GEOLOGICAL, GEOCHEMICAL and GEOPHYSICAL REPORT

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TAKEN 1 MINERAL CLAIM Omineca Mining Division British Columbia

NTS 93F/2,3 53° 02' North Latitude 125° 00' West Longitude

by

P. E. Fox, Ph.D, P. Eng. FOX GEOLOGICAL SERVICES INC. 1409 - 409 Granville Street Vancouver, BC V6C 1T8

Work Paid for by PARAMOUNT VENTURES & FINANCE INC.

January 21, 1999

GEOLOGICAL SURVEY BRANCH

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SUMMARY

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The Taken 1 claim, located in central British Columbia, was staked by Phelps Dodge Corporation of Canada, Limited in January, 1994. The property was staked concurrently with the adjoining Tam and Tommy gold prospects following a government geochemical release in January, 1994. The Tommy prospect, currently being explored by Teck Corporation, is estimated to contain 440,000 tonnes of gold grading 8.5 gpt. The Mint vein, located on the adjacent Tam prospect some 600 metres west of Taken 1, has returned 1.4 gpt gold over an estimated true width of 3.9 metres in drill core.

The prospect lies within the Nechako Arch, a basement high composed of Jurassic Hazelton Group volcanics intruded by Cretaceous and younger intrusive rocks. The claim is underlain by west-dipping volcanic rocks of the Hazelton Group, Naglico Formation, consisting of rhyolitic lapilli tuff with lesser andesite and basalt flows. The Taken prospect was explored by Phelps Dodge Corporation of Canada in 1994 and 1995. Phelps Dodge defined a number of areas with elevated to anomalous concentrations of gold and silver in soil.

The 1998 field program was conducted between September 30 and October 13. Work consisted of establishing 2.95 line-kilometres of in-fill soil grid from which 97 soil samples were collected, a 5 kilometre induced polarization survey, excavation of 6 soil test pits and a 77.5-metre trench. The trench was mapped and 32 rock chip and grab samples were collected along its length. Trenching excavated brecciated, quartz-carbonate veined felsic tuff which returned an average of 4.7 gpt Ag, 680 ppm Cu, 1810 ppm Pb and 637 ppm Zn over 29.5 metres. The Induced Polarization survey outlined the southern tips of three areas of steep chargeability gradient on line 108+00N, with a trend to increasing apparent resistivity with increasing electrode separations. The central structure is less intense but still visible on line 106+00N, in the vicinity of the trench. Geology and mineralogy indicate that the trench may have exposed the upper levels of an epithermal vein system similar to those on the adjoining Tam and Tommy prospects. Geophysics indicates that this system trends to the north. Diamond drilling will be necessary to further test and delineate this system.

INTRODUCTION

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This report details an exploration program conducted on the Taken 1 claim between September 30 and October 29, 1998. The Taken 1 claim was staked by Phelps Dodge Corporation of Canada, Limited in January 1994 and is currently under option to Paramount Ventures and Finance Inc. Work done this year consisted of in-fill soil sampling, test pits, trenching and an induced polarization survey.

LOCATION, ACCESS and PHYSIOGRAPHY

The Taken 1 claim is located 160 road-kilometres southwest of Vanderhoof, British Columbia in the Naglico Hills. The claim lies between Tommy Lakes and Tsacha Lake, about 3km north of the West Road (Blackwater) River (see Figure 1).

Access from Vanderhoof is via the Kluskus-Ootsa Forest Service Road, southwest for 140 kilometres then southeast along the 8000 Forest Service Road which runs through the Naglico Hills to a large Forestry landing area. Two roads continue onto the Taken claim from the landing area. A fire access road heads eastward onto the central claim area and the Tommy property access road trends southward, connecting with a network of drill roads that cross the Tam property, accessing the southern Taken claim area.

The property is situated on the lower south- and west-facing slopes of the Naglico Hills. These gently rolling hills range in elevation from approximately 1550 metres on a knoll in the northwesterly claim area to a low of about 1190 metres in the southeast. A southeasterly flowing tributary to the West Road (Blackwater) River, with associated small lakes, dissects the claim block resulting in some localized, swampy areas. Rock exposures are infrequent, limited to hilltops and steeper slopes within the property.

Forest cover consists primarily of open-spaced spruce and pine which are typical of the area. A large burn area comprising a thick tangle of deadfall occupies the western portion of the claim.

CLAIM INFORMATION

The Taken 1 is a four-post mineral claim, staked on January 30, 1994 for Phelps Dodge Corporation of Canada Limited. It straddles B.C. Mineral Titles' claim maps 093F/2W and 093F/3E in the Omineca Mining Division of British Columbia (Figure 2). The property is currently under option to Paramount Ventures & Finance Inc. who acted as operators for the 1998 work program. Pertinent claim information is outlined in Table 1 below. The expiry date shown below assumes that current work is accepted for assessment purposes.





	Table 1: CL/	AIM STATUS	
	TENURE NO.	EXPIRY DATE	UNITS
Taken 1	323457	36921	20

Taken 1 partially overstakes the adjacent Tam 3 claim, reducing the effective claim area to approximately 18.5 units.

PERMITS and RECLAMATION

All work conducted on the Taken 1 claim during 1998 was performed under B.C. Ministry of Energy and Mines Annual Work Approval Number PRG-1998-1101404-9052, Reclamation Permit number MX-11-134 and a Ministry of Forests Licence to Cut number L44193. Disturbance during 1998 consisted of a 2.1-kilometre temporary access road, a 77.5-metre trench and 6 test pits, all of which have been infilled, recontoured and seeded.

HISTORY

A 1994 government publication (Diakow, et.al. 1993) reported the discovery of an epithermal quartz vein, the Tommy prospect, near Tsacha Lake and a localized staking rush ensued. During this rush, the Taken 1 claim was staked by Phelps Dodge Corporation of Canada, the Tommy showing was staked by Teck Corporation (Tsacha and Tasha claims) and the Tam claims were staked by Cogema Resources (Figure 2). Phelps Dodge explored the Taken claim in 1994 and 1995, with geological mapping, prospecting, rock sampling and soil sampling on two variously-oriented grids totalling approximately 32 line-kilometres. Work to date has defined a number of areas that contain elevated to anomalous gold and silver in soil.

REGIONAL GEOLOGY

The Taken 1 claim is centrally located in the Intermontane Belt of British Columbia's Interior Plateau. The Intermontane Belt consists of accretionary plates of the Stikinia, Cache Creek and Quesnellia Terranes. These are composed of late Palaeozoic to mid-Mesozoic marine volcanic and sedimentary rocks and mid-Mesozoic to late Tertiary marine and non-marine sedimentary and volcanic rocks. The claims lie in the Nechako Arch, which consists of several volcanic-stratigraphic groups ranging in age from Jurassic to Miocene. Pre-Tertiary rocks of the Nechako Arch include lower Cretaceous Skeena Group, an assemblage of easterly derived back arc clastic rocks, and the middle Jurassic Hazelton Group composed of arc-type calcalkaline volcanics and

volcaniclastics. Diakow and Webster (1993) have informally classified rocks outcropping in the Fawnie Creek as belonging to the Naglico formation, Hazelton Group. In the vicinity of the property, the Naglico formation consists of rhyolite, andesite and basalt flows, tuff and lapilli tuff. These rocks are intruded by Cretaceous biotite diorite to monzodiorite bodies. Regional geology is represented in Figure 3.

Tertiary and younger rocks comprise the Ootsa Lake Group, which consists of rhyolitic to dacitic tuff, flows and breccias. Miocene Chilcotin Group vesicular basalt flows and Late Miocene to Quaternary Anahim Group plume volcanics form the Rainbow, Ilgachuz and Itcha shield volcanoes just to the south of the Taken prospect. An arcuate belt of Paleocene Nanika and Quanchus quartz monzonite and granite intrudes Ootsa Lake Group and older rocks of the Nechako Arch.

The Tommy occurrence, located about 1.5 kilometres west of the Taken 1 LCP, consists of a series of north striking, steeply dipping, gold bearing veins. Of these, the Tommy vein is the most significant, estimated by Teck to contain 440,000 tonnes grading 8.5 gpt gold, using a 5 gpt cutoff. Teck is currently exploring the Larry vein, which has been traced over a strike length of 300 metres and has returned up to 6.8 gpt gold over 3.8 metres in drill core. The Mint vein, 600 metres west of Taken 1, has returned 1.4 gpt gold over an estimated true width of 3.9 metres in drill core.

PROPERTY GEOLOGY

Volcanic rocks of the Naglico formation underlie the Taken claim, exposed sporadically in small exposures of outcrop and rubble-crop situated on small rocky knobs and ridge summits. The volcanic units form a southwesterly dipping assemblage composed predominantly of rhyolitic lapilli tuff (Figure 4, Unit Nr) with andesite (Na) and basalt (Nb) flows in the northwest and interfingered with lapilli tuff on the west. The welded rhyolite tuff units, which underlie most of the claim, host all of the mineralization in the area. All units are shades of grey, green and maroon with grey-green and brown weathered surfaces. Most of the rhyolite tuffs are massive, laminated and subvitreous, containing phenocrysts of potassium feldspar and quartz and local exotic clasts of darker volcanic rocks. Flow banding and a flow breccia have both been observed. Interbeds of tuff, lapilli tuff and breccia are common in the central part of the property.

Andesite flows are greyish-green, fine grained, weakly to moderately magnetic and contain lath-like feldspar phenocrysts up to 4 millimetres in size. The andesite flows are locally intercalated with massive, strongly magnetic basalt flows.



An outcrop of quartz-eye dacite porphyry (Nd) occurs in the eastern claim area and a lens of maroon shale (Ns) outcrops in the southwest. Late Cretaceous diorite (Di) occurs as a large sill that lies along the western claim boundary and as several smaller bodies throughout the claim. The intrusive bodies are fine grained, gray, weakly magnetic and dioritic to monzonitic in composition with biotite phenocrysts set in a fine grained matrix. These rocks have been weakly chloritized.

1998 WORK PROGRAM

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The 1998 field program was conducted between September 30 and October 13. Work consisted of in-fill soil sampling, test pits, trenching and an induced polarization survey. A total of 64.5 man-days was spent on the property.

Three grid lines (101+00N, 103+00N, 105+00N) were established in the southwestern corner of the claim to obtain more detailed geochemical information. Line spacing in this area is now 100 metres. Total new grid length is 2.95 line-kilometres. Soil samples were collected along these lines at 50 metre intervals. Samples were obtained from the B horizon, where possible, stored in paper sample bags, tagged with a unique number and submitted to Acme Analytical Laboratories Ltd. in Vancouver, B.C. for analyses. Each sample was dried, sieved to -80 mesh and analyzed for 34 elements by ICP techniques and for gold by geochemical atomic absorption analysis. Field notes detail location, topography, type and colour of material. A total of 97 soil samples were collected. Soil geochemical results for gold and silver are plotted in Figures 7 and 8. Analytical method and data comprise Appendix II.

Six soil test pits were also dug. The purpose of this was two-fold: 1) to determine if previously obtained soil geochemical anomalies were derived from bedrock or glacial till and 2) to determine bedrock depth for possible trenching. The pits, up to 3.7 metres deep, all failed to reach bedrock. They were sampled at 0.5-metre intervals from bottom to surface. Results are displayed in Table 3, analyses are in Appendix II.

A single trench, 77.5 metres in length, was excavated to test a soil geochemical anomaly on line 106+00N that returned elevated gold and silver concentrations. The trench was mapped at a scale of 1:100. Twenty-nine one-metre chip samples were collected over mineralized rocks exposed in the last third of the trench, between 48.0 and 77.5 metres, and 3 grab samples were collected at irregular intervals from the rest of the trench. The trench geology and sampling plan comprise Figure 5. All rock samples were submitted to Acme Analytical Laboratories in Vancouver, B.C. for analysis. Rocks were crushed and pulverized to -100 mesh. All samples were

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analyzed for 34 elements by ICP techniques and for gold by geochemical AA methods. sample descriptions comprise Appendix 1, analytical procedures and data constitute Appendix II. Rock sample locations are shown in Figure 5 with gold, silver, copper, lead and zinc contents noted.

Scott Geophysics Ltd. of Vancouver was commissioned to conduct an induced polarization (IP) survey over the southwestern corner of the property. To this end, four lines (102+00N, 104+00N, 106+00N, 108+00N), totalling 5 line-kilometres, were brushed to facilitate movement of the IP crew and equipment. Instrumentation and procedures involved in the collection of data are presented in a report by David C. Hall, dated October 19, 1998, which is included as Appendix III of this report. IP data is presented as pseudosections and contoured resistivity and chargeability filter plans comprise Figures 9 through 11.

RESULTS

Trenching

The trench excavated during 1998 (Figure 5) exposed approximately 60 metres of felsic tuff with minor sections of coarser felsic pyroclastics and more mafic flows and tuff. Between 45 and 70 metres, the felsic tuff is brecciated and dissected by quartz-carbonate veins that contain local concentrations of disseminated to blebby bornite and/or galena. Malachite and azurite are abundant. Trench samples returned up to 45 gpt Au, 33 gpt Ag, 0.36% Cu, 1.36% Pb and 0.21% Zn with elevated arsenic, cadmium, antimony and mercury. The entire chip sampled interval, from 48 to 77.5 metres, averaged 6.86 ppb Au, 4.7 gpt Ag, 680 ppm Cu, 1810 ppm Pb and 637 ppm Zn over 29.5 metres. Grab samples of tuff and tuff breccia collected in the unmineralized portion of the trench returned background concentrations for all elements of interest.

Geophysics

Induced polarization (IP) chargeabilities (Figure 10) range from 1.4 to 11.0 mV/V over the survey area. There is a noticeable increase in overall chargeability toward the northwest, from line 102+00N to line 108+00N. Pseudosections (Figure 11) indicate three areas with steep chargeability gradients on line: 1) at 110+00E, in the vicinity of a diorite/tuff contact, 2) at 113+75E, due north of the 1998 trench and 3) at 115+75E. The central structure is the southern edge of a chargeability low, flanked by two chargeability anomalies that trend off the grid to the north.

