

**INTERNATIONAL SKYLINE GOLD CORPORATION**

**SUMMARY OF 1995 EXPLORATION WORK ON THE RED BLUFF AREA  
BRONSON SLOPE PROJECT**

**FOR  
EXPLORE B.C.**

**BY  
SANDY MARTIN, B.A.Sc.**

**February 22, 1996**

*95/96 - m67*

**GEOLOGICAL SURVEY BRANCH  
ASSESSMENT REPORT**

**25,373**

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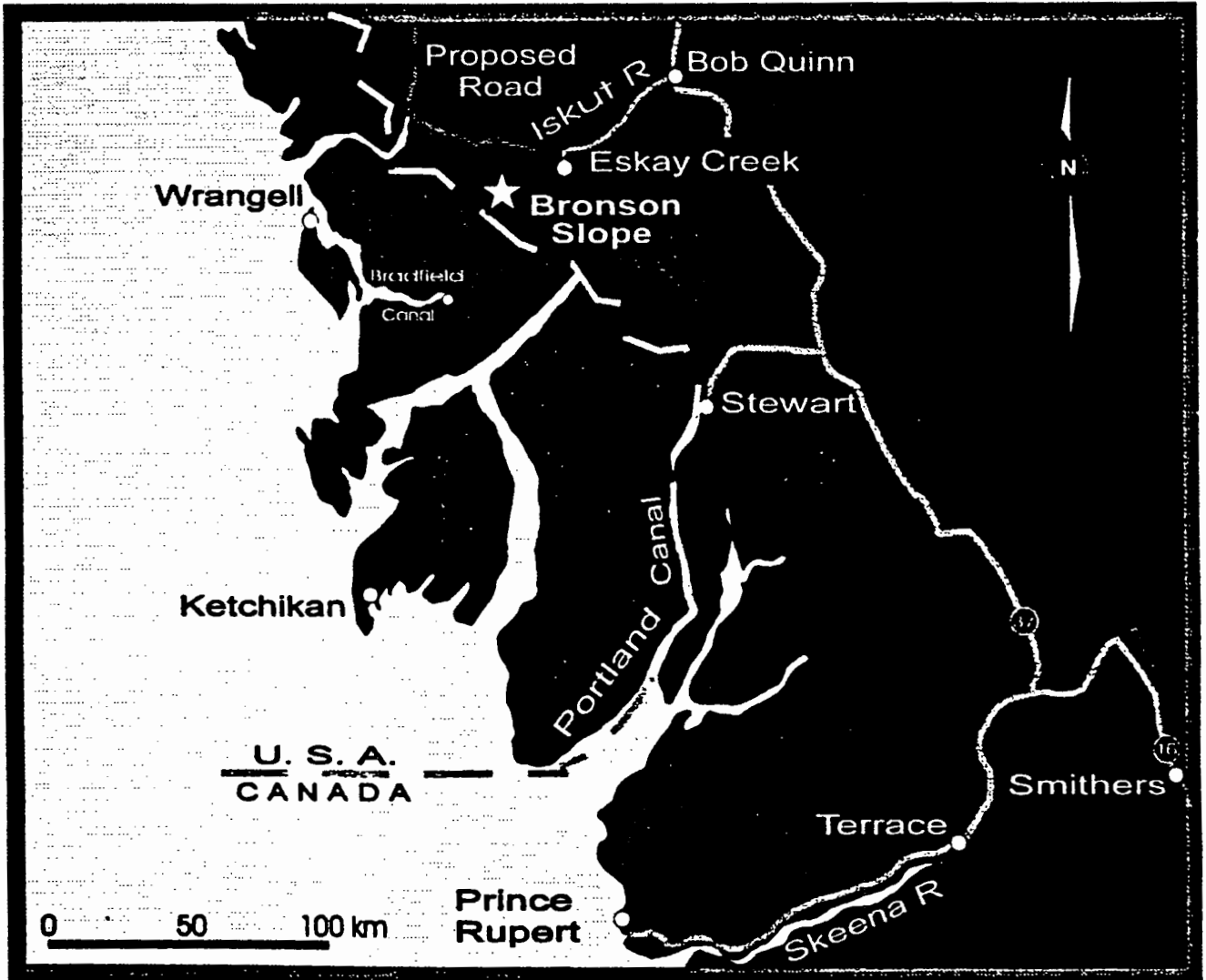
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## **1.0 INTRODUCTION**

During the period of April to October 1995 International Skyline Gold Corporation performed a number of exploration programs on its Bronson Slope porphyry gold, copper, silver, molybdenum deposit located in the Iskut River region adjacent to the Johnny Mountain mine of International Skyline and the Snip mine of Cominco (see figure 1). The exploration programs allowed International Skyline to refine its resource estimation to an inferred resource of 90 million tonnes containing 0.749 grams gold/mt, 0.159% copper, 4.17 grams silver/mt and 0.005% molybdenum. The minimum estimated mineable resource contains 56,728,000 tonnes of ore grading 0.545 grams/tonne gold, 2.4 grams/tonne silver, 0.18% copper, and 0.01% molybdenum. The deposit realizes an ultimate strip ratio of 0.29:1 waste to ore.

The exploration programs comprised the following:

- A review of the drill core from the 1994 drilling program to identify potential controls on the distribution of mineralization.
- Surveys were carried out to identify the dip and orientation of previous drill holes. Surveys were also completed to accurately establish the location and dip of drilling to be accomplished in the 1995 program.
- A diamond drill program consisting of 7 drill holes totalling more than 10,000 feet in length.
- Using the information generated from the exploration a new resource model was completed.
- As a result of the 1995 exploration program, International Skyline Gold Corporation submitted an Approval Certificate Application as the first step in the Environmental Approval Process to develop the Bronson Slope Deposit.



**LOCATION MAP  
BRONSON SLOPE PROJECT**

INTERNATIONAL SKYLINE GOLD CORP.

OCTOBER 1995

FIGURE 1

## **2.0 HISTORY OF WORK**

The earliest recorded work on the deposit was by the Iskut Mining Company who performed between 1907 and 1920, surface and minor underground exploration of a number of base and precious metal prospects on the south-west slope of Bronson Creek valley.

The next phase of work for which accurate records are available was done during the period of 1962 to 1965 during which time Cominco Ltd. had an option to develop the ground. Both regional and property scale surface mapping and prospecting were performed. This culminated in 1965 with a pack sack drill program comprising seven holes for a total of 1105 feet of drilling. This program discovered several areas of promising copper and molybdenum mineralization, however the low gold prices prevailing at the time prohibited realization of the potential of the deposit.

During the construction, in 1987, of the Johnny Mountain mine facilities by Skyline Explorations Ltd., several contour lines were soil sampled in the vicinity of the Red Bluff as a preliminary step to performing a comprehensive exploration program to rediscover the object of the early 1900s prospecting and claim staking activity. The soil samples contained, among other metals, extremely high gold values. In 1988, following initial grid soil sampling and prospecting, a total of 1938 meters of diamond drilling was performed in five areas of the Bronson Slope, defined by anomalous gold concentrations in rock and soil samples and by base metal sulphide mineralization. The object of the drilling was to locate high grade concentrations of precious metals similar to the nearby Stonehouse and Twin zone deposits and therefore it was directed at mineralized cross structures. Again, promising low grade concentrations of gold, copper and molybdenum were found but the values encountered were insufficiently high to interest the company in continuing the program.

After a corporate reorganization in 1992, attention was directed to evaluating the low grade potential of the deposit. In 1993, International Skyline Gold Corporation performed an Induced Polarization survey of the deposit and the surrounding alteration zones and completed 872 meters (7 holes) of fence drilling of two cross sections of the deposit. The program was successful in partially delineating a gold, copper porphyry system. In 1994, the company commissioned a computer model and reserve estimate of the deposit using polygonal weighting by levels and preliminary metallurgical studies of composited core samples. The studies confirmed the presence of a significant low grade reserve with very favourable froth flotation recovery characteristics of both gold and copper and were pivotal in giving the company the confidence to progress with exploration of the deposit. The studies were followed by a seven hole drill program totalling 951 meters. The drilling explored undefined zones within the reserve block and untested zones along strike from the deposit. The presence of a high grade zone within the deposit was indicated. Following drilling, detailed surface mapping was performed over the deposit area to try to correlate structural geologic information with observations of the mineralization from core logging.

In addition, the mapping defined the limits of the surface trace of the high grade core of the deposit.

### **3.0 THE 1995 EXPLORATION PROGRAM**

#### **3.1 REVIEW OF 1994 DRILL CORE**

In April and May of 1994, David Rhys, a consulting geologist, was engaged by International Skyline to review the core from the 1994 diamond drilling program on Bronson Slope (hole numbers S1208-S1216 inclusive). The core was quick logged to identify potential controls on the distribution and mineralization with respect to alteration and vein type, structure and lithology. A core library of type samples was also compiled. Details of the review are contained in Appendix 1.

#### **3.2 SURVEY PROGRAMS**

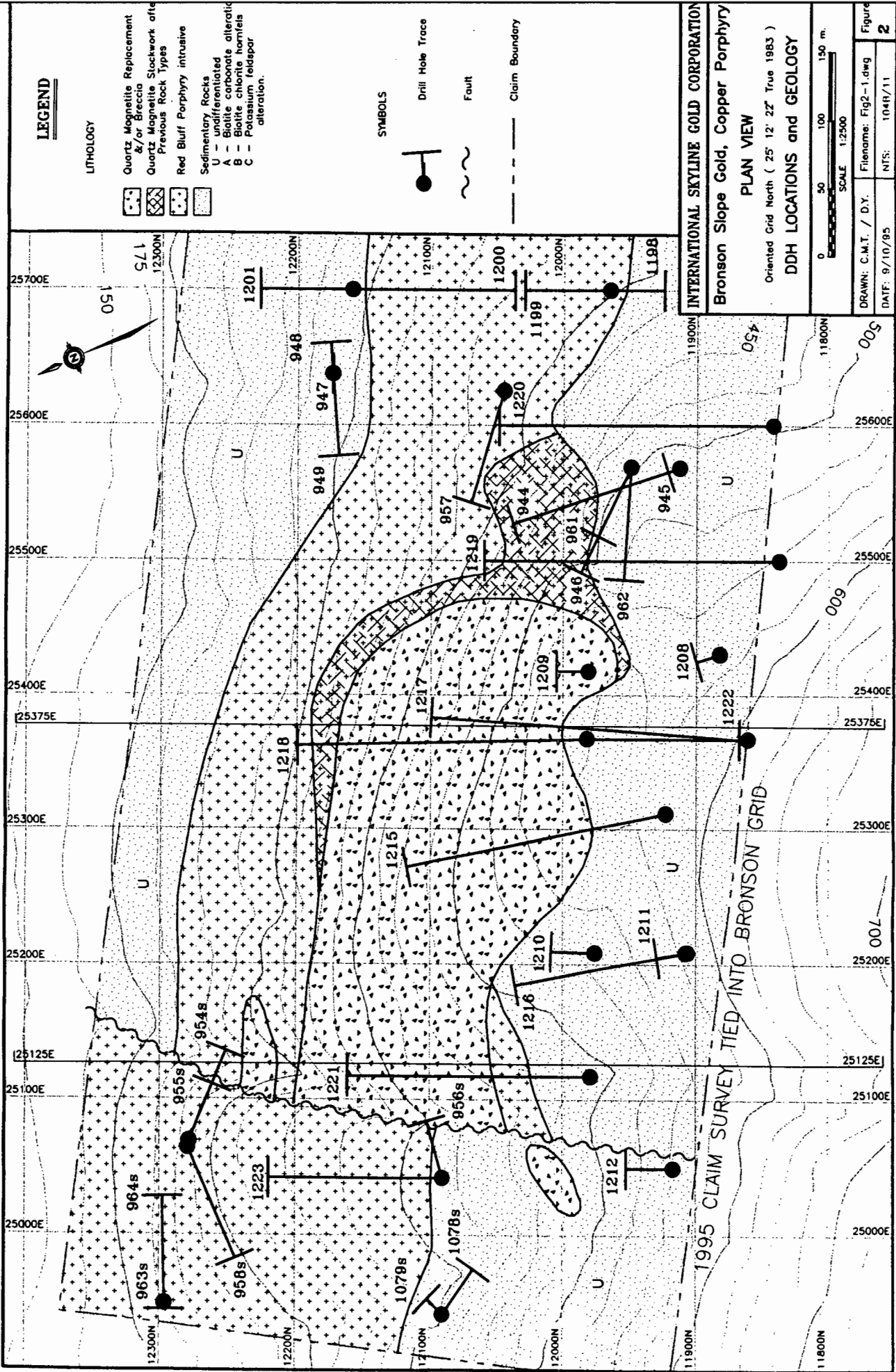
In May 1995, a surveying program was carried out on Bronson Slope to (1) accurately establish the location, dip, and dip direction of diamond drill holes from the previous 1994 diamond drilling program, and (2), to precisely orient and locate drilling for the upcoming 1995 program. Results from the surveys allowed the new resource model to be built with greater precision.

A second survey was performed between July 16 and July 25 1995 by Mathews and Lloyd Professional Land Surveying Ltd. to establish the precise claim boundaries between International Skyline and the Cominco-Snip Joint Venture..

#### **3.3 1995 DIAMOND DRILLING**

A diamond drilling program consisting of seven holes and totalling more than 10,000 feet was conducted on Bronson Slope. Supervision was provided by David Yeager (P. Geo. and Chief Geologist, International Skyline Gold ) and Cameron Scott. Additional geological services were provided by Lou Straith. Locations of drill holes on the Red Bluff can be seen in figure 2 including those from 1995 (S1217 - S1223, inclusive). Drill logs can be reviewed in Appendix 2.

Cover sheets for the drill logs could not be located, if indeed they exist. Details regarding locations and elevations were included with the drill logs, however, exact dates of the start and conclusion of each hole are not available. It can be assumed that all drilling was concluded prior to July 14, 1995.



**LEGEND**

**LITHOLOGY**

- Quartz Magnetite Replacement &/or Breccia
- Quartz Magnetite Stockwork of Previous Rock Types
- Red Bluff Porphyry intrusive
- Sedimentary Rocks

- U - undifferentiated alteration
- A - Biotite carbonate alteration
- B - Biotite chlorite hornfels
- C - Potassium feldspar alteration

**SYMBOLS**

- Drill Hole Trace
- Fault
- Claim Boundary

**INTERNATIONAL SKYLINE GOLD CORPORATION**  
**Bronson Slope Gold, Copper Porphyry**  
**PLAN VIEW**  
 Oriented Grid North ( 25° 12' 22" True 1983 )  
**DDH LOCATIONS and GEOLOGY**

0 50 100 150 m.  
 SCALE 1:2500  
 DRAWN: C.M.T. / D.Y.    File name: Fig2-1.dwg    Figure  
 DATE: 9/10/95    NTS: 1041/11    2

1995 CLAIM SURVEY TIED INTO BRONSON GRID

Tables indicating the assay results for each of the 1995 holes are included in Appendix 3.

As of the date of this report, although the drilling results have been fully assessed, no comprehensive analysis or conclusions have been compiled in the form of a geological report. The reader is referred to the Geology and Project Description sections of International Skyline's Bronson Slope Mine Approval Certificate Application duplicated in Appendix 4. These listed sections were generated using the 1995 drilling results and represent the most recent compilation of geologic data on the Bronson Slope Project.

### **3.4 COMPUTER MODEL AND RESERVE ESTIMATE**

The entire drill hole database was computerized and a reserve estimate calculated using PC-EXPLOR software from Gemcom Services in Vancouver. This work made it possible to identify zones within the deposit that were undefined or incorrectly defined by previous drilling due to insufficient density of data or due to a lack of accurate assay information.

The study was performed by Christopher M. Turek, P.Eng, Chief Engineer, International Skyline Gold Corporation. Reserve polygons based on drill hole assay composites were prepared for 10 meter elevation slices of the deposit. The report is presented in Appendix 5.



#### **4.0 CONCLUSIONS**

International Skyline Gold Corporation feels that the exploration program of 1995 has allowed the Bronson Slope Project to advance to the initial mine development phase. Encouraging results from the 1995 exploration program have led to:

- the Company's application for the construction of a spur road extension to the existing Eskay Creek Road which will lead to the Bronson Slope project location;
- an application to the Environmental Assessment Office (included as part of the Bronson Slope Certificate Application) for permission to construct a 20 MW run of river, hydro-electric generation facility on the Iskut River to supply power to the project;
- a geotechnical study by R.C. Dick, P.Eng. (Geotechnical Engineering Consultant), into the proposed Bronson Slope Project Sky Creek tailings impoundment locations and creek diversions;
- a design study for the Bronson Slope pit, including a starter pit;
- a study by Fluor Daniel Wright Ltd. (Vancouver) on various ore pass and crushing options for the Bronson Slope Project;
- a mill facility report on mineral processing options was completed by Rescan Engineering and a mill flowsheet was generated.

The company intends to continue to pursue Provincial environmental approval for the Bronson Slope Project. A 12 hole drilling program is anticipated on Bronson Slope for the 1996 exploration season. A number of environmental and geotechnical studies are anticipated for 1996. The company also intends to update the reserve following the seasons drilling as well as to conduct further metallurgical research on the Bronson ore. The feasibility of recovering and marketing the deposit's magnetite, which constitutes an estimated 11% of the resource, will also be investigated.

Respectfully Submitted,



Sandy Martin, B.A.Sc.

**APPENDIX 1**

**Report of 1994 Drill Core Review**

David Rhys  
Consulting Geologist  
1077 Gordon Avenue  
West Vancouver  
B.C.  
V7T 1P7

May, 1995

**Memo:**

**To:** D. Yeager, International Skyline Gold Corp.

**Re.:** Red Bluff porphyry (Bronson Slope Project) - geology, core library and core logging procedures

This memo reports the results of a review of 1994 drill core from the Red Bluff porphyry by the author, with assistance by Al Chapman. The work was completed at the Pamicon camp, located at the north end of the Bronson Creek airstrip, northwestern British Columbia, between April 26 and May 2, 1995. The core from drill holes S1208 to S1216 (inclusive) was examined and quick logged to identify potential controls on the distribution of mineralization with respect to alteration and vein type, structure and lithology. In addition, a core library of type samples was created for future reference.

The reader is referred to Rhys (1995) for a description of the geologic setting and exploration history of the Red Bluff area and to Moore (1994) and Weekes (1994) for a summary of the 1994 exploration program. The observations reported here, however, supersede those made by Rhys (1995) on the alteration, vein types and distribution of mineralization within the Red Bluff porphyry system.

**Geology and mineralization related to the Red Bluff porphyry:**

*Lithologies*

The Red Bluff porphyry hydrothermal system is spatially associated with, and overprints a northwest-trending body or series of dykes of an Early Jurassic intrusion. The porphyry intrusion (195±1 Ma), termed the Red Bluff porphyry, is a K-feldspar megacrystic, plagioclase porphyritic intrusion of probable quartz diorite to monzodiorite composition. Subhedral tabular pink K-feldspar phenocrysts generally range in length from 2 to 20 mm, and they are rarely up to 7 cm long. They usually comprise from <1 to 5% of the modal mineralogy. The matrix to the K-feldspar megacrysts consists of medium-grained porphyry containing phenocrysts of albitic plagioclase (1-3 mm, 35-55 volume %), altered amphibole (up to 4%) and quartz. The plagioclase is usually completely altered to aggregates of sericite ± quartz ± K-feldspar. Mafic phenocrysts, probably originally

hornblende from crystal shapes, are commonly altered to magnetite, hematite, pyrite, biotite, and chlorite. Equant, clear to smoky subrounded quartz phenocrysts, 0.2-1.5 mm in diameter, comprise <1 to 4%.

The Red Bluff porphyry intrudes a sequence of biotite altered turbiditic greywacke, siltstone and mudstone that is of probable Triassic age. These rocks are an extension of the thick sequence that hosts the Snip mine. Bedding generally dips moderately to shallowly to the northeast adjacent to the porphyry, and is upright. The 1994 drill holes intersected the greywacke sequence along the southwest side of the porphyry system. Here, the sedimentary rocks are usually foliated and have a slaty to locally phyllitic foliation defined by biotite and sericite. Foliation is commonly spaced. Numerous calcite  $\pm$  quartz  $\pm$  pyrite  $\pm$  chlorite veinlets and stringers are (a) parallel to foliation (predominant) or (b) folded by the foliation. The veinlets commonly occur in densities of >10 per metre. Thin (<2 mm) biotite envelopes and selvages are common on the veinlets. 0.5 to 40 centimetre wide quartz + pyrite + chlorite + chalcopyrite  $\pm$  sericite  $\pm$  Fe-carbonate  $\pm$  biotite veins are developed throughout the greywacke intersect on the southwest side of the porphyry system in 1994. Sericitic shear zones (pale grey) are developed locally and are parallel to the surrounding pervasive foliation. Limited surface mapping in the area southwest of the porphyry suggests that the foliation has a shallow to moderate southwest dip.

On the southwest side of the Red Bluff porphyry within 25 to 50 metres of the quartz-magnetite-hematite stockwork that defines the core of the system, foliation in the sediments generally disappears, magnetite appears (disseminated, in veinlets and in quartz veins), veins become quartz-dominant with sparse calcite and intense K-feldspar alteration is widespread. The rock is commonly pale to dark green, mottled with disseminated blebs of magnetite + hematite. Quartz-magnetite-hematite veins, generally 0.3 to 2 centimetres wide, increase in density and thickness gradually downhole as the quartz-Fe-oxide stockwork is approached. This area of distinctive alteration, termed the "transition zone" in previous drill logs, occurs in the following intervals: S1208 = 90- approx. 115 metres; S1210 = top of hole-57 metres; S1211 = 80-117 metres; S1212 = 125 metres to end of hole; S-1215 = 35-80 metres; S-1216 = 82-125 metres. In these intervals, quartz veins with magnetite are clearly cut by 0.5 to >50 centimetre wide (apparent thickness) white to pink quartz + pyrite + chalcopyrite + chlorite + biotite + sericite + carbonates veins of the same type described in the preceding paragraph.

#### *Quartz-Fe-oxide and younger mineralization*

The Red Bluff porphyry hydrothermal system is dominated by an intense quartz-magnetite-hematite stockwork that trends northwest along the northern slope of Johnny Mountain. The stockwork overprints and is intimately associated with the Red Bluff porphyry intrusion. Margins of the quartz-magnetite-hematite stockwork are usually discrete. Over intervals of < 5 metres, and commonly < 1 metre, vein abundance increases from 10-25% of the total rock outside the stockwork to >60% (commonly >90%) within

it. The veins form an intense stockwork that usually contains less than 20% interstitial rock. Locally, drill intersections 20 to >100 m long are composed entirely of intersecting to sheeted sets of quartz-magnetite-hematite veins. Individual veins usually range from 0.5 to 10 cm in thickness. Magnetite with subordinate hematite constitutes from 0.5 to 25% of the vein volume, often occurring as multiple 0.1 to 1 mm-wide bands in white quartz. Microscopically, magnetite and hematite commonly occur together in individual grains with undulating irregular boundaries separating the two phases. Magnetite:hematite ratios are usually greater than 3:1. Multiple generations of obliquely cross-cutting quartz-magnetite-hematite veins are common. Vein core axis angles are highly variable in the 1994 drill core, but elsewhere veins are locally sheeted (e.g. Snip 130 portal area - veins dip southwest: Rhys, 1995). Younger veins contain progressively less magnetite and hematite, from 10 to % in the oldest veins to 0.5-5% in the youngest. Overall Fe-oxide content in the stockwork is estimated at between 8 and 15%. Interstitial wallrock within the quartz-magnetite-hematite stockwork is intensely altered to sericite + magnetite + hematite + quartz + K-feldspar + biotite + chlorite. A bright green phyllosilicate (possibly chlorite, biotite or sericite) is locally abundant.

The quartz-magnetite-hematite stockwork is overprinted by quartz + pyrite + chalcopyrite ± carbonate veins and alteration equivalent to the veins of similar mineralogy outside the stockwork, and by pyrite and carbonate veins. Grey to pale pink quartz forms 5 centimetre to 3 metre wide patches and veins that typically comprise 10 to 30% of drill intersections in the quartz-magnetite-hematite stockwork. The quartz typically contains 1 to 10% disseminated, blebby and veinlet pyrite + chalcopyrite. Carbonates (?Fe-carbonates, and more rarely, calcite), sericite chlorite and green biotite commonly occur with the sulphides. Margins of the quartz-pyrite veins/patches, although locally sharp like quartz-pyrite-chalcopyrite veins outside the stockwork, are typically irregular and gradational with the quartz-magnetite-hematite veins. Over <1 to 5 centimetre widths on the margins of the quartz-pyrite veins/patches, pyrite + chalcopyrite ± Fe-carbonate entirely replace the magnetite and hematite, but preserve relict Fe-oxide banding of the adjacent quartz-magnetite-hematite assemblage. Isolated patches of Fe-oxide bearing vein material are commonly preserved within the white/pink quartz and are sulphidised on their margins. These textures suggest that much of the quartz-pyrite may this be an in situ alteration of the quartz-Fe-oxide assemblage, with little introduction of new vein material. The total sulphide content in the quartz-pyrite assemblage (generally approximately 5%), is less than the total Fe-oxide content if the older quartz-magnetite-hematite veins (generally 10%), resulting in a net loss of Fe from the system.

Pyrite + chalcopyrite ± carbonate veinlets and veins frequently cut, but are intimately associated with the quartz-pyrite veins and alteration. They commonly have consistent core axis angles, suggesting that they are sheeted. The veins are typically 0.5 to 4 millimetres wide, but are locally up to 30 centimetres thick. Pyrite + chalcopyrite veins are often spatially related to the quartz-pyrite veins/alteration described above: veinlet densities are usually highest in areas of quartz-pyrite-chalcopyrite veining/alteration, commonly >10 per metre, and drop to usually < 5 per metre in areas of quartz - magnetite - hematite veining that are unaffected by late quartz-pyrite veining/alteration. Pyrite ±

chalcopyrite veins locally have narrow alteration envelopes in which Fe-oxides are sulphidized. White, grey and pink (yellow to brown in old core) Fe-carbonate veinlets and stringers are locally abundant and cut the pyrite veins. Progressive mineralogic changes from early pink/white quartz > pyrite - chalcopyrite  $\pm$  carbonate veins, intermediate pyrite + chalcopyrite  $\pm$  carbonate veins to late carbonate  $\pm$  pyrite  $\pm$  chalcopyrite veins suggest that the veins are part of a single, evolving veining event that terminates in the formation of the late carbonate veinlets.

The quartz-pyrite veins/alteration are locally brecciated. Breccias have variable contacts with the surrounding quartz veins that vary from gradational to sharp. They consist of 25 to 70% angular to subround fragments of quartz-pyrite veins, typically 0.2 to 5 centimetres wide, in a matrix of carbonate (usually calcite) + biotite (black and/or green) + chlorite + sericite + pyrite  $\pm$  chalcopyrite. Breccia fragments locally contain pyrite veinlets that are truncated at the edges of the fragments. This suggests that brecciation postdates or is late during both the quartz-pyrite and pyrite veining events. The late relative timing and abundance of carbonate in the breccia matrix suggests that brecciation occurred during the late carbonate veining event.

A late set of quartz veins that is probably Tertiary in age cuts all of the above rock types and veins. The veins occur throughout the Johnny Mountain area and are flat to shallow southeast dipping, lenticular in shape and commonly occur in an echelon arrays. They are generally widely spaced (<1 per metre usually) and commonly fibrous. In drill core they are difficult to distinguish from veins in the Red Bluff porphyry system.

#### *Metal Distribution*

Au and Cu grades reflect the distribution of the different vein and alteration types. Areas of quartz-magnetite-hematite veining with sparse or no pyrite-chalcopyrite or quartz-pyrite overprinting typically grade <600 ppm Cu and <0.2 g/t Au (e.g. S1209, 146.5 to 169.2 metres). Highest Cu and Au grades (locally >1,000 ppm Cu and 10 g/t Au) occur in quartz-pyrite-chalcopyrite veins and alteration and in areas of abundant pyrite-chalcopyrite veining both inside the quartz-Fe-oxide stockwork and in adjacent greywacke. Au and Cu grades generally correlate positively and commonly have a linear relationship (Rhys, 1993) suggesting that they were introduced together. In greywacke outside of the stockwork, many quartz-pyrite veins with high Cu and Au grades are subparallel to shallowly oblique to the core axis (e.g. S-1210, multiple veins from 26.2 to 41.1 metres), and are thus steeply dipping.

#### *Geologic summary:*

- Quartz-magnetite-hematite veins are the earliest phase of veining in the Red Bluff porphyry system. They form an intense stockwork that is spatially related to the Red Bluff porphyry.

- The quartz-Fe-oxide stockwork and altered sediments on its southwest margin are overprinted by quartz-pyrite +/- chalcopyrite veins/alteration and pyrite + chalcopyrite veinlets that are associated with the highest Au and Cu grades. Where quartz-pyrite assemblages overprint and sulphidize the quartz-Fe-oxide stockwork there is a net loss of Fe from the system. Veins are discrete, with sharp boundaries outside the stockwork in greywacke, but have indistinct alteration boundaries with quartz-Fe-oxide veins within the stockwork.

- The overall sequence from intense early Fe-oxide veining to less intense quartz-pyrite-chalcopyrite veins and finally to pyrite and carbonate stringers corresponds with a progressive decrease in the total amount and intensity of veining through time.

- A 25 to 50 metre wide zone ("transition zone") of K-feldspar + Fe-oxide alteration in greywacke occurs along the western upper periphery of the quartz-magnetite-hematite stockwork and separates the stockwork from biotitic greywacke to the west. Calcite veinlets, common in the biotitic greywacke, become predominantly quartz veinlets in the transition zone.

#### Core Library:

The core library contains representative samples of vein types, alteration and lithologies from holes 1208-1216. The samples, numbered 1 to 70 are listed with the hole numbers and metres they were collected from in Table 1. The samples are ordered in a sequence that represents a typical walk through a drill hole, from altered sediments along the southwest margin of the porphyry system into the core of the quartz-magnetite-hematite stockwork that characterizes the system.

Samples 1-7 are typical of the biotite+pyrite+sericite+calcite altered siltstone adjacent to (SW of) the porphyry system. Note the foliation defined by biotite and muscovite. Calcite+quartz+pyrite+chlorite veinlets are abundant and are commonly foliation parallel or discordant, and folded by the foliation. Narrow biotite envelopes occur on the margins of some calcite and quartz veinlets (samples 1, 5 and 7). Magnetite is absent and K-feldspar stain is variable, but commonly moderate (samples 4 and 5).

Samples 8-19 are from the "transition zone" adjacent to (25-50m from) the quartz Fe-oxide stockwork. Foliation virtually disappears in this zone, quartz content increases in veins, calcite is no longer a significant vein constituent, and Fe-oxides appear both in quartz veins and disseminated. This area is characterized by intense K-feldspar alteration (samples 15, 17, and 19 are stained) that imparts, with Fe-oxides, a green-grey, mottled texture to the rock. The lack of foliation is probably due to the abundant K-feldspar and the relatively low phyllosilicate content when compared to the previous interval. Fe-oxide content gradually increases as the quartz-magnetite-hematite stockwork is approached. Two main generations of veining are apparent in this zone: early quartz-Fe-oxide veins/veinlets and related Fe-oxide stringers (samples 9-12, 15, 16, 18 and 19) are cut by quartz-pyrite-chalcopyrite veins and veinlets (samples 8-11, 13, 14 and 16). Good

crosscutting relationships are in samples 9 and 11. Note the biotite envelopes on some quartz-pyrite veins (samples 13 and 14) and the common pyrite-chalcopyrite stringers that are completely contained within the quartz-pyrite veins and terminate at the vein boundaries (samples 8-10, and 14). Carbonates occur as stringers in the quartz-pyrite veins (samples 9, 13, and 14), as late veinlets that occur outside the quartz veins (sample 10) or more rarely, as irregular veinlets associated with the quartz-Fe-oxide assemblage (sample 17).

Samples 20-34 show vein and alteration styles related to the quartz-magnetite-hematite stockwork. Samples 20-27 are typical examples. Note the abundant laminae of Fe-oxides, multiple cross-cutting phases of veining, and the general decrease in Fe-oxide content in younger veins. Quartz > pyrite + chalcopyrite and pyrite veinlets cut the Fe-oxide quartz assemblage (samples 25-27) and Fe-oxides are locally sulphidized in the pyrite vein envelopes (sample 26). Samples 28-34 show the intense alteration of interstitial wallrock in the quartz-magnetite-hematite stockwork. Wallrock is entirely altered to grey-green sericite > magnetite + hematite + chlorite + green biotite + K-feldspar (samples 23, 30-34). K-feldspar is not abundant and is often absent (samples 30, 31, and 34 are stained). A bright green phyllosilicate (samples 28 and 29) predominates locally (possibly sericite, chlorite or green biotite - petrography is needed.) Late carbonate (sample 29) and quartz-pyrite (sample 32) veins cut the quartz-Fe-oxide veins and their alteration assemblage.

Samples 35-42 show quartz-pyrite-chalcopyrite alteration/vein assemblages progressively replacing the textures and mineralogy of quartz-magnetite-hematite veins. Domains of grey, white and pink quartz, here with 5-15% disseminated and veinlet pyrite + chalcopyrite + brown carbonate preserve relict textures of the quartz + magnetite + hematite assemblage on their margins (samples 38-41). Note the net loss of Fe-bearing minerals from the quartz-magnetite-hematite to the quartz-pyrite-chalcopyrite assemblage. Samples 35, 36, and 37 show sulphidization of the Fe-oxides adjacent to pyrite veinlets, again with an overall loss in Fe content. Sample 42 shows complete replacement of the Fe-oxides, with relict textures of the oxide assemblage remaining.

Samples 43-55 show the textural and mineralogical variation in the areas of white/pink quartz-pyrite-chalcopyrite veining. All of these samples come from veins that generally lack discrete boundaries and usually exhibit replacement textures at their margins with the quartz-Fe-oxide assemblage. Pyrite and chalcopyrite are present in all samples; they are disseminated in veinlets or in irregular anastomosing blebs with sericite, carbonates, (samples 43, 44, 46: ?Fe-carbonate and more rarely calcite), chlorite and green biotite. Specular hematite, K-feldspar (sample 51) and a pink carbonate (sample 55) locally occur as coarse blebs in the quartz-pyrite-chalcopyrite veins. Late ?Fe-carbonate (brown to pink when oxidized in air, grey on fresh surfaces: samples 52-54) veinlets locally cut the quartz-pyrite veins. These latter veins may contain chalcopyrite, pyrite, and/or specular hematite (sample 53).



Samples 56-59 show breccia textures that occur locally in quartz-pyrite-chalcopyrite veins. The breccias have gradational to sharp boundaries with the surrounding veins, and contain brecciated quartz fragments in a matrix of green biotite, chlorite, sericite, carbonate (generally calcite), pyrite, and chalcopyrite. Sample 57 is exception and has a reddish matrix, possibly coloured by fine-grained hematite and /or Fe-carbonates.

Samples 60-63 are from southeast of the Red Bluff cliffs (holes S1213 and S1214) in intense sericite - pyrite + quartz alteration. K-feldspar content is low (samples 60, 61, and 63 are stained). These samples are from well outside the quartz-magnetite-hematite stockwork.

Samples 64 and 65 are of post-mineral mafic dykes that occur locally throughout the area tested by drilling. These are fine-grained, dark grey, commonly magnetic and calcareous. Note the weak foliation developed in sample 65.

Samples 66-70 are of K-feldspar megacrystic porphyry, typical of the Red Bluff. Note the pink K-feldspar megacrysts and the complete pale green-grey sericitization of the smaller plagioclase phenocrysts. Chlorite-biotite-Fe-oxide altered mafic phenocrysts have crystal shapes that suggest they are amphiboles. Samples 67, 69 and 70 are from within the quartz-magnetite-hematite stockwork. Sample 69 is stained and has abundant fine-grained K-feldspar in the matrix. Sample 68 is from a Cominco quarry approximately halfway down the Bronson airstrip (NW side). It is of a K-feldspar megacrystic dyke that is typical of Red Bluff type intrusions in the area.

#### 1995 core logging sheet:

The 1995 core logging sheet is designed to record the abundance and distribution of predominant vein types, minerals and alteration types in relation to Au and Cu grades. The following column headings and sections are indicated:

#### 1. Geological Description

From/To: Interval of distinctive lithology, etc.

Description: To include rock type and/or dominant pervasive alteration (e.g. ALT for a highly altered rock of uncertain protolith). The most common lithologies are: (a) K-feldspar megacrystic porphyry; (b) Greywacke and siltstone; (c) Mafic dykes (distinguish foliated from unfoliated, etc.) and (d) alteration. Common pervasive alteration assemblages include: (a) biotite +/- sericite +/- calcite (Snip-type sediments SW of the porphyry system) (b) sericite-pyrite (intense alteration of sediments SE of the porphyry system) (c) K-feldspar +/- Fe-oxides ("Transition zone" adjacent to the quartz-Fe-oxide stockwork in sediments) (d) sericite +/- K-feldspar +/- magnetite +/- ?chlorite (altered wallrock in the quartz-Fe-oxide stockwork). In many highly altered wallrocks within the quartz-Fe-oxide stockwork, only the presence of K-feldspar megacrysts can distinguish between altered porphyry and sedimentary protolith.

## 2. Graphic Log

Provided to allow sketching of contact relationships, angles between structures, etc.

## 3. Structure

From/To: Interval over which the structure(s) is developed

Struct: Type of structure, such as foliation (FLTN), fault (FALT), shear zone (SHR), vein (list predominant mineralogy, e.g. quartz-magnetite = QzMag)

TCA: Angle that the structure makes to the core axis, or predominant angles in the case of multiple structures of the same type (e.g. pyrite veinlets).

%TCA: Percentage of structures of a single type that display a common angle to the core axis  
(e.g. 60% of pyrite veins are at 50 degrees to the core axis). Two or more orientations may be common in which case a second row could be used.

## 4. Mineralization:

Columns under mineralization are designed to be recorded with each assay interval so that a direct correlation between assays/analyses and mineralogy and vein types can be made.

Sample #: Number from the tag book (a tag should be stapled into the core box at the beginning of each assay interval).

From/To: Sample interval

Minerals: Contains the following columns:

Py - visual estimate of the total pyrite content in the assay interval  
Cpy - visual estimate of the total chalcopyrite content in the assay interval  
FeOx - visual estimate of the total magnetite + hematite content in the assay interval  
Cal - visual estimate of the total calcite content in the assay interval  
Carb - visual estimate of the total carbonate (excluding calcite) content in the interval  
Blank column - for extra minerals

Veins: Columns are designed to record the number of veins/veinlets in each assay interval and their total cumulate thickness. Pairs of columns for three common vein/alteration types are shown (pyrite veins, quartz-pyrite veins and carbonate veins). The two columns are as follows: # veins is the total number of veins of one type in the assay

interval (e.g. 18 pyrite veinlets); cumulative thickness is the total thickness of veins (thickness of all veins added together) recorded in centimetres. These numbers can later be divided by the thickness of the assay interval to obtain a density of veins per metre and a total % of veins in the interval. Average vein thickness in each interval can be calculated by dividing cumulative thickness by the # veins. For white/pink quartz -pyrite veins/alteration in the quartz-Fe-oxide stockwork which often lack distinct boundaries, measurement of the cumulative thickness is subjective, but important to measure due to the strong influence of these veins/alteration on Au and Cu grades.

One blank column pair under veins is provided. In the quartz-Fe-oxide stockwork, veins are so abundant that it is more practical to measure what is not vein. Thus, I would suggest filling one of these columns with the cumulate thickness of interstitial altered wallrock in each assay interval that is in the stockwork. Other types of veins that could be recorded in these columns are: (a) quartz veins - timing indeterminate (generally in the sediments) (b) calcite veinlets (in the sediments) and (c) breccias and breccia veins.

### 5. Assays

Au: g/t

Cu: ppm

Ag: ppm

Mo: ppm

One extra column for any new element

### **Misused or vague terms in previous core logging**

Misused or vague core logging terms that have been commonly used in previous Skyline drill logs include the following:

(i) "Sheared", "shearing" or "shear" when foliation is meant. Large volumes of rock on Johnny Mountain are foliated but not "sheared". If the foliation is a discrete and definite shear zone (e.g. rapid increase in foliation intensity; oblique and asymmetric fabrics, etc.), it should be named as such (shear zone) with its foliation angle listed under the structure heading. In addition, the vague term "shear" is commonly applied to gouge-filled faults. If gouge is present its thickness should be noted, and any consistent angle of gouge seams to the core axis. I recommend that such a structure (gouge-filled) be described as a "fault" while a discrete, foliated zone be described as a "shear zone" to avoid confusion.

(ii) The term "flooding" is a vague term that can mean veining or pervasive alteration (e.g. quartz flooding). More definite terminology, such as "intense veining" or "stockwork" could be used to describe veining. Pervasive alteration should be described as such (e.g. pervasive K-feldspar alteration and not K-feldspar flooding).

(iii) The term "fracture fill" is a cumbersome term that means stringers or veinlets. The latter terms are clearer, and shorter.

(iv) Andesite/andesitic, dacite/dacitic are commonly used to describe grey to green fine-grained rocks, including dykes, often based on the vague hint of a crystalline matrix or a green tint to the rock. If the rock can not be identified mineralogically (i.e. grains are

clearly visible) a name should be reserved until thin section petrography and/or geochemistry is completed.

(v) Alteration types such as silicification, K-feldspar alteration, sericitization, albitization etc. are commonly assigned to fine grained rocks of varying hardness or colour. For example, hard white or grey altered rocks are commonly called silicified while hard pink altered rocks are commonly called K-feldspar altered. These assignments are usually erroneous. If the alteration mineralogy is too fine-grained to identify while logging core, final identification of alteration type should be made petrographically or by mineral staining (e.g. K-feldspar stain). In addition, if the rock is so altered that protolith is unclear it should be called "altered".

### References

- Moore, M. (1994): Geologic summary of the Red Bluff area, Bronson Slope project; unpublished company report, International Skyline Gold Corp., 5 pages.
- Rhys, D.A. (1995, in press): The Red Bluff Au-Cu Porphyry System and Related Precious and Base Metal Vein Systems, Northwestern British Columbia; Canadian Institute of Mining and Metallurgy, Special Volume 46.
- Weekes, S. (1994): Summary report on the spring, 1994, diamond drilling program, Bronson Creek area; unpublished company report, Pamicon Developments Ltd., for International Skyline Gold Corp., 14 pages + drill logs.

Table 1: Samples in the core library:

Sample #	Hole #	Metres
1	S1211	16.9
2	S1211	60.5
3	S1216	50.8
4	S1212	68.0
5	S1212	55.5
6	S1212	88.1
7	S1211	46.2
8	S1211	100.8
9	S1210	44.8
10	S1210	50.0
11	S1210	38.6
12	S1211	112.5
13	S1216	135.0
14	S1211	101.0
15	S1216	119.8
16	S1216	123.0
17a	S1211	91.5
17b	S1211	91.5
18	S1216	131.8
19	S1216	127.6
20	S1216	198.0
21	S1216	187.0
22	S1211	138.2
23	S1216	191.2
24	S1210	92.0
25	S1215	206.9
26	S1216	204.6
27	S1215	146.7
28	S1215	267.7
29	S1215	152.5
30a	S1211	161.4
30b	S1211	161.5
31	S1216	144.8
32	S1216	148.6
33	S1210	109.8
34	S1215	300.6
35	S1215	137.4

Sample #	Hole #	Metres
36	S1209	101.4
37a	S1215	194.5
37b	S1215	194.6
38	S1216	205.5
39	S1209	105.3
40	S1209	63.3
41	S1209	66.2
42	S1211	139.8
43	S1211	158.3
44	S1210	25.3
45	S1216	137.0
46	S1210	36.0
47	S1216	133.6
48	S1214	19.5
49	S1211	136.7
50	S1216	153.1
51	S1211	98.0
52	S1215	89.7
53	S1211	137.4
54	S1210	67.0
55	S1215	72.1
56	S1209	5.6
57	S1209	45.0
58	S1216	133.2
59	S1211	120.3
60	S1214	61.0
61	S1214	45.4
62	S1213	20.5
63	S1213	20.7
64	S1215	232.7
65	S1216	253.6
66	S1210	33.9
67	S1208	115.0
68	not core	
69	S1216	197.5
70	S1216	196.4

**APPENDIX 2**

1995 Drill Logs

**HOLE 1217**

**11869.07 NORTH**

**25366.97 EAST**

**603.53 m ELEVATION**

**LENGTH: 423.4 m**

Meters		GEOLOGIC DESCRIPTION	STRUCTURE					SAMPLES		MINERALIZATION						ASSAYS													
FROM	TO		FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeOx	Cal	Carb	VEINS PYRITE		Qz-Py		CARB				Au	Cu	Ag	Mo		
																No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk						
0	12.2	Capings																											
12.2	23.5	Altered Siltstone: vlg qtz-ser ± bi; rock cut by 0.2-0.5cm calcite vein (leached out to 14m) Subsequently rock appears to have undergone intense brecciation resulting dislocation and fragment- ation of early veins. Fragments range from 0.2-25.0cm with angular to subrounded margins. Matrix of breccia comprises biotite + pyrite. Calcite-qtz-py = chlorite ± biotite veins 0.5-1.0cm are later. General elongation of bx frags at 20°/CA.	19.1	19.2	Breccia	60°	100%	2251	14.3	17.4	2.0%																		
			23.5	23.5	Calc vein 500m	05°	100%	2253	17.4	20.9	1.0%																		
					"	40°	40%	2254	20.4	23.5	3.0%																		
					Calc-qtz- py	45°	70%																						
					"	20°	30%																						
23.5	26.9	Altered Siltstone: vlg chl-bi-ser hornfelsed? appearance. Segmented calcite veins prominent 0.3-1.0cm. Dark green-blk colour of rock masks any obvious brecciation. Fine 0.5mm subhedral py occurs on reticulate fractures and as disseminations	23.5	25.7	Calcite veins	60°	80%	2255	23.5	26.9	3%																		
			23.5	26.9	Weak slaty chl Calc-qtz-py	65°	20%																						
						85°																							
						85°																							
			25.7	26.9	Breccia	50°																							
			25.9	26.2	Broken																								
			26.2	26.3	Fault	45°																							
26.9	36.8	Altered Siltstone brecciated appearance with frags bounded by somewhat reticulate biotite-pyrite stromaers 0.5mm which cut across segmented calcite ± qtz veins (early)	26.9	36.8	Calcite ± qtz (early)	70°	70%	2256	26.9	29.3	3%	<1%	-	5%															
			26.9	36.8	py-biotite	45°	35%	2257	29.3	32.6	3%	<1%	-	5%															
					"	80°	35%	2258	32.6	35.7	3%	<1%	-	5%															
			26.9	29.3	Calcite-qtz py ± strom.	35°		2259	35.7	38.7	3%	<1%	-	7%															
			26.9	36.8	Weak slaty cleavages	80°	90%																						

9cm

31 } 15cm

1 }  
1 } 25cm

5 } 10cm



FROM	TO	GEOLOGIC DESCRIPTION	STRUCTURE		MINERALIZATION															
					SAMPLES		MINERALS					VEINS				ASSAYS				
					FROM	TO	Py	Cpy	FeOx	Cal	Carb	PYRITE		Qz-Py		CARB		Au	Cu	Ag
NUMBER							No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk						
26.9	36.8	(cont) - Qtz-calc-chl-py ± magn. veins crosscut biot-py stringers Magnetite in vein at 29.1m. P set of late 1mm qtz carb stringers with a carbonate rich bleached alteration envelope cuts all mineralization and structure between 36.4 and 32.6m. At 35.5m 1cm calcite vein 20°C with sericite, Biotite & py & magn. margins; tr cp in wall. Rock frags (bonding?) steadily more sericitic with biotite & pyrite & magn. reticulate margins. 36.0m-3mm biotite & py & magn stringer OCA crenulated normal to cleavage of 75°C																		
36.8	41.9	Altered Siltstone: slaty cleavage & <del>75°</del> prominent at 75°C, Fault at 37.8m-10cm sericite gouge parallel cleavage. Crenulated banding normal to cleavage. Reticulate pyrite & biotite & magnetite vein parallel crenulations and cleavage. Carbonate-quartz veins segmented and folded by cleavage. 36.9m-10cm pinkish qtz-calc v. at 75°C. 41-41.9 pinkish qtz-calc-chl vein containing 30% horst's. Cp & Sph prominent in 3cm pyritic vein at 35.2m adjacent to horst at 41.15m (sphalerite yellow to orange) 41.85 cp on horst margin	36.8	41.0	slaty cle.	75°	80%	2260	38.7	41.0	5%	tr								
			37.8		Fault	75°														
			38.7	38.75	Qtz-calc	80°	100													
			41.0	41.9	Pinkish qtz-calc-chl	80°		2261	41.0	41.9	1%	tr	tr	Sph	tr.					







FROM		TO		GEOLOGIC DESCRIPTION					STRUCTURE					SAMPLES		MINERALIZATION					ASSAYS						
FROM	TO	FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeO*	Cal	CaO*	PYRITE		Qz-Py		CARB				Au	Cu	Ag	Mo	
															No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk					
84.4	87.5	25 zone	84.4	10cm	Shattered CP-Py Glaucophane (Thin?) 61"	45° 60° 50° 60°	2277	84.4	87.5	5%	0.8	1	1		2	2cm	6	10		3	0						
87.5	90.5	25 zone			calc.	70° 0° 45°	2278	87.5	90.5	2%	0.5	0	1				6	27		3	0						
90.5	93.6	25 zone			Qtz-py	70° 45° 15°	2277	90.5	93.6	2.0	1.0	0.1	2				18	22		2	0						
93.6	96.6	25 zone			Qtz-py	65° 45° 0	2280	93.6	96.6	2.0	0.5	0.1	4				18	25	14	8.5							
96.6	99.7	45 zone lets hair-line Qtz carb ± 10° CA			Qtz-py	60° 45°	2281	96.6	99.7	1.5	0.2	1.0	2				12	14.5		1.5							
99.7	102.7	As zone, broken - v. fine py-cp disseminated and on micro fract, often weakly foliated			Qtz-py	0° 45°	2282	99.7	102.7	3.0	0.5	6	5				3	1.5	25	10							
		As zone, segmented zone hair-line calcite veining			Qtz-py	60° 40° 5	2283	102.7	104.4	3.0	0.2	6	5				8	10		2							
104.4	105.4	Basinal Qtz-py vein. 0.2-3cm <sup>thin</sup> Qtz clasts in foliated matrix of chlorite, see calc py; mylonitic in part, cleavage tension. Hornbls: 25 zone			FLTN in py BR	60-65°	2284	104.4	105.4	8	0.1	6	15														
105.4							2285	105.4	107.7	2	0.1	6	4				15	21	5	1.5							

Note: disrupted late  
carbonate veining

FROM TO		GEOLOGIC DESCRIPTION	STRUCTURE				SAMPLE NUMBER	FROM TO		MINERALS					MINERALIZATION				ASSAYS							
FROM	TO		FROM	TO	TYPE	TCA		%TCA	FROM	TO	Py	Cpy	Feldt	Cal	Carb	VEINS PYRITE		Qz-Py		CARB		Au		Cu	Ag	Mo
															No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	Au TBX	Cu SBX	Ag GBX	Mo
107.4	109.1	Qtz stockwork: All <sup>d</sup> Sed protoliths 109.0 30cm Qtz py cp @ 60°CA ser. s <sup>+</sup> network veinlets in Qtz. Pink silicate Kspar? late py cp	107.4	109.1	Qtz Py cp	60	40	2286	107.7	110.2	2	0.2	5	4		18	65					2	1	45	5	50
					"	40	40																			
					whl Qtz	15	20								3	1										
					Py cp	80'	85'								?	2										
					0"	15"																				
		Transition Zone: Position Kspar lost on groundmass of Inter. protolith.			Qtz py chl + cp	30	20	2287	110.2	111.5	3	.1	8	4	41	?	15	12	15				25	60	15	
						40	50																			
						65	30																			
111.5	114.0	Qtz-py vein: strong, rose Kspar alteration low S <sup>+</sup> generally rimming protoliths and in network ser. chl veins. Strong mag rimming protoliths.			Qtz v.	35°		2288	111.5	114.0	2	.1	4	2									5		95	
114.0	115.7	Qtz Feox Stockwork Zone: moderate to strong Fe ox replacement of protoliths. strong chl ill <sup>d</sup> Grey Qtz - pinkish - Kspar.			Heinlma py cp	45		2289	114.0	115.7	2	.1	6	3		?	1								25	161%
115.7	117.9	As zone: Calcite localized from minor calc. Qtz S <sup>+</sup> veinlets common blocky frags.			NO Py cp sec	90	10	2290	115.7	117.9	3	.2	5	4		3	1				2				40	141%
						65-75	50																			
						45	25																			
						0±5	5																			
					Py cp	45																				
117.9	119.9	As zone: w/ NW py cp veinlets in wide Qtz veinlets 118.0-118.6; ser-calc alteration of protoliths late calc-s <sup>+</sup> veinlets @ 60° protoliths localized.			Gr Qtz Py cp	45	80	2291	117.9	119.9	2	.1	6	4		2	2				2				50	137%
						45°	100																			

FROM	TO	GEOLOGIC DESCRIPTION	STRUCTURE		SAMPLE NUMBER	FROM	TO	MINERALIZATION					VEINS								ASSAYS									
			FROM	TO				TYPE	TCA	%TCA	Py	Cpy	FeD <sup>+</sup>	Col	Carb	PYRITE		Qz-Py		CARB				Au	Cu	Ag	Mo			
															No.	Cum	No.	Cum	No.	Cum	No.	Cum	No.	Cum	18g	58g	Ag	Mo		
117.7	122.2	Sheeted Qtz-py + cp 117.7 - 120.3 semi massive py in matrix cp-py network veins; 1cm Hom cemented 121.1 - 121.4 wk S <sup>+</sup> - FW 1cm homitic cemented Bx @ 45° 121.0 - 122.0 3cm semimassive cp + py			2292	119.9	122.2	60	0.8	8	6	1				3	60										40	15		
122.2	124.0	Grey gtz cut through moderately zoned K <sub>2</sub> rock (ser + calc) imparting Feor as rims on bx frags and 25 minute veinlets and dis <sup>s</sup> within the frags. Weakly developed py-cp veinlets ± ser, gtz, carb cut both grey gtz and bx frags with S <sup>+</sup> deposited primarily in grey gtz. Protoliths may be chilled margin of intrusion as matrix equigranular and most magnetite replacement is irregular except along walls of grey gtz veins. Protoliths show no fabric to indicate deformed sediment origin.	Grey Qtz	30°	20	2293	122.2	124.0	1.0	0.1	8	8	1														20	22?		
		As above	Grey Qtz	70°	60	2294	124.0	127.1	1.0	0.1	6	5	1												45	5	5.5	23.14		
		125.15 - Slickensided S <sup>+</sup> on lsh calc gtz S <sup>+</sup> veinlet @ 75° CA → pitch 20°/70°; some protolith homitic?	thin py-cp	65-70	80																									
			lsh calc cp gtz S <sup>+</sup>	± 30	10																									
127.1	130.1	As above. v weak S <sup>+</sup> veinlets Minor lsh cream chromated gtz + cp-py in 1cm veinlet at 45° CA 128.8 Sem-py band FLTN @ 65° CA	grey gtz	55°	60°	2295	127.1	130.1	1.0	0.1	8	5	2														40	10	50	24.11

FROM	TO	GEOLOGIC DESCRIPTION	STRUCTURE		TCA	%TCA	SAMPLES		MINERALIZATION						ASSAYS														
			FROM	TO			TYPE	SAMPLE NUMBER	FROM	TO	Py	Cpy	Fe <sup>+</sup>	Cal	carb	VEINS PYRITE	Qz-Py	CARB	Au	Cu	Ag <sup>+</sup>	Mu							
														No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	LIBX	SBA	g/t	g/t				
130.1	133.2	Qtz Feox <sup>starkwork</sup> Protolith: calcite sericit chl mgn. Green to brownish carbonate in a network of micro- fractures (Fe carb?); minor cp-py w late carbonate			Grny Qtz carb ± cp-py	45/50 80 50 30 0	65 25 50 15 10	2296	130.1	133.2	21.0	0.1	8	5	4										25	75	28	11	
133.2	136.2	As above: moderate to strong network cp-py ± carb, ser chl gln concentrated in more massive gray veins - splayed, 2 x 1 cm wll. gln 45°			Grny gln carb ± cp-py py cp	45/50 70 20/50/30 75	75 15 75	2297	133.2	136.2	3.0	0.5	8	5	2										40	60	40	15	
136.2	139.3	As above: Qtz-Feox replacement more intense with wide silice with bands requiring a pinkish tone. Network late Fe carb ± 20°			Grny Qtz Network cp-py ± carb late Qtz ± Fe carb py	±30 40/60 50-55 70,30	60 60 75	2298	136.1	139.3	0.7	0.6	10	1	4	2	2									3	3		80
139.3	142.3	As above: 140.4 to 140.55 - 3 x 1 cm carb cemented Qtz bx @ 50° subll Mgn FLTN 140.7 green phyllosilicate becoming prominent in protoliths. Mod late Fe-carb staining			Mgn FLTN Network cp-py ± carb late Fe carb ± py cp	30-45 I 35° 60 80 10 30 +45	80 50 25 25 40 3 35	2299	139.3	142.3	0.5	0.5	7	1	4										25	75			
142.3	145.9	As above: Protolith 85% replaced by Qtz - little evidence of the sericit all-angles etc in 121B late cp-py Qtz ser. calc, often at 45° near normal to general Mgn FLTN Although some of the gray Qtz veins contain pyrites and zones of cp-py in sericit (ie Qtz py veins), the 5° zone to be more closely related to late fractures (ie intersections, open spaces etc) or a later white Qtz. Green phyllosilicate 140-143			Mgn FLTN cp-py ± calc. etc	5-60 +40 -95 60	65	2300	142.3	145.9	1.0	0.5	10	1	2										7	7	55	21.1	

a later white Qtz. Green phyllosilicate  
140-143



FROM	TO	GEOLOGIC DESCRIPTION	STRUCTURE		SAMPLES		MINERALIZATION																		
							MINERALS					VEINS				ASSAYS									
							Py	Cpy	Fe <sup>3+</sup>	Cal	Carb	PYRITE		Oz-Py		CARB		Wt %		Au	Cu	Ag	Mo		
No.	Cum	No.	Cum	No.	Cum	No.	Cum	No.	Cum	No.	Cum	g/t	%	g/t	%	g/t	%								
145.9	148.4	As Above: 145.4 - slickenside sp on 65° cp-py-mga-gtz chl s2lc - 70° pitch left (Normal). Pinkish tinge to gray gtz to ser on margins 145.1 - 3cm gtz bx cemented by cp-py, mga ser chl? @ 50° - cuts 70° smy gtz. wk ltk 5° ser veinlets	gmy gtz	50-55	60	2301	145.4	148.4	1.0	0.1	20	2	<1	3	4					3	2	?		70	25%
148.4	151.5	Granitic texture of protoliths more replacement as pervasion sil <sup>n</sup> masses - 0.5 - 1cm feldspars - 2ser/calc. Few hairline gtz - calc cp mon py 149.6 - 1cm gtz - coarse calc with vug containing spec hem.	gmy gtz	75	80	2302	148.4	151.5	1.0	0.1	12	2	<1											60	42%
151.5	154.5	As Above: cp-py min <sup>o</sup> mainly on hairline fractures; 1" 0.5cm py @ 60° CA	gmy gtz	45	35	2303	151.5	154.5	1.0	0.3	8	2	<1	1	0.5									725	65%
154.5	157.6	As Above: in wk ser - gtz all <sup>n</sup> env. developing zls to gray gtz veins cp-py + ser gtz concentrating mainly in gtz v and all <sup>n</sup> envelopes (95/3.1m) - gray gtz in part milky white - diffused distribution and zoning. - green phyllosilicate in protoliths and as vein @ 157.0-30 across gtz vas.	gmy gtz	±45°	65	2304	154.5	157.6	1.5	0.5	10	2	<1											725	<65%
157.6	160.6	gray to milky gtz. cp-py veinlets in and adjacent to gtz veins - green phyllosil. generally as replacement in protoliths	cp-py ± ser gtz	50-60	100	2305	157.6	160.6	1.0	0.5	10	2	<1	1	0.5									720	<80



		GEOLOGIC DESCRIPTION	STRUCTURE			SAMPLE NUMBER	MINERALS		MINERALIZATION						ASSAYS												
FROM	TO		FROM	TO	TYPE		TCA	%TCA	Py	Cpy	FeOx	Cal	Carb	VEINS		PYRITE		Qz-Py		CARB		WHITE QTZ		Au TBR	Cu SBR	Ag 20% Gr	Mo Gr
														No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk				
1706	173.1	Dyke: l's as above, wk FLTN @ 45° CA; HW contact 35°; FV 25° - slickenside			FLTN	45													3	0.5							
173.1	175.9	Quartz-Feox Stockwork. Gray-white calc veins with pervasive silica ± sericite and Feox replacement of protoliths (Inte.?) cut by cp-py ± ser ± carb microveinlets; thence by an irregular network of carb ± py, cp veinlets often appearing to coat cp with magnetite? (replacement) where cp-py ± ser ± carb veinlets concentrate the development of sericitic envelope more pronounced. Late carb alt <sup>n</sup> rims and invade alt <sup>n</sup> protoliths.			Py Gray Qtz + mag carb ± py cp	50 45/55 50° 30-60 50	2309	173.1	175.9	2.0	0.3	12		4	1	1											80
175.9	178.9	As Above: with weaker S <sup>e</sup> veinletting; 177.1 elongate vug @ 45° in 0.3cm very late weakly cockcomb Qtz-spec vein. Occasional protolith ~ 100% replaced by FeOx; 178.2 - 0.4cm py			white Qtz ± spec. PY	60 40 25 60	2310	175.9	178.9	1.0	0.1	15		2	1	0.4					22	16					275
178.9	182.0	As Above			gray wht Qtz white Qtz carb ±	45-50 60 50 80 0-40 60	2311	178.9	182.0	1.0	0.2	15		4	1	1.0					10	9					775 215
182.0	185.0	As Above 183.3 - 184.0 - stringer zone py-cp some diss <sup>n</sup> , blobs cp			Py Gray wht Qtz white Qtz	60 50 60 40-50 50 50-55 100	2312	182.0	185.0	1.5	0.2	15		3	4	2					3	8	15				760 63

FROM TO		GEOLOGIC DESCRIPTION	STRUCTURE				SAMPLE NUMBER	FROM TO		MINERALIZATION					VEINS				ASSAYS										
FROM	TO		FROM	TO	TYPE	TCA		%TCA	FROM	TO	Py	Cpy	Fe <sup>2+</sup>	Cal	Carb	Pyrite	Qtz-Py	Carb	wht Qtz	Au	Cu	Ag	Mo						
															No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	18x	58x	97x	6x			
185.0	188.0	As above: minor py stringers @ 30°; late carbonate stringers partially leached - carb replacing remnants of pyrite. Minor chlorite in py stringers. Late open fractures in chl, spec.			MIN FLSTN	30°	40	2313	185.0	188.0	1.0	0.1	20	1	1	0.5										75	5		
					Carb.	25/45	60																						
					late Qtz Carb spec.	45																							
					py stringers	53-60	70																						
188.0	190.0	As above: Carbonate stringers with chl + spec.			py-qtz carb stringers	30		2314	188.0	190.0	1.0	0.1	20	3				1	1								10	65	10
					late carbonate	10	25																						
						45	50																						
190.0	190.6	Qtz pyrite vein: v.fg. py in semi massive bands with loose hematite. Although noted as Qtz-py vein.			pyrite banding	30°		2315	190.0	190.6	1.2	0.1	1	1		1	60												80
190.6	194.2	Qtz Feon Stockwork: As above. Grey Qtz running sub parallel to core. ie <30 with some network of ep-py stringers. Stringers not continuous to Qtz. Late carb ± spec @ 40° and fill late 'crackle' fractures. Sub parallel to core.			ep-py carb spec.	10/50	50	2316	190.6	194.2	2.0	0.5	15	4				8	5										70
					Carb.	40	30																						
194.2	196.3	As above: py cp stringers and patches cut by py-cp carbonate veinlets. Appears to carbonate sulphide cemented breccia. Chlorite present.			ep-Qtz	10°		2317	194.2	196.3	3.0	0.5	15	4															80
						30°																							
					py-cp carb	5°	40																						
						45°	35																						
						90°	20																						
196.3	197.3	Qtz Breccia: carbonate-S <sup>2+</sup> cemented with sericitic sil <sup>10</sup> envelope. S <sup>2+</sup> banding, carbonate veining and brecciation 30° CA. Ep in 0.5 cm seams and blebs. Leaching of carbonates.			Brecciation Carb	30	60	2318	196.3	197.3	5.0	1.5	3	10															75
					py cp																								
					silica																								
					ep																								

Leaching of carbonates.



