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ASSESSMENT REPORT

GEOPHYSICAL AND SOIL GEOCHEMICAL REPORT ON THE

COPPER KING PROPERTY

CK2, CK3, CK4, CK8 and CK9 CLAIMS

NTS 93 B/8,9
52° 33' North Latitude
122° 10' West Longitude
CARIBOO MINING DIVISION
BRITISH COLUMBIA

FOR
UNITED GUNN RESOURCES LTD.
1016 - 1030 WEST GEORGIA STREET
VANCOUVER, BRITISH COLUMBIA V6E 2Y3

BY

CREST GEOLOGICAL CONSULTANTS LTD.
2197 PARK CRESCENT
COQUITLAM, BRITISH COLUMBIA V3J 6T1

Craig W. Payne M.Sc., P.Geo.
January 10, 1999

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SUMMARY AND CONCLUSIONS

During May to August, 1998 mineral exploration work was carried out on the Copper King North grid which forms part of the Granite Mountain Project.

Selection of exploration targets was based on compilation work carried out in 1997.

The Copper King Property comprises 169 units (4225ha) located along the eastern side of the Granite Mountain Pluton which hosts Gibraltar Mines disseminated copper deposits.

The **Copper King North Grid** is located in the northeast corner of the claim block. The southern and eastern parts of the grid area is underlain by Cache Creek Group, siliceous argillite, chert, ribbon chert and minor volcanic rocks. These rocks appear to be in fault contact with younger early to middle Jurassic intermediate volcanic rocks, a thick sequence of intercalated volcanics and lapilli tuff and sheared interbedded limestone and tuff. This dominantly volcanic sequence is exposed throughout most of the grid area. Immediately west of the grid is epidote-chlorite altered medium to coarse grained quartz diorite. Contact relations between the quartz diorite and volcanic rocks is obscured by overburden.

Two areas of interest were partially defined from the exploration work. Mapping and prospecting discovered a northwest orientated, southwest dipping intercalated limestone-tuff horizon extending through the west-central part of the grid. This package of rocks is not well exposed but extends some 1400m through the grid and is up to 150m wide. The rocks have been sheared, deformed and silicified. Locally throughout the horizon is <1% to 1% disseminated pyrite and chalcopyrite with malachite along foliation planes and joints. Coincident with the limestone-tuff horizon is anomalous zinc values in soils extending to the northwest, VLF-EM conductive zone and a linear northwest trending magnetic low. Along strike to the northwest at the contact between the limestone-tuff horizon (to the west) and volcanic rocks (to the east) is a grey, sericite rich schist which is up to 25m wide. Locally this zone contains up to 10% disseminated fine grained pyrite and is located within the zinc soil anomaly. The limestone-tuff horizon, and coincident zinc soil anomaly remain open to the southeast. No "zinc" mineralization was found to explain the zinc soil anomaly.

The second area of interest is located in the northeastern corner of the grid. Copper mineralization consisting of disseminated and stringers of chalcopyrite is found in intensely silicified, brecciated and sheared lapilli tuff. The mineralization is spotty with no apparent lateral continuity. Coincident with the copper mineralization is an intense copper soil anomaly (up to 970.4ppm Cu) which is also of limited lateral extent. However it is possible that the copper mineralization extends to the east of the grid.

The 1998 exploration program on the Copper King Property was successful in discovering two areas containing significant copper and zinc mineralization within different geological settings. Based on the encouraging results further work is recommended on the property.

INTRODUCTION

This report describes the exploration results of grid establishment, soil sampling and geophysical work carried out on the Copper King North grid area which forms part of the Granite Mountain Project. Exploration work was carried out on behalf of United Gunn Resources Ltd., Vancouver, British Columbia. The above described surveys were used to investigate the property for signatures indicative of economic concentrations of disseminated base metal and bonanza style precious metal mineralization.

LOCATION AND ACCESS

The Copper King property is located in central British Columbia approximately 370 kilometres north of Vancouver, British Columbia (Figure 1).

Generally, road access is fairly good with Highway 97 following along the east side of the Fraser River with numerous secondary roads and trails throughout the area.

Copper King property (north grid area) is located on the eastern flank of Granite Mountain centred at 52°33' north latitude and 122°11' west longitude on NTS map sheets 93 B/8,9.

Road access to the property is via highway 97 north from Williams Lake to McLeese Lake, then east on Beaver Creek road for approximately 10 kilometres and then north on forest access roads to within 3.5 kilometres of the central part of the property. From there the forestry roads have been deactivated which requires 4trax access to the grid area. Old drill roads crossing the grid could be upgraded to allow access to most of the claims.

Sufficient water is available on the property to carry out drilling operations.

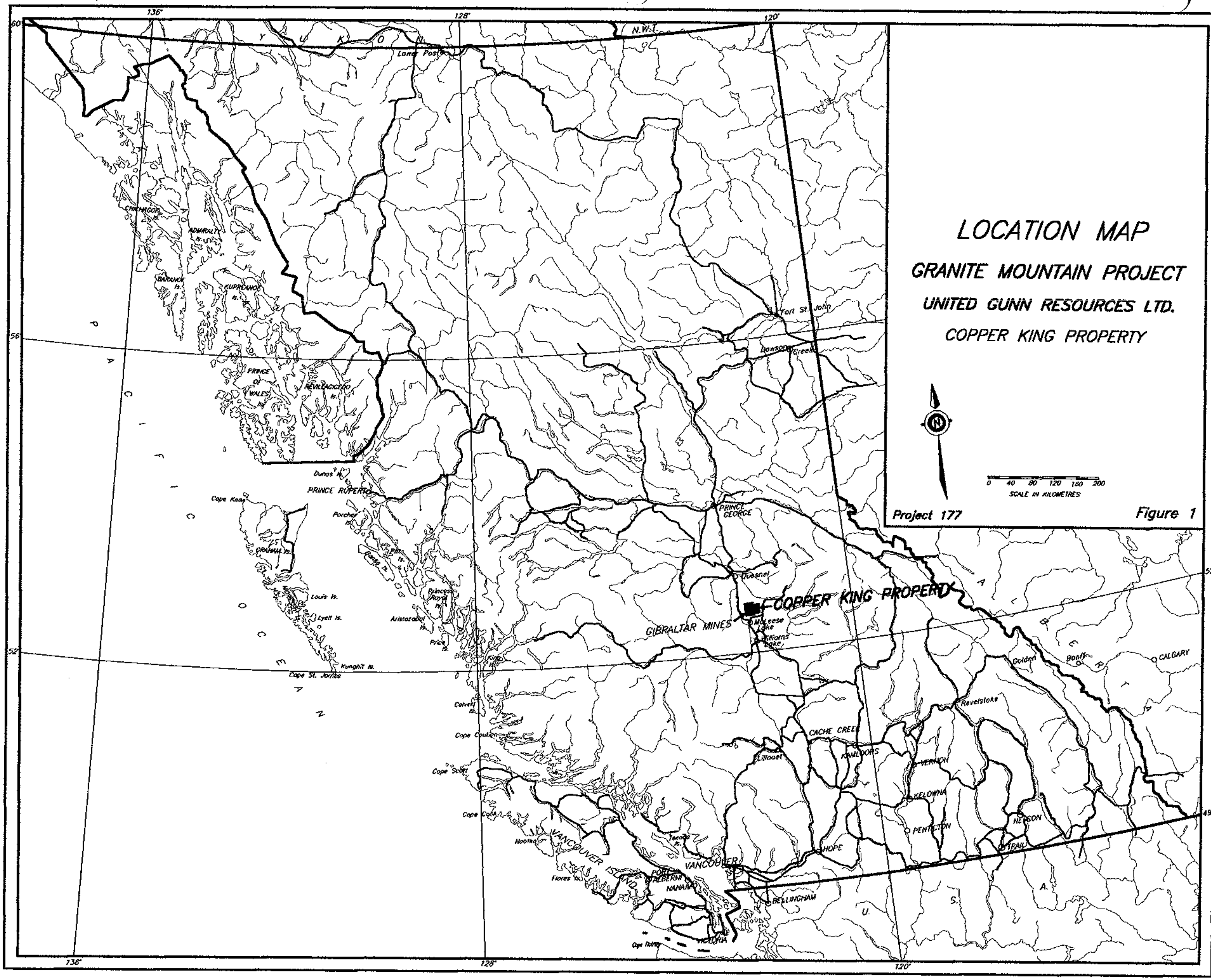
CLAIMS STATUS

The Copper King Property comprised of 17 claims totalling 169 units (4,225ha). Part of the claim block known as the Copper King North grid area is comprised of 5 claims totalling 94 units (2350ha) which forms the CK 98-2 group. The claims are 100% owned by United Gunn Resources Ltd. Table 1 provides pertinent claims data for the property (Figure 2).

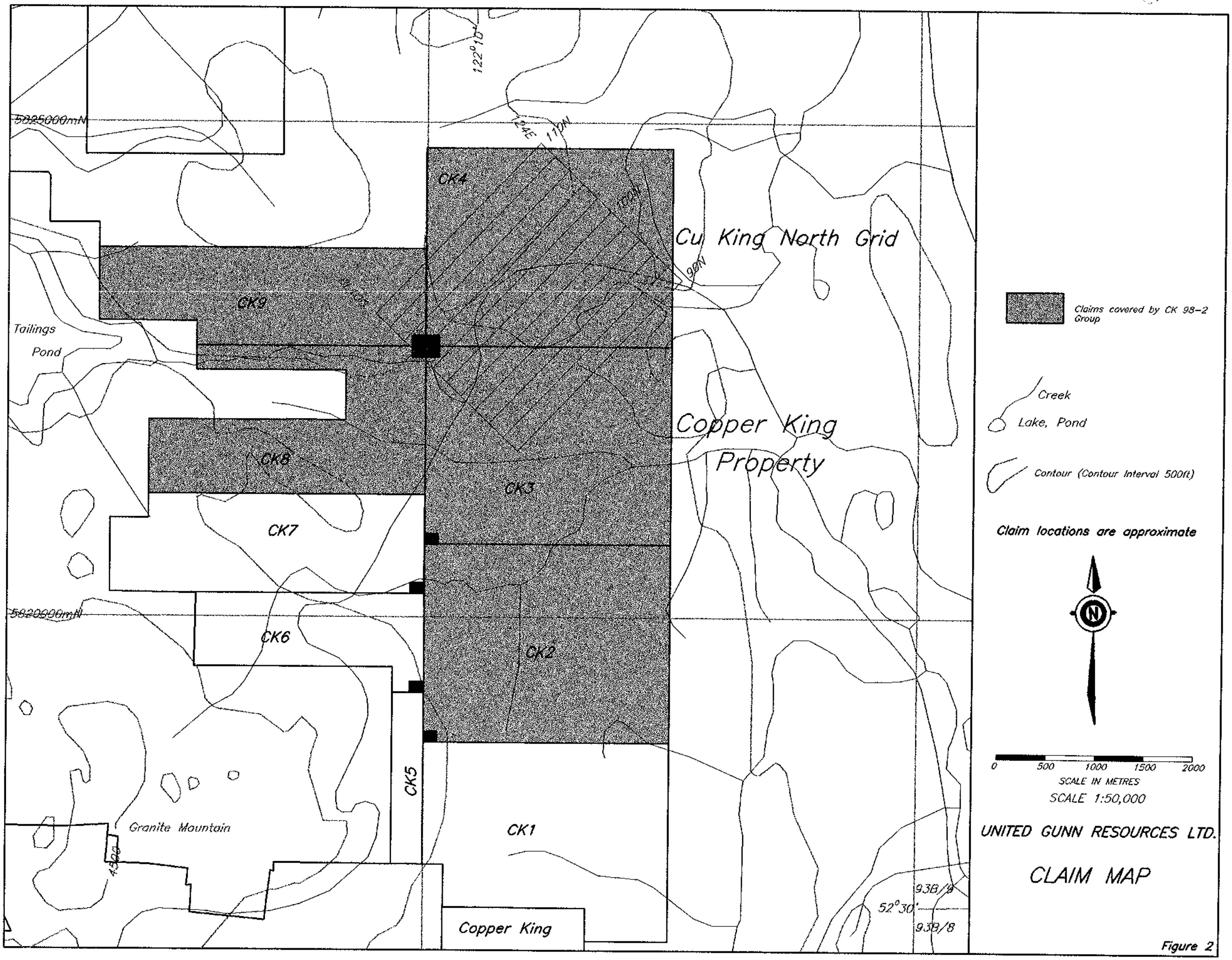
TABLE 1 CLAIMS DATA

COPPER KING PROPERTY			
CLAIM NAME	**TENURE NO.**	**NO. OF UNITS**	**EXPIRY DATE**
CK 2	359916	20	October 11, 2002
CK 3	359917	20	October 12, 2002
CK 4	359918	20	October 16, 2002
CK 8	359922	18	October 13, 2002
CK 9	359923	16	October 16, 2002
Total Number of Units		**94**	

*Subject to acceptance of 1998 assessment work.


LOCATION MAP
GRANITE MOUNTAIN PROJECT
UNITED GUNN RESOURCES LTD.
COPPER KING PROPERTY
0 40 80 120 160 200
SCALE IN KILOMETRES
Project 177
Figure 1
COPPER KING PROPERTY
GIBRALTAR MINES
Quesnel
PRINCE GEORGE
Fort St. John
Dawson Creek
PRINCE RUPERT
CACHE CREEK
KAMLOOPS
Lillooet
VERNON
KELOWNA
PENTICTON
NELSON
TRAIL
HOPE
VANCOUVER
VICTORIA
BELLINGHAM
NANAIMO
VANCOUVER ISLAND
Revelstoke
Golden
Banff
CALGARY
Lower Post
N.W.T.
Y U K O N
P A C I F I C O C E A N
A L B E R T A
U. S. A.
Cape St. James
Cape Scott
Cape Cook
Cape Knox
Nootka
Flores Is.
136°
128°
120°
60°
56°
52°
49°

2



5825000mN
122°10'
124E
110N
100N
90N
CK4
Cu King North Grid
CK9
Tailings
Pond
CK8
CK3
Copper King
Property
CK7
5820000mN
CK6
CK2
CK5
Granite Mountain
4500
CK1
Copper King
93B/9
52°30'
93B/8
Claims covered by CK 98-2 Group
Creek
Lake, Pond
Contour (Contour Interval 500ft)
Claim locations are approximate
N
0
500
1000
1500
2000
SCALE IN METRES
SCALE 1:50,000
UNITED GUNN RESOURCES LTD.
CLAIM MAP
Figure 2

TOPOGRAPHY AND VEGETATION

The property is located on the eastern slopes of Granite Mountain and extends out into a broad northerly trending valley known as Beaver Creek valley. Topography varies considerably within the grid area.

The Copper King North grid is located in the northeast corner of the property and varies from flat in the southern part with deeply incised valleys to steep terrain in the north. Elevations range from 980m in the south to 1200m in the north.

Vegetation on the grid area consists of pine, fir, cedar and balsam with stands of poplar trees near lakes and stream courses. Locally, parts of the grid areas have been clear cut and logging is active in the area.

HISTORY

In 1997 limited silt sampling and prospecting was carried out by Crest Geological Consultants Ltd. on behalf of United Gunn Resources Ltd. during staking of the Copper King property.

Most of the exploration work in the area concentrated on the Gibraltar property which is located to the west of the Copper King property. The original discovery of copper mineralization was made in 1927. Later, in 1957 Kimaclo Mines Ltd. drove an adit in high grade shear zones in the Gibraltar West zone. The Gibraltar property was then sold to Major Mines Ltd. in 1958 and was allowed to lapse. In 1962, J. Hilton restaked the Gibraltar property and optioned it to Keevil Mines Ltd. During 1964, Gibraltar Mines Ltd. acquired the property from Hilton and optioned the claims to Cominco Ltd. and Mitsubishi Mining Co. who delineated the Gibraltar West zone before terminating the option in 1967. In 1969 Canex Placer Ltd. and Duval Corp. acquired an option on the ground from Gibraltar Mines Ltd. Duval Corp. optioned the adjoining Pollyanna ground and in 1969 the Duval interest was acquired by Canex Placer Ltd. In 1970 the Granite Lake zone was discovered. In 1972 the mine was put into production at a rate of approximately 36,000 tonnes per day (Drummond et al, 1976).

Cuisson Mines Ltd. owns the claims adjoining Gibraltar Mines Ltd. on the east. These claims cover the eastern part of the Granite Lake ore body. United Gunn Resources Ltd. is a 30% partner in Cuisson Mines Ltd. along with Placer Dome, Inc. and Gibraltar Mines Ltd. Currently, copper leaching operations are underway on the Granite Lake ore body from which United Gunn receives a royalty.

In the area of the Copper King property which is located to the east and southeast of Gibraltar Mines, exploration work has been carried out intermittently since the 1960s. Gunn Mines Ltd. carried out magnetometer, induced polarization and drilled twelve diamond drill holes totalling 3,506 feet (1,068.6 metres) in the area of the claims during 1967 to 1971. In 1970 Primac Exploration Services Ltd. carried out geological, magnetometer and soil geochemical surveys on ground located just south of the present Copper King property.

In April 1991 the Copper King, Copper Queen and CP 1 to 6 claims were staked by Promin Explorations Limited on behalf of United Gunn Resources Ltd. to cover previously, partially defined induced polarization anomalies.

In October, 1991 a wide spaced soil geochemical survey was carried out over the IP anomalies to investigate for surface expressions of copper mineralization at depth.

REGIONAL GEOLOGY

The claims are located within a wedge shaped segment of late Palaeozoic to Miocene volcanic and sedimentary rocks which are intruded by several stocks/batholiths ranging in composition from diorite to granodiorite. This wedge shaped segment is located between the northwest-southeast trending Quesnel Trough to the east and the Pinchi Geanticline on the west, all of which forms part of the Intermontane Tectonic Belt (Figure 3).

Within the area of the claims the oldest rocks are a sequence of Permian, Cache Creek Group sedimentary and volcanic rocks (Tipper, 1959; Drummond et al, 1976). The Cache Creek Group rocks have been intruded by early Jurassic aged diorite to granodiorite Granite Mountain pluton.

Gibraltar Mines disseminated copper/molybdenum deposits are located eight kilometres northwest of the Copper King property. The mine consists of five deposits known as the Granite Lake, Pollyanna, Gibraltar East, Gibraltar West and Gibraltar West Extension. Original tonnage figures for the combined deposits are 326,000,000 tonnes grading 0.37% copper and 0.016% MoS_2 (Drummond et al, 1976).

Intrusion of the Granite Mountain pluton into Cache Creek Group metavolcanic and metasedimentary rocks has metamorphosed the surrounding rocks forming skarn zones. Panteleyev, 1977 suggests that the presence of chalcopyrite, magnetite and hematite in some of the skarn zones indicates that economically significant mineral deposits may be found peripheral to the Granite Mountain pluton.

1998 EXPLORATION PROGRAMS

Copper King North Grid

A total of 28.4km of northeast-southwest orientated grid lines were established, 562 soil samples were collected at 50m spacing along the grid lines and 26.4km of magnetometer and VLF-EM surveying at 12.5m stations was completed.

GENERAL PROPERTY GEOLOGY

Copper King North Grid - Geology

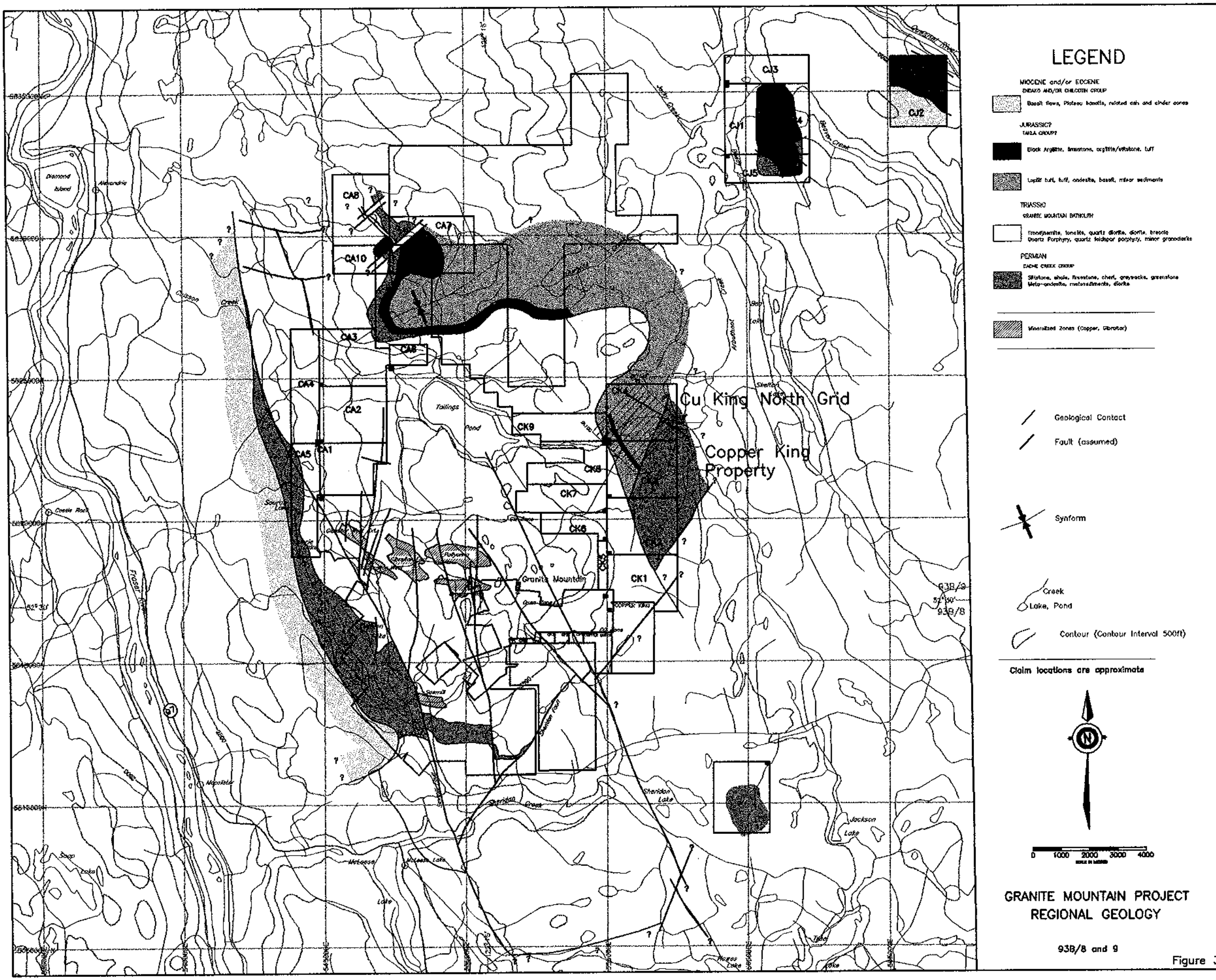
The Copper King North grid area is underlain by a northwest trending, folded and faulted sequence of sedimentary, tuffaceous and intermediate volcanic rocks of early to middle Jurassic age which are locally intruded by quartz porphyry dykes. The Granite Mountain pluton outcrops immediately to the west of the grid area. The southern and southeastern parts of the grid area are believed to be underlain by Cache Creek Group rocks.

SOIL GEOCHEMICAL SURVEYS

The purpose of the soil geochemical survey was to define anomalous areas indicative of economic concentrations of base and or precious metals in the underlying rock.

Copper King North Grid – Soil Geochemical Survey Results

A total of 562 soil samples were collected every 50m along northeast orientated grid lines spaced 200m apart. Soil sampling was offset by 25m on alternating grid lines. Depth of overburden in the grid area varies from <1m to greater than 18m in the south. Analytical certificates, sample descriptions and general statistical treatment of the data set are listed in Appendix I along with a grid map showing sample number locations (Figure 4). Sample collection and analytical techniques are described in Appendix II.



GRANITE MOUNTAIN PROJECT
REGIONAL GEOLOGY

93B/8 and 9

Figure 3

Anomalous values for base and precious metals were visually estimated from the data set based in part on the 90th to 95th percentile values.

Copper values in soils are generally low with 29 samples higher than the 95th percentile value of 74.4ppm. Throughout most of the central and western parts of the grid area anomalous copper values are spot highs associated with organic rich samples collected in proximity to creeks (Figure 5). Two areas in the eastern part of the grid show highly anomalous areas in copper, although there is no lateral continuity to the soil anomalies. The first area is centred at L102N, 122+25E and extends to L104N, 122+00E. Copper values in this anomaly range from 528.2ppm Cu to 970.4ppm Cu (two sample sites). This area is underlain by intensely silicified, epidote-chlorite altered and fractured lapilli tuff which contains disseminated and stringers of chalcopyrite and pyrite along fractures. Rock grab samples from this area contain up to 13967ppm Cu. Locally the rock is magnetic. Quartz veinlets and weak quartz/carbonate stockworks are developed. This mineralization is of limited lateral extent.

The second area of anomalous copper values (542.2ppm Cu) in soils is located at L106N, 124+00E. The soil sample was collected from the bottom of a northwest orientated gully. Prospecting in the area did not reveal the source for the copper soil anomaly, although there is abundant outcrop in the area. This copper soil anomaly remains open to the east.

Zinc values in soils range from 18.8ppm Zn to 1217.6ppm Zn. Spot zinc soil anomalies occur throughout the central and eastern parts of the grid area. The only significant zinc soil anomaly is a stepped, northwest orientated linear anomaly extending some 1400m long from L90N, 102+25E through to L104N, 105+50E and is coincident with a VLF-EM conductive zone (Figure 6). This anomaly ranges up to 75m wide and remains open to the southeast. The southeastern part of this soil anomaly is underlain by intercalated limestone-tuff. Rock grab samples of the limestone-tuff material did not contain any significant zinc values (up to 451ppm Zn). However, copper values in the limestone-tuff horizon range up to 2825ppm Cu. The central part of this zinc soil anomaly lies at the contact between andesite to the east and limestone-tuff to the west. Outcrop in this area consists of grey highly altered tuffaceous rock containing up to 10% disseminated fine grained pyrite. Rock samples of this material did not contain any significant metal values. Therefore this zinc soil anomaly remains unexplained.

GEOPHYSICAL SURVEYS

A total of 26.4km of magnetometer and VLF-EM surveying was carried out on the Copper King North grid. Readings were taken at 12.5m along grid lines spaced 100m or 200m apart. Total field magnetometer and inphase, quadrature and field strength measurements for two VLF-EM transmitters were recorded at each station along the grid lines.

Copper King North Grid – Geophysical Survey Results

Generally the magnetic data shows two distinct signatures, the southern and eastern part of the grid shows a low amplitude magnetic response indicative of sedimentary rocks. In this case the area is underlain by Cache Creek Group rocks. The central and western areas of the grid shows a moderate to high amplitude change in magnetic readings indicative of an intercalated sequence of tuffaceous and volcanic rocks. Within the moderate to high amplitude magnetic response are several well defined northwest orientated linear magnetic lows located in the west-central part of the grid area which have inpart defined an intercalated sequence of limestone and tuffaceous rocks which are mineralized with pyrite, chalcopyrite and malachite. In the northeastern part of the grid area is a well defined linear northwest orientated magnetic low which is bounded on the east and west by conductive zones. The magnetic low represents the trace of a fault structure and the conductive zones represent the boundary of the fault and enclosing rocks.

A complete interpretation of the magnetic and VLF-EM data was completed by Trent Pezzot of SJV Geophysics Ltd. The report and accompanying maps are presented in Appendix X.

RECOMMENDATIONS

Copper King North Grid

Two areas containing significant copper mineralization have been found on the Copper King North grid.

The first area is located in the west-central part of the grid area and is the limestone-tuff horizon which contains significant copper mineralization up to 2825ppm Cu (0.28% Cu). This horizon is also in part coincident with a zinc soil anomaly extending some 1400m along strike to the northwest. No explanation was found for the zinc soil anomaly. Also within this area is a grey sericite rich schist which contains up to 10% disseminated fine grained pyrite. Limited exploration work consisting of detailed soil sampling, magnetometer and VLF-EM surveys and prospecting and geological mapping is required to determine the cause of the zinc soil anomaly and tracing out the mineralized limestone-tuff horizon.

The second area of interest is located in the northeast corner of the grid where significant copper values was discovered in rock grab samples from altered and siliceous lapilli tuff. This area appears to extend further to the east off the grid. Geological mapping and prospecting coverage should be extended to the east of the known mineralization in the northeast corner of the grid area.

Respectfully Submitted,

CREST GEOLOGICAL CONSULTANTS LIMITED

Craig W. Payne, M.Sc., P.Geo.
January 10, 1999

ITEMIZED COST STATEMENT

Grid Establishment and soil sampling 28.4 kilometres at $275.00 per kilometre	$7,810.00
Assays/Geochem 562 samples at $16.38 per sample	9,205.56
Truck Rental 20 days at $65 per day (During period May 1 to August 31, 1998)	1,300.00
4Trax Rental 20 days at $64.20 per day(2 4trax's) (During period May 1 to August 31, 1998)	1,284.00
Fuel	398.50
Salaries - 20 mandays each during the period May 1 to August 31, 1998	
R. Roe at $176 per day	3,520.00
C. Roe at $160 per day	3,200.00
C. Thorsen at $170 per day	3,400.00
R. Bailey at $160 per day	3,200.00
Room and Board - 20 days (4 men) (During period May 1 to August 31, 1998)	3,600.00
Mag/VLF Survey (Field) - 12 days at 600.00/day (During period May 1 to July 19, 1998)	7,200.00
Assessment and Geophysical Reports	4,381.94
TOTAL	**$48,500.00**

STATEMENT OF QUALIFICATIONS

I, Craig W. Payne of Coquitlam, British Columbia do hereby certify that I:

1. am a graduate of Brock University St. Catharines, Ontario with a Master of Science degree in Geological Sciences, 1979.
2. am a Fellow of the Geological Association of Canada.
3. am a member of the Association of Professional Engineers and Geoscientists of British Columbia.
4. have practiced my profession since 1972.
5. am consulting geologist with Crest Geological Consultants Limited.
6. am the author of the report entitled "Geophysical and Soil Geochemical Report on the Copper King Property"; Cariboo Mining Division, dated: January 10,1999.

Dated at Coquitlam, B.C. this 10th day of January, 1999.

Respectfully submitted,

CREST GEOLOGICAL CONSULTANTS LIMITED

Craig W. Payne M.Sc., P.Geo.
January 10, 1999

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APPENDIX I

COPPER KING NORTH GRID

GENERAL STATISICS
SOIL SAMPLE DESCRIPTIONS AND ANALYTICAL CERTIFICATES

Crest Geological Consultants Ltd. Project 177

COPPER KING PROPERTY - NORTH GRID

GENERAL STATISTICS FOR SOIL GEOCHEMICAL DATA SET

	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Tl	Hg	Se	Te	Ga	Au
Number of Samples	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562	562
Max Value	2.5	970.4	91.9	1217.6	1713	155	97	3476	7.75	167	8	3	145	5.4	8.6	1	158	6.33	0.56	33	147	2.06	1042	0.22	5	5.86	0.03	0.6	2	0.4	133	1.3	0.7	13.5	923
Min Value	0.2	3.7	1.4	18.8	30	4	2	113	0.71	0.5	5	2	8	0.02	0.2	0.2	24	0.09	0.008	1	8	0.11	34	0.02	3	0.45	0.01	0.02	2	0.2	10	0.3	0.2	1.4	1
Average	0.7	27.3	4.6	66.5	139.0	19.3	8.0	396.8	2.0	3.6	5.1	2.0	22.3	0.2	0.4	0.2	47.9	0.4	0.1	7.0	32.6	0.4	107.9	0.1	3.0	1.3	0.0	0.1	2.0	0.2	24.1	0.3	0.2	4.2	5.7
Median	0.6	14.85	4.1	53.15	77	16	7	271.5	1.81	2.35	5	2	20	0.14	0.3	0.2	44	0.31	0.047	6	29	0.32	88	0.065	3	1.125	0.01	0.06	2	0.2	18	0.3	0.2	3.75	1
Variance	0.1	3299.1	16.4	4484.6	31703.4	207.6	33.3	135776.6	0.9	74.0	0.1	0.0	100.3	0.1	0.2	0.0	262.2	0.1	0.0	9.9	240.1	0.0	5740.7	0.0	0.0	0.5	0.0	0.0	0.0	0.0	342.1	0.0	0.0	3.1	1683.8
Standard Deviation	0.3	57.4	4.1	67.0	178.1	14.4	5.8	368.5	0.9	8.6	0.4	0.1	10.0	0.3	0.5	0.0	16.2	0.3	0.1	3.2	15.5	0.2	75.8	0.0	0.2	0.7	0.0	0.0	0.0	0.0	18.5	0.0	0.0	1.7	41.0
Mean+2STD'S	1.3	142.2	12.8	200.4	495.1	48.1	19.5	1133.8	3.9	20.8	5.8	2.3	42.3	0.8	1.4	0.3	80.3	1.0	0.2	13.3	63.6	0.8	259.4	0.1	3.4	2.7	0.0	0.2	2.0	0.2	61.1	0.4	0.2	7.7	87.8
Mean+3STD'S	1.7	199.7	16.8	267.4	673.1	62.5	25.3	1502.3	4.8	29.4	6.1	2.4	52.3	1.0	1.9	0.3	96.5	1.3	0.3	16.4	79.1	1.0	335.2	0.1	3.6	3.4	0.0	0.2	2.0	0.2	79.6	0.5	0.3	9.5	128.8
90th Percentile	1.1	48.0	6.5	106.7	348.5	30.9	13.0	814.4	3.1	5.3	5.0	2.0	30.9	0.4	0.6	0.2	70.0	0.5	0.1	9.0	46.9	0.6	192.8	0.1	3.0	2.2	0.0	0.1	2.0	0.2	45.9	0.3	0.2	6.7	6.0
95th Percentile	1.3	74.4	8.1	137.7	505.0	41.0	16.0	1057.0	3.9	8.1	5.0	2.0	40.0	0.6	0.7	0.2	81.0	0.6	0.2	12.0	63.0	0.7	247.0	0.1	3.0	2.6	0.0	0.1	2.0	0.2	61.0	0.3	0.2	7.5	10.0
98th Percentile	1.6	118.9	10.2	182.9	695.0	64.6	22.0	1586.0	4.6	12.3	6.0	2.0	51.0	0.7	1.0	0.2	89.8	0.9	0.3	17.0	79.8	0.9	308.1	0.2	3.8	3.2	0.0	0.2	2.0	0.2	82.1	0.3	0.2	9.0	37.3
99th Percentile	1.9	198.5	10.9	226.1	853.7	80.6	26.0	2100.1	4.9	21.5	7.0	3.0	57.6	0.9	1.1	0.2	99.3	1.0	0.3	21.0	89.1	1.1	370.7	0.2	4.0	3.6	0.0	0.2	2.0	0.2	101.3	0.5	0.2	9.7	61.1

