	L	2499		114.6
											117.7
											120.7
				132						126.8	123.7
					1930					129.8	126.8
										132.9	129.8
											132.9
			<u> </u>								135.9
7	6300	7.8	1.32	26	2100	2.€	0.44	3.0	2907	142.0	139.0

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w°a)	Cu(w*a)	Mo(w°a)
142.0	145.1	2908	3.1	0.71	1.8	1960	38	2.201	5.58	6076	117.8
145.1	148.1	2909	3.0	0.41	2.7	2630	310	1.23	8.1	7890	930
148.1	151.2	2910	3.1	0.49	1.4	2120	24	1.519	4.34	6572	74.4
151.2	154.2	2911	3.0	0.77	1.9	2400	264	2.31	5.7	7200	792
154.2	157.3	2912	3.1	0.30	1.2	1550	22	0.93	3.72	4805	68.2
157.3	160.3	2913	3.0	0.20	1.4	1180	20	0.6	4.2	3540	60
160.3	163.4	2914	3.1	0.29	2.0	1600	26	0.899	6.2	4960	<b>80</b> .6
163.4	166.4	2915	3.0	0.36	1.9	2360	54	1.08	5.7	7080	162
166.4	169.5	2916	3.1	0.26	2.6	1750	16	0.806	8.06	5425	49.6
169.5	172.5	2917	3.0	0.26	3.8	1570	22	0.78	11.4	4710	66
172.5	175.6	2918	3.1	0.60	10.0	1640	16	1.86	31	5084	49.6
175.6	178.6	2919	3.0	0.21	1.5	680	20	0.63	4.5	2040	60
178.6	181.7	2920	3.1	0.10	1.4	686	16	0.31	4.34	2126.6	49.6
181.7	183.8	2921	2.1	0.11	1.4	520	8	0.231	2.94	1092	16.8
183.8	184.9	2922	1.1	0.36	3.2	740	22	0.396	3.52	814	24.2
184.9	187.8	2923	2.9	0.17	1.2	850	20	0.493	3.48	2465	58
187.8	190.2	2924	2.4	0.11	1.2	440	12	0.264	2.88	1056	28.8
190.2	192.7	2925	2.5	0.18	1.7	930	16	0.45	4.25	2325	40
192.7	195.7	2926	3.0	0.17	2.6	980	20	0.51	7.8	2940	60
195.7	199.1	2927	3.4	0.35	2.8	1420	36	1.19	9.52	4828	122.4
199.1	199.5	2928	0.4	1.10	43.0	4280	10	0.473	18.49	1840.4	4.3
199.5	203.0	2929	3.5	0.29	4.5	710	19	1.0063	15.615	2463.7	65.93
203.0	205.7	2930	2.7	0.02	1.3	380	4	0.054	3.51	1026	10.8
205.7	208.7	2931	3.0	0.10	1.4	722	16	0.3	4.2	2166	48
208.7	211.7	2932	3.0	0.33	1.8	1430	14	0.99	5.4	4290	
211.7	214.7	2933	3.0	0.25	1.7	1320	22	0.75			
214.7	216.5	2934	1.8	0.10	1.2	610	10	0.18			
216.5	218.3	2935	1.8	0.35	2.0	1800	52	0.63			
218.3	221.3	2936	3.0	0.10	1.0	490	10	0.3		1	
221.3	224.3	2937	3.0	0.16	1.4	820	14	0.48			42
224.3	227.3	2938	3.0	0.15	1.8	850	10	0.45		2550	
227.3	230.5	2939	3.2	0.12	1.4	590	14	0.384	4.48		
230.5	233.5	2940	3.0	0.14	1.6	880	16	0.42			
233.5	236.5	2941	3.0	0.13	1.4	780	12				
236.5	239.6	2942	3.1	0.66	5.4	2280	24	2.046			
239.6	242.6	2943	3.0	0.23	1.9	990	16				
242.6	245.7	2944	3.1	0.53	2.4	1750	14	1.643		5425	
245.7	248.7	2945	3.0	0.31	3.2	1170		0.93			
248.7	251.9	2946	3.2	0.44	3.4	1230	13				
251.9	254.9	2947	3.0	0.27	1.3	1100	14	0.81	3.9	3300	42

From	То	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w°a)	Ag (wa)	Cu(w*a)	Mo(w*a)
254.9	257.9	2948	3.0	0.15	0.9	830	14	0.45	2.7	2490	42
257.9	260.9	2949	3.0	0.32	1.3	1240	12	0.96	3.9	3720	36
260.9	263.9	2950	3.0	0.48	1.4	960	22	1.44	4.2	2880	<b>6</b> 6
263.9	267.0	2951	3.1	0.40	3.4	1360	12	1.24	10.54	4216	37.2
267.0	270.1	2952	3.1	0.29	2.4	810	26	0.899	7.44	2511	80.6
270.1	273.1	2953	3.0	0.18	1.2	510	10	0.54	3.6	1530	30
273.1	276.1	2954	3.0	0.12	0.5	520	21	0.36	1.5	1560	63
276.1	279.2	2955	3.1	0.21	4.8	1390	11	0.651	14.88	4309	34.1
279.2	282.2	2956	3.0	0.19	1.4	1000	9	0.57	4.2	3000	27
282.2	285.3	2957	3.1	0.38	3.0	2020	11	1.178	9.3	6262	34.1
285.3	288.3	2958	3.0	0.12	0.6	450	8	0.36	1.8	1350	24
288.3	291.4	2959	3.1	0.23	1.0	880	26	0.713	3.1	2728	80.6
291.4	294.4	2960	3.0	0.26	0.7	646	24	0.78	2.1	1938	72
294.4	297.5	2961	3.1	0.15	1.0	686	24	0.465	3.1	2126.6	74.4
297.5	299.9	2962	2.4	0.09	0.7	362	6	0.216	1.68	868.8	14.4
299.9	300.5	2963	0.6	0.64	54.0	10000	21	0.384	32.4	6000	12.6
300.5	303.6	2964	3.1	0.22	2.3	1140	76	0.682	7.13	3534	235.6
303.6	306.6	2965	3.0	0.11	0.8	410	18	0.33	2.4	1230	54
306.6	309.0	2966	2.4	0.10	1.2	400	6	0.24	2.88	960	14.4
309.0	311.7	2967	2.7	0.14	2.2	690	6	0.378	5.94	1863	16.2
311.7	315.4	2968	3.7	0.07	1.0	346	12	0.259	3.7	1280.2	44.4
315,4	318.0	2969	2.6	0.15	0.9	630	13	0.39	2.34	1638	33.8
318.0	321.0	2970	3.0	0.04	0.7	182	8	0.12	2.1	546	24
321.0	324.3	2971	3.3	0.09	8.0	410	48	0.297	2.64	1353	158.4
324.3	325.4	2972	1.1	0.01	0.3	30	8	0.011	0.33	33	8.8
325.4	327.3	2973	1.9	0.19	1.0	640	20	0.361	1.9	1216	38
327.3	330.3	2974	3.0	0.07	0.6	280	20	0.21	1.8	840	60 36
330.3	333.3	2975	3.0	0.08	0.6	210	12		1.8	630	
333.3	336.4	2976	3.1	0.12	1.0	400	14			1240	43.4
336.4	339.4	2977	3.0	0.20	0.7	486	14			1458	42
339.4	342.4	2978	3.0	0.31	2.8	910				2730	
342.4	345.4	2979	3.0	0.33	1.8	512				1536	
345.4	348.4	2980	3.0	0.13		330		1		990	
348.4	351.4	2981	3.0	0.17	0.8	476				1428	
351.4	354.5	2982	3.1	0.14	0.8						
354.5	357.5	2983	3.0	0.20			·				
357.5	360.5	2984	3.0	0.13							
360.5	363.5	2985	3.0	0.50							
363.5	366.5	2986	3.0	0.39							
366.5	369.5	2987	3.0	0.22	1.4	1130	6	0.66	4.2	3390	18

From	То	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
369.5	372.5	2988	3.0	0.16	1.4	396	5	0.48	4.2	1188	15
372.5	375.7	2989	3.2	0.33	4.2	1350	8	1.056	13.44	4320	25.6
375.7	378.7	2990	3.0	0.19	1.2	1180	5	0.57	3.6	3540	15
378.7	381.7	2991	3.0	0.11	0.3	830	28	0.33	0.9	2490	84
381.7	383.7	2992	2.0	0.15	0.4	710	8	0.3	0.8	1420	16
383.7	386.7	2993	3.0	0.16	0.4	530	10	0.48	1.2	1590	30
386.7	390.0	2994	3.3	0.30	2.7	2900	4	0.99	8.91	9570	13.2
390.0	393.5	2995	3.5	0.33	0.3	920	14	1.155	1.05	3220	49
393.5	396.5	2996	3.0	0.17	2.8	530	8	0.51	8.4	1590	24
396.5	399.5	2997	3.0	0.10	0.6	400	12	0.3	1.8	1200	36
399.5	402.5	2998	3.0	0.14	0.8	610	14	0.42	2.4	1830	42
402.5	405.4	2999	2.9	0.22	1.4	886	30	0.638	4.06	2569.4	87
405.4	408.4	3000	3.0	0.42	6.0	966	16	1.26	18	2898	48
408.4	410.7	3001	2.3	0.16	1.8	280	10	0.368	4.14	644	23
410.7	413.7	3002	3.0	1.90	22.4	1910	12	5.7	67.2	5730	36
413.7	416.7	3003	3.0		5.4	530	24	1.05	16.2	1590	72 48
416.7	419.7	3004	3.0	0.08	1.4	310	16	0.24	4.2	930	48
419.7	422.7	3005	3.0	0.10		410		0.3	2.7	1230	42
422.7	425.7	3006	3.0	0.18	1.0	610	13	0.54	3	1830	39
425.7	428.7	3007	3.0	0.21	2.8		76	0.63	8.4	4200	228
428.7	431.7	3008	3.0		1.2		16	0.54	3.6		48
431.7	434.7	3009	3.0	0.17	0.8				2.4	1788	30
434.7	437.7	3010	3.0	0.19	0.7				2.1	1428	27
437.7	440.7	3011	3.0	0.32	1.0	750				2250	108
440.7	443.7	3012	3.0	0.31	1.7	980				2940	126
443.7	448.8	3013	5.1	0.20		750	<del></del>			3825	295.8
448.8		3014	1.1	0.23							74.8
449.9	452.9	3015	3.0	0.19	0.6	610	50	0.57	1.8	1830	150

## CT1219.XLS

From	То	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w^a)	Ag (w*a)	Cu(w*a)	Mo(w°a)
24.1m - 51	1m										
Total (w*a)			27.0	3.93	63.9	26508	2358				
Mean				0.15	2.4	982	87				
51.1 m - 1	75.6 m										
Total (w*a)			124.5	54.36	352.2	285483	11190				
Mean				0.44	2.8	2293	90				
175.6 m -											
Total (wa			128.0	30.70	295.2	130351	2324				
Mean				0.24	2.3	1018	18				
303.6 m -	360.5 m										
Total (w*a	)		56.9	8.05	57.4	24934	985				
Mean				0.14	1.0	438	17				
360.5 m -	428.7 m										
Total (w*a			68.2	20.65	187.8	64949	1141				
Mear				0.30	2.8	952	17				
428.7 m -	452.9 m										
Total (w*a	)		24.2	5.35	23.8	17117	860				
Mear				0.22	1.0	707	36				
24.1 m - 3	03.6 m										
Total (w*a	)		279.5	88.99	711.3	442342	15873				
Mear				0.32	2.5	1583	57		-		
24.1 m - 4	52.9 m										
Total (w*a	)		428.8	123.04	980.3		18858				
Mear				0.29	2.3	1281	44				

<b>DDH 1220</b>	ASSAY TA	BLE					I		1	· · · · · · · · · · · · · · · · · · ·	
From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w^a)	Cu(w*a)	Mo(w°a)
25.6	28.6	2747	3.0	0.40	1.4	2670	65	1.2	4.2	8010	195
28.6	31.8	2748	3.2	0.56	1.3	990	140	1.792	4.16	3168	448
31.8	34.8	2749	3.0	1.00	2.8	1900	158	3	8.4	5700	474
34.8	37.8	2750	3.0	0.90	2.2	3650	268	2.7	6.6	10950	804
37.8	41.1	2751	3.3	1.00	2.0	3000	92	3.3	6.6	9900	303.6
41.1	44.1	2752	3.0	0.47	1.8	2430	106	1.41	5.4	7290	318
44.1	47.1	2753	3.0	0.60	5.8	2500	120	1.8	17.4	7500	360
47.1	50.1	2754	3.0	0.64	1.6	2760	62	1.92	4.8	8280	186
50.1	53.1	2755	3.0	0.34	0.4	1910	89	1.02	1.2	5730	267
53.1	55.8	2756	2.7	0.36	0.4	1610	84	0.972	1.08	4347	226.8
55.8	58.8	2757	3.0	0.12	0.2	1080	79	0.36	0.6	3240	237
58.8	61.8	2758	3.0	0.43	2.0	2220	72	1.29	6	6660	216
61.8	64.8	2759	3.0	0.76	5.0	5400	72	2.28	15	16200	216
64.8		2760	3.0	0.61	1.4	3260	70	1.83	4.2	9780	210
67.8		2761	2.9	0.66	1.2	2780	70	1.914	3.48	8062	203
70.7		2762	3.0	0.68	1.5	3350	48	2.04	4.5	10050	144
73.7		2763	2.9	0.69	1.1	2560	71	2.001	3.19	7424	205.9
76.6	79.6	2764	3.0	0.26		2310	73	0.78	9.3	6930	219
79.6		2765	0.9	0.73	21.6	5900	36	0.657	19.44	5310	32.4
80.5		2766	2.0	0.54	3.2	3760	80	1.08	6.4	7520	160
82.5		2767	3.0	0.48	1.6	3600	43	1.44	4.8	10800	129
85.5		2768	3.0	0.73	2.6	4580	277	2.19		13740	831
88.5	90.6	2769	2.1	1.20	2.4	4720	313	2.52	5.04	9912	657.3
90.6		2770	3.0	0.45	1.6	3100	219	1.35	4.8	9300	657
93.6		2771	3.0	0.40	1.1	2460	112	1.2	3.3	7380	336
96.6		2772	3.0	0.37	1.4	2280	83	1.11	4.2	6840	249
99.6		2773	3.0	0.25		1900	292	0.75	7.2	5700	876
102.6		2774	3.0	0.31	1.2	1760	70	0.93	3.6	5280	210
105.6		2775	2.1	0.53		2020	76	1.113	3.78	4242	159.6
107.7		2776	3.0	0.39		2650	177	1.17	7.2	7950	531
110.7		2777	3.0	0.43		2100		1.29	5.1	6300	426
113.7	1	2778	3.0	0.39		2350	143				
116.7							205				615
119.7		2780	2.8								
122.5			3.2								
125.7		2782									
128.7		2783									
131.7		2784	3.4	0.18						<del></del>	
135.1	137.3	2785	2.2	0.16	0.7	590	47	0.352	1.54	1298	103.4

137.3         140.7         2786         3.4           140.7         143.7         2787         3.0           143.7         146.7         2788         3.0           146.7         149.7         2789         3.0           149.7         152.7         2790         3.0           152.7         155.7         2791         3.0           155.7         158.7         2792         3.0           158.7         161.5         2793         2.8           161.5         163.3         2794         1.8           163.3         166.1         2795         2.8           166.1         169.1         2796         3.0           169.1         172.1         2797         3.0           175.1         178.1         2799         3.0           178.1         181.1         2800         3.0           181.1         184.2         2801         3.1           184.2         187.2         2802         3.0           187.2         190.2         2803         3.0	Au ppm 0.22 0.21 0.18 0.23 0.26 0.15 0.22 0.17 0.16 0.23 0.43 0.34 0.28	Ag ppm 0.9 1.1 0.7 1.3 0.7 0.3 0.6 0.9 0.9	594 730 580 1140 1000 580 862 610 1030	40 38 28 71 49 24 20	0.748 0.63 0.54 0.69 0.78 0.45	3.06 3.3 2.1 3.9 2.1 0.9	2019.6 2190 1740 3420 3000 1740	136 114 84 213 147
140.7       143.7       2787       3.0         143.7       146.7       2788       3.0         146.7       149.7       2789       3.0         149.7       152.7       2790       3.0         152.7       155.7       2791       3.0         155.7       158.7       2792       3.0         158.7       161.5       2793       2.8         161.5       163.3       2794       1.8         163.3       166.1       2795       2.8         166.1       169.1       2796       3.0         169.1       172.1       2797       3.0         172.1       175.1       2798       3.0         175.1       178.1       2799       3.0         178.1       181.1       2800       3.0         181.1       184.2       2801       3.1         184.2       187.2       2802       3.0         187.2       190.2       2803       3.0	0.18 0.23 0.26 0.15 0.22 0.17 0.16 0.23 0.43 0.34	0.7 1.3 0.7 0.3 0.6 0.9 0.9	580 1140 1000 580 862 610	28 71 49 24 20	0.54 0.69 0.78 0.45	2.1 3.9 2.1 0.9	1740 3420 3000	84 213 147
143.7       146.7       2788       3.0         146.7       149.7       2789       3.0         149.7       152.7       2790       3.0         152.7       155.7       2791       3.0         155.7       158.7       2792       3.0         158.7       161.5       2793       2.8         161.5       163.3       2794       1.8         163.3       166.1       2795       2.8         166.1       169.1       2796       3.0         169.1       172.1       2797       3.0         172.1       175.1       2798       3.0         175.1       178.1       2799       3.0         178.1       181.1       2800       3.0         181.1       184.2       2801       3.1         184.2       187.2       2802       3.0         187.2       190.2       2803       3.0	0.23 0.26 0.15 0.22 0.17 0.16 0.23 0.43 0.34	1.3 0.7 0.3 0.6 0.9 0.9	1140 1000 580 862 610	71 49 24 20	0.69 0.78 0.45	3.9 2.1 0.9	3420 3000	213 147
146.7         149.7         2789         3.0           149.7         152.7         2790         3.0           152.7         155.7         2791         3.0           155.7         158.7         2792         3.0           158.7         161.5         2793         2.8           161.5         163.3         2794         1.8           163.3         166.1         2795         2.8           166.1         169.1         2796         3.0           169.1         172.1         2797         3.0           172.1         175.1         2798         3.0           175.1         178.1         2799         3.0           178.1         181.1         2800         3.0           181.1         184.2         2801         3.1           184.2         187.2         2802         3.0           187.2         190.2         2803         3.0	0.23 0.26 0.15 0.22 0.17 0.16 0.23 0.43 0.34	0.7 0.3 0.6 0.9 0.9	1000 580 862 610	49 24 20	0.78 0.45	2.1 0.9	3000	147
149.7         152.7         2790         3.0           152.7         155.7         2791         3.0           155.7         158.7         2792         3.0           158.7         161.5         2793         2.8           161.5         163.3         2794         1.8           163.3         166.1         2795         2.8           166.1         169.1         2796         3.0           169.1         172.1         2797         3.0           172.1         175.1         2798         3.0           175.1         178.1         2799         3.0           178.1         181.1         2800         3.0           181.1         184.2         2801         3.1           184.2         187.2         2802         3.0           187.2         190.2         2803         3.0	0.26 0.15 0.22 0.17 0.16 0.23 0.43 0.34	0.7 0.3 0.6 0.9 0.9	580 862 610	24 20	0.45	0.9		
152.7         155.7         2791         3.0           155.7         158.7         2792         3.0           158.7         161.5         2793         2.8           161.5         163.3         2794         1.8           163.3         166.1         2795         2.8           166.1         169.1         2796         3.0           169.1         172.1         2797         3.0           172.1         175.1         2798         3.0           175.1         178.1         2799         3.0           178.1         181.1         2800         3.0           181.1         184.2         2801         3.1           184.2         187.2         2802         3.0           187.2         190.2         2803         3.0	0.15 0.22 0.17 0.16 0.23 0.43 0.34	0.3 0.6 0.9 0.9 0.6	862 610	20			1740	36
155.7         158.7         2792         3.0           158.7         161.5         2793         2.8           161.5         163.3         2794         1.8           163.3         166.1         2795         2.8           166.1         169.1         2796         3.0           169.1         172.1         2797         3.0           172.1         175.1         2798         3.0           175.1         178.1         2799         3.0           178.1         181.1         2800         3.0           181.1         184.2         2801         3.1           184.2         187.2         2802         3.0           187.2         190.2         2803         3.0	0.22 0.17 0.16 0.23 0.43 0.34	0.9 0.9 0.6	610		0.66	<del>+</del>	1,70	72
158.7         161.5         2793         2.8           161.5         163.3         2794         1.8           163.3         166.1         2795         2.8           166.1         169.1         2796         3.0           169.1         172.1         2797         3.0           172.1         175.1         2798         3.0           175.1         178.1         2799         3.0           178.1         181.1         2800         3.0           181.1         184.2         2801         3.1           184.2         187.2         2802         3.0           187.2         190.2         2803         3.0	0.17 0.16 0.23 0.43 0.34	0.9 0.6			0.00	1.8	2586	60
161.5     163.3     2794     1.8       163.3     166.1     2795     2.8       166.1     169.1     2796     3.0       169.1     172.1     2797     3.0       172.1     175.1     2798     3.0       175.1     178.1     2799     3.0       178.1     181.1     2800     3.0       181.1     184.2     2801     3.1       184.2     187.2     2802     3.0       187.2     190.2     2803     3.0	0.16 0.23 0.43 0.34	0.6	1030	23	0.476	2.52	1708	64.4
163.3     166.1     2795     2.8       166.1     169.1     2796     3.0       169.1     172.1     2797     3.0       172.1     175.1     2798     3.0       175.1     178.1     2799     3.0       178.1     181.1     2800     3.0       181.1     184.2     2801     3.1       184.2     187.2     2802     3.0       187.2     190.2     2803     3.0	0.43 0.34			45	0.288	1.62	1854	81
166.1     169.1     2796     3.0       169.1     172.1     2797     3.0       172.1     175.1     2798     3.0       175.1     178.1     2799     3.0       178.1     181.1     2800     3.0       181.1     184.2     2801     3.1       184.2     187.2     2802     3.0       187.2     190.2     2803     3.0	0.43 0.34		920	25	0.644	1.68	2576	70
169.1     172.1     2797     3.0       172.1     175.1     2798     3.0       175.1     178.1     2799     3.0       178.1     181.1     2800     3.0       181.1     184.2     2801     3.1       184.2     187.2     2802     3.0       187.2     190.2     2803     3.0		1.1	1620	72	1.29	3.3	4860	216
172.1     175.1     2798     3.0       175.1     178.1     2799     3.0       178.1     181.1     2800     3.0       181.1     184.2     2801     3.1       184.2     187.2     2802     3.0       187.2     190.2     2803     3.0	0.28	0.5	580	20	1.02	1.5	1740	60
175.1     178.1     2799     3.0       178.1     181.1     2800     3.0       181.1     184.2     2801     3.1       184.2     187.2     2802     3.0       187.2     190.2     2803     3.0	0.20	0.8	890	38	0.84	2.4	2670	114
178.1     181.1     2800     3.0       181.1     184.2     2801     3.1       184.2     187.2     2802     3.0       187.2     190.2     2803     3.0	0.38	1.0	1160	24	1.14	3	3480	72
181.1     184.2     2801     3.1       184.2     187.2     2802     3.0       187.2     190.2     2803     3.0	0.41	0.9	900	18	1.23	2.7	2700	54
184.2     187.2     2802     3.0       187.2     190.2     2803     3.0	0.36	0.6	1090	30	1.116	1.86	3379	93
187.2 190.2 2803 3.0	0.44	1.0	1480	57	1.32	3	4440	171
	0.98	1.8	926	32	2.94	5.4	2778	96
190.2 193.0 2804 2.8	0.45	7.0	1950	26	1.26	19.6	5460	72.8
193.0 196.0 2805 3.0	0.34	3.7	1090	433	1.02	11.1	3270	1299
196.0 199.0 2806 3.0	0.30	1.2	730	80	0.9	3.6	2190	240
199.0 202.7 2807 3.7	0.26	0.7	730	51	0.962	2.59	2701	188.7
202.7 204.9 2808 2.2	0.42	1.5	1270	72	0.924	3.3	2794	158.4
204.9 207.0 2809 2.1	0.22	0.4	400	13	0.462		840	27.3
207.0 209.2 2810 2.2	0.30	1.0	820	41	0.66		1804	90.2
209.2 211.0 2811 1.8	0.61	1.6	1510	52	1.098		2718	93.6
211.0 214.0 2812 3.0	0.34	0.6	916	78	1.02			234
214.0 217.0 2813 3.0	0.44	1.5	1260	88	1.32			264
217.0 220.0 2814 3.0	0.18	0.8	624 764	16 7	0.54 0.72		1872 2292	48 21
220.0 223.0 2815 3.0	0.24	0.5 1.5	880	27	1.16			108
223.0 227.0 2816 4.0	0.29	2.9	1180	21	1.178			65.1
227.0 230.1 2817 3.1 230.1 233.0 2818 2.9	0.36	1.0	718	16		4		46.4
	0.24	0.3	820	22	<u> </u>		4	61.6
	0.20	0.9		24	<del></del>	<del></del>		
	0.17	0.5	20	1				
	0.44	1.1	710	5			<del></del>	
	U.77				: 1.32	1 3.3	1 2130	1 13
	0.14	11 8	770				<del></del>	<del> </del>
244.7         247.8         2824         3.1           247.8         250.8         2825         3.0	0.14 0.13	0.8 0.2		19	0.336	1.92	1848	45.6

u(wa) Mo(wa		Ag (w*a)	Au (w*a)	Mo ppm	Cu ppm	Ag ppm	Au ppm	Width m	Number	To	From
3225.6 73.6		2.88	1.152	23	1008	0.9	0.36	3.2	2826	254.0	250.8
7530 423	3.6	3.6	- 1.38	141	2510	1.2	0.46	3.0	2827	257.0	254.0
4557 142.6	.41	3.41	0.899	46	1470	1.1	0.29	3.1	2828	260.1	257.0
1740 168	1.8	1.8	0.42	56	580	0.6	0.14	3.0	2829	263.1	260.1
3420 4	3	3	1.41	15	1140	1.0	0.47	3.0	2830	266.1	263.1
1470 279	0.3	0.3	1.29	93	490	0.1	0.43	3.0	2831	269.1	266.1
1134 4	2.4	2.4	0.45	15	378	0.8	0.15	3.0	2832	272.1	269.1
132 60	0.3	0.3	0.3	20	44	0.1	0.10	3.0	2833	275.1	272.1
390 12	0.3	0.3	0.24	41	130	0.1	0.08	3.0	2834	278.1	275.1
2790 20-	3	3	0.63	68	930	1.0	0.21	3.0	2835	281.1	278.1
2910 7	9		0.93	25	970	3.0	0.31	3.0	2836	284.1	281.1
2580 2	1.5		0.78	9	860	0.5	0.26	3.0	2837	287.1	284.1
3630 6	2.7		0.93	23	1210	0.9	0.31	3.0	2838	290.1	287.1
2430 1	3.3	3.3	0.75	5	810	1.1	0.25	3.0	2839	293.1	290.1
3300 3	4.2	4.2	0.72	12	1100	1.4	0.24	3.0	2840	296.1	293.1
2760 3	6	•	0.78	13	920	2.0	0.26	3.0	2841	299.1	296.1
3600 9	3		0.72	30	1200	1.0	0.24	3.0	2842	302.1	299.1
1710 2	.35	1.3	0.42	16	1140	0.9	0.28	1.5	2843	303.6	302.1
1568 5	.68	1.68	0.336	20	560	0.6	0.12	2.8	2844	306.4	303.6
119 2.	0.28	0.28	0.056	4	170	0.4	0.08	0.7	2845	307.1	306.4
762 3	1.8	1.8	0.18	10	254	0.6	0.06	3.0	2846	310.1	307.1
930 1	0.6			5	310	0.2	0.06	3.0	2847	313.1	310.1
870 1	3		0.15	6	290	1.0	0.05	3.0	2848	316.1	313.1
1170 11	3.6	3.0	0.18	38	390	1.2	0.06	3.0	2849	319.1	316.1
1086 5	3			. 18	362	1.0	0.07	3.0	2850	322.1	319.1
1152 1	2.4			6	384	0.8	0.05	3.0	2851	325.1	322.1
882 3		1.4		10	245	0.4	0.04	3.6	2852	328.7	325.1
439.2 33.		0.4	0.072	14	183	0.2	0.03	2.4	2853	331.1	328.7
391.4 15.	0.38			8	206	0.2	0.04	1.9	2854	333.0	331.1
675 2	0.6			8	225	0.2	0.06	3.0	2855	336.0	333.0
816	0.6			3	272	0.2	0.07	3.0	2856	339.0	336.0
414 1	0.6			4	138	0.2	0.04	3.0	2857	342.0	339.0
1194	0.6			2	398	0.2	0.06	3.0	2858	345.0	342.0
1023 4	1.5			16	341	0.5	80.0	3.0	2859	348.0	345.0
1080 4	0.4			10	270	0.1	0.03	4.0	2860	352.0	348.0
224 1	0.3			8	112	1.2	0.03	2.0	2861	354.0	352.0
348 498 2	0.3			3	116 166	0.1		3.0	2862	357.0	354.0
498 2 462 1	0.6		<del></del>	4	154	0.1	0.02	3.0	2863	360.0	357.0
714 3	0.6			12	238	0.2 0.2	0.02 0.01	3.0 3.0	2864 2865	363.0 366.0	360.0 363.0

<b>5</b>	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w°a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
From		2866	3.1	0.02	0.2	180	4	0.062	0.62	558	12.4
366.0	369.1	2000	3.1	0.02	0.2						
5.6 m - 119	9.7 m					055405.0	11531.6				
Total (w*a)			94.1	51.71	198.7	255425.0					
Mean				0.55	2.1	2714	123				
119.7 m - 30	06.4 m						7920.6				
Total (w*a)			186.7	52.47	198.9	167338.9	7829.5		<del>                                     </del>		
Mean				0.28	1.1	896	42				
306.4 m - 3	69.1 m					45007.6	588.0				<del></del>
Total (w*a)			62.7	2.81	26.1	15807.6			ļi		
Mean				0.04	0.4	252	9		<u></u>		
25.6 m - 30	6.4 m										
Total (w*a)			280.8	104.18	397.5		19361.1				
Mean				0.37	1.4	1506	69				
25.6 m - 36	9.1 m					100504.5	40040.4				
Total (w*a)			343.5	106.99	423.6				<del> </del>		<u> </u>
Mean				0.31	1.2	1277	58	L		L	

## CT1221.XLS

1 1221	ASSAY TAI	BLE							<u> </u>		
From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
13.0	16.0	2647	3.0	0.13	0.2	400	12	0.39	0.6	1200	36
16.0	19.0	2648	3.0	0.09	0.8	800	8	0.27	2.4	2400	24
19.0	22.0	2649	3.0	0.22	0.8	1000	2	0.66	2.4	3000	
22.0	24.0	2650	2.0	0.17	0.6	500	3	0.34	1.2	1000	
24.0	26.9	2651	2.9	0.12	0.4	400	2	0.348	1.16	1160	5.
26.9	30.6	2652	3.7	0.08	0.4	400	4	0.296	1.48	1480	14.
30.6	34.3	2653	3.7	0.12	0.5	500	6	0.444	1.85	1850	22.
34.3	37.4	2654	3.1	0.11	0.4	400	8	0.341	1.24	1240	24.
37.4	41.5	2655	4.1	0.10	0.6	400	5	0.41	2.46	1640	20.
41.5		2656	2.1	0.09	0.6	300	3	0.189	1.26	630	6.
43.6	46.6	2657	3.0	0.51	1.4	1600	4	1.53	4.2	4800	1
46.6		2658	3.0	0.31	1.2	1100	12	0.93	3.6	3300	3
49.6		2659	3.0	0.34	1.5	1700	4	1.02	4.5	5100	1
52.6		2660	3.0	0.30	1.6	1000	2	0.9	4.8	3000	
55.6	58.6	2661	3.0	0.31	1.6	1100	9	0.93	4.8	3300	
58.6	61.6	2662	3.0	0.26	1.8	1500	4	0.78	5.4	4500	
61.6	64.6	2663	3.0	0.13	0.8	600	4	0.39	2.4	1800	
64.6		2664	3.0	0.32	0.7	800	4	0.96	2.1	2400	
67.6		2665	3.0	0.35	1.2	1400	2	1.05	3.6	4200	
70.6		2666	3.0	0.41	1.8	1400	2	1.23	5.4	4200	
73.6		2667	3.0	0.28	0.9	800	4	0.84	2.7	2400	
76.6	1	2668	3.0	0.27	1.2	1400	6	0.81	3.6	4200	
79.6		2669	3.0	0.48	1.6	1700	6	1.44	4.8	5100	
82.6		2670	3.0	1.27	4.0	5100	8	3.81	12	15300	
85.6		2671	3.0	0.76	3.4	4600	4	2.28	10.2	13800	
88.6	91.6	2672	3.0	0.32	1.5	1500	6	0.96	4.5	4500	
91.6		2673	2.9	0.18	0.6	500	4	0.522	1.74	1450	11
94.5	97.6	2674	3.1	0.33	1.2	600	4	1.023	3.72	1860	12
97.6	100.6	2675	3.0	1.13	1.4	500	5	3.39	4.2	1500	
100.6	103.6	2676	3.0	0.40	0.8	300	3	1.2	2.4	900	
103.6		2677	3.0	0.79	1.2	800	7	2.37	3.6	2400	
106.6		2678	3.0	0.29	1.0	700	4	0.87	3	2100	
109.6		2679	2.9	0.22	0.8	400	4	0.638	2.32	1160	11
112.5	1	2680	3.0	0.26	1.0	500	5	0.78	3	1500	
115.5		2681	3.0	0.14	0.6	500	2	0.42	1.8	1500	
118.5		2682	3.0	0.39	1.0	500	13	1.17	3	1500	
121.5		2683		0.13	0.4	300	6			900	
124.		2684		0.11	0.4	200	L		1		3
127.6		2685		0.10							

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## CT1221.XLS

From	То	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
130.6	133.6	2686	3.0	0.23	0.4	200	12	0.69	1.2	600	36
133.6	136.6	2687	3.0	0.14	0.4	160	9	0.42	1.2	480	27
136.6	139.7	2688	3.1	0.48	0.4	190	4	1.488	1.24	589	12.4
139.7	144.1	2689	4.4	0.32	0.5	236	12	1.408	2.2	1038.4	52.8
144.1	148.3	2690	4.2	0.01	0.4	62	4	0.042	1.68	260.4	16.8
148.3	152.6	2691	4.3	0.02	0.3	30	2	0.086	1.29	129	8.6
152.6	155.6	2692	3.0	0.07	0.4	138	4	0.21	1.2	414	12
155.6	158.6	2693	3.0	0.22	0.5	384	12	0.66	1.5	1152	36
158.6	161.7	2694	3.1	0.35	0.5	284	4	1.085	1.55	880.4	12.4
161.7	164.7	2695	3.0	0.56	1.2	348	16	1.68	3.6	1044	48
164.7	167.7	2696	3.0	0.92	1.0	356	4	2.76	3	1068	12
167.7	170.7	2697	3.0	0.20	0.3	137	14	0.6	0.9	411	42
170.7	173.7	2698	3.0	0.33	1.0	234	16	0.99	3	702	48
173.7	176.7	2699	3.0	0.26	1.1	286	13	0.78	3.3	858	39
176.7	180.0	2700	3.3	0.17	0.8	136	5	0.561	2.64	448.8	16.5
180.0	183.1	2701	3.1	0.23	0.6	139	14	0.713	1.86	430.9	43.4
183.1	185.2	2702	2.1	0.40	0.7	480	29	0.84	1.47	1008	60.9
185.2	188.2	2703	3.0	0.15	0.5	350	8	0.45	1.5	1050	24
188.2	191.2	2704	3.0	0.18	0.8	680	9		2.4	2040	27
191.2	194.1	2705	2.9	0.41	1.6	1170	18	1.189	4.64	3393	52.2
194.1	197.5	2706	3.4	0.30	1.3	520	14	1.02	4.42		47.6
197.5	200.5	2707	3.0	0.18	1.0	634	6		3		18
200.5	203.5	<sup>-</sup> 2708	3.0	0.45	1.2	680	7				
203.5	206.3	2709	2.8	0.10	0.2	136	6		0.56		16.8
206.3	209.3	2710	3.0	0.05	0.4	133	5				
209.3	212.3	2711	3.0	0.30	1.4	980	22	L			66
212.3	215.3	2712	3.0	0.07	0.2	96	6	1	0.6		18
215.3	218.3	2713	3.0	0.43	0.8	318	30				
218.3	219.9	2714	1.6	0.10	0.4	210					
219.9	221.9	2715	2.0	0.28	0.8	174	26				
221.9	224.9	2716		0.18	0.8	142					
224.9	227.9	2717	3.0	0.06	0.3	92					
227.9	230.9	2718		0.05	0.3						
230.9	233.9	2719	3.0	0.06 0.07	0.2		8				
233.9	236.9										
236.9	239.9										
239.9	242.9										
242.9	245.9										
245.9		2724					<del></del>				
248.1	250.9	2725	2.8	0.09	0.4	340	7	0.252	1.12	952	19.6

#### CT1221.XLS

From	То	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
250.9	253.9	2726	3.0	0.11	0.2	264	6	0.33	0.6	792	18
253.9	256.9	2727	3.0	0.13	0.2	375	8	0.39	0.6	1125	24
256.9	260.3	2728	3.4	0.15	15.0	231	40	0.51	51	785.4	136
260.3	263.3	2729	3.0	0.18	0.8	116	16	0.54	2.4	348	48
263.3	266.0	2730	2.7	0.44	0.8	60	6	1.188	2.16	162	16.2
266.0	267.5	2731	1.5	3.00	26.0	1520	8	4.5	39	2280	12
267.5	270.5	2732	3.0	0.95	3.2	280	6	2.85	9.6	840	18
270.5	273.8	2733	3.3	0.26	1.0	380	8	0.858	3.3	1254	26.4
273.8	276.8	2734	3.0	0.09	0.2	115	22	0.27	0.6	345	66
276.8	279.7	2735	2.9	0.04	0.3	62	6	0.116	0.87	179.8	17.4
279.7	282.7	2736	3.0	0.10	0.2	118	12	0.3	0.6	354	36
282.7	285.7	2737	3.0	0.13	0.3	113	6	0.39	0.9	339	18
285.7	288.4	2738	2.7	0.07	0.2	136	8	0.189	0.54	367.2	21.6
288.4	291.4	2739	3.0	0.07	0.4	126	5	0.21	1.2	378	15
291.4	294.5	2740	3.1	0.09	0.2	192	10	0.279	0.62	595.2	31
294.5	297.0	2741	2.5	0.41	0.4	376	5	1.025	1	940	12.5
297.0	298.7	2742	1.7	0.75	8.0	1770	8	1.275	13.6	3009	13.6
298.7	301.8	2743	3.1	0.60	1.8	380	9	1.86	5.58	1178	27.9
301.8	305.0	2744	3.2	0.16	0.3	288	6	0.512	0.96	921.6	19.2
305.0	308.1	2745	3.1	0.15	0.8	340	6	0.465	2.48	1054	18.6
308.1	312.1	2746	4.0	0.06	0.2	76	6	0.24	0.8	304	24
13.0 m - 43	3.6 m										
Total (w*a)	)		30.6	3.69	16.1	15600	166				
Mean				0.12	0.5	510	5				
43.6 m - 91	1.6 m										
Total (w*a)	)		48.0	19.86	78.6	81900	243				
Mean				0.41	1.6	1706	5				
91.6 m - 31	12.1 m										
Total (w*a)			220.5	58.00	246.0	70044	2149				
Mean				0.26	1.1	318	10				
13.0 m - 31	12.1 m										
Total (w*a)			299.1	81.55	340.7	167544	2559				
Mean				0.27	1.1	560	9				

### CT1222.XLS

DH 1222 AS											
From	То	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
4.5	5.5	2395	1.0	1.26	8.8	3710	140	1.26	8.8	3710	140
5.5	7.7	2396	2.2	0.02	0.1	290	4	0.044	0.22	638	8.8
7.7	11.0	2397	3.3	0.55	1.9	1480	7	1.815	6.27	4884	23.1
11.0	14.0	2398	3.0	0.48	1.6	1520	4	1.44	4.8	4560	12
14.0	17.0	2399	3.0	0.61	1.2	1000	6	1.83	3.6	3000	18
17.0	20.0	2400	3.0	0.53	1.5	1530	9	1.59	4.5	4590	27
20.0	23.0	2401	3.0	0.56	1.5	1410	11	1.68	4.5	4230	33
23.0	26.0	2402	3.0	0.65	1.6	1310	16	1.95	4.8	3930	48
26.0	29.0	2403	3.0	0.46	1.8	1440	12	1.38	5.4	4320	36
29.0	32.0	2404	3.0	0.50	1.3	1720	12	1.5	3.9	5160	36
32.0	35.0	2405	3.0	0.49	1.6	2740	9	1.47	4.8	8220	27
35.0	38.0	2406	3.0	0.44	1.1	1640	8	1.32	3.3	4920	24
38.0	41.0	2407	3.0	0.64	2.3	1950	200	1.92	6.9	5850	600
41.0	44.0	2408	3.0	0.56	1.6	1050	8	1.68	4.8	3150	24
44.0	47.0	2409	3.0	0.60	2.4	1110	12	1.8	7.2	3330	36
47.0	50.0	2410	3.0	0.51	1.5	1180	8	1.53	4.5	3540	24
50.0	53.0	2411	3.0	0.38	1.6	1500	30	1.14	4.8	4500	9
53.0	56.0	2412	3.0	0.48	1.7	1540	20	1.44	5.1	4620	6
56.0	59.0	2413	3.0	0.66	2.0	1780	40	1.98	6	5340	120
59.0	62.0	2414	3.0	0.72	1.8	1510	16	2.16	5.4	4530	4
62.0	65.0	2415	3.0	0.40	1.5	1500	8	1.2	4.5	4500	2
65.0	68.0	2416	3.0	1.36	2.7				8.1		2
68.0	71.0	2417	3.0	1.70	5.9				17.7		8
71.0	74.0	2418	3.0	0.64	1.0				3		6
74.0	77.0	2419	3.0	0.89	2.0			2.67	6		12
77.0	80.0	2420	3.0	0.27	0.9	1020	8	0.81	2.7	3060	2 7 1
80.0	83.0	2421	3.0	0.99	2.6	4000	24	2.97	7.8	12000	7
83.0	86.0	2422	3.0	0.54	1.3	1430	6	1.62	3.9	4290	1
86.0	89.0	2423	3.0	1.02	1.6	3030	22	3.06	4.8	9090	6
89.0	92.0	2424	3.0	0.36	0.9	1960	10	1.08	2.7	5880	6
92.0	95.0	2425	3.0	0.60	1.0	2670					
95.0	98.0	2426	3.0	10.00	1.5						17
98.0	101.0			0.40							
101.0	104.0	2428	3.0								
104.0	107.0		3.0								
107.0	108.0	2430	<del></del>			<del></del>					
108.0	111.0									·	
111.0	113.1	2432		0.63			<u> </u>				
113.1	115.0	2433	1.9	0.42	100.0	1720	240	0.798	190	3268	45

## CT1222.XLS

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From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
115.0	118.0	2434	3.0	0.37	0.8	1240	12	1,11	2.4	3720	36
118.0	121.0	2435	3.0	0.29	1.4	1020	10	0.87	4.2	3060	30
121.0	124.0	2436	3.0	0.21	0.5	980	14	0.63	1.5	2940	42
124.0	127.0	2437	3.0	0.38	0.6	1240	10	1.14	1.8	3720	30
127.0	130.0	2438	3.0	0.15	0.2	810	36	0.45	0.6	2430	108
130.0	133.0	2439	3.0	0.23	0.4	1280	6	0.69	1.2	3840	18
133.0	136.0	2440	3.0	0.16	0.2	870	30	0.48	0.6	2610	90
136.0	139.0	2441	3.0	0.36	0.6	960	15	1.08	1.8	2880	45
139.0	142.0	2442	3.0	0.30	0.7	1060	15	0.9	2.1	3180	45
142.0	145.0	2443	3.0	0.39	0.6	1300	12	1.17	1.8	3900	36
145.0	148.0	2444	3.0	0.40	0.7	1450	15	1.2	2.1	4350	45
148.0	151.0	2445	3.0	0.34	0.7	1240	8	1.02	2.1	3720	24
151.0	154.0	2446	3.0	0.34	1.4	1475	20	1.02	4.2	4425	60
154.0	157.0	2447	3.0	0.19	0.7	854	15	0.57	2.1	2562	45
157.0	160.0	2448	3.0	0.34	1.6	1100	9	1.02	4.8	3300	27
160.0	163.0	2449	3.0	0.47	2.6	1950	20	1.41	7.8	5850	60
163.0	166.0	2450	3.0	0.69	2.8	1980	17	2.07	8.4	5940	51
166.0	169.0	2457	3.0	0.34	2.0	1429	10	1.02	6	4287	30
169.0	172.0	2458	3.0	0.30	1.4	970	13	0.9	4.2	2910	39
172.0	175.0	2459	3.0	0.21	1.8	580	6	0.63	5.4	1740	18
175.0	178.0	2460	3.0	0.53	1.8	1470	16	1.59	5.4	4410	48
178.0	181.0	2461	3.0	0.44	1.2	1290	9			3870	27
181.0	184.0	2462	3.0	0.64	1.0	945	6			2835	18
184.0	187.0	2463	3.0	0.34	1.2		12	1.02		4062	36
187.0	190.0	2464	3.0	1.08	1.4	2760	24	3.24		8280	72
190.0	193.0	2465	3.0	0.23	0.8					2940	51
193.0	196.0	2466	3.0	0.33	1.8	1100	12			3300	36
196.0	199.0	2467	3.0	0.49	2.2	1190	22	1.47	6.6	3570	66

## CT1222.XLS

From	То	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
4.5 m - 65.	0 m										
Total (wa)			60.5	32.13	104.1	91522	1459			I	
Mean				0.53	1.7	1513	24				
65.0 m - 11	13.1 m										
Total (w*a)			48.1	67.48	96.6	129608	1167				
Mean				1.40	2.0	2695	24				
113.1 m - 1	199.0 m										
Total (w*a)			85.9	32.42	289.3	107899	1689				
Mean				0.38	3.4	1256	20				
4.5 m - 199	9.0 m										
Total (w*a)			194.5	132.03	490.0	329029	4315				
Mean				0.68	2.5	1692	22				

