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Geological, Geophysical, and Geochemical Report

-- on the --

Lottie Claims

Cariboo Mining Division
British Columbia

-- for --

Eureka Resources, Inc
#1000 - 355 Burrard Street
Vancouver, B.C. V6C 2G8

Located: - 53 14'N; 121 36'W,
- 93H/4E, and
- 14 km north of Wells, B.C.

Prepared By:

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November 15, 1999

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SUMMARY

Discovery of massive sulphide float occurrences in at least three different locations in the eastern Cariboo area is indicating the presence of a new volcanogenic massive sulphide (VMS) camp in central British Columbia. Work by Eureka Resources, Inc. in 1998 on the Bow property has identified potential sources of the Bow float area (1 - 3% copper) and the Tow float area (2 - 7% copper, 3 - 5g/t gold, 50 - 70g/t silver, and 0.5 - 1% zinc). Prospecting the general area of the Antler Formation as part of its 1998 program, led to the discovery of the Lottie float area, consisting of several boulders and cobbles of massive sulphides containing 10 - 24% copper. This led to the staking of the Lottie claims, located 10 km south of the Bow property.

The Bow project consists of 52 claims (522 units) and the Lottie project consists of 4 claims (56 units), all recorded in the name of Eureka Resources, Inc. It is understood that additional claims are currently being located (~300 claim units) linking the two claim blocks.

The Lottie claims are located in central British Columbia in the Cariboo Mining Division, approximately 14 km north of the village of Wells. Access is possible via a network of logging roads to the most portions of the claim area. The claims are located on the northwest side of Two Sisters mountain, and covers much of the Lottie creek valley and Lottie lake. A large part of the claim area has been the subject of clear-cut logging, and is currently in various stages of secondary revegetation.

The northern portion of the property is underlain by volcanic rocks of the Mississippian Antler Formation. Rocks are mainly an intermediate to basic sequence of volcanic flows and tuffs, with at least one phyllitic mudstone unit conformably lying within the volcanic lithology, striking 090 - 110 degrees and dipping 35 - 60 degrees north. The Pundata thrust traverses the southcentral portion of the property. To the south of the thrust older Ordivician to Devonian sediments occur. Along the thrust, small listwanite intrusions are common. The float occurrence of massive sulphides is located in the area underlain by the Antler Formation.

The mineralized Lottie float is located over an area of 15x20 meters, and the distribution of boulders and cobbles is suggestive of a train trending to the south and east. At least twenty boulders of massive sulphides have been discovered, with several additional boulders of stringer sulphides in chert. The dominant sulphides are chalcopyrite (75 - 80%), chalcocite (5 - 10%), pyrite (5 - 10%), and minor bornite.

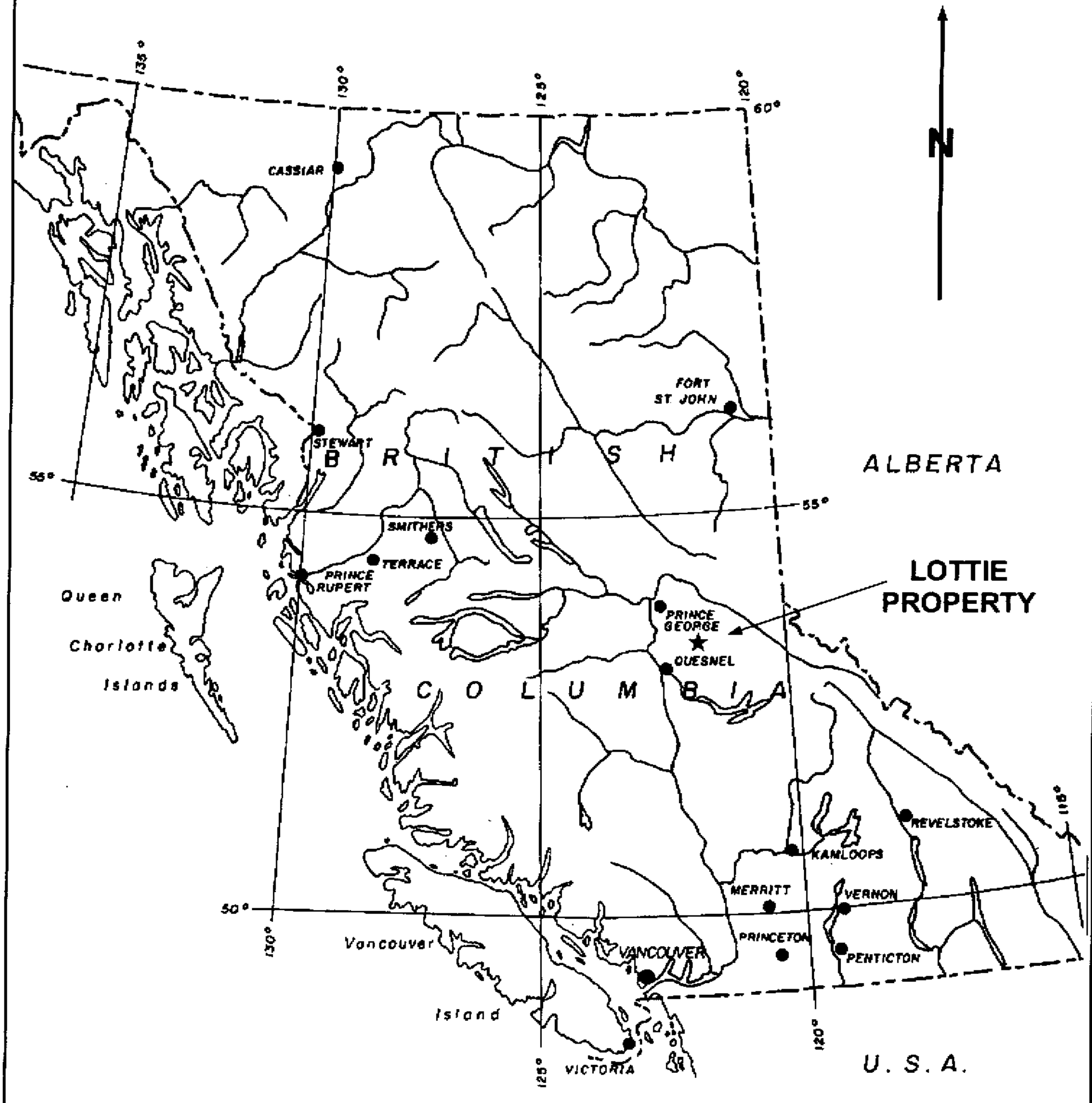
The 1999 field program consisted of a glacial study of ice-flow patterns; a 15.5 km grid being established; 9.8km VLF-EM survey; 13.8km HEM survey; collection of 559 "B" horizon soil samples; collection of 113 basal till samples; 110 meters of trenching; and geological mapping. The program was completed at a cost of **$68,825.**

The results of the 1999 exploration conclude that a likely source of the massive sulphide float has been located. The most compelling data set is the moderate/strong, well-defined conductor interpreted from the HEM survey. The axis of the conductor parallels and superimposes on the footwall zone of the 30 - 100 meter wide sedimentary unit. This conductor is interpreted over a strike length of 900 meters (open), and attains conductivity of 2 - 30 siemens. The conductor is located 200 - 600 meters south and east of the float location (upslope and up-ice). The strength of the conductor is compatible with the conductivity of hand specimens of the massive sulphides.

The conductor is associated with a well-defined "B" horizon copper soil anomaly. The shape and location of the anomaly is reasonably compatible with the conductor and favourable lithology, realizing "B" soils would have downhill, down ice, and hydromorphic dispersion. Lead, zinc and silver distribution in soil is also related to the favourable lithology.

Trenching was completed by excavator in the immediate area of the Lottie float to study the nature and distribution of mineralized float. Trenching was also completed on the interpreted HEM conductor axes to investigate potential causes of the conductor. In most cases, the overburden was deeper than anticipated (5 - 8 meters), therefore bedrock could not be thoroughly examined. In two trenches, massive blebs of pyrite, with trace contents of chalcopyrite were encountered in bedrock at what is believed the contact of a volcanic/sedimentary horizon in the Antler Formation, the mineralization associated with chert. In addition, several small pieces of float were discovered in this area containing disseminated and massive blebs of chalcopyrite, with lesser amounts of galena, sphalerite, and native copper. This contact area in the lithologic sequence is interpreted as a potential host for the massive sulphides.

A 1500 meter drill program (10 holes) is recommended to test the nature, mineral content, and extent of the interpreted conductor as the next phase of exploration. Included with the recommendations for drilling are additional detailed gridwork, an airborne geophysical survey and follow-up surveys.



EUREKA RESOURCES INC.

LOCATION MAP

LOTTIE PROPERTY

Cariboo Mining Division, B.C.

Scale: 1:2,500,000 Figure: 1

INTRODUCTION

General Statement

The Mississippian Antler Formation of rocks of central British Columbia has been regarded as a favourable rock type for the occurrence of volcanogenic massive sulphide (VMS) deposits for the past two decades. This interest was heightened in the early 1980s with the release of regional geochemical data. During the late 1980s and early 1990s several major mining companies embarked on grass-roots exploration programs in a 7500 square kilometer area east of Prince George and Quesnel attempting to trace the source of stream sediment geochemical anomalies to a bedrock source. Much of this early exploration was hampered by extensive and deep glacial overburden along the Bowron River valley, subsequently most activities had ended by 1994.

Logging activities increased during the late 1980s, opening road infrastructure into a large portion of the favourable area, and thereby exposing new outcrops and glacial strewn boulders along roadcuts that had previously been unnoticed. Continued prospecting along these logging roads led to the discovery of two areas of glacial boulders containing VMS style of mineralization on the Bow claims, and evidence that major VMS types of mineral deposits may exist within the area.

Eureka Resources, Inc. had concluded an option-to-purchase agreement with the prospector to earn a 100% interest in the Bow claims by the end of 1997. In 1998, a $225,000 field program was completed on this property, consisting of airborne and ground geophysics, geochemistry, geological mapping, prospecting and additional ground acquisition.

While prospecting the area of the Antler Formation, north and south of the Bow claim block, a boulder of high grade copper was located on Lottie Creek, 10 kilometers to the south. Assays of chips of this boulder yielded copper content up to 24%. Based on this find, Eureka concluded a second agreement with the prospector to option the Lottie claim.

Commencing with a brief program in November, 1998, followed up with more extensive work in 1999, Eureka completed detailed gridwork, consisting of VLF and HEM electromagnetic surveys, "B" and till soil sampling programs, geological mapping, and trenching. In addition, a glacial study was completed in the area to determine the ice history and flow directions. Additional claims were located, bringing the claim package to 4 claims (56 units). This report details the results and summarizes the costs.

Location

The claims are located in the Cariboo area of central British Columbia. Geographic coordinates of the principal showing area of the claims are 53 14'N and 121 36'W, the entire claim block falling within NTS 93H/4E.

The property is located approximately 14 km north of the small community of Wells, located on highway 26, 80 km east of Quesnel. From Wells, access is easiest from highway 26, 24 km west of Wells, north along the Willow Creek logging road (4600) a distance of 27 km, and thence east along the Big Valley logging road (4600A) a distance of 21 km to the property at Lottie Creek. A shorter route exists immediately north of Wells, a road distance of 15 km, however the crossings at Big Valley and Lottie creeks must be upgraded to improve the efficiency of access.

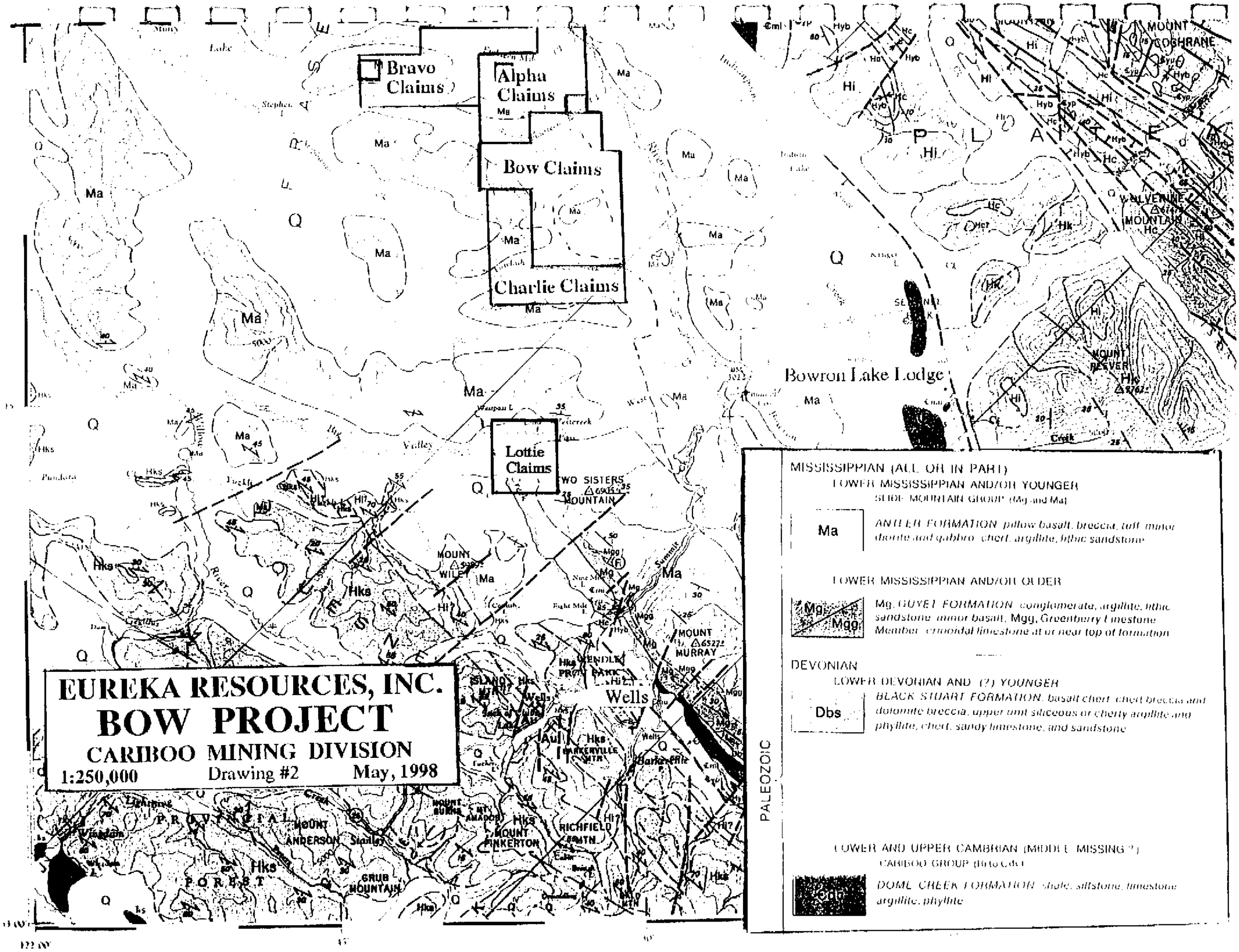
Topography and Vegetation

The claims lie immediately west of the divide forming the Quesnel Highland, in the westerly flowing valley of Lottie Creek. The Quesnel Highland is a local mountain range, the dominant peak being the Two Sisters Mountain attaining an altitude of 2000 meters (asl), 2 km to the southeast of the property. Other mountains in the range rise to elevations of 1500 - 1800 meters. The main areas of interest on the Lottie claims are located at elevations ranging 1200 - 1300 meters, in the broad moderately steep valley of Lottie creek. Outcrop is scarce in the immediate area of interest. Overburden is relatively deep and is mainly a well-sorted basal lodgement till. Ablation till, fluvial and lacustrine deposits are present, however are small and local in nature.

Prior to logging, vegetation was heavily forested, consisting of commercial stands of fir, pine, spruce, cedar, hemlock and balsam. Groves of aspen and poplar are common near major rivers. Underbrush is moderate to thick alder and devil's club.

During the past two decades, the general area of the Bowron River valley and Quesnel Highland was intensely logged. Large clear-cut areas exist in the entire area, and are at varying stages of secondary growth. All clear-cuts have been reforested. Approximately one third of the claimed area has been the subject of clear-cut logging practices.

The southeastern portion of the property rises to an elevation of 1680 meters on the western flank of Two Sisters mountain. A portion of the claim at these elevations are sub-alpine in nature. The peak of Two Sisters mountain is protected area status, and a portion of the Lottie 3 claim is affected by this boundary.



EUREKA RESOURCES, INC.
BOW PROJECT
CARIBOO MINING DIVISION
1:250,000
Drawing #2
May, 1998
Bravo Claims
Alpha Claims
Bow Claims
Charlie Claims
Lottie Claims
Bowron Lake Lodge
Wells
TWO SISTERS MOUNTAIN
MOUNT COCHRANE
WOLVERINE MOUNTAIN
MOUNT WILEY
MOUNT MURRAY
MOUNT ANDERSON
MOUNT PINKERTON
GRUB MOUNTAIN
BARKERVILLE MTN
RICHFIELD MTN
Valley
MISSISSIPPIAN (ALL OR IN PART)
LOWER MISSISSIPPIAN AND/OR YOUNGER
SLIDE MOUNTAIN GROUP (Mg and Ma)
Ma
ANTLER FORMATION: pillow basalt, breccia, tuff, minor diorite and gabbro, chert, argillite, lithic sandstone
LOWER MISSISSIPPIAN AND/OR OLDER
Mg
Mgg
Mg, GUYET FORMATION: conglomerate, argillite, lithic sandstone, minor basalt; Mgg, Greenbury Limestone Member: crinoidal limestone at or near top of formation
DEVONIAN
LOWER DEVONIAN AND (?) YOUNGER
Dbs
BLACK STUART FORMATION: basalt chert, chert breccia and dolomite breccia; upper unit siliceous or cherty argillite and phyllite, chert, sandy limestone, and sandstone
PALEOZOIC
LOWER AND UPPER CAMBRIAN (MIDDLE MISSING ?)
CARIBOO GROUP (Hi to Cdc)
DOME CREEK FORMATION: shale, siltstone, limestone argillite, phyllite

Claims

The property consists of 4 claims (56 claim units) mineral claims, the details listed as follows:

Claim Name	Type of Claim	No. Units	Tenure No.	Expiry Date *
Lottie 1	MGS	20	365443	September 10, 2002
Lottie 2	MGS	20	370289	July 6, 2000
Lottie 3	MGS	12	370290	July 6, 2000
Lottie 4	MGS	4	370291	July 6, 2000

* Expiry dates shown are current at Mining Recorder's Office. Sufficient work is available in this report to record a minimum of three years of work on all claims.

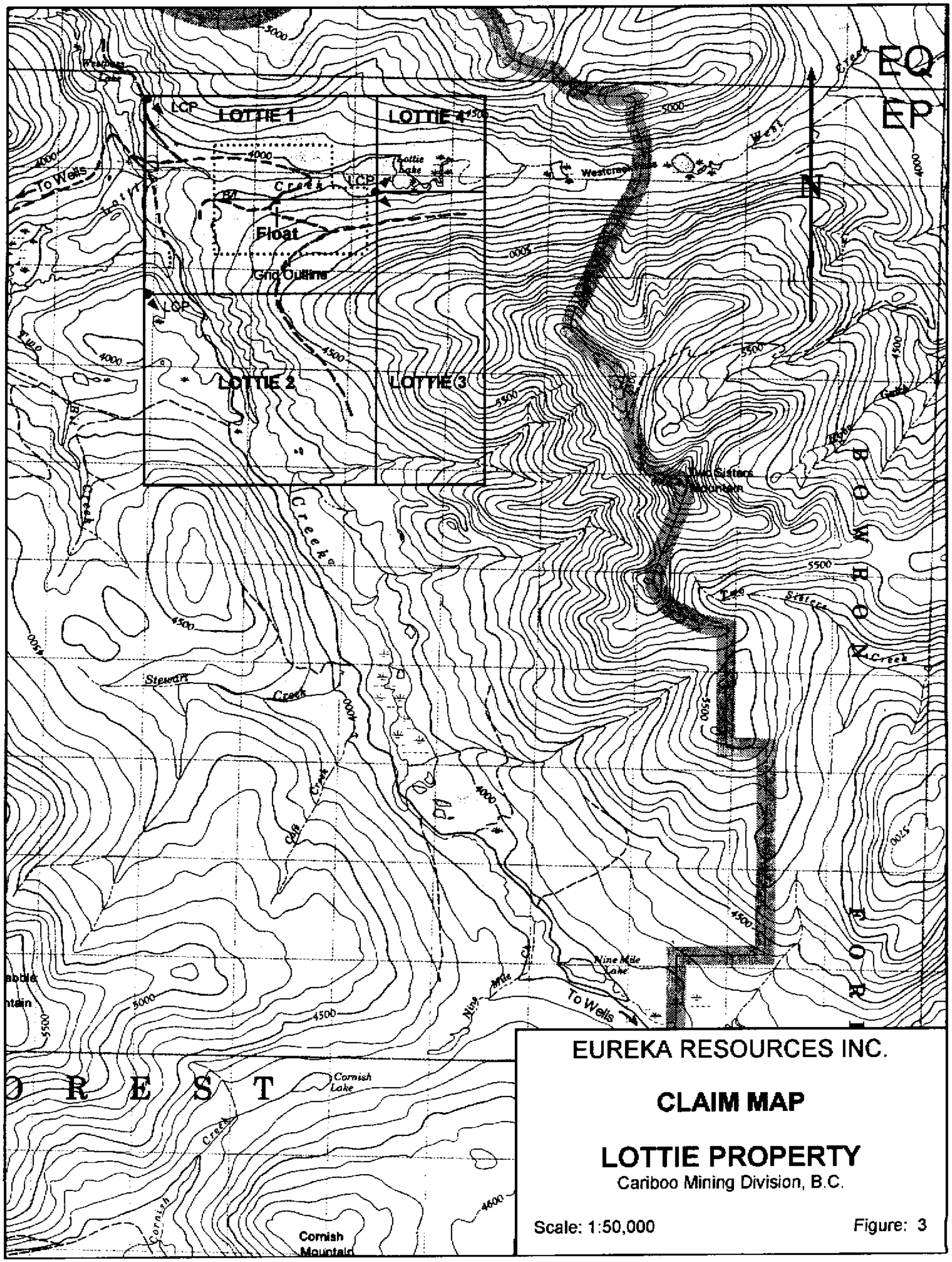
All claims are located in the Cariboo Mining Division, recorded in the name of Eureka Resources, Inc. The Lottie 1 claim is subject to a option-to-purchase agreement with Martin C. Peter, whereby Eureka can earn 100% interest in the claim subject to cash payments totalling $149,500 on production of a feasibility study, share issuances totalling 200,000 shares and work obligations totalling $550,000 over a four year option period, and subject to a 2% NSR interest.

All claims are contiguous, the general configuration shown on Drawing #3 (1:50,000).

History

Prior to 1980, the area of the Lottie property was limited to prospecting ventures. Placer and lode gold mining in the Wells/Barkerville area has persisted since the placer gold discoveries of 1858. A placer property exists in the western portion of the property that has had a history of limited production. A one-man placer operation exists today, recovering gold from small drainages in the western extremities of the Lottie 1 claim. The nature, extent and success of this operation is unknown. The only other mining activity of significance in the general area was development of the Bowron River coal/resin resource, 60 km to the northwest.

The release of the government geochemical data in the early 1980s sparked an interest in early stage exploration for volcanogenic massive sulphide deposits in the Mississippian Antler Formation. Several of the major mining companies, including Noranda, BP Resources, Esso Minerals, Shell Canada, Kennecott, and Cominco conducted grass-roots exploration programs during the period 1981 - 1994, staking large tracts of land, in attempt to trace geochemical anomalies to a bedrock source. Normal gridwork consisting of geophysical and geochemical surveys, geological mapping, and prospecting was completed over areas to the northeast of the claims during this period.



EUREKA RESOURCES INC.

CLAIM MAP

LOTTIE PROPERTY

Cariboo Mining Division, B.C.

Scale: 1:50,000

Figure: 3

There is no documented evidence of bedrock exploration or mining having been completed in the area of the Lottie claims, prior to the work programs of Eureka in 1998.

1998 FIELD PROGRAM

The 1998/99 field program was completed on the Lottie property during four separate stages from November, 1998 to October, 1999 at an overall cost of $68,825 (see Appendix A for details). Reporting endured until November, 1999.

Grid Survey and Work Program Summary

November, 1998 Program During the period November 1 - 3, 1998, a 6.8km grid was established over the Lottie float area, biasing the direction of glacial transport from west to east. Four grid lines were established west of the float area and only one line established to the east. The weather at the time of work was inclement, with a minimum of six inches of snow on the ground. The decision to limit the scope of 1998 work was based mainly on these conditions.

"B" horizon soil samples were collected along all lines at 25 meter intervals, initially submitting only the 50 meter samples for analysis. Based on the initial results, a limited number of the remaining samples were then submitted for analysis. Concurrent with soil sampling, an integrated VLF electromagnetic and magnetic survey was completed along all grid lines, readings taken at 25 meter intervals. Details of each survey are discussed in the geochemical and geophysical section respectively.

July, 1999 Program During the period July 5 - 9, 1999, and additional 4 km of grid were established. The November program indicated anomalous results to the southeast of the float location, therefore the initial assumption of ice-flow appeared wrong, and it was determined to involve a glacial to assist with glacial studies during this program. The results of this work are summarized in the Glacial Geology section, and are detailed in Appendix B.

An Hitachi Ex-200 excavator was hired from Wright Contracting Ltd. of Wells for two days of work during this period. An pit/trench at the float site revealed a minimum of twenty mineralized (massive chalcopyrite) cobbles and boulders, similar in nature to the initial boulder discovery. This confirmed the indigenous source of the mineralized rock, which could only be affected by glacial transport. The excavator was also utilized to dig a series of pits up-ice from the float area, providing three baseline fences of basal till samples, discussed in the geochemical section. All pits were filled in and the surface graded to the original topography on completion of the program.

"B" horizon soils were collected along all grid lines at 25 meter stations, as well as from pits dug for glacial studies and till samples. Silt samples were collected from drainages throughout the claims, the results discussed in the geochemical section.

Three additional claims (Lottie 2, 3, and 4) were located as part of the July program.

August, 1999 Program During the period August 30 - September 1, 1999, 2km of additional grid lines were established. Reconnaissance HEM surveys were initially completed along major access roads (3.8km) on the property, and then along 3km of grid lines. Line cutting was not required as all lines are located in clear-cut or along roads. Results are summarized in the geophysical section and Appendix C.

"B" horizon soil samples were collected along new grid lines at 25 meter intervals. Basal Till "B" horizon soil samples were collected from hand dug pits along available road cuts, results discussed under geochemistry.

September, 1999 Program During the period September 27 - October 1, 1998, an additional 2.5km of grid were established. 2km of road reconnaissance HEM and 5km of grid HEM surveys were completed. As 1.2km of the grid lines surveyed were in dense bush, linecutting was required over these portions of the grid. "B" horizon soil samples were collected on the new grid lines.

Wright Contracting provided the same excavator on site for three days to complete a trenching and test-pitting program on the interpreted electromagnetic conductor and in the area of the mineralized float. Pits and trenches were dug to the limits of the excavator (8 meters) or until bedrock was encountered. All pits and trenches were filled in and contoured to the original topography on completion of the program. Trench and pit areas from all 1999 excavations were reseeded.

Geological mapping was completed in limited outcrop areas of the grid area and in trenches that successfully encountered bedrock. Rock was visually examined for mineralization, and type samples were collected as rock-chips for chemical analysis. Float and suboutcrop areas were also carefully prospected for evidence of economic mineralization.

In summary the following work was completed on the Lottie property during the period November, 1998 to October, 1999:

Gridwork	Baseline	-	1.7km
	Gridlines	-	13.8km
"B" horizon soil samples		-	559
Basal till soil samples		-	113 pits and samples
Silt samples		-	13
Rock chip samples		-	23
VLFEM/Magnetic survey		-	9.8km
HEM survey		-	13.8km
Glacial fabric pits		-	11 pits (2 not used)
Trenches and/or pits		-	10 (110 meters length)

GEOLOGY

Regional Geology

The geology of the general area is well-documented on the 1:250,000 scale McBride area map sheet (92H), by R. B. Campbell, 1966/67, and the 1:50,000 scale map sheet 1635A, an attachment to GSC Memoir 421 by L. C. Struik, 1988. The north and eastern portion of the claim area is underlain by intermediate to basic volcanic rocks of the Mississippian Antler Formation. The rocks of the Antler Formation are described as pillow basalts, andesite to basalt flows, andesite tuffs, with minor dioritic-gabbroic near surface intrusive stocks and sills, cherts, argillitic cherts, and lithic sandstone.

The Pundata thrust crosses the southern portion of the property in a general northwest/southeast direction. This thrust is the major tectonic divide between the Slide Mountain Terrane and the older Cariboo Terrane to the southwest. Sedimentary rocks of Ordivician to Permian age occupy the southern portion of the property. These rocks are dominantly argillites, slate, phyllite, limestone, dolomite, and greywacke. Along the Pundata thrust, listwanite intrusive bodies are common as serpentinized or carbonate altered masses. One such body exists within 1 km to the west of the mineralized float area.

Covering much of the bedrock is a 5 - 20 meter thickness of unconsolidated glacial overburden. Outcrop areas occur abundantly in the northern and western portions of the property.

Regional geology is reproduced from Campbell's map as Drawing #2.

Grid Geology

Located at the 0+00 reference location on the grid is the presence of mineralized boulders containing up to 24% copper. Mineralization is typical banded volcanogenic massive sulphides (VMS), in some instances up to 90% sulphides. The dominant sulphide is chalcopyrite (70 - 80%), however chalcocite (5 - 10%), pyrite (5 - 10%) and traces of bornite are also common. Chemical analysis reports only minor contents of gold, silver, lead, zinc and molybdenum. Where gangue minerals can be identified, the mineralization is always associated with a well-banded chert, believed of felsic origin. The area of mineralized float has been observed over an area of some 20 meters in an east/west direction, and 15 meters in a north/south direction. The train of boulders gives rise to an interpretation that the boulders may have originated east and south of the float location.

The abundance, angularity, broad area of float location recognized, and wide variation in the nature of mineralization is very suggestive that the train and ultimate bedrock source of the mineralized boulders is very local, perhaps within 400 meters. Glacial interpretation of ice movement supports a general east to west direction of basal till.

Approximately 80% of the grid area is covered by a 2 - 20 meter thickness of glacial overburden. Outcrop areas are confined to L7+00W and 1+00E (@3+00S) of the grid, and are most prevalent in the western portion. Outcrops examined on the grid confirmed the underlying presence of the intermediate to basic volcanic rocks of the Antler Formation. Considerable chert was mapped, both as float and as outcrop. Rusty, altered, and chalcopyrite bearing chert, such as associated with the Lottie float area, however was not identified in outcrop. Chert, pyrite and traces of chalcopyrite were identified in bedrock in trenches on L2+00E and 7+00E.

In the vicinity of L7+00E @ 2+75 -3+00S suboutcrop along a roadcut indicates the presence of interbedded mudstone, shale, and phyllite with volcanic flows and tuffs. Trenches on L2+00E, 5+00E, 6+00E and 7+00E confirmed this sedimentary unit in bedrock. Only three bedrock exposure were located that provide sufficient and accessible outcrop for strike/dip measurements. A strike ranging 090 - 110 degrees, dipping 35 - 60 degrees to the north was measured.

The phyllitic mudstone unit has been traced over a strike length of 500 meters, and assuming an east/west strike, would have an interpreted thickness of at least 30 meters in the area of L2+00E. The contact relationship with the volcanic rocks is not well defined, however there appears to be an interbedded relationship of the mudstone with the intermediate volcanic flows and tuffs and chert in the trench on L2+00E, which would be the footwall contact of the sedimentary unit.

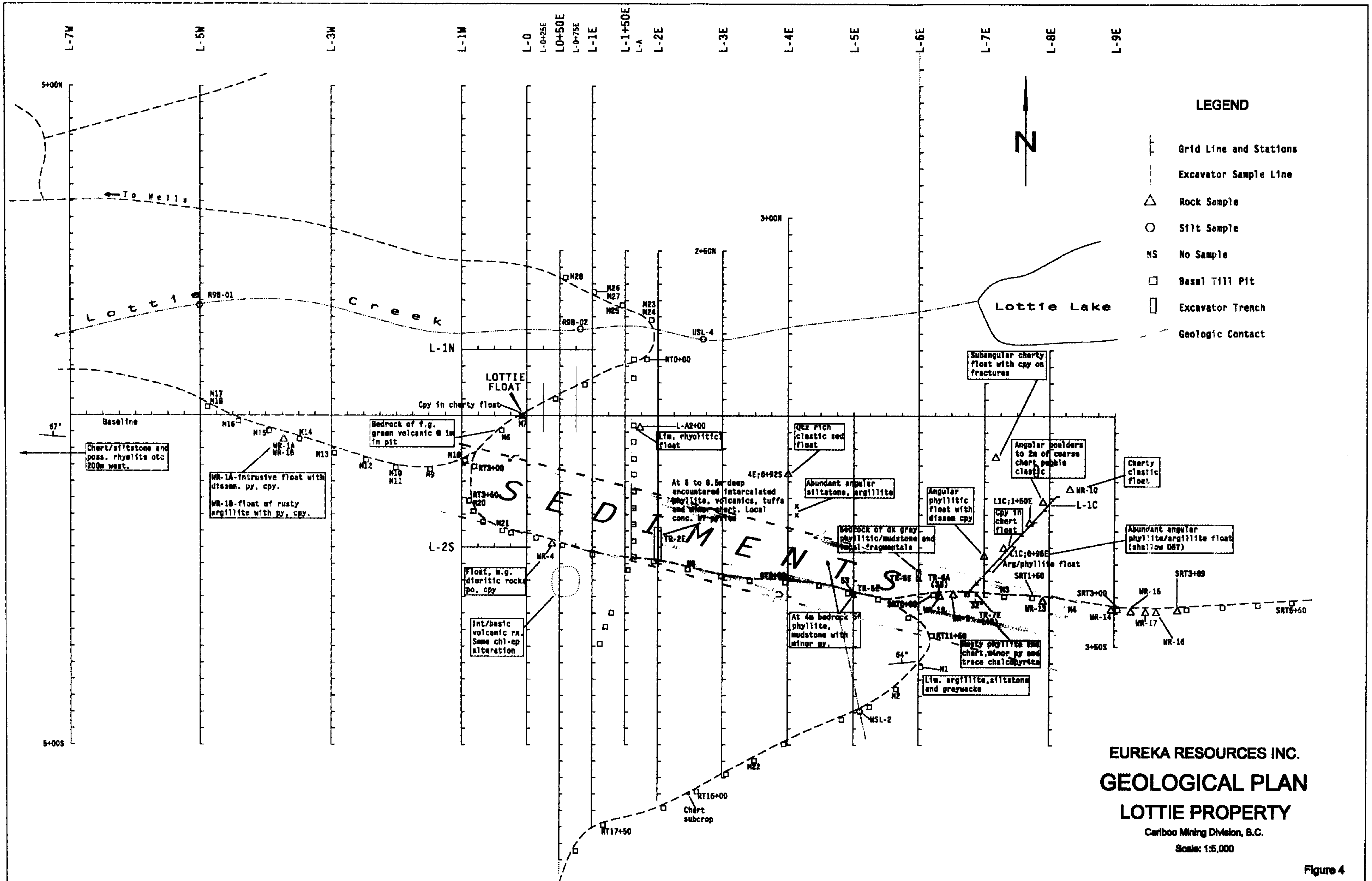
The trench on L5+00E provided some phyllitic mudstone with graphite smeared along cleavage faces. The content of graphite at this location was observed at less than 2% and could not have caused the significant electromagnetic conductor in the area. Trenches on L2+00E and 6+00E confirmed even a lesser content of graphite.

The paucity of outcrop in the grid area prevents any structural features having been identified in the field. Geophysical interpretation suggests the presence of cross-cutting faults or tight folds in the lithology in the vicinity of L6+00E @ 3+00S. Airborne geophysical interpretation may assist with identifying structural features.

The significant mineralization located as float at the 0+00 point on the grid is the primary objective of exploration in the area. The mineralization is typical of VMS deposits, and the grade is certainly of economic importance.

Geological mapping and prospecting of the grid area has revealed several other occurrences of chalcopyrite mineralization in the vicinity of L6+00E to 10+00E in felsic to intermediate volcanic rocks and chert. Of interest is a float occurrence of chalcopyrite (1%Cu), galena (.14%Pb), sphalerite (.21%Zn) and silver (11.5g/t) along the road @ 10+00E in a felsic volcanic rock. Native copper has also been identified in float.

All geological data, rock chip locations and trenches are presented on the Geological Plan (Figure 4).



EUREKA RESOURCES INC.

GEOLOGICAL PLAN

LOTTIE PROPERTY

Cariboo Mining Division, B.C.

Scale: 1:5,000

Figure 4

GLACIAL GEOLOGY

Dr. Peter Bobrowsky, senior Quarternary geologist of the Ministry of Mines and Energy of British Columbia was consulted at the beginning of 1999 to provide assistance and recommendations to implement some glacial geological studies into the 1999 field program at Lottie Lake. He endorsed the hiring of Mr. Roger Paulen, geologist, to help with these glacial studies.

Mr. Paulen was hired for the July, 1999 program to implement recommendations of Dr. Bobrowsky, which included:

- fabric counts in 2 - 3 meter deep pits in the basal lodgement till to determine the direction of the most recent ice flow in the area.
- recognition of regional landforms to assist in determining regional ice flow direction.
- implement a basal till sampling program to determine if metal content of basal till will assist in locating source of high grade float.
- examination of the mineralized float to provide the project with an opinion of the distance of travel.

Mr. Paulen has detailed his findings in a report dated July 14, 1999, which is included with this report as Appendix B, and is summarized below.

Within a 800 meter radius of the mineralized float location, Mr. Paulen selected nine areas for digging pits and completing fabric counts of pebbles in the basal till. The methodology is discussed in his report. In summary, 50 isolated (floating) pebbles in each pit are selected, the direction and plunge of the long axis of each pebble are measured The resulting 50 measurements are plotted on a Schmidt stereoplot. Of the nine pits measured, eight are suggestive of a general east to west ice flow direction with specific direction ranging 232 degrees to 282 degrees. One pit suggests a west to east flow (075 degrees). Mr. Paulen concludes that in the specific float area, the general ice flow direction is east to west.

In the general area of the claims, striations, drumlins, and other major glacial features support the general east/west ice movement.

On the recommendation of Dr. Bobrowsky and Mr. Paulen, sampling of the "C" horizon, the basal lodgement till, could remove the hydromorphic dispersion effects of metals in normal "B" horizon soils. A dispersion train up-ice from the float location may assist the project with determining the bedrock source. During the July program, a total of 55 basal till samples were collected, mainly from a series of three fences east of the float location. These pits were dug with the assistance of an excavator.

During the August program, a further 58 pits were dug by hand in available road cuts. In summary the copper content of these 113 samples varied from only 31 - 172ppm, with very little evidence of a dispersion train pattern developing. For this reason, as well as the high cost of continuing to collect basal till samples, the program was abandoned. Further details of the basal till sampling are discussed in the geochemical section of this report.

At the location of the mineralized float, at least twenty cobbles and boulders of massive sulphides (10 - 25%Cu) have been found in pits and trenches over a minimum area of 20 x 15 meters. Many more boulders and cobbles of chert containing stringer style copper mineralization in this same area. The boulders are angular to subrounded in nature indicating only limited transport distance in this form. The boulders are generally found in a cluster of ferrocrete cemented basal till, the ferrocrete having formed from oxidation of massive sulphides after deposition.

The initial reaction to the discovery is one that transport distance to the source is very limited. However Mr. Paulen postulates that one single boulder may have been transported a considerable distance prior to spalling into several smaller cobbles and boulders. The writer concludes however that the varied nature of mineralization observed in boulders would indicate that several boulders would have been transported, and the distance would be quite minimal.

The divide of the Quesnel Highland is located 2 - 3km east of the Lottie mineralized float and to the east of Lottie Lake. This divide is surmised by the author to be the divide of the most recent ice flow directions locally, the divide having been the origin of ice. If this is true, the impact of ice flow on the Lottie claim would not have as much influence on the distance and direction to source rocks of basal till boulders, and subsequently the mineralized float. It would be this writer's opinion that the source rocks would not only be influenced by glacial flow, however to some extent would be influenced by normal downhill dispersion. In summary, this conclusion would place the source rocks to be to the south and east of the float location.

GEOCHEMISTRY

The geochemical program on the Lottie property was essentially two styles of soil sampling. Normal "B" horizon sampling was initially implemented into the November, 1998 program. On the recommendations of Dr. Peter Bobrowsky, Quarternary geologist, a basal till ("C" horizon) sampling program was implemented into the July, 1999 program. It was identified that "B" horizon samples would compound hydromorphic, downhill, and ice-flow dispersion, whereas basal till sampling would eliminate hydromorphic and greatly reduce downhill dispersion. The costs of collection, however, are considerably more expensive and less practical for a till sample ($20-25/sample) versus the cost of a normal "B" horizon sample ($5-8/sample). The discussion of each sampling style is discussed as follows:

"B" Horizon Soil Sampling: Soil samples were collected from the "B" horizon (depth of 10 - 25cm) along all grid lines at 25 meter intervals. Not all samples collected from the western portion of grid were submitted for analysis. Samples were collected from shallow pits dug by shovel to the desired depth. Samples were placed in premarked kraft envelopes, and prepared for shipment to the laboratory.

Samples from the November program were sent to the laboratories of Ecotech in Kamloops and analyzed by multi-element ICP methods. Samples from the remaining programs were submitted to the laboratories of Bondar-Clegg in North Vancouver for a 34 element ICP analysis. Samples were prepared by screening the -80 mesh fraction, a sufficient aliquot taken for acid digestion and metal determination. Digestion methods are indicated with the lab reports (Appendix D).

On receipt of the results, scanning identified significance of copper, lead, zinc and silver to the point that metal maps were prepared, with anomalous threshold contents appropriately contoured. Threshold values selected for each metal (Figure 5A- copper, 6 - zinc, 7 - lead, and 8 - silver) are as follows:

	Copper	Lead	Zinc	Silver
Negative	0 - 40 ppm	0 - 15 ppm	0 - 70 ppm	0 - .3 ppm
Possibly Anomalous	40 - 100 ppm	15 - 20 ppm	70 - 100 ppm	.3 - .4 ppm
Probably Anomalous	101 - 150 ppm	21 - 25 ppm	101 - 125 ppm	.5 - .6 ppm
Definitely Anomalous	> 150 ppm	> 25 ppm	> 125 ppm	> .6 ppm

The copper distribution in "B" horizon is the most important set of geochemical data. There is a good correlation of results to the HEM conductor between Lines 0+00 to 3+00E and Lines 6+00E to 9+00E. The lack of response on Lines 4+00E and 5+00E is probably due to deep overburden and masking of values. The responses on L0+50, 1+00, and 1+50E to the south of the conductor may have been caused by ice-flow or hydromorphic dispersion, or it may have been caused by normal downhill dispersion from a potential source (VLF conductor?) uphill.

Lead, zinc and silver distribution in "B" soils are also of interest, and in summary mimic the copper results. There is definite evidence of metallogenic zoning, as silver is dominant in the western portion of the grid, while zinc and lead is more dominant in the eastern portion. Gold determinations are recommended on selected samples.

In addition to the elements mentioned, there appears to be strong variations in barium, manganese, iron and yttrium that may provide assistance for future exploration. Iron and barium are important components of VMS deposits.

Basal Till ("C" Horizon) Sampling: In total 113 basal till samples were collected on the property. Three fences of samples were collected to the east of the float location on L 0+25E, 0+75E, and 1+60E. These samples were dug by excavator to depths of 1.5 - 2 meters. Samples were also collected from hand-dug pits in road-cuts, where the till had previously been exposed at depths of 0.75 - 1.5 meters. All samples (3 - 4 kg) were placed in clear plastic sample bags, firmly tied and shipped to the laboratory of Bondar-Clegg in North Vancouver for 34 element ICP analysis. Samples were prepared similarly to the "B" soils.

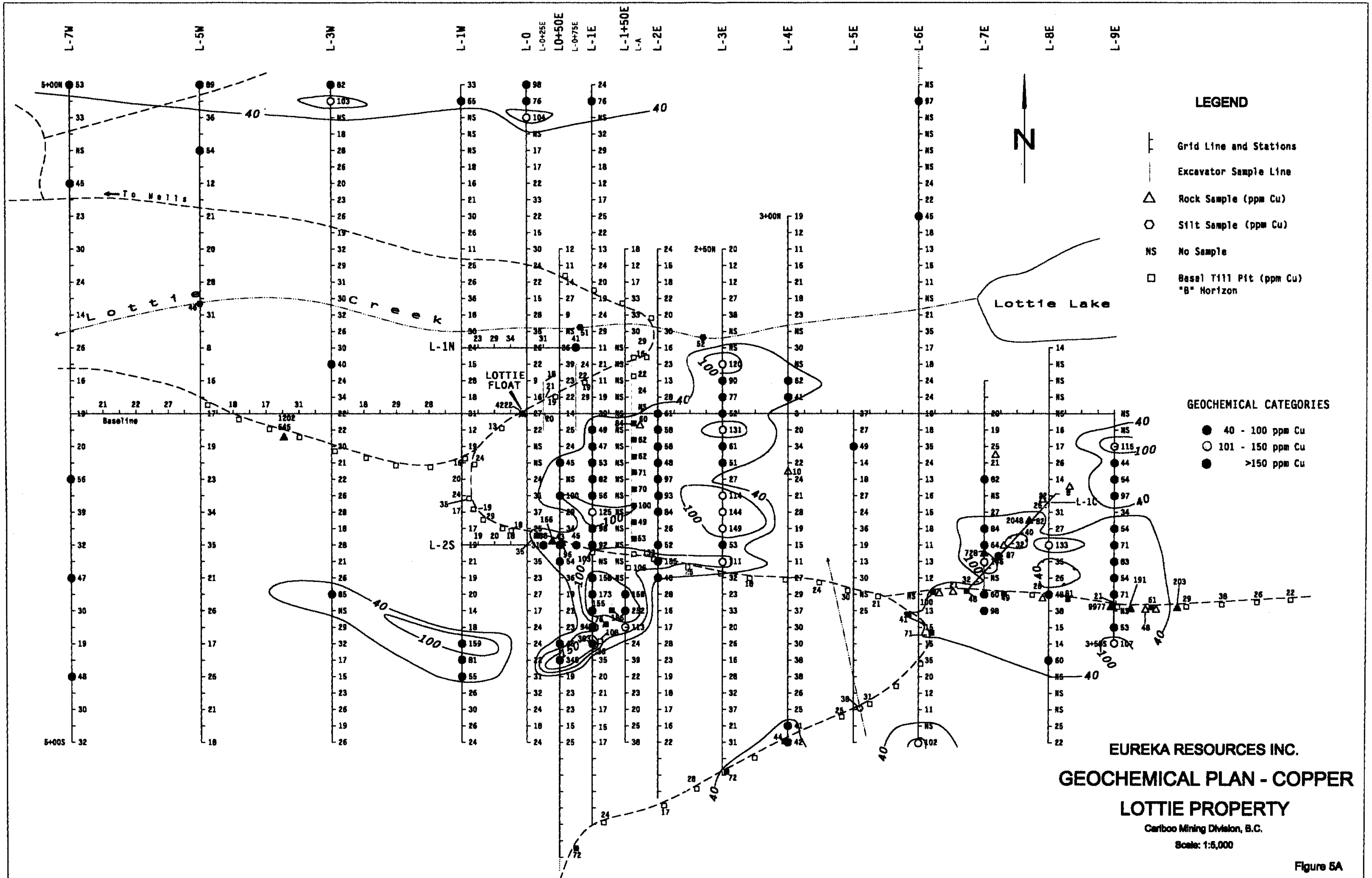
Copper content of till samples are plotted on Figure 5B. There is not much variation of the values, and a definite train (glacial) has not been recognized. A slight elevation of values in till is recognized in the vicinity of L6+00 to 8+00E @ 2+75S, coinciding with the "B" soil anomaly. This confirms a potential target in this area.

Further till sampling should not be abandoned on the Lottie claim and area, as till sampling is a valid exploration tool in glacial overburden. The drawbacks at the Lottie claim are the excessive topography, the vegetation, and the lack of definitive results.

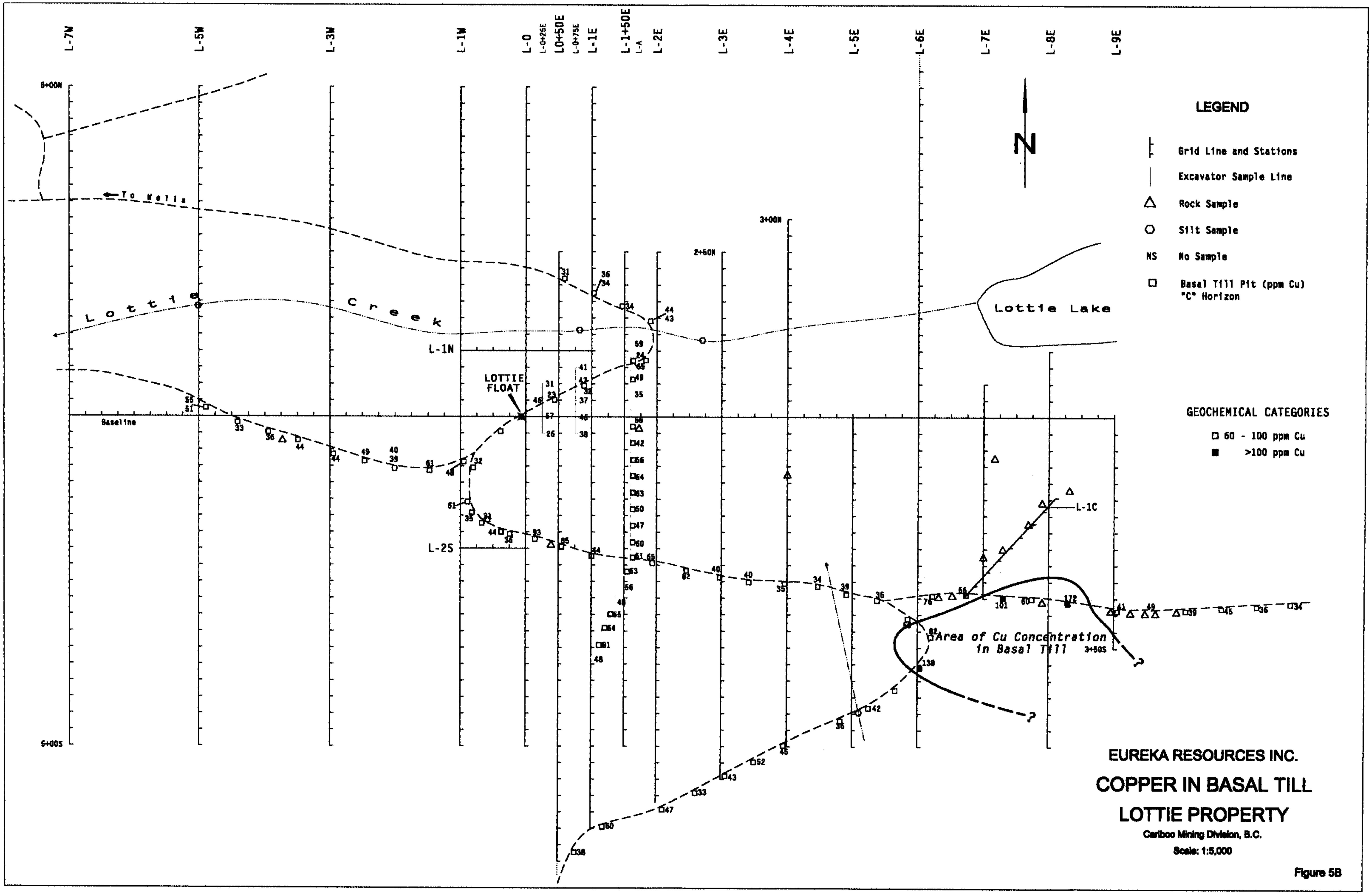
Rock-chip and Silt Sampling: A total of 23 rock-chip and 13 silt samples were collected from various sources on the property. All were submitted to the same laboratories for multi-element ICP analysis. The results of the rock-chip samples basically substantiated visual descriptions, the high-grade concentration of copper in the massive sulphide boulders, the lack of other metals with massive sulphides, and the presence of anomalous copper in trench samples.

