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ASSESSMENT REPORT

on

GEOLOGICAL, GEOPHYSICAL

AND GEOCHEMICAL SURVEYS

on the

SCOTCHMAN AND STANDARD CROWN GRANTS

E and B CLAIM GROUP

OLIVER AREA

OSOYOOS MINING DIVISION

NTS:	82E/04E and 05E
Latitude:	49°14'55"N
Longitude:	119°39'30"W
Owner:	Alvina and Ernie Kilback
Operator:	Discovery Consultants
Author:	T.H. Carpenter, P.Geo.
Date:	December 20, 1999

GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT

26,146

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SUMMARY

The 1999 exploration program on the E and B property was designed to explore the area of the Scotchman and Standard crown grants for possible extensions of auriferous quartz veins exposed in old workings. Field work was carried out between November 02 and November 05, 1999 and comprised grid establishment followed by soil sampling, a combined magnetometer/VLF-EM survey and a mapping and prospecting program. An air photo interpretation of the property area was carried out on November 26.

On the Standard and Scotchman crown grants two showings comprising quartz veins to 3.5' wide occur in a granite type host rock. The quartz veins contain 1"-2" bands of galena and sphalerite. Grab samples collected from the veins over the years are reported to contain up to 1.60 oz/ton Au, 2.90 oz/ton Ag, 5.65% Pb, 1.55% Zn and 0.12% Cu.

LOCATION AND ACCESS

The claims are located approximately 11 km northwest of Oliver, B.C., 1.5 kms east of Orofino Mountain. The Scotchman and Standard crown grants are centred at 119°39'30"W longitude and 49°14'55"N latitude on NTS maps 082E/04E and 05E.

The crown grants and surrounding E & B claims cover the eastern flank of Orofino Mountain.

Elevations range from 3700' at the eastern edge of the claims to 5200' at the western edge of the claims.

Access to the property can be gained from Oliver via two-wheel drive gravel road for 13 kilometres and four-wheel drive road for 2 kilometres.

PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
T. H. CARPENTER
GEOSCIENTIST

DISCOVERY Consultants	KILBACK
SCOTCHMAN PROPERTY	LOCATION MAP

Date:	Project:	Scale:	N.T.S.:	Mining Div:	Figure:
Dec.16/1999	592	1:10,000,000	B.C.	Osoyoos	1

PROPERTY

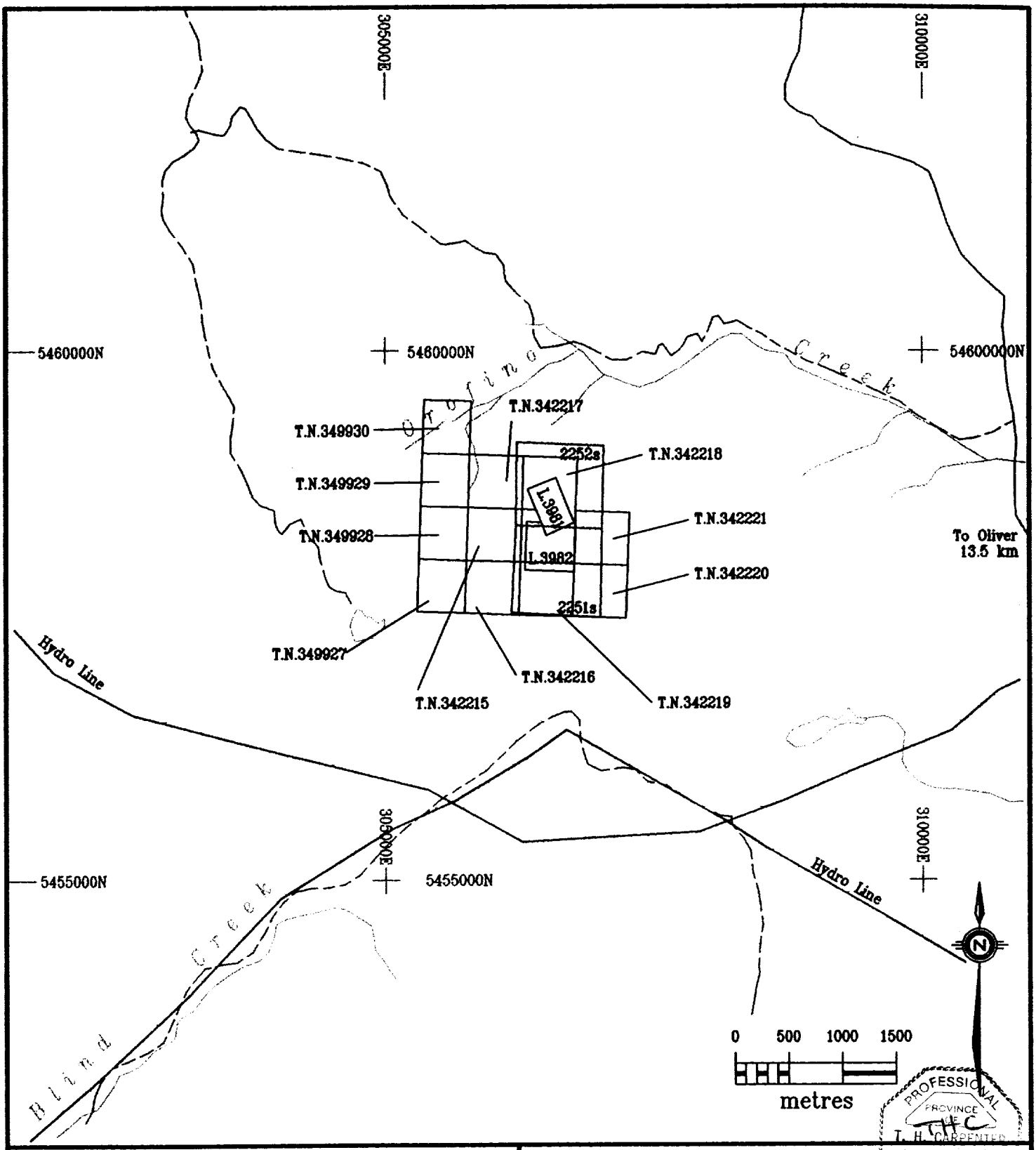
The E & B property comprises two crown-granted mineral claims, the Scotchman and Standard, and eleven two-post claims located by Ernest Kilback on November 16 and 17, 1995 and August 15,1996.

The claims were grouped and assigned a common anniversary date of February 24 on November 15, 1999.

Claim details are as follows:

Claim Name	Record No.	Owner of Record	Anniversary Date *
Scotchman C.G.	L.3981s	Alvina & Ernie Kilback	N/A
Standard C.G.	L.3982s	Alvina & Ernie Kilback	N/A
E & B	342215	Alvina Kilback	February 24, 2004
E & B	342216	Alvina Kilback	February 24, 2004
E & B	342217	Alvina Kilback	February 24, 2004
E & B	342218	Alvina Kilback	February 24, 2004
E & B	342219	Alvina Kilback	February 24, 2004
E & B	342220	Alvina Kilback	February 24, 2004
E & B	342221	Alvina Kilback	February 24, 2004
E + B – 8	349927	Alvina Kilback	February 24, 2004
E + B – 9	349928	Alvina Kilback	February 24, 2004
E + B – 10	349929	Alvina Kilback	February 24, 2004
E + B – 11	349930	Alvina Kilback	February 24, 2004

* Pending acceptance of this report.



DISCOVERY Consultants

KILBACK

Scotchman Property

Claim Location Map

Date:	Dec. 17/1999	Project:	592	Scale:	1:50,000	N.T.S.:	82E/4E,5E	Mining Div:	Osoyoos	Figure:	2

HISTORY

No specific mention of the Standard and Scotchman crown grants is contained in Ministry of Mines annual reports nor have the showings been assigned a Minfile number. The Orofino (L1448) and Independence (L1449) crown grants which lie two kms to the northwest have had work recorded dating from the 1890's. Work on the Orofino claim was first mentioned in 1896 and presumably work was carried out on other properties in the area at that time including the Standard and Scotchman crown grants.

The geology and mineralization of the Orofino and Independence claims appears to be similar to that at the Standard and Scotchman.

Further work was recorded on the Orofino claims from 1930 through 1935 and included production of over 1200 tons of ore with one shipment of 220 tons averaging 1.77 oz/ton gold.

Presumably the open cuts and tunnels on the Standard and Scotchman claims were constructed during the same period. A brief mention is made in the 1934 Minister of Mines report of a Standard crown grant but the location is indefinite and it is uncertain if the reference is to the present Standard property.

From 1981 to 1985 DRC Resources carried out programs of line cutting, rock and soil sampling and ground EM surveys on the Orofino/Independence crown grants and surrounding claims, including the Mo and King claims.

In 1986 Ascent Resources carried out a limited line cutting and soil-sampling program on the Mo 3 & 4 claims.

None of the above work was carried out in the vicinity of Standard and Scotchman crown grants.

J.W. Murton carried out a brief examination of the Scotchman and Standard crown grants for the claim owners in 1986. Another brief examination was carried out in 1990 by Bob Miller on behalf of Crown Resource Corporation.

GEOLOGY

The Orofino Mountain area is underlain by complexly deformed metamorphic rocks of the Carboniferous-Permian(?) Kobau Group, and by west and northwest trending sequences of quartzite, chert and greenstone belonging to the Triassic Shoemaker and Old Tom Formations. These are intruded by the Jurassic-Cretaceous Nelson and Valhalla plutonic complexes of gabbroid to granitic compositions.

The latter are the rock types found on the Scotchman and Standard claims (Figure 3). Mapping has shown four rock types on the ground grants consisting of granite and mega-crystic granite, diorite and gneiss.

Granite forms the principal rock type. Occasional gneissic outcrops may represent remnants of the Kobau Group occurring as rafts or roof pendants.

MINERALIZATION

Gold mineralization occurs in quartz veins cutting porphyritic granite. Similar mineralization was mined in the 1930's from the Orofino and Independence claims (M.I. #082ESW010) 2 km to the west and at the important Fairview camp, 6 km to the southwest.

On the Scotchman claim, a faulted quartz vein, 0.5 to 1.5 metres in width, strikes 070° to 080° with a 40° northwesterly dip. The main vein material is rusty and shattered bull quartz with minor galena and pyrite. Intensely altered & bleached granite wall rock, cut by quartz stringers, is locally incorporated into the vein structure.

Sampling by Murton (1987) and Miller (1990) yielded gold values ranging from 0.002 oz/ton in grab samples to 0.912 oz/tonne across 0.9m.

On the Standard claim sampling by Miller returned values to 2370 ppb gold over 0.9 metres.

STRUCTURE

At the Scotchman showing the main quartz vein is offset 1-2 metres by northerly trending shears. These shears are probably related to a north-south fault zone interpreted from an air photo examination (Figure 11). This fault corresponds to a topographic low on the property. A second parallel structure is interpreted from air photos to occur about 500 metres east of the above fault. Both structures appear to be offset laterally to the northeast by an interpreted north-northeast trending structure to the north of the Scotchman crown grant.

WORK COMPLETED

A program of gridding, geochemical sampling, geophysical surveying, mapping and prospecting was carried out on the property during the period November 02 to November 05, 1999.

Soil sampling and geophysical surveys were carried out over a grid established on the property. A picketed baseline was established using the southwest corner survey pin of L.3981s as control. The 300 metre baseline was run east and west using a declination-corrected tripod-mounted Brunton compass. Seven chained and flagged cross-lines were run at 50 metre intervals for 250 metres north and 250 metres south of the baseline. An examination of 1:15,000 scale coloured air photos of the area was carried out at the B.C. Ministry of Forests, Penticton office on November 26 in an attempt to define structural controls on the property.

Details and results of the various surveys carried out over this grid and the air photo interpretation are discussed below.

SOIL SAMPLING SURVEY

a) Program Parameters

Soil samples were collected at 25 metres along the cross lines using shovels. Soil development on the hillside is very poor. The "B" horizon is non-existent to poorly developed. Consequently samples were collected from the "C" horizon and comprised decomposed bedrock at depths ranging from 10 cm to 40 cm.

Soil material was placed in labelled kraft sample bags and shipped to Chemex Labs Ltd. In North Vancouver, B.C. where they were analyzed for gold by the F.A.-A.A. method and for 32 other elements by ICP methods.

b) *Program Results*

Gold values in soils are, in general, low with a maximum value of 45 ppb obtained at 1200 W, 4750N. Most samples contained gold values below the detection limit (Figure 4).

Gold values in soils on the property would necessarily be sporadic due to the nature of the mineralization and the poorly developed nature of the sampling medium. Perhaps a more suitable pathfinder to gold mineralization would be lead or zinc, which occur with gold in the quartz veins and which would be more susceptible to mechanical and chemical dispersion in soils.

Lead values (Figure 5) are also in general low, but show a distinct anomaly over the Standard Showing with a value of 66 ppm, five to six times background. Weak soil anomalies occur in the northwest part of the grid. However an anomaly similar in amplitude to that over the Standard Showing occurs at 1000W, 5200N and is possibly indicative of mineralization in this area.

Average background Zinc values over the grid area average about 75 ppm with values in excess of 100 ppm considered to be anomalous. The highest Zinc value of 148 ppm occurs over the Standard quartz vein as an isolated anomaly. Isolated single point anomalies occur in the northeastern quarter of the grid area including a value of 138 ppm at 1000W, 5200N and corresponds to the anomalous Lead value noted at the same location. A distinct five point anomaly occurs along line 1300W from ~5075N and may be worthy of further exploration.

GEOPHYSICAL SURVEY

A combined magnetometer and VLF-EM survey was run over the grid with stations at 12.5 metre intervals along lines placed 50 metre apart.

Magnetometer Survey

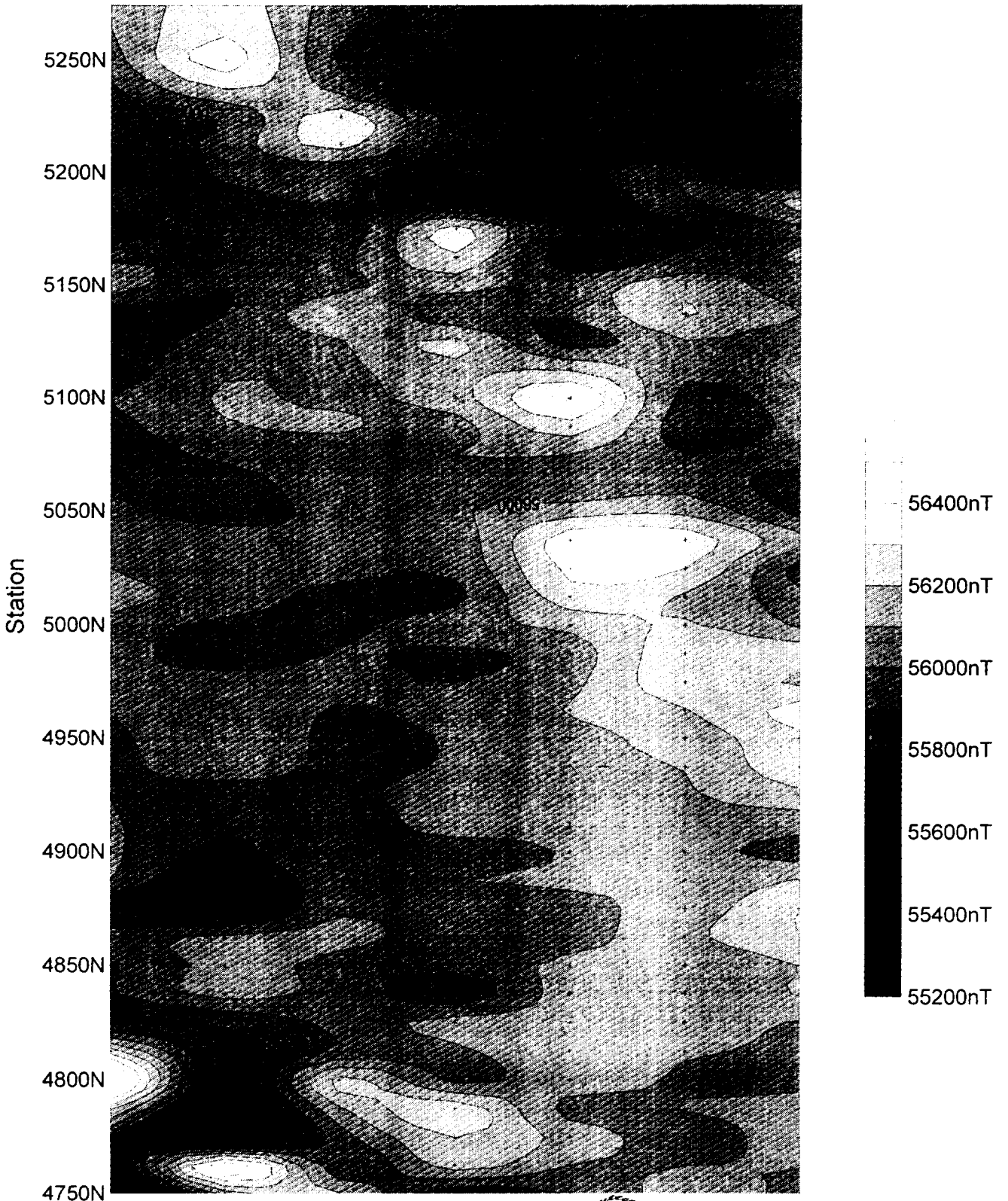
a) Program Parameters

The survey was run using a GEM Systems GSM19v5.0 portable high sensitivity Overhauser effect magnetometer designed for hand-held or base station use. The GSM-19 is a secondary standard for measurement of the Earth's magnetic field, having 0.01 nanoTeslas (nT) resolution and 0.2nT absolute accuracy over its full temperature range. The GSM-19 is a microprocessor based instrument with storing capabilities up to 2Mbytes. Synchronized operation between hand held and base station units is possible and corrections for diurnal variations of magnetic field are done automatically. The results of the measurements are made available in serial form for collection by data acquisition systems, terminals or computers. Both on-line and post-operation transfers are possible. The result is a high quality reading independent of diurnal variations of the magnetic field.

