ASSESSMENT REPORT

GEOPHYSICAL AND SOIL GEOCHEMICAL REPORT ON THE

COPPER ACE PROPERTY
CA1, CA2, CA3, CA4, CA5 and CA6 CLAIMS

NTS 93 B/9
52° 33' NORTH LATITUDE
122° 18' WEST LONGITUDE
CARIBOO MINING DIVISION
BRITISH COLUMBIA

FOR
UNITED GUNN RESOURCES LTD.
1016 - 1030 WEST GEORGIA STREET
VANCOUVER, BRITISH COLUMBIA V6E 2Y3

BY

CREST GEOLOGICAL CONSULTANTS LTD.
2197 PARK CRESCENT
COQUITLAM, BRITISH COLUMBIA V3J 6T1

Craig W. Payne M.Sc., P.Geo.
January 10, 1999

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SUMMARY AND CONCLUSIONS

During May to October, 1998 mineral exploration work was carried out on two separate grid areas covering selected base metal targets within the Copper Ace Property, which forms part of the Granite Mountain Project.

Selection of the grid area was based on compilation work carried out in 1997.

The Copper Ace Property comprises 148 units (3700ha) located along the western side of the Granite Mountain Pluton which hosts Gibraltar Mines, disseminated copper deposits.

The Copper Ace South Grid is located two kilometres northwest of the Gibraltar Mine plant site. Limited outcrop exposures have precluded detailed mapping in the grid area therefore lithology and geological contacts have been interpreted from the geophysical data, mainly magnetic and VLF-EM data.

The grid area is underlain by early Jurassic aged quartz diorite, part of the Granite Mountain pluton which hosts the Gibraltar Mines disseminated copper deposits. The quartz diorite can be subdivided into two main phases. The eastern and northwestern parts of the grid are underlain by a coarse grained, leucocratic, weakly chlorite-epidote altered quartz diorite. The remaining grid area is underlain by a moderately to strongly chlorite-sericite-epidote altered quartz diorite which is interleaved with highly deformed sericite-chlorite altered schist (host to the Gibraltar deposits). Locally discontinuous quartz feldspar porphyry late phase dykes? are present. In the south-central part of the grid disseminated fine grained pyrite and chalcopyrite and stingers of sphalerite have been discovered in highly deformed, altered and foliated quartz diorite and chlorite-sericite altered schist.

The magnetic data confirms the area is underlain by complexly folded and deformed phases of the Granite Mountain Pluton and suggests more complex structures than are indicated by surface geological mapping. Magnetic and VLF-EM data suggests two dominant geological strikes N-S possibly defining fault structures and NW-SE features which define the general strike of the different phases of the pluton.

In the east-central part of the grid is a large northwest trending oval shaped, coincident copper and zinc soil anomaly some 1300m long and up to 850m wide. This area is extensively overburden covered, however angular float boulders of highly altered quartz diorite were found containing disseminated chalcopyrite and malachite in the area. This anomaly is coincident with several VLF-EM conductive zones.

Further to the west is a large zinc soil anomaly which covers the western half of the grid area and remains open to the north, south and west. This area is coincident with a magnetic low and several VLF-EM conductive zones.

Further exploration work is recommended within the grid area.

INTRODUCTION

This report describes the exploration results of grid establishment, soil sampling and geophysical work carried out on the Copper Ace Property South grid which forms part of the Granite Mountain Project. Exploration work was carried out on behalf of United Gunn Resources Ltd., Vancouver, British Columbia. The above described surveys were used to investigate the property for signatures indicative of economic concentrations of disseminated base metal and bonanza style precious metal mineralization.

LOCATION AND ACCESS

The Copper Ace property is located in central British Columbia approximately 370 kilometres north of Vancouver, British Columbia (Figure 1).

Generally, road access is fairly good with Highway 97 following along the east side of the Fraser River with numerous secondary roads and trails throughout the area.

Copper Ace property is located on the western flank of Granite Mountain centred at 52°33' north latitude and 122°18' west longitude on NTS map sheets 93 B/9.

Road access to the Copper Ace Property south grid area is via highway 97 north from Williams Lake to McLeese Lake, then east on Beaver Creek road (Gibraltar Mine road) for approximately 10 kilometres and then west and north on forest access roads to the centre of the property.

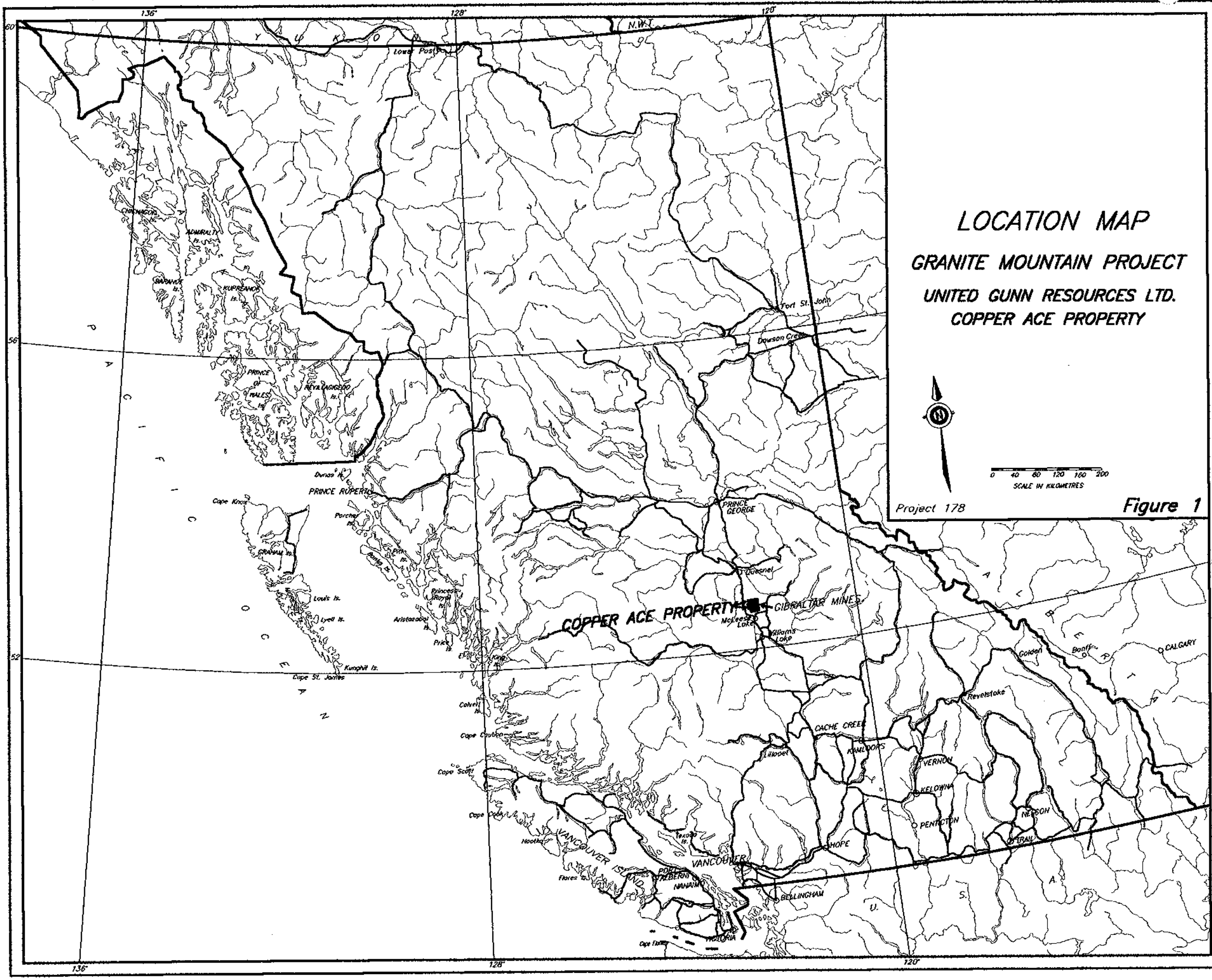
CLAIMS STATUS

The Copper Ace property consists of two claim blocks located along the western side of Gibraltar Mines claims. The Copper Ace South grid claim block is comprised of six claims, totalling 98 units (2450ha) which forms the CA 98-1 Group. The claims are 100% owned by United Gunn Resources Ltd. Table 1 provides pertinent claims data for the property (Figure 2).

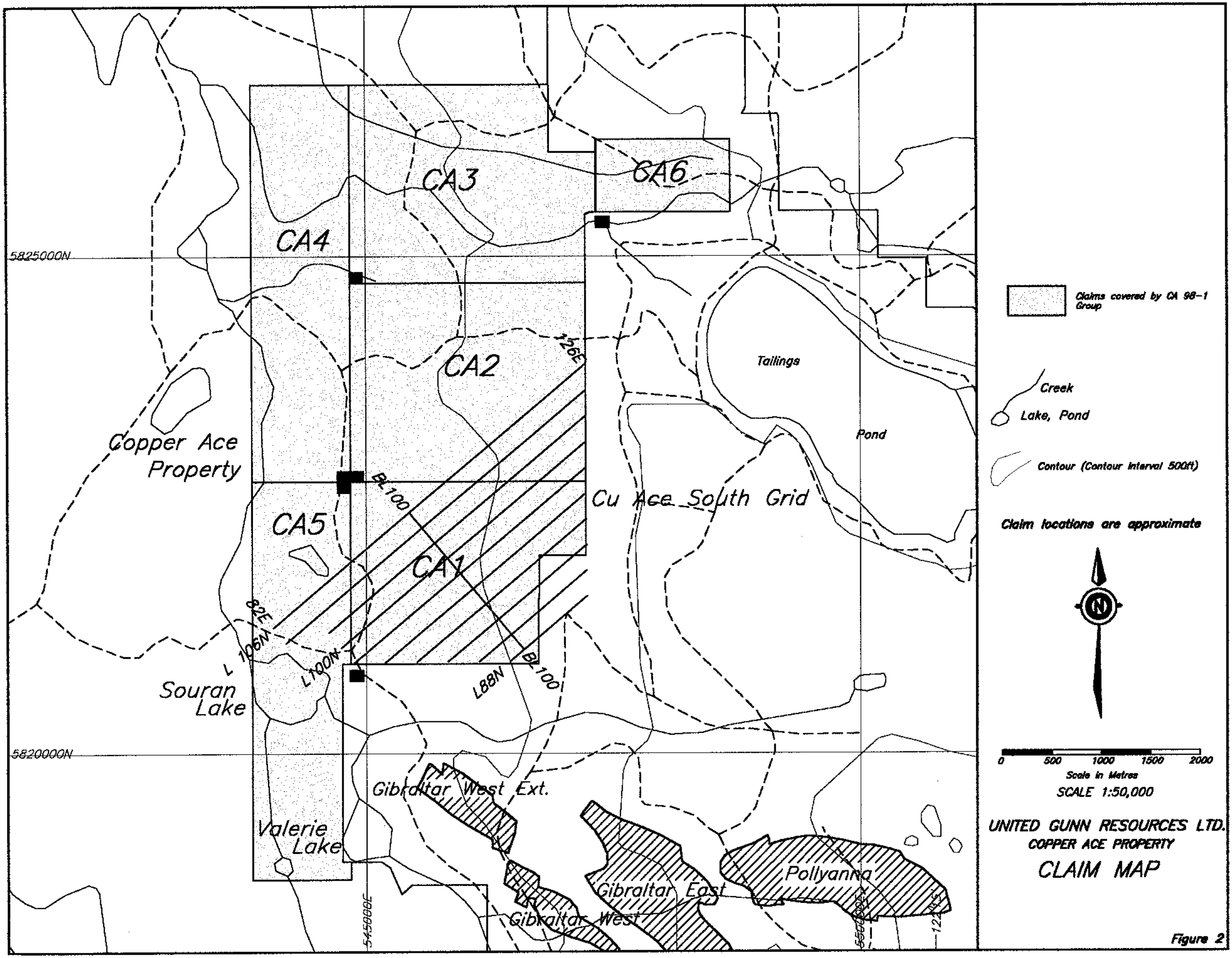
TABLE 1 CLAIMS DATA

COPPER ACE PROPERTY			
CLAIM NAME	TENURE NO.	NO. OF UNITS	EXPIRY DATE
CA 1	359909	20	October 18, 2002
CA 2	359910	20	October 19, 2002
CA 3	359911	20	October 19, 2002
CA 4	359912	16	October 20, 2002
CA 5	359913	16	October 21, 2002
CA 6	359914	6	October 19, 2002
Total Number of Units		98	

*Subject to acceptance of 1998 assessment work.



LOCATION MAP
GRANITE MOUNTAIN PROJECT
UNITED GUNN RESOURCES LTD.
COPPER ACE PROPERTY
0 40 80 120 160 200
SCALE IN KILOMETRES
Project 178
Figure 1
COPPER ACE PROPERTY
GIBRALTAR MINES
YUKON
N.W.T.
Lower Post
Fort St. John
Dawson Creek
PRINCE GEORGE
Quesnel
McLeese Lake
Williams Lake
PRINCE RUPERT
PACIFIC OCEAN
ALBERTA
Golden
Banff
CALGARY
Revelstoke
CACHE CREEK
KAMLOOPS
Lillooet
VERNON
KELOWNA
PENTICTON
NELSON
TRAIL
HOPE
VANCOUVER
VANCOUVER ISLAND
NANAIMO
BELLINGHAM
VICTORIA
U.S.A.
Cape Knox
Cape St. James
Cape Scott
Kunghit Is.
Louis Is.
Lyell Is.
Aristazabal Is.
Princess Royal Is.
Price Is.
Calvert Is.
Cape Caution
Cape Cook
Nootka
Flores Is.
Texada Is.
Dundas Is.
Porcher Is.
Banks Is.
Pitt Is.
GRAHAM Is.
PRINCE OF WALES Is.
REVILLAGIGEDO Is.
KUPREANOF Is.
BARANOF Is.
ADMIRALTY Is.
CHICHAGOF Is.
136°
128°
120°
60°
56°
52°
49°


CA3
CA6
CA4
5825000N
CA2
126E
Copper Ace
Property
Tailings
Pond
Cu Ace South Grid
BL 100
CA5
CA1
82E
L 106N
L100N
L88N
BL 100
Souran
Lake
5820000N
Gibraltar West Ext.
Valerie
Lake
Pollyanna
Gibraltar East
Gibraltar West
545000E
Claims covered by CA 98-1 Group
Creek
Lake, Pond
Contour (Contour interval 500ft)
Claim locations are approximate
N
0
500
1000
1500
2000
Scale in Metres
SCALE 1:50,000
UNITED GUNN RESOURCES LTD.
COPPER ACE PROPERTY
CLAIM MAP
Figure 2

TOPOGRAPHY AND VEGETATION

The property is located on the western slope of Granite Mountain and extends out into a broad northerly trending valley known as Cuisson valley.

The Copper Ace South grid is located on a west facing slope of Granite Mountain two kilometres northwest of Gibraltar Mines. Elevations range from 880m in the western part of the property in Cuisson valley to 1020m along the eastern part of the claims.

Vegetation on the properties consists of pine, fir, cedar and balsam with stands of poplar trees near lakes and stream courses. Locally, parts of the grid areas have been clear cut and logging is active in the area.

HISTORY

In 1997 limited silt sampling and prospecting was carried out by Crest Geological Consultants Ltd. on behalf of United Gunn Resources Ltd. during staking of the Copper Ace property.

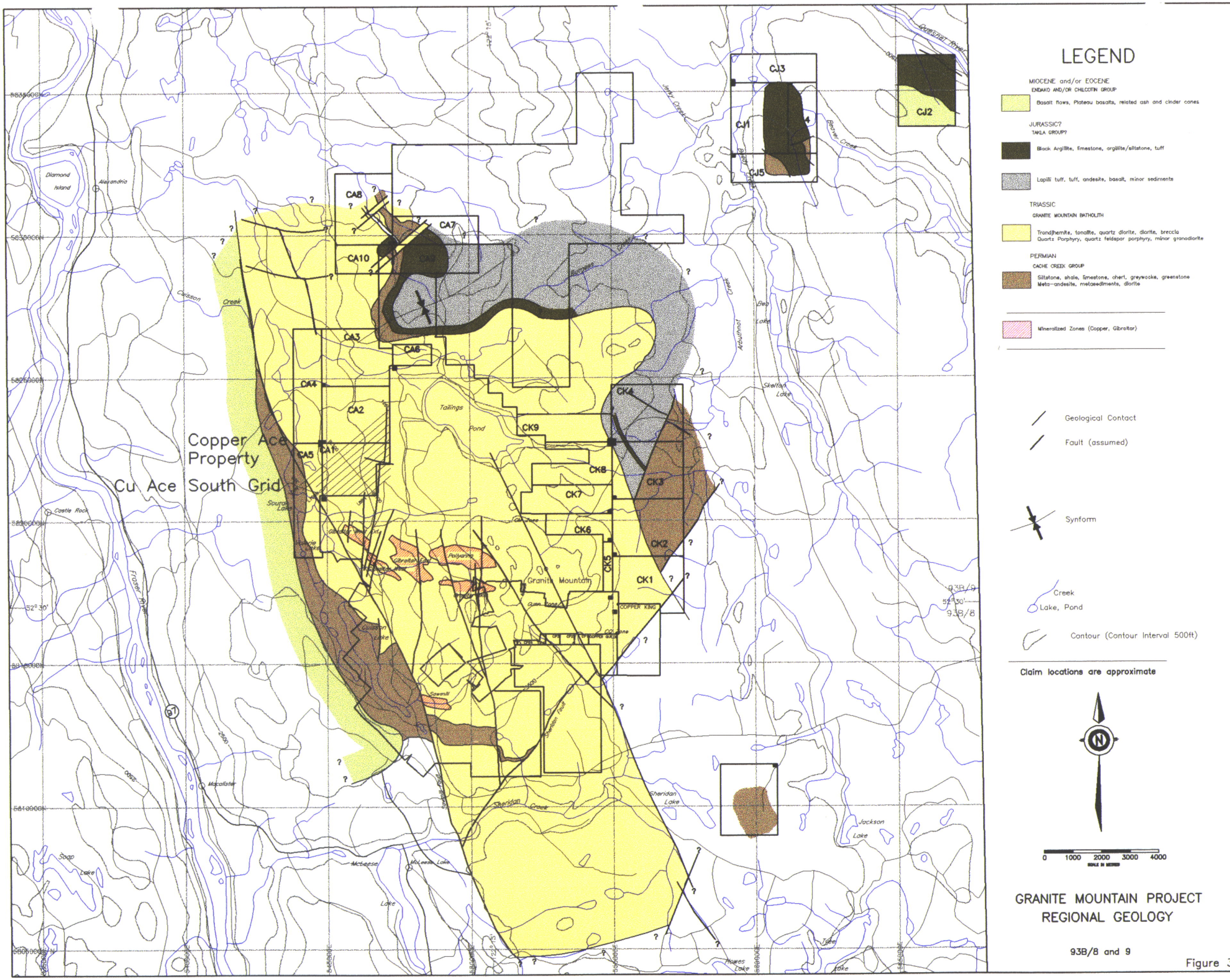
Most exploration work in the area concentrated on the Gibraltar property which is located to the east of the Copper Ace property. The original discovery of copper mineralization was made in 1927. Later, in 1957 Kimaclo Mines Ltd. drove an adit in high grade shear zones in the Gibraltar West zone. The Gibraltar property was then sold to Major Mines Ltd. in 1958 and was allowed to lapse. In 1962, J. Hilton restaked the Gibraltar property and optioned it to Keevil Mines Ltd. During 1964, Gibraltar Mines Ltd. acquired the property from Hilton and optioned the claims to Cominco Ltd. and Mitsubishi Mining Co. who delineated the Gibraltar West zone before terminating the option in 1967. In 1969 Canex Placer Ltd. and Duval Corp. acquired an option on the ground from Gibraltar Mines Ltd. Duval Corp. optioned the adjoining Pollyanna ground and in 1969 the Duval interest was acquired by Canex Placer Ltd. In 1970 the Granite Lake zone was discovered. In 1972 the mine was put into production at a rate of approximately 36,000 tonnes per day (Drummond et al, 1976).

Cuisson Mines Ltd. owns the claims adjoining Gibraltar Mines Ltd. on the east. These claims cover the eastern part of the Granite Lake ore body. United Gunn Resources Ltd. is a 30% partner in Cuisson Mines Ltd. along with Placer Dome, Inc. and Gibraltar Mines Ltd. Currently, copper leaching operations are underway on the Granite Lake ore body from which United Gunn receives a royalty.

In the area of the Copper Ace property which is located to the northwest of Gibraltar Mines, limited exploration work has been carried out intermittently since the 1960s. In 1968 Morocco Mines carried out an IP survey just to the south of the Copper Ace south grid, on ground now owned by Gibraltar Mines. The survey outlined several chargeability anomalies which have not been drill tested to date. In 1982 Garth Johnson drilled a 152.4m drill hole two kilometres northwest of the Copper Ace south grid. The hole intersected foliated chlorite-sericite-epidote altered quartz diorite with trace to <1% disseminated pyrite. To the south and west of the Copper Ace south grid several different types of geophysical surveys have been carried out in the area of the Sawmill deposit. Most of the results have not been reported.

REGIONAL GEOLOGY

The claims are located within a wedge shaped segment of late Palaeozoic to Miocene volcanic and sedimentary rocks which are intruded by several stocks/batholiths ranging in composition from diorite to granodiorite. This wedge shaped segment is located between the northwest-southeast trending Quesnel Trough to the east and the Pinchi Geanticline on the west, all of which forms part of the Intermontane Tectonic Belt (Figure 3).


Copper Ace Property
Cu Ace South Grid
CA1
CA2
CA3
CA4
CA5
CA6
CA7
CA8
CA9
CA10
CJ1
CJ2
CJ3
CJ5
CK1
CK2
CK3
CK4
CK5
CK6
CK7
CK8
CK9
COPPER KING
Granite Mountain
Tailings
Pond
Sheridan Creek
Sheridan Lake
Jackson Lake
McLeese Lake
Soap Lake
Diamond Island
Alexandria
Castle Rock
Fraser River
Quesnel River
Macalister
Arbuthnot Creek
Skelton Lake
Bee Lake
Jerry Creek
Beaver Creek
Cuisson Creek
Cuisson Lake
Sawmill
Pollyanna
Gibraltar
Sheridan Fault
Howes Lake
Tyee Lake
97
93B/9
93B/8
52° 30'
LEGEND
MIOCENE and/or EOCENE
ENDAKO AND/OR CHILCOTIN GROUP
Basalt flows, Plateau basalts, related ash and cinder cones
JURASSIC?
TAKLA GROUP?
Black Argillite, limestone, argillite/siltstone, tuff
Lapilli tuff, tuff, andesite, basalt, minor sediments
TRIASSIC
GRANITE MOUNTAIN BATHOLITH
Trondjhemite, tonalite, quartz diorite, diorite, breccia
Quartz Porphyry, quartz feldspar porphyry, minor granodiorite
PERMIAN
CACHE CREEK GROUP
Siltstone, shale, limestone, chert, greywacke, greenstone
Meta-andesite, metasediments, diorite
Mineralized Zones (Copper, Gibraltar)
Geological Contact
Fault (assumed)
Synform
Creek
Lake, Pond
Contour (Contour Interval 500ft)
Claim locations are approximate
0 1000 2000 3000 4000
GRANITE MOUNTAIN PROJECT
REGIONAL GEOLOGY
93B/8 and 9
Figure 3

Within the area of the claims the oldest rocks are a sequence of Permian, Cache Creek Group sedimentary and volcanic rocks (Tipper, 1959; Drummond et al, 1976). The Cache Creek Group rocks have been intruded by early Jurassic aged diorite to quartz diorite in composition Granite Mountain pluton.

Gibraltar Mines disseminated copper/molybdenum deposits are located two kilometres to the southeast of the Copper Ace property. The mine consists of five deposits known as the Granite Lake, Pollyanna, Gibraltar East, Gibraltar West and Gibraltar West Extension. Original tonnage figures for the combined deposits are 326,000,000 tonnes grading 0.37% copper and 0.016% MoS_2 (Drummond et al, 1976).

Intrusion of the Granite Mountain pluton into Cache Creek Group volcanic and sedimentary rocks has metamorphosed the surrounding rocks forming skarn zones. Panteleyev, 1977 suggests that the presence of chalcopyrite, magnetite and hematite in some of the skarn zones indicate that economically significant mineral deposits may be found peripheral to the Granite Mountain pluton.

1998 EXPLORATION PROGRAMS

Copper Ace South Grid

Thirty two kilometres of northeast-southwest orientated flagged grid lines were established and the collection of 550 soil samples at 50m stations was completed. A total of 29km of magnetometer and VLF-EM surveying was completed at 12.5m stations along the grid lines.

GENERAL PROPERTY GEOLOGY

Copper Ace South Grid – Geology

Sparse outcrop has precluded detailed prospecting and geological mapping of the Copper Ace South grid area (Figure 4). Geological interpretation is based on limited outcrop and has relied heavily on geophysical surveys carried out over the grid area.

The grid area is underlain by three phases of the Granite Mountain pluton. The northeastern and western areas of the grid are believed to be underlain by relatively unaltered coarse grained quartz diorite. This interpretation is based on the premise that the more unaltered the quartz diorite the higher the magnetic response in comparison to the lower magnetic response throughout the remaining grid area. Peripheral to the relatively unaltered quartz diorite is a medium grained, leucocratic, moderately to strongly chlorite-sericite+/-epidote altered quartz diorite. Throughout the central part of the grid area is chlorite-sericite altered schist. Locally the rock is interfingered with the foliated quartz diorite. Generally the foliation trends to the northwest with a shallow to moderate dip to the southwest.

SOIL GEOCHEMICAL SURVEYS

The purpose of the soil geochemical survey was to define anomalous areas indicative of economic concentrations of base and or precious metals in the underlying rock.

Copper Ace South Grid – Soil Geochemical Results

A total of 550 soil samples were collected every 50m along northeast orientated grid lines spaced 100m or 200m apart. Soil sampling was offset by 25m on alternating grid lines. Depth of overburden in the grid area varies from <1m in the central part of the grid just west of the baseline to approximately 21m or greater throughout the rest of the grid area. Analytical certificates, sample descriptions and general statistical treatment of the data set are listed in Appendix I along with a grid map showing sample locations (Figure 4). Sample collection and analytical techniques are described in Appendix II.

Soil sampling results on the Copper Ace South grid shows strong copper, zinc and weakly anomalous molybdenum soil anomalies.

Copper values range from 5.2ppm Cu to 1074.3ppm Cu. Two areas containing anomalous copper values stand out in the data (Figure 5).

The first copper soil anomaly is located in the northeast-central part of the grid. The copper soil anomaly is a large oval shaped feature some 1300m long (to the northwest) and up to 850m wide. The central part of the anomaly does not contain any anomalous copper values. This copper soil anomaly remains open to the northwest. This copper soil anomaly is believed to be underlain by chlorite-sericite schist and chlorite altered strongly foliated quartz diorite. It is also possible that the eastern side of the soil anomaly follows a north trending, mineralized fault system while the northwestern part of the anomaly is the down ice dispersion trail.

The second area of anomalous copper values in soils is located in the south central part of the grid at the baseline and extending some 450m to the northwest. Width of the soil anomaly is up to 300m. This area of the grid is underlain by sericite-chlorite schist and chlorite altered strongly foliated quartz diorite. Copper values in rock grab samples from this area contain up to 1.5% Cu and 1.1% Zn. Soils from this area are also anomalous in zinc and weakly anomalous in molybdenum.

Zinc values in soils range from 34.4ppm Zn to 1174.9ppm Zn. The main zinc soil anomaly is a large irregular feature extending from the baseline to the western edge of the grid and remains open to the south, northwest and west (Figure 6). Anomalous zinc values within this anomaly range up to 1174.3ppm Zn. Most of this area of the grid is underlain by chlorite altered strongly foliated quartz diorite and sericite schist. In the northeastern part of the soil anomaly zinc values in rock grab samples range up to 1.1% Zn and one angular float sample from the western part of the soil anomaly contains 1525ppm Zn.

The second zinc soil anomaly is located in the east-central part of the grid area and is in part coincident with the large oval shaped copper soil anomaly. However the zinc soil anomaly does show a strong down ice dispersion pattern.

GEOPHYSICAL SURVEYS

A total of 29km of magnetometer and VLF-EM surveying was carried out on the Copper Ace South grid. Readings were taken at 12.5m along grid lines spaced 100m or 200m apart. Total field magnetometer and inphase, quadrature and field strength measurements for two VLF-EM transmitters were recorded at each station along the grid lines.

Copper Ace South Grid – Geophysical Survey Results

The highly variable magnetic data suggests the grid is underlain by variably altered quartz diorite and sericite-chlorite schist. The northwestern part of the grid has a higher magnetic background suggesting the quartz diorite is only weakly altered. Locally quartz+/-feldspar porphyry dykes are also associated with linear magnetic highs.

Coincident VLF-EM conductive zones and magnetic lows have defined several north to northeasterly trending fault structures through the central part of the grid. Also coincident with this structure is anomalous values of copper and zinc in soils.

A complete interpretation of the magnetic and VLF-EM data was completed by Trent Pezzot of SJV Geophysics Ltd. The report and accompanying maps are presented in Appendix VI.

RECOMMENDATIONS

Based on the encouraging results from geological, geochemical and geophysical surveys carried out in 1998 the following two phase program is recommended for 1999.

Phase I will consist of diamond drill testing surface copper and zinc mineralization (Rick Showing) and geophysical targets. Five drill holes totalling 1525m are proposed to test the targets.

Contingent on the successful drilling results, the grid should be expanded to the west and northwest where more geological mapping/prospecting, geochemical and geophysical surveying should be carried out.

Respectfully Submitted,

CREST GEOLOGICAL CONSULTANTS LIMITED

Craig W. Payne, M.Sc., P.Geo.
January 10, 1999

ITEMIZED COST STATEMENT

Grid Establishment and soil sampling	
32 kilometres at $275.00 per kilometre	$8,800.00
Assays/Geochem	
550 samples at $16.38 per sample	9,009.00
Truck Rental 26 days at $65 per day (During period May 1 to August 31, 1998)	1,690.00
4Trax Rental 26 days at $64.20 per day(2 4trax's) (During period May 1 to August 31, 1998)	1,669.20
Fuel	698.50
Salaries - 26 mandays each during the period May 1 to August 31, 1998	
R. Roe at $176 per day	4,576.00
C. Roe at $160 per day	4,160.00
C. Thorsen at $170 per day	4,420.00
R. Bailey at $160 per day	4,160.00
Room and Board - 26 days (4 men) (During period May 1 to August 31, 1998)	4,580.00
Mag/VLF Survey (Field) - 13 days at 600.00/day (During period May 1 to July 19, 1998)	7,800.00
Assessment and Geophysical Reports	4,937.30
TOTAL	**$56,500.00**

STATEMENT OF QUALIFICATIONS

I, Craig W. Payne of Coquitlam, British Columbia do hereby certify that I:

1. am a graduate of Brock University St. Catharines, Ontario with a Master of Science degree in Geological Sciences, 1979.
2. am a Fellow of the Geological Association of Canada.
3. am a member of the Association of Professional Engineers and Geoscientists of British Columbia.
4. have practiced my profession since 1972.
5. am consulting geologist with Crest Geological Consultants Limited.
6. am the author of the report entitled "Geophysical and Soil Geochemical Report on the Copper Ace Property"; Cariboo Mining Division, dated: January 10,1999.

Dated at Coquitlam, B.C. this 10th day of January, 1999.

Respectfully submitted,

CREST GEOLOGICAL CONSULTANTS LIMITED

Craig W. Payne M.Sc., P.Geo.
January 10, 1999

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1973. Induced Polarization Surveys Compilation Map, Scale 1 inch to 1,000 feet, Cuisson Lake Mines Ltd. (NPL) Ground; Gibraltar Mines Ltd.

APPENDIX I

COPPER ACE PROPERTY - SOUTH GRID

GENERAL STATISTICS
SOIL SAMPLE DESCRIPTIONS
ANALYTICAL CERTIFICATES

Crest Geological Consultants Ltd.

COPPER ACE PROPERTY - SOUTH GRID

GENERAL STATISTICS FOR SOIL GEOCHEMICAL DATA SET

	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Tl	Hg	Se	Te	Ga	Au
No. of Samples	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549	549
Max Value	11.7	1074.3	8.4	1174.9	1722	135	21	5758	6.17	7.8	18	4	481	2.36	1	1.8	77	30.44	0.344	38	114	1.08	542	0.08	22	5.99	0.03	0.35	2	0.5	138	1.8	0.3	11.8	221
Min Value	0.3	5.2	1.5	34.4	30	4	2	146	0.26	0.5	5	2	10	0.01	0.2	0.2	6	0.13	0.005	1	5	0.19	32	0.01	3	0.24	0.01	0.01	2	0.2	10	0.3	0.2	1	1
Average	1.1	67.5	3.1	139.2	170.1	14.6	6.4	472.0	1.5	1.2	5.3	2.0	30.1	0.2	0.2	0.2	28.2	0.8	0.0	5.7	20.1	0.4	91.0	0.0	3.3	1.1	0.0	0.1	2.0	0.2	20.2	0.3	0.2	3.1	3.2
Median	0.9	34.8	2.9	94.4	124	11	6	366	1.28	0.9	5	2	20	0.11	0.2	0.2	27	0.28	0.029	5	17	0.39	75	0.05	3	0.97	0.01	0.05	2	0.2	16	0.3	0.2	2.9	1
Variance	0.8	12326.0	0.9	18513.0	30896.9	145.3	7.0	181932.0	0.4	1.1	1.5	0.0	2511.3	0.1	0.0	0.0	67.0	8.4	0.0	11.4	119.6	0.0	3336.8	0.0	2.2	0.2	0.0	0.0	0.0	0.0	211.9	0.0	0.0	1.1	158.9
Standard deviation	0.9	111.0	1.0	136.1	175.8	12.1	2.7	426.5	0.6	1.0	1.2	0.1	50.1	0.2	0.1	0.2	8.2	2.9	0.0	3.4	10.9	0.1	57.8	0.0	1.5	0.5	0.0	0.0	0.0	0.0	14.6	0.1	0.0	1.0	12.6
Mean+2STD'S	3.0	289.5	5.0	411.3	521.7	38.7	11.8	1325.0	2.7	3.3	7.8	2.2	130.4	0.7	0.4	0.6	44.6	6.6	0.1	12.5	42.0	0.7	206.6	0.1	6.3	2.1	0.0	0.1	2.0	0.2	49.3	0.5	0.2	5.2	28.4
Mean+3STD'S	3.9	400.6	6.0	547.4	697.4	50.7	14.4	1751.6	3.4	4.3	9.0	2.3	180.5	0.9	0.5	0.7	52.8	9.5	0.1	15.9	53.0	0.8	264.3	0.1	7.8	2.6	0.0	0.2	2.0	0.3	63.9	0.7	0.2	6.2	41.0
90th Percentile	1.9	144.7	4.4	264.5	318.2	24.2	10.0	818.2	2.2	2.5	6.0	2.0	39.2	0.4	0.3	0.2	38.0	0.7	0.1	8.0	31.0	0.6	149.2	0.1	3.0	1.5	0.0	0.1	2.0	0.2	34.2	0.3	0.2	4.1	4.0
95th Percentile	2.4	234.4	5.0	394.0	472.2	33.6	12.0	1057.8	2.5	3.3	7.6	2.0	61.6	0.6	0.4	0.4	43.0	1.2	0.1	12.0	38.6	0.6	195.0	0.1	5.0	1.8	0.0	0.1	2.0	0.2	44.2	0.4	0.2	4.8	6.0
98th Percentile	3.6	416.1	5.8	631.4	691.5	52.0	14.0	1479.9	3.3	4.6	10.0	2.0	129.4	0.9	0.5	0.8	49.0	7.2	0.1	15.0	55.0	0.7	292.1	0.1	6.0	2.5	0.0	0.2	2.0	0.2	62.2	0.7	0.2	5.6	17.0
99th Percentile	4.6	676.1	6.6	762.1	1013.2	62.6	15.5	1670.6	4.2	5.4	10.5	2.0	371.4	1.4	0.6	1.2	54.0	16.5	0.2	20.5	65.0	0.9	340.2	0.1	12.0	3.3	0.0	0.2	2.0	0.2	81.0	0.8	0.2	7.6	40.5

