Kennecott Canada
Exploration Inc.

1998 GEOLOGICAL, GEOCHEMICAL, GEOPHYSICAL, AND DIAMOND DRILLING ASSESSMENT REPORT on the FINDLAY CREEK OPTION

VOLUME 4

APPENDICES VIII TO XI

- Prepared by: -
Kennecott Canada Exploration Inc.
354 - 200 Granville Street
Vancouver, British Columbia, Canada V6C 1S4
Phone: (604) 669-1880
Fax: (604) 669-5255

- Authors -
Steven Coombes, P.Geo.
Rick J. Zuran

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APPENDIX VIII

DIAMOND DRILL HOLE RQD LOGS

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-01	9.14	11.88	2.74	3.33	121.5	11	2.35	0.71
F98-01	11.88	14.94	3.06	3.01	98.4	8	2.42	0.80
F98-01	14.94	15.85	0.91	0.91	100.0	4	0.62	0.68
F98-01	15.85	17.98	2.13	2.45	115.0	9	1.99	0.81
F98-01	17.98	21.03	3.05	3.01	98.7	10	2.57	0.85
F98-01	21.03	24.08	3.05	3.12	102.3	8	2.39	0.77
F98-01	24.08	27.13	3.05	2.99	98.0	12	2.69	0.90
F98-01	27.13	30.18	3.05	3.19	104.6	10	2.12	0.66
F98-01	30.18	33.22	3.04	3.00	98.7	10	2.31	0.77
F98-01	36.27	39.32	3.05	3.01	98.7	12	1.26	0.42
F98-01	39.32	42.37	3.05	3.05	100.0	12	2.39	0.78
F98-01	42.37	44.65	2.28	2.37	103.9	9	1.77	0.75
F98-01	44.65	45.72	1.07	1.24	115.9	10	0.63	0.51
F98-01	45.72	48.46	2.74	2.76	100.7	7	2.26	0.82
F98-01	48.46	51.51	3.05	3.01	98.7	11	2.63	0.87
F98-01	51.51	52.73	1.22	1.50	123.0	1	0.26	0.17
F98-01	52.73	54.56	1.83	1.86	101.6	4	1.53	0.82
F98-01	54.56	57.30	2.74	2.62	95.6	8	2.52	0.96
F98-01	57.30	60.05	2.75	3.05	110.9	7	2.20	0.72
F98-01	60.05	60.66	0.61	0.46	75.4	2	0.46	1.00
F98-01	60.66	63.70	3.04	2.96	97.4	10	2.64	0.89
F98-01	63.70	66.75	3.05	3.01	98.7	9	2.60	0.86
F98-01	66.75	69.80	3.05	3.05	100.0	8	2.15	0.70
F98-01	69.80	72.39	2.59	2.80	108.1	6	2.15	0.77
F98-01	72.39	75.44	3.05	3.09	101.3	9	2.40	0.78
F98-01	75.44	76.89	1.45	1.73	119.3	4	1.50	0.87
F98-01	76.89	78.94	2.05	2.05	100.0	5	1.73	0.84
F98-01	78.94	80.92	1.98	2.00	101.0	5	1.80	0.90
F98-01	80.92	81.99	1.07	1.07	100.0	3	1.07	1.00
F98-01	81.99	85.04	3.05	3.05	100.0	6	2.70	0.89
F98-01	85.04	88.09	3.05	3.05	100.0	9	2.95	0.97
F98-01	88.09	91.14	3.05	2.94	96.4	8	2.42	0.82
F98-01	91.14	94.18	3.04	3.03	99.7	5	2.09	0.69
F98-01	94.18	97.73	3.55	3.05	85.9	9	3.05	1.00
F98-01	97.73	100.28	2.55	3.00	117.6	9	2.20	0.73
F98-01	100.28	103.33	3.05	2.93	96.1	6	2.30	0.78
F98-01	103.33	106.38	3.05	3.05	100.0	7	2.90	0.95
F98-01	106.38	109.42	3.04	2.87	94.4	5	1.83	0.64
F98-01	109.42	111.40	1.98	2.19	110.6	7	1.17	0.53
F98-01	111.40	112.78	1.38	1.45	105.1	2	0.47	0.32
F98-01	112.78	115.52	2.74	2.61	95.3	10	2.11	0.81
F98-01	115.52	116.59	1.07	1.00	93.5	1	0.18	0.18
F98-01	116.59	119.48	2.89	3.03	104.8	6	2.86	0.94
F98-01	119.48	120.40	0.92	0.78	84.8	4	0.72	0.92
F98-01	120.40	123.14	2.74	2.66	97.1	5	2.17	0.82
F98-01	123.14	126.14	3.00	3.00	100.0	7	2.08	0.69
F98-01	126.14	129.24	3.10	3.10	100.0	4	2.06	0.66
F98-01	129.24	132.28	3.04	3.04	100.0	5	2.60	0.86
F98-01	132.28	135.33	3.05	3.05	100.0	9	2.15	0.70
F98-01	135.33	138.38	3.05	2.91	95.4	6	2.20	0.76

FINDLAY CREEK PROJECT - 1998
Diamond Drill Hole RQD Logs

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-01	138.38	141.43	3.05	3.01	98.7	7	2.48	0.82
F98-01	141.43	142.64	1.21	1.37	113.2	5	1.12	0.82
F98-01	142.64	145.69	3.05	3.03	99.3	7	1.87	0.62
F98-01	145.69	148.74	3.05	3.05	100.0	9	2.55	0.84
F98-01	148.74	151.79	3.05	3.10	101.6	6	2.77	0.89
F98-01	151.79	154.53	2.74	2.57	93.8	1	2.00	0.78
F98-01	154.53	157.58	3.05	3.10	101.6	9	2.00	0.65
F98-01	157.58	158.19	0.61	0.61	100.0	0	0.00	0.00
F98-01	158.19	161.24	3.05	2.86	93.8	6	2.15	0.75
F98-01	161.24	164.13	2.89	2.99	103.5	10	2.57	0.86
F98-01	164.16	166.73	2.57	2.83	110.1	5	2.14	0.76
F98-01	166.73	170.23	3.50	3.33	95.1	9	1.73	0.52
F98-01	170.23	172.21	1.98	2.05	103.5	4	0.86	0.42
F98-01	172.21	173.43	1.22	1.22	100.0	3	0.60	0.49
F98-01	173.43	176.48	3.05	3.05	100.0	6	1.90	0.62
F98-01	176.48	179.53	3.05	3.05	100.0	6	2.02	0.66
F98-01	179.53	182.58	3.05	3.05	100.0	6	1.00	0.33
F98-01	182.58	184.70	2.12	2.12	100.0	5	1.08	0.51
F98-01	184.70	186.54	1.84	1.21	65.8	10	0.00	0.00
F98-01	186.54	188.67	2.13	2.80	131.5	10	1.69	0.60
F98-01	188.67	191.11	2.44	2.44	100.0	4	1.06	0.43
F98-01	191.11	194.16	3.05	3.05	100.0	10	1.15	0.38
F98-01	194.16	197.21	3.05	3.05	100.0	5	1.95	0.64
F98-01	197.21	200.25	3.04	2.96	97.4	2	1.09	0.37
F98-01	200.25	201.78	1.53	1.53	100.0	4	0.65	0.42
F98-01	201.78	203.91	2.13	2.09	98.1	7	1.29	0.62
F98-01	203.91	205.13	1.22	1.22	100.0	2	0.74	0.61
F98-01	205.13	206.96	1.83	1.75	95.6	3	0.55	0.31
F98-01	206.96	209.09	2.13	1.96	92.0	5	1.08	0.55
F98-01	209.09	211.89	2.80	2.67	95.4	5	0.98	0.37
F98-01	211.89	213.66	1.77	1.87	105.6	3	0.55	0.29
F98-01	213.66	216.10	2.44	2.44	100.0	8	1.82	0.75
F98-01	216.10	219.15	3.05	3.05	100.0	9	2.07	0.68
F98-01	219.15	222.20	3.05	3.05	100.0	7	1.45	0.48
F98-01	222.20	225.25	3.05	3.05	100.0	8	1.53	0.50
F98-01	225.25	228.30	3.05	3.05	100.0	5	1.15	0.38
F98-01	228.30	231.34	3.04	3.04	100.0	5	1.79	0.59
F98-01	231.34	232.26	0.92	0.88	95.7	3	0.85	0.97
F98-01	232.26	234.70	2.44	2.34	95.9	7	1.55	0.66
F98-01	234.70	237.44	2.74	2.88	105.1	8	2.49	0.86
F98-01	237.44	239.26	1.82	1.65	90.7	4	1.13	0.68
F98-01	239.26	242.32	3.06	3.09	101.0	7	2.32	0.75
F98-01	242.32	244.45	2.13	2.13	100.0	3	1.96	0.92
F98-01	244.45	245.05	0.60	0.79	131.7	2	0.32	0.41
F98-01	245.05	246.38	1.33	1.33	100.0	4	1.18	0.89
F98-01	246.38	249.63	3.25	3.05	93.8	8	2.48	0.81
F98-01	249.63	252.68	3.05	3.05	100.0	7	2.67	0.88
F98-01	252.68	254.20	1.52	1.52	100.0	4	1.05	0.69
F98-01	254.20	255.73	1.53	1.45	94.8	3	1.07	0.74
F98-01	255.73	258.78	3.05	3.08	101.0	7	2.45	0.80

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-01	258.78	261.82	3.04	3.04	100.0	8	2.63	0.87
F98-01	261.82	264.87	3.05	3.05	100.0	9	2.58	0.85
F98-01	264.87	267.92	3.05	3.05	100.0	10	2.40	0.79
F98-01	267.92	270.05	2.13	2.31	108.5	8	1.94	0.84
F98-01	270.05	273.10	3.05	2.91	95.4	8	2.61	0.90
F98-01	273.10	274.02	0.92	0.88	95.7	2	0.63	0.72
F98-01	274.02	277.06	3.04	3.04	100.0	11	2.31	0.76
F98-01	277.06	280.11	3.05	3.05	100.0	12	2.56	0.84
F98-01	280.11	282.55	2.44	2.44	100.0	4	1.29	0.53
F98-01	282.55	284.07	1.52	1.35	88.8	4	1.14	0.84
F98-01	284.07	284.99	0.92	0.92	100.0	4	0.71	0.77
F98-01	284.99	285.90	0.91	0.91	100.0	4	0.69	0.76
F98-01	285.90	287.73	1.83	1.39	76.0	4	0.65	0.47
F98-01	287.73	288.04	0.31	0.31	100.0	1	0.15	0.48
F98-01	288.04	291.08	3.04	3.04	100.0	6	2.33	0.77
F98-01	291.08	294.13	3.05	3.05	100.0	8	2.08	0.68
F98-01	294.13	296.72	2.59	2.59	100.0	6	2.31	0.89
F98-01	296.72	299.77	3.05	3.05	100.0	8	2.20	0.72
F98-01	299.77	302.82	3.05	3.05	100.0	12	2.86	0.94
F98-01	302.82	305.87	3.05	3.02	99.0	9	2.87	0.95
F98-01	305.87	308.76	2.89	2.82	97.6	7	2.66	0.94
F98-01	308.76	311.81	3.05	3.05	100.0	10	2.48	0.81
F98-01	311.81	313.94	2.13	2.00	93.9	3	1.43	0.72
F98-01	313.94	316.69	2.75	2.74	99.6	5	2.68	0.98
F98-01	316.69	319.74	3.05	3.11	102.0	6	2.90	0.93
F98-01	319.74	322.78	3.04	3.04	100.0	9	2.77	0.91
F98-01	322.78	325.83	3.05	3.05	100.0	8	2.60	0.85
F98-01	325.83	328.88	3.05	3.05	100.0	6	2.90	0.95
F98-01	328.88	331.93	3.05	3.02	99.0	8	2.24	0.74
F98-01	331.93	334.98	3.05	3.02	99.0	11	2.75	0.91
F98-01	334.98	338.02	3.04	3.00	98.7	8	2.19	0.73
F98-01	338.02	341.07	3.05	3.05	100.0	6	1.96	0.64
F98-01	341.07	344.12	3.05	3.04	99.7	12	2.72	0.89
F98-01	344.12	346.86	2.74	2.73	99.6	9	2.12	0.78
F98-01	346.86	349.61	2.75	2.65	96.4	8	1.75	0.66
F98-01	349.61	352.65	3.04	3.02	99.3	8	2.76	0.91
F98-01	352.65	355.70	3.05	3.09	101.3	10	2.21	0.72
F98-01	355.70	357.84	2.14	2.14	100.0	7	0.96	0.45
F98-01	357.84	359.36	1.52	1.51	99.3	5	1.09	0.72
F98-01	359.36	360.88	1.52	1.48	97.4	1	0.12	0.08
F98-01	360.88	362.41	1.53	1.54	100.7	2	0.37	0.24
F98-01	362.41	364.54	2.13	2.11	99.1	7	1.47	0.70
F98-01	364.54	367.44	2.90	2.80	96.6	10	2.21	0.79
F98-01	367.44	370.33	2.89	2.96	102.4	10	1.29	0.44
F98-01	370.33	373.08	2.75	2.68	97.5	8	1.68	0.63
F98-01	373.08	376.12	3.04	3.00	98.7	8	1.98	0.66
F98-01	376.12	378.87	2.75	2.74	99.6	7	0.82	0.30
F98-01	378.87	381.91	3.04	3.09	101.6	7	1.82	0.59
F98-01	381.91	382.68	0.77	0.71	92.2	2	0.45	0.63
F98-01	382.68	385.42	2.74	2.68	97.8	7	1.98	0.74

FINDLAY CREEK PROJECT - 1998
Diamond Drill Hole RQD Logs

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-01	385.42	387.86	2.44	2.36	96.7	5	1.63	0.69
F98-01	387.86	390.75	2.89	2.80	96.9	4	0.87	0.31
F98-01	390.75	393.80	3.05	2.97	97.4	7	2.16	0.73
F98-01	393.80	396.09	2.29	2.32	101.3	7	1.86	0.80
F98-01	396.09	398.98	2.89	2.93	101.4	7	2.44	0.83
F98-01	398.98	402.03	3.05	3.10	101.6	6	2.22	0.72
F98-01	402.03	405.08	3.05	3.02	99.0	8	2.47	0.82
F98-01	405.08	407.52	2.44	2.34	95.9	6	2.16	0.92
F98-01	407.52	410.57	3.05	3.09	101.3	9	2.12	0.69
F98-01	410.57	413.61	3.04	3.08	101.3	10	2.15	0.70
F98-01	413.61	416.66	3.05	3.10	101.6	8	1.83	0.59
F98-01	416.66	418.80	2.14	2.16	100.9	6	1.35	0.63
F98-01	418.80	420.78	1.98	1.63	82.3	4	1.49	0.91
F98-01	420.78	422.15	1.37	1.42	103.6	3	0.81	0.57
F98-01	422.15	424.89	2.74	2.68	97.8	6	1.52	0.57
F98-01	424.89	425.50	0.61	0.45	73.8	1	0.12	0.27
F98-01	425.50	428.55	3.05	2.98	97.7	6	1.41	0.47
F98-01	428.55	429.46	0.91	0.75	82.4	1	0.20	0.27
F98-01	429.46	432.51	3.05	2.95	96.7	9	2.67	0.91
F98-01	432.51	435.56	3.05	2.95	96.7	7	2.68	0.91
F98-01	435.56	438.61	3.05	3.07	100.7	6	2.84	0.93
F98-01	438.61	441.66	3.05	2.99	98.0	8	2.53	0.85
F98-01	441.66	444.70	3.04	3.04	100.0	8	2.67	0.88
F98-01	444.70	447.75	3.05	2.99	98.0	10	2.26	0.76
F98-01	447.75	450.80	3.05	3.03	99.3	9	3.03	1.00
F98-01	450.80	453.85	3.05	2.96	97.0	9	2.39	0.81
F98-01	453.85	456.29	2.44	2.38	97.5	8	1.98	0.83
F98-01	456.29	459.33	3.04	3.09	101.6	10	2.98	0.96
F98-01	459.33	462.08	2.75	2.58	93.8	5	2.17	0.84
F98-01	462.08	465.12	3.04	3.08	101.3	9	2.98	0.97
F98-01	465.12	468.17	3.05	3.08	101.0	9	2.89	0.94
F98-01	468.17	469.85	1.68	1.43	85.1	5	0.80	0.56
F98-01	469.85	472.14	2.29	2.36	103.1	7	2.06	0.87
F98-01	472.14	475.18	3.04	2.97	97.7	9	2.44	0.82
F98-01	475.18	478.23	3.05	2.98	97.7	7	2.86	0.96
			466.01	463.88	99.5			

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-02	4.25	4.57	0.32	0.49	153.1	3	0.27	0.55
F98-02	4.57	7.47	2.90	2.40	82.8	10	2.08	0.87
F98-02	7.47	8.69	1.22	1.18	96.7	6	0.87	0.74
F98-02	8.69	10.36	1.67	1.52	91.0	2	0.72	0.47
F98-02	10.36	13.41	3.05	2.97	97.4	8	2.25	0.76
F98-02	13.41	14.94	1.53	1.53	100.0	4	0.96	0.63
F98-02	14.94	16.61	1.67	1.60	95.8	5	0.70	0.44
F98-02	16.61	19.05	2.44	2.15	88.1	14	1.46	0.68
F98-02	19.05	21.03	1.98	1.93	97.5	7	1.67	0.87
F98-02	21.03	24.08	3.05	3.05	100.0	13	2.47	0.81
F98-02	24.08	27.13	3.05	3.05	100.0	11	2.92	0.96
F98-02	27.13	29.29	2.16	2.16	100.0	8	2.11	0.98
F98-02	29.29	32.31	3.02	3.02	100.0	13	3.02	1.00
F98-02	32.31	35.36	3.05	2.98	97.7	13	2.63	0.88
F98-02	35.36	38.10	2.74	2.50	91.2	11	2.46	0.98
F98-02	38.10	41.15	3.05	3.03	99.3	11	2.67	0.88
F98-02	41.15	44.20	3.05	2.75	90.2	7	2.50	0.91
F98-02	44.20	46.50	2.30	2.30	100.0	5	2.17	0.94
F98-02	46.50	49.68	3.18	3.08	96.9	12	2.86	0.93
F98-02	49.68	52.73	3.05	3.05	100.0	13	3.05	1.00
F98-02	52.73	55.47	2.74	2.48	90.5	7	2.48	1.00
F98-02	55.47	57.61	2.14	2.14	100.0	9	2.14	1.00
F98-02	57.61	60.66	3.05	2.75	90.2	12	2.72	0.99
F98-02	60.66	63.70	3.04	2.95	97.0	15	2.86	0.97
F98-02	63.70	65.53	1.83	1.83	100.0	5	1.67	0.91
F98-02	65.53	66.75	1.22	1.22	100.0	9	1.03	0.84
F98-02	66.75	69.30	2.55	2.41	94.5	12	1.12	0.46
F98-02	69.30	71.93	2.63	2.18	82.9	13	1.69	0.78
F98-02	71.93	73.76	1.83	1.80	98.4	8	1.70	0.94
F98-02	73.76	74.98	1.22	1.12	91.8	10	0.88	0.79
F98-02	74.98	76.51	1.53	1.41	92.2	8	1.17	0.83
F98-02	76.51	78.49	1.98	1.93	97.5	12	1.73	0.90
F98-02	78.49	80.77	2.28	2.25	98.7	11	1.42	0.63
F98-02	80.77	82.30	1.53	1.53	100.0	6	0.83	0.54
F98-02	82.30	84.43	2.13	2.13	100.0	8	1.58	0.74
F98-02	84.43	87.48	3.05	2.84	93.1	16	2.42	0.85
F98-02	87.48	89.00	1.52	1.52	100.0	6	1.07	0.70
F98-02	89.00	92.05	3.05	1.91	62.6	5	0.98	0.51
F98-02	92.05	94.18	2.13	2.12	99.5	8	1.70	0.80
F98-02	94.18	97.23	3.05	2.98	97.7	9	2.85	0.96
F98-02	97.23	100.28	3.05	3.02	99.0	8	2.85	0.94
F98-02	100.28	103.17	2.89	2.87	99.3	9	2.33	0.81
F98-02	103.17	106.22	3.05	2.95	96.7	14	2.62	0.89
F98-02	106.22	108.20	1.98	1.98	100.0	13	1.74	0.88
F98-02	108.20	109.42	1.22	1.13	92.6	4	1.07	0.95
F98-02	109.42	110.94	1.52	1.51	99.3	9	1.11	0.74
F98-02	110.94	112.78	1.84	1.84	100.0	10	1.58	0.86
F98-02	112.78	115.21	2.43	2.35	96.7	10	1.98	0.84
F98-02	115.21	117.65	2.44	2.36	96.7	14	2.06	0.87
F98-02	117.65	120.09	2.44	2.27	93.0	13	1.73	0.76

FINDLAY CREEK PROJECT - 1998
Diamond Drill Hole RQD Logs

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-02	120.09	121.92	1.83	1.83	100.0	13	1.83	1.00
F98-02	121.92	123.60	1.68	1.62	96.4	11	1.09	0.67
F98-02	123.60	126.49	2.89	2.89	100.0	17	2.58	0.89
F98-02	126.49	128.02	1.53	1.45	94.8	7	1.11	0.77
F98-02	128.02	130.76	2.74	2.74	100.0	15	2.40	0.88
F98-02	130.76	132.89	2.13	2.13	100.0	15	1.86	0.87
F98-02	132.89	135.33	2.44	2.30	94.3	11	2.11	0.92
			131.08	125.48	95.7			

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-03	0.00	2.74	2.74	2.74	100.0	0	0.00	0.00
F98-03	2.74	5.79	3.05	3.05	100.0	5	0.75	0.25
F98-03	5.79	7.01	1.22	2.30	188.5	6	0.67	0.29
F98-03	7.01	8.84	1.83	1.75	95.6	5	0.92	0.53
F98-03	8.84	11.58	2.74	1.73	63.1	4	0.55	0.32
F98-03	11.58	13.41	1.83	1.75	95.6	4	0.61	0.35
F98-03	13.41	14.48	1.07	0.99	92.5	1	0.17	0.17
F98-03	14.48	16.92	2.44	2.50	102.5	6	0.87	0.35
F98-03	16.92	17.98	1.06	1.00	94.3	4	0.51	0.51
F98-03	17.98	21.03	3.05	2.93	96.1	9	1.68	0.57
F98-03	21.03	24.08	3.05	2.96	97.0	9	1.90	0.64
F98-03	24.08	25.91	1.83	1.91	104.4	7	0.98	0.51
F98-03	25.91	27.74	1.83	1.76	96.2	5	0.93	0.53
F98-03	27.74	30.18	2.44	2.40	98.4	6	1.06	0.44
F98-03	30.18	31.24	1.06	1.02	96.2	3	0.74	0.73
F98-03	31.24	31.85	0.61	0.70	114.8	0	0.00	0.00
F98-03	31.85	34.29	2.44	2.52	103.3	6	1.35	0.54
F98-03	34.29	35.97	1.68	1.51	89.9	4	0.80	0.53
F98-03	35.97	36.73	0.76	0.69	90.8	2	0.28	0.41
F98-03	36.73	37.64	0.91	0.77	84.6	2	0.41	0.53
F98-03	37.64	40.08	2.44	2.25	92.2	2	1.37	0.61
F98-03	40.08	42.06	1.98	2.09	105.6	6	1.32	0.63
F98-03	42.06	45.11	3.05	3.00	98.4	8	1.73	0.58
F98-03	45.11	46.79	1.68	1.66	98.8	7	1.30	0.78
F98-03	46.79	49.38	2.59	2.61	100.8	6	2.07	0.79
F98-03	49.38	52.27	2.89	2.85	98.6	4	2.15	0.75
F98-03	52.27	54.56	2.29	2.12	92.6	2	0.76	0.36
F98-03	54.56	56.38	1.82	2.04	112.1	6	1.36	0.67
F98-03	56.38	57.30	0.92	0.93	101.1	1	0.12	0.13
F98-03	57.30	59.74	2.44	2.23	91.4	8	1.30	0.58
F98-03	59.74	61.57	1.83	1.91	104.4	2	0.48	0.25
F98-03	61.57	62.64	1.07	1.09	101.9	0	0.00	0.00
F98-03	62.64	63.40	0.76	0.67	88.2	1	0.23	0.34
F98-03	63.40	64.62	1.22	0.14	11.5	0	0.00	0.00
F98-03	64.62	65.84	1.22	0.34	27.9	0	0.00	0.00
F98-03	65.84	66.45	0.61	0.68	111.5	0	0.00	0.00
F98-03	66.45	67.51	1.06	1.15	108.5	2	0.22	0.19
F98-03	67.51	68.58	1.07	0.94	87.9	2	0.22	0.23
F98-03	68.58	71.32	2.74	2.73	99.6	7	1.44	0.53
F98-03	71.32	72.54	1.22	1.19	97.5	3	0.35	0.29
F98-03	72.54	73.00	0.46	0.36	78.3	1	0.10	0.28
F98-03	73.00	74.52	1.52	1.35	88.8	2	0.45	0.33
F98-03	74.52	74.98	0.46	0.52	113.0	1	0.11	0.21
F98-03	74.98	76.66	1.68	1.56	92.9	4	0.64	0.41
F98-03	76.66	78.94	2.28	2.15	94.3	7	1.12	0.52
F98-03	78.94	80.31	1.37	1.28	93.4	4	0.70	0.55
F98-03	80.31	82.60	2.29	2.33	101.7	4	0.86	0.37
F98-03	82.60	83.82	1.22	1.36	111.5	3	0.40	0.29
F98-03	83.82	85.34	1.52	1.36	89.5	3	0.40	0.29
F98-03	85.34	88.09	2.75	2.36	85.8	7	1.68	0.71

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-03	88.09	90.22	2.13	2.46	115.5	6	1.28	0.52
F98-03	90.22	91.74	1.52	1.62	106.6	2	0.33	0.20
F98-03	91.74	92.96	1.22	1.22	100.0	0	0.00	0.00
F98-03	92.96	93.88	0.92	0.84	91.3	2	0.61	0.73
F98-03	93.88	95.10	1.22	1.08	88.5	4	0.65	0.60
F98-03	95.10	96.01	0.91	0.98	107.7	1	0.14	0.14
F98-03	96.01	97.23	1.22	0.77	63.1	1	0.15	0.19
F98-03	97.23	97.99	0.76	0.89	117.1	0	0.00	0.00
F98-03	97.99	99.67	1.68	0.97	57.7	2	0.41	0.42
F98-03	99.67	100.58	0.91	0.62	68.1	0	0.00	0.00
F98-03	100.58	102.57	1.99	2.25	113.1	1	0.11	0.05
F98-03	102.57	104.85	2.28	2.33	102.2	5	0.84	0.36
F98-03	104.85	107.38	2.53	2.46	97.2	6	1.53	0.62
F98-03	107.38	109.42	2.04	2.11	103.4	4	1.41	0.67
F98-03	109.42	112.47	3.05	3.00	98.4	3	3.00	1.00
F98-03	112.47	115.52	3.05	3.18	104.3	4	1.65	0.52
F98-03	115.52	118.57	3.05	3.11	102.0	7	2.64	0.85
F98-03	118.57	121.62	3.05	3.01	98.7	6	2.94	0.98
F98-03	121.62	124.66	3.04	3.03	99.7	7	2.84	0.94
F98-03	124.66	127.71	3.05	3.16	103.6	13	2.96	0.94
F98-03	127.71	130.76	3.05	2.95	96.7	7	2.65	0.90
F98-03	130.76	132.13	1.37	1.38	100.7	2	0.17	0.12
F98-03	132.13	133.05	0.92	1.18	128.3	0	0.00	0.00
F98-03	133.05	135.79	2.74	2.67	97.4	4	2.25	0.84
F98-03	135.79	136.25	0.46	0.24	52.2	0	0.00	0.00
F98-03	136.25	136.86	0.61	0.63	103.3	0	0.00	0.00
F98-03	136.86	139.90	3.04	3.04	100.0	5	2.78	0.91
F98-03	139.90	142.95	3.05	3.09	101.3	7	2.84	0.92
F98-03	142.95	145.39	2.44	2.29	93.9	5	1.47	0.64
F98-03	145.39	147.52	2.13	1.84	86.4	3	1.14	0.62
F98-03	147.52	148.44	0.92	1.01	109.8	3	0.64	0.63
F98-03	148.44	149.05	0.61	0.56	91.8	1	0.12	0.21
F98-03	149.05	150.72	1.67	1.77	106.0	2	0.42	0.24
F98-03	150.72	151.33	0.61	0.62	101.6	0	0.00	0.00
F98-03	151.33	153.00	1.67	1.67	100.0	2	1.08	0.65
F98-03	153.00	155.14	2.14	2.11	98.6	3	1.73	0.82
F98-03	155.14	158.04	2.90	2.74	94.5	3	1.96	0.72
F98-03	158.04	159.36	1.32	1.35	102.3	3	0.91	0.67
F98-03	159.36	162.42	3.06	3.03	99.0	5	1.92	0.63
F98-03	162.42	164.29	1.87	1.36	72.7	1	0.55	0.40
F98-03	164.29	165.05	0.76	0.62	81.6	1	0.12	0.19
F98-03	165.05	167.34	2.29	2.37	103.5	2	2.22	0.94
F98-03	167.34	169.47	2.13	2.11	99.1	1	2.11	1.00
F98-03	169.47	172.52	3.05	3.02	99.0	5	2.35	0.78
F98-03	172.52	174.65	2.13	1.91	89.7	3	0.84	0.44
F98-03	174.65	176.48	1.83	2.10	114.8	3	1.44	0.69
F98-03	176.48	179.53	3.05	3.05	100.0	3	1.32	0.43
F98-03	179.53	180.75	1.22	1.41	115.6	4	0.89	0.63
F98-03	180.75	182.58	1.83	1.83	100.0	1	1.83	1.00
F98-03	182.58	185.62	3.04	3.03	99.7	2	2.93	0.97

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-03	185.62	188.67	3.05	2.99	98.0	3	1.84	0.62
F98-03	188.67	191.72	3.05	2.94	96.4	4	2.15	0.73
F98-03	191.72	194.01	2.29	2.44	106.6	3	1.38	0.57
F98-03	194.01	196.29	2.28	2.06	90.4	3	1.38	0.67
F98-03	196.29	197.82	1.53	1.56	102.0	2	0.53	0.34
F98-03	197.82	200.86	3.04	3.04	100.0	4	1.61	0.53
F98-03	200.86	203.91	3.05	3.02	99.0	5	1.78	0.59
F98-03	203.91	206.96	3.05	2.99	98.0	4	2.03	0.68
F98-03	206.96	208.03	1.07	1.07	100.0	3	0.57	0.53
F98-03	208.03	210.92	2.89	2.85	98.6	9	2.17	0.76
F98-03	210.92	213.97	3.05	3.07	100.7	5	2.53	0.82
F98-03	213.97	217.02	3.05	3.07	100.7	1	3.07	1.00
F98-03	217.02	220.07	3.05	3.05	100.0	2	2.99	0.98
F98-03	220.07	223.11	3.04	2.93	96.4	1	2.93	1.00
F98-03	223.11	225.25	2.14	2.32	108.4	2	2.28	0.98
F98-03	225.25	228.30	3.05	2.81	92.1	2	2.79	0.99
F98-03	228.30	231.34	3.04	3.05	100.3	2	2.90	0.95
F98-03	231.34	233.17	1.83	1.79	97.8	2	1.57	0.88
F98-03	233.17	235.15	1.98	2.04	103.0	3	1.88	0.92
F98-03	235.15	237.44	2.29	2.08	90.8	4	1.72	0.83
F98-03	237.44	240.33	2.89	3.06	105.9	7	2.36	0.77
F98-03	240.33	242.01	1.68	1.65	98.2	3	1.47	0.89
F98-03	242.01	244.60	2.59	2.64	101.9	3	2.43	0.92
F98-03	244.60	247.19	2.59	2.63	101.5	4	2.35	0.89
F98-03	247.19	249.63	2.44	2.29	93.9	1	2.29	1.00
F98-03	249.63	252.68	3.05	2.85	93.4	3	2.39	0.84
F98-03	252.68	255.42	2.74	3.09	112.8	4	3.00	0.97
F98-03	255.42	258.17	2.75	2.71	98.5	5	2.11	0.78
F98-03	258.17	259.84	1.67	1.67	100.0	1	1.67	1.00
F98-03	259.84	261.82	1.98	1.90	96.0	4	1.72	0.91
F98-03	261.82	264.57	2.75	2.86	104.0	6	2.31	0.81
F98-03	264.57	267.46	2.89	2.82	97.6	6	1.74	0.62
F98-03	267.46	268.99	1.53	1.60	104.6	4	0.66	0.41
F98-03	268.99	270.97	1.98	1.89	95.5	8	1.34	0.71
F98-03	270.97	274.02	3.05	3.08	101.0	8	2.47	0.80
F98-03	274.02	277.06	3.04	2.82	92.8	8	2.59	0.92
F98-03	277.06	278.28	1.22	1.31	107.4	5	1.12	0.85
F98-03	278.28	280.11	1.83	1.89	103.3	5	1.52	0.80
F98-03	280.11	281.94	1.83	1.78	97.3	3	1.11	0.62
F98-03	281.94	284.99	3.05	2.95	96.7	9	2.76	0.94
F98-03	284.99	287.73	2.74	2.71	98.9	7	1.99	0.73
F98-03	287.73	289.29	1.56	1.43	91.7	4	1.05	0.73
F98-03	289.29	292.30	3.01	3.10	103.0	13	2.58	0.83
F98-03	292.30	294.94	2.64	2.26	85.6	8	1.46	0.65
F98-03	294.94	296.27	1.33	1.83	137.6	7	1.41	0.77
F98-03	296.27	298.40	2.13	2.14	100.5	8	1.65	0.77
F98-03	298.40	301.14	2.74	2.54	92.7	8	1.69	0.67
F98-03	301.14	302.82	1.68	1.74	103.6	4	0.81	0.47
F98-03	302.82	303.89	1.07	1.15	107.5	3	0.56	0.49
F98-03	303.89	306.02	2.13	2.08	97.7	6	1.70	0.82

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-03	306.02	308.46	2.44	2.57	105.3	8	2.26	0.88
F98-03	308.46	309.98	1.52	1.39	91.4	4	1.11	0.80
F98-03	309.98	312.12	2.14	2.07	96.7	5	1.66	0.80
F98-03	312.12	315.16	3.04	3.09	101.6	6	2.47	0.80
F98-03	315.16	317.30	2.14	2.08	97.2	5	1.55	0.75
F98-03	317.30	319.58	2.28	2.35	103.1	6	1.53	0.65
F98-03	319.58	320.95	1.37	1.37	100.0	4	1.06	0.77
F98-03	320.95	322.78	1.83	1.79	97.8	6	1.66	0.93
F98-03	322.78	325.83	3.05	2.82	92.5	10	2.31	0.82
F98-03	325.83	327.81	1.98	2.15	108.6	5	1.83	0.85
F98-03	327.81	330.86	3.05	3.01	98.7	10	2.53	0.84
F98-03	330.86	332.84	1.98	1.87	94.4	6	1.38	0.74
F98-03	332.84	333.60	0.76	0.76	100.0	1	0.24	0.32
F98-03	333.60	334.82	1.22	1.31	107.4	3	0.67	0.51
F98-03	334.82	336.19	1.37	1.34	97.8	4	0.71	0.53
F98-03	336.19	338.02	1.83	1.84	100.5	3	1.42	0.77
F98-03	338.02	339.55	1.53	1.56	102.0	5	1.14	0.73
F98-03	339.55	341.83	2.28	2.25	98.7	6	1.54	0.68
F98-03	341.83	343.51	1.68	1.52	90.5	3	1.52	1.00
F98-03	343.51	345.03	1.52	1.67	109.9	3	0.49	0.29
F98-03	345.03	346.71	1.68	1.66	98.8	3	1.00	0.60
F98-03	346.71	349.91	3.20	3.01	94.1	7	1.69	0.56
F98-03	349.91	352.96	3.05	3.03	99.3	10	2.18	0.72
F98-03	352.96	354.79	1.83	1.74	95.1	4	0.84	0.48
F98-03	354.79	356.31	1.52	1.29	84.9	4	1.27	0.98
F98-03	356.31	359.36	3.05	3.25	106.6	5	2.60	0.80
F98-03	359.36	362.41	3.05	2.87	94.1	6	2.27	0.79
F98-03	362.41	365.46	3.05	3.09	101.3	8	2.61	0.84
F98-03	365.46	368.50	3.04	3.02	99.3	8	2.23	0.74
F98-03	368.50	371.55	3.05	3.08	101.0	4	2.77	0.90
F98-03	371.55	373.53	1.98	1.97	99.5	6	1.55	0.79
F98-03	373.53	374.75	1.22	1.24	101.6	2	0.54	0.44
F98-03	374.75	377.19	2.44	2.30	94.3	4	1.97	0.86
F98-03	377.19	378.56	1.37	1.47	107.3	4	0.92	0.63
F98-03	378.56	380.85	2.29	2.29	100.0	5	1.47	0.64
F98-03	380.85	382.22	1.37	1.25	91.2	3	1.21	0.97
F98-03	382.22	383.90	1.68	1.81	107.7	5	1.31	0.72
F98-03	383.90	385.88	1.98	1.91	96.5	2	0.69	0.36
F98-03	385.88	387.25	1.37	1.20	87.6	0	0.00	0.00
F98-03	387.25	388.92	1.67	1.55	92.8	4	0.89	0.57
F98-03	388.92	391.67	2.75	2.63	95.6	5	1.92	0.73
F98-03	391.67	393.65	1.98	2.17	109.6	2	1.17	0.54
F98-03	393.65	395.02	1.37	1.30	94.9	3	0.56	0.43
F98-03	395.02	395.94	0.92	0.96	104.3	2	0.69	0.72
F98-03	395.94	397.76	1.82	1.94	106.6	5	0.92	0.47
F98-03	397.76	398.98	1.22	1.09	89.3	2	0.43	0.39
F98-03	398.98	402.03	3.05	3.15	103.3	7	1.26	0.40
F98-03	402.03	404.77	2.74	2.80	102.2	7	1.69	0.60
F98-03	404.77	407.67	2.90	2.87	99.0	7	1.75	0.61
F98-03	407.67	410.72	3.05	3.04	99.7	10	1.24	0.41

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-03	410.72	412.09	1.37	1.41	102.9	2	0.41	0.29
F98-03	412.09	415.14	3.05	3.23	105.9	6	2.33	0.72
F98-03	415.14	416.66	1.52	1.31	86.2	3	0.43	0.33
F98-03	416.66	419.71	3.05	3.06	100.3	4	2.79	0.91
F98-03	419.71	422.76	3.05	3.00	98.4	2	2.87	0.96
F98-03	422.76	425.81	3.05	2.96	97.0	3	2.54	0.86
F98-03	425.81	428.40	2.59	2.52	97.3	2	2.24	0.89
F98-03	428.40	430.07	1.67	1.70	101.8	3	1.08	0.64
F98-03	430.07	431.90	1.83	1.82	99.5	2	1.01	0.55
F98-03	431.90	434.34	2.44	2.65	108.6	6	2.29	0.86
F98-03	434.34	437.39	3.05	2.90	95.1	5	1.86	0.64
F98-03	437.39	439.06	1.67	1.64	98.2	3	0.94	0.57
F98-03	439.06	441.66	2.60	2.57	98.8	5	2.25	0.88
F98-03	441.66	444.40	2.74	2.76	100.7	6	2.18	0.79
F98-03	444.40	445.62	1.22	1.25	102.5	2	0.95	0.76
F98-03	445.62	447.75	2.13	1.89	88.7	5	1.11	0.59
F98-03	447.75	450.34	2.59	2.73	105.4	5	2.01	0.74
F98-03	450.34	452.78	2.44	2.29	93.9	5	1.60	0.70
F98-03	452.78	455.07	2.29	2.29	100.0	5	2.03	0.89
F98-03	455.07	457.20	2.13	2.18	102.3	7	1.43	0.66
F98-03	457.20	459.49	2.29	2.26	98.7	6	1.67	0.74
F98-03	459.49	462.38	2.89	2.87	99.3	6	2.09	0.73
F98-03	462.38	463.75	1.37	1.48	108.0	2	1.17	0.79
F98-03	463.75	466.04	2.29	2.08	90.8	3	1.65	0.79
F98-03	466.04	468.78	2.74	2.28	83.2	3	1.71	0.75
			468.78	460.86	98.3			

FINDLAY CREEK PROJECT - 1998
Diamond Drill Hole RQD Logs

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-04	2.13	5.79	3.66	1.79	48.9	0	0.00	0.00
F98-04	5.79	8.23	2.44	2.36	96.7	5	0.95	0.40
F98-04	8.23	11.28	3.05	3.08	101.0	7	1.34	0.44
F98-04	11.28	13.72	2.44	1.28	52.5	3	0.69	0.54
F98-04	13.72	14.94	1.22	1.55	127.0	5	0.61	0.39
F98-04	14.94	17.37	2.43	2.47	101.6	6	1.10	0.45
F98-04	17.37	19.81	2.44	2.60	106.6	8	1.17	0.45
F98-04	19.81	21.64	1.83	1.84	100.5	5	0.95	0.52
F98-04	21.64	23.77	2.13	2.04	95.8	3	0.94	0.46
F98-04	23.77	24.38	0.61	0.97	159.0	1	0.12	0.12
F98-04	24.38	26.52	2.14	1.84	86.0	1	0.29	0.16
F98-04	26.52	28.35	1.83	1.79	97.8	4	1.04	0.58
F98-04	28.35	29.26	0.91	0.74	81.3	0	0.00	0.00
F98-04	29.26	30.18	0.92	0.86	93.5	3	0.36	0.42
F98-04	30.18	31.55	1.37	1.41	102.9	1	0.28	0.20
F98-04	31.55	33.07	1.52	1.44	94.7	4	0.47	0.33
F98-04	33.07	34.90	1.83	1.86	101.6	5	0.79	0.42
F98-04	34.90	36.27	1.37	1.29	94.2	3	0.55	0.43
F98-04	36.27	37.64	1.37	1.43	104.4	4	0.73	0.51
F98-04	37.64	39.78	2.14	1.98	92.5	4	1.14	0.58
F98-04	39.78	40.39	0.61	0.58	95.1	3	0.42	0.72
F98-04	40.39	41.61	1.22	1.33	109.0	3	0.55	0.41
F98-04	41.61	43.28	1.67	1.51	90.4	3	0.58	0.38
F98-04	43.28	44.35	1.07	1.24	115.9	3	0.69	0.56
F98-04	44.35	45.11	0.76	0.61	80.3	0	0.00	0.00
F98-04	45.11	45.87	0.76	0.64	84.2	1	0.12	0.19
F98-04	45.87	47.09	1.22	1.02	83.6	1	0.11	0.11
F98-04	47.09	47.70	0.61	0.58	95.1	0	0.00	0.00
F98-04	47.70	50.29	2.59	2.60	100.4	6	0.74	0.28
F98-04	50.29	51.51	1.22	1.17	95.9	0	0.00	0.00
F98-04	51.51	53.65	2.14	2.03	94.9	2	0.21	0.10
F98-04	53.65	54.56	0.91	0.80	87.9	1	0.12	0.15
F98-04	54.56	55.78	1.22	1.32	108.2	2	0.26	0.20
F98-04	55.78	57.61	1.83	1.58	86.3	4	0.48	0.30
F98-04	57.61	59.89	2.28	1.96	86.0	5	0.72	0.37
F98-04	59.89	61.11	1.22	1.07	87.7	2	0.43	0.40
F98-04	61.11	63.55	2.44	2.26	92.6	7	1.51	0.67
F98-04	63.55	65.53	1.98	1.98	100.0	5	1.15	0.58
F98-04	65.53	67.21	1.68	1.70	101.2	3	0.74	0.44
F98-04	67.21	68.43	1.22	1.24	101.6	2	1.02	0.82
F98-04	68.43	69.80	1.37	1.22	89.1	2	1.17	0.96
F98-04	69.80	71.78	1.98	1.91	96.5	5	1.14	0.60
F98-04	71.78	74.83	3.05	3.00	98.4	5	2.55	0.85
F98-04	74.83	77.27	2.44	2.54	104.1	5	1.09	0.43
F98-04	77.27	78.94	1.67	1.65	98.8	3	1.59	0.96
F98-04	78.94	81.99	3.05	3.04	99.7	8	2.10	0.69
F98-04	81.99	85.04	3.05	2.96	97.0	8	1.84	0.62
F98-04	85.04	86.56	1.52	1.46	96.1	8	1.15	0.79
F98-04	86.56	88.09	1.53	1.30	85.0	2	0.41	0.32
F98-04	88.09	90.37	2.28	2.62	114.9	4	1.31	0.50

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-04	90.37	93.42	3.05	3.04	99.7	5	2.60	0.86
F98-04	93.42	96.47	3.05	2.99	98.0	7	2.55	0.85
F98-04	96.47	98.45	1.98	2.24	113.1	4	1.55	0.69
F98-04	98.45	100.28	1.83	1.70	92.9	3	1.37	0.81
F98-04	100.28	103.17	2.89	2.72	94.1	5	2.56	0.94
F98-04	103.17	105.00	1.83	1.86	101.6	4	1.32	0.71
F98-04	105.00	107.29	2.29	2.46	107.4	7	1.86	0.76
F98-04	107.29	109.42	2.13	1.96	92.0	4	1.29	0.66
F98-04	109.42	112.01	2.59	2.37	91.5	7	1.55	0.65
F98-04	112.01	114.15	2.14	2.24	104.7	5	1.51	0.67
F98-04	114.15	115.52	1.37	1.30	94.9	3	0.46	0.35
F98-04	115.52	116.89	1.37	1.46	106.6	2	0.20	0.14
F98-04	116.89	118.26	1.37	1.35	98.5	3	0.45	0.33
F98-04	118.26	120.09	1.83	1.76	96.2	4	0.85	0.48
F98-04	120.09	121.77	1.68	1.87	111.3	3	0.52	0.28
F98-04	121.77	124.66	2.89	2.88	99.7	4	2.54	0.88
F98-04	124.66	126.80	2.14	2.12	99.1	4	1.14	0.54
F98-04	126.80	128.32	1.52	1.54	101.3	4	0.98	0.64
F98-04	128.32	129.84	1.52	1.51	99.3	4	0.76	0.50
F98-04	129.84	132.59	2.75	2.69	97.8	8	1.68	0.62
F98-04	132.59	135.64	3.05	3.08	101.0	6	2.10	0.68
F98-04	135.64	138.68	3.04	2.96	97.4	5	2.70	0.91
F98-04	138.68	139.90	1.22	1.26	103.3	4	0.93	0.74
F98-04	139.90	142.95	3.05	3.03	99.3	6	2.76	0.91
F98-04	142.95	144.78	1.83	1.84	100.5	7	1.51	0.82
F98-04	144.78	147.07	2.29	2.25	98.3	5	1.24	0.55
F98-04	147.07	149.05	1.98	1.85	93.4	3	1.69	0.91
F98-04	149.05	152.10	3.05	3.07	100.7	6	2.53	0.82
F98-04	152.10	153.47	1.37	1.39	101.5	3	0.68	0.49
F98-04	153.47	154.99	1.52	1.36	89.5	4	0.99	0.73
F98-04	154.99	155.14	0.15	0.21	140.0	0	0.00	0.00
F98-04	155.14	158.19	3.05	3.03	99.3	7	2.22	0.73
F98-04	158.19	160.02	1.83	1.80	98.4	3	1.39	0.77
F98-04	160.02	162.91	2.89	2.93	101.4	6	1.87	0.64
F98-04	162.91	163.98	1.07	1.00	93.5	0	0.00	0.00
F98-04	163.98	167.03	3.05	3.02	99.0	8	1.83	0.61
F98-04	167.03	170.08	3.05	3.07	100.7	7	2.23	0.73
F98-04	170.08	173.13	3.05	2.97	97.4	6	2.34	0.79
F98-04	173.13	173.74	0.61	0.51	83.6	0	0.00	0.00
F98-04	173.74	174.66	0.92	0.85	92.4	3	0.44	0.52
F98-04	174.66	176.17	1.51	1.48	98.0	4	0.72	0.49
F98-04	176.17	179.22	3.05	3.04	99.7	8	2.45	0.81
F98-04	179.22	182.27	3.05	3.02	99.0	9	2.47	0.82
F98-04	182.27	185.47	3.20	3.10	96.9	9	2.65	0.85
F98-04	185.47	188.52	3.05	3.02	99.0	8	2.18	0.72
F98-04	188.52	191.11	2.59	2.77	106.9	8	2.10	0.76
F98-04	191.11	194.31	3.20	3.11	97.2	6	2.20	0.71
F98-04	194.31	196.90	2.59	1.77	68.3	6	1.25	0.71
F98-04	196.90	198.12	1.22	0.84	68.9	2	0.58	0.69
F98-04	198.12	200.56	2.44	2.39	98.0	5	1.00	0.42

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-04	200.56	202.54	1.98	2.02	102.0	6	1.03	0.51
F98-04	202.54	204.37	1.83	1.79	97.8	2	0.49	0.27
F98-04	204.37	205.59	1.22	1.29	105.7	5	0.65	0.50
F98-04	205.59	208.64	3.05	3.03	99.3	6	1.71	0.56
F98-04	208.64	209.85	1.21	1.11	91.7	1	0.25	0.23
F98-04	209.85	210.62	0.77	0.81	105.2	0	0.00	0.00
F98-04	210.62	213.06	2.44	2.55	104.5	7	1.51	0.59
F98-04	213.06	215.04	1.98	2.05	103.5	8	1.19	0.58
F98-04	215.04	217.93	2.89	2.74	94.8	6	1.78	0.65
F98-04	217.93	219.76	1.83	1.75	95.6	4	0.84	0.48
F98-04	219.76	222.05	2.29	2.20	96.1	1	0.17	0.08
F98-04	222.05	223.42	1.37	1.29	94.2	1	0.18	0.14
F98-04	223.42	224.64	1.22	1.44	118.0	3	0.47	0.33
F98-04	224.64	227.08	2.44	2.36	96.7	3	0.71	0.30
F98-04	227.08	229.21	2.13	2.16	101.4	3	1.25	0.58
F98-04	229.21	231.19	1.98	1.97	99.5	3	0.68	0.35
F98-04	231.19	231.95	0.76	0.79	103.9	3	0.59	0.75
F98-04	231.95	232.87	0.92	1.01	109.8	0	0.00	0.00
F98-04	232.87	235.61	2.74	2.58	94.2	5	1.47	0.57
F98-04	235.61	237.44	1.83	1.94	106.0	3	0.92	0.47
F98-04	237.44	238.05	0.61	0.67	109.8	1	0.42	0.63
F98-04	238.05	240.49	2.44	2.52	103.3	6	1.21	0.48
F98-04	240.49	242.16	1.67	1.70	101.8	3	0.79	0.46
F98-04	242.16	245.06	2.90	2.79	96.2	9	1.77	0.63
F98-04	245.06	248.11	3.05	3.05	100.0	8	2.55	0.84
F98-04	248.11	251.16	3.05	3.01	98.7	8	2.74	0.91
F98-04	251.16	254.20	3.04	3.02	99.3	9	2.63	0.87
F98-04	254.20	257.25	3.05	3.02	99.0	7	2.36	0.78
F98-04	257.25	259.38	2.13	2.23	104.7	7	1.79	0.80
F98-04	259.38	261.67	2.29	2.26	98.7	5	1.18	0.52
F98-04	261.67	264.72	3.05	3.01	98.7	5	2.58	0.86
F98-04	264.72	267.16	2.44	2.42	99.2	5	1.44	0.60
F98-04	267.16	269.75	2.59	2.43	93.8	3	1.43	0.59
F98-04	269.75	272.19	2.44	2.53	103.7	6	1.40	0.55
F98-04	272.19	274.62	2.43	2.36	97.1	8	1.85	0.78
F98-04	274.62	276.45	1.83	1.85	101.1	1	0.13	0.07
F98-04	276.45	279.50	3.05	3.06	100.3	7	2.37	0.77
F98-04	279.50	282.55	3.05	3.03	99.3	5	2.70	0.89
F98-04	282.55	284.99	2.44	2.38	97.5	3	1.68	0.71
F98-04	284.99	288.04	3.05	3.05	100.0	5	2.71	0.89
F98-04	288.04	289.56	1.52	1.50	98.7	1	1.50	1.00
F98-04	289.56	292.30	2.74	2.57	93.8	3	2.33	0.91
F98-04	292.30	295.35	3.05	3.01	98.7	7	2.74	0.91
F98-04	295.35	297.64	2.29	2.33	101.7	4	2.03	0.87
F98-04	297.64	300.69	3.05	3.08	101.0	3	2.82	0.92
F98-04	300.69	303.73	3.04	3.03	99.7	5	2.27	0.75
F98-04	303.73	306.93	3.20	3.13	97.8	2	2.81	0.90
F98-04	306.93	309.98	3.05	3.02	99.0	6	2.64	0.87
F98-04	309.98	313.03	3.05	3.12	102.3	4	2.72	0.87
F98-04	313.03	316.08	3.05	3.08	101.0	4	2.60	0.84

FINDLAY CREEK PROJECT - 1998
Diamond Drill Hole RQD Logs

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-04	316.08	318.97	2.89	2.80	96.9	5	2.17	0.78
F98-04	318.97	319.74	0.77	0.86	111.7	3	0.66	0.77
F98-04	319.74	322.78	3.04	2.78	91.4	5	1.63	0.59
F98-04	322.78	325.83	3.05	3.03	99.3	6	2.66	0.88
F98-04	325.83	328.88	3.05	2.99	98.0	5	2.75	0.92
F98-04	328.88	331.93	3.05	3.08	101.0	5	2.37	0.77
F98-04	331.93	334.98	3.05	3.05	100.0	4	2.58	0.85
F98-04	334.98	338.02	3.04	3.01	99.0	4	2.17	0.72
F98-04	338.02	339.70	1.68	1.68	100.0	5	1.35	0.80
F98-04	339.70	342.75	3.05	3.05	100.0	3	2.95	0.97
F98-04	342.75	345.80	3.05	3.07	100.7	5	2.41	0.79
F98-04	345.80	348.39	2.59	2.43	93.8	7	2.13	0.88
F98-04	348.39	350.22	1.83	1.80	98.4	2	1.70	0.94
F98-04	350.22	353.11	2.89	2.97	102.8	10	2.55	0.86
F98-04	353.11	356.24	3.13	3.12	99.7	4	2.77	0.89
F98-04	356.24	357.68	1.44	1.33	92.4	2	1.09	0.82
F98-04	357.68	360.73	3.05	3.03	99.3	6	2.32	0.77
F98-04	360.73	363.78	3.05	3.08	101.0	3	0.60	0.19
F98-04	363.78	365.46	1.68	1.52	90.5	6	0.68	0.45
F98-04	365.46	368.50	3.04	3.02	99.3	7	2.22	0.74
F98-04	368.50	370.94	2.44	2.41	98.8	10	2.57	1.07
F98-04	370.94	371.09	0.15	0.29	193.3	1	0.21	0.72
F98-04	371.09	373.69	2.60	2.38	91.5	9	2.25	0.95
F98-04	373.69	376.73	3.04	3.03	99.7	10	2.89	0.95
F98-04	376.73	379.09	2.36	2.27	96.2	5	1.89	0.83
F98-04	379.02	381.00	1.98	1.98	100.0	7	1.55	0.78
F98-04	381.00	383.74	2.74	2.86	104.4	11	2.86	1.00
F98-04	383.74	386.79	3.05	2.98	97.7	8	2.84	0.95
F98-04	386.79	389.84	3.05	3.04	99.7	9	3.04	1.00
F98-04	389.84	392.58	2.74	2.74	100.0	5	2.79	1.02
F98-04	392.58	395.63	3.05	2.69	88.2	6	2.69	1.00
F98-04	395.63	397.92	2.29	2.29	100.0	9	2.24	0.98
F98-04	397.92	400.96	3.04	3.05	100.3	11	3.00	0.98
F98-04	400.96	404.01	3.05	3.05	100.0	11	3.05	1.00
F98-04	404.01	407.21	3.20	3.03	94.7	8	3.03	1.00
F98-04	407.21	410.26	3.05	3.05	100.0	7	3.05	1.00
F98-04	410.26	413.31	3.05	3.05	100.0	9	3.05	1.00
F98-04	413.31	416.36	3.05	3.05	100.0	7	2.12	0.70
F98-04	416.36	419.40	3.04	3.04	100.0	8	1.81	0.60
F98-04	419.40	420.62	1.22	1.07	87.7	1	0.79	0.74
F98-04	420.62	422.61	1.99	1.87	94.0	13	1.44	0.77
F98-04	422.61	424.28	1.67	1.67	100.0	7	1.43	0.86
F98-04	424.28	426.72	2.44	2.44	100.0	12	2.13	0.87
F98-04	426.72	428.09	1.37	1.21	88.3	7	1.15	0.95
F98-04	428.09	430.68	2.59	2.59	100.0	11	1.95	0.75
F98-04	430.68	433.73	3.05	3.03	99.3	10	3.03	1.00
F98-04	433.73	436.78	3.05	2.38	78.0	12	1.95	0.82
F98-04	436.78	437.69	0.91	0.62	68.1	3	0.27	0.44
F98-04	437.69	438.30	0.61	0.85	139.3	0	0.00	0.00
F98-04	438.30	438.91	0.61	0.60	98.4	2	0.26	0.43

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-04	438.91	440.39	1.48	1.48	100.0	6	0.91	0.61
F98-04	440.39	442.57	2.18	1.97	90.4	8	1.62	0.82
F98-04	442.57	444.40	1.83	1.83	100.0	7	1.80	0.98
F98-04	444.40	447.45	3.05	2.96	97.0	11	2.87	0.97
F98-04	447.45	450.49	3.04	3.04	100.0	11	3.04	1.00
F98-04	450.49	451.10	0.61	0.57	93.4	3	0.57	1.00
F98-04	451.10	451.71	0.61	0.61	100.0	4	0.60	0.98
F98-04	451.71	452.93	1.22	1.21	99.2	2	0.64	0.53
F98-04	452.93	455.98	3.05	3.05	100.0	16	2.56	0.84
F98-04	455.98	459.18	3.20	3.10	96.9	8	3.10	1.00
F98-04	459.18	462.23	3.05	3.05	100.0	10	3.05	1.00
F98-04	462.23	465.28	3.05	3.05	100.0	7	3.05	1.00
F98-04	465.28	468.33	3.05	3.05	100.0	9	3.05	1.00
F98-04	468.33	471.37	3.04	3.05	100.3	5	3.05	1.00
F98-04	471.37	474.42	3.05	3.05	100.0	9	2.92	0.96
F98-04	474.42	477.47	3.05	3.05	100.0	10	2.65	0.87
F98-04	477.47	480.52	3.05	3.05	100.0	9	2.75	0.90
F98-04	480.52	483.57	3.05	3.05	100.0	9	3.05	1.00
F98-04	483.57	486.77	3.20	3.20	100.0	14	3.20	1.00
F98-04	486.77	487.98	1.21	1.15	95.0	4	0.87	0.76
			485.92	475.64	97.9			

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-05	4.57	5.79	1.22	0.84	68.9	8	0.70	0.83
F98-05	5.79	8.08	2.29	2.22	96.9	15	1.39	0.63
F98-05	8.08	8.99	0.91	0.70	76.9	5	0.47	0.67
F98-05	8.99	10.52	1.53	0.93	60.8	5	0.39	0.42
F98-05	10.52	13.41	2.89	2.78	96.2	26	2.12	0.76
F98-05	13.41	15.39	1.98	1.78	89.9	15	1.34	0.75
F98-05	15.39	17.07	1.68	1.47	87.5	18	1.27	0.86
F98-05	17.07	20.12	3.05	1.58	51.8	25	1.26	0.80
F98-05	20.12	21.64	1.52	0.78	51.3	6	0.65	0.83
F98-05	21.64	22.86	1.22	0.84	68.9	4	0.39	0.46
F98-05	22.86	24.23	1.37	0.78	56.9	2	0.10	0.13
F98-05	24.23	25.60	1.37	0.30	21.9	0	0.00	0.00
F98-05	25.60	26.37	0.77	0.50	64.9	0	0.00	0.00
F98-05	26.37	26.97	0.60	0.16	26.7	0	0.00	0.00
F98-05	26.97	28.50	1.53	0.62	40.5	0	0.00	0.00
F98-05	28.50	30.18	1.68	0.27	16.1	0	0.00	0.00
F98-05	30.18	31.09	0.91	0.75	82.4	2	0.11	0.15
F98-05	31.09	31.70	0.61	0.61	100.0	3	0.23	0.38
F98-05	31.70	33.53	1.83	1.33	72.7	6	0.66	0.50
F98-05	33.53	36.27	2.74	2.27	82.8	13	1.45	0.64
F98-05	36.27	39.17	2.90	1.83	63.1	13	1.19	0.65
F98-05	39.17	41.00	1.83	1.48	80.9	6	0.63	0.43
F98-05	41.00	41.61	0.61	0.61	100.0	5	0.64	1.05
F98-05	41.61	42.82	1.21	0.92	76.0	4	0.32	0.35
F98-05	42.82	43.28	0.46	0.67	145.7	3	0.22	0.33
F98-05	43.28	44.50	1.22	1.08	88.5	2	0.28	0.26
F98-05	44.50	45.26	0.76	0.76	100.0	3	0.35	0.46
F98-05	45.26	47.85	2.59	1.27	49.0	8	0.86	0.68
F98-05	47.85	48.77	0.92	0.63	68.5	0	0.00	0.00
F98-05	48.77	49.68	0.91	0.91	100.0	6	0.37	0.41
F98-05	49.68	51.51	1.83	1.68	91.8	1	0.11	0.07
F98-05	51.51	53.04	1.53	1.34	87.6	5	0.38	0.28
F98-05	53.04	54.56	1.52	1.25	82.2	11	0.91	0.73
F98-05	54.56	56.39	1.83	1.74	95.1	7	0.37	0.21
F98-05	56.39	57.61	1.22	0.95	77.9	7	0.48	0.51
F98-05	57.61	58.83	1.22	1.00	82.0	8	0.72	0.72
F98-05	58.83	60.35	1.52	1.52	100.0	4	0.60	0.39
F98-05	60.35	62.18	1.83	1.69	92.3	8	0.79	0.47
F98-05	62.18	63.55	1.37	1.17	85.4	9	0.62	0.53
F98-05	63.55	66.30	2.75	2.59	94.2	16	1.75	0.68
F98-05	66.30	67.97	1.67	1.48	88.6	10	0.80	0.54
F98-05	67.97	69.80	1.83	1.44	78.7	5	0.64	0.44
F98-05	69.80	72.69	2.89	2.50	86.5	18	1.34	0.54
F98-05	72.69	74.22	1.53	1.43	93.5	10	0.97	0.68
F98-05	74.22	75.90	1.68	1.66	98.8	9	0.67	0.40
F98-05	75.90	76.81	0.91	0.91	100.0	7	0.54	0.59
F98-05	76.81	77.42	0.61	0.35	57.4	0	0.00	0.00
F98-05	77.42	78.33	0.91	0.91	100.0	8	0.71	0.78
F98-05	78.33	81.08	2.75	2.50	90.9	15	2.03	0.81
F98-05	81.08	84.12	3.04	2.68	88.2	13	1.22	0.46

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-05	84.12	85.96	1.84	1.82	98.9	7	1.09	0.60
F98-05	85.96	88.09	2.13	2.01	94.4	15	1.67	0.83
F98-05	88.09	90.98	2.89	2.83	97.9	17	1.73	0.61
F98-05	90.98	92.20	1.22	1.11	91.0	6	0.47	0.42
F98-05	92.20	93.27	1.07	0.99	92.5	8	0.54	0.55
F98-05	93.27	94.49	1.22	1.01	82.8	6	0.46	0.46
F98-05	94.49	96.01	1.52	1.52	100.0	15	0.85	0.56
F98-05	96.01	98.60	2.59	1.62	62.5	14	0.89	0.55
F98-05	98.60	99.97	1.37	1.15	83.9	5	0.31	0.27
F98-05	99.97	101.50	1.53	0.76	49.7	4	0.46	0.61
F98-05	101.50	102.41	0.91	0.90	98.9	2	0.22	0.24
F98-05	102.41	103.63	1.22	0.70	57.4	6	0.37	0.53
F98-05	103.63	105.31	1.68	1.26	75.0	11	0.75	0.60
F98-05	105.31	139.90	34.59	core dropped by helicopter				
F98-05	139.90	141.43	1.53	1.42	92.8	6	0.55	0.39
F98-05	141.43	142.49	1.06	0.95	89.6	8	0.56	0.59
F98-05	142.49	144.63	2.14	1.92	89.7	17	1.41	0.73
F98-05	144.63	146.30	1.67	1.66	99.4	4	0.44	0.27
F98-05	146.30	148.29	1.99	1.91	96.0	12	0.86	0.45
F98-05	148.29	149.50	1.21	1.14	94.2	6	0.45	0.39
F98-05	149.50	150.57	1.07	1.07	100.0	0	0.00	0.00
F98-05	150.57	152.25	1.68	1.68	100.0	7	0.44	0.26
F98-05	152.25	153.31	1.06	0.93	87.7	1	0.13	0.14
F98-05	153.31	154.53	1.22	1.22	100.0	10	0.62	0.51
F98-05	154.53	155.14	0.61	0.44	72.1	2	0.09	0.20
F98-05	155.14	158.19	3.05	2.92	95.7	31	2.60	0.89
F98-05	158.19	160.63	2.44	2.37	97.1	19	1.18	0.50
F98-05	160.63	161.70	1.07	0.89	83.2	6	0.40	0.45
F98-05	161.70	164.29	2.59	2.41	93.1	15	0.98	0.41
F98-05	164.29	165.66	1.37	1.25	91.2	5	0.25	0.20
F98-05	165.66	167.03	1.37	1.37	100.0	8	0.67	0.49
F98-05	167.03	169.16	2.13	2.13	100.0	15	1.70	0.80
F98-05	169.16	170.69	1.53	1.43	93.5	6	0.40	0.28
F98-05	170.69	172.52	1.83	1.76	96.2	9	0.70	0.40
F98-05	172.52	174.65	2.13	2.03	95.3	10	1.30	0.64
F98-05	174.65	176.48	1.83	1.83	100.0	6	0.53	0.29
F98-05	176.48	177.70	1.22	1.13	92.6	6	0.32	0.28
F98-05	177.70	178.31	0.61	0.61	100.0	2	0.30	0.49
F98-05	178.31	179.68	1.37	1.16	84.7	2	0.19	0.16
F98-05	179.68	180.75	1.07	0.39	36.4	0	0.00	0.00
F98-05	180.75	182.12	1.37	1.14	83.2	5	0.40	0.35
F98-05	182.12	182.88	0.76	0.76	100.0	3	0.29	0.38
F98-05	182.88	184.71	1.83	1.34	73.2	8	0.74	0.55
F98-05	184.71	186.08	1.37	1.20	87.6	7	0.93	0.78
F98-05	186.08	187.15	1.07	0.93	86.9	1	0.23	0.25
F98-05	187.15	188.82	1.67	1.62	97.0	12	1.24	0.77
F98-05	188.82	190.04	1.22	1.04	85.2	6	0.76	0.73
F98-05	190.04	192.63	2.59	2.50	96.5	10	2.22	0.89
F98-05	192.63	195.68	3.05	3.00	98.4	18	2.77	0.92
F98-05	195.68	197.82	2.14	2.07	96.7	13	1.77	0.86