FROM		TO		GEOLOGIC DESCRIPTION	STRUCTURE	SAMPLES		MINERALIZATION						ASSAYS														
FROM	TO	FROM	TO			TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeO <sup>+</sup>	Cal	Carb	VEINS PYRITE		Oz-Py		CARB		Oz-Fe		Au	Cu	Ag	Mu
							NUMBER								No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	17A	56A	Gtz	Gtz		
209.4	212.4			Qtz Breccia: Badly broken core. py-cp & stringers and diss <sup>d</sup> . Vuggy fractures - carbonate leached?	Py veins Py cp carb stringers	70° 80° 20° 75°	68 60 30	2325	209.4	212.4	7	0.8	3	5	6	6											90	
212.4	215.5			As zone: crushed zone. Network of carb + py cp stringers at 45-60°, 05°. Much of cp terminated or with black sooty coating. Mixed with Quartz-Feox rock	whitish carb py cp	30° 45° 60° 05°	30 50 20	2326	212.4	215.5	6	0.6	10	7							4	3					75	
215.5	217.9			Quartz-Feox Stockwork: fract <sup>s</sup> centrally heavily carb-py-cp stringers sub-parallel to core - open zone 216.3-217.3 Quartz vein with cp-py stringer sub-parallel core - open and at 60° - blobs of cp; spec hem + py on late parallel fracture.	SP Py veinlets carb py stringers	45° ± 5° 60°	50 50	2327	215.5	217.9	5	1.0	4	4			1	100									80	
217.9	218.5			Fault: no core.																								
218.5	221.6			Qtz-Feox Stockwork: broken core (209.4 core) hem >> map.	Py cp stringers	50		2328	218.5	221.6	20	0.1	12	8													760	
221.6	224.6			As zone: 15 S <sup>2</sup> (py >> cp) in Qtz br.; protoliths replaced by mag, chl, carb; Rock tends to fracture parallel to core.	Qtz v. Bx Py cp stringers Py veinlets carb py cp Empty Qtz	40 60 30/45 25/50 45°	50	2329	221.6	224.6	4	0.5	12	5	3	3											60	
224.6				SILICIFIED QUARTZ IRON OXIDE BRECCIA as above	Pink Qtz Py STGR	0 30 50 50	10 50 40 100	2330	224.6	227.0	0.6	Tr	10	0.1	0	-	15	87	0	-	10	18.5						











FROM TO		GEOLOGIC DESCRIPTION	STRUCTURE				SAMPLES		MINERALIZATION						ASSAYS												
			FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FePy	Cal	Fe <sup>2+</sup> O	VEINS PYRITE	Pink Oz-Py		CARB		White Oz-Py		Au	Cu	Ag	Mn	
324.7		(cont'd) SILICIFIED QUARTZ IRON OXIDE BRECCIA @ 347.3: end of coarse grained magnetite vein; UC 20 LC 50; pro- gressively replaced by pyrite 347.0 - 347.3. * Note onset of sheared pink quartz pyrite veins in Samp. No. 2371. These veins also contain several per- cent light green phyllosilicate (chlorite, sericite?) on fractures and shears within the quartz			Py	50	100	2371	346.0	349.3	3.7	Tr	45	0	0.2	8	6	2	130	0	-	0	-				
					PQPy	50	50																				
					"	70	50																				
					very siliceous.			2372	349.3	352.0	0.5	Tr	10	0	0.1	0	-	0	-	0	-	0	-				
					"			2373	352.0	355.0	0.3	Tr	10	0	0.1	0	-	0	-	0	-	0	-				
					PQPy	20	40	2374	355.0	358.0	0.2	1.4	10	0	0.1	0	-	7	175	0	-	0	-				
					"	50	60																				
					PQPy	50	65	2375	358.0	361.0	1.4	Tr	10	0	0.1	0	-	3	12	0	-	1	1				
					"	70	35																				
					WQPy	50	100																				
					PQPy	50	25	2376	361.0	364.0	0.4	Tr	10	0	0.1	0	-	4	4	0	-	1	3				
					"	70	75																				
					WQPy	70	100																				
					PQPy	70	100	2377	364.0	367.1	0.5	Tr	10	0	0.2	0	-	2	3	0	-	0	-				

		GEOLOGIC DESCRIPTION	STRUCTURE					SAMPLES			MINERALS					MINERALIZATION VEINS				ASSAYS									
FROM	TO		FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeO*	Cat	Carb	PYRITE		Pink Oz-Py		CARB		White Oz-Py		Au	Cu	Ag	Mo		
																No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk						
367.1	368.3	Mag-crustic Dyke: 0.5 x 1.0cm blocky phenocrysts in lg. sericitic matrix. Phenos (K <sub>2</sub> SO <sub>4</sub> ?) altering to celestite + sericite. 8% druse Mg = <1% py; 10% (mag-crusts, sericite and magnetite whisps) 15°C A. FW and HW ground.						2378	367.1	368.3	-	-	-	-	-														
368.3	375.9	Sil <sup>1</sup> Breccia: Brecciated gts-mgn altered sediments cut by several large gray/gray-pink qtz veins with well developed network py-cp veinlets. Crushed network appearance extends into diffused 2nd envelope but diminishes markedly in sections of 2nd lithic fragments.	368.3	369.0	CP-PY network	60/70°	80%	2451	368.3	369.0	20%	1.0%	10%	0	tr.	1	0.2cm	0	-	0	-	0	-						
					10% qtz-ss	50°	70%																						
					chlt + py	75°	10%																						
					+ Sphalerite	0°	20%																						
		267.0-270.1 p. gray qtz-crushed appearance (network veinlets). cp and py on network fractures 369.2 - 1cm cp/py veinlet 60° contains tetrahedrite + br maly = sulphosalt	369.0	370.1	CP-PY-PY network	25/50°	50%	2452	369.0	370.1	14%	3.9%	17%	0	tr.	0	-	1	110	0	-	0	-						
					"	75/5°	50%																						
					CP-PY	60°	70%																						
					"	50°	20%																						
		267.0-270.1 p. gray qtz-crushed appearance (network veinlets). cp and py on network fractures 369.2 - 1cm cp/py veinlet 60° contains tetrahedrite + br maly = sulphosalt			PQPy	50	100																						
		370.1 - 371.5 sil-mgn altered well rock weak network hostings with traces cp + py. Wellrock 2nd decreases w depth, comprising ser-cel	370.1	371.5	CP-PY network	±20°	20%	2453	370.1	371.5	1%	1%	10%	0	tr.	1	410cm	5	37	0	-	0	-						
					"	45°	50																						
					"	60°	70°																						
					PQPy	20	20																						
					"	50	60																						
					"	70	20																						
		371.5 - 373.0 p. gray qtz v. network cp-py veinlets as above. cp-py veins ~0.5cm @ 50°C A py veins 2@ 20°C A (tr. cp) Black congl. on cp exposed on 40° fractures - soft, gray black - chalcocite?	371.5	373.0	CP-PY network	50-60°	70%	2454	371.5	373.0	8%	1.5%	4%	0	tr.	2	5cm	1	236	0	-	1	4						
					"	25°																							
					PQPy	20	100																						
					WQPy	20	100																						

fractures - soft, gray black - chalcocite?







**HOLE 1218**

**11981.71 NORTH**

**25367 EAST**

**581.69 m ELEVATION**

**LENGTH: 408.1 m**





GEOLOGIC DESCRIPTION		STRUCTURE					SAMPLES		MINERALS					VEINS				ASSAYS								
FROM	TO	FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeO <sup>+</sup>	Cal	Carb	Pyrite	Qz-Py	CARB	No. Vein		Cum thk		Au	Cu	Ag	Mo	
															No.	Cum	No.	Cum	No.	Cum	No.	Cum				
16.2	17.2	16.2	17.2	Qtz=Magn. " " " " " " Qtz-calc. chl Py-cp chl-carb	15° 45° 60-75° " " 50° 10° 40° 85°	65° 10 25 " " 100 " " " "	2506	16.2	17.2	1%	tr	5%									38	76cm				
19.2		17.2	21.4	Qtz=Magn. " "	45° 15°	70 30	2507	17.2	21.4	2%	tr	3%						1	3cm	19	30cm					
21.4		21.4	24.1	breciated			2508	21.4	24.1	3%	tr	5%						5	6cm							
24.1		24.1	25.6	Qtz <sup>mag</sup> Py-cp	60° 60°	75 75	2509	24.1	25.6	5%	0.2%	9%						5	6cm							

16.2 17.2 Battered Siltstone: dark gray green; ch/bi. ser. + hornfelsic; original fabric obliterated; cut by Qtz<sup>mag</sup> magn. up to 10cm. thence Qtz-calc. chlorite veins followed by a network of hairline Py-cp carb-chl veins. Magnetite concentrated along wall boundaries (replacement of host rock) and replacing horsts from rims into chloritic cores.

21.4 as above with more intense brecciation of 1-2 cm Qtz magn chl veins (90° brecciated), attitudes of segments similar to above. Network of hairline py cp chl veins intensifies down hole. Some Qtz<sup>mag</sup> frs rounded.

24.1 Qtz<sup>mag</sup> veins, intensifies generally 60-95° CA.











FROM	TO	GEOLOGIC DESCRIPTION	STRUCTURE		SAMPLES		MINERALIZATION										ASSAYS					
			FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	MINERALS				VEINS				Au	Cu	Ag	Mo
											Py	Cpy	Fe-ox	Cal	carb	PYRITE		Qz-Py				
No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk															
		Calc = py cp veinlets in network style often filling spaces to 0.5 cm at intersections 77.1 - 20cm semi massive py w vsg cp concentrated on boundaries contained in silice + zones 77.3. 3cm lake limestone qtz v. 20° CA																				
77.1	77.1	Silic <sup>o</sup> Bx marked increase in Fe-ox including 90° replaced lithic frags. Magnetite banding more pronounced - subparallel CN (5-15°) where larger frags occur  Qtz mag = py up to 2cm @ 45° CA - appears to be conduit for per v-25% silic <sup>o</sup> elongation - magnetite on lithic frags and replacement bands with frags. Veins are bidirectional generally in zone from mag > py end or mag mag silic <sup>o</sup> at 50° or 70° Qtz + py mag end py cp veinlets later (± 45° in qtz)  Note: Im rind on mag > py > cp				2527	77.1	77.1	1%	1%	9%	21%	6	4cm	2	30						
77.1	80.2	As above: Negligible py cp Network veins: Calc ± py, mag. ± 15°, 45°, 85° For mag P is 1°-35° fracture w spec. to be filled Mag > py in v. veinlets	85		Mag P1	85°	2528	77.1	82.2	0.5%	1%	10%	1%	0.5	2	14cm						
80.2	83.2	7cm x 3cm massive mag vein segment cut by lake 30° qtz v. wk network ds			Pythn <sup>CP</sup>	60-65	2529	80.2	83.2	0.5%	0.1	6%	1%	3	35cm							

85° 20  
45° 20



FROM TO		GEOLOGIC DESCRIPTION	VEIN THICKNESS	STRUCTURE			SAMPLES		MINERALIZATION						ASSAYS													
FROM	TO			FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	Fe <sup>2+</sup>	Cal	Carb	VEINS PYRITE		Qz-Py		CARB		Au	Cu	Ag	Mo		
																No.	Cum	No.	Cum	No.	Cum	No.	Cum					
																Vein	thk	Vein	thk	Vein	thk	Vein	thk					
80.2	83.2	83.0 - Med Cr/Cu/Fe in silt and silty lith. Frags 1cm py mag & 60CA silt																										
83.2	86.3	Bx cov. - banded mag in Frags. Py cp ± horn network veins subparallel core line and on 5° and mag. Horn predominant 1cm Fe Br.		83.2	86.3	1st-3rd 0.5cm 55° 50% 75° 50% mag 55° 60%		2530	83.2	86.3	1%	0.2	10%	-	-													
86.3	89.3	As Above: Cov. 1st, soft ed. in thin red on westward fracture parallel core. 0.5cm blebs cp 25°CA		87.7	88.7	Qz py Aspition Network 60° 35-45° 5° 1 65° 30%		2531	86.3	89.3	1%	0.1	10%			1	1cm	1	1.0m									
89.3	91.4	Sil <sup>d</sup> Bx - Bx Qtz-pyrom. 89.9 91.2 cp-py network veins with bleby cp & limonite (Fe carb?) and on py cp mag. Carb on network veins - leaching				Qtz-py Mag cp py ? ±5° 40% 60-75° 40%		2532	89.3	91.4	3%	1.0%	2%	2%					1	1.3m								
91.4	92.4	Sil <sup>d</sup> Bx 91.4-92.0 km ± pure? jar?, real? replaced py cp Fe ox 25 matrix in breccia - water course? As usual there is a trace of chlorite with mag in original silt <sup>d</sup> frags		91.4	92.0	Lim Bx Qz py Aspition 45°?? 30° 50 85° 50 As usual 45° 100 ±10°		2533	91.4	92.4	1%	0.2%	5%	3%														
92.4	95.4	Sil <sup>d</sup> Bx - accentuated by weathering of carbonate mag + S <sup>2-</sup> on micro fractures, led creamy-beige min on led breccia fractures 5 cent hematite (jarosite?), horn on led fractures set 0/45° (black spot) at cp py on uk network fractures				As above		2534	92.4	95.4	2%	0.2%	6%	2%														

with  
kade Qtz (hor/hrs)  
87%

Gum Qtz ±5°  
8 50cm  
kade with Qtz  
3 5cm

FROM		TO		GEOLOGIC DESCRIPTION				STRUCTURE				SAMPLES		MINERALS					MINERALIZATION VEINS				ASSAYS			
FROM	TO	FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeOx	Cal	Carb	Pyrite No. Vein	Pyrite Cum thk	Qz-Py No. Vein	Qz-Py Cum thk	Carb No. Vein	Carb Cum thk	Other No. Vein	Other Cum thk	Au	Cu	Ag	Mo
94.5	98.5			As above heavily weathered			2535	95.4	98.5	0.5	0.7%	8%		5%												
98.5	101.1	98.5	101.1	Sil <sup>d</sup> Bx in As above but less weathered. 98m - 90cm Qtz v at 45° CA with 14 cm massive py in middle (bifurcated vein?). Generally v. lg w rolled py clogs to 0.5cm. faulted? No cp in massive py; only in narrow veinlines and weakly disseminated in siliceous zones. Both veinline faultings cut by late FeOx veinlines. NCA.	25/55	80°	2536	98.5	101.1	6%	0.4%	8%		1%			1	40cm								
101.1	100.5	101.1	100.5	Sil <sup>d</sup> Bx includes bx <sup>d</sup> Qtz veins reworked by py-cp-FeOx network vein ± carb. NB. Cp in 1-2 mm seems on network host > py	±45°	40°	2537	101.1	104.5	1.5%	1.0%	6%		1%												
104.5	107.6	104.5	107.6	Sil <sup>d</sup> Bx mainly bx <sup>d</sup> Qtz v. 104.5 - 105.5 bx <sup>d</sup> Qtz v w massive cp=py vein in middle. Bx veins display well developed network veins with py=cp. Section re bx ± 30° veinline (crushed but complete).	45°	35°	2538	104.5	107.6	3%	2.5%	4%		1%												
107.6	110.6	107.6	110.6	Sil <sup>d</sup> Bx - bx <sup>d</sup> Qtz v in 20° hrs. of mag banded with (25° CA). Cp as blebs and seams on network veinlets - numerous 1-3mm sil <sup>d</sup> cavities due to leaching of calcite. mag. cp weakly diss. in siliceous envelopes. NB. - Tr. Ni, Cu 108.5 on weathered fault zone.	15°	45-50°	2539	107.6	110.6	3%	1.0%	5%		1%												
					±20°	40%																				
					45°	30%																				
					70°	30%																				
					35/55	70%																				
					70°	15%																				

- 35° dominant and most weathered veinline. calc v. direction (wk shear?)

70° 15%

Green Qtz

Green Qtz

6m Qtz

3 30m

6m Qtz

8 20m

10 1.8m

1 1.3

FROM TO		GEOLOGIC DESCRIPTION	STRUCTURE		SAMPLES		MINERALIZATION																						
							VEINS						PYRITE				Oz-Py		CARB		ASSAYS								
							FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeO <sup>+</sup>	Cal	Carb	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	Au	Cu
110.6	113.1	Sil <sup>1</sup> Bx - 29 above NO. 0.5' - 1cm angular slats of cp in late white qtz v. 5' to 10' Network coppers to assist	111.8	112.15	Grtz v CP-Py vertical 1-4 dip 45° 15° 45° 50° 85° 50°	45°	2540	110.6	113.1	9%	0.8%																		
113.1	115.9	Sil <sup>1</sup> Bx - strong leaching of carb + FeOx + S <sup>2-</sup> . Rock badly broken - mainly at 5°/30' / 60° CA (Fault?) km on westward surface + thin earthy red brown encrustation assoc w minute blocks of Nat. Cu. Fresh breaks on rock face reveal minute diss <sup>d</sup> cp. It appears that most of rock texture related weathering of cp-py and calcite mg network fractures.	Similar to above.				2541	113.1	115.9	Uncertain due to strong leaching																			
118.7	121.5	Sil <sup>1</sup> Bx - well weathered - most network fractures leached of carb, S <sup>2-</sup> , FeOx and contact with jarositic(?) limonite + Quartz + earthy deep red crustings + Nat. Cu. + malachite. Zone is probable water course!	Similar to above.				2542	118.7	121.5	uncertain due to weathering																			
115.9	118.7	Sil <sup>1</sup> Bx - broken core - light weathering on fractures - ochre hm. 115.9 - 116.3 Gray Qtz v. white cp-py 0.3cm veins @ 45° Ground core 116.9 - fault in gray Qtz vein + leaching of network veins increases w depth. - malachite					2543	118.7	121.5	uncertain due to weathering and disruption of core																			

Note:  
Reverse order  
of description only

Gray Qtz  
2 vein

FROM TO		GEOLOGIC DESCRIPTION	STRUCTURE					SAMPLES		MINERALS					VEINS				ASSAYS								
FROM	TO		FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeO <sup>+</sup>	Cal	Carb	VEINS PYRITE	Qz-Py	CARB			Au	Cu	Ag	Mo			
															No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk					
121.5	122.8	Sil <sup>1</sup> Bx. Gmz qtz v with network py-ep veinlets and 2cm massive py cut off by very thin irregular FW at 55° CA. Distribution of lots which qtz vs generally controlled by breaks between mgn sil <sup>1</sup> lithic frags. 122.4 - man replaced lithic frags enclosed within white qtz rimmed by Nctiv-Cu. Trace Nctiv Cu on some late fractures // CA. Trace chl in mgn in zoned frags.	121.7	122.0	Gmz qtz with white area vs	?		2544	121.5	122.8	4%	0.4%	6%														
122.8	125.9	Sil <sup>1</sup> Bx: Chlorite in late carb S <sup>1</sup> hem hairline network veinlets. Rock has less porphyry of lesser sil <sup>1</sup> - vein boundaries and lithic frags more distinct. Hem 7 mgn in late veins. Sulphides low. Calcite (carbonate) green coloured. 123.6 cp in white qtz rimmed by spec.	122.8	125.9	wh. qtz Gmz qtz with carb chl	45° 60° 46° 0-5°	80° 20%	2545	122.8	125.9	1%	0.1%	8%	4%													late white qtz 13 5cm Gmz qtz 7 5cm
125.9	128.9	Sil <sup>1</sup> Bx: lithic frags contain more carbonate which has not been replaced by silice as well as chl. Network calc + chl ± hem py ep. Blocks cp in white qtz. Slight leaching of CA // veinlets.			Gmz qtz network calc + chl off.	25° 55° 40/50° 0-5° 30°	25° 50°	2546	125.9	128.9	1%	tr.	8%	6%													6mz Al <sub>2</sub> 23 6cm wh. qtz 5 5cm
128.2	131.8	Sil <sup>1</sup> Bx as above - low S <sup>1</sup> late calcite @ 45° CA. Bright green ser. ? in calcite in frags.	128.2	131.8				2547	128.2	131.8	1%	tr	7%	5%													Very fine 6 53



FROM TO		GEOLOGIC DESCRIPTION	STRUCTURE				SAMPLES		MINERALS					VEINS				ASSAYS										
FROM	TO		FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeO	Cal	Carb	Pyrite	Qz-Py	CARB	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	Au 1BX	Cu 5BX	Ag 2BX	Mo
139.1	139.8	Sil <sup>d</sup> Bx ss above bal ser/cerb 21 <sup>st</sup> not evident.	139.1	139.8	Gmy Qtz cp Fe ser-cerb late Fe Hatched 85°	45° 35/45° 0, ±15° 80%	100% 70% 80%	2550	139.1	139.8	0.5%	0.5%	8%	2%									7	30cm				
139.8	141.6	Sil <sup>d</sup> Bx ss above - ser/cerb 21 <sup>st</sup> limited to late stage along irregular fractures abounding serb + S <sup>+</sup> Fe from fractures creates broken core. Water course 2° Cu 1 km on most fractures			cp Fe + Fe late ser cerb ± Fe	25° 60° ± 5 ± 15	50% 50%	2551	139.8	141.6	1.0%	0.2%	8%	8%											5	70	25	
141.6	144.2	As Above relatively solid masses of 'ser' in Lithic frags.	141.6	144.2	Pt-cp ± Fe carb + pyrite quartz	20° 50° ± 30 70 46°	20 50 30 60%	2552	141.6	144.2	0.5%	0.1	8%	5%									3	30cm	70	15	20	
144.2	146.4	As above: heavy weathering 145.3 - 146 - Part 1 ± 2° Cu wt 'crust' mineralization 1 km on south Prad.	144.2	146.4	Broken Part 1?			2553	144.2	146.4	0.5%	0.1	12%	5%											5	70	25	
146.4	149.3	As above: with rock composition 35% Qtz v. with generally diffused boundaries; white thin than grey stz. Finer Lithic frags 1-2° Cu ± Cuprite, Cu			Grey white Qtz v. carb + ser halite	45° 60° ± 15 60° 0	40 40 50% 45 15	2554	147.2	149.3	0.5	1%	15%	3%											5	60	35	
149.3	152.4	As above - Carbonate - S <sup>+</sup> - Feox leaching @ 149.8 (0.5m) 150.7 (3m) late crushed fractures in ser-cerb ± S <sup>+</sup> Feox. Mn on 2x 1cm clots			Gmy Qtz white Qtz cerb	70° 30° 45° 45/20°	70 30 80 70°	2555	149.3	152.4	1.0	1%	15%	5%										3	20cm	70	10	20

Spec on late fractures. Secondary  
Cu - Malin, cuprite etc.

late stage  
ser-cerb  
cp Fe



FROM TO		GEOLOGIC DESCRIPTION	STRUCTURE				SAMPLES		MINERALIZATION						ASSAYS													
FROM	TO		FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeOx	Cal	Carb	VEINS PYRITE No. Vein	Cum thk	Qz-Py No. Vein	Cum thk	CARB No. Vein	Cum thk	No. Vein	Cum thk	Au 70%	Cu 5%	Ag 1%	Mo	
165.5	168.6	25 above: many gtz vein fragments, occasional py in white stz. 5' veinlets irregular and patchy. 166.2 - 10cm mag calc chkr @ 45° CA	165.5	168.6	whit gtz	45-90	70	2561	165.5	168.6	2.0%	0.2%	20		1%							22	30m				30%	
					75-90	30																						
					40°	50																						
					60°	50																						
166.6	171.6	25 above: specularly commonly rimming white gtz v.			whit gtz	65	50	2562	166.6	171.6	1.0%	4.1	75%		1%							17	25				30%	
171.6	173.8	25 above: badly broken and on <sup>d</sup> on fractures at acute angles to core. carb <sup>d</sup> 5' + Feox leached. - watercourse fault?			gtz veinlets	75	30	2563	171.6	173.8	2%	0.2	20		2%													20%
					"	45	30																					
					CP-Py Feox	40°																						
173.8	176.1	25 above: 2 gtz veins with later 1cm py-ep veinlets in each @ 20° CA; minor biotite ep. network. Limonite on acute angled fractures in 2° Cu			ltk carb ep Feox	± 20°	60%	2564	173.8	176.1	2%	0.3%	10%		1%												40%	
176.1	179.5	25 above: with several gtz Feox veins, wk biotite ep-ep. Carb. py-ep-her leaching → lim + 2° Cu	176.1	179.5	Py gtz gtz	45° 60°		2565	176.1	179.5	1.2%	0.2%	15%			1	10m					21	7m				40%	
						45°	30°																					
					carb py ep her	45°																						
						60°																						
179.5	182.9	Sil <sup>d</sup> Breccia: 25 above. weak ep-py stringers; ltk network of gtz carb chl + py ep her			gtz gtz	15°	20	2566	179.5	182.9	2%	0.3%	20%														40%	
						45°	50																					
						60°	30																					
					ep-py	60°																						
182.4	184.0	25 above: strong network fractures of ep-py; 182.7 - 1cm massive cp @ 45° CA. Increases in chl. calcit especially in lithic frags.			cp-py	60°	50	2567	182.4	184.0	5%	1.0	12%														50%	
						35°	20																					
						20°	10																					

gtz gtz 25° 50°



		GEOLOGIC DESCRIPTION	STRUCTURE					SAMPLES		MINERALIZATION				VEINS				ASSAYS												
FROM	TO		FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	MINERALIZATION				PYRITE		Qz-Py		CARB		ASSAYS									
											Py	Cpy	FeOx	Cal	Carb	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	Au 3x	Cu 3x	Ag 3x	Mo			
184.0	185.3	ps above: calc + chl noticeable in ground mass of some lithic bands network of py veinlets mod. developed * NiCu + brassy, angular min (marcesite?) on late acute ch. fractures.			74.7 gtz	15°	70%	2568	184.1	185.3	2%	0.3	12%	2%								7	15							75%
185.3	187.6	2a above: section dominated by acute & made gray gtz vein with well developed network of cp-py-Feox and ser py-cp veinlets.	185.9	187.6	gray gtz cp-py ser-py- hem	20°	60/40 70°	2569	185.3	187.6	2%	0.3	4%	2%									1	1.7m					80%	
187.6	189.9	Sil <sup>10</sup> Breccia - occasional cp-py veinlets @ 60°-45°, wk ser-chl py hem veinlets. Sphalerite on boundary of some white stz e.						2570	187.6	189.9	1%	0.1	30%	1%										9 10m 6 4cm					8%	
189.9	194.1	As above: weak S <sup>-</sup> remains chl/ser hem with gray gtz veins						2571	189.9	192.9	1%	0.1	30%	1%										gray gtz 20 6.5m whl gtz 5 3cm					8%	
								2572	192.9	194.1	1%	0.1	30%	1%															8%	
194.1	199.0	Sil <sup>10</sup> Breccia 2a above 194.2 to 194.85 - 2 crushed gray gtz veins committal with fine stz-calcite-sericite chlorite network of late veinlets. Minor cp-hem stringers 196.6 to 199.0 several gray gtz veins display early brecciation and stringers possibly pre 6° in subsequent movement. gtz calc chl S <sup>-</sup> appear to hold rock together. To Mt. Cu on occass look for calc veinlets			Gray gtz	60°	60%	2573	194.1	196.6	1%	0.1	25%	3%										6 13 whl gtz 5 8cm					35%	
			198.3		ser. shear in stz + S <sup>-</sup>	65°	50°	2574	196.6	199.0	3%	1.0	10%	3%										7 1.1m					60%	

GEOLOGIC DESCRIPTION		STRUCTURE		SAMPLES		MINERALS					VEINS				ASSAYS									
FROM	TO	FROM	TO	TYPE	°TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeOx	Cal	Carb	Pyrite No. Vein	Qz-Py Cum thk	Carb No. Vein	Carb Cum thk	Ag-Cu No. Vein	Ag-Cu Cum thk	Au	Cu	Ag	Mo
199.0	200.9	199.0	200.9	whit quartz w/ hem py-cp epidote 70° 90° QTZV15			2575	199.0	200.9	2%	1.02	20%	4%											
200.9	205.1	200.9	202.4	whit glz smg glz carb py-cp 35-40° 70° 30° 50° QTZV20	45°	60°		200.9	202.4	1%	0.2%	25%	3%											
		202.4	205.1	smg glz whit glz 65-70° 45° 60°	75%	75%	2577	202.4	204.3	2%	0.4	25%	4%											
205.1		205.1	208.1	STGR QTZ MC 50 70 30 STGR QTZ CARBON	20	30	2578	204.3	208.1	Tr	Tr	10	nil	Tr	0	0	3	0.5	1	6.0				
		208.1	211.1	STGR QTZ MC 50 70 STGR QTZ Py 70	20	10	2579	208.1	211.1	Tr	Tr	10.0	0	0.5	6	12.0	4	4.0	0	2	7.0			

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FROM TO		GEOLOGIC DESCRIPTION					STRUCTURE						MINERALIZATION																	
													SAMPLES					MINERALS					VEINS				ASSAYS			
													FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeD <sup>+</sup>	Cal	Carb	Pyrite	Qz-Py	Carb	WGT-P	Au
													No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk										
		SILICIFIED QUARTZ - MAGNETITE BRECCIA (CONT)					238.0	241.0	STRG DQ-P	50	100	2589	238.0	241.0	0.3	0.5	7	0	tr	0	1	3	0	0						
		243.0-244 - Flt 1-3 cm					241	244	STRG DQ-P WAP	50	100	2590	241.0	244.0	1.2	0.8	7	0	tr	0	1	36	0	1	8					
							244	247	STRG WAP DQ-P	50	100	2591	244.0	247.0	0.6	1.0	8	0	0.3	0	2	43	0	2	6					
		247.7-247.8 - Flt 1-3 cm					247	251	STRG PY	70	50	2592	247.0	250.0	1.4	0.9	6	tr	0.5	2	4	2	44	0	2	70				
		248 small bleb spec hem + pylosilicates 247-250 (green)							STRG WAP DQ-P	50	100																			
		251.5 - 1-2 mm WIRE NATIVE Cu					250	253	STRG DQ-P WAP	50	100	2593	250	253.0	1.0	0.8	6	tr	0.3	0	3	73	0	4	36					
		253.9 - STRONG BID MINOR SPEC HEM					253	256	VEIN QTZ-PY	70	100	2594	253	256.0	0.3	0.4	9	0	0.2	1	85	1	120	0	0					
		256 STRONG BID ON FRACTURE SURFACE E Cpy																												
							256	259	STRG WAP	50	100	2595	256	259	2	0.2	6	0	tr	1	50	0	0	3	12					
							259	262	STRG PY DQ-P	70	100	2596	259	262	0.1	0.2	9	tr	0.1	1	2	0	0	2	9					
		263.5 - 25cm GREY QTZ-PY VN E mod. chl.					262	265	VN QZ QTZ-PY STRG DQ-P	50	100	2597	262	265.0	0.2	0.3	6	0.2	0.2		2	110	0	1	25					
		265 chl - mod to STRONG																												
							265	268	VN QZ QTZ-PY			2598	265.0	268.0	1.0	0.3	5	tr	tr	0	2	85	0	1	50					

## MINERALIZATION

FROM	TO	GEOLOGIC DESCRIPTION	STRUCTURE					SAMPLES		MINERALS					VEINS				ASSAYS										
			FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeOx	Cal	Carb	VEINS PYRITE	Cum thk	NO. OF VEINS	Cum thk	CARB	NO. OF VEINS	Cum thk	WHITE QL-PY	NO. OF VEINS	Cum thk	Au	Cu	Ag	Mo
		SILICIFIED QUARTZ-MAGNETITE BRECCIA (CONT)	268	271.0	STR POP VN GREY QTZ-PY	50 70	100 100	2599	268.0	271.0	0.6	0.3	5	tr	tr	0		2	190			GREY 1	80						
		269.4-270.2 - GREY CRACKLE QTZ-PY VN n 1-2% PH * - NATIVE Cu @ 270.2 (PRIMARY) + on FRACTURE - wk - mod ser - epi	271	274	STR POP " " STR WQP	70 50 50	50 50 100	2600	271.0	274.0	0.8	0.5	7	tr	0.1	0		2	50			1	8						
		275-277 - mod. ser - epi	274	277	STR POP STR WQP	20 50	100 100	2601	274.0	277.0	1.2	0.3	8	0	0.1	0		1	2			1	4						
					WQP	50	100	2602	277.0	280.0	0.1	tr	8	tr	0.1	0		0	0		2	4							
					POP	20	50	2603	280.0	283.0	1	1.5	8	tr	0.3	0		3	38	0		1	2						
					WQP	50	100																						
					POP	50	100	2604	283.0	286.0	1	0.6	9	0.2	0.6	0		2	94	0		0							
		288.2-289.5 - Bull QTZ VN			POP	50	100	2605	286.0	290.0	2	0.9	8	0.2	0.4	0		1	66	0		1	26						
					WQP	50	100																						
		* QTZ-MT DYKE 60% MT 40% QTZ - WELL DISSEMINATED						2606	290	291.5	0.2	0.3	13	-	-	-	-	-	-	-	-	-							
								2607	291.5	294.0	0.2	tr	9	tr	tr	-	-	-	-	-	-	-							
								2608	294.0	297.0	0.2	tr	10	tr	0.3	-	-	-	-	-	-	-							
		BECOMING MORE ALTERED & SERICITE OIL & GREEN PHYLLOSILICATES			WQP	50	100	2609	297.0	300.0	0.1	0.2	9	0.1	0.5						1	2							



FROM		TO		GEOLOGIC DESCRIPTION					STRUCTURE					SAMPLES		MINERALIZATION							ASSAYS			
				GANDID										SAMPLE NUMBER		MINERALIZATION							ASSAYS			
FROM	TO	FROM	TO	TYPE	TCA	ZTCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeSt	Cal	Carb	VEINS PYRITE	Pyrite	Pink Oz-Py	CARB	WHITE QZ-PY	ASSAYS	Au	Cu	Ag	Mo		
															No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk				
							2622	336.0	339.0	0.2	tr	1	0.3	0.6	-	-	-	-	-	-	-	-	-	-	-	
							2622	339.0	342	0.3	0.3	3	0.1	0.3	-	2	85	-	-	-	-	-	-	-	-	
							2624	342.0	345.0	0.5	0.3	1	0.1	0.3	-	-	-	-	-	0.95V	2	127	-	-	-	
							2625	345.0	348.0	0.6	0.6	1	0.1	0.2	-	1	60	-	-	0.95V	1	80	-	-	-	
344	363						2626	348.0	351.0	0.1	tr	3	tr	0.5	-	-	-	-	-	-	-	-	-	-	-	
							2627	351.0	354.0	1.2	0.3	3	tr	0.3	2	8	1	40	-	-	-	-	-	-	-	
							2628	354.0	357.0	0.8	0.3	2	tr	0.1	1	2	1	130	-	-	-	-	-	-	-	
							2629	357.0	360.0	0.2	tr	4	tr	0.2	-	-	-	-	-	-	-	-	-	-	-	
							2630	360.0	363.0	0.5	0.3	6	0.1	0.3	1	4	5	110	-	-	-	-	-	-	-	
							2631	363.0	366.0	0.5	0.2	5	0.1	0.2	1	4	4	21	-	-	-	-	-	-	-	
							2632	366.0	369.0	0.1	0.1	6	0.1	0.2	-	12	35	-	-	-	-	-	-	-	-	
							2633	369.0	372.0	0.2	0.2	5	0.1	0.5	1	2	15	86	2	1	-	-	-	-	-	

FROM TO		GEOLOGIC DESCRIPTION	STRUCTURE				SAMPLES		MINERALIZATION						VEINS				ASSAYS							
FROM	TO		FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeSt	Cal	Caro	Pyrite	Qz-Py	CARB					Au	Cu	Ag	Mo
															No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk				
		(CONT)																								
		K SPAR MEGACRYSTIC PORPHYRY			PQP	70	70	2634	372.0	375.0	0.5	0.3	5	0.1	0.3	1	0.5	13	55	-	-					
		- MOD SER				50	20																			
		- WR CHL, BIO				20	10																			
					Ry vnt	70	100																			
					PQP	70	75	2635	375.0	378.0	0.5	0.3	5	0.1	0.3	2	2	9	52	-	-					
						50	25																			
					Py-QC	70	100																			
					PQP	70	50	2636	378.0	381.0	0.6	0.2	6	tr	0.3	-	6	33	1	3	-	-				
						50	50																			
					PQP	70	20	2637	381.0	384.0	0.3	tr	5	0.1	0.3	1	4	6	112	-	-					
						50	80																			
					Py vnt	90	100																			
					PQP	70	40	2638	384.0	387.0	0.4	tr	6	tr	0.2	-	8	58	-	-						
						50	60																			
					PQP	70	20	2639	387.0	390.0	0.4	tr	5	0.1	0.3	-	6	79	-	-						
						50	70																			
						20	10																			
					PQP	70	50	2640	390.0	391.4	0.6	tr	5	0.2	0.4	-	5	47	-	-						
						50	50																			
391.4	396.6	MYLONITE SHEAR ZONE			PQP	70	100	2641	391.4	394.1	0.6	tr	7	tr	1.0	-	1	6	-	-						
396.6	408.1	ALTERED PORPHYRY / QUARTZ EDH Fe-Ox REPLACEMENTS						2642	394.1	396.6	0.8	tr	6	tr	1.0	-	-	-	-							
		- REMNANT K SPAR FRAGMENTS						2643	396.6	400.0	0.8	tr	5	0.1	0.5	-	-	-	-							
		- WE TO MOD CHL						2644	400.0	404.0	0.5	tr	7	0.2	0.8	-	-	-	-							
								2645	404.0	408.1	0.4	tr	6	0.2	1.0	-	-	-	-							

EDH









FROM TO		GEOLOGIC DESCRIPTION	STRUCTURE					MINERALIZATION																				
								SAMPLES			MINERALS					VEINS				WHITE		ASSAYS						
								FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeO <sup>+</sup>	Cal	Ca <sup>2+</sup>	Mo	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein
		ALTERED HORNFELS (SILICIOUS) CONT.			PQ-Py	75	25	2902	123.7	126.8	0.6	1.1	10	0.2	0.2	tr		4	30									
		- moderate chlorite alteration - weak sericite & biotite			PQ-Py	75	75	2903	126.8	129.8	1.0	0.6	9	0.3	0.1	tr		4	20									
		- K SPAC alteration is intense			PQ-Py	75	45	2904	129.8	132.9	1.2	0.5	9	0.1	0.2	-		4	24									
						50	25																					
						20	30																					
					PQ-Py	75	25	2905	132.9	135.9	1.6	0.7	10	0.4	tr	tr		8	28									
						50	75																					
					PQ-Py	75	100	2906	135.9	139.0	1.3	0.9	10	0.1	0.1	0.02		2	14									
					PQ-Py	75	100	2907	139.0	142	1.0	0.6	9	0.3	1.0	tr		2	10	1	1							
					Q-C	85	100																					
					PQ-Py	75	100	2908	142.0	145.1	1.5	0.9	8	0.2	1.2	0.03		3	5									
					PQ-Py	75	15	2909	145.1	148.1	1.4	1.3	9	0.3	1.6	0.06		9	125									
		* healed Q-C shear zone @ 147.9 4cm ± 2-5% Cpy + 0.5% Mo?				40	35																					
						30	50																					
					PQ-Py	50	30	2910	148.1	151.2	1.2	0.9	11	0.1	0.1	-		3	36									
						20	40																					
						70	30																					
					PQ-Py	40	100	2911	151.2	154.2	1.3	1.2	10	0.4	1.3	-		3	93									
					Py Str	75	100	2912	154.2	157.3	1.6	0.7	10	0.1	1.0	tr	1	1	15	50	1	3						
					Q-C	85	100																					
					PQ-Py	70	30																					
						45	55																					

20 15

FROM		TO		GEOLOGIC DESCRIPTION				STRUCTURE				SAMPLES			MINERALIZATION						VEINS				ASSAYS			
FROM	TO	FROM	TO	TYPE	TCA	X TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeOx	Cal	Caro	Mo	Pyrite	Qz-Py	CARB	White Qz-Py	Au	Cu	Ag	Mo					
										No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk									
				PQ-Py	75	60	2913	157.3	160.3	1.0	0.8	11	0.4	0.8	0.03		9	67										
					50	10																						
					20	30																						
				- strong Biotite along margins of Qtz-Py stringers @ 158.3	PQ-Py	70	2914	160.3	163.4	1.1	0.4	12	tr	tr	-		2	2										
				Qtz-Py vein @ 158.7-159.3 UC @ 20° TCA	PQ-Py	70	2915	163.4	166.4	1.5	1.0	9	0.4	1.2	-		5	94										
					55	20																						
					20	10																						
				- core badly broken (4-8cm) from 160.0-166.4	PQ-Py	45	2916	166.4	169.5	1.0	0.6	9	0.1	tr	-		7	25										
				165-165.9 Qtz-Py vein?	PQ-Py	75	2917	169.5	172.5	1.0	0.8	7	0.4	1.6	tr	1	1	6	10									
				- badly broken		50																						
				- no core angles	Py	70																						
				174.5-174.9 - Shear Zone	py shear	45	2918	172.5	175.6	3.8	0.7	10	0.1	0.2	0.05	1	40	13	21									
				" 60% Py	PQ-Py	75																						
						45																						
						30																						
					PQ-Py	75	2919	175.6	178.6	1.1	0.7	9	0.2	0.8	-		13	54										
						45																						
						D-10																						
					PQ-Py	75	2920	178.6	181.7	0.6	0.6	9	0.1	0.6	-		17	24										
						45																						
						20																						
				* speck native Cu @ 181.7	QC	75	2921	181.7	183.8	0.7	0.4	7	0.2	0.8	-		11	43	1	5								
				5cm Q-C chlorite shear @ 181.8	PQ-py	75																						
						45																						
						20																						
						20																						
*				183.8-184.9 - Qtz-vein	Qtz vein		2922	183.8	184.9	0.3	0.4	1	0.3	1.0	-		1	110										
				UC 20° TCA LC 45° TCA	UC	20																						

LC 45











GEOLOGIC DESCRIPTION		STRUCTURE					SAMPLES			MINERALS					VEINS				ASSAYS							
FROM	TO	FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeOx	Cal	Carb	Pyrite No. Vein	Pyrite Cum thk	Qz-Py No. Vein	Qz-Py Cum thk	Carb No. Vein	Carb Cum thk	No. Vein	Cum thk	Au	Cu	Ag	Mo
				Py	75	50	2952	267.0	270.1	4.6	0.6	7	0.3	0.5	2	5	3	200								
				Py	50	50																				
				PQ-Py	70	75																				
				PQ-Py	45	25																				
				PQ-Py	70	40	2953	270.1	273.1	1.8	0.3	10	0.1	tr			8	121								
				PQ-Py	45	60																				
				PQ-Py	70	50	2954	273.1	276.1	2.3	0.4	10	tr	tr			15	71								
				PQ-Py	45	40																				
				PQ-Py	20	10																				
				PQ-Py	70	30	2955	276.1	279.2	3.5	1.2	12	tr	tr	tr	2	6	12	63							
				PQ-Py	45	40																				
				PQ-Py	20	30																				
				Py str	70	100																				
				PQ-Py	70	10	2956	279.7	282.2	3.0	0.6	14	tr	tr			12	111								
				PQ-Py	45	45																				
				PQ-Py	20	45																				
				W-Py	70	100	2957	282.2	285.3	2.5	1.4	9	0.2	0.2			7	173								
				PQ-Py	70	20																				
				PQ-Py	45	70																				
				PQ-Py	20	10																				
				Qz W	40	-																				
				LC	45°	-																				
				PQ-Py	75	20	2958	285.3	288.3	2.0	0.4	12	tr	0.1			7	42								
				PQ-Py	45	20																				
				PQ-Py	20	60																				
				PQ-Py	75	20	2959	288.3	291.4	3.0	0.4	14	tr	tr			5	103								
				PQ-Py	45	40																				
				PQ-Py	10-15	40																				

- weak to mod sericite alt'n  
- moderate chlorite alt'n  
90% of Cpy mineralization is in stringers, micro-fractures. 10% disseminated.

\* 282.2-283.4 - Qz-Py-Cpy VEIN  
- 1.5-2% Cpy in stringers & joints

Bulk Qtz  
1 B

Bulk Qtz  
1 5

Bulk Qtz  
1 3









GEOLOGIC DESCRIPTION		STRUCTURE					SAMPLES		MINERALIZATION							VEINS				ASSAYS										
FROM	TO	FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	K <sub>2</sub> O*	Cal	CaF <sub>2</sub>	MO	VEINS	PYRITE		Qz-Py		CARB		WH. RE QZ-Py		Au	Cu	Ag	Mo		
																No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk							
				Pq-Py	70	25	2991	378.7	381.7	4.6	0.7	10	0.2	tr	-			7	86											
					45	25																								
					20	50																								
				Pd-Py	75	5	2992	381.7	383.7	3.6	0.7	8	0.3	0.2	-			5	38											
					45	15																								
					20	80																								
				Pd-Py	45	80	2993	383.7	386.7	3.0	0.6	6	0.2	0.1	-				7	39										
					20	20																								
				Pd-Py	70	20	2994	386.7	390.0	3.1	1.5	7	0.1	0.1	-				10	65										
					40	40																								
					15	40																								
				Pd-Py	70	10	2995	390.0	393.5	1.9	0.4	8	0.1	0.2	tr				8	60										
					40	80																								
					20	10																								
				Py	85	100	2996	393.5	396.5	2.8	0.6	12	0.1	tr	-	1	4	5	138											
				Pd-Py	40	75																								
					15	25																								
				Pd-Py	40	100	2997	396.5	399.5	3.2	0.5	10	tr	tr					3	39										
				Pd-Py	60	60	2998	399.5	402.5	2.3	0.4	5	0.3	0.6					3	200										
					40	40																								
				Pd-Py	75	50	2999	402.5	405A	1.5	0.3	3	0.3	0.4	tr				5	38										
					45	40																								
					15	10																								

chlorite alt'n - med.

Biolite " - weak to moderate.

399.5 - 400.7 QZ-Py VEIN

weak to med silicite alt'n

FROM		TO	GEOLOGIC DESCRIPTION	STRUCTURE				SAMPLES		MINERALIZATION										ASSAYS									
				FROM	TO	TYPE	TCA	XTC	SAMPLE NUMBER	FROM	TO	Py	Cpy	K <sup>rich</sup>	Cal	carb	Mo	VEINS		Qz-Py		CARB		WHTE		Au	Cu	Ag	Mo
																No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk				
			(cont)																										
			K-SPAR MEGACRYSTIC PORPHYRY			Py vein	45	100	3000	405.4	408.4	10	0.5	0.5	0.7	2.5	-	3	33	11	71	3	12						
			<0.6-407.0 - Py vein - 5% CP LC @ 45° TCA			Q-Carb	30	100																					
						Py-Py	45	50																					
							30	50																					
405.0	411.0		QUARTZ-SERICITE-PYRITE DYKE			Q-Carb			3001	408.4	410.7	5	0.3	3	1.5	3.0	-		2	85	1	90							
			= 10% Py			Calcite	45	100																					
			- Pink Qtz-Py veinlets within unit with cpy in places.			Py-Py	30	100																					
			- also Qtz-Carb-calcite (2-4mm) juggy veinlets with 1-2mm quartz on contacts + 1-90 cm small Qtz-Carb-calcite VN 408.5-409.4			Py vein	45	100	3002	410.7	413.7	7	0.9	2	0.5	1.6	-	2	22	2	18								
						Py-Py	35	100																					
						Py-Py	85	30	3003	413.7	416.7	1.5	0.3	6	0.2	1.2	-		5	115									
							45	50																					
							20	22																					
			* FLT @ 410.7 - 412.5 RUBBLE @ 10% Py			Py-Py	95	90	3004	416.7	419.7	2.0	tr	12	0.3	0.3	-		10	162									
							40	10																					
			FLT @ 414.3 - 414.7 - Badly Broken core @ brown (chocolate) carb staining on fractures			Py-Py	80	30	3005	419.7	422.7	1.6	tr	10	tr	tr	-		7	25									
							40	40																					
							15	30																					
			FLT @ 427.2 5cm approx to TCA			Py-Py	40	100	3006	422.7	425.7	1.5	tr	11	tr	tr	-		3	25									
425.8	431.5		QUARTZ FLOODED SHEAR ZONE			Py	85	100	3007	425.7	429.7	2.5	0.3	10	tr	tr		1	2										
			- INDISTINCT CONTACTS																										
			- Shear @ 70-85°																										
									3008	428.7	431.7	3.5	0.3	7	tr	tr													
431.5			QUARTZ-FE <sub>2</sub> O <sub>3</sub> REPLACEMENT BRECCIA			Py-Py	70	50	3009	431.7	434.7	2.5	0.1	14	tr	tr			4	19									
							45	50																					
			434.9-435.9 - MAFIC DYKE																										
			LT GREEN - SMALL																										
			<1mm blebs MAGNETITE, Qtz						3010	434.7	437.7	-	tr	5	0.2	tr													
			VEINLETS <1cm @ stringers of calcite "laddering"																										

FLT @ 437.0-437.8 - Broken core - strong chlorite





**HOLE 1220**

**11842.89 NORTH**

**25600.05 EAST**

**496.781 m ELEVATION**

**LENGTH: 369.1 m**



























FROM	TO	GEOLOGIC DESCRIPTION	STRUCTURE		SAMPLES		MINERALIZATION							ASSAYS											
							TYPE		TCA	%TCA	MINERALS					PYRITE		Qz-Py		CARB		Au	Cu	Ag	Mo
							FROM	TO			Py	Cpy	FeO <sup>+</sup>	Cal	Co <sup>+</sup>	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk				
		MORINFEZ SILTSTONE - 52% Qtz veining	Pq-Py	70 45 20	30 20 50	2862	357	357.0	1.9	tr	11	0.6	0.2			7	63								
			Pq-Py	70 50	80 20	2863	357.0	360.0	1.2	0.2	2	0.9	1.0			8	98								
			Pq-Py	90 70 50 20	10 40 25 25	2864	360.0	363.0	0.8	tr	6	1.2	0.4			5	175								
			Pq-Py	70 45 20	25 50 25	2865	360.0	366.0	1.2	tr	6	0.7	0.4			6	33								
3691		EDH	Pq-Py	70 50 20	30 30 40	2866	366.0	369.1	1.3	tr	7	0.3	0.2			3	93								

**HOLE 1221**

**11978.53 NORTH**

**25117.19 EAST**

**490.304 m ELEVATION**

**LENGTH: 312.1 m**





FROM	TO	GEOLOGIC DESCRIPTION	STRUCTURE				SAMPLES			MINERALIZATION						VEINS				ASSAYS				
			FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	MINERALS			PYRITE		Gz-Py		CARB		Au	Cu	Ag	M.	
											Py	Cpy	FeO*	Cal	Carb	No. Ven	Cum thk	No. Ven	Cum thk					No. Ven
30.6	34.3	TRANSITION ZONE K SPAR ALTERED INTRUSIVE + SILICIFIED QUARTZ-MAGNETITE REPLACEMENT BRECCIA			PQ-Py	70 50 20	40 55 5	2653	30.6	34.3	0.6	0.2	7	0.3	0.6	-	6	60	-	-				
34.3	37.4	MOSTLY K SPAR ALTERED GREYWACKE & MINOR ALTERED INTRUSIVE			PQ-Py Q-C	70 50 20 70	5 5 90 100	2654	34.3	37.4	0.8	0.4	6	0.4	1.4	-	8	100	1	2	-			
37.4	41.5	SILICIFIED QUARTZ-MAGNETITE REPLACEMENT BRECCIA - mod. ser. chl + bio act.			PQ-Py Q-C	70 50 20 70	70 50 30 100	2655	37.4	41.5	1.2	0.5	8	0.5	1.2	-	8	85	3	5	-			
41.5	43.6	ALTERED GREYWACKE			PQ-Py NR-Py	50 70	100 100	2656	41.5	43.6	0.4	0.3	2	0.5	0.6	-	1	10	-	1	5			
43.6	55.6	ALTERED MEGACRYSTIC KSPAR PORPHYRY - mod. ser. bio chl. alt			PQ-Py Q-C	50 20	60 40	2657	43.6	46.6	1.0	0.5	8	0.3	0.7	-	7	50	-	-				
					PQ-Py	50	100	2658	46.6	49.6	0.5	0.3	6	0.2	1.4	-	8	100	-	-				
					PQ-Py	50 20	75 25	2659	49.6	52.6	0.6	0.6	8	0.5	1.0	-	4	76	-	-				
					PQ-Py Q-C	50 20	25 100	2660	52.6	55.6	1.5	0.4	9	0.2	1.6	-	6	95	1	2	-			









GEOLOGIC DESCRIPTION		STRUCTURE				SAMPLES			MINERALIZATION						VEINS				ASSAYS							
FROM	TO	FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeO*	Cal	Caro	Pyrite	Qtz-Py	Carb	White Qtz-Py	Au	Cu	Ag	M				
															No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk				
197.5				Silicified Quartz - Fe Ox Replacement Breccia (cont)	Po-Py	50	100	2708	200.5	203.5	10	0.6	7	0.2	0.6	3	200									
				* Pink Qtz-Py veins with	Py stor	50	100	2709	203.5	206.3	0.5	0.4	9	0.2	1.4		1	2								
				196.6 - 197.5 ~ 10% Py < 1% Cu																						
				201.3 - 203.4 ~ 5% mt < 1% Cu				2710	206.3	209.3	1.0	0.3	10	0.2	0.5											
				209.7 - 210.7 ~ 2% Cu 10% Py																						
				White/Grey Qtz-Py vein	Po-Py	50	100	2711	209.3	212.3	0.8	0.7	9.0	0.2	1.5	1	97									
								2712	212.3	213.6	1.2	0.2	11.0	0.1	0.6											
				* 213 - 217.7 - crackle texture - waxy from 217.5 - 217.7 - flt @ 20° E 1cm gause	VEIN	NE 30 SE 30		2713	213.6	217.7	2.2	0.2	6	0.3	2.2											
					flt	20°		2714	217.7	219.9	2.0	0.5	10	0.3	2.1											
				* 219.9 - 221.9 - white/grey Qtz-Py vein ~ 10% of Qtz-Ht	VEIN	NE 70 SE 20		2715	219.9	221.9	3.0	0.4	3	0.2	2.0											
					Py wst	50	100	2716	221.9	224.9	4	0.3	11	0.1	2.0	3	18					3	98			
					wo-Py	50	100																			
					wo-Py	50	100	2717	224.9	227.9	0.5	0.2	9	0.1	0.6								1	24		
					wo-Py	50	100	2718	227.9	230.9	1.0	0.3	10	0.2	1.0								1	30		
								2719	230.9	233.9	1.3	0.3	10	0.2	1.0											
				@ 234 - 237.3 green mica alteration very strong				2720	233.9	236.9	1.2	0.2	7	0.1	1.4											
				* 237.3 - 238.6 - white Qtz-Py vein @ 30° W - 2 - 1 mm blebs cpy	W-Py	30	100	2721	236.9	239.7	1.2	0.3	10	0.1	0.6								1	130		







FROM	TO	GEOLOGIC DESCRIPTION	STRUCTURE		SAMPLES		MINERALIZATION										ASSAYS								
			FROM	TO	TYPE	TCA	%TCA	SAMPLE NUMBER	FROM	TO	Py	Cpy	FeDx	Cal	Carb	VEINS PYRITE		Pink Ox-PyC		CARB		Au	Cu	Ag	Mo
																No.	Cum	No.	Cum	No.	Cum	No.	Cum		
0.0	4.5	CASING																							
4.5	5.5	RUBBLE: contains core segments and rounded fragments of very weathered hornfels and pink quartz - pyrite.						2395	4.5	5.5															
5.5	7.7	MAFIC DYKE: red. green with dark green to black biotite spots						2396	5.5	7.7															
7.7		2mm; weakly sericitic; HORNFELS (KSPAR TRANSITION) - dark grey - very fine grained siltstone - weak argill. odour to break test	7.7	11.0	PQP	LC 50 PyC 10	15	2397	7.7	11.0	0.6	0.3	2	Tr	Tr	0	-	19	57	0	-				
		- positive kspar stains @ 8.0 & 14.0 m - angular "crackly" type vein filled fractures and fissures.	11.0	14.0	PQP	PyC 10 " 50	30	2398	11.0	14.0	0.8	0.4	2	0.3	0.4	0	-	10	44	1	1				
			14.0	17.0	PQP	PyC 10 " 50 " 75 Carb 10 " 50 " 75	10 10 15 25	2399	14.0	17.0	0.2	0.1	1	1.2	1.2	0	-	8	48	7	7				
		@ 19.5: positive kspar test	17.0	20.0	PQP	PyC 10 " 50 " 75	35 50 15	2400	17.0	20.0	0.6	0.3	3	0.4	0.4	0	-	12	23	4	3				
			20.0	23.0	PQP	PyC 20 " 50 " 75	20 60 20	2401	20.0	23.0	0.1	0.6	7	0.2	0.2	0	-	10	59	4	2				
		@ 24.7 m: positive kspar test	23.0	26.0	PQP	PyC 50 " 75	55 45	2402	23.0	26.0	0.4	0.6	7	0.3	0.3	0	-	13	49	6	3				
			26.0	29.0	PQP	PyC 30 " 50	25 75	2403	26.0	29.0	1.1	0.3	5	0.7	0.7	0	-	9	102	5	4				

















**HOLE 1223**

**12090 NORTH**

**25042 EAST**

**397 m ELEVATION**

**LENGTH: 264 m**











FROM TO		GEOLOGIC DESCRIPTION	STRUCTURE					MINERALIZATION																	
			FROM	TO	TYPE	TCA	%TCA	SAMPLES			MINERALS					VEINS				ASSAYS					
								SAMPLE NUMBER	FROM	TO	Py	Cpy	Fe <sup>oxy</sup>	Cal	Carb	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	No. Vein	Cum thk	Au	Cu
		QUARTZ-FeO <sub>x</sub> REPLACEMENT BRECCIA / SHEETED QUARTZ VEINS			Pq-Py	70	20	3080	183.4	186.4	4.0	0.3	14	tr	tr			8	69						
					Pq-Py	40	100	3081	186.4	187.4	2.6	0.1	13	tr	tr			4	50						
1930		QUARTZ - MAG STOCKWORK			Pq-Py Py	40 30	100	3082	189.4	193.2	12.0	0.8	8	tr	tr	4	33	4	72						
		THE CORE IS MORE SILICEOUS TO 90% QZ.						3083	193.2	196.2	3.0	0.3	7	0.2	0.1										
								3084	196.2	199.2	3.0	0.2	10	0.3	0.1										
					WQ-Py	40	100	3085	199.2	202.2	2.4	0.1	8	0.2	0.1					2	7				
					QC	90	100	3086	202.2	205.2	2.0	tr	6	0.2	0.1					1	2				
		spic. hem with Q-C stringers			QC	90	100	3087	205.2	208.2	2.2	tr	10	0.2	0.8					5	10				
					WQ-Py	70	25	3088	208.2	211.2	1.8	tr	10	0.1	0.1						6	8			
						45	75																		
								3089	21.2	213.6	2.5	tr	8	0.5	0.1										
2136	2141	MASSIVE PYRITE VEIN - 80% Py - 15% Qtz - 2-3% CO <sub>2</sub>			Bill WQ	45	100	3090	213.6	214.1															
					Bill WQ	45	100	3091	214.1	217.2	1.2	tr	12	0.3	0.1						6	20			
					Bill Qtz	45	100	3092	217.2	220.2	1.3	0.2	12	tr	tr						1	2			
					QC	5	100	3093	220.2	223.2	1.9	0.2	11	0.2	0.6					1	3				
		Strong chl			Bill WQ	75	100	3094	223.2	226.2	1.8	0.2	14	0.1	0.1						7	14			
					Bill Qtz	75	75	3095	226.2	229.2	1.6	tr	15	tr	tr						6	12			





