

GEOCHEMICAL, GEOPHYSICAL AND DIAMOND DRILLING

ASSESSMENT REPORT

ON THE

BROKEN HILL-LEO PROPERTY

NTS: 082M/14

Latitude: 51° 50' N Longitude: 119° 15' W

KAMLOOPS MINING DIVISION

AVOLA AREA

BRITISH COLUMBIA

FOR

CASSIDY GOLD CORPORATION

220-141 Victoria Street

Kamloops, British Columbia

V2C 1Z5

BY

Joseph Eugene Leopold Lindinger, P. Geo

879 McQueen Drive

Kamloops, British Columbia

V2B 7X8

NOVEMBER 20, 2001

GEOLOGICAL SURVEY BRANCH

26,692

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SUMMARY

The 181 unit Broken Hill-Leo property is located 150 km north-northeast of Kamloops and 6 km east of the village of Avola, British Columbia on NTS map sheet 082M/14.

The property covers the newly discovered (September 2000) Vista (15.9% Zn over 0.3m), the Navan (21.5% Zn, 3.8% Pb and 11 g/t Ag) and the Mike (20% Zn in float) occurrences. Cassidy Gold Corp. has an option to earn a 100% interest in the property from Mr. JEL (Leo) Lindinger, the optionor and writer of this report.

The property has no recorded mineral exploration history

The Broken Hill-Leo property is underlain by poorly mapped highly deformed high grade metamorphic rocks of the Proterozoic to Paleozoic Shuswap Metamorphic Complex portion of the Kootenay Terrane. Similar rocks to the east are assigned to the Proterozoic Horsethief Creek Group. The sequence consists of three distinct lithological packages, a lower amphibolite-biotite gneiss unit, a middle biotite gneiss-calc-silicate unit with minor marble and chert, and an upper by mixed siliceous biotite schist and quartzite unit. The middle unit hosts the known zinc-lead-silver mineralization in the region, and on the property. All lithologies are intruded by Devonian orthogneisses, Cretaceous and Tertiary felsic stocks, plugs, sills and dykes. Late Tertiary andesitic to mafic plugs and dykes, and lamprophyric dykes are common

The Broken Hill-Leo property covers a 9 km strike extent of the carbonate stratigraphy on the east side of the North Thompson River valley, favourable for hosting high grade zinc-lead-silver 'Shuswap' style mineralization similar to Ruddock Creek (5 million tonnes grading 7.5% Zn, 2.5% Pb) and CK (1.5 million tonnes grading 8.6% Zn). The Vista Occurrence is in the northwest part of the claims. The Navan occurrences are located 1.3 km southeast of the Vista occurrence. The Mike float showing is located 4 kilometers south of the Navan occurrence.

From late September 2000 to early February 2001 a multiphased rock and soil geochemical, gravity geophysical, and diamond drilling program was completed over parts of the Broken Hill-Leo property to test the economic potential of the property for Shuswap style (carbonate hosted sedimentary exhalative type) mineralization.

In early October 2000, a single grid was established over the new discoveries. This grid was used for control for multielement geochemical soil and rock sampling programs. Results from this program partially outlined strong zinc, lead and silver geochemical soil anomalies. The rock sampling program detailed and expanded the mineralization in and around the known showings.

In late November and early December part of the control grid over the Vista and Navan showings was brushed and expanded to allow for a gravity survey to be completed over the prospective area over and between the Vista and Navan occurrences. Although the completed gravity survey did not actually extend to the Vista and Navan showings, it did produce several moderate anomalies, that upon consideration by Cassidy Gold Corp. management warranted drilling.

In January and February, 2001 a 930meter 13 hole diamond drill program was completed. The holes tested approximately 1.2 kilometers of the strike length of the Vista-Navan horizon between the Vista and Navan showings. Most of the holes tested gravity anomalies that were delineated by the geophysical survey. Several holes tested the down dip extent of known mineralization at the Vista and Navan Showings. The Mike area was not tested.

The drill program was successful in intersecting both the Vista and Navan mineralized horizons, down dip from the surface exposures. The drilling results indicate that the Vista and Navan Horizons appear to be the same

A mineralized portion of the Vista Horizon was intersected in DDHBH 01-03 and DDHBN 01-13, approximately 500m east-southeast of the Vista Showing. A weighted average of the mineralized zone in hole DDHBH01-13 returned 2.5% Zn over 3.9m (2.3m true width). Magnetic pyrrhotite is also present. Another mineralized intersection in DDH 01-03 was interrupted by a pegmatite sill, with the remnant mineralization grading 1.2% Zn over 1.1m (weighted average).

The Navan Horizon was successfully intersected 25m down dip from the surface showing by DDHBH 01-06. However the mineralization was disrupted, diluted and truncated by a pegmatite sill. The diluted intersection grades 1.2% Zn with 0.1% Pb over 0.25m. The Navan Horizon should also have been intersected in DDHBH 01-05, -07 and possibly in the very top of DDHBH 01-08 but a large pegmatite sill of leucogranite-tonalite intrusive invades the stratigraphy in this area.

Zinc mineralization was not intersected in the other holes due to; no actual mineralization being present, the drill hole collared too low in the stratigraphy missing the mineralized horizon, not drilling deep enough, and/or was invaded and destroyed by pegmatite sills.

In conclusion, most of the soil anomalies remain open, the gravity survey tested less than 1 kilometer (about 20% of the known strike length of the favourable lithologies hosting the mineralization), the drilling program partially tested only about 1.2 kilometers of the area between the Vista and Navan showings. Therefore the property remains highly prospective for presence of undiscovered economic quantities of mineralization

The areas north and east of the Vista occurrence remain to be tested. The partially outlined soil anomalies and the source of the mineralized float at the Mike showing remain to be tested and expanded. The prospective stratigraphy between the Vista-Navan-Mike horizon and the bottom of the North Thompson River valley, the extensions of the calc-silicate horizon southeast of the Navan occurrence, and many other prospective areas of the property remain unexplored. The excellent access and infrastructure add to the potential of the property.

To determine the properties full potential for Shuswap style mineralization the prospective stratigraphy needs to be traced and mapped along strike and down-dip. In particular fold closures need to be defined in order to target areas of thickening of the mineralized horizon.

Recommended is a program of detailed geological and structural mapping, prospecting, rock and soil geochemical sampling, ground or airborne magnetic surveys. Excavator trenching of the Vista and Mike showings, and any newly discovered mineralization is also recommended. Diamond drilling of the targets already outlined in the Vista area, and any new targets would follow.

INTRODUCTION

This report documents the results of soil and rock sampling, geophysical (gravity) and 930m diamond drill programs completed between October 1, 2000 and February 5, 2001 on the Broken Hill-Leo property near the North Thompson River village of Avola, British Columbia. The program was designed; to explore for extensions of Shuswap style (carbonate hosted sedimentary exhalative type high grade zinc bearing massive sulphide mineralization discovered in September, 2000 by Mr. Leo Lindinger.

The known massive sulphide showings on the Broken Hill-Leo property include the Vista (15.9% Zn over 0.3m), the Navan (21.5% Zn, 3.8% Pb and 11 g/t Ag) and the Mike (20% Zn in float), hosted by carbonate stratigraphy of the Shuswap Metamorphic Complex portion of the Kootenay Terrane.

LOCATION, ACCESS AND INFRASTRUCTURE (Figure 2)

The Broken Hill-Leo property is located on the east side of the steep sided North Thompson River valley, 150 km north-northeast of Kamloops, and 6 km northeast and east of the village of Avola, British Columbia. The property is located on NTS map sheet 082M/14, at latitude $51^{\circ} 46-50'$ north, longitude $119^{\circ} 12-15'$ west.

Road access to the property is via Highway 5 (Yellowhead Highway) east onto the Shannon Creek logging road, 0.5 km north of Avola. The Shannon Creek logging road crosses through the property from 12.1 km to 19 km. The Cornice logging road originates at the 11.5 km mark of the Shannon Creek logging road, runs onto the property near the 3 km mark and accesses the areas west of Fowler Lake. Road access to the east central side of the property is via the Fowler logging road, which originates from the Shannon Creek logging road at 17.5 km. Road access to the south and east sides of the property are via the Shannon Creek logging road, which at 20 km intersects the Otter Creek logging road at km 29. The Dustin-Shannon spur accesses the east side of Shannon lake and originates at 15.5 km on the Shannon Creek logging road. The southeast part of the property is accessed by the Otter Creek logging road. Road access to the north part of the property is via Highway 5 (Yellowhead Highway) east onto the Finn Creek logging road 19 km north of Avola, then at the 0.75 km mark, south onto the Elevator logging road. The property is first accessed at approximately 18 km on the Elevator logging road.

The Canadian National Railway mainline in the north Thompson River valley is less than 2.5 km west of the property. A medium sized high tension power line strikes through the west side of the valley. Fuel, food, accommodation and freight services are available in Avola and Blue River, which are both less than 40 km from the property.

PHYSIOGRAPHY

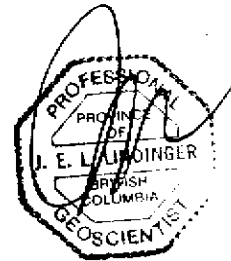
The region lies at the northwest end of the Shuswap Highland of the Interior Plateau. The North Thompson River occupies a south draining, steeply incised valley, the floor of which is about 1200 meters below the surrounding plateau.

The Broken Hill-Leo property covers a 9.5 km portion of the east side of the North Thompson River valley, northeast of Avola surrounding Fowler Lake. The lowest part of the property is the flood plain of the North Thompson River at 580m. The highest parts are at 1750m on the Mike, Jimm and Dian claims east and south of Shannon Lake.

BRITISH COLUMBIA



BROKEN HILL PROJECT



KAMLOOPS

0 250 KM

VANCOUVER

CASSIDY GOLD CORPORATION
BROKEN HILL PROPERTY
FIGURE 1
LOCATION MAP

AVOLA AREA
KAMLOOPS MINING DIVISION

NTS 082M/14 - 51 Deg. 49' N, 119 Deg. 14' W
MARCH 9, 2001

GRAPHICS BY RENAISSANCE GEOSCIENCE SERVICES

The vegetation on the lower parts of the property consists of lodgepole pine, interior fir and black spruce. Balsam predominates at upper elevations, with pine on dry, substrate deficient cliffs.

PROPERTY

The Broken Hill-Leo property consists of eight modified grid and 55 two post claims, totaling 181 units. The claims are contiguous and cover approximately 50 square kilometers. They cover the recently discovered Vista, Navan and Mike high grade carbonate associated zinc+/-lead+/-silver occurrences. Cassidy Gold Corp., has an option to earn a 100% interest in the Broken Hill-Leo property subject to certain cash payments and share allotments to Mr. Lindinger, and incurring certain exploration expenditures. The exploration expenditures made to date are applied for assessment credit in Statement of Work Event# 3170598, Kamloops Mining Division

CLAIM	RECORD	UNITS	EXPIRY DATE	CLAIM	RECORD	UNITS	EXPIRY DATE
VISTA	380752	4	Sept. 14, 2002*	NAVAN 18	380789	1	Sept. 14, 2002*
VISTA 1	380753	1	Sept. 11, 2002*	NAVAN 19	380790	1	Sept. 14, 2002*
VISTA 2	380754	1	Sept. 11, 2002*	NAVAN 20	380791	1	Sept. 14, 2002*
VISTA 3	380755	1	Sept. 11, 2002*	NAVAN 21	380792	1	Sept. 14, 2002*
VISTA 4	380756	1	Sept. 11, 2002*	NAVAN 22	380793	1	Sept. 14, 2002*
VISTA 5	380757	1	Sept. 14, 2002*	NAVAN 23	380794	1	Sept. 14, 2002*
VISTA 6	380758	1	Sept. 14, 2002*	NAVAN 24	380795	1	Sept. 15, 2002*
VISTA 7	380759	1	Sept. 14, 2002*	NAVAN 25	380796	1	Sept. 15, 2002*
VISTA 8	380760	1	Sept. 14, 2002*	NAVAN 26	380889	1	Oct. 01, 2002*
VISTA 9	380761	1	Sept. 14, 2002*	MIKE	380890	20	Oct. 01, 2002*
VISTA 10	380762	1	Sept. 15, 2002*	VISTA A	380891	8	Oct. 01, 2002*
VISTA 11	380763	1	Sept. 15, 2002*	MIK1	381767	1	Oct. 28, 2002*
VISTA 12	380764	1	Sept. 15, 2002*	MIK2	381768	1	Oct. 28, 2002*
VISTA 13	380765	1	Sept. 15, 2002*	MIKY	381777	20	Oct. 26, 2002*
VISTA 14	380766	1	Sept. 15, 2002*	JIMM	381778	18	Oct. 27, 2002*
VISTA 15	380767	1	Sept. 15, 2002*	DIAN	381779	16	Oct. 28, 2002*
VISTA 16	380768	1	Sept. 15, 2002*	LEO 1	381891	20	Nov. 4, 2002*
VISTA 17	380769	1	Sept. 15, 2002*	LEO 2	381892	20	Nov. 4, 2002*
VISTA 18	380770	1	Sept. 15, 2002*	LL1	381893	1	Nov. 2, 2002*
VISTA 19	380771	1	Sept. 15, 2002*	LL2	381894	1	Nov. 2, 2002*
NAVAN 0	380772	1	Sept. 11, 2002*	LL3	381895	1	Nov. 3, 2002*
NAVAN 1	380773	1	Sept. 11, 2002*	LL4	381896	1	Nov. 3, 2002*
NAVAN 2	380774	1	Sept. 11, 2002*	LL5	381897	1	Nov. 3, 2002*
NAVAN 3	380775	1	Sept. 11, 2002*	LL6	381898	1	Nov. 4, 2002*
NAVAN 5	380776	1	Sept. 11, 2002*	LL7	381899	1	Nov. 4, 2002*
NAVAN 6	380777	1	Sept. 15, 2002*	LL8	381900	1	Nov. 4, 2002*
NAVAN 7	380778	1	Sept. 15, 2002*	TOTAL	181		
NAVAN 8	380779	1	Sept. 15, 2002*				
NAVAN 9	380780	1	Sept. 15, 2002*				
NAVAN 10	380781	1	Sept. 14, 2002*				
NAVAN 11	380782	1	Sept. 14, 2002*				
NAVAN 12	380783	1	Sept. 14, 2002*				
NAVAN 13	380784	1	Sept. 14, 2002*				
NAVAN 14	380785	1	Sept. 14, 2002*				
NAVAN 15	380786	1	Sept. 14, 2002*				
NAVAN 16	380787	1	Sept. 14, 2002*				
NAVAN 17	380788	1	Sept. 14, 2002*				

* with acceptance of the work program expenditures by the Ministry of Energy and Mines that this report documents.

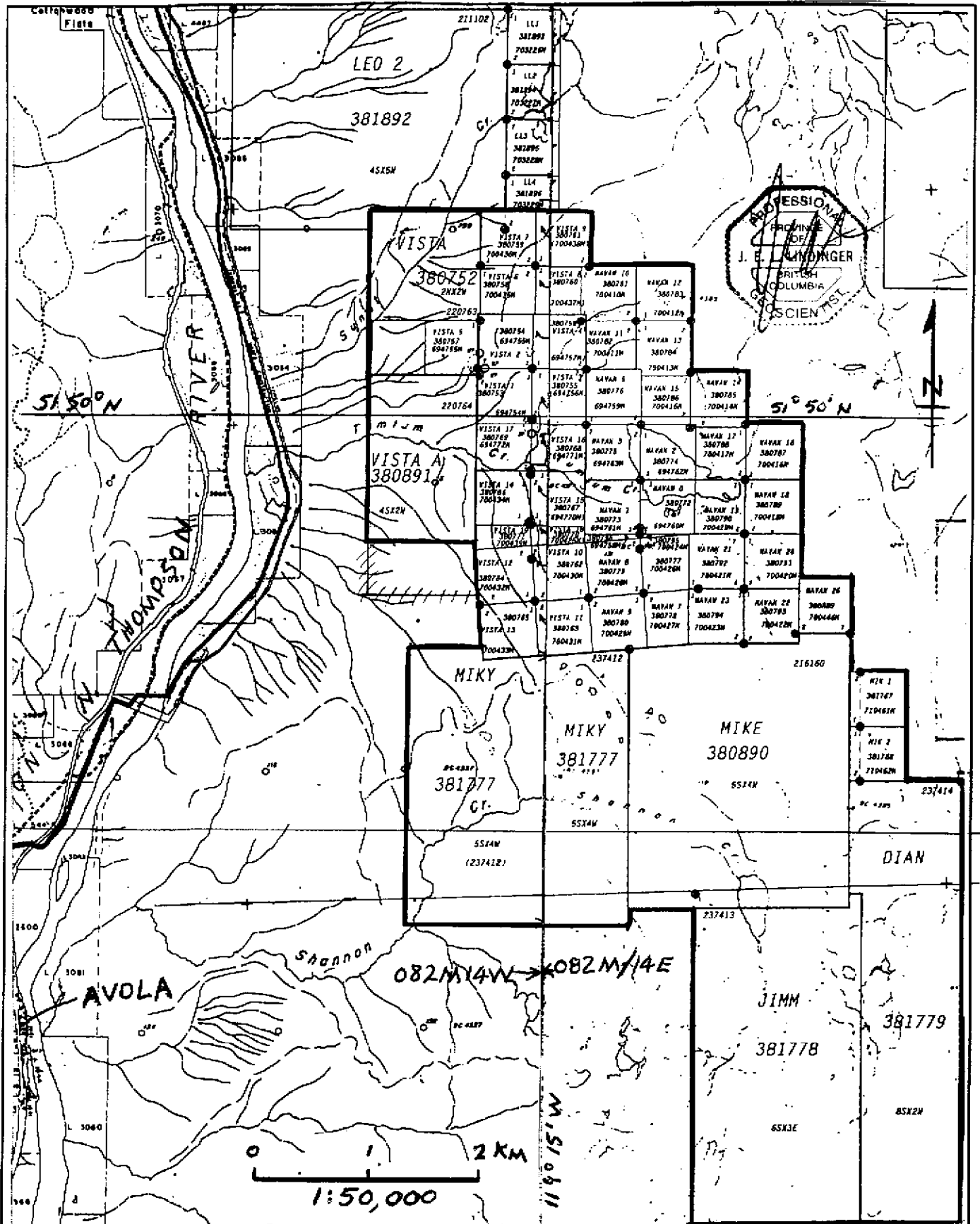


Figure 3 - MINERAL TENURE MAP BROKEN HILL PROPERTY

HISTORY

There is no written record of any previous private industry geological work on the Broken Hill-Leo property. The oldest known significant zinc-lead-silver massive sulphide base metal discoveries in the region include Ruddock Creek (1961) and Cotton Belt (1905) in the Monashee Mountains, east of the area. More recent discoveries, made with the penetration of logging roads into the rugged interior, north and west of the area include, the CK (Zn-Pb-Ag) (1972), Finn (Zn-Pb-Ag), Dimac tungsten skarn, and Trio and Hydro molybdenum prospects. The Finn occurrence, 8 km north of the Broken Hill-Leo property was discovered in 1978 (Murrell, 1980). Very recent discoveries in the area include the Bizar Au-Bi-Cu veins (1998) east of Ground Hog Mountain, the Readymix Au-Bi-Cu veins (2000) about 10 km to the west, and in September 2000 the Vista, Navan and Mike Zn-Pb-Ag massive sulphide showings that the Broken Hill-Leo Property now covers.

A government regional geochemical silt survey was completed in 1972. Results indicate that the drainages originating from the Broken Hill-Leo property are moderately to weakly anomalous in zinc, lead and gold.

Various prospectors and mining companies have since 1979 staked claims north south and east of, but not on the area now covered by the Broken Hill-Leo property.

In October, 2000 a 1x5 km area in the central part of the Broken Hill-Leo property was explored under the direction of Mr. W. Gruenwald, P. Geo. by limited geological mapping and soil and rock sampling. The results of this program produced several open ended soil anomalies. (Figure 7a, 7b, 7c). Based on these results additional claims were staked including the Leo claims north of the Vista area in late October and early November, 2000. In December, 2000 a gravity survey was completed by Discovery Geophysics Ltd. In late January and early February 2001 a 13 hole diamond drill program was completed by LDS Diamond Drilling Ltd. of Kamloops, B.C.. The drill program targets included the earlier defined gravity and geochemical anomalies and down dip extensions of the VISTA and NAVAN mineralized horizons.

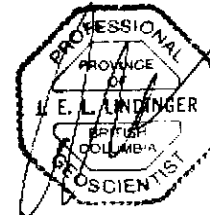
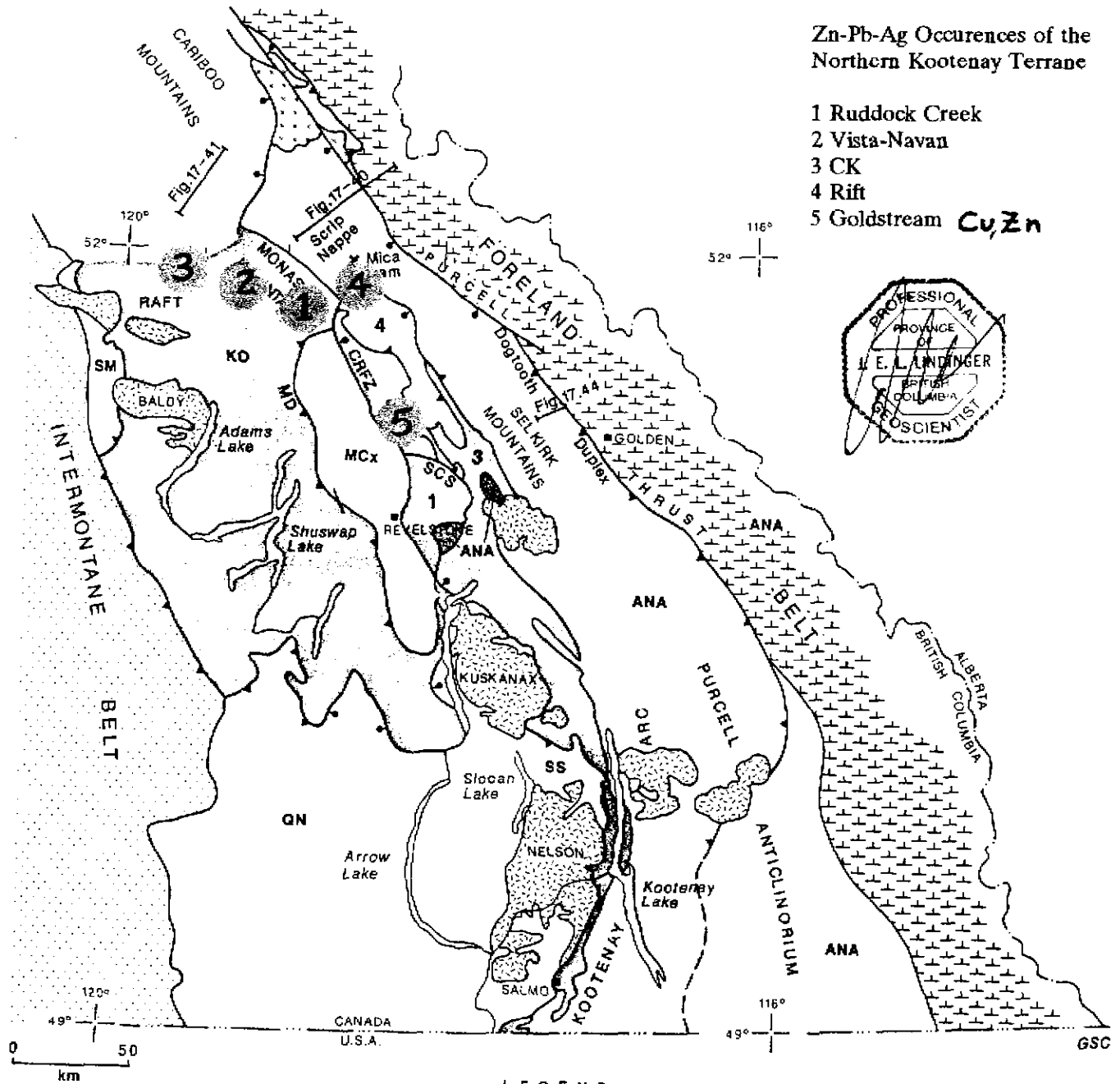
REGIONAL GEOLOGY (Figure 4)

The rocks are thought to be part of the Kootenay Terrane portion of the Omineca Belt. The region is underlain by the Shuswap Metamorphic Complex, which is thought to comprise Upper Proterozoic to early Palaeozoic marine off shore sediments and rare volcanic rocks, derived from the ancestral margin of North America (Wheeler 1992, pp 142-145), and tentatively assigned by the writer to the Horsethief Creek Group (Gibson 1991). The Complex has undergone extensive metamorphism and multiple episodes of deformation, due to collisional orogenic episodes during the Devonian, early Jurassic, mid to late Cretaceous and early to mid Tertiary times. Coincident with these orogenic episodes, intrusive bodies have invaded the rock package. It is assumed that the host lithologies underwent deep burial and deformation until the earliest Tertiary. Significant uplift, and erosion occurred from the mid to late Tertiary. The uplift was accompanied by north trending trans-tensional (basin and range) faulting and emplacement of felsic to intermediate stock and dikes, and recent? basaltic and lamprophyric dykes.

The Shuswap Metamorphic Complex hosts several significant sedimentary hosted zinc-lead-silver massive sulphide occurrences of assumed syngenetic origin, hosted within carbonate bearing lithologies at the transition between platform carbonates and pelitic sediments. The occurrences include Ruddock Creek (5 million tonnes grading 7.5% Zn, 2.5% Pb), Cottonbelt, King Fissure, Big Ledge, CK (1.5 million tonnes grading 8.6% Zn). Clusters of occurrences are generally aligned along north trending large scale folds. The mineralized horizons tend to be laterally extensive but thin. Significant thickness may be present where easterly trending secondary folding occurs. Thickening can occur over short distances (i.e. from 1 to

Zn-Pb-Ag Occurrences of the Northern Kootenay Terrane

- 1 Ruddock Creek
- 2 Vista-Navan
- 3 CK
- 4 Rift
- 5 Goldstream Cu, Zn



LEGEND

Selkirk Allochthon	SS Slokan Synclinorium	SCS Standfast Creek Slide
TERRANES	ANA Ancestral North America	MD Monashee Décollement
KO Kootenay	Mesozoic intrusions	1 Clachnacudainn Slice
QN Quesnellia	Malton Gneiss	2 Goldstream Slice
SM Slide Mountain	CRF2 Columbia River Fault Zone	3 Illecillewaet Slice
MCx Monashee Complex		4 French Creek Slice

Figure 17.30. Southeastern Omineca Belt showing the distribution of terranes, some of the regional structures, and the location of structural cross-sections in Figures 17.40, 17.41 and 17.44.