	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Tl	Hg	Se	Te	Ga	Au
Mo	1.0																																		
Cu	0.5	1.0																																	
Pb	0.4	0.5	1.0																																
Zn	0.1	0.1	0.3	1.0																															
Ag	0.4	0.8	0.6	0.2	1.0																														
Ni	0.5	0.9	0.7	0.2	0.8	1.0																													
Co	0.5	0.6	0.7	0.4	0.7	0.8	1.0																												
Mn	0.7	0.4	0.5	0.4	0.5	0.6	0.6	1.0																											
Fe	0.5	0.7	0.7	0.3	0.7	0.9	0.9	0.6	1.0																										
As	0.4	0.6	0.6	0.1	0.6	0.7	0.6	0.4	0.7	1.0																									
U	-0.1	-0.1	-0.1	0.0	-0.1	0.0	0.0	0.0	-0.1	-0.1	1.0																								
Th	0.0	0.1	0.1	0.0	0.1	0.2	0.2	0.1	0.2	0.2	0.0	1.0																							
Sr	0.2	0.3	0.0	0.1	0.4	0.2	0.1	0.3	0.1	0.2	-0.1	0.0	1.0																						
Cd	0.3	0.4	0.4	0.7	0.5	0.3	0.4	0.5	0.3	0.2	0.0	0.0	0.5	1.0																					
Sb	0.4	0.6	0.5	0.0	0.6	0.7	0.6	0.3	0.7	0.7	-0.1	0.1	0.2	0.2	1.0																				
Bi	0.2	0.5	0.3	0.0	0.5	0.5	0.3	0.2	0.4	0.3	-0.1	0.0	0.2	0.2	0.3	1.0																			
V	0.4	0.5	0.7	0.3	0.5	0.7	0.8	0.5	0.9	0.7	-0.1	0.2	-0.1	0.2	0.6	0.2	1.0																		
Ca	0.1	0.2	-0.1	0.0	0.2	0.1	0.0	0.3	-0.1	0.1	0.0	0.0	0.9	0.4	0.1	0.1	-0.2	1.0																	
P	0.2	0.3	0.2	0.4	0.4	0.3	0.3	0.4	0.3	0.3	0.0	0.0	0.6	0.6	0.2	0.2	0.1	0.5	1.0																
La	0.4	0.8	0.6	0.0	0.7	0.9	0.7	0.5	0.8	0.6	-0.1	0.2	0.1	0.2	0.7	0.4	0.7	-0.1	0.2	1.0															
Cr	0.4	0.8	0.7	0.2	0.8	0.9	0.8	0.5	0.9	0.7	0.0	0.2	0.2	0.3	0.7	0.4	0.8	0.0	0.3	0.9	1.0														
Mg	0.3	0.5	0.4	0.2	0.5	0.6	0.7	0.3	0.7	0.5	-0.1	0.1	0.2	0.2	0.5	0.3	0.5	0.1	0.1	0.5	0.6	1.0													
Ba	0.5	0.7	0.6	0.4	0.7	0.8	0.7	0.7	0.7	0.6	-0.1	0.1	0.4	0.6	0.5	0.4	0.6	0.3	0.6	0.7	0.7	0.4	1.0												
Ti	-0.1	-0.2	0.0	0.0	-0.2	-0.1	0.0	-0.2	0.1	0.0	-0.1	0.0	-0.4	-0.3	0.0	-0.1	0.3	-0.4	-0.4	0.0	0.0	0.0	-0.2	1.0											
B	0.1	0.2	0.0	0.1	0.2	0.1	0.0	0.2	0.0	0.1	0.0	0.0	0.8	0.5	0.0	0.2	-0.1	0.8	0.6	0.0	0.1	0.0	0.3	-0.3	1.0										
Al	0.4	0.7	0.7	0.3	0.8	0.9	0.8	0.5	0.9	0.6	-0.1	0.2	0.1	0.2	0.6	0.4	0.8	-0.1	0.2	0.8	0.9	0.7	0.8	0.0	-0.1	1.0									
Na	0.2	0.6	0.3	0.0	0.6	0.5	0.4	0.3	0.4	0.4	-0.1	0.1	0.5	0.3	0.4	0.4	0.3	0.4	0.3	0.5	0.5	0.4	0.5	-0.1	0.3	0.5	1.0								
K	0.4	0.7	0.6	0.2	0.8	0.8	0.8	0.5	0.8	0.6	0.0	0.2	0.2	0.3	0.6	0.4	0.7	0.0	0.3	0.8	0.8	0.6	0.7	0.0	0.1	0.8	0.5	1.0							
W																													1.0						
Tl	0.0	0.0	-0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.0	-0.1	0.2	0.1	0.0	0.0	0.0	0.0	-0.1	0.2	0.0	0.0	0.0		1.0					
Hg	0.5	0.8	0.5	0.2	0.8	0.8	0.7	0.6	0.7	0.6	0.0	0.1	0.3	0.4	0.6	0.5	0.6	0.2	0.3	0.7	0.7	0.4	0.7	-0.1	0.2	0.7	0.5	0.7		0.0	1.0				
Se	0.2	0.6	0.2	0.1	0.5	0.4	0.3	0.3	0.3	0.3	-0.1	0.1	0.5	0.4	0.3	0.5	0.1	0.4	0.4	0.3	0.4	0.2	0.5	-0.3	0.4	0.3	0.4	0.3		0.1	0.5	1.0			
Te	0.1	0.6	0.1	0.0	0.3	0.3	0.2	0.1	0.2	0.1	0.0	0.0	0.1	0.2	0.2	0.2	0.1	0.0	0.1	0.4	0.2	0.1	0.2	-0.1	0.0	0.2	0.2	0.2		0.0	0.3	0.3	1.0		
Ga	0.4	0.6	0.7	0.3	0.7	0.8	0.8	0.5	0.9	0.6	-0.1	0.2	0.0	0.3	0.6	0.4	0.8	-0.1	0.2	0.8	0.8	0.7	0.7	0.0	-0.1	0.9	0.4	0.8		0.0	0.7	0.3	0.2	1.0	
Au	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	1.0

UNITED GUNN RESOURCES LTD.
COPPER ACE SOUTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
								ppm	ppm	ppm	ppm	ppb	ppb
11500	9800	8800	TILL	B	BROWN	HILLSIDE NE		0.8	32.3	107.7	0.5	16	1
11499	9850	8800	TILL	B	BROWN	HILLSIDE NE		0.6	32.6	136.3	0.5	10	1
11498	9900	8800	TILL	B	BROWN	HILLSIDE SW		1.1	45.1	126.9	1	12	1
11497	9950	8800	TILL	B	BROWN	HILLSIDE SW		0.3	39.9	71.8	0.5	10	1
11496	10000	8800	TILL	B	BROWN	HILLSIDE SW		1	56.3	86.8	0.7	21	2
11495	10050	8800	TILL	B	BROWN	HILLSIDE SW		3.8	181.2	97.3	1.3	22	1
11494	10100	8800	TILL	B	BROWN	HILLSIDE W		1.6	71.6	94.1	1.1	20	4
11493	10150	8800	TILL	B	BROWN	HILLSIDE W		1.7	34.2	108.9	0.9	10	1
11492	10200	8800	TILL	B	BROWN	HILLSIDE SW		2.4	34.8	77.7	1.4	10	1
11491	10250	8800	TILL	B	BROWN	HILLSIDE SW		3.1	191.3	120.1	3	21	1
11490	10300	8800	TILL	B	BROWN	HILLSIDE SW		1.6	181.6	113.1	2.2	31	1
11489	10350	8800	TILL	B	BROWN	HILLSIDE SW		0.6	212.1	154.9	1.5	25	2
11488	10400	8800	TILL	B	BROWN	HILLSIDE SW		1.8	213.1	319.8	2.2	39	3
11487	10450	8800	TILL	B	BROWN	HILLSIDE SW		0.6	40.8	134.4	1.2	15	1
11486	10500	8800	TILL	B	BROWN	HILLSIDE SW		0.7	50.4	103.9	0.6	11	1
11485	10550	8800	TILL	B	BROWN	HILLSIDE SW		0.7	43.9	95.4	0.5	14	1
11484	10600	8800	TILL	B	BROWN	HILLSIDE SW		0.5	31.4	71.6	0.5	22	1
11483	10650	8800	TILL	B	BROWN	HILLSIDE SW		0.8	49.2	91	0.7	10	5
11482	10700	8800	TILL	B	BROWN	HILLSIDE SW	SAMPLE TAKEN 8M FROM STATION TO AVOID ROAD DISTURBANCE.	2.8	240.5	113.5	1.5	17	9
11481	10750	8800	TILL	B	BROWN	HILLSIDE SW	SAMPLE TAKEN 15M TO N OF STATION TO AVOID ROAD DISTURBANCE.	2.4	227.8	111.7	3.7	35	1
11480	10800	8800	TILL	B	BROWN	HILLSIDE SW		0.7	50.8	452	0.5	10	6
11479	10850	8800	TILL	B	BROWN	HILLSIDE SW		1.3	44.5	274.2	0.6	10	1
11966	10000	8850	TILL	B	BROWN	HILLSIDE W		1.2	106.4	100.3	1.3	26	1
11967	10000	8900	TILL	B	BROWN	HILLSIDE W		1.3	53.1	85.1	1.2	28	1
11968	10000	8950	TILL	B	BROWN	HILLSIDE W		2.7	133.4	82.8	1.4	21	1
11747	9625	9000	TILL	B	BROWN	FLAT		1.9	70	135.4	0.8	25	2
11748	9675	9000	TILL	B	BROWN	FLAT		1.2	47.4	121.8	0.5	22	1
11749	9725	9000	TILL	B	BROWN	FLAT		1.1	35.4	111.6	0.5	10	1
11750	9775	9000	TILL	B	BROWN	FLAT		0.8	49.8	83.8	0.7	10	1
11751	9825	9000	TILL	B	BROWN	FLAT		2.2	82.9	125	1.4	10	2
11746	9875	9000	TILL	B	BROWN	FLAT		3.2	99.5	90.7	0.8	37	1
11745	9925	9000	TILL	B	BROWN	FLAT		1.7	81.8	78.9	2.5	80	1
11744	9975	9000	TILL	B	BROWN	FLAT		1.9	102.2	64.1	2	20	1
11743	10000	9000	TILL	B	BROWN	FLAT		1.5	51.9	66.1	1.3	19	2
11742	10025	9000	TILL	B	BROWN	FLAT		2.1	60.2	96.2	0.5	17	2
11741	10075	9000	TILL	B	BROWN	FLAT		1.4	82.9	100.9	0.8	23	1
11740	10125	9000	TILL	B	BROWN	FLAT		2.1	144.3	155.9	2.6	37	1
11739	10175	9000	TILL	B	BROWN	FLAT	SAMPLE TAKEN FROM UPROOTED TREE.	1.9	102	76.5	1.3	31	1
11738	10225	9000	TILL	B	BROWN	FLAT		1.9	100.6	82.7	2.3	20	2
11737	10275	9000	TILL	B	BROWN	FLAT		5.1	176.8	153.5	1.8	29	1
11736	10325	9000	TILL	B	BROWN	FLAT		5.1	232.4	93.7	3.5	32	1
11735	10375	9000	TILL	B	BROWN	FLAT		8.3	466.6	100.1	3.4	35	1
11734	10425	9000	TILL	B	BROWN	FLAT		2.6	82.1	72	0.8	10	2
11733	10475	9000	TILL	B	BROWN	FLAT		5.5	213.3	92.1	0.9	22	5

UNITED GUNN RESOURCES LTD.
COPPER ACE SOUTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
11732	10525	9000	TILL	B	BROWN	FLAT	SAMPLE TAKEN BESIDE DRIED UP CREEKBED.	1	54.6	60.5	0.9	10	2
11731	10575	9000	TILL	B	BROWN	FLAT		1.6	41.8	92	0.5	12	3
11730	10625	9000	TILL	B	BROWN	FLAT		0.3	25.2	62.8	0.5	12	2
11729	10675	9000	TILL	B	BROWN	FLAT		1.1	59	100.6	1.3	21	3
11728	10725	9000	TILL	B	BROWN	FLAT		1	23.8	58	1.1	10	25
11727	10775	9000	TILL	B	BROWN	FLAT		0.7	37.9	109	0.7	19	2
11726	10825	9000	TILL	B	BROWN	FLAT		1	35.9	95.8	1.1	21	2
11725	10875	9000	TILL	B	BROWN	FLAT		0.7	14	202.7	0.6	16	1
11724	10925	9000	TILL	B	BROWN	FLAT		0.8	49.8	93.3	0.6	10	2
11969	10000	9050	TILL	B	BROWN	HILLSIDE W		1.1	76.8	66.7	1.1	11	221
11970	10000	9100	TILL	B	BROWN	HILLSIDE W		1.8	153.8	102.5	1.9	31	5
11971	10000	9150	TILL	B	BROWN	FLAT	SAMPLE TAKEN AT 91+40N DUE TO SWAMP.	3.8	414	184.3	3.1	96	1
11846	9350	9200	TILL	B	BROWN	FLAT		0.9	10.2	394.9	0.5	14	1
11847	9400	9200	TILL	B	GREY	FLAT		0.4	14.7	325.7	0.5	10	3
11848	9450	9200	TILL	B	BROWN	FLAT		0.5	5.2	220.4	0.5	10	1
11849	9500	9200	TILL	B	BROWN	FLAT		0.7	9.3	213.1	0.5	10	1
11850	9550	9200	TILL	B	BROWN	FLAT		0.6	18.9	183	0.5	10	1
11851	9600	9200	TILL	B	GREY	FLAT		0.6	14.3	125.6	0.6	10	5
11852	9650	9200	TILL	B	BROWN	FLAT		0.8	9	93.1	0.5	10	1
11853	9700	9200	TILL	B	BROWN	FLAT		0.6	19.9	101.8	0.7	10	1
11854	9750	9200	TILL	B	BROWN	FLAT		0.9	15.7	151	0.7	17	1
11855	9800	9200	TILL	B	BROWN	HILLSIDE SW		0.7	12.8	213.7	0.6	10	1
11856	9850	9200	TILL	B	BROWN/ORANGE	HILLSIDE S		0.9	21	855.1	0.6	14	1
11857	9900	9200	TILL	B	BROWN	FLAT		0.6	222.3	99.8	1.4	18	3
11858	9950	9200	TILL	B	BROWN	FLAT		1.1	98	174.9	3.7	12	5
11845	10000	9200	TILL	B	BROWN	FLAT	NEXT TO ROAD. DISTURBED SITE.	3.6	165.6	109.1	2.4	31	1
11844	10050	9200	TILL	B	BROWN	FLAT	SANDY MATERIAL.	3.7	260.5	92.1	2.8	25	1
11843	10100	9200	TILL	B	BROWN	HILLSIDE W		3.4	149.4	271.1	2.1	29	1
11842	10150	9200	TILL	B	BROWN	HILLSIDE W		1.4	22	116	0.5	13	15
11841	10200	9200	TILL	B	BROWN	HILLSIDE W		2.8	58.7	83.8	1.1	15	1
11840	10250	9200	TILL	B	GREY	HILLSIDE W		2.5	53.8	89.8	0.8	10	2
11839	10300	9200	TILL	B	BROWN	HILLSIDE W		0.9	19.4	83.8	0.5	10	2
11838	10350	9200	TILL	B	BROWN	FLAT		1.3	38.3	108.3	0.5	30	4
11837	10400	9200	TILL	B	BROWN	HILLSIDE W		1	38.1	84	0.7	10	1
11836	10450	9200	TILL	B	BROWN	FLAT		0.9	64.9	90.2	1	29	2
11835	10500	9200	TILL	B	BROWN	HILLSIDE W		1.1	92.8	206.1	1.1	15	3
11834	10550	9200	TILL	B	BROWN	FLAT		0.6	22.1	74.4	0.6	10	85
11833	10600	9200	TILL	B	BROWN	FLAT		1.3	63.9	122.7	1.8	10	3
11832	10650	9200	TILL	B	BROWN	FLAT		1.1	104.4	137.8	1.2	33	1
11831	10700	9200	TILL	B	BROWN	FLAT		0.6	33.3	75.9	0.8	16	3
11830	10750	9200	TILL	B	BROWN	FLAT		1.9	62.9	92.3	1.8	23	1
11829	10800	9200	TILL	B	BROWN	FLAT		0.9	106.6	202.8	1.8	31	1
11828	10850	9200	TILL	B	BROWN	FLAT		0.9	41.5	54.4	0.9	10	1
11827	10900	9200	TILL	B	BROWN	HILLSIDE W		0.6	32.7	53.9	0.6	10	1
11826	10950	9200	TILL	B	BROWN	HILLSIDE W		0.9	54.6	68.5	0.6	10	1
11825	11000	9200	TILL	B	BROWN	HILLSIDE W		1.3	91.9	107.2	1	13	1

UNITED GUNN RESOURCES LTD.
COPPER ACE SOUTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
11824	11050	9200	TILL	B	BROWN	FLAT		1.1	51.2	96.2	0.9	10	1
11972	10000	9250	TILL	B	BROWN	HILLSIDE W	SAMPLE TAKEN AT EAST SIDE OF ROAD AT 100+15E DUE TO SWAMP.	1.1	110.1	67.6	4.4	33	3
10537	9500	9300	TILL	B	BROWN	FLAT	BESIDE ROAD.	0.6	24.9	102.9	0.7	10	1
10538	9550	9300	TILL	B	BROWN/GREY	HILLSIDE SW		0.7	22.7	280.1	0.5	13	2
10539	9600	9300	TILL	B	BROWN/GREY	HILLSIDE SW		0.6	15.6	116.9	0.5	16	1
10540	9650	9300	TILL	B	BROWN/GREY	FLAT		0.5	17.4	122.3	0.5	10	1
10541	9700	9300	TILL	B	BROWN/GREY	FLAT	ABUNDANT FLOAT OF FOLIATED CHLORITE + SERICITE + EPIDOTE ALTERED QUARTZ DIORITE.	0.9	24.6	152.9	0.6	14	1
10542	9750	9300	TILL	B	BLACK/GREY	FLAT		0.8	23.8	106.6	0.6	12	25
10543	9800	9300	TILL	B	BROWN	FLAT		0.6	26.6	119.1	0.5	13	1
10544	9850	9300	TILL	B	BROWN	GULLY NW-SE		1	17.2	294.2	0.5	23	1
10545	9900	9300	TILL	B	BROWN/ORANGE	HILLSIDE E	NO SAMPLE TAKEN AT 99+50 DUE TO SWAMP.	1.2	37.5	448	0.8	20	1
11973	10000	9300	TILL	B	BROWN	FLAT	SAMPLE TAKEN AT EAST SIDE OF ROAD AT 100+05E. BASELINE ON ROAD.	0.6	53.7	54.2	3	29	1
10584	10050	9300	TILL	B	BROWN	FLAT	GOOD B HORIZON.	1	14.3	47.1	1.1	10	1
10583	10100	9300	TILL	B	LIGHT BROWN	FLAT	ROCKY.	0.9	39.2	73.9	1.7	10	1
10582	10150	9300	TILL	B	BROWN	FLAT		1.2	24.2	70.2	1	13	1
10581	10200	9300	TILL	B	LIGHT BROWN	FLAT		2	66.1	60.9	1.9	17	1
10580	10250	9300	TILL	B	BROWN	HILLSIDE W	GOOD B HORIZON.	0.8	29.9	93.3	0.8	10	1
10579	10300	9300	TILL	B	BROWN	HILLSIDE W		0.6	36.2	112.5	0.9	19	1
10578	10350	9300	TILL	B	BROWN/GREY	HILLSIDE W	ROCKY.	1.5	49.4	73.6	1.1	18	1
10577	10400	9300	TILL	B	BROWN	HILLSIDE W	GOOD B HORIZON.	1.4	42.5	78	1	17	1
10576	10450	9300	TILL	B	BROWN	HILLSIDE W		1	15.5	56.2	0.5	25	1
10575	10500	9300	TILL	B	BROWN	HILLSIDE W		1.7	58.2	96.7	0.7	16	1
10574	10550	9300	TILL	B	LIGHT BROWN	HILLTOP W	ROCKY.	0.7	16.3	76.6	0.5	28	1
10573	10600	9300	TILL	B	LIGHT BROWN	FLAT	OUTCROP QUARTZ FELDSPAR PORPHYRY FOLIATED QUARTZ DIORITE.	0.8	15	50	0.6	13	1
10572	10650	9300	TILL	B	BROWN	FLAT	FROM UPROOTED TREE.	1.1	39.4	62.7	1.2	20	1
10571	10700	9300	TILL	B	BROWN	FLAT	FROM UPROOTED TREE.	2.2	131.5	85.2	3.6	30	1
10570	10750	9300	TILL	B	BROWN	FLAT		1.1	22.7	52.9	1.5	12	1
10569	10800	9300	TILL	B	BROWN	FLAT	ROCKY.	1.6	84	69.6	2.3	27	1
10568	10850	9300	TILL	B	BROWN	FLAT		0.6	43	66.4	0.8	28	1
10567	10900	9300	TILL	B	BROWN/ORANGE	FLAT		0.8	44	70.5	0.9	10	3
10566	10950	9300	TILL	B	LIGHT BROWN	FLAT		0.8	57.5	74.6	0.9	18	1
10565	11000	9300	TILL	B	LIGHT BROWN	FLAT		0.5	45.9	56.8	0.6	19	1
10564	11050	9300	TILL	B	LIGHT BROWN	HILLTOP W		1.4	91.8	82.5	1.9	18	1
10563	11100	9300	TILL	B	BROWN	HILLSIDE W		1.9	177.6	173.9	2.8	25	1
10562	11150	9300	TILL	B	BROWN/GREY	FLAT	ROCKY SOIL.	1	39.5	74.9	1.6	23	1
10561	11200	9300	TILL	B	BROWN/GREY	FLAT	ROCKY SOIL.	1.1	66.8	79.7	1.3	10	2
11974	10000	9350	TILL	B	BROWN	FLAT		2	32.2	62.5	1.5	14	1
11965	9175	9400	SAND	B	BROWN	FLAT	FINE GRAINED SANDY SOIL.	1	60.6	365.4	2	30	1
11964	9225	9400	TILL	B	BROWN	HILLSIDE W	15M W OF CLAIM LINE E-W.	0.6	24.6	332.5	0.7	18	3
11963	9275	9400	TILL	B	BROWN	FLAT		1.1	66.7	517.1	0.9	23	1
11962	9325	9400	TILL	B	BROWN	HILLSIDE W		1.7	19.8	160.3	0.6	16	1
11961	9375	9400	TILL	B	BROWN	HILLSIDE W		0.9	24.6	157.5	0.9	11	1
11960	9425	9400	TILL	B	BROWN	HILLSIDE W		0.8	25.3	213	0.6	12	1
11959	9475	9400	TILL	B	BROWN	FLAT		0.4	15.7	187.8	0.8	18	1

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COPPER ACE SOUTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
11958	9525	9400	TILL	B	BROWN	FLAT		0.8	29.9	199.4	0.6	23	1
11957	9575	9400	TILL	B	BROWN	FLAT	EAST SIDE OF ROAD.	1	16.1	117.7	0.7	12	1
11956	9625	9400	TILL	B	BROWN	HILLSIDE W		0.8	16.2	268.3	0.8	17	3
11955	9675	9400	TILL	B	BROWN	HILLSIDE W		0.9	17.9	101.6	1.6	10	1
11954	9725	9400	TILL	B	BROWN	FLAT		1	22.3	114	1.5	10	1
11953	9775	9400	TILL	B	BROWN	FLAT		0.8	21.1	130.7	0.5	12	1
11952	9825	9400	TILL	B	BROWN	FLAT	QUARTZ FLOAT IN HOLE.	0.9	39.4	105.3	0.9	10	1
11951	9875	9400	TILL	B	BROWN	FLAT		0.8	31.7	120.3	0.9	22	1
11950	9925	9400	TILL	B	BROWN	HILLSIDE E		1	23.4	111.2	1.5	10	1
11949	9975	9400	ORGANIC	TOPSOIL	BLACK	GULLY	CREEK BOTTOM.	0.8	553.1	107.8	3.8	81	2
11948	10000	9400	TILL	B	BROWN	HILLSIDE NW	BASE LINE AT ROAD. SOME DISTURBANCE AT SAMPLE SITE.	1.1	114.3	81.1	5.6	59	3
11947	10025	9400	TILL	B	BROWN	HILLSIDE SW		1.4	25.6	55.8	1.5	13	1
11946	10075	9400	TILL	B	BROWN	FLAT		0.6	22.7	87	1.1	25	1
11945	10125	9400	TILL	B	BROWN	FLAT		0.9	30.2	84.3	1	30	2
11944	10175	9400	TILL	B	BROWN	HILLSIDE W		0.9	25.3	71.5	1.3	12	1
11943	10225	9400	TILL	B	BROWN	HILLSIDE W		1.3	134.4	93.4	2.8	46	1
11942	10275	9400	TILL	B	BROWN	HILLSIDE W		0.7	25.2	86.3	1.3	17	1
11941	10325	9400	TILL	B	BROWN	HILLSIDE W		1.3	31.2	82.6	1.7	16	1
11940	10375	9400	TILL	B	BROWN	HILLSIDE W		1	28.3	86.1	1.1	15	1
11939	10425	9400	TILL	B	BROWN	HILLSIDE W		0.7	24.9	71.9	1	24	1
11938	10475	9400	TILL	B	BROWN	HILLSIDE W		1	38.3	73	1.6	24	1
11937	10525	9400	TILL	B	BROWN	HILLSIDE W		1.1	90.4	77.5	2.2	21	1
11936	10575	9400	TILL	B	BROWN	HILLSIDE W	EAST EDGE OF 4 TRAX ROAD - RUNS N-S.	1.4	157.7	86.8	4.9	46	2
11935	10625	9400	TILL	B	BROWN	HILLSIDE W		0.7	19.3	66.9	1.3	25	1
11934	10675	9400	TILL	B	BROWN	HILLSIDE W		1.2	28	88.9	1.5	28	1
11933	10725	9400	TILL	B	BROWN	FLAT		1.1	30	77.5	1.2	17	136
11932	10775	9400	TILL	B	BROWN	FLAT		1.9	175	160	2.7	62	1
11931	10825	9400	TILL	B	BROWN	HILLSIDE W		2.5	322	273.8	4	52	1
11930	10875	9400	TILL	B	BROWN	FLAT		0.6	41.3	59.6	0.9	19	2
11929	10925	9400	TILL	B	BROWN	FLAT		1.4	216	151.8	2.8	42	1
11928	10975	9400	TILL	B	BROWN	FLAT		1.1	74.4	64.6	1.8	26	1
11927	11025	9400	TILL	B	BROWN	HILLSIDE W		1.9	13.5	51.8	1	13	1
11926	11075	9400	TILL	B	BROWN	FLAT		1.1	95.2	89.6	1.9	18	1
11925	11125	9400	TILL	B	BROWN	HILLSIDE W		0.9	35.1	50.2	1.1	17	1
11924	11175	9400	TILL	B	BROWN	HILLSIDE W		1.3	75.9	68.7	1.1	26	1
11923	11225	9400	TILL	B	BROWN	HILLSIDE W	ROUNDED QUARTZ PEBBLES IN TILL.	0.7	34.7	46.8	0.9	47	1
11975	10000	9450	TILL	B	BROWN	FLAT	SAMPLE TAKEN ON EAST SIDE OF ROAD. BASELINE ON ROAD.	0.9	41	72	2.7	12	4
11976	10000	9500	TILL	B	BROWN	HILLSIDE W	BASELINE BELOW ROAD.	1.5	38.6	740	0.8	28	1
11977	10000	9550	TILL	B	BROWN	FLAT	SAMPLE TAKEN AT 100+05E.	1.5	26.6	342.7	1.1	22	1
11889	8900	9600	TILL	B	BROWN	FLAT		0.9	39.5	892.9	1.5	15	1
11890	8950	9600	TILL	B	BROWN	FLAT		0.8	18.7	642.1	1	20	2
11891	9000	9600	TILL	B	BROWN	HILLSIDE N	SIDE OF GULLY.	0.7	61.2	392.6	1.4	22	1
11892	9050	9600	TILL	B	BROWN	HILLSIDE S	SIDE OF GULLY.	1	65.4	283.3	1.2	25	1
11893	9100	9600	TILL	B	BROWN	FLAT		0.4	8.9	140.7	1.2	11	1
11894	9150	9600	TILL	B	BROWN	FLAT		0.5	11.7	147.4	0.5	23	2

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SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
11895	9200	9600	TILL	B	BROWN	HILLSIDE NE		0.4	12.5	131	0.5	20	1
11896	9250	9600	TILL	B	BROWN	HILLSIDE E		0.7	13.4	143.1	0.8	10	1
11897	9300	9600	TILL	B	BROWN	FLAT		1.9	10.1	78.9	0.5	18	1
11898	9350	9600	TILL	B	BROWN	FLAT		2.2	163.8	465.2	1.4	51	2
11899	9400	9600	TILL	B	BROWN	HILLSIDE SW		1.1	17.4	485.3	1	22	1
11900	9450	9600	TILL	B	GREY	FLAT		0.6	13.7	196.3	0.5	11	14
12201	9500	9600	TILL	B	GREY	FLAT		0.8	17.8	149	0.7	10	3
12202	9550	9600	TILL	B	BROWN	FLAT		0.6	9.4	181.6	0.5	10	1
12203	9600	9600	TILL	B	BROWN	HILLSIDE NE		0.7	13.4	173	0.6	10	3
12204	9650	9600	TILL	B	BROWN	FLAT	NEXT TO OLD ROAD.	0.6	114.8	153.2	0.9	20	3
12205	9700	9600	TILL	B	BROWN	HILLSIDE SW		0.6	22.5	58.3	1	14	2
12206	9750	9600	TILL	B	BROWN	FLAT		0.8	32.8	117	0.5	10	3
12207	9800	9600	TILL	B	BROWN	FLAT		0.9	16.3	142	0.5	10	2
12208	9850	9600	TILL	B	BROWN	FLAT		0.7	16.3	152.8	0.5	10	1
12209	9900	9600	TILL	B	GREY	FLAT		0.7	10.4	96.4	0.5	10	2
12210	9950	9600	TILL	B	BROWN	HILLSIDE E		0.9	76.6	88.9	1.4	10	3
11888	10000	9600	TILL	B	BROWN	HILLSIDE W		1.3	85.5	67.7	4.3	14	1
11887	10050	9600	TILL	B	BROWN	HILLSIDE W		1.3	58.5	109.1	2.8	15	1
11886	10100	9600	TILL	B	BROWN	FLAT		0.9	12.7	74.5	0.5	10	1
11885	10150	9600	TILL	B	BROWN	FLAT		0.6	16.3	102.7	0.6	10	2
11884	10200	9600	TILL	B	BROWN	FLAT		0.6	42.8	75.1	0.8	10	1
11883	10250	9600	TILL	B	BROWN	FLAT		0.6	31.8	71	1	10	1
11882	10300	9600	TILL	B	BROWN	FLAT		0.7	19.5	71.5	0.5	10	1
11881	10350	9600	TILL	B	BROWN	FLAT		0.6	29.3	63.7	0.8	10	4
11880	10400	9600	TILL	B	BROWN	HILLSIDE W		1.2	58.2	79.8	1.4	10	5
11879	10450	9600	TILL	B	BROWN	HILLSIDE W		0.7	32.2	83.2	0.5	10	1
11878	10500	9600	TILL	B	BROWN	HILLSIDE W		0.6	43.9	91.9	0.9	20	1
11877	10550	9600	TILL	B	BROWN	HILLSIDE W		0.5	30.8	81.1	0.5	10	1
11876	10600	9600	TILL	B	BROWN	HILLSIDE W		0.7	38.1	73.3	1.3	13	2
11875	10650	9600	TILL	B	BROWN	FLAT	EDGE OF ROAD.	1	84	70.6	4	10	5
11874	10700	9600	TILL	B	BROWN	HILLSIDE W		0.8	73.5	65.4	2.6	21	2
11873	10750	9600	TILL	B	BROWN	HILLSIDE W		0.9	39.9	63.1	2.2	10	9
11872	10800	9600	TILL	B	BROWN	FLAT		1.5	172.9	225.8	5.7	29	1
11871	10850	9600	TILL	B	BROWN	FLAT		1.4	100.5	91.6	4.8	25	1
11870	10900	9600	TILL	B	BROWN	FLAT		0.8	57.9	60.9	2.6	19	1
11869	10950	9600	TILL	B	BROWN	HILLSIDE W		0.9	104.6	104.8	4.3	28	1
11868	11000	9600	TILL	B	BROWN	FLAT		1.2	97.5	88.3	5.2	21	1
11867	11050	9600	TILL	B	BROWN	FLAT		0.7	66.1	73.3	2.1	14	3
11866	11100	9600	TILL	B	BROWN	FLAT		0.8	44.4	68.4	1.3	20	4
11865	11150	9600	TILL	B	BROWN	FLAT		1.5	272.1	208.5	6.8	38	1
11864	11200	9600	TILL	B	BROWN	FLAT		1	116.8	89.9	3	36	3
11863	11250	9600	TILL	B	BROWN	FLAT		0.7	66.2	82.8	1.4	10	1
11862	11300	9600	TILL	B	BLACK	FLAT	ORGANIC RICH. ALDER, SWAMPY.	2.2	769.8	184.6	7.8	72	1
11861	11350	9600	TILL	B	GREY	HILLSIDE W		0.9	40.7	74.8	0.9	10	1
11860	11400	9600	TILL	B	BROWN	HILLSIDE W		0.4	61.2	63.8	0.6	10	1
11859	11450	9600	TILL	B	BROWN	FLAT		0.6	37.5	61.9	1.2	10	1

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SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
11978	10000	9650	TILL	B	BROWN	FLAT	SAMPLE TAKEN AT 99+90E. BASELINE AT CREEK.	1	27.8	301.5	1.5	23	1
11979	10000	9700	TILL	B	BROWN	FLAT	SAMPLE TAKEN AT 100+20E. BASELINE AT CREEK.	1.2	47.3	150.4	1.5	29	13
11980	10000	9750	TILL	B	BROWN	HILLSIDE S	OUTCROP.	0.5	18	104.5	0.9	12	1
12112	8625	9800	TILL	B	BROWN	FLAT	SAMPLE TAKEN 5M EAST OF ROAD.	0.9	39	95.7	3.1	14	1
12111	8675	9800	TILL	B	BROWN	FLAT		0.5	6	158.9	0.7	16	1
12110	8725	9800	TILL	B	BROWN	FLAT		0.4	10.6	127.1	0.9	10	1
12109	8775	9800	TILL	B	BROWN	FLAT		0.7	13.2	122.1	0.6	15	1
12108	8825	9800	TILL	B	BROWN	FLAT		2	40.5	743.5	0.6	29	2
12107	8875	9800	TILL	B	BROWN	FLAT		1.2	62.3	779.3	0.5	34	2
12106	8925	9800	TILL	B	BROWN	FLAT		1.1	22.6	942.5	1.4	24	27
12105	8975	9800	TILL	B	BROWN	FLAT		1.1	32.3	1175	1	27	1
12104	9025	9800	TILL	B	BROWN	FLAT		1.4	45.8	723.6	0.9	43	1
12103	9075	9800	TILL	B	BROWN/GREY	FLAT		0.7	12.7	206.3	0.5	10	2
12102	9125	9800	TILL	B	BROWN	FLAT		0.8	16.9	234.8	0.6	21	1
12101	9175	9800	TILL	B	BROWN	FLAT		0.7	6.8	257.4	0.5	10	2
11800	9225	9800	TILL	B	BROWN	FLAT		1.1	11.8	305.9	1.2	25	2
11799	9275	9800	TILL	B	BROWN	FLAT		0.7	10.1	281.6	0.5	25	1
11798	9325	9800	TILL	B	BROWN	FLAT		1.9	42.1	483	1.4	40	2
11797	9375	9800	TILL	B	BROWN	FLAT		1.3	45.2	519.7	2.2	40	4
11796	9425	9800	TILL	B	BROWN	FLAT		1.5	35.3	564.3	2.2	30	41
11795	9475	9800	TILL	B	BROWN	FLAT		1.2	19.7	339	0.6	10	1
11794	9525	9800	TILL	B	BROWN	FLAT		3.2	53.2	183	1	30	1
11793	9575	9800	TILL	B	BROWN	FLAT		1.2	25.6	114.4	1	15	4
11792	9625	9800	TILL	B	BROWN	FLAT		1.2	14.7	119.5	0.5	10	1
11791	9675	9800	TILL	B	BROWN	FLAT		1.3	20.5	117.4	0.7	30	2
11790	9725	9800	TILL	B	BROWN	FLAT		0.9	79.2	94.1	1.2	25	1
11789	9775	9800	TILL	B	BROWN	FLAT		0.7	8.8	91.3	0.5	10	8
11788	9825	9800	TILL	B	BROWN	FLAT		1.3	28.9	127.4	0.5	15	1
11787	9875	9800	TILL	B	BROWN	FLAT		1.6	34.9	221	0.8	15	2
11786	9925	9800	TILL	B	BROWN/GREY	FLAT		6.9	160.9	104.5	2.5	55	1
11785	9975	9800	TILL	B	BROWN	FLAT		2.3	39.6	240.9	1.2	15	1
11784	10000	9800	TILL	B	BROWN	FLAT		3.8	66.8	218.1	0.7	25	5
11783	10025	9800	TILL	B	BROWN	FLAT		1.2	33.1	120.7	0.6	25	8
11782	10075	9800	TILL	B	BROWN	FLAT		0.7	17.2	141.3	0.8	25	1
11781	10125	9800	TILL	B	BROWN	FLAT		0.9	22.2	83.2	0.6	20	1
11780	10175	9800	TILL	B	BROWN	FLAT		0.5	32.9	100.2	0.6	15	1
11779	10225	9800	TILL	B	BROWN	FLAT		1.7	111.6	80.5	1.3	35	2
11778	10275	9800	TILL	B	BROWN	FLAT		0.8	16.9	67.9	1.2	10	2
11777	10325	9800	TILL	B	BROWN	FLAT		1.2	58.2	101.4	2.5	20	3
11776	10375	9800	TILL	B	BROWN	FLAT		1.2	52.3	71.4	0.9	15	2
11775	10425	9800	TILL	B	BROWN	FLAT		0.9	19.1	121.5	0.5	15	1
11774	10475	9800	TILL	B	BROWN	FLAT		0.9	18.7	99.4	0.5	20	1
11773	10525	9800	TILL	B	BROWN	FLAT		1.4	38	76.8	0.8	20	1
11772	10575	9800	TILL	B	BROWN	FLAT		3.2	123.7	115.9	0.8	15	1
11771	10625	9800	TILL	B	BROWN	FLAT		3.5	607	345.2	4.1	95	2
11770	10675	9800	TILL	B	BROWN	FLAT		1.5	62.3	76.9	1	25	1