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Paramount Ventures and Finance Inc.										
Property)		OMENICA M	INING DISTRICT							
Trench 1 Geology and Sampling Plan										
Date	By	NTS #	Figure							
Dec.98	Wetherup	92 F/3	# 5							
	nt Vent Property) Tro blogy an Date Dec. 98	nt Ventures and Property) Trench plogy and Samp Date By Dec. 98 Wetherup	nt Ventures and Finance Property) OMENICA M Trench 1 blogy and Sampling Plan Date By NTS # Dec. 98 Wetherup 92 F/3							

Apparent resistivities (Figure 9) range from 215 to 1380 ohm-metres. A broad anomalous area (>300 metres), defined by the 600 ohm-metre contour extends northerly from line 104+00N to 108+00N. This feature coincides with a diorite intrusion mapped on line 108+00N. Pseudosections indicate that apparent resistivities on line 108+00N increase significantly with larger electron spacings suggesting increasing apparent resistivity with depth.

Soil Sampling

The 1998 in-fill soil sampling returned gold and silver concentrations up to 93 and 362 ppb respectively. The survey served to further delineate areas with elevated to anomalous gold and silver concentrations, resolving the previously defined anomalies into several smaller ones (Figures 7 and 8). No additional areas of interest were indicated. Soil sample results are summarized in Table 2.

Table 2: SOIL ANALYTICAL RESULTS											
	Au (ppb)	Ag (ppb)	Cu (ppm)	Pb (ppm)	Zn (ppm)	As (ppm)	Hg (ppm)				
Minimum	0	0	5.9	7.1	34.8	1	0				
Maximum	93	362	36	26	215.9	7.8	38				
Mean	3.9	113.3	11.6	10.2	91.9	2.8	16.1				
Elevated	10	150	20	20	130	5	25				
Anomalous	20	300									

Soil Test Pits

Soil test pit results are graphed in Table 3 below, showing individual pit results for gold and silver vs. increasing depth. Results for both elements are sporadic, revealing systematic trends only in pits 5 and 6. In pit 5, the shallower samples are more enriched in gold and silver than those collected at depth, while the converse is true of Pit 6 which reflects the ideal situation whereby elemental concentrations would increase with depth, reflecting possible mineralization in the underlying bedrock. Pits 5 and 6 are situated only 40 metres apart. Given these data, the value of soil sampling as a tool to locate mineralization on the Taken 1 is questionable.

	Table 3: SOIL TEST PIT RESULTS																							
	Pi	Pit 1		Pit 1		Pit 1 Pit 2		: 2	Pit 3		Pit 4		Pit 5		Pit 6									
Sample Depth	Au (ppb)	Ag (ppb)	Au (ppb)	Ag (ppb)	Au (ppb)	Ag (ppb)	Au (ppb)	Ag (ppb)	Au (ppb)	Ag (ppb)	Au (ppb)	Ag (ppb)												
Increasing	4	138	0	102	0	0	7	130	13	577	1	84												
Depth	2	240	5	116	1	41	2	41	7	237	1	46												
	8	69	6	76	0	73	2	81	1	58	1	81												
					1	92	0	62	57	102	2	69	5	195										
l			1	75	1	93	3	70	1	45	4	320												
			1	125	3	99	3	59			16	1051												
V			22	112	1	82	8	57																

CONCLUSIONS and RECOMMENDATIONS

The trench excavated during 1998 exposed brecciated, quartz-carbonate veined felsic tuff which returned an average of 4.7 gpt Ag, 680 ppm Cu, 1810 ppm Pb and 637 ppm Zn over 29.5 metres. The Induced Polarization outlined the southern tips of three areas of steep chargeability gradients on line 108+00N, with a trend to increasing apparent resistivity with depth. The central structure is less intense but still visible on line 106+00N, in the vicinity of the trench. Geology and mineralogy indicate that the trench may have exposed the upper levels of an epithermal vein system similar to those on the adjoining Tam and Tommy prospects. Geophysics indicates that this system trends to the north where increasing resistivities with depth support this theory. Diamond drilling will be necessary to further test and delineate this system.

Project expenditures for the 1998 work program are \$38,230.00 and are tabulated below.

Accommodation and Board Communication	52 man-days @ \$73.5/day	3,822.00 996.00
Contract Geophysics - Scott Geophy	ysic	
5 line-kilometres IP @ \$1175	.00/km	5,875.00
Contract Trenching - Northern Aggra	agate Ltd.	
Mob-Demob	-	100.00
Trenching		3,042.00
Laboratory		
97 Soil samples @ \$15.00/sa	Imple	1,456.00
32 Rock samples @ \$18.00/s	sample	576.00
Labour		
P. Fox, Geologist	1 days @ \$400/day	400.00
S. Wetherup, Geologist	13 days @ \$375/day	4,875.00
L. Poznikoff, Geologist	5 days @ \$375/day	1,875.00
P. Charbonneau, Sampler	11 days @ \$275/day	3,025.00
G. Charbonneau, Sampler	11 days @ \$275/day	3,025.00
F. Larocque, Sampler	11 days @ \$275/day	3,025.00
Shipping		60.00
Supplies, Services & Equipment		814.00
Transportation		
Scheduled Airline		1,182.00
Trucks		3,110.00
Fuel		<u>973.00</u>
	Total	\$38.230.00

Prepared by:

FOX GEOLOGICAL SERVICES INC.

Peter E. Fox, Ph.D., P.Eng. January 21, 1999 12

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"Bedrock and Surficial Geology of the Fawnie Creek Map Area"; Geological Survey Branch Open File 1994-2

Fox, P. E. (1995)

Geochemical Assessment Report on the Taken 1 Claim ; Assessment Report by Fox Geological Consultants Ltd. for Phelps Dodge Corporation of Canada, Limited, January 16, 1995.

Fox, P. E. (1995)

Geological Report on the Taken 1 Claim ; Assessment Report by Fox Geological Services, Inc., for Phelps Dodge Corporation of Canada, Limited, December 22, 1995.

Fox, P. E. (1996)

Diamond Drilling, Geological and Soil Geochemical Report on the Tam Property (Tam 1 to 3, Taken 1 Mineral Claims); assessment report by Fox Geological Services Inc. for Phelps Dodge Corporation of Canada, Limited, December 20, 1996.

Pautler, Jean (1994)

1994 Assessment Report on the Tsacha Property ; by Teck Exploration Ltd., December, 1994.

Pautler, Jean (1995)

1995 Assessment Report on the Tsacha Property ; by Teck Exploration Ltd., December, 1995.

Pautler, Jean (1996)

Assessment Report on the 1996 Program on the Tsacha Property ; by Teck Exploration Ltd., December, 1996.

Teck Corporation (1998)

Drilling Resumes at Tsacha Property ; news release dated October 21, 1998 in Canada Stockwatch.

CERTIFICATE

- I, Peter Edward Fox, certify to the following:
- 1. I am a consulting geologist residing at #902 2077 Nelson Street, Vancouver, B.C.
- 2. I am a Professional Engineer registered in the Association of Professional Engineers and Geoscientists of British Columbia.
- 3. My academic qualifications are:

B.Sc. and M.Sc., Queens University, Kingston, Ontario Ph.D., Carleton University, Ottawa, Ontario

4. I have been engaged in geological work since graduation in 1966.

Peter E. Fox, Ph.D., P. Eng. Vancouver, B.C. January 21, 1999

APPENDIX I

SAMPLE DESCRIPTIONS AND SELECTED ANALYTICAL RESULTS

Phelps Dodge Corporation of Canada, Limited #912 - 120 Adelaide Street West, Toronto, Ontario M5H 1T1 Telephone (416) 594-0351 Fax (416) 594-0355

SAMPLE DESCRIPTIONS AND SELECTED ANALYTICAL RESULTS Taken Property, Project No. 231

SAMPLE	TYPE	MATERIAL	NORTH	EAST	REMARKS	Au(ppb)	Ag(ppb)	Cu(ppm)	Pb(ppm)	Zn(ppm)	As(ppm)	Cd(ppm)	Sb(ppm)	Hg(ppb)
Tranch Co.														
72405	mples	REDROCK				7.0	165	66	12	116.0	10	0.04	0.0	45
73495	CDAD	BEDROCK			TRENCH 1, SM. FELSIC CRISTAL TUFF	7.0	100	42.5	4.5	165.0	1.9	0.04	1.0	10
73/07	GRAD	BEDROCK			TRENCH 1-31M THEE OTZ-CARB VEINLETS	5.0 6.0	207	42.5	17.6	256.5	33	0.11	1.0	20
73963	CHIP	BEDROCK			TRENCH 1: 48-49 METRES	3.0	1764	133.9	2118.0	727.8	10.7	3.87	1.0	24
73964	CHIP	BEDROCK			TRENCH 1: 49-50 METRES	5.0	2371	100.0	2994 7	669.6	57	2 71	0.0	0
73965	CHIP	BEDROCK			TRENCH 1: 50-51 METRES	3.0	2956	215.2	3775 1	732.5	46.6	6.36	42	100
73966	CHIP	BEDROCK			TRENCH 1: 51-52 METRES	3.0	1525	118.8	774.4	1387.6	42.4	9.56	17	112
73967	CHIP	BEDROCK			TRENCH 1: 52-53 METRES	3.0	1247	155.8	571.3	2149.6	96.1	12.21	2.8	160
73498	CHIP	BEDROCK			TRENCH 1: 53-54 METRES	5.0	666	121.8	3905.8	1270.8	34.5	3.62	0.0	53
73499	CHIP	BEDROCK			TRENCH 1: 54-55 METRES	11.0	964	140.1	2116.0	608.1	54.2	3.67	3.0	56
71946	CHIP	BEDROCK			TRENCH 1: 55-56 METRES	13.0	2597	358.8	3784.8	758.8	132.2	8.41	6.1	132
71947	CHIP	BEDROCK			TRENCH 1: 56-57 METRES	14.0	10983	1419.3	13586.0	1193.3	691.0	16.29	10.5	370
71948	CHIP	BEDROCK			TRENCH 1: 57-58 METRES	45.0	14676	1977.9	12725.0	1091.5	744.2	15.74	14.4	426
71949	CHIP	BEDROCK			TRENCH 1: 58-59 METRES	17.0	2014	275.9	2873.1	645.5	110.2	5.57	15.0	188
71950	CHIP	BEDROCK			TRENCH 1: 59-60 METRES	10.0	2717	543.6	2194.5	851.7	98.8	5.62	14.9	203
71951	CHIP	BEDROCK			TRENCH 1: 60-61 METRES	2.0	8095	1906.5	73.6	512.8	153.9	3.88	4.6	84
71952	CHIP	BEDROCK			TRENCH 1: 61-62 METRES	6.0	33173	3594.8	60.7	342.3	156.5	8.01	7.5	90
71953	CHIP	BEDROCK			TRENCH 1: 62-63 METRES	5.0	7403	1242.1	39.9	501.8	132.7	4.16	3.8	86
71954	CHIP	BEDROCK			TRENCH 1: 63-64 METRES	2.0	3626	965.9	50.3	555.2	70.0	2.25	1.5	24
71955	CHIP	BEDROCK			TRENCH 1: 64-65 METRES	3.0	2511	583.2	296.2	723.4	161.9	3.71	3.2	44
71956	CHIP	BEDROCK			TRENCH 1: 65-66 METRES	5.0	996	330.9	334.6	697.3	71.6	3.07	1.3	33
71957	CHIP	BEDROCK			TRENCH 1: 66-67 METRES	8.0	20410	1984.8	45.8	434.8	159.5	5.34	3.8	57
71958	CHIP	BEDROCK			TRENCH 1: 67-68 METRES	1.0	7290	1063.4	29.2	338.7	231.0	2.78	5.8	115
71959	CHIP	BEDROCK			TRENCH 1: 68-69 METRES	1.0	3386	538.5	21.8	302.1	23.6	1.18	1.2	11
71960	CHIP	BEDROCK			TRENCH 1: 69-70 METRES	1.0	705	123.6	23.1	283.8	12.9	2.32	0.6	0
71961	CHIP	BEDROCK			TRENCH 1: 70-71 METRES	3.0	2004	445.7	19.7	421.2	80.4	3.28	1.4	56
71962	CHIP	BEDROCK			TRENCH 1: 71-72 METRES	6.0	536	114.9	19.5	239.0	20.7	1.60	0.5	18
71963	CHIP	BEDROCK			TRENCH 1: 72-73 METRES	3.0	968	323.5	14.4	235.8	5.6	1.09	0.3	22
71964	CHIP	BEDROCK			TRENCH 1: 73-74 METRES	3.0	616	164.5	18.0	241.4	13.3	1.10	0.4	31
71965	CHIP	BEDROCK			TRENCH 1: 74-75 METRES	3.0	424	154.3	12.2	181.0	12.2	0.93	0.9	16
71966	CHIP	BEDROCK			TRENCH 1: 75-76 METRES	1.0	443	171.5	10.0	179.2	9.0	0.86	0.8	0
71967	CHIP	BEDROCK			TRENCH 1: 76-77.5 METRES (END)	14.0	1232	431.9	9.4	197.7	3.5	0.68	0.4	26
Soil Test P	it Sampl	es												
73968	SOIL	TILL			PIT #1: 2.8 METRES DEPTH	8.0	69	10.6	5.3	60.8	6.7	0.22	0.3	0
73969	SOIL	TILL			PIT #1: 1.6 METRES DEPTH	2.0	240	15.2	6.9	65.4	6.4	0.23	0.4	0
73970	SOIL	TILL			PIT #1, 0.5 METRES DEPTH	4.0	138	20.8	10.1	/1.8	9.9	0.12	0.3	18
71767	SOIL	TILL			PIT #2: 3.7 METRES FROM SURFACE	2.0	112	31.4	10.3	90.4	4.2	0.35	0.3	17
71768	SOIL	TILL			PIT #2: 3 METRES DEPTH	1.0	125	27.7	12.0	90.8	6.7	0.41	0.4	25
71769	SOIL	TILL			PIT #2: 2.5 METRES DEPTH	1.0	/5	26.9	10.4	88.3	1.2	0.33	0.3	-24
71770	SOIL	IILL			PIT #2: 2 METRES DEPTH	1.0	92	26.9	11.0	90.0	5.4	0.38	0.4	0
71771	SOIL	TILL			PIT #2: 1.5 METRES DEPTH	6.0	/6	13.3	5.4	51.5	4.4	0.15	0.3	0
71772	SOIL					5.0	116	13.0	5.2	52.6	3.4	0.13	0.3	14
/1773	SOIL					0.0	102	24.9	10.3	81.8	6.0	0.30	0.3	0
71774	SOIL				PIT #3: 3.2 METRES DEPTH	1.0	82	18,4	8.1	56.9	5.0	0.10	0.3	11
71775	SOIL	11LL			PIT #3: 2.7 METRES DEPTH	3.0	99	25.9	10,3	84.4	4.2	0.32	0.4	31