## CT1223.XLS

<b>DDH 1223</b>	ASSAY TA	BLE			I					ı	
From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
0.0	7.9	3016	7.9	0.42	1.4	740	65	3.318	11.06	5846	513.5
7.9	11.0	3017	3.1	0.60	2.2	1310	100	1.86	6.82	4061	310
11.0	14.0	3018	3.0	0.86	4.6	3150	30	2.58	13.8	9450	90
14.0	17.1	3019	3.1	0.45	1.2	980	12	1.395	3.72	3038	37.2
17.1	19.0	3020	1.9	0.09	0.8	470	9	0.171	1.52	893	17.1
19.0	22.0	3021	3.0	0.13	0.4	260	6	0.39	1.2	780	18
22.0	24.4	3022	2.4	0.22	1.2	670	9	0.528	2.88	1608	21.6
24.4	27.4	3023	3.0	0.74	3.2	3100	26	2.22	9.6	9300	78
27.4	30.4	3024	3.0	0.42	2.0	1540	42	1.26	6	4620	126
30.4	33.8	3025	3.4	1.40	14.6	1950	165	4.76	49.64	6630	561
33.8	36.4	3026	2.6	0.15	1.8	550	10	0.39	4.68	1430	26
36.4	39.4	3027	3.0	0.06	0.6	216	6	0.18	1.8	648	18
39.4	42.4	3028	3.0	0.05	0.6	290	29	0.15	1.8	870	87
42.4	45.6	3029	3.2	2.00	0.8	276	12	6.4	2.56	883.2	38.4
45.6		3030	3.4	0.06	0.8	330	16	0.204	2.72	1122	54.4
49.0		3031	1.3	0.01	0.4	60	2	0.0065	0.52	78	2.6
50.3		3032	1.9	0.10	0.2	186	6	0.19	0.38	353.4	11.4
52.2		3033	2.3	0.16	1.2	330	38	0.368	2.76	759	87.4
54.5		3034	3.5	0.17	1.0	90	82	0.595	3.5	315	287
58.0		3035	2.5	1.08	0.8	210	25	2.7	2	525	62.5
60.5	62.5	3036	2.0	0.25	8.0	88	40	0.5	1.6	176	80
62.5		3037	3.6	0.15	0.6	126	10	0.54	2.16	453.6	36
66.1		3038	3.0	0.09	0.4	160	14	0.27	1.2	480	42
69.1		3039	3.0	0.63	1.0	250	10	1.89	3	750	30
72.1	73.3	3040	1.2	0.10	8.0	132		0.12	0.96	158.4	30
73.3		3041	3.0	0.43	0.9	252	8	1.29	2.7	756	24
76.3		3042	2.7	0.15	1.4	300		0.405	3.78	810	27
79.0		3043	3.6	0.08	1.0	296		0.288	3.6		21.6
82.6		3044	3.0	0.25	4.0	1770					30
85.6		3045	3.0	0.13	2.2	286					30
88.6		3046	3.0	0.18	1.4	210		0.54			42
91.6		3047	3.0	0.21	0.8	200					48
94.6		3048	3.0	0.04	0.6	194					42
97.6		3049	3.0	0.05	0.6	110					36 30
100.6		3050	3.0	0.10	0.8	232					30
103.6		3051	3.0	0.58	8.2	3280					24
106.6		3052	3.0	0.17	1.4	310			4.2		36
109.6		3053	3.0	0.21	1.0	286					54
112.6	115.6	3054	3.0	0.25	1.3	284	14	0.75	3.9	852	42

## CT1223.XLS

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (wa)	Ag (w°a)	Cu(w*a)	Mo(w*a)
115.6	118.0	3055	2.4	0.13	1.1	184	11	0.312	2.64	441.6	26.4
118.0	121.5	3056	3.5	1.61	12.6	2700	24	5.635	44.1	9450	84
121.5	124.5	3057	3.0	0.06	1.0	176	9	0.18	3	528	27
124.5	127.5	3058	3.0	0.05	0.8	154	10	0.15	2.4	462	30
127.5	130.5	3059	3.0	0.25	0.6	210	8	0.75	1.8	630	24
130.5	133.5	3060	3.0	0.23	0.8	210	22	0.69	2.4	630	66
133.5	136.5	3061	3.0	0.10	0.8	136	12	0.3	2.4	408	36
136.5	139.5	3062	3.0	0.33	8.0	160	26	0.99	2.4	480	78
139.5	142.5	3063	3.0	0.28	0.8	316	19	0.84	2.4	948	57
142.5	145.0	3064	2.5	0.06	0.6	200	16	0.15	1.5	500	40
145.0	147.2	3065	2.2	0.19	1.0	386	15	0.418	2.2	849.2	33
147.2	150.2	3066	3.0	0.15	0.8	270	24	0.45	2.4	810	72
150.2	153.2	3067	3.0	0.47	1.6	510	18	1.41	4.8	1530	54
153.2	156.0	3068	2.8	0.46	5.8	2370	24	1.288	16.24	6636	67.2
156.0	158.0	3069	2.0	3.63	3.0	710	30	7.26	6	1420	60
158.0	161.0	3070	3.0	0.17	1.0	290	24	0.51	3	870	72
161.0	164.0	3071	3.0	1.90	0.8	250	6	5.7	2.4	750	18
164.0	166.0	3072	2.0	0.13	0.5	210	15	0.26	1	420	30
166.0	167.9	3073	1.9	0.13	0.6	100	106	0.247	1.14	190	201.4
167.9	168.3	3074	0.4	2.10	13.0	86	21	0.84	5.2	34.4	8.4
168.3	171.3	3075	3.0	0.05	0.4	90	11	0.15	1.2	270	33
171.3	174.3	3076	3.0	0.07	0.4	130	10	0.21	1.2	390	30
174.3	177.3	3077	3.0	0.04	0.6	164	19	0.12	1.8	492	57
177.3	180.3	3078	3.0	0.05	0.4	100	6	0.15	1.2	300	18
180.3	183.4	3079	3.1	0.15	0.6	68	16	0.465	1.86	210.8	49.6
183.4	186.4	3080	3.0	10.00	0.4	158	8	30	1.2	474	24
186.4	189.4	3081	3.0	0.09	0.4	130	8	0.27	1.2	390	24
189.4	193.2	3082	3.8	0.94	14.6	396	12	3.572	55.48	1504.8	45.6
193.2	196.2	3083	3.0	0.41	0.8	110	9	1.23	2.4	330	27
196.2	199.2	3084	3.0	0.03	0.6	80	8	0.09	1.8	240	24
199.2 202.2	202.2	3085	3.0	0.04	0.6	92	12	0.12	1.8	276	36
	205.2	3086	3.0	0.01	0.6	82	11	0.03	1.8	246	33
205.2 208.2	208.2 211.2	3087 3088	3.0	0.03	0.4	60	16	0.09	1.2	180	48
				0.09	0.4	100	16	0.27	1.2	300	48
211.2	213.6	3089	2.4	0.13	0.6	62	20	0.312	1.44	148.8	48
213.6	214.1	3090	0.5	1.61	8.0	186	12	0.805	4	93	
214.1	217.2	3091	3.1	0.06	0.6	62	12	0.186	1.86	192.2	37.2
217.2	220.2	3092	3.0	0.03	0.4	66	11	0.09	1.2	198	33
220.2	223.2	3093	3.0	0.08	0.4	92	22	0.24	1.2	276	66
223.2	226.2	3094	3.0	0.04	0.2	96	10	0.12	0.6	288	30

Page 2

## CT1223.XLS

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
226.2	229.2	3095	3.0	0.02	0.2	110	18	0.06	0.6	330	54
229.2	232.2	3096	3.0	0.03	0.2	100	16	0.09	0.6	300	48
232.2	235.2	3097	3.0	0.06	0.2	120	18	0.18	0.6	360	48 54
235.2	238.2	3098	3.0	0.02	0.2	92	16	0.06	0.6	276	48
238.2	241.2	3099	3.0	0.01	0.4	94	16	0.03	1.2	282	48
241.2	244.2	3100	3.0	0.06	0.3	140	22	0.18	0.9	420	66
244.2	247.2	2867	3.0	0.01	0.2	20	4	0.015	0.6	60	66 12 27 21 72 15
247.2	250.2	2868	3.0	0.03	0.6	62	9	0.09	1.8	186	27
250.2	253.2	2869	3.0	0.02	0.4	42	7	0.06	1.2	126	21
253.2	256.2	2870	3.0	0.11	3.6	140	24	0.33	10.8	420	72
256.2	259.2	2871	3.0	0.06	0.6	68	5	0.18	1.8	204	15
259.2	264.0	2872	4.8	0.01	0.6	164	5	0.048	2.88	787.2	24
0.0 m - 33.	B m										
Total (w*a)			33.8	18.48	106.2	46226	1772				
Mean				0.55	3.1	1368	52				
33.8 m - 19	6.2 m										
Total (w*a)			162.4	87.54	285.6	65468	2772				
Mean				0.54	1.8	403	17				
196.2 m - 2	64.0 m		-								******
Total (w*a)			67.8	3.68	41.7	6189	898				
Mean				0.05	0.6	91	13				
0.0 m - 196	5.2 m										
Total (w*a)			196.2	106.03	391.8	111694	4544				<del></del>
Mean				0.54	2.0	569	23				
0.0 m - 264			004.0	400.70	100 5	447000	5440				
Total (wa)			264.0	109.70	433.5	117883	5443				
Mean	<u> </u>		1	0.42	1.6	447	21				

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## APPENDIX 4

Excerpts from International Skyline's
Bronson Slope Mine
Approval Certificate Application
(sections 2, 3)

## 2.0 GEOLOGY

## 2.1 Regional Geology (after Rhys 1993, 1995)

The Iskut River region is within the Intermontane Belt on the western margin of the Stikine terrane. Three distinct stratigraphic elements are recognised in the western portion of the area (Anderson, 1989): (i) Upper Paleozoic schists, argillites, coralline limestone and volcanic rocks of the Stikine Assemblage, (ii) Triassic Stuhini Group volcanic and sedimentary are related strata, and (iii) Lower to Middle Jurassic Hazelton Group volcanic and sedimentary are related strata.

Intrusive rocks in the Iskut River region comprise five plutonic suites. The Stikine plutonic suite comprises Late Triassic calc-alkaline intrusions which are coeval with Stuhini Group strata. The Copper Mountain, Texas Creek and Three Sisters plutonic suites are variable in composition but are roughly coeval and cospatial with Hazelton Group volcanic strata. Tertiary elements of the Coast Plutonic Complex are represented by predominantly granodioritic to monzonitic Eocene intrusions of the Hyder plutonic suite, exposed 12 kilometres south of the Bronson Slope deposit (Britton et al., 1990).

The age, mineralogy and texture of the Red Bluff porphyry stock (associated with the Bronson Slope deposit), suggest that it belongs to the metallogenetically important Early Jurassic Texas Creek plutonic suite (Alldrick, 1985; Alldrick et al, 1987; Brown, 1987). Plutons of this suite are widespread in the Stewart, Iskut River region and range in age from 196 to 185 million years (Anderson, 1993; MacDonald et al., 1992, and in preparation).

## 2.2 Project Geology

#### 2.2.1 Geology of the Bronson Creek Area

Strata in the Bronson Creek area are divided into a lower and an upper sequence; probably correlating with Triassic Stuhihi Group and Jurassic Hazelton Group respectively. The sequences are separated by a flat lying to gently dipping regional unconformity exposed some three kilometres to the southwest of the deposit near the Johnny Mountain Gold mine (Figure 2-1).

The lower sequence comprises folded turbiditic greywackes with interbedded siltstones, mudstones, volcanic conglomerate and rare lenses of carbonate rocks. The sequence is weakly to moderately metamorphosed (lower greenschist facies).

The lower sequence is intruded by the Red Bluff porphyry stock, a hydrothermally altered, potassium feldspar megacrystic, plagioclase porphyritic intrusion of probable granodioritic composition. The stock is approximately 2.0 kilometres long, up to 0.3 kilometres wide and trends southeast along the southwest side of the Bronson Creek valley. Contacts of the stock with country rocks are not well defined, but where observed in drill core or underground workings are either faulted or intrusive. The southwest and northeast contacts appear to be southwesterly dipping.

#### 2.2.2 Geology of the Bronson Slope Deposit

The Bronson Slope porphyry gold, copper, silver, molybdenum deposit occurs on the southwest flank of the Red Bluff stock in hydrothermally altered country rocks and to a lesser extent in altered intrusive rocks.

The country rocks in the deposit comprise dark coloured, intermediate to mafic mudstones and siltstones with lesser amounts of light coloured wackes as interbeds. The sedimentary rocks are variably hydrothermally altered as a function of proximity to the intrusive porphyry. The alteration sequence in order of increasing distance from the intrusive is: (i) potassium feldspar alteration with subordinate chlorite, sericite and biotite, (ii) chlorite biotite hornfels with subordinate calcite and (iii) biotite carbonate alteration (occasionally schistose) with subordinate chlorite and sericite. There is field mapping evidence of a quartz, sericite, pyrite phyllic zone followed by a calcite, epidote, biotite, chlorite propylitic zone adjacent to those previously mentioned but these zones have not been encountered in the present drill pattern.

The intrusive rocks in the deposit comprise the Red Bluff porphyry stock variably but extensively altered by the overprint of quartz, magnetite mineralization. The quartz, magnetite was emplaced by multiple phases of veining which exhibit a wide range of depositional textures including: (i) simple widely spaced quartz, magnetite stringers ranging from several millimetres to several centimetres thick, (ii) several sets of crosscutting quartz, magnetite stringers of similar size, (iii) a stockwork of multiple sets of crosscutting quartz, magnetite stringers of sufficiently dense spacing to comprise greater than 50% of the whole rock mass, (iv) complete replacement of the original rock by quartz (90%) and magnetite (10%) and (v) a stockwork of quartz magnetite stringers cutting quartz, magnetite replacement to form a quartz, magnetite breccia. The quartz, magnetite mineralization has also occurred in the sedimentary rocks in the deposit.

The deposition of gold, copper, silver and molybdenum has accompanied late quartz, pyrite veining that has cut the sedimentary rocks, the intrusive rocks and the quartz, magnetite mineralization. The ore minerals have deposited as discrete grains in and along boundaries of quartz stringers, as discrete grains disseminated throughout altered mafic sedimentary rocks and as thin films coating closely spaced late hairline fractures.

The metal prices used to define the metal grade categories are: (i) gold at US \$12.06 per gram or US \$375 per troy ounce, (ii) silver at US\$ 0.16 per gram or US \$5.06 per troy ounce and (iii) copper at US \$2,072.34 per metric tonne or US \$0.94 per pound. Molybdenum values were not included in the determination of metal grade categories. The Canadian dollar value used is equivalent to US \$0.75.

In the case of the Bronson Slope deposit, the total inferred and indicated resource of mineralised rock containing greater than Cdn. \$10.00 per metric tonne worth of metal (Gross Contained Metal Value) is 90.2 million metric tonnes containing an average of 0.749 grams gold per metric tonne, 4.2 grams silver per metric tonne, 0.16 % copper and 0.01 % molybdenum. The value of metals contained in this resource is Cdn. \$1.56 billion or an average of Cdn. \$17.34 per metric tonne.

Within this larger deposit, the company has designed an open cut that would initially mine the lower cost material. This open cut contains a probable reserve of 56.7 million metric tonnes containing an average of 0.545 grams gold per metric tonne, 2.4 grams silver per metric tonne, 0.18 % copper and 0.01 % molybdenum including all mineralised rock containing greater than Cdn. \$5.00 per metric tonne worth of metal. The value of metals contained in this reserve is Cdn. \$813.6 million or an average of Cdn. \$14.34 per metric tonne. In order to mine this reserve of mineralised rock, the company will have to mine a total of 16.3 million metric tonnes of waste rock. The ratio of waste rock to ore is 0.29:1. This proposed open cut mine plan is the subject of this Application for Environmental Review.

#### 2.3.2 Mine Life

The company is proposing to construct a concentrator nominally capable of processing 12,000 metric tonnes per day of ore. Assuming a plant availability of 345 days per year, the mine plan should be completed in 13.7 years.

#### 2.2.3 Ore Mineralogy

The ore minerals in the deposit are as follows; (i) copper: chalcopyrite with minor covellite, chalcocite, malachite, native copper and cuprite, (ii) silver: tetrahedrite, (iii) molybdenum: molybdenite and (iv) gold: not seen but demonstrates a correlation with copper and likely occurs microscopically on chalcopyrite grain boundaries. The gangue minerals in the deposit are quartz, pyrite, dolomite and calcite with minor chlorite, biotite and sericite. The magnetite content of the deposit is approximately 10% and represents a recoverable and potentially profitable component of the deposit if transportation costs from the site to tidewater can be minimized.

#### 2.2.4 Host Mineralogy

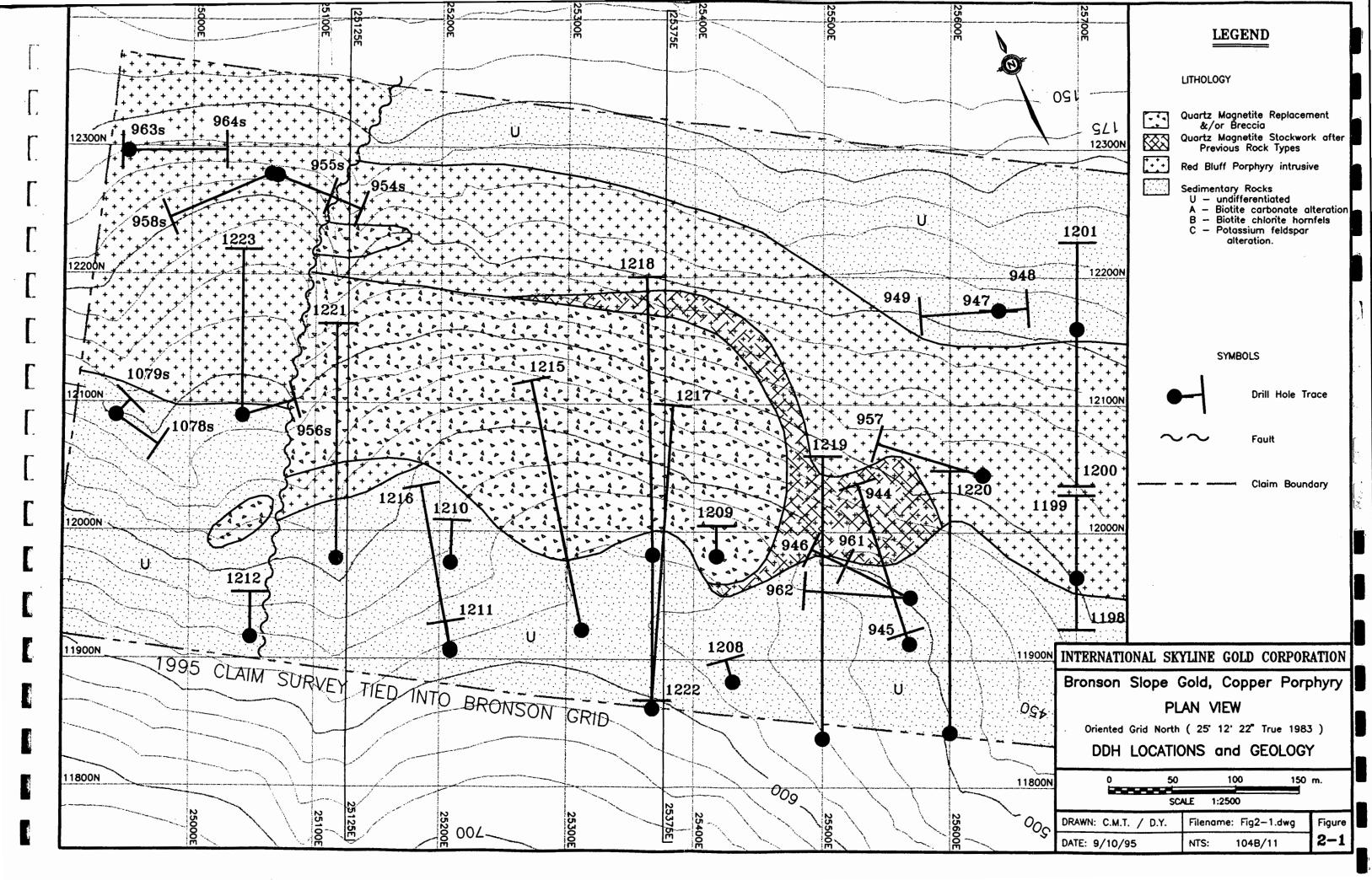
The mineralogy of the host rock and of the waste rock comprises predominantly feldspar, quartz, chlorite, dolomite, pyrite, calcite, biotite, sericite and minor clay minerals.

#### 2.3 Reserves and Mine Life

#### 2.3.1 Reserves

The reserve estimate for the Bronson Slope deposit is based on information from 47 diamond drill holes comprising 7,126 metres of drilling. These holes were drilled during exploration projects in 1965, 1988, 1993, 1994 and 1995. The 1988 program gave preliminary indications of the gold potential of the deposit but it was not until the 1993 drilling that the size potential was discovered. The high grade core of the deposit was outlined in 1994.

Reserves have been calculated using the bench polygonal weighting method. The steps used to calculate reserves in this fashion are as follows: (i) the deposit is divided into a series of horizontal slices approximating mining benches in an open pit mine; in the case of the Bronson Slope deposit the bench thickness is 10 metres, (ii) for each drill hole on each bench, a composite metal assay value is assigned by finding the weighted arithmetic mean of the assay intervals that fall within the 10 metre elevation slice, (iii) the composite metal assay value for each drill hole on each bench is assigned to a polygonal area surrounding the drill hole; the shape of the polygon being determined by perpendicular bisector lines between drill holes, (iv) the volume and weight of mineralised rock associated with each polygon is calculated by multiplying the area of each polygon by the bench thickness and the specific gravity of the rock (S. G. = 2.65), (v) the total tonnages of the polygonal blocks falling within the various metal grade categories are compiled and (vi) the weighted arithmetic means of the metal grades for the total tonnages in each metal grade category are calculated.



## 3.0 PROJECT DESCRIPTION

#### 3.1 Location and Access

#### 3.1.1 Location

The deposit is located in the Liard mining district at 56° 39' 54" N. Latitude, 131° 05' 15" W. Longitude on N. T. S. map sheet 104 B 11E. It is 110 air km northwest of Stewart, B.C.

#### 3.1.2 Present Access

The property is only accessible by air and is serviced by two nearby airstrips, Bronson Creek and Johnny Mountain, both of which are capable of utilizing Hercules C-130 transports. The airstrips are 240 air kilometers from Terrace, B. C. and 82 air kilometers from Wrangell, Alaska. Cominco Ltd. also uses a hovercraft to transport freight via the Iskut and Stikine Rivers to Wrangell.

#### 3.1.3 Planned Access

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The development of the Bronson Slope gold, copper porphyry will be dependent on road access to the site. A 30.5 kilometer extension of the existing Eskay Creek road from Volcano Creek to Bronson Creek is the most logical route. This extension would allow concentrate and supplies to be transported via the Cassiar - Stewart Highway and the existing port facilities located at Stewart, B.C. on the Portland Canal.

The Iskut Valley spur road is planned as an extension to the existing Eskay Creek Road (Figure 3-1) which connects Homestake Canada's Eskay Creek mine to Highway 37 just south of Bob Quinn.

The Iskut Valley spur road was the subject of a study completed by Klohn Leonoff Consulting Engineers on March 28, 1991. The study was commissioned by the British Columbia Ministry of Energy, Mines and Petroleum Resources. The report was intended to provide approval for road access to the Cominco Snip mine located at the junction of Bronson Creek and the Iskut River as well as access to the Eskay Creek mine located near Tom Mackay Lake. The section of the road to Eskay Creek has been completed.

The portion of the road to the Cominco Snip mine has not yet been completed. The construction of the road has been approved in principal. The final routing and design will be carried out under the issuance of a Ministry of Forests Special Use Permit for a Category C Resource Development Road. The construction of the road will have to meet the requirements of the Forest Practices Code.

As the road has been already approved in principal, it is not necessary for it to be reapproved under this application.

Concentrate will be hauled from the mine site by a contractor using highway certified vehicles. Approximately eight truckloads per day of concentrate will be hauled from the mine site to Stewart, British Columbia. General materials, explosives and fuel, as well as other specific materials, will be hauled in vehicles designed for those purposes.

All vehicles using the Iskut Valley Road and the Bronson Slope Spur Road will be in radio contact at all times. The vehicles will be required to give their location at selected points along the access road. Access to the road will be controlled by an existing gate, jointly controlled by Eskay Creek and Bronson Slope mines, in the middle of the Ningunsaw River Bridge at approximately km 4 on the access road. We understand the gate is locked with a rotating combination lock and is adequate to restrict unauthorized access to the area. The component distances between the mine site and shipping point are:

	KiVI
Mine Site to Junction of Eskay Creek Road	30
Iskut Valley Road to Hwy 37 Junction	50
Highway 37 Jct to Bell II	44
Bell II to Meziadin Jct	94
Meziadin Jct to Stewart (Hwy 37A)	62

An avalanche and snow safety study has been completed for the Iskut Valley Road and a study will be undertaken for the Bronson Slope Spur road.

#### 3.1.4 Logging Truck Traffic - Highways 37 and 37A

A major truck traffic source on Highway 37 and 37A is logging traffic. Estimates of logging truck traffic were obtained from Ministry of Forests in Smithers and are as follows:

Highway 37

Yukon traffic

20 to 30 loads/day August 1995 4 to 5 October 1995

British Columbia

8 to 9 loads/day December to March annually

Highway 37A

Approximately 10 percent of this traffic.

Additional logging truck traffic originates from the Bobquin and Nass-Kispiox areas. Estimates are presently unavailable.

#### 3.2 Mine Plan

Figure 3-2 is a site plan showing the relationship of the open pit and tailings impoundment.

#### 3.2.1 Introduction

The Bronson Slope Gold, Copper Porphyry will be developed utilizing conventional open pit methods, keeping in mind that Bronson Slope is not a conventional open pit deposit. The mineral deposit has been exposed on three sides by natural erosion, leaving a steep bluff protruding from a mountain slope. This will allow the deposit to be mined by a series of horizontal benches, which will ultimately result in a slice being taken of the side of the mountain slope (Figures 3-3 to 3-7). The mined deposit will be referred to as an open pit for simplicity throughout the report.

The deposit is located above the planned site facilities, as opposed to being below the facilities. This stratigraphic location will eliminate the need for hauling material to waste storage facilities and the mill. All material moved from the mine area will be dropped down a twin ore pass system to the valley bottom where it will be transferred by conveyor to either the mill or waste storage facility (Figure 3-8).

#### 3.2.2 Mineable Reserve Estimate

The minimum estimated mineable resource at Bronson Slope is 56,728,000 tonnes of ore grading 0.545 grams per tonne gold, 2.4 grams per tonne silver, 0.18 % copper, 0.01 % molybdenum, and 16,347,000 tons of waste material of which 9,502,000 is possible prestrip. The deposit realizes an ultimate strip ratio of 0.29:1 waste to ore. A breakdown of progressive strip ratios is outlined in Table 3-1. These estimates are subject to increase with further drilling, and more detailed economic analyses.

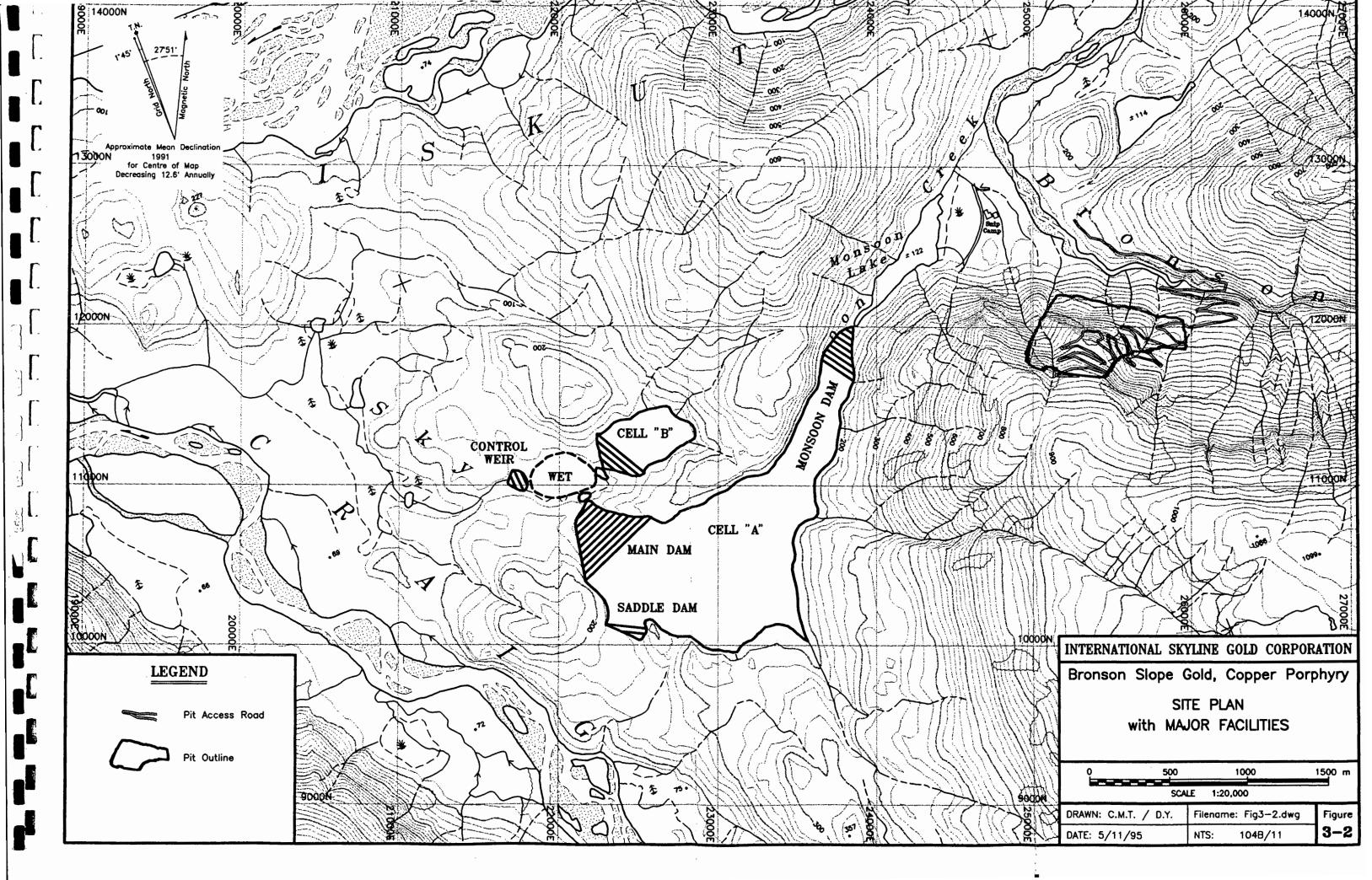
#### 3.2.3 Design Criteria

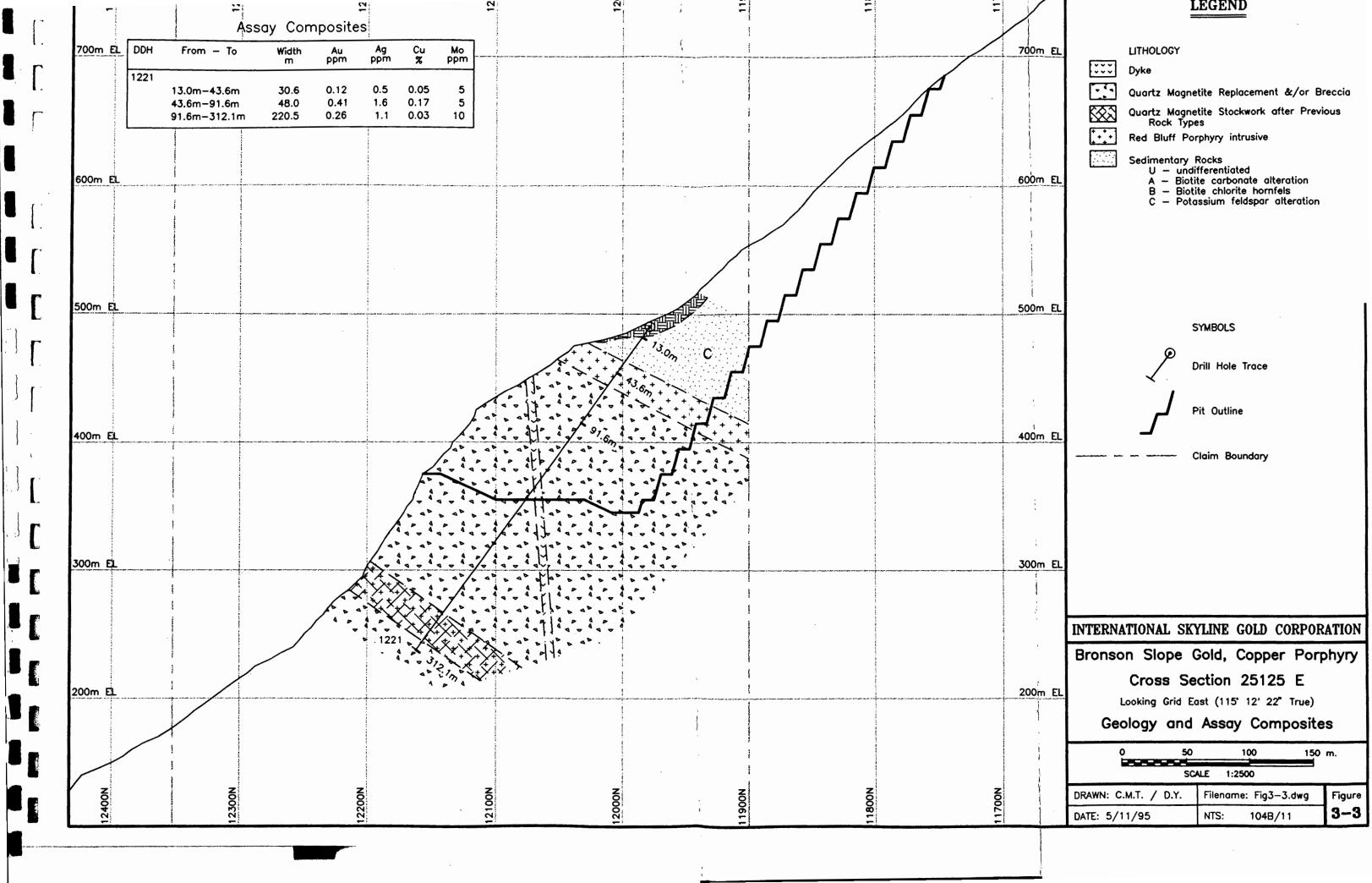
The open pit has been designed with a 55 degree ultimate slope highwall. The Red Bluff itself which forms a good portion of the deposit and has a natural slope of 53 degrees. This is measured from government topographical maps from creek level to the top of Red Bluff. This slope appears to be quite stable with a negligible talus slope at its base. Using this information as a guideline it is assumed a 55 degree highwall will be obtainable. The ultimate highwall slope will be subject to detailed geotechnical studies. The highwall angle will be obtained by mining to 10 meter benches for a total height of 20 meters. The 20 meter benches will be separated by an 8.65 meter berm. The internal bench angle will be 75 degrees (see Figures 3-8 and 3-9). If geotechnical field work indicates a steeper highwall is obtainable, the design criteria may be changed. This would result in an increase in mineable ore and a decrease in prestrip waste.

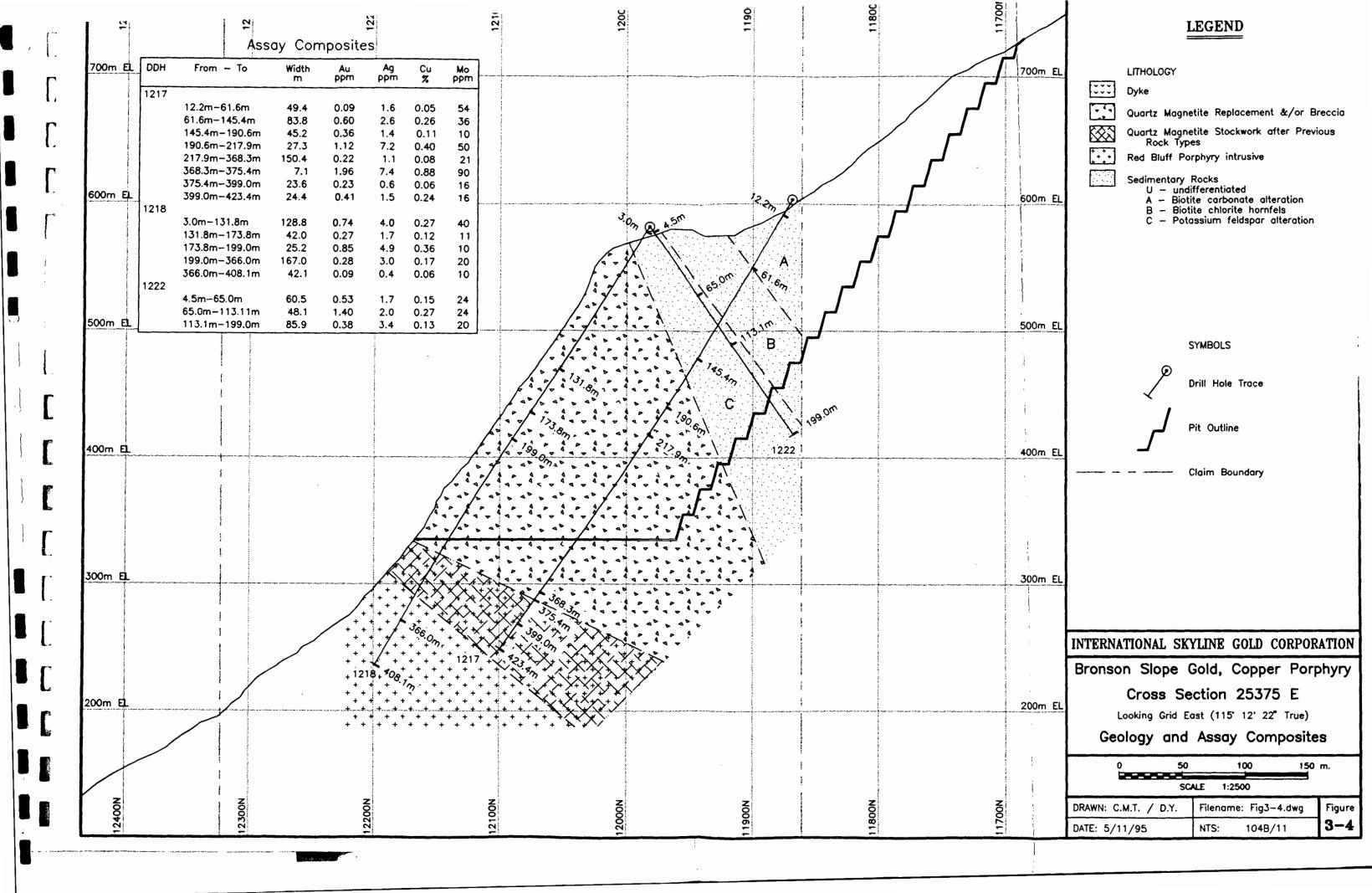
Preliminary geotechnical work carried out during the spring of 1995 indicates that the majority of structures appear to be dipping into the hillside, with one occasional set being near horizontal. This orientation will have to be confirmed at a later date with a core orientation drill hole. No information is yet available on the pore pressure of the highwall, however none of the existing diamond drill holes are making water.

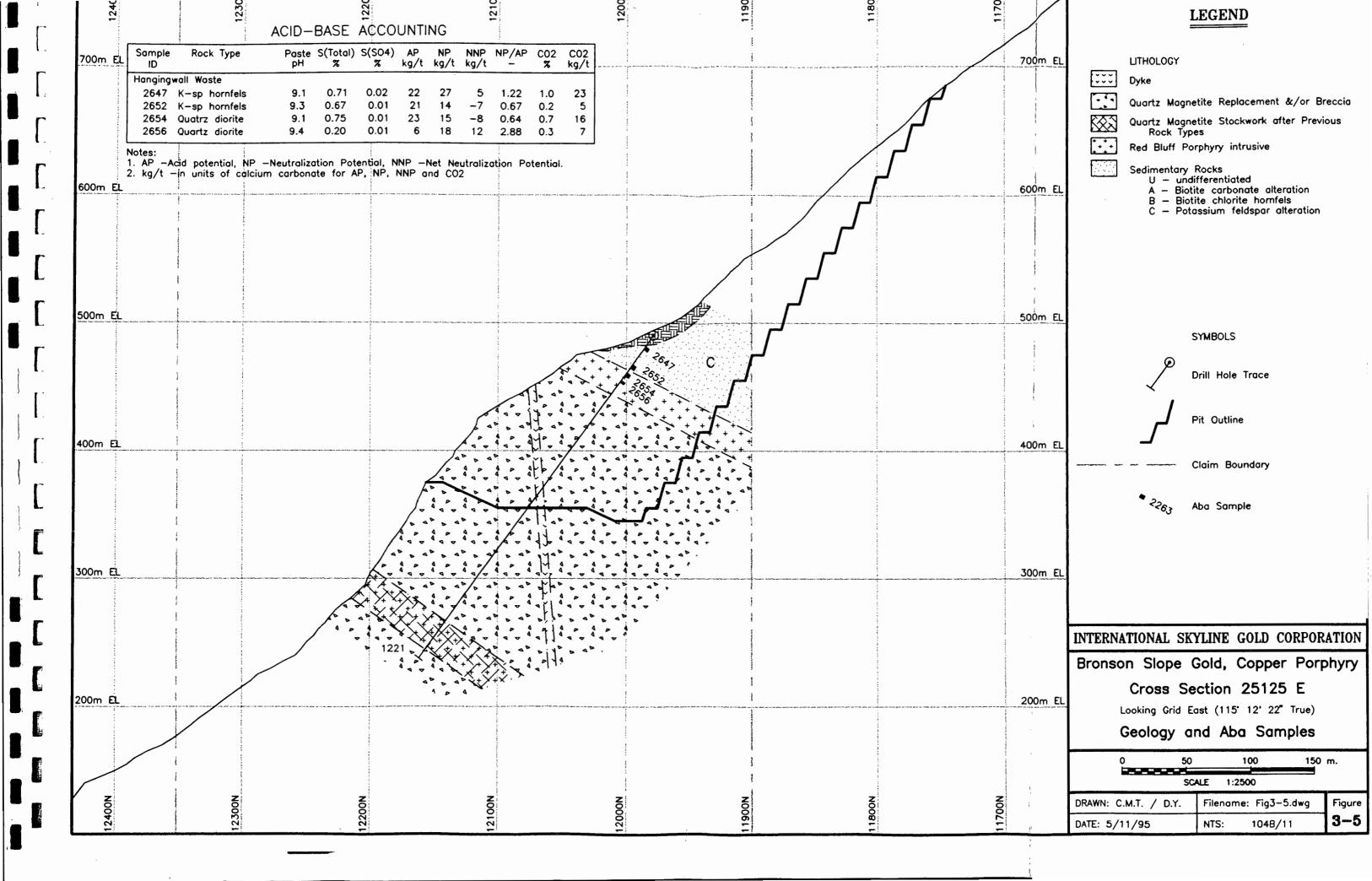
The high wall will not contain any portion of the original pit access road. Due to the nature of the pit access road design, berms will likely be inaccessible after a short period of time. This may result in special procedures to work under berms which may become cluttered with material, or a small cat trail may be required to access berms for cleaning.

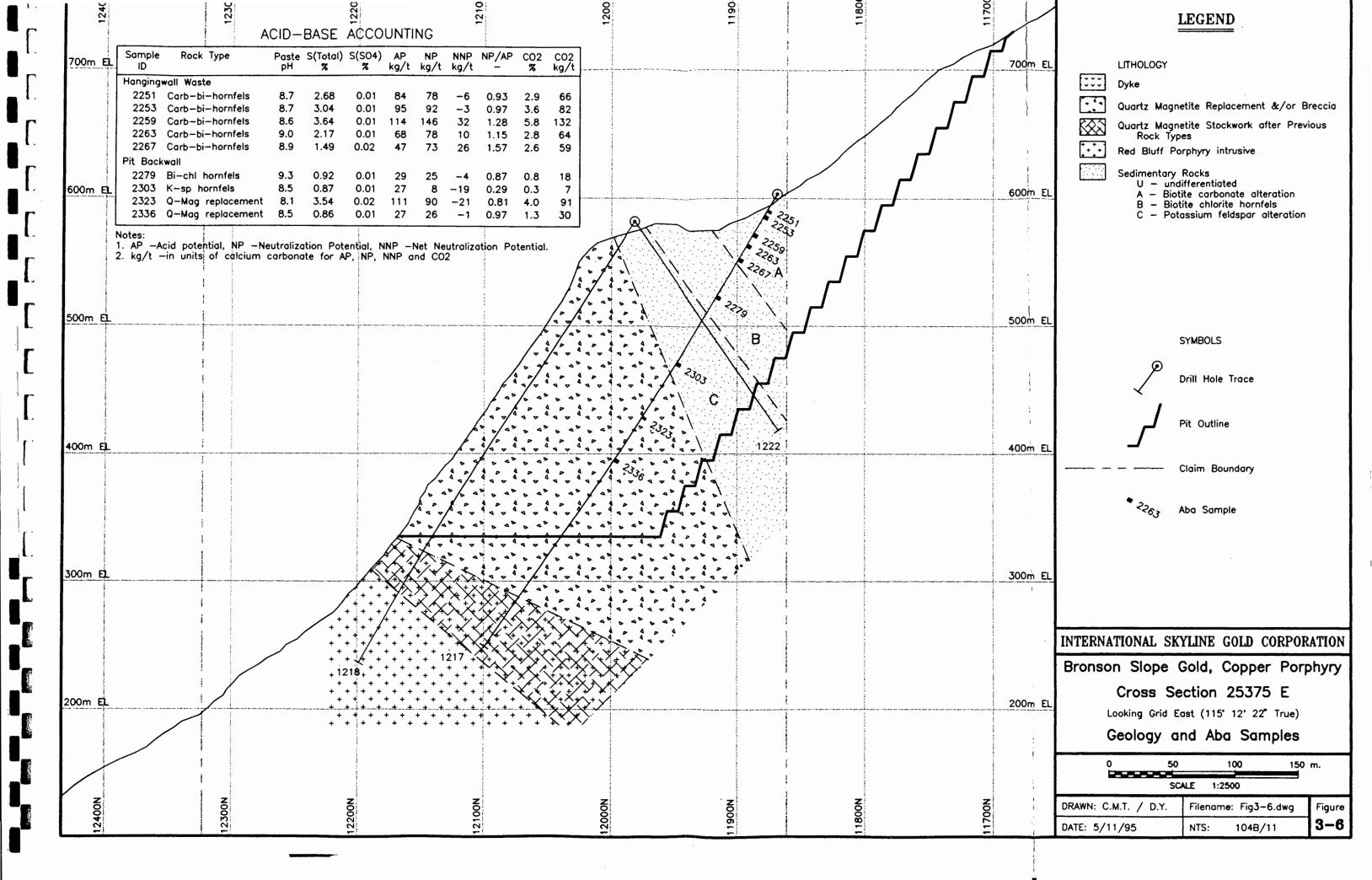
A working bench height of 10 meters has been selected. Due to the unique mineability of the deposit and projected short hauls, relatively small open pit equipment will be utilized. With the internal ore pass system in the pit the longest haul is projected to be 500 meters resulting in short cycle times.

