| N ^{A15} | E LIERES BRANCH |
|------------------|-----------------|
| 1 Kt | |
| LI | |
| File | VANGOUVER, B.C. |

Geophysical and Geochemical Report Doe-Ray Mineral Claims

NTS 82F/10W

UTM Zone 11 Easting: 509000 - 516000 UTM Zone 11 Northing: 5496000 - 5514000

For: Klondike Gold Corp. 1000 - 675 W.Hastings St., Vancouver, B.C. V6B 1N2

By; G.M.Rodgers, P.Eng. P.O. Box 63, Skookumchuck, B.C. V0B 2E0

Oct.26, 1998

GEOLOGICAL SURVEY BRANCH ASSESSMENT DEPORT



Table of Contents

| (i) | summary | | | |
|-------------|---------------------------------|------------|-------|-----------|
| 1.0 Introdu | | Page | | |
| | 1.1 Location and Access | | | 1 |
| | 1.2 Claim Status | | | 1 |
| | 1.3 History | | | 1 |
| | 1.4 Objectives of exploration | n prog | ram | 1 |
| 2.0 Geolog | Ŋ | | | |
| - | 2.1 Regional Geology | | | 5 |
| | 2.2 Property Geology | • | | 5 |
| 3.0 Geoche | emistry | | | |
| | 3.1 Soil sampling program a | ind res | ults. | 5 |
| 4.0 Gravity | Survey | | | 6 |
| 5.0 Conclu | sions and Recommendations | | | 38 |
| 6.0 Statem | ent of Qualifications | | | 38 |
| 7.0 Statem | ent of Costs | | | 39 |
| Fig.1 (Lo | cation Map) (1:1,000,000) | | | 2 |
| Fig.2 (Cl | aim Map) (1:31,680) | | | 3 |
| Fig.3 (Ge | meral Geology) (1:250,000) | - | | 4 |
| Fig.4A (Gr | avity plot with Pb Geochemistry | <i>i</i>) | | In pocket |
| Fig.4B (Gr | avity Plot with Zn Geochemistry | 1) | • | In pocket |

.

1.0 INTRODUCTION

1.1 Location and Access

The property covers the Crawford Bay Peninsula as well as the area near the mouth of Sherredon Creek located 3-8km south of Riondel, B.C.. Access is via good paved roads from Creston, B.C. or via ferry from Nelson, B.C.

1.2 Claim Status

The property consists of 57 units in two blocks (Doe and Ray). The claims were considered as one property for the sake of the gravity survey.

| Claim Name | Tenure # | # of units | Expiry Date |
|------------|----------|------------|--------------|
| Doel | 358996 | 9 | Sept.6,1999 |
| Doe2 | 358997 | 4 | 55 77 66 |
| Rayl | 358150 | 15 | July 31,1999 |
| Ray2 | 358151 | 12 | Aug.1,1999 |
| Ray3 | 358152 | 15 | cc >> cc |
| Ray4 | 358153 | 2 | CC 77 CC |

1.3 History

The area is most famous for hosting the Bluebell deposit which produced over 5.3 million tons of 4.9%Pb, 5.2%Zn, 1.3oz/t Ag. Several large boulders of sulphide ore are found scattered on the claims including one large boulder on the Doe claims which was actually mined (450 tons Pb,Zn, Ag). Previous workers have conducted HLEM and other surveys over the area, drilled anomalies , but never found the source of the boulders or the Pb/Zn anomalies in soil and rock.

1.4 Objectives of the Present Program

The objectives of the 1997 program were to see if gravity would delineate any areas of density contrast that could be interpreted as massive sulphide. The geochemical program was designed to look for East-West and North-South structures that may be mineralized.

(1)







2.0 GEOLOGY

2.1 Regional Geology

The property area lies within the Pb,Zn metallogenic province known as the Kootenay Arc which consists of Late Proterozoic to Early Paleozoic age strataform and stratabound limestones and dolomites. Rocks on the property consist of north-trending and westdipping succession of Lower Cambrian quartzites, pelitic schists, calcareous schists, and marble.

Three kilometers north of the property lies the Bluebell deposit which produced over 5.3 million tons of 4.9%Pb, 5.2%Zn and 1.3oz/tAg.

2.2 Property Geology

The property is underlain by limestone and dolomite of the upper Proterozoic Badshot Formation as well as graphitic schist, chloritic schist quartzites and a gneissic package of the Lardeau Series. Occasional granodiorite intrusions are seen on the claims and these have locally altered the intruded limestones to marble.

The property contains several float boulders of massive sulphide float that could have either come down-ice from the Bluebell deposit or may have not traveled far from a buried local source.

3.0 GEOCHEMISTRY

3.1 Soil Sampling Program and Results

Soil sample sites were chosen to show any mineralized North-South or East-West structures. A total of 290 samples were taken but only samples were submitted to Bondar-Clegg (Intertek Testing) for 32 element geochemical analysis. Figure 4 (in pocket) shows soil sample locations (Lines A-D). Anomalous values in this area are known from previous work to be greater than 70 ppb for Pb and greater than 220 ppm for Zn. These values are higher than normal due to the carbonate terrain. Anomalous results are circled in fig.4 but are not contoured due to the large line spacing.

Results show that more than half the samples assayed were anomalous in Zinc and at least 25% of the samples were anomalous in Pb.(see fig.4)

Samples were taken from the "B" soil horizon at depths of 10-20cm from surface. Samples were sent to Chemex Labs Ltd. For analysis. Samples were sieved to -80 mesh and digested using aqua-regia solution. They were analyzed for ppm Pb,Zn and Ag using Atomic Absorption techniques.

4.0 Gravity Report

•

SUMMARY REPORT

on a

GRAVITY SURVEY

conducted on the

DOE RAY PROJECT

Near Nelson, British Columbia

| PROPERTY | Northeast of Cranbrook, British Columbia UTM Zone 11 Easting: 509000 - 516000 UTM Zone 11 Northing: 5496000 -5514000 |
|---------------|--|
| SURVEY PERIOD | : October 24 to October 25, 1997 |
| WRITTEN FOR | Klondike Gold Corporation 1000 – 675 West Hastings Street Vancouver, British Columbia, V6C 1S4 |
| WRITTEN BY | Tam Mitchell, AScT QUADRA SURVEYS 2-8640 Blundell Road Richmond, British Columbia, V6R 1K1 |
| DATED | November 5, 1997 |

OUADRA SURVEYS

SUMMARY

A regional gravity survey was conducted in the Crawford Bay area. The property hosts a geological terrain known to be prospective for sedex type deposits. The purpose of the work was to define possible mineralized zones and geologic structures in the area.

The gravity survey was conducted with 4WD access on existing roads. Gravity measurements were carried out using a Scintrex gravity meter. The station locations were obtained with a real time Trimble double differential GPS survey system. Inclinometer readings were taken at every station to a distance of 170 meters for terrain corrections.

The gravity data were corrected for the various influences to yield partial Bouguer gravity anomaly values listed herein.

٠

TABLE OF CONTENTS

| Introduction . | • | | | - | • | | | • | 1 |
|--------------------------|--------|---|---|---|---|---|---|---|----|
| Location Map . | - | | • | | | | | • | 2 |
| Location and Access | | • | | | | | | | 3 |
| Survey Procedure | | | | • | | • | • | | 3 |
| Instrumentation | | | | | | | - | | 5 |
| Data Reduction and Fe | ormula | e | | | | • | | • | 6 |
| Results & Interpretation | on | | | | | | | • | 8 |
| Survey Precision | | | | | | | ٠ | | 8 |
| References . | - | | | | | • | • | • | 9 |
| Statement of Qualifica | ations | | | | | | | | 10 |

Appendices

| Gravity & GPS Base Stations . | | | | Ι |
|---|---|---|---|-----|
| Table of Field Notes, Calculations & Gravity Values | • | • | • | Π |
| Partial Bouguer Anomaly Plan Map | | | | III |

Illustrations

| Figure 1 - Location Map | - Scale 1: | :1,000,0 | 000 | • | | • | • | 2 |
|-------------------------|------------|----------|-----|---|---|---|-------|-------|
| Figure 2 – Gravity Base | Station | | | | | | Appen | dix I |
| Figure 3 – GPS Base Sta | ations | | • | | • | • | Appen | dix I |

MAPS

| Location Map | | | | | |
|-------------------------|-------------------|---|---|-------|---------|
| Figure 1 | Scale 1:1,000,000 | - | • | • | 2 |
| Partial Bouguer Anomaly | Plan Map | | | | |
| Figure 5 | Scale 1:100,000 | | | Appen | dix III |

INTRODUCTION

At the request of Klondike Gold Corporation a gravity survey was conducted in the Crawford Bay area, East-Northeast of Nelson BC. This report describes the instrumentation, theory, field procedure, data reduction and results of the 2 day survey which commenced October 24 and was completed October 25, 1997.

The survey was conducted by Tam Mitchell, AscT of Richmond, BC with the assistance of Zyoji Jackson of Cranbrook, BC. The crew was based at the Hastings Management field office at 3380 Wilks Road in Cranbrook, but stayed at Nelson, BC while acquiring data. The exploration program was carried out under the field supervision of Glen Rodgers of Klondike Gold Corporation.

The main purpose of the survey was to identify geologic structures in the area to locate possible zones of sedex type mineralization. Gravity surveying is a very effective tool in locating lead and zinc mineralization, particularly because of the high specific gravity of any sulphide mineralization especially that of lead.

٩.



____ 2 ___

LOCATION and ACCESS

The property is located 30 km. to the East-Northeast of Nelson approximately defined by UTM Zone 11; Easting: 509000 to 516000 and Northing: 5496000 to 5514000. See figure 1.

Access to the property was primarily on existing roads and logging roads accessible from Highway No. 3A at Crawford Bay.

SURVEY PROCEDURE

All gravity readings were tied to the National Gravity Net by a gravity base station established in a 1996 gravity survey. The base is located at the Cranbrook field office at 3380 Wilks Road and is marked by a steel spike and identified by a wooden stake with an aluminum tag reading: "Gravity Base -101". Geographic coordinates for the station were derived by GPS measurements as 49° 32' 48.07384" N and 115° 48' 44.86830" W (see figure 2). The station has a National Gravity Net value of 980688.13 ± 0.02 mgal. Field ties were also made to the nearest field base used for the GPS base station.

All Survey locations were referenced to a control point identified as -271. The coordinates for this station were obtained by an autonomous GPS fix. The station is further described as follows:

| Nad 83 Northing | 5501591.673 m | Approximate only |
|-----------------|---------------|------------------|
| Nad 83 Easting | 513300.825 m | Approximate only |
| CVD28 Elevation | 523.045 m | Approximate only |

ę

Tam Mitchell, AScT, of Richmond BC, with the assistance of Zyoji Jackson of Cranbrook BC acquired the field data. A total of 48 stations were acquired during the 2 days of the survey.

The gravity survey was conducted with 4WD on existing logging roads and public access roads.

Inclinometer readings were taken on each gravity station with a Suunto inclinometer to provide inner zone terrain corrections in accordance with the Hammer Chart method. Zone B inclinometer readings were taken at 0, 90, 180 and 270 at a distance of 9.3 meters from the station. Zones C and D were shot at 0, 60, 120, 180, 240, and 300 degrees at distances of 35 and 112 meters respectively. Distances and angles were estimated.

۹,

INSTRUMENTATION

GRAVITY

The gravity readings were taken with a Scintrex CG-3 gravity meter (serial no. 10345) manufactured in Concord Ontario. The instrument has a world wide calibration range of over 7,000 mgal and a reading resolution of 0.005 mgal. This instrument features a sensor based on a fused quartz elastic system. The proof mass is balanced by a spring and a relatively small electrostatic restoring force. The position of the mass, which is sensed by a capacitative displacement transducer, is altered by a change in gravity. The inherent strength and elastic properties of the fused quartz together with stop limits around the proof mass permit the instrument to be operated without clamping. Instrument drift is considerably reduced by precise thermostatic control of the unit and software correction for residual effects. The instrument's tilt sensors are analog as well as electronic with a resolution of 1 arc second. Real time corrections for tilt errors can be automatically made for a range of \pm 200 arc seconds. The entire gravity sensing mechanism is enclosed in a vacuum chamber to provide isolation from variations in atmospheric pressure. This extremely stable operating environment allows the long term drift of the sensor to be accurately predicted, and real time software correction reduces it to less than 0.02 mGals/day in theory. The unit can also automatically compensate for earth tides. The ETC is generated using the Longman formula (gravimetric factor 1.16).

SURVEYING

Station locations were surveyed using the Trimble Site Surveyor 4400 system with a Pacific Crest radio link. The system used was capable of post-processing rapid static measurements with an accuracy of ± 5 mm +1ppm horizontal and ± 1 cm + 1ppm vertical or real time data acquisition with an accuracy rating of ± 1 cm +2ppm horizontal and ± 2 cm + 2ppm vertical.

The Site Surveyor 4400 is based on Trimble's fourth generation real-time survey technology. Incorporating the latest Trimble real-time GPS engine code and solution alogrithms, the system provides very fast on-the-fly (OTF) initializations with the industry's most reliable position results. With this technology, average initialization times are cut in half. With advanced satellite signal acquisition and tracking, the ability to survey near trees is enhanced and downtime due to loss of signal minimized.

DATA REDUCTION and FORMULAE

The gravity data was processed by computer in the following manner:

- g_n Observed Gravity- field observations corrected for earth tides and long term instrument drift were downloaded from electronic storage in the gravity meter and corrections made for instrument height and residual instrument drift. These values were then tied to the National Gravity Net.
- g_{fa} Free Air Effect- Correction for relative distances of observation points from the centre of mass(earth). This calculation moves all stations to a common elevation datum and corrects for relative distances in distance from the source mass. The elevation datum used was CGVD 28 mean sea level. The formulae used was:

 g_{fa} = -0.3086 mgal/m

g_{bs} Bouger Slab Effect - Correction for the relative differences in amounts of surface rock below gravity stations. This calculation requires that a mean density or rock type between the lowest and highest grid elevations be established. All stations are shifted to a common datum as in the free air effect except that the vertical change is through an assumed slab of the derived density. The elevation datum used was CGVD 28 mean sea level.