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COPPER ACE SOUTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
11769	10725	9800	TILL	B	BROWN	FLAT		1.5	59.2	72.1	0.9	20	1
11768	10775	9800	TILL	B	BROWN	FLAT		1.2	26.8	50.6	0.8	20	1
11767	10825	9800	TILL	B	BROWN	FLAT		1.1	56.6	70.3	2.6	34	1
11766	10875	9800	TILL	B	BROWN	FLAT		0.9	21.6	75.1	1.1	16	1
11765	10925	9800	TILL	B	BROWN	FLAT		1.8	70.6	84.8	1.4	22	2
11764	10975	9800	TILL	B	BROWN	FLAT		0.8	30.5	75.7	1.2	14	1
11763	11025	9800	TILL	B	BROWN	FLAT		0.9	41.2	52.9	1.1	17	1
11762	11075	9800	TILL	B	BROWN	FLAT		0.6	38.6	91.4	1.4	16	1
11761	11125	9800	TILL	B	BROWN	FLAT		2.1	304.5	211.8	6.6	55	1
11760	11175	9800	TILL	B	BROWN	FLAT		0.7	12	88.4	0.8	10	2
11759	11225	9800	TILL	B	BROWN	FLAT		1.9	247.5	114.4	4.6	59	3
11758	11275	9800	TILL	B	BROWN	FLAT		1.7	312.3	80.6	4.9	40	2
11757	11325	9800	TILL	B	BLACK/BROWN	FLAT		2.6	669.4	137	1.9	85	1
11756	11375	9800	TILL	B	BROWN	FLAT		1.5	37.1	317.5	1.5	10	1
11755	11425	9800	TILL	B	BROWN	FLAT		1.2	28.4	120.2	0.9	12	1
11754	11475	9800	TILL	B	BROWN	FLAT		0.8	77.5	87.9	1.1	16	1
11753	11525	9800	TILL	B	BROWN	FLAT		0.8	23.6	73.5	0.5	15	16
11752	11575	9800	TILL	B	BROWN/GREY	FLAT		1.3	42.1	52.4	0.5	10	1
11981	10000	9850	TILL	B	BROWN	FLAT		1.2	30.6	200.8	1.4	22	1
11982	10000	9900	TILL	B	BROWN	HILLSIDE W		1	10.8	185.6	1.5	30	3
11983	10000	9950	TILL	B	BROWN	FLAT		0.6	15.8	176.2	1.1	15	1
12126	8600	10000	TILL	B	BROWN	FLAT		1.2	21	218.1	0.8	15	2
12125	8650	10000	TILL	B	BROWN	FLAT		1.8	168.1	589.7	3.3	51	4
12124	8700	10000	TILL	B	BROWN	FLAT	SAMPLE TAKEN 7M N OF STATION DUE TO SWAMP.	2.1	89	489.7	2.1	34	1
12123	8750	10000	TILL	B	BROWN	FLAT		0.5	10.1	116.5	1	10	1
12122	8800	10000	TILL	B	BROWN	FLAT		0.3	5.6	133.6	0.6	21	1
12121	8850	10000	TILL	B	BROWN	FLAT		0.5	6.8	86.1	0.5	10	1
12120	8900	10000	TILL	B	BROWN	FLAT		0.9	11.7	132.9	0.6	11	1
12119	8950	10000	TILL	B	BROWN	FLAT		1.8	20.7	251.2	0.6	21	1
12118	9000	10000	TILL	B	BROWN	FLAT	SAMPLE TAKEN 10M S OF STATION DUE TO SWAMP.	3.3	35.7	306.7	1.5	12	2
12117	9050	10000	TILL	B	BROWN	FLAT		3.2	36.7	720.8	1.9	23	1
12116	9100	10000	TILL	B	BROWN	FLAT		2.1	40.4	825.7	1.5	32	4
12115	9150	10000	TILL	B	BROWN	FLAT		1.4	53.2	537.9	1.1	19	1
12114	9200	10000	TILL	B	BROWN	FLAT		1	6.9	82.1	0.5	10	1
12113	9250	10000	TILL	B	BROWN/GREY	FLAT	SAMPLE TAKEN 5M W OF CREEK.	1.7	14.1	53.3	1.6	22	1
12038	9300	10000	TILL	B	BROWN	HILLSIDE SW		1.8	17.5	117.9	0.8	22	1
12039	9350	10000	TILL	B	BROWN	HILLSIDE SW		2.2	27.3	621.2	1.3	23	1
12040	9400	10000	TILL	B	BROWN	HILLSIDE NE		0.8	36.7	263.5	1.5	14	5
12041	9500	10000	TILL	B	GREY	HILLSIDE S	NO SAMPLE TAKEN AT 94+50E DUE TO BOG.	1.5	10.7	56	0.5	31	1
12042	9550	10000	TILL	B	GREY	HILLSIDE S		0.7	252.1	220.3	0.7	41	2
12043	9600	10000	TILL	B	GREY	HILLSIDE S		1.3	19.3	124	0.5	19	3
12044	9650	10000	TILL	B	BROWN	HILLSIDE S		0.4	11.9	220.2	0.6	10	1
12045	9700	10000	TILL	B	BROWN	HILLSIDE SW		0.8	15.2	214.1	0.6	10	4
12046	9750	10000	TILL	B	BROWN	HILLSIDE S		0.9	135.7	66.4	1.1	10	1
12047	9800	10000	TILL	B	BROWN	HILLSIDE SW		1.2	54.6	139	3.1	10	1
12048	9850	10000	TILL	B	GREY	HILLSIDE SW		1.9	373.3	631	2.1	27	2

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SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
12049	9900	10000	TILL	B	GREY	HILLSIDE SW		1.7	270.5	227.3	1.4	30	1
12050	9950	10000	TILL	B	BROWN	HILLSIDE S		1.5	63.4	103.4	1.5	10	4
12037	10000	10000	TILL	B	BROWN	HILLSIDE SW		0.9	17.9	126.8	0.5	25	2
12036	10050	10000	TILL	B	BROWN	HILLSIDE NE		0.6	15.4	152.4	0.5	13	1
12035	10100	10000	TILL	B	BROWN	HILLSIDE NE		0.5	13.1	377.5	0.5	10	3
12034	10150	10000	TILL	B	BROWN	HILLSIDE SW		0.6	28.6	150.3	0.5	10	2
12033	10200	10000	TILL	B	BROWN	HILLSIDE SW		0.9	21.1	94.6	0.5	10	1
12032	10250	10000	TILL	B	BROWN	HILLSIDE SW		0.4	37.7	98.2	0.5	12	2
12031	10300	10000	TILL	B	BROWN	HILLSIDE SW		0.9	36.4	63.7	0.6	15	4
12030	10350	10000	TILL	B	BROWN	HILLSIDE SW		0.7	38	70.2	2.2	33	6
12029	10400	10000	TILL	B	BROWN	HILLSIDE SW		0.7	15.2	63.6	0.5	14	6
12028	10450	10000	TILL	B	BROWN	HILLSIDE SW		1	71.7	73.3	1.1	16	3
12027	10500	10000	TILL	B	BROWN	HILLSIDE SW		1	20	81.7	0.5	10	1
12026	10550	10000	TILL	B	BROWN	HILLSIDE SW		1	80.1	97.9	1.5	27	1
12025	10600	10000	TILL	B	BROWN	HILLSIDE SW		2	272.6	172.4	2.3	53	1
12024	10650	10000	TILL	B	BROWN	HILLSIDE SW		0.8	19.8	56.9	1.3	11	1
12023	10700	10000	TILL	B	BROWN	HILLSIDE SW		1.5	235.7	140.4	1.6	68	2
12022	10750	10000	TILL	B	BROWN	HILLSIDE SW		1.2	28.2	69	0.8	14	1
12021	10800	10000	TILL	B	BROWN	HILLSIDE SW		2	132.9	91.1	3.6	46	2
12020	10850	10000	TILL	B	BROWN	HILLSIDE SW		0.9	39.2	69.3	0.6	10	2
12019	10900	10000	TILL	B	BROWN	HILLSIDE W		0.9	45	88.9	0.7	25	2
12018	10950	10000	TILL	B	BROWN	HILLSIDE W		1	58.5	86.3	1.1	32	1
12017	11000	10000	TILL	B	BROWN	HILLSIDE W		0.9	30.8	55.6	0.9	21	1
12016	11050	10000	TILL	B	BROWN	HILLSIDE W		1.1	130.7	148.4	2.3	28	2
12015	11100	10000	TILL	B	BROWN	GULLY		1.3	370.8	98.2	1.9	46	1
12014	11150	10000	TILL	B	BROWN	HILLSIDE SW		1.3	176.9	95.2	1.9	32	1
12013	11200	10000	TILL	B	BROWN	HILLSIDE SW		0.7	79.4	75.2	0.6	31	1
12012	11250	10000	TILL	B	BROWN	HILLSIDE SW		0.8	75.8	86.4	0.8	29	1
12011	11300	10000	TILL	B	BROWN	HILLSIDE SW		0.5	47.2	77.2	0.5	21	1
12010	11350	10000	TILL	B	BROWN	HILLSIDE SW		0.3	28.3	44.4	0.6	10	1
12009	11400	10000	TILL	B	BROWN	HILLSIDE SW		1.1	115.4	99.1	1.8	35	1
12008	11450	10000	TILL	B	BROWN	HILLSIDE SW		1.3	146.1	116.5	3.8	24	1
12007	11500	10000	TILL	B	BROWN	HILLSIDE N		0.7	52.2	73.9	0.6	12	1
12006	11550	10000	TILL	B	BROWN	HILLSIDE N		0.5	58.5	66.1	0.7	20	1
12005	11600	10000	TILL	B	BROWN	HILLSIDE N		0.5	44.2	51.7	1	23	1
12004	11650	10000	TILL	B	BROWN	HILLSIDE N		0.7	74.9	72.7	1.5	15	1
12003	11700	10000	TILL	B	BROWN	HILLSIDE N		0.3	43.7	58.6	0.6	13	2
12002	11750	10000	TILL	B	BROWN	HILLSIDE N		0.5	41	55.8	0.5	10	3
12001	11800	10000	TILL	B	BROWN	HILLSIDE N		0.7	62.9	61.3	2	10	4
11984	10000	10050	TILL	B	BROWN	FLAT		0.6	13.7	154.4	0.7	19	1
11985	10000	10100	TILL	B	BROWN	FLAT		0.9	9	50.4	0.5	10	1
11986	10000	10150	TILL	B	BROWN	FLAT		0.5	10.9	104.3	0.7	18	1
12187	8875	10200	TILL	B	BROWN	FLAT	NO SAMPLES TAKEN AT 88+25E AND 87+75E DUE TO LARGE SWAMP.	1.2	17.6	320.4	0.9	21	4
12186	8925	10200	TILL	B	BROWN	FLAT	SAMPLE TAKEN FROM UPROOTED TREE.	4.1	38.6	190.1	1.6	30	1
12185	8975	10200	TILL	B	BROWN	FLAT		0.9	11.4	160.2	0.5	10	1
12184	9025	10200	TILL	B	BROWN	FLAT		0.5	10.4	135.9	0.8	10	1

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SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
12183	9075	10200	TILL	B	BROWN	FLAT		0.6	7.8	224.7	0.5	10	3
12182	9125	10200	TILL	B	BROWN	FLAT	NO SAMPLES TAKEN AT 92+75E, 92+25E AND 91+75E DUE TO LARGE SWAMP.	1.2	11.6	171.2	0.5	10	1
12181	9325	10200	TILL	B	BROWN	FLAT	SAMPLE TAKEN 10M N OF STATION.	1.1	20.5	65.1	0.6	18	1
12180	9375	10200	TILL	B	BROWN	FLAT		1.2	33.5	159.5	1.7	21	1
12179	9425	10200	TILL	B	BROWN	FLAT		1.5	31.1	400.8	0.7	10	1
12178	9475	10200	TILL	B	BROWN	FLAT		1.3	39.1	130	0.5	14	3
12177	9525	10200	TILL	B	BROWN	FLAT		0.5	12.4	83.2	0.5	10	1
12176	9575	10200	TILL	B	BROWN	FLAT		0.5	14.5	148.2	0.5	10	4
12175	9625	10200	TILL	B	BROWN	FLAT		0.5	17.4	126.9	0.7	17	1
12174	9675	10200	TILL	B	BROWN	FLAT		0.6	10.2	118.5	0.5	10	18
12173	9725	10200	TILL	B	BROWN	FLAT		0.8	14.4	84	0.5	10	1
12172	9775	10200	TILL	B	BROWN/GREY	FLAT		1.5	118	98	1.2	36	2
12171	9825	10200	TILL	B	BROWN/GREY	FLAT	SAMPLE TAKEN 10M N OF STATION.	0.8	120.5	62.3	1.2	28	1
12170	9875	10200	TILL	B	BROWN	FLAT		1.4	18.4	57.9	0.5	18	1
12169	9925	10200	TILL	B	BROWN	FLAT		1.4	13.7	41.3	0.5	10	1
12168	9975	10200	TILL	B	BROWN	FLAT		1	11.8	41.5	1.4	10	1
12167	10000	10200	TILL	B	BROWN	FLAT		1	28.3	94.8	0.9	17	2
12166	10025	10200	TILL	B	BROWN	FLAT		0.8	26.5	108.3	0.5	10	3
12165	10075	10200	TILL	B	BROWN	FLAT		0.7	10.6	79.7	0.5	10	1
12164	10125	10200	TILL	B	BROWN	FLAT		1.5	37.2	181.3	0.5	17	1
12163	10175	10200	TILL	B	BROWN	FLAT		1.1	12.3	34.4	0.5	10	1
12162	10225	10200	TILL	B	BROWN	FLAT		0.5	12.2	81.4	0.5	10	1
12161	10275	10200	TILL	B	BROWN	FLAT		0.8	25.9	66.7	0.6	15	1
12160	10325	10200	TILL	B	BROWN	FLAT		0.6	25.3	63.4	1	10	1
12159	10375	10200	TILL	B	BROWN	FLAT		1	13	102.9	0.8	10	1
12158	10425	10200	TILL	B	BROWN	FLAT		0.6	10	54.4	0.6	10	1
12157	10475	10200	TILL	B	BROWN	FLAT		0.9	15.5	77.6	0.6	11	1
12156	10525	10200	TILL	B	BROWN	FLAT		0.9	13.9	71.1	0.7	10	1
12155	10575	10200	TILL	B	BROWN	FLAT		1.7	36.9	84.3	0.6	12	1
12154	10625	10200	TILL	B	BROWN	FLAT							
12153	10675	10200	TILL	B	BROWN	FLAT		2.1	33.9	43.4	1.5	10	1
12152	10725	10200	TILL	B	BROWN	FLAT		1.7	32.4	50.5	0.6	10	3
12151	10775	10200	TILL	B	BROWN	FLAT		1.2	21.2	55.6	1	10	2
12150	10825	10200	TILL	B	BROWN	FLAT		1.8	1074.3	146.2	3.2	73	2
12149	10875	10200	TILL	B	BROWN	FLAT		1.7	407.8	98.5	3.5	41	3
12148	10925	10200	TILL	B	BROWN	FLAT		1.4	258.2	78.4	2.7	38	2
12147	10975	10200	TILL	B	BROWN	FLAT		0.7	20.4	54.6	0.8	13	2
12146	11025	10200	TILL	B	BROWN	FLAT		2	27.6	120.8	1.4	27	1
12145	11075	10200	TILL	B	BROWN	FLAT		1.5	99.4	87.2	2.2	27	1
12144	11125	10200	TILL	B	BROWN	FLAT		1	83	165.9	0.5	18	1
12143	11175	10200	TILL	B	BROWN	FLAT		1.1	76.8	95.8	1	18	1
12142	11225	10200	TILL	B	BROWN	FLAT		0.7	45.5	57.6	0.8	21	1
12141	11275	10200	TILL	B	BROWN	FLAT		0.6	52.2	72.8	0.9	20	2
12140	11325	10200	TILL	B	BROWN	FLAT		0.4	38.3	47	0.5	24	1
12139	11375	10200	TILL	B	BROWN	FLAT		0.5	45.8	53.8	0.7	10	1
12138	11425	10200	TILL	B	BROWN/GREY	FLAT		0.6	48.6	51.4	0.5	10	1

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12137	11475	10200	TILL	B	BROWN	FLAT		0.6	105.1	81.4	1.1	14	1
12136	11525	10200	TILL	B	BROWN	FLAT		1.3	96.3	83	1.3	16	1
12135	11575	10200	TILL	B	BROWN	FLAT		1.1	194.6	128.7	1.4	19	1
12134	11625	10200	TILL	B	BROWN	FLAT		1.6	261.1	171.5	2.9	59	1
12133	11675	10200	TILL	B	BROWN	FLAT		1	127.6	98.4	1.3	35	2
12132	11725	10200	TILL	B	BROWN	FLAT		0.5	34.2	44.2	0.6	10	3
12131	11775	10200	TILL	B	BROWN	FLAT		0.9	67.5	95	0.9	28	1
12130	11825	10200	TILL	B	BROWN	FLAT		1.2	135	138.7	1.4	35	2
12129	11875	10200	TILL	B	BROWN	FLAT		0.9	100.9	100.5	1.6	31	1
12128	11925	10200	TILL	B	BROWN	FLAT		1.3	119.6	128.7	1.8	32	1
12127	11975	10200	TILL	B	BROWN	FLAT		0.9	122.8	97.9	1.4	27	1
11987	10000	10250	TILL	B	BROWN	FLAT		0.7	12.1	65.6	0.7	19	1
11988	10000	10300	TILL	B	BROWN	FLAT	SAMPLE TAKEN AT 100+10E DUE TO SWAMP.	0.8	40	93.9	2.5	36	1
11989	10000	10350	TILL	B	BROWN	HILLSIDE S		0.5	13.7	77.3	1.5	10	1
12268	9050	10400	TILL	B	BROWN	FLAT	SAMPLE TAKEN AT 90+65E DUE TO SWAMP.	0.6	15.8	107.6	0.9	22	5
12267	9100	10400	TILL	B	BROWN	FLAT		0.7	9.5	96.5	0.5	10	2
12266	9150	10400	TILL	B	BROWN	FLAT		0.9	12.6	424.5	0.7	21	2
12265	9200	10400	TILL	B	BROWN	FLAT		0.9	10.8	353.2	0.5	10	4
12264	9250	10400	TILL	B	BROWN	HILLSIDE W		0.5	14.3	309	0.8	13	3
12263	9300	10400	TILL	B	BROWN	FLAT		0.9	17	361.4	0.5	18	40
12262	9350	10400	TILL	B	BROWN	FLAT		0.6	18.9	103.6	1.3	10	4
12261	9400	10400	TILL	B	GREY	FLAT		0.6	9.2	89.8	1.9	10	9
12260	9450	10400	TILL	B	GREY	FLAT		0.4	16.9	68.2	0.5	10	3
12259	9500	10400	TILL	B	BROWN	HILLSIDE E	BASE OF SLOPE.	0.5	18.1	100.2	0.5	18	1
12258	9550	10400	TILL	B	BROWN	HILLSIDE W	GULLY BANK.	0.4	18.5	112.2	0.5	10	1
12257	9600	10400	TILL	B	GREY	FLAT	NEXT TO ROAD.	0.4	7.9	109	0.5	10	2
12256	9650	10400	TILL	B	BROWN	FLAT		0.4	9.8	92.2	0.5	10	1
12255	9700	10400	TILL	B	BROWN	FLAT		0.4	12.8	89.9	0.5	12	1
12254	9750	10400	TILL	B	BROWN	FLAT		0.5	8.7	91.9	0.5	14	1
12253	9800	10400	TILL	B	GREY	FLAT		0.6	15.5	91.2	0.5	16	1
12252	9850	10400	TILL	B	GREY	FLAT		0.5	16.1	88	0.5	10	1
12251	9900	10400	TILL	B	BROWN	FLAT		0.5	23.2	107.2	0.5	35	1
12250	9950	10400	TILL	B	BROWN	FLAT		0.5	10.1	102.4	0.5	13	1
12249	10000	10400	TILL	B	BROWN	FLAT		0.8	20.8	106.4	0.6	11	1
12248	10050	10400	TILL	B	BROWN	FLAT		0.7	12.7	89.1	0.6	19	1
12247	10100	10400	TILL	B	BROWN	FLAT	NO SAMPLE TAKEN AT 103+00, 102+50, 102+00 AND 101+50 DUE TO SWAMP.	0.4	27.4	39.3	0.6	12	1
12246	10350	10400	TILL	B	BROWN	FLAT		1.1	14.8	84.8	0.5	27	1
12245	10400	10400	TILL	B	BROWN	FLAT		1.2	28.9	112.3	1	36	1
12244	10450	10400	TILL	B	BROWN	FLAT		0.7	13.6	118.2	0.9	16	1
12243	10500	10400	TILL	B	BROWN	FLAT	EDGE OF LANDING.	1	20.6	92.3	0.8	24	79
12242	10550	10400	TILL	B	BROWN	FLAT	EDGE OF LANDING. DISTURBED SITE.	2.4	152.6	123.4	2.2	36	1
12241	10600	10400	TILL	B	BROWN	FLAT		0.7	10.5	68.8	0.5	10	1
12240	10650	10400	TILL	B	ORANGE	FLAT		0.8	16.2	127.1	0.5	10	3
12239	10700	10400	TILL	B	BROWN/GREY	FLAT		0.9	19.1	80	0.6	10	1
12238	10750	10400	TILL	B	BROWN	FLAT		0.9	32.2	174.4	0.9	10	1
12237	10800	10400	TILL	B	BROWN	FLAT		1.4	682.2	115.5	2.4	42	4

UNITED GUNN RESOURCES LTD.
COPPER ACE SOUTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
12236	10850	10400	TILL	B	BROWN	FLAT	ORGANIC RICH. DECIDUOUS STAND.	1.8	758.3	117.5	2.6	60	2
12235	10900	10400	TILL	B	BLACK	FLAT	HUMUS RICH. DECIDUOUS STAND.	2.4	810.2	305.5	5.1	138	4
12234	10950	10400	TILL	B	GREY	HILLSIDE SW	HUMUS RICH. DECIDUOUS STAND.	11.7	726.8	242.2	6.6	127	3
12233	11000	10400	TILL	B	GREY	HILLSIDE SW		0.8	36	69.6	0.7	16	1
12232	11050	10400	TILL	B	GREY	HILLSIDE S		0.5	11.6	81	0.5	10	1
12231	11100	10400	TILL	B	BROWN	HILLSIDE SW		1	68.8	114.1	1	25	1
12230	11150	10400	TILL	B	BROWN	HILLSIDE SW		0.6	31.8	87.2	0.7	24	1
12229	11200	10400	TILL	B	GREY	HILLSIDE SW		0.6	17.1	86.1	0.8	12	2
12228	11250	10400	TILL	B	BROWN	HILLSIDE SW		0.7	21.7	124.2	1.2	19	1
12227	11300	10400	TILL	B	BROWN	HILLSIDE SW		0.9	142.5	124.3	1	42	2
12226	11350	10400	TILL	B	BROWN	HILLSIDE SW		0.7	41.8	62.3	1.3	19	2
12225	11400	10400	TILL	B	BROWN	HILLSIDE SW		0.8	67.9	89	1	23	1
12224	11450	10400	TILL	B	BROWN	HILLSIDE W		0.9	70	90.4	1.2	28	1
12223	11500	10400	TILL	B	BROWN	HILLSIDE SW		1.5	154.1	140.6	2.5	41	6
12222	11550	10400	TILL	B	ORANGE	HILLSIDE SW		1.1	43.8	149.7	1	28	1
12221	11600	10400	TILL	B	BROWN	HILLSIDE SW		0.6	58.4	72.4	0.7	14	1
12220	11650	10400	TILL	B	BROWN	HILLSIDE SW		0.6	30.8	61.5	0.5	11	1
12219	11700	10400	TILL	B	BROWN	HILLSIDE SW		0.5	38.4	61.7	0.5	10	1
12218	11750	10400	TILL	B	BROWN	HILLSIDE S		0.6	37.1	52.5	0.9	10	1
12217	11800	10400	TILL	B	BROWN	HILLSIDE S		0.8	26.4	68.2	0.8	12	1
12216	11850	10400	TILL	B	GREY	HILLSIDE S		0.5	33.9	68.5	0.5	10	1
12215	11900	10400	TILL	B	BROWN	FLAT		0.3	25.8	49.3	0.5	10	4
12214	11950	10400	TILL	B	GREY	FLAT		0.4	26	42.1	0.5	10	1
12213	12000	10400	TILL	B	BROWN	FLAT		1.1	97.7	80.2	0.9	21	1
12212	12050	10400	TILL	B	BROWN	HILLSIDE SW		0.5	32.3	45.6	0.5	10	1
12211	12100	10400	TILL	B	BROWN	HILLSIDE SW		0.4	48.5	63.1	0.5	12	2
11990	10000	10450	TILL	B	BROWN	HILLSIDE S		0.7	13.1	90	1.6	13	1
11991	10000	10500	TILL	B	BROWN	HILLSIDE S		0.4	24.2	68.9	1.1	12	1
11992	10000	10550	TILL	B	BROWN	FLAT		0.4	13.4	95.3	1.2	12	1
12068	9175	10600	TILL	B	BROWN	HILLSIDE W		1.6	10.1	102.9	0.6	10	10
12067	9225	10600	TILL	B	BROWN	HILLSIDE SW		0.4	11.5	429.9	0.5	13	3
12066	9275	10600	TILL	B	BROWN	HILLSIDE SW		0.6	18.6	162.6	0.7	10	1
12065	9325	10600	TILL	B	BROWN	HILLSIDE SW		0.5	12.7	237.9	0.5	10	1
12064	9375	10600	TILL	B	GREY	HILLSIDE W		0.5	10.9	174.3	0.5	10	8
12063	9425	10600	TILL	B	BROWN	HILLSIDE NE		0.7	37.1	237.3	1.2	17	3
12062	9475	10600	TILL	B	BROWN	GULLY	SAMPLE TAKEN 8M N OF STATION.	1.1	56.4	201.2	0.9	23	1
12061	9525	10600	TILL	B	BROWN	HILLSIDE S		0.7	78.9	133	1.7	12	4
12060	9575	10600	TILL	B	BROWN	HILLSIDE NW		0.6	18.1	68.6	0.7	10	17
12059	9625	10600	TILL	B	BROWN	HILLSIDE NW		0.6	10.8	120.8	0.5	11	4
12058	9675	10600	TILL	B	BROWN	HILLSIDE W		0.4	13	83.3	0.5	10	3
12057	9725	10600	TILL	B	GREY	HILLSIDE W		0.6	21.2	94.4	0.7	10	6
12056	9775	10600	TILL	B	BROWN	HILLSIDE W		0.3	12.2	90.8	0.6	10	12
12055	9825	10600	TILL	B	GREY	HILLSIDE N		0.6	18.8	111.5	0.8	10	1
12054	9875	10600	TILL	B	BROWN	HILLSIDE N		0.5	12.5	149.2	0.5	10	3
12053	9925	10600	TILL	B	BROWN	HILLSIDE N		0.4	17.3	93.6	0.5	10	1
12052	9975	10600	TILL	B	BROWN	HILLSIDE SW		0.4	21.1	79.1	0.5	10	51

UNITED GUNN RESOURCES LTD.
COPPER ACE SOUTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
12051	10000	10600	TILL	B	BROWN	HILLSIDE SW		0.6	19.3	83	0.8	10	3
12340	10025	10600	TILL	B	BROWN	FLAT		0.5	26.3	68.9	0.6	11	1
12339	10075	10600	TILL	B	BROWN	FLAT		0.6	16.4	74.5	0.6	10	1
12338	10125	10600	TILL	B	BROWN	FLAT		0.8	16.2	74.1	0.9	16	1
12337	10175	10600	TILL	B	BROWN	FLAT		0.5	12.8	85.3	0.7	10	1
12336	10225	10600	TILL	B	BROWN	HILLSIDE E		0.5	9.7	74.4	0.7	12	2
12335	10275	10600	TILL	B	BROWN	FLAT		0.5	8.1	102.9	0.6	16	1
12334	10325	10600	TILL	B	BROWN	HILLSIDE E		0.7	14.4	86.5	1.1	10	1
12333	10375	10600	TILL	B	BROWN	HILLSIDE E		0.8	11.1	64.4	0.9	10	2
12332	10425	10600	TILL	B	BROWN	FLAT		1.4	29.9	153.8	1.5	10	2
12331	10475	10600	TILL	B	BROWN	FLAT	SAMPLE TAKEN AT 104+70E - WEST EDGE OF SWAMP.	1	36	89.5	1.9	10	1
12330	10525	10600	TILL	B	BROWN	FLAT	SAMPLE TAKEN AT 106+20N/105+35E DUE TO SWAMP/CREEK.	0.6	10.6	73.6	1.1	10	1
12329	10575	10600	TILL	B	BROWN	FLAT	SAMPLE TAKEN AT 106+15N DUE TO CREEK/SWAMP.	0.7	12	53.4	1	10	1
12328	10625	10600	TILL	B	BROWN	FLAT	SAMPLE TAKEN AT 105+85N DUE TO CREEK.	0.5	13.5	68	1	20	1
12327	10675	10600	TILL	B	BROWN	HILLSIDE N	SUBCROP.	0.6	13.8	316.2	0.5	14	1
12326	10725	10600	ORGANIC	TOPSOIL	BLACK	FLAT	EAST SIDE OF CREEK. SWAMPY.	1.3	517.1	100.3	2.3	45	3
12325	10775	10600	TILL	B	BROWN	HILLSIDE W		0.4	6.5	70.6	0.5	10	1
12324	10825	10600	TILL	B	BROWN	FLAT		0.3	16.1	70.6	0.6	10	1
12323	10875	10600	TILL	B	BROWN	HILLSIDE W		0.5	62.4	50.5	3.2	23	1
12322	10925	10600	TILL	B	BROWN	HILLSIDE SW		0.5	85.4	158.3	1.2	25	1
12321	10975	10600	TILL	B	BROWN	FLAT		0.5	83	69.8	0.8	24	1
12320	11025	10600	ORGANIC	TOPSOIL	BLACK	FLAT	SWAMPY.	1.3	210.1	110	3.1	81	4
12319	11075	10600	TILL	B	BROWN	HILLSIDE SW		0.7	54.2	70.3	1.1	18	1
12318	11125	10600	TILL	B	BROWN	HILLSIDE SW		0.5	9.7	73	0.5	10	1
12317	11175	10600	TILL	B	BROWN	HILLSIDE SW		0.4	36.5	71.7	0.5	29	1
12316	11225	10600	TILL	B	BROWN	HILLSIDE W		0.9	62.3	75.6	0.6	25	1
12315	11275	10600	TILL	B	BROWN	HILLSIDE W		0.4	32.4	48.6	0.5	10	1
12314	11325	10600	TILL	B	BROWN	HILLSIDE W		0.7	44.4	85.5	0.6	19	1
12313	11375	10600	TILL	B	BROWN	HILLSIDE W		0.7	76.1	103.1	0.5	23	1
12312	11425	10600	TILL	B	BROWN	HILLSIDE W		0.5	36.1	66.2	0.5	11	5
12311	11475	10600	TILL	B	BROWN	HILLSIDE W		0.3	27.3	39.5	0.6	10	2
12310	11525	10600	TILL	B	BROWN	HILLSIDE W		0.7	43	43.8	1.3	16	3
12309	11575	10600	TILL	B	BROWN	HILLSIDE W		0.3	38.9	56.4	0.5	20	3
12308	11625	10600	TILL	B	BROWN	HILLSIDE W		0.6	32.1	51	0.5	14	1
12307	11675	10600	TILL	B	BROWN	FLAT		0.6	20.4	67.3	0.5	14	1
12306	11725	10600	TILL	B	BROWN	HILLSIDE W		0.3	31	45.3	0.5	10	2
12305	11775	10600	TILL	B	BROWN	HILLSIDE W		0.5	42.9	55.4	0.5	16	2
12304	11825	10600	TILL	B	BROWN	HILLSIDE W		0.5	34.8	56.2	0.5	13	3
12303	11875	10600	TILL	B	BROWN	HILLSIDE W		0.6	28.6	71.7	0.5	19	2
12302	11925	10600	TILL	B	BROWN	HILLSIDE W		0.3	55	54.6	0.5	31	2
12301	11975	10600	TILL	B	BROWN	FLAT		0.9	29.3	50.7	1	17	3
12000	12025	10600	TILL	B	BROWN	HILLSIDE W		0.3	13.2	66.8	0.6	16	8
11999	12075	10600	TILL	B	BROWN	FLAT		0.3	32.9	55.9	0.8	10	2
11998	12125	10600	TILL	B	BROWN	FLAT		0.6	18.2	70	0.9	13	3
11997	12175	10600	TILL	B	BROWN	HILLSIDE W		0.8	27.1	190.1	1.5	20	1
11996	12225	10600	TILL	B	BROWN	FLAT		0.9	19.5	92.5	1.4	32	1

Crest Geological Consultants Ltd.
Project 178

UNITED GUNN RESOURCES LTD.
COPPER ACE SOUTH GRID - 1998 SOIL SAMPLE DESCRIPTIONS

SAMPLE NO.	GRID EAST	GRID NORTH	MATERIAL	HORIZON	COLOUR	TOPOGRAPHY	NOTES	Mo	Cu	Zn	As	Hg	Au
11995	12275	10600	TILL	B	BROWN	FLAT		0.6	26.8	54	0.6	10	1
11994	12325	10600	TILL	B	BROWN	HILLSIDE W		0.9	27.3	74.6	1.7	28	1
11993	12375	10600	TILL	B	BROWN	FLAT		0.9	38.6	60	3.1	17	1

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
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GEOCHEMICAL EXTRACTION-ANALYSIS CERTIFICATE

Crest Geological Consulting PROJECT 178 File # 9804545

2197 Park Crescent, Coquitlam BC V3J 6T1 Submitted by: R. Roe

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
10537	.6	24.9	2.4	102.9	120	8	6	391	1.27	.7	<5	<2	25	.07	.2	.3	22	.35	.018	3	10	.59	65	.04	<3	1.02	.01	.04	<2	<.2	10	.3	<.2	2.7	<1
10538	.7	22.7	2.1	280.1	123	10	7	485	1.37	<.5	6	<2	21	.22	<.2	.2	21	.28	.044	3	10	.66	133	.07	<3	1.11	.01	.08	<2	<.2	13	<.3	<.2	3.0	2
10539	.6	15.6	2.2	116.9	89	8	4	253	1.13	.5	<5	<2	15	.13	.2	.2	22	.22	.028	4	12	.39	70	.05	<3	.84	.01	.04	<2	<.2	16	<.3	<.2	2.5	<1
10540	.5	17.4	2.3	122.3	64	9	6	268	1.50	<.5	<5	<2	18	.09	<.2	.3	24	.24	.034	4	10	.65	77	.05	<3	1.16	.01	.04	<2	.2	<10	<.3	<.2	3.7	<1
10541	.9	24.6	2.5	152.9	42	10	4	393	1.21	.6	<5	<2	15	.15	<.2	.2	24	.20	.045	5	13	.38	134	.05	<3	1.01	.01	.04	<2	<.2	14	<.3	<.2	2.9	<1
10542	.8	23.8	2.4	106.6	<30	7	4	382	1.19	.6	<5	<2	16	.11	<.2	.2	23	.23	.023	4	11	.46	81	.05	<3	.93	.01	.03	<2	<.2	12	<.3	<.2	2.7	25
10543	.6	26.6	2.5	119.1	51	10	4	248	1.10	.5	6	<2	16	.07	<.2	.3	23	.22	.014	5	12	.41	75	.06	<3	.92	.02	.05	<2	<.2	13	<.3	<.2	2.4	<1
10544	1.0	17.2	2.8	294.2	78	10	6	514	1.26	<.5	<5	<2	13	.19	<.2	.2	21	.20	.070	5	12	.43	126	.04	<3	1.15	.01	.06	<2	.2	23	<.3	<.2	3.5	<1
10545	1.2	37.5	2.9	448.0	73	16	11	685	2.17	.8	<5	<2	22	.34	<.2	.3	34	.32	.104	5	19	.62	126	.06	<3	1.81	.01	.07	<2	<.2	20	<.3	<.2	5.1	1
10561	1.1	66.8	2.9	79.7	157	12	4	200	1.17	1.3	<5	<2	25	.13	.3	.4	25	.42	.018	7	17	.30	80	.05	<3	.88	.02	.04	<2	<.2	10	<.3	<.2	2.6	2
10562	1.0	39.5	2.9	74.9	74	10	5	224	1.35	1.6	7	<2	23	.10	.2	.3	29	.33	.059	4	16	.39	63	.05	<3	.92	.02	.05	<2	<.2	23	<.3	<.2	2.8	<1
10563	1.9	177.6	5.1	173.9	321	31	10	1117	2.20	2.8	<5	<2	36	.54	.3	1.0	36	.72	.026	10	27	.42	143	.06	<3	1.58	.02	.08	<2	<.2	25	.4	<.2	4.4	1
10564	1.4	91.8	3.1	82.5	33	19	8	535	1.59	1.9	<5	<2	28	.20	.2	.6	34	.42	.021	7	22	.39	86	.07	<3	1.08	.01	.05	<2	<.2	18	.3	<.2	3.4	<1
10565	.5	45.9	3.6	56.8	87	12	3	208	.99	.6	<5	<2	25	.10	<.2	.4	21	.36	.016	8	30	.40	67	.08	<3	.93	.02	.05	<2	<.2	19	.6	<.2	3.1	<1
10566	.8	57.5	3.2	74.6	60	14	6	365	1.22	.9	<5	2	22	.08	<.2	.4	28	.30	.016	7	20	.35	87	.07	<3	1.00	.02	.05	<2	.2	18	.3	<.2	3.3	<1
10567	.8	44.0	3.0	70.5	116	12	5	278	1.18	.9	<5	<2	25	.09	.2	.4	28	.31	.015	5	17	.39	71	.07	<3	1.03	.02	.05	<2	<.2	<10	<.3	<.2	3.6	3
RE 10538	.9	22.7	2.1	277.7	171	10	7	497	1.34	<.5	<5	<2	21	.23	<.2	.2	21	.28	.043	3	10	.64	137	.07	<3	1.10	.01	.07	<2	<.2	<10	<.3	<.2	3.1	17
10568	.6	43.0	2.6	66.4	33	13	5	370	1.15	.8	<5	2	23	.08	<.2	.3	27	.30	.020	6	18	.37	79	.06	<3	.98	.02	.04	<2	<.2	28	<.3	<.2	3.3	<1
10569	1.6	84.0	3.6	69.6	265	18	8	342	2.06	2.3	5	<2	37	.23	.3	.5	38	.85	.022	6	27	.41	108	.07	<3	1.49	.02	.09	<2	<.2	27	.5	<.2	4.1	1
10570	1.1	22.7	2.8	52.9	46	10	5	257	1.37	1.5	<5	<2	22	.11	.2	.2	32	.35	.022	6	18	.35	53	.08	<3	.88	.02	.05	<2	<.2	12	.3	<.2	2.9	<1
10571	2.2	131.5	3.4	85.2	203	24	8	545	2.13	3.6	<5	<2	29	.20	.5	.7	39	.60	.036	7	28	.56	109	.06	<3	1.45	.02	.10	<2	<.2	30	.4	<.2	4.2	1
10572	1.1	39.4	2.3	62.7	48	10	4	246	1.24	1.2	<5	<2	20	.06	.2	.2	28	.26	.021	4	15	.37	66	.06	<3	.87	.01	.05	<2	<.2	20	<.3	<.2	2.4	<1
10573	.8	15.0	2.3	50.0	<30	7	4	195	1.06	.6	<5	<2	19	.06	<.2	<.2	26	.23	.013	4	12	.30	59	.07	<3	.78	.01	.03	<2	<.2	13	<.3	<.2	2.7	<1
10574	.7	16.3	2.5	76.6	66	7	3	300	.86	.5	<5	<2	17	.09	<.2	.2	21	.23	.027	4	10	.24	84	.05	<3	.72	.01	.03	<2	<.2	28	<.3	<.2	2.4	<1
10575	1.7	58.2	2.4	96.7	141	10	4	464	1.02	.7	<5	<2	21	.17	<.2	.4	22	.29	.034	5	14	.29	102	.05	<3	.79	.01	.05	<2	<.2	16	<.3	<.2	2.9	1
10576	1.0	15.5	2.4	56.2	70	6	3	241	.96	.5	<5	<2	19	.14	<.2	.2	22	.29	.020	3	11	.26	63	.06	<3	.67	.02	.05	<2	<.2	25	<.3	<.2	2.6	<1
10577	1.4	42.5	3.0	78.0	68	11	5	304	1.52	1.0	<5	<2	22	.13	.2	.3	31	.38	.013	5	19	.40	79	.07	<3	1.07	.01	.08	<2	<.2	17	<.3	<.2	3.3	<1
10578	1.5	49.4	2.7	73.6	203	9	4	313	1.13	1.1	<5	<2	21	.15	.2	.4	26	.36	.024	4	14	.30	62	.06	<3	.78	.02	.06	<2	<.2	18	<.3	<.2	2.8	<1
10579	.6	36.2	2.3	112.5	54	12	4	268	1.31	.9	<5	<2	20	.12	<.2	.2	27	.35	.024	5	18	.31	70	.07	<3	.92	.01	.05	<2	<.2	19	<.3	<.2	2.5	<1
10580	.8	29.9	2.5	93.3	70	11	4	243	1.17	.8	<5	<2	17	.13	<.2	.2	25	.24	.029	5	15	.34	62	.06	<3	.78	.01	.06	<2	<.2	<10	<.3	<.2	2.8	<1
10581	2.0	66.1	3.1	60.9	140	14	5	243	1.60	1.9	<5	<2	25	.12	.3	.4	36	.39	.038	6	22	.44	72	.08	<3	.93	.01	.08	<2	<.2	17	<.3	<.2	3.2	<1
10582	1.2	24.2	3.0	70.2	181	12	6	478	1.33	1.0	<5	<2	23	.19	.2	.2	29	.36	.040	5	17	.33	100	.06	<3	.90	.01	.09	<2	<.2	13	<.3	<.2	3.1	<1
10583	.9	39.2	2.9	73.9	159	14	7	485	1.59	1.7	<5	2	25	.11	.3	.3	35	.39	.021	5	21	.45	94	.07	<3	1.07	.02	.07	<2	<.2	<10	<.3	<.2	3.2	<1
10584	1.0	14.3	2.6	47.1	<30	8	5	257	1.29	1.1	<5	<2	17	.09	<.2	<.2	33	.27	.009	4	19	.28	57	.07	<3	.80	.02	.04	<2	<.2	10	<.3	<.2	2.4	<1
STANDARD	23.6	119.0	90.5	240.5	1837	30	15	1023	4.14	66.3	15	21	56	2.17	8.6	19.9	69	.69	.107	18	51	1.07	255	.12	29	2.24	.04	.65	15	1.9	1073	.6	1.9	6.3	50