**APPENDIX 3**

1995 Drill Assay Tables

DDH 1217 ASSAY TABLE												
From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w%a)	Ag (w%a)	Cu(w%a)	Mo(w%a)	
12.2	14.3	2251	2.1	0.05	0.8	288	22	0.105	1.68	604.8	46.2	
14.3	17.4	2252	3.1	0.07	1.0	281	24	0.217	3.1	871.1	74.4	
17.4	20.4	2253	3.0	0.04	1.0	264	18	0.12	3	792	54	
20.4	23.5	2254	3.1	0.04	0.9	290	18	0.124	2.79	899	55.8	
23.5	26.9	2255	3.4	0.06	1.0	408	35	0.204	3.4	1387.2	119	
26.9	29.3	2256	2.4	0.05	0.9	309	65	0.12	2.16	741.6	156	
29.3	32.6	2257	3.3	0.06	1.1	348	19	0.198	3.63	1148.4	62.7	
32.6	35.7	2258	3.1	0.05	1.4	440	58	0.155	4.34	1364	179.8	
35.7	38.7	2259	3.0	0.15	2.2	390	22	0.45	6.6	1170	66	
38.7	41.0	2260	2.3	0.05	1.4	341	43	0.115	3.22	784.3	98.9	
41.0	41.9	2261	0.9	0.12	2.6	413	24	0.108	2.34	371.7	21.6	
41.9	44.8	2262	2.9	0.06	1.6	387	30	0.174	4.64	1122.3	87	
44.8	47.8	2263	3.0	0.06	1.7	385	42	0.18	5.1	1155	126	
47.8	50.9	2264	3.1	0.15	1.8	775	55	0.485	5.58	2402.5	170.5	
50.9	53.9	2265	3.0	0.28	3.3	1190	85	0.84	9.9	3570	255	
53.9	57.0	2266	3.1	0.23	3.8	972	120	0.713	11.78	3013.2	372	
57.0	60.0	2267	3.0	0.08	0.8	402	190	0.24	2.4	1206	570	
60.0	61.6	2268	1.6	0.05	0.6	412	102	0.08	0.96	659.2	163.2	
61.6	63.1	2269	1.5	0.26	2.7	2360	182	0.39	4.05	3540	273	
63.1	66.1	2270	3.0	0.44	2.4	3590	118	1.32	7.2	10770	354	
66.1	69.2	2271	3.1	0.32	2.2	2190	124	0.992	6.82	6789	384.4	
69.2	72.2	2272	3.0	0.34	3.0	2570	80	1.02	9	7710	240	
72.2	75.3	2273	3.1	0.65	3.8	4180	128	2.015	11.78	12958	396.8	
75.3	78.3	2274	3.0	0.73	4.0	3450	40	2.19	12	10350	120	
78.3	81.4	2275	3.1	0.95	6.2	5800	40	2.945	19.22	17980	124	
81.4	84.4	2276	3.0	0.88	6.9	4260	33	2.64	20.7	12780	99	
84.4	87.5	2277	3.1	0.93	10.9	5710	42	2.883	33.79	17701	130.2	
87.5	90.5	2278	3.0	0.58	2.7	3290	13	1.74	8.1	9870	39	
90.5	93.6	2279	3.1	0.60	2.2	2520	5	1.86	6.82	7812	15.5	
93.6	96.6	2280	3.0	0.42	2.2	2430	73	1.26	6.6	7290	219	
96.6	99.7	2281	3.1	0.33	2.0	1550	8	1.023	6.2	4805	24.8	
99.7	102.7	2282	3.0	0.19	1.8	2470	50	0.57	5.4	7410	150	
102.7	104.4	2283	1.7	0.50	1.4	2480	18	0.85	2.38	4216	30.6	
104.4	105.4	2284	1.0	0.63	2.2	1440	12	0.63	2.2	1440	12	
105.4	107.7	2285	2.3	0.32	1.0	1420	6	0.736	2.3	3266	13.8	
107.7	110.2	2286	2.5	0.35	1.2	1245	8	0.875	3	3112.5	20	
110.2	111.5	2287	1.3	0.51	1.6	1919	11	0.663	2.08	2494.7	14.3	
111.5	114.0	2288	2.5	0.25	1.2	855	9	0.625	3	2137.5	22.5	
114.0	115.7	2289	1.7	0.42	1.6	2800	10	0.714	2.72	4760	17	

## CT1217.XLS

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w'a)	Ag (w'a)	Cu(w'a)	Mo(w'a)
115.7	117.9	2290	2.2	0.76	1.8	3800	10	1.672	3.96	8360	22
117.9	119.9	2291	2.0	0.56	1.2	2200	10	1.12	2.4	4400	20
119.9	122.2	2292	2.3	0.78	2.1	3000	10	1.794	4.83	6900	23
122.2	124.0	2293	1.8	0.33	0.6	1700	10	0.594	1.08	3060	18
124.0	127.1	2294	3.1	0.36	0.6	1000	10	1.116	1.86	3100	31
127.1	130.1	2295	3.0	1.50	1.6	1000	10	4.5	4.8	3000	30
130.1	133.2	2296	3.1	0.36	1.4	1300	10	1.116	4.34	4030	31
133.2	136.2	2297	3.0	0.62	2.4	3600	10	1.86	7.2	10800	30
136.2	139.3	2298	3.1	0.76	2.3	2900	10	2.356	7.13	8990	31
139.3	142.3	2299	3.0	0.33	0.8	1000	10	0.99	2.4	3000	30
142.3	145.4	2300	3.1	1.60	2.0	2100	10	4.96	6.2	6510	31
145.4	148.4	2301	3.0	0.18	0.7	800	10	0.54	2.1	2400	30
148.4	151.5	2302	3.1	0.30	0.8	1000	20	0.93	2.48	3100	62
151.5	154.5	2303	3.0	0.22	1.0	1000	10	0.66	3	3000	30
154.5	157.6	2304	3.1	0.33	1.6	800	10	1.023	4.96	2480	31
157.6	160.6	2305	3.0	0.22	1.0	600	10	0.66	3	1800	30
160.6	163.7	2306	3.1	0.18	1.0	800	10	0.558	3.1	2480	31
163.7	165.2	2307	1.5	0.13	0.5	400	10	0.195	0.75	600	15
165.2	166.7	99999	1.5	0.00	0.0	0	0	0	0	0	0
166.7	170.6	2308	3.9	0.35	2.0	2400	10	1.365	7.8	9360	39
170.6	173.1	99999	2.5	0.00	0.0	0	0	0	0	0	0
173.1	175.9	2309	2.8	2.10	3.2	3400	20	5.88	8.96	9520	56
175.9	178.9	2310	3.0	0.24	0.8	800	10	0.72	2.4	2400	30
178.9	182.0	2311	3.1	0.31	1.6	1400	10	0.961	4.96	4340	31
182.0	185.0	2312	3.0	0.37	1.5	1800	10	1.11	4.5	5400	30
185.0	188.0	2313	3.0	0.21	0.9	600	10	0.63	2.7	1800	30
188.0	190.0	2314	2.0	0.18	1.0	200	10	0.36	2	400	20
190.0	190.6	2315	0.6	1.40	16.8	900	10	0.84	10.08	540	6
190.6	194.2	2316	3.6	0.33	2.0	1600	10	1.188	7.2	5760	36
194.2	196.3	2317	2.1	1.42	4.8	3000	10	2.982	10.08	6300	21
196.3	197.3	2318	1.0	0.70	13.8	11000	10	0.7	13.8	11000	10
197.3	199.3	2319	2.0	0.93	6.0	3600	10	1.86	12	7200	20
199.3	202.1	2320	2.8	2.50	18.0	7600	10	7	50.4	21280	28
202.1	203.3	2321	1.2	1.58	10.4	8200	10	1.896	12.48	9840	12
203.3	205.4	2322	2.1	0.58	2.8	2200	30	1.218	5.88	4620	63
205.4	206.3	2323	0.9	1.09	5.8	3600	80	0.981	5.22	3240	72
206.3	209.4	2324	3.1	1.40	12.8	5200	120	4.34	39.68	16120	372
209.4	212.4	2325	3.0	1.05	8.0	2600	140	3.15	24	7800	420
212.4	215.5	2326	3.1	0.51	1.8	1900	60	1.581	5.58	5890	186
215.5	217.9	2327	2.4	1.48	3.8	3800	50	3.552	9.12	9120	120

## CT1217.XLS

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w'a)	Ag (w'a)	Cu(w'a)	Mo(w'a)
217.9	218.5	99999	0.6	0.00	0.0	0	0	0	0	0	0
218.5	221.6	2328	3.1	0.20	1.4	800	20	0.62	4.34	2480	62
221.6	224.6	2329	3.0	0.33	2.8	700	14	0.99	8.4	2100	42
224.6	227.0	2330	2.4	0.18	1.6	500	9	0.432	3.84	1200	21.6
227.0	230.0	2331	3.0	0.07	0.4	300	9	0.21	1.2	900	27
230.0	233.0	2332	3.0	0.17	1.2	800	10	0.51	3.6	2400	30
233.0	236.0	2333	3.0	0.22	1.6	800	7	0.66	4.8	2400	21
236.0	239.0	2334	3.0	0.32	2.0	1500	17	0.96	6	4500	51
239.0	242.0	2335	3.0	0.30	0.8	600	12	0.9	2.4	1800	36
242.0	245.0	2336	3.0	0.13	1.0	700	22	0.39	3	2100	66
245.0	248.0	2337	3.0	0.16	0.8	600	23	0.48	2.4	1800	69
248.0	251.0	2338	3.0	0.08	0.4	300	38	0.24	1.2	900	114
251.0	254.0	2339	3.0	0.11	0.6	500	38	0.33	1.8	1500	114
254.0	257.0	2340	3.0	0.10	0.6	800	12	0.3	1.8	2400	36
257.0	260.0	2341	3.0	0.31	1.5	800	30	0.93	4.5	2400	90
260.0	263.0	2342	3.0	0.11	0.5	400	14	0.33	1.5	1200	42
263.0	266.0	2343	3.0	0.17	1.0	800	25	0.51	3	2400	75
266.0	269.0	2344	3.0	0.32	1.8	1600	18	0.96	5.4	4800	54
269.0	272.0	2345	3.0	0.42	1.0	1000	32	1.26	3	3000	96
272.0	275.0	2346	3.0	0.22	0.8	1000	14	0.66	2.4	3000	42
275.0	278.0	2347	3.0	0.29	1.4	1100	23	0.87	4.2	3300	69
278.0	281.0	2348	3.0	0.33	0.6	600	16	0.99	1.8	1800	48
281.0	284.0	2349	3.0	0.18	0.9	800	22	0.54	2.7	2400	66
284.0	287.0	2350	3.0	0.07	0.6	400	14	0.21	1.8	1200	42
287.0	290.0	2351	3.0	0.08	0.4	300	34	0.24	1.2	900	102
290.0	293.0	2352	3.0	0.43	1.4	1000	27	1.29	4.2	3000	81
293.0	296.0	2353	3.0	0.18	1.2	800	66	0.54	3.6	2400	198
296.0	299.0	2354	3.0	0.23	1.0	1000	26	0.69	3	3000	78
299.0	302.0	2355	3.0	0.05	0.6	400	16	0.15	1.8	1200	48
302.0	305.0	2356	3.0	0.17	1.0	600	28	0.51	3	1800	84
305.0	308.0	2357	3.0	0.15	1.0	600	16	0.45	3	1800	48
308.0	311.0	2358	3.0	0.30	1.6	1200	14	0.9	4.8	3600	42
311.0	314.0	2359	3.0	0.31	1.2	1100	15	0.93	3.6	3300	45
314.0	317.0	2360	3.0	0.09	0.7	600	19	0.27	2.1	1800	57
317.0	320.0	2361	3.0	0.32	1.2	1200	24	0.96	3.6	3600	72
320.0	322.9	2362	2.9	0.37	1.6	1400	40	1.073	4.64	4060	116
322.9	324.7	2363	1.8	0.01	0.3	100	3	0.018	0.54	180	5.4
324.7	328.0	2364	3.3	0.20	1.0	1000	18	0.66	3.3	3300	59.4
328.0	331.0	2365	3.0	0.14	0.8	400	20	0.42	2.4	1200	60
331.0	334.0	2366	3.0	0.25	2.0	1000	35	0.75	6	3000	105

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w%a)	Ag (w%a)	Cu(w%a)	Mo(w%a)
334.0	337.0	2367	3.0	0.22	1.8	800	30	0.66	5.4	2400	90
337.0	340.0	2368	3.0	0.10	0.4	200	9	0.3	1.2	600	27
340.0	343.0	2369	3.0	0.08	0.3	400	38	0.24	0.9	1200	114
343.0	346.0	2370	3.0	0.05	0.4	200	14	0.15	1.2	600	42
346.0	349.3	2371	3.3	0.29	1.9	100	52	0.957	6.27	330	171.6
349.3	352.0	2372	2.7	0.08	0.6	300	4	0.216	1.62	810	10.8
352.0	355.0	2373	3.0	0.06	0.2	200	5	0.18	0.6	600	15
355.0	358.0	2374	3.0	1.34	5.2	4400	12	4.02	15.6	13200	36
358.0	361.0	2375	3.0	0.17	1.0	600	10	0.51	3	1800	30
361.0	364.0	2376	3.0	0.27	1.0	700	14	0.81	3	2100	42
364.0	367.1	2377	3.1	0.15	1.0	500	6	0.465	3.1	1550	18.6
367.1	368.3	2378	1.2	0.20	0.6	500	26	0.24	0.72	600	31.2
368.3	369.0	2451	0.7	0.38	3.4	3000	30	0.266	2.38	2100	21
369.0	370.1	2452	1.1	4.20	8.6	12500	52	4.62	9.46	13750	57.2
370.1	371.5	2453	1.4	1.11	6.2	7200	140	1.554	8.68	10080	196
371.5	373.9	2454	2.4	2.50	10.3	12200	122	6	24.72	29280	292.8
373.9	375.4	2455	1.5	0.98	4.8	5000	50	1.47	7.2	7500	75
375.4	378.0	2379	2.6	0.22	0.8	400	6	0.572	2.08	1040	15.6
378.0	381.0	2380	3.0	0.22	0.8	400	6	0.66	2.4	1200	18
381.0	384.0	2381	3.0	0.44	1.2	1500	48	1.32	3.6	4500	144
384.0	387.0	2382	3.0	0.14	0.4	500	10	0.42	1.2	1500	30
387.0	390.0	2383	3.0	0.39	1.0	400	8	1.17	3	1200	24
390.0	393.0	2384	3.0	0.15	0.2	200	12	0.45	0.6	600	36
393.0	396.0	2385	3.0	0.13	0.4	600	10	0.39	1.2	1800	30
396.0	399.0	2386	3.0	0.17	0.4	600	30	0.51	1.2	1800	90
399.0	402.0	2387	3.0	0.66	2.2	4600	13	1.98	6.6	13800	39
402.0	405.0	2388	3.0	0.82	1.8	3200	13	2.46	5.4	9600	39
405.0	408.0	2389	3.0	0.32	0.6	1000	24	0.96	1.8	3000	72
408.0	411.0	2390	3.0	0.23	0.5	1100	19	0.69	1.5	3300	57
411.0	414.0	2391	3.0	0.11	0.7	800	10	0.33	2.1	2400	30
414.0	417.0	2392	3.0	0.42	2.2	3000	22	1.26	6.6	9000	66
417.0	420.0	2393	3.0	0.49	2.2	3300	8	1.47	6.6	9900	24
420.0	423.4	2394	3.4	0.24	1.6	2400	18	0.816	5.44	8160	61.2

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
<b>12.2 m - 61.6 m</b>											
Total (w*a)			49.4	4.61	76.6	23262	2678				
Mean				0.09	1.6	471	54				
<b>61.6 m - 145.4 m</b>											
Total (w*a)			83.8	50.02	221.6	221342	2997				
Mean				0.60	2.6	2641	36				
<b>145.4 m - 190.6 m</b>											
Total (w*a)			45.2	16.43	62.8	49620	471				
Mean				0.36	1.4	1098	10				
<b>190.6 m - 217.9 m</b>											
Total (w*a)			27.3	30.45	195.4	108170	1360				
Mean				1.12	7.2	3962	50				
<b>217.9 m - 368.3 m</b>											
Total (w*a)			150.4	32.88	168.5	115910	3143				
Mean				0.22	1.1	771	21				
<b>368.3 m - 375.4 m</b>											
Total (w*a)			7.1	13.91	52.4	62710	642				
Mean				1.96	7.4	8832	90				
<b>375.4 m - 399.0 m</b>											
Total (w*a)			23.6	5.49	15.3	13640	388				
Mean				0.23	0.6	578	16				
<b>399.0 m - 423.4 m</b>											
Total (w*a)			24.4	9.97	36.0	59160	388				
Mean				0.41	1.5	2425	16				
<b>12.2 m - 423.4 m</b>											
Total (w*a)			411.2	163.76	828.6	653814	12066				
Mean				0.40	2.0	1590	29				

DDH 1218 ASSAY TABLE												
From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)	
3.0	7.0	2501	4.0	1.18	4.5	3360	19	4.72	18	13440	76	
7.0	10.0	2502	3.0	0.76	4.9	3410	32	2.28	14.7	10230	96	
10.0	12.1	2503	2.1	1.68	7.4	3690	15	3.528	15.54	7749	31.5	
12.1	14.2	2504	2.1	0.34	1.9	1050	23	0.714	3.99	2205	48.3	
14.2	16.2	2505	2.0	0.24	2.2	1260	14	0.48	4.4	2520	28	
16.2	19.2	2506	3.0	0.23	2.4	1150	14	0.69	7.2	3450	42	
19.2	21.4	2507	2.2	0.32	2.5	1890	8	0.704	5.5	4158	17.6	
21.4	24.1	2508	2.7	0.89	5.1	1720	20	2.403	13.77	4644	54	
24.1	25.6	2509	1.5	0.78	20.2	2250	48	1.17	30.3	3375	72	
25.6	28.3	2510	2.7	0.63	3.4	1960	21	1.701	9.18	5292	56.7	
28.3	31.4	2511	3.1	0.62	3.6	2660	54	1.922	11.16	8246	167.4	
31.4	34.5	2512	3.1	0.61	3.3	1560	26	1.891	10.23	4836	80.6	
34.5	37.5	2513	3.0	0.98	5.6	2220	76	2.94	16.8	6660	228	
37.5	40.5	2514	3.0	1.05	3.6	1680	94	3.15	10.8	5040	282	
40.5	43.6	2515	3.1	1.04	4.6	2280	218	3.224	14.26	7068	675.8	
43.6	46.6	2516	3.0	0.35	2.8	1560	16	1.05	8.4	4680	48	
46.6	49.7	2517	3.1	1.36	3.7	950	40	4.216	11.47	2945	124	
49.7	52.7	2518	3.0	1.40	3.4	1450	130	4.2	10.2	4350	390	
52.7	55.8	2519	3.1	0.51	3.3	1810	65	1.581	10.23	5611	201.5	
55.8	58.4	2520	2.6	0.28	2.4	1920	27	0.728	6.24	4992	70.2	
58.4	61.3	2521	2.9	0.59	5.4	1430	38	1.711	15.66	4147	110.2	
61.3	63.4	2522	2.1	0.25	1.8	1730	9	0.525	3.78	3633	18.9	
63.4	65.1	2523	1.7	0.26	1.3	1690	17	0.442	2.21	2873	28.9	
65.1	68.3	2524	3.2	0.44	3.8	2680	22	1.408	12.16	8576	70.4	
68.3	71.0	2525	2.7	0.99	6.9	4500	27	2.673	18.63	12150	72.9	
71.0	74.1	2526	3.1	0.69	11.4	4820	12	2.139	35.34	14942	37.2	
74.1	77.1	2527	3.0	0.51	2.5	2290	32	1.53	7.5	6870	96	
77.1	80.2	2528	3.1	0.33	1.2	1640	16	1.023	3.72	5084	49.6	
80.2	83.2	2529	3.0	0.83	3.6	3100	22	2.49	10.8	9300	66	
83.2	86.3	2530	3.1	0.29	1.2	1600	8	0.899	3.72	4960	24.8	
86.3	89.3	2531	3.0	1.58	6.0	4810	56	4.74	18	14430	168	
89.3	91.4	2532	2.1	1.24	7.6	6840	48	2.604	15.96	14364	100.8	
91.4	92.4	2533	1.0	0.67	2.8	2840	38	0.67	2.8	2840	38	
92.4	95.4	2534	3.0	0.28	1.2	1400	9	0.84	3.6	4200	27	
95.4	98.5	2535	3.1	0.52	1.9	2280	21	1.612	5.89	7068	65.1	
98.5	101.1	2536	2.6	0.45	1.1	1410	11	1.17	2.86	3666	28.6	
101.1	104.5	2537	3.4	1.56	7.0	5450	26	5.304	23.8	18530	88.4	
104.5	107.6	2538	3.1	1.76	7.2	8060	93	5.456	22.32	24986	288.3	
107.6	110.6	2539	3.0	0.60	4.1	3000	136	1.8	12.3	9000	408	



## CT1218.XLS

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w'a)	Ag (w'a)	Cu(w'a)	Mo(w'a)
110.6	113.1	2540	2.5	0.91	4.5	4360	10	2.275	11.25	10900	25
113.1	115.9	2541	2.8	0.28	1.0	2070	18	0.784	2.8	5796	50.4
115.9	118.7	2542	2.8	0.87	4.5	1580	38	2.436	12.6	4424	106.4
118.7	121.5	2543	2.8	0.30	1.0	2450	44	0.84	2.8	6860	123.2
121.5	122.8	2544	1.3	0.60	4.6	8120	104	0.78	5.98	10556	135.2
122.8	125.9	2545	3.1	0.58	1.4	1640	30	1.798	4.34	5084	93
125.9	128.9	2546	3.0	0.87	4.5	3270	16	2.61	13.5	9810	48
128.9	131.8	2547	2.9	0.35	2.5	1950	12	1.015	7.25	5655	34.8
131.8	132.7	99999	0.9	0.00	0.0	0	0	0	0	0	0
132.7	135.0	2548	2.3	0.23	0.6	930	12	0.529	1.38	2139	27.6
135.0	138.1	2549	3.1	0.15	0.5	545	8	0.465	1.55	1689.5	24.8
138.1	139.8	2550	1.7	0.71	3.8	3500	12	1.207	6.46	5950	20.4
139.8	141.6	2551	1.8	0.54	2.7	2520	11	0.972	4.86	4536	19.8
141.6	144.2	2552	2.6	0.68	2.8	2630	16	1.768	7.28	6838	41.6
144.2	146.4	2553	2.2	0.35	1.6	1670	6	0.77	3.52	3674	13.2
146.4	149.3	2554	2.9	0.13	1.0	620	9	0.377	2.9	1798	26.1
149.3	152.4	2555	3.1	0.10	0.8	575	11	0.31	2.48	1782.5	34.1
152.4	155.1	2556	2.7	0.34	2.0	920	13	0.918	5.4	2484	35.1
155.1	156.4	2557	1.3	0.29	2.6	1330	10	0.377	3.38	1729	13
156.4	159.4	2558	3.0	0.29	2.6	1170	14	0.87	7.8	3510	42
159.4	162.5	2559	3.1	0.39	4.0	1940	12	1.209	12.4	6014	37.2
162.5	165.5	2560	3.0	0.11	1.2	455	14	0.33	3.6	1365	42
165.5	168.6	2561	3.1	0.08	1.2	422	7	0.248	3.72	1308.2	21.7
168.6	171.6	2562	3.0	0.09	0.8	418	10	0.27	2.4	1254	30
171.6	173.8	2563	2.2	0.27	1.8	1106	9	0.594	3.96	2433.2	19.8
173.8	176.1	2564	2.3	1.71	10.6	6700	22	3.933	24.38	15410	50.6
176.1	179.5	2565	3.4	0.29	3.4	1820	10	0.986	11.58	6188	34
179.5	182.4	2566	2.9	0.28	2.9	1540	9	0.812	8.41	4466	26.1
182.4	184.0	2567	1.6	1.56	10.4	8000	9	2.496	16.64	12800	14.4
184.0	185.3	2568	1.3	1.67	7.5	6800	8	2.171	9.75	8840	10.4
185.3	187.6	2569	2.3	2.40	10.5	9100	15	5.52	24.15	20930	34.5
187.6	189.9	2570	2.3	0.44	2.9	2300	5	1.012	6.67	5290	11.5
189.9	192.9	2571	3.0	0.54	1.2	910	5	1.62	3.6	2730	15
192.9	194.1	2572	1.2	0.33	1.4	1310	4	0.396	1.68	1572	4.8
194.1	196.6	2573	2.5	0.30	1.4	895	7	0.75	3.5	2237.5	17.5
196.6	199.0	2574	2.4	0.77	5.4	4270	17	1.848	12.96	10248	40.8
199.0	200.9	2575	1.9	0.18	1.5	2040	4	0.342	2.85	3876	7.6
200.9	202.4	2576	1.5	0.19	0.6	710	16	0.285	0.9	1065	24
202.4	204.3	2577	1.9	0.25	1.9	1735	15	0.475	3.61	3296.5	28.5
204.3	208.1	2578	3.8	0.24	1.4	1200	200	0.912	5.32	4560	760

## CT1218.XLS

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w'a)	Ag (w'a)	Cu(w'a)	Mo(w'a)
208.1	211.1	2579	3.0	0.26	1.8	1100	12	0.78	5.4	3300	36
211.1	214.0	2580	2.9	0.40	2.4	2500	24	1.16	6.96	7250	69.6
214.0	217.0	2581	3.0	0.51	2.0	3000	14	1.53	6	9000	42
217.0	220.0	2582	3.0	0.36	1.1	1000	9	1.08	3.3	3000	27
220.0	223.0	2583	3.0	0.25	1.2	800	9	0.75	3.6	2400	27
223.0	226.0	2584	3.0	0.42	3.8	3800	14	1.26	11.4	11400	42
226.0	229.0	2585	3.0	0.30	2.0	2000	12	0.9	6	6000	36
229.0	232.0	2586	3.0	0.58	2.6	3000	12	1.74	7.8	9000	36
232.0	235.0	2587	3.0	0.11	1.1	1000	12	0.33	3.3	3000	36
235.0	238.0	2588	3.0	0.27	1.8	1400	12	0.81	5.4	4200	36
238.0	241.0	2589	3.0	0.43	2.2	1400	6	1.29	6.6	4200	18
241.0	244.0	2590	3.0	0.32	25.0	1800	68	0.96	75	5400	204
244.0	247.0	2591	3.0	0.30	6.8	3600	8	0.9	20.4	10800	24
247.0	250.0	2592	3.0	0.16	3.6	2400	6	0.48	10.8	7200	18
250.0	253.0	2593	3.0	0.25	1.4	2000	38	0.75	4.2	6000	114
253.0	256.0	2594	3.0	0.35	4.5	2000	20	1.05	13.5	6000	60
256.0	259.0	2595	3.0	0.38	9.0	1900	12	1.14	27	5700	36
259.0	262.0	2596	3.0	0.29	2.4	900	6	0.87	7.2	2700	18
262.0	265.0	2597	3.0	0.20	2.6	2400	18	0.6	7.8	7200	54
265.0	268.0	2598	3.0	0.42	3.8	2200	10	1.26	11.4	6600	30
268.0	271.0	2599	3.0	0.26	2.4	1600	10	0.78	7.2	4800	30
271.0	274.0	2600	3.0	0.16	2.2	1400	6	0.48	6.6	4200	18
274.0	277.0	2601	3.0	0.19	1.4	600	5	0.57	4.2	1800	15
277.0	280.0	2602	3.0	0.25	1.8	1000	11	0.75	5.4	3000	33
280.0	283.0	2603	3.0	0.45	3.4	2000	9	1.35	10.2	6000	27
283.0	286.0	2604	3.0	0.31	2.2	1500	6	0.93	6.6	4500	18
286.0	290.0	2605	4.0	0.24	2.5	1000	18	0.96	10	4000	72
290.0	291.5	2606	1.5	0.12	1.6	1200	12	0.18	2.4	1800	18
291.5	294.0	2607	2.5	0.07	1.2	800	6	0.175	3	2000	15
294.0	297.0	2608	3.0	0.14	1.4	1000	6	0.42	4.2	3000	18
297.0	300.0	2609	3.0	0.11	1.4	1200	5	0.33	4.2	3600	15
300.0	303.0	2610	3.0	0.14	1.8	800	10	0.42	5.4	2400	30
303.0	306.0	2611	3.0	0.74	12.0	3500	16	2.22	36	10500	48
306.0	309.0	2612	3.0	0.15	2.4	1600	14	0.45	7.2	4800	42
309.0	312.0	2613	3.0	0.56	3.0	2000	8	1.68	9	6000	24
312.0	315.0	2614	3.0	0.70	6.0	3600	12	2.1	18	10800	36
315.0	318.0	2615	3.0	0.38	2.6	2600	10	1.14	7.8	7800	30
318.0	321.0	2616	3.0	0.23	2.1	1500	10	0.69	6.3	4500	30
321.0	324.0	2617	3.0	0.33	3.2	1500	22	0.99	9.6	4500	66
324.0	327.0	2618	3.0	0.32	9.6	3600	14	0.96	28.8	10800	42

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w'a)	Ag (w'a)	Cu(w'a)	Mo(w'a)
327.0	330.0	2619	3.0	0.15	1.0	1200	110	0.45	3	3600	330
330.0	333.0	2620	3.0	0.22	0.4	900	8	0.66	1.2	2700	24
333.0	336.0	2621	3.0	0.08	3.2	1400	12	0.24	9.6	4200	36
336.0	339.0	2622	3.0	0.06	1.4	900	10	0.18	4.2	2700	30
339.0	342.0	2623	3.0	0.23	1.0	2800	16	0.69	3	8400	48
342.0	345.0	2624	3.0	0.20	1.4	4000	30	0.6	4.2	12000	90
345.0	348.0	2625	3.0	0.33	1.6	1000	26	0.99	4.8	3000	78
348.0	351.0	2626	3.0	0.12	0.9	600	12	0.36	2.7	1800	36
351.0	354.0	2627	3.0	0.16	2.0	1400	14	0.48	6	4200	42
354.0	357.0	2628	3.0	0.17	1.1	800	34	0.51	3.3	2400	102
357.0	360.0	2629	3.0	0.15	0.6	1000	9	0.45	1.8	3000	27
360.0	363.0	2630	3.0	0.40	0.9	1800	7	1.2	2.7	5400	21
363.0	366.0	2631	3.0	0.22	0.8	1200	8	0.66	2.4	3600	24
366.0	369.0	2632	3.0	0.08	0.3	400	10	0.24	0.9	1200	30
369.0	372.0	2633	3.0	0.05	0.2	600	18	0.15	0.6	1800	54
372.0	375.0	2634	3.0	0.09	1.2	400	9	0.27	3.6	1200	27
375.0	378.0	2635	3.0	0.15	0.4	800	15	0.45	1.2	2400	45
378.0	381.0	2636	3.0	0.07	0.3	800	6	0.21	0.9	2400	18
381.0	384.0	2637	3.0	0.08	0.6	600	11	0.24	1.8	1800	33
384.0	387.0	2638	3.0	0.12	0.4	800	18	0.36	1.2	2400	54
387.0	390.0	2639	3.0	0.25	0.3	800	6	0.75	0.9	2400	18
390.0	391.4	2640	1.4	0.09	0.2	600	12	0.126	0.28	840	16.8
391.4	394.1	2641	2.7	0.13	0.8	600	6	0.351	2.16	1620	16.2
394.1	396.6	2642	2.5	0.08	0.4	600	6	0.2	1	1500	15
396.6	400.0	2643	3.4	0.05	0.3	400	6	0.17	1.02	1360	20.4
400.0	404.0	2644	4.0	0.02	0.3	400	8	0.08	1.2	1600	32
404.0	408.1	2645	4.1	0.01	0.2	300	8	0.041	0.82	1230	32.8

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w'a)	Ag (w'a)	Cu(w'a)	Mo(w'a)
<b>3.0 m - 131.8 m</b>											
Total (w'a)			128.8	94.87	513.9	342195	5193				
Mean				0.74	4.0	2657	40				
<b>131.8 m - 173.8 m</b>											
Total (w'a)			42.0	11.21	73.1	48504	448				
Mean				0.27	1.7	1155	11				
<b>173.8 m - 199.0 m</b>											
Total (w'a)			25.2	21.54	123.3	90711	260				
Mean				0.85	4.9	3600	10				
<b>199.0 m - 366.0 m</b>											
Total (w'a)			167.0	46.70	496.7	290948	3299				
Mean				0.28	3.0	1742	20				
<b>366.0 m - 408.1 m</b>											
Total (w'a)			42.1	3.64	17.6	23750	412				
Mean				0.09	0.4	564	10				
<b>3.0 m - 366.0 m</b>											
Total (w'a)			363.0	174.32	1207.1	772358	9199				
Mean				0.48	3.3	2128	25				
<b>3.0 m - 408.1 m</b>											
Total (w'a)			405.1	177.96	1224.7	796108	9612				
Mean				0.44	3.0	1965	24				

DDH 1219 ASSAY TABLE												
From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w'a)	Ag (w'a)	Cu(w'a)	Mo(w'a)	
24.1	27.1	2469	3.0	0.17	7.0	760	32	0.51	21	2280	96	
27.1	30.1	2470	3.0	0.13	2.4	848	58	0.39	7.2	2544	174	
30.1	33.1	2471	3.0	0.27	5.6	1260	48	0.81	16.8	3780	144	
33.1	36.1	2472	3.0	0.15	1.6	800	30	0.45	4.8	2400	90	
36.1	39.1	2473	3.0	0.24	1.8	2280	200	0.72	5.4	6840	600	
39.1	42.1	2474	3.0	0.11	1.0	730	90	0.33	3	2190	270	
42.1	45.1	2475	3.0	0.07	0.8	680	68	0.21	2.4	2040	204	
45.1	48.1	2476	3.0	0.09	0.6	810	118	0.27	1.8	2430	354	
48.1	51.1	2477	3.0	0.08	0.5	668	142	0.24	1.5	2004	426	
51.1	54.1	2478	3.0	0.45	3.7	5060	74	1.35	11.1	15180	222	
54.1	57.1	2479	3.0	0.50	6.4	3460	122	1.5	19.2	10380	366	
57.1	60.1	2480	3.0	0.65	5.6	3550	142	1.95	16.8	10650	426	
60.1	63.1	2481	3.0	0.31	2.4	1480	122	0.93	7.2	4440	366	
63.1	66.1	2482	3.0	0.18	1.4	1440	124	0.54	4.2	4320	372	
66.1	69.1	2483	3.0	0.15	1.0	1150	90	0.45	3	3450	270	
69.1	72.1	2484	3.0	0.24	1.4	1860	98	0.72	4.2	5580	294	
72.1	75.1	2485	3.0	0.22	1.6	1610	130	0.66	4.8	4830	390	
75.1	78.1	2486	3.0	0.66	3.6	3320	136	1.98	10.8	9960	408	
78.1	81.1	2487	3.0	0.06	0.8	170	12	0.18	2.4	510	36	
81.1	84.1	2488	3.0	0.58	2.0	3100	112	1.74	6	9300	336	
84.1	87.1	2489	3.0	0.36	2.2	1810	68	1.08	6.6	5430	204	
87.1	90.1	2490	3.0	0.48	2.6	1900	264	1.44	7.8	5700	792	
90.1	93.3	2491	3.2	0.38	2.2	1540	50	1.216	7.04	4928	160	
93.3	96.3	2492	3.0	1.10	5.0	5300	70	3.3	15	15900	210	
96.3	99.4	2493	3.1	0.92	5.6	5700	240	2.852	17.36	17670	744	
99.4	102.4	2494	3.0	0.41	2.6	1650	75	1.23	7.8	4950	225	
102.4	105.5	2495	3.1	0.52	2.8	1980	80	1.612	8.68	6138	248	
105.5	108.5	2496	3.0	0.38	2.9	2230	60	1.14	8.7	6690	180	
108.5	111.6	2497	3.1	0.23	2.4	1540	90	0.713	7.44	4774	279	
111.6	114.6	2498	3.0	0.49	3.8	3050	100	1.47	11.4	9150	300	
114.6	117.7	2499	3.1	0.54	4.0	3150	80	1.674	12.4	9765	248	
117.7	120.7	2500	3.0	0.51	2.9	2330	126	1.53	8.7	6990	378	
120.7	123.7	2901	3.0	0.38	2.4	2240	54	1.14	7.2	6720	162	
123.7	126.8	2902	3.1	0.49	3.0	2960	132	1.519	9.3	9176	409.2	
126.8	129.8	2903	3.0	0.45	2.8	1930	62	1.35	8.4	5790	186	
129.8	132.9	2904	3.1	0.46	1.9	2100	24	1.426	5.89	6510	74.4	
132.9	135.9	2905	3.0	0.34	1.8	1690	79	1.02	5.4	5070	237	
135.9	139.0	2906	3.1	0.36	1.8	1900	45	1.116	5.58	5890	139.5	
139.0	142.0	2907	3.0	0.44	2.6	2100	26	1.32	7.8	6300	78	

## CT1219.XLS

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w'a)	Ag (w'a)	Cu(w'a)	Mo(w'a)
142.0	145.1	2908	3.1	0.71	1.8	1960	38	2.201	5.58	6076	117.8
145.1	148.1	2909	3.0	0.41	2.7	2630	310	1.23	8.1	7890	930
148.1	151.2	2910	3.1	0.49	1.4	2120	24	1.519	4.34	6572	74.4
151.2	154.2	2911	3.0	0.77	1.9	2400	264	2.31	5.7	7200	792
154.2	157.3	2912	3.1	0.30	1.2	1550	22	0.93	3.72	4805	68.2
157.3	160.3	2913	3.0	0.20	1.4	1180	20	0.6	4.2	3540	60
160.3	163.4	2914	3.1	0.29	2.0	1600	26	0.899	6.2	4960	80.6
163.4	166.4	2915	3.0	0.36	1.9	2360	54	1.08	5.7	7080	162
166.4	169.5	2916	3.1	0.26	2.6	1750	16	0.806	8.06	5425	49.6
169.5	172.5	2917	3.0	0.26	3.8	1570	22	0.78	11.4	4710	66
172.5	175.6	2918	3.1	0.60	10.0	1640	16	1.86	31	5084	49.6
175.6	178.6	2919	3.0	0.21	1.5	680	20	0.63	4.5	2040	60
178.6	181.7	2920	3.1	0.10	1.4	686	16	0.31	4.34	2126.6	49.6
181.7	183.8	2921	2.1	0.11	1.4	520	8	0.231	2.94	1092	16.8
183.8	184.9	2922	1.1	0.36	3.2	740	22	0.396	3.52	814	24.2
184.9	187.8	2923	2.9	0.17	1.2	850	20	0.493	3.48	2465	58
187.8	190.2	2924	2.4	0.11	1.2	440	12	0.264	2.88	1056	28.8
190.2	192.7	2925	2.5	0.18	1.7	930	16	0.45	4.25	2325	40
192.7	195.7	2926	3.0	0.17	2.6	980	20	0.51	7.8	2940	60
195.7	199.1	2927	3.4	0.35	2.8	1420	36	1.19	9.52	4828	122.4
199.1	199.5	2928	0.4	1.10	43.0	4280	10	0.473	18.49	1840.4	4.3
199.5	203.0	2929	3.5	0.29	4.5	710	19	1.0063	15.615	2463.7	65.93
203.0	205.7	2930	2.7	0.02	1.3	380	4	0.054	3.51	1026	10.8
205.7	208.7	2931	3.0	0.10	1.4	722	16	0.3	4.2	2166	48
208.7	211.7	2932	3.0	0.33	1.8	1430	14	0.99	5.4	4290	42
211.7	214.7	2933	3.0	0.25	1.7	1320	22	0.75	5.1	3960	66
214.7	216.5	2934	1.8	0.10	1.2	610	10	0.18	2.16	1098	18
216.5	218.3	2935	1.8	0.35	2.0	1800	52	0.63	3.6	3240	93.6
218.3	221.3	2936	3.0	0.10	1.0	490	10	0.3	3	1470	30
221.3	224.3	2937	3.0	0.16	1.4	820	14	0.48	4.2	2460	42
224.3	227.3	2938	3.0	0.15	1.8	850	10	0.45	5.4	2550	30
227.3	230.5	2939	3.2	0.12	1.4	590	14	0.384	4.48	1888	44.8
230.5	233.5	2940	3.0	0.14	1.6	880	16	0.42	4.8	2640	48
233.5	236.5	2941	3.0	0.13	1.4	780	12	0.39	4.2	2340	36
236.5	239.6	2942	3.1	0.66	5.4	2280	24	2.046	16.74	7068	74.4
239.6	242.6	2943	3.0	0.23	1.9	990	16	0.69	5.7	2970	48
242.6	245.7	2944	3.1	0.53	2.4	1750	14	1.643	7.44	5425	43.4
245.7	248.7	2945	3.0	0.31	3.2	1170	24	0.93	9.6	3510	72
248.7	251.9	2946	3.2	0.44	3.4	1230	13	1.408	10.88	3936	41.6
251.9	254.9	2947	3.0	0.27	1.3	1100	14	0.81	3.9	3300	42

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w'a)	Ag (w'a)	Cu(w'a)	Mo(w'a)
254.9	257.9	2948	3.0	0.15	0.9	830	14	0.45	2.7	2490	42
257.9	260.9	2949	3.0	0.32	1.3	1240	12	0.96	3.9	3720	36
260.9	263.9	2950	3.0	0.48	1.4	960	22	1.44	4.2	2880	66
263.9	267.0	2951	3.1	0.40	3.4	1360	12	1.24	10.54	4216	37.2
267.0	270.1	2952	3.1	0.29	2.4	810	26	0.899	7.44	2511	80.6
270.1	273.1	2953	3.0	0.18	1.2	510	10	0.54	3.6	1530	30
273.1	276.1	2954	3.0	0.12	0.5	520	21	0.36	1.5	1560	63
276.1	279.2	2955	3.1	0.21	4.8	1390	11	0.651	14.88	4309	34.1
279.2	282.2	2956	3.0	0.19	1.4	1000	9	0.57	4.2	3000	27
282.2	285.3	2957	3.1	0.38	3.0	2020	11	1.178	9.3	6262	34.1
285.3	288.3	2958	3.0	0.12	0.6	450	8	0.36	1.8	1350	24
288.3	291.4	2959	3.1	0.23	1.0	880	26	0.713	3.1	2728	80.6
291.4	294.4	2960	3.0	0.26	0.7	646	24	0.78	2.1	1938	72
294.4	297.5	2961	3.1	0.15	1.0	686	24	0.465	3.1	2126.6	74.4
297.5	299.9	2962	2.4	0.09	0.7	362	6	0.216	1.68	868.8	14.4
299.9	300.5	2963	0.6	0.64	54.0	10000	21	0.384	32.4	6000	12.6
300.5	303.6	2964	3.1	0.22	2.3	1140	76	0.682	7.13	3534	235.6
303.6	306.6	2965	3.0	0.11	0.8	410	18	0.33	2.4	1230	54
306.6	309.0	2966	2.4	0.10	1.2	400	6	0.24	2.88	960	14.4
309.0	311.7	2967	2.7	0.14	2.2	690	6	0.378	5.94	1863	16.2
311.7	315.4	2968	3.7	0.07	1.0	346	12	0.259	3.7	1280.2	44.4
315.4	318.0	2969	2.6	0.15	0.9	630	13	0.39	2.34	1638	33.8
318.0	321.0	2970	3.0	0.04	0.7	182	8	0.12	2.1	546	24
321.0	324.3	2971	3.3	0.09	0.8	410	48	0.297	2.64	1353	158.4
324.3	325.4	2972	1.1	0.01	0.3	30	8	0.011	0.33	33	8.8
325.4	327.3	2973	1.9	0.19	1.0	640	20	0.361	1.9	1216	38
327.3	330.3	2974	3.0	0.07	0.6	280	20	0.21	1.8	840	60
330.3	333.3	2975	3.0	0.08	0.6	210	12	0.24	1.8	630	36
333.3	336.4	2976	3.1	0.12	1.0	400	14	0.372	3.1	1240	43.4
336.4	339.4	2977	3.0	0.20	0.7	486	14	0.6	2.1	1458	42
339.4	342.4	2978	3.0	0.31	2.8	910	42	0.93	8.4	2730	126
342.4	345.4	2979	3.0	0.33	1.8	512	12	0.99	5.4	1536	36
345.4	348.4	2980	3.0	0.13	0.7	330	8	0.39	2.1	990	24
348.4	351.4	2981	3.0	0.17	0.8	476	24	0.51	2.4	1428	72
351.4	354.5	2982	3.1	0.14	0.8	330	10	0.434	2.48	1023	31
354.5	357.5	2983	3.0	0.20	0.8	570	32	0.6	2.4	1710	96
357.5	360.5	2984	3.0	0.13	0.4	410	9	0.39	1.2	1230	27
360.5	363.5	2985	3.0	0.50	1.2	1530	40	1.5	3.6	4590	120
363.5	366.5	2986	3.0	0.39	1.8	1130	10	1.17	5.4	3390	30
366.5	369.5	2987	3.0	0.22	1.4	1130	6	0.66	4.2	3390	18

## CT1219.XLS

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
369.5	372.5	2988	3.0	0.16	1.4	396	5	0.48	4.2	1188	15
372.5	375.7	2989	3.2	0.33	4.2	1350	8	1.056	13.44	4320	25.6
375.7	378.7	2990	3.0	0.19	1.2	1180	5	0.57	3.6	3540	15
378.7	381.7	2991	3.0	0.11	0.3	830	28	0.33	0.9	2490	84
381.7	383.7	2992	2.0	0.15	0.4	710	8	0.3	0.8	1420	16
383.7	386.7	2993	3.0	0.16	0.4	530	10	0.48	1.2	1590	30
386.7	390.0	2994	3.3	0.30	2.7	2900	4	0.99	8.91	9570	13.2
390.0	393.5	2995	3.5	0.33	0.3	920	14	1.155	1.05	3220	49
393.5	396.5	2996	3.0	0.17	2.8	530	8	0.51	8.4	1590	24
396.5	399.5	2997	3.0	0.10	0.6	400	12	0.3	1.8	1200	36
399.5	402.5	2998	3.0	0.14	0.8	610	14	0.42	2.4	1830	42
402.5	405.4	2999	2.9	0.22	1.4	886	30	0.638	4.06	2569.4	87
405.4	408.4	3000	3.0	0.42	6.0	966	16	1.26	18	2898	48
408.4	410.7	3001	2.3	0.16	1.8	280	10	0.368	4.14	644	23
410.7	413.7	3002	3.0	1.90	22.4	1910	12	5.7	67.2	5730	36
413.7	416.7	3003	3.0	0.35	5.4	530	24	1.05	16.2	1590	72
416.7	419.7	3004	3.0	0.08	1.4	310	16	0.24	4.2	930	48
419.7	422.7	3005	3.0	0.10	0.9	410	14	0.3	2.7	1230	42
422.7	425.7	3006	3.0	0.18	1.0	610	13	0.54	3	1830	39
425.7	428.7	3007	3.0	0.21	2.8	1400	76	0.63	8.4	4200	228
428.7	431.7	3008	3.0	0.18	1.2	740	16	0.54	3.6	2220	48
431.7	434.7	3009	3.0	0.17	0.8	596	10	0.51	2.4	1788	30
434.7	437.7	3010	3.0	0.19	0.7	476	9	0.57	2.1	1428	27
437.7	440.7	3011	3.0	0.32	1.0	750	36	0.96	3	2250	108
440.7	443.7	3012	3.0	0.31	1.7	980	42	0.93	5.1	2940	126
443.7	448.8	3013	5.1	0.20	1.0	750	58	1.02	5.1	3825	295.8
448.8	449.9	3014	1.1	0.23	0.6	760	68	0.253	0.66	836	74.8
449.9	452.9	3015	3.0	0.19	0.6	610	50	0.57	1.8	1830	150



From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w'a)	Ag (w'a)	Cu(w'a)	Mo(w'a)
<b>24.1m - 51.1m</b>											
Total (w'a)			27.0	3.93	63.9	26508	2358				
Mean				0.15	2.4	982	87				
<b>51.1 m - 175.6 m</b>											
Total (w'a)			124.5	54.36	352.2	285483	11190				
Mean				0.44	2.8	2293	90				
<b>175.6 m - 303.6 m</b>											
Total (w'a)			128.0	30.70	295.2	130351	2324				
Mean				0.24	2.3	1018	18				
<b>303.6 m - 360.5 m</b>											
Total (w'a)			56.9	8.05	57.4	24934	985				
Mean				0.14	1.0	438	17				
<b>360.5 m - 428.7 m</b>											
Total (w'a)			68.2	20.65	187.8	64949	1141				
Mean				0.30	2.8	952	17				
<b>428.7 m - 452.9 m</b>											
Total (w'a)			24.2	5.35	23.8	17117	860				
Mean				0.22	1.0	707	36				
<b>24.1 m - 303.6 m</b>											
Total (w'a)			279.5	88.99	711.3	442342	15873				
Mean				0.32	2.5	1583	57				
<b>24.1 m - 452.9 m</b>											
Total (w'a)			428.8	123.04	980.3	549343	18858				
Mean				0.29	2.3	1281	44				

DDH 1220 ASSAY TABLE											
From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
25.6	28.6	2747	3.0	0.40	1.4	2670	65	1.2	4.2	8010	195
28.6	31.8	2748	3.2	0.58	1.3	990	140	1.792	4.16	3168	448
31.8	34.8	2749	3.0	1.00	2.8	1900	158	3	8.4	5700	474
34.8	37.8	2750	3.0	0.90	2.2	3650	268	2.7	6.6	10950	804
37.8	41.1	2751	3.3	1.00	2.0	3000	92	3.3	6.6	9900	303.6
41.1	44.1	2752	3.0	0.47	1.8	2430	106	1.41	5.4	7290	318
44.1	47.1	2753	3.0	0.60	5.8	2500	120	1.8	17.4	7500	360
47.1	50.1	2754	3.0	0.64	1.6	2760	62	1.92	4.8	8280	186
50.1	53.1	2755	3.0	0.34	0.4	1910	89	1.02	1.2	5730	267
53.1	55.8	2756	2.7	0.36	0.4	1610	84	0.972	1.08	4347	226.8
55.8	58.8	2757	3.0	0.12	0.2	1080	79	0.36	0.6	3240	237
58.8	61.8	2758	3.0	0.43	2.0	2220	72	1.29	6	6660	216
61.8	64.8	2759	3.0	0.76	5.0	5400	72	2.28	15	16200	216
64.8	67.8	2760	3.0	0.61	1.4	3260	70	1.83	4.2	9780	210
67.8	70.7	2761	2.9	0.66	1.2	2780	70	1.914	3.48	8062	203
70.7	73.7	2762	3.0	0.68	1.5	3350	48	2.04	4.5	10050	144
73.7	76.6	2763	2.9	0.69	1.1	2560	71	2.001	3.19	7424	205.9
76.6	79.6	2764	3.0	0.26	3.1	2310	73	0.78	9.3	6930	219
79.6	80.5	2765	0.9	0.73	21.6	5900	36	0.657	19.44	5310	32.4
80.5	82.5	2766	2.0	0.54	3.2	3760	80	1.08	6.4	7520	160
82.5	85.5	2767	3.0	0.48	1.8	3600	43	1.44	4.8	10800	129
85.5	88.5	2768	3.0	0.73	2.6	4580	277	2.19	7.8	13740	831
88.5	90.6	2769	2.1	1.20	2.4	4720	313	2.52	5.04	9912	657.3
90.6	93.6	2770	3.0	0.45	1.6	3100	219	1.35	4.8	9300	657
93.6	96.6	2771	3.0	0.40	1.1	2460	112	1.2	3.3	7380	336
96.6	99.6	2772	3.0	0.37	1.4	2280	83	1.11	4.2	6840	249
99.6	102.6	2773	3.0	0.25	2.4	1900	292	0.75	7.2	5700	876
102.6	105.6	2774	3.0	0.31	1.2	1760	70	0.93	3.6	5280	210
105.6	107.7	2775	2.1	0.53	1.8	2020	76	1.113	3.78	4242	159.6
107.7	110.7	2776	3.0	0.39	2.4	2650	177	1.17	7.2	7950	531
110.7	113.7	2777	3.0	0.43	1.7	2100	142	1.29	5.1	6300	426
113.7	116.7	2778	3.0	0.39	1.5	2350	143	1.17	4.5	7050	429
116.7	119.7	2779	3.0	0.71	1.8	2960	205	2.13	5.4	8880	615
119.7	122.5	2780	2.8	0.30	0.8	1200	35	0.84	2.24	3360	98
122.5	125.7	2781	3.2	0.26	0.8	850	46	0.832	2.56	2720	147.2
125.7	128.7	2782	3.0	0.19	1.0	716	47	0.57	3	2148	141
128.7	131.7	2783	3.0	0.17	0.6	827	31	0.51	1.8	2481	93
131.7	135.1	2784	3.4	0.18	0.8	830	30	0.612	2.72	2822	102
135.1	137.3	2785	2.2	0.16	0.7	590	47	0.352	1.54	1298	103.4

## CT1220.XLS

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w'a)	Ag (w'a)	Cu(w'a)	Mo(w'a)
137.3	140.7	2786	3.4	0.22	0.9	594	40	0.748	3.06	2019.6	136
140.7	143.7	2787	3.0	0.21	1.1	730	38	0.63	3.3	2190	114
143.7	146.7	2788	3.0	0.18	0.7	580	28	0.54	2.1	1740	84
146.7	149.7	2789	3.0	0.23	1.3	1140	71	0.69	3.9	3420	213
149.7	152.7	2790	3.0	0.26	0.7	1000	49	0.78	2.1	3000	147
152.7	155.7	2791	3.0	0.15	0.3	580	24	0.45	0.9	1740	72
155.7	158.7	2792	3.0	0.22	0.6	862	20	0.66	1.8	2586	60
158.7	161.5	2793	2.8	0.17	0.9	610	23	0.476	2.52	1708	64.4
161.5	163.3	2794	1.8	0.16	0.9	1030	45	0.288	1.62	1854	81
163.3	166.1	2795	2.8	0.23	0.6	920	25	0.644	1.68	2576	70
166.1	169.1	2796	3.0	0.43	1.1	1620	72	1.29	3.3	4860	216
169.1	172.1	2797	3.0	0.34	0.5	580	20	1.02	1.5	1740	60
172.1	175.1	2798	3.0	0.28	0.8	890	38	0.84	2.4	2670	114
175.1	178.1	2799	3.0	0.38	1.0	1160	24	1.14	3	3480	72
178.1	181.1	2800	3.0	0.41	0.9	900	18	1.23	2.7	2700	54
181.1	184.2	2801	3.1	0.36	0.6	1090	30	1.116	1.86	3379	93
184.2	187.2	2802	3.0	0.44	1.0	1480	57	1.32	3	4440	171
187.2	190.2	2803	3.0	0.98	1.8	926	32	2.94	5.4	2778	96
190.2	193.0	2804	2.8	0.45	7.0	1950	26	1.26	19.6	5460	72.8
193.0	196.0	2805	3.0	0.34	3.7	1090	433	1.02	11.1	3270	1299
196.0	199.0	2806	3.0	0.30	1.2	730	80	0.9	3.6	2190	240
199.0	202.7	2807	3.7	0.26	0.7	730	51	0.962	2.59	2701	188.7
202.7	204.9	2808	2.2	0.42	1.5	1270	72	0.924	3.3	2794	158.4
204.9	207.0	2809	2.1	0.22	0.4	400	13	0.462	0.84	840	27.3
207.0	209.2	2810	2.2	0.30	1.0	820	41	0.66	2.2	1804	90.2
209.2	211.0	2811	1.8	0.61	1.6	1510	52	1.098	2.88	2718	93.6
211.0	214.0	2812	3.0	0.34	0.6	916	78	1.02	1.8	2748	234
214.0	217.0	2813	3.0	0.44	1.5	1260	88	1.32	4.5	3780	264
217.0	220.0	2814	3.0	0.18	0.8	624	16	0.54	2.4	1872	48
220.0	223.0	2815	3.0	0.24	0.5	764	7	0.72	1.5	2292	21
223.0	227.0	2816	4.0	0.29	1.5	880	27	1.16	6	3520	108
227.0	230.1	2817	3.1	0.38	2.9	1180	21	1.178	8.99	3658	65.1
230.1	233.0	2818	2.9	0.24	1.0	718	16	0.696	2.9	2082.2	46.4
233.0	235.8	2819	2.8	0.20	0.3	820	22	0.56	0.84	2296	61.6
235.8	238.8	2820	3.0	0.17	0.9	530	24	0.51	2.7	1590	72
238.8	239.3	2821	0.5	0.01	0.1	20	1	0.005	0.05	10	0.5
239.3	242.3	2822	3.0	0.44	1.1	710	5	1.32	3.3	2130	15
242.3	244.7	2823	2.4	0.14	0.8	770	19	0.336	1.92	1848	45.6
244.7	247.8	2824	3.1	0.13	0.2	415	11	0.403	0.62	1286.5	34.1
247.8	250.8	2825	3.0	0.12	0.5	621	16	0.36	1.5	1863	48

## CT1220.XLS

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w'a)	Ag (w'a)	Cu(w'a)	Mo(w'a)
250.8	254.0	2826	3.2	0.36	0.9	1008	23	1.152	2.88	3225.6	73.6
254.0	257.0	2827	3.0	0.46	1.2	2510	141	1.38	3.6	7530	423
257.0	260.1	2828	3.1	0.29	1.1	1470	46	0.899	3.41	4557	142.6
260.1	263.1	2829	3.0	0.14	0.6	580	56	0.42	1.8	1740	168
263.1	266.1	2830	3.0	0.47	1.0	1140	15	1.41	3	3420	45
266.1	269.1	2831	3.0	0.43	0.1	490	93	1.29	0.3	1470	279
269.1	272.1	2832	3.0	0.15	0.8	378	15	0.45	2.4	1134	45
272.1	275.1	2833	3.0	0.10	0.1	44	20	0.3	0.3	132	60
275.1	278.1	2834	3.0	0.08	0.1	130	41	0.24	0.3	390	123
278.1	281.1	2835	3.0	0.21	1.0	930	68	0.63	3	2790	204
281.1	284.1	2836	3.0	0.31	3.0	970	25	0.93	9	2910	75
284.1	287.1	2837	3.0	0.26	0.5	860	9	0.78	1.5	2580	27
287.1	290.1	2838	3.0	0.31	0.9	1210	23	0.93	2.7	3630	69
290.1	293.1	2839	3.0	0.25	1.1	810	5	0.75	3.3	2430	15
293.1	296.1	2840	3.0	0.24	1.4	1100	12	0.72	4.2	3300	36
296.1	299.1	2841	3.0	0.26	2.0	920	13	0.78	6	2760	39
299.1	302.1	2842	3.0	0.24	1.0	1200	30	0.72	3	3600	90
302.1	303.6	2843	1.5	0.28	0.9	1140	16	0.42	1.35	1710	24
303.6	306.4	2844	2.8	0.12	0.6	560	20	0.336	1.68	1568	56
306.4	307.1	2845	0.7	0.08	0.4	170	4	0.056	0.28	119	2.8
307.1	310.1	2846	3.0	0.06	0.6	254	10	0.18	1.8	762	30
310.1	313.1	2847	3.0	0.06	0.2	310	5	0.18	0.6	930	15
313.1	316.1	2848	3.0	0.05	1.0	290	6	0.15	3	870	18
316.1	319.1	2849	3.0	0.06	1.2	390	38	0.18	3.6	1170	114
319.1	322.1	2850	3.0	0.07	1.0	362	18	0.21	3	1086	54
322.1	325.1	2851	3.0	0.05	0.8	384	6	0.15	2.4	1152	18
325.1	328.7	2852	3.6	0.04	0.4	245	10	0.144	1.44	882	36
328.7	331.1	2853	2.4	0.03	0.2	183	14	0.072	0.48	439.2	33.6
331.1	333.0	2854	1.9	0.04	0.2	206	8	0.076	0.38	391.4	15.2
333.0	336.0	2855	3.0	0.06	0.2	225	8	0.18	0.6	675	24
336.0	339.0	2856	3.0	0.07	0.2	272	3	0.21	0.6	816	9
339.0	342.0	2857	3.0	0.04	0.2	138	4	0.12	0.6	414	12
342.0	345.0	2858	3.0	0.06	0.2	398	2	0.18	0.6	1194	6
345.0	348.0	2859	3.0	0.08	0.5	341	16	0.24	1.5	1023	48
348.0	352.0	2860	4.0	0.03	0.1	270	10	0.12	0.4	1080	40
352.0	354.0	2861	2.0	0.03	1.2	112	8	0.06	2.4	224	16
354.0	357.0	2862	3.0	0.03	0.1	116	3	0.09	0.3	348	9
357.0	360.0	2863	3.0	0.02	0.1	166	9	0.06	0.3	498	27
360.0	363.0	2864	3.0	0.02	0.2	154	4	0.06	0.6	462	12
363.0	366.0	2865	3.0	0.01	0.2	238	12	0.03	0.6	714	36

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
368.0	369.1	2866	3.1	0.02	0.2	180	4	0.062	0.62	558	12.4
<b>25.6 m - 119.7 m</b>											
<b>Total (w*a)</b>			94.1	51.71	198.7	255425.0	11531.6				
<b>Mean</b>				0.55	2.1	2714	123				
<b>119.7 m - 306.4 m</b>											
<b>Total (w*a)</b>			186.7	52.47	198.9	167338.9	7829.5				
<b>Mean</b>				0.28	1.1	896	42				
<b>306.4 m - 369.1 m</b>											
<b>Total (w*a)</b>			62.7	2.81	26.1	15807.6	588.0				
<b>Mean</b>				0.04	0.4	252	9				
<b>25.6 m - 306.4 m</b>											
<b>Total (w*a)</b>			280.8	104.18	397.5	422763.9	19381.1				
<b>Mean</b>				0.37	1.4	1506	69				
<b>25.6 m - 369.1 m</b>											
<b>Total (w*a)</b>			343.5	106.99	423.6	438571.5	19949.1				
<b>Mean</b>				0.31	1.2	1277	58				

DDH 1221 ASSAY TABLE												
From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w'a)	Ag (w'a)	Cu(w'a)	Mo(w'a)	
13.0	16.0	2647	3.0	0.13	0.2	400	12	0.39	0.6	1200	36	
16.0	19.0	2648	3.0	0.09	0.8	800	8	0.27	2.4	2400	24	
19.0	22.0	2649	3.0	0.22	0.8	1000	2	0.66	2.4	3000	6	
22.0	24.0	2650	2.0	0.17	0.6	500	3	0.34	1.2	1000	6	
24.0	26.9	2651	2.9	0.12	0.4	400	2	0.348	1.16	1160	5.8	
26.9	30.6	2652	3.7	0.08	0.4	400	4	0.296	1.48	1480	14.8	
30.6	34.3	2653	3.7	0.12	0.5	500	6	0.444	1.85	1850	22.2	
34.3	37.4	2654	3.1	0.11	0.4	400	8	0.341	1.24	1240	24.8	
37.4	41.5	2655	4.1	0.10	0.6	400	5	0.41	2.46	1640	20.5	
41.5	43.6	2656	2.1	0.09	0.6	300	3	0.189	1.26	630	6.3	
43.6	46.6	2657	3.0	0.51	1.4	1600	4	1.53	4.2	4800	12	
46.6	49.6	2658	3.0	0.31	1.2	1100	12	0.93	3.6	3300	36	
49.6	52.6	2659	3.0	0.34	1.5	1700	4	1.02	4.5	5100	12	
52.6	55.6	2660	3.0	0.30	1.6	1000	2	0.9	4.8	3000	6	
55.6	58.6	2661	3.0	0.31	1.6	1100	9	0.93	4.8	3300	27	
58.6	61.6	2662	3.0	0.26	1.8	1500	4	0.78	5.4	4500	12	
61.6	64.6	2663	3.0	0.13	0.8	600	4	0.39	2.4	1800	12	
64.6	67.6	2664	3.0	0.32	0.7	800	4	0.96	2.1	2400	12	
67.6	70.6	2665	3.0	0.35	1.2	1400	2	1.05	3.6	4200	6	
70.6	73.6	2666	3.0	0.41	1.8	1400	2	1.23	5.4	4200	6	
73.6	76.6	2667	3.0	0.28	0.9	800	4	0.84	2.7	2400	12	
76.6	79.6	2668	3.0	0.27	1.2	1400	6	0.81	3.6	4200	18	
79.6	82.6	2669	3.0	0.48	1.6	1700	6	1.44	4.8	5100	18	
82.6	85.6	2670	3.0	1.27	4.0	5100	8	3.81	12	15300	24	
85.6	88.6	2671	3.0	0.76	3.4	4600	4	2.28	10.2	13800	12	
88.6	91.6	2672	3.0	0.32	1.5	1500	6	0.96	4.5	4500	18	
91.6	94.5	2673	2.9	0.18	0.6	500	4	0.522	1.74	1450	11.6	
94.5	97.6	2674	3.1	0.33	1.2	600	4	1.023	3.72	1860	12.4	
97.6	100.6	2675	3.0	1.13	1.4	500	5	3.39	4.2	1500	15	
100.6	103.6	2676	3.0	0.40	0.8	300	3	1.2	2.4	900	9	
103.6	106.6	2677	3.0	0.79	1.2	800	7	2.37	3.6	2400	21	
106.6	109.6	2678	3.0	0.29	1.0	700	4	0.87	3	2100	12	
109.6	112.5	2679	2.9	0.22	0.8	400	4	0.638	2.32	1160	11.6	
112.5	115.5	2680	3.0	0.26	1.0	500	5	0.78	3	1500	15	
115.5	118.5	2681	3.0	0.14	0.6	500	2	0.42	1.8	1500	6	
118.5	121.5	2682	3.0	0.39	1.0	500	13	1.17	3	1500	39	
121.5	124.5	2683	3.0	0.13	0.4	300	6	0.39	1.2	900	18	
124.5	127.6	2684	3.1	0.11	0.4	200	12	0.341	1.24	620	37.2	
127.6	130.6	2685	3.0	0.10	1.0	700	5	0.3	3	2100	15	