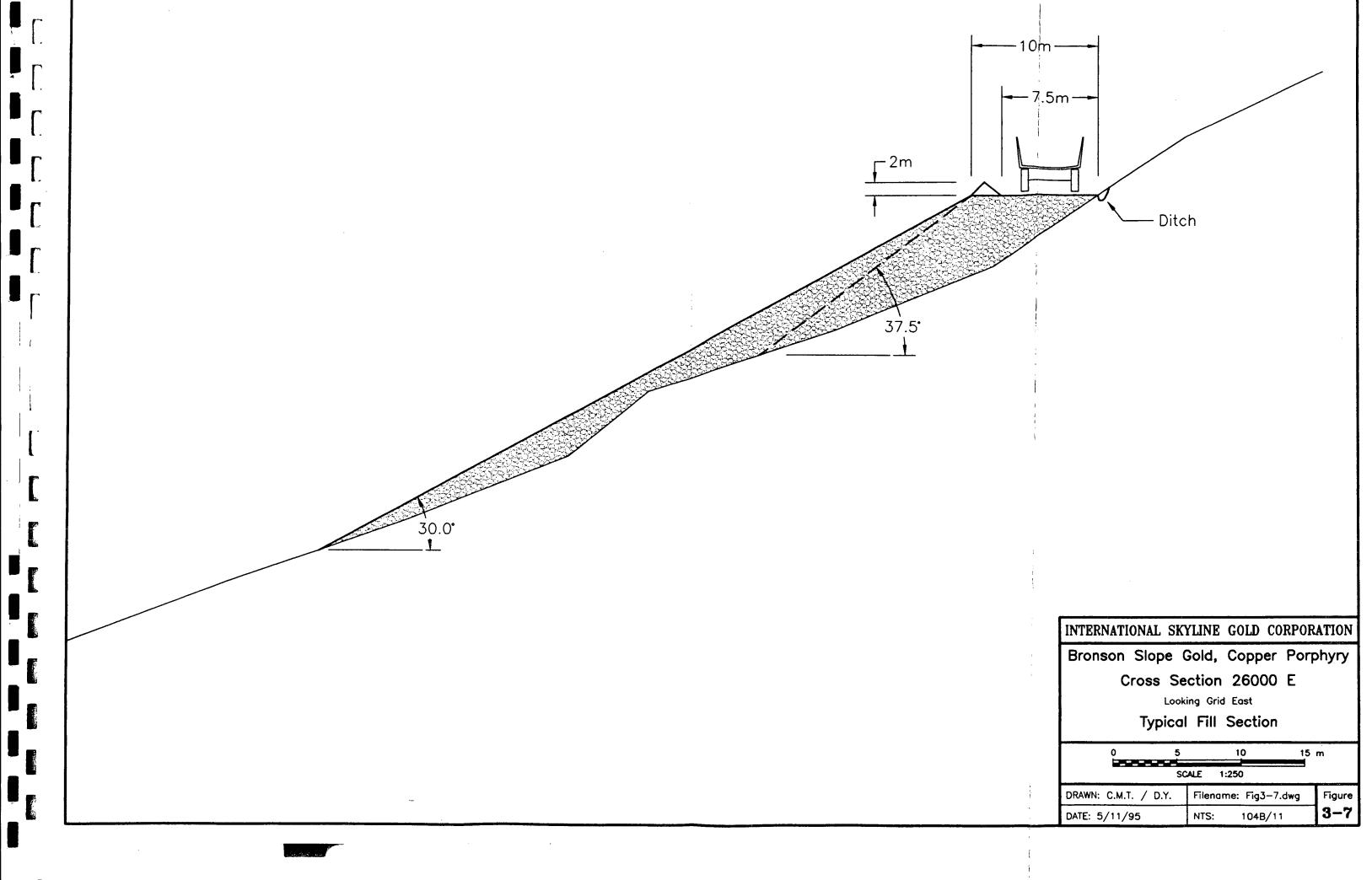


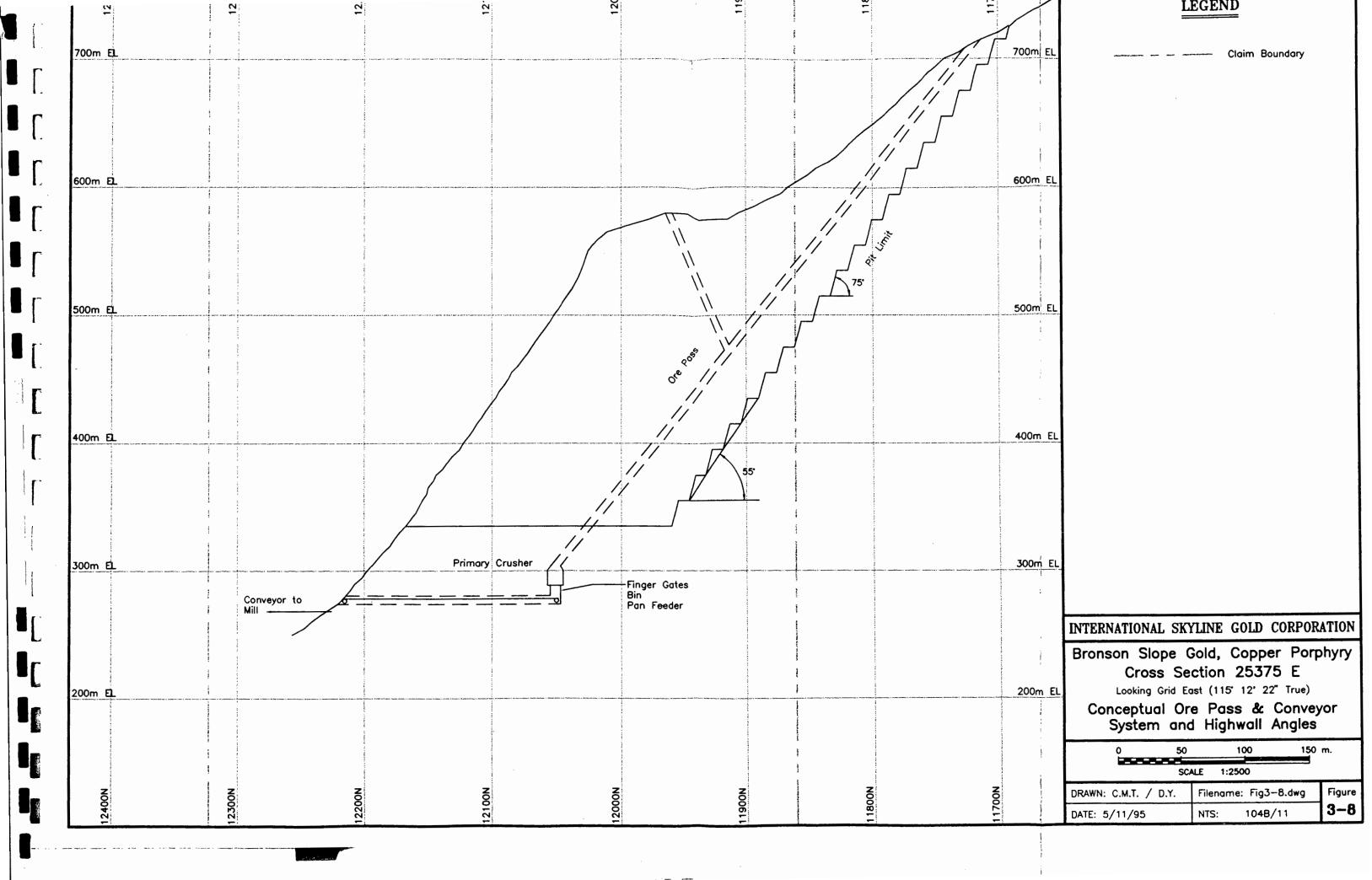






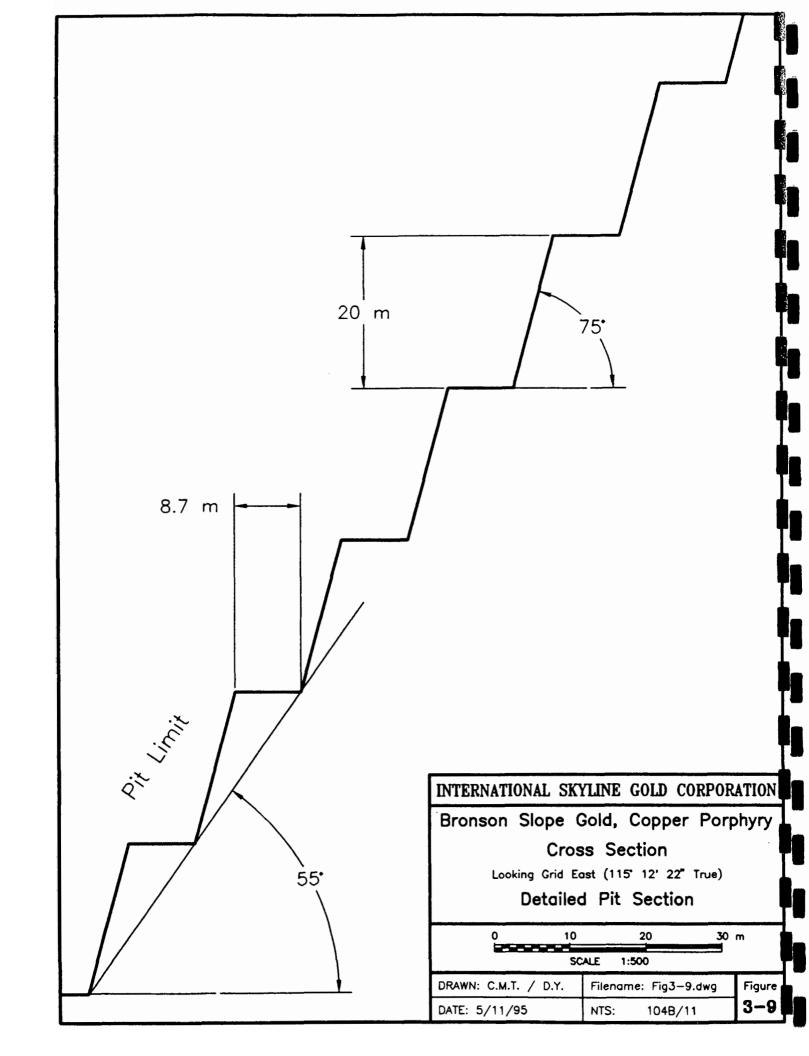






# TABLE 3-1 PROGRESSIVE STRIP RATIOS

Bench	Ore	Waste	Strip	Cumulative	Cumulative	Cumulative
Elevation	Tonnes	Tonnes	Ratio	Ore	Waste	Strip Ratio
710	0	136,246	0.00	0	136,246	0.00
700	0	318,531	0.00	0	454,777	0.00
690	0	338,544	0.00	0	793,321	0.00
680	0	489,190	0.00	0	1,282,511	0.00
670	0	528,146	0.00	0	1,810,657	0.00
660	0	643,146	0.00	0	2,453,803	0.00
650	0	635,192	0.00	0	3,088,995	0.00
640	0	739,911	0.00	0	3,828,906	0.00
630	0	720,642	0.00	0	4,549,548	0.00
620	0	825,162	0.00	0	5,374,710	0.00
610	0	806,727	0.00	0	6,181,437	0.00
600	0	921,224	0.00	0	7,102,661	0.00
590	0	951,875	0.00	0	8,054,536	0.00
580	0	951,875	0.00	0	9,006,412	0.00
570	827,216	495,853	0.60	827,216	9,502,265	11.49
560	1,320,796	316,859	0.24	2,148,011	9,819,123	4.57
550	1,479,258	248,137	0.17	3,627,269	10,067,260	2.78
540	1,769,642	137,233	0.08	5,396,911	10,204,494	1.89
530	1,777,169	173,265	0.10	7,174,079	10,377,758	1.45
520	2,135,339	0	0.00	9,309,418	10,377,758	1.11
510	2,025,978	186,837	0.09	11,335,396	10,564,595	0.93
500	2,020,083	418,161	0.21	13,355,479	10,982,756	0.82
490	2,186,716	252,844	0.12	15,542,195	11,235,600	0.72
480	2,192,583	404,047	0.18	17,734,778	11,639,646	0.66
470	2,259,326	328,356	0.15	19,994,104	11,968,002	0.60
460	2,356,270	358,408	0.15	22,350,374	12,326,410	0.55
450	2,687,198		0.00	25,037,572	12,326,410	
440	2,784,697	26,648	0.01	27,822,269	12,353,058	
430			0.00	30,614,552	12,353,058	
420			0.05		12,503,387	0.37
410						
400			0.00			
390				41,637,100	13,288,669	
380			0.14	44,632,281	13,712,666	
370		748,682	0.28	47,338,542	14,461,348	
360	2,613,216		0.41	49,951,758		
350			0.14	53,201,730		
340	3,527,066	340,331	0.10	56,728,796	16,347,440	0.29



#### 3.2.4 Ore and Waste Movement

Ore and waste will be removed from the open pit via a twin internal ore pass system to the valley bottom. An underground crusher will be located at the bottom of the ore pass system. Ore will be transferred from the crusher to a gravity conveyor for transport to the ore stockpile or the waste storage facility. The ore stockpile will be a live pile. The pile will be used when the fine ore bin is full, and is not planned as a long term storage facility. It is possible that a low grade stockpile will be located on the site. The exact location and size is yet to be determined. The low grade stockpile will be a function of economics.

Waste material will likely be divided into two categories, potential acid generating and acid consuming. All waste material considered to be acid generating will be disposed of in the tailings facility. Waste material considered acid consuming will be used for construction material, and road surfacing during the life of the mine, including the tailings pond dikes. A detailed description of the tailings disposal plan is outlined in Appendix 3-1.

All material within the pit will be moved by conventional truck and shovel operations to the internal ore pass system. Rubber tire loaders may be used in lieu of a shovel and trucks during the early years of operation. This may be possible due to the extremely short hauls that will be realized during the first 3 years of operation. All mobile open pit equipment will be diesel powered.

#### 3.2.5 Ore Pass and Conveyor System

The internal ore pass system will consist of a twin ore pass system within the centroid of the pit. The ore pass system will converge at the bottom of the pit to a central underground crushing facility (Figure 3-6). The ore/waste will be crushed and transferred to either the mill facility for processing or to a waste storage facility.

The pass within the pit area will be kept approximately 2 meters above bench elevation to prevent excessive water flow down the pass, and as a safety barrier to personnel and equipment. A grizzly will be placed on top of the ore pass system to prevent oversize material from entering the pass and causing hang-ups. A mobile rock breaker will be located in the pit area to deal with oversize. The twin system will be required to allow continued access to a pass at all times during operations either for bench development, or during times of material hang-ups.

An inclined horizontal tunnel will be developed to the mill facility. This will allow a positive generation conveyor to be used. The conveyor system will be designed to allow for ore to be delivered to the mill facility, or for waste material to be delivered to the waste storage facility.

#### 3.2.6 Drilling and Blasting

Drilling will be carried out utilizing large diameter rotary drills (127 mm - 254 mm). A smaller sized rotary percussion drill may be required for controlled blasting along the highwall and for opening the ore pass from bench to bench.

Blasting will be carried out utilizing ammonia nitrate based explosives and blasting agents. Specialized explosives may be required for highwall blasting control and for opening of the ore pass from bench to bench. It is anticipated a bulk explosives facility will be located on site, which will supply the mine with both ANFO and slurry type explosives for use in the pit. The bulk explosives facility will meet Federal and Provincial Explosive Guidelines.

Blasting will be carried out using a non-electric system utilizing both surface and down hole delays. Some consideration may have to be given to blast size due the close proximity of the camp facilities to the open pit. Blasting procedures will meet B.C. Mine Health and Safety Regulations.

#### 3.2.7 Waste Rock Disposal

Waste rock disposal will be in the acid consuming rougher (flotation) tailings cell of the tailings impoundment. Rock, once shown to be non-acid generating, may be used for construction purposes. Waste rock disposal is discussed in more detail in Section 3.4.2.

#### 3.2.8 Mining Alternatives

Given the configuration of the deposit and economics of mining, there are no viable alternatives to the proposed mining method. The deposit is near surface on a relatively steep slope and is not amenable to underground mining which produces less surface disturbance than open pit. The total disturbance from the pit for the projected mine life of 15 years will be 51.9 ha, or 23% of the total projected disturbance.

#### 3.3 Mill

#### 3.3.1 Conceptual Design

In order to accommodate the large tonnage requirements of the Bronson Slope Porphyry deposit a new high tonnage mill facility will have to be constructed. The new facility is designed to process 12,000 mtpd of ore grade material. An exact location for this facility has not yet been isolated, however it is anticipated that it will be located in the vicinity of the existing Snip site, on the Bronson Creek alluvial fan.

The location of the mill facility will be subject to geotechnical constraints, ore stockpile locations, location of the ore transport conveyor with respect to the deposit, and tailings location. Concentrate storage will be required on site. The amount of concentrate stored on site would be a minimal amount to keep slightly ahead of the transportation to Stewart.

A detailed report and mill facility plans are available in Appendix 3-2.

Conceptual design as of spring 1995 was for installation of a semi-autogenous grind (SAG) - ball mill grinding circuit with a capacity of 12 000 tonnes per day of ore. Milling will be followed by conventional gravity concentration and flotation circuits to produce a copper concentrate with recoverable molybdenum. The copper concentrate will be further treated to recover a separate molybdenum concentrate. The final copper concentrate will be dewatered using conventional thickening and filtration; all process water will be recycled.

Gravity concentration following milling will be used to recover a portion of the free gold. Flotation, using a bulk rougher and scavenger stages followed by a regrind and three stages of cleaning, will follow to recover much of the remaining gold, silver, copper and molybdenum.

In the future, magnetite may be recovered from the rougher flotation tailings using a wet drum magnetic separator. Cyanide leaching of ore is not contemplated at this time.

Process flow sheets are shown in Appendix 3-2.

#### 3.3.2 Metallurgy

The state of the s

Information in this section was obtained from Process Research Assoc. Ltd. (1995) and is based on four samples of soft, hard, composite (normal grade), and composite low grade ore.

The main copper mineral in the Bronson Slope ore is chalcopyrite, with minor covellite, tetrahedrite and native copper. Molybdenum occurs as molybdenite. Pyrite is the most abundant sulphide gangue mineral, together with minor sphalerite and galena. Gold and silver occur mostly associated with copper sulphide minerals with a minor amount of free gold.

Processing will be carried out by floating the sulphides using reagents that are selective toward the copper minerals. A copper concentrate is produced by regrinding the rougher product, adding reagents to depress pyrite and selectively floating the copper. Molybdenum is separated from the concentrate by depressing the chalcopyrite and floating the molybdenite. Precious metals (gold and silver) are

recovered with the copper product; free gold is recovered by initial gravity concentration.

Microscopic examination of pilot-scale rougher tailings revealed only trace amounts of pyrite and chalcopyrite, thus indicating almost complete sulphide flotation was achieved.

Copper cleaning flotation will follow and is directed at producing a high grade copper concentrate by rejecting pyrite while maintaining high copper, gold, silver and molybdenum recoveries. After initial bulk sulphide float, the concentrate will be reground and sodium cyanide, lime and flotation collector A208 added to selectively depress the pyrite and improve recovery.

Microscopic examination of pilot-scale cleaner tailings and concentrate showed almost complete liberation of chalcopyrite from pyrite.

Molybdenite is naturally hydrophobic, floats with the copper and reports to the copper concentrate. To separate molybdenum from copper, copper minerals will be depressed by maintaining a reducing environment with the addition of sulphur dioxide gas or sodium hydrosulphide and floating under anoxic conditions maintained with nitrogen gas. Molybdenum floation will be enhanced by the addition of oil as a collector.

#### 3.3.3 Process Chemical Use

Mill reagents will include the following: lime, PAX (copper collector), A208 (flotation promoter), methyl isobutyl carbanol (MIBC) (frother), fuel oil (molybdenum collector), sodium bi-sulphide (copper depressant), nitrogen gas (molybdenum flotation), sodium cyanide (pyrite depressant). Table 3-2 lists reagents and quantities required.

#### **TABLE 3-2** MILL REAGENT USE **Daily Consumption** Reagent Use/Tonne of Ore **(g)** (kg) 127 1524 Lime PAX 10 120 108 9 A208 **MIBC** 53 636 S5100 2 24 Sulphuric Acid 196 2352 Sodium cyanide 10 120

# 3.4 Waste Management Plan

# 3.4.1 Tailings Disposal

The tailings from the Bronson Slope deposit will be disposed of in a conventional tailings dam type facility located on the Jim and Sky 3 claim area. A detailed description of the tailings facility location, volumes, and possible creek diversions are described in a report prepared by Robert C. Dick, P. Eng. in Appendix 3-1.

The tailings are expected, on average, to be acid generating. Segregation of tailings into acid consuming rougher tails and acid generating scavenger tailings is planned. On closure the rougher tailings impoundment will be covered capped with neutral or alkaline tailings, if necessary and the surface stabilized to prevent erosion. Scavenger tailings will be permanently flooded. Reclamation is discussed further in Section 5.9

# 3.4.1.1 Acid-Base Accounting and Metals Leaching

The following information was obtained from Process Research Associates Ltd. (1995) tests.

Samples of normal grade composite and flotation tailings were subjected to acid-base accounting (ABA) and inductively coupled argon plasma (ICP) analyses. Tailings samples were produced from lock-cycle pilot scale tests by Process Research Associates Ltd. A multi-element ICP metals analysis was also performed on samples of rougher and cleaner scavenger flotation tailings water. Results are summarized in Tables 3-3 and 3-4.

The metals concentrations in the feed and tailings were quite low. The sulphur content of the feed (2%) produced a negative net neutralization potential of -19.8 kg CaCO<sub>3</sub>/t (NP:AP=0.68). Removal of sulphide minerals during flotation causes the rougher tails to have a negligible sulphur (0.03%) and a positive net neutralizing potential of 36.7 kg CaCO<sub>3</sub>/t. The cleaner tailings contained 67% pyrite or 24.6% sulphur resulting in a net neutralizing potential of -729 kg CaCO<sub>3</sub>/t. Rougher tailings will account for 94.5% of the flotation waste and the cleaner scavenger tailings for 5.5%. The presence of 6% carbonate minerals in the rougher tailings provided some neutralization potential to the combined rougher and cleaner flotation tailings. Blended, the two tailings products produced a calculated net neutralization potential of -5.4 kg CaCO<sub>3</sub>/t.

TABLE 3-3 SUMMARY OF ENVIRONMENTAL TEST RESULTS FOR COMPOSITE 1, ROUGHER TAILINGS AND CLEANER TAILINGS<sup>1</sup>

	TAILINGS AND CL	I	
Parameter (ppm)	Composite 1	Rougher Tailings	Cleaner Tailings
Мо	50	37	94
Cu	2169	309	1970
Pb	23	6	225
Zn	314	77	146
Ni	31	206	662
Co	10	8	112
Mn	658	618	782
Fe(%)	6.35	4.24	16.00
As	24	<5	77
Cd	2	1.0	5.0
Sb	9	<5	<5
v	46	49	49
Cr	185	374	1019
	Acid-Base	Accounting	
S <sub>tot</sub> (%)	2.00	0.03	24.6
Paste pH	9.1	8.6	6.6
NP <sup>2</sup> (kg CaCO <sub>3</sub> /t)	42.7	37.6	39.7
MPA <sup>3</sup> (kg CaCO <sub>3</sub> /t)	62.5	0.94	769
NPR⁴	0.68	40.0	0.05
Net NP <sup>5</sup> (kg CaCO₃/t)	-19.8	36.7	-729

<sup>&</sup>lt;sup>1</sup> Source: Process Research Associates, 1995

<sup>&</sup>lt;sup>2</sup> Neutralization Potential

<sup>3</sup> Maximum Potential Acidity

<sup>&</sup>lt;sup>4</sup> Ratio of Neutralization Potential to Maximum Potential Acidity

Net Neutralization Potential

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# TABLE 3-4 SUMMARY OF ENVIRONMENTAL TEST RESULTS FOR ROUGHER TAILINGS WATER AND CLEANER SCVENGER TAILINGS WATER

Parameter (mg/L)	Rougher Tailings	Cleaner Tailings
CN <sub>tot</sub>		<0.005
Мо	0.06	0.02
Cu	0.05	0.06
Pb	0.13	<0.05
Zn	0.42	2.23
Ag	<0.005	<0.005
Ni	0.18	<0.02
Co	0.01	<0.01
Mn	7.157	0.294
Fe	0.09	0.22
As	<0.05	<0.05
Cd	<0.005	0.011
Ca	189.95	25.79
Mg	13.10	1.08

Note: Total metals analyzed.

Tailings water had relatively low metals concentrations with zinc in the cleaner tailings water at a concentration of 2.23 mg/L. The pH of the rougher tailings water was greater than 8.0 and of the cleaner tailings water, greater than 9.0. Metals levels, are however, higher in concentration than would allow for discharge to the environment undiluted.

#### 3.4.1.2 Site Topography

Site topography is shown in Figure 3-10.

The confluence area of Sky Creek with its two tributaries is a relatively wide valley, with steep bedrock sides, and contains an extensive wetland.

At the downstream end of this area is a narrow gap between bedrock slopes, through which Sky Creek drops into a second wetland around the confluence with a stream on the right bank, which drains a small lake.

This lake is surrounded on three sides by steep bedrock slopes, and its water level is controlled by a bedrock ledge across its discharge.

Below this confluence, Sky Creek continues through this second wetland, then drops rapidly through a canyon, in a series of rapids and falls. This canyon is reported to be the upstream limit of salmon in Sky Creek.

### 3.4.1.3 Proposed Dam Arrangement

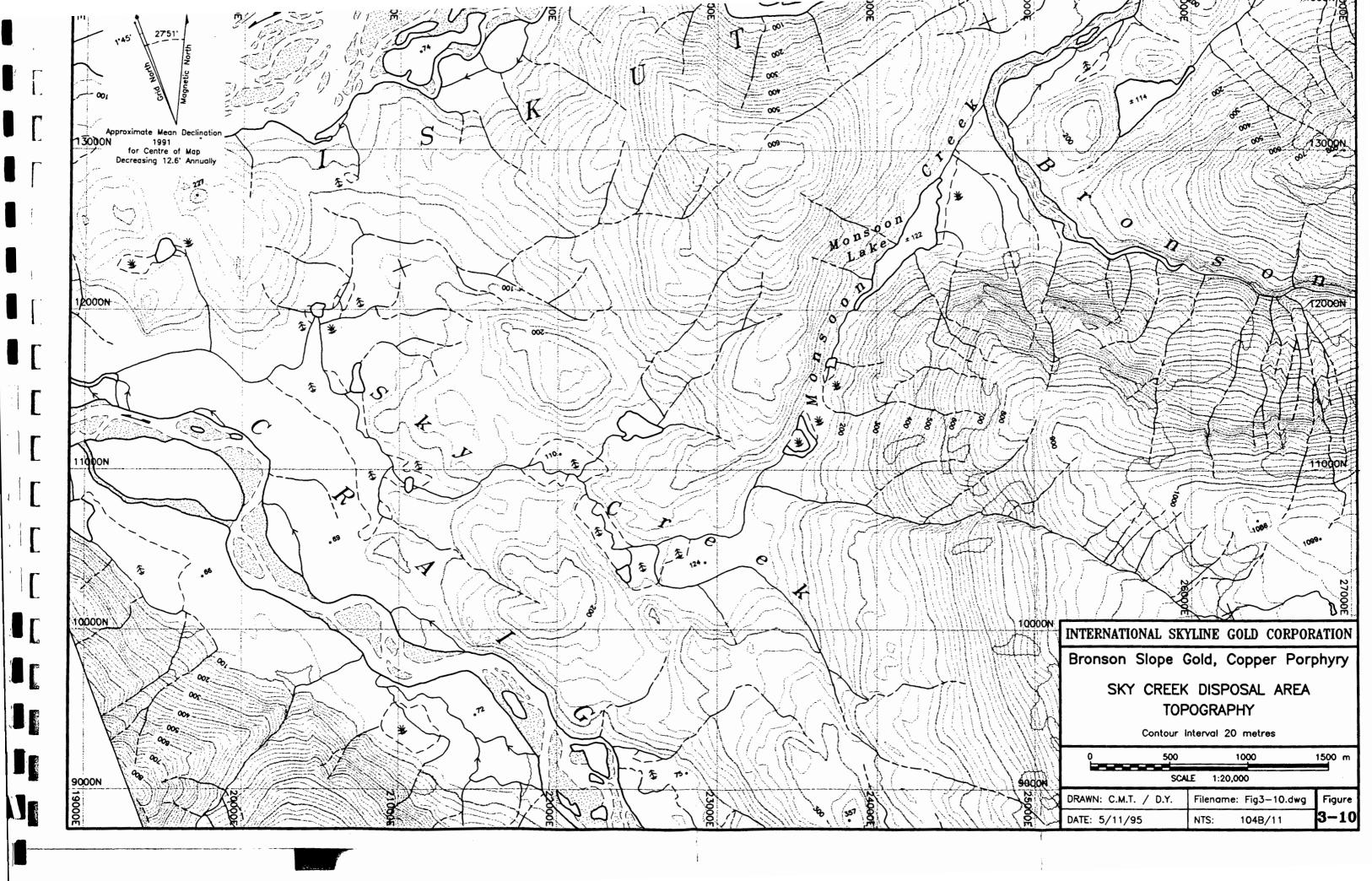
The proposed dam arrangement is shown in Figure 3-11.

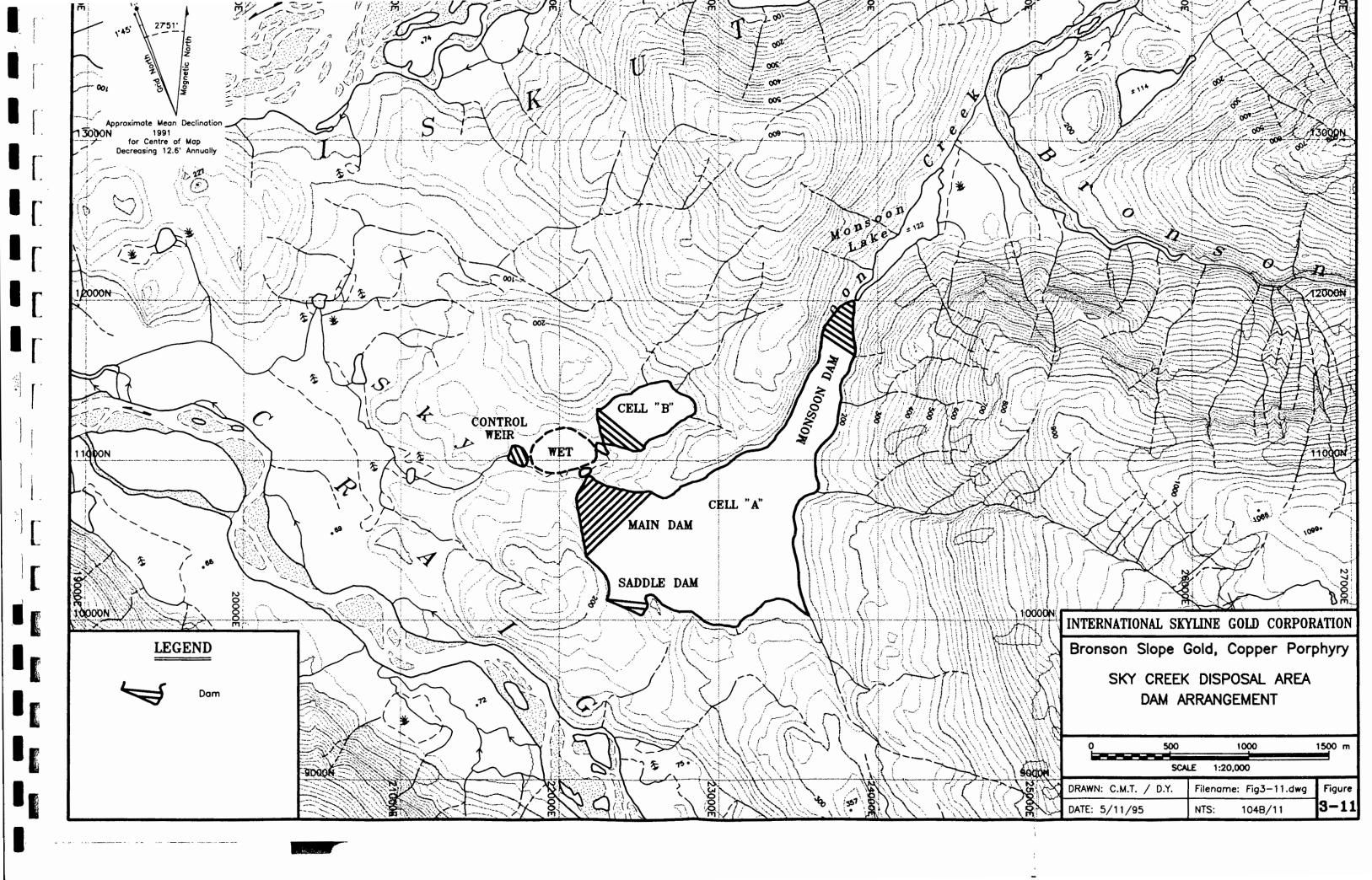
In order to provide natural runoff from the Cominco tailings area into the Sky Creek system, Cell "A" has been extended through the Monsoon Creek valley to the head of Monsoon Lake. A dam will be constructed to elev. 180 metres over the existing Cominco dam (crest about elev. 155 metres).

At the downstream end of Cell "A", a main dam, also to elev. 180 metres, will be built. The downstream toe will be located at the narrowest point of the gap between the two wetland areas.

A small dam some 25 metres high will be built across a saddle on the left bank of Cell "A", some 200 metres upstream of the main dam.

These three Cell "A" dams will be built mainly of tailings, using a centreline method of construction similar to that used in other large tailings dams in B.C.





The downstream slopes will have an overall slope of 5H:1V. To provide control of surface erosion, access for maintenance, and staged reclamation throughout the life of the mine, wide benches will be provided every 10 metres of height. Bench slopes will be 3H:1V, and each bench will be 20 metres wide.

The Cell "B" dam must be an engineered, zoned embankment for secure containment of the acid producing tailings and covering water. The downstream slope would be 3H:1V, with bench slopes 2H:1V and 10 metre wide benches every 10 metres of height. The upstream slope would be 2H:1V without berms.

All Cell "A" and "B" dams could be built in staged fashion.

Small containment ponds at the toes of Cell "A" main dam and Cell "B" dam would provide opportunity for sampling and, if necessary, treatment of runoff and seepage.

The remaining wetland downstream of these ponds would provide natural biological treatment of the water. This area would be left undisturbed throughout construction and operation.

At the head of the canyon, a small weir would be built to control water level in the wetland and provide a second opportunity for sampling and treatment.

## 3.4.1.4 Diversions and Spillways

Diversions and spillways are shown in Figure 3-12.

#### **Diversions**

It will be necessary to divert Sky Creek and its two tributaries above elev. 180 metres to prevent water management problems in Cell "A".

It may be found necessary, after commencement of dam construction, to re-introduce the flow to the natural course of Sky Creek downstream of the canyon for fisheries habitat preservation.

The diversion channel would follow a contour above the left bank of Cell "A" to a small saddle at about elev. 155. The channel would then turn away from Cell "A" and pass through this saddle. A side-channel spillway would be built at this point, to allow the desired flow to continue, while discharging excess water down a small streambed directly into the Craig River.

In the relatively flat gap below the saddle dam, at approximately 155 m elevation, a small wetland could be created to partly replace that covered by Cell "A".

If necessary, the diversion channel could then be carried around the small hill near elev. 150 metres. Where it crosses a small stream on the north side of this hill, another side-channel spillway could ensure the required flow in this tributary, in which fish have been observed by others.

Finally, the diversion channel would lead down into a depression on the left bank of Sky Creek just below the canyon. Another wetland and, possibly, a spawning channel could be created at this point of final discharge into the original Sky Creek channel.

#### Spillways

If conditions permit, the service and emergency spillways from Cells "A" and "B" would be located on the ridge separating the cells. This would permit operation of both spillways from one easily-accessed location.

A common chute would carry spilled water down the bedrock hillside and into the wetland. A containment pond for sampling/treatment will be considered at this location, but may not be practical.

The spillway discharge would then flow through the wetland and the sampling/treatment pond at the control weir.

### 3.4.2 Waste Rock Disposal

Development of the waste rock management plan will to a large extent depend on the acid generation potential of the waste rock. Preliminary acid-base accounting (ABA) and metals analyses have been completed to assess acid generation and metal leaching potential in both waste rock and mine walls. The ABA results are summarized in Table 3-5. Figures depicting the locations of the samples and the results are attached in Appendix 3-3.

Assessment of the mineralogy of the deposit by Skyline indicates that the type and occurrence of minerals of relevance to acid generation is fairly simple. The main sulphide mineral is pyrite (FeS<sub>2</sub>). No zones of massive or banded mineralization have been encountered to date. The other main sulphide mineral is chalcopyrite (CuFeS<sub>2</sub>). No sulphate minerals (such as gypsum) have been reported. This was confirmed by sulphate-sulphur concentrations which are very low.

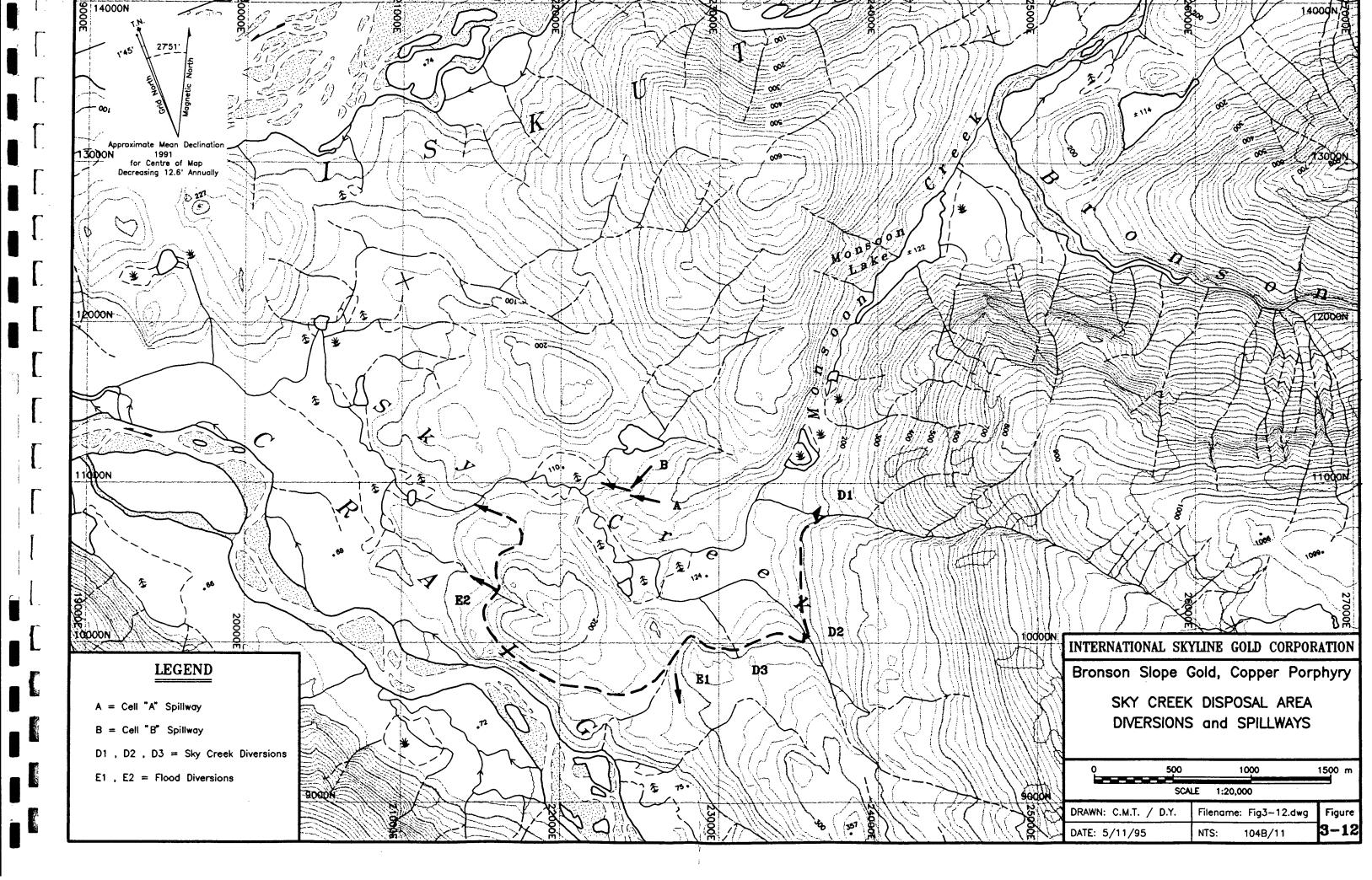


TABLE 3-5
INTERNATIONAL SKYLINE RESOURCES - BRONSON SLOPE PROJECT
ACID-BASE ACCOUNTING

Sample 1D	Rock Type	Paste pH	S(Total)	S(SO4)	AP	NP	NNP	NP/AP	CO2	CO2
		-	%	%	kg/t	kg/t	kg/t	-	%	kg/t
Hangingwall V	<u>Vaste</u>									
2251 C	arb-bi alteration	8.7	2.68	0.01	84	78	-6	0.93	2.9	66
2253 C	arb-bi alteration	8.7	3.04	0.01	95	92	-3	0.97	3.6	82
2259 C	Carb-bi alteration	8.6	3.64	0.01	114	146	32	1.28	5.8	132
2263 C	Carb-bi alteration	9.0	2.17	0.01	68	78	10	1.15	2.8	64
2267 C	Carb-bi alteration	8.9	1.49	0.02	47	73	26	1.57	2.6	59
Pit Backwall										
2279 B	i-chl hornfels	9.3	0.92	0.01	29	25	-4	0.87	0.8	18
2303 K	-sp alteration	8.5	0.87	0.01	27	8	-19	0.29	0.3	7
2323 Q	-Mag replacement	8.1	3.54	0.02	111	90	-21	0.81	4.0	91
2336 Q	-Mag replacement	8.5	0.86	0.01	27	26	-1	0.97	1.3	30
Pit Sidewall an	id Waste									
2647 K	-sp alteration	9.1	0.71	0.02	22	27	5	1.22	1.0	23
	-sp alteration	9.3	0.67	0.01	21	14	-7	0.67	0.2	5
2654 Q	uartz diorite	9.1	0.75	0.01	23	15	-8	0.64	0.7	16
2656 Q	uartz diorite	9.4	0.20	0.01	6	18	12	2.88	0.3	7

#### Notes:

<sup>1.</sup> AP - Acid potential, NP - Neutralization Potential, NNP - Net Neutralization Potential.

<sup>2.</sup> kg/t - in units of calcium carbonate for AP, NP, NNP and CO2.

Comparison of neutralization potential determinations with total inorganic carbon (TIC) indicates that carbonates are the only significant potential acid neutralizers. ISGC has determined that the minerals calcite (CaCO<sub>3</sub>) and dolomite (CaMg(CO<sub>3</sub>)) are present. This further confirmed by the very strong correlation between neutralization potential and calcium concentrations determined by ICP. The carbonate minerals occur as a biotite carbonate alteration (occasionally schistose) with subordinate chlorite and sericite.

Five samples of hangingwall wall waste (ie waste rock removed to expose the ore zone for mining), described geologically as carbonate-biotite alteration contained between 1.5 and 3.6% total sulphur and neutralization potential between 78 and 146 kg CaCO<sub>3</sub>/t. Results for the samples are classified as being of uncertain acid generation potential (neutralization potential/acid potential, NP/AP between 0.9 and 1.6).

The pit backwall will be composed of both waste rock and ore-grade material for which removal is uneconomical. For the four samples tested, this rock had lower sulphur concentrations than the hangingwall waste but also lower neutralization potential. The NP/APs for these samples were marginally less than 1.0, implying uncertain potential for acid generation.

The pit sidewalls, and waste removed to slope back the walls had the lowest total sulphur concentrations of any of the samples tested. Relatively, NPs were relatively higher resulting in NP/APs varying from 0.6 to 2.9. Some of this rock may be acid consuming; however, most samples indicated uncertain acid generation potential.

In summary, all rock types are considered to have uncertain acid generation potential. Further evaluation is required. Additional testing will be required to determine the estimated volumes of material that may be stored in a conventional method, and volumes that will require possible subaqueous deposition. The conceptual plan will have non acid generating material stored in a conventional manner. Material required for construction will consist of this rock.

Waste rock with a slight ARD potential will be evaluated for possible blending with non ARD or highly acid consuming material and possible conventional storage. Material determined to have a high ARD potential will be disposed of in the area of tailings facility for the high acid consuming tailings. This waste rock will be surrounded by acid consuming tailings. (an overview description of the tailings facility is described in Appendix 3-1).

#### 3.4.3 Mechanical Wastes

The operation of mobile equipment in an isolated area results in waste oils and lubricants being produced on site. Disposal of these special wastes will be handled on site in a manner acceptable to the Ministry of Environment. Waste oil may be

used as a fuel for heat sources provided it meets Section 41 of the Special Waste Regulation. The waste oil may also be used in the production of the Ammonia Nitrate based explosives and Blasting Agents. All other special wastes will be disposed of in an acceptable manner

#### 3.4.4 Refuse Disposal

A Waste Management Branch permit will be required for the disposal of industrial and putrescible refuse originating from the mine and camp operations. In accordance with permit requirements, putrescible and other burnable wastes will be incinerated daily in order to minimize attraction of nuisance wildlife and reduce refuse volumes.

Industrial refuse and non-burnable wastes will be collected and trucked to a landfill site at the mine. Only waste approved for disposal in this facility will be buried. The landfill site will occupy approximately 1 ha. Granular backfill will be placed around the fill as cells are formed. The landfill area will be ditched to prevent adjacent runoff from entering the pit. The area will be fenced to discourage bears or other large foraging animals.

#### 3.4.5 Other Wastes

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All remaining or special wastes will be disposed of in a manner acceptable to all Ministries involved.

# 3.5 Water Management Plan

This section deals with the mine area and camp facilities. Diversions and runoff control for the tailings facility are dealt with in the tailings dam section in Appendix 3-1.

#### 3.5.1 Runoff Control and Diversion

#### 3.5.1.1 Pit Area & Pit Access Road

The Bronson Slope pit area is going to interfere with water flow from small runoff channels and creeks. A large number of the channels and creeks on Bronson Slope only carry water during spring runoff and during periods of heavy precipitation. All efforts will be made to divert the water courses above the pit area to West Gully to the west or to East Gully to the east. The preference would be to West Gully as East Gully may affect pit access during periods of heavy precipitation during the early life of the mine.

All water courses intercepted by the pit access road will be maintained with the use of culverts. Water collected by the road courses will be channelled to existing water

courses by the road ditch system. Water that collects on the working pit benches will likely be channelled down the pit access road. A need for settling ponds will be evaluated as required following a survey of water flows in the creeks and gullies that will be affected by the excavation of the Bronson Slope deposit.

#### 3.5.1.2 Camp Area

Runoff control for the camp area will involve maintenance of the existing Bronson Creek dike and diversion system. Upgrades to the system will only be made as required. All remaining runoff controls and diversions will be maintained as required.

#### 3.5.2 Water Balance

#### 3.5.2.1 Mill Facility

The mill facility will require the majority of water for the production of copper concentrate. The details of the mill water balance are not yet available. It has been determined that the primary water source for the mill during startup will be Bronson Creek. Continuous operation of the mill will be supplied by reclaim water from the tailings facility with makeup water being supplied by precipitation and Bronson Creek. The amount of makeup water taken from Bronson Creek should have no significant impact on the flows. The impact should be less than 1% at any given time.

#### 3.5.2.2 Camp Facility

Water for the camp facilities will be supplied by the existing well system. The water quality of Bronson Creek is generally unacceptable for human consumption due to natural metal loading and sedimentation levels. Camp waste water will be directed to the septic field.

#### 3.5.2.3 Sewage Disposal

Camp sewage will be disposed of in the existing septic field area. If this is not possible a new or expanded facility will be utilized. A location for this system will be located if required.

#### 3.6 Infrastructure

It is anticipated that the Cominco Snip operation will be closing down based on present reserve estimates at approximately the same time the Bronson Slope Project would be preparing for start-up, resulting in the possibility of International Skyline acquiring these facilities for the Bronson Slope Project.

### 3.6.1 Camp

The buildings required for the camp are available from two potential sources:

- the Skyline Johnny Mountain mine; or
- use of the Cominco Snip Mine.

The Johnny Mountain camp facilities are available for construction and possible seasonal operations at its present location. This location is fully permitted and usable on short notice. Movement of this camp down to Bronson Creek is also an option. A possible site for this camp would be the present location of the Skyline sawmill. This area is presently under a Forestry Special Use Permit # 14944.

The ideal situation would be the takeover of the Cominco Camp upon the closure of the Snip deposit and all ancillary facilities.