The addition of a VLF sensor allows a combined magnetometer-VLF-EM survey. On the property three VLF surveys were run at frequencies of 21.4 kHz, 24.0 kHz and 24.8 kHz using transmitters located in Hawaii, Cutler, Maine and Seattle respectively.

b) Program Results

Magnetic Readings ranging from 55,200 nanoTeslas (nT) to 56,600 nT were noted in the magnetic survey for a contrast of 1,400 nT. Magnetic contours are shown on Figure 7. Complete magnetometer data are contained in Appendix 3.



Scotchman Property

corrected magnetics
contour interval 100nT
Nov 17, 1999

0 25 50 75 100
metres
(1:2500)

c:/592/12X50A.srf

Fig_7

Of particular interest is a magnetic linear extending in a westerly direction from approximately 1000W, 4950N to 1250W, 5250N. This feature corresponds in part to dioritic rocks mapped at 5000N, 1030W and may indicate that this rock type extends as a possible dyke in a northwesterly direction. None of the mineralized quartz veins on the property are located within this magnetic feature which may indicate that it post dates or is contemporaneous with mineralization. However there is some indication that this feature may be locally offset by a north-northeasterly trending fault, locally mapped on the claims and interpreted from air photos (Figure 11).

The quartz veining on the property occurs in areas of lower magnetic relief. However it is not possible to trace possible extensions of the veins utilizing collected data. A more detailed survey on tight grids within the vicinity of the veins may be more successful in this regard.

VLF-EM Survey

a) Program Parameters

A very Low Frequency Electromagnetic survey was carried out on the property in conjunction with the Magnetometer Survey. The VLF survey comprised three individual surveys utilizing U.S. Navy transmitters located in Hawaii (21.4 kHz), Cutler, Maine (24.0 kHz) and Seattle, Washington (24.8 kHz).

Field data were converted to Fraser Filter data for ease of interpretation. Individual surveys are shown on Figures 8, 9 and 10. Field data and details of the Fraser Filter process are contained in Appendix 4.

b) Program Results

All three frequencies appear to show two conductors extending east-northeasterly from approximately 4875N and 5025N. These anomalies are most well defined on the Seattle and Hawaii frequencies (Figures 8 and 10).

These anomalies are in contrast to the geology and the magnetometer survey and may represent a bias error within the data sets.

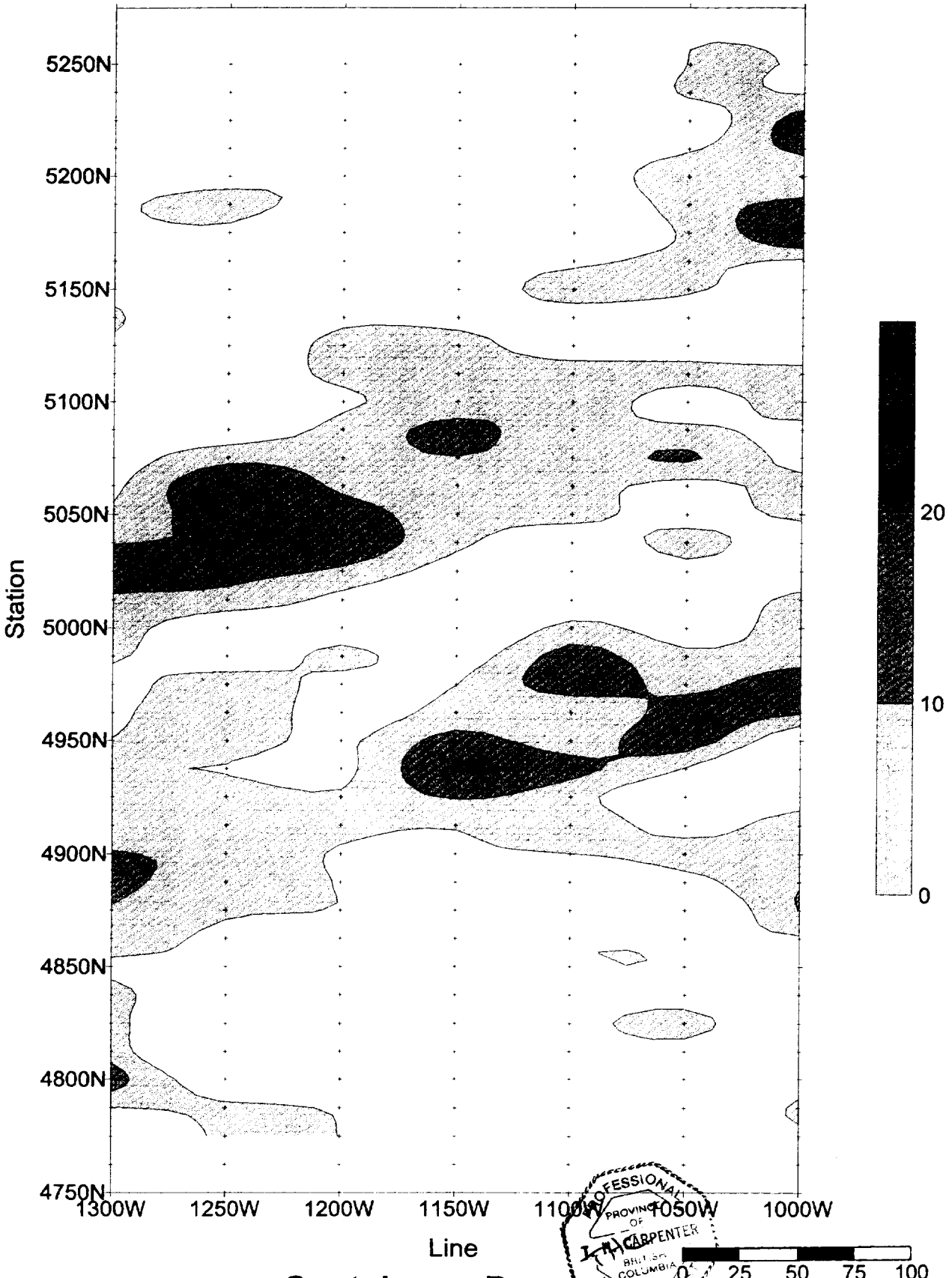
Analysis of the data could also show several conductors trending in a northwesterly direction parallel to the magnetic feature previously noted. One of these conductors would then extend from 1250W, 5190N in a southwesterly direction to 1150W,5090N and from 1100W,4990N to 1050W,4950N.

This proposed conductor might be offset dextrally by the fault interpreted from air photos.

MAPPING AND PROSPECTING

a) Program Parameters

A mapping and prospecting program was carried out on the grid area at a scale of 1:1000. Chip samples were collected from any quartz veining encountered. In total six rock samples were collected. Details of the mapping program and rock sample locations are shown of Figure 3 and 3a at scales of 1:5000 and 1:2500 respectively. Complete analytical results are contained in Appendix 2. . Prospecting for additional mineralization was hampered during the time of the program by snow cover.



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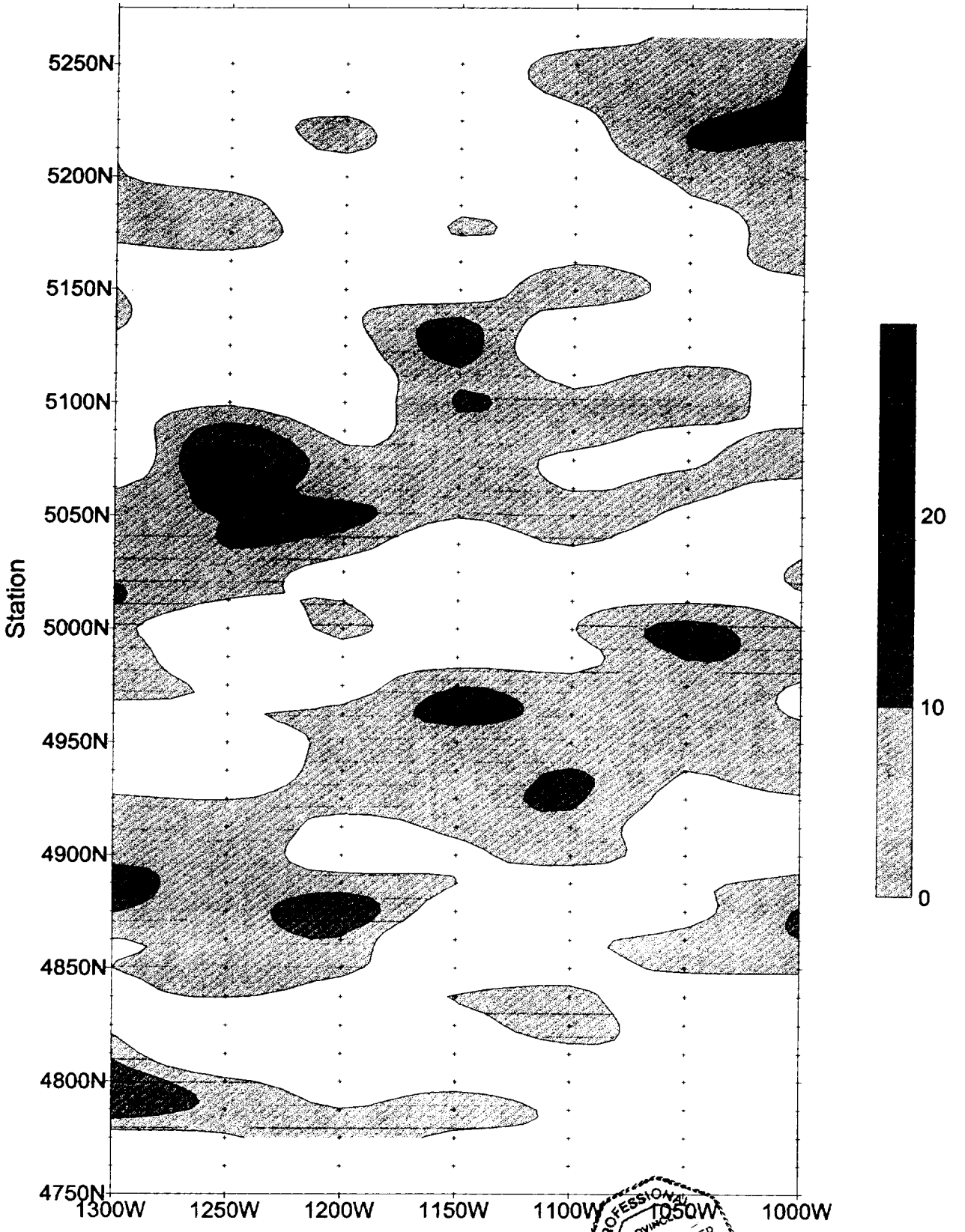
Scotchman Property

VLF Fraser Filter values
frequency: 21.4 kHz (Hawaii)

Nov 17, 1999

Fig. 8



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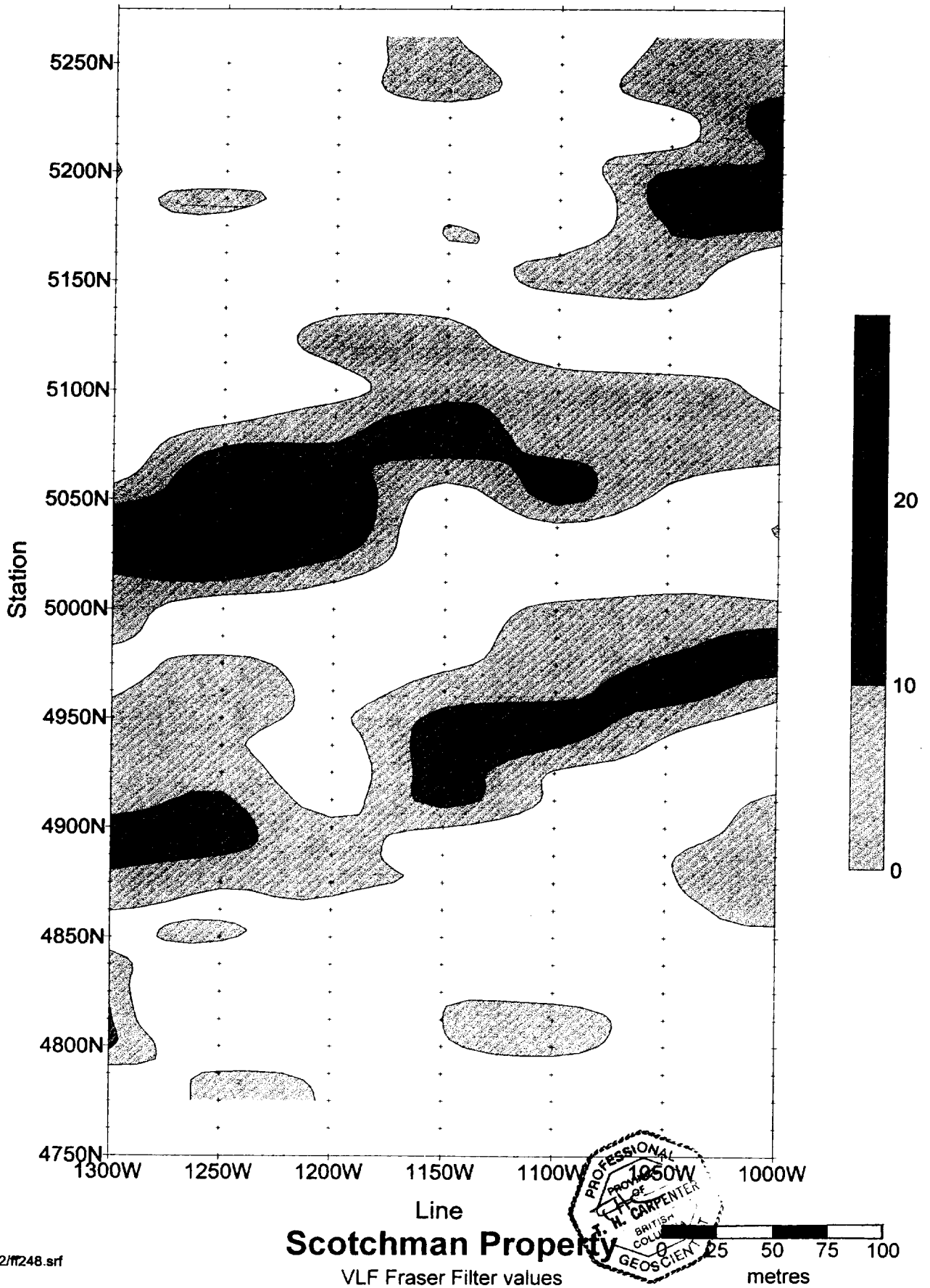
Scotchman Property

VLF Fraser Filter values
frequency: 24.0 kHz (Cutler)

Nov 17, 1999

Fig. 9



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Scotchman Property

VLF Fraser Filter values
frequency: 24.8 kHz (Seattle)

Nov 17, 1999

Fig. 10

b) Program Results

The predominant rock type on the property comprises megacrystic granite. In the east central part of the grid, diorite outcrops are located along the baseline from 1000W to 1035W. These outcrops coincide in part with a magnetic high extending northwesterly. Other outcrops of gneissic material occur to the north and northwest of this location and may represent rafts or roof pendants of Kobau Group metamorphic rocks.

The maximum gold value obtained from the six rock samples collected was 60 ppb in sample 197805. No attempt was made to duplicate previous sampling. A thorough program of channel sampling would need to be carried out on the quartz veins to accurately determine the gold content and overcome the sporadic results generated by grab and chip sampling.

AIR PHOTO INTERPRETATION

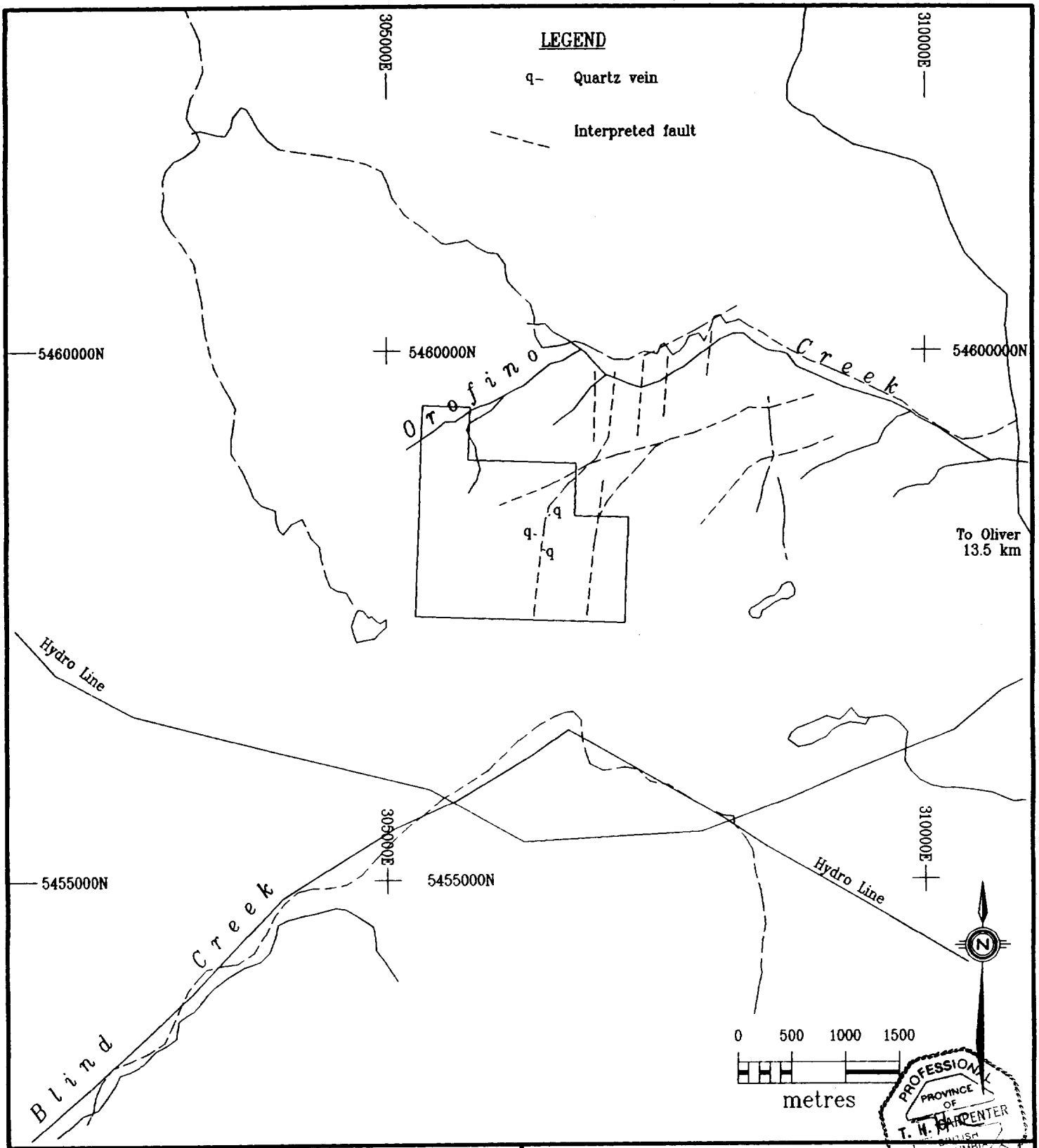
a) Program Parameters

A stereoscopic examination of 1:15,000 scale coloured air photos of the project area was carried out at the B.C. Ministry of Forests office in Penticton, B.C.

b) Program Results

Results of the interpretation are shown on Figure 11.