Silt samples did not provide potential source areas that are not currently being investigated.

It must be pointed out that the copper content of "B" soils and till in the area of the Lottie float is very low. The maximum "B" soil is 27ppm, and till is 47ppm. This is unusual considering the content of copper in the boulders and may be rationalized by a general lack of chemical dispersion of copper in soils.



L-7W
L-5W
L-3W
L-1W
L-0
L-0+25E
L0+50E
L-0+75E
L-1E
L-1+50E
L-A
L-2E
L-3E
L-4E
L-5E
L-6E
L-7E
L-8E
L-9E
L-1N
L-2S
L-1C
Baseline
5+00N
5+00S
3+00N
2+50N
3+50S
LOTTIE FLOAT
Lottie Creek
Lottie Lake
To Wells
N
LEGEND
Grid Line and Stations
Excavator Sample Line
Rock Sample (ppm Cu)
Silt Sample (ppm Cu)
NS No Sample
Basal Till Pit (ppm Cu) "B" Horizon
GEOCHEMICAL CATEGORIES
40 - 100 ppm Cu
101 - 150 ppm Cu
>150 ppm Cu
EUREKA RESOURCES INC.
GEOCHEMICAL PLAN - COPPER
LOTTIE PROPERTY
Cariboo Mining Division, B.C.
Scale: 1:5,000
Figure 5A



EUREKA RESOURCES INC.

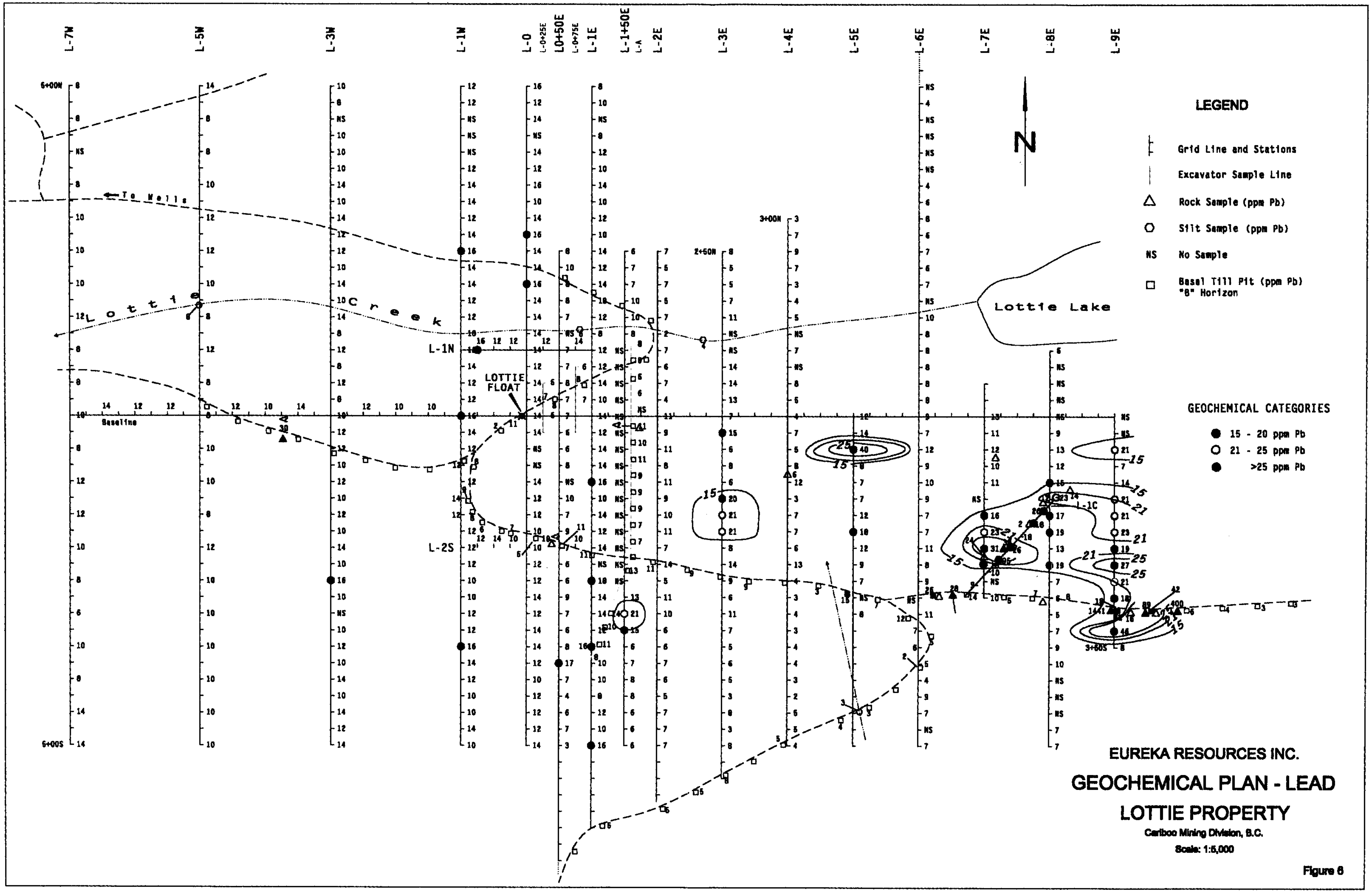
COPPER IN BASAL TILL

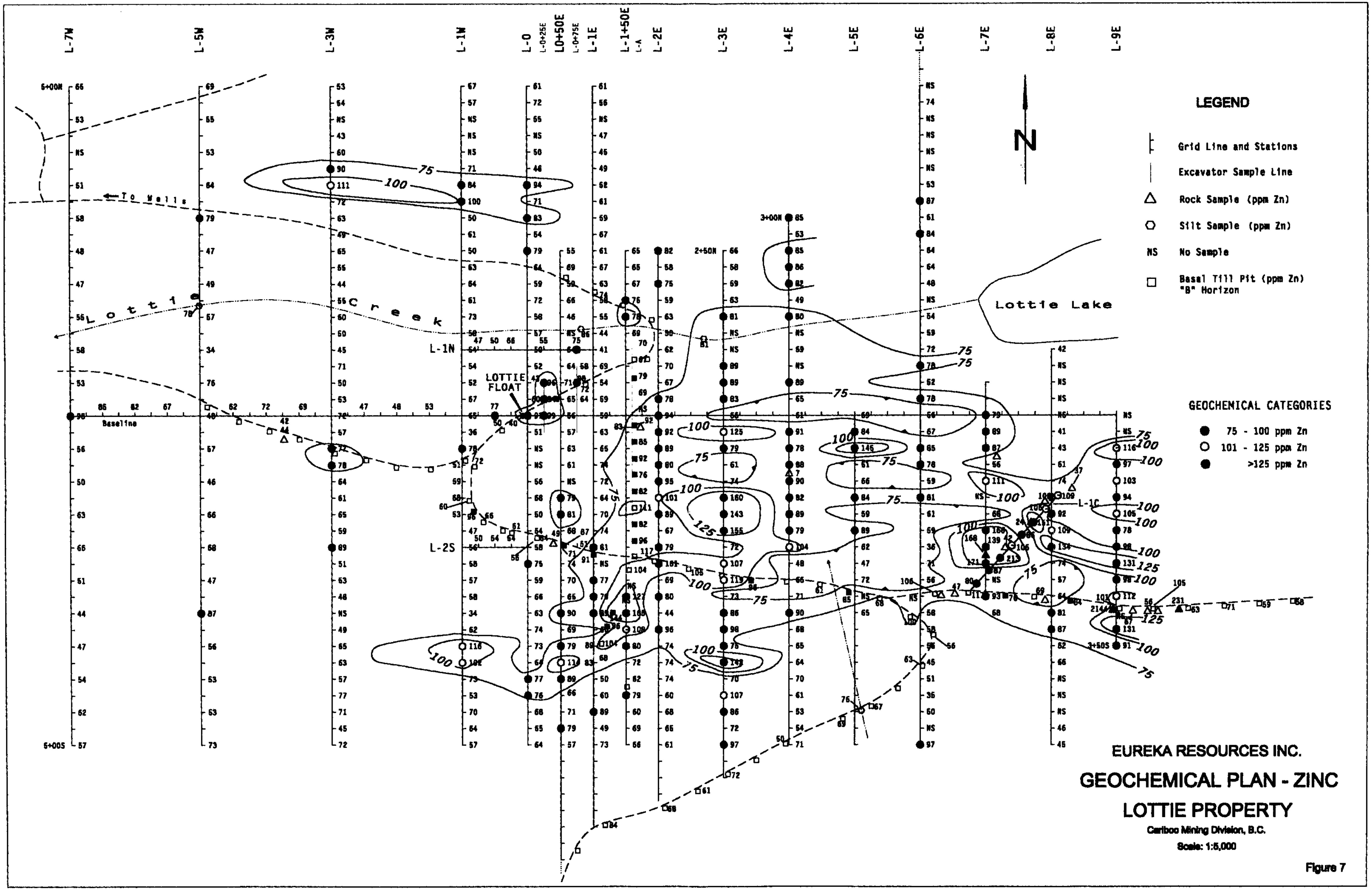
LOTTIE PROPERTY

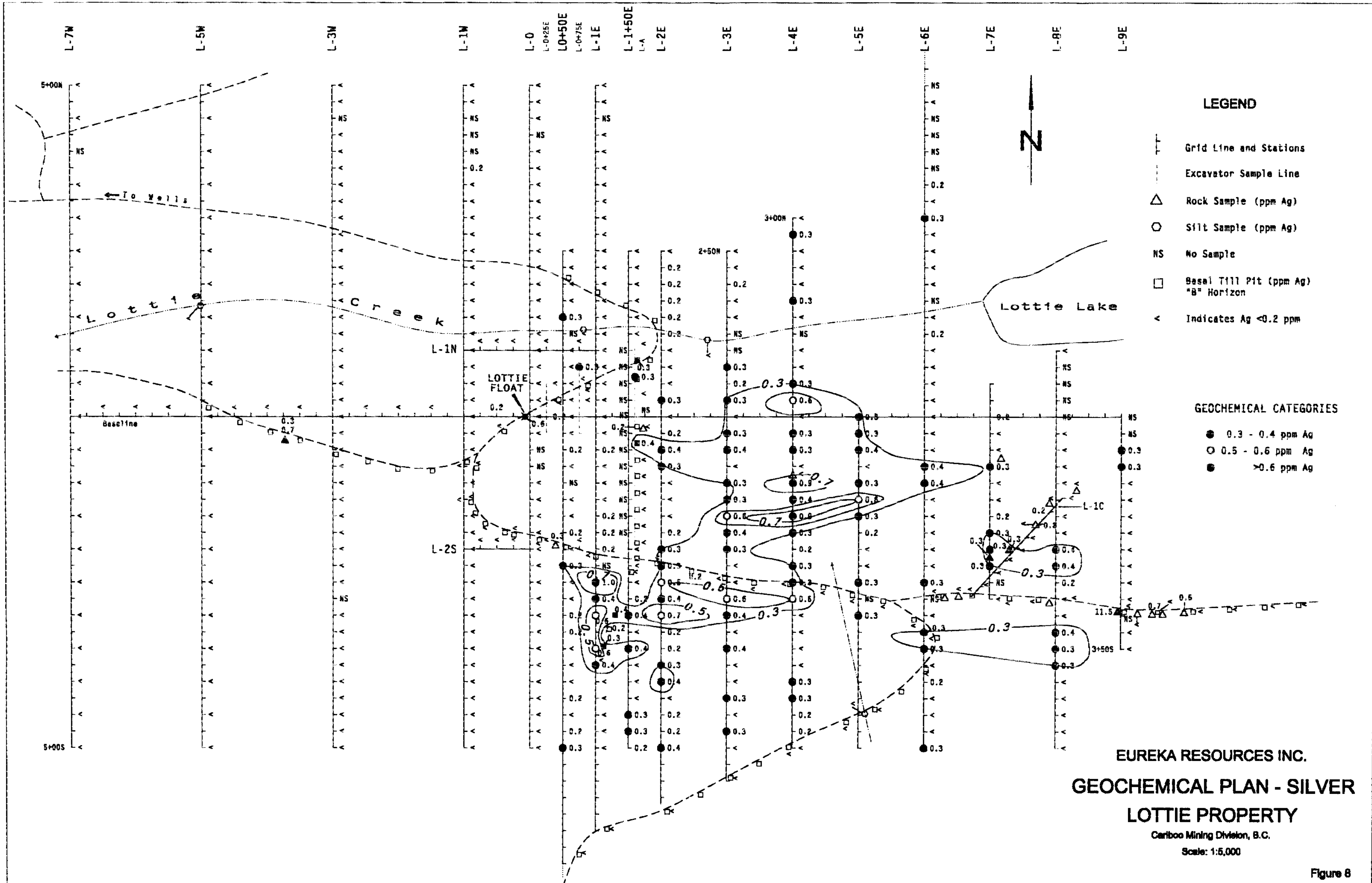
Cariboo Mining Division, B.C.

Scale: 1:5,000

Figure 5B


L-7W
L-5W
L-3W
L-1W
L-0
L-0+25E
L0+50E
L-0+75E
L-1E
L-1+50E
L-A
L-2E
L-3E
L-4E
L-5E
L-6E
L-7E
L-8E
L-9E
6+00N
6+00S
3+00N
2+50N
3+60S
Baseline
L-1N
L-2S
L-1C
LOTTIE FLOAT
Lottie Creek
Lottie Lake
To Wells
N
LEGEND
Grid Line and Stations
Excavator Sample Line
Rock Sample (ppm Pb)
Silt Sample (ppm Pb)
NS No Sample
Basal Till Pit (ppm Pb) "B" Horizon
GEOCHEMICAL CATEGORIES
15 - 20 ppm Pb
21 - 25 ppm Pb
>25 ppm Pb
EUREKA RESOURCES INC.
GEOCHEMICAL PLAN - LEAD
LOTTIE PROPERTY
Cariboo Mining Division, B.C.
Scale: 1:5,000
Figure 6


LEGEND
Grid Line and Stations
Excavator Sample Line
Rock Sample (ppm Zn)
Silt Sample (ppm Zn)
NS No Sample
Basal Till Pit (ppm Zn) "B" Horizon
GEOCHEMICAL CATEGORIES
75 - 100 ppm Zn
101 - 125 ppm Zn
>125 ppm Zn
N
Lottie Creek
Lottie Lake
LOTTIE FLOAT
To Wells
Baseline
L-7W
L-5W
L-3W
L-1W
L-0
L0+50E
L-1E
L-1+50E
L-2E
L-3E
L-4E
L-5E
L-6E
L-7E
L-8E
L-9E
L-1N
L-2S
L-1C
EUREKA RESOURCES INC.
GEOCHEMICAL PLAN - ZINC
LOTTIE PROPERTY
Cariboo Mining Division, B.C.
Scale: 1:5,000
Figure 7



EUREKA RESOURCES INC.

GEOCHEMICAL PLAN - SILVER

LOTTIE PROPERTY

Cariboo Mining Division, B.C.

Scale: 1:5,000

Figure 8

GEOPHYSICAL SURVEYS

There are three components of geophysics completed on the Lottie property. The November, 1998 and July, 1999 programs incorporated a magnetic survey and VLF electromagnetic survey over 9.8km of the grid area and the August and September, 1999 programs incorporated a horizontal loop electromagnetic survey over 13.8km of the grid area. There is sufficient duplication of surveyed lines to relate the results of one survey to another.

VLF-EM/Magnetic Surveys: John Osterhagen, geophysical technician from Vernon, B.C. was employed for the November and July programs to complete preliminary magnetic and VLF electromagnetic surveys on the property, supplying an integrated GEM-19T magnetometer/VLF electromagnetic unit. Readings were taken along all grid lines established at this time at 25 meter intervals.

Figure 9 compiles the results of the VLF-EM survey and indicates the resulting Fraser filtered electromagnetic conductors from the Hawaii transmitting station. Readings were also collected from the Cutler, Maine station, however are not displayed in this report as interpreted conductors from both data sets are relatively similar. In summary, there is general compatibility of the conductors derived from the HEM survey with those of the VLF-EM survey on grid lines surveyed by both methods. Of interest is a VLF-EM conductor expressed from l+00E to L5+00W @2+50 to 4+00S on lines only partially covered by the HEM survey. This conductor was not noticeably detected by the HEM survey results.

Other isolated conductors are indicated on the VLF-EM plan, and are interpreted as noted changes in slope and/or overburden effects (road culverts). The VLF methods do not correct for slope, and will result in spurious conductor interpretation. Fraser filter anomalies in the Lottie Creek drainage may well have been caused by slope changes.

Figure 10 compiles the results of the magnetometer survey. In summary, magnetic relief over the survey area is 160 gammas, this relief probably a reflection of variations of the depth and nature of the overburden. There is no obvious magnetic signature that enables reliable interpretation of structures or lithology. Magnetic relief over the mineralized float location, and HEM conductor location is less than 40 gammas.

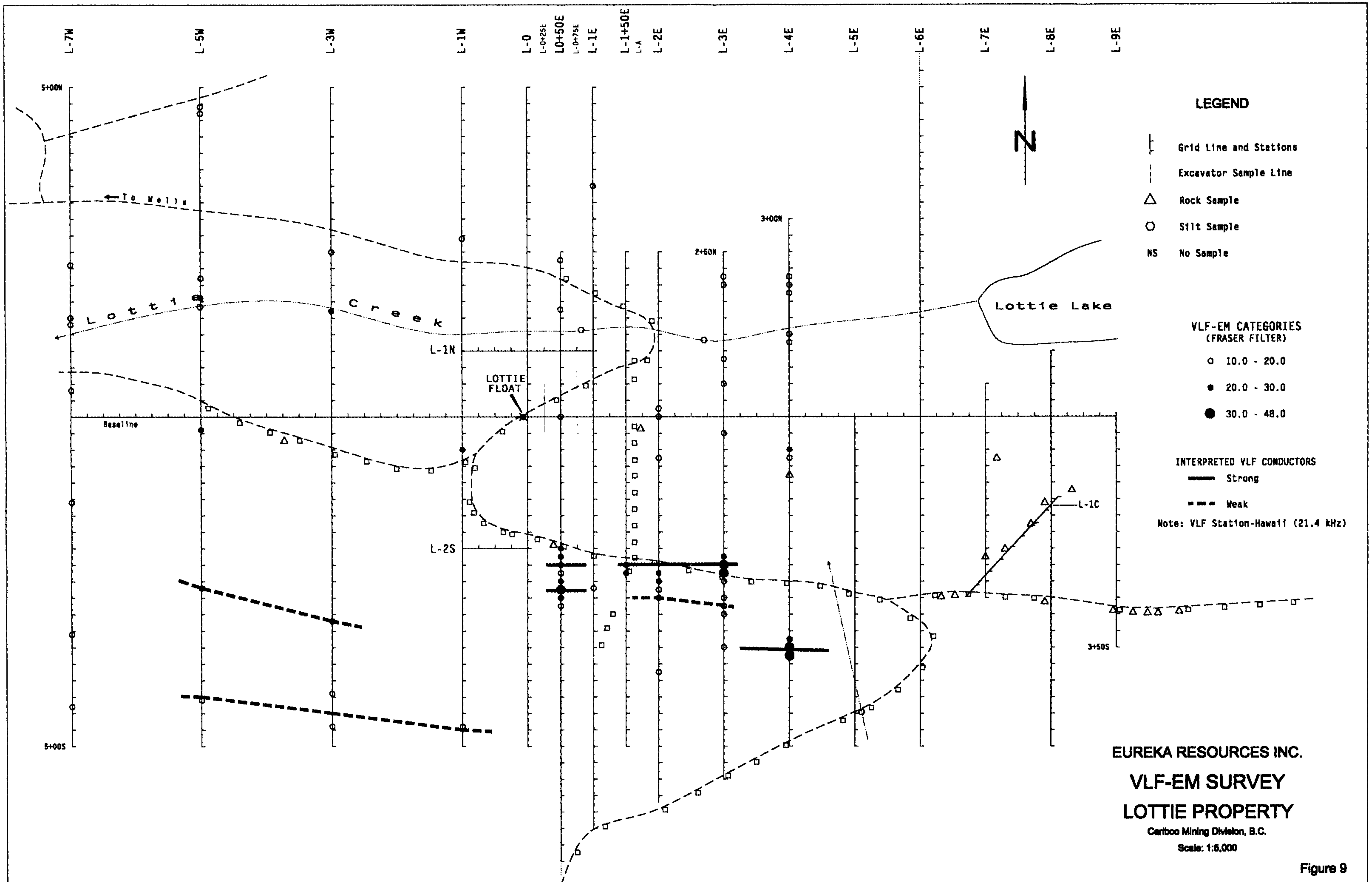
HEM Survey: SJ Geophysics Ltd. of Delta, B.C. was retained to conduct the horizontal loop electromagnetic surveys in both the August and September programs, completing a total of 13.8km. Details of the survey are compiled in in two reports (Appendix C) dated September 13 and October 12, 1999. All maps pertaining to the HEM survey results, the equipment used, the methodology, operators, and timing are thoroughly discussed in these reports.

The most interesting data set derived from the Lottie property in 1999 are the electromagnetic conductors traversing the Lottie grid in an east/west direction from 1+75S to 3+00S, summarized on the Interpretation Plan (Plate G8) of the addendum report. This conductor has been interpreted over a strike length 900 meters and is open in both directions along strike. The strongest readings occur between L0+00 and 4+00E and is classified as a good conductor ranging in strength up to 30 siemens. Along the full strike length, the conductor strength is estimated to be 2 - 30 siemens. The conductor axis is shouldered by a broad conductive zone 50 - 100 meters wide. Depth to the top of the conductor has been interpreted to be 3 - 20 meters, which is probably a reflection of the depth of overburden. Dip of the conductor cannot be determined, however is apparently to the north.

The cause of the electromagnetic conductor has yet to be determined, however all indications are that this is the source of the high grade massive sulphide float located at the 0+00 point of the grid. There is definitely a relationship of an electromagnetic conductor of this strength to the conductivity of hand specimens collected at the site. Although graphite has been observed as smears along cleavage faces associated with the sediments, the content of graphite (less than 2%) observed could not have caused a conductor of this magnitude. The relationship of the conductor to geochemical anomalies, location of mineralized float occurrences, the interpreted geological lithology, and abundance of chert associated with this favourable lithology is too dramatic to be considered a mere coincidence. The trenching completed over the conductor confirms the depth of overburden to be 2 - at least 8 meters deep. In most cases, the depth being too prohibitive to complete adequate bedrock investigations. There is some evidence of splaying of the conductor axis along its length, which may have been caused by cross-faulting or lithological deformation. This conductor is definitely a drill target for ongoing work programs, which is incorporated in the discussion of results and recommendations.

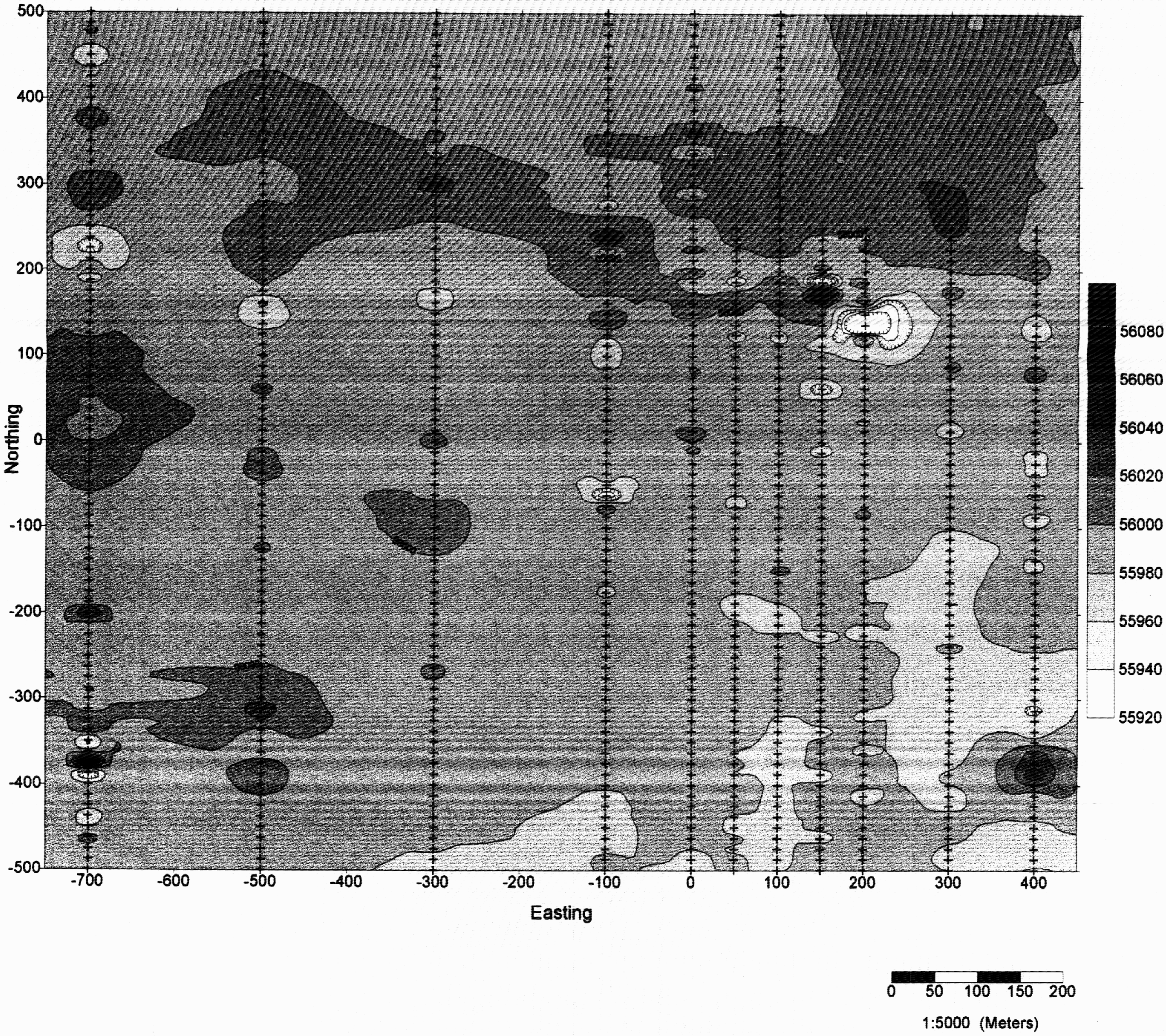
Two secondary weak conductors are interpreted subparallel to the main conductor between L2+00E and 7+00E as shown on the Interpretive Plan. These conductors are of significance and should be investigated as part of ongoing programs.

The reconnaissance work along roads did not yield any other potential targets of interest.



L-7W
L-5W
L-3W
L-1W
L-0
L-0+25E
L0+50E
L-0+75E
L-1E
L-1+50E
L-A
L-2E
L-3E
L-4E
L-5E
L-6E
L-7E
L-8E
L-9E
5+00N
3+00N
2+50N
5+00S
3+50S
To Wells
Lottie Creek
Lottie Lake
L-1N
L-2S
L-1C
LOTTIE FLOAT
Baseline
N
LEGEND
Grid Line and Stations
Excavator Sample Line
Rock Sample
Silt Sample
NS No Sample
VLF-EM CATEGORIES
(FRASER FILTER)
10.0 - 20.0
20.0 - 30.0
30.0 - 48.0
INTERPRETED VLF CONDUCTORS
Strong
Weak
Note: VLF Station-Hawaii (21.4 kHz)
EUREKA RESOURCES INC.
VLF-EM SURVEY
LOTTIE PROPERTY
Cariboo Mining Division, B.C.
Scale: 1:5,000

Figure 9



LOTTIE PROPERTY

Total magnetic field

Figure 10

Nov 2, 1998 and Jul 9, 1999

DISCUSSION OF RESULTS

1) The noted float area of volcanogenic massive sulphide boulders contain copper contents of up to 24%, which is definitely of economic significance. The sulphide distribution, estimated from hand specimens is 70 - 80% chalcopyrite, 5 - 10% pyrite, 5 - 10% chalcocite and minor bornite. The source of the mineralized float has yet to be determined, however a well-defined electromagnetic conductor within 200 - 800 meters of the float occurrence is the most likely source.

2) The occurrences are located in an area of British Columbia where economic VMS mineral deposits have not been discovered to date, however the Antler Formation can be geologically related to similar geologic rocks of southern B.C that host the CC and Goldstream deposits, and of northern B.C. and the Yukon that host the Kutchko Creek and Wolverine deposits.

3) The mineralized float area has been determined by trenching to be 15x20 meters and up to 3 meters deep. At least twenty angular to subangular boulders and cobbles of massive sulphides have been collected from this area, with many more boulders of chert with stringer mineralization observed. The distribution, nature of mineralization and the number of boulders is suggestive that the bedrock source of the float is nearby.

4) Glacial studies have assisted the program in determining the ice flow to be a general east to west direction, with local minor variations. Combining this data set with normal downhill dispersion, it would be logical to assume that the bedrock source to be south and east of the mineralized float.

5) The most compelling data set derived from the 1998/99 are the horizontal loop electromagnetic results. A 2 - 30 siemen conductor has been interpreted over a strike length of 900 meters, the western end of the conductor 200 meters upslope of the float location. The strength of the conductor is compatible with the conductivity of hand specimens of massive sulphide mineralization. Graphite observed to date is less than 2% content, which could not have been the cause of the conductor of this strength.

6) The geological setting of the conductor is an interpreted zone of sediments (fissile mudstone or phyllite) over a minimum thickness of 30 meters corresponding with the location and trend of the electromagnetic conductor. Measured attitudes of the sediments indicate a strike of 090 - 110 degrees and dip of 30 - 65 degrees north. This is considered an ideal setting for a typical volcanogenic massive sulphide deposit, as it is within a strata sequence of volcanic quiescence, with limited turbidity in the volcano/sedimentary accumulation. The relationship of the conductor axis and geochemistry to the sedimentary package suggest the favourable horizon would be the footwall of the sediments.

7) Trenching along L2+00E across the conductor axis yielded abundant angular chert boulders, being dominant in the southern portion of the trench. The portion of the trench from 2+10 to 2+25S had considerable bedrock exposures of interbedded sediments and volcanic tuffs and flows. It is apparent that this portion of the trench is at or very near the footwall contact of the sedimentary unit. The overburden being deep in this area (7 - 8 meters) prohibited an ideal exposure of bedrock for thorough examination. Chips of bedrock exposed at 2+25S contained massive blebs of pyrite, with possible traces of chalcopyrite.

8) Trenching on L7+00E @ 2+50S has revealed disseminated chalcopyrite in phyllitic mudstone and chert in the area of a weak conductor axis. Several float specimens in this area also revealed disseminated and massive blebs of pyrite and chalcopyrite. One specimen contained galena (.14%Pb), sphalerite (.21%Zn), chalcopyrite (1%Cu) and silver (11g/t), and another contained native copper.

9) There is a definite correlation of the "B" horizon copper geochemistry in soil to the electromagnetic conductor and favourable lithology. Although this relationship is not a perfect fit, geochemical dispersion of copper hydromorphically, downhill and down ice in the "B" horizon would have to be accounted for. Lead, zinc and silver also correlate to the favourable lithology, expressing evidence of metallogenic zoning.

10) Basal till ("C" horizon) soil sampling has not provided a good set of data to interpret the bedrock source of mineralization, however the three highest values obtained in the basal till (>100ppm Cu) were all located in the area of L7+00E @ 3+00S, associated with float occurrences of mineralization and the bedrock conductor. Although inconclusive, this also substantiates the conductor as being the bedrock source of mineralization.

11) Second priority conductors and copper anomalies are interpreted on the grid area, and all should be regarded as targets for further exploration and drilling.

12) Regional silt geochemistry and prospecting in the area of the claims indicates anomalous zinc in stream sediments to the northwest of the Lottie 1 claim on the western side of Wespass Lake, and float occurrences of chalcopyrite in andesite to the northeast of Wespass Lake. It is recommended that the area be staked to cover all ground to the north, east and west of the Lottie claims (~350 claim units) tying this project in to the Bow claim group to the north. This work is evidently in progress as this report is being written.

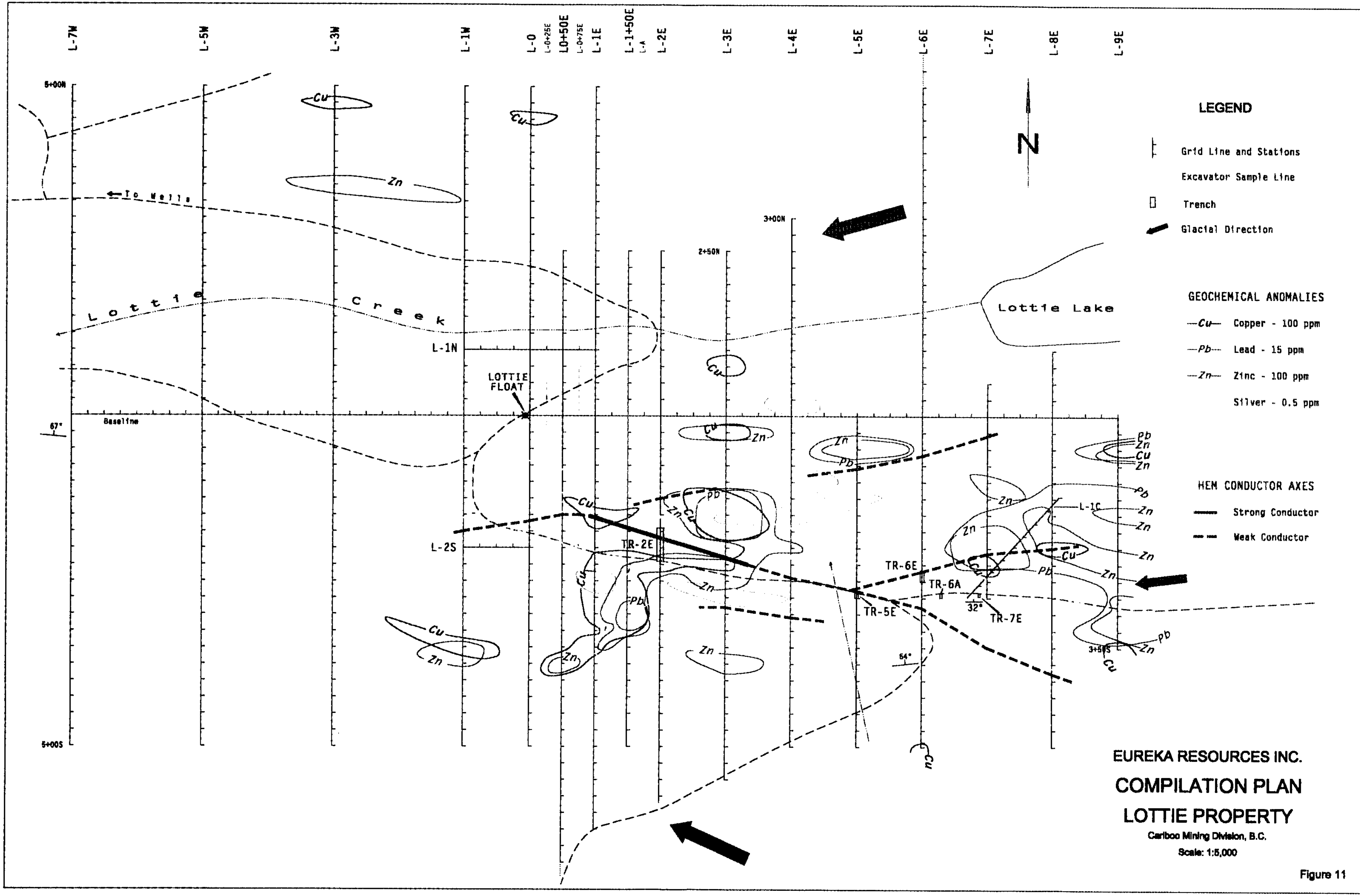

L-7W
L-5W
L-3W
L-1W
L-0
L-0+25E
L0+50E
L-0+75E
L-1E
L-1+50E
L-2E
L-3E
L-4E
L-5E
L-6E
L-7E
L-8E
L-9E
5+00N
3+00N
2+50N
5+00S
3+50S
Baseline
L-1N
L-2S
LOTTIE FLOAT
To Wells
Lottie Creek
Lottie Lake
N
TR-2E
TR-5E
TR-6E
TR-6A
TR-7E
L-1C
67°
64°
32°
Cu
Zn
Pb
LEGEND
Grid Line and Stations
Excavator Sample Line
Trench
Glacial Direction
GEOCHEMICAL ANOMALIES
Copper - 100 ppm
Lead - 15 ppm
Zinc - 100 ppm
Silver - 0.5 ppm
HEM CONDUCTOR AXES
Strong Conductor
Weak Conductor
EUREKA RESOURCES INC.
COMPILATION PLAN
LOTTIE PROPERTY
Cariboo Mining Division, B.C.
Scale: 1:5,000

Figure 11

CONCLUSIONS and RECOMMENDATIONS

The 1999/98 work program on the Lottie claims concludes that volcanogenic massive sulphide mineralization is present on the property in the form of high grade copper, and that an economic bedrock source may be very near (within 400 meters) of the float location. Horizontal loop electromagnetic surveys have clearly identified a very viable target for drill testing that is situated in an ideal geological environment associated with a well-defined soil anomaly. The location of the conductor relative to the float location can be rationalized by a combination of glacial and downhill dispersion.

The definitive work of the 1998/999 program should not rule out the possibility that the source of float mineralization may be elsewhere, nor should it dictate that only one bedrock source of massive sulphides is present in the area. Typical VMS camps are formed by a clustering of such deposits along strike of a favourable lithology or in two or more lithologic units. Therefore continued exploration should keep an open objective for work of a reconnaissance nature as well as drilling of the defined target. Recommended work on the Lottie claims therefore is a blend of ongoing detailed grid work as well as a sufficient drill program to test the nature and cause of the HEM conductor.

Details of the next phase of exploration are as follows:

1) Locate approximately 300 - 350 claim units to the north and east of the property to cover all unstaked ground between the Lottie and Bow claims. It is understood that this program is currently in progress.

2) Airborne geophysical survey over the Lottie property and newly staked ground tying into the airborne geophysical survey completed in 1998 on the Bow claims. This would incorporate approximately 250 line kilometers of survey at 200 meter line spacing.

3) Extending the Lottie grid an additional 2 km to the east, with lines extending 1 km north and south of the existing grid. Attendant work on these lines should incorporate horizontal loop electromagnetic surveys,, "B" horizon soil sampling, some continued experimentation with basal till ("C" horizon) sampling, some limited induced polarisation surveys and geological mapping.

5) Regional silt sampling the area of newly acquired claims at a greater detail than the government RGS survey.

6) A minimum of ten diamond drill holes, each hole 150 meters deep, along the strike of the identified electromagnetic conductor, the spacing of the initial five holes to be approximately 200 meters, which would serve to establish favourable lithologies, dips of lithology, and presence of economic mineralization. The location of the remaining five holes would depend on the initial results. From the data gathered to date, the preferred direction of drilling would be from north to south, however would be reversed if initial holes indicated a southerly dipping strata. Allow a total of 1500 meters.

Respectfully Submitted By:

John R. Kerr

John R. Kerr, P. Eng.,

APPENDIX A - Cost Statement

Integrated Cost Statement: Programs November 1 - 3, 1998
July 5 - 9, 1999
August 30 - September 1, 1999
September 27, - October 1, 1999

Labour:	John R. Kerr, P. Eng.	9 days @ 375/day	3,375.00	
	W. Gruenwald, P. Geo	24.25 days @ 375/d	9,093.75	
	R. Paulen, MSc	8 days @ 300/d	2,400.00	
	R. Montgomery, BSc	24 days @ 300/d	7,200.00	
	J. Osterhagen, Technician	13 days @ 300/day	3,900.00	
	D. Mason, Assistant	5 days @ 200/d	1,000.00	$ 26,968.75
Geophysical Contract:	SJ Geophysics Ltd. (HEM Survey)			
	Operating days	6 @ 850/d	5100.00	
	Mob/demob days	4 @ 637.50/d	2550.00	
	Travel Costs		1494.85	
	Report and Map Production		2700.00	$ 11,844.85
Excavator Charges:	Wright Contracting Ltd., Wells, B.C.			
	Mob/demob	18 hrs @ 100/hr	1800.00	
	Operating hours	43.5 hrs @ 121.56/hr	5287.86	$ 7,087.86
Laboratory Charges:	Bondar-Clegg and Co. Ltd.			
	Ecotech laboratories Ltd.			
	685 soils/silts @ 7.20/sample		4932.00	
	23 rock chips @ 10.00/sample		230.00	$ 5,162.00
Vehicle Costs and Transportation:				$ 5,089.45
Room and Board:	(109 man days)			$ 5,446.20
Miscellaneous Supplies, Eqpt Rental, Communication, etc				$ 1,855.41
Compilation of Data and Report Production:				
	John R. Kerr, P. Eng	6 days @ 375/d	2250.00	
	W. Gruenwald, P. Geo	4 days @ 375/d	1500.00	
	Drafting		1200.00	
	Map plotting, photocopying and binding		420.00	$ 5,370.00
TOTAL				**$ 68,824.52**

Appendix B - Glacial geological Study
Ice Flow Patterns on the Lottie Claim
Wells, B.C.
Roger C. Paulen, Glacial Geologist

Ice Flow Patterns on the Lottie Claim

Wells, B.C.

Roger C. Paulen
July 14, 1999

Introduction

The Lottie claim sits north of Two Sisters Mountain, at the northernmost extension of the Palmer Range, within the northwest part of the Caribou Mountains. A study was initiated to interpret and map out regional and local variations of the Cordilleran Ice Sheet at the site of the Lottie claim. The results, in turn, are intended to apply boulder tracing and drift geochemistry methods to find the up-ice source of the copper-rich boulders found south of Lottie Creek.

Background

Several times during the Pleistocene, British Columbia was covered by an interconnected mass of valley glaciers and mountain ice sheets, collectively known as the Cordilleran Ice Sheet (Flint, 1971). The mountain systems remained the major source areas of glaciers and ice flow was controlled by topography (Fig. 1). However, as ice thickened to form ice domes, radial flow occurred away from their centres. In central British Columbia, glaciers flowed eastward from the Coast Mountains and westward from the Caribou Mountains to merge over the Interior Plateau (Fig. 2) (Fulton, 1971; Tipper, 1971; Clague, 1981).

Each glacial cycle terminated with rapid deglaciation with complex frontal retreat in peripheral glacial areas and by downwasting accompanied by widespread stagnation throughout much of the interior (Fulton, 1967, Tipper, 1971, Clague, 1989). In central British Columbia, the ice front retreated and several glacial lakes formed in the valleys and adjacent plateau surfaces. Regional evidence suggests that the British Columbia interior became deglaciated about 11 ± 1 ka BP (Clague, 1980, 1981) and deglaciation was well advanced, if not complete, by 10 ka BP.

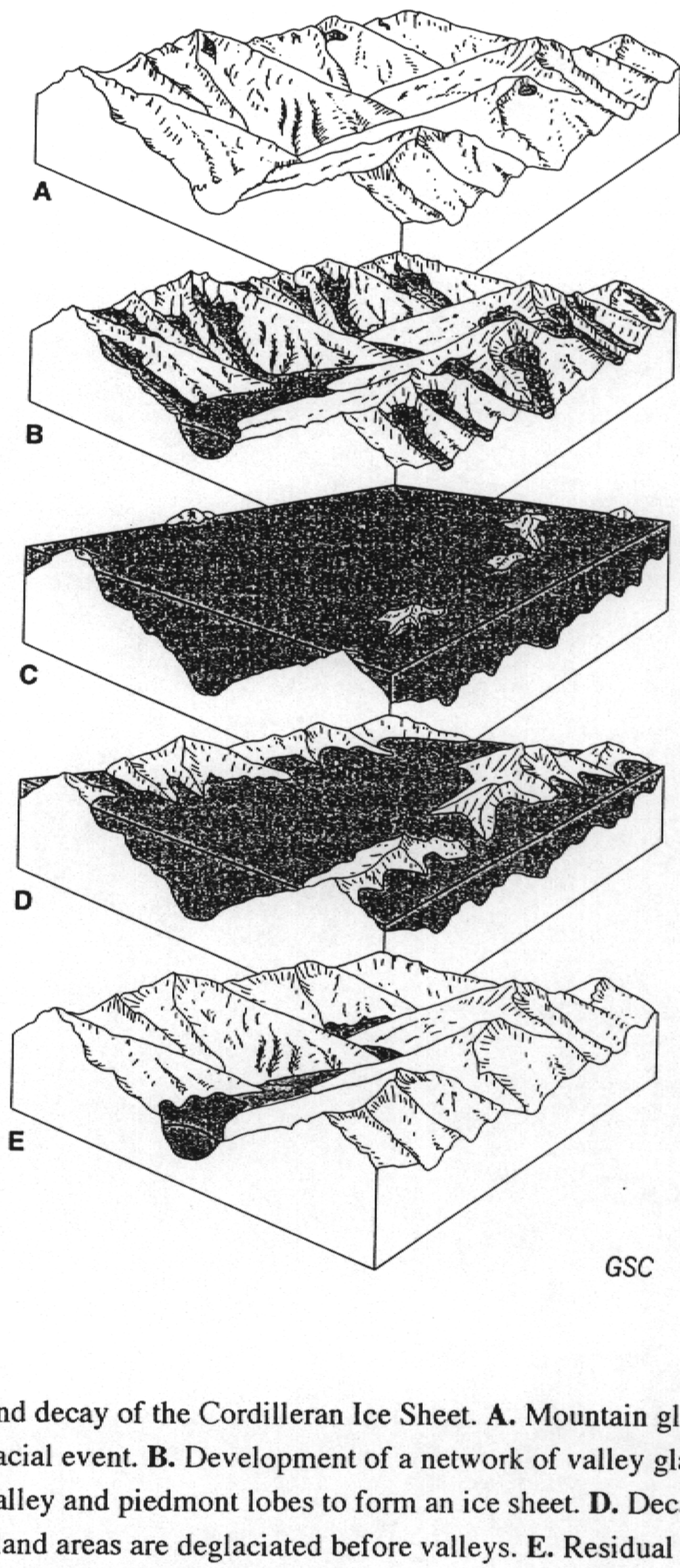


Fig. 1. Growth and decay of the Cordilleran Ice Sheet. **A.** Mountain glaciation at the beginning of a glacial event. **B.** Development of a network of valley glaciers. **C.** Coalescence of valley and piedmont lobes to form an ice sheet. **D.** Decay of ice sheet by downwasting, upland areas are deglaciated before valleys. **E.** Residual dead ice masses confined to valleys (from Clague, 1989, p. 42).

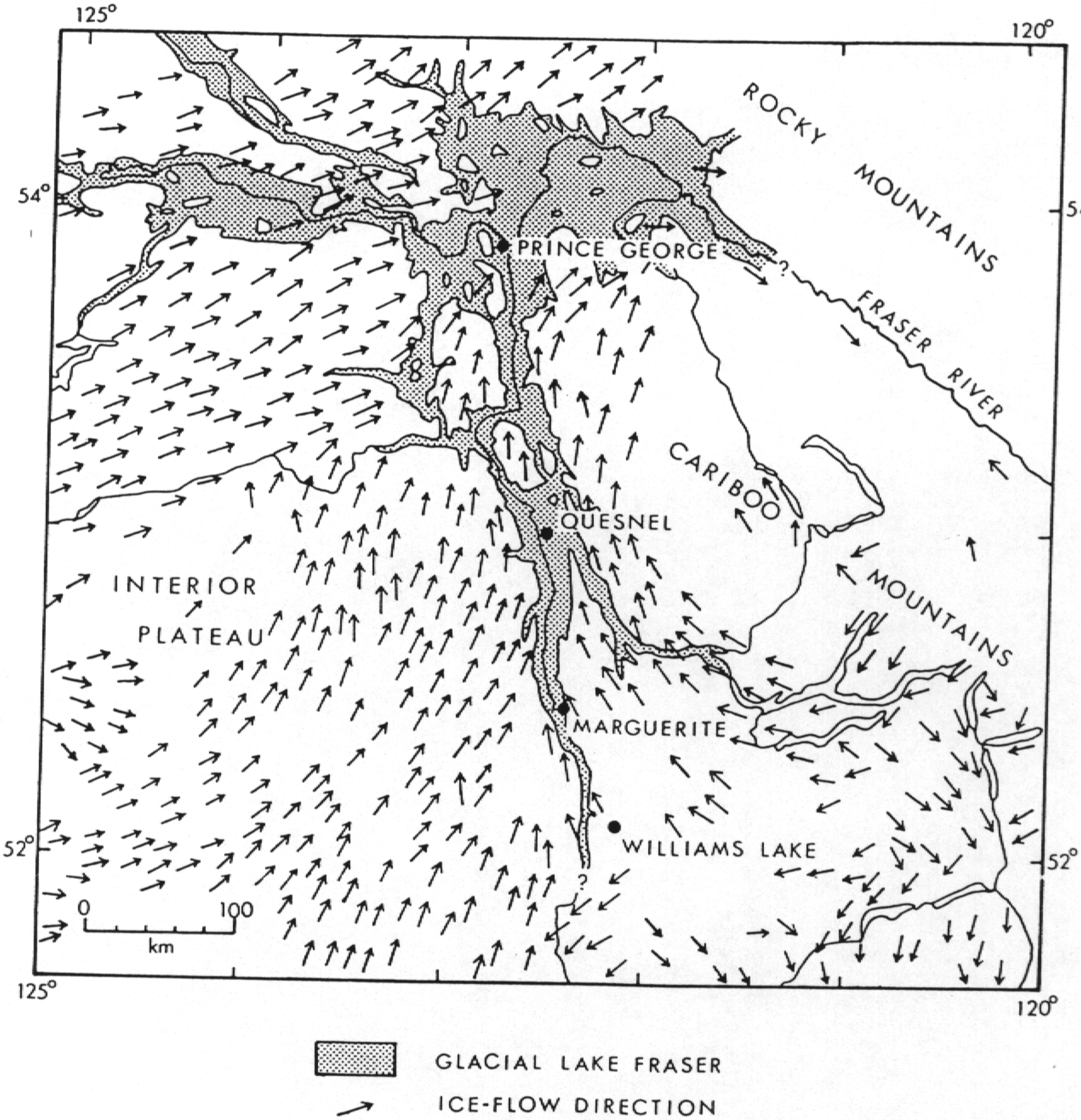


Fig. 2. Map showing the late Wisconsinan ice-flow directions and glacial Lake Fraser that formed in central British Columbia. Ice flow directions from Tipper (1971) and Clague (1987).

There was intense erosion and paraglacial fluvial aggradation in the valleys during the early Holocene. Rapid sedimentation occurred in the glacial lakes and as these drained, modern drainage patterns established in their present valleys. Rivers then became to incise their valley fills, producing terraces.

Methods

Work on the property consisted of three components:

1. Recognition of landforms and striations in the region to confirm and outline the regional ice flow history.
2. Fabric data to interpret site-specific ice flow indicators to delineate localized flow directions.
3. Outlining and discussing the properties and nature of the surficial sediments at the property and their implications for continuing drift prospecting.

Recognition of landforms was first interpreted from airphotos and confirmed with the recognition of several large landforms such as rock-cored drumlins, craig and tail features and glacial striations (Fig 3) This included observing these landforms outside the claim block to provide a regional sense of ice-flow that affected the claim site.