 $g_{bs} = 2*PI*.00667*\sigma mgal/m$

Where $\sigma = \text{slab density (gm/cc)}$

g₁ Theoretical Gravity - Yields correction for change of observed gravity with change in latitude which is due primarily to the rotation of the earth and the difference in earth's radius between the poles and the equator.

۹

2

2

 $g_l = g_e(1 + \alpha \sin^2 \theta + \beta \sin^2 2\theta)$

Where $g_e =$ equatorial gravity = 978,031.85 mgal.

- $\alpha = 0.005278895$
- $\beta = -0.000023462$
- θ = Latitude

Terrain Correction- corrections for variations caused by local terrain. The vertical component of the gravitational effect exerted by nearby hills, or not exerted by nearby valleys or gullies, will effect the net reading obtained on any one station. The overall effect on a given line profile or area will be a function of the station spacing relative to the frequency of terrain undulations. Areas were segmented using circular sectors in zones developed by Hammer (1939). Corrections were made for zones B, C, and D (covering an area from 2 to 170 meters from the station).

g₁ was calculated from the following expression:

gt

$$g_{t} = \Sigma \Phi \tau \sigma [r_{o} - r_{i} + (r_{o}^{2} + z^{2})^{\frac{1}{2}} - (r_{o}^{2} + z^{2})^{\frac{1}{2}}]$$

Where Φ = Sector angle (B = 90°, C & D = 60 °)

 $\tau = \text{gravitational constant} = 0.00667$

- σ = average density (gm/cc)
- r_0 = outer sector radius (B=16.6, C=53.3, D=170)
- $r_i = inner sector radius (B=2, C=16.6, D=53.3)$
- z = elevation difference between sector and station.

٩

g_{fas} Free Air Anomaly: is derived from the following formulae:

 $g_{faa} = g_0 - (g_1 - 0.3086 * E) =$ Free Air Anomaly

Where g_0 = observed gravity g_1 = theoretical gravity E = CGVD 28 elevation

g_{ba} **Bouguer Anomaly:** was derived from the following formulae:

 $g_{ba} = g_b + g_{faa} + g_t = Bouguer Gravity$

Where $g_b =$ Bouguer gravity

 $g_{faa} = free air anomaly$

 $g_t = terrain \ corrections$

---- 7 -----

RESULTS & INTERPRETATION

The data was reduced to partial Bouguer gravity anomaly values. Terrain corrections have been applied to 170 meters. A density of 2.67 gm/cc was used throughout the survey. The partial Bouguer Gravity anomaly values spanned a range of 15.01 milligals from a low of -172.35 mgal to a high of -157.34 mgal. The mean partial Bouguer value was -163.93 ± 3.73 mgal. The survey identified a number of major and minor geologic trends and areas of interest.

SURVEY PRECISION

GRAVITY

Daily gravity loop ties were made to the base station -101 and to field base -271 as follows:

| Station | Loop Tie in mgal | Notes |
|---------|------------------|--------------------------|
| -101 | 0.01 | Calculated 2 day closure |
| -271 | 0.06 | |
| -271 | 0.07 | |

LOCATION

On every station location the GPS system was re-initialized to verify the accuracy of the recorded station location.

REFERENCES

LaCoste & Romberg Instruction Manual, Model G and D Gravity Meter, June 1989

Seigel, H.O.; A Guide to High Precision Land Gravimeter Surveys, August 1995

Telford, W. M., Geldart, L. P., Sheriff, R. E., Keys, D. A.; Applied Geophysics, 1982

Longman, I. M.; Journal of Geophysical Research, Volume 64, No. 12; Formulas for Computing the Tidal Accelerations Due to the Moon and Sun, December 1959

۹,

Hammer, 1939; (Terrain Correction Model)

STATEMENT OF QUALIFICATIONS

I Thomas L. Mitchell, AScT, of the city of Richmond, Province of British Columbia, DO HEREBY CERTIFY THAT:

- 1. I am the owner of Quadra Surveys with office at 2-8640 Blundell Road, Richmond, British Columbia, V6R 1K1.
- 2. 1 am a graduate of BCIT, with a diploma in Surveying Technology (1977).
- 3. 1 am a geophysical surveyor, registered with the Association of Applied Science Technologists and Technicians of British Columbia.
- 4. I have practiced my profession in Africa, Canada, Japan and USA for 19 years.
- 5. This report is based on a gravity survey which I conducted.
- 6. I have no direct or indirect interest in the property nor do I expect to receive any.

ę



Dated at Cranbrook, British Columbia, this 5th day of November, 1997.

APPENDIX I

Gravity & GPS Base Stations







APPENDIX II

Partial Bouguer Anomaly Gravity Data Listing

Real Time GPS Station Locations and Elevation Calculations

Observed Gravity Values – Electronic Notes from Gravity Meter

Observed Gravity Data Reduction and Calculations

Inner Zone Terrain Corrections



...

1997 Doe Ray Property Gravity Survey

Partial Bouguer Anomaly Gravity Data Listing Instrumentation: Scintrex CG3 Gravity Meter No.10345

Surveyed by: Quadra Surveys, October 1997

Operator: Tam Mitchell

Density 2.67

| | NAD 83 | NAD 83 | NAD 83 | NAD 83 | CGVD28 | | Theoretical | Terrain | Free Air | Bouguer |
|------|-------------|------------|-------------|---------------|---------|------------|-------------|---------|----------|---------|
| Stn | Northing | Easting | Latitude | Longitude | Elev | Observed G | Gravity | to 170m | Anomaly | Anomaly |
| 9711 | 5499818.956 | 514400.906 | 49.65074267 | -116.80049971 | 540.747 | 980736.20 | 981038.30 | 0.96 | -135.22 | -194.77 |
| 9712 | 5498697.215 | 515075.753 | 49.64063663 | -116.79119407 | 540.571 | 980733.24 | 981037.39 | 0.46 | -137.34 | -197.36 |
| 9713 | 5496617.843 | 515274.019 | 49.62192859 | -116.78852900 | 536.580 | 980734.45 | 981035.72 | 0.34 | -135.68 | -195.38 |
| 9714 | 5502054.771 | 512232.483 | 49.67090066 | -116.83046955 | 527.075 | 980749.33 | 981040.10 | 0.38 | -128.12 | -186.71 |
| 9715 | 5501333.603 | 512141.753 | 49.66441592 | -116.83174935 | 568.312 | 980744.15 | 981039.52 | 0.12 | -119.99 | -183.46 |
| 9716 | 5500611.237 | 512509.959 | 49.65791105 | -116.82667015 | 545.772 | 980746.74 | 981038.94 | 0.23 | -123.77 | -184.62 |
| 9717 | 5500625.529 | 512001.585 | 49.65804993 | -116.83371339 | 637.299 | 980731.02 | 981038.95 | 0.23 | -111.26 | -182.34 |
| 9718 | 5500665.007 | 511528.079 | 49.65841425 | -116.84027280 | 740.635 | 980712.19 | 981038.98 | 0.44 | -98.23 | -180.66 |
| 9719 | 5500841.449 | 511215,432 | 49.66000716 | -116.84459962 | 787.846 | 980704.41 | 981039.12 | 0.23 | -91.58 | -179.50 |
| 9720 | 5501080.234 | 511246.013 | 49.66215435 | -116.84416903 | 777.176 | 980706.95 | 981039.32 | 0.16 | -92.52 | -179.33 |
| 9721 | 5499737.531 | 511694.04 | 49.65006882 | -116.83800104 | 821.415 | 980696.58 | 981038.23 | 0.15 | -88.17 | -179.93 |
| 9722 | 5499587 185 | 512079.931 | 49.64870892 | -116.83265989 | 818.620 | 980695.56 | 981038.11 | 0.70 | -89.93 | -180.83 |
| 9723 | 5499337.65 | 512106.224 | 49.64646393 | -116.83230338 | 830.255 | 980693.47 | 981037.91 | 0.30 | -88.22 | -180.83 |
| 9724 | 5498566.465 | 512059.691 | 49.63952838 | -116.83297169 | 840.181 | 980692.04 | 981037.29 | 0.20 | -85.97 | -179.79 |
| 9725 | 5505508.435 | 509707.517 | 49.70201064 | -116.86537729 | 623.706 | 980734.70 | 981042.88 | 0.22 | -115.70 | -185.27 |
| 9726 | 5506311.326 | 509648.859 | 49.70923318 | -116.86617091 | 545.515 | 980747.84 | 981043.52 | 0.24 | -127.34 | -188.14 |
| 9727 | 5504867.146 | 509484.047 | 49.69624613 | -116.86849190 | 593.515 | 980739.61 | 981042.36 | 0.35 | -119.59 | -185.66 |
| 9728 | 5504174.217 | 509522.637 | 49.69001296 | -116.86797369 | 591.691 | 980739.97 | 981041.80 | 0.48 | -119.24 | -184.97 |
| 9729 | 5503023.421 | 509247.044 | 49.67966640 | -116.87182185 | 548.729 | 980749.07 | 981040.88 | 0.07 | -122.47 | -183.80 |
| 9730 | 5502369.146 | 509161.138 | 49.67378281 | -116.87302796 | 531.433 | 980751.19 | 981040.35 | 0.60 | -125.16 | -184.03 |
| 9731 | 5503904.246 | 510275.151 | 49.68757234 | -116.85754761 | 663.052 | 980729.93 | 981041.59 | 0.22 | -107.04 | -181.01 |
| 9732 | 5503757.344 | 509569.583 | 49.68626265 | -116.86733301 | 599.390 | 980739.93 | 981041.47 | 0.23 | -116.57 | -183.42 |

·

1997 Doe Ray Property Gravity Survey

Partial Bouguer Anomaly Gravity Data Listing

Instrumentation: Scintrex CG3 Gravity Meter No.10345

Surveyed by: Quadra Surveys, October 1997

Operator: Tam Mitchell

Density 2.67

| | NAD 83 | NAD 83 | NAD 83 | NAD 83 | CGVD28 | | Theoretical | Terrain | Free Air | Bouguer |
|------|-------------|---------------------|-------------|---------------|---------|------------|-------------|---------|-----------------|---------|
| Stn | Northing | Easting | Latitude | Longitude | Elev | Observed G | Gravity | to 170m | Anomaly | Anomaly |
| -271 | 5501591.673 | 513300.825 | 49.66671269 | -116.81567918 | 523.045 | 980745.14 | 981039.72 | 0.00 | -133.17 | -191.70 |
| 9601 | 5503715.66 | 511195.846 | 49.68585970 | -116.84478874 | 645.916 | 980733.54 | 981041.43 | 0.06 | -108.56 | -180.78 |
| 9602 | 5505110.528 | 510063.459 | 49.69842583 | -116.86045139 | 721.186 | 980717.92 | 981042.56 | 0.19 | -102.08 | -182.58 |
| 9603 | 5513216.989 | 510305.172 | 49.77133481 | -116.85688534 | 525,935 | 980740.98 | 981049.07 | 0.07 | -145.79 | -204.57 |
| 9604 | 5512270.479 | 510264.619 | 49.76282223 | -116.85747349 | 548.331 | 980739.72 | 981048.31 | 0.03 | -139.37 | -200.70 |
| 9605 | 5512133.841 | 510037.537 | 49.76159708 | -116.86063009 | 546.813 | 980739.78 | 981048.20 | 0.10 | -139.67 | -200.76 |
| 9606 | 5512169.57 | 509849.161 | 49.76192157 | -116.86324475 | 528.234 | 980742.14 | 981048.23 | 0.24 | -143.08 | -201.95 |
| 9607 | 5512039.715 | 510458. 49 4 | 49.76074330 | -116.85478770 | 559,129 | 980737.45 | 981048.12 | 0.02 | -138.13 | -200.67 |
| 9608 | 5511017.22 | 510493.917 | 49.75154595 | -116.85432342 | 589,747 | 980732.50 | 981047.30 | 0.31 | -132.81 | -198.49 |
| 9609 | 5509462.784 | 510399.678 | 49.73756633 | -116.85567312 | 646.207 | 980725.40 | 981046.05 | 0.69 | -121.23 | -192.85 |
| 9610 | 5508753.385 | 510509.133 | 49.73118379 | -116.85417324 | 661.817 | 980724.43 | 981045.48 | 0.19 | -116.81 | -190.68 |
| 9611 | 5508421.865 | 509936.362 | 49.72821168 | -116.86212953 | 550.236 | 980743.99 | 981045.22 | 0.39 | -131.43 | -192.60 |
| 9612 | 5508773.847 | 511012.884 | 49.73135882 | -116.84718253 | 732.845 | 980711.82 | 981045.50 | 0.22 | -107.52 | -189.31 |
| 9613 | 5507857.29 | 510526.921 | 49.72312359 | -116.85395059 | 678.011 | 980722.34 | 981044.76 | 0.59 | -113.19 | -188.46 |
| 9614 | 5507122.001 | 509842.868 | 49.71652164 | -116.86345958 | 594.825 | 980738.35 | 981044.17 | 0.28 | -122.26 | -188.53 |
| 9615 | 5506447.515 | 510119.449 | 49.71045040 | -116.85964035 | 652.997 | 980728.77 | 981043.63 | 0.58 | -113.35 | -185.84 |
| 9701 | 5502292.652 | 513044.073 | 49.67302328 | -116.81921383 | 529.557 | 980747.82 | 981040.29 | 0.00 | -129.05 | -188.30 |
| 9702 | 5502894.308 | 512564.653 | 49.67844506 | -116.82583905 | 543.940 | 980748.88 | 981040.77 | 0.00 | -124.03 | -184.89 |
| 9703 | 5502111.988 | 513497.16 | 49.67138832 | -116.81294047 | 539.669 | 980745.93 | 981040.14 | 0.12 | -127.67 | -187.93 |
| 9704 | 5502931.122 | 513499.307 | 49.67875598 | -116.81288245 | 579.989 | 980741.64 | 981040.80 | 0.09 | -120.17 | -184.98 |
| 9705 | 5504602.169 | 514145.232 | 49.69377138 | -116.80386869 | 615.343 | 980733.15 | 981042.14 | 0.22 | -119.09 | -187.73 |
| 9706 | 5506105.796 | 514694.543 | 49.70728255 | -116.79619569 | 666.990 | 980722.32 | 981043.35 | 0.06 | -115.19 | -189.77 |
| 9707 | 5504788.291 | 513358.56 | 49.69546341 | -116.81476991 | 602.938 | 980737.00 | 981042.29 | 0.00 | -119.22 | -186.69 |
| 9708 | 5504115.307 | 512827.944 | 49.68942180 | -116.82214949 | 593.991 | 980740.80 | 981041.75 | 0.06 | -117.65 | -184.05 |
| 9709 | 5503435.83 | 512455.28 | 49.68331806 | -116.82733784 | 570.866 | 980745.39 | 981041.21 | 0.03 | -119.65 | -183.49 |
| 9710 | 5501191.743 | 513922.609 | 49.66310148 | -116.80707686 | 541.711 | 980742.08 | 981039.40 | 0.76 | -1 30.15 | -190.00 |

....