Two distinct linears are noted on the property, trending in the north-south direction. The westerly of these linears corresponds with an interpreted fault on the Scotchman and Standard claims which occurs in close proximity to mineralized quartz veins. At the Scotchman showing the mineralized quartz vein is offset by a northerly trending shear which may be a part of a larger shear zone as interpreted from the air photo (Figure 11).



DISCOVERY Consultants

KILBACK

Scotchman Property

Air Photo Interpretation

Date:	Dec. 17/1999	Project:	592	Scale:	1:50,000	N.T.S.:	82E/4E,5E	Mining Div:	Osoyoos	Figure:	11

This interpreted fault corresponds to a topographic low extending from the Scotchman showing southerly to the area of the Standard showing (Figures 3 and 3a).

The quartz veining on the property may be dilatant zones or splays off this fault. If quartz veining on the property is related to these structures then later movement along the faults is postulated by the apparent vein offset at the Scotchman showing.

The second linear occurs above 500 metres east of the above but has not been observed in outcrop nor is any quartz veining known to be associated with this feature.

Both linears appear to continue to the north but are offset about 500 metres easterly by a northeast trending linear that occurs near the northeast corner of the claim block.

CONCLUSIONS

The Standard and Scotchman crown grants contain mineralized quartz veins up to 3.5-ft. (1.07m). Previous sampling of these veins has yielded values to 1.6 oz./ton Au in grab samples and 0.912 oz/tonne across 0.9 metres in a chip sample. Limited rock sampling in the recent exploration program has not duplicated these values but has confirmed anomalous gold values within the quartz veins.

The veins occur within granitic rocks and appear to be associated with a north-south trending fault zone interpreted from air photos and mapped locally in outcrop and may be emplaced in dilatant zones related to this fault or possibly splays off the fault. A second parallel fault zone is interpreted 500 metres to the east.

These veins are in a setting similar to the Elk deposit some 80 km northwest which in 1995 contained measured reserves of 156,000 tonnes containing 36.55 grams per tonne gold and 50.00 grams per tonne silver. At the Elk deposit structurally controlled quartz veining occurs in a number of parallel to subparallel zones. In the Siwash North zone of the Elk deposit, the structure has a strike length of 925 metres and has been tested to 335 metres down dip.

Soil sampling has not been successful in delineating additional gold mineralization away from known showings. Anomalous lead and zinc soil values over the Standard showing indicate that these elements may be useful as pathfinder elements on the property and may indicate that areas with anomalous Pb and Zn values should be further explored.

Prospecting may provide a more useful tool on the property than soil sampling as the soil cover is relatively thin and quart material in float should be readily apparent.

The magnetometer survey shows that quartz veining occurs in areas of lower magnetic relief and appears to be unrelated to a magnetic high which transects the Scotchman crown grant

and which appears to be caused by late stage mafic intrusive rocks. An orientation survey confirms that the known quartz veins occur as magnetic lows. Quite detailed magnetic surveys would need to be carried out to trace these veins away from known showings.

The results of the VLF-EM survey are somewhat ambiguous, possibly due to a contouring bias within the computer software used. The results show northeast trending conductors in the grid area. There is no reflection of this trend in bedrock based on present work. The data do appear to confirm however the north-south fault zone interpreted from air photos and mapping as an offset to a proposed northwest trending conductor can be interpreted.

RECOMMENDATIONS

Additional mapping and prospecting on the property are recommended to check for additional quartz veining in outcrop and float. At the time of the present program snow cover precluded detailed claim coverage and prospecting.

Particular emphasis should be placed on prospecting along the interpreted north-south fault zone, along an interpreted parallel structure to the east, and within the area of anomalous zinc and lead values in the grid area to explore for additional quartz veining in these areas. Prospecting should be concentrated on finding quartz float away from known showings.

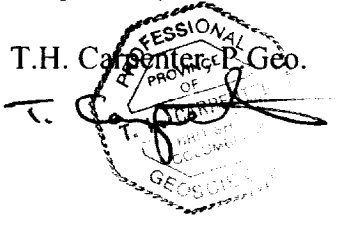
The area of northeast trending VLF conductors on the grid should be investigated to determine if these conductors accurately reflect bedrock conditions.

Detailed magnetometer surveys could be carried in areas of soil anomalies to help define magnetic lows associated with possible recessive quartz veins.

Trenching and sampling should be carried out on any quartz veining defined by the above program. Drilling should be carried out only if defined veins are of sufficient size to develop significant reserves of gold mineralization similar to those at the Elk property.

Respectfully submitted,

T.H. Carpenter, P.Geo.



Vernon, BC
December 20, 1999

REFERENCES

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Miller, R., 1990 Scotchman L-3981 and Standard L-3982 claims, Oliver, B.C. for Crown Resource Corporation, Denver, Colorado.

Hedley, M.S. and K. DeP. Watson, 1945 British Columbia Ministry of Energy, Mines and Petroleum Resources, Bulletin 20, Part III, pg. 19

Annual Report – 1933, British Columbia Ministry of Mines, pg. 168

Annual Report – 1934, British Columbia Ministry of Mines, pg. D16

STATEMENT OF COSTS
E & B Property

1	Professional Services			
	K.L. Daughtry (P.Eng.)			
	Field Examination & Planning			
	1.0 days @$450/day	$ 450.00		
	T. Carpenter (P.Geo.)			
	Planning, Airphoto Interpretation, & Reporting			
	2.5 days @$450/day	1,125.00		
	R. Tilsley (Geol.) Nov. 2 - 5			
	Mapping & Rock Sampling			
	4.0 days @$425/day	1,700.00		
	Data Compilation – Nov. 6			
	0.5 days @$375/day	187.50		
				$ 3,462.50
2	Field Personnel			
	John Osterhagen (Nov. 2 - 5)			
	Grid Establishment, Soil Sampling & Geophysics			
	4.0 days @$375/day	1,500.00		
	Melvin Kilback (Nov. 2 - 5)			
	Grid Establishment, Soil Sampling			
	4.0 days @$185/day	740.00		
				2,240.00
3	Office Personnel			
	Drafting	350.00		
	Secretarial	200.00		
	Data Compilation (incl JO ½day)	178.93		
				728.93
4	Expenses			
	Analysis - Chemex Labs Ltd.			
	(Au + 32 elements ICP)			
	6 Rocks @$18.28/sample		$ 109.68	
	77 soils @15.92/sample		1,225.84	
	Field Supplies		40.20	
	Equipment Rental		291.00	
	Freight		24.36	
	Lodging & Meals		341.71	
	Maps & Publications		35.00	
	Communications, Report & Map printing		150.00	
	Management Fee		206.32	
				2,424.11
		Exploration Costs :		$ 8,855.54
5	Transportation			
	a) 4x4 Truck	4 days @$40.00/day	$ 160.00	
		527km @30¢/km	158.10	
	gas		43.46	
			$ 361.56	
	b) @20% of Exploration Costs of $8,855.54		$1,771.11	
	(a) or (b) - whichever is less			361.56
		Total Exploration Costs :		$ 9,217.10

STATEMENT OF QUALIFICATIONS

I, THOMAS H. CARPENTER of 3902 14th Street, Vernon, B.C. V1T 3V2, DO HEREBY CERTIFY that:

1. I am a consulting geologist in mineral exploration with Discovery Consultants, Vernon B.C.

2. I am a 1971 graduate of the Memorial University of Newfoundland with a Bachelor of Science degree in geology.

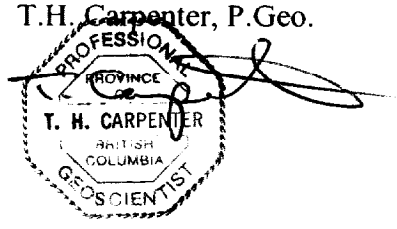
3. I have been practicing my profession since graduation.

4. I am a Professional Geoscientist with the Association of Professional Engineers and Geoscientists of British Columbia.

5. This report is based upon knowledge of the Scotchman and Standard property gained from research, observation and supervision.

6. I hold no interest either directly or indirectly in the Scotchman or Standard crown grants or the E & B claims.

T.H. Carpenter, P.Geo.



December 20, 1999
Vernon, B.C.

APPENDIX 1

Soil Sampling Program

ANALYTICAL PROCEDURES

Geochemical Analysis

by Chemex Labs Ltd.

ELEMENT		LOWER DETECTION LIMIT	EXTRACTION	METHOD
Au	Gold	5 ppb	fire assay	A.A.
Al*	Aluminum	0.01%	Aqua-Regia digestion	Ind. Coupled Plasma
Sb	Antimony	2 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
As	Arsenic	2 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Ba*	Barium	10 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Be*	Beryllium	0.5 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Bi	Bismuth	2 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Cd	Cadmium	0.5 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Ca*	Calcium	0.01%	Aqua-Regia digestion	Ind. Coupled Plasma
Cr*	Chromium	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Co	Cobalt	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Cu	Copper	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Ga*	Gallium	10 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Fe	Iron	0.01%	Aqua-Regia digestion	Ind. Coupled Plasma
La*	Lanthanum	10 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Pb	Lead	2 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Mg*	Magnesium	0.01%	Aqua-Regia digestion	Ind. Coupled Plasma
Mn	Maganese	5 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Hg	Mercury	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Mo	Molybdenum	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Ni	Nickel	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
P	Phosphorus	10 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
K*	Potassium	0.01%	Aqua-Regia digestion	Ind. Coupled Plasma
Sc*	Scandium	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Ag	Silver	0.2 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Na*	Sodium	0.01%	Aqua-Regia digestion	Ind. Coupled Plasma
Sr*	Strontium	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Tl*	Thallium	10 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Ti*	Titanium	0.01%	Aqua-Regia digestion	Ind. Coupled Plasma
W*	Tungsten	10 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
U	Uranium	10 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
V	Vanadium	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Zn	Zinc	2 ppm	Aqua-Regia digestion	Ind. Coupled Plasma

* Incomplete digeston.

Project 592

Standard/Scotchman

file: 592\geodata\Rock_99.wk4

Soil Sample Analyses
1999

Reference : a9933736

Sample ID	Lab report #	30g FA/AA Au ppb	ICP Ag ppm	ICP As ppm	ICP Sb ppm	ICP Cu ppm	ICP Pb ppm	ICP Zn ppm	ICP W ppm	ICP Cd ppm	ICP Mo ppm	ICP Bi ppm	ICP Ni ppm	ICP Co ppm	ICP Cr ppm	ICP Fe %	ICP Mn ppm
1000W-4750N	a9933736	<5	<0.2	4	<2	20	8	60	<10	<0.5	1	<2	14	10	23	2.47	565
1000W-4800N	a9933736	<5	<0.2	2	<2	20	8	48	<10	<0.5	1	<2	12	9	20	2.21	345
1000W-4850N	a9933736	<5	<0.2	6	<2	24	6	58	<10	0.5	<1	<2	13	10	26	2.60	460
1000W-4900N	a9933736	<5	<0.2	6	<2	20	6	68	<10	<0.5	<1	<2	14	11	26	2.71	555
1000W-4950N	a9933736	20	<0.2	6	<2	24	4	118	<10	<0.5	<1	<2	13	9	19	2.29	860
1000W-5000N	a9933736	<5	<0.2	6	<2	23	8	174	<10	0.5	1	<2	14	14	23	3.12	2280
1000W-5050N	a9933736	<5	<0.2	6	<2	18	6	92	<10	<0.5	1	<2	15	12	24	2.93	1235
1000W-5100N	a9933736	<5	<0.2	6	<2	20	6	66	<10	<0.5	1	<2	15	11	27	2.77	925
1000W-5150N	a9933736	<5	<0.2	<2	<2	15	6	58	<10	<0.5	1	<2	15	9	22	2.17	570
1000W-5200N	a9933736	5	<0.2	6	<2	23	58	138	<10	1.5	1	<2	16	13	26	2.94	590
1000W-5250N	a9933736	<5	<0.2	6	<2	17	6	58	<10	<0.5	<1	<2	16	9	26	2.38	445
1050W-4750N	a9933736	<5	<0.2	6	<2	23	12	130	<10	<0.5	1	<2	13	14	22	3.72	935
1050W-4800N	a9933736	<5	<0.2	6	<2	20	8	60	<10	<0.5	<1	<2	15	11	27	2.72	650
1050W-4850N	a9933736	5	<0.2	6	<2	18	8	80	<10	<0.5	1	<2	15	11	25	2.83	805
1050W-4900N	a9933736	<5	<0.2	2	<2	14	4	60	<10	1.5	1	<2	7	6	11	1.37	455
1050W-4950N	a9933736	<5	<0.2	6	<2	15	6	64	<10	<0.5	<1	<2	12	9	21	2.35	420
1050W-5000N	a9933736	<5	<0.2	4	<2	15	8	70	<10	<0.5	1	<2	14	11	24	2.73	590
1050W-5050N	a9933736	<5	<0.2	6	<2	16	8	54	<10	<0.5	1	<2	15	10	27	2.48	435
1050W-5100N	a9933736	<5	<0.2	2	<2	18	8	100	<10	<0.5	1	<2	15	10	25	2.52	1210
1050W-5150N	a9933736	<5	<0.2	6	<2	16	6	76	<10	<0.5	1	<2	14	11	24	2.64	700
1050W-5200N	a9933736	<5	<0.2	4	<2	25	10	68	<10	<0.5	1	<2	18	11	29	2.75	490
1050W-5250N	a9933736	<5	<0.2	6	<2	17	8	80	<10	<0.5	1	<2	15	10	30	2.71	405
1075W-5250N	a9933736	<5	<0.2	<2	<2	12	6	42	<10	<0.5	1	<2	12	8	17	1.89	480
1100W-4750N	a9933736	<5	<0.2	10	<2	22	10	88	<10	<0.5	<1	<2	15	14	28	3.49	1045
1100W-4800N	a9933736	<5	<0.2	6	<2	17	6	72	<10	<0.5	1	<2	14	12	27	3.31	480
1100W-4850N	a9933736	<5	<0.2	6	<2	16	6	74	<10	<0.5	1	<2	14	12	25	2.96	615
1100W-4900N	a9933736	<5	<0.2	2	<2	23	12	90	<10	0.5	1	<2	13	10	21	2.41	555
1100W-4950N	a9933736	<5	<0.2	8	<2	15	6	54	<10	<0.5	1	<2	13	8	21	2.12	330
1100W-5000N	a9933736	<5	<0.2	6	<2	14	6	62	<10	<0.5	<1	<2	14	9	22	2.35	455
1100W-5050N	a9933736	<5	<0.2	<2	<2	21	6	54	<10	<0.5	<1	<2	14	11	29	2.98	350
1100W-5100N	a9933736	<5	<0.2	2	<2	27	4	176	<10	<0.5	<1	<2	12	10	20	2.34	1770
1100W-5150N	a9933736	5	<0.2	6	<2	16	6	64	<10	<0.5	1	<2	13	9	21	2.29	495
1100W-5200N	a9933736	<5	<0.2	6	<2	17	8	82	<10	<0.5	1	<2	10	7	15	1.93	530
1100W-5250N	a9933736	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s
1150W-4750N	a9933736	<5	<0.2	6	<2	22	8	100	<10	<0.5	<1	<2	14	14	25	3.25	960
1150W-4800N	a9933736	<5	<0.2	4	<2	15	10	92	<10	<0.5	1	<2	14	12	24	3.04	700
1150W-4850N	a9933736	<5	<0.2	2	<2	18	10	68	<10	<0.5	1	<2	13	10	21	2.47	585
1150W-4900N	a9933736	<5	<0.2	6	<2	17	66	148	<10	2.0	1	<2	13	11	23	2.78	1230
1150W-4950N	a9933736	<5	<0.2	2	<2	15	10	80	<10	<0.5	1	<2	17	10	23	2.58	695
1150W-5000N	a9933736	<5	<0.2	4	<2	19	6	68	<10	<0.5	1	<2	14	10	27	2.66	490
1150W-5050N	a9933736	<5	0.2	4	<2	43	8	34	<10	<0.5	1	<2	22	8	22	2.42	500
1150W-5100N	a9933736	<5	<0.2	6	<2	35	8	52	<10	<0.5	<1	<2	17	9	20	2.37	590
1150W-5150N	a9933736	<5	<0.2	2	<2	11	4	58	<10	<0.5	<1	<2	11	8	22	2.21	380
1150W-5200N	a9933736	<5	<0.2	4	<2	13	6	52	<10	<0.5	1	<2	12	8	23	2.42	365
1150W-5250N	a9933736	<5	<0.2	6	<2	19	12	112	<10	0.5	1	<2	14	11	24	2.94	2160
1200W-4750N	a9933736	<5	<0.2	2	<2	15	6	64	<10	<0.5	<1	<2	13	11	27	2.79	610
1200W-4800N	a9933736	<5	0.2	6	<2	24	10	76	<10	<0.5	1	<2	14	12	27	2.90	555
1200W-4850N	a9933736	45	<0.2	6	<2	16	10	76	<10	<0.5	<1	<2	13	10	26	2.63	555
1200W-4900N	a9933736	<5	<0.2	4	<2	17	6	74	<10	<0.5	<1	<2	12	9	20	2.33	650
1200W-4950N	a9933736	<5	<0.2	6	<2	23	10	62	<10	<0.5	1	<2	15	9	22	2.40	410
1200W-5000N	a9933736	<5	<0.2	8	<2	13	8	48	<10	<0.5	1	<2	13	9	22	2.26	445
1200W-5050N	a9933736	<5	<0.2	2	<2	12	8	30	<10	<0.5	1	<2	12	7	18	1.98	175
1200W-5100N	a9933736	5	<0.2	2	<2	24	6	54	<10	<0.5	1	<2	16	9	20	2.25	425
1200W-5150N	a9933736	<5	<0.2	4	<2	14	6	78	<10	<0.5	<1	<2	12	8	18	2.12	650
1200W-5200N	a9933736	<5	<0.2	8	<2	21	6	98	<10	<0.5	1	<2	14	11	26	2.96	1275
1200W-5250N	a9933736	<5	<0.2	6	<2	15	4	66	<10	<0.5	1	<2	14	10	25	2.84	360
1250W-4750N	a9933736	<5	<0.2	6	<2	17	16	72	<10	<0.5	1	<2	13	10	26	2.80	515
1250W-4800N	a9933736	5	<0.2	8	<2	17	8	62	<10	<0.5	<1	<2	14	10	23	2.46	630
1250W-4850N	a9933736	<5	<0.2	2	<2	14	12	94	<10	<0.5	<1	<2	14	10	25	2.74	650
1250W-4900N	a9933736	<5	<0.2	4	<2	17	10	72	<10	<0.5	<1	<2	15	10	24	2.55	580
1250W-4950N	a9933736	<5	<0.2	6	<2	20	6	58	<10	<0.5	1	<2	13	9	23	2.68	480
1250W-5000N	a9933736	25	<0.2	4	<2	16	8	62	<10	<0.5	<1	<2	13	8	22	2.33	535
1250W-5050N	a9933736	<5	<0.2	2	<2	18	8	92	<10	<0.5	1	<2	12	10	22	2.53	1410
1250W-5100N	a9933736	5	0.2	10	<2	22	10	118	<10	<0.5	<1	<2	15	10	21	2.40	430
1250W-5150N	a9933736	<5	<0.2	2	<2	16	4	10	<10	<0.5	<1	<2	4	2	5	0.65	40
1250W-5200N	a9933736	<5	<0.2	2	<2	19	10	70	<10	<0.5	3	<2	12	9	21	2.53	640
1250W-5250N	a9933736	<5	<0.2	4	<2	25	8	54	<10	<0.5	1	<2	12	8	18	2.18	425
1300W-4750N	a9933736	<5	<0.2	8	<2	29	12	68	<10	<0.5	<1	<2	14	11	23	2.71	405
1300W-4800N	a9933736	<5	<0.2	2	<2	22	10	96	<10	<0.5	1	<2	17	13	27	3.38	550
1300W-4850N	a9933736	5	<0.2	8	<2	19	12	78	<10	<0.5	1	<2	14	10	24	3.16	360
1300W-4900N	a9933736	<5	<0.2	10	<2	19	8	88	<10	<0.5	<1	<2	14	11	24	2.94	495