Standard is STANDARD D2/C3/AU-S.
ICP - 15 GRAM SAMPLE IS DIGESTED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 300 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K GA AND AL. SOLUTION ANALYSED DIRECTLY BY ICP. MO CU PB ZN AG AS AU CD SB BI TL HG SE TE AND GA ARE EXTRACTED WITH MIBK-ALIQUAT 336 AND ANALYSED BY ICP. ELEVATED DETECTION LIMITS FOR SAMPLES CONTAIN CU,PB,ZN,AS>1500 PPM,Fe>20%.
- SAMPLE TYPE: SOIL AU+ - AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 14 1998 DATE REPORT MAILED: Oct 19/98 SIGNED BY......D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data___ FA ___

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(640)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL EXTRACTION-ANALYSIS CERTIFICATE

Crest Geological Consulting PROJECT 178 File # 9801731 Page 1
2197 Park Crescent, Coquitlam BC V3J 6T1 Submitted by: R. Roe

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
11479	1.3	44.5	2.7	274.2	64	11	5	302	1.23	.6	<5	<2	16	.23	.2	<.2	29	.19	.029	5	17	.31	114	.05	<3	1.04	.01	.03	<2	<.2	<10	<.3	<.2	3.3	<1
11480	.7	50.8	2.3	452.0	<30	9	4	199	1.07	<.5	<5	<2	18	.32	<.2	<.2	29	.22	.016	5	16	.28	58	.05	<3	.85	.01	.03	<2	<.2	<10	<.3	<.2	2.8	6
11481	2.4	227.8	4.5	111.7	80	27	11	674	2.44	3.7	5	<2	38	.22	.7	<.2	40	.80	.076	8	32	.63	108	.05	<3	1.32	.01	.07	<2	<.2	35	<.3	<.2	3.5	1
11482	2.8	240.5	4.1	113.5	135	14	6	441	1.30	1.5	6	<2	25	.17	.3	<.2	29	.42	.026	6	18	.38	78	.05	<3	.95	.01	.07	<2	<.2	17	<.3	<.2	3.2	9
11483	.8	49.2	2.7	91.0	79	13	5	305	1.16	.7	<5	<2	21	.07	<.2	<.2	27	.24	.021	6	17	.39	70	.05	<3	.97	.01	.04	<2	<.2	<10	<.3	<.2	2.8	5
11484	.5	31.4	2.3	71.6	<30	10	4	227	.98	<.5	<5	<2	18	.04	<.2	<.2	22	.22	.013	5	16	.36	58	.06	<3	.83	.01	.03	<2	<.2	22	<.3	<.2	2.3	<1
11485	.7	43.9	2.2	95.4	55	13	6	301	1.21	.5	6	<2	20	.06	.2	<.2	27	.23	.016	6	16	.40	77	.06	<3	.98	.01	.04	<2	<.2	14	<.3	<.2	2.6	1
11486	.7	50.4	2.3	103.9	139	14	6	330	1.31	.6	<5	<2	21	.07	.3	<.2	27	.25	.024	6	20	.45	69	.05	<3	1.04	.01	.05	<2	<.2	11	<.3	<.2	3.2	<1
11487	.6	40.8	2.9	134.4	155	15	6	300	1.22	1.2	<5	<2	18	.10	.2	<.2	26	.22	.020	7	23	.39	68	.06	<3	1.02	.01	.05	<2	<.2	15	<.3	<.2	3.0	<1
11488	1.8	213.1	3.8	319.8	358	36	12	937	2.16	2.2	<5	2	39	.62	.3	<.2	37	.59	.057	15	36	.60	143	.07	<3	1.82	.02	.12	<2	<.2	39	.3	<.2	4.9	3
11489	.6	212.1	1.7	154.9	272	12	3	229	.31	1.5	<5	<2	380	.87	.3	<.2	6	25.89	.164	1	5	.38	125	<.01	10	.33	.02	.02	<2	<.2	25	.4	<.2	1.0	2
11490	1.6	181.6	3.9	113.1	445	22	9	942	2.11	2.2	<5	<2	43	.35	.3	<.2	27	1.23	.050	7	21	.47	131	.03	<3	1.41	.01	.10	<2	<.2	31	.3	<.2	4.0	<1
11491	3.1	191.3	3.4	120.1	307	25	11	976	2.33	3.0	<5	<2	39	.33	.3	<.2	37	.88	.030	8	23	.52	112	.04	<3	1.48	.01	.10	<2	<.2	21	<.3	<.2	4.6	1
11492	2.4	34.8	2.8	77.7	175	10	7	531	1.48	1.4	<5	<2	24	.13	.2	<.2	32	.36	.011	5	17	.38	69	.06	<3	.98	.01	.06	<2	<.2	<10	<.3	<.2	3.3	1
11493	1.7	34.2	3.0	108.9	162	11	6	580	1.34	.9	7	<2	23	.16	.2	<.2	29	.35	.011	5	17	.31	74	.06	<3	.96	.01	.06	<2	<.2	<10	<.3	<.2	3.1	1
11494	1.6	71.6	2.4	94.1	211	15	7	413	1.46	1.1	<5	<2	24	.11	.2	<.2	29	.29	.023	6	22	.45	63	.06	<3	1.02	.01	.06	<2	<.2	20	<.3	<.2	3.2	4
RE 11494	1.3	68.4	2.3	91.4	215	15	6	402	1.40	1.3	<5	<2	21	.10	.2	<.2	28	.26	.024	6	20	.44	60	.05	<3	.97	.01	.06	<2	<.2	17	<.3	<.2	2.9	1
11495	3.8	181.2	2.6	97.3	194	18	6	429	1.64	1.3	<5	<2	27	.11	.2	<.2	27	.35	.045	7	20	.53	84	.05	<3	1.23	.01	.08	<2	<.2	22	<.3	<.2	3.5	1
11496	1.0	56.3	2.7	86.8	130	15	5	287	1.26	.7	<5	<2	21	.08	.2	<.2	27	.27	.016	6	20	.38	61	.07	<3	.96	.01	.06	<2	<.2	21	<.3	<.2	3.4	2
11497	.3	39.9	2.3	71.8	66	11	4	196	1.01	.5	<5	<2	18	.05	<.2	<.2	22	.23	.011	5	15	.34	48	.07	<3	.81	.01	.04	<2	<.2	<10	<.3	<.2	2.0	1
11498	1.1	45.1	2.6	126.9	153	12	6	329	1.35	1.0	<5	<2	20	.15	.2	<.2	30	.26	.041	6	17	.37	81	.06	<3	.99	.01	.05	<2	<.2	12	<.3	<.2	3.5	1
11499	.6	32.6	2.2	136.3	41	9	4	251	1.04	.5	5	<2	16	.08	<.2	<.2	21	.22	.026	5	11	.41	48	.05	<3	.87	.01	.03	<2	<.2	<10	<.3	<.2	2.9	<1
11500	.8	32.3	2.6	107.7	159	7	4	245	.96	<.5	<5	<2	17	.05	<.2	<.2	22	.21	.018	4	13	.37	59	.04	<3	.94	.01	.03	<2	<.2	16	<.3	<.2	3.3	1
11724	.8	49.8	2.2	93.3	92	13	5	267	1.21	.6	<5	<2	21	.09	.2	<.2	28	.26	.019	6	17	.37	67	.06	<3	.93	.01	.04	<2	<.2	<10	<.3	<.2	2.8	2
11725	.7	14.0	3.0	202.7	120	9	4	408	.94	.6	<5	<2	19	.21	<.2	<.2	23	.25	.057	5	14	.20	121	.05	<3	.82	.01	.05	<2	<.2	16	<.3	<.2	2.9	1
11726	1.0	35.9	2.9	95.8	136	13	6	253	1.34	1.1	<5	<2	20	.18	.2	<.2	34	.27	.023	6	22	.39	68	.07	<3	.89	.01	.04	<2	<.2	21	<.3	<.2	3.0	2
11727	.7	37.9	2.6	109.0	173	12	5	403	1.02	.7	<5	<2	19	.13	<.2	<.2	24	.25	.016	6	20	.31	64	.05	3	.88	.01	.04	<2	<.2	19	<.3	<.2	2.8	2
11728	1.0	23.8	2.5	58.0	83	7	4	163	1.13	1.1	<5	<2	18	.13	.2	<.2	29	.23	.027	5	15	.28	57	.06	<3	.71	.01	.04	<2	<.2	<10	<.3	<.2	2.8	25
11729	1.1	59.0	2.6	100.6	151	17	7	661	1.40	1.3	<5	<2	24	.10	.2	<.2	31	.29	.033	7	23	.42	86	.05	<3	1.15	.01	.05	<2	<.2	21	<.3	<.2	3.5	3
11730	.3	25.2	2.4	62.8	56	8	4	198	.85	.5	<5	<2	16	.05	<.2	<.2	20	.21	.017	5	12	.34	40	.05	<3	.76	.01	.03	<2	<.2	12	<.3	<.2	2.4	2
11731	1.6	41.8	2.4	92.0	71	11	4	280	.92	<.5	<5	<2	19	.07	<.2	<.2	21	.23	.019	5	16	.31	62	.04	<3	.87	.01	.04	<2	<.2	12	<.3	<.2	2.8	3
11732	1.0	54.6	2.3	60.5	35	10	5	259	1.11	.9	<5	<2	18	.05	<.2	<.2	24	.26	.031	5	14	.41	39	.06	<3	.84	.01	.05	<2	<.2	<10	<.3	<.2	2.5	2
11733	5.5	213.3	3.0	92.1	206	15	6	606	1.33	.9	<5	<2	24	.11	.2	<.2	25	.34	.030	6	20	.43	95	.04	<3	1.09	.01	.05	<2	<.2	22	<.3	<.2	3.6	5
11734	2.6	82.1	2.1	72.0	65	10	5	362	1.12	.8	<5	<2	23	.08	.2	<.2	23	.29	.021	6	12	.40	51	.06	<3	.83	.01	.03	<2	<.2	<10	<.3	<.2	2.8	2
STANDARD	25.0	123.6	94.8	276.5	1949	32	18	1031	4.83	79.7	18	20	60	1.98	9.3	20.1	73	.68	.112	17	59	1.16	276	.11	25	2.35	.05	.71	18	2.4	928	.6	2.1	7.6	52

Standard is STANDARD D2/C3/AU-S.
ICP - 15 GRAM SAMPLE IS DIGESTED WITH 90 ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 300 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K GA AND AL. SOLUTION ANALYSED DIRECTLY BY ICP. MO CU PB ZN AG AS AU CD SB BI TL HG SE TE AND GA ARE EXTRACTED WITH MIBK-ALIQUAT 336 AND ANALYSED BY ICP. ELEVATED DETECTION LIMITS FOR SAMPLES CONTAIN CU,PB,ZN,AS>1500 PPM,Fe>20%.
- SAMPLE TYPE: SOIL AU* - AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: MAY 19 1998 DATE REPORT MAILED: May 22/98 SIGNED BY. .... D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

 Data___ FA ____

ACME ANALYTICAL

Crest Geological Consulting PROJECT 178 FILE # 9801731

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
11735	8.3	466.6	3.6	100.1	162	17	9	706	1.61	3.4	<5	2	25	.20	.3	.7	31	.40	.062	6	21	.48	86	.04	<3	.99	.01	.06	<2	.2	35	<.3	.2	3.1	1
11736	5.1	232.4	3.0	93.7	144	18	7	583	1.63	3.5	<5	2	25	.15	.3	<.2	31	.41	.050	8	21	.48	91	.04	<3	1.10	.01	.06	<2	<.2	32	<.3	<.2	3.1	1
11737	5.1	176.8	3.0	153.5	204	21	8	740	1.58	1.8	<5	2	26	.32	.2	<.2	30	.42	.035	8	21	.44	118	.04	<3	1.15	.01	.06	<2	<.2	29	<.3	<.2	3.4	1
11738	1.9	100.6	2.7	82.7	123	14	7	424	1.57	2.3	<5	2	21	.09	.3	<.2	33	.31	.045	6	19	.53	50	.05	<3	1.00	.01	.05	<2	.2	20	<.3	<.2	3.1	2
11739	1.9	102.0	2.4	76.5	123	12	6	298	1.32	1.3	<5	<2	17	.06	.2	<.2	29	.24	.030	5	15	.45	42	.05	<3	.92	.01	.05	<2	<.2	31	<.3	<.2	2.7	1
11740	2.1	144.3	3.6	155.9	373	27	9	867	1.89	2.6	<5	2	25	.20	.3	<.2	36	.38	.044	8	28	.47	126	.04	<3	1.37	.01	.10	<2	<.2	37	<.3	<.2	3.8	1
11741	1.4	82.9	2.5	100.9	152	13	5	350	1.12	.8	<5	2	16	.12	.2	<.2	24	.23	.021	5	17	.35	61	.05	<3	.84	.01	.06	<2	<.2	23	<.3	<.2	2.3	<1
11742	2.1	60.2	2.8	96.2	115	10	6	497	1.25	.5	<5	<2	21	.18	.2	<.2	27	.29	.030	4	14	.35	80	.05	<3	.84	.01	.06	<2	<.2	17	<.3	<.2	2.7	2
11743	1.5	51.9	2.9	66.1	112	11	7	640	1.38	1.3	<5	<2	20	.08	<.2	<.2	31	.31	.034	5	19	.35	94	.05	<3	.89	.01	.06	<2	<.2	19	<.3	<.2	2.6	2
11744	1.9	102.2	2.9	64.1	158	11	6	394	1.41	2.0	<5	<2	25	.08	.2	<.2	33	.40	.024	5	20	.38	68	.05	<3	.95	.01	.06	<2	<.2	20	<.3	<.2	2.6	<1
11745	1.7	81.8	2.1	78.9	89	12	7	285	1.52	2.5	<5	2	20	.08	.3	<.2	34	.28	.035	5	17	.47	49	.05	<3	.95	.01	.08	<2	<.2	80	<.3	<.2	2.6	1
11746	3.2	99.5	2.7	90.7	164	8	5	533	1.18	.8	<5	<2	18	.12	.2	<.2	28	.26	.033	4	16	.32	88	.04	<3	.82	.01	.03	<2	<.2	37	<.3	<.2	2.8	1
11747	1.9	70.0	3.0	135.4	119	12	6	616	1.08	.8	<5	<2	18	.14	<.2	<.2	25	.23	.022	5	13	.35	95	.04	<3	1.04	.01	.04	<2	<.2	25	<.3	<.2	3.2	2
11748	1.2	47.4	3.0	121.8	54	11	5	232	1.01	<.5	<5	2	14	.04	<.2	<.2	23	.20	.020	5	10	.39	57	.05	<3	.97	.01	.03	<2	<.2	22	<.3	<.2	2.7	1
11749	1.1	35.4	3.0	111.6	60	9	5	282	1.11	.5	<5	<2	15	.09	<.2	<.2	26	.20	.022	5	14	.37	62	.06	<3	.92	.01	.04	<2	<.2	10	<.3	<.2	2.7	<1
11750	.8	49.8	3.2	83.8	171	11	5	248	1.18	.7	<5	<2	21	.07	<.2	<.2	30	.23	.012	7	16	.35	81	.04	<3	1.08	.01	.05	<2	<.2	<10	<.3	<.2	3.1	<1
11751	2.2	82.9	3.8	125.0	177	12	6	277	1.39	1.4	<5	2	21	.10	.2	<.2	33	.28	.022	7	22	.41	80	.05	<3	1.07	.01	.05	<2	<.2	<10	<.3	<.2	3.2	2
RE 11751	2.2	79.9	3.3	118.3	143	11	6	262	1.30	.5	<5	2	20	.08	.2	<.2	30	.26	.021	6	16	.39	75	.05	<3	1.01	.01	.04	<2	<.2	<10	<.3	<.2	2.8	3
11752	1.3	42.1	2.4	52.4	113	7	4	187	.93	<.5	<5	<2	14	.20	.2	<.2	26	.21	.018	3	13	.23	50	.04	<3	.58	.01	.04	<2	<.2	<10	<.3	<.2	1.9	1
11753	.8	23.6	2.5	73.5	45	8	4	192	.90	<.5	6	<2	18	.12	<.2	<.2	23	.24	.017	4	12	.27	42	.05	<3	.71	.01	.04	<2	<.2	15	<.3	<.2	2.4	16
11754	.8	77.5	3.0	87.9	139	18	7	455	1.37	1.1	<5	<2	22	.09	.2	<.2	33	.31	.023	6	23	.35	79	.04	<3	1.14	.01	.06	<2	<.2	16	<.3	<.2	3.1	1
11755	1.2	28.4	2.9	120.2	72	9	6	395	1.14	.9	<5	<2	23	.25	<.2	<.2	27	.33	.067	4	18	.26	95	.04	<3	.82	.01	.05	<2	<.2	12	<.3	<.2	2.6	1
11756	1.5	37.1	3.9	317.5	244	12	9	1284	1.51	1.5	<5	<2	33	.67	<.2	<.2	28	.53	.154	5	20	.25	281	.04	<3	1.06	.01	.10	<2	<.2	<10	<.3	<.2	3.3	<1
11757	2.6	669.4	3.1	137.0	690	51	8	641	1.92	1.9	<5	<2	101	.83	.5	<.2	29	2.34	.097	13	32	.43	191	.02	5	1.51	.01	.12	<2	<.2	85	.9	.3	4.4	1
11758	1.7	312.3	3.5	80.6	284	32	10	597	2.36	4.9	<5	2	48	.23	.3	<.2	44	.99	.046	10	40	.49	126	.04	<3	1.74	.01	.10	<2	<.2	40	.4	<.2	3.6	2
11759	1.9	247.5	4.4	114.4	319	34	11	1067	2.37	4.6	<5	3	43	.39	.3	<.2	42	.73	.060	12	38	.55	128	.05	3	1.70	.01	.14	<2	<.2	59	.4	<.2	4.1	3
11760	.7	12.0	3.0	88.4	102	6	4	246	.80	.8	<5	<2	18	.15	.2	<.2	23	.25	.024	4	13	.23	47	.05	<3	.72	.01	.03	<2	<.2	<10	<.3	<.2	2.7	2
11761	2.1	304.5	5.4	211.8	635	61	18	1324	4.33	6.6	<5	4	62	.34	.6	.3	62	.94	.048	18	66	.87	312	.05	<3	3.62	.02	.19	<2	<.2	55	.6	.2	8.9	1
11762	.6	38.6	2.7	91.4	126	13	7	396	1.16	1.4	<5	<2	24	.06	.2	<.2	30	.30	.022	6	19	.36	68	.05	<3	1.05	.01	.05	<2	<.2	16	<.3	<.2	2.8	1
11763	.9	41.2	2.6	52.9	67	12	7	400	1.18	1.1	<5	2	20	.05	.2	<.2	30	.28	.020	6	18	.40	49	.06	<3	.86	.01	.04	<2	<.2	17	<.3	<.2	2.3	1
11764	.8	30.5	2.5	75.7	123	12	5	228	1.23	1.2	<5	2	18	.08	.2	<.2	33	.26	.017	6	19	.31	54	.06	<3	.86	.01	.05	<2	<.2	14	<.3	<.2	2.2	1
11765	1.8	70.6	3.1	84.8	213	13	6	517	1.36	1.4	<5	2	21	.18	.3	<.2	33	.32	.031	6	21	.38	69	.05	<3	.92	.01	.05	<2	<.2	22	<.3	<.2	2.6	2
11766	.9	21.6	2.3	75.1	106	9	5	389	1.03	1.1	<5	<2	19	.12	.2	<.2	27	.30	.028	4	15	.26	66	.05	<3	.71	.01	.05	<2	<.2	16	<.3	<.2	1.8	1
11767	1.1	56.6	3.2	70.3	210	14	7	566	1.44	2.6	6	<2	24	.15	.3	<.2	38	.42	.023	6	21	.32	75	.05	<3	.95	.01	.06	<2	<.2	34	<.3	<.2	2.5	<1
STANDARD	23.8	118.0	98.5	258.9	1987	31	17	1000	4.70	74.5	25	20	58	1.98	8.5	18.0	76	.64	.107	17	52	1.09	269	.11	25	2.33	.06	.69	15	2.5	898	.6	2.1	7.0	51

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA ____

Crest Geological Consulting PROJECT 178 FILE # 9801731

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
11768	1.2	26.8	2.3	50.6	57	10	5	278	1.23	.8	<5	<2	17	.06	.3	<.2	29	.26	.014	4	15	.34	53	.05	<3	.80	.01	.05	<2	.2	20	<.3	<.2	2.7	1
11769	1.5	59.2	2.6	72.1	135	10	6	259	1.30	.9	<5	2	20	.13	.3	<.2	30	.36	.031	5	20	.33	58	.05	<3	.89	.01	.06	<2	.2	20	<.3	<.2	2.8	1
11770	1.5	62.3	2.9	76.9	280	11	6	462	1.17	1.0	<5	2	26	.26	.3	<.2	28	.54	.033	5	18	.28	75	.05	3	.86	.01	.05	<2	<.2	25	<.3	<.2	2.7	<1
11771	3.5	607.0	6.8	345.2	1326	87	18	1063	4.96	4.1	<5	2	74	.72	1.0	<.2	61	1.52	.066	25	80	.89	363	.05	<3	4.05	.02	.26	<2	.2	95	.7	.2	9.3	2
11772	3.2	123.7	3.1	115.9	193	15	6	636	1.40	.8	<5	<2	29	.23	.3	<.2	29	.48	.040	9	18	.39	102	.05	<3	1.00	.01	.08	<2	<.2	15	<.3	<.2	3.6	1
11773	1.4	38.0	2.4	76.8	50	10	6	397	1.34	.8	<5	<2	21	.08	.2	<.2	31	.33	.027	5	18	.38	62	.06	<3	.91	.01	.06	<2	<.2	20	<.3	<.2	2.7	<1
11774	.9	18.7	2.1	99.4	73	8	5	330	1.10	.5	<5	<2	17	.11	.2	<.2	24	.26	.023	4	16	.31	56	.06	<3	.75	.01	.05	<2	.2	20	<.3	<.2	2.7	<1
11775	.9	19.1	2.8	121.5	56	8	5	481	1.10	<.5	<5	<2	19	.12	<.2	<.2	25	.30	.026	5	17	.29	80	.05	<3	.86	.01	.07	<2	<.2	15	<.3	<.2	2.7	1
11776	1.2	52.3	2.4	71.4	124	12	6	481	1.25	.9	10	<2	22	.09	.2	<.2	30	.39	.026	5	24	.29	49	.05	3	.81	.01	.05	<2	<.2	15	<.3	<.2	2.4	2
11777	1.2	58.2	4.4	101.4	264	17	8	769	1.58	2.5	<5	<2	25	.18	.4	<.2	35	.41	.022	8	23	.35	105	.06	<3	1.12	.01	.06	<2	<.2	20	<.3	<.2	3.3	3
11778	.8	16.9	3.6	67.9	54	7	5	446	1.13	1.2	<5	<2	19	.07	.2	<.2	27	.27	.019	5	14	.28	71	.05	<3	.89	.01	.06	<2	.2	<10	<.3	<.2	2.7	2
11779	1.7	111.6	2.9	80.5	210	16	7	446	1.45	1.3	<5	<2	24	.11	.2	<.2	33	.43	.020	7	23	.34	72	.05	<3	1.08	.01	.05	<2	<.2	35	<.3	<.2	2.9	2
11780	.5	32.9	2.7	100.2	91	10	4	165	.94	.6	<5	<2	14	.09	<.2	<.2	20	.23	.017	5	16	.28	42	.06	<3	.76	.01	.04	<2	<.2	15	<.3	<.2	2.5	<1
11781	.9	22.2	2.6	83.2	115	8	4	294	.93	.6	<5	<2	16	.11	<.2	<.2	21	.27	.023	4	14	.26	57	.05	<3	.74	.01	.04	<2	.2	20	<.3	<.2	2.6	<1
RE 11781	.9	22.4	2.6	84.1	98	8	4	291	.94	.7	<5	<2	17	.10	<.2	<.2	21	.28	.022	4	15	.26	57	.05	<3	.75	.01	.04	<2	<.2	20	<.3	<.2	2.7	<1
11782	.7	17.2	2.7	141.3	60	9	4	218	1.11	.8	<5	<2	14	.09	<.2	<.2	24	.23	.056	5	16	.29	84	.05	<3	.99	.01	.03	<2	.2	25	<.3	<.2	3.2	1
11783	1.2	33.1	2.8	120.7	<30	8	5	262	1.23	.6	<5	<2	11	.10	.2	<.2	28	.16	.025	3	12	.36	51	.03	<3	1.08	.01	.03	<2	<.2	25	<.3	<.2	3.6	8
11784	3.8	66.8	2.4	218.1	<30	9	6	805	1.65	.7	<5	<2	14	.19	<.2	<.2	24	.25	.037	5	13	.34	112	.03	<3	1.02	.01	.05	<2	<.2	25	<.3	<.2	3.0	5
11785	2.3	39.6	3.0	240.9	<30	16	9	528	3.40	1.2	<5	<2	19	.25	.2	<.2	31	.39	.098	7	18	.38	74	.03	<3	1.48	.01	.07	<2	.2	15	<.3	<.2	4.0	<1
11786	6.9	160.9	1.6	104.5	268	23	7	5006	.86	2.5	<5	2	362	.73	.2	<.2	15	29.80	.101	2	14	.34	344	.01	9	.55	.02	.04	<2	.2	55	.7	<.2	1.7	1
11787	1.6	34.9	2.6	221.0	57	10	6	411	1.34	.8	<5	<2	19	.18	<.2	<.2	25	.56	.060	5	16	.36	102	.05	<3	1.07	.01	.05	<2	<.2	15	<.3	<.2	3.0	2
11788	1.3	28.9	2.4	127.4	63	7	5	430	1.10	.5	<5	<2	16	.13	<.2	<.2	22	.25	.031	5	13	.37	86	.05	<3	.87	.01	.07	<2	.2	15	<.3	<.2	2.6	<1
11789	.7	8.8	2.0	91.3	<30	7	5	368	1.14	.5	<5	<2	17	.06	<.2	<.2	24	.25	.016	5	17	.33	69	.07	<3	.80	.01	.07	<2	.2	<10	<.3	<.2	2.5	8
11790	.9	79.2	2.8	94.1	182	15	7	345	1.42	1.2	<5	<2	34	.13	.2	<.2	28	.72	.033	5	19	.49	72	.04	3	.98	.01	.05	<2	<.2	25	.4	<.2	2.9	<1
11791	1.3	20.5	2.3	117.4	91	8	6	449	1.29	.7	5	<2	17	.08	<.2	<.2	28	.26	.022	4	17	.37	79	.05	<3	.93	.01	.05	<2	<.2	30	<.3	<.2	2.8	2
11792	1.2	14.7	2.3	119.5	<30	9	10	458	1.88	<.5	<5	<2	24	.08	<.2	<.2	30	.41	.024	4	17	.87	73	.07	<3	1.44	.01	.18	<2	.2	<10	<.3	<.2	4.2	1
11793	1.2	25.6	2.0	114.4	64	10	7	476	1.58	1.0	<5	<2	20	.07	.2	<.2	27	.66	.021	3	19	.52	54	.04	<3	1.02	.01	.04	<2	<.2	15	<.3	<.2	3.0	4
11794	3.2	53.2	3.2	183.0	387	9	8	1655	1.36	1.0	<5	<2	38	.36	<.2	<.2	27	.77	.030	4	16	.33	115	.03	<3	.95	.01	.07	<2	<.2	30	<.3	<.2	3.2	<1
11795	1.2	19.7	2.2	339.0	162	7	6	754	1.23	.6	<5	<2	19	.30	<.2	<.2	21	.32	.052	4	12	.38	88	.04	3	.90	.01	.05	<2	.2	10	<.3	<.2	3.1	<1
11796	1.5	35.3	4.0	564.3	133	21	11	1359	2.41	2.2	6	<2	15	.51	.2	<.2	43	.24	.113	5	31	.37	176	.06	<3	1.54	.01	.05	<2	.2	30	<.3	<.2	4.9	41
11797	1.3	45.2	3.6	519.7	272	25	8	550	2.23	2.2	<5	<2	15	.38	<.2	<.2	39	.27	.106	5	32	.37	261	.05	<3	1.67	.01	.05	<2	.2	40	<.3	<.2	4.9	4
11798	1.9	42.1	4.0	483.0	161	18	9	1045	1.85	1.4	<5	<2	20	.44	.2	<.2	35	.35	.069	5	26	.37	216	.05	3	1.29	.01	.06	<2	.2	40	<.3	<.2	4.2	2
11799	.7	10.1	3.4	281.6	84	7	5	577	1.04	.5	<5	<2	11	.19	<.2	<.2	23	.20	.033	5	15	.23	87	.05	3	.84	.01	.04	<2	.2	25	<.3	<.2	3.3	<1
11800	1.1	11.8	3.3	305.9	65	10	6	881	1.44	1.2	<5	<2	19	.58	<.2	<.2	33	.33	.051	4	23	.31	107	.05	<3	.97	.01	.05	<2	<.2	25	<.3	<.2	4.0	2
STANDARD	24.7	120.5	93.9	263.3	1960	31	18	1004	4.71	75.2	21	20	58	1.98	6.9	18.3	72	.72	.108	18	56	1.09	267	.11	26	2.35	.06	.69	15	2.5	940	.7	2.0	7.0	53

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA ____

ACME ANALYTICAL

Crest Geological Consulting PROJECT 178 FILE # 9801731

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
11824	1.1	51.2	2.3	96.2	128	12	5	312	1.21	.9	<5	<2	17	.14	.3	<.2	27	.24	.018	5	18	.32	61	.05	<3	.81	.01	.04	<2	<.2	<10	<.3	<.2	2.8	1
11825	1.3	91.9	2.9	107.2	150	19	8	626	1.54	1.0	<5	<2	23	.12	.3	<.2	30	.31	.024	7	27	.44	100	.04	<3	1.22	.01	.06	<2	<.2	13	<.3	<.2	3.3	<1
11826	.9	54.6	2.3	68.5	104	12	5	331	.99	.6	<5	<2	16	.06	<.2	<.2	22	.20	.020	4	16	.31	61	.04	<3	.88	.01	.04	<2	<.2	<10	<.3	<.2	2.6	<1
11827	.6	32.7	3.0	53.9	138	9	4	223	.97	.6	<5	<2	16	.05	.2	<.2	23	.19	.013	4	15	.32	54	.05	<3	.78	.01	.03	<2	<.2	<10	<.3	<.2	3.0	<1
11828	.9	41.5	2.4	54.4	76	10	6	425	1.13	.9	<5	<2	19	.13	.2	<.2	25	.26	.026	5	15	.36	45	.05	<3	.74	.01	.04	<2	<.2	<10	<.3	<.2	2.3	<1
11829	.9	106.6	2.1	202.8	531	15	5	467	.64	1.8	<5	<2	416	1.69	.4	<.2	9	21.11	.182	3	7	.31	150	.01	12	.52	.01	.04	<2	.2	31	.7	<.2	2.3	<1
11830	1.9	62.9	4.5	92.3	169	16	10	630	2.12	1.8	<5	<2	24	.10	.3	<.2	35	.48	.013	6	30	.41	83	.05	<3	1.42	.01	.09	<2	<.2	23	<.3	<.2	3.1	<1
11831	.6	33.3	3.0	75.9	162	12	5	231	.99	.8	<5	<2	16	.08	.2	<.2	22	.21	.020	5	16	.32	62	.04	<3	.85	.01	.04	<2	<.2	16	<.3	<.2	3.0	3
11832	1.1	104.4	3.6	137.8	236	25	8	558	1.88	1.2	9	<2	28	.11	.2	<.2	35	.34	.038	8	31	.48	129	.04	<3	1.61	.01	.08	<2	<.2	33	<.3	<.2	4.1	1
11833	1.3	63.9	4.1	122.7	171	14	6	531	1.25	1.8	<5	<2	26	.24	.3	<.2	25	.34	.037	7	21	.40	80	.04	<3	1.00	.01	.06	<2	<.2	<10	<.3	<.2	2.8	3
RE 11834	.6	22.1	2.1	75.7	105	10	4	177	.99	.6	<5	<2	15	.09	.2	<.2	23	.19	.021	4	16	.28	41	.05	<3	.69	.01	.04	<2	<.2	<10	<.3	<.2	2.0	28
11834	.6	22.1	2.3	74.4	129	9	4	174	.98	.6	<5	<2	13	.10	.3	<.2	22	.19	.022	4	13	.28	41	.04	<3	.66	.01	.03	<2	<.2	<10	<.3	<.2	2.5	85
11835	1.1	92.8	3.2	206.1	320	28	7	800	1.85	1.1	<5	<2	35	.28	.3	<.2	31	.41	.050	14	31	.42	152	.04	<3	1.52	.01	.08	<2	<.2	15	<.3	<.2	4.2	3
11836	.9	64.9	2.7	90.2	268	16	6	441	1.27	1.0	<5	<2	19	.12	.3	<.2	25	.28	.027	8	19	.32	67	.04	<3	1.00	.01	.06	<2	<.2	29	<.3	<.2	2.8	2
11837	1.0	38.1	2.8	84.0	209	12	5	239	1.30	.7	<5	<2	21	.11	.2	<.2	26	.30	.027	5	16	.37	58	.05	<3	.93	.01	.06	<2	<.2	<10	<.3	<.2	2.9	1
11838	1.3	38.3	2.6	108.3	193	13	5	300	1.26	.5	<5	<2	17	.14	.2	<.2	25	.25	.019	5	17	.35	65	.05	<3	.91	.01	.05	<2	<.2	30	<.3	<.2	2.5	4
11839	.9	19.4	2.1	83.8	147	9	4	235	1.06	.5	<5	<2	18	.12	.2	<.2	22	.24	.033	4	14	.30	66	.05	<3	.74	.01	.05	<2	<.2	<10	<.3	<.2	2.1	2
11840	2.5	53.8	2.9	89.8	112	9	5	457	1.17	.8	<5	<2	22	.18	.3	<.2	23	.30	.027	5	18	.33	89	.05	3	.79	.01	.05	<2	<.2	<10	<.3	<.2	2.8	2
11841	2.8	58.7	2.8	83.8	161	11	5	400	1.24	1.1	<5	<2	23	.18	.4	<.2	26	.35	.030	5	19	.33	74	.06	<3	.81	.01	.05	<2	<.2	15	<.3	<.2	2.7	1
11842	1.4	22.0	2.8	116.0	183	11	6	361	1.37	.5	<5	<2	20	.13	.2	<.2	29	.25	.023	5	19	.37	78	.06	<3	.91	.01	.06	<2	<.2	13	<.3	<.2	2.8	15
11843	3.4	149.4	4.1	271.1	654	25	13	371	2.39	2.1	<5	<2	31	.47	.4	<.2	41	.54	.031	7	43	.57	106	.05	<3	1.58	.01	.10	<2	<.2	29	.4	.2	4.1	1
11844	3.7	260.5	4.7	92.1	161	20	10	445	2.00	2.8	<5	<2	33	.19	.6	<.2	35	.51	.065	7	23	.49	88	.05	<3	1.10	.01	.06	<2	<.2	25	<.3	.2	3.0	1
11845	3.6	165.6	4.0	109.1	215	19	8	557	1.82	2.4	<5	<2	75	.63	.5	<.2	31	3.98	.038	5	30	.46	97	.04	<3	1.02	.01	.10	<2	<.2	31	.3	<.2	3.3	1
11846	.9	10.2	2.3	394.9	133	6	6	458	1.45	<.5	<5	<2	19	.14	<.2	<.2	23	.23	.010	3	13	.54	59	.05	<3	1.06	.01	.07	<2	<.2	14	<.3	<.2	3.1	<1
11847	.4	14.7	2.0	325.7	172	8	6	393	1.44	<.5	<5	<2	15	.12	<.2	<.2	19	.17	.044	3	11	.58	90	.04	<3	1.07	<.01	.06	<2	<.2	<10	<.3	<.2	3.0	3
11848	.5	5.2	2.3	220.4	153	6	5	365	1.11	<.5	<5	<2	17	.06	<.2	<.2	18	.20	.017	4	10	.47	55	.04	<3	.92	<.01	.05	<2	<.2	<10	<.3	<.2	2.7	1
11849	.7	9.3	1.8	213.1	173	7	5	343	1.39	.5	<5	<2	16	.08	<.2	<.2	22	.20	.018	3	12	.55	53	.04	<3	1.04	.01	.04	<2	<.2	<10	<.3	<.2	2.9	<1
11850	.6	18.9	2.3	183.0	180	10	5	248	1.20	<.5	<5	<2	18	.10	<.2	<.2	24	.23	.023	4	14	.35	66	.05	<3	.96	.01	.05	<2	<.2	<10	<.3	<.2	2.7	1
11851	.6	14.3	2.1	125.6	145	9	5	236	1.17	.6	<5	<2	18	.09	<.2	<.2	24	.21	.027	5	12	.37	73	.05	<3	.93	.01	.04	<2	<.2	<10	<.3	<.2	2.4	5
11852	.8	9.0	2.5	93.1	219	6	4	281	.89	.5	<5	<2	14	.09	<.2	<.2	19	.18	.033	3	12	.26	80	.03	<3	.74	<.01	.04	<2	<.2	<10	<.3	<.2	2.6	1
11853	.6	19.9	2.3	101.8	247	8	4	212	1.10	.7	<5	<2	15	.09	.2	<.2	21	.17	.032	3	15	.36	51	.04	<3	.87	.01	.03	<2	<.2	<10	<.3	<.2	2.8	<1
11854	.9	15.7	2.5	151.0	153	8	5	241	1.27	.7	<5	<2	14	.23	.2	<.2	25	.16	.034	4	15	.38	77	.05	<3	.89	<.01	.04	<2	<.2	17	<.3	<.2	3.2	<1
11855	.7	12.8	2.5	213.7	113	9	5	368	1.21	.6	<5	<2	18	.19	<.2	<.2	24	.24	.025	4	14	.33	104	.05	<3	1.00	.01	.05	<2	<.2	<10	<.3	<.2	2.8	<1
11856	.9	21.0	2.6	855.1	138	12	7	353	1.69	.6	<5	<2	18	.45	<.2	<.2	29	.30	.049	4	19	.44	103	.04	<3	1.43	.01	.05	<2	<.2	14	<.3	.2	3.6	<1
STANDARD	23.4	118.6	101.5	258.4	2066	30	17	1006	4.69	85.8	27	17	59	2.03	10.1	19.7	69	.66	.108	16	53	1.08	231	.10	25	2.26	.04	.68	15	2.4	990	.7	2.0	6.9	55