.

1997 Doe Ray Property Gravity Survey

Real Time Station Locations and Elevation Calculations

Instrumentation: Trimble RTK 4400 SSI Surveyor

Surveyed by: Quadra Surveys, October 1997

| | | | Latit | tude | | Long | itude \ | Nest | | | | | Corrected |
|------|-------------|------------|-------|------|----------|------|---------|-------------------|---------|--------|-------|---------------------|-----------|
| Name | Northing | Easting | dd | mm | 85.85555 | dd | mm | 55.855 5 5 | Elev | GSD95W | Lat | Long | Elev |
| 9712 | 5498697.215 | 515075.753 | 49 | 38 | 26.29188 | 116 | 47 | 28.29864 | 540,631 | -14.89 | 49,64 | -116.79 | 540.571 |
| 9713 | 5496617.843 | 515274.019 | 49 | 37 | 18.94294 | 116 | 47 | 18.7044 | 536.65 | -14.88 | 49.62 | -116.7 9 | 536.580 |
| 9714 | 5502054.771 | 512232.483 | 49 | 40 | 15.24239 | 116 | 49 | 49.69039 | 527.025 | -15 | 49.67 | -116.83 | 527.075 |
| 9715 | 5501333.603 | 512141.753 | 49 | 39 | 51.89731 | 116 | 49 | 54.29767 | 568.232 | -15.03 | 49.66 | -116.83 | 568.312 |
| 9716 | 5500611.237 | 512509 959 | 49 | 39 | 28.47979 | 116 | 49 | 36.01255 | 545.702 | -15.02 | 49.66 | -116.83 | 545.772 |
| 9717 | 5500625.529 | 512001.585 | 49 | 39 | 28.97973 | 116 | 50 | 1.3682 | 637.189 | -15.06 | 49.66 | -116.83 | 637.299 |
| 9718 | 5500665.007 | 511528.079 | 49 | 39 | 30.29129 | 116 | 50 | 24.98208 | 740.505 | -15.08 | 49.66 | -116.84 | 740.635 |
| 9719 | 5500841.449 | 511215.432 | 49 | 39 | 36.02578 | 116 | 50 | 40.55862 | 787.696 | -15.1 | 49.66 | -116.84 | 787.846 |
| 9720 | 5501080.234 | 511246.013 | 49 | 39 | 43.75567 | 116 | 50 | 39.00852 | 777.036 | -15.09 | 49.66 | -116.84 | 777.176 |
| 9721 | 5499737.531 | 511694.04 | 49 | 39 | 0.24774 | 116 | 50 | 16.80375 | 821.285 | -15,08 | 49.65 | -116.84 | 821.415 |
| 9722 | 5499587.185 | 512079.931 | 49 | 38 | 55.3521 | 116 | 49 | 57.57562 | 818.53 | -15.04 | 49,65 | -116.83 | 818.620 |
| 9723 | 5499337.65 | 512106.224 | 49 | 38 | 47.27016 | 116 | 49 | 56.29218 | 830.165 | -15.04 | 49.65 | -116.83 | 830.255 |
| 9724 | 5498566.465 | 512059.691 | 49 | 38 | 22.30218 | 116 | 49 | 58.6981 | 840.091 | -15.04 | 49.64 | -116.83 | 840.181 |
| 9725 | 5505508.435 | 509707.517 | 49 | 42 | 7.23832 | 116 | 51 | 55.35824 | 623.556 | -15.1 | 49.70 | -116.87 | 623.706 |
| 9726 | 5506311.326 | 509648.859 | 49 | 42 | 33.23943 | 116 | 51 | 58.21527 | 545.375 | -15.09 | 49.71 | -116.87 | 545.515 |
| 9727 | 5504867.146 | 509484.047 | 49 | 41 | 46.48605 | 116 | 52 | 6.57083 | 593.365 | -15,1 | 49.70 | -116.87 | 593.515 |
| 9728 | 5504174.217 | 509522.637 | 49 | 41 | 24.04667 | 116 | 52 | 4.70528 | 591.541 | -15.1 | 49.69 | -116.87 | 591.691 |
| 9729 | 5503023.421 | 509247.044 | 49 | 40 | 46.79903 | 116 | 52 | 18.55865 | 548.569 | -15,11 | 49.68 | -116.87 | 548.729 |
| 9730 | 5502369.146 | 509161.138 | 49 | 40 | 25.61812 | 116 | 52 | 22.90065 | 531.263 | -15.12 | 49.67 | -116.87 | 531.433 |
| 9731 | 5503904.246 | 510275.151 | 49 | 41 | 15.26043 | 116 | 51 | 27.17141 | 662,912 | -15.09 | 49.69 | -116.86 | 663.052 |
| 9732 | 5503757.344 | 509569.583 | 49 | 41 | 10.54554 | 116 | 52 | 2.39885 | 599.23 | -15.11 | 49.69 | -116.87 | 599.390 |

1997 Doe Ray Property Gravity Survey

Real Time Station Locations and Elevation Calculations Instrumentation; Trimble RTK 4400 SSI Surveyor Surveyed by: Quadra Surveys, October 1997

| | | | Latit | ude | | Long | itude \ | West | | | | | Corrected |
|------|-------------|------------|-------|------------|----------|------|---------|------------------|---------|--------|---------------|---------|-----------|
| Name | Northing | Easting | dd | mm | 88,88888 | dd | mm | 55.55855 | Elev | GSD95W | Lat | Long | Elev |
| -271 | 5501591.673 | 513300.825 | 49 | 4 0 | 0.1657 | 116 | 48 | 56.44504 | 523.045 | -14.95 | 49.67 | -116.82 | 523.045 |
| 9601 | 5503715.66 | 511195.846 | 49 | 41 | 9.09492 | 116 | 50 | 41.23947 | 645.796 | -15.07 | 49.69 | -116.84 | 645.916 |
| 9602 | 5505110.528 | 510063.459 | 49 | 41 | 54,33298 | 116 | 51 | 37,625 | 721.046 | -15.09 | 49.70 | -116.86 | 721.186 |
| 9603 | 5513216.989 | 510305.172 | 49 | 46 | 16.80533 | 116 | 51 | 24.78723 | 525.885 | -15 | 4 9.77 | -116.86 | 525.935 |
| 9604 | 5512270.479 | 510264.619 | 49 | 45 | 46.16001 | 116 | 51 | 26.90455 | 548,271 | -15.01 | 49.76 | -116.86 | 548.331 |
| 9605 | 5512133.841 | 510037.537 | 49 | 45 | 41.7495 | 116 | 51 | 38.26831 | 546,743 | -15.02 | 49.76 | -116.86 | 546.813 |
| 9606 | 5512169.57 | 509849.161 | 49 | 45 | 42.91764 | 116 | 51 | 47.681 11 | 528,154 | -15.03 | 49.76 | -116.86 | 528.234 |
| 9607 | 5512039.715 | 510458.494 | 49 | 45 | 38.67589 | 116 | 51 | 17.23571 | 559.069 | -15.01 | 49 .76 | -116.85 | 559.129 |
| 9608 | 5511017.22 | 510493.917 | 49 | 45 | 5.56542 | 116 | 51 | 15.56431 | 589.677 | -15.02 | 49.75 | -116.85 | 589.747 |
| 9609 | 5509462.784 | 510399.678 | 49 | 44 | 15.2388 | 116 | 51 | 20.42323 | 646,107 | -15.05 | 49.74 | -116.86 | 646.207 |
| 9610 | 5508753.385 | 510509.133 | 49 | 43 | 52.26163 | 116 | 51 | 15.02365 | 661.717 | -15.05 | 49.73 | -116.85 | 661.817 |
| 9611 | 5508421.865 | 509936.362 | 49 | 43 | 41.56205 | 116 | 51 | 43.66631 | 550,116 | -15.07 | 49.73 | -116.86 | 550.236 |
| 9612 | 5508773.847 | 511012.884 | 49 | 43 | 52.89174 | 116 | 50 | 49.8571 | 732.755 | -15.04 | 49.73 | -116.85 | 732.845 |
| 9613 | 5507857.29 | 510526.921 | 49 | 43 | 23.24492 | 116 | 51 | 14.22212 | 677.901 | -15.06 | 49.72 | -116.85 | 678.011 |
| 9614 | 5507122.001 | 509842.868 | 49 | 42 | 59.4779 | 116 | 51 | 48.45449 | 594.695 | -15.08 | 49.72 | -116.86 | 594.825 |
| 9615 | 5506447.515 | 510119.449 | 49 | 42 | 37.62144 | 116 | 51 | 34.70525 | 652.867 | -15.08 | 49.71 | -116.86 | 652.997 |
| 9701 | 5502292.652 | 513044.073 | 49 | 40 | 22.88379 | 116 | 49 | 9.16978 | 529.547 | -14.96 | 49.67 | -116.82 | 529.557 |
| 9702 | 5502894.308 | 512564.653 | 49 | 40 | 42.40223 | 116 | 49 | 33.02058 | 543.91 | -14.98 | 49.68 | -116.83 | 543.940 |
| 9703 | 5502111.988 | 513497.16 | 49 | 40 | 16.99794 | 116 | 48 | 46.58569 | 539.679 | -14,94 | 49.67 | -116.81 | 539.669 |
| 9704 | 5502931.122 | 513499.307 | 49 | 40 | 43.52152 | 116 | 48 | 46.37683 | 580,009 | -14,93 | 49.68 | -116.81 | 579.989 |
| 9705 | 5504602.169 | 514145.232 | 49 | 41 | 37.57696 | 116 | 48 | 13.9273 | 615.413 | -14,88 | 49.69 | -116.80 | 615.343 |
| 9706 | 5506105.796 | 514694.543 | 49 | 42 | 26.21717 | 116 | 47 | 46.30449 | 667.11 | -14.83 | 49.71 | -116.80 | 666.990 |
| 9707 | 5504788.291 | 513358.56 | 49 | 41 | 43.66828 | 116 | 48 | 53,17169 | 602,968 | -14.92 | 49.70 | -116.81 | 602.938 |
| 9708 | 5504115.307 | 512827.944 | 49 | 41 | 21.91847 | 116 | 49 | 19.73817 | 593.991 | -14.95 | 49.69 | -116.82 | 593.991 |
| 9709 | 5503435.83 | 512455.28 | 49 | 40 | 59.94501 | 116 | 49 | 38.41623 | 570.836 | -14.98 | 49.68 | -116.83 | 570.866 |
| 9710 | 5501191.743 | 513922.609 | 49 | 39 | 47.16532 | 116 | 48 | 25.47671 | 541.721 | -14.94 | 49.66 | -116.81 | 541.711 |
| 9711 | 5499818.956 | 514400.906 | 49 | 39 | 2.6736 | 116 | 48 | 1.79897 | 540.777 | -14.92 | 49.65 | -116.80 | 540.747 |

1997 Doe Ray Property Gravity Survey

ī irta

Instrumentation; Scintrex CG3 Gravity Meter No.10345 Surveyed by: Quadra Surveys, October 1997