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w'a)	Ag (w'a)	Cu(w'a)	Mo(w'a)
130.6	133.6	2686	3.0	0.23	0.4	200	12	0.69	1.2	600	36
133.6	136.6	2687	3.0	0.14	0.4	160	9	0.42	1.2	480	27
136.6	139.7	2688	3.1	0.48	0.4	190	4	1.488	1.24	589	12.4
139.7	144.1	2689	4.4	0.32	0.5	236	12	1.408	2.2	1038.4	52.8
144.1	148.3	2690	4.2	0.01	0.4	62	4	0.042	1.68	260.4	16.8
148.3	152.6	2691	4.3	0.02	0.3	30	2	0.086	1.29	129	8.6
152.6	155.6	2692	3.0	0.07	0.4	138	4	0.21	1.2	414	12
155.6	158.6	2693	3.0	0.22	0.5	384	12	0.66	1.5	1152	36
158.6	161.7	2694	3.1	0.35	0.5	284	4	1.085	1.55	880.4	12.4
161.7	164.7	2695	3.0	0.56	1.2	348	16	1.68	3.6	1044	48
164.7	167.7	2696	3.0	0.92	1.0	356	4	2.76	3	1068	12
167.7	170.7	2697	3.0	0.20	0.3	137	14	0.6	0.9	411	42
170.7	173.7	2698	3.0	0.33	1.0	234	16	0.99	3	702	48
173.7	176.7	2699	3.0	0.26	1.1	286	13	0.78	3.3	858	39
176.7	180.0	2700	3.3	0.17	0.8	136	5	0.561	2.64	448.8	16.5
180.0	183.1	2701	3.1	0.23	0.6	139	14	0.713	1.86	430.9	43.4
183.1	185.2	2702	2.1	0.40	0.7	480	29	0.84	1.47	1008	60.9
185.2	188.2	2703	3.0	0.15	0.5	350	8	0.45	1.5	1050	24
188.2	191.2	2704	3.0	0.18	0.8	680	9	0.54	2.4	2040	27
191.2	194.1	2705	2.9	0.41	1.6	1170	18	1.189	4.64	3393	52.2
194.1	197.5	2706	3.4	0.30	1.3	520	14	1.02	4.42	1768	47.6
197.5	200.5	2707	3.0	0.18	1.0	634	6	0.54	3	1902	18
200.5	203.5	2708	3.0	0.45	1.2	680	7	1.35	3.6	2040	21
203.5	206.3	2709	2.8	0.10	0.2	136	6	0.28	0.56	380.8	16.8
206.3	209.3	2710	3.0	0.05	0.4	133	5	0.15	1.2	399	15
209.3	212.3	2711	3.0	0.30	1.4	980	22	0.9	4.2	2940	66
212.3	215.3	2712	3.0	0.07	0.2	96	6	0.21	0.6	288	18
215.3	218.3	2713	3.0	0.43	0.8	318	30	1.29	2.4	954	90
218.3	219.9	2714	1.6	0.10	0.4	210	6	0.16	0.64	336	9.6
219.9	221.9	2715	2.0	0.28	0.8	174	26	0.56	1.6	348	52
221.9	224.9	2716	3.0	0.18	0.8	142	20	0.54	2.4	426	60
224.9	227.9	2717	3.0	0.06	0.3	92	8	0.18	0.9	276	24
227.9	230.9	2718	3.0	0.05	0.3	56	6	0.15	0.9	168	18
230.9	233.9	2719	3.0	0.06	0.2	80	8	0.18	0.6	240	24
233.9	236.9	2720	3.0	0.07	0.2	64	14	0.21	0.6	192	42
236.9	239.9	2721	3.0	0.19	0.2	78	10	0.57	0.6	234	30
239.9	242.9	2722	3.0	0.01	0.2	92	16	0.03	0.6	276	48
242.9	245.9	2723	3.0	0.13	0.4	178	7	0.39	1.2	534	21
245.9	248.1	2724	2.2	0.06	0.4	160	18	0.132	0.88	352	39.6
248.1	250.9	2725	2.8	0.09	0.4	340	7	0.252	1.12	952	19.6

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w <sup>a</sup> )	Ag (w <sup>a</sup> )	Cu(w <sup>a</sup> )	Mo(w <sup>a</sup> )
250.9	253.9	2726	3.0	0.11	0.2	264	6	0.33	0.6	792	18
253.9	256.9	2727	3.0	0.13	0.2	375	8	0.39	0.6	1125	24
256.9	260.3	2728	3.4	0.15	15.0	231	40	0.51	51	785.4	136
260.3	263.3	2729	3.0	0.18	0.8	116	16	0.54	2.4	348	48
263.3	266.0	2730	2.7	0.44	0.8	60	6	1.188	2.16	162	16.2
266.0	267.5	2731	1.5	3.00	26.0	1520	8	4.5	39	2280	12
267.5	270.5	2732	3.0	0.95	3.2	280	6	2.85	9.6	840	18
270.5	273.8	2733	3.3	0.26	1.0	380	8	0.858	3.3	1254	26.4
273.8	276.8	2734	3.0	0.09	0.2	115	22	0.27	0.8	345	66
276.8	279.7	2735	2.9	0.04	0.3	62	6	0.116	0.87	179.8	17.4
279.7	282.7	2736	3.0	0.10	0.2	118	12	0.3	0.6	354	36
282.7	285.7	2737	3.0	0.13	0.3	113	6	0.39	0.9	339	18
285.7	288.4	2738	2.7	0.07	0.2	136	8	0.189	0.54	367.2	21.6
288.4	291.4	2739	3.0	0.07	0.4	126	5	0.21	1.2	378	15
291.4	294.5	2740	3.1	0.09	0.2	192	10	0.279	0.62	595.2	31
294.5	297.0	2741	2.5	0.41	0.4	376	5	1.025	1	940	12.5
297.0	298.7	2742	1.7	0.75	8.0	1770	8	1.275	13.6	3009	13.6
298.7	301.8	2743	3.1	0.60	1.8	380	9	1.86	5.58	1178	27.9
301.8	305.0	2744	3.2	0.16	0.3	288	6	0.512	0.96	921.6	19.2
305.0	308.1	2745	3.1	0.15	0.8	340	6	0.465	2.48	1054	18.6
308.1	312.1	2746	4.0	0.06	0.2	76	6	0.24	0.8	304	24
<b>13.0 m - 43.6 m</b>											
<b>Total (w<sup>a</sup>)</b>			<b>30.6</b>	<b>3.69</b>	<b>16.1</b>	<b>15600</b>	<b>166</b>				
<b>Mean</b>				<b>0.12</b>	<b>0.5</b>	<b>510</b>	<b>5</b>				
<b>43.6 m - 91.6 m</b>											
<b>Total (w<sup>a</sup>)</b>			<b>48.0</b>	<b>19.86</b>	<b>78.6</b>	<b>81900</b>	<b>243</b>				
<b>Mean</b>				<b>0.41</b>	<b>1.6</b>	<b>1706</b>	<b>5</b>				
<b>91.6 m - 312.1 m</b>											
<b>Total (w<sup>a</sup>)</b>			<b>220.5</b>	<b>58.00</b>	<b>246.0</b>	<b>70044</b>	<b>2149</b>				
<b>Mean</b>				<b>0.26</b>	<b>1.1</b>	<b>318</b>	<b>10</b>				
<b>13.0 m - 312.1 m</b>											
<b>Total (w<sup>a</sup>)</b>			<b>299.1</b>	<b>81.55</b>	<b>340.7</b>	<b>167544</b>	<b>2559</b>				
<b>Mean</b>				<b>0.27</b>	<b>1.1</b>	<b>560</b>	<b>9</b>				



DDH 1222 ASSAY TABLE												
From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w%a)	Ag (w%a)	Cu(w%a)	Mo(w%a)	
4.5	5.5	2395	1.0	1.26	8.8	3710	140	1.26	8.8	3710	140	
5.5	7.7	2396	2.2	0.02	0.1	290	4	0.044	0.22	638	8.8	
7.7	11.0	2397	3.3	0.55	1.9	1480	7	1.815	6.27	4884	23.1	
11.0	14.0	2398	3.0	0.48	1.6	1520	4	1.44	4.8	4560	12	
14.0	17.0	2399	3.0	0.61	1.2	1000	6	1.83	3.6	3000	18	
17.0	20.0	2400	3.0	0.53	1.5	1530	9	1.59	4.5	4590	27	
20.0	23.0	2401	3.0	0.56	1.5	1410	11	1.68	4.5	4230	33	
23.0	26.0	2402	3.0	0.65	1.6	1310	16	1.95	4.8	3930	48	
26.0	29.0	2403	3.0	0.46	1.8	1440	12	1.38	5.4	4320	36	
29.0	32.0	2404	3.0	0.50	1.3	1720	12	1.5	3.9	5160	36	
32.0	35.0	2405	3.0	0.49	1.6	2740	9	1.47	4.8	8220	27	
35.0	38.0	2406	3.0	0.44	1.1	1640	8	1.32	3.3	4920	24	
38.0	41.0	2407	3.0	0.64	2.3	1950	200	1.92	6.9	5850	600	
41.0	44.0	2408	3.0	0.56	1.8	1050	8	1.68	4.8	3150	24	
44.0	47.0	2409	3.0	0.60	2.4	1110	12	1.8	7.2	3330	36	
47.0	50.0	2410	3.0	0.51	1.5	1180	8	1.53	4.5	3540	24	
50.0	53.0	2411	3.0	0.38	1.6	1500	30	1.14	4.8	4500	90	
53.0	56.0	2412	3.0	0.48	1.7	1540	20	1.44	5.1	4620	60	
56.0	59.0	2413	3.0	0.66	2.0	1780	40	1.98	6	5340	120	
59.0	62.0	2414	3.0	0.72	1.8	1510	16	2.16	5.4	4530	48	
62.0	65.0	2415	3.0	0.40	1.5	1500	8	1.2	4.5	4500	24	
65.0	68.0	2416	3.0	1.36	2.7	3150	8	4.08	8.1	9450	24	
68.0	71.0	2417	3.0	1.70	5.9	7560	28	5.1	17.7	22680	84	
71.0	74.0	2418	3.0	0.64	1.0	820	22	1.92	3	2460	66	
74.0	77.0	2419	3.0	0.89	2.0	2620	42	2.67	6	7860	126	
77.0	80.0	2420	3.0	0.27	0.9	1020	8	0.81	2.7	3060	24	
80.0	83.0	2421	3.0	0.99	2.6	4000	24	2.97	7.8	12000	72	
83.0	86.0	2422	3.0	0.54	1.3	1430	6	1.62	3.9	4290	18	
86.0	89.0	2423	3.0	1.02	1.6	3030	22	3.06	4.8	9090	66	
89.0	92.0	2424	3.0	0.36	0.9	1960	10	1.08	2.7	5880	30	
92.0	95.0	2425	3.0	0.60	1.0	2670	66	1.8	3	8010	198	
95.0	98.0	2426	3.0	10.00	1.5	5460	58	30	4.5	16380	174	
98.0	101.0	2427	3.0	0.40	0.8	1520	30	1.2	2.4	4560	90	
101.0	104.0	2428	3.0	0.21	0.5	780	10	0.63	1.5	2340	30	
104.0	107.0	2429	3.0	0.36	0.8	1530	26	1.08	2.4	4590	78	
107.0	108.0	2430	1.0	0.34	1.4	1400	22	0.34	1.4	1400	22	
108.0	111.0	2431	3.0	2.60	6.4	4220	16	7.8	19.2	12660	48	
111.0	113.1	2432	2.1	0.63	2.6	1380	8	1.323	5.46	2898	16.8	
113.1	115.0	2433	1.9	0.42	100.0	1720	240	0.788	190	3268	456	

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w'a)	Ag (w'a)	Cu(w'a)	Mo(w'a)
115.0	118.0	2434	3.0	0.37	0.8	1240	12	1.11	2.4	3720	36
118.0	121.0	2435	3.0	0.29	1.4	1020	10	0.87	4.2	3060	30
121.0	124.0	2436	3.0	0.21	0.5	980	14	0.63	1.5	2940	42
124.0	127.0	2437	3.0	0.38	0.6	1240	10	1.14	1.8	3720	30
127.0	130.0	2438	3.0	0.15	0.2	810	36	0.45	0.6	2430	108
130.0	133.0	2439	3.0	0.23	0.4	1280	6	0.69	1.2	3840	18
133.0	136.0	2440	3.0	0.16	0.2	870	30	0.48	0.6	2610	90
136.0	139.0	2441	3.0	0.36	0.6	960	15	1.08	1.8	2880	45
139.0	142.0	2442	3.0	0.30	0.7	1060	15	0.9	2.1	3180	45
142.0	145.0	2443	3.0	0.39	0.6	1300	12	1.17	1.8	3900	36
145.0	148.0	2444	3.0	0.40	0.7	1450	15	1.2	2.1	4350	45
148.0	151.0	2445	3.0	0.34	0.7	1240	8	1.02	2.1	3720	24
151.0	154.0	2446	3.0	0.34	1.4	1475	20	1.02	4.2	4425	60
154.0	157.0	2447	3.0	0.19	0.7	854	15	0.57	2.1	2562	45
157.0	160.0	2448	3.0	0.34	1.6	1100	9	1.02	4.8	3300	27
160.0	163.0	2449	3.0	0.47	2.6	1950	20	1.41	7.8	5850	60
163.0	166.0	2450	3.0	0.69	2.8	1980	17	2.07	8.4	5940	51
166.0	169.0	2457	3.0	0.34	2.0	1429	10	1.02	6	4287	30
169.0	172.0	2458	3.0	0.30	1.4	970	13	0.9	4.2	2910	39
172.0	175.0	2459	3.0	0.21	1.8	580	6	0.63	5.4	1740	18
175.0	178.0	2460	3.0	0.53	1.8	1470	16	1.59	5.4	4410	48
178.0	181.0	2461	3.0	0.44	1.2	1290	9	1.32	3.6	3870	27
181.0	184.0	2462	3.0	0.64	1.0	945	6	1.92	3	2835	18
184.0	187.0	2463	3.0	0.34	1.2	1354	12	1.02	3.6	4062	36
187.0	190.0	2464	3.0	1.08	1.4	2760	24	3.24	4.2	8280	72
190.0	193.0	2465	3.0	0.23	0.8	980	17	0.69	2.4	2940	51
193.0	196.0	2466	3.0	0.33	1.8	1100	12	0.99	5.4	3300	36
196.0	199.0	2467	3.0	0.49	2.2	1190	22	1.47	6.6	3570	66

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w*a)	Ag (w*a)	Cu(w*a)	Mo(w*a)
<b>4.5 m - 65.0 m</b>											
<b>Total (w*a)</b>			60.5	32.13	104.1	91522	1459				
<b>Mean</b>				0.53	1.7	1513	24				
<b>65.0 m - 113.1 m</b>											
<b>Total (w*a)</b>			48.1	67.48	96.6	129608	1167				
<b>Mean</b>				1.40	2.0	2695	24				
<b>113.1 m - 199.0 m</b>											
<b>Total (w*a)</b>			85.9	32.42	289.3	107899	1689				
<b>Mean</b>				0.38	3.4	1256	20				
<b>4.5 m - 199.0 m</b>											
<b>Total (w*a)</b>			194.5	132.03	490.0	329029	4315				
<b>Mean</b>				0.68	2.5	1692	22				

DDH 1223 ASSAY TABLE											
From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w'a)	Ag (w'a)	Cu(w'a)	Mo(w'a)
0.0	7.9	3016	7.9	0.42	1.4	740	65	3.318	11.06	5846	513.5
7.9	11.0	3017	3.1	0.60	2.2	1310	100	1.86	6.82	4061	310
11.0	14.0	3018	3.0	0.86	4.6	3150	30	2.58	13.8	9450	90
14.0	17.1	3019	3.1	0.45	1.2	980	12	1.395	3.72	3038	37.2
17.1	19.0	3020	1.9	0.09	0.8	470	9	0.171	1.52	893	17.1
19.0	22.0	3021	3.0	0.13	0.4	260	6	0.39	1.2	780	18
22.0	24.4	3022	2.4	0.22	1.2	670	9	0.528	2.88	1608	21.6
24.4	27.4	3023	3.0	0.74	3.2	3100	26	2.22	9.6	9300	78
27.4	30.4	3024	3.0	0.42	2.0	1540	42	1.26	6	4620	126
30.4	33.8	3025	3.4	1.40	14.6	1950	165	4.76	49.64	6630	561
33.8	36.4	3026	2.6	0.15	1.8	550	10	0.39	4.68	1430	26
36.4	39.4	3027	3.0	0.06	0.6	216	6	0.18	1.8	648	18
39.4	42.4	3028	3.0	0.05	0.6	290	29	0.15	1.8	870	87
42.4	45.6	3029	3.2	2.00	0.8	276	12	6.4	2.56	883.2	38.4
45.6	49.0	3030	3.4	0.06	0.8	330	16	0.204	2.72	1122	54.4
49.0	50.3	3031	1.3	0.01	0.4	60	2	0.0065	0.52	78	2.6
50.3	52.2	3032	1.9	0.10	0.2	186	6	0.19	0.38	353.4	11.4
52.2	54.5	3033	2.3	0.16	1.2	330	38	0.368	2.76	759	87.4
54.5	58.0	3034	3.5	0.17	1.0	90	82	0.595	3.5	315	287
58.0	60.5	3035	2.5	1.08	0.8	210	25	2.7	2	525	62.5
60.5	62.5	3036	2.0	0.25	0.8	88	40	0.5	1.6	176	80
62.5	66.1	3037	3.6	0.15	0.6	126	10	0.54	2.16	453.6	36
66.1	69.1	3038	3.0	0.09	0.4	160	14	0.27	1.2	480	42
69.1	72.1	3039	3.0	0.63	1.0	250	10	1.89	3	750	30
72.1	73.3	3040	1.2	0.10	0.8	132	25	0.12	0.96	158.4	30
73.3	76.3	3041	3.0	0.43	0.9	252	8	1.29	2.7	756	24
76.3	79.0	3042	2.7	0.15	1.4	300	10	0.405	3.78	810	27
79.0	82.6	3043	3.6	0.08	1.0	296	6	0.288	3.6	1065.6	21.6
82.6	85.6	3044	3.0	0.25	4.0	1770	10	0.75	12	5310	30
85.6	88.6	3045	3.0	0.13	2.2	286	10	0.39	6.6	858	30
88.6	91.6	3046	3.0	0.18	1.4	210	14	0.54	4.2	630	42
91.6	94.6	3047	3.0	0.21	0.8	200	16	0.63	2.4	600	48
94.6	97.6	3048	3.0	0.04	0.6	194	14	0.12	1.8	582	42
97.6	100.6	3049	3.0	0.05	0.6	110	12	0.15	1.8	330	36
100.6	103.6	3050	3.0	0.10	0.8	232	10	0.3	2.4	696	30
103.6	106.6	3051	3.0	0.58	8.2	3280	8	1.74	24.6	9840	24
106.6	109.6	3052	3.0	0.17	1.4	310	12	0.51	4.2	930	36
109.6	112.6	3053	3.0	0.21	1.0	286	18	0.63	3	858	54
112.6	115.6	3054	3.0	0.25	1.3	284	14	0.75	3.9	852	42

## CT1223.XLS

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w%a)	Ag (w%a)	Cu(w%a)	Mo(w%a)
115.6	118.0	3055	2.4	0.13	1.1	184	11	0.312	2.64	441.6	26.4
118.0	121.5	3056	3.5	1.61	12.6	2700	24	5.635	44.1	9450	84
121.5	124.5	3057	3.0	0.06	1.0	176	9	0.18	3	528	27
124.5	127.5	3058	3.0	0.05	0.8	154	10	0.15	2.4	462	30
127.5	130.5	3059	3.0	0.25	0.6	210	8	0.75	1.8	630	24
130.5	133.5	3060	3.0	0.23	0.8	210	22	0.69	2.4	630	66
133.5	136.5	3061	3.0	0.10	0.8	136	12	0.3	2.4	408	36
136.5	139.5	3062	3.0	0.33	0.8	160	26	0.99	2.4	480	78
139.5	142.5	3063	3.0	0.28	0.8	316	19	0.84	2.4	948	57
142.5	145.0	3064	2.5	0.06	0.6	200	16	0.15	1.5	500	40
145.0	147.2	3065	2.2	0.19	1.0	386	15	0.418	2.2	849.2	33
147.2	150.2	3066	3.0	0.15	0.8	270	24	0.45	2.4	810	72
150.2	153.2	3067	3.0	0.47	1.6	510	18	1.41	4.8	1530	54
153.2	156.0	3068	2.8	0.46	5.8	2370	24	1.288	16.24	6636	67.2
156.0	158.0	3069	2.0	3.63	3.0	710	30	7.26	6	1420	60
158.0	161.0	3070	3.0	0.17	1.0	290	24	0.51	3	870	72
161.0	164.0	3071	3.0	1.90	0.8	250	6	5.7	2.4	750	18
164.0	166.0	3072	2.0	0.13	0.5	210	15	0.26	1	420	30
166.0	167.9	3073	1.9	0.13	0.6	100	106	0.247	1.14	190	201.4
167.9	168.3	3074	0.4	2.10	13.0	86	21	0.84	5.2	34.4	8.4
168.3	171.3	3075	3.0	0.05	0.4	90	11	0.15	1.2	270	33
171.3	174.3	3076	3.0	0.07	0.4	130	10	0.21	1.2	390	30
174.3	177.3	3077	3.0	0.04	0.6	164	19	0.12	1.8	492	57
177.3	180.3	3078	3.0	0.05	0.4	100	6	0.15	1.2	300	18
180.3	183.4	3079	3.1	0.15	0.6	68	16	0.465	1.86	210.8	49.6
183.4	186.4	3080	3.0	10.00	0.4	158	8	30	1.2	474	24
186.4	189.4	3081	3.0	0.09	0.4	130	8	0.27	1.2	390	24
189.4	193.2	3082	3.8	0.94	14.6	396	12	3.572	55.48	1504.8	45.6
193.2	196.2	3083	3.0	0.41	0.8	110	9	1.23	2.4	330	27
196.2	199.2	3084	3.0	0.03	0.6	80	8	0.09	1.8	240	24
199.2	202.2	3085	3.0	0.04	0.6	92	12	0.12	1.8	276	36
202.2	205.2	3086	3.0	0.01	0.6	82	11	0.03	1.8	246	33
205.2	208.2	3087	3.0	0.03	0.4	60	16	0.09	1.2	180	48
208.2	211.2	3088	3.0	0.09	0.4	100	16	0.27	1.2	300	48
211.2	213.6	3089	2.4	0.13	0.6	62	20	0.312	1.44	148.8	48
213.6	214.1	3090	0.5	1.61	8.0	186	12	0.805	4	93	6
214.1	217.2	3091	3.1	0.06	0.6	62	12	0.186	1.86	192.2	37.2
217.2	220.2	3092	3.0	0.03	0.4	66	11	0.09	1.2	198	33
220.2	223.2	3093	3.0	0.08	0.4	92	22	0.24	1.2	276	66
223.2	226.2	3094	3.0	0.04	0.2	96	10	0.12	0.6	288	30

From	To	Number	Width m	Au ppm	Ag ppm	Cu ppm	Mo ppm	Au (w%a)	Ag (w%a)	Cu(w%a)	Mo(w%a)
226.2	229.2	3095	3.0	0.02	0.2	110	18	0.06	0.6	330	54
229.2	232.2	3096	3.0	0.03	0.2	100	16	0.09	0.6	300	48
232.2	235.2	3097	3.0	0.06	0.2	120	18	0.18	0.6	360	54
235.2	238.2	3098	3.0	0.02	0.2	92	16	0.06	0.6	276	48
238.2	241.2	3099	3.0	0.01	0.4	94	16	0.03	1.2	282	48
241.2	244.2	3100	3.0	0.06	0.3	140	22	0.18	0.9	420	66
244.2	247.2	2867	3.0	0.01	0.2	20	4	0.015	0.6	60	12
247.2	250.2	2868	3.0	0.03	0.6	62	9	0.09	1.8	186	27
250.2	253.2	2869	3.0	0.02	0.4	42	7	0.06	1.2	126	21
253.2	256.2	2870	3.0	0.11	3.6	140	24	0.33	10.8	420	72
256.2	259.2	2871	3.0	0.06	0.6	68	5	0.18	1.8	204	15
259.2	264.0	2872	4.8	0.01	0.6	164	5	0.048	2.88	787.2	24
<b>0.0 m - 33.8 m</b>											
<b>Total (w%a)</b>			<b>33.8</b>	<b>18.48</b>	<b>106.2</b>	<b>46226</b>	<b>1772</b>				
<b>Mean</b>				<b>0.55</b>	<b>3.1</b>	<b>1368</b>	<b>52</b>				
<b>33.8 m - 196.2 m</b>											
<b>Total (w%a)</b>			<b>162.4</b>	<b>87.54</b>	<b>285.6</b>	<b>65468</b>	<b>2772</b>				
<b>Mean</b>				<b>0.54</b>	<b>1.8</b>	<b>403</b>	<b>17</b>				
<b>196.2 m - 264.0 m</b>											
<b>Total (w%a)</b>			<b>67.8</b>	<b>3.68</b>	<b>41.7</b>	<b>6189</b>	<b>898</b>				
<b>Mean</b>				<b>0.05</b>	<b>0.6</b>	<b>91</b>	<b>13</b>				
<b>0.0 m - 196.2 m</b>											
<b>Total (w%a)</b>			<b>196.2</b>	<b>106.03</b>	<b>391.8</b>	<b>111694</b>	<b>4544</b>				
<b>Mean</b>				<b>0.54</b>	<b>2.0</b>	<b>569</b>	<b>23</b>				
<b>0.0 m - 264.0 m</b>											
<b>Total (w%a)</b>			<b>264.0</b>	<b>109.70</b>	<b>433.5</b>	<b>117883</b>	<b>5443</b>				
<b>Mean</b>				<b>0.42</b>	<b>1.6</b>	<b>447</b>	<b>21</b>				

*change to  
7.9m to -*

**APPENDIX 4**

Excerpts from International Skyline's  
Bronson Slope Mine  
Approval Certificate Application  
(sections 2, 3)

## **2.0 GEOLOGY**

### **2.1 Regional Geology (after Rhys 1993, 1995)**

The Iskut River region is within the Intermontane Belt on the western margin of the Stikine terrane. Three distinct stratigraphic elements are recognised in the western portion of the area (Anderson, 1989): (i) Upper Paleozoic schists, argillites, coralline limestone and volcanic rocks of the Stikine Assemblage, (ii) Triassic Stuhini Group volcanic and sedimentary arc related strata, and (iii) Lower to Middle Jurassic Hazelton Group volcanic and sedimentary arc related strata.

Intrusive rocks in the Iskut River region comprise five plutonic suites. The Stikine plutonic suite comprises Late Triassic calc-alkaline intrusions which are coeval with Stuhini Group strata. The Copper Mountain, Texas Creek and Three Sisters plutonic suites are variable in composition but are roughly coeval and cospatial with Hazelton Group volcanic strata. Tertiary elements of the Coast Plutonic Complex are represented by predominantly granodioritic to monzonitic Eocene intrusions of the Hyder plutonic suite, exposed 12 kilometres south of the Bronson Slope deposit (Britton et al., 1990).

The age, mineralogy and texture of the Red Bluff porphyry stock (associated with the Bronson Slope deposit), suggest that it belongs to the metallogenetically important Early Jurassic Texas Creek plutonic suite (Alldrick, 1985; Alldrick et al, 1987; Brown, 1987). Plutons of this suite are widespread in the Stewart, Iskut River region and range in age from 196 to 185 million years (Anderson, 1993; MacDonald et al., 1992, and in preparation).

### **2.2 Project Geology**

#### **2.2.1 Geology of the Bronson Creek Area**

Strata in the Bronson Creek area are divided into a lower and an upper sequence; probably correlating with Triassic Stuhihi Group and Jurassic Hazelton Group respectively. The sequences are separated by a flat lying to gently dipping regional unconformity exposed some three kilometres to the southwest of the deposit near the Johnny Mountain Gold mine (Figure 2-1).

The lower sequence comprises folded turbiditic greywackes with interbedded siltstones, mudstones, volcanic conglomerate and rare lenses of carbonate rocks. The sequence is weakly to moderately metamorphosed (lower greenschist facies).



The lower sequence is intruded by the Red Bluff porphyry stock, a hydrothermally altered, potassium feldspar megacrystic, plagioclase porphyritic intrusion of probable granodioritic composition. The stock is approximately 2.0 kilometres long, up to 0.3 kilometres wide and trends southeast along the southwest side of the Bronson Creek valley. Contacts of the stock with country rocks are not well defined, but where observed in drill core or underground workings are either faulted or intrusive. The southwest and northeast contacts appear to be southwesterly dipping.

### 2.2.2 Geology of the Bronson Slope Deposit

The Bronson Slope porphyry gold, copper, silver, molybdenum deposit occurs on the southwest flank of the Red Bluff stock in hydrothermally altered country rocks and to a lesser extent in altered intrusive rocks.

The country rocks in the deposit comprise dark coloured, intermediate to mafic mudstones and siltstones with lesser amounts of light coloured wackes as interbeds. The sedimentary rocks are variably hydrothermally altered as a function of proximity to the intrusive porphyry. The alteration sequence in order of increasing distance from the intrusive is: (i) potassium feldspar alteration with subordinate chlorite, sericite and biotite, (ii) chlorite biotite hornfels with subordinate calcite and (iii) biotite carbonate alteration (occasionally schistose) with subordinate chlorite and sericite. There is field mapping evidence of a quartz, sericite, pyrite phyllic zone followed by a calcite, epidote, biotite, chlorite propylitic zone adjacent to those previously mentioned but these zones have not been encountered in the present drill pattern.

The intrusive rocks in the deposit comprise the Red Bluff porphyry stock variably but extensively altered by the overprint of quartz, magnetite mineralization. The quartz, magnetite was emplaced by multiple phases of veining which exhibit a wide range of depositional textures including: (i) simple widely spaced quartz, magnetite stringers ranging from several millimetres to several centimetres thick, (ii) several sets of crosscutting quartz, magnetite stringers of similar size, (iii) a stockwork of multiple sets of crosscutting quartz, magnetite stringers of sufficiently dense spacing to comprise greater than 50% of the whole rock mass, (iv) complete replacement of the original rock by quartz (90%) and magnetite (10%) and (v) a stockwork of quartz magnetite stringers cutting quartz, magnetite replacement to form a quartz, magnetite breccia. The quartz, magnetite mineralization has also occurred in the sedimentary rocks in the deposit.

The deposition of gold, copper, silver and molybdenum has accompanied late quartz, pyrite veining that has cut the sedimentary rocks, the intrusive rocks and the quartz, magnetite mineralization. The ore minerals have deposited as discrete grains in and along boundaries of quartz stringers, as discrete grains disseminated throughout altered mafic sedimentary rocks and as thin films coating closely spaced late hairline fractures.

The metal prices used to define the metal grade categories are: (i) gold at US \$12.06 per gram or US \$375 per troy ounce, (ii) silver at US\$ 0.16 per gram or US \$5.06 per troy ounce and (iii) copper at US \$2,072.34 per metric tonne or US \$0.94 per pound. Molybdenum values were not included in the determination of metal grade categories. The Canadian dollar value used is equivalent to US \$0.75.

In the case of the Bronson Slope deposit, the total inferred and indicated resource of mineralised rock containing greater than Cdn. \$10.00 per metric tonne worth of metal (Gross Contained Metal Value) is 90.2 million metric tonnes containing an average of 0.749 grams gold per metric tonne, 4.2 grams silver per metric tonne, 0.16 % copper and 0.01 % molybdenum. The value of metals contained in this resource is Cdn. \$1.56 billion or an average of Cdn. \$17.34 per metric tonne.

Within this larger deposit, the company has designed an open cut that would initially mine the lower cost material. This open cut contains a probable reserve of 56.7 million metric tonnes containing an average of 0.545 grams gold per metric tonne, 2.4 grams silver per metric tonne, 0.18 % copper and 0.01 % molybdenum including all mineralised rock containing greater than Cdn. \$5.00 per metric tonne worth of metal. The value of metals contained in this reserve is Cdn. \$813.6 million or an average of Cdn. \$14.34 per metric tonne. In order to mine this reserve of mineralised rock, the company will have to mine a total of 16.3 million metric tonnes of waste rock. The ratio of waste rock to ore is 0.29:1. This proposed open cut mine plan is the subject of this Application for Environmental Review.

### **2.3.2 Mine Life**

The company is proposing to construct a concentrator nominally capable of processing 12,000 metric tonnes per day of ore. Assuming a plant availability of 345 days per year, the mine plan should be completed in 13.7 years.

### **2.2.3 Ore Mineralogy**

The ore minerals in the deposit are as follows; (i) copper: chalcopyrite with minor covellite, chalcocite, malachite, native copper and cuprite, (ii) silver: tetrahedrite, (iii) molybdenum: molybdenite and (iv) gold: not seen but demonstrates a correlation with copper and likely occurs microscopically on chalcopyrite grain boundaries. The gangue minerals in the deposit are quartz, pyrite, dolomite and calcite with minor chlorite, biotite and sericite. The magnetite content of the deposit is approximately 10% and represents a recoverable and potentially profitable component of the deposit if transportation costs from the site to tidewater can be minimized.

### **2.2.4 Host Mineralogy**

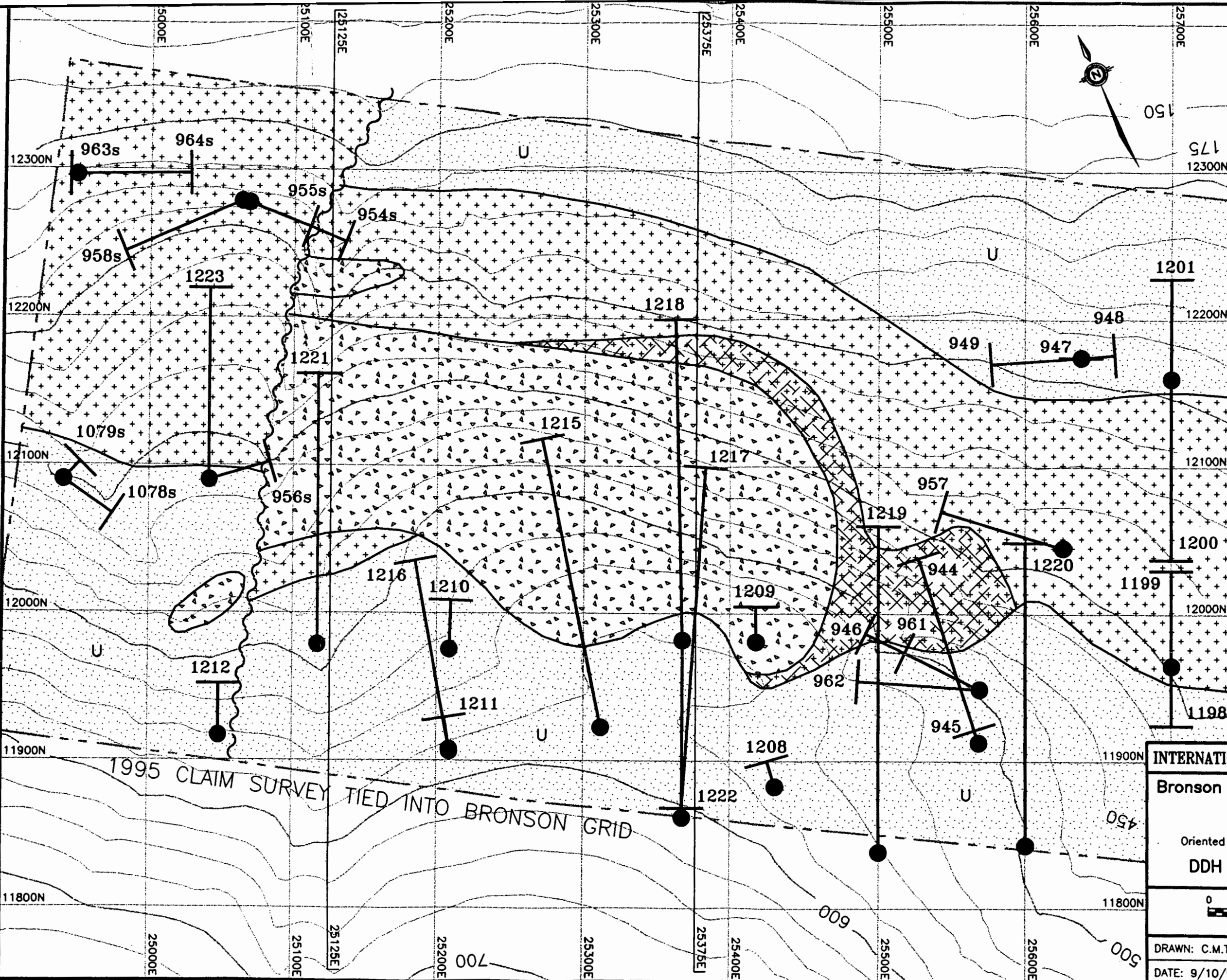
The mineralogy of the host rock and of the waste rock comprises predominantly feldspar, quartz, chlorite, dolomite, pyrite, calcite, biotite, sericite and minor clay minerals.

## **2.3 Reserves and Mine Life**

### **2.3.1 Reserves**





The reserve estimate for the Bronson Slope deposit is based on information from 47 diamond drill holes comprising 7,126 metres of drilling. These holes were drilled during exploration projects in 1965, 1988, 1993, 1994 and 1995. The 1988 program gave preliminary indications of the gold potential of the deposit but it was not until the 1993 drilling that the size potential was discovered. The high grade core of the deposit was outlined in 1994.

Reserves have been calculated using the bench polygonal weighting method. The steps used to calculate reserves in this fashion are as follows: (i) the deposit is divided into a series of horizontal slices approximating mining benches in an open pit mine; in the case of the Bronson Slope deposit the bench thickness is 10 metres, (ii) for each drill hole on each bench, a composite metal assay value is assigned by finding the weighted arithmetic mean of the assay intervals that fall within the 10 metre elevation slice, (iii) the composite metal assay value for each drill hole on each bench is assigned to a polygonal area surrounding the drill hole; the shape of the polygon being determined by perpendicular bisector lines between drill holes, (iv) the volume and weight of mineralised rock associated with each polygon is calculated by multiplying the area of each polygon by the bench thickness and the specific gravity of the rock (S. G. = 2.65), (v) the total tonnages of the polygonal blocks falling within the various metal grade categories are compiled and (vi) the weighted arithmetic means of the metal grades for the total tonnages in each metal grade category are calculated.






**LEGEND**

LITHOLOGY

-  Quartz Magnetite Replacement &/or Breccia
-  Quartz Magnetite Stockwork after Previous Rock Types
-  Red Bluff Porphyry intrusive
-  Sedimentary Rocks
  - U - undifferentiated
  - A - Biotite carbonate alteration
  - B - Biotite chlorite hornfels
  - C - Potassium feldspar alteration.

SYMBOLS

-  Drill Hole Trace
-  Fault
-  Claim Boundary

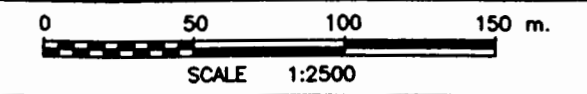
INTERNATIONAL SKYLINE GOLD CORPORATION

Bronson Slope Gold, Copper Porphyry

PLAN VIEW

Oriented Grid North ( 25° 12' 22" True 1983 )

DDH LOCATIONS and GEOLOGY



DRAWN: C.M.T. / D.Y.	Filename: Fig2-1.dwg	Figure
DATE: 9/10/95	NTS: 104B/11	<b>2-1</b>

## **3.0 PROJECT DESCRIPTION**

### **3.1 Location and Access**

#### **3.1.1 Location**

The deposit is located in the Liard mining district at 56° 39' 54" N. Latitude, 131° 05' 15" W. Longitude on N. T. S. map sheet 104 B 11E. It is 110 air km northwest of Stewart, B.C.

#### **3.1.2 Present Access**

The property is only accessible by air and is serviced by two nearby airstrips, Bronson Creek and Johnny Mountain, both of which are capable of utilizing Hercules C-130 transports. The airstrips are 240 air kilometers from Terrace, B. C. and 82 air kilometers from Wrangell, Alaska. Cominco Ltd. also uses a hovercraft to transport freight via the Iskut and Stikine Rivers to Wrangell.

#### **3.1.3 Planned Access**

The development of the Bronson Slope gold, copper porphyry will be dependent on road access to the site. A 30.5 kilometer extension of the existing Eskay Creek road from Volcano Creek to Bronson Creek is the most logical route. This extension would allow concentrate and supplies to be transported via the Cassiar - Stewart Highway and the existing port facilities located at Stewart, B.C. on the Portland Canal.

The Iskut Valley spur road is planned as an extension to the existing Eskay Creek Road (Figure 3-1) which connects Homestake Canada's Eskay Creek mine to Highway 37 just south of Bob Quinn.

The Iskut Valley spur road was the subject of a study completed by Klohn Leonoff Consulting Engineers on March 28, 1991. The study was commissioned by the British Columbia Ministry of Energy, Mines and Petroleum Resources. The report was intended to provide approval for road access to the Cominco Snip mine located at the junction of Bronson Creek and the Iskut River as well as access to the Eskay Creek mine located near Tom Mackay Lake. The section of the road to Eskay Creek has been completed.

The portion of the road to the Cominco Snip mine has not yet been completed. The construction of the road has been approved in principal. The final routing and design will be carried out under the issuance of a Ministry of Forests Special Use Permit for a Category C Resource Development Road. The construction of the road will have to meet the requirements of the Forest Practices Code.

As the road has been already approved in principal, it is not necessary for it to be re-approved under this application.

Concentrate will be hauled from the mine site by a contractor using highway certified vehicles. Approximately eight truckloads per day of concentrate will be hauled from the mine site to Stewart, British Columbia. General materials, explosives and fuel, as well as other specific materials, will be hauled in vehicles designed for those purposes.

All vehicles using the Iskut Valley Road and the Bronson Slope Spur Road will be in radio contact at all times. The vehicles will be required to give their location at selected points along the access road. Access to the road will be controlled by an existing gate, jointly controlled by Eskay Creek and Bronson Slope mines, in the middle of the Ningunsa River Bridge at approximately km 4 on the access road. We understand the gate is locked with a rotating combination lock and is adequate to restrict unauthorized access to the area. The component distances between the mine site and shipping point are:

	KM
Mine Site to Junction of Eskay Creek Road	30
Iskut Valley Road to Hwy 37 Junction	50
Highway 37 Jct to Bell II	44
Bell II to Meziadin Jct	94
Meziadin Jct to Stewart (Hwy 37A)	62

An avalanche and snow safety study has been completed for the Iskut Valley Road and a study will be undertaken for the Bronson Slope Spur road.

### 3.1.4 Logging Truck Traffic - Highways 37 and 37A

A major truck traffic source on Highway 37 and 37A is logging traffic. Estimates of logging truck traffic were obtained from Ministry of Forests in Smithers and are as follows:

Highway 37

Yukon traffic

20 to 30 loads/day  
August 1995  
4 to 5 October 1995

British Columbia

8 to 9 loads/day  
December to March  
annually

Highway 37A

Approximately 10 percent of this traffic.

Additional logging truck traffic originates from the Bobquin and Nass-Kispiox areas. Estimates are presently unavailable.

**3.2 Mine Plan**

Figure 3-2 is a site plan showing the relationship of the open pit and tailings impoundment.

**3.2.1 Introduction**

The Bronson Slope Gold, Copper Porphyry will be developed utilizing conventional open pit methods, keeping in mind that Bronson Slope is not a conventional open pit deposit. The mineral deposit has been exposed on three sides by natural erosion, leaving a steep bluff protruding from a mountain slope. This will allow the deposit to be mined by a series of horizontal benches, which will ultimately result in a slice being taken of the side of the mountain slope (Figures 3-3 to 3-7). The mined deposit will be referred to as an open pit for simplicity throughout the report.

The deposit is located above the planned site facilities, as opposed to being below the facilities. This stratigraphic location will eliminate the need for hauling material to waste storage facilities and the mill. All material moved from the mine area will be dropped down a twin ore pass system to the valley bottom where it will be transferred by conveyor to either the mill or waste storage facility (Figure 3-8).

### 3.2.2 Mineable Reserve Estimate

The minimum estimated mineable resource at Bronson Slope is 56,728,000 tonnes of ore grading 0.545 grams per tonne gold, 2.4 grams per tonne silver, 0.18 % copper, 0.01 % molybdenum, and 16,347,000 tons of waste material of which 9,502,000 is possible prestrip. The deposit realizes an ultimate strip ratio of 0.29:1 waste to ore. A breakdown of progressive strip ratios is outlined in Table 3-1. These estimates are subject to increase with further drilling, and more detailed economic analyses.

### 3.2.3 Design Criteria

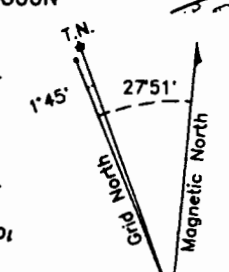
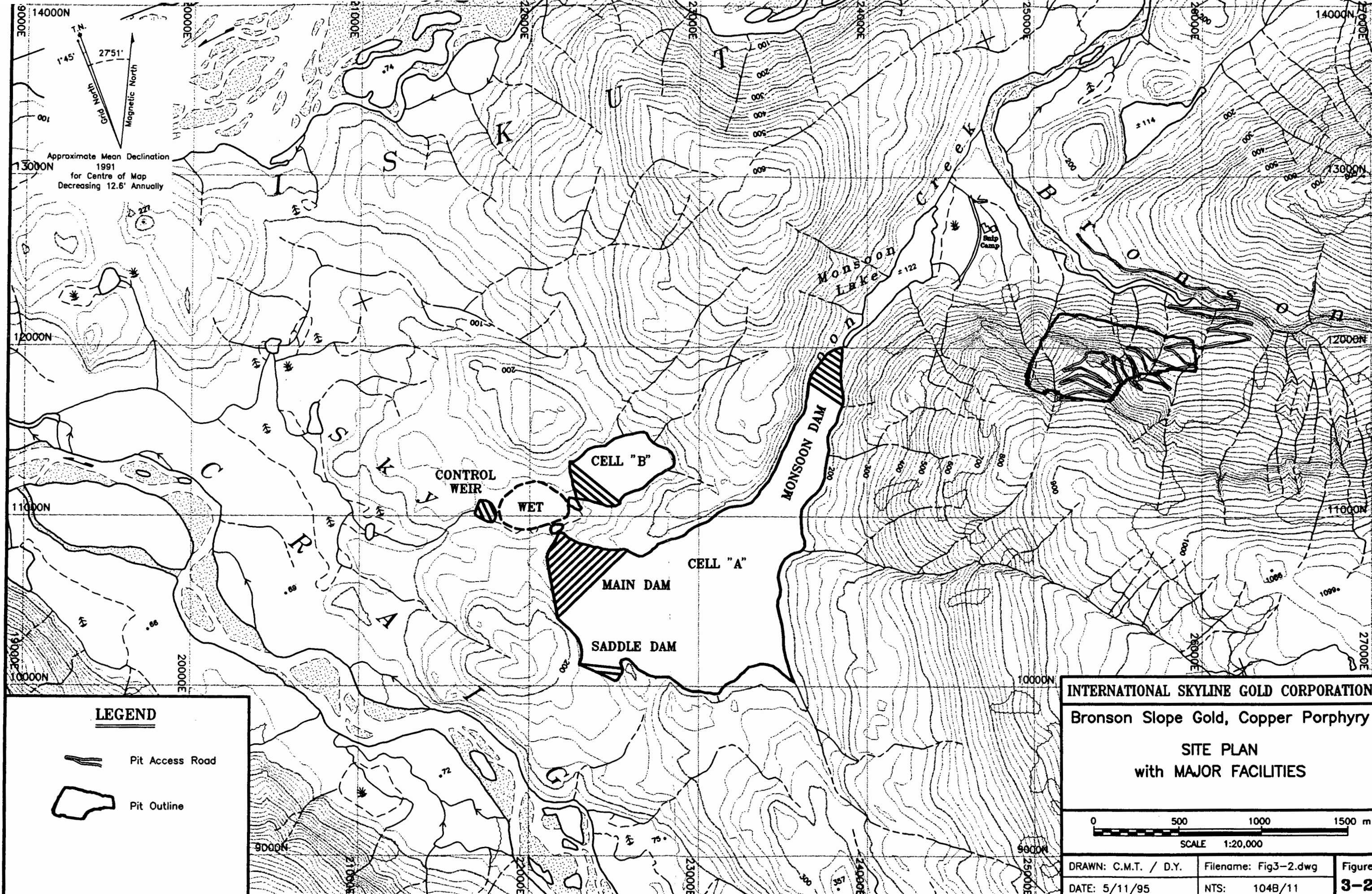
The open pit has been designed with a 55 degree ultimate slope highwall. The Red Bluff itself which forms a good portion of the deposit and has a natural slope of 53 degrees. This is measured from government topographical maps from creek level to the top of Red Bluff. This slope appears to be quite stable with a negligible talus slope at its base. Using this information as a guideline it is assumed a 55 degree highwall will be obtainable. The ultimate highwall slope will be subject to detailed geotechnical studies. The highwall angle will be obtained by mining to 10 meter benches for a total height of 20 meters. The 20 meter benches will be separated by an 8.65 meter berm. The internal bench angle will be 75 degrees (see Figures 3-8 and 3-9). If geotechnical field work indicates a steeper highwall is obtainable, the design criteria may be changed. This would result in an increase in mineable ore and a decrease in prestrip waste.

Preliminary geotechnical work carried out during the spring of 1995 indicates that the majority of structures appear to be dipping into the hillside, with one occasional set being near horizontal. This orientation will have to be confirmed at a later date with a core orientation drill hole. No information is yet available on the pore pressure of the highwall, however none of the existing diamond drill holes are making water.

The high wall will not contain any portion of the original pit access road. Due to the nature of the pit access road design, berms will likely be inaccessible after a short period of time. This may result in special procedures to work under berms which may become cluttered with material, or a small cat trail may be required to access berms for cleaning.

A working bench height of 10 meters has been selected. Due to the unique mineability of the deposit and projected short hauls, relatively small open pit equipment will be utilized. With the internal ore pass system in the pit the longest haul is projected to be 500 meters resulting in short cycle times.





Approximate Mean Declination  
1991  
for Centre of Map  
Decreasing 12.6' Annually

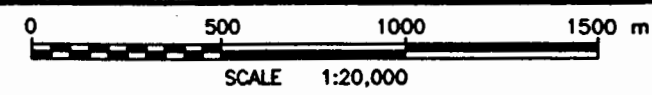
**LEGEND**

- Pit Access Road
- Pit Outline

INTERNATIONAL SKYLINE GOLD CORPORATION

Bronson Slope Gold, Copper Porphyry

**SITE PLAN  
with MAJOR FACILITIES**








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DATE: 5/11/95	NTS: 1048/11	<b>3-2</b>




Assay Composites

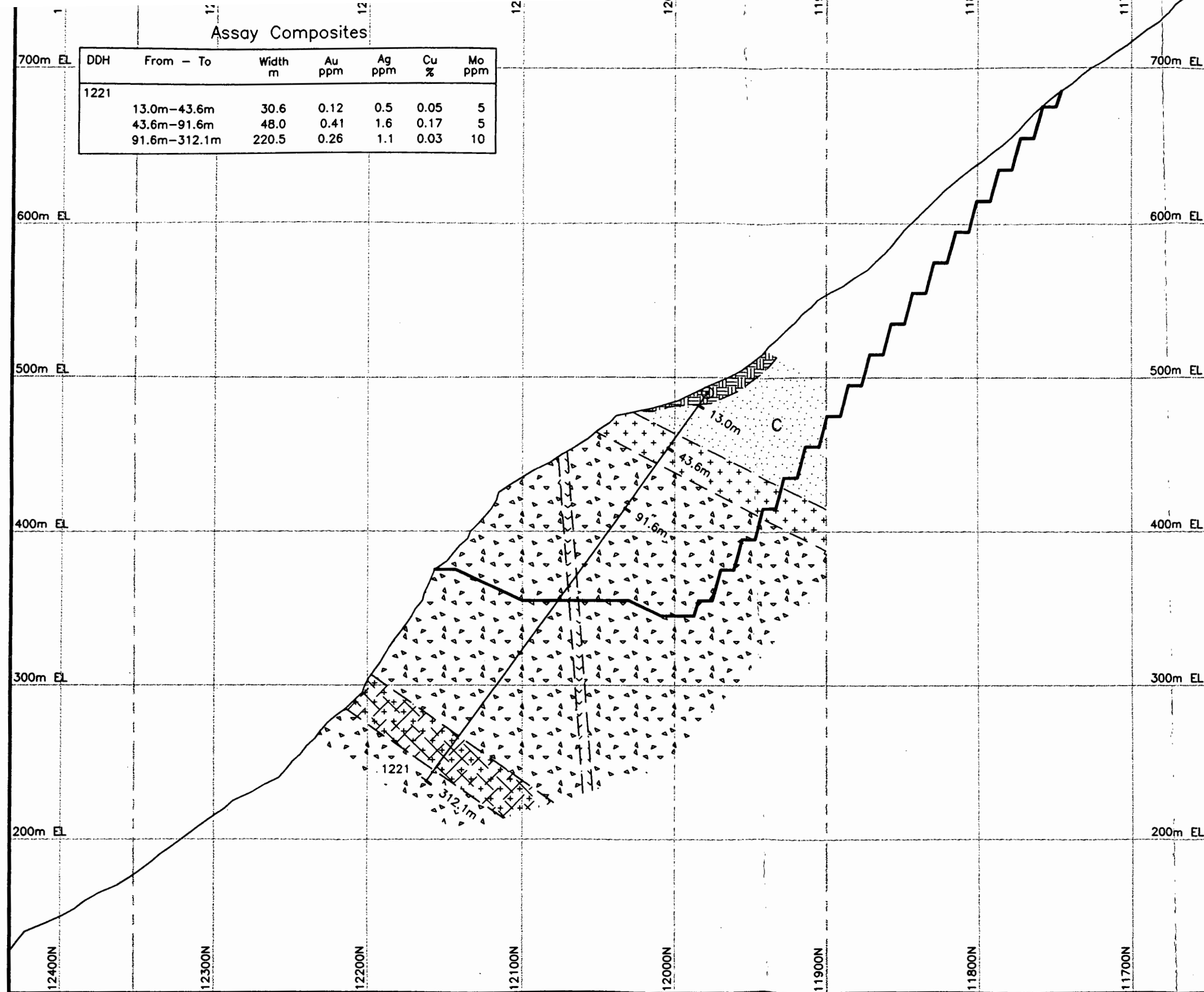
DDH	From - To	Width m	Au ppm	Ag ppm	Cu %	Mo ppm
1221	13.0m-43.6m	30.6	0.12	0.5	0.05	5
	43.6m-91.6m	48.0	0.41	1.6	0.17	5
	91.6m-312.1m	220.5	0.26	1.1	0.03	10

LEGEND

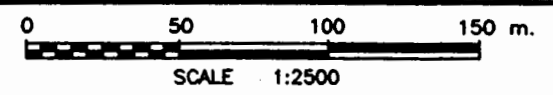
- LITHOLOGY
-  Dyke
  -  Quartz Magnetite Replacement &/or Breccia
  -  Quartz Magnetite Stockwork after Previous Rock Types
  -  Red Bluff Porphyry intrusive
  -  Sedimentary Rocks
    - U - undifferentiated
    - A - Biotite carbonate alteration
    - B - Biotite chlorite hornfels
    - C - Potassium feldspar alteration

SYMBOLS

-  Drill Hole Trace
-  Pit Outline
-  Claim Boundary



INTERNATIONAL SKYLINE GOLD CORPORATION  
 Bronson Slope Gold, Copper Porphyry  
 Cross Section 25125 E  
 Looking Grid East (115° 12' 22" True)  
 Geology and Assay Composites



DRAWN: C.M.T. / D.Y.	Filename: Fig3-3.dwg	Figure
DATE: 5/11/95	NTS: 104B/11	<b>3-3</b>

**LEGEND**

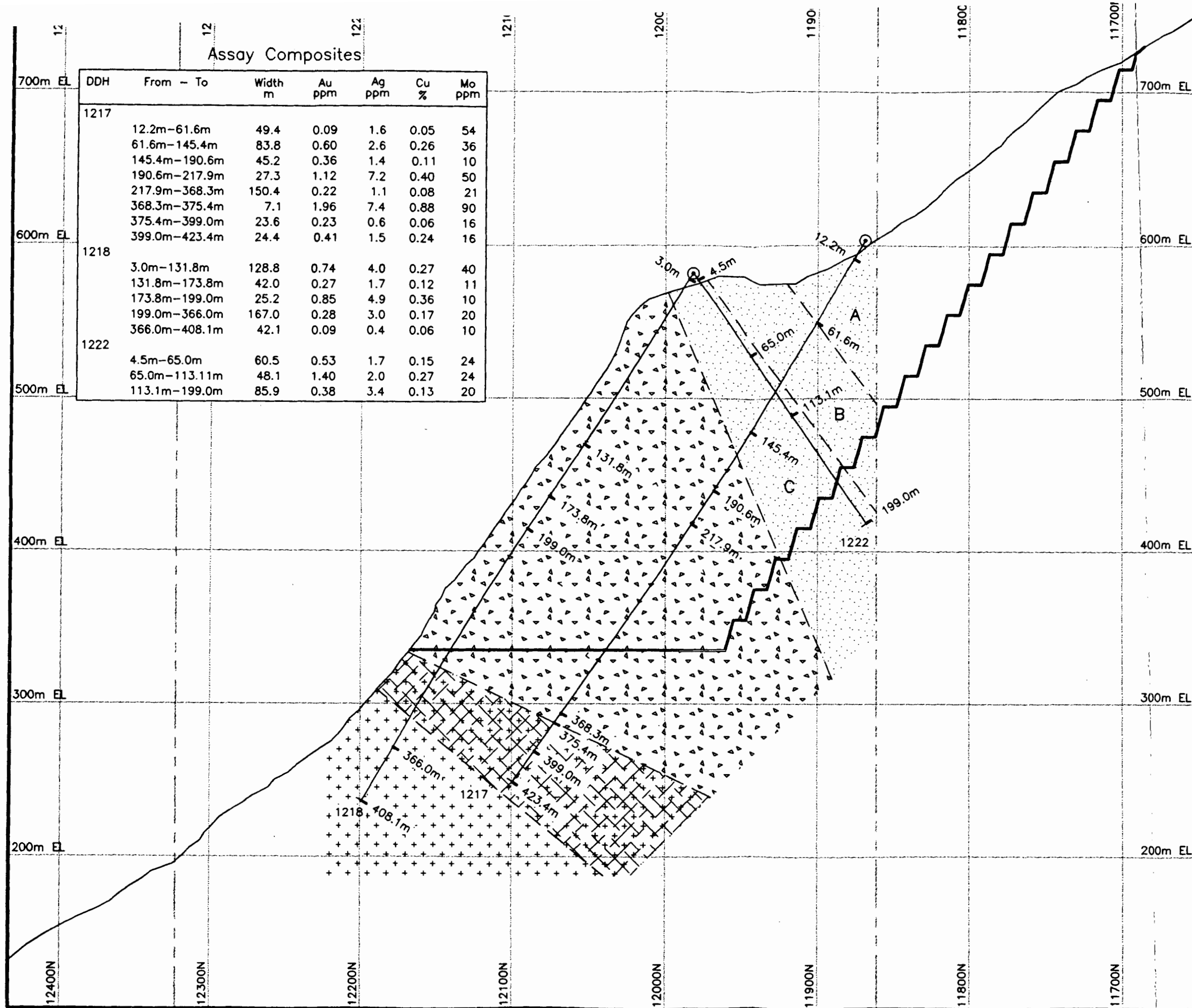
- LITHOLOGY**
- Dyke
  - Quartz Magnetite Replacement &/or Breccia
  - Quartz Magnetite Stockwork after Previous Rock Types
  - Red Bluff Porphyry intrusive
  - Sedimentary Rocks**
    - U - undifferentiated
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    - C - Potassium feldspar alteration

**SYMBOLS**

- Drill Hole Trace
- Pit Outline
- Claim Boundary

**Assay Composites**

DDH	From - To	Width m	Au ppm	Ag ppm	Cu %	Mo ppm
1217	12.2m-61.6m	49.4	0.09	1.6	0.05	54
	61.6m-145.4m	83.8	0.60	2.6	0.26	36
	145.4m-190.6m	45.2	0.36	1.4	0.11	10
	190.6m-217.9m	27.3	1.12	7.2	0.40	50
	217.9m-368.3m	150.4	0.22	1.1	0.08	21
	368.3m-375.4m	7.1	1.96	7.4	0.88	90
1218	3.0m-131.8m	128.8	0.74	4.0	0.27	40
	131.8m-173.8m	42.0	0.27	1.7	0.12	11
	173.8m-199.0m	25.2	0.85	4.9	0.36	10
1222	4.5m-65.0m	60.5	0.53	1.7	0.15	24
	65.0m-113.1m	48.1	1.40	2.0	0.27	24
	113.1m-199.0m	85.9	0.38	3.4	0.13	20



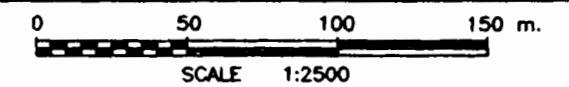
INTERNATIONAL SKYLINE GOLD CORPORATION

Bronson Slope Gold, Copper Porphyry

Cross Section 25375 E

Looking Grid East (115° 12' 22" True)

Geology and Assay Composites



DRAWN: C.M.T. / D.Y.