#### 3.6.2 Maintenance Facilities

The existing facilities at the Snip camp would be sufficient for small vehicles only. An additional facility will have to be constructed to handle the larger open pit equipment. The facility itself is expected to be small and may be located on a portion of the mine access road which will remain open for the life of the mine. This will reduce the travel time to and from the pit area due to the length of the pit access road.

#### 3.6.3 Mine Roads

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#### 3.6.3.1 General Concepts

Other than the access road to the site (possibly from the Eskay Creek Mine road along the Iskut River to Bronson Creek), the only road at the mine will connect the camp and mill with the open pit (Figure 3-13). Assuming the Bronson Slope Mine were to use the existing Snip Mine camp, a total of 6.5 km of local mine roads would be required, including the major in-pit access road, but not bench branch roads which would be placed on alternate benches as the pit developed. Roads would be gravel-surfaced, average 10 m width and ditched. Fills would be avoided in road construction where ever possible. Side-casting onto unstable slopes would be avoided. Culverts and cross drains would be placed to maximize stability and downslopes from culverts outside the pit proper would be armoured where necessary to prevent erosion.

The unique stratigraphic location of the Bronson Slope deposit with respect to the location of the site facilities will allow the movement of ore and waste down an ore pass to the mill and waste storage facilities (Figure 3-8). The material will be moved via conveyor from the ore/waste pass system to the mill. The Bronson Slope access

road will be approximately 6550 meters long and has an average grade of 9.2% (Figure 3-13).

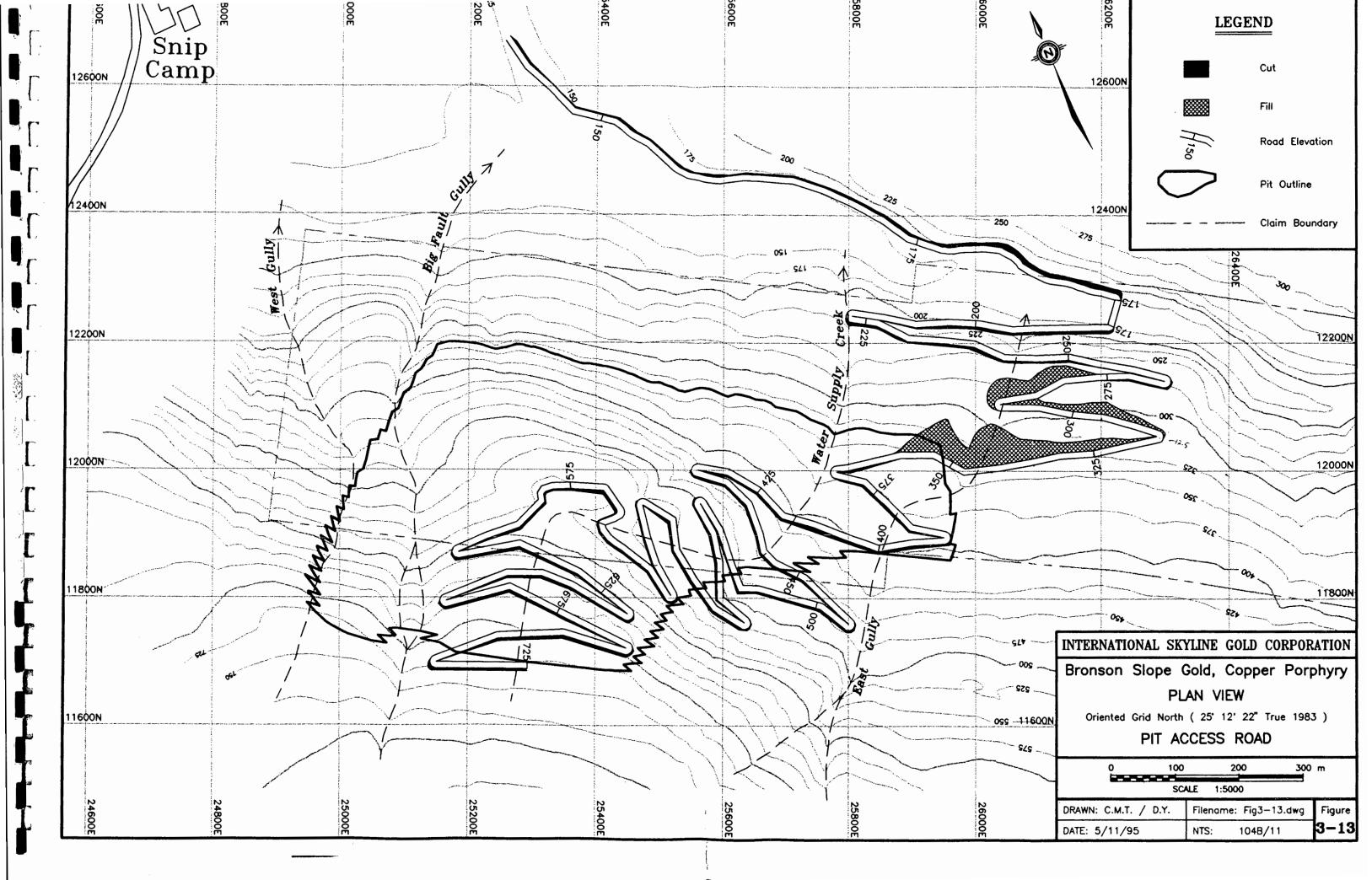
#### 3.6.3.2 Pit Access Road Route

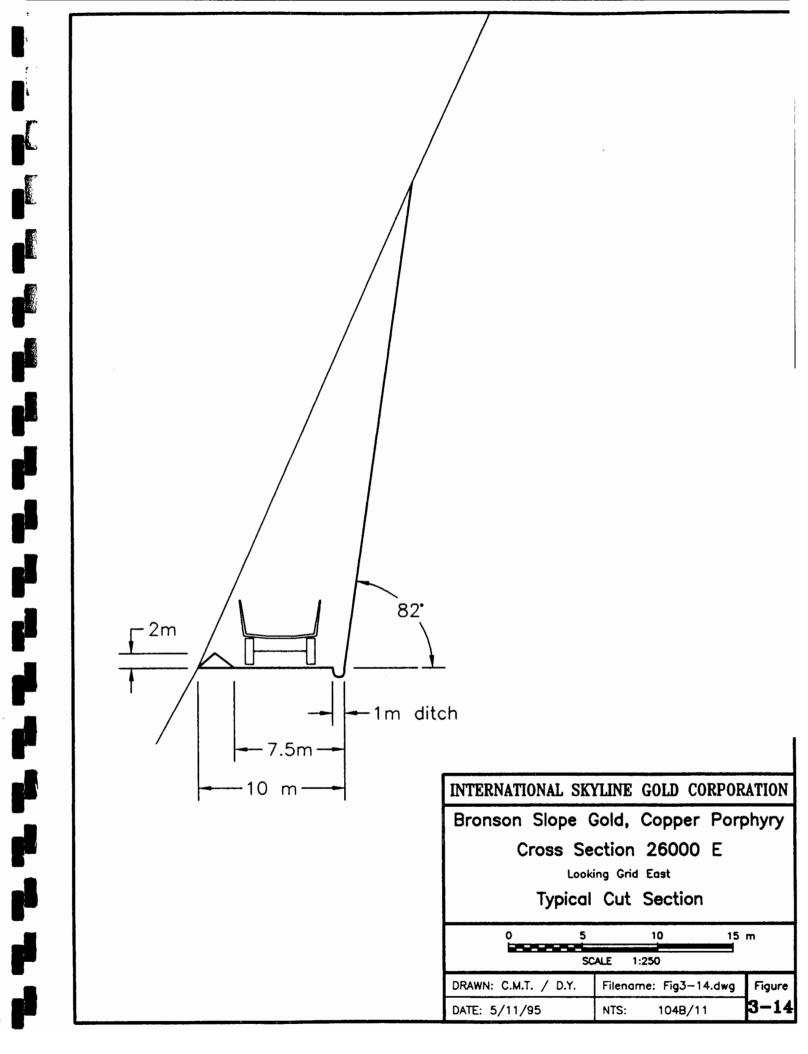
The Bronson Slope pit access road will start on the north side of Bronson Creek in the area of the present Keewatin Camp at the north end of the Bronson Creek airstrip (See Figure 3-8). The exact starting point has not been chosen as it will likely tie into the planned Iskut road extension at this point. The road will be developed on the north side of Bronson Creek. It is necessary to construct this portion of the road on the north side of Bronson Creek to avoid any safety problems with a south side construction which would place the road directly under Bronson Slope itself and directly under mining operations.

Starting at the 125 meter elevation the road will climb at a 10% grade for a distance of 250 meters to the 150 meter elevation. The road will then follow the 150 meter contour for approximately 300 meters before climbing to the 175 meter elevation at 10%. Due to the steep terrain in this area the road will be developed as a cut road. A typical cut section is shown in Figure 3-14.

A crossing of Bronson Creek to the south side will take place in this area. This portion of Bronson Creek is in a canyon. This appears to be one of the better and shorter areas to cross the river. This crossing will be subject to several studies at the feasibility level which will ultimately determine the type of bridge structure required.

The remainder of the road from this point will remain on the south side of Bronson Creek. The road will climb from this point to the 725 meter elevation through a series of switchbacks. The portion of the road from 175 meter elevation to the 275 meter elevation will be cut a road. The portion from 275 meter elevation travels through an area of shallow dipping terrain (less than 30 degrees) and will be developed as a fill road through the 360 meter elevation. Figure 3-5 shows a typical fill section with fill at an angle of repose of 30 degrees and an angle of repose of 37.5 degrees. All fill volumes have been calculated using an angle of repose of 30 degrees. The remainder of the road will be a cut road which will continue to the 725 meter elevation. A cut angle of 89 degrees has been used. This will be subject to on site geotechnical evaluations, and constraints laid out in the Forest practice Code. The road will generate a total of 1,200,000 tons of cut material. A large portion of this material will be ore grade and will be stockpiled until mill startup. The fill portion of the road will require 162,000 tons of material. This material will likely be generated from the cut area on the north side of Bronson Creek. All material used for construction will have to meet ARD standards and be an acceptable rock quality for fill.





# 3.6.3.3 Design Criteria

The application assumes the largest vehicle to use the road will be a Caterpillar 777C haul truck with an operating width of 5.5 meters. The Bronson Slope pit access road will be used for pit access only, therefor it will not be required to be designed to haul road standards.

The present access road design has the road with a total width of 10.0 meters. This includes a 1.0 meter wide ditch and a 2 meter wide berm. The berm will be 1.6 meters high which will meet the 3/4 wheel height berm requirement.

The excessive length of road at a 10% grade will require runaway lanes at given intervals along the route. These lanes will be constructed in such a manner as to high center the vehicle as quickly as possible and bring the vehicle to a safe stop. Other safety measures for bringing equipment down the access road may be required. The road will be radio controlled and pullouts will also be available.

# 3.6.3.4 Runoff Control and Settling Ponds

All road runoff will be directed to the ditch system located along the inside portion of the road. Small creeks and water channels will be diverted or culverts put into place to allow unobstructed flows during normal run-off, and snow melt. The use of settling ponds for ditch water will be subject to further studies with regard to sedimentation loading and flows of water courses in the area.

# 3.7 Power Supply

Three individual power supply options have been addressed and are outlined. The economic benefits and potential drawbacks are outlined below. The Bronson Slope project will require a peak load of approximately 18 megawatts with an operating load in the order of 14 megawatts.

#### 3.7.1 Diesel Power

Diesel power has been reviewed and entered into the cash flow model. At an estimated cost of \$0.09/kwhr the operation likely will not be economic. The post payback portion of the cash flow would generate some revenue, however costs during the payback period would increase the payback period to an unacceptable level. Diesel backup will likely be required for partial power backup regardless which option is chosen.

## 3.7.2 B.C. Hydro Option

The existing line to Stewart B.C. could be extended from Meziaden Junction. The existing line could supply the power required by the Bronson Slope project, however the capacity of the line would be maximized. This will require extra switchgear for line and surge protection as well as transformers to compensate for line losses etc. During times of inadequate supply or peak demand the diesel generators will be required to subsidize the B.C. Hydro option. Costs for power are estimated at \$0.035 kwhr. The capital cost of the extension would be comparable to the diesel option however with a much lower operating cost. The operation could likely proceed economically with this level of costs.

## 3.7.3 Iskut River Run-of-River Option

A run of river power option is being proposed as a power option for the Bronson Slope project. This option has a higher capital cost than the previous two options but a significantly lower operating cost. The operating cost for the run of river option is in the order of \$0.019/kwhr. Extensive work has been carried out in the area in previous years and this option is feasible. This is the preferred hydro option for the company.

The run of river hydroelectric generating plant would have a capacity of between 16 and 20 MW and be located at the Iskut River canyon. This site is approximately 31 km upstream from the mine location. Power would be delivered to the site via a transmission line located along the Iskut River road corridor. The mine would be the only load served by this facility. At the time of this report, the Company does not intend to sell power to other users.

Further details are provided in the accompanying document, "Iskut Canyon Hydroelectric Plant. Application to the Environmental Assessment Office for a Project Approval Certificate", Section 8.0 of this report.

# 3.8 Project Alternatives

#### Magnetite

Basic metallurgical work has indicated that magnetite will be recoverable from the ore. Preliminary resource grades indicate approximately 500,000 recoverable tons per year are achievable of which 10 - 15% could supply the western Canadian coal industry.

Presently the coal industry is being supplied magnetite from the old Craigmont Mine, however quality of the product is poor. The supply of a superior quality of magnetite is being investigated by the coal industry and it is thought the project will be able to

produce the required product. The coal industry uses magnetite for heavy media separation. The industry consumes between 60 - 80 thousand metric tons per year. Other markets for a high quality magnetite product are also available in the Western U.S. and Australia.

If grades and qualities of the remaining magnetite are adequate the possibility of shipping this product as iron ore does exist. If this were possible approximately 420,000 tonnes of magnetite could be shipped each year to offshore smelters depending on sale prices at port. If the product could not be sold in any given year a plan to stockpile would be established. The storage of magnetite has no significant environmental concerns.

# APPENDIX 5

1995 Computer Model

International Skyline Gold Corporation
Bronson Slope Gold, Copper Porphyry
Mineral Resource Inventory
250 meter Search Radius Model
Corrected Topography & Re-assay of 1988 Drilling
December 21, 1995

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# RESOURCE MODELING CRITERIA 250 meter search radius model

The following resource base utilized an updated claim boundary outline based on survey points located in the field which truly represents the claim group. All 1994 and 1995 drill hole locations were surveyed. Topography was adjusted to fit the available survey data. Reserve polygons which represented areas of undefined material in space were left in the database.

- This resource estimate is a guideline which is to assist in the development of future drill plans, and is also to be used to generate a higher confidence level in the starter pit area. This resource update utilizes all drilling and the re-assay values of all 1988 holes.
- The resource is developed on 10m. benches.
- Resource polygons are generated using a search radius of <u>250m</u>. Polygon grades are developed using drill hole composites contained within the 10m. bench.
- No geological or structural constraints are used to limit polygon search radius. Claim boundaries and topography are the only lithological constraints used.
- Molybdenum values are not included in the gross contained metal values.
- Gold is priced @ \$500.00 Canadian per ounce.
- Silver is priced @ \$6.75 Canadian per ounce.
- Copper is priced @ \$1.25 Canadian per pound.
- This resource utilizes the 1995 assaying of the 1988 holes with the exception of drill hole 944 which
  utilizes the 1994 re-assay results.

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590	10	WST	1217	2.65	238,660	0.041	9,785	0.747	178,279	0.020%	105,231	0.002%	10,523	\$1 37	\$328,104
SUBTOTAL	<del> </del>	WST			238,660	0.041	9.785	0.747	178,279	0.020%	105,231	0.002%	10,523	91.37	#328,104
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580	10	WST	1217	2 65	110,025	0.054	5,941	1 005	110,575	0.030%	72,769	0.004%	9,703	\$1 91	\$210,824
SUBTOTAL		WST			286,660		5,941	0.386	110,575	0.012%		0.002%	9,703	10.74	9210,824
CUMPLATIVE TOTAL	-	WST			642,444	0.024	15,726	0.450	288,854	0.013%	178,000	0.001%	20,228	●0.84	+538,928
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580	10	LGD	1211	2.65	81,136	0.126	10,223	04	32,454	0.150%	268,310	0 005%	8,944	56 25	\$506,914
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SUBTOTAL	+	LGD		··	81,136		10,223		32,454 32,454			0.006%	8,944		9506,914 9506,914
CUMULATIVE TOTAL	+	LGO	1		61,130	0.120	10,223	0.400		0.150%	266,310	0.000 ×		10.23	
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580	-10	HGD	1216	2.65	10,617	0.22	2,336	1.8	19,110	0.270%		0.007%		\$11.37	\$120,756
SUBTOTAL		HGD				0.220		1.800	19,110			0.007%	1,638	911,37	\$120,75
CUMULATIVE TOTAL	-	HGD			10,617	0.220	2,330	1.800	19,110	0.270%	63,196	0.007%	1,638	411.37	e120,75
BENCH TOTAL	1	HGD/LGD			91,752	0.137	12,559	0.582	51,564	0.164%	331,505	0.005%	10,582	\$6.84	<b>6527,87</b>
CVM. BENCH TOTAL	+	HGD/LGD		<del></del>	91,752	L	12,659	L	51,564	0.184%	1	1	10,582	1	4627,67

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				BRC	DNSON SLO				TED TOPO	GRAPHY					
			100.0				Om SEARC					*****	4400	AME:	
19-12-95 9:31 AM	BENCH	POLYGON MATERIAL	HOLE	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	COPPER %	POUNDS	MOLY %	POUNDS	TOME	VALUE
LEVEL 870	neuni	MA I ENAL	10	DENSITY	1 Offices	77.00	GIVINS		Uroma		POUNDS	7	roombs	10100	VALUE
	-														
UBTOTAL		UDF			0										
UMULATIVE TOTAL		UDF	-		56,707										
														\$0.00	\$0
														●0.00	\$0
	<u> </u>													●0.00	\$0
												-		10.00	\$0
	+			<del></del>										\$0.00	\$0 \$0
	+			<del>  </del>	<del></del>							-		00.00	<del>20</del>
570	10	WST	1208	2.65	42,226	0	0	0	0	0 000%	0	0.000%	0		\$0
570	10	WST	1217	2.65	115,443	0.084	9,697	1.748	201,794	0.040%	101,803	0.004%	10,160	\$2.83	\$327,579
UBTOTAL		WST			157,669		9,697		201,794	0.029%		0.003%	10,180	12.08	0327,679
CUMULATIVE TOTAL		WST			800,113	0.032	25,424	0.813	490,648	0.016%	279,803	0.002%	30,406	91.08	\$866,507
	1													●0.00	\$0
														40.00	\$0
												<b>-</b>		\$0.00 \$0.00	\$0 \$0
				<b></b>								<del> </del>		\$0.00	\$0
		<del> </del>	<del> </del>	<b> </b>										●0.00	\$0
	<del></del>	<del> </del>	<del> </del>	<u> </u>										\$0.00	\$0
	+	<del> </del>	<del> </del> -	<del> </del>		-						<del>                                     </del>		\$0.00	\$0
	+		1	1										\$0.00	\$0
570	10	LGD	1211	2.65	95,527	0.13	12,419	0.696	66,487	0 120%	252,721	0 012%	25,272	\$5.55	\$530,217
570	10	red	1216	2.65	36,540	0.169	6,175	0.9	32,886	0.160%	128,891	0.010%	8,056	\$7 32	\$267,647
SUBTOTAL	+	LGD	<del> </del>		132,067	0.141	18,594	0.752	99,373	0.131%	381,612	0.011%	33,328	16.04	1797,805
CUMULATIVE TOTAL		LGD			213,203		28,817		131,827	0.138%		0.009%	42,271	98.12	01,304,779
	-		<del> </del>			-						<del> </del>		10.00	\$0
														●0.00	\$0
			-									-		●0.00	\$0 \$0
		<del> </del>	<del> </del>					<del>  </del>		ļ		<del> </del>		<b>●0.00</b>	\$0 \$0
	+	<del> </del>	+	<del>                                     </del>		<del>                                     </del>		1				<del>                                     </del>		90.00	\$0
		1												10.00	\$0
														90.00	80
			1									-	<b></b>	90.00	\$0
			<b>+</b>			<del> </del>		l						\$0.00 \$0.00	20 20
570	40	HGD	1222	2.65	75, 277	0.543	40,876	1.54	115,927	0.140%	232 342	0.001%	1 660	\$12.92	\$973,212
570		HGD	1218			0.601		3.583				0.001%		\$15.95	\$1,131,425
570		HGD	1215			0.377		18.353	4,395,677			0.006%		\$21.62	\$5,191,098
SUBTOTAL		HGD			385,659	0.451	173,765	12 287	4,765,548	0.325%	2,762,537	0.004	36 466	<b>*18.92</b>	\$7,295,735
CUMULATIVE TOTAL		HGD			396,275			12.074	4,784,656			0.004%	38,104	118.72	97,416,491
BENCH TOTAL	-	HGD/LGD	-		517,726	0.372	192,359	9 307	4,864,918	0.275%	3,144,146	0.000	89 794	915.63	18,093,599
	1											T			
CUM, BENCH TOTAL		HGD/LGD			609,478	0,336	204,918	8,007	4,916,483	0.259%	3,475,654	0.008%	80,376	014,31	\$8,721,270

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							om SEARCH		TED TOPOG						
19-12-95 9:31 AM	BEICH	POLYGON	HOLE	· · · · · ·	METRIC	AU	AU AU	AG		COPPER	COPPER	MOLY	MOLY	OVAL	TOTAL
LEVEL	HEGHT	MATERIAL	ID I	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	*	POUNDS	TONNE	VALUE
540	/ESIII			- J	10.000	*****									
	-														
JETOTAL		UDF			0									+	
UMULATIVE TOTAL		UDF	<u> </u>	l	56,707										
			<b></b> _						<del></del> +	+				●0.00	
	<u> </u>			<b></b>										10.00	
														\$0.00	
	<del></del>			1		$\overline{}$								\$0.00	
			<del> </del>											●0.00	
	<del> </del>	<del></del>	<del></del>					-						0.00	
	<del> </del>	<del> </del>	<del>                                     </del>	-										90.00	
	<del> </del>		1											00.00	-
560	10	WST	1208	2.65	82,754	0.145	11,999	1.035	85,651	0.070%	127,710	0.001%	1,824	\$4 48	\$371,4
		1													
USTOTAL	1	WST			82,754		11,999		85,651	0.070%		0.001%	1,824	64.49	0371,43
UMULATIVE TOTAL		WST			882,867	0.042	37,423	0.653	576,299	0.021%	407,512	0.002%	32,230	81.40	81,237,93
	I													●0.00	
	1											<del>  </del>		90.00	
		<del> </del>										<del>  </del>		\$0.00	
	<del> </del>	<del> </del>												●0.00	
	<del> </del>													\$0.00	
	<del> </del>	<del> </del>	1	1										\$0.00	
	1													●0.00	
560	10	LGD	1217				23,179	2.553	338,153	0.080%		0 007%	20,441	\$5.57	\$739 12 \$520.0
560		LGO	1216			0.193	17,544	0 622	56,542	0 090%		0 009%	18,037 7,966	\$5 72 \$7 27	\$438,4
560		LGD	1209				16,319	2.017	121,463 132,612	0 090%		0.006%	30,587	\$8.38	\$269,1
560	10	LGD	1211	2.65	115,616	0.18	20,811	-1.14/	132,012	0.1807	404,231	30.22	55,557	-	
	<del> </del>		<del></del>	<del> </del>	399,193	0 195	77,854	1.025	648,769	0.116%	1,017,750	0.009%	77,030	\$8.68	02,666,6
UBTOTAL		LGD		<del> </del>	612,395		106,671	1.275	780,596	0.124%	1,667,672		119,301	10.49	13,971,59
CUMULATIVE TOTAL	+	LGO	-	<del> </del>	0.2,555	0,174	100,01								
	+	<del></del>	+		1										
	+	<del></del>	+	1											
	+	<del> </del>	1											●0.00	
	1	1										<b></b>	L	90.00	
														\$0.00	
													<del> </del>	0.00	
						<b></b>						-	<del></del>	<b>●0.00</b>	
			-	<b></b>	<b></b>							+	<del> </del>	●0.00	
	+	ļ			<del> </del>							+		0.00	
	+	<del> </del>	+	+	+	<del> </del>				<u> </u>	<del> </del>	+	<del> </del>	10.00	
	+	+	+	+	<del> </del>	1	<del> </del>				1	1		90.00	
	1		+-	1	1	1								●0.00	
560	10	HGD	122	2 2 65		0.538			130,102	0.150%		3 0 001%			\$1,097,
560	10	HGD	121			0.666			742,608	0.210%		1 0.003%			\$2,256,
560	1	OHGD	121	5 2.65	273,076	0.894	244,130	2.24	611,691	0.280%	1,685,68	2 0.004%	24,081	\$22.57	\$6,167,
	+	1			400000	0 33-			1 461 451	0.2202	3.540.55	0.000		1 416 45	en 834
SUBTOTAL	+	HGD		-	483,587			3.070	1,484,401	0.239%		0.003%		119.69	\$9,521,
CUMULATIVE TOTAL	+	HGD		<del></del>	879,863	0.025	548,728	7.125	6,269,056	0.277%	0,3/0,41	7 0.004%	12,42	•19.25	116,938,1
BENCH TOTAL		HGDAGD			882,780	0.511	451,482	2.416	2,133,170	0.183%	3,567,43	5 0 0000	111 341	13.81	412,188,4
BENCH TOTAL	+	AGD/LGD	+	-	802,780	0.011	701,482	4.310	2,133,170	0.10376	3,507,43	U.000X	1,1,35,	7,3.01	412,100,
		1	_ i	I	L	L	I	l			1		1	1	

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19-12-95 9:31 AM LEVEL	BENCH	POLYGON	HOLE	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER	COPPER	MOLY X	MOLY	TOME	TOTAL
550	1.00		1			77.00	7	1,7							
550	10	UDF		2.65	7,513	0	0	0	0	0.000%	0	0 000%	0	\$0.00	
			<del>  </del>		7.7.0										
UBTOTAL UMULATIVE TOTAL		UDF	<del>}</del>		7,513 64,220	<del></del>									
MOCK HAE LOTYE	<del> </del>	00-	1		04,220										
	1													90.00	
														●0.00	
			1											●0.00 ●0.00	
	<del> </del>													\$0.00	
	<del> </del>		1											00.00	
														90.00	
	<del> </del>	1000	4246	2.55	133,402	0 140	19,877	0.245	32,683	0.050%	147 050	0.009%	26,469	\$3.83	\$510,6
550	10	WST	1216	2.65	133,402	J. 149	19,077	0.2-3	32,003	0.03378	147,000	3.000 A	20,400		
UBTOTAL		WST	1		133,402	0.149	19,877	0.245	32,683	0.050%	147,060		26,469	●3.83	<b>#510,62</b>
UMULATIVE TOTAL		WST			1,016,269		57,300	0.599	608,982	0.025%	554,562	0.003%	58,699	91.72	\$1,748,5¢
														●0.00	
														10.00	
	<del> </del>	<del>                                     </del>	<del></del>					<del></del>						10.00	
	+	<del> </del>	+											10.00	
	<del>                                     </del>	<del> </del>											ļ	00.00	
														0.00	
		ļ												●0.00	
550	+	LGD	1208	2.65	142,270	0.197	28,027	0 602	85,646	0 120%	376,381	0.003%		\$6 60	\$939,9
550		LGD	1211		138,602	0.176	24,394	1.338	185,450			0 010%			\$1,005,9
550		LGD	1217	2.65	139,728	0.237	33,115	1.848	258,217	0 180%	554,483	0.014%	43,120	\$ \$9 17	\$1,282,4
		<del> </del>			420,600	0.303	85,537	1.258	529,313	0.150%	1,389,213	0.009%	83,093	97.68	03,228,3
UBTOTAL		LGD	<del></del>	<del> </del>	1,032,995			1.268	1,309,909		3,056,884				\$7,199,9
	1														
														♦0.00	
		<del> </del>		<del> </del>	<del> </del>	<b></b>		<del> </del>		<del>                                     </del>	<del> </del>			00.00	
	<del> </del>			·										\$0.00	
							· · ·					ļ	ļ—	00.00	
		<del></del>				<u> </u>		<del> </del>		<del> </del>	<del> </del>	<del></del>		90.00 90.00	
		<del></del>		<del> </del>	<del> </del>	<del> </del>		<del> </del>		<del> </del>	<del> </del>	1	<del> </del>	10.00	
		<del></del>	-	<del> </del>		1		<u> </u>						\$0.00	
														00.00	
								1	444.644	0 4704	343.66	0.000	11,07	90.00 \$13.77	\$1,153,
550		0 HGD	1227			0.542			144,619 342,005			0.006% 0.003%			\$1,133,
550		0 HGD 0 HGD	1209			0.616						8 0.0119		6 \$21.35	\$3,116,
550 550		0 HGD	121		283,53	0.92	260,85	3.181				2 0.0179		6 \$23.20	\$8,580
SUBTOTAL		HGD		-	616,49	0.819	805 126	3.269	2,015,236	0.241%	3,276,94	0.0129	159.55	0 \$20.54	\$12,661,
CUMULATIVE TOTAL		HGD		<del>                                     </del>	1,496.35	0.705	1,054,85	5.536	8,284,292					2 019.78	\$29,000,°
		<u> </u>													
SENCH TOTAL		HGD/LGD			1,037,09	0.670	590,661	2.454	2,544,549	0.204%	4,666,15	9 0.0119	242,64	3 015.32	\$15,890,E
JUM. BENCH TOTAL		HGD/LGD			2,529,341	1		1	9,594,20		11,709,24		434,30		936,800

							Om SEARC		CTED TOPO						
19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU AU	AG	AG	COPPER	COPPER	MOLY	MOLY	•VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID.	DENSITY	TONNES	PPM	GRAM8	PPM	GRAMS	*	POUNDS	*	POUNDS	TONNE	VALUE
540															
540		UDF		2.65	18,891	0	0	0	0	0.000%		0.000%		\$0.00	
340	10	00+	-	2.63	10,091			- 0		0.000%		0.000%		30.00	
WBTOTAL	-	UDF	1		18,891										
UMULATIVE TOTAL		UDF			83,111										
														\$0.00	\$0
	<del> </del>		<del> </del>	<del></del>										90.00	<b>\$0</b>
			<del> </del>											●0.00	\$0
														●0.00	80
														●0.00	\$0
														●0.00	\$0
	ļ		1212		400 000	-				0.0000		A 2000		40.00	80
540	10	WST	1210	2.65	132,320	0	0	0	0	0.000%		0.000%	0	\$0.00	
SUBTOTAL		WST			132,320	0.000	0	0.000	0	0.000%		0.000%	0	0.00	•0
CUMULATIVE TOTAL		WST		<del> </del>	1,148,589		57,300		608,982	0.022%	554,562		58,699	91.52	11,748,560
COMOCHIVE TOTAL					.,,	0.000		0.000	330,333			5.050,0	33,333		
														10.00	\$0
														\$0.00	20
						-								●0.00	\$0 \$0
	<del> </del>	<b></b>	<del> </del>											\$0.00	\$0
	<del> </del>		<del> </del>											10.00	\$0
	+		<del> </del>											\$0.00	\$0
														10.00	\$0
														•0.00	\$0
			<del></del>	L		-								0.00	\$0
	<del> </del>	ļ	<del> </del>	<u> </u>				<del>                                     </del>						●0.00	\$0
CURTOTAL	<del> </del>	1.00	<del> </del>			0.000	0	0.000		0.000%		0.000%	0	0.00	•0
SUBTOTAL CUMULATIVE TOTAL		LGD	+		1,032,995		192,208		1,309,909	0.134%	3,056,884		202,394	#6.97	17,199,983
COMOCATIVE TOTAL	+	100	<del>                                     </del>		1,002,000	00	,,,,,,,,	1	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		-11	71			
	<del>                                     </del>	<del> </del>													
	1		1												
						Ι								\$0.00	\$0
			<del></del>	<u> </u>	ļ	<del> </del>								90.00	\$0
		<b>_</b>	+	<b></b>	ļ	┼						<del></del>		<b>●0.00</b>	\$0 \$0
		<del> </del>		<del> </del>		-		<del> </del>						\$0.00	\$0
		<del></del>			· · ·	<del> </del>						-		#0.00	\$0
540	10	HGD	1216	2.65	118,625	0 533	63,227	1.486	176,277	0 120%	313,828	0 014%	36,613		\$1,447,759
540		HGD	1222			0.502	42,072		147,839			0.002%	3,695		\$1,032,389
540		HGD	1215			0.576	141,048		661,163			0.005%			\$3,490,226
540 540		HGD	1206			0.687	131,852 138,046		283,665 496,846	0.240%		0.004%			\$3,451,958
540		HGD	1217			0.578	84,001		533,365		1,121,399	0.006%	19,891	\$19 33 \$19 73	\$2,909,258 \$2,869,831
540		HGD	121			1.093		1.811				0.005%		\$21 55	\$3,503,226
540		HGD	1209		153,97	0.858	132,112	3.387	521,521		1,120,222			\$23 62	\$3,639,380
			1	L		1									
SUBTOTAL		HGD			1,261,431		909,988	2.489	3,114,991	0.204%				917.86	\$22,347,026
CUMULATIVE TOTAL		HGD			2,747,781	0.715	1,964,840	4.149	11,399,293	0.236%	14,275,652	0.007%	422,253	418.91	451,847,126
BENCH TOTAL	<del></del>	HODEGO	+	<del> </del>	1 251 42	1	000 000	1 2 4 2 2	3.114.000	0.3346		0.0000	162.65	<del>  </del>	
BENCH TOTAL		HGD/LGD			1,251,43	0.727	909,989	2.489	3,114,991	0.204%	8,823,289	0.007%	190,281	\$17.86	\$22,347,026
CUM. BENCH TOTAL		HGD/LGD	1		l	L	I.	1				1	1	. 1	

						25	om SEARCE	H RADII	JS						
19-12-95 9:31 AM	BENCH	POLYGON	HOLE	T	METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	AVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TOMNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	*	POUNDS	TONNE	VALUE
520															
			1												
SUBTOTAL		UDF			0										
CUMBRATIVE TOTAL		UDF			83,213						·			- · - · · -	
			1											•0.00	\$0
														\$0.00	\$0
														●0.00	\$0
														●0.00	\$0
														●0.00	\$0 \$0
	<u> </u>			<b> </b>										●0.00	
														●0.00	\$0 \$0
		<b></b>		<b></b>										\$0.00	\$0
				<b></b>										\$0.00	
	·	-	·			0.000		0.000		0.000%		0.000%	0	10.00	•0
SUBTOTAL		WST		h	1,272,491	0.000	57,300	0.000	608,982	0.020%	554,582		58,699	\$1,37	91,748,560
CUMULATIVE TOTAL		WST		<del> </del>	1,272,491	0.045	67,300	0.7/3	000,902	0.020%	004,502	0.002 /5	00,033	<u> </u>	V1,740,000
	<del> </del>		<del> </del>	<del> </del>								-		\$0.00	\$0
	<del> </del>	<del> </del>	<del> </del>	<del>  </del>				<del></del>						10.00	\$0
	<del> </del>	<del> </del>	<del> </del>	<del> </del>										♦0.00	\$0
	<del> </del>	1	+	1										\$0.00	\$4
	+			1										10.00	\$0
				1										\$0.00	80
														10.00	ä
520		rco	1212		191,028		27,699	0.854	163,138	0 100%		0.000%	33,692	\$5 27	\$1,007,722
520		LGD	1219		146,534		19,762	1 169	171,298	0 110%		0 011%	35,536		\$799,976
520		LGD	1211		186,565 115,176		48,694 34,438	0.757 0.875	141,230 100,779	0.170% 0.150%		0.017%	69,922 55,862		\$1,686,087 \$1,052,031
520	<del></del>	LGU	1210	2.65	113,176	0.299	34,436	0.673	100,779	0.130%	360,860	0.022	30,502	35 13	31,002,00
SUBTOTAL	+	LGO	<del> </del>	1	639,303	0.204	130,612	0.902	576,445	0.132%	1,858,600	0.014%	195,012	97.11	94,547,816
CUMULATIVE TOTAL	1	LGD	<del> </del>	·	2,279,762		508,572		2,699,273		6,253,147		451,885		\$16,586,114
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	1	1				L						ļ		\$0.00	X X
				<u> </u>								<del>                                     </del>	<b> </b>	0.00	
	<b></b> _	ļ		L								<del></del>		\$0.00	<del>\$</del>
	·	1			250.005	0.406	120 614	1 000	405.761	0 120%	687,007	0.001%	5,725		\$3,032,52
520		HGD	1215		259,685 153,122		128,544 57,727		485,351 312,828	0.220%		0 004%	13,503		\$1,925,40
520 520		HGD	1217		209,456		94,884		271,665	0.210%	969,720		9,235		\$2,797,64
520		HGD	1210		213,717		109,851		147,251	0.180%	848,097		9,423		\$2,858,91
520		HGD	1222			0.783	68 104	2.019	175,610		479,388	0 002%	3,835	\$19 91	\$1,732,98
520	1(	HGD	1218	2 65	160,893	0 63	101,363	5.714	919,345	0.340%		0 002%	7,094	\$20 74	
520	10	HGD	1206			1.173	203,885	2.703	469,823	0 320%		0 009%	34,486	\$28 26	\$4,914,62
SUBTOTAL		HGD			1,267,667			2.212	2,781,872		6,159,118			610.38	
CUMULATIVE TOTAL	-	HGD	-		4,918,168	0.683	3,367,562	3,435	16,895,997	0.238%	25,792,775	0.000%	680,695	118.29	109,947,52
BENCH TOTAL		HGD/LGD			1,896,971	0.472	894,970	1.770	3,358,318	0.192%	8,015,719	0.007%	278,315	#13.20	025,149,60
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						26	Om SEARC	H RADI	US						
19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	IVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	10	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS_	*	POUNDS	*	POUNDS	TONNE	VALUE
510															
				<del></del>											
UBTOTAL		UDF			0										
UMULATIVE TOTAL	<del> </del>	UOF			83,213										
														10.00	
														●0.00	
				l										00.00	
	·			·										●0.00 ●0.00	
	<del> </del>		<del></del>									-		10.00	
														\$0.00	
														\$0.00	
510	10	WST	1212	2.65	261,508	0.078	20,397	0 258	67,469	0.060%	345,913	0 007%	40,356	\$2.96	\$775,2
UBTOTAL		WST			261,506	0.078	20,397	0.258	67,469	0.060%	345,913	0.007%	40,356	\$2.96	9775,2
UMULATIVE TOTAL		WST			1,533,996	0.051	77,697	0.441	676,451	0.027%	900,475	0.003%	99,056	91.05	12,523,7
	<del> </del>		<del>}</del>	<del>  </del>										90.00	
	<del>                                     </del>		<del>                                     </del>	t				-						90.00	
														10.00	
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	L		<b></b>	<u> </u>										0.00	
				1										0.00	
	<del> </del>	ļ	ļ	<del></del>			<del></del>					<del>  </del>		<b>●0.00</b>	
510	100	LGD	1211	2.65	205,707	0.252	51,838	0 838	172,382	0.140%	634 907	0 016%	72,561	\$8.09	\$1,665
	<del>  "</del>	100	1211	1.00	200,707	0.25	31,550	- 5000	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	0,1,0,0					
SUBTOTAL		LGD			205,707		61,838		172,382	0.140%	634,907		72,561	18.09	1,665,1
UMULATIVE TOTAL		LGD	-		2,485,469	0.225	560,410	1.155	2,871,655	0.126%	0,888,054	0.010%	524,446	97.34	<b>118,253,2</b>
														€0.00	
		<del>}</del>	<del> </del>											\$0.00 \$0.00	
	<del> </del>	<del> </del>	<del> </del>	i		-						<del></del>		\$0.00	
														90.00	
510		HGD	1217		138,927	0.389	54,043		185,329			0 001%	3,063		\$1,484,0
510 510		HGD	1219		237,510 268,394		75,528 178,750		752,671 811,892		1,466,137	0.002%	57,598 11,834		\$3,212, \$4,162,
510		HGD	1222		101,560		68,147					0.002%	4,478		\$1,798,
510		HGD	1216		130,104		104,344		93,155		602,345	0.004%	11,473		\$2,451
510		HGD	1208		173,982		120,221		502,285		997,264	0.008%	30,685		\$3,290,
510		HGD	1218		163,923		146,875		649,298		1,300,994	0 003%	10,842	\$25 18	\$4,130
510		HGD	1210	2.65	258,479	1 36	351,532	3 753		0 560%	3, 191, 154	0.006%	34,191	\$38 11	\$9,854
510	10	HGD	1209	2.65	248,741	1.931	480,319	11.668	2,902,309	0.550%	3,016,086	0.047%	257,738	\$48 73	\$12,132
UBTOTAL		HGD	-	-	1,721,621	0.918	1,579,759	4.069	7,006,048	0.328%	12,458,328	0.011%	421,902	924.70	\$42,516
UMULATIVE TOTAL		HGD			6,639,789		4,937,311	3.600	23,902,044	0.261%					1132,464
ENCH TOTAL	<del>                                     </del>	HGD/LGD	<del> </del> -	<del> </del>	1,927,326	0.847	1,631,597	3.726	7,178,430	0.308%	13,093,234	0.012%	494,463	022.92	\$44,181,0
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				BRO	ONSON SLO				CTED TOPO	GRAPHY					
10-12-96 9:31 AM	BENCH	POLYGON	HOLE		METRIC	250 AU	Om SEARCE	H RADII	AG	COPPER	COPPER	MOLY	MOLY	OVAL	TOTAL
LEVEL	HEGHT	MATERIAL	D D	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	*	POUNDS	TONNE	VALUE
	MEGITI	MA I ENGAL	<del>                                     </del>	DEMOIT	TORRES	****	OWNED.	- Trans	unama		rounds		romos	TOIME	AUFOR
500															
SUBTOTAL	<del></del>	UDF	-		0										
CUMULATIVE TOTAL		UDF			83,213										
	<del> </del>	ļ												10.00	\$0
	<del> </del>		<del> </del>	-				$\overline{}$						10.00	\$0
	<del>                                     </del>					-								10.00	\$0
														●0.00	\$0
	1													\$0.00	\$0
														\$0.00	\$0
500	10	WST	944	2.65	127,457	0	0	0	0			0 000%	0	\$0.00	\$0
500	10	WST	945		71,539	0	0	0	0			0.000%	0		\$0
500		WST	1212	2.65	336,490	0.146	49,127	0.682	229,486	0.060%	445,099	0.006%	44,510	\$4.15	\$1,396,630
SUBTOTAL	<del> </del>	WST	+		535,486	0.092	49,127	0.429	229,486	0.038%	445,099	0.004%	44,510	92.61	1,396,830
CUMULATIVE TOTAL	<del> </del>	WST	1	1	2,069,483		126,825	0.438	905,936	0.029%	1,345,674	0.003%	143,566	\$1.89	93,920,616
COMOCATIVE YOUR	1	1	1												
	1													40.00	\$0
	<del>                                     </del>		1	1										\$0.00	\$0
	1	1	1											\$0.00	\$0
	<del></del>													●0.00	\$0
	<del>                                     </del>		1											90.00	\$0
	1													\$0.00	\$0
														<b>\$0.00</b>	\$0
														♦0.00	80
														●0.00	\$0
			1											●0.00	\$0
														\$0.00	80
SUBTOTAL	1	LGD			0	0.000		0.000	0	0.000%	0	0.000%	0	\$0.00	•0
CUMULATIVE TOTAL		LGD			2,485,469	0.225	560,410	1.155	2,871,655	0.126%	0,888,054	0.010%	524,446	97.34	<b>018,253,227</b>
	<del> </del>		+												
														\$0.00	\$0
	<del></del>	<del> </del>		<del> </del>										\$0.00	
	<del></del>					-								♦0.00	\$0
		<del></del>		<del>                                     </del>	ļ							<del> </del>		80.00	
	·	tuen .	1000		14.004	0.343	47,423	2.501	380,147	0 180%	AM3 177	0.012%	40,212		\$1,600,172
500		HGO	1219		151,998		75,033		455,321			0.004%		\$13.58	\$3,024,719
500		HGD	1211		222,651		47,974		115,380			0.001%		\$15.79	\$1,370,564
500		HGD	1217			0.553	107,816		435,664			0.002%		\$17.69	\$2,995,603
500		HGD	1218			0.749	107,681		124,502			0.006%		\$18.02	\$2,590,892
500		HGD	1208		171,721		132,225					0.015%	56,787		\$3,484,219
500		HGD	1210			0.736						0.002%	13,817		\$8,468,114
500		HGO	1215		277,309		312,528					0.005%	30,568		\$7,529,548
500		HGD	1209			0 954			1,343,654			0 003%	16,921		\$7,040,331
500		HGD	1222			2.751	460,379					0.004%		\$51 04	\$8,543,553
SUBTOTAL		HOD	-}	·	1,959,999	0.901	1,765,769	3.008	6,012,829	0.278%	11,945,239	0.005	221.089	922.7B	\$44,647,716
CUMULATIVE TOTAL		HGD					4,703,070								6177,112,002
BENCH TOTAL		HGD/LGD	1		1,959,999										
					1,000,000	0,501	1,705,709	3,066	6,012,629	0.276%	11,945,238	0.000%	221,089	922.78	144,847,716
CUM, BENCH TOTAL		HGD/LGO			11,005,256	0.655	7,263,480	2.958	32,786,226	0.234%	57,084,395	0.000%	1,848,132	117.62	#195,365,228