CORRELATION TABLE

	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Tl	Hg	Se	Te	Ga	Au
Mo	1.0																																		
Cu	0.4	1.0																																	
Pb	0.2	0.2	1.0																																
Zn	0.2	0.2	0.8	1.0																															
Ag	0.3	0.4	0.2	0.2	1.0																														
Ni	0.5	0.4	0.2	0.2	0.3	1.0																													
Co	0.5	0.3	0.3	0.4	0.2	0.6	1.0																												
Mn	0.5	0.3	0.3	0.4	0.3	0.4	0.6	1.0																											
Fe	0.6	0.4	0.3	0.4	0.3	0.7	0.7	0.5	1.0																										
As	0.4	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.2	1.0																									
U	0.2	0.1	0.0	0.0	0.1	0.1	0.0	0.1	0.1	0.0	1.0																								
Th	0.1	0.1	0.1	0.0	0.0	0.3	0.2	0.1	0.2	0.1	0.0	1.0																							
Sr	0.3	0.3	0.3	0.2	0.3	0.6	0.3	0.4	0.4	0.3	0.1	0.3	1.0																						
Cd	0.2	0.1	0.8	0.8	0.3	0.2	0.2	0.4	0.2	0.1	0.1	0.0	0.4	1.0																					
Sb	0.3	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.2	0.9	0.0	0.1	0.4	0.1	1.0																				
Bi	0.1	0.4	0.1	0.1	0.2	0.5	0.2	0.2	0.2	0.0	0.1	0.0	0.2	0.1	0.1	1.0																			
V	0.6	0.3	0.2	0.3	0.2	0.6	0.6	0.4	0.9	0.2	0.1	0.2	0.3	0.1	0.2	0.2	1.0																		
Ca	0.1	0.2	0.8	0.7	0.2	0.3	0.2	0.3	0.3	0.1	0.1	0.1	0.7	0.8	0.1	0.1	0.1	1.0																	
P	0.3	0.1	0.2	0.4	0.2	0.1	0.2	0.2	0.3	0.1	0.1	0.0	0.1	0.3	0.1	0.0	0.2	0.1	1.0																
La	0.3	0.3	0.2	0.0	0.3	0.8	0.3	0.3	0.4	0.2	0.1	0.3	0.6	0.1	0.3	0.3	0.3	0.3	-0.1	1.0															
Cr	0.5	0.4	0.2	0.1	0.3	0.9	0.6	0.3	0.7	0.2	0.1	0.3	0.5	0.1	0.2	0.4	0.6	0.2	0.1	0.7	1.0														
Mg	0.2	0.3	0.2	0.3	0.2	0.5	0.6	0.4	0.7	0.1	0.1	0.2	0.4	0.1	0.2	0.2	0.6	0.3	0.0	0.3	0.5	1.0													
Ba	0.4	0.3	0.2	0.3	0.4	0.7	0.5	0.5	0.6	0.2	0.1	0.1	0.5	0.4	0.2	0.3	0.4	0.3	0.4	0.4	0.6	0.4	1.0												
Ti	-0.2	0.0	-0.1	0.0	-0.1	0.0	0.1	-0.1	0.2	-0.1	0.0	0.1	0.0	-0.2	0.0	-0.1	0.3	0.0	-0.3	0.0	0.0	0.5	-0.1	1.0											
B	0.0	0.0	0.4	0.3	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.0	0.1	0.4	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.1	0.0	0.0	1.0										
Al	0.6	0.5	0.3	0.4	0.3	0.8	0.7	0.5	0.9	0.1	0.1	0.2	0.4	0.2	0.1	0.3	0.8	0.2	0.3	0.5	0.8	0.7	0.6	0.1	0.0	1.0									
Na	0.1	0.2	0.1	0.0	0.1	0.5	0.2	0.1	0.3	0.0	0.0	0.2	0.3	0.1	0.1	0.2	0.2	0.2	-0.1	0.5	0.5	0.2	0.2	0.2	0.1	0.3	1.0								
K	0.2	0.2	0.1	0.2	0.2	0.5	0.4	0.4	0.6	0.2	0.1	0.2	0.4	0.2	0.2	0.2	0.4	0.2	0.0	0.3	0.5	0.6	0.5	0.3	0.0	0.5	0.2	1.0							
W																													1.0						
Tl	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.2	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.2	0.1	0.1	0.0	0.1	0.0	0.5		1.0					
Hg	0.7	0.4	0.3	0.3	0.4	0.6	0.4	0.5	0.6	0.2	0.3	0.2	0.4	0.3	0.2	0.2	0.6	0.3	0.3	0.5	0.6	0.4	0.5	-0.1	0.0	0.6	0.2	0.3		0.1	1.0				
Se	0.2	0.1	0.1	0.0	0.2	0.3	0.1	0.2	0.2	0.0	0.3	0.0	0.6	0.2	0.1	0.1	0.2	0.4	0.0	0.4	0.3	0.2	0.3	-0.1	0.0	0.2	0.1	0.2		0.0	0.4	1.0			
Te	0.1	0.3	0.1	0.0	0.1	0.2	0.1	0.1	0.1	0.0	0.0	0.0	0.1	0.1	0.1	0.4	0.0	0.0	0.0	0.2	0.2	0.1	0.1	-0.1	0.0	0.2	0.1	0.1		0.5	0.2	0.1	1.0		
Ga	0.7	0.4	0.3	0.3	0.3	0.6	0.6	0.4	0.9	0.1	0.2	0.2	0.2	0.1	0.1	0.2	0.8	0.1	0.4	0.3	0.6	0.5	0.5	0.1	0.0	0.9	0.2	0.4		0.1	0.7	0.2	0.1	1.0	
Au*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	-0.1	0.0	-0.1	0.0	0.0		0.0	0.0	0.0	0.0	0.0	1.0

UNITED GUNN [illegible]OURCES LTD.
COPPER KING NORTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
								ppm	ppm	ppm	ppm	ppb	ppb
12619	10000	9000	TILL	B	BROWN	FLAT		0.7	9.6	70.5	2.3	35	1
12618	10025	9000	TILL	B	BROWN	FLAT		0.6	14.6	107.5	1.7	24	2
12617	10075	9000	TILL	B	BROWN	FLAT		0.9	20.1	137.5	2.2	42	1
12616	10125	9000	TILL	B	BROWN	FLAT		0.8	11	91	3.7	16	1
12615	10175	9000	TILL	B	BROWN	FLAT		0.5	10.6	46.4	2.2	19	1
12614	10225	9000	ORGANIC	TOPSOIL	BLACK	FLAT		0.8	46.1	80.1	2	35	1
12613	10275	9000	TILL	B	BROWN	FLAT		1	12.6	78.4	3.2	11	1
12612	10325	9000	TILL	B	BROWN	FLAT		1.1	62.1	132.5	6.4	64	2
12611	10375	9000	TILL	B	BROWN	FLAT		0.5	10.9	33.5	2.4	19	1
12610	10425	9000	TILL	B	BROWN	FLAT		0.6	8.6	49.2	2.8	10	1
12609	10475	9000	TILL	B	BROWN	FLAT		0.6	3.7	222.6	1.1	14	1
12608	10525	9000	TILL	B	BROWN	HILLSIDE SE		0.5	8.4	186.9	3.3	21	3
12607	10575	9000	TILL	B	BROWN	HILLSIDE SE		0.5	5.4	185.4	2.3	27	1
12606	10625	9000	TILL	B	BROWN	HILLSIDE SE		0.5	20.5	65.5	2.3	11	1
12605	10675	9000	TILL	B	BROWN	FLAT		0.6	4.7	105.6	0.9	18	1
12604	10725	9000	TILL	B	BROWN	FLAT		0.5	15.1	41.6	3.5	10	2
12603	10775	9000	TILL	B	BROWN	FLAT		0.7	14.4	58.3	2	26	1
12602	10825	9000	TILL	B	GREY	FLAT		0.7	15.7	69.3	3	11	1
12601	10875	9000	TILL	B	BROWN	GULLY		1	98.3	96.1	6.4	61	1
12400	10925	9000	TILL	B	BROWN	GULLY		0.8	16.1	137.1	9.5	30	3
12399	10975	9000	TILL	B	BROWN	FLAT		0.6	16.7	98.5	2.2	25	33
12398	11025	9000	TILL	B	BROWN	FLAT		0.6	11.9	97.6	1.1	39	1
12397	11075	9000	TILL	B	BROWN	FLAT		0.5	21.9	98.9	1.6	27	1
12396	11125	9000	TILL	B	BROWN	FLAT		0.7	17.9	102.5	1.6	14	2
12395	11175	9000	TILL	B	BROWN	FLAT		0.6	25.7	99.3	3.1	24	1
12394	11225	9000	TILL	B	BROWN	FLAT		0.5	29.2	153.3	2.5	25	1
12393	11275	9000	TILL	B	BROWN	HILLSIDE NE		0.5	34	145.7	0.7	23	1
12392	11325	9000	TILL	B	BROWN	HILLSIDE NE		0.8	48.1	86.9	2	18	1
12391	11375	9000	TILL	B	BROWN	FLAT		0.6	61.7	59.2	1.2	19	1
12390	11425	9000	TILL	B	BROWN	FLAT		0.7	30.7	130.3	5	29	2
12389	11475	9000	TILL	B	BROWN	FLAT		0.6	12	41	2.9	10	4
12388	11525	9000	TILL	B	BROWN	FLAT		0.6	16.5	61.3	2.3	14	49
12387	11575	9000	TILL	B	BROWN	FLAT		1	11	128.3	2.8	46	1
12386	11625	9000	TILL	B	BROWN	FLAT		0.6	7.8	26.9	1.6	43	16
12385	11675	9000	TILL	B	BROWN	FLAT		0.9	25.6	50.2	4.2	29	7
12384	11725	9000	TILL	B	BROWN	FLAT		0.9	39.4	49.2	5.9	75	1
12383	11775	9000	TILL	B	BROWN	HILLSIDE SE		0.9	17.3	52.1	2.9	18	1
12382	11825	9000	TILL	B	BROWN	FLAT		0.9	12.6	53.6	1.7	35	10
12381	11875	9000	TILL	B	BROWN	FLAT		0.8	14.2	56	2	30	923
12380	11925	9000	TILL	B	BROWN	HILLSIDE SE		0.6	19.5	43.8	2.2	14	4
12379	11975	9000	TILL	B	BROWN	FLAT		0.7	6	64.2	1	17	2
12378	12025	9000	TILL	B	BROWN	HILLSIDE N		0.8	8.5	38.9	3.3	27	2
12377	12075	9000	TILL	B	BROWN	HILLSIDE S		0.9	39.7	74.7	5.5	66	2
12376	12125	9000	TILL	B	BROWN	HILLSIDE SE		0.7	18.4	43.1	3.6	28	2
12375	12175	9000	TILL	B	BROWN	HILLSIDE N		1.3	31.7	75.4	4.9	44	6
12374	12225	9000	TILL	B	BROWN	HILLSIDE N		1	23.4	134.8	5.1	57	1
12373	12275	9000	TILL	B	BROWN	GULLY		0.7	17.2	44.4	3.2	26	1
12372	12325	9000	TILL	B	BROWN	HILLSIDE SW		0.5	11	61.4	2.4	12	2

UNITED GUNN ( )OURCES LTD.
COPPER KING NORTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
								ppm	ppm	ppm	ppm	ppb	ppb
12371	12375	9000	TILL	B	BROWN	HILLSIDE SE	NE SIDE (SW ASPECT) OF STEEP GULLY.	0.7	26.7	50.8	3.2	32	3
12341	10000	9050	TILL	B	BLACK	FLAT	SAMPLE TAKEN AT 122+10 (BASE OF SLOPE) DUE TO CREEK.	0.8	25.9	56.6	4.3	45	7
12342	10000	9100	TILL	B	BROWN	FLAT	SW SIDE (NE ASPECT) OF LARGE GULLY	0.8	16	41.3	2.5	10	1
12343	10000	9150	TILL	B	BROWN	FLAT	CUTBLOCK.	0.7	17	66.4	3.3	21	1
12717	10000	9200	TILL	B	BROWN	FLAT	CUTBLOCK.	0.8	14.8	67.5	2.7	26	2
12716	10050	9200	TILL	B	BROWN	FLAT	CUTBLOCK.	0.7	14.7	62.7	4.6	23	4
12715	10100	9200	TILL	B	BROWN	FLAT	CUTBLOCK.	0.8	15.6	56.8	3.7	11	1
12714	10150	9200	TILL	B	BROWN	FLAT	CUTBLOCK.	0.5	8.8	48.7	1	10	4
12713	10200	9200	TILL	B	ORANGE	FLAT	CUTBLOCK.	0.7	13.3	79.4	3.5	18	4
12712	10250	9200	TILL	B	BROWN	FLAT	CUTBLOCK. DISTURBED SITE.	0.7	11.9	47.4	1.7	31	2
12711	10300	9200	TILL	B	BROWN/ORANGE	FLAT		0.7	21.4	52.6	4	24	4
12710	10350	9200	TILL	B	ORANGE	FLAT	CUTBLOCK.	0.7	10.6	37.7	1.7	10	1
12709	10400	9200	TILL	B	BROWN	FLAT	CUTBLOCK.	0.4	10.4	46.8	1.6	14	1
12708	10450	9200	TILL	B	BROWN	FLAT		0.4	11.1	41.3	1.1	22	1
12707	10500	9200	TILL	B	BROWN	FLAT		0.6	10.7	53.2	1.2	19	1
12706	10550	9200	TILL	B	BROWN	FLAT		0.6	11.3	54.6	1.8	19	1
12705	10600	9200	TILL	B	BROWN	HILLSIDE E		0.8	19.3	49	3.5	39	8
12704	10650	9200	TILL	B	BROWN	HILLSIDE W		0.4	10.5	44.4	1.4	14	5
12703	10700	9200	TILL	B	BROWN	FLAT		0.3	13.8	37.4	2	12	1
12702	10750	9200	TILL	B	BROWN	FLAT		0.3	15	44.8	1.6	28	1
12701	10800	9200	TILL	B	BROWN	FLAT		0.4	11.2	41	1.1	10	1
12300	10850	9200	TILL	B	BROWN	FLAT		0.4	10.2	30	1.4	12	2
12299	10900	9200	TILL	B	ORANGE	FLAT		0.3	7	31.9	0.9	12	1
12298	10950	9200	TILL	B	BROWN	HILLSIDE E		0.6	13.9	51	2.8	23	3
12297	11000	9200	TILL	B	ORANGE	HILLSIDE W		0.8	20.1	44.9	5.6	11	2
12296	11050	9200	TILL	B	ORANGE	HILLSIDE W	SAMPLE TAKEN BASE OF GULLY SLOPE 110+25E DUE TO SWAMP.	1	12.1	46.6	3.9	12	144
12295	11100	9200	TILL	B	BROWN	FLAT		0.6	18.7	38.9	4.5	25	1
12294	11150	9200	TILL	B	BROWN	FLAT		1	14.7	87.8	3.9	55	1
12293	11200	9200	TILL	B	BROWN/GREY	FLAT		0.3	11.2	53.8	1.3	10	1
12292	11250	9200	TILL	B	BROWN/GREY	FLAT		1.3	47	86.4	3.6	88	3
12291	11300	9200	TILL	B	BROWN	FLAT		0.2	8.4	27.9	1	14	7
12290	11350	9200	TILL	B	BROWN	FLAT		0.5	11.7	38.1	1.1	21	1
12289	11400	9200	TILL	B	BROWN	FLAT		0.3	9.5	25.4	1.1	10	3
12288	11450	9200	TILL	B	BROWN	FLAT	TRACE QUARTZ PEBBLES IN SOIL.	0.4	9.3	21.5	1.1	16	1
12287	11500	9200	TILL	B	BROWN	HILLSIDE E		0.4	8.7	23.8	1.2	11	6
12286	11550	9200	TILL	B	BROWN	FLAT		0.3	9.5	23	1.1	10	3
12285	11600	9200	TILL	B	BROWN	FLAT		0.4	11.3	26.9	1.8	13	1
12284	11650	9200	TILL	B	BROWN	FLAT	TOP OF SOUTH GULLY.	0.6	12.3	42.9	2.9	28	16
12283	11700	9200	TILL	B	BROWN	FLAT		0.3	9.9	35.7	1.2	17	2
12282	11750	9200	TILL	B	BROWN	FLAT		0.5	13.5	39.8	2.1	22	187
12281	11800	9200	TILL	B	BROWN	FLAT	BASE LINE NEXT TO SMALL POND. FINE GRAINED SANDY SOIL.	0.6	42.9	67.1	6.5	21	3
12280	11850	9200	TILL	B	ORANGE	FLAT		0.5	14.8	55.1	3.5	20	3
12279	11900	9200	TILL	B	BROWN	FLAT		0.4	8.8	29.7	1.1	11	2

UNITED GUNN [illegible]SOURCES LTD.

COPPER KING NORTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
								ppm	ppm	ppm	ppm	ppb	ppb
12278	11950	9200	TILL	B	BROWN	HILLSIDE W		0.2	8.2	22.8	1.2	10	1
12277	12000	9200	TILL	B	ORANGE	FLAT	BASE LINE NEXT TO NORTH ROAD AT JUNCTION.	0.3	18.3	36	2.8	15	2
12276	12050	9200	TILL	B	ORANGE	FLAT		0.4	12	31.6	1.9	17	1
12275	12100	9200	TILL	B	BROWN	FLAT		0.3	8.8	30	1	10	2
12274	12150	9200	TILL	B	BROWN	HILLSIDE NE		0.7	14.7	44.1	4.2	29	34
12273	12200	9200	TILL	B	BROWN	HILLSIDE SW		0.4	21	34.1	4.2	22	3
12272	12250	9200	TILL	B	BROWN	HILLSIDE SW		0.8	15.7	77.7	2.1	25	1
12271	12300	9200	TILL	B	ORANGE	FLAT		0.6	11.3	50.4	2.8	34	1
12270	12350	9200	TILL	B	BROWN	FLAT		0.6	24.5	48.2	2.8	22	21
12269	12400	9200	TILL	B	ORANGE	FLAT	BASE LINE NORTH SIDE OF ROAD.	0.5	32.3	50	3.9	38	5
12344	10000	9250	TILL	B	BROWN	FLAT		0.6	40.9	64.7	5.4	73	2
12345	10000	9300	TILL	B	BROWN	FLAT		0.3	9.3	26.6	1.2	13	2
12346	10000	9350	TILL	B	BROWN	FLAT		0.2	10.7	33.7	0.8	20	1
12536	10000	9400	TILL	B	BROWN	FLAT		0.3	8.8	26.7	1.1	10	8
12535	10025	9400	TILL	B	BROWN	FLAT		0.4	13.8	41.6	1.2	25	1
12534	10075	9400	TILL	B	BROWN	FLAT		0.3	8.7	27.9	1.1	16	9
12533	10125	9400	TILL	B	BROWN	FLAT		0.6	16	37.5	3.6	10	1
12532	10175	9400	TILL	B	BROWN	FLAT	EAST SIDE OF GULLY. QUARTZ PEBBLES THROUGHOUT SOIL.	0.5	9.3	41.6	2.3	10	1
12531	10225	9400	TILL	B	BROWN	FLAT	EAST SIDE AT BOTTOM.	0.9	13.8	67.7	4.3	13	4
12530	10275	9400	TILL	B	BROWN	FLAT	SIDE OF GULLY.	0.8	13.5	66.4	3.5	15	2
12529	10325	9400	TILL	B	BROWN	FLAT	SIDE OF GULLY E-W.	0.8	27.4	50.4	5.5	21	1
12528	10375	9400	TILL	B	BROWN	FLAT	SIDE OF GULLY N-S.	1	8.4	87.7	2	21	1
12527	10425	9400	TILL	B	BROWN	FLAT	SIDE OF GULLY.	0.6	24.3	46	4.8	28	1
12526	10475	9400	TILL	B	BROWN	FLAT	HEAD OF SMALL GULLY.	0.5	9.8	53	1.5	10	1
12525	10525	9400	TILL	B	BROWN	FLAT	LOGGING BLOCK.	0.7	10.3	64.9	3.5	10	1
12524	10575	9400	TILL	B	BROWN	FLAT	LOGGING BLOCK.	0.7	18.8	89.8	5.3	22	2
12523	10625	9400	TILL	B	BROWN	FLAT	LOGGING BLOCK.	0.7	12.9	71.7	1.8	10	1
12522	10675	9400	TILL	B	BROWN	FLAT	LOGGING BLOCK.	0.6	10.8	50	1.7	10	9
12521	10725	9400	TILL	B	BROWN	FLAT	LOGGING BLOCK.	0.5	14.3	59	3.8	10	1
12520	10775	9400	TILL	B	BROWN	FLAT		0.4	10.6	64.2	1.6	10	1
12519	10825	9400	TILL	B	BROWN	FLAT	ON ROAD.	0.4	8.9	67.8	1.2	10	1
12518	10875	9400	TILL	B	BROWN	FLAT	NEXT TO ROAD.	0.4	12	52.1	1.7	16	2
12517	10925	9400	TILL	B	BROWN	GULLY		0.4	11.6	48.3	1.6	10	5
12516	10975	9400	TILL	B	BROWN	FLAT		0.3	9.9	45.6	1.1	10	1
12515	11025	9400	TILL	B	BROWN	FLAT	ON ROAD.	0.3	10.7	50.8	1.5	19	1
12514	11075	9400	TILL	B	BROWN	HILLSIDE E		0.4	11.9	51.1	1.3	15	3
12513	11125	9400	TILL	B	BROWN	GULLY		0.6	15.3	62.8	1.9	14	4
12512	11175	9400	TILL	B	BROWN	GULLY		0.6	14.9	55.7	2.2	25	2
12511	11225	9400	TILL	B	BROWN	GULLY	NEXT TO ROAD.	0.5	18.9	44.6	2	10	2
12510	11275	9400	TILL	B	BROWN	HILLSIDE W	NEXT TO ROAD.	0.4	15	37.4	2.3	18	1
12509	11325	9400	TILL	B	BROWN	HILLSIDE NE	AT ROAD JUNCTION.	1	65.5	86.8	12.6	98	2
12508	11400	9400	TILL	B	BROWN	GULLY		0.4	13.8	46.1	1.5	11	1
12507	11425	9400	TILL	B	BROWN	GULLY		0.4	12.6	34.1	2.7	10	1
12504	11575	9400	TILL	B	BROWN	HILLSIDE S		0.5	10.6	36	1.5	14	1
12503	11625	9400	TILL	B	BROWN	HILLSIDE NE		0.3	9.1	31.9	1	13	15
12502	11675	9400	TILL	B	BROWN	HILLSIDE NE	TOP OF GULLY EAST SIDE.	0.8	17.7	34.9	3.4	10	1

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COPPER KING NORTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
								ppm	ppm	ppm	ppm	ppb	ppb
12501	11725	9400	TILL	B	BLACK	GULLY		0.7	74.6	132.9	3.5	29	1
12200	11775	9400	TILL	B	BROWN	GULLY		0.5	9.3	38.8	1.8	21	1
12199	11825	9400	TILL	B	BROWN/ORANGE	HILLSIDE NE		0.7	59.6	109.7	2.1	21	1
12198	11875	9400	TILL	B	BROWN	HILLSIDE NE		0.8	10.6	94.5	1.1	15	1
12197	11925	9400	TILL	B	BROWN	FLAT		0.9	13.3	58.4	3.1	15	1
12196	11975	9400	TILL	B	BROWN	FLAT		0.6	10.4	83.5	2.8	12	3
12195	12025	9400	TILL	B	BROWN	FLAT		0.7	18.9	204.2	4.6	40	1
12194	12075	9400	TILL	B	BROWN	FLAT		1.3	7	40.2	10.7	36	1
12193	12125	9400	TILL	B	BROWN	HILLSIDE NE		0.8	23.9	58.2	4.7	27	2
12192	12175	9400	TILL	B	BROWN	HILLSIDE NE		1.1	56.6	179	10.1	43	2
12191	12225	9400	TILL	B	BROWN	GULLY		0.7	18.2	108.3	4.7	17	1
12190	12275	9400	TILL	B	BROWN	HILLSIDE SE		1.1	21.4	180.2	4.9	22	1
12189	12325	9400	TILL	B	BROWN	HILLSIDE SW		0.7	9.2	77.2	3	26	1
12188	12375	9400	TILL	B	BROWN/GREY	FLAT		0.8	33.2	107.3	3.9	59	1
12347	10000	9450	TILL	B	BROWN	FLAT		0.6	16.3	59.8	2.7	25	1
12348	10000	9500	TILL	B	BROWN	FLAT		0.5	18	69.5	2.4	27	1
12349	10000	9550	TILL	B	BROWN	FLAT		0.4	12.2	40.1	2.5	11	1
12620	10000	9600	TILL	B	BROWN	HILLSIDE S		0.5	6.7	23.7	1.6	19	1
12621	10050	9600	TILL	B	BROWN	HILLSIDE S		0.4	11.2	37.5	1.5	17	1
12622	10100	9600	TILL	B	BROWN	GULLY		0.6	11.3	74.1	2.4	40	1
12623	10150	9600	TILL	B	BROWN	HILLSIDE SE		0.8	13.3	35.6	3.3	18	2
12624	10200	9600	TILL	B	BROWN	FLAT		0.5	12.6	45.1	2.9	10	1
12625	10250	9600	TILL	B	BROWN	FLAT		2.5	117.7	52.6	22.4	88	1
12626	10300	9600	TILL	B	BROWN	FLAT		2.3	41	58.8	5.1	55	1
12627	10350	9600	TILL	B	BROWN	HILLSIDE SE		0.6	12.3	139.9	3.3	12	3
12628	10400	9600	TILL	B	BROWN	HILLSIDE SE		0.5	12.6	58.8	3.1	10	2
12629	10450	9600	TILL	B	BROWN	HILLSIDE SE		0.8	29	171	1.7	22	1
12630	10500	9600	TILL	B	BROWN	HILLTOP		0.7	20.3	92.7	3.1	28	3
12631	10550	9600	TILL	B	BROWN	HILLSIDE NE		1.1	45.7	542.6	8.1	15	2
12632	10600	9600	TILL	B	BROWN	HILLSIDE NE	NO SAMPLE TAKEN AT 105+75E.	0.4	12.1	37.8	2.3	10	1
12633	10650	9600	TILL	B	BROWN	GULLY		0.6	5.2	43	3	11	1
12634	10700	9600	TILL	B	BROWN	FLAT		0.5	12.3	101.6	2.5	24	1
12635	10750	9600	TILL	B	BROWN	FLAT		0.4	20.7	37.2	5.4	12	11
12636	10800	9600	TILL	B	BROWN	FLAT		0.3	12.7	65.5	3.3	10	14
12637	10850	9600	TILL	B	BROWN	FLAT		0.5	18.2	38.6	3.7	10	1
12638	10900	9600	TILL	B	BROWN	HILLSIDE E		0.5	11.7	61	3.6	20	2
12639	10950	9600	ORGANIC	TOPSOIL	BLACK	FLAT		0.9	24.3	27.2	4.4	27	138
12718	11000	9600	TILL	B	ORANGE	FLAT		0.5	10.8	75.1	1.6	14	2
12719	11050	9600	TILL	B	BROWN	HILLSIDE N		0.7	15.2	96.4	1.8	14	1
12720	11100	9600	TILL	B	BROWN	GULLY		0.9	105.1	89.6	8	108	5
12721	11150	9600	TILL	B	BROWN	HILLSIDE S		0.9	17.3	92.1	4	27	8
12722	11200	9600	TILL	B	BROWN	HILLSIDE S		0.6	17.5	30.6	3.8	10	1
12723	11250	9600	TILL	B	BROWN/GREY	HILLSIDE SE		0.7	67.7	49.4	1.5	29	1
12724	11300	9600	TILL	B	BROWN	HILLSIDE SE		1	18.1	82.9	3.1	29	2
12725	11350	9600	TILL	B	BROWN	HILLSIDE SE		0.7	17.3	55.7	4.1	17	1
12726	11400	9600	TILL	B	BROWN	FLAT		0.6	23.4	70.2	2.6	18	1
12727	11450	9600	TILL	B	BROWN	HILLSIDE E		0.7	10	50	3.1	22	1
12728	11500	9600	TILL	B	BROWN	FLAT		0.5	7.5	29.4	2.6	10	5

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COPPER KING NORTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
								ppm	ppm	ppm	ppm	ppb	ppb
12729	11550	9600	TILL	B	BROWN	HILLSIDE NW		0.6	18.5	34.6	4.6	10	4
12730	11600	9600	TILL	B	BROWN	HILLSIDE SE	NO SAMPLE TAKEN AT 116+25E.	0.6	29.5	76.5	4.8	12	1
12731	11650	9600	TILL	B	BROWN	HILLSIDE SE		0.6	40.7	160.3	4.1	27	1
12732	11700	9600	TILL	B	BROWN	HILLSIDE SE		0.5	10.4	47.7	1.2	22	1
12733	11750	9600	TILL	B	BROWN	FLAT		0.4	16.4	113	2	22	1
12547	11800	9600	TILL	B	BROWN	FLAT		0.3	19.7	72	1.1	13	1
12546	11850	9600	TILL	B	BROWN	HILLSIDE SE		0.5	21.7	97.6	1.8	10	5
12545	11900	9600	TILL	B	BROWN	HILLSIDE SE		0.4	17.3	85.5	3.2	20	1
12544	11950	9600	TILL	B	BROWN	HILLSIDE E		0.4	14.1	67.2	2.9	30	1
12543	12000	9600	TILL	B	BROWN	GULLY		0.5	15.9	33.8	3.8	11	1
12542	12050	9600	TILL	B	BROWN	GULLY		0.7	14	69.8	2.8	15	1
12541	12100	9600	TILL	B	BROWN	GULLY		0.5	11.9	29.6	4.9	10	1
12540	12150	9600	TILL	B	BROWN	HILLSIDE S		0.5	27.3	38.8	5.4	21	1
12539	12200	9600	TILL	B	BROWN	HILLSIDE S		1	34.8	47.5	4.9	12	1
12538	12250	9600	TILL	B	BROWN	FLAT		0.6	11.5	44.9	3.3	11	8
12537	12300	9600	TILL	B	BROWN	FLAT		0.7	18.1	35.1	4	10	10
12506	12350	9600	TILL	B	BROWN/ORANGE	FLAT	NO SAMPLE TAKEN AT 123+25E - LOCATED ON ROCK BLUFF.	1.2	36	70.8	3	51	1
12505	12400	9600	TILL	B	BROWN/ORANGE	FLAT		2.1	86.1	75.2	7.5	77	6
12350	10000	9650	TILL	B	BROWN	FLAT		1.3	970.4	71.3	3.8	52	2
12351	10000	9700	TILL	B	BROWN	FLAT		1.2	32.4	67.7	1.5	35	5
12352	10000	9750	TILL	B	BROWN	FLAT	NO SAMPLE TAKEN AT 121+25E - LOCATED ON ROCK BLUFF.	0.6	12.2	124.4	2.3	22	1
12418	10000	9800	TILL	B	BROWN	HILLSIDE NE		1.1	96.9	111	13.4	31	1
12419	10025	9800	TILL	B	BROWN	HILLSIDE N		0.9	19.7	54.7	5.6	22	1
12420	10075	9800	TILL	B	BROWN	HILLSIDE NE		1	15.8	36.6	4.4	10	1
12421	10125	9800	TILL	B	BROWN	HILLSIDE E		0.9	9.1	81.7	1.2	18	1
12422	10175	9800	TILL	B	BROWN	HILLSIDE NE		1.2	84.4	164.7	4.3	44	1
12423	10225	9800	TILL	B	GREY	FLAT		1	31.1	99	4	25	1
12424	10275	9800	TILL	B	BROWN	FLAT		0.9	19.1	79.4	3	11	5
12425	10325	9800	TILL	B	BROWN	HILLSIDE NE		0.7	11.9	47.8	1.8	21	2
12426	10375	9800	TILL	B	BROWN	HILLSIDE SW		0.7	12.4	52	2.1	19	5
12427	10425	9800	TILL	B	GREY	HILLSIDE S		0.4	10.5	34.8	1.7	14	3
12428	10475	9800	TILL	B	BROWN	HILLSIDE NE		0.4	9.6	47.8	1.4	21	1
12429	10525	9800	TILL	B	BROWN	HILLSIDE NE		0.6	24.8	39	3.3	36	5
12430	10625	9800	TILL	B	BROWN	HILLSIDE SE		0.7	40.5	57.3	3.2	35	1
12431	10675	9800	TILL	B	BROWN	HILLSIDE SE		0.6	23.7	62.2	2.6	14	1
12432	10725	9800	TILL	B	BROWN	HILLSIDE E		1	22.5	69.1	3.7	10	3
12433	10775	9800	TILL	B	BROWN	HILLSIDE E		0.7	14.1	39.2	2.9	10	9
12434	10825	9800	TILL	B	BROWN	HILLSIDE E		0.2	15.1	53.3	1.7	16	3
12435	10875	9800	TILL	B	BROWN	HILLSIDE E		0.6	53.9	57.1	5.9	37	3
12436	10925	9800	TILL	B	BROWN	HILLSIDE E		1.5	166.1	99.1	10	77	4
12437	10975	9800	TILL	B	BROWN	HILLSIDE NE		0.6	15	53	3.4	18	2
12438	11025	9800	TILL	B	BROWN	HILLSIDE SE		0.5	16.9	43.4	2.7	15	10
12439	11075	9800	TILL	B	BROWN	HILLSIDE SE		0.6	16.3	38.6	3.8	19	5
12440	11125	9800	TILL	B	BROWN	HILLSIDE SE		0.9	20.4	35	4.8	28	7
12441	11175	9800	TILL	B	BROWN	HILLSIDE E		0.7	15.1	35.4	4.4	10	2
12442	11225	9800	TILL	B	BROWN	HILLSIDE E	NO SAMPLE TAKEN AT 108+25E.	0.5	8.5	30.2	1.7	10	1

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COPPER KING NORTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
								ppm	ppm	ppm	ppm	ppb	ppb
12443	11275	9800	TILL	B	BROWN	HILLSIDE E		0.4	12.1	41.5	2.5	10	1
12444	11325	9800	TILL	B	BROWN	HILLSIDE SE		0.5	9.1	25.8	1.7	23	2
12445	11375	9800	TILL	B	BROWN	HILLSIDE SE		0.4	10.6	27.6	1.7	10	1
12446	11425	9800	TILL	B	BROWN	HILLSIDE SE		0.7	20.9	156.4	2.9	17	1
12447	11475	9800	TILL	B	BROWN	HILLSIDE NE		0.5	13.9	76.8	2.7	33	1
12448	11525	9800	TILL	B	BROWN	GULLY		0.8	13.1	48	2.9	22	1
12449	11575	9800	TILL	B	BROWN	HILLSIDE SE		1.8	78.5	63.9	3.7	133	2
12450	11675	9800	TILL	B	BROWN	HILLSIDE E		0.9	17.7	78.8	3.5	10	1
12451	11725	9800	TILL	B	BROWN	HILLSIDE E		1	48.1	66.3	11.8	46	2
12452	11775	9800	TILL	B	BROWN	HILLSIDE E	NO SAMPLES AT 114+75, 115+25E DUE TO LARGE SWAMP IN GULLY.	0.6	11.2	32.3	2.8	10	1
12453	11825	9800	TILL	B	GREY	HILLSIDE NE		0.9	10	67.2	2.4	32	1
12454	11875	9800	TILL	B	GREY	HILLSIDE N		1	11	82.2	2.9	32	1
12455	11925	9800	TILL	B	BROWN	HILLSIDE NE		1	10	67.3	1.8	10	1
12456	11975	9800	TILL	B	BROWN	HILLSIDE NE	SAMPLE TAKEN AT 114+00E DUE TO LARGE SWAMP.	1.4	13	69.5	2.5	22	3
12457	12025	9800	TILL	B	BROWN	HILLSIDE NE		0.9	13	58.4	2.8	10	2
12458	12075	9800	TILL	B	BROWN	HILLSIDE NE		0.6	8.4	55.3	1.1	10	7
12459	12125	9800	TILL	B	BROWN	HILLSIDE NE	SAMPLE TAKEN AT 112+35E DUE TO LARGE SWAMP.	1	8.8	48.8	0.9	10	2
12460	12175	9800	TILL	B	BROWN	HILLSIDE NE		0.8	25.7	64.7	4.5	13	7
12461	12225	9800	TILL	B	BROWN	FLAT		0.6	42.7	52	2.2	15	1
12462	12275	9800	TILL	B	BROWN	FLAT		0.6	7.3	41.6	1.2	10	2
12463	12325	9800	TILL	B	BROWN	HILLSIDE NW		0.7	9.2	48.5	1.3	16	1
12464	12375	9800	TILL	B	BROWN	HILLSIDE NE		0.6	10.9	85.8	2.6	13	7
12353	10000	9850	TILL	B	BROWN	FLAT		0.5	17.9	56.3	1.1	12	1
12354	10000	9900	TILL	B	BROWN	FLAT		0.3	8.5	29.2	1	10	1
12355	10000	9950	TILL	B	GREY	FLAT		0.5	14	34.6	1.5	23	9
12069	10000	10000	TILL	B	BROWN	HILLSIDE SE		0.3	8.9	25.5	1.3	12	1
12070	10050	10000	TILL	B	BROWN	HILLSIDE SE		0.3	11.1	31.5	1.8	12	27
12071	10100	10000	TILL	B	BROWN	HILLSIDE SE		0.3	10.7	29.3	1.4	17	57
12072	10150	10000	TILL	B	BROWN	HILLSIDE SE		0.4	12.1	28.7	1.7	15	11
12073	10200	10000	TILL	B	BROWN	HILLSIDE E		0.3	11.2	24.8	3.2	15	1
12074	10250	10000	TILL	B	BROWN	GULLY		0.4	5.7	23.4	1.6	13	1
12075	10300	10000	TILL	B	BROWN	HILLSIDE NE		0.3	4.3	71.1	1.7	11	1
12076	10350	10000	TILL	B	BROWN	HILLSIDE SE		0.3	8.3	36	2.2	17	1
12077	10400	10000	TILL	B	BROWN	HILLSIDE SE		0.5	24.6	536	8.3	28	1
12078	10450	10000	TILL	B	BROWN	HILLSIDE SE		0.5	15.1	37.9	3	10	1
12079	10500	10000	TILL	B	BROWN	HILLSIDE SW		0.9	28.6	88.1	3.5	39	1
12080	10550	10000	TILL	B	BROWN	HILLSIDE NE		0.6	13.1	52.3	1.3	16	5
12081	10600	10000	TILL	B	BROWN	HILLSIDE NE		0.4	10.3	29.3	2.1	14	1
12082	10650	10000	TILL	B	BROWN	HILLSIDE E		0.4	8.4	29.7	1.3	15	18
12083	10700	10000	TILL	B	BROWN	HILLSIDE E		0.3	7.4	27.9	0.9	13	3
12084	10750	10000	TILL	B	BROWN	HILLSIDE E		0.4	14.9	43.2	1.6	20	2
12085	10800	10000	TILL	B	BROWN	HILLSIDE E		0.3	9.3	24.4	1.5	15	1
12086	10850	10000	TILL	B	BROWN	HILLSIDE NE		0.6	15.2	59.3	3.6	26	1
12087	10900	10000	TILL	B	BROWN	HILLSIDE E		0.6	9.5	97.6	3.4	31	1
12088	10950	10000	TILL	B	BROWN	HILLSIDE E		0.4	8.4	40.5	2.2	10	6