		<u> </u>												
71776	SOIL	TILL			PIT #3: 2.2 METRES DEPTH	1.0	93	16.2	7.5	63.1	3.7	0.18	0.4	0
71777	SOIL	TILL			PIT #3: 1.7 METRES DEPTH	0.0	62	13.3	6.1	61.4	4.6	0.15	0.3	0
71778	SOIL	TILL			PIT #3: 1.2 METRES DEPTH	0.0	73	13.6	6.5	61.8	4.5	0.13	0.3	0
71779	SOIL	TILL			PIT #3: 0.7 METRES DEPTH	1.0	41	13.3	5.9	59.1	2.9	0.09	0.2	0
71780	SOIL	TILL			PIT #3: 0.2 METRES DEPTH	0.0	0	12.1	6.0	69.0	3.4	0.08	0.0	21
71781	SOIL	TILL			PIT #4: 3.5 METRES DEPTH	8.0	57	11.7	6.1	65.9	4.5	0.28	0.2	17
71782	SOIL	TILL			PIT #4: 3.0 METRES DEPTH	3.0	59	16.4	6.6	70.1	3.9	0.22	0.2	0
71783	SOIL	TILL			PIT #4: 2.5 METRES DEPTH	3.0	70	19.5	10.2	76.6	5.7	0.19	0.3	14
71784	SOIL	TILL			PIT #4: 2.0 METRES DEPTH	57.0	102	17.7	7.9	74.8	6.0	0.20	0.4	12
71785	SOIL	TILL			PIT #4: 1.5 METRES DEPTH	2.0	81	15.1	7.4	66.9	4.3	0.15	0.3	0
71786	SOIL	TILL			PIT #4: 1.0 METRE DEPTH	2.0	41	15.5	6.1	62.8	4.7	0.09	0.2	õ
71787	SOIL	TILL			PIT #4: 0.5 METRES DEPTH	7.0	130	13.3	7.1	72.9	3.2	0.08	0.2	11
73932	SOIL	TILL			PIT #5: 3.5 METRES DEPTH	1.0	45	19.8	8.0	76.2	3.7	0.16	0.3	14
73933	SOIL	TILL			PIT #5: 3.0 METRES DEPTH	2.0	69	19.0	8.8	77.0	2.3	0.20	0.3	11
73934	SOIL	TILL			PIT #5: 2.5 METRES DEPTH	1.0	58	21.8	10.4	87.1	5.1	0.21	0.4	10
73935	SOIL	TILL			PIT #5: 2.0 METRES DEPTH	7.0	237	19.9	8.8	63.1	4.3	0.10	0.6	33
73936	SOIL	TILL			PIT #5: 1.5 METRES DEPTH	13.0	577	28.1	14.6	67.3	9.2	0.08	1.0	14
73937	SOIL	TILL			PIT #6: 3.0 METRES DEPTH	16.0	1051	35.1	14.9	68.3	12.8	0.22	1.2	19
73958	SOIL	TILL			PIT #6: 2.5 METRES DEPTH	4.0	320	16.7	10.0	62.2	6.6	0.14	1.2	33
73959	SOIL	TILL			PIT #6: 2.0 METRES DEPTH	5.0	195	13.5	11.1	56.2	4.2	0.13	11	23
73960	SOIL	TILL			PIT #6: 1.5 METRES DEPTH	1.0	81	11.3	7.5	55.4	3.5	0.12	0.3	-0
73961	SOIL	TILL			PIT #6: 1.0 METRES DEPTH	1.0	46	12.0	6.2	55.4	3.9	0.08	0.0	14
73962	SOIL	TILL			PIT #6: 0.5 METRES DEPTH	1.0	84	10.3	6.9	55.0	43	0.05	0.3	0
Soil Samp	les									0010		0.00	0.0	Ŭ
73913	SOIL	COLLUVIUM	10100	11000		4.0	30	13.5	7.2	132.1	17	0 15	0.0	19
73914	SOIL	COLLUVIUM	10100	11050		8.0	161	20.0	14.2	63.3	7.8	0.10	0.0	12
73915	SOIL	COLLUVIUM	10100	11100		1.0	58	13.1	7.3	135.8	26	0.13	0.7	11
73916	SOIL	COLLUVIUM	10100	11150		0.0	138	7.8	9.0	113.4	1.5	0.22	0.0	10
73917	SOIL	COLLUVIUM	10100	11200		0.0	98	7.1	94	137.9	1.0	0.22	0.0	13
73918	SOIL	COLLUVIUM	10100	11250		0.0	58	86	79	99.1	1.5	0.21	0.0	13
73919	SOIL	COLLUVIUM	10100	11300		14.0	102	11.6	91	105.3	23	0.10	0.0	15
73920	SOIL	COLLUVIUM	10100	11350		0.0	44	79	87	83.9	16	0.12	0.0	10
73921	SOIL	COLLUVIUM	10100	11400		0.0	36	11 1	10.6	85.3	23	0.11	0.0	10
73922	SOIL	COLLUVIUM	10100	11450	CLAYEY	0.0	69	10.2	7 1	34.8	2.0	0.00	0.0	17
73923	SOIL	COLLUVIUM	10100	11500		0.0	146	12.3	8.3	86 1	3.2	0.07	0.0	12
73924	SOIL	COLLUVIUM	10100	11550		0.0	104	73	8.2	87.4	1.8	0.10	0.2	22
73925	SOIL	COLLUVIUM	10100	11600		1.0	122	9.0	13.4	128.6	2.0	0.03	0.2	17
73926	SOIL	COLLUVIUM	10100	11650		14.0	228	14.2	10.4	120.0	4.2	0.14	0.0	10
73927	SOIL	COLLUVIUM	10100	11700		4.0	102	15.2	83	78.4	5.0	0.10	0.2	19
73928	SOIL	COLLUVIUM	10100	11750			60	11 7	0.0 Q Q	107 1	3.0	0.10	0.2	10
73929	SOIL	COLLUVIUM	10100	11800		93.0	78	7.5	9.0 9.0	95.9	2.5	0.12	0.2	12
73930	SOIL	COLLUVIUM	10100	11850		0.0	57	11 0	0.5	JO 5	2.5	0.09	0.0	13
73931	SOIL	COLLIVIUM	10100	11900		0.0		12.2	9.0 8 0	49.5	2.1	0.09	0.2	10
74630	SOIL	COLLIVIUM	10300	10600		0.0	200	10.2	10.9	214.7	2.0	0.07	0.2	10
74631	SOIL	COLLIVIUM	10300	10650		0.0	209	10.5	11.0	214.7	2.0	0.40	0.0	19
74632	SOIL	COLLIVIUM	10300	10000		0.0	222	9.9	10.0	93.7	1.9	0.25	0.0	22
74622	SOIL	COLLIVIUM	10300	10750		20.0	72	0.1 11 Q	10.8	90.9 80.0	1.0	0.10	0.0	23
74624	SOIL	COLLINAUM	10200	10200		20.0	10	11.0	(). <i>(</i>	0U.Z	3.1 A A	0.11	0.0	15
74626	SOIL	COLLINIUM	10200	10000		0.0	00 75	10.0	0.0	00.7	4,4	0.11	0.0	14
74626	SOIL	COLLOVIUM	10200	10000		0.0	15 67	10.0	0.9	92.0	4.0	0.13	0.0	0
72020	SOIL	COLLINIUM	10300	10900		0.0	0/	11.0	0.0	0U./ 51.0	3.9	0.14	0.0	24
72020	SOL	COLLOVIUM	10300	11000		0.0	202	11.4	10.7	51.9	1.5	0.14	0.0	33
12928	SUL	COLLOVIUM	10300	11000		0.0	80	15.9	10.9	57.9	3.0	0.08	0.2	20

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73940	SOIL	COLLUVIUM	10300	11050		0.0	100	12.2	9.6	98.0	2.2	0.17	0.2	16
73941	SOIL	COLLUVIUM	10300	11100		1.0	88	8.3	11.8	79.8	2.6	0.12	0.2	15
73942	SOIL	COLLUVIUM	10300	11150		0.0	138	10.0	10.0	80.7	2.3	0.12	0.3	0
73943	SOIL	COLLUVIUM	10300	11200		0.0	144	7.8	8.9	94.3	1.7	0.22	0.0	17
73944	SOIL	COLLUVIUM	10300	11250		0.0	216	7.8	12.5	91.9	2.7	0.14	0.2	27
73945	SOIL	COLLUVIUM	10300	11300		1.0	218	7.4	10.3	116.7	2.1	0.17	0.2	22
73946	SOIL	COLLUVIUM	10300	11350		0.0	37	7.9	7.2	83.8	2.7	0.10	0.0	26
73947	SOIL	COLLUVIUM	10300	11400		0.0	50	7.1	7.2	80.9	2.4	0.10	0.0	29
73948	SOIL	COLLUVIUM	10300	11450		0.0	35	8.2	7.8	79.3	2.9	0.09	0.0	27
73949	SOIL	COLLUVIUM	10300	11500		0.0	65	8.0	7.9	72.9	2.5	0.11	0.2	15
73950	SOIL	COLLUVIUM	10300	11550		0.0	82	8.1	11.1	97.4	2.6	0.14	0.2	18
73951	SOIL	COLLUVIUM	10300	11600		0.0	0	8.6	10.7	74.6	4.4	0.10	0.2	24
73952	SOIL	COLLUVIUM	10300	11650		5.0	66	10.3	23.6	62.6	4.1	0.15	0.3	22
73953	SOIL	COLLUVIUM	10300	11700		0.0	101	11.1	12.7	91.5	3.0	0.15	0.2	24
73954	SOIL	COLLUVIUM	10300	11750		0.0	43	7.4	10.2	70.6	1.8	0.10	0.2	11
73955	SOIL	COLLUVIUM	10300	11800		0.0	35	7.5	8.7	126.5	3.0	0.11	0.0	26
73956	SOIL	COLLUVIUM	10300	11850		0.0	36	9.1	8.7	53.3	1.8	0.12	0.2	21
73957	SOIL	COLLUVIUM	10300	11900		2.0	249	19.6	19.4	215.9	5.5	0.35	0.5	38
71751	SOIL	COLLUVIUM	10500	10700		3.0	106	8.4	7.9	68.0	1.1	0.10	0.0	11
71752	SOIL	COLLUVIUM	10500	10750		7.0	283	17.9	26.0	209.1	2.0	0.75	0.6	36
71753	SOIL	COLLUVIUM	10500	10800		1.0	89	11.5	8.9	52.8	3.1	0.10	0.2	10
71754	SOIL	COLLUVIUM	10500	10850		51.0	150	11.5	11.2	102.9	2.2	0.17	0.2	20
71755	SOIL	COLLUVIUM	10500	10900	BROWN-GREY	3.0	88	10.5	7.6	72.0	1.6	0.08	0.2	18
71756	SOIL	COLLUVIUM	10500	10950		1.0	70	12.1	9.0	53.8	3.1	0.10	0.3	0
71757	SOIL	COLLUVIUM	10500	11000		0.0	110	5.9	9.5	93.4	1.0	0.10	0.2	0
71758	SOIL	COLLUVIUM	10500	11050		1.0	185	10.2	10.3	104.2	1.5	0.57	0.2	10
71759	SOIL	COLLUVIUM	10500	11100		0.0	162	10.5	8.6	76.6	2.4	0.11	0.2	15
71760	SOIL	COLLUVIUM	10500	11150		0.0	128	12.3	9.6	84.0	2.3	0.12	0.2	0
71761	SOIL	COLLUVIUM	10500	11200		0.0	362	36.0	12.7	147.9	5.5	0.40	0.4	27
71762	SOIL	COLLUVIUM	10500	11250		0.0	179	9.5	7.9	70.4	2.9	0.21	0.2	14
71763	SOIL	COLLUVIUM	10500	11300		1.0	304	30.7	8.7	78.2	3.4	0.14	0.4	10
71764	SOIL	COLLUVIUM	10500	11350	SANDY	0.0	115	23.7	8.7	52.6	3.6	0.07	0.4	24
71765	SOIL	COLLUVIUM	10500	11400		0.0	56	10.5	8.3	72.8	3.4	0.09	0.0	0
71766	SOIL	COLLUVIUM	10500	11450	10 NORTHWEST OF 104+00N, 114+75E	6.0	50	16.4	8.7	56.4	3.5	0.06	0.3	13

APPENDIX II

GEOCHEMICAL ANALYSES

ANALYTICAL PROCEDURES

Rock and Soil Samples:

- ICP: A 15 gram sample is digested with 90 millilitres 3-1-2 HCI-HNO₃-H₂O at 95° Centigrade for one hour and is diluted to 300 millilitres with water. This leach is partial for Mn, Fe, Sr, Ca, P, La, Cr, Mg, Ba, Ti, B, W and limited for Na, K, Ga and Al. Solution is analysed directly by ICP. Mo, Cu, Pb, Zn, Ag, As, Au, Cd, Sb, Bi, Tl, Hg, Se, Te and Ga are extracted with MIBK-aliquat 336 and analysed by ICP.
- Au: Gold is extracted by aqua-regia/MIBK extract, GF/AA finished.