Clast-fabric analysis were measured from several sites on the property. A large pit was dug well below the B-horizon and into the C-horizon. Inspection confirmed the presence of a suitable material (i.e. basal till) for clast fabric analysis. A minimum of 50 medium and coarse pebbles with long:intermediate axial ratios of 2:1 or greater were selected from a maximum of 1 m^3 of sediment for each analysis (Fig.4). Typically, the established ratio for long:intermediate axial ratios is 1.5:1 with counts of 25 or more being statistically adequate (c.f. Catto, 1998), but the nature of the source bedrock

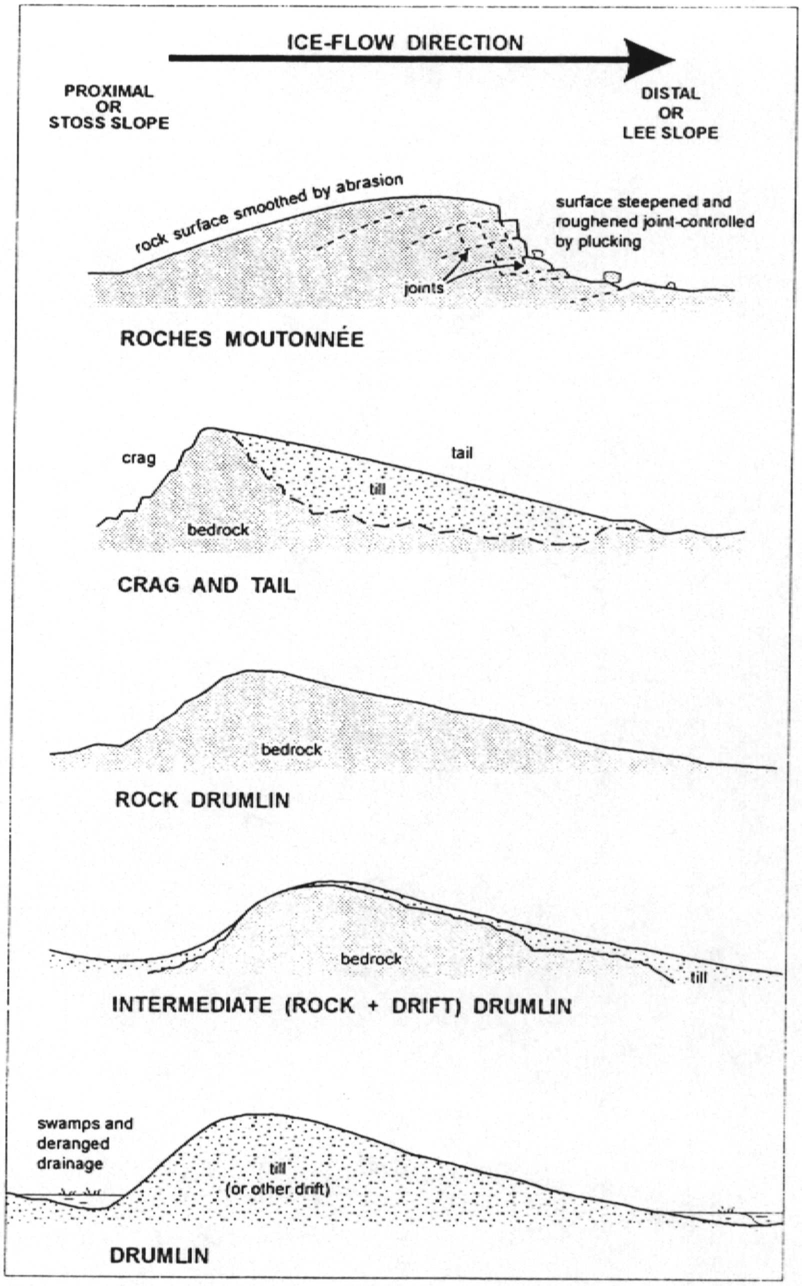


Fig. 3. Schematic cross-sections of streamlined landforms with asymmetric longitudinal profiles. Ice flow direction and related terminology for all landforms are shown at the top of the diagram (from Ryder, 1995, p. 4)

allowed for greater discrepancy at this site. The fabric orientations were plotted on rose and equal-area stereonet plots, based on the eigenvector method of Mark (1973).

Notes were made at each fabric site with respect to the character and nature of the sediment, stratigraphy, soil profile and weathering characteristics. Large features were also noted that could possibly affect potential drift prospecting.

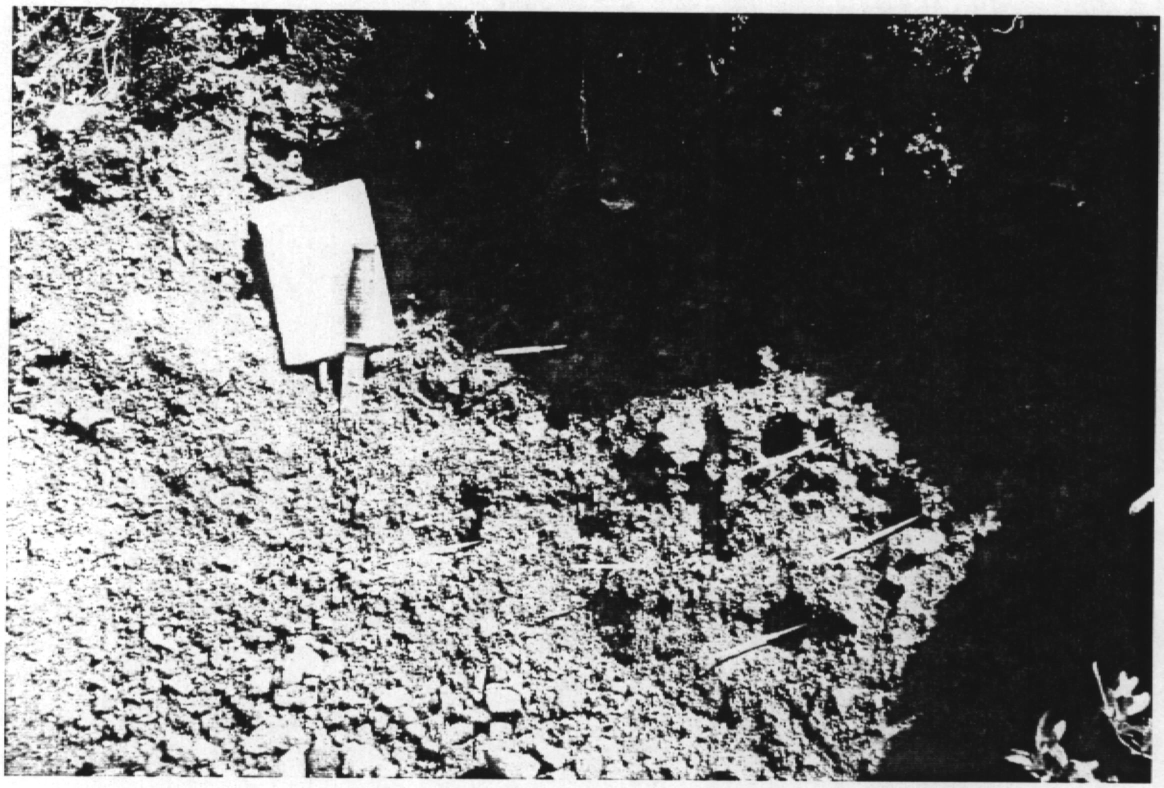


Fig. 4. Clast fabric analysis in basal till. Aluminum knitting needles placed in pebble casts parallel to the long axis of the pebbles and plunge.

Ice flow indicators

Several large glacially streamlined landforms can be seen in clear cuts to the north of Lottie Creek. These include rock-cored drumlins and craig and tail structures (Fig. 5). These were also confirmed by airphoto analysis. These features indicate a regional ice flow trending approximately 250°. Striations were measured at several sites. The thick drift cover, bedrock structure and weathering nature of the bedrock all hamper the observation of striae. At the few sites where striations were measured, a sense of direction could not be confirmed. However, one location in the clear cut north of Lottie Creek provided ample striations and direction. The average of striations measured at this site indicated an ice flow direction of 254°.

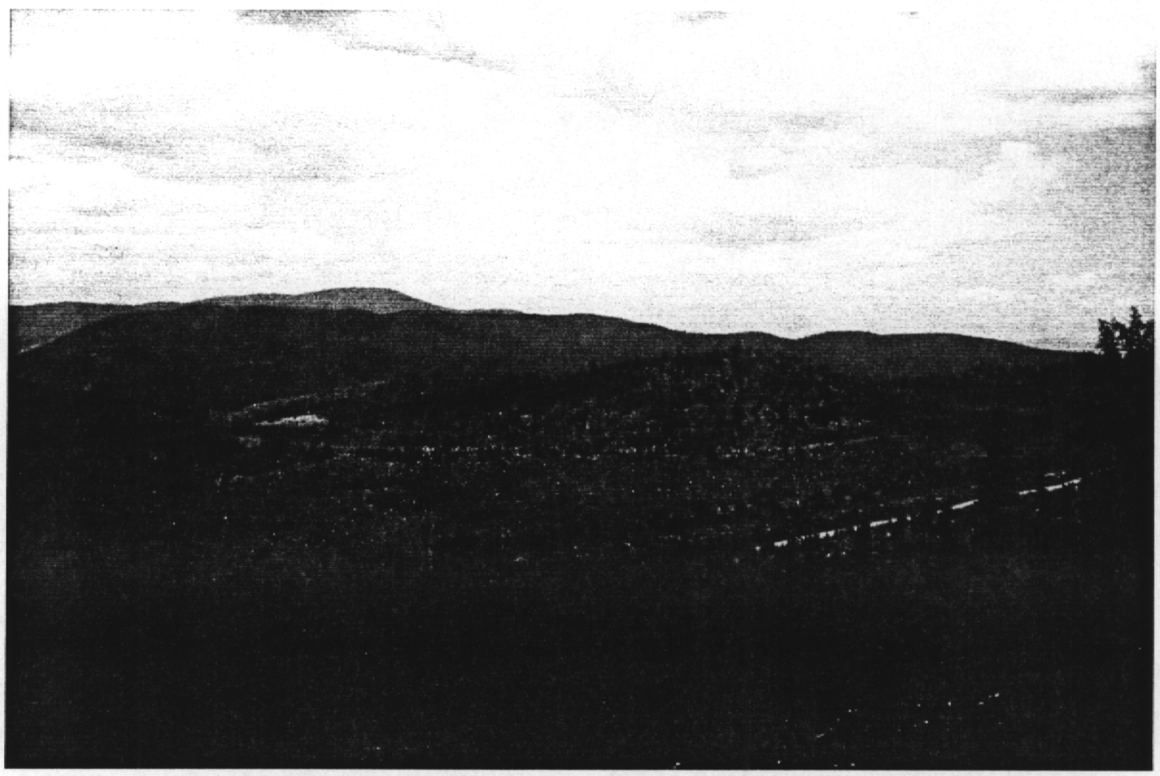


Fig. 5. Craig and tail structure in clear cut to the north of Lottie Creek. Ice flow is from right (east-northeast) to left (west-southwest).

Fabric Measurements

Clast-fabric analysis were measured from nine sites (Table 1) on the property. Fabric analysis is a major diagnostic tool used in the determination of depositional environments. Lodgement tills deposited subglacially are characterized by strong fabrics, with primary eigenvalues (E1) in excess of 0.6, aligned in the direction of glacial transport, and tertiary (E3) eigenvalues of less than 0.15 (Dowdeswell and Sharpe, 1986; Hicock *et al.*, 1996). Modal plunge angles are generally low, with pebble plunging in the direction of up-ice. Basal lodgement till fabric also are characterized by clustered distributions, where the cluster index (K) is in excess of 1.0 (Woodcock, 1977; Hicock *et al.*, 1996).

Basal melt-out and ablation till fabrics may show a lesser degree of orientation, with primary eigenvalues of less than 0.6, and cluster distributions with $K < 1$. Plunge angles are more variable with both up-ice and down-ice plunge angles (Dowdeswell and Sharpe, 1986; Hicock *et al.*, 1996).

Areas interpreted to represent ablation till have lower primary eigenvalues than those deposits interpreted as basal lodgement tills. The lowest values recorded were at pits M-4 and M-22, having eigenvalues of 0.559 and 0.565, respectively. Clustering distribution is low with K values as low as 0.28. These pits are at the highest elevation and southernmost on the claim. These likely reflect the local ice downwasting from the Twin Sisters Mountain and deposited as ablation till.

Pits interpreted to contain basal till have high primary eigenvalues. These range from 0.635 to 0.864 with varying plunge angles that likely are influenced by steep slope angles. Clustering is variable, but most values of clustering exhibit $K > 1$.

Local deviations of fabric trend within a cubic metre are common. The alignment of clasts flowing within ice are products of local ice flow conditions. Local variations in subglacial topography, ice temperature and ductility, and debris concentrations exist, producing differing stress fields, ice flow direction and fabric alignment. Larger clasts may be of a different alignment from smaller ones, as ice carrying smaller clasts flows around the boulders and cobbles. Modification can be expected during deposition around drumlins, flutings and craig and tail structures as ice flows from high pressure regimes to low pressure 'shadows' down-ice of the obstacle.

Pits interpreted to contain basal till show a strong east to west trend. Bimodal azimuths range from 231.9° (southwest) to 282.8°(west) and mean fabric trend is 252.7°(Fig 6). Plunge angles range from 0.3° to 11.4° and appear to dip down-ice with a mean plunge angle of 5.4°. Slopes on the property often exceed 10° so using plunge direction as a sole means to ice flow directions are inadequate, which is often the case in regions of moderate to high relief.

Site	n	Mean Azimuth	Mean Plunge	E1	E3	K
Discovery boulder site	50	246.2	0.4	0.768	0.080	2.53
Line 1+60E 2+75N	50	263.2	4.7	0.674	0.078	0.86
Pit M-2	50	231.9	11.4	0.706	0.111	2.65
Pit M-4	50	282.8	1.0	0.559	0.077	0.28
Pit M-5	50	075.6	5.3	0.635	0.080	0.64
Pit M-6	50	252.1	11.4	0.641	0.077	0.63
Pit M-9	50	249.2	0.3	0.692	0.077	1.00
Pit M-22	50	236.9	3.5	0.565	0.051	0.19
Pit M-23	50	256.0	11.4	0.864	0.030	1.67

Table 1. Fabric analysis sites. E1 and E3 are primary and tertiary eigenvectors, K is the clustering distribution.

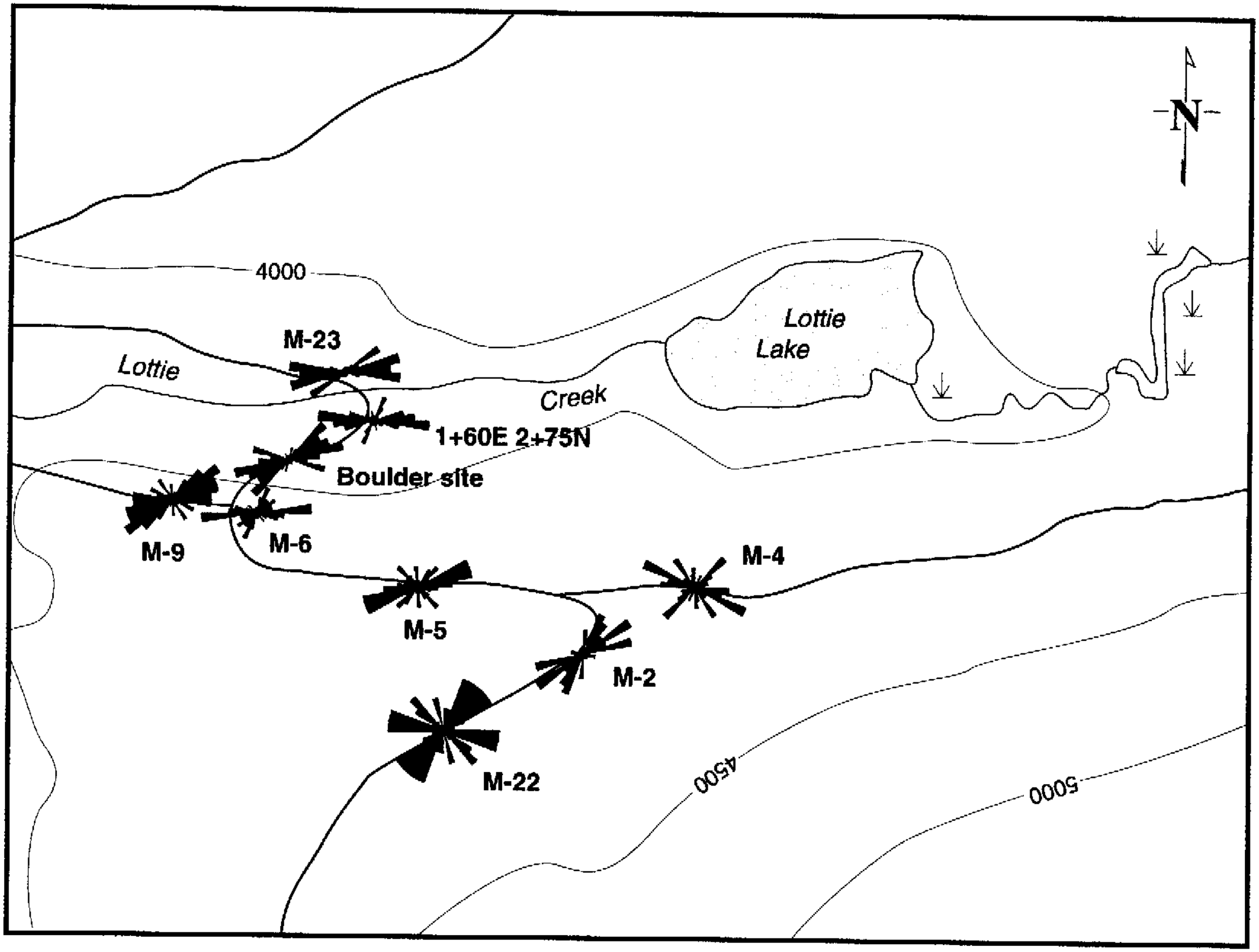


Fig. 6. Map showing the fabric locations and bidirectional rose plots.

Surficial deposits

The property is underlain by basal lodgement till with thicknesses ranging from < 1 m to over 5 m. The till is compact, fissile and has clast content ranging from 10 to 25%. Clasts are often faceted and striated, commonly subangular to subrounded shapes. The till directly overlies bedrock except in the Lottie Creek valley, where fluvial gravel was found in the base of pit M-8. This gravel was deposited into the valley during the onset of glaciation in the region. Locally overlying the basal lodgement till is ablation till and/or basal melt-out till, sometimes combinations of both. Ablation till can be expected at the higher elevations, with deposits locally exceeding 2 metres. Basal melt-out till was found in the lower elevations (pit M-6) and diamictons commonly exhibit crude stratigraphy. The till is moderately to weakly compacted with clast contents ranging from 35 to almost 50%. Areas of clast-supported till are not uncommon. Clasts are sometimes faceted and striated, but many are not, suggesting supraglacial transport. Roundness ranges from subrounded to very angular.

The lower part of Lottie Creek valley was subject to glaciolacustrine sedimentation and was likely a small arm of a large lake that occupied the Big Creek Valley and which deposited massive to varved silts and clays. Shallow water deposition of massive silts to bedded silts and sands occur in the lowermost part of the valley at the property. Local ponding of silt occurs in the flat region between pits M-23 and M-5, with silt thicknesses ranging from a few centimetres to > 1 m.

Discussion

The major source of ice in the region was the Caribou Mountains to the southeast. Ice flowed locally during the onset of glaciation, following the valley from east to west.

Regional work by Clague (1987), shows as the ice sheet thickened, ice flowed southwesterly from the Caribou Mountains, across the Mowdish Range and then flowed to the northwest roughly parallel to the regional bedrock structure that is occupied by the Bowron, Swan and Spectacle lakes. The exact extent of the southwesterly flow and its incorporation into the northwestern flow is unknown.

Local flows appear to be the predominate factor in controlling the deposition of sediments within the Lottie Creek Valley below the Twin Sisters Mountains. In fact, ice probably flowed around the Twin Sisters and into the valley, flowing east to west. As ice thickened and topped over the Twin Sisters, ice flowed to the northwest, as indicated by flutings and striations to the northwest of the property, likely out of the influence of the Twin Sisters Mountain (Fig. 7). Mapping of ice flow indicators from the top of Twin Sisters Mountain should confirm the regional ice flow direction.

Deglaciation was typical of that described by Clague (1989), ice downwasted at the higher elevations, and flowed locally in the valleys. A large ice-dammed lake formed in Big Valley and thick glaciolacustrine deposits were deposited in the lower part of the valley and a thin veneer of silt overlies the Lottie Creek Valley, suggesting either possible stagnant ice sat in the valley or maximum lake level was just over 4000 ft asl.

Implications for Drift Prospecting

The initial discovery boulders are established to be contained within basal lodgement till. This eliminates the possibility of long distance transport and the mineral-rich boulders being deposited in supraglacial debris. The low frequency of boulders discovered suggested that the immediate area is likely within a distal dispersal fan. Additional basal till geochemistry should provide indications of distance to source, but, I

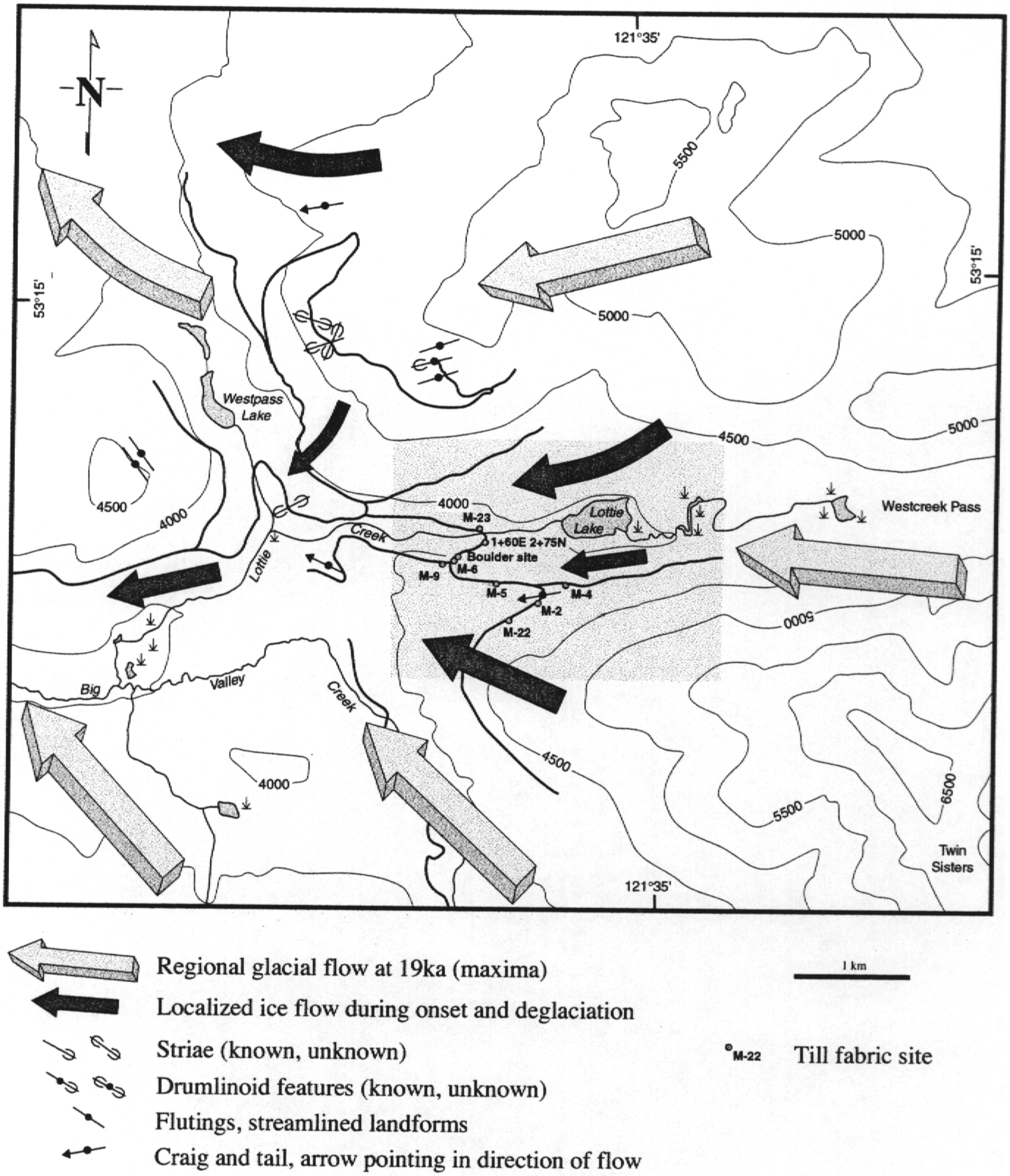


Fig. 7 Map of the Lottie Creek Valley showing major and minor ice flow directions. The shaded region is the property scale fabric work (see Fig. 6).

am reluctant to speculate the transport distance without studying the follow-up basal till geochemistry.

However, conditions such as variable relief and a strong local influence of ice flow should be considered as well as a regional flow component. Examples show that in areas of moderate relief, these dispersal fans can range from hundreds of metres to several kilometres down-ice from source (Paulen, 1999). The down-ice dispersal model at the Samatosum and Rea Gold mines in the Adams Lake area also show that the distance from source to the initial surface expression is almost 2 km (Lett *et al.*, 1998; Paulen, 1999). Therefore, regional till geochemistry should be applied to aid in hunting down the source of the mineralized boulders before additional resources such as close-spaced sampling and geophysics are applied.

Care must be taken in interpretation of B-horizon sampling on the property. The slope is steep enough to be a factor with hydromorphic dispersal. The presence of a silt veneer in the low-lying areas also becomes problematic. B-horizon sampling will only reflect the geochemistry of the silt, which was post-glacially remobilized and deposited. This enhances your target regionally, but causes false anomalies when property-scale surveys are utilized.

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Discovery site

Azimuth	Plunge
257	15
215	16
270	06
243	14
040	15
035	15
105	12
250	24
254	22
276	47
065	05
068	17
242	25
285	03
250	10
106	17
204	06
055	19
043	09
015	16
225	21
055	18
078	04
227	14
055	08
253	07
016	14
060	28
079	10
085	18
140	01
081	12
077	01
250	15
238	14
082	17
263	29
045	17
235	15
040	06
103	11
245	20
242	02
220	05
105	15
087	02
092	12
105	41
222	15
235	15

Line 1+60E 2+75N

Azimuth	Plunge
261	03
289	16
339	09
025	29
252	17
009	13
216	18
274	15
290	10
215	06
120	10
290	30
329	16
091	19
095	01
082	20
270	06
262	26
206	20
200	06
274	15
274	09
083	11
100	06
284	49
280	31
300	07
255	01
055	15
089	08
092	10
169	04
276	34
084	19
269	25
098	39
025	18
265	32
215	03
072	12
079	05
276	13
282	03
247	07
251	15
346	01
045	12
095	05
072	06
205	04

Pit M-2

Azimuth	Plunge
074	06
275	03
024	18
219	48
032	07
250	16
272	41
252	20
185	01
216	46
068	05
066	04
255	18
215	18
201	30
205	08
186	45
009	19
214	18
225	32
294	16
202	22
186	01
232	06
016	14
030	24
265	09
284	02
221	16
058	15
280	29
245	16
055	63
027	45
231	24
200	01
239	01
232	08
258	19
256	35
321	11
074	04
252	03
236	14
233	08
228	41
226	02
060	03
230	09
202	33

Pit M-4

Azimuth	Plunge
058	33
179	01
232	24
228	24
240	03
149	01
115	09
019	07
290	04
276	16
358	30
025	01
119	16
060	31
272	39
025	12
132	06
325	05
112	16
096	11
058	33
263	04
304	19
291	02
285	11
035	16
281	04
225	16
291	02
105	02
049	30
092	19
138	09
296	10
353	14
335	02
043	05
252	05
225	13
271	23
251	02
304	13
102	25
111	04
148	26
348	16
325	13
345	32
324	07
223	11

Pit M-5

Azimuth	Plunge
316	17
125	14
175	01
313	25
328	07
220	01
348	01
219	08
136	19
171	46
081	05
241	13
256	21
280	04
300	09
250	23
138	03
085	24
065	06
249	19
141	24
116	10
155	20
092	16
033	11
235	01
070	25
072	24
259	02
062	02
055	32
035	21
258	18
090	17
277	04
048	21
082	01
247	11
256	10
016	14
240	19
170	11
078	27
049	18
088	34
043	19
240	02
241	04
085	12
102	22

Pit M-6

Azimuth	Plunge
030	25
139	01
173	06
331	35
287	01
225	08
200	03
201	06
263	25
230	08
045	22
285	26
065	07
053	11
222	06
105	05
021	31
083	03
312	29
265	14
013	48
110	04
274	21
268	29
265	09
274	15
250	25
260	11
270	26
205	32
255	52
265	11
286	33
195	01
025	16
232	03
160	18
245	06
260	17
265	03
275	10
019	34
239	21
210	06
295	29
275	12
251	02
269	26
241	38
038	16

Pit M-9

Azimuth	Plunge
334	32
292	06
248	03
255	07
242	01
240	01
231	09
264	17
293	05
276	15
190	01
354	14
244	16
083	09
115	12
355	13
270	10
140	21
148	16
222	05
071	06
254	04
281	04
053	03
073	54
071	40
071	42
084	11
065	10
036	05
215	18
280	22
081	10
223	06
038	01
242	07
273	23
234	15
098	26
055	08
055	02
321	17
054	14
262	15
234	06
271	01
047	03
049	09
306	36
222	13

Pit M-22

Azimuth	Plunge
054	02
045	01
145	29
121	01
139	05
285	12
107	02
021	06
035	18
275	11
214	05
195	16
198	03
265	14
043	27
228	08
201	01
207	15
168	04
227	10
120	01
055	05
215	15
214	01
162	10
092	01
050	26
256	20
005	17
025	07
066	01
220	03
216	06
245	17
310	11
295	05
131	17
281	25
270	46
160	14
050	03
056	05
272	16
287	06
023	05
275	10
127	04
005	19
286	09
135	04

Pit M-23

Azimuth	Plunge
079	05
268	09
280	17
231	15
270	06
280	09
189	09
256	06
235	10
268	19
036	16
060	09
255	38
244	10
027	06
274	08
270	02
262	04
277	11
229	09
235	06
238	33
275	08
266	19
255	13
262	33
271	02
236	06
240	24
254	05
276	20
278	06
282	17
230	24
251	13
237	17
275	08
256	05
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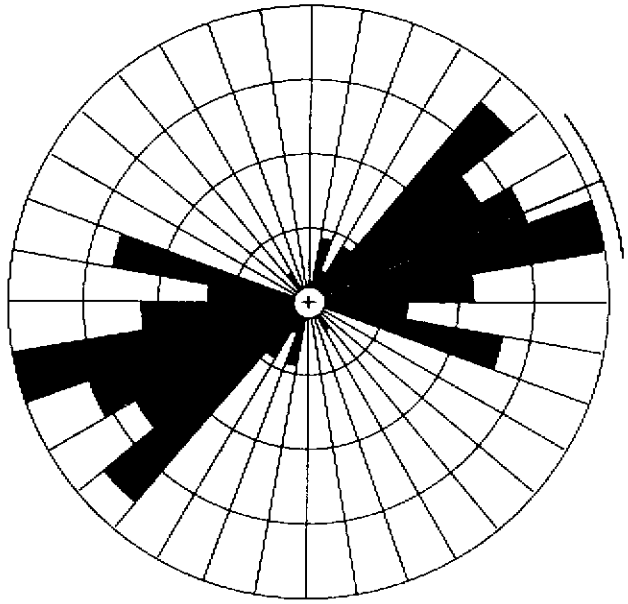
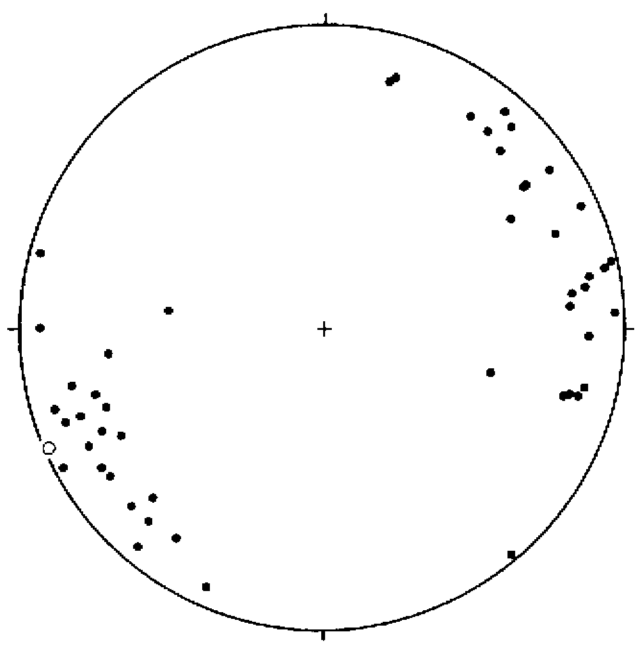
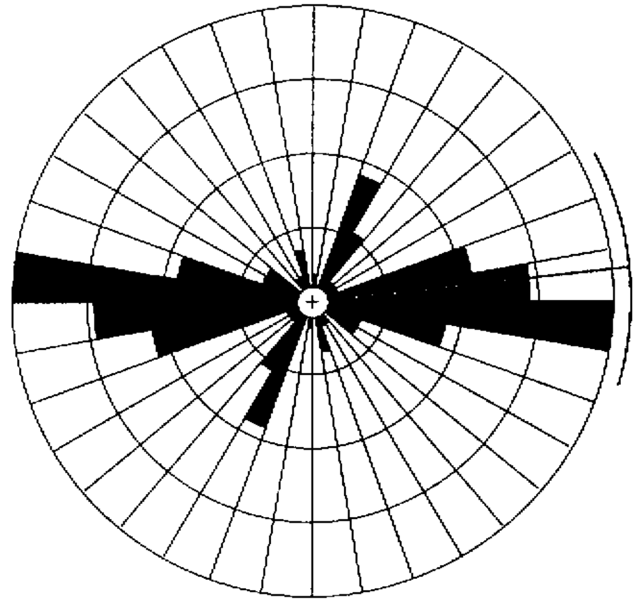
050	04
275	18
266	12



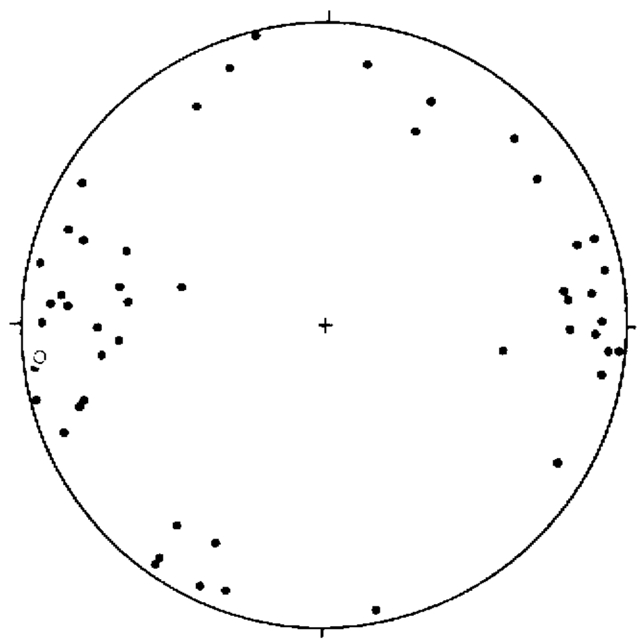
Ore boulder site - Fabric #1	Statistics
N = 50 Class Interval = 10 degrees Maximum Percentage = 18.0 Mean Percentage = 9.09 Standard Deviation = 5.61	Vector Mean = 66.8 Conf. Angle = 14.28 R Magnitude = 0.671 Rayleigh = 0.0000



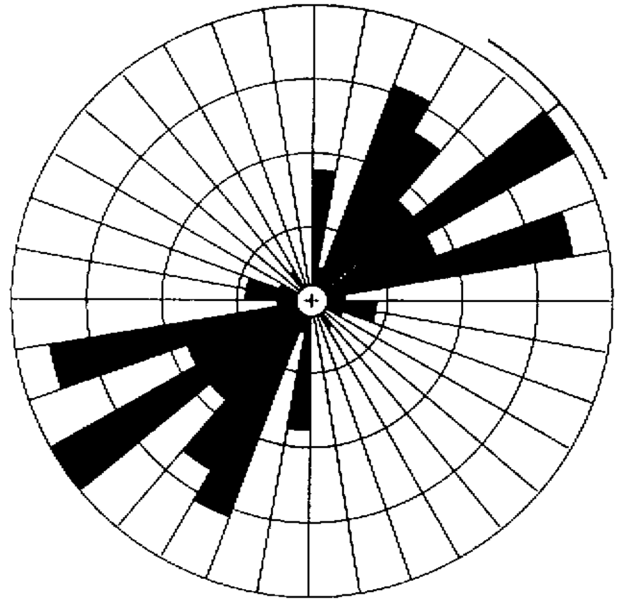
Data	Schmidt Equal Area Projection	Statistics
• Ore Boulder site - Fabric 1	N = 50	○ Mean Lineation Vector 246.2 0.4 E1 = 0.768 E2 = 0.152 E3 = 0.080 r1 = 1.62 r2 = 0.64 K = 2.53 s. var. = 0.745 Rbar = 0.255



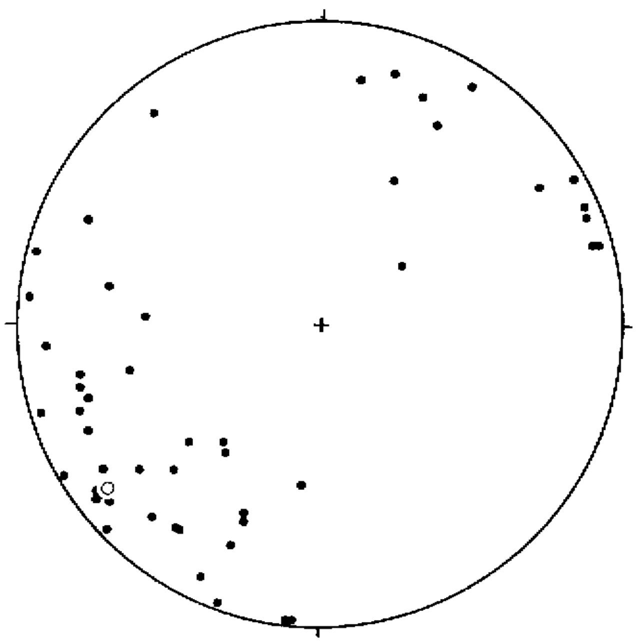
Lottie Creek pit	Statistics
N = 50 Class Interval = 10 degrees Maximum Percentage = 22.0 Mean Percentage = 6.67 Standard Deviation = 6.02	Vector Mean = 83.8 Conf. Angle = 21.88 R Magnitude = 0.480 Rayleigh = 0.0000



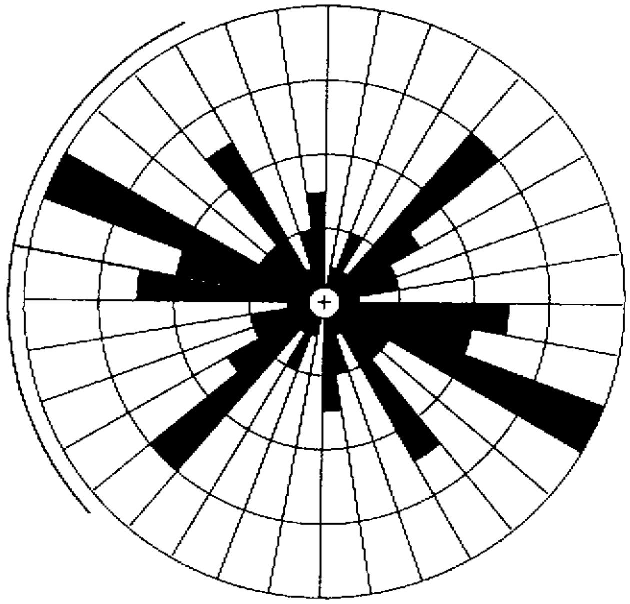
Data	Schmidt Equal Area Projection	Statistics
▪ Lottie Creek Pit - Line 1+60E 2+75N		○ Mean Lineation Vector 263.2 4.7 E1 = 0.674 E2 = 0.248 E3 = 0.078 r1 = 1.00 r2 = 1.15 K = 0.86 s. var. = 0.719 Rbar = 0.281
	N = 50	



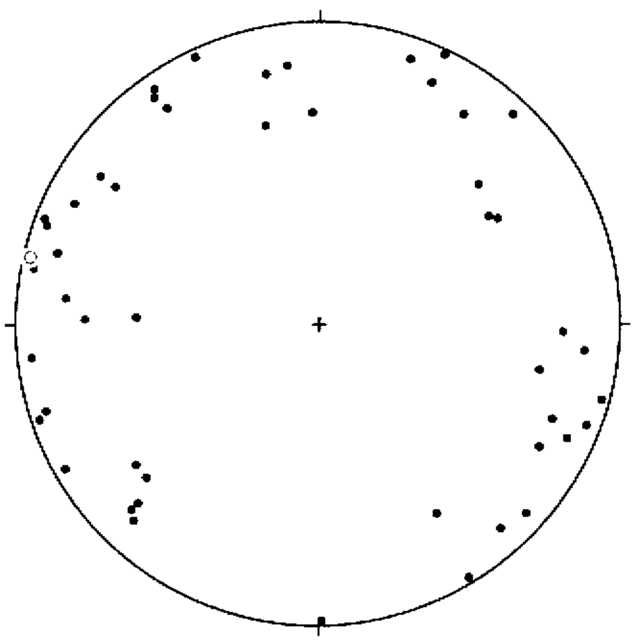
Pit M-2	Statistics
N = 50 Class Interval = 10 degrees Maximum Percentage = 18.0 Mean Percentage = 7.69 Standard Deviation = 5.59	Vector Mean = 50.4 Conf. Angle = 16.95 R Magnitude = 0.595 Rayleigh = 0.0000



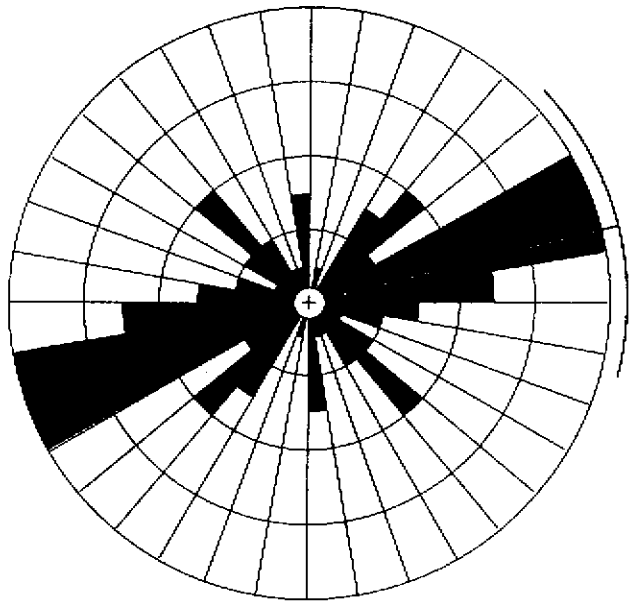
Data	Schmidt Equal Area Projection	Statistics
• Pit M-2	N = 50	○ Mean Lineation Vector 231.9 11.4 E1 = 0.706 E2 = 0.184 E3 = 0.111 r1 = 1.35 r2 = 0.51 K = 2.65 s. var. = 0.525 Rbar = 0.475



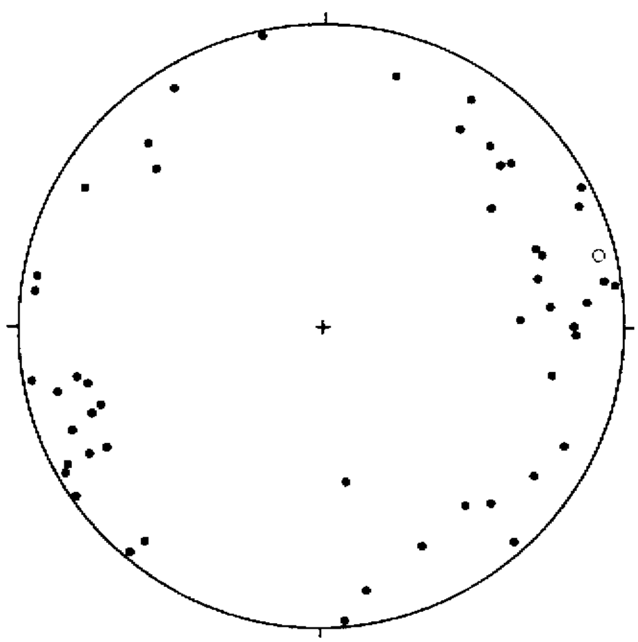
Pit M-4	Statistics
N = 50 Class Interval = 10 degrees Maximum Percentage = 16.0 Mean Percentage = 5.88 Standard Deviation = 3.97	Vector Mean = 280.0 Conf. Angle = 52.90 R Magnitude = 0.210 Rayleigh = 0.1107



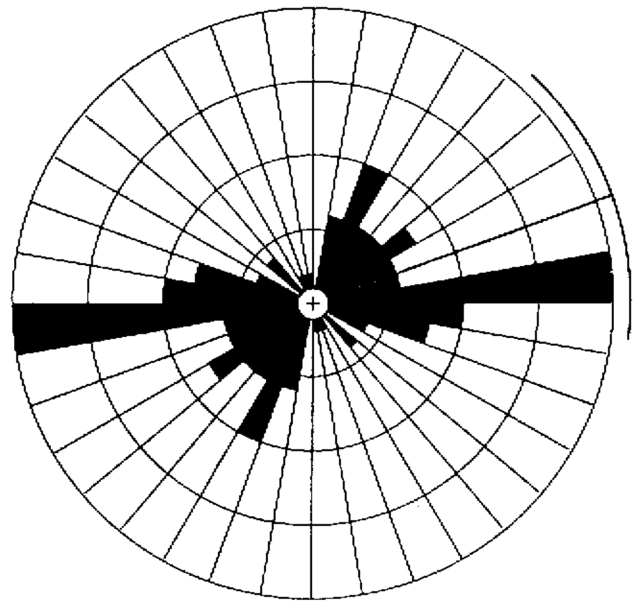
Data	Schmidt Equal Area Projection	Statistics
• Pit M-4	N = 50	○ Mean Lineation Vector 282.8 1.0 E1 = 0.559 E2 = 0.364 E3 = 0.077 r1 = 0.43 r2 = 1.55 K = 0.28 s. var. = 0.728 Rbar = 0.272



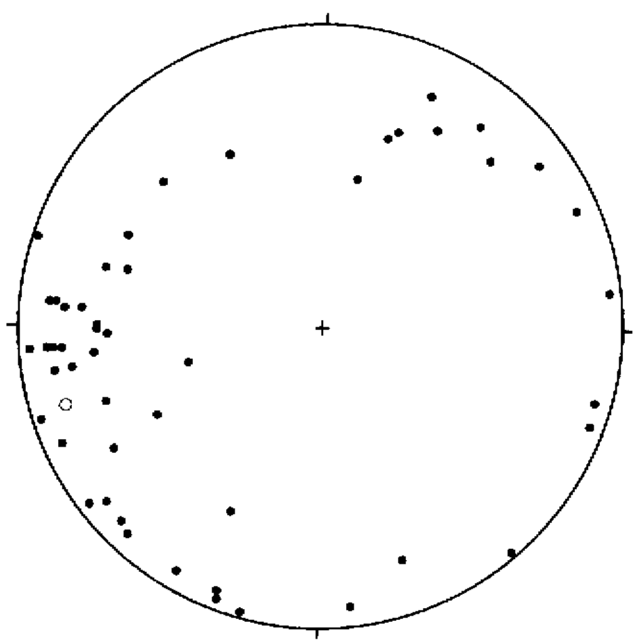
Pit M-5	Statistics
N = 50	Vector Mean = 75.5
Class Interval = 10 degrees	Conf. Angle = 28.58
Maximum Percentage = 16.0	R Magnitude = 0.375
Mean Percentage = 6.25 Standard Deviation = 4.42	Rayleigh = 0.0009



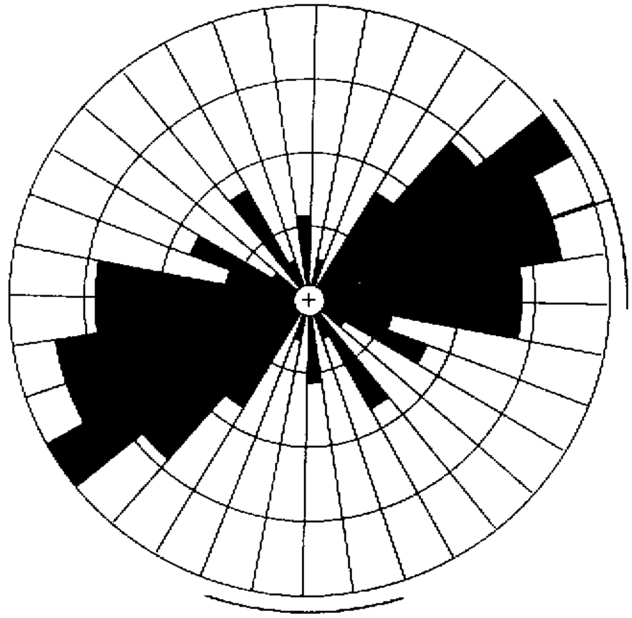
Data	Schmidt Equal Area Projection	Statistics
• Pit M-5	N = 50	○ Mean Lineation Vector 75.6 5.3 E1 = 0.635 E2 = 0.284 E3 = 0.080 r1 = 0.80 r2 = 1.26 K = 0.64 s. var. = 0.744 Rbar = 0.256



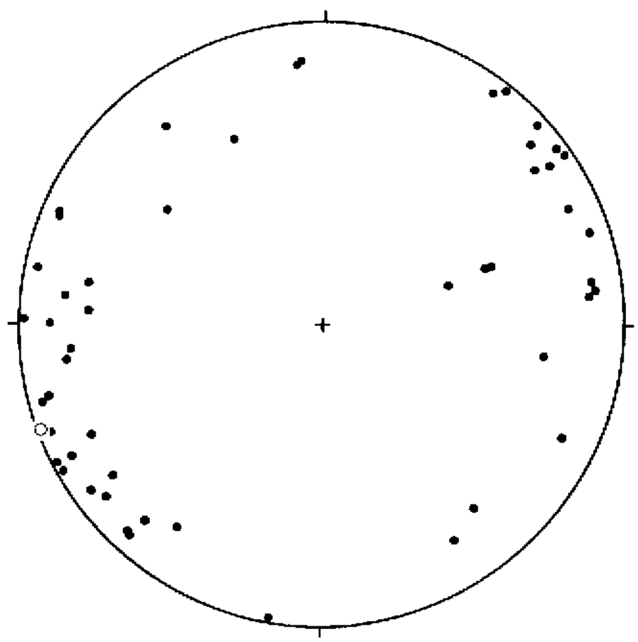
Pit M-6	Statistics
N = 50 Class Interval = 10 degrees Maximum Percentage = 20.0 Mean Percentage = 6.67 Standard Deviation = 4.44	Vector Mean = 69.9 Conf. Angle = 26.94 R Magnitude = 0.398 Rayleigh = 0.0004



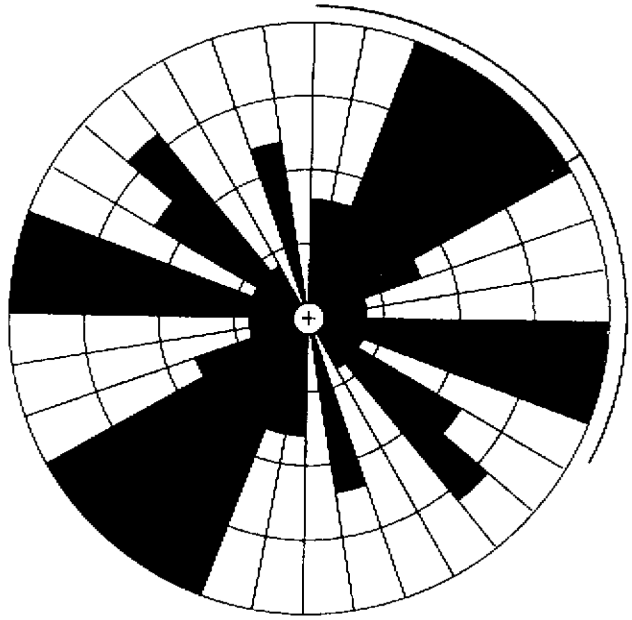
Data	Schmidt Equal Area Projection	Statistics
• Pit M-6	N = 50	○ Mean Lineation Vector 252.1 11.4 E1 = 0.641 E2 = 0.282 E3 = 0.077 r1 = 0.82 r2 = 1.30 K = 0.63 s. var. = 0.524 Rbar = 0.476



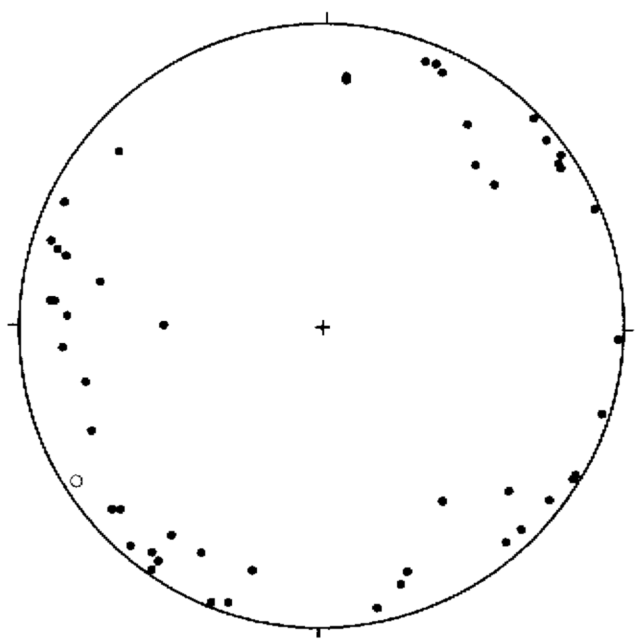
Pit M-9	Statistics
N = 50 Class Interval = 10 degrees Maximum Percentage = 14.0 Mean Percentage = 7.14 Standard Deviation = 4.05	Vector Mean = 70.3 Conf. Angle = 20.88 R Magnitude = 0.499 Rayleigh = 0.0000



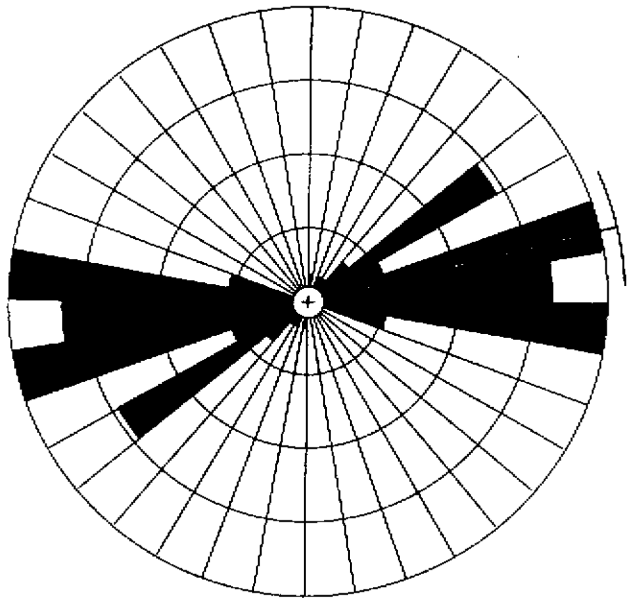
Data	Schmidt Equal Area Projection	Statistics
• Pit M-9	N = 50	○ Mean Lineation Vector 249.2 0.3 E1 = 0.692 E2 = 0.231 E3 = 0.077 r1 = 1.10 r2 = 1.10 K = 1.00 s. var. = 0.738 Rbar = 0.262



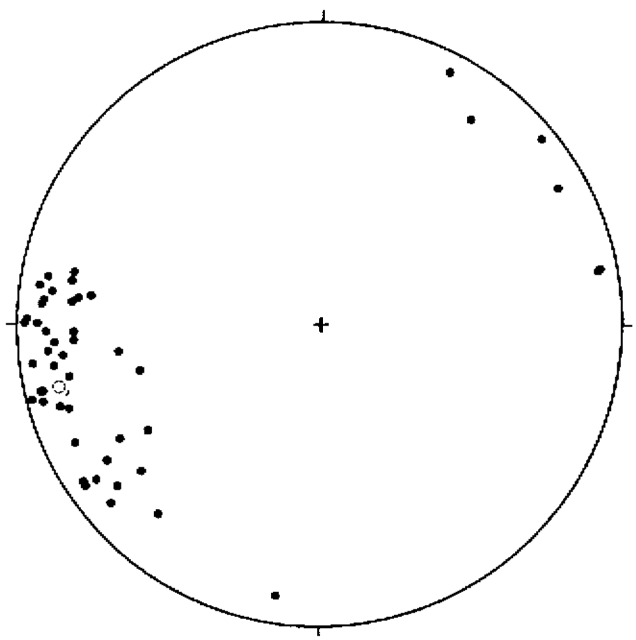
Pit M-22	Statistics
N = 50 Class Interval = 10 degrees Maximum Percentage = 10.0 Mean Percentage = 6.25 Standard Deviation = 3.36	Vector Mean = 57.9 Conf. Angle = 58.27 R Magnitude = 0.192 Rayleigh = 0.1585



Data	Schmidt Equal Area Projection	Statistics
• Pit M-22	N = 50	○ Mean Lineation Vector 236.9 3.5 E1 = 0.565 E2 = 0.384 E3 = 0.051 r1 = 0.39 r2 = 2.02 K = 0.19 s. var. = 0.795 Rbar = 0.205



Pit M-23	Statistics
N = 50 Class Interval = 10 degrees Maximum Percentage = 22.0 Mean Percentage = 10.00 Standard Deviation = 8.26	Vector Mean = 75.8 Conf. Angle = 11.08 R Magnitude = 0.777 Rayleigh = 0.0000



Data	Schmidt Equal Area Projection	Statistics
• Pit M-23	N = 50	○ Mean Lineation Vector 256.0 11.4 E1 = 0.864 E2 = 0.106 E3 = 0.030 r1 = 2.10 r2 = 1.26 K = 1.67 s. var. = 0.269 Rbar = 0.731

Appendix C - Geophysical Report
Horizontal Loop EM Survey
Lottie Project
-- by --
SJ Geophysics Ltd.
- Zorn Dujakovic, Geophysicist
- E. Trent Pezzot, BSc P. Geo.