Filename: Fig3-4.dwg

Figure

DATE: 5/11/95

NTS: 104B/11

**3-4**

# ACID-BASE ACCOUNTING

Sample ID	Rock Type	Paste pH	S(Total) %	S(SO4) %	AP kg/t	NP kg/t	NNP kg/t	NP/AP -	CO2 %	CO2 kg/t
Hangingwall Waste										
2647	K-sp hornfels	9.1	0.71	0.02	22	27	5	1.22	1.0	23
2652	K-sp hornfels	9.3	0.67	0.01	21	14	-7	0.67	0.2	5
2654	Quartz diorite	9.1	0.75	0.01	23	15	-8	0.64	0.7	16
2656	Quartz diorite	9.4	0.20	0.01	6	18	12	2.88	0.3	7

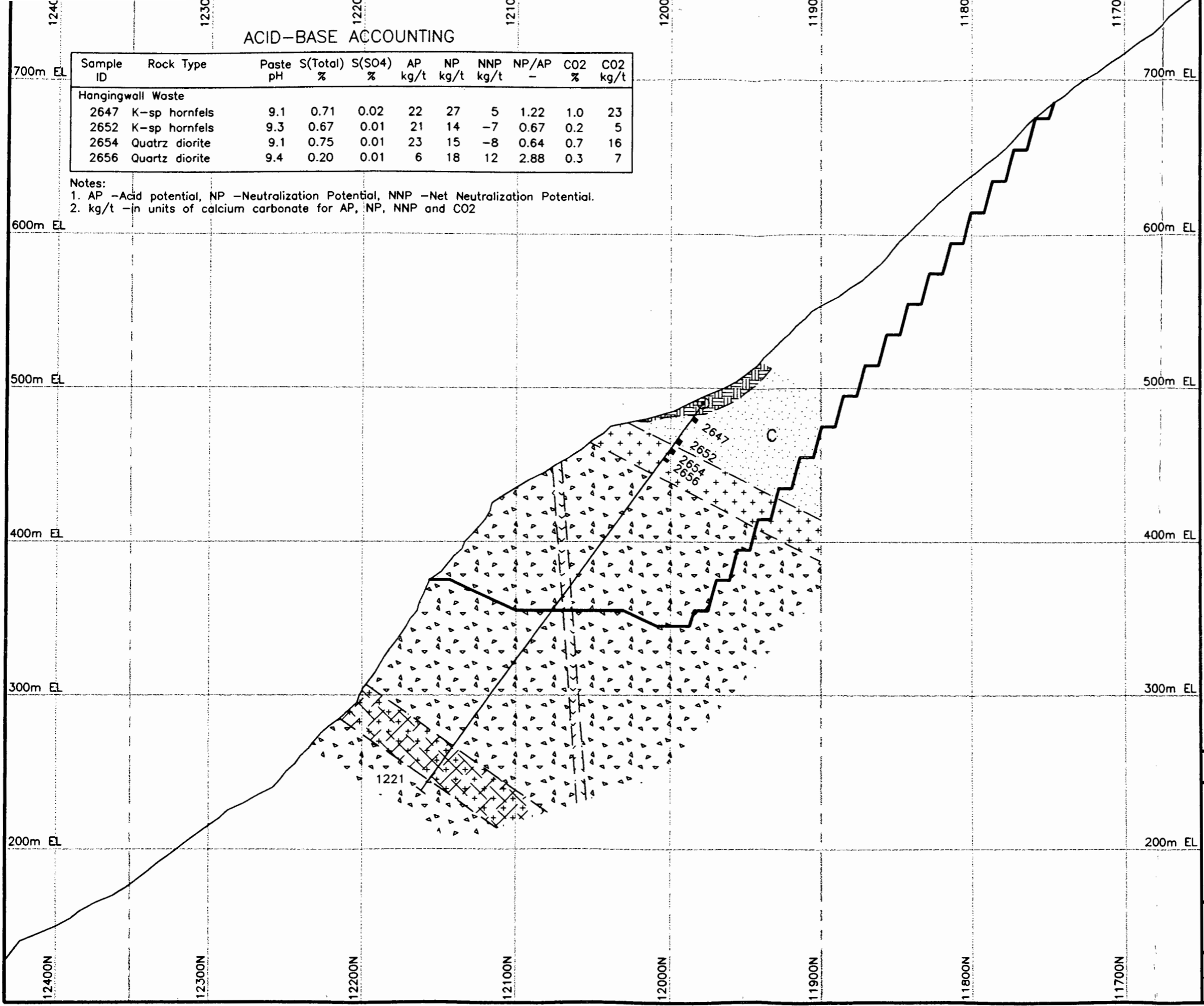
Notes:  
 1. AP -Acid potential, NP -Neutralization Potential, NNP -Net Neutralization Potential.  
 2. kg/t -in units of calcium carbonate for AP, NP, NNP and CO2

## LEGEND

- LITHOLOGY**
- Dyke
  - Quartz Magnetite Replacement &/or Breccia
  - Quartz Magnetite Stockwork after Previous Rock Types
  - Red Bluff Porphyry intrusive
  - Sedimentary Rocks**
    - U - undifferentiated
    - A - Biotite carbonate alteration
    - B - Biotite chlorite hornfels
    - C - Potassium feldspar alteration

## SYMBOLS

- Drill Hole Trace
- Pit Outline
- Claim Boundary
- Aba Sample



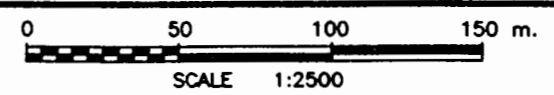
INTERNATIONAL SKYLINE GOLD CORPORATION

Bronson Slope Gold, Copper Porphyry

Cross Section 25125 E

Looking Grid East (115° 12' 22" True)

Geology and Aba Samples



DRAWN: C.M.T. / D.Y.

Filename: Fig3-5.dwg

Figure

DATE: 5/11/95

NTS: 104B/11

**3-5**

# ACID-BASE ACCOUNTING

Sample ID	Rock Type	Paste pH	S(Total) %	S(SO4) %	AP kg/t	NP kg/t	NNP kg/t	NP/AP -	CO2 %	CO2 kg/t
<b>Hangingwall Waste</b>										
2251	Carb-bi-hornfels	8.7	2.68	0.01	84	78	-6	0.93	2.9	66
2253	Carb-bi-hornfels	8.7	3.04	0.01	95	92	-3	0.97	3.6	82
2259	Carb-bi-hornfels	8.6	3.64	0.01	114	146	32	1.28	5.8	132
2263	Carb-bi-hornfels	9.0	2.17	0.01	68	78	10	1.15	2.8	64
2267	Carb-bi-hornfels	8.9	1.49	0.02	47	73	26	1.57	2.6	59
<b>Pit Backwall</b>										
2279	Bi-chl hornfels	9.3	0.92	0.01	29	25	-4	0.87	0.8	18
2303	K-sp hornfels	8.5	0.87	0.01	27	8	-19	0.29	0.3	7
2323	Q-Mag replacement	8.1	3.54	0.02	111	90	-21	0.81	4.0	91
2336	Q-Mag replacement	8.5	0.86	0.01	27	26	-1	0.97	1.3	30

**Notes:**

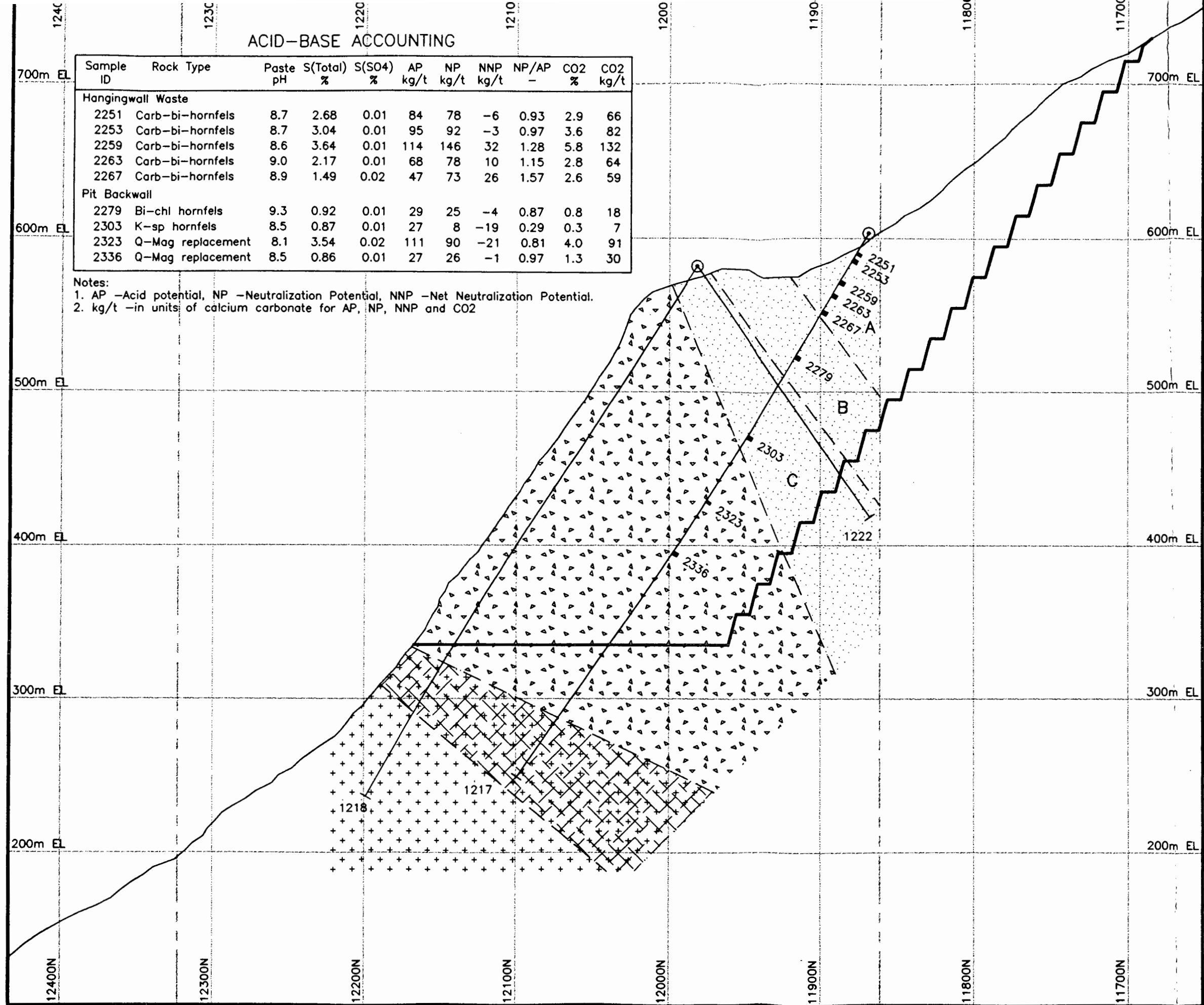
1. AP -Acid potential, NP -Neutralization Potential, NNP -Net Neutralization Potential.
2. kg/t -in units of calcium carbonate for AP, NP, NNP and CO2

## LEGEND

- LITHOLOGY**
- Dyke
  - Quartz Magnetite Replacement &/or Breccia
  - Quartz Magnetite Stockwork after Previous Rock Types
  - Red Bluff Porphyry intrusive
  - Sedimentary Rocks
    - U - undifferentiated
    - A - Biotite carbonate alteration
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    - C - Potassium feldspar alteration

**SYMBOLS**

- Drill Hole Trace
- Pit Outline
- Claim Boundary
- Aba Sample



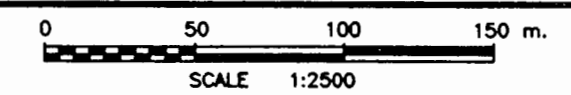
INTERNATIONAL SKYLINE GOLD CORPORATION

Bronson Slope Gold, Copper Porphyry

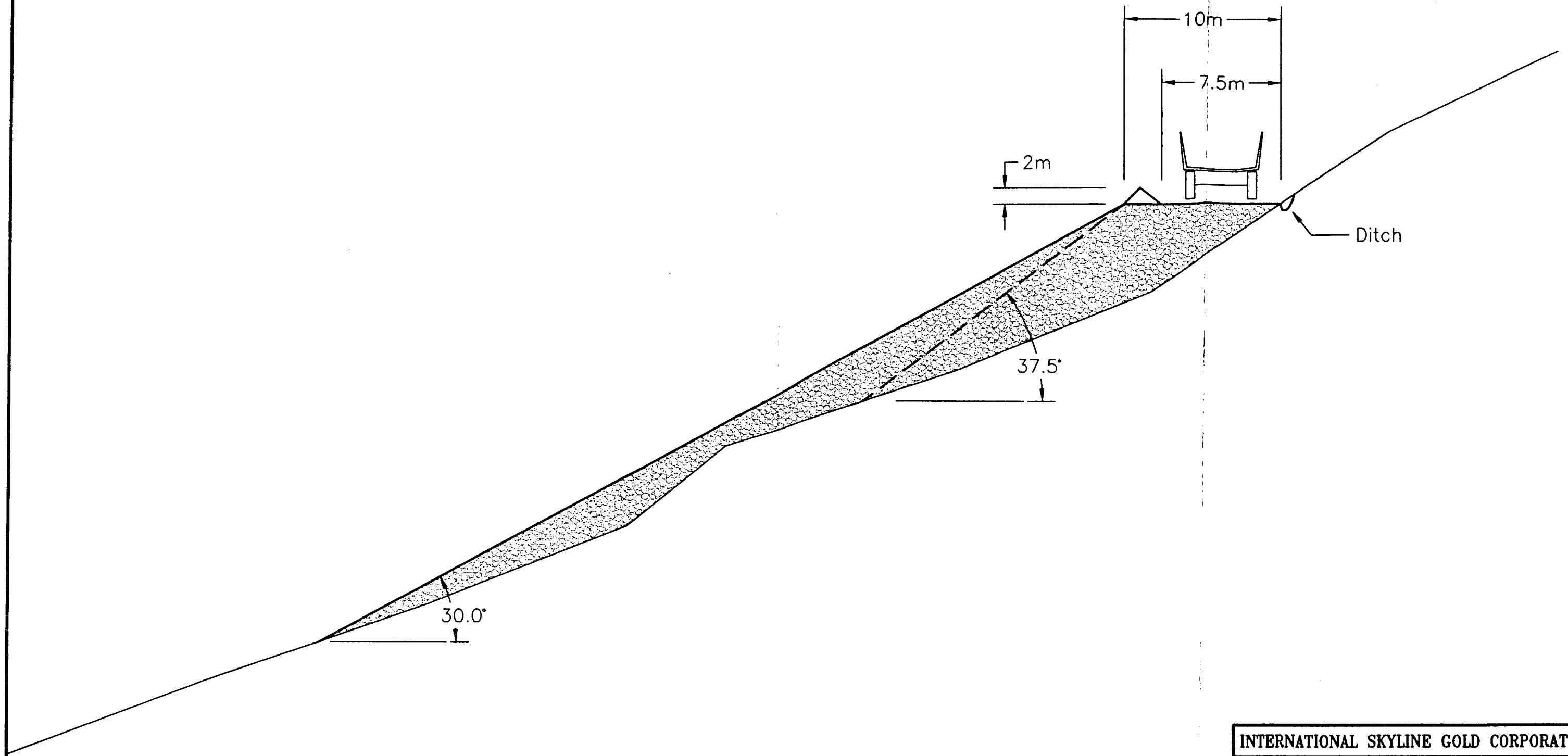
Cross Section 25375 E

Looking Grid East (115° 12' 22" True)

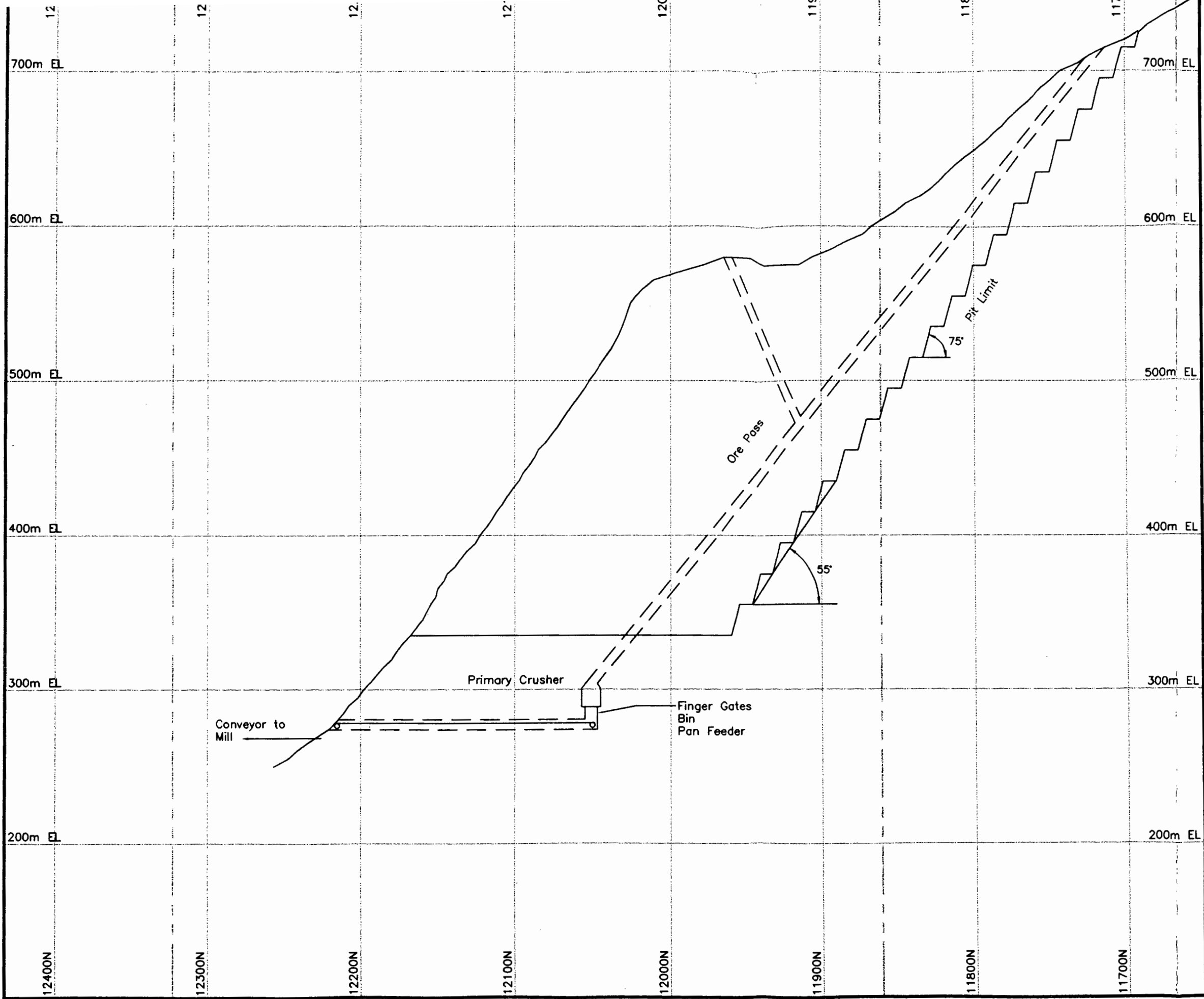
Geology and Aba Samples



DRAWN: C.M.T. / D.Y.	Filename: Fig3-6.dwg	Figure
DATE: 5/11/95	NTS: 104B/11	<b>3-6</b>



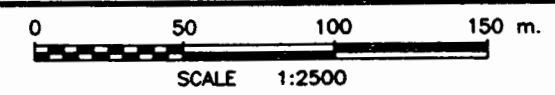
INTERNATIONAL SKYLINE GOLD CORPORATION		
Bronson Slope Gold, Copper Porphyry		
Cross Section 26000 E		
Looking Grid East		
Typical Fill Section		
SCALE 1:250		
DRAWN: C.M.T. / D.Y.	Filename: Fig3-7.dwg	Figure
DATE: 5/11/95	NTS: 104B/11	<b>3-7</b>



**LEGEND**

----- Claim Boundary

**INTERNATIONAL SKYLINE GOLD CORPORATION**  
**Bronson Slope Gold, Copper Porphyry**  
**Cross Section 25375 E**  
 Looking Grid East (115° 12' 22" True)  
**Conceptual Ore Pass & Conveyor**  
**System and Highwall Angles**

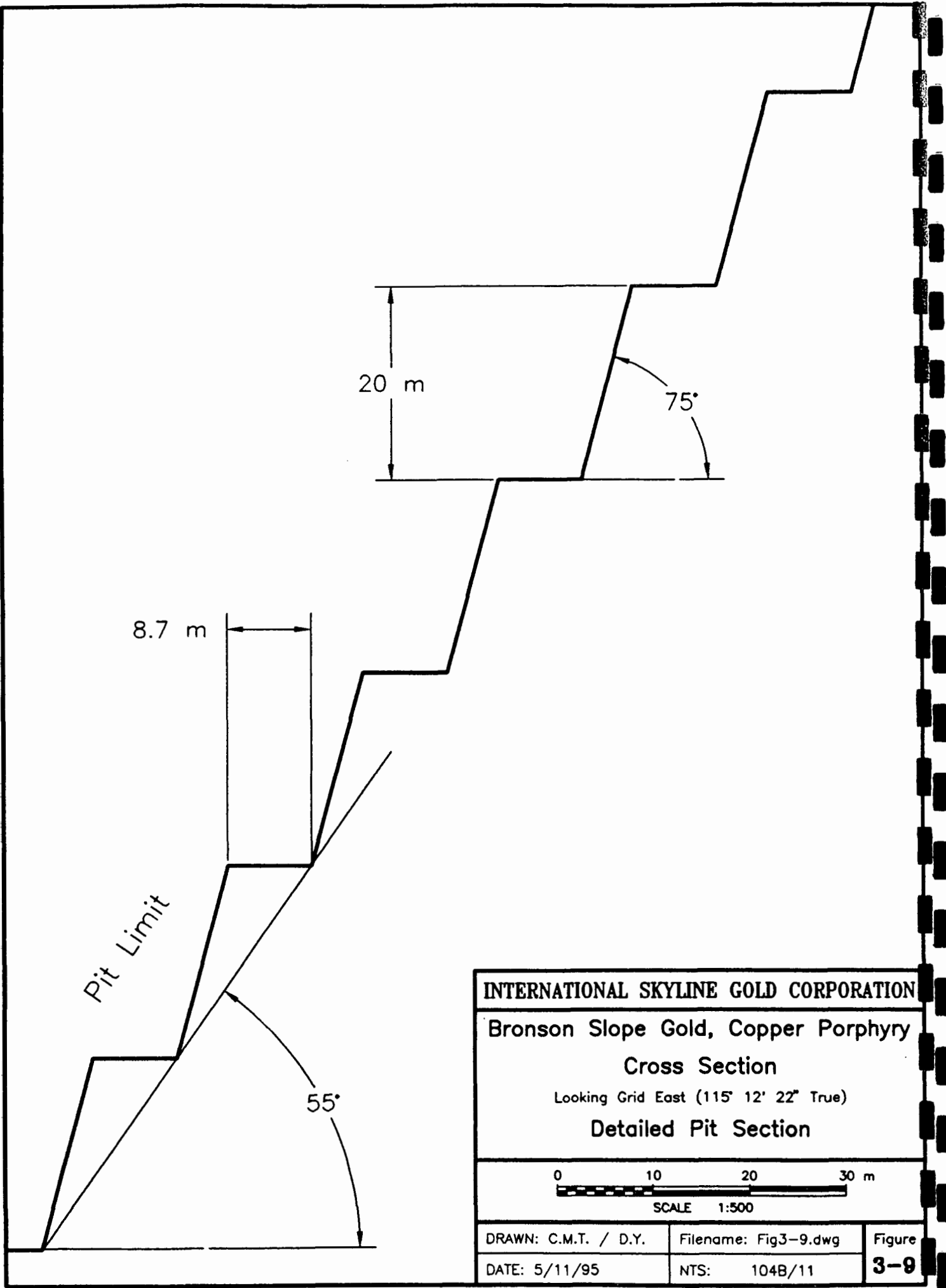


DRAWN: C.M.T. / D.Y.	Filename: Fig3-8.dwg	Figure
DATE: 5/11/95	NTS: 1048/11	<b>3-8</b>

**TABLE 3-1  
PROGRESSIVE STRIP RATIOS**

<b>Bench Elevation</b>	<b>Ore Tonnes</b>	<b>Waste Tonnes</b>	<b>Strip Ratio</b>	<b>Cumulative Ore</b>	<b>Cumulative Waste</b>	<b>Cumulative Strip Ratio</b>
710	0	136,246	0.00	0	136,246	0.00
700	0	318,531	0.00	0	454,777	0.00
690	0	338,544	0.00	0	793,321	0.00
680	0	489,190	0.00	0	1,282,511	0.00
670	0	528,146	0.00	0	1,810,657	0.00
660	0	643,146	0.00	0	2,453,803	0.00
650	0	635,192	0.00	0	3,088,995	0.00
640	0	739,911	0.00	0	3,828,906	0.00
630	0	720,642	0.00	0	4,549,548	0.00
620	0	825,162	0.00	0	5,374,710	0.00
610	0	806,727	0.00	0	6,181,437	0.00
600	0	921,224	0.00	0	7,102,661	0.00
590	0	951,875	0.00	0	8,054,536	0.00
580	0	951,875	0.00	0	9,006,412	0.00
570	827,216	495,853	0.60	827,216	9,502,265	11.49
560	1,320,796	316,859	0.24	2,148,011	9,819,123	4.57
550	1,479,258	248,137	0.17	3,627,269	10,067,260	2.78
540	1,769,642	137,233	0.08	5,396,911	10,204,494	1.89
530	1,777,169	173,265	0.10	7,174,079	10,377,758	1.45
520	2,135,339	0	0.00	9,309,418	10,377,758	1.11
510	2,025,978	186,837	0.09	11,335,396	10,564,595	0.93
500	2,020,083	418,161	0.21	13,355,479	10,982,756	0.82
490	2,186,716	252,844	0.12	15,542,195	11,235,600	0.72
480	2,192,583	404,047	0.18	17,734,778	11,639,646	0.66
470	2,259,326	328,356	0.15	19,994,104	11,968,002	0.60
460	2,356,270	358,408	0.15	22,350,374	12,326,410	0.55
450	2,687,198	0	0.00	25,037,572	12,326,410	0.49
440	2,784,697	26,648	0.01	27,822,269	12,353,058	0.44
430	2,792,283	0	0.00	30,614,552	12,353,058	0.40
420	2,793,196	150,329	0.05	33,407,748	12,503,387	0.37
410	2,868,108	0	0.00	36,275,856	12,503,387	0.34
400	3,045,759	11,888	0.00	39,321,616	12,515,275	0.32
390	2,315,484	773,394	0.33	41,637,100	13,288,669	0.32
380	2,995,181	423,997	0.14	44,632,281	13,712,666	0.31
370	2,706,261	748,682	0.28	47,338,542	14,461,348	0.31
360	2,613,216	1,080,397	0.41	49,951,758	15,541,745	0.31
350	3,249,972	465,364	0.14	53,201,730	16,007,109	0.30
340	3,527,066	340,331	0.10	56,728,796	16,347,440	0.29





INTERNATIONAL SKYLINE GOLD CORPORATION		
Bronson Slope Gold, Copper Porphyry		
Cross Section		
Looking Grid East (115° 12' 22" True)		
Detailed Pit Section		
SCALE 1:500		
DRAWN: C.M.T. / D.Y.	Filename: Fig3-9.dwg	Figure
DATE: 5/11/95	NTS: 104B/11	<b>3-9</b>

### 3.2.4 Ore and Waste Movement

Ore and waste will be removed from the open pit via a twin internal ore pass system to the valley bottom. An underground crusher will be located at the bottom of the ore pass system. Ore will be transferred from the crusher to a gravity conveyor for transport to the ore stockpile or the waste storage facility. The ore stockpile will be a live pile. The pile will be used when the fine ore bin is full, and is not planned as a long term storage facility. It is possible that a low grade stockpile will be located on the site. The exact location and size is yet to be determined. The low grade stockpile will be a function of economics.

Waste material will likely be divided into two categories, potential acid generating and acid consuming. All waste material considered to be acid generating will be disposed of in the tailings facility. Waste material considered acid consuming will be used for construction material, and road surfacing during the life of the mine, including the tailings pond dikes. A detailed description of the tailings disposal plan is outlined in Appendix 3-1.

All material within the pit will be moved by conventional truck and shovel operations to the internal ore pass system. Rubber tire loaders may be used in lieu of a shovel and trucks during the early years of operation. This may be possible due to the extremely short hauls that will be realized during the first 3 years of operation. All mobile open pit equipment will be diesel powered.

### 3.2.5 Ore Pass and Conveyor System

The internal ore pass system will consist of a twin ore pass system within the centroid of the pit. The ore pass system will converge at the bottom of the pit to a central underground crushing facility (Figure 3-6). The ore/waste will be crushed and transferred to either the mill facility for processing or to a waste storage facility.

The pass within the pit area will be kept approximately 2 meters above bench elevation to prevent excessive water flow down the pass, and as a safety barrier to personnel and equipment. A grizzly will be placed on top of the ore pass system to prevent oversize material from entering the pass and causing hang-ups. A mobile rock breaker will be located in the pit area to deal with oversize. The twin system will be required to allow continued access to a pass at all times during operations either for bench development, or during times of material hang-ups.

An inclined horizontal tunnel will be developed to the mill facility. This will allow a positive generation conveyor to be used. The conveyor system will be designed to allow for ore to be delivered to the mill facility, or for waste material to be delivered to the waste storage facility.

### **3.2.6 Drilling and Blasting**

Drilling will be carried out utilizing large diameter rotary drills (127 mm - 254 mm). A smaller sized rotary percussion drill may be required for controlled blasting along the highwall and for opening the ore pass from bench to bench.

Blasting will be carried out utilizing ammonia nitrate based explosives and blasting agents. Specialized explosives may be required for highwall blasting control and for opening of the ore pass from bench to bench. It is anticipated a bulk explosives facility will be located on site, which will supply the mine with both ANFO and slurry type explosives for use in the pit. The bulk explosives facility will meet Federal and Provincial Explosive Guidelines.

Blasting will be carried out using a non-electric system utilizing both surface and down hole delays. Some consideration may have to be given to blast size due the close proximity of the camp facilities to the open pit. Blasting procedures will meet B.C. Mine Health and Safety Regulations.

### **3.2.7 Waste Rock Disposal**

Waste rock disposal will be in the acid consuming rougher (flotation) tailings cell of the tailings impoundment. Rock, once shown to be non-acid generating, may be used for construction purposes. Waste rock disposal is discussed in more detail in Section 3.4.2.

### **3.2.8 Mining Alternatives**

Given the configuration of the deposit and economics of mining, there are no viable alternatives to the proposed mining method. The deposit is near surface on a relatively steep slope and is not amenable to underground mining which produces less surface disturbance than open pit. The total disturbance from the pit for the projected mine life of 15 years will be 51.9 ha, or 23% of the total projected disturbance.

## **3.3 Mill**

### **3.3.1 Conceptual Design**

In order to accommodate the large tonnage requirements of the Bronson Slope Porphyry deposit a new high tonnage mill facility will have to be constructed. The new facility is designed to process 12,000 mtpd of ore grade material. An exact location for this facility has not yet been isolated, however it is anticipated that it will be located in the vicinity of the existing Snip site, on the Bronson Creek alluvial fan.

The location of the mill facility will be subject to geotechnical constraints, ore stockpile locations, location of the ore transport conveyor with respect to the deposit, and tailings location. Concentrate storage will be required on site. The amount of concentrate stored on site would be a minimal amount to keep slightly ahead of the transportation to Stewart.

A detailed report and mill facility plans are available in Appendix 3-2.

Conceptual design as of spring 1995 was for installation of a semi-autogenous grind (SAG) - ball mill grinding circuit with a capacity of 12 000 tonnes per day of ore. Milling will be followed by conventional gravity concentration and flotation circuits to produce a copper concentrate with recoverable molybdenum. The copper concentrate will be further treated to recover a separate molybdenum concentrate. The final copper concentrate will be dewatered using conventional thickening and filtration; all process water will be recycled.

Gravity concentration following milling will be used to recover a portion of the free gold. Flotation, using a bulk rougher and scavenger stages followed by a regrind and three stages of cleaning, will follow to recover much of the remaining gold, silver, copper and molybdenum.

In the future, magnetite may be recovered from the rougher flotation tailings using a wet drum magnetic separator. Cyanide leaching of ore is not contemplated at this time.

Process flow sheets are shown in Appendix 3-2.

### 3.3.2 Metallurgy

Information in this section was obtained from Process Research Assoc. Ltd. (1995) and is based on four samples of soft, hard, composite (normal grade), and composite low grade ore.

The main copper mineral in the Bronson Slope ore is chalcopyrite, with minor covellite, tetrahedrite and native copper. Molybdenum occurs as molybdenite. Pyrite is the most abundant sulphide gangue mineral, together with minor sphalerite and galena. Gold and silver occur mostly associated with copper sulphide minerals with a minor amount of free gold.

Processing will be carried out by floating the sulphides using reagents that are selective toward the copper minerals. A copper concentrate is produced by re-grinding the rougher product, adding reagents to depress pyrite and selectively floating the copper. Molybdenum is separated from the concentrate by depressing the chalcopyrite and floating the molybdenite. Precious metals (gold and silver) are

recovered with the copper product; free gold is recovered by initial gravity concentration.

Microscopic examination of pilot-scale rougher tailings revealed only trace amounts of pyrite and chalcopyrite, thus indicating almost complete sulphide flotation was achieved.

Copper cleaning flotation will follow and is directed at producing a high grade copper concentrate by rejecting pyrite while maintaining high copper, gold, silver and molybdenum recoveries. After initial bulk sulphide float, the concentrate will be reground and sodium cyanide, lime and flotation collector A208 added to selectively depress the pyrite and improve recovery.

Microscopic examination of pilot-scale cleaner tailings and concentrate showed almost complete liberation of chalcopyrite from pyrite.

Molybdenite is naturally hydrophobic, floats with the copper and reports to the copper concentrate. To separate molybdenum from copper, copper minerals will be depressed by maintaining a reducing environment with the addition of sulphur dioxide gas or sodium hydrosulphide and floating under anoxic conditions maintained with nitrogen gas. Molybdenum flotation will be enhanced by the addition of oil as a collector.

### 3.3.3 Process Chemical Use

Mill reagents will include the following: lime, PAX (copper collector), A208 (flotation promoter), methyl isobutyl carbanol (MIBC) (frother), fuel oil (molybdenum collector), sodium bi-sulphide (copper depressant), nitrogen gas (molybdenum flotation), sodium cyanide (pyrite depressant). Table 3-2 lists reagents and quantities required.

**TABLE 3-2  
MILL REAGENT USE**

<b>Reagent</b>	<b>Use/Tonne of Ore (g)</b>	<b>Daily Consumption (kg)</b>
Lime	127	1524
PAX	10	120
A208	9	108
MIBC	53	636
S5100	2	24
Sulphuric Acid	196	2352
Sodium cyanide	10	120

### 3.4 Waste Management Plan

#### 3.4.1 Tailings Disposal

The tailings from the Bronson Slope deposit will be disposed of in a conventional tailings dam type facility located on the Jim and Sky 3 claim area. A detailed description of the tailings facility location, volumes, and possible creek diversions are described in a report prepared by Robert C. Dick, P. Eng. in Appendix 3-1.

The tailings are expected, on average, to be acid generating. Segregation of tailings into acid consuming rougher tails and acid generating scavenger tailings is planned. On closure the rougher tailings impoundment will be covered capped with neutral or alkaline tailings, if necessary and the surface stabilized to prevent erosion. Scavenger tailings will be permanently flooded. Reclamation is discussed further in Section 5.9

##### 3.4.1.1 Acid-Base Accounting and Metals Leaching

The following information was obtained from Process Research Associates Ltd. (1995) tests.

Samples of normal grade composite and flotation tailings were subjected to acid-base accounting (ABA) and inductively coupled argon plasma (ICP) analyses. Tailings samples were produced from lock-cycle pilot scale tests by Process Research Associates Ltd. A multi-element ICP metals analysis was also performed on samples of rougher and cleaner scavenger flotation tailings water. Results are summarized in Tables 3-3 and 3-4.

The metals concentrations in the feed and tailings were quite low. The sulphur content of the feed (2%) produced a negative net neutralization potential of -19.8 kg CaCO<sub>3</sub>/t (NP:AP=0.68). Removal of sulphide minerals during flotation causes the rougher tails to have a negligible sulphur (0.03%) and a positive net neutralizing potential of 36.7 kg CaCO<sub>3</sub>/t. The cleaner tailings contained 67% pyrite or 24.6% sulphur resulting in a net neutralizing potential of -729 kg CaCO<sub>3</sub>/t. Rougher tailings will account for 94.5% of the flotation waste and the cleaner scavenger tailings for 5.5%. The presence of 6% carbonate minerals in the rougher tailings provided some neutralization potential to the combined rougher and cleaner flotation tailings. Blended, the two tailings products produced a calculated net neutralization potential of -5.4 kg CaCO<sub>3</sub>/t.

**TABLE 3-3  
SUMMARY OF ENVIRONMENTAL TEST RESULTS FOR COMPOSITE 1, ROUGHER  
TAILINGS AND CLEANER TAILINGS<sup>1</sup>**

<b>Parameter (ppm)</b>	<b>Composite 1</b>	<b>Rougher Tailings</b>	<b>Cleaner Tailings</b>
Mo	50	37	94
Cu	2169	309	1970
Pb	23	6	225
Zn	314	77	146
Ni	31	206	662
Co	10	8	112
Mn	658	618	782
Fe(%)	6.35	4.24	16.00
As	24	<5	77
Cd	2	1.0	5.0
Sb	9	<5	<5
V	46	49	49
Cr	185	374	1019
<b>Acid-Base Accounting</b>			
S <sub>tot</sub> (%)	2.00	0.03	24.6
Paste pH	9.1	8.6	6.6
NP <sup>2</sup> (kg CaCO <sub>3</sub> /t)	42.7	37.6	39.7
MPA <sup>3</sup> (kg CaCO <sub>3</sub> /t)	62.5	0.94	769
NPR <sup>4</sup>	0.68	40.0	0.05
Net NP <sup>5</sup> (kg CaCO <sub>3</sub> /t)	-19.8	36.7	-729

<sup>1</sup> Source: Process Research Associates, 1995

<sup>2</sup> Neutralization Potential

<sup>3</sup> Maximum Potential Acidity

<sup>4</sup> Ratio of Neutralization Potential to Maximum Potential Acidity

<sup>5</sup> Net Neutralization Potential



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**TABLE 3-4  
SUMMARY OF ENVIRONMENTAL TEST RESULTS FOR ROUGHER TAILINGS  
WATER AND CLEANER SCVENGER TAILINGS WATER**

<b>Parameter (mg/L)</b>	<b>Rougher Tailings</b>	<b>Cleaner Tailings</b>
CN <sub>tot</sub>	—	<0.005
Mo	0.06	0.02
Cu	0.05	0.06
Pb	0.13	<0.05
Zn	0.42	2.23
Ag	<0.005	<0.005
Ni	0.18	<0.02
Co	0.01	<0.01
Mn	7.157	0.294
Fe	0.09	0.22
As	<0.05	<0.05
Cd	<0.005	0.011
Ca	189.95	25.79
Mg	13.10	1.08

Note: Total metals analyzed.

Tailings water had relatively low metals concentrations with zinc in the cleaner tailings water at a concentration of 2.23 mg/L. The pH of the rougher tailings water was greater than 8.0 and of the cleaner tailings water, greater than 9.0. Metals levels, are however, higher in concentration than would allow for discharge to the environment undiluted.

#### 3.4.1.2 *Site Topography*

Site topography is shown in Figure 3-10.

The confluence area of Sky Creek with its two tributaries is a relatively wide valley, with steep bedrock sides, and contains an extensive wetland.

At the downstream end of this area is a narrow gap between bedrock slopes, through which Sky Creek drops into a second wetland around the confluence with a stream on the right bank, which drains a small lake.

This lake is surrounded on three sides by steep bedrock slopes, and its water level is controlled by a bedrock ledge across its discharge.

Below this confluence, Sky Creek continues through this second wetland, then drops rapidly through a canyon, in a series of rapids and falls. This canyon is reported to be the upstream limit of salmon in Sky Creek.

#### 3.4.1.3 *Proposed Dam Arrangement*

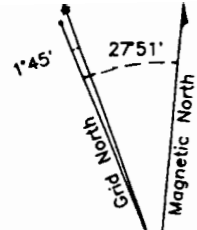
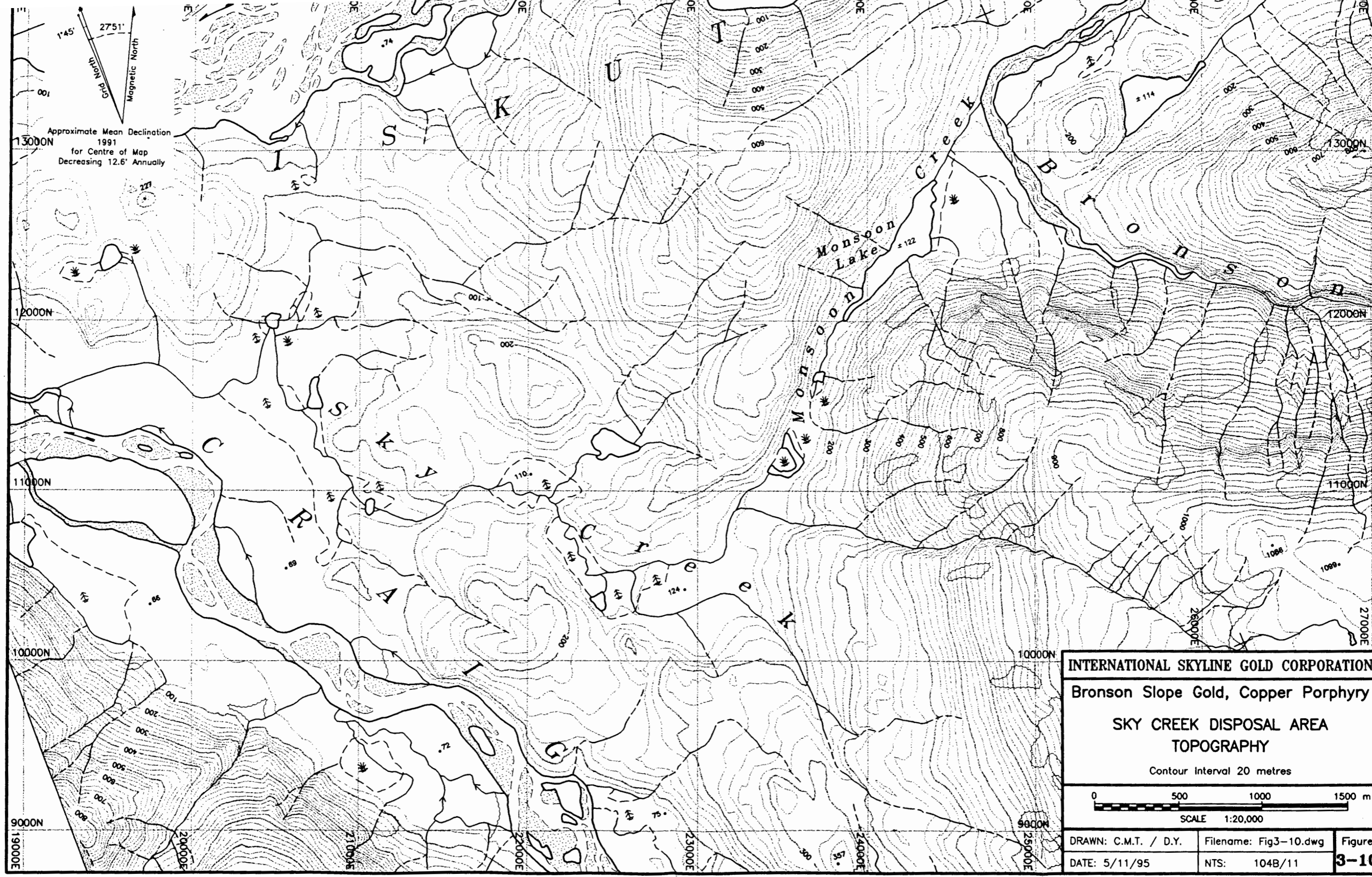
The proposed dam arrangement is shown in Figure 3-11.

In order to provide natural runoff from the Cominco tailings area into the Sky Creek system, Cell "A" has been extended through the Monsoon Creek valley to the head of Monsoon Lake. A dam will be constructed to elev. 180 metres over the existing Cominco dam (crest about elev. 155 metres).

At the downstream end of Cell "A", a main dam, also to elev. 180 metres, will be built. The downstream toe will be located at the narrowest point of the gap between the two wetland areas.

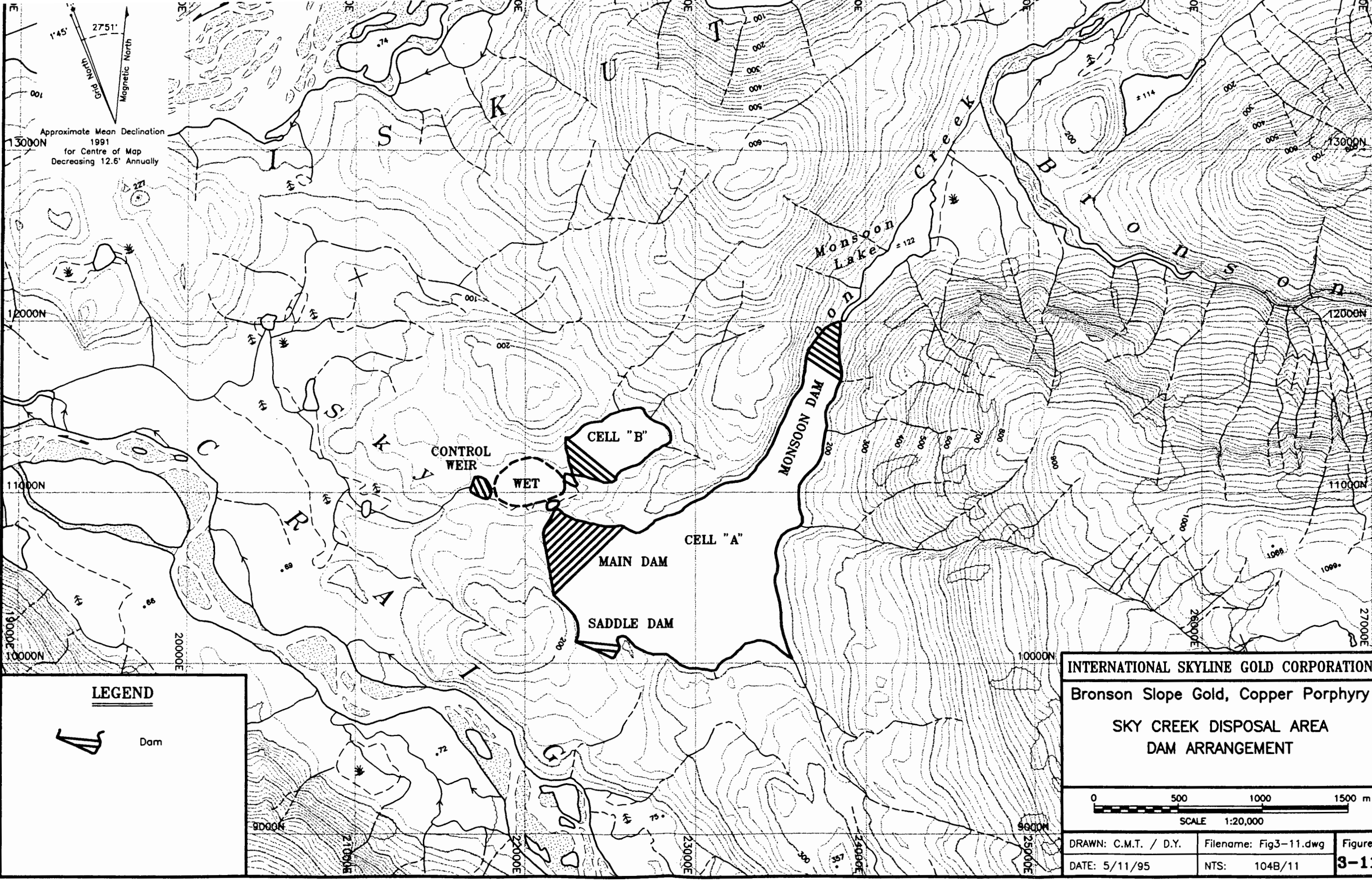
A small dam some 25 metres high will be built across a saddle on the left bank of Cell "A", some 200 metres upstream of the main dam.

These three Cell "A" dams will be built mainly of tailings, using a centreline method of construction similar to that used in other large tailings dams in B.C.



Approximate Mean Declination  
1991  
for Centre of Map  
Decreasing 12.6' Annually

INTERNATIONAL SKYLINE GOLD CORPORATION		
Bronson Slope Gold, Copper Porphyry		
SKY CREEK DISPOSAL AREA TOPOGRAPHY		
Contour Interval 20 metres		
SCALE 1:20,000		
DRAWN: C.M.T. / D.Y.	Filename: Fig3-10.dwg	Figure
DATE: 5/11/95	NTS: 104B/11	<b>3-10</b>



The downstream slopes will have an overall slope of 5H:1V. To provide control of surface erosion, access for maintenance, and staged reclamation throughout the life of the mine, wide benches will be provided every 10 metres of height. Bench slopes will be 3H:1V, and each bench will be 20 metres wide.

The Cell "B" dam must be an engineered, zoned embankment for secure containment of the acid producing tailings and covering water. The downstream slope would be 3H:1V, with bench slopes 2H:1V and 10 metre wide benches every 10 metres of height. The upstream slope would be 2H:1V without berms.

All Cell "A" and "B" dams could be built in staged fashion.

Small containment ponds at the toes of Cell "A" main dam and Cell "B" dam would provide opportunity for sampling and, if necessary, treatment of runoff and seepage.

The remaining wetland downstream of these ponds would provide natural biological treatment of the water. This area would be left undisturbed throughout construction and operation.

At the head of the canyon, a small weir would be built to control water level in the wetland and provide a second opportunity for sampling and treatment.

#### 3.4.1.4 *Diversions and Spillways*

Diversions and spillways are shown in Figure 3-12.

##### *Diversions*

It will be necessary to divert Sky Creek and its two tributaries above elev. 180 metres to prevent water management problems in Cell "A".

It may be found necessary, after commencement of dam construction, to re-introduce the flow to the natural course of Sky Creek downstream of the canyon for fisheries habitat preservation.

The diversion channel would follow a contour above the left bank of Cell "A" to a small saddle at about elev. 155. The channel would then turn away from Cell "A" and pass through this saddle. A side-channel spillway would be built at this point, to allow the desired flow to continue, while discharging excess water down a small streambed directly into the Craig River.

In the relatively flat gap below the saddle dam, at approximately 155 m elevation, a small wetland could be created to partly replace that covered by Cell "A".

If necessary, the diversion channel could then be carried around the small hill near elev. 150 metres. Where it crosses a small stream on the north side of this hill, another side-channel spillway could ensure the required flow in this tributary, in which fish have been observed by others.

Finally, the diversion channel would lead down into a depression on the left bank of Sky Creek just below the canyon. Another wetland and, possibly, a spawning channel could be created at this point of final discharge into the original Sky Creek channel.

### *Spillways*

If conditions permit, the service and emergency spillways from Cells "A" and "B" would be located on the ridge separating the cells. This would permit operation of both spillways from one easily-accessed location.

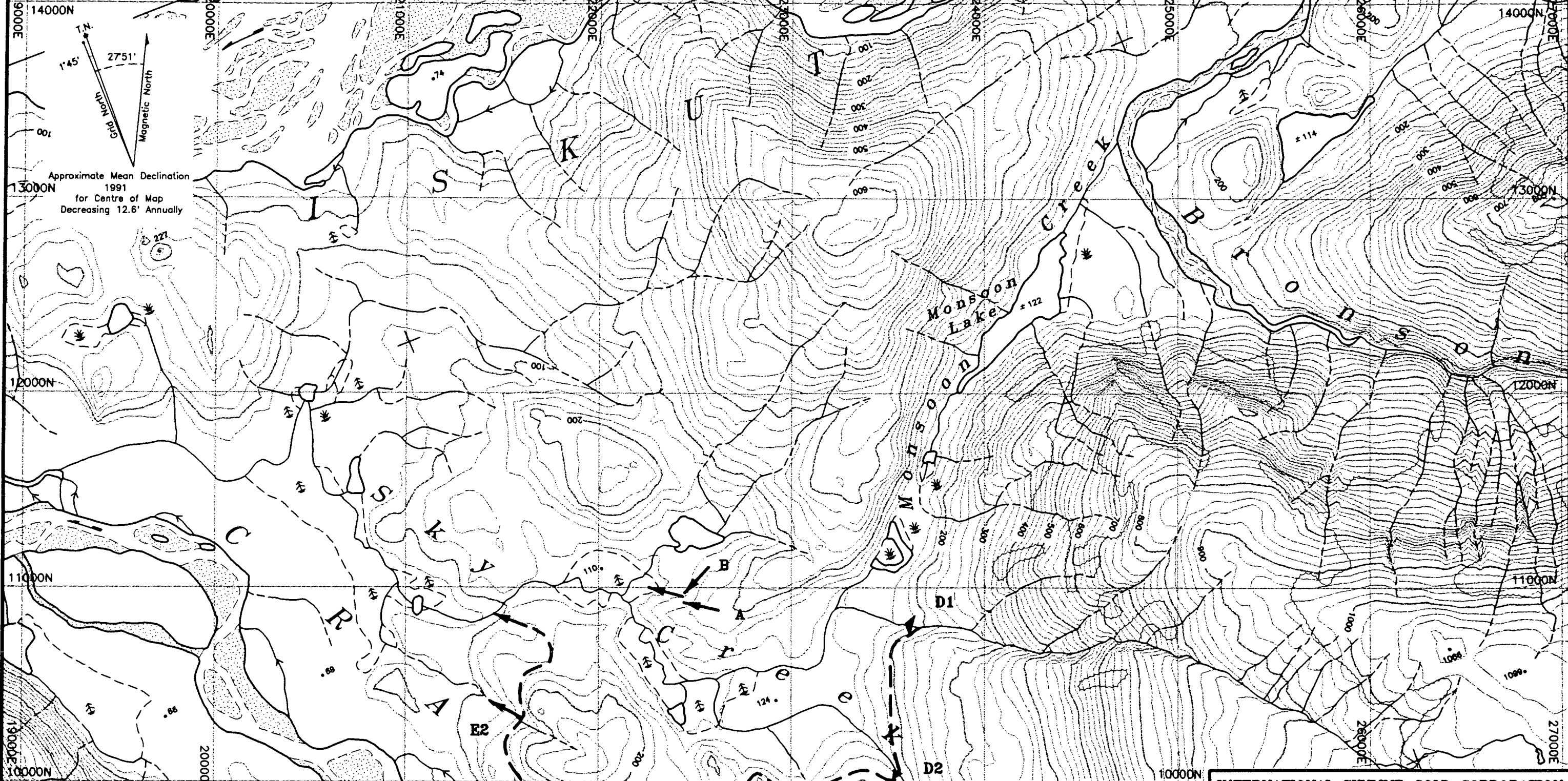
A common chute would carry spilled water down the bedrock hillside and into the wetland. A containment pond for sampling/treatment will be considered at this location, but may not be practical.

The spillway discharge would then flow through the wetland and the sampling/treatment pond at the control weir.

### 3.4.2 Waste Rock Disposal

Development of the waste rock management plan will to a large extent depend on the acid generation potential of the waste rock. Preliminary acid-base accounting (ABA) and metals analyses have been completed to assess acid generation and metal leaching potential in both waste rock and mine walls. The ABA results are summarized in Table 3-5. Figures depicting the locations of the samples and the results are attached in Appendix 3-3.

Assessment of the mineralogy of the deposit by Skyline indicates that the type and occurrence of minerals of relevance to acid generation is fairly simple. The main sulphide mineral is pyrite ( $\text{FeS}_2$ ). No zones of massive or banded mineralization have been encountered to date. The other main sulphide mineral is chalcopyrite ( $\text{CuFeS}_2$ ). No sulphate minerals (such as gypsum) have been reported. This was confirmed by sulphate-sulphur concentrations which are very low.



Approximate Mean Declination  
1991  
for Centre of Map  
Decreasing 12.6' Annually

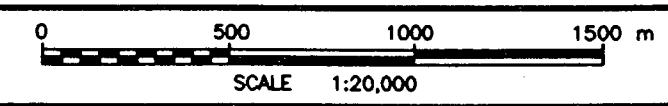
**LEGEND**

- A = Cell "A" Spillway
- B = Cell "B" Spillway
- D1 , D2 , D3 = Sky Creek Diversions
- E1 , E2 = Flood Diversions

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**SKY CREEK DISPOSAL AREA  
DIVERSIONS and SPILLWAYS**



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DATE: 5/11/95	NTS: 104B/11	<b>3-12</b>



**TABLE 3-5**  
**INTERNATIONAL SKYLINE RESOURCES - BRONSON SLOPE PROJECT**  
**ACID-BASE ACCOUNTING**

Sample ID	Rock Type	Paste pH	S(Total) %	S(SO4) %	AP kg/t	NP kg/t	NNP kg/t	NP/AP -	CO2 %	CO2 kg/t
<b><i>Hangingwall Waste</i></b>										
2251	Carb-bi alteration	8.7	2.68	0.01	84	78	-6	0.93	2.9	66
2253	Carb-bi alteration	8.7	3.04	0.01	95	92	-3	0.97	3.6	82
2259	Carb-bi alteration	8.6	3.64	0.01	114	146	32	1.28	5.8	132
2263	Carb-bi alteration	9.0	2.17	0.01	68	78	10	1.15	2.8	64
2267	Carb-bi alteration	8.9	1.49	0.02	47	73	26	1.57	2.6	59
<b><i>Pit Backwall</i></b>										
2279	Bi-chl hornfels	9.3	0.92	0.01	29	25	-4	0.87	0.8	18
2303	K-sp alteration	8.5	0.87	0.01	27	8	-19	0.29	0.3	7
2323	Q-Mag replacement	8.1	3.54	0.02	111	90	-21	0.81	4.0	91
2336	Q-Mag replacement	8.5	0.86	0.01	27	26	-1	0.97	1.3	30
<b><i>Pit Sidewall and Waste</i></b>										
2647	K-sp alteration	9.1	0.71	0.02	22	27	5	1.22	1.0	23
2652	K-sp alteration	9.3	0.67	0.01	21	14	-7	0.67	0.2	5
2654	Quartz diorite	9.1	0.75	0.01	23	15	-8	0.64	0.7	16
2656	Quartz diorite	9.4	0.20	0.01	6	18	12	2.88	0.3	7

Notes:

1. AP - Acid potential, NP - Neutralization Potential, NNP - Net Neutralization Potential.
2. kg/t - in units of calcium carbonate for AP, NP, NNP and CO2.

Comparison of neutralization potential determinations with total inorganic carbon (TIC) indicates that carbonates are the only significant potential acid neutralizers. ISGC has determined that the minerals calcite ( $\text{CaCO}_3$ ) and dolomite ( $\text{CaMg}(\text{CO}_3)_2$ ) are present. This further confirmed by the very strong correlation between neutralization potential and calcium concentrations determined by ICP. The carbonate minerals occur as a biotite carbonate alteration (occasionally schistose) with subordinate chlorite and sericite.

Five samples of hangingwall wall waste (ie waste rock removed to expose the ore zone for mining), described geologically as carbonate-biotite alteration contained between 1.5 and 3.6% total sulphur and neutralization potential between 78 and 146 kg  $\text{CaCO}_3$ /t. Results for the samples are classified as being of uncertain acid generation potential (neutralization potential/acid potential, NP/AP between 0.9 and 1.6).

The pit backwall will be composed of both waste rock and ore-grade material for which removal is uneconomical. For the four samples tested, this rock had lower sulphur concentrations than the hangingwall waste but also lower neutralization potential. The NP/APs for these samples were marginally less than 1.0, implying uncertain potential for acid generation.

The pit sidewalls, and waste removed to slope back the walls had the lowest total sulphur concentrations of any of the samples tested. Relatively, NPs were relatively higher resulting in NP/APs varying from 0.6 to 2.9. Some of this rock may be acid consuming; however, most samples indicated uncertain acid generation potential.

In summary, all rock types are considered to have uncertain acid generation potential. Further evaluation is required. Additional testing will be required to determine the estimated volumes of material that may be stored in a conventional method, and volumes that will require possible subaqueous deposition. The conceptual plan will have non acid generating material stored in a conventional manner. Material required for construction will consist of this rock.

Waste rock with a slight ARD potential will be evaluated for possible blending with non ARD or highly acid consuming material and possible conventional storage. Material determined to have a high ARD potential will be disposed of in the area of tailings facility for the high acid consuming tailings. This waste rock will be surrounded by acid consuming tailings. (an overview description of the tailings facility is described in Appendix 3-1).

### 3.4.3 Mechanical Wastes

The operation of mobile equipment in an isolated area results in waste oils and lubricants being produced on site. Disposal of these special wastes will be handled on site in a manner acceptable to the Ministry of Environment. Waste oil may be

used as a fuel for heat sources provided it meets Section 41 of the Special Waste Regulation. The waste oil may also be used in the production of the Ammonia Nitrate based explosives and Blasting Agents. All other special wastes will be disposed of in an acceptable manner

#### **3.4.4 Refuse Disposal**

A Waste Management Branch permit will be required for the disposal of industrial and putrescible refuse originating from the mine and camp operations. In accordance with permit requirements, putrescible and other burnable wastes will be incinerated daily in order to minimize attraction of nuisance wildlife and reduce refuse volumes.

Industrial refuse and non-burnable wastes will be collected and trucked to a landfill site at the mine. Only waste approved for disposal in this facility will be buried. The landfill site will occupy approximately 1 ha. Granular backfill will be placed around the fill as cells are formed. The landfill area will be ditched to prevent adjacent runoff from entering the pit. The area will be fenced to discourage bears or other large foraging animals.

#### **3.4.5 Other Wastes**

All remaining or special wastes will be disposed of in a manner acceptable to all Ministries involved.

### **3.5 Water Management Plan**

This section deals with the mine area and camp facilities. Diversions and runoff control for the tailings facility are dealt with in the tailings dam section in Appendix 3-1.

#### **3.5.1 Runoff Control and Diversion**

##### **3.5.1.1 Pit Area & Pit Access Road**

The Bronson Slope pit area is going to interfere with water flow from small runoff channels and creeks. A large number of the channels and creeks on Bronson Slope only carry water during spring runoff and during periods of heavy precipitation. All efforts will be made to divert the water courses above the pit area to West Gully to the west or to East Gully to the east. The preference would be to West Gully as East Gully may affect pit access during periods of heavy precipitation during the early life of the mine.

All water courses intercepted by the pit access road will be maintained with the use of culverts. Water collected by the road courses will be channelled to existing water

courses by the road ditch system. Water that collects on the working pit benches will likely be channelled down the pit access road. A need for settling ponds will be evaluated as required following a survey of water flows in the creeks and gullies that will be affected by the excavation of the Bronson Slope deposit.

**3.5.1.2**    *Camp Area*

Runoff control for the camp area will involve maintenance of the existing Bronson Creek dike and diversion system. Upgrades to the system will only be made as required. All remaining runoff controls and diversions will be maintained as required.