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
11857	.6	222.3	3.0	99.8	140	23	9	366	2.19	1.4	<5	<2	58	.19	.4	<.2	28	2.42	.052	8	27	.66	77	.05	4	1.30	.02	.08	<2	<.2	18	<.3	<.2	3.5	3
11858	1.1	98.0	2.1	174.9	129	18	6	362	1.36	3.7	5	<2	90	.25	.2	<.2	20	7.12	.030	6	18	.35	70	.03	6	.71	.01	.06	<2	<.2	12	.3	<.2	2.2	5
11859	.6	37.5	3.1	61.9	83	10	4	196	1.11	1.2	<5	<2	18	.06	.2	.2	26	.28	.020	4	14	.34	49	.05	<3	.89	.01	.04	<2	<.2	10	<.3	<.2	3.1	<1
11860	.4	61.2	2.6	63.8	45	12	5	308	1.09	.6	<5	<2	19	.04	<.2	<.2	23	.29	.025	6	16	.35	70	.04	5	1.02	.01	.04	<2	<.2	<10	<.3	<.2	2.6	1
11861	.9	40.7	2.1	74.8	53	10	5	275	1.21	.9	<5	<2	20	.08	.2	<.2	27	.30	.025	5	15	.37	53	.05	3	.84	.01	.04	<2	<.2	<10	<.3	<.2	2.5	<1
11862	2.2	769.8	5.1	184.6	944	77	15	996	4.27	7.8	<5	<2	71	.45	.4	<.2	55	1.09	.069	21	68	.79	399	.04	<3	3.84	.02	.16	<2	<.2	72	.4	.2	7.9	1
11863	.7	66.2	1.9	82.8	150	13	4	206	1.05	1.4	<5	<2	15	.19	.2	<.2	21	.23	.020	3	20	.22	44	.03	<3	.75	.01	.04	<2	<.2	<10	<.3	<.2	2.6	<1
11864	1.0	116.8	4.0	89.9	140	19	6	369	1.55	3.0	<5	<2	28	.11	.2	<.2	32	.44	.025	7	26	.35	87	.04	<3	1.19	.01	.06	<2	<.2	36	<.3	<.2	3.0	3
11865	1.5	272.1	5.3	208.5	354	47	12	915	4.06	6.8	<5	<2	47	.23	.6	1.1	53	.82	.046	14	55	.71	259	.04	<3	2.85	.02	.15	<2	<.2	38	.3	<.2	6.2	1
11866	.8	44.4	3.2	68.4	94	13	6	384	1.20	1.3	<5	<2	22	.05	.2	.2	25	.31	.016	6	19	.41	92	.04	<3	1.07	.01	.05	<2	<.2	20	<.3	<.2	2.9	4
11867	.7	66.1	3.0	73.3	92	15	7	409	1.50	2.1	<5	<2	26	.05	.2	<.2	31	.40	.011	6	25	.39	83	.06	<3	1.09	.01	.05	<2	<.2	14	<.3	<.2	2.9	3
11868	1.2	97.5	4.7	88.3	364	22	10	690	2.12	5.2	<5	<2	31	.17	.5	.2	35	.60	.020	8	30	.44	103	.06	<3	1.46	.01	.07	<2	<.2	21	<.3	<.2	3.6	1
11869	.9	104.6	4.6	104.8	381	20	10	526	2.35	4.3	<5	<2	34	.19	.4	<.2	35	.72	.019	8	36	.42	98	.06	<3	1.63	.01	.07	<2	<.2	28	<.3	<.2	4.0	1
11870	.8	57.9	3.4	60.9	259	14	6	325	1.42	2.6	<5	<2	26	.17	.3	<.2	28	.51	.016	6	22	.33	65	.05	<3	1.01	.01	.05	<2	<.2	19	<.3	<.2	2.9	<1
11871	1.4	100.5	4.6	91.6	396	24	9	630	2.13	4.8	<5	<2	33	.26	.4	<.2	38	.63	.024	10	29	.40	100	.05	<3	1.44	.01	.08	<2	<.2	25	<.3	<.2	3.8	1
11872	1.5	172.9	5.7	225.8	495	47	11	1148	3.11	5.7	<5	<2	40	.41	.4	<.2	42	.75	.035	10	44	.53	219	.06	<3	2.27	.02	.14	<2	<.2	29	<.3	<.2	4.6	1
11873	.9	39.9	3.3	63.1	79	13	7	366	1.32	2.2	8	<2	18	.09	.3	.2	30	.28	.016	6	18	.39	50	.06	<3	.82	.01	.04	<2	<.2	<10	<.3	<.2	2.2	9
RE 11873	1.0	42.2	2.9	64.8	69	13	7	377	1.38	1.7	<5	<2	20	.08	.3	<.2	31	.30	.016	6	18	.40	52	.07	<3	.86	.01	.05	<2	<.2	<10	<.3	<.2	2.5	5
11874	.8	73.5	4.2	65.4	268	19	7	454	1.52	2.6	<5	<2	26	.10	.4	<.2	33	.40	.022	8	25	.34	80	.05	<3	1.10	.01	.07	<2	<.2	21	<.3	<.2	3.0	2
11875	1.0	84.0	3.5	70.6	119	18	7	412	1.73	4.0	7	<2	27	.07	.4	.2	32	.44	.041	7	25	.48	73	.06	<3	1.21	.01	.06	<2	<.2	<10	<.3	<.2	3.0	5
11876	.7	38.1	2.7	73.3	92	12	4	218	1.22	1.3	<5	<2	18	.04	.2	<.2	26	.25	.023	5	18	.38	61	.05	<3	.94	.01	.04	<2	<.2	13	<.3	<.2	2.5	2
11877	.5	30.8	3.4	81.1	119	12	5	230	1.21	<.5	<5	<2	19	.06	<.2	.2	25	.29	.019	5	18	.36	79	.05	<3	.97	.01	.05	<2	<.2	<10	<.3	<.2	2.7	1
11878	.6	43.9	3.3	91.9	141	16	5	348	1.40	.9	<5	<2	22	.05	.2	.2	30	.33	.021	6	27	.37	89	.06	<3	1.18	.01	.06	<2	<.2	20	<.3	<.2	2.9	1
11879	.7	32.2	2.9	83.2	118	12	5	491	1.08	<.5	<5	<2	18	.04	<.2	<.2	23	.25	.018	5	17	.29	81	.04	<3	.92	.01	.04	<2	.2	<10	<.3	<.2	2.4	1
11880	1.2	58.2	3.5	79.8	126	15	6	396	1.43	1.4	8	<2	24	.07	.3	.2	28	.31	.026	7	18	.44	72	.05	<3	1.04	.01	.05	<2	<.2	<10	<.3	<.2	3.1	5
11881	.6	29.3	2.7	63.7	68	10	4	209	1.26	.8	<5	<2	21	.05	.2	.2	28	.29	.016	5	16	.35	49	.07	<3	.85	.01	.05	<2	<.2	<10	<.3	<.2	2.4	4
11882	.7	19.5	2.9	71.5	77	8	4	284	1.03	<.5	<5	<2	20	.07	<.2	<.2	23	.28	.020	4	16	.30	67	.05	<3	.70	.01	.05	<2	<.2	<10	<.3	<.2	2.5	1
11883	.6	31.8	2.5	71.0	80	11	5	245	1.30	1.0	<5	<2	18	.05	.2	.2	27	.27	.020	5	18	.37	52	.06	<3	.86	.01	.05	<2	<.2	<10	<.3	<.2	2.4	1
11884	.6	42.8	3.1	75.1	97	12	5	274	1.29	.8	<5	<2	20	.05	.2	.2	25	.30	.023	6	20	.42	60	.07	<3	.98	.01	.05	<2	<.2	<10	<.3	<.2	3.0	1
11885	.6	16.3	2.6	102.7	223	9	4	232	1.19	.6	<5	<2	21	.11	.2	.2	24	.32	.037	5	17	.31	62	.06	<3	.84	.01	.06	<2	<.2	<10	<.3	<.2	2.6	2
11886	.9	12.7	2.3	74.5	85	6	4	189	.98	<.5	<5	<2	13	.10	<.2	.2	23	.21	.025	3	12	.25	50	.05	<3	.64	.01	.03	<2	<.2	<10	<.3	<.2	2.1	1
11887	1.3	58.5	3.1	109.1	368	13	7	542	1.52	2.8	5	<2	25	.19	.3	.2	28	.43	.075	5	24	.38	95	.05	<3	.94	.01	.09	<2	<.2	15	<.3	<.2	3.0	<1
11888	1.3	85.5	3.4	67.7	113	16	8	718	1.58	4.3	7	<2	26	.11	.4	<.2	33	.58	.054	5	24	.42	65	.05	<3	.89	.01	.04	<2	<.2	14	<.3	<.2	2.6	1
11889	.9	39.5	3.9	892.9	198	20	11	753	2.35	1.5	<5	<2	21	.52	.3	.2	34	.31	.048	5	28	.54	163	.06	<3	1.54	.01	.07	<2	<.2	15	<.3	<.2	3.9	1
STANDARD	23.7	122.4	101.7	264.0	2026	31	17	1025	4.80	76.5	19	17	60	1.97	10.9	19.8	69	.74	.111	17	56	1.10	275	.11	24	2.29	.05	.70	16	2.4	1026	.4	1.8	7.0	53

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data ___ FA ____

ACME ANALYTICAL

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ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
11890	.8	18.7	3.5	642.1	237	13	8	712	1.81	1.0	<5	<2	19	.55	<.2	.2	37	.24	.037	4	20	.39	141	.05	<3	1.25	.01	.05	<2	<.2	20	<.3	<.2	4.3	2
11891	.7	61.2	3.4	392.6	164	22	10	847	2.35	1.4	<5	<2	28	.65	.4	<.2	40	.35	.054	6	28	.57	146	.05	<3	1.46	.01	.08	<2	<.2	22	<.3	<.2	4.1	1
11892	1.0	65.4	3.3	283.3	55	18	9	778	2.16	1.2	<5	<2	21	.36	.3	<.2	39	.27	.029	7	28	.56	81	.05	<3	1.26	.01	.13	<2	<.2	25	<.3	<.2	3.7	<1
11893	.4	8.9	1.8	140.7	<30	7	4	282	1.10	1.2	<5	<2	18	.11	<.2	<.2	22	.21	.020	3	11	.37	62	.04	<3	.82	<.01	.04	<2	<.2	11	<.3	<.2	2.8	<1
11894	.5	11.7	2.1	147.4	53	7	5	253	1.19	<.5	<5	<2	19	.14	<.2	<.2	23	.23	.051	4	11	.38	77	.04	<3	.92	<.01	.05	<2	<.2	23	<.3	<.2	2.7	2
11895	.4	12.5	2.1	131.0	145	7	4	238	1.15	<.5	<5	<2	13	.09	<.2	<.2	21	.17	.042	4	11	.40	56	.04	<3	.91	<.01	.03	<2	<.2	20	<.3	<.2	3.1	<1
11896	.7	13.4	2.8	143.1	83	7	5	260	1.22	.8	<5	<2	14	.12	<.2	.2	25	.17	.024	4	13	.44	49	.04	<3	.94	<.01	.03	<2	<.2	<10	<.3	<.2	3.1	<1
11897	1.9	10.1	2.8	78.9	176	7	5	238	1.38	.5	<5	<2	18	.07	<.2	<.2	34	.20	.009	4	14	.44	59	.04	<3	1.07	.01	.03	<2	<.2	18	<.3	<.2	3.5	1
11898	2.2	163.8	4.7	465.2	473	33	13	2634	2.56	1.4	<5	<2	43	.58	.3	<.2	49	.48	.026	10	27	.56	186	.05	<3	1.76	.01	.07	<2	<.2	51	.4	<.2	4.7	2
11899	1.1	17.4	3.3	485.3	182	11	6	970	1.49	1.0	<5	<2	22	.56	<.2	<.2	25	.22	.064	4	19	.34	211	.05	<3	1.13	.01	.10	<2	<.2	22	<.3	<.2	3.6	1
11900	.6	13.7	2.4	196.3	121	8	5	339	1.25	<.5	<5	<2	17	.17	<.2	<.2	25	.20	.022	4	13	.42	66	.05	<3	.90	.01	.05	<2	<.2	11	<.3	<.2	3.3	14
11923	.7	34.7	3.1	46.8	50	10	4	266	1.12	.9	<5	<2	23	.05	.2	<.2	27	.31	.028	6	16	.42	43	.06	<3	.87	.01	.04	<2	<.2	47	<.3	<.2	3.1	1
11924	1.3	75.9	2.7	68.7	106	15	6	452	1.33	1.1	<5	<2	26	.13	.2	<.2	30	.37	.018	7	20	.37	76	.05	<3	1.05	.01	.05	<2	<.2	26	<.3	<.2	3.4	1
11925	.9	35.1	2.4	50.2	72	9	4	247	1.09	1.1	5	<2	16	.07	.3	<.2	28	.22	.012	4	15	.28	50	.05	<3	.72	.01	.04	<2	<.2	17	<.3	<.2	2.4	1
11926	1.1	95.2	4.5	89.6	325	18	7	453	1.70	1.9	<5	<2	28	.24	.5	<.2	35	.50	.019	8	26	.33	81	.05	<3	1.25	.01	.06	<2	<.2	18	<.3	<.2	3.6	<1
RE 11927	1.9	13.3	3.4	49.2	77	7	4	173	1.14	1.2	<5	<2	16	.08	.2	<.2	31	.19	.025	4	15	.27	51	.05	<3	.88	.01	.03	<2	<.2	10	<.3	<.2	3.9	3
11927	1.9	13.5	3.4	51.8	72	8	4	179	1.20	1.0	<5	<2	18	.08	<.2	<.2	32	.21	.025	5	15	.28	53	.05	<3	.94	.01	.03	<2	<.2	13	<.3	<.2	3.9	1
11928	1.1	74.4	3.1	64.6	104	16	7	460	1.56	1.8	<5	<2	24	.11	.4	<.2	34	.33	.018	7	24	.41	63	.06	<3	1.05	.01	.05	<2	<.2	26	<.3	<.2	3.4	1
11929	1.4	216.0	4.2	151.8	447	34	11	755	2.55	2.8	<5	<2	37	.22	.4	<.2	44	.56	.029	10	38	.54	136	.05	<3	1.79	.02	.11	<2	<.2	42	<.3	<.2	4.4	1
11930	.6	41.3	3.2	59.6	82	12	5	293	1.23	.9	<5	<2	23	.05	.2	<.2	30	.29	.015	6	19	.44	52	.07	<3	.97	.01	.05	<2	<.2	19	<.3	<.2	3.0	2
11931	2.5	322.0	6.5	273.8	530	64	17	1279	4.92	4.0	<5	2	59	.17	.6	.7	77	.67	.070	14	81	1.03	352	.05	<3	4.07	.02	.22	<2	<.2	52	.3	<.2	10.0	1
11932	1.9	175.0	4.1	160.0	616	48	11	824	2.94	2.7	<5	<2	55	.36	.6	<.2	47	.72	.035	16	47	.57	178	.05	<3	2.52	.01	.12	<2	<.2	62	.6	<.2	5.9	1
11933	1.1	30.0	3.0	77.5	173	14	6	239	1.44	1.2	5	<2	19	.14	.3	<.2	33	.30	.025	5	19	.36	53	.05	<3	.95	.01	.04	<2	<.2	17	<.3	<.2	3.3	136
11934	1.2	28.0	3.1	88.9	154	12	6	296	1.49	1.5	<5	<2	28	.10	.2	<.2	31	.43	.117	5	20	.32	115	.04	<3	1.07	.01	.06	<2	<.2	28	<.3	<.2	3.4	1
11935	.7	19.3	2.2	66.9	56	10	5	217	1.21	1.3	<5	<2	20	.07	.2	<.2	28	.25	.039	5	18	.34	75	.05	<3	.87	.01	.04	<2	<.2	25	<.3	<.2	2.4	1
11936	1.4	157.7	3.7	86.8	102	28	9	395	2.49	4.9	<5	<2	28	.05	.6	<.2	49	.35	.045	8	37	.68	87	.06	<3	1.68	.01	.09	<2	<.2	46	<.3	<.2	4.6	2
11937	1.1	90.4	3.7	77.5	166	20	7	479	1.51	2.2	<5	<2	24	.09	.4	<.2	35	.31	.022	8	27	.46	81	.06	<3	1.19	.01	.07	<2	<.2	21	<.3	<.2	3.7	<1
11938	1.0	38.3	2.9	73.0	104	15	6	235	1.47	1.6	<5	<2	21	.09	.3	<.2	35	.28	.022	7	22	.40	59	.07	<3	1.02	.01	.05	<2	<.2	24	<.3	<.2	3.7	1
11939	.7	24.9	2.6	71.9	46	10	4	216	1.11	1.0	<5	<2	18	.06	.2	<.2	26	.22	.021	5	16	.35	46	.06	<3	.84	.01	.04	<2	<.2	24	<.3	<.2	2.6	<1
11940	1.0	28.3	2.7	86.1	125	11	5	239	1.23	1.1	<5	<2	21	.11	<.2	<.2	29	.25	.029	5	18	.36	62	.06	<3	.91	.01	.05	<2	<.2	15	<.3	<.2	3.1	1
11941	1.3	31.2	2.7	82.6	117	13	6	334	1.34	1.7	<5	<2	17	.14	.2	<.2	33	.24	.027	6	23	.37	69	.07	<3	.88	.01	.05	<2	<.2	16	<.3	<.2	3.0	<1
11942	.7	25.2	2.7	86.3	136	10	4	210	1.22	1.3	<5	<2	19	.08	<.2	<.2	27	.25	.025	5	17	.36	63	.06	<3	.88	.01	.05	<2	<.2	17	<.3	<.2	2.9	<1
11943	1.3	134.4	3.5	93.4	229	23	8	618	2.23	2.8	<5	2	31	.16	.5	<.2	38	.52	.040	12	32	.54	102	.05	<3	1.48	.01	.10	<2	<.2	46	<.3	<.2	4.4	1
11944	.9	25.3	2.8	71.5	92	11	5	345	1.30	1.3	<5	<2	22	.09	.2	<.2	30	.31	.023	5	19	.36	71	.06	<3	.92	.01	.06	<2	<.2	12	<.3	<.2	3.0	<1
STANDARD	23.7	119.7	102.2	260.2	2055	31	17	1024	4.85	79.1	24	17	59	2.02	10.1	20.1	76	.72	.110	16	56	1.10	234	.11	25	2.31	.04	.69	16	2.6	974	.5	2.2	7.9	52

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA _____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
11945	.9	30.2	2.8	84.3	75	11	5	267	1.23	1.0	<5	<2	18	.10	<.2	<.2	25	.30	.020	5	16	.36	51	.06	<3	.84	.01	.05	<2	.2	30	<.3	<.2	2.3	2
11946	.6	22.7	2.6	87.0	48	12	5	231	1.29	1.1	<5	<2	16	.09	.2	<.2	29	.25	.027	5	22	.33	59	.06	<3	.81	.01	.05	<2	.2	25	<.3	<.2	2.0	1
11947	1.4	25.6	3.1	55.8	33	12	6	217	1.42	1.5	<5	<2	17	.08	<.2	<.2	30	.25	.046	4	20	.36	53	.05	<3	.87	.01	.07	<2	<.2	13	<.3	<.2	2.3	1
11948	1.1	114.3	4.1	81.1	282	32	11	493	2.62	5.6	<5	2	37	.12	.6	<.2	46	.69	.066	9	41	.73	86	.06	<3	1.40	.02	.08	<2	.2	59	<.3	<.2	3.5	3
11949	.8	553.1	3.9	107.8	608	36	8	495	1.89	3.8	<5	<2	76	.39	.4	1.8	31	1.74	.067	7	33	.36	191	.02	4	1.26	.01	.06	<2	<.2	81	1.8	<.2	3.0	2
11950	1.0	23.4	3.8	111.2	80	8	5	398	1.18	1.5	<5	<2	13	.18	<.2	<.2	25	.19	.038	4	18	.32	67	.05	<3	.82	.01	.04	<2	<.2	<10	<.3	<.2	2.4	<1
11951	.8	31.7	3.0	120.3	213	10	5	353	1.18	.9	<5	<2	19	.06	<.2	<.2	21	.29	.029	4	14	.43	80	.03	<3	.99	.01	.05	<2	.3	22	<.3	<.2	2.7	<1
11952	.9	39.4	2.8	105.3	95	10	6	328	1.30	.9	5	<2	15	.04	<.2	<.2	25	.21	.020	5	14	.51	58	.04	<3	1.06	.01	.03	<2	<.2	<10	<.3	<.2	2.8	1
11953	.8	21.1	2.7	130.7	137	9	5	483	1.21	.5	<5	<2	17	.09	<.2	<.2	24	.22	.023	5	16	.42	94	.05	<3	1.00	.01	.05	<2	.2	12	<.3	<.2	2.7	1
11954	1.0	22.3	3.4	114.0	148	9	6	293	1.45	1.5	<5	<2	18	.08	.2	<.2	26	.25	.040	5	15	.53	81	.05	<3	1.16	.01	.04	<2	<.2	<10	<.3	<.2	3.3	1
11955	.9	17.9	2.9	101.6	140	8	6	311	1.33	1.6	<5	<2	18	.06	.2	<.2	25	.23	.020	4	14	.48	49	.05	<3	.95	.01	.04	<2	<.2	<10	<.3	<.2	2.8	1
11956	.8	16.2	2.9	268.3	224	10	6	408	1.35	.8	<5	<2	18	.14	<.2	<.2	23	.26	.036	5	14	.44	95	.05	<3	1.09	.01	.05	<2	.3	17	<.3	<.2	3.4	3
11957	1.0	16.1	2.2	117.7	81	7	6	496	1.34	.7	<5	<2	20	.04	<.2	<.2	24	.25	.016	4	13	.53	60	.05	<3	1.01	.01	.05	<2	<.2	12	<.3	<.2	2.7	<1
RE 11957	1.1	17.5	2.2	119.8	91	7	6	508	1.39	.8	<5	<2	21	.03	<.2	<.2	25	.26	.017	4	12	.54	60	.05	<3	1.05	.01	.06	<2	<.2	14	<.3	<.2	2.9	1
11958	.8	29.9	2.9	199.4	195	9	5	366	1.19	.6	<5	<2	17	.09	<.2	<.2	23	.22	.025	5	13	.42	73	.05	<3	1.02	.01	.04	<2	<.2	23	<.3	<.2	3.3	1
11959	.4	15.7	2.4	187.8	240	9	5	343	1.17	.8	<5	<2	19	.09	<.2	<.2	21	.25	.034	4	13	.41	82	.04	<3	.97	.01	.04	<2	<.2	18	<.3	<.2	2.6	1
11960	.8	25.3	2.4	213.0	203	10	6	369	1.40	.6	<5	<2	21	.16	<.2	<.2	25	.26	.027	5	18	.48	82	.05	<3	.99	.01	.05	<2	<.2	12	<.3	<.2	2.7	1
11961	.9	24.6	2.6	157.5	133	11	7	418	1.68	.9	<5	<2	24	.11	.2	<.2	31	.32	.020	5	20	.55	72	.07	<3	1.13	.01	.08	<2	<.2	11	<.3	<.2	3.2	1
11962	1.7	19.8	2.3	160.3	128	8	6	405	1.50	.6	<5	<2	19	.07	<.2	<.2	29	.24	.015	4	15	.47	51	.06	<3	.97	.01	.07	<2	<.2	16	<.3	<.2	2.7	<1
11963	1.1	66.7	3.0	517.1	582	11	9	712	1.89	.9	5	<2	33	.30	<.2	<.2	29	.53	.024	4	15	.64	83	.05	<3	1.35	.01	.08	<2	<.2	23	<.3	<.2	3.5	<1
11964	.6	24.6	2.3	332.5	235	10	7	394	1.56	.7	<5	<2	20	.25	.2	<.2	28	.26	.031	4	18	.50	57	.05	<3	1.03	.01	.05	<2	<.2	18	<.3	<.2	2.9	3
11965	1.0	60.6	3.4	365.4	250	32	12	368	2.44	2.0	<5	<2	22	.32	.3	<.2	43	.32	.087	6	36	.54	121	.06	<3	1.61	.01	.06	<2	<.2	30	<.3	<.2	4.2	1
11966	1.2	106.4	3.3	100.3	155	23	7	468	1.84	1.3	<5	<2	25	.12	.2	<.2	32	.35	.027	6	25	.40	98	.06	<3	1.35	.01	.10	<2	<.2	26	<.3	<.2	3.4	<1
11967	1.3	53.1	3.1	85.1	157	12	8	385	1.75	1.2	<5	<2	25	.07	.2	<.2	36	.38	.015	6	25	.44	74	.07	3	1.18	.01	.06	<2	<.2	28	<.3	<.2	3.2	<1
11968	2.7	133.4	3.7	82.8	236	17	8	1159	1.75	1.4	<5	<2	26	.12	.2	<.2	33	.43	.024	7	24	.39	105	.05	<3	1.20	.01	.07	<2	<.2	21	<.3	<.2	3.5	<1
11969	1.1	76.8	2.5	66.7	207	13	6	515	1.41	1.1	<5	<2	21	.03	.2	<.2	30	.28	.033	6	21	.39	60	.05	<3	.97	.01	.06	<2	<.2	11	<.3	<.2	2.5	221
11970	1.8	153.8	3.3	102.5	557	19	8	754	1.88	1.9	<5	<2	29	.12	.3	.2	35	.40	.040	9	28	.47	102	.05	4	1.28	.01	.10	<2	<.2	31	<.3	<.2	3.7	5
11971	3.8	414.0	4.8	184.3	1133	45	14	1184	3.26	3.1	<5	<2	54	.35	.4	.2	43	.91	.059	11	55	.69	165	.05	4	2.29	.02	.18	<2	<.2	96	.4	<.2	5.1	1
11972	1.1	110.1	2.6	67.6	260	19	8	346	1.65	4.4	<5	<2	139	.34	.4	<.2	29	10.94	.058	7	23	.60	96	.03	<3	.96	.02	.06	<2	<.2	33	.3	<.2	2.6	3
11973	.6	53.7	2.0	54.2	112	15	6	272	1.50	3.0	<5	<2	122	.25	.3	<.2	24	10.28	.059	5	19	.55	88	.03	<3	.83	.01	.05	<2	<.2	29	.3	<.2	2.5	1
11974	2.0	32.2	3.6	62.5	168	10	7	681	1.59	1.5	<5	<2	24	.09	.2	<.2	36	.47	.019	5	24	.31	99	.06	<3	1.04	.01	.07	<2	<.2	14	<.3	<.2	3.2	<1
11975	.9	41.0	2.4	72.0	95	15	8	345	1.77	2.7	<5	<2	22	.06	.3	<.2	38	.35	.053	6	25	.52	33	.06	<3	.98	.01	.05	<2	<.2	12	<.3	<.2	2.6	4
11976	1.5	38.6	3.1	740.0	203	11	9	670	1.83	.8	<5	<2	25	.68	.2	<.2	33	.37	.068	6	25	.38	96	.05	5	1.23	.01	.08	<2	<.2	28	<.3	<.2	2.6	<1
11977	1.5	26.6	2.7	342.7	249	8	6	326	1.42	1.1	<5	<2	29	.20	<.2	<.2	30	.48	.020	4	20	.31	60	.05	<3	.98	.01	.04	<2	<.2	22	.3	<.2	2.7	1
STANDARD	25.3	125.0	104.4	264.6	2020	31	18	1016	4.74	72.6	28	19	59	1.96	9.7	20.2	70	.68	.110	17	57	1.11	245	.11	31	2.30	.04	.68	15	2.5	993	.7	2.0	6.9	55

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA ____

ACME ANALYTICAL

Crest Geological Consulting PROJECT 178 FILE # 9801731

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
11978	1.0	27.8	3.5	301.5	185	10	10	681	1.64	1.5	<5	<2	27	.28	<.2	<.2	26	.55	.030	4	18	.43	83	.04	3	1.18	.01	.07	<2	<.2	23	.7	<.2	2.8	<1
11979	1.2	47.3	3.8	150.4	138	10	9	265	1.71	1.5	<5	<2	41	.23	<.2	<.2	22	.88	.016	4	15	.51	92	.03	3	1.40	.01	.05	<2	<.2	29	1.2	<.2	3.4	13
11980	.5	18.0	2.3	104.5	51	7	4	290	1.09	.9	<5	<2	12	.06	<.2	<.2	21	.18	.033	4	14	.37	57	.04	<3	.82	<.01	.03	<2	<.2	12	<.3	<.2	2.1	1
11981	1.2	30.6	2.7	200.8	127	10	6	337	1.73	1.4	<5	<2	15	.17	<.2	<.2	28	.20	.035	6	16	.54	70	.04	<3	1.19	.01	.04	<2	<.2	22	<.3	<.2	3.3	<1
11982	1.0	10.8	3.4	185.6	210	6	4	386	.97	1.5	<5	<2	11	.15	<.2	<.2	17	.18	.026	4	9	.33	60	.03	3	.79	.01	.04	<2	<.2	30	<.3	<.2	2.0	3
11983	.6	15.8	2.6	176.2	159	10	6	238	1.40	1.1	<5	<2	15	.08	<.2	<.2	23	.27	.092	4	15	.43	75	.04	<3	1.14	.01	.05	<2	<.2	15	<.3	<.2	2.9	<1
11984	.6	13.7	3.4	154.4	119	7	5	578	1.17	.7	<5	<2	18	.19	<.2	<.2	19	.29	.034	4	9	.45	97	.04	<3	.94	.01	.06	<2	<.2	19	<.3	<.2	2.4	1
11985	.9	9.0	2.8	50.4	48	6	5	206	1.13	<.5	<5	<2	15	.02	<.2	<.2	22	.24	.005	3	14	.37	47	.04	<3	.91	.01	.04	<2	<.2	<10	<.3	<.2	2.5	<1
11986	.5	10.9	2.1	104.3	144	7	5	269	1.16	.7	<5	<2	15	.03	<.2	<.2	20	.21	.025	3	12	.43	65	.04	3	.90	.01	.04	<2	<.2	18	<.3	<.2	2.0	1
RE 11986	.6	11.6	2.4	111.2	163	7	5	285	1.21	<.5	<5	<2	16	.05	<.2	<.2	21	.22	.025	3	13	.45	69	.04	<3	.96	.01	.05	<2	<.2	17	<.3	<.2	2.6	1
11987	.7	12.1	2.5	65.6	54	6	5	366	1.13	.7	<5	<2	13	.05	<.2	<.2	22	.19	.020	3	15	.38	58	.05	<3	.82	.01	.03	<2	<.2	19	<.3	<.2	2.4	1
11988	.8	40.0	2.7	93.9	276	10	6	560	1.43	2.5	<5	<2	106	.15	<.2	<.2	20	4.56	.046	3	17	.44	117	.02	3	1.06	.01	.03	<2	<.2	36	.3	<.2	3.0	<1
11989	.5	13.7	2.3	77.3	92	8	5	212	1.20	1.5	<5	<2	14	.05	<.2	<.2	22	.23	.045	4	13	.41	82	.04	<3	.86	.01	.05	<2	<.2	<10	<.3	<.2	2.6	1
11990	.7	13.1	2.4	90.0	123	8	5	231	1.13	1.6	<5	<2	13	.08	<.2	<.2	21	.18	.041	4	14	.37	101	.04	<3	.86	.01	.04	<2	<.2	13	<.3	<.2	2.0	1
11991	.4	24.2	2.2	68.9	<30	10	6	250	1.38	1.1	<5	<2	16	.04	<.2	<.2	26	.24	.035	5	17	.48	65	.05	<3	.93	.01	.04	<2	<.2	12	<.3	<.2	2.2	1
11992	.4	13.4	2.8	95.3	65	8	5	200	1.15	1.2	<5	<2	15	.05	<.2	<.2	21	.22	.041	4	14	.39	83	.04	3	.94	.01	.05	<2	<.2	12	<.3	<.2	2.6	1
11993	.9	38.6	2.7	60.0	36	17	5	211	1.44	3.1	<5	<2	19	.04	<.2	<.2	30	.25	.100	5	19	.33	105	.04	3	1.27	.01	.05	<2	<.2	17	<.3	<.2	2.8	1
11994	.9	27.3	3.3	74.6	<30	17	6	247	1.42	1.7	<5	<2	19	.05	<.2	<.2	29	.23	.089	5	19	.30	97	.04	<3	1.38	.01	.03	<2	<.2	28	<.3	<.2	3.8	1
11995	.6	26.8	3.3	54.0	<30	9	3	176	.90	.6	<5	<2	16	.03	<.2	<.2	22	.22	.018	5	11	.29	57	.05	<3	.83	.01	.03	<2	<.2	<10	<.3	<.2	2.7	1
11996	.9	19.5	3.3	92.5	<30	12	5	440	1.17	1.4	<5	<2	16	.08	<.2	<.2	25	.20	.088	4	14	.24	106	.03	3	1.14	.01	.03	<2	<.2	32	<.3	<.2	3.2	1
11997	.8	27.1	3.1	190.1	<30	13	5	323	1.39	1.5	<5	<2	18	.17	<.2	<.2	28	.26	.086	5	19	.33	84	.04	<3	1.25	.01	.04	<2	<.2	20	<.3	<.2	3.2	1
11998	.6	18.2	2.8	70.0	<30	10	5	354	1.21	.9	<5	<2	23	.09	<.2	<.2	28	.28	.051	5	15	.31	66	.04	<3	.92	.01	.03	<2	<.2	13	<.3	<.2	2.9	3
11999	.3	32.9	2.8	55.9	<30	11	4	199	1.00	.8	<5	<2	17	.02	<.2	<.2	22	.22	.017	5	16	.37	56	.05	<3	.94	.01	.03	<2	<.2	<10	<.3	<.2	2.5	2
12000	.3	13.2	2.0	66.8	35	8	4	300	.98	.6	<5	<2	26	.15	<.2	<.2	22	.35	.041	4	14	.24	102	.04	3	.64	.01	.04	<2	<.2	16	<.3	<.2	1.6	8
12001	.7	62.9	2.5	61.3	65	13	5	221	1.24	2.0	<5	<2	20	.05	<.2	<.2	29	.26	.018	6	16	.38	66	.05	<3	1.06	.01	.05	<2	<.2	<10	<.3	<.2	2.7	4
12002	.5	41.0	3.0	55.8	<30	11	5	247	1.12	.5	<5	<2	22	.03	<.2	<.2	24	.30	.018	6	18	.43	56	.06	<3	1.03	.01	.04	<2	<.2	<10	<.3	<.2	2.5	3
12003	.3	43.7	3.3	58.6	<30	13	5	223	1.15	.6	<5	<2	20	.03	<.2	<.2	25	.26	.016	6	17	.43	61	.06	<3	1.06	.01	.04	<2	<.2	13	<.3	<.2	2.8	2
12004	.7	74.9	2.5	72.7	54	17	6	438	1.27	1.5	<5	<2	24	.05	<.2	<.2	26	.30	.028	7	21	.40	82	.04	3	1.26	.01	.05	<2	<.2	15	<.3	<.2	2.9	<1
12005	.5	44.2	4.8	51.7	70	12	5	333	1.07	1.0	<5	<2	21	.13	<.2	<.2	23	.28	.021	6	20	.41	60	.06	<3	1.01	.01	.04	<2	<.2	23	<.3	<.2	3.1	1
12006	.5	58.5	3.1	66.1	91	14	6	335	1.14	.7	<5	2	22	.05	.2	<.2	25	.29	.024	7	19	.39	70	.05	4	1.02	.01	.04	<2	<.2	20	<.3	<.2	2.7	<1
12007	.7	52.2	2.0	73.9	66	12	5	226	1.18	.6	<5	<2	16	.05	<.2	<.2	24	.21	.020	5	16	.36	59	.04	<3	.90	.01	.04	<2	.2	12	<.3	<.2	2.4	1
12008	1.3	146.1	3.4	116.5	217	32	11	718	2.43	3.8	<5	<2	33	.09	.3	<.2	46	.42	.043	9	39	.53	145	.05	3	1.88	.01	.10	<2	<.2	24	<.3	<.2	4.5	1
12009	1.1	115.4	3.0	99.1	208	23	8	547	1.66	1.8	<5	<2	29	.09	.2	<.2	31	.39	.033	8	26	.44	108	.04	<3	1.48	.01	.07	<2	<.2	35	<.3	<.2	4.0	1
12010	.3	28.3	1.5	44.4	<30	8	3	147	.77	.6	<5	<2	15	.02	<.2	<.2	18	.21	.015	4	14	.27	35	.05	<3	.65	.01	.03	<2	<.2	<10	<.3	<.2	1.6	1
STANDARD	23.3	118.9	101.1	260.2	1915	30	17	1008	4.69	72.0	26	17	58	1.93	10.6	19.6	68	.69	.109	16	51	1.09	228	.10	31	2.24	.04	.68	16	2.4	987	.4	1.8	6.1	52