Standard/Scotchman

Soil Sample Analyses (part 2)

Sample ID	ICP Ba ppm	ICP V ppm	ICP Hg ppm	ICP Sr ppm	ICP La ppm	ICP Al %	ICP Mg %	ICP Ca %	ICP Na %	ICP K %	ICP Ti %	ICP U ppm	ICP Be ppm	ICP Ga ppm	ICP P ppm	ICP Sc ppm	ICP Tl ppm	ICP B ppm	ICP S %
1000W-4750N	170	54	<1	35	10	2.24	0.45	0.28	0.01	0.13	0.11	<10	0.5	<10	920	3	<10	<10	0.01
1000W-4800N	100	48	<1	36	20	2.27	0.38	0.31	0.01	0.08	0.10	<10	0.5	<10	1100	3	<10	<10	0.01
1000W-4850N	150	59	<1	52	10	1.70	0.54	0.59	0.01	0.13	0.09	<10	<0.5	<10	1810	3	<10	<10	0.01
1000W-4900N	150	59	<1	44	10	2.38	0.51	0.42	0.01	0.11	0.10	<10	0.5	<10	1940	4	<10	<10	0.01
1000W-4950N	360	43	<1	67	10	2.20	0.39	0.55	0.01	0.22	0.10	<10	<0.5	<10	3290	3	<10	<10	0.01
1000W-5000N	540	55	<1	86	<10	2.51	0.70	0.93	0.01	0.28	0.13	10	0.5	<10	3570	3	<10	<10	0.01
1000W-5050N	270	60	<1	48	10	2.53	0.52	0.46	0.01	0.20	0.12	<10	0.5	<10	1170	3	<10	<10	0.01
1000W-5100N	180	61	<1	54	20	2.11	0.47	0.46	0.01	0.15	0.11	<10	0.5	<10	1600	3	<10	<10	0.01
1000W-5150N	190	46	<1	43	10	2.07	0.34	0.44	0.01	0.14	0.10	<10	0.5	<10	940	3	<10	<10	<0.01
1000W-5200N	210	69	<1	43	10	2.46	0.64	0.40	0.01	0.18	0.12	<10	0.5	<10	1830	4	<10	<10	<0.01
1000W-5250N	210	49	<1	38	10	2.13	0.42	0.39	0.03	0.14	0.10	<10	<0.5	<10	1460	4	<10	<10	<0.01
1050W-4750N	170	75	<1	56	30	2.56	0.82	0.50	0.01	0.18	0.12	<10	0.5	10	2560	4	<10	<10	0.02
1050W-4800N	170	60	<1	50	10	2.25	0.51	0.42	0.01	0.15	0.11	<10	0.5	<10	1190	3	<10	<10	0.01
1050W-4850N	160	59	<1	38	20	2.53	0.57	0.34	0.01	0.16	0.13	<10	0.5	<10	1420	4	<10	<10	0.01
1050W-4900N	120	28	<1	28	10	1.22	0.23	0.34	0.01	0.09	0.05	<10	<0.5	<10	1170	1	<10	<10	<0.01
1050W-4950N	170	48	<1	38	10	2.37	0.42	0.29	0.01	0.14	0.10	<10	0.5	<10	1410	3	<10	<10	0.01
1050W-5000N	170	59	<1	39	10	2.64	0.50	0.29	0.01	0.12	0.13	<10	0.5	<10	690	3	<10	<10	0.01
1050W-5050N	170	55	<1	46	10	2.28	0.43	0.35	0.01	0.14	0.11	<10	0.5	<10	870	3	<10	<10	0.01
1050W-5100N	300	51	<1	53	10	2.04	0.40	0.46	0.01	0.13	0.10	<10	0.5	<10	1570	3	<10	<10	<0.01
1050W-5150N	230	54	<1	47	10	2.42	0.46	0.44	0.02	0.16	0.11	<10	0.5	<10	2050	4	<10	<10	<0.01
1050W-5200N	200	56	<1	54	30	2.75	0.49	0.48	0.03	0.13	0.13	<10	0.5	<10	650	5	<10	<10	0.01
1050W-5250N	190	56	<1	48	20	2.35	0.41	0.41	0.02	0.25	0.12	<10	0.5	<10	750	5	<10	<10	<0.01
1075W-5250N	150	36	<1	35	10	2.33	0.24	0.48	0.03	0.11	0.10	<10	<0.5	<10	730	3	<10	<10	<0.01
1100W-4750N	250	77	<1	60	20	2.76	0.70	0.56	0.01	0.36	0.14	<10	0.5	<10	1030	5	<10	<10	0.01
1100W-4800N	150	75	<1	49	10	2.92	0.67	0.41	0.01	0.17	0.14	<10	0.5	<10	1380	3	<10	<10	0.01
1100W-4850N	180	63	<1	48	10	2.36	0.61	0.40	0.02	0.18	0.12	<10	0.5	<10	1360	4	<10	<10	<0.01
1100W-4900N	210	46	<1	48	50	2.84	0.38	0.44	0.03	0.15	0.12	<10	0.5	<10	1640	4	<10	<10	0.01
1100W-4950N	160	46	<1	45	10	2.08	0.34	0.35	0.03	0.11	0.10	<10	<0.5	<10	1140	3	<10	<10	<0.01
1100W-5000N	210	49	<1	56	10	2.41	0.39	0.33	0.02	0.16	0.11	<10	0.5	<10	1080	3	<10	<10	<0.01
1100W-5050N	140	71	<1	58	10	2.06	0.68	0.43	0.01	0.15	0.15	<10	<0.5	<10	530	4	<10	<10	<0.01
1100W-5100N	820	38	<1	112	10	2.25	0.33	0.93	0.02	0.19	0.08	<10	0.5	<10	3900	4	<10	10	0.01
1100W-5150N	150	48	<1	50	10	2.19	0.31	0.44	0.03	0.14	0.11	<10	<0.5	<10	1070	3	<10	<10	0.01
1100W-5200N	250	33	<1	51	10	2.31	0.25	0.48	0.03	0.11	0.08	<10	0.5	<10	2140	3	<10	<10	0.01
1100W-5250N	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s	n/s
1150W-4750N	290	65	<1	70	20	2.66	0.65	0.52	0.01	0.39	0.13	<10	0.5	<10	1360	4	<10	<10	<0.01
1150W-4800N	210	62	<1	39	10	2.56	0.59	0.33	0.01	0.19	0.13	<10	0.5	<10	1100	3	<10	<10	0.01
1150W-4850N	200	51	<1	38	10	2.63	0.42	0.37	0.02	0.14	0.11	<10	0.5	<10	1520	3	<10	<10	<0.01
1150W-4900N	230	56	<1	45	10	2.22	0.50	0.46	0.01	0.12	0.11	<10	0.5	<10	2430	3	<10	<10	0.02
1150W-4950N	210	54	<1	39	10	2.55	0.46	0.33	0.02	0.11	0.11	<10	0.5	<10	2000	3	<10	<10	<0.01
1150W-5000N	140	60	<1	58	20	2.20	0.50	0.45	0.02	0.12	0.10	<10	0.5	<10	1610	4	<10	<10	<0.01
1150W-5050N	340	40	<1	68	60	3.31	0.29	0.57	0.06	0.11	0.11	<10	1.0	<10	380	6	<10	<10	0.01
1150W-5100N	170	44	<1	57	50	2.68	0.30	0.57	0.03	0.12	0.12	10	0.5	<10	390	4	<10	<10	0.01
1150W-5150N	210	48	<1	47	10	1.63	0.30	0.38	0.02	0.15	0.10	<10	<0.5	<10	940	3	<10	<10	<0.01
1150W-5200N	140	53	<1	51	20	1.88	0.34	0.37	0.01	0.19	0.11	<10	<0.5	<10	640	3	<10	<10	<0.01
1150W-5250N	280	58	<1	57	10	2.42	0.48	0.38	0.01	0.15	0.12	<10	0.5	<10	1590	3	<10	<10	0.03
1200W-4750N	160	64	<1	56	10	1.88	0.49	0.45	0.01	0.18	0.12	<10	<0.5	<10	520	4	<10	<10	<0.01
1200W-4800N	170	68	<1	60	10	1.97	0.53	0.47	0.01	0.10	0.11	<10	<0.5	<10	1380	4	<10	<10	0.01
1200W-4850N	210	57	<1	42	10	2.27	0.42	0.35	0.01	0.13	0.11	<10	0.5	<10	1380	3	<10	<10	<0.01
1200W-4900N	260	47	<1	50	10	2.02	0.41	0.44	0.02	0.14	0.09	<10	<0.5	<10	2040	3	<10	<10	<0.01
1200W-4950N	110	45	<1	43	40	3.14	0.35	0.39	0.03	0.08	0.13	30	1.0	<10	570	5	<10	<10	0.01
1200W-5000N	150	50	<1	42	20	2.03	0.29	0.41	0.03	0.09	0.11	<10	<0.5	<10	470	3	<10	<10	<0.01
1200W-5050N	190	43	<1	48	10	2.57	0.25	0.27	0.04	0.09	0.12	<10	0.5	<10	200	2	<10	<10	<0.01
1200W-5100N	160	46	<1	61	30	2.26	0.30	0.51	0.03	0.15	0.13	<10	<0.5	<10	280	3	<10	<10	<0.01
1200W-5150N	200	41	<1	46	10	2.16	0.32	0.44	0.03	0.17	0.09	<10	<0.5	<10	2110	3	<10	<10	0.01
1200W-5200N	230	63	<1	74	20	2.25	0.48	0.63	0.01	0.22	0.11	<10	<0.5	<10	1470	4	<10	<10	0.02
1200W-5250N	170	66	<1	59	10	2.43	0.42	0.31	0.01	0.11	0.12	<10	0.5	<10	750	3	<10	<10	<0.01
1250W-4750N	180	63	<1	50	10	2.35	0.51	0.39	0.01	0.11	0.12	<10	<0.5	<10	890	3	<10	<10	<0.01
1250W-4800N	190	52	<1	40	10	2.25	0.39	0.44	0.02	0.13	0.11	<10	0.5	<10	970	3	<10	<10	0.01
1250W-4850N	260	57	<1	53	10	2.18	0.47	0.42	0.01	0.14	0.12	<10	<0.5	<10	1310	3	<10	<10	0.01
1250W-4900N	220	55	<1	47	10	2.49	0.45	0.42	0.02	0.18	0.12	<10	0.5	<10	1520	3	<10	<10	0.01
1250W-4950N	190	68	<1	49	10	1.97	0.46	0.42	0.01	0.17	0.10	<10	<0.5	<10	1130	3	<10	<10	<0.01
1250W-5000N	240	51	<1	65	10	1.87	0.33	0.58	0.02	0.17	0.10	<10	<0.5	<10	940	3	<10	<10	<0.01
1250W-5050N	340	52	<1	65	20	1.86	0.35	0.49	0.01	0.11	0.10	<10	0.5	<10	1640	3	<10	<10	0.01
1250W-5100N	280	45	<1	51	10	2.83	0.43	0.46	0.03	0.18	0.11	<10	0.5	<10	4270	3	<10	<10	0.01
1250W-5150N	110	9	<1	45	10	1.61	0.10	0.59	0.11	0.04	0.04	30	<0.5	<10	310	1	<10	<10	0.03
1250W-5200N	180	50	<1	35	20	2.81	0.40	0.32	0.03	0.14	0.12	<10	0.5	<10	1220	4	<10	<10	<0.01
1250W-5250N	200	43	<1	58	40	2.90	0.30	0.42	0.04	0.15	0.11	<10	0.5	<10	1040	4	<10	<10	0.01
1300W-4750N	120	49	<1	39	30	3.29	0.46	0.49	0.03	0.11	0.15	<10	0.5	<10	710	4	<10	<10	0.01
1300W-4800N	240	72	<1	47	10	3.71	0.67	0.34	0.02	0.15	0.16	<10	0.5	10	1040	3	<10	<10	0.01
1300W-4850N	100	65	<1	34	10	3.24	0.52	0.25	0.01	0.11	0.13	<10	0.5	10	1770	3	<10	<10	0.02
1300W-4900N	200	62	<1	43	10	3.06	0.56	0.37	0.01	0.16	0.15	<10	0.5	10	1030	3	<10	<10	0.01

Project 592

Standard/Scotchman

file: 592\geodata\Rock_99.wk4

Soil Sample Analyses
1999

Reference : a9933736

Sample ID	Lab report #	30g FA/AA Au ppb	ICP Ag ppm	ICP As ppm	ICP Sb ppm	ICP Cu ppm	ICP Pb ppm	ICP Zn ppm	ICP W ppm	ICP Cd ppm	ICP Mo ppm	ICP Bi ppm	ICP Ni ppm	ICP Co ppm	ICP Cr ppm	ICP Fe %	ICP Mn ppm
1300W-4950N	a9933736	<5	<0.2	6	<2	21	6	96	<10	<0.5	1	<2	12	9	19	2.26	850
1300W-5000N	a9933736	<5	<0.2	4	<2	13	8	78	<10	<0.5	<1	<2	12	9	23	2.42	470
1300W-5050N	a9933736	<5	0.2	4	<2	33	8	72	<10	<0.5	1	<2	17	9	20	2.34	555
1300W-5100N	a9933736	<5	<0.2	6	<2	17	12	136	<10	<0.5	1	<2	13	12	22	3.31	1215
1300W-5150N	a9933736	<5	<0.2	2	<2	18	18	132	<10	<0.5	1	<2	15	12	25	3.70	1020
1300W-5200N	a9933736	<5	<0.2	6	<2	20	16	108	<10	<0.5	2	<2	15	13	24	3.68	795
1300W-5250N	a9933736	<5	<0.2	10	<2	18	12	118	<10	<0.5	1	<2	12	10	27	2.91	1310

Standard/Scotchman

Soil Sample Analyses (part 2)

Sample ID	ICP Ba ppm	ICP V ppm	ICP Hg ppm	ICP Sr ppm	ICP La ppm	ICP Al %	ICP Mg %	ICP Ca %	ICP Na %	ICP K %	ICP Ti %	ICP U ppm	ICP Be ppm	ICP Ga ppm	ICP P ppm	ICP Sc ppm	ICP Tl ppm	ICP B ppm	ICP S %
1300W-4950N	310	42	<1	52	10	2.71	0.32	0.56	0.03	0.13	0.11	<10	0.5	<10	2030	3	<10	<10	0.01
1300W-5000N	210	50	<1	44	10	2.15	0.39	0.38	0.02	0.17	0.11	<10	<0.5	<10	1540	3	<10	<10	<0.01
1300W-5050N	140	44	<1	47	50	2.96	0.34	0.45	0.04	0.10	0.12	10	0.5	<10	720	4	<10	<10	0.01
1300W-5100N	430	59	<1	48	10	2.86	0.64	0.44	0.02	0.27	0.13	<10	0.5	10	2840	3	<10	<10	0.01
1300W-5150N	270	70	<1	51	10	3.64	0.72	0.40	0.01	0.25	0.14	<10	0.5	10	1370	4	<10	<10	0.01
1300W-5200N	170	72	<1	46	30	3.50	0.76	0.40	0.02	0.27	0.16	<10	0.5	10	880	4	<10	<10	0.01
1300W-5250N	330	59	<1	61	10	2.34	0.52	0.51	0.01	0.14	0.10	<10	0.5	<10	2110	3	<10	<10	0.01

APPENDIX 2

Rock Sample Results

ANALYTICAL PROCEDURES

Geochemical Analysis

by Chemex Labs Ltd.