FINDLAY CREEK PROJECT - 1998
Diamond Drill Hole RQD Logs

Hole	From	To	Ind. Length	Meas. Length	% Recovery	# > 2.5 core d.	sum of pieces	RQD
F98-05	197.82	199.19	1.37	1.27	92.7	9	0.90	0.71
F98-05	199.19	202.39	3.20	2.97	92.8	17	2.54	0.86
F98-05	202.39	203.15	0.76	0.76	100.0	5	0.58	0.76
F98-05	203.15	204.06	0.91	0.74	81.3	0	0.00	0.00
F98-05	204.06	206.81	2.75	2.72	98.9	13	1.87	0.69
F98-05	206.81	209.85	3.04	2.98	98.0	15	2.38	0.80
F98-05	209.85	211.53	1.68	1.62	96.4	5	0.97	0.60
F98-05	211.53	212.90	1.37	1.37	100.0	7	0.63	0.46
F98-05	212.90	214.88	1.98	1.78	89.9	11	0.99	0.56
F98-05	214.88	215.95	1.07	0.80	74.8	3	0.31	0.39
F98-05	215.95	219.00	3.05	2.90	95.1	13	2.49	0.86
F98-05	219.00	220.98	1.98	1.98	100.0	9	1.62	0.82
F98-05	220.98	223.42	2.44	2.36	96.7	6	1.51	0.64
F98-05	223.42	226.47	3.05	2.97	97.4	12	2.56	0.86
F98-05	226.47	228.30	1.83	1.77	96.7	12	1.48	0.84
F98-05	228.30	231.34	3.04	3.04	100.0	14	2.98	0.98
F98-05	231.34	233.63	2.29	2.04	89.1	13	1.02	0.50
F98-05	233.63	235.15	1.52	1.14	75.0	3	0.22	0.19
F98-05	235.15	236.22	1.07	1.01	94.4	1	0.10	0.10
F98-05	236.22	237.13	0.91	0.90	98.9	3	0.32	0.36
F98-05	237.13	238.35	1.22	0.67	54.9	4	0.25	0.37
F98-05	238.35	239.42	1.07	1.07	100.0	7	1.06	0.99
F98-05	239.42	242.32	2.90	2.78	95.9	10	2.44	0.88
F98-05	242.32	244.30	1.98	1.87	94.4	9	1.14	0.61
F98-05	244.30	247.35	3.05	2.98	97.7	21	2.64	0.89
F98-05	247.35	248.26	0.91	0.91	100.0	3	0.18	0.20
F98-05	248.26	251.31	3.05	2.98	97.7	15	2.65	0.89
F98-05	251.31	254.20	2.89	2.75	95.2	18	2.24	0.81
F98-05	254.20	256.64	2.44	2.32	95.1	21	1.82	0.78
F98-05	256.64	258.17	1.53	1.48	96.7	9	0.76	0.51
F98-05	258.17	259.54	1.37	1.32	96.4	12	1.00	0.76
F98-05	259.54	260.76	1.22	1.22	100.0	9	0.98	0.80
F98-05	260.76	262.28	1.52	1.36	89.5	8	0.58	0.43
F98-05	262.28	263.96	1.68	1.44	85.7	11	0.74	0.51
F98-05	263.96	266.55	2.59	2.59	100.0	27	2.10	0.81
F98-05	266.55	268.38	1.83	1.73	94.5	11	0.85	0.49
F98-05	268.38	269.90	1.52	1.52	100.0	11	0.73	0.48
F98-05	269.90	271.12	1.22	1.04	85.2	5	0.36	0.35
F98-05	271.12	272.80	1.68	1.60	95.2	12	0.82	0.51
F98-05	272.80	274.02	1.22	1.21	99.2	5	0.60	0.50
F98-05	274.02	274.47	0.45	0.45	100.0	3	0.45	1.00
F98-05	274.47	277.06	2.59	2.59	100.0	15	2.58	1.00
F98-05	277.06	279.81	2.75	2.68	97.5	9	2.64	0.99
F98-05	279.81	282.85	3.04	3.04	100.0	11	3.04	1.00
			243.69	214.48	88.0			

Note: calculation of total percent recovery does not include interval lost between 105.31 and 139.90 metres

APPENDIX IX

DRILL CORE SAMPLE RESULTS

FINDLAY CREEK PROJECT - 1998

Drill Core Sample Results

Appendix IX

SAMPLE	HOLE	FROM	TO	WIDTH	AU_PPB	AG_PPM	AL_PCT	AS_PPM	BA_PPM	BE_PPM	BI_PPM	CA_PCT	CD_PPM	CO_PPM	CR_PPM	CU_PPM	FE_PCT	GA_PPM	HG_PPM	K_PCT
VR 74301 A	F98-01	40.50	45.72	5.22		-0.2	1.51	-2	230	-0.5	-2	0.4	0.5	9	67	29	2.57	-10	-1	0.8
VR 74302 A	F98-01	173.31	176.00	2.69		-0.2	3.59	6	100	-0.5	-2	1.81	-0.5	18	102	45	2.66	-10	-1	0.76
VR 74303 A	F98-01	176.00	179.00	3.00		-0.2	1.02	-2	90	-0.5	-2	0.34	-0.5	6	53	21	1.71	-10	-1	0.59
VR 74304 A	F98-01	179.00	182.00	3.00		-0.2	1.51	-2	60	-0.5	-2	0.59	1	10	47	32	2.99	-10	-1	0.88
VR 74305 A	F98-01	182.00	185.00	3.00		-0.2	1.64	-2	90	-0.5	-2	1.07	6	9	62	34	2.93	-10	-1	0.98
VR 74306 A	F98-01	185.00	188.00	3.00		-0.2	1.79	-2	110	-0.5	-2	0.51	-0.5	10	59	26	2.97	-10	-1	1.04
VR 74307 A	F98-01	188.00	191.00	3.00		-0.2	1.86	10	130	-0.5	-2	0.64	1	9	61	34	2.95	-10	-1	1.14
VR 74308 A	F98-01	191.00	191.69	0.69		-0.2	1.85	-2	140	-0.5	-2	0.55	-0.5	12	48	36	3.26	-10	-1	1.11
VR 74309 A	F98-01	191.69	194.00	2.31		-0.2	1.58	-2	100	-0.5	-2	0.5	-0.5	9	48	23	2.78	-10	-1	0.87
VR 74310 A	F98-01	194.00	197.00	3.00		-0.2	1.71	4	110	-0.5	-2	0.41	-0.5	9	71	15	2.61	-10	-1	1.03
VR 74311 A	F98-01	197.00	200.00	3.00		-0.2	1.76	12	140	-0.5	-2	0.36	-0.5	10	92	19	2.78	-10	-1	1.12
VR 74312 A	F98-01	200.00	203.00	3.00		-0.2	1.89	6	170	-0.5	-2	0.29	-0.5	12	92	34	3.1	-10	-1	1.19
VR 74313 A	F98-01	203.00	205.00	2.00		-0.2	1.85	-2	170	-0.5	-2	0.26	-0.5	10	74	30	3.02	-10	-1	1.25
VR 74314 A	F98-01	205.00	207.00	2.00		0.6	1.63	6	110	0.5	22	1.02	-0.5	21	60	269	4.73	-10	-1	0.79
VR 74315 A	F98-01	207.00	210.00	3.00		-0.2	1.94	2	160	-0.5	-2	0.53	-0.5	8	91	7	2.88	-10	-1	1.19
VR 74316 A	F98-01	210.00	211.40	1.40		-0.2	1.9	-2	180	-0.5	-2	0.7	-0.5	9	75	27	2.9	-10	-1	1.13
VR 74317 A	F98-01	211.40	212.00	0.60		0.4	2.57	28	100	0.5	2	0.97	-0.5	18	108	62	6.05	-10	-1	1.19
VR 74318 A	F98-01	212.00	215.00	3.00		-0.2	1.93	-2	160	-0.5	-2	0.47	-0.5	10	63	23	2.93	-10	-1	1.09
VR 74319 A	F98-01	215.00	218.00	3.00		-0.2	2.04	-2	210	-0.5	-2	0.39	-0.5	9	86	17	3.14	-10	-1	1.41
VR 74320 A	F98-01	218.00	221.00	3.00		-0.2	1.61	-2	130	-0.5	-2	0.45	-0.5	8	67	15	2.8	-10	-1	1.01
VR 74321 A	F98-01	221.00	224.00	3.00		-0.2	1.74	2	140	-0.5	-2	0.64	0.5	8	78	19	2.82	-10	-1	1.16
VR 74322 A	F98-01	224.00	227.00	3.00		-0.2	1.66	2	150	-0.5	-2	0.61	-0.5	9	62	32	2.91	-10	-1	1.1
VR 74323 A	F98-01	227.00	230.00	3.00		-0.2	1.91	-2	170	-0.5	-2	0.5	-0.5	10	75	20	3.1	-10	-1	1.25
VR 74324 A	F98-01	230.00	233.00	3.00		-0.2	1.87	2	130	-0.5	-2	0.57	-0.5	8	78	18	2.79	-10	-1	1.29
VR 74325 A	F98-01	233.00	236.00	3.00		-0.2	1.75	-2	110	-0.5	-2	0.33	-0.5	9	49	24	2.81	-10	-1	1.24
VR 74326 A	F98-01	236.00	239.00	3.00		-0.2	1.94	-2	130	-0.5	-2	0.28	-0.5	10	50	22	3.01	-10	-1	1.35
VR 74327 A	F98-01	239.00	242.00	3.00		-0.2	2.11	-2	120	-0.5	-2	0.27	-0.5	9	58	28	3.08	-10	-1	1.49
VR 74328 A	F98-01	242.00	245.00	3.00		-0.2	2.05	-2	110	-0.5	-2	0.33	-0.5	9	61	22	3.14	-10	-1	1.48
VR 74329 A	F98-01	245.00	248.00	3.00		-0.2	2.06	-2	130	-0.5	-2	0.29	-0.5	9	59	19	3.05	-10	-1	1.46
VR 74330 A	F98-01	248.00	251.00	3.00		-0.2	1.81	-2	140	0.5	-2	0.71	-0.5	7	51	12	2.69	-10	-1	1.28
VR 74331 A	F98-01	251.00	254.00	3.00		-0.2	1.72	-2	110	-0.5	4	1.16	-0.5	9	52	27	3.2	-10	-1	1.18
VR 74332 A	F98-01	254.00	257.00	3.00		-0.2	0.73	-2	60	-0.5	-2	0.82	-0.5	4	57	21	1.51	-10	-1	0.41
VR 74333 A	F98-01	257.00	260.00	3.00		-0.2	0.76	-2	50	-0.5	-2	0.48	-0.5	5	58	8	1.45	-10	-1	0.45
VR 74334 A	F98-01	260.00	264.00	4.00		-0.2	0.5	-2	40	-0.5	-2	0.65	-0.5	4	46	21	1.49	-10	-1	0.28
VR 74335 A	F98-01	264.00	266.75	2.75		-0.2	0.88	-2	70	-0.5	-2	0.38	-0.5	9	37	25	2.68	-10	-1	0.54
VR 74336 A	F98-01	266.75	270.00	3.25		-0.2	1.05	-2	80	-0.5	-2	0.49	-0.5	7	40	25	2.33	-10	-1	0.67
VR 74337 A	F98-01	270.00	273.00	3.00		-0.2	1.17	-2	70	-0.5	-2	0.51	-0.5	8	42	22	2.3	-10	-1	0.77
VR 74338 A	F98-01	273.00	275.00	2.00		-0.2	0.76	-2	60	-0.5	2	0.42	-0.5	6	34	35	1.68	-10	-1	0.51
VR 74339 A	F98-01	275.00	276.00	1.00		-0.2	0.64	-2	50	-0.5	-2	0.48	-0.5	4	45	8	1.4	-10	-1	0.42
VR 74657 A	F98-01	276.00	280.00	4.00		-0.2	0.51	-2	60	-0.5	-2	1.32	-0.5	6	60	17	1.23	-10	-1	0.3
VR 74658 A	F98-01	280.00	283.00	3.00		-0.2	0.72	-2	60	-0.5	2	0.5	-0.5	4	90	2	1.13	-10	-1	0.39
VR 74659 A	F98-01	283.00	286.00	3.00		-0.2	0.85	2	60	-0.5	2	0.39	-0.5	5	93	3	1.18	-10	-1	0.45

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Appendix IX

Drill Core Sample Results

SAMPLE			LA_PPM	MG_PCT	MN_PPM	MO_PPM	NA_PCT	NI_PPM	P_PPM	PB_PPM	SB_PPM	SC_PPM	SR_PPM	TI_PCT	TL_PPM	U_PPM	V_PPM	W_PPM	ZN_PPM	CERTIF	ALT_CERTIF
VR	74301	A	10	0.76	340	3	0.03	14	250	6	-2	4	6	0.13	-10	-10	28	-10	160	A9833239	
VR	74302	A	-10	1.23	345	1	0.28	25	170	2'	-2	4	42	0.15	-10	-10	52	-10	52	A9833239	
VR	74303	A	20	0.32	310	-1	0.02	12	170	10	-2	1	7	0.07	-10	-10	9	-10	46	A9833239	
VR	74304	A	20	0.97	485	3	0.01	19	380	32	-2	2	15	0.1	-10	-10	19	-10	260	A9833239	
VR	74305	A	10	1.04	670	2	0.01	20	360	36	-2	2	18	0.1	-10	-10	19	140	1175	A9833239	
VR	74306	A	10	1.14	495	2	0.03	20	350	36	-2	3	13	0.11	-10	-10	24	-10	98	A9833239	
VR	74307	A	10	1.02	460	4	0.01	17	360	26	-2	2	10	0.14	-10	-10	18	-10	290	A9833239	
VR	74308	A	10	0.9	380	3	0.01	20	320	2	-2	2	8	0.13	-10	-10	16	-10	126	A9833239	
VR	74309	A	10	0.71	365	1	0.01	19	320	10	-2	1	7	0.1	-10	-10	14	-10	78	A9833239	
VR	74310	A	10	0.69	435	2	0.02	16	280	4	-2	2	9	0.13	-10	-10	19	-10	48	A9833239	
VR	74311	A	10	0.7	455	-1	0.02	17	300	4	-2	3	10	0.15	-10	-10	21	-10	44	A9833753	
VR	74312	A	20	0.73	440	4	0.02	18	350	4	-2	3	6	0.14	-10	-10	21	-10	52	A9833753	
VR	74313	A	10	0.73	445	3	0.02	18	310	-2	-2	3	4	0.17	-10	-10	22	-10	48	A9833753	
VR	74314	A	10	0.69	735	2	0.02	22	330	18	-2	2	13	0.07	-10	-10	14	-10	104	A9833753	
VR	74315	A	10	0.9	535	1	0.04	13	330	2	-2	4	8	0.17	-10	-10	26	-10	98	A9833753	
VR	74316	A	10	0.91	535	5	0.04	14	370	22	-2	3	9	0.13	-10	-10	23	-10	78	A9833753	
VR	74317	A	10	1.61	2180	1	0.01	33	280	18	-2	9	16	0.09	-10	-10	47	-10	76	A9833753	
VR	74318	A	20	0.86	445	1	0.03	17	310	2	-2	3	9	0.13	-10	-10	22	-10	116	A9833753	
VR	74319	A	10	1	550	-1	0.04	17	350	36	-2	4	10	0.17	-10	-10	26	-10	158	A9833753	
VR	74320	A	10	0.89	525	1	0.04	15	320	22	-2	4	13	0.11	-10	-10	24	-10	102	A9833753	
VR	74321	A	10	0.94	655	-1	0.04	15	340	36	-2	4	12	0.14	-10	-10	24	-10	140	A9833753	
VR	74322	A	10	0.85	575	1	0.03	14	320	10	-2	3	12	0.13	-10	-10	20	-10	130	A9833753	
VR	74323	A	10	0.95	500	1	0.04	15	370	12	-2	4	10	0.15	-10	-10	27	-10	88	A9833753	
VR	74324	A	10	1.03	540	-1	0.05	14	370	64	-2	5	10	0.16	-10	-10	32	-10	156	A9833753	
VR	74325	A	-10	0.94	515	1	0.01	13	380	24	-2	4	5	0.15	-10	-10	30	-10	152	A9834124	
VR	74326	A	10	1.11	555	1	0.01	15	390	22	-2	5	5	0.16	-10	-10	33	-10	136	A9834124	
VR	74327	A	10	1.25	590	2	0.01	14	360	24	-2	7	4	0.17	-10	-10	40	-10	132	A9834124	
VR	74328	A	10	1.22	615	-1	0.01	15	390	20	-2	6	6	0.17	-10	-10	35	-10	172	A9834124	
VR	74329	A	10	1.18	560	1	0.01	15	380	12	-2	5	3	0.17	-10	-10	34	-10	124	A9834124	
VR	74330	A	10	1.02	615	2	0.01	13	330	6	-2	3	9	0.15	-10	-10	23	-10	146	A9834124	
VR	74331	A	10	1.06	780	1	-0.01	14	350	8	-2	3	12	0.15	-10	-10	22	-10	150	A9834124	
VR	74332	A	10	0.32	410	1	0.02	9	110	2	-2	1	8	0.06	-10	-10	9	-10	134	A9834124	
VR	74333	A	10	0.32	245	1	0.01	8	130	2	-2	1	4	0.07	-10	-10	11	-10	30	A9834124	
VR	74334	A	10	0.28	430	1	0.01	10	160	-2	-2	1	7	0.03	-10	-10	7	-10	20	A9834124	
VR	74335	A	10	0.57	420	-1	-0.01	15	210	12	-2	1	7	0.07	-10	-10	11	-10	38	A9834124	
VR	74336	A	10	0.51	310	1	-0.01	12	220	6	-2	1	6	0.09	-10	-10	11	-10	38	A9834124	
VR	74337	A	-10	0.58	340	4	0.01	12	260	2	-2	2	4	0.1	-10	-10	16	-10	40	A9834124	
VR	74338	A	10	0.32	270	1	0.01	10	120	6	-2	1	4	0.07	-10	-10	8	-10	34	A9834124	
VR	74339	A	10	0.3	320	-1	0.01	8	110	8	-2	1	6	0.06	-10	-10	9	-10	38	A9834124	
VR	74657	A	10	0.23	785	-1	0.03	10	110	8	-2	-1	18	0.02	-10	-10	5	-10	14	A9837363	
VR	74658	A	10	0.23	275	-1	0.03	6	170	6	-2	1	10	0.04	-10	-10	7	-10	14	A9837363	
VR	74659	A	20	0.23	215	1	0.04	8	180	2	-2	1	8	0.04	-10	-10	7	-10	16	A9837363	

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Drill Core Sample Results

SAMPLE			HOLE	FROM	TO	WIDTH	AU_PPB	AG_PPM	AL_PCT	AS_PPM	BA_PPM	BE_PPM	BI_PPM	CA_PCT	CD_PPM	CO_PPM	CR_PPM	CU_PPM	FE_PCT	GA_PPM	HG_PPM	K_PCT
VR	74660	A	F98-01	286.00	289.00	3.00		-0.2	0.66	-2	50	-0.5	-2	0.31	-0.5	4	42	6	1.22	-10	-1	0.36
VR	74661	A	F98-01	289.00	292.00	3.00		-0.2	1.27	-2	120	-0.5	-2	0.33	-0.5	8	76	15	2.13	-10	-1	0.74
VR	74662	A	F98-01	292.00	295.00	3.00		-0.2	1.5	-2	140	-0.5	-2	0.4	-0.5	10	96	11	2.44	-10	-1	0.91
VR	74663	A	F98-01	295.00	298.00	3.00		-0.2	2.18	2	130	-0.5	2	0.33	-0.5	11	88	21	3.26	-10	-1	1.41
VR	74664	A	F98-01	298.00	301.00	3.00		-0.2	1.8	2	120	-0.5	-2	0.22	-0.5	10	82	17	2.86	-10	-1	1.18
VR	74665	A	F98-01	301.00	304.00	3.00		-0.2	2.1	-2	90	-0.5	-2	0.26	-0.5	11	82	23	3.25	-10	-1	1.44
VR	74666	A	F98-01	304.00	307.00	3.00		-0.2	1.04	6	70	-0.5	-2	0.35	-0.5	8	54	8	1.87	-10	-1	0.62
VR	74667	A	F98-01	307.00	310.00	3.00		-0.2	1.3	-2	120	-0.5	-2	0.32	-0.5	9	76	25	2.39	-10	-1	0.8
VR	74668	A	F98-01	310.00	313.00	3.00		-0.2	1.37	-2	100	-0.5	-2	0.27	-0.5	8	84	9	2.28	-10	-1	0.79
VR	74669	A	F98-01	313.00	316.00	3.00		-0.2	1.06	-2	50	-0.5	-2	0.4	-0.5	4	89	1	1.46	-10	-1	0.56
VR	74670	A	F98-01	316.00	319.00	3.00		-0.2	1.07	-2	60	-0.5	-2	0.52	-0.5	5	96	8	1.69	-10	-1	0.6
VR	74671	A	F98-01	319.00	322.00	3.00		-0.2	1.19	2	70	-0.5	-2	0.78	-0.5	7	89	18	2.01	-10	-1	0.66
VR	74672	A	F98-01	322.00	324.00	2.00		-0.2	1.26	-2	70	-0.5	-2	0.73	-0.5	7	54	24	2.21	-10	-1	0.69
VR	74673	A	F98-01	324.00	327.00	3.00		-0.2	1.96	2	70	-0.5	2	1.49	-0.5	8	103	22	1.9	-10	-1	0.65
VR	74674	A	F98-01	327.00	330.00	3.00		-0.2	1.45	-2	70	-0.5	-2	0.55	-0.5	11	49	25	2.81	-10	-1	0.73
VR	74675	A	F98-01	330.00	333.00	3.00		-0.2	1.67	2	110	-0.5	2	0.43	-0.5	13	45	43	3.42	-10	-1	0.95
VR	74676	A	F98-01	333.00	336.00	3.00		-0.2	1.76	-2	130	-0.5	-2	0.5	-0.5	13	83	30	3.47	-10	-1	0.96
VR	74677	A	F98-01	336.00	339.00	3.00		-0.2	1.65	-2	130	-0.5	-2	0.34	-0.5	11	72	29	3.07	-10	-1	0.94
VR	74678	A	F98-01	339.00	342.00	3.00		-0.2	1.76	14	150	-0.5	-2	0.29	-0.5	12	41	39	3.02	-10	-1	0.99
VR	74679	A	F98-01	342.00	345.00	3.00		-0.2	1.85	-2	140	-0.5	-2	0.19	-0.5	12	44	24	3.29	-10	-1	1.1
VR	74680	A	F98-01	345.00	348.00	3.00		-0.2	1.58	-2	130	-0.5	2	0.22	-0.5	12	53	45	3.07	-10	-1	0.92
VR	74681	A	F98-01	348.00	351.00	3.00		-0.2	1.71	-2	120	-0.5	-2	0.37	-0.5	11	50	29	3.23	-10	-1	1.08
VR	74682	A	F98-01	351.00	354.00	3.00		-0.2	1.55	-2	120	-0.5	-2	0.27	-0.5	12	45	25	2.9	-10	-1	0.97
VR	74683	A	F98-01	354.00	357.00	3.00		-0.2	1.34	2	110	-0.5	-2	0.28	-0.5	12	62	28	2.98	-10	-1	0.8
VR	74684	A	F98-01	357.00	360.00	3.00		-0.2	1.24	2	80	-0.5	-2	0.33	-0.5	11	55	22	2.62	-10	-1	0.69
VR	74685	A	F98-01	360.00	360.30	0.30		-0.2	1.25	10	70	-0.5	-2	0.33	-0.5	10	57	22	2.67	-10	-1	0.71
VR	74686	A	F98-01	360.30	361.36	1.06		0.8	1.74	218	70	0.5	-2	0.29	-0.5	7	69	25	3.05	-10	-1	0.8
VR	74687	A	F98-01	361.36	365.00	3.64		0.2	1.69	2	100	-0.5	-2	0.31	-0.5	13	64	28	2.99	-10	-1	0.97
VR	74688	A	F98-01	365.00	368.00	3.00		-0.2	1.63	-2	90	-0.5	-2	0.3	-0.5	11	60	26	2.79	-10	-1	0.96
VR	74689	A	F98-01	368.00	371.00	3.00		-0.2	1.71	2	100	-0.5	-2	0.33	-0.5	11	61	38	3.4	-10	-1	0.91
VR	74690	A	F98-01	371.00	374.00	3.00		-0.2	1.52	6	120	-0.5	6	0.37	-0.5	12	45	49	2.76	-10	-1	0.88
VR	74691	A	F98-01	374.00	377.00	3.00		-0.2	1.62	-2	140	-0.5	2	0.35	-0.5	10	50	28	3.11	-10	-1	0.92
VR	74692	A	F98-01	377.00	380.00	3.00		-0.2	1.54	12	110	0.5	-2	0.26	-0.5	12	60	28	3.22	-10	-1	0.7
VR	74693	A	F98-01	380.00	383.00	3.00		-0.2	1.64	8	110	-0.5	-2	0.38	-0.5	11	57	24	3.15	-10	-1	0.87
VR	74694	A	F98-01	383.00	385.25	2.25		-0.2	1.57	-2	150	-0.5	2	0.26	-0.5	12	59	29	2.99	-10	-1	0.95
VR	74695	A	F98-01	385.25	388.10	2.85		0.6	3.05	8	210	1.5	-2	6.34	0.5	32	264	55	5.45	10	-1	2.95
VR	74696	A	F98-01	388.10	391.00	2.90		-0.2	1.04	-2	90	-0.5	-2	0.96	-0.5	7	77	14	1.77	-10	-1	0.41
VR	74697	A	F98-01	391.00	394.00	3.00		-0.2	1.01	-2	100	-0.5	-2	0.53	-0.5	5	58	6	1.89	-10	-1	0.52
VR	74698	A	F98-01	394.00	397.00	3.00		-0.2	0.77	148	60	-0.5	-2	0.41	-0.5	5	107	11	1.07	-10	-1	0.33
VR	74699	A	F98-01	397.00	399.20	2.20		-0.2	1.26	-2	110	-0.5	-2	0.44	-0.5	7	69	11	1.65	-10	-1	0.68
VR	74700	A	F98-01	399.20	399.40	0.20		-0.2	0.79	14	70	0.5	-2	1.17	-0.5	15	70	35	1.6	-10	-1	0.46
VR	74701	A	F98-01	399.40	403.00	3.60		-0.2	1.51	-2	140	-0.5	-2	0.28	-0.5	8	62	12	2.25	-10	-1	0.84

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Appendix IX

SAMPLE			LA_PPM	MG_PCT	MN_PPM	MO_PPM	NA_PCT	NI_PPM	P_PPM	PB_PPM	SB_PPM	SC_PPM	SR_PPM	TI_PCT	TL_PPM	U_PPM	V_PPM	W_PPM	ZN_PPM	CERTIF	ALT_CERTIF
VR	74660	A	10	0.23	205	-1	0.03	5	160	14	-2	-1	5	0.04	-10	-10	6	-10	24	A9837363	
VR	74661	A	10	0.41	235	1	0.04	11	170	2	-2	1	6	0.09	-10	-10	12	-10	40	A9837363	
VR	74662	A	10	0.63	325	1	0.03	11	250	8	-2	3	7	0.12	-10	-10	19	-10	46	A9837363	
VR	74663	A	10	1.26	630	1	0.04	17	330	22	-2	5	8	0.17	-10	-10	30	-10	96	A9837363	
VR	74664	A	10	1.02	495	1	0.04	16	280	-2	-2	4	6	0.15	-10	-10	25	-10	40	A9837363	
VR	74665	A	10	1.5	635	1	0.05	16	330	20	-2	6	8	0.17	-10	-10	37	-10	148	A9837363	
VR	74666	A	10	0.39	240	-1	0.01	9	120	2	-2	1	4	0.09	-10	-10	11	-10	40	A9837363	
VR	74667	A	10	0.51	265	1	0.03	11	200	12	-2	2	4	0.11	-10	-10	13	-10	66	A9837363	
VR	74668	A	10	0.45	280	1	0.02	11	140	8	-2	1	4	0.1	-10	-10	13	-10	56	A9837363	
VR	74669	A	10	0.29	260	-1	0.04	7	90	8	-2	1	4	0.09	-10	-10	12	-10	46	A9837363	
VR	74670	A	10	0.32	350	-1	0.03	10	110	12	-2	1	6	0.08	-10	-10	11	-10	68	A9837363	
VR	74671	A	10	0.45	455	1	0.03	12	140	4	-2	1	10	0.09	-10	-10	12	-10	50	A9837363	
VR	74672	A	10	0.51	405	3	0.02	15	250	2	-2	1	10	0.09	-10	-10	11	-10	50	A9837363	
VR	74673	A	10	0.45	460	1	0.11	18	150	12	2	1	11	0.1	-10	-10	15	-10	62	A9837363	
VR	74674	A	10	0.61	305	1	0.03	17	220	2	-2	1	6	0.11	-10	-10	15	-10	36	A9837363	
VR	74675	A	10	0.93	355	6	0.01	18	320	-2	-2	3	7	0.13	-10	-10	19	-10	54	A9837363	
VR	74676	A	10	0.86	345	1	0.02	20	280	4	-2	3	9	0.13	-10	-10	19	-10	54	A9837363	
VR	74677	A	10	0.78	280	1	0.03	18	240	-2	-2	2	6	0.12	-10	-10	18	-10	70	A9837363	
VR	74678	A	10	0.7	270	1	0.02	18	270	-2	-2	2	6	0.11	-10	-10	16	-10	54	A9837362	
VR	74679	A	10	0.67	295	1	0.02	16	220	-2	-2	3	5	0.12	-10	-10	22	-10	42	A9837362	
VR	74680	A	20	0.61	245	2	0.02	19	230	-2	-2	2	7	0.1	-10	-10	15	-10	38	A9837362	
VR	74681	A	10	1.02	335	1	0.04	17	370	36	-2	3	12	0.12	-10	-10	25	-10	90	A9837362	
VR	74682	A	10	0.82	245	-1	0.05	15	340	6	-2	3	8	0.12	-10	-10	23	-10	42	A9837362	
VR	74683	A	10	0.85	230	2	0.04	16	350	30	-2	3	11	0.08	-10	-10	20	-10	46	A9837362	
VR	74684	A	10	0.79	210	1	0.05	15	390	10	2	3	16	0.06	-10	-10	21	-10	22	A9837362	
VR	74685	A	20	0.81	295	2	0.05	16	350	10	-2	3	19	0.06	-10	-10	17	-10	30	A9837362	
VR	74686	A	10	0.77	1090	2	0.02	17	300	166	-2	3	19	0.05	-10	-10	18	-10	42	A9837362	
VR	74687	A	10	0.92	340	1	0.06	17	420	38	-2	4	13	0.11	-10	-10	29	-10	50	A9837362	
VR	74688	A	10	0.93	255	1	0.06	16	350	18	-2	4	11	0.11	-10	-10	25	-10	34	A9837362	
VR	74689	A	10	0.95	405	1	0.05	15	350	30	-2	4	20	0.09	-10	-10	21	-10	66	A9837362	
VR	74690	A	10	0.77	275	3	0.05	15	310	10	-2	3	11	0.09	-10	-10	19	-10	34	A9837362	
VR	74691	A	10	0.8	260	1	0.06	16	360	4	-2	3	17	0.1	-10	-10	19	-10	32	A9837362	
VR	74692	A	20	0.58	325	2	0.03	18	280	-2	2	2	17	0.05	-10	-10	12	-10	40	A9837362	
VR	74693	A	20	0.8	245	3	0.04	17	310	8	-2	2	23	0.08	-10	-10	16	-10	42	A9837362	
VR	74694	A	10	0.84	220	3	0.07	17	320	20	-2	4	15	0.13	-10	-10	27	-10	44	A9837362	
VR	74695	A	40	3.6	1290	3	0.04	60	3550	266	-2	9	787	0.04	-10	-10	146	-10	220	A9837362	
VR	74696	A	30	0.66	290	3	0.05	14	650	62	2	3	81	0.03	-10	-10	15	-10	46	A9837362	
VR	74697	A	20	0.43	345	-1	0.04	11	230	2	-2	2	27	0.04	-10	-10	11	-10	32	A9837362	
VR	74698	A	20	0.22	195	-1	0.05	7	90	18	-2	1	13	0.05	-10	-10	9	-10	32	A9837362	
VR	74699	A	20	0.41	205	-1	0.05	13	150	6	-2	2	10	0.08	-10	-10	14	-10	30	A9837362	
VR	74700	A	30	0.4	550	1	0.04	23	320	6	6	2	35	-0.01	-10	-10	5	-10	6	A9837362	
VR	74701	A	20	0.53	230	1	0.03	12	170	2	-2	2	10	0.09	-10	-10	16	-10	34	A9837362	

SAMPLE	HOLE	FROM	TO	WIDTH	AU_PPB	AG_PPM	AL_PCT	AS_PPM	BA_PPM	BE_PPM	BI_PPM	CA_PCT	CD_PPM	CO_PPM	CR_PPM	CU_PPM	FE_PCT	GA_PPM	HG_PPM	K_PCT
VR 74702 A	F98-01	403.00	406.00	3.00		-0.2	1.72	2	170	-0.5	-2	0.25	-0.5	12	44	32	3.05	-10	-1	1.01
VR 74703 A	F98-01	406.00	409.00	3.00		-0.2	1.47	2	130	-0.5	-2	0.29	-0.5	12	60	16	2.26	-10	-1	0.86
VR 74704 A	F98-01	409.00	412.00	3.00		-0.2	1.69	6	160	-0.5	-2	0.19	-0.5	10	38	17	2.67	-10	-1	0.96
VR 74705 A	F98-01	412.00	415.00	3.00		-0.2	1.97	56	120	-0.5	-2	0.3	0.5	15	64	30	3.82	-10	-1	1.15
VR 74706 A	F98-01	415.00	418.00	3.00		-0.2	1.84	2	100	-0.5	2	0.3	-0.5	12	68	25	3.23	-10	-1	1.13
VR 74707 A	F98-01	418.00	421.00	3.00		-0.2	2.05	-2	110	-0.5	2	0.54	-0.5	11	72	30	3.49	-10	-1	1.23
VR 74708 A	F98-01	421.00	424.00	3.00		-0.2	1.12	-2	70	-0.5	-2	0.49	-0.5	6	72	14	1.69	-10	-1	0.54
VR 74709 A	F98-01	424.00	427.00	3.00		-0.2	1.41	-2	120	-0.5	-2	0.39	-0.5	9	67	19	2.26	-10	-1	0.74
VR 74710 A	F98-01	427.00	428.70	1.70		-0.2	1.62	6	150	-0.5	-2	0.19	-0.5	17	60	18	2.71	-10	-1	0.9
VR 74711 A	F98-01	428.70	428.90	0.20		-0.2	0.92	4	100	-0.5	-2	0.46	-0.5	5	58	-1	1.35	-10	-1	0.4
VR 74712 A	F98-01	428.90	432.00	3.10		-0.2	1.59	-2	120	-0.5	-2	0.28	-0.5	9	83	14	2.4	-10	-1	0.78
VR 74713 A	F98-01	432.00	435.00	3.00		-0.2	0.93	2	70	-0.5	-2	0.41	-0.5	4	98	12	1.47	-10	-1	0.54
VR 74714 A	F98-01	435.00	438.00	3.00		-0.2	0.64	-2	50	-0.5	-2	0.37	-0.5	1	102	4	1.02	-10	-1	0.35
VR 74715 A	F98-01	438.00	441.00	3.00		-0.2	0.65	-2	50	-0.5	-2	0.24	-0.5	1	87	1	1.01	-10	1	0.38
VR 74716 A	F98-01	441.00	444.00	3.00		-0.2	0.68	2	70	-0.5	-2	0.35	-0.5	4	70	23	1.29	-10	-1	0.4
VR 74717 A	F98-01	444.00	447.00	3.00		-0.2	1.41	4	150	-0.5	-2	0.31	-0.5	8	63	21	2.47	-10	-1	0.89
VR 74718 A	F98-01	447.00	450.00	3.00		-0.2	1.25	2	140	-0.5	-2	0.27	-0.5	5	69	15	2.07	-10	-1	0.79
VR 74719 A	F98-01	450.00	453.00	3.00		-0.2	1.8	-2	190	-0.5	-2	0.29	-0.5	8	67	23	3.04	-10	1	1.19
VR 74720 A	F98-01	453.00	456.00	3.00		-0.2	1.54	-2	170	-0.5	-2	0.29	-0.5	8	60	22	2.56	-10	-1	0.94
VR 74721 A	F98-01	456.00	459.00	3.00		-0.2	0.97	-2	100	-0.5	-2	0.34	-0.5	5	76	9	1.54	-10	-1	0.54
VR 74722 A	F98-01	459.00	462.00	3.00		-0.2	1.62	-2	180	-0.5	-2	0.21	-0.5	8	47	22	2.82	-10	1	1.04
VR 74723 A	F98-01	462.00	465.00	3.00		-0.2	1.23	-2	140	-0.5	-2	0.26	-0.5	5	66	11	1.99	-10	-1	0.73
VR 74724 A	F98-01	465.00	468.00	3.00		-0.2	1.81	4	160	-0.5	-2	0.23	-0.5	10	44	28	3.22	-10	-1	1.16
VR 74725 A	F98-01	468.00	471.00	3.00		-0.2	1.17	2	140	-0.5	-2	0.28	-0.5	5	82	9	1.95	-10	1	0.66
VR 74726 A	F98-01	471.00	474.00	3.00		-0.2	1.97	2	160	0.5	-2	0.22	-0.5	10	33	28	3.4	-10	-1	1.31
VR 74727 A	F98-01	474.00	477.00	3.00		-0.2	1.28	6	140	-0.5	-2	0.24	-0.5	6	71	7	1.95	-10	-1	0.79
VR 74728 A	F98-01	477.00	478.23	1.23		-0.2	1.44	-2	170	-0.5	-2	0.22	-0.5	6	58	12	2.4	-10	-1	0.93
VR 74590 A	F98-04	2.13	6.00	3.87		-0.2	1.19	6	100	1.5	-2	0.21	0.5	7	49	41	2.13	-10	-1	0.67
VR 74591 A	F98-04	6.00	9.00	3.00		-0.2	0.98	4	100	2	2	0.34	1.5	8	91	26	1.28	-10	-1	0.54
VR 74592 A	F98-04	9.00	12.00	3.00		-0.2	1.13	6	100	2	-2	0.38	0.5	7	64	28	1.87	-10	-1	0.68
VR 74593 A	F98-04	12.00	15.00	3.00		0.2	1.32	2	130	1.5	2	0.28	-0.5	6	75	20	2.12	-10	-1	0.76
VR 74594 A	F98-04	15.00	15.50	0.50		-0.2	1.52	-2	160	1	-2	0.53	0.5	9	67	50	2.25	-10	-1	0.88
VR 74595 A	F98-04	15.50	15.90	0.40		-0.2	5.25	6	360	2	-2	1.56	2	28	161	5	7.24	10	-1	3.98
VR 74596 A	F98-04	15.90	18.00	2.10		-0.2	1.6	2	160	0.5	-2	0.3	0.5	13	53	93	2.91	-10	-1	0.93
VR 74597 A	F98-04	18.00	21.00	3.00		-0.2	1.55	4	140	2	2	0.33	1	8	93	30	2.23	-10	-1	0.86
VR 74598 A	F98-04	21.00	24.00	3.00		-0.2	1.39	2	110	2	-2	0.45	1.5	10	63	43	2	-10	-1	0.76
VR 74599 A	F98-04	24.00	27.00	3.00		-0.2	1.54	-2	120	1.5	-2	0.55	1.5	12	59	94	2.73	-10	-1	0.91
VR 74600 A	F98-04	27.00	30.00	3.00		-0.2	1.05	2	50	2.5	2	0.57	0.5	4	79	39	1.01	-10	-1	0.48
VR 74601 A	F98-04	30.00	33.00	3.00		-0.2	1.48	2	90	2.5	2	0.65	0.5	8	44	51	1.87	-10	-1	0.78
VR 74602 A	F98-04	33.00	36.00	3.00		-0.2	1.66	6	120	2	-2	0.65	1.5	15	61	87	2.63	-10	-1	0.91
VR 74603 A	F98-04	36.00	39.00	3.00		-0.2	1.96	-2	160	1	-2	0.64	1.5	16	74	123	3.53	-10	-1	1.26
VR 74604 A	F98-04	39.00	42.00	3.00		-0.2	1.35	4	100	1.5	-2	0.33	0.5	9	80	44	2.22	-10	-1	0.68

FINDLAY CREEK PROJECT - 1998 Appendix IX

Drill Core Sample Results

SAMPLE			LA_PPM	MG_PCT	MN_PPM	MO_PPM	NA_PCT	NI_PPM	P_PPM	PB_PPM	SB_PPM	SC_PPM	SR_PPM	TI_PCT	TL_PPM	U_PPM	V_PPM	W_PPM	ZN_PPM	CERTIF	ALT_CERTIF
VR	74702	A	10	0.7	200	3	0.05	16	300	6	-2	3	8	0.13	-10	-10	18	-10	26	A9837362	
VR	74703	A	10	0.59	205	-1	0.04	14	270	2	-2	2	7	0.11	-10	-10	16	-10	28	A9837362	
VR	74704	A	10	0.64	225	1	0.04	14	240	4	-2	3	9	0.11	-10	-10	16	-10	30	A9837362	
VR	74705	A	10	0.98	280	3	0.05	21	320	18	-2	3	13	0.13	-10	-10	24	-10	88	A9837362	
VR	74706	A	10	1.05	305	1	0.07	17	340	40	-2	4	12	0.15	-10	-10	27	-10	106	A9837362	
VR	74707	A	10	1.21	365	3	0.07	17	470	6	-2	5	16	0.16	-10	-10	34	-10	84	A9837362	
VR	74708	A	10	0.39	205	-1	0.03	11	140	2	-2	1	11	0.06	-10	-10	11	-10	24	A9837362	
VR	74709	A	20	0.47	195	1	0.03	16	190	-2	-2	1	10	0.09	-10	-10	14	-10	20	A9837362	
VR	74710	A	10	0.52	215	1	0.02	18	190	-2	-2	2	6	0.1	-10	-10	17	-10	32	A9837362	
VR	74711	A	10	0.14	200	1	0.03	7	190	-2	-2	1	18	-0.01	-10	-10	4	-10	2	A9837362	
VR	74712	A	30	0.48	225	1	0.03	16	240	-2	-2	3	11	0.09	-10	-10	16	-10	22	A9837362	
VR	74713	A	10	0.32	205	1	0.04	8	170	2	-2	1	7	0.1	-10	-10	14	-10	26	A9837568	
VR	74714	A	10	0.23	150	1	0.04	7	210	2	-2	1	6	0.07	-10	-10	12	-10	16	A9837568	
VR	74715	A	10	0.25	110	-1	0.05	7	130	2	-2	1	5	0.07	-10	-10	12	-10	12	A9837568	
VR	74716	A	10	0.27	230	-1	0.04	10	130	4	-2	1	7	0.05	-10	-10	11	-10	18	A9837568	
VR	74717	A	10	0.51	200	1	0.03	12	270	10	-2	2	8	0.1	-10	-10	16	-10	62	A9837568	
VR	74718	A	10	0.43	200	-1	0.03	13	170	6	-2	2	6	0.1	-10	-10	16	-10	46	A9837568	
VR	74719	A	10	0.72	285	1	0.03	13	270	16	-2	3	8	0.13	-10	-10	20	-10	60	A9837568	
VR	74720	A	10	0.5	240	-1	0.03	13	220	6	-2	3	8	0.11	-10	-10	16	-10	60	A9837568	
VR	74721	A	20	0.31	185	-1	0.04	9	120	6	-2	2	9	0.07	-10	-10	12	-10	30	A9837568	
VR	74722	A	10	0.52	240	-1	0.03	14	190	2	2	3	6	0.13	-10	-10	18	-10	52	A9837568	
VR	74723	A	10	0.39	210	-1	0.05	10	130	8	2	3	8	0.1	-10	-10	15	-10	38	A9837568	
VR	74724	A	20	0.75	345	1	0.03	16	230	6	-2	3	9	0.12	-10	-10	23	-10	52	A9837568	
VR	74725	A	10	0.41	245	1	0.04	10	120	2	-2	3	10	0.09	-10	-10	16	-10	30	A9837568	
VR	74726	A	30	0.7	320	-1	0.01	19	270	2	-2	2	8	0.15	-10	-10	22	-10	48	A9837568	
VR	74727	A	10	0.43	240	1	0.04	11	160	2	2	3	7	0.1	-10	-10	17	-10	24	A9837568	
VR	74728	A	10	0.46	260	-1	0.04	12	140	4	-2	3	6	0.13	-10	-10	20	-10	30	A9837568	
VR	74590	A	20	0.5	330	1	0.03	14	340	2	2	3	5	0.08	-10	-10	20	-10	194	A9836577	
VR	74591	A	20	0.22	385	2	0.03	12	160	10	-2	1	4	0.06	-10	-10	11	-10	326	A9836577	
VR	74592	A	10	0.31	465	1	0.02	12	170	8	2	1	5	0.08	-10	-10	12	-10	174	A9836577	
VR	74593	A	10	0.42	325	2	0.02	13	210	2	2	2	4	0.08	-10	-10	14	-10	86	A9836577	
VR	74594	A	10	0.51	570	-1	0.04	11	200	4	-2	1	9	0.12	-10	-10	14	10	222	A9836577	
VR	74595	A	-10	3.19	3280	1	-0.01	47	200	-2	2	18	7	0.26	10	-10	163	-10	768	A9836577	
VR	74596	A	10	0.58	475	3	0.03	17	310	12	2	2	5	0.12	-10	-10	15	-10	246	A9836577	
VR	74597	A	10	0.39	425	3	0.03	12	190	8	-2	2	5	0.09	-10	-10	13	-10	304	A9836577	
VR	74598	A	10	0.41	470	1	0.01	13	220	14	2	1	6	0.08	-10	-10	12	-10	286	A9836577	
VR	74599	A	10	0.52	455	4	0.02	17	330	10	2	1	5	0.11	-10	-10	14	-10	332	A9836577	
VR	74600	A	30	0.16	250	1	0.01	5	110	-2	2	1	5	0.05	-10	-10	9	-10	246	A9836577	
VR	74601	A	20	0.33	445	1	0.01	15	230	2	-2	1	6	0.07	-10	-10	11	-10	226	A9836577	
VR	74602	A	20	0.53	480	2	0.01	15	320	8	-2	1	7	0.09	-10	-10	13	-10	328	A9836577	
VR	74603	A	20	0.97	575	3	0.03	16	430	18	-2	5	9	0.16	-10	-10	29	-10	374	A9836577	
VR	74604	A	10	0.47	410	1	0.02	14	220	4	2	1	6	0.08	-10	-10	13	-10	182	A9836577	

SAMPLE	HOLE	FROM	TO	WIDTH	AU_PPB	AG_PPM	AL_PCT	AS_PPM	BA_PPM	BE_PPM	BI_PPM	CA_PCT	CD_PPM	CO_PPM	CR_PPM	CU_PPM	FE_PCT	GA_PPM	HG_PPM	K_PCT
VR 74605 A	F98-04	42.00	45.00	3.00		-0.2	1.25	2	80	1.5	-2	0.45	0.5	6	82	38	1.9	-10	-1	0.52
VR 74606 A	F98-04	45.00	48.00	3.00		-0.2	1.21	14	30	1.5	-2	0.14	0.5	10	109	19	1.76	-10	-1	0.34
VR 74607 A	F98-04	48.00	50.00	2.00		-0.2	1.27	158	60	1.5	-2	0.3	3	85	81	53	3.44	-10	-1	0.46
VR 74608 A	F98-04	50.00	52.00	2.00		-0.2	1.57	6	70	2	-2	0.31	1.5	7	86	29	2.8	-10	-1	0.54
VR 74609 A	F98-04	52.00	53.00	1.00		1.6	1.74	18	110	3	4	0.54	4	21	54	209	4.43	-10	-1	0.6
VR 74610 A	F98-04	53.00	55.75	2.75		-0.2	2.21	4	190	4	8	1.25	1	15	70	192	4.74	-10	-1	0.89
VR 74611 A	F98-04	55.75	57.70	1.95		-0.2	4.72	8	510	6.5	-2	5.36	-0.5	26	258	11	6.98	10	-1	3.38
VR 74612 A	F98-04	57.70	60.00	2.30		-0.2	3.05	2	200	3	4	2.41	-0.5	24	49	256	7.75	-10	-1	1.36
VR 74613 A	F98-04	60.00	63.00	3.00		-0.2	3.08	2	140	2	6	2.47	-0.5	21	45	169	6.94	-10	-1	1.07
VR 74614 A	F98-04	65.50	66.70	1.20		0.8	2.07	-2	110	3	24	2.86	-0.5	54	57	675	8.3	-10	-1	0.82
VR 74615 A	F98-04	80.00	83.00	3.00		-0.2	3.07	10	110	2	-2	2.59	-0.5	31	40	85	6.23	-10	-1	0.74
VR 74616 A	F98-04	93.08	93.75	0.67	-5	1.4	1.76	-2	20	3.5	58	1.33	5	368	54	2720	15	-10	-1	0.62
VR 74617 A	F98-04	181.23	181.42	0.19	5	0.8	5.43	-2	200	5.5	22	2.57	17.5	35	621	434	5.85	-10	-1	3.96
VR 74618 A	F98-04	205.10	205.25	0.15	10	0.4	6.02	-2	240	12.5	84	5.67	9.5	42	254	664	6.28	-10	-1	3.32
VR 74619 A	F98-04	207.96	211.00	3.04		-0.2	1.85	-2	160	0.5	-2	0.75	-0.5	7	101	21	2.22	-10	-1	0.81
VR 74620 A	F98-04	211.00	214.00	3.00		-0.2	1.66	4	130	0.5	-2	0.66	-0.5	10	85	30	2.81	-10	-1	0.75
VR 74621 A	F98-04	214.00	217.00	3.00		-0.2	0.83	2	90	0.5	-2	0.68	-0.5	3	121	13	1.16	-10	-1	0.39
VR 74622 A	F98-04	217.00	220.00	3.00		-0.2	1.55	2	140	1.5	-2	0.57	-0.5	8	65	40	1.95	-10	-1	0.82
VR 74623 A	F98-04	220.00	223.00	3.00		-0.2	0.96	-2	70	1	-2	0.82	-0.5	5	86	42	1.49	-10	-1	0.45
VR 74624 A	F98-04	223.00	226.00	3.00		-0.2	1.31	-2	80	0.5	-2	0.72	-0.5	7	87	21	2.26	-10	-1	0.5
VR 74625 A	F98-04	226.00	229.40	3.40		-0.2	1.42	2	100	0.5	-2	0.75	-0.5	11	100	37	2.18	-10	-1	0.6
VR 74626 A	F98-04	229.40	232.00	2.60		-0.2	4.89	18	200	1.5	-2	2.35	2.5	26	144	30	4.68	-10	-1	2.15
VR 74627 A	F98-04	250.60	251.25	0.65	10	0.8	5.85	-2	160	21.5	44	5.43	44	38	95	580	5.77	-10	-1	2.99
VR 74628 A	F98-04	264.72	264.95	0.23	5	1	4.89	-2	130	6	10	3.67	12.5	29	114	639	4.64	-10	-1	2.75
VR 74629 A	F98-04	273.20	273.45	0.25	-5	-0.2	5.11	-2	140	100	-2	7.79	10	15	130	35	3.3	-10	-1	2.8
VR 74630 A	F98-04	411.55	412.84	1.29	10	-0.2	3.25	-2	180	3.5	78	1.49	105	45	279	235	6.04	-10	-1	2.45
VR 74631 A	F98-04	417.20	420.00	2.80		-0.2	1.65	-2	140	3	-2	0.53	0.5	8	85	47	2.16	-10	-1	0.89
VR 74632 A	F98-04	420.00	423.00	3.00		-0.2	1.19	4	70	0.5	4	0.6	-0.5	5	83	15	1.79	-10	-1	0.53
VR 74633 A	F98-04	423.00	426.00	3.00		-0.2	1.29	-2	80	0.5	-2	0.55	-0.5	5	96	13	1.72	-10	-1	0.66
VR 74634 A	F98-04	426.00	429.00	3.00		-0.2	1.56	8	130	0.5	-2	0.61	-0.5	8	91	25	2.55	-10	-1	0.87
VR 74635 A	F98-04	429.00	432.00	3.00		-0.2	1.59	-2	140	0.5	-2	0.41	1	8	81	24	2.39	-10	-1	0.84
VR 74636 A	F98-04	432.00	435.00	3.00		-0.2	1.22	-2	130	0.5	-2	0.41	-0.5	5	68	7	1.64	-10	-1	0.65
VR 74637 A	F98-04	435.00	438.00	3.00		0.6	1.63	18	120	0.5	-2	0.59	0.5	9	73	37	3.01	-10	-1	0.8
VR 74638 A	F98-04	438.00	439.00	1.00		1.2	0.99	22	70	0.5	-2	0.4	0.5	4	89	37	2.23	-10	-1	0.47
VR 74639 A	F98-04	439.00	439.34	0.34	-5	7.4	0.4	2	10	0.5	4	0.4	39	1	115	110	9.61	-10	-1	0.28
VR 74640 A	F98-04	439.34	442.00	2.66		1	0.87	12	70	0.5	-2	0.54	2	3	101	20	2.03	-10	-1	0.49
VR 74641 A	F98-04	442.00	445.00	3.00		-0.2	1.12	2	130	0.5	-2	0.34	-0.5	5	93	5	1.79	-10	-1	0.63
VR 74642 A	F98-04	445.00	448.00	3.00		-0.2	1.84	-2	190	0.5	-2	0.28	-0.5	9	51	18	2.74	-10	-1	1.12
VR 74643 A	F98-04	448.00	451.00	3.00		-0.2	1.75	-2	120	-0.5	-2	0.29	-0.5	10	70	31	3.11	-10	-1	1.12
VR 74644 A	F98-04	451.00	454.00	3.00		-0.2	1.2	-2	120	0.5	-2	0.32	-0.5	5	88	15	1.82	-10	-1	0.67
VR 74645 A	F98-04	454.00	457.00	3.00		-0.2	1.21	2	120	1.5	2	0.36	-0.5	6	77	23	1.51	-10	-1	0.7
VR 74646 A	F98-04	457.00	460.00	3.00		-0.2	1.81	-2	160	-0.5	-2	0.35	-0.5	10	45	31	3.15	-10	-1	1.08

SAMPLE	LA_PPM	MG_PCT	MN_PPM	MO_PPM	NA_PCT	NI_PPM	P_PPM	PB_PPM	SB_PPM	SC_PPM	SR_PPM	TI_PCT	TL_PPM	U_PPM	V_PPM	W_PPM	ZN_PPM	CERTIF	ALT_CERTIF
VR 74605 A	20	0.28	385	1	0.04	10	200	-2	-2	1	7	0.05	-10	-10	12	10	196	A9837222	
VR 74606 A	20	0.21	345	-1	0.04	10	120	10	-2	1	5	0.04	-10	-10	10	-10	360	A9837222	
VR 74607 A	40	0.26	640	1	0.03	18	370	6	-2	1	5	0.04	-10	-10	10	10	838	A9837222	
VR 74608 A	10	0.32	620	1	0.03	7	180	14	-2	3	7	0.06	-10	-10	16	-10	514	A9837222	
VR 74609 A	30	0.21	505	1	0.01	4	770	220	2	5	7	0.05	-10	-10	4	30	530	A9837222	
VR 74610 A	10	0.26	580	1	0.03	2	730	6	-2	7	13	0.14	-10	-10	1	110	354	A9837222	
VR 74611 A	40	3.7	1985	-1	0.02	104	5150	2	2	15	140	0.03	-10	-10	118	20	350	A9837222	
VR 74612 A	-10	0.73	1405	1	0.08	1	610	-2	-2	20	18	0.27	-10	-10	14	80	166	A9837222	
VR 74613 A	-10	0.73	840	-1	0.15	1	470	-2	-2	21	11	0.27	-10	-10	39	30	98	A9837222	
VR 74614 A	-10	0.68	1435	1	0.03	1	380	2	-2	11	21	0.13	-10	-10	49	20	82	A9837222	
VR 74615 A	-10	1.06	920	1	0.2	2	350	-2	2	19	14	0.31	-10	-10	305	10	126	A9837222	
VR 74616 A	-10	0.62	480	-1	0.15	149	60	2	4	7	15	0.08	-10	-10	64	120	1200	A9837222	
VR 74617 A	-10	4.54	1710	-1	0.13	64	130	-2	4	7	18	0.14	10	-10	122	370	4340	A9837222	
VR 74618 A	-10	3.04	1880	-1	0.62	45	210	-2	2	9	57	0.15	-10	-10	109	590	2470	A9837222	
VR 74619 A	20	0.68	335	1	0.1	13	210	-2	-2	5	15	0.12	-10	-10	29	10	54	A9837222	
VR 74620 A	20	0.66	525	1	0.04	16	200	-2	-2	2	16	0.08	-10	-10	17	10	54	A9837222	
VR 74621 A	10	0.26	385	1	0.06	9	160	2	-2	1	14	0.07	-10	-10	12	30	114	A9837222	
VR 74622 A	20	0.46	475	-1	0.05	13	180	-2	-2	2	12	0.08	-10	-10	15	40	134	A9837222	
VR 74623 A	30	0.29	585	1	0.06	10	130	6	-2	1	15	0.03	-10	-10	10	110	62	A9837222	
VR 74624 A	30	0.48	550	-1	0.05	14	190	-2	-2	2	17	0.04	-10	-10	12	-10	52	A9837222	
VR 74625 A	10	0.63	565	1	0.06	15	260	-2	-2	4	15	0.08	-10	-10	23	20	56	A9837222	
VR 74626 A	-10	2.43	990	-1	0.19	29	190	-2	2	11	40	0.16	-10	-10	96	110	662	A9837222	
VR 74627 A	-10	3.08	1245	-1	0.66	25	230	-2	4	9	42	0.17	10	10	121	940	9440	A9837222	
VR 74628 A	-10	3.23	1480	-1	0.22	24	150	-2	2	8	23	0.1	-10	-10	94	500	3150	A9837222	
VR 74629 A	-10	2.15	1685	-1	0.49	20	140	-2	2	14	38	0.11	-10	-10	91	170	2440	A9837222	
VR 74630 A	-10	2.57	1325	1	0.03	81	140	-2	4	18	7	0.13	-10	10	109	340	25500	A9837222	A9837861
VR 74631 A	20	0.55	410	-1	0.03	14	180	-2	-2	3	7	0.06	-10	-10	18	80	310	A9837222	
VR 74632 A	30	0.42	575	1	0.04	11	170	6	-2	2	8	0.05	-10	-10	12	10	100	A9837222	
VR 74633 A	10	0.45	355	-1	0.05	12	130	2	-2	2	5	0.09	-10	-10	16	-10	50	A9837222	
VR 74634 A	10	0.64	465	1	0.05	14	240	-2	-2	3	9	0.11	-10	-10	20	-10	52	A9837222	
VR 74635 A	10	0.53	320	1	0.05	14	190	4	-2	2	7	0.09	-10	-10	17	200	302	A9837222	
VR 74636 A	10	0.42	310	1	0.05	10	170	2	-2	2	10	0.08	-10	-10	15	-10	62	A9837222	
VR 74637 A	20	0.67	1195	1	0.03	22	360	154	-2	2	13	0.05	-10	-10	15	20	194	A9837222	
VR 74638 A	20	0.24	1815	-1	0.02	9	410	232	-2	1	9	-0.01	-10	-10	6	-10	134	A9837222	
VR 74639 A	-10	0.63	10000	-1	-0.01	4	40	3550	6	1	12	-0.01	-10	-10	2	-10	7140	A9837222	
VR 74640 A	10	0.33	1970	-1	0.03	9	200	504	-2	1	12	0.01	-10	-10	9	-10	406	A9837222	
VR 74641 A	10	0.41	400	-1	0.05	10	150	18	-2	2	10	0.08	-10	-10	15	-10	88	A9837222	
VR 74642 A	10	0.62	280	-1	0.03	14	390	8	-2	3	5	0.14	-10	-10	19	-10	92	A9837222	
VR 74643 A	10	0.96	250	1	0.05	14	400	10	-2	4	8	0.14	-10	-10	26	-10	56	A9837222	
VR 74644 A	10	0.51	200	1	0.06	10	200	2	-2	3	8	0.1	-10	-10	18	-10	44	A9837222	
VR 74645 A	10	0.4	340	-1	0.05	12	140	2	-2	2	9	0.08	-10	-10	15	10	130	A9837222	
VR 74646 A	10	0.72	280	1	0.03	16	320	6	-2	2	8	0.13	-10	-10	19	-10	56	A9837222	

FINDLAY CREEK PROJECT - 1998 Appendix IX

Drill Core Sample Results

SAMPLE	HOLE	FROM	TO	WIDTH	AU_PPB	AG_PPM	AL_PCT	AS_PPM	BA_PPM	BE_PPM	BI_PPM	CA_PCT	CD_PPM	CO_PPM	CR_PPM	CU_PPM	FE_PCT	GA_PPM	HG_PPM	K_PCT
VR 74647 A	F98-04	460.00	463.00	3.00		-0.2	0.82	2	70	0.5	2	0.41	-0.5	8	78	16	1.44	-10	-1	0.49
VR 74648 A	F98-04	463.00	466.00	3.00		-0.2	1.17	2	130	0.5	-2	0.31	-0.5	8	131	11	1.71	-10	-1	0.68
VR 74649 A	F98-04	466.00	469.00	3.00		-0.2	0.67	-2	50	-0.5	-2	0.31	-0.5	5	82	-1	1.05	-10	-1	0.36
VR 74650 A	F98-04	469.00	472.00	3.00		-0.2	1.27	-2	120	0.5	-2	0.27	-0.5	11	96	28	2.29	-10	-1	0.79
VR 74651 A	F98-04	472.00	475.00	3.00		-0.2	0.68	2	40	-0.5	-2	0.33	-0.5	5	75	-1	0.96	-10	-1	0.4
VR 74652 A	F98-04	475.00	478.00	3.00		-0.2	1.42	2	150	1.5	2	0.36	0.5	9	125	32	1.83	-10	-1	0.8
VR 74653 A	F98-04	478.00	481.00	3.00		-0.2	1.51	2	170	1.5	2	0.28	1	10	110	28	1.94	-10	-1	0.85
VR 74654 A	F98-04	481.00	484.00	3.00		-0.2	1.64	-2	140	-0.5	-2	0.2	-0.5	12	84	25	2.75	-10	-1	0.96
VR 74655 A	F98-04	484.00	486.00	2.00		-0.2	1.91	-2	140	-0.5	2	0.28	-0.5	16	68	49	3.77	-10	-1	1.14
VR 74656 A	F98-04	486.00	487.98	1.98		-0.2	0.81	-2	70	-0.5	-2	0.36	-0.5	7	57	13	1.62	-10	-1	0.45
VR 74451 A	F98-05	4.57	7.00	2.43		-0.2	0.8	6	70	-0.5	-2	0.44	-0.5	5	69	12	1.42	-10	-1	0.25
VR 74452 A	F98-05	7.10	10.00	2.90		-0.2	0.93	8	80	-0.5	-2	0.34	-0.5	6	55	8	1.68	-10	-1	0.26
VR 74453 A	F98-05	10.00	10.35	0.35		-0.2	0.88	8	60	-0.5	-2	0.07	-0.5	6	54	13	1.88	-10	-1	0.22
VR 74454 A	F98-05	10.35	13.00	2.65		-0.2	1.15	6	80	-0.5	-2	0.42	-0.5	11	26	29	2.74	-10	-1	0.34
VR 74455 A	F98-05	13.00	16.00	3.00		-0.2	1.07	26	70	-0.5	2	0.29	-0.5	11	22	29	2.6	-10	-1	0.33
VR 74456 A	F98-05	16.00	19.00	3.00		0.2	1.12	12	60	-0.5	-2	0.42	-0.5	11	29	25	2.77	-10	-1	0.28
VR 74457 A	F98-05	19.00	21.70	2.70		-0.2	1.26	6	80	-0.5	-2	0.37	-0.5	10	25	25	2.79	-10	-1	0.37
VR 74458 A	F98-05	21.70	23.06	1.36		-0.2	1.43	10	60	-0.5	-2	0.57	-0.5	8	40	22	2.29	-10	-1	0.26
VR 74459 A	F98-05	23.06	26.00	2.94		-0.2	0.96	12	70	-0.5	-2	0.83	-0.5	7	38	9	1.61	-10	-1	0.31
VR 74460 A	F98-05	26.00	29.00	3.00		-0.2	0.9	12	60	-0.5	-2	0.47	-0.5	7	34	12	1.74	-10	-1	0.27
VR 74461 A	F98-05	29.00	32.00	3.00		-0.2	0.88	10	70	-0.5	-2	0.9	-0.5	8	30	19	2.04	-10	-1	0.31
VR 74462 A	F98-05	32.00	33.18	1.18		-0.2	0.97	12	80	-0.5	-2	0.56	-0.5	10	27	21	1.93	-10	-1	0.36
VR 74463 A	F98-05	33.18	36.00	2.82		-0.2	0.72	6	80	-0.5	-2	0.96	-0.5	7	27	18	1.68	-10	-1	0.31
VR 74464 A	F98-05	36.00	38.16	2.16		-0.2	0.86	12	80	-0.5	-2	1.02	-0.5	8	21	15	1.77	-10	-1	0.31
VR 74465 A	F98-05	38.16	38.25	0.09		-0.2	0.98	16	70	-0.5	-2	0.65	0.5	9	35	17	2.21	-10	-1	0.3
VR 74466 A	F98-05	38.25	41.00	2.75		0.2	0.88	10	80	-0.5	-2	0.57	2	8	24	19	1.81	-10	-1	0.31
VR 74467 A	F98-05	41.00	42.50	1.50		-0.2	0.58	10	70	-0.5	-2	0.82	-0.5	7	27	15	1.78	-10	-1	0.29
VR 74468 A	F98-05	42.50	44.50	2.00		-0.2	1.05	16	100	-0.5	-2	0.51	1	14	19	38	2.7	-10	-1	0.45
VR 74469 A	F98-05	44.50	46.28	1.78		-0.2	0.6	10	80	-0.5	-2	0.59	-0.5	5	61	9	1.48	-10	-1	0.31
VR 74470 A	F98-05	46.28	48.77	2.49		-0.2	0.98	10	80	-0.5	-2	0.41	-0.5	8	25	22	2.11	-10	-1	0.35
VR 74471 A	F98-05	48.77	51.00	2.23		-0.2	0.56	4	80	-0.5	-2	0.95	-0.5	5	35	9	1.33	-10	-1	0.26
VR 74472 A	F98-05	51.00	53.00	2.00		-0.2	0.73	12	60	-0.5	-2	0.87	-0.5	6	24	16	1.53	-10	-1	0.23
VR 74473 A	F98-05	53.00	54.80	1.80		-0.2	1	34	70	-0.5	-2	1.24	-0.5	8	30	23	2.25	-10	-1	0.31
VR 74474 A	F98-05	54.80	55.50	0.70		-0.2	0.8	10	60	-0.5	-2	0.66	0.5	7	40	20	1.8	-10	-1	0.24
VR 74475 A	F98-05	55.50	57.75	2.25		0.4	0.78	164	70	-0.5	-2	0.94	0.5	17	17	44	2.76	-10	-1	0.34
VR 74476 A	F98-05	57.75	60.60	2.85		-0.2	0.49	20	70	-0.5	-2	0.53	-0.5	5	37	12	1.29	-10	-1	0.26
VR 74477 A	F98-05	60.60	63.00	2.40		-0.2	0.42	8	70	-0.5	-2	0.89	-0.5	4	41	8	0.92	-10	-1	0.22
VR 74478 A	F98-05	63.00	66.00	3.00		-0.2	0.66	8	90	-0.5	-2	0.34	-0.5	7	38	13	1.66	-10	-1	0.35
VR 74479 A	F98-05	66.00	69.25	3.25		-0.2	0.61	18	90	-0.5	-2	0.45	-0.5	5	51	14	1.34	-10	-1	0.33
VR 74480 A	F98-05	69.25	71.00	1.75		-0.2	1.17	34	90	-0.5	-2	0.68	-0.5	14	22	35	2.74	-10	-1	0.42
VR 74481 A	F98-05	71.00	72.85	1.85		-0.2	0.5	2	60	-0.5	-2	0.62	-0.5	4	50	7	1.11	-10	-1	0.21
VR 74482 A	F98-05	72.85	73.40	0.55		-0.2	1.25	-2	90	-0.5	-2	0.13	-0.5	14	21	35	2.85	-10	-1	0.43