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12011	.5	47.2	3.0	77.2	69	12	4	202	.95	<.5	<5	<2	19	.03	<.2	<.2	21	.26	.016	5	16	.30	57	.05	4	.84	.01	.05	<2	<.2	21	<.3	<.2	2.4	1
12012	.8	75.8	3.6	86.4	221	20	7	425	1.70	.8	<5	<2	28	.13	.3	<.2	35	.42	.028	7	24	.40	90	.05	<3	1.23	.01	.08	<2	<.2	29	<.3	<.2	3.4	1
12013	.7	79.4	3.6	75.2	171	17	8	465	1.88	.6	<5	<2	30	.09	.4	<.2	33	.47	.031	7	26	.51	79	.06	<3	1.27	.01	.07	<2	<.2	31	<.3	<.2	3.3	1
12014	1.3	176.9	4.4	95.2	231	28	11	1226	2.28	1.9	5	<2	45	.33	.4	<.2	37	.99	.025	11	26	.48	143	.04	6	1.49	.01	.09	<2	<.2	32	.3	<.2	3.5	<1
12015	1.3	370.8	4.5	98.2	423	49	12	805	3.12	1.9	<5	2	60	.32	.3	<.2	44	.97	.029	13	55	.60	202	.04	4	2.60	.02	.11	<2	<.2	46	.4	<.2	5.3	1
12016	1.1	130.7	5.0	148.4	318	31	12	750	2.40	2.3	<5	2	38	.30	.4	<.2	41	.59	.035	10	35	.52	134	.06	3	1.69	.02	.10	<2	<.2	28	<.3	<.2	4.4	2
12017	.9	30.8	2.6	55.6	92	11	5	250	1.16	.9	<5	<2	22	.07	.2	<.2	26	.31	.030	6	15	.38	42	.06	<3	.81	.01	.04	<2	.2	21	<.3	<.2	2.6	<1
12018	1.0	58.5	2.9	86.3	212	18	7	407	1.56	1.1	<5	<2	26	.07	.2	<.2	33	.34	.039	8	22	.45	77	.05	4	1.16	.01	.06	<2	<.2	32	<.3	<.2	2.7	1
12019	.9	45.0	3.1	88.9	154	15	6	282	1.46	.7	<5	<2	22	.08	.3	<.2	33	.31	.032	7	21	.37	58	.06	<3	.98	.01	.05	<2	<.2	25	<.3	<.2	3.1	2
12020	.9	39.2	2.7	69.3	222	14	6	323	1.31	.6	<5	<2	21	.08	.2	<.2	30	.30	.022	7	18	.32	57	.06	3	.89	.01	.05	<2	<.2	<10	<.3	<.2	2.6	2
12021	2.0	132.9	5.8	91.1	166	27	11	627	2.39	3.6	<5	<2	38	.18	.6	.2	40	.87	.065	8	33	.63	90	.05	<3	1.41	.01	.14	<2	<.2	46	<.3	<.2	4.1	2
12022	1.2	28.2	3.4	69.0	125	8	5	325	1.11	.8	<5	<2	26	.12	.3	<.2	25	.46	.032	4	13	.30	57	.04	<3	.76	.01	.04	<2	<.2	14	<.3	<.2	2.3	<1
12023	1.5	235.7	5.6	140.4	469	31	12	1038	2.43	1.6	<5	<2	52	.29	.4	1.3	32	1.09	.036	12	28	.56	103	.04	3	1.56	.02	.09	<2	<.2	68	.3	<.2	4.0	2
12024	.8	19.8	4.0	56.9	115	10	6	341	1.53	1.3	<5	<2	27	.06	.3	<.2	36	.42	.011	5	20	.39	72	.06	4	1.07	.01	.04	<2	<.2	11	<.3	<.2	3.7	<1
12025	2.0	272.6	6.8	172.4	728	36	15	1685	2.73	2.3	<5	<2	62	.51	.5	1.0	41	1.34	.052	14	34	.48	203	.04	6	1.91	.02	.11	<2	<.2	53	.4	<.2	4.9	<1
12026	1.0	80.1	4.7	97.9	237	18	8	568	1.90	1.5	<5	<2	31	.17	.3	<.2	37	.43	.014	7	23	.45	89	.05	<3	1.27	.01	.05	<2	<.2	27	<.3	<.2	3.7	<1
12027	1.0	20.0	3.3	81.7	105	10	6	293	1.49	.5	<5	<2	28	.05	<.2	<.2	33	.32	.014	6	19	.43	81	.05	<3	1.17	.01	.04	<2	<.2	<10	<.3	<.2	3.3	1
12028	1.0	71.7	4.3	73.3	87	16	10	467	2.38	1.1	6	2	45	.07	.3	<.2	37	.58	.013	8	31	.66	113	.05	5	1.63	.01	.08	<2	<.2	16	<.3	<.2	4.4	3
12029	.7	15.2	4.3	63.6	89	9	5	209	1.31	.5	<5	<2	24	.06	.3	<.2	29	.29	.040	5	16	.37	71	.05	4	.96	.01	.04	<2	<.2	14	<.3	<.2	3.1	6
RE 12029	.7	13.4	3.5	60.0	87	8	5	195	1.24	<.5	<5	<2	21	.06	.2	<.2	27	.27	.039	5	15	.35	68	.05	<3	.91	.01	.04	<2	<.2	17	<.3	<.2	3.3	4
12030	.7	38.0	3.0	70.2	111	15	6	309	1.90	2.2	<5	<2	27	.03	.3	<.2	35	.37	.023	6	25	.58	72	.07	3	1.24	.01	.04	<2	<.2	33	<.3	<.2	3.5	6
12031	.9	36.4	2.8	63.7	130	11	7	285	1.61	.6	<5	<2	24	.03	.2	<.2	33	.34	.014	5	24	.48	48	.07	<3	1.09	.01	.05	<2	<.2	15	<.3	<.2	3.4	4
12032	.4	37.7	3.1	98.2	120	11	4	187	1.01	<.5	<5	<2	15	.03	<.2	<.2	20	.24	.025	5	13	.33	54	.05	<3	.97	.01	.04	<2	<.2	12	<.3	<.2	2.9	2
12033	.9	21.1	3.1	94.6	65	7	5	234	1.19	<.5	<5	<2	16	.05	<.2	<.2	23	.21	.031	5	10	.40	68	.05	<3	.98	.01	.04	<2	<.2	<10	<.3	<.2	3.2	<1
12034	.6	28.6	2.4	150.3	118	11	7	284	1.47	<.5	<5	<2	20	.11	<.2	<.2	22	.27	.066	4	12	.57	121	.05	<3	1.22	.01	.05	<2	<.2	<10	<.3	<.2	3.4	2
12035	.5	13.1	3.1	377.5	46	7	5	339	1.20	<.5	<5	<2	18	.31	<.2	<.2	22	.24	.031	5	10	.44	93	.05	3	1.06	.01	.05	<2	<.2	<10	<.3	<.2	3.5	3
12036	.6	15.4	2.1	152.4	63	9	7	277	1.68	<.5	<5	<2	16	.06	<.2	<.2	23	.20	.018	4	11	.73	40	.03	<3	1.29	<.01	.03	<2	<.2	13	<.3	<.2	4.0	1
12037	.9	17.9	2.6	126.8	113	8	5	240	1.28	<.5	<5	<2	17	.07	.2	<.2	22	.22	.031	4	10	.45	48	.05	<3	.97	.01	.04	<2	<.2	25	<.3	<.2	3.4	2
12038	1.8	17.5	3.8	117.9	67	13	7	281	1.76	.8	5	<2	61	.22	.3	<.2	36	1.86	.012	4	22	.43	90	.05	<3	1.12	.02	.04	<2	<.2	22	<.3	<.2	4.0	<1
12039	2.2	27.3	5.3	621.2	355	20	13	822	2.77	1.3	<5	<2	23	.50	.2	<.2	46	.34	.076	6	31	.50	192	.05	<3	1.69	.01	.07	<2	<.2	23	<.3	<.2	5.2	1
12040	.8	36.7	2.9	263.5	146	18	10	425	2.13	1.5	<5	<2	19	.26	.3	<.2	42	.29	.080	5	30	.49	91	.05	<3	1.11	.01	.03	<2	<.2	14	<.3	<.2	3.3	5
12041	1.5	10.7	3.0	56.0	321	5	4	216	.89	<.5	<5	<2	61	.10	<.2	<.2	15	.76	.012	2	8	.36	74	.02	<3	.74	.01	.04	<2	<.2	31	<.3	<.2	2.5	<1
12042	.7	252.1	2.4	220.3	549	18	5	389	1.15	.7	<5	<2	354	.82	.2	1.4	12	12.81	.187	4	14	.54	158	.02	14	.98	.02	.08	<2	<.2	41	.6	<.2	2.5	2
12043	1.3	19.3	2.7	124.0	136	8	8	593	1.74	<.5	<5	<2	21	.07	<.2	<.2	25	.34	.023	3	9	.72	65	.05	<3	1.29	.01	.06	<2	<.2	19	.3	<.2	4.1	3
STANDARD	23.8	122.6	103.3	263.8	2001	31	17	1023	4.78	75.9	21	19	59	1.91	11.1	17.4	69	.69	.111	16	51	1.10	248	.11	26	2.30	.04	.69	15	2.4	986	.7	2.2	7.6	53

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA ____

ACME ANALYTICAL

Crest Geological Consulting PROJECT 178 FILE # 9801731

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12044	.4	11.9	2.7	220.2	139	8	7	480	1.40	.6	<5	<2	14	.08	<.2	<.2	23	.19	.041	4	16	.55	102	.04	<3	1.10	.01	.04	<2	<.2	10	<.3	<.2	3.3	1
12045	.8	15.2	2.3	214.1	139	8	6	774	1.56	.6	<5	<2	20	.11	<.2	<.2	22	.25	.033	4	17	.57	120	.04	<3	1.16	.01	.06	<2	<.2	<10	<.3	<.2	3.1	4
12046	.9	135.7	2.1	66.4	186	11	3	562	.65	1.1	<5	<2	428	.39	.2	<.2	8	30.44	.098	<1	46	.31	179	.01	15	.33	.02	.04	<2	.4	<10	.6	<.2	3.1	1
12047	1.2	54.6	4.0	139.0	107	14	8	711	1.75	3.1	5	<2	22	.14	.4	<.2	29	.37	.068	6	24	.57	71	.05	<3	1.10	.01	.06	<2	<.2	<10	<.3	<.2	3.2	1
12048	1.9	373.3	3.6	631.0	626	28	8	1126	1.17	2.1	<5	<2	432	1.55	.2	.2	19	16.62	.344	4	24	.42	336	.02	22	1.02	.02	.11	<2	<.2	27	.6	<.2	2.0	2
12049	1.7	270.5	2.7	227.3	753	25	5	703	1.10	1.4	<5	<2	276	1.71	.2	1.1	12	16.31	.115	3	35	.33	185	.01	12	1.00	.02	.08	<2	<.2	30	.8	<.2	2.4	1
12050	1.5	63.4	2.3	103.4	177	12	8	349	1.97	1.5	8	2	19	.15	.2	<.2	30	.32	.050	5	21	.69	32	.05	<3	1.20	.01	.04	<2	<.2	<10	<.3	<.2	3.7	4
12051	.6	19.3	2.8	83.0	128	9	5	227	1.23	.8	<5	<2	18	.06	.2	<.2	25	.24	.033	5	19	.42	68	.05	3	.97	.01	.04	<2	<.2	<10	<.3	<.2	3.1	3
12052	.4	21.1	2.8	79.1	101	10	5	247	1.22	<.5	<5	<2	19	.04	<.2	<.2	22	.25	.036	5	17	.52	55	.05	<3	1.01	.01	.04	<2	<.2	<10	<.3	<.2	2.8	51
12053	.4	17.3	2.6	93.6	56	10	5	332	1.20	.5	6	2	17	.03	<.2	<.2	23	.23	.033	4	15	.48	62	.05	<3	.95	.01	.05	<2	<.2	<10	<.3	<.2	2.8	1
12054	.5	12.5	2.9	149.2	160	10	5	293	1.23	<.5	7	<2	15	.12	.2	<.2	24	.21	.032	4	17	.41	92	.05	<3	.94	.01	.04	<2	<.2	<10	<.3	<.2	3.1	3
12055	.6	18.8	2.7	111.5	122	11	6	283	1.52	.8	6	<2	17	.06	.2	<.2	30	.22	.043	4	17	.55	72	.06	<3	1.10	.01	.04	<2	<.2	<10	<.3	<.2	3.1	<1
12056	.3	12.2	2.5	90.8	81	8	5	238	1.24	.6	<5	<2	15	.06	<.2	<.2	23	.20	.027	3	15	.45	66	.05	<3	.92	.01	.04	<2	<.2	<10	<.3	<.2	2.9	12
RE 12056	.5	13.3	2.5	92.0	102	9	5	248	1.31	.5	<5	<2	16	.06	.2	<.2	25	.22	.028	4	15	.48	67	.06	<3	.97	.01	.04	<2	<.2	16	<.3	<.2	2.9	6
12057	.6	21.2	2.5	94.4	53	12	7	285	1.58	.7	6	2	19	.05	.2	<.2	30	.24	.047	5	20	.54	62	.06	<3	1.10	.01	.05	<2	<.2	<10	<.3	<.2	3.2	6
12058	.4	13.0	2.3	83.3	45	10	6	234	1.34	.5	<5	2	15	.04	.2	<.2	26	.18	.046	4	19	.42	43	.05	<3	.95	.01	.04	<2	<.2	<10	<.3	<.2	2.6	3
12059	.6	10.8	2.8	120.8	85	9	5	302	1.26	<.5	<5	<2	15	.06	<.2	<.2	25	.21	.051	4	19	.37	72	.05	<3	.96	.01	.06	<2	<.2	11	<.3	<.2	2.9	4
12060	.6	18.1	2.3	68.6	93	10	6	234	1.33	.7	6	<2	14	.04	.2	<.2	26	.18	.039	4	17	.45	43	.05	<3	.93	<.01	.03	<2	<.2	10	<.3	<.2	3.2	17
12061	.7	78.9	3.6	133.0	61	23	11	500	2.35	1.7	<5	2	24	.12	.4	<.2	39	.36	.041	7	29	.70	60	.05	<3	1.46	.01	.08	<2	<.2	12	<.3	<.2	4.0	4
12062	1.1	56.4	4.1	201.2	417	27	12	688	2.74	.9	<5	2	105	.29	<.2	<.2	31	2.38	.027	9	35	.96	117	.04	3	1.68	.02	.13	<2	<.2	23	.4	<.2	4.3	1
12063	.7	37.1	3.3	237.3	52	16	9	583	2.22	1.2	<5	2	24	.16	.2	<.2	36	.32	.027	5	30	.59	67	.05	<3	1.42	.01	.08	<2	<.2	17	<.3	<.2	3.6	3
12064	.5	10.9	2.4	174.3	78	10	6	358	1.45	<.5	10	<2	18	.14	<.2	<.2	27	.23	.025	4	20	.51	70	.06	<3	1.02	.01	.05	<2	<.2	<10	<.3	<.2	3.3	8
12065	.5	12.7	2.3	237.9	43	10	7	394	1.56	.5	<5	<2	17	.15	<.2	<.2	28	.21	.024	4	18	.58	46	.05	<3	1.05	.01	.05	<2	<.2	<10	<.3	<.2	3.0	1
12066	.6	18.6	3.3	162.6	85	13	7	446	1.75	.7	<5	<2	23	.12	.2	<.2	36	.30	.016	5	24	.51	59	.07	<3	1.08	.01	.09	<2	<.2	<10	<.3	<.2	3.1	1
12067	.4	11.5	3.7	429.9	184	11	7	681	1.78	.5	<5	<2	18	.29	.2	<.2	28	.25	.043	5	19	.61	93	.05	<3	1.21	.01	.09	<2	<.2	13	<.3	<.2	3.4	3
12068	1.6	10.1	5.6	102.9	76	11	9	583	2.11	.6	<5	<2	17	.03	<.2	<.2	30	.17	.012	3	13	1.05	35	.02	<3	1.64	.01	.02	<2	<.2	<10	<.3	<.2	3.8	10
12101	.7	6.8	2.8	257.4	98	7	4	539	1.04	<.5	6	<2	11	.24	<.2	<.2	23	.15	.023	4	16	.29	78	.05	<3	.82	.01	.04	<2	<.2	<10	<.3	<.2	2.9	2
12102	.8	16.9	2.4	234.8	201	12	6	391	1.29	.6	<5	<2	12	.25	.2	<.2	29	.21	.057	4	22	.30	92	.05	<3	.96	.01	.04	<2	<.2	21	<.3	<.2	3.2	1
12103	.7	12.7	2.6	206.3	91	7	4	404	1.12	<.5	6	<2	12	.24	<.2	<.2	25	.17	.022	4	13	.33	65	.06	<3	.79	.01	.04	<2	<.2	<10	<.3	<.2	2.5	2
12104	1.4	45.8	4.1	723.6	234	16	8	819	1.92	.9	10	2	23	.63	<.2	<.2	33	.35	.064	6	21	.42	173	.05	<3	1.37	.01	.08	<2	<.2	43	<.3	<.2	4.4	<1
12105	1.1	32.3	4.4	1174.9	234	19	9	1137	2.25	1.0	7	2	20	.77	.2	<.2	38	.28	.052	5	24	.44	284	.05	<3	1.64	.01	.07	<2	<.2	27	<.3	.2	4.9	1
12106	1.1	22.6	3.8	942.5	284	14	9	1571	1.97	1.4	<5	<2	21	1.12	<.2	<.2	36	.25	.044	5	23	.38	294	.05	<3	1.33	.01	.04	<2	<.2	24	<.3	.2	3.9	27
12107	1.2	62.3	4.6	779.3	196	23	11	401	1.90	<.5	5	<2	24	2.36	<.2	.2	34	.41	.023	5	19	.63	75	.04	<3	1.25	.01	.05	<2	<.2	34	<.3	.2	4.2	2
12108	2.0	40.5	6.0	743.5	440	12	10	640	2.00	.6	6	<2	16	1.12	.2	<.2	38	.23	.036	4	21	.46	70	.05	<3	1.38	.01	.06	<2	<.2	29	<.3	.2	4.5	2
STANDARD	25.2	124.3	104.0	269.9	2075	32	18	1060	4.96	78.6	26	21	61	2.03	8.8	19.5	71	.66	.115	18	58	1.14	284	.11	26	2.40	.05	.72	17	2.5	1026	.4	2.3	7.3	52

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA ____

Crest Geological Consulting PROJECT 178 FILE # 9801731

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12109	.7	13.2	2.5	122.1	58	8	5	576	1.03	.6	7	<2	11	.13	<.2	<.2	27	.18	.029	4	15	.27	84	.05	3	.71	.01	.03	<2	.2	15	<.3	<.2	1.8	<1
12110	.4	10.6	3.6	127.1	89	10	5	517	1.19	.9	5	<2	14	.15	<.2	<.2	30	.21	.036	4	20	.29	96	.05	4	.83	.01	.03	<2	<.2	<10	<.3	<.2	2.6	<1
12111	.5	6.0	3.0	158.9	79	8	4	540	1.02	.7	<5	2	14	.15	<.2	<.2	26	.22	.028	4	13	.26	87	.05	4	.75	.01	.04	<2	<.2	16	<.3	<.2	2.2	<1
12112	.9	39.0	6.4	95.7	121	23	9	424	2.20	3.1	<5	<2	21	.11	.3	<.2	47	.33	.052	6	36	.58	52	.07	<3	1.25	.01	.07	<2	<.2	14	<.3	<.2	3.0	<1
12113	1.7	14.1	4.1	53.3	100	6	4	169	1.00	1.6	<5	<2	32	.06	<.2	<.2	24	.35	.007	2	11	.46	45	.01	<3	.95	.01	.01	<2	<.2	22	<.3	<.2	2.8	<1
12114	1.0	6.9	2.4	82.1	35	5	4	273	.90	<.5	<5	<2	11	.03	<.2	<.2	23	.15	.010	4	13	.32	33	.03	3	.76	.01	.02	<2	<.2	<10	<.3	<.2	2.2	<1
12115	1.4	53.2	3.9	537.9	182	21	10	1279	2.21	1.1	<5	<2	28	.72	<.2	<.2	37	.41	.082	5	26	.54	203	.04	<3	1.34	.01	.04	<2	<.2	19	<.3	<.2	3.4	1
12116	2.1	40.4	5.0	825.7	305	17	11	1525	2.18	1.5	6	<2	31	1.73	.2	<.2	36	.51	.107	5	24	.41	197	.04	<3	1.33	.01	.05	<2	<.2	32	<.3	<.2	3.8	4
12117	3.2	36.7	5.8	720.8	274	17	14	1655	2.61	1.9	<5	<2	32	1.06	.2	<.2	44	.59	.085	6	28	.44	149	.04	<3	1.45	.01	.06	<2	<.2	23	<.3	<.2	4.3	<1
12118	3.3	35.7	4.5	306.7	94	12	10	778	2.11	1.5	<5	<2	25	.70	.2	<.2	47	.53	.026	4	28	.43	60	.05	3	1.05	.01	.05	<2	<.2	12	<.3	<.2	3.0	2
12119	1.8	20.7	4.0	251.2	199	9	7	911	1.37	.6	<5	<2	14	.27	<.2	<.2	33	.20	.022	4	21	.32	120	.04	3	.93	.01	.04	<2	<.2	21	<.3	<.2	3.0	1
12120	.9	11.7	3.6	132.9	90	7	4	387	1.10	.6	<5	2	14	.13	<.2	<.2	24	.20	.038	4	17	.37	79	.04	4	.86	.01	.03	<2	<.2	11	<.3	<.2	2.9	1
12121	.5	6.8	2.7	86.1	100	7	4	372	1.02	.5	<5	<2	15	.07	<.2	<.2	26	.20	.033	4	16	.32	64	.05	<3	.78	.01	.03	<2	<.2	<10	<.3	<.2	2.5	1
12122	.3	5.6	2.6	133.6	94	8	5	457	1.03	.6	<5	<2	13	.12	<.2	<.2	26	.20	.034	4	14	.30	78	.05	<3	.86	.01	.03	<2	<.2	21	<.3	<.2	2.2	1
12123	.5	10.1	3.4	116.5	53	12	6	378	1.28	1.0	5	2	14	.12	<.2	<.2	30	.23	.059	4	23	.31	90	.04	5	.98	.01	.04	<2	<.2	<10	<.3	<.2	2.8	<1
12124	2.1	89.0	5.1	489.7	154	22	11	915	2.75	2.1	5	2	41	.87	.2	<.2	45	.82	.061	5	38	.51	130	.05	5	1.34	.01	.09	<2	<.2	34	<.3	<.2	3.1	1
12125	1.8	168.1	5.5	589.7	369	25	16	2630	3.85	3.3	6	<2	138	1.51	<.2	.2	51	3.20	.162	7	29	.42	292	.03	15	1.26	.02	.13	<2	<.2	51	.4	<.2	3.3	4
12126	1.2	21.0	5.7	218.1	184	13	7	868	1.44	.8	<5	2	24	.33	.2	<.2	29	.36	.052	6	21	.40	152	.05	5	1.05	.01	.07	<2	.2	15	<.3	<.2	3.4	2
12127	.9	122.8	4.7	97.9	287	23	12	817	1.79	1.4	<5	<2	32	.12	.2	<.2	35	.37	.040	13	31	.46	135	.04	<3	1.73	.01	.07	<2	<.2	27	<.3	<.2	3.9	1
12128	1.3	119.6	5.0	128.7	298	28	13	792	2.19	1.8	<5	<2	36	.12	.3	.2	48	.42	.052	12	35	.49	161	.04	<3	1.95	.01	.08	<2	<.2	32	<.3	<.2	5.0	<1
RE 12129	1.0	100.2	4.1	101.0	386	24	12	788	1.85	1.8	<5	<2	32	.08	.2	<.2	41	.37	.042	11	34	.49	137	.04	<3	1.77	.01	.08	<2	<.2	42	<.3	<.2	4.6	1
12129	.9	100.9	4.2	100.5	369	24	12	771	1.85	1.6	<5	<2	31	.08	.2	<.2	41	.37	.041	11	33	.49	137	.04	3	1.76	.01	.08	<2	<.2	31	<.3	<.2	4.5	<1
12130	1.2	135.0	3.9	138.7	390	33	12	1034	2.32	1.4	<5	<2	40	.16	.2	<.2	48	.45	.047	12	39	.54	181	.04	3	2.11	.02	.10	<2	<.2	35	<.3	<.2	4.9	2
12131	.9	67.5	3.3	95.0	239	21	11	691	1.48	.9	<5	2	28	.11	.2	<.2	35	.35	.027	9	28	.44	114	.05	5	1.42	.01	.07	<2	<.2	28	<.3	<.2	3.4	1
12132	.5	34.2	2.7	44.2	76	10	4	245	.93	.6	<5	2	22	.04	<.2	<.2	23	.28	.019	5	17	.36	49	.05	4	.88	.01	.04	<2	<.2	<10	<.3	<.2	2.6	3
12133	1.0	127.6	3.9	98.4	353	27	10	870	1.87	1.3	<5	<2	41	.17	.4	.2	36	.53	.035	14	32	.51	144	.04	3	1.63	.01	.09	<2	<.2	35	<.3	<.2	4.1	2
12134	1.6	261.1	5.3	171.5	573	53	14	1049	3.65	2.9	<5	<2	59	.29	.5	.5	53	.89	.069	20	55	.71	290	.04	4	3.02	.02	.17	<2	<.2	59	<.3	<.2	7.2	<1
12135	1.1	194.6	4.5	128.7	471	40	10	587	2.56	1.4	<5	<2	45	.24	.3	1.3	39	.59	.043	11	41	.61	182	.05	3	2.25	.02	.15	<2	<.2	19	<.3	<.2	5.6	<1
12136	1.3	96.3	3.2	83.0	203	20	8	516	1.62	1.3	<5	<2	28	.12	.3	.2	33	.38	.029	7	23	.49	93	.04	4	1.34	.01	.06	<2	<.2	16	<.3	<.2	3.9	<1
12137	.6	105.1	3.2	81.4	217	18	7	426	1.35	1.1	<5	2	27	.09	.2	<.2	33	.36	.021	8	24	.35	96	.05	3	1.20	.01	.06	<2	<.2	14	<.3	<.2	3.3	1
12138	.6	48.6	2.3	51.4	62	11	4	303	.85	.5	9	2	20	.03	.2	<.2	20	.29	.025	5	16	.31	50	.04	6	.82	.01	.04	<2	<.2	10	<.3	<.2	2.2	<1
12139	.5	45.8	2.2	53.8	100	11	4	306	.87	.7	7	3	19	.04	.2	<.2	22	.26	.020	6	15	.28	54	.05	6	.82	.01	.04	<2	<.2	<10	<.3	<.2	2.3	<1
12140	.4	38.3	3.0	47.0	65	9	4	204	.78	<.5	6	2	19	.03	<.2	<.2	19	.27	.021	5	16	.29	44	.05	5	.78	.01	.04	<2	<.2	24	<.3	<.2	2.3	<1
12141	.6	52.2	2.9	72.8	125	13	5	265	1.08	.9	5	2	24	.07	.2	<.2	27	.35	.025	6	20	.32	77	.04	6	.98	.01	.05	<2	<.2	20	<.3	.2	3.1	2
STANDARD	24.1	120.3	102.2	259.7	1953	31	17	998	4.69	71.3	25	17	57	1.85	9.3	19.9	76	.67	.107	17	56	1.09	212	.11	25	2.27	.05	.69	16	2.5	982	.3	1.9	7.2	54

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA ____

Crest Geological Consulting PROJECT 178 FILE # 9801731

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Tl	Hg	Se	Te	Ga	Au*
	ppm	ppm	ppm	ppm	ppb	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	ppm	ppb	ppm	ppm	ppm	ppb
12142	.7	45.5	2.9	57.6	57	12	5	350	1.08	.8	9	<2	19	.06	.2	<.2	27	.27	.025	6	20	.32	67	.04	<3	.88	.01	.05	<2	<.2	21	<.3	<.2	2.5	<1
12143	1.1	76.8	3.3	95.8	85	20	8	607	1.50	1.0	7	<2	23	.14	.2	<.2	35	.30	.031	7	24	.39	91	.05	<3	1.26	.01	.06	<2	<.2	18	<.3	<.2	3.2	<1
12144	1.0	83.0	3.4	165.9	128	25	7	1050	1.64	.5	<5	<2	28	.39	<.2	<.2	31	.33	.065	11	27	.36	179	.04	<3	1.38	.01	.10	<2	<.2	18	<.3	<.2	3.3	<1
12145	1.5	99.4	4.3	87.2	218	19	7	623	1.46	2.2	5	<2	26	.18	.3	<.2	34	.42	.031	10	25	.35	79	.04	<3	1.07	.01	.06	<2	<.2	27	<.3	<.2	3.1	1
12146	2.0	27.6	3.7	120.8	150	9	5	1027	1.07	1.4	<5	<2	27	.25	<.2	<.2	22	.42	.096	4	18	.21	161	.03	5	.76	.01	.06	<2	<.2	27	<.3	<.2	2.9	<1
12147	.7	20.4	3.6	54.6	93	9	5	397	1.06	.8	<5	2	20	.12	<.2	<.2	29	.32	.032	4	18	.19	54	.04	5	.73	.01	.08	<2	<.2	13	<.3	<.2	2.6	2
12148	1.4	258.2	3.7	78.4	252	32	8	590	2.17	2.7	<5	<2	49	.15	.2	.9	37	.90	.056	14	43	.46	139	.03	4	1.84	.01	.08	<2	<.2	38	.5	<.2	3.7	2
12149	1.7	407.8	5.0	98.5	574	59	12	818	3.29	3.5	<5	2	69	.39	.4	<.2	41	1.15	.072	16	64	.63	298	.03	5	2.77	.02	.13	<2	<.2	41	.5	.2	5.9	3
12150	1.8	1074.3	5.0	146.2	1111	68	15	1100	3.09	3.2	<5	<2	86	.96	.5	.4	39	1.76	.112	27	56	.58	334	.03	5	2.48	.03	.13	<2	<.2	73	.6	.3	5.0	2
12151	1.2	21.2	3.9	55.6	57	7	5	459	1.08	1.0	<5	<2	18	.08	<.2	<.2	26	.34	.015	4	17	.27	58	.04	<3	.79	.01	.05	<2	<.2	10	<.3	<.2	2.3	2
12152	1.7	32.4	3.2	50.5	61	8	5	396	1.12	.6	<5	2	14	.07	.2	<.2	28	.22	.013	4	18	.30	54	.04	<3	.78	.01	.03	<2	<.2	<10	<.3	<.2	2.7	3
12153	2.1	33.9	3.1	43.4	106	9	5	240	1.19	1.5	<5	<2	16	.06	.2	<.2	29	.23	.015	4	17	.32	41	.04	<3	.80	.01	.05	<2	.2	<10	<.3	<.2	2.8	<1
12154 N.S.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
12155	1.7	36.9	3.3	84.3	93	8	5	254	1.15	.6	10	<2	17	.14	.2	<.2	26	.26	.058	4	14	.34	55	.04	<3	.81	.01	.04	<2	<.2	12	<.3	<.2	2.5	<1
12156	.9	13.9	3.4	71.1	137	7	4	164	1.04	.7	11	<2	12	.08	<.2	<.2	26	.18	.060	4	16	.23	62	.04	<3	.85	.01	.03	<2	<.2	<10	<.3	<.2	2.7	<1
12157	.9	15.5	3.3	77.6	68	9	4	261	1.16	.6	<5	<2	16	.12	.2	<.2	28	.25	.047	5	19	.30	84	.05	<3	.84	.01	.05	<2	<.2	11	<.3	<.2	2.9	1
12158	.6	10.0	2.9	54.4	75	7	4	242	1.04	.6	<5	<2	14	.06	<.2	<.2	25	.19	.023	4	14	.31	74	.05	<3	.83	.01	.04	<2	<.2	<10	<.3	<.2	2.5	<1
12159	1.0	13.0	3.2	102.9	169	7	5	501	.98	.8	<5	2	13	.11	<.2	<.2	26	.20	.057	4	18	.23	83	.04	<3	.89	.01	.04	<2	<.2	<10	<.3	<.2	2.9	<1
12160	.6	25.3	2.7	63.4	106	11	5	226	1.24	1.0	5	2	15	.08	.2	<.2	27	.24	.040	5	19	.45	45	.05	4	.95	.01	.04	<2	<.2	<10	<.3	<.2	2.6	<1
12161	.8	25.9	2.7	66.7	149	9	5	209	1.14	.6	<5	<2	14	.15	<.2	<.2	25	.24	.060	4	17	.33	57	.04	<3	.82	.01	.03	<2	<.2	15	<.3	<.2	2.5	<1
12162	.5	12.2	2.4	81.4	65	8	5	259	1.20	.5	<5	<2	16	.06	<.2	<.2	25	.23	.042	5	14	.40	62	.05	<3	.89	.01	.04	<2	<.2	<10	<.3	<.2	2.5	<1
12163	1.1	12.3	2.5	34.4	<30	5	5	261	1.08	<.5	5	<2	22	.02	<.2	<.2	22	.33	.009	4	8	.48	48	.05	<3	.87	.01	.05	<2	<.2	<10	<.3	<.2	3.0	<1
12164	1.5	37.2	2.6	181.3	185	5	4	413	.89	.5	<5	<2	14	.20	<.2	<.2	20	.21	.026	3	8	.28	69	.04	<3	.69	.01	.04	<2	<.2	17	<.3	<.2	2.5	<1
12165	.7	10.6	2.0	79.7	73	4	3	327	.67	<.5	5	<2	11	.10	<.2	<.2	15	.17	.016	3	9	.23	38	.03	<3	.54	.01	.03	<2	<.2	<10	<.3	<.2	1.9	<1
12166	.8	26.5	2.4	108.3	70	7	5	391	1.09	<.5	<5	<2	13	.12	<.2	<.2	20	.17	.020	4	9	.43	70	.03	<3	.90	.01	.04	<2	<.2	<10	<.3	<.2	2.3	3
12167	1.0	28.3	2.6	94.8	137	10	6	404	1.39	.9	<5	<2	19	.11	.2	<.2	28	.26	.029	5	17	.47	77	.05	<3	1.03	.01	.05	<2	<.2	17	<.3	<.2	2.9	2
12168	1.0	11.8	1.9	41.5	47	6	4	203	.99	1.4	<5	<2	11	.02	<.2	<.2	23	.16	.013	3	12	.30	33	.04	<3	.68	.01	.03	<2	<.2	<10	<.3	<.2	2.1	<1
12169	1.4	13.7	3.1	41.3	99	5	4	186	.93	.5	10	<2	17	.04	<.2	<.2	21	.23	.010	3	13	.37	45	.04	<3	.76	.01	.05	<2	.2	<10	<.3	<.2	3.4	1
12170	1.4	18.4	2.5	57.9	63	7	5	281	1.21	<.5	6	<2	22	.02	<.2	<.2	25	.23	.007	4	15	.47	85	.04	<3	.98	.01	.05	<2	<.2	18	<.3	<.2	2.7	<1
12171	.8	120.5	4.2	62.3	248	16	8	225	1.86	1.2	<5	<2	56	.13	.2	<.2	29	.89	.019	12	22	.57	113	.04	3	1.42	.02	.08	<2	<.2	28	.4	<.2	4.1	<1
12172	1.5	118.0	1.6	98.0	556	8	2	954	.26	1.2	<5	<2	481	1.28	.4	<.2	6	26.68	.184	2	5	.43	171	.01	14	.24	.03	.02	<2	<.2	36	1.1	.2	1.3	2
12173	.8	14.4	3.3	84.0	109	7	5	218	1.11	<.5	8	<2	18	.08	<.2	<.2	23	.33	.022	4	12	.40	71	.04	<3	.95	.01	.04	<2	<.2	<10	<.3	<.2	3.0	<1
12174	.6	10.2	2.3	118.5	78	7	5	321	1.21	<.5	9	<2	16	.09	<.2	<.2	22	.23	.026	4	15	.49	62	.05	<3	.90	.01	.06	<2	<.2	10	<.3	<.2	2.6	18
STANDARD D	24.8	119.9	100.7	265.4	1861	31	18	1023	4.75	74.8	30	19	59	1.87	11.3	20.0	76	.69	.110	17	57	1.12	233	.11	29	2.32	.05	.70	16	2.2	987	<.3	1.8	6.3	44

Standard is STANDARD D2/C3/AU-S.