GEOPHYSICAL REPORT

HORIZONTAL LOOP EM SURVEY

LOTTIE PROJECT

Cariboo Mining Division, N.T.S. 93H/4

5898775N, 5932374E, Zone 10, NAD27
British Columbia, Canada

EUREKA RESOURCES INC.

Vancouver, BC

Canada

Survey by

SJ GEOPHYSICS LTD.

Report by

S.J.V. CONSULTANTS LTD.

Zoran Dujakovic, Geophysicist

September, 1999

TABLE OF CONTENTS

<u>List of Plates</u>:- These maps are located in the map pocket at the back of the report.

1. SUMMARY

A reconnaissance Horizontal Loop EM Survey was undertaken on behalf of Eureka Resources Inc. on three road traverses and a small grid (of five traverses) covering parts of the Lottie property. A shallow conductor with a conductivity of between 10 to 30 siemens was found to strike across the grid. This conductor could indicate metallic sulphide mineralization. Recommendations for a more regional evaluation have been made.

2. INTRODUCTION

This report describes the results of a ground geophysical exploration program that was undertaken during the period August 30 to September 3, 1999 on the Lottie Project. The purpose of the survey was to detect conductive sulphide mineralization. A frequency domain horizontal loop electromagnetic survey (HLEM) was carried out to evaluate a limited region of the Lottie property.

The survey was conducted under supervision of Warner Gruenwald, project geologist from Geoquest Consulting Ltd. and totalled 7.4 km of HLEM measurements. The survey area is located about 15 km north-west of Wells, B.C. The property is accessible by Highway 26 approximately 26 km west of Wells, then about 27 km north by logging road called 2400 road (or Kechum Creek road) and then about 23km to the east by 24A logging road.

This report is meant to be an addendum to a more complete report, and thus location maps, comprehensive description of geology and previous exploration work are treated only briefly, or not included.

3. FIELD WORK AND INSTRUMENTATION

The geophysical survey was conducted from August 30 to September 3, 1999, which included two mob-demob days and three production days. The geophysical crew consisted of Zoran Dujakovic (geophysicist) and Neil Visser (technician), both employees of SJ Geophysics Ltd. A discussion of the geophysical method used on this survey is included in Section 5. "Principle of HLEM Surveying."

The survey grid was prepared by Warner Gruenwald, project geologist and comprises three (approximately E-W) road traverses and the Lottie grid (five N-S traverses) at 100 and 200 metre intervals.

The HLEM equipment used was an APEX MAX-MIN I-10 horizontal loop EM system with MMC data logger. A 100 metre coil separation was used for the survey and the data from four frequencies was recorded; 220Hz, 880Hz, 3520Hz and 7040Hz.

The HLEM data was gathered at 25 metre station intervals. All data was downloaded daily from the field instrumentation to a computer and processed using Geopak Systems software.

4. Data Presentation

The geophysical data from this survey are displayed in two formats, as indicated below.

4.1 Stacked Profiles

The in-phase and quadrature components of the HLEM data are presented as stacked profiles on separate maps at a scale of 1:5,000. All data are relatively positioned from averages of 3 UTM measurements (NAD 27, Zone 10) made using a hand held GPS unit. (Accuracy is approximately +/- 100 m).

The in-phase and quadrature components of the HLEM data from three road traverses are presented as profiles on separate maps at a scale of 1:5,000 (Plate G2-G4).

4.2 Interpretation Plan Map

The Interpretation Plan Map (Plate G5) was made to highlight the general trends of the conductors.

5. HLEM Technique

The basic principle behind HLEM surveying is that conductive rocks in the subsurface can be excited electrically by an applying a time varying electromagnetic field at the surface. In the Max-Min I-10 horizontal loop system, the oscillating primary field is transmitted by a coil at selected frequencies between 110 Hz to 56320 Hz.

The primary field induces a secondary field in the ground as well as any conductive "target." The receiver system detects a combination of the secondary field and the primary field. The secondary field, however, is quite small compared to the primary field so it is necessary to account for the primary field by means of a reference signal from the transmitter.

The reference signal also serves to make it possible to resolve the secondary field into two components: the in-phase (real) and out-of-phase (imaginary or quadrature). The relative strengths of in-phase and out-of-phase components are a guide to the conductivity-width product (also called conductance) of the buried conductor, which is normally related to the quantity of the conductive minerals present.

The strength of the secondary field is dependent on the size and conductance of the conductor, as well as the response from the host rocks and overburden.

The separation distance between the transmitter and receiver coils approximately determines the depth of penetration of the electromagnetic signal. The choice of coil separation is dependent on the depth of the overburden (if known) or the desired depth of penetration, or both. The midpoint between transmitting and receiving coils is taken as the measuring point.

Measurement of the strength, character, and distribution of the secondary field also permits mapping of conductive formations and tells something about their size and spatial distribution.

6. INTERPRETATION

The HLEM survey shows two conductivity features across the Lottie grid. The principal conductor or conductive zone strikes across the whole grid as shown on the interpretation map Plate G5. This conductive zone was also noted on the earlier road traverse Line 1B and Line 1C, which prompted the location of the Lottie grid. The second conductor is a short strike length, very weak conductor located to the north of the main zone on Lines 4E and 6E.

The main conductive zone has an apparent thickness of up to 100m especially on Lines 6E and 2E. The conductance within this zone varies from a few seimens up to approximately 30 seimens. It is unclear if this zone consists of a number (at least two) discrete conductors or if it is a wide zone with a variable conductivity across its width. The depth to top of this conductive zone varies from a few metres on Lines 2E and 6E to possibly as much as 20 metres on Line 4E. Because of the complexity of this zone is not appropriate to determine any dips, although there is some indication that it is dipping fairly steeply to the north.

7. CONCLUSIONS & RECOMMENDATIONS

The HLEM survey on the Lottie Grid identified one HLEM conductor or conductive zone that could be related to sulphide mineralization or graphitic units. The same conductor is also partially detected across the road traverse Line 1B and Line 1C. No HLEM responses were recorded across Line 1A that would indicate conductive materials.

The geophysical interpretation should be reviewed by the project geologist and compiled with any available geological and geochemical data. Additionally, the results from a recent soil-sampling program need to be included in the analysis.

Based on encouraging results, survey grid (N-S traverse) should be extended to the east and to the west to fully delineate HLEM conductor. A 100m line spacing for additional HLEM survey is recommended.

If any of further investigation shows that disseminated sulphide mineralization is present on the Lottie Property, an Induced Polarization (IP) survey is recommended.

Respectfully submitted,

Per S.J.V. Consultants Ltd.

Zoran Dujakovic, (B.Sc.) Geophysicist

Z. Dujakovic

Date Signed: Sep. 13, 1999

SJ Geophysics Ltd.
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Eureka Resources Inc.,
1000 – 355 Burrard Street,
Vancouver, B.C., V6C 2G8

October 12, 1999

Dear Sirs:

This letter describes the results of a second phase of MaxMin surveying conducted on Erureka Resources' Lottie Property, near Wells, B.C. The first phase was completed on September 3, 1999 and the results were reported on by Zoran Dujakovic in a report dated September, 1999. This letter is written as an addendum to that report.

The second phase survey was undertaken by Chris Basil and Neil Visser from September 27 through October 1, 1999. It was designed as an extension to the previous survey where N-S lines were nominally spaced at 200 metres and data gathered at 25 metre station increments using a transmitter – receiver separation of 100 metres. This latest survey was run along intermediate lines, resulting in a final survey with 100 metre line separations. Line 600E was also extended an additional 800 metres to the north. Two lines (2E and 6E) were also surveyed with a Tx-Rx separation of 50 metres. Two reconnaissance lines (2A and 3A), following logging roads, were also surveyed.

The data from this latest survey were merged with the previous data and maps combining both data sets have been compiled. A list of the maps attached to this letter is provided as Appendix 1.

The data reveals a conductive zone (nominally 100 metres wide) that strikes east-west across the grid and is open along strike at both ends (Plate G8). This zone appears to host at least two narrow, sub-parallel, plate-like conductors. The responses on lines 0E and 100E are the most similar to those generated by a single conductor. Even so, the anomaly is wider than expected and it is likely mapping two zones that are very close together. Type curve matching in this area suggests the depth to the target is 25 to 30 metres, and that the individual zones dip near vertically or very steeply to the north. These estimates may have been affected by the presence of multiple conductors however they are supported by the 50 metre Tx–Rx data. Two very weak anomalies are noted in this data on line 2E within the broad zone. They appear to be near the maximum depth of investigation for the horizontal, coplanar configuration used here, which is approximately ½ the Tx-Rx separation, or 25 metres.

The ratio of inphase to quadrature amplitudes are very near 1:1 over most of the grid. An increase to ~ 1.5:1 is noted across lines 100E to 300E, implying an increase in the conductivity of the source in this area.

The responses in the area around line 300E are more complex than elsewhere on the grid. There is a possibility that the conductor(s) may be offset in the manner of a right-lateral fault in this area.

Line 600E was extended from station 50N to 850N. No significant anomalies were mapped on this line.

Line "2A" commences at STN 1+50N on Line 2+00E, on a road by Lottie Creek. The line extends at 280^0 along the road for 400 meters.

Line "3A" is located off the plan maps. It starts at STN 4+75N on Line 7+00W, which is at junction of logging roads. It extends along a logging road (Spur 10) at an initial bearing of 72^0 to station 7+75. From 7+75 to 11+50 the bearing along the road is 64^0. From 11+50 to 13+75 the road bearing is 75^0. This line intersects Line 6+00E, station 8+15N at station 13+90.

There are no significant anomalies noted on either of the road traverses (2A and 3A). One very weak (quadrature component only) response is noted on line 3A near station 1+75.

In summary, the MaxMin survey has detected an east-west trending zone of increased conductivity crossing the survey grid. This zone likely hosts at least two narrow, closely spaced, sub-parallel, plate-like conductors that could be related to massive sulphide mineralization or graphitic units. The depth to the top of these zones is estimated at 25 to 30 metres and they are likely oriented near vertically or dip very steeply to grid north. These targets appear to be most conductive from line 100E to 300E. They may also be offset in the manner of a right lateral fault in the vicinity of 300E.

Shallow drilling will be required to test these targets. A fence of drill holes, crossing the anomalous trend in the area of lines 100E to 200E is recommended. Holes should be angled (45^0 to 75^0) from north to south and test to a depth of at least 50 metres.

Respectfully submitted
Per S.J.V. Consultants Ltd.

E. Trent Pezzot, B.Sc., P.Geo.
Geophysics, Geology

SJ Geophysics Ltd / S.J.V. Consultants Ltd 11762 - 94th Ave., Delta, B.C. Canada
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Appendix 1

List of Plates:- The following maps are associated with this letter. Plates G-1A and G-1B replace similar numbered plates from the previous report. Plate G-5 (interpretation) from the previous report is replaced with Plate G-8. Plates G-2A to G-4B included in the previous report have not changed and are not reproduced here.

Plate G1A	HLEM Survey, In-Phase Profiles – 100 metre Tx-Rx separation
Plate G1B	HLEM Survey, Quadrature Profiles – 100 metre Tx-Rx separation
Plate G1C	HLEM Survey, In-Phase Profiles – 50 metre Tx-Rx separation
Plate G1D	HLEM Survey, Quadrature Profiles – 50 metre Tx-Rx separation
Plate G5A	HLEM Survey, In-Phase & Quadrature Profiles, Line 2A
Plate G6A	HLEM Survey, In-Phase & Quadrature Profiles, Line 3A
Plate G7A	HLEM Survey, In-Phase & Quadrature Profiles, Line 600E extension
Plate G8	HLEM Survey, Interpretation Map

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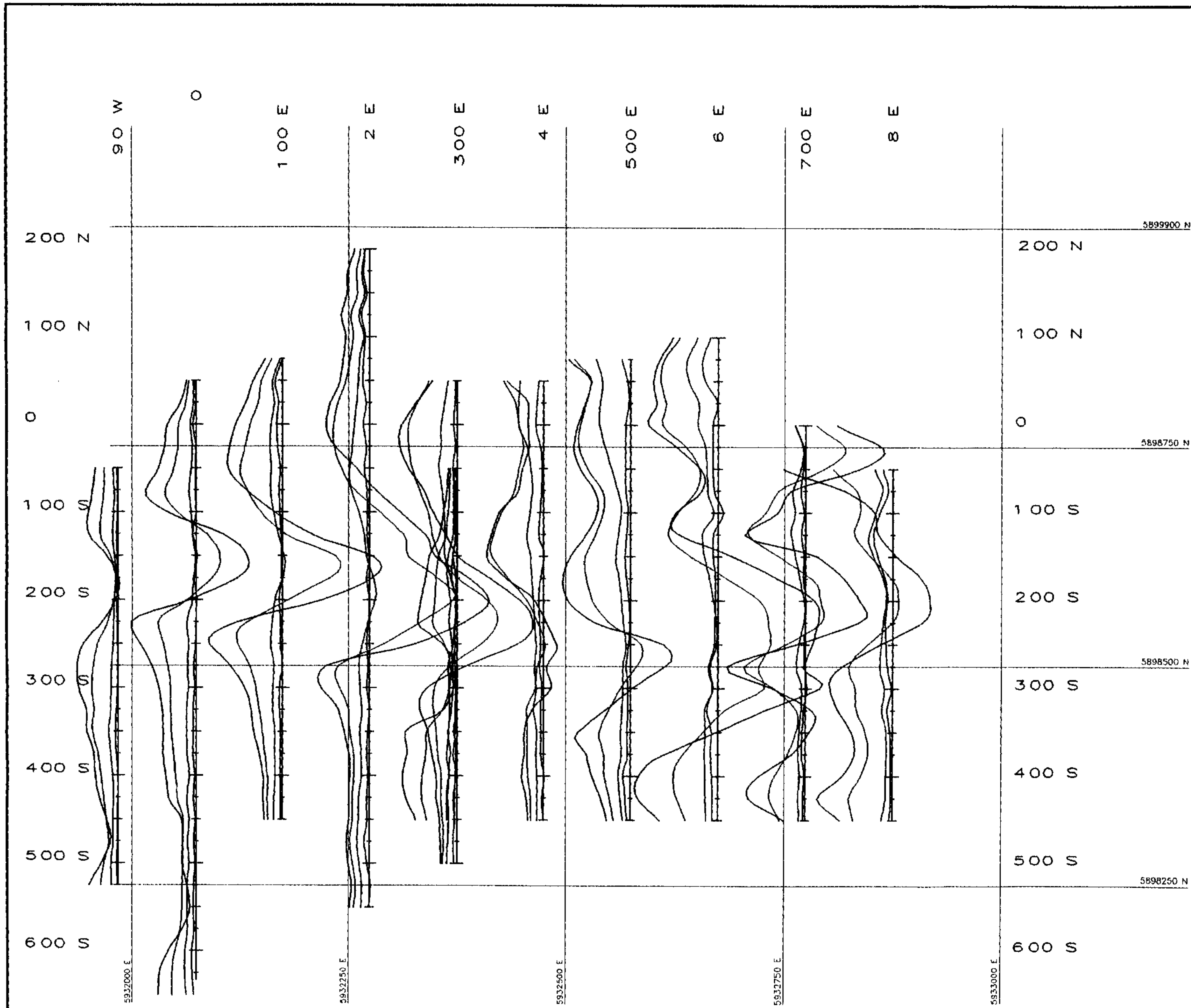
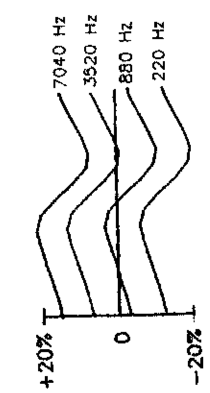
tel: (604) 582-1100 fax: (604) 589-7466 e-mail: sydv@sjgeop.bc.ca



LEGEND

IN-PHASE PROFILES



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MaxMin Equipment: MM I-10 S/N 10357
Mode: Max1 (Horizontal Coplanar)
Coil Separation: 100m
Station Spacing: 25m
Frequencies (Hz): 220, 880, 3520 & 7040

EUREKA RESOURCES INC.

Lottie Project

HLEM SURVEY
IN-PHASE PROFILES

CARIBOO MD., NTS 93H/4, NAD 27, ZONE 10

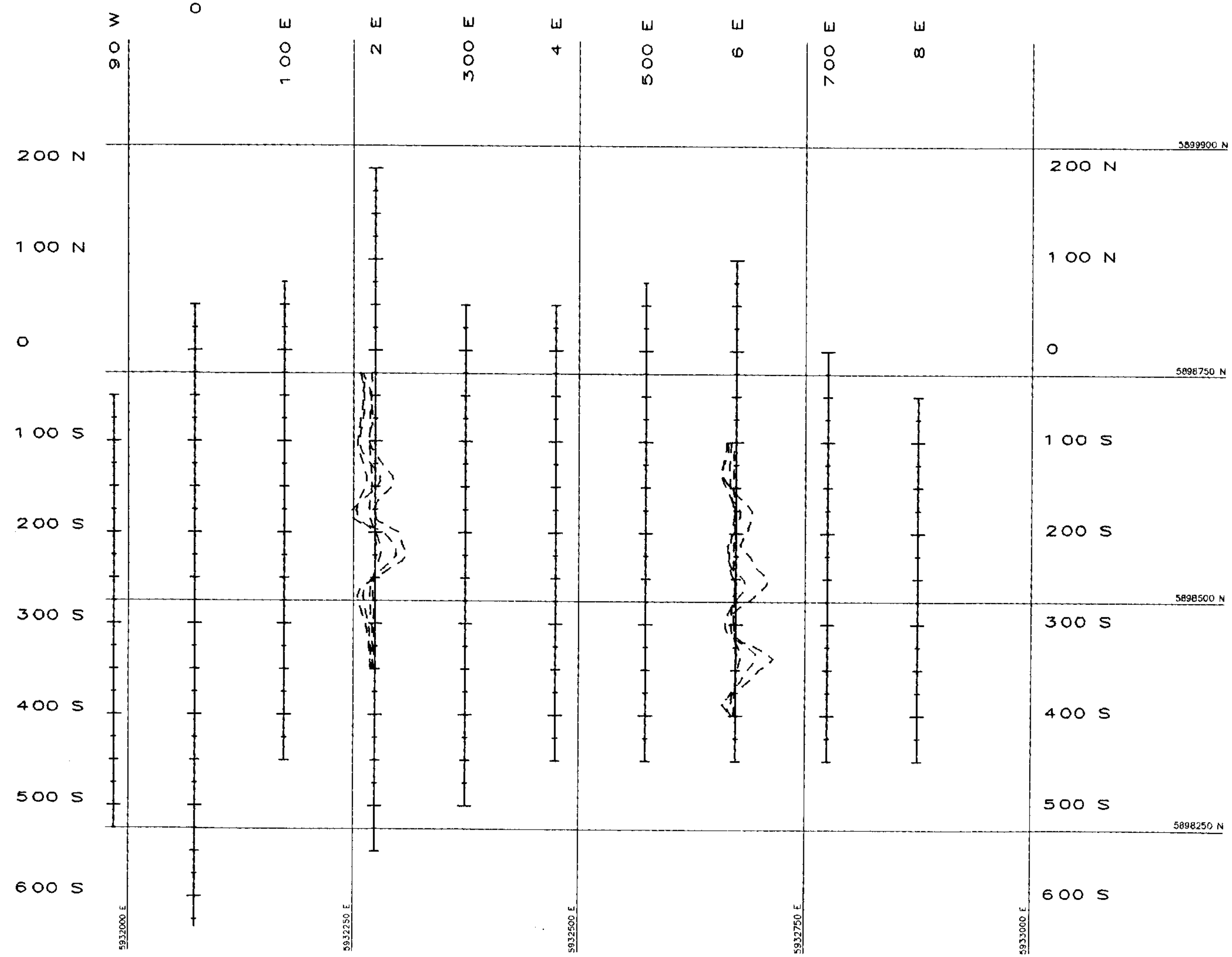
Scale in Metres

50 0 50 100 150

SJ GEOPHYSICS LTD.

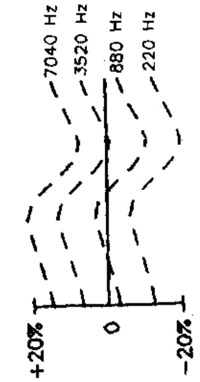
PLOTTING DATE: OCT/99

PLATE G1A



LEGEND

QUADRATURE PROFILES



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Frequencies (Hz): 220, 880, 3520 & 7040

EUREKA RESOURCES INC.

Lottie Project

HLEM SURVEY
QUADRATURE PROFILES

CARIBOO MD, NTS 93H/4, NAD 27, ZONE 10

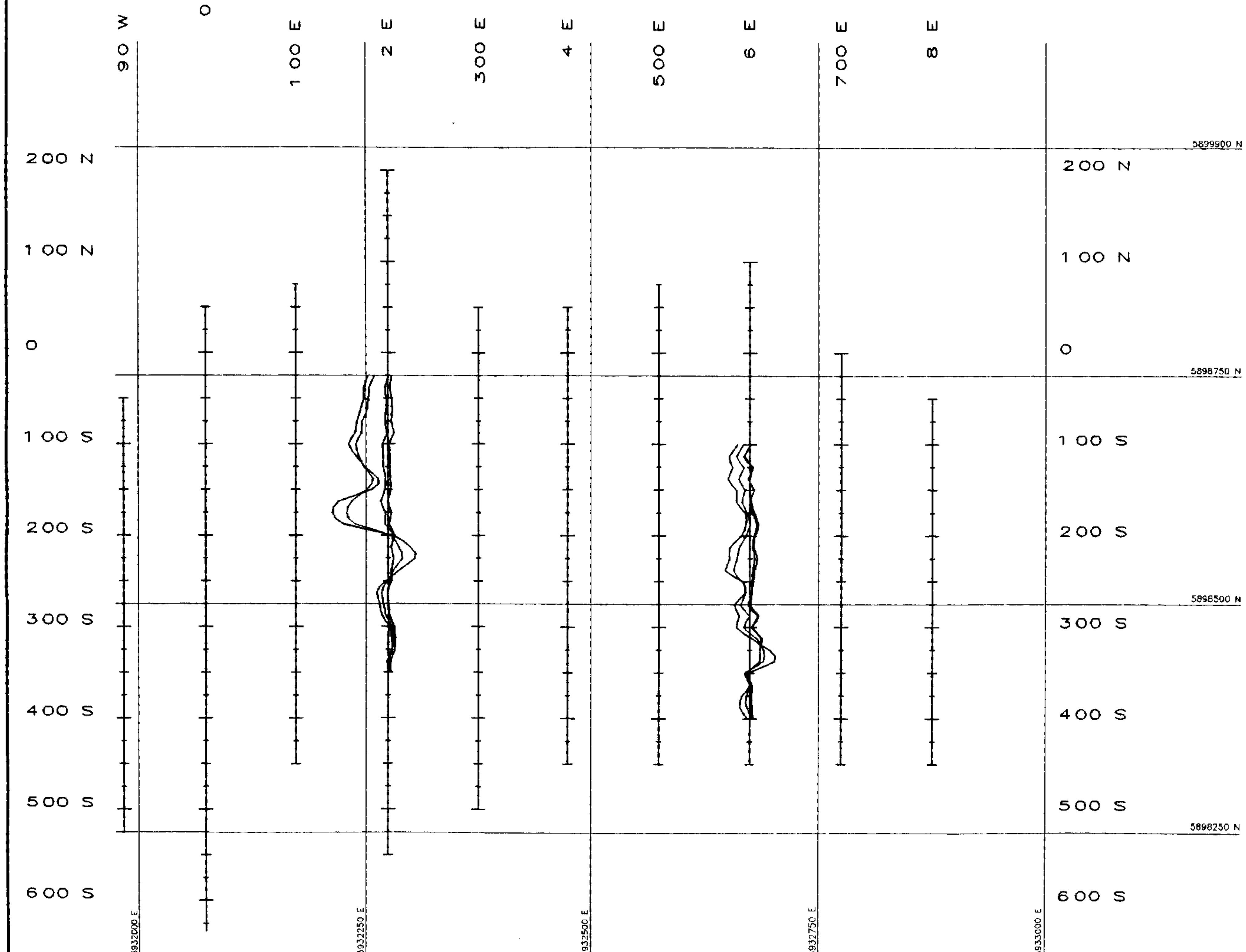
Scale in Metres

50 0 50 100 150

SJ GEOPHYSICS LTD.

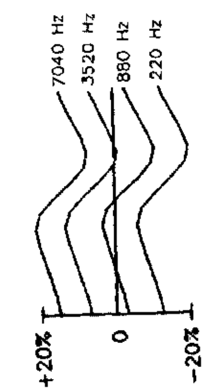
PLOTTING DATE: OCT/99

PLATE G11
G18



LEGEND

IN-PHASE PROFILES



INSTRUMENTATION:

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Mode: Max1 (Horizontal Coplanar)
Coil Separation: 50m
Station Spacing: 12.5m
Frequencies (Hz): 220, 880, 3520 & 7040

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Lottie Project

HLEM SURVEY
IN-PHASE PROFILES

CARIBOO MD, NTS 93H/4, NAD 27, ZONE 10

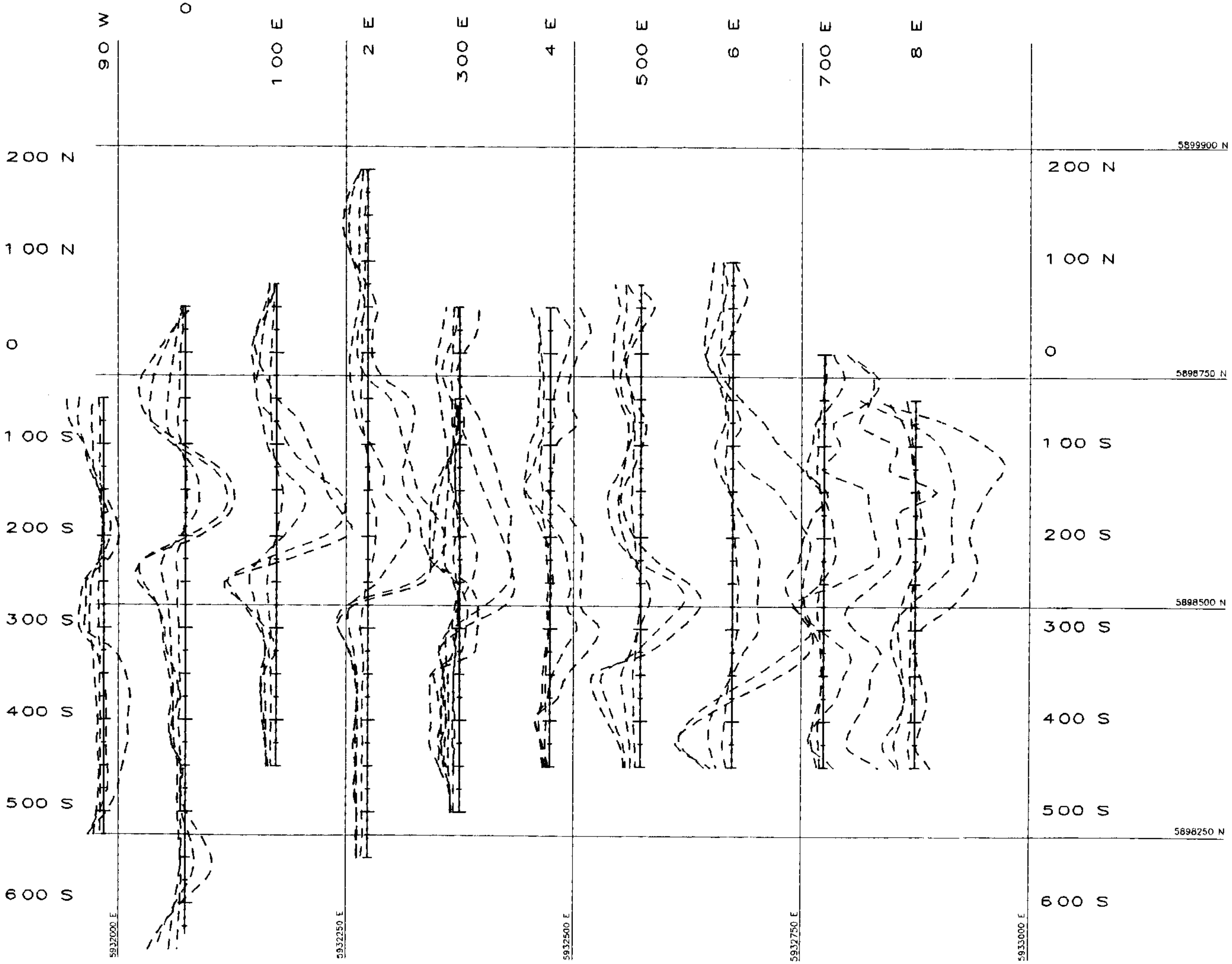
Scale in Metres

50 0 50 100 150

SJ GEOPHYSICS LTD.

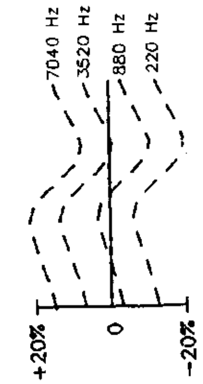
PLOTTING DATE: OCT/99

PLATE G1
G1C



LEGEND

QUADRATURE PROFILES



INSTRUMENTATION:

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Mode: Max1 (Horizontal Coplanar)
Coil Separation: 100m
Station Spacing: 25m
Frequencies (Hz): 220, 880, 3520 & 7040

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Lottie Project

HLEM SURVEY QUADRATURE PROFILES

CARIBOO MD, NTS 93H/4, NAD 27, ZONE 10

Scale in Metres

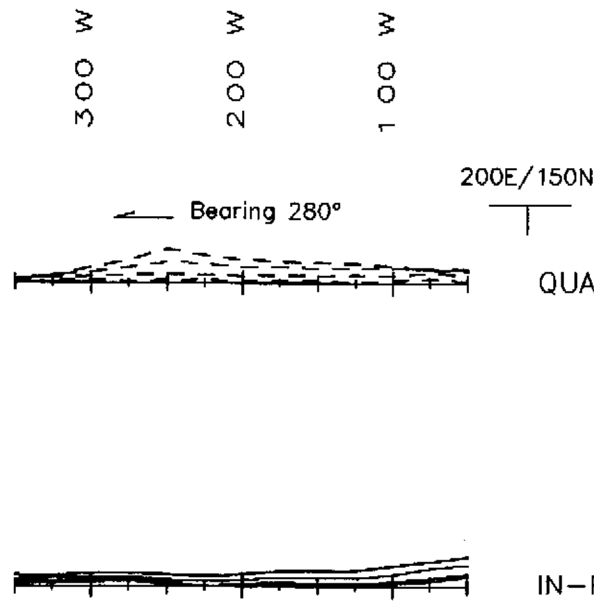
50 0 50 100 150

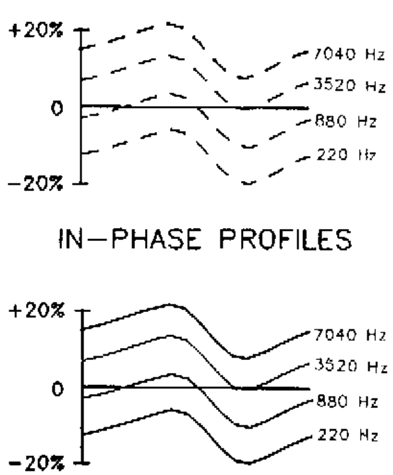
SJ GEOPHYSICS LTD.

PLOTTING DATE: OCT/99

PLATE G11
G10

Line 2A





INSTRUMENTATION:

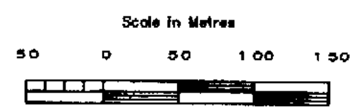
MaxMin Equipment: MM I-10 S/N 10357
Mode: Max1 (Horizontal Coplanar)
Coil Separation: 100m
Station Spacing: 25m
Frequencies (Hz): 220, 880, 3520 & 7040

EUREKA RESOURCES INC.

Lottie Project

HLEM SURVEY
IN-PHASE & QUADRATURE PROFILES

CARIBOO MD, NTS 93H/4, NAD27, ZONE 10



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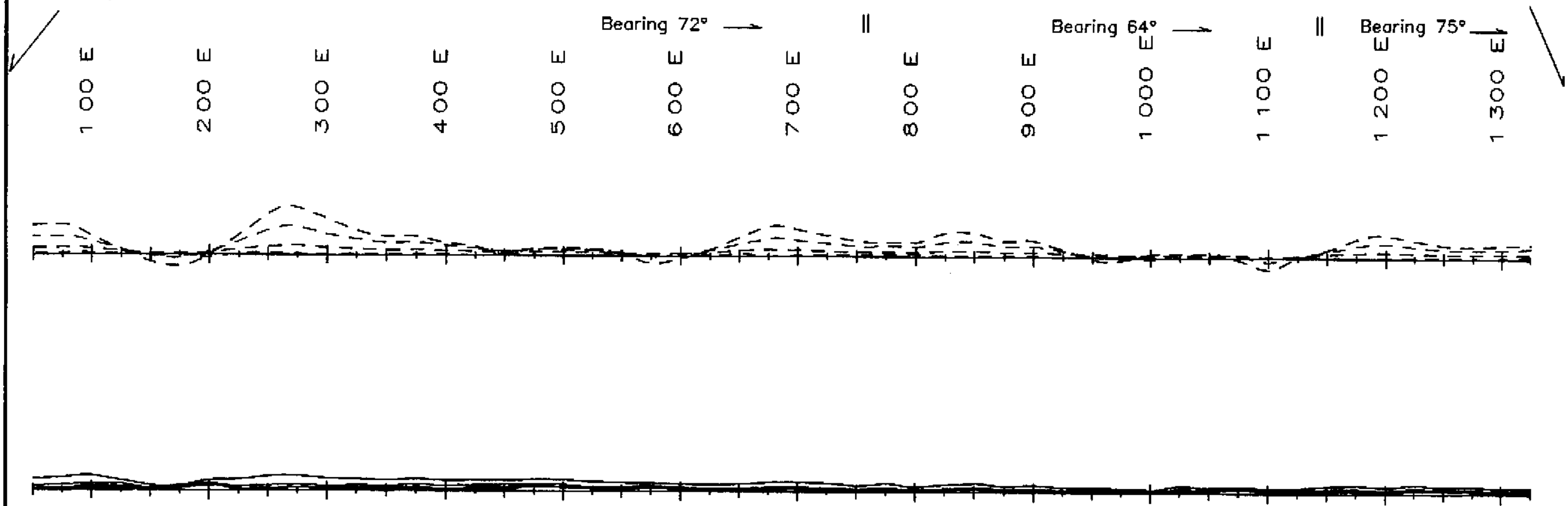
PLOTTING DATE: OCT/99

PLATE G5A

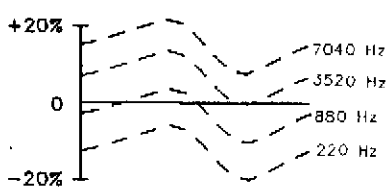
Line 3A

700W/475N @ 0E

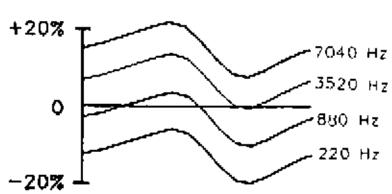
600E/815N @ 1390E



QUADRATURE PROFILES



IN-PHASE PROFILES



INSTRUMENTATION:

MaxMin Equipment: MM I-10 S/N 10357
Mode: Max1 (Horizontal Coplanar)
Coil Separation: 100m
Station Spacing: 25m
Frequencies (Hz): 220, 880, 3520 & 7040

EUREKA RESOURCES INC.

Lottie Project

HLEM SURVEY
IN-PHASE & QUADRATURE PROFILES

CARIBOO MD, NTS 93H/4, NAD27, ZONE 10

Scale in Metres

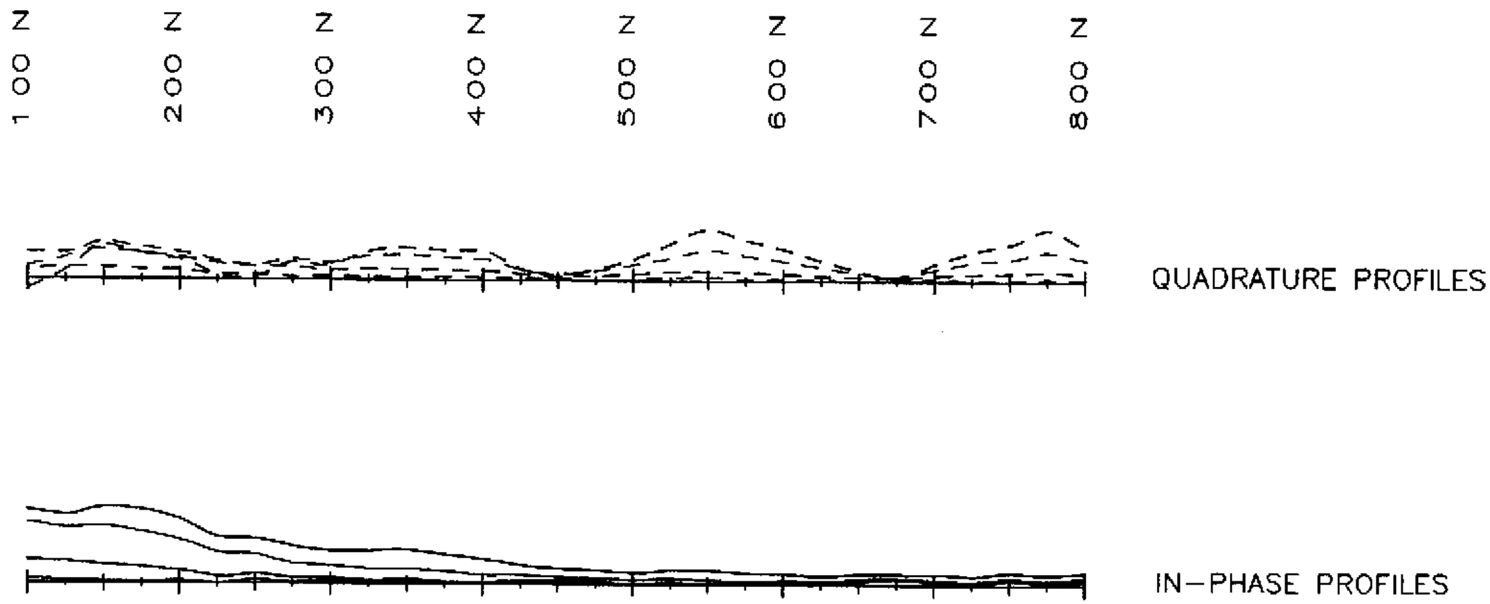
50 0 50 100 150

SJ GEOPHYSICS LTD.

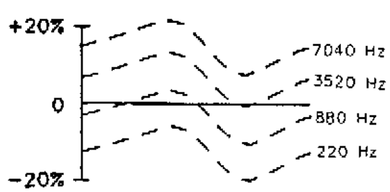
PLOTTING DATE: OCT/99

PLATE G6A

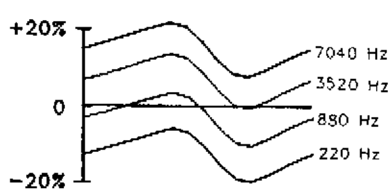
Line 600 E



QUADRATURE PROFILES



IN-PHASE PROFILES



INSTRUMENTATION:

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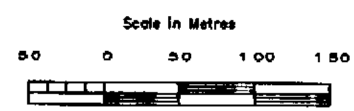
Mode: Max1 (Horizontal Coplanar)
Coil Separation: 100m
Station Spacing: 25m
Frequencies (Hz): 220, 880, 3520 & 7040

EUREKA RESOURCES INC.

Lottie Project

HLEM SURVEY
IN-PHASE & QUADRATURE PROFILES

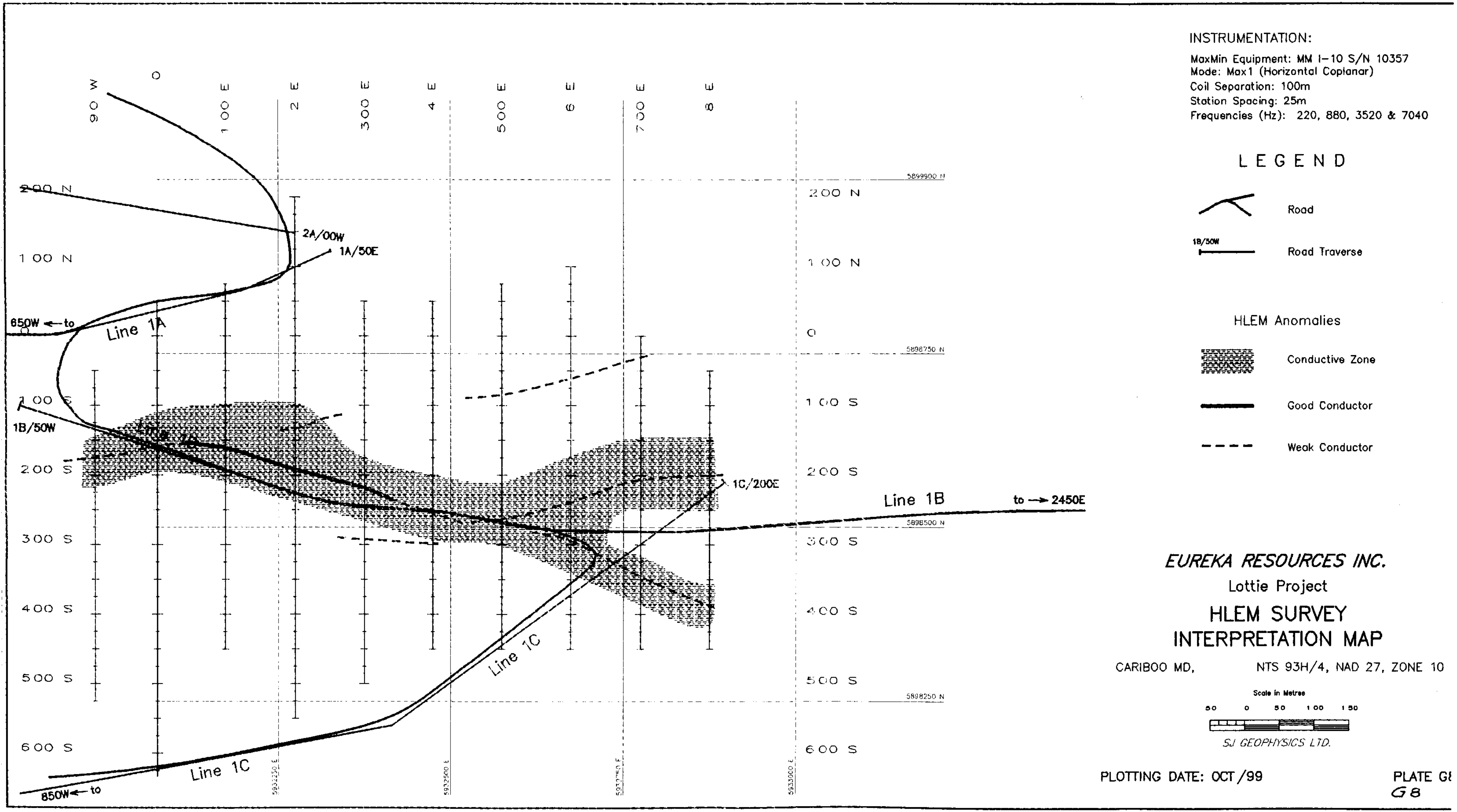
CARIBOO MD, NTS 93H/4, NAD27, ZONE 10



SJ GEOPHYSICS LTD.