**3.5.2**        **Water Balance**

**3.5.2.1**    *Mill Facility*

The mill facility will require the majority of water for the production of copper concentrate. The details of the mill water balance are not yet available. It has been determined that the primary water source for the mill during startup will be Bronson Creek. Continuous operation of the mill will be supplied by reclaim water from the tailings facility with makeup water being supplied by precipitation and Bronson Creek. The amount of makeup water taken from Bronson Creek should have no significant impact on the flows. The impact should be less than 1% at any given time.

**3.5.2.2**    *Camp Facility*

Water for the camp facilities will be supplied by the existing well system. The water quality of Bronson Creek is generally unacceptable for human consumption due to natural metal loading and sedimentation levels. Camp waste water will be directed to the septic field.

**3.5.2.3**    *Sewage Disposal*

Camp sewage will be disposed of in the existing septic field area. If this is not possible a new or expanded facility will be utilized. A location for this system will be located if required.

**3.6**            **Infrastructure**

It is anticipated that the Cominco Snip operation will be closing down based on present reserve estimates at approximately the same time the Bronson Slope Project would be preparing for start-up, resulting in the possibility of International Skyline acquiring these facilities for the Bronson Slope Project.

### 3.6.1 Camp

The buildings required for the camp are available from two potential sources:

- the Skyline Johnny Mountain mine; or
- use of the Cominco Snip Mine.

The Johnny Mountain camp facilities are available for construction and possible seasonal operations at its present location. This location is fully permitted and usable on short notice. Movement of this camp down to Bronson Creek is also an option. A possible site for this camp would be the present location of the Skyline sawmill. This area is presently under a Forestry Special Use Permit # 14944.

The ideal situation would be the takeover of the Cominco Camp upon the closure of the Snip deposit and all ancillary facilities.

### 3.6.2 Maintenance Facilities

The existing facilities at the Snip camp would be sufficient for small vehicles only. An additional facility will have to be constructed to handle the larger open pit equipment. The facility itself is expected to be small and may be located on a portion of the mine access road which will remain open for the life of the mine. This will reduce the travel time to and from the pit area due to the length of the pit access road.

### 3.6.3 Mine Roads

#### 3.6.3.1 General Concepts

Other than the access road to the site (possibly from the Eskay Creek Mine road along the Iskut River to Bronson Creek), the only road at the mine will connect the camp and mill with the open pit (Figure 3-13). Assuming the Bronson Slope Mine were to use the existing Snip Mine camp, a total of 6.5 km of local mine roads would be required, including the major in-pit access road, but not bench branch roads which would be placed on alternate benches as the pit developed. Roads would be gravel-surfaced, average 10 m width and ditched. Fills would be avoided in road construction where ever possible. Side-casting onto unstable slopes would be avoided. Culverts and cross drains would be placed to maximize stability and downslopes from culverts outside the pit proper would be armoured where necessary to prevent erosion.

The unique stratigraphic location of the Bronson Slope deposit with respect to the location of the site facilities will allow the movement of ore and waste down an ore pass to the mill and waste storage facilities (Figure 3-8). The material will be moved via conveyor from the ore/waste pass system to the mill. The Bronson Slope access

road will be approximately 6550 meters long and has an average grade of 9.2% (Figure 3-13).

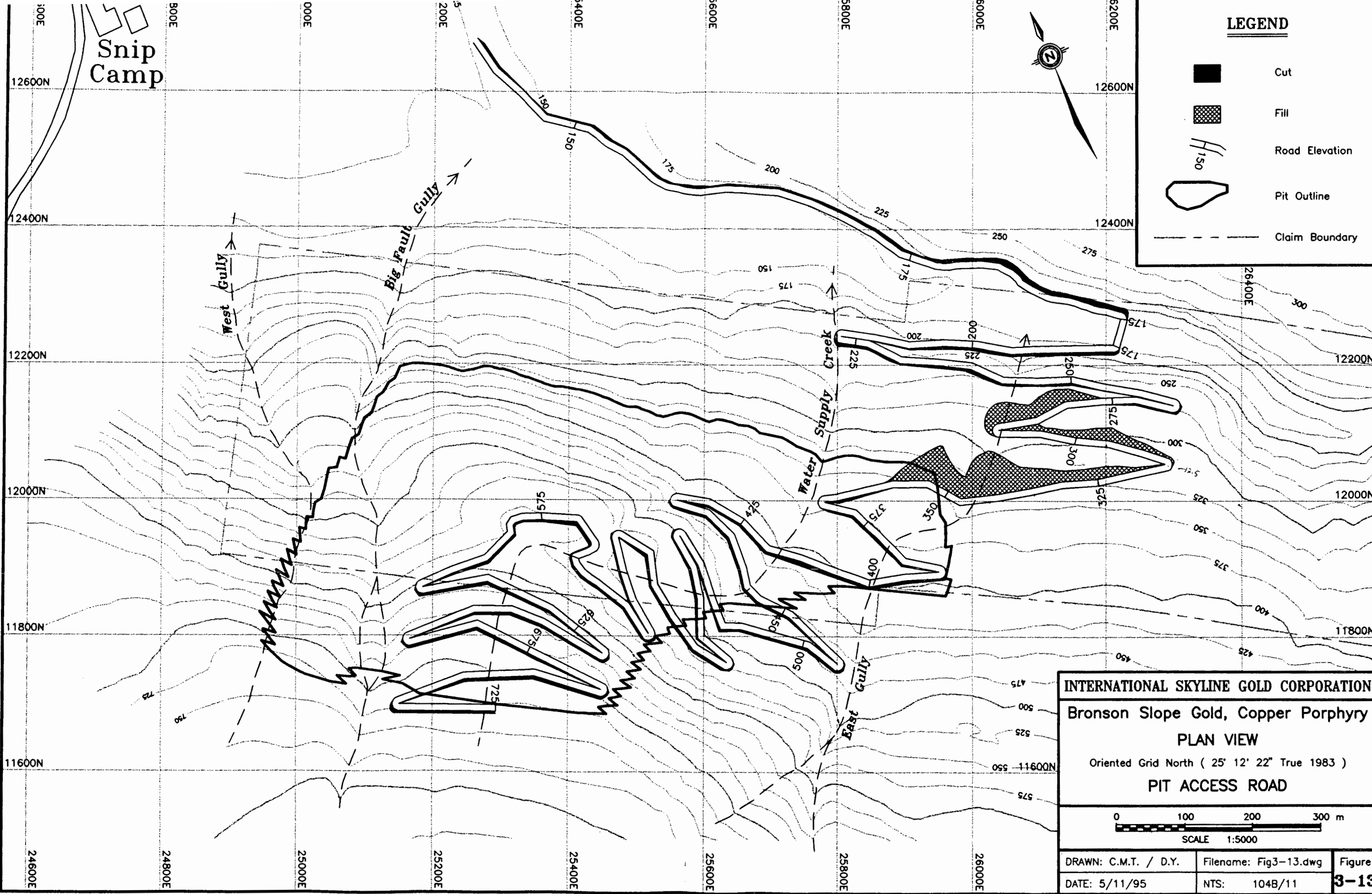
### 3.6.3.2 *Pit Access Road Route*

The Bronson Slope pit access road will start on the north side of Bronson Creek in the area of the present Keewatin Camp at the north end of the Bronson Creek airstrip (See Figure 3-8). The exact starting point has not been chosen as it will likely tie into the planned Iskut road extension at this point. The road will be developed on the north side of Bronson Creek. It is necessary to construct this portion of the road on the north side of Bronson Creek to avoid any safety problems with a south side construction which would place the road directly under Bronson Slope itself and directly under mining operations.






Starting at the 125 meter elevation the road will climb at a 10% grade for a distance of 250 meters to the 150 meter elevation. The road will then follow the 150 meter contour for approximately 300 meters before climbing to the 175 meter elevation at 10%. Due to the steep terrain in this area the road will be developed as a cut road. A typical cut section is shown in Figure 3-14.


A crossing of Bronson Creek to the south side will take place in this area. This portion of Bronson Creek is in a canyon. This appears to be one of the better and shorter areas to cross the river. This crossing will be subject to several studies at the feasibility level which will ultimately determine the type of bridge structure required.

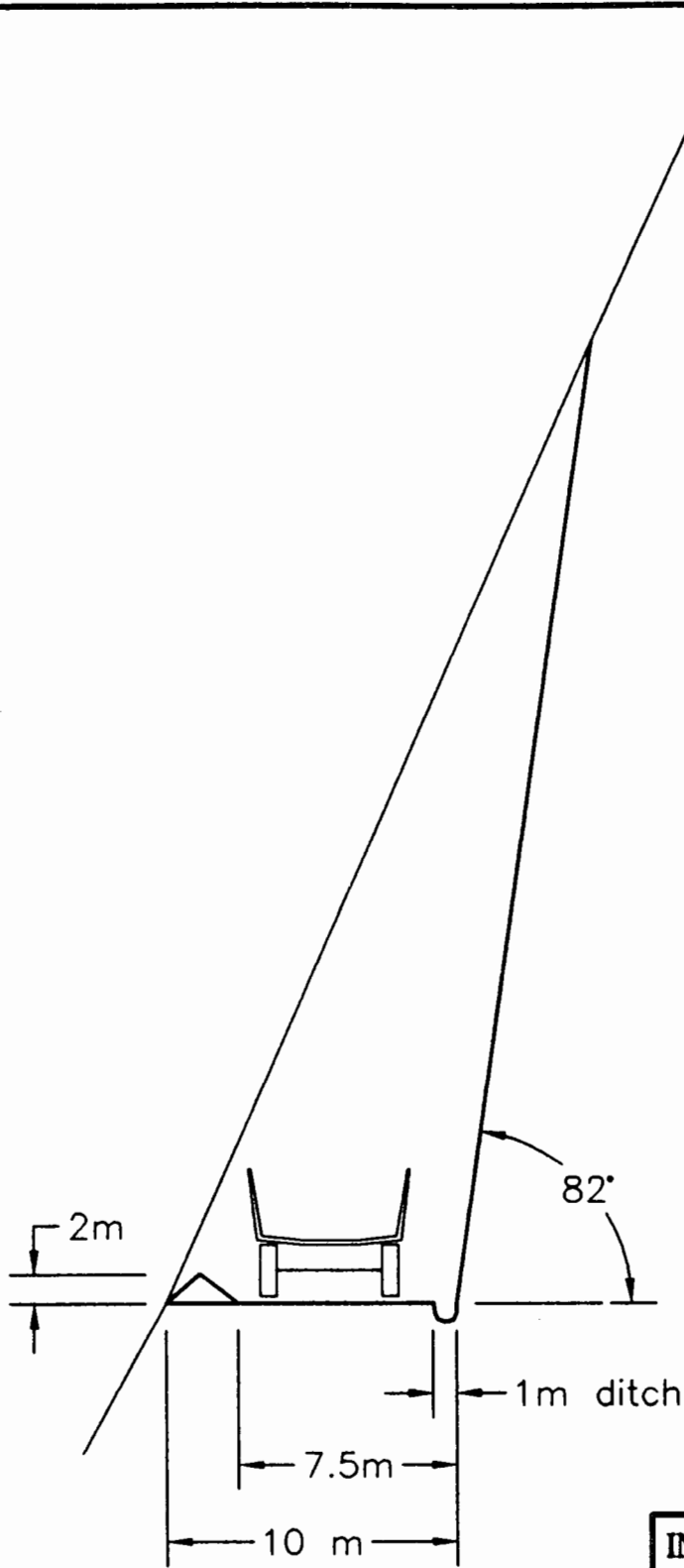
The remainder of the road from this point will remain on the south side of Bronson Creek. The road will climb from this point to the 725 meter elevation through a series of switchbacks. The portion of the road from 175 meter elevation to the 275 meter elevation will be cut a road. The portion from 275 meter elevation travels through an area of shallow dipping terrain (less than 30 degrees) and will be developed as a fill road through the 360 meter elevation. Figure 3-5 shows a typical fill section with fill at an angle of repose of 30 degrees and an angle of repose of 37.5 degrees. All fill volumes have been calculated using an angle of repose of 30 degrees. The remainder of the road will be a cut road which will continue to the 725 meter elevation. A cut angle of 89 degrees has been used. This will be subject to on site geotechnical evaluations, and constraints laid out in the Forest practice Code. The road will generate a total of 1,200,000 tons of cut material. A large portion of this material will be ore grade and will be stockpiled until mill startup. The fill portion of the road will require 162,000 tons of material. This material will likely be generated from the cut area on the north side of Bronson Creek. All material used for construction will have to meet ARD standards and be an acceptable rock quality for fill.



**LEGEND**

-  Cut
-  Fill
-  Road Elevation
-  Pit Outline
-  Claim Boundary

INTERNATIONAL SKYLINE GOLD CORPORATION		
Bronson Slope Gold, Copper Porphyry		
PLAN VIEW		
Oriented Grid North ( 25° 12' 22" True 1983 )		
PIT ACCESS ROAD		
 SCALE 1:5000		
DRAWN: C.M.T. / D.Y.	Filename: Fig3-13.dwg	Figure
DATE: 5/11/95	NTS: 104B/11	<b>3-13</b>



INTERNATIONAL SKYLINE GOLD CORPORATION		
Bronson Slope Gold, Copper Porphyry		
Cross Section 26000 E		
Looking Grid East		
Typical Cut Section		
SCALE 1:250		
DRAWN: C.M.T. / D.Y.	Filename: Fig3-14.dwg	Figure
DATE: 5/11/95	NTS: 104B/11	<b>3-14</b>



### 3.6.3.3 *Design Criteria*

The application assumes the largest vehicle to use the road will be a Caterpillar 777C haul truck with an operating width of 5.5 meters. The Bronson Slope pit access road will be used for pit access only, therefor it will not be required to be designed to haul road standards.

The present access road design has the road with a total width of 10.0 meters. This includes a 1.0 meter wide ditch and a 2 meter wide berm. The berm will be 1.6 meters high which will meet the 3/4 wheel height berm requirement.

The excessive length of road at a 10% grade will require runaway lanes at given intervals along the route. These lanes will be constructed in such a manner as to high center the vehicle as quickly as possible and bring the vehicle to a safe stop. Other safety measures for bringing equipment down the access road may be required. The road will be radio controlled and pullouts will also be available.

### 3.6.3.4 *Runoff Control and Settling Ponds*

All road runoff will be directed to the ditch system located along the inside portion of the road. Small creeks and water channels will be diverted or culverts put into place to allow unobstructed flows during normal run-off, and snow melt. The use of settling ponds for ditch water will be subject to further studies with regard to sedimentation loading and flows of water courses in the area.

## 3.7 **Power Supply**

Three individual power supply options have been addressed and are outlined. The economic benefits and potential drawbacks are outlined below. The Bronson Slope project will require a peak load of approximately 18 megawatts with an operating load in the order of 14 megawatts.

### 3.7.1 **Diesel Power**

Diesel power has been reviewed and entered into the cash flow model. At an estimated cost of \$0.09/kwhr the operation likely will not be economic. The post payback portion of the cash flow would generate some revenue, however costs during the payback period would increase the payback period to an unacceptable level. Diesel backup will likely be required for partial power backup regardless which option is chosen.

### 3.7.2 B.C. Hydro Option

The existing line to Stewart B.C. could be extended from Meziaden Junction. The existing line could supply the power required by the Bronson Slope project, however the capacity of the line would be maximized. This will require extra switchgear for line and surge protection as well as transformers to compensate for line losses etc. During times of inadequate supply or peak demand the diesel generators will be required to subsidize the B.C. Hydro option. Costs for power are estimated at \$0.035 kwhr. The capital cost of the extension would be comparable to the diesel option however with a much lower operating cost. The operation could likely proceed economically with this level of costs.

### 3.7.3 Iskut River Run-of-River Option

A run of river power option is being proposed as a power option for the Bronson Slope project. This option has a higher capital cost than the previous two options but a significantly lower operating cost. The operating cost for the run of river option is in the order of \$0.019/kwhr. Extensive work has been carried out in the area in previous years and this option is feasible. This is the preferred hydro option for the company.

The run of river hydroelectric generating plant would have a capacity of between 16 and 20 MW and be located at the Iskut River canyon. This site is approximately 31 km upstream from the mine location. Power would be delivered to the site via a transmission line located along the Iskut River road corridor. The mine would be the only load served by this facility. At the time of this report, the Company does not intend to sell power to other users.

Further details are provided in the accompanying document, "Iskut Canyon Hydroelectric Plant. Application to the Environmental Assessment Office for a Project Approval Certificate", Section 8.0 of this report.

## 3.8 Project Alternatives

### *Magnetite*

Basic metallurgical work has indicated that magnetite will be recoverable from the ore. Preliminary resource grades indicate approximately 500,000 recoverable tons per year are achievable of which 10 - 15% could supply the western Canadian coal industry.

Presently the coal industry is being supplied magnetite from the old Craigmont Mine, however quality of the product is poor. The supply of a superior quality of magnetite is being investigated by the coal industry and it is thought the project will be able to

*PROJECT DESCRIPTION*

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produce the required product. The coal industry uses magnetite for heavy media separation. The industry consumes between 60 - 80 thousand metric tons per year. Other markets for a high quality magnetite product are also available in the Western U.S. and Australia.

If grades and qualities of the remaining magnetite are adequate the possibility of shipping this product as iron ore does exist. If this were possible approximately 420,000 tonnes of magnetite could be shipped each year to offshore smelters depending on sale prices at port. If the product could not be sold in any given year a plan to stockpile would be established. The storage of magnetite has no significant environmental concerns.

**APPENDIX 5**

1995 Computer Model

**International Skyline Gold Corporation  
Bronson Slope Gold, Copper Porphyry  
Mineral Resource Inventory  
250 meter Search Radius Model  
Corrected Topography & Re-assay of 1988 Drilling  
December 21, 1995**

## RESOURCE MODELING CRITERIA

### 250 meter search radius model

The following resource base utilized an updated claim boundary outline based on survey points located in the field which truly represents the claim group. All 1994 and 1995 drill hole locations were surveyed. Topography was adjusted to fit the available survey data. Reserve polygons which represented areas of undefined material in space were left in the database.

- *This resource estimate is a guideline which is to assist in the development of future drill plans, and is also to be used to generate a higher confidence level in the starter pit area. This resource update utilizes all drilling and the re-assay values of all 1988 holes.*
- The resource is developed on 10m. benches.
- Resource polygons are generated using a search radius of 250m. Polygon grades are developed using drill hole composites contained within the 10m. bench.
- No geological or structural constraints are used to limit polygon search radius. Claim boundaries and topography are the only lithological constraints used.
- Molybdenum values are not included in the gross contained metal values.
- Gold is priced @ \$500.00 Canadian per ounce.
- Silver is priced @ \$6.75 Canadian per ounce.
- Copper is priced @ \$1.25 Canadian per pound.
- This resource utilizes the 1995 assaying of the 1988 holes with the exception of drill hole 944 which utilizes the 1994 re-assay results.



**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM LEVEL	BENCH HEIGHT	POLYGON MATERIAL	HOLE ID	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER %	COPPER POUNDS	MOLY %	MOLY POUNDS	\$VAL TONNE	TOTAL VALUE
610															
610	10	UDF		2.65	49,072	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
<b>SUBTOTAL</b>		UDF			49,072										
<b>CUMULATIVE TOTAL</b>		UDF			56,707										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
<b>SUBTOTAL</b>		WST			0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
<b>CUMULATIVE TOTAL</b>		WST			0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
<b>SUBTOTAL</b>		LGD			0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
<b>CUMULATIVE TOTAL</b>		LGD			0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
<b>SUBTOTAL</b>		HGD			0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
<b>CUMULATIVE TOTAL</b>		HGD			0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
<b>BENCH TOTAL</b>		HGD/LGD			0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
<b>CUM. BENCH TOTAL</b>		HGD/LGD			0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0



BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY

250m SEARCH RADIUS

19-12-95 9:31 AM LEVEL	BENCH HEIGHT	POLYGON MATERIAL	HOLE ID	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER %	COPPER POUNDS	MOLY %	MOLY POUNDS	VAL TONNE	TOTAL VALUE
600															
SUBTOTAL		UDF				0									
CUMULATIVE TOTAL		UDF				58,707									
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
600	10	WST	1217	2.65	117,125	0	0	0	0	0.000%	0	0.000%	0	\$0.00	\$0
SUBTOTAL		WST			117,125	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
CUMULATIVE TOTAL		WST			117,125	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
SUBTOTAL		LGD				0 0.000	0 0.000	0 0.000	0 0.000	0 0.000%	0 0.000%	0 0.000%	0	\$0.00	\$0
CUMULATIVE TOTAL		LGD				0 0.000	0 0.000	0 0.000	0 0.000	0 0.000%	0 0.000%	0 0.000%	0	\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
SUBTOTAL		HGD				0 0.000	0 0.000	0 0.000	0 0.000	0 0.000%	0 0.000%	0 0.000%	0	\$0.00	\$0
CUMULATIVE TOTAL		HGD				0 0.000	0 0.000	0 0.000	0 0.000	0 0.000%	0 0.000%	0 0.000%	0	\$0.00	\$0
BENCH TOTAL		HGD/LGD				0 0.000	0 0.000	0 0.000	0 0.000	0 0.000%	0 0.000%	0 0.000%	0	\$0.00	\$0
CUM. BENCH TOTAL		HGD/LGD				0 0.000	0 0.000	0 0.000	0 0.000	0 0.000%	0 0.000%	0 0.000%	0	\$0.00	\$0

LEAD AND ZINC ARE NOT INCLUDED IN TOTAL METAL VALUES

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	#VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
890															
SUBTOTAL		UDF				0									
CUMULATIVE TOTAL		UDF				66,707									
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
500	10	WST	1217	2.65	238,660	0.041	9,785	0.747	178,279	0.020%	105,231	0.002%	10,523	\$1.37	\$328,104
SUBTOTAL		WST			238,660	0.041	9,785	0.747	178,279	0.020%	105,231	0.002%	10,523	\$1.37	\$328,104
CUMULATIVE TOTAL		WST			365,784	0.028	9,785	0.501	178,279	0.013%	105,231	0.001%	10,523	\$0.92	\$328,104
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
SUBTOTAL		LGD				0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00
CUMULATIVE TOTAL		LGD				0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
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														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
SUBTOTAL		HGD				0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00
CUMULATIVE TOTAL		HGD				0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00
														\$0.00	\$0
BENCH TOTAL		HGD/LGD				0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00
CUM. BENCH TOTAL		HGD/LGD				0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00

## BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY

## 250m SEARCH RADIUS

18-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	#VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
580															
SUBTOTAL		UDF			0										
CUMULATIVE TOTAL		UDF			56,707										
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
580	10	WST	1215	2.65	176,635	0	0	0	0	0.000%	0	0.000%	0	\$0.00	\$0
580	10	WST	1217	2.65	110,025	0.054	5,941	1,005	110,575	0.030%	72,769	0.004%	9,703	\$1.91	\$210,824
SUBTOTAL		WST			286,660	0.021	5,941	0.386	110,575	0.012%	72,769	0.002%	9,703	\$0.74	\$210,824
CUMULATIVE TOTAL		WST			642,444	0.024	15,726	0.450	288,854	0.013%	178,000	0.001%	20,226	\$0.84	\$538,928
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
580	10	LGD	1211	2.65	81,136	0.126	10,223	0.4	32,454	0.150%	268,310	0.005%	8,944	\$6.25	\$506,914
SUBTOTAL		LGD			81,136	0.126	10,223	0.400	32,454	0.150%	268,310	0.005%	8,944	\$6.25	\$506,914
CUMULATIVE TOTAL		LGD			81,136	0.126	10,223	0.400	32,454	0.150%	268,310	0.005%	8,944	\$6.25	\$506,914
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
580	10	HGD	1216	2.65	10,617	0.22	2,336	1.8	19,110	0.270%	63,196	0.007%	1,838	\$11.37	\$120,756
SUBTOTAL		HGD			10,617	0.220	2,336	1.800	19,110	0.270%	63,196	0.007%	1,838	\$11.37	\$120,756
CUMULATIVE TOTAL		HGD			10,617	0.220	2,336	1.800	19,110	0.270%	63,196	0.007%	1,838	\$11.37	\$120,756
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
															\$0.00
															\$0
BENCH TOTAL		HGD/LGD			91,752	0.137	12,559	0.562	51,564	0.164%	331,505	0.005%	10,582	\$6.84	\$627,671
CUM. BENCH TOTAL		HGD/LGD			91,752	0.137	12,559	0.562	51,564	0.164%	331,505	0.005%	10,582	\$6.84	\$627,671

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY****250m SEARCH RADIUS**

18-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	#VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
570															
SUBTOTAL		UDF			0										
CUMULATIVE TOTAL		UDF			66,707										
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
570	10	WST	1208	2.65	42,226	0	0	0	0	0.000%	0	0.000%	0		\$0.00 \$0
570	10	WST	1217	2.65	115,443	0.064	9,697	1.748	201,794	0.040%	101,803	0.004%	10,180	\$2.83	\$327,579
SUBTOTAL		WST			157,669	0.062	9,697	1.280	201,794	0.029%	101,803	0.003%	10,180	\$2.08	\$327,579
CUMULATIVE TOTAL		WST			800,113	0.032	26,424	0.613	490,648	0.016%	279,803	0.002%	30,406	\$1.08	\$866,507
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
570	10	LGD	1211	2.65	95,527	0.13	12,419	0.696	66,487	0.120%	252,721	0.012%	25,272	\$5.55	\$530,217
570	10	LGD	1218	2.65	36,540	0.169	6,175	0.9	32,868	0.160%	128,891	0.010%	8,056	\$7.32	\$267,647
SUBTOTAL		LGD			132,067	0.141	18,594	0.752	99,373	0.131%	381,612	0.011%	33,328	\$6.04	\$797,865
CUMULATIVE TOTAL		LGD			213,203	0.135	28,817	0.618	131,827	0.138%	649,921	0.009%	42,271	\$6.12	\$1,304,779
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
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															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
															\$0.00 \$0
570	10	HGD	1222	2.65	75,277	0.543	40,876	1.54	115,927	0.140%	232,342	0.001%	1,660	\$12.92	\$973,212
570	10	HGD	1218	2.65	70,874	0.601	42,595	3.583	253,941	0.200%	312,500	0.002%	3,125	\$15.95	\$1,131,425
570	10	HGD	1215	2.65	239,507	0.377	90,294	18.353	4,365,677	0.420%	2,217,695	0.006%	31,681	\$21.62	\$5,191,068
SUBTOTAL		HGD			385,658	0.451	173,765	12.357	4,785,546	0.325%	2,782,537	0.004%	36,466	\$18.92	\$7,295,735
CUMULATIVE TOTAL		HGD			396,275	0.444	178,101	12.074	4,784,856	0.323%	2,825,732	0.004%	38,104	\$18.72	\$7,416,481
BENCH TOTAL		HGD/LGD			617,226	0.372	192,359	9.397	4,864,918	0.275%	3,144,148	0.006%	69,794	\$16.83	\$8,093,589
CUM. BENCH TOTAL		HGD/LGD			609,478	0.336	204,918	8.087	4,916,483	0.259%	3,475,654	0.006%	80,378	\$14.31	\$8,721,270

BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY															
250m SEARCH RADIUS															
19-12-95 9:31 AM LEVEL	BENCH HEIGHT	POLYGON MATERIAL	HOLE ID	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER %	COPPER POUNDS	MOLY %	MOLY POUNDS	#VAL TONNE	TOTAL VALUE
560															
SUBTOTAL		UDF			0										
CUMULATIVE TOTAL		UDF			88,707										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
560	10	WST	1208	2.65	82,754	0.145	11,999	1.035	85,851	0.070%	127,710	0.001%	1,824	\$4.48	\$371,430
SUBTOTAL		WST			82,754	0.145	11,999	1.035	85,851	0.070%	127,710	0.001%	1,824	\$4.49	\$371,430
CUMULATIVE TOTAL		WST			882,867	0.042	37,423	0.853	576,299	0.021%	407,512	0.002%	32,230	\$1.40	\$1,237,937
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
560	10	LGD	1217	2.65	132,453	0.175	23,179	2.553	338,153	0.080%	233,607	0.007%	20,441	\$5.57	\$730,125
560	10	LGO	1216	2.65	90,804	0.193	17,544	0.622	56,542	0.090%	180,367	0.009%	16,037	\$5.72	\$520,013
560	10	LGD	1209	2.65	60,219	0.271	16,319	2.017	121,463	0.080%	119,485	0.006%	7,966	\$7.27	\$438,495
560	10	LGO	1211	2.65	115,616	0.18	20,811	1.147	132,812	0.190%	484,291	0.012%	30,587	\$8.38	\$969,178
SUBTOTAL		LGD			399,193	0.195	77,854	1.825	648,789	0.110%	1,017,750	0.009%	77,030	\$8.88	\$2,886,811
CUMULATIVE TOTAL		LGO			612,395	0.174	106,671	1.276	780,596	0.124%	1,687,672	0.009%	119,301	\$8.49	\$3,971,590
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
560	10	HGD	1222	2.65	83,613	0.538	44,984	1.556	130,102	0.150%	276,503	0.001%	1,843	\$13.12	\$1,097,591
560	10	HGD	1218	2.65	126,898	0.668	84,514	5.852	742,608	0.210%	587,501	0.003%	6,393	\$17.78	\$2,256,738
560	10	HGD	1215	2.65	273,076	0.894	244,130	2.24	611,691	0.280%	1,685,682	0.004%	24,081	\$22.57	\$8,167,285
SUBTOTAL		HGD			483,587	0.773	373,628	3.070	1,484,401	0.239%	2,549,685	0.003%	34,317	\$19.89	\$9,521,614
CUMULATIVE TOTAL		HGD			879,883	0.625	549,729	7.125	6,269,056	0.277%	5,378,417	0.004%	72,422	\$19.25	\$18,838,105
BENCH TOTAL		HGD/LGD			882,780	0.611	461,482	2.418	2,133,170	0.183%	3,567,435	0.006%	111,347	\$13.81	\$12,188,425
CUM. BENCH TOTAL		HGD/LGD			1,492,258	0.440	656,400	4.724	7,049,653	0.214%	7,043,089	0.006%	191,723	\$14.01	\$20,908,695

BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY															
250m SEARCH RADIUS															
19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	#VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
550															
550	10	UDF		2.65	7,513	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			7,513										
CUMULATIVE TOTAL		UDF			64,220										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
550	10	WST	1216	2.65	133,402	0.149	19,877	0.245	32,883	0.050%	147,050	0.009%	26,469	\$3.83	\$510,623
SUBTOTAL		WST			133,402	0.149	19,877	0.245	32,883	0.050%	147,050	0.009%	26,469	\$3.83	\$510,623
CUMULATIVE TOTAL		WST			1,016,269	0.056	67,300	0.599	606,982	0.025%	564,662	0.003%	68,699	\$1.72	\$1,748,660
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
550	10	LGD	1208	2.65	142,270	0.197	28,027	0.602	85,646	0.120%	376,361	0.003%	9,410	\$6.60	\$939,995
550	10	LGD	1211	2.65	138,802	0.176	24,394	1.338	185,450	0.150%	458,349	0.010%	30,557	\$7.25	\$1,005,991
550	10	LGD	1217	2.65	139,728	0.237	33,115	1.848	258,217	0.180%	554,483	0.014%	43,128	\$9.17	\$1,282,406
SUBTOTAL		LGD			420,600	0.203	85,537	1.258	529,313	0.150%	1,389,213	0.009%	83,093	\$7.68	\$3,228,393
CUMULATIVE TOTAL		LGD			1,032,995	0.186	192,208	1.268	1,309,909	0.134%	3,056,884	0.009%	202,394	\$6.97	\$7,199,983
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
550	10	HGD	1222	2.65	83,692	0.542	45,361	1.728	144,619	0.170%	313,664	0.006%	11,070	\$13.77	\$1,153,297
550	10	HGD	1209	2.65	103,387	0.616	63,687	3.308	342,005	0.250%	569,825	0.003%	6,838	\$17.51	\$1,811,603
550	10	HGD	1218	2.65	145,875	0.927	135,226	4.298	626,677	0.200%	643,196	0.011%	35,376	\$21.35	\$3,116,293
550	10	HGD	1215	2.65	283,538	0.92	260,855	3.181	901,935	0.280%	1,750,262	0.017%	106,266	\$23.20	\$8,580,802
SUBTOTAL		HGD			616,491	0.819	605,128	3.269	2,015,236	0.241%	3,276,946	0.012%	159,550	\$20.54	\$12,661,998
CUMULATIVE TOTAL		HGD			1,486,364	0.705	1,064,857	5.538	8,284,292	0.282%	8,652,363	0.007%	231,972	\$19.78	\$29,800,100
BENCH TOTAL		HGD/LGD			1,037,091	0.670	590,665	2.454	2,544,549	0.204%	4,666,159	0.011%	242,643	\$16.32	\$15,890,369
CUM. BENCH TOTAL		HGD/LGD			2,529,349	0.493	1,247,095	3.793	9,594,202	0.210%	11,709,248	0.008%	434,366	\$14.55	\$36,600,064

BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY															
250m SEARCH RADIUS															
18-12-95 9:31 AM	BENCH	POLYGON	MOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	IVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
540															
540	10	UDF		2.65	18,891	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			18,891										
CUMULATIVE TOTAL		UDF			83,111										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
540	10	WST	1210	2.65	132,320	0	0	0	0	0.000%	0	0.000%	0	\$0.00	\$0
SUBTOTAL		WST			132,320	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
CUMULATIVE TOTAL		WST			1,148,589	0.050	57,300	0.530	808,982	0.022%	554,582	0.002%	58,899	\$1.52	\$1,748,560
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
SUBTOTAL		LGD			0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
CUMULATIVE TOTAL		LGD			1,032,995	0.180	192,208	1.288	1,309,909	0.134%	3,056,884	0.009%	202,394	\$6.97	\$7,199,883
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
540	10	HGD	1216	2.65	118,625	0.533	63,227	1.486	176,277	0.120%	313,828	0.014%	36,613	\$12.20	\$1,447,759
540	10	HGD	1222	2.65	83,809	0.502	42,072	1.784	147,839	0.140%	258,674	0.002%	3,695	\$12.31	\$1,032,389
540	10	HGD	1215	2.65	244,875	0.578	141,048	2.7	661,163	0.160%	883,771	0.005%	26,983	\$14.25	\$3,493,226
540	10	HGD	1208	2.65	191,925	0.687	131,852	1.478	283,665	0.240%	1,015,492	0.004%	16,925	\$17.98	\$3,451,956
540	10	HGD	1218	2.65	150,377	0.918	138,046	3.304	496,846	0.140%	464,134	0.008%	19,891	\$19.33	\$2,909,258
540	10	HGD	1217	2.65	145,331	0.578	84,001	3.67	533,365	0.350%	1,121,399	0.008%	25,632	\$19.73	\$2,869,631
540	10	HGD	1211	2.65	162,515	1.093	177,629	1.811	294,314	0.130%	465,768	0.015%	53,742	\$21.55	\$3,503,226
540	10	HGD	1209	2.65	153,977	0.858	132,112	3.387	521,521	0.330%	1,120,222	0.002%	6,789	\$23.62	\$3,639,360
SUBTOTAL		HGD			1,261,436	0.727	909,989	2.489	3,114,991	0.204%	6,623,289	0.007%	190,281	\$17.88	\$22,347,028
CUMULATIVE TOTAL		HGD			2,747,789	0.716	1,964,846	4.149	11,399,283	0.238%	14,275,852	0.007%	422,253	\$18.81	\$51,847,126
BENCH TOTAL		HGD/LGD			1,261,436	0.727	909,989	2.489	3,114,991	0.204%	6,623,289	0.007%	190,281	\$17.88	\$22,347,028
CUM. BENCH TOTAL		HGD/LGD			3,780,784	0.871	2,157,053	3.382	12,709,192	0.208%	17,332,537	0.007%	624,647	\$18.64	\$58,147,109

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

18-12-96 8:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	4VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
520															
<b>SUBTOTAL</b>					0										
<b>CUMULATIVE TOTAL</b>					83,213										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
<b>SUBTOTAL</b>					0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
<b>CUMULATIVE TOTAL</b>					1,272,491	0.045	67,300	0.479	608,982	0.020%	664,662	0.002%	68,699	\$1.37	\$1,748,560
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
520	10	LGD	1212	2.65	191,028	0.145	27,699	0.654	163,136	0.100%	421,145	0.008%	33,692	\$5.27	\$1,007,772
520	10	LGD	1219	2.65	146,534	0.135	19,782	1.168	171,298	0.110%	355,356	0.011%	35,536	\$5.46	\$799,976
520	10	LGD	1211	2.65	186,565	0.261	48,694	0.757	141,230	0.170%	699,220	0.017%	69,922	\$9.04	\$1,668,067
520	10	LGD	1216	2.65	115,176	0.299	34,438	0.875	100,779	0.150%	380,880	0.022%	56,862	\$8.13	\$1,052,031
<b>SUBTOTAL</b>					639,303	0.204	130,612	0.902	676,445	0.132%	1,856,600	0.014%	195,012	\$7.11	\$4,547,816
<b>CUMULATIVE TOTAL</b>					2,279,762	0.223	608,572	1.184	2,699,273	0.124%	6,263,147	0.009%	451,886	\$7.28	\$16,688,114
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
520	10	HGD	1215	2.65	259,685	0.495	128,544	1.869	485,351	0.120%	687,007	0.001%	5,725	\$11.67	\$3,032,522
520	10	HGD	1217	2.65	153,122	0.377	57,727	2.043	312,828	0.220%	742,668	0.004%	13,503	\$12.57	\$1,923,400
520	10	HGD	1209	2.65	209,456	0.453	94,864	1.297	271,665	0.210%	969,720	0.002%	9,235	\$13.35	\$2,797,646
520	10	HGD	1210	2.65	213,717	0.514	109,851	0.689	147,251	0.180%	848,097	0.002%	9,423	\$13.37	\$2,858,915
520	10	HGD	1222	2.65	86,979	0.783	68,104	2.019	175,610	0.250%	479,368	0.002%	3,835	\$19.91	\$1,732,989
520	10	HGD	1218	2.65	160,893	0.63	101,363	5.714	919,345	0.340%	1,206,010	0.002%	7,094	\$20.74	\$3,339,683
520	10	HGD	1208	2.65	173,815	1.173	203,885	2.703	469,823	0.320%	1,226,230	0.009%	34,468	\$28.26	\$4,914,626
<b>SUBTOTAL</b>					1,267,667	0.608	764,358	2.212	2,781,872	0.222%	6,159,118	0.003%	83,304	\$16.38	\$20,601,764
<b>CUMULATIVE TOTAL</b>					4,918,168	0.683	3,367,662	3.436	16,895,697	0.238%	25,792,778	0.006%	680,695	\$18.28	\$69,847,621
<b>BENCH TOTAL</b>					1,896,971	0.472	894,970	1.770	3,358,318	0.192%	8,016,719	0.007%	278,315	\$13.28	\$26,149,600
<b>CUM. BENCH TOTAL</b>					7,197,930	0.837	3,866,124	2.722	18,895,270	0.202%	32,045,922	0.007%	1,132,980	\$14.80	\$106,835,836



**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	#VAL	TOTAL	
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE	
510																
SUBTOTAL						0										
CUMULATIVE TOTAL						83,213										
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
510	10	WST	1212	2.65	261,508	0.078	20,397	0.258	67,469	0.060%	345,913	0.007%	40,356	\$2.96	\$775,225	
SUBTOTAL						261,508	0.078	20,397	0.258	67,469	0.060%	345,913	0.007%	40,356	\$2.96	\$775,225
CUMULATIVE TOTAL						1,533,996	0.051	77,697	0.441	676,451	0.027%	900,475	0.003%	99,056	\$1.85	\$2,523,786
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
510	10	LGD	1211	2.65	205,707	0.252	51,838	0.838	172,382	0.140%	634,907	0.016%	72,561	\$8.09	\$1,665,113	
SUBTOTAL						205,707	0.252	51,838	0.838	172,382	0.140%	634,907	0.016%	72,561	\$8.09	\$1,665,113
CUMULATIVE TOTAL						2,485,469	0.225	660,410	1.155	2,871,655	0.126%	6,888,054	0.010%	524,446	\$7.34	\$18,253,227
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
														\$0.00	\$0	
510	10	HGD	1217	2.65	138,927	0.389	54,043	1.334	185,329	0.150%	459,423	0.001%	3,063	\$10.68	\$1,484,056	
510	10	HGD	1219	2.65	237,510	0.318	75,528	3.169	752,671	0.280%	1,466,137	0.011%	57,598	\$13.52	\$3,212,755	
510	10	HGD	1215	2.65	268,304	0.668	178,750	3.025	811,892	0.150%	887,561	0.002%	11,834	\$15.50	\$4,182,375	
510	10	HGD	1222	2.65	101,560	0.671	68,147	1.369	139,036	0.240%	537,365	0.002%	4,478	\$17.70	\$1,796,089	
510	10	HGD	1216	2.65	130,104	0.802	104,344	0.716	93,155	0.210%	602,345	0.004%	11,473	\$18.83	\$2,451,272	
510	10	HGD	1208	2.65	173,982	0.891	120,221	2.887	502,285	0.260%	997,264	0.008%	30,685	\$18.90	\$3,290,240	
510	10	HGD	1218	2.65	183,923	0.898	146,875	3.961	649,296	0.360%	1,300,994	0.003%	10,642	\$25.18	\$4,130,832	
510	10	HGD	1210	2.65	258,479	1.36	351,532	3.753	970,073	0.560%	3,191,154	0.006%	34,191	\$38.11	\$9,854,993	
510	10	HGD	1209	2.65	248,741	1.931	480,319	11.668	2,902,309	0.550%	3,016,086	0.047%	257,736	\$48.73	\$12,132,140	
SUBTOTAL						1,721,621	0.918	1,679,769	4.069	7,006,048	0.328%	12,458,328	0.011%	421,902	\$24.70	\$42,516,764
CUMULATIVE TOTAL						6,639,789	0.744	4,837,311	3.600	23,802,044	0.261%	38,251,103	0.008%	1,102,697	\$18.96	\$132,484,286
BENCH TOTAL						1,927,328	0.847	1,831,697	3.726	7,178,430	0.308%	13,093,234	0.012%	484,463	\$22.92	\$44,181,677
CUM. BENCH TOTAL						8,125,258	0.602	5,497,721	2.934	26,773,699	0.224%	46,139,166	0.006%	1,627,043	\$16.52	\$150,717,512

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

18-12-98 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
500															
SUBTOTAL		UDF			0										
CUMULATIVE TOTAL		UDF			83,213										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
500	10	WST	944	2.65	127,457	0	0	0	0	0.000%	0	0.000%	0	\$0.00	\$0
500	10	WST	945	2.65	71,539	0	0	0	0	0.000%	0	0.000%	0	\$0.00	\$0
500	10	WST	1212	2.65	338,490	0.148	49,127	0.682	229,488	0.060%	445,099	0.008%	44,510	\$4.15	\$1,398,830
SUBTOTAL		WST			535,486	0.092	49,127	0.429	229,488	0.038%	445,099	0.004%	44,510	\$2.61	\$1,398,830
CUMULATIVE TOTAL		WST			2,069,483	0.061	126,825	0.438	905,936	0.029%	1,345,574	0.003%	143,568	\$1.89	\$3,920,818
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
SUBTOTAL		LGD			0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
CUMULATIVE TOTAL		LGD			2,485,469	0.225	580,410	1.155	2,871,655	0.126%	6,888,054	0.010%	524,448	\$7.34	\$18,253,227
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
500	10	HGD	1219	2.65	151,998	0.312	47,423	2.501	380,147	0.180%	603,177	0.012%	40,212	\$10.52	\$1,600,172
500	10	HGD	1211	2.65	222,851	0.337	75,033	2.045	455,321	0.280%	1,374,410	0.004%	19,634	\$13.58	\$3,024,719
500	10	HGD	1217	2.65	86,752	0.553	47,974	1.33	115,380	0.240%	459,011	0.001%	1,913	\$15.79	\$1,370,564
500	10	HGD	1218	2.65	169,256	0.637	107,816	2.574	435,664	0.250%	932,862	0.002%	7,463	\$17.69	\$2,995,603
500	10	HGD	1218	2.65	143,766	0.749	107,681	0.868	124,502	0.210%	665,595	0.008%	19,017	\$18.02	\$2,590,892
500	10	HGD	1208	2.65	171,721	0.77	132,225	3.379	580,245	0.260%	984,307	0.015%	56,787	\$20.28	\$3,484,219
500	10	HGD	1210	2.65	313,359	0.738	230,832	2.45	787,730	0.300%	2,072,515	0.002%	13,817	\$20.63	\$8,468,114
500	10	HGD	1215	2.65	277,309	1.127	312,528	5.972	1,658,091	0.280%	1,711,812	0.005%	30,568	\$27.13	\$7,529,548
500	10	HGD	1209	2.65	255,837	0.954	244,068	5.252	1,343,654	0.400%	2,256,090	0.003%	16,921	\$27.50	\$7,040,331
500	10	HGD	1222	2.65	167,350	2.751	460,379	0.919	153,794	0.240%	885,462	0.004%	14,758	\$51.04	\$8,543,553
SUBTOTAL		HGD			1,959,999	0.901	1,785,769	3.088	6,012,529	0.276%	11,948,239	0.008%	221,089	\$22.78	\$44,847,716
CUMULATIVE TOTAL		HGD			6,889,788	0.778	6,703,070	3.478	28,914,573	0.265%	60,186,342	0.007%	1,323,688	\$20.68	\$177,112,002
BENCH TOTAL		HGD/LGD			1,959,999	0.901	1,785,769	3.088	6,012,529	0.276%	11,948,239	0.008%	221,089	\$22.78	\$44,847,716
CUM. BENCH TOTAL		HGD/LGD			11,085,256	0.655	7,263,480	2.956	32,786,228	0.234%	57,084,395	0.009%	1,848,132	\$17.82	\$195,365,228

UDF MATERIALS ARE NOT INCLUDED IN DATABASE WITH THIS SEARCH. MOLYBDENUM VALUES ARE NOT INCLUDED IN TOTAL METAL VALUES.

BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY

250m SEARCH RADIUS

18-12-85 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	\$VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
490															
SUBTOTAL		UDF			0										
CUMULATIVE TOTAL		UDF			83,213										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
490	10	WST	1221	2.65	182,126	0	0	0	0	0.000%	0	0.000%	0	\$0.00	\$0
490	10	WST	1220	2.65	51,674	0	0	0	0	0.000%	0	0.000%	0	\$0.00	\$0
490	10	WST	1212	2.65	346,731	0.129	44,728	0.734	254,500	0.070%	535,086	0.009%	68,797	\$4.16	\$1,444,076
SUBTOTAL		WST			580,531	0.077	44,728	0.438	254,500	0.042%	535,086	0.005%	68,797	\$2.49	\$1,444,076
CUMULATIVE TOTAL		WST			2,050,013	0.065	171,553	0.438	1,160,437	0.032%	1,880,660	0.004%	212,383	\$2.02	\$5,364,694
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
490	10	LGD	946	2.65	76,915	0.193	14,845	0.839	64,532	0.160%	271,311	0.001%	1,696	\$7.69	\$502,036
490	10	LGD	961	2.65	5,745	0.193	1,109	0.803	4,614	0.160%	20,267	0.002%	253	\$7.69	\$44,179
490	10	LGD	1216	2.65	87,548	0.407	35,632	0.555	48,589	0.080%	154,408	0.002%	3,860	\$8.67	\$776,663
490	10	LGD	962	2.65	54,128	0.284	15,372	0.726	39,295	0.160%	190,924	0.003%	3,580	\$9.13	\$494,478
490	10	LGD	1210	2.65	284,882	0.429	122,214	0.889	253,260	0.100%	828,056	0.002%	12,561	\$9.84	\$2,805,994
490	10	LGD	1209	2.65	251,917	0.327	82,377	1.437	362,005	0.160%	888,611	0.001%	5,554	\$9.96	\$2,515,026
SUBTOTAL		LGD			761,134	0.357	271,649	1.016	772,296	0.128%	2,183,576	0.002%	27,504	\$9.50	\$7,228,378
CUMULATIVE TOTAL		LGD			3,246,603	0.256	831,959	1.122	3,643,950	0.126%	9,041,630	0.008%	551,950	\$7.85	\$25,481,604
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
490	10	HGD	1219	2.65	147,543	0.312	46,033	1.922	283,577	0.190%	618,024	0.010%	32,528	\$10.67	\$1,575,133
490	10	HGD	945	2.65	57,406	0.515	29,564	2.531	145,296	0.160%	202,495	0.008%	10,125	\$13.24	\$760,478
490	10	HGD	944	2.65	35,627	0.528	18,811	1.951	69,509	0.180%	141,381	0.006%	4,713	\$13.87	\$494,503
490	10	HGD	1208	2.65	171,690	0.521	89,450	2.891	496,355	0.180%	681,319	0.004%	15,140	\$13.98	\$2,369,209
490	10	HGD	1211	2.65	231,395	0.298	68,956	1.047	242,271	0.400%	2,040,553	0.025%	127,535	\$16.04	\$3,712,799
490	10	HGD	1217	2.65	104,605	0.776	81,173	1.774	185,569	0.200%	461,228	0.001%	2,308	\$18.37	\$1,922,626
490	10	HGD	1222	2.65	175,587	0.973	170,847	18.142	3,185,507	0.210%	812,917	0.005%	19,355	\$25.37	\$4,484,171
490	10	HGD	1218	2.65	176,378	1.049	185,021	4.929	869,369	0.480%	1,866,468	0.007%	27,219	\$31.16	\$5,499,483
490	10	HGD	1215	2.65	285,159	1.429	407,492	7.5	2,138,691	0.480%	3,017,601	0.011%	69,153	\$37.83	\$10,794,984
SUBTOTAL		HGD			1,385,391	0.782	1,097,348	6.497	7,616,144	0.322%	9,841,985	0.010%	308,074	\$22.83	\$31,623,368
CUMULATIVE TOTAL		HGD			8,885,178	0.781	7,800,418	3.759	37,830,717	0.273%	60,038,327	0.007%	1,631,760	\$20.80	\$208,735,387
BENCH TOTAL		HGD/LGD			2,146,525	0.638	1,368,896	3.906	8,388,439	0.263%	11,995,561	0.007%	335,578	\$18.10	\$38,851,763
CUM. BENCH TOTAL		HGD/LGD			13,231,781	0.652	8,632,377	3.112	41,174,697	0.237%	69,078,957	0.007%	2,183,710	\$17.70	\$234,218,991

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-98 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	IVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
480															
480	10	UDF		2.65	14,115	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
<b>SUBTOTAL</b>															
<b>CUMULATIVE TOTAL</b>															
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
480	10	WST	1270	2.65	112,723	0.032	3,607	0.113	12,738	0.020%	49,702	0.001%	2,485	\$1.09	\$122,932
480	10	WST	1212	2.65	400,133	0.088	35,212	0.39	156,052	0.080%	705,712	0.012%	105,857	\$3.70	\$1,482,675
480	10	WST	1221	2.65	225,371	0.147	33,130	0.553	124,630	0.070%	347,801	0.001%	4,969	\$4.41	\$994,683
<b>SUBTOTAL</b>															
<b>CUMULATIVE TOTAL</b>															
														\$0.52	\$2,600,501
														\$2.36	\$7,965,195
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
480	10	LGD	981	2.65	23,440	0.147	3,448	1.129	26,464	0.160%	82,683	0.002%	1,034	\$7.02	\$184,563
480	10	LGD	1222	2.65	182,421	0.258	47,065	0.874	122,952	0.100%	402,168	0.002%	8,043	\$7.05	\$1,286,558
480	10	LGD	962	2.65	59,972	0.177	10,615	0.444	26,628	0.160%	211,544	0.002%	2,644	\$7.35	\$440,978
480	10	LGD	946	2.65	93,959	0.25	23,490	0.915	85,973	0.160%	331,431	0.002%	4,143	\$8.63	\$810,919
480	10	LGD	1211	2.65	251,295	0.327	82,173	0.807	202,795	0.150%	631,015	0.023%	127,422	\$9.57	\$2,404,733
<b>SUBTOTAL</b>															
<b>CUMULATIVE TOTAL</b>															
														\$8.38	\$5,107,770
														\$7.93	\$30,589,375
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
480	10	HGD	1210	2.65	283,728	0.452	128,245	0.911	258,478	0.110%	688,084	0.005%	31,278	\$10.50	\$2,979,126
480	10	HGD	945	2.65	70,388	0.35	24,636	2.933	208,447	0.160%	248,285	0.004%	8,207	\$10.87	\$751,917
480	10	HGD	1209	2.65	258,898	0.463	119,870	1.474	381,618	0.140%	799,082	0.001%	5,708	\$11.62	\$3,010,316
480	10	HGD	1219	2.65	153,329	0.427	65,472	2.133	327,051	0.200%	678,066	0.012%	40,564	\$12.84	\$1,969,816
480	10	HGD	944	2.65	33,289	0.461	15,348	5.415	180,257	0.190%	139,438	0.007%	5,137	\$13.82	\$460,718
480	10	HGD	1217	2.65	121,938	0.872	81,942	1.264	154,129	0.150%	403,239	0.001%	2,688	\$15.21	\$1,855,586
480	10	HGD	1208	2.65	182,887	0.611	99,524	3.675	598,609	0.200%	718,207	0.005%	17,955	\$16.13	\$2,629,795
480	10	HGD	1218	2.65	186,914	0.578	108,036	2.567	479,809	0.270%	1,112,603	0.004%	18,483	\$17.29	\$3,233,538
480	10	HGD	1216	2.65	86,868	0.746	64,803	2.062	179,121	0.240%	459,625	0.003%	5,745	\$19.05	\$1,655,976
480	10	HGD	1215	2.65	295,601	1.448	428,031	3.781	1,117,669	0.240%	1,584,053	0.011%	71,686	\$30.71	\$9,083,689
<b>SUBTOTAL</b>															
<b>CUMULATIVE TOTAL</b>															
														\$18.71	\$27,630,478
														\$20.31	\$238,265,885
<b>BENCH TOTAL</b>															
<b>CUM. BENCH TOTAL</b>															
														\$14.45	\$32,738,248
														\$17.23	\$268,959,240

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

18-12-96 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	#VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
470															
470	10	UDF	1213	2.65	74,342	0.186	14,571	0.165	12,266	0.000%	0	0.000%	0	\$3.19	
<b>SUBTOTAL</b>		UDF			74,342										
<b>CUMULATIVE TOTAL</b>		UDF			171,670										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
470	10	WST	1212	2.65	454,586	0.111	50,459	0.262	119,102	0.050%	501,095	0.009%	90,197	\$3.22	\$1,463,953
470	10	WST	1221	2.65	259,117	0.14	36,276	0.538	139,405	0.060%	342,753	0.000%	0	\$4.02	\$1,042,435
<b>SUBTOTAL</b>		WST			713,704	0.122	86,735	0.362	258,507	0.054%	843,848	0.006%	90,197	\$3.51	\$2,506,388
<b>CUMULATIVE TOTAL</b>		WST			4,101,943	0.081	330,237	0.417	1,712,363	0.042%	3,827,723	0.005%	415,870	\$2.55	\$10,471,583
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
470	10	LGD	1217	2.65	139,722	0.257	35,908	1.127	157,466	0.080%	246,427	0.001%	3,080	\$6.58	\$920,085
470	10	LGD	1222	2.65	186,755	0.265	49,490	0.477	89,082	0.110%	452,896	0.002%	6,234	\$7.39	\$1,381,519
470	10	LGD	961	2.65	39,818	0.187	7,446	0.578	22,935	0.160%	140,452	0.002%	1,756	\$7.54	\$300,341
470	10	LGD	962	2.65	68,714	0.315	21,645	1.431	98,330	0.160%	242,381	0.002%	3,030	\$9.78	\$672,659
470	10	LGD	944	2.65	30,871	0.341	10,527	1.619	49,980	0.150%	102,068	0.004%	2,722	\$9.07	\$307,879
<b>SUBTOTAL</b>		LGD			465,879	0.268	125,016	0.897	417,793	0.115%	1,184,244	0.002%	18,823	\$7.69	\$3,582,483
<b>CUMULATIVE TOTAL</b>		LGD			4,323,569	0.260	1,123,764	1.047	4,526,555	0.127%	12,084,716	0.007%	714,059	\$7.90	\$34,171,857
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
470	10	HGD	1218	2.65	197,553	0.361	71,317	1.854	366,264	0.150%	653,295	0.001%	4,355	\$10.34	\$2,043,969
470	10	HGD	1210	2.65	281,872	0.411	115,767	1.297	365,329	0.140%	869,371	0.004%	24,839	\$10.75	\$3,028,623
470	10	HGD	945	2.65	83,655	0.372	31,120	4.248	355,366	0.160%	295,084	0.008%	11,066	\$11.31	\$947,439
470	10	HGD	1209	2.65	264,028	0.42	110,892	3.118	823,240	0.230%	1,338,788	0.002%	11,642	\$13.77	\$3,637,740
470	10	HGD	1211	2.65	266,663	0.541	144,265	1.641	437,594	0.190%	1,116,992	0.007%	41,152	\$14.29	\$3,812,285
470	10	HGD	1208	2.65	154,382	0.571	88,152	2.255	348,132	0.170%	578,603	0.005%	17,018	\$14.35	\$2,217,332
470	10	HGD	1220	2.65	168,752	0.761	142,118	1.963	366,594	0.230%	946,949	0.016%	65,875	\$19.00	\$3,549,597
470	10	HGD	946	2.65	106,323	0.928	98,667	3.737	397,327	0.160%	375,041	0.002%	4,688	\$20.14	\$2,142,783
470	10	HGD	1219	2.65	157,947	0.731	115,460	3.999	631,632	0.370%	1,288,392	0.011%	38,304	\$27.82	\$3,606,039
470	10	HGD	1215	2.65	308,379	1.229	378,998	2.972	916,502	0.330%	2,243,532	0.008%	54,389	\$29.50	\$9,100,329
470	10	HGD	1218	2.65	91,322	1.777	162,280	3.959	361,545	0.540%	1,087,186	0.016%	32,213	\$44.31	\$4,047,977
<b>SUBTOTAL</b>		HGD			2,098,677	0.695	1,459,035	2.559	5,369,524	0.233%	10,793,233	0.007%	305,540	\$18.17	\$36,134,112
<b>CUMULATIVE TOTAL</b>		HGD			13,737,696	0.757	10,395,397	3.406	46,783,426	0.256%	77,640,220	0.007%	2,140,749	\$18.98	\$274,489,977
<b>BENCH TOTAL</b>		HGD/LGD			2,564,656	0.618	1,584,061	2.257	5,787,317	0.212%	11,977,477	0.006%	324,362	\$16.27	\$41,716,595
<b>CUM. BENCH TOTAL</b>		HGD/LGD			18,061,264	0.639	11,519,121	2.841	51,309,981	0.225%	89,724,936	0.007%	2,854,809	\$17.09	\$309,671,834

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	IVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
460															
460	10	UDF		2.65	23,811	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			23,811										
CUMULATIVE TOTAL		UDF			195,481										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
460	10	WST	1213	2.65	204,855	0.133	27,246	0.993	203,421	0.000%	0	0.001%	4,516	\$2.35	\$482,863
460	10	WST	1221	2.65	292,513	0.107	31,299	0.529	154,740	0.040%	257,952	0.001%	6,449	\$2.94	\$859,770
460	10	WST	1212	2.65	504,640	0.187	94,368	0.525	264,936	0.060%	667,523	0.008%	89,003	\$4.77	\$2,410,120
SUBTOTAL		WST			1,002,008	0.153	152,912	0.622	623,096	0.042%	925,475	0.005%	99,968	\$3.75	\$3,752,754
CUMULATIVE TOTAL		WST			5,103,951	0.095	483,149	0.458	2,335,459	0.042%	4,753,199	0.005%	515,838	\$2.79	\$14,224,337
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
460	10	LGD	1217	2.65	157,996	0.224	35,391	0.991	156,574	0.110%	383,154	0.001%	3,483	\$6.85	\$1,082,478
460	10	LGD	944	2.65	39,786	0.316	12,572	1.612	64,136	0.110%	96,485	0.004%	3,509	\$8.46	\$336,881
460	10	LGD	962	2.65	70,112	0.245	17,177	1.062	74,458	0.160%	247,311	0.001%	1,546	\$8.58	\$601,731
460	10	LGD	961	2.65	49,339	0.266	13,124	1.081	53,335	0.160%	174,038	0.003%	3,263	\$8.92	\$440,318
460	10	LGD	1222	2.65	188,605	0.362	68,275	0.85	160,314	0.130%	540,543	0.002%	8,318	\$9.59	\$1,808,810
SUBTOTAL		LGD			605,838	0.290	146,640	1.006	508,818	0.129%	1,441,531	0.002%	20,117	\$8.44	\$4,270,219
CUMULATIVE TOTAL		LGD			4,829,407	0.263	1,270,304	1.043	5,035,373	0.127%	13,626,247	0.007%	734,176	\$7.96	\$38,442,077
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
460	10	HGD	1210	2.65	278,230	0.459	127,708	1.314	365,595	0.100%	613,392	0.003%	18,402	\$10.42	\$2,900,712
460	10	HGD	1218	2.65	208,041	0.4	83,216	1.988	413,189	0.180%	825,572	0.001%	4,587	\$11.82	\$2,460,981
460	10	HGD	1211	2.65	284,534	0.411	116,943	2.39	680,035	0.180%	1,129,120	0.013%	81,548	\$12.09	\$3,441,456
460	10	HGD	1208	2.65	148,000	0.478	70,448	1.538	227,624	0.150%	489,425	0.008%	19,577	\$12.12	\$1,794,661
460	10	HGD	946	2.65	117,951	0.464	54,729	2.083	243,333	0.160%	418,059	0.001%	2,600	\$12.32	\$1,453,654
460	10	HGD	1209	2.65	258,837	0.52	134,595	1.801	466,166	0.140%	798,893	0.002%	11,413	\$12.61	\$3,265,468
460	10	HGD	1219	2.65	165,202	0.397	65,585	2.931	484,206	0.220%	801,255	0.008%	29,137	\$13.08	\$2,162,700
460	10	HGD	945	2.65	95,527	0.523	49,961	6.116	584,244	0.160%	336,982	0.007%	14,742	\$14.14	\$1,353,105
460	10	HGD	1220	2.65	278,718	0.635	176,986	2.672	744,734	0.260%	1,597,613	0.009%	55,302	\$17.95	\$5,008,789
460	10	HGD	1216	2.65	94,319	0.801	75,550	1.971	185,903	0.250%	519,846	0.002%	4,159	\$20.19	\$1,905,546
460	10	HGD	1215	2.65	321,598	1.276	410,359	3.206	1,031,044	0.190%	1,347,103	0.008%	42,540	\$26.44	\$8,509,286
SUBTOTAL		HGD			2,250,957	0.607	1,366,081	2.411	5,426,063	0.179%	8,875,241	0.006%	284,005	\$15.22	\$34,254,359
CUMULATIVE TOTAL		HGD			15,868,852	0.738	11,781,438	3.265	52,209,480	0.245%	86,515,461	0.007%	2,424,784	\$18.31	\$308,784,338
BENCH TOTAL		HGD/LGD			2,766,795	0.649	1,612,621	2.163	5,934,871	0.170%	10,318,771	0.005%	304,122	\$13.97	\$38,524,578
CUM. BENCH TOTAL		HGD/LGD			20,818,059	0.626	13,931,742	2.750	67,244,852	0.218%	100,041,708	0.007%	3,158,930	\$16.68	\$347,199,412