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COPPER KING NORTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
								ppm	ppm	ppm	ppm	ppb	ppb
12089	11000	10000	TILL	B	GREY	HILLSIDE E		0.8	21	152	5	12	1
12090	11050	10000	TILL	B	BROWN	HILLSIDE E		0.6	43.9	56.9	26.6	42	1
12091	11100	10000	TILL	B	BROWN	HILLSIDE E		2.1	64.4	84.8	167	63	11
12092	11150	10000	TILL	B	BROWN	HILLSIDE E		1.3	56.4	86.4	101.2	50	1
12093	11200	10000	TILL	B	BROWN	HILLSIDE E		1.3	84.3	52.5	11.8	94	1
12094	11250	10000	TILL	B	BROWN	HILLSIDE NW		0.9	36.3	47.2	7.9	31	1
12095	11300	10000	TILL	B	BROWN	HILLSIDE SW		1	15.3	44.3	4.4	22	2
12096	11350	10000	TILL	B	BROWN	HILLSIDE NE		0.5	6.5	53.3	1.8	16	18
12097	11400	10000	TILL	B	BROWN	HILLSIDE SW		0.3	10.8	22.4	1.7	18	1
12098	11450	10000	TILL	B	BROWN	HILLSIDE E		0.3	11.9	32.1	0.8	18	1
12099	11500	10000	TILL	B	BROWN	HILLSIDE E		0.3	8.4	21.3	1.4	15	1
12100	11550	10000	TILL	B	BROWN	HILLSIDE E		0.5	8.7	39.4	0.8	10	2
12401	11600	10000	TILL	B	BROWN	HILLSIDE SE		0.9	96.8	92.6	2.9	29	3
12402	11650	10000	TILL	B	BROWN	HILLSIDE SE	SAMPLE TAKEN 17M S/E OF STATION DUE TO SWAMP.	0.6	19.6	36.7	1.8	20	1
12403	11700	10000	TILL	B	BROWN	HILLSIDE SE	SAMPLE TAKEN 15M SE DUE TO SWAMP.	0.9	46	52.9	4.5	39	4
12404	11750	10000	TILL	B	BROWN	HILLSIDE SE	SAMPLE TAKEN 10M SE DUE TO SWAMP.	0.6	18.3	61	1.4	10	1
12405	11800	10000	TILL	B	BROWN	HILLSIDE SE		0.7	14.6	66.7	1.7	10	1
12406	11850	10000	TILL	B	BROWN	HILLSIDE SE		0.2	10.6	35.8	1.3	10	4
12407	11900	10000	TILL	B	BROWN	HILLSIDE E		0.5	15.9	52	0.9	10	1
12408	11950	10000	TILL	B	BROWN	HILLSIDE NE		0.2	9.1	25.5	0.8	15	6
12409	12000	10000	TILL	B	BROWN	HILLSIDE NE		0.4	19.5	54.7	1.8	19	3
12410	12050	10000	TILL	B	BROWN	HILLSIDE E		0.4	10.6	40.8	1.4	10	4
12411	12100	10000	TILL	B	BROWN	HILLSIDE E		0.4	10.8	52.3	1.4	22	2
12412	12150	10000	TILL	B	BROWN	HILLSIDE SE		0.3	13.4	31.6	1.8	21	4
12413	12200	10000	TILL	B	BROWN	HILLSIDE E		0.4	6.9	33.7	1.5	10	2
12414	12250	10000	TILL	B	BROWN	HILLSIDE SE		0.4	10	32.6	2.3	10	1
12415	12300	10000	TILL	B	BROWN	HILLSIDE SE		0.4	10.2	39	1.5	10	3
12416	12350	10000	TILL	B	BROWN	HILLSIDE SE		0.5	10.4	106.8	1.4	14	48
12417	12400	10000	TILL	B	BROWN	HILLSIDE SE		0.4	6	28.2	1	10	5
12356	10000	10050	TILL	B	GREY	FLAT		0.4	8.4	29.4	1	13	3
12357	10000	10100	TILL	B	BROWN	FLAT		0.4	7.7	34.8	0.8	11	3
12358	10000	10150	TILL	B	BROWN	HILLSIDE SE		0.4	8	30	0.7	10	4
13032	10000	10200	TILL	B	BROWN	FLAT		0.4	12.6	36.5	1.9	10	5
13033	10050	10200	TILL	B	BROWN	FLAT		0.5	22.9	50.8	0.7	24	3
13034	10100	10200	TILL	B	BROWN	FLAT		0.6	42.7	47.6	1.3	28	3
13035	10150	10200	TILL	B	BROWN	FLAT		0.7	191.1	93.4	4.7	36	3
13036	10200	10200	TILL	B	ORANGE	FLAT		0.5	29.4	56.4	1.9	13	1
13037	10250	10200	TILL	B	BROWN	FLAT		1	18.3	75.7	3.6	59	1
13038	10300	10200	TILL	B	BROWN	FLAT		0.3	11	63.2	0.8	10	1
13039	10350	10200	TILL	B	BROWN	FLAT	SAMPLE TAKEN AT 115+50E IN SMALL GULLY DUE TO OUTCROP.	0.6	48.5	92.3	1.2	31	2
13040	10400	10200	TILL	B	BROWN	FLAT		0.5	43	56.2	1.2	26	2
13041	10450	10200	TILL	B	BROWN	FLAT	SAMPLE TAKEN AT 116+15E.	1.2	70.6	60.5	3.9	29	4
12500	10475	10200	TILL	B	BROWN	HILLSIDE SW		1.4	26.6	69.9	3.6	67	1
12499	10525	10200	TILL	B	BROWN	HILLSIDE NE		0.7	20	64.1	2	33	10

COPPER KING NORTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
								ppm	ppm	ppm	ppm	ppb	ppb
12498	10575	10200	TILL	B	BROWN	HILLSIDE SW		0.8	17.8	50.8	1.5	27	4
12497	10625	10200	TILL	B	BROWN	HILLSIDE SE		0.6	14.6	35.1	2.6	28	1
12496	10675	10200	TILL	B	BROWN	HILLSIDE NE		1.4	36.8	183.5	31.1	33	1
12495	10725	10200	TILL	B	BROWN	HILLSIDE NE		0.6	45.6	37.7	8.6	23	1
12494	10775	10200	TILL	B	BROWN	HILLSIDE NE	SAMPLE TAKEN AT 119+65E.	0.9	58.7	89.6	17	32	1
12493	10875	10200	TILL	B	BROWN	HILLSIDE SE		1.4	119	101.2	6.2	38	1
12492	10925	10200	TILL	B	BROWN	HILLSIDE SE		0.8	17.4	135.7	2.2	32	1
12491	10975	10200	TILL	B	BROWN	HILLSIDE SE		2	7.9	53.6	3.2	106	1
12490	11025	10200	TILL	B	BROWN	HILLSIDE SE		1.4	31.2	143.1	2.3	126	1
12489	11075	10200	TILL	B	BROWN	HILLSIDE SE		0.8	33.8	65.1	1.1	38	1
12488	11125	10200	TILL	B	BROWN	FLAT		1	14.7	64.2	2.2	36	1
12487	11175	10200	TILL	B	BROWN	FLAT		0.9	39.5	70.5	1.2	49	2
12486	11225	10200	TILL	B	BROWN	HILLSIDE SE		2.1	10	65.5	4.1	108	1
12485	11275	10200	TILL	B	BROWN	HILLSIDE SE		0.8	14.9	35.7	2.6	12	1
12484	11325	10200	TILL	B	BROWN	HILLSIDE SE		0.6	11.3	19.6	2.2	10	1
12483	11375	10200	TILL	B	BROWN	HILLSIDE SE		0.7	27.4	32.7	2.2	25	2
12482	11425	10200	TILL	B	BROWN	HILLSIDE SE		0.5	19.2	24.5	4.4	38	1
12481	11475	10200	TILL	B	BROWN	HILLSIDE SE	WEST SIDE.	0.6	23.8	42.8	3.9	26	2
12480	11525	10200	TILL	B	BROWN	HILLSIDE SE	ROCKY.	0.6	13.7	27.2	2.2	14	6
12479	11575	10200	TILL	B	GREY	HILLSIDE SE		0.9	21.5	100	3.6	33	3
12478	11625	10200	TILL	B	BROWN	HILLSIDE SE		0.6	13.6	42.7	2	16	2
12477	11675	10200	TILL	B	BROWN	HILLSIDE SE		0.8	19.9	76.6	3.7	44	1
12476	11725	10200	TILL	B	BROWN	HILLSIDE SE		0.9	39.9	69.3	4	48	3
12475	11775	10200	TILL	B	BROWN	HILLSIDE SE	ROUNDED QUARTZ PEBBLES IN SOIL.	0.5	11.8	25	1.9	15	1
12474	11825	10200	TILL	B	BROWN	HILLSIDE SE		0.4	11.8	25.6	1.4	13	1
12473	11875	10200	TILL	B	BROWN	HILLSIDE SE		0.6	15.9	59.3	3.2	17	2
12472	11925	10200	TILL	B	BROWN	HILLSIDE SE	SMALL GULLY.	0.6	19.6	44.5	3	15	18
12471	11975	10200	TILL	B	BROWN	HILLSIDE SE		0.3	12.1	26.9	1.6	21	1
12470	12025	10200	TILL	B	BROWN	HILLSIDE SE		0.4	8.7	24.4	0.5	13	1
12469	12075	10200	TILL	B	BROWN	HILLSIDE SE	NEXT TO ROAD.	0.6	12.5	76.3	1.4	23	2
12468	12175	10200	TILL	B	BROWN	HILLSIDE SE	WET AREA.	1.2	114.6	155.6	5	78	1
12467	12225	10200	TILL	B	BROWN	HILLSIDE SE		0.9	20.4	89.3	5.3	58	1
12466	12275	10200	TILL	B	BROWN	HILLSIDE SE		0.9	15	89.8	3.3	49	1
12465	12375	10200	TILL	B	BROWN	HILLSIDE SE		0.8	21.9	48.8	2.8	40	4
12359	10000	10250	TILL	B	ORANGE	FLAT		0.8	40.3	100.5	3.6	42	1
12360	10000	10300	TILL	B	BROWN	FLAT		0.9	38.3	90.4	3.9	45	1
12361	10000	10350	TILL	B	BROWN	FLAT		0.5	14.5	41.5	2.2	34	8
12782	10000	10400	TILL	B	BROWN	FLAT		0.5	16.4	47.6	2.6	15	3
12781	10050	10400	TILL	B	ORANGE	FLAT	SANDY SOIL.	0.4	17.8	21.5	1.9	32	1
12780	10100	10400	TILL	B	BROWN	FLAT		0.5	16.1	28.6	2.9	24	2
12779	10150	10400	TILL	B	BROWN	HILLSIDE SW	OUTCROP IN AREA.	0.6	15.9	32.4	3.2	10	1
12778	10200	10400	TILL	B	GREY	FLAT		0.6	10	87.5	2.8	23	1
12777	10250	10400	TILL	B	BROWN	FLAT	VERY ROCKY.	0.7	18.7	59.6	2.1	29	1
12776	10300	10400	TILL	B	BROWN	HILLSIDE E		0.5	10.9	49.7	2.4	26	46
12775	10350	10400	TILL	B	ORANGE	FLAT		0.5	12.4	45.9	3	19	7
12774	10400	10400	TILL	B	BROWN	HILLSIDE SW	SMALL DEPRESSION.	0.4	7.5	37.2	1.6	10	1
12773	10450	10400	TILL	B	BROWN	FLAT	OUTCROP STARTING AT 94+75E.	0.5	6.4	68.4	1.1	14	1

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COPPER KING NORTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
								ppm	ppm	ppm	ppm	ppb	ppb
12772	10500	10400	TILL	B	BROWN	FLAT	OUTCROP END AT 105+45 E.	0.6	8.8	38.4	1.5	38	1
12771	10550	10400	TILL	B	BROWN	HILLTOP	WEST SIDE OF GULLY.	0.5	9.1	59.2	1.9	26	1
12770	10600	10400	TILL	B	BROWN	HILLSIDE W	NORTH SIDE.	0.7	27.9	70.6	3.8	21	1
12769	10650	10400	TILL	B	BROWN	HILLSIDE NW	TRACE ANGULAR ROCK FRAGMENT.	0.7	10.5	58.6	1.4	13	1
12768	10700	10400	TILL	B	BROWN	FLAT		0.5	23.7	67.8	2.9	18	1
12767	10750	10400	TILL	B	BROWN	HILLSIDE SE		0.5	15.7	89.3	1.9	11	1
12766	10800	10400	TILL	B	BROWN	FLAT		0.6	20.4	132.2	2.4	22	2
12765	10850	10400	TILL	B	ORANGE	FLAT	BOTTOM OF GULLY.	0.5	17.5	44.6	2.1	16	1
12764	10900	10400	TILL	B	ORANGE	FLAT	BOTTOM OF GULLY. WET AREA.	1.3	281.2	135.9	8.9	123	4
12763	10950	10400	TILL	B	BROWN	FLAT		0.6	17.5	28.8	1.5	10	1
12762	11000	10400	TILL	B	BROWN	FLAT		0.5	13.1	33.7	1.9	10	99
12761	11050	10400	TILL	B	BROWN	FLAT		0.4	7.1	24.3	0.7	15	1
12760	11100	10400	TILL	B	ORANGE	FLAT		0.5	11.4	39.3	2.2	20	1
12759	11150	10400	TILL	B	BROWN	FLAT		0.4	13	40.9	2.1	16	67
12758	11200	10400	TILL	B	BROWN	FLAT		0.6	16	30.9	2.6	21	1
12757	11250	10400	TILL	B	BROWN	FLAT		0.5	9.6	29.1	1.3	20	1
12756	11300	10400	TILL	B	BROWN	HILLSIDE E		0.3	10.5	22	2.2	13	1
12755	11350	10400	TILL	B	BROWN	FLAT		0.5	17.2	49.3	1.1	22	3
12754	11400	10400	TILL	B	ORANGE	HILLTOP		1.1	19.7	101.1	3.5	10	1
12753	11450	10400	TILL	B	BROWN	FLAT		0.7	8.9	41.7	1.6	16	1
12752	11500	10400	TILL	B	BROWN	HILLSIDE SE		0.8	11.7	100.5	2	10	1
12751	11550	10400	TILL	B	BROWN	HILLSIDE S		1	19.2	111.8	3.2	57	2
12750	11600	10400	COLLUVIUM/ TILL	B	BROWN	HILLSIDE SE		0.7	13.5	40.1	1.8	26	1
12749	11650	10400	COLLUVIUM	B	BROWN	HILLTOP		1.8	81.9	137.3	10	78	1
12748	11700	10400	COLLUVIUM/ ORGANIC	B	BROWN	HILLSIDE SE		0.4	9.7	21.1	1.4	11	1
12747	11750	10400	COLLUVIUM	B	BROWN	HILLSIDE S		0.3	8.7	27.7	0.7	12	1
12746	11800	10400	TILL	B	BROWN	HILLSIDE E		0.7	10.1	82.6	4.2	13	4
12745	11850	10400	TILL	B	BROWN	HILLSIDE E		0.6	17.4	53.4	4.1	10	1
12744	11900	10400	TILL	B	BROWN	HILLSIDE S		0.3	58.8	60	3.5	16	3
12743	11950	10400	TILL	B	BROWN	HILLSIDE SE		0.6	9.5	36.4	1.1	10	2
12742	12000	10400	TILL	B	BROWN	HILLSIDE SE		0.7	14.2	29.2	3.4	12	5
12741	12050	10400	TILL	B	BROWN	HILLSIDE S		0.5	11.7	57.1	2.2	11	1
12740	12100	10400	COLLUVIUM	B	BROWN	HILLSIDE SE		0.4	5.5	24.1	0.7	10	1
12739	12150	10400	COLLUVIUM	B	BROWN	HILLSIDE SE		0.4	11.5	40.1	0.8	12	4
12738	12200	10400	COLLUVIUM	B	BROWN	HILLSIDE SE	TOP OF WEST BANK OF BIG GULLY.	0.8	21.2	39.1	3.8	14	5
12737	12250	10400	COLLUVIUM	B	BROWN	HILLSIDE SE		0.7	14.9	45.3	1.9	28	47
12736	12300	10400	COLLUVIUM	B	BROWN	HILLSIDE SE	SAMPLE TAKEN AT BASE OF SLOPE 115+10E, 10ME OF LINE, CREEK.	1.1	41.9	99	6.1	29	4
12735	12350	10400	COLLUVIUM	B	BROWN	HILLSIDE SE	BASE OF SLOPE.	1	21	63.3	4.2	10	1
12734	12400	10400	COLLUVIUM	B	BROWN	HILLSIDE SE		1	68.6	102.3	5.1	51	1
12362	10000	10450	TILL	B	BROWN	FLAT		0.6	28	49.8	4.4	10	1
12363	10000	10500	TILL	B	BROWN	FLAT		0.6	10.2	77.9	2.9	20	1
12364	10000	10550	TILL	B	GREY	HILLSIDE SE		0.7	13.6	56.5	3.1	35	1

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COPPER KING NORTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
								ppm	ppm	ppm	ppm	ppb	ppb
12548	10000	10600	TILL	B	BROWN	FLAT	ROCKY SITE.	0.8	31.1	54	2.1	33	3
12549	10025	10600	TILL	B	BROWN/GREY	FLAT	ROCKY SITE.	0.8	43.1	114	1.9	37	3
12550	10075	10600	TILL	B	BROWN/GREY	FLAT	ROCKY SITE.	1.2	30.9	104.7	2	87	1
12551	10125	10600	TILL	B	BROWN	HILLSIDE E	ROCKY SITE.	1.2	15.3	61.2	1	61	1
12552	10175	10600	TILL	TOPSOIL	BLACK	GULLY	ROCKY SITE.	1.3	528.2	58.7	1.4	59	2
12553	10225	10600	TILL	B	BROWN	GULLY	ROCKY SITE.	1.4	20.4	66.8	2.1	30	1
12554	10275	10600	TILL	B	BROWN	GULLY	ROCKY SITE.	0.7	14.7	64.7	1.1	23	1
12555	10325	10600	TILL	B	BROWN	GULLY		0.7	20.8	79.6	2.8	20	1
12556	10375	10600	TILL	B	BROWN	GULLY		1	29.2	102.9	6.9	46	1
12557	10425	10600	TILL	B	BROWN	FLAT		0.7	21	123.6	3.6	24	1
12558	10475	10600	TILL	B	BROWN	FLAT		0.8	14.2	51.8	3	13	1
12559	10525	10600	TILL	B	BROWN	FLAT		0.6	8.2	36.5	1.3	10	5
12560	10575	10600	TILL	B	BROWN	FLAT	SAMPLE TAKEN AT 117+80 DUE TO CONTINUOUS OUTCROP. ROCKY.	0.8	16.1	50.6	3.6	12	2
12561	10625	10600	TILL	B	BROWN	FLAT	ROCKY. OUTCROP IN AREA.	1.2	66.1	143.5	1.9	75	1
12562	10675	10600	TILL	B	BROWN	FLAT	ROCKY. OUTCROP IN AREA.	0.9	24.7	92.7	1.1	26	1
12563	10725	10600	TILL	B	BROWN	FLAT	ROCKY SITE.	1.1	209.2	103.6	3.3	34	1
12564	10775	10600	TILL	B	BROWN/GREY	FLAT	ROCKY SITE.	0.6	18.8	41.9	1.4	14	3
12565	10825	10600	TILL	B	BROWN	FLAT	ROCKY. OUTCROP IN AREA.	0.3	12.1	58.8	1.1	10	1
12566	10875	10600	TILL	B	BROWN	FLAT		0.6	35.2	56.5	3	20	1
12567	10925	10600	TILL	B	BROWN	FLAT		0.6	24.8	50.4	1.5	36	1
12568	10975	10600	TILL	B	BROWN	FLAT		0.6	20.9	91.7	2.5	23	3
12569	11025	10600	TILL	B	BROWN	FLAT		0.5	10.3	46	1.4	10	1
12570	11075	10600	TILL	B	BROWN	FLAT		0.5	15.6	33.1	1.3	18	1
12571	11125	10600	TILL	B	BROWN	FLAT		0.5	14	54.3	0.5	10	3
12572	11175	10600	TILL	B	BROWN	FLAT	WET SAMPLE.	0.8	133.1	61.8	2.6	30	2
12573	11225	10600	TILL	B	BROWN	FLAT		0.9	65.3	82.7	3.9	37	1
12574	11275	10600	TILL	B	BROWN	FLAT		0.6	15	87	1.6	10	1
12575	11325	10600	TILL	B	BROWN	HILLSIDE SW		0.5	21.1	54.1	1.3	13	1
12576	11375	10600	TILL	B	BROWN	HILLSIDE S		0.3	9.9	29.7	0.7	17	4
12577	11425	10600	TILL	B	BROWN	HILLSIDE S		0.4	10.3	43.4	1.3	11	3
12578	11475	10600	TILL	B	BROWN	HILLSIDE SE		0.6	9.8	48	1.1	23	7
12579	11525	10600	TILL	B	BROWN	GULLY		0.8	14.8	84.4	2.9	38	1
12580	11575	10600	TILL	B	BROWN	GULLY		0.4	14.1	39.8	0.9	10	1
12581	11625	10600	TILL	B	BROWN	HILLSIDE W		0.7	33.9	169.8	2.7	21	1
12582	11675	10600	TILL	B	BROWN	HILLSIDE E		0.8	64.2	103	2.3	10	1
12583	11725	10600	TILL	B	BROWN	FLAT		0.6	26.4	40.5	3.2	10	1
12584	11775	10600	TILL	B	BROWN	FLAT		0.6	60.7	260.2	2.6	16	38
12585	11825	10600	TILL	B	BROWN	FLAT	SMALL RIDGETOP. SUBCROP IN AREA.	0.6	118.2	1217.6	9.5	74	1
12586	11875	10600	TILL	B	BROWN	HILLSIDE S		1	79.9	92.8	4.8	56	2
12587	11925	10600	TILL	B	BROWN	HILLSIDE S		0.5	22.7	111.7	2.7	12	1
12588	11975	10600	TILL	B	BROWN	HILLSIDE SE	GULLY.	0.7	13.7	71	1.9	10	1
12589	12025	10600	TILL	B	BROWN	HILLSIDE E		0.7	10.9	108.1	1.7	23	1
12590	12075	10600	TILL	B	BROWN	FLAT		0.6	18.3	62.3	2.4	18	1
12591	12125	10600	TILL	B	BROWN	HILLSIDE SE		0.5	9.3	26.3	1.3	10	3
12592	12175	10600	TILL	B	BROWN	HILLSIDE N		0.5	9.2	32	1	10	1
12593	12225	10600	TILL	B	BROWN	HILLSIDE NE		0.7	16.9	65.7	3.3	10	1

COPPER KING NORTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
								ppm	ppm	ppm	ppm	ppb	ppb
12594	12275	10600	TILL	B	BROWN	GULLY	SAMPLE TAKEN AT 100+90E DUE TO SWAMP.	0.6	11.8	53.9	1.2	17	2
12595	12325	10600	TILL	B	BROWN	FLAT		1.1	13.6	76.2	3.2	47	1
12596	12375	10600	TILL	B	BROWN	FLAT		0.7	13.7	69.4	2.9	36	1
12365	10000	10650	TILL	B	BROWN	FLAT		0.6	10.8	50.6	4.5	10	1
12366	10000	10700	TILL	B	BROWN	FLAT		1.8	50.6	122.6	25.7	75	1
12367	10000	10750	TILL	B	BROWN	FLAT		0.7	17.7	41.7	4.7	10	1
13010	10000	10800	TILL	B	BROWN	FLAT		1	18.3	159.4	3.1	15	1
13011	10050	10800	TILL	B	BROWN	FLAT		0.8	7.7	38.7	1.1	16	1
13012	10100	10800	TILL	B	BROWN	FLAT		0.8	11.1	115.5	1.1	26	1
13013	10150	10800	TILL	B	BROWN	FLAT		0.8	11.6	75.8	2	12	4
13014	10200	10800	TILL	B	BROWN	FLAT	SAMPLE TAKEN AT 116+15E DUE TO OUTCROP.	0.7	19.1	96.7	2.2	14	2
13015	10250	10800	TILL	B	GREY	FLAT	ROCKY. OUTCROP.	1.2	52.6	69.5	5.3	62	2
13016	10300	10800	TILL	B	BROWN	FLAT	ROCKY. OUTCROP.	0.7	24.8	40.8	2.9	15	1
13017	10350	10800	TILL	B	BROWN	FLAT	ROCKY.	0.4	25.6	39.9	3	19	1
13018	10400	10800	TILL	B	BROWN	FLAT		0.6	41.1	49.5	1.7	12	2
13019	10450	10800	TILL	B	BROWN	FLAT		0.6	39.8	50.5	1.2	10	1
13020	10500	10800	TILL	B	BROWN	FLAT		0.5	76.6	80.5	1.9	16	4
13021	10550	10800	TILL	B	BROWN	FLAT		0.6	32.3	63.1	2.7	39	1
13022	10600	10800	TILL	B	BROWN	HILLSIDE SE		0.5	13	53.9	1.4	11	1
13023	10650	10800	TILL	B	BROWN	HILLSIDE SE		0.5	20.2	38.6	2.1	24	1
13024	10700	10800	TILL	B	BROWN	HILLSIDE S		0.4	11.6	32.2	1.2	10	1
13025	10750	10800	TILL	B	BROWN	HILLSIDE SE		0.3	7.6	22	1.1	10	1
13026	10800	10800	TILL	B	BROWN	HILLSIDE S		0.4	8.9	24.9	1.1	10	6
13027	10850	10800	TILL	B	BROWN	HILLSIDE S		0.3	11.1	30.2	2.3	10	1
13028	10900	10800	TILL	B	BROWN	HILLSIDE SE		0.8	35.8	65.2	2.2	33	1
13029	10950	10800	TILL	B	GREY	HILLSIDE SE		0.7	21.9	47.1	1.7	12	1
13030	11000	10800	TILL	B	BROWN	HILLSIDE SE		0.3	13.2	38.2	1.2	10	3
13031	11050	10800	TILL	B	BROWN	HILLSIDE SE		0.5	21.3	53.1	2	30	1
12800	11100	10800	TILL	B	GREY	HILLSIDE E		0.3	12.3	25.6	1.8	10	1
12799	11150	10800	TILL	B	BROWN	HILLSIDE E		0.6	36.9	57.4	5.5	58	2
12798	11200	10800	TILL	B	BROWN	HILLSIDE SE		0.5	15.2	56.2	1.2	17	1
12797	11250	10800	TILL	B	BROWN	HILLSIDE SE		0.4	12.9	51.5	1.1	22	3
12796	11300	10800	TILL	B	BROWN	HILLSIDE SW		0.6	11.4	42.7	1.3	10	2
12795	11350	10800	TILL	B	BROWN	HILLSIDE S		0.7	9.5	32.9	1.7	12	1
12794	11400	10800	TILL	B	BROWN	HILLSIDE S		0.5	10.9	30.8	1.9	11	1
12793	11450	10800	TILL	B	GREY	HILLSIDE SW		0.3	4.5	36.9	1.6	15	2
12792	11500	10800	TILL	B	GREY	HILLSIDE SW		0.6	4.8	231.1	1.1	40	1
12791	11550	10800	TILL	B	ORANGE	HILLSIDE N		0.3	3.7	27.3	1.2	10	1
12790	11600	10800	TILL	B	BROWN	HILLSIDE NE		1.7	153.3	77	5.6	47	3
12789	11650	10800	TILL	B	ORANGE	HILLSIDE NE		0.8	51.7	41.4	2.8	19	1
12788	11700	10800	TILL	B	BROWN	FLAT		0.6	21.9	62.9	4	24	2
12787	11750	10800	TILL	B	BROWN	HILLSIDE NE		0.5	11	29.2	3.4	13	1
12786	11800	10800	TILL	B	ORANGE	FLAT		0.3	4.8	32.8	1.9	10	1
12785	11850	10800	TILL	B	BROWN	FLAT		0.5	8.9	33.8	1	10	1
12784	11900	10800	TILL	B	BROWN/ORANGE	FLAT		0.5	12.6	38.7	3.5	10	2
12783	11950	10800	TILL	B	ORANGE	HILLSIDE S		0.9	26	74.8	3.8	31	2

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COPPER KING NORTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
								ppm	ppm	ppm	ppm	ppb	ppb
13009	12000	10800	TILL	B	BROWN	FLAT		0.8	61.8	51.6	5.5	10	8
13008	12050	10800	COLLUVIUM/ TILL	B	BROWN	FLAT		1.9	234.2	117.6	8.5	53	1
13007	12100	10800	TILL	B	BROWN	HILLSIDE NE		1.1	37.2	60.1	5.3	46	1
13006	12150	10800	TILL	B	ORANGE	HILLSIDE SE		0.9	27.1	83.1	5.7	23	1
13005	12200	10800	COLLUVIUM/ TILL	B	BROWN	FLAT		0.6	74.4	70.2	6.3	20	1
13004	12250	10800	TILL	B	BROWN	HILLSIDE E		1.4	14.3	255.8	10.8	11	2
13003	12300	10800	TILL	B	BROWN	HILLSIDE E		0.4	14.1	38.2	5.1	24	1
13002	12350	10800	TILL	B	BROWN	FLAT		0.7	27	35.5	4.5	22	3
13001	12400	10800	TILL	B	BROWN	FLAT		0.4	6.4	43.3	2	10	3
12368	10000	10850	TILL	B	BROWN	FLAT		1.1	40.6	51	12.1	26	1
12369	10000	10900	TILL	B	BROWN	FLAT		1	71	91.3	20.8	31	1
12370	10000	10950	TILL	B	BROWN	FLAT		1.3	50.1	82.6	17.6	35	2
12597	10000	11000	TILL	B	BROWN	FLAT		1.2	29.8	85.9	7.1	35	1
12598	10025	11000	TILL	B	BROWN	FLAT		0.5	20.1	67.8	11.4	24	4
12599	10075	11000	TILL	B	BROWN	FLAT		0.6	10.5	56.6	4.7	20	2
12600	10125	11000	TILL	B	BROWN	FLAT		0.5	13	48.1	5.2	16	2
12801	10175	11000	TILL	B	BROWN	FLAT		1.4	35	137.7	9.4	66	1
12802	10225	11000	TILL	B	BROWN	FLAT		1.2	31.2	79.3	3.3	46	1
12803	10275	11000	TILL	B	BROWN	FLAT		1.5	34.3	68.4	3.4	48	1
12804	10325	11000	TILL	B	BROWN	FLAT		0.5	9.4	147.5	1.6	13	1
12805	10375	11000	TILL	B	BROWN	FLAT	OUTCROP IN AREA.	1.6	542.2	111.4	6.2	83	1
12806	10425	11000	TILL	B	BROWN	FLAT	ROCKY SAMPLE. OUTCROP IN AREA.	1	7.6	45.9	1.4	30	1
12807	10475	11000	TILL	B	BROWN	FLAT	ROCKY SAMPLE. OUTCROP IN AREA.	1.1	179.9	48.9	2.9	17	1
12808	10525	11000	TILL	B	BROWN	FLAT	ROCKY SAMPLE. OUTCROP IN AREA.	1.6	62.8	214.6	3.3	44	4
12809	10575	11000	TILL	B	BROWN	FLAT	ROCKY SAMPLE. OUTCROP IN AREA.	1.1	39.4	88.5	4.1	41	1
12810	10625	11000	TILL	B	BROWN	FLAT	OUTCROP IN AREA.	1.1	46.5	73.1	5	26	1
12811	10675	11000	TILL	B	BROWN	FLAT	OUTCROP IN AREA.	0.8	22.6	57.3	4.4	32	1
12812	10725	11000	TILL	B	BROWN	FLAT	OUTCROP IN AREA.	0.6	10.2	57.9	1.3	23	2
12813	10775	11000	TILL	B	BROWN	FLAT	SAMPLE TAKEN AT 119+90E DUE TO OUTCROP.	0.9	48.3	58.4	12.3	27	5
12814	10825	11000	TILL	B	BROWN	FLAT		0.4	13.2	32.4	1.5	27	1
12815	10875	11000	TILL	B	BROWN	FLAT		0.2	7.3	19.9	1.4	10	1
12816	10925	11000	TILL	B	BROWN	FLAT		0.4	10.9	24	2.1	14	1
12817	10975	11000	TILL	B	BROWN	HILLSIDE S		0.8	43.3	80.9	3.2	51	1
12818	11025	11000	TILL	B	BROWN	HILLSIDE S		0.6	10.3	33.2	0.8	10	1
12819	11075	11000	TILL	B	BROWN	HILLSIDE S		0.4	8.4	18.8	1.1	10	1
12820	11125	11000	TILL	B	BROWN	HILLSIDE SE		0.3	8.7	31.1	0.6	10	1
12821	11175	11000	TILL	B	BROWN	HILLSIDE SE		0.5	16.3	50.1	1.3	22	1
12822	11225	11000	TILL	B	BROWN	HILLSIDE SE		0.6	12.7	41.7	0.7	11	1
12823	11275	11000	TILL	B	BROWN	HILLSIDE SE		0.4	10.7	32.5	0.9	22	2
12824	11325	11000	TILL	B	BROWN	HILLSIDE SE		0.6	7.3	38.9	1	10	1
12825	11375	11000	TILL	B	BROWN	HILLSIDE SE		0.4	13.5	56.5	1	20	1

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COPPER KING NORTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
								ppm	ppm	ppm	ppm	ppb	ppb
12826	11425	11000	TILL	B	BROWN	HILLSIDE E		0.4	6.3	22.2	0.5	10	15
12827	11475	11000	TILL	B	BROWN	GULLY		0.5	13.2	55.6	2.3	10	3
12828	11525	11000	TILL	B	BROWN	HILLSIDE SW		0.5	11	41.6	0.9	10	1
12829	11575	11000	TILL	B	BROWN	HILLSIDE NE		0.7	35.7	54.7	3.6	32	1
12830	11625	11000	TILL	B	BROWN	FLAT		0.6	11.5	32.9	2	11	1
12831	11675	11000	TILL	B	BROWN	HILLSIDE NE		0.5	10.3	53.4	0.9	10	5
12832	11725	11000	TILL	B	BROWN	FLAT		0.5	13.1	26	1.8	10	1
12833	11775	11000	TILL	B	BROWN	HILLSIDE SE		0.7	10.6	38.4	1.3	11	1
12834	11825	11000	TILL	B	BROWN	HILLSIDE SE		0.5	17.2	30.4	2.4	10	1
12835	11875	11000	TILL	B	BROWN	FLAT		0.7	11.1	32.5	2	13	5
12836	11925	11000	TILL	B	BROWN	FLAT		0.3	8.8	22.2	1.6	15	1
12837	11975	11000	TILL	B	BROWN	HILLSIDE SE		0.4	9.2	32.7	1.9	16	2
12838	12025	11000	TILL	B	BROWN	HILLSIDE S		0.5	13	40.6	3.3	12	1
12839	12075	11000	TILL	B	BROWN	HILLSIDE SE	ORGANIC RICH.	1.1	93.9	93.1	4.7	58	2
12840	12125	11000	TILL	B	BROWN	FLAT		0.8	16.3	73.6	4.3	21	1
12841	12175	11000	TILL	B	BROWN	HILLSIDE W		0.5	15.4	92.6	2.7	20	14
12842	12225	11000	TILL	B	BROWN	FLAT	ROCKY SAMPLE. OUTCROP IN AREA.	0.9	19.4	23.5	0.6	29	2
12843	12275	11000	TILL	B	BROWN	FLAT	OUTCROP IN AREA.	0.4	41.9	93.3	3	10	1
12844	12325	11000	TILL	B	BROWN	FLAT		0.6	10	36	1.2	10	2
12845	12375	11000	TILL	B	BROWN	FLAT		0.7	16.4	55.5	2.2	22	1