PLOTTING DATE: OCT/99

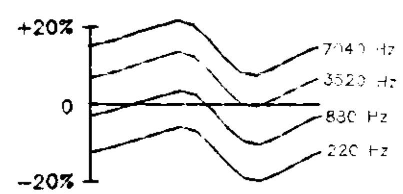
PLATE G7A


INSTRUMENTATION:
MaxMin Equipment: MM I-10 S/N 10357
Mode: Max1 (Horizontal Coplanar)
Coil Separation: 100m
Station Spacing: 25m
Frequencies (Hz): 220, 880, 3520 & 7040
LEGEND
Road
1B/50W
Road Traverse
HLEM Anomalies
Conductive Zone
Good Conductor
Weak Conductor
EUREKA RESOURCES INC.
Lottie Project
HLEM SURVEY
INTERPRETATION MAP
CARIBOO MD,
NTS 93H/4, NAD 27, ZONE 10
Scale in Metres
50 0 50 100 150
SJ GEOPHYSICS LTD.
PLOTTING DATE: OCT/99
PLATE G8
G8
Line 1A
Line 1B
Line 1C
2A/00W
1A/50E
1B/50W
1C/200E
650W ← to
850W ← to
to → 2450E
200 N
100 N
0
100 S
200 S
300 S
400 S
500 S
600 S
90 W
0
100 E
2
300 E
4
500 E
6
700 E
8
5899900 N
5898750 N
5898500 N
5898250 N

Line 1A

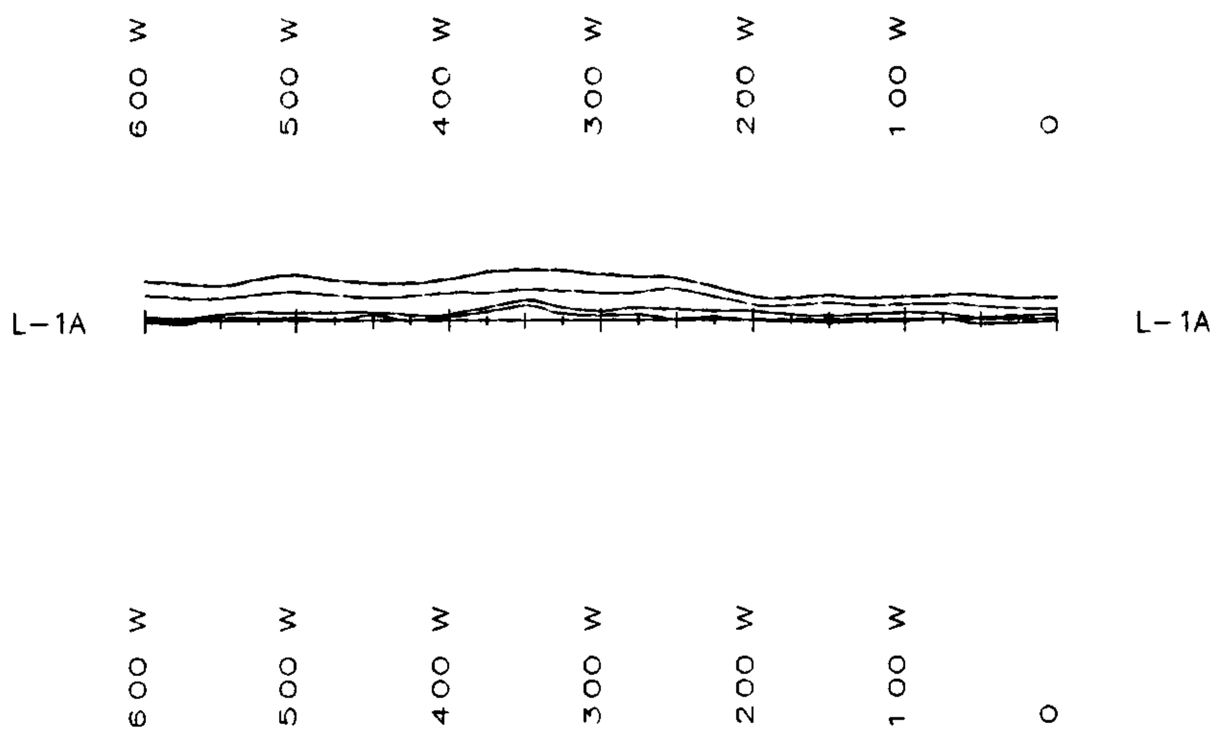
LEGEND

IN-PHASE PROFILES



INSTRUMENTATION:

MaxMin Equipment: MM I-10 S/N 10357
Mode: Max1 (Horizontal Coplanar)
Coil Separation: 100m
Station Spacing: 25m
Frequencies (Hz): 220, 880, 3520 & 7040



EUREKA RESOURCES INC.

Lottie Project

HLEM SURVEY
IN-PHASE PROFILES

CARIBOO MD, NTS 93H/4, NAD27, ZONE 10

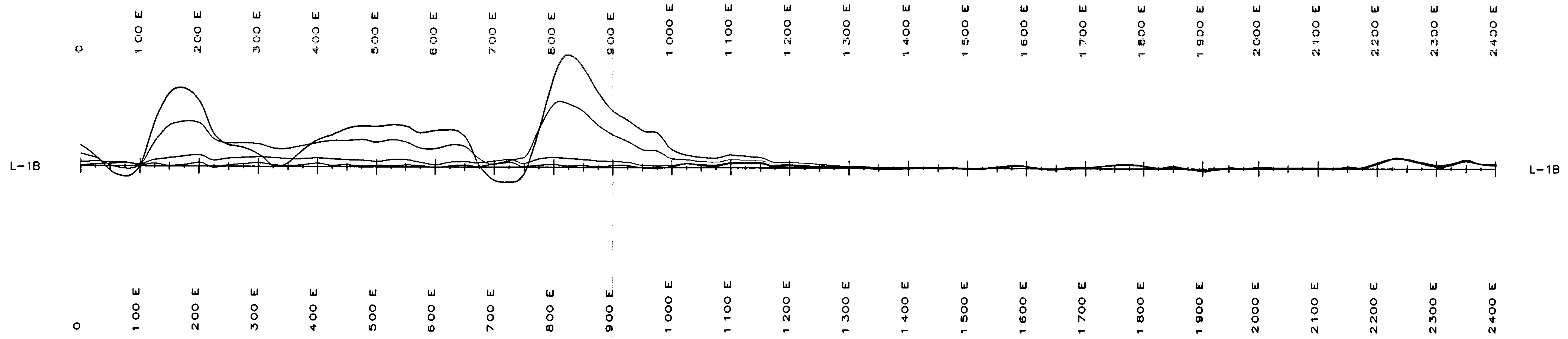
Scale in Metres

50 0 50 100 150

PLOTTING DATE: SEP/99

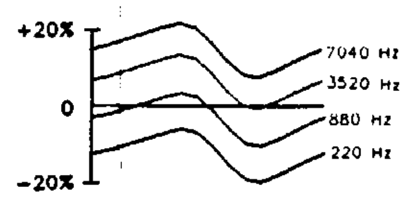
PLATE G2A

Line 1B



LEGEND

IN-PHASE PROFILES



INSTRUMENTATION:

MaxMin Equipment: MM I-10 S/N 10357
Mode: Max1 (Horizontal Coplanar)
Coil Separation: 100m
Station Spacing: 25m
Frequencies (Hz): 220, 880, 3520 & 7040

EUREKA RESOURCES INC.

Lottie Project

HLEM SURVEY
IN-PHASE PROFILES

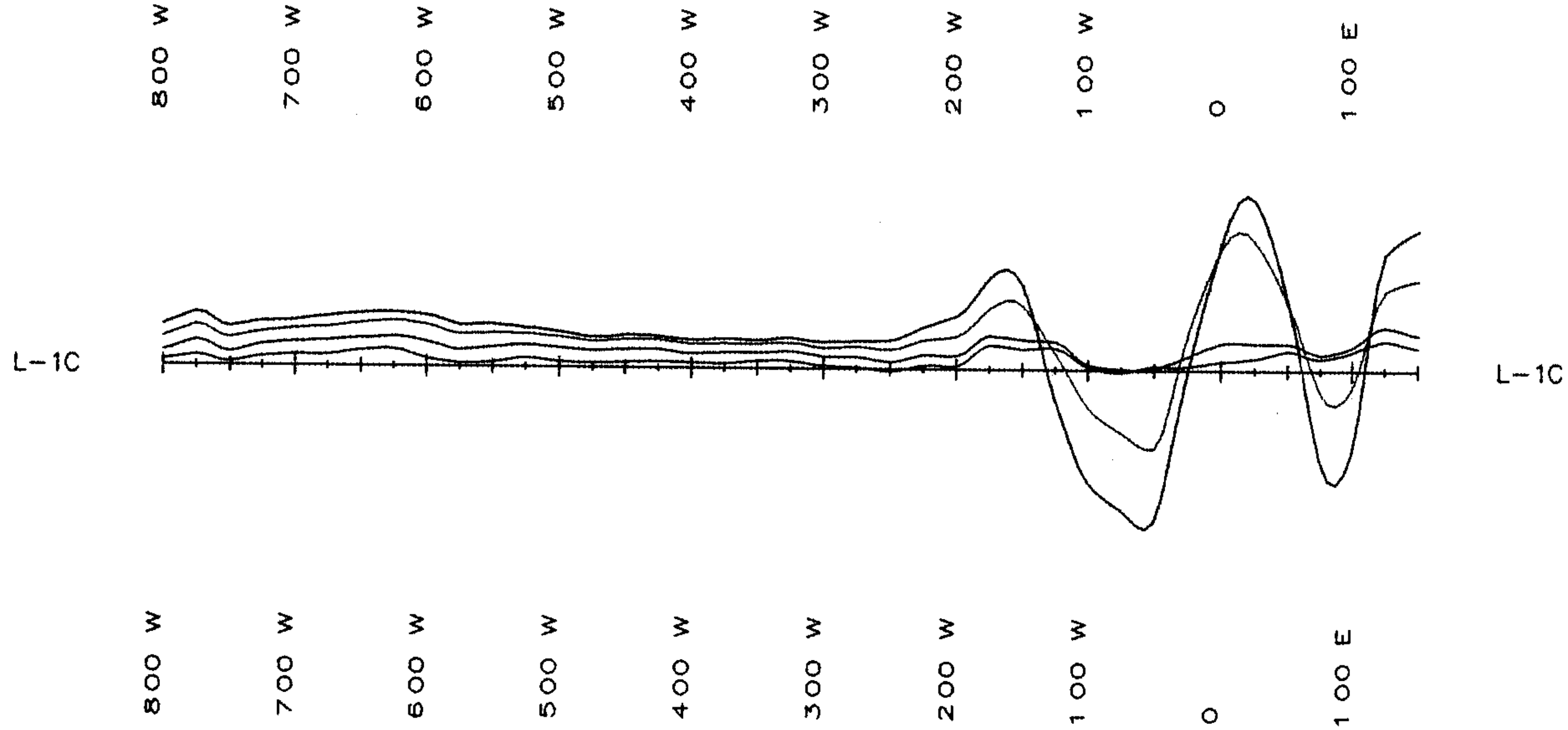
CARIBOO MD, NTS 93H/4, NAD 27, ZONE 10

Scale in Metres

PLOTTING DATE: SEP/99

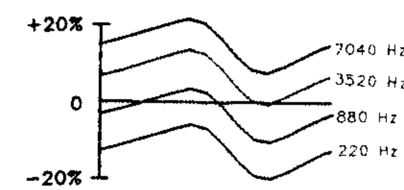
PLATE G3A

Line 1C



LEGEND

IN-PHASE PROFILES



INSTRUMENTATION:

MaxMin Equipment: MM I-10 S/N 10357
Mode: Max1 (Horizontal Coplanar)
Coil Separation: 100m
Station Spacing: 25m
Frequencies (Hz): 220, 880, 3520 & 70

EUREKA RESOURCES INC.

Lottie Project

HLEM SURVEY
IN-PHASE PROFILES

CARIBOO MD, NTS 93H/4, NAD 27, ZONE 10

Scale in Metres

50 0 50 100 150

PLOTTING DATE: SEP/99

PLATE G4A

Appendix D - Laboratory Reports

ITS Intertek Testing Services
Bondar Clegg

Geochemical Lab Report

REPORT: V99-01169.0 (COMPLETE)

REFERENCE:

CLIENT: GEOQUEST CONSULTING LTD.
PROJECT: NONE GIVEN1

SUBMITTED BY: W.G.
DATE RECEIVED: 08-OCT-99 DATE PRINTED: 11-OCT-99

DATE APPROVED	ELEMENT		NUMBER OF ANALYSES	LOWER DETECTION	EXTRACTION	METHOD
991009	1 Ag	Silver	55	0.2 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	2 Cu	Copper	55	1 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	3 Pb	Lead	55	2 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	4 Zn	Zinc	55	1 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	5 Mo	Molybdenum	55	1 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	6 Ni	Nickel	55	1 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	7 Co	Cobalt	55	1 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	8 Cd	Cadmium	55	0.2 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	9 Bi	Bismuth	55	5 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	10 As	Arsenic	55	5 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	11 Sb	Antimony	55	5 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	12 Fe	Iron	55	0.01 PCT	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	13 Mn	Manganese	55	1 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	14 Te	Tellurium	55	10 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	15 Ba	Barium	55	1 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	16 Cr	Chromium	55	1 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	17 V	Vanadium	55	1 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	18 Sn	Tin	55	20 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	19 W	Tungsten	55	20 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	20 La	Lanthanum	55	1 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	21 Al	Aluminum	55	0.01 PCT	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	22 Mg	Magnesium	55	0.01 PCT	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	23 Ca	Calcium	55	0.01 PCT	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	24 Na	Sodium	55	0.01 PCT	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	25 K	Potassium	55	0.01 PCT	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	26 Sr	Strontium	55	1 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	27 Y	Yttrium	55	1 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	28 Ga	Gallium	55	2 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	29 Li	Lithium	55	1 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	30 Nb	Niobium	55	1 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	31 Sc	Scandium	55	5 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	32 Ta	Tantalum	55	10 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	33 Ti	Titanium	55	0.010 PCT	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA
991009	34 Zr	Zirconium	55	1 PPM	HCL:HNO3 (3:1)	INDUC. COUP. PLASMA

SAMPLE TYPES	NUMBER	SIZE FRACTIONS	NUMBER	SAMPLE PREPARATIONS	NUMBER
S SOIL	55	1 -80	55	DRY, SIEVE -80	55

REPORT COPIES TO: MR. JOHN KERR

INVOICE TO: MR. JOHN KERR

Intertek Testing Services

Bondar Clegg

Geochemical Lab Report

CLIENT: GEOQUEST CONSULTING LTD.
REPORT: V99-01169.0 (COMPLETE)

PROJECT: NONE GIVEN1

DATE RECEIVED: 08-OCT-99 DATE PRINTED: 11-OCT-99

SAMPLE NUMBER	ELEMENT UNITS	Ag PPM	Cu PPM	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	Sb PPM	Fe PCT	Mn PPM	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	W PPM	La PPM	Al PCT	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM	Ga PPM	Li PPM	Nb PPM	Sc PPM	Ta PPM	Ti PCT	Zr PPM
L5E B/L		0.3	37	12	69	<1	29	13	0.3	<5	5	<5	3.79	425	<10	187	51	102	<20	<20	14	2.03	0.76	0.71	<.01	0.05	17	6	3	18	7	<5	<10	.170	<1
L5E 0+25S		0.3	27	14	84	<1	24	13	<.2	<5	6	<5	4.03	904	<10	180	47	118	<20	<20	13	1.81	0.69	0.70	0.01	0.08	14	5	3	10	8	<5	<10	.155	<1
L5E 0+50S		0.4	49	40	145	<1	35	14	0.2	<5	18	<5	4.64	694	<10	161	42	85	<20	<20	26	1.81	0.90	0.31	<.01	0.07	11	4	<2	16	6	<5	<10	.060	<1
L5E 0+75S		<.2	14	8	51	<1	16	10	<.2	<5	<5	<5	3.55	334	<10	196	45	129	<20	<20	13	1.79	0.50	0.60	<.01	0.04	9	4	5	7	10	<5	<10	.233	<1
L5E 1+00S		0.3	18	7	66	<1	27	14	<.2	<5	<5	<5	3.88	326	<10	167	51	121	<20	<20	12	2.37	0.75	0.70	0.01	0.03	11	5	3	16	9	<5	<10	.256	<1
L5E 1+25S		0.6	27	7	84	1	29	19	<.2	<5	5	<5	5.73	619	<10	211	84	183	<20	<20	7	1.92	0.86	1.20	<.01	0.05	37	4	4	17	14	<5	<10	.335	<1
L5E 1+50S		0.3	24	12	59	<1	26	14	<.2	<5	6	<5	4.57	434	<10	152	54	134	<20	<20	14	1.96	0.67	0.72	<.01	0.04	20	5	4	16	10	<5	<10	.237	<1
L5E 1+75S		0.2	36	18	89	<1	35	19	<.2	<5	8	<5	4.86	838	<10	174	52	109	<20	<20	18	2.04	1.00	0.68	<.01	0.05	14	6	<2	22	7	<5	<10	.164	<1
L5E 2+00S		<.2	19	12	62	<1	23	11	<.2	<5	<5	<5	3.85	373	<10	213	50	121	<20	<20	16	1.88	0.58	0.70	<.01	0.05	14	5	4	14	9	<5	<10	.198	<1
L5E 2+25S		<.2	13	9	47	<1	17	11	<.2	<5	<5	<5	2.71	726	<10	178	49	101	<20	<20	17	1.89	0.47	0.70	<.01	0.04	13	5	5	9	8	<5	<10	.206	<1
L5E 2+50S		0.3	30	7	72	<1	41	20	0.2	<5	<5	<5	3.26	489	<10	131	53	99	<20	<20	14	2.31	0.98	0.95	0.02	0.04	14	10	<2	14	6	6	<10	.229	<1
L5E		0.3	25	8	65	<1	45	16	0.5	<5	<5	<5	3.71	429	<10	123	63	97	<20	<20	11	2.17	1.05	0.78	0.01	0.03	9	7	<2	19	7	<5	<10	.210	<1
L6E 2+75N		<.2	18	6	84	1	34	17	<.2	<5	<5	<5	4.11	364	<10	201	59	109	<20	<20	13	2.90	0.86	0.64	0.02	0.04	10	6	3	21	7	6	<10	.238	3
L6E 3+00N		0.3	45	8	61	<1	41	21	<.2	<5	<5	<5	4.15	495	<10	222	70	153	<20	<20	11	3.04	0.81	0.89	0.02	0.04	14	16	5	19	10	10	<10	.313	<1
L6E 3+25N		<.2	22	6	87	<1	44	22	<.2	<5	<5	<5	4.28	358	<10	145	61	107	<20	<20	11	3.23	0.89	0.69	0.02	0.04	9	7	3	19	7	6	<10	.253	5
L6E 3+50N		0.2	24	4	53	<1	33	19	0.2	<5	<5	<5	3.37	363	<10	123	53	121	<20	<20	8	2.68	0.79	0.92	0.02	0.03	11	8	3	11	8	6	<10	.345	<1
L6E 4+75N		<.2	97	4	74	<1	53	31	<.2	<5	<5	<5	4.57	1266	<10	150	77	176	<20	<20	12	3.31	1.30	1.67	0.03	0.04	25	45	3	16	11	22	<10	.294	<1
L6E 6+00N		<.2	25	4	70	<1	45	22	<.2	<5	<5	<5	4.96	371	<10	175	62	124	<20	<20	9	3.24	0.91	0.91	0.02	0.03	12	8	2	20	8	6	<10	.284	4
L6E 6+25N		0.2	18	4	71	<1	32	19	<.2	<5	<5	<5	4.79	297	<10	118	57	138	<20	<20	8	2.94	0.64	0.73	0.01	0.03	11	6	4	15	10	5	<10	.324	2
L6E 6+50N		<.2	20	4	62	<1	27	17	<.2	<5	<5	<5	5.49	339	<10	98	59	154	<20	<20	11	2.59	0.73	0.80	0.02	0.03	13	8	4	18	10	5	<10	.338	<1
L6E 6+75N		0.2	27	3	54	<1	32	22	<.2	<5	<5	<5	4.14	487	<10	121	51	141	<20	<20	6	2.89	0.86	1.31	0.02	0.03	13	9	3	11	9	6	<10	.373	4
L6E 7+00N		<.2	16	5	75	<1	24	16	<.2	<5	<5	<5	4.67	360	<10	100	54	141	<20	<20	9	2.56	0.65	0.76	0.01	0.03	11	6	4	16	10	<5	<10	.319	<1
L6E 7+25N		<.2	36	<2	69	<1	36	27	<.2	<5	<5	<5	5.03	582	<10	94	49	152	<20	<20	6	2.93	1.00	1.33	0.02	0.02	17	10	3	11	10	7	<10	.396	2
L6E 7+50N		0.5	26	4	72	1	17	19	<.2	<5	<5	<5	5.86	593	<10	190	61	243	<20	<20	5	1.98	0.48	0.95	0.01	0.04	16	10	7	7	19	6	<10	.528	<1
L6E 7+75N		<.2	40	3	67	<1	31	27	<.2	<5	<5	<5	6.04	831	<10	93	73	231	<20	<20	6	2.68	0.98	1.81	0.02	0.03	26	16	5	15	16	8	<10	.394	<1
L6E 8+00N		<.2	54	3	60	<1	45	27	<.2	<5	<5	<5	3.86	945	<10	83	57	141	<20	<20	8	2.63	1.14	1.92	0.02	0.04	21	21	<2	12	9	8	<10	.334	<1
L6E 8+25N		<.2	23	3	67	<1	33	23	<.2	<5	<5	<5	5.58	389	<10	90	63	171	<20	<20	7	2.96	0.84	1.08	0.02	0.02	15	9	4	18	11	6	<10	.404	3
L6E 8+50N		0.4	38	3	58	<1	43	27	<.2	<5	<5	<5	4.53	469	<10	99	59	142	<20	<20	6	2.97	1.06	1.33	0.03	0.03	14	9	3	12	9	6	<10	.363	7
L6E 8+75N		0.3	14	4	59	<1	21	16	<.2	<5	<5	<5	5.67	287	<10	135	61	179	<20	<20	8	2.51	0.53	0.81	0.01	0.03	12	6	5	15	13	<5	<10	.392	<1
L6E 9+00N		<.2	18	3	65	<1	29	23	<.2	<5	<5	<5	5.54	358	<10	92	66	185	<20	<20	6	2.90	0.68	1.00	0.02	0.03	13	7	6	15	13	6	<10	.454	3

Intertek Testing Services

Bondar Clegg

Geochemical Lab Report

CLIENT: GEOQUEST CONSULTING LTD.

PROJECT: NONE GIVEN1

REPORT: V99-01169.0 (COMPLETE)

DATE RECEIVED: 08-OCT-99   DATE PRINTED: 11-OCT-99

SAMPLE NUMBER	ELEMENT UNITS	Ag PPM	Cu PPM	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	Sb PPM	Fe PCT	Mn PPM	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	W PPM	La PPM	Al PCT	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM	Ga PPM	Li PPM	Nb PPM	Sc PPM	Ta PPM	Ti PCT	Zr PPM
L6E 9+25N		0.2	46	3	66	<1	46	24	0.3	<5	<5	<5	4.71	438	<10	139	61	143	<20	<20	6	2.90	0.96	1.14	0.02	0.03	13	9	3	13	10	7	<10	.345	5
L6E 9+50N		<.2	15	5	47	<1	18	15	<.2	<5	<5	<5	4.23	294	<10	131	49	169	<20	<20	7	2.07	0.44	0.96	0.01	0.04	14	5	6	7	13	<5	<10	.404	<1
L7E B/L		0.2	20	13	78	<1	28	13	<.2	<5	8	<5	5.66	380	<10	174	57	130	<20	<20	17	2.37	0.76	0.48	<.01	0.05	10	4	3	18	9	<5	<10	.185	<1
L7E 0+25S		<.2	19	11	89	<1	23	10	<.2	<5	5	<5	4.00	362	<10	131	52	97	<20	<20	17	2.26	0.65	0.41	<.01	0.04	9	4	4	19	7	<5	<10	.140	<1
L7E 0+50S		<.2	25	12	87	<1	32	15	<.2	<5	7	<5	4.91	535	<10	154	62	124	<20	<20	18	2.34	0.84	0.46	0.01	0.05	10	5	3	18	9	<5	<10	.184	<1
L7E 0+75S		0.3	21	10	56	<1	19	10	<.2	<5	<5	<5	3.01	311	<10	165	48	109	<20	<20	16	1.82	0.50	0.51	<.01	0.05	10	4	5	11	9	<5	<10	.234	<1
L7E 1+00S		<.2	82	11	111	<1	93	25	0.4	<5	8	<5	3.57	793	<10	138	76	80	<20	<20	32	2.09	1.15	0.95	0.01	0.05	23	31	<2	23	5	11	<10	.152	<1
L7E 1+50S		0.2	27	16	68	<1	31	12	0.2	<5	8	<5	4.33	429	<10	117	61	103	<20	<20	12	1.54	0.53	0.30	<.01	0.03	7	4	3	8	8	<5	<10	.118	<1
L7E 1+75S		0.3	84	23	166	1	112	36	0.5	<5	13	<5	4.43	694	<10	119	75	67	<20	<20	23	2.30	1.12	0.58	<.01	0.04	17	17	<2	22	4	6	<10	.098	<1
L7E 2+00S		0.3	64	31	139	2	50	17	0.7	<5	12	<5	4.24	617	<10	107	70	87	<20	<20	15	1.77	0.84	0.52	<.01	0.04	11	5	<2	15	6	<5	<10	.098	<1
L7E 2+25S		0.3	146	18	171	<1	87	27	0.8	<5	10	<5	4.13	554	<10	109	69	74	<20	<20	18	2.18	1.11	0.62	<.01	0.03	13	13	<2	28	5	<5	<10	.139	<1
L7E 3+00S		0.3	98	5	68	<1	203	32	0.3	<5	6	<5	4.09	577	<10	58	156	84	<20	<20	13	2.49	2.16	0.52	<.01	0.02	12	11	<2	28	5	<5	<10	.122	<1
L7E 2+75S		<.2	60	10	93	<1	100	31	0.2	<5	9	<5	4.46	795	<10	95	100	91	<20	<20	20	2.17	1.56	0.80	<.01	0.04	16	17	<2	28	6	6	<10	.134	<1
L9E 0+50S		<.2	115	21	116	1	71	25	0.3	<5	10	<5	3.98	1508	<10	151	87	88	<20	<20	38	2.35	1.15	1.09	<.01	0.05	26	38	<2	19	5	11	<10	.057	<1
L9E 0+75S		0.3	44	7	97	1	46	19	<.2	<5	7	<5	4.91	524	<10	113	75	117	<20	<20	15	1.98	1.11	1.24	<.01	0.03	20	12	<2	22	8	5	<10	.199	<1
L9E 1+00S		0.3	54	14	103	1	45	22	0.3	<5	8	<5	4.55	843	<10	121	66	108	<20	<20	15	2.10	0.85	0.99	<.01	0.03	18	10	2	19	7	<5	<10	.156	<1
L9E 1+25S		<.2	87	21	94	1	48	18	0.3	<5	11	<5	4.12	765	<10	129	65	84	<20	<20	26	1.79	0.75	1.00	<.01	0.04	19	18	<2	16	6	5	<10	.074	<1
L9E 1+50S		<.2	34	21	105	1	37	15	0.3	<5	12	<5	4.86	546	<10	106	59	74	<20	<20	15	1.52	0.67	0.56	<.01	0.04	16	5	<2	17	5	<5	<10	.088	<1
L9E 1+75S		<.2	54	23	78	<1	56	19	<.2	<5	11	<5	4.15	808	<10	102	71	69	<20	<20	21	1.74	0.83	0.69	<.01	0.04	15	7	<2	14	5	<5	<10	.067	<1
L9E 2+00S		<.2	71	19	98	<1	166	51	<.2	<5	24	<5	4.19	948	<10	89	143	81	<20	<20	15	2.15	2.13	0.38	<.01	0.03	9	11	<2	23	5	<5	<10	.105	<1
L9E 2+25S		<.2	83	27	131	<1	120	39	0.3	<5	15	<5	4.30	1159	<10	133	125	86	<20	<20	27	2.31	1.89	0.65	<.01	0.06	15	23	<2	23	5	9	<10	.073	<1
L9E 2+50S		<.2	54	21	98	<1	97	31	<.2	<5	15	<5	4.08	790	<10	101	99	75	<20	<20	26	2.10	1.73	0.66	<.01	0.06	14	14	<2	21	4	6	<10	.094	<1
L9E 2+75S		<.2	71	18	112	<1	64	24	0.3	<5	8	<5	4.35	731	<10	120	84	86	<20	<20	22	2.06	1.24	0.83	<.01	0.05	17	16	<2	23	6	6	<10	.094	<1
L9E 3+25S		<.2	53	46	131	1	46	22	0.2	<5	9	<5	4.53	453	<10	127	60	94	<20	<20	23	2.54	0.90	0.80	0.01	0.05	15	13	2	23	6	6	<10	.112	<1
L9E 3+50S		<.2	107	8	91	<1	47	29	0.3	<5	<5	<5	3.90	1680	<10	180	68	131	<20	<20	14	2.51	1.04	1.50	0.01	0.05	22	29	3	15	9	14	<10	.166	<1

ITS **Intertek Testing Services**
Bondar Clegg

Geochemical Lab Report

CLIENT: GEOQUEST CONSULTING LTD.
REPORT: V99-01170.0 (COMPLETE)

PROJECT: NONE GIVEN1
DATE RECEIVED: 07-OCT-99 DATE PRINTED: 11-OCT-99

SAMPLE NUMBER	ELEMENT UNITS	Ag PPM	Cu PPM	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	Sb PPM	Fe PCT	Mn PPM	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM
TR-5E		<0.2	53	19	131	4	39	11	1.0	<5	13	<5	3.09	1022	<10	55	75	50	<20
TR-6A		<0.2	36	40	51	2	16	6	0.4	<5	<5	<5	2.42	242	<10	65	174	8	<20
TR-7E		<0.2	48	23	64	3	30	12	0.4	<5	13	<5	2.26	266	<10	127	46	24	<20
L6E 5+75N		<0.2	36	3	71	<1	50	31	0.3	<5	<5	<5	3.90	922	<10	97	61	149	<20
L7E 2+15N		0.5	728	24	168	2	38	11	0.7	<5	<5	<5	3.73	558	<10	71	78	57	<20
WR-14		11.5	9977	1441	2144	2	19	89	6.4	13	75	<5	4.50	202	<10	43	182	10	<20
WR-15		<0.2	191	16	67	<1	11	17	<.2	<5	<5	<5	4.45	357	<10	27	107	12	<20
WR-17		0.7	48	89	56	3	118	52	0.4	7	105	16	>10.00	133	<10	5	94	35	<20

SAMPLE NUMBER	W PPM	La PPM	Al PCT	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM	Ga PPM	Li PPM	Nb PPM	Sc PPM	Ta PPM	Ti PCT	Zr PPM
TR-5E	<20	5	1.15	0.84	6.52	<.01	0.18	170	12	<2	15	3	<5	<10	<.01	9
TR-6A	<20	9	0.90	0.35	0.26	0.02	0.22	9	3	<2	6	<1	<5	<10	<.01	4
TR-7E	<20	20	1.06	0.44	0.29	<.01	0.35	13	13	<2	7	2	<5	<10	.060	18
L6E 5+75N	<20	3	2.47	1.81	2.36	0.06	0.05	16	16	<2	9	8	8	<10	.423	12
L7E 2+15N	<20	11	1.65	1.15	0.39	<.01	0.17	18	7	<2	17	3	<5	<10	.066	8
WR-14	<20	8	0.98	0.37	0.04	0.01	0.19	2	2	<2	7	<1	<5	<10	<.01	4
WR-15	<20	13	1.45	0.58	0.09	<.01	0.15	2	3	<2	13	<1	<5	<10	<.01	4
WR-17	<20	10	0.71	0.23	0.20	<.01	0.22	6	6	<2	3	2	<5	<10	.054	11

ITS Intertek Testing Services
Bondar Clegg

Geochemical Lab Report

CLIENT: EUREKA RESOURCES, INC.
REPORT: V99-01022.0 (COMPLETE)

PROJECT: NONE GIVEN
DATE RECEIVED: 09-SEP-99 DATE PRINTED: 16-SEP-99

SAMPLE NUMBER	ELEMENT / UNITS	Ag PPM	Cu PPM	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	Sb PPM	Fe PCT	Mn PPM	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	W PPM	La PPM	Al PCT	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM	Ga PPM	Li PPM	Nb PPM	Sc PPM	Ta PPM	Ti PCT	Zr PPM
RTB 1+50		<.2	19	8	72	1	33	16	0.3	<5	<5	<5	3.90	591	<10	154	58	83	<20	<20	15	2.02	0.83	0.90	0.02	0.06	16	8	<2	15	6	<5	<10	0.24	1
RTB 3+00		<.2	24	8	72	1	35	13	<.2	<5	5	<5	3.99	456	<10	200	55	87	<20	<20	16	2.46	0.81	0.75	0.02	0.10	14	7	3	17	7	<5	<10	0.22	3
RTB 3+50		<.2	35	9	80	1	38	15	<.2	<5	6	<5	4.50	436	<10	215	60	90	<20	<20	17	2.65	0.80	0.61	0.02	0.07	13	8	3	18	7	6	<10	0.21	4
RTB 3+70		<.2	19	8	96	2	36	16	0.3	<5	6	<5	3.88	391	<10	172	60	82	<20	<20	19	2.72	0.80	0.64	0.03	0.08	15	8	3	17	6	<5	<10	0.21	3
RTB 4+00		<.2	29	6	66	1	40	18	<.2	<5	6	<5	5.17	603	<10	133	66	125	<20	<20	10	3.25	1.34	1.32	0.03	0.05	18	13	4	17	9	7	<10	0.37	4
RTB 4+50		<.2	18	7	61	1	29	9	0.3	<5	<5	<5	4.15	293	<10	160	52	81	<20	<20	17	2.55	0.72	0.67	0.02	0.06	13	7	2	18	7	<5	<10	0.21	1
RTB 5+00		<.2	35	6	56	2	48	15	0.3	<5	11	<5	4.65	448	<10	180	76	90	<20	<20	13	2.47	1.00	0.81	0.02	0.04	14	11	3	21	7	7	<10	0.22	<1
RTB 5+50		<.2	96	11	87	2	61	16	0.3	<5	12	<5	4.29	684	<10	259	91	82	<20	<20	24	2.61	0.83	0.82	0.02	0.06	24	32	3	23	6	18	<10	0.11	<1
RTB 6+00		<.2	103	11	81	2	53	24	0.4	<5	10	<5	4.46	991	<10	296	91	91	<20	<20	49	2.57	0.94	0.84	0.02	0.06	24	52	2	21	7	17	<10	0.12	<1
RTB 7+00		<.2	133	11	117	2	66	19	0.3	<5	11	<5	4.05	582	<10	227	89	78	<20	<20	23	2.81	0.82	0.57	0.01	0.06	18	19	3	25	6	11	<10	0.13	<1
RTB 8+50		<.2	18	9	96	2	32	12	<.2	<5	5	<5	4.39	304	<10	183	51	72	<20	<20	17	2.27	0.67	0.44	0.02	0.05	14	5	<2	20	5	<5	<10	0.14	1
RTB 9+50		<.2	24	5	61	2	35	13	0.3	<5	6	<5	5.23	479	<10	161	66	118	<20	<20	10	2.60	1.03	1.10	0.02	0.05	17	10	3	16	9	5	<10	0.31	<1
RTB 10+00		<.2	30	15	85	1	52	14	0.2	<5	8	<5	5.32	444	<10	145	77	94	<20	<20	15	2.65	1.14	0.76	0.02	0.07	13	9	<2	20	7	<5	<10	0.21	2
RTB 10+50		<.2	21	7	68	1	50	16	<.2	<5	<5	<5	3.96	405	<10	192	74	85	<20	<20	13	2.55	1.17	0.89	0.02	0.04	15	8	2	17	6	<5	<10	0.24	2
RTB 11+00		<.2	41	12	100	1	88	28	0.4	<5	10	<5	5.20	1305	<10	142	138	90	<20	<20	13	2.99	1.70	0.43	0.01	0.05	11	7	3	23	6	<5	<10	0.19	<1
RTB 11+50		<.2	71	5	56	2	138	26	<.2	<5	12	<5	5.63	540	<10	116	143	99	<20	<20	10	2.78	1.93	0.99	0.02	0.04	23	10	<2	29	7	<5	<10	0.22	<1
RTB 13+00		<.2	31	3	67	1	46	17	<.2	<5	6	<5	4.84	427	<10	197	74	106	<20	<20	11	3.10	1.23	0.91	0.02	0.05	14	12	3	21	8	7	<10	0.26	2
RTB 13+50		<.2	25	4	69	1	48	16	0.2	<5	5	<5	4.80	396	<10	205	79	105	<20	<20	11	3.10	1.18	0.95	0.02	0.04	16	8	3	22	8	6	<10	0.28	3
RTB 14+50		<.2	44	5	50	1	51	19	0.2	<5	<5	<5	4.63	617	<10	201	76	112	<20	<20	17	2.75	1.38	1.23	0.03	0.05	20	16	4	17	8	7	<10	0.31	2
RTB 15+50		<.2	72	8	72	1	40	20	0.2	<5	6	<5	4.52	896	<10	358	88	125	<20	<20	46	2.88	1.03	1.02	0.02	0.05	24	28	5	19	9	11	<10	0.21	<1
RTB 16+00		<.2	28	5	61	1	40	15	0.2	<5	5	<5	4.80	505	<10	120	72	110	<20	<20	12	2.71	1.16	1.06	0.02	0.06	15	10	3	17	8	6	<10	0.31	3
RTB 16+50		<.2	17	5	68	1	27	9	0.3	<5	<5	<5	4.50	300	<10	192	64	111	<20	<20	11	2.68	0.78	0.76	0.02	0.03	13	7	4	18	9	<5	<10	0.29	<1
RTB 17+50		<.2	24	5	84	1	48	15	0.2	<5	5	<5	5.18	470	<10	177	103	125	<20	<20	10	3.15	1.37	1.03	0.02	0.04	18	7	4	26	9	6	<10	0.27	<1
RTB 18+00		<.2	72	9	81	1	44	16	0.3	<5	7	<5	4.57	882	<10	305	89	112	<20	<20	38	2.53	0.94	1.14	0.02	0.06	25	34	4	19	9	13	<10	0.21	<1
SRTB 0+00		<.2	100	26	106	2	89	26	0.4	<5	18	<5	5.00	735	<10	146	94	66	<20	<20	22	2.63	1.58	0.51	0.01	0.12	18	11	<2	19	5	<5	<10	0.12	6
SRTB 0+50		<.2	48	14	117	2	64	25	0.3	<5	8	<5	4.84	880	<10	115	97	76	<20	<20	17	2.15	1.05	0.74	0.01	0.05	25	11	2	25	5	<5	<10	0.12	<1
SRTB 1+50		<.2	25	7	69	1	82	16	0.3	<5	9	<5	5.17	381	<10	131	146	84	<20	<20	11	2.43	1.60	0.48	0.01	0.03	11	5	<2	29	6	<5	<10	0.16	<1
SRTB 3+00		<.2	21	18	101	1	37	11	0.4	<5	8	<5	4.68	298	<10	118	63	63	<20	<20	22	2.15	0.89	0.43	0.01	0.05	9	7	<2	24	4	<5	<10	0.10	1
SRTB 3+50		<.2	61	42	105	1	40	16	0.2	<5	6	<5	4.17	611	<10	152	63	96	<20	<20	21	2.62	1.00	0.99	0.02	0.06	22	19	3	17	7	9	<10	0.16	<1
SRTB 4+00		<.2	29	6	63	1	38	18	0.3	<5	5	<5	4.89	535	<10	126	67	113	<20	<20	9	3.01	1.17	1.08	0.02	0.04	16	13	3	16	8	7	<10	0.32	3

Intertek Testing Services

Bondar Clegg

Geochemical Lab Report

CLIENT: EUREKA RESOURCES, INC.
REPORT: V99-01022.0 (COMPLETE)

PROJECT: NONE GIVEN

DATE RECEIVED: 09-SEP-99 DATE PRINTED: 16-SEP-99

SAMPLE NUMBER	ELEMENT	Ag	Cu	Pb	Zn	Mo	Ni	Co	Cd	Bi	As	Sb	Fe	Mn	Te	Ba	Cr	V	Sn	W	La	Al	Mg	Ca	Na	K	Sr	Y	Ga	Li	Nb	Sc	Ta	Ti	Zr
	UNITS	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PCT	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PCT	PCT	PCT	PCT	PCT	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PCT	PPM
SRTB 4+50		<.2	38	4	71	2	44	24	0.2	<5	<5	<5	5.75	772	<10	158	75	156	<20	<20	7	3.57	1.59	1.36	0.03	0.04	34	14	4	20	11	10	<10	0.40	3
SRTB 5+00		<.2	26	3	59	1	39	16	<.2	<5	<5	<5	4.45	475	<10	191	62	115	<20	<20	8	3.21	1.19	1.28	0.03	0.04	20	11	3	15	9	7	<10	0.35	4
SRTB 5+50		<.2	21	3	58	1	31	12	0.3	<5	<5	<5	4.88	403	<10	138	65	124	<20	<20	9	2.80	0.88	0.84	0.02	0.03	18	9	4	16	10	6	<10	0.31	1
SRTB 6+00		<.2	27	4	49	1	36	15	<.2	<5	<5	<5	4.42	444	<10	145	61	108	<20	<20	9	2.82	1.06	1.10	0.03	0.03	17	10	3	14	8	6	<10	0.30	3
SRTB 6+50		<.2	20	5	64	2	33	14	<.2	<5	<5	<5	5.12	480	<10	134	71	122	<20	<20	9	2.99	0.94	0.78	0.02	0.03	14	8	4	17	9	6	<10	0.32	2
SRTB 7+00		<.2	37	6	57	1	45	21	<.2	<5	<5	<5	4.60	490	<10	124	69	109	<20	<20	9	3.61	1.20	1.13	0.03	0.04	19	12	3	14	8	7	<10	0.32	4
SRTB 7+50		<.2	51	3	61	2	51	21	<.2	<5	<5	<5	5.05	500	<10	149	84	109	<20	<20	8	4.19	1.22	1.00	0.02	0.03	13	11	3	15	8	7	<10	0.28	3
SRTB 8+00		<.2	41	4	59	2	56	24	0.2	<5	<5	<5	5.32	530	<10	182	76	112	<20	<20	9	3.50	1.44	1.03	0.03	0.04	17	10	3	16	8	7	<10	0.27	3
SRTB 8+50		<.2	21	4	72	2	32	14	0.2	<5	<5	<5	5.58	413	<10	136	68	114	<20	<20	7	3.29	0.92	0.84	0.02	0.03	11	8	2	16	9	6	<10	0.30	3
SRTB 9+00		<.2	41	5	62	1	46	21	0.2	<5	5	<5	5.02	614	<10	135	74	111	<20	<20	10	2.93	1.33	1.17	0.03	0.04	21	12	3	17	9	6	<10	0.30	2
SRTB 9+50		<.2	53	<2	74	2	46	31	<.2	<5	<5	<5	6.51	719	<10	169	75	152	<20	<20	5	3.68	2.05	1.20	0.02	0.03	17	11	3	17	11	8	<10	0.41	2
SRTB 10+00		0.2	85	4	59	1	50	31	0.2	<5	5	<5	5.80	823	<10	154	69	140	<20	<20	6	3.74	1.81	1.24	0.02	0.03	16	14	3	13	10	8	<10	0.41	6
SRTB 10+50		<.2	65	6	67	2	32	16	0.2	<5	<5	<5	5.48	597	<10	141	75	150	<20	<20	12	3.01	0.98	0.79	0.02	0.03	17	14	5	14	11	8	<10	0.33	<1
SRTB 11+00		<.2	24	6	75	2	32	13	0.3	<5	5	<5	5.51	422	<10	107	67	123	<20	<20	11	2.72	0.92	0.70	0.02	0.04	12	8	3	16	9	6	<10	0.28	2
SRTB 11+50		<.2	46	5	68	1	58	25	<.2	<5	5	<5	5.47	647	<10	154	82	119	<20	<20	12	3.57	1.51	0.99	0.03	0.06	16	14	4	19	8	8	<10	0.28	3
SRTB 12+00		<.2	46	3	64	1	47	24	<.2	<5	<5	<5	5.21	632	<10	179	71	120	<20	<20	7	3.56	1.41	1.17	0.03	0.04	14	12	4	13	9	7	<10	0.32	<1
SRTB 12+50		<.2	77	6	57	2	43	24	0.3	<5	7	<5	5.64	780	<10	103	63	143	<20	<20	8	3.57	1.40	1.59	0.02	0.02	17	21	3	15	11	8	<10	0.38	2
SRTB 13+00		<.2	49	3	57	2	50	30	<.2	<5	<5	<5	6.78	713	<10	78	82	155	<20	<20	5	4.56	2.07	1.82	0.02	0.03	10	16	5	17	11	12	<10	0.38	<1
SRTB 13+50		<.2	35	3	67	2	43	22	<.2	<5	<5	<5	5.06	514	<10	157	59	128	<20	<20	7	3.45	1.30	1.28	0.02	0.04	13	11	4	13	9	7	<10	0.34	2
SRTB 14+00		<.2	30	4	67	2	36	17	<.2	<5	<5	<5	5.43	483	<10	138	58	128	<20	<20	7	3.55	1.14	1.10	0.02	0.03	13	10	4	15	9	7	<10	0.31	<1
SRTB 15+00		0.2	30	3	58	1	37	18	0.2	<5	<5	<5	4.60	494	<10	122	57	115	<20	<20	6	3.72	1.16	1.15	0.02	0.03	12	10	3	12	9	6	<10	0.32	2
SRTB 15+50		0.2	29	3	68	2	39	18	0.2	<5	5	<5	5.71	467	<10	137	68	133	<20	<20	7	3.74	1.16	0.87	0.02	0.03	11	11	4	17	11	7	<10	0.37	4
SRTB 16+00		<.2	25	3	93	2	37	16	0.2	<5	<5	<5	5.51	455	<10	145	61	124	<20	<20	7	3.39	1.09	0.94	0.02	0.03	12	8	4	18	9	6	<10	0.29	1
SRTB 16+50		<.2	23	4	79	2	28	12	0.2	<5	<5	<5	4.92	344	<10	88	55	98	<20	<20	7	3.42	0.86	0.77	0.01	0.02	12	7	2	15	7	6	<10	0.23	2
L-1C 0+25E		<.2	32	8	80	2	50	15	0.3	<5	6	<5	4.35	706	<10	109	83	88	<20	<20	11	1.74	0.95	0.98	0.01	0.04	21	7	2	16	7	<5	<10	0.15	<1
L-1C 0+50E		<.2	39	10	87	2	45	17	0.5	<5	19	<5	4.42	505	<10	62	70	75	<20	<20	16	2.00	0.87	0.67	<.01	0.04	17	6	<2	17	6	<5	<10	0.13	<1
L-1C 0+75E		<.2	87	95	213	4	50	15	0.6	<5	25	<5	6.47	423	<10	185	59	47	<20	<20	20	2.21	0.94	0.27	0.01	0.09	31	6	<2	23	4	<5	<10	0.07	1
L-1C 1+00E		<.2	32	26	105	2	29	11	0.3	<5	15	<5	5.07	452	<10	127	42	63	<20	<20	21	2.12	0.61	0.37	<.01	0.06	14	5	<2	12	5	<5	<10	0.05	<1
L-1C 1+25E		<.2	40	19	86	2	36	13	0.7	<5	8	<5	3.75	505	<10	67	64	53	<20	<20	27	1.86	0.66	0.27	<.01	0.05	9	10	2	14	4	<5	<10	0.07	<1
L-1C 1+50E		0.2	82	18	151	1	93	18	1.2	<5	7	<5	3.47	1090	<10	129	90	49	<20	<20	23	1.92	1.09	1.31	0.01	0.05	38	19	<2	21	3	<5	<10	0.08	<1

Intertek Testing Services
Bondar Clegg

Geochemical Lab Report

CLIENT: EUREKA RESOURCES, INC.
REPORT: V99-01022.0 (COMPLETE)

PROJECT: NONE GIVEN

DATE RECEIVED: 09-SEP-99   DATE PRINTED: 16-SEP-99

SAMPLE NUMBER	ELEMENT UNITS	Ag PPM	Cu PPM	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	Sb PPM	Fe PCT	Mn PPM	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	W PPM	La PPM	Al PCT	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM	Ga PPM	Li PPM	Nb PPM	Sc PPM	Ta PPM	Ti PCT	Zr PPM
L-1C 1+75E		0.2	26	26	106	3	39	12	0.6	<5	13	<5	6.75	292	<10	99	79	73	<20	<20	18	2.54	0.85	0.27	<.01	0.04	9	4	<2	27	7	<5	<10	0.13	2
L-1C 2+00E		<.2	27	23	109	2	42	18	0.5	<5	21	<5	6.15	735	<10	135	59	77	<20	<20	24	1.85	0.93	0.46	<.01	0.05	15	7	<2	13	6	<5	<10	0.12	<1
L-6E 0+25S		<.2	18	7	67	2	22	9	0.3	<5	6	<5	5.06	279	<10	173	52	94	<20	<20	11	2.17	0.63	0.37	0.01	0.03	10	4	2	18	8	<5	<10	0.21	<1
L-6E 0+50S		<.2	35	12	85	1	45	14	0.2	<5	8	<5	4.66	477	<10	166	62	86	<20	<20	16	2.43	1.08	0.60	0.02	0.04	13	6	2	21	6	<5	<10	0.18	2
L-6E 0+75S		0.4	24	9	78	1	29	12	0.2	<5	7	<5	6.07	589	<10	217	83	125	<20	<20	9	2.51	0.98	0.46	0.01	0.03	11	5	3	23	10	<5	<10	0.21	<1
L-6E 1+00S		0.4	13	10	59	2	24	9	<.2	<5	7	<5	5.31	386	<10	128	60	125	<20	<20	10	1.93	0.67	0.44	<.01	0.04	9	3	3	14	10	<5	<10	0.19	<1
L-6E 1+25S		<.2	16	9	81	2	29	11	0.3	<5	5	<5	4.91	376	<10	157	60	99	<20	<20	11	2.13	0.77	0.56	0.01	0.04	10	5	3	20	8	<5	<10	0.19	<1
L-6E 1+50S		<.2	15	7	61	2	23	9	0.4	<5	<5	<5	5.07	577	<10	164	65	133	<20	<20	9	2.13	0.64	0.52	<.01	0.03	10	4	4	13	10	<5	<10	0.23	<1
L-6E 1+75S		<.2	18	7	59	1	32	11	0.4	<5	6	<5	4.30	312	<10	153	61	90	<20	<20	10	2.29	0.87	0.67	0.01	0.03	10	6	<2	18	8	<5	<10	0.23	<1
L-6E 2+00S		<.2	11	11	36	1	14	5	<.2	<5	<5	<5	2.34	246	<10	150	40	96	<20	<20	14	1.40	0.35	0.59	0.01	0.04	13	4	5	7	8	<5	<10	0.20	<1
L-6E 2+25S		<.2	13	8	71	1	27	9	0.3	<5	<5	<5	4.03	295	<10	122	57	90	<20	<20	11	2.51	0.74	0.57	0.01	0.03	10	5	3	17	7	<5	<10	0.21	<1
L-6E 2+50S		0.3	12	9	56	<1	24	8	0.3	<5	<5	<5	3.98	376	<10	115	57	107	<20	<20	11	2.14	0.66	0.57	0.01	0.04	10	4	4	13	9	<5	<10	0.22	<1
L-6E 3+00S		<.2	13	11	58	2	25	9	0.2	<5	6	<5	4.50	537	<10	227	59	121	<20	<20	12	1.64	0.55	0.37	<.01	0.05	8	3	4	7	10	<5	<10	0.13	<1
L-6E 3+25S		0.3	15	7	58	1	87	16	0.2	<5	<5	<5	4.27	494	<10	106	159	102	<20	<20	5	1.89	1.67	0.32	<.01	0.03	6	2	4	14	8	<5	<10	0.21	<1
L-6E 3+50S		0.3	15	6	56	1	43	10	0.2	<5	<5	<5	4.32	376	<10	135	84	103	<20	<20	7	1.92	0.94	0.58	<.01	0.05	10	3	3	21	8	<5	<10	0.22	<1
L-6E 3+75S		<.2	35	5	45	1	62	20	<.2	<5	6	<5	4.19	403	<10	183	69	87	<20	<20	9	2.80	1.14	0.98	0.02	0.03	25	10	<2	16	7	6	<10	0.21	2
L-6E 4+00S		0.2	20	6	51	1	40	11	0.3	<5	6	<5	4.94	301	<10	131	77	108	<20	<20	8	2.12	0.95	0.57	0.01	0.03	9	4	3	19	8	<5	<10	0.25	<1
L-6E 4+25S		<.2	12	9	35	1	17	6	0.3	<5	<5	<5	4.09	174	<10	121	46	129	<20	<20	9	1.64	0.44	0.37	<.01	0.03	7	3	5	8	11	<5	<10	0.24	<1
L-6E 4+50S		<.2	11	7	50	1	18	6	0.3	<5	<5	<5	3.42	188	<10	137	43	130	<20	<20	9	1.56	0.47	0.39	<.01	0.03	8	3	5	8	11	<5	<10	0.27	<1
L-6E 5+00S		0.3	102	7	87	2	53	21	0.3	<5	6	<5	4.85	1073	<10	240	78	114	<20	<20	29	3.17	1.33	1.31	0.02	0.06	34	37	4	17	8	14	<10	0.20	<1
L8E 1+00N		<.2	14	6	42	1	21	7	0.2	<5	<5	<5	4.66	193	<10	100	50	95	<20	<20	9	1.94	0.51	0.35	0.01	0.04	6	3	2	15	8	<5	<10	0.19	<1
L8E 0+25S		<.2	16	9	41	2	23	8	<.2	<5	<5	<5	3.82	277	<10	149	49	95	<20	<20	10	1.38	0.52	0.36	0.01	0.03	11	4	3	10	8	<5	<10	0.20	<1
L8E 0+50S		<.2	17	13	43	1	20	6	0.2	<5	6	<5	3.47	234	<10	160	43	79	<20	<20	11	1.39	0.42	0.31	<.01	0.03	8	3	3	9	7	<5	<10	0.14	<1
L8E 0+75S		<.2	26	12	61	1	32	17	0.2	<5	7	<5	4.38	1569	<10	174	61	91	<20	<20	10	1.78	0.76	0.43	<.01	0.04	8	5	<2	12	6	<5	<10	0.12	<1
L8E 1+00S		<.2	14	15	74	1	23	9	0.2	<5	6	<5	4.05	334	<10	196	45	75	<20	<20	14	1.52	0.45	0.40	<.01	0.05	12	3	3	11	6	<5	<10	0.11	<1
L8E 1+25S		<.2	22	12	100	2	35	12	0.5	<5	9	<5	4.30	337	<10	107	54	75	<20	<20	14	2.13	0.80	0.46	0.01	0.04	13	5	2	17	6	<5	<10	0.14	1
L8E 1+50S		<.2	31	17	82	2	38	11	0.6	<5	10	<5	4.24	298	<10	117	63	71	<20	<20	15	1.51	0.71	0.51	<.01	0.04	13	6	<2	13	6	<5	<10	0.10	<1
L8E 1+75S		<.2	27	19	109	2	40	15	0.4	<5	11	<5	5.14	394	<10	98	64	69	<20	<20	15	1.75	0.78	0.42	<.01	0.05	15	5	<2	17	5	<5	<10	0.11	<1
L8E 2+00S		0.4	133	13	134	2	102	20	1.2	<5	11	<5	3.95	492	<10	95	99	50	<20	<20	26	2.17	0.77	0.82	0.01	0.04	27	23	<2	21	4	5	<10	0.07	<1
L8E 2+25S		0.4	35	19	74	2	48	16	0.4	<5	10	<5	5.06	673	<10	59	98	65	<20	<20	14	2.01	0.94	0.34	<.01	0.04	10	4	<2	17	5	<5	<10	0.08	<1