)ME (TO	LYTI)]	LA A	TOR)Ľ	FĽ	1	É	e . 1	ŀ	ING		1.	V	bu	VI.	B		h	LR6] p	Ĥ.	_16	04,]	-3:	IFI	<u>مx</u> , .	. Jī	25.	_F	1.6	
AA	30 3002	ACI	STeat	.ceu c	0.)		GE(oche	MIC	al I	CXT	RA	CT	ION	-AN	ALS	SI	s (IER	тт	TIC	ATI	3									A	A	
				<u>F</u>	<u>ox (</u>	leol	oq	ical	Co	nsu.	lta	nt	8	PRO	JEC	T. 2	231	I	711	e i	# 9	804	186	6										
						1409	+ 40	9 Gran	ville	St.,	Vanc	ouve	er B	C V6C	118	Su	bmit	ted	by: S	Step	nen l	lethe	rup									Ŀ		
SAMPLE#		Mo	Cu	Pb	Zn	Ag	Ni	Co Mi	n Fe	As	U	Th	Sr	Cd	Sb	Bi	V	Ca	P ¥	La	Cr	Mg	Ba	Ti	В	Al	Na K	W	T1 H	g Se	Te	Ga Au	+ -	
71046		2.0	250.0	2704.0	750.0	0503	<u> </u>			100.0	ppm	Phu		- ppm	ppii	-ppiii	ppin		*		<u>hhu</u>	* ;		<u> </u>			* *	ppin p	л рі	o ppm	ppm p	pm pp		
71940		<1.4	1419.3	13585.7	1193.3	10983	11	15 238	2.25	132.2 691.0	<5 <5	4 15	33	8.41	6.1 10.5	<2.8	15 1 35	.88	.031	7 9	15 13	.22 2	207<. L72 .	01 01	4 5	.38 .77	01 .28 02 .31	2<2 <?</td <td>.8 13 .8 37</td> <td>2<4.2: 0<4 2:</td> <td><2.8 <2.8</td> <td><7] <7]</td> <td>3</td> <td></td>	.8 13 .8 37	2<4.2: 0<4 2:	<2.8 <2.8	<7] <7]	3	
71948		3.2	1977.9	12724.5	1091.5	14676	3	7 260	3 1.91	744.2	<5	15	38	15.74	14.4	<2.6	9 1	1.12	.023	10	10	.29	365<.	01	4	32<.	01 .24	2<2	.6 42	6<3.9	<2.6<6	.5 4	15	
71949		4.2	2/5.9 543.6	28/3.1 2194.5	645.5 851.7	2014 2717	8 12	21 402	3 4.33	98.8	ہ 5<	4 4	16 45	5.5/	15.0 14.9	<1 <1.2	10 34 1	.67 1.54	.024	5 6	9 19	.05 .38 2	65. 245.	01 02	4 7	.35<. .81 .	01 .21 02 .47	<2 <2<1	<1 180 .2 20	8<1.5 3<1.8	<1<2 <1.2	.5 1 <3 1	l7 l0	
71951		3.0	1906.5	73.6	512.8	8095	13	18 395	3 3.87	153.9	5	2	51	3.88	4.6	<.2	36	1.72	.062	5	10	.34 4	24	01	9	84	01 51	<2 <	2 8	4 < 3	< 21	2	2	
71952		2.1	3594.8	60.7	342.3	33173	6	13 348	2 2.72	156.5	<5	2	72	8.01	7.5	12.7	35 2	2.92	.050	4	12	.74]	. 68	01	10	91 .	01 .57	<2 <	.2 9	0 <.3	<.2 2	.4	6	
71955		1.9	965.9	50.3	555.2	3626	13	20 508	5 4.44	70.0	<5	<2	45 58	4.16	3.8	3.1	3/ 1	L.80 L.95	.044	6 7	9 10	.35 4	106 . 106 .	01 01	8 10	.82 . .83 .	01 .49 01 .48	<2 <2 <	.6 80	5 <.3 4 <.3	.23	.0	5 2	
71955		1.9	583.2	296.2	723.4	2511	14	21 530	\$ 5.10	161.9	<5	<2	77	3.71	3.2	<.2	33 2	2.63	.051	6	14	.51 4	122 .	01	7	71 .	01.44	<2 <	.2 4	4 <.3	<.2 1	.1	3	
71956		2.2	330.9	334.6	697.3	996	10	17 415	3.97	71.6	<5	2	43	3.07	1.3	<.2	32	1.56	.045	6	14	.33 3	342 .	01	7	. 68 .	01.43	<2 <	.2 3	3 <.3	<.2 1	.1	5	
71958		2.4	1964.6	45.8 29.2	434.0 338.7	7290	o 4	11 316	5 3.00	231.0	<5	<2	89 39	5.34 2.78	3.8 5.8	<.2 .5	31 31	3.22 1.52	.041	5	9 7	.89 /	437 . 451 .	01 02	8	.61. .84.	01 .39 01 .54	<2 <	.2 5. .2 11!	/ <.3 5 <.3	<.2	.6 .3	8 1	
71959		2.1	538.5	21.8	302.1	3386	5	12 257	1 3.37	23.6	<5	<2	19	1.18	1.2	.2	39	.73	.046	9	7	.11 4	457 .	02	5	.71 .	01.46	<2 <	.2 1	1 <.3	<.2 1	.2	1	
71500		1.5	125.0	20.1	203.0	705		11 345		12.9			51	2.52	.0	~.2	34.	1.41	.041	12	9	.20 1	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		/	.89 .	01.54	~~~~	.2 <11	0 <.3	<.2	.9	1	
71961 71962		2.1	445.7	19.7	421.2	2004 536	5 1	13 382	i 3.43 L 2.32	20.7	<5 <5	~2	42 10	3.28	1.4	.3	29 2 12	2.07	.053	10 13	6 3	.38	369 . 200<.	01 01	6 4	.81 . 43<	01 .49 01 .26	<2 <	.2 51 2 11	6 <.3 8 < 3	<.2 < 2	.7 9	3 6	
71963		1.9	323.5	14.4	235.8	968	3	7 247	7 2.61	5.6	<5	<2	13	1.09	.3	<.2	15	.90	.071	12	3	.05	348 .	01	4	.59 .	01.39	<2 <	.2 2	2 <.3	<.2	.8	3	
RE 71963 71964		2.5	321.8	14.3	237.5	616	3	8 287	3 2.60	5.0 13.3	<5 <5	~2 <2	13	1.10	.3 .4	<.2 <.2	14 16	.90 .26	.0/2	11 16	2 4	.05 3	346 . 370 .	01 01	6 4	.64 . .66<.	01 .42 01 .39	<2 < <2	.2 10 .2 3	0 <.3 1 <.3	<.2 <.2 1	.6 .2	5 · 3	
71965		2.6	154.3	12.2	181.0	424	4	6 221	3 2 35	12.2	<5	<2	10	93	9	< 2	13	25	067	14	4	04 3	227	01	3	170	01 29		2 1	6 < 3	<pre></pre>	n	2	
71966		3.3	171.5	10.0	179.2	443	1	6 237	2.15	9.0	< <u>5</u>	<2	14	.86	.8	<.2	14	.34	.076	13	6	.05 4	409 .	01	4	48.	01 .31	<2 <	.2 <1	0 <.3	<.21	.2	1	
/196/ 73495		2.4	431.9	9.4	197.7	1232	4	7 214	32.45	3.5	<5 5	2 <2	10	.68	.4	1.3	18 11	.21	.073	12	4	.05 :	191 . 07e	01	3 ⊿	.46 .	01.26	<2 <	.2 2	6 <.3	<.2	.9 1	.4	
73496		1.9	42.5	14.1	165.9	287	ĝ	13 288	3 3.94	6.1	<5	<2	21	.11	1.3	<.2	85	.17	.073	10	12	.14 9	926 .	03	5	.54 .	01 .37	<2	.3 2	0 <.3	<.2 2	.5	5	
73497		1.0	41.7	17.6	256.5	285	8	19 409	5 4.72	3.3	<5	2	13	.89	.4	<.2	53	.85	.083	12	7	.19 :	335 .	01	10 1	.06.	01.65	<2	.3 2	4 <.3	<.2 2	.1	6	
73498 73499		3.6	121.8	3905.8	1270.8	665 964	6 2	17 371	54.55 72.40	34.5	<5 <5	6 4	16 9	3.62	<1.6	<1.6 <1	30 12	.23	.074	10 12	5 15	.09 1	167 . 88<	01 01	6 4	.77 . 37<	01 .48 01 26	<2<1	.6 5 <1 5	3<2.4 6<1 5	<1.6	<4 5 1	5	
73963		1.9	133.9	2118.0	727.8	1764	6	13 323	3 3.65	10.7	<5	3	15	3.87	1.0	<1	28	.26	.064	8	5	.11	173	01	7	.77 .	01 .49	<2 ·	<1 3	0<1.5	<1<2	2.5	3	
73964		3.6	127.2	2994.7	669.6	2371	5	12 296	3 2.88	5.7	<5	4	11	2.71	<1.8	<1.8	20	.13	.040	10	9	.06 :	145 .	01	5	.58.	01 .37	<2<1	.8 <1	0<2.7	<1.8<4	.5	5	
73965 73966		3.4	215.2	3775.1	732.5	2956 1525	6	9 331	5 2.59	46.6	<5	5	15 16	6.36	4.2	<2.2	20 24	.35	.063	9	6	.08	147.	01	4	.70.	01.44	<2<2	.2 10	0<3.3	<2.2<5	5.5	3	
73967		1.5	155.8	571.3	2149.6	1247	6	18 451	0 4.71	96.1	<5	2	22	12.21	2.8	<.2	31	.64	.045	7	2	.13	441 .	01	6	.79. .78.	01.48	<2	.2 16	23 03	<.21	5	3	
STANDARD D	2/C3/AU-R	23.2	124.5	96.2	258.5	1865	29	17 97	2 4.22	68.0	24	21	59	2.01	8.7	17.1	69	.71	.106	17	55 1	.06	226 .	11	29 2	. 19 .	05 .64	12 1	.9 93	1.5	1.4 5	.3 49	8	

ICP - 15 GRAM SAMPLE IS DIGESTED WITH 90 ML 2-2-2 HCL-HN03-H20 AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 300 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K GA AND AL. SOLUTION ANALYSED DIRECTLY BY ICP. MO CU PB ZN AG AS AU CD SB BI TL HG SE TE AND GA ARE EXTRACTED WITH MIBK-ALIQUAT 336 AND ANALYSED BY ICP. ELEVATED DETECTION LIMITS FOR SAMPLES CONTAIN CU, PB, ZN, AS>1500 PPM, Fe>20%. - SAMPLE TYPE: ROCK AU+ - AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: NOV 2 1998

DATE REPORT MAILED: Nov 16/98 SIGNED BY. A. D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