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GEOCHEMICAL EXTRACTION-ANALYSIS CERTIFICATE

Crest Geological Consulting PROJECT 177 File # 9801830 Page 1

2197 Park Crescent, Coquitlam BC V3J 6T1 Submitted by: R. Roe

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12069	.7	9.6	3.8	70.5	122	21	7	154	1.98	2.3	<5	<2	16	.17	.3	<.2	47	.22	.127	6	26	.18	126	.06	<3	1.44	.01	.03	<2	<.2	35	<.3	<.2	4.3	<1
12070	.6	14.6	4.6	107.5	117	30	10	260	2.35	1.7	<5	<2	15	.14	.2	<.2	43	.22	.099	7	30	.39	138	.05	<3	1.98	.01	.05	<2	<.2	24	<.3	<.2	5.0	2
12071	.9	20.1	4.0	137.5	240	19	10	687	2.25	2.2	<5	2	16	.34	.3	<.2	46	.22	.152	6	29	.27	150	.05	<3	1.70	.01	.05	<2	<.2	42	<.3	<.2	4.2	1
12072	.8	11.0	4.4	91.0	54	19	7	274	2.29	3.7	<5	<2	19	.16	.4	<.2	53	.32	.161	7	32	.23	113	.07	4	1.59	.01	.05	<2	<.2	16	<.3	<.2	5.3	<1
12073	.5	10.6	4.0	46.4	<30	13	4	153	1.37	2.2	<5	<2	18	.10	.3	<.2	38	.27	.047	7	23	.24	79	.07	<3	.80	.01	.03	<2	<.2	19	<.3	<.2	3.2	<1
12074	.8	46.1	2.9	80.1	158	29	15	1306	3.32	2.0	<5	<2	29	.25	.2	<.2	81	.52	.029	10	32	1.00	161	.03	<3	2.48	.01	.09	<2	<.2	35	<.3	<.2	6.6	1
12075	1.0	12.6	4.5	78.4	74	11	7	201	2.45	3.2	<5	<2	17	.26	.3	<.2	55	.29	.163	4	26	.32	166	.06	<3	1.32	.01	.04	<2	<.2	11	<.3	<.2	5.6	1
12076	1.1	62.1	6.5	132.5	221	75	18	956	4.21	6.4	<5	<2	44	.28	.5	<.2	86	.73	.063	14	80	.87	304	.06	<3	3.53	.01	.13	<2	<.2	64	<.3	<.2	6.6	2
12077	.5	10.9	4.0	33.5	46	13	4	143	1.28	2.4	<5	<2	20	.09	.4	<.2	38	.32	.032	7	23	.26	58	.08	<3	.77	.01	.03	<2	<.2	19	<.3	<.2	2.9	<1
12078	.6	8.6	4.4	49.2	75	9	4	326	1.26	2.8	<5	<2	19	.20	.4	<.2	39	.30	.033	6	21	.17	75	.07	<3	.69	.01	.04	<2	<.2	<10	<.3	<.2	2.7	1
12079	.6	3.7	2.4	222.6	<30	14	24	1128	3.57	1.1	<5	<2	18	.02	.4	<.2	75	.32	.008	1	15	2.06	134	.22	<3	2.63	.01	.18	<2	<.2	14	<.3	<.2	7.2	1
12080	.5	8.4	5.5	186.9	34	13	16	826	3.13	3.3	<5	<2	14	.09	.4	<.2	85	.27	.067	3	19	1.09	138	.17	<3	2.46	.01	.11	<2	<.2	21	<.3	<.2	6.7	3
12081	.5	5.4	4.3	185.4	33	21	16	809	3.90	2.3	<5	<2	13	.07	.3	<.2	96	.28	.126	2	36	1.04	212	.19	<3	2.90	.01	.05	<2	<.2	27	<.3	<.2	8.3	<1
12082	.5	20.5	3.8	65.5	44	21	9	364	2.00	2.3	<5	<2	22	.08	.4	<.2	50	.37	.047	7	28	.50	83	.09	<3	1.34	.01	.06	<2	<.2	11	<.3	<.2	4.1	1
RE 12082	.6	19.9	3.6	64.0	61	21	9	357	1.96	2.6	<5	<2	22	.13	.4	<.2	49	.37	.046	7	28	.49	81	.08	<3	1.31	.01	.06	<2	<.2	24	<.3	<.2	3.8	1
12083	.6	4.7	1.4	105.6	50	19	26	858	6.59	.9	<5	<2	20	.04	.5	<.2	52	.36	.030	<1	43	1.36	254	.21	<3	1.97	.01	.60	<2	.3	18	<.3	<.2	7.4	1
12084	.5	15.1	4.1	41.6	73	17	6	158	1.79	3.5	<5	<2	18	.11	.5	<.2	47	.27	.057	7	30	.32	70	.07	<3	1.07	.01	.04	<2	<.2	<10	<.3	<.2	3.3	2
12085	.7	14.4	4.3	58.3	38	16	6	174	1.83	2.0	<5	<2	21	.09	.3	<.2	46	.32	.060	7	27	.33	93	.08	<3	1.36	.01	.05	<2	<.2	26	<.3	<.2	4.4	<1
12086	.7	15.7	3.7	69.3	145	19	7	299	1.85	3.0	<5	<2	25	.32	.4	<.2	43	.43	.136	6	27	.29	159	.06	<3	1.12	.01	.05	<2	.2	11	<.3	<.2	3.7	<1
12087	1.0	98.3	6.0	96.1	417	79	17	1212	4.32	6.4	5	2	50	.48	.6	<.2	80	1.11	.043	21	85	.84	282	.08	<3	3.66	.01	.17	<2	<.2	61	.5	<.2	7.3	1
12088	.8	16.1	5.0	137.1	223	17	9	394	2.26	9.5	<5	<2	36	.50	.7	<.2	42	.45	.417	5	30	.25	475	.06	<3	1.32	<.01	.11	<2	.2	30	<.3	<.2	4.7	3
12089	.6	16.7	3.4	98.5	94	10	7	376	1.89	2.2	<5	<2	20	.28	.3	<.2	47	.39	.088	4	20	.33	153	.06	<3	1.26	.01	.05	<2	.2	25	<.3	<.2	4.8	33
12090	.6	11.9	3.3	97.6	245	7	6	499	1.47	1.1	<5	<2	16	.22	.2	<.2	37	.31	.062	4	15	.26	87	.08	<3	.96	.01	.04	<2	<.2	39	<.3	<.2	4.1	1
12091	.5	21.9	3.5	98.9	166	7	7	947	1.89	1.6	<5	<2	22	.37	.2	<.2	46	.45	.075	3	17	.33	171	.07	<3	1.17	.01	.06	<2	<.2	27	<.3	<.2	4.3	<1
12092	.7	17.9	2.9	102.5	60	6	7	1070	1.78	1.6	<5	<2	15	.38	.2	<.2	42	.28	.080	3	17	.36	130	.06	<3	1.08	.01	.06	<2	<.2	14	<.3	<.2	3.7	2
12093	.6	25.7	3.6	99.3	55	24	9	405	2.22	3.1	<5	<2	25	.24	.3	<.2	46	.37	.141	7	39	.37	178	.07	<3	1.54	.01	.05	<2	.2	24	<.3	<.2	4.2	1
12094	.5	29.2	3.5	153.3	154	11	9	344	2.42	2.5	<5	<2	22	.41	.4	<.2	50	.40	.161	3	25	.40	155	.06	<3	1.44	.01	.06	<2	.2	25	<.3	.2	4.7	1
12095	.5	34.0	3.4	145.7	71	11	9	376	2.27	.7	<5	<2	16	.10	.2	<.2	65	.36	.045	4	21	.52	92	.11	<3	1.67	.01	.04	<2	<.2	23	<.3	<.2	6.2	1
12096	.8	48.1	3.7	86.9	41	23	10	339	2.62	2.0	<5	<2	18	.10	.3	<.2	69	.32	.047	5	31	.47	114	.07	<3	2.22	.01	.04	<2	.2	18	<.3	<.2	5.5	<1
12097	.6	61.7	3.7	59.2	59	14	7	243	2.34	1.2	<5	<2	16	.06	.3	<.2	59	.25	.085	4	22	.28	113	.06	<3	1.49	.01	.03	<2	.2	19	<.3	<.2	5.2	<1
12098	.7	30.7	3.0	130.3	87	11	12	550	3.59	5.0	<5	<2	16	.08	.3	<.2	64	.29	.137	3	16	.67	127	.10	<3	2.45	.01	.03	<2	.3	29	<.3	<.2	8.4	2
12099	.6	12.0	3.2	41.0	50	14	5	201	1.54	2.9	<5	<2	19	.09	.5	<.2	41	.31	.034	6	25	.30	65	.07	<3	.80	.01	.03	<2	.2	<10	<.3	<.2	2.8	4
12100	.6	16.5	3.5	61.3	53	17	8	527	1.81	2.3	<5	<2	22	.10	.4	<.2	48	.36	.032	5	30	.42	155	.07	<3	1.36	.01	.04	<2	.2	14	<.3	<.2	4.4	49
12188	1.0	11.0	4.6	128.3	174	11	6	2608	1.44	2.8	<5	<2	31	.61	.3	<.2	37	.55	.146	4	19	.16	231	.04	3	.98	.01	.06	<2	.2	46	<.3	<.2	3.7	1
STANDARD	24.3	121.7	97.3	274.5	1921	30	17	1063	4.24	77.0	23	19	58	1.99	8.9	19.8	72	.69	.109	16	53	1.08	256	.13	25	2.27	.05	.72	19	2.4	966	.6	1.9	6.0	51

Standard is STANDARD D2/C3/AU-S.
ICP - 15 GRAM SAMPLE IS DIGESTED WITH 90 ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 300 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K GA AND AL. SOLUTION ANALYSED DIRECTLY BY ICP. MO CU PB ZN AG AS AU CD SB BI TL HG SE TE AND GA ARE EXTRACTED WITH MIBK-ALIQUAT 336 AND ANALYSED BY ICP. ELEVATED DETECTION LIMITS FOR SAMPLES CONTAIN CU,PB,ZN,AS>1500 PPM,Fe>20%.
- SAMPLE TYPE: SOIL AU* - AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: MAY 22 1998 DATE REPORT MAILED: May 29/98 SIGNED BY........D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12189	.6	7.8	3.0	26.9	129	12	4	116	1.40	1.6	<5	<2	21	.08	.2	<.2	41	.33	.029	3	22	.16	87	.06	<3	.71	.01	.03	<2	<.2	43	<.3	<.2	3.2	16
12190	.9	25.6	4.9	50.2	<30	25	9	336	2.27	4.2	<5	2	30	.35	.8	<.2	54	.63	.045	7	35	.33	111	.08	3	1.00	.01	.10	<2	<.2	29	<.3	<.2	3.3	7
12191	.9	39.4	4.7	49.2	83	29	9	433	1.82	5.9	<5	<2	35	.29	1.0	<.2	49	.79	.061	8	38	.44	110	.07	3	1.05	.01	.07	<2	<.2	75	.5	<.2	3.3	1
12192	.9	17.3	4.0	52.1	110	17	8	523	1.84	2.9	<5	<2	19	.20	.5	<.2	45	.31	.097	6	30	.28	135	.05	<3	.99	.01	.05	<2	<.2	18	<.3	<.2	3.2	1
12193	.9	12.6	4.1	53.6	53	10	5	779	1.29	1.7	<5	<2	35	.44	.2	<.2	34	.56	.053	4	20	.19	209	.05	<3	.75	.01	.05	<2	<.2	35	<.3	<.2	2.9	10
12194	.8	14.2	3.7	56.0	110	10	6	776	1.56	2.0	<5	<2	28	.32	.3	<.2	36	.46	.142	4	20	.23	244	.04	<3	.88	<.01	.06	<2	<.2	30	<.3	<.2	3.5	923
12195	.6	19.5	3.0	43.8	77	22	8	189	1.99	2.2	<5	<2	17	.14	.4	<.2	52	.32	.076	5	31	.26	86	.06	<3	1.05	.01	.04	<2	<.2	14	<.3	<.2	3.1	4
12196	.7	6.0	4.3	64.2	76	5	4	975	1.05	1.0	<5	<2	19	.31	<.2	<.2	29	.36	.080	4	14	.13	191	.05	<3	.71	.01	.05	<2	<.2	17	<.3	<.2	3.2	2
12197	.8	8.5	4.7	38.9	97	11	5	226	1.78	3.3	<5	<2	15	.16	.3	<.2	46	.29	.159	5	26	.15	118	.05	<3	.90	<.01	.05	<2	<.2	27	<.3	<.2	3.9	2
12198	.9	39.7	6.2	74.7	108	41	12	472	2.56	5.5	<5	2	54	.42	1.1	<.2	58	1.23	.064	9	49	.69	143	.08	<3	1.33	.02	.09	<2	.2	66	<.3	<.2	4.4	2
12199	.7	18.4	3.5	43.1	35	15	6	295	1.78	3.6	<5	<2	18	.26	.5	<.2	45	.35	.106	4	29	.28	106	.06	<3	.88	.01	.04	<2	<.2	28	<.3	<.2	3.0	2
12200	1.3	31.7	5.3	75.4	59	23	14	643	2.58	4.9	<5	<2	41	.55	.6	<.2	59	.86	.053	6	34	.63	134	.08	<3	1.59	.01	.07	<2	<.2	44	<.3	<.2	4.7	6
12269	1.0	23.4	5.6	134.8	397	30	12	267	3.58	5.1	<5	2	34	.24	.4	<.2	66	.39	.560	6	56	.35	359	.05	<3	2.53	.01	.06	<2	<.2	57	<.3	<.2	6.9	1
RE 12270	.6	17.9	3.7	45.2	95	18	7	370	1.73	3.6	<5	<2	19	.15	.5	<.2	44	.36	.075	5	28	.25	101	.06	<3	.85	.01	.04	<2	<.2	32	<.3	<.2	2.9	<1
12270	.7	17.2	3.8	44.4	84	18	7	364	1.71	3.2	<5	<2	18	.15	.5	<.2	43	.34	.073	5	27	.25	99	.06	<3	.81	<.01	.04	<2	<.2	26	<.3	<.2	2.9	<1
12271	.5	11.0	3.4	61.4	81	23	7	142	1.78	2.4	<5	<2	19	.18	.3	<.2	43	.33	.111	6	29	.21	187	.06	<3	1.06	.01	.03	<2	<.2	12	<.3	<.2	3.5	2
12272	.7	26.7	5.5	50.8	106	34	12	546	2.56	3.2	<5	3	28	.14	.8	<.2	54	.57	.036	9	47	.48	150	.09	<3	1.41	.01	.11	<2	<.2	32	<.3	<.2	4.4	3
12273	.8	25.9	4.3	56.6	86	29	11	735	2.27	4.3	<5	2	32	.17	.8	<.2	51	.62	.042	9	40	.45	133	.09	<3	1.19	.01	.07	<2	<.2	45	<.3	<.2	3.6	7
12274	.8	16.0	4.0	41.3	<30	21	8	348	1.84	2.5	<5	<2	23	.21	.6	<.2	40	.37	.057	7	33	.34	104	.07	<3	.86	.01	.06	<2	<.2	<10	<.3	<.2	2.8	1
12275	.7	17.0	4.2	66.4	96	23	7	248	2.08	3.3	<5	<2	21	.17	.5	<.2	51	.36	.064	8	33	.38	109	.07	<3	1.22	.01	.03	<2	<.2	21	<.3	<.2	4.1	1
12276	.8	14.8	3.9	67.5	138	22	6	158	1.80	2.7	<5	<2	22	.21	.5	<.2	47	.34	.056	8	32	.36	93	.08	<3	1.18	.01	.04	<2	<.2	26	<.3	<.2	4.2	2
12277	.7	14.7	4.5	62.7	97	22	8	139	2.15	4.6	<5	<2	18	.24	.4	<.2	51	.29	.133	6	33	.27	90	.07	<3	1.31	.01	.03	<2	<.2	23	<.3	<.2	4.2	4
12278	.8	15.6	3.9	56.8	53	22	7	155	1.82	3.7	<5	<2	17	.18	.6	<.2	47	.26	.041	8	35	.36	75	.08	<3	.90	.01	.05	<2	<.2	11	<.3	<.2	2.9	1
12279	.5	8.8	3.8	48.7	92	10	4	122	1.07	1.0	<5	<2	14	.15	.3	<.2	31	.24	.021	5	20	.20	69	.06	<3	.71	.01	.02	<2	<.2	<10	<.3	<.2	2.7	4
12280	.7	13.3	3.9	79.4	202	23	9	148	2.48	3.5	<5	<2	21	.26	.4	<.2	52	.35	.299	6	38	.27	159	.06	<3	1.52	.01	.03	<2	<.2	18	<.3	<.2	4.2	4
12281	.7	11.9	3.6	47.4	85	16	5	176	1.36	1.7	<5	<2	21	.11	.3	<.2	36	.32	.044	8	27	.31	79	.07	<3	.97	.01	.04	<2	<.2	31	<.3	<.2	3.3	2
12282	.7	21.4	4.9	52.6	55	25	8	270	1.91	4.0	<5	2	27	.12	.5	<.2	49	.42	.060	9	41	.47	95	.09	<3	1.29	.01	.06	<2	.2	24	<.3	<.2	4.1	4
12283	.7	10.6	4.3	37.7	110	13	4	167	1.16	1.7	<5	<2	20	.13	.3	<.2	33	.30	.036	7	23	.28	72	.06	<3	.80	.01	.03	<2	<.2	<10	<.3	<.2	3.3	1
12284	.4	10.4	3.7	46.8	38	15	5	133	1.29	1.6	<5	<2	21	.13	.3	<.2	37	.33	.038	8	27	.33	66	.08	<3	.80	.01	.03	<2	<.2	14	<.3	<.2	2.9	<1
12285	.4	11.1	3.6	41.3	37	15	4	140	1.15	1.1	<5	<2	23	.11	.3	<.2	33	.34	.039	8	25	.32	68	.07	<3	.79	.01	.03	<2	<.2	22	<.3	<.2	3.0	<1
12286	.6	10.7	3.8	53.2	142	16	5	211	1.23	1.2	<5	<2	17	.15	.3	<.2	34	.26	.025	7	25	.28	91	.05	<3	.81	.01	.04	<2	.2	19	<.3	<.2	3.1	1
12287	.6	11.3	3.7	54.6	99	17	5	145	1.48	1.8	<5	<2	18	.22	.4	<.2	38	.27	.032	7	30	.24	82	.06	<3	.75	.01	.04	<2	.2	19	<.3	<.2	2.8	<1
12288	.8	19.3	4.2	49.0	119	23	7	191	1.95	3.5	<5	<2	25	.17	.6	<.2	45	.31	.061	9	33	.38	93	.07	<3	.91	.01	.04	<2	<.2	39	<.3	<.2	3.1	8
12289	.4	10.5	3.5	44.4	50	12	4	124	1.24	1.4	<5	<2	14	.10	.3	<.2	36	.24	.026	5	25	.23	68	.05	<3	.68	.01	.03	<2	<.2	14	<.3	<.2	2.5	5
STANDARD	23.8	125.0	91.8	271.5	2017	29	17	1067	4.16	78.3	26	19	59	1.92	8.3	19.6	71	.74	.109	15	52	1.07	262	.13	25	2.35	.05	.73	18	2.6	978	.6	2.3	7.2	54

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data ___ FA ___

Crest Geological Consulting PROJECT 177 FILE # 9801830

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12290	.3	13.8	4.1	37.4	62	16	5	236	1.27	2.0	<5	<2	21	.08	.5	<.2	35	.32	.042	7	29	.36	58	.06	<3	.93	.01	.05	<2	.2	12	<.3	<.2	3.4	<1
12291	.3	15.0	4.8	44.8	163	17	5	166	1.40	1.6	<5	<2	18	.11	.4	<.2	37	.28	.047	6	31	.32	67	.05	<3	1.16	.01	.05	<2	<.2	28	<.3	<.2	3.9	<1
12292	.4	11.2	5.0	41.0	82	14	4	194	1.13	1.1	<5	<2	17	.10	.3	<.2	31	.25	.030	8	25	.29	59	.05	<3	.87	.01	.05	<2	<.2	<10	<.3	<.2	3.2	1
12293	.4	10.2	4.3	30.0	56	11	3	134	.92	1.4	<5	<2	14	.05	.3	<.2	26	.24	.022	6	21	.27	46	.05	<3	.74	.01	.03	<2	.2	12	<.3	<.2	3.1	2
12294	.3	7.0	3.8	31.9	60	9	4	207	.90	.9	<5	<2	15	.07	.2	<.2	27	.25	.021	6	18	.21	45	.05	<3	.67	.01	.04	<2	<.2	12	<.3	<.2	2.6	1
12295	.6	13.9	5.0	51.0	95	18	5	192	1.60	2.8	<5	<2	19	.15	.5	<.2	41	.28	.085	7	34	.33	75	.05	<3	1.08	.01	.05	<2	<.2	23	<.3	<.2	3.9	3
12296	.8	20.1	4.4	44.9	99	23	8	240	2.08	5.6	<5	<2	22	.17	.8	<.2	48	.34	.087	7	40	.42	79	.05	<3	1.15	.01	.06	<2	<.2	11	<.3	<.2	3.8	2
12297	1.0	12.1	4.2	46.6	98	13	6	156	1.85	3.9	<5	2	15	.19	.5	<.2	53	.25	.035	5	29	.24	64	.05	4	.92	.01	.04	<2	<.2	12	<.3	<.2	4.0	144
12298	.6	18.7	4.4	38.9	69	19	7	265	1.65	4.5	<5	<2	24	.11	.7	<.2	43	.33	.043	8	35	.32	85	.06	<3	.90	.01	.08	<2	<.2	25	<.3	<.2	3.2	1
12299	1.0	14.7	5.0	87.8	181	15	8	276	2.60	3.9	<5	<2	14	.28	.4	<.2	53	.22	.311	6	31	.26	106	.05	<3	2.02	.01	.05	<2	<.2	55	<.3	<.2	5.9	1
12300	.3	11.2	3.0	53.8	62	12	4	203	1.05	1.3	<5	<2	21	.10	.2	<.2	29	.32	.022	6	20	.25	66	.06	<3	.80	.01	.04	<2	<.2	10	<.3	<.2	3.0	1
12341	1.3	47.0	11.2	86.4	558	51	12	385	3.10	3.6	5	<2	40	.75	1.6	.4	53	.44	.063	16	70	.67	225	.04	<3	3.11	.01	.13	<2	.4	88	.4	.7	8.5	3
RE 12342	.3	8.2	3.9	29.9	57	12	3	177	.97	1.3	<5	<2	17	.09	.3	<.2	27	.25	.022	7	22	.24	54	.07	<3	.78	.01	.05	<2	<.2	23	<.3	<.2	2.8	1
12342	.2	8.4	3.6	27.9	55	11	3	182	.97	1.0	<5	<2	17	.08	.3	<.2	28	.26	.021	8	22	.24	53	.07	<3	.77	.01	.05	<2	<.2	14	<.3	<.2	2.9	7
12343	.5	11.7	4.1	38.1	78	13	4	203	1.14	1.1	<5	<2	17	.10	.2	<.2	32	.23	.028	7	25	.29	66	.06	<3	1.02	.01	.05	<2	<.2	21	<.3	<.2	3.7	1
12344	.3	9.5	4.3	25.4	63	11	3	160	.99	1.1	<5	2	19	.06	.3	<.2	30	.29	.029	8	23	.26	50	.07	<3	.84	.01	.05	<2	<.2	<10	<.3	<.2	3.4	3
12345	.4	9.3	4.3	21.5	52	9	3	161	.87	1.1	<5	<2	15	.09	.3	<.2	26	.24	.026	7	20	.23	45	.06	<3	.70	.01	.03	<2	<.2	16	<.3	<.2	2.9	1
12346	.4	8.7	3.8	23.8	45	10	3	147	.87	1.2	<5	2	15	.05	.3	<.2	26	.24	.023	7	19	.22	41	.07	<3	.68	.01	.04	<2	<.2	11	<.3	<.2	2.9	6
12347	.3	9.5	4.2	23.0	68	10	3	155	.91	1.1	<5	<2	17	.07	.3	<.2	28	.27	.029	7	18	.23	49	.07	<3	.74	.01	.04	<2	<.2	10	<.3	<.2	3.0	3
12348	.4	11.3	4.3	26.9	65	12	3	149	1.13	1.8	<5	2	18	.08	.4	<.2	34	.28	.041	8	22	.23	56	.07	<3	.82	.01	.04	<2	<.2	13	<.3	<.2	3.6	1
12349	.6	12.3	3.5	42.9	46	20	7	162	1.65	2.9	<5	2	16	.10	.5	<.2	41	.25	.118	7	31	.24	83	.06	<3	1.16	.01	.05	<2	<.2	28	<.3	<.2	3.2	16
12350	.3	9.9	3.8	35.7	43	14	4	152	1.15	1.2	<5	2	18	.09	.2	<.2	32	.28	.034	8	25	.27	54	.08	<3	.86	.01	.05	<2	<.2	17	<.3	<.2	3.2	2
12351	.5	13.5	4.5	39.8	146	17	5	173	1.50	2.1	<5	<2	19	.12	.4	<.2	41	.28	.047	8	31	.30	62	.07	<3	1.15	.01	.06	<2	<.2	22	<.3	<.2	3.9	187
12352	.6	42.9	3.9	67.1	69	25	12	275	3.10	6.5	6	<2	24	.18	.8	<.2	64	.44	.113	5	43	.60	69	.06	<3	1.66	.01	.10	<2	<.2	21	<.3	<.2	4.6	3
12353	.5	14.8	3.8	55.1	81	23	7	196	1.81	3.5	<5	<2	22	.20	.6	<.2	44	.30	.137	7	33	.27	100	.05	<3	1.21	.01	.07	<2	<.2	20	<.3	<.2	4.0	3
12354	.4	8.8	3.4	29.7	46	10	3	158	.86	1.1	<5	<2	15	.08	.3	<.2	24	.23	.019	6	17	.22	45	.06	<3	.67	.01	.04	<2	<.2	11	<.3	<.2	2.9	2
12355	.2	8.2	4.5	22.8	33	9	3	135	.88	1.2	<5	<2	17	.05	.2	<.2	26	.26	.021	8	20	.24	43	.08	<3	.74	.01	.04	<2	<.2	<10	<.3	<.2	2.7	<1
12356	.3	18.3	4.4	36.0	52	18	6	287	1.60	2.8	<5	2	22	.08	.6	<.2	41	.32	.047	9	35	.38	74	.07	<3	1.12	.01	.08	<2	<.2	15	<.3	<.2	3.8	2
12357	.4	12.0	3.9	31.6	80	12	4	209	1.28	1.9	<5	2	20	.10	.3	<.2	34	.33	.031	7	23	.38	50	.06	<3	.96	.01	.06	<2	<.2	17	<.3	<.2	3.3	1
12358	.3	8.8	3.1	30.0	42	10	3	157	.98	1.0	5	<2	15	.09	.2	<.2	28	.25	.018	6	18	.25	47	.06	<3	.68	.01	.04	<2	<.2	<10	<.3	<.2	2.7	2
12359	.7	14.7	3.7	44.1	88	25	8	177	2.26	4.2	<5	2	15	.15	.6	<.2	47	.23	.177	5	33	.26	79	.05	<3	1.57	.01	.04	<2	<.2	29	<.3	<.2	4.4	34
12360	.4	21.0	4.4	34.1	43	20	6	224	1.84	4.2	<5	2	24	.04	.5	<.2	44	.33	.052	8	39	.43	71	.08	<3	1.24	.01	.09	<2	<.2	22	<.3	<.2	3.2	3
12361	.8	15.7	3.6	77.7	151	16	7	809	1.82	2.1	<5	<2	16	.21	.3	<.2	42	.27	.084	5	25	.34	193	.05	<3	1.40	.01	.06	<2	<.2	25	<.3	<.2	4.6	1
12362	.6	11.3	3.4	50.4	263	7	5	187	1.61	2.8	<5	<2	13	.12	.3	<.2	39	.21	.152	5	18	.14	65	.04	<3	1.17	.01	.04	<2	<.2	34	<.3	<.2	4.1	1
STANDARD	23.8	122.3	99.0	250.8	2139	30	16	1008	4.69	78.1	23	19	65	2.18	11.5	17.6	71	.71	.109	17	57	1.08	243	.12	26	2.28	.07	.72	15	2.6	972	.3	2.2	7.6	53

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data 4 FA ____

ACME ANALYTICAL

Crest Geological Consulting PROJECT 177 FILE # 9801830

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12363	.6	24.5	4.6	48.2	74	23	7	317	1.90	2.8	<5	2	26	.16	.4	<.2	44	.43	.038	7	35	.42	104	.08	<3	1.30	.01	.06	<2	<.2	22	<.3	<.2	3.8	21
12364	.5	32.3	4.3	50.0	46	28	9	344	2.51	3.9	<5	2	33	.11	.7	<.2	57	.51	.053	8	43	.57	108	.10	<3	1.38	.01	.06	<2	<.2	38	<.3	<.2	3.4	5
12365	.6	40.9	6.1	64.7	64	39	14	510	2.90	5.4	<5	2	40	.10	.8	<.2	63	.59	.066	11	60	.69	165	.11	<3	1.90	.01	.13	<2	.2	73	<.3	<.2	4.9	2
12366	.3	9.3	4.0	26.6	<30	11	3	141	1.04	1.2	<5	<2	22	.07	.2	<.2	29	.36	.028	8	22	.28	67	.08	<3	.81	.01	.04	<2	<.2	13	<.3	<.2	2.6	2
12367	.2	10.7	4.7	33.7	36	13	4	138	1.07	.8	<5	<2	21	.06	.2	<.2	29	.31	.017	7	24	.29	81	.08	<3	.93	.01	.03	<2	<.2	20	<.3	<.2	2.8	1
12368	.3	8.8	4.0	26.7	31	11	3	145	1.06	1.1	<5	<2	20	.06	.2	<.2	30	.31	.019	8	21	.27	63	.08	<3	.77	.01	.03	<2	<.2	<10	<.3	<.2	2.4	8
12369	.4	13.8	5.4	41.6	41	16	5	208	1.56	1.2	<5	<2	23	.07	.3	<.2	41	.32	.027	8	31	.37	89	.09	<3	1.07	.01	.04	<2	<.2	25	<.3	<.2	3.3	1
12370	.3	8.7	3.7	27.9	34	10	3	132	1.18	1.1	<5	<2	20	.09	.3	<.2	35	.31	.013	8	20	.26	63	.08	<3	.77	.01	.02	<2	<.2	16	<.3	<.2	2.7	9
12371	.6	16.0	3.0	37.5	96	22	6	176	1.65	3.6	<5	2	19	.07	.5	<.2	39	.31	.035	7	29	.26	102	.07	<3	.86	.01	.06	<2	<.2	<10	<.3	<.2	2.4	1
12372	.5	9.3	2.9	41.6	53	19	6	171	1.73	2.3	<5	<2	21	.09	.3	<.2	43	.35	.056	5	27	.28	98	.08	<3	.99	.01	.05	<2	<.2	<10	<.3	<.2	3.1	1
12373	.9	13.8	3.8	67.7	218	20	7	168	1.87	4.3	<5	<2	19	.34	.6	<.2	39	.37	.149	7	30	.29	98	.05	<3	.99	.01	.04	<2	.2	13	<.3	<.2	3.5	4
12374	.8	13.5	4.3	66.4	130	18	7	828	1.76	3.5	<5	<2	21	.40	.5	<.2	38	.33	.076	7	30	.25	226	.05	<3	.90	.01	.05	<2	.2	15	<.3	<.2	3.3	2
12375	.8	27.4	4.9	50.4	46	36	10	215	2.59	5.5	<5	2	25	.08	1.0	<.2	56	.44	.036	7	46	.50	101	.09	<3	1.37	.01	.07	<2	.2	21	<.3	<.2	3.8	1
12376	1.0	8.4	4.4	87.7	143	19	7	606	1.65	2.0	<5	<2	24	.49	.3	<.2	36	.30	.103	7	32	.24	226	.06	<3	.92	.01	.06	<2	<.2	21	<.3	<.2	3.3	<1
12377	.6	24.3	4.4	46.0	<30	26	8	335	2.02	4.8	<5	<2	27	.12	.8	<.2	48	.42	.034	11	37	.39	113	.09	<3	.99	.01	.07	<2	<.2	28	<.3	<.2	2.3	1
12378	.5	9.8	3.7	53.0	88	15	6	284	1.42	1.5	<5	<2	20	.29	.3	<.2	37	.29	.050	8	26	.21	121	.07	<3	.82	.01	.04	<2	<.2	<10	<.3	<.2	2.9	<1
12379	.7	10.3	5.0	64.9	86	16	5	145	1.58	3.5	<5	<2	17	.23	.5	<.2	43	.29	.050	7	30	.29	85	.07	<3	.89	.01	.03	<2	<.2	<10	<.3	<.2	2.9	<1
12380	.7	18.8	4.4	89.8	138	25	9	191	2.30	5.3	<5	<2	19	.29	.5	<.2	51	.33	.157	6	35	.38	123	.07	<3	1.51	.01	.04	<2	.2	22	<.3	<.2	3.9	2
RE 12380	.8	19.0	4.1	90.5	150	24	9	195	2.30	5.2	<5	<2	20	.30	.5	<.2	52	.34	.145	6	35	.38	125	.07	<3	1.52	.01	.04	<2	<.2	26	<.3	<.2	4.1	2
12381	.7	12.9	4.4	71.7	75	19	6	258	1.48	1.8	<5	2	22	.22	.3	<.2	40	.32	.032	9	28	.38	94	.08	<3	1.07	.01	.04	<2	<.2	<10	<.3	<.2	3.1	1
12382	.6	10.8	4.0	50.0	100	15	5	162	1.22	1.7	<5	<2	20	.20	.3	<.2	36	.33	.036	8	24	.31	71	.07	<3	.90	.01	.03	<2	.2	<10	<.3	<.2	2.9	9
12383	.5	14.3	4.6	59.0	58	16	7	163	1.86	3.8	<5	<2	24	.23	.4	<.2	41	.40	.171	5	28	.23	132	.06	<3	1.04	.01	.05	<2	<.2	<10	<.3	<.2	3.2	<1
12384	.4	10.6	4.1	64.2	79	16	5	178	1.32	1.6	<5	<2	21	.19	.3	<.2	35	.34	.030	7	24	.25	83	.07	<3	.85	.01	.03	<2	<.2	<10	<.3	<.2	2.9	<1
12385	.4	8.9	4.1	67.8	59	14	4	132	1.19	1.2	<5	<2	22	.15	.2	<.2	34	.32	.021	8	23	.27	80	.09	<3	.91	.01	.03	<2	.2	10	<.3	<.2	2.9	<1
12386	.4	12.0	3.6	52.1	81	15	6	172	1.37	1.7	<5	<2	22	.16	.3	<.2	38	.35	.038	8	27	.33	87	.07	<3	.96	.01	.03	<2	<.2	16	<.3	<.2	3.3	2
12387	.4	11.6	3.7	48.3	<30	18	5	157	1.22	1.6	<5	2	26	.10	.3	<.2	34	.39	.039	8	29	.38	70	.09	<3	.90	.01	.04	<2	<.2	10	<.3	<.2	2.7	5
12388	.3	9.9	3.8	45.6	56	15	4	124	1.12	1.1	<5	<2	22	.11	.3	<.2	31	.32	.021	7	26	.32	67	.08	<3	.83	.01	.03	<2	<.2	10	<.3	<.2	2.6	1
12389	.3	10.7	4.3	50.8	69	18	5	159	1.27	1.5	<5	2	24	.11	.3	<.2	34	.36	.031	9	31	.39	75	.10	<3	1.00	.01	.05	<2	<.2	19	<.3	<.2	2.9	1
12390	.4	11.9	4.7	51.1	86	18	5	140	1.29	1.3	<5	<2	20	.13	.2	<.2	33	.29	.028	8	28	.36	80	.08	<3	.97	.01	.04	<2	<.2	15	<.3	<.2	3.1	3
12391	.6	15.3	4.1	62.8	72	22	6	189	1.60	1.9	<5	2	20	.15	.3	<.2	41	.28	.025	8	33	.39	98	.08	<3	1.16	.01	.04	<2	.2	14	<.3	<.2	3.4	4
12392	.6	14.9	4.1	55.7	53	20	6	159	1.64	2.2	<5	2	19	.10	.3	<.2	43	.26	.027	9	32	.41	88	.08	<3	1.08	.01	.04	<2	<.2	25	<.3	<.2	3.1	2
12393	.5	18.9	3.5	44.6	47	16	8	337	1.69	2.0	<5	<2	20	.07	.3	<.2	40	.41	.055	6	26	.42	85	.05	<3	1.18	.01	.03	<2	<.2	<10	<.3	<.2	3.0	2
12394	.4	15.0	4.3	37.4	56	15	5	171	1.32	2.3	<5	<2	23	.07	.4	<.2	36	.39	.042	6	29	.36	70	.06	<3	.97	.01	.04	<2	<.2	18	<.3	<.2	3.1	1
12395	1.0	65.5	6.0	86.8	<30	47	15	381	3.63	12.6	<5	3	35	.07	1.3	<.2	77	.47	.065	10	85	.83	166	.11	<3	2.24	.01	.13	<2	.2	98	<.3	<.2	5.0	2
STANDARD	24.5	123.3	100.3	276.1	1905	30	17	1056	4.41	83.1	23	19	59	1.91	8.0	21.7	73	.69	.112	16	52	1.11	260	.14	26	2.35	.05	.74	19	2.3	988	.4	1.8	5.6	51