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19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	AVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	10	DENSITY	TOMNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	%	POUNDS	TONNE	VALUE
490															
JBTOTAL		UDF			0										
JMULATIVE TOTAL		UDF			83,213										
														90.00	
														\$0.00 \$0.00	
	<del> </del>	<del></del>		<del></del>										0.00	
	<del> </del>													€0.00	
	<del>                                     </del>		1											●0.00	
490	10	WST	1221	2.65	182,126	0	0	0	0	0 000%	0		0	\$0 00	
490		WST	1220	2.65	51,674	0	0	Ō	0	0.000%	Ó	0 000%	0	\$0 00	
490	10	WST	1212	2.65	346,731	0 129	44,728	0.734	254,500	0.070%	535,086	0.009%	68,797	\$4 16	\$1,444,0
JBTOTAL	1	WST	<del> </del>	<del> </del>	580,531	0.077	44,728	0.43B	254,500	0.042%	535,086	0.005%	68,797	12.49	61,444,0
UMULATIVE TOTAL		wst			2,650,013		171,563		1,160,437	0.032%	1,880,660		212,363	92.02	15,364,6
														\$0.00	
						-								90.00	
	<del>  </del>	ļ	<del> </del>	ļ										\$0.00 \$0.00	
	<b>—</b>	<del> </del>												90.00	
490	+	LGO	946	2.65	76,915	n 103	14,845	0.839	64,532	0.160%	271 311	0 001%	1,696	\$7 69	\$592,0
490		LGD	961	2.65		0.193	1,109		4,614	0 160%	20,267		253	57 69	\$44.1
490		LGD	1216		87,548		35,632	0.555	48,589	0.080%		0.002%	3,860	\$8 87	\$776.6
490		LGO	962		54,126	0 284	15,372		39, 295	0.160%		0.003%	3,580	\$9 13	\$494,4
490		LGD	1210		284,882		122,214	0 889	253,260	0.100%	628,056	0 002%	12,561	\$9 84	\$2,805,9
490	10	LGD	1209	2.65	251,917	0.327	82,377	1.437	362,005	0.160%	888,611	0.001%	5,554	\$9.98	\$2,515,0
UBTOTAL	+	LGD		1	751,134	0.357	271,549	1.015	772,295	0.128%	2,153,576	0.002%	27,504	99.50	<b>#7,228,3</b>
UMULATIVE TOTAL		reo			3,246,603		831,959		3,643,950		9,041,630		551,950	47.85	025,401,0
	<u> </u>													●0.00	
														\$0.00	
		<del> </del>										ļ	<del></del>	\$0.00	
		<del> </del>	<del> </del>	<del>                                     </del>				<del> </del>				<del> </del>		\$0.00	
490	10	HGD	1219	2.65	147,543	0.312	46,033	1.922	283,577	0.190%	618,024	0.010%	32,528		\$1,575,1
490		HGD	945			0.515	29,564		145,296		202,495	0 008%	10,125		\$760,4
490	10	HGD	944			0.528	18,811		69,509	0 180%		0.006%		\$13.87	\$494,
490		HGD	1208	2.65	171,690		89,450		496,355			0.004%		\$13.96	\$2,399,
490		HGD	1211		231,395		68,956		242,271	0 400%		0.025%			\$3,712,
490		HGD	1217		104,605				185,569			0.001%			\$1,922,
490		HGD	1222		175,587	0 9/3	170,847	18.142	3,185,507	0.210%	812,917	0.005%	19,355		\$4,464,
490 490		HGD HGD	1218			1.049	185,021 407,492	4.929 7.5		0.480%		0.007%	69,153	\$31.16 \$37.83	\$5,499, \$10,794,
UBTOTAL		HGD			1,385,391	0.792	1,097,348	5 497	7,616,144	0.322%	9,841,985	0.010%	308 074	<b>#22.83</b>	\$31,623,
CUMULATIVE TOTAL		HGD	1		9,985,178								1,631,760		1208,735,3
SENCH TOTAL		HGDAGD			2,146,525	0.638	1,368,896	3,906	8,388,439	0.253%	11,995,561	0.007%	335,578	918,10	\$38,861,7
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19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	OVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	10	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	*	POUNDS	TONNE	VALUE
480															
480	10	UDF		2.65	14,115	0	0	0	0	0 000%	0	0.000%	0	\$0.00	
		1000													
CUMULATIVE TOTAL	<del></del>	UDF	<del>  </del>		14,115 97,328										
OMOCATIVE TOTAL	<del> </del>	00-	<del>  </del>		37,320										
			1											10.00	\$0
														●0.00	\$0
														•0.00	\$0
			<del>                                     </del>											●0.00	\$0
			<del>├</del>											0.00	50
480	10	WST	1220	2 65	112,723	0 032	3,607	0 113	12,738	0 020%	49,702	0.001%	2,485	\$1 09	\$122,932
480		WST	1212	2.65	400,133		35,212	0.39	156,052	0 080%	705,712	0 012%	105,857	\$3 70	\$1,482,675
480		WST	1221	2.65	225,371		33,130	0.553	124,630	0.070%	347,801	0.001%	4,969	\$4,41	\$994,693
						I									
SUBTOTAL		WST	1		730,226		71,948	0.397	293,420	0.068%	1,103,215		113,311	93.52	\$2,600,501
CUMULATIVE TOTAL		wst	1		3,388,240	0.072	243,501	0.429	1,453,850	0.040%	2,983,876	0.004%	325,073	•2.36	47,985,195
			<del>}</del>							·				\$0.00	\$0
			1											10.00	\$0
	<del></del>	<del> </del>	<del>  </del>					-						0.00	\$0
	<del> </del>	<del> </del>	1											€0.00	\$0
	<del> </del>	<del></del>	11											€0.00	\$0
	<del>                                     </del>	<del> </del>	-											90,00	\$0
480	10	LGD	961	2 65	23,440	0.147	3,446	1,129	26,464	0 160%		0 002%	1,034	\$7 02	\$164,583
480	10	LGD	1222	2.65	182,421	0.258	47,065	0.674	122,952	0.100%		0.002%	8,043	\$7.05	\$1,286,556
480		LGD	962	2.65	59,972		10,615		26,628			0.002%	2,644	\$7.35	\$440,978
480		red	946		93,959		23,490		85,973			0.002%	4,143 127,422	\$8.63 \$9.57	\$810,919 \$2,404,730
460	10	LGO	1211	2.65	251,295	0.327	82,173	0.807	202,795	0.150%	831,013	0.023%	141,422		
SUBTOTAL	<del> </del>	LGD	+		611,087	0.273	166,789	0.761	464,811	0.138%	1,858,842	0.011%	143,286	18.36	15,107,770
CUMULATIVE TOTAL	<del>                                     </del>	LGD	1		3,857,690		998,747		4,108,761		10,900,472				030,589,375
	1														
														10.00	S
														10.00	\$4
														\$0.00	<b>\$</b>
			1310	3.06	303 730	0.452	438 348	0011	269 470	0 1100		0.005	31 370	90.00	\$2,079.13
480 480		HGD	1210 945		283,726 70,388		128,245 24,636		258,476 208,447			0.005%			\$2,979,120 \$751,91
480		HGD	1209		258,898		119,870		381,618			0.001%	5,708		\$3,010,310
480		HGD	1219		153,329		65,472		327,051			0.012%	40,564		\$1,969,810
480		HGD	944				15,348		180,257			0.007%			\$460,71
480		HGD	1217		121,938		81,942		154,129	0.150%	403,239	0.001%	2,688	\$15.21	\$1,855,58
480	10	HGD	1208	2 65	162,887	0.611	99,524		598,609			0.005%	17,955		\$2,629,79
480	10	HGD	1218			0.578	108,036		479,809			0.004%	16,483		ສຸກນຸນ
480		HGD	1215			0.746		2.062	179,121			0 003%			\$1,655,97
480	10	HGD	1215	2.65	295,601	1.448	428,031	3.781	1,117,669	0.240%	1,564,053	0.011%	71,686	\$3071	\$9,063,68
SUBTOTAL	1	HGD	1		1,653,840									\$18.71	\$27,630,47 •236,365,86
CUMULATIVE TOTAL		HGD			11,639,018	0.748	0,936,323	3.008	41,413,902	0.261%	64,846,981	0.00/7	1,530,200	720.31	7434,345,64
BENCH TOTAL		HGD/LGD			2,264,927	0.575	1,302,693	1.920	4,347,996	0.174%	8,667,503	0.007%	346,736	814.45	032,738,24
	1	1	1	1	1	1	I	1		1	1	1	1		

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						26	Om SEARC	H RADII	JS						
19-12-96 9:31 AM LEVEL	BENCH	POLYGON MATERIAL	HOLE	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER	COPPER	MOLY %	POUNDS	TONNE	TOTAL
470	742-0771	- MANUAL			, 0, 1, 1, 2										
470	10	UDF	1213	2.65	74,342	0.196	14,571	0.165	12,266	0.000%	0	0.000%	0	\$3 19	<del></del>
				<b></b>	34 343							<del>-</del>			
UBTOTAL	<del> </del>	UDF	<del> </del>	<del> </del>	74,342 171,670										
OMULATIVE TOTAL	<del> </del>	007	1	<del> </del>	171,070										
		<del></del>	1	t										\$0.00	
														●0.00	
														\$0.00	
			<del> </del>									<del>  </del>		\$0.00 \$0.00	
	<b></b>		<del> </del>									<del>  </del>		\$0.00	
			+	1		-						-		\$0.00	
470	10	WST	1212	2.65	454,586	0.111	50,459	0.262	119,102	0.050%		0.009%	90,197	\$3.22	\$1,463,9
470		WST	1221		259,117		36,276	0.538	139,405	0.060%	342,753	0.000%	0	\$4.02	\$1,042,4
							a		750 757	0.0545	042.000	0.0000	00.107		42 504 T
UBTOTAL		WST	<del> </del>		713,704 4,101,943		86,735 330,237	0.362	258,507 1,712,363	0.054%	3,827,723	0.006%	90,197 415,870		92,508,30 910,471,50
UMULATIVE TOTAL	+	1	<del> </del>	<del> </del>	4,101,343	0.001	330,237	0.4.7	1,712,505	0,042.6	5,027,725	0.0007			
	1					1								0.00	
		1				l l					· · · <del> · ·</del> · ·			●0.00 ●0.00	
		<del> </del>		<del> </del>				<del>                                     </del>						90.00	
	<del></del>	<del> </del>		<del> </del>				<del>                                     </del>						\$0.00	
	<del> </del>	<del> </del>		1										●0.00	
470	10	LGD	1217				35,908		157,466	0 080%	246,427		3,080		\$920,0
470		LGD	1222				49,490		89,082	0.110%	452,896		6,234		\$1,381,5
470		LGD	961			0 187	7,446		22,935 98,330			0 002%	1,756 3,030		\$300,3 \$672,6
470		LGD	962		<del></del>	0.315	21,645 10,527	1 619	49,980			0 004%	2,722		\$307,6
470	"	rod		' <sup>2</sup> '''		1.03-1	10,327	, , , ,	45,510	0.50%	102,000	0 00 1.75		1555.4	
SUBTOTAL	+	LGO	+	<del>                                     </del>	465,879	0.268	125,016	0.897	417,793	0.115%	1,184,244	0.002%	18,823	17.69	13,582,4
CUMULATIVE TOTAL	+	LGD		<b>+</b>	4,323,509				4,526,555				714,059	\$7.90	\$34,171,8
			-												
			-			-								\$0.00	
														0.00	
														●0.00	<b>2000</b>
470		0 HGD	121			3 0.361	71,317					5 0.001%			\$2,043, \$3,028,
470		O HGD	121						365,329 355,366			1 0.004%			\$947
470 470		0 HGD	120									8 0 002%			\$3,637
470		0 HGD	120			3 0.541								2 \$14 29	\$3,812,
470	1	0 HGD	120	8 2.6	154,38	2 0 571	88, 152	2.255	348,132	0.170%					\$2,217,
470	1	0 HGD	122									9 0.016%			\$3,549
470		0 HGD	94									1 0.002%			\$2,142 \$3,606
470 470		0 HGD	121			7 0.731 9 1.229						2 0 0011%			\$3,606, \$9,100
470		0 HGD	121			2 1.777						6 0.016%			\$4,047
SUBTOTAL		HGD			2,098,67									0 818.17	\$38,134,
CUMULATIVE TOTAL		HGD		+	13,737,69	B   0.757	10,395,357	3.405	46,783,426	0.256%	77,640,220	0.007%	2,140,74	119.90	4274,499,1
BENCH TOTAL		HGD/LGD			2,564,55	0.618	1,584,051	2.257	5,787,317	0.212%	11,977,47	7 0.006%	324,36	2 816.27	941,716,9
CUM, BENCH TOTAL		HGD/LGD	-	<del></del>			11,619,121	1	<b></b>		89.724.936	<del></del>		1	#308,671,

									TED TOPO						
10 10 00 0 01 111		201 7000	Lucie		4457510		Om SEARCI			COCOCO	COMME	4404.9	MOLY	IVAL	TOTAL
19-12-96 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG.	AG	COPPER	COPPER	MOLY	POUNDS	TONNE	VALUE
LEVEL 460	HEGHT	MATERIAL	D	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	_*	rounus	10100	ANTOR
460	10	UDF	<del>├</del>	2.65	23,811	0	- 0	0	0	0 000%	0	0 000%	0	\$0.00	
BTOTAL		UDF			23,811										
UMULATIVE TOTAL		UDF			195,481										
			┼┼					+						0.00	\$
														●0.00	
														0.00	
														\$0.00	
	<del> </del>		1											00.00	•
460	10	WST	1213	2 65	204,855	0.133	27,246	0 993	203,421	0 000%	0	0 001%	4,516	\$2 35	\$482,86
460		WST	1221	2.65	292,513		31,299	0.529	154,740	0 040%	257,952		6,449	\$2.94	\$859,77
460		WST	1212	2 65	504,640		94,368	0 525	264,936	0 060%	667,523	0.008%	89,003	\$4.77	\$2,410,12
			<del>  </del>		1,002,008	0.153	152,912	0.622	623,096	0.042%	925,475	0.005%	99,968	13.75	03,752,75
UBTOTAL		WST	+		5,103,951		483,149		2,335,459	0.042%	4,753,199		515,838	\$2.79	014,224,33
UMULATIVE TOTAL	+	14431			0,103,331	0.033		0,430	2,500,400	0,010,0	11,000				
	<del>                                     </del>	<del> </del>	1											●0.00	
														●0.00	
														00.00	
										l				\$0.00	
										ļ				♦0.00	
										l			2 402	10.00	
460		LGD	1217	2.65	157,996		35,391	0.991	156,574	0.110%	383,154		3,483	\$6 85 \$8 46	\$1,082,47 \$336,86
460		LGD	944	2.65		0 316	12,572	1.612	64,136		96,485		3,509 1,546	\$8 58	\$601,7
460		LGD	962			0 245	17,177	1.062	74,458 53,335		247,311 174,038		3,263	\$8 92	\$440,3
460		LGO	961	2 65	49,339		13,124 68,275	1.081	160,314			0.002%	8,316		\$1,806,8
460	1 10	LGO	1222	2.65	188,605	0.362	00,2/3	0 83	100,314	0.130%	340,343	0.002.70	0,5.0		0.150010
SUBTOTAL	+	LGD	+	-	505,838	0.290	146,540	1.006	508,818	0.129%	1,441,531	0.002%	20,117	18.44	14,270,2
CUMULATIVE TOTAL		red			4,829,407		1,270,304	1,043	8,035,373	0.127%	13,520,247	0.007%	734,176	<b>●7.96</b>	<b>#38,442,0</b> 3
				ļ — — — — — — — — — — — — — — — — — — —											
													<del> ,</del>	€0.00	
	+	+	-			<del> </del>								\$0.00	
	<del> </del>													\$0.00	
460	10	HGD	1210	2.65	278,230	0.459	127,708	1.314	365,595		613,392		18,402		\$2,900,7
460		HGD	1218						413,169			0.001%	4,587		\$2,460,9
460		HGD	1211					2.39	680,035			0.013%	81,548		\$3,441,4
460		HGD	1208						227,624			0 006%	19,577		\$1,794,6 \$1,453,6
460		HGD	946						243,333			0.001%	11,413	\$12.32 \$12.61	\$3,265,4
460		HGD	1209						466,166 484,206			0.008%	29,137		\$2,162,7
460		OHGD	1215				65,585 49,961	2.931 6 116			336,967		14,742		\$1,353,1
460		0 HGD	1220			0.523						0 009%	55,302		\$5,006,7
460		0 HGD	1216			0.801									\$1,905,5
460 460		0 HGD 0 HGD	1210			1.276		3 206				0.006%		\$26 44	\$8,509,2
						1									
SUBTOTAL		HGD		<del> </del>			1,366,081							015.22 419.31	\$34,254,1 4308,754,1
CUMULATIVE TOTAL		HGD		+	10,500,00	0./3	11,/01,034	3,200	32,205,464	V.245/	30,0,0,0	1			
BENCH TOTAL		HGD/LGD			2,756,79	0.549	1,612,621	2.153	5,934,87	0.170%	10,316,77	0.005%	304,12	1 013.97	139,524,5
		.1		1	20.818.06			L		1	100,041,70	1			8347,190,4

TO A SOCIAL PROCESSION OF SOME MICH INCREDITION TOTAL METAL VALUES

				bhu	MOON SEC		Om SEARCI		TED TOPO	GIVAFIII					
19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU AU	AG	AG	COPPER	COPPER	MOLY	MOLY	•VAL	TOTAL
LEVB.	HEGHT	MATERIAL	10	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	*	POUNDS	TONNE	VALUE
450															
460		1105		2.05	34 440					0.000%	0	0.000%	0	\$0.00	
450	10	UDF		2.65	31,110	0	0	- 0		0.000%		0.000%		30.00	
UBTOTAL	<del> </del>	UDF	<del>   </del>		31,110										
UMULATIVE TOTAL		UDF			226,592										
														●0.00	
	ļ		<del>  </del>											\$0.00 \$0.00	
	<del> </del>		<del>  </del>					+		·				●0.00	\$
	<del> </del>	<del></del>	1											●0.00	S
														10.00	\$
450		WST	1214	2.65	240,533	0.122	29,345	2.16	519,550	0 010%		0 000%	0	\$2.71	\$652,45
450		WST	1212	2.65	552,638	0.075	41,448	0.244	134,844	0 060%		0 017%	207,121	\$2 91 \$4 76	\$1,609,91 \$1,169,09
450	10	WST	1213	2.65	245,012	0.263	64,438	2.466	604,200	0 000%		0.000%		34 /0	31,100,03
		1000			1 020 102	0.130	135,231	1.212	1,258,594	0.034%	784 043	0.009%	207,121	\$3.31	\$3,431,45
UBTOTAL		WST			1,038,183		618,380		3,594,053	0.041%	5,537,241		722,959	02.87	17,656,79
UMULATIVE TOTAL	<del> </del>	W31	<del> </del>	<del> </del>	0,142,134	0.101	0.10,300	0.000	0,000,000						
	<del> </del>	<del> </del>		<del></del>										\$0.00	
	<del>                                     </del>	<u> </u>	+											\$0.00	
												-		\$0.00	
450	10	LGD	961	2.65		0.096	4,840		24,502			0 002%			\$305,51
450	10	LGD	944	2.65		0.246	14,731	1 37	82,038		92,411				\$370,43 \$1,140,37
450	10	LGD	946	2.65	132,108		33,423	0 703	92,872			0 000%			\$1,919.97
450		LGD	1218		222,153		65,979		565,156		587,713 440,422	0.001%			\$2,224,9
450		LGD	1209		249,715		101,884		164,063 177,010			0.002%			\$698,10
450		LGD	962		272,518	0.267	110,370		263,797			0.004%			\$2,583,77
450		LGD	1210	2.65	331,609		120,374		474,533		950,39				\$3,228,0
450	<del> "</del>	, coo	1221			0.500	120,011	1,151							
SUBTOTAL	<del></del>	LGD			1,394,144	0.338	471,824	1.323	1,843,972	0.117%	3,582,750				\$12,471,04
CUMULATIVE TOTAL		LGD			6,223,551		1,742,128	1.105	6,879,344	0.125%	17,108,997	0.006%	787,824	●8.18	#50,913,12
						<u> </u>		<b></b>		-			<del> </del>	<del> </del> -	
		ļ		<u> </u>			<b></b>			<del> </del>		<del> </del>	<del> </del>	<del> </del>	
		<del> </del>	+							<del> </del>				\$0.00	
	+	+	+	<del> </del>				<del>                                     </del>		<del> </del>		<del>                                     </del>		\$0.00	
	+			·			1							\$0.00	
														\$0.00	
								-				1 00000	1	10.00	21 544 3
450		HGD	1208		152,502		62,069		190,171			0.001%			\$1,544,2 \$2,106,0
450		HGD	1222		184,758				362,310			0.008%			\$2,106,0 \$4,741,7
450		HGD	1220		400,025						1,851,99	0.002%			<ul><li>€ \$1,250,1</li></ul>
450		O HGD	1216		98,526 104,474							0.003%			\$1,359,8
450 450		0 HGD 0 HGD	1218		158,585							0 009%			\$2,469,4
450		OHGD	1211		302,435					0.250%	1,666,88	0 015%	100,013	\$15 64	\$4,731,0
450		OHGO	1217		182,327	0.674	122,888	1.683	306,856	0 170%		0.001%		\$15.88	\$2,897,7
450		0 HGD	1215			0.833					883,19	4 0.004%	29,440	\$17.28	\$5,773,9
							4 607 655	+	2 5 2 2 4 4 4	0.1022	7.001.47	0.000	250 25	414.63	\$26,874,0
SUBTOTAL	+	HGD	-	+			1,025,897							614.02 618.74	\$20,674,0 \$335,629,4
CUMULATIVE TOTAL		HGD			17,500,127	0.714	12,/0/,335	3.113	00,733,63	0.2357	, 150,55	J.307 X	2,000,007	7.0.74	,,-
BENCH TOTAL		HGD/LGD			3,311,616	0.452	1,497,721	1.622	5,370,388	0.154%	11,264,22	5 0.004%	311,901	\$11,68	039,345,1
						T	1		1	1	T			1	1

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						25	Om SEARC	H RADI	US						
19-12-95 9-31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	DA	AG	COPPER	COPPER	MOLY	MOLY	OVAL	TOTAL
LEVE	HEIGHT	MATERIAL	10	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMB	*	POUNDS	*	POUNDS	TONNE	VALUE
440															
											0	0.000%		\$0.00	
440	10	UDF	-	2.65	52, 167	0	0	- 0	0	0.000%		0000	<del></del>		
						<del></del>									
UBTOTAL		UDF		<del></del>	52,167										
CUMPLATIVE TOTAL		UDF		<del> </del>	278,759										
		<del></del>	·					1						\$0.00	S
	<del></del>	<del></del>	<del> </del>											10.00	\$
	<del> </del>		1											\$0.00	
			1											\$0.00	
	<del>                                     </del>													*0.00	
														10.00	
											000 307	0.044	146 674	90.00	\$1,899,38
440		WST	1212		601,521		43,310		193,690	0 070%		0.000%	145,874	\$3 16 \$3 48	\$1,225,26
440	10	WST	1213	2.65	351,780	0.172	60,506	2.008	706,375	0.010%	77,334	0.000%		270	₩ 1,44 J,45
CURTOTAL		WST		<del>  </del>	953,301	0.109	103,816	0.944	900,065	0.048%	1,005,842	0.007%	145,874	#3.28	93,124,67
SUBTOTAL CUMULATIVE TOTAL	<del> </del> -	WST	+	<del> </del>	7,096,435		722,196		4,494,118		8,543,083		868,833	92.93	\$20,780,46
COMPONITE TOTAL		1	1	1	.,,-,,-,,,										
														●0.00	
												-		\$0.00	
			L											\$0.00	
	1	<u> </u>	<del> </del>	L			22.42.4	4 200	206 002	0.000	268,004	0 003%	9,975	90.00 \$5.72	\$862,87
440		LGD	944		150,822	0.2	30,164	1.366	206,023	0.080%	151,997		1,900		\$299,43
440		red	961			0 147	6,334 96,305		34,472 450,292			0.000%	0		\$2,672,34
440		LGD	1221		371,835 320,475		91,656		158,956			0.006%	42 392	\$7.19	\$2,303,63
440		LGD	1211					1 997	452,605			0.001%	4,997	\$7 64	\$1,734,15
440	<b></b>	rep	1218						197,728			0 001%	3 189	\$9 03	\$1,306,93
440		LGD	946		144,644				316,748			0.001%	4,084	\$9.03	\$1,673,67
440	10	LGO	1222	2.65	185,233	0.35	04,031	1.,,,	310,740	0.1102	4.0,20	0.00.7			
	<del></del>	1.00	<del></del>	<del>                                     </del>	1,442,741	0 268	387,127	1.259	1,916,823	0.108%	3,382,675	0.002%	66,536	17.52	110,853,05
SUBTOTAL	<del></del>	LGD	+		7,666,292				8,696,168		20,491,672		854,360		161,766,17
CUMULATIVE TOTAL	<del></del>	LGU	<del></del>	<del> </del>	7,000,292	0.270	41.00.00	1,100	0,000,.00	<u> </u>					
	+	+	+	<del> </del>		-									
	<del> </del>	<del> </del>	+			1									
	1	1	1											●0.00	
										<b>-</b>		<del> </del>		90.00	
						L		<del> </del>		<del> </del>		<del> </del>		90.00	
						1	430.05		245.040	0 440=	414 477	0.001=	6,590	\$11.04	\$2,600,00
440		HGO	1210						245,943 529,357		846,232	0.001%	23,679		\$3,957,3
440		HGO	121								278,962		3,487		\$923,4
440		HGD	962									0.006%	22,430		\$2,171,7
440		HGO	1200			0 443			466,594		1,109,496		15,850		\$3,196,6
440		HGD	1217						740,319		905,297		4,311		\$3,006,4
440		HGD	1220								4,174,625		85,948		\$11,441,30
440		HGD	1210				_				760,168		13,821		\$2,327,10
440	_	HGD	121		391,969	1 024	401,376	18.242	7,150,302	0 080%	691,314	0 000%	0	\$22 62	\$8,691,3
440	10	HGD	120				237,829	4.401	682,769	0.510%	1,744,320	0.002%		\$39 65	\$6,154,89
					I										
SUBTOTAL		HGD							11,680,016		11,872,946			\$18.00	\$44,900,3
CUMULATIVE TOTAL		HGD			20,400,990	0.711	14,496,887	3.306	67,415,911	0.236%	106,069,882	0.006%	2,864,363	118.65	1300,528,75
		1		1				<del></del>	<b></b>			<b></b>			
BENCH TOTAL		HGD/LGD	-	<del></del>	3,937,609	0.532	2,096,679	3.428	13,498,839	0.178%	15,255,621	0.003%	247,892	814.16	955,753,43
1	1	1	1	1	1		1		1	1	1	1	1		

					STOOK SEC		Om SEARC		CTED TOPOG						
19-12-96 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU SEARC	AG	AG	COPPER	COPPER	MOLY	MOLV	- AVA T	70741
LEVEL	HEIGHT	MATERIAL	10	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	MULT X	POUNDS	TONNE	VALUE
430	1,23.11		-	<b>J.C.</b>	1014423	****	0.0.00		- GIAMO		roomus	_ <del>^</del> _	rounds	10reac	VALUE
430	10	UDF		2.65	152,288	0	0	0	0	0 000%	0	0 000%	0	\$0.00	
			1												
SUBTOTAL		UDF	<b>├</b>		152,288										
CUMULATIVE TOTAL		UDF	<del>  </del>		431,047										
	<del> </del>													\$0.00	\$0 \$0
	<del> </del>		+											\$0.00 \$0.00	\$0
	<del>                                     </del>		+											●0.00	<del>2</del> 0
			1											10.00	\$0
	1													●0.00	\$0
														●0.00	\$0
														●0.00	\$0
430	10	WST	1213	2 65	451,744	0.134	60,534	3 943	1,781,226	0 000%	0	0 000%	0	\$3.01	\$1,365,251
			-												
SUBTOTAL	ļ	WST			451,744		60,534	3.943	1,781,226	0.000%		0.000%	0	03.02	1,365,251
CUMULATIVE TOTAL		WST			7,547,179	0.104	782,730	0.831	6,275,344	0.039%	6,643,083	0.005%	968,833	92.93	122,145,720
	<del> </del>	<u> </u>												●0.00	\$0
	<del> </del>	<del> </del>												0.00	
430	+	LGO	944	2 65	195,163	0 103	37,667	1.228	239,660	0.100%	430 261	0.001%	4,303		\$1,196,229
430		LGD	1214	2.65			84,758		10,272,067		430,201		7,300		\$3,622,759
430		LGO	946	2 65	157,102		21,837	1.25	196,377	0 160%		0.000%	ő		\$1,087,042
430		LGO	1212		655,020		168,340		490,610			0.012%			\$4,800,441
430		LGD	1211		338,391		118,437	0 563	190,514			0 005%	37,301		\$2,785,652
430		LGD	1210	2 65	233,235	0 401	93,527	0.65	151,603	0 090%		0 001%	5,142	\$9 07	\$2,115,742
430		LGD	1221				141,529		544,886		1,193,006		0		\$3 686,915
430		LGD	961	2.65			12,466		32,747	0.160%		0 002%	1,767		\$384,384
430	10	reo	1216	2.65	113,039	0.464	52,450	0.953	107,726	0.070%	174,446	0 001%	2,492	\$9 59	\$1,085,156
SUBTOTAL	<del> </del>	1.60	<del> </del>		2 21 2 245	0.300	731 010	4 500	12 220 101	0.087%	5 315 031	0.0048	224 204	47.77	430 004 310
CUMULATIVE TOTAL		LGD	<del> </del>		2,713,345		731,010		12,226,191 20,922,359		5,215,931 25,707,604		1,078,654	97.73 97.97	#20,964,318 #82,730,497
COMOCATIVE TOTAL	+				10,379,037	0.270	2,600,200	2.010	20,322,333	0.112%	25,707,004	0.003%	1,078,854	37.57	162,730,437
			1											●0.00	\$0
	1													#0.00	\$0
														\$0.00	\$0
			1											10.00	\$0
430		HGO	1209	2 65			99,926		358,317	0 140%		0 005%	25,208		\$7,567,853
430		HGD	1208	2.65	159,842		63,937		484,482			0 002%	7,048		\$1,927,574
430		HGD	962	2.65			30,350		512,985			0.001%		\$12 09	\$944,895
430 430		HGD	1222				109,702		211,814 389,878			0.001%	3,984 42,134		\$2,607,484 \$2,508,071
430		HGD	1220				85,134 362,480		2,683,196		5,409,980				\$13,181,461
430		HGD	1215				294,956		781,361			0.002%			\$6,909,467
430		HGD	1218				238,776		1,471,212		2,355,531				\$7,107,597
430		HGD	1217				304,817		2,211,633		2,447,082				\$8,446,674
			1											\$0.00	\$0
SUBTOTAL	1	HGD			2,329,759		1,590,078		9,104,878	0.290%	14,903,794			119.83	\$46,201,277
CUMULATIVE TOTAL		HGD	-		22,730,754	0.708	16,086,965	3.366	76,520,790	0.241%	120,973,677	0.006%	3,143,634	618.77	1426,730,073
BENCH TOTAL	ļ	HGD/LGD			5,043,104	0.460	2,321,088	4.230	21,331,069	0.181%	20,119,726	0.005%	503,564	913.32	067,165,595
			. L		l	L	l	l		i	I	1	1	1	

				BHC	MSON SEC		Om SEARC		CTED TOPO	GRAPHY					
19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU AU	AG	AG	COPPER	COPPER	MOLY	MOLY	•VAL	TOTAL
LEVEL	HEGHT	MATERIAL	ID ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	*	POUNDS	TONNE	VALUE
420															
			-												
420	10	UDF	<del> </del>	2.65	281,276	0	0	0	. 0	0.000%	- 0	0 000%	0	\$0.00	
HTOTAL		UDF			281,276									<del></del>	
SUBTOTAL CUMULATIVE TOTAL		UDF	<del> </del>		712,323										
SOME TOTAL		<del></del>	1		7,1,000										
														\$0.00	\$0
														\$0.00	\$0
														●0.00	\$0 \$0
				<del></del>										90.00 90.00	\$0
			<del> </del>	<b></b>										\$0.00	\$0
	<del></del>													●0.00	\$0
420		WST	944	2 65	232,629		27,683		150,977	0.040%		0.002%	10,257	\$3 16	\$734,786
420	10	WST	1214	2.65	734,344	0.178	130,713	4.725	3,469,776	0.010%	161,895	0.001%	16,189	\$4.16	\$3,067,569
SUBTOTAL		WST	<del> </del>		966,974	0 164	158,396	3.744	3,620,753	0.017%	367,039	0.001%	26,447	13.93	03,802,374
CUMULATIVE TOTAL		WST	<del> </del>		8,514,152		941,126		9,896,097	0.037%	6,910,122		695,279	#3.05	125,948,094
JOHN DATITE TOTAL	1														
														●0.00	<u>\$0</u>
														●0.00 ●0.00	\$0 \$0
	ļ									<del></del>				\$0.00	
	<del></del>													●0.00	\$0
		1.60	1213	2.65	533,784	0.33	176,149	3 258	1,739,069	0.000%	0	0.001%	11,768	\$6.01	\$3,215,068
420 420		LGD	1209		215,353		55 130		201,355	0 090%	427,295		9.495	\$6 80	\$1,464,915
420		LGD	962		77,988		11,542		96,471	0 160%		0 001%	1,719		\$550,690
420		LGD	1211	2.65	353,835		102,258	0.75	265,376			0 006%	46,604	\$7 29	\$2,580,276
420		LGD	1212		703,923		167,534		748,975		2,017,449	0 007%	108,632	\$7 64	\$5,380,529
420		LGD	1222				64,162		297,479	0.110%	428,645	0 002%	7,794	\$9 23	\$1,632,978
	1		1												
SUBTOTAL		LGD			2,061,639		576,776		3,348,725		3,850,548		186,212	67.19	114,824,455
CUMULATIVE TOTAL		LGD			12,441,275	0.276	3,437,041	1,951	24,271,083	0.108%	29,558,151	0.005%	1,264,866	<b>\$7.84</b>	997,554,952
												<del></del>		\$0.00 \$0.00	\$0
	<del></del>	<del> </del>		<b></b>						<del> </del>				\$0.00	
420	10	HGD	961	2.65			21,017	1.022	55,074	0.160%		0.001%	1,188		\$587,670
420	10	HGD	1208				75,770		411,349			0.002%	7,311		\$1,902,864
420		HGD	1219				79,783		258,510			0.008%	30,723		\$2,251,877 \$2,939,571
420		HGD HGD	1210 946				98,353 120,663		369,191 497,307	0.220%		0.001%	4,643 3,590		\$2,767,660
420 420		HGO	1218				145,306		704,614		1,260,371		5,252		\$4,066,996
420		HGD	1215				289,941		1,205,031	0.180%		0.001%	8,248		\$6,783,120
420		HGD	1220				484,599		1,398,728		5,976,816		336,196		\$15,571,086
420		HGO	1217				172,611					0.007%			\$4,350,510
420		HGD	1221											\$19 49	\$8,791,513
420	10	HGD	1216	2.65	129,776	1.177	152,746	2.093	271,621	0.160%	457,771	0.002%	5,722	\$23.78	\$3,066,133
SUBTOTAL CUMULATIVE TOTAL		HGD HGD		-	3,036,278		1,940,517		7,137,868 83,658,658		16,261,721 137,235,369			117.49	\$53,101,007 0479,\$31,075
COMPENSATIVE TOTAL			1	<del>                                     </del>	23,747,032	3.700	15,027,463		30,000,000	V.242 //	.57,255,356	3.000 %	3,051,772	7,0.02	24,2,00,,070
BENCH TOTAL		HGD/LGD	-		5,097,916	0.494	2,517,293	2.057	10,486,593	0.179%	20,112,268	0.006%	634,350	#13,32	167,925,457
CUM. BENCH TOTAL		HGD/LGD			20 200 203		21,464,524	2 0 25	107,929,741	0.1000	166,793,549	0.000	4,858,638	410.00	<b>\$577,386,027</b>

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19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	OVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID.	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	*	POUNDS	TONNE	VALUE
410															
410	10	UDF		2 65	279.501		0	0	0	0 000%		0 000%	0	\$0.00	
410	\ <u>'U</u>	00-			2/9,301	0				- 0000		0007		-2000	
SUBTOTAL		UDF			279,501										
CUMULATIVE TOTAL		UDF			991,823										
	<del></del>													#0.00	\$0
	+		1											\$0.00	\$0
														\$0.00	\$0
	<del>                                     </del>		1											\$0.00	\$0
	<del>                                     </del>													\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
			-											\$0.00	\$0
	<del> </del>		<b> </b>											\$0.00	\$0
SUBTOTAL	<del></del>	WST				0.000		0.000		0.000%		0.000%		\$0.00	•0
CUMULATIVE TOTAL		WST			8,514,152		941,126	1.162	9,896,097	0.037%	6,910,122		895,279		125,948,094
AANTONINE IN THE		1	†···		, 0,0,7,1,04	1	941,180	.1.1.1.9.2	0,030,037		···· 'o'o , ò'', 'a'a				
	1													●0.00	\$0
														\$0.00	\$0
410		LGD	1199	2 65	72,391		12,234	0 413	29,898	0 080%		0 001%	1,596	\$5.01	\$362,897
410		LGD	1217	2 65	331,426		62,640		495, 151	0.060%	438,402		7,307	\$5 02	\$1,664,160
410		LGD	944	2.65	237,630		48,001	1.002	238,106	0.070%	366,719		0		\$1,282,643
410		LGD	1214	2.65	934,535		231,765	2.774	2,592,399	0.030%	618,088	0.001%	20,603 9,070		\$5,069,713 \$1,145,297
410		LGD	1209	2.65 2.65	205,701 76,219		37,232 10,671	0.805	165,589 106,706	0.160%	268,853		1,680		\$531,124
410		LGD	962 961	2.65	61,346		10,613	0.615		0.160%	216,392		2,705		\$449,445
410		LGD	1212		787,999		213,548	1.118	680,983	0 120%	2,084,687		86,862		\$6,233,523
410		LGO	1218		246,347		58,631	1 542	379,867	0.140%		0 007%	38,017		\$1,976,778
	<del> </del>		1												
SUBTOTAL		LGD			2,953,594		685,333		4,926,427	0.081%	5,289,301		167,840		818,715,600
CUMULATIVE TOTAL		LGD			15,394,870	0.268	4,122,375	1.897	29,197,510	0.103%	34,847,452	0.004%	1,432,706	<b>\$7.55</b>	116,270,553
						<del> </del>				-				●0.00	\$4
	1	<del> </del>	-			1								♦0.00	S.
	1		1										L	\$0.00	S
													<u> </u>	●0.00	\$
				<u> </u>								1	-	●0.00	<b>X</b>
410		HGD	1219									0 003%			\$1,795,614
410	10	HGD	1221			0 592			534,209			0.000%		\$11 13	\$5,497,75
410		HGD	1220			0.363						0.016%			\$4,525,37 \$8,456,68
410		HGD	1208			0.502						0.001%		\$12.55	\$3,655,67
410		HGD	946			0.502						0.005%			\$2,226,52
410		HGD	1215									0 002%			\$10,836,27
410	10	HGD	1216	2 65	582,413	1.188	691,906	3 979	2,317,420	0 390%	5,007,595	0 004%	51 360		\$17,895,18
410	10	HGD	1213	2.65	628,48	0.207						0 001%			\$20,033,64
SUBTOTAL		HGD			3,833,749	0.595	2,281,918	17.501	67,093,313	0.222%	18,775,157	0.004%	373,480	\$19.54	\$74,922,71
CUMULATIVE TOTAL	-	HGD			29,600,781	0.686	20,309,401	5.093	150,751,971		156,010,555	0.006%	3,965,252	<b>\$18.74</b>	4554,753,79
BENCH TOTAL		HGD/LGD			6,787,344	0.437	2,967,251	10.611	72,019,740	0.161%	24,064,458	0.004%	541,319	613.80	193,638,311
	<del> </del>	1		ļ		-			1						
CUM, BENCH TOTAL		HGD/LGD			44,995,651	0.543	1 24,431,776	3,999	179,949,481	0.192%	190,858,007	0.005%	5,397,957	\$14.91	8671,024,34

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19-12-95 9:31 AM	SENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	SVAL	TOTAL
LEVEL	HEGHT	MATERIAL	10	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	*	POUNDS	TOMME	VALUE
400															
400	10	UDF		2.65	401,507	0	0	ā		0.000%		0 000%	0	\$0 00	
	<u> </u>				10.,507							V 333.10			
UBTOTAL		UDF			401,507										
UMULATIVE TOTAL	<del> </del>	UDF			1,393,330	-								+	~ <del>~~~~</del>
	<del> </del>		<u> </u>	1										10.00	\$0
														\$0.00	\$0
														\$0.00	90
														\$0.00	×
														\$0.00	
														\$0.00	\$0
	1													\$0.00	\$0
400		WST	1214		1,157,623		60, 196		567,235	0.000%	0		25,521	\$0.00	\$1,092,750
400	10	WST	1213	2.65	743,611	0.111	82,541	3.378	2,511,917	0 030%	491,814	0 002%	32,788	\$3.34	\$2,494,645
USTOTAL		WST			1,901,234	0.075	142,737	1.620	3,079,152	0.012%	491,814		58,309	11.89	13,587,398
CUMULATIVE TOTAL	I	WST			10,415,386	0.104	1,083,863	1.246	12,975,249	0.032%	7,401,935	0.004%	953,588	\$2.84	129,535,489
	<del> </del>		<del> </del>											●0.00	\$0
400	10	LGD	1212	2 65	838,456	0.106	88,876	1 185	993,570	0 130%	2,403,019		18,485	\$5.54	\$4,651,491
400	10	LGD	1221	2.65	542,990	0 285	154,752	0 897	487,062	0 060%		0 000%	0	\$6 43	\$3,493,385
400		LGD	1217	2.65	331,936	0 241	79,997	1.329	441,143	0 090%	658,614		14,636	\$6 64	\$2,206,664
400		LGD	944	2.65	233,366	0.288	67,210	1.485	346,549	0 090%	463,036	0 001%	5, 145		\$1,735,765
400	10	LGD	1208	2.65	326,230	0 302	98,522	1.896	618,533	0.080%	575,371	0 003%	21,576		\$2,439,516
400		LGD	1209	2.65	279,988	0 248	69,437	1.079	302,107	0 140%	864,175	0 002%	12,345	\$8.08	\$2,263,232
400		LGD	1219	2.65	220,958	0 289	63,857	4 123	911,010	0 110%	535,841	0 002%	9,743	\$8 57	\$1,897,043
400	10	LGD	961	2 65	114,212		30,152		114,783	0 160%	402,871		2,518	\$8 87	\$1,013,685
400	10	LGD	1199		90,802		24,880		77,454	0 160%		0.004%	8,007	29 00	\$817,474
400	10	LGD	1216	2 65	594,672	0.41	243,815	0.798	474,548	0.090%	1,179,923	0 002%	26,221	\$9 24	\$5,499,857
SUBTOTAL		LGD	-		3,573,611	0.258	921,497	1.334	4,766,760	0.103%	8,121,397	0.002%	118,878	97.28	\$26,016,113
CUMULATIVE TOTAL		LGD			18,968,481	0.266	5,043,872	1.791	33,964,270	0.103%	42,968,849	0.004%	1,551,381	\$7.50	\$142,288,665
			-												
														\$0.00	30
		<b></b>				<del></del>		<u> </u>		<del> </del>				\$0.00	
		<del> </del>		<del> </del>	<del> </del>		<del></del>			<del> </del>		<del> </del>		●0.00 ●0.00	
		ļ		·	<del></del>							<del> </del>		10.00	
	+	<del> </del>	+	<del> </del>	<del> </del>	<del> </del>	<del> </del>	<del>}</del>						00.00	
	<del></del>	+	-			<del> </del>	<del></del>			<del> </del>		<del> </del>		10.00	
	<del></del>	<del> </del>	+	<del>\</del>		<del> </del>		<del></del>		<del> </del>	<del></del>	<del> </del>		10.00	
		<del> </del>	+	<del> </del> -		<del> </del>		+		<del></del>		<del> </del>	<del></del>	\$0.00	
400	<del></del>	OHGO	1216	2.65	258,634	0.38	98,281	1 684	435,539	0.180%	1,026,341	0.001%	5,702		\$2,959,10
400		0 HGO	1220						513,129			0.012%			\$4,829,79
400		0 HGD	119									0.005%			\$13,456,98
400	_		95			1.163		1.146				0.000%	3 230	\$23.35	\$3,432,35
400		O HGD	1215			2 076					3,231,714	0.002%	19,586	\$43.87	\$19,500,47
CURTOVAL		NCO.			2.001.00										67.196
SUBTOTAL CUMULATIVE TOTAL		HGD	-	<del> </del>			1,880,818		4,789,449		10,305,180			021.43 418.92	\$44,178,71 4590,932,50
			1											1	
BENCH TOTAL	<del></del>	HGD/LGD	<del></del>	<del></del> -	5,635,414	0.497	2,802,316	1.696	9,556,210	0.148%	18,426,577	0.003%	338,567	812.46	970,196,82
CUM. BENCH TOTAL	1	HGD/LGD	+	-	50 631 065	0.538	27,234,091	2 743	100 000 000		209,284,584	1		1	0741,221,17

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ALL MARK CHILL HOLDE HOLLED HER STADAGE WITH 1006 ACCASE MOLYDDENHA VALHES ARE NOT INCLHIDED IN TOTAL METAL VALUES

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19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	IVAL	TOTAL
TENE	HEIGHT	MATERIAL	10	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	*	POUNDS	TONNE	VALUE
390															
390	10	UDF		2.65	525,891	0	O	0	0	0.000%	0	0 000%	0	\$0.00	
UBTOTAL UMULATIVE TOTAL	<del></del>	UDF			525,891 1,919,221										
UMUCATIVE TOTAL	+	554	1		1,515,221										
														\$0.00	\$
														\$0.00	
	<del> </del>		<del>  </del>											\$0.00 \$0.00	s
	<del> </del>		1											0.00	<u>-</u>
390	10	WST	1214	2 65	1,324,238	0.044	58,266	0.228	301,926	0 000%	0	0.001%	29,194	\$0.76	\$1,003,34
390		WST	1213	2.65	857,263		117,445		3,291,032	0.020%		0.004%	75,598	\$3.59	\$3,085,02
390		WST	1217	2.65	486,285		57,382	0.627	304,901	0.060%		0.003%	32,162	\$3 69	\$1,793,83
390	10	WST	1221	2.65	618,708	0.182	112,605	0.681	421,340	0.040%	545,607	0.001%	13,640	\$4 18	\$2,585,39
UBTOTAL	+	WST	+		3,286,494	0.105	345,698	1.314	4,319,199	0.022%	1,566,839	0.002%	150,594	\$2.58	18,467,59
UMULATIVE TOTAL	1	WST			13,701,881				17,294,448				1,104,183		\$38,003,08
														\$0.00	
	ļ													\$0.00	
	<del> </del>													<b>●0.00</b>	\$
390	10	LGD	1219	2.65	232,138	0.169	39,231	1.643	381,403	0.070%	358 243	0.002%	10,236	\$5.00	\$1,162,55
390		LGO	1220		374,491		71,528		297,346			0 004%	33,024	\$5 45	\$2,041,19
390		LGD	1216		690,473		198,856		621,425	0.050%		0.004%	60,889		\$4,285,71
390		LGD	1199	2 65	196,618		44,632		107,157			0.002%	8,669		\$1,391,46 \$1,005,27
390 390		LGD	961 1198	2.65 2.65	139,645 922,393		22,483 230,598		127,356 437,214		3,253,640	0.001%	3,079 61,006		\$7,871,25
390		LGD	956			0 253	93,382		168,677		1,301,951		8,137		\$3,166,12
	1	1	1												
UBTOTAL		LGD			2,924,855		700,710		2,140,579		7,348,183		185,040		\$20,923,57
CUMULATIVE TOTAL		LGD	<del> </del>		21,893,336	0.262	5,744,582	1.649	36,104,849	0.104%	50,317,032	0.004%	1,736,421	17.45	\$163,212,24
			-												
														90.00	
	+	<del></del>					<del> </del>			<del> </del>	<del> </del>			90.00 90.00	
	+	<del> </del>	+			<del> </del>		<del> </del>	<del> </del>	<del> </del>	<b></b>	1		●0.00	
	1													●0.00	
														\$0.00	
		ļ								ļ				●0.00	
390	40	HGD	1208	2.65	384 147	0 498	181,343	7.864	2,863,619	0.090%	722 647	0.001%	8,028	\$12.19	\$4,449,1
390		HGD	1218			0.358						0.001%			\$4,170,60
390		HGD	1223			0.577					1,303,850	0.007%	60,846	\$13.93	\$5,496,7
390		HGD	1215		447,002	0 751	335,699		1,762,083	0 140%	1,379,658	0 001%	9,855	\$16 79	\$7,510,2
390		HGD	957					2.055		0 160%		0 001%	4,483	\$17.48	\$3,551,6
390	10	HGD	944	2.65	281,734	0.777	218,907	6.713	1,891,280	0.460%	2,857,135	0.002%	12,422	\$26.62	\$7,507,5
UBTOTAL	+	HGD	+		2 007 129	0.616	1,236,217	4 305	8,639,993	0.197%	8,725,566	0.0029	102 615	116.29	\$32,686,1
UMULATIVE TOTAL		HQD							164,181,413		175,041,302				+631,618,6
ENCH TOTAL		HGD/LGD	+		4,931,984	0.393	1,935,927	2.186	10,780,571	0.148%	16,073,780	0.003%	287.655	<b>#10.87</b>	163,609,6
					11441144	7.555	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1	1	J., 40 %	10,070,700	J.505 N	237,000	7.0,07	100,000,0
UM, BENCH TOTAL		HGD/LGD		I	55,563,046	0.525	29,171,018	3.605	200,286,262	0.184%	225,358,334	0.006%	6,024,179	\$14.31	<b>●794,830,8</b>