| Station | Grav. | SD. | Tilt | x | Tilt y | Temp | . E | T.C. | Dur | # Rej | Tin | ne |
|---------|-------|-------|-------------|---|--------|------|-----|------|------|-------|-----|----------|
| | -271 | 4265. | 856 | • | 0 | -19 | 6 | -1.3 | 0 | 60 | 6 | 11:21:54 |
| | 9701 | 4268 | 526 | * | 0.1 | -1 | 3 | -1.3 | 0 | 60 | 0 | 11:28:56 |
| | 9702 | 4269. | 598 | * | 0.1 | -15 | 13 | -1.4 | 0 | 60 | 1 | 11:34:12 |
| | 9703 | 4266. | .645 | * | 0 | -4 | 8 | -1.4 | 0 | 60 | 6 | 11:39:59 |
| | 9704 | 4262 | 354 | * | 0 | 3 | 12 | -1.4 | 0 | 60 | 0 | 11:46:05 |
| | 9705 | 4253. | 867 | * | 0 | -5 | 6 | -1.4 | 0 | 60 | 0 | 11:52:16 |
| | 9706 | 4243. | 034 | # | 0 | -6 | 5 | -1.4 | 0 | 60 | 5 | 11:58:03 |
| | 9707 | 4257. | 736 | * | 0.1 | 4 | 9 | -1.3 | -0 | 60 | 0 | 12:06:17 |
| | 9708 | 4261. | 533 | * | 0 | -12 | 4 | -1.3 | -0 | 60 | 2 | 12:16:31 |
| | 9709 | 4266. | 116 | * | 0.1 | -2 | 0 | -1.3 | -0 | 60 | 0 | 12:22:53 |
| | 9710 | 4262. | 812 | * | 0 | 11 | 13 | -1.3 | -0 | 60 | 0 | 12:35:08 |
| | 9711 | 4256. | 938 | * | 0.1 | -12 | 7 | -1.3 | -0 | 60 | 0 | 12:40:35 |
| | 9712 | 4253. | 974 | * | 0.1 | 1 | 7 | -1.3 | -0 | 60 | 0 | 12:51:50 |
| | 9713 | 4255. | 198 | * | 0.1 | -9 | 11 | -1.3 | -0 | 60 | 0 | 12:58:52 |
| | 9714 | 4270. | 058 | * | 0.1 | -20 | 12 | -1.3 | -0 | 60 | 0 | 13:12:44 |
| | 9715 | 4264 | 878 | * | 0.1 | -13 | -28 | -13 | -0 | 60 | 6 | 13:17:43 |
| | 9716 | 4267. | 471 | • | 0 | 2 | 4 | -1.3 | -0 | 60 | 0 | 13:23:08 |
| | 9717 | 4251. | 757 | * | 0.1 | -22 | 17 | -1.4 | -0 | 60 | 0 | 13:33:22 |
| | 9718 | 4232 | 932 | • | 0.1 | 0 | 3 | -1.3 | -0 | 60 | 2 | 13:44:58 |
| | 9719 | 4225. | .154 | * | 0 | -1 | 10 | -1.3 | -0 | 60 | 1 | 13:51:51 |
| | 9720 | 4227 | 707 | ¥ | 0 | 9 | 13 | -1.3 | -0 | 60 | 0 | 13:56:26 |
| | 9721 | 4217 | .318 | * | 0 | -9 | 1 | -1.3 | -0 | 60 | 3 | 14:09:18 |
| | 9722 | 4216. | 303 | * | 0.1 | 4 | 4 | -1.3 | -0 | 60 | 0 | 14:22:09 |
| | 9723 | 4214 | .228 | * | 0 | -6 | 2 | -1.3 | -0.1 | 60 | 0 | 14:27:30 |
| | 9724 | 4212. | 791 | 4 | 0 | -12 | 2 | -1.3 | -0.1 | 60 | 3 | 14:43:25 |
| | 9725 | 4255. | 453 | ŧ | 0 | -18 | 17 | -1.2 | -0.1 | 60 | 1 | 15:32:43 |
| | 9726 | 4268. | 603 | * | 0.1 | -27 | 6 | -1.2 | -0.1 | 60 | 5 | 15:47:58 |
| | 9727 | 426 | 0.37 | * | 0 | -10 | - 7 | -1.3 | -0.1 | 60 | 0 | 15:54:54 |
| | 9728 | 4260. | 748 | * | 0.1 | -10 | 3 | -1.3 | -0.1 | 60 | 0 | 16:00:05 |
| | 9729 | 4269. | 838 | * | 0.1 | 6 | 15 | -1.3 | -0.1 | 60 | 0 | 16:06:03 |
| | 9730 | 4271. | 953 | * | 0 | 32 | 17 | -1.3 | -0.1 | 60 | 1 | 16:11:03 |
| | 9731 | 4250 | .701 | * | 0 | -2 | 26 | -14 | -0.1 | 60 | 1 | 16:45:38 |
| | 9732 | 4260. | 69 8 | • | 0 | -1 | 6 | -1.3 | -0.1 | 60 | 0 | 16:50:53 |
| | -271 | 4265 | 936 | * | 0.1 | -19 | -1 | -1.3 | -0.1 | 60 | 5 | 17:19:54 |
| | -101 | 4208. | 857 | 1 | 0 | -33 | 16 | -1.2 | -0 | 60 | 3 | 20:55:52 |

٩

1.1.1.1.1

۰

1997 Doe Ray Property Gravity Survey

Instrumentation; Scintrex CG3 Gravity Meter No.10345 Surveyed by: Quadra Surveys, October 1997

| SCINTREX V5. | 0 AUTOG | RAV / Fie | eld Mode | 10' | R4. | 4 | | |
|--|---|---------------------|---|---------------------------------------|----------------|--|-----|-----------------|
| Line: 1024. G GREF.: GCAL.1: GCAL.2: TEMPCO: | irid: 0. Jot 0. mGa 5861.733 0. -0.1355 | o: 1. l Is De | Date: 97/ Tilt x sen Tilt y se g.Latitud | 10/24 nsit.: nsit.: e: e: | Ope | rator: 271.4 287.4 49.5 e [.] | 777 | 5.7 |
| Drift const.: | 0.17 | G | NT Differ | ence: | .9 | 6.hr | | |
| Drift Correction | Start Time: 2 Date: 97/07/15 | 3:33:43 5 O | Cal In-Line Ti | .after ilt Cor | x san recte | nples: d = "*" | 1 | 12 |
| Station Grav. | SD. Tilt x 7 | Filty Te | emp. E. | T.C. | Dur a | # Rej | Tim | е |
| -101 | 4208.877 * | 0 - | 11 0 | 09 | 0 | 60 | 0 | 9:08:09 |
| -271 | 4265.799 * | 0 - | 22 19 | -0.9 | -0.1 | 60 | 5 | 14:09:47 |
| 9601 | 4254.22 * | 0.1 | -6 11 | -1 | -0,1 | 60 | 2 | 14:49:00 |
| 9602 | 4238.595 * | 0 | 47 -11 | -1 | -0.1 | 60 | 3 | 15:13:27 |
| 9603 | 4261.668 * | 0 | 17 -10 | -1 | -0.1 | 60 | 1 | 15:36:51 |
| 9604 | 4260.425 * | 0.1 | 85 | -1.1 | -0.1 | 60 | 1 | 15:56:33 |
| 9605 | 4260.477 * | 0 | 7 25 | -1.1 | -0.1 | 60 | 0 | 16:08:11 |
| 9606 | 4262.845 * | 0 | -2 14 | -1.1 | -0.1 | 60 | 0 | 16:11:51 |
| 9607 | 4258.142 * | 0.1 - | 23 44 | -1.1 | -0.1 | 60 | 0 | 16:18:46 |
| 9608 | 4253.203 * | 0.1 - | 19 -6 | -1.2 | -0.1 | 60 | 0 | 16:25:57 |
| 9609 | 4246.109 * | 0.1 | 18 -5 | -1.2 | -0.1 | 60 | 0 | 16:38:38 |
| 9610 | 4245.136 * | 0.1 | -6 3 | -1.1 | -0.1 | 60 | 0 | 16:47:49 |
| 9611 | 4264.696 * | 0.1 | 4 1 | -1.1 | -0.1 | 60 | 0 | 17:02:52 |
| 9612 | 4232.535 * | 0 | 29 25 | -1.2 | -0.1 | 60 | 1 | 17:17:48 |
| 9613 | 4243.073 * | 0.1 - | 18 22 | -1.2 | -0,1 | 60 | 1 | 17:32:26 |
| 9614 | 4259.081 * | 0 | 5 15 | -1.2 | -0.1 | 60 | 1 | 17:50:52 |
| 9615 | 4249.513 * | 0.1 | -8 8 | -1.2 | -0.1 | 60 | 1 | 18:01:34 |
| -271 | 4265.875 * | 0.2 - | 22 -4 | -1.1 | -0.1 | 60 | 1 | 18:38:02 |
| SCINTREX V5. | 0 AUTOG | RAV / Fi | eld Mode Ser No: | 10: | R4. 345. | 4 | | |
| Line: 1025. G | arid: 0. Jol | x 1. I | Date: 97/ | 10/25 | Ope | rator: | 777 | 7 . |
| GREF.: | 0. mGa | ls | Tilt x ser | sit.: | | 271.4 | | |
| GCAL.1: | 5861,733 | | Tilt y se | nsit.: | | 287.4 | | |
| GCAL.2: | 0. | De | g.Latitud | e: | | 49.5 | | |
| TEMPCO | -0.1355 | mGal/mk | ζ De | a.Lor | ngitud | e: | 11 | 5.7 |
| Drift const.: | 0.17 | G | MT Differ | ence: | - | 6.hr | | |
| Drift Correction | Start Time: 2 | 3:33:43 | Cal | after | x san | nples: | 1 | 12 |
| | Date: 97/07/15 | 5 0 | n-Line Ti | ilt Cor | recte | d = "*" | | |

1997 Doe Ray Property Gravity Survey

Observed Gravity Data Reduction and Calculations Instrumentation; Scintrex CG3 Gravity Meter No.10345

Surveyed by: Quadra Surveys, October 1997

Operator: Tam Mitchell

| | Meter | | | IH | | Drift | | | |
|---------|----------|----------|------|---------|-------|---------|--------------------|-----------|--------------------|
| | Reading | | | Corr. | | Corr. | Base | Observed | |
| Station | mGal | Time | Ħ | mGal | Drift | mGal | Shift | Gravity | Notes |
| 9706 | 4243.034 | 11:58:03 | 0.59 | 4243.22 | -0.01 | 4243.21 | 976479.11 | 980722.32 | 9706 |
| 9707 | 4257.736 | 12:06:17 | 0.53 | 4257.90 | -0.01 | 4257.89 | 976479.11 | 980737.00 | 9707 |
| 9708 | 4261.533 | 12:16:31 | 0.53 | 4261.70 | -0.01 | 4261.69 | 976479.11 | 980740.80 | 9708 |
| 9709 | 4266.116 | 12:22:53 | 0.57 | 4266.29 | -0.01 | 4266.28 | 976479.11 | 980745.39 | 9709 |
| 9710 | 4262.812 | 12:35:08 | 0.56 | 4262.98 | -0.01 | 4262.97 | 976479.11 | 980742.08 | 9710 |
| 9711 | 4256.938 | 12:40:35 | 0.53 | 4257.10 | -0.01 | 4257.09 | 976479.11 | 980736.20 | 9711 |
| 9712 | 4253.974 | 12:51:50 | 0.54 | 4254.14 | -0.02 | 4254.13 | 976479.11 | 980733.24 | 9712 |
| 9713 | 4255.198 | 12:58:52 | 0.51 | 4255.36 | -0.02 | 4255.34 | 976479.11 | 980734.45 | 9713 |
| 9714 | 4270.058 | 13:12:44 | 0.57 | 4270.23 | -0.02 | 4270.22 | 976479.11 | 980749.33 | 9714 |
| 9715 | 4264.878 | 13:17:43 | 0.58 | 4265.06 | -0.02 | 4265.04 | 976479.11 | 980744.15 | 9715 |
| 9716 | 4267.471 | 13:23:08 | 0.57 | 4267.65 | -0.02 | 4267.63 | 976479.11 | 980746.74 | 9716 |
| 9717 | 4251.757 | 13:33:22 | 0.57 | 4251.93 | -0.02 | 4251.91 | 976479.11 | 980731.02 | 9717 |
| 9718 | 4232.932 | 13:44:58 | 0.57 | 4233.11 | -0.02 | 4233.08 | 976479.11 | 980712.19 | 9718 |
| 9719 | 4225.154 | 13:51:51 | 0.57 | 4225.33 | -0.03 | 4225.30 | 976479.11 | 980704.41 | 9719 |
| 9720 | 4227.707 | 13:56:26 | 0.53 | 4227.87 | -0.03 | 4227.84 | 976479.11 | 980706.95 | 9720 |
| 9721 | 4217.318 | 14:09:18 | 0.58 | 4217.50 | -0.03 | 4217.47 | 976479.11 | 980696.58 | 9721 |
| 9722 | 4216.303 | 14:22:09 | 0.57 | 4216.48 | -0.03 | 4216.45 | 976479.11 | 980695.56 | 9722 |
| 9723 | 4214.228 | 14:27:30 | 0.54 | 4214.39 | -0.03 | 4214.36 | 9 764 79.11 | 980693.47 | 9723 |
| 9724 | 4212.791 | 14:43:25 | 0.56 | 4212.96 | -0.03 | 4212.93 | 976479.11 | 980692.04 | 9724 |
| 9725 | 4255.453 | 15:32:43 | 0.58 | 4255.63 | -0.04 | 4255.59 | 976479.11 | 980734.70 | 9725 |
| 9726 | 4268.603 | 15:47:58 | 0.55 | 4268.77 | -0.04 | 4268.73 | 976479.11 | 980747.84 | 9726 |
| 9727 | 4260.37 | 15:54:54 | 0.57 | 4260.55 | -0.05 | 4260.50 | 976479.11 | 980739.61 | 9727 |
| 9728 | 4260.748 | 16:00:05 | 0.5 | 4260.90 | -0.05 | 4260.86 | 976479.11 | 980739.97 | 9728 |
| 9729 | 4269.838 | 16:06:03 | 0.56 | 4270.01 | -0.05 | 4269.96 | 976479.11 | 980749.07 | 9729 |
| 9730 | 4271.953 | 16:11:03 | 0.58 | 4272.13 | -0.05 | 4272.08 | 976479.11 | 980751.19 | 9730 |
| 9731 | 4250.701 | 16:45:38 | 0.57 | 4250.88 | -0.05 | 4250.82 | 976479.11 | 980729.93 | 9731 |
| 9732 | 4260.698 | 16:50:53 | 0.56 | 4260.87 | -0.06 | 4260.82 | 976479.11 | 980739.93 | 9732 |
| -271 | 4265.936 | 17:19:54 | 0.5 | 4266.09 | -0.06 | 4266.03 | 976479.11 | 980745.14 | -271 |
| -101 | 4208.857 | 20:55:52 | 0.54 | 4209.02 | 0.00 | 4209.02 | 976479.11 | 980688.13 | -101 Loop Tie 0.06 |

1997 Doe Ray Property Gravity Survey

Observed Gravity Data Reduction and Calculations Instrumentation; Scintrex CG3 Gravity Meter No.10345