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data JL FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12396	.4	13.8	4.1	46.1	<30	16	5	194	1.37	1.5	<5	<2	21	.11	.3	<.2	35	.32	.039	7	28	.38	72	.07	<3	1.01	.01	.03	<2	<.2	11	<.3	<.2	3.3	<1
12397	.4	12.6	4.3	34.1	40	14	4	154	1.30	2.7	<5	<2	20	.11	.5	<.2	33	.30	.061	6	25	.35	61	.06	<3	.80	.01	.03	<2	<.2	<10	<.3	<.2	3.2	1
12398	.5	10.6	3.5	36.0	107	13	4	133	1.19	1.5	<5	<2	19	.10	.3	<.2	32	.29	.042	6	24	.31	62	.06	<3	.79	.01	.03	<2	<.2	14	<.3	<.2	3.0	<1
12399	.3	9.1	3.6	31.9	38	12	3	123	1.05	1.0	<5	<2	18	.05	.2	<.2	29	.27	.031	6	20	.28	53	.07	<3	.73	.01	.02	<2	<.2	13	<.3	<.2	3.2	15
12400	.8	17.7	3.5	34.9	<30	18	7	158	1.83	3.4	<5	<2	19	.08	.6	<.2	44	.34	.061	7	28	.37	63	.06	<3	1.03	.01	.04	<2	<.2	<10	<.3	<.2	3.2	1
12401	.7	74.6	3.2	132.9	155	12	20	809	4.24	3.5	<5	<2	27	.21	.3	<.2	58	.35	.095	2	15	.95	140	.06	<3	2.40	.01	.06	<2	<.2	29	<.3	<.2	7.8	<1
12402	.5	9.3	3.5	38.8	<30	20	7	169	1.57	1.8	<5	<2	19	.09	.4	<.2	40	.33	.041	6	29	.32	90	.06	<3	1.03	.01	.03	<2	<.2	21	<.3	<.2	3.2	<1
12403	.7	59.6	2.7	109.7	104	12	15	437	3.34	2.1	<5	<2	24	.11	.3	<.2	89	.36	.046	5	16	.70	86	.10	<3	1.68	.01	.05	<2	<.2	21	<.3	<.2	7.1	<1
12404	.8	10.6	3.8	94.5	105	8	12	815	2.70	1.1	<5	<2	18	.09	<.2	<.2	48	.25	.077	3	15	.59	153	.08	<3	1.75	.01	.04	<2	<.2	15	<.3	<.2	6.6	<1
12405	.9	13.3	4.9	58.4	84	10	6	170	1.37	3.1	<5	<2	18	.15	.4	<.2	31	.30	.055	7	20	.26	63	.04	<3	.91	<.01	.04	<2	<.2	15	<.3	<.2	3.5	<1
12406	.6	10.4	3.4	83.5	47	16	6	168	1.68	2.8	<5	<2	15	.17	.4	<.2	38	.24	.071	6	25	.26	121	.06	<3	1.00	.01	.04	<2	<.2	12	<.3	<.2	3.4	3
12407	.7	18.9	4.9	204.2	110	18	15	291	2.15	4.6	<5	<2	21	.28	.3	<.2	43	.31	.168	6	28	.27	144	.05	<3	1.58	.01	.05	<2	<.2	40	<.3	<.2	5.4	1
12408	1.3	7.0	4.2	40.2	71	4	5	220	2.19	10.7	<5	<2	10	.06	.2	<.2	45	.20	.036	2	9	.18	58	.13	<3	1.21	.01	.02	<2	<.2	36	<.3	<.2	6.6	<1
12409	.8	23.9	3.8	58.2	32	23	9	259	2.11	4.7	<5	<2	27	.15	.7	<.2	45	.39	.099	7	34	.43	103	.07	<3	1.01	.01	.05	<2	<.2	27	<.3	<.2	3.2	2
12410	1.1	56.6	10.2	179.0	255	63	27	1647	3.13	10.1	<5	<2	39	.85	1.1	<.2	57	.54	.126	9	77	.56	312	.05	<3	2.12	.01	.10	<2	<.2	43	<.3	<.2	5.5	2
12411	.7	18.2	4.1	108.3	188	19	8	208	1.76	4.7	<5	<2	27	.43	.5	<.2	41	.35	.117	6	33	.27	154	.06	<3	.97	.01	.04	<2	<.2	17	<.3	<.2	3.6	<1
12412	1.1	21.4	4.1	180.2	190	20	10	683	2.40	4.9	<5	2	25	.51	.7	<.2	40	.28	.314	6	33	.31	441	.05	<3	1.35	.01	.06	<2	<.2	22	<.3	<.2	3.9	1
RE 12412	1.1	20.5	3.6	178.7	193	20	10	680	2.37	5.1	<5	<2	24	.49	.8	<.2	38	.28	.318	5	31	.31	446	.04	<3	1.34	.01	.06	<2	<.2	26	<.3	<.2	3.5	9
12413	.7	9.2	3.9	77.2	185	12	7	328	1.68	3.0	<5	<2	24	.41	.4	<.2	35	.31	.187	6	26	.20	317	.05	<3	.93	.01	.05	<2	.2	26	<.3	<.2	4.3	<1
12414	.8	33.2	4.0	107.3	309	35	8	1308	2.14	3.9	<5	<2	30	.59	.6	<.2	46	.40	.052	12	43	.47	173	.05	<3	1.39	.01	.08	<2	.2	59	<.3	.2	4.0	1
12415	.6	16.3	3.3	59.8	98	14	6	275	1.61	2.7	<5	<2	23	.25	.5	<.2	39	.31	.041	7	25	.29	117	.07	<3	.87	.01	.04	<2	<.2	25	<.3	<.2	3.2	<1
12416	.5	18.0	3.6	69.5	149	19	7	464	1.50	2.4	<5	<2	25	.28	.4	<.2	41	.35	.034	8	32	.36	136	.07	<3	1.13	.01	.05	<2	.2	27	<.3	<.2	3.6	<1
12417	.4	12.2	3.6	40.1	106	14	5	156	1.37	2.5	<5	<2	20	.11	.4	<.2	38	.34	.043	5	23	.33	68	.07	<3	.88	.01	.03	<2	<.2	11	<.3	<.2	3.2	1
12418	.5	6.7	3.9	23.7	65	8	3	223	1.12	1.6	<5	<2	20	.11	.4	<.2	33	.26	.056	5	19	.12	95	.06	<3	.60	.01	.04	<2	<.2	19	<.3	<.2	2.6	<1
12419	.4	11.2	3.2	37.5	65	15	4	155	1.35	1.5	<5	<2	18	.09	.4	<.2	37	.28	.029	7	24	.25	79	.08	<3	.84	.01	.03	<2	<.2	17	<.3	<.2	3.2	<1
12420	.6	11.3	4.0	74.1	157	25	8	191	1.98	2.4	<5	<2	22	.21	.5	<.2	44	.33	.136	7	31	.25	123	.07	<3	1.56	.01	.05	<2	<.2	40	<.3	<.2	4.2	<1
12421	.8	13.3	3.6	35.6	120	11	5	164	1.99	3.3	<5	<2	19	.12	.6	<.2	53	.34	.063	5	23	.25	70	.08	<3	1.25	.01	.03	<2	<.2	18	<.3	<.2	4.2	2
12422	.5	12.6	3.4	45.1	85	18	5	195	1.69	2.9	<5	<2	20	.11	.6	<.2	46	.30	.066	7	29	.28	88	.08	<3	1.06	.01	.03	<2	<.2	<10	<.3	<.2	3.7	1
12423	2.5	117.7	6.0	52.6	367	50	21	591	7.75	22.4	<5	<2	47	.18	1.0	<.2	158	.73	.043	33	76	.92	244	.07	<3	2.84	.01	.07	<2	<.2	88	.5	<.2	7.2	<1
12424	2.3	41.0	5.9	58.8	245	34	22	2501	2.74	5.1	<5	<2	55	.66	.6	<.2	62	.87	.038	15	39	.50	257	.06	<3	1.92	.01	.09	<2	<.2	55	<.3	<.2	5.9	<1
12425	.6	12.3	3.7	139.9	150	13	7	209	1.76	3.3	<5	<2	22	.74	.7	<.2	44	.37	.084	6	27	.27	86	.08	<3	.88	.01	.04	<2	<.2	12	<.3	.2	3.4	3
12426	.5	12.6	2.9	58.8	94	15	5	180	1.61	3.1	<5	<2	20	.21	.5	<.2	44	.31	.056	7	27	.28	79	.08	<3	.96	.01	.03	<2	<.2	10	<.3	<.2	2.9	2
12427	.8	29.0	3.7	171.0	239	4	5	663	1.73	1.7	<5	<2	11	.68	.2	<.2	24	.36	.046	2	9	.75	83	.02	<3	1.26	<.01	.06	<2	<.2	22	<.3	<.2	5.1	<1
12428	.7	20.3	5.1	92.7	97	25	8	350	2.24	3.1	<5	<2	20	.18	.7	<.2	46	.33	.072	8	30	.36	124	.05	<3	1.67	.01	.06	<2	<.2	28	<.3	<.2	4.5	3
STANDARD	24.3	123.9	99.1	274.7	1967	29	17	1065	4.37	78.5	26	19	59	2.05	9.5	21.3	72	.68	.110	15	52	1.09	261	.14	25	2.35	.05	.73	20	2.6	996	.7	2.0	7.1	55

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12429	1.1	45.7	4.9	542.6	388	13	14	926	2.75	8.1	<5	<2	19	1.26	.4	<.2	49	.41	.055	4	18	.41	104	.04	<3	1.71	.01	.09	<2	<.2	15	<.3	.2	5.5	2
12430	.4	12.1	2.7	37.8	48	13	5	169	1.20	2.3	<5	2	22	.11	.4	<.2	34	.30	.063	6	24	.24	53	.06	3	.76	.01	.06	<2	<.2	<10	<.3	<.2	2.5	1
12431	.6	5.2	3.9	43.0	55	10	5	165	1.40	3.0	<5	<2	13	.14	.2	<.2	38	.21	.137	5	24	.14	83	.05	3	.99	.01	.06	<2	<.2	11	<.3	<.2	3.6	1
12432	.5	12.3	3.9	101.6	135	14	10	634	2.02	2.5	<5	<2	12	.13	.4	<.2	46	.22	.099	5	25	.39	118	.07	<3	1.19	.01	.10	<2	<.2	24	<.3	<.2	5.1	<1
12433	.4	20.7	4.1	37.2	<30	15	7	373	1.69	5.4	<5	2	18	.08	.6	<.2	46	.33	.045	5	28	.35	77	.06	3	1.12	.01	.05	<2	<.2	12	<.3	<.2	3.6	11
12434	.3	12.7	2.9	65.5	30	12	7	468	2.00	3.3	<5	<2	17	.07	.5	<.2	49	.30	.063	4	22	.38	91	.07	<3	1.21	.01	.09	<2	<.2	10	<.3	<.2	4.6	14
12435	.5	18.2	3.4	38.6	58	14	6	206	1.70	3.7	<5	2	18	.10	.5	<.2	47	.30	.044	6	27	.38	65	.07	3	.91	.01	.05	<2	<.2	<10	<.3	<.2	3.5	<1
12436	.5	11.7	4.2	61.0	108	20	7	161	1.74	3.6	<5	<2	20	.20	.4	<.2	41	.32	.151	6	31	.25	83	.05	<3	1.11	.01	.06	<2	<.2	20	<.3	<.2	4.1	2
12437	.9	24.3	5.1	27.2	133	20	6	133	2.07	4.4	<5	<2	30	.20	.7	<.2	61	.44	.015	9	38	.24	90	.06	<3	.95	.01	.06	<2	<.2	27	<.3	<.2	3.6	138
12438	.5	10.8	3.7	75.1	95	10	6	401	1.63	1.6	<5	2	16	.30	.3	<.2	41	.27	.106	5	21	.34	89	.06	3	1.06	.01	.09	<2	<.2	14	<.3	<.2	4.5	2
12439	.7	15.2	4.1	96.4	163	9	7	924	1.84	1.8	5	<2	14	.23	.3	<.2	47	.27	.061	5	17	.38	97	.07	<3	1.20	.01	.08	<2	<.2	14	<.3	<.2	4.7	1
12440	.9	105.1	10.7	89.6	545	73	17	916	4.65	8.0	<5	2	51	.40	1.0	<.2	85	.95	.053	21	95	.87	243	.06	<3	3.20	.02	.19	<2	<.2	108	.6	<.2	9.0	5
RE 12440	.9	111.9	10.3	96.2	527	78	18	971	4.90	9.6	<5	2	54	.39	.9	<.2	93	1.02	.057	23	102	.92	254	.07	<3	3.50	.02	.18	<2	.2	110	.6	<.2	9.2	4
12441	.9	17.3	5.2	92.1	167	19	9	509	2.62	4.0	<5	<2	18	.23	.5	<.2	58	.32	.097	6	33	.29	113	.07	<3	1.55	.01	.14	<2	<.2	27	<.3	<.2	5.9	8
12442	.6	17.5	3.8	30.6	40	18	7	178	1.49	3.8	<5	<2	20	.08	.5	<.2	43	.29	.029	6	32	.30	67	.06	<3	.89	.01	.05	<2	<.2	<10	<.3	<.2	3.0	1
12443	.7	67.7	2.3	49.4	<30	7	8	274	2.34	1.5	<5	<2	19	.05	<.2	<.2	82	.37	.034	2	28	.50	54	.18	<3	1.15	.01	.04	<2	<.2	29	<.3	<.2	4.9	1
12444	1.0	18.1	5.1	82.9	<30	21	10	260	3.00	3.1	<5	<2	14	.07	.3	<.2	72	.21	.084	6	33	.32	100	.08	<3	2.05	.01	.07	<2	<.2	29	<.3	<.2	6.7	2
12445	.7	17.3	4.4	55.7	31	21	10	544	1.73	4.1	<5	<2	20	.10	.4	<.2	48	.25	.031	8	36	.33	94	.07	<3	1.25	.01	.06	<2	.2	17	<.3	<.2	4.3	1
12446	.6	23.4	4.6	70.2	50	20	16	583	4.57	2.6	<5	<2	28	.08	.4	<.2	128	.49	.052	6	32	.79	119	.10	<3	2.31	.01	.07	<2	<.2	18	<.3	<.2	7.6	1
12447	.7	10.0	4.9	50.0	<30	10	6	238	2.89	3.1	<5	<2	15	.06	.4	<.2	70	.27	.069	6	27	.40	121	.06	<3	1.48	.01	.03	<2	<.2	22	<.3	<.2	7.4	1
12448	.5	7.5	3.5	29.4	<30	14	5	137	1.22	2.6	<5	<2	15	.08	.3	<.2	33	.22	.032	8	26	.22	66	.05	<3	.79	.01	.05	<2	<.2	<10	<.3	<.2	2.8	5
12449	.6	18.5	4.3	34.6	<30	18	6	163	1.62	4.6	<5	<2	21	.11	.6	<.2	47	.32	.030	7	39	.36	56	.08	<3	.83	.01	.06	<2	<.2	<10	<.3	<.2	2.8	4
12450	.6	29.5	3.5	76.5	40	13	11	276	2.86	4.8	<5	<2	23	.20	.4	<.2	66	.56	.059	4	19	.53	69	.08	<3	1.82	.01	.03	<2	<.2	12	<.3	<.2	5.0	1
12451	.6	40.7	5.3	160.3	109	25	10	377	2.80	4.1	<5	<2	27	.31	.3	<.2	46	.37	.289	7	46	.45	291	.04	<3	2.14	.01	.14	<2	<.2	27	<.3	<.2	6.9	1
12452	.5	10.4	3.1	47.7	39	6	6	216	2.04	1.2	<5	<2	20	.23	<.2	<.2	40	.26	.120	5	17	.40	97	.03	<3	1.04	.01	.06	<2	<.2	22	<.3	<.2	4.7	1
12453	.4	16.4	2.5	113.0	49	9	8	478	1.95	2.0	6	<2	21	.14	<.2	<.2	38	.32	.096	4	24	.55	126	.05	<3	1.28	.01	.05	<2	<.2	22	<.3	<.2	5.1	1
12454	.3	19.7	2.6	72.0	<30	16	9	456	2.05	1.1	<5	<2	20	.16	<.2	<.2	45	.37	.037	5	40	.68	72	.07	<3	1.30	.01	.07	<2	<.2	13	<.3	<.2	4.5	1
12455	.5	21.7	2.4	97.6	149	15	9	865	2.08	1.8	<5	<2	18	.29	<.2	<.2	44	.29	.069	5	35	.58	93	.06	<3	1.33	.01	.05	<2	<.2	<10	<.3	<.2	4.3	5
12456	.4	17.3	2.8	85.5	121	14	8	535	2.25	3.2	<5	<2	21	.21	.2	<.2	48	.32	.104	5	30	.49	124	.05	<3	1.42	.01	.06	<2	.2	20	<.3	<.2	4.7	1
12457	.4	14.1	2.5	67.2	130	12	6	219	1.97	2.9	<5	<2	14	.15	.3	<.2	43	.26	.095	4	26	.39	82	.03	<3	1.29	.01	.06	<2	<.2	30	<.3	<.2	4.1	1
12458	.5	15.9	3.2	33.8	58	18	6	170	1.71	3.8	<5	<2	17	.12	.5	<.2	44	.26	.058	5	30	.31	64	.05	<3	.97	.01	.04	<2	<.2	11	<.3	<.2	3.0	1
12459	.7	14.0	3.9	69.8	178	14	6	1184	1.57	2.8	<5	<2	22	.57	.5	<.2	39	.32	.095	5	27	.20	269	.05	<3	.84	.01	.07	<2	<.2	15	<.3	<.2	3.0	1
12460	.5	11.9	3.0	29.6	110	11	5	202	1.29	4.9	<5	<2	17	.17	.5	<.2	34	.30	.042	5	25	.24	46	.07	<3	.73	.01	.05	<2	<.2	<10	<.3	<.2	3.4	<1
12461	.5	27.3	3.7	38.8	32	17	8	371	1.78	5.4	<5	2	21	.13	.6	<.2	47	.38	.021	7	37	.35	55	.08	<3	.85	.01	.05	<2	<.2	21	<.3	<.2	2.8	1
STANDARD	22.9	122.5	98.8	247.7	2026	29	16	959	4.65	77.6	27	18	64	2.01	11.6	17.7	72	.71	.106	17	52	1.07	240	.11	25	2.27	.06	.70	15	2.4	951	.6	2.2	6.8	54

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

ACME ANALYTICAL

Crest Geological Consulting PROJECT 177 FILE # 9801830

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12462	1.0	34.8	3.6	47.5	102	20	8	357	1.85	4.9	<5	2	22	.17	.5	<.2	48	.42	.020	8	38	.34	57	.08	<3	1.02	.02	.06	<2	.2	12	<.3	<.2	3.4	1
12463	.6	11.5	3.1	44.9	68	13	6	236	1.42	3.3	<5	2	19	.20	.4	<.2	34	.29	.135	5	23	.23	113	.05	<3	.81	.01	.05	<2	<.2	11	<.3	<.2	2.8	8
12464	.7	18.1	3.6	35.1	47	14	5	185	1.55	4.0	<5	2	23	.07	.4	<.2	42	.35	.057	8	29	.35	56	.07	<3	.90	.01	.05	<2	<.2	<10	<.3	<.2	2.9	10
12465	1.2	36.0	4.5	70.8	69	28	8	849	1.78	3.0	5	2	26	.24	.4	<.2	41	.42	.061	13	35	.36	130	.04	3	1.39	.01	.11	<2	<.2	51	<.3	<.2	3.9	1
12466	2.1	86.1	8.2	75.2	355	15	10	367	3.04	7.5	8	2	12	.12	.4	<.2	79	.16	.091	6	26	.40	54	.10	<3	1.60	.01	.05	<2	<.2	77	<.3	.2	7.2	6
12467	1.3	970.4	3.9	71.3	702	20	16	679	3.03	3.8	<5	2	20	.11	.3	<.2	52	.30	.130	6	29	.43	103	.06	<3	2.55	.01	.10	<2	<.2	52	<.3	.3	6.0	2
12468	1.2	32.4	6.9	67.7	134	12	9	922	2.61	1.5	<5	<2	21	.10	.2	.2	47	.32	.084	6	21	.43	96	.07	<3	1.42	.01	.07	<2	<.2	35	<.3	<.2	6.0	5
12469	.6	12.2	3.1	124.4	66	14	15	945	4.06	2.3	<5	<2	40	.16	.2	<.2	80	.64	.070	5	20	1.24	106	.18	<3	2.52	.01	.08	<2	<.2	22	<.3	<.2	6.5	1
12470	1.1	96.9	5.0	111.0	117	24	16	532	2.68	13.4	<5	<2	27	.18	.3	<.2	54	.40	.035	11	31	.54	80	.05	<3	1.70	.01	.10	<2	<.2	31	<.3	<.2	5.0	1
12471	.9	19.7	4.3	54.7	42	20	7	214	1.85	5.6	<5	2	20	.13	.4	<.2	41	.28	.073	8	31	.42	72	.06	<3	1.07	.01	.06	<2	<.2	22	<.3	<.2	3.5	1
12472	1.0	15.8	4.4	36.6	55	20	7	214	1.74	4.4	<5	2	19	.14	.5	.2	45	.34	.027	6	31	.37	52	.07	<3	.92	.01	.08	<2	<.2	10	<.3	<.2	3.6	1
12473	.9	9.1	5.0	81.7	76	6	5	217	1.72	1.2	<5	<2	19	.19	<.2	<.2	31	.29	.079	6	15	.31	38	.03	<3	1.30	.01	.09	<2	<.2	18	<.3	<.2	5.7	1
RE 12473	.9	9.5	5.2	86.9	90	6	5	223	1.85	1.4	<5	<2	20	.21	<.2	.2	32	.30	.080	6	16	.32	38	.03	<3	1.36	.01	.10	<2	<.2	17	<.3	<.2	6.5	4
12474	1.2	84.4	9.3	164.7	192	66	19	1189	4.37	4.3	<5	2	30	.20	.4	<.2	78	.62	.085	16	81	.63	238	.06	<3	3.64	.02	.12	<2	<.2	44	<.3	<.2	9.1	1
12475	1.0	31.1	7.2	99.0	<30	42	11	457	3.12	4.0	<5	2	21	.08	.4	<.2	71	.26	.059	7	59	.50	214	.08	<3	2.62	.01	.08	<2	<.2	25	<.3	<.2	7.4	1
12476	.9	19.1	5.0	79.4	47	26	8	460	2.03	3.0	<5	2	21	.19	.3	<.2	46	.31	.074	7	38	.34	121	.06	3	1.40	.01	.08	<2	<.2	11	<.3	<.2	4.6	5
12477	.7	11.9	4.1	47.8	38	18	5	251	1.44	1.8	<5	<2	21	.14	.3	<.2	39	.33	.043	7	29	.25	80	.07	<3	.99	.01	.07	<2	<.2	21	<.3	<.2	3.7	2
12501	1.8	78.5	5.9	63.9	384	48	10	1084	2.80	3.7	7	<2	145	1.09	.5	<.2	58	2.68	.132	17	50	.46	290	.03	<3	2.04	.01	.11	<2	<.2	133	1.3	<.2	5.6	2
12502	.9	17.7	5.8	78.8	106	19	7	460	2.20	3.5	<5	2	26	.40	.5	<.2	45	.41	.163	8	37	.35	152	.06	<3	1.28	.01	.10	<2	<.2	<10	<.3	<.2	5.3	1
12503	1.0	48.1	6.3	66.3	49	39	12	406	2.92	11.8	<5	3	35	.16	.9	<.2	63	.49	.057	11	68	.62	119	.08	<3	1.49	.01	.15	<2	<.2	46	<.3	<.2	4.4	2
12504	.6	11.2	3.8	32.3	<30	15	5	278	1.47	2.8	<5	2	21	.11	.3	<.2	39	.29	.032	7	33	.23	94	.07	3	.82	.01	.11	<2	<.2	<10	<.3	<.2	3.2	<1
12505	.9	10.0	4.5	67.2	138	13	6	823	1.71	2.4	<5	<2	15	.27	.2	<.2	40	.24	.183	6	29	.21	94	.04	3	1.12	.01	.07	<2	<.2	32	<.3	<.2	4.3	<1
12506	1.0	11.0	5.2	82.2	156	14	7	347	2.30	2.9	<5	2	16	.33	.2	<.2	54	.29	.240	6	33	.23	121	.05	<3	1.33	.01	.06	<2	<.2	32	<.3	<.2	5.3	1
12507	1.0	10.0	4.9	67.3	45	11	6	334	1.68	1.8	<5	<2	20	.27	.3	<.2	45	.30	.075	7	29	.19	124	.07	<3	.83	.01	.08	<2	<.2	<10	<.3	<.2	4.3	<1
12508	1.4	13.0	4.2	69.5	<30	16	7	508	1.81	2.5	<5	2	21	.44	.4	<.2	47	.34	.032	6	31	.26	149	.06	3	.89	.01	.08	<2	<.2	22	<.3	<.2	3.1	3
12509	.9	13.0	4.5	58.4	62	16	7	984	1.53	2.8	<5	<2	22	.31	.4	<.2	39	.35	.071	7	30	.26	135	.05	3	.86	.01	.07	<2	<.2	<10	<.3	<.2	3.3	2
12510	.6	8.4	4.2	55.3	<30	14	6	413	1.49	1.1	<5	<2	19	.21	.2	<.2	41	.27	.071	5	26	.17	115	.04	<3	.79	.01	.07	<2	<.2	<10	<.3	<.2	2.9	7
12511	1.0	8.8	5.1	48.8	82	7	2	275	.90	.9	<5	<2	25	.41	.3	.2	29	.36	.031	5	18	.12	211	.05	<3	.49	.01	.08	<2	<.2	10	<.3	<.2	3.2	2
12512	.8	25.7	4.4	64.7	63	31	10	295	2.92	4.5	<5	2	24	.37	.6	<.2	76	.40	.055	9	54	.48	76	.09	<3	1.13	.01	.06	<2	<.2	13	<.3	<.2	4.4	7
12513	.6	42.7	3.8	52.0	79	15	8	440	2.20	2.2	<5	<2	23	.21	.3	<.2	53	.40	.031	6	31	.47	87	.07	<3	.96	.01	.07	<2	<.2	15	<.3	<.2	3.9	1
12514	.6	7.3	3.6	41.6	33	10	4	854	1.15	1.2	<5	<2	18	.26	.2	<.2	30	.32	.049	5	22	.16	121	.05	<3	.71	.01	.08	<2	<.2	<10	<.3	<.2	2.8	2
12515	.7	9.2	3.7	48.5	43	11	5	259	1.17	1.3	<5	<2	19	.18	.2	<.2	34	.28	.035	6	27	.23	67	.06	<3	.72	.01	.05	<2	<.2	16	<.3	<.2	3.2	1
12516	.6	10.9	4.3	85.8	36	15	5	173	1.52	2.6	<5	<2	21	.20	.3	<.2	39	.32	.098	7	31	.25	129	.06	<3	1.00	.01	.06	<2	<.2	13	<.3	<.2	4.1	7
12517	.5	17.9	5.2	56.3	216	13	5	230	1.29	1.1	<5	<2	25	.30	.2	<.2	37	.40	.041	8	20	.18	113	.06	<3	1.01	.01	.06	<2	<.2	12	<.3	<.2	3.7	1
STANDARD	26.0	115.9	107.2	258.2	2013	31	17	994	4.54	76.1	27	19	63	1.98	9.0	22.1	70	.72	.108	18	50	1.10	238	.11	24	2.35	.06	.63	15	2.4	936	.4	2.0	6.5	54

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

ACME ANALYTICAL

Crest Geological Consulting PROJECT 177 FILE # 9801830

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12518	.3	8.5	2.9	29.2	<30	9	3	165	.90	1.0	<5	<2	18	.10	.2	<.2	27	.28	.018	7	21	.23	46	.06	<3	.64	.01	.04	<2	<.2	<10	<.3	<.2	2.1	<1
12519	.5	14.0	2.9	34.6	43	10	5	389	1.17	1.5	<5	<2	18	.13	.3	<.2	34	.28	.026	6	23	.25	57	.06	<3	.70	.01	.05	<2	<.2	23	<.3	<.2	2.5	9
12520	.3	8.9	3.3	25.5	52	8	4	392	.87	1.3	<5	<2	17	.15	.3	<.2	27	.26	.024	6	18	.20	62	.05	<3	.64	.01	.04	<2	<.2	12	<.3	<.2	2.2	<1
12521	.3	11.1	3.7	31.5	100	11	4	172	1.15	1.8	<5	<2	17	.12	.3	<.2	35	.25	.023	6	24	.24	61	.06	<3	.82	.01	.05	<2	<.2	12	<.3	<.2	2.7	27
12522	.3	10.7	3.3	29.3	<30	11	4	157	1.12	1.4	<5	<2	20	.09	<.2	<.2	33	.28	.015	7	24	.29	50	.07	<3	.81	.01	.05	<2	<.2	17	<.3	<.2	2.3	57
12523	.4	12.1	3.7	28.7	70	13	5	234	1.15	1.7	<5	<2	21	.10	.3	<.2	33	.30	.026	7	25	.31	64	.06	<3	.87	.01	.06	<2	<.2	15	<.3	<.2	2.7	11
12524	.3	11.2	4.5	24.8	68	13	4	192	1.10	3.2	<5	<2	21	.15	.5	.2	32	.34	.042	8	27	.32	58	.08	<3	.81	.01	.06	<2	<.2	15	<.3	<.2	2.4	1
12525	.4	5.7	4.4	23.4	40	6	3	121	.95	1.6	<5	<2	14	.12	.3	<.2	31	.22	.038	6	20	.12	53	.06	<3	.61	.01	.04	<2	<.2	13	<.3	<.2	2.8	1
12526	.3	4.3	2.0	71.1	149	12	11	507	4.32	1.7	<5	<2	19	.06	.2	<.2	70	.31	.033	4	15	1.80	118	.22	<3	2.70	.01	.31	<2	.2	11	<.3	<.2	6.1	<1
RE 12526	.2	4.5	2.0	71.0	113	12	11	502	4.22	1.4	<5	<2	17	.06	.2	<.2	68	.29	.033	4	16	1.80	115	.21	<3	2.66	.01	.31	<2	<.2	15	<.3	<.2	5.9	<1
12527	.3	8.3	2.9	36.0	<30	11	4	178	1.19	2.2	<5	<2	17	.12	.4	<.2	37	.27	.031	7	23	.23	48	.08	<3	.70	.01	.04	<2	<.2	17	<.3	<.2	2.5	<1
12528	.5	24.6	13.8	536.0	308	17	8	473	2.09	8.3	<5	<2	22	.92	.5	<.2	50	.36	.066	7	31	.46	91	.06	3	1.41	.01	.08	<2	.2	28	<.3	<.2	4.0	<1
12529	.5	15.1	3.9	37.9	420	11	5	233	1.48	3.0	<5	<2	22	.20	.5	<.2	42	.37	.038	7	26	.30	59	.08	<3	.76	.01	.05	<2	<.2	<10	<.3	<.2	2.8	<1
12530	.9	28.6	4.5	88.1	467	30	10	396	2.67	3.5	<5	<2	30	.30	.4	<.2	56	.42	.078	9	52	.58	127	.05	<3	1.88	.01	.13	<2	<.2	39	<.3	<.2	5.8	1
12531	.6	13.1	3.6	52.3	765	14	6	234	1.50	1.3	<5	<2	17	.23	.3	<.2	41	.25	.043	7	25	.31	59	.06	<3	1.02	.01	.05	<2	<.2	16	<.3	<.2	3.3	5
12532	.4	10.3	3.2	29.3	560	11	4	153	1.26	2.1	<5	<2	22	.11	.5	<.2	36	.31	.024	8	29	.28	50	.07	<3	.76	.01	.05	<2	<.2	14	<.3	<.2	3.0	<1
12533	.4	8.4	2.9	29.7	<30	11	4	191	1.13	1.3	<5	<2	17	.13	.3	<.2	35	.26	.032	8	23	.22	56	.08	<3	.73	.01	.03	<2	<.2	15	<.3	<.2	2.4	18
12534	.3	7.4	3.1	27.9	<30	10	3	175	.94	.9	<5	<2	18	.11	.2	<.2	29	.27	.023	7	21	.21	51	.08	<3	.70	.01	.04	<2	.2	13	<.3	<.2	2.6	3
12535	.4	14.9	4.1	43.2	850	17	6	269	1.49	1.6	<5	<2	20	.13	.3	<.2	41	.27	.045	8	32	.31	85	.06	<3	1.25	.01	.07	<2	<.2	20	<.3	<.2	4.0	2
12536	.3	9.3	4.0	24.4	167	10	4	353	1.06	1.5	<5	<2	16	.11	.3	<.2	32	.25	.036	8	22	.22	54	.06	<3	.74	.01	.04	<2	<.2	15	<.3	<.2	2.6	<1
12537	.6	15.2	3.3	59.3	859	22	7	186	2.09	3.6	<5	<2	23	.24	.5	<.2	53	.34	.120	5	36	.25	84	.05	<3	1.31	.01	.06	<2	<.2	26	<.3	<.2	3.4	<1
12538	.6	9.5	4.4	97.6	378	15	7	433	2.17	3.4	<5	<2	17	.42	.4	<.2	50	.30	.203	6	33	.24	198	.05	<3	1.41	.01	.06	<2	<.2	31	<.3	<.2	4.7	<1
12539	.4	8.4	3.5	40.5	206	14	6	334	1.51	2.2	<5	2	15	.16	.5	<.2	46	.26	.042	6	29	.18	109	.06	3	.80	.01	.05	<2	<.2	<10	<.3	<.2	2.6	6
12540	.8	21.0	3.8	152.0	748	20	10	600	2.45	5.0	<5	<2	38	.78	.6	<.2	49	.65	.169	6	35	.47	229	.07	3	1.46	.01	.12	<2	<.2	12	<.3	<.2	4.3	<1
12541	.6	43.9	4.6	56.9	374	38	13	507	3.20	26.6	<5	3	80	.17	1.7	<.2	70	.77	.116	16	46	.93	187	.19	<3	1.72	.01	.16	<2	.2	42	<.3	<.2	6.1	1
12542	2.1	64.4	6.2	84.8	791	30	13	1801	2.99	167.0	<5	<2	51	.38	8.6	<.2	62	.55	.097	12	33	.47	302	.04	<3	1.24	.01	.18	<2	.2	63	<.3	.2	4.2	11
12543	1.3	56.4	5.4	86.4	259	30	13	1000	3.05	101.2	<5	<2	62	.38	7.5	<.2	54	.70	.136	11	54	.43	249	.04	<3	1.36	.01	.16	<2	<.2	50	.3	<.2	4.0	<1
12544	1.3	84.3	6.2	52.5	518	50	15	2243	3.25	11.8	7	<2	45	.39	1.0	<.2	70	.73	.045	16	63	.53	225	.06	<3	1.95	.01	.14	<2	<.2	94	.5	.2	5.4	<1
12545	.9	36.3	4.1	47.2	212	23	10	843	2.35	7.9	<5	<2	56	.61	.8	<.2	54	.97	.025	6	39	.44	134	.08	3	1.33	.01	.19	<2	<.2	31	.4	<.2	4.0	1
12546	1.0	15.3	4.1	44.3	913	18	7	536	1.62	4.4	<5	<2	29	.46	.6	<.2	42	.44	.034	5	30	.24	157	.06	3	.85	.01	.12	<2	<.2	22	.3	<.2	3.1	2
12547	.5	6.5	3.2	53.3	532	10	5	305	1.16	1.8	<5	<2	17	.30	.3	<.2	30	.28	.077	5	21	.19	111	.04	<3	.71	.01	.07	<2	<.2	16	<.3	<.2	2.2	18
12548	.3	10.8	4.7	22.4	167	13	4	182	1.07	1.7	<5	<2	20	.06	.4	<.2	30	.30	.026	9	26	.28	56	.08	<3	.83	.01	.05	<2	.2	18	<.3	<.2	2.8	1
12549	.3	11.9	4.8	32.1	455	13	4	193	.98	.8	<5	<2	23	.09	.3	<.2	27	.33	.021	9	25	.25	83	.05	<3	1.00	.01	.05	<2	<.2	18	<.3	<.2	3.4	<1
12550	.3	8.4	4.2	21.3	<30	10	3	188	.93	1.4	5	<2	19	.09	.3	<.2	29	.30	.023	8	21	.27	53	.07	<3	.74	.01	.05	<2	<.2	15	<.3	<.2	2.4	1
STANDARD	23.1	121.4	94.2	251.8	2006	30	16	991	4.75	75.9	24	17	65	2.01	10.5	22.5	70	.70	.108	17	54	1.07	242	.11	25	2.28	.07	.73	15	2.3	965	.6	1.9	6.7	53