					DITO OIT OL				CTED TOPO	9191111					
	45.04		1				Om SEARC							I	
19-12-96 9:31 AM LEVEL	BENCH	MATERIAL	HOLE	DENSITY	TONNES	PPM	GRAMS	AG	AG GRAMB	COPPER	COPPER	MOLY	MOLY	TOWNE	VALUE
300				- Vertain						*	POUNDS	*	POUNDS	TONNE	
380	10	UDF		2.65	960,661	0	ō	0	0	0 000%	0	0 000%	0	\$0.00	
		00*		2.03	800,001					0 000 %		0000			
BTOTAL		UDF			960,661										
UMULATIVE TOTAL		UDF			2,879,882										
														●0.00	\$0
														\$0.00 \$0.00	\$C
			<del>                                     </del>											●0.00	<u>ĝ</u>
	<del></del>	<del> </del>	1	I										10.00	
	+	<del> </del>	+											\$0.00	\$1
380	10	WST	1214	2 65	2,166,457	0 077	166,817	0 594	1,286,876	0 000%		0.001%	47,762	\$1 37	\$2,965,53
380	10	WST	1216	2 65	724,297		127,476		351,284	0.050%	798,399		31,936	\$4.31	\$3,125,090
380	10	wst	1199	2.65	447,960	0.162	72,569	0.571	255,785	0 070%	691,307	0.005%	49,379	\$4 66	\$2,067,32
UBTOTAL	<del> </del>	WST	<del> </del>		3,338,714	0.110	366,863	0.587	1,893,945	0.020%	1,489,706	0.002%	129,077	02.46	18,177,956
UMULATIVE TOTAL		WST	1		17,040,594	0.105	1,795,424	1.126	19,188,393	0.028%	10,458,480	0.003%	1,233,260	42.71	948,181,04
	<del> </del>		<del>}</del> -	<del> </del>										●0.00	×
	<del> </del>	<del> </del>	<del> </del>	-		1								●0.00	×
	<del>                                     </del>	<del>                                     </del>												\$0.00	æ
380	10	LGO	1221	2.65	589,753	0.287	169,259	0 444	261,650	0 020%		0 001%	13,002	\$5 26	\$3,104,33
380		LGD	1220	2 65			75,568	0.915	344,002	0.070%		0 004%	33,154	\$5.36	\$2,016,05
380	10	LGO	961	2.65			10,194		45,599			0.001%	3,037		\$781,371
380		LGD	1217				164,104		827,531		1,391,484	0 003%	30,922		\$4,560,190
360		LGD	1223			0 29	133,631	1.141	525,770			0 001%	10,159 18,329		\$3,407,320 \$3,327,527
380		LGD	1219				110,574 122,926	1.019	1,836,108		1,417,018		8.856	\$9 55	\$3,837,97
380 380		LCD	956				259,987	0.695	831,029		3,684,676		347,997	SD 66	\$8,969,25
														17.10	422 224 24
WETOTAL		LGD	<del> </del>	<u> </u>	4,011,501		1,046,242		5,081,240		9,650,081		465,456 2,201,877		\$30,004,041 \$193,216,290
UMULATIVE TOTAL		LGD	1		25,904,837	0.262	6,790,825	1.590	41,186,089	0.105%	09,907,113	0.007	2,201,017	V/	7103,210,23
			-											●0.00	9
	1													●0.00	
										ļ				00.00	\$
			-		ļ	<del> </del>								90.00	3
		<del> </del>										<del> </del>		40.00	
	<del></del>	<del></del>		<del></del>	<del> </del>			<del> </del>		<del> </del>		<del></del>		\$0.00	\$
		<del> </del>			<del> </del>	<del> </del>					<b></b>	<del></del>		10.00	3
	<del> </del>	<del> </del>	+	<del> </del>	<del> </del>	1				<del>                                     </del>	1	1		\$0.00	
		<del> </del>	<del> </del>	<del> </del>	<del> </del>	1		-						●0.00	
380	10	HGD	1215	2.65	453,76	0.483	219,166	2.148	974,684	0.130%		0 002%	20,000		\$5,364,25
380		HGD	95			0 481	140,352	0.621	181,203			0.001%		\$12.28	\$3,583,30
360		HGD	1210		324,66	0.324	105,191	8.781	2,850,870	0.190%		0.003%	21,473		\$4,018,56
380		HGD	94	4 2 65	281,70	1.381	389,030	7 263	2,046,001	0 640%	3,974,692	0 003%	18,631	\$41.41	\$11,674,08
SUBTOTAL	+	HGD	+	+	1,361,92	0.632	853,741	4.477	6,062,757			0.002%		#18.23	\$24,640,24
CUMULATIVE TOTAL		HGD					24,280,177		170,234,170	0.237%	182,705,690	0.006%	4,354,302	418.74	4654,258,87
BENCH TOTAL		HGD/LGD			5,363,42	0.354	1,899,983	2.076	11,133,997	0.148%	17,314,469	0.004%	632,000	910.19	054,644,29
		1			1			1		1		1		1	]

				DAL	ALCON OL		Om SEARC		CTED TOPO	<u> </u>					
19-12-95 9:31 AM LEVEL	BENCH	POLYGON MATERIAL	HOLE	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER	COPPER POUNDS	MOLY %	MOLY POUNDS	TONNE	TOTAL
370															
370	10	UDF	<del>                                     </del>	2.65	387,827		0	0	0	0.000%		0.000%	0	\$0.00	
3/0	10		<del>   </del>	2.00	301,021					0.000 %		0.000.0			
UBTOTAL		UDF			387,827										
UMULATIVE TOTAL		UDF			3,267,710										
										ļI				\$0.00	\$0
	<del> </del>									l				\$0.00 \$0.00	\$X
	<del> </del>	<del> </del>	+					<del>   </del>		<del> </del>		<del> </del>		●0.00	<u>2</u>
	<del></del>	<del> </del>	+							<del> </del>				0.00	80
370	10	WST	960	2.65	1,478,793	0	0	0	0	0.000%	0	0.000%	0		SC
370		WST	1221		553,770		35,441	0.378	209,325			0 000%	0		\$768,55
370		WST	1214		1,708,229		189,613		3,050,898			0.002%	75,320	\$2.72	\$4,661,681
370		WST	1216		759,532		123,804		259,000	0 020%		0.002%	33,490	\$3 25	\$2,466,362
			1												
SUBTOTAL		WST			4,500,324		348,858		3,519,223		1,210,180		108,810		67,896,596
CUMULATIVE TOTAL		WST			21,540,919	0.100	2,145,282	1.054	22,707,616	0.025%	11,668,661	0.003%	1,342,069	92.51	\$54,077,640
		<b></b>				-				ļ				0.00	\$6
	<del> </del>	+								<del> </del>				0.00	
	+	<del></del> -	+	<del> </del>		-								\$0.00	\$
	+	1	1											●0.00	\$
														\$0.00	\$
										<del> </del>				\$0.00 \$0.00	\$X \$X
370	<del></del> ;	LGD	1220	2 65	383 220	0 209	80,095	0 686	262,695	0 060%	675 900	0 003%	25,346		\$2,190,63
370		LGD	1219		500,211		97,541	1 547	773.826			0 001%	11,028		\$3,117,170
370		LGD	956			0.138	59,632		121,425	0.160%		0.002%	19,053		\$2,890,90
370		LGD	1217	2.65	721,031	0.302	217,751	0.945	681,374	0.090%	1,430,639	0.002%	31,792	\$7.54	\$5,439,64
				I											
SUBTOTAL		LGD		ļ	2,036,587		455,019		1,839,520		4,733,557		87,219		113,638,35
CUMULATIVE TOTAL		LGD			27,941,424	0.259	7,245,844	1,540	43,025,609	0.105%	64,700,670	0.004%	2,289,096	\$7.40	\$206,854,64
	<del> </del>	<b>!</b>	-											\$0.00	
	+	1		<del> </del>	<del></del>	<del> </del>		1		<del> </del>				\$0.00	\$
			+	<del></del>	<del>                                     </del>	1				1	1			●0.00	S
														\$0.00	S
												ļ		\$0.00	\$
						<b></b>				ļ			<del> </del>	\$0.00	
							A. 70	1-4	1 460 603	0.3304	1 500 404	0.000	44.44	10.00	\$3,781,53
370		HGD	1218						1,460,697 868,445			0.002%	14,441		\$8,327,28
370 370		HGD HGD	1198						1,901,359			0.000%	223,616		\$12,664,09
370	_	HGD	944						1,412,587			0.001%	7,55		\$5,633,62
370		HGD	1223								1,865,567	0.007%	81,619		\$8,841,40
370	10	HGD	1215	2 65	458,478	0 707	324,144	2.824	1,294,742			0.001%		\$18 04	\$8,276,69
370	10	OHGO	957	2.65	369,193	0 854	315,29	0.596	220,039			0.001%		\$18.27	\$6,746,15
e11070741	<del></del>	1400				1 2 2 2 2	0.040.55	+	10 000 000			-		1	44.452.44
SUBTOTAL CUMULATIVE TOTAL	+	HGD	+	<del> </del>					10,228,019					915.15	\$54,270,99
TOWNS TO INC	<del>                                     </del>	1.00			35,505,220	0.652	40,320,20	4.0/5	100,502,188	0.233%	198,078,626	0.006%	4,811,576	110.41	4710,529,86
BENCH TOTAL		HGD/LGD	1-		5,619,174	0.444	2,495,110	2.148	12,067,639	0.162%	20,106,493	0.004%	544,493	112.09	967,909,34
CUM. BENCH TOTAL	+	HGD/LGD		+	40 545 04	0.004	33,500,111	1			262,779,296	+		-	9917,384,50

				DN	DASON SEC				CTED TOPO	GRAPHI					
19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	Dm SEARCI	AG AG	AG	COPPER	COPPER	MOLY	MOLY	•VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	*	POUNDS	TOMME	VALUE
360			1			*****									
360	10	UDF		2.65	1,580,162	0	0	0	0	0.000%	0	0 000%	0	\$0.00	
SUBTOTAL	ļ ——	UDF	+		1,580,162										
CUMULATIVE TOTAL	<del></del>	UDF	+		4,847,872								<del></del>		
														●0.00	\$0
														●0.00	\$0
														●0.00	\$0 \$0
														90.00 90.00	\$0 \$0
			+											\$0.00	\$0
			1											●0.00	\$0
360	10	WST	1216	2.65	804,443		8,044	0.1	80,444	0.000%		0.000%	0	\$0.18	\$147,052
360	10	WST	1217	2.65	730,148	0.19	138,728	0.85	620,626	0.060%	965,820	0.003%	48,291	\$4 89	\$3,574,561
ALIOTOTAL		MET	ļ		1,534,691	0.004	146,773	0.457	701,070	0.029%	965,820	0.001%	48,291	02.43	#3,721,613
SUBTOTAL CUMULATIVE TOTAL		WST	<del> </del>		23,075,510		2,292,055	1.014	23,408,686	0.025%	12,634,480				157,799,253
COMOLATIVE TOTAL	<del> </del>	W31	<del> </del>		23,070,010	0.000	2,252,000	1,0,1	20,400,000	0.020 %		0.000	100000		
			1											\$0.00	\$0
														●0.00	\$0
														\$0.00	\$0
														\$0.00	\$0 \$0
	ļ	ļ	1212			0.400	00.046	1 404	700 000	0.090%	1,054,480	0.000*	23,433	\$5.52	\$2,937,003
360		LGD	1219		531,450 326,671		89,815 66,641	1.494	793,986 480,208	0.080%		0.002%	7,202	\$5.80	\$1,697,414
360		LGD	956		462,623		73.094	0313	144,801	0.160%	1,631,853		10,199		\$3,247,030
360 360		LGD	1198				269,733	0.605	562,718	0.100%	2,050,546		82,022	\$7 55	\$7,024,284
360		LGD	1220				111,936		305,491	0.100%	856,861	0.004%	34,274	\$7 56	\$2,938,212
360		LGO	1221				239,720	0.767	390,372	0.030%	336,619	0.001%	11,221	\$8.56	\$4,361,354
SUBTOTAL		LGD			3,148,482		850,939		2,677,575	0.094%	6,506,506		168,351	97.12	122,405,297
CUMULATIVE TOTAL	<del></del>	LGO		<del> </del>	31,089,906	0.260	8,096,783	1.470	45,703,184	0.104%	71,207,176	0.004%	2,457,447	67.37	1229,259,938
		<del> </del>												<b>♦0.00</b>	\$0
														●0.00	\$0
														●0.00	20
		<del> </del>	<del></del>	<del> </del>								<del></del>		\$0,00 \$0.00	\$0 \$0
	<del> </del>	<del> </del>	+											\$0.00	\$0
														\$0.00	\$0
									10000		4 6 4 4 4 4 4	0.0000		0.00	\$0
360		HGD	1218				98,315		1,050,004	0.180%	1,300,484		7,225		\$3,437,511
360		HGD	1223				353,165		419,050 4,322,965		392,569 8,471,551		26,171 688,314		\$6,261,796 \$25,829,332
360		HGD	960				888,610 293,105		1,710,336		3,120,783		146,860		\$8,990,385
360		HGD HGD	957						354,748						\$4,613,965
360 360		HGO	1215		1			1.966				0 001%		\$37 73	\$17,541,829
<del></del>	<del> </del> "	1	<del>  '2''</del>	2.00	100,100		330,500	1	2.5,						
SUBTOTAL		HGD			5,029,090	0.548	2,754,172	1.744	8,770,879		16,366,513			\$13.26	\$66,674,818
CUMULATIVE TOTAL		HGD		ļ	43,633,308	0.666	29,074,439	4.337	189,233,068	0.223%	214,445,140	0.006%	5,699,403	417.81	6777,204, <b>68</b> 4
		14007.00		·	0 177 577	0.44	3 805 111	1 400	11,448,454	0.127%	22,873,019	0.0042	1,058,178	810.88	\$89,080,115
BENCH TOTAL	+	HGD/LGD	<del> </del>		0,1//,0/2	0.441	3,000,111	1,500	11,770,734	V.12/70	22,073,013	0.000 %	1,030,176	7.0.03	705,000,110
CUM, BENCH TOTAL	<del></del>	HGD/LGD	<del> </del>	<del> </del>	74 723 218	0.407	37 171 222	3 144	234,936,252	0.173%	285 652 316	0.005%	8 156 850	913.47	91,006,464,622

19-12-98-2-17-AM BROCH FOLYGON HOLE LYPE 19-10 LYPE 19-								Om SEARC		CTED TOPO						
LIVEL MODET MATERIAL D DENSITY TORRES PRIE GRAMS PPM GRAMS 9, FOUNDS 9, FOUNDS 100005  350 10 UCF 265 1,789,462 0 0 0 0 0 0 0 00005 0 0 00005 0 30.00  UNITOTAL UCF 6,037,333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	19.12.95 9:31 AM	RENCH	POLYGON	HOLE		METRIC					CUDDER	COPPER	MMY	MMY	AVAL	TOTAL
390 10 UPF 2.65 1,789.462 0 0 0 0 0 0.000% 0 0.000% 0 30.00 UNIONAL UPFOTAL UP					DENSITY											VALUE
350 10 UPF 2.55 17,69,462 0 0 0 0 0 0 0 000% 0 000% 0 30 00 30 00 1000% 0 30 00 1000% 0 30 00 1000% 0 30 00 1000 10		1,					****								,,,,,,,	
UNDALATIVE TOTAL  UDF  1,789,462  6,837,333  1,89,462  6,837,333  1,89,462																
DABLATIVE TOTAL   UPST   1217   2.65   768,466   0.155   123,767   0.935   746,566   0.070%   1,232,760   0.003%   52,812   54.00   15.00	350	10	UDF		2.65	1,769,462	0	0	0	0	0.000%	0	0 000%	0	\$0.00	
DABLATIVE TOTAL   UPST   1217   2.65   768,466   0.155   123,767   0.935   746,566   0.070%   1,232,760   0.003%   52,812   54.00   15.00																
10.00   10.00	UBTOTAL															
10.00   10.0	UMULATIVE TOTAL		UDF			6,637,333					<b> </b>					
10.00   10.0					<b></b>											<u>_</u>
10,000   1					<del> </del>						<del> </del>					
10.00   10.0		<del> </del>												-		
\$60 10 WST 1217 2.65 786,486 0.155 123,767 0.935 746,596 0.070% 1,232,269 0.003% 52,812 44.62 53, 19570TAL WST 798,498 0.155 123,767 0.935 746,596 0.070% 1,232,269 0.003% 52,812 44.62 53, 19570TAL WST 22,874,008 0.101 2,415,822 1.012 24,155,292 0.029% 13,866,750 0.003% 1443,172 92.59 191,4 191				ļ												
\$60 10 WST 1217 2 65 766,466 0.150 123,767 0.935 746,566 0.070% 1,232,269 0.003% 52,812 54.62 \$3.  UBTOTAL WST 798,498 0.150 123,767 0.935 746,566 0.070% 1,232,269 0.003% 52,812 44.63 \$3.  UBARLATIVE TOTAL WST 23,874,008 0.101 2,415,822 1.012 24,155,282 0.028% 13,866,750 0.003% 1443,172 42.56 181.6  UBARLATIVE TOTAL WST 22,874,008 0.101 2,415,822 1.012 24,155,282 0.028% 13,866,750 0.003% 1443,172 42.56 181.6  UBARLATIVE TOTAL WST 23,874,008 0.101 2,415,822 1.012 24,155,282 0.028% 13,866,750 0.003% 1443,172 42.56 181.6  UBARLATIVE TOTAL WST 22,874,008 0.101 2,415,822 1.012 24,155,282 0.028% 13,866,750 0.003% 1443,172 42.56 181.6  UBARLATIVE TOTAL WST 22,874,008 0.101 2,415,822 1.012 24,155,282 0.028% 13,866,750 0.003% 1443,172 42.56 181.6  UBARLATIVE TOTAL WST 24,864 0.100 1221 2 65 973,341 0.266 2258,999 0.807 785,486 0.000% 429,189 0.001% 21,456 55 0.00 44.00 0.00 180,000		<del></del>		<del>                                     </del>											90.00	
\$60 10 WST 1217 2.65 788,460 0.155 123,767 0.935 746,596 0.070% 1,232,269 0.003% 52,812 44.03 53,000 1.000 1																
950 10 WST 1217 2.65 788,468 0.155 123,767 0.935 748,596 0.070% 1,232,769 0.003% 52,812 \$4.02 \$3.  UBTOTAL WST 7 198,498 0.155 123,767 0.935 746,596 0.070% 1,232,728 0.003% 52,812 \$4.03 \$3.00  DAMALATIVE TOTAL WST 7 22,674,008 0.101 2,415,822 1.012 24,155,282 0.026% 13,866,750 0.003% 1,443,172 42,58 181,40  23,674,008 0.101 2,415,822 1.012 24,155,282 0.026% 13,866,750 0.003% 1,443,172 42,58 181,40  350 10 LGO 1221 2.65 973,341 0.266 258,909 0.807 785,486 0.020% 429,169 0.001% 21,458 15.00 \$6.00  350 10 LGO 1221 2.65 662,019 0.203 193,972 0.797 527,679 0.020% 29,190 0.004% 43,974 155.70 330 350 10 LGO 1221 0.265 380,263 0.465 0.8079 2.096 2.66,835 0.160% 1,758,956 0.004% 43,974 156.75 330 350 10 LGO 1216 2.65 330,263 0.246 80.979 2.096 2.66,835 0.160% 1,758,956 0.004% 43,974 156.75 330 350 10 LGO 1216 2.65 330,263 0.246 80.979 2.096 2.66,835 0.160% 1,758,956 0.004% 43,974 156.75 330 350 10 LGO 1216 2.65 330,263 0.246 80.979 2.096 2.66,835 0.160% 1,758,956 0.004% 43,974 156.75 330 350 10 LGO 1216 2.65 330,263 0.046 0.046 1.046 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000																
10   10   10   10   10   10   10   10		ļ				700 100	0.55	400 700	0000	740 500	0.070*	1 222 200	0.003*	57 617		\$3,694,76
DAULATIVE TOTAL  WST  23,874,008  0.101  23,874,008  0.101  23,874,008  0.101  23,874,008  0.101  24,156,202  0.028  13,866,750  0.0038  1,443,172  12,58  180,00  10,000  10,	350	10	WST	1217	2.65	798,498	0.155	123,767	0.935	740,396	0.070%	1,232,269	0.005%	32,012	€4.02	
DAULATIVE TOTAL  WST  23,874,008  0.101  23,874,008  0.101  23,874,008  0.101  23,874,008  0.101  24,156,202  0.028  13,866,750  0.0038  1,443,172  12,58  180,00  10,000  10,		<del></del>	MET	<del> </del>	<del> </del>	708 409	0.155	123 767	0.935	746 596	0.070%	1.232.269	0.003%	52,812	14.63	13,694,76
10   10   10   10   10   10   10   10				+		23.874.00B	0.101									\$61,494,01
360 10 LGO 1221 2.65 973,341 0.266 258,909 0.807 785,485 0.020% 429,469 0.001% 21,459 55.00 54. 350 10 LGD 1223 2.65 662,019 0.293 139,972 0.797 52,7679 0.020% 29,1900 0.001% 53,300 54.34 33. 350 10 LGD 1216 2.65 330,243 0.744 60,579 2.066 692,650 0.465 246,635 0.160% 1,759,595 0.004% 43,974 36.57 33. 350 10 LGD 1216 2.65 330,243 0.744 60,579 2.066 692,650 0.120% 87,2673 0.001% 7,261 57.68 35.0 10 LGD 1219 2.65 546,686 0.26 159,771 2.486 1,403,809 0.120% 41,409,001 0.007% 24,689 581 45. 350 10 LGD 957 2.65 446,666 0.26 159,771 2.486 1,403,809 0.120% 1,403,901 0.007% 24,689 581 45. 350 10 LGD 1220 2.65 533,190 0.357 100,357 0.823 488,622 0.100% 1,175,969 0.003% 35,655 587 34. 350 10 LGD 1220 2.65 533,190 0.357 100,357 0.823 488,622 0.100% 1,175,959 0.003% 35,655 587 34. 350 10 LGD 1199 2.65 1,446,200 0.302 557,554 2.006 3,703,490 0.130% 5,781,230 0.003% 35,655 587 34. 350 10 LGD 1220 2.65 1,446,200 0.302 557,554 2.006 3,703,490 0.130% 5,781,230 0.003% 35,655 587 34. 350 10 LGD 1590 2.65 1,446,200 0.302 557,554 2.006 3,703,490 0.130% 5,781,230 0.003% 35,655 587 34. 350 10 LGD 5,855,015 0.273 1,599,911 3,399 8,015,107 0.100% 1,288,902 0.003% 414,400 97,44 143,144 144,400 97,444 143,144 144,400 97,444 143,144 144,400 97,444 143,144 144,400 97,444 143,144 144,400 97,444 143,144 144,400 97,444 143,144 144,400 97,444 143,144 144,400 97,444 143,144 144,400 97,444 143,144 144,400 97,444 143,144 144,400 97,444 143,144 144,14	OMOUNTIVE TOTAL	+	117.51	1		15,071,000		21-1-1-1-1		3,1,3,1,3,1	1					
350 10 LGO 1221 2 65 973,341 0 266 258,909 0 807 785,485 0 000% 429,190 0 001% 521,455 5500 34 300 10 LGO 1223 2 65 662,019 0 263 193,972 0 797 527,629 0 020% 291,900 0 004% 58,380 \$5.43 \$3.3 30 10 LGO 956 2 65 496,656 0 128 63,629 0 450 246,855 0 160% 1,758,956 0 004% 43,974 365.77 \$3.3 300 10 LGO 1218 2 65 300,243 0 744 60,579 2 006 692,850 0 120% 17,758,956 0 004% 43,974 365.77 \$3.3 300 10 LGO 1219 2 65 544,666 0 267 150,771 2 486 1,403,809 0 120% 1,493,901 0 007% 42,869 \$814 \$44 \$3.5 30 10 LGO 1220 2 65 533,189 0 367 190,352 0 823 436,822 0 100% 1,175,499 0 003% 35,265 \$46,74 \$40		<del> </del>	-	1												
350 10 LGD 1221 2.65 673,341 0.266 2.556,900 0.807 765,486 0.000% 4.29,169 0.001% 21,456 55.00 54.353 350 10 LGD 1223 2.65 662,019 0.205 193,972 0.797 527,679 0.000% 29,900 0.004% 4.39,74 56,340 53.00 30 10 LGD 1218 2.65 300,243 0.744 60,579 2.086 672,630 0.120% 0.120% 0.004% 4.39,74 56,57 53.350 10 LGD 1218 2.65 300,243 0.744 60,579 2.086 672,850 0.120% 0.120% 0.130% 7,261 37.08 52 53.00 10 LGD 1218 2.65 300,243 0.744 60,579 2.086 672,850 0.120% 0.120% 0.130% 7,261 37.08 52 53.00 10 LGD 1210 2.65 544,666 0.266 10.266 10.20% 0.120% 0.120% 1.49,300 10.002% 21,858 58 14 54 54 53.00 10 LGD 957 2.65 446,666 0.266 10.266 0.004% 0.444 216,166 0.160% 1.575,565 0.002% 19,895 58 15 53.00 10 LGD 1220 2.65 530,3190 0.307 100,357 100,352 0.823 438,822 0.100% 1,175,499 0.003% 30,265 58 67 54 54 50 50 50 50 50 50 50 50 50 50 50 50 50		1		1												
\$\frac{\text{XO}}{\text{30}}\$\$ 10 \( \text{LCD}{\text{12}} \) 2 \( 25 \) 662\( \text{0.19} \) 0.295\( 25 \) 682\( \text{0.19} \) 0.295\( 25 \) 682\( 65 \) 692\( 65 \) 682\( 65 \) 692\( 65 \) 682\( 6																
300 10 LGD 956 265 498,656 0128 63,028 0.495 246,835 0.160% 1,759,565 0.004% 43,974 36.57 33 300 10 LGD 1218 265 330,243 0.244 80,579 2.098 692,650 0.120% 873,673 0.001% 7,261 37.68 32 330 10 LGD 1219 265 546,666 0.267 150,771 2.486 1,403,609 0.120% 1493,001 0.007% 24,689 35 14 34 330 10 LGD 1220 2.65 344,666 0.267 150,771 2.486 1,403,609 0.120% 1,939,001 0.007% 24,689 35 14 34 330 10 LGD 1220 2.65 344,666 0.267 150,771 2.486 1,403,609 0.120% 1,755,565 0.007% 19,695 35 15 33 350 10 LGD 1220 2.65 353,198 0.367 100,946 0.464 216,186 0.160% 1,755,565 0.007% 19,695 35 15 33 350 10 LGD 1199 2.65 1,846,206 0.302 557,554 2.006 3,703,490 0.130% 3,291,238 0.005% 203,509 36 87 346 350 10 LGD 1199 2.65 1,846,206 0.302 557,554 2.006 3,703,490 0.130% 3,291,238 0.005% 203,509 36 87 346 350 10 LGD 1199 2.65 1,846,206 0.302 557,554 2.006 3,703,490 0.130% 3,291,238 0.005% 203,509 36 87 346 350 10 LGD 1199 2.65 1,846,206 0.302 557,554 2.006 3,703,490 0.130% 3,291,238 0.005% 203,509 36 87 346 350 10 LGD 1199 2.65 1,846,206 0.302 557,554 2.006 3,703,490 0.130% 3,291,238 0.005% 203,509 36 87 346 350 10 LGD 1199 2.65 1,846,206 0.002 1,969,309,694 1.484 53,718,291 0.103% 84,097,079 0.004% 2,871,907 97,38 92,224,492 10.202 9,693,694 1.484 53,718,291 0.103% 84,097,079 0.004% 2,871,907 97,38 92,224,492 10.202 9,693,694 1.484 53,718,291 0.103% 84,097,079 0.004% 2,871,907 97,38 92,224,492 10.202 9,693,694 1.484 53,718,291 0.103% 84,097,079 0.004% 2,871,907 97,38 92,224,492 10.202 9,693,694 1.184 53,718,291 0.103% 84,097,079 0.004% 2,871,907 97,38 92,224 92,400 0.000 90,00																\$4,672,5
350   10   GD   1218   2.65   330 243   0.244   80.379   2.098   692,850   0.120%   673,673   0.001%   7,281   \$7.68   \$2.585   \$4.586   0.267   150,771   2.468   1,403,809   0.120%   1,403,809   0.120%   1,403,809   0.002%   2.4689   351   4.585   4.586   3.467   150,771   2.468   1,403,809   0.120%																\$3,600,01 \$3,279,30
350 10 GO 1219 2.65 564,686 0.26 150,771 2.496 1,403,699 0.20% 1,403,001 0.007% 2.499 38 1.4 54 350 10 GD 957 2.63 446,666 0.226 100,946 0.464 216,186 0.160% 1,575,585 0.002% 19,695 38 15 53 350 10 GD 1220 2.65 533,196 0.357 180,352 0.623 48 6.22 0.100% 1,755,990 0.003% 32,855 58 67 54 350 10 GD 1199 2.65 1,846,206 0.307 557,554 2.006 3,703,490 0.130% 3,291,330 0.005% 203,908 58 67 54  SUBTOTAL GO 5,865,015 0.273 1,999,911 1,399 8,015,107 0.100% 12,869,902 0.003% 414,400 97.44 843,2  SUBMERT TOYAL GO 36,944,921 0.202 9,993,994 1,454 53,718,291 0.103% 84,097,079 0.004% 2,871,907 97.38 9272,4  SUBMERT TOYAL GO 36,944,921 0.202 9,993,994 1,454 53,718,291 0.103% 84,097,079 0.004% 2,871,907 97.38 9272,4  SUBMERT TOYAL GO 36,944,921 0.202 9,993,994 1,454 53,718,291 0.103% 84,097,079 0.004% 2,871,907 97.38 9272,4  SUBMERT TOYAL GO 36,944,921 0.202 9,993,994 1,454 53,718,291 0.103% 84,097,079 0.004% 2,871,907 97.38 9272,4  SUBMERT TOYAL GO 36,944,921 0.202 9,993,994 1,454 53,718,291 0.103% 84,097,079 0.004% 2,871,907 97.38 9272,4  SUBMERT TOYAL GO 42,000 42,																\$2,540,2
350 10 LGD 957 2.65 446,666 0.226 100.946 0.464 2.16,186 0.180% 1,575,665 0.002% 19.895 \$4.15 \$5. 350 10 LGD 1120 2.65 333,196 0.357 160,352 0.823 436,822 0.100% 1,175,499 0.003% 35,265 \$8.67 \$4. 350 10 LGD 1199 2.65 1,486,200 0.307 557,554 2.003 3,703,490 0.130% 5,291,236 0.005% 203,509 \$8.75 \$4.  SUBTOTAL LGD 5,865,016 0.273 1,596,911 1,389 8,015,107 0.100% 12,889,902 0.003% 414,400 97,44 \$43,504 \$1.0000 \$1.0000 \$1.0000 \$1.0000 \$1.0000 \$1.0000 \$1.0000 \$1.0000 \$1.0000 \$1.0000 \$1.0000 \$1.0000 \$1.0000 \$1.0000 \$1.0000 \$1.0000 \$1.0																\$4,600,61
350 10 GG 1220 2.65 533,196 0.357 150,352 0.623 436,622 0.100% 1,175,499 0.003% 35,265 \$8.67 \$4.  350 10 LGO 1199 2.65 1,846,206 0.302 557,554 2.006 3,703,490 0.130% 5,291,236 0.005% 203,509 \$8.67 \$16.  SUBTOTAL LGO 5,855,015 0.273 1,599,911 1,399 8,015,107 0.100% 12,889,902 0.003% 414,460 97,44 \$43,215  ELMARATIVE YOTAL LGO 36,944,921 0.262 9,893,694 1.654 53,718,291 0.103% 84,097,079 0.004% 2,871,907 97,396 92,724																\$3,640,21
350 10 LGO 1199 2.65 1,846,206 0.302 557,554 2.006 3,703,490 0.130% 5,291,238 0.005% 203,509 \$8.87 \$16  SUBTOTAL LGO 5,855,015 0.273 1,590,911 1.369 8,015,107 0.100% 12,889,902 0.003% 414,460 97,44 843,1  SUMARIATIVE TOTAL LGO 36,944,921 0.202 9,693,694 1.454 53,718,291 0.103% 84,097,079 0.004% 2,871,907 97.38 9272,4  1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0																\$4,626,7
200 36,944,921 0.292 9,093,694 1.454 53,718,291 0.103% 84,097,079 0.004% 2,071,907 07.38 9272,4	350			1199	2.65	1,846,206	0.302	557,554	2.006	3,703,490	0.130%	5,291,236	0.005%	203,509	\$8 87	\$16,394,20
200 36,944,921 0.292 9,093,694 1.454 53,718,291 0.103% 84,097,079 0.004% 2,071,907 07.38 9272,4				I												
90.00 90.00		<del></del>		-												943,554,03
\$0.00   \$0.00	CUMULATIVE TOTAL	<del></del>	LGD		<del> </del>	36,944,921	0.262	9,093,094	1,404	23,718,291	0.103%	84,097,079	0.005	2,8/1,90/	₩7.36	<b>\$272,613,97</b>
\$0.00   \$0.00		<del>}</del>	<del></del>	<del></del>	+	t	1									
\$0.00   \$0.00		1		1	1											
\$0.00   \$0.00													<del></del>			
\$\\\ \begin{array}{cccccccccccccccccccccccccccccccccccc					·		ļ	ļ		<del> </del>	<del></del>	<del> </del> -	<del> </del>	<del>                                     </del>		
90.00   90.00		<del></del>		· <del> </del>	.}	<del> </del>	<del> </del>			<del> </del>	<del></del>	<del> </del>	<del> </del>	<del></del>		
90.00 90.00		<del></del>	<del> </del>	+	<del>                                     </del>	<del> </del>	<del> </del> -	<del></del>	<del> </del>	<del> </del>	<del> </del>	<del> </del>	<del> </del>			
80,00   80,00		<del></del>	<del> </del>	<del> </del>		<del>                                     </del>	<del> </del>									
90.00  350 10 HGD 944 2.65 309,597 0.386 119,504 1.561 483,281 0.130% 887,306 0.001% 6.625 \$10.13 \$3  350 10 HGD 960 2.65 2.694,173 0.37 996,844 1.8 4,849,511 0.160% 9,503,403 0.013% 772,151 \$10.75 \$28  350 10 HGD 1215 2.65 742,301 0.713 529,261 4.262 3,163,688 0.130% 2,127,440 0.009% 147,264 \$15.97 \$11  AUBTOTAL HGD 3,746,071 0.439 1,645,609 2.268 8,496,479 0.152% 12,518,149 0.011% 920,261 011.74 \$43  SUMMERATIVE YOTAL HGD 47,579,380 0.648 30,720,048 4.173 187,728,548 0.217% 226,843,289 0.006% 8,625,465 017.33 0821,			<del>                                     </del>	1												
350 10 HGD 944 2.65 309,597 0.386 119,504 1.561 483,281 0.130% 887,306 0.001% 6.825 \$10.13 \$3 350 10 HGD 960 2.65 2.694,173 0.37 996,844 1.8 4,849,511 0.160% 9.503,403 0.013% 772,151 \$10.75 \$28 350 10 HGD 1215 2.65 742,301 0.713 529,261 4.262 3,163,688 0.130% 2,127,440 0.009% 147,284 \$15.97 \$11  WBTOTAL HGD 3,746,071 0.439 1,645,609 2.268 8,496,479 0.152% 12,518,149 0.011% 926,261 \$11.74 \$43  SUMBLIATIVE TOTAL HGD 47,379,380 0.649 30,720,048 4.173 187,729,548 0.217% 226,863,289 0.006% 8,625,465 917.33 9821,		1	1			1										
350 10 HGD 944 2.65 309,597 0.386 119,504 1.561 483,281 0.130% 887,306 0.001% 6.825 \$10.13 \$3 350 10 HGD 960 2.65 2.694,173 0.37 996,844 1.8 4,849,511 0.160% 9.503,403 0.013% 772,151 \$10.75 \$28 350 10 HGD 1215 2.65 742,301 0.713 529,261 4.262 3,163,688 0.130% 2,127,440 0.009% 147,284 \$15.97 \$11  WBTOTAL HGD 3,746,071 0.439 1,846,609 2.268 8,496,479 0.152% 12,518,149 0.011% 9.26,261 911,74 \$43  SMALLA TIVE TOTAL HGD 47,379,380 0.449 30,720,048 4.173 187,728,548 0.217% 226,843,289 0.006% 8,625,465 917,33 9821,											1					
350 10 HGD 944 2.65 309,597 0.386 119,504 1.561 483,281 0.130% 887,306 0.001% 6,825 \$10.13 \$3 350 10 HGD 960 2.65 2,694,173 0.37 996,844 1.8 4,849,511 0.160% 9,503,403 0.013% 772,151 \$10.75 \$28 350 10 HGD 1215 2.65 742,301 0.713 529,261 4.262 3,163,688 0.130% 2,127,440 0.009% 147,284 \$15.97 \$11  AUBTOTAL HGD 3,746,071 0.439 1,645,609 2.268 8,496,479 0.152% 12,518,149 0.011% 9.26,261 \$11.74 \$43  SUMBLIANTIVE YOTAL HGD 47,379,390 0.648 30,720,048 4.173 197,729,548 0.217% 226,863,289 0.006% 8,625,665 \$17.33 \$821,							<b></b>				<del> </del>		<del> </del>			
350 10 HGO 960 2.65 2.694,173 0.37 996,844 1.8 4,849,511 0.160% 9,503,400 0.013% 772,151 \$10.75 \$28 350 10 HGO 1215 2.65 742,301 0.713 529,261 4.262 3,163,688 0.130% 2,127,440 0.009% 147,284 \$15.97 \$11  UBTOTAL HGO 3,746,071 0.439 1,646,609 2.268 8,496,479 0.152% 12,518,149 0.011% 928,261 \$11.74 \$43  UMAILLATIVE TOTAL HGO 47,579,380 0.449 30,720,048 4,173 197,728,548 0.217% 226,843,289 0.006% 8,625,465 417.33 4821,	340	+	Hen	-	266	200 507	0 396	110 504	1501	483 281	0 130%	887 30	0.001%	8.625		\$3,137,0
350 10 HGD 1215 265 742,301 0.713 529,261 4.262 3,163,688 0.130% 2,127,440 0.009% 147,284 \$15.97 \$11  UBTOTAL HGD 3,746,071 0.439 1,645,009 2.268 6,496,479 0.152% 12,516,149 0.011% 920,261 011.74 \$43  UMANUALITYE TOTAL HGO 47,379,380 0.448 30,720,048 4.173 197,728,548 0.217% 226,843,289 0.006% 8,625,465 017.33 0821,																\$28,975,3
UBTOTAL HGD 3,746,071 0.439 1,645,609 2.268 8,495,479 0.152% 12,518,149 0.011% 920,261 911.74 \$43																\$11,865,8
TUMINATIVE TOTAL HGD 47,379,390 0 649 30,720,049 4.173 197,729,548 0.217% 226,963,289 0.006% 6,625,665 617.33 6821,																
																\$43,978,3
ENCH TOTAL HGD/LGD 9,801,088 0.338 3,242,520 1.720 18,511,587 0.120% 25,408,052 0,008% 1,340,721 89.12 887,	CUMULATIVE TOTAL		HGD	-	-	47,379,390	0.640	30,720,048	4.173	197,729,548	0.217%	226,963,281	0.006%	6,625,665	417.33	4821,182,9
	ENCH TOTAL	+	MGDA GD			9 801 004	0 339	3 242 830	1 730	18 811 807	0.1209	25 409 05	0.000	1 340 231	40.12	407417
	WIGHT TOTAL	+	HODICOD	-	<del> </del>	9,001,086	0.330	3,4-4,020	1.720	10,311,567	0.120%	29,400,032	10,000	1,340,721	*****	187,532,3

							Om SEARCE		CTED TOPO						
19-12-95 9:31 AM LEVEL	BENCH	POLYGON	HOLE	DENSITY	METRIC	AU	AU	AG PPM	AG	COPPER	COPPER	MOLY	MOLY POUNDS	TOME	TOTAL
340	reuni	MA I ENALL	-	DEMONIT	10 mas	****	Givino		GRAMS	*	POUNDS	~	roomes	10100	AVENE
340	10	UDF		2 65	1,951,819	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
USTOTAL	<del>                                     </del>	UDF	<del> </del> -		1,951,819 8,589,152									+	
CUMULATIVE TOTAL	<del></del>	004	<del>  </del>		0,005,102	<del></del>									
			1											●0.00	\$4
	1													10.00	<u> </u>
														0.00	
														<b>90.00</b>	<u>*</u>
	<b></b>													\$0.00	
	<del></del>	<del> </del>												10.00	<u> </u>
	<del> </del>		<del>  </del>											10.00	\$
	+	<del> </del>	1											\$0.00	\$4
	<del> </del>	<del></del>	1												
SUBTOTAL		WST				0.000		0.000	0	0.000%		0.000%	0		•(
CUMULATIVE TOTAL		WST			23,874,008	0.101	2,415,822	1.012	24,155,282	0.026%	13,866,750	0.003%	1,443,172	\$2.58	\$61,494,017
	-		<b></b>					<del></del>		ļ				●0.00	
	<del></del>	<del> </del>	-											●0.00	<u>s</u>
	1	<del> </del>												●0.00	34
														\$0.00	2
340		LGD	1221	2.65	929,501		220,292		659,016		1,024,598		20,492	\$5.34	\$4,968,023
340		LGD	1223		724,887		211,667	0.677	490,748 936,141	0 020%	1,622,229	0.002%	31,962 36,050	\$5.39 \$6.43	\$3,911,094 \$5,257,513
340		LGD	1217	2 65 2 65	817,590 1,968,132		188,048 431,021		1,846,108	0.120%	5,206,780		216,949		\$13,845,436
340 340		LGD	1215				219,457		1,704,601	0.070%	1,175,949		50,396		\$5,373,815
340		LGD	1218		339,451		79 092		735,251			0.001%	7,484	\$7 52	\$2,556,09
340		LGO	956						429,685	0.160%	1,916,142	0 000%	0	\$9 55	\$5,188,80
SUBTOTAL		LGD					1,517,429		6,801,551	0.091%					141,100,76
CUMULATIVE TOTAL	<del> </del> -	red		<del> </del>	43,029,704	0.261	11,211,123	1,406	60,519,842	0.101%	96,260,430	0.003%	3,235,241	17.30	9313,914,754
														90.00	\$
			<b></b>	ļ <u>.</u>		ļ					<u> </u>	<del> </del>	<del>}</del>	\$0.00	S
	<del></del>	<del></del>	-	<del></del>			<del> </del>	<del> </del>		<del> </del>	<del> </del>	+		\$0.00	3
	+	<del> </del>	-	<del> </del>		<del> </del>		<del> </del>		<del></del>	t	<del>                                     </del>	<del> </del>	\$0.00	Š
	+	<del> </del>	1	<del> </del>	<del> </del>					<del>                                     </del>	<u> </u>	1		\$0.00	\$
	1													\$0.00	S
														\$0.00	\$
						0.55				0.1000	4 344 55	0.000	20.000	10.00	\$ 20 122 74
340		HGD	1219						1,617,963			0.002%			\$8,123,74 \$30,098,77
340 340		D HGD	960			0.352			4,126,092 201,650			0.003%			\$5,663,75
340		D HGD	1220	<del></del>	<del></del>				1,806,123			0 003%		\$13 16	\$7,316,74
340		HGD	944						974,082			0.001%			\$3,848,61
											1	1			
SUBTOTAL		HGD			4,810,773	0.395	1,903,909	1,812	8,727,908	0.155%	16,413,312	0.008%	802,905	\$11.01	\$53,051,60
CUMULATIVE TOTAL		HGD	-		52,196,153	0.625	32,623,957	3.955	206,457,456		243,376,600	0.007%	7,488,549	116.75	4874,234,82
BENCH TOTAL		HGD/LGD			10,901,555	0.314	3,421,338	1,425	15,529,459	0.119%	28,576,663	0.005%	1,226,238	18.64	994,152,41
			i			1		1	1	1	1	1			1

					ONSON SLO		m SEARCH								
19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	.VAL	TOTAL
LEVE	HEIGHT	MATERIAL	10	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	*	POUNDS	TONNE	VALUE
330															
330	10	UDF		2.65	2,161,126	O	0	0	0	0 000%	0	0 000%	0	20 00	
			-												
UBTOTAL	<del> </del>	UOF	<del>  </del>		2,161,126										
UMULATIVE TOTAL	<b></b>	UDF	1		10,750,279										·
		ļ													
	<del> </del>	<del></del>	<del>  </del>				<del>}</del>							<b>●0.00</b>	×
			1	-										10.00	\$0 \$0
			1											10.00	- SX
														10.00	SC
														\$0.00	X
330		WST WST	1202	2 65	749,533		86,196	0 621	465,460	0.080%	1,321,948		165,244	\$4 19	\$3,140,871
330		WST	1215	2.65 2.65	772,743 794,656		142,185 176,414	1.187	850,017 943,257	0.050%		0 002%	34,072 17,519		\$3,536,068 \$3,701,216
	10	14431	1223	1.03	734,636	9.222	1,0,414	1.10/	5-3,231	0000%	323,314	0 00178	17,319	-1.00	23,701,210
UBTOTAL		WST			2,316,932	0.175	404,795	0.975	2,258,734	0.053%	2,699,325	0.004%	216,835	94.48	\$10,380,176
UMULATIVE TOTAL	1	WST			26,180,940	0.108	2,820,617		26,414,016		16,566,075				971,874,193
	1	1													
														●0.00	\$(
														\$0.00	\$(
														●0.00	\$1
330		LGO	956	2 65	603,319		33,786	0.2	120,664	0.160%	2,128,143		13,301		\$3,230,007
330		LGD	1217	2 65	858,176		185,368		878,772	0.090%	1,702,758		37,839		\$5,302,46
330	10	LGD	1220		582,660		172,467		561,684	0 080%	1,027,635		77,073		\$4,181,390
330		LGD	1221	2.65	883,381	0 313	276,498	1,181	1,043,274		1,363,264		19,475		\$6,379,69
330		LGD	1199		1,963,438		492,823	1.185	2,326,674	0.110%	4,761,499		129,859		\$14,388,336
330		LGD	1219		679,428		200,431	1 379	936,931		1,497,880		14,979		\$5,301,400 \$3,142,320
330		LGD	1218		352,753		87,483 769,041		1,261,093 1,836,333	0.150%	1,166,530 8,694,585	0.001%	7,777 217,365		\$23,638,41
330	11	reo	960	2.65	2,464,876	0.312	709,041	0.745	1,030,333	0.160%	8,084,363	0.00= %	217,30	80.30	23,000,41
SUBTOTAL	+	LGD	<del></del>	<del></del>	8,388,032	0.264	2,217,896	1.009	9,965,424	0.121%	22,342,292	0.003%	517,667	<b>\$7.82</b>	165,564,02
CUMPLATIVE TOTAL	-	LGD	+				13,429,019		69,485,266		118,602,722				0379,478,78
						-									
	<del>                                     </del>	<del> </del>	+	<del> </del>						<del> </del>		<del>}</del>			
														#0.00	\$
	<del></del>	<del> </del>	ļ											\$0.00	s
	+	<del> </del>		<del> </del>						<del> </del>		ļ		\$0.00	s
	+	<del> </del>	+									+		<b>●0.00</b>	
	<del> </del>	1	1			<u> </u>		-		<del> </del>		<del>                                     </del>		●0.00	
		1	1									I		\$0.00	
														\$0.00	
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		1												\$0.00	
												<b>↓</b>		●0.00	
	J	1		<b></b>		1				-				\$0.00	
330	10	HGD	957	2 65	697,176	0.491	342,314	0.49	341,616	0.160%	2,459,214	0.002%	30,74	\$12.41	\$8,653,57
SUBTOTAL		HGD			697,176									912,41	\$8,653,57
CUMULATIVE TOTAL		HGD		-	52,893,329	0.623	32,966,271	3.910	206,799,072	0.211%	245,835,814	0.006%	7,519,301	116.69	4002,000,20
BENCH TOTAL	1	HGD/LGD	<del> </del>		9,085,208	0.282	2,560,210	1.024	9,307,040	0.124%	24,801,807	0.003%	548,40	98.17	874,217,60
												L			
JAM, BENCH TOTAL		HGD/LGD			104,311,065	0.445	46,395,289	2.049	276,284,338	0.158%	364,438,536	0.005%	11 272 21	1 412 10	11 262 366 9