		FI 202.2	- LAI	dite	COR:		LTD		8 100	<u>]</u> нем			ENG	קרי	.). 	v	JUN ANT	ле. ат. ч	_ J	ī. 		.6 T 12 T	F	PHC.	Jō	04,	7 ر	31.	.F	AX \	J	25.	/	16
AA				F	<u>ox (</u>	<u>Gec</u>	<u>)10</u>	<u>gic</u> .09 -	al 409 (<u>Con</u> irany	sul ile:	<u>ta</u> St.,	nts Van	s Pl	ROJ ir BC		7001 178	31 Sul	Fi Fi	le d by	#:: St	980 epher	486 1 Wet	57 herup	P	age	1							A
SAMPLE#	Mo ppm	Cu ppm	Pb ppn	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	pbw k	Th pm p	Sr opm	Cd ppm	Sb ppm	Bi ppm	V mqq	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti % p	B	Al %	Va %	K V % ppr	ITL nppm	Hg ppb	Se ppm	Te ppm p	Ga A opm p	ku+ xpb
71767 71768 71769 71770 71771	1.1 1.2 1.2 1.0 .7	31.4 27.7 26.9 26.9 13.3	10.3 12.0 10.4 11.0 5.4	90.4 90.8 88.3 90.0 51.5	112 125 75 92 76	18 19 18 18 10	16 16 17 17 9	764 1014 923 993 515	3.99 3.93 3.85 3.91 2.49	4.2 6.7 7.2 5.4 4.4	<5 <5 <5 <5 <5	3 3 3 3 2	82 80 75 74 50	.35 .41 .33 .38 .15	.3 .4 .3 .4 .3	<.2 <.2 <.2 <.2 <.2 <.2	79 77 76 78 63	1.45 1.42 1.35 1.08 .57	.125 .127 .123 .126 .091	19 18 18 19 12	24 20 20 18 19	.75 .72 .67 .66 .38	175 184 175 180 115	.23 .23 .22 .22 .22	<3 1. <3 1. <3 1. <3 1. <3 1. <3 .	58 . 57 . 55 . 58 . 74 .	07 .1 07 .1 07 .1 07 .1 07 .1	8 <2 8 <2 7 <2 6 <2 5 <2	2 <.2 2 <.2 2 <.2 2 <.2 2 <.2 2 <.2	17 25 24 <10 <10	<.3 <.3 <.3 <.3 <.3	<.2 6 <.2 6 <.2 6 <.2 6 <.2 3	5.2 5.5 5.0 5.3 5.3	2 1 1 1 6
71772 71773 71774 71775 71776	.7 1.0 1.0 1.0 1.0	13.0 24.9 18.4 25.9 16.2	5.2 10.3 8.1 10.3 7.5	52.6 81.8 56.9 84.4 63.1	116 102 82 99 93	10 17 12 17 12	9 15 10 16 11	454 860 408 903 603	2.64 3.67 3.34 3.75 3.17	3.4 6.0 5.0 4.2 3.7	<5 <5 5 5 5 5	2 3 2 3 2 3 2	54 73 47 72 58	.13 .30 .10 .32 .18	.3 .3 .4 .4	<.2 <.2 <.2 <.2 <.2	67 73 77 76 76	.56 1.35 .55 1.21 .66	.089 .117 .067 .120 .100	12 17 15 18 14	18 22 28 20 19	.37 .63 .32 .63 .43	98 189 101 188 144	.23 .22 .30 .22 .25	<3 . <3 1. <3 1. <3 1. <3 1. <3 .	72 . 44 . 42 . 47 . 90 .	04 .0 07 .1 05 .0 07 .1 05 .0	5 <2 5 <2 8 <2 6 <2 7 <2	2 <.2 2 <.2 2 <.2 2 <.2 2 <.2 2 <.2	14 <10 11 31 <10	<.3 <.3 <.3 <.3 <.3	<.2 <.2 <.2 <.2 <.2 <.2 <.2	5.3 5.9 5.6 5.9	5 <1 1 3 1
71777 71778 71779 71780 71781	.8 .9 .9 1.0 1.1	13.3 13.6 13.3 12.1 11.7	6.1 6.5 5.9 6.0 6.1	61.4 61.8 59.1 69.0 65.9	62 73 41 <30 57	12 11 14 15 13	11 10 10 10 11	578 495 425 351 545	3.06 3.08 3.20 3.35 3.17	4.6 4.5 2.9 3.4 4.5	<5 <5 <5 <5 <5	2 2 2 3 2	47 67 65 32 58	.15 .13 .09 .08 .28	.3 .3 .2 <.2	<.2 <.2 <.2 <.2 <.2	75 73 76 87 81	.56 .68 .67 .39 .62	.089 .112 .120 .095 .095	14 15 17 14 13	23 22 27 28 23	.45 .38 .36 .31 .43	113 140 106 83 95	.22 .26 .27 .36 .26	<3 . <3 . <3 1. <3 1. <3 .	76 . 90 . 15 . 67 . 81 .	04 .0 06 .0 05 .0 03 .0 04 .0	5 <2 6 <2 9 <2 5 <2	2 <.2 2 <.2 2 <.2 2 <.2 2 <.2 2 <.2	<10 <10 <10 21 17	<.3 <.3 <.3 <.3 <.3	<.2 3 <.2 4 .2 5 <.2 6 <.2 4	5.6 5.4 5.3 4.5	<1 <1 1 <1 8
71782 71783 71784 71785 71786	.8 .9 1.0 .9 1.0	16.4 19.5 17.7 15.1 15.5	6.6 10.2 7.9 7.4 6.1	70.1 76.6 74.8 66.9 62.8	59 70 102 81 41	14 14 17 15 17	12 12 14 12 13	661 676 686 592 510	3.46 3.58 4.06 3.58 3.87	3.9 5.7 6.0 4.3 4.7	<5 <5 <5 <5 <5	2 2 2 2 3	64 55 54 50 50	.22 .19 .20 .15 .09	.2 .3 .4 .3 .2	<.2 <.2 <.2 <.2 <.2	82 84 101 89 93	.70 .59 .58 .52 .48	.113 .102 .101 .098 .081	16 14 14 14 16	25 24 25 24 26	.43 .46 .53 .48 .48	133 124 100 91 126	.27 .23 .27 .27 .27	<3 1. <3 1. <3 . <3 . <3 .	02 . 04 . 99 . 99 . 60 .	05 .0 04 .0 04 .0 03 .0 03 .0	6 <2 6 <2 5 <2 6 <2	2 <.2 2 <.2 2 <.2 2 <.2 2 <.2 2 <.2	<10 14 12 <10 <10	<.3 <.3 <.3 <.3 <.3	<.2 / <.2 / <.2 / <.2 / <.2 /	4.4 4.6 5.0 4.7 5.3	3 3 57 2 2
71787 RE 71787 73932 73933 73934	1.2 1.2 1.1 1.0 1.1	13.3 13.4 19.8 19.0 21.8	7.1 7.2 8.0 8.8 10.4	72.9 72.5 76.2 77.0 87.1	130 133 45 69 58	16 15 14 15 15	12 12 14 15 15	313 315 805 881 848	3.60 3.64 3.51 3.58 3.78	3.2 5.3 3.7 2.3 5.1	6 5 5 5 5 5	2 2 3 3 3	20 20 56 59 58	.08 .08 .16 .20 .21	.2 .2 .3 .3	<.2 <.2 <.2 <.2 <.2	92 92 71 73 74	.25 .24 .68 .74 .71	.090 .090 .099 .099 .099 .105	9 9 18 18 20	27 24 16 18 19	.34 .34 .49 .51 .52	114 114 103 102 137	.27 .28 .24 .24 .25	<3 1. <3 1. <3 1. <3 1. <3 1. <3 1.	.85 . .85 . .33 . .33 . .51 .	02 .0 02 .0 05 .1 06 .1 05 .1	4 < 4 < 1 < 2 <	2 <.2 2 <.2 2 <.2 2 <.2 2 <.2 2 <.2	11 16 14 11 10	<.3 <.3 <.3 <.3 <.3	<.2 (<.2 (<.2 5 <.2 5 <.2 5 <.2 5	5.7 5.6 5.4 5.6 5.0	7 4 1 2 1
73935 73936 73937 73958 73959	.8 1.1 1.1 1.0 1.0	19.9 28.1 35.1 16.7 13.5	8.8 14.6 14.9 10.0 11.1	63.1 67.3 68.3 62.2 56.2	237 577 1051 320 195	12 10 9 8 8	10 9 12 9 8	553 438 1006 837 1036	3.17 3.10 3.06 2.79 2.62	4.3 9.2 12.8 6.6 4.2	<5 <5 5 <5 5 5 5	3 2 2 2 3	41 37 73 43 41	.10 .08 .22 .14 .13	.6 1.0 1.2 1.2 1.1	<.2 <.2 <.2 <.2 <.2	71 72 61 63 59	.56 .50 3.34 .84 .60	.097 .069 .102 .093 .091	16 16 14 15 17	17 21 16 15 16	.37 .25 .27 .25 .23	199 183 437 391 365	.25 .27 .14 .22 .22	<3 1. <3 1. <3 . <3 . <3 .	.30 . .24 . .79 . .85 . .77 .	04 .0 04 .1 06 .1 05 .1 05 .1	9 < 0 < 3 < 0 < 1 <	2 <.2 2 <.2 2 <.2 2 <.2 2 <.2	33 14 19 33 23	<.3 <.3 <.3 <.3 <.3	<.2 <.2 <.2 <.2 <.2 <.2	4.9 4.9 3.3 3.7 3.2	7 13 16 4 5
73960 73961 73962 STANDARD	.9 1.0 1.1 24.7	11.3 12.0 10.3 118.0	7.5 6.2 6.9 92.3	55.4 55.4 55.0 251.9	81 46 84 2165	11 12 12 29	9 9 9 17	491 442 371 992	2.97 3.23 3.26 4.21	3.5 3.9 4.3 70.2	<5 <5 <5 16	2 2 2 20	52 45 33 58	.12 .08 .05 2.10	.3 .2 .3 8.7	<.2 <.2 <.2 21.1	79 81 86 68	.62 .59 .44 .72	.098 .091 .050 .106	14 16 10 17	18 21 22 52	.34 .34 .30 1.10	145 124 126 226	.26 .27 .37 .11	<3 1. <3 1. <3 1. 26 2.	.77 . .08 . .56 . .19 .	05 .0 04 .0 03 .0 05 .0	16 <; 16 <; 17 <; 54 1;	2 <.2 2 <.2 2 <.2 4 2.3	<pre><10 14 <10 <10 <70 </pre>	<.3 <.3 <.3 .4	<.2 <.2 <.2 2.0	3.7 4.4 5.7 7.2	1 1 1 51

Standard is STANDARD D2/C3/AU-S.

ICP - 15 GRAM SAMPLE IS DIGESTED WITH 90 ML 2-2-2 HCL-HN03-H20 AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 300 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K GA AND AL. SOLUTION ANALYSED DIRECTLY BY ICP. MO CU PB ZN AG AS AU CD SB BI TL HG SE TE AND GA ARE EXTRACTED WITH MIBK-ALIQUAT 336 AND ANALYSED BY ICP. ELEVATED DETECTION LIMITS FOR SAMPLES CONTAIN CU,PB,ZN,AS>1500 PPM,Fe>20%. - SAMPLE TYPE: SOIL AU+ - AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED. <u>Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.</u>

DATE RECEIVED: NOV 2 1998 DATE REPORT MAILED: NOV 16/98 SIGNED BY. A.D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

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ADE ANALYTICAL				F	ox	Ge	old	ogic	al	Cor	isu	lta	ant	s I	PRO	JEC	т 2	231	F	ILI	3 #	98	04	867	,			F	ag	e :	2			ACHE	ANALYTICAL
SAMPLE#	Mo ppm	Cu ppm	Pb ppm	2n ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Tî %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
73968 73969 73970 RE 73969	.9 .8 .9	10.6 15.2 20.8 16.3	5.3 6.9 10.1 7.1	60.8 65.4 71.8 64.3	69 240 138 254	13 13 16 13	13 13 16 13	710 672 756 671	2.93 3.22 3.88 3.23	6.7 6.4 9.9 6.7	18 5 11 19	3 2 4 2	44 48 52 47	.22 .23 .12 .24	.3 .4 .3	<.2 <.2 <.2 <.2	75 78 75 78	.54 .60 .75	.100 .104 .105 .102	13 14 23 14	23 21 24 23	.41 .45 .55	139 126 136 123	.19 .20 .21	<3 3 <3 1 <3	.69 .85 .55	.03 .03 .04 .03	.05 .06 .12	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <	<.2 <.2 <.2 <.2	<10 <10 18 <10	<.3 <.3 <.3 <.3	<.2 <.2 <.2 <.2	3.5 4.0 5.9 4.3	8 2 4 2
STANDARD	25.8	123.5	101.3	267.8	2185	29	18	1003	4.30	72.3	32	21	56	2.19	8.8	18.9	69	.72	.107	16	56	1.11	250	.13	31 2	.25	.05	.67	15	2.4	930	.6	2.2	6.9	46