Surveyed by: Quadra Surveys, October 1997

Operator: Tam Mitchell

| | Meter | | | IH | | Drift | | | | |
|---------|----------|----------|------|---------|-------|---------|-----------|-----------|-------|----------------|
| | Reading | | | Corr. | | Corr. | Base | Observed | | |
| Station | mGal | Time | IH | mGal | Drift | mGal | Shift | Gravity | Notes | |
| | | | | | -0.38 | | | | | |
| -101 | 4208 877 | 9.08.09 | 0.54 | 4209.04 | 0.00 | 4209 04 | 976479 09 | 980688 13 | -101 | |
| -101 | 4265 799 | 14-09-47 | 0.54 | 4265.04 | 0.00 | 4266.05 | 976479.09 | 980745 14 | -271 | |
| 9601 | 4254 22 | 14.00.47 | 0.56 | 4254 39 | 0.06 | 4254 45 | 976479.09 | 980733.54 | 9601 | |
| 9602 | 4238 595 | 15.13.27 | 0.59 | 4238 78 | 0.05 | 4238 83 | 976479.09 | 980717.92 | 9602 | |
| 9603 | 4261 668 | 15:36:51 | 0.57 | 4261.84 | 0.05 | 4261.89 | 976479.09 | 980740.98 | 9603 | |
| 9604 | 4260.425 | 15:56:33 | 0.53 | 4260.59 | 0.04 | 4260.63 | 976479.09 | 980739.72 | 9604 | |
| 9605 | 4260,477 | 16:08:11 | 0.57 | 4260.65 | 0.04 | 4260.69 | 976479.09 | 980739.78 | 9605 | |
| 9606 | 4262.845 | 16:11:51 | 0,53 | 4263.01 | 0.04 | 4263.05 | 976479.09 | 980742.14 | 9606 | |
| 9607 | 4258,142 | 16;18;46 | 0.58 | 4258.32 | 0.04 | 4258.36 | 976479.09 | 980737.45 | 9607 | |
| 9608 | 4253.203 | 16:25:57 | 0.55 | 4253.37 | 0.03 | 4253.41 | 976479.09 | 980732.50 | 9608 | |
| 9609 | 4246.109 | 16:38:38 | 0.56 | 4246.28 | 0.03 | 4246.31 | 976479.09 | 980725.40 | 9609 | |
| 9610 | 4245.136 | 16:47:49 | 0.58 | 4245.31 | 0.03 | 4245.34 | 976479.09 | 980724.43 | 9610 | |
| 9611 | 4264.696 | 17:02:52 | 0.58 | 4264.87 | 0.02 | 4264.90 | 976479.09 | 980743.99 | 9611 | |
| 9612 | 4232.535 | 17:17:48 | 0.56 | 4232.71 | 0.02 | 4232.73 | 976479.09 | 980711.82 | 9612 | |
| 9613 | 4243.073 | 17:32:26 | 0.53 | 4243.24 | 0.02 | 4243.25 | 976479.09 | 980722.34 | 9613 | |
| 9614 | 4259.081 | 17:50:52 | 0.55 | 4259,25 | 0.01 | 4259,26 | 976479.09 | 980738.35 | 9614 | |
| 9615 | 4249.513 | 18:01:34 | 0.5 | 4249.67 | 0.01 | 4249.68 | 976479.09 | 980728.77 | 9615 | |
| -271 | 4265.875 | 18:38:02 | 0.57 | 4266.05 | 0.00 | 4266.05 | 976479.09 | 980745.14 | -271 | Loop Tie -0.07 |
| | | | | | | | | | | |
| 674 | 1005 050 | | 0.57 | (000 00 | -0.24 | 1000.00 | 07047044 | 00074644 | 0.74 | |
| -271 | 4265.856 | 11:21:54 | 0,57 | 4266.03 | 0.00 | 4266.03 | 9/64/9.11 | 980/45.14 | -2/1 | |
| 9701 | 4268,526 | 11:28:56 | 0.5 | 4268.71 | 0.00 | 4268.71 | 9/64/9.11 | 980/47.82 | 9701 | |
| 9/02 | 4269.598 | 11:34:12 | 0.57 | 4269.77 | 0.00 | 4269.77 | 9/64/9.11 | 980/48.88 | 9702 | |
| 9703 | 4266.645 | 11:39:59 | 0.58 | 4266.82 | 0.00 | 4200.82 | 9/64/9.11 | 980/45.93 | 9703 | |
| 9704 | 4262.354 | 11:46:05 | 0.59 | 4262.54 | 0.00 | 4262.53 | 9/64/9.11 | 980/41.64 | 9/04 | |
| 9705 | 4253.867 | 11:52:16 | 0,58 | 4254.05 | -0.01 | 4254.04 | 9/64/9.11 | 980733.15 | 9705 | |

.....

1997 Doe Ray Property Gravity Survey

Inner Zone Terrain Corrections Surveyed by Quadra Surveys

| | Inc | line | ome | ete | r R | ea | ding | gs i | n C |)eg | j to |) Te | erra | lin ' | Cor | rec | tior | Zc | Zo | ne-B | | | Zon | e-C | | | | | Zon | e-D | | | | | B, C, & D | |
|------|------------|-----------|------|-----|-----|------|------|------|-----|------|------------|------|------------|-------|-----|-----|------|----|-------|------|------------|------|------|------|------|------|------|------|------|------|------|------|------|------|-----------|------|
| Stn | B 1 | B2 | B3 | B4 | 4 C | :1 (| C2 | Ċ3 | C4 | C5 | 5 C | 6 C |) 1 | D2 | D3 | D4 | D5 | D6 | 81 | B2 | B 3 | B4 | C1 | C2 | C3 | C4 | C5 | C6 | D1 | D2 | D3 | D4 | D5 | D6 | Ter Cor | Stn |
| 9716 | 0 | 0 | 0 |) (| 0 | 0 | 11 | 12 | 0 | 10 | 0 1 | 0 | 0 | 11 | 12 | 0 | 7 | 7 | .000 | .000 | .000 | .000 | .000 | .017 | .020 | .000 | .014 | .014 | .000 | .054 | .063 | .000 | .022 | .022 | 0.23 | 9716 |
| 9717 | 0 | 0 |) 11 | 10 | D | Û | 12 | 10 | 0 | 10 | 0 1 | 0 | 0 | 10 | 7 | 0 | 10 | 7 | .000 | .000 | .017 | .014 | .000 | .020 | .014 | .000 | .014 | .014 | .000 | .044 | .022 | .000 | .044 | .022 | 0.23 | 9717 |
| 9718 | 0 | 12 | 2 0 | 11 | 0 | 0 | 12 | 17 | 0 | 10 |) | 9 | 0 | 17 | 17 | 0 | 10 | 9 | ,000, | .020 | .000 | .014 | .000 | .020 | .039 | .000 | .014 | .011 | .000 | .123 | .123 | .000 | .044 | .036 | 0.44 | 9718 |
| 9719 | 0 | 0 |) () |) (| 0 | 0 | 10 | 10 | 0 | 3 | 3 | 6 | 0 | 14 | 13 | 0 | 7 | 6 | .000 | .000 | .000 | .000 | .000 | .014 | .014 | .000 | .001 | .005 | .000 | .085 | .074 | .000 | ,022 | ,016 | 0.23 | 9719 |
| 9720 | 0 | 0 |) (|) (| 0 | 0 | 10 | 9 | 0 | - 6 | 5 | 5 | 0 | 10 | 9 | 0 | 7 | 7 | .000 | .000 | .000 | .000 | .000 | .014 | .011 | ,000 | .004 | .004 | .000 | .044 | .036 | .000 | .022 | .022 | 0.16 | 9720 |
| 9721 | 0 | 12 | 2 8 | 3 | 7 | 0 | 10 | Ö | 0 | 5 | 5 | 7 | 0 | 10 | 7 | 7 | 0 | 0 | .000 | ,020 | .009 | .007 | .000 | .014 | .000 | .000 | .004 | .007 | .000 | .044 | .022 | .022 | .000 | .000 | 0.15 | 9721 |
| 9722 | 22 | 10 |) (|) (| 02 | 20 | 17 | 0 | 18 | 17 | 7 | 0 | 14 | 15 | 0 | 18 | 18 | 0 | .052 | .014 | .000 | .000 | .052 | .039 | .000 | .043 | .039 | ,000 | .085 | .097 | .000 | .137 | .137 | .000 | 0.70 | 9722 |
| 9723 | 0 | 8 | 3 0 |) 1 | 7 | 0 | 6 | 4 | 0 | 1: | 3 1 | 3 | 0 | 8 | 7 | 0 | 13 | 13 | .000 | .009 | .000 | .035 | .000 | .005 | .002 | .000 | .023 | .023 | .000 | .029 | .022 | .000 | .074 | .074 | 0.30 | 9723 |
| 9724 | 0 | -14 | 0 |) (| 0 | 0 | 10 | 10 | 0 | (| D | 0 | 0 | 13 | 13 | 0 | 0 | 0 | .000 | .025 | .000 | .000 | .000 | .014 | .014 | .000 | .000 | .000 | .000 | .074 | .074 | .000 | .000 | .000 | 0.20 | 9724 |
| 9725 | 7 | C |) (|) | 01 | 0 | 10 | 0 | 0 | (| 0 | 0 | 0 | 15 | 12 | 0 | 5 | 5 | .007 | .000 | .000 | .000 | .014 | .014 | .000 | ,000 | .000 | .000 | .000 | .097 | .063 | .000 | .011 | .011 | 0.22 | 9725 |
| 9726 | 0 | 10 |) (|) | 7 | 0 | 9 | 9 | 0 | 1 | 8 | 8 | 0 | 13 | 12 | 0 | 7 | 7 | .000 | .014 | .000 | .007 | .000 | .011 | .011 | .000 | .009 | .009 | .000 | .074 | .063 | .000 | .022 | .022 | 0.24 | 9726 |
| 9727 | 0 | 10 |) (|) | 7 | 0 | 13 | 13 | 0 | 10 | D 1 | 0 | 0 | 12 | 12 | 0 | 12 | 12 | .000 | .014 | .000 | .007 | .000 | .023 | .023 | .000 | .014 | .014 | .000 | .063 | .063 | .000 | .063 | .063 | 0.35 | 9727 |
| 9728 | 0 | Ç |) (| 2 | 0 | 0 | 8 | 9 | 0 | 18 | 8 1 | 8 | 0 | 8 | 8 | 0 | 18 | 18 | .000 | .000 | .000 | .045 | .000 | .009 | .011 | .000 | .043 | .043 | .000 | .029 | .029 | .000 | .137 | .137 | 0.48 | 9728 |
| 9729 | 0 | C |) (|) | 0 | 0 | 6 | 6 | 0 | E t | 5 | 0 | 0 | 6 | 6 | 0 | 5 | 5 | .000 | .000 | .000 | .000 | .000 | .005 | .005 | .000 | ,004 | .000 | .000 | .016 | .016 | .000 | .011 | .011 | 0.07 | 9729 |
| 9730 | 0 | -20 |) (|) 1 | 3 | 0 | 17 | 17 | 0 | 23 | 3 2 | 20 | 0 | 10 | 10 | 0 | 17 | 17 | .000 | .045 | .000 | .022 | .000 | .039 | .039 | .000 | .068 | .052 | .000 | .044 | .044 | .000 | .123 | .123 | 0.60 | 9730 |
| 9731 | 0 | 5 | 5 C |) 1 | 5 | 0 | 10 | 15 | 0 |) 7 | 7 | 5 | 0 | 7 | 12 | 0 | - 7 | -7 | .000 | .004 | .000 | .028 | .000 | .014 | .031 | .000 | .007 | .004 | .000 | .022 | .063 | .000 | .022 | .022 | 0.22 | 9731 |
| 9732 | 0 | - 3 | 3 (|) | 0 | 0 | 14 | 10 | 0 |) 1(| 0 1 | 10 | 0 | 10 | 7 | 0 | 10 | 10 | .000 | .001 | .000 | .000 | .000 | .027 | .014 | .000 | .014 | .014 | .000 | .044 | .022 | .000 | ,044 | .044 | 0.23 | 9732 |