ITS Intertek Testing Services
Bondar Clegg

Geochemical Lab Report

CLIENT: EUREKA RESOURCES, INC.
REPORT: V99-01022.0 (COMPLETE)

PROJECT: NONE GIVEN

DATE RECEIVED: 09-SEP-99 DATE PRINTED: 16-SEP-99

SAMPLE NUMBER	Ag PPM	Cu PPM	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	Sb PPM	Fe PCT	Mn PPM	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	W PPM	La PPM	Al PCT	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM	Ga PPM	Li PPM	Nb PPM	Sc PPM	Ta PPM	Ti PCT	Zr PPM
L8E 2+50S	0.2	26	7	57	1	69	15	<.2	<5	6	<5	4.68	359	<10	60	121	76	<20	<20	11	2.19	1.36	0.32	<.01	0.03	8	3	2	21	6	<5	<10	0.14	<1
L8E 2+75S	<.2	48	6	64	1	226	42	0.4	<5	18	<5	5.37	724	<10	54	271	81	<20	<20	7	3.43	3.93	0.40	<.01	0.03	8	7	<2	26	5	<5	<10	0.15	<1
L8E 3+00S	<.2	38	5	81	1	132	23	0.4	<5	23	<5	5.61	683	<10	132	231	87	<20	<20	7	3.08	2.81	0.29	<.01	0.02	6	3	<2	29	6	<5	<10	0.10	<1
L8E 3+25S	0.4	15	7	87	2	62	14	<.2	<5	11	<5	4.43	423	<10	202	123	83	<20	<20	10	2.11	1.45	0.37	<.01	0.04	10	3	3	23	6	<5	<10	0.11	<1
L8E 3+50S	0.3	14	9	62	1	47	11	0.2	<5	6	<5	4.18	320	<10	131	92	86	<20	<20	10	1.80	1.07	0.35	<.01	0.04	8	3	2	15	7	<5	<10	0.15	<1
L8E 3+75S	0.3	60	10	66	2	62	17	0.3	<5	7	<5	3.59	745	<10	134	98	75	<20	<20	15	2.13	1.35	1.19	0.01	0.04	23	15	<2	13	6	7	<10	0.10	<1
L8E 4+75S	<.2	25	7	46	2	35	15	<.2	<5	<5	<5	3.65	510	<10	139	52	99	<20	<20	11	2.38	0.99	1.15	0.02	0.04	16	11	3	13	7	7	<10	0.23	2
L8E 5+00S	<.2	22	7	45	2	17	9	0.2	<5	<5	<5	4.19	486	<10	139	45	109	<20	<20	8	1.50	0.45	1.24	0.01	0.03	23	8	3	7	9	<5	<10	0.21	<1
6+00E 0+25N	<.2	22	8	78	<1	35	13	0.2	<5	<5	<5	3.87	736	<10	201	54	81	<20	<20	13	2.26	0.85	0.71	0.01	0.07	14	6	2	16	6	<5	<10	0.18	<1
6+00E 0+50N	<.2	24	8	52	1	34	12	0.2	<5	6	<5	3.73	303	<10	175	55	88	<20	<20	12	2.28	0.79	0.55	0.01	0.03	10	5	3	14	7	<5	<10	0.17	2
6+00E 0+75N	<.2	18	8	78	1	27	8	<.2	<5	5	<5	3.37	781	<10	277	46	81	<20	<20	12	1.69	0.73	1.32	0.01	0.12	26	4	3	12	6	<5	<10	0.13	<1
6+00E 1+00N	<.2	17	8	72	1	24	10	0.3	<5	6	<5	5.33	388	<10	149	57	116	<20	<20	11	2.25	0.67	0.36	<.01	0.03	9	4	3	22	9	<5	<10	0.20	<1
6+00E 1+25N	0.2	35	8	59	1	39	14	<.2	<5	7	<5	3.79	357	<10	149	65	81	<20	<20	13	2.21	0.80	0.55	0.01	0.05	11	7	3	18	6	5	<10	0.15	<1
6+00E 1+50N	<.2	21	10	54	<1	31	11	0.2	<5	<5	<5	3.20	505	<10	203	54	78	<20	<20	12	1.94	0.74	0.57	0.01	0.04	12	6	3	15	6	<5	<10	0.13	<1
6+00E 2+00N	<.2	11	7	48	<1	21	8	<.2	<5	<5	<5	4.07	219	<10	95	52	66	<20	<20	10	2.29	0.53	0.32	0.01	0.03	7	3	<2	19	6	<5	<10	0.12	<1
6+00E 2+25N	<.2	15	6	54	2	26	9	0.2	<5	<5	<5	4.68	231	<10	144	59	93	<20	<20	11	2.42	0.64	0.45	0.01	0.04	10	4	2	19	7	<5	<10	0.16	2
6+00E 2+50N	<.2	13	7	64	2	24	9	<.2	<5	<5	<5	5.13	308	<10	149	56	125	<20	<20	10	2.35	0.61	0.44	0.01	0.03	10	4	4	16	9	<5	<10	0.26	<1
BL 6+00E	<.2	10	9	56	1	23	8	<.2	<5	<5	<5	3.47	337	<10	139	49	88	<20	<20	14	1.89	0.68	0.52	<.01	0.04	10	4	4	15	7	<5	<10	0.19	<1

Intertek Testing Services
Bondar Clegg

Geochemical Lab Report

CLIENT: EUREKA RESOURCES, INC.
REPORT: V99-01023.0 (COMPLETE)

PROJECT: NONE GIVEN
DATE RECEIVED: 09-SEP-99 DATE PRINTED: 16-SEP-99

SAMPLE NUMBER	ELEMENT UNITS	Ag PPM	Cu PPM	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	Sb PPM	Fe PCT	Mn PPM	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	W PPM	La PPM	Al PCT	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM	Ga PPM	Li PPM	Nb PPM	Sc PPM	Ta PPM	Ti PCT	Zr PPM
RTC 0+00		<.2	24	8	67	<1	35	17	0.2	<5	5	<5	3.70	405	<10	146	57	74	<20	<20	24	2.46	0.90	0.62	0.03	0.08	15	8	3	18	6	<5	<10	0.19	4
RTC 1+00		<.2	32	9	63	<1	38	17	<.2	<5	<5	<5	3.67	549	<10	230	56	81	<20	<20	19	2.08	0.92	0.90	0.03	0.10	21	11	2	14	6	7	<10	0.21	10
RTC 1+50		<.2	23	7	64	<1	36	18	<.2	<5	5	<5	3.51	532	<10	146	52	83	<20	<20	19	2.09	0.88	0.99	0.02	0.08	19	9	3	13	6	<5	<10	0.25	3
RTC 3+00		<.2	32	7	64	<1	42	22	<.2	<5	<5	<5	3.49	596	<10	170	52	85	<20	<20	14	2.46	0.88	0.95	0.02	0.09	15	9	2	12	6	5	<10	0.24	5
RTC 3+50		<.2	61	9	67	<1	47	27	<.2	<5	7	<5	4.06	955	<10	233	60	96	<20	<20	15	2.56	1.15	0.93	0.03	0.07	14	10	3	14	7	6	<10	0.25	5
RTC 4+00		<.2	31	6	49	<1	38	20	<.2	<5	<5	<5	3.25	607	<10	132	46	87	<20	<20	13	2.19	0.87	1.11	0.02	0.06	16	10	2	10	7	<5	<10	0.27	6
RTC 4+50		<.2	36	8	60	<1	48	25	<.2	<5	6	<5	3.70	673	<10	190	65	87	<20	<20	15	2.97	1.02	1.02	0.03	0.08	15	13	2	13	7	7	<10	0.26	3
RTC 5+00		<.2	93	8	63	<1	84	27	<.2	<5	14	<5	4.62	863	<10	239	108	94	<20	<20	19	2.84	1.25	1.01	0.02	0.07	17	25	2	21	7	18	<10	0.22	<1
RTC 5+50		<.2	85	10	81	<1	80	28	<.2	<5	16	<5	5.06	1094	<10	329	115	97	<20	<20	19	3.13	1.35	1.06	0.02	0.08	21	28	3	25	7	17	<10	0.19	<1
RTC 6+00		<.2	44	6	55	<1	49	22	<.2	<5	7	<5	3.73	674	<10	226	74	97	<20	<20	17	2.32	1.24	1.28	0.03	0.05	20	17	<2	15	7	8	<10	0.27	5
RTC 7+00		<.2	65	7	67	<1	47	21	<.2	<5	7	<5	3.79	593	<10	211	71	94	<20	<20	19	2.39	1.09	1.08	0.02	0.07	20	15	3	16	7	9	<10	0.26	8
RTC 8+00		<.2	40	9	81	<1	52	29	0.2	<5	8	<5	4.41	1121	<10	148	68	106	<20	<20	12	2.84	1.25	1.24	0.02	0.06	14	11	4	15	8	7	<10	0.31	3
RTC 8+50		<.2	40	7	56	<1	46	23	<.2	<5	<5	<5	3.64	679	<10	176	56	95	<20	<20	14	2.51	1.12	1.20	0.03	0.08	19	11	2	13	7	6	<10	0.29	3
RTC 9+00		<.2	35	5	64	<1	42	23	<.2	<5	<5	<5	4.01	692	<10	171	63	109	<20	<20	13	2.82	1.20	1.26	0.03	0.09	20	11	4	13	9	6	<10	0.33	4
RTC 9+50		<.2	34	5	57	<1	43	22	<.2	<5	<5	<5	3.87	613	<10	150	58	102	<20	<20	13	2.59	1.13	1.17	0.03	0.07	17	11	3	14	8	6	<10	0.29	4
RTC 10+00		<.2	39	13	79	<1	62	27	<.2	<5	7	<5	4.00	626	<10	136	63	92	<20	<20	16	2.72	1.30	1.12	0.03	0.09	15	12	2	14	8	5	<10	0.29	6
RTC 10+50		<.2	35	6	48	<1	70	29	<.2	<5	<5	<5	3.76	649	<10	108	79	96	<20	<20	10	2.71	1.61	1.25	0.02	0.05	14	11	3	14	7	6	<10	0.31	3
RTC 11+00		<.2	59	9	67	<1	93	32	0.2	<5	9	<5	4.98	853	<10	134	105	103	<20	<20	14	2.98	1.84	0.92	0.02	0.06	14	11	<2	20	8	6	<10	0.26	<1
RTC 11+50		<.2	82	2	52	<1	198	35	<.2	<5	<5	<5	4.89	662	<10	89	177	98	<20	<20	8	3.19	3.20	1.00	0.02	0.04	16	10	<2	27	7	<5	<10	0.26	<1
RTC 13+00		<.2	42	5	57	<1	52	29	<.2	<5	<5	<5	4.34	679	<10	184	68	112	<20	<20	11	3.01	1.40	1.17	0.03	0.08	17	11	4	16	8	7	<10	0.30	5
RTC 13+50		<.2	36	3	58	<1	59	27	<.2	<5	<5	<5	4.14	530	<10	188	72	107	<20	<20	11	3.07	1.39	1.12	0.03	0.06	15	11	3	16	8	6	<10	0.30	3
RTC 14+50		<.2	45	4	49	<1	46	24	<.2	<5	<5	<5	3.89	639	<10	180	67	109	<20	<20	13	2.60	1.30	1.33	0.03	0.06	19	12	3	14	8	6	<10	0.33	5
RTC 15+50		<.2	43	5	55	<1	42	22	<.2	<5	<5	<5	3.88	685	<10	196	77	109	<20	<20	22	2.73	1.18	1.23	0.02	0.06	20	16	3	15	9	7	<10	0.30	1
RTC 16+00		<.2	33	5	59	<1	44	24	<.2	<5	<5	<5	4.19	597	<10	119	68	108	<20	<20	12	2.72	1.22	1.22	0.03	0.08	15	10	3	14	8	6	<10	0.31	4
RTC 16+50		<.2	47	2	60	<1	45	26	<.2	<5	<5	<5	4.40	700	<10	211	74	120	<20	<20	10	3.36	1.35	1.31	0.03	0.08	18	12	4	12	9	8	<10	0.36	3
RTC 17+50		<.2	60	5	57	<1	106	33	<.2	<5	8	<5	5.24	832	<10	195	252	118	<20	<20	8	4.01	2.76	0.90	0.02	0.10	18	12	3	40	8	11	<10	0.27	1
RTC 18+00		<.2	38	7	60	<1	43	23	<.2	<5	<5	<5	3.97	704	<10	198	70	107	<20	<20	18	2.54	1.19	1.33	0.02	0.07	19	16	3	13	8	7	<10	0.33	2
RTC 18+50		<.2	46	10	65	<1	49	22	<.2	<5	6	<5	4.15	691	<10	186	80	98	<20	<20	19	2.61	1.15	1.22	0.02	0.08	19	16	3	16	7	9	<10	0.24	1
SRTC 0+00		<.2	76	35	164	<1	94	32	0.3	<5	13	<5	4.23	814	<10	121	92	65	<20	<20	24	2.36	1.65	0.69	0.01	0.10	20	12	3	17	4	<5	<10	0.16	8
SRTC 0+50		0.2	56	10	71	<1	102	26	<.2	<5	6	<5	4.18	677	<10	115	96	80	<20	<20	17	2.48	1.49	1.01	0.02	0.05	21	13	<2	19	6	6	<10	0.20	<1

ITS **Intertek Testing Services**
Bondar Clegg

Geochemical Lab Report

CLIENT: EUREKA RESOURCES, INC.
REPORT: V99-01023.0 (COMPLETE)

PROJECT: NONE GIVEN
DATE RECEIVED: 09-SEP-99 DATE PRINTED: 16-SEP-99

SAMPLE NUMBER	Ag	Cu	Pb	Zn	Mo	Ni	Co	Cd	Bi	As	Sb	Fe	Mn	Te	Ba	Cr	V	Sn	W	La	Al	Mg	Ca	Na	K	Sr	Y	Ga	Li	Nb	Sc	Ta	Ti	Zr
UNITS	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PCT	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PCT	PCT	PCT	PCT	PCT	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PCT	PPM
SRTC 1+50	<.2	60	5	60	<1	223	42	<.2	<5	9	<5	5.43	699	<10	67	260	87	<20	<20	9	3.57	3.84	0.61	0.01	0.04	8	9	<2	26	6	<5	<10	0.22	<1
SRTC 3+00	<.2	41	21	82	<1	57	24	<.2	<5	10	<5	4.19	572	<10	113	66	69	<20	<20	29	2.44	1.21	0.72	0.02	0.10	14	13	<2	18	5	<5	<10	0.16	5
SRTC 3+50	<.2	49	199	248	<1	43	22	0.2	<5	13	<5	4.90	860	<10	149	49	82	<20	<20	37	2.52	0.99	0.79	0.02	0.14	26	15	2	15	6	6	<10	0.13	6
SRTC 4+00	0.2	39	5	58	<1	39	29	<.2	<5	<5	<5	4.83	749	<10	117	67	124	<20	<20	8	3.20	1.38	1.42	0.02	0.06	18	13	4	13	9	7	<10	0.40	2
SRTC 4+50	<.2	45	2	73	<1	43	34	<.2	<5	<5	<5	5.68	881	<10	109	74	163	<20	<20	7	3.63	1.67	1.66	0.04	0.05	27	15	4	17	12	11	<10	0.43	7
SRTC 5+00	<.2	36	2	49	<1	41	26	<.2	<5	<5	<5	4.10	648	<10	148	58	119	<20	<20	9	3.01	1.30	1.52	0.03	0.05	20	12	4	12	8	7	<10	0.37	4
SRTC 5+50	<.2	34	<2	51	<1	46	28	<.2	<5	<5	<5	4.89	583	<10	131	64	128	<20	<20	11	3.19	1.35	1.32	0.03	0.05	19	15	3	14	8	8	<10	0.34	6
SRTC 6+00	<.2	33	<2	47	<1	40	23	<.2	<5	<5	<5	3.95	511	<10	130	61	108	<20	<20	8	3.00	1.21	1.27	0.03	0.05	17	12	3	11	8	6	<10	0.34	4
SRTC 6+50	<.2	41	<2	49	<1	44	33	<.2	<5	<5	<5	4.08	672	<10	113	62	123	<20	<20	6	3.30	1.26	1.58	0.03	0.04	17	13	4	10	9	7	<10	0.40	8
SRTC 7+00	<.2	45	<2	55	<1	46	29	<.2	<5	<5	<5	4.38	710	<10	132	59	120	<20	<20	9	3.21	1.31	1.48	0.03	0.06	22	13	3	12	9	7	<10	0.36	6
SRTC 7+50	0.3	65	2	64	<1	59	34	<.2	<5	6	<5	4.87	712	<10	137	88	119	<20	<20	9	4.28	1.46	1.46	0.04	0.05	18	13	4	13	8	8	<10	0.33	4
SRTC 8+00	<.2	55	<2	59	<1	50	29	<.2	<5	<5	<5	4.64	795	<10	178	68	127	<20	<20	9	3.30	1.55	1.52	0.05	0.08	25	13	4	14	9	7	<10	0.38	10
SRTC 8+50	<.2	39	<2	60	<1	46	25	<.2	<5	<5	<5	4.39	538	<10	135	66	110	<20	<20	11	3.30	1.26	1.16	0.03	0.05	17	11	3	14	8	6	<10	0.32	5
SRTC 9+00	<.2	50	<2	57	<1	50	29	<.2	<5	<5	<5	4.37	684	<10	138	69	114	<20	<20	11	3.00	1.35	1.37	0.04	0.06	25	12	3	14	8	7	<10	0.32	4
SRTC 9+50	<.2	52	4	55	<1	49	24	<.2	<5	<5	<5	4.10	646	<10	145	69	104	<20	<20	12	2.81	1.43	1.23	0.03	0.06	22	11	3	14	8	6	<10	0.30	8
SRTC 10+00	<.2	85	<2	60	<1	55	33	<.2	<5	<5	<5	4.89	794	<10	134	71	126	<20	<20	8	3.45	1.63	1.54	0.04	0.05	24	13	2	12	9	8	<10	0.39	6
SRTC 10+50	<.2	49	2	61	<1	52	29	<.2	<5	<5	<5	4.58	579	<10	136	75	112	<20	<20	12	3.52	1.33	1.16	0.03	0.06	22	15	4	14	8	8	<10	0.30	3
SRTC 11+00	0.2	39	<2	66	<1	48	26	<.2	<5	<5	<5	5.07	571	<10	143	78	120	<20	<20	9	3.72	1.42	1.23	0.03	0.06	18	12	5	16	9	8	<10	0.33	3
SRTC 11+50	<.2	52	2	63	<1	58	33	<.2	<5	<5	<5	4.85	751	<10	145	77	127	<20	<20	10	3.65	1.60	1.45	0.04	0.07	22	14	4	15	9	8	<10	0.36	8
SRTC 12+00	<.2	42	<2	51	<1	42	29	<.2	<5	<5	<5	4.67	685	<10	117	57	134	<20	<20	6	3.44	1.42	1.79	0.03	0.04	16	13	5	10	10	7	<10	0.41	4
SRTC 12+50	0.2	71	<2	50	<1	49	28	<.2	<5	<5	<5	4.45	723	<10	123	60	127	<20	<20	7	3.24	1.41	1.83	0.03	0.04	17	14	4	12	10	8	<10	0.41	4
SRTC 13+00	<.2	66	<2	57	<1	52	37	<.2	<5	<5	<5	6.43	689	<10	78	88	146	<20	<20	6	4.78	1.96	1.88	0.02	0.03	11	16	4	15	10	12	<10	0.36	<1
SRTC 13+50	<.2	49	2	85	<1	46	33	<.2	<5	<5	<5	5.26	618	<10	128	58	130	<20	<20	8	3.46	1.38	1.43	0.02	0.05	17	12	4	12	10	7	<10	0.36	3
SRTC 14+00	<.2	66	<2	61	<1	48	40	<.2	<5	5	<5	5.94	813	<10	111	66	156	<20	<20	6	3.77	1.80	1.63	0.03	0.05	31	12	4	14	11	8	<10	0.42	<1
SRTC 15+00	<.2	35	<2	68	<1	42	22	<.2	<5	<5	<5	4.81	451	<10	121	68	120	<20	<20	9	3.73	1.22	1.14	0.02	0.04	14	11	3	15	9	7	<10	0.33	2
SRTC 15+50	<.2	46	3	64	<1	47	25	<.2	<5	<5	<5	4.71	500	<10	142	64	119	<20	<20	13	3.53	1.33	1.18	0.03	0.05	18	13	4	16	9	8	<10	0.32	3
SRTC 16+00	<.2	56	<2	60	<1	49	34	<.2	<5	<5	<5	5.10	685	<10	181	56	128	<20	<20	10	3.47	1.46	1.30	0.03	0.06	21	12	4	15	9	7	<10	0.31	3
SRTC 16+50	<.2	45	2	76	<1	41	26	<.2	<5	<5	<5	5.76	550	<10	115	65	139	<20	<20	9	3.84	1.35	1.23	0.02	0.05	16	12	4	15	10	8	<10	0.33	1

ITS Intertek Testing Services
Bondar Clegg

Geochemical Lab Report

CLIENT: EUREKA RESOURCES, INC.
REPORT: V99-01024.0 (COMPLETE)

PROJECT: NONE GIVEN
DATE RECEIVED: 08-SEP-99 DATE PRINTED: 10-SEP-99

SAMPLE NUMBER	ELEMENT UNITS	Ag PPM	Cu PPM	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	Sb PPM	Fe PCT	Mn PPM	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	W PPM
LIC 1+50E R		<.2	2048	2	24	6	14	11	<.2	<5	<5	<5	1.42	233	<10	110	55	7	<20	<20
LIC 0+95E R		0.3	30	32	42	2	29	10	0.3	<5	78	<5	3.77	241	<10	105	41	34	<20	<20
SRT 3+89		0.5	203	400	231	1	27	33	0.6	<5	76	<5	7.88	314	<10	45	76	12	<20	<20
WR 10		<.2	8	14	37	<1	10	4	<.2	<5	13	<5	2.23	173	<10	120	78	9	<20	<20

SAMPLE NUMBER	La PPM	Al PCT	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM	Ga PPM	Li PPM	Nb PPM	Sc PPM	Ta PPM	Ti PCT	Zr PPM
LIC 1+50E R	4	0.36	0.19	0.14	<.01	0.07	3	6	<2	2	<1	<5	<10	0.06	4
LIC 0+95E R	9	1.32	0.61	0.20	<.01	0.24	10	6	<2	9	2	<5	<10	0.06	15
SRT 3+89	8	1.89	0.59	0.04	<.01	0.24	4	4	<2	13	<1	<5	<10	<.01	10
WR 10	5	0.90	0.44	0.15	<.01	0.21	10	3	<2	7	<1	<5	<10	0.06	5

ITS Intertek Testing Services
Bondar Clegg

Geochemical Lab Report

CLIENT: EUREKA RESOURCES, INC.
PROJECT: NONE GIVEN
REPORT: V99-01025.0 (COMPLETE)
DATE RECEIVED: 08-SEP-99 DATE PRINTED: 16-SEP-99

SAMPLE NUMBER	ELEMENT / UNITS	Ag PPM	Cu PPM	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	Sb PPM	Fe PCT	Mn PPM	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	W PPM	La PPM	Al PCT	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM	Ga PPM	Li PPM	Nb PPM	Sc PPM	Ta PPM	Ti PCT	Zr PPM
SRLM01		<.2	30	3	63	1	41	17	<.2	<5	<5	<5	4.63	836	<10	121	56	134	<20	<20	4	2.87	1.42	1.65	0.03	0.02	18	16	5	13	10	8	<10	0.43	3

CLIENT: EUREKA RESOURCES, INC.
REPORT: V99-00744.0 (COMPLETE)

PROJECT: NONE GIVEN

DATE RECEIVED: 16-JUL-99 DATE PRINTED: 24-JUL-99

SAMPLE NUMBER	ELEMENT UNITS	Ag PPM	Cu PPM	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	Sb PPM	Fe PCT	Mn PPM	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	W PPM	La PPM	Al PCT	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM	Ga PPM	Li PPM	Nb PPM	Sc PPM	Ta PPM	Ti PCT	Zr PPM
WR-1A		0.3	1202	<2	42	2	31	34	0.2	<5	<5	<5	6.84	507	<10	96	76	208	<20	<20	3	3.62	2.25	2.21	0.05	0.08	11	20	3	18	16	16	<10	0.38	<1
WR-1B		0.7	545	30	44	4	192	52	<.2	<5	26	<5	>10.00	188	<10	9	164	50	<20	<20	13	1.23	0.36	0.26	0.01	0.40	5	5	<2	5	3	<5	<10	0.10	13
WR-2		<.2	21	28	47	3	26	4	<.2	<5	14	<5	3.37	228	<10	111	67	30	<20	<20	20	1.85	0.74	0.16	<.01	0.42	11	10	<2	12	1	<5	<10	0.02	4
WR-3		0.2	58	<2	58	1	23	30	<.2	<5	9	<5	5.51	651	<10	21	59	166	<20	<20	2	3.12	1.66	2.28	0.04	0.04	9	14	3	10	12	5	<10	0.55	<1
WR-4		0.3	166	<2	49	1	41	50	<.2	<5	<5	<5	7.71	423	<10	37	50	373	<20	<20	3	2.97	2.08	2.25	0.06	<.01	8	21	3	29	31	9	<10	0.65	<1
M-1-3		<.2	37	25	59	3	37	14	<.2	<5	28	<5	3.75	296	<10	199	116	13	<20	<20	71	1.72	0.68	0.18	<.01	0.40	25	8	<2	15	<1	<5	<10	<.01	10
M7-R		0.6	4222	11	40	35	31	68	<.2	<5	30	<5	5.79	224	<10	67	123	75	<20	<20	9	1.19	0.79	0.44	0.02	0.18	9	9	3	7	4	<5	<10	0.14	3
L-A2+00N		0.2	69	<2	83	1	34	45	0.3	<5	54	<5	>10.00	1331	<10	108	21	92	<20	<20	2	1.05	3.08	4.15	0.21	0.13	90	11	<2	6	6	23	<10	<.01	<1
L-4E-0+92		<.2	10	6	7	9	18	2	<.2	<5	<5	<5	0.82	100	<10	54	363	4	<20	<20	9	0.25	0.03	0.03	<.01	0.16	1	<1	<2	<1	<1	<5	<10	<.01	4
M-6		<.2	13	<2	50	<1	24	28	<.2	<5	<5	<5	5.50	678	<10	23	36	158	<20	<20	3	3.31	1.75	2.18	0.05	0.02	7	18	6	8	12	<5	<10	0.37	4
WSL-1		<.2	44	5	79	<1	45	24	0.3	<5	<5	<5	4.30	824	<10	187	73	117	<20	<20	10	2.94	1.19	1.25	0.02	0.05	18	18	<2	13	9	9	<10	0.29	1
WSL-2		<.2	38	3	76	<1	47	24	0.2	<5	<5	<5	3.97	804	<10	153	59	104	<20	<20	9	2.53	1.50	1.36	0.01	0.05	16	14	<2	13	8	7	<10	0.31	3
WSL-3		0.4	86	6	76	<1	44	25	0.3	<5	<5	<5	4.65	948	<10	192	79	152	<20	<20	9	3.46	1.32	2.13	0.03	0.05	30	34	2	14	12	18	<10	0.37	2
WSL-4		<.2	52	4	81	2	47	35	0.3	<5	8	<5	6.09	2735	<10	177	69	171	<20	<20	8	2.98	1.45	1.82	0.03	0.04	20	20	<2	14	13	10	<10	0.38	3
L-A0+25N		<.2	53	7	96	<1	64	27	0.3	<5	10	<5	4.64	786	<10	230	79	92	<20	<20	23	3.18	1.13	0.88	0.02	0.06	18	20	<2	23	7	8	<10	0.21	2
L-A0+50N		<.2	49	7	82	<1	51	20	<.2	<5	9	<5	4.63	597	<10	212	73	97	<20	<20	23	2.40	1.12	0.93	0.02	0.06	20	16	<2	22	8	7	<10	0.20	<1
L-A0+75N		<.2	100	9	111	<1	59	24	0.3	<5	10	<5	4.68	1265	<10	275	94	100	<20	<20	27	2.80	1.13	0.97	0.02	0.08	23	26	<2	20	8	15	<10	0.15	<1
L-A1+00N		<.2	70	9	82	<1	47	22	0.3	<5	7	<5	4.09	982	<10	250	77	91	<20	<20	22	2.35	1.04	0.92	0.01	0.07	21	15	<2	18	7	9	<10	0.19	<1
L-A1+25N		<.2	71	9	76	<1	51	23	0.3	<5	7	<5	3.84	1074	<10	299	85	93	<20	<20	23	2.49	1.00	0.91	0.02	0.07	18	22	<2	16	7	16	<10	0.20	<1
L-A1+50N		<.2	62	11	92	1	49	22	0.3	<5	7	<5	4.89	856	<10	329	89	98	<20	<20	21	2.75	0.99	0.83	0.01	0.08	18	15	3	20	8	11	<10	0.16	<1
L-A1+75NB		0.4	62	10	88	<1	47	17	0.3	<5	7	<5	4.41	497	<10	324	82	88	<20	<20	22	2.59	0.94	0.89	0.02	0.08	20	17	<2	18	7	13	<10	0.16	<1
L-A2+00NB		<.2	84	11	92	1	47	19	0.4	<5	8	<5	4.85	1016	<10	300	87	93	<20	<20	26	2.39	0.94	0.87	0.02	0.07	21	23	<2	19	7	14	<10	0.15	<1
L-A2+50NB		<.2	24	6	69	<1	37	15	<.2	<5	6	<5	5.01	345	<10	195	65	86	<20	<20	22	2.53	0.92	0.67	0.01	0.05	17	7	<2	24	7	<5	<10	0.19	1
L-A2+75NB		0.3	22	6	79	<1	32	15	0.3	<5	5	<5	5.17	392	<10	182	65	96	<20	<20	15	3.08	0.78	0.69	0.01	0.04	11	6	<2	21	8	<5	<10	0.24	1
L-A3+00NB		0.3	16	5	67	<1	28	15	0.3	<5	<5	<5	5.12	326	<10	134	64	104	<20	<20	14	2.79	0.74	0.79	0.02	0.04	11	6	3	19	8	<5	<10	0.28	3
L-A3+25NB		0.2	29	8	70	<1	39	21	0.2	<5	6	<5	4.70	591	<10	209	63	93	<20	<20	20	2.39	0.97	0.89	0.02	0.06	17	10	<2	19	7	5	<10	0.24	1
L-A0+25SB		<.2	106	13	101	2	58	29	0.4	<5	10	<5	5.21	1432	<10	292	96	113	<20	<20	31	2.88	0.90	0.97	0.02	0.07	22	26	3	22	9	15	<10	0.17	<1
L-A1+00SB		0.4	186	14	144	1	78	29	0.4	<5	23	<5	6.77	1122	<10	381	138	119	<20	<20	79	3.51	0.97	0.97	0.02	0.09	29	89	<2	30	9	34	<10	0.12	<1
L-A1+50SB		0.3	108	11	104	<1	83	25	0.4	<5	11	<5	6.09	628	<10	302	94	105	<20	<20	20	3.41	1.13	0.84	0.01	0.08	14	17	<2	25	8	10	<10	0.21	<1
L-A1+75SB		<.2	36	8	68	<1	46	20	<.2	<5	6	<5	4.71	751	<10	254	66	92	<20	<20	17	2.55	1.25	0.81	0.01	0.05	11	8	<2	22	7	<5	<10	0.19	1

ITS Intertek Testing Services

Bondar Clegg

Geochemical Lab Report

CLIENT: EUREKA RESOURCES, INC.
REPORT: V99-00744.0 (COMPLETE)

PROJECT: NONE GIVEN

DATE RECEIVED: 16-JUL-99 DATE PRINTED: 24-JUL-99

SAMPLE NUMBER	ELEMENT UNITS	Ag PPM	Cu PPM	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	Sb PPM	Fe PCT	Mn PPM	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	W PPM	La PPM	Al PCT	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM	Ga PPM	Li PPM	Nb PPM	Sc PPM	Ta PPM	Ti PCT	Zr PPM
L-A1+25SB		0.2	76	10	96	<1	58	21	0.3	<5	9	<5	5.67	547	<10	291	88	114	<20	<20	24	3.08	1.15	1.04	0.01	0.07	17	23	<2	27	9	12	<10	0.21	<1
L0+25E-0+00B		0.2	20	6	99	<1	35	15	0.4	<5	<5	<5	4.09	329	<10	176	58	84	<20	<20	16	2.59	0.82	0.79	0.02	0.05	14	7	2	20	6	<5	<10	0.20	2
L0+25E-0+25NB		<.2	21	7	84	<1	36	17	0.3	<5	<5	<5	4.39	400	<10	153	60	89	<20	<20	18	2.68	0.87	0.75	0.01	0.05	14	7	<2	19	7	<5	<10	0.21	1
L0+25E-0+50NB		<.2	18	6	96	<1	33	14	0.3	<5	<5	<5	4.60	325	<10	147	61	90	<20	<20	17	2.61	0.81	0.85	0.01	0.04	15	6	<2	21	7	<5	<10	0.20	<1
L0+75E-0+25NB		0.2	29	7	64	<1	43	19	<.2	<5	5	<5	3.76	518	<10	156	65	83	<20	<20	20	2.04	1.03	0.91	0.02	0.06	19	9	<2	17	6	5	<10	0.22	3
L0+75E-0+50NB		<.2	22	8	98	<1	39	17	0.2	<5	5	<5	4.39	390	<10	179	61	90	<20	<20	19	2.64	0.86	0.80	0.02	0.05	15	7	<2	21	7	<5	<10	0.22	3
L0+75E-0+75NB		0.3	24	6	58	<1	33	18	0.3	<5	<5	<5	3.42	449	<10	135	51	92	<20	<20	12	1.99	0.79	1.10	0.01	0.04	16	8	<2	13	8	<5	<10	0.26	1
L1E-3+75SB		0.7	38	8	74	<1	43	18	0.3	<5	7	<5	4.92	566	<10	176	65	102	<20	<20	11	2.34	0.92	0.76	0.01	0.06	9	6	<2	17	8	<5	<10	0.19	<1
M1-1		<.2	59	<2	63	<1	200	42	0.2	<5	<5	<5	5.89	515	<10	102	314	105	<20	<20	7	3.49	3.37	0.69	0.01	0.02	11	7	<2	20	7	<5	<10	0.23	<1
M3-1		<.2	49	5	76	<1	128	34	0.2	<5	12	<5	5.56	716	<10	84	145	101	<20	<20	11	2.98	2.19	0.91	0.01	0.04	13	9	<2	32	7	<5	<10	0.23	<1
M4-1		<.2	81	8	84	<1	234	47	0.2	<5	33	<5	6.33	873	<10	98	295	109	<20	<20	11	3.98	4.00	0.43	<.01	0.04	7	9	<2	30	7	8	<10	0.14	<1
M5-1		0.2	25	9	106	<1	37	14	0.3	<5	7	<5	4.73	344	<10	194	56	84	<20	<20	15	2.86	0.90	0.74	0.01	0.05	11	7	<2	24	7	<5	<10	0.17	4
L-0+50E-B/LS		<.2	14	7	56	<1	21	11	<.2	<5	<5	<5	3.05	338	<10	179	47	85	<20	<20	19	1.73	0.54	0.63	0.01	0.04	12	6	3	14	7	<5	<10	0.18	<1
L-0+50E-0+25SS		<.2	25	6	57	<1	35	17	<.2	<5	<5	<5	3.12	507	<10	183	52	80	<20	<20	16	2.09	0.82	0.82	0.01	0.04	13	8	<2	15	6	<5	<10	0.19	<1
L-0+50E-0+50SS		0.2	24	6	63	<1	39	16	<.2	<5	<5	<5	3.59	304	<10	220	59	91	<20	<20	14	2.73	0.86	0.75	0.01	0.03	11	7	3	24	8	5	<10	0.21	1
L-0+50E-0+75SS		<.2	45	8	61	<1	49	20	0.2	<5	13	<5	3.65	709	<10	281	76	94	<20	<20	19	2.29	0.93	0.96	0.01	0.05	19	15	<2	20	8	13	<10	0.16	3
L-0+50E-1+25SS		<.2	100	10	79	1	73	31	0.4	<5	14	<5	4.63	2148	<10	365	100	104	<20	<20	32	2.68	1.06	0.94	0.01	0.07	21	37	<2	19	8	19	<10	0.16	<1
L-0+50E-1+50SS		<.2	29	7	81	<1	37	15	<.2	<5	9	<5	4.03	442	<10	217	69	90	<20	<20	18	2.03	0.87	0.74	0.01	0.05	14	8	<2	19	8	<5	<10	0.18	<1
L-0+50E-1+75SS		0.2	34	9	68	1	35	13	<.2	<5	8	<5	4.04	370	<10	226	64	89	<20	<20	17	1.96	0.71	0.69	0.01	0.04	15	7	2	19	7	<5	<10	0.15	<1
L-0+50E-2+00SS		<.2	43	7	71	<1	50	20	0.2	<5	10	<5	4.39	588	<10	208	72	89	<20	<20	18	2.27	0.94	0.76	0.01	0.05	16	10	<2	24	7	7	<10	0.16	<1
L-0+50E-2+25SS		0.3	54	6	74	1	49	16	0.2	<5	9	<5	4.38	625	<10	278	80	100	<20	<20	19	2.12	0.83	0.85	0.01	0.05	19	16	<2	21	8	6	<10	0.15	<1
L-0+50E-2+50SS		<.2	36	6	70	<1	44	15	0.3	<5	7	<5	5.18	422	<10	209	72	95	<20	<20	16	2.35	0.92	0.63	0.01	0.04	12	6	<2	25	8	<5	<10	0.17	<1
L-0+50E-2+75SS		<.2	19	9	65	<1	25	10	0.3	<5	5	<5	3.77	371	<10	234	56	95	<20	<20	17	1.90	0.60	0.47	<.01	0.04	8	4	4	16	8	<5	<10	0.15	<1
L-0+50E-3+00SS		0.2	21	7	90	<1	35	14	0.3	<5	12	<5	4.59	365	<10	153	70	94	<20	<20	15	2.37	0.88	0.53	0.01	0.04	7	4	2	25	8	<5	<10	0.19	<1
L-0+50E-3+25SS		0.2	23	6	69	<1	33	12	0.3	<5	5	<5	4.47	304	<10	163	61	93	<20	<20	16	2.12	0.73	0.68	0.01	0.04	13	4	4	19	8	<5	<10	0.15	<1
L-0+50E-3+50SS		<.2	45	8	79	1	32	16	<.2	<5	7	<5	3.84	1002	<10	184	69	95	<20	<20	27	1.92	0.69	0.76	0.01	0.05	17	19	<2	18	8	8	<10	0.15	<1
L-0+50E-3+75SS		<.2	345	17	114	2	114	41	0.5	<5	20	<5	6.07	3253	<10	579	209	137	<20	<20	108	4.18	1.00	1.19	0.01	0.12	34	101	2	20	10	53	<10	0.10	<1
L-0+50E-4+00SS		<.2	19	7	89	<1	33	15	<.2	<5	6	<5	4.01	332	<10	171	65	95	<20	<20	15	2.50	0.81	0.63	0.01	0.03	10	6	2	19	8	<5	<10	0.19	<1
L-0+50E-4+25SS		0.2	23	4	66	<1	35	15	0.2	<5	<5	<5	4.31	360	<10	157	66	99	<20	<20	14	2.44	0.90	0.88	0.01	0.04	11	8	2	16	8	5	<10	0.25	<1
L-0+50E-4+50SS		<.2	23	6	71	<1	36	18	0.3	<5	<5	<5	3.59	405	<10	177	60	94	<20	<20	14	2.50	0.89	0.94	0.01	0.04	12	8	<2	14	7	<5	<10	0.25	2

ITS Intertek Testing Services
Bondar Clegg

Geochemical
Lab
Report

CLIENT: EUREKA RESOURCES, INC.
REPORT: V99-00744.0 (COMPLETE)

PROJECT: NONE GIVEN
DATE RECEIVED: 16-JUL-99 DATE PRINTED: 24-JUL-99

SAMPLE NUMBER	ELEMENT UNITS	Ag PPM	Cu PPM	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	Sb PPM	Fe PCT	Mn PPM	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	W PPM	La PPM	Al PCT	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM	Ga PPM	Li PPM	Nb PPM	Sc PPM	Ta PPM	Ti PCT	Zr PPM
L-0+50E-4+75SS		0.2	15	7	79	1	20	11	0.2	<5	<5	<5	3.91	391	<10	189	54	98	<20	<20	15	2.08	0.52	0.54	0.01	0.03	8	4	3	16	8	<5	<10	0.19	<1
L-0+50E-5+00SS		0.3	25	3	57	<1	34	17	0.3	<5	<5	<5	3.63	418	<10	175	62	100	<20	<20	10	2.59	0.90	1.02	0.02	0.04	11	7	<2	13	8	<5	<10	0.27	2
L-1+50E-1+25N		<.2	30	8	69	<1	35	15	<.2	<5	<5	<5	3.59	590	<10	226	70	81	<20	<20	20	2.20	0.91	0.79	0.01	0.06	17	11	<2	18	6	8	<10	0.16	<1
L-1+50E-1+50N		<.2	33	10	78	<1	38	18	0.2	<5	<5	<5	3.79	744	<10	274	79	84	<20	<20	20	2.33	0.91	0.76	0.01	0.08	18	13	<2	18	7	10	<10	0.13	<1
L-1+50E-1+75N		<.2	33	10	75	1	39	17	<.2	<5	<5	<5	3.82	626	<10	278	79	88	<20	<20	24	2.42	0.92	0.76	0.01	0.07	19	15	<2	22	7	8	<10	0.13	<1
L-1+50E-2+00N		<.2	17	7	67	<1	31	14	<.2	<5	<5	<5	4.10	335	<10	132	61	91	<20	<20	20	2.27	0.85	0.61	0.01	0.05	13	6	<2	19	7	<5	<10	0.21	1
L-1+50E-2+25N		<.2	12	7	65	<1	22	12	<.2	<5	<5	<5	2.95	253	<10	140	46	79	<20	<20	21	2.00	0.70	0.57	0.01	0.05	12	5	3	18	6	<5	<10	0.19	<1
L-1+50E-2+50N		<.2	18	6	65	<1	31	15	0.2	<5	<5	<5	3.66	326	<10	130	56	92	<20	<20	19	2.21	0.87	0.73	0.02	0.05	14	6	<2	17	7	<5	<10	0.23	<1
L-1+50E-2+75N		0.2	188	13	127	<1	84	26	0.4	<5	12	<5	3.99	860	<10	314	117	103	<20	<20	75	3.10	1.04	1.08	0.02	0.07	21	59	<2	23	8	29	<10	0.19	<1
L-1+50E-3+00N		0.4	252	21	165	1	93	28	0.4	<5	18	<5	5.00	752	<10	373	138	116	<20	<20	72	3.59	0.94	0.77	0.01	0.09	24	52	<2	27	9	28	<10	0.12	<1
L-1+50E-3+25N		<.2	113	15	108	1	54	20	0.2	<5	14	<5	5.16	493	<10	276	97	122	<20	<20	60	2.70	0.72	0.66	0.01	0.06	15	44	3	23	10	15	<10	0.17	<1
L-1+50E-3+50N		0.4	24	6	80	1	36	16	0.3	<5	7	<5	4.76	425	<10	170	72	108	<20	<20	13	2.60	0.93	0.71	0.01	0.04	9	7	2	23	9	<5	<10	0.25	<1
L-1+50E-3+75N		<.2	59	7	72	<1	48	21	0.2	<5	7	<5	4.07	688	<10	208	74	102	<20	<20	20	2.51	1.02	0.93	0.01	0.05	14	15	<2	18	8	9	<10	0.24	<1
L-1+50E-4+00N		<.2	22	8	62	<1	19	11	<.2	<5	7	<5	4.04	425	<10	197	58	101	<20	<20	16	2.17	0.44	0.50	<.01	0.04	9	4	4	15	9	<5	<10	0.20	<1
L-1+50E-4+25N		<.2	23	8	79	<1	33	15	0.3	<5	5	<5	3.80	443	<10	167	63	93	<20	<20	17	2.50	0.84	0.66	0.01	0.04	10	7	<2	18	8	<5	<10	0.19	<1
L-1+50E-4+50N		0.3	20	6	60	1	28	13	<.2	<5	<5	<5	3.89	458	<10	239	66	110	<20	<20	15	2.36	0.71	0.67	0.01	0.04	12	5	3	15	9	<5	<10	0.24	<1
L-1+50E-4+75N		0.3	25	6	69	<1	39	19	0.2	<5	6	<5	3.89	414	<10	161	65	92	<20	<20	15	2.74	0.93	0.89	0.02	0.04	11	8	<2	16	7	<5	<10	0.24	<1
L-1+50E-5+00N		0.2	38	6	66	<1	45	24	0.2	<5	6	<5	3.74	467	<10	167	73	98	<20	<20	14	2.78	1.07	0.98	0.02	0.04	12	11	<2	15	8	6	<10	0.26	<1
L-2+00E-B/LN		<.2	61	11	94	<1	43	21	0.3	<5	10	<5	4.10	804	<10	300	84	92	<20	<20	22	2.45	0.91	0.70	0.01	0.06	15	18	<2	20	7	11	<10	0.14	<1
L-2+00E-0+25N		0.3	28	4	78	<1	35	16	0.3	<5	<5	<5	4.28	342	<10	219	59	89	<20	<20	14	2.79	0.81	0.75	0.01	0.03	13	6	3	21	7	<5	<10	0.23	5
L-2+00E-0+50N		<.2	13	7	87	<1	23	11	0.3	<5	<5	<5	3.49	276	<10	210	55	82	<20	<20	18	2.63	0.55	0.51	0.01	0.04	9	5	4	18	7	<5	<10	0.17	<1
L-2+00E-0+75N		<.2	23	6	70	<1	34	16	0.2	<5	<5	<5	4.13	407	<10	170	56	92	<20	<20	14	2.45	0.80	0.77	0.02	0.03	12	6	<2	19	7	<5	<10	0.22	<1
L-2+00E-1+00N		<.2	16	7	62	<1	26	11	<.2	<5	<5	<5	3.48	273	<10	162	56	81	<20	<20	20	2.26	0.72	0.57	0.01	0.05	12	5	3	19	7	<5	<10	0.18	<1
L-2+00E-1+25N		0.2	30	<2	50	<1	37	25	0.2	<5	<5	<5	4.28	550	<10	168	67	127	<20	<20	7	2.99	0.94	1.18	0.02	0.03	13	8	<2	12	10	6	<10	0.38	5
L-2+00E-1+50N		0.2	20	7	63	<1	35	14	0.2	<5	6	<5	3.71	330	<10	192	64	93	<20	<20	19	2.40	0.82	0.73	0.02	0.05	13	7	2	18	8	<5	<10	0.22	<1
L-2+00E-1+75N		0.2	22	5	59	<1	37	17	0.3	<5	<5	<5	3.81	319	<10	147	60	92	<20	<20	14	2.78	0.79	0.77	0.02	0.04	12	7	<2	14	7	5	<10	0.26	3
L-2+00E-2+00N		0.2	18	7	75	<1	34	15	0.2	<5	<5	<5	3.69	266	<10	150	61	81	<20	<20	17	2.75	0.70	0.58	0.01	0.04	10	5	2	18	7	<5	<10	0.20	2
L-2+00E-2+25N		0.2	15	5	58	<1	31	15	<.2	<5	<5	<5	3.73	244	<10	156	56	95	<20	<20	14	2.48	0.66	0.66	0.01	0.03	10	5	3	18	8	<5	<10	0.23	2
L-2+00E-2+50N		<.2	24	7	82	<1	42	21	0.2	<5	5	<5	4.49	353	<10	174	67	92	<20	<20	15	3.12	0.84	0.60	0.01	0.05	10	7	<2	21	8	5	<10	0.23	6
L-2+00E-0+25S		0.2	58	9	92	<1	47	18	0.3	<5	8	<5	3.58	618	<10	329	77	83	<20	<20	23	2.31	0.91	0.97	0.01	0.06	21	21	<2	19	7	11	<10	0.17	<1

CLIENT: EUREKA RESOURCES, INC.
REPORT: V99-00744.0 (COMPLETE)