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

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Crest Geological Consulting PROJECT 177 FILE # 9801830

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12551	.5	8.7	2.4	39.4	38	10	5	276	1.23	.8	<5	<2	18	.15	.3	<.2	35	.30	.026	6	23	.23	53	.06	<3	.69	.01	.04	<2	<.2	10	<.3	<.2	2.4	2
12552	.9	96.8	5.1	92.6	437	63	12	575	3.55	2.9	<5	<2	44	.68	.6	<.2	60	.59	.061	14	75	.68	253	.06	<3	2.64	.02	.20	<2	<.2	29	<.3	<.2	7.0	3
12553	.6	19.6	3.3	36.7	279	14	6	201	1.91	1.8	<5	<2	26	.24	.4	<.2	48	.32	.023	7	30	.34	72	.07	<3	1.09	.01	.07	<2	<.2	20	<.3	<.2	4.0	1
12554	.9	46.0	2.8	52.9	749	23	13	1208	2.65	4.5	<5	<2	32	.27	.6	<.2	57	.60	.030	6	34	.62	84	.08	<3	1.55	.01	.08	<2	<.2	39	<.3	<.2	4.4	4
12555	.6	18.3	2.8	61.0	267	10	8	280	2.04	1.4	<5	<2	20	.38	.3	<.2	47	.37	.062	4	21	.30	101	.06	<3	1.09	.01	.06	<2	<.2	10	<.3	<.2	3.9	1
12556	.7	14.6	3.0	66.7	349	15	8	304	1.96	1.7	<5	<2	26	.26	.4	<.2	41	.41	.079	5	25	.33	107	.06	<3	1.16	.01	.10	<2	<.2	<10	<.3	<.2	3.6	1
12557	.2	10.6	2.7	35.8	<30	11	5	279	1.45	1.3	<5	<2	19	.12	.3	<.2	38	.32	.042	6	22	.31	69	.06	<3	.81	.01	.06	<2	<.2	<10	<.3	<.2	2.3	4
12558	.5	15.9	3.7	52.0	64	17	7	333	1.69	.9	<5	<2	23	.32	.4	<.2	41	.40	.042	6	27	.32	82	.07	<3	.92	.01	.09	<2	<.2	<10	<.3	<.2	3.0	1
12559	.2	9.1	3.0	25.5	<30	9	4	210	1.24	.8	<5	<2	21	.08	.2	<.2	33	.33	.026	6	21	.35	45	.09	<3	.78	.01	.08	<2	<.2	15	<.3	<.2	2.4	6
12560	.4	19.5	2.6	54.7	47	17	8	362	1.95	1.8	<5	<2	22	.09	.2	<.2	45	.32	.027	6	27	.48	84	.07	3	1.31	.01	.09	<2	<.2	19	<.3	<.2	3.7	3
12561	.4	10.6	3.0	40.8	<30	10	5	244	1.46	1.4	<5	<2	18	.20	.3	<.2	38	.29	.017	5	19	.34	62	.08	<3	.81	.01	.07	<2	<.2	<10	<.3	<.2	2.6	4
12562	.4	10.8	3.5	52.3	66	13	6	474	1.53	1.4	<5	<2	18	.25	.2	<.2	40	.27	.048	5	21	.27	76	.06	<3	.95	.01	.06	<2	<.2	22	<.3	<.2	2.9	2
12563	.3	13.4	3.2	31.6	143	14	5	339	1.17	1.8	<5	<2	23	.11	.4	<.2	32	.32	.020	8	22	.31	73	.07	<3	.85	.01	.06	<2	<.2	21	<.3	<.2	2.3	4
12564	.4	6.9	3.0	33.7	136	8	4	246	1.25	1.5	<5	<2	17	.17	.3	<.2	35	.27	.035	6	21	.18	54	.07	<3	.65	.01	.05	<2	<.2	<10	<.3	<.2	2.5	2
RE 12564	.4	6.6	3.0	34.5	51	8	4	261	1.24	1.4	<5	<2	16	.18	.3	<.2	36	.26	.036	6	20	.18	54	.07	<3	.64	.01	.04	<2	<.2	11	<.3	<.2	2.5	11
12565	.4	10.0	2.9	32.6	83	11	6	259	1.51	2.3	<5	<2	20	.08	.4	<.2	38	.37	.049	6	22	.28	89	.07	3	.88	.01	.05	<2	<.2	<10	<.3	<.2	2.8	1
12566	.4	10.2	2.8	39.0	<30	14	5	157	1.50	1.5	<5	<2	16	.06	.3	<.2	40	.28	.032	5	25	.24	87	.06	<3	.87	.01	.05	<2	.2	<10	<.3	<.2	3.0	3
12567	.5	10.4	3.9	106.8	65	17	7	807	1.63	1.4	<5	<2	18	.22	.3	<.2	38	.30	.078	5	25	.23	211	.05	<3	1.14	.01	.06	<2	<.2	14	<.3	<.2	3.9	48
12568	.4	6.0	2.9	28.2	<30	7	3	159	1.04	1.0	<5	<2	16	.11	.3	<.2	31	.24	.024	5	19	.12	74	.07	<3	.54	.01	.05	<2	<.2	<10	<.3	<.2	2.2	5
12569	.4	8.4	3.2	29.4	248	11	4	159	1.31	1.0	<5	<2	19	.11	.3	<.2	37	.27	.013	6	23	.21	51	.09	<3	.68	.01	.05	<2	<.2	13	<.3	<.2	2.6	3
12570	.4	7.7	3.4	34.8	77	11	4	377	1.15	.8	<5	<2	21	.18	.3	<.2	33	.32	.031	5	21	.18	61	.06	<3	.66	.01	.10	<2	<.2	11	<.3	<.2	2.2	3
12571	.4	8.0	3.0	30.0	<30	10	3	139	1.13	.7	<5	<2	18	.11	.2	<.2	33	.28	.020	7	22	.19	65	.07	<3	.69	.01	.05	<2	<.2	<10	<.3	<.2	2.5	4
12572	.4	12.6	3.5	36.5	<30	14	6	177	1.51	1.9	<5	<2	19	.15	.5	<.2	38	.33	.040	6	27	.29	34	.07	<3	.74	.01	.06	<2	<.2	<10	<.3	<.2	2.5	5
12573	.5	22.9	4.3	50.8	<30	24	7	384	2.38	.7	<5	<2	31	.16	.3	<.2	53	.37	.021	9	45	.39	84	.16	<3	1.20	.03	.09	<2	<.2	24	<.3	<.2	3.9	3
12574	.6	42.7	4.7	47.6	<30	23	8	399	2.00	1.3	<5	<2	25	.09	.3	<.2	48	.32	.020	7	36	.37	80	.10	<3	1.32	.01	.05	<2	<.2	28	<.3	<.2	4.0	3
12575	.7	191.1	7.0	93.4	68	73	21	775	4.31	4.7	<5	<2	39	.11	.5	.8	84	.52	.056	11	85	.87	240	.07	<3	3.46	.01	.15	<2	<.2	36	<.3	.2	7.4	3
12576	.5	29.4	5.3	56.4	<30	23	13	1081	2.42	1.9	<5	<2	20	.12	.3	<.2	57	.25	.039	7	39	.36	137	.07	<3	1.76	.01	.06	<2	.2	13	<.3	<.2	4.9	1
12577	1.0	18.3	6.5	75.7	<30	22	11	498	4.18	3.6	<5	<2	16	.09	.4	<.2	96	.23	.207	5	40	.53	108	.09	<3	2.60	.01	.06	<2	<.2	59	<.3	<.2	9.3	1
12578	.3	11.0	4.1	63.2	<30	18	9	572	1.79	.8	<5	<2	17	.08	.3	<.2	42	.27	.050	5	26	.32	128	.06	<3	1.36	.01	.06	<2	.2	<10	<.3	<.2	4.4	1
12579	.6	48.5	4.1	92.3	317	14	8	765	2.26	1.2	<5	<2	21	.29	.3	<.2	52	.31	.129	5	26	.30	122	.05	<3	1.40	.01	.07	<2	<.2	31	<.3	<.2	5.2	2
12580	.5	43.0	4.1	56.2	75	10	6	550	1.54	1.2	<5	<2	20	.18	.3	<.2	44	.24	.071	5	23	.19	118	.04	<3	1.13	.01	.03	<2	<.2	26	<.3	<.2	4.3	2
12581	1.2	70.6	4.7	60.5	<30	21	10	195	3.54	3.9	<5	<2	12	.07	.5	<.2	72	.18	.084	5	38	.37	90	.06	<3	2.57	.01	.07	<2	<.2	29	<.3	<.2	7.8	4
12582	1.4	26.6	6.5	69.9	242	19	7	395	3.87	3.6	<5	<2	11	.09	.6	<.2	75	.14	.190	6	36	.33	88	.07	<3	2.55	.01	.04	<2	<.2	67	<.3	<.2	9.4	1
12583	.7	20.0	5.1	64.1	155	22	7	326	2.32	2.0	<5	<2	12	.08	.4	<.2	51	.18	.081	5	35	.35	78	.05	<3	2.02	.01	.05	<2	<.2	33	<.3	<.2	5.4	10
STANDARD	23.9	122.1	96.9	262.7	1881	30	17	1042	4.77	76.4	27	17	65	2.01	8.8	18.5	72	.74	.110	17	55	1.12	245	.13	24	2.37	.07	.74	15	2.6	925	.7	2.3	7.3	53

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data h FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12584	.8	17.8	4.9	50.8	<30	15	7	356	1.95	1.5	<5	<2	28	.23	.4	<.2	40	.50	.137	6	37	.35	128	.04	<3	1.10	.01	.09	<2	<.2	27	<.3	<.2	4.0	4
12585	.6	14.6	3.8	35.1	86	15	6	391	1.54	2.6	<5	2	22	.09	.3	<.2	36	.50	.040	8	33	.44	62	.06	<3	.98	.01	.07	<2	<.2	28	<.3	<.2	3.3	<1
12586	1.4	36.8	8.0	183.5	177	9	26	836	3.17	31.1	<5	<2	30	1.07	.2	.2	82	.47	.171	5	20	.21	96	.05	<3	1.39	.01	.07	<2	<.2	33	<.3	<.2	6.4	<1
12587	.6	45.6	3.2	37.7	82	9	7	232	1.49	8.6	<5	<2	17	.11	.2	<.2	44	.28	.025	6	23	.28	38	.06	<3	.86	.01	.04	<2	<.2	23	<.3	<.2	3.3	1
12588	.9	58.7	6.5	89.6	61	39	13	459	3.13	17.0	<5	2	22	.26	.5	<.2	66	.30	.052	7	58	.52	204	.07	<3	2.35	.01	.13	<2	.2	32	<.3	<.2	6.3	<1
12589	1.4	119.0	6.5	101.2	197	40	13	580	4.06	6.2	<5	2	17	.14	.6	<.2	90	.24	.062	6	62	.61	124	.10	<3	2.92	.01	.07	<2	<.2	38	<.3	<.2	7.6	1
12590	.8	17.4	6.4	135.7	60	24	13	2037	2.60	2.2	<5	<2	20	.27	.2	<.2	49	.25	.136	6	31	.31	360	.06	<3	1.86	.01	.07	<2	<.2	32	<.3	<.2	6.2	1
12591	2.0	7.9	6.3	53.6	<30	9	5	277	3.15	3.2	<5	<2	8	.07	.2	<.2	64	.11	.198	5	21	.24	56	.07	<3	1.60	.01	.03	<2	<.2	106	<.3	<.2	9.0	<1
12592	1.4	31.2	8.1	143.1	291	13	11	3476	2.28	2.3	<5	<2	8	.62	.2	.3	41	.10	.259	6	21	.12	75	.02	<3	1.94	.01	.04	<2	<.2	126	<.3	<.2	6.5	1
12593	.8	33.8	4.2	65.1	547	7	8	912	2.16	1.1	<5	<2	17	.13	.2	<.2	42	.21	.068	4	13	.45	84	.08	<3	1.50	.01	.04	<2	<.2	38	<.3	<.2	6.0	<1
12594	1.0	14.7	4.6	64.2	85	17	11	1057	1.50	2.2	<5	<2	19	.17	.3	<.2	41	.29	.046	6	26	.25	187	.05	<3	1.11	.01	.06	<2	<.2	36	<.3	<.2	4.2	1
12595	.9	39.5	3.5	70.5	72	11	10	738	2.55	1.2	<5	<2	14	.09	<.2	<.2	40	.25	.072	4	19	.67	87	.06	<3	1.73	.01	.04	<2	<.2	49	<.3	<.2	5.8	2
12596	2.1	10.0	9.2	65.5	138	12	5	363	4.14	4.1	6	2	8	.09	.3	.2	90	.09	.179	6	31	.28	69	.09	<3	2.03	.01	.03	<2	<.2	108	<.3	<.2	13.5	<1
12597	.8	14.9	4.1	35.7	78	17	7	405	1.49	2.6	<5	<2	23	.11	.4	<.2	40	.31	.040	8	30	.33	78	.05	3	1.11	.01	.07	<2	<.2	12	<.3	<.2	4.2	<1
12598	.6	11.3	3.8	19.6	52	11	4	241	1.15	2.2	<5	<2	21	.07	.3	<.2	34	.31	.027	8	24	.27	51	.07	<3	.77	.01	.05	<2	<.2	10	<.3	<.2	3.0	<1
12599	.7	27.4	5.0	32.7	86	23	7	514	1.70	2.2	<5	2	28	.18	.4	<.2	41	.50	.022	10	40	.40	105	.06	3	1.27	.01	.08	<2	<.2	25	<.3	<.2	4.1	2
12600	.5	19.2	4.5	24.5	49	17	5	283	1.76	4.4	<5	2	25	.06	.5	<.2	45	.41	.038	9	43	.35	82	.09	<3	1.02	.02	.10	<2	<.2	38	<.3	<.2	3.4	1
RE 12600	.5	16.8	4.6	24.1	56	18	6	280	1.69	4.3	<5	2	25	.06	.5	<.2	45	.42	.038	9	40	.35	80	.09	<3	1.02	.01	.09	<2	<.2	30	<.3	<.2	3.5	2
12601	.6	23.8	3.3	42.8	72	18	8	220	2.15	3.9	<5	2	23	.27	.5	<.2	42	.41	.150	6	34	.48	87	.05	<3	1.26	.01	.05	<2	<.2	26	<.3	<.2	3.7	2
12602	.6	13.7	4.3	27.2	43	17	4	211	1.26	2.2	<5	<2	23	.10	.3	<.2	35	.36	.039	8	31	.34	57	.07	<3	.96	.01	.06	<2	<.2	14	<.3	<.2	3.4	6
12603	.9	21.5	4.8	100.0	171	35	12	284	3.03	3.6	<5	2	16	.23	.4	<.2	64	.28	.194	5	46	.27	93	.05	<3	2.24	.01	.06	<2	<.2	33	<.3	<.2	6.2	3
12604	.6	13.6	3.9	42.7	91	16	5	149	1.41	2.0	<5	<2	17	.12	.3	<.2	39	.28	.042	6	28	.29	58	.05	<3	1.01	.01	.04	<2	<.2	16	<.3	<.2	3.9	2
12605	.8	19.9	4.3	76.6	125	36	9	216	2.46	3.7	<5	<2	19	.20	.3	<.2	53	.29	.171	7	46	.30	124	.05	<3	1.98	.01	.05	<2	<.2	44	<.3	<.2	5.4	1
12606	.9	39.9	5.7	69.3	182	37	8	273	2.77	4.0	<5	<2	24	.09	.4	<.2	57	.37	.056	9	54	.60	144	.05	<3	2.17	.01	.12	<2	.2	48	<.3	<.2	6.1	3
12607	.5	11.8	3.3	25.0	37	12	4	186	1.19	1.9	<5	<2	16	.10	.2	<.2	31	.30	.028	7	23	.32	43	.05	<3	.75	.01	.05	<2	<.2	15	<.3	<.2	3.0	1
12608	.4	11.8	3.0	25.6	<30	11	4	172	1.13	1.4	<5	<2	16	.07	.2	<.2	33	.29	.026	6	24	.27	41	.06	3	.72	.01	.03	<2	<.2	13	<.3	<.2	2.8	1
12609	.6	15.9	3.5	59.3	77	18	6	242	1.96	3.2	<5	<2	19	.18	.4	<.2	47	.34	.121	8	41	.32	81	.06	<3	1.19	.01	.07	<2	<.2	17	<.3	<.2	3.8	2
12610	.6	19.6	3.1	44.5	46	17	6	268	1.68	3.0	<5	<2	22	.20	.4	<.2	40	.44	.053	7	29	.39	51	.06	<3	.92	.01	.05	<2	<.2	15	<.3	<.2	3.0	18
12611	.3	12.1	3.2	26.9	45	13	4	212	1.18	1.6	<5	<2	21	.10	.2	<.2	31	.37	.032	7	26	.31	61	.07	<3	.95	.01	.06	<2	<.2	21	<.3	<.2	3.0	1
12612	.4	8.7	3.5	24.4	54	10	3	157	.93	.5	<5	<2	14	.09	.2	<.2	27	.24	.024	6	21	.21	45	.06	<3	.71	.01	.04	<2	<.2	13	<.3	<.2	2.8	1
12613	.6	12.5	3.6	76.3	109	13	6	551	1.39	1.4	<5	<2	19	.31	.2	<.2	35	.31	.053	7	29	.25	99	.05	<3	.95	.01	.07	<2	<.2	23	<.3	<.2	3.3	2
12614	1.2	114.6	8.7	155.6	602	111	21	1746	5.84	5.0	<5	3	72	.80	.7	<.2	87	1.19	.071	21	123	.94	443	.06	<3	4.87	.02	.20	<2	<.2	78	.3	<.2	11.0	1
12615	.9	20.4	4.7	89.3	224	17	7	504	3.06	5.3	<5	<2	17	.34	.2	<.2	61	.31	.254	5	39	.30	88	.05	<3	2.06	.01	.07	<2	<.2	58	<.3	<.2	6.0	<1
12616	.9	15.0	4.6	89.8	238	13	6	168	2.82	3.3	<5	<2	14	.33	.2	<.2	60	.26	.279	5	35	.26	77	.04	<3	2.04	.01	.05	<2	<.2	49	<.3	<.2	6.2	<1
STANDARD	22.5	119.7	93.0	242.2	2077	28	16	1013	4.61	74.5	24	18	62	2.09	9.4	22.2	69	.76	.106	17	57	1.04	236	.11	25	2.23	.06	.66	14	2.4	939	.5	2.2	7.4	51

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

Crest Geological Consulting PROJECT 177 FILE # 9801830

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12617	.8	21.9	5.0	48.8	218	23	6	190	2.16	2.8	6	<2	19	.16	.4	<.2	47	.28	.068	8	40	.40	124	.06	3	1.65	.01	.07	<2	<.2	40	<.3	<.2	5.1	4
12618	.8	40.3	6.2	100.5	242	48	11	286	3.65	3.6	8	<2	28	.20	.4	<.2	68	.34	.095	8	69	.56	264	.05	<3	3.27	.01	.13	<2	<.2	42	<.3	<.2	9.3	1
12619	.9	38.3	6.4	90.4	201	47	9	296	3.18	3.9	6	<2	26	.14	.5	<.2	61	.31	.061	8	69	.60	187	.05	<3	2.72	.01	.14	<2	<.2	45	<.3	<.2	7.5	<1
12620	.5	14.5	4.1	41.5	165	19	7	217	2.20	2.2	8	2	19	.28	.4	<.2	60	.29	.064	8	43	.25	119	.07	3	.93	.01	.08	<2	<.2	34	<.3	<.2	3.7	8
12621	.5	16.4	4.0	47.6	164	14	7	183	2.00	2.6	5	<2	27	.28	.3	<.2	41	.42	.140	5	27	.33	108	.05	<3	1.26	.01	.07	<2	<.2	15	<.3	<.2	3.9	3
12622	.4	17.8	3.7	21.5	106	14	7	444	1.35	1.9	<5	<2	26	.10	.3	<.2	34	.41	.012	9	24	.31	97	.06	<3	1.01	.01	.04	<2	<.2	32	<.3	<.2	3.0	<1
12623	.5	16.1	3.9	28.6	85	15	6	176	1.72	2.9	<5	<2	19	.10	.4	<.2	45	.34	.047	6	28	.34	77	.06	<3	1.05	.01	.04	<2	<.2	24	<.3	<.2	3.2	2
12624	.6	15.9	3.2	32.4	37	13	5	160	1.70	3.2	5	<2	23	.13	.5	<.2	45	.35	.025	4	26	.30	109	.06	<3	.89	.01	.06	<2	<.2	10	<.3	<.2	3.2	<1
12625	.6	10.0	4.0	87.5	226	13	10	441	2.09	2.8	5	<2	18	.34	.2	<.2	45	.28	.165	5	26	.21	149	.05	<3	1.56	.01	.08	<2	<.2	23	<.3	<.2	4.7	<1
12626	.7	18.7	3.2	59.6	191	11	9	470	2.44	2.1	7	<2	16	.38	.3	<.2	49	.28	.113	4	23	.52	77	.04	<3	1.51	.01	.09	<2	<.2	29	<.3	<.2	4.8	<1
12627	.5	10.9	3.7	49.7	104	16	5	188	1.54	2.4	<5	<2	18	.28	.3	<.2	42	.28	.042	7	30	.25	97	.07	<3	.97	.01	.06	<2	<.2	26	<.3	<.2	3.3	46
RE 12627	.6	11.1	3.7	51.8	60	17	5	194	1.61	2.4	5	<2	19	.29	.4	<.2	44	.29	.044	7	32	.25	100	.07	<3	1.01	.01	.06	<2	<.2	22	<.3	<.2	3.4	1
12628	.5	12.4	3.6	45.9	51	18	6	225	1.57	3.0	8	<2	20	.20	.4	<.2	42	.31	.059	8	31	.27	95	.07	4	.94	.01	.06	<2	<.2	19	<.3	<.2	3.0	7
12629	.4	7.5	3.2	37.2	43	12	4	185	1.28	1.6	<5	<2	18	.13	.2	<.2	37	.26	.035	7	27	.18	83	.08	<3	.70	.01	.05	<2	<.2	10	<.3	<.2	2.7	1
12630	.5	6.4	3.3	68.4	<30	15	7	227	1.80	1.1	<5	<2	17	.10	<.2	<.2	45	.27	.036	6	30	.24	112	.08	<3	1.23	.01	.08	<2	<.2	14	<.3	<.2	3.5	1
12631	.6	8.8	3.6	38.4	102	10	5	604	1.40	1.5	<5	<2	17	.20	.3	<.2	36	.26	.030	7	24	.21	83	.07	<3	.83	.01	.07	<2	<.2	38	<.3	<.2	3.3	<1
12632	.5	9.1	3.9	59.2	113	14	6	206	1.51	1.9	<5	<2	20	.25	.3	<.2	38	.34	.088	6	30	.23	88	.06	4	1.01	.01	.05	<2	<.2	26	<.3	<.2	3.4	<1
12633	.7	27.9	3.7	70.6	150	20	7	229	2.23	3.8	<5	<2	19	.33	.5	<.2	49	.35	.111	6	36	.40	89	.06	3	1.26	.01	.07	<2	<.2	21	<.3	<.2	3.7	1
12634	.7	10.5	4.0	58.6	167	7	5	339	1.72	1.4	<5	<2	17	.20	.3	<.2	46	.30	.072	4	21	.30	106	.07	<3	1.10	.01	.07	<2	<.2	13	<.3	<.2	5.2	1
12635	.5	23.7	3.2	67.8	54	15	9	316	2.40	2.9	<5	<2	16	.13	.3	<.2	54	.30	.115	4	30	.39	122	.05	<3	1.48	.01	.07	<2	<.2	18	<.3	<.2	4.4	1
12636	.5	15.7	4.3	89.3	75	13	7	189	2.17	1.9	<5	<2	16	.17	.2	<.2	47	.25	.182	5	23	.28	286	.05	<3	1.60	.01	.07	<2	<.2	11	<.3	<.2	5.2	<1
12637	.6	20.4	5.1	132.2	145	14	7	415	2.38	2.4	<5	<2	24	.38	.3	<.2	49	.34	.205	5	28	.35	268	.06	<3	1.47	.01	.09	<2	<.2	22	<.3	<.2	5.9	2
12638	.5	17.5	3.6	44.6	181	21	8	362	1.84	2.1	<5	<2	24	.21	.3	<.2	50	.36	.029	6	40	.32	113	.06	<3	1.05	.01	.07	<2	<.2	16	<.3	<.2	3.5	1
12639	1.3	281.2	10.0	135.9	1500	155	24	971	7.26	8.9	<5	2	60	.78	.9	.5	104	1.29,	.083	29	147	1.21	1042	.06	<3	5.86	.02	.30	<2	<.2	123	.5	.2	12.6	4
12701	.6	17.5	4.2	28.8	155	9	4	140	1.19	1.5	5	<2	17	.10	.2	<.2	36	.26	.022	5	22	.22	70	.06	<3	.84	.01	.05	<2	<.2	<10	<.3	<.2	3.7	<1
12702	.5	13.1	4.1	33.7	128	12	5	269	1.25	1.9	<5	<2	18	.07	.3	<.2	36	.29	.029	7	27	.30	78	.06	<3	.91	.01	.04	<2	<.2	<10	<.3	<.2	3.5	99
12703	.4	7.1	3.7	24.3	54	7	4	283	.88	.7	<5	<2	14	.07	.2	<.2	27	.21	.022	5	17	.16	70	.05	<3	.62	.01	.04	<2	<.2	15	<.3	<.2	2.5	1
12704	.5	11.4	3.8	39.3	153	14	6	356	1.51	2.2	5	<2	27	.22	.3	<.2	36	.39	.097	5	28	.26	133	.04	3	.95	.01	.05	<2	<.2	20	<.3	<.2	3.2	1
12705	.4	13.0	2.9	40.9	68	15	5	221	1.38	2.1	<5	<2	25	.16	.3	<.2	35	.33	.073	4	27	.24	78	.04	<3	.85	.01	.05	<2	<.2	16	<.3	<.2	2.8	67
12706	.6	16.0	3.6	30.9	66	13	5	218	1.43	2.6	<5	<2	20	.10	.4	<.2	38	.35	.045	6	28	.34	67	.05	3	.90	.01	.04	<2	<.2	21	<.3	<.2	3.3	1
12707	.5	9.6	3.8	29.1	136	11	4	126	1.19	1.3	<5	<2	16	.09	.2	<.2	34	.26	.026	5	24	.19	79	.06	<3	.91	.01	.04	<2	<.2	20	<.3	<.2	3.2	1
12708	.3	10.5	3.9	22.0	74	11	3	157	1.14	2.2	<5	<2	17	.04	.3	<.2	34	.27	.036	6	24	.26	50	.06	<3	.82	.01	.04	<2	<.2	13	<.3	<.2	2.7	1
12709	.5	17.2	5.0	49.3	124	21	6	203	1.58	1.1	<5	<2	21	.05	.2	<.2	35	.29	.042	8	43	.38	113	.06	<3	1.59	.01	.08	<2	<.2	22	<.3	<.2	5.0	3
12710	1.1	19.7	4.2	101.1	178	21	9	194	3.08	3.5	<5	2	16	.24	.3	<.2	64	.28	.198	5	45	.36	126	.05	<3	2.47	.01	.06	<2	<.2	<10	<.3	<.2	6.5	1
STANDARD	24.4	118.0	106.6	255.3	2053	30	17	1025	4.74	76.7	26	17	65	1.98	9.6	15.8	72	.73	.109	17	54	1.11	317	.12	24	2.33	.06	.73	15	2.4	917	.3	2.3	6.8	52

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

Crest Geological Consulting PROJECT 177 FILE # 9801830

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12711	.7	8.9	3.9	41.7	528	12	5	348	1.25	1.6	6	<2	15	.17	.3	<.2	40	.25	.057	6	25	.19	79	.06	<3	.91	.01	.04	<2	<.2	16	<.3	<.2	3.2	1
12712	.8	11.7	4.3	100.5	344	12	5	152	1.72	2.0	<5	<2	28	.54	.3	<.2	47	.37	.171	5	28	.25	106	.05	<3	1.07	.01	.06	<2	<.2	<10	<.3	<.2	4.7	<1
12713	1.0	19.2	5.3	111.8	648	17	7	298	3.06	3.2	<5	2	23	.35	.4	<.2	70	.32	.431	5	38	.32	252	.04	<3	2.00	.01	.06	<2	<.2	57	<.3	<.2	6.2	2
12714	.7	13.5	4.0	40.1	254	16	4	123	1.83	1.8	<5	<2	22	.13	.3	<.2	51	.30	.060	6	29	.21	74	.06	<3	1.37	.01	.05	<2	<.2	26	<.3	.2	5.1	<1
12715	1.8	81.9	8.2	137.3	570	83	29	1080	5.35	10.0	<5	2	47	.16	.6	<.2	119	.50	.105	17	112	1.09	309	.04	<3	4.76	.01	.18	<2	<.2	78	<.3	<.2	12.5	1
12716	.4	9.7	3.7	21.1	118	9	3	136	.90	1.4	<5	<2	18	.08	.3	<.2	32	.27	.021	7	19	.23	43	.08	<3	.72	.01	.04	<2	<.2	11	<.3	<.2	2.7	1
12717	.3	8.7	3.8	27.7	213	10	3	181	.92	.7	<5	<2	16	.09	.2	<.2	30	.24	.020	7	21	.25	50	.07	<3	.76	.01	.04	<2	<.2	12	<.3	<.2	2.5	1
12718	.7	10.1	5.6	82.6	277	17	7	495	1.72	4.2	<5	<2	17	.26	.4	.2	42	.22	.269	6	35	.19	288	.04	<3	1.26	.01	.06	<2	.2	13	<.3	<.2	3.8	4
12719	.6	17.4	4.4	53.4	132	23	7	209	1.77	4.1	<5	<2	24	.14	.6	<.2	50	.32	.098	7	44	.39	95	.06	<3	1.16	.01	.07	<2	<.2	<10	<.3	<.2	3.6	1
12720	.3	58.8	2.3	60.0	307	12	12	523	3.47	3.5	<5	<2	27	.18	.4	<.2	95	.50	.065	4	26	.57	80	.11	<3	1.21	.01	.07	<2	<.2	16	<.3	<.2	4.2	3
12721	.6	9.5	4.1	36.4	554	9	4	179	1.11	1.1	<5	<2	14	.28	.3	<.2	34	.26	.065	5	22	.17	75	.05	<3	.72	.01	.05	<2	<.2	<10	<.3	<.2	2.6	2
12722	.7	14.2	3.5	29.2	161	12	6	195	1.35	3.4	<5	<2	20	.18	.5	<.2	42	.40	.036	6	32	.25	45	.07	<3	.69	.01	.05	<2	<.2	12	<.3	<.2	2.3	5
12723	.5	11.7	3.5	57.1	310	15	5	229	1.30	2.2	<5	<2	21	.23	.3	<.2	39	.34	.046	6	30	.27	75	.06	<3	.87	.01	.06	<2	<.2	11	<.3	<.2	3.0	<1
RE 12723	.6	11.4	3.6	59.5	152	17	6	231	1.41	2.2	<5	<2	22	.24	.3	<.2	41	.36	.048	6	32	.28	81	.07	<3	.90	.01	.08	<2	<.2	19	<.3	<.2	3.2	<1
12724	.4	5.5	2.9	24.1	153	5	3	156	.71	.7	5	<2	14	.21	.2	<.2	27	.25	.019	5	15	.11	44	.06	<3	.45	.01	.04	<2	<.2	<10	<.3	<.2	2.2	1
12725	.4	11.5	3.3	40.1	84	11	4	253	1.02	.8	<5	<2	18	.14	.3	<.2	34	.28	.016	6	26	.23	56	.06	<3	.72	.01	.05	<2	<.2	12	<.3	<.2	2.5	4
12726	.8	21.2	4.3	39.1	92	22	8	262	1.87	3.8	<5	<2	23	.14	.5	<.2	52	.34	.048	9	39	.39	93	.07	<3	1.11	.01	.08	<2	.2	14	<.3	<.2	3.3	5
12727	.7	14.9	3.4	45.3	84	13	6	219	1.69	1.9	<5	<2	18	.25	.4	<.2	44	.31	.101	5	33	.32	89	.05	<3	.96	.01	.08	<2	<.2	28	<.3	<.2	3.2	47
12728	1.1	41.9	4.7	99.0	174	18	11	549	2.86	6.1	<5	<2	36	.71	.6	<.2	62	.65	.053	6	36	.50	103	.06	<3	1.52	.01	.12	<2	<.2	29	<.3	<.2	5.5	4
12729	1.0	21.0	4.1	63.3	46	15	8	721	1.71	4.2	<5	<2	31	.49	.4	<.2	48	.55	.060	5	29	.32	111	.06	<3	.96	.01	.07	<2	<.2	<10	<.3	<.2	3.8	1
12730	1.0	68.6	4.3	102.3	115	23	12	696	2.43	5.1	<5	<2	34	.51	.5	<.2	58	.62	.056	13	41	.49	104	.06	3	1.41	.01	.09	<2	<.2	51	<.3	<.2	4.6	<1
12731	.6	28.0	3.8	49.8	663	16	9	368	2.46	4.4	<5	<2	28	.19	.5	<.2	59	.46	.040	6	27	.48	61	.09	<3	1.24	.01	.12	<2	<.2	<10	<.3	<.2	4.2	1
12732	.6	10.2	3.4	77.9	150	13	6	245	1.44	2.9	<5	<2	21	.32	.3	<.2	38	.29	.142	6	28	.24	90	.05	3	.98	.01	.06	<2	<.2	20	<.3	<.2	3.4	1
12733	.7	13.6	4.0	56.5	48	23	6	187	1.81	3.1	6	<2	20	.23	.5	<.2	47	.28	.136	7	38	.28	127	.05	<3	1.16	.01	.08	<2	<.2	35	<.3	<.2	4.0	1
12734	.8	31.1	3.7	54.0	<30	20	7	396	1.83	2.1	<5	<2	23	.12	.3	<.2	50	.35	.058	5	34	.39	105	.05	4	1.50	.01	.08	<2	<.2	33	<.3	<.2	4.7	3
12735	.8	43.1	6.6	114.0	<30	18	12	1160	2.30	1.9	<5	<2	27	.16	.2	<.2	60	.37	.185	7	35	.28	205	.04	3	2.04	.01	.09	<2	.2	37	<.3	<.2	6.8	3
12736	1.2	30.9	7.1	104.7	222	10	7	633	2.72	2.0	<5	<2	14	.19	.2	<.2	56	.19	.252	5	25	.22	113	.05	3	1.88	.01	.05	<2	<.2	87	<.3	<.2	7.7	1
12737	1.2	15.3	8.0	61.2	87	9	7	656	3.14	1.0	7	<2	11	.09	.2	<.2	81	.15	.076	5	20	.26	78	.12	<3	1.50	.01	.05	<2	<.2	61	<.3	<.2	10.0	<1
12738	1.3	528.2	5.2	58.7	1713	9	6	482	2.74	1.4	<5	<2	11	.10	.2	<.2	74	.17	.113	6	20	.19	69	.07	<3	1.59	.01	.04	<2	<.2	59	<.3	.2	6.3	2
12739	1.4	20.4	6.8	66.8	1032	20	7	378	2.66	2.1	<5	<2	12	.12	.4	<.2	79	.15	.054	6	36	.26	86	.08	<3	1.85	.01	.05	<2	<.2	30	<.3	<.2	8.1	<1
12740	.7	14.7	4.4	64.7	<30	23	8	394	1.61	1.1	6	<2	17	.10	.2	<.2	48	.23	.023	6	32	.31	124	.06	<3	1.49	.01	.05	<2	<.2	23	<.3	<.2	4.3	<1
12741	.7	20.8	4.7	79.6	<30	26	10	361	2.22	2.8	<5	<2	17	.11	.3	<.2	60	.24	.044	7	42	.38	100	.07	<3	1.72	.01	.06	<2	<.2	20	<.3	<.2	5.0	1
12742	1.0	29.2	5.6	102.9	<30	30	11	463	2.42	6.9	<5	<2	15	.23	.4	<.2	61	.22	.083	6	39	.44	132	.05	3	2.04	.01	.06	<2	<.2	46	<.3	<.2	5.9	<1
12743	.7	21.0	5.0	123.6	46	25	9	458	2.14	3.6	<5	<2	21	.26	.2	<.2	49	.29	.129	7	34	.34	156	.06	<3	1.64	.01	.08	<2	.2	24	<.3	<.2	5.5	<1
STANDARD	24.1	128.5	104.9	258.7	1785	30	16	1035	4.67	79.0	25	18	66	1.80	7.8	18.4	79	.72	.111	17	59	1.11	249	.13	25	2.36	.07	.82	16	2.3	916	.5	1.9	6.3	50