Appendix IX

FINDLAY CREEK PROJECT - 1998
Drill Core Sample Results

SAMPLE	LA_PPM	MG_PCT	MN_PPM	MO_PPM	NA_PCT	NI_PPM	P_PPM	PB_PPM	SB_PPM	SC_PPM	SR_PPM	TI_PCT	TL_PPM	U_PPM	V_PPM	W_PPM	ZN_PPM	CERTIF	ALT_CERTIF
VR 74647 A	10	0.35	505	-1	0.02	11	140	6	-2	1	8	0.08	-10	-10	13	-10	104	A9837363	
VR 74648 A	10	0.39	345	1	0.05	13	140	-2	-2	2	8	0.09	-10	-10	17	-10	148	A9837363	
VR 74649 A	-10	0.28	140	-1	0.02	8	140	-2	-2	1	5	0.08	-10	-10	14	-10	20	A9837363	
VR 74650 A	10	0.53	305	1	0.01	15	200	-2	-2	1	5	0.1	-10	-10	15	20	54	A9837363	
VR 74651 A	-10	0.39	195	-1	0.03	10	140	6	-2	2	7	0.06	-10	-10	18	-10	32	A9837363	
VR 74652 A	10	0.42	395	-1	0.04	14	180	-2	-2	2	8	0.08	-10	-10	17	40	224	A9837363	
VR 74653 A	20	0.37	315	1	0.04	14	170	-2	-2	2	7	0.05	-10	-10	13	240	314	A9837363	
VR 74654 A	10	0.57	270	1	0.01	17	250	2	-2	2	4	0.11	-10	-10	18	-10	54	A9837363	
VR 74655 A	20	0.73	345	2	0.01	23	370	-2	-2	2	6	0.13	-10	-10	19	-10	54	A9837363	
VR 74656 A	10	0.33	320	-1	0.01	11	130	-2	-2	1	7	0.06	-10	-10	14	-10	32	A9837363	
VR 74451 A	30	0.23	205	-1	0.04	8	110	8	-2	1	28	-0.01	-10	-10	5	-10	26	A9835790	
VR 74452 A	40	0.25	225	-1	0.04	10	150	4	-2	1	28	-0.01	-10	-10	6	-10	36	A9835790	
VR 74453 A	20	0.25	185	-1	0.04	11	140	6	-2	-1	7	-0.01	-10	-10	5	-10	46	A9835790	
VR 74454 A	10	0.48	290	5	0.01	20	290	68	-2	1	25	-0.01	-10	-10	5	-10	104	A9835790	
VR 74455 A	10	0.49	230	2	0.01	18	210	30	-2	-1	19	-0.01	-10	-10	4	-10	56	A9835790	
VR 74456 A	10	0.5	265	1	0.01	16	180	38	-2	-1	26	-0.01	-10	-10	5	-10	56	A9835790	
VR 74457 A	10	0.47	285	1	0.01	17	240	6	-2	1	24	-0.01	-10	-10	6	-10	48	A9835790	
VR 74458 A	10	0.66	245	1	-0.01	15	200	6	-2	-1	35	-0.01	-10	-10	4	-10	38	A9835790	
VR 74459 A	30	0.48	305	-1	0.01	12	170	16	-2	1	45	-0.01	-10	-10	4	-10	30	A9835790	
VR 74460 A	20	0.41	225	-1	0.02	12	140	6	-2	-1	26	-0.01	-10	-10	5	-10	28	A9835790	
VR 74461 A	10	0.44	345	-1	0.01	16	160	12	-2	1	48	-0.01	-10	-10	4	-10	58	A9835790	
VR 74462 A	20	0.38	285	-1	0.01	17	180	4	-2	1	30	-0.01	-10	-10	4	-10	46	A9835790	
VR 74463 A	20	0.3	420	1	0.02	13	150	10	-2	1	57	0.01	-10	-10	4	-10	48	A9835790	
VR 74464 A	20	0.35	425	-1	0.01	13	180	16	-2	1	61	0.01	-10	-10	4	-10	64	A9835790	
VR 74465 A	10	0.48	335	-1	0.01	14	190	34	-2	-1	39	-0.01	-10	-10	4	-10	146	A9835790	
VR 74466 A	20	0.36	295	1	0.02	13	160	214	-2	1	32	-0.01	-10	-10	5	-10	592	A9835790	
VR 74467 A	20	0.34	360	2	0.02	13	170	18	-2	-1	40	-0.01	-10	-10	3	-10	74	A9835790	
VR 74468 A	10	0.43	280	4	0.01	26	330	14	-2	1	33	-0.01	-10	-10	5	-10	144	A9835790	
VR 74469 A	20	0.26	315	-1	0.03	9	190	20	-2	1	36	-0.01	-10	-10	3	-10	44	A9835790	
VR 74470 A	20	0.32	265	1	0.01	16	220	8	-2	1	28	-0.01	-10	-10	3	-10	52	A9835790	
VR 74471 A	30	0.32	450	1	0.03	8	140	102	-2	-1	56	0.01	-10	-10	3	-10	40	A9835790	
VR 74472 A	10	0.38	310	-1	0.02	12	180	-2	-2	-1	49	-0.01	-10	-10	3	-10	28	A9835790	
VR 74473 A	10	0.73	320	3	0.02	16	260	10	-2	1	64	-0.01	-10	-10	5	-10	32	A9835790	
VR 74474 A	10	0.39	285	3	0.01	14	190	14	-2	-1	41	-0.01	-10	-10	2	-10	170	A9835790	
VR 74475 A	-10	0.46	415	10	-0.01	28	430	68	-2	-1	57	-0.01	-10	-10	3	-10	140	A9835790	
VR 74476 A	10	0.2	270	-1	0.01	8	150	10	-2	-1	28	-0.01	-10	-10	1	-10	30	A9835790	
VR 74477 A	20	0.15	375	-1	0.03	6	120	14	-2	-1	49	0.01	-10	-10	2	-10	26	A9835790	
VR 74478 A	20	0.25	260	-1	0.03	11	170	16	-2	1	22	-0.01	-10	-10	3	-10	40	A9835790	
VR 74479 A	30	0.19	255	-1	0.03	9	150	14	-2	-1	25	-0.01	-10	-10	3	-10	20	A9835790	
VR 74480 A	10	0.54	325	10	0.01	27	460	22	-2	1	40	-0.01	-10	-10	5	-10	48	A9835790	
VR 74481 A	20	0.24	250	-1	0.03	5	120	12	-2	-1	30	-0.01	-10	-10	3	-10	18	A9835790	
VR 74482 A	10	0.4	160	4	-0.01	23	310	-2	-2	1	11	-0.01	-10	-10	6	-10	56	A9835790	

FINDLAY CREEK PROJECT - 1998
Drill Core Sample Results

SAMPLE			HOLE	FROM	TO	WIDTH	AU_PPB	AG_PPM	AL_PCT	AS_PPM	BA_PPM	BE_PPM	BI_PPM	CA_PCT	CD_PPM	CO_PPM	CR_PPM	CU_PPM	FE_PCT	GA_PPM	HG_PPM	K_PCT
VR	74483	A	F98-05	73.40	76.00	2.60		-0.2	0.57	24	80	-0.5	-2	0.65	-0.5	6	50	8	1.08	-10	-1	0.29
VR	74484	A	F98-05	76.00	79.00	3.00		-0.2	0.62	8	60	-0.5	-2	0.78	-0.5	6	37	10	1.28	-10	-1	0.26
VR	74485	A	F98-05	79.00	82.00	3.00		-0.2	0.5	10	70	-0.5	-2	1.31	-0.5	5	46	9	1.34	-10	-1	0.26
VR	74486	A	F98-05	82.00	83.50	1.50		-0.2	0.49	2	70	-0.5	-2	0.58	-0.5	11	36	31	2.66	-10	-1	0.33
VR	74487	A	F98-05	83.50	86.75	3.25		-0.2	0.77	4	70	-0.5	-2	0.56	-0.5	7	27	18	1.88	-10	-1	0.28
VR	74488	A	F98-05	86.75	88.25	1.50		-0.2	1.24	2	100	-0.5	-2	0.27	-0.5	17	21	39	3.29	-10	-1	0.44
VR	74489	A	F98-05	88.25	91.00	2.75		-0.2	0.82	4	60	-0.5	-2	0.47	-0.5	5	50	9	1.47	-10	-1	0.23
VR	74490	A	F98-05	91.00	94.00	3.00		-0.2	1.07	14	90	-0.5	-2	0.29	-0.5	7	45	11	1.74	-10	-1	0.34
VR	74491	A	F98-05	94.00	97.00	3.00		-0.2	0.81	8	70	-0.5	-2	0.79	-0.5	5	43	10	1.74	-10	-1	0.28
VR	74492	A	F98-05	97.00	98.10	1.10		-0.2	0.92	12	80	-0.5	-2	0.14	-0.5	9	40	18	2.09	-10	-1	0.36
VR	74493	A	F98-05	98.10	100.00	1.90		-0.2	1.78	26	60	-0.5	-2	0.49	-0.5	8	54	18	2.6	-10	-1	0.26
VR	74494	A	F98-05	100.00	103.00	3.00		0.2	1.15	66	30	-0.5	-2	1.78	-0.5	9	39	59	2.9	-10	-1	0.15
VR	74495	A	F98-05	103.00	105.94	2.94		0.2	1.46	64	50	-0.5	-2	1.01	3	14	45	41	3.16	-10	-1	0.27
VR	74496	A	F98-05	138.68	140.40	1.72		0.4	1.06	18	80	-0.5	-2	0.75	-0.5	13	29	71	2.9	-10	-1	0.35
VR	74497	A	F98-05	140.40	143.00	2.60		0.2	1.16	40	90	-0.5	-2	0.98	-0.5	11	94	21	2.34	-10	-1	0.41
VR	74498	A	F98-05	143.00	146.00	3.00		-0.2	0.86	22	80	-0.5	-2	0.63	-0.5	8	43	22	2.07	-10	-1	0.35
VR	74499	A	F98-05	146.00	149.00	3.00		-0.2	0.56	54	60	-0.5	-2	0.6	-0.5	9	44	23	1.85	-10	-1	0.28
VR	74500	A	F98-05	149.00	152.00	3.00		-0.2	0.82	96	50	-0.5	-2	0.59	-0.5	10	32	64	2.42	-10	-1	0.27
VR	74501	A	F98-05	152.00	152.65	0.65		0.4	0.55	312	90	-0.5	-2	2.45	1	14	21	89	2.94	-10	-1	0.34
VR	74502	A	F98-05	152.65	153.00	0.35		0.8	0.69	304	80	0.5	-2	2.32	-0.5	9	41	25	2.46	-10	-1	0.39
VR	74503	A	F98-05	153.00	153.50	0.50		0.2	0.72	180	70	0.5	-2	3.01	-0.5	9	36	21	2.69	-10	-1	0.32
VR	74504	A	F98-05	153.50	156.00	2.50		0.2	0.67	4	70	0.5	-2	2.84	-0.5	12	26	37	3.16	-10	-1	0.32
VR	74505	A	F98-05	156.00	158.50	2.50		0.6	0.63	8	60	-0.5	-2	1.77	-0.5	16	26	43	3.13	-10	-1	0.29
VR	74506	A	F98-05	158.50	161.00	2.50		0.2	0.89	40	60	-0.5	-2	0.82	-0.5	12	48	29	2.47	-10	-1	0.28
VR	74507	A	F98-05	161.00	164.00	3.00		-0.2	1.11	22	60	-0.5	-2	1.08	-0.5	8	41	27	2.26	-10	-1	0.24
VR	74508	A	F98-05	164.00	167.00	3.00		-0.2	1.09	84	70	-0.5	-2	0.64	-0.5	9	56	51	2.28	-10	-1	0.32
VR	74509	A	F98-05	167.00	170.00	3.00		-0.2	0.68	98	60	-0.5	-2	0.72	-0.5	8	67	44	1.75	-10	-1	0.27
VR	74510	A	F98-05	170.00	171.80	1.80		-0.2	0.86	186	90	-0.5	-2	0.26	-0.5	10	81	36	2.03	-10	-1	0.35
VR	74511	A	F98-05	171.80	173.00	1.20		0.6	0.93	364	60	0.5	-2	0.36	-0.5	9	38	78	2.31	-10	-1	0.25
VR	74512	A	F98-05	173.00	176.00	3.00		6.8	0.7	766	70	-0.5	2	1.2	3.5	10	73	243	2.04	-10	-1	0.26
VR	74513	A	F98-05	176.00	176.48	0.48		14.4	0.48	2870	60	-0.5	10	2.12	5.5	12	60	275	2.49	-10	-1	0.2
VR	74514	A	F98-05	176.48	179.00	2.52		7.8	0.56	1325	80	-0.5	6	0.7	5	12	66	140	2.3	-10	-1	0.25
VR	74515	A	F98-05	179.00	182.00	3.00		5.2	0.65	1965	80	-0.5	-2	0.65	2	13	50	234	2.34	-10	-1	0.28
VR	74516	A	F98-05	182.00	185.00	3.00		0.6	0.81	652	90	-0.5	-2	0.45	-0.5	8	60	79	1.81	-10	-1	0.31
VR	74517	A	F98-05	185.00	188.00	3.00		0.6	0.73	252	90	-0.5	-2	0.51	-0.5	9	53	68	1.98	-10	-1	0.34
VR	74518	A	F98-05	188.00	191.00	3.00		0.8	0.8	324	90	-0.5	-2	0.58	0.5	9	54	86	2.07	-10	-1	0.33
VR	74519	A	F98-05	191.00	193.00	2.00		1.2	0.79	520	120	-0.5	-2	0.41	0.5	12	69	223	2.9	-10	-1	0.41
VR	74520	A	F98-05	193.00	193.17	0.17		32.6	0.25	2580	50	-0.5	60	1.68	15.5	28	98	1065	3.83	-10	-1	0.15
VR	74521	A	F98-05	193.17	194.00	0.83		-0.2	0.51	258	70	-0.5	-2	1.15	-0.5	6	84	59	1.55	-10	-1	0.24
VR	74522	A	F98-05	194.00	194.20	0.20		0.6	1.03	836	100	-0.5	-2	0.47	1	11	69	143	2.9	-10	-1	0.33
VR	74523	A	F98-05	194.20	195.26	1.06		-0.2	0.65	12	90	-0.5	-2	0.91	-0.5	4	73	42	1.78	-10	-1	0.32
VR	74524	A	F98-05	195.26	195.36	0.10		0.6	0.79	8220	120	-0.5	-2	0.57	-0.5	44	46	304	3.27	-10	-1	0.41

SAMPLE			LA_PPM	MG_PCT	MN_PPM	MO_PPM	NA_PCT	NI_PPM	P_PPM	PB_PPM	SB_PPM	SC_PPM	SR_PPM	TI_PCT	TL_PPM	U_PPM	V_PPM	W_PPM	ZN_PPM	CERTIF	ALT_CERTIF
VR	74483	A	10	0.21	295	1	0.03	7	110	16	-2	-1	43	0.01	-10	-10	4	-10	66	A9835790	
VR	74484	A	10	0.25	275	1	0.02	9	140	10	-2	-1	49	-0.01	-10	-10	3	-10	30	A9835790	
VR	74485	A	10	0.29	400	-1	0.03	8	120	24	-2	-1	73	-0.01	-10	-10	3	-10	32	A9835790	
VR	74486	A	10	0.39	430	10	0.01	20	370	30	2	-1	36	-0.01	-10	-10	3	-10	36	A9835790	
VR	74487	A	10	0.37	305	2	0.02	11	140	2	-2	-1	30	-0.01	-10	-10	4	-10	34	A9835790	
VR	74488	A	10	0.47	220	10	0.01	27	420	16	-2	1	20	-0.01	-10	-10	6	-10	40	A9835790	
VR	74489	A	10	0.47	215	1	0.03	7	130	14	-2	-1	27	-0.01	-10	-10	4	-10	24	A9835790	
VR	74490	A	20	0.47	140	-1	0.02	11	160	2	4	1	17	-0.01	-10	-10	5	-10	22	A9835790	
VR	74491	A	20	0.56	320	1	0.03	8	140	16	-2	1	40	-0.01	-10	-10	4	-10	24	A9835790	
VR	74492	A	20	0.45	180	1	0.01	14	190	2	-2	1	11	-0.01	-10	-10	4	-10	30	A9835790	
VR	74493	A	10	1.29	240	2	0.01	14	280	68	2	1	29	-0.01	-10	-10	7	-10	70	A9835790	
VR	74494	A	-10	1.45	705	3	0.02	19	270	106	-2	2	75	-0.01	-10	-10	7	-10	90	A9836422	
VR	74495	A	10	1.07	510	4	0.01	28	400	198	-2	1	55	-0.01	-10	-10	8	-10	908	A9836422	
VR	74496	A	10	0.62	360	4	0.01	27	510	140	-2	1	61	-0.01	-10	-10	7	-10	50	A9836422	
VR	74497	A	30	0.73	505	1	0.02	30	390	60	-2	3	85	0.01	-10	-10	14	-10	60	A9836422	
VR	74498	A	20	0.3	370	1	0.01	13	160	16	-2	1	43	0.01	-10	-10	5	-10	42	A9836422	
VR	74499	A	20	0.28	410	1	0.02	13	150	14	-2	-1	37	-0.01	-10	-10	3	-10	30	A9836422	
VR	74500	A	10	0.46	330	2	0.01	19	250	94	-2	1	35	-0.01	-10	-10	5	-10	44	A9836422	
VR	74501	A	10	0.94	730	1	0.01	24	480	382	-2	2	98	-0.01	-10	-10	5	-10	156	A9836422	
VR	74502	A	20	0.85	835	6	0.01	15	280	670	-2	3	101	-0.01	-10	-10	5	-10	62	A9836422	
VR	74503	A	20	1.04	920	1	0.01	17	380	142	-2	3	134	-0.01	-10	-10	6	-10	62	A9836422	
VR	74504	A	10	1.26	820	4	0.02	24	450	150	-2	3	123	-0.01	-10	-10	7	-10	80	A9836422	
VR	74505	A	10	1.09	555	5	0.02	25	410	214	-2	2	88	-0.01	-10	-10	7	-10	82	A9836422	
VR	74506	A	20	0.42	400	1	0.01	16	200	294	-2	1	48	-0.01	-10	-10	5	-10	82	A9836422	
VR	74507	A	20	0.42	415	1	-0.01	16	220	60	-2	1	60	-0.01	-10	-10	5	-10	46	A9836422	
VR	74508	A	20	0.37	370	1	0.01	17	220	26	-2	1	39	-0.01	-10	-10	6	-10	48	A9836422	
VR	74509	A	10	0.22	355	1	0.01	13	180	22	-2	-1	39	-0.01	-10	-10	4	-10	28	A9836422	
VR	74510	A	30	0.24	330	-1	0.01	16	240	16	-2	1	30	-0.01	-10	-10	5	-10	40	A9836422	
VR	74511	A	30	0.26	325	-1	-0.01	13	210	516	-2	1	55	-0.01	-10	-10	5	-10	38	A9836422	
VR	74512	A	20	0.22	440	1	-0.01	18	220	5590	2	1	63	-0.01	-10	-10	4	-10	30	A9836422	
VR	74513	A	10	0.13	430	1	-0.01	21	180	17700	6	1	83	-0.01	-10	-10	4	-10	12	A9836422	A9836931
VR	74514	A	20	0.2	360	3	0.01	14	250	7180	2	1	32	-0.01	-10	-10	4	-10	38	A9836422	
VR	74515	A	20	0.28	425	1	-0.01	17	250	4540	2	1	27	-0.01	-10	-10	4	-10	92	A9836422	
VR	74516	A	30	0.26	330	-1	0.01	12	200	546	-2	1	24	-0.01	-10	-10	6	-10	32	A9836422	
VR	74517	A	30	0.28	375	1	0.01	14	200	538	-2	1	27	-0.01	-10	-10	5	-10	30	A9836422	
VR	74518	A	30	0.32	395	-1	0.01	14	200	708	-2	1	26	-0.01	-10	-10	6	-10	34	A9836422	
VR	74519	A	30	0.33	370	1	-0.01	24	290	794	-2	1	21	-0.01	-10	-10	6	-10	38	A9836422	
VR	74520	A	10	0.06	555	5	-0.01	26	440	18800	2	-1	42	-0.01	-10	-10	3	-10	30	A9836422	A9836931
VR	74521	A	30	0.24	415	1	0.01	10	150	102	-2	1	38	-0.01	-10	-10	4	-10	26	A9836422	
VR	74522	A	10	0.4	360	-1	-0.01	17	220	324	-2	1	19	-0.01	-10	-10	5	-10	68	A9836422	
VR	74523	A	30	0.3	445	1	0.02	12	170	84	-2	1	35	-0.01	-10	-10	5	-10	36	A9836422	
VR	74524	A	10	0.26	365	1	-0.01	38	270	288	2	1	23	-0.01	-10	-10	5	-10	78	A9836422	

FINDLAY CREEK PROJECT - 1998
Drill Core Sample Results

Appendix IX

SAMPLE			HOLE	FROM	TO	WIDTH	AU_PPB	AG_PPM	AL_PCT	AS_PPM	BA_PPM	BE_PPM	BI_PPM	CA_PCT	CD_PPM	CO_PPM	CR_PPM	CU_PPM	FE_PCT	GA_PPM	HG_PPM	K_PCT
VR	74525	A	F98-05	195.36	195.75	0.39		-0.2	0.58	202	70	-0.5	-2	0.55	-0.5	4	85	26	1.31	-10	-1	0.25
VR	74526	A	F98-05	195.75	196.00	0.25		5.8	1.07	400	110	-0.5	10	0.4	3	12	42	379	3.95	-10	-1	0.36
VR	74527	A	F98-05	196.00	196.75	0.75		0.2	0.89	422	100	-0.5	-2	0.54	-0.5	7	71	99	2.16	-10	-1	0.34
VR	74528	A	F98-05	196.75	196.85	0.10		2.4	1.05	1220	120	-0.5	-2	0.3	3	27	41	448	3.53	-10	-1	0.43
VR	74529	A	F98-05	196.85	198.80	1.95		0.4	0.72	118	100	-0.5	-2	0.62	-0.5	10	48	33	1.69	-10	-1	0.28
VR	74530	A	F98-05	198.80	198.90	0.10		9	0.68	5420	100	-0.5	14	0.95	3	23	57	291	2.45	-10	-1	0.32
VR	74531	A	F98-05	198.90	199.98	1.08		0.8	1.01	588	110	-0.5	-2	0.61	0.5	17	56	222	2.71	-10	-1	0.39
VR	74532	A	F98-05	199.98	200.15	0.17		62.2	0.19	1035	30	-0.5	118	0.31	23.5	8	119	592	7.12	-10	-1	0.07
VR	74533	A	F98-05	200.15	201.20	1.05		0.8	0.85	1590	120	-0.5	-2	0.61	-0.5	15	38	200	2.44	-10	-1	0.35
VR	74534	A	F98-05	201.20	202.35	1.15		3.8	0.58	1040	80	-0.5	6	0.43	1.5	15	86	360	2.69	-10	-1	0.24
VR	74535	A	F98-05	202.35	202.80	0.45		-0.2	0.55	68	60	-0.5	-2	1.86	-0.5	5	73	79	1.75	-10	-1	0.21
VR	74536	A	F98-05	202.80	202.88	0.08		16	0.41	16	30	-0.5	22	0.26	10	8	146	1530	10.1	-10	-1	0.29
VR	74537	A	F98-05	202.88	204.35	1.47		-0.2	0.51	120	70	-0.5	-2	0.55	-0.5	7	82	37	1.79	-10	-1	0.23
VR	74538	A	F98-05	204.35	204.55	0.20		7.4	0.38	732	50	-0.5	16	1.49	3.5	10	92	1165	5.29	-10	-1	0.15
VR	74539	A	F98-05	204.55	204.80	0.25		0.4	0.68	344	120	-0.5	-2	0.32	-0.5	5	77	202	2.01	-10	-1	0.35
VR	74540	A	F98-05	204.80	204.95	0.15		4.4	0.45	42	80	-0.5	10	0.8	2	4	92	619	4.87	-10	-1	0.33
VR	74541	A	F98-05	204.95	205.50	0.55		-0.2	0.68	44	80	-0.5	-2	0.59	-0.5	6	70	41	1.49	-10	-1	0.24
VR	74542	A	F98-05	205.50	206.05	0.55		1.4	0.89	666	110	-0.5	-2	0.56	1	13	70	300	2.93	-10	-1	0.39
VR	74543	A	F98-05	206.05	207.75	1.70		0.6	0.92	128	100	-0.5	-2	0.46	-0.5	6	44	83	2.22	-10	-1	0.38
VR	74544	A	F98-05	207.75	208.08	0.33		29.6	0.79	798	80	-0.5	54	1.8	11	15	82	372	4.62	-10	-1	0.27
VR	74545	A	F98-05	208.08	209.20	1.12		-0.2	0.77	102	80	-0.5	-2	0.83	-0.5	6	50	42	1.54	-10	-1	0.28
VR	74546	A	F98-05	209.20	209.30	0.10		14.4	0.82	3240	140	-0.5	30	0.85	5	19	81	205	2.64	-10	-1	0.41
VR	74547	A	F98-05	209.30	210.10	0.80		-0.2	0.85	140	90	-0.5	-2	0.6	-0.5	5	79	59	1.82	-10	-1	0.28
VR	74548	A	F98-05	210.10	210.30	0.20		5.8	1	750	110	-0.5	8	0.39	3	10	101	372	3.69	-10	-1	0.33
VR	74549	A	F98-05	210.30	210.80	0.50		0.8	0.53	382	70	-0.5	-2	1.5	-0.5	7	67	58	1.33	-10	-1	0.21
VR	74550	A	F98-05	210.80	211.00	0.20		7.4	0.65	634	60	-0.5	2	1.43	5.5	10	83	365	2.15	-10	-1	0.21
VR	74551	A	F98-05	211.00	212.97	1.97		0.2	0.8	428	100	-0.5	-2	0.69	-0.5	11	63	113	2.47	-10	-1	0.34
VR	74552	A	F98-05	212.97	213.30	0.33		57	0.49	2290	100	-0.5	116	0.57	21	21	86	2020	2.94	-10	-1	0.28
VR	74553	A	F98-05	213.30	215.03	1.73		-0.2	0.96	824	100	-0.5	-2	0.82	-0.5	13	59	102	2.26	-10	-1	0.32
VR	74554	A	F98-05	215.03	215.35	0.32		41.8	0.74	1150	100	-0.5	102	0.67	11.5	11	79	116	2.04	-10	-1	0.28
VR	74555	A	F98-05	215.35	216.16	0.81		1.8	0.8	1120	80	-0.5	2	0.87	0.5	24	50	211	2.56	-10	-1	0.27
VR	74556	A	F98-05	216.16	216.25	0.09		264	0.19	66	30	-0.5	708	1.25	101	6	107	2640	6.25	-10	-1	0.08
VR	74557	A	F98-05	216.25	217.00	0.75		1.6	0.78	514	90	-0.5	2	1.31	0.5	8	56	51	2.38	-10	-1	0.27
VR	74558	A	F98-05	217.00	219.35	2.35		10.4	0.32	2460	60	-0.5	24	2.74	0.5	16	59	145	2.42	-10	-1	0.15
VR	74559	A	F98-05	219.35	220.00	0.65		1.6	3.57	62	40	-0.5	6	2.34	-0.5	37	75	159	6.47	10	-1	0.39
VR	74560	A	F98-05	229.00	230.04	1.04		0.2	3.72	32	10	-0.5	-2	2.63	0.5	33	80	153	6.66	-10	-1	0.14
VR	74561	A	F98-05	230.04	231.34	1.30		7.6	0.78	2250	70	-0.5	20	0.63	0.5	25	43	411	4.85	-10	-1	0.21
VR	74562	A	F98-05	231.34	232.50	1.16		6	0.33	1035	60	-0.5	12	0.68	0.5	10	49	172	2.06	-10	-1	0.21
VR	74563	A	F98-05	232.50	233.50	1.00		3	0.56	490	60	-0.5	6	0.99	1	9	47	190	2.66	-10	-1	0.23
VR	74564	A	F98-05	233.50	236.00	2.50		1	0.61	468	60	-0.5	2	0.68	0.5	7	55	101	1.72	-10	-1	0.2
VR	74565	A	F98-05	236.00	239.00	3.00		1	0.57	54	60	-0.5	4	1.06	-0.5	4	62	55	1.48	-10	-1	0.18
VR	74566	A	F98-05	239.00	240.70	1.70		0.2	0.81	46	80	-0.5	-2	0.57	-0.5	6	56	44	1.6	-10	-1	0.32

FINDLAY CREEK PROJECT - 1998 Appendix IX

Drill Core Sample Results

SAMPLE			LA_PPM	MG_PCT	MN_PPM	MO_PPM	NA_PCT	NI_PPM	P_PPM	PB_PPM	SB_PPM	SC_PPM	SR_PPM	TI_PCT	TL_PPM	U_PPM	V_PPM	W_PPM	ZN_PPM	CERTIF	ALT_CERTIF
VR	74525	A	30	0.21	285	1	0.03	8	120	28	-2	1	23	-0.01	-10	-10	5	-10	26	A9836422	
VR	74526	A	10	0.39	400	5	-0.01	37	360	3720	-2	1	17	-0.01	-10	-10	7	-10	74	A9836422	
VR	74527	A	30	0.35	355	-1	0.01	15	180	266	-2	1	26	-0.01	-10	-10	6	-10	44	A9836422	
VR	74528	A	10	0.33	260	-1	-0.01	38	290	1860	-2	1	13	-0.01	-10	-10	7	-10	70	A9836422	
VR	74529	A	30	0.3	340	-1	0.01	12	170	286	-2	1	29	0.01	-10	-10	6	-10	32	A9836422	
VR	74530	A	10	0.15	290	1	-0.01	22	280	5940	6	1	39	-0.01	-10	-10	4	-10	18	A9836422	
VR	74531	A	20	0.38	345	2	-0.01	27	320	444	-2	1	31	-0.01	-10	-10	7	-10	42	A9836422	
VR	74532	A	10	0.07	265	6	-0.01	63	200	37500	6	-1	10	-0.01	-10	-10	2	-10	4	A9836422	A9836931
VR	74533	A	20	0.28	325	4	-0.01	22	410	410	-2	1	19	-0.01	-10	-10	5	-10	26	A9836422	
VR	74534	A	10	0.18	260	3	-0.01	23	330	2170	-2	-1	17	-0.01	-10	-10	5	-10	26	A9836422	
VR	74535	A	20	0.26	595	1	0.01	12	190	92	-2	-1	59	-0.01	-10	-10	4	-10	28	A9836422	
VR	74536	A	-10	0.12	415	1	-0.01	135	320	12000	-2	-1	7	-0.01	-10	-10	5	-10	36	A9836422	A9836931
VR	74537	A	40	0.23	320	-1	0.01	11	180	44	-2	1	32	-0.01	-10	-10	4	-10	28	A9836422	
VR	74538	A	10	0.29	550	-1	-0.01	38	460	4090	-2	1	57	-0.01	-10	-10	3	-10	42	A9836422	
VR	74539	A	20	0.14	215	1	-0.01	15	270	186	-2	1	21	-0.01	-10	-10	4	-10	16	A9836422	
VR	74540	A	-10	0.15	335	1	-0.01	39	300	1725	4	-1	28	-0.01	-10	-10	4	-10	28	A9836422	
VR	74541	A	30	0.2	270	-1	0.02	9	190	28	-2	1	26	0.01	-10	-10	5	-10	24	A9836422	
VR	74542	A	10	0.3	460	-1	-0.01	22	260	1330	-2	1	23	-0.01	-10	-10	6	-10	34	A9836422	
VR	74543	A	30	0.33	395	-1	0.01	14	220	458	-2	1	21	0.01	-10	-10	7	-10	36	A9836422	
VR	74544	A	20	0.3	610	-1	-0.01	38	230	22200	4	1	62	-0.01	-10	-10	4	-10	32	A9836422	A9836931
VR	74545	A	30	0.23	310	1	0.01	10	160	82	-2	1	30	0.01	-10	-10	7	-10	26	A9836422	
VR	74546	A	20	0.16	285	1	-0.01	30	360	7460	-2	1	31	-0.01	-10	-10	5	-10	14	A9836422	
VR	74547	A	40	0.25	265	-1	0.01	11	190	196	-2	1	29	0.01	-10	-10	7	-10	26	A9836422	
VR	74548	A	30	0.3	285	-1	-0.01	25	220	4440	-2	1	18	-0.01	-10	-10	6	-10	34	A9836422	
VR	74549	A	40	0.15	400	1	0.03	8	150	654	-2	1	47	-0.01	-10	-10	4	-10	14	A9836422	
VR	74550	A	30	0.26	405	1	0.01	14	150	7380	2	1	44	-0.01	-10	-10	4	-10	34	A9836422	
VR	74551	A	30	0.34	405	-1	0.01	18	270	190	-2	1	33	-0.01	-10	-10	6	-10	38	A9836422	
VR	74552	A	20	0.1	270	-1	-0.01	23	270	24200	2	1	18	-0.01	-10	-10	4	-10	40	A9836422	A9836931
VR	74553	A	30	0.36	415	1	0.01	16	220	122	-2	1	30	-0.01	-10	-10	6	-10	36	A9836422	
VR	74554	A	10	0.26	315	1	-0.01	16	290	16200	-2	1	20	-0.01	-10	-10	4	-10	30	A9836422	A9836931
VR	74555	A	10	0.37	405	3	-0.01	20	300	626	-2	1	32	-0.01	-10	-10	5	-10	38	A9836422	
VR	74556	A	-10	0.12	375	1	-0.01	63	150	129500	10	-1	34	-0.01	-10	-10	2	-10	68	A9836422	A9836931
VR	74557	A	30	0.45	485	3	-0.01	13	260	590	-2	1	50	-0.01	-10	-10	5	-10	52	A9836422	
VR	74558	A	10	0.32	975	1	0.01	22	410	3430	-2	2	112	-0.01	-10	-10	5	-10	30	A9836422	
VR	74559	A	-10	2.28	910	-1	-0.01	46	720	374	-2	9	50	0.41	-10	-10	146	-10	96	A9836422	
VR	74560	A	-10	2.27	1020	1	-0.01	46	720	70	-2	10	38	0.29	-10	-10	134	-10	102	A9836577	
VR	74561	A	10	0.54	365	-1	-0.01	27	350	2590	6	3	21	-0.01	-10	-10	17	-10	70	A9836577	
VR	74562	A	10	0.26	400	-1	0.01	12	160	2200	2	1	20	-0.01	-10	-10	1	-10	112	A9836577	
VR	74563	A	10	0.35	420	3	0.01	16	310	938	2	1	37	-0.01	-10	-10	3	-10	138	A9836577	
VR	74564	A	20	0.27	325	1	0.01	11	200	446	-2	-1	27	-0.01	-10	-10	2	-10	52	A9836577	
VR	74565	A	30	0.25	425	1	0.02	7	140	376	-2	1	34	-0.01	-10	-10	3	-10	28	A9836577	
VR	74566	A	40	0.29	250	1	0.02	9	170	118	-2	1	20	0.03	-10	-10	7	-10	30	A9836577	

SAMPLE			HOLE	FROM	TO	WIDTH	AU_PPB	AG_PPM	AL_PCT	AS_PPM	BA_PPM	BE_PPM	BI_PPM	CA_PCT	CD_PPM	CO_PPM	CR_PPM	CU_PPM	FE_PCT	GA_PPM	HG_PPM	K_PCT
VR	74567	A	F98-05	240.70	241.02	0.32		0.4	1.06	162	90	-0.5	-2	0.43	-0.5	4	65	145	2.57	-10	-1	0.3
VR	74568	A	F98-05	241.02	242.04	1.02		-0.2	0.95	310	80	-0.5	-2	1.08	-0.5	18	74	36	1.73	-10	-1	0.38
VR	74569	A	F98-05	242.04	242.35	0.31		1.8	0.84	510	90	-0.5	6	0.69	-0.5	11	70	185	2.27	-10	-1	0.28
VR	74570	A	F98-05	242.35	244.00	1.65		-0.2	1.08	344	90	-0.5	-2	1.02	-0.5	6	66	39	2.03	-10	-1	0.32
VR	74571	A	F98-05	244.00	244.30	0.30		23.8	0.21	2000	10	-0.5	74	2.07	4.5	5	126	352	2.51	-10	-1	0.05
VR	74572	A	F98-05	244.30	246.00	1.70		2.4	1.2	702	80	-0.5	8	1.44	0.5	12	65	87	2.96	-10	-1	0.33
VR	74573	A	F98-05	246.00	246.90	0.90		4.6	0.87	858	100	-0.5	10	0.57	1.5	10	87	155	2.85	-10	1	0.31
VR	74574	A	F98-05	246.90	249.90	3.00		0.2	0.53	326	40	-0.5	-2	1.11	-0.5	8	38	38	1.83	-10	-1	0.15
VR	74575	A	F98-05	249.90	252.00	2.10		0.2	0.75	510	80	-0.5	-2	1	-0.5	11	73	184	2.09	-10	-1	0.25
VR	74576	A	F98-05	252.00	253.50	1.50		0.8	0.92	302	100	-0.5	-2	1.27	-0.5	12	83	209	2.84	-10	-1	0.33
VR	74577	A	F98-05	253.50	256.00	2.50		0.8	0.48	550	80	-0.5	4	1.07	0.5	8	88	70	1.77	-10	-1	0.25
VR	74578	A	F98-05	256.00	259.00	3.00		-0.2	0.51	282	70	-0.5	-2	0.87	-0.5	6	73	37	1.7	-10	-1	0.23
VR	74579	A	F98-05	259.00	260.98	1.98		0.2	0.48	304	60	-0.5	-2	0.82	-0.5	7	82	47	1.59	-10	-1	0.2
VR	74580	A	F98-05	260.98	261.20	0.22		10.2	0.2	398	30	-0.5	28	1.62	0.5	6	122	36	0.95	-10	-1	0.09
VR	74581	A	F98-05	261.20	263.50	2.30		2.4	0.4	746	60	-0.5	2	1.17	1	16	72	132	2.14	-10	-1	0.22
VR	74582	A	F98-05	263.50	265.79	2.29		1.6	0.55	472	80	-0.5	2	0.69	0.5	14	60	133	2.48	-10	-1	0.27
VR	74583	A	F98-05	265.79	269.00	3.21		0.8	0.52	290	60	-0.5	2	0.93	0.5	12	34	132	2.46	-10	-1	0.18
VR	74584	A	F98-05	269.00	272.50	3.50		-0.2	0.57	122	90	-0.5	-2	0.77	-0.5	7	82	82	2.08	-10	-1	0.29
VR	74585	A	F98-05	272.50	274.00	1.50		205	0.63	60	70	-0.5	-2	1.38	-0.5	7	80	388	2.02	-10	-1	0.24
VR	74586	A	F98-05	274.00	277.00	3.00		2	1.04	146	90	-0.5	6	0.57	-0.5	9	47	111	2.5	-10	-1	0.3
VR	74587	A	F98-05	277.00	278.00	1.00		-0.2	1.24	46	80	-0.5	-2	0.35	-0.5	9	58	67	2.39	-10	-1	0.3
VR	74588	A	F98-05	278.00	280.00	2.00		-0.2	1.1	10	80	-0.5	-2	0.79	-0.5	8	62	24	1.83	-10	-1	0.4
VR	74589	A	F98-05	280.00	282.85	2.85		-0.2	0.85	22	40	-0.5	-2	0.65	-0.5	8	41	37	1.88	-10	-1	0.27

SAMPLE			LA_PPM	MG_PCT	MN_PPM	MO_PPM	NA_PCT	NI_PPM	P_PPM	PB_PPM	SB_PPM	SC_PPM	SR_PPM	TI_PCT	TL_PPM	U_PPM	V_PPM	W_PPM	ZN_PPM	CERTIF	ALT_CERTIF
VR	74567	A	40	0.38	290	-1	-0.01	26	380	152	-2	1	16	-0.01	-10	-10	5	-10	38	A9836577	
VR	74568	A	40	0.34	335	1	0.02	13	190	24	-2	1	33	0.03	-10	-10	7	-10	36	A9836577	
VR	74569	A	40	0.33	330	1	0.01	16	210	652	-2	1	24	-0.01	-10	-10	3	-10	32	A9836577	
VR	74570	A	40	0.41	345	3	0.01	13	250	78	2	1	34	0.01	-10	-10	6	-10	40	A9836577	
VR	74571	A	20	0.09	450	3	0.02	25	310	8040	2	-1	60	-0.01	-10	-10	-1	-10	26	A9836577	
VR	74572	A	30	0.53	485	3	0.01	21	470	890	-2	1	46	0.01	-10	-10	8	-10	56	A9836577	
VR	74573	A	30	0.32	360	3	0.01	23	320	1670	4	1	21	-0.01	-10	-10	4	-10	36	A9836577	
VR	74574	A	30	0.32	385	1	0.01	10	210	176	-2	-1	38	-0.01	-10	-10	3	-10	44	A9836577	
VR	74575	A	20	0.22	365	-1	0.01	17	290	126	-2	1	32	-0.01	-10	-10	4	-10	26	A9836577	
VR	74576	A	20	0.28	470	1	0.01	21	350	302	2	1	35	-0.01	-10	-10	4	-10	30	A9836577	
VR	74577	A	30	0.25	405	3	0.03	12	240	314	-2	1	41	-0.01	-10	-10	3	-10	54	A9836577	
VR	74578	A	30	0.26	370	1	0.03	10	180	48	2	1	36	-0.01	-10	-10	3	-10	34	A9836577	
VR	74579	A	30	0.21	310	1	0.02	10	190	122	-2	1	35	-0.01	-10	-10	3	-10	32	A9836577	
VR	74580	A	10	0.1	355	2	-0.01	8	190	3120	-2	-1	52	-0.01	-10	-10	1	-10	30	A9836577	
VR	74581	A	10	0.27	495	-1	0.01	15	210	618	2	1	42	-0.01	-10	-10	2	-10	144	A9836577	
VR	74582	A	30	0.35	415	-1	0.01	14	270	512	6	1	29	-0.01	-10	-10	3	-10	104	A9836577	
VR	74583	A	30	0.34	385	3	0.01	18	320	314	-2	1	36	-0.01	-10	-10	3	-10	52	A9836577	
VR	74584	A	40	0.29	365	1	0.03	13	210	50	8	1	41	-0.01	-10	-10	4	-10	46	A9836577	
VR	74585	A	30	0.35	515	258	0.01	26	180	134	6	1	76	-0.01	-10	-10	3	60	34	A9836577	A9837095
VR	74586	A	10	0.43	325	3	0.01	17	260	542	-2	1	24	-0.01	-10	-10	5	-10	40	A9836577	
VR	74587	A	20	0.49	260	1	0.02	16	240	28	6	1	16	0.01	-10	-10	6	-10	44	A9836577	
VR	74588	A	30	0.34	270	1	0.03	13	190	10	-2	1	34	0.04	-10	-10	8	-10	40	A9836577	
VR	74589	A	30	0.31	240	1	0.01	14	210	8	-2	1	27	0.03	-10	-10	6	-10	40	A9836577	

APPENDIX X

SURFACE TEM GEOPHYSICS REPORT

Quantec Consulting Inc.
P.O Box 580, 101 King Street
Porcupine, ON P0N 1C0
Phone (705) 235-2166
Fax (705) 235-2255

Quantec Consulting Inc.

Geophysical Survey Logistical Report

Quantec

Regarding the
TRANSIENT ELECTROMAGNETIC
SURFACE PROFILING SURVEYS
over the FINDLAY CREEK PROJECT
near Cranbrook, BC
on behalf of
KENNECOTT CANADA EXPLORATION INC.
Vancouver, BC

QCI-QCI QCI QCI QCI QCI

P.Plazek
J.M.Legault
Sept., 1998
Project C436

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LIST OF FIGURES AND TABLES

1. INTRODUCTION

- **QCI Project No:** C-436
- **Client Name:** KENNECOTT CANADA EXPLORATION INC.
- **Client Address:** 354 - 200 Granville Street
Vancouver BC V6C 1S4
- **Project Name:** Findlay Creek Project
- **Survey Grids**
  1. Clear Cut
  2. Tourmalinite
  3. Cassat
  4. Pico
  5. Doctor Lake
  6. Echo Lake
- **Survey Period:** August 27TH to September 15TH, 1998
- **Survey Types:** LPTEM Fixed Loop Profiling and Moving Loop Sounding
- **Client Representatives:** Andrew Cole
- **Objectives:**
  1. Exploration objectives:
  To detect and characterize large areas of massive sulphide mineralization associated with a possible Sullivan - type deposit, as ground follow - up to airborne FDEM anomalies and to correlate these with the geology in the area.
  2. Geophysical objectives:
  To utilize the **LPTEM** method, based on its deep penetration capabilities, to detect massive sulphide conductors and determine their characteristics. Also, to compare the capabilities of moving center loop soundings versus large fixed loop profiling in this area of mountainous terrain.
- **Report Type:** Logistical

2. GENERAL SURVEY DETAILS

2.1. LOCATION

- **Province:** British Colombia
- **Country:** Canada
- **Nearest Settlement** Cranbrook, BC
- **NTS Map Reference:** 82 K/1

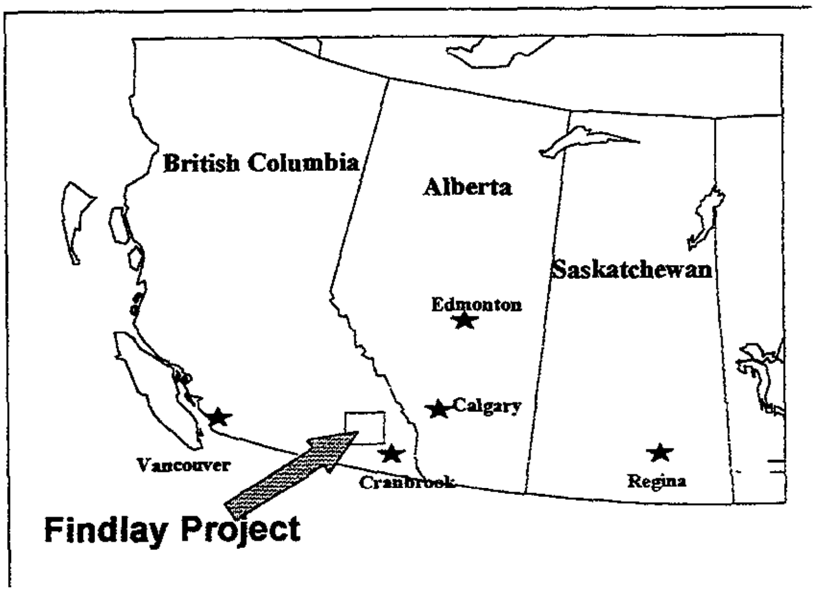

Figure 1: General Survey Location of the Findlay Creek Project.

2.2. ACCESS

- **General Location of Property:** approx. 2 hours north of Cranbrook BC.
- **Base of Operations:** Field camp near Findlay Creek, BC
- **Distance by Land to Grids:** approx. 2-10 kilometres from camp.
- **Nearest Highway:** Hwy. 93/95
- **Mode of Access to Property:** 4x4 truck
- **Mode of Access to Grids:** Helicopter and 4x4 truck

2.3. SURVEY GRID

- **Coordinate Reference System**: Local exploration grid (Non UTM referenced)
- **Line Direction:** Variable orientation EW or NS reconnaissance profiles (generally following creek beds or contour lines).
- **Line Separation:** Tourmalinite and Doctor (see Table I) = 200m
All other grids = reconnaissance / orthogonal profiles
- **Station Interval:** 50 - 100m
- **Base and Tie Lines:** Tourmalinite grid: BL 2000E.
All other grids: single line / orthogonal profiles
- **Established:** Tourmalinite, Clear Cut, and Doctor grid: Kennecott
All other grids: Quantec (hip chained)
- **Method of Chaining:** Tourmalinite, Clear Cut, Doctor grid: Secant chained (Kennecott)
All other grids: Slope chained (Quantec)

3. SURVEY WORK

3.1. GENERALITIES

- **Survey Dates:** August 27TH - September 15TH, 1998
- **Survey Period:** 20 days
- **Survey/Loop Days:** 16 days
- **Mob Demob days:** 3
- **Total Survey Coverage:** Surface TEM: 22.2km (see Table I)

GRID	SURVEY TYPE	SURVEY LINE	START	END	TOTAL(m)
1. Clear Cut	Moving loop	L 5000 N	5000 E	5600 E	600
2. Tourmalinite	Moving loop	L 2000 N	1100 E	2300 E	1200
2. Tourmalinite	Profiling	L 2050 N	1300 E	2600 E	1300
		L 2250 N	1500 E	2600 E	1100
		L 2450N	1600 E	2600 E	1000
		L 2650 N	2000 E	2600 E	600
		L 2850 N	1800 E	2600 E	800
		L 3050 N	2000 E	2600 E	600
3. Cassat - Loop1	Profiling	L 11	3150 E	4900 E	1750
		L 12	1000 E	1200 E	200
		L 11 N	4900 E	6100 E	1200
		L 4500 E	1700 S	800 N	2500
3. Cassat - Loop2	Profiling	L 21 N	4900 E	6300 E	1400
		L 22 N	6400 E	7500 E	1100
4. Pico Grid (Cassat Loop 3)	Profiling	L 31 E	3500 E	5000 E	1500
5. Doctor Lake	Profiling	L 1000 N	1000 E	2300 E	1300
		L 1200 N	1000 E	2300 E	1300
6. Echo Lake	Profiling	L 1000 E	600 N	1000 S	1600
		L 300 S	400 E	700 W	1100

Table I: Surface LPTEM Coverage at the Findlay Creek Project

3.2. SPECIFICATIONS

3.2.1. TEM Profiling Survey

- **Method:** Transient Electromagnetic
- **Technique:** Profiling
- **Configuration:** Both inside and outside loop measurements
- **Output Power Stage:** Low Power (2.8 kW)
- **Dimension:** 3-D (X, Y and Z components)
- **Loop Locations:** See Table II and Appendix I
- **Loop Sizes:** See Table II and Appendix I
- **Line Interval:** 200m
- **Sampling Interval:** 50 - 100m

GRID	EW LOOP BOUNDARIES	NS LOOP BOUNDARIES	LOOP SIZE (mxm)
Tourmalinite	1100E - 2000E	1900N - 3100N	1200m x 900m
Cassat Loop1	3950E - 5000E	300N - 400N	oval shaped: approx. area = 750m x 750m
Cassat Loop 2	5100E - 6350E	approx. 600m	approx. area = 1000m x 600m
Pico	approx. 600m	4000N - 5000N	oval shape: approx. area = 700m x 700m
Doctor Lake	n/a	n/a	irregular shape: approx. area = 750m x 600m
Echo Lake	n/a	n/a	irregular shape: approx. area = 1000mx1000m

Table II: Size and Location of TEM Transmit Loops.

3.2.2. TEM Moving Loop Survey

- **Method:** Transient Electromagnetic
- **Technique:** Moving Loop
- **Configuration:** Moving center and 50m outside loop along line
- **Output Power Stage:** Low Power
- **Dimension:** 3-D (X, Y and Z components)
- **Loop Locations:** Center-Loop: centered on Rx
  Off-Loop: 100m away from loop center along survey line

- **Moving Loop Sizes:** 100m x 100m
- **Line Interval:** only 1 line read per grid
- **Sampling Interval:** 100m

3.3. PERSONNEL

- **Field Supervisor:** Sherwood T. Coulson, Porcupine, ON
- **Field Project Manager:** Paul Plazek, Porcupine, ON
- **Field Assistants:** Roch Michaud, North Bay, ON
  Up to 4 additional assistants supplied by Kennecott

3.4. INSTRUMENTATION

3.4.1. TEM Profiling Survey

- **Receiver:** Geonics Digital Protem (3 channel, 20 time gates)
- **Receiver Coil:** Geonics 3D, 200m^2 Ferro Magnetic coil
- **Transmitter:** Geonics EM-37 (7.5 Hz, 50% duty cycle)
- **Power Supply:** Honda 5.5HP with Geonics Generator alternator (2.8kVA @ 400Hz)

3.4.2. TEM Moving Loop Survey

- **Receiver:** Geonics Digital Protem (3 channel, 20 time gates)
- **Receiver Coil:** Geonics 3D, 200m^2 Ferro Magnetic coil
- **Transmitter:** Geonics EM-57 (7.5 Hz, 50% duty cycle)
- **Power Supply:** Portable Honda EX-650 Motor Generator (600W)

3.5. PARAMETERS

3.5.1. TEM Profiling Survey

Pulse repetition frequency:	7.5Hz
Gain:	3-6
Integration number:	30 sec (Protem Rx)
Approximate Loop Size:	see Table II
Current:	see Table IV
Turn-off time:	see Table IV
Gate positions	(see Appendix C)
Synchronization mode:	Crystal

Table III: System Parameters for Profiling TEM Survey.

- **Coil Conventions:** (see Table V)

GRID	Current (amps)	Turn-off Time(micro-seconds)
1. Tourmalinite	7	265
2. Cassat Loop1	7.5	215
2. Cassat Loop 2	8	210
3. Pico	9	215
4. Doctor Lake	11	260
5. Echo Lake	7	255

Table IV: Current and Turn-off times for TEM Transmit Loops.

GRID	COMPONENT	COIL ORIENTATION
1. Tourmalinite	Z	Positive Vertical Up
	X	Positive Grid East
	Y	Positive Grid North
2.Cassat Loop 1	Z	Positive Vertical Up
	X	Positive Grid East
	Y	Positive Grid North
2.Cassat Loop 2	Z	Positive Vertical Up
	X	Positive Grid East
	Y	Positive Grid North
3. Pico	Z	Positive Vertical Up
	X	Positive Grid North
	Y	Positive Grid West
4. Doctor Lake	Z	Positive Vertical Up
	X	Positive Grid East
	Y	Positive Grid North
5. Echo Lake	Z	Positive Vertical Up
	X	Positive Grid North
	Y	Positive Grid West

Table V: Coil Conventions for TEM Surveys.

- **Data Reduction**[1]: nanoVolts/Ampere-metre^2

3.5.2. TEM Moving Loop Survey

Pulse repetition frequency:	7.5Hz
Gain:	3-6
Integration number:	30 sec (Protem Rx)
Loop Size:	100m x 100m
Current:	10.5 - 11 Amps
Turn-off time:	220 - 55 micro seconds
Gate positions	(see Appendix C)
Synchronization mode:	Reference Cable

Table VI: System Parameters for Moving Loop TEM Survey.

- **Coil Conventions:** (see Table VII)

GRID	COMPONENT	COIL ORIENTATION
1. Tourmalinite	Z	Positive Vertical Up
	X	Positive Grid East
	Y	Positive Grid North
2. Clear Cut	Z	Positive Vertical Up
	X	Positive Grid East
	Y	Positive Grid North

Table VII: Coil Conventions for Moving Loop TEM Survey.

Data Reduction[2]: nanoVolts/Ampere-metre^2

3.6. MEASUREMENT ACCURACY AND REPEATABILITY

3.6.1. TEM Profiling Survey

- **Number of Repeats per Station:** 1-2
- **Number of Repeats per Day:** 20-40
- **Number of Repeats per Grid:** at least 1 per station
- **Average Repeatability at Channel 1 and 20:** 1-3%
- **Worst Repeatability at Channel 1 and 20:** 12%, 20%

3.6.2. TEM Moving Loop Survey

- **Number of Repeats per Station:** 2-3

[1] Equivalent to Crone units of nanoTesla/second normalized to a unit current.
[2] Equivalent to Crone units of nanoTesla/second normalized to a unit current.

- **Average Repeatability at Channel 1 and 20:** 2-3%
- **Worst Repeatability at Channel 1 and 20:** 9%, 15%

3.7. DATA PRESENTATION

- **Profiles:**

Profile Format	4-Axis (see Fig.3)
# of Profiles	68
Horizontal Map Scales:	1:5000
Vertical Profile Scales:	Early Channels: 5 - 100 nV/Am^2 Late Channels: 2 - 0.05 nV/Am^2
Components:	X ,Y, Z and Total Field

Table VIII: Surface TEM Profile Specifications.

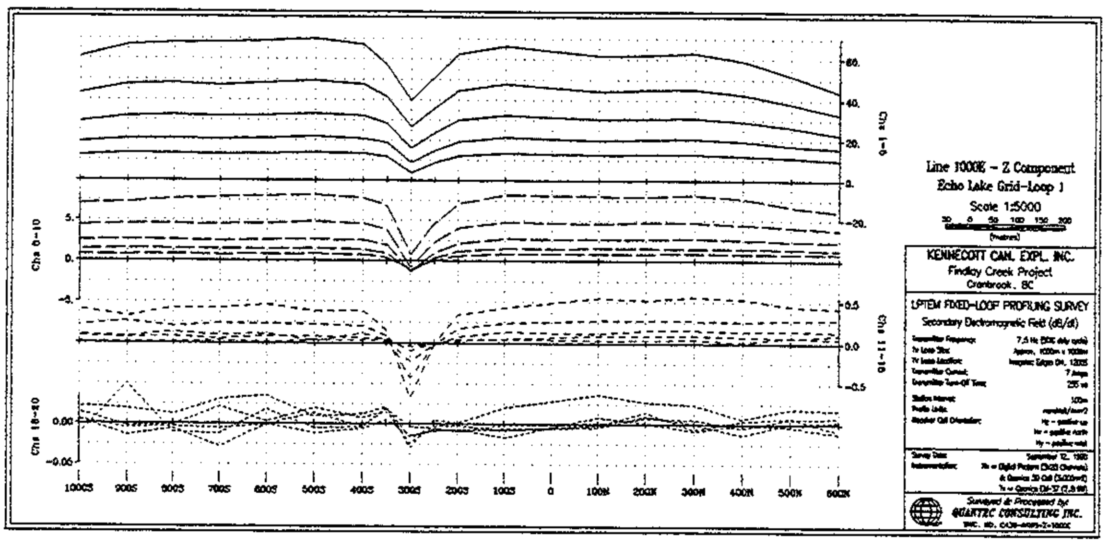

Figure 2: Surface TEM 4-Axis Profile Format.

- **Digital Data:** Daily raw files and processed data (Geosoft .XYZ format) on 3.5 inch HD (1.44 Mbytes) diskette(s).

a) raw data dump files, according to acquisition date (DDMMYY.RAW)
Geonics Digital Protem format (refer to Protem manual)

b) reduced XYZ ASCII data files, according to line number and component
(i.e. 76wk.xyz where k=component - Z, X, Y or T for Total Field).

Column 1: NS Station number (m)
Column 2: EW Line number (m)
Column 3: Primary pulse (millivolts)
Column 4: Channel 1 secondary rate of decay of TEM field (nanoVolt/ampere*m^2)
Column 5: Channel 2 ...
⇓
Column 23: Channel 20 secondary rate of decay of TEM field (nanoVolt/ampere*m^2)

RESPECTFULLY SUBMITTED

J. M. Legault
Senior Geophysicist

Paul Plazek
Crew Chief

Porcupine, ON
September 1998

APPENDIX A

STATEMENT OF QUALIFICATIONS:

I, Paul J. Plazek, declare that:

1. I am a geophysicist with residence in Porcupine, Ontario and am presently employed in this capacity with Quantec Consulting Inc. of Porcupine, Ontario.
2. I am a graduate of Queen's University, Kingston, Ont., in 1989, with an Honours Bachelor of Science Degree in Geological Engineering.
3. I have practiced my profession in Canada since graduation.
4. I have no interest nor do I expect to receive any interest, direct or indirect, in the properties or securities of Kennecott Canada Exploration Inc.
5. I am responsible for the data acquisition, validation, and plotting of the results for this survey. I am also the technical writer for this report. The statements made in this report represent my professional opinion based on my consideration of the information available to me at the time this report was written.

Porcupine, Ontario
September, 1998

Paul J. Plazek, B.Sc.
Geophysicist
Quantec Consulting Inc.

APPENDIX A

STATEMENT OF QUALIFIATIONS

I, Jean M. Legault, declare that:

1. I am a consulting geophysicist with residence in Timmins, Ontario and am presently employed in this capacity with Quantec Consulting Inc. of Porcupine, Ontario.
2. I obtained a Bachelor's Degree, with Honours, in Applied Science (B.A.Sc.), Geological Engineering (Geophysics Option), from Queen's University at Kingston, Ontario, in Spring 1982.
3. I am a registered professional engineer, since 1985, with license to practice in the Province of Ontario.(Reg. # 90531542-09)
4. I have practiced my profession continuously, since May, 1982, in North-America, South-America and North-Africa.
5. I am a member of the Association of Professional Engineers of Ontario, the Quebec Prospectors Association, the Prospectors and Developers Association of Canada, and the Society of Exploration Geophysicists.
6. I have no interest, nor do I expect to receive any interest in the properties or securities of Kennecott Canada Exploration Inc.
7. I oversaw the report construction. The statements made in this report represent my professional opinion based on my consideration of the information available to me at the time of writing this report.

Porcupine, Ontario
September, 1998

Jean M. Legault, P.Eng. (O/S)
Dir. of Technical Services
Chief Geophysicist
Quantec Group

APPENDIX B

SURVEY PROCEDURES AND GENERAL THEORY

TEM Surface

TEM profiling is conducted on lines either adjacent to (Off-Loop mode) or surrounded by (In-Loop mode) a large fixed rectangular transmit loop. Current is passed through the loop which following the Turn-Off, produces a primary magnetic field (H) both inside and outside (Figure B1). This primary field induces a vortex current pattern, which energizes conductors and which in turn create their own secondary magnetic field (Bs). The rate of change of the decaying secondary magnetic flux (dBs/dt) is measured as the vertical (**Hz**), in-line horizontal (**Hx**) and/or cross line horizontal (**Hy**) vector components on surface using an air-core sensor coil. These measurements of the TEM decay (20 log-time slices) are taken during the "Off-Time", using a 30 cycle/sec, base repetition rate.

In keeping with the industry standard, the primary field is always considered positive up inside the loop and negative down outside. Similarly, for secondary EM fields, the receiver coil is oriented positive vertical up for the **Hz** component. The convention for In-Loop surveys, has the in-line component, **Hx** oriented either positive east (for grid EW lines) or north (for grid NS lines). The Off-Loop survey convention differs, with the receiver coil orientation for **Hx** pointing positive away from the transmit loop (for EW or NS lines). Finally, the sign convention in all cases, has the **Hy** component pointing positive orthogonal to the left of the **Hx**, according to the right-hand-rule.

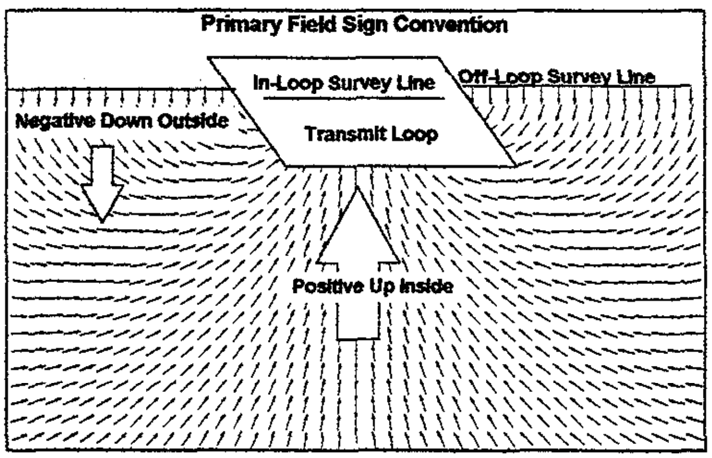

Figure B1: Primary field sign convention for TEM surveys.

At the end of each survey day, the stored data are transferred to a microcomputer where they corrected for the turn-off time, loop area, system gain and current, and converted from millivolts to nanoVolts per ampere meter squared or nanoVolts per meter squared. The data are then transferred to disk for storage and processing. Report quality field plots are generated on site, using a 24-pin printer in order to monitor the data characteristics and to provide a preliminary interpretation capability.