1997 Doe Ray Property Gravity Survey

Inner Zone Terrain Corrections Surveyed by Quadra Surveys

| | Inci | lino | mete | ər R | lead | ing | Is ir | ۱De | ag t | o Te | erra | in (| Cori | rect | lion | Zc | Zoi | ne-B | | | Zon | e-C | | | | | Zon | e-D | | | | | B, C, & D | |
|------|----------|------|------|------|------|--------------|-------|------|------|------|------|------|------|------|------|----|---------------|-----------|------------|-----------|------|------|------|----------------|------|------|------|------|------|------|------|-------|-----------|------------------|
| Stn | B1 | B2 | 83 E | 34 (| 21 C | 2 Ĉ | 3 (| 24 (| 25 (| C6 [| D1 E |)2 I | D3 | D4 1 | D5 | D6 | B1 | B2 | B 3 | B4 | C1 | Č2 | C3 | C4 | C5 | C6 | D1 | D2 | D3 | D4 | D5 | D6 | Ter Cor | Stn |
| -271 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | θ | 0 | 0 | 000. | 000 | .000 | .000 | .000 | .000 | .000 | 000. | .000 | .000 | .000 | .000 | .000 | .000 | 000 | 000 | 0.00 | -271 |
| 9601 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 8 | 0 | . 0 00 | 000. | .000 | 000. | .000 | .000 | 000 | .000 | .000 | .000 | .000 | .000 | .000 | .029 | .029 | .000 | 0.06 | 9 601 |
| 9602 | 0 | 0 | 0 | 0 | 0 | Ò | 0 | 0 | Ö | 0 | 0 | 0 | 0 | 15 | 15 | 0 | .000 | ,000, | .000 | 000. | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .097 | .097 | .000 | 0.19 | 9602 |
| 9603 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 7 | 5 | 5 | 0 | 7 | 7 | 0 | 0 | 0 | .000 | .000 | .000 | .000 | .000 | .000 | .007 | .007 | .004 | .004 | .000 | .022 | .022 | .000 | .000 | .000 | 0.07 | 9603 |
| 9604 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 6 | 0 | 0 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .011 | .016 | .000 | .000 | 0.03 | 9604 |
| 9605 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 7 | 0 | 0 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .074 | .022 | .000 | .000 | 0.10 | 9605 |
| 9606 | 0 | 0 | 0 1 | 12 | 0 | 5 ° | 10 | 0 | 7 | 7 | 0 | 0 | 17 | 12 | 0 | 0 | 000. | .000 | .000 | .020 | .000 | .004 | .014 | , 0 00, | .007 | .007 | .000 | .000 | .123 | .063 | .000 | .000 | 0.24 | 9606 |
| 9607 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Ò | 5 | 5 | 0 | 0 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .011 | .011 | .000 | ,000, | 0.02 | 9607 |
| 9608 | 5 | 6 | 5 | 5 | 0 | 5 | 5 | 0 | 14 | 14 | 0 | 8 | 8 | 0 | 14 | 14 | .004 | .006 | .004 | .004 | .000 | .004 | .004 | .000 | .027 | .027 | .000 | .029 | .029 | .000 | .085 | .085 | 0.31 | 9608 |
| 9609 | 0 | 10 | 0 2 | 26 | 0 1 | 3 | 17 | 0 | 17 | 20 | 0 | 13 | 15 | 0 | 17 | 20 | .000 | .014 | .000 | .066 | .000 | .023 | .039 | .000 | .039 | .052 | .000 | .074 | .097 | .000 | .123 | .167 | 0.69 | 9609 |
| 9610 | 0 | 5 | 0 | 3 | 0 | 9 | 10 | 0 | 8 | 8 | 0 | 9 | 10 | 0 | 8 | 8 | .000 | .004 | .000 | .001 | .000 | .011 | 014 | .000 | .009 | .009 | .000 | .036 | .044 | .000 | .029 | .029 | 0.19 | 9610 |
| 9611 | 0 | 17 | 0 | 7 | 0 1 | 9 | 18 | 0 | 9 | 9 | 0 | 15 | 15 | 0 | 7 | 7 | .000 | .035 | .000 | .007 | .000 | .048 | .043 | .000 | 011 | .011 | .000 | .097 | .097 | .000 | .022 | .022 | 0.39 | 9611 |
| 9612 | 0 | 10 | 0 ' | 10 | 0 1 | 0 | 10 | 0 | 8 | 8 | 0 | 10 | 10 | 0 | 8 | 8 | .000 | .014 | .000 | .014 | .000 | .014 | .014 | .000 | .009 | .009 | .000 | .044 | .044 | .000 | .029 | .029 | 0.22 | 9612 |
| 9613 | 0 | 33 | 0 | 8 | 03 | 30 : | 30 | 0 | 5 | 7 | 0 | 15 | 15 | 0 | 7 | 10 | .000 | .093 | .000 | .009 | .000 | .109 | .109 | .000 | .004 | .007 | .000 | .097 | .097 | .000 | .022 | .044 | 0.59 | 9613 |
| 9614 | 0 | 6 | 5 | 0 | 0 1 | i 0 - | 13 | 0 | 10 | 10 | 10 | 13 | 0 | 10 | 10 | 0 | .000. | ,006 | .004 | .000 | .000 | .014 | .023 | .000 | .014 | .014 | .044 | .074 | .000 | 044 | .044 | .000 | 0.28 | 9614 |
| 9615 | 0 | 15 | 0 2 | 27 | 0 1 | 13 | 10 | 0 | 17 | 17 | 0 | 13 | 10 | 0 | 17 | 17 | .000 | .028 | .000 | .070 | .000 | .023 | .014 | .000 | .039 | .039 | .000 | .074 | .044 | .000 | .123 | .123 | 0.58 | 9615 |
| 9701 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | 0.00 | 9701 |
| 9702 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | ,000 | ,000 | .000 | .000 | .000 | .000 | .000 | .000 | 0.00 | 9702 |
| 9703 | 0 | 7 | 0 | 5 | 0 | 7 | 7 | Q | 8 | 5 | 0 | 0 | 0 | 12 | 7 | 0 | .000 | .007 | .000 | .004 | .000 | .007 | .007 | .000 | .009 | .004 | .000 | .000 | .000 | .063 | .022 | .000 | 0.12 | 9703 |
| 9704 | 0 | 7 | 0 | 5 | 0 | 7 | 7 | 0 | 5 | 5 | 0 | 7 | 5 | 0 | 5 | 5 | .000 | .007 | .000 | .004 | .000 | .007 | .007 | .000 | .004 | .004 | .000 | .022 | .011 | .000 | .011 | .011 | 0.09 | 9704 |
| 9705 | 0 | 0 | 0 | 0 | 0 ′ | 12 | 14 | 0 | 0 | 0 | 0 | 13 | 15 | 0 | 0 | 0 | .000 | .000 | .000 | .000 | .000 | .020 | .027 | ,000, | .000 | .000 | .000 | .074 | .097 | .000 | .000 | .000 | 0.22 | 9705 |
| 9706 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 8 | 0 | 0 | .000 | .000 | 000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .029 | .029 | .000 | .000 | 0.06 | 9706 |
| 9707 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | 0.00 | 9707 |
| 9708 | 0 | 0 | 0 | 0 | 0 | 5 | 5 | 5 | 5 | 0 | 0 | 5 | 5 | 5 | 5 | 0 | .000 | .000 | .000 | .000 | .000 | .004 | .004 | .004 | .004 | ,000 | .000 | .011 | .011 | .011 | .011 | .000 | 0.06 | 9708 |
| 9709 | 0 (| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 5 | 5 | 0 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .011 | .011 | .011 | .000 | 0.03 | 9709 |
| 9710 | 0 (| 0 | 0 | 0 | 0 | 17 | 15 | 0 | 25 | 25 | 0 | 25 | 22 | 0 | 10 | 10 | .000 | .000 | .000 | .000 | .000 | .039 | 031 | .000 | .079 | .079 | .000 | .250 | .199 | .000 | .044 | .044 | 0.76 | 9710 |
| 9711 | 0 | 33 | 0 | 0 | 0 | 17 | 17 | 0 | 27 | 27 | 0 | 20 | 22 | 0 | 17 | 17 | .000 | .093 | .000 | .000 | .000 | .039 | .039 | .000 | .090 | .090 | .000 | .167 | .199 | .000 | .123 | .123 | 0.96 | 9711 |
| 9712 | 2 0 | 10 | 0 | 25 | Q ' | 19 | 18 | 0 | 20 | 20 | 0 | 13 | 13 | 0 | 7 | 7 | .000 | .014 | .000 | .062 | .000 | .048 | .043 | .000 | .052 | .052 | .000 | .074 | .074 | .000 | .022 | .022 | 0.46 | 9712 |
| 971: | 0 | 30 | 0 | 10 | 0 | 13 | 13 | 0 | 10 | 7 | 0 | 6 | 6 | 0 | 13 | 13 | .000 | .081 | .000 | .014 | .000 | .023 | .023 | .000 | .014 | .007 | .000 | .016 | .016 | .000 | .074 | .074 | 0.34 | 9713 |
| 9714 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 20 | 0 | 0 | 0 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .215 | .167 | .000 | .000 | .000 | 0.38 | 9714 |
| 971 | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 10 | 10 | -5 | 0 | 0 | .000 | ,000, | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .022 | .044 | .044 | .011 | .000 | .000 | 0.12 | 9715 |

APPENDIX III

Partial Bouguer Anomaly Plan Map





DOE RAY PROJECT



5.0 CONCLUSIONS AND RECOMMENDATIONS

Soil samples that were submitted for geochem analysis show areas of very anomalous Pb and Zn. Gravity results show a large anomalous area that underlies the northern half of the Crawford Bay Peninsula as well as a secondary anomaly north of the highway. Other soil samples collected should also be run for 32 element geochem.

Follow-up prospecting with rock sampling should be done over all anomalous area as well as geological mapping.

6.0 STATEMENT OF QUALIFICATIONS

This is to certify that I, Glen M. Rodgers, P.Eng.;

-am a graduate of the University of Manitoba with a Bsc. in Geological Engineering (1977).

-am a member in good standing of the British Columbia Association of Professional Engineers and Geoscientists (P.Eng.).

-have practiced my profession over the last 22 years working as a geologist and engineer in B.C., Yukon, NWT., Alaska and Central America.

-base this report on first hand experience on the Doe-Ray property and do not expect to receive any shares of Klondike Gold Corp. as a result of writing this report.



Statement of Costs

| | \$ 100.\$ 500.\$ 240. |
|-------------|---|
| • | \$ 100.\$ 500. |
| • | \$ 100. |
| | |
| . <u>.</u> | \$ 220. |
| s @ \$10.ea | \$ 1,4 50. |
| | \$ 1,450. |
| | |
| · · | \$ 3,350. |
| | s @ \$10.ea |

-certified as a true estimate of costs incurred,

÷.



(39)

Intertek Testing Services Bondar Clegg

.