ELEMENT		LOWER DETECTION LIMIT	EXTRACTION	METHOD
Au	Gold	5 ppb	fire assay	A.A.
Al*	Aluminum	0.01%	Aqua-Regia digestion	Ind. Coupled Plasma
Sb	Antimony	2 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
As	Arsenic	2 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Ba*	Barium	10 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Be*	Beryllium	0.5 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Bi	Bismuth	2 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Cd	Cadmium	0.5 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Ca*	Calcium	0.01%	Aqua-Regia digestion	Ind. Coupled Plasma
Cr*	Chromium	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Co	Cobalt	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Cu	Copper	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Ga*	Gallium	10 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Fe	Iron	0.01%	Aqua-Regia digestion	Ind. Coupled Plasma
La*	Lanthanum	10 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Pb	Lead	2 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Mg*	Magnesium	0.01%	Aqua-Regia digestion	Ind. Coupled Plasma
Mn	Maganese	5 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Hg	Mercury	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Mo	Molybdenum	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Ni	Nickel	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
P	Phosphorus	10 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
K*	Potassium	0.01%	Aqua-Regia digestion	Ind. Coupled Plasma
Sc*	Scandium	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Ag	Silver	0.2 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Na*	Sodium	0.01%	Aqua-Regia digestion	Ind. Coupled Plasma
Sr*	Strontium	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Tl*	Thallium	10 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Ti*	Titanium	0.01%	Aqua-Regia digestion	Ind. Coupled Plasma
W*	Tungsten	10 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
U	Uranium	10 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
V	Vanadium	1 ppm	Aqua-Regia digestion	Ind. Coupled Plasma
Zn	Zinc	2 ppm	Aqua-Regia digestion	Ind. Coupled Plasma

* Incomplete digeston.

Project 592

Standard/Scotchman

file: 592\geodata\Rock_99.wk4

Rock Sample Analyses
1999

Reference : a9933730

Sample ID	Lab report #	30g FA/AA Au ppb	ICP Ag ppm	ICP As ppm	ICP Sb ppm	ICP Cu ppm	ICP Pb ppm	ICP Zn ppm	ICP W ppm	ICP Cd ppm	ICP Mo ppm	ICP Bi ppm	ICP Ni ppm	ICP Co ppm	ICP Cr ppm	ICP Fe %	ICP Mn ppm
197801	a9933730	15	<0.2	8	<2	3	16	6	<10	<0.5	<1	<2	1	1	133	0.25	40
197802	a9933730	15	0.2	2	<2	3	14	6	<10	<0.5	<1	<2	1	2	142	0.34	90
197803	a9933730	30	<0.2	4	<2	3	4	2	<10	<0.5	3	<2	3	<1	277	0.32	40
197804	a9933730	15	<0.2	<2	<2	2	<2	6	<10	<0.5	3	<2	3	<1	269	0.38	80
197805	a9933730	60	0.2	4	<2	5	2	6	<10	<0.5	8	<2	4	1	285	0.56	50
197806	a9933730	<5	<0.2	<2	<2	2	<2	2	<10	<0.5	<1	<2	3	<1	242	0.33	50

Standard/Scotchman

Rock Sample Analyses (part 2)

Sample ID	ICP Ba ppm	ICP V ppm	ICP Hg ppm	ICP Sr ppm	ICP La ppm	ICP Al %	ICP Mg %	ICP Ca %	ICP Na %	ICP K %	ICP Ti %	ICP U ppm	ICP Be ppm	ICP Ga ppm	ICP P ppm	ICP Sc ppm	ICP Tl ppm	ICP B ppm	ICP S %
197801	60	6	<1	6	<10	0.38	0.03	0.06	0.06	0.20	<0.01	<10	<0.5	<10	180	<1	<10	<10	<0.01
197802	60	4	<1	14	10	0.43	0.04	0.18	0.07	0.21	<0.01	<10	<0.5	<10	220	<1	<10	<10	<0.01
197803	10	3	<1	4	<10	0.10	0.01	0.06	<0.01	0.05	<0.01	<10	<0.5	<10	20	<1	<10	<10	0.01
197804	10	2	<1	4	<10	0.11	0.05	0.22	<0.01	0.03	<0.01	<10	<0.5	<10	20	<1	<10	<10	<0.01
197805	40	4	<1	6	<10	0.24	0.06	0.04	0.02	0.11	<0.01	<10	<0.5	<10	100	<1	<10	<10	0.04
197806	10	1	<1	3	<10	0.08	0.02	0.03	<0.01	0.03	<0.01	<10	<0.5	<10	40	<1	<10	<10	<0.01

APPENDIX 3

Magnetometer Results

Project 592

Standard/Scotchman

file: 592\geophysc\mag_99.wk4

Magnetometer Survey

Line	Station	Time (hr min sec)	Magnetic Field (nT) Uncorrected	Corrected
1300 W	5250.0 N	90915.7	56791.7	56055.2
	5237.5	91030.7	56720.4	55984.0
	5225.0	91234.6	56666.8	55930.7
	5212.5	91326.4	56633.4	55897.5
	5200.0	91401.4	56569.6	55834.0
	5187.5	91741.9	56675.0	55939.5
	5175.0	91828.9	56564.4	55829.1
	5162.5	91855.3	56712.7	55977.6
	5150.0	91936.8	56793.1	56058.1
	5137.5	92016.7	56586.5	55851.5
	5125.0	92111.7	56566.7	55831.7
	5112.5	92410.9	56560.5	55826.0
	5100.0	92548.9	56632.7	55898.6
	5087.5	92727.0	56596.0	55862.1
	5075.0	92813.1	56581.9	55848.0
	5062.5	92906.1	56607.1	55873.6
	5050.0	92945.9	56659.6	55926.2
	5037.5	93030.2	56695.1	55961.6
	5025.0	93102.4	56733.8	56000.1
	5012.5	93134.9	56760.8	56027.4
	5000.0	93245.5	56711.1	55977.7
	4987.5	93357.7	56682.9	55949.4
	4975.0	93454.0	56658.4	55925.3
	4962.5	93528.9	56639.3	55906.2
	4950.0	93606.3	56601.6	55868.6
	4937.5	93714.9	56589.9	55857.3
	4925.0	93805.2	56627.7	55895.5
	4912.5	93901.1	56644.1	55911.6
	4900.0	93939.3	56653.5	55921.0
	4887.5	94022.0	56625.2	55892.8
	4875.0	94101.3	56431.3	55698.9
	4862.5	94223.8	56576.6	55844.3
	4850.0	94251.7	56519.8	55787.5
	4837.5	94322.0	56518.9	55786.5
	4825.0	94354.8	56414.6	55682.3
	4812.5	94428.0	56887.0	56154.6
	4800.0	94504.7	57330.4	56598.1

Project 592

Standard/Scotchman

file: 592\geophysc\mag_99.wk4

Magnetometer Survey

Line	Station	Time (hr min sec)	Magnetic Field (nT) Uncorrected	Corrected
	4787.5	94548.2	56860.1	56128.1
	4775.0	94636.8	56517.8	55785.9
	4762.5	94719.1	56234.2	55502.4
	4750.0	94754.1	55944.9	55213.3
1250 W	4750.0 N	95128.3	56668.9	55937.8
	4762.5	95407.2	57094.7	56364.0
	4775.0	95532.6	56151.0	55421.1
	4787.5	95639.1	56263.6	55534.0
	4800.0	95731.3	56367.3	55637.8
	4812.5	95831.7	56420.8	55691.3
	4825.0	95912.9	56439.1	55709.4
	4837.5	100047.5	56658.8	55929.3
	4850.0	100113.5	56656.8	55927.4
	4862.5	100141.6	56653.0	55923.6
	4875.0	100217.8	56327.9	55598.5
	4887.5	100306.1	56430.3	55701.0
	4900.0	100345.7	56499.6	55770.5
	4912.5	100448.1	56545.1	55816.1
	4925.0	100526.1	56561.5	55832.4
	4937.5	100557.0	56697.7	55968.6
	4950.0	100628.3	56730.3	56001.2
	4962.5	100659.0	56688.8	55959.7
	4975.0	100723.3	56667.3	55938.0
	4987.5	100811.0	56567.0	55837.6
	5000.0	100905.3	56604.6	55875.5
	5012.5	100957.7	56694.9	55965.8
	5025.0	101030.1	56657.7	55928.8
	5037.5	101101.3	56660.7	55932.0
	5050.0	101146.3	56593.1	55864.6
	5062.5	101256.8	56597.8	55869.0
	5075.0	101356.3	56647.2	55918.5
	5087.5	101503.3	56717.3	55988.7
	5100.0	101553.8	56738.7	56010.4
	5112.5	101629.4	56715.7	55987.5
	5125.0	101748.0	56681.7	55953.3
	5137.5	101834.9	56627.5	55899.0

Project 592

Standard/Scotchman

file: 592\geophysc\mag_99.wk4

Magnetometer Survey

Line	Station	Time (hr min sec)	Magnetic Field (nT) Uncorrected	Corrected
	5150.0	101906.4	56631.5	55903.1
	5162.5	102014.4	56718.7	55991.0
	5175.0	102055.8	56705.6	55977.9
	5187.5	102137.8	56695.3	55967.6
	5200.0	102210.7	56749.9	56022.2
	5212.5	102241.8	56764.6	56037.1
	5225.0	102305.2	56741.6	56014.2
	5237.5	102349.8	56930.7	56203.2
	5250.0	102423.9	57074.6	56346.8
1200 W	5250.0 N	102615.4	56713.3	55985.2
	5237.5	102653.4	56793.4	56065.1
	5225.0	102719.6	56972.6	56244.4
	5212.5	102751.9	56960.3	56232.3
	5200.0	102857.7	56758.3	56030.2
	5187.5	102935.7	56735.5	56007.5
	5175.0	103020.7	56656.8	55928.9
	5162.5	103110.1	56703.0	55975.2
	5150.0	103209.2	56706.8	55978.8
	5137.5	103310.3	56795.8	56068.0
	5125.0	103358.3	56721.5	55994.0
	5112.5	103513.9	56707.4	55980.5
	5100.0	103546.5	56710.7	55984.1
	5087.5	103630.5	56738.2	56011.8
	5075.0	103744.3	56679.2	55952.8
	5062.5	103842.0	56673.4	55947.0
	5050.0	103931.0	56657.1	55930.5
	5037.5	104036.4	56640.5	55913.7
	5025.0	104136.7	56662.8	55936.0
	5012.5	104219.6	56589.2	55862.4
	5000.0	104304.5	56607.2	55880.4
	4987.5	104418.3	56633.6	55906.8
	4975.0	104518.3	56654.0	55927.3
	4962.5	104646.8	56620.4	55893.3
	4950.0	104733.5	56594.5	55867.2
	4937.5	104843.1	56600.9	55873.5
	4925.0	104953.4	56591.0	55863.5

Project 592

Standard/Scotchman

file: 592\geophysc\mag_99.wk4

Magnetometer Survey

Line	Station	Time (hr min sec)	Magnetic Field (nT) Uncorrected	Corrected
	4912.5	105105.8	56549.6	55821.8
	4900.0	105200.7	56630.3	55902.5
	4887.5	105306.6	56592.0	55864.3
	4875.0	105345.4	56615.8	55888.0
	4862.5	105520.7	56652.2	55924.3
	4850.0	105616.7	56598.2	55870.4
	4837.5	105711.1	56590.1	55862.4
	4825.0	105816.4	56557.1	55829.7
	4812.5	110024.4	56549.1	55820.9
	4800.0	110113.7	56857.1	56128.9
	4787.5	110200.3	56713.8	55986.0
	4775.0	110226.0	56579.6	55851.7
	4762.5	110319.0	56548.3	55820.3
	4750.0	110355.0	56731.0	56002.9
1150 W	4750.0 N	110732.0	56442.1	55714.2
	4762.5	110828.1	56773.6	56045.8
	4775.0	110918.7	56829.9	56101.7
	4787.5	110959.5	56891.3	56162.7
	4800.0	111032.9	56604.5	55875.6
	4812.5	111114.8	56607.8	55878.6
	4825.0	111154.2	56664.4	55935.2
	4837.5	111337.9	56463.0	55734.2
	4850.0	111423.3	56557.1	55828.2
	4862.5	111520.3	56591.7	55862.8
	4875.0	111609.4	56560.1	55830.8
	4887.5	111704.7	56627.3	55898.0
	4900.0	111738.1	56575.0	55845.3
	4912.5	111902.5	56684.5	55954.8
	4925.0	112014.6	56696.7	55966.6
	4937.5	112126.1	56645.0	55915.4
	4950.0	112209.8	56642.1	55912.6
	4962.5	112331.8	56663.5	55933.8
	4975.0	112413.9	56629.4	55899.7
	4987.5	112450.0	56613.3	55883.4
	5000.0	112518.1	56689.6	55959.6
	5012.5	112623.7	56601.9	55871.8

Project 592

Standard/Scotchman

file: 592\geophysc\mag_99.wk4

Magnetometer Survey

Line	Station	Time (hr min sec)	Magnetic Field (nT) Uncorrected	Corrected
	5025.0	113036.5	56655.5	55924.7
	5037.5	113119.5	56667.7	55936.9
	5050.0	113158.9	56720.8	55990.0
	5062.5	113254.1	56704.6	55973.4
	5075.0	113351.6	56731.0	55999.9
	5087.5	113430.6	56695.8	55964.7
	5100.0	113528.3	56786.8	56055.4
	5112.5	113558.1	56804.9	56073.2
	5125.0	113632.8	56851.7	56119.9
	5137.5	113715.9	56659.9	55928.1
	5150.0	113746.7	56772.7	56041.2
	5162.5	113858.0	56913.3	56181.3
	5175.0	113934.1	56962.8	56231.0
	5187.5	114051.5	56604.5	55872.2
	5200.0	114121.5	56666.1	55933.7
	5212.5	114208.2	56669.8	55937.5
	5225.0	114239.4	56683.5	55950.9
	5237.5	114323.1	56509.4	55776.7
	5250.0	114406.5	56622.8	55889.9
1100 W	5275.0 N	115305.0	56625.9	55892.0
	5262.5	115358.2	56620.9	55886.4
	5250.0	115434.5	56602.4	55868.1
	5237.5	115514.5	56608.5	55874.4
	5225.0	115609.3	56612.4	55878.2
	5212.5	115710.5	56595.7	55861.6
	5200.0	120323.4	56595.2	55861.4
	5187.5	120424.0	56552.5	55818.7
	5175.0	120505.7	56622.1	55888.4
	5162.5	120602.6	56561.3	55827.3
	5150.0	120648.7	56689.4	55955.4
	5137.5	120757.5	56651.3	55917.4
	5125.0	120840.2	56590.3	55856.8
	5112.5	120936.3	56826.3	56092.9
	5100.0	121031.8	57036.2	56303.0
	5087.5	121129.5	56892.6	56159.5
	5075.0	121217.9	56732.5	55999.2

Project 592 # Standard/Scotchman

file: 592\geophysc\mag_99.wk4 ## Magnetometer Survey

Line	Station	Time (hr min sec)	Magnetic Field (nT) Uncorrected	Corrected
	5062.5	121301.1	56659.7	55926.9
	5050.0	121351.8	56784.3	56051.4
	5037.5	121422.9	56994.0	56261.0
	5025.0	121456.5	56958.0	56224.8
	5012.5	121545.2	56892.6	56159.2
	5000.0	122524.0	56761.8	56028.9
	4987.5	122643.1	56680.7	55948.0
	4975.0	122717.8	56704.7	55972.3
	4962.5	122745.2	56737.6	56005.2
	4950.0	122830.6	56701.5	55969.3
	4937.5	122920.3	56731.7	55999.6
	4925.0	123031.4	56700.4	55968.0
	4912.5	123111.6	56665.5	55933.3
	4900.0	123206.8	56640.4	55908.2
	4887.5	123259.2	56645.4	55912.5
	4875.0	123351.9	56607.1	55873.9
	4862.5	123516.4	56598.1	55864.6
	4850.0	123617.4	56658.9	55925.2
	4837.5	123706.2	56680.8	55946.9
	4825.0	123738.4	56662.0	55928.1
	4812.5	123814.2	56708.2	55974.2
	4800.0	123845.0	56698.0	55964.0
	4787.5	123919.6	56599.2	55865.0
	4775.0	123953.2	56695.2	55960.7
	4762.5	124028.0	56635.0	55900.4
	4750.0	124107.1	56547.3	55812.8
1050 W	4750.0 N	124305.0	56667.4	55933.0
	4762.5	124345.6	56634.4	55900.1
	4775.0	124414.3	56592.1	55857.8
	4787.5	124450.6	56637.6	55903.3
	4800.0	124519.4	56617.7	55883.3
	4812.5	124810.5	56647.1	55912.5
	4825.0	124850.9	56681.6	55946.6
	4837.5	124934.0	56665.0	55929.8
	4850.0	125006.2	56655.4	55920.0
	4862.5	125040.5	56710.7	55975.2