PROJECT: NONE GIVEN
DATE RECEIVED: 16-JUL-99 DATE PRINTED: 24-JUL-99

SAMPLE NUMBER	Ag	Cu	Pb	Zn	Mo	Ni	Co	Cd	Bi	As	Sb	Fe	Mn	Te	Ba	Cr	V	Sn	W	La	Al	Mg	Ca	Na	K	Sr	Y	Ga	Li	Nb	Sc	Ta	Ti	Zr
ELEMENT UNITS	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PCT	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PCT	PCT	PCT	PCT	PCT	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PCT	PPM
L-2+00E-0+50S	0.4	58	11	89	1	45	20	0.4	<5	7	<5	3.41	522	<10	486	77	88	<20	<20	22	2.67	0.88	0.87	0.01	0.06	20	19	3	22	7	7	<10	0.13	<1
L-2+00E-0+75S	0.3	48	8	80	1	43	17	0.3	<5	8	<5	3.71	515	<10	278	76	92	<20	<20	21	2.29	0.96	0.87	0.01	0.06	17	13	<2	18	7	9	<10	0.18	<1
L-2+00E-1+00S	<.2	97	11	95	<1	51	22	0.3	<5	10	<5	4.32	978	<10	271	92	92	<20	<20	27	2.35	1.00	0.81	0.01	0.07	21	25	2	18	7	13	<10	0.15	<1
L-2+00E-1+25S	<.2	93	9	101	<1	51	21	0.4	<5	9	<5	4.18	1042	<10	253	87	92	<20	<20	27	2.24	1.02	0.96	0.01	0.07	23	27	<2	17	7	12	<10	0.17	<1
L-2+00E-1+50S	<.2	84	10	89	1	47	19	0.3	<5	9	<5	4.48	745	<10	287	80	105	<20	<20	23	2.35	0.76	0.51	0.01	0.06	12	14	3	17	9	7	<10	0.14	<1
L-2+00E-1+75S	0.2	26	11	67	2	20	9	<.2	<5	8	<5	4.25	229	<10	250	55	113	<20	<20	18	1.60	0.34	0.43	<.01	0.05	12	4	6	12	10	<5	<10	0.17	<1
L-2+00E-2+00S	0.3	52	7	79	<1	34	15	0.3	<5	7	<5	4.64	442	<10	161	76	96	<20	<20	20	2.60	0.74	0.70	0.01	0.04	15	11	2	22	8	6	<10	0.19	<1
L-2+00E-2+25S	0.3	153	14	161	1	73	23	0.2	<5	10	<5	4.28	619	<10	312	104	96	<20	<20	30	3.35	0.92	0.83	0.01	0.11	23	19	3	28	8	11	<10	0.12	<1
L-2+00E-2+50S	0.5	40	5	69	<1	52	20	0.3	<5	6	<5	4.31	439	<10	208	75	106	<20	<20	11	2.81	1.09	0.99	0.02	0.05	14	8	<2	18	9	6	<10	0.29	1
L-2+00E-2+75S	0.4	28	11	80	1	29	12	0.2	<5	7	<5	4.44	303	<10	216	60	111	<20	<20	15	2.22	0.71	0.59	0.01	0.06	11	5	3	16	10	<5	<10	0.20	<1
L-2+00E-3+00S	0.7	16	10	44	<1	12	7	0.3	<5	<5	<5	2.29	269	<10	127	38	76	<20	<20	14	1.37	0.33	0.50	<.01	0.05	7	4	4	6	7	<5	<10	0.16	<1
L-2+00E-3+25S	0.2	17	6	96	<1	29	14	0.2	<5	6	<5	4.10	357	<10	161	65	99	<20	<20	14	2.54	0.69	0.57	0.01	0.04	9	5	2	19	8	<5	<10	0.22	<1
L-2+00E-3+50S	0.2	28	6	74	<1	38	17	<.2	<5	6	<5	4.08	602	<10	223	64	105	<20	<20	14	2.45	0.88	0.80	0.01	0.04	12	7	2	17	9	<5	<10	0.24	<1
L-2+00E-3+75S	0.3	23	7	74	<1	41	18	0.2	<5	7	<5	4.12	372	<10	167	63	95	<20	<20	15	2.87	0.95	0.79	0.01	0.04	11	7	<2	18	8	<5	<10	0.24	1
L-2+00E-4+00S	0.4	19	6	74	<1	32	14	0.2	<5	6	<5	3.98	426	<10	181	62	85	<20	<20	16	2.67	0.73	0.56	0.01	0.04	9	5	<2	19	7	<5	<10	0.19	<1
L-2+00E-4+25S	<.2	18	5	80	<1	29	14	0.2	<5	<5	<5	4.77	304	<10	162	70	95	<20	<20	14	2.67	0.73	0.58	0.01	0.04	9	5	<2	20	8	<5	<10	0.23	<1
L-2+00E-4+50S	0.2	17	7	68	<1	25	12	0.2	<5	<5	<5	4.40	315	<10	166	60	89	<20	<20	14	2.39	0.59	0.55	0.01	0.03	9	5	2	17	7	<5	<10	0.19	<1
L-2+00E-4+75S	0.2	16	7	65	1	20	12	0.3	<5	<5	<5	3.79	320	<10	156	57	92	<20	<20	14	2.24	0.50	0.51	<.01	0.03	9	4	4	15	8	<5	<10	0.20	<1
L-2+00E-5+00S	0.4	22	7	61	<1	27	13	0.3	<5	<5	<5	4.09	391	<10	145	55	99	<20	<20	11	2.00	0.69	0.65	0.01	0.04	9	5	3	15	9	<5	<10	0.22	<1
L-0+50E-0+25N	<.2	22	7	65	<1	23	11	<.2	<5	<5	<5	2.95	1049	<10	197	54	71	<20	<20	12	1.63	0.60	0.96	<.01	0.05	20	9	<2	13	6	6	<10	0.10	<1
L-0+50E-0+50N	<.2	23	8	71	<1	27	14	<.2	<5	<5	<5	3.03	734	<10	205	62	75	<20	<20	16	1.78	0.67	0.86	<.01	0.05	18	7	<2	14	6	6	<10	0.13	<1
L-0+50E-0+75N	<.2	39	7	64	<1	40	17	0.2	<5	<5	<5	3.49	542	<10	150	64	89	<20	<20	17	2.10	0.83	0.91	0.01	0.04	17	14	<2	16	7	8	<10	0.20	<1
L-0+50E-1+00N	<.2	37	7	64	<1	34	17	0.2	<5	<5	<5	3.25	679	<10	200	60	85	<20	<20	14	1.94	0.76	0.97	0.01	0.05	19	12	<2	13	7	8	<10	0.17	<1
L-0+50E-1+25N	<.2	112	18	143	<1	126	32	<.2	<5	11	<5	5.49	1098	<10	411	118	125	<20	<20	27	4.22	1.27	1.04	0.02	0.12	29	29	3	42	8	19	<10	0.15	<1
L-0+50E-1+50N	0.3	9	7	46	<1	16	9	<.2	<5	<5	<5	2.47	197	<10	159	40	64	<20	<20	19	1.69	0.42	0.41	<.01	0.04	8	4	3	13	5	<5	<10	0.13	<1
L-0+50E-1+75N	<.2	27	8	66	<1	36	14	0.2	<5	5	<5	3.80	355	<10	133	64	74	<20	<20	19	2.22	0.80	0.45	0.01	0.05	10	6	<2	18	6	<5	<10	0.16	2
L-0+50E-2+00N	<.2	14	8	59	<1	27	12	0.2	<5	<5	<5	4.26	233	<10	116	63	89	<20	<20	15	2.57	0.59	0.41	0.01	0.03	7	4	2	19	8	<5	<10	0.17	2
L-0+50E-2+25N	<.2	11	10	69	<1	24	11	<.2	<5	<5	<5	4.22	201	<10	125	59	91	<20	<20	14	2.60	0.48	0.41	<.01	0.03	7	4	4	17	8	<5	<10	0.19	2
L-0+50E-2+50N	<.2	12	8	55	<1	19	10	<.2	<5	<5	<5	3.91	183	<10	104	56	82	<20	<20	13	2.64	0.38	0.39	<.01	0.02	6	3	4	18	7	<5	<10	0.17	2
L-3+00E-B/LN	<.2	32	7	66	<1	36	13	<.2	<5	<5	<5	4.04	317	<10	236	67	98	<20	<20	14	2.14	0.74	0.76	0.01	0.05	16	7	3	19	8	<5	<10	0.20	<1

Intertek Testing Services
Bondar Clegg

Geochemical Lab Report

CLIENT: EUREKA RESOURCES, INC. — PROJECT: NONE GIVEN

REPORT: V99-00744.0 (COMPLETE) — DATE RECEIVED: 16-JUL-99 — DATE PRINTED: 24-JUL-99 —

SAMPLE NUMBER	Ag	Cu	Pb	Zn	Mo	Ni	Co	Cd	Bi	As	Sb	Fe	Mn	Te	Ba	Cr	V	Sn	W	La	Al	Mg	Ca	Na	K	Sr	Y	Ga	Li	Nb	Sc	Ta	Ti	Zr
ELEMENT UNITS	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PCT	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PCT	PCT	PCT	PCT	PCT	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PCT	PPM
L-3+00E-0+25N	0.3	77	13	83	<1	51	19	<.2	<5	7	<5	4.04	520	<10	246	89	95	<20	<20	19	2.51	0.74	0.75	0.01	0.06	18	17	3	20	8	10	<10	0.13	<1
L-3+00E-0+50N	0.2	90	14	89	<1	57	19	0.2	<5	5	<5	3.25	385	<10	256	88	90	<20	<20	25	2.33	0.95	1.13	0.02	0.06	24	27	<2	16	8	15	<10	0.17	4
L-3+00E-0+75N	0.3	120	14	89	<1	62	13	0.2	<5	5	<5	2.98	336	<10	286	100	79	<20	<20	28	2.78	0.87	1.09	0.01	0.06	26	31	3	18	7	17	<10	0.13	2
L-3+00E-1+50N	<.2	38	11	81	2	44	15	<.2	<5	<5	<5	3.25	617	<10	309	86	73	<20	<20	19	2.64	0.79	0.90	0.01	0.06	22	18	3	18	6	10	<10	0.11	<1
L-3+00E-1+75N	<.2	27	7	63	<1	37	15	<.2	<5	<5	<5	3.28	394	<10	168	58	70	<20	<20	17	1.79	0.84	0.87	0.01	0.05	17	9	<2	15	6	5	<10	0.18	1
L-3+00E-2+25N	<.2	12	5	58	<1	23	13	<.2	<5	<5	<5	4.72	235	<10	107	62	111	<20	<20	8	2.10	0.53	0.51	0.01	0.03	7	3	2	18	9	<5	<10	0.27	2
L-3+00E-2+50N	<.2	20	8	66	1	34	13	<.2	<5	<5	<5	4.49	299	<10	121	67	73	<20	<20	15	2.35	0.80	0.43	0.01	0.04	8	4	<2	21	6	<5	<10	0.17	1
L-3+00E-2+00N	0.2	12	5	59	<1	17	10	<.2	<5	<5	<5	4.66	212	<10	109	50	111	<20	<20	8	1.67	0.39	0.48	<.01	0.03	7	3	5	11	10	<5	<10	0.25	<1
L-3+00E-0+25S	0.3	131	15	125	<1	94	21	0.2	<5	9	<5	4.82	1141	<10	351	109	105	<20	<20	26	3.31	0.92	1.19	0.01	0.08	30	34	3	21	8	16	<10	0.13	<1
L-3+00E-0+50S	0.4	61	5	79	<1	45	17	<.2	<5	5	<5	4.67	537	<10	188	75	107	<20	<20	17	2.40	0.84	1.01	0.01	0.04	20	20	3	17	9	8	<10	0.25	<1
L-3+00E-0+75S	<.2	51	8	61	<1	54	21	<.2	<5	7	<5	3.86	577	<10	188	70	86	<20	<20	16	2.25	1.02	0.90	0.01	0.04	14	15	<2	16	7	7	<10	0.22	1
L-3+00E-1+00S	0.3	27	6	74	<1	30	14	<.2	<5	<5	<5	4.13	366	<10	146	61	105	<20	<20	10	2.39	0.69	0.71	0.01	0.03	10	6	2	14	9	<5	<10	0.25	<1
L-3+00E-1+25S	0.3	114	20	160	<1	121	29	0.2	<5	9	<5	5.34	1119	<10	358	120	110	<20	<20	23	3.79	1.15	1.06	0.01	0.10	26	27	2	26	8	16	<10	0.14	<1
L-3+00E-1+50S	0.6	144	21	143	<1	118	26	0.3	<5	11	<5	4.87	1329	<10	405	125	95	<20	<20	36	3.63	0.99	1.33	0.01	0.10	36	46	<2	23	7	21	<10	0.14	<1
L-3+00E-1+75S	0.4	149	21	155	<1	132	29	0.2	<5	11	<5	5.16	1328	<10	361	119	103	<20	<20	33	3.71	1.03	1.05	0.01	0.09	27	36	2	25	8	17	<10	0.14	<1
L-3+00E-2+00S	0.3	53	8	72	<1	33	13	0.2	<5	7	<5	4.62	427	<10	205	70	117	<20	<20	14	2.32	0.58	0.55	0.01	0.03	9	8	5	15	10	5	<10	0.24	<1
L-3+00E-2+25S	<.2	111	14	107	<1	82	26	<.2	<5	14	<5	5.15	983	<10	246	94	107	<20	<20	25	2.92	1.08	1.17	0.01	0.07	24	32	<2	21	9	12	<10	0.19	<1
L-3+00E-2+50S	<.2	32	9	119	<1	30	18	<.2	<5	<5	<5	4.75	858	<10	170	71	99	<20	<20	12	2.25	0.65	0.57	<.01	0.05	9	5	3	17	8	<5	<10	0.18	<1
L-3+00E-2+75S	0.6	23	6	73	<1	28	12	<.2	<5	<5	<5	4.88	341	<10	146	64	90	<20	<20	10	2.42	0.63	0.61	0.01	0.03	8	5	<2	18	8	<5	<10	0.19	<1
L-3+00E-3+00S	0.4	33	11	86	<1	38	18	<.2	<5	6	<5	5.15	676	<10	181	69	109	<20	<20	12	2.48	0.84	0.69	0.01	0.04	9	6	3	16	9	<5	<10	0.20	<1
L-3+00E-3+25S	<.2	20	7	98	<1	39	15	<.2	<5	5	<5	4.44	441	<10	182	68	81	<20	<20	13	2.53	0.98	0.66	0.01	0.04	8	7	<2	24	7	<5	<10	0.18	<1
L-3+00E-3+50S	0.4	26	5	75	<1	44	18	<.2	<5	5	<5	5.33	504	<10	169	80	110	<20	<20	9	2.88	1.18	0.73	0.01	0.03	7	7	<2	27	9	5	<10	0.24	<1
L-3+00E-3+75S	<.2	16	6	142	<1	26	15	<.2	<5	<5	<5	4.10	599	<10	227	65	81	<20	<20	14	2.45	0.56	0.43	<.01	0.04	7	4	3	20	7	<5	<10	0.16	<1
L-3+00E-4+00S	<.2	28	5	70	<1	36	17	0.2	<5	<5	<5	4.03	512	<10	176	69	123	<20	<20	12	2.97	0.97	0.88	0.01	0.05	12	7	2	19	10	5	<10	0.27	<1
L-3+00E-4+25S	0.3	32	3	107	<1	46	18	<.2	<5	6	<5	4.34	486	<10	213	79	114	<20	<20	12	3.02	1.13	0.89	0.01	0.04	13	7	<2	26	9	5	<10	0.24	<1
L-3+00E-4+50S	<.2	37	6	86	<1	37	20	<.2	<5	<5	<5	3.95	1068	<10	239	81	114	<20	<20	29	2.61	0.93	0.84	0.01	0.05	18	20	2	19	9	8	<10	0.23	<1
L-3+00E-4+75S	0.3	21	3	72	<1	28	15	<.2	<5	<5	<5	4.67	459	<10	189	83	134	<20	<20	12	2.84	0.81	0.79	0.01	0.04	12	5	4	17	11	<5	<10	0.28	<1
L-3+00E-5+00S	<.2	31	8	97	<1	36	11	0.3	<5	8	<5	4.53	351	<10	558	65	89	<20	<20	21	2.56	0.80	0.49	0.01	0.11	10	5	2	22	7	<5	<10	0.10	<1
L-4+00E-0+25N	0.6	41	5	65	<1	49	22	0.3	<5	7	<5	4.20	437	<10	222	72	100	<20	<20	13	3.70	0.97	0.98	0.02	0.04	15	13	<2	18	8	7	<10	0.26	2
L-4+00E-0+50N	0.3	62	8	89	<1	49	18	0.3	<5	11	<5	4.68	446	<10	234	79	110	<20	<20	15	3.31	0.97	0.76	0.02	0.06	14	7	<2	26	9	6	<10	0.24	<1

Intertek Testing Services

Bondar Clegg

Geochemical Lab Report

CLIENT: EUREKA RESOURCES, INC. PROJECT: NONE GIVEN

REPORT: V99-00744.0 (COMPLETE) DATE RECEIVED: 16-JUL-99 DATE PRINTED: 24-JUL-99

SAMPLE NUMBER	ELEMENT UNITS	Ag PPM	Cu PPM	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	Sb PPM	Fe PCT	Mn PPM	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	W PPM	La PPM	Al PCT	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM	Ga PPM	Li PPM	Nb PPM	Sc PPM	Ta PPM	Ti PCT	Zr PPM
L-4+00E-1+00N		<.2	30	7	69	<1	38	23	0.3	<5	<5	<5	3.19	742	<10	240	71	100	<20	<20	17	2.67	0.99	1.18	0.02	0.06	22	11	<2	16	8	8	<10	0.26	<1
L-4+00E-1+50N		<.2	23	5	80	1	37	16	<.2	<5	5	<5	4.48	313	<10	211	63	93	<20	<20	18	3.27	0.79	0.50	0.01	0.05	10	5	<2	26	7	<5	<10	0.20	2
L-4+00E-1+75N		0.3	18	4	49	<1	20	14	<.2	<5	<5	<5	4.94	308	<10	126	53	158	<20	<20	9	2.39	0.51	0.69	0.01	0.07	9	4	5	11	14	<5	<10	0.34	<1
L-4+00E-2+00N		<.2	21	3	82	<1	43	21	<.2	<5	6	<5	4.79	365	<10	239	74	125	<20	<20	10	3.60	0.81	0.67	0.01	0.04	10	5	3	21	10	<5	<10	0.30	5
L-4+00E-2+25N		<.2	16	7	84	<1	33	16	<.2	<5	<5	<5	3.63	251	<10	171	58	94	<20	<20	15	3.31	0.62	0.50	0.01	0.04	10	4	3	20	8	<5	<10	0.20	<1
L-4+00E-2+50N		<.2	11	9	85	<1	20	12	0.2	<5	<5	<5	2.73	309	<10	167	48	81	<20	<20	18	2.81	0.43	0.44	0.01	0.04	9	4	5	18	7	<5	<10	0.20	<1
L-4+00E-2+75N		0.3	12	7	63	<1	15	10	0.2	<5	<5	<5	3.51	358	<10	152	50	114	<20	<20	14	2.55	0.43	0.57	0.01	0.04	10	4	7	13	9	<5	<10	0.25	<1
L-4+00E-3+00N		<.2	19	3	84	<1	33	17	0.2	<5	<5	<5	4.26	334	<10	144	68	102	<20	<20	12	3.59	0.73	0.69	0.02	0.04	10	6	<2	19	8	5	<10	0.26	3
L-4+00E-B/LS		<.2	31	4	61	<1	40	23	0.3	<5	7	<5	3.91	567	<10	155	64	108	<20	<20	11	3.20	1.04	1.00	0.02	0.05	15	9	<2	16	9	6	<10	0.32	3
L-4+00E-0+25S		0.3	20	7	91	<1	25	13	0.2	<5	<5	<5	3.97	353	<10	131	58	92	<20	<20	18	2.70	0.65	0.55	0.01	0.07	12	5	2	19	8	<5	<10	0.19	<1
L-4+00E-0+50S		0.3	34	5	78	<1	37	22	0.3	<5	6	<5	3.80	816	<10	179	63	107	<20	<20	13	2.71	1.01	1.28	0.02	0.06	23	12	<2	15	9	6	<10	0.27	<1
L-4+00E-0+75S		<.2	22	8	88	<1	32	15	0.4	<5	7	<5	4.24	367	<10	144	58	86	<20	<20	15	2.92	0.77	0.62	0.01	0.05	11	7	<2	19	7	<5	<10	0.19	<1
L-4+00E-1+00S		0.9	24	12	90	<1	26	13	0.4	<5	6	<5	4.01	469	<10	174	48	103	<20	<20	15	2.16	0.72	0.71	0.01	0.07	12	5	2	13	8	<5	<10	0.17	<1
L-4+00E-1+25S		0.4	21	3	82	<1	29	14	0.5	<5	<5	<5	4.26	361	<10	124	60	102	<20	<20	9	2.95	0.84	0.85	0.01	0.04	11	6	<2	19	9	<5	<10	0.24	<1
L-4+00E-1+50S		0.9	28	7	89	<1	30	15	0.3	<5	6	<5	4.35	803	<10	274	62	121	<20	<20	13	2.62	0.79	0.78	0.01	0.06	12	6	<2	19	10	<5	<10	0.21	<1
L-4+00E-1+75S		0.3	19	7	79	<1	23	12	0.3	<5	<5	<5	4.16	459	<10	187	57	117	<20	<20	14	2.61	0.60	0.59	<.01	0.04	9	5	4	17	9	<5	<10	0.20	<1
L-4+00E-2+00S		0.2	15	6	104	<1	23	13	0.3	<5	<5	<5	4.98	704	<10	277	66	141	<20	<20	15	2.73	0.63	0.64	<.01	0.07	11	4	5	16	12	<5	<10	0.23	<1
L-4+00E-2+25S		0.3	11	13	48	<1	11	5	<.2	<5	<5	<5	2.10	211	<10	252	33	62	<20	<20	29	1.66	0.25	0.43	<.01	0.06	15	4	5	7	6	<5	<10	0.08	<1
L-4+00E-2+50S		0.3	27	4	66	<1	34	18	0.3	<5	<5	<5	3.90	538	<10	178	64	123	<20	<20	14	2.87	0.98	1.17	0.02	0.08	22	9	3	16	10	6	<10	0.29	<1
L-4+00E-2+75S		0.5	29	3	71	<1	40	20	0.3	<5	<5	<5	4.47	491	<10	191	71	128	<20	<20	14	3.04	1.17	1.21	0.02	0.06	21	10	3	18	10	6	<10	0.33	<1
L-4+00E-3+00S		<.2	27	4	90	<1	34	19	0.3	<5	<5	<5	4.57	518	<10	162	74	119	<20	<20	13	3.03	1.01	0.91	0.02	0.05	16	10	3	19	10	6	<10	0.33	<1
L-4+00E-3+25S		<.2	30	3	68	<1	38	21	<.2	<5	<5	<5	3.73	503	<10	164	62	109	<20	<20	13	2.78	1.06	1.07	0.02	0.05	18	10	<2	16	9	6	<10	0.31	1
L-4+00E-3+50S		<.2	30	4	65	<1	42	21	0.2	<5	<5	<5	3.78	503	<10	190	64	109	<20	<20	13	2.92	1.12	0.97	0.02	0.04	13	9	<2	17	9	5	<10	0.30	1
L-4+00E-3+75S		<.2	38	4	64	<1	54	23	0.2	<5	<5	<5	3.99	690	<10	192	73	118	<20	<20	13	3.12	1.36	1.29	0.02	0.05	21	13	<2	18	10	7	<10	0.32	<1
L-4+00E-4+00S		0.3	33	3	70	<1	49	21	<.2	<5	<5	<5	3.53	576	<10	180	70	105	<20	<20	14	2.86	1.16	1.15	0.02	0.04	20	14	<2	18	8	7	<10	0.26	<1
L-4+00E-4+25S		0.3	26	2	61	<1	31	17	0.3	<5	<5	<5	4.89	357	<10	158	67	117	<20	<20	12	3.08	0.88	0.91	0.01	0.04	14	12	<2	18	10	6	<10	0.31	<1
L-4+00E-4+50S		0.2	25	5	53	<1	24	15	0.3	<5	<5	<5	3.65	481	<10	205	64	130	<20	<20	12	2.56	0.61	0.75	0.01	0.04	12	7	4	11	11	<5	<10	0.28	<1
L-4+00E-4+75S		0.2	41	5	54	<1	41	17	<.2	<5	<5	<5	3.56	326	<10	189	75	103	<20	<20	18	3.05	0.78	0.77	0.01	0.04	17	13	3	19	9	7	<10	0.23	<1
L-4+00E-5+00S		<.2	42	4	71	<1	51	23	<.2	<5	<5	<5	3.92	731	<10	184	88	116	<20	<20	19	2.86	1.19	1.20	0.01	0.06	20	18	<2	18	9	9	<10	0.28	<1

Intertek Testing Services
Bondar Clegg

Geochemical Lab Report

CLIENT: EUREKA RESOURCES, INC.
REPORT: V99-00745.0 (COMPLETE)

PROJECT: NONE GIVEN
DATE RECEIVED: 17-JUL-99   DATE PRINTED: 21-JUL-99

SAMPLE NUMBER	ELEMENT UNITS	Ag PPM	Cu PPM	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	Sb PPM	Fe PCT	Mn PPM	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	W PPM	La PPM	Al PCT	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM	Ga PPM	Li PPM	Nb PPM	Sc PPM	Ta PPM	Ti PCT	Zr PPM
L-A1+75N		0.2	42	8	64	<1	46	20	0.3	<5	9	<5	3.65	700	<10	323	56	82	<20	<20	17	1.99	1.03	0.99	0.02	0.05	19	12	<2	14	7	7	<10	0.23	4
L-A2+00N		<.2	56	25	101	<1	48	20	0.2	<5	9	<5	3.59	625	<10	278	65	83	<20	<20	20	2.08	1.01	1.00	0.02	0.07	20	13	<2	14	6	8	<10	0.23	7
L-A2+50N		<.2	35	5	55	<1	43	21	0.2	<5	<5	<5	3.52	1141	<10	253	65	96	<20	<20	13	2.31	0.98	1.23	0.03	0.05	20	14	<2	13	7	10	<10	0.29	4
L-A2+75N		<.2	48	5	53	<1	38	20	<.2	<5	5	<5	3.40	643	<10	231	47	96	<20	<20	13	2.19	0.96	1.21	0.02	0.04	18	12	<2	11	8	7	<10	0.31	8
L-A3+00N		<.2	65	8	73	<1	49	24	<.2	<5	7	<5	4.12	832	<10	300	61	103	<20	<20	19	2.41	1.09	1.22	0.03	0.07	22	17	<2	14	8	11	<10	0.30	9
L-A3+25N		<.2	59	10	75	<1	44	22	<.2	<5	7	<5	3.99	771	<10	281	55	93	<20	<20	19	2.19	1.05	1.12	0.02	0.07	23	14	<2	14	7	9	<10	0.25	10
L-A0+25N		<.2	60	8	60	<1	60	26	<.2	<5	9	<5	4.11	795	<10	264	72	100	<20	<20	19	2.53	1.34	1.19	0.02	0.06	22	15	<2	17	7	8	<10	0.27	4
L-A0+50N		<.2	47	7	57	<1	60	24	<.2	<5	10	<5	3.68	726	<10	288	62	79	<20	<20	16	2.08	1.22	0.90	0.02	0.05	16	11	<2	17	6	6	<10	0.20	3
L-A0+75N		<.2	50	11	68	<1	54	23	<.2	<5	8	<5	3.74	843	<10	359	63	88	<20	<20	15	2.14	1.17	1.05	0.02	0.05	18	13	<2	15	7	7	<10	0.25	1
L-A1+00N		<.2	63	9	75	<1	63	25	0.2	<5	11	<5	4.23	847	<10	329	68	89	<20	<20	17	2.32	1.23	0.93	0.02	0.06	19	11	<2	16	7	8	<10	0.22	5
L-A1+25N		<.2	64	9	67	<1	55	22	<.2	<5	10	<5	3.90	584	<10	290	68	92	<20	<20	17	2.21	1.17	1.08	0.02	0.05	20	14	<2	14	7	9	<10	0.25	8
L-A1+50N		<.2	56	6	73	<1	51	22	0.2	<5	6	<5	4.26	604	<10	262	71	102	<20	<20	13	2.53	1.19	1.28	0.03	0.08	24	15	<2	14	8	11	<10	0.27	10
L-A0+00S		<.2	61	5	71	<1	52	24	0.2	<5	6	<5	4.56	774	<10	265	67	117	<20	<20	10	2.94	1.48	1.56	0.04	0.09	28	15	3	14	9	10	<10	0.30	9
L-A0+25S		<.2	63	7	62	<1	52	22	<.2	<5	8	<5	3.76	726	<10	240	71	94	<20	<20	17	2.25	1.20	1.10	0.02	0.05	20	15	<2	16	7	9	<10	0.25	3
L-A0+50S		0.2	56	4	57	<1	54	23	<.2	<5	8	<5	3.96	632	<10	255	79	100	<20	<20	15	2.42	1.46	1.25	0.02	0.05	20	16	<2	18	7	9	<10	0.26	4
L-A0+75S		<.2	48	7	59	<1	62	26	<.2	<5	9	<5	4.37	707	<10	213	86	106	<20	<20	16	2.72	1.64	1.22	0.03	0.07	17	15	<2	21	8	8	<10	0.27	2
L-A1+00S		<.2	65	4	65	<1	54	24	<.2	<5	10	<5	4.46	792	<10	267	81	116	<20	<20	14	2.90	1.41	1.52	0.04	0.08	23	18	<2	13	9	12	<10	0.32	6
L-A1+25S		<.2	64	12	92	<1	51	22	0.2	<5	7	<5	4.31	739	<10	222	59	88	<20	<20	16	2.51	1.13	1.03	0.03	0.13	24	15	<2	13	6	9	<10	0.22	11
L-A1+50SA		<.2	81	5	62	<1	56	25	<.2	<5	6	<5	4.46	828	<10	247	78	108	<20	<20	14	2.74	1.51	1.15	0.02	0.07	18	19	<2	16	8	12	<10	0.27	7
L-A1+50SB		<.2	74	7	57	<1	66	25	<.2	<5	5	<5	3.59	714	<10	167	62	89	<20	<20	13	2.43	1.35	0.99	0.02	0.06	14	10	<2	16	7	5	<10	0.25	3
L-A1+75S		<.2	48	6	52	<1	49	19	<.2	<5	6	<5	3.32	1040	<10	269	58	71	<20	<20	17	2.27	1.42	0.61	0.02	0.07	9	8	<2	19	6	<5	<10	0.16	2
M-1-2		<.2	138	<2	63	<1	468	85	<.2	<5	<5	<5	7.14	852	<10	34	570	84	<20	<20	3	4.08	6.56	0.55	<.01	<.01	8	8	<2	20	4	<5	<10	0.17	<1
M-3-2		<.2	101	3	59	<1	320	56	<.2	<5	11	<5	5.66	917	<10	67	311	94	<20	<20	7	3.89	4.64	0.73	0.02	0.03	9	10	<2	37	6	<5	<10	0.24	<1
M-4-2		<.2	172	6	73	<1	251	51	<.2	<5	25	<5	5.53	1135	<10	131	250	99	<20	<20	14	3.36	3.79	0.64	0.01	0.06	11	17	<2	25	7	12	<10	0.19	6
M-5-2		<.2	62	<2	66	<1	47	24	<.2	<5	<5	<5	4.36	801	<10	219	66	113	<20	<20	9	2.84	1.37	1.47	0.04	0.08	22	15	<2	12	8	10	<10	0.29	10
M-6-1		<.2	90	12	77	<1	46	25	0.2	<5	8	<5	4.03	988	<10	329	54	92	<20	<20	13	2.22	1.21	1.07	0.03	0.07	20	16	<2	12	7	10	<10	0.24	10
M-9		<.2	61	6	66	<1	50	22	<.2	<5	7	<5	4.13	1029	<10	389	62	98	<20	<20	13	2.43	1.14	0.97	0.02	0.08	17	13	<2	12	7	10	<10	0.24	9
M-10		<.2	40	8	62	<1	49	21	<.2	<5	6	<5	3.60	652	<10	194	55	85	<20	<20	16	2.32	1.04	0.92	0.02	0.06	15	9	<2	13	7	<5	<10	0.23	1
M-11		<.2	39	7	59	<1	45	21	<.2	<5	<5	<5	3.58	691	<10	202	51	85	<20	<20	14	2.27	1.05	0.90	0.02	0.06	15	9	<2	13	7	<5	<10	0.23	2
M-12		<.2	49	5	60	<1	47	23	<.2	<5	<5	<5	4.16	742	<10	270	60	111	<20	<20	10	2.80	1.21	1.21	0.03	0.07	16	12	<2	12	8	8	<10	0.32	11

ITS Intertek Testing Services
Bondar Clegg

Geochemical Lab Report

CLIENT: EUREKA RESOURCES, INC.
REPORT: V99-00745.0 (COMPLETE)

PROJECT: NONE GIVEN

DATE RECEIVED: 17-JUL-99 DATE PRINTED: 21-JUL-99

SAMPLE NUMBER	ELEMENT UNITS	Ag PPM	Cu PPM	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	Sb PPM	Fe PCT	Mn PPM	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	W PPM	La PPM	Al PCT	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM	Ga PPM	Li PPM	Nb PPM	Sc PPM	Ta PPM	Ti PCT	Zr PPM
M-13		<.2	44	6	60	<1	49	23	<.2	<5	<5	<5	3.86	732	<10	198	58	101	<20	<20	11	2.65	1.18	1.13	0.03	0.07	15	10	<2	12	8	6	<10	0.29	7
M-14		<.2	44	<2	55	<1	45	23	<.2	<5	<5	<5	3.96	726	<10	219	58	114	<20	<20	8	2.85	1.17	1.31	0.03	0.06	16	11	<2	10	9	7	<10	0.35	8
M-15		<.2	36	4	51	<1	46	23	0.2	<5	<5	<5	3.60	686	<10	174	58	103	<20	<20	10	2.54	1.13	1.20	0.03	0.06	15	10	<2	11	8	6	<10	0.31	6
M-16		<.2	33	3	58	<1	44	24	<.2	<5	<5	<5	3.79	707	<10	243	50	104	<20	<20	11	2.56	1.10	1.23	0.03	0.06	16	10	<2	12	8	6	<10	0.33	6
M-17		<.2	55	6	65	<1	50	23	<.2	<5	6	<5	4.27	738	<10	280	67	102	<20	<20	14	2.67	1.18	1.05	0.03	0.08	19	12	<2	14	8	10	<10	0.26	8
M-18		<.2	51	6	62	<1	48	22	<.2	<5	6	<5	4.00	715	<10	257	60	96	<20	<20	12	2.41	1.09	1.06	0.03	0.06	18	12	<2	12	7	9	<10	0.25	8
M-19		<.2	48	8	61	<1	45	22	<.2	<5	7	<5	3.74	882	<10	207	59	90	<20	<20	15	2.32	1.05	0.78	0.02	0.06	13	8	<2	13	7	6	<10	0.23	5
M-20		<.2	35	7	57	<1	39	18	<.2	<5	5	<5	3.18	568	<10	140	48	75	<20	<20	14	1.95	0.83	0.72	0.01	0.05	13	7	<2	11	6	<5	<10	0.20	2
M-21		<.2	44	10	63	<1	43	20	<.2	<5	7	<5	3.68	669	<10	231	62	80	<20	<20	17	2.02	0.97	0.85	0.02	0.06	18	13	<2	13	6	9	<10	0.19	6
M-22		<.2	62	<2	57	<1	81	33	<.2	<5	<5	<5	4.86	733	<10	184	78	115	<20	<20	9	3.18	1.88	1.37	0.02	0.05	15	12	<2	22	8	8	<10	0.30	3
M-23		<.2	44	7	58	<1	46	21	<.2	<5	6	<5	3.73	687	<10	209	62	91	<20	<20	14	2.22	1.03	1.04	0.03	0.07	18	13	<2	13	7	9	<10	0.25	9
M-24		<.2	43	7	57	<1	42	19	<.2	<5	6	<5	3.45	637	<10	180	55	78	<20	<20	12	1.91	0.94	0.82	0.02	0.05	15	12	<2	11	6	8	<10	0.19	6
M-25		<.2	34	7	60	<1	40	18	0.2	<5	7	<5	3.44	591	<10	143	55	76	<20	<20	13	1.92	0.91	0.74	0.02	0.06	14	8	<2	13	6	<5	<10	0.20	3
M-26		<.2	36	7	66	<1	39	16	0.4	<5	5	<5	3.45	555	<10	165	44	69	<20	<20	14	1.65	0.85	0.73	0.01	0.05	18	10	<2	13	5	7	<10	0.16	7
M-27		<.2	34	7	64	<1	38	15	0.2	<5	7	<5	3.39	530	<10	157	42	66	<20	<20	14	1.58	0.81	0.68	0.02	0.05	18	10	<2	13	5	7	<10	0.15	7
M-28		<.2	31	7	58	<1	35	16	<.2	<5	5	<5	3.37	524	<10	168	43	74	<20	<20	15	1.74	0.81	0.76	0.02	0.05	18	11	<2	12	5	7	<10	0.19	9
L-0+75E-0+25N		<.2	37	4	58	<1	45	25	<.2	<5	5	<5	4.12	809	<10	160	56	101	<20	<20	8	2.42	1.28	1.29	0.03	0.05	16	12	<2	12	8	6	<10	0.30	4
L-0+75E-0+50N		<.2	47	5	57	<1	46	21	<.2	<5	5	<5	3.48	731	<10	217	47	84	<20	<20	9	2.21	1.04	0.95	0.02	0.04	13	9	<2	10	6	5	<10	0.24	3
L-0+75E-0+75N		<.2	41	8	65	<1	42	18	<.2	<5	6	<5	3.62	624	<10	198	54	81	<20	<20	15	1.96	0.92	0.82	0.02	0.07	18	10	<2	12	6	7	<10	0.20	7
L-0+75E-0+00S		<.2	46	6	62	<1	42	19	<.2	<5	<5	<5	3.63	610	<10	198	59	86	<20	<20	13	1.98	0.99	1.03	0.02	0.06	19	12	<2	12	6	9	<10	0.22	6
L-0+75E-0+25S		<.2	38	5	62	<1	46	22	<.2	<5	7	<5	4.05	1205	<10	204	63	91	<20	<20	10	2.15	1.23	1.09	0.02	0.05	16	12	<2	13	7	8	<10	0.22	4
L-0+25E 0+00N		<.2	57	7	59	<1	39	19	<.2	<5	<5	<5	3.39	833	<10	364	47	80	<20	<20	11	1.86	1.00	0.90	0.02	0.04	14	10	<2	11	6	6	<10	0.21	6
L-0+25E 0+25N		0.2	46	6	61	<1	43	21	<.2	<5	7	<5	3.90	671	<10	239	58	93	<20	<20	10	2.40	1.06	0.93	0.02	0.05	14	9	<2	11	7	8	<10	0.23	4
L-0+25E 0+50N		<.2	31	5	55	<1	41	21	<.2	<5	5	<5	3.48	627	<10	145	50	89	<20	<20	11	2.20	0.98	0.95	0.02	0.04	13	8	<2	11	7	<5	<10	0.25	3
L-0+25S-0+25S		<.2	25	5	56	<1	36	18	<.2	<5	5	<5	3.77	512	<10	168	52	97	<20	<20	7	2.02	1.20	0.96	0.02	0.04	14	11	<2	12	7	7	<10	0.21	2

ITS Intertek Testing Services
Bondar Clegg

Geochemical Lab Report

CLIENT: EUREKA RESOURCES, INC.
REPORT: V99-00805.0 (COMPLETE)

PROJECT: LOTTIE
DATE RECEIVED: 13-JUL-99 DATE PRINTED: 30-JUL-99 PAGE 1A(1/ 4)

SAMPLE NUMBER	ELEMENT UNITS	Au30 PPB	Au Wt1 GM	Ag PPM	Cu PPM	Cu PCT	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	Sb PPM	Fe PCT
LOTTIE 1		435	15.22	13.8	>10000	10.96	179	343	581	18	644	1.0	53	604	16	>10.00

SAMPLE NUMBER	Fe PCT	Mn PPM	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	W PPM	La PPM	Al PCT	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM	Ga PPM	Li PPM	Nb PPM	Sc PPM	Ta PPM	Ti PCT
LOTTIE 1	27.27	103	19	8	<1	56	76	<20	2	0.53	0.43	0.16	<.01	0.04	10	2	14	6	<1	<5	<10	0.03

13-Nov 98

ECO-TECH LABORATORIES LTD.
10041 East Trans Canada Highway
KAMLOOPS, B.C.
V2C 6T4

Phone: 604-573-5700
Fax : 604-573-4557

ICP CERTIFICATE OF ANALYSIS AK 98-686

GEOQUEST CONSULTING LTD.
8055 ASPEN ROAD
VERNON, B.C.
V1B 3M9

ATTENTION: WARNER GRUENWALD

No. of samples: 183
Sample type: Soil
PROJECT #: 74
SHIPMENT #: None Given
Samples submitted by: W. Gruenwald

Values in ppm unless otherwise reported

Et #.	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
1	B/L 0+50 W	0.2	2.36	5	185	10	0.94	<1	15	52	25	4.50	<10	0.71	339	<1	0.01	27	460	18	<5	<20	11	0.15	<10	75	<10	<1	77
2	B/L 1+50 W	<0.2	2.26	5	200	20	0.62	<1	23	58	26	4.49	<10	0.92	546	<1	0.02	35	460	10	<5	<20	11	0.26	<10	109	<10	<1	53
3	B/L 2+00 W	<0.2	2.38	<5	165	15	0.83	<1	24	49	29	3.69	<10	0.86	489	<1	0.02	34	520	10	<5	<20	12	0.29	<10	91	<10	2	48
4	B/L 2+50 W	<0.2	1.75	<5	135	15	0.57	<1	16	48	18	3.24	<10	0.51	637	<1	0.01	17	410	12	<5	<20	10	0.18	<10	93	<10	2	47
5	B/L 3+50 W	<0.2	2.66	<5	230	15	0.51	<1	16	73	31	4.42	<10	0.85	460	<1	0.01	36	520	14	<5	<20	9	0.20	<10	108	<10	<1	89
6	B/L 4+00 W	<0.2	2.35	<5	210	15	0.56	<1	14	55	17	4.15	<10	0.62	282	<1	0.01	24	470	10	<5	<20	8	0.23	<10	89	<10	<1	72
7	B/L 4+50 W	<0.2	2.10	<5	140	15	0.52	<1	13	49	18	4.34	<10	0.54	274	<1	0.01	18	480	12	<5	<20	10	0.24	<10	104	<10	<1	62
8	B/L 5+50 W	<0.2	2.83	10	190	15	0.59	<1	16	58	27	4.13	<10	0.84	358	<1	0.01	37	570	12	<5	<20	7	0.23	<10	86	<10	<1	67
9	B/L 6+00 W	<0.2	2.76	<5	195	15	0.56	<1	21	53	22	4.11	<10	0.77	371	<1	0.01	35	620	12	<5	<20	7	0.23	<10	84	<10	<1	82
10	B/L 6+50 W	<0.2	2.81	5	190	10	0.59	<1	19	56	21	4.07	<10	0.76	324	<1	0.01	35	690	14	<5	<20	10	0.22	<10	69	<10	<1	85
11	L0 0+25 N	<0.2	2.33	<5	185	15	0.46	<1	14	52	16	4.35	<10	0.58	311	<1	0.01	19	460	14	<5	<20	10	0.24	<10	98	<10	<1	60
12	L0 0+50 N	<0.2	1.72	<5	170	15	0.41	<1	7	34	9	2.82	<10	0.30	126	<1	<0.01	8	390	14	<5	<20	5	0.15	<10	78	<10	<1	43
13	L0 0+75 N	<0.2	2.24	<5	175	15	0.64	<1	16	50	22	3.84	<10	0.72	386	<1	0.01	24	510	12	<5	<20	11	0.22	<10	90	<10	1	52
14	L0 1+00 N	<0.2	1.86	5	140	15	0.61	<1	18	49	28	3.89	<10	0.60	388	<1	0.01	30	410	14	<5	<20	11	0.22	<10	84	<10	<1	50
15	L0 1+25 N	<0.2	2.04	5	225	10	0.89	<1	21	56	36	3.37	<10	0.61	531	<1	0.02	34	630	14	<5	<20	15	0.21	<10	93	<10	11	67
16	L0 1+50 N	<0.2	2.46	5	160	10	0.47	<1	22	67	28	4.03	<10	0.79	359	<1	0.01	37	510	14	<5	<20	7	0.21	<10	62	<10	<1	58
17	L0 1+75 N	<0.2	2.66	<5	165	15	0.41	<1	15	64	15	4.82	<10	0.54	194	<1	0.01	24	990	14	<5	<20	8	0.18	10	91	<10	<1	72
18	L0 2+00 N	<0.2	2.40	5	170	10	0.33	<1	19	59	22	3.75	<10	0.72	273	<1	0.01	36	490	16	<5	<20	7	0.15	<10	69	<10	<1	59
19	L0 2+25 N	<0.2	2.01	5	115	15	0.33	<1	21	56	24	4.03	<10	0.82	545	<1	0.01	30	510	14	<5	<20	8	0.17	<10	72	<10	<1	64
20	L0 2+50 N	<0.2	3.28	10	135	10	0.49	<1	23	82	30	4.59	<10	0.78	373	<1	0.02	44	1020	14	<5	<20	7	0.25	<10	95	<10	<1	79
21	L0 2+75 N	<0.2	2.06	5	115	10	0.29	<1	13	47	16	3.52	<10	0.58	292	<1	0.01	18	450	16	<5	<20	5	0.12	<10	69	<10	<1	54
22	L0 3+00 N	<0.2	3.67	5	175	20	0.32	<1	21	68	22	5.67	<10	0.66	268	<1	0.01	34	1130	14	<5	<20	4	0.19	<10	99	<10	<1	83
23	L0 3+25 N	<0.2	3.69	<5	170	15	0.68	<1	24	63	33	5.17	<10	0.87	391	<1	0.02	40	970	10	<5	<20	10	0.25	<10	107	<10	<1	71
24	L0 3+50 N	<0.2	2.76	10	155	15	0.32	<1	24	62	22	4.34	<10	0.81	334	<1	0.01	39	480	16	<5	<20	6	0.16	<10	81	<10	<1	94
25	L0 3+75 N	<0.2	2.01	<5	145	15	0.41	<1	12	44	17	3.95	<10	0.52	234	<1	0.01	16	1140	12	<5	<20	7	0.17	<10	88	<10	<1	46
26	L0 4+00 N	<0.2	1.98	<5	165	10	0.47	<1	14	45	17	3.74	<10	0.61	246	<1	0.01	21	350	14	<5	<20	10	0.14	<10	63	<10	1	50
27	L0 4+25 N	NO SAMPLE																											
28	L0 4+50 N	<0.2	2.80	<5	210	5	1.06	<1	23	103	104	6.05	<10	0.85	636	<1	0.02	40	720	14	<5	<20	18	0.16	<10	216	<10	61	56
29	L0 4+75 N	<0.2	2.93	<5	180	10	1.20	<1	34	100	76	5.49	<10	1.13	1476	<1	0.02	45	400	12	<5	<20	19	0.29	<10	158	<10	20	72
30	L0 5+00 N	<0.2	3.07	5	255	5	1.32	1	33	88	98	4.69	<10	0.61	1274	<1	0.02	37	720	18	<5	<20	26	0.13	<10	144	<10	38	61

GEOQUEST CONSULTING LTD. ICP CERTIFICATE OF ANALYSIS AK 98-688 ECO-TECH LABORATORIES LTD.