The following equations govern the transient EM response for buried plate-like conductive bodies[1]

Target Response to Transmitter Current Waveform:

$$emf = \frac{1}{\tau} e^{-t/\tau}$$

$$\begin{aligned} \text{where: } t &= \textit{fixed time} \\ e &= \textit{exponential decay} \\ \tau &= \textit{time constant of conductor} \end{aligned}$$

The time constant of the response is alternatively defined as the slope of the lin-log decay curve (Geonics) or, more exactly, as the time channel where the amplitude of the decay collapses to 37% (1/e) of its maximum value. Both τ and the analogous decay strength (i.e., the number of anomalous channels above background), are commonly used as indicators of conductor quality. This relationship between decay-strength and the conductivity-thickness can easily be demonstrated in the following equation for a vertically dipping conductive sheet:

$$\tau = \frac{\sigma\mu t h}{\pi^2} \textit{ for a thin plate}$$

$$\begin{aligned} \text{where } \sigma &= \textit{conductivity of target} \\ \mu &= \textit{magnetic susceptibility} \\ t &= \textit{thickness of plate} \\ h &= \textit{vertical extension of plate} \end{aligned}$$

thereby giving, for an infinite vertical sheet:

$$\sigma t = \frac{\pi^2}{\mu h} \tau \approx \tau/0.31 \textit{ mhos / metre (siemens)}$$

From these equations and relationships, it therefore becomes obvious of the common use of the anomaly strength of decay as a simple, rule-of thumb indicator of the relative conductivity-thickness product for TEM surveys.

In addition, the total secondary field is calculated using the three components (Hx, Hy and Hz) in the following formula

$$Htot = \sqrt{Hx^2 + Hy^2 + Hz^2} \textit{ nanoVolt / } Am^2.$$

[1] From Geonics Limited, EM-37 TEM System Design Parameter, Mississauga, Ont., 1982.

APPENDIX C

INSTRUMENT SPECIFICATIONS

GEONICS LIMITED

EM-37 Transmitter
Technical Specifications

Current Wave form: bipolar square wave.

Repetition Rate: 3Hz, 7.5Hz or 30Hz in countries using 60Hz power line frequency; 2.5Hz, 6.25Hz or 25Hz in countries using 50Hz power line frequency; all six base frequencies are switch selectable.

Turn-off Time(t): fast linear turn-off maximum of 450 µsec. at 30 amps into a 300x600 meter loop. Decreases proportionally with current and the root of the loop area to a maximum of 20 µsec. Actual value of t read on front panel meter.

Transmitter Loop: any dimensions from 40x40 meters to 300x600 meters maximum at 30 amps. Larger dimensions at reduced current. Transmitter output voltage switch adjustable for smaller loops. Value of loop resistance read from front panel meter; resistance must be greater than 1 ohm on lowest setting to prevent overload.

Protection: circuit breaker protection against input over voltage; instantaneous solid state protection against output short circuit; automatically resets on removal of short circuit. Input voltage output voltage and current indicated on front panel meter.

Output voltage: 24 to 160 volts (zero to peak) maximum

Output power: 2800 watt maximum

Motor generator: 5 HP Honda gasoline engine coupled to a 120 volt, three phase, 400 Hz alternator. Approximately 8 hours continuous operation from built-in fuel tank.

Component Dimensions and Weights

Transmitter Console : 20 by 42 by 32 cm, 20 kg

GPU: 44 by 32 by 21 cm, 65 kg

APPENDIX C

INSTRUMENT SPECIFICATIONS

GEONICS LIMITED

Digital Protem Ground Transient Electromagnetic System Technical Specifications

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Receiver

Measured Quantity: Time rate of decay of magnetic flux along 3 axes

Sensors:
1. (L.F.): Air-cored coil of bandwidth 60 kHz; 100 cm diameter
2. (H.F.): Air-cored coil of bandwidth 850 kHz; 100 cm diameter
3. (3D-3): Three orthogonal component sensor; simultaneous operation
4. (3D-1): Three orthogonal component sensor; sequential operation

Time channels: 20 geometrically spaced time gates for each base frequency gives range from 6 μsec to 800 msec.

Repetition Rate: 0.3 Hz, 0.75, 3, 7.4, 30, 75 or 285 Hz for 60 Hz power-line networks (Base Frequency)

Synchronization: (switch selectable): (1) reference cable
(2) high stability (oven controlled) quartz crystals.

Integration time: 2, 4, 8, 15, 30, 60, 120, 240 sec.

Calibration: Internal self calibration
External Q coil calibration (optional)

Keyboards: Two 3 x 4 matrix sealed key pads with positive tactile feedback

Gain: Automatic or manual control

Dynamic Range: 23 bits (132 dB)

Display Quantity:
(1) Table of time rate of decay of magnetic flux (dB/dt)
(2) Curve of rate of decay of magnetic flux (dB/dt)
(3) Table of apparent resistivity (ρ_a)
(4) Curve of apparent resistivity (ρ_a)
(5) Profile of dB/dt
(6) Real time noise monitor
(7) Calibration curve
(8) Data acquisition statistics (real time)

Storage: Solid state memory with capacity for over 3000 data sets

Display: 8 lines by 40 character (240 x 64 dot) graphic LCD

Data Transfer: Standard RS-232 communications port.

Processor: CMOS 68HC000 8 MHz CPU

Receiver Battery: 12 volts rechargeable battery for 8 hours continuous operation. 6 hours in XTAL mode

Receiver Size: 34 x 38 x 27 cm

Receiver Weight: 15 kg

Operating Temp.: -40°C to +50°C

Transmitters:
(1) Geonics TEM47
(2) Geonics TEM57
(3) Geonics TEM37

Gate Locations

GATE	285/237.5 Hz			75/62.5 Hz			30/25 Hz			GATE
1	6.000	6.813	1.625	32.00	35.25	6.500	80.00	88.13	16.25	1
2	7.625	8.688	2.125	38.50	42.75	8.500	96.25	106.9	21.25	2
3	9.750	11.13	2.750	47.00	52.5	11.00	117.5	131.3	27.5	3
4	12.50	14.19	3.375	58.00	64.75	13.50	145.0	161.9	33.75	4
5	15.88	18.07	4.375	71.5	80.25	17.50	178.8	200.6	43.75	5
6	20.25	23.06	5.625	89.00	100.3	22.50	222.5	250.6	56.25	6
7	25.88	29.44	7.125	111.5	125.8	28.50	278.8	314.4	71.25	7
8	33.00	37.56	9.125	140.0	158.3	36.50	350.0	395.6	91.25	8
9	42.13	47.94	11.63	176.5	199.8	46.50	441.3	499.4	116.3	9
10	53.75	61.13	14.75	223.0	252.5	59.00	557.5	631.3	147.5	10
11	68.50	77.94	18.88	282.0	319.8	75.50	705.0	799.4	188.8	11
12	87.38	99.38	24.00	357.5	405.5	96.00	893.8	1014	240.0	12
13	111.4	126.7	30.63	453.5	514.8	122.5	1134	1287	306.3	13
14	151.7**	166.4	29.38	576.0	654.3	156.5	1440	1636	391.3	14
15	181.1	206.0	49.88	732.5	832.3	199.5	1831	2081	498.8	15
16	231.0	262.8	62.63	932.0	1059	254.5	2330	2648	636.3	16
17	294.6	335.2	81.25	1187	1349	325.0	2966	3373	812.5	17
18	375.9	427.7	103.6	1512	1719	414.5	3779	4297	1036	18
19	479.5	545.6	132.1	1926	2190	528.5	4815	5475	1321	19
20	611.6	695.9	168.5	2455	2792	674.0	6136	6978	1685	20
21*	780.1			3129			7821			21*

* End of Gate 20
** A Gap of 9.7 µsec exists between Gate 13 and Gate 14 in the micro-frequency range/

This Table applies to both synchronization modes regardless of which of TEM37, TEM47 and TEM57 transmitters is used, provided that correct Tx model is selected in Header (2.4).

Note: 7.5/6.25 and 0.75/0.625 Hz proportional to 75/62.5 Hz
3/2.5 and 0.3/0.25 Hz proportional to 30/25 Hz

APPENDIX D

PRODUCTION SUMMARY

FINDLAY CREEK PROJECT - C436					
SURFACE TEM SURVEY					
DATE	DESCRIPTION	LINE	START (m)	END (m)	TOTAL (m)
27-Aug	Mob from Timmins to Invermere, BC.				
28-Aug	Mob from Invermere to camp and do moving loop survey over Clear Cut Anomaly (inside and outside loop readings)	5000N	5000E	5600E	600
29-Aug	Moving loop survey over Tourmalinite Anomaly (inside and outside loop readings)	2000N	1100E	2300E	1200
30-Aug	Lay loop for LPTEM survey and sling generator and transmitter into place.(Tourmalinite anomaly)				
31-Aug	LPTEM survey on Tourmalinite grid.	2050N	2600E	1300E	1300
		2250N	2600E	1500E	1100
		2450N	2600E	2000E	600
1-Sep	LPTEM survey on Tourmalinite grid. Caught line cutters which slowed production	2450N	2000E	1600E	400
		2850N	1800E	2600E	800
		3050N	2000E	2600E	600
2-Sep	LPTEM survey on Tourmalinite grid. Pick up loop and move all equipment back to camp.	2650N	2000E	2600E	600
3-Sep	LPTEM survey on Cassat Grid 1. Loop laid out and 2 riverbed lines(not cut or chained) read.	11, 12			1850
4-Sep	LPTEM survey on Cassat Grid 1. Two perpendicular lines read - one along a creek and the other bush crashed.	11N	4900E	6100E	1200
		4500E	1700S	800N	2500

5-Sep	LPTEM survey on Cassat Grid 2. Loop 1 picked up and loop 2 put in place. Inside loop line read.	21N	4900E	6300E	1400
6-Sep	Outside loop 2 read and loop 2 picked up.	22N	6400E	7500E	1100
7-Sep	All equipment moved to loop 3 and 700m x 1000m loop laid. One line read	31E	3500E	5000E	1500
8-Sep	All equipment moved to Doctor Lake grid and loop 4 laid out. No surveying done due to Tx malfunction. Replacement sent in from Geonics.	.			
9-Sep	Weather day - rain. Roch drove from camp to Calgary (5 hrs) and back to pickup rental Tx.	.			
10-Sep	2 lines surveyed on Doctor Lake grid.	1000N	1000E	2300E	1300
		1200N	1000E	2300E	1300
11-Sep	1000m x 1000m Echo Lake loop laid in extremely mountainous terrain.	.			
12-Sep	Survey 2 perpendicular lines on Echo Lake Grid.	1000E	600N	1000S	1600
		300S	400E	700W	1100
13-Sep	Pick up Echo Lake Loop and return all equipment to camp	.			
14-Sep	Mob - Camp to Calgary	.			
15-Sep	Mob - Calgary to Timmins	.			
				TOTAL	22.2km

APPENDIX E

OPERATOR COMMENTS

TEM Surface Profiling

The extreme mountainous terrain was by far the most limiting factor with respect to types of surveys logistically possible, the production, and the man power required. Because of the reconnaissance nature of the project, a LPTEM profiling survey was used which allowed the read lines to follow paths of least resistance such as creeks and contour lines while the loop remained stationary. The lines for over half the grids (generally creek beds) were not picketed so a hip chain had to be used.

There were a limited number of unusual spikes in the Y component of the data but it was repeatable and no system source was detected. However, since no extra coil cable was available at the time the connections cannot be entirely ruled out as a possible source.

The EM-37 transmitter broke down on the Doctor Lake Grid but a replacement was received from Porcupine in just over 1 day and only a single day of surveying was lost.

Paul Plazek
Project Manager
pers.com., 09/98

APPENDIX F

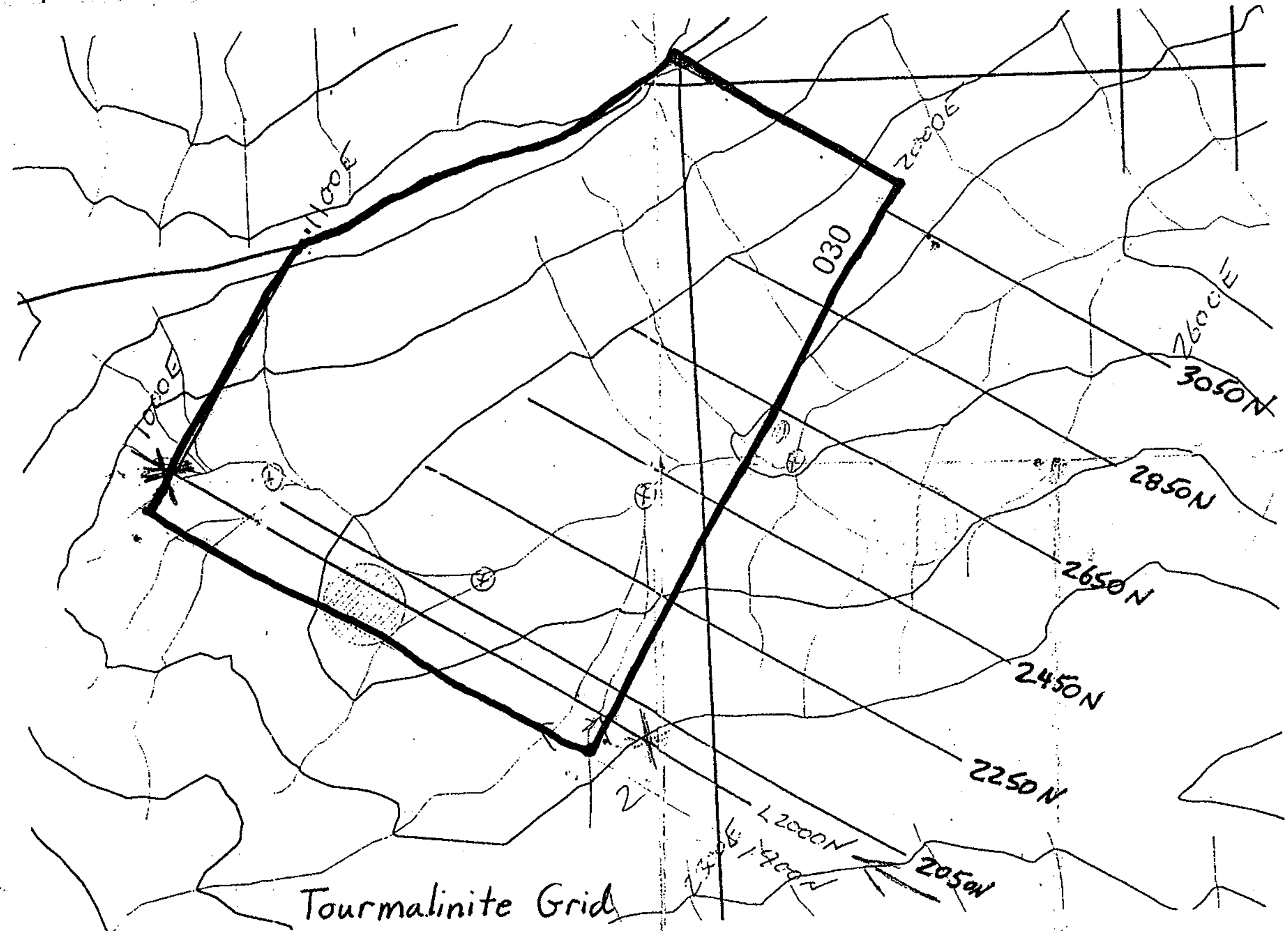
- **LPTEM Surface Profiles: <u>Multi-Channel 4-Axis Profile Plots:</u>** (time rate of decay of the secondary EM field, Total Field X, Y, and Z components, 1:5000, nanovolts per A*meter^2)

LOOP	LINE	DRAWING # (K=X,Y,Z and TF)
2. Tourmalinite	L 2050 N	C436-4AXIS-K-2050N
	L 2250 N	C436-4AXIS-K-2250N
	L 2450N	C436-4AXIS-K-2450N
	L 2650 N	C436-4AXIS-K-2650N
	L 2850 N	C436-4AXIS-K-2850N
	L 3050 N	C436-4AXIS-K-3050N
3. Cassat - Loop1	L 11	C436-4AXIS-K-11
	L 12	C436-4AXIS-K-12
	L 11 N	C436-4AXIS-K-11N
	L 4500 E	C436-4AXIS-K-4500E
3. Cassat - Loop2	L 21 N	C436-4AXIS-K-21N
	L 22 N	C436-4AXIS-K-22N
4. Pico Grid (Cassat Loop 3)	L 31 E	C436-4AXIS-K-31E
5. Doctor Lake	L 1000 N	C436-4AXIS-K-1000N
	L 1200 N	C436-4AXIS-K-1200N
6. Echo Lake	L 1000 E	C436-4AXIS-K-1000E
	L 300 S	C436-4AXIS-K-300S
	TOTAL	68

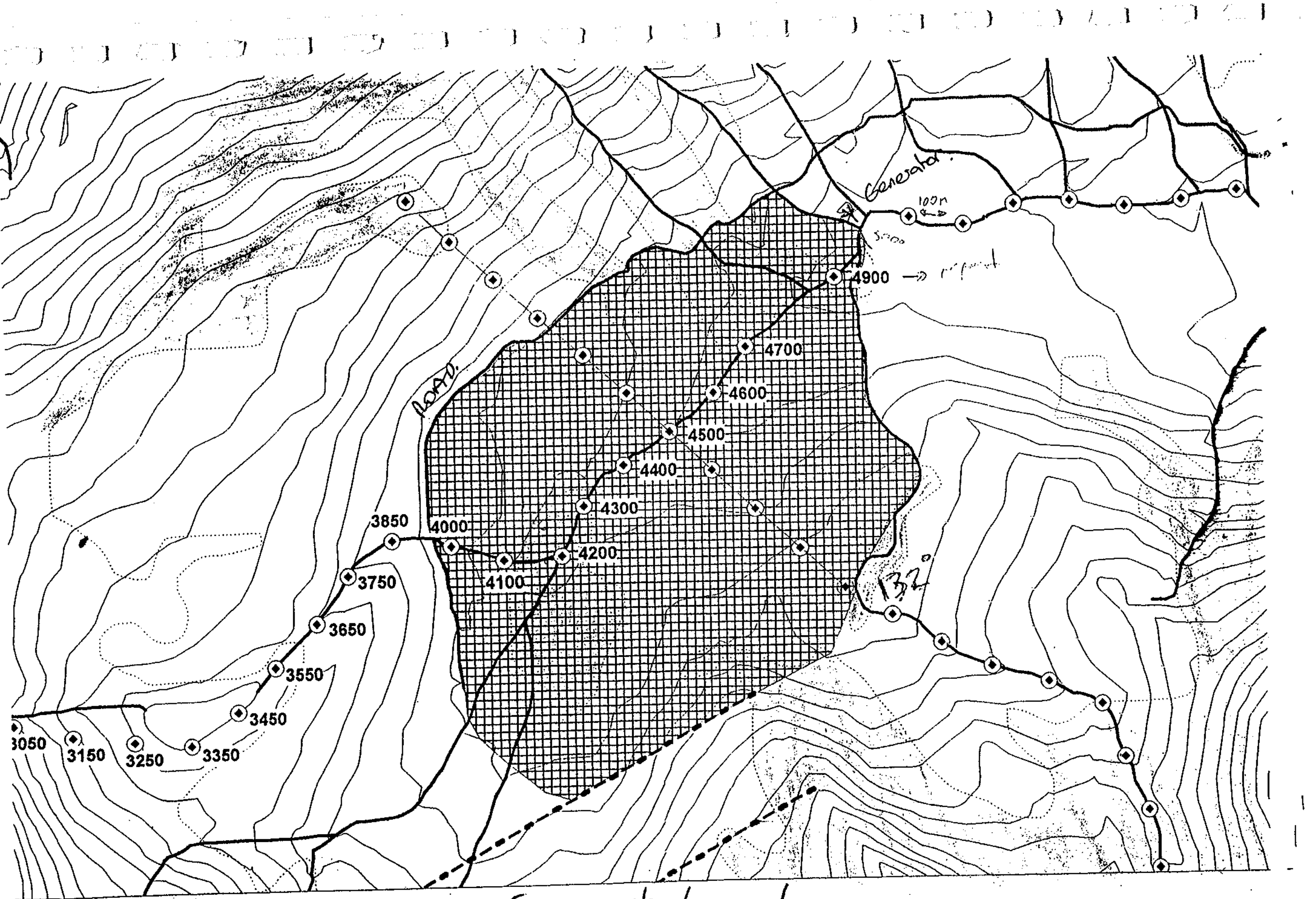
- **TEM Loop Location Maps (field copies):**
  1) <u>Tourmalinite Grid</u>
  2) <u>Cassat Loop 1</u>
  3) <u>Cassat Loop 2</u>
  4) <u>Doctor Lake Grid</u>
  5) <u>Pico Grid</u>
  6) <u>Echo Lake Grid</u>

APPENDIX G

PROFILES AND MAPS

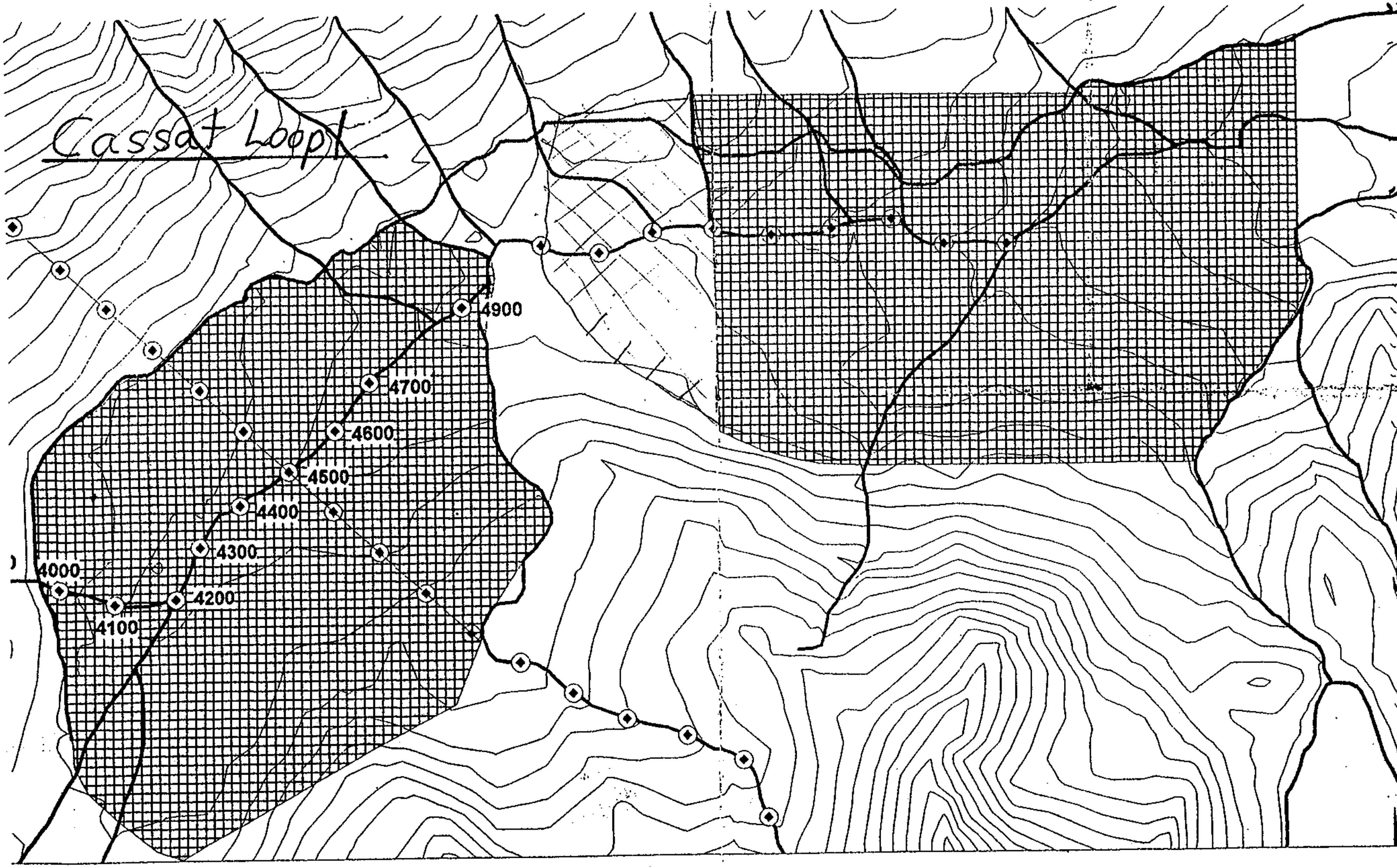


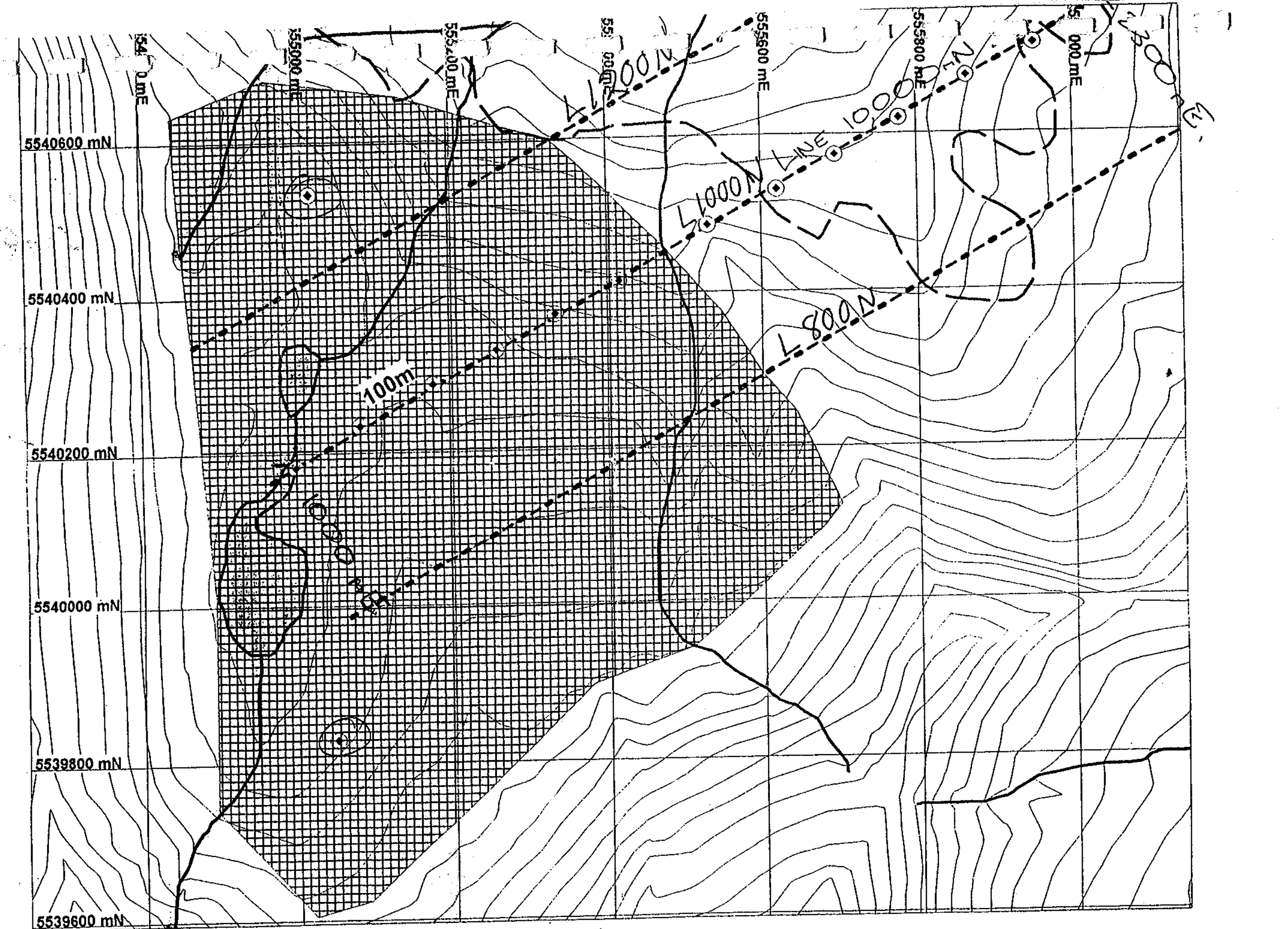
Tourmalinite Grid



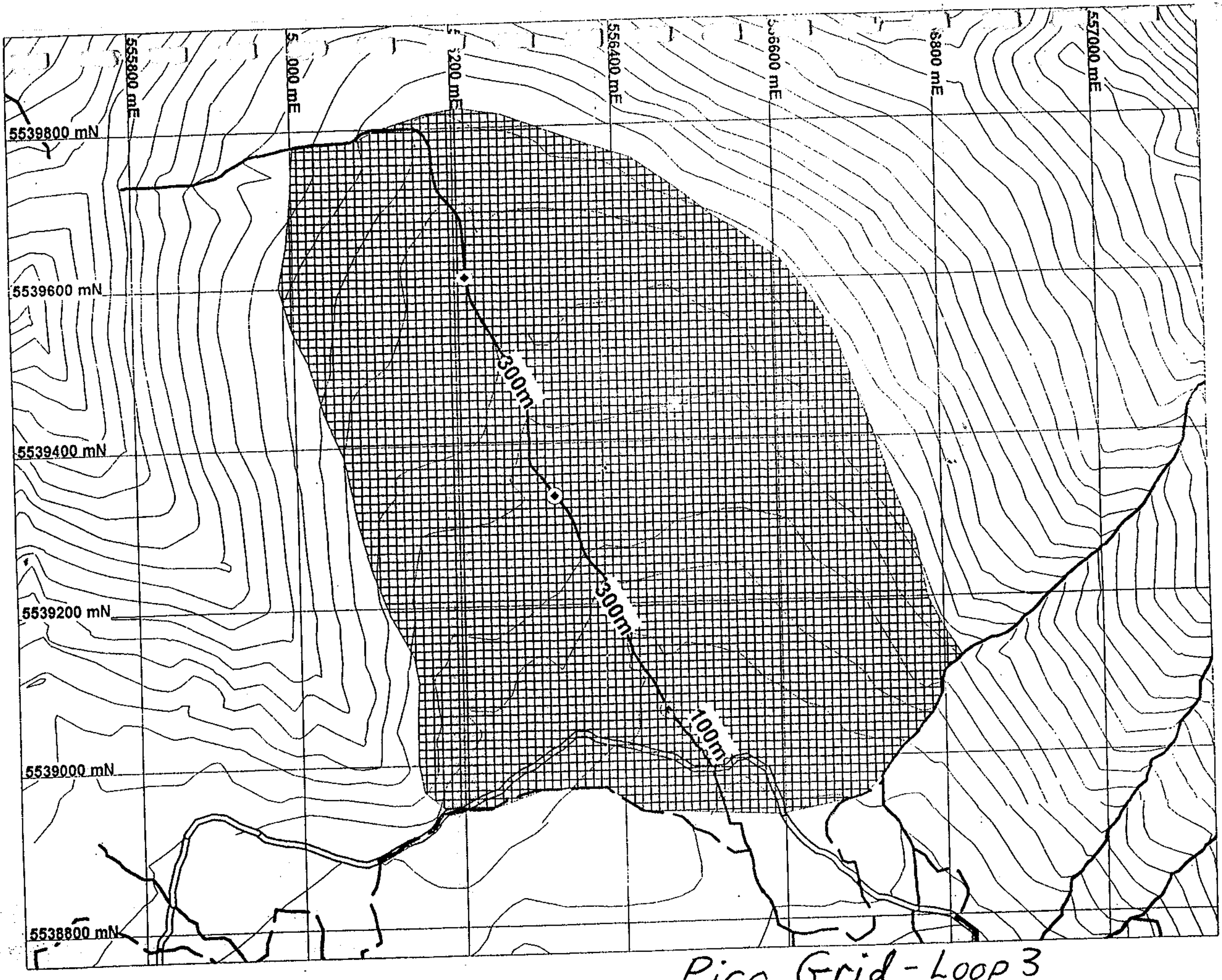
Cassat Loop 1

AREA = 0.5816 km²
≈ 760m x 760m.

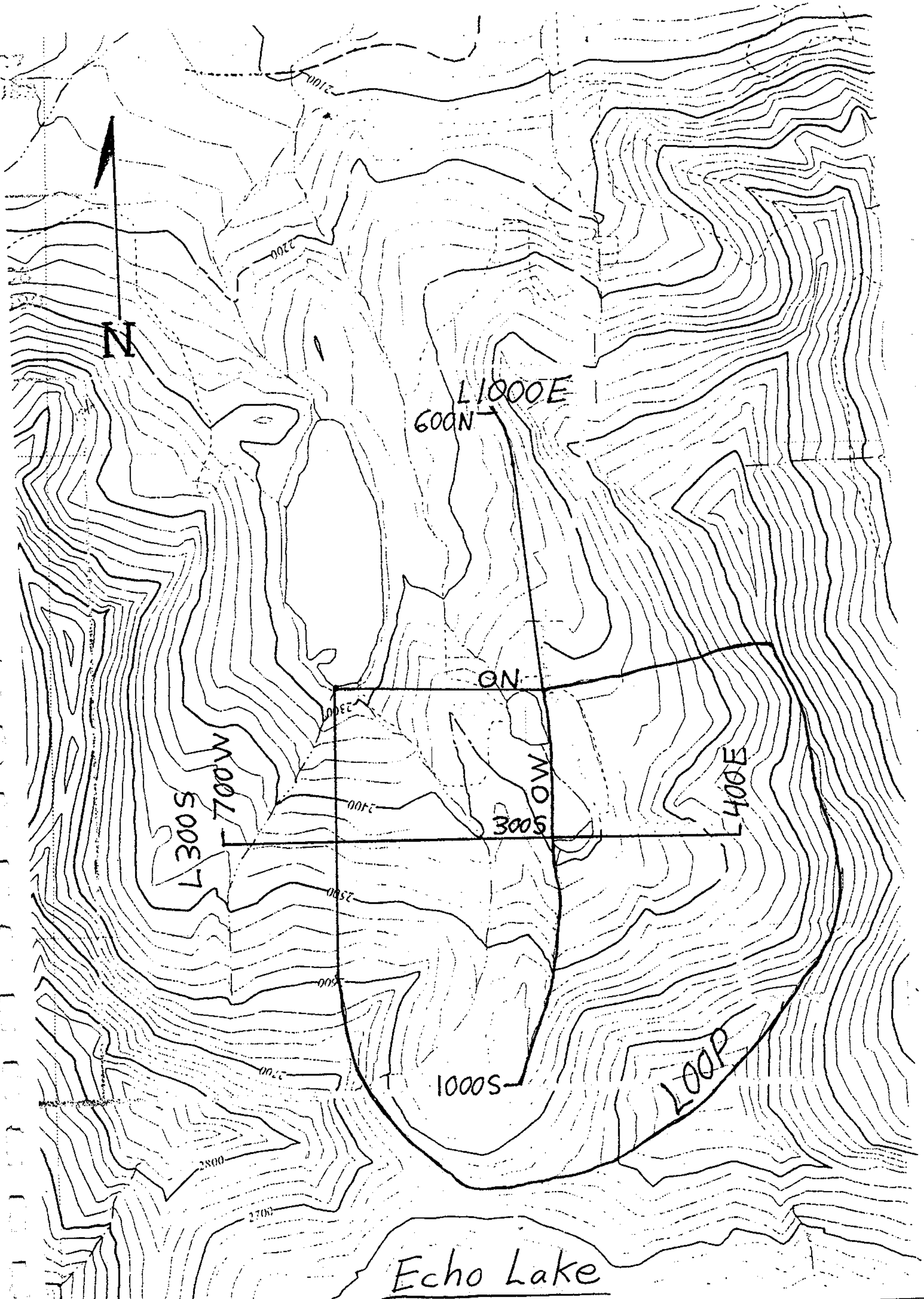




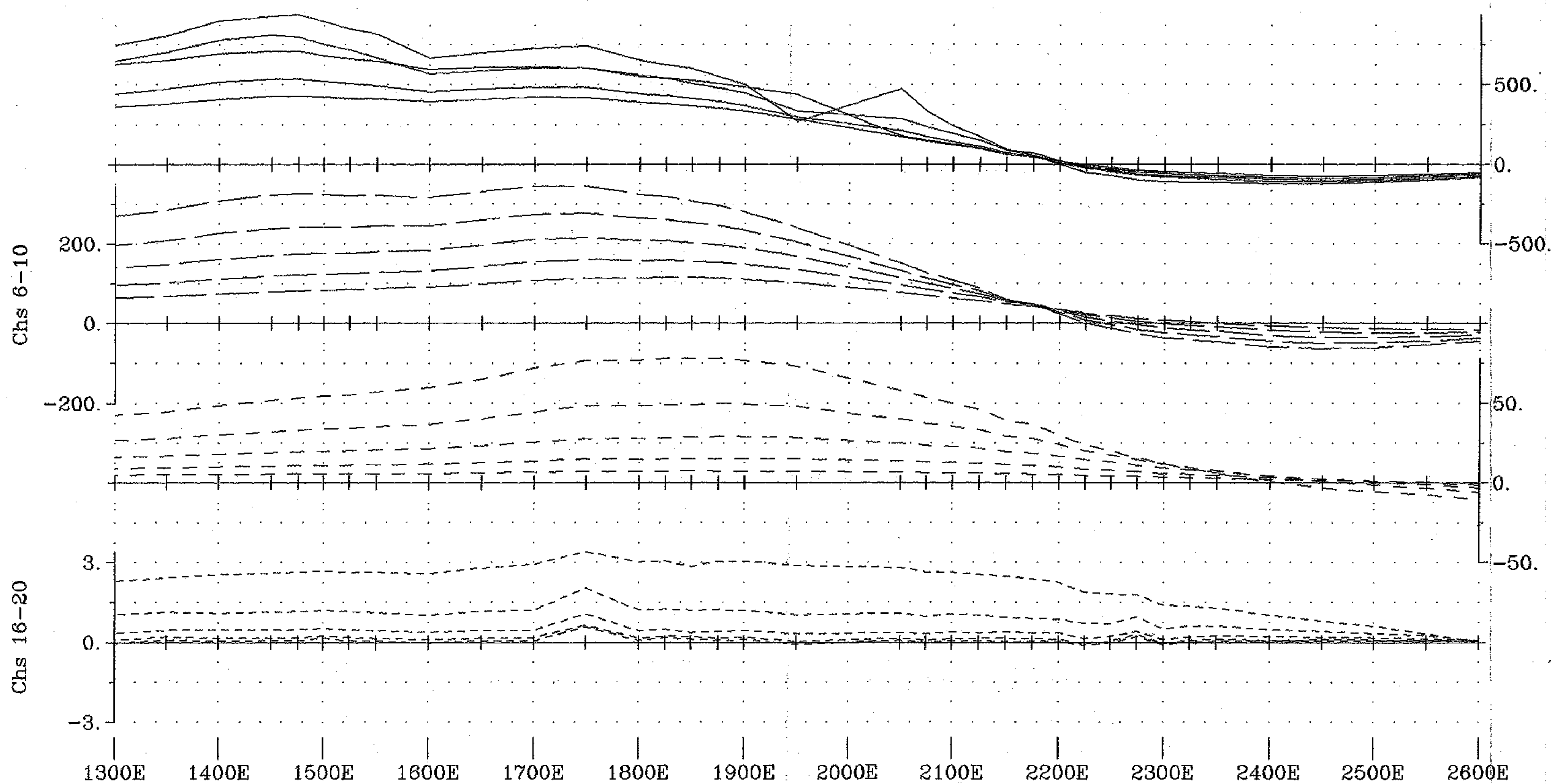
Doctor Lake Grid



Pico Grid - Loop 3



N
L1000E
600N
ON
700W
L300S
OW
300S
400E
1000S
LOOP
2100
2200
2300
2400
2500
2600
2700
2800
Echo Lake



Line 2050N - Z Component
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200
(metres)

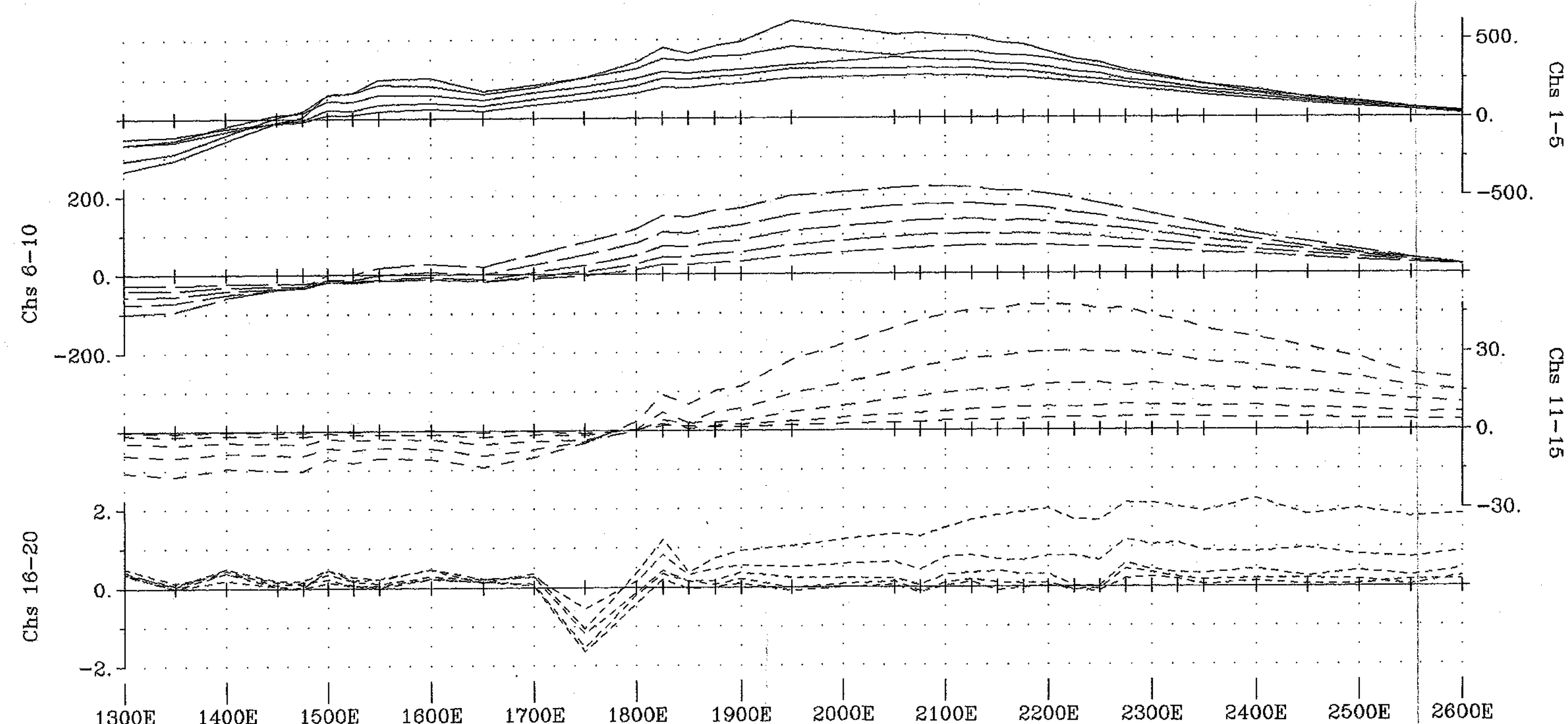
KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N,1100E; 3100N,2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	August 31, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Z-2050N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 2050N - X Component
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200
(metres)

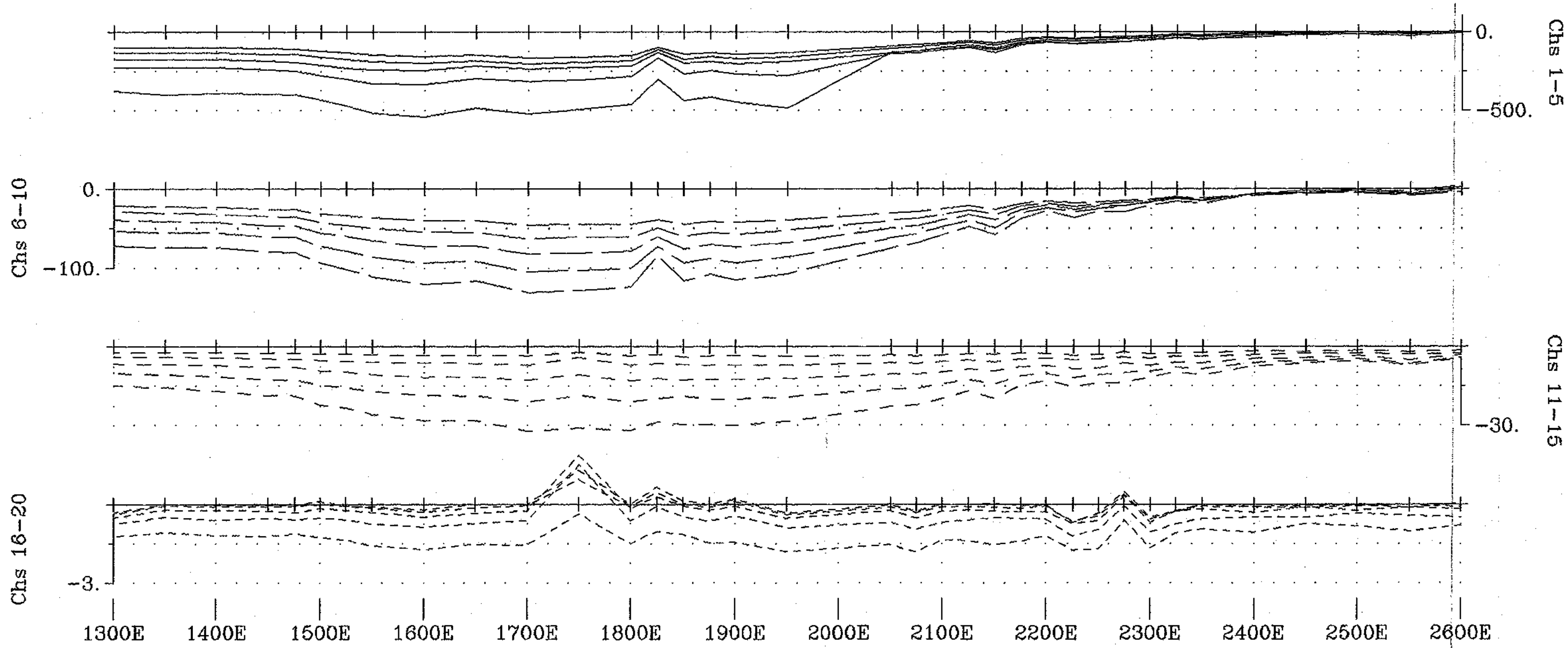
KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N, 1100E; 3100N, 2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	August 31, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-X-2050N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 2050N – Y Component
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200
(metres)

KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N,1100E; 3100N,2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up
	Hx – positive east
	Hy – positive north
Survey Date:	August 31, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Y-2050N

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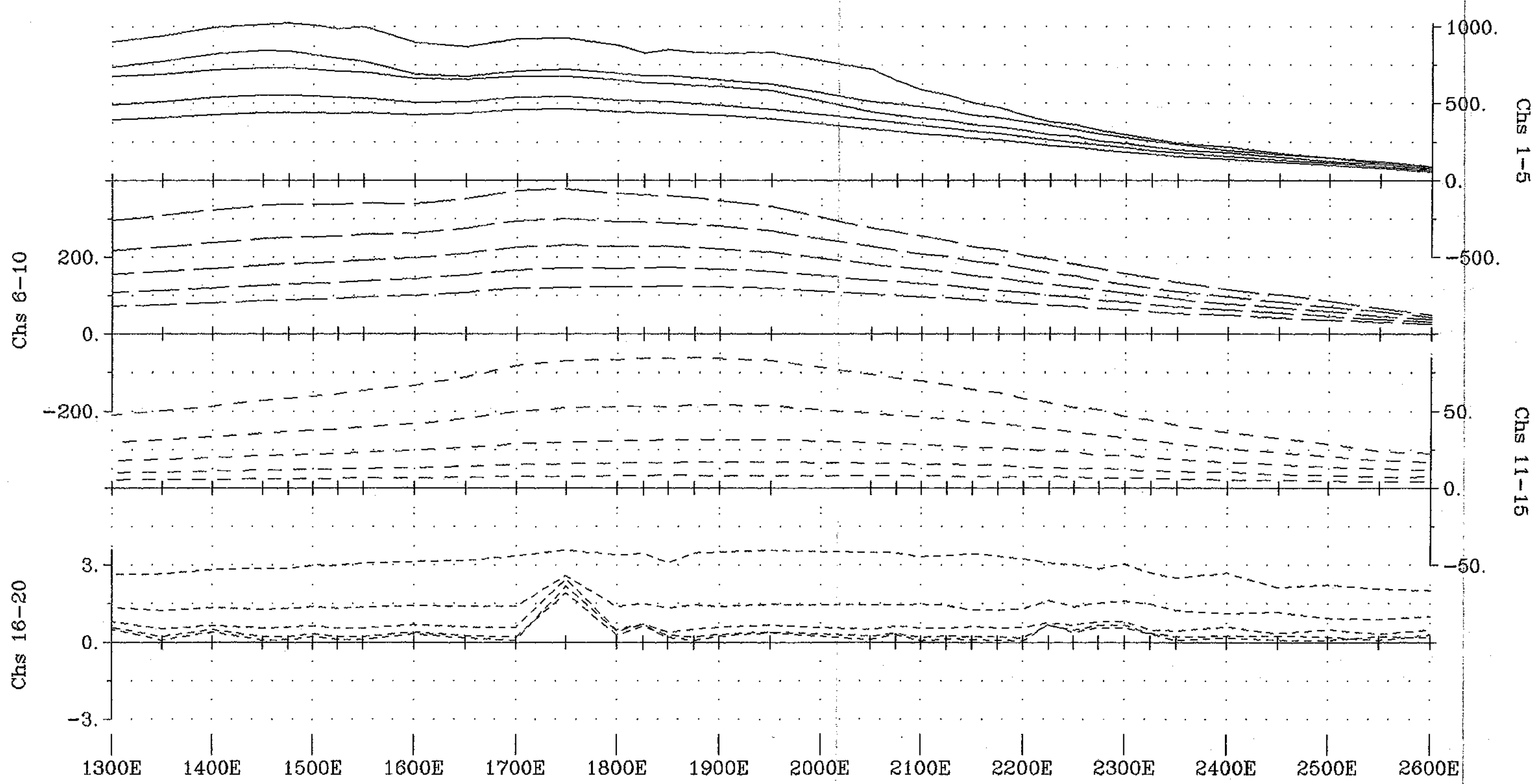


Line 2050N - Total Field
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N,1100E; 3100N,2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	August 31, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

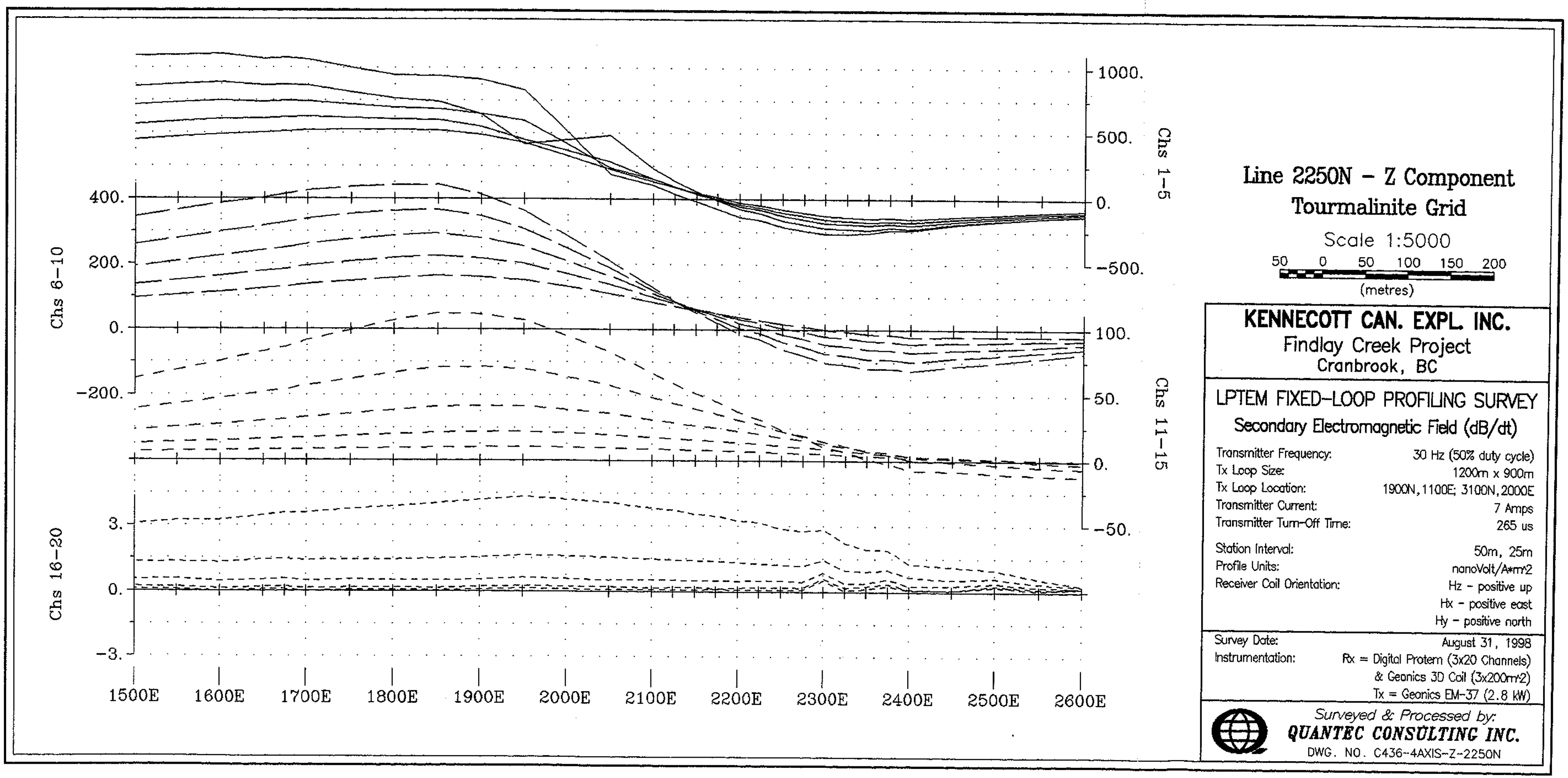
Surveyed & Processed by:

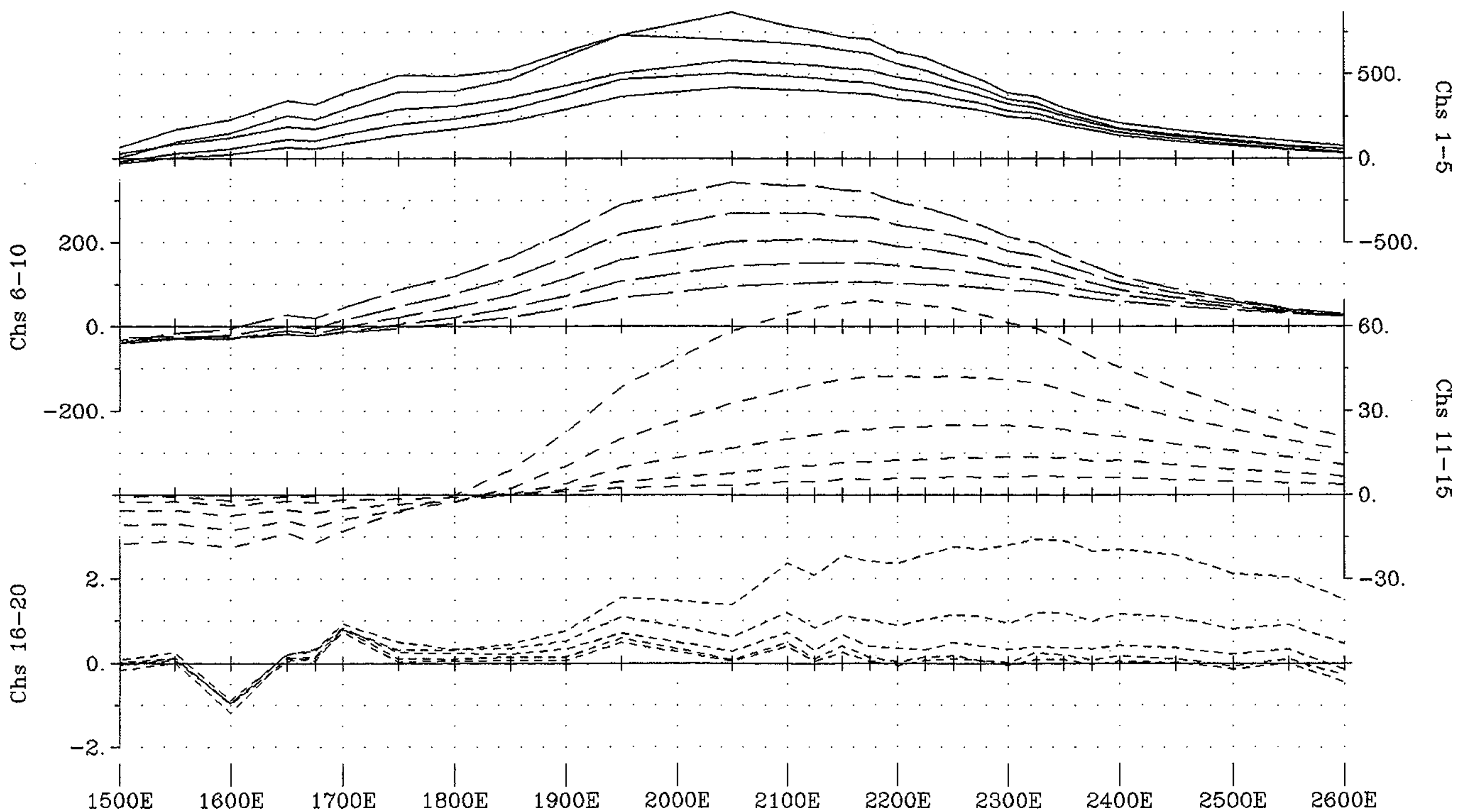
QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-TF-2050N

Plotted Fri 09-25-1998 @ 17:44:50.81

Plotted Fri 09-25-1998 @ 17:44:50.81





Line 2250N - X Component
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200
(metres)

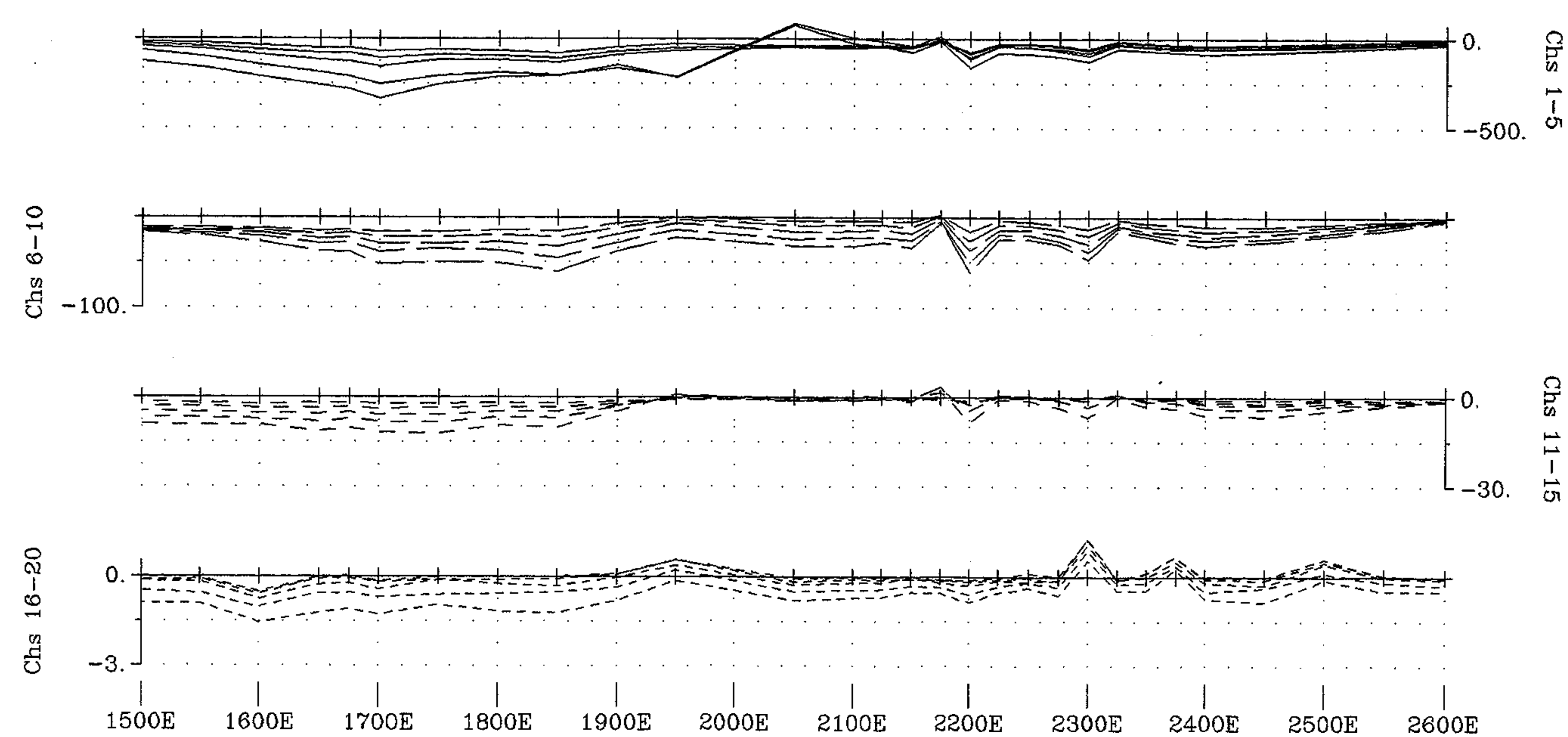
KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N,1100E; 3100N,2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	August 31, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-X-2250N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 2250N – Y Component
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

Secondary Electromagnetic Field (dB/dt)

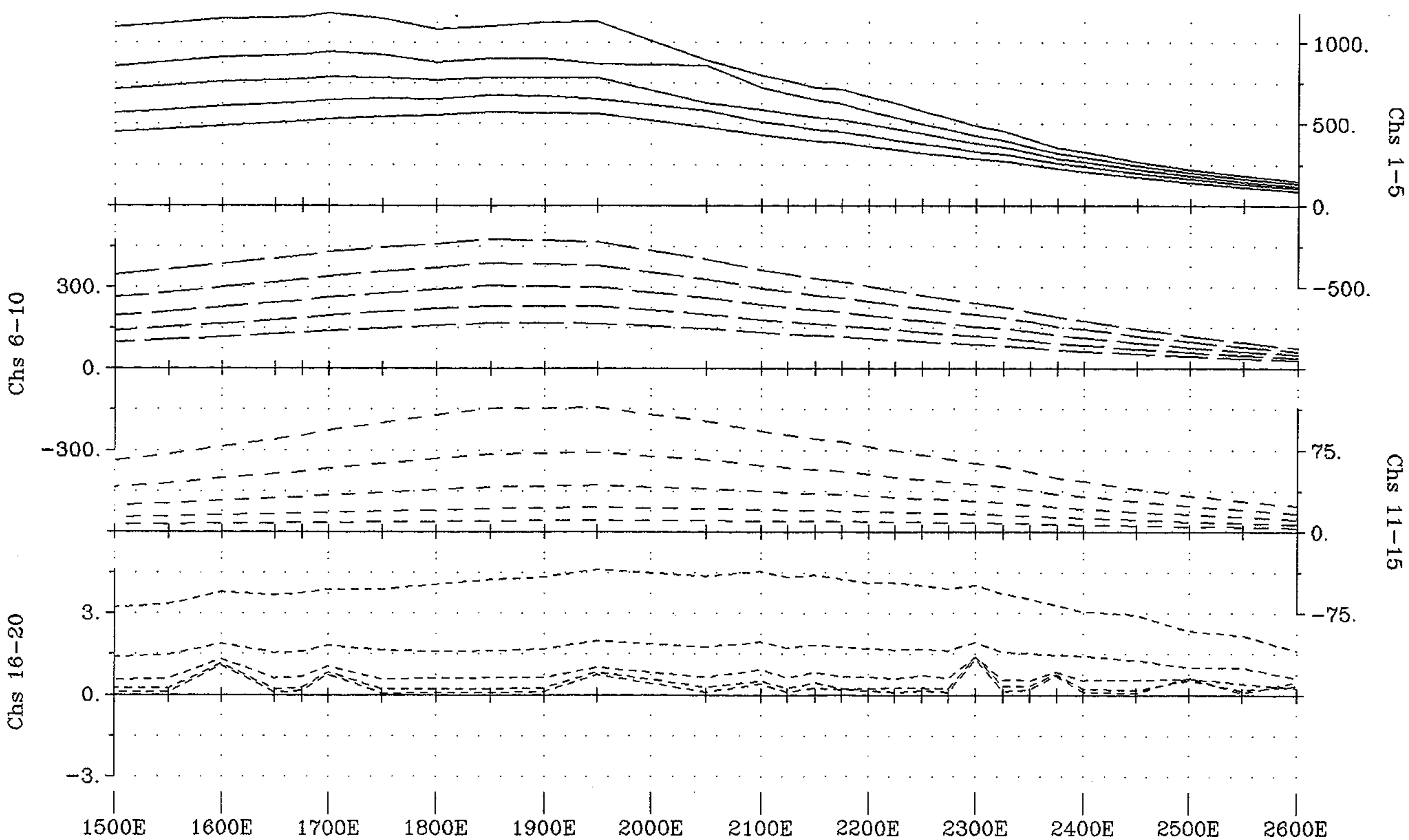
Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N,1100E; 3100N,2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up Hx – positive east Hy – positive north
Survey Date:	August 31, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-Y-2250N