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data_AFA

) EM	רצן 50 90	CI DO2 1)LA Accr	E edit	rori ed C	0.)	LTD) 8		. I		LNG	K).	v .	lu	VE	ł	<u>v</u> _	- 1	R6	J	PH	ί]60	4 , -]-:	1.	. Fi	.	. 5	25	/	16
##				E	<u>′ox</u>	Geo	<u>210</u> 14	<u>gic</u> 09 -	EOC <u>al</u> 409 (HEM <u>Cor</u> Iranv	ILC2 (SU) Ille	AL <u>Lta</u> St.,	EX: <u>nt:</u> Van	I'RA <u>3 P</u> couvi	CT. <u>ROL</u> er Bi	ION <u>JEC'</u> c v6c	- AN <u>F 2</u> 178	NAL 231 S	YSI: F: ubmiti	S C ile ted b	'ER' # %; \$	CIF 98 tephe	ICA 046 en We	TE 12 ther	up	Pa	ge	l						A	
SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V mqq	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	К %	M M	T L Drac	Hg ppb	Se opm (Te ppm p	Ga/ ppm p	lu+ Spb
71751 71752 71753 71754 71755	.6 1.9 .8 1.1 .8	8.4 17.9 11.5 11.5 10.5	7.9 26.0 8.9 11.2 7.6	68.0 209.1 52.8 102.9 72.0	106 283 89 150 88	9 10 10 10 12	7 11 9 9 7	385 1629 408 852 303	2.36 3.28 2.65 2.75 2.71	1.1 2.0 3.1 2.2 1.6	<5 <5 5 9 5	<2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	24 35 27 26 23	.10 .75 .10 .17 .08	<.2 .6 .2 .2	<.2 <.2 <.2 <.2 <.2 <.2	62 56 71 66 75	.34 .62 .41 .36 .35	.040 .237 .070 .067 .100	10 11 13 10 9	20 19 22 24 22	.26 .26 .29 .24 .22	93 728 76 340 117	.19 .07 .22 .16 .22	<3 <3 <3 <3 <3 <3	1.03 1.56 .96 1.44 1.18	.02 .01 .02 .02 .02	.07 .11 .08 .09 .06	<2 < <2 < <2 < <2 < <2 <	<.2 <.2 <.2 <.2	11 36 10 20 18	<.3 < <.3 < <.3 < <.3 <	<.2 2 <.2 4 <.2 4 <.2 5	.2	3 7 1 51 3
71756 71757 71758 71759 71760	1.1 .7 .9 .9 .8	12.1 5.9 10.2 10.5 12.3	9.0 9.5 10.3 8.6 9.6	53.8 93.4 104.2 76.6 84.0	70 110 185 162 128	10 8 10 14 11	8 6 7 8 7	247 380 405 265 282	2.68 2.29 2.62 2.87 2.43	3.1 1.0 1.5 2.4 2.3	6 <5 9 5 5	<2 <2 <2 <2 <2 <2 <2	28 24 36 29 28	.10 .10 .57 .11 .12	.3 .2 .2 .2 .2	.2 <.2 <.2 <.2 <.2	70 57 63 70 58	.35 .39 .71 .40 .34	.083 .099 .147 .167 .114	9 9 8 8 9	23 18 20 23 19	.24 .18 .23 .26 .22	79 258 303 147 101	.23 .18 .20 .20 .20	<3 <3 <3 <3 <3	1.32 1.24 1.25 1.54 1.33	.02 .02 .02 .02 .02	.05 .07 .08 .07 .06	<2 < <2 < <2 < <2 < <2 <	<.2 <.2 <.2 <.2	<10 <10 10 15 <10	<.3 < <.3 < <.3 < <.3 <	<.2 7 <.2 4 <.2 4 <.2 5	.3	1 <1 1 <1 <1
71761 71762 71763 71764 71765	1.0 1.0 .8 .8 1.1	36.0 9.5 30.7 23.7 10.5	12.7 7.9 8.7 8.7 8.3	147.9 70.4 78.2 52.6 72.8	362 179 304 115 56	10 10 11 13 14	10 8 9 10	870 349 382 394 289	2.39 2.65 2.80 3.33 3.21	5.5 2.9 3.4 3.6 3.4	9 <5 <5 <5 <5	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2	26 37 23 33 22	.40 .21 .14 .07 .09	.4 .2 .4 .4 .2	.2 <.2 <.2 <.2 <.2	54 66 64 74 86	.39 .38 .36 .53 .31	.167 .176 .061 .056 .134	9 7 12 16 7	17 17 18 21 24	.21 .25 .32 .48 .30	272 85 134 162 85	.16 .16 .20 .22 .22	ও ও ও ও ও ও ও ও ও ও ও ও ও ও ও ও ও ও	1.18 1.20 1.17 1.30 1.43	.01 .01 .02 .03 .01	.08 .06 .07 .06 .05	<2 < <2 < <2 < <2 < <2 <	<.2 <.2 <.2 <.2	27 - 14 - 10 - 24 - <10 -	<.3 < <.3 < <.3 < <.3 <	<.2 5 <.2 5 <.2 4 <.2 4 <.2 5	.5 .4 .9 .8	<া <া <া <া
RE 71765 71766 73913 73914 73915	1.0 1.0 1.2 1.6 1.2	10.2 16.4 13.5 20.0 13.1	8.7 8.7 7.2 14.2 7.3	75.8 56.4 132.1 63.3 135.8	74 50 30 161 58	14 12 16 13 19	10 10 12 10 13	305 430 569 366 462	3.35 3.40 3.33 3.01 4.05	3.4 3.5 1.7 7.8 2.6	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	<2 <2 <2 <2 <2 <2 <2 <2 <2	22 28 31 25 33	.10 .06 .15 .14 .13	.2 .3 <.2 .7 <.2	<.2 <.2 <.2 .2 <.2	88 87 79 74 94	.33 .41 .38 .32 .40	.142 .055 .123 .097 .140	7 12 17 9 13	24 29 23 23 26	.31 .35 .27 .28 .31	90 87 175 292 285	.23 .27 .27 .22 .32	<3 <3 <3 <3 <3 <3	1.50 1.21 1.80 1.55 2.06	.02 .03 .02 .02 .02	.05 .07 .09 .05 .08	<2 < <2 < <2 < <2 < <2 < <2 <	<.2 <.2 <.2 <.2	<10 · 13 · 19 · 12 · 11 ·	<.3 < <.3 < <.3 < <.3 <	<.2 6 <.2 5 <.2 6 <.2 9	.0	<1 6 4 8 1
73916 73917 73918 73919 73920	1.1 1.1 1.3 1.3	7.8 7.1 8.6 11.6 7.9	9.0 9.4 7.9 9.1 8.7	113.4 137.9 99.1 105.3 83.9	138 98 58 102 44	13 11 16 18 14	9 10 10 12 10	757 849 469 349 609	2.81 3.00 3.30 3.70 3.16	1.5 1.5 1.5 2.3 1.6	7 <5 <5 <5 <5	<2 <2 <2 <2 <2 <2 <2	24 24 27 23 34	.22 .21 .10 .12 .11	<.2 <.2 <.2 <.2 <.2 <.2	<.2 <.2 <.2 <.2 <.2	64 70 76 93 77	.32 .37 .33 .29 .40	.143 .200 .139 .138 .161	8 9 10 10 7	22 20 23 28 23	.22 .22 .26 .29 .26	336 267 109 118 129	.21 .20 .25 .30 .26	<3 <3 <3 <3 <3 <3 <3	1.56 1.44 1.78 2.00 1.60	.02 .02 .02 .02 .02	.06 .06 .10 .06 .06	<pre><2 < <2 < <2 < <2 < <2 < <2 <</pre>	<.2 <.2 <.2 <.2	10 13 <10 15 16	<.3 < <.3 < <.3 < <.3 <	<.2 6 <.2 5 <.2 6 <.2 7 <.2 6	.1 .7 .5 .1	<1 <1 <1 14 <1
73921 73922 73923 73924 73925	1.0 .5 1.0 1.0 1.1	11.1 10.2 12.3 7.3 9.0	10.6 7.1 8.3 8.2 13.4	85.3 34.8 86.1 87.4 128.6	36 69 146 104 122	16 7 16 12 14	12 6 11 9 9	383 264 297 503 573	3.40 2.75 3.44 2.96 2.77	2.3 2.6 3.2 1.8 2.0	5 <5 <5 <5 <5	<2 <2 <2 <2 <2 <2	24 42 23 23 22	.09 .07 .10 .09 .14	<.2 <.2 .2 .2 .2 <.2	<.2 <.2 <.2 <.2 <.2	84 60 82 74 62	.29 .80 .34 .25 .27	.130 .118 .148 .080 .127	9 17 9 8 8	27 20 26 24 18	.30 .29 .31 .23 .23	130 99 97 147 162	.27 .22 .23 .24 .23	<3 <3 <3 <3 <3	1.95 .97 1.71 1.71 1.85	.02 .04 .02 .01 .01	.06 .05 .06 .05 .05	<2 < <2 < <2 < <2 < <2 <	<.2 <.2 <.2 <.2	15 · 17 · 12 · 23 · 17 ·	<.3 < <.3 < <.3 < <.3 <	<.2 6 <.2 6 <.2 6 <.2 6	.5	<1 <1 <1 <1 1
73926 73927 73928 73929 STANDARD	1.4 1.1 1.1 1.1 25.2	14.2 15.2 11.7 7.5 120.4	10.4 8.3 9.9 9.0 96.8	127.2 78.4 107.1 95.9 255.1	228 102 60 78 2088	17 14 13 13 29	12 10 10 9 17	838 664 678 718 980	3.60 3.12 3.09 2.79 4.20	4.2 5.0 3.4 2.5 68.7	<5 <5 <5 12	<2 <2 <2 <2 <2 19	22 14 14 11 57 2	.16 .10 .12 .09 2.10	.2 .2 .2 <.2 7.3	<.2 <.2 <.2 <.2 17.0	87 79 73 70 68	.32 .21 .19 .16 .70	.148 .107 .125 .089 .103	8 7 9 7 17	23 21 24 19 52	.34 .32 .26 .22 1.11	161 120 114 127 243	.23 .20 .21 .20 .20 .12	<3 <3 <3 <3 25	1.73 1.46 1.73 1.59 2.19	.01 .01 .01 .01 .05	.05 .04 .05 .04 .66	<2 < <2 < <2 < <2 < 13 2	2.2 2.2 2.0 1	19 - <10 - 12 - 13 - 084	<.3 < .3 < .3 < .3 < .3 <	<.2 7 <.2 5 <.2 6 <.2 6 <.2 6 <.2 6	.0 .9 .9 .1	14 4 <1 93 46
Standard	IS STA ICP - FOR MN	NDARD 15 GR/ FE SF	D2/C3 M SAM CA P	AU-S. Ple IS	5 DIGE 7 Mg B	STED	WIT B W	H 90 AND	ML 2- LIMIT	2-2 H ED FO	ICL-H	NO3- K G	H20 /	AT 95	DEG	G. C F	OR C	ONE H	IOUR A	ND I	S DII Y BY	UTED	TO I MO	300 I CU I	ML WI PB ZI	ITH W	ATER	. THI	IS LE	ACH	IS PA	RTIA	۱L.		

HG SE TE AND GA ARE EXTRACTED WITH MIBK-ALIQUAT 336 AND ANALYSED BY ICP. ELEVATED DETECTION LIMITS FOR SAMPLES CONTAIN CU, PB, ZN, AS>1500 PPM, Fe>20%. - SAMPLE TYPE: SOIL AU+ - AQUA-REGIA/MIBK EXTRACT; GF/AA FINISHED. Samples beginning 'RE' are Reject Reruns.

Data NFA

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Fox Geological Consultants PROJECT 231 FILE # 9804612

Page 2



Data

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm (Co ppm	Mn ppm	Fe %	As ppm	U mqq	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V mqq	Ca %	P %	La ppm	rC mqq	Mg %	Ba ppm	Ti %	B	Al %	Na %	K %	W a mac	TL	Hg daa	Se	Te	Ga A	 \u+ oob
73930 73931 73938 73939 73940	.8 .8 .6 .8 .8	11.9 13.2 11.4 15.9 12.2	9.5 8.9 10.7 10.9 9.6	49.5 48.6 51.9 57.9 98.0	57 <30 252 85 100	10 11 7 11 14	8 8 6 9 11	390 434 238 298 488	2.59 2.84 2.64 3.21 3.29	3.1 2.8 1.5 3.0 2.2	<5 <5 <5 <5 <5	<2 <2 <2 <2 <2 <2 <2 <2 <2	23 37 47 29 29	.09 .07 .14 .08 .17	.2 .2 <.2 .2	<.2 <.2 <.2 <.2 <.2 <.2	66 70 41 75 75	.32 .47 .98 .47 .36	.086 .077 .036 .168 .181	12 15 17 11 9	20 19 24 23 25	.27 .33 .36 .28 .29	86 91 81 97 111	.23 .22 .20 .23 .21	<3 <3 <3 <3 <3 <3	1.09 1.06 1.68 1.43 1.87	.02 .03 .03 .03 .02	.04 .05 .08 .05 .09	<2 <2 <2 <2 <2 <2 <2	.2 <.2 <.2 <.2 <.2	<10 16 33 20 16	<.3 <.3 <.3 <.3 <.3	<.2 5 <.2 5 <.2 5 <.2 5 <.2 5 <.2 6	5.3 5.1 5.1 5.2	<1 <1 <1 <1 <1 <1 <1
73941 73942 73943 73944 73945	1.0 _9 1.3 _9 _8	8.3 10.0 7.8 7.8 7.4	11.8 10.0 8.9 12.5 10.3	79.8 80.7 94.3 91.9 116.7	88 138 144 216 218	11 11 9 11 11	9 8 9 7 7	315 429 705 306 381	2.98 2.80 2.76 2.69 2.53	2.6 2.3 1.7 2.7 2.1	<5 <5 <5 <5 <5	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <	16 16 15 18 25	.12 .12 .22 .14 .17	.2 .3 <.2 .2	<.2 <.2 <.2 <.2 <.2	73 67 71 53 55	.24 .22 .22 .25 .32	.143 .132 .128 .198 .183	7 7 7 9 9	22 20 21 15 19	.20 .21 .17 .21 .21	186 133 92 197 107	.17 .16 .20 .18 .19	<3 <3 <3 <3 <3 <3	1.53 1.55 1.27 1.77 1.45	.02 .01 .01 .02 .02	.05 .06 .05 .06 .06	<2 < <2 < <2 < <2 < <2 <	<.2 <.2 <.2 <.2 <.2	15 <10 17 27 22	<.3 <.3 <.3 <.3 <.3	<.2 <.2 <.2 <.2 <.2	5.3 5.2 5.2 5.2	1 <1 <1 <1 1
73946 73947 73948 73949 73950	.9 1.1 1.0 1.0 1.1	7.9 7.1 8.2 8.0 8.1	7.2 7.2 7.8 7.9 11.1	83.8 80.9 79.3 72.9 97.4	37 50 35 65 82	11 12 12 12 13	9 10 9 9	470 482 230 428 431	2.90 3.06 2.91 2.87 3.10	2.7 2.4 2.9 2.5 2.6	<5 <5 <5 <5 <5	~2 ~2 ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	28 20 23 17 21	.10 .10 .09 .11 .14	<.2 <.2 <.2 .2	<.2 <.2 <.2 <.2 <.2	71 71 64 70 75	.37 .27 .28 .24 .30	.126 .182 .154 .127 .133	9 8 8 8 8	20 16 16 18 24	.26 .24 .22 .22 .23	103 83 102 102 95	.17 .20 .19 .22 .22	<3 <3 <3 <3 <3 <3 <3 <3 <3 <3 <3 <3 <3 <	1.53 1.70 1.73 1.64 1.73	.02 .02 .02 .02 .02	.09 .06 .06 .05 .06	<pre><2 < <2 < <2 < <2 < <2 < <2 <</pre>	<.2 <.2 <.2 <.2 <.2	26 29 27 15 18	<.3 <.3 <.3 <.3 <.3	<.2 5 <.2 6 <.2 6 <.2 5 <.2 5	5.2 5.0 5.3 5.9 5.4	<1 <1 <1 <1 <1
RE 73950 73951 73952 73953 73954	1.3 .7 1.2 1.0 1.2	10.9 8.6 10.3 11.1 7.4	13.0 10.7 23.6 12.7 10.2	101.9 74.6 62.6 91.5 70.6	<30 <30 66 101 43	14 14 11 12 8	10 9 10 9 7	442 378 223 369 195	3.18 2.93 2.67 2.93 2.28	3.0 4.4 4.1 3.0 1.8	<5 6 <5 5 5 5	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <	22 17 25 17 26	.17 .10 .15 .15 .10	.2 .2 .3 .2 .2	<.2 <.2 <.2 <.2 <.2	79 67 61 67 55	.31 .22 .28 .23 .31	.136 .152 .072 .115 .059	8 7 7 10 7	24 21 16 25 15	.23 .22 .24 .25 .20	96 128 175 107 82	.24 .19 .18 .21 .15	<3 <3 <3 <3 <3 <3	1.78 1.83 1.71 1.83 1.20	.02 .02 .02 .02 .02	.06 .05 .04 .06 .04	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<.2 <.2 <.2 <.2	14 24 22 24 11	<.3 <.3 <.3 <.3 <.3	<.2 8 <.2 5 <.2 7 <.2 7 <.2 7	3.6 5.7 7.1 5.8 5.8	<1 <1 5 <1 <1
73955 73956 73957 74630 74631	1.1 1.2 1.1 1.0 1.1	7.5 9.1 19.6 10.5 9.9	8.7 8.7 19.4 10.8 11.7	126.5 53.3 215.9 214.7 95.7	35 36 249 209 151	14 7 13 15 13	10 8 13 11 9	429 518 1385 591 581	3.18 2.59 3.47 3.08 2.86	3.0 1.8 5.5 2.8 1.9	<5 <5 <5 <5 <5 <5	<2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2	14 18 36 20 31	.11 .12 .35 .40 .25	<.2 .2 .5 <.2 <.2	<.2 <.2 <.2 <.2 <.2	67 64 72 66 59	.21 .30 .59 .26 .32	.204 .042 .136 .187 .160	8 8 13 9 9	18 12 15 22 18	.23 .24 .34 .27 .22	167 335 514 188 171	.20 .17 .12 .21 .24	<3 <3 <3 <3 <3	2.04 1.36 1.82 1.83 1.84	.02 .02 .01 .02 .02	.04 .04 .17 .06 .06		<.2 <.2 <.2 <.2 <.2	26 21 38 19 22	<.3 <.3 <.3 <.3 <.3	<.2 (<.2 5 <.2 5 <.2 (<.2 (5.5 5.7 5.8 5.6	<1 <1 2 <1 <1
74632 74633 74634 74635 74636	.8 1.1 .9 .9 1.2	8.1 11.8 11.7 10.8 11.5	10.9 11.7 8.6 8.9 8.5	93.9 80.2 66.7 92.8 80.7	222 78 55 75 67	10 15 13 13 16	7 10 10 10 11	419 449 291 322 329	2.53 3.32 3.06 3.16 3.23	1.8 3.7 4.4 4.0 3.9	5 5 5 5 5 5 5 5 5	~2 ~2 ~2 ~2 ~2 ~2 ~2 ~2 ~2 ~2 ~2 ~2 ~2 ~	25 33 27 20 22	.18 .11 .11 .13 .14	<.2 <.2 <.2 <.2 <.2 <.2	<.2 <.2 <.2 <.2 <.2	55 80 76 80 75	.39 .42 .33 .29 .32	.050 .142 .165 .153 .176	11 10 10 8 9	21 23 23 26 23	.26 .27 .25 .24 .28	116 123 113 85 96	.24 .24 .24 .24 .24	<3 <3 <3 <3 <3 <3	1.54 1.84 1.83 1.67 1.94	.02 .02 .02 .02 .02	.07 .07 .04 .05 .05	<2 < <2 < <2 < <2 < <2 <	<.2 <.2 <.2 <.2 <.2	23 15 14 <10 24	<.3 <.3 <.3 <.3 <.3	<.2 <.2 <.2 <.2 <.2 <.2	5.4 5.3 5.7 5.8 5.3	<1 20 <1 <1 <1
STANDARD	25.1	120.4	101.0	258.1	2109	30	17	1009	4.33	69.0	13	20.	58	2.15	7.5	21.6	71	.71	.105	18	54	1.09	246	.12	29	2.23	.05	.67	14 2	2.0	1049	.4	1.9 6	5.6	57