Project 592

Standard/Scotchman

file: 592\geophysc\mag_99.wk4

Magnetometer Survey

Line	Station	Time (hr min sec)	Magnetic Field (nT) Uncorrected	Corrected
	4875.0	125115.3	56681.1	55945.4
	4887.5	125207.9	56655.1	55918.9
	4900.0	125257.3	56660.2	55924.2
	4912.5	125335.9	56707.5	55971.3
	4925.0	125414.7	56726.6	55990.2
	4937.5	125447.6	56740.1	56003.5
	4950.0	125541.1	56780.9	56044.0
	4962.5	125720.5	56832.0	56094.7
	4975.0	125806.5	56905.8	56168.3
	4987.5	130549.9	56910.6	56174.1
	5000.0	130644.6	56847.0	56110.8
	5012.5	130721.6	56824.2	56088.1
	5025.0	130747.1	56935.1	56199.0
	5037.5	130843.4	56989.0	56253.1
	5050.0	131058.9	56810.0	56075.0
	5062.5	131143.1	56692.3	55957.7
	5075.0	131218.3	56634.5	55899.9
	5087.5	131254.1	56575.2	55840.4
	5100.0	131335.9	56596.4	55861.7
	5112.5	131429.8	56664.8	55930.2
	5125.0	131459.5	56727.5	55992.9
	5137.5	131536.0	56838.6	56104.2
	5150.0	131607.6	56791.3	56057.0
	5162.5	131651.1	56656.6	55922.3
	5175.0	131729.0	56614.0	55879.8
	5187.5	131815.8	56721.3	55987.0
	5200.0	131853.1	56722.5	55987.9
	5212.5	132010.0	56488.8	55754.1
	5225.0	132144.7	56532.6	55797.6
	5237.5	132247.2	56573.1	55837.8
	5250.0	132318.2	56593.3	55857.9
1000 W	5250.0 N	132932.7	56657.3	55921.0
	5237.5	133054.9	56716.9	55980.3
	5225.0	133142.3	56573.9	55837.2
	5212.5	133306.4	56577.6	55841.1
	5200.0	133415.0	56493.8	55757.6

Project 592

Standard/Scotchman

file: 592\geophysc\mag_99.wk4

Magnetometer Survey

Line	Station	Time (hr min sec)	Magnetic Field (nT) Uncorrected	Corrected
	5187.5	133539.7	56864.0	56127.7
	5175.0	133633.5	56715.2	55978.8
	5162.5	133715.4	56754.8	56018.6
	5150.0	133752.1	56673.5	55936.8
	5137.5	133842.8	56736.6	56000.1
	5125.0	134004.7	56658.3	55922.3
	5112.5	134143.8	56753.4	56017.0
	5100.0	134252.5	56703.7	55966.8
	5087.5	134339.7	56666.0	55928.8
	5075.0	134419.6	56688.6	55951.5
	5062.5	134500.6	56577.1	55840.3
	5050.0	134528.5	56603.8	55866.9
	5037.5	134602.7	56758.6	56021.6
	5025.0	134629.2	56591.0	55854.2
	5012.5	134713.0	56672.8	55936.2
	5000.0	134753.5	56724.4	55987.6
	4987.5	134836.1	56894.6	56157.6
	4975.0	134908.7	56817.7	56080.5
	4962.5	134959.8	56984.5	56247.4
	4950.0	135051.9	56916.1	56178.7
	4937.5	135219.9	56926.7	56189.5
	4925.0	135321.2	56802.1	56064.6
	4912.5	135449.8	56682.5	55945.0
	4900.0	135632.6	56601.2	55863.5
	4887.5	135738.0	56747.4	56010.0
	4875.0	135838.3	56834.9	56097.5
	4862.5	135919.4	56830.0	56092.6
	4850.0	140000.3	56739.8	56002.6
	4837.5	140031.7	56743.7	56006.4
	4825.0	140121.2	56629.1	55891.8
	4812.5	140232.2	56624.5	55887.2
	4800.0	140311.8	56626.4	55888.8
	4787.5	140401.6	56659.1	55921.4
	4775.0	140503.7	56693.2	55955.4
	4762.5	140536.1	56640.5	55902.8
	4750.0	140608.9	56615.8	55878.1

APPENDIX 4

VLF-EM Values and Fraser Filter Data

Project 592

Standard/Scotchman

file: 592\geophysc\vlf_99.wk4

VLF Survey

Line	Station	Frequency (Cutter-Maine - 24.0 kHz) In Phase	Fraser Filter	Out Phase	Field Strength	Frequency (Hawaii - 21.4 kHz) In Phase	Fraser Filter	Out Phase	Field Strength	Frequency (Seattle - 24.8 kHz) In Phase	Fraser Filter	Out Phase	Field Strength
1300 W	5250.0 N	-13.6		38.2	4.7	6.9		1.3	8.2	5.2		1.2	105.5
	5237.5	-13.2	-9	32.6	5.0	10.0	-2	2.5	8.5	9.1	-3	0.6	110.4
	5225.0	-16.0	-9	29.1	5.1	7.4	-3	0.5	8.3	5.3	-5	-0.4	109.0
	5212.5	-20.0	-1	30.4	5.0	7.9	-3	-0.4	8.2	6.0	-2	-1.7	106.9
	5200.0	-17.7	1	29.9	5.2	6.5	-3	-0.8	8.1	3.3	0	-1.7	108.5
	5187.5	-19.5	4	29.2	4.9	5.9	-1	-0.4	8.3	6.4	-2	-1.8	104.8
	5175.0	-17.6	2	27.6	5.0	5.3	-2	0.9	8.4	3.2	-1	-1.2	111.0
	5162.5	-16.1	-4	25.7	4.9	6.2	-7	0.4	8.4	4.9	-4	-2.0	106.0
	5150.0	-18.6	0	26.9	4.9	3.2	-4	-1.3	8.6	3.8	-5	-3.5	109.5
	5137.5	-18.7	4	26.9	4.9	1.2	2	-3.5	8.4	0.5	-2	-3.6	108.6
	5125.0	-15.7	-5	23.8	4.7	3.9	-3	-2.4	8.6	3.2	-8	-3.9	113.0
	5112.5	-17.6	-12	24.4	4.8	2.3	-11	-2.8	8.6	-0.5	-13	-4.2	113.1
	5100.0	-22.2	-6	25.2	4.8	-0.6	-11	-5.8	8.3	-3.8	-12	-4.4	108.1
	5087.5	-22.6	-10	23.7	5.1	-3.8	-8	-5.8	8.4	-6.7	-8	-3.8	109.7
	5075.0	-22.7	-16	22.9	5.0	-5.6	-6	-4.1	8.8	-9.1	-8	-6.0	110.2
	5062.5	-31.8	-1	29.4	4.9	-7.1	-2	-7.4	8.2	-9.6	-6	-6.8	105.6
	5050.0	-29.8	8	27.7	4.8	-7.8	2	-7.9	8.0	-14.4	8	-6.5	97.5
	5037.5	-25.7	-1	32.0	4.6	-7.1	10	-4.9	7.7	-9.8	15	-5.0	99.8
	5025.0	-27.7	8	31.8	4.6	-5.4	14	-3.3	7.7	-6.6	14	-3.0	92.6
	5012.5	-28.5	11	31.5	4.6	0.2	9	-1.0	7.4	-2.2	9	-1.3	93.6
	5000.0	-17.0	4	27.9	4.2	1.1	5	0.0	7.8	-0.4	7	0.0	97.0
	4987.5	-28.1	10	26.5	4.6	2.5	1	-0.2	7.6	0.5	3	-1.4	98.1
	4975.0	-13.8	5	26.9	4.3	3.5	-4	1.8	7.6	3.5	-5	-0.7	97.3
	4962.5	-21.7	-5	28.9	4.7	1.5	-3	-2.4	7.9	-0.5	-2	-1.9	100.4
	4950.0	-15.0	-15	25.9	4.3	0.6	0	-3.9	7.7	-0.6	4	-4.3	99.0
	4937.5	-25.4	-11	28.4	4.7	1.8	0	-1.1	7.6	2.0	3	-3.2	94.7
	4925.0	-26.4	1	28.9	4.6	0.5	1	-1.3	7.7	0.9	3	-2.4	94.7
	4912.5	-24.6	2	28.1	4.4	2.1	4	-1.1	7.8	3.7	5	-2.4	99.2
	4900.0	-26.0	7	28.3	4.5	1.4	11	-2.8	7.7	2.3	13	-3.0	99.3
	4887.5	-22.8	15	28.5	4.4	5.5	12	-2.4	7.6	7.5	14	-4.3	92.7
	4875.0	-20.9	11	33.0	4.5	8.6	9	0.1	7.7	11.3	6	-4.1	96.6
	4862.5	-13.1	0	31.4	4.4	10.1	5	1.5	7.8	12.0	0	-2.7	96.1
	4850.0	-20.1	0	29.3	4.5	13.4	-1	1.4	7.6	13.1	-2	-3.3	95.8
	4837.5	-14.2	-3	29.1	4.6	10.1	3	-3.2	8.0	10.4	3	-4.9	101.7
	4825.0	-19.0	-3	28.0	4.6	12.0	5	-3.1	7.8	12.4	9	-4.9	102.0
	4812.5	-17.9	8	30.2	4.6	14.3	6	0.0	8.1	14.3	11	-5.8	105.3
	4800.0	-17.8	18	25.5	4.7	12.9	14	-0.6	8.4	17.0	11	-5.3	106.9
	4787.5	-11.6	17	26.4	4.8	19.6	0	4.4	8.7	20.9	-6	-2.9	113.8
	4775.0	-5.9	-7	26.1	5.0	21.6	-32	4.7	9.5	21.7	-37	-1.7	125.0
	4762.5	-6.8		24.2	5.5	10.8		-3.1	10.4	9.8		-6.4	133.4
	4750.0	-17.3		17.2	5.4	-2.0		-8.9	10.2	-4.0		-10.2	124.7
1250 W	4750.0 N	18.6		-26.3	4.9	2.2		-2.7	9.1	-1.6		-5.1	115.8
	4762.5	22.4		-28.3	5.1	2.4		-3.3	8.9	-0.3		-6.4	110.1
	4775.0	22.2	-2	-27.8	4.8	-0.3	4	-6.1	9.0	-5.9	8	-7.7	111.5
	4787.5	20.3	7	-29.9	4.8	0.8	2	-6.9	9.0	-3.7	1	-9.0	115.6
	4800.0	16.9	3	-29.0	4.7	-0.2	-8	-8.0	9.0	-3.2	-12	-9.6	119.9
	4812.5	23.0	-20	-28.7	4.9	8.7	-23	-5.1	9.9	5.2	-28	-7.2	125.9
	4825.0	33.7	-19	-27.2	4.7	14.6	-23	2.6	8.4	16.3	-31	-3.0	106.3
	4837.5	25.4	1	-27.0	4.5	16.6	-9	2.8	8.2	17.0	-11	-2.4	103.2
	4850.0	30.7	3	-26.9	4.7	15.8	-2	2.1	8.1	15.7	1	-2.5	100.1
	4862.5	25.9	3	-24.9	4.5	17.1	-2	3.9	7.8	16.4	-1	0.4	101.1
	4875.0	27.6	4	-27.4	4.3	17.2	1	4.5	7.7	17.7	1	0.9	95.0

Project 592

Standard/Scotchman

file: 592\geophysc\vlf_99.wk4

VLF Survey

Line	Station	Frequency (Cutter-Maine - 24.0 kHz) In Phase	Fraser Filter	Out Phase	Field Strength	Frequency (Hawaii - 21.4 kHz) In Phase	Fraser Filter	Out Phase	Field Strength	Frequency (Seattle - 24.8 kHz) In Phase	Fraser Filter	Out Phase	Field Strength
	4887.5	24.5	5	-26.4	4.2	14.4	6	1.3	7.6	13.2	10	-0.8	90.6
	4900.0	24.4	8	-28.4	4.3	14.1	8	1.8	7.3	10.7	13	-1.2	87.8
	4912.5	20.0	9	-23.5	4.1	10.0	9	0.1	7.4	7.2	11	-2.0	92.5
	4925.0	20.3	-1	-28.6	4.3	10.0	4	-1.2	7.6	5.5	6	-3.2	89.5
	4937.5	24.6	-9	-28.4	4.4	10.5	0	0.9	7.4	6.3	2	-0.9	91.4
	4950.0	24.2	-6	-27.8	4.3	9.8	4	0.5	7.6	4.8	4	-0.4	91.6
	4962.5	26.8	-1	-22.8	4.4	6.7	9	-0.6	7.3	2.8	8	-0.7	89.0
	4975.0	22.7	-2	-27.6	4.4	5.0	5	-0.6	7.3	0.0	4	-0.5	94.7
	4987.5	30.5	-14	-28.2	4.5	6.2	-7	1.5	7.6	3.5	-10	-1.2	93.9
	5000.0	32.5	-12	-21.8	4.3	12.2	-8	3.8	7.2	9.0	-8	3.4	90.1
	5012.5	32.8	0	-31.0	4.4	6.9	6	0.8	7.0	2.9	10	0.9	87.9
	5025.0	30.6	6	-31.9	4.4	5.5	13	-0.6	7.0	-0.2	16	-0.7	86.4
	5037.5	28.9	11	-28.3	4.3	1.1	11	-1.7	6.9	-3.4	13	-2.4	86.3
	5050.0	24.0	10	-34.7	4.4	-0.1	16	-3.5	7.2	-6.7	16	-2.4	87.9
	5062.5	25.2	14	-32.5	4.4	-8.8	19	-7.0	7.2	-12.8	18	-5.2	87.1
	5075.0	14.0	24	-28.5	4.2	-9.3	7	-7.9	7.4	-15.4	9	-6.3	90.2
	5087.5	11.5	14	-28.8	4.3	-6.5	-6	-5.0	7.7	-13.4	-3	-4.7	91.9
	5100.0	13.3	-2	-24.9	4.4	-5.3	-5	-7.1	7.7	-12.0	-8	-4.2	96.6
	5112.5	13.8	-5	-27.9	4.5	-5.4	-6	-4.9	7.8	-8.8	-10	-4.1	99.3
	5125.0	16.0	-16	-23.6	4.3	-0.9	-13	-1.7	7.7	-6.5	-15	-2.4	99.5
	5137.5	26.8	-23	-25.1	4.8	3.6	-14	-0.4	7.8	0.2	-16	-1.3	96.5
	5150.0	26.1	-15	-26.8	4.7	4.3	-12	-0.1	7.9	0.0	-11	-0.6	95.4
	5162.5	31.8	-5	-23.0	4.6	10.5	-11	-0.2	7.6	5.1	-10	-1.8	92.2
	5175.0	26.2	7	-26.3	4.6	8.7	-2	-2.7	7.7	4.7	-3	-2.7	93.0
	5187.5	24.9	5	-26.3	4.5	8.3	2	-2.4	7.8	3.5	2	-3.1	90.8
	5200.0	27.9	-6	-26.5	4.6	8.7	-3	-1.5	7.5	4.7	-5	-2.8	95.3
	5212.5	29.4	-8	-25.8	4.7	11.2	-8	0.5	7.7	8.8	-12	-1.4	93.2
	5225.0	31.1	-5	-24.0	4.6	14.2	-9	2.3	7.4	11.3	-6	-0.1	92.1
	5237.5	31.2	-8	-23.4	4.5	14.4	-6	1.2	7.6	8.3	-2	0.8	89.3
	5250.0	36.8		-28.9	4.6	16.9		4.4	7.1	13.9		1.6	86.2
1200 W	5250.0 N	0.6		30.8	4.4	12.1		2.0	7.5	12.3		0.2	94.5
	5237.5	-8.8	-11	29.7	4.5	12.3	-3	1.2	7.6	13.0	-3	-1.4	91.7
	5225.0	-8.8	1	28.7	4.4	10.4	-6	2.7	7.6	10.6	-5	-2.0	90.0
	5212.5	-10.3	1	33.8	4.5	10.7	-7	1.4	7.3	11.5	-7	-2.7	90.8
	5200.0	-6.0	-9	25.9	4.4	6.0	-1	-1.4	7.5	7.3	-3	-3.9	95.6
	5187.5	-11.7	-13	25.9	4.4	8.0	-4	1.4	7.6	7.8	-4	-1.6	98.8
	5175.0	-13.7	-8	26.2	4.4	7.5	-12	1.1	7.6	8.5	-14	-1.8	96.8
	5162.5	-17.0	-6	28.1	4.7	2.6	-14	-0.7	7.8	2.2	-18	-2.9	97.7
	5150.0	-16.8	-4	24.4	4.5	1.1	-13	-4.6	7.2	-0.3	-16	-4.8	93.2
	5137.5	-20.0	-3	25.2	4.3	-4.8	-4	-5.0	7.2	-6.8	-4	-6.1	89.4
	5125.0	-18.1	-6	23.7	4.3	-4.4	5	-6.2	7.0	-7.4	7	-5.6	86.0
	5112.5	-21.3	-8	32.5	4.4	-2.9	2	-4.8	6.6	-3.3	0	-5.2	84.6
	5100.0	-22.7	-9	28.6	4.2	-1.7	-1	-4.6	6.6	-3.6	-4	-5.3	83.2
	5087.5	-24.8	-3	29.2	4.3	-3.8	3	-6.5	6.4	-6.9	6	-4.8	80.6
	5075.0	-27.7	3	29.5	4.4	-1.9	6	-4.7	6.1	-3.6	10	-3.8	79.0
	5062.5	-23.1	6	34.0	4.2	-0.8	8	-2.3	6.4	-1.3	13	-2.8	76.5
	5050.0	-26.2	13	31.6	4.1	1.0	15	-1.8	6.1	1.1	20	-1.6	74.8
	5037.5	-18.4	5	37.7	4.2	4.4	17	-0.3	5.9	7.3	20	0.4	73.0
	5025.0	-17.9	-5	33.0	4.2	10.9	8	6.1	6.1	12.9	12	4.0	75.1
	5012.5	-21.3	0	32.6	4.5	11.2	-3	6.1	6.6	15.7	0	4.6	81.1
	5000.0	-20.2	2	31.0	4.5	12.2	-5	7.7	6.6	16.6	-7	3.0	84.1
	4987.5	-19.1	-5	31.6	4.4	6.9	2	3.6	6.8	12.3	-6	2.1	84.8