Data ___ FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12175	.5	17.4	2.0	126.9	104	7	5	360	1.16	.7	<5	<2	14	.04	<.2	<.2	20	.21	.041	3	11	.42	71	.03	<3	.89	.01	.05	<2	<.2	17	<.3	<.2	2.7	1
12176	.5	14.5	2.7	148.2	92	8	5	349	1.09	<.5	<5	<2	14	.06	<.2	<.2	20	.22	.027	4	12	.40	71	.04	<3	.80	.01	.06	<2	<.2	<10	<.3	<.2	2.8	4
12177	.5	12.4	1.9	83.2	79	6	5	400	1.04	<.5	<5	<2	11	.01	<.2	<.2	15	.13	.015	2	9	.52	63	.02	3	.87	.01	.05	<2	<.2	<10	<.3	<.2	2.4	<1
12178	1.3	39.1	1.8	130.0	149	7	6	424	1.23	.5	<5	<2	14	.06	<.2	<.2	18	.19	.027	3	10	.54	40	.03	<3	.83	.01	.07	<2	<.2	14	<.3	<.2	2.5	3
12179	1.5	31.1	4.7	400.8	141	16	11	1089	2.26	.7	<5	<2	22	.46	<.2	<.2	43	.37	.054	5	25	.39	169	.05	<3	1.27	.01	.08	<2	<.2	10	<.3	<.2	3.8	<1
12180	1.2	33.5	3.2	159.5	202	13	11	583	1.81	1.7	<5	<2	14	.13	<.2	<.2	35	.22	.044	4	23	.51	70	.04	<3	1.05	.01	.04	<2	<.2	21	<.3	<.2	3.1	1
12181	1.1	20.5	2.6	65.1	225	8	6	218	1.30	.6	5	<2	129	.17	<.2	<.2	17	2.78	.017	3	11	.62	66	.02	<3	.90	.03	.06	<2	<.2	18	<.3	<.2	2.4	<1
12182	1.2	11.6	4.2	171.2	165	7	5	308	1.11	<.5	<5	<2	13	.07	<.2	<.2	25	.17	.012	3	10	.44	61	.02	<3	.98	.01	.01	<2	<.2	<10	<.3	<.2	3.1	<1
12183	.6	7.8	3.7	224.7	158	6	4	443	.93	<.5	<5	2	10	.16	<.2	<.2	19	.15	.033	3	12	.31	59	.03	3	.77	.01	.02	<2	<.2	<10	<.3	<.2	2.2	3
12184	.5	10.4	3.8	135.9	105	8	5	559	1.14	.8	<5	<2	11	.11	.2	<.2	22	.18	.042	4	16	.38	61	.03	<3	.82	.01	.03	<2	<.2	<10	<.3	<.2	2.9	1
12185	.9	11.4	3.6	160.2	130	9	6	591	1.38	<.5	6	<2	19	.13	<.2	<.2	26	.36	.054	4	18	.35	83	.03	<3	.95	.01	.04	<2	<.2	<10	<.3	<.2	3.0	<1
RE 12185	.9	12.4	3.8	168.5	150	10	7	589	1.45	<.5	<5	<2	20	.13	<.2	<.2	27	.37	.056	4	18	.36	86	.03	<3	1.00	.01	.04	<2	<.2	<10	<.3	<.2	3.3	<1
12186	4.1	38.6	4.7	190.1	152	17	10	1932	2.01	1.6	7	2	37	.28	.2	<.2	37	.79	.065	5	31	.36	128	.04	6	1.17	.01	.05	<2	<.2	30	<.3	<.2	3.7	<1
12187	1.2	17.6	6.6	320.4	133	12	8	428	1.66	.9	<5	<2	19	.21	<.2	<.2	32	.31	.059	4	22	.35	111	.04	<3	1.08	.01	.05	<2	<.2	21	<.3	<.2	3.3	4
12201	.8	17.8	2.2	149.0	113	9	5	278	1.32	.7	<5	<2	13	.06	.2	<.2	24	.17	.022	4	14	.46	45	.05	<3	.90	.01	.03	<2	<.2	<10	<.3	<.2	3.0	3
12202	.6	9.4	2.2	181.6	85	6	4	386	.96	<.5	<5	<2	15	.11	<.2	<.2	18	.22	.038	3	10	.33	84	.03	<3	.73	.01	.04	<2	<.2	<10	<.3	<.2	2.3	1
12203	.7	13.4	2.4	173.0	183	8	5	306	1.27	.6	<5	<2	18	.08	<.2	<.2	23	.27	.030	4	16	.44	58	.04	<3	.93	.01	.05	<2	<.2	<10	<.3	<.2	2.9	3
12204	.6	114.8	3.1	153.2	314	13	7	342	1.85	.9	6	<2	31	.10	.2	<.2	23	.52	.025	5	24	.55	75	.04	<3	1.23	.01	.07	<2	<.2	20	<.3	<.2	3.5	3
12205	.6	22.5	2.9	58.3	62	13	8	400	1.57	1.0	<5	<2	20	.06	.2	<.2	33	.27	.033	6	23	.42	57	.07	<3	.88	.01	.09	<2	<.2	14	<.3	<.2	2.8	2
12206	.8	32.8	2.4	117.0	99	11	6	316	1.48	.5	<5	2	16	.08	.2	<.2	26	.20	.050	5	18	.51	62	.04	3	1.04	.01	.04	<2	<.2	<10	<.3	<.2	3.0	3
12207	.9	16.3	2.4	142.0	123	7	5	387	1.04	<.5	<5	<2	14	.07	<.2	<.2	20	.20	.024	4	12	.37	73	.04	<3	.84	.01	.04	<2	<.2	<10	<.3	<.2	2.8	2
12208	.7	16.3	3.0	152.8	183	9	5	258	1.10	<.5	<5	<2	15	.09	<.2	<.2	21	.21	.029	5	15	.37	88	.04	3	.93	.01	.05	<2	<.2	<10	<.3	<.2	3.2	1
12209	.7	10.4	2.6	96.4	155	6	5	247	1.12	<.5	<5	<2	13	.06	<.2	<.2	21	.16	.040	4	13	.36	72	.04	<3	.90	.01	.04	<2	<.2	<10	<.3	<.2	3.0	2
12210	.9	76.6	2.5	88.9	111	15	7	409	1.74	1.4	6	2	20	.06	.3	<.2	31	.32	.052	6	25	.55	58	.05	3	1.10	.01	.05	<2	<.2	<10	<.3	<.2	3.1	3
12211	.4	48.5	2.3	63.1	114	12	4	213	1.03	.5	<5	<2	17	.03	.2	<.2	23	.21	.024	6	15	.30	77	.04	<3	.91	.01	.03	<2	<.2	12	<.3	<.2	2.3	2
12212	.5	32.3	2.7	45.6	36	9	4	205	.93	<.5	<5	<2	18	.01	.2	<.2	22	.23	.015	6	13	.34	55	.05	3	.82	.01	.03	<2	<.2	<10	<.3	<.2	2.5	1
12213	1.1	97.7	3.7	80.2	171	18	9	523	1.48	.9	<5	<2	24	.04	.2	<.2	34	.30	.026	8	27	.39	111	.03	3	1.40	.01	.05	<2	<.2	21	<.3	<.2	4.0	<1
12214	.4	26.0	2.6	42.1	55	7	3	194	.86	<.5	<5	<2	16	<.01	<.2	<.2	21	.23	.021	5	14	.35	44	.04	<3	.75	.01	.02	<2	<.2	<10	<.3	<.2	2.4	<1
12215	.3	25.8	2.8	49.3	55	8	3	161	.82	<.5	<5	<2	16	.01	<.2	<.2	21	.19	.013	5	11	.25	70	.04	<3	.78	.01	.03	<2	<.2	<10	<.3	<.2	2.7	4
12216	.5	33.9	2.9	68.5	<30	11	5	201	1.07	.5	<5	<2	17	.03	<.2	<.2	26	.23	.018	5	14	.33	75	.05	<3	.95	.01	.04	<2	<.2	<10	<.3	<.2	2.8	<1
12217	.8	26.4	3.0	68.2	218	12	5	171	1.31	.8	5	<2	16	.07	.3	<.2	31	.23	.036	5	20	.29	80	.04	3	.99	.01	.04	<2	<.2	12	<.3	<.2	3.4	<1
12218	.6	37.1	2.4	52.5	97	10	4	175	1.06	.9	<5	2	14	.04	<.2	<.2	27	.19	.021	5	17	.30	65	.04	3	.83	.01	.03	<2	<.2	<10	<.3	<.2	2.5	1
12219	.5	38.4	2.4	61.7	93	11	4	193	.98	<.5	<5	<2	16	.04	.2	<.2	23	.21	.019	5	15	.30	69	.04	<3	.82	.01	.03	<2	<.2	<10	<.3	<.2	2.6	1
12220	.6	30.8	2.5	61.5	109	10	5	231	.96	.5	<5	<2	14	.04	.2	<.2	23	.21	.023	5	17	.27	51	.04	3	.73	.01	.03	<2	<.2	11	<.3	<.2	2.6	<1
STANDARD	24.9	121.2	100.3	267.7	2054	31	18	1015	4.69	78.0	22	19	59	2.00	11.3	21.5	70	.68	.110	17	56	1.10	233	.11	26	2.27	.05	.70	17	2.5	965	.3	1.9	7.3	46

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data ___ FA ____

ACME ANALYTICAL

Crest Geological Consulting PROJECT 178 FILE # 9801731

ACME ANALYTICAL

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Tl	Hg	Se	Te	Ga	Au*
	ppm	ppm	ppm	ppm	ppb	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	ppm	ppb	ppm	ppm	ppm	ppb
12221	.6	58.4	3.3	72.4	165	14	6	295	1.21	.7	<5	<2	20	.04	.2	<.2	27	.25	.022	6	17	.38	72	.05	<3	1.08	.01	.04	<2	<.2	14	<.3	<.2	2.9	<1
12222	1.1	43.8	3.6	149.7	133	18	7	358	1.79	1.0	<5	<2	26	.14	.2	<.2	32	.38	.178	5	25	.33	146	.04	<3	1.36	.01	.06	<2	<.2	28	<.3	<.2	3.7	1
12223	1.5	154.1	4.6	140.6	385	43	15	1018	2.91	2.5	9	<2	35	.12	.3	<.2	51	.40	.052	12	46	.63	190	.04	<3	2.49	.02	.12	<2	<.2	41	<.3	<.2	5.8	6
12224	.9	70.0	3.3	90.4	137	20	8	451	1.52	1.2	5	<2	23	.07	.2	<.2	35	.28	.025	6	25	.41	89	.05	<3	1.33	.01	.06	<2	<.2	28	<.3	<.2	3.5	<1
12225	.8	67.9	3.6	89.0	144	20	9	480	1.54	1.0	8	<2	26	.06	.2	<.2	31	.32	.028	8	24	.44	96	.05	<3	1.41	.01	.07	<2	<.2	23	<.3	<.2	4.2	1
12226	.7	41.8	3.7	62.3	128	12	6	300	1.14	1.3	<5	<2	20	.06	.2	<.2	27	.26	.016	5	19	.35	62	.05	<3	.96	.01	.05	<2	<.2	19	<.3	<.2	2.6	2
12227	.9	142.5	3.9	124.3	322	36	11	788	2.27	1.0	<5	<2	36	.11	.3	<.2	37	.42	.042	12	39	.54	175	.03	<3	2.18	.01	.11	<2	<.2	42	<.3	<.2	4.8	2
12228	.7	21.7	4.6	124.2	170	11	5	512	1.12	1.2	8	<2	24	.25	.2	<.2	23	.35	.039	4	17	.22	136	.04	<3	.92	.01	.07	<2	<.2	19	<.3	<.2	2.7	1
12229	.6	17.1	2.9	86.1	104	11	5	214	1.24	.8	<5	<2	19	.13	<.2	<.2	28	.24	.029	6	20	.31	77	.05	<3	.93	.01	.05	<2	<.2	12	<.3	<.2	2.5	2
RE 12229	.7	17.5	2.9	82.1	100	11	5	209	1.18	.8	<5	<2	17	.12	<.2	<.2	26	.22	.028	5	17	.30	74	.05	<3	.88	.01	.05	<2	<.2	<10	<.3	<.2	2.5	1
12230	.6	31.8	2.9	87.2	201	13	5	270	1.18	.7	<5	<2	20	.14	.2	<.2	25	.30	.031	7	17	.30	67	.04	<3	.89	.01	.06	<2	<.2	24	<.3	<.2	2.4	<1
12231	1.0	68.8	3.3	114.1	208	22	7	554	1.75	1.0	6	<2	25	.14	.2	<.2	35	.36	.029	7	30	.39	95	.05	3	1.30	.01	.08	<2	<.2	25	<.3	<.2	3.5	<1
12232	.5	11.6	2.3	81.0	53	7	4	213	1.06	.5	<5	<2	19	.06	<.2	<.2	20	.24	.050	4	9	.32	62	.03	<3	.90	.01	.04	<2	<.2	<10	<.3	<.2	2.5	<1
12233	.8	36.0	2.3	69.6	84	12	5	250	1.23	.7	<5	<2	20	.04	.2	<.2	27	.27	.016	6	19	.37	57	.05	3	.90	.01	.05	<2	<.2	16	<.3	<.2	2.2	<1
12234	11.7	726.8	8.4	242.2	1295	135	21	5758	5.69	6.6	<5	2	82	.48	.7	.8	77	1.21	.104	38	97	.94	542	.03	<3	4.80	.02	.29	<2	<.2	127	.9	.2	10.1	3
12235	2.4	810.2	8.0	305.5	1722	112	19	950	6.17	5.1	5	2	90	.34	.5	1.7	65	1.29	.078	26	114	1.08	437	.04	<3	5.99	.03	.35	<2	<.2	138	.7	.2	11.8	4
12236	1.8	758.3	5.1	117.5	1077	59	11	841	2.90	2.6	<5	2	50	.75	.5	1.2	39	.79	.073	18	52	.56	208	.04	3	2.33	.02	.14	<2	<.2	60	.7	.3	5.2	2
12237	1.4	682.2	4.7	115.5	532	52	11	462	3.06	2.4	<5	<2	52	.35	.5	.6	39	.87	.066	25	55	.64	190	.04	<3	2.47	.02	.14	<2	<.2	42	.7	.3	5.3	4
12238	.9	32.2	1.6	174.4	62	12	7	425	1.51	.9	7	<2	24	.17	.2	<.2	27	.37	.083	5	14	.42	85	.04	<3	1.00	.01	.08	<2	.5	<10	.5	<.2	2.6	1
12239	.9	19.1	3.0	80.0	88	10	5	194	1.26	.6	<5	<2	15	.08	.2	<.2	27	.19	.047	5	10	.38	76	.04	<3	1.05	.01	.03	<2	<.2	<10	<.3	<.2	3.2	<1
12240	.8	16.2	3.0	127.1	92	13	6	330	1.36	.5	<5	<2	16	.07	<.2	<.2	26	.22	.065	5	17	.35	134	.04	3	1.23	.01	.05	<2	<.2	<10	<.3	<.2	3.1	3
12241	.7	10.5	2.4	68.8	57	7	5	220	1.20	.5	<5	2	14	.08	.2	<.2	27	.21	.064	5	16	.28	61	.05	<3	.83	.01	.04	<2	<.2	<10	<.3	<.2	2.5	<1
12242	2.4	152.6	3.4	123.4	177	21	9	556	2.25	2.2	<5	<2	30	.14	.4	<.2	39	.44	.062	9	29	.67	83	.06	<3	1.40	.01	.06	<2	<.2	36	.3	<.2	3.8	<1
12243	1.0	20.6	3.2	92.3	160	12	7	236	1.48	.8	<5	2	22	.09	.2	<.2	32	.35	.051	6	21	.40	102	.05	3	1.14	.01	.05	<2	<.2	24	<.3	<.2	3.0	79
12244	.7	13.6	2.7	118.2	143	9	5	251	1.23	.9	5	<2	15	.09	<.2	<.2	26	.23	.056	6	18	.36	82	.05	4	1.04	.01	.04	<2	<.2	16	<.3	<.2	2.7	<1
12245	1.2	28.9	2.7	112.3	260	10	6	310	1.47	1.0	<5	<2	16	.12	<.2	<.2	29	.23	.071	5	14	.40	82	.05	<3	1.15	.01	.04	<2	<.2	36	<.3	<.2	3.3	<1
12246	1.1	14.8	2.8	84.8	137	8	6	311	1.23	<.5	<5	<2	17	.08	<.2	<.2	29	.23	.021	4	16	.34	65	.05	<3	.91	.01	.04	<2	<.2	27	<.3	<.2	2.8	<1
12247	.4	27.4	1.6	39.3	117	10	5	313	.81	.6	<5	<2	413	.10	<.2	<.2	10	13.18	.035	3	14	.84	161	.02	<3	.58	.02	.05	<2	<.2	12	.3	<.2	1.6	<1
12248	.7	12.7	2.6	89.1	118	9	6	264	1.22	.6	<5	<2	19	.07	<.2	<.2	23	.35	.058	5	16	.41	78	.04	<3	.95	.01	.06	<2	<.2	19	<.3	<.2	2.8	<1
12249	.8	20.8	2.5	106.4	108	9	5	315	1.18	.6	<5	<2	16	.08	.2	<.2	23	.24	.040	4	14	.42	100	.04	<3	.98	.01	.05	<2	<.2	11	<.3	<.2	2.8	<1
12250	.5	10.1	2.2	102.4	105	9	5	220	1.14	.5	<5	<2	15	.08	.2	<.2	21	.20	.046	4	11	.36	114	.05	<3	.94	.01	.04	<2	<.2	13	<.3	<.2	2.6	<1
12251	.5	23.2	2.8	107.2	101	8	4	193	.99	.5	<5	<2	16	.06	<.2	<.2	19	.25	.037	4	10	.32	66	.04	<3	.87	.01	.05	<2	<.2	35	<.3	<.2	2.3	<1
12252	.5	16.1	2.3	88.0	65	10	6	296	1.40	<.5	<5	<2	16	.04	.2	<.2	25	.22	.034	4	16	.55	58	.05	<3	1.01	.01	.03	<2	<.2	10	<.3	<.2	2.6	1
12253	.6	15.5	2.6	91.2	82	11	7	290	1.46	.5	<5	<2	20	.05	<.2	<.2	27	.27	.020	5	18	.57	68	.06	<3	1.08	.01	.06	<2	.2	16	<.3	<.2	2.8	<1
STANDARD	23.7	115.9	99.6	263.8	1888	31	18	1015	4.74	77.0	33	18	65	1.87	10.6	20.3	70	.73	.110	17	57	1.11	232	.11	26	2.34	.06	.70	15	2.3	966	.7	1.8	6.4	47

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12254	.5	8.7	2.8	91.9	88	7	5	290	1.02	<.5	<5	<2	12	.06	<.2	<.2	19	.16	.015	3	7	.44	69	.04	<3	.80	.01	.04	<2	<.2	14	<.3	<.2	2.9	1
12255	.4	12.8	2.8	89.9	59	8	5	291	1.05	.5	<5	<2	12	.06	<.2	<.2	20	.20	.025	3	9	.41	66	.04	<3	.81	.01	.06	<2	<.2	12	<.3	<.2	2.7	<1
12256	.4	9.8	2.7	92.2	83	8	5	221	1.08	<.5	<5	<2	14	.09	<.2	<.2	20	.22	.037	3	10	.42	67	.04	<3	.81	.01	.07	<2	.2	10	<.3	<.2	2.6	<1
12257	.4	7.9	2.4	109.0	92	7	4	236	.98	<.5	<5	<2	11	.06	<.2	<.2	18	.16	.030	3	8	.38	81	.03	<3	.79	.01	.03	<2	<.2	<10	<.3	<.2	2.6	2
12258	.4	18.5	2.8	112.2	64	12	7	453	1.49	<.5	5	<2	16	.11	<.2	<.2	27	.19	.019	5	16	.46	82	.06	<3	.95	.01	.09	<2	<.2	<10	<.3	<.2	2.7	<1
12259	.5	18.1	3.1	100.2	80	13	8	559	1.61	<.5	<5	<2	20	.12	<.2	<.2	27	.23	.025	4	20	.50	88	.05	<3	1.09	.01	.09	<2	.2	18	<.3	<.2	3.5	1
12260	.4	16.9	2.9	68.2	103	10	6	245	1.30	<.5	<5	<2	14	.05	<.2	<.2	24	.19	.021	3	15	.43	84	.04	<3	.91	.01	.04	<2	.2	<10	<.3	<.2	2.9	3
12261	.6	9.2	4.1	89.8	121	9	5	225	1.22	1.9	<5	<2	14	.10	.2	.2	25	.23	.024	3	12	.40	63	.05	<3	.83	.01	.06	<2	<.2	10	<.3	<.2	2.8	9
12262	.6	18.9	3.4	103.6	85	12	7	350	1.54	1.3	<5	<2	14	.08	<.2	<.2	30	.23	.028	4	19	.53	47	.05	<3	1.02	.01	.05	<2	<.2	<10	<.3	<.2	2.7	4
12263	.9	17.0	3.4	361.4	186	8	5	538	1.16	<.5	<5	<2	15	.48	<.2	<.2	21	.26	.032	3	11	.39	70	.03	<3	.83	.01	.04	<2	<.2	18	<.3	<.2	2.7	40
12264	.5	14.3	3.6	309.0	88	10	7	666	1.43	.8	<5	<2	12	.26	<.2	<.2	24	.19	.041	4	15	.45	60	.04	<3	.91	.01	.05	<2	<.2	13	<.3	<.2	2.6	3
12265	.9	10.8	4.0	353.2	142	8	5	542	1.18	<.5	6	<2	13	.36	<.2	<.2	21	.21	.036	3	15	.40	58	.03	<3	.84	.01	.03	<2	<.2	10	<.3	<.2	2.8	4
12266	.9	12.6	3.7	424.5	290	8	6	725	1.24	.7	8	<2	17	.40	<.2	<.2	21	.31	.064	3	10	.39	79	.03	<3	.86	.01	.06	<2	<.2	21	<.3	<.2	2.8	2
RE 12266	.9	12.3	3.7	398.4	293	7	5	694	1.16	<.5	<5	<2	16	.41	<.2	<.2	20	.29	.063	2	11	.37	77	.03	<3	.79	.01	.05	<2	<.2	17	<.3	<.2	2.4	2
12267	.7	9.5	2.8	96.5	154	8	6	417	1.21	.5	<5	<2	10	.14	<.2	.2	25	.18	.044	3	15	.32	45	.04	<3	.71	.01	.03	<2	<.2	10	<.3	<.2	2.6	2
12268	.6	15.8	3.0	107.6	98	13	8	464	1.51	.9	6	<2	33	.14	.2	<.2	30	.75	.031	4	21	.42	68	.04	<3	.90	.01	.03	<2	<.2	22	<.3	<.2	2.4	5
12301	.9	29.3	2.7	50.7	119	12	5	178	1.21	1.0	7	<2	19	.08	.2	<.2	30	.27	.030	5	16	.31	53	.04	<3	.87	.01	.03	<2	.2	17	<.3	<.2	2.8	3
12302	.3	55.0	2.7	54.6	83	13	5	296	.95	<.5	<5	<2	16	.07	<.2	<.2	21	.22	.018	6	15	.32	60	.03	<3	.88	.01	.04	<2	<.2	31	<.3	<.2	2.3	2
12303	.6	28.6	2.9	71.7	76	11	4	194	1.07	<.5	8	<2	17	.10	<.2	<.2	26	.24	.018	5	15	.34	56	.04	<3	.87	.01	.04	<2	<.2	19	<.3	<.2	2.9	2
12304	.5	34.8	3.0	56.2	65	10	4	215	.91	<.5	<5	<2	16	.04	<.2	<.2	20	.23	.014	5	14	.33	50	.04	<3	.85	.01	.04	<2	<.2	13	<.3	<.2	2.3	3
12305	.5	42.9	2.6	55.4	132	12	5	255	.97	<.5	<5	<2	17	.03	<.2	<.2	21	.24	.019	5	16	.35	57	.04	<3	.91	.01	.04	<2	<.2	16	<.3	<.2	2.7	2
12306	.3	31.0	2.5	45.3	67	9	4	202	.84	<.5	12	<2	15	.02	<.2	<.2	19	.21	.016	4	10	.34	41	.04	<3	.77	.01	.03	<2	<.2	<10	<.3	<.2	2.2	2
12307	.6	20.4	1.9	67.3	31	7	4	193	.89	<.5	9	<2	13	.04	<.2	<.2	22	.18	.013	4	12	.26	38	.05	<3	.64	.01	.03	<2	<.2	14	<.3	<.2	1.9	1
12308	.6	32.1	2.1	51.0	39	8	4	193	.97	<.5	<5	<2	17	.03	<.2	<.2	22	.22	.022	5	12	.34	41	.04	<3	.79	.01	.04	<2	<.2	14	<.3	<.2	2.0	1
12309	.3	38.9	2.6	56.4	32	10	4	158	.85	<.5	7	<2	14	.02	<.2	<.2	20	.21	.016	5	13	.31	42	.05	<3	.77	.01	.04	<2	<.2	20	<.3	<.2	2.0	3
12310	.7	43.0	3.7	43.8	32	11	5	267	1.17	1.3	<5	<2	19	.04	<.2	<.2	28	.30	.048	6	15	.38	36	.06	<3	.80	.01	.04	<2	<.2	16	<.3	<.2	2.2	3
12311	.3	27.3	2.4	39.5	<30	9	4	199	.87	.6	<5	<2	16	.01	<.2	<.2	20	.25	.027	4	13	.32	35	.06	<3	.69	.01	.04	<2	<.2	<10	<.3	<.2	1.9	2
12312	.5	36.1	2.7	66.2	131	12	5	227	.96	<.5	7	<2	16	.04	<.2	<.2	22	.23	.019	5	15	.31	61	.04	<3	.89	.01	.04	<2	<.2	11	<.3	<.2	2.5	5
12313	.7	76.1	3.0	103.1	197	21	7	563	1.47	.5	9	<2	24	.08	<.2	<.2	27	.32	.035	7	22	.40	114	.03	<3	1.38	.01	.07	<2	<.2	23	<.3	<.2	3.6	1
12314	.7	44.4	2.1	85.5	123	16	5	559	1.19	.6	18	<2	18	.09	<.2	<.2	27	.26	.041	5	21	.27	78	.03	<3	.99	.01	.06	<2	<.2	19	<.3	<.2	2.3	1
12315	.4	32.4	2.4	48.6	139	10	5	288	.93	<.5	11	2	15	.03	<.2	<.2	22	.22	.015	5	15	.31	48	.04	<3	.79	.01	.05	<2	<.2	10	<.3	<.2	2.4	1
12316	.9	62.3	2.6	75.6	194	18	8	605	1.40	.6	12	<2	24	.08	.2	<.2	29	.31	.024	8	22	.38	97	.04	<3	1.11	.01	.07	<2	<.2	25	<.3	<.2	2.7	<1
12317	.4	36.5	2.2	71.7	153	13	5	468	1.06	<.5	16	<2	18	.07	<.2	<.2	21	.22	.019	5	16	.30	69	.04	<3	.88	.01	.08	<2	<.2	29	<.3	<.2	2.5	<1
12318	.5	9.7	2.0	73.0	<30	6	3	211	.77	<.5	9	<2	15	.07	<.2	<.2	15	.17	.042	4	7	.22	84	.03	<3	.69	.01	.04	<2	<.2	<10	<.3	<.2	2.0	<1
STANDARD	23.4	117.0	102.0	262.3	2007	30	17	991	4.60	73.5	26	18	56	1.97	9.8	19.8	67	.68	.108	16	52	1.10	222	.10	24	2.27	.04	.67	16	2.6	984	.7	1.9	7.2	54

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data ✓ FA ____

ACME ANALYTICAL

Crest Geological Consulting PROJECT 178 FILE # 9801731

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
12319	.7	54.2	3.0	70.3	182	13	5	453	1.10	1.1	<5	<2	23	.05	.2	<.2	19	.33	.034	6	14	.33	73	.02	<3	.87	.01	.08	<2	<.2	18	.3	<.2	3.0	1
12320	1.3	210.1	4.2	110.0	750	54	9	1548	2.44	3.1	<5	<2	47	.16	.3	.6	29	.77	.059	14	43	.51	214	.03	4	2.11	.01	.19	<2	<.2	81	.5	<.2	5.6	4
12321	.5	83.0	3.6	69.8	219	23	8	1019	1.47	.8	<5	<2	32	.20	<.2	<.2	25	.48	.028	6	21	.37	117	.03	<3	1.14	.01	.11	<2	<.2	24	<.3	<.2	2.9	<1
12322	.5	85.4	5.8	158.3	239	34	13	1478	2.10	1.2	<5	<2	39	.39	<.2	<.2	28	.74	.056	6	27	.46	220	.03	3	1.42	.01	.12	<2	<.2	25	<.3	<.2	3.6	1
12323	.5	62.4	3.8	50.5	221	12	4	369	1.15	3.2	<5	<2	26	.10	.2	<.2	25	.47	.030	5	17	.26	76	.02	<3	.93	.01	.07	<2	<.2	23	<.3	<.2	2.7	<1
12324	.3	16.1	7.6	70.6	101	8	8	715	1.13	.6	<5	<2	20	.12	<.2	<.2	16	.42	.035	3	14	.27	118	.02	<3	.83	.01	.07	<2	<.2	<10	<.3	<.2	2.4	<1
RE 12324	.5	14.9	8.5	67.5	134	8	7	679	1.06	<.5	7	<2	19	.14	<.2	<.2	15	.40	.033	3	10	.26	112	.02	<3	.80	.01	.07	<2	<.2	<10	<.3	<.2	2.9	1
12325	.4	6.5	3.2	70.6	53	4	4	281	.83	<.5	<5	<2	14	.06	<.2	<.2	16	.23	.029	3	10	.21	63	.03	<3	.56	<.01	.04	<2	<.2	10	<.3	<.2	2.3	1
12326	1.3	517.1	4.6	100.3	891	42	9	719	2.38	2.3	<5	<2	71	.82	.4	<.2	28	1.27	.061	11	47	.51	223	.02	<3	1.90	.02	.13	<2	<.2	45	.8	.2	4.7	3
12327	.6	13.8	3.9	316.2	221	7	5	472	1.14	<.5	<5	<2	21	.40	<.2	<.2	18	.26	.151	4	13	.24	150	.03	<3	.82	.01	.09	<2	<.2	14	<.3	<.2	3.3	1
12328	.5	13.5	2.3	68.0	106	5	5	387	.99	1.0	<5	<2	13	.30	<.2	<.2	16	.15	.023	2	10	.33	49	.02	<3	.80	<.01	.04	<2	<.2	20	<.3	<.2	2.5	1
12329	.7	12.0	3.0	53.4	83	6	5	168	1.14	1.0	<5	<2	14	.07	<.2	<.2	23	.20	.035	3	13	.30	55	.03	<3	.74	.01	.07	<2	<.2	<10	<.3	<.2	2.8	<1
12330	.6	10.6	2.3	73.6	113	7	6	286	1.27	1.1	7	<2	16	.10	.2	<.2	24	.21	.026	3	11	.41	59	.04	<3	.80	<.01	.07	<2	<.2	<10	<.3	<.2	2.5	1
12331	1.0	36.0	3.5	89.5	165	14	8	301	1.76	1.9	<5	<2	24	.12	.3	<.2	30	.32	.080	4	19	.46	78	.04	<3	1.07	.01	.10	<2	<.2	10	<.3	<.2	3.4	1
12332	1.4	29.9	5.0	153.8	197	11	6	294	1.77	1.5	<5	<2	17	.13	.2	<.2	32	.22	.091	4	20	.38	116	.03	<3	1.26	.01	.05	<2	<.2	<10	<.3	<.2	4.2	2
12333	.8	11.1	3.1	64.4	91	7	4	146	1.13	.9	<5	<2	12	.04	<.2	<.2	24	.17	.038	3	12	.32	49	.03	<3	.77	<.01	.05	<2	<.2	<10	<.3	<.2	2.9	2
12334	.7	14.4	2.6	86.5	154	8	4	264	1.05	1.1	<5	<2	11	.06	<.2	<.2	20	.15	.067	3	13	.30	76	.03	<3	.80	<.01	.04	<2	<.2	<10	<.3	<.2	2.6	1
12335	.5	8.1	2.9	102.9	120	6	4	246	.82	.6	<5	<2	10	.07	.2	<.2	17	.14	.032	3	8	.26	79	.03	<3	.67	<.01	.06	<2	<.2	16	<.3	<.2	2.5	1
12336	.5	9.7	2.4	74.4	113	7	4	177	1.04	.7	<5	<2	12	.05	.2	<.2	20	.17	.036	3	11	.33	82	.04	<3	.74	<.01	.04	<2	<.2	12	<.3	<.2	2.6	2
12337	.5	12.8	2.5	85.3	83	9	5	216	1.15	.7	10	<2	14	.05	.2	<.2	21	.21	.044	3	14	.41	69	.04	<3	.86	<.01	.06	<2	<.2	<10	<.3	<.2	2.9	1
12338	.8	16.2	2.8	74.1	121	8	5	274	1.12	.9	<5	<2	14	.05	.2	<.2	20	.19	.034	3	12	.40	74	.03	<3	.80	<.01	.05	<2	.2	16	<.3	<.2	3.0	<1
12339	.6	16.4	2.4	74.5	123	8	5	229	1.22	.6	<5	<2	13	.05	.2	<.2	21	.17	.053	3	12	.40	85	.03	<3	.84	.01	.09	<2	<.2	<10	<.3	<.2	2.7	1
12340	.5	26.3	2.7	68.9	94	9	5	296	1.19	.6	<5	<2	15	.03	.2	<.2	21	.22	.035	4	15	.47	57	.04	<3	.88	.01	.05	<2	<.2	11	<.3	<.2	2.6	1
STANDARD	26.2	122.1	110.4	275.4	2096	32	17	1011	4.70	74.0	22	17	59	2.08	10.8	20.6	71	.74	.109	16	53	1.18	244	.14	24	2.36	.04	.71	17	2.5	931	.7	2.1	7.5	50

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data / FA ____

APPENDIX II

SOIL SAMPLING METHODOLOGY
ANALYTICAL TECHNIQUES

APPENDIX II

SOIL SAMPLING METHODOLOGY
ANALYTICAL TECHNIQUES

SOIL SAMPLING METHODOLOGY and ANALYTICAL TECHNIQUES

Soil sampling was carried out along grid lines with sampling at a 50m spacing. Alternate lines were sampled at 50m also except that sample stations are offset by 25m so that the "implied" sampling "screen" is approximately 25m when the data is contoured.

B horizon material was sampled where available and placed in kraft sample bags and given a unique sample number. All samples were analysed for 35 elements by ultratrace ICP methods, gold by GF/AA analysis and mercury by cold vapour A.A. at Acme Analytical Laboratories Ltd., Vancouver, B.C. A detailed description of analytical reagents and procedures are listed on the first page of the analytical certificates.

ROCK SAMPLE ANALYTICAL TECHNIQUES

All rock samples were analysed for 30 elements by ICP methods used a 30gm aliquot, gold by atomic absorption (AA) and mercury by flameless AA at Acme Analytical Laboratories Ltd., Vancouver, B.C. A detailed description of analytical reagents and procedures are listed on the first page of the analytical certificates.

APPENDIX III

COPPER ACE PROPERTY - SOUTH GRID

GEOPHYSICAL SURVEY REPORT AND MAPS

GEOPHYSICAL INTERPRETATION REPORT

on the

CA 1, CA 2 CLAIMS

COPPER ACE SOUTH GRID

PROJECT NO. 178

CARIBOO MINING DIVISION, B.C. N.T.S. 93B/8,9

Latitude: 52° 33′ N, Longitude: 122° 19′ W

Prepared for:

UNITED GUNN RESOURCES LTD.

by

E. Trent Pezzot, B. Sc., P. Geo.

S.J.V. Consultants Ltd.

Date of Work: June 23 - July 9, 1998

Date of Report: November 30, 1998

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SJ Geophysics Ltd/S.J.V. Consultants Ltd. 11762 - 94th Ave., Delta, B.C. Canada
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List of Plates

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Introduction

S.J.V. Consultants Ltd. was commissioned to process and interpret geophysical data gathered across United Gunn Resources Ltd.'s Copper Ace South property in central B.C. The geophysical data was gathered by Crest Geological Consultants Ltd. and included some 28.8 line km of total field magnetic and vlf-em (Seattle and Hawaii frequencies) surveys. The geophysical surveys were completed as part of a larger exploration program that included geological mapping, geochemical sampling and induced polarization surveying on several properties in the area.

Targets are described as porphyry and shear hosted copper and zinc deposits. It was the intention of these surveys to assist in the general geological mapping of the area as well as to delineate magnetic and/or conductivity responses that may be related to exploration targets.

This report is intended to be used as an addendum to a more complete report being prepared by Crest Geological Consultants Ltd. Readers are referred to Crests' report for more detailed descriptions of the claims, their ownership, geology and previous and concurrent work.

Location and Access

The project area is located approximately midway between Quesnel and Williams Lake, B.C., in the Cariboo Mining Division and N.T.S. 93B/8,9. The approximate geographical co-ordinates near the centre of the claims are latitude 52° 33' N and longitude 122° 19' W.

The property is located some 10 km east of BC highway #2 and several logging roads provide direct access to various parts of the grid.

Property

The Copper Ace South (Project No 178) is comprised of the CA 1 & 2 claims as outlined on all of the maps included in this report.