Plotted Fri 09-25-1998 @ 17:44:50.81



Plotted Fri 09-25-1998 @ 17:44:50.81

Line 2250N - Total Field
Tourmalinite Grid

Scale 1:5000

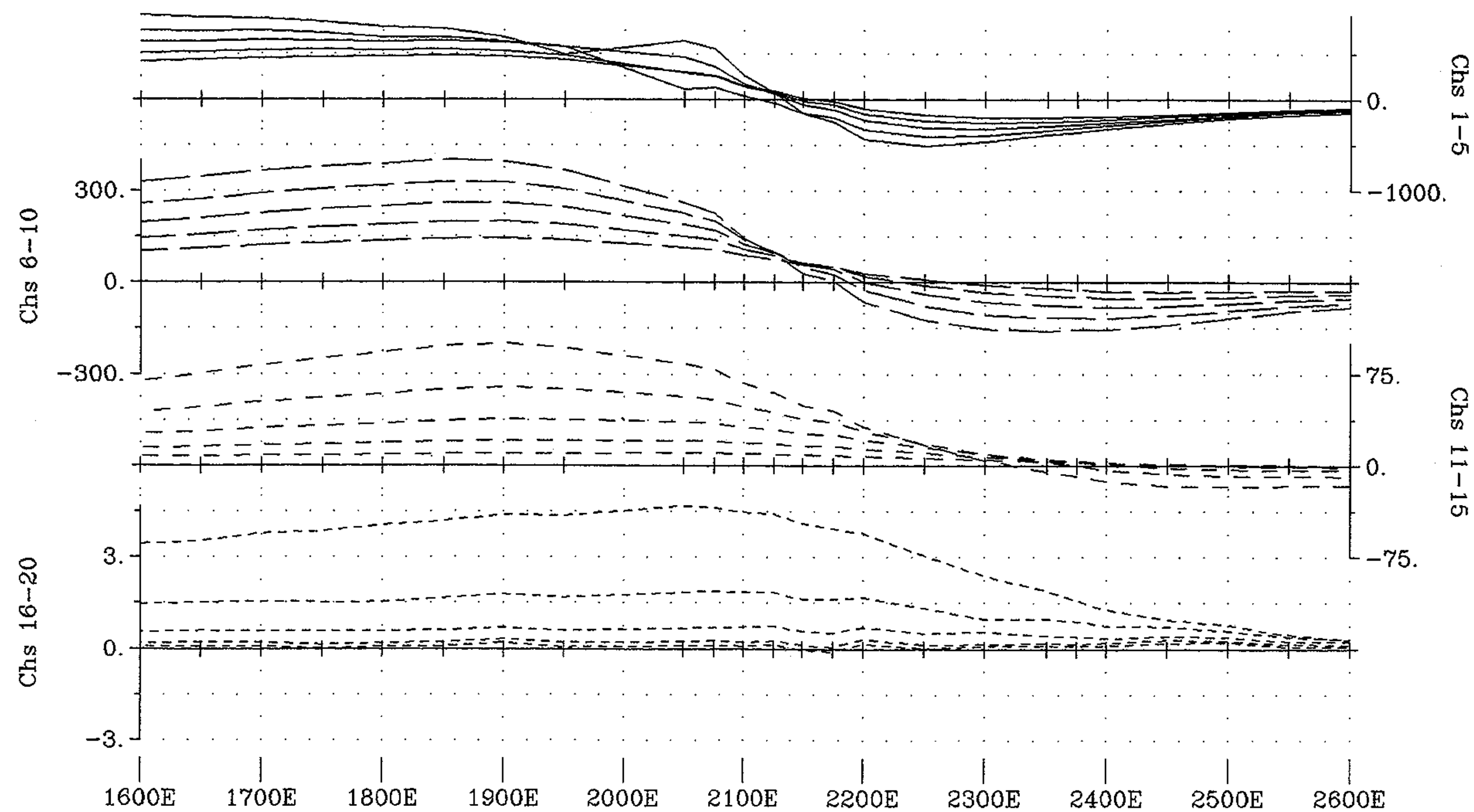
50 0 50 100 150 200
(metres)

KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N,1100E; 3100N,2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	August 31, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-TF-2250N



Line 2450N - Z Component
Tourmalinite Grid
Scale 1:5000
50 0 50 100 150 200
(metres)

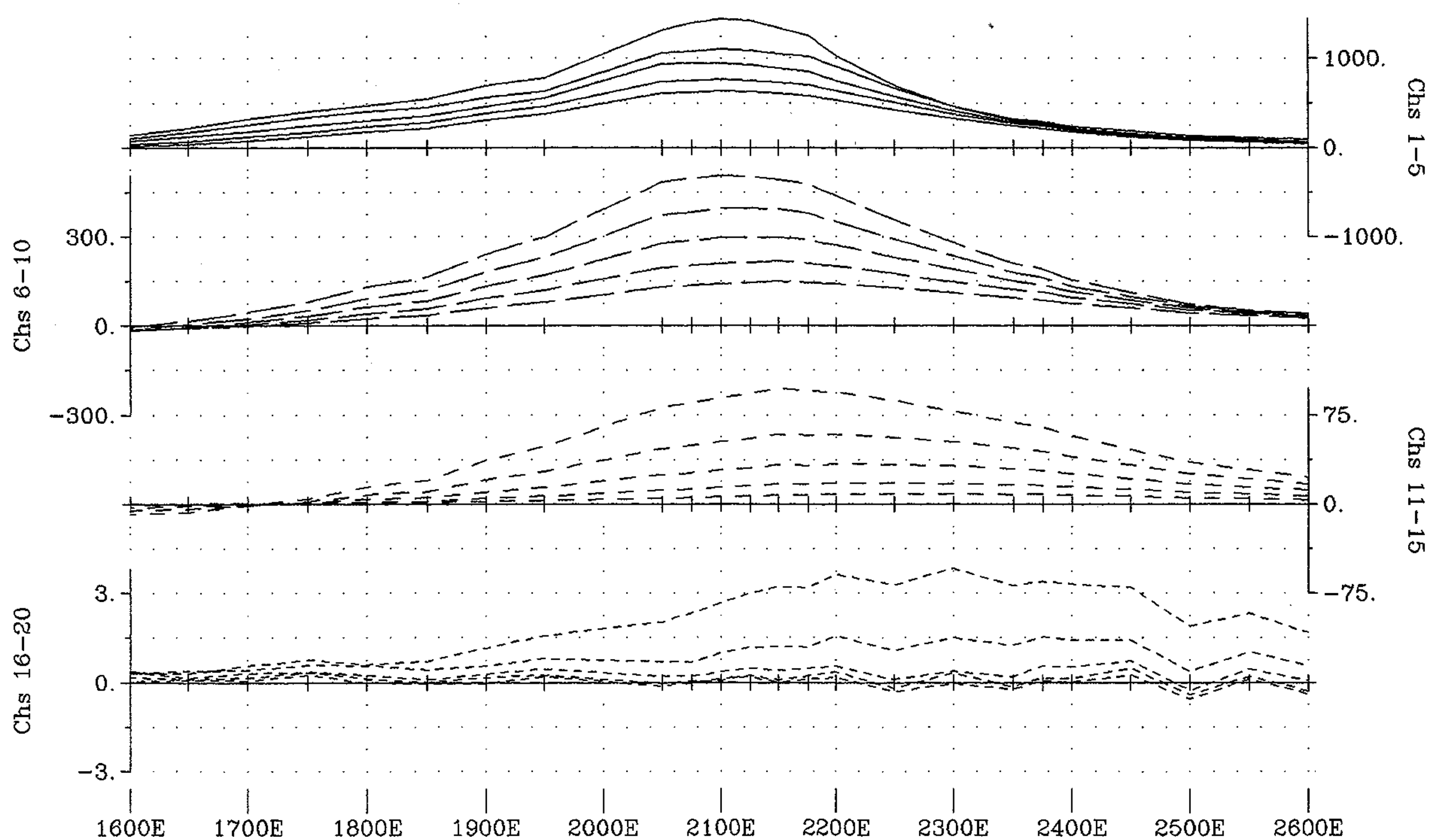
KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N, 1100E; 3100N, 2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 1, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Z-2450N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 2450N – X Component
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200
(metres)

KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

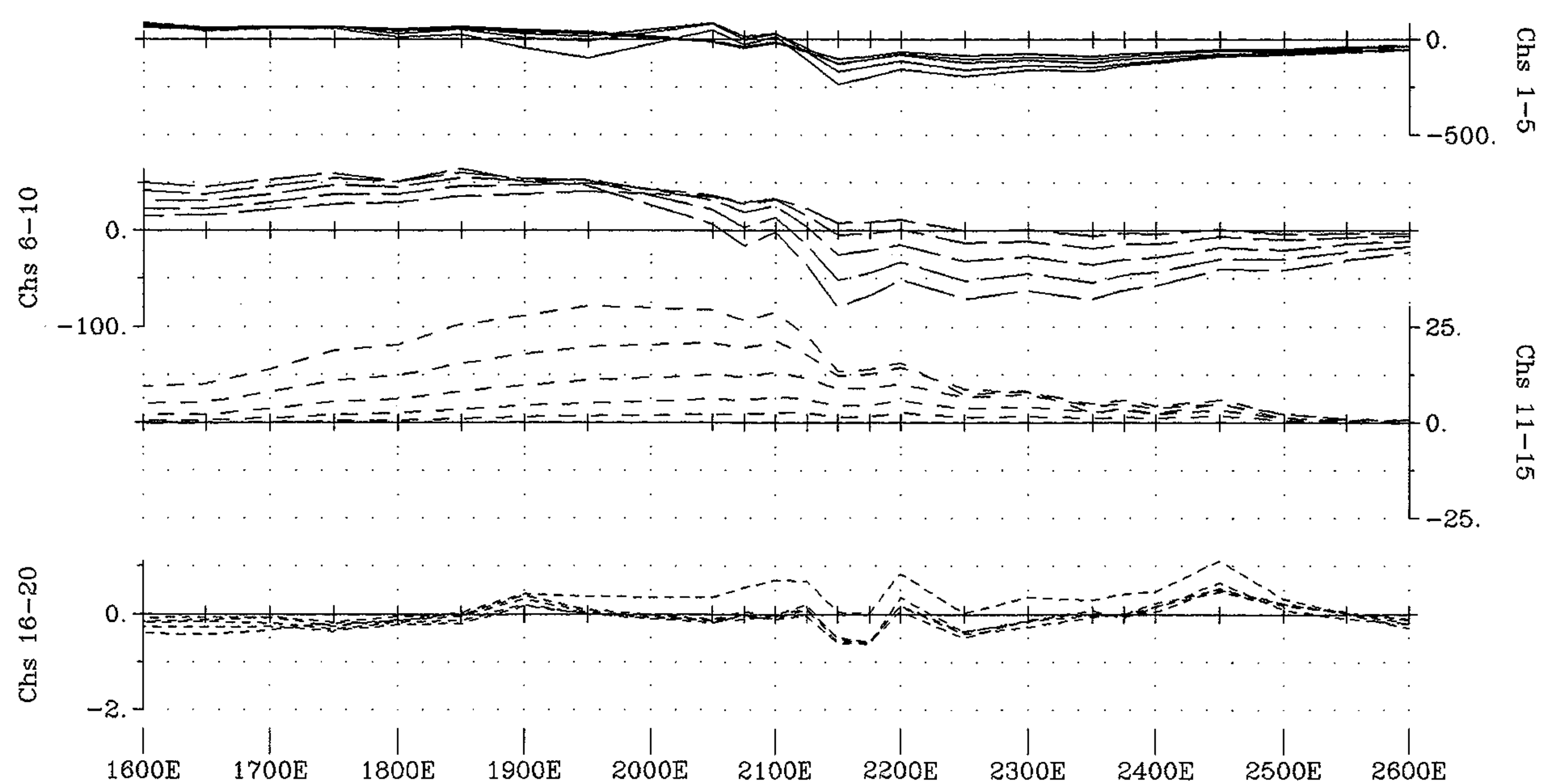
LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N,1100E; 3100N,2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up
	Hx – positive east
	Hy – positive north
Survey Date:	September 1, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-X-2450N

Plotted Fri 09-25-1998 @ 17:44:50.81

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 2450N - Y Component
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

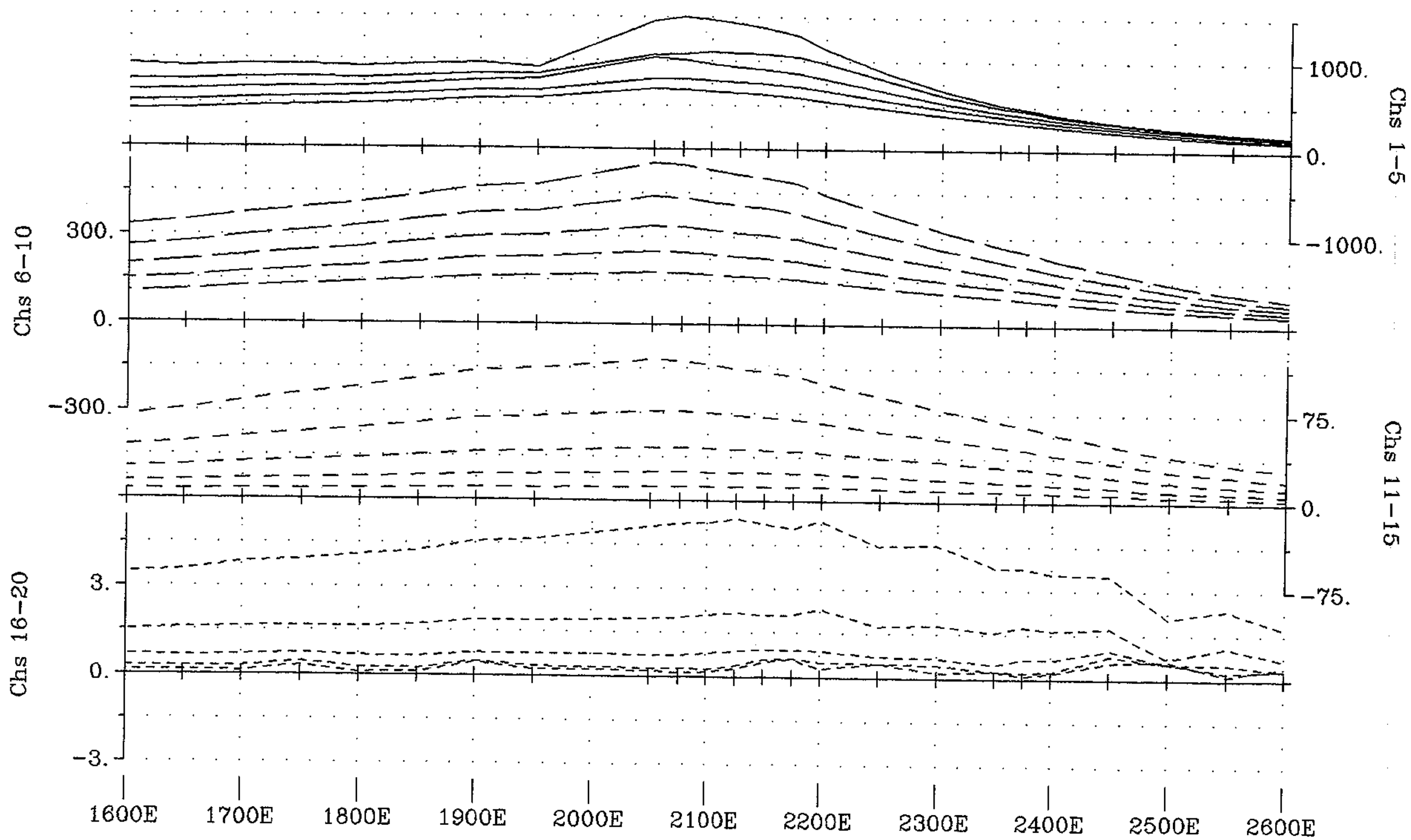
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N,1100E; 3100N,2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 1, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-Y-2450N



Line 2450N – Total Field
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

Secondary Electromagnetic Field (dB/dt)

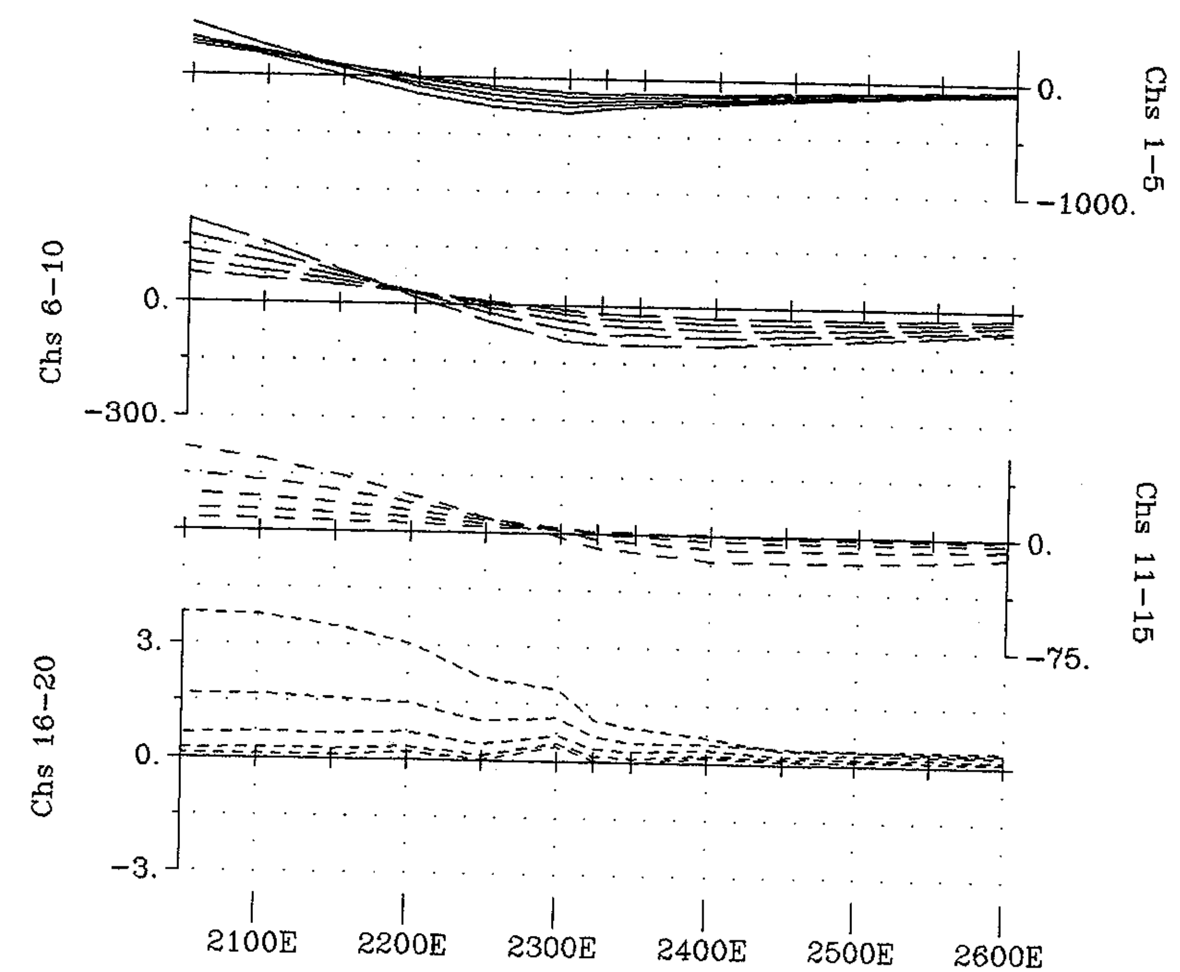
Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N, 1100E; 3100N, 2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up
	Hx – positive east
	Hy – positive north
Survey Date:	September 1, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-TF-2450N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 2650N – Z Component
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200
(metres)

KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

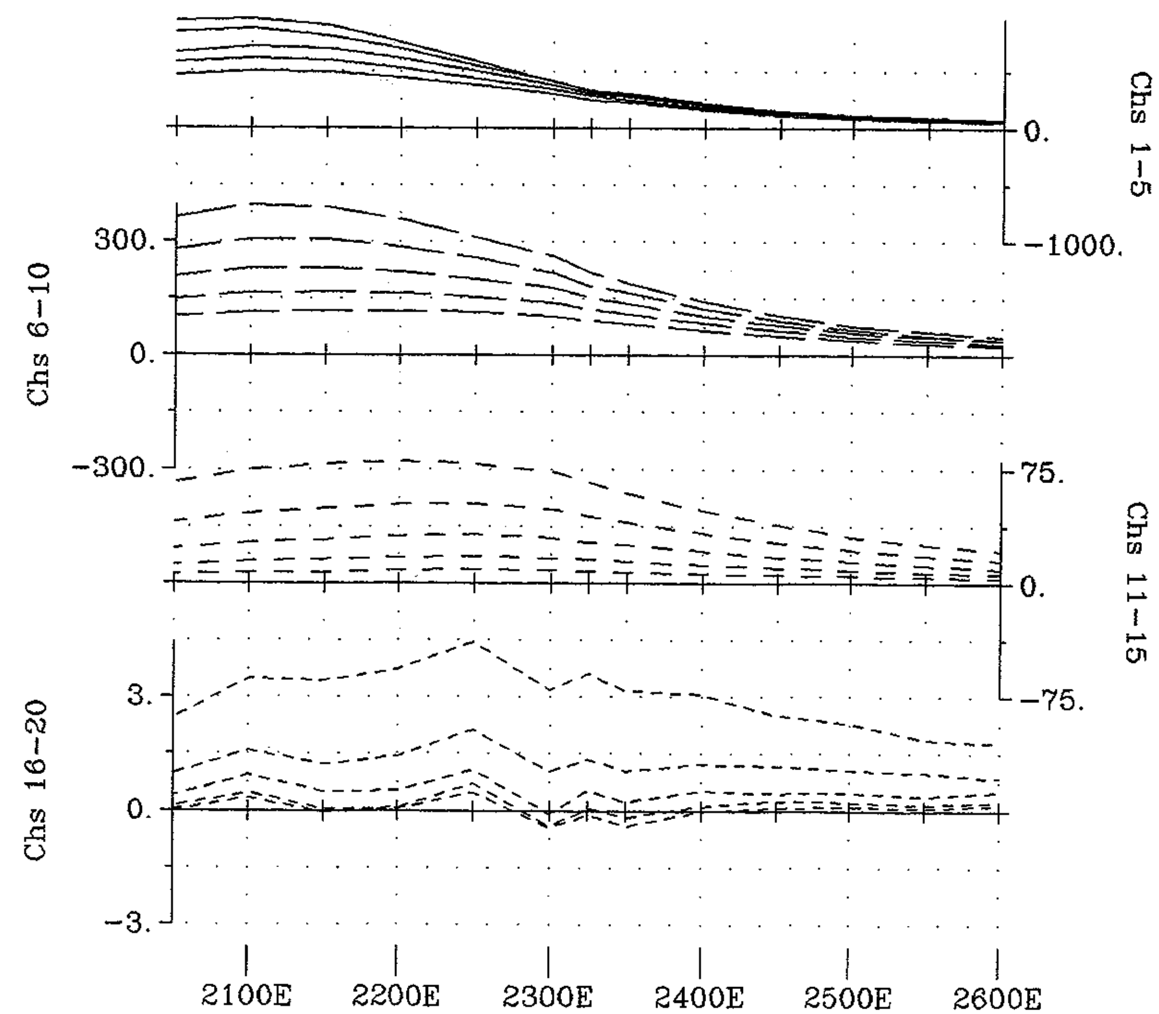
LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N, 1100E; 3100N, 2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up
	Hx – positive east
	Hy – positive north
Survey Date:	September 2, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Z-2650N

Plotted Fri 09-25-1998 @ 17:44:50.81

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 2650N – X Component
Tourmalinite Grid

Scale 1:5000

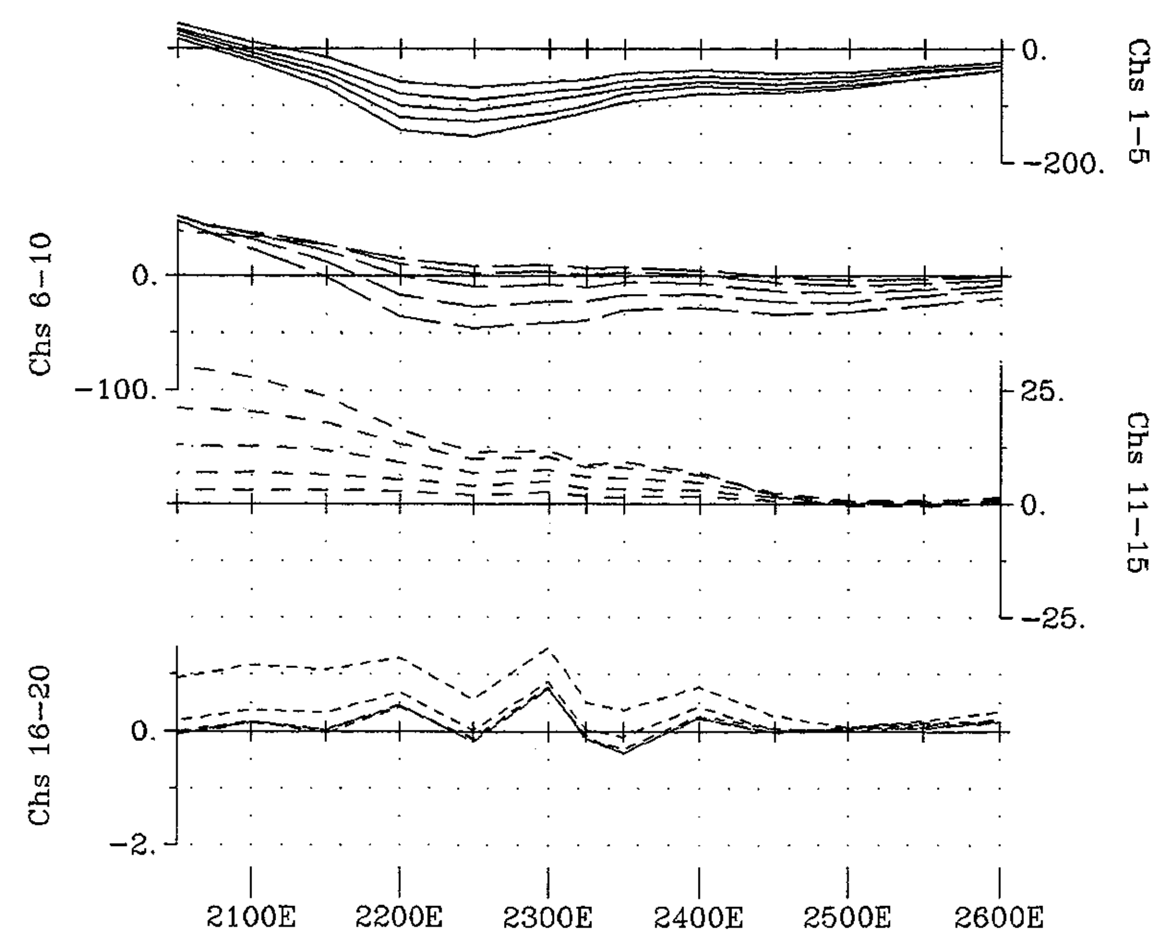
50 0 50 100 150 200
(metres)

KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N,1100E; 3100N,2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up Hx – positive east Hy – positive north
Survey Date:	September 2, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-X-2650N



Plotted Fri 09-25-1998 @ 17:44:50.81

Line 2650N – Y Component

Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

Secondary Electromagnetic Field (dB/dt)

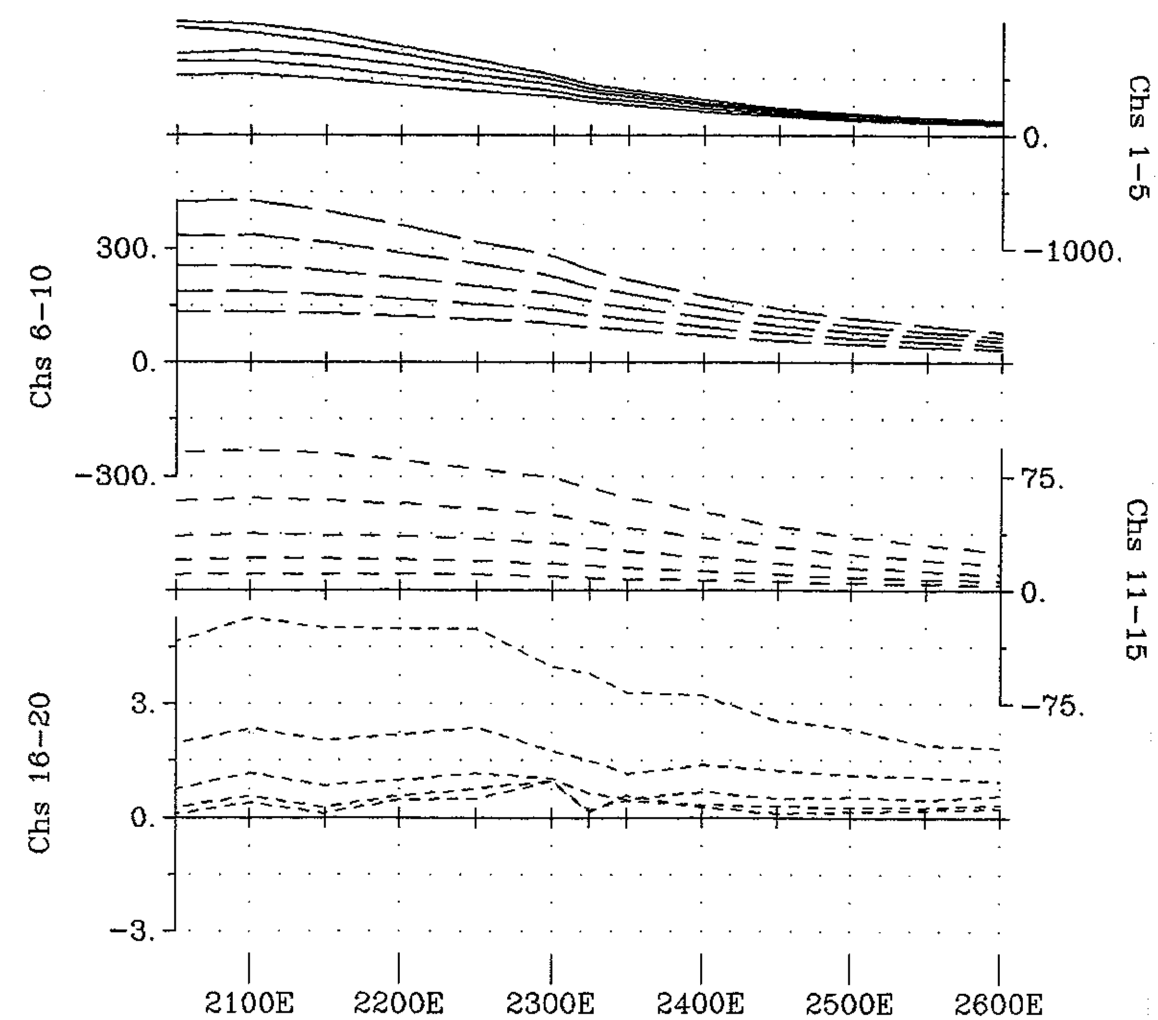
Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N, 1100E; 3100N, 2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up
	Hx – positive east
	Hy – positive north
Survey Date:	September 2, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-Y-2650N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 2650N - Total Field
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

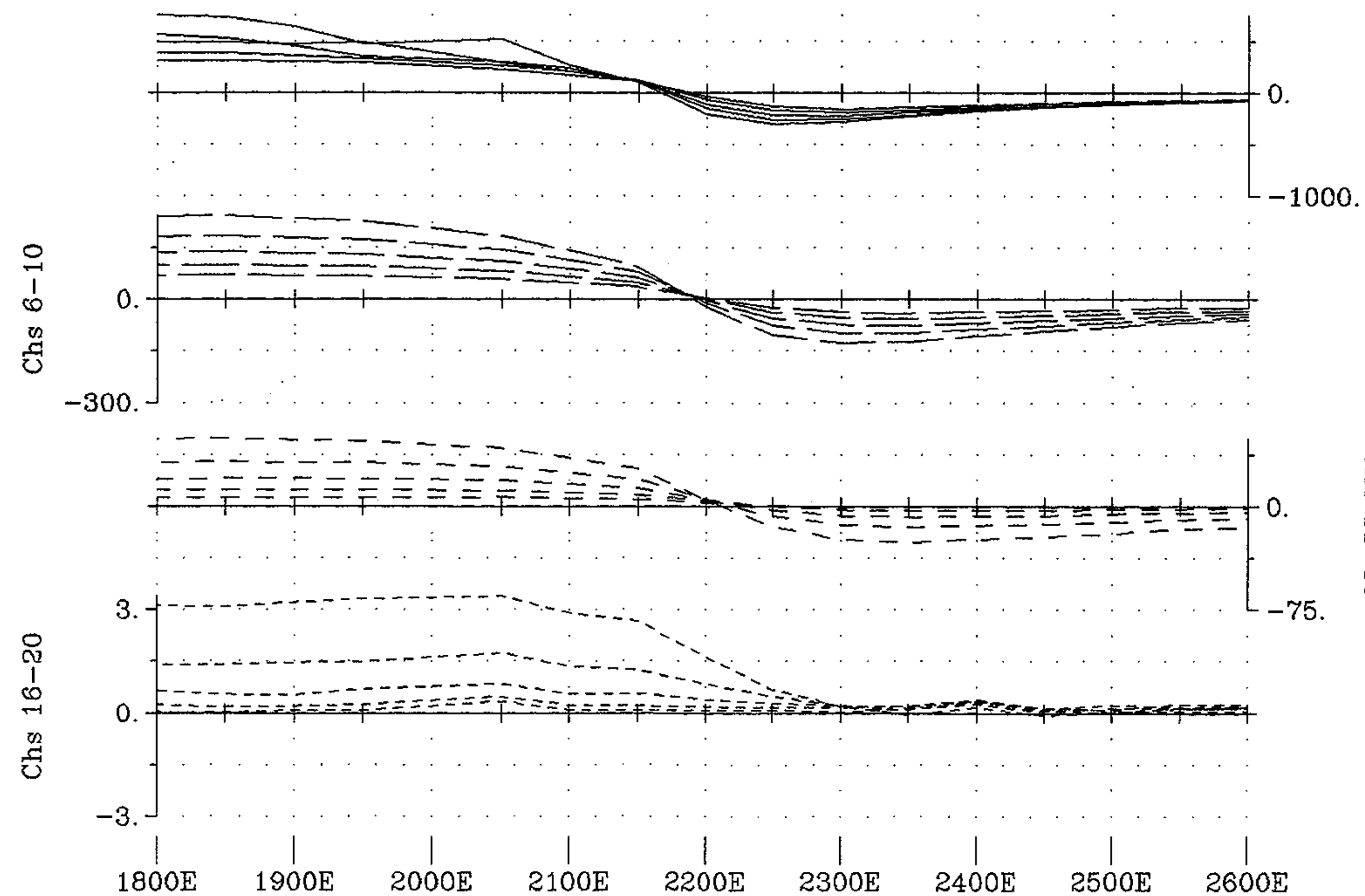
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N,1100E; 3100N,2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 2, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-TF-2650N



Line 2850N - Z Component
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200
(metres)

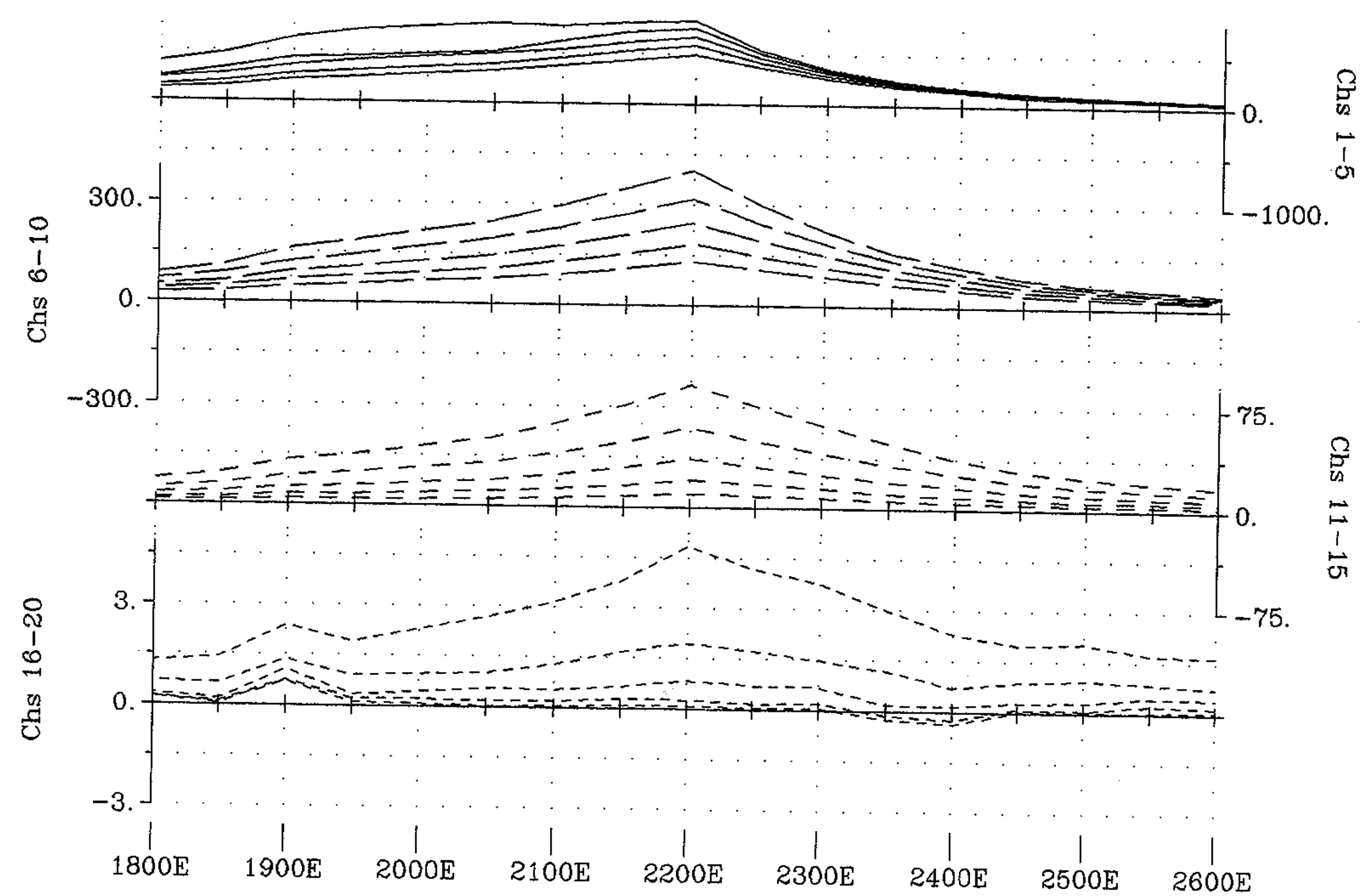
KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N,1100E; 3100N,2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	September 1, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Z-2850N

Plotted Fri 09-25-1998 @ 17:44:50.81



Plotted Fri 09-25-1998 @ 17:44:50.81

Line 2850N - X Component
Tourmalinite Grid

Scale 1:5000

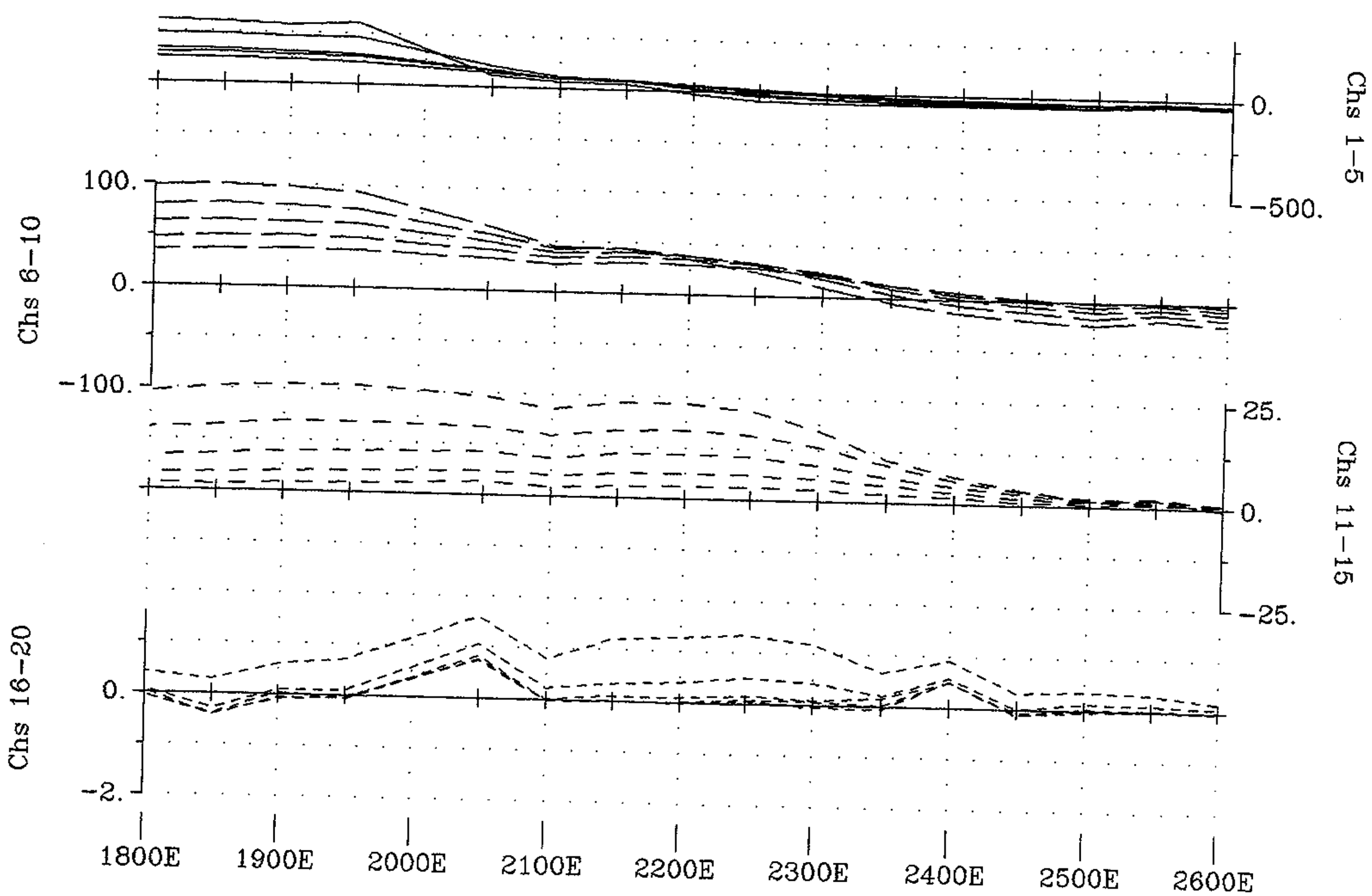
50 0 50 100 150 200
(metres)

KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N, 1100E; 3100N, 2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	September 1, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-X-2850N



Line 2850N – Y Component
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N, 1100E; 3100N, 2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up
	Hx – positive east
	Hy – positive north
Survey Date:	September 1, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

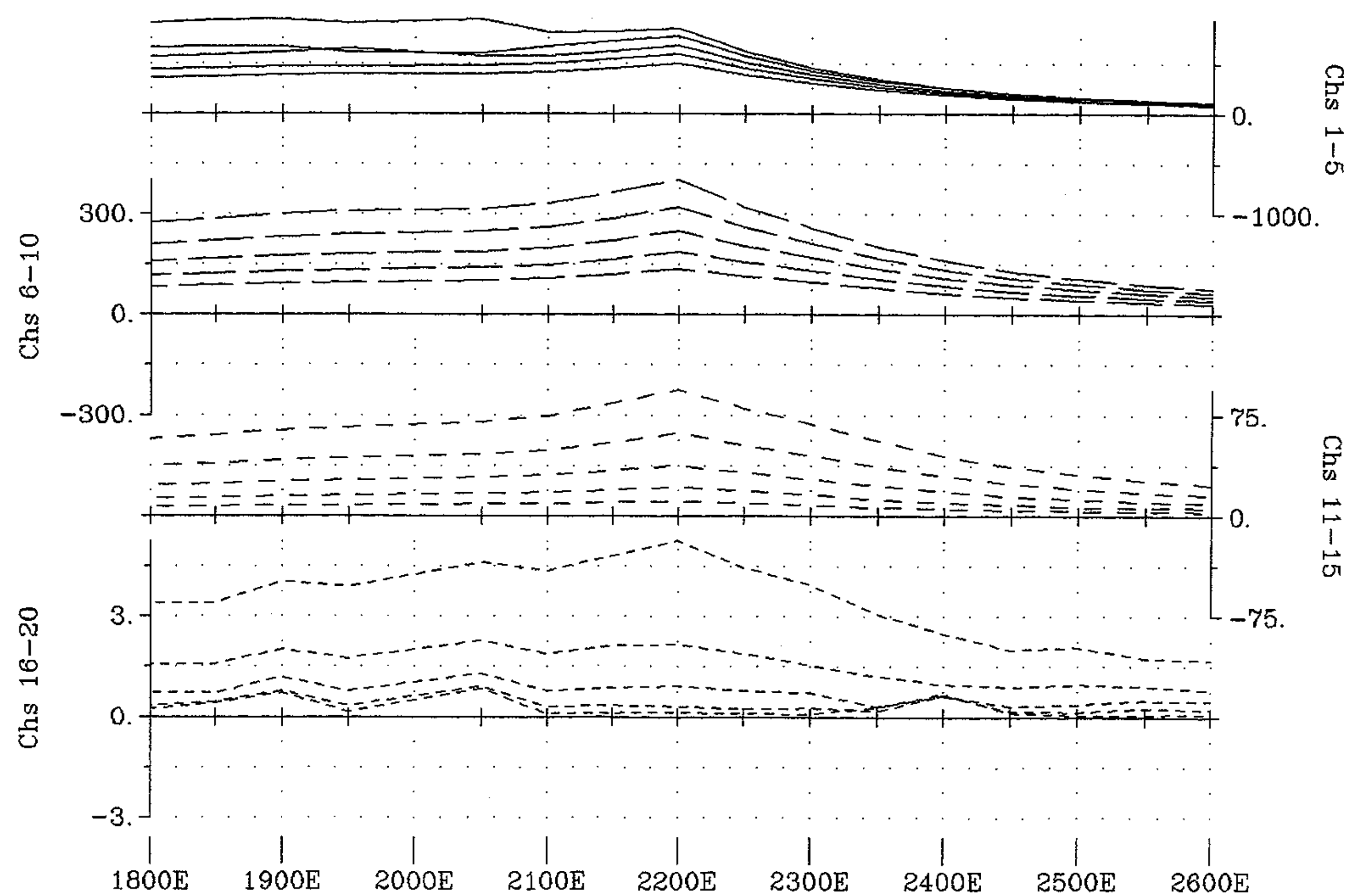
Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-Y-2850N

Plotted Fri 09-25-1998 @ 17:44:50.81

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 2850N – Total Field
Tourmalinite Grid

Scale 1:5000

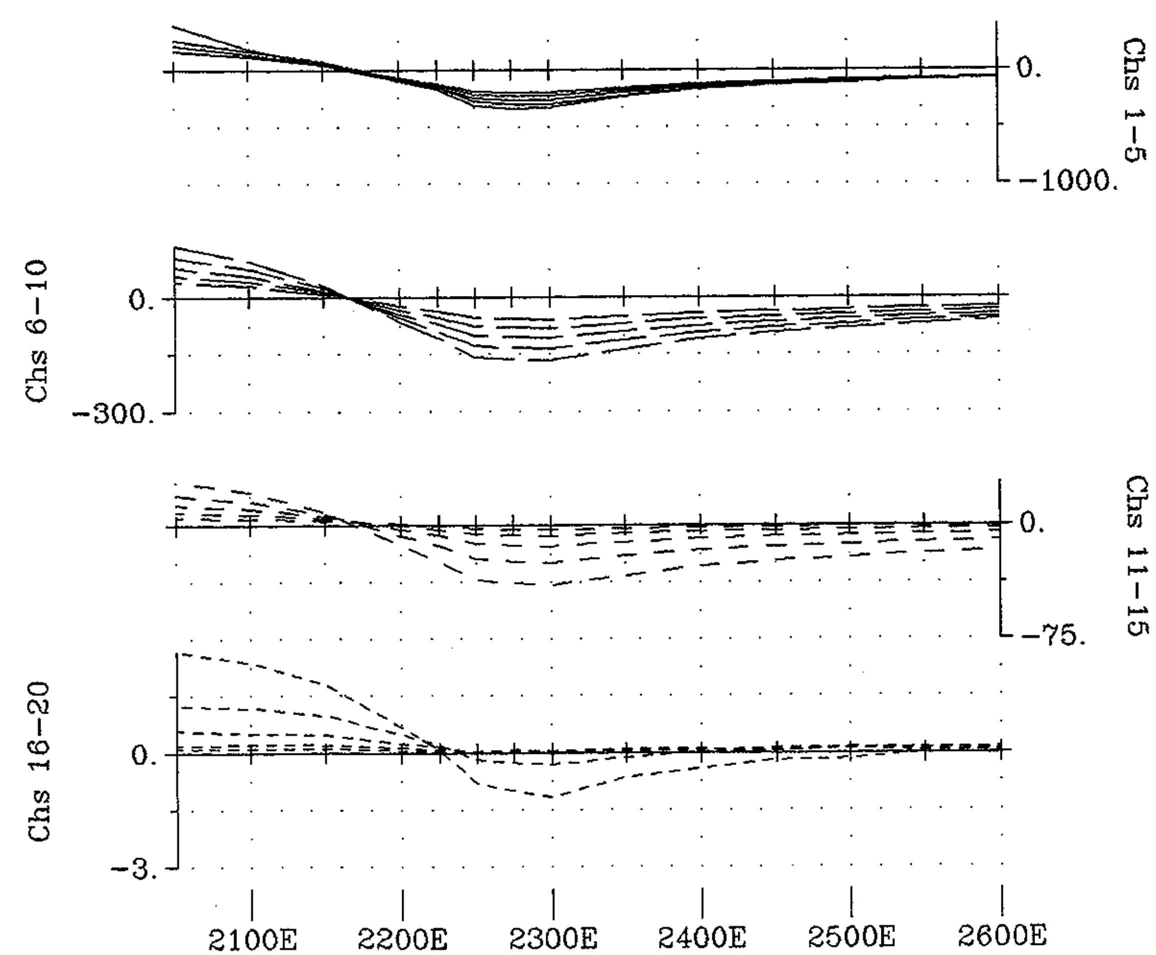
50 0 50 100 150 200
(metres)

KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N, 1100E; 3100N, 2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up
	Hx – positive east
	Hy – positive north
Survey Date:	September 1, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-TF-2850N



Line 3050N – Z Component
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

Secondary Electromagnetic Field (dB/dt)

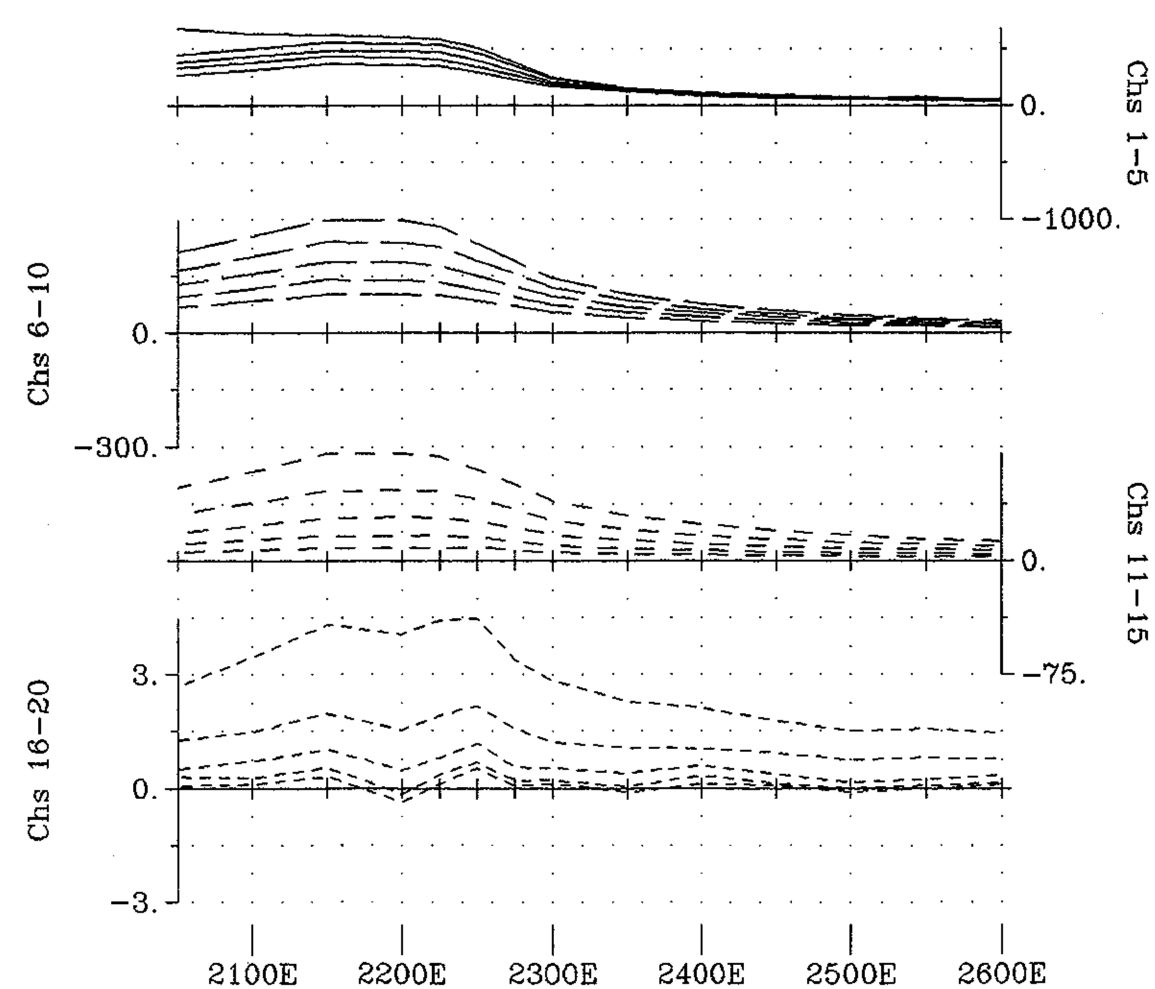
Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N, 1100E; 3100N, 2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up
	Hx – positive east
	Hy – positive north
Survey Date:	September 1, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-Z-3050N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 3050N – X Component
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N, 1100E; 3100N, 2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up
	Hx – positive east
	Hy – positive north
Survey Date:	September 1, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

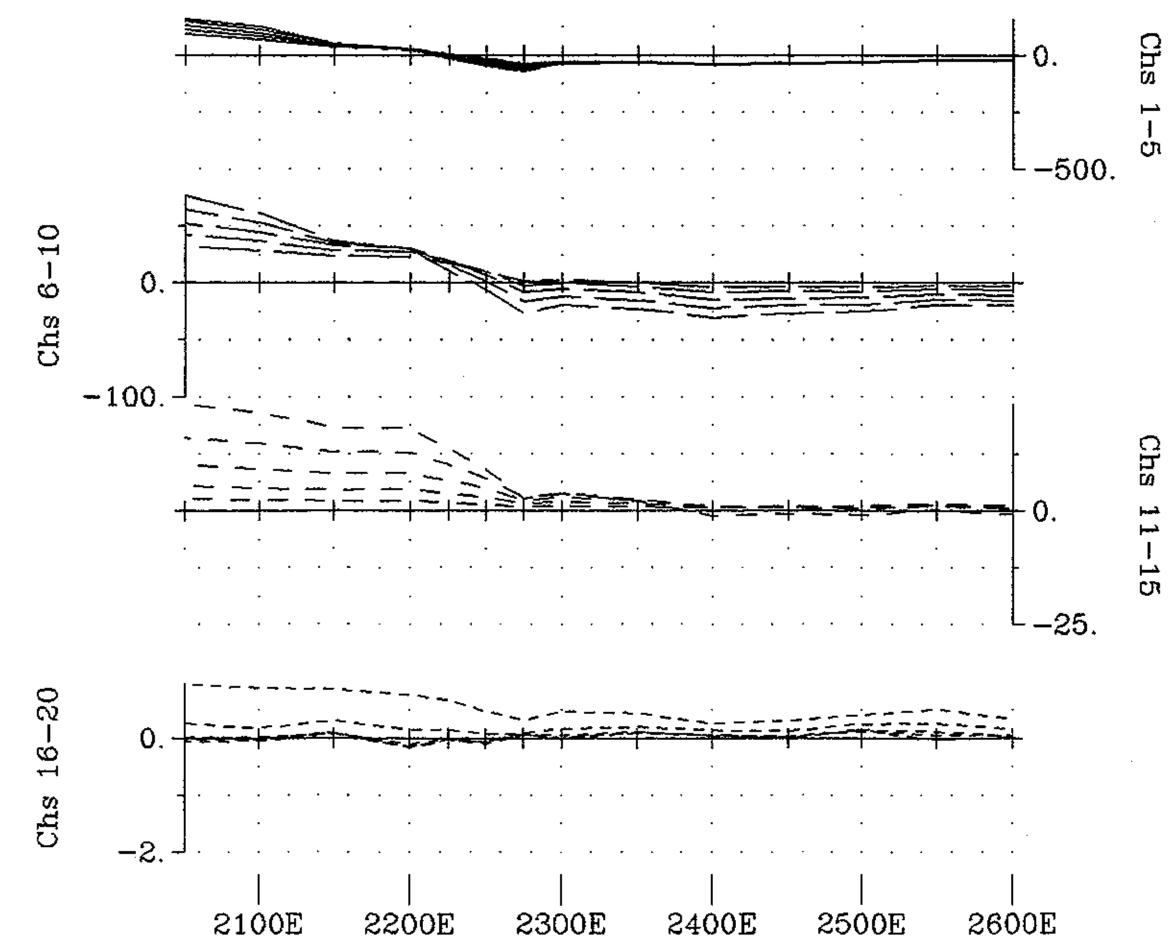
Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-X-3050N

Plotted Fri 09-25-1998 @ 17:44:50.81

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 3050N – Y Component
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

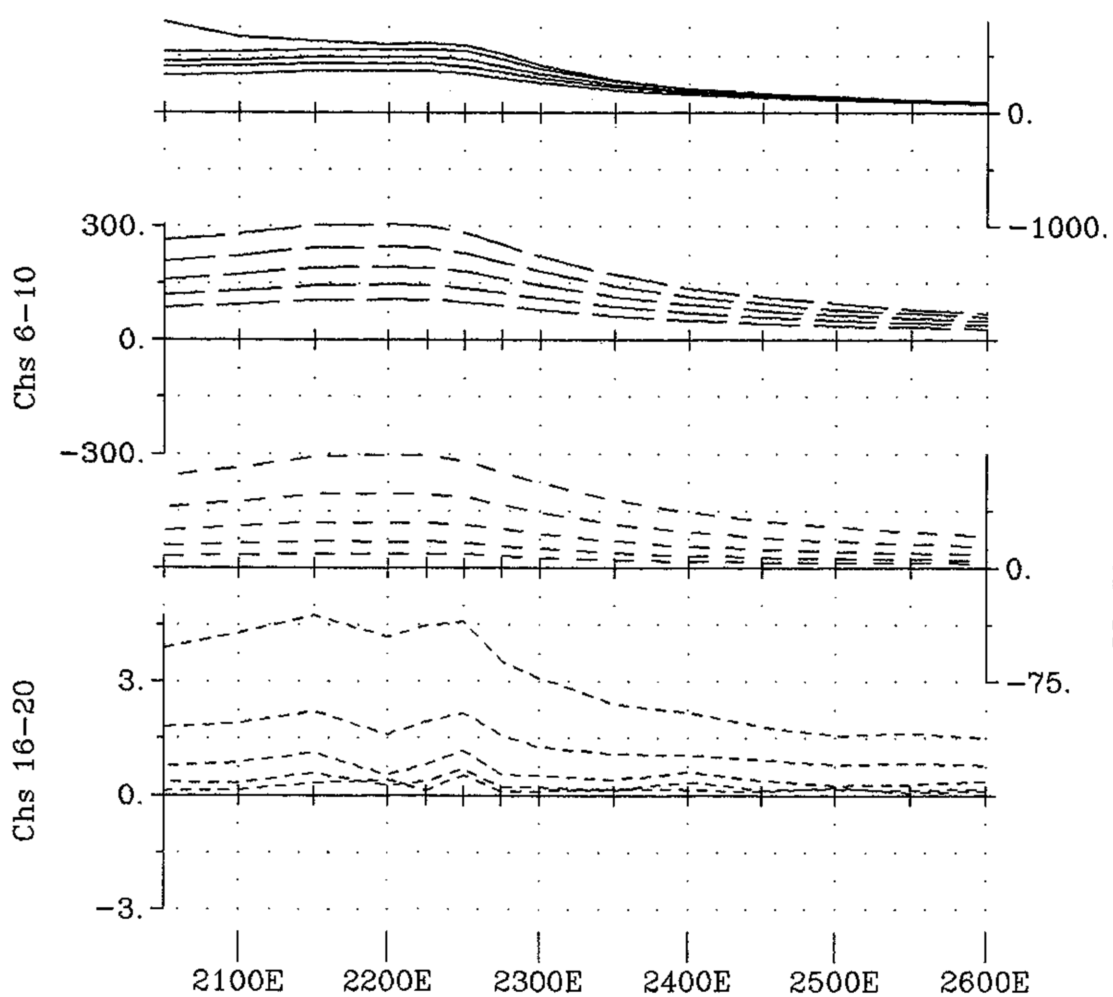
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N, 1100E; 3100N, 2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up
	Hx – positive east
	Hy – positive north
Survey Date:	September 1, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-Y-3050N



Plotted Fri 09-25-1998 @ 17:44:50.81

Line 3050N – Total Field
Tourmalinite Grid

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

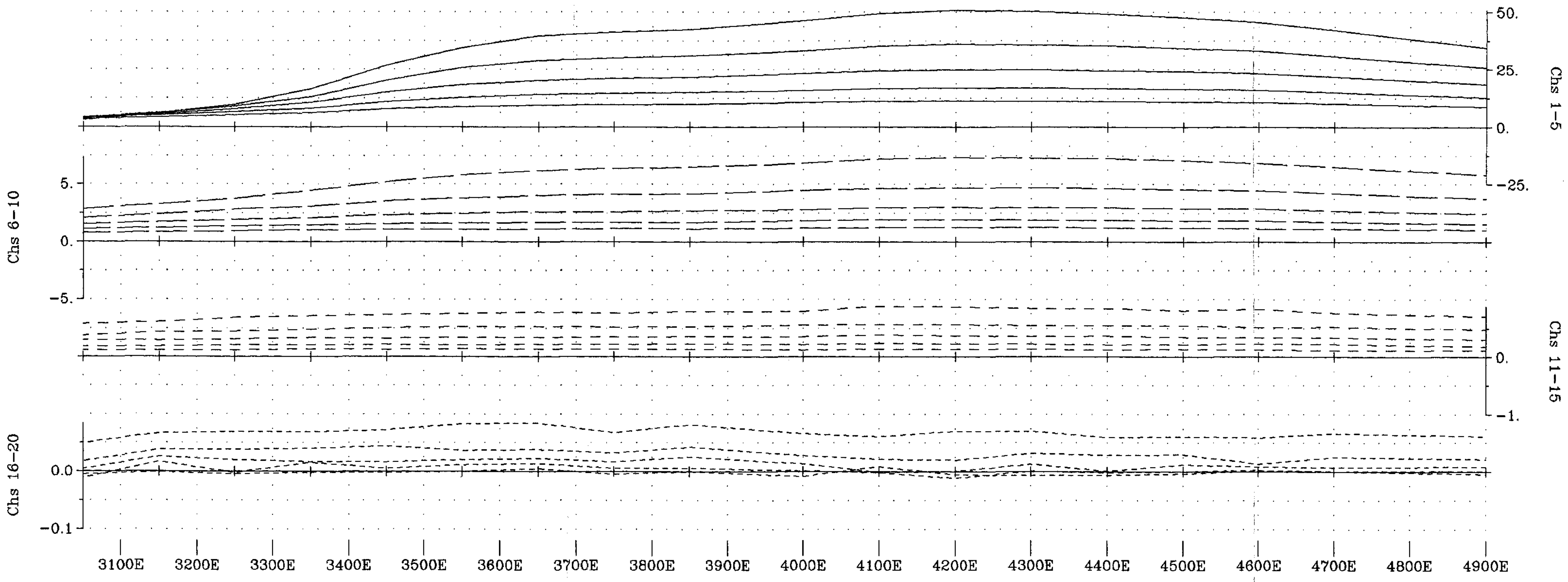
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	30 Hz (50% duty cycle)
Tx Loop Size:	1200m x 900m
Tx Loop Location:	1900N, 1100E; 3100N, 2000E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	265 us
Station Interval:	50m, 25m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up
	Hx – positive east
	Hy – positive north
Survey Date:	September 1, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-TF-3050N



Plotted Fri 09-25-1998 @ 17:44:50.81

Line 11 - Z Component
Cassat Grid-Loop 1

Scale 1:5000

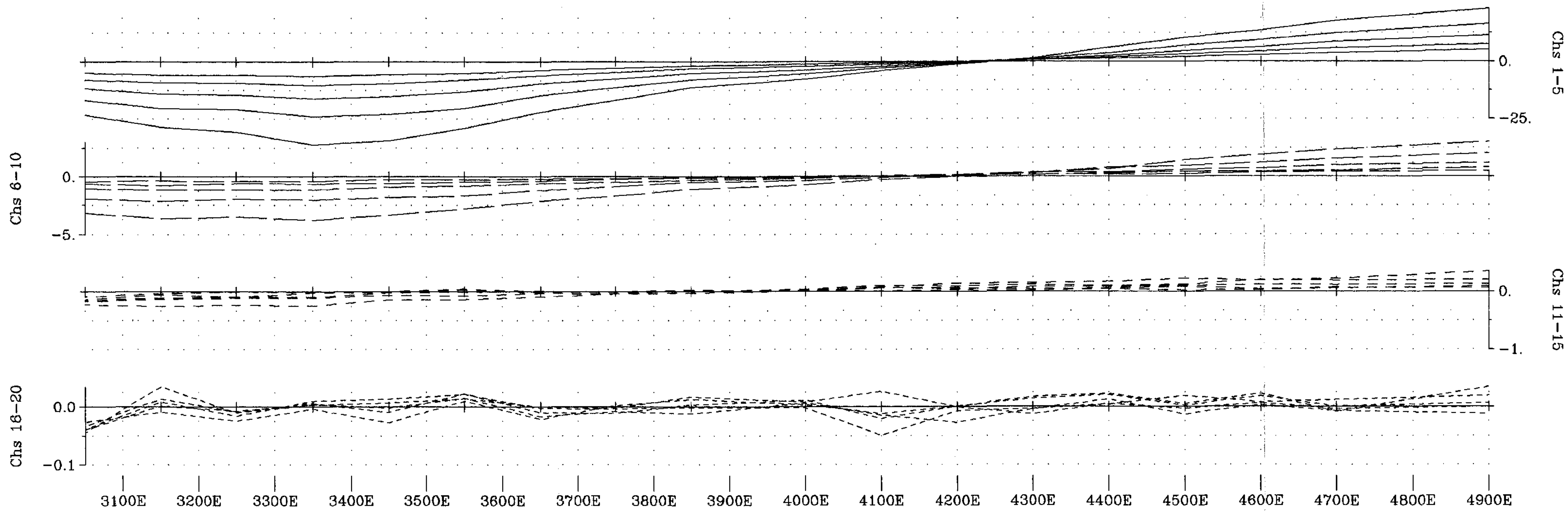
50 0 50 100 150 200
(metres)

Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 750m
Tx Loop Location:	Oval shape; Edges 3950E, 5000E
Transmitter Current:	7.5 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	September 3, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Z-11