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

APPENDIX III

INDUCED POLARIZATION SURVEY LOGISTICAL REPORT

Phelps Dodge Corporation of Canada, Limited #912 - 120 Adelaide Street West, Toronto, Ontario M5H 1T1 Telephone (416) 594-0351 Fax (416) 594-0355

LOGISTICAL REPORT

INDUCED POLARIZATION SURVEY

ON THE

TAKEN PROPERTY

VANDERHOOF AREA, B.C.

on behalf of

PARAMOUNT VENTURES AND FINANCE INC. #1260-355 Burrard Street Vancouver, B.C. V6C 2G8

Field work completed: October 9 to 14, 1998

by

David C. Hall, Geophysicist SCOTT GEOPHYSICS LTD. 4013 West 14th Avenue Vancouver, B.C. V6R 2X3

October 19, 1998

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1	Introduction	1
2	Survey Coverage	1
3	Personnel	1
4	Instrumentation	2
5	Recommendations	2

<u>Appendix</u>

rear of report

Map pocket

Statement of Qualifications

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Accompanying maps and materials

Chargeability/Resistivity Pseudosections	1
Chargeability Triangular Filter Plan	1
Resistivity Triangular Filter Plan	1
Floppy Disc: all final survey data (ASCII format)	2

1. INTRODUCTION

An induced polarization/resistivity (IP/RES) survey was completed on the Taken property, located approximately 200 kms. south of Vanderhoof, B.C, during the period October 9 to 14, 1998. The work was conducted by Scott Geophysics Ltd. on behalf of Paramount Ventures and Finance Inc.

This report presents the results of the survey and describes the instrumentation and procedures involved in the collection of data.

2. SURVEY COVERAGE

A total of some 5 line kms of IP/RES survey was completed on the Taken property.

The IP survey utilized the pole-dipole array, at an "a" spacing of 25m. Readings were taken at "n" separations of 1 to 5 on all lines The on-line current electrode was located to grid west of the receiving electrodes for all lines.

The pole dipole chargeability and resistivity results are presented as pseudosections, located in map pocket 1 at the rear of this report. In addition, triangular filter plan maps have been prepared for chargeability and resistivity data.

All final survey data is given in ASCII format on the floppy disk located in map pocket 2 at the rear of this report.

3. PERSONNEL

David Hall, geophysicist, was the party chief for the IP/RES survey on behalf of Scott Geophysics.

A Scintrex IPR12 receiver and Scintrex TSQ3 (3kw) transmitter were used for the survey. The waveform timing was 2 seconds on/2 seconds off. The Mx chargeability plotted on the maps and pseudosections is for the interval 690 to 1050 msecs after shutoff.

5. RECOMMENDATIONS

A preliminary examination of the LP./RES survey results from the Taken Property indicates several zones of weakly to moderately anomalous chargeability response. The longest of these is a feature which cuts the east side of the grid which is at least 500 metres long by roughly 200 metres wide. These zones do not appear to be directly associated with elevated resistivities. Correlation with geological and geochemical results may indicate the need to further investigate these responses.

Respectfully Submitted,

and c Hall

David C. Hall, Geophysicist

Statement of Qualifications

For

David C. Hall, Geophysicist

Of

3476 W. 22nd Avenue Vancouver, B.C. V6S1J2

I, David C. Hall, hereby certify the following statements regarding my qualifications and my involvement in the program of work described in this report.

- 1. The work was performed by individuals sufficiently trained and qualified for its performance.
- 2. I have no material interest in the Taken property, on which the surveys discussed in this report were performed.
- 3. I graduated from the University of Manitoba with an Honours Bachelor of Science degree (Geophysics) in 1976.
- 4. I have been practicing my profession as a Geophysicist in the field of Mineral Exploration since 1976.

Respectfully submitted,

Tand C Hall

David C. Hall





GEOLOGICAL SURVEY BRANCH

25,810

A CAR CAR THE ACCOUNT OF A CAR A CAR



	LLGLIND
(XXX)	Lake / pond
	Creek
	Contour; (contour interval 100ft)
	UTM coordinate
	Road
	Depression
	Marsh/Swamp
	4
0	100 200 300 400

 Soil Sample Locations

 Scale
 DATE
 BY
 NTS NO.
 FIGURE

 1:5000
 Dec.98
 Wetherup
 93F/2,3
 # 6

 FOX GEOLOGICAL SERVICES INC.

PROJECT NO .: 231 (TAKEN PROPERTY)

ROLOGICAL SURVEY BRANCH

25, 810

OMINECA MINING DIVISION



. 4

• • • • • • • • • • • • • • • • • • •		LEGEND
	LAT	E CRETACEOUS
	Di Diorit abun MIDI	te, greenish grey, fine grained with dant biotite phenocrysts DLE JURASSIC
	HAZELT Ns Sand Rock	ON GROUP distone, siltstone and minor conglomerate < is tan to dark green with angular feldspar lithic fragments
\mathbf{X}	Nb Base	alt and minor andesite, locally abundant
A	Na Ande	esitic flows and lapilli tuff, tuff and minor clastic rocks
	Nd Dacit	e flows and tuff, locally quartz phyric
1990) - ¹⁹⁹⁵ - 1999 - 1997, 1990 - 1995 - 1997 - 1997, 1990 - 1997 - 1997 - 1997,		li tuff, mottled maroon to green with
an a	quar to li	tz phenocrysts, minor rhyolite maroon ght green, flow banded.
•		SYMBOLS
	×××	Lake / pond
	/	Creek
· · · · · · · · · · · · · · · · · · ·		Contour; (contour interval 100ft)
- 142 	-1- 59,57,690 ж. र भ ह ह ह ह ह ह	UTM coordinat e
		Road
	Second Second	Depression
		Marsh/Swamp
and a second	+3	Soil sample location and Au analyses (in ppb)
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and a second		
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No		
land a start and a start		I I
	0	100 200 300 400
• 140 - 124 - 1 40 - 124 - 12	- -	SCALE IN METRES
	Paramou Project No.: 240	nt Ventures and Finance Inc. (TAKEN PROPERTY) OMINECA MINING DIVISION
		Gold Soil Geochemistry
5 s _{ingu tan} asa	SCALE	DATE BY NTS NO. FIGURE
	1:5000	Dec.98 Wetherup 93F/2,3 # 7 FOX GEOLOGICAL SERVICES INC.

GEOLOGICAL SURVEY BRANCH

25,010



		LEGEND
	LAT	E CRETACEOUS
	Di Dior	ite, greenish grey, fine grained with ndant biotite phenocrysts
	MID	DLE JURASSIC
-	HAZEL Ns San	ION GROUP dstone, siltstone and minor conglomerate
		k is tan to dark green with angular felaspar lithic fragments
	ND Bas	alt and minor andesite, locally abundant ite phenocrysts
Ť		oclastic rocks
	Nd Daci light	te flows and tuff, locally quartz phyric grey to white
	Nr Lapi qua to	lli tuff, mottled maroon to green with rtz phenocrysts, minor rhyolite maroon jaht green, flow banded.
~ ~		
	_	SYMBOLS
	×××	Lake / pond
/	/	Creek
	Start Contraction of the second se	Contour; (contour interval 100ft)
	∳-563700/ m ≌ ₩ ≈	LITM coordinate
•		Road
		Depression
		Marsh/Swamp
, . 41	+120	Soil sample location and Ag analyses
		(in ppb)
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4	0	100 200 300 400 scale in metres
N	To Accompany	1998 Assessment Report on the Taken Property
	Paramou PROJECT NO.: 231	(TAKEN PROPERTY) OMINECA MINING DIVISION
		Silver
		Soil Geochemistry
1	SCALE	DATE BY NTS NO. FIGURE
	F:5000	FOX GEOLOGICAL SERVICES INC.

CONDICAL SURVEY BRANCH

25.010

SURVEY SPECIFICATIONS:

Survey performed Oct. 98

TRANSMITTER: Scintrex TSQ3 RECEIVER: Scintrex IPR12 Pulse time 2 secs Mx receive window 690 –1050 msecs

Array: pole dipole a spacing 25 metres n separations: 1,2,3,4,5 Contoured values: filtered resistivity Contour interval: 100 ohm-metres

NOTE: The filter applied to this data is the standard Fraser triangular filter whereby one value is selected at n=1, two values at n=2, three values at n=3, etc. The plotted value is the average of the average values of the n separations and is plotted at the n=1 data point. The filtered values give only general trends. The pseudosections must be referred to in order to assess specific features.

GEOLOGICAL SURVEY BRANCH ASSESSMENT REPORT

FIGURE 9

PARAMOUNT VENTURES AND FINANCE INC.

TAKEN GRID VANDERHOOF AREA, B. C. INDUCED POLARIZATION SURVEY RESISTIVITY TRIANGULAR FILTER PLAN

SCOTT GEOPHYSICS LTD.

L 10600 N

SURVEY SPECIFICATIONS:

Survey performed Oct. 98

L 10600 N

TRANSMITTER: Scintrex TSQ3 RECEIVER: Scintrex IPR12 Pulse time 2 secs Mx receive window 690 -1050 msecs

Array: pole dipole a spacing 25 metres n separations: 1,2,3,4,5

Contoured values: filtered chargeability Contour interval : 1 msec

NOTE: The filter applied to this data is the standard Fraser triangular filter whereby one value is selected at n=1, two values at n=2, three values at n=3, etc. The plotted value is the average of the average values of the n separations and is plotted at the n=1 data point. The filtered values give only general trends. The pseudosections must be referred to in order to assess specific features.

GEOLOGICAL SURVEY BRANCH ASSESSMENT REPORT

FIGURE 10

PARAMOUNT VENTURES AND FINANCE	INC.
TAKEN GRID VANDERHOOF AREA, B. C. INDUCED POLARIZATION SURVEY CHARGEABILITY TRIANGULAR FILTER PLAN	
SCOTT GEOPHYSICS LTD.	