FIGURE 4 - REGIONAL GEOLOGY

From Wheeler, 1992: Page 608

5m over a distance of 25m – Oliver, 1988). The newly discovered Vista, Navan and Mike discoveries that comprise the Broken Hill-Leo property are situated between Ruddock Creek and CK (with Ruddock Creek 25 km to the east and CK, 25 km to the west) and are tentatively hosted by the same lithologies.

Other deposit types known in the region are epigenetic deposits, commonly related to one or more of the many an intrusive events that occurred in the region. Some of these are high grade gold-bismuth-copper-arsenic veins of unknown but possibly Tertiary age (e.g. Bizar, Readymix), copper, tungsten, molybdenum, zinc-lead silver and gold bearing intrusive and associated skarn and wallrock hosted deposits, metamorphic related gemstone and industrial mineral (ie. garnet) deposits and carbonatite hosted niobium-tantalum occurrences.

PROPERTY GEOLOGY (Figure 5)

The Broken Hill-Leo property is underlain by highly deformed (multi-episodically ductily folded) rocks of the Shuswap Metamorphic Complex portion of the Kootenay Terrane. The metamorphic grade of the Kootenay rocks is upper amphibolite. The sequence is interpreted to consist of three distinct lithological packages that are strongly intruded by pegmatite sills and dykes.

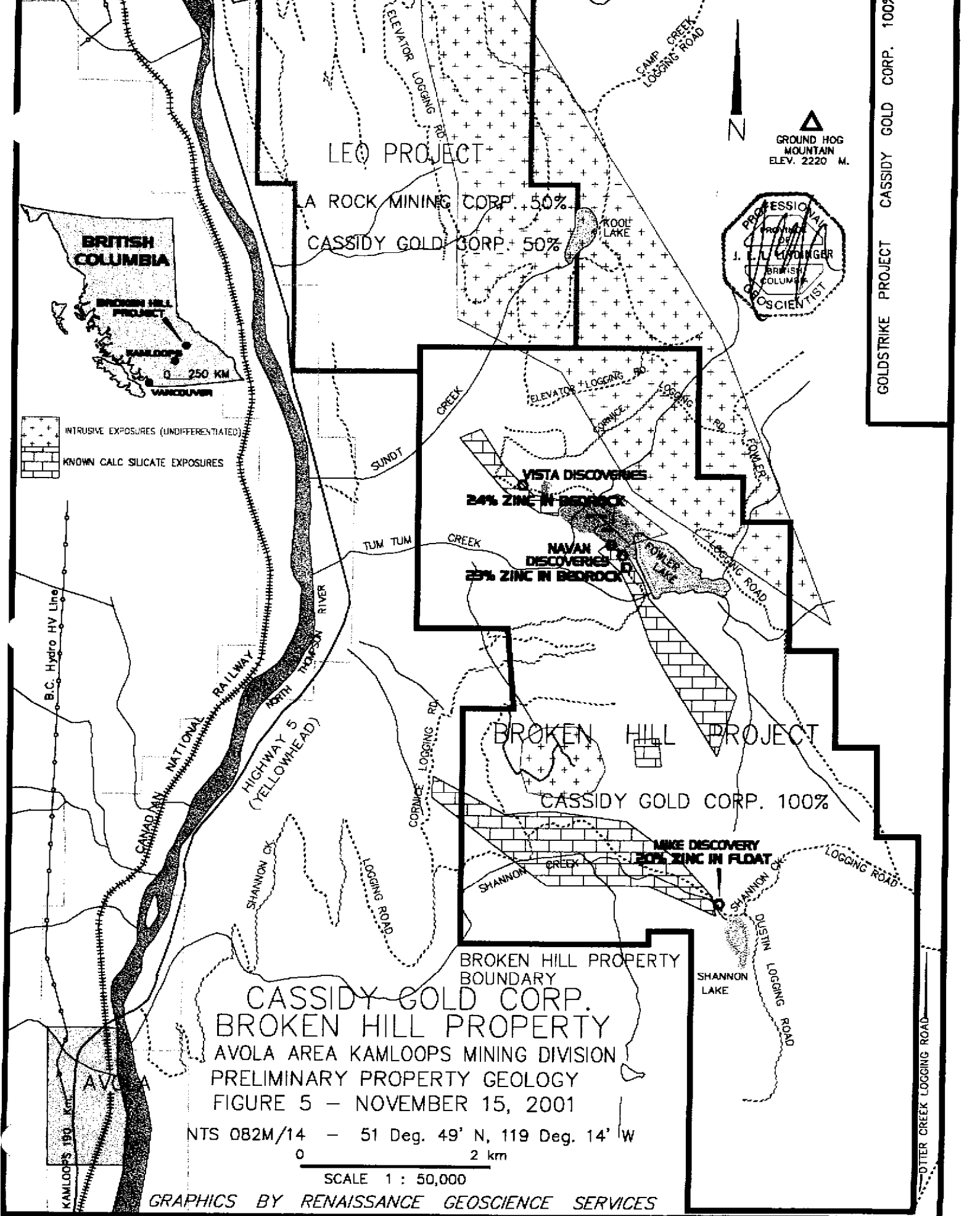
The overall stratigraphic sequence of the property is unknown and has not been mapped. The overall stratigraphy is presently structurally north striking and moderately east dipping. Late stage east plunging parallel folds have gently north and south dipping fold flanks. The general stratigraphy near the mineralized horizons in the Vista and Navan areas is somewhat better known and is described below.

From Lindinger and Pautler 2001, page 6.

“The lowest structural package consists of amphibolite with lesser biotite gneiss and forms a thick monotonous sequence. This is overlain by a sequence dominated by biotite gneiss. The third package consists of calc-silicate rocks with minor marble and chert. This package hosts the known zinc-lead-silver mineralization at the Vista, Navan and Mike Showings, on the property. The Broken Hill-Leo property covers an unexplored 9 km extent of the favourable lithology. In addition the Finn and Pica zinc-lead-silver occurrences lie 8 km and 7 km to the north-northwest of the property, respectively (Evans, 1993).

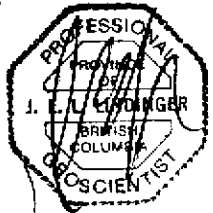
The rocks, although highly folded, have a common north to northwesterly strike with moderate easterly dips. Secondary fold structures observed elsewhere, include late easterly trending roll folds that may reflect larger structures.

Invading the host lithologies is an augen orthogneiss of assumed Devonian Age, which has been observed along the east side of the property. The rocks have been further intruded by weakly deformed to massive leucogranites of late Cretaceous and early Tertiary ages. Accompanying and/or post dating in part, the larger intrusive bodies, are at least two generations of coarse grained leucogranite intrusions, including pegmatite. These occur as tabular to highly irregular cross cutting and concordant pods, dykes and sills. Undeformed mid Tertiary (and later?) intrusions include grey 'dacitic' feldspar porphyry stocks and dykes intrude steeply dipping brittle tensional fractures. Melanocratic lamprophyric dykes also intrude similar structures. (Wheeler 1992, pp. 508, 514, and Lindinger, personal observations).”



LEO PROJECT

AVOLA ROCK MINING CORP. 50%
 CASSIDY GOLD CORP. 50%



GROUND HOG MOUNTAIN
 ELEV. 2220 M.

GOLDSTRIKE PROJECT CASSIDY GOLD CORP. 100%



INTRUSIVE EXPOSURES (UNDIFFERENTIATED)
 KNOWN CALC SILICATE EXPOSURES

VISTA DISCOVERIES
 24% ZINC IN BEDROCK

NAVAN DISCOVERIES
 25% ZINC IN BEDROCK

BROKEN HILL PROJECT
 CASSIDY GOLD CORP. 100%

MIKE DISCOVERY
 20% ZINC IN FLOAT

CASSIDY GOLD CORP.
BROKEN HILL PROPERTY
 AVOLA AREA KAMLOOPS MINING DIVISION
 PRELIMINARY PROPERTY GEOLOGY
 FIGURE 5 - NOVEMBER 15, 2001

NTS 082M/14 - 51 Deg. 49' N, 119 Deg. 14' W
 0 2 km

SCALE 1 : 50,000

GRAPHICS BY RENAISSANCE GEOSCIENCE SERVICES

The following descriptions of the VISTA, NAVAN and MIKE showings are part of the original information sent for Minfile description by the writer. Additional information is in italics.

"VISTA SHOWING - Location: UTM zone 11 5745390 N 344370 E, 1415 m. el., Lat. 51° 50' 15" N, 119° 15' 31"W.. About 1 km northwest of Fowler Lake. and 10 km NNE of Avola.

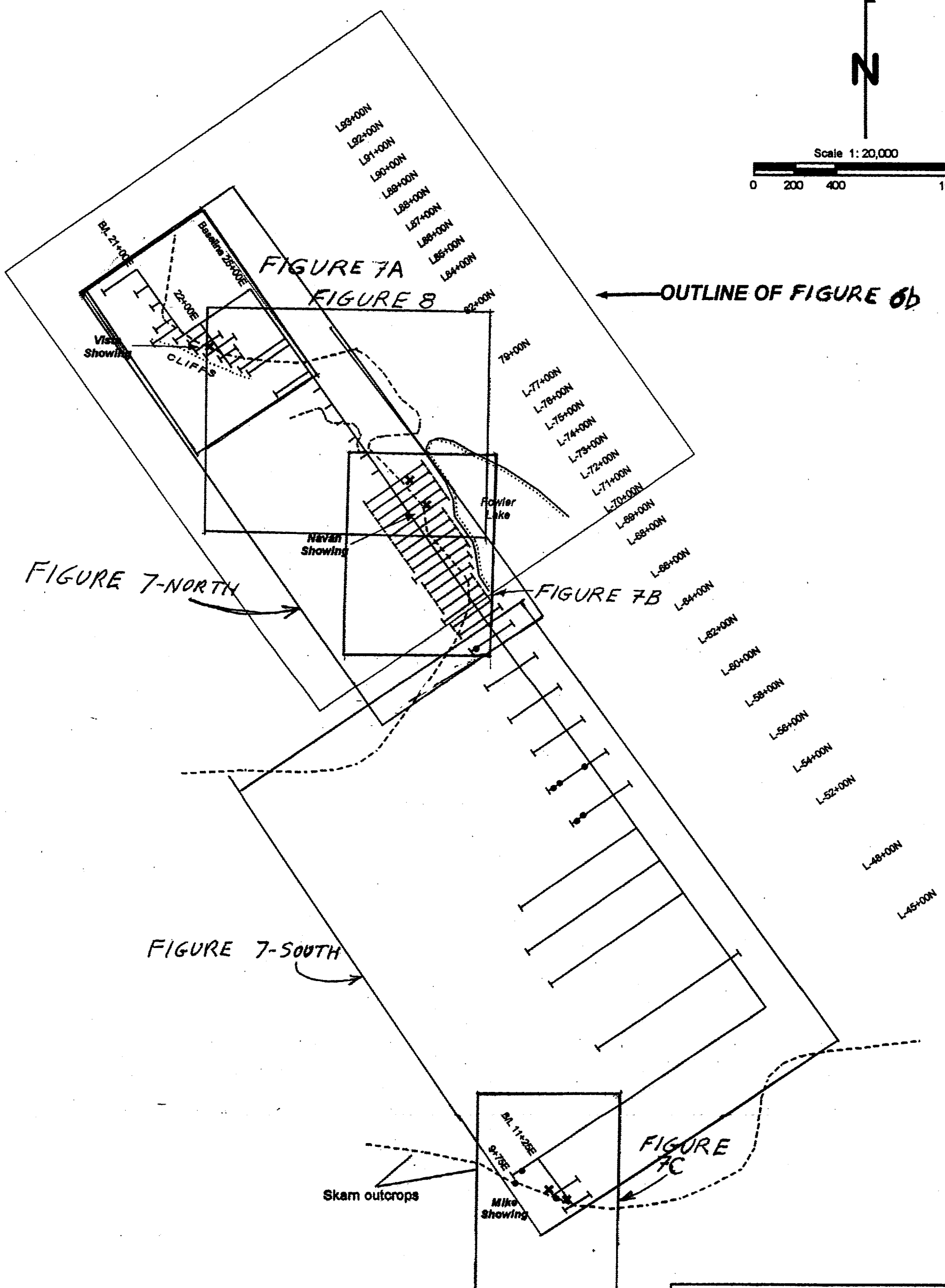
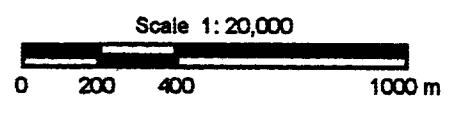
The Vista "I" showing is a partially exposed band of very dark brown fine to medium grained massive sphalerite with subordinate galena, pyrrhotite, chalcopyrite and pyrite?. The band was exposed by blasting to establish a road surface for the Cornice Logging road at about Km 9.3. The band is at the contact of sulphidic siliceous gneisses on the structural footwall, and an overlying 2+ meter thick band of calc-silicate rocks that appear to be highly metamorphosed limestone. The showing appears to be part of a moderately (10-20 degrees) south-east plunging partially eroded antiform or northeast dipping monocline. Rocks to the northeast change dip to moderate to steep northeast dips. Exposures to the south-west are eroded off, and covered by glacial debris, or have not been mapped.

The observed mineralization is in the form of planar to swirling bands of nearly 100% sulphides up to 35 cm thick that grade upward into the calc-silicate host rocks into less intense massive and semi massive sulphides bands. The contact with the underlying silicate rock appears very sharp. The band of Vista "A" type mineralization is discontinuously exposed over about 20 meters, and is assumed to be continuous except for the following. It is truncated at surface to the northwest by a northwest striking moderately northeast dipping fault that brings a pegmatite dyke into direct contact with the mineralization. It plunges below the logging road to the south-east. High grade representative grabs from bedrock exposures report up to 24% zinc, 4.9% lead and 72 g/t silver.

Vista "II" type mineralization occurs 2 to 3 meters structurally above the Vista "A" horizon and is hosted by and contained within the calc-silicate rocks. This zone is also stratiform and is as exposed, a 5 to 10 cm thick band of dark brown coarse grained massive to semi-massive sphalerite. Not even trace amounts of lead, silver and copper are reported. This band is exposed in its unweathered form for at least 5 meters about 20 meters south-east of the Vista "A" discovery outcrop. To the northwest it is eroded off. To the south-east it also plunges below the road. To the northeast, if continuous it would dip to the northeast as part of the stratigraphic package.

Vista "III" type mineralization (discovered by M. Warner Gruenwald, P.Geo.) are fault? hosted 4 to 6 cm thick silvery-grey medium to fine grained massive to semi-massive sphalerite and galena bands that appear to both occupy the top of and crosscut the calc-silicate horizon hosting the Vista "A" and "B" mineralization. Weathered exposures are visible over a planar 8 by 2.5 meter exposure of the top of the calc silicate horizon above the fresh exposures of the Vista "B" mineral band. A sample (0.8 m. long by 8 cm thick) taken by Mr. Gruenwald returned 6.6% zinc, 4.1% lead and 6.2 g/t silver.

The calc silicate unit hosting the various types of zinc rich sulphide mineralization appears to contain erratically generally weakly disseminated sphalerite with probably subsidiary argentiferous galena. Traces of other iron and copper bearing sulphides are also present....



- LEGEND**
- Logging Road
 - Grid Line
 - * Mineral Occurrence
 - Calc-silicate/skam float

MAP BASE FROM GRUENWALD 2000

CASSIDY GOLD CORP INC.	
INDEX MAP	
GRID OUTLINE	
2000	
BROKEN HILL PROPERTY	
FIGURE 6a	
<small>Kamloops Mining Division, B.C.</small>	
<small>Geoquest Consulting Ltd.</small>	<small>Date: November, 200</small>
<small>Drawn by: EG</small>	<small>Figure:</small>

NAVAN SHOWINGS - Location (Navan A): UTM zone 11 5744500 N 344500 E, 1385 m. el.. Lat. 51° 49' 49" N, 119° 14' 32"W.. About 10 km NE of Avola, 0.2 km west of Fowler Lake at 7.4 km point on the Cornice Logging road.

The Navan "1" showing is a partially weathered poorly exposed band of dark brown fine grained massive sulphides hosted by disrupted (frost heaved?) calc-silicate rocks. The grade and style of mineralization are very similar to the Vista "A" type with the following difference, the highest grade exposures are totally within calc-silicate (meta-carbonate) host rocks. *Disrupted lenses of massive zinc sulphides over 15 cm thick are found in the disrupted bedrock forming the cut that hosts the showing. However boulders of massive sulphide mineralization up to 30 cm in diameter grading up to 23% zinc, 4.05% lead and 17 g/t silver. occur as float that was dug out of the subcrop exposures hosting the sulphides by the road construction crew. The package hosting the mineralization appears to be part of a moderately south-east plunging antiform. A 25 cm thick second layer of semi massive sulphides occurs less than 1 meter above the massive sulphide horizon. Still higher are disseminated medium grained sulphides in highly weathered pitted garnetiferous cal-silicate rock.*

The Navan "2" showing is about 130 meters north of the Navan "1" exposure. Here a small 1.5 meter long 5 to 10 cm band thick of massive sphalerite that is hosted by westerly dipping silicate rocks is found. No real bedrock exposures can be seen here and the rocks hosting the sulphides may be a large rotated sub crop boulder. A 0.3 meter thick sample taken by Mr. Warner Gruenwald P. Geo. of Geoquest Consulting Ltd. including the massive sulphide mineralization returned 5.6% zinc, 0.6% lead and 8.4 g/t silver. *The host rocks are very different from the NAVAN "A" mineralization and probably represent a separate layer not seen at the NAVAN "A" showing.*

The Navan "3" float showing is a 30 cm diameter piece of siliceous calc silicate and biotite gneiss float occurring in basal till that has on one side part of a massive sulphide layer. The remnant sulphide layer was about 12 cm thick. Based on glacial information the source of the boulder was to the northeast and away from the NAVAN "A", and NAVAN "B" showings.

The NAVAN "4" float showing occurs 300 meters south of the NAVAN "1" showing. Here small (less than 10 cm diameter) fragments of zinc bearing semi-massive sulphides hosted by calc-silicate and chert occur in a basal till and subcrop road cut. This is the area of the original rock sample taken by the writer in July 2000 that returned nearly 1% zinc with anomalous copper, lead silver and tungsten values.

An open ended to the north soil anomaly immediately north (up ice) and west (down hill of the Navan "2" and "3" showings that contains the highest zinc (2590 ppm) and lead (412 ppm) values in soil found to date.

MIKE FLOAT SHOWING - Location: UTM zone 11 5740800 N 346400 E, 1610 m. el.. Lat. 51° 47' 49" N, 119° 13' 39"W.. About 0.5 km northwest of Shannon Lake, 4.0 km SSE of the Navan showings at Km 15.2 on the Shannon Ck Logging road. (Figure 5, 6, 7c)

The Mike Float showing contain cobbles and boulders of dark brown massive, semi massive and disseminated fine to coarse grained sphalerite and pyrrhotite associated with

gametiferous calc-silicate, pyrrhotitic silicate and coarse grained pegmatitic rocks that are exposed over 225 meters in a series of pits *and scrapings* dug for material to upgrade the Shannon Ck. logging road. The *semi massive and massive sulphide* boulders and cobbles can be dug out of the cut bank and occur within discreet stratigraphic zones near to and overlying possibly glacially disrupted pegmatitic bedrock. Northwest of the float occurrence is an area of calc silicate float and bedrock extending for over 2 km. To the south-east is glacial till extending to Shannon Lake. One *select sulphide* sample taken by Gruenwald from a *40 cm boulder with 20 cm of massive sphalerite on one side* returned 19.6 % zinc, and 352 ppm cadmium. The lead content of this and other samples have consistently lower lead values than the Vista and Navan areas. However a soil sample site approximately 100 meters north of the float area returned the second highest lead (350 ppm) (with accompanying high zinc (270 ppm) along with weakly anomalous chrome and nickel) of all the samples taken on the Vista, Navan and Mike areas. This may have significant implications in the Mike area as the geochemical signatures of the sampled mineralized rocks in the road exposures when compared with the preliminary soil results 100 to 300 meters to the north (up ice) are quite different.”

2000-2001 WORK PROGRAMS

SOIL GEOCHEMISTRY (Figures 7a, 7b, 7c)

In early October 2000, a 6 kilometer long brushed, compassed, slope corrected and tight chained baseline oriented at 325 degrees was established to provide field survey control over the areas surrounding and in between the Vista, Navan and Mike showings. In the Vista area to the north and the Mike area at the south end orthogonal tie lines and additional baselines were established to cover the most prospective exploration areas. From these base lines variably spaced (50, 100 and 200 meters) orthogonal grid lines were established in conjunction with soil sampling.

The soil survey on the grid lines were taken at 25 meter stations. Due to the late season the sampled survey lines were completed to only cover the most prospective areas. 479 soil samples and 30 rock samples were sent to ALS-Chemex Laboratories Ltd. in Vancouver, B.C. and analyzed for Al, Ba, Be, Bi, Cd, Ca, Cr, Co, Cu, Fe, K, Pb, Mg, Mn, Mo, Na, Ni, P, Ag, Sr, Ti, W, V and Zn using a 24 element 'total digestion' ICP package which involves a hot Aqua regia plus hydrofluoric acid digestion. This process was used to enable more accurate analyses of barium (Ba) and tungsten (W). Rock samples returning overlimits in any specific element(s) had that/those element(s) assayed with procedures specified to provide an accurate quantity of the element(s) in that sample.

Although most of the area around the Vista and Navan showings received adequate coverage, some of the southern areas around the Mike showing were not completed to a heavy early snowfall.

ROCK GEOCHEMISTRY (Figure 6b, Appendix II)

30 selected rock samples were taken by W. Gruenwald, P.Geo. as part of an examination of the showings and intervening lithologies. The samples were taken from exposures created by the cornice logging road construction crew which cut through the Vista-Navan horizon in several places.

GRAVITY SURVEY (Appendix III)

A gravity survey was completed over grid lines 7650N to 8600N in December, 2000 by Woods Geophysical Consulting Inc.. The coverage was about 500 meters for each line. The lines ended at steep terrain or the shore of Fowler Lake. The program was terminated early before covering the Vista or Navan showings due to heavy snowfall. In order to facilitate the gravity surveyors the pre-existing lines to be surveyed were brushed out and the stations were improved. Lines were also added or extended where the soil survey coverage stopped.

Several diamond drill holes were drilled base on the results of the gravity survey. The details are discussed in the following section.

DIAMOND DRILLING (Figure 8, Table 1)

The following descriptions are from (Lindinger and Pautler 2001)

“Drilling was carried out between January 27 and February 3, 2001 by LDS Diamond Drilling of Kamloops, B.C., using a skid mounted Longyear 38 core drill with NQ wireline tools. A total of 930.1m of diamond drilling in 13 holes was completed. The drill holes tested the most promising gravity anomalies delineated by the geophysical survey. Several holes tested the down dip extent of known mineralization at the Vista and Navan Showings.

A total of 51 samples of core were split and sent to Eco-Tech Labs, Kamloops, B.C. and analyzed for and analyzed for Al, Sb, As, Ba, Bi, Cd, Ca, Cr, Co, Cu, Fe, La, Pb, Mg, Mn, Hg, Mo, Na, Ni, P, Ag, Sr, Ti, Sn, W, U, V and Zn using a 32 element ICP package which involves a nitric-aqua regia digestion. Most of the samples were also analyzed for gold, which was completed by fire assay with an atomic absorption finish. Anomalous samples were assayed for zinc and lead. Select samples were analyzed for the presence of rare earth elements. The rare earth analyses, including tantalum were forwarded to Activation Labs in Ontario to be analyzed by neutron activation procedures. Laboratory procedures and results are outlined in Appendix IV.

All pertinent drill data is summarized in Table 1 and drill hole locations are shown on Figure 8. Drill logs are included in Appendix V. Sample locations and significant results are plotted on the cross sections (Figures 9A-G. Descriptions of the lithologies encountered, with an accompanying legend, is provided in Table 2. The core is stored on the property at approximately L9025N/2075E. Core recovery averaged 99%.”