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

Crest Geological Consulting PROJECT 177 FILE # 9801830

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Tl	Hg	Se	Te	Ga	Au*
	ppm	ppm	ppm	ppm	ppb	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	ppm	ppb	ppm	ppm	ppm	ppb
12744	.8	14.2	5.0	51.8	<30	15	7	356	1.64	3.0	<5	<2	16	.17	.4	<.2	40	.27	.075	5	32	.31	89	.04	<3	.96	.01	.05	<2	<.2	13	<.3	<.2	3.6	1
12745	.6	8.2	3.9	36.5	<30	12	6	255	1.37	1.3	<5	2	17	.20	.4	<.2	38	.31	.023	6	29	.23	63	.06	<3	.74	.01	.05	<2	<.2	<10	<.3	<.2	3.0	5
12746	.8	16.1	7.2	50.6	59	16	6	183	1.85	3.6	<5	<2	18	.31	.6	<.2	45	.36	.088	7	37	.27	65	.06	<3	1.07	.01	.07	<2	<.2	12	<.3	<.2	4.6	2
12747	1.2	66.1	16.8	143.5	128	13	13	1195	2.54	1.9	<5	<2	17	.74	.3	<.2	52	.25	.103	6	21	.26	113	.05	<3	1.78	.01	.06	<2	<.2	75	<.3	<.2	7.2	1
12748	.9	24.7	5.5	92.7	85	9	9	1011	2.01	1.1	<5	<2	12	.43	.2	<.2	40	.16	.076	4	16	.39	118	.03	<3	1.59	.01	.05	<2	<.2	26	<.3	<.2	5.9	<1
12749	1.1	209.2	11.7	103.6	125	63	25	431	3.98	3.3	<5	3	23	.12	.4	<.2	83	.36	.081	8	64	.58	185	.05	<3	3.42	.01	.08	<2	.2	34	<.3	<.2	7.9	<1
RE 12750	.6	21.8	5.5	44.4	<30	23	10	405	2.04	2.2	<5	2	19	.07	.5	<.2	49	.28	.023	8	40	.39	106	.06	<3	1.42	.01	.06	<2	<.2	20	<.3	<.2	4.2	<1
12750	.6	18.8	5.5	41.9	<30	22	9	388	1.81	1.4	<5	2	17	.08	.4	<.2	45	.25	.021	8	36	.38	99	.05	<3	1.31	.01	.05	<2	<.2	14	<.3	<.2	4.0	3
12751	.3	12.1	3.9	58.8	50	14	7	179	1.27	1.1	<5	<2	20	.08	.2	<.2	35	.33	.026	6	26	.28	60	.07	<3	1.01	.01	.04	<2	<.2	<10	<.3	<.2	3.6	<1
12752	.6	35.2	6.2	56.5	119	36	14	301	2.78	3.0	<5	2	31	.10	.6	<.2	60	.53	.020	9	67	.62	98	.09	<3	1.75	.02	.13	<2	<.2	20	.3	<.2	5.1	1
12753	.6	24.8	4.2	50.4	89	27	8	341	2.09	1.5	<5	2	30	.17	.5	<.2	47	.52	.017	9	48	.38	88	.09	<3	1.28	.02	.09	<2	<.2	36	<.3	<.2	4.0	1
12754	.6	20.9	5.2	91.7	30	25	9	518	2.33	2.5	<5	2	18	.16	.4	<.2	54	.24	.109	6	45	.33	144	.07	<3	1.85	.01	.06	<2	<.2	23	<.3	<.2	5.5	3
12755	.5	10.3	3.9	46.0	54	15	5	221	1.68	1.4	<5	<2	21	.10	.3	<.2	44	.30	.059	6	32	.25	88	.09	<3	1.06	.01	.06	<2	<.2	<10	<.3	<.2	4.3	1
12756	.5	15.6	3.8	33.1	51	19	6	224	1.71	1.3	<5	<2	27	.06	.3	<.2	45	.38	.017	8	34	.38	62	.11	<3	.99	.02	.06	<2	<.2	18	<.3	<.2	3.5	<1
12757	.5	14.0	4.4	54.3	<30	20	8	142	1.98	.5	<5	2	23	.08	.2	<.2	52	.29	.019	7	37	.31	58	.11	<3	1.17	.01	.04	<2	<.2	<10	<.3	<.2	4.1	3
12758	.8	133.1	5.6	61.8	138	41	12	462	3.11	2.6	<5	3	41	.14	.5	<.2	69	.58	.031	15	64	.64	114	.10	<3	2.13	.02	.09	<2	<.2	30	<.3	<.2	6.1	2
12759	.9	65.3	6.3	82.7	190	57	14	627	3.81	3.9	<5	3	46	.36	.7	<.2	71	.81	.047	19	79	.72	207	.09	<3	2.43	.02	.14	<2	<.2	37	.3	<.2	6.7	1
12760	.6	15.0	4.9	87.0	75	27	9	165	2.46	1.6	<5	2	25	.31	.3	<.2	51	.31	.181	7	43	.28	125	.08	<3	1.64	.01	.08	<2	<.2	<10	<.3	<.2	5.4	<1
12761	.5	21.1	4.4	54.1	73	23	7	456	1.67	1.3	<5	2	24	.21	.4	<.2	43	.34	.027	9	41	.39	88	.07	<3	1.23	.01	.06	<2	<.2	13	<.3	<.2	3.9	<1
12762	.3	9.9	3.8	29.7	34	13	4	176	1.13	.7	5	2	21	.07	.2	<.2	30	.32	.012	7	28	.28	52	.10	<3	.84	.01	.05	<2	<.2	17	<.3	<.2	2.9	4
12763	.4	10.3	4.0	43.4	74	14	4	133	1.46	1.3	<5	2	22	.16	.3	<.2	41	.31	.045	7	31	.22	66	.07	<3	.91	.01	.05	<2	<.2	11	<.3	<.2	3.8	3
12764	.6	9.8	4.3	48.0	110	17	5	113	1.89	1.1	<5	<2	15	.13	.3	<.2	48	.25	.104	5	34	.21	77	.06	<3	1.25	.01	.05	<2	<.2	23	<.3	<.2	4.5	7
12765	.8	14.8	4.5	84.4	398	17	9	227	2.68	2.9	6	<2	21	.23	.3	<.2	62	.31	.184	6	31	.25	120	.06	<3	1.73	.01	.07	<2	.2	38	<.3	<.2	6.5	1
12766	.4	14.1	3.1	39.8	54	15	6	255	1.47	.9	<5	<2	20	.07	.3	<.2	38	.33	.015	6	28	.29	82	.07	<3	.89	.01	.05	<2	<.2	<10	<.3	<.2	3.0	<1
12767	.7	33.9	3.2	169.8	124	21	11	1070	2.85	2.7	<5	<2	55	.86	.5	<.2	55	.85	.152	4	31	.51	386	.06	<3	1.54	.01	.13	<2	<.2	21	<.3	<.2	4.3	<1
12768	.8	64.2	3.9	103.0	172	16	11	611	2.32	2.3	<5	<2	36	.55	.4	<.2	47	.50	.039	6	35	.37	215	.08	<3	1.17	.01	.10	<2	<.2	<10	<.3	<.2	4.1	1
12769	.6	26.4	2.7	40.5	47	11	8	191	2.19	3.2	5	2	26	.17	.4	<.2	53	.52	.082	5	23	.34	47	.06	<3	1.13	.01	.05	<2	<.2	<10	<.3	<.2	3.8	<1
12770	.6	60.7	2.4	260.2	116	7	12	1000	3.45	2.6	5	<2	29	.88	.3	<.2	57	.46	.049	2	8	.69	214	.11	<3	1.54	.01	.58	<2	.4	16	<.3	<.2	4.8	38
12771	.6	118.2	91.9	1217.6	437	17	18	2001	3.37	9.5	<5	<2	67	5.40	.5	<.2	37	6.33	.273	6	21	.88	202	.03	5	2.00	.01	.09	<2	.2	74	<.3	.2	4.7	1
12772	1.0	79.9	9.6	92.8	475	58	14	854	4.22	4.8	8	2	33	.61	.7	<.2	69	.87	.051	17	65	.76	196	.07	<3	2.53	.01	.17	<2	.2	56	.5	<.2	6.9	2
12773	.5	22.7	2.9	111.7	129	10	8	222	2.40	2.7	<5	<2	38	.59	.3	<.2	45	.62	.252	4	20	.37	161	.04	<3	1.20	.01	.05	<2	<.2	12	<.3	<.2	3.7	<1
12774	.7	13.7	3.1	71.0	108	14	9	227	2.02	1.9	6	<2	23	.33	.4	<.2	48	.40	.043	5	25	.35	76	.07	<3	1.01	.01	.07	<2	<.2	<10	<.3	<.2	3.8	<1
12775	.7	10.9	3.8	108.1	141	9	6	192	2.36	1.7	6	2	14	.37	.2	<.2	52	.25	.230	5	23	.24	84	.04	<3	1.45	.01	.04	<2	<.2	23	<.3	<.2	5.4	<1
12776	.6	18.3	3.4	62.3	177	28	9	213	2.12	2.4	<5	2	18	.19	.4	<.2	44	.27	.135	7	33	.35	79	.06	<3	1.45	.01	.06	<2	<.2	18	<.3	<.2	4.1	<1
STANDARD	24.4	120.8	98.1	257.2	1966	31	17	1018	4.77	76.7	22	20	66	1.92	10.3	21.3	72	.74	.109	17	56	1.13	249	.13	27	2.38	.06	.71	17	2.5	913	.3	2.1	7.0	55

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data 4 FA ____

Crest Geological Consulting PROJECT 177 FILE # 9801830

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12777	.5	9.3	3.6	26.3	106	11	4	199	1.18	1.3	<5	<2	18	.07	.2	<.2	35	.26	.023	7	22	.27	54	.07	<3	.86	.01	.04	<2	<.2	<10	<.3	<.2	3.1	3
12778	.5	9.2	4.1	32.0	388	12	4	163	1.14	1.0	<5	<2	17	.09	.3	<.2	32	.27	.019	8	21	.28	51	.07	<3	.83	.01	.03	<2	<.2	<10	<.3	<.2	3.0	1
12779	.7	16.9	4.1	65.7	167	16	7	206	2.26	3.3	<5	<2	35	.21	.4	<.2	50	.48	.115	7	31	.39	82	.07	<3	1.22	.01	.06	<2	<.2	<10	<.3	<.2	4.2	1
12780	.6	11.8	3.1	53.9	584	10	5	228	1.47	1.2	<5	<2	25	.24	.2	<.2	40	.35	.023	7	29	.22	90	.07	<3	.88	.01	.05	<2	<.2	17	<.3	<.2	3.5	2
12781	1.1	13.6	4.8	76.2	505	14	7	207	2.84	3.2	5	<2	16	.15	.3	<.2	58	.21	.191	6	31	.22	90	.05	<3	1.93	.01	.04	<2	<.2	47	<.3	<.2	6.3	<1
12782	.7	13.7	3.4	69.4	333	17	8	269	1.84	2.9	6	<2	16	.19	.4	<.2	43	.24	.125	5	28	.23	90	.05	<3	1.58	.01	.05	<2	<.2	36	<.3	<.2	4.6	<1
12783	.6	10.8	5.3	50.6	55	9	8	157	1.58	4.5	5	<2	18	.17	.2	<.2	44	.26	.050	6	24	.23	57	.06	<3	1.13	.01	.04	<2	<.2	<10	<.3	<.2	4.5	<1
12784	1.8	50.6	9.0	122.6	164	37	25	279	4.86	25.7	5	2	15	.13	.5	<.2	111	.13	.155	11	69	.37	138	.08	3	3.42	.01	.07	<2	.2	75	<.3	<.2	11.9	<1
12785	.7	17.7	4.5	41.7	52	17	7	250	1.85	4.7	<5	<2	31	.12	.6	<.2	47	.42	.070	9	39	.41	67	.08	<3	1.01	.01	.08	<2	<.2	<10	<.3	<.2	3.8	1
12786	1.0	18.3	7.0	159.4	208	18	13	655	2.52	3.1	<5	<2	24	.63	.4	<.2	53	.33	.191	6	40	.33	219	.06	<3	1.48	.01	.08	<2	<.2	15	<.3	<.2	5.5	<1
12787	.8	7.7	4.1	38.7	366	7	4	130	1.19	1.1	5	<2	22	.23	.3	<.2	38	.28	.021	4	20	.12	61	.05	<3	.55	.01	.06	<2	<.2	16	<.3	<.2	3.3	<1
12788	.8	11.1	4.9	115.5	101	9	7	285	1.43	1.1	<5	<2	29	.37	.2	<.2	36	.56	.039	5	24	.15	138	.06	<3	.84	.01	.05	<2	<.2	26	<.3	<.2	4.1	<1
12789	.8	11.6	5.4	75.8	355	13	8	483	1.62	2.0	5	<2	19	.38	.4	<.2	40	.32	.086	6	28	.24	132	.07	<3	.98	.01	.06	<2	<.2	12	<.3	<.2	4.6	4
12790	.7	19.1	6.2	96.7	130	19	10	558	2.35	2.2	<5	<2	34	.36	.3	<.2	48	.58	.223	7	34	.27	208	.06	<3	1.46	.01	.07	<2	<.2	14	<.3	<.2	6.1	2
12791	1.2	52.6	6.9	69.5	310	41	12	298	3.61	5.3	<5	<2	15	.12	.7	<.2	81	.20	.095	6	66	.57	106	.07	<3	2.82	.01	.08	<2	<.2	62	<.3	<.2	7.2	2
12792	.7	24.8	4.3	40.8	251	20	9	277	2.31	2.9	<5	<2	27	.08	.4	<.2	57	.40	.038	7	42	.46	109	.09	<3	1.53	.01	.07	<2	<.2	15	<.3	<.2	5.0	<1
RE 12793	.4	23.2	3.9	36.9	75	15	7	256	1.91	2.4	<5	<2	22	.06	.4	<.2	54	.35	.039	6	32	.39	76	.09	<3	1.18	.01	.05	<2	<.2	11	<.3	<.2	4.3	1
12793	.4	25.6	3.6	39.9	<30	16	8	273	2.09	3.0	<5	<2	24	.05	.3	<.2	58	.37	.042	6	35	.42	81	.10	<3	1.27	.01	.05	<2	<.2	19	<.3	<.2	4.1	<1
12794	.6	41.1	3.8	49.5	487	21	16	468	2.22	1.7	<5	<2	22	.09	.3	<.2	56	.33	.032	7	39	.42	88	.08	<3	1.44	.01	.06	<2	<.2	12	<.3	<.2	4.6	2
12795	.6	39.8	6.6	50.5	634	21	15	266	2.17	1.2	<5	<2	19	.07	.3	<.2	57	.28	.019	7	41	.35	71	.10	<3	1.46	.01	.05	<2	<.2	<10	<.3	<.2	4.6	1
12796	.5	76.6	7.0	80.5	447	30	11	328	2.57	1.9	<5	<2	25	.09	.3	<.2	62	.43	.026	9	54	.37	95	.10	<3	1.78	.02	.06	<2	<.2	16	<.3	<.2	5.6	4
12797	.6	32.3	5.9	63.1	30	38	12	531	2.93	2.7	<5	2	33	.24	.5	<.2	64	.52	.028	12	60	.53	101	.10	<3	1.66	.02	.11	<2	<.2	39	<.3	<.2	5.4	1
12798	.5	13.0	4.2	53.9	381	20	6	190	1.73	1.4	<5	<2	23	.19	.2	<.2	45	.30	.023	9	39	.30	68	.09	<3	1.07	.01	.07	<2	<.2	11	<.3	<.2	3.8	1
12799	.5	20.2	4.8	38.6	78	26	9	475	1.71	2.1	<5	<2	25	.12	.4	<.2	43	.38	.036	9	39	.43	93	.06	<3	1.21	.01	.07	<2	<.2	24	<.3	<.2	3.5	1
12800	.4	11.6	3.9	32.2	37	16	5	164	1.40	1.2	<5	<2	21	.07	.2	<.2	38	.30	.018	7	29	.33	65	.09	<3	.91	.01	.05	<2	<.2	<10	<.3	<.2	2.8	1
12801	.3	7.6	3.5	22.0	451	8	4	159	.95	1.1	<5	<2	18	.11	.2	<.2	32	.29	.019	7	21	.18	46	.07	3	.61	.01	.04	<2	<.2	<10	<.3	<.2	2.7	<1
12802	.4	8.9	3.7	24.9	102	10	4	152	1.13	1.1	<5	<2	17	.08	.2	<.2	35	.26	.021	7	23	.21	57	.07	<3	.82	.01	.04	<2	<.2	<10	<.3	<.2	3.0	6
12803	.3	11.1	4.3	30.2	67	14	5	249	1.46	2.3	<5	<2	22	.07	.3	<.2	39	.37	.040	7	30	.40	55	.09	<3	1.03	.01	.07	<2	<.2	<10	<.3	<.2	3.4	1
12804	.8	35.8	5.1	65.2	369	31	15	914	2.44	2.2	<5	<2	32	.28	.3	<.2	51	.43	.050	12	51	.58	147	.05	<3	2.00	.01	.11	<2	<.2	33	<.3	<.2	5.5	<1
12805	.7	21.9	3.9	47.1	395	20	9	504	1.88	1.7	<5	<2	25	.20	.3	<.2	43	.41	.031	10	34	.52	108	.05	<3	1.43	.01	.09	<2	<.2	12	<.3	<.2	3.9	<1
12806	.3	13.2	3.4	38.2	467	13	6	275	1.50	1.2	<5	<2	19	.12	.2	<.2	38	.29	.028	6	25	.42	72	.05	<3	1.13	.01	.06	<2	<.2	<10	<.3	<.2	3.6	3
12807	.5	21.3	3.8	53.1	105	21	8	551	1.93	2.0	<5	<2	24	.20	.3	<.2	45	.32	.041	9	36	.47	107	.05	<3	1.55	.01	.09	<2	<.2	30	<.3	<.2	4.7	<1
12808	.3	12.3	4.2	25.6	197	11	5	240	1.39	1.8	<5	<2	20	.05	.2	<.2	37	.35	.037	7	27	.45	45	.09	<3	1.00	.01	.07	<2	<.2	<10	<.3	<.2	3.3	1
12809	.6	36.9	4.7	57.4	452	35	11	467	2.89	5.5	<5	2	27	.15	.6	<.2	59	.71	.031	11	56	.62	111	.08	<3	1.80	.01	.13	<2	<.2	58	<.3	<.2	5.5	2
STANDARD	24.8	122.3	105.2	264.4	1983	31	17	1043	4.88	76.9	23	19	67	2.07	10.4	18.9	73	.75	.110	18	57	1.12	254	.12	27	2.38	.07	.74	17	2.5	959	.6	2.4	7.7	52

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

ACME ANALYTICAL

Crest Geological Consulting PROJECT 177 FILE # 9801830

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12810	.5	15.2	4.8	56.2	47	15	6	338	1.52	1.2	<5	<2	18	.17	.2	<.2	36	.24	.025	6	29	.41	81	.05	<3	1.13	.01	.06	<2	<.2	17	<.3	<.2	3.3	1
12811	.4	12.9	3.9	51.5	<30	13	6	259	1.46	1.1	<5	<2	16	.11	.2	.2	36	.24	.022	5	22	.40	83	.05	<3	1.04	.01	.06	<2	<.2	22	<.3	<.2	2.9	3
12812	.6	11.4	4.6	42.7	56	14	5	207	1.38	1.3	<5	<2	19	.11	.3	<.2	36	.25	.023	6	27	.33	66	.07	<3	.89	.01	.06	<2	<.2	10	<.3	<.2	2.9	2
12813	.7	9.5	4.8	32.9	31	9	4	432	1.26	1.7	<5	<2	20	.14	.3	<.2	36	.26	.039	6	24	.24	63	.06	<3	.77	.01	.06	<2	.2	12	<.3	<.2	2.7	<1
12814	.5	10.9	3.9	30.8	30	12	6	331	1.15	1.9	<5	<2	18	.09	.2	<.2	31	.28	.022	7	22	.28	64	.05	<3	.80	.01	.04	<2	<.2	11	<.3	<.2	2.2	<1
12815	.3	4.5	1.9	36.9	<30	12	5	279	1.38	1.6	<5	<2	16	.07	<.2	<.2	37	.25	.017	7	27	.24	116	.07	<3	.82	.01	.06	<2	<.2	15	<.3	<.2	1.6	2
12816	.6	4.8	2.8	231.1	<30	18	17	953	5.00	1.1	<5	<2	12	.04	<.2	<.2	107	.18	.087	4	40	1.32	171	.21	<3	3.20	.01	.09	<2	<.2	40	<.3	<.2	5.4	<1
12817	.3	3.7	2.0	27.3	<30	9	5	192	1.26	1.2	<5	<2	17	.04	.2	<.2	38	.24	.021	6	22	.22	44	.08	<3	.68	.01	.04	<2	<.2	<10	<.3	<.2	1.8	<1
12818	1.7	153.3	10.2	77.0	<30	32	9	346	3.00	5.6	<5	<2	16	.14	.6	<.2	70	.23	.086	6	47	.37	87	.08	<3	2.44	.01	.10	<2	<.2	47	<.3	<.2	7.5	3
12819	.8	51.7	5.6	41.4	<30	16	8	483	1.62	2.8	<5	<2	21	.07	.3	<.2	45	.33	.017	7	33	.31	73	.06	<3	1.37	.01	.05	<2	<.2	19	<.3	<.2	3.4	1
12820	.6	21.9	5.7	62.9	<30	29	9	192	2.27	4.0	<5	<2	19	.10	.4	<.2	51	.21	.044	8	43	.37	101	.07	<3	1.68	.01	.08	<2	<.2	24	<.3	<.2	4.4	2
12821	.5	11.0	4.8	29.2	<30	11	5	152	1.39	3.4	<5	<2	19	.13	.3	<.2	40	.26	.026	7	29	.24	39	.08	<3	.68	.01	.05	<2	<.2	13	<.3	<.2	2.4	<1
12822	.3	4.8	1.9	32.8	<30	13	5	164	1.31	1.9	<5	<2	21	.04	.2	<.2	38	.28	.021	7	31	.28	52	.08	<3	.83	.01	.05	<2	<.2	<10	<.3	<.2	1.4	<1
12823	.5	8.9	5.3	33.8	32	11	4	140	1.25	1.0	<5	<2	18	.09	.2	<.2	38	.27	.015	7	29	.21	53	.08	<3	.77	.01	.04	<2	<.2	10	<.3	<.2	2.7	1
12824	.5	12.6	5.6	38.7	918	14	8	590	1.61	3.5	<5	<2	26	.18	.3	.2	44	.36	.027	8	27	.31	93	.08	<3	1.00	.01	.06	<2	<.2	<10	<.3	<.2	3.3	2
12825	.9	26.0	10.7	74.8	<30	24	10	651	2.87	3.8	<5	<2	14	.10	.3	<.2	74	.16	.059	6	39	.36	100	.08	<3	2.06	.01	.06	<2	<.2	31	<.3	<.2	6.7	2
12826	.8	61.8	7.4	51.6	130	22	10	389	2.43	5.5	<5	<2	17	.13	.4	.2	62	.44	.031	6	32	.40	69	.08	3	1.66	.01	.06	<2	.2	10	<.3	.2	5.1	8
RE 12825	.8	27.6	9.7	78.6	<30	25	11	698	2.99	4.2	<5	<2	16	.10	.3	<.2	76	.18	.061	6	39	.37	106	.10	<3	2.19	.01	.06	<2	<.2	30	<.3	<.2	6.4	3
12827	1.9	234.2	9.3	117.6	99	54	28	2397	4.59	8.5	<5	<2	28	.16	.5	<.2	91	.58	.060	10	85	.81	187	.05	<3	3.16	.01	.12	<2	<.2	53	.3	<.2	8.4	1
12828	1.1	37.2	7.6	60.1	<30	10	7	245	2.92	5.3	<5	<2	17	.07	.2	<.2	77	.24	.130	5	26	.24	75	.07	3	1.72	.01	.05	<2	<.2	46	<.3	<.2	7.1	1
12829	.9	27.1	8.6	83.1	<30	28	12	414	3.33	5.7	<5	<2	15	.09	.4	<.2	81	.21	.086	6	53	.42	95	.08	<3	2.32	.01	.08	<2	<.2	23	<.3	<.2	6.9	1
12830	.6	74.4	9.8	70.2	100	31	9	292	2.51	6.3	<5	2	21	.18	.3	<.2	67	.46	.045	11	51	.51	111	.08	<3	2.51	.02	.06	<2	.3	20	<.3	<.2	6.5	<1
12831	1.4	14.3	8.5	255.8	120	5	6	636	3.33	10.8	<5	<2	14	.74	.2	.2	48	.28	.112	4	16	.12	51	.05	<3	1.02	.01	.04	<2	<.2	11	<.3	<.2	5.1	2
12832	.4	14.1	4.8	38.2	41	13	5	177	1.74	5.1	<5	<2	17	.15	.3	<.2	45	.29	.065	6	29	.39	47	.06	<3	.97	.01	.03	<2	<.2	24	<.3	<.2	2.9	1
12833	.7	27.0	5.7	35.5	174	20	8	318	1.66	4.5	<5	<2	26	.14	.3	<.2	44	.40	.028	8	36	.32	111	.05	<3	1.20	.01	.07	<2	<.2	22	<.3	<.2	3.7	3
12834	.4	6.4	1.9	43.3	<30	11	5	205	1.41	2.0	<5	<2	21	.06	<.2	<.2	38	.32	.033	6	26	.30	58	.06	<3	.91	.01	.04	<2	<.2	<10	<.3	<.2	2.0	3
12835	1.1	40.6	10.4	51.0	41	24	8	153	2.99	12.1	<5	<2	16	.05	.6	<.2	83	.14	.033	8	58	.41	93	.06	<3	2.17	.01	.06	<2	<.2	26	<.3	<.2	6.8	1
12836	1.0	71.0	8.1	91.3	164	36	22	621	3.51	20.8	<5	<2	14	.18	.6	<.2	77	.17	.106	5	46	.44	105	.07	<3	2.39	.01	.06	<2	<.2	31	<.3	.2	7.1	<1
12837	1.3	50.1	8.5	82.6	<30	37	16	565	3.40	17.6	<5	<2	19	.13	.6	<.2	81	.25	.068	6	55	.54	141	.07	<3	2.32	.01	.09	<2	<.2	35	<.3	<.2	6.9	2
12838	1.2	29.8	10.2	85.9	77	21	12	680	2.90	7.1	5	<2	16	.16	.4	<.2	75	.18	.093	5	37	.45	90	.06	3	1.86	.01	.05	<2	<.2	35	<.3	<.2	6.6	1
12839	.5	20.1	6.6	67.8	<30	24	13	412	2.09	11.4	<5	<2	14	.09	.2	<.2	44	.18	.088	5	30	.30	99	.05	<3	1.60	.01	.06	<2	<.2	24	<.3	<.2	3.9	4
12840	.6	10.5	4.7	56.6	<30	12	6	365	1.52	4.7	<5	<2	16	.16	.2	<.2	41	.22	.062	5	27	.24	65	.05	<3	.89	.01	.05	<2	<.2	20	<.3	<.2	2.9	2
12841	.5	13.0	4.7	48.1	<30	17	8	214	1.94	5.2	<5	<2	14	.07	.2	<.2	49	.18	.051	5	30	.34	77	.05	<3	1.34	.01	.04	<2	<.2	16	<.3	<.2	3.3	2
12842	1.4	35.0	9.7	137.7	<30	33	36	1221	4.53	9.4	<5	<2	14	.11	.5	<.2	85	.15	.209	6	56	.31	124	.05	<3	2.57	.01	.06	<2	.2	66	<.3	<.2	7.5	<1
STANDARD	23.8	119.6	102.6	262.4	1876	31	17	1023	4.76	77.3	18	19	65	1.92	9.5	21.5	72	.69	.109	17	54	1.13	245	.12	27	2.35	.06	.70	15	2.4	956	.3	2.2	6.7	51

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data 4 FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %
12843	1.2	31.2	7.6	79.3	<30	32	11	366	3.37	3.3	5	<2	18	.08	.5	<.2	77	.22	.077
12844	1.5	34.3	7.1	68.4	<30	20	9	548	3.61	3.4	<5	<2	16	.05	.4	<.2	87	.20	.087
12845	.5	9.4	3.9	147.5	70	20	7	264	1.65	1.6	<5	<2	24	.31	.3	<.2	37	.34	.133
13001	1.6	542.2	10.3	111.4	507	127	21	1798	4.69	6.2	6	2	56	.47	.7	1.0	78	.86	.071
13002	1.0	7.6	3.6	45.9	<30	9	5	207	2.67	1.4	<5	<2	12	.04	.2	<.2	50	.13	.072
13003	1.1	179.9	5.4	48.9	67	22	17	445	2.45	2.9	<5	<2	18	.04	.2	<.2	60	.24	.039
13004	1.6	62.8	11.4	214.6	139	86	97	2191	4.76	3.3	<5	<2	31	.16	.4	.2	89	.26	.179
13005	1.1	39.4	7.0	88.5	<30	26	13	362	2.77	4.1	<5	<2	16	.09	.3	<.2	57	.20	.137
RE 13005	1.0	43.2	6.3	86.1	<30	25	12	342	2.80	3.4	<5	<2	15	.08	.3	<.2	56	.18	.140
13006	1.1	46.5	7.4	73.1	<30	35	12	395	3.13	5.0	<5	<2	16	.09	.7	<.2	72	.18	.049
13007	.8	22.6	5.4	57.3	<30	23	9	316	2.60	4.4	<5	<2	15	.10	.5	<.2	54	.21	.115
13008	.6	10.2	4.5	57.9	<30	20	10	284	1.67	1.3	<5	<2	14	.07	<.2	<.2	39	.17	.081
13009	.9	48.3	5.9	58.4	39	26	16	384	2.17	12.3	<5	<2	21	.09	.4	<.2	53	.23	.038
STANDARD	26.2	122.0	105.1	269.7	1974	32	18	1047	4.77	76.0	21	17	66	1.97	9.4	18.9	73	.69	.110

SAMPLE#	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12843	6	48	.40	132	.08	<3	2.57	.01	.08	<2	.2	46	<.3	<.2	7.6	1
12844	6	38	.39	95	.08	<3	2.53	.01	.05	<2	.2	48	<.3	<.2	8.2	1
12845	7	27	.30	129	.06	<3	1.13	.01	.09	<2	<.2	13	<.3	<.2	3.8	1
13001	27	124	1.08	392	.04	<3	4.81	.02	.17	<2	.2	83	<.3	.4	9.3	1
13002	4	15	.23	46	.07	<3	1.73	.01	.03	<2	<.2	30	<.3	<.2	5.2	<1
13003	7	40	.51	77	.04	<3	1.78	.01	.05	<2	<.2	17	<.3	<.2	5.3	1
13004	7	79	.65	355	.05	<3	4.68	.01	.11	<2	.2	44	<.3	<.2	9.5	4
13005	6	35	.35	117	.06	<3	2.36	.01	.06	<2	.2	41	<.3	<.2	6.6	1
RE 13005	6	37	.34	117	.06	<3	2.33	.01	.06	<2	<.2	44	<.3	<.2	6.0	8
13006	6	56	.54	133	.07	<3	2.40	.01	.07	<2	<.2	26	<.3	<.2	6.5	1
13007	6	44	.44	81	.05	<3	1.82	.01	.06	<2	<.2	32	<.3	<.2	5.1	1
13008	5	25	.26	95	.05	<3	1.41	.01	.04	<2	<.2	23	<.3	<.2	4.1	2
13009	8	46	.52	90	.05	4	1.55	.01	.06	<2	<.2	27	<.3	<.2	4.7	5
STANDARD	18	54	1.15	248	.12	27	2.45	.07	.76	16	2.6	970	<.3	2.3	7.5	54