Line 11 - X Component

Cassat Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200

(metres)

Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

Secondary Electromagnetic Field (dB/dt)

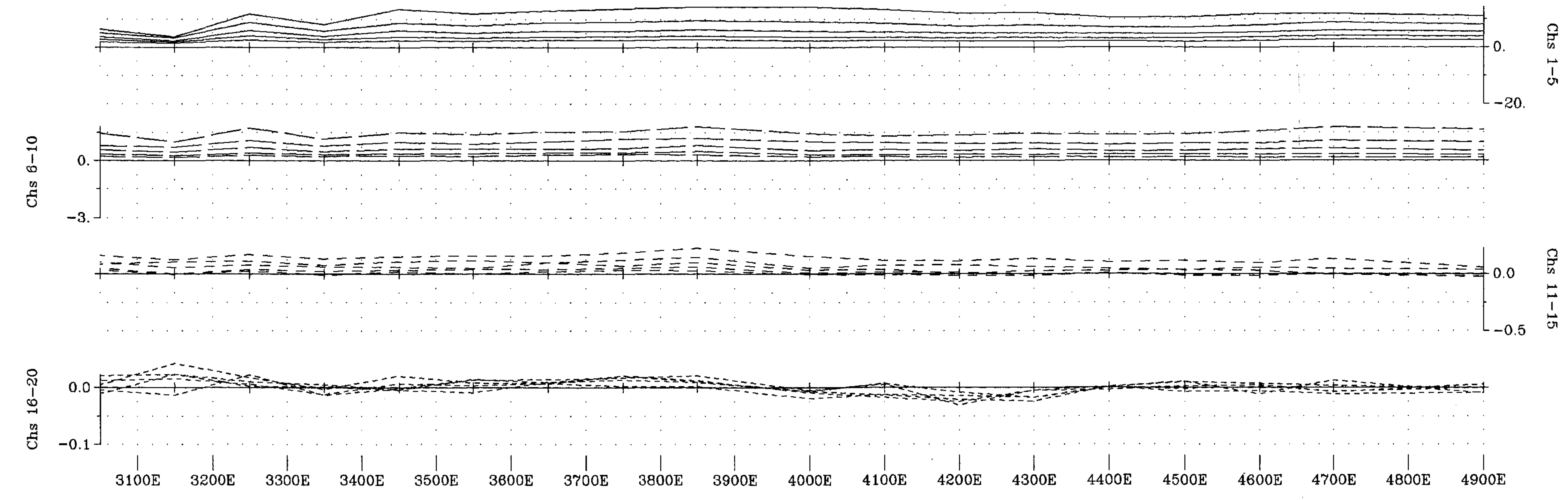
Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 750m
Tx Loop Location:	Oval shape; Edges 3950E, 5000E
Transmitter Current:	7.5 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 3, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-X-11

Plotted Fri 09-25-1998 @ 17:44:50.81



Plotted Fri 09-25-1998 @ 17:44:50.81

Line 11 - Y Component
Cassat Grid-Loop 1

Scale 1:5000

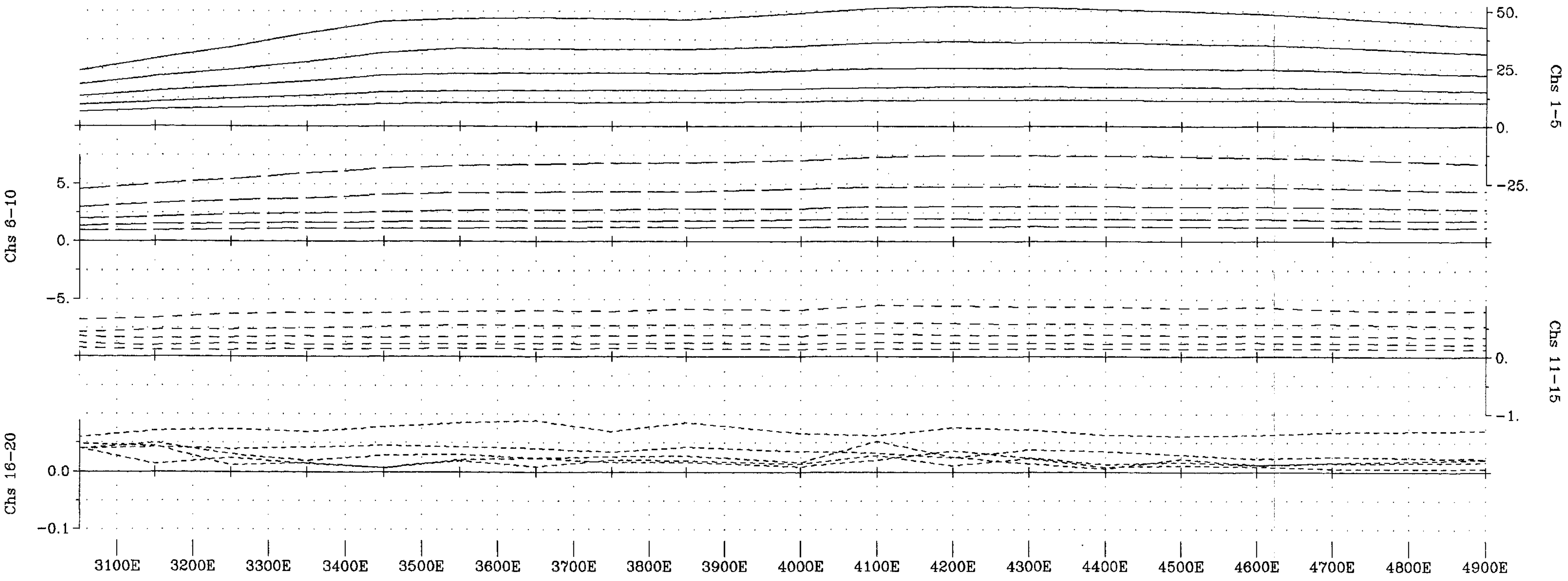
50 0 50 100 150 200
(metres)

KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 750m
Tx Loop Location:	Oval shape; Edges 3950E, 5000E
Transmitter Current:	7.5 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 3, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Y-11



Line 11 - Total Field
Cassat Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200
(metres)

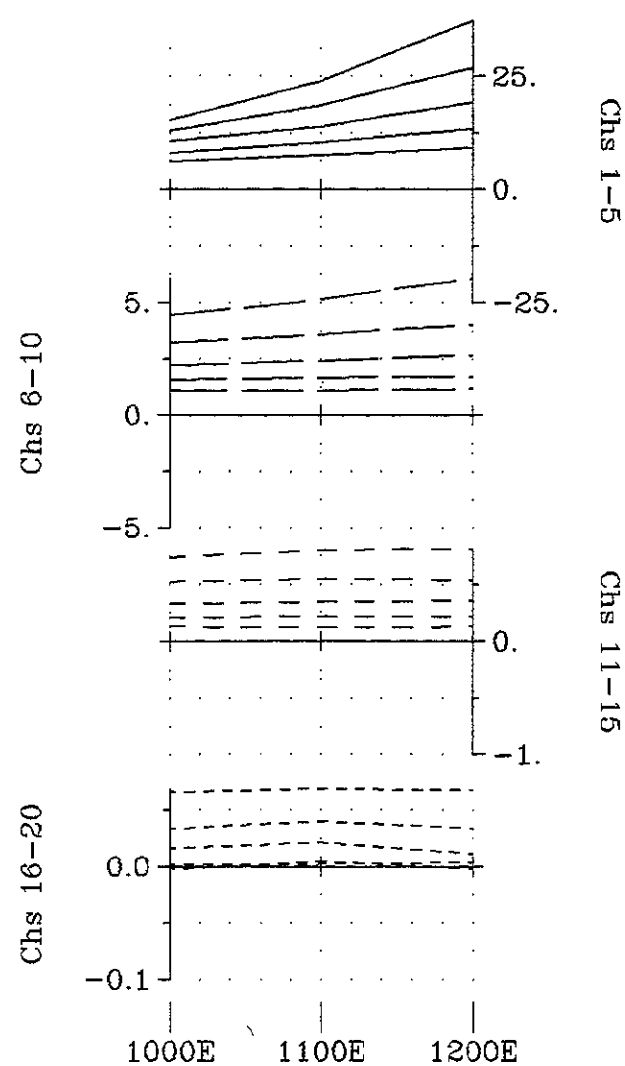
KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 750m
Tx Loop Location:	Oval shape; Edges 3950E, 5000E
Transmitter Current:	7.5 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 3, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-TF-11

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 12 - Z Component
Cassat Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200
(metres)

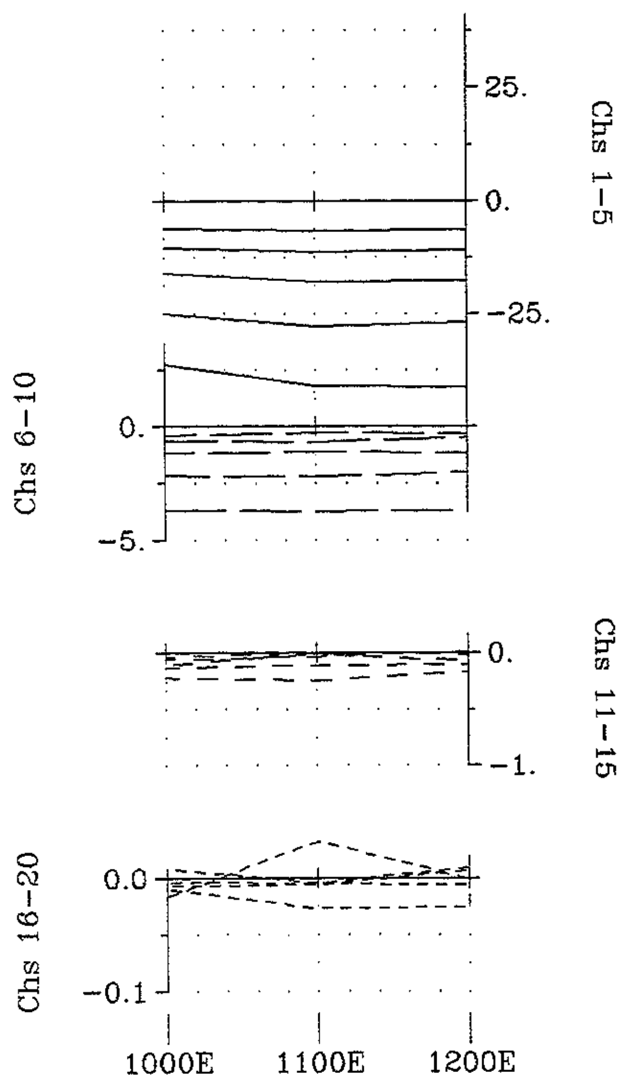
KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 750m
Tx Loop Location:	Oval shape; Edges 3950E, 5000E
Transmitter Current:	7.5 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	September 3, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Z-12

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 12 - X Component
Cassat Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200
(metres)

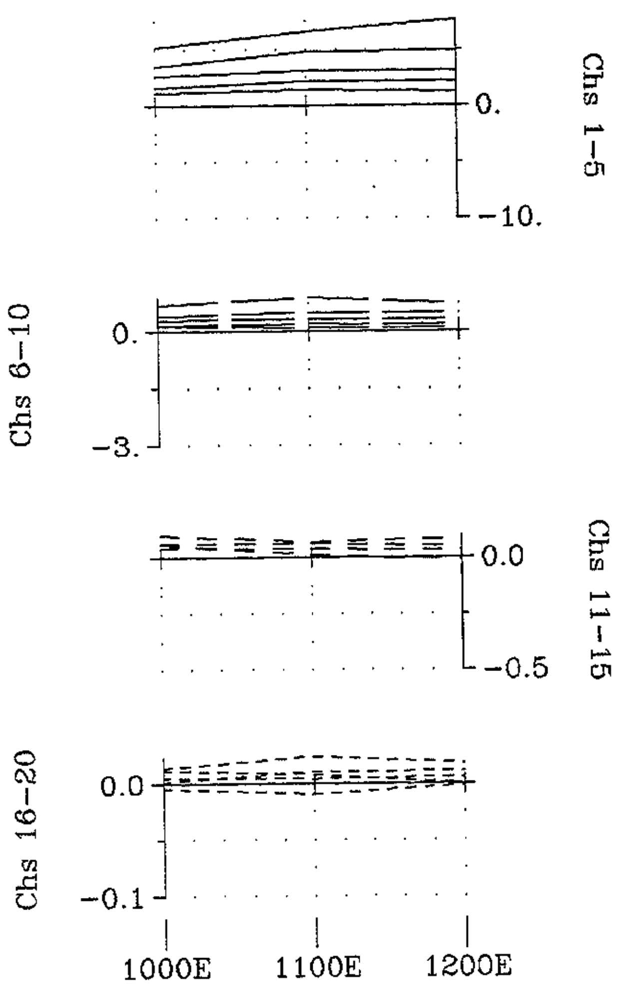
KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 750m
Tx Loop Location:	Oval shape; Edges 3950E, 5000E
Transmitter Current:	7.5 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 3, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-X-12

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 12 - Y Component
Cassat Grid-Loop 1

Scale 1:5000

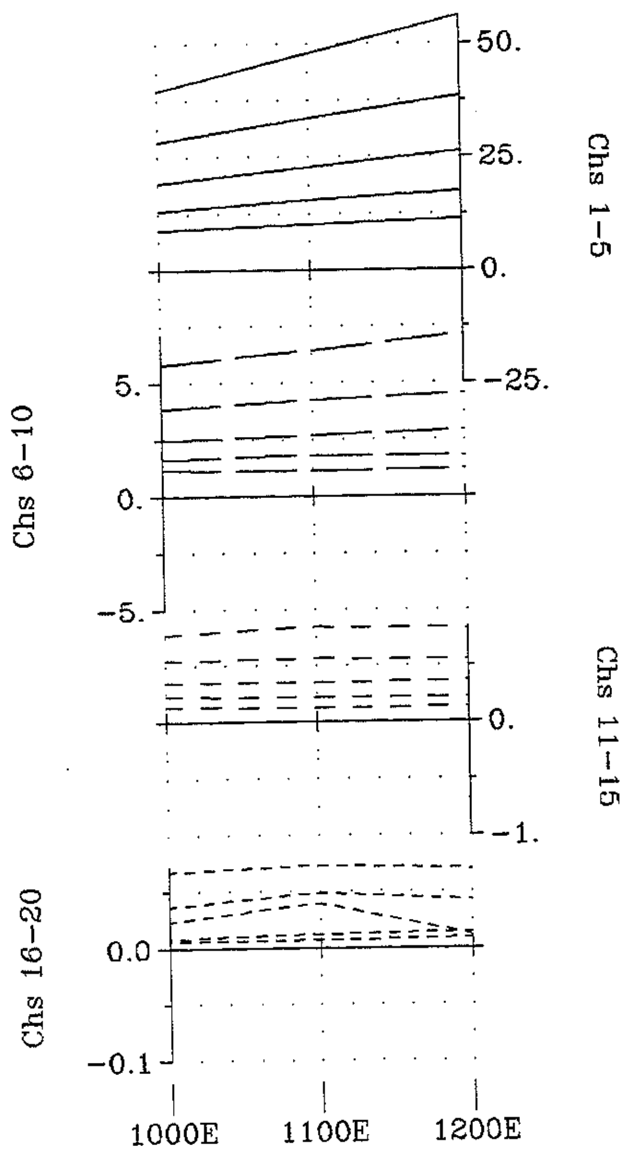
50 0 50 100 150 200
(metres)

KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 750m
Tx Loop Location:	Oval shape; Edges 3950E, 5000E
Transmitter Current:	7.5 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	September 3, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Y-12



Line 12 - Total Field
Cassat Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200
(metres)

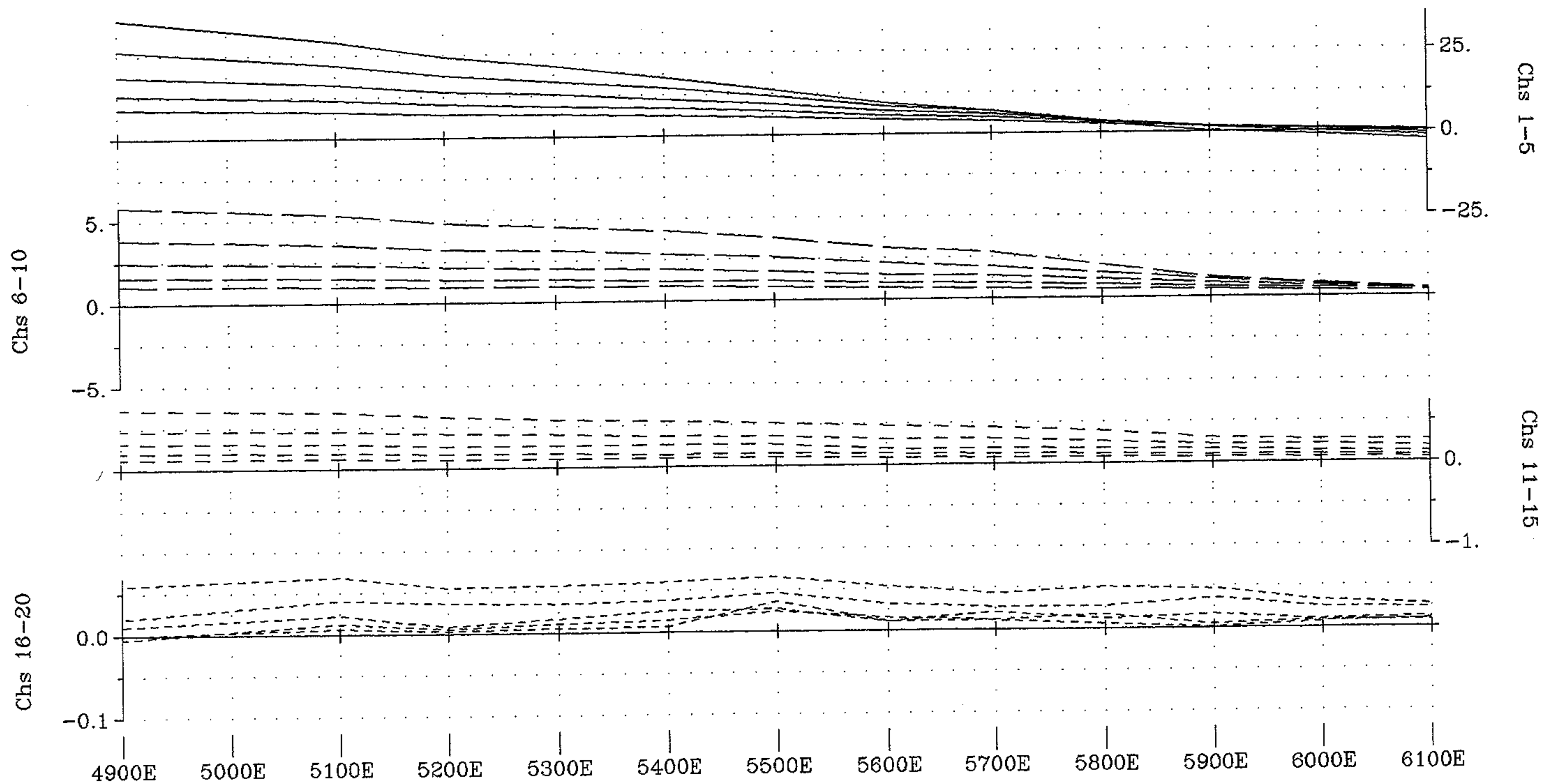
KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 750m
Tx Loop Location:	Oval shape; Edges 3950E, 5000E
Transmitter Current:	7.5 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 3, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-TF-12

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 11N - Z Component
Cassat Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200
(metres)

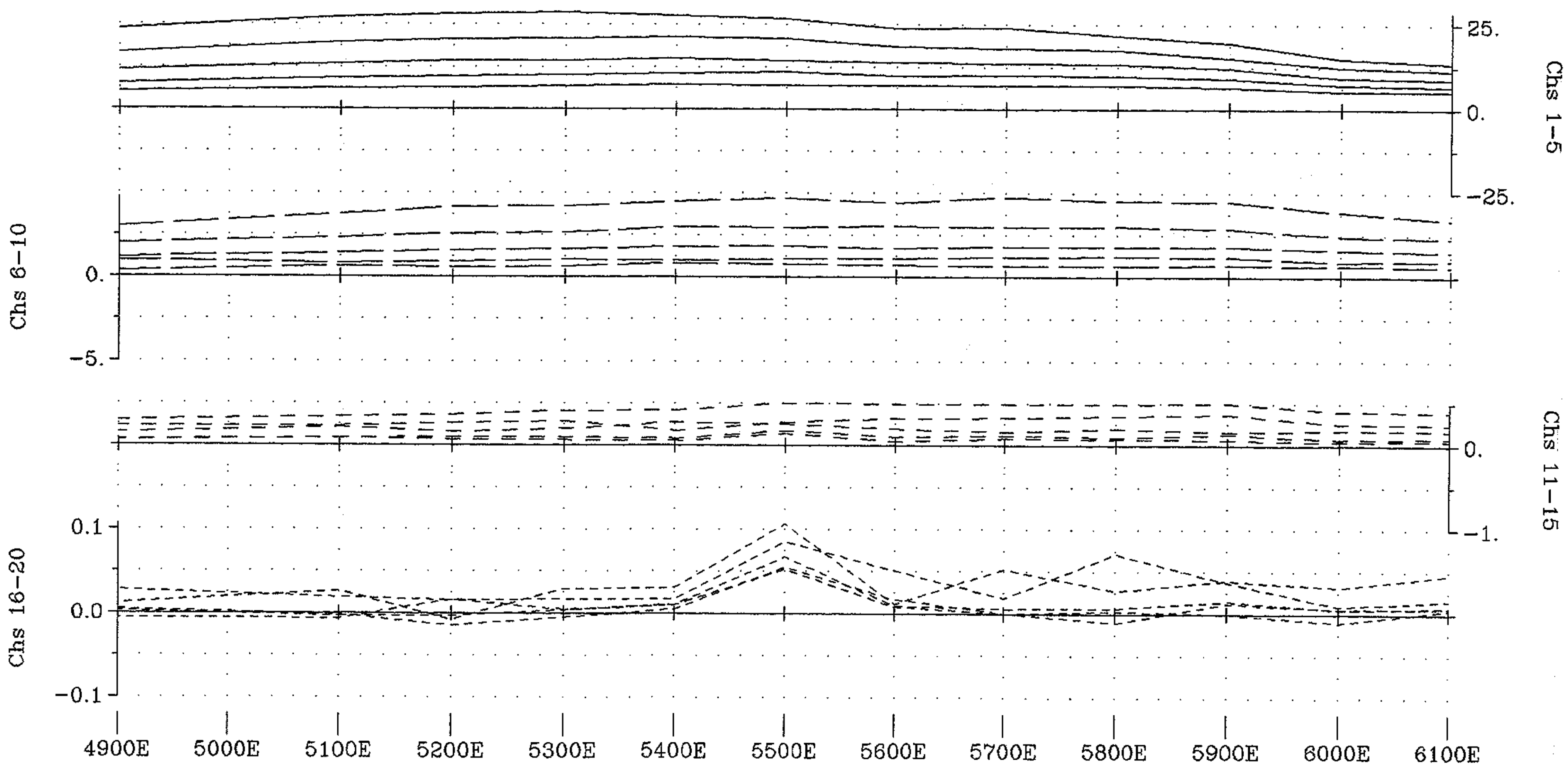
KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 750m
Tx Loop Location:	Oval shape; Edges 3950E, 5000E
Transmitter Current:	7.5 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 4, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Z-11N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 11N – X Component
Cassat Grid–Loop 1

Scale 1:5000

50 0 50 100 150 200
(metres)

KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

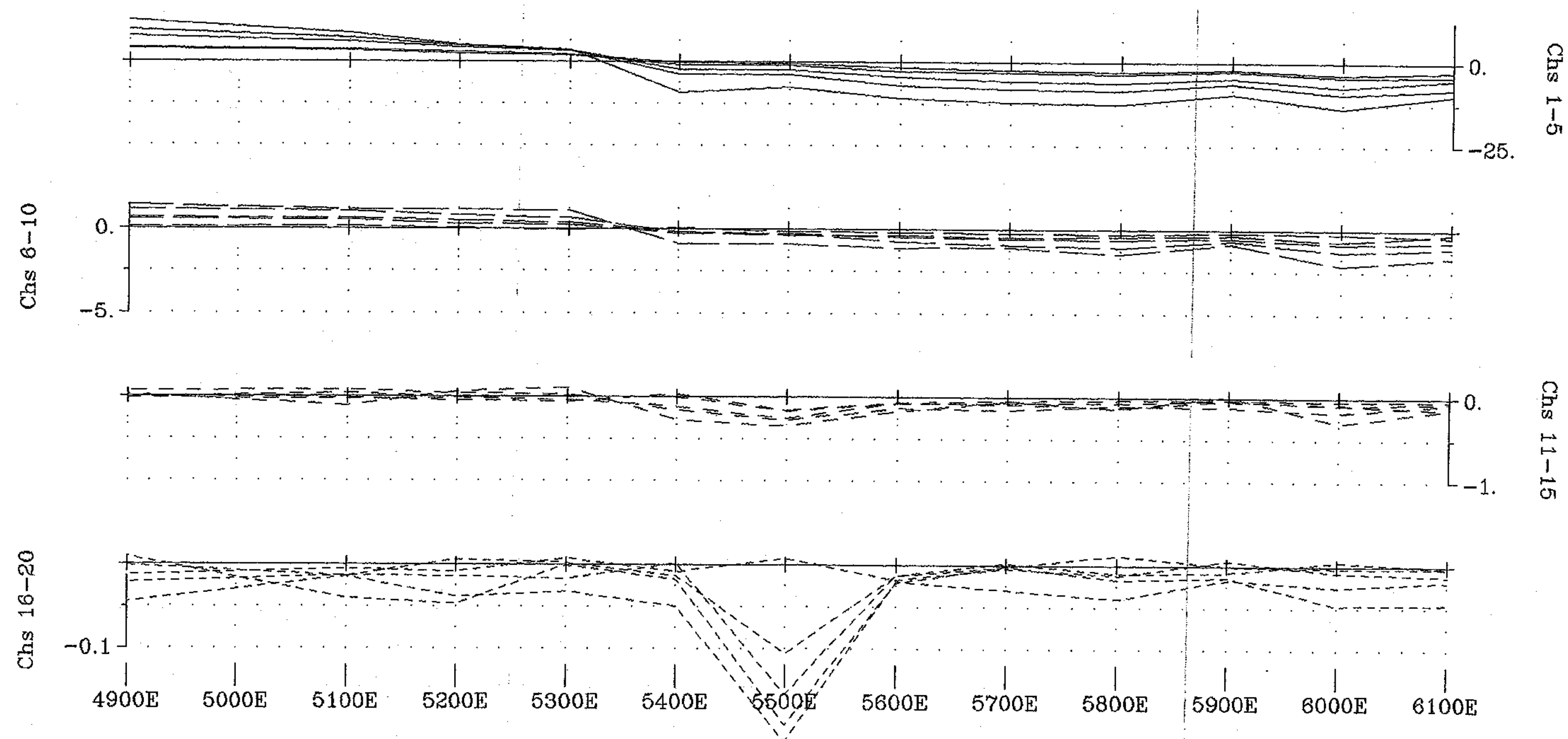
LPTEM FIXED–LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 750m
Tx Loop Location:	Oval shape; Edges 3950E, 5000E
Transmitter Current:	7.5 Amps
Transmitter Turn–Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up Hx – positive east Hy – positive north
Survey Date:	September 4, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-X-11N

Plotted Fri 09-25-1998 @ 17:44:50.81

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 11N - Y Component
Cassat Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200 (metres)

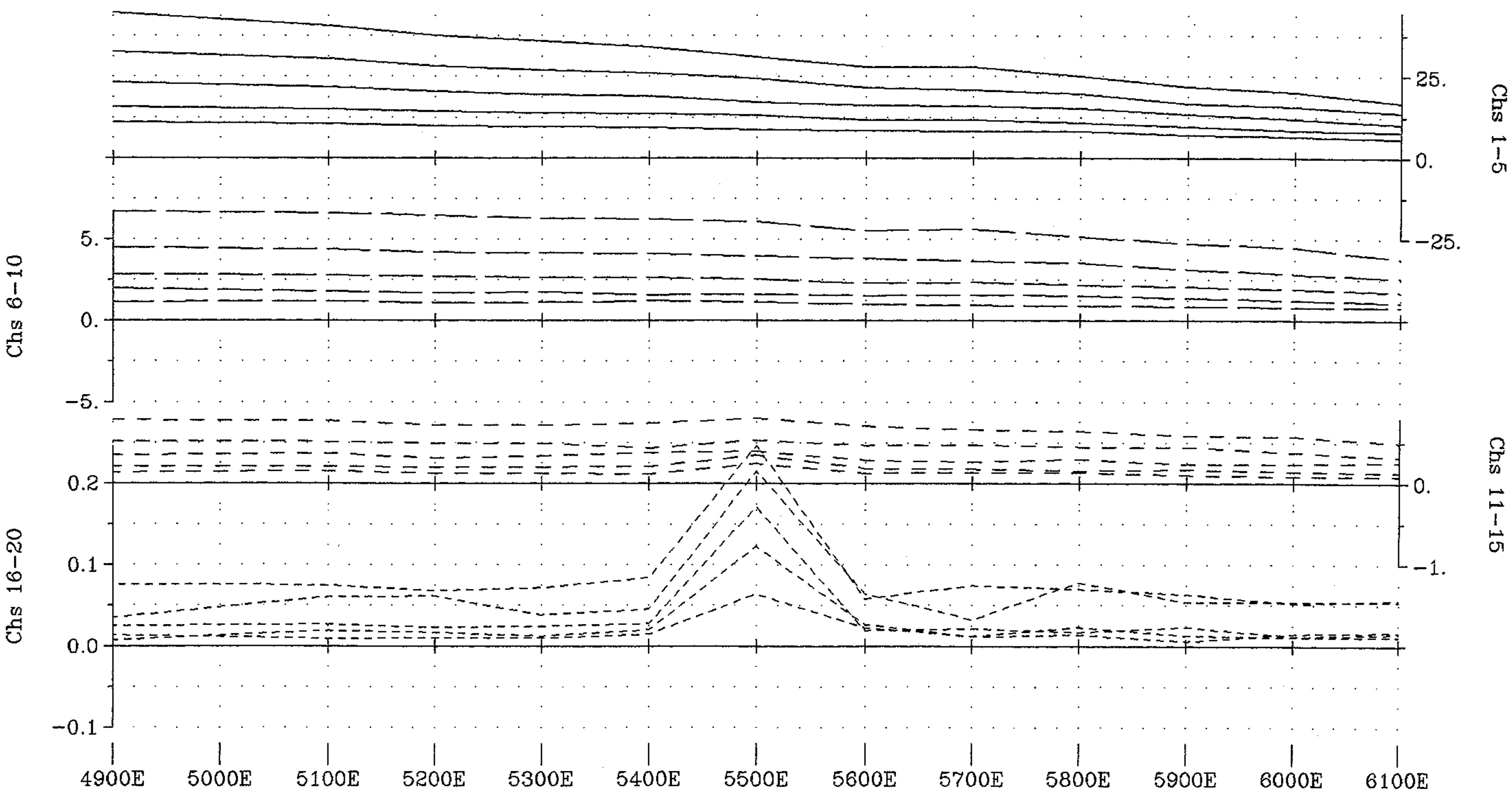
KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 750m
Tx Loop Location:	Oval shape; Edges 3950E, 5000E
Transmitter Current:	7.5 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	September 4, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Y-11N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 11N - Total Field
Cassat Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

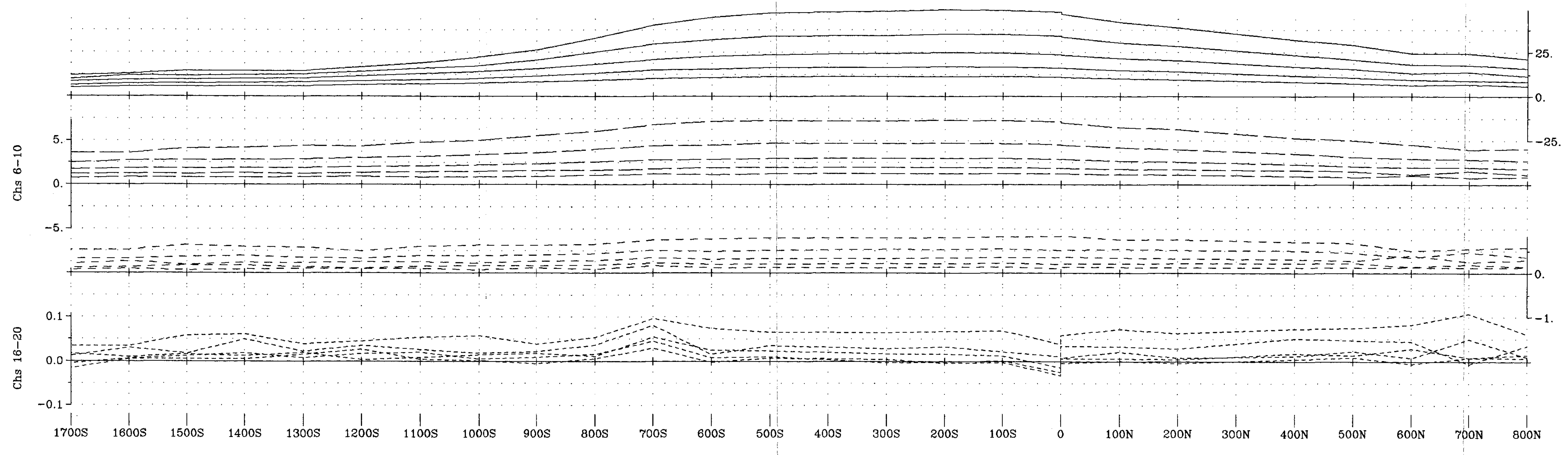
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 750m
Tx Loop Location:	Oval shape; Edges 3950E, 5000E
Transmitter Current:	7.5 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 4, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-TF-11N



Line 4500E - Z Component
Cassat Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200
(metres)

Findlay Creek Project
Cranbrook, BC

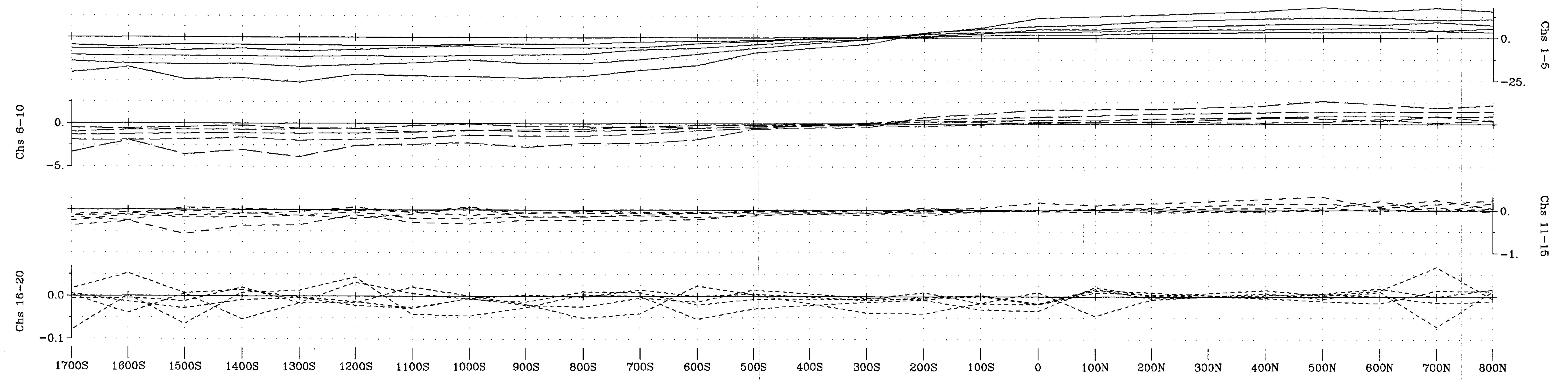
LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 750m
Tx Loop Location:	Oval shape; Edges 300N, 400S
Transmitter Current:	7.5 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive north
	Hy - positive west
Survey Date:	September 4, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Z-4500E

Plotted Fri 09-25-1998 @ 17:44:50.81

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 4500E - X Component
Cassat Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200

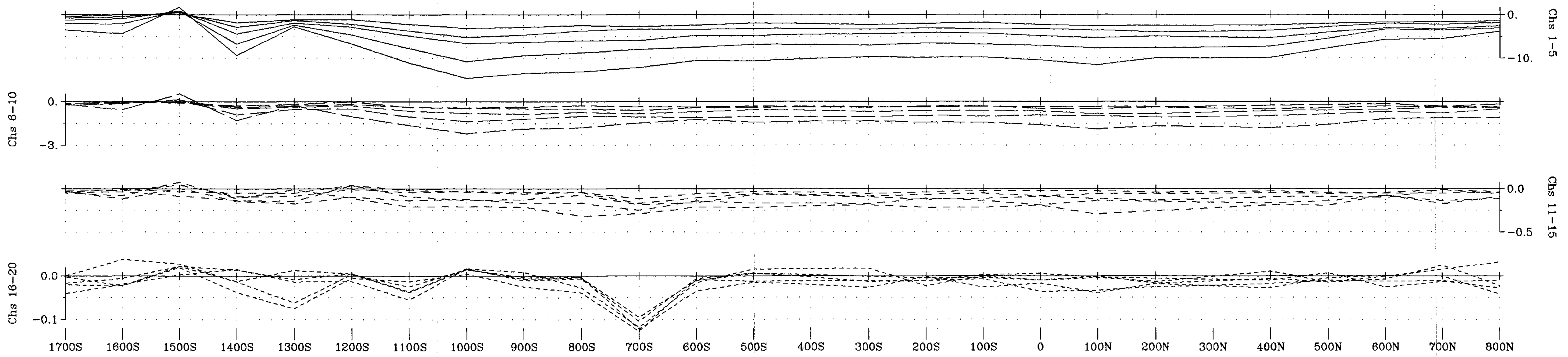
(metres)

Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 750m
Tx Loop Location:	Oval shape; Edges 300N, 400S
Transmitter Current:	7.5 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive north
	Hy - positive west
Survey Date:	September 4, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-X-4500E



Line 4500E - Y Component
Cassat Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200

(metres)

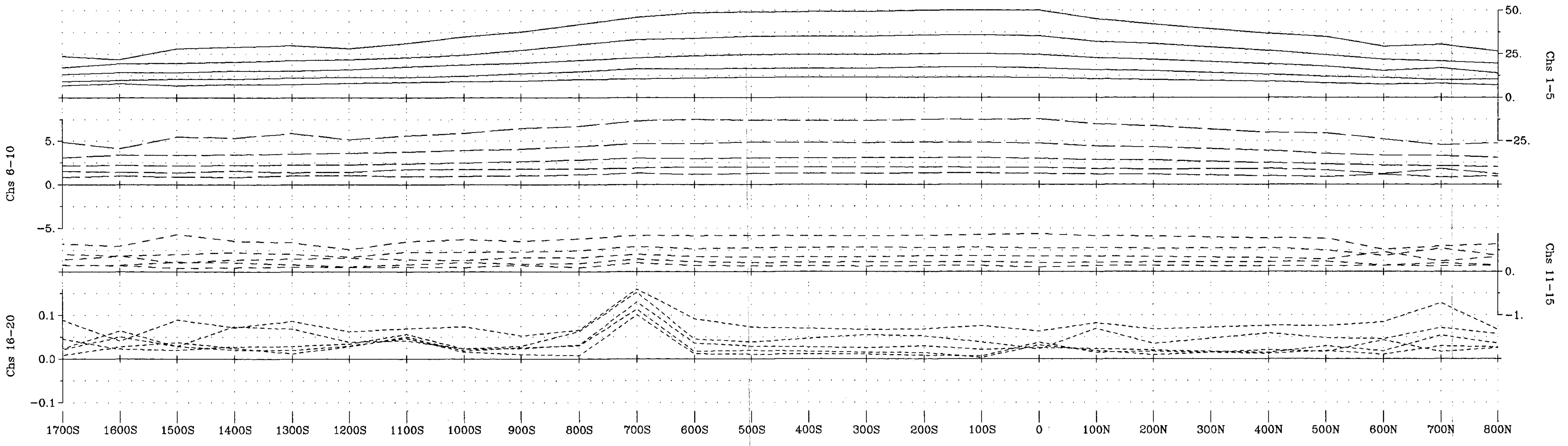
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 750m
Tx Loop Location:	Oval shape; Edges 300N, 400S
Transmitter Current:	7.5 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive north Hy - positive west
Survey Date:	September 4, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Y-4500E

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 4500E – Total Field
Cassat Grid–Loop 1

Scale 1:5000

50 0 50 100 150 200
(metres)

Findlay Creek Project
Cranbrook, BC

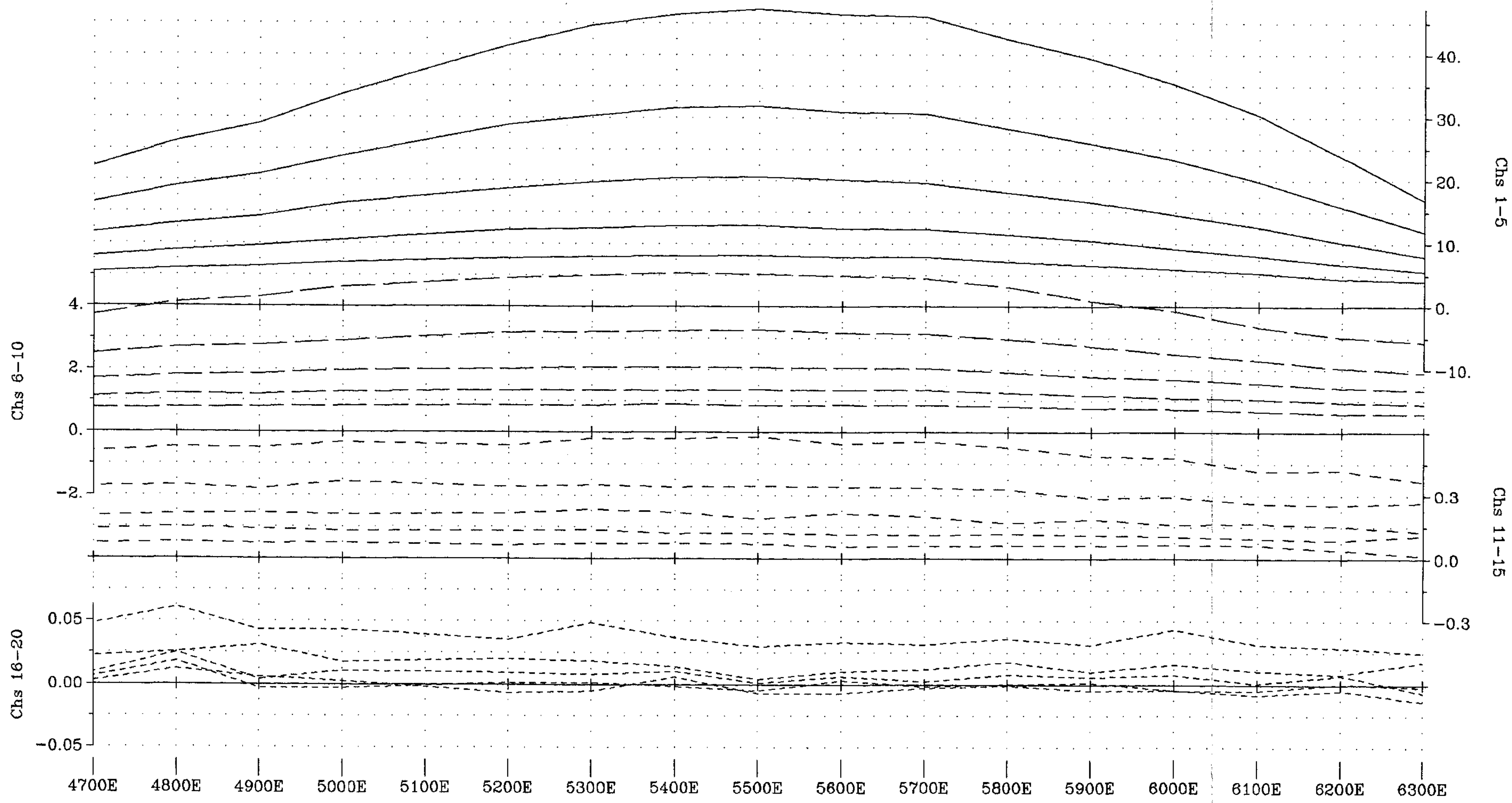
LPTEM FIXED–LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 750m
Tx Loop Location:	Oval shape; Edges 300N, 400S
Transmitter Current:	7.5 Amps
Transmitter Turn–Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up Hx – positive north Hy – positive west
Survey Date:	September 4, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM–37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-TF-4500E

Plotted Fri 09-25-1998 @ 17:44:50.81

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 21N - Z Component
Cassat Grid
Scale 1:5000
50 0 50 100 150 200
(metres)

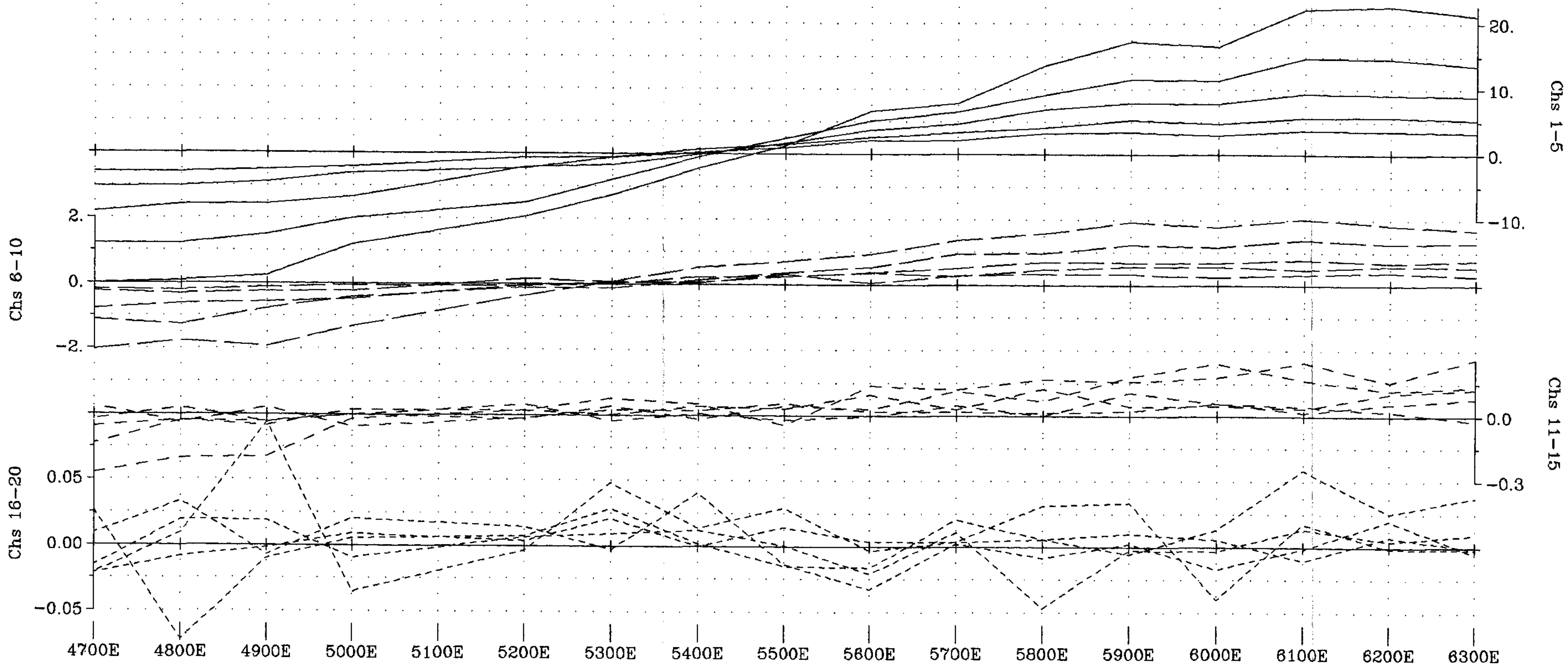
KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 1000m
Tx Loop Location:	Irregular Shape
Transmitter Current:	8 Amps
Transmitter Turn-Off Time:	210 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	September 5, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Z-21N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 21N - X Component

Cassat Grid

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

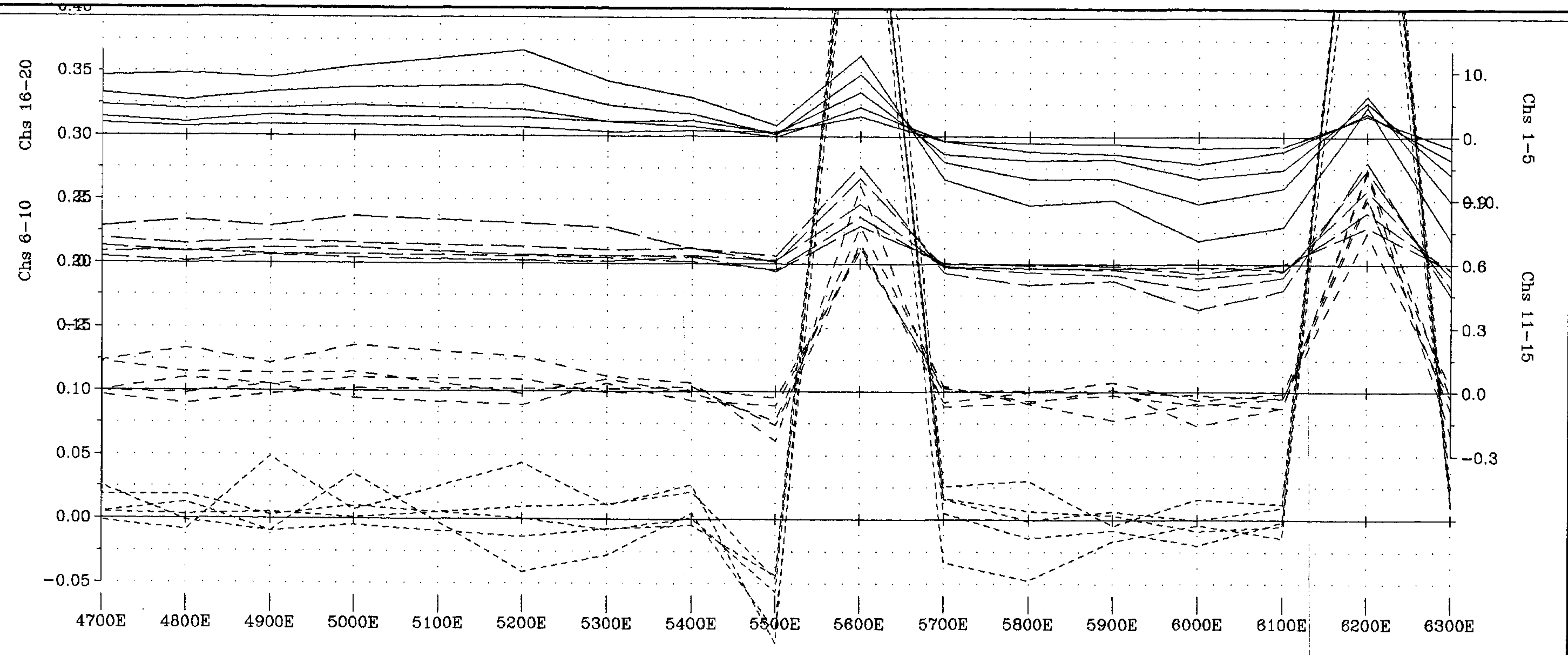
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 1000m
Tx Loop Location:	Irregular Shape
Transmitter Current:	8 Amps
Transmitter Turn-Off Time:	210 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	September 5, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-X-21N



Line 21N - Y Component
Cassat Grid

Scale 1:5000

50 0 50 100 150 200
(metres)

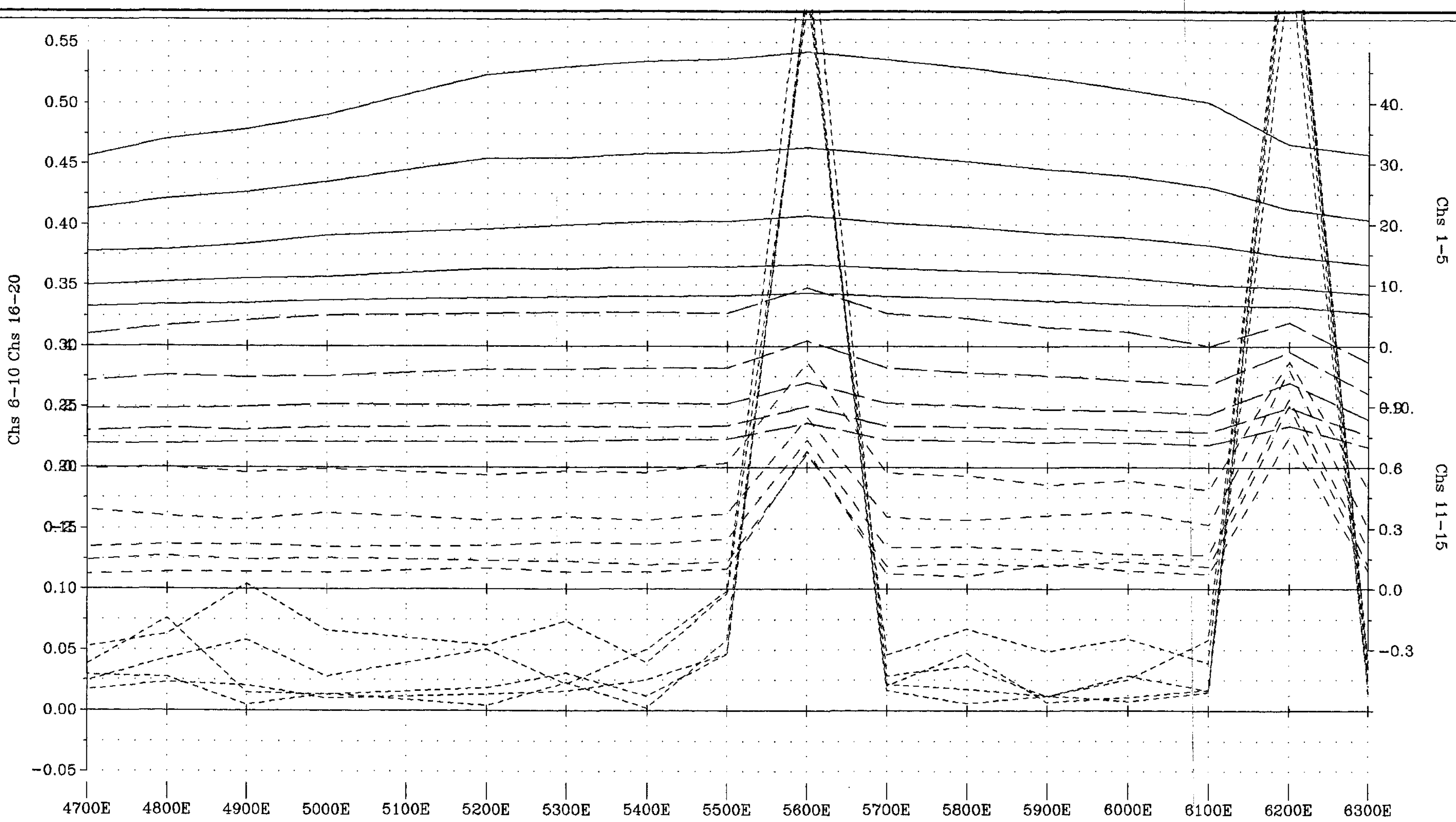
KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 1000m
Tx Loop Location:	Irregular Shape
Transmitter Current:	8 Amps
Transmitter Turn-Off Time:	210 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 5, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Y-21N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 21N - Total Field
Cassat Grid

Scale 1:5000

50 0 50 100 150 200
(metres)

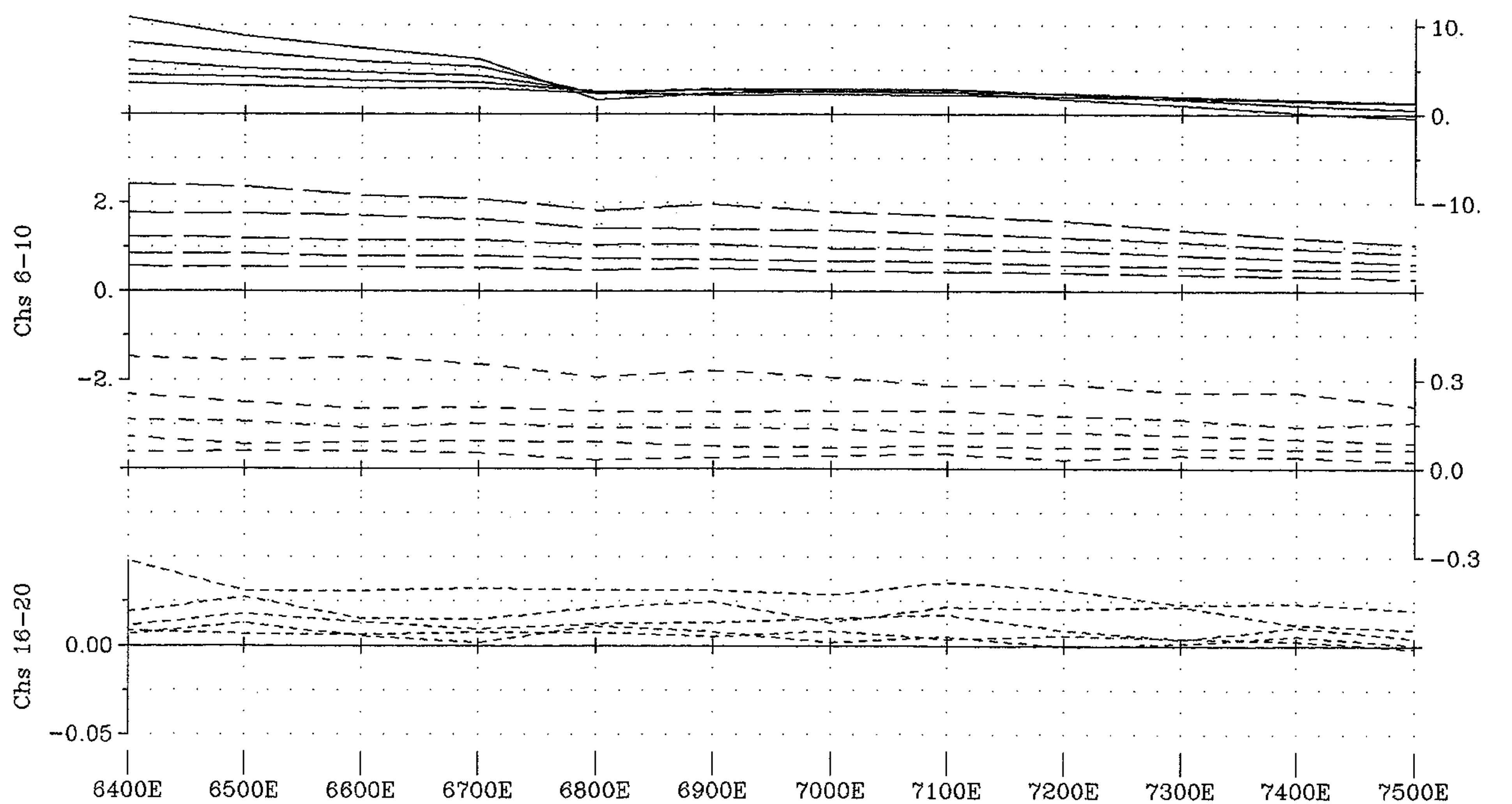
KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 1000m
Tx Loop Location:	Irregular Shape
Transmitter Current:	8 Amps
Transmitter Turn-Off Time:	210 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	September 5, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-TF-21N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 22N - Z Component
Cassat Grid

Scale 1:5000

50 0 50 100 150 200
(metres)

KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

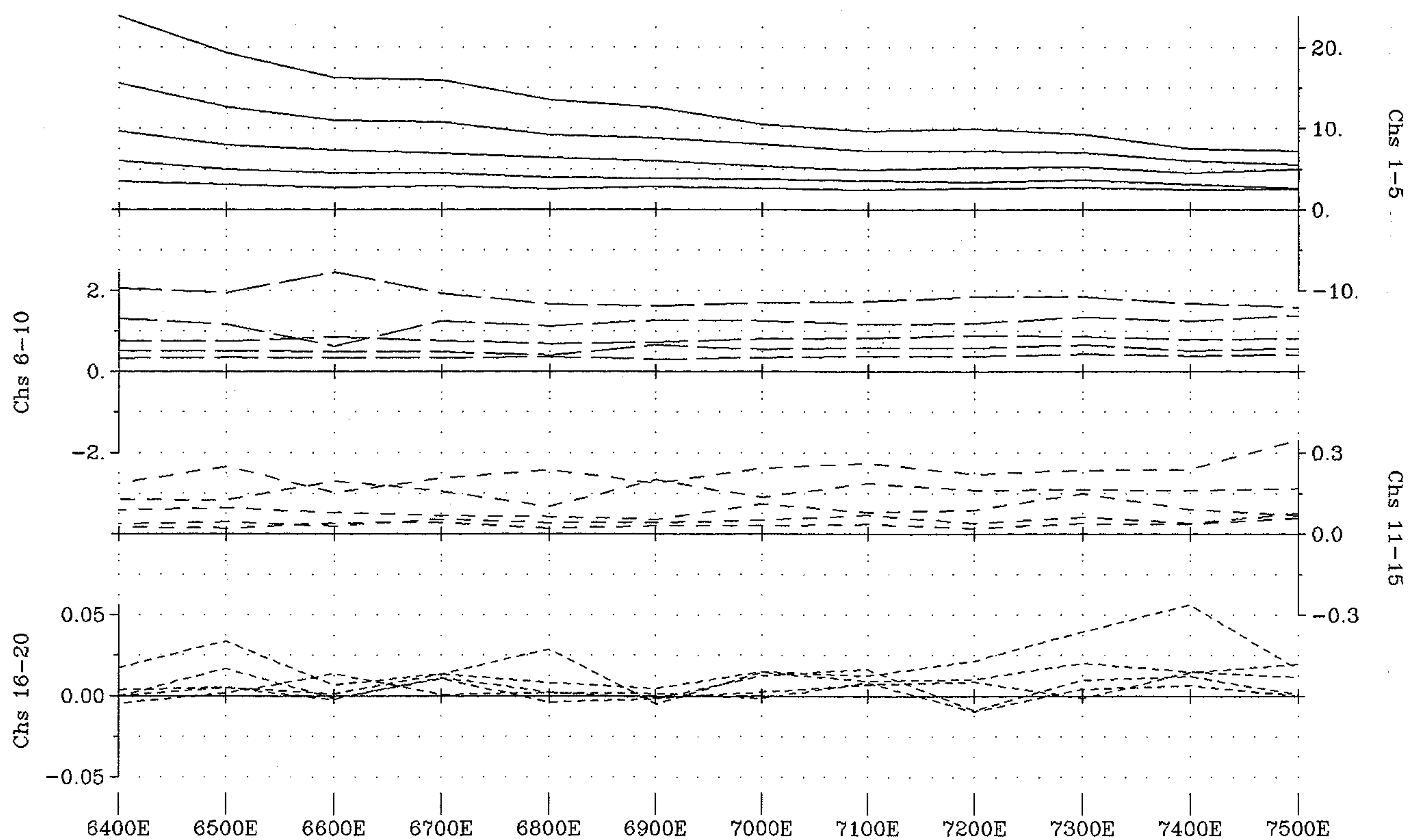
LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 1000m
Tx Loop Location:	Irregular Shape
Transmitter Current:	8 Amps
Transmitter Turn-Off Time:	210 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 6, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Z-22N

Plotted Fri 09-25-1998 @ 17:44:50.81

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 22N – X Component
Cassat Grid

Scale 1:5000

50 0 50 100 150 200
(metres)

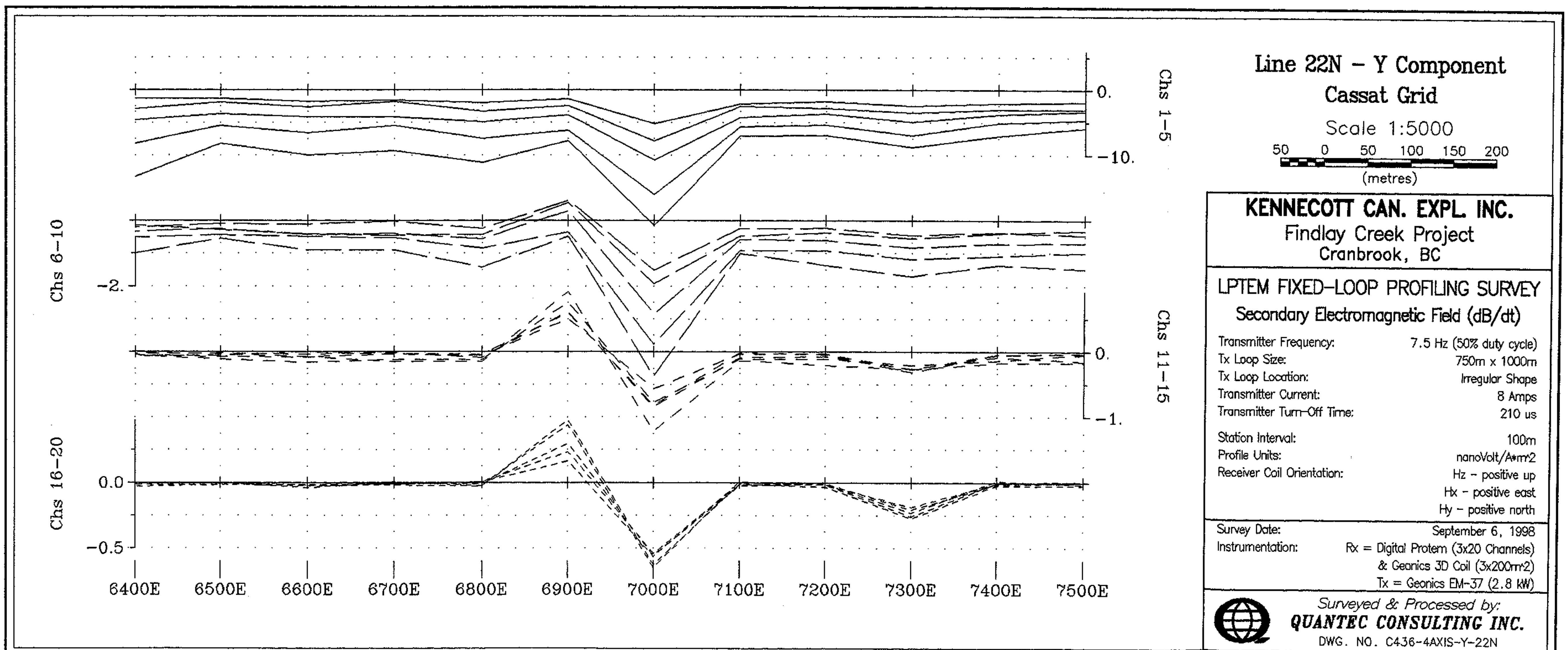
KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