RESULTS

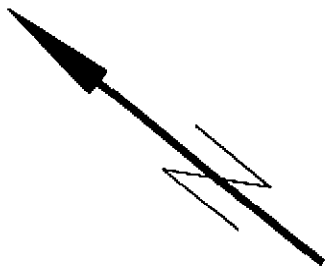
Soil Sampling (Figures 7a, 7b, 7c, Appendix I)

Briefly most of the significant soil anomalies to date on the Broken Hill-Leo property at least spatially coincide with known massive sulphide outcrop and float occurrences. A limited soil anomaly south of the VISTA Occurrence suggests that the anomaly is derived from at least in part from the mineralized outcrop. The partially defined anomaly on line 84+00 N is interpreted to be sourced from extensions of the mineralized horizon east of the VISTA Occurrence. The strong open ended to the north, zinc-lead-silver anomaly north of and up ice of the NAVAN 1 showing strongly suggests a significant unknown metal source north of this anomaly exists. Similarly the strength of the partially defined zinc and lead soil

BL25+00E

CORNICE LOGGING ROAD

ppm Pb 70
ppm Zn 730
634



VISTA
SHOWING

L93+00N

L92+00N

L91+00N

L90+00N

L89+50N

106

156

126

328

584

1090

380

282

106

L86+00N

432

L85+00N

L84+00N

118
110
20+00E
19+00E

108

102

168

168

TL89+00N

128

BL21+00E

L88+50N

L88+00N

L87+50N

L87+00N

L86+50N

L86+00N

L85+50N

180

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194

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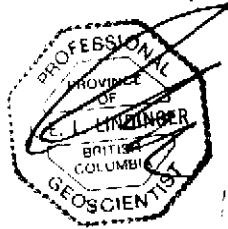
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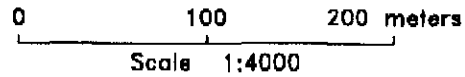
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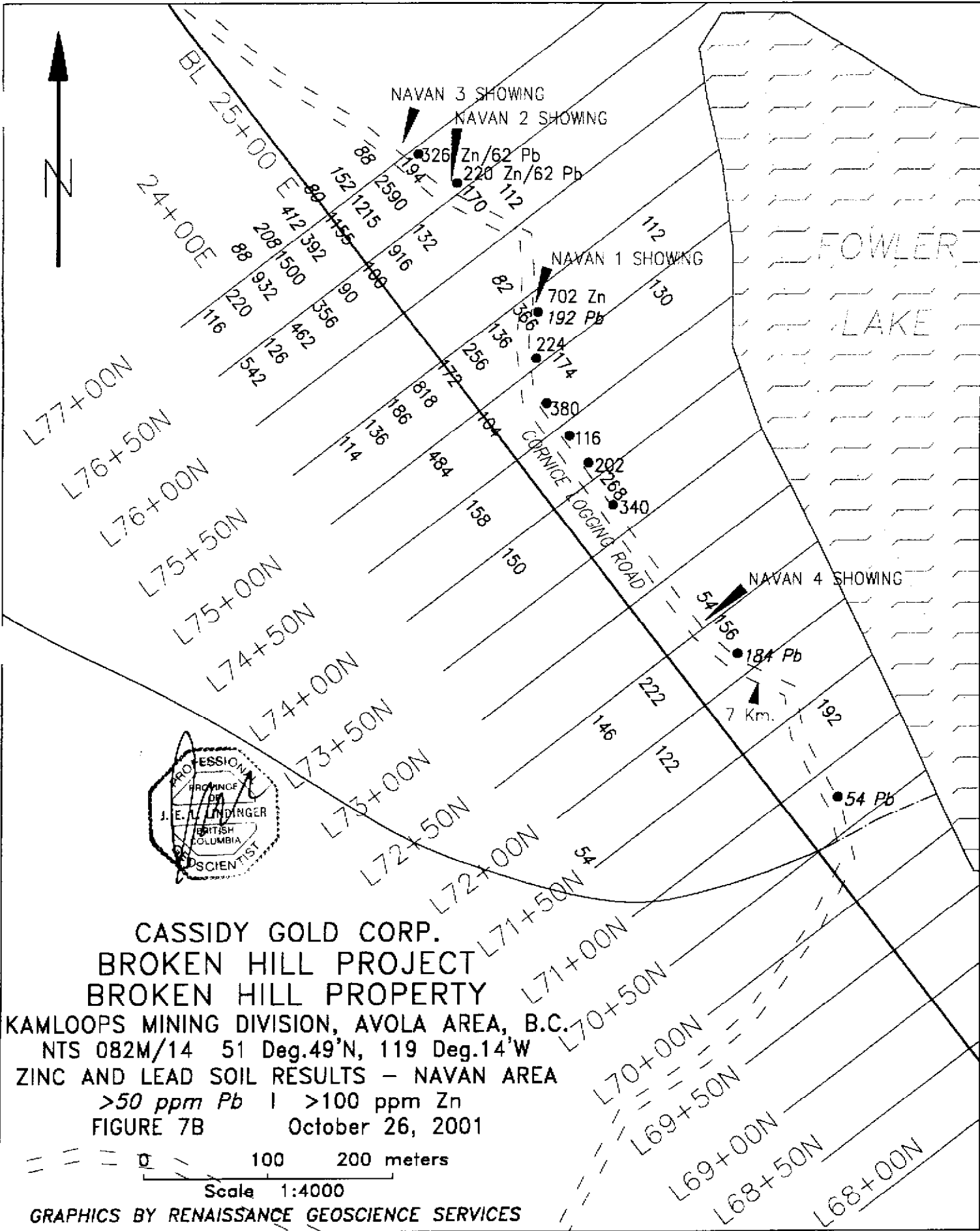
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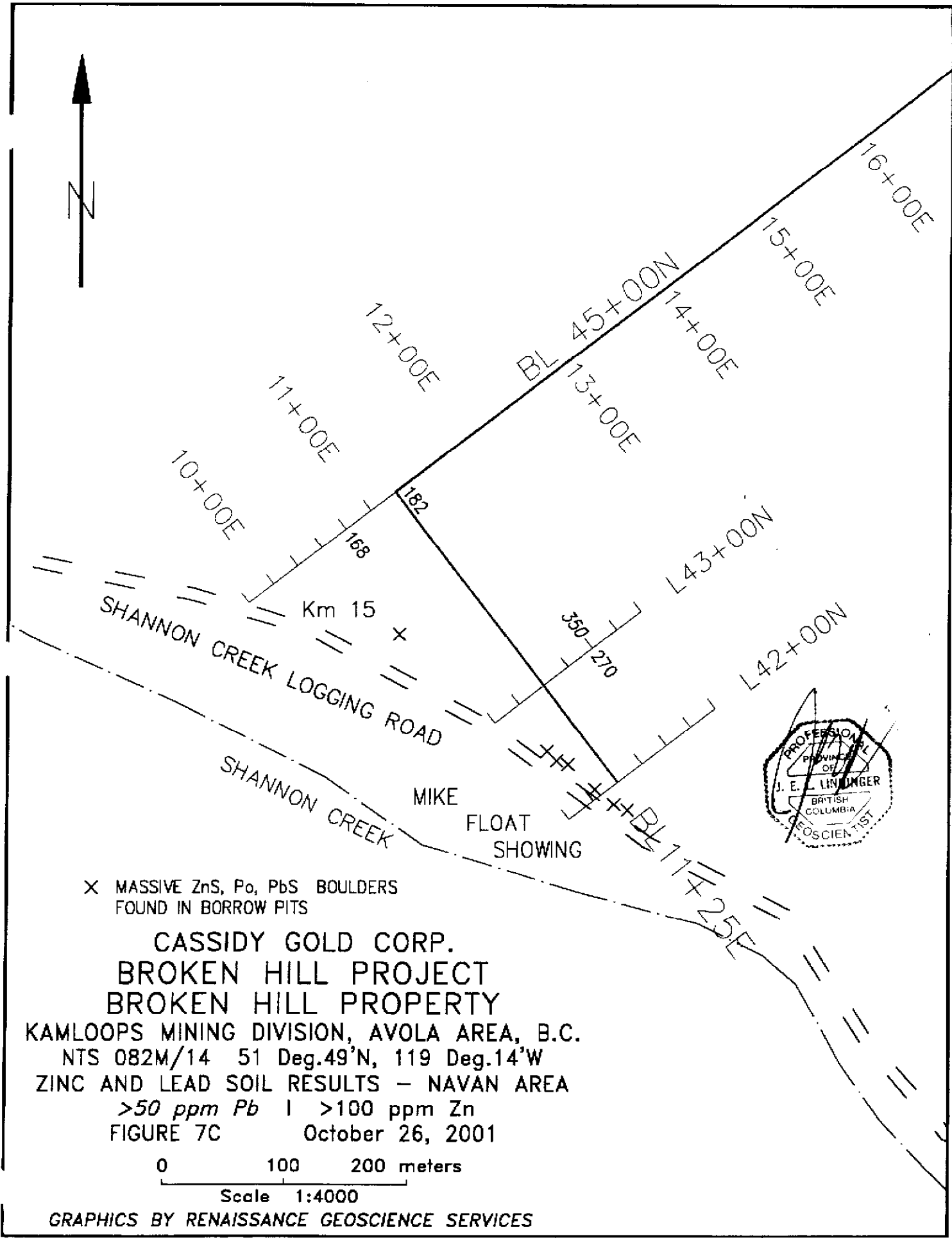


CASSIDY GOLD CORP.
BROKEN HILL PROJECT
BROKEN HILL PROPERTY
KAMLOOPS MINING DIVISION, AVOLA AREA, B.C.
NTS 082M/14 51 Deg.49'N, 119 Deg.14'W
ZINC AND LEAD SOIL RESULTS - VISTA AREA
>50 ppm Pb | > 100 ppm Zn
FIGURE 7A October 25, 2001



GRAPHICS BY RENAISSANCE GEOSCIENCE SERVICES





X MASSIVE ZnS, Po, PbS BOULDERS
FOUND IN BORROW PITS

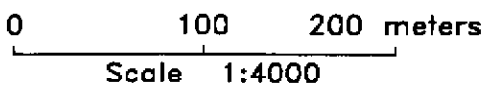
**CASSIDY GOLD CORP.
BROKEN HILL PROJECT
BROKEN HILL PROPERTY**

KAMLOOPS MINING DIVISION, AVOLA AREA, B.C.

NTS 082M/14 51 Deg.49'N, 119 Deg.14'W

ZINC AND LEAD SOIL RESULTS - NAVAN AREA

>50 ppm Pb | >100 ppm Zn
FIGURE 7C October 26, 2001



GRAPHICS BY RENAISSANCE GEOSCIENCE SERVICES

anomaly north of (up ice and uphill) of the MIKE Float occurrence strongly suggests that a significant base metal source may occur a short distance north of the showings.

Rock Sampling (Figure 6b, Appendix I, Appendix II)

The rock sampling was completed by W. Gruenwald, P. Geo. and was essentially confined to samples of mineralized rock exposed in the road cut of the Cornice Logging road. Briefly Mineralized outcrop, subcrop and float samples from the Vista, Navan, and Mike returned 16%, 21.5% and 19.6% zinc respectively with up to 4% lead and 11 g/t silver. The Vista and Navan mineralization was also distinctly anomalous in barium, bismuth, cadmium, copper and nickel. The samples from the Mike area were notable in their lack of silver, bismuth and lead mineralization.

Gravity Survey (Appendix III)

The gravity survey, as mentioned previously did not extend to cover either the Vista or Navan showings. However the following information was derived from the survey results. The results in this section are also discussed with the results of the drilling known. The surveyed area can grossly be divided into two areas. Please refer to COMPLETE BOUGUER GRAVITY plan in Appendix III. The area grid south of line 8250 north has a distinctively lower density than north of and including line 8250 N. Based on the drilling to date the low density area coincides with an interpreted felsic intrusive body that underlies the flat area northwest of Fowler Lake. The abrupt linear density change at line 8200 N probably coincides with a intrusive contact. Whether the contact is fault controlled or not is unknown, although the gravity anomaly does coincide with Ground Hog Creek which may reflect the surface expression of a fault. The denser material north of 8200N is interpreted to comprise a mixture of carbonate rich (relatively dense) Shuswap metamorphic rocks intermixed with pegmatitic bodies. The localized higher density anomalies in both areas can tentatively be interpreted to be derived from local topographic features. For example most one point density anomalies coincide with mounds (density low) and pits (density high) rather than any underlying rock difference. The density anomaly along the west end of line 8350 N coincides with the base of a steep line parallel slope, that flattens out along the line AND a thick carbonate amphibolite package that underlies the line. One interpretation is that the favourable horizon hosting the zinc mineralization outcrops a short distance north of the line. The effect of this dense material in the survey is unknown. The west 100 meters of line 8400 N coincides with the base of a large pegmatitic sill or dyke. Additional information correlating gravity information with drilling results are discussed with respect to the individual drill holes results in the next section.

Diamond Drilling (Figure 9, Appendix IV, Appendix V)

A brief description of the results each of the drill holes follows as discussed in Lindinger and Pautler 2001: TW denotes true width. Italics are additional comments made by Lindinger this report.

BH DDH 01-1 (Figure 9A)

DDH 01-1 was drilled to test the down dip extent of mineralization exposed at the Vista Showing and is 93m at 110° from the Showing. The Vista Showing reportedly contains Zn values up to 15.95% over 0.3m (Gruenwald, 2000). The hole also tested a soil anomaly that contains up to 1090 ppm Zn and 92 ppm Pb.

Approximately 60% of DDH 01-1 consists of pegmatite sills. Apart from the sills, a thick sequence of calc-silicate to diopside-garnet-actinolite skarn with minor biotite gneiss was intersected in the top half of the hole to 40m. A grey banded marble that may be useful as a marker horizon and a cherty unit, possibly representing an exhalite, were intersected

between 26.8 and 32.3m. The bottom half of the hole was dominated by the amphibolite gneiss which was intersected at 49.1m. A high angle, probable westerly dipping fault was intersected at the base of the calc-silicate unit within the pegmatite.

Although no significant mineralization was intersected, a thick sequence of the favourable calc-silicate unit was encountered that contains a possible cherty exhalite. The mineralized horizon in this hole *may not exist*, may have been engulfed by the pegmatite, proximal to the chert unit, *or due to the flat stratigraphy may have been missed by collaring the hole.*

BH DDH 01-2 (Figure 9A)

DDH 01-2 was drilled to test a gravity anomaly along trend and down dip of mineralization exposed at the Vista Showing and is 285m bearing 108° from the Vista Showing. *A northerly trending depression between holes 01 AND 02 may represent the surface expression of a fault.*

The hole intersected a thick sequence of the calc-silicate unit, grading to coarser grained skarn, with minor biotite gneiss. The grey banded marble unit was intersected between 23.8 and 31.3m, at a similar depth to the intersection in DDH 01-1. The lower elevation of DDH 01-2 accounts for the fact that the hole is further down dip from the marble intersection in DDH 01-1. The amphibolite unit, with minor calc-silicate beds, was encountered below 55m. Pegmatite sills make up 30% of the hole.

No significant mineralization was intersected. However, a thick sequence of calc-silicate to skarn and the marble marker horizon were encountered. The near surface effect and thickness of the calc-silicate to skarn unit may be responsible for the weak gravity anomaly.

BH DDH 01-3(Figure 9-B)

DDH 01-3 was drilled to test a gravity anomaly along trend and down dip of mineralization exposed at the Vista Showing and is 460 m. bearing 100° from the Vista Showing.

Biotite gneiss with minor beds of calc-silicate was intersected down to 37.5m. A white marble horizon occurs with calc-silicate to skarn within the biotite gneiss package between 32.2 and 33.8m. A Tertiary mafic dyke cuts the biotite gneiss package at 37.5 to 42.1m with an apparent dip of 45° (SW). Two similar zones of calc-silicate to marble were intersected between 47.2m and 59.2m and from 99.3m to 109.2m. The amphibolite package, dominated by amphibolite gneiss with some biotite gneiss zones, was intersected at 109.2m to the end of the hole at 139.3m. Pegmatite sills constitute 50% of the hole with a large interval from 59.2m to 99.1m.

A high angle, westerly dipping fault, was intersected at 59.2 to 67.9m. Approximately 40m of reverse movement along the fault (northeast side down) could explain the repetition of the calc-silicate to marble units. With restoration along the reverse fault the lower pegmatite sill would correspond to a pegmatite dominant zone between 17.1 and 47.2m. The amphibolite contact would then be at 59.2m. Local quartzite intervals were encountered proximal to the fault and may reflect silicification related to the structure as opposed to primary lithology.

Sphalerite mineralization was encountered as bands up to 5cm wide and disseminations in quartz-calcite-diopside-actinolite-garnet skarn at 25.9 to 26.5m and at 26.9m. The banding in the skarn and sphalerite bands is at 70° to the core axis. The mineralized zone is dissected by pegmatite sills, reducing the grade and overall width.

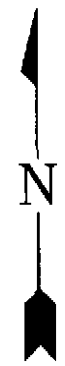
TABLE 1: DIAMOND DRILL HOLE DATA

Hole No.	Grid Location	Elev.	Az.	Dip	Total Length	Began d/m/y	Finished d/m/y	Sample Numbers
BH DDH 01-1	87+00N/22+35E	1421 m		-90°	78.3m	27/1/01	27/1/01	131865-75,900
BH DDH 01-2	85+50N/23+50E	1410 m		-90°	84.4 m	27/1/01	28/1/01	131876-77,82
BH DDH 01-3	84+55N/25+00E	1397 m		-90°	139.3 m	28/1/01	29/1/01	131855-64
BH DDH 01-4	84+00N/26+70E	1375 m		-90°	57.0 m	29/1/01	29/1/01	
BH DDH 01-5	78+70N/26+00E	1354 m		-90°	81.4 m	29/1/01	30/1/01	131884-87
BH DDH 01-6	74+85N/26+25E	1342 m	295°	-60°	99.7 m	30/1/01	31/1/01	318179-81,83
BH DDH 01-7	77+00N/26+25E	1348 m	235°	-60°	38.7 m	31/1/01	31/1/01	131888-89
BH DDH 01-8	77+20N/25+65E	1345 m	235°	-60°	99.7 m	31/1/01	1/2/01	131890-94
BH DDH 01-9	83+50N/25+50E	1353 m	235°	-50°	93.6 m	1/2/01	2/2/01	131895-99
BH DDH 01-10	83+50N/25+50E	1353 m		-90°	29.6 m	2/2/01	2/2/01	
BH DDH 01-11	83+50N/24+91E	1345 m	230°	-70°	41.8 m	2/2/01	2/2/01	
BH DDH 01-12	84+90N/24+50E	1406 m		-90°	44.8 m	3/2/01	3/2/01	
BH DDH 01-13	84+90N/24+50E	1406 m	055°	-45°	41.8 m	3/2/01	3/2/01	131301-06
TOTALS:					930.1 m			51 Samples

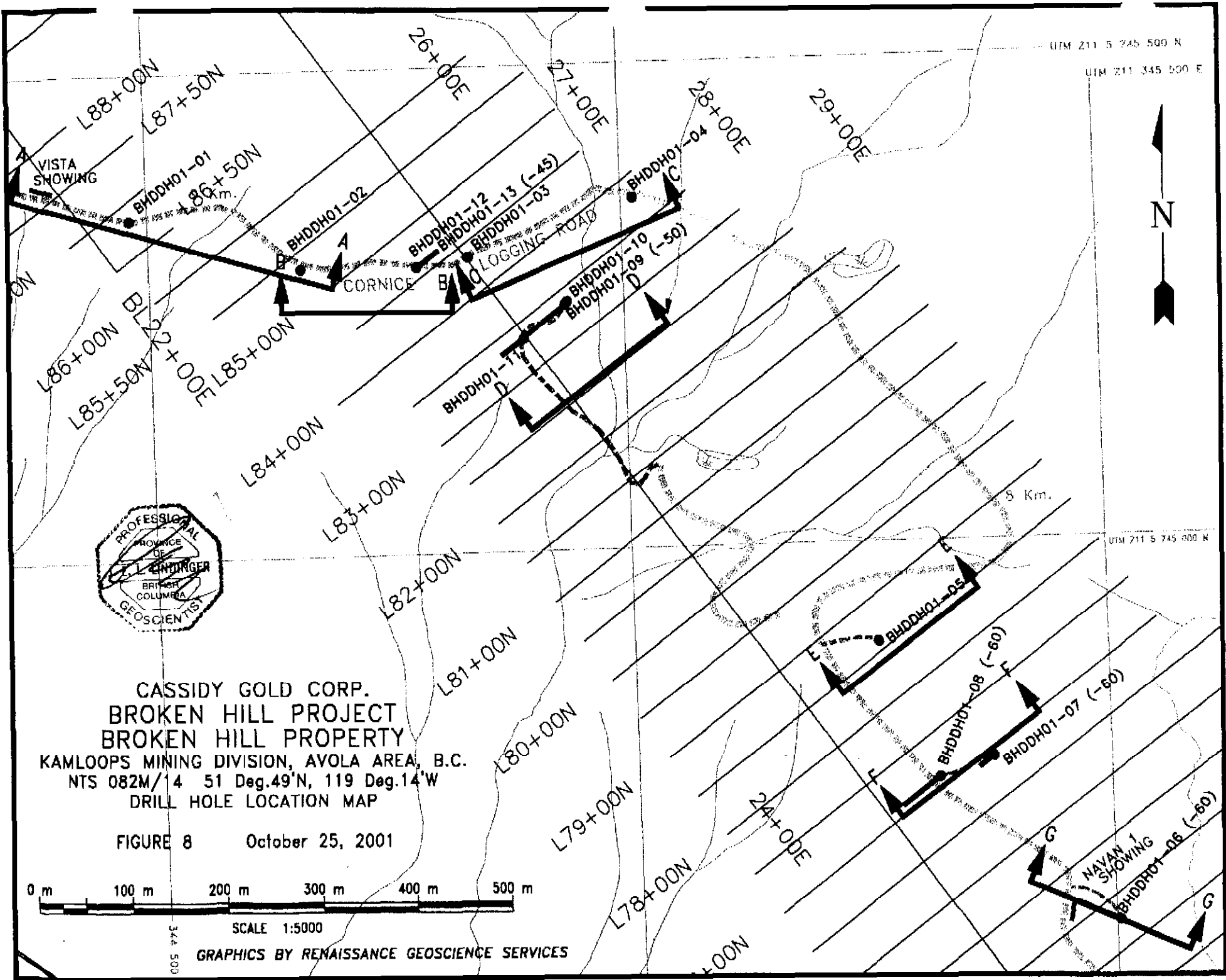


UTM 211 5 745 500 N

UTM 211 345 500 E



UTM 211 5 745 000 N



CASSIDY GOLD CORP.
BROKEN HILL PROJECT
BROKEN HILL PROPERTY
KAMLOOPS MINING DIVISION, AVOLA AREA, B.C.
NTS 082M/4 51 Deg.49'N, 119 Deg.14'W
DRILL HOLE LOCATION MAP

FIGURE 8 October 25, 2001



SCALE 1:5000
GRAPHICS BY RENAISSANCE GEOSCIENCE SERVICES

SIGNIFICANT INTERSECTIONS

FROM (m)	TO	% Zn	ppm Zn
25.9	26.5	1.69	
26.5	26.9		476
26.9	27.0	1.58	

Weighted average from 25.9 to 27.0m is 1.22% Zn over 1.1m.

BH DDH 01-4:(Figure 9-B)

BH DDH 01-4 was drilled to test a gravity anomaly along trend and down dip of mineralization exposed at the Vista Showing and is 625m at 093° from the Vista Showing. A Tertiary mafic dyke with an apparent dip of 45° to the southwest was intersected in the top of the hole from 4.3 to 7.9m and appears to correlate with the mafic dyke intersected in DDH 01-3. The dyke is cut by a high angle, westerly dipping fault that may be correlative with the possible reverse fault intersected in DDH 01-3. The top half of the hole primarily consists of the biotite gneiss unit, down to 30m. Amphibolite gneiss is more dominant below 30m. The contact between the two units is gradational. Core axes of the foliations within the gneisses average 65°, resulting in an apparent dip of 25°E. Pegmatite sills are less prevalent, making up only 20-25% of the hole.

No significant mineralization was intersected. A mafic dyke was intersected in the top of the hole and no significant intervals of calc-silicate were encountered. The near surface effect of the dyke (and the limited amount of pegmatite) may explain the weak gravity anomaly.

BH DDH 01-5:(Figure 9E)

DDH 01-5 was drilled to test a gravity anomaly between and along trend of mineralization exposed at the Vista and Navan Showings.

Pegmatite sills constitute approximately 75% of DDH 01-5. Biotite gneiss with minor calc-silicate occurs between 11.1 and 31.3m. Some intervals of biotite gneiss were evident within the pegmatite down to 48.6m. At 76.3m amphibolite gneiss is more dominant. Core axes of the foliations within the gneiss units average 65°, resulting in an apparent dip of 25°E. A steep, possibly westerly dipping fault was intersected at 14 and 21m.

No significant mineralization was intersected. Extensive pegmatite was encountered and calc-silicate was intersected near the top of the hole. The gravity anomaly may be related to the density contrast between the pegmatite, the near surface effect of the calc-silicate and/or local topographic variations.

BH DDH 01-6:(Figure 9G)

DDH 01-6 was drilled to test the Navan Showing approximately 25m down dip from the surface showing that reportedly grades up to 21.5% Zn, 3.8% Pb and 11 g/t Ag from grab samples (Gruenwald, 2000). The hole also tested the down dip extent of a soil geochemical anomaly that contains up to 818 ppm Zn and 82 ppm Pb.

A Tertiary *intermediate*-mafic dyke was encountered in the top of the hole from 7.6 to 10.8m, cutting the pegmatite. It appears to correlate with the dyke observed in DDH 01-3 and -4. The biotite gneiss unit, with significant calc-silicate horizons, was intersected between 23.7 and 66.0m. The banded grey marble marker unit, which appears to be

TABLE 2

GEOLOGICAL LEGEND - BROKEN HILL PROJECT

to accompany Figure 9

TERTIARY

TDIKE - Grey fine to medium grained intermediate intrusive rock. Fine to medium grained hornblende and feldspars in a grey aphanitic groundmass. (Pautler unit 6)

CRETACEOUS AND/OR TERTIARY

PEG. - Pegmatite sills and dykes. Leucocratic medium but usually coarse grained quartz-plagioclase biotite or muscovite intrusive. Often 'contaminated' with partially assimilated wall rocks. (Pautler unit 5)

GRANO - Leucocratic fine grained granodioritic intrusive. (Pautler unit 4)

PROTEROZOIC to PALAEOZOIC: KOOTENAY TERRANE

(Shuswap Metamorphic Complex)

DEVONIAN?

ORTHGN - Feldspar augen orthogneiss ranges from dioritic to quartz dioritic. (not seen in drill core).

PROTEROZOIC? - HORSETHIEF CREEK GROUP?