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data ___ FA ___

ACME ANALYTICAL

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
13010	.4	13.2	4.2	32.4	121	16	5	268	1.38	1.5	<5	<2	22	.12	.4	<.2	37	.29	.026	8	28	.32	78	.06	<3	1.21	.01	.05	<2	<.2	27	<.3	<.2	3.1	<1
13011	.2	7.3	4.3	19.9	36	9	3	137	.93	1.4	<5	<2	20	.05	.2	<.2	29	.32	.013	7	21	.25	44	.09	<3	.77	.01	.04	<2	<.2	<10	<.3	<.2	2.0	1
13012	.4	10.9	4.2	24.0	52	13	4	242	1.27	2.1	<5	<2	26	.07	.3	<.2	37	.41	.030	8	31	.32	59	.09	<3	.95	.01	.06	<2	<.2	14	<.3	<.2	2.5	<1
RE 13012	.3	10.7	4.3	24.5	64	12	4	235	1.23	1.8	<5	<2	24	.07	.3	<.2	35	.39	.030	8	28	.32	57	.08	<3	.92	.01	.05	<2	<.2	15	<.3	<.2	2.2	<1
13013	.8	43.3	6.1	80.9	164	54	14	1186	3.30	3.2	<5	2	41	.32	.5	<.2	66	.48	.043	18	76	.71	241	.07	3	2.80	.02	.13	<2	<.2	51	.3	<.2	6.5	<1
13014	.6	10.3	3.1	33.2	39	12	5	195	1.22	.8	<5	<2	18	.12	.3	<.2	35	.30	.011	6	25	.24	52	.08	<3	.80	.01	.04	<2	<.2	<10	<.3	<.2	2.4	<1
13015	.4	8.4	3.8	18.8	<30	9	3	166	1.04	1.1	<5	<2	22	.06	.2	<.2	32	.34	.021	8	21	.28	43	.08	3	.78	.01	.04	<2	.2	<10	<.3	<.2	2.4	1
13016	.3	8.7	3.5	31.1	<30	10	4	158	1.09	.6	<5	<2	21	.06	<.2	<.2	33	.33	.009	6	20	.26	57	.08	<3	.92	.01	.04	<2	<.2	<10	<.3	<.2	2.5	<1
13017	.5	16.3	3.3	50.1	94	18	7	321	2.03	1.3	<5	<2	23	.11	.3	<.2	46	.34	.024	8	33	.53	75	.07	<3	1.47	.01	.07	<2	<.2	22	<.3	<.2	3.6	<1
13018	.6	12.7	3.7	41.7	90	15	5	254	1.66	.7	<5	<2	25	.08	.2	<.2	39	.35	.019	8	28	.47	68	.09	<3	1.31	.01	.06	<2	.2	11	<.3	<.2	3.6	<1
13019	.4	10.7	3.6	32.5	51	13	4	219	1.37	.9	<5	<2	25	.08	.2	<.2	36	.37	.025	8	26	.40	60	.09	<3	1.13	.01	.06	<2	<.2	22	<.3	<.2	3.0	2
13020	.6	7.3	3.4	38.9	44	8	4	183	1.46	1.0	<5	<2	21	.14	.2	<.2	41	.31	.045	7	25	.20	57	.09	<3	.82	.01	.05	<2	<.2	<10	<.3	<.2	3.1	1
13021	.4	13.5	3.2	56.5	58	15	7	366	1.87	1.0	<5	<2	24	.10	.3	<.2	49	.37	.018	6	31	.60	79	.10	3	1.34	.01	.08	<2	<.2	20	<.3	<.2	2.9	<1
13022	.4	6.3	2.7	22.2	65	7	3	137	.97	<.5	<5	<2	16	.09	.2	<.2	30	.24	.018	6	17	.18	42	.07	<3	.60	.01	.04	<2	<.2	<10	<.3	<.2	2.1	15
13023	.5	13.2	3.5	55.6	78	12	8	470	2.13	2.3	<5	<2	27	.12	.4	<.2	50	.45	.037	6	24	.59	72	.14	<3	1.23	.01	.10	<2	<.2	10	<.3	<.2	3.8	3
13024	.5	11.0	3.4	41.6	46	11	5	187	1.29	.9	5	<2	20	.09	.2	<.2	38	.30	.015	7	22	.26	59	.08	<3	.89	.01	.04	<2	.2	<10	<.3	<.2	2.9	1
13025	.7	35.7	4.0	54.7	135	30	10	582	2.44	3.6	<5	<2	29	.11	.4	<.2	57	.37	.037	10	44	.58	127	.06	3	1.87	.01	.09	<2	.2	32	<.3	<.2	5.1	<1
13026	.6	11.5	3.3	32.9	35	15	6	248	1.61	2.0	<5	<2	21	.12	.3	<.2	42	.32	.048	7	28	.29	66	.08	<3	.90	.01	.05	<2	<.2	11	<.3	<.2	2.9	1
13027	.5	10.3	3.6	53.4	37	14	6	215	1.61	.9	<5	<2	20	.12	.3	<.2	42	.32	.042	7	27	.31	67	.08	<3	.96	.01	.05	<2	<.2	<10	<.3	<.2	2.9	5
13028	.5	13.1	3.0	26.0	<30	14	6	205	1.62	1.8	<5	<2	22	.05	.4	<.2	43	.37	.022	7	27	.31	76	.09	<3	.80	.01	.04	<2	<.2	<10	<.3	<.2	2.6	1
13029	.7	10.6	3.2	38.4	76	16	7	228	1.72	1.3	<5	<2	19	.11	.4	<.2	48	.34	.030	5	30	.30	87	.08	3	.99	.01	.04	<2	<.2	11	<.3	<.2	3.2	1
13030	.5	17.2	3.5	30.4	41	16	6	162	1.83	2.4	<5	<2	17	.07	.4	<.2	51	.30	.035	5	32	.30	52	.07	<3	1.07	.01	.04	<2	.2	<10	<.3	<.2	3.1	1
STANDARD	24.9	125.3	105.7	263.3	1938	31	17	1021	4.78	72.8	21	19	62	1.98	10.0	18.0	72	.70	.107	17	58	1.12	242	.13	27	2.39	.06	.68	16	2.3	945	.6	1.8	6.3	53
13031	.7	11.1	3.8	32.5	<30	15	6	177	1.65	2.0	<5	<2	22	.11	.6	<.2	45	.34	.029	8	28	.32	43	.09	4	.85	.01	.04	<2	<.2	13	<.3	<.2	2.4	5
13032	.3	8.8	3.8	22.2	39	11	3	298	1.10	1.6	<5	<2	26	.08	.3	<.2	32	.34	.021	7	19	.26	64	.07	<3	.87	.01	.03	<2	<.2	15	<.3	<.2	2.3	1
13033	.4	9.2	3.8	32.7	59	10	4	247	1.15	1.9	5	<2	18	.18	.3	<.2	33	.28	.021	7	22	.23	42	.06	3	.79	.01	.04	<2	<.2	16	<.3	<.2	2.1	2
13034	.5	13.0	4.0	40.6	38	15	6	242	1.85	3.3	<5	<2	23	.22	.4	<.2	45	.39	.076	8	27	.42	59	.07	3	1.07	.01	.04	<2	<.2	12	<.3	<.2	3.0	1
13035	1.1	93.9	6.6	93.1	376	65	13	684	3.95	4.7	<5	<2	51	.40	.6	<.2	69	.66	.060	21	76	.79	247	.06	<3	3.24	.02	.17	<2	<.2	58	.3	<.2	7.5	2
13036	.8	16.3	4.4	73.6	154	16	6	233	2.28	4.3	<5	<2	22	.24	.5	<.2	51	.38	.080	8	31	.43	64	.08	3	1.30	.01	.05	<2	<.2	21	<.3	<.2	3.7	<1
13037	.5	15.4	3.3	92.6	94	15	11	530	3.43	2.7	<5	<2	24	.13	.5	<.2	67	.42	.075	5	29	.71	104	.16	4	1.61	.01	.16	<2	<.2	20	<.3	<.2	4.5	14
13038	.9	19.4	4.8	23.5	59	5	4	186	1.89	.6	<5	<2	13	.03	.2	<.2	60	.18	.034	5	17	.18	50	.07	<3	1.21	.01	.02	<2	<.2	29	<.3	<.2	5.9	2
RE 13038	.6	18.9	5.5	23.2	79	5	3	179	1.86	.6	<5	<2	13	.04	.2	<.2	60	.18	.033	5	17	.17	49	.07	<3	1.21	.01	.02	<2	<.2	24	<.3	<.2	6.4	<1
13039	.4	41.9	3.2	93.3	40	17	12	420	3.86	3.0	<5	<2	25	.10	.5	<.2	82	.46	.031	4	29	.78	91	.18	<3	2.05	.01	.13	<2	.2	<10	<.3	<.2	5.0	1
13040	.6	10.0	4.1	36.0	101	11	5	214	1.36	1.2	<5	<2	20	.11	.3	<.2	41	.28	.016	8	23	.27	53	.09	4	1.02	.01	.04	<2	<.2	<10	<.3	<.2	3.3	2
13041	.7	16.4	4.5	55.5	93	22	7	332	1.97	2.2	<5	<2	26	.11	.3	<.2	51	.33	.024	9	36	.41	85	.08	4	1.53	.01	.07	<2	<.2	22	<.3	<.2	4.0	<1

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA ____

APPENDIX II

SOIL SAMPLING METHODOLOGY
ANALYTICAL TECHNIQUES

SOIL SAMPLING METHODOLOGY and ANALYTICAL TECHNIQUES

Soil sampling was carried out along grid lines with sampling at a 50m spacing. Alternate lines were sampled at 50m also except that sample stations are offset by 25m so that the "implied" sampling "screen" is approximately 25m when the data is contoured.

B horizon material was sampled where available and placed in kraft sample bags and given a unique sample number. All samples were analysed for 35 elements by ultratrace ICP methods, gold by GF/AA analysis and mercury by cold vapour A.A. at Acme Analytical Laboratories Ltd., Vancouver, B.C. A detailed description of analytical reagents and procedures are listed on the first page of the analytical certificates.

ROCK SAMPLE ANALYTICAL TECHNIQUES

All rock samples were analysed for 30 elements by ICP methods used a 30gm aliquot , gold by atomic absorption (AA) and mercury by flameless AA at Acme Analytical Laboratories Ltd., Vancouver, B.C. A detailed description of analytical reagents and procedures are listed on the first page of the analytical certificates.

APPENDIX III

COPPER KING NORTH GRID

GEOPHYSICAL SURVEY REPORT

GEOPHYSICAL INTERPRETATION REPORT

on the

COPPER KING NORTH GRID PROJECT NO. 177

CARIBOO MINING DIVISION, B.C.   N.T.S. 93B/8,9

Latitude: 52° 33′ N, Longitude: 122° 10′ W

Prepared for:

UNITED GUNN RESOURCES LTD.

by

E. Trent Pezzot, B. Sc., P. Geo.

S.J.V. Consultants Ltd.

Date of Work: July 10-12, Aug. 8-13, 1998

Date of Report: November 24, 1998

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SJ Geophysics Ltd/S.J.V. Consultants Ltd. 11762 - 94th Ave., Delta, B.C. Canada
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List of Plates

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Introduction

S.J.V. Consultants Ltd. was commissioned to process and interpret geophysical data gathered across United Gunn Resources Ltd.'s Copper King property in central B.C. The geophysical data was gathered by Crest Geological Consultants Ltd. and included some 26.4 line km of total field magnetic and vlf-em surveys gathered across the North grid.

The geophysical surveys were completed as part of a larger exploration program that included geological mapping and geochemical sampling. Most of the property appears to be underlain by altered quartz diorite and the exploration targets are described as shear hosted disseminated copper mineralization. It was the intention of the geophysical surveys to assist in the general geological mapping of the area as well as to delineate magnetic and/or conductivity responses that may be related to fault and shear zones.

This report is intended to be used as an addendum to a more complete report being prepared by Crest Geological Consultants Ltd. Readers are referred to Crests' report for detailed descriptions of the claims, their ownership, geology, previous and concurrent work.

Location and Access

The project area is located approximately midway between Quesnel and Williams Lake, B.C., in the Cariboo Mining Division and N.T.S. 93B/8,9. The approximate geographical co-ordinates near the centre of the North grid are latitude 52° 31' N and longitude 122° 13' W.

The project is located approximately 18 km east of B.C. highway #2. Several logging and forestry roads provide access to various parts of the properties.

Geology

The Geological Survey of Canada Map 12-1959 shows the claims lie along the western flank of the Granite Mountain - Dragon Mountain range. The area is mapped as undifferentiated granitic rocks. It falls along a linear feature extending up the Fraser

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River valley that appears to be a zone of faults and of tight folds. No single, large fault has been traced along it.

No detailed geological maps of the areas were available. Project geologist Craig Payne describes the properties as being primarily underlain by medium to coarse grained quartz diorite. In some areas, the quartz diorite shows chlorite, sericite, epidote and/or sauserite alteration.

Exploration targets are shear hosted copper mineralization. Localized faults and shears are expected to be oriented NW-SE, roughly perpendicular to the more regional alteration trends.

Geophysical Surveys and Processing

A survey grid comprised of 11 NE-SW oriented lines, nominally spaced at 200 metre intervals, was established.

Total field magnetometer and inphase, quadrature and field strength measurements for two vlf-em transmitters were recorded at 12.5 metre station increments along these lines. A GEM GSM-19 combination magnetometer and vlf-em instrument was used as a field unit. Diurnal variations were recorded on a second GEM GSM-19 magnetometer located in the grid area and appropriate corrections were applied to the field data. The Seattle vlf-em frequency (NLK 24.8 kHz) was recorded on all lines. Either Cutler (NAA 24.0 kHz) or Hawaii (NPM 23.4 kHz) was recorded as a backup. The data from these backup stations was plotted and analyzed but did not assist in the interpretation. This data is not included in this report.

Geophysical data was provided to S.J.V. Consultants Ltd. as a digital file with all appropriate leveling corrections applied. All data was registered to the NAD 83, Zone 10 UTM co-ordinate system. Digital base maps (Autocad format) showing the grid position with respect to the UTM co-ordinates, claims, streams, roads and topography were also provided.

Final processing and maps were produced by S.J.V. Consultants Ltd. in Vancouver, using AutoCad, Geopak and RTICAD software.

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Discussion of Results

The magnetic and vlf-em data are presented in both stacked profile and contour formats. In addition to UTM coordinates, the survey grid, claim outlines, topography and streams provide common reference points on all maps. Plots are numbered from Plate 7a to 9a. This scheme was chosen to avoid confusion with plots generated for two other grids (Mid and South) on the same project, that had been surveyed earlier this summer.

Based on discussions with the project geologist Craig Payne, it is understood that the exploration targets are shear hosted, disseminated copper mineralization hosted in an altered quartz diorite stock. Survey lines were oriented NE-SW, perpendicular to the expected strike of the shear zone targets. This orientation provided minimal coupling to large NE-SW trending alteration zones mapped to the southwest of the survey grids.

Magnetic Survey

The magnetic data is presented in stacked profile format as plate G-7a and in contour form as plate G-7b.

There are two clear magnetic signatures in this data. Very quiet, low amplitude data recorded along the southern lines and eastern portions of the rest of the lines is indicative of underlying sedimentary rocks. The bulk of the survey area reflects moderate to high, amplitude magnetic intensities. The "choppy" nature of this signal suggests the underlying rocks are volcanic. There is a distinct magnetic gradient that follows the contact between these two rock units.

There are a number of areas within the volcanic response that exhibit very high magnetic amplitudes. These anomalies tend to align in a NW-SE (N35°W to N50°W) direction and form linear features, between 50 and 250 metres wide, that extend for 200m to 1000m in length. Additionally, there are a number of strong magnetic responses that appear to be localized on single lines.

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Vlf-em Survey

The Seattle vlf-em data is presented in stacked profile format as plate G-8a and the fraser filtered inphase component is presented as contours on plate G-8b.

There are over 50 well-defined conductive responses evident in the vlf-em data. These responses have been flagged on both the stacked profile and compilation maps. Neither the Cutler nor the Hawaii data provided any additional information.

Approximately one quarter of the vlf-em defined conductors correlate with streams and/or topographic breaks. They are likely directly attributed to these features and have been highlighted accordingly. Several of these, however, also correlate with magnetic anomalies and some exhibit very high amplitudes. Although these anomalies may coincide with streams, they are likely due, in part, to underlying geological sources.

Many of the conductors coincide with magnetic anomalies. In some cases elongated magnetic highs directly overlie conductors but in most cases the conductors lie along the flanks of the magnetic trends. In these instances, the conductors are likely mapping a geological contact.

The contour display of the fraser filtered inphase component gives the impression that most of the conductors align in a NW-SE direction. This is due to a combination of the wide (200 m) line spacing and gridding algorithm and is slightly misleading. Although this is the dominant structural trend, several of the conductors can be clearly seen in the stacked profile display to align along different azimuths.

Summary and Conclusions

An exploration program, including magnetic and vlf-em surveys, was conducted by Crest Geological Consultants Ltd. across the Copper King North Grid, on behalf of United Gunn Resources Ltd. Approximately 26 line kilometers of geophysical data were forwarded to S.J.V. Consultants Ltd. for plotting and analysis. The geophysical data was examined to assist in the general geological mapping of the area as well as to identify any anomalous responses that may be of exploration interest.

The compilation map, plate G-9a, overlies a simplified magnetic contour map and interpreted vlf-em conductor axes with the topographic base. An area of quiet and low amplitude magnetics located along the southern and eastern portions of the grid likely outlines an area underlain by sedimentary rocks. The northwestern portion of the grid is

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characterized by relatively "choppy" and higher amplitude magnetics that likely reflect a volcanic host. Several NW-SE oriented trends within the volcanics highlight underlying units and structures.

A number of conductivity anomalies are mapped across the grid. Some coincide with and are attributed to streams and topography. Several coincide with magnetic anomalies and may be mapping discrete geological units or contacts.

A small band of high magnetic amplitudes in the NE corner of the grid forms a 300 metre wide, 600 metre long unit, trending NW and open in that direction. This magnetic feature may reflect a window of volcanics or an alteration zone within the sedimentary host.

Recommendations

The geophysical interpretation presented here should be correlated with the geochemical and geological data, as it becomes available. Hopefully, several of the mapped magnetic and vlf-em lineations can be identified through normal geological mapping and prospecting techniques. Recommendations for future work will be contingent upon this exercise.

Coincident geochemical, geological and geophysical anomalies will warrant further examination. Targeted areas will require additional geophysical data to be gathered at a higher density. A maximum line separation of 100 metres will likely be recommended.

Respectfully submitted

per S.J.V. Consultants Ltd.

PROFESSIONAL
PROVINCE OF
E. T. PEZZOT
BRITISH COLUMBIA
GEOSCIENTIST

E. Trent Pezzot, B.Sc., P.Geo.

Geophysics, Geology

APPENDIX 1

Statement of Qualifications

I, E. Trent Pezzot, of the city of Surrey, Province of British Columbia, hereby certify:

- I graduated from the University of British Columbia in 1974 with a B.Sc. degree in the combined Honours Geology and Geophysics program.

- I have practised my profession continuously from that date.

- I am a registered member of the Association of Professional Engineers and Geoscientists of British Columbia.

- I hold no direct or indirect interest in, nor expect to receive any benefits from, the mineral property or properties described in this report.

November 24, 1998

PROFESSIONAL PROVINCE OF E. T. PEZZOT BRITISH COLUMBIA GEOSCIENTIST

E. Trent Pezzot, B.Sc., P.Geo.

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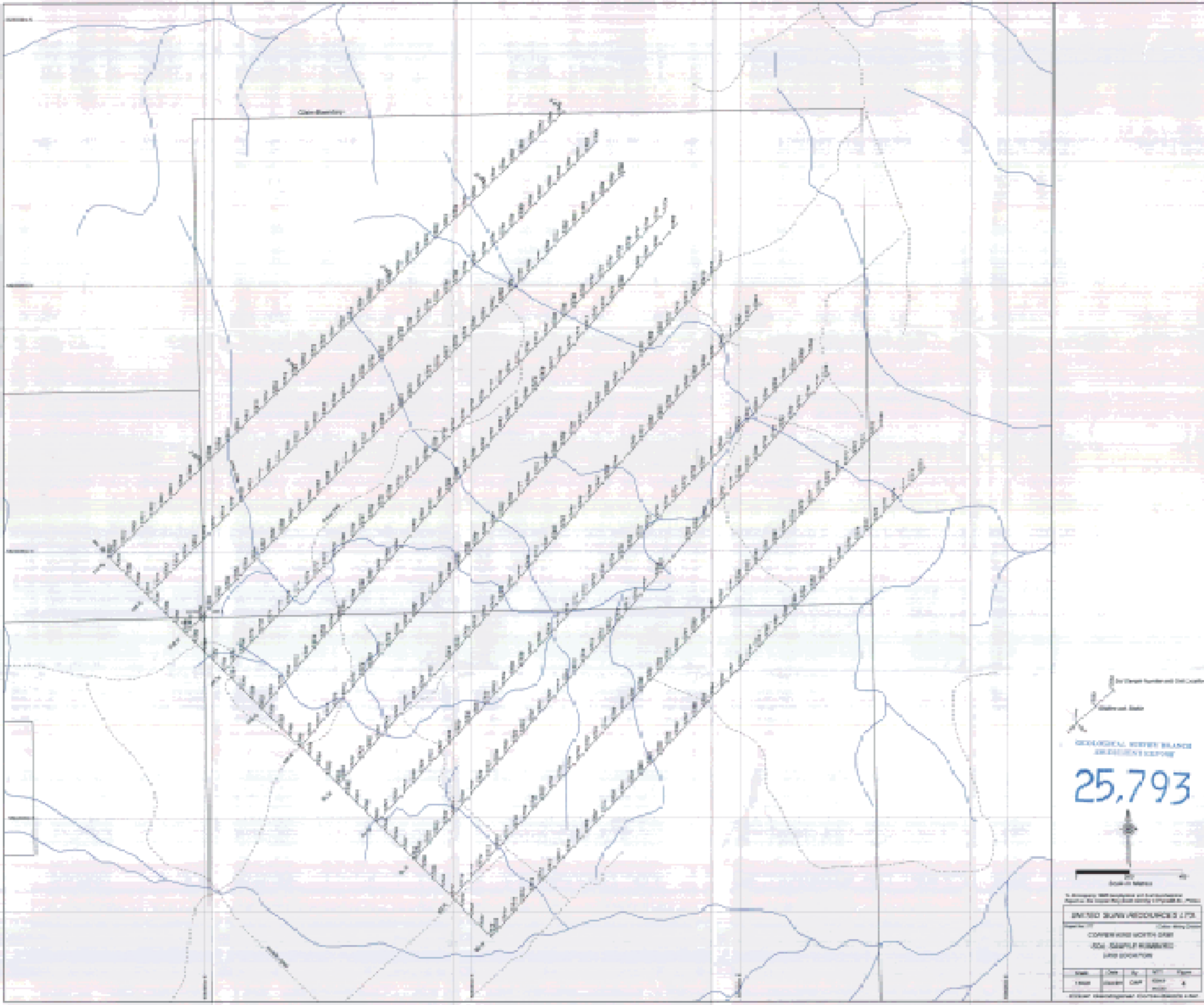
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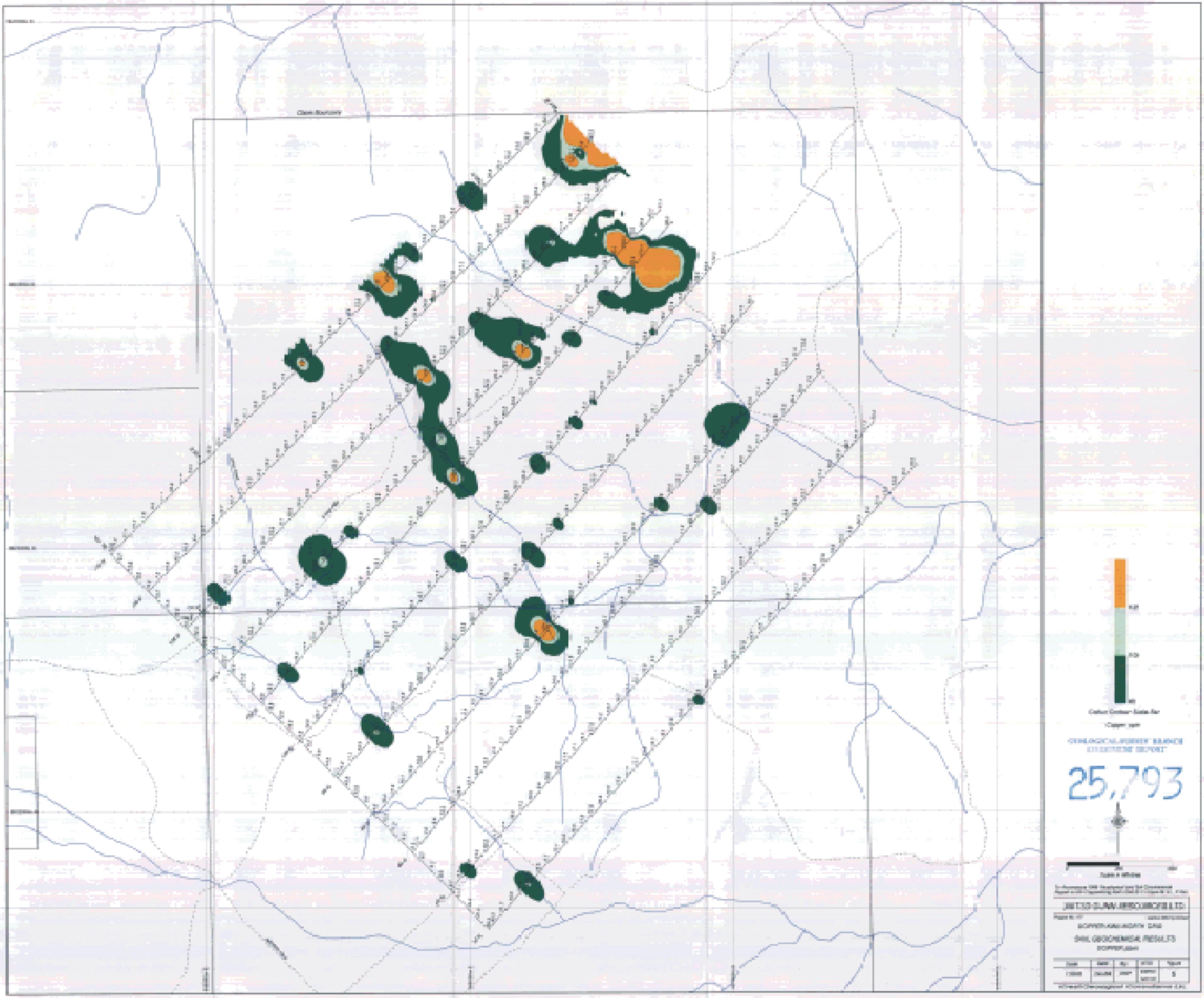
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Copper ppm
GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT
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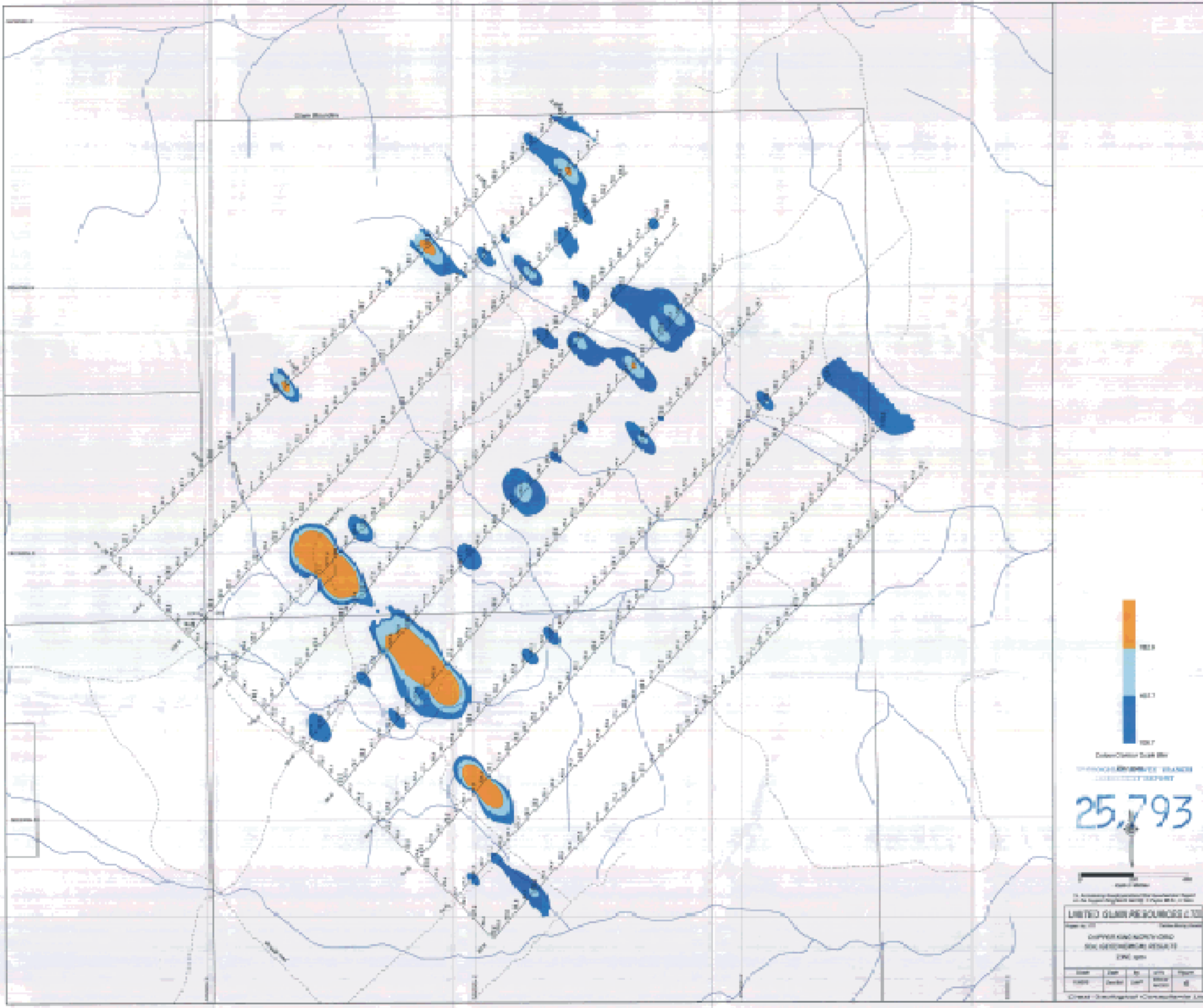
SOIL GEOCHEMICAL RESULTS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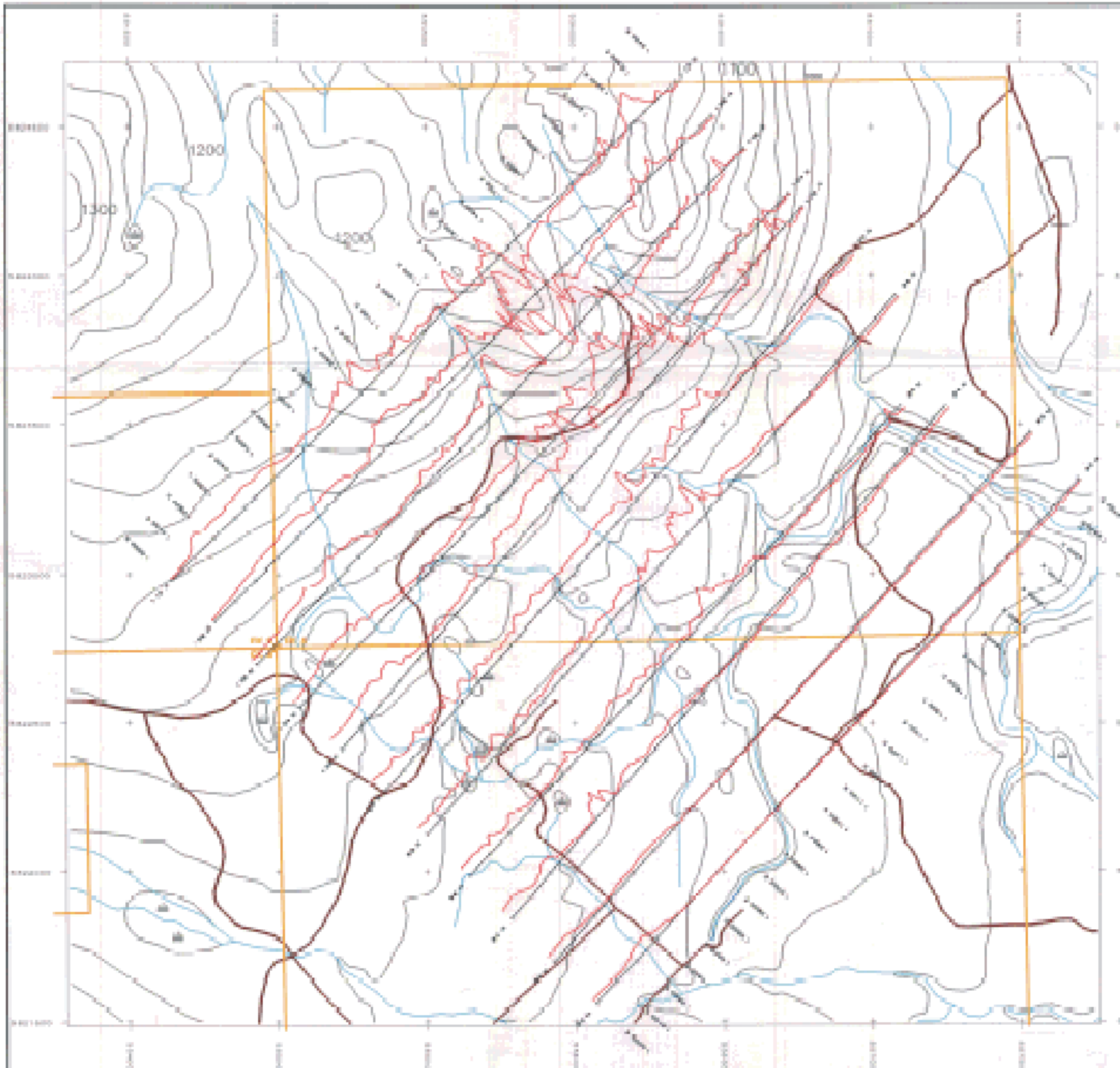


UNITED GUNN RESOURCES LTD.

COPPER KING NORTH GRID

PROJECT NO. 177

TOTAL MAGNETIC FIELD
INTENSITY (nT)
STACKED PROFILE MAP

CARIBOO MINING DIVISION

NAD 83

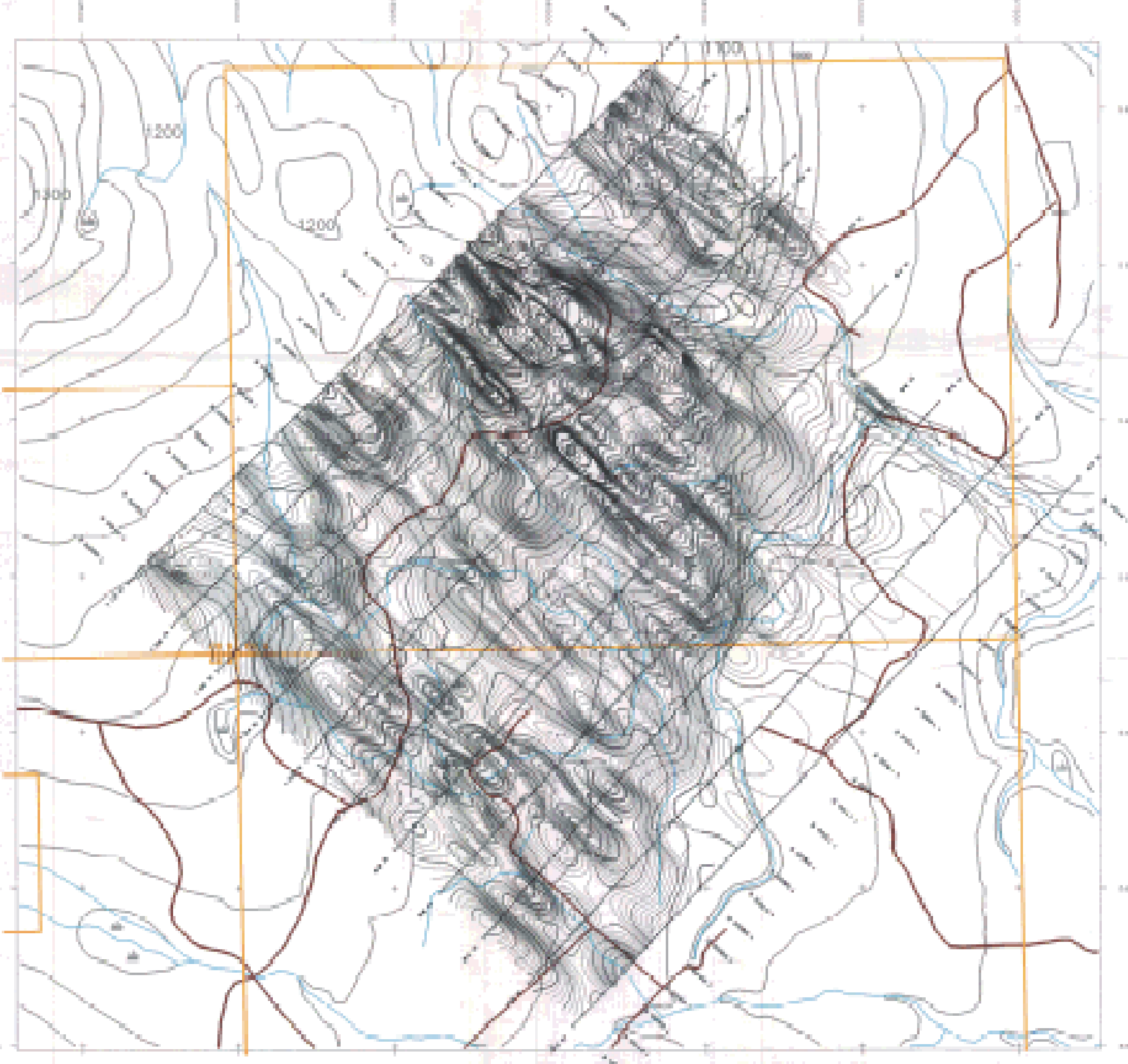
SCALE IN METRES

DATA COLLECTED BY CREST GEOLOGICAL CONSULTANTS LTD.

PLOTTING BY SJV CONSULTANTS LTD.

DATE: NOV./98

PLATE: G7c



GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT

25,793

UNITED GUNN RESOURCES LTD.

COPPER KING NORTH GRID

PROJECT NO. 177

TOTAL MAGNETIC FIELD
INTENSITY (nT)
CONTOUR MAP

CARIBOO MINING DIVISION — NAD 83 — ZONE 10

SCALE IN METRES

DATA COLLECTED BY CREST GEOLOGICAL CONSULTANTS LTD.

PLOTTING BY SJV CONSULTANTS LTD.

DATE: NOV./98

PLATE: 07b