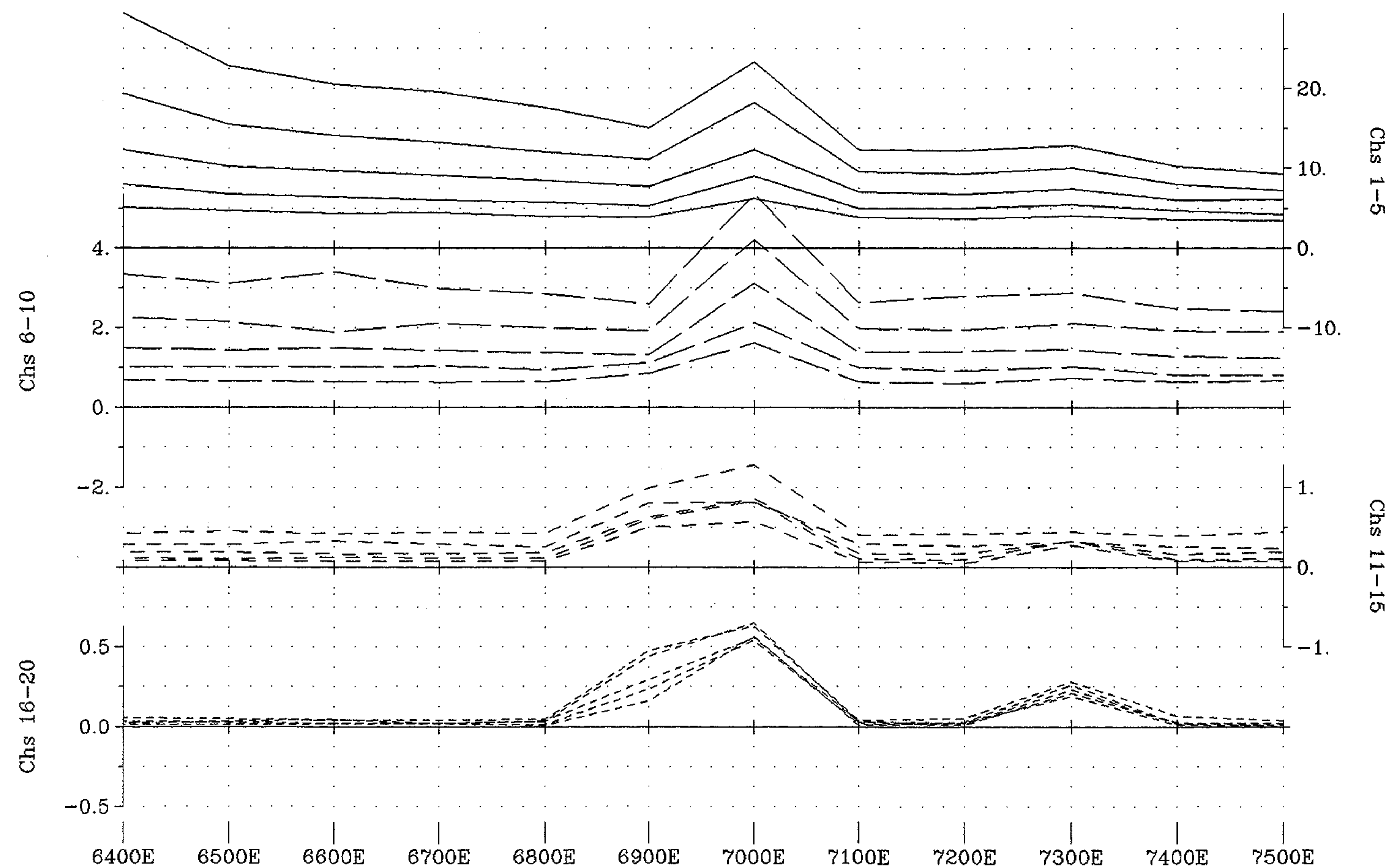
LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 1000m
Tx Loop Location:	Irregular Shape
Transmitter Current:	8 Amps
Transmitter Turn-Off Time:	210 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up
	Hx – positive east
	Hy – positive north
Survey Date:	September 6, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-X-22N

Plotted Fri 09-25-1998 @ 17:44:50.81





Line 22N – Total Field
Cassat Grid

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

Secondary Electromagnetic Field (dB/dt)

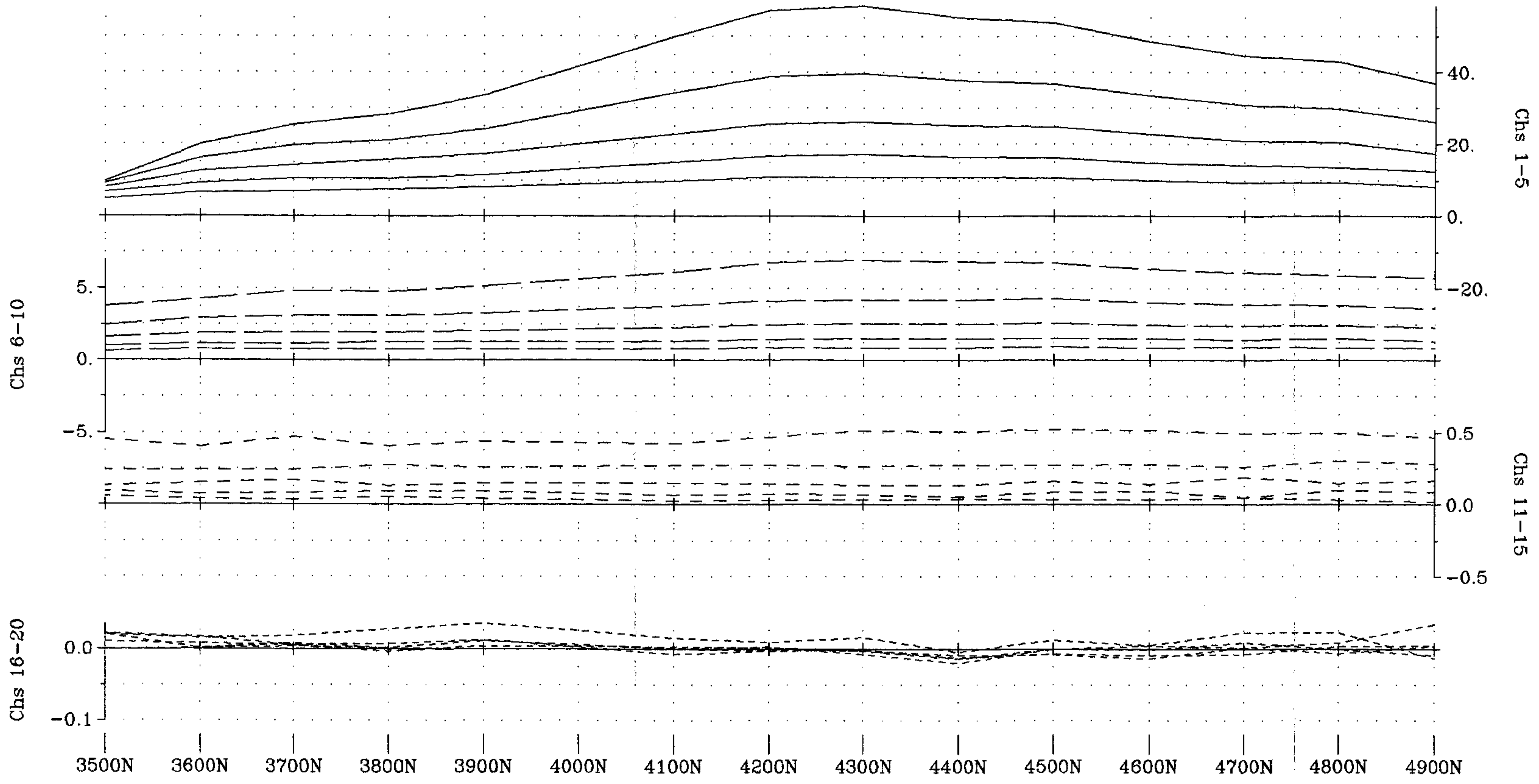
Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 1000m
Tx Loop Location:	Irregular Shape
Transmitter Current:	8 Amps
Transmitter Turn-Off Time:	210 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up
	Hx – positive east
	Hy – positive north
Survey Date:	September 6, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-TF-22N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 31E - Z Component
Pico Grid

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project
Cranbrook, BC

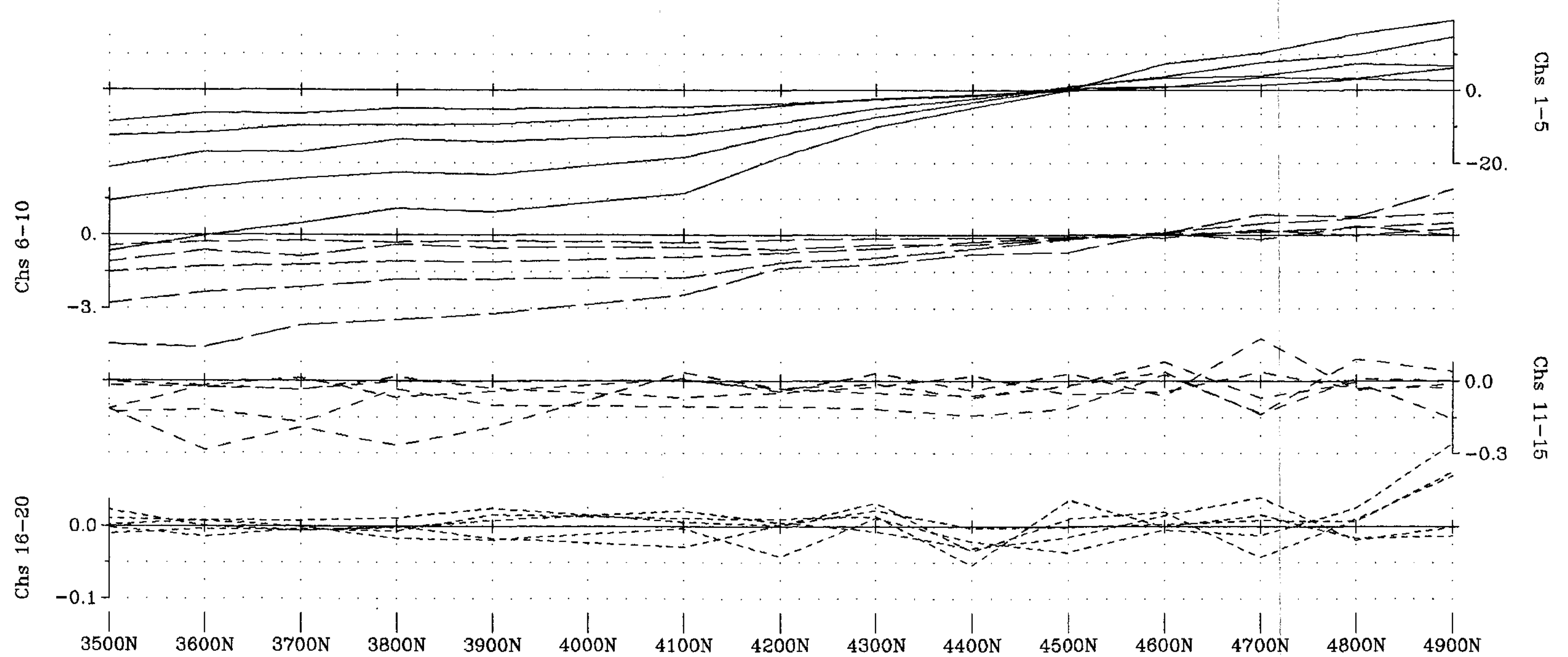
LPTEM FIXED-LOOP PROFILING SURVEY

Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	1000m x 725m
Tx Loop Location:	Oval shape;Loop at 5000E, 4000E
Transmitter Current:	9 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive north Hy - positive west
Survey Date:	September 7, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-Z-31E



Line 31E – X Component
Pico Grid

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	1000m x 725m
Tx Loop Location:	Oval shape;Loop at 5000E, 4000E
Transmitter Current:	9 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz – positive up
	Hx – positive north
	Hy – positive west
Survey Date:	September 7, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

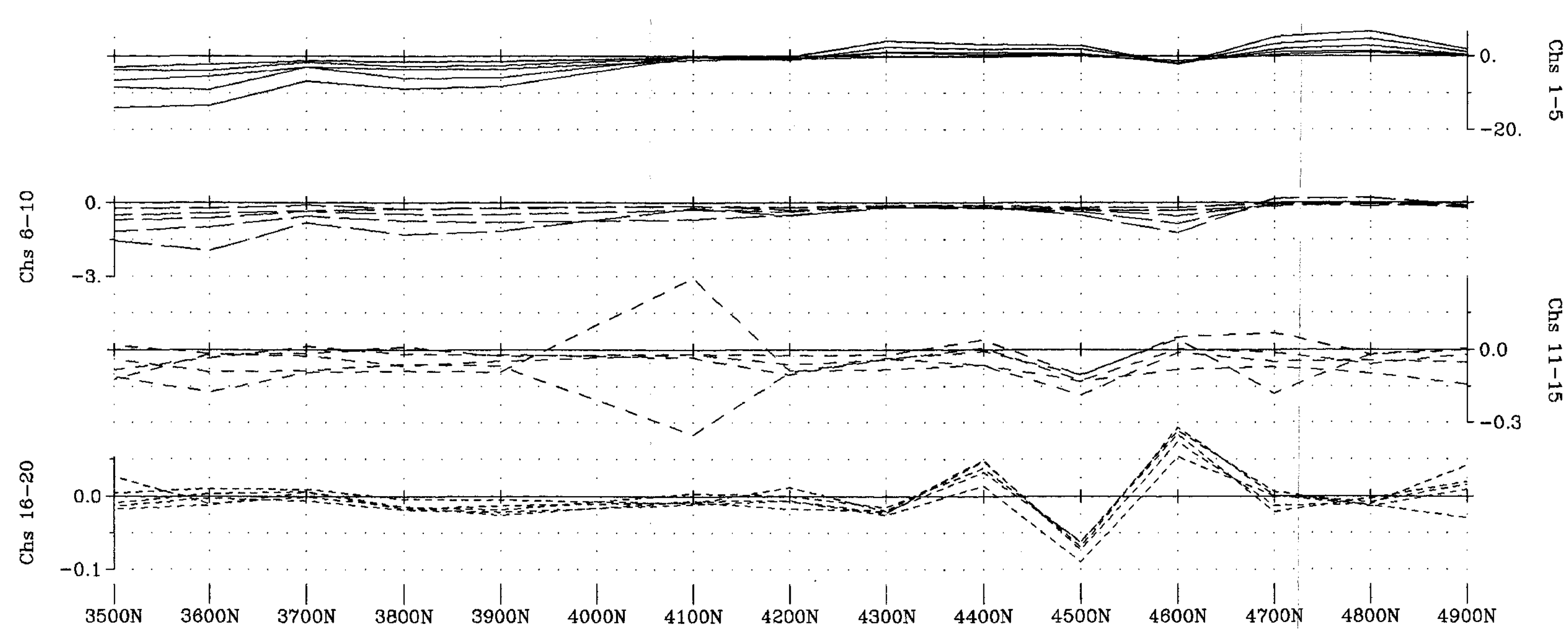
Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-X-31E

Plotted Fri 09-25-1998 @ 17:44:50.81

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 31E - Y Component
Pico Grid

Scale 1:5000

50 0 50 100 150 200

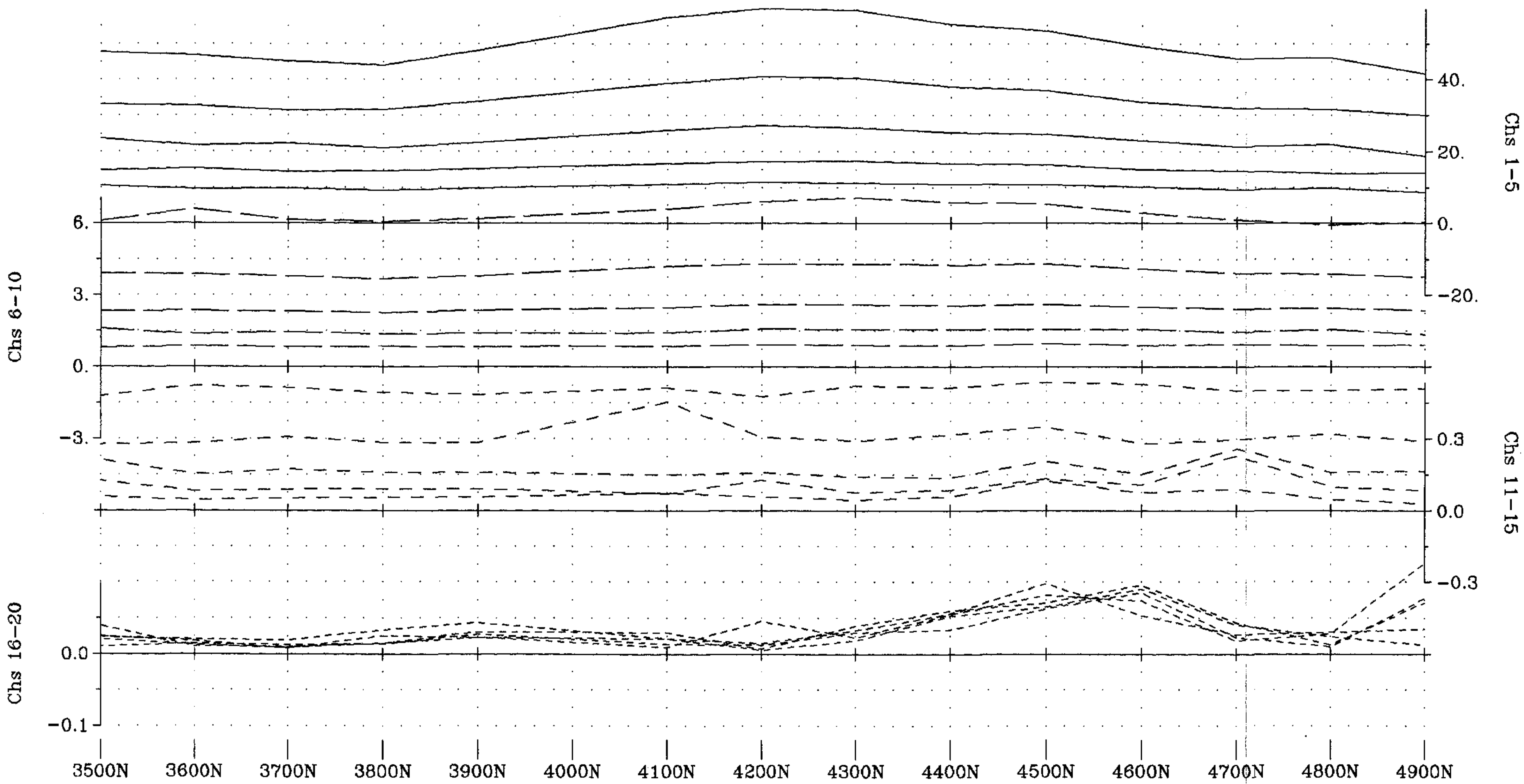
(metres)

KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	1000m x 725m
Tx Loop Location:	Oval shape;Loop at 5000E, 4000E
Transmitter Current:	9 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive north Hy - positive west
Survey Date:	September 7, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Y-31E



Line 31E – Total Field
Pico Grid

Scale 1:5000

50 0 50 100 150 200
(metres)

KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

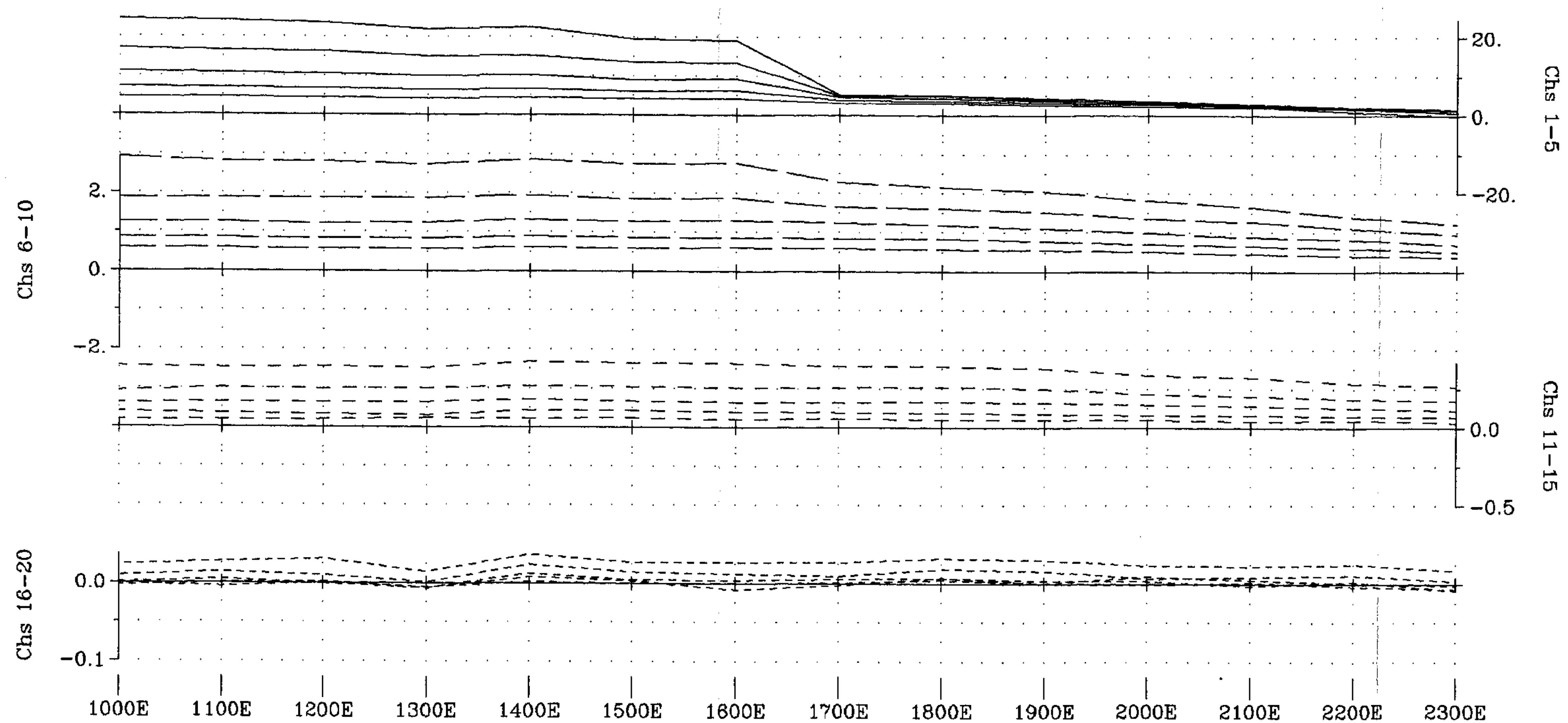
LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	1000m x 725m
Tx Loop Location:	Oval shape;Loop at 5000E, 4000E
Transmitter Current:	9 Amps
Transmitter Turn-Off Time:	215 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive north Hy - positive west
Survey Date:	September 7, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-TF-31E

Plotted Fri 09-25-1998 @ 17:44:50.81

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 1000N - Z Component
Doctor Lake Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200

(metres)

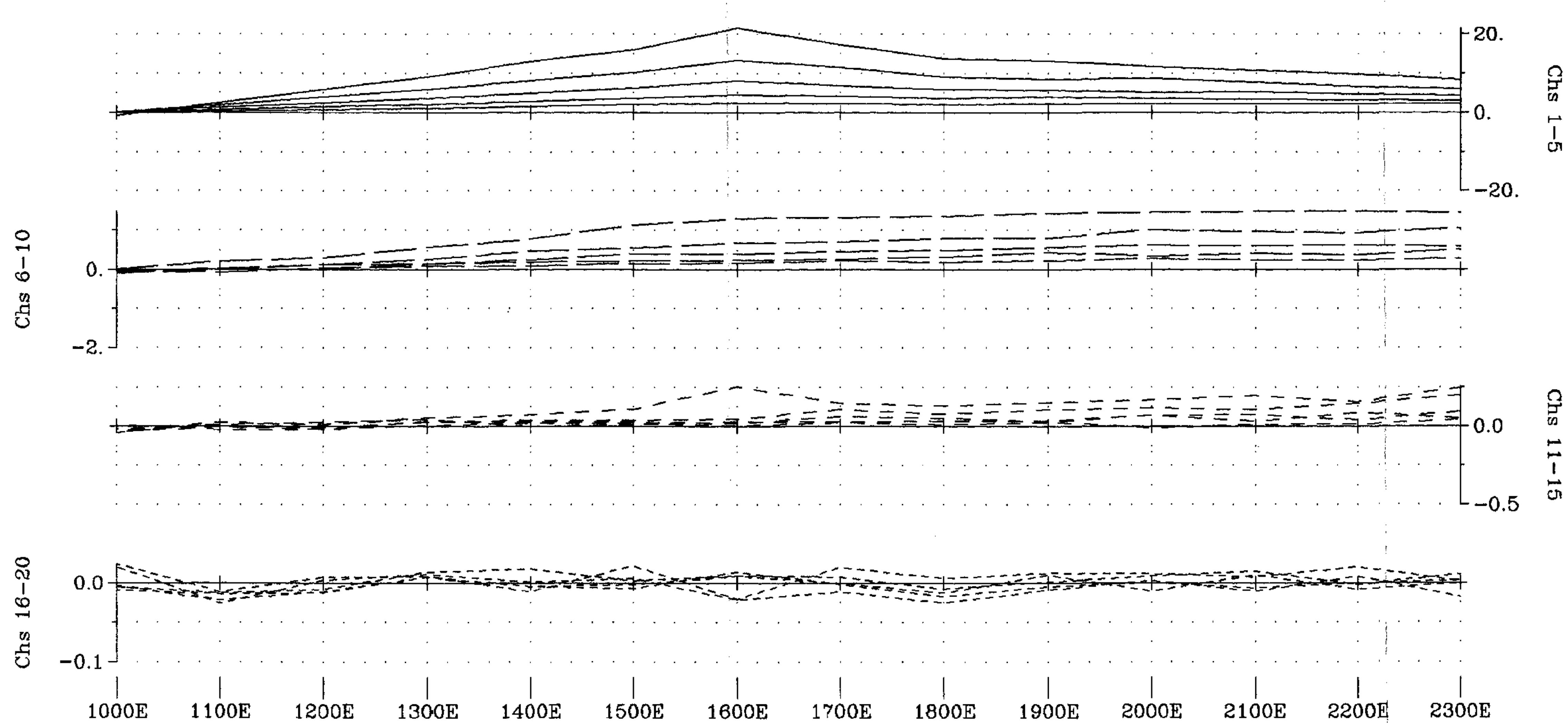
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 600m
Tx Loop Location:	Irregular; Edges 1350E, 900E
Transmitter Current:	11 Amps
Transmitter Turn-Off Time:	260 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 10, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-Z-1000N



Line 1000N - X Component
Doctor Lake Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200
(metres)

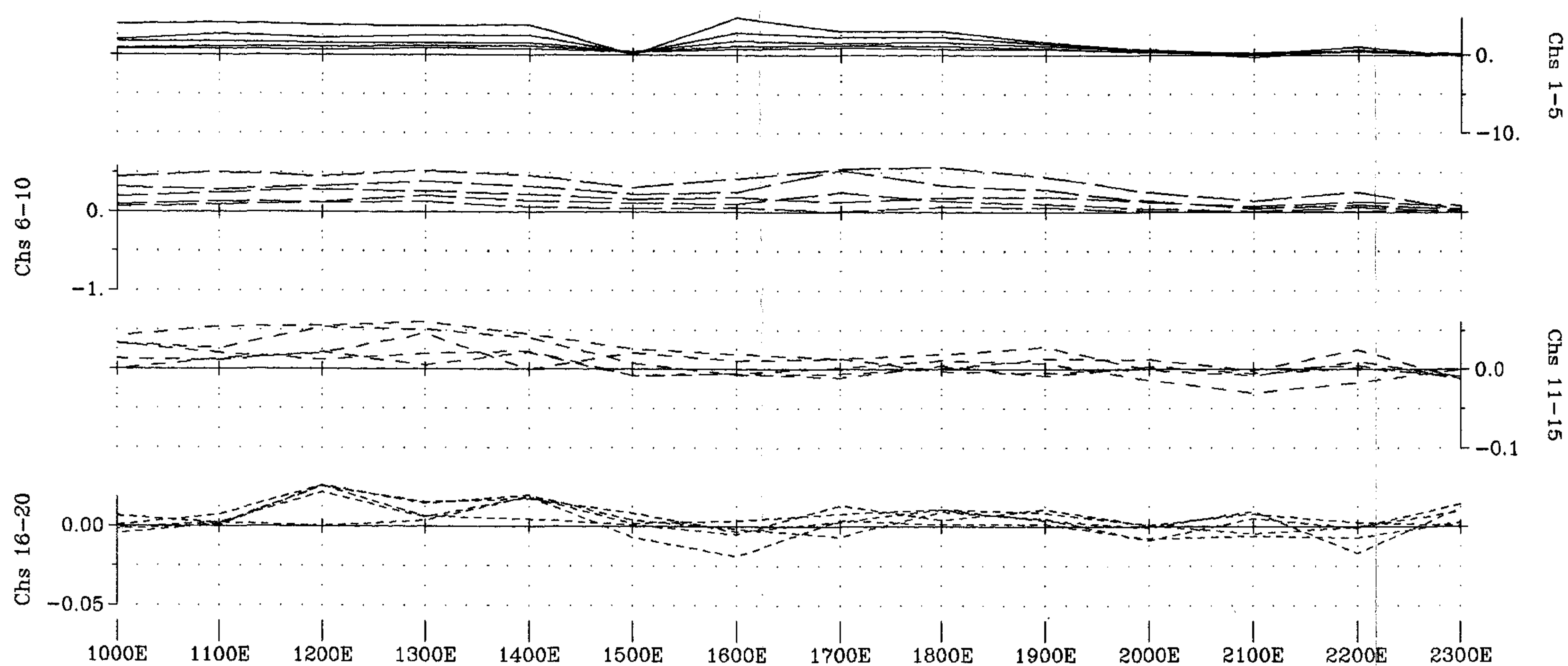
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 600m
Tx Loop Location:	Irregular; Edges 1350E, 900E
Transmitter Current:	11 Amps
Transmitter Turn-Off Time:	260 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 10, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-X-1000N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 1000N - Y Component
Doctor Lake Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200

(metres)

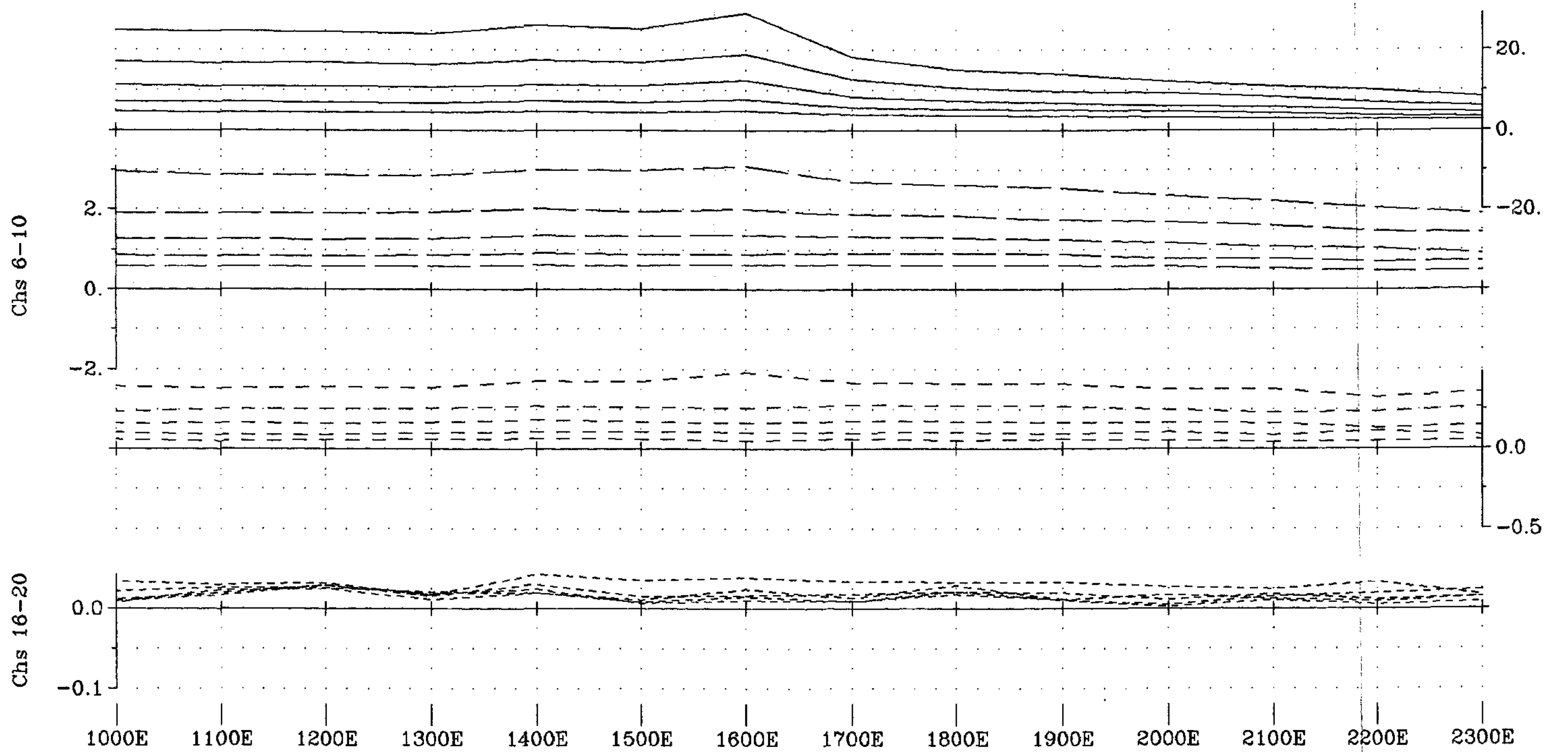
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 600m
Tx Loop Location:	Irregular; Edges 1350E, 900E
Transmitter Current:	11 Amps
Transmitter Turn-Off Time:	260 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 10, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Y-1000N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 1000N - Total Field
Doctor Lake Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200

(metres)

Findlay Creek Project
Cranbrook, BC

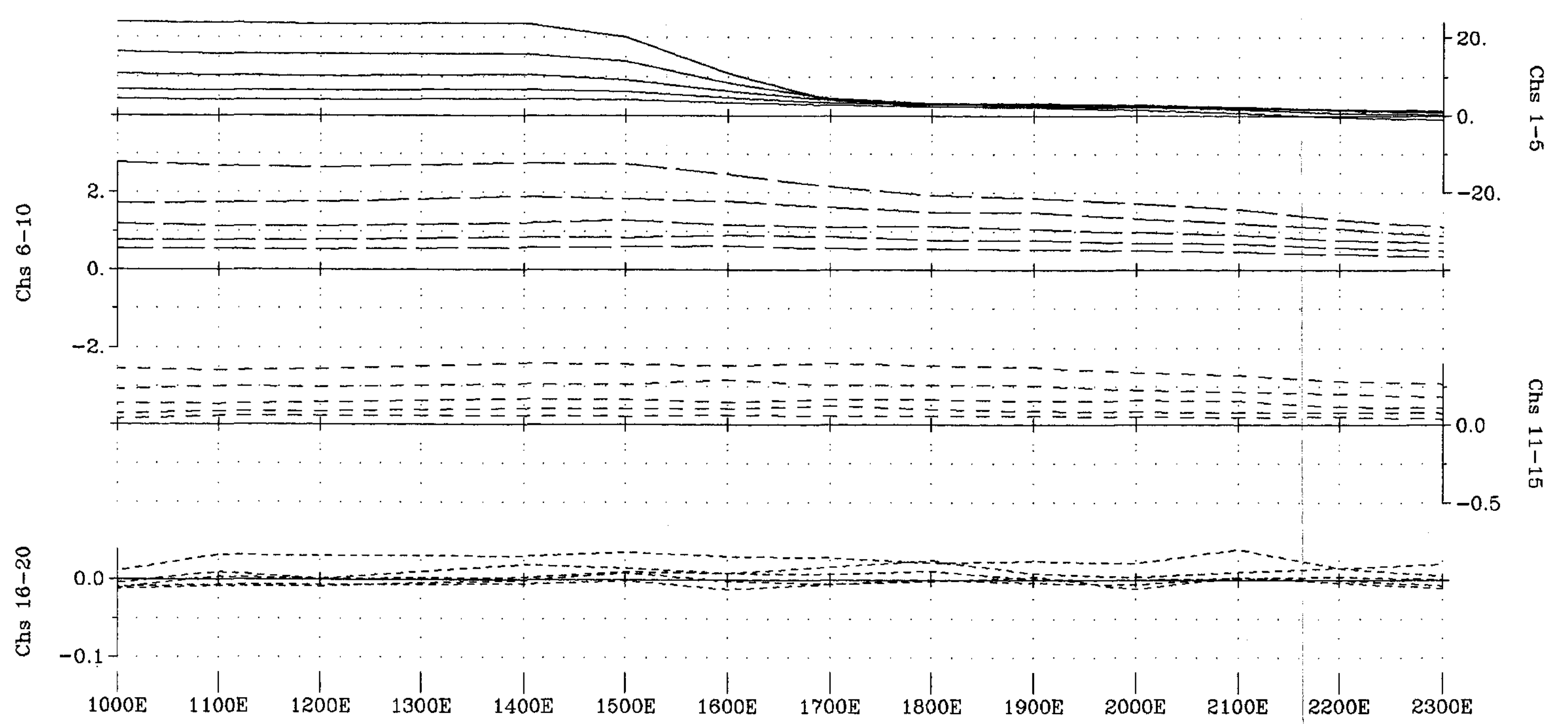
LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 600m
Tx Loop Location:	Irregular; Edges 1350E, 900E
Transmitter Current:	11 Amps
Transmitter Turn-Off Time:	260 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	September 10, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-TF-1000N

Plotted Fri 09-25-1998 @ 17:44:50.81

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 1200N - Z Component
Doctor Lake Grid-Loop 1

Scale 1:5000

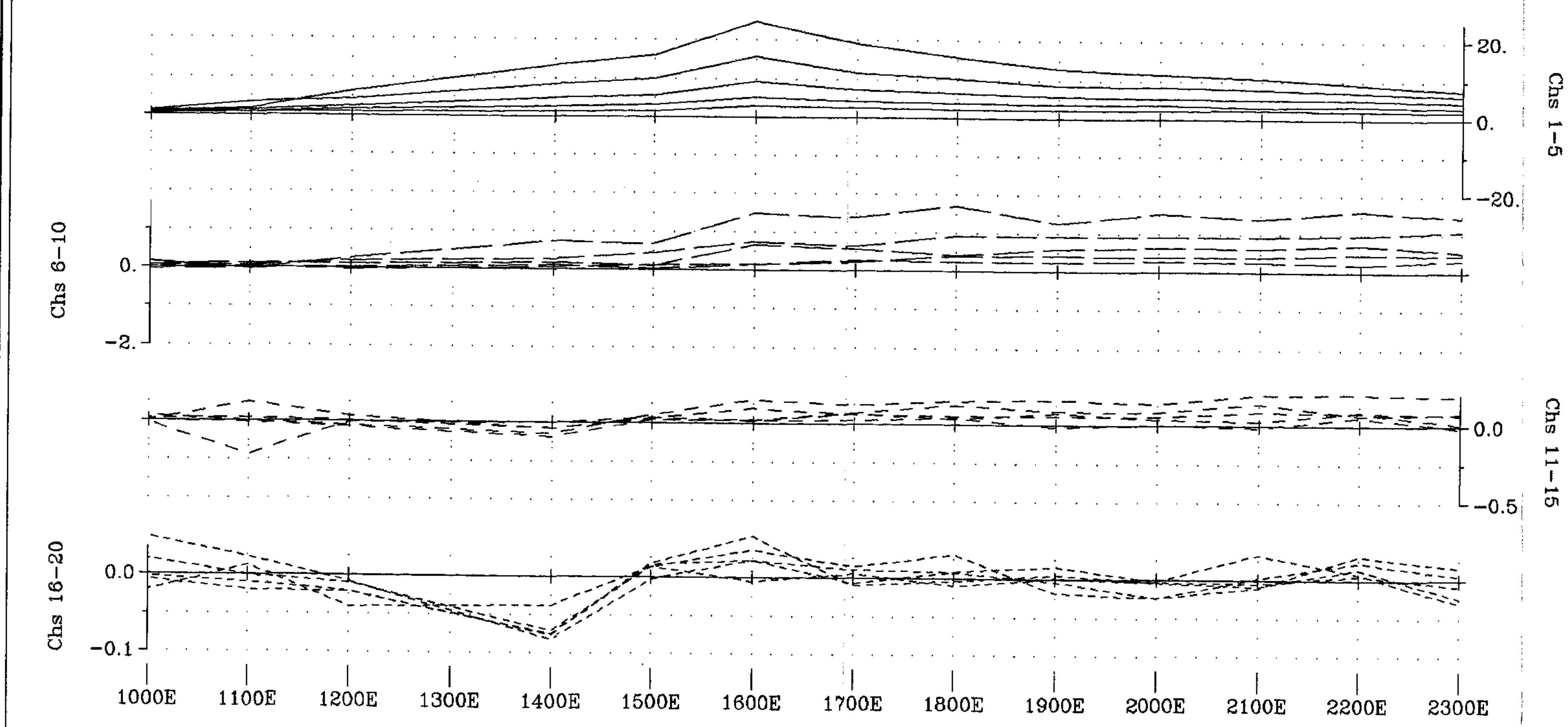
50 0 50 100 150 200
(metres)

Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 600m
Tx Loop Location:	Irregular; Edges 1300E, 950E
Transmitter Current:	11 Amps
Transmitter Turn-Off Time:	260 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 10, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Z-1200N



Line 1200N - X Component
Doctor Lake Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200
(metres)

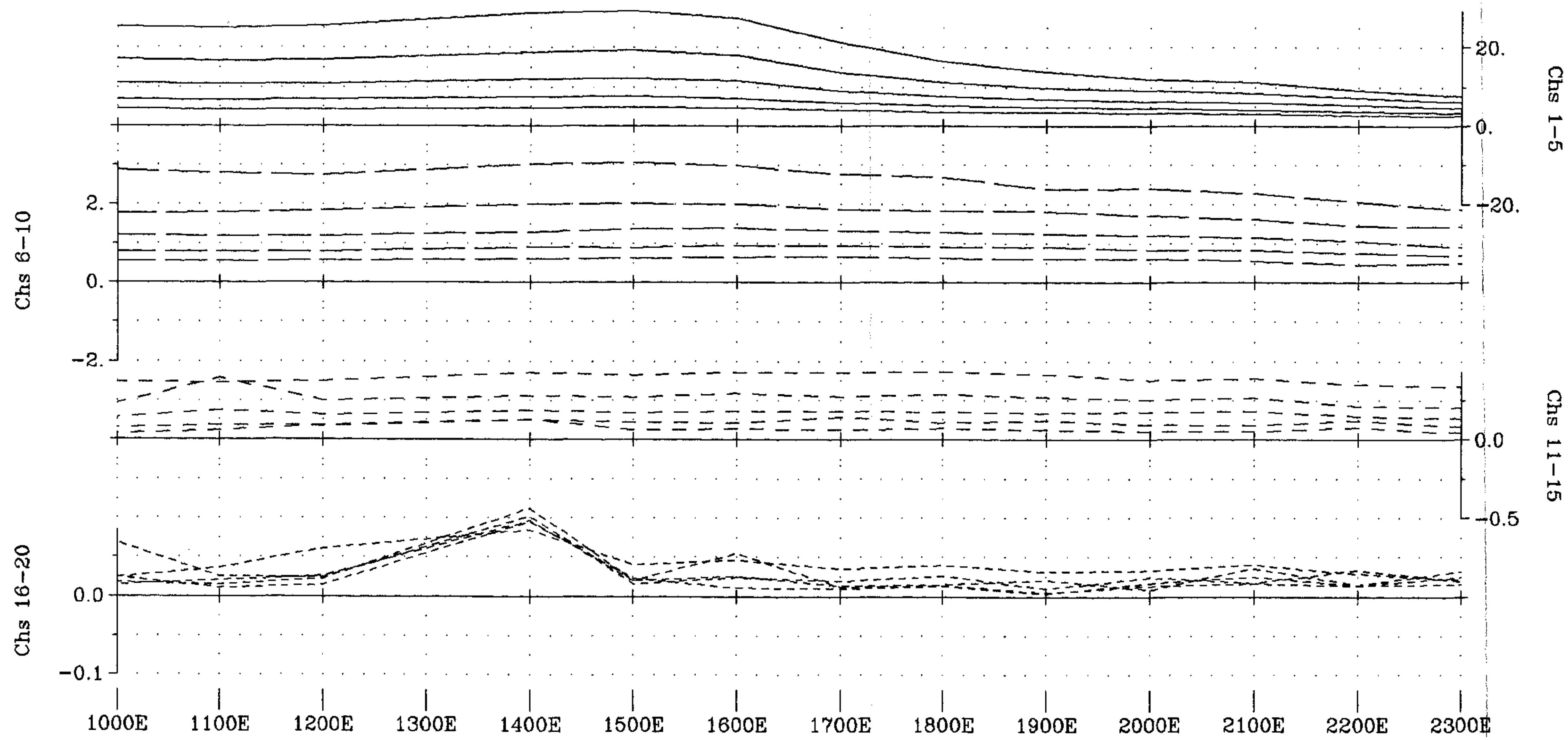
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 600m
Tx Loop Location:	Irregular; Edges 1300E, 950E
Transmitter Current:	11 Amps
Transmitter Turn-Off Time:	260 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	September 10, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-X-1200N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 1200N - Total Field
Doctor Lake Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200
(metres)

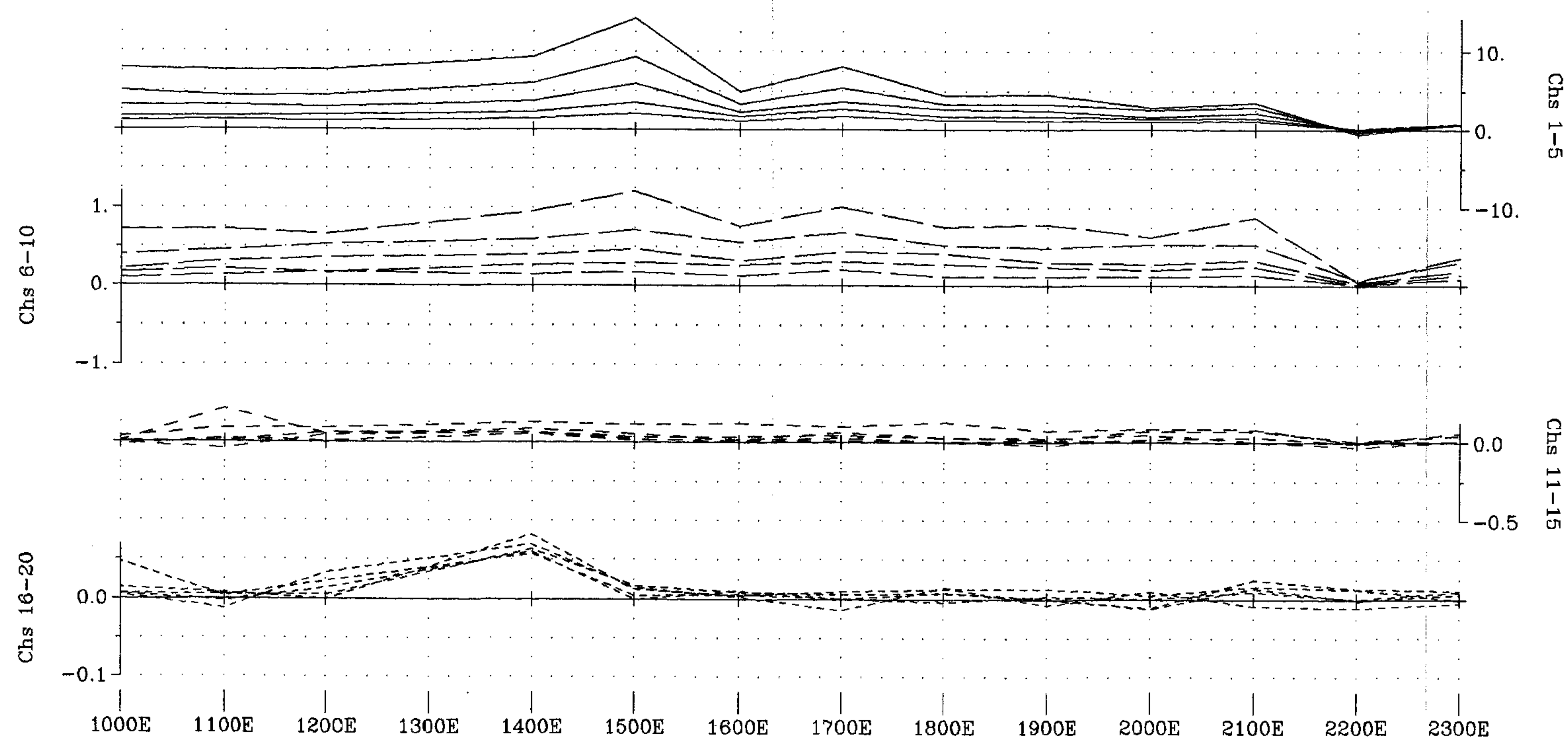
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 600m
Tx Loop Location:	Irregular; Edges 1300E, 950E
Transmitter Current:	11 Amps
Transmitter Turn-Off Time:	260 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	September 10, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-TF-1200N

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 1200N - Y Component
Doctor Lake Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200
(metres)

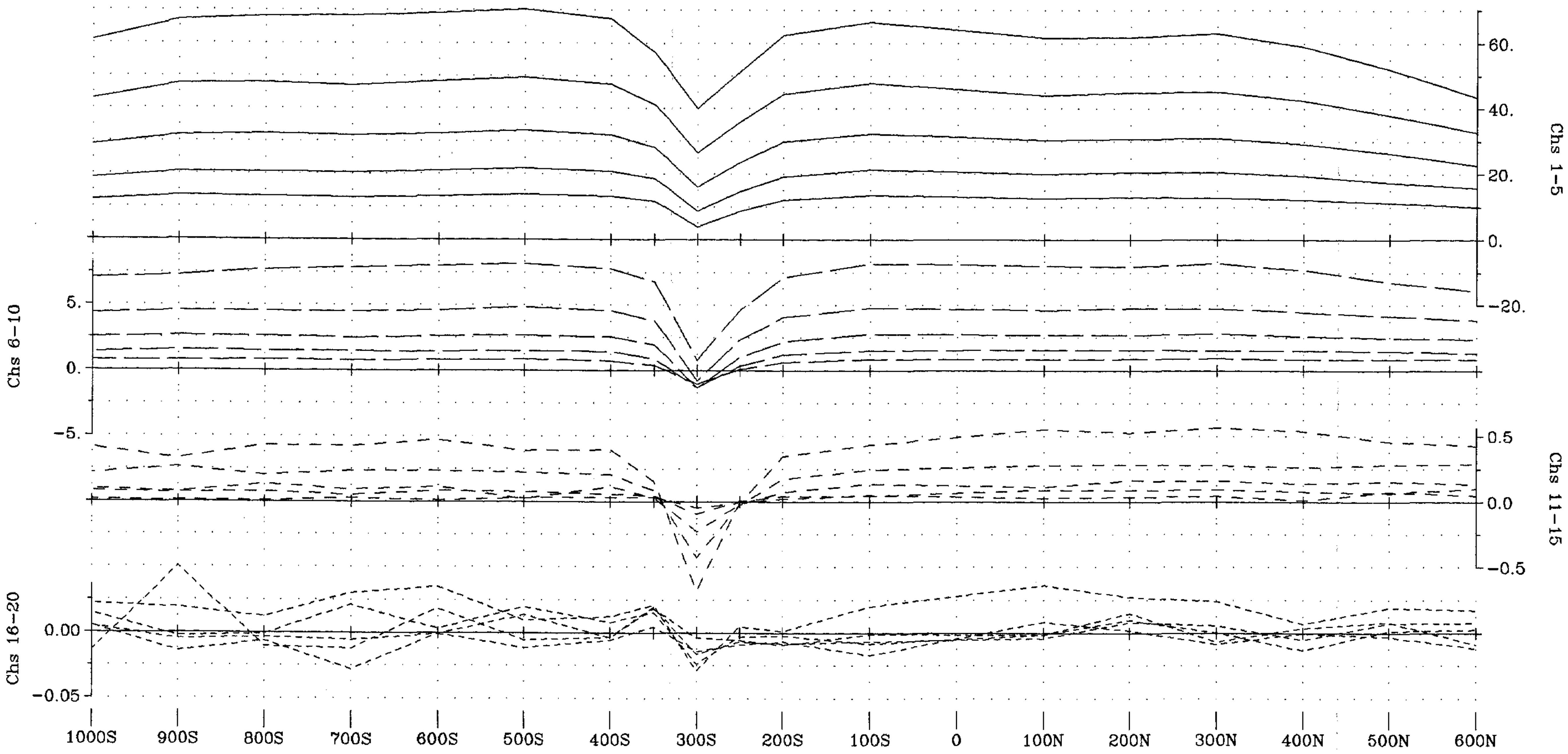
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	750m x 600m
Tx Loop Location:	Irregular; Edges 1300E, 950E
Transmitter Current:	11 Amps
Transmitter Turn-Off Time:	260 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	September 10, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Y-1200N

Plotted Fri 09-25-1998 @ 17:44:50.81



Plotted Fri 09-25-1998 @ 17:44:50.81

Line 1000E - Z Component
Echo Lake Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200

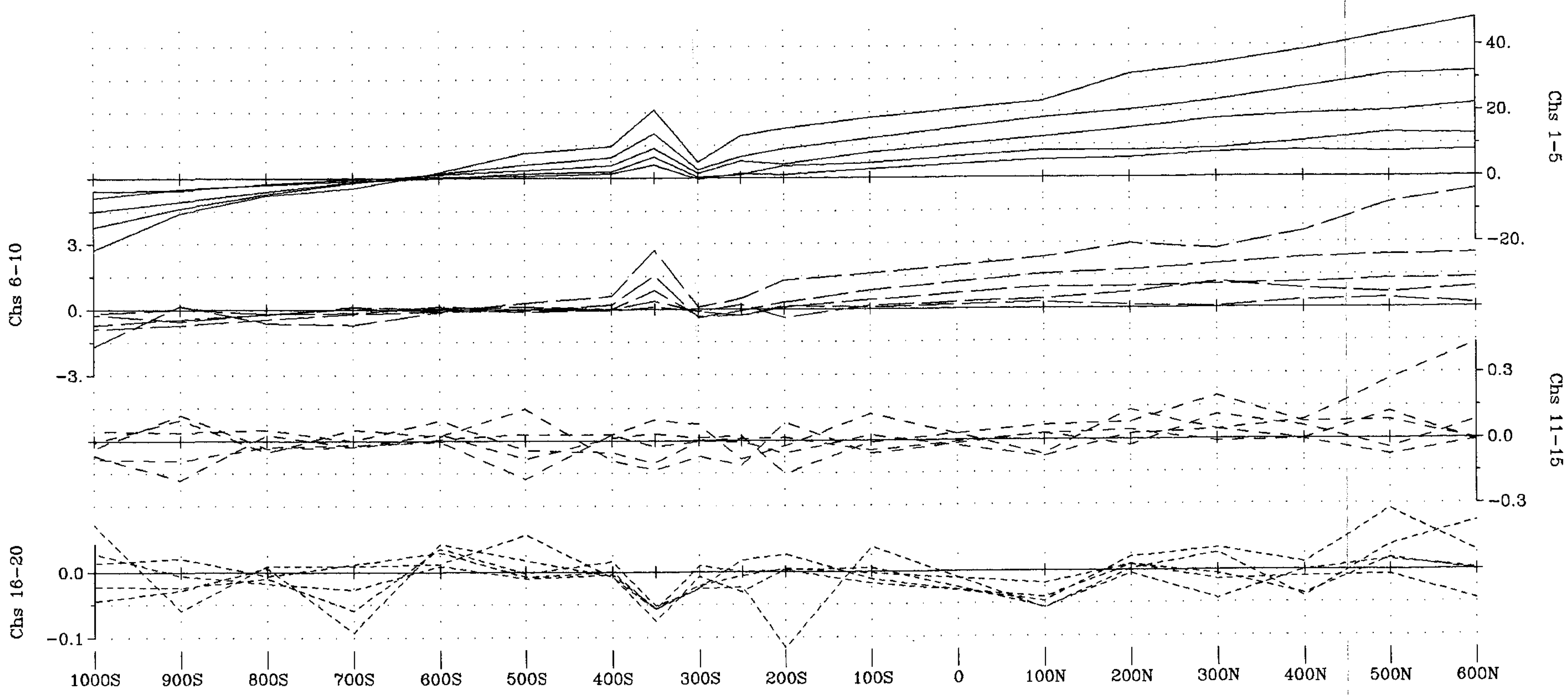
(metres)

KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	Approx. 1000m x 1000m
Tx Loop Location:	Irregular; Edges ON, 1200S
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	255 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive north
	Hy - positive west
Survey Date:	September 12, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Z-1000E



Line 1000E - X Component
Echo Lake Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

Secondary Electromagnetic Field (dB/dt)

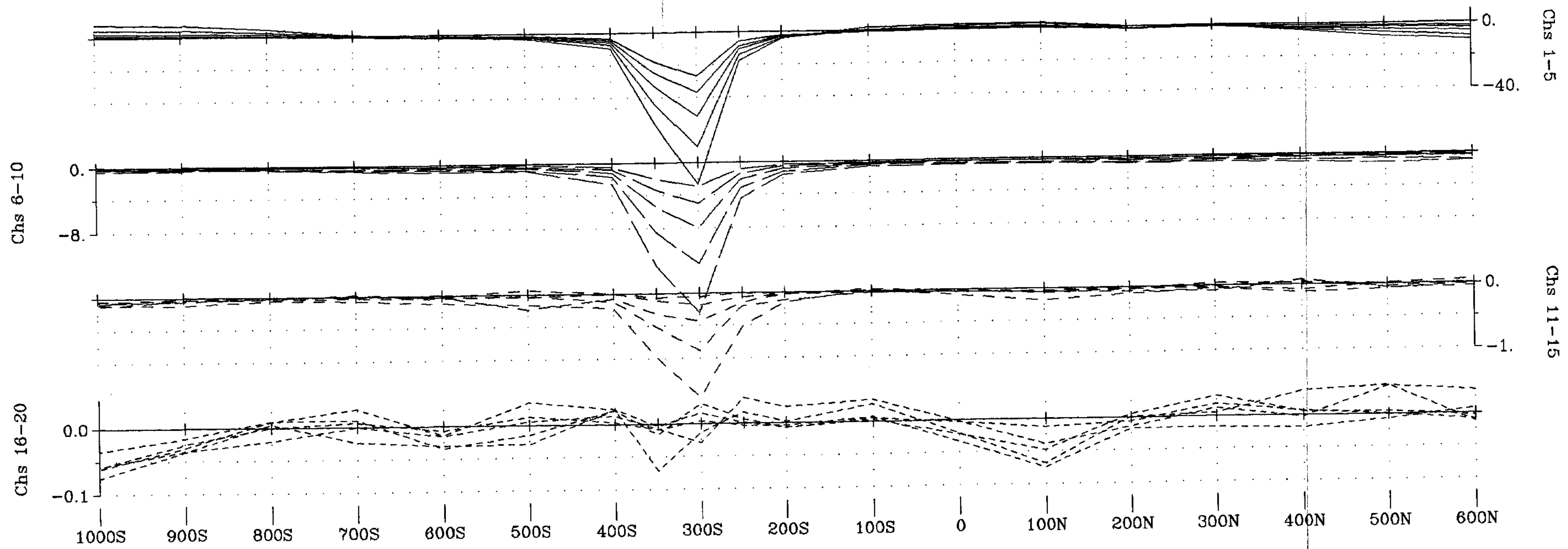
Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	Approx. 1000m x 1000m
Tx Loop Location:	Irregular; Edges 0N, 1200S
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	255 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive north
	Hy - positive west
Survey Date:	September 12, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-X-1000E

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 1000E - Y Component
Echo Lake Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

Secondary Electromagnetic Field (dB/dt)

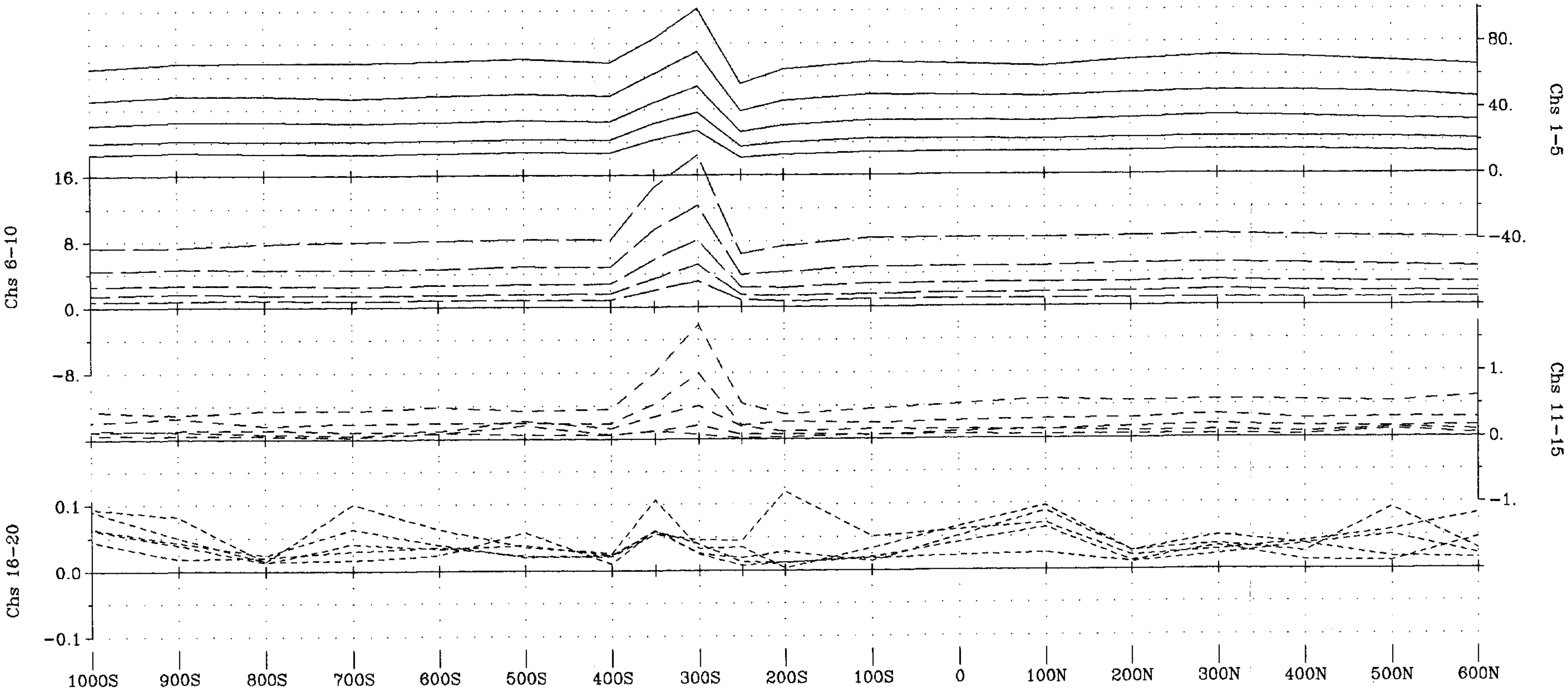
Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	Approx. 1000m x 1000m
Tx Loop Location:	Irregular; Edges 0N, 1200S
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	255 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive north
	Hy - positive west
Survey Date:	September 12, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-Y-1000E

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 1000E - Total Field
Echo Lake Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

Secondary Electromagnetic Field (dB/dt)

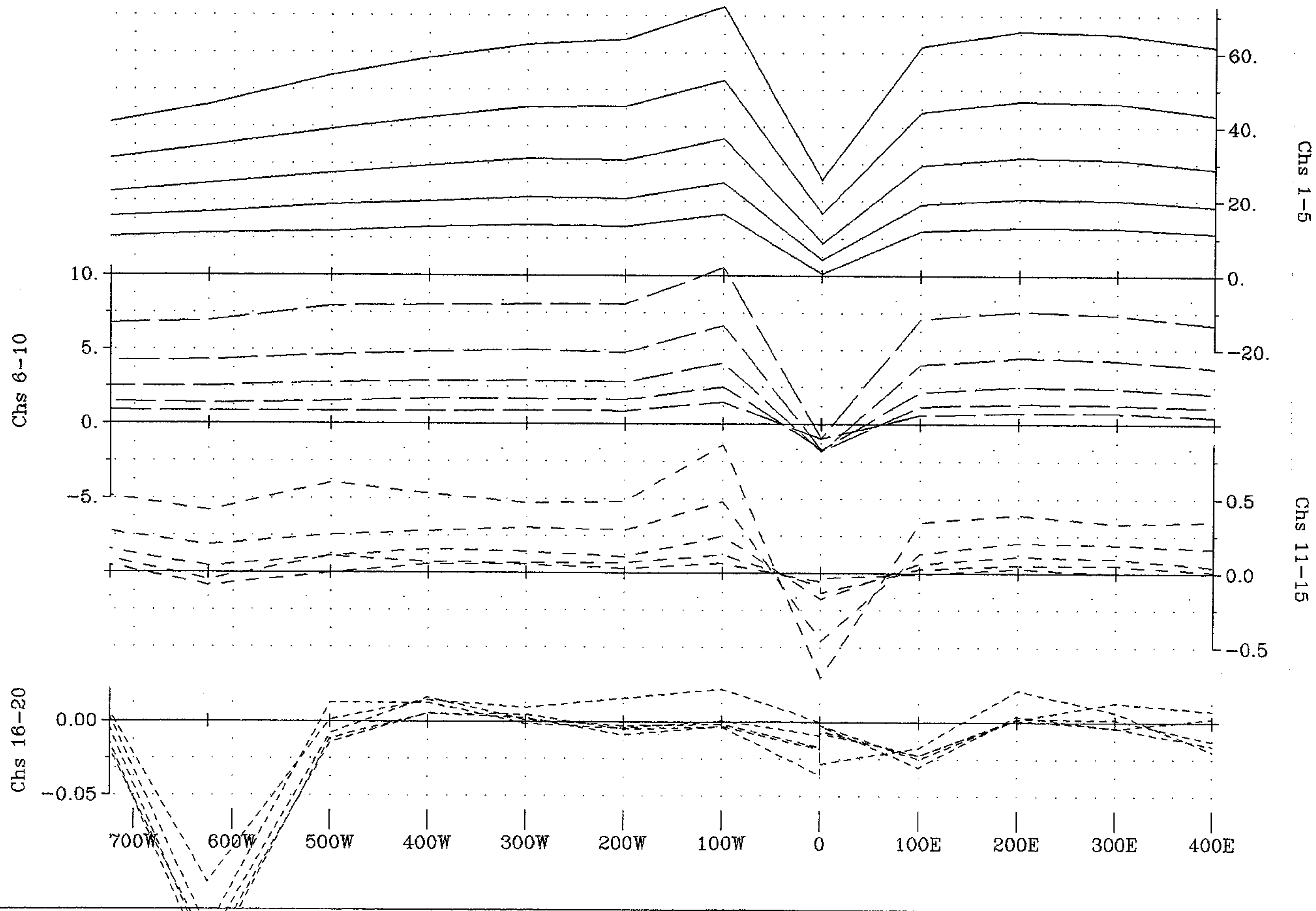
Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	Approx. 1000m x 1000m
Tx Loop Location:	Irregular; Edges ON, 1200S
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	255 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive north
	Hy - positive west
Survey Date:	September 12, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-TF-1000E