Et #.	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
31	L0 B/L	<0.2	2.88	5	215	10	0.69	<1	20	53	27	4.50	<10	0.86	508	<1	0.01	34	700	14	<5	<20	10	0.24	<10	97	<10	<1	91
32	L0 0+25 S	<0.2	2.24	5	200	15	0.69	<1	20	59	22	4.28	<10	0.84	610	<1	0.02	28	390	14	<5	<20	12	0.21	<10	101	<10	<1	51
33	L0 0+50 S	NO SAMPLE																											
34	L0 0+75 S	NO SAMPLE																											
35	L0 1+00 S	<0.2	2.13	10	215	10	0.76	<1	17	65	24	3.20	<10	0.84	322	<1	0.01	31	370	14	<5	<20	12	0.22	<10	104	<10	2	56
36	L0 1+25 S	<0.2	1.92	<5	165	10	0.98	<1	16	67	31	3.07	<10	0.81	436	<1	0.03	30	490	12	<5	<20	20	0.17	<10	88	<10	4	68
37	L0 1+50 S	<0.2	2.11	5	170	10	0.74	<1	19	54	37	3.69	<10	0.78	386	<1	0.01	38	530	12	<5	<20	14	0.20	<10	83	<10	13	60
38	L0 1+75 S	<0.2	2.03	5	225	10	0.66	<1	15	50	25	4.47	<10	0.74	291	<1	0.01	28	610	10	<5	<20	10	0.18	<10	81	<10	<1	54
39	L0 2+00 S	<0.2	2.27	10	165	15	0.62	<1	19	70	31	4.63	<10	0.93	370	<1	0.01	46	460	10	<5	<20	13	0.16	<10	79	<10	<1	58
40	L0 2+25 S	<0.2	2.18	10	165	5	0.45	<1	22	73	35	4.40	<10	0.70	626	<1	0.01	33	430	12	<5	<20	7	0.16	<10	90	<10	<1	75
41	L0 2+50 S	<0.2	2.28	5	145	15	0.47	<1	18	58	23	4.71	<10	0.76	309	<1	0.01	30	470	12	<5	<20	4	0.19	<10	90	<10	<1	59
42	L0 2+75 S	<0.2	2.23	5	145	15	0.64	<1	22	50	27	3.78	<10	0.81	413	<1	0.01	34	660	14	<5	<20	11	0.23	<10	85	<10	<1	66
43	L0 3+00 S	<0.2	1.88	5	160	10	0.38	<1	13	44	17	4.64	<10	0.49	264	<1	0.01	17	690	12	<5	<20	9	0.17	<10	89	<10	<1	63
44	L0 3+25 S	<0.2	2.18	5	200	15	0.67	<1	17	58	24	5.17	<10	0.79	360	<1	0.01	30	540	14	<5	<20	11	0.22	<10	94	<10	<1	74
45	L0 3+50 S	<0.2	2.55	<5	210	10	0.51	<1	17	57	24	4.41	<10	0.71	343	<1	0.01	35	740	14	<5	<20	8	0.19	<10	90	<10	<1	73
46	L0 3+75 S	<0.2	2.11	5	270	15	0.44	<1	15	61	22	4.50	<10	0.71	513	<1	0.01	27	550	12	<5	<20	9	0.17	<10	99	<10	<1	64
47	L0 4+00 S	<0.2	1.94	<5	185	10	0.48	<1	15	54	31	4.30	<10	0.61	408	<1	0.01	30	840	10	<5	<20	7	0.13	<10	86	<10	<1	77
48	L0 4+25 S	<0.2	2.53	5	225	15	0.63	<1	25	73	32	4.65	<10	0.92	593	<1	0.01	43	530	12	<5	<20	10	0.22	<10	100	<10	2	76
49	L0 4+50 S	<0.2	2.27	5	185	15	0.58	<1	21	65	24	4.06	<10	0.82	453	<1	0.01	33	620	12	<5	<20	9	0.21	<10	94	<10	<1	68
50	L0 4+75 S	<0.2	2.07	5	155	10	0.43	<1	14	53	18	4.66	<10	0.59	277	<1	0.01	19	460	12	<5	<20	8	0.21	<10	98	<10	<1	65
51	L0 5+00 S	<0.2	2.19	<5	165	10	0.44	<1	18	57	24	3.98	<10	0.81	379	<1	0.01	28	350	14	<5	<20	7	0.19	<10	95	<10	<1	64
52	L1 0+25 N	<0.2	1.97	<5	235	20	0.50	<1	15	53	18	4.25	<10	0.68	316	<1	0.01	23	410	12	<5	<20	8	0.19	<10	84	<10	<1	67
53	L1 0+50 N	<0.2	2.08	5	165	15	0.63	<1	18	47	28	3.67	<10	0.74	349	<1	0.01	29	710	12	<5	<20	12	0.19	<10	83	<10	2	52
54	L1 0+75 N	<0.2	1.60	<5	150	10	0.41	<1	12	39	15	3.30	<10	0.57	248	<1	0.01	16	380	14	<5	<20	11	0.15	<10	79	<10	<1	54
55	L1 1+00 N	<0.2	1.85	5	180	10	0.54	<1	19	50	24	3.66	<10	0.78	525	<1	0.01	27	450	12	<5	<20	12	0.16	<10	81	<10	<1	54
55	L1 1+25 N	<0.2	2.84	5	240	20	0.46	<1	21	62	30	6.84	<10	0.71	410	<1	0.01	23	510	10	<5	<20	5	0.43	<10	180	<10	<1	58
57	L1 1+50 N	<0.2	1.85	<5	240	15	0.87	<1	21	50	18	3.90	<10	0.59	661	<1	0.01	16	660	12	<5	<20	13	0.25	<10	117	<10	2	73
58	L1 1+75 N	<0.2	1.71	10	225	10	0.61	<1	19	54	38	3.67	<10	0.84	568	<1	0.01	37	690	12	<5	<20	20	0.18	<10	76	<10	5	61
59	L1 2+00 N	<0.2	1.95	<5	130	10	0.41	<1	18	55	26	3.86	<10	0.82	370	<1	0.01	31	660	14	<5	<20	9	0.16	<10	73	<10	<1	64
60	L1 2+25 N	<0.2	1.93	5	130	10	0.40	<1	18	55	25	3.89	<10	0.79	366	<1	0.01	30	690	14	<5	<20	10	0.15	<10	73	<10	<1	63
61	L1 2+50 N	<0.2	1.94	<5	120	10	0.28	<1	10	44	11	3.39	<10	0.51	262	<1	<0.01	14	680	16	<5	<20	2	0.10	<10	66	<10	<1	50
62	L1 2+75 N	<0.2	1.83	<5	160	5	0.40	<1	16	60	28	3.91	<10	0.77	436	<1	0.01	27	520	14	<5	<20	12	0.16	<10	73	<10	<1	61
63	L1 3+00 N	<0.2	2.04	<5	205	10	0.87	<1	21	57	30	3.94	<10	0.79	1398	<1	0.01	28	500	12	<5	<20	21	0.14	<10	90	<10	8	50
64	L1 3+25 N	<0.2	2.50	10	135	10	0.38	<1	18	48	21	4.17	<10	0.72	313	<1	0.01	33	980	14	<5	<20	6	0.13	<10	67	<10	<1	100
65	L1 3+50 N	<0.2	2.31	<5	115	10	0.27	<1	15	49	18	3.94	<10	0.70	264	<1	0.01	28	810	14	<5	<20	6	0.10	<10	84	<10	<1	84
66	L1 3+75 N	0.2	1.96	<5	135	20	0.43	<1	12	43	18	5.05	<10	0.58	351	<1	0.01	19	1830	12	<5	<20	7	0.11	<10	80	<10	<1	71
67	L1 4+75 N	<0.2	3.23	<5	270	10	1.37	<1	29	106	65	5.58	<10	1.04	1005	<1	0.02	44	370	12	<5	<20	22	0.35	<10	182	<10	22	57
68	L1 5+00 N	<0.2	2.45	<5	220	5	0.82	<1	24	71	33	4.41	<10	0.81	750	<1	0.02	31	370	12	<5	<20	13	0.24	<10	123	<10	2	57
68	L1 W B/L	<0.2	2.42	10	170	10	0.51	<1	17	56	31	4.19	<10	0.83	350	<1	0.01	36	580	16	<5	<20	8	0.19	<10	84	<10	<1	65
70	L1 W 0+25 S	<0.2	1.38	<5	180	10	0.29	<1	10	35	12	3.86	<10	0.31	236	<1	<0.01	9	550	14	<5	<20	5	0.24	<10	109	<10	<1	36

Et #.	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
71	L1 W 0+50 S	<0.2	2.14	5	265	10	0.36	<1	13	49	19	3.82	<10	0.50	347	<1	<0.01	19	660	12	<5	<20	6	0.18	<10	92	<10	<1	78
72	L1 W 0+75 S	<0.2	1.49	<5	210	15	0.39	<1	13	42	16	4.16	<10	0.41	925	<1	<0.01	14	1450	12	<5	<20	4	0.18	<10	102	<10	<1	51
73	L1 W 1+00 S	<0.2	2.43	5	170	10	0.41	<1	12	48	20	3.86	<10	0.52	286	<1	0.01	19	660	12	<5	<20	6	0.16	<10	81	<10	<1	59
74	L1 W 1+25 S	<0.2	2.60	10	190	10	0.54	<1	17	53	24	3.76	<10	0.70	284	<1	0.01	34	700	14	<5	<20	10	0.18	<10	78	<10	<1	68
75	L1 W 1+50 S	<0.2	1.77	10	145	10	0.45	<1	13	47	17	4.33	<10	0.46	253	<1	0.01	16	750	12	<5	<20	5	0.23	<10	96	<10	<1	53
76	L1 W 1+75 S	<0.2	1.45	5	200	15	0.38	<1	12	44	17	4.40	<10	0.41	326	<1	<0.01	13	900	12	<5	<20	6	0.28	<10	117	<10	<1	47
77	L1 W 2+00 S	<0.2	1.63	<5	175	10	0.42	<1	13	49	19	3.22	<10	0.47	674	<1	0.01	17	460	12	<5	<20	4	0.18	<10	81	<10	<1	56
78	L1 W 2+25 S	<0.2	1.86	<5	220	10	0.51	<1	16	49	21	3.57	<10	0.56	533	<1	0.01	21	450	12	<5	<20	7	0.16	<10	83	<10	2	56
79	L1 W 2+50 S	<0.2	1.58	5	190	15	0.30	<1	13	61	19	4.72	<10	0.40	336	<1	<0.01	17	1040	10	<5	<20	4	0.17	<10	102	<10	<1	57
80	L1 W 2+75 S	<0.2	1.95	10	200	15	0.30	<1	14	73	20	5.98	<10	0.58	290	<1	0.01	24	480	10	<5	<20	7	0.15	<10	90	<10	<1	58
81	L1 W 3+00 S	<0.2	1.13	<5	235	15	0.40	<1	9	31	14	2.67	<10	0.23	178	<1	<0.01	9	350	12	<5	<20	5	0.26	<10	107	<10	<1	34
82	L1 W 3+25 S	<0.2	1.82	<5	190	10	0.39	<1	13	48	16	4.24	<10	0.45	243	<1	0.01	17	640	12	<5	<20	7	0.24	<10	99	<10	<1	62
83	L1 W 3+50 S	<0.2	2.75	15	350	<5	0.68	<1	27	96	159	4.61	10	0.88	893	<1	0.01	103	420	16	<5	<20	17	0.15	<10	101	<10	20	116
84	L1 W 3+75 S	0.4	2.61	10	315	<5	0.88	<1	25	89	81	4.27	10	0.87	1235	<1	0.01	63	880	14	<5	<20	20	0.11	<10	99	<10	25	102
85	L1 W 4+00 S	<0.2	1.97	5	225	<5	0.70	<1	22	78	55	4.14	<10	0.70	1438	<1	0.01	34	650	12	<5	<20	14	0.12	<10	98	<10	15	73
86	L1 W 4+25 S	<0.2	1.80	5	215	15	0.50	<1	15	62	26	4.92	<10	0.72	395	<1	0.01	29	540	10	<5	<20	10	0.21	<10	104	<10	<1	53
87	L1 W 4+50 S	<0.2	2.14	10	245	10	0.60	<1	18	64	30	4.59	<10	0.90	460	<1	0.01	37	610	10	<5	<20	9	0.19	<10	97	<10	<1	70
88	L1 W 4+75 S	<0.2	1.87	10	255	5	0.68	<1	24	58	26	3.61	<10	0.72	1045	<1	0.01	28	820	14	<5	<20	12	0.13	<10	89	<10	<1	64
89	L1 W 5+00 S	<0.2	1.65	15	260	10	0.47	<1	17	57	24	4.54	<10	0.63	683	<1	0.01	29	710	10	<5	<20	8	0.18	<10	99	<10	<1	57
90	L1 E 0+50 N	<0.2	1.59	<5	155	10	0.34	<1	8	37	11	2.98	<10	0.42	288	<1	<0.01	12	470	14	<5	<20	5	0.13	<10	71	<10	<1	54
91	L1 E 1+00 N	<0.2	1.18	<5	220	10	0.68	<1	9	31	11	2.54	<10	0.41	444	<1	0.01	9	670	12	<5	<20	12	0.23	<10	93	<10	<1	41
92	L1 E 1+50 N	<0.2	2.06	10	140	15	0.44	<1	20	57	24	4.14	<10	0.77	477	<1	0.01	28	490	12	<5	<20	9	0.20	<10	86	<10	<1	55
93	L1 E 2+00 N	<0.2	2.57	10	120	15	0.35	<1	17	59	20	4.18	<10	0.68	261	<1	0.01	34	730	14	<5	<20	4	0.15	<10	72	<10	<1	63
94	L1 E 2+50 N	<0.2	2.39	<5	140	10	0.30	<1	13	46	13	3.61	<10	0.41	199	<1	0.01	19	590	14	<5	<20	6	0.14	<10	73	<10	<1	61
95	L1 E 3+00 N	<0.2	3.04	5	155	15	0.41	<1	18	58	26	4.61	<10	0.67	290	<1	0.01	33	980	12	<5	<20	7	0.19	<10	93	<10	<1	59
96	L1 E 3+50 N	<0.2	2.08	5	115	10	0.31	<1	10	42	12	3.33	<10	0.42	178	<1	0.01	13	870	14	<5	<20	5	0.14	<10	79	<10	<1	52
97	L1 E 4+00 N	<0.2	2.47	5	165	15	0.87	<1	19	65	29	4.11	<10	0.85	310	<1	0.01	29	330	12	<5	<20	10	0.21	<10	102	<10	3	45
98	L1 E 5+00 N	<0.2	2.19	<5	205	15	0.88	<1	16	51	24	5.69	<10	0.63	412	<1	0.02	23	1000	8	<5	<20	9	0.20	<10	154	<10	<1	81
99	L1 E B/L	<0.2	2.08	10	280	5	0.71	<1	19	69	39	4.05	<10	0.81	598	<1	0.01	38	600	14	<5	<20	17	0.11	<10	88	<10	6	59
100	L1 E 0+50 S	0.2	2.16	10	365	10	0.81	<1	20	76	47	3.98	<10	0.79	991	<1	0.01	35	650	14	<5	<20	18	0.11	<10	88	<10	9	65
101	L1 E 1+00 S	<0.2	2.22	5	380	<5	0.73	<1	22	85	82	3.99	<10	0.95	525	<1	0.01	54	560	16	<5	<20	18	0.14	<10	84	<10	17	72
102	L1 E 1+50 S	0.2	2.48	10	345	<5	0.88	<1	24	91	125	4.58	30	0.85	1082	<1	0.01	51	750	14	<5	<20	27	0.09	<10	109	<10	44	70
103	L1 E 2+00 S	0.2	2.31	10	390	<5	1.15	<1	22	85	92	3.05	40	0.83	1075	<1	0.01	49	810	14	<5	<20	36	0.09	<10	66	<10	54	61
104	L1 E 2+50 S	1.0	2.82	20	385	<5	1.06	<1	27	107	158	5.09	70	0.73	1179	1	0.01	55	1100	18	<5	<20	34	0.07	<10	117	<10	83	77
105	L1 E 3+00 S	0.6	2.84	15	385	<5	1.22	<1	28	104	155	4.83	70	0.78	1323	<1	0.01	65	980	14	<5	<20	38	0.09	<10	102	<10	98	89
106	L1 E 3+50 S	0.8	3.81	15	470	<5	1.08	<1	37	162	303	5.59	80	1.14	2306	<1	0.02	89	700	16	<5	<20	31	0.17	<10	124	<10	67	88
107	L1 E 4+00 S	<0.2	1.79	<5	230	15	0.51	<1	12	49	20	4.24	<10	0.49	276	<1	0.01	16	590	10	<5	<20	6	0.25	<10	122	<10	<1	50
108	L1 E 4+50 S	<0.2	2.46	<5	165	10	0.46	<1	17	57	17	4.16	<10	0.53	342	<1	0.01	22	810	12	<5	<20	6	0.21	<10	84	<10	<1	80
109	L1 E 5+00 S	<0.2	2.41	<5	200	15	0.60	<1	17	58	17	4.07	<10	0.55	479	<1	0.01	21	790	18	<5	<20	7	0.27	<10	101	<10	<1	73
110	L1 N 0+25 E	<0.2	2.23	5	210	15	0.96	<1	20	61	31	3.85	<10	0.82	591	<1	0.02	31	490	12	<5	<20	17	0.23	<10	103	<10	5	55

GEOQUEST CONSULTING LTD. ICP CERTIFICATE OF ANALYSIS AK 98-688 ECO-TECH LABORATORIES LTD.

Et #.	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
111	L1 N 0+50 E	<0.2	2.17	10	225	10	1.12	<1	22	60	38	3.68	<10	0.92	667	<1	0.02	37	600	12	<5	<20	20	0.28	<10	101	<10	4	60
112	L1 N 0+75 E	<0.2	2.42	5	410	5	0.63	<1	18	71	41	4.17	<10	0.71	714	<1	0.02	31	600	16	<5	<20	22	0.18	<10	111	<10	7	75
113	L1 N 0+25 W	<0.2	2.14	5	170	15	0.72	<1	22	56	34	3.96	<10	0.87	510	<1	0.02	37	600	12	<5	<20	16	0.28	<10	88	<10	<1	68
114	L1 N 0+50 W	<0.2	2.11	5	165	16	0.83	<1	18	47	29	3.92	<10	0.77	368	<1	0.02	33	650	10	<5	<20	16	0.29	<10	91	<10	<1	50
115	L1 N 0+75 W	<0.2	1.77	<5	225	10	0.67	<1	14	44	23	3.25	<10	0.67	374	<1	0.01	24	580	14	<5	<20	13	0.21	<10	63	<10	<1	47
116	L2 S 0+25 E	<0.2	2.17	10	265	6	0.89	<1	27	70	58	4.06	<10	1.18	749	<1	0.02	58	560	10	<5	<20	18	0.23	<10	89	<10	6	54
117	L2 S 0+50 E	<0.2	2.53	15	275	10	0.80	<1	30	87	65	4.76	10	0.99	1141	<1	0.02	64	710	14	<5	<20	20	0.16	<10	91	<10	28	68
118	L2 S 0+75 E	<0.2	2.74	15	205	10	0.86	<1	33	80	45	4.46	<10	1.19	721	<1	0.02	62	600	12	<5	<20	12	0.27	<10	99	<10	2	51
119	L2 S 0+25 W	<0.2	1.76	10	200	15	0.63	<1	13	57	16	3.92	<10	0.64	337	<1	0.01	24	530	10	<5	<20	8	0.22	<10	108	<10	<1	64
120	L2 S 0+50 W	<0.2	1.02	<5	260	10	0.45	<1	14	56	20	5.14	<10	0.46	408	<1	0.01	17	1410	10	<5	<20	9	0.19	<10	120	<10	<1	54
121	L2 S 0+75 W	<0.2	1.69	5	215	15	0.80	<1	12	48	19	4.02	<10	0.49	270	<1	0.01	18	530	10	<5	<20	10	0.24	<10	95	<10	<1	50
122	L3 W 0+50 N	<0.2	2.19	5	145	15	0.67	<1	15	52	24	3.44	<10	0.69	278	<1	0.02	26	520	12	<5	<20	9	0.26	<10	94	<10	1	43
123	L3 W 1+00 N	<0.2	2.26	10	180	10	0.79	<1	19	56	30	3.73	<10	0.89	436	<1	0.02	33	530	12	<5	<20	11	0.26	<10	101	<10	2	45
124	L3 W 1+50 N	<0.2	2.40	<5	250	10	0.68	<1	24	72	32	4.07	<10	0.91	709	<1	0.02	35	540	14	<5	<20	16	0.19	<10	100	<10	2	60
125	L3 W 2+00 N	<0.2	2.38	<5	170	10	0.63	<1	17	80	31	3.79	<10	0.85	293	<1	0.02	32	320	14	<5	<20	11	0.21	<10	118	<10	2	44
126	L3 W 2+50 N	<0.2	2.73	6	155	10	0.57	<1	26	56	32	4.03	<10	0.84	398	<1	0.02	41	590	12	<5	<20	7	0.24	<10	86	<10	<1	85
127	L3 W 3+00 N	<0.2	2.53	5	165	10	0.48	<1	20	61	26	4.16	<10	0.81	347	<1	0.02	36	410	14	<5	<20	10	0.21	<10	86	<10	<1	63
128	L3 W 3+50 N	<0.2	2.58	<5	160	10	0.44	<1	19	56	20	3.97	<10	0.74	325	<1	0.02	31	780	14	<5	<20	9	0.19	<10	80	<10	<1	111
129	L3 W 4+00 N	<0.2	2.32	5	145	10	0.66	<1	16	51	28	3.64	<10	0.80	330	<1	0.02	33	560	10	<5	<20	13	0.21	<10	80	<10	<1	80
130	L3 W 5+00 N	<0.2	3.30	6	255	10	1.41	<1	27	108	82	6.41	<10	1.02	737	<1	0.02	46	530	10	<5	<20	26	0.30	<10	187	<10	36	63
131	L3 W B/L	<0.2	2.37	<5	165	15	0.70	<1	19	66	22	4.61	<10	0.81	462	<1	0.02	27	750	10	<5	<20	13	0.25	<10	112	<10	<1	72
132	L3 W 0+50 S	<0.2	2.66	5	160	10	0.61	<1	22	57	20	3.89	<10	0.74	542	<1	0.02	29	690	12	<5	<20	11	0.23	<10	86	<10	<1	77
133	L3 W 1+00 S	<0.2	2.63	10	190	15	0.54	<1	16	59	22	4.18	<10	0.75	324	<1	0.02	34	680	12	<5	<20	6	0.23	<10	86	<10	<1	64
134	L3 W 1+50 S	<0.2	2.63	5	315	10	0.59	<1	18	53	28	3.64	<10	0.77	355	<1	0.02	36	470	12	<5	<20	7	0.22	<10	81	<10	<1	65
135	L3 W 2+00 S	<0.2	2.71	10	235	10	0.62	<1	22	58	26	4.10	<10	0.87	362	<1	0.02	44	630	14	<5	<20	10	0.21	<10	86	<10	<1	89
136	L3 W 2+50 S	<0.2	2.57	<5	255	5	0.62	<1	16	62	26	4.11	<10	0.62	276	<1	0.01	27	320	16	<5	<20	15	0.19	<10	107	<10	6	53
137	L3 W 3+50 S	<0.2	2.54	<5	210	16	0.70	<1	20	84	32	4.93	<10	0.89	422	<1	0.02	38	520	12	<5	<20	11	0.25	<10	108	<10	<1	65
138	L3 W 4+00 S	<0.2	1.44	<5	165	10	0.30	<1	11	34	15	4.03	<10	0.34	320	<1	0.01	12	910	14	<5	<20	9	0.17	<10	66	<10	<1	57
139	L3 W 4+50 S	<0.2	2.96	10	250	16	0.59	<1	18	66	26	4.60	<10	0.85	315	<1	0.02	39	660	14	<5	<20	8	0.21	<10	93	<10	<1	71
140	L3 W 5+00 S	<0.2	2.33	10	190	10	0.50	<1	20	57	26	4.45	<10	0.76	430	<1	0.02	38	640	14	<5	<20	8	0.25	<10	93	<10	<1	72
141	L5 W 0+50 N	<0.2	2.24	<5	220	10	0.60	<1	12	52	16	4.18	<10	0.60	245	<1	0.01	22	580	8	<5	<20	11	0.16	<10	74	<10	<1	76
142	L5 W 1+00 N	<0.2	1.38	<5	150	10	0.32	<1	8	29	8	2.43	<10	0.29	164	<1	<0.01	7	230	12	<5	<20	4	0.15	<10	73	<10	<1	34
143	L5 W 1+50 N	<0.2	2.03	<5	230	10	0.90	<1	21	58	31	3.78	<10	0.89	594	<1	0.02	32	580	8	<5	<20	14	0.26	<10	91	<10	5	57
144	L5 W 2+00 N	<0.2	2.15	<5	165	10	0.57	<1	18	53	28	3.87	<10	0.76	356	<1	0.01	32	620	10	<5	<20	9	0.20	<10	69	<10	<1	49
145	L5 W 2+50 N	<0.2	2.72	<5	160	10	0.44	<1	17	57	20	3.94	<10	0.55	222	<1	0.02	26	800	12	<5	<20	3	0.21	<10	96	<10	<1	47
146	L5 W 3+00 N	<0.2	3.15	<5	200	10	0.44	<1	23	61	21	4.33	<10	0.71	371	<1	0.01	38	860	12	<5	<20	4	0.20	<10	86	<10	<1	78
147	L5 W 3+50 N	<0.2	2.25	<5	135	15	0.45	<1	14	50	12	3.93	<10	0.51	273	<1	0.01	17	520	10	<5	<20	4	0.22	<10	85	<10	<1	64
148	L5 W 4+00 N	<0.2	2.28	<5	155	15	1.25	<1	23	74	54	4.19	<10	0.86	685	<1	0.02	33	430	8	<5	<20	14	0.30	<10	121	<10	13	53
149	L5 W 4+50 N	<0.2	2.50	<5	180	10	1.04	<1	23	74	36	4.50	<10	0.95	603	<1	0.02	34	310	8	<5	<20	12	0.28	<10	113	<10	12	55
150	L5 W 5+00 N	<0.2	3.62	<5	285	10	0.74	<1	32	117	89	6.24	<10	0.75	1104	<1	0.02	44	490	14	<5	<20	12	0.23	<10	177	<10	18	69

GEOQUEST CONSULTING LTD. ICP CERTIFICATE OF ANALYSIS AK 98-888 ECO-TECH LABORATORIES LTD.

Et #.	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
151	L5 W B/L	<0.2	1.60	<5	215	15	0.48	<1	11	48	17	4.44	<10	0.27	779	<1	0.01	10	990	8	<5	<20	5	0.21	<10	132	<10	<1	48
152	L5 W 0+50 S	<0.2	1.98	5	140	15	0.50	<1	15	56	19	4.14	<10	0.71	334	<1	0.01	22	460	10	<5	<20	3	0.29	<10	107	<10	<1	57
153	L5 W 1+00 S	<0.2	2.16	<5	165	10	0.58	<1	18	51	23	3.82	<10	0.65	286	<1	0.01	35	610	10	<5	<20	8	0.22	<10	77	<10	<1	46
154	L5 W 1+50 S	<0.2	2.87	5	265	10	0.64	<1	25	85	34	5.12	<10	0.93	462	<1	0.02	45	430	8	<5	<20	6	0.24	<10	125	<10	4	66
155	L5 W 2+00 S	<0.2	2.21	<5	230	10	0.73	<1	22	77	35	3.72	<10	0.88	859	<1	0.02	37	480	12	<5	<20	12	0.16	<10	88	<10	4	68
156	L5 W 2+50 S	<0.2	1.80	<5	200	10	0.71	<1	17	54	21	3.38	<10	0.78	416	<1	0.01	26	350	10	<5	<20	10	0.19	<10	80	<10	2	47
157	L5 W 3+00 S	<0.2	2.01	<5	155	5	0.65	<1	18	59	28	3.94	<10	0.70	293	<1	0.01	29	370	10	<5	<20	10	0.17	<10	84	<10	1	67
158	L5 W 3+50 S	<0.2	1.76	5	250	15	0.46	<1	13	56	17	4.18	<10	0.59	323	<1	0.01	22	600	10	<5	<20	2	0.27	<10	124	<10	<1	66
159	L5 W 4+00 S	<0.2	2.13	<5	175	5	0.66	<1	16	52	28	3.66	<10	0.73	299	<1	0.01	31	410	10	<5	<20	8	0.18	<10	80	<10	1	53
160	L5 W 4+50 S	<0.2	2.03	<5	245	10	0.50	<1	17	59	21	4.11	<10	0.64	467	<1	0.01	24	280	10	<5	<20	4	0.20	<10	97	<10	<1	53
161	L5 W 5+00 S	<0.2	2.16	<5	240	10	0.44	<1	16	60	18	5.01	<10	0.60	315	<1	0.01	24	340	10	<5	<20	5	0.28	<10	114	<10	<1	73
162	L7 W 0+50 N	<0.2	2.06	<5	135	15	0.58	<1	12	45	16	3.61	<10	0.52	411	<1	0.01	18	630	8	<5	<20	2	0.20	<10	69	<10	<1	53
163	L7 W 1+00 N	<0.2	2.30	<5	150	10	0.73	<1	21	51	28	3.80	<10	0.74	673	<1	0.02	28	720	8	<5	<20	7	0.27	<10	96	<10	1	58
164	L7 W 1+50 N	<0.2	2.04	<5	160	20	0.37	<1	12	50	14	5.02	<10	0.44	216	<1	0.01	16	490	12	<5	<20	1	0.22	<10	100	<10	<1	55
165	L7 W 2+00 N	<0.2	2.18	<5	190	10	0.62	<1	18	47	24	3.72	<10	0.59	290	<1	0.01	27	590	10	<5	<20	5	0.22	<10	86	<10	3	47
166	L7 W 2+50 N	<0.2	2.25	5	150	15	0.48	<1	21	58	30	3.96	<10	0.75	387	<1	0.01	33	320	10	<5	<20	6	0.22	<10	86	<10	2	48
167	L7 W 3+00 N	<0.2	2.42	5	150	10	0.43	<1	17	70	23	5.36	<10	0.77	274	<1	0.01	32	640	10	<5	<20	7	0.21	<10	89	<10	<1	58
168	L7 W 3+50 N	<0.2	2.24	5	225	5	1.13	<1	20	76	45	4.66	<10	0.78	1221	<1	0.02	30	640	8	<5	<20	17	0.19	<10	125	<10	22	51
169	L7 W 4+50 N	<0.2	2.40	<5	170	10	1.02	<1	23	58	33	4.12	<10	0.88	539	<1	0.02	33	690	8	<5	<20	12	0.30	<10	106	<10	3	53
170	L7 W 5+00 N	<0.2	3.12	<5	175	15	1.29	<1	30	105	53	5.27	<10	0.92	931	<1	0.02	36	400	8	<5	<20	18	0.32	<10	178	<10	31	65
171	L7 W B/L	<0.2	2.56	<5	170	15	0.55	<1	19	58	19	4.33	<10	0.79	423	<1	0.01	33	870	10	<5	<20	9	0.20	<10	85	<10	<1	98
172	L7 W 0+50 S	<0.2	2.89	<5	240	15	0.67	<1	23	80	20	4.29	<10	0.64	336	<1	0.02	38	400	8	<5	<20	5	0.30	<10	101	<10	<1	56
173	L7 W 1+00 S	<0.2	2.96	5	570	5	0.64	<1	21	92	56	4.78	<10	0.93	1205	<1	0.02	44	390	12	<5	<20	12	0.22	<10	129	<10	24	50
174	L7 W 1+50 S	<0.2	2.71	5	210	15	0.72	<1	27	82	39	4.48	<10	1.04	571	<1	0.02	48	550	12	<5	<20	9	0.23	<10	98	<10	2	63
175	L7 W 2+00 S	<0.2	2.34	5	210	10	0.78	<1	23	65	32	4.06	<10	0.83	432	<1	0.02	48	630	10	<5	<20	10	0.22	<10	90	<10	7	88
176	L7 W 2+50 S	<0.2	2.08	5	195	10	0.69	<1	23	65	47	3.87	<10	0.71	635	<1	0.01	48	450	8	<5	<20	11	0.17	<10	81	<10	7	51
177	L7 W 3+00 S	<0.2	2.49	<5	220	15	0.70	<1	23	72	30	4.42	<10	0.91	372	<1	0.02	46	380	6	<5	<20	10	0.25	<10	93	<10	1	44
178	L7 W 3+50 S	<0.2	1.67	<5	190	10	0.30	<1	12	54	19	4.66	<10	0.48	211	<1	0.01	20	680	10	<5	<20	5	0.17	<10	112	<10	<1	47
179	L7 W 4+00 S	0.2	2.08	10	190	10	0.77	<1	17	80	48	5.13	<10	0.59	244	1	0.01	46	480	8	<5	<20	15	0.08	<10	77	<10	8	54
180	L7 W 4+50 S	<0.2	2.29	<5	150	10	0.27	<1	12	59	30	4.33	<10	0.46	211	<1	0.01	24	990	14	<5	<20	2	0.13	<10	89	<10	<1	62
181	L7 W 5+00 S	<0.2	2.83	<5	280	15	0.40	<1	18	88	32	6.27	<10	0.54	297	<1	0.01	34	710	14	<5	<20	<1	0.22	<10	149	<10	<1	57
182	SLT 98-R-01	<0.2	1.83	<5	200	5	1.22	<1	21	55	48	3.47	<10	0.69	1802	<1	0.02	28	780	8	<5	<20	16	0.13	<10	97	<10	19	78
183	SLT R-98-02	<0.2	2.60	<5	205	10	1.47	<1	30	68	51	4.74	<10	1.10	2680	<1	0.02	30	640	8	<5	<20	16	0.25	<10	139	<10	21	88

GEOQUEST CONSULTING LTD. ICP CERTIFICATE OF ANALYSIS AK 98-688 ECO-TECH LABORATORIES LTD.

Et #.	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
QC/DATA:																													
Repeat:																													
1	B/L 0+50 W	<0.2	2.33	<5	175	10	0.34	<1	15	51	23	4.43	<10	0.70	333	<1	0.01	27	480	18	<5	<20	10	0.14	<10	74	<10	<1	74
10	B/L 6+50 W	<0.2	2.93	<5	195	20	0.62	<1	20	58	21	4.20	<10	0.79	337	<1	0.02	36	650	12	<5	<20	9	0.24	<10	92	<10	<1	86
19	L0 2+25 N	<0.2	2.05	<5	115	10	0.34	<1	21	57	24	4.08	<10	0.84	554	<1	0.01	31	500	14	<5	<20	8	0.17	<10	74	<10	<1	66
26	L0 4+50 N	<0.2	2.90	<5	220	<5	1.10	1	24	106	108	6.10	<10	0.87	646	<1	0.02	40	730	14	<5	<20	20	0.16	<10	220	<10	63	57
36	L0 1+25 S	<0.2	1.90	5	175	5	0.93	<1	16	65	28	3.03	<10	0.82	411	<1	0.03	30	460	14	<5	<20	17	0.18	<10	88	<10	4	65
45	L0 3+50 S	<0.2	2.56	5	210	10	0.52	<1	17	57	24	4.42	<10	0.72	344	<1	0.01	35	730	14	<5	<20	9	0.19	<10	90	<10	<1	73
54	L1 0+75 N	<0.2	1.68	<5	155	10	0.43	<1	12	42	15	3.46	<10	0.60	260	<1	0.01	18	400	14	<5	<20	7	0.16	<10	83	<10	<1	56
63	L1 3+00 N	<0.2	1.99	5	200	10	0.94	<1	21	56	29	3.85	<10	0.78	1367	<1	0.02	27	580	12	<5	<20	19	0.14	<10	88	<10	7	49
71	L1 W 0+50 S	<0.2	2.12	5	270	10	0.35	<1	13	48	16	3.76	<10	0.49	347	<1	0.01	17	660	12	<5	<20	6	0.19	<10	93	<10	<1	79
80	L1 W 2+75 S	<0.2	2.01	15	205	15	0.38	<1	14	76	21	6.10	<10	0.58	300	<1	<0.01	25	500	12	<5	<20	7	0.15	<10	92	<10	<1	59
89	L1 W 5+00 S	<0.2	1.62	5	250	15	0.47	<1	17	58	24	4.41	<10	0.61	668	<1	0.01	29	710	10	<5	<20	6	0.16	<10	97	<10	<1	56
98	L1 E 5+00 N	<0.2	2.28	<5	210	10	0.73	<1	17	53	26	6.06	<10	0.64	423	<1	0.02	24	1970	8	<5	<20	9	0.22	<10	158	<10	<1	63
105	L1 E 3+50 S	0.4	3.85	15	465	<5	1.08	<1	37	162	303	5.61	80	1.15	2275	<1	0.02	69	720	18	<5	<20	27	0.18	<10	126	<10	67	90
115	L1 N 0+75 W	<0.2	1.79	<5	225	15	0.88	<1	14	43	22	3.25	<10	0.67	364	<1	0.01	24	570	12	<5	<20	13	0.21	<10	84	<10	<1	48
124	L3 W 1+50 N	<0.2	2.49	5	255	15	0.89	<1	25	74	33	4.19	<10	0.84	731	<1	0.02	36	570	14	<5	<20	13	0.20	<10	103	<10	3	63
133	L3 W 1+00 S	<0.2	2.70	<5	200	15	0.56	<1	19	61	22	4.25	<10	0.76	327	<1	0.01	36	690	10	<5	<20	8	0.24	<10	90	<10	<1	85
141	L5 W 0+50 N	<0.2	2.40	<5	230	15	0.88	<1	13	55	16	4.35	<10	0.84	281	<1	0.01	24	600	8	<5	<20	10	0.18	<10	80	<10	<1	79
150	L5 W 6+00 N	<0.2	3.67	<5	295	<5	0.73	<1	33	118	89	6.27	<10	0.74	1123	<1	0.02	46	520	12	<5	<20	13	0.24	<10	179	<10	17	69
159	L5 W 4+00 S	<0.2	2.18	<5	170	10	0.58	<1	17	53	28	3.87	<10	0.74	298	<1	0.01	33	410	10	<5	<20	6	0.20	<10	82	<10	1	53
168	L7 W 3+50 N	<0.2	2.41	<5	225	10	1.20	<1	22	77	45	4.69	<10	0.84	1244	<1	0.02	32	680	8	<5	<20	20	0.16	<10	129	<10	22	63
176	L7 W 2+50 S	<0.2	2.26	10	205	<5	0.76	<1	25	70	49	4.15	<10	0.77	687	<1	0.01	51	490	10	<5	<20	13	0.18	<10	89	<10	7	54
Standard:																													
GEO'98		1.6	1.76	65	160	<5	1.76	<1	19	64	81	4.02	<10	0.98	688	<1	0.02	21	660	22	<5	<20	58	0.11	<10	78	<10	5	69
GEO'98		1.4	1.73	70	160	<5	1.74	<1	19	66	81	3.97	<10	0.96	688	<1	0.02	23	660	20	<5	<20	58	0.11	<10	76	<10	6	68
GEO'98		1.4	1.68	65	160	<5	1.80	<1	19	61	80	3.86	<10	0.98	670	<1	0.02	21	630	20	<5	<20	66	0.10	<10	76	<10	5	66
GEO'98		1.4	1.64	65	165	5	1.75	<1	20	64	81	4.04	<10	0.95	691	<1	0.03	21	630	20	<5	<20	64	0.13	<10	81	<10	5	68
GEO'98		1.4	1.87	65	165	<5	1.82	<1	20	60	85	4.21	<10	1.00	708	<1	0.03	23	670	18	<5	<20	64	0.13	<10	82	<10	5	71
GEO'98		1.2	1.72	65	165	<5	1.82	<1	19	60	79	3.96	<10	0.98	673	<1	0.02	22	640	18	<5	<20	64	0.11	<10	76	<10	6	67

df/688/688a
XLS/98Geoquest
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ECO-TECH LABORATORIES LTD.
Frank J. Pezzotti, A.Sc.T.
B.C. Certified Assayer

12-Nov-98

ECO-TECH LABORATORIES LTD.
10041 East Trans Canada Highway
KAMLOOPS, B.C.
V2C 6T4

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ICP CERTIFICATE OF ANALYSIS AK 98-667

GEOQUEST CONSULTING LTD.
8055 ASPEN ROAD
VERNON, B.C.
V1B 3M9

ATTENTION: WARNER GRUENWALD

No. of samples: 1
Sample type: Rock
PROJECT #: 74
SHIPMENT #: None Given
Samples submitted by: W. Gruenwald

Values in ppm unless otherwise reported

Et #.	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
1	LR98-01	<0.2	3.01	<5	45	<5	1.69	<1	58	64	250	8.24	<10	2.07	694	<1	0.05	43	670	26	<5	<20	6	0.43	<10	136	<10	<1	51

QC/DATA:

Et #.	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
Resplit:																													
1	LR98-01	<0.2	3.07	<5	40	10	1.71	<1	61	87	263	8.48	<10	2.12	713	<1	0.05	45	720	30	<5	<20	4	0.43	<10	137	<10	<1	52
Repeat:																													
1	LR98-01	<0.2	3.16	<5	35	10	1.83	<1	60	87	258	8.46	<10	2.16	719	<1	0.06	44	730	30	<5	<20	4	0.48	<10	142	<10	1	53
Standard:																													
GEO'98		1.2	1.81	65	160	<5	1.79	<1	20	66	84	4.16	<10	0.96	699	<1	0.02	24	690	26	<5	<20	57	0.11	<10	79	<10	6	77

df/689
XLS/98Geoquest
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ECO-TECH LABORATORIES LTD.
Frank J. Pezzotti, A.Sc.T.
B.C. Certified Assayer

28-Oct-98

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ICP CERTIFICATE OF ANALYSIS AK 98-659

GEOQUEST CONSULTING LTD.
8055 ASPEN ROAD
VERNON, B.C.
V1B 3M9

ATTENTION: WARNER GRUENWALD

No. of samples: 5
Sample type: Rock
PROJECT #: 74
SHIPMENT #: None Given
Samples submitted by: W. Gruenwald

Values in ppm unless otherwise reported

Et #.	Tag #	Au(ppb)	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
1	1893	5	<0.2	2.60	<5	50	<5	1.86	2	32	51	431	6.15	<10	1.29	660	<1	0.11	36	500	20	<5	<20	6	0.39	<10	145	<10	17	356
2	LOTTIE #1	5	<0.2	0.05	<5	130	10	0.03	<1	1	121	10	1.77	<10	<0.01	86	2	<0.01	7	10	<2	<5	<20	<1	<0.01	<10	15	<10	<1	5
3	LOTTIE #2	10	<0.2	0.10	60	55	10	0.09	1	43	84	54	3.66	<10	0.01	36	16	<0.01	22	20	6	<5	<20	<1	0.05	<10	9	<10	<1	<1
4	LOTTIE MAIN A	285	14.6	0.84	420	150	<5	0.30	5	635	39	>10000	>10	<10	0.61	205	613	0.01	23	<10	54	<5	<20	2	0.18	10	47	10	<1	336
5	LOTTIE MAIN B	25	0.8	1.52	30	65	<5	0.44	1	93	90	>10000	7.09	<10	1.16	367	114	0.02	29	<10	30	<5	<20	4	0.19	<10	65	<10	4	52
QC/DATA:																														
Resplit:																														
1	1893	5	<0.2	2.47	<5	55	<5	1.79	2	32	48	461	6.00	<10	1.24	669	<1	0.09	34	470	18	<5	<20	8	0.35	<10	134	<10	15	351
Repeat:																														
1	1893	5	<0.2	2.64	<5	55	<5	1.86	2	32	50	487	6.14	<10	1.27	620	<1	0.10	36	480	18	<5	<20	8	0.36	<10	140	<10	16	351
Standard:																														
GEO'98		140	1.0	1.82	60	175	10	1.79	<1	20	60	92	4.17	<10	0.96	669	<1	0.02	22	670	20	10	<20	61	0.12	<10	80	<10	5	76

ECO-TECH LABORATORIES LTD.
Frank J. Pezzotti, A.Sc.T.
B.C. Certified Assayer

df/857
XLS/98Geoquest
fax: 549-5262

ASSAYING
GEOCHEMISTRY
ANALYTICAL CHEMISTRY
ENVIRONMENTAL TESTING

Eco-Tech LABORATORIES LTD.

10041 E. Trans Canada Hwy., R.R. #2, Kamloops, B.C. V2C 6T4
Phone (250) 573-5700 Fax (250) 573-4557
email: ecotech@mail.wkpowerlink.com

CERTIFICATE OF ASSAY AK 98-659

GEOQUEST CONSULTING 28-Oct-98
8055 ASPEN ROAD
VERNON, B.C.
V1B 3M9

ATTENTION: WARNER GRUENWALD

No. of samples received: 5
Sample type: Rock
PROJECT #: 74
SHIPMENT #: None Given
Samples submitted by: W. Gruenwald

ET #.	Tag #	Cu (%)
4	LOTTIE MAIN A	15.60
5	LOTTIE MAIN B	1.77

QC/DATA:
Repeat:

4	LOTTIE MAIN A	15.70

Standard:

Mp-IA	1.44

ECO-TECH LABORATORIES LTD.
Frank J. Pezzotti, A.Sc.T.
B.C. Certified Assayer

XLS/98

20-Nov-98

ECO-TECH LABORATORIES LTD.
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ICP CERTIFICATE OF ANALYSIS AK 98-699

GEOQUEST CONSULTING LTD.
8055 ASPEN ROAD
VERNON, B.C.
V1B 3M9

ATTENTION: WARNER GRUENWALD

No. of samples: 39
Sample type: Soil
PROJECT #: 74
SHIPMENT #: None Given
Samples submitted by: W. Gruenwald

Values in ppm unless otherwise reported

Et #.	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
1	L-1 E 0+25 S	<0.2	1.81	10	220	10	0.84	<1	23	54	45	4.13	<10	0.89	810	<1	0.02	39	710	12	<5	<20	21	0.18	<10	78	<10	8	63
2	L-1 E 0+75 S	<0.2	2.61	5	405	<5	0.82	<1	20	76	53	4.42	<10	0.80	889	<1	0.01	39	540	14	<5	<20	18	0.12	<10	98	<10	10	74
3	L-1 E 1+25 S	<0.2	2.16	10	285	<5	0.81	<1	23	77	58	4.40	<10	0.94	787	<1	0.01	41	450	10	<5	<20	16	0.18	<10	96	<10	6	84
4	L-1 E 1+75 S	0.2	2.51	15	305	<5	0.78	<1	20	90	98	4.46	30	0.77	846	<1	0.01	46	720	12	<5	<20	20	0.10	<10	100	<10	41	74
5	L-1 E 2+75 S	0.4	2.58	45	350	<5	0.83	<1	26	103	173	4.69	80	0.80	1525	<1	<0.01	50	930	14	<5	<20	32	0.08	<10	103	<10	103	79
6	L-1 E 3+25 S	<0.2	2.06	10	205	<5	0.65	<1	17	80	94	3.82	30	0.83	411	<1	<0.01	39	600	12	<5	<20	10	0.13	<10	90	<10	29	60
7	L-1 E 3+75 S	<0.2	2.04	<5	270	5	0.73	<1	19	55	35	4.21	<10	0.74	1464	<1	<0.01	30	1100	10	<5	<20	6	0.19	<10	90	<10	<1	83
8	L-1 E 4+25 S	<0.2	2.33	5	185	5	0.80	<1	14	52	21	4.38	<10	0.86	338	<1	0.01	22	700	8	<5	<20	8	0.21	<10	89	<10	<1	60
9	L-1 E 4+75 S	<0.2	2.06	5	120	15	0.47	<1	11	46	15	3.63	<10	0.48	276	<1	<0.01	14	610	10	<5	<20	4	0.20	<10	88	<10	<1	49
10	L-1 E 0+25 N	<0.2	1.94	<5	180	10	0.50	<1	14	51	19	3.76	<10	0.82	341	<1	<0.01	20	470	10	<5	<20	6	0.19	<10	85	<10	<1	59
11	L-1 E 0+75 N	<0.2	2.20	<5	265	5	0.58	<1	17	64	21	4.21	<10	0.82	428	<1	0.01	22	490	12	<5	<20	13	0.22	<10	99	<10	<1	69
12	L-1 E 1+25 N	<0.2	1.71	<5	190	5	0.93	<1	19	43	29	3.24	<10	0.80	540	<1	0.02	28	560	8	<5	<20	12	0.26	<10	86	<10	1	44
13	L-1 E 1+75 N	<0.2	2.36	<5	166	10	0.47	<1	14	54	19	3.84	<10	0.63	259	<1	0.01	26	650	10	<5	<20	8	0.16	<10	80	<10	<1	68
14	L-1 E 2+25 N	<0.2	2.08	5	125	5	0.40	<1	19	57	24	3.98	<10	0.79	431	<1	<0.01	30	480	12	<5	<20	8	0.16	<10	72	<10	<1	67
15	L-1 E 2+75 N	<0.2	3.07	5	155	15	0.54	<1	18	63	22	4.46	<10	0.65	322	<1	0.02	27	980	10	<5	<20	5	0.27	<10	101	<10	<1	87
16	L-1 E 3+25 N	<0.2	2.66	<5	140	5	0.45	<1	16	47	17	4.38	<10	0.52	250	<1	0.01	22	690	10	<5	<20	7	0.23	<10	91	<10	<1	61
17	L-1 E 3+75 N	<0.2	1.72	<5	145	5	0.68	<1	15	50	18	2.95	<10	0.72	281	<1	0.01	21	310	10	<5	<20	11	0.18	<10	69	<10	<1	49
18	L-1 E 4+25 N	<0.2	2.37	<5	126	10	0.94	<1	23	49	32	4.08	<10	0.78	389	<1	0.01	30	450	8	<5	<20	18	0.25	<10	97	<10	<1	47
19	L-1 E 4+75 N	<0.2	2.74	<5	220	<5	1.29	1	21	69	76	4.48	<10	0.83	1273	<1	0.02	33	670	10	<5	<20	22	0.18	<10	145	<10	30	66
20	L-3 W 0+25 S	<0.2	2.34	10	130	15	0.58	<1	19	50	22	4.14	<10	0.67	346	<1	0.01	25	460	12	<5	<20	7	0.25	<10	88	<10	<1	57
21	L-3 W 0+75 S	<0.2	2.46	5	200	10	0.64	<1	15	54	21	4.12	<10	0.72	293	<1	0.01	30	560	10	<5	<20	12	0.19	<10	80	<10	<1	76
22	L-3 W 1+25 S	<0.2	2.34	<5	155	10	0.62	<1	18	67	28	4.05	<10	0.82	346	<1	0.01	34	600	10	<5	<20	9	0.22	<10	83	<10	<1	61
23	L-3 W 1+75 S	<0.2	2.33	5	275	5	0.61	<1	14	53	16	4.02	<10	0.65	428	<1	0.01	19	730	10	<5	<20	4	0.20	<10	112	<10	<1	59
24	L-3 W 2+25 S	<0.2	2.30	<5	205	10	0.49	<1	15	55	21	5.09	<10	0.69	264	<1	0.01	24	570	10	<5	<20	6	0.23	<10	115	<10	<1	51
25	L-3 W 2+75 S	<0.2	1.81	<5	240	5	0.87	<1	19	73	86	3.76	<10	0.81	768	<1	0.01	43	420	10	<5	<20	16	0.21	<10	80	<10	15	48
26	L-3 W 3+25 S	<0.2	1.84	<5	170	10	0.87	<1	21	56	29	3.71	<10	0.90	592	<1	0.01	34	320	10	<5	<20	14	0.24	<10	83	<10	<1	49
27	L-3 W 3+75 S	<0.2	1.77	<5	245	10	0.54	<1	10	40	17	4.55	<10	0.43	217	<1	0.01	13	750	10	<5	<20	7	0.17	<10	97	<10	<1	63
28	L-3 W 4+25 S	<0.2	2.04	<5	160	15	0.40	<1	18	58	23	4.75	<10	0.71	347	<1	0.01	27	610	10	<5	<20	6	0.24	<10	89	<10	<1	77
29	L-3 W 4+75 S	<0.2	2.04	<5	245	10	0.52	<1	11	48	19	3.38	<10	0.55	239	<1	<0.01	19	460	12	<5	<20	6	0.19	<10	68	<10	<1	45
30	L-3 W 0+25 N	<0.2	2.96	5	160	5	0.84	<1	28	52	34	3.66	<10	0.92	825	<1	0.01	38	470	8	<5	<20	10	0.29	<10	92	<10	<1	53

Et #.	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
31	L-3 W 0+75 N	<0.2	2.23	20	250	15	0.52	<1	20	64	40	5.67	<10	0.61	553	<1	<0.01	29	680	8	<5	<20	9	0.20	<10	112	<10	<1	71
32	L-3 W 1+25 N	<0.2	1.93	<5	195	10	0.74	<1	19	58	26	3.48	<10	0.80	508	<1	0.01	26	490	8	<5	<20	12	0.22	<10	69	<10	<1	60
33	L-3 W 1+75 N	<0.2	2.12	<5	190	10	0.67	<1	19	61	30	3.90	<10	0.83	566	<1	0.01	28	630	10	<5	<20	13	0.19	<10	90	<10	1	65
34	L-3 W 2+25 N	<0.2	2.76	5	155	10	0.64	<1	24	63	28	3.79	<10	0.77	362	<1	0.01	40	850	10	<5	<20	5	0.25	<10	84	<10	<1	55
35	L-3 W 2+75 N	<0.2	1.63	5	115	<5	0.34	<1	12	40	19	3.53	<10	0.57	207	<1	<0.01	19	450	12	<5	<20	8	0.14	<10	87	<10	<1	49
36	L-3 W 3+25 N	<0.2	2.27	<5	130	10	0.55	<1	14	49	23	4.08	<10	0.68	258	<1	0.01	21	710	10	<5	<20	11	0.20	<10	85	<10	<1	72
37	L-3 W 3+75 N	<0.2	2.51	5	140	10	0.53	<1	26	63	26	4.06	<10	0.80	426	<1	0.01	37	860	10	<5	<20	9	0.21	<10	76	<10	<1	90
38	L-3 W 4+25 N	<0.2	1.95	<5	125	5	0.79	<1	13	41	18	3.67	<10	0.66	243	<1	0.01	17	400	10	<5	<20	15	0.21	<10	88	<10	<1	43
39	L-3 W 4+75 N	<0.2	3.19	<5	215	<5	1.44	1	27	106	103	5.41	<10	0.96	1132	<1	0.02	41	510	8	<5	<20	22	0.24	<10	178	<10	39	54

QC/DATA:

Et #.	Tag #	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
Repeat:																													
1	L-1 E 0+25 S	<0.2	1.61	10	220	10	0.79	<1	23	54	46	4.24	<10	0.90	523	<1	0.01	42	760	12	<5	<20	19	0.17	<10	77	<10	7	65
10	L-1 E 0+25 N	<0.2	1.69	10	150	5	0.47	<1	13	50	19	3.75	<10	0.62	338	<1	<0.01	20	460	10	<5	<20	7	0.18	<10	64	<10	<1	58
19	L-1 E 4+75 N	<0.2	2.64	<5	220	<5	1.25	<1	20	88	75	4.48	<10	0.82	1288	<1	0.02	31	640	10	<5	<20	23	0.17	<10	144	<10	31	54
28	L-3 W 4+25 S	<0.2	2.58	<5	155	10	0.43	<1	17	54	22	4.71	<10	0.69	336	<1	0.01	26	600	10	<5	<20	8	0.23	<10	86	<10	<1	76
36	L-3 W 3+25 N	<0.2	2.28	<5	130	15	0.57	<1	14	49	21	4.09	<10	0.76	267	<1	0.01	22	710	10	<5	<20	9	0.21	<10	86	<10	<1	72
Standard:																													
GEO'98		1.2	1.77	65	155	<5	1.64	<1	19	64	81	4.05	<10	0.84	673	<1	0.02	20	640	18	<5	<20	58	0.11	<10	76	<10	5	60
GEO'98		1.2	1.83	65	155	<5	1.75	<1	19	66	81	4.08	<10	0.96	675	<1	0.03	19	640	18	<5	<20	63	0.13	<10	80	<10	6	68

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Appendix E - Writer's Certificate

Writer's Certificate

I, John R. Kerr, of the City of Vancouver, B.C., hereby certify that:

1) I am a member of the Association of Professional Engineers of British Columbia (membership #6858).

2) I am a graduate of the University of British Columbia (1964) with a BASc degree in Geological Engineering. I have practised my profession continuously since graduation.

3) I supervised and assisted with the collection of data as discussed in this report. I am the author of this report, and verify the costs as reported to be true.

4) I am an officer and director of Eureka Resources, Inc., and hold a direct and indirect interest in the shares of the company.

Dated the 15th day of November, 1999

John R. Kerr

John R. Kerr, P. Eng