BIOGN - Metapelitic medium grained usually siliceous biotite gneiss. (Pautler unit 2)

CALC-SIL - red-pink to green usually coarse grained, coarsely banded garnet-amphibole-quartz clac silicate and skarn with remnant calcite rich pods. (Pautler unit 3)

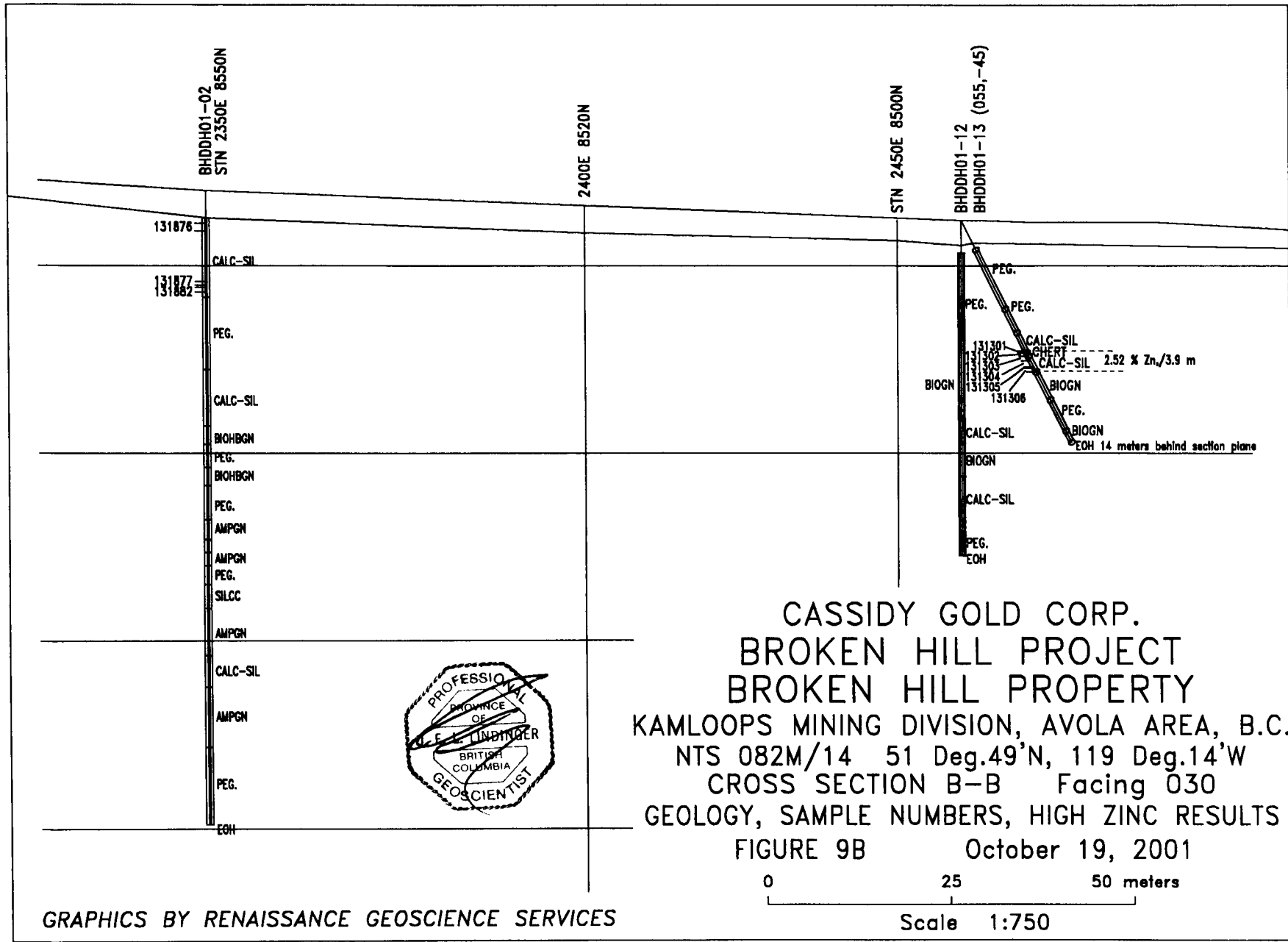
MARB - Leucocratic grey to white crystalline marble. (Pautler unit 3-Mb)

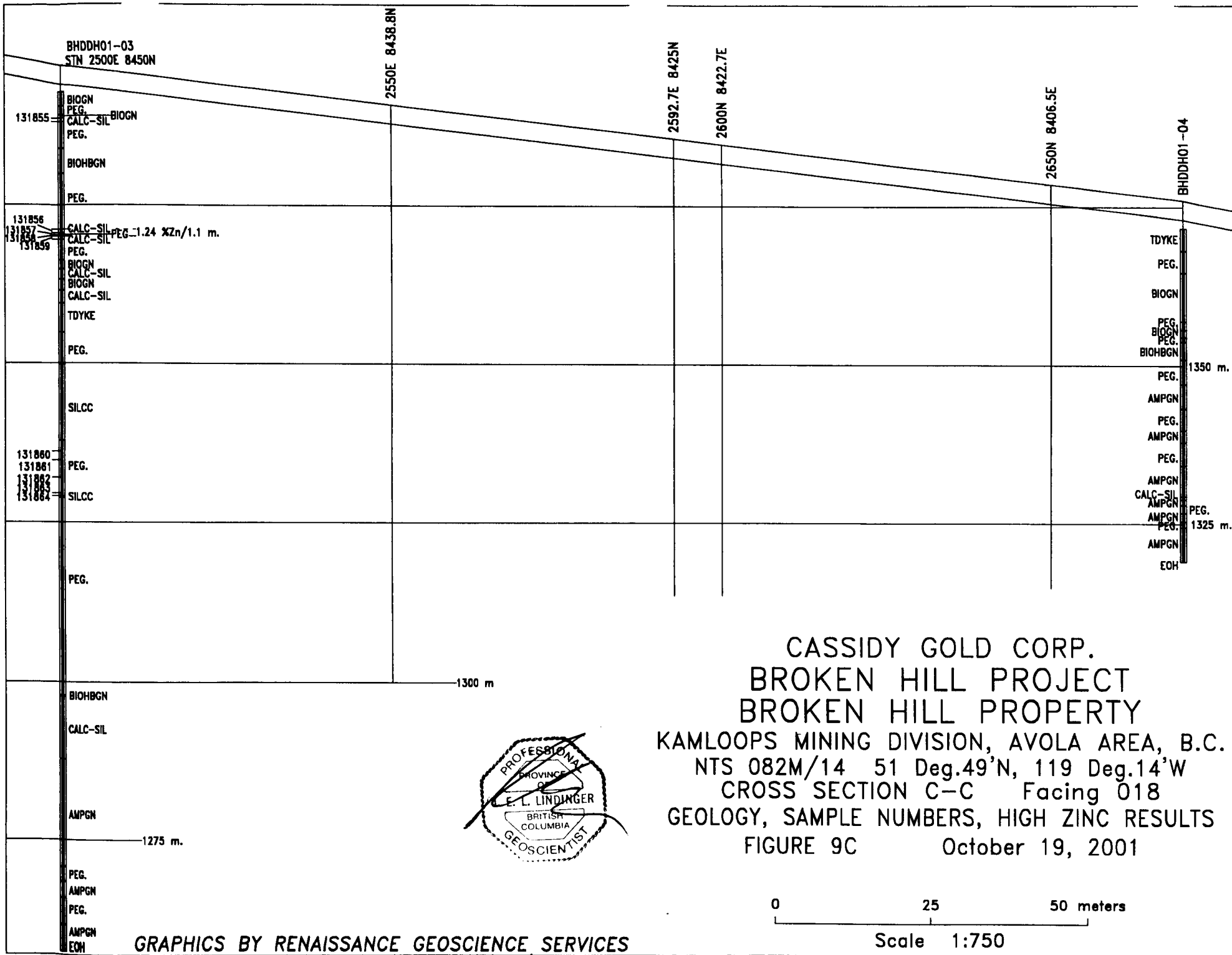
SILCC - Siliceous calc-silicate subunit of CALC-SIL. Leucocratic laminated and banded moderately to highly siliceous rock. Over 35% free cryptocrystalline quartz. (incorporated into Pautler unit 3)

CHERT - Cryptocrystalline laminated siliceous subunit of CALC-SIL. Possibly meta-exhalite. Over 75% free quartz. (incorporated into Pautler unit 3)

BIOHBGN - Intermediate fine to medium grained banded metapelite? Similar to BIOGN but with less quartz and the appearance of trace to 15% amphibole. (incorporated into Pautler unit 1)

AMPHGN - Melanocratic grey to grey-green fine to medium grained banded amphibole gneiss. Often biotite rich. Trace quartz. (Pautler unit 1)





BHDDH01-03
STN 2500E 8450N

2550E 8438.8N

2592.7E 8425N

2600N 8422.7E

2650N 8406.5E

BHDDH01-04

131855
BIOGN
PEG.
CALC-SIL
BIOGN
PEG.

131856
131857
131858
131859
CALC-SIL
CALC-SIL
PEG.
BIOGN
CALC-SIL
BIOGN
CALC-SIL
TDYKE
PEG.

131860
131861
131862
131863
131864
PEG.
SILCC

PEG.

BIOHBN

CALC-SIL

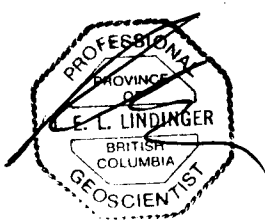
AMPGN

PEG.
AMPGN
PEG.
AMPGN
E.O.H.

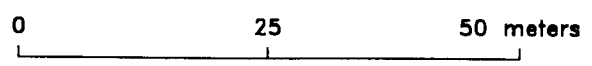
TDYKE
PEG.
BIOGN
PEG.
BIOGN
PEG.
BIOHBN
1350 m.
PEG.
AMPGN
PEG.
AMPGN
PEG.
AMPGN
CALC-SIL
AMPGN
AMPGN
1325 m.
AMPGN
E.O.H.

1300 m

1275 m.

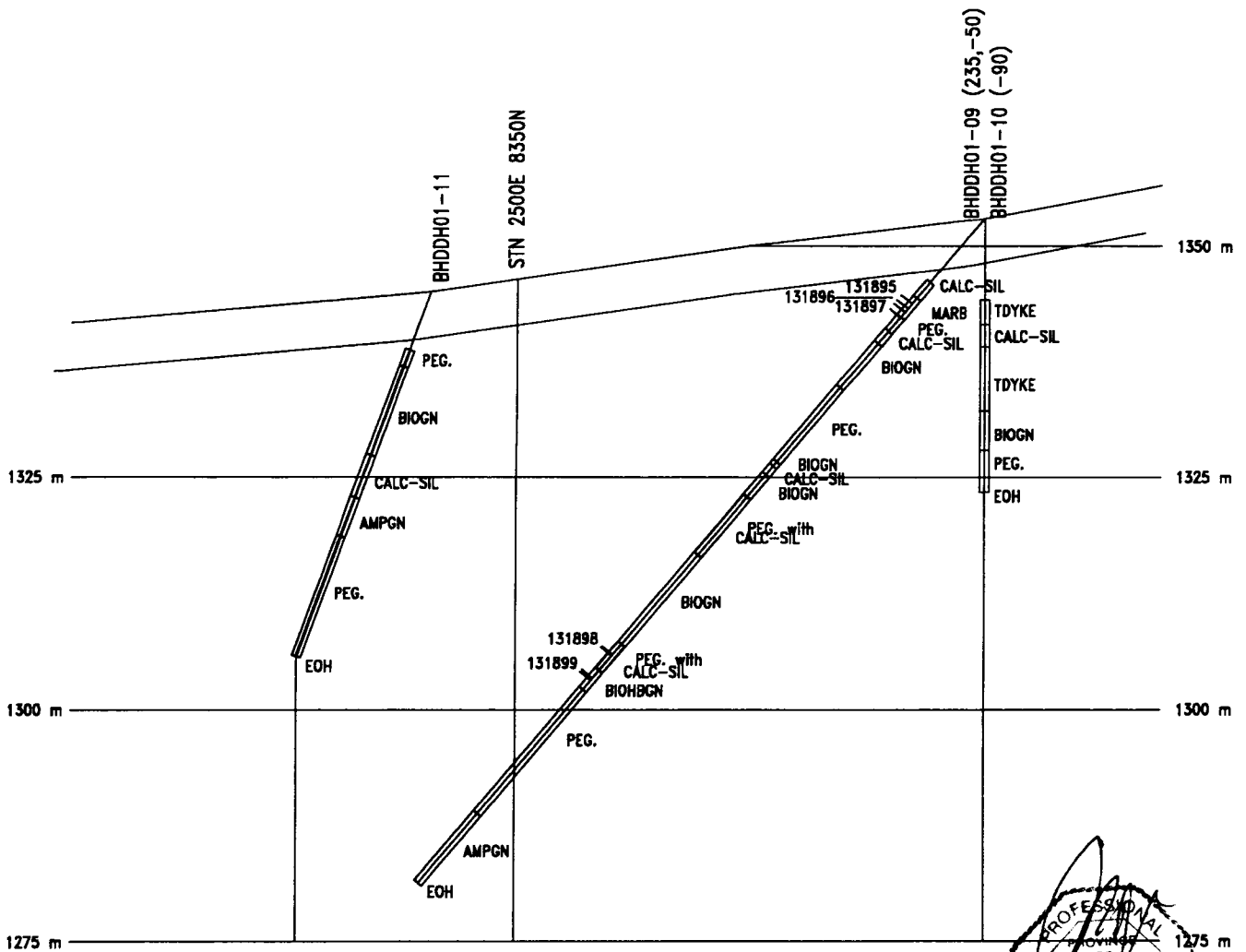


CASSIDY GOLD CORP.
BROKEN HILL PROJECT
BROKEN HILL PROPERTY
KAMLOOPS MINING DIVISION, AVOLA AREA, B.C.
NTS 082M/14 51 Deg.49'N, 119 Deg.14'W
CROSS SECTION C-C Facing 018
GEOLOGY, SAMPLE NUMBERS, HIGH ZINC RESULTS
FIGURE 9C October 19, 2001

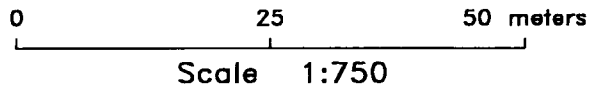


Scale 1:750

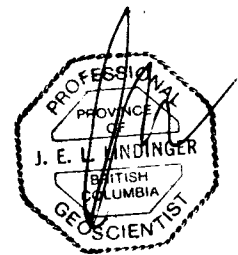
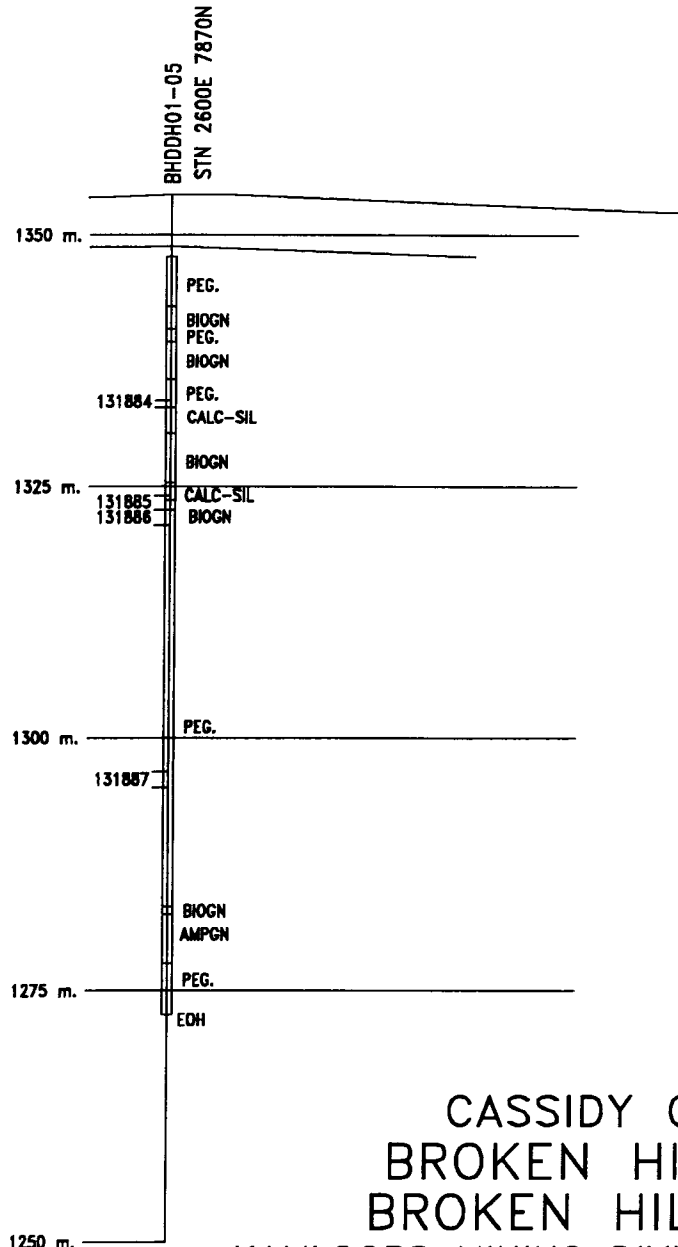
GRAPHICS BY RENAISSANCE GEOSCIENCE SERVICES



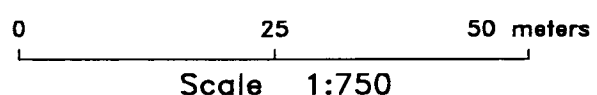
CASSIDY GOLD CORP.
 BROKEN HILL PROJECT
 BROKEN HILL PROPERTY
 KAMLOOPS MINING DIVISION, AVOLA AREA, B.C.
 NTS 082M/14 51 Deg.49'N, 119 Deg.14'W
 CROSS SECTION D-D (8350N) FACING 360
 GEOLOGY, SAMPLE NUMBERS, HIGH ZINC RESULTS
 FIGURE 9D October 19, 2001



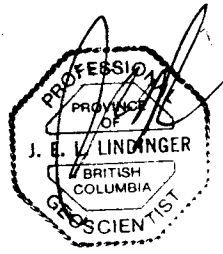
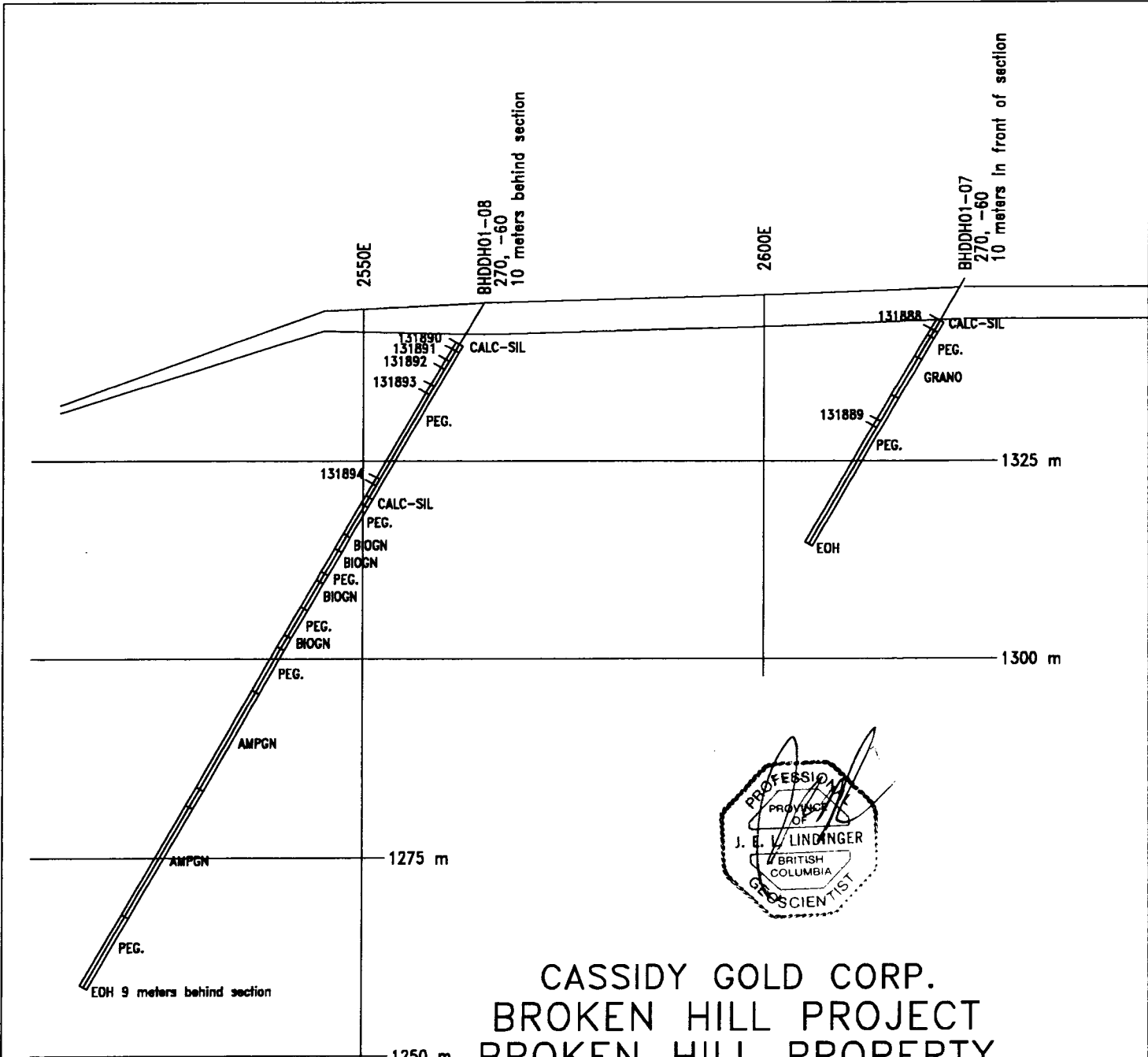
GRAPHICS BY RENAISSANCE GEOSCIENCE SERVICES



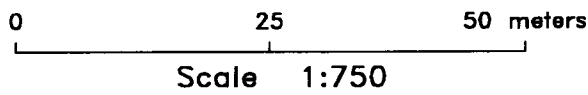
CASSIDY GOLD CORP.
BROKEN HILL PROJECT
BROKEN HILL PROPERTY
 KAMLOOPS MINING DIVISION, AVOLA AREA, B.C.
 NTS 082M/14 51 Deg.49'N, 119 Deg.14'W
 CROSS SECTION E-E (7870N) FACING 360
 GEOLOGY, SAMPLE NUMBERS, HIGH ZINC RESULTS
 FIGURE 9E October 19, 2001



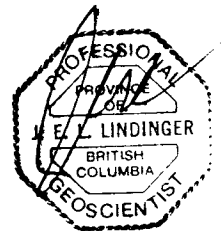
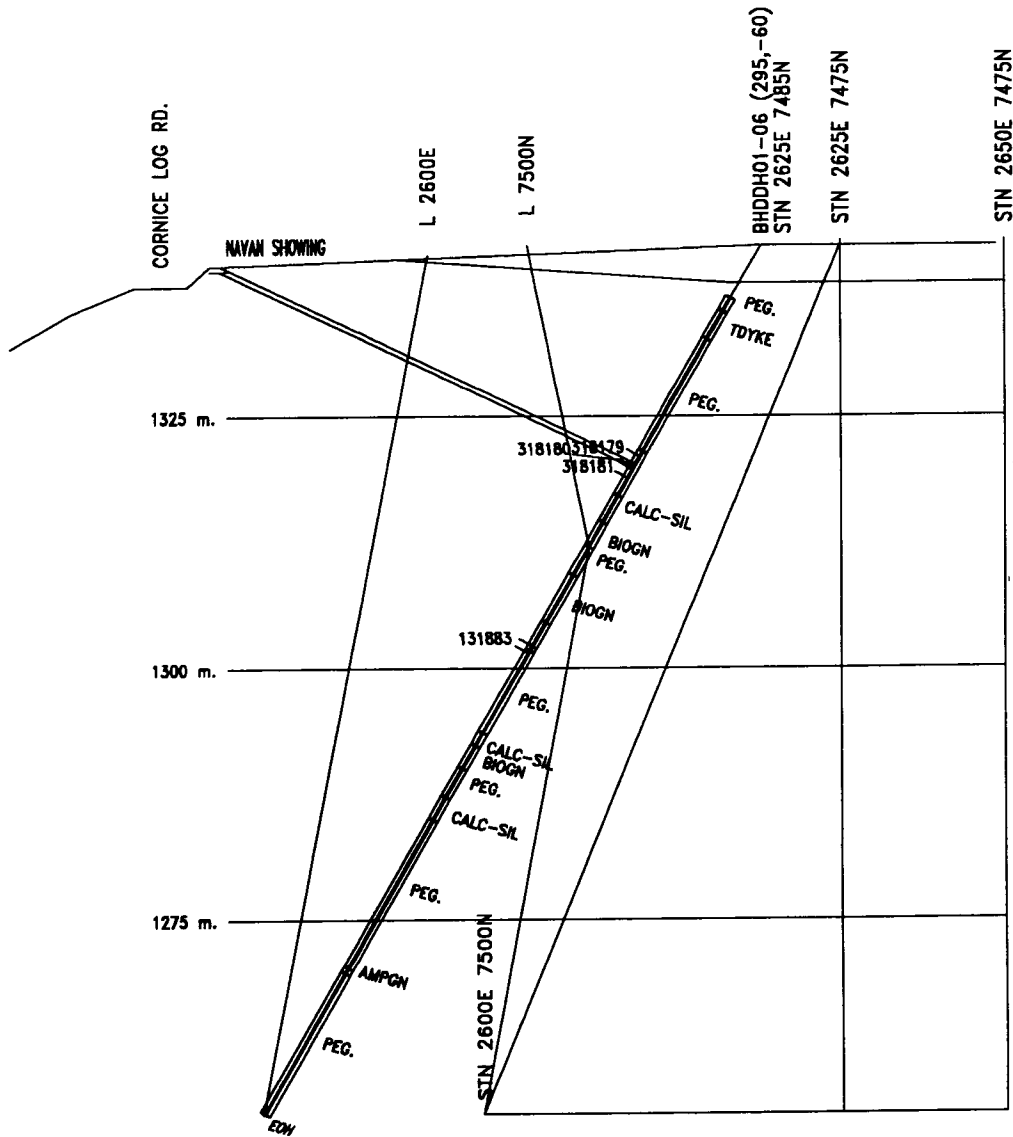
GRAPHICS BY RENAISSANCE GEOSCIENCE SERVICES



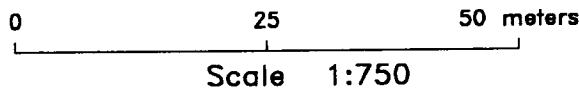
CASSIDY GOLD CORP.
 BROKEN HILL PROJECT
 BROKEN HILL PROPERTY
 KAMLOOPS MINING DIVISION, AVOLA AREA, B.C.
 NTS 082M/14 51 Deg.49'N, 119 Deg.14'W
 CROSS SECTION F-F (7710N) FACING 360
 GEOLOGY, SAMPLE NUMBERS, HIGH ZINC RESULTS
 FIGURE 9F October 19, 2001



GRAPHICS BY RENAISSANCE GEOSCIENCE SERVICES



CASSIDY GOLD CORP.
 BROKEN HILL PROJECT
 BROKEN HILL PROPERTY
 KAMLOOPS MINING DIVISION, AVOLA AREA, B.C.
 NTS 082M/14 51 Deg.49'N, 119 Deg.14'W
 CROSS SECTION G-G FACING 060
 GEOLOGY, SAMPLE NUMBERS, HIGH ZINC RESULTS
 FIGURE 9G October 19, 2001



GRAPHICS BY RENAISSANCE GEOSCIENCE SERVICES

silicified, and a cherty unit was encountered between 46.0 and 46.5m. From the texture within the intruding pegmatite sill, this unit appears to be more extensive and may extend from between 43.3 and 56.0m. Possible amphibolite gneiss was encountered at 83m, but is obscured by pegmatite. Pegmatite constitutes over 60% of the hole. A near vertical fault was intersected at 18m.

Sphalerite and galena mineralization were encountered at the target depth at 25.5m to 25.75m. The mineralization is hosted by a calc-silicate band in the biotite gneiss package and by the intruding pegmatite sill. The mineralized section consists of narrow, 1-2 mm wide bands of sphalerite within the calc-silicate band (which has been intruded by a 0.4m wide pegmatite sill) followed by a 3 cm wide band of massive sphalerite below the pegmatite, hosted by the biotite gneiss. Minor disseminated galena and sphalerite occur within the invading pegmatite.

SIGNIFICANT INTERSECTIONS

FROM (m)	TO	% Zn	% Pb
25.5	25.75	1.19	0.12

BH DDH 01-7 (Figure 9F)

BH DDH 01-7 was drilled to test a gravity anomaly in an area of sphalerite mineralization hosted by skarn and biotite gneiss, 200 meters to the northwest of the Navan Showing. The mineralization exposed at 7660N/2580E is reported to grade up to 5.5 % Zn with 0.6% Pb (Gruenwald, 2000). The down dip extent of a strong soil anomaly on L7700N with values up to 2590 ppm Zn and 412 ppm Pb was also tested.