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM LEVEL	BENCH HEIGHT	POLYGON MATERIAL	HOLE ID	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER %	COPPER POUNDS	MOLY %	MOLY POUNDS	#VAL TONNE	TOTAL VALUE
450															
450	10	UDF		2.65	31,110	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			31,110										
CUMULATIVE TOTAL		UDF			226,592										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
450	10	WST	1214	2.65	240,533	0.122	29,345	2.16	519,550	0.010%	53,028	0.000%	0	\$2.71	\$652,454
450	10	WST	1212	2.65	552,638	0.075	41,448	0.244	134,844	0.060%	731,014	0.017%	207,121	\$2.91	\$1,609,915
450	10	WST	1213	2.65	245,012	0.263	64,438	2.466	604,200	0.000%	0	0.000%	0	\$4.76	\$1,169,090
SUBTOTAL		WST			1,038,183	0.130	135,231	1.212	1,258,594	0.034%	784,043	0.009%	207,121	\$3.31	\$3,431,459
CUMULATIVE TOTAL		WST			6,142,134	0.101	618,380	0.585	3,584,053	0.041%	5,537,241	0.005%	722,959	\$2.87	\$17,656,796
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
450	10	LGD	961	2.65	50,417	0.096	4,840	0.486	24,502	0.160%	177,839	0.002%	2,223	\$6.06	\$305,516
450	10	LGD	944	2.65	59,882	0.246	14,731	1.37	82,038	0.070%	92,411	0.002%	2,640	\$6.18	\$370,434
450	10	LGD	946	2.65	132,108	0.253	33,423	0.703	92,872	0.160%	465,998	0.000%	0	\$8.63	\$1,140,378
450	10	LGD	1218	2.65	222,153	0.297	65,979	2.544	565,156	0.120%	587,715	0.001%	4,898	\$8.63	\$1,919,926
450	10	LGD	1209	2.65	249,715	0.408	101,884	0.657	164,063	0.080%	440,422	0.003%	16,516	\$8.91	\$2,224,914
450	10	LGD	962	2.65	75,743	0.267	20,223	2.337	177,010	0.160%	267,174	0.002%	3,340	\$9.21	\$668,100
450	10	LGD	1210	2.65	272,518	0.405	110,370	0.988	263,797	0.100%	600,798	0.004%	24,032	\$9.48	\$2,583,775
450	10	LGD	1221	2.65	331,609	0.363	120,374	1.431	474,533	0.130%	950,364	0.000%	0	\$9.73	\$3,228,007
SUBTOTAL		LGD			1,394,144	0.338	471,824	1.323	1,843,972	0.117%	3,582,750	0.002%	53,648	\$8.95	\$12,471,049
CUMULATIVE TOTAL		LGD			6,223,551	0.280	1,742,128	1.105	6,879,344	0.125%	17,108,997	0.006%	787,824	\$8.18	\$50,913,126
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
450	10	HGD	1208	2.65	152,502	0.407	62,069	1.247	190,171	0.120%	403,452	0.001%	3,362	\$10.12	\$1,544,214
450	10	HGD	1222	2.65	184,758	0.425	78,522	1.961	362,310	0.150%	610,982	0.002%	6,146	\$11.39	\$2,106,072
450	10	HGD	1220	2.65	400,025	0.36	144,009	1.262	504,832	0.210%	1,851,999	0.008%	70,552	\$11.85	\$4,741,729
450	10	HGD	1216	2.65	98,528	0.528	52,022	1.545	152,223	0.140%	304,099	0.002%	4,344	\$12.68	\$1,250,126
450	10	HGD	945	2.65	104,474	0.514	53,700	1.552	162,144	0.160%	368,521	0.003%	6,910	\$13.01	\$1,356,814
450	10	HGD	1219	2.65	158,585	0.48	78,121	3.129	496,212	0.260%	909,010	0.009%	31,466	\$15.56	\$2,469,449
450	10	HGD	1211	2.65	302,435	0.524	158,478	1.49	450,628	0.250%	1,666,885	0.015%	100,013	\$15.64	\$4,731,036
450	10	HGD	1217	2.65	182,327	0.674	122,888	1.683	306,856	0.170%	683,334	0.001%	4,420	\$15.88	\$2,897,717
450	10	HGD	1215	2.65	333,842	0.833	278,091	2.699	901,040	0.120%	883,194	0.004%	29,440	\$17.28	\$5,773,918
SUBTOTAL		HGD			1,917,476	0.536	1,025,897	1.839	3,526,416	0.182%	7,681,475	0.006%	258,253	\$14.02	\$26,874,076
CUMULATIVE TOTAL		HGD			17,906,127	0.714	12,787,335	3.113	65,735,896	0.239%	94,196,936	0.007%	2,683,007	\$18.74	\$335,628,412
BENCH TOTAL		HGD/LGD			3,311,619	0.452	1,497,721	1.822	5,370,388	0.154%	11,264,225	0.004%	311,901	\$11.88	\$39,346,126
CUM. BENCH TOTAL		HGD/LGD			24,129,678	0.602	14,529,463	2.895	62,615,240	0.209%	111,305,933	0.007%	3,470,831	\$16.02	\$386,541,538

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**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

18-12-95 @ 31 AM LEVEL	BENCH HEIGHT	POLYGON MATERIAL	HOLE ID	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER %	COPPER POUNDS	MOLY %	MOLY POUNDS	\$VAL TONNE	TOTAL VALUE
440															
440	10	UDF		2.65	52,167	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			52,167										
CUMULATIVE TOTAL		UDF			278,759										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
440	10	WST	1212	2.65	601,521	0.072	43,310	0.322	193,680	0.070%	928,287	0.011%	145,874	\$3.16	\$1,899,388
440	10	WST	1213	2.65	351,780	0.172	60,506	2.008	708,375	0.010%	77,554	0.000%	0	\$3.48	\$1,225,265
SUBTOTAL		WST			953,301	0.109	103,816	0.944	900,055	0.048%	1,005,842	0.007%	145,874	\$3.28	\$3,124,673
CUMULATIVE TOTAL		WST			7,098,435	0.102	722,198	0.833	4,494,118	0.042%	6,543,083	0.006%	868,833	\$2.93	\$20,780,469
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
440	10	LGD	944	2.65	150,822	0.2	30,164	1.388	206,023	0.080%	268,004	0.003%	9,975	\$5.72	\$862,873
440	10	LGD	961	2.65	43,081	0.147	6,334	0.8	34,472	0.160%	151,997	0.007%	1,900	\$6.95	\$299,437
440	10	LGD	1221	2.65	371,835	0.259	96,305	1.211	450,292	0.100%	819,755	0.000%	0	\$7.18	\$2,872,347
440	10	LGD	1211	2.65	320,475	0.288	91,656	0.496	158,958	0.090%	635,873	0.006%	42,392	\$7.19	\$2,303,636
440	10	LGD	1218	2.65	228,642	0.26	58,927	1.997	452,605	0.110%	549,826	0.001%	4,997	\$7.64	\$1,734,152
440	10	LGD	946	2.65	144,644	0.269	38,909	1.367	197,728	0.160%	510,216	0.001%	3,189	\$9.03	\$1,308,930
440	10	LGD	1222	2.65	185,233	0.35	64,831	1.71	318,748	0.110%	449,204	0.001%	4,084	\$9.03	\$1,673,679
SUBTOTAL		LGD			1,442,741	0.268	387,127	1.259	1,818,823	0.106%	3,382,678	0.002%	68,636	\$7.52	\$10,853,053
CUMULATIVE TOTAL		LGD			7,666,292	0.278	2,129,256	1.134	8,698,168	0.121%	20,491,672	0.005%	854,360	\$8.06	\$61,766,179
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
440	10	HGD	1210	2.65	253,549	0.485	122,971	0.97	245,943	0.110%	614,877	0.001%	6,590	\$11.04	\$2,800,083
440	10	HGD	1215	2.65	348,950	0.498	173,079	1.517	529,357	0.110%	846,232	0.003%	23,079	\$11.33	\$3,957,361
440	10	HGD	962	2.65	79,084	0.428	33,848	1.752	138,556	0.160%	278,962	0.002%	3,487	\$11.87	\$923,463
440	10	HGD	1219	2.65	189,565	0.423	71,726	2.248	380,844	0.200%	747,654	0.006%	22,430	\$12.80	\$2,171,709
440	10	HGD	1209	2.65	239,647	0.443	108,164	1.947	468,594	0.210%	1,108,498	0.003%	15,850	\$13.33	\$3,198,635
440	10	HGD	1217	2.65	185,541	0.554	108,330	3.788	740,319	0.210%	905,297	0.001%	4,311	\$15.51	\$3,008,434
440	10	HGD	1220	2.65	556,935	0.67	373,147	1.819	1,013,065	0.340%	4,174,625	0.007%	85,948	\$20.53	\$11,441,355
440	10	HGD	1216	2.65	104,487	0.776	81,082	3.18	332,268	0.330%	760,168	0.006%	13,821	\$22.26	\$2,327,104
440	10	HGD	1214	2.65	391,969	1.024	401,376	18.242	7,150,302	0.080%	691,314	0.000%	0	\$22.82	\$8,891,343
440	10	HGD	1208	2.65	155,139	1.533	237,829	4.401	682,769	0.510%	1,744,320	0.002%	6,840	\$39.65	\$8,154,897
SUBTOTAL		HGD			2,494,868	0.685	1,709,552	4.682	11,680,018	0.216%	11,872,948	0.003%	181,358	\$18.00	\$44,900,364
CUMULATIVE TOTAL		HGD			20,400,896	0.711	14,498,887	3.306	67,415,911	0.238%	106,069,882	0.004%	2,864,363	\$18.88	\$390,628,786
BENCH TOTAL		HGD/LGD			3,837,609	0.532	2,096,679	3.428	13,498,939	0.176%	16,258,621	0.003%	247,892	\$14.16	\$65,753,437
CUM. BENCH TOTAL		HGD/LGD			28,097,287	0.692	18,628,143	2.712	78,112,079	0.205%	128,691,558	0.004%	3,718,723	\$16.76	\$442,294,976



**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-98 9:31 AM LEVEL	BENCH HEIGHT	POLYGON MATERIAL	HOLE ID	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER %	COPPER POUNDS	MOLY %	MOLY POUNDS	IVAL TONNE	TOTAL VALUE
430															
430	10	UDF		2.65	152,288	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			152,288										
CUMULATIVE TOTAL		UDF			431,047										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
430	10	WST	1213	2.65	451,744	0.134	60,534	3.943	1,781,226	0.000%	0	0.000%	0	\$3.01	\$1,365,251
SUBTOTAL		WST			451,744	0.134	60,534	3.943	1,781,226	0.000%	0	0.000%	0	\$3.02	\$1,365,251
CUMULATIVE TOTAL		WST			7,647,179	0.104	782,730	0.831	6,275,344	0.039%	6,643,083	0.005%	868,833	\$2.93	\$22,145,720
														\$0.00	\$0
														\$0.00	\$0
430	10	LGD	944	2.65	195,163	0.193	37,667	1.228	239,660	0.100%	430,261	0.001%	4,303	\$6.12	\$1,196,229
430	10	LGD	1214	2.65	565,051	0.15	84,758	18.179	10,272,067	0.000%	0	0.000%	0	\$6.36	\$3,622,756
430	10	LGD	946	2.65	157,102	0.139	21,837	1.25	198,377	0.160%	554,159	0.000%	0	\$6.91	\$1,087,042
430	10	LGD	1212	2.65	655,020	0.257	168,340	0.749	490,810	0.110%	1,588,477	0.012%	173,288	\$7.33	\$4,800,441
430	10	LGD	1211	2.65	338,391	0.35	118,437	0.563	190,514	0.090%	671,421	0.005%	37,301	\$8.23	\$2,785,652
430	10	LGD	1210	2.65	233,235	0.401	93,527	0.65	151,603	0.090%	462,776	0.001%	5,142	\$9.07	\$2,115,742
430	10	LGD	1221	2.65	416,261	0.34	141,529	1.309	544,886	0.130%	1,193,006	0.000%	0	\$9.33	\$3,886,915
430	10	LGD	961	2.65	40,082	0.311	12,466	0.817	32,747	0.160%	141,386	0.002%	1,767	\$9.59	\$364,384
430	10	LGD	1216	2.65	113,039	0.464	52,450	0.953	107,726	0.070%	174,446	0.001%	2,492	\$9.59	\$1,085,156
SUBTOTAL		LGD			2,713,345	0.269	731,010	4.506	12,226,191	0.087%	5,215,931	0.004%	224,294	\$7.73	\$20,964,318
CUMULATIVE TOTAL		LGD			10,379,637	0.276	2,860,266	2.016	20,922,359	0.112%	25,707,604	0.005%	1,078,654	\$7.97	\$82,730,497
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
430	10	HGD	1209	2.65	228,665	0.437	99,926	1.567	356,317	0.140%	705,766	0.005%	25,206	\$11.22	\$7,567,653
430	10	HGD	1208	2.65	159,842	0.4	63,937	3.031	484,482	0.180%	634,305	0.002%	7,048	\$12.05	\$1,927,574
430	10	HGD	962	2.65	78,021	0.389	30,350	6.575	512,985	0.160%	275,209	0.001%	1,720	\$12.09	\$844,895
430	10	HGD	1222	2.65	180,728	0.607	109,702	1.172	211,814	0.160%	637,500	0.001%	3,984	\$14.42	\$2,607,484
430	10	HGD	1219	2.65	173,742	0.49	65,134	2.244	389,878	0.220%	842,678	0.011%	42,134	\$14.43	\$2,508,071
430	10	HGD	1220	2.65	701,122	0.517	362,480	3.827	2,683,196	0.350%	5,409,980	0.010%	154,571	\$18.79	\$13,181,461
430	10	HGD	1215	2.65	361,909	0.815	294,956	2.159	781,361	0.200%	1,595,743	0.002%	15,957	\$19.08	\$6,909,467
430	10	HGD	1218	2.65	232,272	1.028	238,776	6.334	1,471,212	0.460%	2,355,531	0.001%	5,121	\$30.58	\$7,107,597
430	10	HGD	1217	2.65	213,458	1.428	304,817	10.361	2,211,833	0.520%	2,447,062	0.005%	23,530	\$39.53	\$8,446,674
														\$0.00	\$0
SUBTOTAL		HGD			2,329,759	0.683	1,590,078	3.908	9,104,878	0.290%	14,903,794	0.005%	279,271	\$19.83	\$46,201,277
CUMULATIVE TOTAL		HGD			22,730,754	0.708	16,086,965	3.366	76,520,790	0.241%	120,973,677	0.006%	3,143,634	\$18.77	\$426,730,073
BENCH TOTAL		HGD/LGD			6,043,104	0.460	2,321,088	4.230	21,331,069	0.181%	20,119,726	0.005%	603,564	\$13.32	\$67,165,595
CUM. BENCH TOTAL		HGD/LGD			33,110,391	0.572	18,947,231	2.943	97,443,148	0.201%	146,681,280	0.006%	4,222,288	\$15.39	\$509,460,570

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	gVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
420															
420	10	UDF		2.65	281,278	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			281,278										
CUMULATIVE TOTAL		UDF			712,323										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
420	10	WST	944	2.65	232,629	0.119	27,683	0.649	150,977	0.040%	205,144	0.002%	10,257	\$3.16	\$734,786
420	10	WST	1214	2.65	734,344	0.178	130,713	4.725	3,469,776	0.010%	161,895	0.001%	16,189	\$4.16	\$3,067,569
SUBTOTAL		WST			966,974	0.164	158,396	3.744	3,620,753	0.017%	367,039	0.001%	26,447	\$3.93	\$3,802,374
CUMULATIVE TOTAL		WST			8,514,152	0.111	941,126	1.162	9,896,097	0.037%	6,910,122	0.006%	695,279	\$3.05	\$25,946,094
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
420	10	LGD	1213	2.65	533,784	0.33	178,149	3.258	1,739,069	0.000%	0	0.001%	11,768	\$6.01	\$3,215,068
420	10	LGD	1209	2.65	215,353	0.256	55,130	0.935	201,355	0.080%	427,295	0.002%	9,495	\$6.80	\$1,464,915
420	10	LGD	962	2.65	77,968	0.148	11,542	1.237	96,471	0.160%	275,094	0.001%	1,719	\$7.06	\$550,690
420	10	LGD	1211	2.65	353,835	0.289	102,258	0.75	265,376	0.090%	702,064	0.006%	46,804	\$7.29	\$2,580,276
420	10	LGD	1212	2.65	703,923	0.238	167,534	1.064	748,975	0.130%	2,017,449	0.007%	108,632	\$7.64	\$5,360,529
420	10	LGD	1222	2.65	176,755	0.363	64,162	1.683	297,479	0.110%	428,645	0.002%	7,794	\$9.23	\$1,632,978
SUBTOTAL		LGD			2,081,639	0.280	576,776	1.624	3,348,726	0.085%	3,850,548	0.004%	186,212	\$7.19	\$14,824,455
CUMULATIVE TOTAL		LGD			12,441,275	0.276	3,437,041	1.951	24,271,083	0.108%	29,558,151	0.005%	1,264,866	\$7.84	\$97,554,952
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
420	10	HGD	961	2.65	53,889	0.39	21,017	1.022	55,074	0.160%	190,066	0.001%	1,166	\$10.90	\$567,670
420	10	HGD	1208	2.65	165,800	0.457	75,770	2.481	411,349	0.130%	475,183	0.002%	7,311	\$11.47	\$1,902,864
420	10	HGD	1219	2.65	174,198	0.458	79,783	1.484	258,510	0.190%	729,678	0.006%	30,723	\$12.92	\$2,251,677
420	10	HGD	1210	2.65	210,605	0.467	98,353	1.753	369,191	0.220%	1,021,470	0.001%	4,643	\$13.95	\$2,939,571
420	10	HGD	946	2.65	162,838	0.741	120,663	3.054	497,307	0.160%	574,393	0.001%	3,590	\$16.98	\$2,767,660
420	10	HGD	1218	2.65	238,206	0.61	145,306	2.958	704,614	0.240%	1,260,371	0.001%	5,252	\$17.06	\$4,066,996
420	10	HGD	1215	2.65	374,117	0.775	289,941	3.221	1,205,031	0.180%	1,484,614	0.001%	8,248	\$18.12	\$6,783,120
420	10	HGD	1220	2.65	847,200	0.572	484,599	1.651	1,398,728	0.320%	5,976,816	0.018%	336,196	\$18.37	\$15,571,088
420	10	HGD	1217	2.65	228,927	0.754	172,611	3.713	850,007	0.220%	1,110,335	0.007%	35,329	\$18.99	\$4,350,510
420	10	HGD	1221	2.65	450,720	0.665	299,729	2.477	1,116,435	0.300%	2,981,002	0.001%	9,937	\$19.49	\$8,791,513
420	10	HGD	1216	2.65	129,776	1.177	152,746	2.093	271,621	0.160%	457,771	0.002%	5,722	\$23.78	\$3,068,133
SUBTOTAL		HGD			3,036,278	0.639	1,940,517	2.361	7,137,868	0.243%	16,261,721	0.007%	448,138	\$17.49	\$53,101,002
CUMULATIVE TOTAL		HGD			25,787,032	0.700	18,027,483	3.247	83,658,858	0.242%	137,235,368	0.006%	3,591,772	\$18.62	\$479,831,076
BENCH TOTAL		HGD/LGD			6,087,916	0.494	2,517,293	2.067	10,486,593	0.179%	20,112,268	0.006%	634,350	\$13.32	\$67,925,457
CUM. BENCH TOTAL		HGD/LGD			38,208,307	0.562	21,464,524	2.825	107,929,741	0.198%	166,793,549	0.006%	4,866,638	\$15.11	\$577,386,027

NON-METAL VALUES ARE NOT INCLUDED IN TOTAL METAL VALUES

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

18-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	#VAL	TOTAL	
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
410															
410	10	UDF		2.65	279,501	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
<b>SUBTOTAL</b>		UDF			279,501										
<b>CUMULATIVE TOTAL</b>		UDF			991,823										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
<b>SUBTOTAL</b>		WSF			0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
<b>CUMULATIVE TOTAL</b>		WSF			8,614,152	0.111	941,126	1.162	8,896,097	0.037%	6,910,122	0.005%	896,279	\$3.05	\$25,948,094
														\$0.00	\$0
														\$0.00	\$0
410	10	LGD	1199	2.65	72,391	0.169	12,234	0.413	29,898	0.080%	127,676	0.001%	1,596	\$5.01	\$362,897
410	10	LGD	1217	2.65	331,426	0.189	62,640	1.494	495,151	0.060%	436,402	0.001%	7,307	\$3.02	\$1,664,180
410	10	LGD	944	2.65	237,630	0.202	48,001	1.002	238,106	0.070%	366,719	0.000%	0	\$5.39	\$1,282,643
410	10	LGD	1214	2.65	934,535	0.248	231,765	2.774	2,592,399	0.030%	818,088	0.001%	20,603	\$5.42	\$5,069,713
410	10	LGD	1209	2.65	205,701	0.181	37,232	0.805	165,589	0.090%	408,143	0.002%	9,070	\$5.56	\$1,145,297
410	10	LGD	962	2.65	76,219	0.14	10,671	1.4	106,706	0.160%	268,853	0.001%	1,680	\$6.96	\$531,124
410	10	LGD	981	2.65	61,346	0.173	10,613	0.615	37,728	0.160%	216,392	0.002%	2,705	\$7.32	\$449,445
410	10	LGD	1212	2.65	787,999	0.271	213,548	1.118	880,983	0.120%	2,084,687	0.005%	86,862	\$7.91	\$6,233,523
410	10	LGD	1218	2.65	246,347	0.238	58,631	1.542	379,867	0.140%	760,342	0.007%	38,017	\$8.02	\$1,976,778
<b>SUBTOTAL</b>		LGD			2,953,694	0.232	685,333	1.688	4,926,427	0.081%	5,289,301	0.003%	167,840	\$6.34	\$18,715,600
<b>CUMULATIVE TOTAL</b>		LGD			15,394,870	0.268	4,122,375	1.897	29,197,510	0.103%	34,847,452	0.004%	1,432,706	\$7.55	\$116,270,553
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
410	10	HGD	1219	2.65	177,283	0.29	51,412	2.295	406,865	0.180%	703,517	0.003%	11,725	\$10.12	\$1,795,614
410	10	HGD	1221	2.65	493,723	0.592	292,284	1.082	534,209	0.050%	544,236	0.000%	0	\$11.13	\$5,497,752
410	10	HGD	1220	2.65	375,519	0.363	136,314	1.94	728,507	0.210%	1,738,543	0.016%	132,460	\$12.04	\$4,525,371
410	10	HGD	1198	2.65	680,551	0.421	286,512	4.417	3,005,993	0.170%	2,550,605	0.008%	120,028	\$12.41	\$8,456,685
410	10	HGD	1208	2.65	290,879	0.502	146,021	4.15	1,207,149	0.130%	833,662	0.001%	6,413	\$12.55	\$3,655,675
410	10	HGD	946	2.65	165,795	0.547	90,690	1.02	169,110	0.160%	584,823	0.005%	18,276	\$13.42	\$2,226,522
410	10	HGD	1215	2.65	439,122	1.04	456,687	3.586	1,574,691	0.260%	2,517,052	0.002%	19,362	\$24.66	\$10,836,272
410	10	HGD	1216	2.65	582,413	1.188	691,906	3.979	2,317,420	0.390%	5,007,595	0.004%	-51,360	\$30.71	\$17,895,181
410	10	HGD	1213	2.65	628,464	0.207	130,092	90.935	57,149,367	0.310%	4,295,125	0.001%	13,855	\$31.60	\$20,033,647
<b>SUBTOTAL</b>		HGD			3,833,749	0.595	2,281,918	17.501	67,093,313	0.222%	18,775,157	0.004%	373,480	\$19.54	\$74,922,719
<b>CUMULATIVE TOTAL</b>		HGD			29,600,781	0.888	20,309,401	5.093	150,761,971	0.238%	156,010,565	0.006%	3,985,252	\$18.74	\$554,753,794
														\$0.00	\$0
														\$0.00	\$0
<b>BENCH TOTAL</b>		HGD/LGD			6,787,344	0.437	2,967,251	10.611	72,019,740	0.161%	24,064,458	0.004%	541,319	\$13.80	\$93,638,319
<b>CUM. BENCH TOTAL</b>		HGD/LGD			44,995,661	0.543	24,431,776	3.999	179,949,481	0.192%	190,858,007	0.005%	5,397,957	\$14.91	\$671,024,346

COPPER AND MOLYBDENUM ARE NOT INCLUDED IN TOTAL METAL VALUES

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	*VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
400															
400	10	UDF		2.65	401,507	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			401,507										
CUMULATIVE TOTAL		UDF			1,393,330										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
400	10	WST	1214	2.65	1,157,623	0.052	60,196	0.49	567,235	0.000%	0	0.001%	25,521	\$0.00	\$1,092,750
400	10	WST	1213	2.65	743,611	0.111	82,541	3.378	2,511,917	0.030%	491,814	0.002%	32,788	\$3.34	\$2,494,645
SUBTOTAL		WST			1,901,234	0.075	142,737	1.620	3,079,152	0.012%	491,814	0.001%	58,309	\$1.89	\$3,587,395
CUMULATIVE TOTAL		WST			10,415,386	0.104	1,083,863	1.246	12,975,249	0.032%	7,401,936	0.004%	953,588	\$2.84	\$29,536,489
														\$0.00	\$0
400	10	LGD	1212	2.65	836,456	0.106	88,876	1.185	993,570	0.130%	2,403,019	0.001%	18,485	\$5.54	\$4,651,491
400	10	LGD	1221	2.65	542,990	0.285	154,752	0.897	487,062	0.060%	718,252	0.000%	0	\$6.43	\$3,493,365
400	10	LGD	1217	2.65	331,936	0.241	79,997	1.329	441,143	0.090%	658,614	0.002%	14,636	\$6.64	\$2,208,664
400	10	LGD	944	2.65	233,366	0.288	67,210	1.485	346,549	0.090%	463,036	0.001%	5,145	\$7.43	\$1,735,765
400	10	LGD	1208	2.65	326,230	0.302	98,522	1.896	618,533	0.080%	575,371	0.003%	21,576	\$7.47	\$2,436,518
400	10	LGD	1209	2.65	279,988	0.248	69,437	1.079	302,107	0.140%	864,175	0.002%	12,345	\$8.08	\$2,263,232
400	10	LGD	1219	2.65	220,956	0.289	63,857	4.123	911,010	0.110%	535,841	0.002%	9,743	\$8.57	\$1,697,043
400	10	LGD	961	2.65	114,212	0.264	30,152	1.005	114,783	0.160%	402,871	0.001%	2,518	\$8.87	\$1,013,685
400	10	LGD	1199	2.65	90,802	0.274	24,880	0.853	77,454	0.160%	320,294	0.004%	8,007	\$9.00	\$817,474
400	10	LGD	1216	2.65	594,672	0.41	243,815	0.788	474,548	0.090%	1,179,923	0.002%	26,221	\$9.24	\$5,499,857
SUBTOTAL		LGD			3,573,611	0.258	921,497	1.334	4,766,760	0.103%	8,121,397	0.002%	118,876	\$7.28	\$26,016,113
CUMULATIVE TOTAL		LGD			18,968,481	0.266	5,043,872	1.791	33,964,270	0.103%	42,968,849	0.004%	1,551,381	\$7.50	\$142,288,605
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
400	10	HGD	1218	2.65	258,634	0.38	98,281	1.684	435,539	0.180%	1,028,341	0.001%	5,702	\$11.43	\$2,959,102
400	10	HGD	1220	2.65	374,274	0.441	165,056	1.371	513,129	0.200%	1,650,263	0.012%	99,016	\$12.90	\$4,829,798
400	10	HGD	1198	2.65	837,770	0.628	524,444	0.953	798,395	0.210%	3,878,625	0.005%	92,348	\$16.06	\$13,456,988
400	10	HGD	957	2.65	146,918	1.163	170,865	1.146	168,368	0.160%	518,237	0.001%	3,239	\$23.35	\$3,432,354
400	10	HGD	1215	2.65	444,207	2.076	922,173	6.47	2,874,018	0.330%	3,231,714	0.002%	19,586	\$43.87	\$19,500,472
SUBTOTAL		HGD			2,081,802	0.912	1,880,818	2.323	4,789,449	0.227%	10,305,180	0.005%	219,891	\$21.43	\$44,178,713
CUMULATIVE TOTAL		HGD			31,662,684	0.701	22,180,219	4.912	185,641,420	0.238%	186,315,735	0.006%	4,185,143	\$18.92	\$698,832,606
BENCH TOTAL		HGD/LGD			8,635,414	0.497	2,802,316	1.696	8,566,210	0.148%	18,426,577	0.003%	338,567	\$12.46	\$70,196,826
CUM. BENCH TOTAL		HGD/LGD			50,631,098	0.538	27,234,091	3.743	189,505,691	0.187%	209,284,564	0.005%	5,736,524	\$14.84	\$741,221,172

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

18-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
390															
390	10	UDF		2.65	525,891	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			525,891										
CUMULATIVE TOTAL		UDF			1,919,221										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
390	10	WST	1214	2.65	1,324,238	0.044	58,268	0.228	301,928	0.000%	0	0.001%	29,194	\$0.78	\$1,003,349
390	10	WST	1213	2.65	857,263	0.137	117,445	3.839	3,291,032	0.020%	377,988	0.004%	75,598	\$3.59	\$3,085,027
390	10	WST	1217	2.65	486,285	0.118	57,382	0.627	304,901	0.080%	643,245	0.003%	32,162	\$3.69	\$1,793,831
390	10	WST	1221	2.65	618,708	0.182	112,605	0.681	421,340	0.040%	545,807	0.001%	13,640	\$4.18	\$2,585,390
SUBTOTAL		WST			3,286,494	0.105	345,698	1.314	4,319,199	0.022%	1,566,839	0.002%	150,594	\$2.58	\$8,487,597
CUMULATIVE TOTAL		WST			13,701,881	0.104	1,429,561	1.282	17,294,448	0.030%	8,988,774	0.004%	1,104,183	\$2.77	\$38,003,086
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
390	10	LGD	1219	2.65	232,138	0.189	39,231	1.643	381,403	0.070%	358,243	0.002%	10,238	\$5.00	\$1,182,552
390	10	LGD	1220	2.65	374,491	0.191	71,528	0.794	297,348	0.080%	660,489	0.004%	33,024	\$5.45	\$2,041,195
390	10	LGD	1218	2.65	690,473	0.288	198,858	0.9	621,425	0.050%	761,115	0.004%	60,889	\$6.20	\$4,285,713
390	10	LGD	1199	2.65	198,618	0.227	44,832	0.545	107,157	0.120%	520,161	0.002%	8,689	\$7.07	\$1,391,482
390	10	LGD	961	2.65	139,645	0.161	22,483	0.912	127,356	0.160%	492,583	0.001%	3,079	\$7.20	\$1,005,272
390	10	LGD	1198	2.65	922,393	0.25	230,598	0.474	437,214	0.160%	3,253,640	0.003%	61,006	\$8.53	\$7,871,256
390	10	LGD	956	2.65	369,097	0.253	93,382	0.457	168,677	0.160%	1,301,951	0.001%	8,137	\$8.58	\$3,168,124
SUBTOTAL		LGD			2,924,855	0.240	700,710	0.732	2,140,579	0.114%	7,348,183	0.003%	185,040	\$7.15	\$20,923,575
CUMULATIVE TOTAL		LGD			21,893,336	0.262	5,744,582	1.649	36,104,849	0.104%	80,317,032	0.004%	1,736,421	\$7.45	\$163,212,240
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
390	10	HGD	1208	2.65	384,143	0.498	181,343	7.864	2,863,619	0.090%	722,517	0.001%	8,028	\$12.19	\$4,449,140
390	10	HGD	1218	2.65	316,840	0.358	113,357	2.388	756,136	0.250%	1,745,177	0.001%	6,981	\$13.16	\$4,170,604
390	10	HGD	1223	2.65	394,278	0.577	227,498	2.407	949,027	0.150%	1,303,850	0.007%	60,846	\$13.93	\$5,496,774
390	10	HGD	1215	2.65	447,002	0.751	335,699	3.942	1,782,083	0.140%	1,379,658	0.001%	9,855	\$18.79	\$7,510,266
390	10	HGD	957	2.65	203,332	0.784	159,412	2.055	417,848	0.160%	717,230	0.001%	4,483	\$17.48	\$3,551,808
390	10	HGD	944	2.65	281,734	0.777	218,907	6.713	1,891,280	0.460%	2,857,135	0.002%	12,422	\$26.62	\$7,507,530
SUBTOTAL		HGD			2,007,129	0.618	1,236,217	4.306	8,639,993	0.197%	8,725,508	0.002%	102,616	\$18.29	\$32,686,123
CUMULATIVE TOTAL		HGD			23,889,713	0.698	23,428,438	4.878	184,181,413	0.238%	175,041,302	0.006%	4,287,787	\$18.76	\$631,618,629
BENCH TOTAL		HGD/LGD			4,931,884	0.393	1,938,927	2.188	10,780,571	0.148%	18,073,780	0.003%	287,656	\$10.87	\$83,609,698
CUM. BENCH TOTAL		HGD/LGD			55,563,048	0.525	29,171,018	3.605	200,286,262	0.184%	225,358,334	0.006%	6,024,179	\$14.31	\$794,830,870

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM	BENCH	POLYGON	HOLE	METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	IVAL	TOTAL	
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
380															
380	10	UDF		2.65	960,661	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
<b>SUBTOTAL</b>		UDF			960,661										
<b>CUMULATIVE TOTAL</b>		UDF			2,879,882										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
380	10	WST	1214	2.65	2,166,457	0.077	166,817	0.594	1,286,876	0.000%	0	0.001%	47,762	\$1.37	\$2,965,534
380	10	WST	1218	2.65	724,297	0.176	127,476	0.485	351,284	0.050%	798,399	0.002%	31,936	\$4.31	\$3,125,099
380	10	WST	1199	2.65	447,960	0.162	72,569	0.571	255,785	0.070%	691,307	0.005%	49,379	\$4.66	\$2,087,323
<b>SUBTOTAL</b>		WST			3,338,714	0.110	366,863	0.667	1,893,945	0.020%	1,489,706	0.002%	129,077	\$2.46	\$8,177,956
<b>CUMULATIVE TOTAL</b>		WST			17,040,594	0.105	1,796,424	1.126	19,188,393	0.028%	10,468,480	0.003%	1,233,260	\$2.71	\$46,181,042
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
380	10	LGD	1221	2.65	589,733	0.287	169,259	0.444	261,850	0.020%	260,036	0.001%	13,002	\$5.26	\$3,104,337
380	10	LGD	1220	2.65	375,959	0.201	75,568	0.915	344,002	0.070%	580,193	0.004%	33,154	\$5.36	\$2,016,051
380	10	LGD	981	2.65	137,781	0.074	10,194	0.331	45,599	0.180%	485,938	0.001%	3,037	\$5.67	\$781,379
380	10	LGD	1217	2.65	701,297	0.234	164,104	1.18	827,531	0.090%	1,391,484	0.002%	30,922	\$6.50	\$4,560,196
380	10	LGD	1223	2.65	460,797	0.29	133,631	1.141	525,770	0.090%	914,295	0.001%	10,159	\$7.36	\$3,407,328
380	10	LGD	1219	2.65	415,691	0.266	110,574	4.417	1,836,106	0.100%	916,441	0.002%	18,329	\$7.99	\$3,327,523
380	10	LGD	956	2.65	401,718	0.306	122,926	1.019	409,351	0.160%	1,417,018	0.001%	6,856	\$9.55	\$3,637,976
380	10	LGD	1198	2.65	928,524	0.28	259,987	0.895	831,029	0.180%	3,684,676	0.017%	347,997	\$9.66	\$8,999,258
<b>SUBTOTAL</b>		LGD			4,011,501	0.261	1,046,242	1.267	6,081,240	0.109%	9,650,081	0.005%	465,456	\$7.48	\$30,004,048
<b>CUMULATIVE TOTAL</b>		LGD			25,904,837	0.262	6,790,825	1.690	41,186,089	0.105%	89,867,113	0.004%	2,201,677	\$7.48	\$193,216,290
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
380	10	HGD	1215	2.65	453,763	0.483	219,168	2.148	974,684	0.130%	1,300,489	0.002%	20,006	\$11.81	\$5,364,259
380	10	HGD	957	2.65	291,792	0.481	140,352	0.621	181,203	0.160%	1,029,264	0.001%	6,433	\$12.28	\$3,583,302
380	10	HGD	1218	2.65	324,663	0.324	105,191	8.781	2,850,870	0.190%	1,359,943	0.003%	21,473	\$12.35	\$4,018,591
380	10	HGD	944	2.65	281,702	1.381	389,030	7.263	2,046,001	0.640%	3,974,692	0.003%	18,631	\$41.41	\$11,674,093
<b>SUBTOTAL</b>		HGD			1,351,921	0.632	653,741	4.477	6,062,757	0.257%	7,664,388	0.002%	66,545	\$18.23	\$24,640,244
<b>CUMULATIVE TOTAL</b>		HGD			35,021,633	0.693	24,280,177	4.861	170,234,170	0.237%	182,795,880	0.006%	4,364,302	\$18.74	\$666,258,873
<b>BENCH TOTAL</b>		HGD/LGD			6,363,421	0.354	1,899,983	2.076	11,133,997	0.146%	17,314,469	0.004%	632,000	\$10.19	\$54,644,294
<b>CUM. BENCH TOTAL</b>		HGD/LGD			60,928,470	0.610	31,071,007	3.470	211,420,269	0.181%	242,872,893	0.006%	6,559,179	\$13.84	\$849,475,193

NO MINERAL CONSTRAINTS USED. ALL 1991 DRILL HOLES INCLUDED IN DATABASE WITH 1995 ASSAYS. MOLYBDENUM VALUES ARE NOT INCLUDED IN TOTAL METAL VALUES

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	6VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
370															
370	10	UDF		2.65	387,827	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			387,827										
CUMULATIVE TOTAL		UDF			3,267,710										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
370	10	WST	960	2.65	1,478,793	0	0	0	0	0.000%	0	0.000%	0	\$0.00	\$0
370	10	WST	1221	2.65	553,770	0.064	35,441	0.378	209,325	0.010%	122,085	0.000%	0	\$1.39	\$768,554
370	10	WST	1214	2.65	1,708,229	0.111	189,813	1.786	3,050,898	0.020%	753,199	0.002%	75,320	\$2.72	\$4,661,681
370	10	WST	1216	2.65	759,532	0.163	123,804	0.341	259,000	0.020%	334,898	0.002%	33,490	\$3.25	\$2,466,362
SUBTOTAL		WST			4,500,324	0.078	348,858	0.782	3,519,223	0.012%	1,210,180	0.001%	108,810	\$1.75	\$7,896,598
CUMULATIVE TOTAL		WST			21,540,919	0.100	2,145,282	1.054	22,707,616	0.025%	11,868,661	0.003%	1,342,069	\$2.51	\$54,077,640
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
370	10	LGD	1220	2.65	383,229	0.209	80,095	0.688	262,895	0.060%	675,900	0.003%	25,348	\$5.71	\$2,190,638
370	10	LGD	1219	2.65	500,211	0.195	97,541	1.547	773,826	0.100%	1,102,774	0.001%	11,028	\$6.23	\$3,117,170
370	10	LGD	958	2.65	432,116	0.138	59,632	0.281	121,425	0.160%	1,524,244	0.002%	19,053	\$6.69	\$2,890,902
370	10	LGD	1217	2.65	721,031	0.302	217,751	0.945	681,374	0.060%	1,430,839	0.002%	31,792	\$7.54	\$5,439,642
SUBTOTAL		LGD			2,036,587	0.223	455,019	0.903	1,839,520	0.105%	4,733,557	0.002%	87,219	\$6.70	\$13,638,352
CUMULATIVE TOTAL		LGD			27,941,424	0.269	7,245,844	1.540	43,025,809	0.105%	64,700,670	0.004%	2,289,098	\$7.40	\$208,854,641
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
370	10	HGD	1218	2.65	327,511	0.28	91,703	4.46	1,460,697	0.220%	1,588,480	0.002%	14,441	\$11.53	\$3,781,537
370	10	HGD	1199	2.65	833,901	0.524	332,164	1.37	868,445	0.160%	2,236,018	0.008%	111,801	\$13.13	\$8,327,281
370	10	HGD	1198	2.65	922,095	0.466	429,698	2.062	1,901,359	0.210%	4,269,024	0.011%	223,616	\$13.73	\$12,664,094
370	10	HGD	944	2.65	342,528	0.538	184,280	4.124	1,412,587	0.250%	1,887,862	0.001%	7,551	\$16.43	\$5,633,824
370	10	HGD	1223	2.65	528,880	0.686	362,812	5.805	3,070,149	0.160%	1,865,567	0.007%	81,619	\$16.70	\$8,841,405
370	10	HGD	1215	2.65	458,478	0.707	324,144	2.824	1,294,742	0.220%	2,223,694	0.001%	10,108	\$18.04	\$8,276,696
370	10	HGD	957	2.65	369,193	0.854	315,291	0.598	220,039	0.160%	1,302,290	0.001%	8,139	\$18.27	\$6,746,155
SUBTOTAL		HGD			3,582,587	0.569	2,040,091	2.955	10,228,019	0.195%	15,372,938	0.006%	457,274	\$15.15	\$34,270,982
CUMULATIVE TOTAL		HGD			38,604,220	0.882	20,320,267	4.875	180,482,189	0.233%	198,078,826	0.006%	4,811,578	\$18.41	\$710,829,868
BENCH TOTAL		HGD/LGD			6,619,174	0.444	2,495,110	2.148	12,087,539	0.182%	20,106,493	0.004%	644,493	\$12.09	\$67,909,344
CUM. BENCH TOTAL		HGD/LGD			86,645,644	0.504	33,568,111	3.358	223,487,798	0.179%	282,779,299	0.006%	7,100,672	\$13.79	\$917,384,507

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	VAL	TOTAL		
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE		
360																	
360	10	UDF		2.65	1,580,162	0	0	0	0	0.000%	0	0.000%	0	\$0.00			
<b>SUBTOTAL</b>							1,580,162										
<b>CUMULATIVE TOTAL</b>							4,847,872										
														\$0.00	\$0		
														\$0.00	\$0		
														\$0.00	\$0		
														\$0.00	\$0		
														\$0.00	\$0		
														\$0.00	\$0		
360	10	WST	1216	2.65	804,443	0.01	8,044	0.1	80,444	0.000%	0	0.000%	0	\$0.18	\$147,052		
360	10	WST	1217	2.65	730,148	0.19	138,728	0.85	620,628	0.060%	985,820	0.003%	48,291	\$4.89	\$3,574,561		
<b>SUBTOTAL</b>							1,534,591	0.096	146,773	0.457	701,070	0.029%	985,820	0.001%	48,291	\$2.43	\$3,721,613
<b>CUMULATIVE TOTAL</b>							23,075,510	0.099	2,292,056	1.014	23,408,688	0.025%	12,634,480	0.003%	1,390,360	\$2.50	\$57,799,253
														\$0.00	\$0		
														\$0.00	\$0		
														\$0.00	\$0		
														\$0.00	\$0		
														\$0.00	\$0		
360	10	LGD	1219	2.65	531,450	0.169	89,815	1.494	793,988	0.090%	1,054,480	0.002%	23,433	\$5.52	\$2,937,003		
360	10	LGD	944	2.65	328,871	0.204	86,841	1.47	480,206	0.080%	578,148	0.001%	7,202	\$5.80	\$1,867,414		
360	10	LGD	956	2.65	462,623	0.158	73,094	0.313	144,801	0.160%	1,631,853	0.001%	10,199	\$7.02	\$3,247,030		
360	10	LGD	1198	2.65	930,113	0.29	269,733	0.605	562,718	0.100%	2,050,548	0.004%	82,022	\$7.55	\$7,024,284		
360	10	LGD	1220	2.65	388,668	0.288	111,938	0.786	305,491	0.100%	858,861	0.004%	34,274	\$7.56	\$2,938,212		
360	10	LGD	1221	2.65	508,980	0.471	239,720	0.767	360,372	0.030%	338,819	0.001%	11,221	\$8.58	\$4,381,354		
<b>SUBTOTAL</b>							3,148,482	0.270	850,939	0.850	2,677,575	0.094%	6,508,506	0.002%	168,351	\$7.12	\$22,405,297
<b>CUMULATIVE TOTAL</b>							31,089,906	0.260	8,098,783	1.470	45,703,184	0.104%	71,207,178	0.004%	2,457,447	\$7.37	\$229,259,938
														\$0.00	\$0		
														\$0.00	\$0		
														\$0.00	\$0		
														\$0.00	\$0		
														\$0.00	\$0		
														\$0.00	\$0		
														\$0.00	\$0		
														\$0.00	\$0		
360	10	HGD	1218	2.65	327,717	0.3	98,315	3.204	1,050,004	0.180%	1,300,484	0.001%	7,225	\$10.48	\$3,437,511		
360	10	HGD	1223	2.65	593,555	0.595	353,165	0.708	419,050	0.030%	392,569	0.002%	28,171	\$10.54	\$6,281,798		
360	10	HGD	980	2.65	2,401,847	0.37	888,610	1.8	4,322,965	0.160%	8,471,551	0.013%	888,314	\$10.75	\$25,829,332		
360	10	HGD	1199	2.65	832,685	0.352	293,105	2.054	1,710,338	0.170%	3,120,783	0.008%	146,860	\$10.79	\$8,990,385		
360	10	HGD	957	2.65	408,898	0.418	170,018	0.868	354,748	0.160%	1,441,631	0.001%	9,010	\$11.28	\$4,613,965		
360	10	HGD	1215	2.65	484,790	2.046	950,960	1.966	913,776	0.160%	1,839,495	0.001%	10,247	\$37.73	\$17,541,829		
<b>SUBTOTAL</b>							6,029,090	0.548	2,754,172	1.744	8,770,879	0.148%	16,366,513	0.008%	887,827	\$13.28	\$66,674,618
<b>CUMULATIVE TOTAL</b>							43,633,308	0.666	28,074,439	4.337	189,233,068	0.223%	214,448,140	0.006%	8,689,403	\$17.91	\$777,204,684
<b>BENCH TOTAL</b>							8,177,572	0.441	3,605,111	1.400	11,448,454	0.127%	22,873,019	0.006%	1,058,178	\$10.89	\$89,080,115
<b>CUM. BENCH TOTAL</b>							74,723,218	0.497	37,171,222	3.144	234,936,252	0.173%	285,652,316	0.005%	8,156,850	\$13.47	\$1,006,494,622



**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
350															
350	10	UDF		2.65	1,789,462	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			1,789,462										
CUMULATIVE TOTAL		UDF			6,637,333										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
350	10	WST	1217	2.65	798,498	0.155	123,767	0.935	746,596	0.070%	1,232,269	0.003%	52,812	\$4.62	\$3,694,764
SUBTOTAL		WST			798,498	0.155	123,767	0.935	746,596	0.070%	1,232,269	0.003%	52,812	\$4.63	\$3,694,764
CUMULATIVE TOTAL		WST			23,874,008	0.101	2,415,822	1.012	24,155,282	0.026%	13,866,750	0.003%	1,443,172	\$2.58	\$61,494,017
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
350	10	LGD	1221	2.65	973,341	0.266	258,909	0.807	785,486	0.020%	429,169	0.001%	21,458	\$5.00	\$4,872,520
350	10	LGD	1223	2.65	662,019	0.293	193,972	0.797	527,629	0.020%	291,900	0.004%	58,380	\$5.43	\$3,600,016
350	10	LGD	956	2.65	498,658	0.128	63,828	0.495	246,835	0.160%	1,758,956	0.004%	43,974	\$6.57	\$3,279,354
350	10	LGD	1218	2.65	330,243	0.244	80,579	2.098	692,850	0.120%	873,673	0.001%	7,261	\$7.68	\$2,540,234
350	10	LGD	1219	2.65	564,686	0.267	150,771	2.488	1,403,809	0.120%	1,493,901	0.002%	24,898	\$8.14	\$4,600,614
350	10	LGD	957	2.65	446,666	0.226	100,946	0.484	216,186	0.160%	1,575,565	0.002%	19,895	\$8.15	\$3,640,236
350	10	LGD	1220	2.65	533,198	0.357	190,352	0.823	438,822	0.100%	1,175,499	0.003%	35,265	\$8.67	\$4,626,770
350	10	LGD	1199	2.65	1,846,206	0.302	557,554	2.008	3,703,490	0.130%	5,291,236	0.005%	203,508	\$8.67	\$16,394,268
SUBTOTAL		LGD			6,856,015	0.273	1,596,911	1.369	6,015,107	0.100%	12,889,802	0.003%	414,460	\$7.44	\$43,554,033
CUMULATIVE TOTAL		LGD			36,944,921	0.202	9,693,694	1.464	63,718,291	0.103%	84,097,079	0.004%	2,871,907	\$7.38	\$272,613,971
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
350	10	HGD	944	2.65	309,597	0.386	119,504	1.561	483,281	0.130%	887,306	0.001%	6,825	\$10.13	\$3,137,085
350	10	HGD	960	2.65	2,694,173	0.37	896,844	1.8	4,849,511	0.160%	9,503,403	0.013%	772,151	\$10.75	\$28,975,395
350	10	HGD	1215	2.65	742,301	0.713	528,261	4.262	3,163,688	0.130%	2,127,440	0.009%	147,264	\$15.97	\$11,865,826
SUBTOTAL		HGD			3,746,071	0.439	1,645,609	2.268	8,496,479	0.152%	12,518,149	0.011%	926,261	\$11.74	\$43,978,306
CUMULATIVE TOTAL		HGD			47,379,390	0.648	30,720,048	4.173	187,729,548	0.217%	226,963,289	0.006%	6,626,665	\$17.33	\$821,182,990
BENCH TOTAL		HGD/LGD			9,801,088	0.338	3,242,520	1.720	16,511,587	0.120%	25,408,052	0.006%	1,340,721	\$9.12	\$87,532,338
CUM. BENCH TOTAL		HGD/LGD			64,324,301	0.479	40,413,742	2.992	251,447,839	0.167%	311,060,367	0.005%	9,497,572	\$12.97	\$1,093,996,961

NO GEOLOGICAL OR LITHOLOGICAL CONSTRAINTS USED. ALL 100% DRILL HOLES INCLUDED IN DATABASE WITH 100% ASSAYS. MOLYBDENUM VALUES ARE NOT INCLUDED IN TOTAL METAL VALUES.



**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

18-12-88 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	*VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
330															
330	10	UDF		2.65	2,161,126	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
<b>SUBTOTAL</b>		UDF			2,161,126										
<b>CUMULATIVE TOTAL</b>		UDF			10,750,279										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
330	10	WST	1202	2.65	749,533	0.115	86,196	0.621	465,460	0.080%	1,321,948	0.010%	165,244	\$4.19	\$3,140,873
330	10	WST	1215	2.65	772,743	0.184	142,185	1.1	850,017	0.050%	851,803	0.002%	34,072	\$4.57	\$3,536,088
330	10	WST	1223	2.65	794,656	0.222	176,414	1.187	943,257	0.030%	525,574	0.001%	17,519	\$4.65	\$3,701,216
<b>SUBTOTAL</b>		WST			2,316,932	0.175	404,795	0.975	2,258,734	0.053%	2,699,325	0.004%	216,835	\$4.48	\$10,380,176
<b>CUMULATIVE TOTAL</b>		WST			26,180,940	0.108	2,820,617	1.009	26,414,018	0.029%	16,568,075	0.003%	1,680,007	\$2.74	\$71,874,193
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
330	10	LGD	956	2.65	603,319	0.056	33,786	0.2	120,664	0.160%	2,128,143	0.001%	13,301	\$5.35	\$3,230,072
330	10	LGD	1217	2.65	858,176	0.210	185,368	1.024	876,772	0.090%	1,702,756	0.002%	37,839	\$6.17	\$5,302,460
330	10	LGD	1220	2.65	582,660	0.296	172,467	0.964	561,884	0.080%	1,027,635	0.006%	77,073	\$7.17	\$4,181,380
330	10	LGD	1221	2.65	883,381	0.313	278,498	1.181	1,043,274	0.070%	1,383,284	0.001%	19,475	\$7.22	\$6,379,695
330	10	LGD	1199	2.65	1,963,438	0.251	492,823	1.185	2,326,674	0.110%	4,761,499	0.003%	129,859	\$7.32	\$14,368,336
330	10	LGD	1219	2.65	679,428	0.295	200,431	1.379	936,931	0.100%	1,497,880	0.001%	14,979	\$7.80	\$5,301,408
330	10	LGD	1218	2.65	352,753	0.248	87,483	3.575	1,281,093	0.150%	1,166,530	0.001%	7,777	\$8.90	\$3,142,326
330	10	LGD	960	2.65	2,464,876	0.312	769,041	0.745	1,838,333	0.160%	8,694,585	0.004%	217,365	\$9.59	\$23,636,410
<b>SUBTOTAL</b>		LGD			8,388,032	0.264	2,217,896	1.069	8,965,424	0.121%	22,342,292	0.003%	517,667	\$7.82	\$65,564,026
<b>CUMULATIVE TOTAL</b>		LGD			51,417,735	0.261	13,429,019	1.361	69,485,266	0.105%	118,802,722	0.003%	3,752,908	\$7.38	\$379,478,780
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
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														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
330	10	HGD	957	2.65	697,176	0.491	342,314	0.49	341,616	0.160%	2,459,214	0.002%	30,740	\$12.41	\$8,653,575
<b>SUBTOTAL</b>		HGD			697,176	0.491	342,314	0.490	341,616	0.160%	2,459,214	0.002%	30,740	\$12.41	\$8,653,575
<b>CUMULATIVE TOTAL</b>		HGD			82,683,328	0.623	32,866,271	3.910	208,799,072	0.211%	245,835,814	0.006%	7,519,309	\$16.69	\$682,888,200
<b>BENCH TOTAL</b>		HGD/LGD			9,085,208	0.282	2,560,210	1.024	9,307,040	0.124%	24,801,807	0.003%	548,407	\$8.17	\$74,217,601
<b>CUM. BENCH TOTAL</b>		HGD/LGD			104,311,066	0.445	46,395,289	2.649	276,284,338	0.158%	364,436,536	0.005%	11,272,216	\$12.10	\$1,262,368,980

NOTE: CALC. CONCENTRATIONS USED. ALL HOLE DRILL HOLES INCLUDED IN DATABASE WITH 1995 ASSAYS. MOLYBDENUM VALUES ARE NOT INCLUDED IN TOTAL METAL VALUES

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

250m SEARCH RADIUS

19-12-95 9:31 AM	BENCH	POLYGON	HOLE	DENSITY	METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	#VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID		TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
320															
320	10	UDF		2.65	2,418,524	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
<b>SUBTOTAL</b>		UDF			2,418,524										
<b>CUMULATIVE TOTAL</b>		UDF			13,168,803										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
320	10	WST	1215	2.65	781,054	0.135	105,442	0.647	505,342	0.010%	172,193	0.001%	17,219	\$2.59	\$2,021,929
320	10	WST	1221	2.65	803,586	0.166	133,397	0.607	487,783	0.030%	531,487	0.001%	17,716	\$3.63	\$2,916,693
320	10	WST	1217	2.65	870,883	0.163	141,921	1.13	983,872	0.060%	1,151,715	0.003%	57,586	\$4.52	\$3,938,190
<b>SUBTOTAL</b>		WST			2,455,523	0.165	380,761	0.805	1,976,997	0.034%	1,855,395	0.002%	92,521	\$3.82	\$8,876,813
<b>CUMULATIVE TOTAL</b>		WST			28,646,273	0.112	3,201,377	0.991	28,391,012	0.029%	18,421,470	0.003%	1,752,528	\$2.82	\$80,751,006
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
320	10	LGD	1223	2.65	825,517	0.189	158,023	1.999	1,650,209	0.060%	1,091,971	0.001%	18,200	\$5.13	\$4,236,857
320	10	LGD	1202	2.65	809,447	0.134	108,466	0.738	597,372	0.110%	1,962,975	0.017%	303,369	\$5.35	\$4,329,271
320	10	LGD	1203	2.65	86,704	0.155	13,439	0.836	72,484	0.110%	210,264	0.002%	3,823	\$5.70	\$494,877
320	10	LGD	1199	2.65	2,042,148	0.252	514,621	0.685	1,398,870	0.120%	5,402,587	0.002%	90,043	\$7.51	\$15,336,087
320	10	LGD	956	2.65	717,083	0.205	147,002	0.2	143,417	0.160%	2,529,433	0.001%	15,809	\$7.75	\$5,557,138
320	10	LGD	1219	2.65	705,896	0.301	212,475	2.087	1,473,209	0.090%	1,400,613	0.002%	31,125	\$7.77	\$5,491,475
320	10	LGD	957	2.65	738,360	0.26	191,981	0.6	443,034	0.160%	2,604,592	0.002%	32,557	\$8.72	\$6,440,269
320	10	LGD	1220	2.65	803,084	0.364	219,523	1.068	844,084	0.100%	1,329,571	0.008%	79,774	\$8.84	\$5,333,568
<b>SUBTOTAL</b>		LGD			8,828,269	0.240	1,563,530	0.884	6,422,889	0.116%	16,832,006	0.004%	574,700	\$7.23	\$47,219,559
<b>CUMULATIVE TOTAL</b>		LGD			57,946,005	0.259	14,992,548	1.310	75,907,956	0.108%	135,134,728	0.003%	4,327,608	\$7.36	\$428,896,339
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
320	10	HGD	960	2.65	2,495,238	0.5	1,247,618	2.884	7,196,261	0.160%	8,801,677	0.019%	1,045,199	\$13.07	\$32,646,973
320	10	HGD	1218	2.65	384,801	0.471	171,821	4.084	1,489,848	0.250%	2,010,620	0.001%	8,042	\$15.35	\$5,603,928
<b>SUBTOTAL</b>		HGD			2,880,037	0.496	1,419,439	3.037	8,686,109	0.171%	10,812,298	0.017%	1,053,242	\$13.37	\$38,250,901
<b>CUMULATIVE TOTAL</b>		HGD			56,753,367	0.617	34,385,710	3.865	215,485,181	0.209%	256,648,111	0.007%	8,572,551	\$16.52	\$821,139,101
<b>BENCH TOTAL</b>		HGD/LGD			9,388,307	0.318	2,982,969	1.609	16,108,798	0.132%	27,344,302	0.008%	1,827,941	\$9.10	\$85,470,460
<b>CLM. BENCH TOTAL</b>		HGD/LGD			113,699,371	0.434	49,378,259	2.563	291,393,136	0.166%	391,782,838	0.005%	12,900,159	\$11.85	\$1,347,837,440

NOTE: THESE VALUES ARE NOT INCLUDED IN TOTAL METAL VALUES

BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY															
250m SEARCH RADIUS															
18-12-95 9:31 AM	BENCH	POLYGON	HOLE	METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	#VAL	TOTAL	
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
310															
310	10	UDF		2.65	2,521,913	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			2,521,913										
CUMULATIVE TOTAL		UDF			15,690,716										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
310	10	WST	1217	2.65	950,363	0.124	117,845	0.799	759,340	0.020%	419,038	0.002%	41,904	\$2.72	\$2,565,799
310	10	WST	1221	2.65	1,230,647	0.177	217,825	0.58	713,775	0.020%	542,622	0.002%	54,262	\$3.52	\$4,337,926
310	10	WST	1202	2.65	693,108	0.101	80,204	0.774	691,266	0.100%	1,068,966	0.011%	216,588	\$4.55	\$4,063,766
SUBTOTAL		WST			3,074,118	0.139	425,873	0.704	2,164,381	0.043%	2,930,625	0.005%	312,752	\$3.57	\$10,987,491
CUMULATIVE TOTAL		WST			31,720,392	0.114	3,627,281	0.863	30,655,394	0.031%	21,352,095	0.003%	2,065,280	\$2.89	\$91,738,496
														\$0.00	\$0
310	10	LGD	1200	2.65	483,686	0.163	78,841	0.8	290,211	0.080%	959,709	0.003%	31,990	\$5.23	\$2,531,242
310	10	LGD	1223	2.65	1,168,645	0.181	211,525	2.379	2,780,208	0.090%	2,318,776	0.001%	25,764	\$5.91	\$6,911,434
310	10	LGD	1215	2.65	788,941	0.297	234,315	4.437	3,500,531	0.050%	869,658	0.001%	17,393	\$7.12	\$5,624,982
310	10	LGD	1220	2.65	710,845	0.292	207,587	1.533	1,089,725	0.080%	1,410,428	0.002%	31,343	\$7.51	\$5,340,447
310	10	LGD	1199	2.65	1,637,601	0.258	422,553	1.492	2,443,599	0.120%	4,332,874	0.004%	144,429	\$7.78	\$12,748,329
310	10	LGD	1219	2.65	878,468	0.232	203,804	2.556	2,245,363	0.130%	2,517,693	0.001%	19,387	\$7.87	\$6,918,273
310	10	LGD	1201	2.65	14,340	0.238	3,413	3.454	49,532	0.140%	44,281	0.009%	2,845	\$8.43	\$121,105
310	10	LGD	948	2.65	42,772	0.233	9,966	1.523	65,141	0.160%	150,872	0.004%	3,772	\$8.49	\$363,170
310	10	LGD	947	2.65	5,117	0.24	1,228	2.039	10,433	0.160%	18,048	0.007%	790	\$8.71	\$44,602
310	10	LGD	949	2.65	381,139	0.28	108,719	3.026	1,153,328	0.160%	1,344,426	0.006%	50,416	\$9.57	\$3,650,304
SUBTOTAL		LGD			6,111,762	0.242	1,479,930	2.230	13,628,068	0.104%	13,988,746	0.002%	328,109	\$7.24	\$44,253,888
CUMULATIVE TOTAL		LGD			64,087,767	0.257	18,472,479	1.398	89,536,023	0.106%	149,101,474	0.003%	4,655,717	\$7.35	\$470,952,228
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
310	10	HGD	1203	2.65	386,278	0.377	145,627	0.829	320,224	0.160%	1,362,553	0.004%	34,064	\$10.65	\$4,115,318
310	10	HGD	1218	2.65	422,250	0.28	118,230	4.189	1,768,808	0.210%	1,954,893	0.003%	27,927	\$11.20	\$4,733,892
310	10	HGD	960	2.65	2,508,187	0.472	1,183,864	4.262	10,689,895	0.160%	8,847,360	0.019%	1,050,624	\$12.92	\$32,447,517
SUBTOTAL		HGD			3,316,716	0.436	1,447,721	3.853	12,778,925	0.166%	12,164,808	0.015%	1,112,615	\$12.45	\$41,298,728
CUMULATIVE TOTAL		HGD			68,070,062	0.607	36,833,432	3.864	228,264,106	0.206%	268,812,918	0.007%	9,885,188	\$16.28	\$682,438,829
BENCH TOTAL		HGD/LGD			9,428,488	0.311	2,927,852	2.801	26,406,993	0.126%	26,131,862	0.007%	1,440,724	\$9.07	\$85,580,816
CUM. BENCH TOTAL		HGD/LGD			123,127,839	0.426	62,308,910	2.581	317,600,129	0.184%	417,914,390	0.005%	14,340,893	\$11.64	\$1,433,388,067

BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY															
250m SEARCH RADIUS															
19-12-95 9:31 AM	BENCH	POLYGON	HOLE	METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	WVAL	TOTAL	
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	
300															
300	10	UDF		2.65	2,728,445	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			2,728,445										
CUMULATIVE TOTAL		UDF			18,419,161										
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
300	10	WST	1221	2.65	1,242,244	0.088	108,833	0.215	267,082	0.010%	273,868	0.001%	27,387	\$1.70	
300	10	WST	1215	2.65	824,382	0.15	123,654	1.1	908,798	0.040%	726,982	0.001%	18,174	\$3.75	
300	10	WST	1223	2.65	1,201,577	0.207	248,727	1.437	1,726,667	0.040%	1,058,609	0.001%	26,480	\$4.74	
SUBTOTAL		WST			3,268,183	0.147	479,214	0.888	2,900,547	0.029%	2,060,438	0.001%	72,051	\$3.34	
CUMULATIVE TOTAL		WST			34,988,575	0.117	4,106,464	0.958	33,455,941	0.030%	23,412,532	0.003%	2,137,331	\$2.83	
														\$0.00	
														\$0.00	
300	10	LGD	1219	2.65	908,949	0.193	175,620	0.828	753,438	0.070%	1,404,264	0.002%	40,122	\$5.21	
300	10	LGD	1202	2.65	992,852	0.15	148,928	0.522	518,269	0.110%	2,407,749	0.020%	437,772	\$5.56	
300	10	LGD	1220	2.65	721,234	0.242	174,539	0.775	558,958	0.070%	1,113,033	0.002%	31,807	\$5.99	
300	10	LGD	1218	2.65	435,200	0.136	59,187	1.513	658,457	0.130%	1,247,285	0.002%	19,189	\$8.10	
300	10	LGD	1200	2.65	519,010	0.216	112,106	0.81	420,398	0.100%	1,144,220	0.004%	45,769	\$8.40	
300	10	LGD	1201	2.65	89,388	0.237	21,185	1.628	145,344	0.100%	197,066	0.003%	5,912	\$8.92	
300	10	LGD	947	2.65	17,819	0.192	3,383	0.878	15,435	0.160%	62,150	0.004%	1,554	\$7.69	
300	10	LGD	1199	2.65	1,593,078	0.278	442,875	2.04	3,249,875	0.110%	3,883,340	0.008%	210,728	\$7.94	
300	10	LGD	1203	2.65	657,098	0.207	136,019	0.933	613,073	0.180%	2,607,573	0.012%	173,838	\$8.49	
300	10	LGD	948	2.65	48,867	0.281	13,875	1.583	77,040	0.160%	171,668	0.004%	4,292	\$9.27	
SUBTOTAL		LGD			6,984,094	0.215	1,287,518	1.171	7,010,286	0.108%	14,218,349	0.007%	970,978	\$8.89	
CUMULATIVE TOTAL		LGD			70,041,861	0.254	17,759,997	1.378	86,848,308	0.106%	163,319,823	0.004%	6,626,694	\$7.30	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
300	10	HGD	949	2.65	413,741	0.342	141,499	2.934	1,213,915	0.160%	1,459,425	0.008%	72,971	\$10.54	
300	10	HGD	960	2.65	2,481,755	0.361	888,693	2.973	7,318,796	0.160%	8,683,573	0.044%	2,387,983	\$10.88	
300	10	HGD	1217	2.65	947,893	0.477	452,145	2.029	1,923,275	0.150%	3,134,816	0.001%	20,897	\$12.24	
SUBTOTAL		HGD			3,823,388	0.388	1,482,338	2.736	10,465,986	0.158%	13,277,816	0.029%	2,481,851	\$11.18	
CUMULATIVE TOTAL		HGD			62,893,470	0.593	37,315,789	3.786	238,720,093	0.203%	282,090,531	0.009%	12,187,017	\$16.98	
BENCH TOTAL		HGD/LGD			9,807,482	0.282	2,789,855	1.781	17,486,272	0.127%	27,495,964	0.018%	3,452,828	\$8.44	
CUM. BENCH TOTAL		HGD/LGD			132,935,321	0.414	85,075,766	2.522	338,286,401	0.162%	445,410,354	0.006%	17,793,711	\$11.41	

ALL CONTRIBUTIONS TO ALL 1998 HOLE LOCES INCLUDED IN DATABASE WITH 1998 ASSAYS. MOLYBDENUM VALUES ARE NOT INCLUDED IN TOTAL METAL VALUES

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

250m SEARCH RADIUS

18-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	\$VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
290															
290	10	UDF		2.65	2,868,101	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			2,868,101										
CUMULATIVE TOTAL		UDF			21,287,261										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
290	10	WST	1221	2.65	1,569,687	0.089	141,482	0.329	523,007	0.020%	700,931	0.001%	35,047	\$2.05	\$3,266,259
290	10	WST	1202	2.65	1,100,307	0.067	95,727	1	1,100,307	0.070%	1,698,031	0.023%	557,924	\$3.54	\$3,903,891
290	10	WST	1201	2.65	169,155	0.113	19,115	1.297	219,394	0.070%	281,046	0.002%	7,458	\$4.03	\$681,936
SUBTOTAL		WST			2,839,149	0.090	256,323	0.844	1,842,708	0.042%	2,660,008	0.010%	600,429	\$2.75	\$7,852,086
CUMULATIVE TOTAL		WST			37,847,724	0.115	4,382,788	0.933	35,298,849	0.031%	26,072,540	0.003%	2,737,760	\$2.92	\$110,510,007
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
290	10	LGD	1203	2.65	870,815	0.118	102,758	0.503	438,020	0.110%	2,111,799	0.018%	307,171	\$5.04	\$4,388,433
290	10	LGD	1220	2.65	723,784	0.233	188,842	0.648	467,564	0.060%	1,436,102	0.003%	47,870	\$6.37	\$4,609,749
290	10	LGD	1200	2.65	530,485	0.215	114,054	1.317	698,849	0.100%	1,169,519	0.006%	70,171	\$8.50	\$3,449,568
290	10	LGD	1219	2.65	943,088	0.182	152,777	4.014	3,785,475	0.110%	2,287,017	0.003%	62,373	\$8.51	\$6,148,230
290	10	LGD	1199	2.65	1,563,882	0.269	420,684	1.412	2,208,201	0.140%	4,828,871	0.006%	208,868	\$8.49	\$13,283,988
290	10	LGD	1218	2.65	672,795	0.213	143,305	1.322	889,435	0.200%	2,966,516	0.002%	29,665	\$9.22	\$6,208,171
290	10	LGD	949	2.65	453,493	0.277	125,818	3.043	1,379,981	0.160%	1,599,649	0.008%	79,982	\$9.52	\$4,323,089
SUBTOTAL		LGD			5,758,323	0.213	1,227,837	1.714	9,867,328	0.129%	16,397,473	0.006%	804,099	\$7.37	\$42,411,264
CUMULATIVE TOTAL		LGD			76,800,174	0.250	18,987,833	1.404	106,413,634	0.108%	179,717,298	0.004%	6,430,792	\$7.30	\$553,381,978
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
290	10	HGD	948	2.65	56,658	0.305	17,280	5.571	315,830	0.160%	199,848	0.010%	12,490	\$10.52	\$597,112
290	10	HGD	947	2.65	30,875	0.357	10,951	1.825	55,982	0.160%	108,204	0.005%	3,381	\$10.54	\$323,685
290	10	HGD	960	2.65	2,384,839	0.441	1,051,826	1.485	3,493,498	0.160%	8,411,566	0.032%	1,682,311	\$11.82	\$26,193,155
290	10	HGD	1223	2.65	1,214,241	0.559	878,761	4.402	5,345,091	0.100%	2,676,941	0.001%	26,769	\$12.70	\$15,436,572
SUBTOTAL		HGD			3,688,211	0.477	1,758,818	2.499	9,210,199	0.140%	11,396,548	0.021%	1,724,952	\$12.09	\$44,550,504
CUMULATIVE TOTAL		HGD			66,878,682	0.587	39,074,387	3.724	247,930,282	0.200%	283,487,079	0.009%	13,891,970	\$15.77	\$1,049,719,857
BENCH TOTAL		HGD/LGD			8,444,535	0.316	2,986,454	2.020	19,077,525	0.133%	27,794,021	0.012%	2,528,051	\$9.21	\$86,981,768
CUM. BENCH TOTAL		HGD/LGD			142,379,856	0.408	58,062,220	2.489	354,343,926	0.151%	473,204,375	0.008%	20,322,762	\$11.26	\$1,803,101,839

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

18-12-95 9:31 AM LEVEL	BENCH HEIGHT	POLYGON MATERIAL	HOLE ID	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER %	COPPER POUNDS	MOLY %	MOLY POUNDS	IVAL TONNE	TOTAL VALUE
280															
280	10	UDF		2.65	4,244,027	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			4,244,027										
CUMULATIVE TOTAL		UDF			25,531,288										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
280	10	WST	1219	2.65	977,832	0.099	98,805	1.202	1,175,354	0.040%	862,299	0.001%	21,557	\$2.95	\$2,893,081
280	10	WST	1202	2.65	1,198,748	0.123	147,448	1	1,198,748	0.070%	1,849,945	0.021%	554,984	\$4.12	\$4,947,083
280	10	WST	1223	2.65	1,232,157	0.23	283,396	0.78	961,082	0.070%	543,287	0.002%	54,329	\$4.42	\$5,447,556
280	10	WST	1200	2.65	548,808	0.148	81,223	1.362	747,473	0.080%	967,928	0.004%	48,398	\$4.88	\$2,680,422
SUBTOTAL		WST			3,957,540	0.164	608,870	1.032	4,082,855	0.048%	4,223,458	0.008%	679,268	\$4.03	\$15,968,142
CUMULATIVE TOTAL		WST			41,805,264	0.119	4,971,658	0.942	39,381,304	0.033%	30,295,999	0.004%	3,417,027	\$3.03	\$126,478,149
														\$0.00	\$0
280	10	LGD	1221	2.65	1,613,019	0.243	391,964	4.802	7,745,718	0.020%	711,219	0.002%	71,122	\$5.50	\$8,895,857
280	10	LGD	1199	2.65	1,511,237	0.191	288,846	1.082	1,635,159	0.110%	3,664,875	0.005%	166,585	\$6.34	\$9,582,262
280	10	LGD	1217	2.65	1,247,443	0.287	358,016	0.77	960,531	0.070%	1,925,097	0.002%	55,003	\$6.71	\$8,374,589
280	10	LGD	1203	2.65	858,735	0.179	117,914	1.167	768,744	0.130%	1,887,938	0.016%	232,362	\$6.71	\$4,425,096
280	10	LGD	1218	2.65	681,919	0.225	153,432	1.051	718,697	0.120%	1,804,048	0.002%	30,067	\$7.15	\$4,879,918
280	10	LGD	949	2.65	493,413	0.146	72,038	2.477	1,222,184	0.160%	1,740,461	0.005%	54,389	\$7.29	\$3,602,833
280	10	LGD	1201	2.65	272,974	0.158	43,130	4.665	1,273,425	0.140%	842,527	0.008%	36,108	\$7.41	\$2,026,842
280	10	LGD	960	2.65	2,308,709	0.254	586,412	0.844	1,948,551	0.160%	8,143,722	0.029%	1,478,050	\$8.68	\$20,037,841
280	10	LGD	1220	2.65	737,944	0.334	246,473	0.849	628,515	0.120%	1,952,264	0.006%	97,613	\$8.86	\$6,541,454
280	10	LGD	947	2.65	48,983	0.277	13,568	2.007	98,309	0.160%	172,782	0.007%	7,559	\$9.30	\$455,783
SUBTOTAL		LGD			9,574,378	0.237	2,271,694	1.775	16,995,833	0.108%	22,844,932	0.011%	2,226,859	\$7.19	\$68,822,475
CUMULATIVE TOTAL		LGD			85,374,552	0.249	21,259,427	1.446	123,409,467	0.108%	202,662,228	0.006%	8,657,851	\$7.29	\$622,204,453
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
280	10	HGD	1204	2.65	490,169	0.342	187,638	6.493	3,182,668	0.140%	1,512,891	0.023%	248,548	\$10.76	\$5,286,918
280	10	HGD	948	2.65	70,872	0.423	29,979	13.695	970,587	0.180%	249,992	0.003%	4,687	\$14.18	\$1,008,076
SUBTOTAL		HGD			601,041	0.362	197,617	7.403	4,153,255	0.143%	1,762,883	0.020%	253,234	\$11.22	\$6,294,994
CUMULATIVE TOTAL		HGD			87,140,723	0.589	38,272,004	3.755	252,083,547	0.199%	296,249,963	0.010%	14,145,203	\$15.73	\$1,056,014,652
BENCH TOTAL		HGD/LGD			10,138,419	0.244	2,469,210	2.087	21,149,088	0.110%	24,607,816	0.011%	2,480,092	\$7.41	\$75,117,469
CUM. BENCH TOTAL		HGD/LGD			152,615,275	0.397	60,531,431	2.482	375,493,014	0.148%	497,812,191	0.007%	22,802,854	\$11.00	\$1,678,219,105

NO GEOLOGICAL OR LITHOLOGICAL CONSTRAINTS USED - ALL 1988 DRILL HOLES INCLUDED IN DATABASE WITH 1995 ASSAYS - MOLYBDENUM VALUES ARE NOT INCLUDED IN TOTAL METAL VALUES



**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	6VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
270															
270	10	UDF		2.65	3,151,225	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
<b>SUBTOTAL</b>		UDF			3,151,225										
<b>CUMULATIVE TOTAL</b>		UDF			28,882,613										
														\$0.00	\$0
														\$0.00	\$0
270	10	WST	1219	2.65	1,014,175	0.089	90,262	0.7	709,923	0.030%	670,761	0.003%	67,076	\$2.41	\$2,446,041
270	10	WST	1200	2.65	558,002	0.104	56,032	1.184	649,514	0.050%	615,091	0.003%	36,905	\$3.30	\$1,844,914
270	10	WST	1199	2.65	1,471,510	0.094	138,322	0.727	1,089,788	0.060%	1,946,472	0.004%	129,765	\$3.32	\$4,892,680
270	10	WST	1218	2.65	712,014	0.105	74,761	0.607	432,192	0.060%	941,832	0.001%	15,697	\$3.47	\$2,474,537
270	10	WST	1201	2.65	368,282	0.093	34,064	0.598	219,037	0.070%	565,260	0.000%	0	\$3.55	\$1,302,516
270	10	WST	1220	2.65	743,809	0.165	122,728	0.368	273,722	0.030%	491,945	0.004%	65,593	\$3.56	\$2,648,623
270	10	WST	1223	2.65	1,243,531	0.218	271,090	0.947	1,177,624	0.030%	622,454	0.002%	54,830	\$4.54	\$5,646,299
<b>SUBTOTAL</b>		WST			6,109,323	0.129	789,260	0.742	4,531,800	0.045%	6,053,815	0.003%	369,866	\$3.48	\$21,255,560
<b>CUMULATIVE TOTAL</b>		WST			47,914,687	0.120	5,780,918	0.916	43,913,103	0.034%	36,349,813	0.004%	3,786,893	\$3.08	\$147,733,709
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
270	10	LGD	1202	2.65	1,286,352	0.127	163,367	1.077	1,385,401	0.130%	3,686,691	0.005%	992,571	\$5.86	\$7,540,088
270	10	LGD	1203	2.65	745,467	0.141	105,111	0.876	653,029	0.130%	2,136,513	0.017%	279,390	\$6.04	\$4,504,490
270	10	LGD	1204	2.65	591,938	0.178	105,365	2.939	1,739,705	0.100%	1,304,998	0.026%	339,299	\$6.25	\$3,706,250
270	10	LGD	948	2.65	80,627	0.101	8,143	1.06	85,465	0.160%	284,404	0.003%	5,333	\$6.26	\$505,253
270	10	LGD	949	2.65	519,468	0.106	55,064	1.544	802,058	0.160%	1,832,366	0.002%	22,905	\$6.45	\$3,352,332
270	10	LGD	960	2.65	2,244,433	0.151	338,909	0.6	1,346,660	0.160%	7,918,995	0.030%	1,484,437	\$6.97	\$15,642,173
270	10	LGD	947	2.65	68,788	0.188	12,932	2.513	172,865	0.160%	242,643	0.003%	4,550	\$7.98	\$549,283
<b>SUBTOTAL</b>		LGD			5,537,072	0.142	788,891	1.117	6,185,182	0.143%	17,404,610	0.026%	3,128,484	\$6.47	\$35,801,868
<b>CUMULATIVE TOTAL</b>		LGD			90,911,625	0.243	22,048,318	1.426	129,694,649	0.110%	219,966,838	0.006%	11,786,135	\$7.24	\$668,006,321
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
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														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
270	10	HGD	1217	2.65	1,253,100	0.375	489,913	1.028	1,288,187	0.180%	5,248,960	0.001%	27,626	\$11.49	\$14,400,797
270	10	HGD	1221	2.65	1,626,166	0.662	1,076,523	4.033	6,558,337	0.040%	1,434,033	0.001%	35,851	\$12.62	\$20,545,672
<b>SUBTOTAL</b>		HGD			2,879,266	0.537	1,546,436	2.725	7,846,524	0.105%	6,682,993	0.001%	63,477	\$12.14	\$34,946,668
<b>CUMULATIVE TOTAL</b>		HGD			70,019,891	0.583	40,818,440	3.712	258,830,071	0.186%	301,932,956	0.009%	14,208,680	\$15.58	\$1,080,961,320
<b>BENCH TOTAL</b>		HGD/LGD			8,416,341	0.277	2,335,327	1.667	14,031,706	0.130%	24,087,803	0.017%	3,191,961	\$8.41	\$70,748,537
<b>CUM. BENCH TOTAL</b>		HGD/LGD			160,931,616	0.391	62,866,757	2.420	389,524,720	0.147%	521,899,794	0.007%	25,994,815	\$10.67	\$1,748,967,641

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

18-12-98 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	#VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
260															
260	10	UDF		2.65	3,320,287	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			3,320,287										
CUMULATIVE TOTAL		UDF			32,002,800										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
260	10	WST	1199	2.65	1,435,527	0.03	43,068	0.2	287,105	0.030%	949,438	0.001%	31,648	\$1.35	\$1,942,459
260	10	WST	1221	2.65	1,627,883	0.089	144,864	0.274	445,985	0.010%	358,842	0.001%	35,884	\$1.77	\$2,876,079
260	10	WST	1203	2.65	561,397	0.071	39,859	1.581	887,569	0.080%	990,134	0.022%	272,287	\$3.69	\$2,073,870
260	10	WST	1218	2.65	752,178	0.104	78,227	0.426	320,428	0.070%	1,160,787	0.001%	16,583	\$3.69	\$2,779,361
260	10	WST	1200	2.65	527,252	0.138	72,761	1.447	762,934	0.050%	581,195	0.001%	11,624	\$3.91	\$2,084,332
260	10	WST	1204	2.65	473,915	0.118	55,922	1.574	745,943	0.080%	835,843	0.008%	83,584	\$4.44	\$2,108,137
SUBTOTAL		WST			5,377,953	0.081	434,898	0.642	3,449,964	0.041%	4,876,239	0.004%	451,610	\$2.57	\$13,844,238
CUMULATIVE TOTAL		WST			63,292,640	0.118	6,195,616	0.889	47,363,068	0.035%	41,226,053	0.004%	4,238,503	\$3.03	\$181,577,947
														\$0.00	\$0
260	10	LGD	1219	2.65	1,052,120	0.206	216,737	1.419	1,492,958	0.050%	1,159,762	0.002%	46,390	\$5.00	\$5,263,280
260	10	LGD	1202	2.65	1,334,425	0.111	148,121	0.949	1,266,370	0.120%	3,530,281	0.025%	735,475	\$5.30	\$7,073,241
260	10	LGD	960	2.65	2,180,048	0.097	211,465	0.76	1,656,837	0.160%	7,689,885	0.023%	1,105,421	\$6.13	\$13,377,212
260	10	LGD	948	2.65	86,811	0.108	9,354	1.445	125,153	0.180%	305,510	0.009%	17,185	\$8.48	\$559,833
260	10	LGD	1201	2.65	371,942	0.172	63,974	2.268	843,583	0.140%	1,147,986	0.014%	114,799	\$7.12	\$2,649,267
260	10	LGD	1220	2.65	744,330	0.277	208,179	1.362	1,013,778	0.100%	1,840,985	0.002%	32,819	\$7.50	\$5,589,603
260	10	LGD	947	2.65	91,219	0.191	17,423	3.642	332,221	0.180%	321,766	0.005%	10,056	\$8.27	\$755,457
260	10	LGD	949	2.65	551,607	0.207	114,201	3.732	2,058,935	0.180%	1,946,053	0.002%	24,328	\$8.55	\$4,721,890
260	10	LGD	1217	2.65	1,254,177	0.312	391,303	0.982	1,231,601	0.150%	4,147,474	0.002%	55,300	\$9.36	\$11,747,449
260	10	LGD	959	2.65	639,468	0.3	191,840	1.8	1,023,148	0.160%	2,255,853	0.010%	140,978	\$9.58	\$6,129,450
SUBTOTAL		LGD			8,306,037	0.189	1,670,898	1.330	11,044,683	0.132%	24,145,335	0.012%	2,282,748	\$6.97	\$87,866,682
CUMULATIVE TOTAL		LGD			99,217,661	0.238	23,618,915	1.417	140,639,212	0.112%	244,112,173	0.006%	14,066,883	\$7.22	\$718,873,003
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
260	10	HGD	1223	2.65	1,252,417	1.299	1,626,890	2.508	3,141,062	0.090%	2,484,993	0.002%	55,222	\$23.91	\$29,957,662
SUBTOTAL		HGD			1,252,417	1.299	1,626,890	2.508	3,141,062	0.090%	2,484,993	0.002%	55,222	\$23.92	\$29,957,662
CUMULATIVE TOTAL		HGD			71,272,408	0.598	42,445,329	3.681	263,071,133	0.184%	304,417,848	0.009%	14,263,802	\$15.73	\$1,120,818,982
BENCH TOTAL		HGD/LGD			9,558,464	0.335	3,197,487	1.484	14,185,825	0.128%	26,630,328	0.011%	2,337,970	\$9.19	\$87,824,343
CUM. BENCH TOTAL		HGD/LGD			170,480,070	0.387	66,064,245	2.388	403,710,345	0.148%	548,530,122	0.008%	28,332,785	\$10.77	\$1,838,791,985

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	IVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
250															
250	10	UDF		2.65	3,636,194	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			3,636,194										
CUMULATIVE TOTAL		UDF			36,636,996										
														\$0.00	\$0
														\$0.00	\$0
250	10	WST	1202	2.65	1,435,882	0	0	0	0	0.000%	0	0.000%	0	\$0.00	\$0
250	10	WST	1203	2.65	607,020	0.057	34,600	1.383	827,368	0.070%	936,773	0.049%	655,741	\$3.14	\$1,909,357
250	10	WST	1223	2.65	1,264,395	0.169	213,683	0.912	1,153,129	0.010%	278,751	0.003%	83,625	\$3.19	\$4,038,147
250	10	WST	1200	2.65	1,348,554	0.08	107,724	0.445	599,216	0.070%	2,078,048	0.001%	29,686	\$3.31	\$4,461,594
250	10	WST	1204	2.65	525,636	0.114	59,923	1.134	596,072	0.050%	579,414	0.007%	81,118	\$3.46	\$1,818,958
250	10	WST	1218	2.65	806,164	0.131	105,607	0.426	343,426	0.060%	1,066,371	0.001%	17,773	\$3.85	\$3,106,685
250	10	WST	1219	2.65	1,083,864	0.179	194,012	0.933	1,011,245	0.040%	956,804	0.001%	23,695	\$4.18	\$4,536,937
SUBTOTAL		WST			7,069,514	0.101	715,649	0.641	4,530,455	0.038%	6,895,160	0.006%	891,839	\$2.81	\$19,871,677
CUMULATIVE TOTAL		WST			60,362,056	0.114	6,811,165	0.860	61,893,523	0.035%	47,121,213	0.004%	5,130,342	\$3.01	\$181,449,624
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
250	10	LGD	960	2.65	2,141,628	0.085	182,038	0.901	1,929,607	0.160%	7,554,360	0.025%	1,180,369	\$5.97	\$12,794,641
250	10	LGD	947	2.65	115,070	0.134	15,419	1.344	154,654	0.160%	405,896	0.004%	10,147	\$6.85	\$789,336
250	10	LGD	1220	2.65	1,146,672	0.25	286,668	1.359	1,558,327	0.100%	2,527,976	0.002%	50,560	\$7.07	\$8,112,423
250	10	LGD	1201	2.65	462,216	0.186	85,972	3.806	1,759,195	0.140%	1,426,615	0.006%	61,141	\$7.67	\$3,552,725
250	10	LGD	1221	2.65	1,619,670	0.381	817,094	1.735	2,810,127	0.050%	1,785,378	0.001%	35,708	\$7.88	\$12,772,824
250	10	LGD	949	2.65	579,420	0.199	115,304	3.028	1,754,483	0.160%	2,043,840	0.003%	38,322	\$8.27	\$4,794,862
250	10	LGD	959	2.65	735,189	0.248	182,322	3.668	2,695,131	0.160%	2,583,231	0.008%	129,662	\$9.19	\$6,766,205
SUBTOTAL		LGD			6,799,844	0.218	1,484,819	1.882	12,861,822	0.122%	16,337,296	0.010%	1,606,907	\$7.29	\$49,583,037
CUMULATIVE TOTAL		LGD			106,017,606	0.237	25,103,734	1.448	183,300,736	0.112%	262,449,469	0.007%	16,574,790	\$7.22	\$765,456,040
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
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														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
250	10	HGD	948	2.65	91,928	0.541	49,733	3.179	292,239	0.160%	324,266	0.024%	48,640	\$13.80	\$1,269,332
250	10	HGD	1217	2.65	1,258,444	0.368	460,560	1.924	2,421,246	0.280%	7,768,292	0.002%	55,488	\$14.02	\$17,649,333
SUBTOTAL		HGD			1,350,372	0.378	510,323	2.009	2,713,485	0.272%	8,092,558	0.003%	104,128	\$14.01	\$18,918,665
CUMULATIVE TOTAL		HGD			72,622,780	0.591	42,985,653	3.680	285,784,617	0.195%	312,510,507	0.009%	14,368,030	\$18.70	\$1,139,837,647
BENCH TOTAL		HGD/LGD			8,150,218	0.246	1,995,142	1.886	15,375,007	0.147%	26,429,854	0.009%	1,610,035	\$8.40	\$68,501,702
CUM. BENCH TOTAL		HGD/LGD			178,640,288	0.381	68,059,387	2.346	419,085,352	0.146%	674,959,976	0.008%	29,942,820	\$10.67	\$1,905,293,686

NOTE: CONCENTRATIONS OF ALL OTHER METALS ARE INCLUDED IN DATABASE WITH 100% ASSAYS. MOLYBDENUM VALUES ARE NOT INCLUDED IN TOTAL METAL VALUES.

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

18-12-98 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	#VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
240															
240	10	UDF		2.65	3,918,157	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			3,918,157										
CUMULATIVE TOTAL		UDF			39,557,162										
														\$0.00	\$0
														\$0.00	\$0
240	10	WST	1203	2.65	794,804	0	0	0	0	0.000%	0	0.000%	0	\$0.00	\$0
240	10	WST	1218	2.65	1,373,436	0.02	27,469	0.257	352,973	0.040%	1,211,162	0.001%	30,279	\$1.48	\$2,033,304
240	10	WST	1201	2.65	619,555	0.055	34,076	0.786	486,970	0.040%	546,353	0.004%	54,635	\$2.18	\$1,338,010
240	10	WST	1221	2.65	1,777,971	0.112	199,133	0.429	762,749	0.020%	783,950	0.001%	39,197	\$2.44	\$4,349,796
240	10	WST	1220	2.65	1,065,777	0.082	87,394	0.567	604,295	0.040%	939,853	0.001%	23,496	\$2.54	\$2,713,052
240	10	WST	1204	2.65	520,262	0.102	53,067	1.646	856,351	0.070%	802,886	0.019%	217,926	\$3.93	\$2,045,318
240	10	WST	1200	2.65	1,538,827	0.162	249,290	2.077	3,196,144	0.060%	2,035,517	0.002%	67,851	\$4.71	\$7,256,132
SUBTOTAL		WST			7,690,632	0.085	650,427	0.814	6,259,484	0.037%	6,319,722	0.003%	433,385	\$2.57	\$19,735,611
CUMULATIVE TOTAL		WST			68,052,688	0.111	7,661,592	0.855	58,153,007	0.036%	53,440,936	0.004%	5,563,727	\$2.96	\$201,185,235
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
240	10	LGD	960	2.65	3,170,864	0.071	225,131	1.068	3,388,483	0.160%	11,184,882	0.029%	2,027,260	\$5.78	\$18,346,241
240	10	LGD	947	2.65	202,527	0.142	28,759	1.173	237,584	0.160%	714,392	0.004%	17,860	\$6.95	\$1,407,697
240	10	LGD	949	2.65	609,662	0.15	91,449	1.126	686,479	0.160%	2,150,517	0.004%	53,763	\$7.06	\$4,309,676
240	10	LGD	1219	2.65	1,612,827	0.309	498,364	1.074	1,732,176	0.090%	3,200,104	0.002%	71,113	\$7.68	\$12,394,895
240	10	LGD	959	2.65	869,408	0.238	208,919	1.123	976,346	0.160%	3,066,744	0.014%	268,340	\$8.48	\$7,375,486
SUBTOTAL		LGD			6,466,289	0.163	1,050,622	1.086	7,019,049	0.143%	20,318,838	0.017%	2,438,338	\$6.78	\$43,833,994
CUMULATIVE TOTAL		LGD			112,482,794	0.233	26,164,358	1.425	160,319,783	0.114%	282,766,107	0.007%	18,013,128	\$7.19	\$809,290,034
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
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														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
240	10	HGD	1223	2.65	1,267,729	2.686	3,405,121	0.488	618,652	0.010%	279,488	0.001%	27,949	\$43.56	\$55,238,803
SUBTOTAL		HGD			1,267,729	2.686	3,405,121	0.488	618,652	0.010%	279,488	0.001%	27,949	\$43.67	\$55,238,803
CUMULATIVE TOTAL		HGD			73,890,508	0.627	44,360,774	3.608	266,403,269	0.182%	312,788,893	0.008%	14,395,979	\$16.17	\$1,185,077,480
BENCH TOTAL		HGD/LGD			7,733,018	0.576	4,455,743	0.988	7,637,700	0.121%	20,596,124	0.014%	2,468,285	\$12.81	\$99,073,798
CUM. BENCH TOTAL		HGD/LGD			186,373,303	0.399	72,515,130	2.280	426,723,052	0.145%	695,556,101	0.008%	32,409,105	\$10.75	\$2,004,397,484



**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

18-12-98 9:31 AM LEVEL	BENCH HEIGHT	POLYGON MATERIAL	HOLE ID	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER %	COPPER POUNDS	MOLY %	MOLY POUNDS	\$VAL TONNE	TOTAL VALUE
220															
220	10	UDF		2.65	4,485,103	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			4,485,103										
CUMULATIVE TOTAL		UDF			48,520,492										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
220	10	WST	1223	2.65	2,423,072	0.035	84,808	0.522	1,264,844	0.010%	534,195	0.001%	53,420	\$0.95	\$2,309,715
220	10	WST	1220	2.65	830,857	0.05	41,543	0.226	187,774	0.020%	366,345	0.001%	18,317	\$1.40	\$1,167,251
220	10	WST	1204	2.65	921,920	0.085	78,363	0.982	905,326	0.050%	1,016,242	0.015%	304,873	\$2.96	\$2,729,554
220	10	WST	1201	2.65	877,951	0.085	74,828	0.834	732,211	0.070%	1,354,684	0.006%	116,133	\$3.48	\$3,054,675
SUBTOTAL		WST			6,053,801	0.055	279,339	0.611	3,090,154	0.029%	3,271,666	0.004%	492,742	\$1.83	\$9,281,195
CUMULATIVE TOTAL		WST			77,925,976	0.105	8,198,369	0.846	65,895,885	0.038%	62,298,774	0.004%	6,557,822	\$2.88	\$224,200,343
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
220	10	LGD	1200	2.65	1,859,832	0.182	338,453	2.325	4,323,845	0.080%	2,459,870	0.002%	81,998	\$5.08	\$8,488,385
220	10	LGD	960	2.65	3,428,166	0.073	250,256	0.717	2,457,995	0.180%	12,092,487	0.021%	1,587,139	\$5.74	\$19,680,488
220	10	LGD	958	2.65	738,795	0.082	60,581	0.703	519,373	0.160%	2,808,018	0.001%	18,288	\$5.88	\$4,345,929
220	10	LGD	1219	2.65	2,275,699	0.188	427,831	1.04	2,366,727	0.130%	6,522,187	0.001%	50,171	\$6.83	\$15,552,919
220	10	LGD	949	2.65	1,188,877	0.177	210,431	4.484	5,330,925	0.160%	4,193,638	0.003%	78,831	\$8.23	\$9,788,583
220	10	LGD	959	2.65	1,170,234	0.233	272,664	8.008	7,030,765	0.160%	4,127,874	0.025%	644,980	\$9.48	\$11,091,058
SUBTOTAL		LGD			10,661,404	0.148	1,560,218	2.068	22,029,431	0.138%	32,002,052	0.010%	2,489,204	\$6.66	\$89,937,339
CUMULATIVE TOTAL		LGD			133,700,880	0.228	30,188,782	1.549	207,112,080	0.115%	339,638,252	0.008%	22,391,513	\$7.15	\$955,515,923
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
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														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
SUBTOTAL		HGD			0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
CUMULATIVE TOTAL		HGD			73,890,508	0.627	48,380,774	3.608	288,403,289	0.182%	312,788,883	0.009%	14,398,878	\$16.17	\$1,186,077,488
BENCH TOTAL		HGD/LGD			10,661,404	0.148	1,560,218	2.068	22,029,431	0.138%	32,002,052	0.010%	2,489,204	\$6.66	\$89,937,339
CUM. BENCH TOTAL		HGD/LGD			207,591,389	0.399	78,647,886	2.281	473,615,349	0.143%	652,428,248	0.008%	36,787,491	\$10.36	\$2,180,893,373

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

18-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	#VAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
210															
210	10	UDF		2.65	4,496,025	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			4,496,025										
CUMULATIVE TOTAL		UDF			53,016,517										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
210	10	WST	1220	2.65	733,024	0.052	38,117	0.247	181,057	0.030%	484,812	0.001%	16,160	\$1.72	\$1,258,772
210	10	WST	1204	2.65	895,883	0.047	42,106	1.499	1,342,928	0.050%	987,541	0.032%	632,026	\$2.46	\$2,206,942
210	10	WST	1223	2.65	2,187,884	0.141	308,492	0.831	1,818,132	0.010%	482,345	0.001%	48,235	\$2.72	\$5,963,467
210	10	WST	1201	2.65	906,010	0.08	72,481	0.8	724,808	0.060%	1,198,445	0.004%	79,896	\$3.11	\$2,823,005
210	10	WST	1200	2.65	1,981,290	0.087	172,372	0.905	1,793,068	0.080%	3,494,394	0.001%	43,680	\$3.80	\$7,534,213
210	10	WST	1219	2.65	2,282,445	0.192	438,229	1.118	2,551,774	0.060%	3,019,154	0.001%	50,319	\$4.98	\$11,382,062
SUBTOTAL		WST			8,986,536	0.119	1,071,798	0.938	8,411,766	0.049%	9,666,691	0.004%	870,316	\$3.47	\$31,168,462
CUMULATIVE TOTAL		WST			86,912,512	0.107	9,270,167	0.855	74,307,651	0.038%	71,965,484	0.004%	7,428,138	\$2.94	\$255,368,805
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
210	10	LGD	958	2.65	207,652	0.046	9,562	0.529	109,848	0.160%	732,471	0.001%	4,578	\$5.26	\$1,080,362
210	10	LGD	949	2.65	1,239,583	0.088	108,083	1.705	2,113,488	0.160%	4,372,494	0.002%	54,656	\$6.19	\$7,684,643
210	10	LGD	955	2.65	12,307	0.141	1,735	0.74	9,107	0.160%	43,410	0.000%	0	\$6.84	\$84,168
210	10	LGD	959	2.65	1,225,954	0.147	180,215	1.016	1,245,569	0.160%	4,324,419	0.026%	702,718	\$6.99	\$8,577,409
210	10	LGD	960	2.65	3,437,908	0.115	395,359	3.351	11,520,428	0.160%	12,128,848	0.020%	1,515,856	\$6.99	\$24,050,432
SUBTOTAL		LGD			6,123,403	0.114	695,945	2.449	14,998,440	0.160%	21,599,642	0.017%	2,277,808	\$6.78	\$41,490,006
CUMULATIVE TOTAL		LGD			139,824,283	0.221	30,882,727	1.688	222,110,621	0.117%	361,237,893	0.008%	24,669,321	\$7.13	\$997,006,928
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
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														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
210	10	HGD	954	2.65	893,946	1	893,946	1.494	1,335,555	0.160%	3,153,298	0.000%	0	\$136.10	\$18,610,096
SUBTOTAL		HGD			893,946	1.000	893,946	1.494	1,335,555	0.160%	3,153,298	0.000%	0	\$20.82	\$18,610,096
CUMULATIVE TOTAL		HGD			74,784,455	0.632	47,254,720	3.580	287,738,824	0.182%	315,843,291	0.009%	14,395,978	\$18.23	\$1,213,687,546
BENCH TOTAL		HGD/LGD			7,017,349	0.227	1,589,891	2.328	16,333,996	0.160%	24,752,940	0.015%	2,277,808	\$8.56	\$60,100,101
CUM. BENCH TOTAL		HGD/LGD			214,608,739	0.364	78,137,448	2.283	489,849,345	0.143%	677,181,184	0.008%	39,065,299	\$10.30	\$2,210,693,474

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	IVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
200															
200	10	UDF		2.65	4,700,557	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			4,700,557										
CUMULATIVE TOTAL		UDF			57,717,075										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
200	10	WST	1201	2.65	1,384,476	0	0	0	0	0.000%	0	0.000%	0	\$0.00	\$0
200	10	WST	1204	2.65	870,219	0	0	0	0	0.000%	0	0.000%	0	\$0.00	\$0
200	10	WST	1223	2.65	1,972,871	0.04	78,915	0.238	469,543	0.010%	434,943	0.002%	86,989	\$0.97	\$1,915,929
200	10	WST	1220	2.65	825,977	0.024	19,823	0.31	256,053	0.020%	364,193	0.001%	18,210	\$1.00	\$830,334
200	10	WST	1200	2.65	2,062,824	0.063	129,958	0.717	1,479,045	0.060%	2,728,648	0.001%	45,477	\$2.82	\$5,825,921
SUBTOTAL		WST			7,116,367	0.032	228,698	0.310	2,204,841	0.022%	3,627,782	0.001%	150,678	\$1.20	\$8,572,184
CUMULATIVE TOTAL		WST			84,028,878	0.101	8,499,864	0.814	76,812,292	0.036%	76,493,247	0.004%	7,578,814	\$2.81	\$263,940,989
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
200	10	LGD	958	2.65	129,552	0.03	3,887	0.48	62,185	0.180%	456,980	0.001%	2,856	\$5.00	\$647,402
200	10	LGD	960	2.65	3,442,029	0.082	282,246	1.465	5,042,572	0.160%	12,141,384	0.027%	2,048,859	\$8.05	\$20,824,617
200	10	LGD	955	2.65	38,304	0.24	9,193	2.445	93,853	0.160%	135,113	0.000%	0	\$8.80	\$337,317
200	10	LGD	959	2.65	1,270,471	0.276	350,650	0.698	886,789	0.160%	4,481,450	0.034%	952,308	\$9.00	\$11,435,359
200	10	LGD	964	2.65	98,782	0.302	29,222	2.044	197,781	0.160%	341,318	0.001%	2,133	\$9.71	\$940,048
SUBTOTAL		LGD			4,977,117	0.136	675,198	1.262	6,282,979	0.160%	17,668,243	0.027%	3,008,166	\$8.87	\$34,184,741
CUMULATIVE TOTAL		LGD			144,801,400	0.218	31,667,925	1.677	228,393,600	0.118%	378,794,136	0.009%	27,675,477	\$7.12	\$1,031,190,669
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
200	10	HGD	1219	2.65	2,787,118	0.659	1,836,711	7.679	21,402,280	0.100%	6,144,538	0.002%	122,891	\$15.02	\$41,923,483
200	10	HGD	963	2.65	80,659	0.728	58,720	3.681	296,906	0.160%	284,516	0.001%	1,778	\$16.91	\$1,365,180
200	10	HGD	954	2.65	1,091,201	1	1,091,201	1.968	2,147,483	0.160%	3,849,093	0.001%	24,057	\$72.26	\$22,830,322
SUBTOTAL		HGD			3,958,978	0.754	2,986,632	6.023	23,846,670	0.118%	10,278,148	0.002%	148,726	\$16.70	\$68,118,985
CUMULATIVE TOTAL		HGD			78,743,433	0.838	60,241,381	3.703	281,585,484	0.188%	328,221,437	0.008%	14,844,704	\$16.25	\$1,279,806,530
BENCH TOTAL		HGD/LGD			8,936,095	0.410	3,661,829	3.372	30,129,649	0.141%	27,834,389	0.016%	3,164,882	\$11.22	\$100,303,726
CUM. BENCH TOTAL		HGD/LGD			223,844,833	0.366	81,799,276	2.328	619,978,894	0.143%	705,015,573	0.009%	42,220,181	\$10.34	\$2,310,997,200



**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM	BENCH	POLYGON	HOLE	METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	#VAL	TOTAL	
LEVEL	HIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
190	10	UDF		2.65	5,538,424	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			5,538,424										
CUMULATIVE TOTAL		UDF			63,253,498									\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
190	10	WST	1220	2.65	3,083,170	0.018	49,331	0.2	616,634	0.020%	1,359,444	0.000%	0	\$0.85	
190	10	WST	1223	2.65	1,825,198	0.036	85,707	0.275	501,929	0.010%	402,387	0.002%	80,477	\$0.91	
SUBTOTAL		WST			4,908,368	0.023	115,038	0.228	1,118,563	0.016%	1,761,830	0.001%	80,477	\$0.88	
CUMULATIVE TOTAL		WST			98,937,246	0.097	9,813,901	0.785	77,630,856	0.035%	77,255,077	0.004%	7,859,291	\$2.71	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
190	10	LGD	1219	2.65	2,898,068	0.204	591,206	2.534	7,343,703	0.050%	3,194,569	0.002%	127,783	\$5.21	
190	10	LGD	958	2.65	138,043	0.072	9,939	0.261	36,029	0.160%	486,931	0.001%	3,043	\$5.62	
190	10	LGD	960	2.65	3,622,319	0.08	217,339	1.2	4,346,782	0.160%	12,777,338	0.024%	1,916,801	\$5.63	
190	10	LGD	959	2.65	2,333,441	0.126	294,014	0.527	1,229,723	0.160%	8,230,980	0.019%	977,427	\$6.55	
SUBTOTAL		LGD			8,991,870	0.124	1,112,498	1.441	12,956,238	0.125%	24,889,798	0.015%	3,024,853	\$5.74	
CUMULATIVE TOTAL		LGD			153,793,269	0.212	32,870,422	1.569	241,349,738	0.119%	403,483,934	0.009%	30,700,330	\$7.04	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
														\$0.00	
190	10	HGD	964	2.65	85,924	0.385	36,931	3.04	291,609	0.160%	338,382	0.001%	2,115	\$11.28	
190	10	HGD	955	2.65	74,958	0.466	34,930	3.18	238,385	0.160%	264,405	0.000%	0	\$12.59	
190	10	HGD	963	2.65	99,780	1.051	104,868	7.733	771,596	0.160%	351,962	0.001%	2,200	\$22.98	
190	10	HGD	954	2.65	1,250,453	1	1,250,453	2.338	2,923,560	0.160%	4,410,839	0.001%	27,568	\$65.13	
SUBTOTAL		HGD			1,521,116	0.938	1,427,183	2.778	4,225,131	0.160%	6,385,588	0.001%	31,882	\$20.11	
CUMULATIVE TOTAL		HGD			80,264,548	0.644	81,688,534	3.685	295,810,625	0.187%	331,587,008	0.008%	14,576,587	\$18.33	
BENCH TOTAL		HGD/LGD			10,612,985	0.242	2,539,680	1.634	17,181,369	0.130%	30,065,386	0.013%	3,066,736	\$7.82	
CUM. BENCH TOTAL		HGD/LGD			234,067,817	0.360	84,338,950	2.295	637,180,363	0.142%	735,070,939	0.009%	45,276,917	\$10.22	

ALL METAL VALUES ARE IN METRIC UNITS. METROLOGICAL CONSTRAINTS USED: ALL 1998 DRILL HOLES INCLUDED IN DATABASE WITH 1998 ASSAYS. MOLYBDENUM VALUES ARE NOT INCLUDED IN TOTAL METAL VALUES

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM LEVEL	BENCH HEIGHT	POLYGON MATERIAL	HOLE ID	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER %	COPPER POUNDS	MOLY %	MOLY POUNDS	\$VAL TONNE	TOTAL VALUE
180															
180	10	UDF		2.65	9,247,024	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			9,247,024										
CUMULATIVE TOTAL		UDF			72,500,523										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
180	10	WST	1223	2.65	1,853,802	0.034	56,222	0.919	1,519,660	0.000%	0	0.001%	36,456	\$0.75	\$1,238,382
SUBTOTAL		WST			1,853,802	0.034	56,222	0.919	1,519,660	0.000%	0	0.001%	36,456	\$0.75	\$1,238,382
CUMULATIVE TOTAL		WST			100,590,848	0.086	9,670,124	0.797	79,150,516	0.035%	77,255,077	0.003%	7,895,747	\$2.68	\$269,477,552
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
180	10	LGD	958	2.65	144,853	0.052	7,532	0.228	32,737	0.160%	510,954	0.001%	3,183	\$5.29	\$767,015
180	10	LGO	1219	2.65	4,790,811	0.187	895,882	1.403	8,721,507	0.080%	8,449,534	0.003%	318,858	\$5.52	\$26,448,425
180	10	LGD	959	2.65	3,512,392	0.101	354,752	0.668	2,346,278	0.160%	12,369,583	0.029%	2,245,612	\$6.18	\$21,707,585
180	10	LGD	964	2.65	102,778	0.16	16,444	0.99	101,750	0.160%	362,538	0.001%	2,268	\$7.20	\$739,984
180	10	LGD	963	2.65	119,084	0.206	24,531	1.01	120,275	0.160%	420,055	0.001%	2,625	\$7.94	\$945,993
180	10	LGD	955	2.65	131,009	0.256	33,536	0.952	124,721	0.160%	462,120	0.000%	0	\$8.73	\$1,144,368
SUBTOTAL		LGD			6,800,827	0.151	1,332,680	1.073	9,447,267	0.116%	22,894,785	0.013%	2,670,854	\$5.88	\$51,751,368
CUMULATIVE TOTAL		LGD			162,594,196	0.209	34,003,102	1.542	250,797,005	0.119%	426,078,719	0.009%	33,270,684	\$6.98	\$1,134,543,617
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
180	10	HGD	954	2.65	1,400,875	1.433	2,007,453	0.672	941,388	0.160%	4,941,434	0.000%	0	\$27.59	\$38,663,745
SUBTOTAL		HGD			1,400,875	1.433	2,007,453	0.672	941,388	0.160%	4,941,434	0.000%	0	\$27.60	\$38,663,745
CUMULATIVE TOTAL		HGD			81,865,423	0.657	83,875,867	3.434	286,762,013	0.187%	338,528,439	0.008%	14,576,887	\$16.52	\$1,349,058,866
BENCH TOTAL		HGD/LGD			10,201,801	0.327	3,340,133	1.018	10,388,655	0.122%	27,536,218	0.011%	2,570,554	\$8.86	\$90,415,113
CUM. BENCH TOTAL		HGD/LGD			244,259,619	0.359	87,879,089	2.242	547,549,018	0.142%	762,607,158	0.009%	47,847,471	\$10.17	\$2,483,599,482

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM LEVEL	BENCH HEIGHT	POLYGON MATERIAL	HOLE ID	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER %	COPPER POUNDS	MOLY %	MOLY POUNDS	#VAL TONNE	TOTAL VALUE
170															
170	10	UDF		2.65	9,336,639	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			9,336,639										
CUMULATIVE TOTAL		UDF			81,837,182										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
170	10	WST	1223	2.65	1,497,270	0.04	59,891	0.985	1,474,811	0.020%	660,182	0.001%	33,009	\$1.41	\$2,112,730
SUBTOTAL		WST			1,497,270	0.040	59,891	0.985	1,474,811	0.020%	660,182	0.001%	33,009	\$1.41	\$2,112,730
CUMULATIVE TOTAL		WST			102,088,118	0.095	9,730,015	0.790	80,825,328	0.035%	77,915,259	0.003%	7,728,756	\$2.68	\$271,690,282
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
170	10	LGD	958	2.65	168,812	0.054	9,105	0.2	33,722	0.160%	594,780	0.000%	0	\$5.32	\$897,278
170	10	LGD	964	2.65	138,055	0.056	7,731	0.335	46,248	0.160%	486,974	0.001%	3,044	\$5.38	\$743,208
170	10	LGD	959	2.65	3,527,853	0.086	303,395	0.483	1,703,953	0.160%	12,444,122	0.039%	3,033,255	\$5.90	\$20,808,619
170	10	LGD	955	2.65	185,918	0.089	16,547	0.765	142,228	0.160%	655,807	0.000%	0	\$6.01	\$1,117,121
170	10	LGD	1219	2.65	4,797,658	0.258	1,237,796	1.18	5,585,283	0.080%	8,461,609	0.005%	528,851	\$6.60	\$31,705,128
170	10	LGD	983	2.65	122,685	0.232	28,463	0.578	70,912	0.160%	432,757	0.001%	2,705	\$8.28	\$1,014,229
SUBTOTAL		LGD			8,940,781	0.179	1,803,037	0.846	7,562,346	0.117%	23,076,029	0.018%	3,567,854	\$6.30	\$56,285,583
CUMULATIVE TOTAL		LGD			171,634,977	0.208	36,806,139	1.606	258,369,351	0.119%	449,164,748	0.010%	36,838,738	\$6.84	\$1,190,829,200
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
170	10	HGD	954	2.65	1,514,105	0.871	1,318,786	0.79	1,196,143	0.160%	5,340,843	0.000%	0	\$18.58	\$28,145,280
SUBTOTAL		HGD			1,514,105	0.871	1,318,786	0.790	1,196,143	0.160%	5,340,843	0.000%	0	\$18.58	\$28,145,280
CUMULATIVE TOTAL		HGD			83,179,528	0.661	84,994,773	3.882	297,848,158	0.166%	341,889,282	0.008%	14,678,887	\$18.58	\$1,377,201,145
BENCH TOTAL		HGD/LGD			10,484,888	0.279	2,921,822	0.838	8,758,489	0.123%	28,416,872	0.015%	3,567,854	\$8.08	\$84,430,863
CUM. BENCH TOTAL		HGD/LGD			254,714,805	0.358	90,600,911	2.184	856,307,507	0.141%	791,024,030	0.009%	51,416,324	\$10.08	\$2,568,030,344

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM LEVEL	BENCH HEIGHT	POLYGON MATERIAL	HOLE ID	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER %	COPPER POUNDS	MOLY %	MOLY POUNDS	\$VAL TONNE	TOTAL VALUE
160															
160	10	UDF		2.65	9,501,122	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			9,501,122										
CUMULATIVE TOTAL		UDF			91,338,284										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
SUBTOTAL		WST			0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
CUMULATIVE TOTAL		WST			102,088,118	0.095	9,730,015	0.790	80,825,320	0.035%	77,915,259	0.003%	7,728,756	\$2.66	\$271,590,282
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
160	10	LGD	955	2.65	272,447	0.047	12,805	0.291	79,282	0.160%	961,028	0.000%	0	\$5.23	\$1,424,828
160	10	LGD	1219	2.85	4,785,841	0.201	961,954	0.613	2,933,721	0.070%	7,385,673	0.006%	633,058	\$5.29	\$25,345,731
160	10	LGD	958	2.65	997,347	0.08	79,788	0.373	372,010	0.160%	3,518,033	0.000%	0	\$5.78	\$5,762,371
160	10	LGD	959	2.65	3,538,839	0.09	318,478	0.3	1,061,592	0.160%	12,482,167	0.035%	2,730,474	\$5.92	\$20,957,378
160	10	LGD	963	2.65	120,311	0.221	26,569	1.265	152,194	0.160%	424,385	0.000%	0	\$8.24	\$961,512
SUBTOTAL		LGD			9,714,585	0.144	1,399,613	0.473	4,598,798	0.116%	24,771,284	0.016%	3,363,532	\$5.61	\$54,481,820
CUMULATIVE TOTAL		LGD			181,249,562	0.204	37,005,752	1.451	262,958,150	0.119%	473,928,032	0.010%	40,202,269	\$6.87	\$1,245,310,820
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
160	10	HGD	964	2.65	184,418	0.363	70,574	3.608	701,070	0.160%	685,787	0.001%	4,288	\$11.03	\$2,148,292
160	10	HGD	954	2.65	1,957,209	0.481	941,418	0.969	1,896,536	0.160%	6,903,845	0.001%	43,149	\$12.35	\$24,185,041
SUBTOTAL		HGD			2,151,627	0.470	1,011,991	1.207	2,597,606	0.160%	7,589,632	0.001%	47,435	\$12.24	\$26,331,333
CUMULATIVE TOTAL		HGD			85,331,185	0.856	84,008,764	3.822	300,645,761	0.186%	348,468,914	0.008%	14,624,022	\$18.48	\$1,463,832,478
BENCH TOTAL		HGD/LGD			11,866,212	0.203	2,411,804	0.608	7,198,404	0.124%	32,380,918	0.013%	3,410,967	\$6.81	\$80,812,953
CUM. BENCH TOTAL		HGD/LGD			280,680,717	0.349	93,012,610	2.114	593,503,911	0.140%	823,384,945	0.009%	54,828,291	\$9.94	\$2,648,843,297

NO GEOLOGICAL OR LITHOLOGICAL CONSTRAINTS USED - ALL 1988 DRILL HOLES INCLUDED IN DATABASE WITH 1995 ASSAYS - MOLYBDENUM VALUES ARE NOT INCLUDED IN TOTAL METAL VALUES

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

18-12-88 8:31 AM LEVEL	BENCH HEIGHT	POLYGON MATERIAL	HOLE ID	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER %	COPPER POUNDS	MOLY %	MOLY POUNDS	\$VAL TONNE	TOTAL VALUE
150															
150	10	UDF		2.65	17,541,668	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			17,541,668										
CUMULATIVE TOTAL		UDF			108,879,950										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
150	10	WST	958	2.65	1,013,328	0.033	33,440	0.2	202,668	0.160%	3,574,408	0.000%	0	\$4.98	\$5,050,308
SUBTOTAL		WST			1,013,328	0.033	33,440	0.200	202,668	0.160%	3,574,408	0.000%	0	\$4.98	\$5,050,308
CUMULATIVE TOTAL		WST			103,101,448	0.095	9,763,465	0.784	80,827,992	0.036%	81,489,685	0.003%	7,728,756	\$2.68	\$278,640,588
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
150	10	LGD	964	2.65	228,064	0.163	37,174	1.397	318,608	0.160%	804,472	0.000%	0	\$7.33	\$1,673,449
150	10	LGD	963	2.65	125,597	0.265	33,283	1.685	211,631	0.160%	443,031	0.001%	2,788	\$9.03	\$1,135,543
150	10	LGD	955	2.65	299,023	0.257	76,649	3.057	914,114	0.160%	1,054,772	0.001%	6,592	\$9.20	\$2,755,300
SUBTOTAL		LGD			652,685	0.228	147,307	2.213	1,444,351	0.160%	2,302,275	0.001%	9,381	\$8.53	\$5,564,292
CUMULATIVE TOTAL		LGD			181,902,248	0.204	37,153,058	1.464	264,402,501	0.119%	476,228,306	0.010%	40,211,631	\$6.88	\$1,250,875,112
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
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														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
150	10	HGD	954	2.65	2,180,108	1.34	2,921,342	1.032	2,249,869	0.160%	7,690,088	0.001%	48,063	\$26.17	\$57,082,761
SUBTOTAL		HGD			2,180,108	1.340	2,921,342	1.032	2,249,869	0.160%	7,690,088	0.001%	48,063	\$26.18	\$57,082,761
CUMULATIVE TOTAL		HGD			87,611,261	0.673	58,928,108	3.480	302,795,631	0.185%	357,149,002	0.008%	14,872,089	\$18.89	\$1,480,615,239
BENCH TOTAL		HGD/LGD			2,832,791	1.083	3,088,649	1.304	3,694,220	0.160%	9,992,363	0.001%	57,424	\$22.11	\$62,647,053
CUM. BENCH TOTAL		HGD/LGD			299,413,507	0.357	96,081,165	2,105	567,198,131	0.140%	833,377,308	0.009%	64,883,716	\$10.09	\$2,711,490,351

MINERALOGICAL CONSTRAINTS USED. ALL 1988 DRILL HOLES INCLUDED IN DATABASE WITH 100% ASSAYS. MOLYBDFENIM VALUES ARE NOT INCLUDED IN TOTAL METAL VALUES

**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

250m SEARCH RADIUS

19-12-95 9:31 AM	BENCH	POLYGON	HOLE		METRIC	AU	AU	AG	AG	COPPER	COPPER	MOLY	MOLY	IVAL	TOTAL
LEVEL	HEIGHT	MATERIAL	ID	DENSITY	TONNES	PPM	GRAMS	PPM	GRAMS	%	POUNDS	%	POUNDS	TONNE	VALUE
140															
140	10	UDF		2.65	17,790,836	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
SUBTOTAL		UDF			17,790,836										
CUMULATIVE TOTAL		UDF			126,670,785										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
SUBTOTAL		WST			0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
CUMULATIVE TOTAL		WST			103,101,446	0.095	9,783,455	0.784	80,827,892	0.036%	81,489,685	0.003%	7,728,756	\$2.68	\$276,640,588
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
140	10	LGD	955	2.65	2,183,500	0.036	78,608	0.2	436,700	0.160%	7,702,060	0.001%	48,138	\$5.03	\$10,987,633
140	10	LGD	956	2.65	1,035,636	0.037	38,319	0.2	207,127	0.160%	3,653,095	0.000%	0	\$5.05	\$5,228,068
140	10	LGD	963	2.65	137,724	0.068	13,221	0.614	84,582	0.160%	485,805	0.001%	3,038	\$6.08	\$838,482
SUBTOTAL		LGD			3,356,860	0.039	130,146	0.217	728,390	0.160%	11,840,960	0.001%	51,174	\$5.08	\$17,054,193
CUMULATIVE TOTAL		LGD			185,259,108	0.201	37,283,204	1.431	285,130,890	0.120%	488,089,268	0.010%	40,262,805	\$6.84	\$1,267,929,305
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
140	10	HGD	964	2.65	251,174	0.392	98,460	8.319	2,089,520	0.160%	885,991	0.001%	5,537	\$12.52	\$3,150,425
SUBTOTAL		HGD			251,174	0.392	98,460	8.319	2,089,520	0.160%	885,991	0.001%	5,537	\$12.54	\$3,150,425
CUMULATIVE TOTAL		HGD			87,762,435	0.673	59,029,567	3.474	304,885,151	0.185%	358,034,993	0.008%	14,877,822	\$18.68	\$1,483,785,684
BENCH TOTAL		HGD/LGD			3,608,034	0.063	228,606	0.781	2,817,910	0.160%	12,726,951	0.001%	56,712	\$5.60	\$20,204,819
CUM. BENCH TOTAL		HGD/LGD			273,021,541	0.353	99,309,771	2.088	579,016,041	0.141%	846,104,259	0.009%	54,940,427	\$10.01	\$2,731,894,989

... INCLUDED IN TOTAL METAL VALUES



**BRONSON SLOPE RESOURCE - CORRECTED TOPOGRAPHY**

**250m SEARCH RADIUS**

19-12-95 9:31 AM LEVEL	BENCH HEIGHT	POLYGON MATERIAL	HOLE ID	DENSITY	METRIC TONNES	AU PPM	AU GRAMS	AG PPM	AG GRAMS	COPPER %	COPPER POUNDS	MOLY %	MOLY POUNDS	\$VAL TONNE	TOTAL VALUE
120															
120	10	UDF		2.65	19,497,730	0	0	0	0	0.000%	0	0.000%	0	\$0.00	
<b>SUBTOTAL</b>		UDF			19,497,730										
<b>CUMULATIVE TOTAL</b>		UDF			164,752,524										
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
<b>SUBTOTAL</b>		WST			0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
<b>CUMULATIVE TOTAL</b>		WST			104,550,061	0.094	9,806,913	0.776	81,117,713	0.038%	86,599,461	0.003%	7,780,892	\$2.71	\$283,790,378
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
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														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
120	10	LGD	863	2.65	1,901,139	0.155	294,677	3.258	6,193,912	0.160%	6,706,064	0.001%	41,913	\$7.61	\$14,483,641
<b>SUBTOTAL</b>		LGD			1,901,139	0.155	294,677	3.258	6,193,912	0.160%	6,706,064	0.001%	41,913	\$7.62	\$14,483,641
<b>CUMULATIVE TOTAL</b>		LGD			188,526,502	0.200	37,632,462	1.445	272,433,644	0.120%	499,594,663	0.010%	40,334,836	\$8.84	\$1,289,658,713
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
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														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
														\$0.00	\$0
<b>SUBTOTAL</b>		HGD			0	0.000	0	0.000	0	0.000%	0	0.000%	0	\$0.00	\$0
<b>CUMULATIVE TOTAL</b>		HGD			87,782,435	0.673	59,026,567	3.474	304,885,151	0.185%	358,034,993	0.008%	14,677,622	\$16.68	\$1,443,765,644
<b>BENCH TOTAL</b>		HGD/LGD			1,901,139	0.156	294,677	3.258	6,193,912	0.160%	6,706,064	0.001%	41,913	\$7.62	\$14,483,641
<b>CUM. BENCH TOTAL</b>		HGD/LGD			276,288,937	0.350	96,659,029	2.090	677,318,794	0.141%	857,629,645	0.009%	55,012,461	\$9.97	\$2,753,324,378

THIS REPORT IS UNCLASSIFIED AND IS AVAILABLE TO THE PUBLIC. MOLYBDENUM VALUES ARE NOT INCLUDED IN TOTAL METAL VALUES