Geochemical Lab Report

| CLIENT: REPORT: | KENNECOTT CANADA V98-00051.0 (COM | INC IPI E | TE) | | | | | | | | | | | | | | DA | TER | ECEI | VED : | 12 | JAN-98 | 3 | DATE | PRIN | TED: | 19-J/ | AN-98 | F | PAGE | F 1 (| PRÓJ DF 5 | ECT: | CRAWFORD BA |
|--------------------|---------------------------------------|-------------------|-----------------|-----------|-----------|-----------|-------------|-----------|-------------|-----------|----------------|-----------|------------|------------------|-----------|-------------|----------|-----------|------------|-----------|-----------|-----------|-----------|-----------|----------|-----------|------------|-------------|------------|-------------|---------------|--------------|------------|-------------|
| SAMPLE NUMBER | ELEMENT Ag UNITS PPM | Cu PP M | i Pida I PPM | Zn PPM | Mo PPM | Ni PPM | Co PPM | Cd PPM | Bi PPM (| As PPM | s6 PPM | Fe PCT | Mrs PPM | Te PPM | Ba PPM | Cr PPM F | V PPM | Sn PPM | W PPM I | La PPM | AL PCT | Mg PCT | Ca PCT | Na PCT | K PCT | Sr PPM | Y PPM I | Ga PPM P | Lİ PM F | Nd PPM I | Sc PPM (| ta PPM | T i PCT | Zr PPM |
| IB OW | <.2 | 35 | 197 | 676 | 1 | 40 | 11 | 1.0 | <5 | 53 | <5 | 2.73 | 454 | <10 | 94 | 34 | 40 | <20 | <20 | 10 | 2.92 | 0.61 | 0.36 | 0.02 | 0.10 | 13 | 4 | 2 | 27 | 6 | -5 | <10 | 0.14 | 9 |
| 18 504 | 0.9 | 21 | 80 | 532 | <1 | 39 | 13 | 0.8 | <5 | 17 | 4 5 | 2.28 | 341 | <10 | 101 | 21 | 36 | <20 | <20 | 6 | 4.31 | 0.33 | 0,18 | 0,03 | 0,08 | 12 | 3 | 3 | 35 | 7 | <5 · | <10 | 0.18 | 35 |
| LB 100W | <.2 | 31 | 77 | 221 | <1 | 34 | 12 | <.2 | <5 | 10 | <5 | 2.58 | 254 | <10 | 154 | 30 | 42 | <20 | <20 | 10 | 3.00 | 0.68 | 0.28 | 0.02 | 0.13 | 15 | 4 | 3 | 35 | 5 | <5 | <10 | 0.16 | 12 |
| 18 150W | <.2 | 11 | 37 | 253 | <1 | 11 | 9 | 0.5 | <5 | 6 | <5 | 2.05 | 2336 | <10 | 357 | 14 | 35 | <20 | <20 | 9 | 2.03 | 0.34 | 0.36 | 0.02 | 0.1Z | 50 | 3 | 6 | 25 | 4 | <5 | <10 | 0.12 | <1 |
| LB 2004 | <.2 | 22 | 2 50 | 276 | <1 | 57 | 12 | 0.3 | <5 | 10 | <5 | 2.60 | 445 | <10 | 185 | 2 9 | 43 | <20 | <20 | 10 | 3.46 | 0.62 | 0,22 | 0.02 | 0.11 | 12 | 4 | 4 | 34 | 6 | <5 · | <10 | 0.18 | 17 |
| LB 250W | 0,3 | 25 | 79 | 177 | <1 | 60 | 13 | <.2 | <5 | 9 | ~ 5 | 2.81 | 399 | <10 | 184 | 28 | 46 | <20 | <20 | 14 | 3.07 | 0.50 | 0.24 | 0.03 | 0.12 | 14 | 9 | 5 | 44 | 6 | <5 | <10 | 0.22 | 12 |
| LB 300W | 0.3 | 27 | 7 27 | 270 | <1 | 41 | 13 | <.2 | <5 | 7 | 45 | 3.19 | 472 | <10 | 274 | 26 | 54 | <20 | <20 | 6 | 4.22 | 1.13 | 0.28 | 0.03 | 0.11 | 16 | 4 | - 6 | 41 | 6 | ્ર્ડ | <10 | 0.22 | 12 |
| 18 350W | ۰.× | 44 | 96 | 207 | <1 | 37 | 11 | <.2 | <5 | 16 | <5 | 2.44 | 286 | <10 | 110 | 35 | 37 | <20 | <20 | 17 | 2.29 | 0.69 | 0.32 | 0.02 | 0.11 | 22 | - 7 | <2 | 33 | 5 | <5 | <10, | 0.12 | 5 |
| LB 400M | 0.3 | 18 | 3 42 | \$35 | <1 | 26 | 10 | 1.0 | \$ 5 | 13 | <5 | 2.20 | 847 | <10 | 212 | 25 | 31 | <20 | <20 | 12 | 3.21 | 0.45 | 0.29 | 0.03 | 0.10 | 18 | 5 | 4 | 29 | 4 | <5 | <10 | 0.14 | 9 |
| LB 450W | 0.3 | 11 | i 51 | 575 | <1 | 34 | 11 | 0.4 | <5 | 8 | <5 | 2.47 | 917 | <10 | 259 | 22 | 36 | <20 | <20 | 14 | 3.59 | 0.36 | 0.15 | 0.03 | 0.10 |) 16 | 5 | 3 | 29 | 5 | <5 | <10 | 0.17 | 18 |
| 18 500W | 0.3 | 15 | 7 66 | 277 | <1 | 26 | 10 | 0.3 | \$ | 11 | <5 | 2.43 | 324 | <10 | 139 | 17 | 36 | <20 | <20 | 9 | 4.71 | 0.30 | 0,10 | 0.02 | 0.08 | 39 | 5 | 5 | 24 | 7 | <5 | <10 | 0.17 | 37 |
| 1.8 550M | i <.2 | 1 | 3 67 | 247 | <1 | 55 | 11 | 0.3 | <5 | 9 | <5 | 2.30 | 821 | < 1 0 | 266 | 28 | 35 | <20 | <20 | 12 | 2.98 | 0.43 | 0,20 | 0.02 | 0.10 |) 17 | 5 | 3 | 27 | 4 | -5 | <10 | 0.14 | 13 |
| LB 600W | ، ×.2 | 50 | 0 87 | 283 | <1 | 51 | 12 | <.2 | <5 | 20 | <5 | 2.74 | 364 | <10 | 117 | 35 | 41 | <20 | <20 | 15 | 2.62 | 0.73 | 0.22 | 0.01 | 0.13 | 5 15 | 4 | 2 | 33 | 4 | < 5 | <10 | 0.10 | 7 |
| LB 650W | ×.2 (| 20 | 0 56 | 164 | <1 | 17 | 8 | <.2 | <5 | 17 | 5 | 2.94 | 1741 | <10 | 302 | 16 | 39 | <20 | <20 | 13 | 2.80 | 0.32 | 0.17 | 0.02 | 0.12 | 23 | 6 | 6 | 28 | 5 | <5 | <10 | 0.10 | 3 |
| LB 700W | .> ۲ | 29 | 9 59 | 178 | <1 | 40 | 11 | 0.3 | -5 | 9 | <5 | 2.42 | 252 | <10 | 170 | 22 | 38 | <20 | <20 | 31 | 4.96 | 0.41 | 0.23 | 0.04 | 0,10 |) 22 | 28 | 5 | 29 | 6 | 9 | <10 | 0.20 | 72 |
| .B 750₩ | د.2 | 1 | 1 38 | 294 | <1 | 24 | - 11 | 0.5 | <5 | 15 | <5 | 2.62 | 924 | <10 | 242 | 22 | 37 | <20 | <20 | 10 | 3.03 | 0.43 | 0.22 | 0.02 | 0.10 |) 19 | , 3 | 5 | 35 | 5 | <5 | <10 | 0,17 | 8 |
| .B 800w | i <.2 | 1 | 1 178 | 292 | <1 | 24 | 12 | <،2 | <5 | 6 | <5 | 2.51 | 1516 | <10 | 281 | 19 | 38 | <20 | <20 | 10 | 3.21 | 0.26 | 0.27 | 0.02 | 0.0 | 34 | 3 | 4 | 25 | 6 | <5 | <10 | 0.17 | 11 |
| .B 850W | ، <.2 | 13 | 2 27 | 171 | <1 | 22 | 8 | <.2 | <5 | 6 | < 5 | 2.30 | 1071 | <10 | 192 | 22 | 34 | <20 | <20 | 13 | 2.19 | 0.42 | 0.24 | 0.02 | 0.09 | 23 | 4 | 3 | 26 | 5 | <5 | <10 | 0.12 | 3 |
| .B 900in | J 0.4 | 1 | 5 30 | 266 | <1 | 38 | 10 | 0.3 | <5 | 7 | <5 | 2.04 | 449 | <10 | 208 | 19 | 33 | <20 | <20 | 11 | 3.17 | 0.32 | 0.23 | 6 0.03 | 6 0.10 | 21 | 5 | 3 | 25 | 4 | <5 | <10 | 0,17 | 22 |
| -B 50E | 2.0 | 7 | 6 302 | 1142 | 2 | 92 | 14 | 2.1 | <5 | 43 | ر ې | 3.25 | 566 | <10 | 151 | 51 | 51 | <20 | <20 | 22 | 3.68 | 8 0.73 | 0.49 | 0.03 | 0.13 | 3 22 | 31 | <2 | 145 | 5 | 6 | <10 | 0,17 | 20 |
| . 8 1008 | E 0.7 | 3 | 5 243 | 751 | <1 | 33 | 11 | 1.1 | <5 | 44 | <5 | 2.65 | 223 | <10 | 196 | 28 | 40 | <20 | <20 | 14 | 2.90 | 0.58 | 0.23 | 5 0.02 | 2 0.13 | 5 15 | 7 | 2 | 31 | 3 | <5 | <10 | 0.13 | 22 |
| . B 150E | E 0.6 | 1 | 9 176 | 670 | <1 | 31 | 11 | 2.3 | <5 | 65 | <5 | 2.43 | 1387 | <10 | 177 | 18 | 34 | <20 | <20 | 8 | 4.32 | 2 0.37 | 0.17 | 0.03 | 0.0 | 9 12 | 4 | 3 | 27 | 5 | <5 | <10 | 0.16 | 13 |
| .B 2006 | = <.2 | 4 | 9 192 | 524 | <1 | 37 | 7 14 | 0.4 | -5 | 37 | <5 | 2.99 | 808 | <10 | 104 | 45 | 51 | <20 | <20 | 12 | 2.34 | 1.12 | 0.29 | 0.02 | 2 0.12 | 2 12 | 4 | ຸ 2 | 46 | 5 | <5 | <10 | 0.17 | 2 |
| 8 2506 | E 0.4 | 9 | 5 140 | 326 | s <1 | - 37 | r 17 | 1.1 | <5 | 30 | <5 | 2.67 | 1823 | <10 | 191 | 21 | 46 | <20 | <20 | 11 | 5,05 | 6 0.53 | 0.30 | 0.03 | \$ 0.0 | 5 19 | 10 | 5 | 31 | 5 | 6 | <10 | 0.21 | 32 |
| .B 300E | . 0. 3 | 1 | 7 175 | 583 | <1 | 41 | 11 | 1.0 | <5 | 27 | <5 | 2.52 | 878 | <10 | 234 | 29 | 37 | <20 | <20 | 11 | 2.94 | 0.63 | 0.29 | 9 0.02 | 2 0.14 | 6 17 | 4 | 2 | 34 | 4 | < 5 | <10 | 0.16 | 8 |
| .8 3506 | E 1.2 | : 1 | 5 281 | 952 | 2 <1 | 31 | 10 | 2.8 | <5 | 31 | <5 | 2.34 | 417 | ′ <10 | 192 | : 19 | 36 | <20 | <20 | 10 | 3.29 | 0,38 | 0.24 | 0.03 | 5 0.1 | 1 13 | 5 | 2 | 24 | 5 | <5 | <10 | 0.16 | 21 |
| в 400£ | E 0.3 | i 7 | 8 84 | 304 | <1 | 131 | 20 | 0.5 | <5 | 14 | <5 | 2.74 | 485 | <10 | 141 | 118 | 44 | <20 | <20 | 11 | 3.65 | 5 1.43 | 6 0.48 | 3 0.03 | 5 0.20 | 0 20 | 8 | 4 | 74 | 6 | <5 | <10 | 0.20 | 16 |
| B 4508 | E 0.2 | ! 1 | 5 28 | 713 | 5 1 | 43 | 5 16 | 1.0 | <5 | 9 | <5 | 2.49 | 157 | ' <1 0 | 73 | 41 | 42 | <20 | <20 | 9 | 3.07 | 7 1.12 | 0.41 | 0.03 | 5 0.04 | 6 15 | 5 | 3 | 74 | 9 | <5 | <10 | 0.26 | 8 |
| .B 5008 | E <,2 | ! 1 | 8 42 | 272 | 2 <1 | - 30 |) 13 | 0.8 | <5 | 12 | <5 | 2,86 | 218 | 3 <10 | 148 | 20 | 42 | <20 | <20 | 9 | 5.61 | 0.70 | 0.32 | 0.03 | 5 0.1 | 0 17 | 7 | 5 | 62 | 7 | <5 | <10 | 0.23 | 41 |
| B 5508 | E <.2 | 2 | 7 47 | 391 | <1 | 20 | 5 12 | 0.6 | \$ | 6 | <5 | 2.34 | 326 | 5 <10 | 199 | 23 | 36 | <20 | <20 | 8 | 3.10 | 1.08 | 3 0.32 | 2 0.03 | 5 0.1 | 0 17 | 6 | 4 | 66 | 5 | <5 | <10 | 0,18 | 20 |



Geochemical Lab Report

÷ i

| CLIENT: KEN | NECOTT CANADA INC. | | | | | | | PROJECT; CRAWFORD BAY |
|------------------|---------------------------------------|-------------------------|---|-------------------------------------|----------------------------------|--|--------------------------------------|--------------------------------|
| REPORT: V98 | 00051.0 (COMPLETE) | | | | DATE RECEIVED: 12 | 2-JAN-98 DATE PRINTED | : 19-JAN-98 PAGE | 2 OF 5 |
| SAMPLE NUMBER | ELEMENT Ag Cu PD UNITS PPM PPM PPM | Zn Mo Ni PPM PPM PPM | i Co Cci Bi As Sib 1 PPM PPM PPM PPM | Fe Mn Te Ba Cr PCT PPM PPM PPM F | V SN W La A PM PPM PPM PPM PC | AL Mg Ce Na K Si CT PCT PCT PCT PCT PPI | , r y Ga Li Nd A PPM PPM PPM I | Sc Ta Ti Zr PPM PPM PCT PPM |
| 10.4005 | 05 17 72 | 776 <1 20 | 1022 <5 16 <5 | 2 36 281 <10 177 13 | 35 <20 <20 8 3.8 | 98 0.21 0.22 0.03 0.07 1 | 3 5 5 20 5 | <5 <10 0.22 32 |
| | 2 30 151 | B34 <1 20 | 5 16 2.2 -5 16 -5 5 16 0 5 -5 26 -5 | 3 45 429 410 161 39 | 54 <20 <20 11 3 0 | | 1 4 4 44 6 | <5 <10 0.20 4 |
| | 0.6 50 182 | 716 <1 53 | 3 13 1 3 <5 20 <5 | 2 72 277 <10 146 19 | 40 <20 <20 10 4.7 | 76 0.33 0.24 0.04 0.09 1 | 6 10 3 46 7 | <5 <10 0.21 46 |
| | 0.0 0.02 | 327 <1 /9 | 2206 <5 15 <5 | 4 69 785 <10 245 52 | 89 <20 <20 9 3.4 | 46 2.21 0.57 0.03 0.36 2 | 0 11 2 53 6 | 6 <10 0.21 9 |
| | 0.2 00 110 | 255 ×1 47 | 2 12 0 9 45 17 45 | 2 23 435 <10 113 36 | 38 <20 <20 10 1 6 | 64 0.63 0.24 0.02 0.09 1 | 0 3 2 45 4 | <5 <10 0.13 2 |
| 18 0000 | < <u>,</u> 2 37 10 | | | | | | | |
| LB 850F | < 2 37 114 | 599 <1 41 | 1 16 1.6 <5 16 <5 | 3,24 1057 <10 232 41 | 60 <20 <20 13 1.7 | 74 0.93 0.77 0.02 0.16 2 | 6 8 2 40 4 | <5 <10 0.09 <1 |
| 18-900E | <.2 36 57 | 191 <1 36 | 6 13 <.2 <5 12 <5 | 2.63 207 <10 86 22 | 43 <20 <20 13 3.7 | 78 0.45 0.14 0.02 0.10 | 7 10 4 30 8 | |
| LB 950E | 0.3 25 20 | 151 1 31 | 1 16 <.2 <5 7 <5 | 3.93 440 <10 201 25 | 59 <20 <20 12 4.8 | 88 0.42 0.12 0.02 0.18 1 | 1 6 5 32 8 | 5 <10 0.24 30 |
| LC OW | <.2 47 21 | 493 <1 44 | 4 18 0.7 <5 5 <5 | 2.98 662 <10 352 31 | 41 <20 <20 7 3.2 | 28 1.11 0.49 0.02 0.23 2 | 234665 | <5 <10 0.17 4 |
| IC SOW | <.2 48 19 | 119 <1 35 | 5 14 0.4 <5 <5 <5 | 2,24 1933 <10 385 32 | 33 <20 <20 6 2.5 | 58 1.45 0.96 0.03 0.21 3 | 1 4 2 90 5 ` | <5 <10 0.15 1 |
| | | | | | · · | | | ·• |
| LC 100W | <.2 91 8 | 85 <1 37 | 7 20 <.2 <5 <5 <5 | 2.35 540 <10 195 24 | 40 <20 <20 5 2.3 | 34 1.04 0.37 0.03 0.20 1 | 2 3 <2 65 4 | <5 <10 0.15 2 |
| IC 1500 | 0.4 25 18 | 171 <1 47 | 7 11 <.2 <5 5 <5 | 2.25 269 <10 273 24 | 33 <20 <20 14 3.6 | 64 0.56 0.27 0.03 0.14 2 | 0 7 3 38 5 | <5 <10 0.17 20 |
| LC 200W | <.2 19 11 | 212 <1 26 | 6 12 <.2 <5 <5 <5 | 1.88 690 <10 205 24 | 33 <20 <20 8 2.1 | 11 1.24 0.34 0.02 0.16 1 | 2 4 2 88 4 | <5 <10 0.18 <1 |
| LC 250W | <.2 55 15 | 90 <1 52 | 2 16 <.2 <5 <5 <5 | 2.59 259 <10 102 52 | 48 <20 <20 9 2.6 | 60 1.50 0.44 0.02 0.30 1 | 4 4 <2 111 8 | <5 <10 0.21 1 |
| EC 3000 | <.2 24 3 2 | 228 <1 50 | 0 13 <.2 <5 7 <5 | 2.60 445 <10 238 26 | 37 <20 <20 12 3.8 | 84 0.54 0.32 0.03 0.17 1 | 7 5 3 52 6 | <5 <10 0.18 18 |
| | | | | | | | | |
| LC 35DM | <.2 14 14 | 116 <1 38 | 8 9 <.2 <5 <5 <5 | 1.81 469 <10 275 27 | 27 <20 <20 14 2.0 | 04 0.59 0.22 0.02 0.20 1 | 5 4 <2 36 4 | <5 <10 0.12 1 |
| 1C 400W | 0.6 46 21 | 196 <1 47 | 7 12 <.2 <5 15 <5 | 2.75 264 <10 359 23 | 35 <20 <20 9 4.0 | 04 0.74 0.49 0.03 0.18 3 | 0 4 4 57 6 | <5 <10 0.20 16 |
| LC 450W | 0.3 67 38 | 266 <1 46 | 6 13 <.2 <5 6 <5 | 2.56 336 <10 194 29 | 40 <20 <20 8 3. 0 | 07 0.93 0.42 0.02 0.23 1 | 4 6 3 49 5 | <5 <10 0.17 7 |
| LC 500W | <.2 54 78 | 351 <1 44 | 4 11 <.2 <5 24 <5 | 2,23 203 <10 113 41 | 38 <20 <20 13 1.5 | 54 0.80 0.35 0.02 0.24 1 | 2 5 <2 30 4 | <5 <10 0.12 <1 |
| IC 550W | 0.4 25 128 | 713 1 58 | 8 14 1.1 <5 10 <5 | 2,78 393 <10 260 32 | 44 <20 <20 10 3.4 | 45 0.63 0.33 0.03 0.20 1 | 8 6 3 34 7 | <5 <10 0.19 18 |
| | | | | | | | | |
| LC 600W | 0.4 28 102 | 402 <1 39 | 9 12 0.7 <5 55 <5 | 2.60 465 <10 189 24 | 40 <20 <20 20 4.2 | 26 0.62 0.37 0.03 0.16 2 | 1 14 4 35 6 | 5 <10 0.20 34 |
| LC 650W | <,2 24 30 | 169 <1 27 | 7 11 <.2 <5 9 <5 | 2.75 601 <10 325 18 | 44 <20 <20 8 5.5 | 58 0.55 0.39 0.03 0.08 1 | 8 7 6 36 7 | <5 <10 0.20 33 |
| LC 700W | 0.3 52 47 | 239 <1 35 | 5 14 0.2 <5 15 <5 | 2.68 309 <10 196 20 | 42 <20 <20 7 5.7 | 74 0.46 0.41 0.03 0.08 2 | 0 7 6 31 6 | <5 <10 0.21 28 |
| LC 750V | <.2 22 158 | 8 199 <1 12 | 2 10 3.2 <5 9 <5 | 1.42 3419 <10 337 15 | 29 <20 <20 8 1.0 | 02 0.36 0.75 0.03 0.15 3 | 6 4 <2 14 2 | <5 <10 0.10 <1 |
| LC OF | <.2 20 30 |) 154 <1 42 | 2 14 <.2 <5 7 <5 | 2.81 244 <10 307 27 | 44 <20 <20 7 4.3 | 31 0.35 0.14 0.03 0.11 1 | 4 3 4 28 6 | <5 <10 0.21 37 |
| | | | | | | | | F 40 0 01 1 |
| LC SOE | <.2 43 18 | 3 234 1 82 | 2 22 <.2 <5 8 <5 | 3.87 636 <10 352 96 | 64 <20 <20 13 3.4 | 40 1.15 0.31 0.02 0.36 3 | 0 5 2 42 7 | 5 <10 0.24 4 |
| 1 C 100E | <.2 21 21 | 177 <1 39 | 9 12 <.2 <5 6 <5 | 2.47 580 <10 273 29 | 38 <20 <20 13 3.0 | 67 0.42 0.19 0.03 0.13 1 | 8 6 3 27 6 | <5 <10 0.18 32 |
| LC 150E | <.2 8 26 | 5 249 <1 10 | 690.3<57<5 | 1.54 2387 <10 238 15 | 28 <20 <20 9 1.0 | 60 0.21 0.10 0.02 0.08 1 | 0 2 <2 20 3 | <> <10 0,15 4 |
| LC 200E | <.2 17 26 | 5 135 <1 2 | 8 11 <.2 <5 8 <5 | 2,58 345 <10 156 15 | 38 <20 <20 6 5.5 | 51 0.25 0.22 0.02 0.08 1 | 7 5 6 21 7 | <5 <10 0,19 49 |
| LC 250E | <.2 52 75 | 5 278 2 88 | 88 19 0.2 <5 9 <5 | 3.74 2525 <10 321 50 | 53 <20 <20 38 5. | 17 0.68 0.53 0.03 0.25 | 28 5 119 7 | 7 <10 0.18 6 |