Diopside-garnet-actinolite skarn with minor pyrrhotite was intersected in the top of the hole down to 7.6m, followed by an extensive pegmatite sill and minor foliated, medium grained granodiorite dykes.

No significant mineralization was intersected. The hole was cut short due to the extensive intersection of pegmatite and consequently did not test the soil anomaly. The weak gravity anomaly may be related to the density contrast between the pegmatite and the near surface effect of the skarn or local topographic variations.

BH DDH 01-8 (Figure 9F)

Due to the extensive pegmatite intersected in DDH 01-7, DDH 01-8 was drilled closer to the above-mentioned soil anomaly on line 7700 N in order to test for the down dip extension.

Extensive pegmatite was encountered (60% of the hole) with narrow remnant bands of biotite gneiss and calc-silicate down to 56.8m. A marble horizon was intersected from 25.9 to 26.6m. Amphibolite gneiss predominates with minor pegmatite below 56.8m. Faults are evident between 7.1m and 19.9m at 39.5m, 51.4m, 61.4m and at 99m. Core axes suggest an apparent relatively flat to 15°E dip for the foliations. Minor folding, with an apparent 30°NE plunge, is evident within the biotite gneiss at 48.7 to 50.4m.

No significant mineralization was intersected possibly due to the extensive pegmatite that was encountered above the amphibolite unit.

BH DDH 01-9 (Figure 9D)

BH DDH 01-9 was drilled to test the down dip extension of an extensive 0.3 mgal gravity anomaly on line 8350 N.

Calc-silicate skarn was intersected in the top of the hole to 11.3m, followed by the white and the grey banded marble and chert horizons to 14.0m. Biotite gneiss, with calc-silicate bands, is the dominant lithology between 14.0 and 66.4m. A pegmatite sill cuts the gneiss from 23.9 to 34.4m. The amphibolite gneiss unit was intersected at 66.4m but is intruded by abundant pegmatite sills. A vertical fault was encountered at 34m, which may have down-dropped the stratigraphy on the southwest side. In this case the chert unit intersected at the top of the pegmatite sill at 66.4m, may correlate with the marble/chert horizon from 11.3 to 14.0m.

No significant mineralization was intersected. The presence of skarn in the top of the hole and a relatively thick sequence of calc-silicate may be partially responsible for the gravity anomaly. The marble and exhalite marker horizons, similar to those in DDH 01-01, -02 and -03, were also encountered. *Local topographic effects may also be partially responsible for the gravity anomaly.*

BH DDH 01-10(Figure 9D)

BH DDH 01-10 was collared at the same site as DDH 01-9 and drilled vertically to test for the down dip extent of the marble/exhalite units intersected in hole 9.

A Tertiary mafic dyke, with a narrow interval of calc-silicate and biotite gneiss, was intersected from the top of the hole to 20.8m. The dyke appears to dip steeply to the southwest at an apparent dip of 60-70° and appears to be correlative with mafic dykes intersected in DDH 01-3, -4 and -6. The dyke would consequently trend west-northwesterly and dip to the southwest. Biotite gneiss was encountered from 20.8 to 25.1m, followed by pegmatite to the end of the hole at 29.6m. The pegmatite appears to be correlative with the pegmatite sill that intrudes the biotite gneiss from 23.9 to 34.4 m in DDH 01-9.

The Tertiary dyke appears to have obscured the favourable horizon consequently no significant mineralization was intersected. The mafic dyke, intersected in the top of the hole, may be partially responsible for the gravity anomaly.

BH DDH 01-11(Figure 9D)

BH DDH 01-11 was drilled to test the down dip extension of a 0.4 mgal gravity anomaly, which forms the locus of a large gravity anomaly on L8350N and stratigraphic continuity west of hole BHDDH 09-09.

The top of the hole down to 23.6m consists primarily of calc-silicate with a biotite gneiss interval from 13.3 to 18.8m and 25-30% pegmatite. Amphibolite gneiss, extensively intruded by pegmatite, was encountered from 23.6 to 28.0m, followed by pegmatite. This appears to correlate with the amphibolite/pegmatite interval intersected at 66.8m in DDH 01-9. Approximately 60% of the hole consists of pegmatite.

No significant mineralization was intersected. The near surface effect of the calc-silicate compared to the pegmatite, and local topographic effects each may be partially responsible for the gravity anomaly. *Also the mineralized horizon may have been missed and be exposed uphill to the north of holes 9,10, and 11.*

BH DDH 01-12 (Figure 9B)

BH DDH 01-12 was drilled to test the *for the updip* extension of mineralization intersected in DDH 01-3 and is located 395 meters at 102° from the Vista Showing and 65 meters west of DDH 01-3.

Pegmatite, with remnant zones of skarn, was intersected from the top of the hole to 15.9m. A chert band was noted at 13.5m. Biotite gneiss predominates from 15.9 to 34.1m with a calc-silicate and grey banded marble interval from 26.4 to 29.6m. A calc-silicate band was again intersected from 34.1 to 42.0m, with grey banded marble occurring near the base of the interval. Pegmatite with minor amphibolite gneiss continued to the end of the hole at 44.8m.

No significant mineralization was intersected. However, a thick sequence of calc-silicate and the marble marker unit were encountered.

BH DDH 01-13 (Figure 9B)

BH DDH 01-13 was collared from the same site as hole 12 and was drilled at bearing 055 at a dip of 45° to test for the north extent of mineralization in DDH 01-3, approximately 30m to the northwest of hole 3.

Pegmatite was encountered in the top of the hole down to 21.1m with biotite gneiss making up to 30% of the interval below 16.7m. From 21.1m to 28.4m quartz-calcite-garnet-diopside-actinolite-tremolite skarn was intersected with a cherty exhalite from 24.9 to 25.5m. Biotite gneiss was intersected from 28.4 to the end of the hole at 41.8m and was intruded by a pegmatite sill from 33.7 to 39.6m.

A 3.9m wide interval with sphalerite and minor galena mineralization was intersected from 24.5m to 28.4m. The mineralization occurs as bands up to 5 cm wide and as disseminations of sphalerite, with minor galena, pyrrhotite and pyrite, hosted by the calc-silicate skarn and an exhalite unit. Some of the skarn within the section is unmineralized. *This zone is very similar and stronger to the mineralization intersected in hole 3 and has similarities to the Vista Showing. The chert hosting the mineralization also describes a shallow fold closure with repetition of the units hosting the zinc mineralization.*

SIGNIFICANT INTERSECTIONS

FROM (m)	TO	Width (m)	% Zn	ppm Zn	% Pb
24.5	24.9	0.4	2.83		
24.9	25.5	0.6	2.96	0.82	
25.5	26.3	0.8	162		
26.3	27.5	1.2	3.92		
27.5	27.8	0.3	505		
27.8	28.4	0.6	3.65		

Weighted average from 24.5 - 28.4 is 2.52 % Zn over 3.9m (estimated true width 2.3m)."

DISCUSSION

This section is as written in Lindinger and Pautler 2001. Sections in italics are added by Lindinger, this report.

“Mineralization in the zinc-lead-silver deposits of the Shuswap Metamorphic Complex is associated with clean marble horizons at the transition between platformal carbonates (calc-silicate) and pelitic sediments (biotite gneiss). Chert commonly underlies mineralization (Oliver, 1988).

Although the favourable marble/chert horizon at the calc-silicate/biotite gneiss transition was intersected in DDH 01-1 at the target depth for the down dip extent of the Vista Showing, no mineralization was encountered. The Vista Showing contains Zn values up to 15.9% over 0.3m (Gruenwald, 2000). The marble horizon at the same transitional zone was also encountered in DDH 01-2, with no accompanying mineralization. Correlation of the stratigraphy encountered in DDH 01-3 and 13, in which mineralization was encountered, with that in DDH 01-1 and -2 suggests that the Vista Horizon may flatten through this area and consequently airs out. Pegmatite in the very top of DDH 01-1 may even have obscured the mineralized horizon. Although accessibility is difficult, sites above (north) of the road should test the Vista Horizon, provided that the pegmatite sills that occur through this area are not too extensive. An attempt should be made to target possible fold closures. From the limited geological mapping on the property, a favourable location is at L8700N/ 2400E with a -90° and -50 ° hole at 200° azimuth.

DDH 01-13 intersected what appears to be the Vista Horizon at 24.5 to 28.4m. Mineralization is associated with skarn and a chert (possible exhalite) unit at a favourable calc-silicate/biotite gneiss transition, approximately 20-25m above the marble/chert horizon intersected in DDH 01-1 and -2. The mineralized zone grades 2.5% Zn over 3.9m (2.3m true width) as a weighted average and is magnetic due to the presence of pyrrhotite. DDH 01-3 also intersected the same mineralized horizon but was interrupted by a pegmatite sill. The remnant mineralization grades 1.2% Zn over 1.1m (weighted average). The same horizon should have been encountered in DDH 01-12 but is *interpreted to be* interrupted by extensive pegmatite sills. Future drill holes should target possible fold closures in this area. Sufficient data is not currently known to accomplish this but a vertical drill hole from L8500N/2575E should intersect the horizon, hopefully without extensive pegmatite.

A possible north to northeasterly trending down-dropped block may occur between DDH 01-3 and -4. If this is the case, the Vista Horizon is down-dropped in DDH 01-9 to -11 and should have been intersected again in DDH 01-3 at a depth of 70m and possibly at 35m in DDH 01-9. A large pegmatite sill is present through this area that may have obliterated the mineralized horizon. If down-dropping hasn't occurred, the horizon would air out through this region *possibly above the collars of holes 9, 10 and 11*. Evidence for the fault block includes the intersection of the high-angle faults, repetition of stratigraphy above the amphibolite unit, and the lower level of the amphibolite within the proposed fault block.

The calc-silicate unit was not intersected in DDH 01-4. It appears to be too low in the stratigraphy since the amphibolite was intersected at 30m. Drill holes would need to be targeted higher on the hillside, northeast of the road. *An unnamed Creek a short distance*

west of hole 4 returned anomalous in zinc and lead from moss mat sampling (Lindinger 2000).

DDH 01-6 was successful in intersecting the Navan Showing at the projected down dip target depth of 25m. The Navan Showing reportedly grades up to 21.5% Zn, 3.8% Pb and 11 g/t Ag from grab samples (Gruenwald, 2000). The Navan Horizon was encountered at 25.5 to 25.75m, grading 1.2% Zn with 0.1% Pb, but was disrupted by a pegmatite sill. The mineralization occurs 20m above a marker marble/chert horizon. This represents the same distance that the Vista Horizon was intersected above the marker horizon in DDH 01-13. Hence it is probable that the Vista and Navan Horizons are the same.

Based on the intersection in DDH 01-6, the Navan Horizon should have been intersected in DDH 01-5 at an approximate depth of 30m, at 30-35m in DDH 01-7 and 5-10m in DDH 01-8. Unfortunately, a large pegmatite sill or coarse grained leucogranitic stock invades the stratigraphy in this area. The marble horizon was intersected in DDH 01-8 at 26m. The Navan Horizon should therefore occur near the top of the hole. Approximately 60% of the core from the casing consisted of skarn with 30% pegmatite. At the Navan Showing, mineralization occurs within the skarn, adjacent to pegmatite (Gruenwald, 2000). In the Navan area, the amphibolite contact appears to be at 1275m, dipping shallowly northeast. Potential occurs east of the road, further down dip and hopefully away from the pegmatite. A prospective drill site, targeting a possible fold closure in the area would be at 7625N/2700E with a -90° and -50° hole at 200° azimuth.

The large soil anomaly on L7700N with values up 2590 ppm Zn and 412 ppm Pb may be due to downslope dispersion of mineralization related to the airing out of the Navan Horizon near the collar of DDH 01-8. Mineralized boulders in this area returned values up to 5.5 % Zn with 0.6% Pb (Gruenwald, 2000).

CONCLUSIONS

The preliminary soil and rock sampling programs partially outlined several open ended multi-element soil anomalies, especially in the Navan and Mike areas. These anomalies have not been tested by subsequent programs. Rock samples of mineralized material from the VISTA, NAVAN, and MIKE showings returned economic grades of zinc-lead-silver mineralization.

A preliminary gravity survey over a small portion of the property failed to outline mineralization. However the survey was incomplete and the most prospective areas remain untested. The survey did succeed in outlining larger areas underlain by felsic intrusive (gravity low) and thick calc-silicate (gravity high) areas.

The following conclusions on the diamond drilling is excerpted from Lindinger and Pautler 2001.

“The 2001 diamond drill program on the Broken Hill-Leo property was successful in intersecting both the Vista and Navan mineralized horizons, down dip from the surface exposures. An interpretation of the drill hole intersections of the horizons indicates that the Vista and Navan Horizons are probably the same. The Navan Showing is located 1.3 km southeast of the Vista. The Vista-Navan Horizon occurs approximately 20m above a marker marble (chert) horizon.

The Vista Horizon, which reportedly contains 15.9% Zn over 0.3m at the Vista Showing (Gruenwald, 2000), was intersected in DDH 01-3 and -13, approximately 500m east-

southeast of the Vista Showing. The mineralized zone grades 2.5% Zn over 3.9m (2.3m true width) as a weighted average in DDH 01-13 and is magnetic due to the presence of pyrrhotite. The intersection in DDH 01-3 was interrupted by a pegmatite sill, with the remnant mineralization grading 1.2% Zn over 1.1m (weighted average). It appears that pegmatite sills obliterated the Vista Horizon in DDH 01-12. The Horizon appears to air out along the road between the Vista Showing and DDH 01-13. Future drilling should concentrate to the north of the road, further down dip on the Horizon.

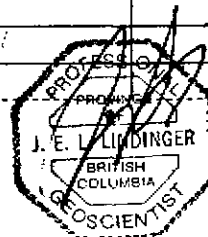
DDH 01-6 was successful in intersecting the Navan Horizon 25m down dip from the surface showing but was disrupted by a pegmatite sill. The diluted intersection grades 1.2% Zn with 0.1% Pb over 0.25m. The Navan Showing reportedly grades up to 21.5% Zn, 3.8% Pb and 11 g/t Ag from grab samples (Gruenwald, 2000). The Navan Horizon should also have been intersected in DDH 01-5, -7 and possibly in the very top of -8 but a large pegmatite sill invades the stratigraphy in this area.

A possible down-dropped fault block was delineated midway between the Vista and Navan Showings. In this case a pegmatite sill obliterated the Horizon in DDH 01-9, -10 and -11. *Or the mineralization outcrops above holes 9 10 and 11. Also it is interpreted that the horizon has aired above DDH 01-4 and future drill holes need to be targeted higher on the hillside.*

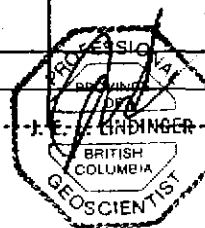
In conclusion, the Broken Hill-Leo property covers a 9 km strike extent of the carbonate stratigraphy, favourable for hosting high grade zinc-lead-silver Shuswap style mineralization similar to the Ruddock Creek (5 million tonnes grading 7.5% Zn, 2.5% Pb), CK (1.5 million tonnes grading 8.6% Zn), and Finn occurrences. Similar style mineralization occurs on the property and needs to be traced down dip, into potential fold closures and away from the pegmatite sills. The excellent access and infrastructure, in contrast to the Ruddock Creek, Cottonbelt and CK occurrences, add to the potential of the property.”

TABLE 3 - EXPENSES

A.	B.	C.	D.	E.	F.
2.	COST ITEM	dates (2000)	Rate/Day or km	Days or km	TOTAL
3.	Preparatory survey - 6.1 km cut tight chained baselines				
4.	Wages- L Lindinger, P. Geo.	Oct 9-13	\$ 347.75	4.5	\$1,564.88
5.	Wages - Denis Delisle	Oct 10-13	\$ 256.80	4	\$1027.20
6.	Geochemical survey - 479 soil samples				
7.	Wages- L Lindinger, P. Geo.	Oct 14-17	\$ 347.75	3	\$1,043.25
8.	Wages - Denis Delisle	Oct 14-17	\$ 256.80	3	\$ 770.40
9.	Wages - Warner Gruenwald, P.Geo mapping, 30 rock samples	Oct 12-17	\$ 374.50	6	\$2,247.00
10.	Wages - Rob Montgomery	Oct 12-17	\$ 267.50	6	\$1,605.00
11.	Transportation				
12.	Wages - L. Lindinger, P.Geo.	Oct 9, 18	\$ 347.75	2	\$ 695.50
13.	Wages - Denis Delisle	Oct 9, 18	\$ 256.80	2	\$ 513.60
14.	Wages - Warner Gruenwald, P.Geo	Oct 11, 18	\$ 214.00	2	\$ 428.00
15.	Wages - Rob Montgomery	Oct 11, 18	\$ 187.25	2	\$ 374.50
16.	Vehicle - Lindinger	Oct 9-17	\$ 53.50	8	\$ 428.00
17.	extra kilometers		\$ 0.27	470	\$ 126.90
18.	Vehicle - Delisle	Oct 9, 18	\$ 53.50	2	\$ 107.00
19.	Vehicle - Gruenwald	Oct 11, 18	\$ 40.66	2	\$ 81.32
20.	extra kilometers		\$ 0.27	400	\$ 108.00
21.	Vehicle - Montgomery		\$ 37.45	2	\$ 74.90
22.	extra kilometers	Oct 11, 18	\$ 0.27	400	\$ 108.00
23.	Accommodation				
24.	30 mandays	Oct 10-17	\$ 95.00	30	\$2,850.00
25.	Supplies, equipment rental and fuel				\$2,420.58
26.	Analyses				
27.	Analyses costs soils 479 samples		\$ 10.43	479	\$4,995.97
28.	Analyses - rocks 30 samples		\$ 15.52	30	\$ 465.60
29.	Analyses - metallic assays				\$ 105.81
30.	total preparatory and geochemistry				\$22,547.03
31.	Photogrammetry - 8 square km				
32.	Eagle Mapping Ltd.				\$6,329.05
33.	Preparatory work. Line brushing (13.2 km) and logistical support gravity survey.	Nov 24-Dec17			
34.	Wages - L. Lindinger, P.Geo. Supervision surveying and line brushing.	Nov 24-Dec 1, 5-8, 13, 17-18	\$ 353.10	10.3	\$3,636.93
35.	Wages - Denis Delisle - line brushing	Nov 24-29	\$ 262.15	6	\$1,572.90
36.	Wages - Mickey Sidhu - line brushing	Dec1-10, 15-18	\$ 219.35	13	\$2,851.55
37.	Accommodation per inv. Blue River Motel	Dec 1-18			\$2,628.53
38.	food, fuel, supplies, radio rental	Dec1 - Dec 18			\$1,632.34
39.	Snowmobile & skimmer rental	Dec1-Dec18			\$3,289.52



A.	B.	C.	D.	E.	F.
2.	COST ITEM	dates (2000)	Rate/Day or km	Days or km	TOTAL
40.	Truck rental - Canex rental	Dec1-18			\$1,650.76;
41.	Chainsaw rental	Dec 1-18	\$ 33.67	9	\$ 303.05;
42.	4x4 vehicle -Lindinger	Dec 5-7, 14	\$ 58.85	4	\$ 235.40;
43.	4x4 vehicle Mickey Sidhu	Dec1, Dec18	\$ 53.50	2	\$ 107.00;
44.	Gravity survey - Discovery Geophysics 8.3 line km at 25 m spacing	Dec 1 to 17			\$22,272.33;
45.	Diamond Drilling	Jan - Feb 2002			
46.	Plowing road d7 and grader - 21 km	Jan 19, Feb 12			\$6,981.88;
47.	L. Lindinger, P.Geo	Jan 15, 27-Feb 1, Feb 5-8	\$ 353.10	10.5	\$3,707.55;
48.	J. Pautler, P. Geo.	Jan 28-Feb 7	\$ 428.00	11	\$4,708.00;
49.	Accomodation and food 22 mandays @\$60.	Jan 28-Feb7	\$ 60.00	22	\$1,320.00;
50.	Vehicle rental Lindinger 4X4	Jan28-Feb7	\$ 58.85	12	\$ 706.20;
51.	Vehicle Lindinger 1 ton van	Jan 28-29	\$ 53.50	2	\$ 107.00;
52.	3 tonne 4x4 pickup Canex rental				\$ 653.63;
53.	Core Shack rental	Jan 28-Feb 7	\$ 32.10	11	\$ 353.10;
54.	Chain saw rental	Jan 28-Feb 7	\$ 21.40	13	\$ 278.20;
55.	Radio rental	Jan 28 Feb 7	\$ 10.70	13	\$ 139.10;
56.	Generator rental per invoice	Jan 28, - Feb 7			\$ 610.00;
57.	Core Splitter rental per invoice				\$ 133.75;
58.	Rock Saw rental		\$ 21.40	11	\$ 235.40;
59.	Geochemical analyses per inv. 41 samples				\$1,347.00;
60.	fuel, supplies				\$2,177.28;
61.	Drilling - 930 meters in 13 holes				\$61,075.32;
62.	Project preparation and administration				\$5,096.00;
63.	report				\$5,000.00;
64.	grand total expenditures				\$163,280.18;



RECOMMENDATIONS

The following recommendations are excerpted from Lindinger and Pautler, 2001.

“A program of detailed geological mapping, prospecting, a possible magnetic survey and excavator trenching is proposed. This should be followed by a second phase diamond drill program.

The geological mapping is necessary to expand the knowledge in and outside of the known grid area to delineate possible fold closures, to exclude areas with a high concentration of pegmatite and to incorporate the Mike Showing, 5 km southeast of the Vista. Only very limited geological mapping for the Vista-Navan area has been completed. Prospecting is necessary to follow up the high grade float, carrying 20% Zn, from the Mike Showing. Since the Vista-Navan Horizon is magnetic in DDH 01-13, the magnetic signature of the existing core that intersects the Horizon should be tested and if the Horizon has a distinct

signature, the Vista and Navan Showings should be surveyed magnetically. If favourable a magnetic survey should be completed over the grid and as possible reconnaissance lines to follow up the Mike Showing. Excavator trenching should be undertaken on the Vista, Navan and on the Mike, if a bedrock source is suspected or located, and trace them along strike. This would provide more geological, particularly structural data.

The second phase diamond drill program would target fold closures and projected extents of the Vista-Navan and possibly the Mike Horizons through areas of lower pegmatite content. Possible favourable drill sites that have already been identified, but should be confirmed by additional mapping, include the following:

- 1) L8700N/ 2400E -90° and -50 ° 200° azimuth
- 2) L8500N/2575E-90°
- 3) 7625N/27E-90° and -50° 200° azimuth
- 4) higher on the hillside, northeast of the road from DDH 01-4
- 5) north of the road, further down dip between the Vista Showing and DDH 01-13.”

Selected References

- Campbell, R.B. 1963: Geological Map of Adams Lake, 82M W½. GSC Map 48-1963.
- Evans, G. 1993: Geological, Geochemical and Geophysical Assessment Report on the Blue River Property for Teck Corp. 10 pages plus attachments. EMPR Assessment Report# 22742.
- Gibson, G. 1991: Geological Report on the Hos 1-19 Mineral Claims, for Bethlehem Resources Corp. 16 pages plus attachments. EMPR Assessment Report# 21201.
- Gruenwald, W. 2000: Preliminary Report on the Broken Hill Property. Unpublished report for Cassidy Gold Corp., 3 pages plus attachments.
- Hoy, T. 1996: Irish-Type Carbonate Hosted Zn-Pb. BC Mineral Deposit Model E13, 5 pages.
- Hoy, T. 1996: Broken Hill-Type Pb-Zn-Ag+/-Cu. BC Mineral Deposit Model S01, 5 pages.
- Lewis, T.D. 1883: Geological and Geochemical Report on the Otter Creek Property, for Noranda Exploration Company, Ltd. 5 pages plus attachments. EMPR Assessment Report# 11904.
- Lindinger, 2000. Unpublished prospecting program
- Lindinger, 2000: Report on the Leo Property. Unpublished report for La Rock Mining Corp. 10 pages plus attachments.
- Lindinger and Pautler, 2001; Report on the 2001 Diamond drill Program on the Broken Hill Property. Unpublished report for Cassidy Gold Corp. 17 pages plus attachments..
- MacIntyre D. 1992: Sedimentary Exhalitive Zn-Pb-Ag. BC Mineral Deposit Models E14, 4 pages.
- Murrell, M. 1980: Geochemical Assessment report on the Finn 1 Claim for Cominco Ltd. 2 pages plus attachments. EMPR Assessment Report# 9027.
- Oliver, J. 1988: Drilling and geological report on the 1987 exploration of the CK property, 54 pages plus attachments. EMPR Assessment Report# 17539.
- Scammell, R.J. 1990: Preliminary results of stratigraphy, structure, and metamorphism in the southern Scrip and northern Seymour ranges, southern Omineca Belt, British Columbia. In Current Research, Part E, Geological Survey of Canada, Paper 90-1E: pp 97-106.
- Wheeler J.O., & Palmer A.R. ed, 1992: Geology of the Cordilleran Orogen in Canada. Geology of North America, Volume G-2; Geology of Canada No. 4, pages 146, 162, 195-196, 293, 508, 514, 545-546, 607-610, 619, 621-622, 715,

STATEMENT OF QUALIFICATION

I, J E. L.(Leo) Lindinger, hereby do certify that:

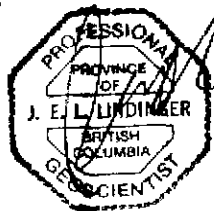
I am a graduate of the University of Waterloo (1980) and hold a BSc. degree in honors Earth Sciences.

I have been practicing my profession as an exploration and mine geologist continually for the past 20 years.