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 300S - Z Component
Echo Lake Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200
(metres)

KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

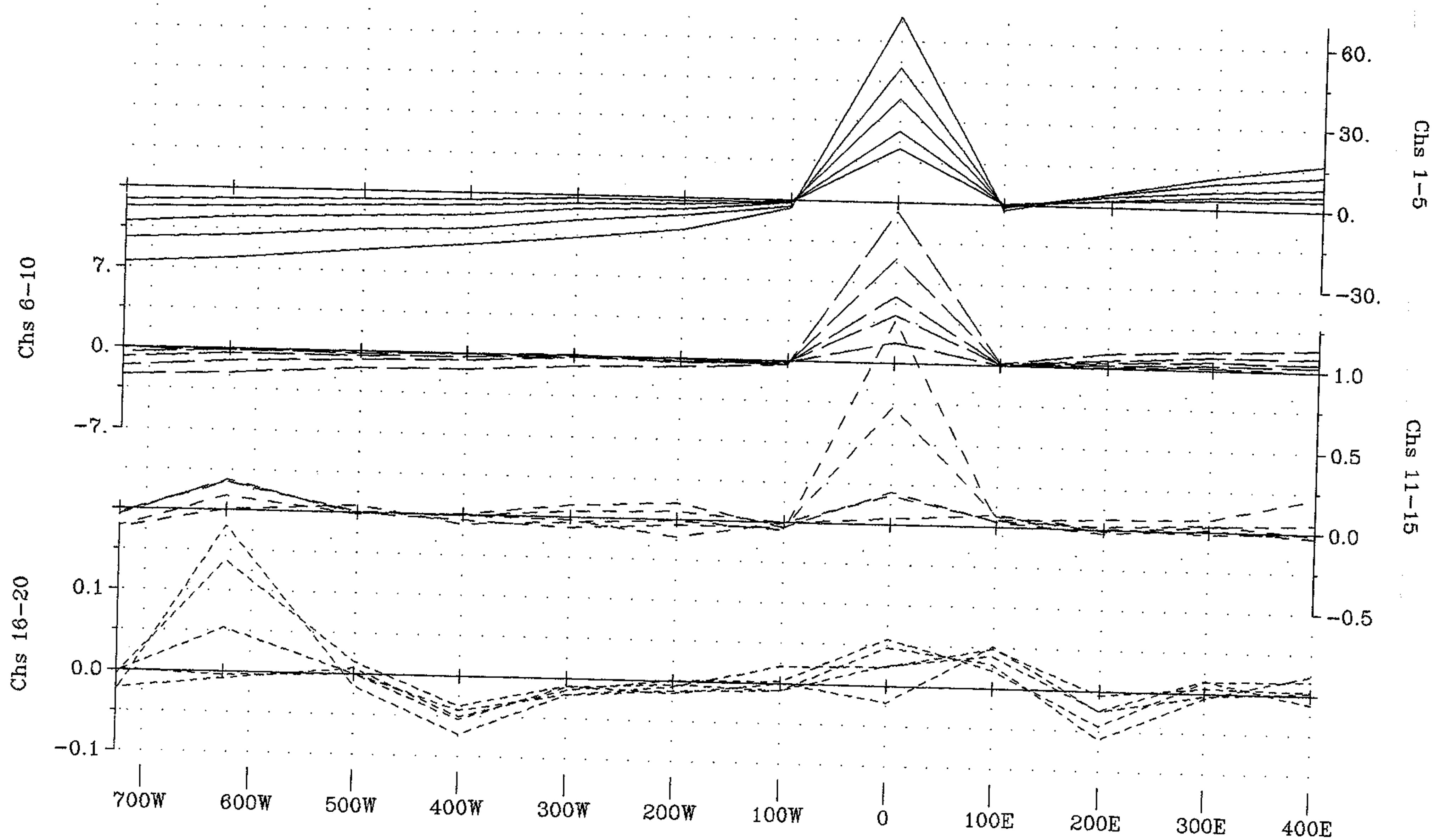
LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	Approx. 1000m x 1000m
Tx Loop Location:	Irregular; Edges 525W, 600E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	255 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 12, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Z-300S

Plotted Fri 09-25-1998 @ 17:44:50.81

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 300S - X Component
Echo Lake Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

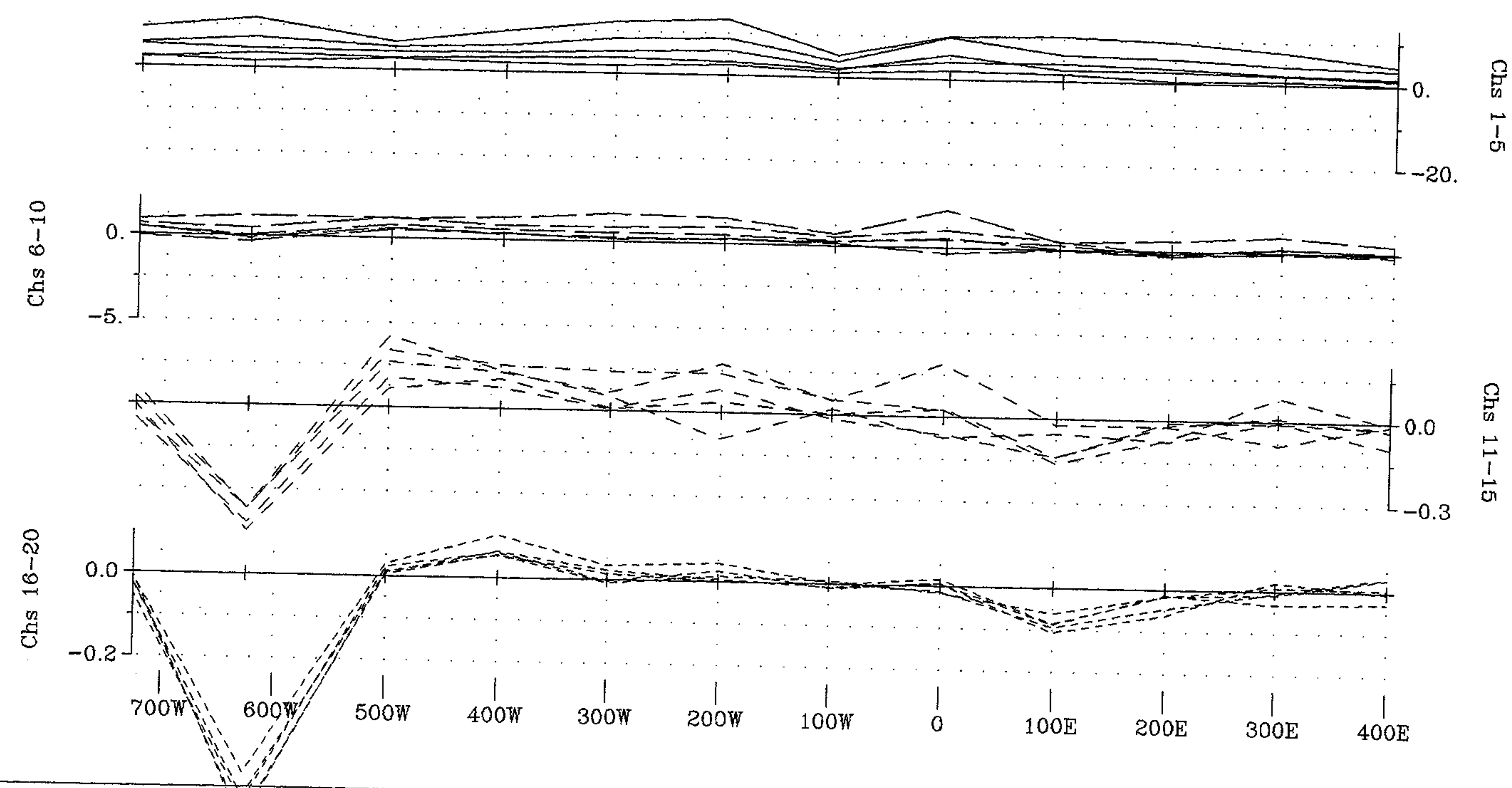
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	Approx. 1000m x 1000m
Tx Loop Location:	Irregular; Edges 525W, 600E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	255 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	September 12, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-X-300S



Line 300S - Y Component
Echo Lake Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200
(metres)

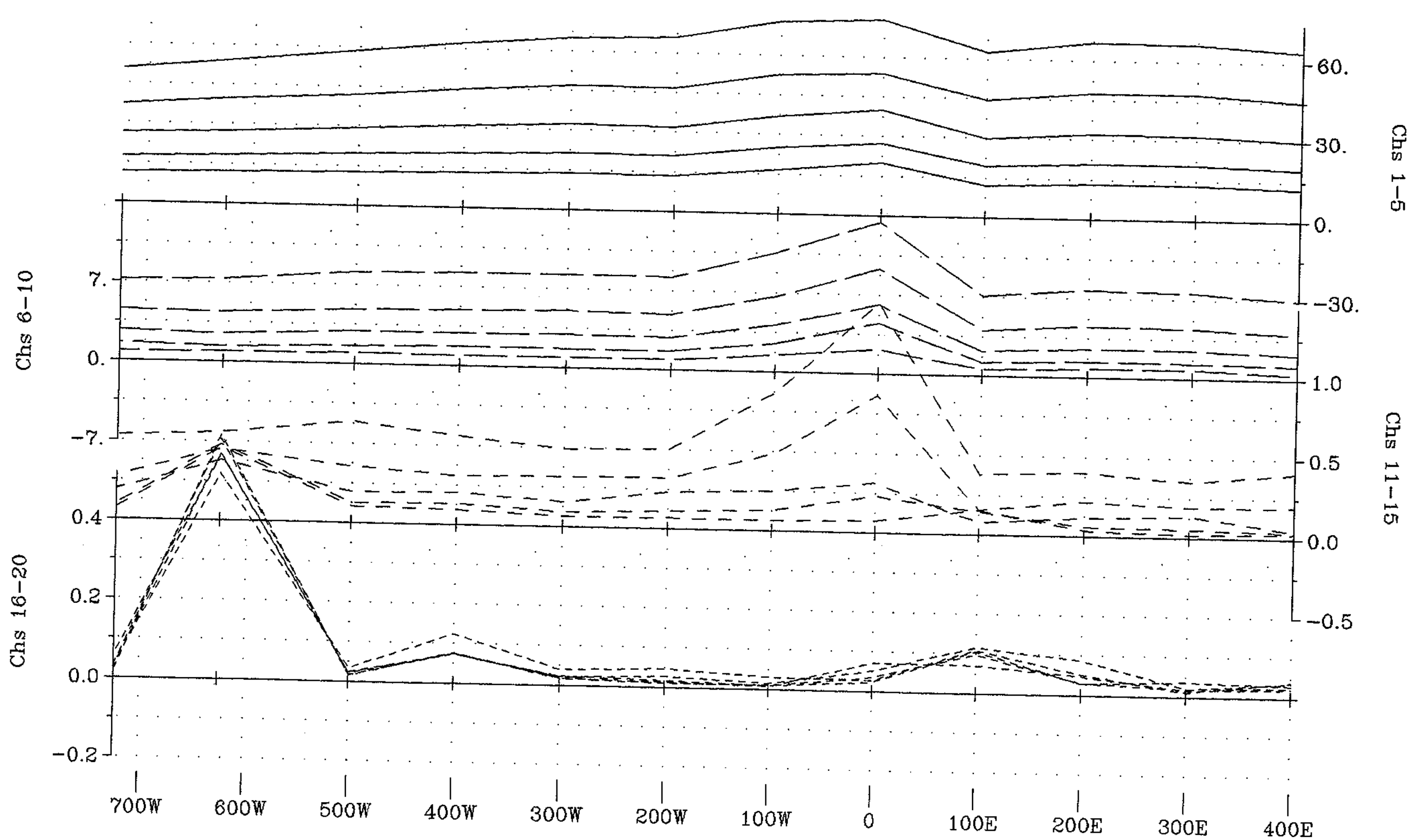
KENNECOTT CAN. EXPL. INC.
Findlay Creek Project
Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY
Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	Approx. 1000m x 1000m
Tx Loop Location:	Irregular; Edges 525W, 600E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	255 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up
	Hx - positive east
	Hy - positive north
Survey Date:	September 12, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels)
	& Geonics 3D Coil (3x200m^2)
	Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:
QUANTEC CONSULTING INC.
DWG. NO. C436-4AXIS-Y-300S

Plotted Fri 09-25-1998 @ 17:44:50.81



Line 300S - Total Field
Echo Lake Grid-Loop 1

Scale 1:5000

50 0 50 100 150 200

(metres)

KENNECOTT CAN. EXPL. INC.

Findlay Creek Project

Cranbrook, BC

LPTEM FIXED-LOOP PROFILING SURVEY

Secondary Electromagnetic Field (dB/dt)

Transmitter Frequency:	7.5 Hz (50% duty cycle)
Tx Loop Size:	Approx. 1000m x 1000m
Tx Loop Location:	Irregular; Edges 525W, 600E
Transmitter Current:	7 Amps
Transmitter Turn-Off Time:	255 us
Station Interval:	100m
Profile Units:	nanoVolt/A*m^2
Receiver Coil Orientation:	Hz - positive up Hx - positive east Hy - positive north
Survey Date:	September 12, 1998
Instrumentation:	Rx = Digital Protem (3x20 Channels) & Geonics 3D Coil (3x200m^2) Tx = Geonics EM-37 (2.8 kW)

Surveyed & Processed by:

QUANTEC CONSULTING INC.

DWG. NO. C436-4AXIS-TF-300S

Plotted Fri 09-25-1998 @ 17:44:50.81

APPENDIX XI

PETROGRAPHIC REPORTS

PETROGRAPHIC REPORT ON 15 SAMPLES FROM FINDLAY CREEK, B.C.

Report for: Rick Zuran
Kennecott Canada Exploration Inc.
#354 - 200 Granville Street
Vancouver, B.C. V6C 1S4

Invoice No. 980561

October 30, 1998

SUMMARY:

The samples submitted may be roughly divided into Moyie intrusives (gabbro, granophyre and altered equivalents: seven samples, including 55596, 55598, 55778, 55781, 55786-88) and altered meta-sediments (mostly siltstone, minor arenite; including 55595, 55777, 55780, 55782-85); one sample is a strongly altered fragmental rock (55779).

The Moyie intrusives are mostly granophyre altered or were likely granophyres before being overprinted by later phyllic (muscovite, sericite) alteration. The granophyre alteration includes major biotite after amphibole (the amphibole itself probably a product of hydrous alteration of original pyroxene during deuteric alteration of the gabbros) and development of quartz-alkali feldspar intergrowths that give the name to the alteration type (micrographic, or "granophyric" texture). However, later alteration to epidote, sericite, carbonate and chlorite has obscured this in several samples (e.g. 55598, 55778, 55781, 55786 and 55787). Only 55788 is a relatively unaltered gabbro (chloritized, epidotized; original accessory ?ilmenite altered to sphene). Sample 55596 contains significant clusters of **garnet** and is cut by veinlets of chlorite, calcite and K-feldspar; sample 55598 contains unusual quartz "eyes" that have an enigmatic origin (see comments in description). It seems likely that sample 55781 is similar to 55778 and 55786 in being a strongly phyllic (sericite, quartz +/-Fe carbonate) altered gabbro or granophyre. No galena, sphalerite, or silver oxide minerals could be identified in 55781.

The metasediments are mostly altered siltstones, composed of detrital quartz with variable amounts of interstitial relict alkali feldspar and mica (muscovite, biotite) and accessory Fe-Ti minerals such as sphene/rutile. However, several show significant **tourmaline** alteration (generally dark green to brown-coloured, Fe-rich schorl, in either irregular veins as in 55595, or layers in 55784). In the former, the wallrock appears to be moderately albitized, although there is minor K-feldspar (likely a remnant of primary mineralogy) present. In the latter, the interlayered white rock appears to be silicified; there is no evidence for albitization. Note that although considerably less in abundance, there is evidence the **fragments** in 55779 were partly tourmalinized before intense muscovite (sericite) alteration. Sample 55780 is cut by magnetite-quartz-albite veins and is thoroughly **albitized**. Sample55782 contains signifcant "clotty" alteration, with clots composed of ?galena-Fe sulfide-quartz-muscovite-chlorite-tourmaline in a silicified, albitized siltstone (+/- sericite, tourmaline).

Mineralized veins are significant in samples 55783 (Silver Key property) and 55785 (Good Boy), and in gabbro-granophyre samples 55786 and 55787. In 55783, the vein consists of quartz and Fe-carbonate plus a sulfosalt that could be ?miargyrite, as you suggest, but this cannot be confirmed without more detailed SEM or microprobe analysis. The wallrock is silicified and sericitized. In 55785, the vein consists of quartz-amphibole-**garnet**-arsenopyrite-sphalerite-pyrrhotite+/-chalcopyrite, trace ?sulfosalt (again, the latter is unidentifiable with certainty), in a quartz-biotite-**garnet** altered rock. It is unfortunately not obvious whether part of the sulfides in this sample belong to or are remobilized from an earlier ?sedex phase of mineralization. An unusual assemblage of muscovite-?beryl-?fluorite, +/- quartz, biotite and trace oxidized ?sulfide is present in the vein in sample 55786 cutting granophyritized gabbro (biotite-muscovite-quartz-limonite assemblage). The vein in 55787 is composed of quartz-amphibole-albite-arsenopyrite, cutting quartz-biotite-amhibole-sphene-?epidote altered ?granophyre. The reason for the anomalous zinc in sample 55788 is not obvious.

Craig H.B. Leitch, Ph.D P.Eng 492 Isabella Point Road, Saltspring Island, B.C. V8K 1V4 (250) 653-9158
Currently chez Levy, Hameau de Janoulie, 32360 GERS, France; 011-3356-264-5562
email Craig.Leitch@wanadoo.fr

VR55595A: FINE-GRAINED, PARTLY ALBITIZED METASEDIMENT (QUARTZ-ALBITE-BIOTITE-KSPAR-MUSCOVITE-SPHENE/RUTILE) CUT BY TOURMALINE-QUARTZ VEIN

From mapping station MB067, described as tourmaline? in albitized (meta)sediments. The rock is grey-white, sucrosic, fine-grained, with small dark dots that could be tourmaline or biotite; it is cut by an irregular black veinlet <1 cm thick that could be mainly tourmaline. The sample is not magnetic and shows no reaction to cold dilute HCl; minute crystals of K-feldspar are indicated by yellow stain in the offcut except in and along the vein. Estimated mode in thin section is approximately:

Quartz (?largely primary)	45%
?Albite (?secondary)	25%
Biotite (rarely chloritized)	10%
Tourmaline	10%
K-feldspar (?likely primary)	5%
Muscovite	3%
Sphene, rutile	1%
Opaque	1%
Apatite	<1%

Wallrock is composed of very fine-grained quartz and alkali feldspar, containing clotty concentrations of biotite +/- minor sphene/rutile. The quartz and feldspar is intimately intergrown, composed of subhedral to anhedral quartz crystals mostly <50 microns in diameter (probably largely detrital) and smaller, inter-stitial feldspar mainly <20 microns in diameter. The relief of the feldspar is distinctly negative compared to quartz; since only a portion of it stains yellow for K-feldspar, it is likely that the bulk of it is albite. Most of the small dark dots seen in hand specimen are composed of biotite, not tourmaline. The biotite forms subhedral flakes mostly <0.1 mm in diameter, commonly aggregating in clots up to about 0.35 mm in size. Minor sphene (sub- to euhedral crystals up to 50 microns in size, commonly containing tiny opaques that are likely rutile <15 microns in size) is common in the biotite clots. In places minor muscovite is associated with the biotite, as subhedral flakes up to 0.15 mm in diameter; also, some biotite is converted to chlorite in places. Minor opaques less than 0.1 mm in diameter could include ?sulfides but are usually associated with sphene and therefore more likely to be ?rutile. Tourmaline is rare in the wallrock, forming small (<50 micron) subhedral crystals. Rare apatite crystals are rounded to subhedral and <35 microns in diameter (likely primary).

The "vein" is actually a loose agglomeration of clotty tourmaline concentrations that are roughly circular in shape, up to almost 1 cm in diameter, and composed of subhedral schorl crystals mostly less than about 0.35 mm in size. Pleochroic colours are greenish-blue to dark brown, implying a high Fe:Fe+Mg (F:M) ratio, likely 0.8 to 0.9. The rest of the "vein" consists mostly of subhedral quartz (up to 0.3 mm in diameter), plus minor muscovite (to 0.1 mm) and rare apatite (to 75 microns). There are no opaques associated with the vein (i.e., no sulfides).

In summary, the field description appears to be accurate: a fine-grained metasediment that has been partly albitized (although K-feldspar is present, likely remnant primary), and is cut by a tourmaline-bearing irregular veinlet.

VR55596A: GRANOPHYRE (BIOTITE-QUARTZ-ALKALI FELDSPAR-CHLORITE-GARNET-EPIDOTE) ALTERED GABBRO; FRACTURES OF CHLORITE-CARBONATE-KSPAR

From mapping station SM087, described as ?garnet in gabbro; stained offcut shows a dark green-grey, medium-grained intrusive rock containing scattered clots of pink garnet up to 0.5 cm in diameter, and cut by rare narrow stringers that stain yellow for K-feldspar. The rock is weakly magnetic but shows no reaction to cold dilute HCl; estimated mode in thin section is approximately:

Biotite	45%
Quartz	25%
Chlorite	7%
Relict plagioclase	5%
K-feldspar (?mainly secondary)	5%
Amphibole	5%
Garnet	3%
Opaque (?ilmenite, magnetite)	1-2%
Epidote/clinozoisite	1-2%
Carbonate (veinlets)	1%
Apatite	<1%
Sphene	<1%

This sample should more properly be termed a granophyre than a gabbro; it retains the gabbroic intrusive texture, but the original pyroxene and amphibole is almost completely replaced by biotite and chlorite plus minor opaques and apatite, and the interstitial feldspars almost completely replaced by quartz and secondary feldspars plus minor epidote/trace carbonate. Garnets form irregular clusters up to almost 6 mm in diameter, composed of subhedral crystals mostly <0.5 mm in diameter, that in part appear to replace former mafic sites, but also locally contain abundant quartz that may be largely secondary.

Former mafic sites appear to have been subhedral, up to about 2.5 mm in size. Amphibole is relatively uncommon, forming sub- to euhedral dark green crystals up to 0.5 mm long preserverd either in the cores of biotite clusters, or else crystals <0.1 mm long in relict feldspar. Throughout much of the slide, amphibole is pseudomorphed by chlorite (subhedral flakes up to 0.3 mm in diameter, with moderate green pleochroism and length-fast birefringence indicating moderately high Fe content, F/M perhaps 0.5-0.6). Biotite forms subhedral dark brown flakes mostly <0.35 mm in diameter, in places altered to chlorite, carbonate, and epidote.

Opaques form rounded clusters up to about 0.35 mm in diameter, commonly associated with mafic sites. Traces of sphene around the margins of the opaque clusters suggest the opaques could be mostly ?ilmenite, with minor magnetite admixed as indicated by weak magnetism in hand specimen. Apatite is common in some areas, forming euhedral prisms up to 0.2 mm long.

Former feldspar sites with rounded to subhedral outlines up to 1.5 mm in size are mostly occupied by quartz (likely mostly secondary) as subhedral crystals up to 0.3 mm in diameter, in places mixed with lesser relict alkali feldspar (partly K-feldspar where near fractures, and partly relict ?plagioclase, likely albitic, as subhedral relics up to 0.35 mm long that contain minor fine-grained epidote to 0.1 mm and rare carbonate to 50 microns).

Narrow veinlets, mostly <0.1 mm thick, are composed of chlorite and carbonate as subhedra up to 0.1 mm in diameter, and in places K-feldspar of similar size.

In summary, this sample appears to represent a granophyre (biotite-quartz-alkali feldspar altered gabbro) that in addition contains coarse clots of garnet +/- quartz.

VR55598A: CARBONATE-CHLORITE-EPIDOTE ALTERED GRANOPHYRE (BIOTITE-QUARTZ-ALKALI FELDSPAR ALTERED FINE-GRAINED GABBRO) WITH RARE QUARTZ EYES

From mapping station MB013, described as dark grey, brown weathering, calcareous intrusive with quartz eye in fine-grained matrix). The sample reacts strongly to cold dilute HCl, but is not magnetic and shows only traces of yellow stain for K-feldspar in the etched slab (possibly along a fracture). Estimated mode in thin section is approximately as follows:

Carbonate (?mostly calcite)	30%
Biotite	25%
Chlorite	20%
Relict alkali feldspar (albitic; rare Kspar)	10%
Quartz (partly secondary)	10%
Epidote	3%
Sphene	<1%
Allanite	<1%
Apatite	<1%
Sphalerite	tr

As deduced in the field, this fine-grained gabbroic rock is extensively carbonatized; it likely was also a granophyre prior to this alteration. Amphibole is no longer present; all mafic sites are altered to biotite and chlorite, and lesser plagioclase feldspar sites are altered to alkali feldspar, carbonate and epidote. Rare quartz eyes are rounded in outline, composed of single clear crystals up to 2 mm in diameter, generally overgrown by finely crystalline carbonate. Thus they could be either phenocrystic or amygdular in origin; I have seen similar occurrences before in the gabbros at Sullivan, but could not conclusively determine their origin (although at Sullivan some contain highly saline fluid inclusions similar to those in the quartz vein stockwork underlying the orebody, suggesting they could be fragments of vein quartz).

Former mafic sites that made up over half of the rock are generally <1.5 mm in diameter, now pseeudomorphed by carbonate, biotite and chlorite plus very fine-grained sphene and /or epidote; in places, clusters or sprays of epidote crystals, possibly mixed with a little sphene, appear to mark the sites of former sphene (and likely before that, ilmenite) crystals up to 0.5 mm in diameter. Carbonate forms fine rounded subhedra mostly <0.1 mm in diameter; biotite mostly forms pale brown flakes up to 0.25 mm in diameter, and chlorite forms subhedral flakes up to almost 0.75 mm in diameter. Rarely, however, there are larger, subhedral, bent brown biotite flakes up to 1.25 mm in diameter with ragged terminations that could rrepresent former ?phenocrysts. Chlorite flakes are almost colourless and are length-fast, and with first-order grey birefringence indicating moderately Mg-rich composition (F/M perhaps 0.3-0.4). Epidote in places forms crystals up to 0.2 mm in diameter with strong yellow pleochroism indicating high Fe content. Rare apatite crystals are sub- to euhedral prisms up to 0.15 mm long; brownish coloured "epidote" crystals to 0.15 mm diameter could be allanite (REE-bearing epidote commonly found in Aldridge rocks and gabbros). Extremely rare bright red crystals <20 microns in size could be sphalerite.

Former feldspar sites are harder to detect, possibly of 1 mm size or smaller, now replaced by ragged aggregates of carbonate, epidote, and quartz plus relict alkali feldspars, all mostly <0.1 mm (commonly <50 microns) in diameter. In these areas, epidote does not appear to be pleochroic and so may be of low Fe content (clinozoisite). Alkali feldspars are difficult to detect and identify, but are likely mostly albitic with minor to rare K-spar.

In summary, this appears to be a strongly carbonate-chlorite-epidote altered , fine-grained gabbro or more properly granophyre (biotite-quartz-alkali feldspar altered gabbro). The origin of the quartz eyes is enigmatic.

VR55777A: FINE SILTSTONE (DETRITAL QUARTZ, PLAGIOCLASE, WHITE MICA, RARE TOURMALINE) ALTERED TO CARBONATE AND WITH CLOTS OF LIMONITE-?SPHALERITE

From mapping station NT118 (VR55735A); described as containing hydrozincite in fine-grained, thick bedded calcareously altered siltstone. Stained offcut is a fine-grained, even-textured, relatively homogeneous rock except for lensed and disseminated specks of pale brownish material (that are slightly harder than the rest of the rock, i.e. not as easily scratched by steel). The rock is not magnetic and shows no reaction to cold dilute HCl, and no stain for K-feldspar; estimated mode in thin section is approximately:

Quartz	50%
Carbonate (?partly dolomitic)	20%
Plagioclase	15%
Muscovite, sericite	10%
Opaque (?sulfide, limonite)	1-2%
Sphalerite	1-2%
Sphene, rutile	1%
Tourmaline	<1%

In the thin section, the pale brownish areas are evidenced by areas of more abundant limonite; thus they may merely represent more oxidized portions of the sample. In general, the slide consists of fine-grained quartz with intersitial carbonate, plagioclase and white mica, marked by common clotty concentrations of opaques and carbonate (+/- sphene, rutile) that make up about 5% of the rock.

Quartz forms mainly subhedral crystals, likely mostly detrital grains, up to about 0.15 mm in diameter separated by a "hash" of mainly finer-grained carbonate, plagioclase and white mica. The plagioclase is only separable from the quartz where it displays fine polysynthetic twinning; there is no appreciable relief difference from quartz. Thus the extinction angle on 010 of up to about 15 degrees may indicate a composition near oligoclase-andesine (not common, but not unheard of , particulary where associated with otherwise calcareous alteration, e.g. at the Fors property). Alternatively, but less likely, the composition could be albitic and the relief difference being masked by the ubiquitous presence of fine-grained sericite. The form of the plagioclase does not suggest a secondary origin; it looks like primary detrital feldspar. Carbonate crystals are generally sub- to euhedral, up to 0.15 mm in diameter, and could be partly dolomitic, especially in the clotty concentrations. Mica flakes are ragged to subhedral and rarely over 0.1 mm in diameter; some may represent former ?biotite, and some may be detrital. It is not clear whether some may replace former feldspar; in spite of the abundant carbonate, the overall appearance of the rock is not suggestive of muscovite alteration. Rare tourmaline crystals are euhedral, up to 0.15 mm long, and greenish to brownish (likely schorlitic, with F/M perhaps 0.7-0.8; most likely they are detrital as well, and not due to hydrothermal activity).

Opaques in the clots could be partly iron sulfide or their limonitized relics, but appear to also be partly ?sphalerite (red-brown, moderate Fe content) based on 1) presence of hydrozincite and 2) isotropic character under crossed polars, whereas the limonite is anisotropic. Both the relict ?Fe sulfides and the ?sphalerite form subhedral crystals up to about 0.2 mm in diameter, and are mainly interstitial to the detrital quartz grains. Carbonate crystals are also interstitial, and appear to have higher relief than carbonate outside the clots, suggesting it may be in part dolomitic (or be mixed with a little sphene and or rutile).

In summary, this sample appears to be a relatively unaltered sediment consisting of detrital quartz, plagioclase feldspar and mica plus rare tourmaline and containing significant clotty concentrations of iron and zinc sulfides (although part or most of the carbonate may well be secondary).

VR55778A: INTENSELY PHYLLIC (QUARTZ-SERICITE-SULFIDE) ALTERED ?GABBRO, CUT BY QUARTZ-SERICITE-?PYRRHOTITE-?SPHALERITE VEIN; SIGNIFICANTLY OXIDIZED

From mapping station NT200 (VR55761A); described as sphalerite vein with disseminated pyrite in gabbro in shear. Offcut shows a pale greenish-grey, altered fine-grained gabbro cut by a rusty, limonitic shear (vugs in places, possibly in secondary quartz). The rock is magnetic in places, shows no reaction to cold dilute HCl, and no stain for K-feldspar in the etched offcut. Estimated mode in thin section is approximately:

Quartz (?largely secondary)	45%
Muscovite (largely secondary)	35%
Opaques (limonite)	10%
(?pyrrhotite)	3%
(sphalerite)	1-2%
Carbonate (?ankerite or siderite)	5%
Amphibole (?)	1-2%
Sphene	<1%

Although the rock is strongly stained by limonite due to weathering of the sulfides and transport of the limonite, a strongly phyllic altered ?gabbro is distinguishable, composed now mostly of quartz and muscovite away from the central vein system.

The wallrock consists of an aggregate of quartz (subhedral to anhedral crystals up to 0.5 mm in diameter, commonly with a secondary appearance) and abundant muscovite (generally euhedral crystals up to 0.4 mm in diameter) plus intersitial limonite. Feldspar and relict mafic sites are no longer distinguishable due to the strong alteration. In places there is minor carbonate, most of which has relatively high relief, is strongly altered to limonite, and since it does not react to HCl in the offcut, may be Fe/Mg rich (ankerite or ?siderite). Near the vein there are minor amounts of a bright green pleochroic mineral with tabular form that may be ?amphibole as subhedra to 0.15 mm long, commonly mixed with the muscovite.

The central vein system is poorly defined due to the shearing, weathering and oxidation (transported limonite blurs the boundaries) but appears to be composed mainly of oxidized sulfides and areas of quartz and fine-grained sericite. Oxidized sulfides are not directly identifiable, lacking a polished surface to examine, but look to be mostly Fe-sulfides (likely partly oxidized pyrrhotite to judge by the magnetic character), largely coated and replaced by limonite. In places there are relicts at the center of limonitic areas that appear to be isotropic under crossed polars, suggesting the presence of minor sphalerite (?).

In summary, I would characterize this sample as an intensely sericite-quartz altered ?gabbro cut by a quartz-sericite-?pyrrhotite-?sphalerite vein that has been strongly oxidized to limonite. It is not clear whether any of the former sulfide (e.g. in the wallrock) was pyrite; pyrrhotite seems more likely.

VR55779A: INTENSELY MUSCOVITE (+/-TOURMALINE) ALTERED CLASTS IN COARSE-GRAINED MUSCOVITE-QUARTZ-BIOTITE-LIMONITE (?AFTER SULFIDE) MATRIX

From mapping station SM (559950mE, 5543275mN); descibed as meta fragmental? 60% subrounded clasts, muscovite matrix. The clasts are up to about 1 cm in diameter and are dark grey, in places containing elongated black needle-like crystals of ?tourmaline up to several mm long. The matrix stains pale yellow in the etched offcut, confirming muscovite; the rock is not magnetic and shows no reaction to cold dilute HCl. Estimated mode in thin section is approximately:

Muscovite, sericite	65%
Quartz (?partly secondary)	15%
Biotite	10%
Opaque (limonite)	5%
Tourmaline	5%

This slide is made up of about 40% clasts and 60% matrix. The clasts are rounded to subrounded in outline and are composed principally of very fine-grained muscovite (sericite) and slender prismatic crystals of tourmaline, plus scattered opaques. The matrix is mainly composed of coarser-grained muscovite with lesser, variable amounts of quartz and in places significant biotite or opaques (mainly limonite); minor tourmaline also occurs.

In the clasts, sericite forms fine flakes mostly <50 microns in diameter. Tourmaline crystals are up to 1.5 mm long and have very deep green to blackish pleochroism, suggesting very high Fe content (schorl, with F/M perhaps 0.9). The tourmaline crystals tend to be clustered in the center of the clasts, and the muscovite tends to be coarser at the margins of the clasts, in a sort of progression (or recrystallization) towards the matrix. Most of the opaques are pseudomorphs of limonite, but they have subhedral to euhedral outlines up to 0.4 mm in diameter, suggesting they are after former sulfides such as ?pyrrhotite.

In the matrix, muscovite flakes are subhedral, with ragged terminations, up to about 0.75 mm in diameter (rarely to 2.5 mm). Quartz is interstitial and forms subhedral to anhedral crystals up to 0.25 mm in diameter. Biotite forms mainly fine,, sub- to euhedral flakes < 0.15 mm in diameter (rarely to 0.35 mm), with deep greenish brown to blackish pleochroism; in places biotite forms up to 25% of the matrix. Opaques are mostly discrete, pseudomorphic grains of limonite that could be after former significant quantites of sulfide such as ?pyrrhotite, but in places there azre also modest amounts of interstitial, transported limonite derived from the weathering of the sulfides.

In summary, this sample looks to be an intensely muscovite (sericite) altered fragmental rock, with significant tourmaline (especially in the clasts) and possibly significant Fe-sulfide before weathering and oxidation. Certainly a "prospective" sample due to the tourmaline content; it could come from the LMC as far as the lithology is concerned, although obviously I have not seen the field setting. It is possible (although not conclusive) that the muscovite, or sericite, alteration is due to the Cretaceous batholith, which is accompanied by sericitic alteration elsewhere in the district.

VR55780A: MAGNETITE-QUARTZ+/-ALBITE VEINS IN INTENSELY ALBITE-QUARTZ ALTERED ARENITE

From mapping station RZ (VR55984A); described as tan brown oxidized, bleached, quartz arenite with trace magnetite in stringers along fracture. The magnetite is partly associated with quartz veining sub-parallel to beddiing (aggregate veins up to about 6 mm thick); some irregular veinlets of quartz and ?feldspar are cross-cutting to bedding. The rock shows no yellow stain for K-feldspar in the etched offcut (and no reaction to cold dilute HCl). Estimated mode in thin section is approximately as follows:

Quartz (mainly detrital; minor secondary)	50%
Alkali feldspar (?albite)	40%
Magnetite (veins)	5%
Sericite	3%
Opaque (Fe-Ti oxides; wallrock)	2%
Zircon	tr

This is a thoroughly altered and veined (stockworked) rock, composed principally of quartz and albitic alkali feldspar that may both be largely secondary, cut by veins of magnetite and quartz plus minor alkali feldspar.

Typical wallrock consists of rounded to anhedral, likely originally detrital, grains of quartz up to about 0.2 mm in diameter, in a matrix of mainly finer-grained, anhedral, tightly interlocking crystals of alkali feldspar with distinctly negative relief compared to quartz, and minor fine-grained quartz, sericite, and opaques. The feldspar is not twinned, but the negative relief of the feldspar and lack of yellow stain in the offcut suggests it is mostly albite. Individual crystals are generally <25 microns in diameter. Interstitial sericite, or fine-grained muscovite, is generally <25 microns in diameter (<10 microns where present in feldspar), and is commonly intergrown with or in places stained by opaque (mainly limonite, or possibly Fe-Ti oxides such as rutile and leucoxene). Rare euhedral crystals of zircon are up to 45 microns long, probably relict detrital grains.

Veins are everywhere in this rock, ranging from the obvious 0.5 cm thick planar veins down to a network of fine (<0.1 mm thick) microveinlets or fractures that are barely distinguishable from the matrix. Most veins are composed mainly of quartz, forming subhedral to rounded crystals up to about 0.65 mm in diameter; in places, subhedral to anhedral, rarely polysynthetic twinned, crystals of plagioclase (?albite) are seen. Magnetite occurs as subhedral crystals or aggregates mostly <0.5 mm in diameter, partly oxidized at rims and along fractures to ?hematite.

This would appear to be classic albite-quartz-magnetite alteration, both vein controlled and (in the case of the albite and quartz) pervasive.

VR55781A: INTENSELY FE-CARBONATE, MUSCOVITE, QUARTZ ALTERED ?FINE-GRAINED GABBRO (POSSIBLY ORIGINALLY GRANOPHYRE ALTERED); FE-CARBONATE VEINED

From mapping station RZ044 (VR55891A); described as blue-black, strongly oxidized, phyllitic, quartz arenite with PbOx?, MnOx, galena, limonite and sphalerite; possible silver oxide minerals. The offcut appears to be a greyish, sheared, veined/stockworked, ?arenite rich in quartz and muscovite (sericite). It is weakly magnetic, but shows no stain for K-feldspar, and no reaction to cold dilute HCl (even after scratching), in the etched offcut. Estimated mode in thin section is approximately:

Carbonate (?ankerite, siderite)	40%
Muscovite	35%
Quartz (?partly secondary)	20%
Opaque (largely Fe-Ti oxides?; limonite)	3%
Sphene, rutile	1-2%
Apatite	<1%

In thin section, the overall texture and mineralogy, plus abundance and texture of opaques, suggest that this rock is actually a highly altered gabbro, not an arenite. The veins (which are buff-coloured in hand specimen) are carbonate, presumably Fe-carbonate such as ankerite or ?siderite to judge by the lack of reaction (although etching by HF does sometimes interfere with the subsequent ability to react to HCl). The bulk of the slide is composed of a fine-grained, heterogeneous aggregate of carbonate, muscovite (sericite) and quartz; relict alkali feldspar could also be present, but cannot be distinguished due to lack of twinning or relief difference against the quartz. The abundance of carbonate is not typical of arenites in the Aldridge, supporting the hypothesis of an altered Moyie intrusive as the precursor rock.

Carbonate forms mainly subhedral, interlocking crystals mostly <0.2 mm in diameter. Distribution of the carbonate, and intergrowth with muscovite, suggests the replacement of former mafic sites in a gabbro. Muscovite forms subhedral flakes and booklets up to 0.2 mm in diameter, containing minor interleaved ?sphene and rutile that suggest the muscovite could be after relict ?biotite crystals, i.e. the gabbro could have been granophyre altered. The presence of small (<0.1 mm long) euhedral prisms of apatite reinforces the possiblity of an altered gabbro.

This hypothesis is supported by the abundance of quartz (rather high for the average gabbro), which normally accompanies biotite in granophyre alteration. Quartz occurs as mostly anhedral to subhedral, interlocking, ragged crystals commonly containing inclusions of muscovite, that could have been intergrown with alkali feldspar, together as a replacement of former feldspar sites.

Opaques are commonly confined to clusters or clots with (in places) subhedral outlines suggestive of former crystals of ?ilmenite or ilmeno-magnetite; the trace remnant magnetism supports this contention. The opaques appear to be mostly ?rutile or possibly ilmenite, and are commonly surrounded by a rim of transparent ?sphene. However, some clusters of opaques contain cubic-shaped crystals or pseudomorphs, possibly indicating limonite replacement of sulfides such as pyrite. At the margins of the sample, there is a weathered rind up to about 4 mm thick containing significant limonite and possibly Mn-oxides; I do not see any indications of galena, sphalerite or silver oxide minerals. Presumably you have geochemical indications to support those identifications; however, a polished thin section would be required, possibly accompanied by SEM (scanning electron microscope) analysis, to confirm their presence.

Veins, mostly less than 2.5 mm in thickness, are composed principally of coarse-grained, subhedral, interlocking Fe-carbonate crystals up to about 1 mm in diameter.

In summary, I believe this sample is best explained as an intensely carbonate-sericite altered and Fe-carbonate veined, likely originally granophyre altered, fine-grained Moyie intrusive (gabbro).

VR55782A: ALTERED (SILICIFIED, ?ALBITIZED, MINOR SERICITIZED) SILTSTONE; CLOTS OF OXIDIZED SULFIDE-MUSCOVITE-?CHLORITE-TOURMALINE

From mapping station NT210 (VR55774A); described as orange/white, strongly oxidized, moderately bleached (?argillic alteration), thick bedded siltstone with 5% galena. The offcut shows a grey-white, blotchy-textured, fine- to medium-grained, siliceous rock, with abundant red-brown limonite on weathered surfaces; there is no yellow stain for K-feldspar,and no reaction to cold dilute HCl, and the rock is not magnetic. Estimated mode in thin section is approximately:

Quartz (?partly secondary)	45%
Opaque (mainly limonite; some ?galena)	25%
Alkali feldspar (?albite)	20%
Muscovite, sericite	5%
Chlorite	2-3%
Tourmaline (schorl)	1%
?Pb-oxides or ?jarosite	<1%
Unidentified (?allanite)	<1%

This sample is so heavily overprinted with limonite that it is difficult to see the rock. However, it appears to be mostly composed of quartz, with interstitial, partly sericitized alkali feldspar.

Quartz forms subrounded to anhedral, likely mostly originally detrital, grains up to 0.25 mm in diameter that are separated by a "hash" of finer-grained (mostly <35 micron) anhedral, interlocking, variably altered alkali feldspar crystals. The feldspar has distinctly negative relief compared to the quartz and is therefore likely albitic. Rarely, polysynthetic twinning is visible, with extinction on 010 up to 12 degrees. In places the feldspar is replaced by up to 10% fine flakes of sericite (mostly <25 microns in diameter).

Scattered "clots" of opaque and limonite, plus muscovite, are similar to peripheral alteration and mineralization seen near Sullivan (for instance, on North Star Hill. near the base of the ski runs and on the ski slopes). Opaques consist of both ?sulfides (could be galena and/or iron sulfides, the former surrounded by narrow, generally <0.1 mm thick rims of ?Pb oxide or ?jarosite, but without a polished surface it is not possible to be sure). Limonite is bright red-brown and abundant; no sphalerite, which would be isotropic under crossed polars, is identifiable. Minor green-brown tourmaline (schorl, F/M perhaps 0.7) forms subhedral and in places ragged prisms up to 0.25 mm long, that commonly appear to be related to or more abundant in and near the clots. Muscovite flakes are subhedral to somewhat ragged, up to 0.25 mm in diameter; in places they are intergrown with a low birefringence, but length-fast, micaceous mineral that could be chlorite (fairly Fe-rich), but is also so Fe-stained that it is hard to be sure they are not Fe-stained muscovite. Aggregates up to 0.3 mm across composed of an unidentified, moderately high relief but low birefringence mineral are also found in some of the clots; I am not sure what this mineral is, but it could be ?allanite, but it usually shows radiation-damaged haloes around it if it is near chlorite, and these haloes are not evident in this sample.

In summary, this sample does appear to be an altered siltstone (possibly silicified and albitized, partly sericitized, and with minor but likely hydrothermal tourmaline) that contains clotty concentrations of sulfide-muscovite-?chlorite-tourmaline and sulfides (likely including ?galena but now mainly converted to limonite). This type of alteration is typical of the periphery of mineralized systems in the Aldreidge (such as North Star Hill - Sullivan).

VR55783A: SILICIFIED, SERICITIZED SILTSTONE CUT BY IRREGULAR VEINLETS OF QUARTZ FE-CARBONATE AND SULFOSALT; RARE ARSENOPYRITE

From Silver Key property, described as tan/brown, moderately silicified siltstone with miargyrite? in stringers along fractures. Offcut is grey to tan and fine-grained, composed mainly of quartz with minor interstitial feldspar (does not stain yellow for K-feldspar) and is cut by narrow stringers of quartz and later sulfides or sulfosalts. The rock is not magnetic and shows no reaction to cold dilute HCl; estimated mode in polished thin section is approximately as follows:

Quartz (partly secondary)	65%
Sericite (mainly after feldspar)	25%
Alkali feldspar (sericitized)	3-5%
Carbonate (?ankerite/siderite)	3-5%
Sulfosalt (could be miargyrite)	1-2%
Rutile	<1%
Arsenopyrite	tr

The bulk of this slide is composed of relatively fine-grained quartz and interstitial sericite (likely mostly after feldspar, but some could be after former ?biotite). However, there is a good deal of secondary silica, in the form of coarser overgrowths, finer pervasive material, and poorly organized veinlets (some with significant sulfide content). There are also veinlets of carbonate.

In general, former ?detrital grains of quartz are subhedral to subrounded in outline and up to about 0.35 mm in diameter. Interstices are filled by fine-grained sericite (ragged to subhedral flakes mainly < 20 microns in diameter) but there are also scattered flakes of muscovite up to 0.1 mm in diameter, that could be ?detrital. The distribution of the fine-grained sericite is clearly after former alkali feldspar that formed anhedral to subhedral crystals, <0.1 mm in diameter; traces of this feldspar remain in places, but most are completely sericitized. Traces of ?rutile form clusters of 10-25 micron crystals in some mica and carbonate clusters.

Carbonate is scattered throughout the rock, forming small subhedral crystals mostly <0.1 mm in diameter, also interstitial to the quartz and possibly replacing former ?mafic or feldspar crystals. The high relief of this carbonate and the lack of reaction in the offcut suggests it may be Mg- or Fe-carbonate (dolomite or ?ankerite).

Secondary quartz is generally coarser, forming subhedral crystals that range up to almost 2 mm in diameter and have ragged, scalloped borders along which they are intergrown with other quartz crystals or muscovite (ragged flakes up to 0.5 mm in diameter), minor carbonate (ragged subhedra to 0.25 mm diameter) or, in places, sulfides. However, there is a progression from carbonate-poor veins to those with abundant carbonate (euhedral crystals up to 2.2 mm long, possibly ankerite or ?siderite since they are commonly strongly altered along fractures and rims to limonite).

Opaques include sulfosalts similar in reflectance to galena but mainly anisotropic, forming sub- to euhedral crystals up to 0.5 mm in diameter and possibly containing rounded blebs of ?another sulfosalt up to 0.2 mm long (distinguished by more pronounced anisotropism, although this could be a function of the orientation of the crystals and there only be one sulfosalt present), and euhedral rhombs of arsenopyrite to 0.25 mm diameter (mainly scattered in the wallrock). The optical properties (reflectance, colour, anisotropic colours) and habit are certainly permissive for miargyrite, but this is not conclusive. In general, it is not possible to identify sulfosalts, particularly Ag-Sb-Pb sulfosalts, with certainty, without at least SEM and usually microprobe analysis.

VR55784A: INTERLAYERED TOURMALINITE (SCHORL, QUARTZ, SERICITE) AND SILICIFIED SILTSTONE (QUARTZ, SERICITE, TOURMALINE) CUT BY QUARTZ-TOURMALINE-?PYRITE

From mapping station RZ036 (VR55867A); described as off-white, bleached siltstone with dark grey acicular tourmaline bands <1 cm thick. Offcut shows interbedded black ?tourmaline layers and white ?albite or silicified beds, cut by a black and white breccia or brecciated vein of similar but comminuted material. The vein or breccia is also distinguished by minor amounts of red-brown ?limonite (or partly oxidized Fe-carbonate). The rock is not magnetic, and shows no reaction to cold dilute HCl (even where powdered) and no stain for K-feldspar in the etched offcut. Estimated mode in thin section is approximately:

Quartz (partly secondary)	50%
Tourmaline (schorl)	35%
Sericite (muscovite)	13-15%
Opaque (limonite after ?pyrite)	1-2%
?Rutile	<1%

Pale-colured bands in this sample are composed primarily of quartz and minor interstitial sericite, with scattered tourmaline crystals. The quartz crystals are very fine-grained (anhedral and average about 50 microns, but rarely up to 0.1 mm and subhedral). They may represent mainly detrital grains that have been partly recrystallized and overgrown by secondary silica. Sericite, or muscovite, forms subhedral to euhedral flakes mainly <30 microns in diameter. Tourmaline "crystals" are mainly green to brown and consist of somewhat ragged aggregates of 20-30 micron crystals with subhedral outlines up to 0.15 mm long. Opaques look to be minute (10-20 micron) euhedral, dark brown (?Fe-rich) crystals of ?rutile.

Dark-coloured bands are composed primarily of tourmaline with minor interstitial quartz and sericite. Tourmaline crystals are subhedral to euhedral, up to 1 mm long, and dark brown to green in colour (indicating schorl with a relatively high F/M ratio possibly up to 0.8 or 0.9). They have the same recrystallized look as the disseminated crystals in the pale-coloured bands, but are coarser and less obviously composed of small sub-domains. Quartz forms subheddral interlocking crystals up to 0.15 mm in diameter; sericite forms interstitial flakes up to 30 microns in diameter that appear in places to ?replace tourmaline, but this may be an erroneous impression. Minor opaques appear to be mostly interstitial and largely limonite, although there may be traces of rutile also. The limonite appears to be after former ?sulfide such as ?pyrrhotite, or in one clot (see below) where coarser (up to 1.5 mm) pseudomorphs have cubic to rectangular outlines, could be after ?pyrite.

The brecciated portion of the sample is composed of coarse, sub- to euhedral crystals of quartz up to3.5 mm in size, containing euhedral limonite pseudomorphs and clots of needle-like to extremely fine (felted) tourmaline, similar in composition to that in the main body of the rock. This portion of the rock is clearly a vein when seen in thin section, cutting off the tourmalinite layers in the rock.

Thus this sample is confirmed as interbedded intensely tourmalinized ("tourmalinite") and ?silicified rock, with minor to possibly significant oxidized remnants of sulfide in some places.

VR55785A: QUARTZ-AMPHIBOLE-GARNET-SPHALERITE-ARSENOPYRITE-PYRRHOTITE VEIN IN QUARTZ-BIOTITE-GARNET-SPHENE ALTERED SILTSTONE

From the Good Boy prospect, described as <2 cm widequartz vein with sphalerite, silver/arsenic sulfide on selvages, in light grey siltstone. Offcut shows 2-3 cm diameter pink (Mn-rich) clots of garnet in the dark grey, micaceous wallrock adjacent to and ?included in the vein. Both the vein and wallrock are slightly magnetic but show no reaction to cold dilute HCl and no stain for K-feldspar. Estimated mode in polished thin section is approximately:

Quartz (largely secondary, vein)	55%
Biotite (partly chloritized)	15%
Garnet	10%
Amphibole (?tremolite-actinolite)	10%
Sphalerite	3-5%
?Arsenopyrite	3-5%
Pyrrhotite	1-2%
Sphene	<1%
Chalcopyrite	tr

Wallrock consists mainly of a fine-grained aggregate of quartz and biotite, with minor sphene and sulfides, hosting scattered large clusters of garnet. In general, quartz occurs as subangular to anhedral grains mostly <0.1 mm in diameter and probably mostly relict detrital in origin, in a matrix of fine subhedral (25-75 micron) pale brown biotite flakes. However, in places the quartz is organized along narrow fractures or veinlets (mostly <0.5 mm thick), and in these the quartz forms subhedral to anhedral crystals up to 0.3 mm in diameter, mixed in places with minor amphibole; minor amphibole also occurs along the selvages of these veinlets, as for the major vein (see below). Garnet occurs as clusters up to 3 mm in diameter composed of sieve-like crystals that contain abundant inclusions (of amphibole, quartz and biotite, plus minor ?sphene). Amphibole cyrstals are subhedral to ragged and up to 0.25 mm long, with pale green pleochroism suggesting a member of the ?tremolite-actinolite series, and in places partly altered to fine flakes of secondary biotite. The garnet appears to be completely isotropic and unzoned.

The major vein is composed of coarse, subhedral to anhedral crystals of quartz that in places are optically continuous for up to almost 1 cm, although showing undulose extinction and other signs of strain. Most are smaller and subhedral, less than about 1.5 mm in maximum dimension, and relatively unstrained. The vein contains stringers and schlieren of sulfide and highly altered wallrock that mostly consist of amphibole (colourless subhedral crystals that may be more Mg-rich, less Fe-rich than in the wallrock) but in places also consist of abundant biotite and garnet plus scattered clusters of sphene or ?rutile. Garnet crystals are in general more euhedral and less sieved by inclusions than the crystals in the wallrock; they are however all isotropic and unzoned. In places the garnet crystals are set in a matrix of chlorite (subhedral flakes to 0.15 mm with optical characteristics (near-zero to length-fast birefringence, very pale green colour, non-pleochroic) suggestive of median F/M near ?0.4-0.5; the chlorite may be after biotite. Sphene forms ragged, shapeless clusters up to 0.5 mm across composed of subhedra mostly <50 microns in diameter.

Sulfides include bright red-brown sphalerite (with moderate Fe content indicated by the colour) forming mainly subhedral crystals up to 0.5 mm diameter but aggregating to 1.5 mm, and rhombic to needle-shaped crystals of arsenopyrite up to 0.5 mm long, plus minor pyrrhotite as subhedral to rounded crystals mostly <0.3 mm in diameter. Most of the pyrrhotite appears to be peripheral to the arsenopyrite (i.e., surrounds it as discontinuous layers) and is partly oxidized (shows lamellar to bird's-eye texture typical of weathering and replacement by pyrite/marcasite, but is still magnetic as indicated in hand specimen). The arsenopyrite contains rare subhedral chalcopyrite crystals up to 0.1 mm in diameter and traces of fresh pyrrhotite up to 20 microns in diameter, plus rare inclusions of a silvery mineral that could be galena or a silver sulfosalt (at 20 microns, too small to detect anisotropism).

Thus the vein contains zinc, iron, and arsenic; traces of silver could be present in the inclusions in the arsenopyrite. In response to your question about the origin of the various sulfides, I am sorry that there does not appear to be any obvious separation into a vein or remobilized, or pre-vein, ?sedex sulfide assemblage. Such questions are usually better defined with larger-scale features than with petrographic-scale observations. The presence of garnet both in the vein and the altered wallrock is interesting, especially if it could be analysed by SEM or probe and found to be manganiferous; this might suggest the observed vein mineralization is in part a remobilization of former sedex mineralization.

VR55786A: INTENSELY MUSCOVITE-BIOTITE+/-QUARTZ, ?SULFIDE ALTERED GRANOPHYRE OR GABBRO CUT BY MUSCOVITE-BIOTITE-?BERYL-?FLUORITE+/-?SULFIDE VEIN

From mapping station RZ052 (VR55957A); described as brown, micaceous, recrystallized and strongly oxidized gabbro, with small veinlets that seem to be anomalous in Zn and W, plus ?beryl, muscovite and quartz (similar veinlets occur as sheets in Lower Aldridge). The offcut shows a dark, strongly altered gabbro traversed by a 1-2 cm thick, coarse-grained quartz vein; the offcut is not magnetic and shows no reaction to cold dilute HCl or stain for K-feldspar. Estimated mode in thin section is approximately as follows:

Wallrock		**Vein**	
Biotite	40%	Muscovite	60%
Muscovite	40%	?Beryl	30%
Quartz (?secondary)	10%	?Fluorite	5%
Opaque (limonite, ?sulfide)	10%	Biotite	3%
		Opaques (limonite)	2%

Wallrock consists of sprays of intergrown, fine-grained pale brown (partly "bleached", or sericitized) biotite, forming subhedral flakes mostly <0.1 mm in diameter, and coarser, more euhedral crystals of muscovite (up to 0.35 mm in diameter), in places mixed with a little quartz (anhedral, likely secondary crystals up to 0.7 mm indiameter) plus minor opaques. The opaques are all basically limonite, with outlines that vary from subhedral, up to 0.7 mm in diameter (could be pseudomorphs after ?pyrrhotite; associated with the coarser quartz) to transported interstitial stains of mostly <25 microns in diameter. The overall impression is of an intensely altered gabbro that may have been granophyre altered initially and then been largely muscovitized (sericitized) adjacent to the vein.

The vein consists of an unusual mineralogy in that quartz is relatively rare (as in the wallrock) and instead is composed mainly of mica and what appears to be ?beryl and minor ?fluorite. The mineral tentatively identified as beryl has all the right optical characteristics: low birefringence (weak first-order grey, similar to apatite but slightly lower); positive relief compared to quartz; negative sign (length-fast), and forms slender elongated prismatic crystals up to 4 mm long that in places show minor 0001 parting, or in cross section have rounded to hexagonal outlines. Most of the mica is coarse, euhedral muscovite (up to about 1.5 mm in diameter) but in places there is also minor very pale, washed-out looking ("bleached") biotite to about 0.5 mm in diameter. Fluorite (?) forms subhedral crystals or masses up to 3 mm in diameter that are isotropic and have negative relief, and a moderately well-developed cleavage at somewhat more than right angles. Quartz forms relatively uncommon, large rounded to anhedral crystals up to 2 mm in diameter with positive optic sign distinguishing them from ?beryl.

The assemblage muscovite-beryl-quartz-?fluorite in veins, with Zn and W (and usually Sn) is something I would associate with Cretaceous granites (which are certainly known in the area, and on the other side of the ridge from your camp, early exploration was focussed on such vein mineralization in several large trenches in the cirques at the head of Greenland Creek). The critical question in sedex exploration in that area is, how much of the anomalous Zn is due to (remobilized) sedex mineralization and how much to introduction by the Cretaceous intrusives?

VR55787A: FOLIATED, GRANOPHYRE (QUARTZ-BIOTITE-AMPHIBOLE-SPHENE-?EPIDOTE) ALTERED GABBRO CUT BY QUARTZ-AMPHIBOLE-ALBITE-ARSENOPYRITE VEIN

From station VR55896A, described as brown, foliated, medium-grained, strongly oxidized gabbro with 3% blebby arsenopyrite, trace pyrite along a fracture plane. The offcut shows a dark green gabbro with an altered texture, cut by a <1 cm thick vein of quartz and sulfides (arsenopyrite, ?pyrrhotite that is weakly magnetic). There is no reaction to cold dilute HCl and no stain for K-feldspar; estimated mode in thin section is approximately:

Quartz (?partly secondary; vein)	45%
Biotite (brown and green)	35%
Amphibole (?hornblende)	7%
Plagioclase (?albite;vein)	5%
Opaques (?arsenopyrite, pyrrhotite)	5%
Sphene	1-2%
Unidentified (??allanite or epidote)	1%
Apatite	<1%

The bulk of this section consists of an intergrowth of quartz and biotite crystals with a somewhat layered texture; some of the ill-defined layers, which are generally less than about 1 mm in thickness, contain scattered amphibole, minor sphene and an unidentified mineral that could be ?allanite. Quartz forms small subhedral crystals mostly <0.1 mm in diameter, commonly in lensey to subrounded aggregates or domains up to about 1 mm in diameter, with a tendency to elongation parallel to the foliation of the rock; these domains are suggestive of the sites of former ?feldspar crystals. The foliation is mostly defined by alignment of biotite flakes, which are mostly pleochroic from pale yellow to dark brown and <0.25 mm in diameter, but in some layers are mixed with bright green pleochroic crystals up to 0.5 mm in diameter (probably distinctly Fe-rich to judge by their colour). Amphibole is generally not important in these layers except near the vein. Sphene is important in some layers, forming small sub- to euhedral crystals up to 0.25 mm in diameter; this abundance and distribution of sphene is typical of all gabbros in the Aldridge. In some layers, minor amounts of another mineral with lower relief and lower birefringence than sphene are difficult to identify with certainty, but could be ?allanite or merely epidote; they form rounded to subhedral crystals up to 0.1 mm in diameter, but lack obvious radiation-damaged haloes around them. Rare apatite forms subhedral crystals up to 0.1 mm long, concentrated in the mafic layers which probably represent sheared-out, altered former mafic minerals.

The vein consists of quartz, amphibole, biotite, plagioclase and sulfides. In the vein, irregular bunches or lenses of quartz consist of subhedral crystals up to 1.25 mm in diameter showing slight evidence of strain (undulose extinction, some sub-grain development). Amphibole forms very dark green subhedral crystals up to 1 mm long (could be hornblende) commonly intergrown with, but not obviously replaced by, the biotite. Biotite forms subhedral crystals up to 0.3 mm in diameter with pale yellow to dark brown pleochroism. Sulfides, based on hand sample examination only, appear to be mostly arsenopyrite but may also include minor ?pyrrhotite (no polished surface to examine). In places, the vein contains medium- to coarse-grained, subhedral to rounded crystals of ?plagioclase up to 1.5 mm in diameter, distinguished by hosts of fine (micron-sized) inclusions and relief apparently negative compared to quartz. This suggests that the composition is likely albitic (no yellow stain for K-feldspar in the etched slab). Twinning is only rarely seen and is very poorly defined.

This gabbro has probably been strongly granophyre altered, and has been foliated,but does not appear to me to be strongly oxidized (e.g. the fresh sulfide).

VR55788A: GABBRO (AMPHIBOLE-PLAGIOCLASE-?ILMENITE) ALTERED TO CHLORITE-EPIDOTE-SPHENE AND MINOR LIMONITE

From mapping station RZ025 (VR55854A); described as green, equigranular, medium-grained, strongly chloritized gabbro with anomalous zinc geochemistry. Offcut shows a fairly typical gabbro without obvious signs of mineralization except rare clots of red-brown ?limonite or sphalerite. The sample is not demonstrably magnetic and shows no reaction to cold dilute HCl and no stain for K-feldspar in the offcut; estimated mode in thin section is approximately:

Amphibole (?hornblende)	40%
Plagioclase (altered, relict)	35%
Chlorite (after amphibole)	10%
Epidote (after plagioclase)	10%
Sphene	3-5%
Opaques (?ilmenite; included in sphene)	<1%
Limonite	<1%

This is actually a fairly fresh (unaltered), non-granophyre altered gabbro which retains traces of its original igneous texture with subhedral amphibole and ragged, altered plagioclase relics both of around 1-2 mm size.

Amphibole crystals are generally subhedral, up to 1.5 mm in diameter, and have pale green pleochroism suggesting hornblende or ?actinolitic hornblende. Some of the better preserved crystals contain trails of micron-sized inclusions suggestive of former Schiller structure (a characteristic texture of pyroxenes that likely formed the precursor to most of the amphibole in the Moyie intrusives). The more altered crystals are attacked at the margins by fine, fibrous ?secondary amphibole (needles mainly <0.25 mm long) and then by surrounding or cross-cutting chlorite (subhedral flakes up to 0.2 mm diameter, with optical characteristics such as strong green pleochroism and length-slow birefringence indicating moderate Fe content, F/M perhaps 0.5).

Plagioclase crystals are only vaguely twinned or zoned and show moderate to strong alteration to fine epidote and lesser chlorite (both as subhedral crystals mostly <50 microns in diameter; the epidote is relatively colourless, implying low Fe content). The composition of the plagioclase is no longer determinable due to the alteration, and lack of quartz to compare refractive indices with, but the general appearance and abundance of epidote suggests a fairly calcic composition.

Accessory minerals are mainly euhedral to subhedral aggregates of sphene or sphene with cores of ?ilmenite, in places partly oxidized to limonite. It is likely these that are seen as red-brown aggregates in the offcut, as no iron sulfides, limonite pseudomorphs after sulfides, or sphalerite can be seen in the thin sectdion. The sphene crystals are subhedral and up to 1 mm across; ?ilmenite is corroded to rounded and generally <0.5 mm in size. Limonite mostly forms amorphous stains interstitial to silicates, presumably due to transport of material from oxidizing Fe-Ti oxides.