Geology

The Geological Survey of Canada Map 12-1959 shows the claims area to lie along the western flank of the Granite Mountain - Dragon Mountain range. The area is mapped as undifferentiated granitic rocks. It falls along a linear feature extending up the

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Fraser River valley that appears to be a zone of faults and of tight folds. No single, large fault has, however, been traced along it.

A preliminary geological interpretation was provided on a hardcopy map. Four lithological units are mapped on the property: a quartz-feldspar porphyry, granite mountain phase (), mine phase schist and mine phase. Six rock sample locations showing anomalous Cu and Zn values are located in the mine phase and mine phase schist units. Seven faults are also mapped, oriented NW-SE, E-W and N-S.

Geophysical Surveys and Processing

A grid comprised of 13 NE-SW oriented lines, of variable length, spaced at 100 and 200 metre intervals was established. A total of some 28.8 line kilometres of grid were surveyed.

Total field magnetic and inphase, quadrature and field strength measurements for two vlf-em transmitters (Seattle: NLK 24.8 kHz and Hawaii: NPM 23.4 kHz) were recorded at 12.5 metre station increments along these lines. A GEM GSM-19 combination magnetometer and vlf-em instrument was used as a field unit. Diurnal variations were recorded on a second GEM GSM-19 magnetometer located in the grid area and appropriate corrections were applied to the field data.

Geophysical data was provided to S.J.V. Consultants Ltd. as a digital file with all appropriate corrections applied. All data was registered to the NAD 83, Zone 10 UTM co-ordinate system. An AutoCAD format drawing of the base map that shows the claims, topography, streams, roads and survey grid was also provided.

Final processing and maps were produced by S.J.V. Consultants Ltd. in Vancouver, using AutoCad, Geopak and RTICAD software.

Discussion of Results

The magnetic and vlf-em data are presented in both stacked profile and contour formats. All maps included in this report are registered to the NAD 83, Zone 10 UTM co-ordinate system. The survey grid, claim outlines, streams and roads also provide common reference points on all maps.

MAGNETICS

The magnetic data is presented in stacked profile format as Plate G-1a and in contour format as Plate G-1b. The magnetic amplitudes all fall within a relatively narrow

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(229 nT) range however the station to station variations are quite high, with a standard deviation of some 14 nT. This "choppy" character is indicative of volcanic rocks. There are a few magnetic responses, evident in the stacked profile display that exhibit similar characteristics between lines and can be interpreted as showing linear trends. Seven such responses are flagged on the compilation map, plate G-3a.

There are some correlations between the total magnetic intensity and the preliminary geological map however the magnetic data suggests more complex patterns. Two of three areas mapped as quartz/feldspar porphyry are distinguishable as magnetic highs (>57040 nT). Two areas of mine phase schists dominate the south-eastern corner of the grid. This area exhibits relatively low (< 56990 nT) magnetic intensities.

VLF-EM

Inphase, quadrature and field strength data was recorded for both the Seattle (NLK - 24.8 kHz) and Hawaii (NPM - 23.4 kHz) stations. The Seattle data is presented in stacked profile format as Plate G-2a and the fraser filtered inphase data in contour format as Plate G-2b. The Hawaii data was analyzed but did not assist in the interpretation and is not presented here.

Forty-three conductivity type responses are identified in the vlf-em data. Sixteen of these are likely generated from streams and/or topographic breaks. Most of the inphase component responses are on the order of <25% peak to peak amplitude, although one instance of 73% peak to peak amplitude is observed. The majority of the conductors exhibit an inphase to quadrature ratio of greater than 1.0, indicating relatively good conductivity. Approximately one third of the responses flagged extend over multiple lines, suggesting continuity to the sources. The majority of these strike N-S (+/- 10^{o}). There are also a couple of instances where the conductors align NW-SE.

Five of the seven magnetically defined lineations coincide with vlf-em anomalies. A number of the conductors are also parallel and adjacent to contacts drawn on the preliminary geology map. It is likely that these conductors are related to geological contacts or shear/fault zones.

Summary and Conclusions

An exploration program, including magnetic and vlf-em surveys, was conducted by Crest Geological Consultants Ltd. across the Copper Ace South Grid, on behalf of

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United Gunn Resources Ltd. Approximately 28.8 line kilometres of geophysical data was forwarded to S.J.V. Consultants Ltd. for plotting and analysis. The survey was completed as part of a larger exploration program that included geological mapping, geochemical sampling and induced polarization surveying. The results of these other exploration techniques are currently being reviewed.

The area is being explored for porphyry and/or shear hosted copper and zinc deposits. Preliminary geological data shows the area as being underlain by four different volcanic units.

The magnetic data confirms the area is underlain by volcanics and suggests more complex structures than are indicated on the preliminary geological map. There are indications that the magnetic amplitudes may be useful in delineating at least two of the geological units.

Magnetic and vlf-em data suggest two dominant geological strikes: N-S and NW-SE. There are also indications of some NE-SW structures however this angle parallels the survey grid lines and these trends are not clearly delineated in this data.

The vlf-em defined conductors likely trace geological contacts or fault/shear zones.

Recommendations

There are several magnetic and vlf-em trends that can be interpreted as shear or fault zones. However, at this time, I feel it is premature to provide specific recommendations for follow-up. The prioritisation of anomalies and recommendations for further work should completed after the rest of the geological, geochemical and induced polarization results have been compiled.

Respectfully submitted
per S.J.V. Consultants Ltd.

PROFESSIONAL PROVINCE OF E. T. PEZZOT BRITISH COLUMBIA GEOSCIENTIST

E. Trent Pezzot, B.Sc., P.Geo.
Geophysics, Geology

APPENDIX 1

Statement of Qualifications

I, E. Trent Pezzot, of the city of Surrey, Province of British Columbia, hereby certify:

- I graduated from the University of British Columbia in 1974 with a B.Sc. degree in the combined Honours Geology and Geophysics program.

- I have practised my profession continuously from that date.

- I am a registered member of the Association of Professional Engineers and Geoscientists of British Columbia.

- I hold no direct or indirect interest in, nor expect to receive any benefits from, the mineral property or properties described in this report.

November 30, 1998

PROFESSIONAL PROVINCE OF E. T. PEZZOT BRITISH COLUMBIA GEOSCIENTIST

E. Trent Pezzot, B.Sc., P.Geo.

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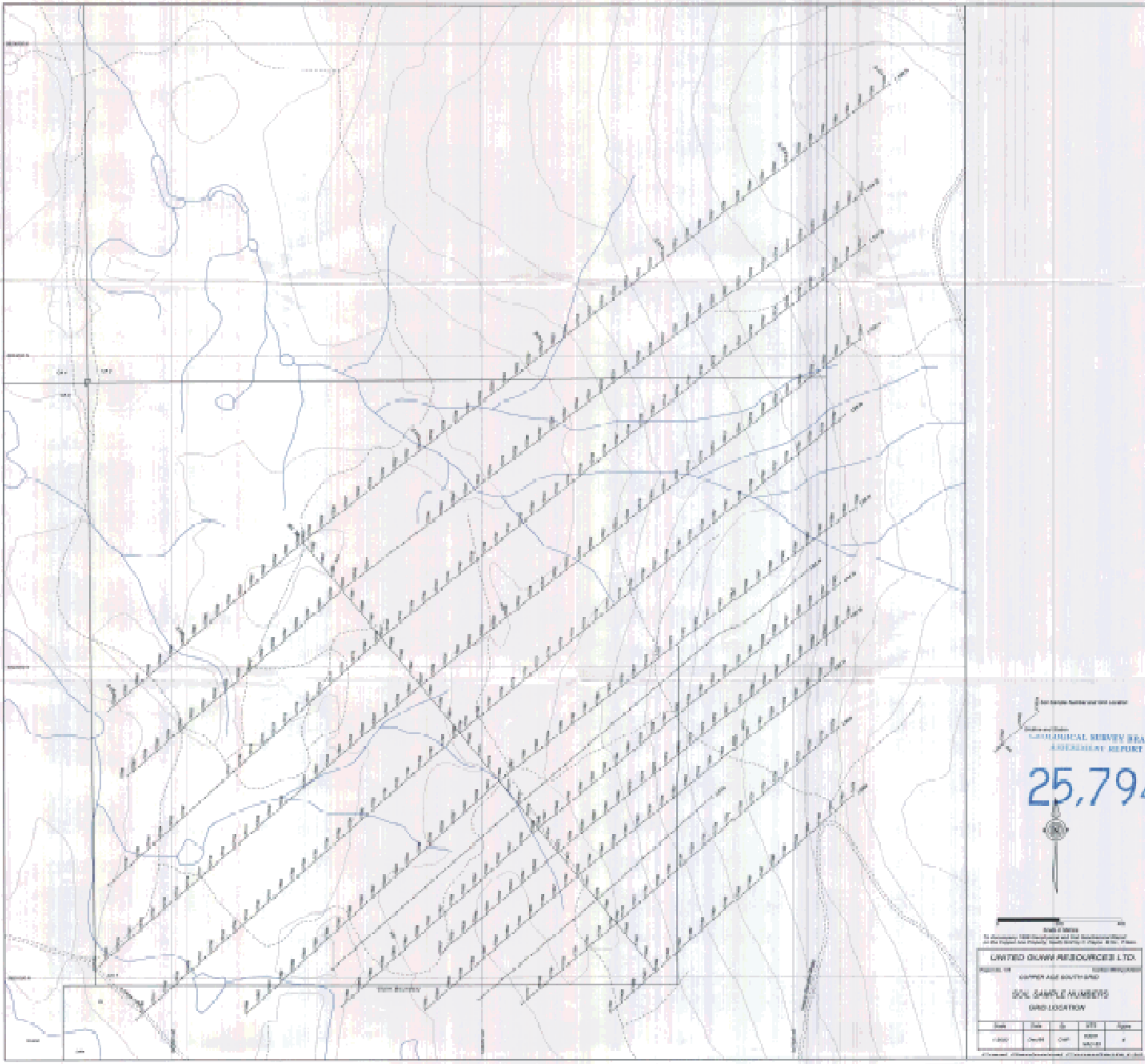
GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT
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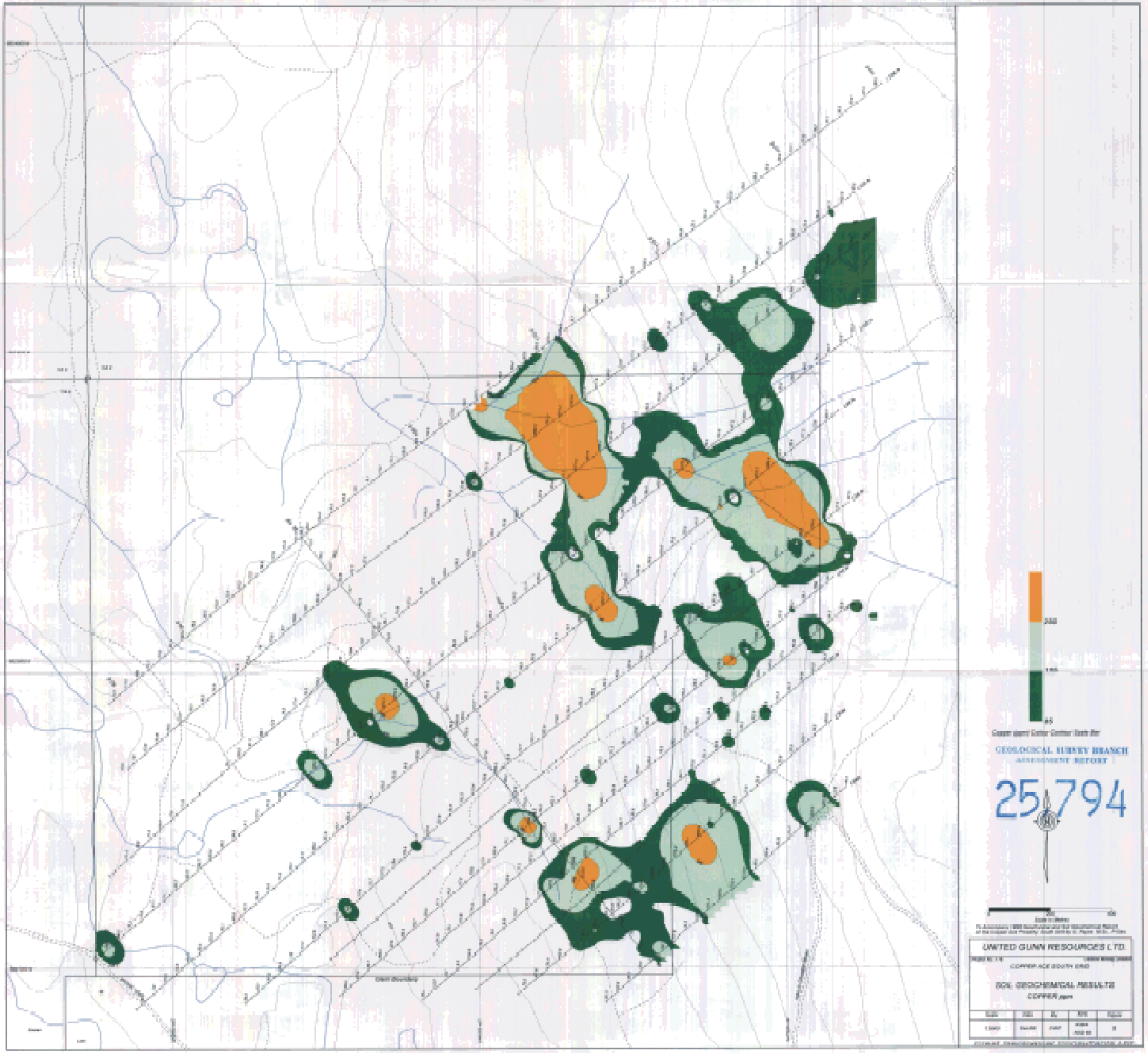
UNITED GUNN RESOURCES LTD.
COPPER AGE SOUTH GRID
SOIL SAMPLE NUMBERS
GRID LOCATION



GEOLOGICAL SURVEY BRANCH
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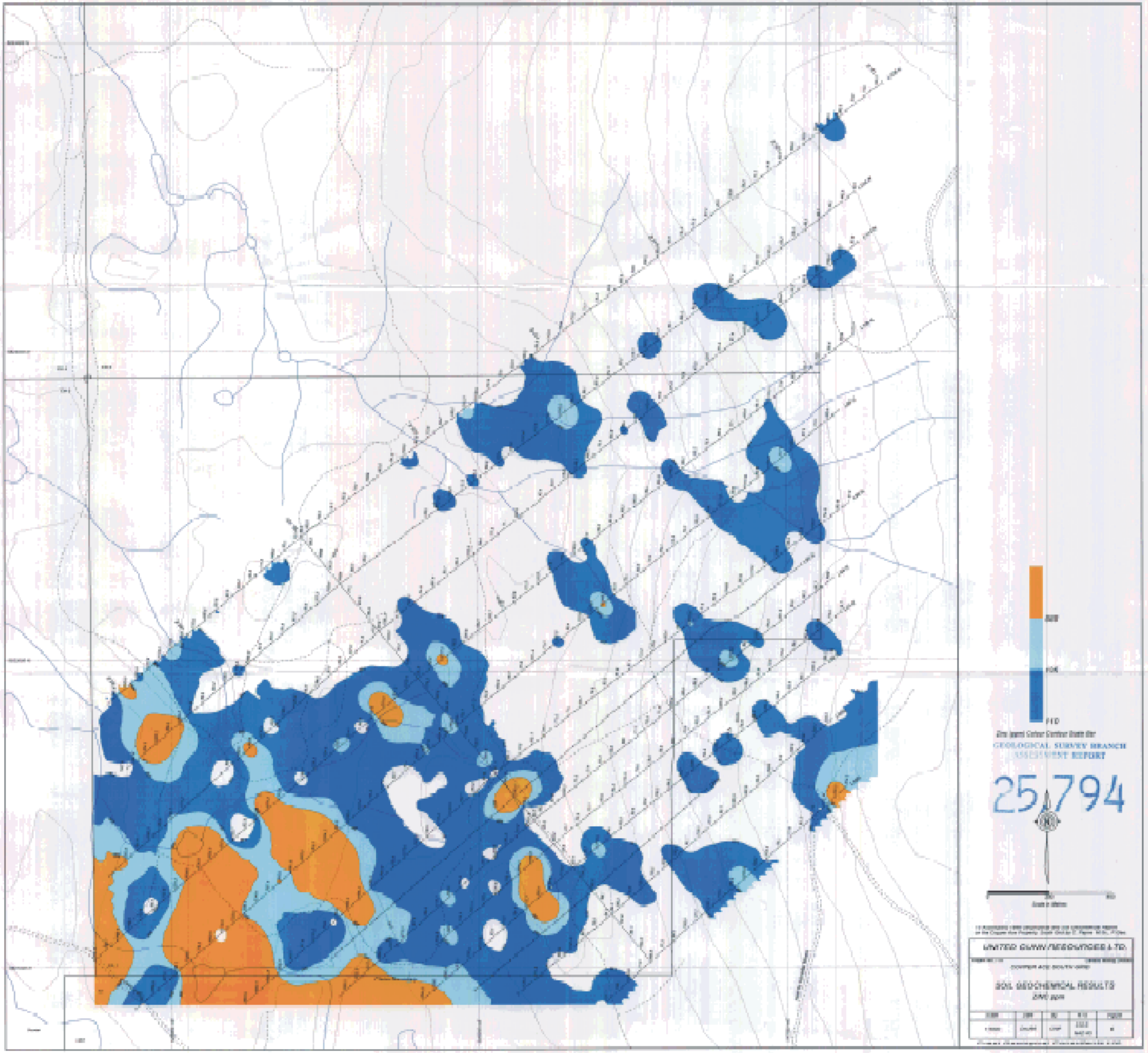
UNITED GUNN RESOURCES LTD.
COPPER ACE SOUTH GRID
SOIL GEOCHEMICAL RESULTS
COPPER ppm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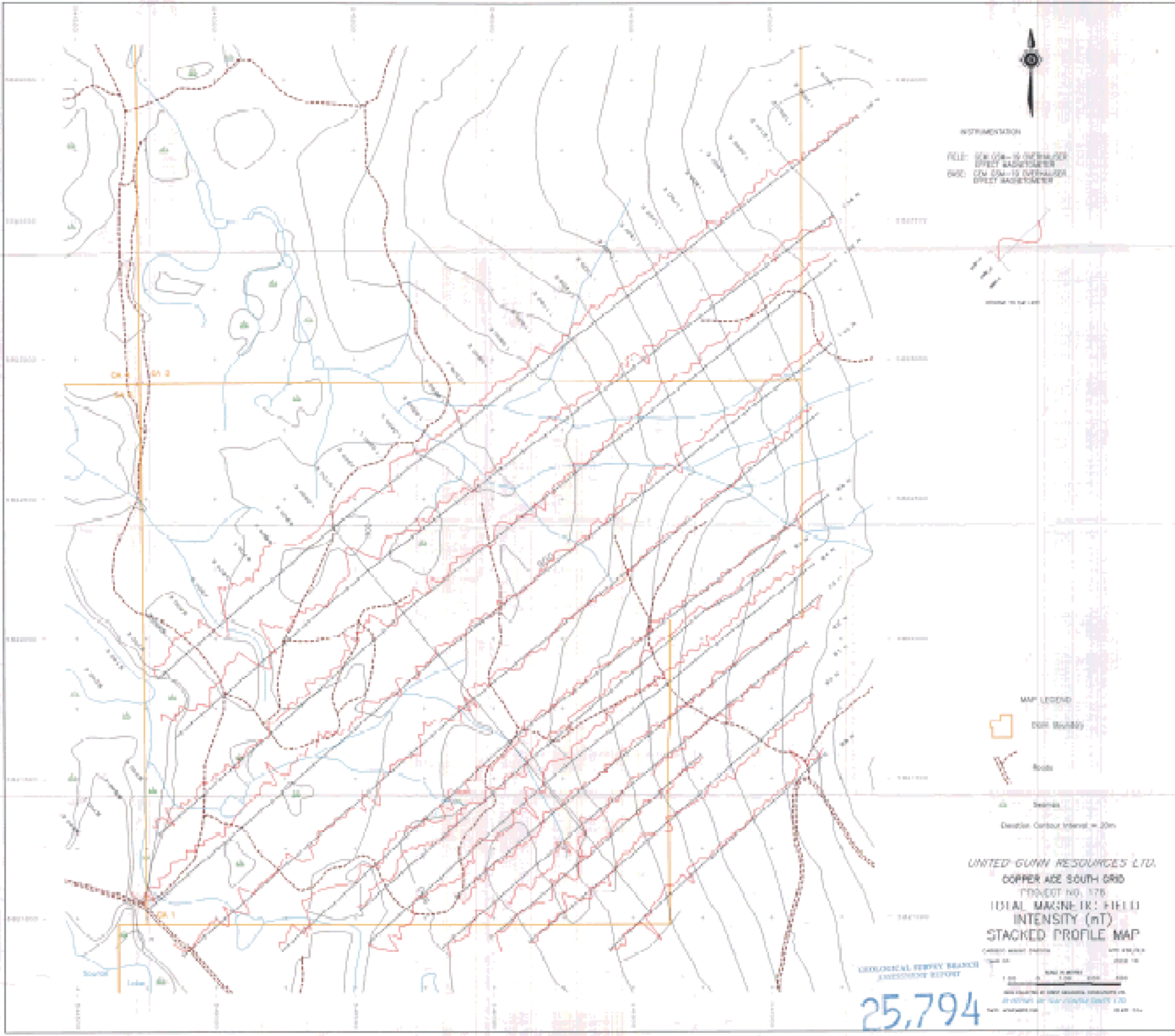
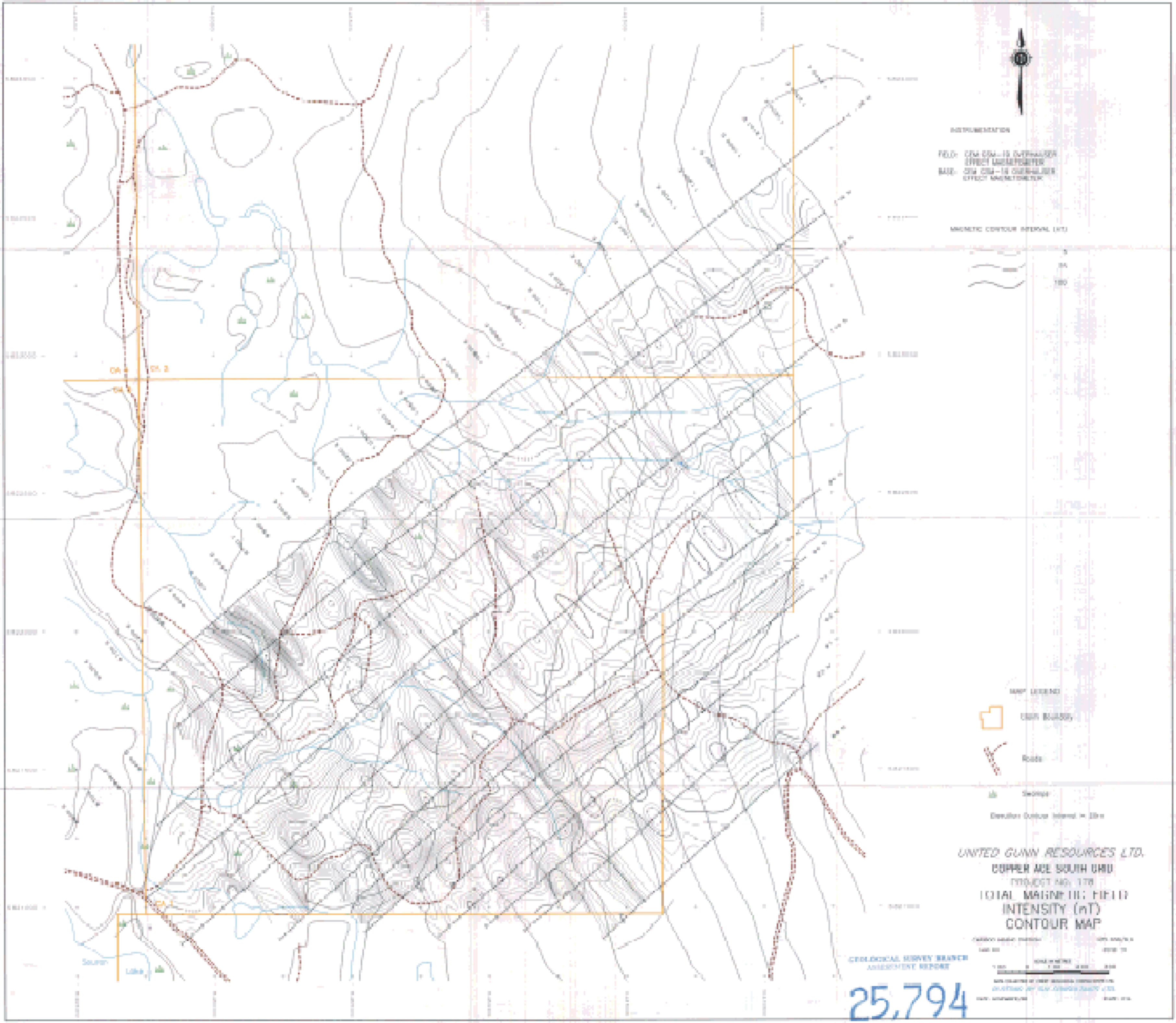
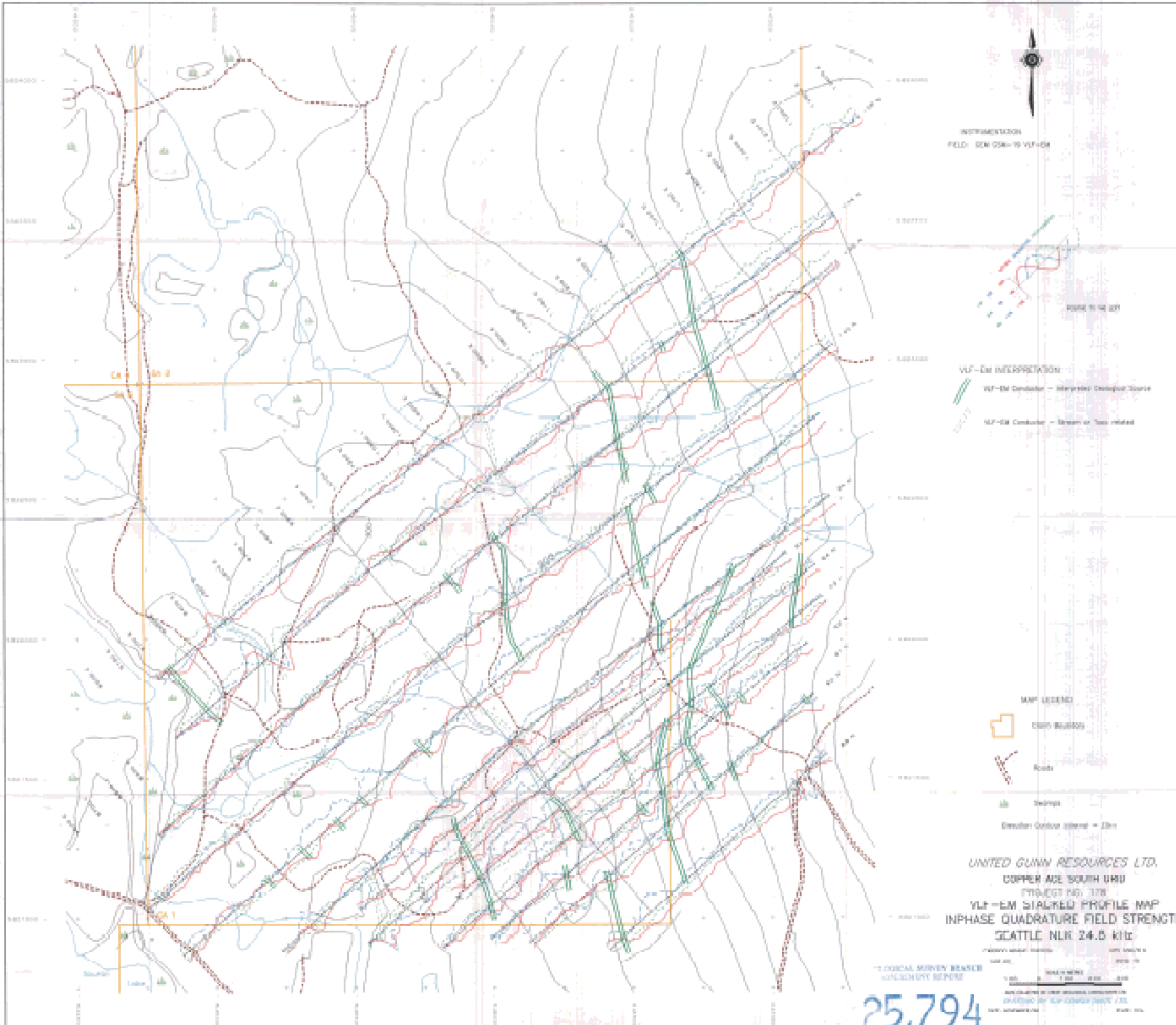

INSTRUMENTATION
MAP LEGEND
Roads
Elevation Contour Interval = 20m
UNITED GUNN RESOURCES LTD.
COPPER AGE SOUTH GRID
TOTAL MAGNETIC FIELD
INTENSITY (nT)
STACKED PROFILE MAP
GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT
25,794



INSTRUMENTATION
MAGNETIC CONTOUR INTERVAL (nT)
100
MAP LEGEND
Roads
Swamps
UNITED GUNN RESOURCES LTD.
TOTAL MAGNETIC FIELD
INTENSITY (nT)
CONTOUR MAP
GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT
25,794
Lake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VLF–EM INTERPRETATION
MAP LEGEND
Roads
UNITED GUNN RESOURCES LTD.
VLF–EM STACKED PROFILE MAP
INPHASE QUADRATURE FIELD STRENGTH
SEATTLE NLK 24.8 kHz
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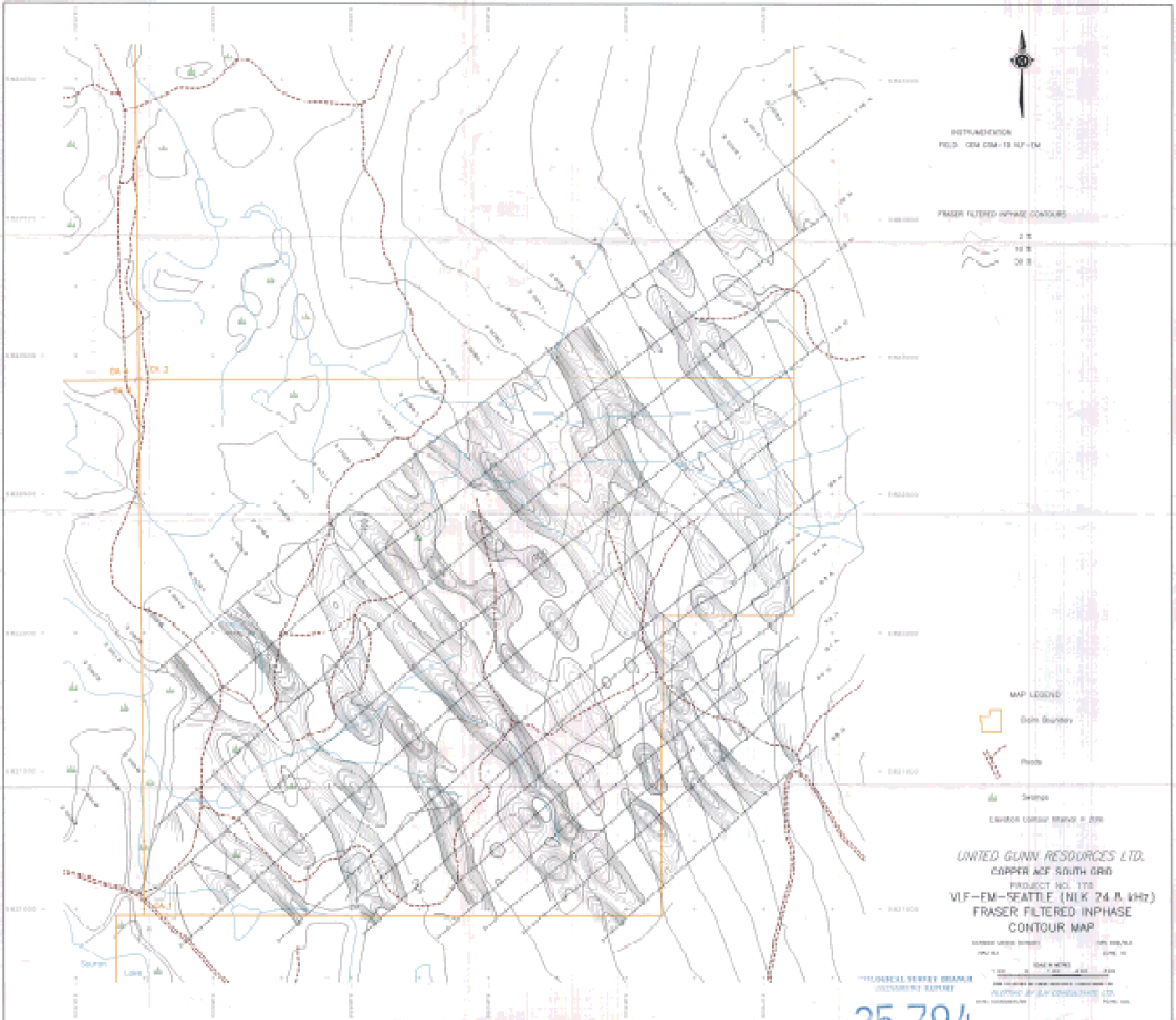
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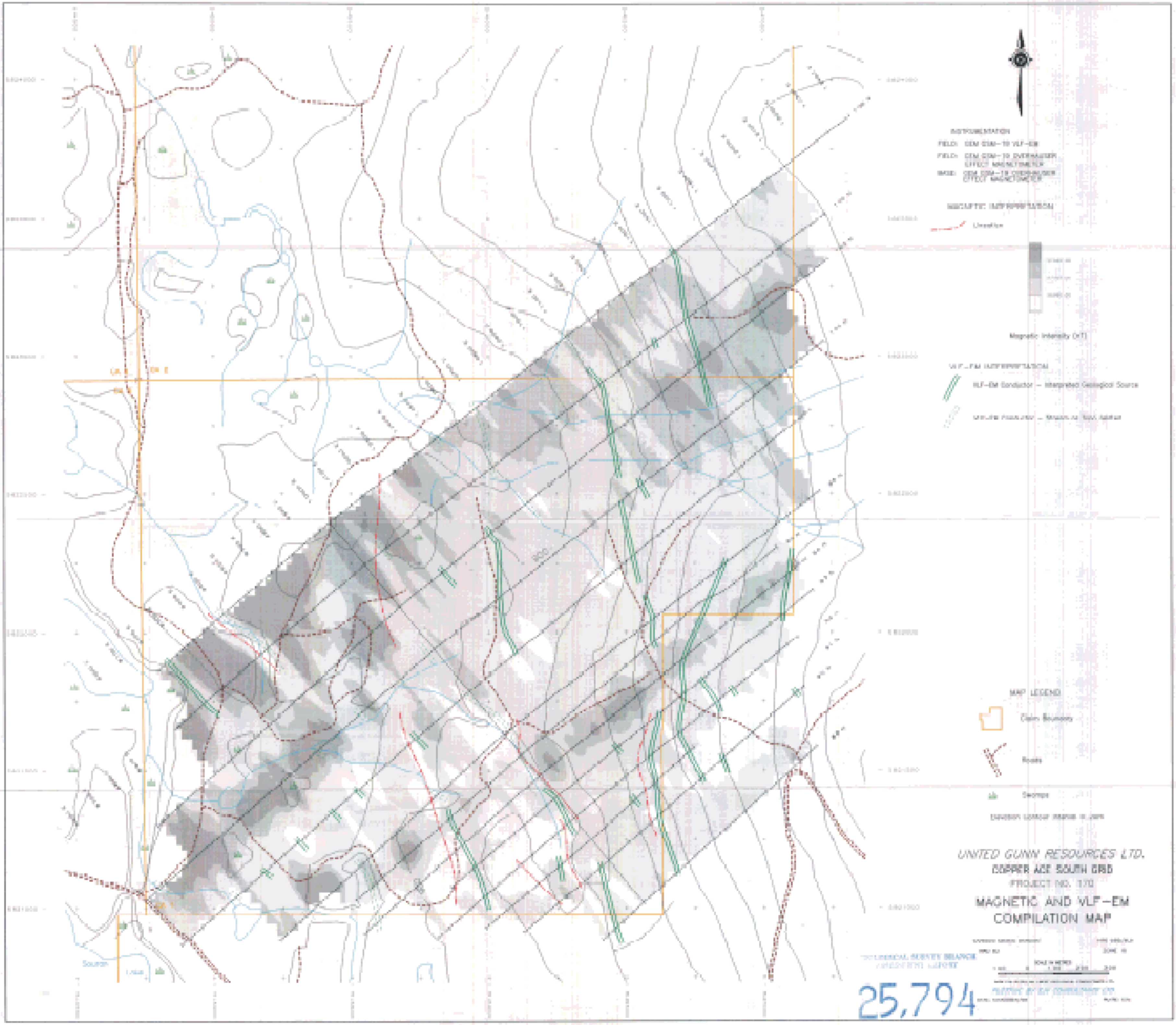
MAP LEGEND
Roads
UNITED GUNN RESOURCES LTD.
PROJECT NO. 178
VLF-EM-SEATTLE (NLK 24.8 kHz)
FRASER FILTERED INPHASE
CONTOUR MAP
25,794



INSTRUMENTATION
FIELD: GEM GSM-19 VLF-EM
FIELD: GEM GSM-19 OVERHAUSER EFFECT MAGNETOMETER
BASE: GEM GSM-19 OVERHAUSER EFFECT MAGNETOMETER
MAGNETIC INTERPRETATION
Lineation
Magnetic Intensity (nT)
VLF-EM INTERPRETATION
VLF-EM Conductor — Interpreted Geological Source
MAP LEGEND
Claim Boundary
Roads
Swamps
UNITED GUNN RESOURCES LTD.
COPPER ACE SOUTH GRID
PROJECT NO. 170
MAGNETIC AND VLF-EM COMPILATION MAP
25,794