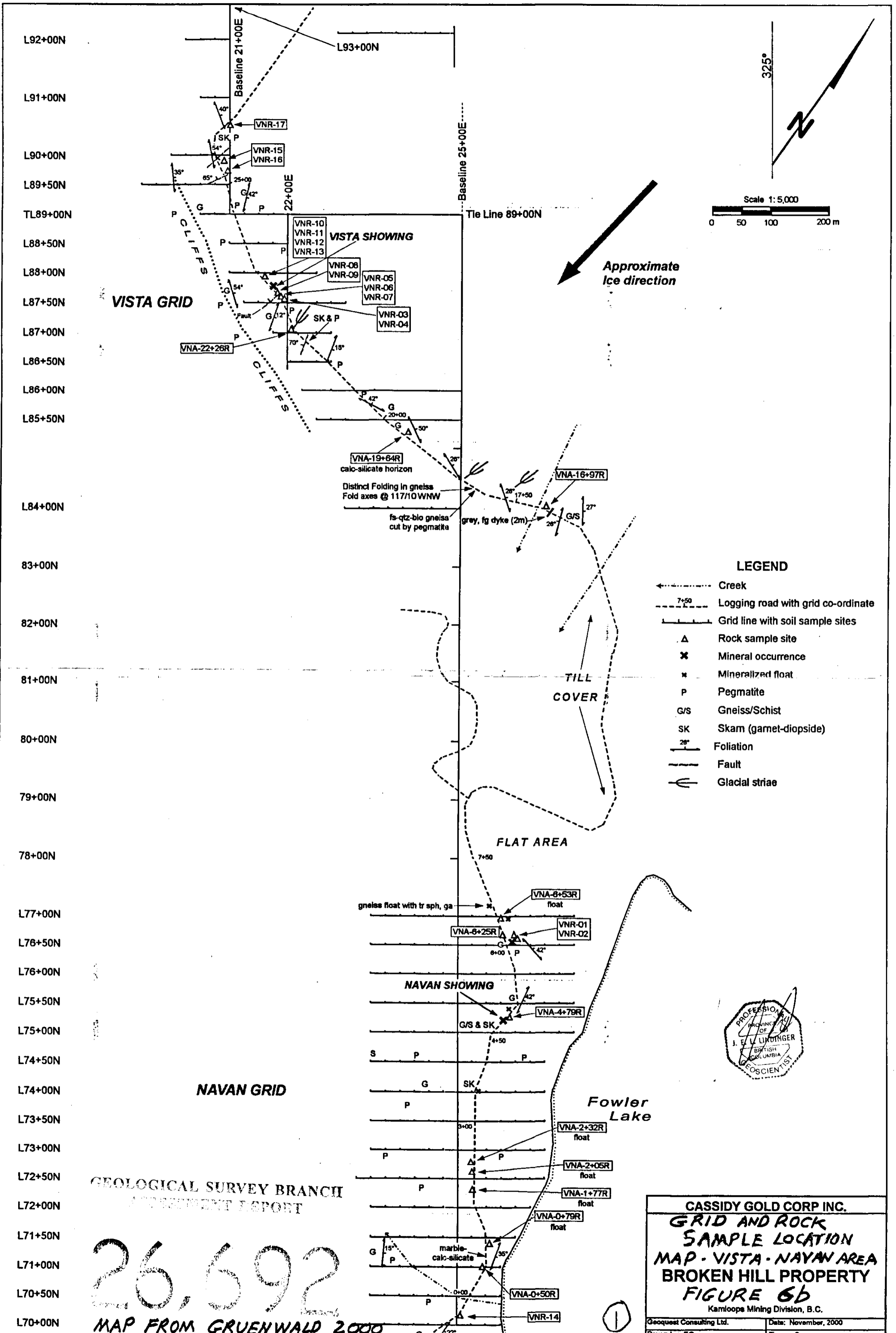
I am a registered member, in good standing as a Professional Geoscientist with the Association of Professional Engineers and Geoscientists of the Province of British Columbia (1992).

I am the vendor of the Broken Hill-Leo property and have an interest in the securities of Cassidy Gold Corp.

The sections of the report that I have participated in writing do not include the discussion, conclusions and recommendation described in this report of the drilling program.



J.E.L.(Leo) Lindinger. P. Geo.



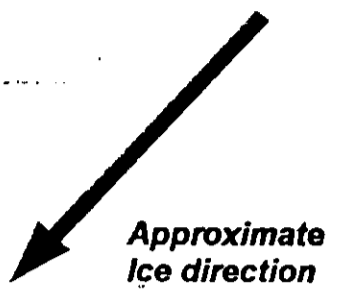
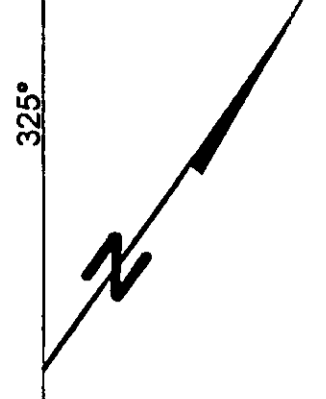
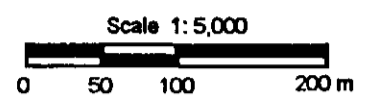
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VISTA GRID

NAVAN GRID

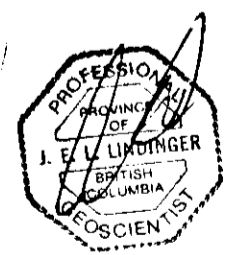
GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT

26,692
MAP FROM GRUENWALD 2000



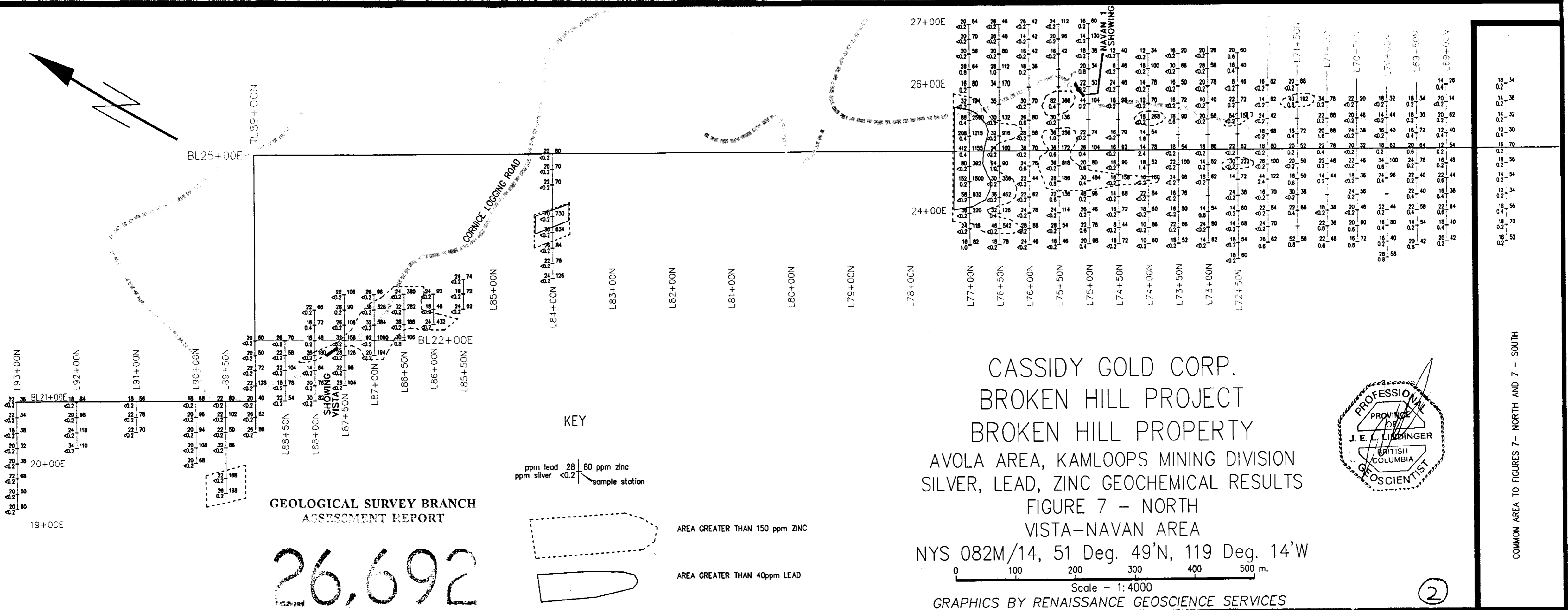
LEGEND

- Creek
- Logging road with grid co-ordinate
- Grid line with soil sample sites
- Rock sample site
- Mineral occurrence
- Mineralized float
- Pegmatite
- Gneiss/Schist
- Skam (gamet-diopside)
- Foliation
- Fault
- Glacial striae



CASSIDY GOLD CORP INC.
GRID AND ROCK
SAMPLE LOCATION
MAP - VISTA - NAVAN AREA
BROKEN HILL PROPERTY
FIGURE 6B
 Kamloops Mining Division, B.C.

Geoquest Consulting Ltd. Date: November, 2000
 Drawn by: EG Figure: 6



GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT

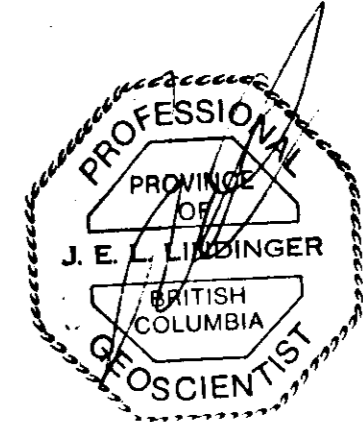
26,692

KEY
 ppm lead 28 | 80 ppm zinc
 ppm silver <0.2 | sample station

AREA GREATER THAN 150 ppm ZINC
 AREA GREATER THAN 40ppm LEAD

CASSIDY GOLD CORP.
 BROKEN HILL PROJECT
 BROKEN HILL PROPERTY
 AVOLA AREA, KAMLOOPS MINING DIVISION
 SILVER, LEAD, ZINC GEOCHEMICAL RESULTS
 FIGURE 7 - NORTH
 VISTA-NAVAN AREA
 NYS 082M/14, 51 Deg. 49'N, 119 Deg. 14'W

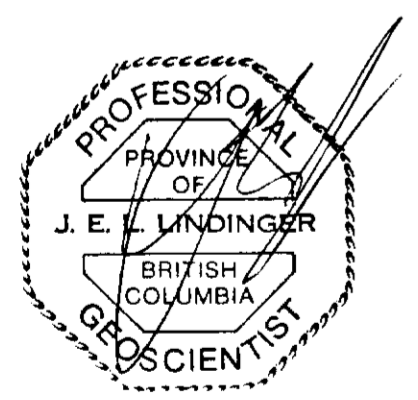
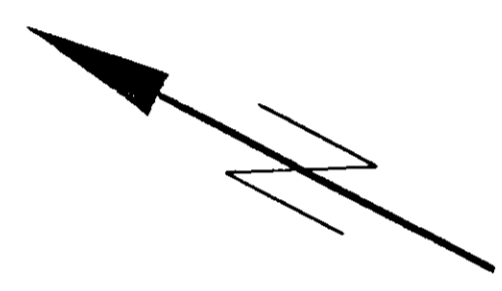
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 GRAPHICS BY RENAISSANCE GEOSCIENCE SERVICES



COMMON AREA TO FIGURES 7 - NORTH AND 7 - SOUTH

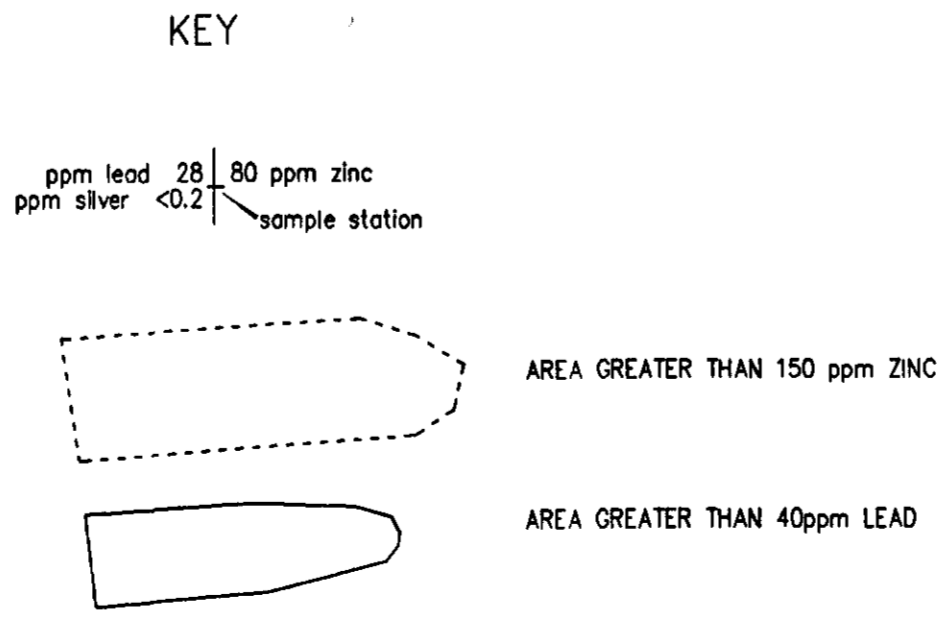
2

COMMON AREA TO FIGURES 7 - NORTH AND 7 - SOUTH



CASSIDY GOLD CORP.
 BROKEN HILL PROJECT
 BROKEN HILL PROPERTY
 AVOLA AREA, KAMLOOPS MINING DIVISION
 SILVER, LEAD, ZINC GEOCHEMICAL RESULTS
 FIGURE 7 - SOUTH
 SOUTH GRID EXTENSION - MIKE AREA
 NYS 082M/14, 51 Deg. 49'N, 119 Deg. 14'W

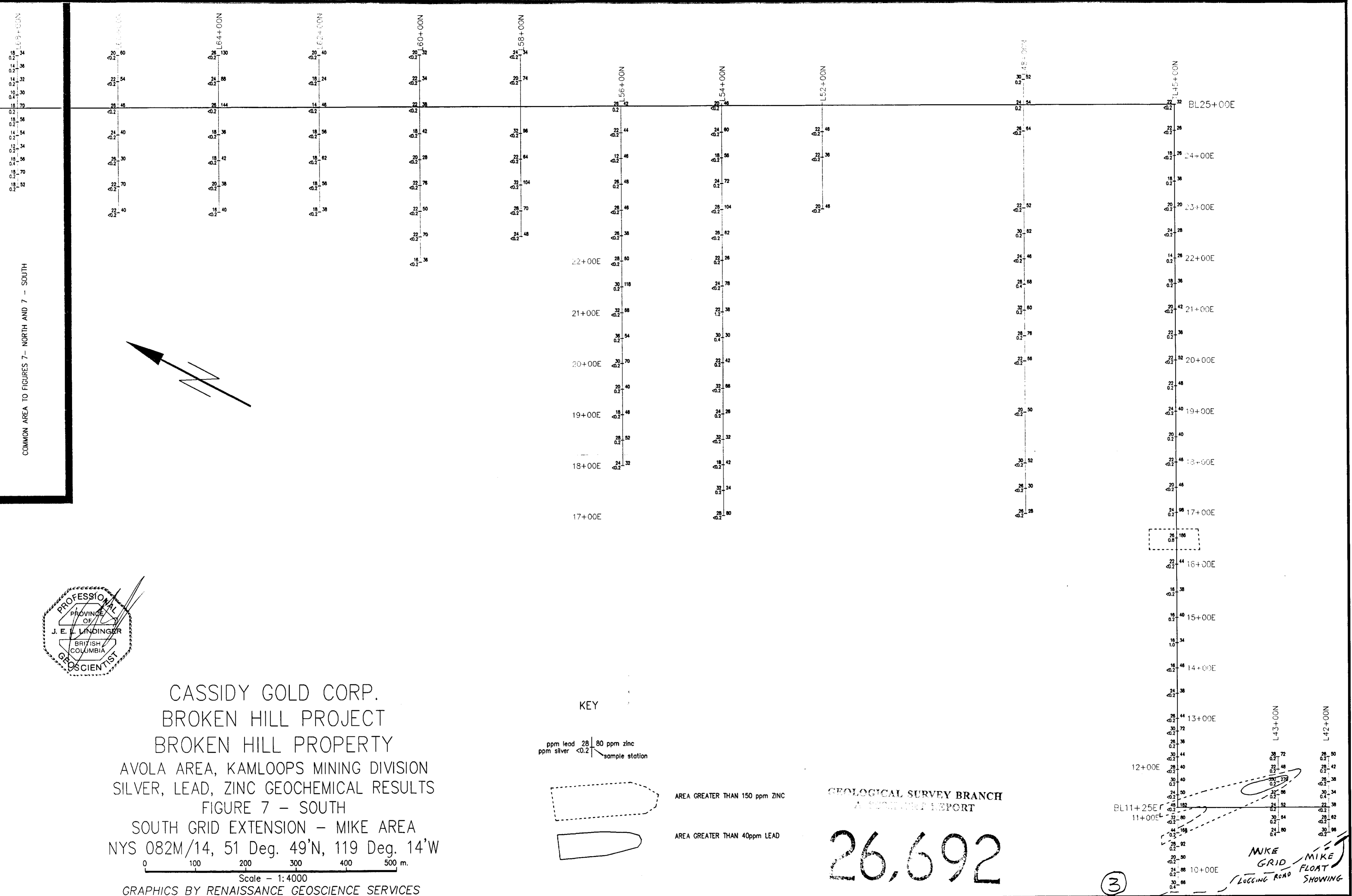
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 GRAPHICS BY RENAISSANCE GEOSCIENCE SERVICES



GEOLOGICAL SURVEY BRANCH
 A SCIENTIFIC REPORT

26,692

3



APPENDIX I

SOIL AND ROCK GEOCHEMISTRY



ALS Chemex

Aurora Laboratory Services Ltd.
 Analytical Chemists * Geochemists * Registered Assayers
 212 Brooksbank Ave., North Vancouver
 British Columbia, Canada V7J 2C1
 PHONE: 604-984-0221 FAX: 604-984-0218

by: GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

Page or : 1-A
 Total : 4 : 2
 Certificate Date: 24-OCT-2000
 Invoice No. : I0031433
 P.O. Number :
 Account : CYO

CERTIFICATE OF ANALYSIS A0031433

SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
VNA 0+00B	201 285	0.2	7.88	560	3.0	< 2	1.26	< 0.5	10	47	11	4.07	1.56	0.65	415
VNA 0+25B	201 285	0.2	8.07	1090	2.5	2	1.20	< 0.5	7	33	12	2.91	1.42	0.49	370
VNA 0+50B	201 285	< 0.2	7.84	630	2.5	< 2	1.13	< 0.5	9	52	12	3.74	1.70	0.76	470
VNA 0+75B	201 285	0.2	8.41	440	4.0	4	3.77	< 0.5	18	56	18	3.72	1.32	0.96	470
VNA 1+00B	201 285	0.2	8.17	450	2.0	2	1.08	< 0.5	6	16	15	2.43	1.15	0.29	420
VNA 1+25B	201 285	< 0.2	8.09	470	2.0	< 2	0.95	< 0.5	7	23	14	2.38	1.26	0.33	365
VNA 1+50B	201 285	0.2	10.15	480	3.0	< 2	1.51	< 0.5	13	49	20	4.22	1.36	0.54	455
VNA 1+75B	201 285	0.6	9.09	190	10.5	16	3.07	< 0.5	10	35	23	4.03	0.57	0.57	635
VNA 2+00B	201 285	0.2	8.58	590	3.0	< 2	1.22	< 0.5	12	49	23	3.76	1.50	0.71	515
VNA 2+25B	201 285	< 0.2	8.51	440	2.5	< 2	1.00	< 0.5	9	33	11	2.83	1.48	0.42	385
VNA 2+50B	201 285	0.6	8.44	490	2.5	< 2	0.99	< 0.5	8	33	10	3.09	1.46	0.43	360
VNA 2+75B	201 285	0.2	8.86	470	2.0	< 2	0.94	< 0.5	7	31	12	2.71	1.21	0.36	360
VNA 3+00B	201 285	< 0.2	7.78	560	3.0	< 2	1.17	< 0.5	9	37	17	2.87	1.77	0.56	375
VNA 3+25B	201 285	0.8	9.58	490	6.0	2	1.91	< 0.5	20	66	20	4.66	1.28	0.76	535
VNA 3+50B	201 285	0.4	8.48	450	3.5	2	1.65	< 0.5	14	54	18	4.35	1.03	0.56	625
VNA 3+75B	201 285	0.2	9.12	640	2.5	< 2	1.38	< 0.5	13	69	14	5.46	1.84	0.80	580
VNA 4+00B	201 285	0.2	7.31	500	2.0	< 2	0.93	< 0.5	9	35	14	2.92	1.40	0.39	460
VNA 4+25B	201 285	0.4	>25.0	2030	8.0	< 2	3.04	0.5	26	149	49	11.55	6.02	1.92	1225
VNA 4+50B	201 285	0.2	9.51	510	3.0	< 2	1.56	0.5	12	72	27	4.68	1.38	0.68	440
VNA 4+75B	201 285	0.2	10.00	460	6.5	4	1.75	1.0	15	40	16	4.19	1.00	0.40	955
VNA 5+00B	201 285	0.2	9.35	470	2.0	< 2	0.83	< 0.5	7	33	9	3.07	1.32	0.37	405
VNA 0+00C	201 285	< 0.2	8.51	720	3.5	< 2	1.60	< 0.5	13	42	22	2.79	2.19	0.80	545
VNA 1+00C	201 285	< 0.2	7.18	610	3.5	< 2	1.57	< 0.5	11	36	29	2.57	2.07	0.70	625
VNA 2+00C	201 285	0.2	6.72	640	3.5	< 2	1.72	0.5	7	28	12	1.90	2.09	0.58	550
VNA 3+00C	201 285	< 0.2	7.68	600	3.5	< 2	1.22	< 0.5	10	36	24	2.15	2.35	0.64	485
VNA 4+00C	201 285	0.2	8.43	770	3.5	< 2	1.34	< 0.5	10	41	18	2.75	2.24	0.69	445
VNA 4+50C	201 285	0.8	8.32	590	3.5	< 2	3.47	< 0.5	26	71	73	3.69	1.61	1.14	620
VNA 5+00C	201 285	< 0.2	6.67	640	2.5	< 2	1.48	< 0.5	7	23	11	1.71	1.94	0.40	535
L70+00N 23+25E	201 285	0.8	7.19	490	2.5	< 2	1.52	< 0.5	14	26	56	2.44	1.44	0.62	1015
L70+00N 23+50E	201 285	0.2	7.20	500	1.5	< 2	1.64	< 0.5	5	17	8	1.73	1.53	0.53	415
L70+00N 23+75E	201 285	0.4	7.04	480	2.0	< 2	1.60	< 0.5	14	40	25	3.45	1.46	0.77	640
L70+00N 24+00E	201 285	0.2	7.22	620	3.0	< 2	1.65	< 0.5	12	44	22	2.91	2.07	0.74	495
L70+00N 24+50E	201 285	0.4	7.74	630	3.5	< 2	1.52	< 0.5	19	55	52	3.72	2.08	1.04	690
L70+00N 24+75E	201 285	0.6	7.09	570	4.5	< 2	1.07	< 0.5	12	35	32	3.69	1.89	0.55	595
L70+00N 25+00E	201 285	0.2	6.76	590	2.0	< 2	1.18	< 0.5	9	43	12	3.41	1.87	0.57	420
L70+00N 25+25E	201 285	< 0.2	7.09	590	2.5	< 2	1.84	< 0.5	11	34	13	2.37	1.91	0.58	520
L70+00N 25+50E	201 285	< 0.2	7.50	510	2.0	< 2	0.92	< 0.5	4	28	10	2.77	1.47	0.37	290
L70+00N 25+75E	201 285	< 0.2	7.29	590	2.5	< 2	1.24	< 0.5	6	31	10	2.53	1.89	0.45	320
L70+50N 23+50E	201 285	0.6	6.75	540	2.0	< 2	1.07	< 0.5	9	39	13	3.44	1.55	0.57	470
L70+50N 23+75E	201 285	0.6	7.14	590	2.5	< 2	1.37	< 0.5	10	33	20	3.00	1.72	0.61	445

CERTIFICATION: 



ALS Chemex

Aurora Laboratory Services Ltd.
 Analytical Chemists * Geochemists * Registered Assayers
 212 Brooksbank Ave., North Vancouver
 British Columbia, Canada V7J 2C1
 PHONE: 604-984-0221 FAX: 604-984-0218

To: GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

Page 1 of 1
 Total 12
 Certificate Date: 24-OCT-2000
 Invoice No. : 10031433
 P.O. Number :
 Account : CYO

Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

CERTIFICATE OF ANALYSIS A0031433

SAMPLE	PREP CODE	Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)			
VNA 0+00B	201 285	< 1	1.55	17	580	32	272	0.39	100	< 10	104			
VNA 0+25B	201 285	< 1	1.94	9	750	54	255	0.35	66	< 10	88			
VNA 0+50B	201 285	< 1	1.55	15	830	24	246	0.35	89	< 10	108			
VNA 0+75B	201 285	< 1	1.46	38	1560	38	856	0.38	68	< 10	140			
VNA 1+00B	201 285	1	2.20	4	760	16	228	0.33	45	< 10	70			
VNA 1+25B	201 285	< 1	1.95	7	970	20	206	0.31	46	< 10	88			
VNA 1+50B	201 285	1	1.81	15	1790	28	321	0.45	90	< 10	148			
VNA 1+75B	201 285	1	1.08	29	1250	184	483	0.27	63	< 10	184			
VNA 2+00B	201 285	1	1.64	23	750	32	264	0.31	77	< 10	190			
VNA 2+25B	201 285	1	1.54	12	780	28	203	0.27	59	< 10	94			
VNA 2+50B	201 285	< 1	1.51	10	600	24	233	0.27	64	< 10	84			
VNA 2+75B	201 285	< 1	2.00	11	830	22	216	0.33	56	< 10	88			
VNA 3+00B	201 285	< 1	1.64	19	710	24	253	0.26	63	< 10	84			
VNA 3+25B	201 285	< 1	1.63	23	1660	26	228	0.53	97	< 10	340			
VNA 3+50B	201 285	2	1.68	19	2690	24	202	0.59	99	< 10	178			
VNA 3+75B	201 285	1	2.01	22	1130	30	272	0.74	164	< 10	202			
VNA 4+00B	201 285	< 1	1.42	9	1160	26	199	0.30	64	< 10	116			
VNA 4+25B	201 285	2	5.03	45	4590	22	785	1.08	271	< 10	380			
VNA 4+50B	201 285	4	1.42	26	1560	30	206	0.46	105	< 10	224			
VNA 4+75B	201 285	4	1.63	11	2600	192	182	0.45	86	< 10	702			
VNA 5+00B	201 285	< 1	1.33	8	880	30	195	0.27	66	< 10	90			
VNA 0+00C	201 285	< 1	2.07	24	710	30	339	0.33	76	< 10	86			
VNA 1+00C	201 285	< 1	1.80	23	790	30	310	0.26	60	< 10	80			
VNA 2+00C	201 285	< 1	2.07	14	680	104	374	0.25	50	< 10	448			
VNA 3+00C	201 285	< 1	2.05	20	540	34	280	0.22	53	< 10	60			
VNA 4+00C	201 285	1	2.06	21	760	20	329	0.29	69	< 10	122			
VNA 4+50C	201 285	2	1.54	96	1200	22	285	0.60	110	< 10	210			
VNA 5+00C	201 285	< 1	1.95	12	720	22	344	0.24	49	< 10	60			
L70+00N 23+25E	201 285	1	2.05	14	1420	28	285	0.33	59	< 10	58			
L70+00N 23+50E	201 285	1	2.57	6	430	16	315	0.37	45	< 10	40			
L70+00N 23+75E	201 285	2	1.63	15	800	16	239	0.46	95	< 10	80			
L70+00N 24+00E	201 285	1	1.83	22	690	22	332	0.35	74	< 10	44			
L70+00N 24+50E	201 285	1	1.55	53	890	24	268	0.47	89	< 10	96			
L70+00N 24+75E	201 285	1	1.48	21	1200	34	242	0.32	65	< 10	100			
L70+00N 25+00E	201 285	< 1	1.68	11	650	18	259	0.40	80	< 10	62			
L70+00N 25+25E	201 285	< 1	1.83	13	780	16	392	0.29	71	< 10	40			
L70+00N 25+50E	201 285	< 1	1.50	8	720	14	225	0.27	60	< 10	44			
L70+00N 25+75E	201 285	< 1	1.74	7	350	18	305	0.26	65	< 10	32			
L70+50N 23+50E	201 285	1	1.42	12	670	16	225	0.31	71	< 10	72			
L70+50N 23+75E	201 285	1	1.69	12	940	20	279	0.32	68	< 10	60			