GEOLOGICAL SURVEY BRANCH ASSESSMENT REPORT

25,810

		CHARGEABILIIT mV/V	Y Filter n=1 n=2 n=3 n=4 n=5	5.5 6.9 3.4 3. 4.1	$ \begin{array}{c} \frac{110+00}{9} \\ \frac{10}{10} \\ \frac{13}{13} \\ \frac{13}{7.9} \\ \frac{5.8}{6} \end{array} $	110+50 E 9.9 7.9 15 9.5 7.9 9 5.7 6 4.4 4.5	$\begin{array}{c} 111+00 \ \overline{E} \\ 6.3 \ 5.7 \\ 5.4 \ \overline{5} \\ 6.7 \ 6.7 \\ .4 \ 7.6 \ 7 \\ 7.2 \ 7.7 \end{array}$	$ \begin{array}{c} 111+50 \\ 5.6 \\ 5.6 \\ -4.1 \\ -7 \\ 5.1 \\ -6 \\ 5.5 \\ 5.3 \\ 4.3 \\ \end{array} $
		RESISTIVITY OHM-METRES	Filter n=1 n=2 n=3 n=4 n=5	1322 B9 1721 108 1173 79	110+00 E 7 653 9 580 515 57 3 597 817 85 1217	110+50 E 650 693 574 753 1 842 4 7 98 505 7 441 4 461 360	111+00 E 603 773 462 493 73 443 10 421 884 36 804 14 812 1386	$\begin{array}{c} 111+50 \\ 888 \\ 752 \\ 567 \\ 578 \\ 1256 \\ 1805 \\ 415 \\ 488 \\ 468 \\ 763 \\ - \end{array}$
CHARGEABILIITY mV/V	Filter 4 n=1 3 n=2 n≈3 n=4 n=5	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+50 E 4.6 4.7 3.7 3.9 .4 4.7 4.6 4.8 (4.7 5	$ \begin{array}{r} 110+00 E \\ 7 4.7 \\ 9 3.4 \\ 4.5 4. \\ 9 5.2 \\ 5.3 5. \\ 5.5 \end{array} $	$\begin{array}{c} 110+50 \ E \\ 4.7 \\ 4.6 \\ 3.3 \\ 3.8 \\ 3.8 \\ 4.9 \\ 4.4 \\ 6 \\ 5.4 \\ 5.9 \\ 6.3 \end{array}$	111+00 E $4.7 5.1$ $3.2 3.7$ $4.1 - 4$ $4.7 4.7$ $.3 5.3$ $6 6.6$	111+50 E 5.4 5.9 3.7 4 .1 4.7 5.3 5.7 6 6.2 8 6.9 8.6
RESISTIVITY OHM-METRES	, Filter ⁸⁵ n≕1 50 n=2 n=3 n≕4 n=5	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+50 E 1097 114 22 1194 105 1199 (162 117 1059 - 1138 738	110+00 E 1173 161 1664 1563 10 781 831 84 919 -	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	111+00 E 1324 1321 1333 1075 139 1056 12 1149 1394 60 1450 20 1427 2026	111+50 E 1380 1316 1025 1241 1732 12 1926 1397 121 1395 10 1407 1016
107+00 E 107+50 E 1.6 1.7 1.6 1.5	108+00 E	E 108+50 E 109+0 4 1.3 1.5 2	0 E 109 2.6 3.2	+50 E 3.6 3.7	<u>110+00 E</u> 7 3.6	110+50 E 3.6 3.7	111+00 E 3.9 4.3	111+50 E 4.7 5

CHARGEABILIITY		→	10/+	00 E	107	(+50 E	,	28+00 E	108	3+50 E	109	+00 E	109+	50 E	110	00 E	110	0+50 E	11	1+00 E	111+50
mV/V	Filter	1.6	1.6	1.7	1.6	1.5	1.5	1.4	1.3	1.5	2	2.6	3.2	3.6	3.7	3.6	3.6	3.7	3.9	4.3	4.7
	n=1	1.5	1.3	1.5	1.1	1.1	1	- 0.92	0.72	0.68	1	, 2.2	3.2	3.7	3.8	3.5	2.6	2.1	2	2.4	2.7 -
	n=2	1.5	5 1.6	3 1.5	5 1	.4 1	.4	1.2 0	.94 0.	<u>.9</u> 3 Í	.2 ,3	າ 2	.6 3.4	4.	1) 3	.7	3.5	3.1 ~~~~	2.9	3.4	4-4.6
	n=3		1.8	1.6	1,7	1.7	1.5	1.2	1.1	1.4	2.2	2.5	3	_₊	3.8	3.6	3.7	3.8 -	4.2	4.6	5.2
	n=4		1.8	8 1,9	9 1.	.9 1	.7	1.5	1.4 1	.6 2	.4 2	.6 .3	.1 3.9	3.	4 3	.4	3.7	4.2	4.8 !	5.2 5	5.6 5.8
	n≈5			1.9	2	2	1.7	1.6	1.8 1	2.5	2.8	3.3	4	3.1	2.9	3.5	4.2	5.1	5.6	5.8	5.9
			107.			1.FA F		18.00 F			(100										
RESISTIVITY	Filtor	,+ 520	107+	00 E	107	7+50 E	<u>, 1(</u> 502	28+00 E	, <u>10</u> 8	8+50 E	109	+00 E	109+	50 E	110	<u>)+00 E</u>	111	0+50 <u>E</u>	<u>– 11</u>	1+00 E	<u>111+5(</u>
RESISTIVITY OHM-METRES	Filter	, 520	107++ 495	00 E 490	107 520	7+50 E 516	, <u>10</u> 502	08+00 E 542	10E 659	8+50 E 817	109	+00 E 1055	109+ 1015	50 E	110)+00 E 720	<u>, 111</u> 763	0+50 E 779	<u>, 11</u> 773	1+00 E 684	<u>, 111+5</u> 545
RESISTIVITY OHM-METRES	Filter n=1	↓ 520 435	107+ 495 304	00 E 490 216	107 520 256	7+50 E 516 286	10 502 290	28+00 E 542 252	<u>108</u> 659 255	8+50 E 817 303	109 1022	+00 E 1055 1172	109+ 1015 1513	50 E 1182 2131	110 1163 2274	0+00 E 720	110 763 718	0+50 E 779 484	11 773 382	1+00 E 684 326	<u>111+5(</u> 545 308
RESISTIVITY OHM-METRES	Filter n=1 n=2	520 435 50	107+ 495 304 5 372	00 E 490 216 2 41/	107 520 25644	7+50 E 516 	<u>1(</u> 502 290 24	08+00 E 542 252 330	108 859 255 358 4	3+50 E 817 43 9	109 1022 699	+00 E 1055 · 1172	109+1 1015 1513 59 128	50 E 1182 2131	110 1163 2274 94	0+00 E 720 61	111 763 718 718	0+50 E 779 484	11 773 382 741	1+00 E 684 326 704 5	111+5/ 545 308 511 375
RESISTIVITY OHM-METRES	Filter n≂1 n=2 n=3	520 435 509	107+ 495 304 5 372 503	00 E 490 216 2 411 554	107 520 2564 4 4	7+50 E 516 	10 502 290 24 417	28+00 E 542 252 330 431	10E 659 255 358 4 537	3+50 E 817 43 1057	109 1022 599 11 12 1369	+00 E 1055 1172 921	109+ 1015 1513 128 823	50 E 1182 2131 1 184	110 1163 2274 34 99 750	0+00 E 720 61 738	111 763 718 718 665	0+50 E 779 484 903 366	11 773 382 741	1+00 E 684 326 704 824	111+5 545 308 511 375 502
RESISTIVITY онм-метres	Filter n=1 n=2 n=3 n=4	520 435 505	107+ 495 304 5 372 503 670	00 E 490 216 2 41- 554 0 73:	107 520 256 - 4 4 619 3 6	7+50 E 516 	10 502 290 24 417 23	28+00 E 542 252 330 431 507	102 859 255 358 4 537	8+50 E 817 303 1057 186 14	109 1022 599 11 12 1369 9:	+00 E 1055 1172 921 51 7	109+ 1015 1513 69 128 823 71 872	50 E 1182 2131 1 182 1154 50	110 1163 2274 94 95 750 8 5	0+00 E 720 61 738 92	11/ 763 718 665 636	0+50 E 779 484 966 754	11 773 382 741 1037 1204	1+00 E 684 326 704 824 705 707	111+50 545 308 511 375 502 714 561
RESISTIVITY OHM-METRES	Filter n=1 n=2 n=3 n=4 n=5	520 435 505	107+ 495 304 5 372 503 670	00 E 490 216 2 411 554 0 733 828	107 520 256 - 4 4 618 3 8 772	7+50 E 516 	290 24 23 601	28+00 E 542 252 330 431 507 672	10E 659 255 358 4 537 606 11 1283	8+50 E 817 303 9 9 1057 186 14	109 1022 599 11 12 1369 977	+00 E 1055 1172 921 51 7 797	109+1 1015 1513 59 128 823 71 872 900	50 E 1182 2131 1 182 1154 50 368	1163 1163 2274 94 95 750 8 5 437	0+00 E 720 61 738 92 512	111 763 718 718 665 636 706	0+50 E 779 484 903 966 - 754 936	11 773 382 741	1+00 E 684 326 704 5 824 7 800	111+50 545 308 511 375 502 714 561 744
RESISTIVITY OHM-METRES	Filter n=1 n=2 n=3 n=4 n=5	520 435 509	107+ 495 304 5 304 5 372 503 670	00 E 490 216 2 411 554 0 733 828	107 520 256 4 4 618 3 8' 772	7+50 E 518 	11 502 290 24 417 23 601	28+00 E 542 252 330 431 507 672 ~	10E 659 255 358 4 537 11 1283	9+50 E 817 303 443 9 9 1057 186 143	109 1022 599 11 1369 977	+00 E 1055 1172 921 51 7 797	109+ 1015 1513 128 823 71 872 900	50 E 1182 2131 1154 358	110 1163 2274 94 750 8 437	0+00 E 720 61 738 92 512	111 763 718 718 665 636 706	0+50 E 779 484 803 966 754 936	11 773 382 741	1+00 E 684 326 704 824 704 824 704 860	111+50 545 308 511 375 502 714 561 744
RESISTIVITY OHM-METRES	Filter n=1 n=2 n=3 n=4 n=5	435 50	107+ 495 304 503 670	00 E 490 216 2 41/ 554 0 73 828	107 520 256 - 4 4 618 3 6 ¹ 772	7+50 E 518 	290 24 23 601	08+00 E 542 252 330 431 507 672	10E 659 255 358 4 537 11 1283	8+50 E 817 303 9 1057 186 1586	109 1022 699 11 12 1369 977	+00 E 1055 1172 72 921 51 7 797	109+ 1015 1513 59 823 71 872 900	50 E 1182 2131 1154 358	110 1163 2274 9 750 8 5 437	0+00 E 720 61 738 92 512	111 763 718 665 636 706	0+50 E 779 484 966 754 936	11 773 382 741 1037 1204 1 1163	1+00 E 684 326 704 5 824 70 860	111+5 545 308 511 375 502 714 561 744
RESISTIVITY OHM-METRES	Filter n=1 n=2 n=3 n=4 n=5	435 509	107+ 495 304 5 372 503 670	00 E 490 216 2 411 554 0 73 828	107 520 256 44 618 3772	7+50 E 516 	290 24 23 601	28+00 E 542 252 330 431 507 672	10E 659 255 358 4 537 11 1283	8+50 E 817 303 9 1057 186 1586	109 1022 599 11 12 1369 977	+00 E 1055 1172 921 51 7 797	109+1 1015 1513 59 128 823 71 872 900	50 E 1182 2131 1154 50 358	110 1163 2274 94 95 750 8 5 437	0+00 E 720 61 738 92 512	111 763 718 665 636 706	0+50 E 779 484 903 966 936	11 773 382 741 1037 1204 1 1163	1+00 E 684 326 704 824 70 860	111+5 545 308 511 375 502 714 561 744

$\begin{array}{c} \text{CHARGEABILIITY} \\ \text{mV/V} \end{array} \begin{array}{c} \text{Filter} & \frac{106+50}{5} \frac{5}{3.7} & \frac{107+50}{3.2} \frac{5}{2.7} & \frac{107+50}{2.4} \frac{5}{2.2} & \frac{107+50}{2.5} \frac{5}{1.8} & \frac{107+50}{1.5} \frac{5}{1.8} & \frac{109+50}{1.5} \frac{5}{1.8} & \frac{109+50}{1.5} \frac{5}{1.7} & \frac{109+50}{1.8} \frac{5}{1.7} & \frac{110+50}{1.8} \frac{5}{1.8} & \frac{111+50}{1.7} \frac{5}{1.7} \frac{5}{1.7} & \frac{111+50}{1.7} \frac{5}{1.7} \frac{5}{1.7} & \frac{111+50}{1.7} \frac{5}{1.7} $																								
$\begin{array}{c} \text{RESISTIVITY} \\ \text{OHM-METRES} \end{array} \begin{array}{c} \begin{array}{c} n=1 & 3.5 & 4.1 & 5 & 4 & 2.5 & 1.4 & 1.$		Filter	, — , — , — 3.5	106+00 E 3.7 3.7	, <u>1</u> 3.2	106+50 E 2.7	107+ 2.4	00 E	107+ 2	+50 E 1.8	108+0 1.8	0 E	<u>108+50 E</u> 1.7 1.8	<u>1</u> 1.8	09+00 E 1.6	10	9+50 E 1.8	110 1.9	+00 E	1104 2	+50 E 1.8	<u>111</u> 1.7	1.7	111+5
RESISTIVITY 106+00 E 106+50 E 107+50 E 108+00 E 108+50 E 109+00 E 109+50 E 110+00 E 110+50 E 111+00 E 111 OHM-METRES Filter 449 423 364 278 313 345 368 383 419 460 535 563 611 537 529 510 572 577 562 550 386 362 310 295 n=1 480 490 415 178 178 177 203 203 313 316 547 552 641 391 361 292 316 518 272 335 187 172		n=1 n=2 n=3 n=4 n=5	3.5 4.2	4.1 5 4.6 4 3.1 2.7 2.3	3.8 	2.9 2.9 2.6	1.9 2.6 2.7 2.5 2.6	1.6 2.2 5 2.3 2.6	1.4 9 1.7 2	1.1 7 1.4 1.9 2 2.4 2.4	1.1 6 1.8 	1.5 1.4 1.6 2.3	1.3 1.5 1.6 1.8 2.1 2.3 / 2.4 1.8	2.2 2.1 1.5 1.6 1.7	- 1.8 1.4 1.3 1.5 1.5	1.6 1.7 1 1.7 1.4 1 1.7	1.4 .7 1. .9 2 / 2.3	1.4 .7 1. 2.1 .3 2. 2.5	1.4 .8 1. 2 .3 2. 2.4	1.8 .8 1. 3 2.3	1.4 6 1 1.7 1 1 2.2	1.2 .6 1 1.7 .9 2.1	1.1 .5 1 1.6 2	0.98 .4 1.4 1.7 2 2.2 2.2
CHM-METRES Filter 449 423 364 278 313 345 368 383 419 460 535 563 611 537 529 510 572 577 562 550 386 362 310 295 $n=1$ 480 490 415 135 167 178 179 203 203 313 316 547 552 641 391 361 292 316 518 272 335 187 172																								
	RESISTIVITY			106+00 E	1	106+50 E	107+	00 E	107 1	+50 E	108+0	0 E	108+50 E	1	09+00 F	10	++50 F	110	4400 F	110-	+50 F	111	1+00 F	1114

112+50 E 113+50 E 7.1 6.1 5.5 4.9 4.5 4.3 12 12

118+00 E 118+50 E 119+00 E 119+50 E 114+00 E 115+00 E 115+50 E 116+00 E 116+50 E 117+00 E 117+50 E 114+50 E 112+00 E 112+50 E 113+50 E 113+00 E 170 - 217 - 108 - 200 - 176 - 309 - 314 - 330 - 244