CONCENTRATED IN COUNTRY OF THE PROPERTY OF THE

					ONSON SLO		m SEARCH					**********			
19-12-95 9:31 AM LEVEL	BENCH	POLYGON	HOLE	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER	COPPER	MOLY	MOLY	TONNE	TOTAL
320				000.11		*****	Green and		Uning		700403		rooms		7,100
320	10	UDF		2 65	2,418,524	0	0	0	0	0.000%	0	0 000%	- 0	\$0.00	
USTOTAL		UDF	-		2,418,524		<del></del> +	<del></del>							
UMULATIVE TOTAL	<del>                                     </del>	UDF			13,168,803										
														\$0.00	\$0
			-	<b></b>										\$0.00	\$0 \$0
	<del> </del>			<b>}</b>										90.00	\$0
	<del> </del>		-	<del> </del>										\$0.00	\$0
	1		1											●0.00	\$0
320	10	WST	1215	2.65	781,054	0 135	105,442	0 647	505,342	0.010%		0 001%	17,219	\$2 59	\$2,021,929
320	10	WST	1221	2.65	803,596		133,397	0.607	487,783	0.030%		0.001%	17,716	23 63	\$2,916,693
320	10	WST	1217	2.65	670,683	0 163	141,921	1.13	983,872	0.060%	1,151,715	0.003%	57,586	\$4 52	\$3,938,190
		11000		<del> </del>	3 455 355		300 74.	0.00	1 074 007	0.0345	1 055 305	0.003	93 831	93.62	48,676,613
UBTOTAL	+	WST	·	<del> </del>	2,455,333 28,646,273		380,761	0.805	1,976,997	0.034%	1,855,395		92,521	\$3.02 \$2.82	180,751,006
OMOUNTE TOTAL		1		<del>                                     </del>	20,040,273	J. 1 14	3,201,377	0.331	20,001,012	U.U25 N	10,421,470	3,000 %	.,, .,,,,,,,	*****	
														●0.00	\$0
														●0.00	\$0
320	<del> </del>	LGD	1223	2.65	825,517				1.640.300	0.000		0.0018		90.00 \$5 13	\$4,236,857
320		LGD	1202		809,447	0 189	156,023 108,466	1.999 0.738	1,650,209 597,372	0.060%	1,091,971	0.001%	18,200 303,369	\$5.35	\$4,329,271
320		LGD	1203		86,704		13,439	0 836	72,484			0.002%	3,823	\$5.70	\$494.877
320		LGD	1199		2,042,146		514,621	0.685	1,398,870		5,402,587		90,043	\$7.51	\$15,336,087
320		LGD	956		717,083		147,002	0.2	143,417		2,529,433		15,809	\$7.75	\$5,557,136
320		LGD	1219		705,898		212,475	2.087	1,473,209		1,400,613		31,125	\$7.77	\$5,491,475
320		LGD	957	2.65	738,390	0.26	191,981	0.6	443,034		2,604,592		32,557	\$8 72	\$6,440,269
320	10	red	1220	2.65	603,084	0.364	219,523	1.068	644,094	0.100%	1,329,571	0.006%	79,774	\$8.84	\$5,333,586
	<del></del>	1	<del></del>	<del></del>	4 4 20 200	0.000						0.0040	674 700	47.33	447 310 660
SUBTOTAL		160	<del></del>	<del>  </del>	6,528,269				75,907,955		16,632,006		674,700 4,327,608	97.23 97.36	947,219,559 9420,698,339
SUMULATIVE TOTAL	<b></b>	LGD	1		87,940,000	0.239	14,992,546	1.310	70,907,900	0,100%	130,134,720	0.003 %	4,327,000	77.30	V420,030,333
	-		-											90.00	×
	+	+	<del> </del>											10.00	\$4
		1	1											\$0.00	\$
														♦0.00	\$
														●0.00	
		1												10.00	
	+	<del> </del>	+	<b></b>										90.00	
	-	<del> </del>	+	-									<del> </del>	\$0.00	\$
			1					1				1		●0.00	S
														\$0.00	s
200	1	1										1		\$0.00	\$
320 320		HGD	960									0 019%			\$32,646,97
320	<del></del> "	7700	1218	2.65	364,801	0.4/1	1/1,621	4.084	1,489,848	0.250%	2,010,620	0.001%	8,042	\$15 35	\$5,600,92
UBTOTAL	<del> </del>	HGD	<del> </del>	<del> </del>	2 860 037	0.496	1,419,439	3 037	8,686,109	0.171%	10 812 294	0.017%	1,053,242	413.32	\$38,250,90
CUMULATIVE TOTAL	1	HGD	1	1					215,485,181		256,648,111	0.017%	2 572 861	418 97	<b>#921,139,10</b>
								7,000				J	0,072,001	1	
BENCH TOTAL		HGD/LGD			9,388,307	0.318	2,982,969	1.609	15,108,798	0,132%	27,344,302	0.008%	1,627,941	19.10	185,470,46
UM. BENCH TOTAL	+	HGD/LGD	+	<del> </del>	113,699,371	0.474	40 370 360	2 542	201 202 120	0.1500	201 200 000		t	<del> </del>	81,347,837,44

					DNSON SLO		m SEARCH	1 1400,11- 5							
19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	•VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID I	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	%	POUNDS	TONNE	VALUE
210															
310	10	UDF		2.65	2,521,913	0	0	- 0	0	0.000%	Ö	0.000%	0	\$0.00	
310		-			2,521,615										
BTOTAL		UDF			2,521,913										
MULATIVE TOTAL	<del></del>	UDF			15,690,716										
	<del> </del>													10.00	
														●0.00	
														\$0.00	
				<b></b>										\$0.00	
	<del> </del>		<del> </del>	<del> </del>										10.00	
310	10	WST	1217	2.65	950,363	0 124	117,845	0.799	759,340	0.020%		0.002%	41,904	\$2 72	\$2,585,
310		WST	1221	2.65	1,230,647		217,825	0.58	713,775	0.020%		0 002%	54,262	\$3 52	\$4,337,
310		WST	1202	2.65	893,109		90,204	0.774	691,266	0 100%	1,968,966	0 011%	216,586	\$4.55	\$4,060
			<del></del>	<del>  </del>	3,074,118	0.130	425,873	0.704	2,164,381	0.043%	2,930,625	0.005%	312,752	93.57	110,987
BTOTAL	<del> </del>	WST	<del> </del>	<del> </del>	31,720,392			0.963	30,555,394	0.031%			2,065,280		991,738,
MULATIVE TOTAL	<del> </del>	1431	<del> </del>	<del> </del>		9.1.7	3,027,20	-0.200							
	1	<del></del>	1											●0.00	
310		LGD	1200		483,686		78,841	0.6	290,211	0 090%		0 003%	31,990		\$2,531 \$6,911
310		LGD	1223		1,168,645		211,525	2.379	2,780,208	0.090%		0.001%	25,764 17,393	\$7 12	\$5,624
310		LGD	1215		788,941	0 297	234,315	4 437	3,500,531 1,089,725			0 002%	31,343		\$5,340
310		LGD	1220		710,845		207,567 422,553	1 533	2,443,599		4,332,874		144,429		\$12,748
310		LGD	1199		1,637,601 878,468		203,804	2 556	2 245 363		2,517,693		19,367	\$7.87	\$6,918
310 310		LGO	1201		14,340		3,413	3.454	49,532		44,261		2,845	\$8.43	\$121
310		LGO	948		42,772		9,966	1.523	65,141	0 160%	150,872		3,772	\$8 49	\$363
310		LGD	947		5,117	0 24	1,228	2 039	10,433	0 160%	18,048	0.007%	790		\$44
310		LGD	949	2.65	381,139	0.28	106,719	3.026	1,153,326	0.160%	1,344,426	0.006%	50,416	\$9 57	23,650
		1.60	<del></del>	<del> </del>	6,111,752	0.242	1,479,930	2 230	13,628,068	0.104%	13,966,746	0.002%	328,109	87.24	144,253,
IBTOTAL	<del></del>	LGD	+	<del> </del>			16,472,479				149,101,474				8470,952
THE TOTAL			-												
				<u> </u>										20.00	
												<del></del>		90.00	
				<del> </del>										10.00	
		<del> </del>		<del></del>							<del></del> _	<del> </del>	<b></b>	10.00	
	<del> </del>	<del> </del>	+	<del> </del>		<del> </del>						1		\$0.00	
	+	<del> </del>	<del></del>	1										●0.00	
	+	<del> </del>	<del></del>	<del> </del>										●0.00	
	<del> </del>			1										\$0.00	
										<u> </u>	ļ	<del> </del>	<del> </del>	90.00	
				<b></b>							ļ <u> </u>		<del> </del>	90.00 80.00	ļ
					200 210	0327	145,627	0 829	320,224	0.160%	1 267 44	3 0 004%	34.064		\$4,11
310		OHGD	120			03//	118 230					3 0.003%			
310 310		O HGD	121			0.472	1,183,664					0 0.019%		\$12.92	
															446.55
UBTOTAL		HGD			3,316,718	0.430	1,447,721	3.853	12,778,925	0.166%	12,164,80	6 0.015%	1,112,61	012.46	\$41,29 0962,431
UMULATIVE TOTAL		HGD	-		59,070,082	0.607	30,833,432	3.854	228,264,106	0.200%	200,612,91	U.00/%	7,000,100	V10.29	1502,730
ENCH TOTAL		HGD/LGD			9,428,458	0.311	2,927,652	2.801	26,406,993	0.126%	26,131,65	2 0.007%	1,440,72	1 99.07	185,550
					1	1				1		i	14,340,88		1

					ONSON SLO		m SEARCH								
19-12-95 9:31 AM LEVEL	BENCH HEIGHT	POLYGON MATERIAL	HOLE	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER	COPPER POUNDS	MOLY %	MOLY POUNDS	TONNE	TOTAL VALUE
300			-												
300	10	UDF	<del>   </del>	2 65	2,728,445	0		0	0	0 000%		0.000%	0	\$0.00	
		-		•	2,720,410							0000			
USTOTAL		UDF			2,728,445										
UMULATIVE TOTAL		UDF			18,419,161										
	<del> </del>	<del> </del>		<del></del>										90.00	\$0
				<del></del>					<del></del>					\$0.00	- si
	1		1					. 1						\$0.00	
														●0.00	\$
														10.00	<u> </u>
100		WST	1221	2.65	1,242,244	O OBB	106,833	0 215	267,082	0 010%	273.866	0 001%	27,347	\$170	\$2,118,967
300		WST	1215	2.65	824,362	0 15	123,654	1.1	906,798	0.040%		0.001%	18,174	\$3.75	\$3,096,556
300		WST	1223	2.65	1,201,577		248,727	1.437	1,726,667	0.040%	1,059,609		26,490	\$4.74	\$5,703,900
															410.010.435
SUBTOTAL		WST			3,268,183		479,214	0.668	2,900,547	0.029%	2,060,438	0.001%	72,051	43.34 42.93	\$10,919,425 \$102,657,921
MALATIVE TOTAL		WST			34,988,575	0.117	4,106,464	0.958	33,455,941	0.030%	23,412,532	0.00376	2,137,331	44.83	4104,057,321
		ļ		<b> </b>										●0.00	\$
300	1	LGO	1219	2.65	909,949	0.193	175,620	0.628	753,438	0.070%	1,404,264	0.002%	40, 122	\$5 21	\$4,745,050
300		LGO	1202		992,852		148,928	0 522	518,269		2,407,749		437,772		\$5,518,465
300		LGO	1220		721,234		174,539	0775	558,956		1,113,033		31,807		\$4,320,84
300		LGD	1218	2.65	435,200	0.136	59,187	1.513	658,457	0.130%	1,247,285		19,189		\$2,655,69
300	10	LGD	1200		519,010		112,106	0.81	420,398	0.100%	1,144,220		45,769		\$3,325,43 \$618,96
300		LGD	1201		89,388		21,185		145,344			0 003%	5,912 1,554		\$135,48
300		LCD	947		17,619		3,383 442,875		15,435 3,249,875			0.006%	210,728		\$12,665,58
300 300		LGD	1199		1,593,076 657,098		136,019		613,073			0.000%	173,838		\$5,581,53
300		LGD	948		48,667		13,675		77,040			D 004%	4,292		\$451,43
SUBTOTAL		LGD					1,287,518		7,010,286				970,976		940,018,481
CUMULATIVE TOTAL		LGO	-		70,041,851	0.254	17,759,997	1.378	96,546,308	0.106%	163,319,823	0.004%	5,626,694	<b>♦7.30</b>	\$510,970,71s
														<b>0.00</b>	
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	+	<del> </del>	<del> </del>	<b> </b>							·			00.00	
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	+	+	+			<del> </del>	<del> </del>						<u> </u>	●0.00	
300	11	HGD	949	2.65	413,741	0.342	141,499					0.008%			\$4,366,65
300		HGD	960		2,481,755	0 361	888,693	2.973				0.044%			\$26,754,79
300	1	HGD	1217	2.65	947,893	0.477	452,145	2.029	1,923,275	0 150%	3,134,616	0 001%	20,897	\$12.24	\$11,611,68
				1		ļ			10.000.000		12.022.00	10 0000	240: 05:	1	\$42,733,33
SUBTOTAL		HGD			3,823,388	0.388	1,482,338	2.736	10,465,966	0.158%	13,277,616	0.029%	12 187 013	416.00	41,005,169,18
CUMULATIVE TOTAL		HGD		<del></del>	6Z,893,470	0.583	3/,310,/69	3./90	236,720,093	0.203%	262,050,831	0.0007	12,107,017	7,0.00	1,000,100,10
BENCH TOTAL	-	HGD/LGD	-		9,807,482	0.282	2,769,855	1,781	17,466,272	0.127%	27,495,964	0.016%	3,452,826	18.44	482,751,81
CUM, BENCH TOTAL	<del></del>	HGD/LGD	-	I	132,935,321						445,410,354				

					ONSON SLO		m SEARCH								
19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	SVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	*	POUNDS	TONNE	VALUE
290															
290	10	UDF	1	2 65	2,668,101			0		0 000%		0 000%		\$0.00	
UBTOTAL		UDF			2,868,101										
UMULATIVE TOTAL	<del> </del>	UDF	<del> </del>		21,297,261										
			<del> </del>											●0.00	\$0
	-		1											#0.00	\$0
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														\$0.00	\$ \$
														0.00	<u>\$</u>
290	10	wst	1221	2 65	1,589,687	0.089	141,482	0.329	523,007	0.020%	700,931	0.001%	35,047	\$2.05	\$3,266,256
290		wst	1202	2 65	1,100,307		95,727	1	1,100,307	0.070%	1,696,031	0 023%	557,924	\$3.54	\$3,903,69
290		wst	1201	2.65	169,155		19,115	1.297	219,394	0.070%	261,046	0 002%	7,458	\$400	\$661,930
SUBTOTAL		WST	-	<del></del>	2,859,149	0.090	256,323	0.844	1,842,708	0.042%	2,660,008	0.010%	600,429	#2.75	17,852,086
CUMULATIVE TOTAL	<del></del>	WST	+		37,847,724				35,298,649	0.031%	26,072,540		2,737,760		8110,510,007
omooning rome		112.				<u> </u>		- 0.0.00	33,133,13	2,44					
														00.00	\$X
														●0.00	\$
	<del> </del>	ļ <u>.</u>	<del> </del> -	<u> </u>										10.00	\$
200	100	1.60	1202	2.65	970 915	0 110	100 750	0.503	438,020	0.110%	2,111,799	0.018%	307,171	\$0.00 \$5.04	\$4.399.43
290 290		LGD	1203	2.65	870,815 723,784		102,756 168,642	0.503	467,564	0.110%	1,436,102		47,870		\$4,388,430 \$4,609,740
290		LGD	1200	2 65	530,485		114,054	1 317	698,649	0.100%	1,169,519		70,171		\$3,449,590
290		LGD	1219		943,068		152 777	4 014	3,785,475	0 110%	2,287,017		62,373		\$6,148,230
290		LGD	1199	2 65	1,563,882		420,684	1.412	2,208,201	0 140%	4,826,871		206,666	\$8 49	\$13,283,996
290		LGD	1218	2 65	672,795		143,305	1.322	889,435	0.200%	2,966,516		29,665	\$9 22	\$6,208,17
290		LGD	949		453,493		125,618	3 043	1,379,981	0 160%	1,599,649	0.006%	79,982	\$9 52	\$4,323,08
SUBTOTAL		LGD					1,227,837		9,867,326	0.129%			804,099	17.37 17.30	942,411,264
CUMULATIVE TOTAL		LGD			75,800,174	0.250	18,987,833	1.404	106,413,634	0.108%	179,717,296	0.004%	6,430,792	67.30	<b>#553,381,97</b>
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	<del></del>	ļ				<del> </del>	<del> </del>			<b> </b>				\$0.00	\$
	+	<del> </del>	+	<del> </del>		<del></del>				<del> </del>				90.00	Š
	+	<del> </del>	+											\$0.00	\$
														\$0.00	9
290		HGD	948				17,280					0.010%	12,490		\$597,11
290		HGD	947			0 357	10,951	1.825			108,204		3,361		\$323,66
290		HGD	960				1,051,626						1,682,311		\$26,193,15
290	10	HGD	1223	2.65	1,214,241	0.559	678,761	4.402	5,345,091	0.100%	2,676,941	0.001%	25,769	\$12.70	\$15,436,57
SUBTOTAL	1	HGD	+		3,686,211	0.477	1,758,618	2.499	9,210,199	0.140%	11,396,548	0.021%	1,724,952	912.09	\$44,550,50
CUMULATIVE TOTAL		HGD							247,930,292						61,049,719,65
BENCH TOTAL		HGD/LGD	<u> </u>		9,444,535	0.316	2,986,454	2.020	19,077,525	0,133%	27,794,021	0.012%	2,529,061	89.21	086,961,76
CUM, BENCH TOTAL		HGD/LGD		<u> </u>	142,379,856	0,408	58,062,220	2,489	354,343,926	0.151%	473,204,378	0.006%	20,322,762	\$11,26	\$1,603,101,63

					ONSON SLO		m SEARCH			TOPE THE					
19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	OVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID I	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	*	POUNDS	TONNE	VALUE
280	resent	mr. i Erent	<del>  ~  </del>	000011	·Oues		0.0		- Growns		roomas	~	700100	TOTALE	*****
						<del></del>						<del></del>			
280	10	UDF	1	2.65	4,244,027	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
100	<del>                                     </del>	-	<del>   </del>		7,277,027					0.000 N	<del>`</del>	0.00070			
UBTOTAL	<del> </del>	UDF	<del> </del>		4,244,027										
UMULATIVE TOTAL	<del> </del>	UDF	<del> </del>		25,531,288										
OMOUNTIVE TOTAL	+	007	+		23,031,200										
	<del></del>			·										\$0.00	\$
	<del> </del>		<del> </del>											*0.00	
	<del></del>		<del> </del>											\$0.00	
	<del> </del>		-	<del></del>										●0.00	
	<del> </del>	<del> </del>	+											\$0.00	
280	1 10	WST	1219	2.65	977.832	0.000	96,805	1 202	1,175,354	0.040%	862,299	0.001%	21,557	\$2.95	\$2,693,06
		WST	1202	2 65	1,198,746		147,446	1 202	1,198,746	0 070%	1,849,945		554,984	\$4 12	\$4,947,06
280 280		WST	1223		1,232,157	0.123	283,396	0.78	961,082	0.020%		0.002%	54,329	\$4.42	\$5,447,56
		WST	1200		548,806		81,223	1.362	747,473	0.080%		0.004%	48,396	\$4 88	\$2,680,42
280	10	1431	1200	2.63		0.140	31,223	1.502	, 4, 4, 5		50,,520	2.237.6			,,
		MET		<del>  </del>	3,957,540	0.154	608,870	1.032	4,082,855	0.048%	4,223,458	0.008%	679,266	94.03	115,968,14
LIBTOTAL		WST	+	<del> </del>	41,805,264		4,971,658		39,381,304	0.033%				\$3.03	126,478,14
UMULATIVE TOTAL	<del></del>	WST	<del> </del>	<del> </del>	41,000,204	0.115	4,571,000	0.372	39,301,304	0.033 %	30,230,333	0.00 \ 7	3,417,027		V.201.101.
	<b></b>		<del></del>	·	·									●0.00	
		100	4224	3.05	1,613,019	0.242	391,964	4.802	7,745,718	0 020%	711 219	0.002%	71,122	\$5.50	\$8,895,85
280		LGD	1221	2 65			288,646		1,635,159				166,585	\$6.34	\$9,582,26
280		LGD	1199		1,511,237 1,247,443		358,016		960,531	0.070%	1,925,097		55,003	\$6.71	\$8,374,56
280		LGD	1217		658,735		117,914		768,744		1,887,938		232,362		\$4,425,06
280		LGD	1203		681,919		153,432	1 051	716,697	0.130%	1,804,048		30,067	\$7.15	\$4,879,91
280 280		LGO	949		493,413		72,038		1,222,184	0.160%	1,740,461		54,389	\$7 29	\$3,602,83
280		LGD	1201		272,974		43,130		1,273,425			0 006%	36,108		\$2,026,84
280		LGD	960		2,308,709		586,412		1,948,551	0 160%	8,143,722		1,476,050		\$20,037,84
260		LGD	1220		737,944		246,473		626,515		1,952,264		97,613		\$6,541,45
280		LGD	947			0.277	13.568		98,309			0 007%	7 559		\$455,78
	<u> </u>	1===													
SUBTOTAL	1	LGD			9,574,378	0.237	2,271,594	1.775	16,995,833	0.108%	22,844,932	0.011%	2,226,859	97.19	\$66,822,47
CUMULATIVE TOTAL		LGD					21,259,427		123,409,407	0.108%	202,562,228	0.005%	8,657,651	<b>\$7.29</b>	9622, 204, 45
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				<del> </del>		0.000			2 (22 22	0.1100	4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0.0000	246 5 45	90.00	PS 204 0
280		HGD	1204				167,638						248,546		\$5,286,9
280	10	HGD	948	2.65	70,872	0.423	29,979	13.695	970,587	0.160%	249,992	0.003%	4,687	\$14.18	\$1,008,0
		1466		·		0.343	167.55	7.405	4 153 355	0.143%	1,762,883	0.0202	253 334	411 33	\$6,294,9
SUSTOTAL	+	HGD	+	<del> </del>	661,041		197,617							611.22	61,056,014,6
CUMULATIVE TOTAL	<del></del>	HGD		+	97,140,723	0.565	39,272,004	3./35	252,083,547	0.199%	230,245,563	0.010%	14,145,203	715.73	- 1,035,014,61
BENCH TOTAL		HGD/LGD		<del></del>	10 135 419	0.244	2 469 210	2 087	21,149,088	0.110%	24 607 616	0.011%	2,480,092	67.41	875,117,46
	<del> </del>	1		<del> </del>	10,130,419	V. 4-	8,-35,210	8.507	2.,, 45,000	J.1107	47,007,010	- · · · · · · ·	2,400,092	77.71	U/ 3, 11 /, 44
UM, BENCH TOTAL				A	L	1	L	1							

					ONSON SLO		m SEARCH								
19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	OVAL	TOTAL
LEVE.	HEGHT	MATERIAL	D	DENSITY	TOMNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	*	POUNDS	TONNE	VALUE
270															
270	10	UDF		2.65	3,151,225	0	0	0	0	0 000%	Ö	0 000%	0	\$0.00	
		-	<del>                                     </del>			<del></del> +	<del>-</del>					-			
SUBTOTAL	<del> </del>	UDF			3,151,225				<del></del>						
	<del> </del>	UDF													
CUMULATIVE TOTAL	·	005			28,682,513		· ··· •				·-· ··· · - <del></del> ·· ···	-			
	<del></del>													40.00	
	<del> </del>													10.00	\$0
	<del> </del>						20.000				270 704			●0.00	\$0
270		WST	1219	2.65	1,014,175	0.089	90,262	0.7	709,923	0.030%	670,761		67,076	\$2 41	\$2,446,041
270		WST	1200	2.65	558,002	0.104	58,032	1.164	649,514	0 050%	615,091		36,905	\$3.30	\$1,844,914
270		WST	1199	2 65	1,471,510	0 094	138,322	0 727	1,069,788	0.060%	1,946,472	0 004%	129,765	\$3 32	\$4,692,660
270		WST	1218	2.65	712,014 368,282		74,761	0 607	432,192	0 060%	941,832 565,260		15,697	\$3 47 \$3 55	\$2,474,537 \$1,302,516
270		WST	1201	2 65 2 65	743,809	0 093	122,728	0.368	219,037 273,722	0 030%	491,945	0 004%	65,593	\$3.56	\$2,648,623
270		WST_	1220	2 65	1,243,531		271,090	0 947	1,177,624	0 030%	822,454	0 002%	54,830	- 22 54	\$5,646,269
270	10	4431	1223	2 63	1,243,331	-0218						. 5 552 70			
CLIPTOTAL	+	WST	<del> </del>		6,109,323	0120	789,260	0.742	4,531,800	0.045%	6,053,815	0.003%	369,866	93.48	921,255,560
SUBTOTAL	<del> </del>				47,914,587		5,760,918		43,913,103	0.034%			3,786,893	●3.08	1147,733,709
CUMULATIVE TOTAL		WST			47,814,567	0.120	0,700,310	0.510	45,515,105	0.034 7	30,343,043	0.004.77	5,1,55,555	13.00	
	<del></del>	<del> </del>												♦0.00	\$0
	<del> </del>		<del> </del>											\$0.00	\$0
	ļ	<u> </u>												●0.00	\$0
	<del> </del>	<del></del>	<del> </del>	l										\$0.00	\$0
	·			200	4 200 252	0.433	463 367	- 077	1 205 404	0 130%	3,686,691	0 035%	992,571	\$5.86	\$7,540,088
270		LGO	1202	2 65	1,286,352	0.127	163,367	1 077	1,385,401					\$6 04	\$4,504,490
270		LGD	1203	2 65	745,467	0 141	105,111	0 876	653,029	0 130%	2,136,513		279,390		\$3,708,250
270		LGD	1204	2.65	591,938		105,365	2.939	1,739,705	0 100%	1,304,998		339,299	\$6 25	
270	10	LGD	948		80,627	0.101	8,143	1 06	85,465	0.160%	284,404		5,333	\$6.26	\$505,253
270	10	LGD	949		519,468		55,064	1.544	802,058	0.160%	1,832,366		22,905	\$6 45	\$3,352,332
270	10	LGD	960	2.65	2,244,433	0 151	338,909	0 6	1,346,660	0.160%	7,916,995		1,484,437	\$6 97	\$15,642,173
270	10	LGD	947	2.65	68,788	0.188	12,932	2.513	172,865	0 160%	242,643	0.003%	4,550	\$7.98	\$549,283
	1													L	
SUBTOTAL		LGD	1		5,537,072	0.142	788,891	1,117	6,185,182	0.143%	17,404,610	0.026%	3,128,484	18.47	135,801,866
CUMULATIVE TOTAL	1	LGD	1				22,048,318	1.426	129,694,649	0.110%	219,966,838	0.006%	11,786,135	07.24	1658,006,321
			-											●0.00	\$6
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	<del>-i</del>	<del> </del>	+	<del> </del>										●0.00	×
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	1	<del> </del>												10.00	\$0
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	<del></del>		1										1	●0.00	\$0
270	10	HGD	1217	2 65	1,253,100	0.375	469,913	1 028	1,288,187	0 190%	5,248,960	0.001%	27 626	\$11.49	\$14,400,797
270		HGD	1221								1,434,033			\$12.62	\$20,545,872
210	<del></del> "	1.00	1221	2.65	1,020,100	0 002	1,0/0,323	033	0,330,337	0.0-0.8	1,434,033	U.UU N	37,651	#12.0Z	ezu, 3-3,677
CURTOTAL	<del></del>	HCD	+	<b> </b>	2 070 240	0.537	1 544 434	2 725	7,846,524	0.105%	6,682,993	0.001#	63 477	812.14	\$34,946,668
SUBTOTAL	<del></del>	HGD	+	<del> </del>			1,546,436								
CUMULATIVE TOTAL	<del></del>	HGD			70,019,991	0.583	40,818,440	3.712	259,930,071	0.196%	301,932,958	0.009%	14,208,680	15.58	41,090,961,320
		<b>_</b>		1								ļ	<u> </u>		
BENCH TOTAL		HGD/LGD		1	8,416,341	0.277	2,335,327	1.667	14,031,708	0.130%	24,087,603	0.017%	3,191,961	98.41	170,748,53
	1	1		L									<u> </u>		
CUM, BENCH TOTAL		HGD/LGD			160,931,616										\$1,748,967,64

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						250	m SEARCH	RADIL	<u>  S</u>						
19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	SVAL	TOTAL
TEAST	HEIGHT	MATERIAL	10	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNOS	%	POUNDS	TONNE	VALUE
260	<u></u>														
	ļ														
260	10	UDF		2.65	3,320,287	0	0	0	0	0.000%	0	0.000%	0	\$0.00	····
	ļ		<u> </u>												
SUBTOTAL	<del> </del>	UDF		<del></del>	3,320,287										
CUMULATIVE TOTAL	<del> </del>	UDF	<b></b>	<del></del>	32,002,800										
·	<del> </del>			<del>  </del>			<del></del>							\$0.00	\$
				<del></del>										\$0.00	s
														00.00	s
260	10	WST	1199	2.65	1,435,527	003	43,066	0.2	287,105	0.030%	949,438	0 001%	31,648	\$1.35	\$1,942,45
260		WST	1221	2.65	1,627,683		144,864	0 274	445,985	0.010%	358,842		35,884	\$1 77	\$2,876,07
260	10	WST	1203	2 65	561,397	0 071	39,859	1.581	887,569	0 060%	990,134		272,287	23 69	\$2,073,87
260		WST	1218	2 65	752,178		78,227	0.426	320,428	0.070%	1,160,787		16,583	23 69	\$2,779,36
260		WST	1200	2 65	527,252		72,761	1.447	762,934	0.050%	581,195		11,624	\$3.91	\$2,064,33
260	10	WST	1204	2 65	473,915	0 118	55,922	1.574	745,943	0 080%	835,843	0 000%	83,584	844	\$2,108,13
	<del> </del>		<del> </del>	ļI		200						0.00:00			413.644.55
SUBTOTAL	ļ	WST		<del> </del>	5,377,953		434,698	0.642	3,449,964	0.041%	4,876,239		451,610	02.57	\$13,644,23
CUMULATIVE TOTAL		WST	<del> </del>	<del> </del>	63,292,640	0.116	6,195,616	0.889	47,363,068	0.035%	41,226,053	0.004%	4,238,503	•3.03	\$161,577, <del>9</del> 4
			<del> </del>	<del> </del>										\$0.00	s
260	·	LGD	1219	2.65	1.063.130	0 200	216 727	4 440	4 402 050	0.050%	1 150 760	0.000	46,390	\$5.00	\$5,263,26
260		LGD	1202	2.65	1,052,120		216,737	1.419	1,492,958		1,159,762		735,475		\$7,073,24
260		LGD	960		1,334,425 2,180,048		148,121 211,465	0 949	1,266,370 1,656,837	0.120%	3,530,281 7,689,885		1,105,421	\$5 30 \$5 13	\$13,377,21
				4											\$559.83
260		LGO	948			0 108	9,354	1.445	125,153	0.160%		0 009%	17,185	\$6 46	
260 260		LGD	1201	2 65 2.65	371,942 744 330		63,974 206,179		843,563 1,013,778	0.140%	1,147,986 1,640,965		114,799 32,819	\$7 12 \$7 50	\$2,649,26 \$5,589,60
260		LGD	947			0.191	17,423		332,221	0.100%		0.005%	10,055	\$8 27	\$7,56,45
260		LGD	949		551,697		114,201		2,058,935		1,946,053		24,326	\$8 55	\$4,721,89
260		LGD	1217		1,254,177		391,303		1,231,601	0 150%	4,147,474		55,300	\$9.36	\$11,747,44
260		LGO	959		639,468		191,840		1,023,148		2,255,653		140,978	\$9 58	\$6,129,45
SUBTOTAL		LGD			8,306,037	0.189	1,570,598	1.330	11,044,563	0.132%		0.012%	2,282,748	16.97	\$57,866,68
CUMULATIVE TOTAL		LGD			99,217,661	0.238	23,618,915	1.417	140,639,212	0.112%	244,112,173	0.006%	14,058,883	<b>97.22</b>	1715,873,00
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	<del> </del>													\$0.00	
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	+			<del> </del>		<del> </del>								\$0.00	
	+		+	<del>                                     </del>		<del> </del>				<del> </del>		<del> </del>		10.00	
	+	<del> </del>	+											\$0.00	
	<del> </del>	<del> </del>		<del> </del>		-						<b></b>		\$0.00	
	<del>                                     </del>		1	1		1				t				\$0.00	
	+	1	1			1								\$0.00	
			1	1		1							l	10.00	
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260	10	HGD	1223	2.65	1,252,417	1 299	1,626,890	2.508	3,141,062	0.090%	2,484,993	0.002%	55,222	\$23.91	\$29,957,66
	<del></del>	<del> </del>													
SUBTOTAL		HGD					1,626,890						55,222	123.92	\$29,957,6
CUMULATIVE TOTAL		HGD	-		71,272,408	0.596	42,445,329	3.691	263,071,133	0.194%	304,417,949	0.009%	14,263,902	15.73	61,120,918,90
BENCH TOTAL	+	HGD/LGD	+	<del> </del>	0 550 454	0.335	3 103 463	1 404	14 105 435	0.344	30.030.330	00:10	2 222 624	40.10	407.074.74
BENCH TOTAL		חטטונטט	+		9,000,404	0.335	3,197,487	1.484	14,185,825	0.126%	20,030,328	0.011%	2,337,970	19,19	187,824,34
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						250	m SEARCH	RADIU	8						
19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	OVAL	TOTAL
LEVEL	HEGHT	MATERIAL	10	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	*	POUNDS	TOMME	VALUE
250														+	
240	10	UDF		2.65	3,636,194	0			0	0.000%	ō	0.000%	0	\$0.00	
250		UUF		2.65	3,030,154				<del></del>	-0.0007					
BTOTAL	-	UDF			3,636,194										
UMULATIVE TOTAL		UDF	1		35,638,995										
	1														
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250	10	WST	1202	2.65	1,435,882	0	0	0	0	0 000%		0.000%	0	\$0.00	9
250	10	WST	1203	2 65	607,020	0 057	34,600	1 363	627,368	0 070%	936,773		655,741	\$3 14	\$1,909,35
250		WST	1223	2.65	1,264,395	0 169	213,683	0 912	1,153,129	0 010%		0 003%	83,625	\$3 19	\$4,038,14 \$4,461,59
250		WST	1200	2.65	1,346,554	0.08	107,724	0 445	599,216	0 070%	2,078,048		29,686	\$3.45	\$1,618,956
250		WST	1204	2.65	525,636	0 114	59,923	1.134	596,072	0.050%	1,066,371	0.007%	81,118 17,773	\$3.85	\$3,106,680
250		WST	1218	2.65	806,164	0.131	105,607	0.426	343,426	0.060%		0.001%	23,895	\$4.18	\$4,536,93
250	10	WST	1219	2.65	1,083,864	0.179	194,012	0.933	1,011,245	0.040%	833,804	J 00 / A	13,083		4.,22,00
		NAME T		<del> </del>	7,069,514	0.101	715,549	0.641	4,530,455	0.038%	5,895,160	0.000%	891,839	62.81	\$19,871,67
UBTOTAL UMULATIVE TOTAL	+	WST	-		60,362,055		0,911,165		61,893,523	0.035%				#3.01	0181,449,62
UMULATIVE TOTAL	+	WSI			00,302,033	V.114	0,011,100	0.000							
	+	<del> </del>	<del> </del>											00.00	
	+													●0.00	s
														00.00	
	T									0.4000	7,554,360	0000	1.180.369	\$5.00 \$5.97	\$12,794,64
250		LGD	960	2 65	2,141,628		182,036	0 901	1,929,607	0.160%		0.004%	10,147	\$6.85	\$789,33
250		LGD	947	2.65	115,070		15,419		154,654	0 160%	2,527,976		50,560	\$7 07	\$8,112,42
250		LGD	1220	2.65	1,146,672	0.25	286,668		1,558,327	0.100%	1,426,615		61,141	\$7 67	\$3,552,72
250		LGD	1201	2.65	462,216 1,619,670		85,972 617,094		1,759,195 2,810,127	0 050%	1,785,378		35,708	\$7.88	\$12,772,82
250		red	1221	2.65			115,304		1,754,483	0 160%	2,043,840		38,322	\$8 27	\$4,794,86
250		LGD	949		579,420 735,169		182,322		2,695,131	0 160%	2,593,231		129,662	\$9 19	\$6,766,20
250	10	LGD	959	200	733,108	0.240	102,322	3.000	2,000,101	0 100 %	2,300,40	0.000			
	<del></del>	100	<del> </del>		4 700 PAA	0.218	1,484,819	1 862	12,861,822	0.122%	18,337,296	0.010%	1.505.907	07.29	149,583,03
WBTOTAL		LGO	-	<b> </b>	104 017 505	0.210	25 103 734	1 448	183,300,736		262,449,469	0.007%	15 574 790		1765,456,04
UMULATIVE TOTAL		LGD	1		100,017,008	0.237	25,105,754	1.440	100,000,700						
														90.00	
		<del></del>	-					-				1		10.00	
			-	<del> </del>		-								●0.00	
				<del> </del>	<del></del>			-		-		1		10.00	
	+	+		<del></del>	<del></del>			-						\$0.00	
				+	-	1		1						\$0.00	
	+	+		+	-	-		1				T		\$0.00	
		+	+	1	1	1								\$0.00	
	-	<del> </del>	+	1	1	1								●0.00	
	-	1	1	1		1				T				●0.00	
				1	1	1								\$0.00	
	+	1	-	1		1								\$0.00	
250	1	0 HGD	94	2 65	91,926	0 541	49,73	3 179				6 0 024%			
250		0 HGD	121					1 924	2,421,246	0 280%	7,768,29	0 002%	55,48	\$14.02	\$17,649,3
		1				<b></b>		L				1	100000	1	
SUBTOTAL		HGD		<u> </u>	1,350,372	0.378	510,32	2.009	2,713,485	0.272%				014.01	\$18,918,6
CUMULATIVE TOTAL		HGD			72,622,780	0.591	42,986,68	3.660	265,784,617	0.195%	312,510,50	0.009%	14,368,030	015.70	01,139,837,6
DELIGH TOTAL		Webs oc	-	+	0.100	1000		1 000	18 136 203	0 1 4 3 2	20 420 22	10.0000	1 010 000	1 00 00	200 501 3
BENCH TOTAL		HGD/LGD		<del> </del>	0,150,216	0.246	1,995,14	1.860	15,375,007	0.147%	20,429,854	0.009%	1,610,035	¥8.40	968,501,7
	1	1		1	1	1	1	1	1		1	1	i .	1	i .

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					ONSON SLO		m SEARCH								
18-12-96 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	SVAL	TOTAL
LEVB.	HEIGHT	MATERIAL	10	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	*	POUNDS	TOMME	VALUE
240						11.11									
				2.05	2042443							أنفتحة		- en m	
240	10	UDF	1	2.65	3,918,157		<u></u>	0	0	0.000%		0 000%		\$0.00	
UBTOTAL	<del>                                     </del>	UDF	1		3,918,157										
UMULATIVE TOTAL		UDF			39,557,152										
															\$0
	<del>  </del>		<del>  </del>	<del> </del>										\$0.00 \$0.00	
240	10	WST	1203	2.65	794,804	0	0	0	0	0.000%	0	0 000%	0	\$0.00	\$0
240		WST	1218	2.65	1,373,436	0.02	27,469	0.257	352,973	0.040%	1,211,162		30,279	\$1.48	\$2,033,30
240		WST	1201	2 65	619,555	0.055	34,076	0 786	486,970	0.040%	546,353		54,635	\$2.16	\$1,338,010
240		WST	1221	2 65	1,777,971	0 112	199,133	0.429	762,749	0 020%	783,950		39,197	\$2 44	\$4,349,790
240		WST	1220	2.65	1,065,777		87,394	0 587	604,295	0.070%	939,853 802,886		23,496 217,926	\$2.54	\$2,713,052 \$2,045,318
240 240		WST	1204	2.65 2.65	520,262 1,538,827		53,067 249,290	2.077	856,351 3,196,144	0.060%	2,035,517		67,851	\$471	\$7,256,132
40	<del>  "</del>	****	1200	1.00	.,320,027	0.102	2-10,200	2.077	3,150,144	0.300.4					-,,,,
UBTOTAL		WST			7,690,632	0.085	650,427	0.814	6,259,484	0.037%	6,319,722		433,385	\$2.57	\$19,735,611
CUMULATIVE TOTAL		WST			68,052,686	0.111	7,561,592	0.855	58,153,007	0.036%	53,440,935	0.004%	5,563,727	12.96	\$201,185,235
			ļ											40.00	90
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	<del></del>		<del> </del>	<del> </del>										10.00	- SC
	· <del> </del>	-	· }											10.00	S
	<del></del>		1	1										●0.00	
														10.00	\$0
240		LGD	960		3,170,864		225,131	1.068	3,386,483	0.160%	11,184,882		2,027,260	\$5 78	\$18,346,241
240		LGD	947		202,527		28,759	1,173	237,584	0.160%		0.004%	17,860 53,763	\$6.95 \$7.06	\$1,407,697 \$4,309,670
240		LGD	949				91,449 498,364	1.126	686,479 1,732,176	0.160%	2,150,517 3,200,104		71,113		\$12,394,890
240		LGD	1219				206,919		976,346	0.160%	3,066,744		268,340		\$7,375,48
240	<del></del>	LGO		1.05	000,000	0.230	100,010			0,100.0					
SUBTOTAL		LGD			6,465,289	0.163	1,050,622	1,086		0.143%					443,833,994
CUMULATIVE TOTAL		LGD			112,482,794	0.233	26,154,356	1.425	160,319,763	0.114%	282,786,107	0.007%	18,013,128	17.19	1809,290,03
				ļ		<b></b>								\$0.00 \$0.00	
		<del></del>		<del></del>		<del> </del> -	ļ	<del></del>						10.00	
	+	<del> </del>		<del></del>	<del> </del>	<del> </del>	<del> </del>							●0.00	•
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		<del> </del>				<b></b>		<u></u>						10.00	\$
		<del></del>		<del> </del>	ļ		<del> </del>							90.00	
	<del></del>	<del> </del>	-	+	<del> </del>	<del> </del>					<u> </u>			#0.00	\$
		<del></del>		1	t	1		t	<del></del>	<del></del>				0,00	\$
				1										00.00	3
240	10	HGD	122	2 65	1,267,729	2 686	3,405,121	0.488	618,652	0.010%	279,486	0.001%	27,949	\$43.56	\$55,239,80
SUBTOTAL		HGD			1,267,729	2.686	3,405,121	0.488	618,652	0.010%	279,486	0.001%	27,949	943.57	\$55,239,80
CUMULATIVE TOTAL		HGD	+	+	73,890,501	0.627	46,360,774	3.605	266,403,269	0.192%	312,789,993	0.009%	14,395,979	416,17	41,195,077,48
BENCH TOTAL		HGD/LGD			7,733,018	0.676	4,455,743	0.988	7,637,700	0.121%	20,596,124	0.014%	2,466,285	012.81	999,073,79
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					ONSON SLO		m SEARCH								
19-12-95 9:31 AM	SENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	.VAL	TOTAL
LEVB.	HEGHT	MATERIAL	O C	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	*	POUNDS	TOMME	VALUE
230	1							11							
230	10	UDF		2.65	4,476,237	a	0		0	0.000%	0	0.000%		\$0.00	
					1, 1, 5, 5, 5					0.000.0					
SUBTOTAL		UDF			4,478,237										
CUMULATIVE TOTAL	<del></del>	UDF	<del> </del>		44,035,389										
			1											●0.00	\$0
														\$0.00	×
	<del> </del>	ļ	<del> </del>											\$0.00 \$0.00	<u> </u>
230	10	WST	1203	2 65	796,727	0	ō		0	0 000%	0	0.000%	0	\$0.00	\$X
230		WST	1220	2.65	940,283	0 056	52,656	0 898	844,374	0.040%	829,186		41,459	\$2.20	\$2,068,95
230		WST	1201		833,002		64,974	0.57	474,811	0.070%	1,285,517		91,823 37,797	\$3 31 \$3 66	\$2,756,138 \$6,269,025
230 230		WST	1200		1,714,442 535,035	0.094	161,158 78,650	1.035	1,774,448	0.070%	2,645,786 825,684	0.028%	330,274	\$4.92	\$2,639,790
230	<del> </del>	10031	1204	100			70,000	2,5,4	1,23,031	0.0.0%	V25,55				
SUBTOTAL		WST			4,819,488		357,438	0.965	4,652,724	0.053%	5,560,173		501,352	02.85	913,753,912
CUMULATIVE TOTAL	ļ	WST	<del> </del>		72,872,175	0.109	7,919,030	0.862	62,805,730	0.037%	59,027,108	0.004%	6,085,079	12.95	0214,939,148
	<del> </del>		<del> </del>	<del> </del>										\$0.00	\$0
		<del> </del>												\$0.00	\$0
														●0.00	<b>X</b>
				<del>                                     </del>										#0.00 #0.00	
	<b></b>	<u> </u>		<del> </del>										\$0.00	
230	<del> </del>	LGD	960	2 65	3,188,735	0.061	258,288	0 493	1,572,046	0 160%	11,247,917	0 019%	1,335,690	\$5.82	\$18,559,010
230		LGO	1219		2,265,686		518,622	2.121	4,605,944	0 100%	4,995,417		49,954	\$6 66	\$15,608,861
230		LGD	949		1,130,752		158,305	1 467	1,658,813	0 160%	3,988,604		74,786	\$6 98	\$7,896,242
230		red	959				188,017		763,293	0 160%	3,299,552		391,822	\$7 82	\$7,315,679
230	10	LGD	1223	2.65	3,035,901	0.445	1,350,976	5.258	15,962,770	0.020%	1,338,602	0.001%	66,930	\$8.85	\$26,908,756
SUBTOTAL	<del> </del>	LGD		·	10,656,682	0.234	2,472,208	2.346	24,762,966	0.107%	24,870,093	0.008%	1,919,183	97.23	076,288,556
CUMULATIVE TOTAL		LGO							185,082,649		307,636,200	0.007%	19,932,309	97.20	1885,578,58
		ļ.——	+	ļ		<del> </del>	<u> </u>					<del> </del>			
		ļ	<del> </del>				<del></del>			<u> </u>	<b></b>	<del> </del>		90.00 80.00	<b>8</b> 5
		+	+	<del> </del>		<del> </del>	<del></del>					<del> </del>		●0.00	\$
	+	+	<del> </del>		<del></del>									\$0.00	
	1		1											90.00	\$
											<del></del>		<del></del>	90.00	\$ \$
	<del> </del>	-		<del> </del>							<del> </del>	<del> </del>		\$0.00 \$0.00	
		<del> </del>		<del> </del>						<del> </del>	<del> </del>	1		\$0.00	\$
	+	1	1											\$0.00	\$
														\$0.00	5
	1					-								\$0.00	3
		<del> </del>	<del> </del>	<del> </del>	<del> </del>	<del> </del> -					<del> </del>	<del> </del>		\$0.00 \$0.00	3
SUBTOTAL		HGD				0.000						0.000%			
CUMULATIVE TOTAL	<del></del>	HGD	+	<del></del>	73,890,508	0.527	46,360,774	3.605	266,403,269	0.192%	312,789,993	0.009%	74,395,979	<b>016.17</b>	61,195,077,45
BENCH TOTAL		HGD/LGD			10,556,682	0.234	2,472,208	2.346	24,762,866	0.107%	24,870,093	0.008%	1,919,183	87,23	976,288,85
		1												1	