Geochemical Lab Report

| CLIENT: | KENNECOTT CANAL | DA | INC. | | | | | | | | | | | | | | | DA | TF R | FCET | VED : | 12 | JAN-98 | 3 | DATE | PRIN | TED: | 19-J | IAN-S | 8 | PAGE | 3 | PROJ OF 5 | ECT: | CRAWFORD | BAY |
|-----------|-----------------|-----|------|-----|-----|-----|-----|-----|-----|----------------|-----|----------------|---------------------|-----|-----|-----|-----|-----|------|------|-------|------|--------|------|------|-------|------|---------|-------|-----|----------|------------|--------------|------|----------|-------|
| REPORT: | AA9-0002110 (/ | LOM | | | | | | | | | | | · · · · · · · · · · | | | | | | | | | | | | | ••••• | • | ••••••• | | | •••••• | ••••• | • • • • • • | ••• | | ••••• |
| SAMPLE | ELEMENT / | Ag | նս | Рb | Zń | Мо | Ni | Co | Cd | Bi | As | \$b | fe | Mn | Te | Ba | Cr | ۷ | \$n | W | La | AL | Mg | Ca | Na | κ | Sr | Y | Ga | Li | Nb | \$c | Ţa | τi | Zr | |
| NUMBER | UNITS P | PM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM : | PPM | PPN | PCT | РРМ | PPM | PPM | PPM | PPN | PPM | PPM | PPM | PCT | PCT | PCT | PCT | PCT | PPM | PPM | PPM | PPM | РРМ | PPM | PPN | PCT | PPM | |
| 1.C. 300F | | .2 | 21 | 31 | 133 | <1 | 42 | 12 | <,2 | <5 | 6 | ~ 5 | 2.34 | 250 | <10 | 219 | 27 | 38 | <20 | <20 | 18 | 3.71 | 0.48 | 0.23 | 0.03 | 0.11 | 17 | 9 | 3 | 28 | 5 | <5 | <10 | 0.17 | 34 | |
| 10 3506 | < | 2 | 31 | 38 | 122 | <1 | 33 | 11 | <.2 | ر ج | 7 | <5 | 2.37 | 303 | <10 | 185 | 29 | 37 | <20 | <20 | 17 | 3.65 | 0.49 | 0,26 | 0.03 | 0.13 | 22 | 10 | 3 | 27 | 7 | | <10 | 0.17 | 38 | |
| | | 7 | 23 | 54 | 126 | <1 | 27 | 10 | <.2 | <5 | 7 | <5 | 2.18 | 187 | <10 | 123 | 23 | 35 | <20 | <20 | 15 | 3.25 | 0.44 | 0,19 | 0.02 | 0.08 | 17 | 8 | 3 | 24 | 6 | <5 | <10 | 0.15 | 35 | |
| 10 4000 | 0 | | 30 | 24 | 174 | <1 | 20 | 10 | <.2 | <5 | <5 | <5 | 2.92 | 468 | <10 | 212 | 15 | 38 | <20 | <20 | 17 | 3.07 | 0.37 | 0.13 | 0.02 | 0.11 | 23 | 6 | 4 | 29 | 5 | <5 | <10 | 0.13 | 10 | |
| LC 500E | 0 | .3 | 60 | 36 | 35 | <1 | 54 | 5 | <.2 | - <5 | <5 | <5 | 0.98 | 34 | <10 | 320 | 17 | 26 | <20 | <20 | 93 | 5.15 | 0.21 | 0.39 | 0.05 | 0.06 | 57 | 82 | 8 | 74 | 6 | 6 | <10 | 0.17 | 39 | |
| 1 C 550E | ¢ | .2 | 21 | 28 | 177 | <1 | 32 | 12 | <.2 | <5 | 8 | ر ج | 2.56 | 791 | <10 | 246 | 22 | 45 | <20 | <20 | 11 | 3.01 | 0.44 | 0.18 | 0.02 | 0.13 | 13 | 5 | | 25 | 5 | <5 | <10 | 0.16 | 14 | |
| LC 600E | 0 | .4 | 21 | 84 | 315 | <1 | 47 | 14 | 0.2 | <5 | 12 | -5 | 2,55 | 337 | <10 | 191 | 21 | 38 | <20 | <20 | 13 | 3.50 | 0.31 | 0,14 | 0.03 | 0.09 | 15 | 11 | ·· 5 | 38 | 6 | ્ડ્ | <10 | 0.21 | 29 | |
| LC 650E | < | z.z | 25 | 34 | 171 | <1 | 33 | 10 | <.2 | <5 | 11 | <5 | 2.26 | 496 | <10 | 125 | 28 | 38 | <20 | <20 | 11 | 2.65 | 0.53 | 0.13 | 0.02 | 0.10 | 9 | 3 | <2 | 25 | 5 | 4 5 | <10, | 0.12 | 15 | |
| LC 700E | ~ | 4,2 | 24 | 35 | 355 | <1 | 23 | 11 | 0.6 | <5 | 10 | <5 | 2.53 | 626 | <10 | 173 | 19 | 36 | <20 | <20 | 10 | 2.12 | 0.43 | 0.23 | 0,02 | 0.13 | 15 | 3 | <2 | 25 | 5 ~ | ·5 | <10 | 0.15 | 8 | |

Bondru Clerg & Company 1.64 - 130 Pemberton Avenue, North Vancouver, B.C. - V7P 2R5, (604) 985 0681



Chemex Labs Ltd.

Analytical Chemists * Geochemists * Registered Assayers

212 Brooksbank Ave. North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218 To: KLONDIKE GOLD CORP

P.O. BOX 215 CRANBROOK, BC V1C 4H7 Page Number :2 Total Pages :6 Certificate Date:06-OCT-Invoice No. :1983225 P.O. Number : Account :QNA

Project : Comments: ATTN: GLEN RODGERS

CERTIFICATE OF ANALYSIS A98

...

A9832251

| SAMPLE | PREP CODE | Ag ppm Aqua R | Pb ppm 109 | Zn ppm 399 | | | | | | | |
|-------------|-----------------------|------------------|------------------|------------------|----|---|----------|-----|----------------|-------|---|
| CB LA 2050E | 201 202 | | 118 | 362 | | | | | | | |
| CB LA 2150E | 201 202 | | 31 | 236 | | | | | | | |
| CB LA 2200E | 201 202 | | 25 | 269 | | | | | | | |
| CB LA 2250E | 201 202 | | 29 | 247 | | | | | | | |
| CB LA 2300E | | | 26 | 139 | | | 1 | | | | |
| CB LA 2400E | 201 202 | | 28 | 371 | | | | | | | |
| CB LA 2450E | 201 202 | | 21 | 106 | | | | | | | |
| CB LD 0400E | 201 202 | | 12 | 100 | | | | | · · · | | |
| CB LD 0450g | 201 202 | | 23 | 84 | | | | | | | |
| CB LD 0500K | 201 202 | | 10 | 95 | | | | | | | |
| CB LD 0600E | 201 202 | | 9 | 41 | | | | | | | |
| CB LD 0650E | 201 202 | | 37 | 65 | | | | i · | | | |
| CB LD 0700E | 201 202 | | 18 | 95 | | | | | | | |
| CB LD 0750E | 201 202 | | 13 | 122 | | | | | | | |
| CB LD 0850K | | | 16 | 114 | | | | | | | |
| | | | | | · | |] | | | | |
| CB LD 0900E | | | 22 | 76 | | | | | | | |
| CB LD 10008 | 201 202 | | 20 | 67 | 1 | | | 1 | | | |
| CB LD 1050g | 201 202 | | 16 | 53 | | 1 | | | | | |
| CB LD 1100E | 201 202 | | 24 | 152 | | | | | | | |
| CB LD 1150E | 201 202 | | 25 | 172 | | | | | | 1 | |
| CB LD 1200E | 201 202 | | 26 | | | | | 1 | 1 | | l |
| CB LD 1300E | 201 202 | | | 104 | | | 1 | | | [| |
| CB LD 1350E | 201 202 | | 18 | 141 | | | | | | | |
| CB LD 1400E | 201 202 | | 15 | 84 | | | | 1 | - | 1 | |
| CB LD 1450E | 201 202 | | 16 | 83 | | | | |] | l | |
| CB LD 1500E | 201 202 | | 18 | 48 | | | | | | t | |
| CB LD 1600E | 201 202 | | 17 | 59 | ļ | | 1 | 1 | | | |
| | 202 302 | | | | | · | - | | | | |
| | l enn HE | ÷ . | 1 | | l. | | | | | 1 | |
| ' | | 2 | | • | | | | | | | · |
| | ∎ sets bet L Spott | | 1 | 4 | | | | | | 1 | |
| · · | | 1 | 1 | · · · | | | ł | | | 1 | |
| l | | <u> </u> | 1 | L | 1 | I | <u> </u> | l | Part Personale | 1 e 🛌 | L |

_

CERTIFICATION: How R 20



Chemex Labs Ltd.

Analytical Chemists * Geochemists * Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 FAX: 604-984-0218

To: KLONDIKE GOLD CORP

**

P.O. BOX 215 CRANBROOK, BC V1C 4H7

Project : Comments: ATTN: GLEN RODGERS Page Number 11 Total Pages 16 Certificate Date: 06-OCT-199 ; 9832251 Invoice No. P.O. Number QNA Account

| | | | CERTIFICATE OF ANALYSIS | A9832251 | | |
|--|--|-----------------------------------|-------------------------|----------|--|--|
| SAMPLE | PREP Ag ppm Pb CODE Aqua R ppm | Zn ppm | | | | |
| CB LA 000E CB LA 050E CB LA 100E CB LA 150E CB LA 200E | 201 202 24 201 202 27 201 202 32 201 202 38 201 202 49 | 118 87 126 114 120 | | | | |
| CB LA 250E CB LA 300E CB LA 350E CB LA 400E CB LA 450E | 201 202 78 201 202 85 201 202 33 201 202 47 201 202 47 201 202 105 | 226 108 92 182 112 | | | | |
| CB LA 500E CB LA 550E CB LA 600E CB LA 650E CB LA 700E | 201 202 50 201 202 37 201 202 35 201 202 47 201 202 83 | 180 135 259 154 371 | | | | |
| CB LA 750E CB LA 800E CB LA 850E CB LA 900E CB LA 950E | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | 271 132 213 141 140 | | | | |
| CB LA 1000E CB LA 1050E CB LA 1100E CB LA 1150E CB LA 1200E | 201 202 81 201 202 74 201 202 23 201 202 26 201 202 489 | 197 33 242 49 1075 | | | | |
| CB LA 1250E CB LA 1300E CB LA 1350E CB LA 1350E CB LA 1400E CB LA 1450E | 201 202 55 201 202 136 201 202 115 201 202 90 201 202 90 201 202 217 | 242 314 580 398 513 | | | | |
| CB LA 1500E CB LA 1550E CB LA 1600E CB LA 1650E CB LA 1650E CB LA 1700E | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | 450 147 701 611 402 | | | | |
| CB LA 1750E CB LA 1800E CB LA 1850E CB LA 1850E CB LA 1900E CB LA 1950E | 201 202 84 201 202 84 201 202 95 201 202 55 201 202 55 201 202 25 | 389 526 3885 405 5302 | | • | | |

1

CERTIFICATION:_

Harther Lo