Project 592

Standard/Scotchman

file: 592\geophyscwlf_99.wk4

VLF Survey

Line	Station	Frequency (Cutter-Maine - 24.0 kHz) In Phase	Fraser Filter	Out Phase	Field Strength	Frequency (Hawaii - 21.4 kHz) In Phase	Fraser Filter	Out Phase	Field Strength	Frequency (Seattle - 24.8 kHz) In Phase	Fraser Filter	Out Phase	Field Strength
	4975.0	-20.1	-5	28.6	4.3	11.9	-3	3.6	6.5	13.2	-6	1.9	81.1
	4962.5	-23.8	2	32.4	4.3	9.4	-6	4.3	6.5	9.6	-4	2.2	84.3
	4950.0	-20.3	2	31.7	4.2	6.4	-2	1.7	6.7	9.5	-2	0.5	88.2
	4937.5	-21.5	4	28.8	4.4	8.9	-3	1.6	6.6	9.5	-5	0.0	87.7
	4925.0	-20.9	4	30.4	4.5	4.9	1	4.0	6.5	8.0	-7	-0.3	84.1
	4912.5	-17.2	-4	30.6	4.3	7.6	2	-1.6	6.4	6.1	-4	-1.9	85.9
	4900.0	-20.9	-7	31.2	4.3	7.1	-1	0.6	6.4	4.7	2	-2.7	85.1
	4887.5	-21.2	5	32.1	4.4	7.6	0	-2.0	6.5	5.5	5	-2.3	87.8
	4875.0	-23.9	17	31.9	4.5	6.2	0	0.4	6.8	7.3	2	-1.7	85.3
	4862.5	-13.0	9	28.2	4.3	8.1	-4	1.2	7.1	8.0	-3	-0.4	87.9
	4850.0	-14.9	2	27.7	4.3	5.4	-9	1.5	6.9	7.2	-11	-0.6	93.4
	4837.5	-13.1	-4	26.6	4.6	5.1	-12	1.0	7.3	5.1	-15	-2.3	98.8
	4825.0	-13.0	-11	24.3	4.5	-0.6	-10	-5.0	7.1	-0.9	-10	-4.4	91.9
	4812.5	-18.9	-6	27.2	4.5	-1.0	-6	-4.3	6.9	-1.9	-5	-3.6	95.7
	4800.0	-18.2	-5	24.3	4.4	-4.0	-3	-6.0	6.9	-3.8	-3	-3.8	93.3
	4787.5	-19.8	0	22.6	4.7	-4.0	-1	-1.3	7.2	-4.1	-2	-3.8	94.4
	4775.0	-21.9	6	22.9	4.6	-4.3	0	-3.9	7.4	-4.3	-2	-4.1	93.0
	4762.5	-15.9		23.4	4.5	-4.2		-5.2	7.0	-5.2		-3.5	97.2
	4750.0	-19.4		23.3	4.7	-4.2		-4.3	7.1	-4.7		-3.9	98.5
1150 W	4750.0 N	20.1		-28.3	4.5	-2.1		-4.4	7.3	-5.4		-3.2	97.6
	4762.5	22.0		-30.4	4.7	-1.3		-6.1	6.9	-7.7		-3.2	93.0
	4775.0	24.5	-2	-26.0	4.6	-1.8	-1	-5.3	6.8	-5.5	-4	-3.5	92.7
	4787.5	19.7	5	-30.5	4.3	-0.2	-2	-3.5	6.9	-3.4	-6	-2.9	93.5
	4800.0	22.3	-3	-28.1	4.5	-0.8	-4	-3.8	7.0	-3.8	-1	-2.4	89.3
	4812.5	25.0	-10	-30.4	4.5	2.4	-7	-3.2	6.7	-3.8	0	-2.2	91.4
	4825.0	26.8	-6	-25.7	4.4	3.5	-4	-3.6	6.7	-3.3	-1	-2.0	96.2
	4837.5	26.4	0	-27.6	4.6	2.4	-6	-2.1	6.9	-2.9	-9	-1.9	96.6
	4850.0	25.1	-9	-25.3	4.5	9.8	-21	-2.8	7.2	4.9	-26	0.7	97.7
	4862.5	36.8	-22	-22.1	4.3	17.0	-18	5.2	6.8	15.2	-21	4.0	93.6
	4875.0	36.3	-9	-24.9	4.1	13.4	-5	6.7	6.2	7.4	-3	4.7	88.8
	4887.5	34.5	0	-30.6	4.2	18.7	-4	2.3	6.0	15.9	-7	2.8	84.7
	4900.0	38.5	-3	-30.0	4.2	15.5	-2	4.8	5.7	13.4	0	0.9	80.5
	4912.5	35.5	2	-32.2	4.1	18.4	1	0.0	5.8	9.9	13	0.3	78.4
	4925.0	35.1	5	-36.4	3.9	15.0	11	-3.6	6.1	6.5	14	-1.2	82.1
	4937.5	33.6	1	-34.7	3.9	7.9	21	-2.7	5.9	2.9	15	-3.2	82.8
	4950.0	35.8	3	-33.8	4.2	4.8	14	-2.5	5.6	-1.5	13	-4.1	82.7
	4962.5	29.7	13	-31.4	4.0	4.5	4	-2.9	6.0	-1.8	5	-3.6	87.9
	4975.0	26.3	10	-29.3	4.1	4.7	0	-1.8	5.9	-1.6	-2	-3.2	85.2
	4987.5	29.6	-6	-30.4	4.2	4.7	-5	-1.7	6.1	0.0	-7	-2.5	87.0
	5000.0	31.9	-12	-27.4	4.2	9.8	-14	-2.5	6.1	3.7	-11	-0.4	89.0
	5012.5	35.9	-11	-27.7	4.2	14.0	-15	0.5	6.0	5.2	-10	0.3	89.4
	5025.0	36.3	-11	-34.3	4.1	15.0	-6	1.9	5.7	8.1	-11	2.7	88.4
	5037.5	42.1	-11	-32.3	4.1	14.8	2	1.3	5.8	11.9	-13	3.3	84.0
	5050.0	40.7	1	-41.9	3.9	12.3	3	6.3	5.5	14.0	-7	4.1	85.2
	5062.5	37.1	9	-30.5	3.9	14.5	1	1.5	5.6	12.6	4	5.4	80.6
	5075.0	36.7	5	-32.2	3.9	11.4	10	1.2	5.3	9.3	14	3.5	76.8
	5087.5	36.2	7	-31.5	4.1	5.7	13	-3.5	5.6	3.5	13	0.0	78.3
	5100.0	30.7	11	-31.0	4.0	7.3	5	-3.2	6.1	5.0	8	0.0	80.3
	5112.5	31.3	9	-30.1	3.9	5.2	5	-3.4	5.7	-0.1	9	0.1	81.6
	5125.0	26.5	14	-31.9	4.0	2.5	4	-0.9	5.7	-0.4	6	-1.8	78.6
	5137.5	21.4	10	-35.9	4.1	5.6	-4	-4.9	6.0	-0.5	-3	-2.6	83.7
	5150.0	26.1	-9	-30.6	4.1	5.7	-6	-1.2	5.8	2.7	-7	-2.2	86.5

Project 592

Standard/Scotchman

file: 592\geophysc\vlf_99.wk4

VLF Survey

Line	Station	Frequency (Cutter-Maine - 24.0 kHz) In Phase	Fraser Filter	Out Phase	Field Strength	Frequency (Hawaii - 21.4 kHz) In Phase	Fraser Filter	Out Phase	Field Strength	Frequency (Seattle - 24.8 kHz) In Phase	Fraser Filter	Out Phase	Field Strength
	5162.5	30.9	-10	-29.8	4.0	8.3	-5	-2.4	6.0	3.2	-2	-3.3	85.5
	5175.0	26.7	1	-32.6	4.3	7.8	-3	-4.0	6.1	0.9	1	-3.9	90.3
	5187.5	29.7	-2	-29.0	4.2	9.3	-5	-3.2	6.2	4.5	-8	-3.9	92.8
	5200.0	29.5	-6	-29.7	4.2	11.3	-8	0.1	6.1	7.7	-14	-4.3	90.8
	5212.5	33.3	-11	-27.6	4.1	13.4	-11	0.4	6.3	11.5	-12	-2.8	94.7
	5225.0	36.8	-13	-32.6	4.2	17.9	-13	0.1	5.9	13.0	-7	-2.0	90.5
	5237.5	38.9	-6	-32.3	4.1	19.8	-2	-0.6	6.1	12.9	4	-2.5	88.0
	5250.0	37.3		-33.4	3.9	13.8		1.4	5.7	7.9		-3.0	86.3
1100 W	5275.0 N	-14.6		41.9	4.1	15.1		9.7	6.3	21.3		2.7	91.9
	5262.5	-16.4	-4	37.3	4.2	18.9	-1	5.7	6.2	19.0	-11	1.2	92.5
	5250.0	-18.7	3	35.0	4.0	18.6	-12	5.0	6.0	15.7	-6	-0.4	94.4
	5237.5	-16.0	2	38.6	4.2	14.8	-13	3.1	6.1	13.5	-5	0.0	92.6
	5225.0	-15.9	-3	32.5	4.1	10.9	-10	6.0	6.2	15.7	-9	-0.3	96.8
	5212.5	-17.1	-6	33.8	4.1	9.3	-9	4.2	6.0	8.5	-3	-2.0	96.3
	5200.0	-17.5	-12	40.2	4.0	6.6	-10	5.4	5.9	11.4	-7	-1.5	94.4
	5187.5	-21.4	-7	37.2	4.1	5.1	-10	4.5	5.9	9.9	-15	-1.1	89.6
	5175.0	-24.7	-5	35.2	4.0	0.5	-6	3.6	6.0	3.0	-8	-1.3	88.8
	5162.5	-21.1	-1	38.9	4.1	0.9	-2	3.9	5.7	3.4	0	0.9	93.5
	5150.0	-29.8	10	41.3	4.0	-1.7	4	6.9	5.6	1.2	3	1.3	89.3
	5137.5	-16.7	-8	44.9	3.8	1.5	-5	8.2	5.6	4.9	-8	5.3	89.3
	5125.0	-24.3	-17	37.9	4.0	1.4	-9	9.3	6.0	2.9	-15	4.0	91.1
	5112.5	-30.2	-3	38.8	4.1	-6.6	8	3.0	5.8	-5.2	-1	0.0	88.7
	5100.0	-28.2	2	41.5	3.8	0.9	8	1.4	5.2	-1.8	5	2.5	84.5
	5087.5	-29.7	4	40.8	4.0	1.9	3	1.6	5.2	-1.8	5	3.3	86.8
	5075.0	-26.5	-2	40.6	3.9	0.7	5	7.5	5.5	0.0	8	4.0	89.3
	5062.5	-27.9	-1	40.8	3.9	4.6	3	4.1	5.3	1.0	13	4.0	87.6
	5050.0	-30.1	8	42.3	3.8	2.5	2	9.8	5.4	4.8	12	4.5	88.1
	5037.5	-24.9	1	41.7	3.8	6.1	-7	6.2	5.7	8.8	-3	5.6	88.7
	5025.0	-24.7	-10	43.1	4.0	3.4	-17	6.7	5.6	8.7	-18	4.3	92.8
	5012.5	-29.8	-4	34.7	4.1	-2.1	-9	1.1	6.0	2.1	-12	0.4	96.3
	5000.0	-29.6	0	41.2	3.8	-5.1	3	-1.8	5.5	-3.0	5	-3.3	91.0
	4987.5	-28.5	-4	35.8	3.6	-2.5	14	0.7	5.6	2.0	8	-3.6	88.6
	4975.0	-31.4	4	37.2	3.6	-1.5	16	1.4	5.4	1.8	6	-1.8	89.7
	4962.5	-30.5	6	38.8	3.6	7.5	1	0.7	5.1	5.5	7	-0.6	89.5
	4950.0	-25.6	2	41.0	3.6	4.0	5	1.6	5.6	3.9	15	-0.1	94.1
	4937.5	-29.8	11	39.8	3.7	2.8	13	6.0	5.5	10.6	11	0.0	96.9
	4925.0	-24.3	11	40.4	3.7	13.6	4	5.0	5.4	13.9	-1	0.8	91.2
	4912.5	-20.3	7	40.1	3.6	6.1	7	7.2	5.5	11.1	-2	0.6	96.0
	4900.0	-22.5	5	44.1	3.7	14.1	0	5.1	5.4	12.4	-6	2.8	94.9
	4887.5	-14.8	-11	39.6	3.8	12.8	-20	5.1	5.8	10.7	-15	4.7	105.1
	4875.0	-22.6	-12	37.1	3.9	7.2	-17	2.4	6.1	6.6	-15	2.9	106.8
	4862.5	-25.7	-3	35.5	3.9	-0.7	-3	3.6	6.1	1.8	-9	2.0	101.8
	4850.0	-23.4	-4	34.0	3.9	3.8	-3	-1.9	5.6	0.3	-6	2.2	105.2
	4837.5	-27.8	3	35.4	4.0	0.0	-6	0.2	6.0	-1.3	-6	2.1	100.9
	4825.0	-25.7	6	36.6	4.0	0.5	-3	-1.0	5.8	-2.3	-4	2.2	104.4
	4812.5	-22.3	-4	33.9	3.9	-2.2	-5	-2.2	5.8	-4.5	6	2.0	102.4
	4800.0	-25.3	-6	36.5	3.9	-0.1	-7	-1.2	5.7	-3.0	5	2.2	100.0
	4787.5	-26.2	-2	35.6	3.9	-6.8	-4	0.6	5.8	2.3	-14	0.3	103.9
	4775.0	-27.7	-1	33.8	4.0	-2.5	-9	-0.6	6.0	-4.4	-18	1.6	108.8
	4762.5	-26.0		30.2	4.0	-8.0		-0.4	6.0	-9.8		-0.4	107.6
	4750.0	-29.0		26.4	4.1	-9.9		0.4	6.1	-9.9		-2.3	108.2