					ONSON BLO		m SEARCH								
19-12-96 9:31 AM LEVEL	BENCH HEIGHT	POLYGON MATERIAL	HOLE	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER	COPPER POUNDS	MOLY %	MOLY POUNDS	TOMME	TOTAL
220															
220	10	UOF		2.65	4,485,103	0	0	0	o	0 000%	0	0 000%		_\$0.00	
UBTOTAL		UDF	<del> </del>		4,485,103										
CUMULATIVE TOTAL		UDF			48,520,492										
														●0.00	\$0
			ļ	L										\$0.00	20
	<b></b>	ļ	<del> </del>	<del> </del>	<del></del>	<del>}</del>			<del></del>					\$0.00	\$0
	<del> </del>	<b></b>	<del> </del>	<del> </del>										10.00	\$0
	<del> </del>	<del> </del>	-	<del> </del>										\$0.00	\$0
220	10	WST	1223	2 65	2,423,072	0 035	84,808	0 522	1,264,844	0 010%	534,195	0.001%	53,420	\$0.95	\$2,309,715
220		WST	1220		830,657	0.05	41,543	0 226	187,774	0 020%		0 001%	18,317	\$1.40	\$1,167,251
220		WST	1204		921,920	0.085	78,363	0.982	905,326	0.050%	1,016,242		304,873	\$2 96	\$2,729,554
220		WST	1201	2.65	877,951	0 085	74,626	0.834	732,211	0 070%	1,354,684	0 006%	116,133	\$3.48	\$3,054,675
SUBTOTAL		WST	+	<del> </del>	5,053,801	0.055	279,339	0.611	3,090,154	0.029%	3,271,666	0.004%	492,742	\$1.83	\$9,261,195
CUMULATIVE TOTAL		WST			77,925,975				65,895,885	0.030%	62,298,774	0.004%	6,557,822	\$2.88	1224,200,343
	<del> </del>		<del></del>											\$0.00	\$0
	<del> </del>	+												●0.00	\$0
														₩0.00	\$0
														0.00	\$0 \$0
	<del></del>	LGD	·~~	2 65	1,859,632	0.183	338, 453	2.325	4,323,645	0.060%	2,459,870	0.0003	81,996	\$5.00	\$9,466,365
220		LGD	1200		3,428,166		250,256	0717	2,457,995		12,092,487				\$19,680,486
220		LGD	958		738,795		60,581	0.703	519,373		2,606,018		16,288	\$5.88	\$4,345,929
220		LGD	1218		2,275,699		427,831	1.04	2,366,727	0.130%	6,522,167		50,171	\$6.63	\$15,552,919
220		LGD	949		1,188,877	0 177	210,431	4 484	5,330,925		4,193,636		78,631	\$8 23	\$9,798,583
220	10	LGD	959	2.65	1,170,234	0 233	272,664	6.006	7,030,765	0.160%	4,127,874	0 025%	644,980	\$9 46	\$11,001,056
SUBTOTAL	<del> </del>	LGO	1		10,661,404	0.146	1,560,218	2.066	22,029,431	0.136%	32,002,052	0.010%	2,459,204	●0.66	469,937,339
CUMULATIVE TOTAL		LGD			133,700,880	0.226	30,186,782	1.549	207,112,080	0.115%	339,638,252	0.008%	22,391,513	87.15	9955,515,923
			-									-		●0.00	\$0
		<del> </del>	<del></del>	<del> </del>					<del></del>					10.00	\$0
	<del> </del>		<del> </del>	<del></del> -	<del></del>	<del>                                     </del>	<del></del>			<del> </del>				\$0.00	\$0
		<del> </del>	<del></del>	-		<del>                                     </del>								\$0.00	SC
	1	<del>                                     </del>	1							1				\$0.00	80
													<b></b>	●0.00	\$4 \$4
										<b> </b>		ļ		\$0.00	
		<b></b>	-	<b>_</b>								<del></del>	<del></del>	\$0.00	\$ \$ \$ \$ \$ \$ \$ \$
		<del> </del>		<del></del>						<del> </del>		+	<del> </del>	\$0.00	SC
	+	<del> </del>	+	<del> </del>		<del> </del>				<del> </del>	<del> </del>	<del> </del>	<del> </del>	●0.00	\$0
	+	<del> </del>	+	+			-			<del> </del>	<del>                                     </del>		1	\$0.00	\$0
	1		-			1	t	t			<u> </u>			\$0.00	
	1													\$0.00	80
SUBTOTAL	+	HGD	+	+	0	0.000	0					0.000%	0	\$0.00	\$60
CUMULATIVE TOTAL		HGD			73,890,509	0.627	46,360,774	3.605	266,403,269	0.192%					01,196,077,450
BENCH TOTAL	+	HGD/LG0			10,881,404	0.146	1,800,218	2.000	22,029,431	0.136%	32,002,082	0.010%	2,459,204	96.56	169,937,331
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						250	m SEARCH	BADII	e						
10 12 05 0.21 0.4	BENCH	POLYGON	HOLE		METERS	AU	M SEARCH	AG	AG	COPPER	COPPER	MOLY	MOLY	•VAL	TOTAL
19-12-96 9:31 AM				00000	TONNES	PPM	GRAMS	PPM			POUNDS	MOLV	POUNDS	TOMME	VALUE
UEVEL.	HEGHT	MATERIAL	ID.	DENSITY	1 Uranes	FFRE	GIVAMS	****	GRAMS	<b>×</b>	rounds		rounus	- I Oreste	- VALUE
210															
	<del></del>			2 66	4 400 ME		0			0.000%		0 000%	0	\$0.00	
210	10	UDF		2 65	4,496,025	0				0.000%		0000		3000	
						-									
SUBTOTAL	<b></b>	UDF			4,496,025										
CUMULATIVE TOTAL	ļ	UDF			53,016,617										
	ļ		ļ											40.00	\$0
	<b></b>			ļ										0.00	\$0 \$0
	<b></b>			l										10.00	
			1					0.0.7	404.003	0.0000	404.043	0.0044	10 100	\$0.00 \$1.72	\$1,258,772
210		WST	1220		733,024		38,117	0.247	181,057	0.030%	484,812		16,160 632,026	\$2.46	\$2,206,942
210		WST	1204	2 65	895,683		42,106	1 499	1,342,928	0.050%	987,541				
210		WST	1223	2 65	2,187,884		308,492	0 831	1,818,132	0 010%	482,345		48,235	\$2.72	\$5,963,467 \$2,823,005
210		WST	1201	2 65	906,010	0 08	72,481	0.8	724,808	0.060%	1,198,445		79,896	\$3 11	
210		WST	1200		1,981,290		172,372	0.905	1,793,068	0.080%	3,494,394		43,680	\$3.60	\$7,534,213
210	10	WST	1219	2.65	2,282,445	0.192	438,229	1.118	2,551,774	0.060%	3,019,154	0.001%	50,319	\$4.98	\$11,382,062
															444 444 444
SUBTOTAL		WST			8,986,536		1,071,798		8,411,766	0.049%	9,666,691		870,316	\$3.47	931,168,462
CUMULATIVE TOTAL		WST			86,912,512	0.107	9,270,167	0.855	74,307,651	0.038%	71,965,464	0.004%	7,428,138	12.94	<b>\$255,368,805</b>
													i		
														\$0.00	\$0
	1													10.00	\$0
		1	1											●0.00	\$0
	<del> </del>	<del> </del> -	1											\$0.00	\$0
	<del> </del>	<del>                                     </del>	-	<del> </del>										\$0.00	\$0
	<del> </del>	<del> </del>	<del></del>											●0.00	\$0
340		LGO	958	2.65	207,652	0.046	9.562	0.529	109,848	0.160%	732,471	0.001%	4,578	\$5.26	\$1,093,352
210		LGD	949		1,239,583		109,083		2,113,488	0.160%	4,372,494	0 002%	54,656	\$6 19	\$7,684,643
210		LGD	955			0.141	1,735	0.74	9,107			0 000%	0	\$8 84	\$84,169
210		LGD	959		1,225,954		180,215		1,245,569		4,324,419		702,718	\$6.99	\$8,577,409
210			960		3,437,908				11,520,428		12,126,848	0.020%	1,515,856	\$6.99	\$24,050,432
210	10	LGD		2.00	3,437,800	0.113	303,300	3 30.	11,020,120	0.100.0	15,120,0				
	<del></del>	LGD	+		6,123,403	0 114	695,945	2 449	14,998,440	0.160%	21,599,642	0.017%	2.277.808	16.78	941,490,006
SUBTOTAL CUMULATIVE TOTAL	<del> </del>	LGD	+		139 824 283	0.117	30 882 727		222,110,621		361,237,893				4997,005,928
COMOCATIVE TOTAL	+	100	<del> </del>	<u> </u>	135,021,1203			1							
	1	<del>                                     </del>	+	<del> </del>		1		1							
	+	-	+			1									
	1	<del>                                     </del>		<del>                                     </del>						1				\$0.00	\$0
	1	t				<del> </del>	1	1						\$0.00	\$0
	+	<del> </del>	+			<del>                                     </del>		1						\$0.00	\$0
	+	<del> </del>	+	+		<del>                                     </del>								\$0.00	\$0
	+	+	+	<del> </del>		<del>                                     </del>								\$0.00	\$0
	<del> </del>	<del> </del>	+	<del> </del>				<del>                                     </del>						\$0.00	\$0
	1	-	+	<del> </del>		-		1		1				●0.00	\$0
	+	+	+	1	<del></del>	<del> </del>	<del> </del>	-		<del> </del>				0.00	\$0
	<del>                                     </del>	+	<del></del>			<del> </del>	<del> </del>							\$0.00	\$0
		<del> </del>		+		<del> </del>				<del> </del>				●0.00	80
	+	<del> </del>	+	<del> </del>		<del> </del>		<del> </del>						\$0.00	80
	+	<del> </del>	-	<del></del>				<del> </del>		<del> </del>			·····	\$0.00	\$0
	+	<del> </del>	+	+		<del> </del>		1		<del>                                     </del>		<del> </del>		●0.00	sc
	<del> </del>	1.100				<del> </del>	603.046	4 404	1 225 555	0.160%	3,153,298	0.000		\$136 10	\$18,610,096
210	10	HGO	954	2.65	893,946	1	893,946	1.494	1,335,555	0.100%	3, 153,290	0.000%		3130 10	\$10,010,000
						<del> </del>		1				0.0000	<del></del>	420.00	212 210 20
SUBTOTAL		HGD			893,946	1.000	893,946					0.000%	0	\$20.82	\$18,610,090
CUMULATIVE TOTAL		HGD			74,784,455	0.632	47,254,720	3.580	267,738,824	0.192%	315,943,291	0.009%	14,395,979	916.23	41,213,697,540
BENCH TOTAL	1	HGD/LGD			7,017,349	0.227	1,589,891	2.328	16,333,996	0.160%	24,752,940	0.015%	2,277,808	18.56	\$60,100,10

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19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	IVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	10	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	%	POUNDS	TONNE	VALUE
200															
			1										1		
200	10	UDF	1	2.65	4,700,557		ol	0	0	0.000%	0	0 000%	0	\$0.00	
	<del> </del> ''	-	<del> </del>		7,700,007			-		0.000 //					
SUBTOTAL		UDF	1	<del></del>	4,700,557							<del></del>			
	<del></del>		<del> </del>	<del></del>	57,717,075										
CUMULATIVE TOTAL	<del> </del>	UDF	<del> </del>		37,717,075			<del></del>		<del></del>					
			<del> </del>											\$0.00	
	<del></del>		<del></del> -											\$0.00	
	ļ			<b></b>										\$0.00	
· · · · · · · · · · · · · · · · · · ·	<b></b>		ļ	<b> </b>										●0.00	
	ļ	ļ	125	l	1 22 1 172					0 0000		0.000%	0		
200		WST	1201	2.65	1,384,476	0	0	0	0						
200		WST	1204	2.65	870,219	0	0	0	0			0 000%	0 000		\$1,915,9
200		WST	1223	2.65	1,972,871	0 04	78,915	0.238	469,543			0.002%	86,989		\$830.3
200		WST	1220		825,977	0.024	19,823	0.31	256,053			0.001%	18,210		
200	10	WST	1200	2.65	2,062,824	0.063	129,958	0.717	1,479,045	0.060%	2,728,646	0.001%	45,477	\$2.82	\$5,825,9
				<u> </u>											46.434
SUBTOTAL		WST			7,116,367		228,696	0.310	2,204,641	0.022%	3,527,782		150,676	\$1.20	10,572,11
CUMULATIVE TOTAL	1	WST	Ļ	1	94,028,879	0.101	9,490,864	0.814	76,612,292	0.036%	75,493,247	0.004%	7,579,914	02.81	1263,940,90
	I														
			1											●0.00	
										L				\$0.00	
		<u> </u>	1											10.00	
			J											\$0.00	
			İ											\$0.00	
	I	I	I											\$0.00	
200	10	LGD	958	2 65	129,552	003	3,887	0 48	62,185	0.160%		0 001%	2,856		\$647,4
200	10	LGO	960	2 65	3,442,029	0 082	282,246	1 465	5,042,572	0.160%	12,141,384	0.027%	2,048,859	\$6 05	\$20,824,6
200		LGD	955	2 65	38,304	0 24	9,193	2 445	93,653	0.160%		0.000%	0	\$8.80	\$337,3
200		LGD	959		1,270,471	0.276		0.698	886,789	0.160%	4,481,450	0 034%	952,308	\$9 00	\$11,435,3
200		LGD	964		96,762		29,222	2.044	197,781			0.001%	2,133	\$9.71	\$940,0
	<u> </u>	12.7	<del> </del>							1					
SUBTOTAL	<del></del>	LGD	<del>                                     </del>	†	4,977,117	0.136	675,198	1.262	6,282,979	0.160%	17,550,243	0.027%	3,000,150	16.87	834,184,74
CUMULATIVE TOTAL	1	LGD	+	· · · · · · · · · · · · · · · · · · ·	144,801,400				228,393,500	0.119%	378,794,136				91,031,190,60
COMPONITE TOTAL	1	1500	+	1	7 1 1,100 1,100	V.2.0	5.155.1555	1,9,7		1		1		1	
	<del> </del>	<del>                                     </del>	· <del> </del>	<del></del>						1		1			
	<del>                                     </del>	<del> </del>	+	1						ţ	<del> </del>	1			
		+	+	<del> </del>						<u> </u>		1		♦0.00	
	<del></del>	<del> </del>	<del> </del>	1						1	1	1	1	\$0.00	
	<del> </del>	<del> </del>	+	<del>   </del>									T	\$0.00	
	+	<del> </del>	+	<del> </del>						<b>———</b>		1		♦0.00	
		+	+	<del> </del>				<b></b>		1	1	1		\$0.00	
	· <del>†</del> · · · <del></del>	<del> </del>	+					i		1	1	T		\$0.00	
	1	<del>                                     </del>	1	1			1			1		I		●0.00	
	<del>                                     </del>		1	1					1	1				\$0.00	
	<del> </del>	<b></b>					1			T	1			\$0.00	
	1	T	+						1	1	I	I		\$0.00	
	1	1	<del>                                     </del>	1			1							\$0.00	
200	10	HGD	1219	2 65	2,787,118	0.659	1,836,711	7.679	21,402,280	0.100%	6,144,536	0.002%	122,891	\$15 02	\$41,923,4
200		HGD	963			0 728			296,906			0 001%			\$1,365,1
200		HGD	954			1	1,091,201					0 001%			\$22,830,3
	<del>- </del> "	1	+	1.00	1,001,201	<del> </del>	1,50,1201	1.500	5,141,400	1 3	5,00,00	+ · · · · ·		1	
SUBTOTAL	-	HCD	-	<del> </del>	1 050 070	0.754	2 004 433	8.022	23,846,670	01100	10,278,146	10.0024	149 724	916.70	\$66,118,9
		HGD		<del> </del>	3,958,978										
CUMULATIVE TOTAL		HGD	+		/8,/43,433	0.638	50,241,351	3.703	291,585,494	0.188%	320,221,437	U.000%	14,544,704	V16.25	41,279,906,5
AF1.001 TAT		1	+	<del></del>						1				1	1000
BENCH TOTAL	1	HGD/LGD		<del></del>	8,936,095	0.410	3,661,629	3.372	30,129,649	0,141%	27,834,389	0.016%	3,154,882	111.22	\$100,303,7

								m SEARCH		ONSON SLOP					
TOTAL	IVAL	MOLY	MOLY	COPPER	COPPER		AG	AU	AU	METRIC	T	HOLE	POLYGON	BENCH	19-12-95 9:31 AM
VALUE	TONNE	POUNDS	*	POUNOS	*	GRAMS	PPM	GRAMS	PPM	TONNES	DEMITY	10	MATERIAL	HEIGHT	LEVE.
															190
	\$0.00		0 000%		0 000%					5,536,424	2 65		UDF	10	190
			3007	<del></del>	- 0000					3,500,424			-		
										5,535,424			UDF		UBTOTAL
										63,253,498			UOF		UMULATIVE TOTAL
	●0.00	1			.									<del> </del>	
	90.00													1	
	10.00														
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	10.00														
\$2,628,20	\$0.85	0	0.000%	1,359,444	0.020%	616,634	0.2	49,331	0.016	3,083,170	2.65	1220	MET		100
\$1,669,97	\$0.91	80,477		402,387	0 010%	501,929	0.275	65,707		1,825,198	2.65	1223	WST		190 190
														ļ	
44,298,18	10.88	80,477		1,761,830	0.016%	1,118,563		115,038		4,908,368			WST		UBTOTAL
\$268,239,16	\$2.71	7,659,291	0.004%	77,255,077	0.035%	77,630,856	0.785	9,613,901	0.097	98,937,246		ļ	WST		UMULATIVE TOTAL
	10.00										<del> </del>		ļ		
	●0.00										<del> +</del>	<del> </del> -	<del> </del>		
1	\$0.00														
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	0.00										<b> </b>	ļ		ļ	
	\$0.00 \$0.00										<del> </del>	<del> </del>		<del>                                     </del>	
\$15,115,41	\$5.21	127,783	0 002%	3,194,569	0.050%	7,343,703	2.534	591,206	0.204	2,898,068	2.65	1219	LGD	10	190
\$776,41	\$5.62	3,043		486,931	0 160%	36,029	0.261	9,939		136,043		958	LGD		190
\$20,422,77 \$15,286,97	\$5 63 \$6 55	1,916,601 977,427		12,777,338	0.160%	4,346,782	1.2	217,339	0.06	3,622,319		960	red		190
\$13,200,91	-8033	911,321	0.010%	8,230,960	0.160%	1,229,723	0.527	294,014	U. 120	2,333,441	2.65	959	red	10	190
851,601,56	15.74	3,024,853	0.015%	24,689,798	0.126%	12,950,238	1,441	1,112,498	0.124	8,991,870	<del> </del>		LGD	<del> </del>	USTOTAL
\$1,082,792,24	97.04	30,700,330	0.009%	403,483,934	0.119%					153,793,269			LGD		UMULATIVE TOTAL
	+											<b></b>		<del></del>	
									+		<del> </del>	<del> </del> -	<del></del>		
	\$0.00										1	1	-	<del>                                     </del>	
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	#0.00 #0.00										<b></b>				
	\$0.00										<del> </del>		<del> </del>	+	
	0.00										<del> </del>		<del> </del>	+	
	\$0.00										1	-		1	
	\$0.00														
\$1,080,9	\$0.00	346	0.0044	220 200	A 4856	204 800		20.004	0.205	~~~~~					
\$1,060,9	\$11.26 \$12.59	2,115	0 000%		0 160%	291,609 238,365	3.04	36,931 34,930		95,924 74,958		964 955	HGD HGO		190 190
\$2,295,9	\$22 98		0 001%		0.160%	771,596		104,868		99,780		963	HGO		190
\$26,264,0		27,568		4,410,839	0.160%	2,923,560		1,250,453		1,250,453		954	HGD		190
\$30,585,5	120.11				0.160%			1,427,183				-	HGD		UBTOTAL
01,310,392,1	116.33	14,576,587	0.008%	331,587,005	0.187%	295,810,625	3.685	51,668,534	0.644	80,244,548	<b> </b>	+	HGD		LIMILATIVE TOTAL
\$82,187,1	87.82	3 056 736	0.013%	30,055,366	0.130%	17,181,369	1 634	2,539,680	0.242	10.612.985	·	+	HGD/LGD		ENCH TOTAL
		2,000,130	212127	30,555,550	U. 150 A	111.01,000		2,000,000	F-8-4	,	+	+	1	+	

						250	m SEARCH	RADIU	S						
19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	IVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	D	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TOMME	VALUE
180															
100		100	1	3.05	0.043.004					0000	<del>-</del>	0000	0	\$0.00	
180	10	UOF		2.65	9,247,024	9	- 0	0	- 0	0 000%	0	0 000%		30 W	
UBTOTAL		UDF	+		9,247,024										
UMPLATIVE TOTAL		UDF			72,500,523										
				<del></del>										90.00	20 20
	<del> </del>	ļ	+											●0.00	
			1											90.00	\$0 \$0
														●0.00	\$0
														0.00	<b>20</b>
														90.00 90.00	
180	10	WST	1223	2.65	1,653,602	0.034	56,222	0919	1,519,660	0.000%	0	0.001%	38,456	\$0.75	\$1,236,382
SUBTOTAL		WST			1,853,802		56,222		1,519,660	0.000%		0.001%	38,456	90.75	\$1,238,382 \$269,477,552
CUMULATIVE TOTAL		WST	-		100,590,848	0.096	9,070,124	0.787	79,150,516	0.035%	77,255,077	0.003%	7,090,747	12.68	*203,477,332
	<del> </del>		<del> </del>	<del> </del>										●0.00	\$0
	+		<del>                                     </del>											€0.00	\$0
														●0.00	\$0
														0.00	\$0 \$0
								- 0 000		0 160%	440.044	0.001%	3,193	\$0.00 \$5.29	\$767,015
180		LG0	958		144,853 4,790,811		7,532 895,882	0.226	32,737 6,721,507	0.080%	8,449,534		316,858		\$26,446,425
180		LGD	959				354,752		2,346,278	0 160%	12,389,583		2.245,612		\$21,707,560
180		LGD	964				16,444	0 99				0 001%	2,268		\$739,984
180		LGD	963				24,531	1.01	120,275	0 160%		0.001%	2,625		\$945,993
180	10	LGD	955	2.65	131,009	0 256	33,538	0 952	124,721	0 160%	462,120	0 000%	0	\$8 73	\$1,144,380
SUBTOTAL	<del></del>	1.60	<del></del>		8 800 027		1,332,680	1.022	9,447,267	01144	22,594,785	00112	2 570 554	\$5.88	951,751,368
CUMPLATIVE TOTAL	+	LGD	+	<del> </del>					250,797,005	0.119%	426,078,719	0.009%	33,270,684	16.98	81,134,543,617
			-											90.00	**
	1	<del> </del>												10.00	\$0
														●0.00	\$(
	<del></del>					ļ		<del> </del>					<b></b>	\$0.00 \$0.00	\$X
	<del> </del>	<del></del>				<del> </del>	<del></del>					<del> </del>	<del> </del>	10.00	8
	<del>                                     </del>	1	+	-	-	<del> </del>								\$0.00	3
														10.00	\$
														0.00	ä
		-	4								ļ			\$0.00	\$
					<del> </del>									\$0.00	\$
	+	<del> </del>		+		<del> </del>			<del> </del>			<del> </del>		\$0.00	\$
180	1	HGD	95	2.65	1,400,875	1.433	2,007,453	0.672	941,388	0.160%	4,941,434	0 000%		\$27 59	\$38,663,74
SUBTOTAL		HGD					2,007,453			0.160%	4,941,434	0.000%		027.60	\$38,663,74
CUMULATIVE TOTAL		HGD		<del></del>	01,005,423	0.657	53,675,967	3,634	296,752,013	0.187%	336,528,439	0.006%	14,576,587	116.52	01,349,055,86
BENCH TOTAL		HGD/LGD			10,201,801	0.327	3,340,133	1.018	10,389,865	0.122%	27,536,216	0.011%	2,570,554	18.86	890,415,11
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				BR	IONSON BLO					RAPHY					
							m SEARCH								
19-12-96 9:31 AM	SENCH	POLYGON	HOLE		METRIC	_AU	AU	_ AG	AG	COPPER	COPPER	MOLY	MOLY	OVAL	TOTAL
TENE	HEIGHT	MATERIAL	0	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	*_	POUNDS	*	POUNDS	TONNE	VALUE
170		<del> </del>	<del> </del>												
170	10	UDF	<del> </del>	2.65	9,336,639	0	0	0		0 000%		0 000%	Ö	\$0.00	
	<del>                                     </del>	-			0,500,500					0000					
SUBTOTAL		UDF			9,336,639										
CUMULATIVE TOTAL		UDF	1		81,837,182										
														\$0.00	\$0
														♦0.00	\$0 \$0
														♦0.00	\$0
														#0.00	\$0
			-											\$0.00	\$0
														10.00	\$0
	ļ	<del></del>	ļ											\$0.00	\$0
			<del> </del>	ļ								0.0012		•0.00	\$0
170	10	WST	1223	2 65	1,497,270	0.04	59,891	0 985	1,474,811	0 020%	550,182	0 001%	33,009	81 41	\$2,112,730
SUBTOTAL		MCT			1 407 330	0.040	60.001	0.005	1 474 611	0.020%	860 183	0.0012	33,009	\$1,41	\$2,112,730
SUBTOTAL CUMULATIVE TOTAL		WST	+		1,497,270 102,088,118		59,891	0.985	1,474,811		77,915,269				0271,690,282
COMOCATIVE TOTAL	<del> </del>	+ vv. b			102,000,110	<u> </u>	_ B'\20'01 8	0,780		_9.035.4	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	0.005.2	, , , , , , , , , , , , ,		
	<del> </del>		<del> </del>											#0.00	\$0
	1	1	<del> </del>											10.00	\$0
			1											10.00	\$0
														\$0.00	\$0
														10.00	\$0
170		LGD	958	2.65	168,612		9,105	0.2				0.000%	0		\$897,278
170	10	LGD	964	2.65	138,055	0.056	7,731	0.335	46,248	0 160%		0 001%	3,044		\$743,208
170	10	LGD	959	2 65	3,527,853	0.086	303,395	0.483	1,703,953	0.160%	12,444,122		3,033,255		\$20,808,619
170	10	LGD	955		185,918	0 089	16,547	0.765				0 000%	0		\$1,117,121
170	10	LGD	1219	2 65	4,797,658	0.258	1,237,796	1 16			8,461,609		528,851	\$6 60	\$31,705,128
170	10	LGD	963	2.65	122,685	0.232	28,463	0 578	70,912	0.160%	432,757	0.001%	2,705	\$8 26	\$1,014,229
														<u> </u>	
SUBTOTAL		LGD			8,940,781	0.179	1,603,037	0.846	7,562,346		23,076,029				<b>\$56,285,503</b>
CUMULATIVE TOTAL		LGD		L	171,534,977	0.208	35,500,139	1,506	250,359,351	0.119%	449,154,748	0.010%	30,838,738	96.94	\$1,190,829,200
				<del> </del>				<del> </del>							
	1													\$0.00	\$0
	<del> </del>	<del> </del>	<del> </del>	+					<del></del>	<del> </del>	<del></del>		<del></del>	\$0.00	80
·	<del> </del>	<del></del>	<del></del>	+		<del> </del>				<del>                                     </del>		<del> </del>	<del> </del>	\$0.00	\$0
}	+	<del> </del>	<del> </del>	<del> </del>		<del> </del>	<del> </del>							90.00	
	<del> </del>	+	<del> </del>	+		<del> </del>	<del> </del>		<del> </del>	<del>                                     </del>			<del></del>	10.00	\$0 \$0
<del></del>				-	1				-			-		\$0.00	\$0
	<b>—</b>	1	1	<del>                                     </del>	†	1								\$0.00	\$0
	I	I								1				10.00	\$0
						I								♦0.00	\$0
	-	1	-											\$0.00	20 20
				<del></del>										10.00	50
		-	+			-								●0.00	\$0
454	<del> </del>	0.00	+			1000							L	●0.00	
170	10	HGD	954	2.65	1,514,105	0.871	1,318,786	0.79	1,196,143	0.160%	5,340,843	0.000%	0	\$18 58	\$28,145,280
CLATOTAL	+	1460		<del> </del>									ļ		
SUBTOTAL	+	HGO	<del> </del>	<del> </del>			1,319,786					0.000%	0	118.59	\$28,145,280
CUMULATIVE TOTAL	<del></del>	HGD	<del></del>		<b>#3,179,528</b>	0.661	54,394,773	3.582	297,948,156	0.106%	341,000,202	0.008%	14,576,587	016.56	01,377,201,145
		1		<b></b>				<u> </u>		<u> </u>	ļ			ļ	
BENCH TOTAL		HGD/LGD			10,454,886	0.279	2,921,822	0.038	9,758,489	0.123%	28,416,872	0.015%	3,567,854	18.08	\$84,430,863
	<b></b>		1	1		1	1			1	L			L	
CUM, BENCH TOTAL		HGD/LGD		1	254,714,500	0.350	90,600,911	2.184	556,307,507	0.141%	791,024,030	0.009%	51,415,324	\$10.00	12,568,030,344

19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	M SEARCH	AG	AG	COPPER	COPPER	MOLY	MOLY	IVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	10	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	*	POUNDS	TOMME	VALUE
160															
160	10	UDF		2.65	9,501,122	0	0		0	0.000%		0.000%	ō	\$0.00	<del></del>
	10	00-		2.00	8,301,122					0.000%		0.000%		- ww	
UBTOTAL	<b>†</b>	UDF	<b></b>		9,601,122										
UMULATIVE TOTAL		UDF			91,338,284										
	ļ														
			<del> </del>											\$0.00	\$1 \$1
	<del> </del>	<b></b>											<del>-</del>	10.00	
														●0.00	\$0
														90.00 90.00	\$0 \$0
	<del>                                     </del>		<del> </del>	<del>-</del>										\$0.00	
														●0.00	
														•0.00	
SUBTOTAL	<del> </del>	WST	<del> </del>		0	0.000	0	0.000	o	0.000%	0	0.000%	0	\$0.00	90
UMULATIVE TOTAL		WST							80,625,326		77,915,259		7,728,756	12.66	4271,590,282
														●0.00	
	+		<del> </del> -	<del> </del>										\$0.00	8
	<del>                                     </del>		<del>                                     </del>	<del>                                     </del>										10.00	SC
														\$0.00	\$X
														10.00	\$(
160	+	LGD	955	2 65	272,447	0.047	12,805	0 291	79,282	0.160%	981 026	0 000%	0	\$0.00 \$5.23	\$1,424,628
160		LGD	1219		4,785,841		961,954		2,933,721				633,058	\$5 29	\$25,345,73
160		LGD	958		997,347		79,788		372,010		3,518,033		0	\$5.78	\$5,762,37
160		LGD	959		3,538,639		318,478	0.3	1,061,592				2,730,474		\$20,957,370
160	10	LGO	963	2.65	120,311	0.221	26,589	1.265	152,194	0.160%	424,385	0.000%	0	\$8.24	\$991,51
SUBTOTAL	+	LGD			9 714 585	0 144	1,399,613	0.473	4,598,798	0.116%	24,771,284	0.016%	3.363.532	#5.61	954,481,620
CUMULATIVE TOTAL	1	LGD	1						262,958,150		473,926,032				11,245,310,820
	<del></del>	ļ	<del> </del>							<del> </del>					·····
	+	<del>                                     </del>	<del> </del>											●0.00	
														\$0.00	\$
														\$0.00 \$0.00	\$
	+		-											●0.00	\$
	1	<del>                                     </del>	1											●0.00	S
														●0.00	
		<del> </del>	<del></del>	ļ							<del></del>			\$0.00 \$0.00	\$
	<del> </del>	<del> </del>						-		<del> </del>	<del> </del>			♦0.00	•
		<del> </del>	1	<del> </del>				1						\$0.00	\$
														\$0.00	s
160		HGD	964					3.606				0.001%		\$11.03	
160	10	HGD	954	2.65	1,957,209	0.481	941,418	0.969	1,896,536	0.160%	6,903,845	0.001%	43,149	\$12.35	\$24,185,04
SUBTOTAL	<del></del>	HGD		<del> </del>	2 151 527	0.470	1,011,991	1.207	2,597,606	0.160%	7,589,632	0.001%	47 435	912.24	\$26,331,33
CUMULATIVE TOTAL		HGD	-	-			56,006,764		300,545,761	0.186%				116.45	11,403,532,47
	1	<u>. I</u>			I	Ţ				I		I			
BENCH TOTAL		HGD/LGD	+		11,866,212	0.203	2,411,604	0.606	7,196,404	0.124%	32,360,916	0.013%	3,410,967	96.81	80,812,95
CUM. BENCH TOTAL		HGD/LGD	<del> </del> -	<del> </del>	300 500 313	0.340	93 013 515		563,503,911	0.1105		0.0000	84 922 251	45.5	12,648,843,29

250m SEARCH RADIUS															
19-12-96 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	OVAL	TOTAL
TEAB	HEIGHT	MATERIAL	ID.	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	*	POUNDS	*	POUNDS	TONNE	VALUE
150															
			L											\$0.00	
150	10	UDF	1	2.65	17,541,668	0	0	0		0.000%	0	0.000%	0	30 00	
MYOTA!		UDF	<del> </del>		17,541,666									<del></del>	
UBTOTAL	<del>}</del>	UDF	-		108,879,950									+	
UMULATIVE TOTAL	<del> </del>	007			100,579,950									<del></del>	
	<del> </del>													\$0.00	\$
	<del> </del>		t											10.00	
	<del> </del>		<del>  </del>											\$0.00	
	<b></b>		-											10.00	
			1											\$0.00	
	1													\$0.00	3
	1													10.00	- 5
														●0.00	s
150	10	WST	958	2.65	1,013,328	0 033	33,440	02	202,666	0.160%	3,574,408	0.000%	0	\$4.98	\$5,050,30
	1											I			
UBTOTAL	1	WST			1,013,320		33,440	0.200	202,666	0.160%	3,574,408		0		<b>#5,050,30</b>
UNAULATIVE TOTAL		WST			103,101,446	0.095	9,763,455	0.784	80,827,992	0.036%	81,489,685	0.003%	7,728,750	12.66	<b>#276,640,58</b>
			1												
														●0.00	
	1													00.00	s
														10.00	
	1													\$0.00	
														10.00	3
														\$0.00	
	T													\$0.00	
									2.0.000	0.4604	904 473	0.000%	o		\$1,673,44
150		LGD	984				37,174		318,606	0.160%		0.000%	2,769		\$1,135,54
150		LGO	963		125,597		33,283		211,631	0.160%	1,054,772		6,592		\$2,756,30
150	10	LGD	955	2.65	299,023	0.25/	76,849	3.057	914,114	0.100%	1,034,112	000.2	0,302		<b></b> ,,
		<del> </del>	<del> </del>	<del> </del>		0 220	147 207		1,444,351	0.160%	2,302,275	0.001%	9,361	18.53	15,564,29
SUBTOTAL		LGD		<del> </del>	652,685				264,402,501	0.100%	470,228,306	0.010%	40 211 631		01,250,875,11
CUMULATIVE TOTAL	1	LGD	1		101,302,240	0.20	37,133,030	1.404	203,300	<u> </u>		-			
	<del> </del>		<del> </del>											●0.00	
	-		+	+		<del> </del>		-						10.00	
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	+	<del> </del>	+	<del> </del>				<del> </del>						10.00	
	-	-	+			1								●0.00	
	+	<del> </del>	+	<del> </del>										10.00	
	<del> </del>	<del> </del>	+	<del> </del>		-							1	10.00	
	-	<del> </del>	1	<del> </del>	<del> </del>	<del>                                     </del>		t				1		10.00	
		1	+	1		1								\$0.00	
	+		1	<u> </u>		1								10,00	
	+	1	1			1								10.00	
	+	1		1			1							●0.00	
	1	1	1	1				1						10.00	
150	10	HGO	954	2.65	2,180,106	1.34	2,921,342	1.032	2,249,869	0.160%	7,690,088	0.001%		\$26.17	\$57,082,7
UBTOTAL	1	HGD HGD	-		2,180,106	1.340	2,921,342	1.032	2,249,869 302,795,631				48,063	126.18	\$57,082,7 61,460,615,2
OMULA IOIAL		MGU	+	+	87,811,201	0.6/3	20,525,100	3,400	302,183,631	V. 18576	357,148,002	U.505 %	1-1-12	7.0.05	1,100,010,0
SENCH TOTAL	1	HGD/LGD	-	-	2,832,791	1.083	3,068,649	1.304	3,694,220	0.160%	9,992,363	0.001%	57,424	022.11	982,647,0
					1										

						250	m SEARCH	RADIL	18						
19-12-95 9:31 AM LEVEL	BENCH	POLYGON	HOLE	DENSITY	METRIC TONNES	AU	GRAMS	AG PPM	AG GRAMS	COPPER	COPPER	MOLY	MOLY	TONNE	TOTAL
140	1.20		<del>  -  </del>	0000111			9/5/110				-700,000	-~-	-,00.00	10,000	- 17.00
140	10	UDF		2.65	17,790,836	0	0	0	0	0.000%	0	0 000%	0	\$0.00	
UBTOTAL		UDF	1		17,790,636										
CUMULATIVE TOTAL	<del>}</del>	UDF			126,670,785									<del></del>	
	-		-											€0.00	1
														10.00	
														0.00	
														\$0.00 \$0.00	
			1											10.00	
														10.00	
			1											\$0.00	
			1											\$0.00	
UBTOTAL		WST	1		0	0.000	0	0.000	o	0.000%	0	0.000%	0	90.00	
UMULATIVE TOTAL		WST			103,101,446		_		80,827,992	0.036%			7,728,756	12.68	1276,640,5
	-														
	<del></del>	<del> </del>	1											0.00	
	<del> </del>	<del> </del>	-											<b>♦0.00</b>	
		<del> </del>	+											\$0.00	
			1											●0.00	
	1													\$0.00	
														₩0.00	
							70.000		426 700	0.4600	2 700 000	00010	48,138	\$5.03	\$10,987,6
140		LGD	955		2,183,500 1,035,636		78,606 38,319	0.2	436,700 207,127	0.160%	7,702,060 3,653,095		70,130	\$5.05	\$5,228,0
140		LGD	958		137,724		13,221		84,582	0.160%		0 001%	3,036	\$6.09	\$838,4
	<del></del>	1	+												
JUBTOTAL		LGD			3,356,860	0.039	130,146				11,840,960	0.001%	51,174	15.08	817,054,1
CUMULATIVE TOTAL		LGO			185,259,106	0.201	37,283,204	1.431	265,130,890	0.120%	488,009,266	0.010%	40,262,905	*0.84	\$1,267,929,3
		<u> </u>												\$0.00	
	<del> </del>	1	+	<del> </del>										\$0.00	
														●0.00	
													ļ	10.00	
	+		<del></del>								ļ		<u> </u>	90,00 90.00	
												-		\$0.00	
														\$0.00	
			-											\$0.00	
			+			-								<b>♦0.00</b>	
	1		+											\$0.00	
														0.00	
140	10	HGD	964	2.65	251,174	0.392	98,460	8.319	2,089,520	0.160%	885,991	0.001%	5,537	\$12.52	\$3,150,4
UBTOTAL	<del> </del>	HGO	+		251,174	0.392	98 460	8.319	2,089,520	0.180%	885,991	0.001%	5.537	112.54	\$3,150,4
UMULATIVE TOTAL	1	HGD	1					3.474	304,885,151				14,077,622	116.68	11,463,765,6
ENCH TOTAL		HGD/LGD	-		3,608,034	0.063	228,506	0.781	2,817,910	0.160%	12,726,951	0.001%	56,712	15.60	920,204,6
UM. BENCH TOTAL	+	HGD/LGD		<b></b>	273,021,541				670,016,041		846,104,259	L			

THE STATE WAS THE STATE WETAL VALUES

BRONS ON SLOPE RESOURCE - CORRECTED TOPOGRAPHY 250m SEARCH RADIUS															
19-12-95 9:31 AM LEVEL	BENCH	POLYGON	HOLE	DENSITY	METNC TONNES	AU	AU GRAMS	AG PPM	AG GRAMS	COPPER	POUNDS	MOLY	MOLY POUNDS	TONNE	VALUE
130															
										0.0004		0 0000			
130	10	UDF		2.65	18,584,009	0	0		0	0.000%		0 000%	0	\$0.00	
UBTOTAL		UDF			18,584,009										
UMULATIVE TOTAL		UDF	<del> </del>	<del> </del>	145,254,794									-	
OMODATIVE TOTAL		-	<del>                                     </del>	1	140,254,754	-									
			<u> </u>											90.00	
														\$0.00	
														\$0.00	
														\$0.00	
			<del> </del>	ļ		-								<b>●0.00</b>	
														●0.00	
														●0.00	
130	10	WST	958	2 65	1,448,604	003	43,458	8.2	289,721	0.160%	5,109,796	0.001%	31,936	\$4.93	\$7,149,79
	<del> </del>	1	1 30		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		,								
USTOTAL		WST	1		1,448,604			0.200	289,721	0.160%	5,109,796		31,936	14.94	17,149,79
WALLATIVE TOTAL	1	WST			104,550,051	0.094	9,806,913	0.776	81,117,713	0.038%	66,599,461	0.003%	7,760,692	82.71	1283,790,37
														40.00	
														90.00	
		-	<del>}</del>											\$0.00 \$0.00	
	<del></del>	<del></del>	<del> </del>	<del> </del>		├				<del> </del>				●0.00	
	+		1											10.00	
														●0.00	
														\$0.00	
			<del> </del>			lI				<del></del>				\$0.00	
130	10	LGD	964	2 65	1,226,115	0 03	36,783	0.8	980,892	0.160%	4,324,987	0.001%	27,031		\$6,213,50
130		LGO	963				17,798		127,949			0.001%	3,090		\$932,20
SUBTOTAL		LGD			1,366,257		54,581								17,145,76
CUMULATIVE TOTAL		LGD			186,625,363	0.200	37,337,786	1.427	266,239,731	0.120%	492,888,589	0.010%	40,292,926	\$6.83	<b>\$1,275,075,0</b> 7
			_											\$0.00	
			+	<del></del>		-		-						10.00	
		<del> </del>	<del></del>	<del> </del>						<del> </del>				●0.00	
	+	<del> </del>	+	<del> </del>										\$0.00	
	+	-	1	<del> </del>										\$0.00	
			1	1										#0.00	
			1											●0.00	
														40.00	
			-								<b></b>	<del> </del>	<del></del>	\$0.00 \$0.00	<u> </u>
	+	<b></b>			<del></del>							<del> </del>		\$0.00	<del></del>
	+	<del> </del>		<del> </del>		-		-						10.00	
	+	+	+	<del> </del>	<del> </del>			-		1	<del> </del>			\$0.00	
		1												10.00	
SUBTOTAL		HGD				0.000		0.000		0.000%		0.000%	0		42 422 222 2
CUMULATIVE TOTAL		HGD	+		67,762,435	0.673	55,026,567	3.474	304,885,151	0.185%	358,034,993	0.000%	14,6/7,622	916.50	11,463,765,6
SENCH TOTAL	#==	нарлар	+	-	1,360,257	0.040	54,581	0.812	1,108,841	0.160%	4,819,322	0.001%	30,121	05.23	97,145,7
UM. BENCH TOTAL		HGD/LGD		+	274,387,798							L			92,736,840,7

BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY 250m SEARCH RADIUS															
19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	IVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	10	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	*	POUNDS	TONNE	VALUE
120															
120	10	UDF		2 65	10 407 730	0	0	0	0	0.000%		0 000%	-	\$0.00	
120	10	ULF		200	19,497,730	<del>'</del>				0.000%		U WW		- <b>2</b> 00	
UBTOTAL		UDF	-		19,497,730										
CUMULATIVE TOTAL		UDF			164,752,524										
														10.00	<del></del>
				<del></del>							<del></del>			\$0.00	\$
														●0.00	9
														10.00	
														10.00	
														\$0.00 \$0.00	
				<del> </del>										10.00	<u>\$</u>
														40.00	
USTOTAL		wst				0.000		0.000		0.000%		0.000%	7 700 002	90.00 92.71	1283,790,37
CUMULATIVE TOTAL		WST	<b> </b>		104,860,061	0.094	9,806,913	0.778	81,117,713	0.036%	86,599,461	0.003%	7,700,092	•2./1	¥263,780,376
	<del> </del>	<del></del>												●0.00	9
														\$0,00	s
	I													00.00	<u>\$</u>
														\$0.00 \$0.00	
		<del></del>		<del> </del>										\$0.00	s
	1		1											\$0.00	
														●0.00	5
						<u> </u>								\$0.00 \$0.00	
120	+	LGD	963	2.65	1,901,139	0.155	294,677	3.258	6,193,912	0.160%	6,706,064	0.001%	41,913	\$7.61	\$14,483,64
120	<del>                                     </del>	100			.,,,,,,,,	91.100									
SUBTOTAL		LGD			1,901,139	0.155	294,677	3.258	6,193,912	0.160%	6,706,064	0.001%	41,913	97.62	014,483,64
CUMULATIVE TOTAL		LGD			188,526,502	0.200	37,632,462	1.445	272,433,644	0.120%	499,594,663	0.010%	40,334,838	₹0.B4	61,289,658,71
	1														
			<del> </del>											10.00	
	<del> </del>	<del> </del>	<del> </del>	<del> </del>	<del></del>	-								10.00	
														\$0.00	
														\$0.00	
	<del> </del>	<del> </del>	<del> </del>	<del> </del>							<del></del>		<del> </del>	90.00	
	1	<b> </b>		<del>                                     </del>		1								●0.00	
														●0.00	
	<del> </del>		<del> </del>	<del> </del>										10.00	
	<del> </del>	<del> </del>		<del>}</del>								<del></del>		<b>00.00</b>	<del></del>
	1	<del></del>	+	<del> </del>		-								\$0.00	
	1			1	1									10.00	
														10.00	
CLERTOTAL		WCD.				0.000		0.000	0	0.000%		0.000%	0	10.00	
SUBTOTAL CUMULATIVE TOTAL		HGD							304,885,151						11,443,765,64
BENCH TOTAL	+	HGD/LGD	+		1,901,139	0.155	294,677	3,258	6,193,912	0.160%	8,708,084	0.00176	41,913	07.62	014,483,64
CUM, BENCH TOTAL		HGD/LGD			276,288,937	0.350	96,659,029	2.090	577,318,794	0,141%	857,629,645	0.009%	55,012,461	19.97	\$2,753,324,37

THE REPORT OF THE PARTY OF THE