CERTIFICATION: _____



ALS Chemex

Aurora Laboratory Services Ltd.
 Analytical Chemists * Geochemists * Registered Assayers
 212 Brooksbank Ave., North Vancouver
 British Columbia, Canada V7J 2C1
 PHONE: 604-984-0221 FAX: 604-984-0218

Client: GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

Page: 2-A
 Total: 2
 Certificate Date: 24-OCT-2000
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CERTIFICATE OF ANALYSIS A0031433

SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
L70+50N 24+00E	201 285	< 0.2	7.37	620	2.0	< 2	1.22	< 0.5	6	33	11	2.67	1.88	0.48	395
L70+50N 24+25E	201 285	0.2	7.38	640	2.5	< 2	1.23	< 0.5	8	40	11	3.01	1.96	0.61	405
L70+50N 24+50E	201 285	< 0.2	6.78	660	2.0	< 2	1.28	< 0.5	5	19	12	1.81	1.88	0.38	335
L70+50N 24+75E	201 285	< 0.2	6.50	590	2.0	< 2	1.29	< 0.5	7	36	13	2.89	1.75	0.56	405
L70+50N 25+00E	201 285	< 0.2	6.38	680	2.0	< 2	1.34	< 0.5	7	34	8	2.11	2.13	0.44	340
L70+50N 25+25E	201 285	< 0.2	6.72	550	2.0	< 2	1.24	< 0.5	6	48	16	3.14	1.59	0.49	425
L70+50N 25+50E	201 285	< 0.2	6.91	640	2.0	< 2	1.22	< 0.5	7	43	8	3.57	1.93	0.54	365
L70+50N 25+75E	201 285	< 0.2	7.07	650	2.0	< 2	1.09	< 0.5	5	28	6	2.27	1.94	0.36	270
L71+00N 23+50E	201 285	0.6	6.78	540	2.0	< 2	1.24	< 0.5	8	33	23	2.09	1.54	0.47	390
L71+00N 23+75E	201 285	0.8	7.14	560	2.5	< 2	1.55	< 0.5	11	32	15	2.42	1.74	0.54	535
L71+00N 24+00E	201 285	< 0.2	7.02	540	2.5	< 2	1.16	< 0.5	8	30	19	2.11	1.55	0.42	350
L71+00N 24+50E	201 285	0.2	6.86	560	1.5	< 2	1.31	< 0.5	7	19	8	1.88	1.71	0.47	400
L71+00N 24+75E	201 285	0.2	6.80	570	2.5	< 2	1.77	< 0.5	7	28	9	2.52	1.73	0.56	450
L71+00N 25+00E	201 285	0.4	7.11	490	2.0	< 2	0.97	< 0.5	7	56	9	2.98	1.43	0.53	305
L71+00N 25+25E	201 285	1.6	7.87	560	3.0	< 2	1.19	< 0.5	7	31	10	2.93	1.58	0.49	380
L71+00N 25+50E	201 285	0.2	7.36	600	2.5	< 2	1.42	< 0.5	8	36	12	3.06	1.73	0.58	440
L71+00N 25+75E	201 285	0.2	7.05	620	2.0	< 2	1.31	0.5	6	33	14	1.98	1.68	0.38	430
L71+50N 23+50E	201 285	0.8	7.20	610	2.5	< 2	0.96	< 0.5	8	52	24	2.92	1.72	0.56	400
L71+50N 23+75E	-- --	NotRcd	NotRcd	NotRcd	NotRcd	NotRcd	NotRcd	NotRcd	NotRcd	NotRcd	NotRcd	NotRcd	NotRcd	NotRcd	NotRcd
L71+50N 24+00E	201 285	0.4	7.46	520	2.5	< 2	1.25	< 0.5	8	36	11	2.87	1.41	0.46	430
L71+50N 24+25E	201 285	< 0.2	6.91	570	3.0	< 2	1.46	< 0.5	8	32	13	2.33	1.67	0.50	435
L71+50N 24+50E	201 285	0.6	7.13	560	2.0	< 2	1.51	< 0.5	7	20	19	2.32	1.64	0.57	580
L71+50N 24+75E	201 285	< 0.2	7.45	530	2.5	< 2	1.45	< 0.5	7	38	13	3.33	1.57	0.60	415
L71+50N 25+00E	201 285	0.2	7.65	520	2.0	< 2	1.37	< 0.5	6	30	10	2.82	1.55	0.52	385
L71+50N 25+25E	201 285	0.4	7.49	540	1.5	< 2	1.53	< 0.5	7	29	12	2.26	1.63	0.50	425
L71+50N 25+75E	201 285	0.8	8.44	350	5.0	< 2	1.77	< 0.5	13	53	9	3.28	0.90	0.66	815
L71+50N 26+00E	201 285	< 0.2	7.42	690	2.0	< 2	1.30	< 0.5	7	32	7	2.58	2.06	0.52	340

CERTIFICATION: _____



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GEOQUEST CONSULTING LTD.

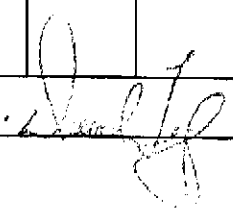
8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

Page: 2-B
 Total: 2
 Certificate Date: 24-OCT-2000
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CERTIFICATE OF ANALYSIS A0031433

SAMPLE	PREP CODE	Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)				
L70+50N 24+00E	201 285	3	2.06	7	330	20	292	0.39	73	< 10	46				
L70+50N 24+25E	201 285	1	1.75	11	420	24	279	0.34	76	< 10	56				
L70+50N 24+50E	201 285	1	2.31	5	290	18	301	0.35	53	< 10	36				
L70+50N 24+75E	201 285	< 1	1.77	14	400	22	289	0.33	67	< 10	46				
L70+50N 25+00E	201 285	< 1	1.87	8	170	20	323	0.31	73	< 10	32				
L70+50N 25+25E	201 285	1	1.86	18	480	24	278	0.33	75	< 10	38				
L70+50N 25+50E	201 285	< 1	1.68	10	330	20	280	0.42	95	< 10	46				
L70+50N 25+75E	201 285	< 1	1.69	4	230	22	269	0.39	72	< 10	20				
L71+00N 23+50E	201 285	3	1.98	10	820	22	266	0.32	51	< 10	46				
L71+00N 23+75E	201 285	< 1	1.75	11	530	22	319	0.32	63	< 10	36				
L71+00N 24+00E	201 285	< 1	1.79	15	290	18	265	0.26	49	< 10	36				
L71+00N 24+50E	201 285	< 1	2.63	5	260	14	287	0.36	52	< 10	44				
L71+00N 24+75E	201 285	1	2.31	10	360	22	311	0.51	95	< 10	48				
L71+00N 25+00E	201 285	1	1.48	15	620	22	202	0.40	80	< 10	78				
L71+00N 25+25E	201 285	< 1	1.86	10	750	20	271	0.32	65	< 10	68				
L71+00N 25+50E	201 285	< 1	1.92	12	820	22	308	0.36	73	< 10	88				
L71+00N 25+75E	201 285	1	2.61	7	470	34	284	0.44	57	< 10	76				
L71+50N 23+50E	201 285	< 1	1.63	20	360	52	248	0.29	67	< 10	56				
L71+50N 23+75E	-- --	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed				
L71+50N 24+00E	201 285	1	1.93	12	320	22	262	0.38	68	< 10	66				
L71+50N 24+25E	201 285	< 1	1.94	13	400	30	312	0.30	61	< 10	38				
L71+50N 24+50E	201 285	3	2.55	6	340	18	319	0.36	62	< 10	50				
L71+50N 24+75E	201 285	1	1.97	11	330	20	273	0.40	81	< 10	50				
L71+50N 25+00E	201 285	1	2.22	9	340	20	283	0.41	77	< 10	52				
L71+50N 25+25E	201 285	1	2.45	10	650	18	307	0.35	52	< 10	72				
L71+50N 25+75E	201 285	1	1.36	14	1420	40	194	0.31	65	< 10	192				
L71+50N 26+00E	201 285	< 1	1.99	9	210	24	284	0.43	88	< 10	88				

CERTIFICATION: 



ALS Chemex

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by: GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

Page 1 of 1-A
 Total 4
 Certificate Date: 25-OCT-2000
 Invoice No. : I0031547
 P.O. Number :
 Account : CYO

Project : PROJECT #86
 Comments : ATTN: WARNER GRUENWALD

CERTIFICATE OF ANALYSIS A0031547

SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
L68+00N 23+50E	201 285	0.4	7.86	530	2.5	< 2	0.98	< 0.5	7	40	12	2.82	1.59	0.42	385
L68+00N 23+75E	201 285	0.2	7.80	480	2.0	< 2	1.73	< 0.5	10	40	16	3.47	1.43	0.65	490
L68+00N 24+00E	201 285	0.2	7.44	550	2.5	< 2	1.40	< 0.5	7	35	11	2.58	1.83	0.48	390
L68+00N 24+25E	201 285	0.4	7.26	570	1.5	< 2	1.51	< 0.5	5	18	7	1.90	1.84	0.40	410
L68+00N 24+50E	201 285	0.2	7.53	640	2.0	< 2	1.36	< 0.5	7	38	10	2.38	2.00	0.54	415
L68+00N 24+75E	201 285	0.2	6.74	480	2.0	< 2	0.88	< 0.5	8	56	15	3.55	1.37	0.63	450
L68+00N 25+00E	201 285	0.2	6.83	610	2.0	< 2	1.06	< 0.5	7	32	13	3.18	1.73	0.47	530
L68+00N 25+25E	201 285	0.4	6.95	400	1.5	< 2	1.01	< 0.5	5	17	18	1.91	1.14	0.30	280
L68+00N 25+50E	201 285	0.2	7.16	470	1.5	< 2	1.28	< 0.5	4	17	9	1.93	1.42	0.34	315
L68+00N 25+75E	201 285	0.2	7.70	650	2.0	< 2	1.33	< 0.5	7	33	11	2.35	2.02	0.55	370
L68+00N 26+00E	201 285	0.2	6.87	650	2.0	< 2	1.07	< 0.5	6	30	8	3.00	1.93	0.47	385
L69+00N 23+50E	201 285	0.2	5.93	510	2.0	< 2	1.39	< 0.5	7	29	12	3.27	1.55	0.44	395
L69+00N 23+75E	201 285	0.2	6.67	600	1.5	< 2	1.18	< 0.5	5	23	15	2.60	1.77	0.41	340
L69+00N 24+00E	201 285	0.6	6.84	560	2.0	< 2	1.10	< 0.5	10	42	18	4.03	1.87	0.66	475
L69+00N 24+25E	201 285	0.4	7.32	570	2.0	< 2	1.47	< 0.5	6	16	9	1.80	1.75	0.54	390
L69+00N 24+50E	201 285	0.6	7.40	500	2.0	< 2	1.67	< 0.5	6	25	15	2.90	1.45	0.46	420
L69+00N 24+75E	201 285	0.2	7.02	530	1.5	< 2	1.55	< 0.5	7	27	16	3.62	1.54	0.66	470
L69+00N 25+00E	201 285	0.2	7.23	530	2.0	< 2	1.20	< 0.5	5	30	13	2.35	1.52	0.40	430
L69+00N 25+25E	201 285	0.2	6.84	540	2.0	< 2	1.27	< 0.5	7	32	16	2.69	1.58	0.53	385
L69+00N 25+50E	201 285	0.2	8.00	510	2.5	< 2	1.69	< 0.5	10	33	12	3.07	1.61	0.63	725
L69+00N 25+75E	201 285	< 0.2	7.31	210	1.0	< 2	0.38	< 0.5	3	16	9	2.30	0.61	0.11	130
L69+00N 26+00E	201 285	0.4	6.11	580	1.5	< 2	0.92	< 0.5	3	11	16	1.60	1.63	0.20	255
L69+50N 23+45E	201 285	0.8	6.42	530	2.0	< 2	1.45	< 0.5	10	36	17	4.52	1.65	0.67	480
L69+50N 23+75E	201 285	0.2	8.42	530	2.0	< 2	1.05	< 0.5	7	26	16	2.72	1.48	0.38	405
L69+50N 24+00E	201 285	0.4	7.34	600	1.5	< 2	1.38	< 0.5	7	39	11	2.68	1.83	0.54	415
L69+50N 24+25E	201 285	0.4	6.43	510	1.5	< 2	0.95	< 0.5	6	37	11	4.30	1.58	0.44	350
L69+50N 24+50E	201 285	0.2	6.81	440	1.5	8	1.04	< 0.5	5	13	14	1.80	1.19	0.31	310
L69+50N 24+75E	201 285	0.2	7.11	540	2.5	< 2	1.10	< 0.5	8	40	16	4.02	1.56	0.61	525
L69+50N 25+00E	201 285	0.6	7.21	620	2.0	< 2	1.43	< 0.5	7	32	13	3.12	1.78	0.57	460
L69+50N 25+25E	201 285	0.4	6.99	500	2.5	< 2	1.77	< 0.5	9	26	18	2.09	1.51	0.52	980
L69+50N 25+50E	201 285	0.2	6.73	440	1.5	< 2	0.79	< 0.5	4	22	15	2.34	1.28	0.24	275
L69+50N 25+75E	201 285	0.2	6.75	810	1.5	< 2	1.12	< 0.5	4	18	12	1.62	1.93	0.42	320
L75+00N 23+50E	201 285	0.4	7.74	650	2.0	< 2	1.47	< 0.5	8	34	9	2.65	1.86	0.56	470
L75+00N 23+75E	201 285	0.6	7.72	630	2.5	< 2	1.29	< 0.5	8	38	15	2.75	1.88	0.57	380
L75+00N 24+00E	201 285	0.2	7.40	560	2.5	< 2	1.69	< 0.5	6	22	10	2.41	1.78	0.55	405
L75+00N 24+25E	201 285	0.2	7.66	580	2.0	< 2	1.45	< 0.5	7	29	13	2.88	1.65	0.55	425
L75+00N 24+50E	201 285	0.4	8.23	580	3.5	< 2	1.69	< 0.5	9	45	25	3.61	1.64	0.63	415
L75+00N 24+75E	201 285	0.6	7.80	540	2.5	< 2	1.74	< 0.5	8	29	9	2.37	1.65	0.57	445
L75+00N 25+00E	201 285	0.4	7.90	560	2.0	< 2	1.37	< 0.5	6	27	12	2.50	1.48	0.44	410
L75+00N 25+25E	201 285	< 0.2	8.60	510	2.0	< 2	1.44	< 0.5	7	22	11	2.49	1.42	0.44	340

CERTIFICATION:



ALS Chemex

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o: GEOQUEST CONSULTING LTD.

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CERTIFICATE OF ANALYSIS

A0031547

SAMPLE	PREP CODE	Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)				
L68+00N 23+50E	201 285	< 1	1.67	11	660	18	235	0.26	60	< 10	52				
L68+00N 23+75E	201 285	< 1	2.23	14	430	18	282	0.48	87	< 10	70				
L68+00N 24+00E	201 285	1	1.86	9	450	18	300	0.28	61	< 10	56				
L68+00N 24+25E	201 285	1	2.54	4	290	12	331	0.30	50	< 10	34				
L68+00N 24+50E	201 285	< 1	1.86	11	530	14	324	0.29	70	< 10	54				
L68+00N 24+75E	201 285	< 1	1.39	18	850	18	214	0.30	72	< 10	56				
L68+00N 25+00E	201 285	< 1	1.72	8	580	16	246	0.33	70	< 10	70				
L68+00N 25+25E	201 285	1	1.72	5	830	10	214	0.24	38	< 10	30				
L68+00N 25+50E	201 285	2	2.14	2	370	14	280	0.28	45	< 10	32				
L68+00N 25+75E	201 285	< 1	1.83	8	390	14	330	0.30	70	< 10	36				
L68+00N 26+00E	201 285	< 1	1.84	8	240	18	287	0.31	68	< 10	34				
L69+00N 23+50E	201 285	2	1.49	9	480	20	253	0.47	85	< 10	42				
L69+00N 23+75E	201 285	< 1	1.96	6	510	18	268	0.39	64	< 10	40				
L69+00N 24+00E	201 285	1	1.63	15	950	22	242	0.32	87	< 10	64				
L69+00N 24+25E	201 285	< 1	2.53	5	530	16	315	0.35	49	< 10	38				
L69+00N 24+50E	201 285	2	1.80	8	1300	22	245	0.48	74	< 10	44				
L69+00N 24+75E	201 285	< 1	2.29	8	760	16	258	0.60	103	< 10	48				
L69+00N 25+00E	201 285	3	1.65	8	640	12	259	0.33	61	< 10	54				
L69+00N 25+25E	201 285	1	1.50	8	620	12	273	0.35	62	< 10	40				
L69+00N 25+50E	201 285	< 1	1.69	12	980	20	455	0.28	64	< 10	62				
L69+00N 25+75E	201 285	3	0.72	2	660	20	92	0.16	39	< 10	14				
L69+50N 26+00E	201 285	< 1	2.23	1	380	14	239	0.31	36	< 10	26				
L69+50N 23+45E	201 285	1	1.63	15	480	20	264	0.48	94	< 10	42				
L69+50N 23+75E	201 285	3	1.67	7	760	14	233	0.29	59	< 10	54				
L69+50N 24+00E	201 285	1	2.05	10	440	22	272	0.53	81	< 10	58				
L69+50N 24+25E	201 285	1	1.32	9	530	22	206	0.39	95	< 10	40				
L69+50N 24+50E	201 285	3	2.19	3	900	22	222	0.38	39	< 10	40				
L69+50N 24+75E	201 285	2	1.67	12	1540	24	226	0.42	93	< 10	78				
L69+50N 25+00E	201 285	< 1	1.96	10	840	20	272	0.43	80	< 10	64				
L69+50N 25+25E	201 285	1	1.73	14	1340	16	324	0.27	61	< 10	72				
L69+50N 25+50E	201 285	1	1.46	3	1040	18	192	0.28	54	< 10	30				
L69+50N 25+75E	201 285	1	2.69	7	370	18	411	0.44	59	< 10	34				
L75+00N 23+50E	201 285	< 1	2.23	11	490	20	309	0.40	77	< 10	98				
L75+00N 23+75E	201 285	1	1.86	16	440	22	285	0.33	74	< 10	76				
L75+00N 24+00E	201 285	< 1	2.46	9	240	26	328	0.35	72	< 10	46				
L75+00N 24+25E	201 285	< 1	2.03	13	440	48	289	0.35	72	< 10	96				
L75+00N 24+50E	201 285	< 1	1.76	28	500	30	281	0.41	85	< 10	484				
L75+00N 24+75E	201 285	1	2.56	8	360	20	311	0.42	66	< 10	80				
L75+00N 25+00E	201 285	1	2.57	7	590	26	285	0.48	64	< 10	104				
L75+00N 25+25E	201 285	1	2.43	6	430	22	277	0.40	60	< 10	74				

CERTIFICATION: 



ALS Chemex

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GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

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 Certificate Date: 25-OCT-2000
 Invoice No. : 10031547
 P.O. Number :
 Account : CYO

Project : PROJECT #86
 Comments : ATTN: WARNER GRUENWALD

CERTIFICATE OF ANALYSIS A0031547

SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
L75+00N 25+75E	201 285	< 0.2	7.99	420	3.5	< 2	1.48	< 0.5	8	58	13	4.60	1.00	0.48	445
L75+00N 26+00E	201 285	< 0.2	8.64	510	1.5	< 2	0.84	< 0.5	4	18	8	2.62	1.47	0.22	410
L75+00N 26+25E	201 285	0.8	6.84	630	1.5	< 2	1.24	< 0.5	3	16	6	1.33	2.04	0.32	305
L75+00N 26+50E	201 285	< 0.2	6.78	640	1.5	< 2	1.15	< 0.5	5	10	6	1.89	2.07	0.47	435
L75+00N 26+75E	201 285	< 0.2	7.24	750	2.0	< 2	1.22	< 0.5	6	33	8	2.53	2.36	0.60	450
L75+00N 27+00E	201 285	< 0.2	7.23	700	2.0	< 2	1.18	< 0.5	6	36	11	2.44	2.18	0.62	380
L75+50N 23+50E	201 285	< 0.2	7.33	570	1.5	< 2	1.49	< 0.5	7	18	8	2.35	1.89	0.59	395
L75+50N 23+75E	201 285	< 0.2	7.44	780	2.0	< 2	1.37	< 0.5	6	30	7	2.36	2.35	0.54	350
L75+50N 24+00E	201 285	< 0.2	7.22	700	2.5	< 2	1.16	< 0.5	11	44	17	3.42	2.09	0.68	425
L75+50N 24+25E	201 285	0.6	7.16	570	2.0	< 2	1.56	< 0.5	7	29	11	2.70	1.74	0.53	420
L75+50N 24+50E	201 285	0.8	8.00	550	2.0	< 2	1.24	< 0.5	10	33	11	3.34	1.68	0.45	470
L75+50N 24+75E	201 285	< 0.2	8.37	600	2.5	< 2	1.45	< 0.5	12	43	26	3.62	1.73	0.68	795
L75+50N 25+00E	201 285	0.6	8.59	560	2.5	< 2	0.96	< 0.5	8	40	21	3.65	1.55	0.50	330
L75+50N 25+25E	201 285	1.0	7.58	540	2.0	< 2	1.28	< 0.5	11	57	11	4.14	1.43	0.53	460
L75+50N 25+50E	201 285	< 0.2	7.35	480	1.5	< 2	1.40	< 0.5	6	22	10	2.82	1.41	0.47	420
L75+50N 25+75E	201 285	0.4	7.00	560	2.0	< 2	1.47	< 0.5	7	36	9	3.39	1.67	0.56	450
L75+50N 26+50E	201 285	< 0.2	6.62	630	2.0	< 2	1.08	< 0.5	6	32	8	2.42	1.98	0.51	370
L75+50N 26+75E	201 285	< 0.2	7.06	550	2.0	< 2	0.94	< 0.5	5	28	7	3.38	1.65	0.40	280
L75+50N 27+00E	201 285	< 0.2	8.09	660	2.5	< 2	0.91	< 0.5	12	52	30	3.93	2.08	0.99	635
L76+00N 23+50E	201 285	0.2	7.16	680	2.5	< 2	1.67	< 0.5	8	34	19	2.40	2.01	0.69	660
L76+00N 23+75E	201 285	< 0.2	8.01	680	3.0	< 2	1.34	< 0.5	13	35	34	2.89	1.55	0.69	830
L76+00N 24+00E	201 285	0.2	7.36	630	2.0	< 2	1.31	< 0.5	9	31	17	2.46	1.60	0.55	435
L76+00N 24+25E	201 285	< 0.2	6.63	600	2.0	< 2	1.44	< 0.5	6	28	9	2.39	1.84	0.42	400
L76+00N 24+50E	201 285	< 0.2	6.83	530	1.5	< 2	1.14	< 0.5	3	20	8	2.32	1.63	0.30	315
L76+00N 24+75E	201 285	0.6	7.00	580	2.0	< 2	1.41	< 0.5	6	35	8	2.12	1.94	0.46	365
L76+00N 25+00E	201 285	< 0.2	9.37	420	2.0	< 2	0.84	< 0.5	4	15	11	3.33	1.17	0.22	260
L76+00N 25+25E	201 285	< 0.2	7.86	480	2.5	< 2	1.22	< 0.5	6	39	12	3.11	1.72	0.51	345
L76+00N 25+50E	201 285	0.6	7.06	540	3.0	< 2	1.59	< 0.5	11	41	19	2.83	1.65	0.55	455
L76+00N 25+75E	201 285	< 0.2	7.46	510	1.5	< 2	1.00	< 0.5	5	30	9	2.72	1.57	0.36	330
L76+00N 26+25E	201 285	0.2	7.32	660	2.0	< 2	1.07	< 0.5	3	22	10	1.21	1.96	0.34	285
L76+00N 26+50E	201 285	< 0.2	7.20	510	2.0	< 2	0.97	< 0.5	4	23	7	2.52	1.44	0.34	310
L76+00N 26+75E	201 285	< 0.2	6.90	670	2.0	< 2	1.26	< 0.5	4	28	7	1.73	2.05	0.48	375
L76+00N 27+00E	201 285	< 0.2	6.71	660	2.0	< 2	1.15	< 0.5	7	36	11	3.62	2.17	0.56	440
L76+50N 23+50E	201 285	< 0.2	7.01	640	2.0	< 2	1.19	< 0.5	6	30	8	2.31	2.09	0.45	345
L76+50N 23+75E	201 285	< 0.2	7.23	570	2.5	< 2	1.09	< 0.5	8	33	14	2.90	1.76	0.50	470
L76+50N 24+00E	201 285	0.4	8.72	450	2.0	< 2	0.75	< 0.5	4	24	12	3.19	1.39	0.21	245
L76+50N 24+25E	201 285	< 0.2	7.94	460	2.5	< 2	0.95	< 0.5	6	29	9	3.55	1.44	0.31	275
L76+50N 24+50E	201 285	< 0.2	7.05	560	2.5	< 2	1.36	< 0.5	7	32	8	2.61	1.71	0.49	440
L76+50N 24+75E	201 285	1.0	7.49	420	1.5	< 2	1.00	< 0.5	3	10	10	2.39	1.30	0.27	315
L76+50N 25+00E	201 285	< 0.2	7.94	360	2.0	< 2	1.66	< 0.5	5	25	9	2.90	1.24	0.52	395

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8055 ASPEN RD.
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CERTIFICATE OF ANALYSIS A0031547