Project 592

Standard/Scotchman

file: 592\geophysc\vlf_99.wk4

VLF Survey

Line	Station	Frequency (Cutter-Maine - 24.0 kHz) In Phase	Fraser Filter	Out Phase	Field Strength	Frequency (Hawaii - 21.4 kHz) In Phase	Fraser Filter	Out Phase	Field Strength	Frequency (Seattle - 24.8 kHz) In Phase	Fraser Filter	Out Phase	Field Strength
1050 W	4750.0 N	22.3		-30.7	4.0	-1.4		-6.3	6.3	-6.4		2.2	107.8
	4762.5	21.4		-32.8	4.1	-0.6		-4.2	6.0	-9.2		2.0	110.2
	4775.0	22.3	-4	-29.7	4.1	-0.3	-2	-3.2	6.0	-6.8	-5	2.9	111.9
	4787.5	25.6	-9	-27.7	4.0	0.2	-8	1.7	5.9	-3.6	-12	4.8	109.9
	4800.0	26.8	-4	-30.0	4.0	6.9	-15	-2.6	6.2	-0.5	-9	5.1	112.1
	4812.5	24.9	0	-26.9	3.9	7.7	-4	-1.8	5.8	-1.2	-6	5.4	105.5
	4825.0	27.7	-9	-26.9	3.9	3.6	3	2.6	5.7	2.7	-6	4.9	105.2
	4837.5	32.8	-11	-24.8	3.8	8.1	-3	-1.7	5.8	1.3	-2	5.8	109.8
	4850.0	30.9	2	-26.8	3.9	6.5	-1	-1.2	5.6	1.7	-1	4.3	107.1
	4862.5	28.1	3	-31.0	3.9	5.8	-3	4.4	5.4	2.9	-3	4.8	102.7
	4875.0	33.0	-4	-26.3	4.0	11.5	-12	-4.2	5.9	2.6	-1	4.7	104.4
	4887.5	29.5	-2	-27.6	3.6	13.0	-4	-1.9	5.8	3.1	-1	4.4	108.7
	4900.0	33.6	-7	-32.1	3.9	8.7	5	2.6	5.7	3.3	-5	5.1	106.9
	4912.5	35.8	-10	-31.9	3.9	11.3	-5	4.3	5.3	7.4	-8	4.7	106.8
	4925.0	37.3	-4	-34.2	3.8	15.1	-12	-3.2	5.5	7.2	-5	3.9	102.2
	4937.5	36.2	0	-34.3	3.7	16.9	0	-4.2	5.1	8.4	-2	2.1	98.8
	4950.0	37.0	3	-33.3	3.8	9.9	15	1.4	5.0	8.5	5	1.3	94.2
	4962.5	33.7	7	-39.6	3.6	7.1	14	2.2	4.8	2.2	14	0.9	99.5
	4975.0	32.6	7	-35.6	3.8	5.6	7	-0.8	5.1	0.6	11	0.0	101.3
	4987.5	31.6	10	-37.8	3.7	4.0	2	-3.9	5.2	-1.1	8	-1.1	102.1
	5000.0	24.4	13	-32.0	3.6	6.5	-5	-9.8	5.6	-4.1	6	-1.4	104.3
	5012.5	26.4	-1	-33.8	3.9	8.2	-8	-7.7	5.7	-2.7	-4	-0.3	108.0
	5025.0	30.4	-14	-28.5	3.7	10.7	-4	-1.3	5.4	1.6	-12	4.0	106.9
	5037.5	34.7	-13	-32.6	3.5	7.5	3	5.9	5.1	3.8	-9	7.2	105.6
	5050.0	34.8	-4	-34.8	3.8	8.4	-3	6.9	5.0	4.2	-3	7.1	106.0
	5062.5	34.1	2	-28.6	3.5	13.1	-3	-1.1	5.3	4.4	2	5.8	100.3
	5075.0	33.0	-1	-29.9	3.6	5.8	11	4.5	4.8	1.6	7	6.0	99.5
	5087.5	37.1	-2	-30.0	3.6	4.5	3	3.0	5.1	0.2	5	6.0	102.5
	5100.0	31.7	6	-29.4	3.7	11.9	-6	-1.3	5.3	0.4	2	7.7	101.5
	5112.5	32.1	4	-29.5	3.7	4.7	4	2.2	5.5	-0.8	-1	7.3	106.0
	5125.0	32.8	-9	-25.1	3.9	8.2	-6	5.4	5.5	2.7	-7	9.6	108.6
	5137.5	39.5	-13	-23.6	3.9	14.7	-10	5.1	5.2	3.7	-4	13.3	100.1
	5150.0	38.4	-6	-23.7	3.7	8.1	2	10.0	4.8	2.4	6	11.2	100.6
	5162.5	39.7	-6	-27.5	3.8	13.1	2	0.2	5.2	-1.8	10	10.4	97.4
	5175.0	43.8	-8	-24.2	3.7	7.9	1	7.9	4.8	-1.6	10	13.5	96.3
	5187.5	42.3	-2	-30.3	3.6	11.9	5	-5.6	5.1	-8.2	15	10.7	92.8
	5200.0	42.9	2	-34.8	3.4	4.1	9	1.2	4.7	-10.5	12	10.0	91.2
	5212.5	40.8	10	-37.1	3.6	7.0	-1	-6.7	4.7	-10.8	-1	3.0	98.5
	5225.0	34.7	9	-37.7	3.5	10.3	-7	-7.1	5.4	-6.7	-4	1.5	100.8
	5237.5	39.7	2	-34.1	3.8	7.8	1	-10.1	5.4	-10.6	5	-0.6	102.1
	5250.0	34.3		-42.3	3.6	8.2		-12.0	5.2	-12.1		-0.5	105.1
1000 W	5250.0 N	-29.7		57.7	3.3	1.9		6.4	4.4	-2.8		9.6	88.4
	5237.5	-33.0	13	53.7	3.5	-6.0	-1	12.9	4.7	-5.3	9	9.4	93.2
	5225.0	-27.0	15	46.5	3.6	-3.6	16	12.7	4.9	-3.2	18	10.1	95.8
	5212.5	-23.1	6	49.6	3.5	-1.2	13	15.7	4.8	3.9	13	13.0	94.3
	5200.0	-22.0	2	52.3	3.5	7.3	-1	12.3	4.7	5.3	11	16.0	93.1
	5187.5	-21.7	3	52.1	3.6	1.1	14	17.6	5.2	7.9	15	15.5	99.4
	5175.0	-21.2	10	44.3	3.8	4.5	22	17.2	5.4	11.9	11	15.7	100.3
	5162.5	-19.2	6	47.0	3.8	17.6	-2	15.7	5.1	16.0	-7	16.7	108.2
	5150.0	-13.8	-8	47.6	3.8	10.1	-13	15.9	5.4	14.5	-20	16.1	113.7
	5137.5	-20.5	-9	36.5	4.2	10.5	-18	5.0	5.6	6.7	-14	6.8	116.7
	5125.0	-20.0	-6	38.6	3.9	4.5	-14	3.7	5.3	3.6	-4	6.1	112.9

Project 592

Standard/Scotchman

file: 592\geophysc\vlf_99.wk4

VLF Survey

Line	Station	Frequency (Cutter-Maine - 24.0 kHz) In Phase	Fraser Filter	Out Phase	Field Strength	Frequency (Hawaii - 21.4 kHz) In Phase	Fraser Filter	Out Phase	Field Strength	Frequency (Seattle - 24.8 kHz) In Phase	Fraser Filter	Out Phase	Field Strength
	5112.5	-23.7	-6	38.5	3.7	-1.9	6	8.8	5.3	4.1	0	5.2	112.3
	5100.0	-22.6	-7	42.1	3.7	2.8	9	3.8	5.1	2.5	-1	5.8	109.7
	5087.5	-26.6	2	42.8	3.7	5.7	-5	5.9	5.4	5.1	1	6.4	111.5
	5075.0	-27.0	7	42.3	3.8	3.7	-5	4.7	5.1	0.6	5	8.3	110.0
	5062.5	-20.4	-6	39.3	3.7	0.2	5	9.4	5.2	7.9	-4	5.2	112.0
	5050.0	-25.8	-13	39.9	3.9	4.2	2	2.2	5.1	3.2	-5	3.6	107.3
	5037.5	-27.8	-4	36.1	3.7	4.3	-8	1.5	5.2	1.8	1	3.5	109.9
	5025.0	-31.2	3	41.1	3.9	2.0	-9	0.0	5.3	4.0	-3	0.4	107.3
	5012.5	-26.3	-2	41.7	3.7	-1.9	3	5.5	5.2	1.7	-3	1.4	107.2
	5000.0	-29.8	0	38.2	3.7	-0.5	5	7.4	5.4	1.1	3	1.8	115.3
	4987.5	-30.0	6	38.9	3.8	4.0	5	0.1	5.0	1.2	14	2.4	108.5
	4975.0	-25.9	-1	43.0	3.5	-1.3	18	9.3	5.2	4.9	13	1.6	108.1
	4962.5	-28.3	-1	39.3	3.6	10.1	11	2.8	5.0	11.0	3	0.8	106.4
	4950.0	-28.7	8	37.9	3.9	10.6	-13	3.1	5.3	8.4	-6	2.4	110.9
	4937.5	-26.4	8	35.5	3.7	9.2	-26	3.0	5.3	10.5	-15	2.0	112.9
	4925.0	-23.1	-2	41.6	3.7	-1.0	-9	5.1	5.7	2.8	-9	3.0	121.5
	4912.5	-23.6	-9	39.9	3.7	-4.7	7	7.1	5.7	1.5	3	2.8	114.2
	4900.0	-27.8	-5	37.4	3.7	4.1	2	2.1	5.1	2.8	5	6.2	113.4
	4887.5	-27.7	3	37.7	3.9	-3.0	9	9.1	5.7	4.4	6	7.4	115.0
	4875.0	-28.2	11	36.1	4.0	3.9	10	4.2	5.3	4.9	5	7.4	115.1
	4862.5	-24.4	10	39.7	3.8	6.2	-1	6.5	5.3	8.2	3	6.7	112.5
	4850.0	-20.5	1	40.5	3.8	4.7	-7	5.5	5.0	6.4	-4	7.1	118.2
	4837.5	-22.5	-1	36.5	4.0	4.0	-10	4.0	5.7	9.9	-16	3.6	117.2
	4825.0	-21.8	-2	32.7	3.9	-0.1	-13	2.2	5.6	0.7	-12	8.0	123.1
	4812.5	-22.2	-3	30.3	3.9	-1.5	-12	1.7	5.7	-0.1	-2	6.0	122.6
	4800.0	-24.2	-1	30.7	4.0	-7.2	-5	4.9	5.6	-1.1	0	5.1	121.6
	4787.5	-23.0	-2	31.3	3.9	-6.3	1	6.7	6.0	-0.7	-4	5.7	120.7
	4775.0	-24.6	-8	32.9	4.0	-7.0	-2	6.8	5.9	-0.9	-11	3.5	122.8
	4762.5	-24.4		30.0	4.0	-5.4		-0.2	5.6	-5.1		4.4	125.5
	4750.0	-31.0		31.2	4.1	-9.8		-2.2	5.7	-7.6		1.3	126.4

5460000N

3050000E

3060000E

3070000E

Orofino Creek

E & B Claim Group

5459000N

5458000N

5457250N

4500

4000

3600

3000

5000

197801
197802
197803

197804 15
197805 60

35cm q-py

1.5m q

1.5cm q

2m q

slump

cabin

2a

2

1

3

5250N

5000N

4750N

1300E

1250E

1200E

1150E

1100E

1050E

1000E

LEGEND

- Soil sample location
- 197805 X — Rock sample location
- 30 — Values shown in ppb gold
- \- — Indicates <2 ppb Au
- Trench location
- 30 — Attitude of shear/fault
- 85 — Attitude of bedding
- q.py — Quartz, pyrite
- Geological boundary
- Outcrop area

Geology

- 3 — Diorite
- 2 — Granite
- 2a — Mega-crystic granite
- 1 — Gneiss

26,146

DRAWN:		Dec.1/1999
REVISION DATE	REVISED BY	REVISION
Dec.3/1999	RM	Geology+data
Path:		592/geoc_592dwg

2°05'

UTM Grid North

True North

Topographic contour interval = 100 feet

0 50 100 150 200 250 300 350

METRES

DISCOVERY Consultants

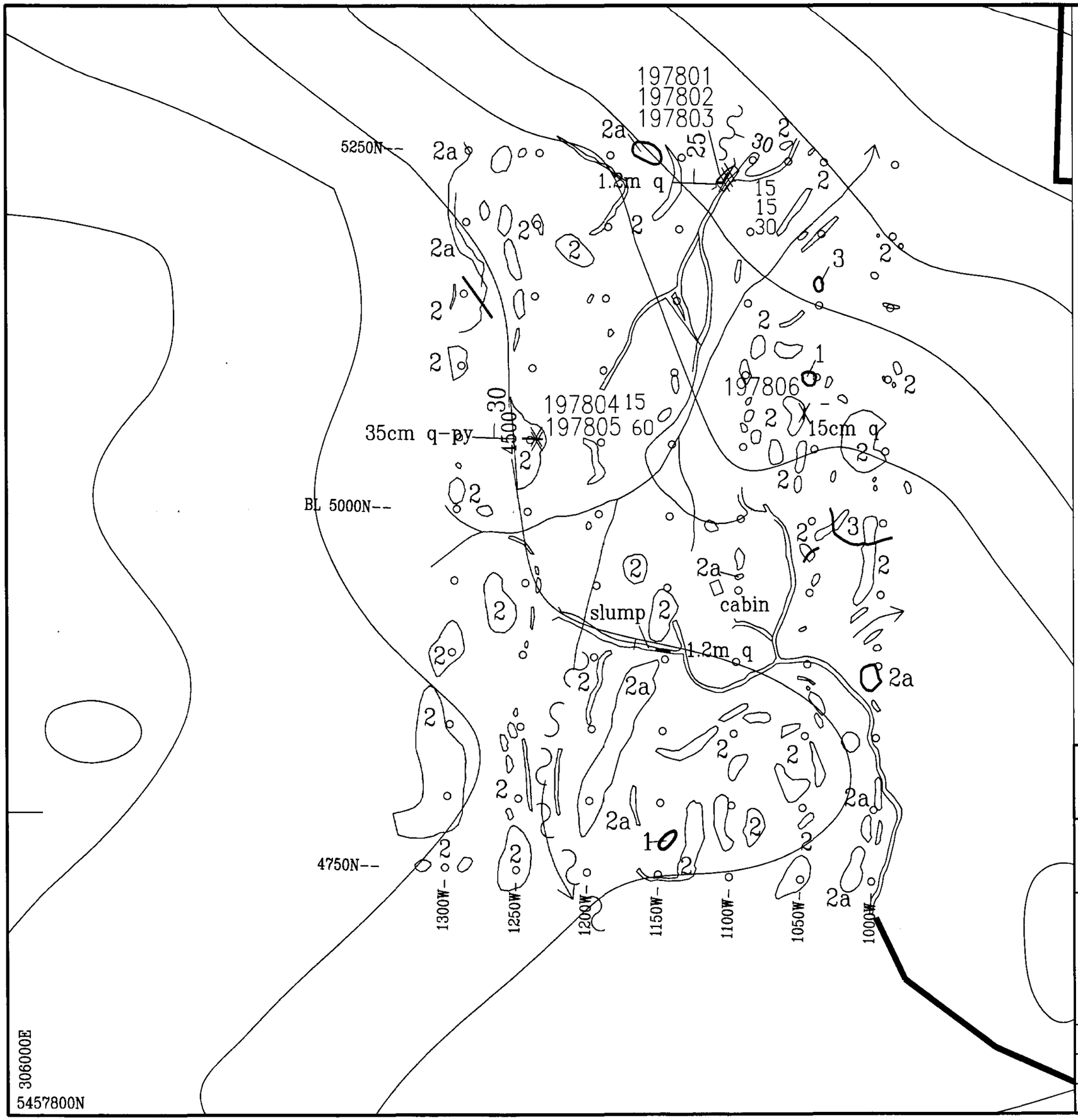
KILBACK

Scotchman Property

Geochemical Sampling

Geology + Gold in Rocks

Location: Oliver		Mining Jurisdiction:	Osoyoos
Datum: NAD27	Map Ref.: 082E/4E,5E	Scale: 1:5000	UTM: 11
Project: 592	Date: Dec.17/1999	Drawn By: RM	Figure: 3



LEGEND

197805 X	Rock sample location
30	Values shown in ppb gold
-	Indicates <2 ppb Au
	Trench location
30	Attitude of shear/fault
85	Attitude of bedding
q,py	Quartz, pyrite
	Geological boundary
	Outcrop area

Geology

3	Diorite
2	Granite
2a	Mega-crystic granite
1	Gneiss

0 50 100 150m

metres

GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT

21,217

DISCOVERY Consultants

KILBACK

Scotchman Property

Geochemical Sampling

Geology + Gold in Rocks

Location: Oliver		Mining Jurisdiction: Osoyoos	
Datum: NAD27	Map Ref.: 082E/4E,5E	Scale: 1:2500	UTM: 11
Project: 592	Date: Dec.17/1999	Drawn By: RM	Figure: 3a

PROFESSIONAL ENGINEER C.H. CARPENTER BRITISH COLUMBIA

5480000N

3905000E

3910000E

3915000E

3920000E

Orofino Creek

4500

4000

3500

3000

E & B Claim Group

5459000N

5458000N

5457250N

5250N

BL 5000N

4750N

1300W 1250W 1200W 1150W 1100W 1050W 1000W

5000

4500

4000

3500

n/s

LEGEND

- ∘ Soil sample location
- 10 Values shown in ppb gold
- - Indicates <2 ppb au

Trench location

GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT

26,146

DRAWN:	Dec.1/1999
REVISION DATE	REVISED BY	REVISION
Dec.3/1999	RM	Geology+data
Path:	592/geoc_592dwg

2°05'

UTM Grid North

True North

Topographic contour interval = 100 feet

0 50 100 150 200 250 300 350

METRES

DISCOVERY Consultants

KILBACK

Scotchman Property

Geochemical Sampling

Gold in Soils

Location: Oliver		Mining Jurisdiction: Osoyoos	
Datum: NAD27	Map Ref.: 082E/4E,5E	Scale: 1:5000	UTM: 11
Project: 592	Date: Dec.17/1999	Drawn By: RM	Figure: 4

PROFESSIONAL ENGINEER PROVINCE OF BRITISH COLUMBIA T. M. CARPENTER

5460000N

5459000N

5458000N

5457250N

3050000E

3060000E

3070000E

3080000E

Orofino Creek

4500

4000

3500

3000

E & B Claim Group

BL 5000N

5250N

4750N

1300W

1250W

1200W

1150W

1100W

1050W

1000W

5000

4500

4000

3500

LEGEND

- Soil sample location
- 6 Values shown in ppm lead
- Trench location

26,146

DRAWN:		Dec.1/1999
REVISION DATE	REVISED BY	REVISION
Dec.3/1999	RM	Geology+data
Path:		592/geoc_592dwg

2°05'

UTM Grid North

True North

Topographic contour interval = 100 feet

0 50 100 150 200 250 300 350

METRES

DISCOVERY Consultants

KILBACK

Scotchman Property

Geochemical Sampling

Lead in Soils

Location: Oliver		Mining Jurisdiction: Osoyoos	
Datum: NAD27	Map Ref.: 082E/4E,5E	Scale: 1:5000	UTM: 11
Project: 592	Date: Dec.17/1999	Drawn By: RM	Figure: 5

PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
GEOSCIENTIST

5480000N

3950000E

3960000E

3970000E

3980000E

5480000N

Orofino Creek

4500

4000

3600

3000

5459000N

E & B Claim Group

5250N

BL 5000N

4750N

1300W 1250W 1200W 1150W 1100W 1050W 1000W

5458000N

5000

4500

4000

3500

5457250N

LEGEND

- Soil sample location
- 58 Values shown in ppm zinc
- Trench location

GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT

26,146

DRAWN:		Dec.1/1999
REVISION DATE	REVISED BY	REVISION
Dec.3/1999	RM	Geology+data
Path:		592/geoc_592dwg

UTM Grid North
2°05'
True North

Topographic contour interval = 100 feet

0 50 100 150 200 250 300 350

METRES

DISCOVERY Consultants

KILBACK

Scotchman Property

Geochemical Sampling

Zinc in Soils

Location: Oliver		Mining Jurisdiction:	Osoyoos
Datum: NAD27	Map Ref.: 082E/4E,5E	Scale: 1:5000	UTM: 11
Project: 592	Date: Dec.17/1999	Drawn By: RM	Figure: 6

PROFESSIONAL ENGINEER J. W. CARPENTER BRITISH COLUMBIA GEOSCIENTIST