SAMPLE	PREP CODE	Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)				
L75+00N 25+75E	201 285	2	1.44	13	4670	44	155	0.62	120	< 10	174				
L75+00N 26+00E	201 285	2	1.93	2	1530	22	208	0.33	55	< 10	50				
L75+00N 26+25E	201 285	1	2.41	1	340	20	291	0.36	45	< 10	34				
L75+00N 26+50E	201 285	< 1	2.64	3	440	18	282	0.27	47	< 10	38				
L75+00N 26+75E	201 285	1	1.84	8	400	14	328	0.25	70	< 10	130				
L75+00N 27+00E	201 285	< 1	1.79	10	460	16	308	0.27	67	< 10	60				
L75+50N 23+50E	201 285	< 1	2.30	6	360	16	319	0.26	58	< 10	46				
L75+50N 23+75E	201 285	2	2.03	8	260	28	338	0.29	71	< 10	54				
L75+50N 24+00E	201 285	< 1	1.75	17	410	24	272	0.33	84	< 10	114				
L75+50N 24+25E	201 285	< 1	1.98	12	480	22	305	0.32	69	< 10	136				
L75+50N 24+50E	201 285	1	1.82	9	990	28	258	0.34	71	< 10	186				
L75+50N 24+75E	201 285	1	1.76	32	700	36	270	0.42	79	< 10	818				
L75+50N 25+00E	201 285	1	1.95	14	780	36	233	0.32	71	< 10	172				
L75+50N 25+25E	201 285	1	1.74	13	1860	36	227	0.64	122	< 10	256				
L75+50N 25+50E	201 285	1	2.50	5	2470	30	280	0.40	61	< 10	136				
L75+50N 25+75E	201 285	1	2.13	9	1290	82	303	0.39	83	< 10	366				
L75+50N 26+50E	201 285	1	1.55	7	690	16	277	0.23	66	< 10	42				
L75+50N 26+75E	201 285	2	1.17	6	710	20	227	0.26	73	< 10	96				
L75+50N 27+00E	201 285	2	1.35	20	790	24	243	0.34	108	< 10	112				
L76+00N 23+50E	201 285	1	1.85	12	660	24	359	0.28	73	< 10	46				
L76+00N 23+75E	201 285	< 1	1.68	24	670	28	291	0.28	69	< 10	88				
L76+00N 24+00E	201 285	1	1.88	19	290	24	290	0.31	65	< 10	78				
L76+00N 24+25E	201 285	5	2.05	7	400	22	308	0.38	80	< 10	62				
L76+00N 24+50E	201 285	1	2.13	3	450	22	253	0.43	67	< 10	44				
L76+00N 24+75E	201 285	< 1	1.99	8	620	24	274	0.42	70	< 10	76				
L76+00N 25+00E	201 285	2	1.87	3	1740	36	187	0.38	64	< 10	70				
L76+00N 25+25E	201 285	1	1.78	13	870	28	233	0.31	71	< 10	56				
L76+00N 25+50E	201 285	< 1	1.73	23	800	26	282	0.33	62	< 10	80				
L76+00N 25+75E	201 285	< 1	1.93	7	1540	30	236	0.39	72	< 10	70				
L76+00N 26+25E	201 285	< 1	2.22	3	840	18	275	0.37	50	< 10	36				
L76+00N 26+50E	201 285	< 1	1.66	3	850	16	243	0.28	57	< 10	42				
L76+00N 26+75E	201 285	< 1	1.96	6	580	14	326	0.32	60	< 10	42				
L76+00N 27+00E	201 285	< 1	1.60	9	550	26	295	0.29	83	< 10	42				
L76+50N 23+50E	201 285	< 1	1.68	8	540	18	299	0.23	64	< 10	78				
L76+50N 23+75E	201 285	< 1	1.59	16	800	46	240	0.26	64	< 10	542				
L76+50N 24+00E	201 285	< 1	1.88	1	2240	32	188	0.41	64	< 10	126				
L76+50N 24+25E	201 285	2	1.63	8	690	36	212	0.39	77	< 10	462				
L76+50N 24+50E	201 285	1	2.02	10	1040	30	277	0.33	63	< 10	356				
L76+50N 24+75E	201 285	< 1	2.24	2	710	24	219	0.35	48	< 10	90				
L76+50N 25+00E	201 285	1	2.40	5	650	24	301	0.35	53	< 10	100				

CERTIFICATION:



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SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
L76+50N 25+25E	201 285	< 0.2	7.79	560	4.0	< 2	1.60	< 0.5	8	47	13	3.96	1.75	0.56	400
L76+50N 25+50E	201 285	< 0.2	7.21	530	2.0	< 2	1.24	< 0.5	5	28	6	2.62	1.97	0.36	375
L76+50N 25+75E	-- --	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed
L76+50N 26+00E	201 285	< 0.2	8.13	580	2.0	< 2	0.96	< 0.5	6	41	12	2.66	1.58	0.40	850
L76+50N 26+25E	201 285	1.0	7.87	600	2.0	< 2	1.06	< 0.5	6	34	14	2.60	1.89	0.50	370
L76+50N 26+50E	201 285	< 0.2	7.80	490	2.0	< 2	0.75	< 0.5	6	30	11	3.14	1.46	0.33	420
L76+50N 26+75E	201 285	0.2	6.90	480	2.0	< 2	1.10	< 0.5	7	35	12	4.18	1.53	0.44	545
L76+50N 27+00E	201 285	0.6	6.74	690	2.5	2	1.14	< 0.5	7	36	10	2.65	2.22	0.55	495
L77+00N 23+50E	201 285	1.0	8.52	460	1.5	< 2	1.44	< 0.5	5	15	6	2.17	1.47	0.38	330
L77+00N 23+75E	201 285	< 0.2	7.73	540	2.0	< 2	1.49	< 0.5	7	19	6	2.09	1.67	0.47	415
L77+00N 24+00E	201 285	< 0.2	8.56	520	2.5	10	1.03	< 0.5	9	24	11	2.39	1.44	0.29	375
L77+00N 24+25E	201 285	< 0.2	8.09	630	3.0	< 2	1.19	< 0.5	12	47	24	3.63	1.90	0.71	405
L77+00N 24+50E	201 285	0.2	9.57	540	3.0	< 2	1.02	< 0.5	8	37	16	3.22	1.61	0.49	370
L77+00N 24+75E	201 285	< 0.2	8.90	370	2.5	< 2	1.20	< 0.5	6	26	7	3.31	1.16	0.39	290
L77+00N 25+00E	201 285	0.4	7.56	560	5.0	4	1.71	< 0.5	8	49	9	3.60	1.71	0.57	415
L77+00N 25+25E	201 285	0.4	7.75	550	5.5	4	1.84	< 0.5	8	42	9	3.37	1.73	0.52	405
L77+00N 25+50E	201 285	0.4	8.05	630	13.0	6	2.85	0.9	9	44	10	3.43	1.61	0.63	435
L77+00N 25+75E	201 285	< 0.2	8.14	700	2.5	< 2	1.06	< 0.5	11	45	13	3.02	2.25	0.71	400
L77+00N 26+00E	201 285	0.2	6.29	660	2.0	< 2	1.02	< 0.5	6	36	9	3.64	1.94	0.45	520
L77+00N 26+25E	201 285	0.8	8.67	460	2.0	< 2	0.84	< 0.5	5	27	13	2.77	1.39	0.27	325
L77+00N 26+50E	201 285	< 0.2	7.49	670	2.5	< 2	1.26	< 0.5	8	23	16	2.36	2.29	0.43	290
L77+00N 26+75E	201 285	< 0.2	7.39	550	2.0	< 2	1.03	< 0.5	7	42	13	3.77	1.82	0.54	455
L77+00N 27+00E	201 285	< 0.2	7.98	540	2.0	< 2	0.98	< 0.5	6	27	12	2.45	1.64	0.33	400
L84+00N 23+00E	201 285	< 0.2	7.46	490	2.0	< 2	1.53	< 0.5	11	17	9	2.27	1.37	0.41	410
L84+00N 23+25E	201 285	< 0.2	7.59	470	2.0	< 2	1.50	< 0.5	8	17	8	2.48	1.57	0.45	385
L84+00N 23+50E	201 285	< 0.2	8.06	650	3.0	< 2	1.15	< 0.5	6	25	7	2.54	2.14	0.39	285
L84+00N 23+75E	201 285	< 0.2	8.90	600	4.0	< 2	1.33	< 0.5	13	31	13	3.45	1.55	0.51	450
L84+00N 24+00E	201 285	< 0.2	11.65	330	6.5	< 2	0.67	< 0.5	29	33	36	2.72	1.08	0.61	930
L84+00N 24+50E	201 285	< 0.2	8.11	700	3.0	< 2	1.28	< 0.5	8	27	15	2.59	2.30	0.41	300
L84+00N 24+75E	201 285	< 0.2	8.15	700	3.0	< 2	1.25	< 0.5	8	27	15	2.64	2.14	0.42	305
L84+00N 25+00E	201 285	< 0.2	8.17	430	1.5	< 2	0.75	< 0.5	4	17	14	2.67	1.18	0.20	335
L85+50N 22+50E	201 285	< 0.2	8.25	680	2.5	< 2	1.11	< 0.5	10	29	14	2.54	2.04	0.46	300
L85+50N 22+75E	201 285	< 0.2	8.31	580	2.0	< 2	1.12	< 0.5	8	23	8	2.45	1.72	0.32	280
L85+50N 23+00E	201 285	< 0.2	7.93	520	2.0	2	1.09	< 0.5	5	25	8	3.29	1.62	0.35	290
L86+00N 22+25E	201 285	< 0.2	8.03	560	2.5	< 2	1.35	< 0.5	12	34	18	2.80	1.77	0.64	565
L86+00N 22+75E	201 285	< 0.2	8.45	440	2.0	< 2	1.53	< 0.5	5	15	6	2.68	1.56	0.45	310
L86+00N 23+50E	201 285	0.2	8.27	720	2.5	< 2	0.95	< 0.5	11	36	18	2.90	2.28	0.67	345
L86+50N 22+05E	201 285	0.8	7.97	640	2.0	< 2	1.24	< 0.5	11	32	15	2.58	1.86	0.49	310
L86+50N 22+25E	201 285	< 0.2	8.34	590	2.0	< 2	1.20	< 0.5	10	32	10	3.12	1.84	0.47	320
L86+50N 22+50E	201 285	< 0.2	9.01	510	3.0	< 2	1.20	< 0.5	8	30	9	3.25	1.97	0.44	275

CERTIFICATION: *[Signature]*



ALS Chemex

Aurora Laboratory Services Ltd.
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GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

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 Total F : 4
 Certificate Date: 25-OCT-2000
 Invoice No. : 10031547
 P.O. Number :
 Account : CYO

CERTIFICATE OF ANALYSIS A0031547

SAMPLE	PREP CODE	Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)			
L76+50N 25+25E	201 285	2	1.58	26	490	32	271	0.32	69	< 10	916			
L76+50N 25+50E	201 285	< 1	1.77	6	840	30	263	0.31	72	< 10	132			
L76+50N 25+75E	-- --	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed	NotRed			
L76+50N 26+00E	201 285	< 1	1.96	8	1950	34	209	0.39	65	< 10	170			
L76+50N 26+25E	201 285	< 1	1.83	9	840	28	262	0.32	64	< 10	112			
L76+50N 26+50E	201 285	1	1.27	7	1080	20	190	0.29	65	< 10	80			
L76+50N 26+75E	201 285	1	1.53	7	1240	26	245	0.31	81	< 10	48			
L76+50N 27+00E	201 285	< 1	1.68	11	680	26	299	0.29	70	< 10	46			
L77+00N 23+50E	201 285	< 1	2.29	3	460	16	308	0.30	48	< 10	82			
L77+00N 23+75E	201 285	1	2.25	6	640	24	329	0.31	49	< 10	116			
L77+00N 24+00E	201 285	< 1	1.94	7	1050	36	240	0.35	49	< 10	220			
L77+00N 24+25E	201 285	1	1.60	24	410	58	258	0.41	91	< 10	932			
L77+00N 24+50E	201 285	< 1	1.82	21	920	152	217	0.37	69	< 10	1500			
L77+00N 24+75E	201 285	1	1.80	6	940	60	225	0.36	75	< 10	392			
L77+00N 25+00E	201 285	2	1.65	12	1320	412	235	0.38	87	< 10	1155			
L77+00N 25+25E	201 285	< 1	1.73	11	980	208	255	0.35	80	< 10	1215			
L77+00N 25+50E	201 285	2	1.48	15	1210	88	254	0.38	83	< 10	2590			
L77+00N 25+75E	201 285	< 1	1.58	16	650	32	285	0.30	76	< 10	194			
L77+00N 26+00E	201 285	2	1.53	8	1880	16	265	0.32	93	< 10	80			
L77+00N 26+25E	201 285	< 1	1.92	5	1800	28	206	0.29	48	< 10	64			
L77+00N 26+50E	201 285	< 1	1.80	10	430	20	331	0.24	64	< 10	56			
L77+00N 26+75E	201 285	< 1	1.39	13	790	20	240	0.29	75	< 10	70			
L77+00N 27+00E	201 285	< 1	1.64	6	920	20	249	0.28	56	< 10	54			
L84+00N 23+00E	201 285	1	2.13	5	2180	24	274	0.38	48	< 10	126			
L84+00N 23+25E	201 285	1	2.25	6	740	22	316	0.34	59	< 10	76			
L84+00N 23+50E	201 285	< 1	1.72	9	1190	26	300	0.24	68	< 10	84			
L84+00N 23+75E	201 285	< 1	1.78	26	1370	36	256	0.38	80	< 10	634			
L84+00N 24+00E	201 285	2	0.71	58	1090	70	174	0.18	57	< 10	730			
L84+00N 24+50E	201 285	< 1	1.93	9	630	22	342	0.25	71	< 10	70			
L84+00N 24+75E	201 285	2	1.85	9	620	20	342	0.26	71	< 10	70			
L84+00N 25+00E	201 285	1	1.72	3	810	22	187	0.28	44	< 10	60			
L85+50N 22+50E	201 285	1	1.88	14	670	24	296	0.28	65	< 10	62			
L85+50N 22+75E	201 285	1	1.85	6	1230	18	279	0.30	57	< 10	72			
L85+50N 23+00E	201 285	< 1	1.51	7	1790	24	246	0.31	75	< 10	74			
L86+00N 22+25E	201 285	< 1	1.84	29	490	28	290	0.33	67	< 10	432			
L86+00N 22+75E	201 285	< 1	2.33	4	940	18	323	0.29	55	< 10	48			
L86+00N 23+50E	201 285	1	1.58	19	550	28	258	0.30	77	< 10	92			
L86+50N 22+05E	201 285	< 1	1.76	26	460	30	298	0.33	70	< 10	106			
L86+50N 22+25E	201 285	< 1	1.78	16	860	28	292	0.34	79	< 10	188			
L86+50N 22+50E	201 285	< 1	1.57	12	1610	32	293	0.34	76	< 10	282			

CERTIFICATION:



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Client: GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

Page: 4-A
 Total: 4
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CERTIFICATE OF ANALYSIS A0031547

SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
L86+50N 22+75E	201 285	< 0.2	7.34	680	2.0	< 2	1.14	< 0.5	6	32	14	2.78	2.07	0.54	320
L87+00N 21+75E	201 285	< 0.2	7.91	520	2.0	< 2	1.52	< 0.5	10	39	14	2.07	1.65	0.63	355
L87+00N 22+00E	201 285	< 0.2	7.66	540	2.0	< 2	1.42	< 0.5	7	28	7	2.83	1.76	0.61	385
L87+00N 22+15E	201 285	< 0.2	9.10	650	3.0	< 2	1.16	< 0.5	13	54	18	3.12	2.22	0.61	330
L87+00N 22+50E	201 285	0.2	8.88	560	2.0	< 2	1.07	< 0.5	7	31	14	2.95	1.65	0.41	290
L87+00N 22+75E	201 285	< 0.2	7.50	580	2.0	< 2	1.03	< 0.5	6	35	12	3.98	1.84	0.45	260
L87+50N 21+25E	201 285	< 0.2	7.66	560	2.0	< 2	1.97	< 0.5	10	33	11	2.41	1.82	0.70	420
L87+50N 21+50E	201 285	< 0.2	7.58	680	2.5	< 2	1.56	< 0.5	7	24	9	2.10	2.34	0.57	310
L87+50N 22+00E	201 285	< 0.2	8.64	560	2.5	< 2	1.24	< 0.5	13	36	16	2.92	1.67	0.52	435
L88+00N 21+00E	201 285	< 0.2	8.22	740	2.5	< 2	1.61	< 0.5	8	32	13	2.51	2.33	0.60	370
L88+00N 21+25E	201 285	0.2	8.13	600	2.0	< 2	1.71	< 0.5	7	23	8	2.63	2.03	0.58	400
L88+00N 21+50E	201 285	< 0.2	8.50	400	1.5	< 2	1.65	< 0.5	6	14	7	2.70	1.41	0.48	365
L88+00N 21+75E	201 285	< 0.2	7.73	590	2.0	< 2	1.54	< 0.5	11	28	13	2.37	1.86	0.55	415
L88+00N 22+00E	201 285	0.2	9.01	450	1.5	< 2	1.18	< 0.5	4	14	12	2.58	1.38	0.35	290
L88+00N 22+25E	201 285	0.4	8.02	640	2.0	< 2	1.32	< 0.5	12	28	20	2.94	2.03	0.55	350
L88+00N 22+50E	201 285	< 0.2	8.44	640	2.5	< 2	1.24	< 0.5	8	39	16	3.60	1.98	0.53	335

CERTIFICATION:



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8055 ASPEN RD.
 VERNON, BC
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 Account : CYO

Project : PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

CERTIFICATE OF ANALYSIS	A0031547
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SAMPLE	PREP CODE	Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)				
L86+50N 22+75E	201 285	< 1	1.78	12	520	24	289	0.32	74	< 10	380				
L87+00N 21+75E	201 285	1	1.90	19	340	20	318	0.34	77	< 10	194				
L87+00N 22+00E	201 285	1	2.26	13	540	92	312	0.36	68	< 10	1090				
L87+00N 22+15E	201 285	3	1.68	21	850	32	283	0.35	90	< 10	584				
L87+00N 22+50E	201 285	< 1	1.85	10	1240	36	262	0.36	77	< 10	328				
L87+00N 22+75E	201 285	1	1.43	10	930	26	262	0.32	103	< 10	96				
L87+50N 21+25E	201 285	< 1	2.25	17	320	26	378	0.38	70	< 10	104				
L87+50N 21+50E	201 285	< 1	2.08	9	230	22	384	0.25	66	< 10	96				
L87+50N 22+00E	201 285	< 1	1.93	19	1140	28	281	0.38	75	< 10	126				
L88+00N 21+00E	201 285	3	1.94	11	330	30	392	0.30	82	< 10	82				
L88+00N 21+25E	201 285	< 1	2.38	8	720	20	381	0.36	78	< 10	76				
L88+00N 21+50E	201 285	1	2.50	3	1130	14	331	0.35	63	< 10	64				
L88+00N 21+75E	201 285	1	2.16	15	520	26	342	0.31	64	< 10	180				
L88+00N 22+00E	201 285	< 1	2.20	3	960	18	264	0.36	55	< 10	48				
L88+00N 22+25E	201 285	< 1	1.85	18	900	16	327	0.30	78	< 10	72				
L88+00N 22+50E	201 285	1	1.70	13	800	22	311	0.34	90	< 10	66				

CERTIFICATION:



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o: GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

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 Invoice No.: I0031747
 P.O. Number:
 Account: CYO

CERTIFICATE OF ANALYSIS A0031747

SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
L72+00N 23+50E	201 202	0.6	7.92	470	4.0	< 2	1.55	< 0.5	15	37	38	3.37	1.42	0.65	500
L72+00N 23+75E	201 202	< 0.2	7.36	480	2.0	< 2	0.99	< 0.5	7	46	9	3.45	1.42	0.42	320
L72+00N 24+00E	201 202	< 0.2	6.42	480	1.5	< 2	1.13	< 0.5	6	37	12	3.40	1.35	0.45	360
L72+00N 24+25E	201 202	< 0.2	7.21	430	2.0	< 2	1.00	< 0.5	7	38	12	3.65	1.26	0.43	335
L72+00N 24+50E	201 202	2.4	7.55	620	2.5	< 2	1.33	< 0.5	7	61	16	4.69	1.78	0.88	435
L72+00N 24+75E	201 202	< 0.2	7.18	610	2.5	< 2	1.16	< 0.5	8	54	14	3.64	1.94	0.58	395
L72+00N 25+00E	201 202	< 0.2	7.66	500	2.5	< 2	0.96	< 0.5	9	72	16	3.96	1.65	0.65	340
L72+00N 25+50E	201 202	< 0.2	8.12	610	2.0	< 2	1.01	0.5	7	39	13	2.91	1.96	0.57	350
L72+00N 25+75E	201 202	< 0.2	7.16	610	1.5	< 2	1.05	< 0.5	9	19	14	1.93	1.74	0.34	420
L72+00N 26+00E	201 202	< 0.2	7.82	470	2.0	< 2	1.19	< 0.5	8	44	15	3.53	1.47	0.50	400
L72+00N 26+25E	201 202	< 0.2	7.11	520	2.0	< 2	1.66	< 0.5	7	31	15	2.58	1.50	0.47	370
L72+50N 23+25E	201 202	< 0.2	7.65	530	3.0	< 2	1.40	< 0.5	11	41	17	3.45	1.51	0.62	435
L72+50N 23+50E	201 202	< 0.2	7.69	530	2.0	< 2	1.13	< 0.5	8	37	11	3.09	1.53	0.48	350
L72+50N 23+75E	201 202	< 0.2	7.67	570	2.5	< 2	1.22	< 0.5	9	38	15	2.79	1.63	0.62	425
L72+50N 24+00E	201 202	< 0.2	6.83	540	2.0	< 2	1.23	< 0.5	7	71	11	2.62	1.73	0.61	405
L72+50N 24+25E	201 202	< 0.2	8.12	700	2.5	< 2	1.37	< 0.5	13	52	21	4.00	2.03	0.87	490
L72+50N 24+50E	201 202	1.0	8.41	420	2.0	< 2	1.11	< 0.5	6	37	14	3.05	1.21	0.48	360
L72+50N 24+75E	201 202	< 0.2	7.27	620	2.0	< 2	1.24	< 0.5	13	83	13	3.53	1.92	0.82	420
L72+50N 25+00E	201 202	< 0.2	7.01	540	2.0	< 2	1.04	< 0.5	7	73	11	4.08	1.60	0.50	315
L72+50N 25+50E	201 202	< 0.2	7.39	570	2.0	< 2	1.13	< 0.5	8	37	15	3.86	1.71	0.58	515
L72+50N 25+75E	201 202	0.2	7.41	480	1.5	< 2	1.14	< 0.5	6	27	11	2.28	1.67	0.40	465
L72+50N 26+00E	201 202	< 0.2	7.42	480	1.5	< 2	1.56	< 0.5	5	12	9	1.60	1.59	0.51	385
L72+50N 26+25E	201 202	0.4	6.52	640	2.0	< 2	1.11	< 0.5	8	37	11	3.58	1.84	0.51	385
L72+50N 26+50E	201 202	0.6	6.78	630	1.5	< 2	1.15	< 0.5	7	50	11	2.42	1.65	0.43	300
L73+00N 23+50E	201 202	< 0.2	7.44	610	2.0	< 2	1.39	< 0.5	7	40	9	2.50	1.85	0.54	430
L73+00N 23+75E	201 202	< 0.2	6.53	590	1.5	< 2	1.07	< 0.5	6	42	12	2.52	1.67	0.42	325
L73+00N 24+00E	201 202	0.6	6.93	640	2.0	< 2	1.42	< 0.5	6	24	9	1.82	2.03	0.60	515
L73+00N 24+50E	201 202	< 0.2	6.91	560	2.0	< 2	1.37	< 0.5	6	36	10	2.38	1.81	0.59	370
L73+00N 24+75E	201 202	0.2	6.87	560	2.0	< 2	1.35	< 0.5	6	33	9	2.17	1.74	0.57	395
L73+00N 25+00E	201 202	< 0.2	8.43	610	2.0	< 2	1.13	< 0.5	10	70	13	4.32	1.56	0.81	350
L73+00N 25+50E	201 202	< 0.2	7.24	530	2.0	< 2	1.12	< 0.5	5	22	12	2.47	1.58	0.36	340
L73+00N 25+75E	201 202	< 0.2	9.37	360	1.5	< 2	1.49	< 0.5	6	8	10	2.25	1.22	0.47	365
L73+00N 26+00E	201 202	< 0.2	7.50	560	1.5	< 2	0.97	< 0.5	6	31	11	2.51	1.69	0.40	895
L73+00N 26+25E	201 202	< 0.2	7.87	520	1.5	< 2	0.87	< 0.5	4	23	9	2.48	1.36	0.38	360
L73+00N 26+50E	201 202	< 0.2	7.50	610	2.0	< 2	0.93	< 0.5	4	29	11	2.41	1.80	0.40	275
L73+50N 23+50E	201 202	< 0.2	7.74	590	2.5	< 2	1.30	< 0.5	11	32	15	2.61	0.69	0.57	395
L73+50N 23+75E	201 202	0.2	8.34	570	2.5	< 2	1.31	< 0.5	11	36	25	3.42	1.66	0.59	390
L73+50N 24+00E	201 202	< 0.2	7.07	640	2.0	< 2	1.48	< 0.5	7	30	9	2.38	1.83	0.63	435
L73+50N 24+25E	201 202	< 0.2	7.18	620	2.5	< 2	1.46	< 0.5	9	38	10	2.60	1.91	0.67	405
L73+50N 24+50E	201 202	< 0.2	7.67	560	2.5	< 2	1.26	< 0.5	8	41	12	2.98	1.83	0.55	395

CERTIFICATION:



ALS Chemex

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A0031747

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L72+00N 23+50E	201 202	< 1	1.91	24	760	26	288	0.30	60	< 10	62				
L72+00N 23+75E	201 202	1	1.50	9	640	24	199	0.43	97	< 10	70				
L72+00N 24+00E	201 202	< 1	1.57	10	1300	22	210	0.37	79	< 10	54				
L72+00N 24+25E	201 202	1	1.65	8	1120	16	188	0.46	82	< 10	70				
L72+00N 24+50E	201 202	1	2.08	10	810	44	252	0.57	144	< 10	122				
L72+00N 24+75E	201 202	1	1.84	17	700	26	238	0.43	96	< 10	100				
L72+00N 25+00E	201 202	< 1	1.63	24	810	18	211	0.32	73	< 10	80				
L72+00N 25+50E	201 202	< 1	1.85	8	1180	18	235	0.36	74	< 10	68				
L72+00N 25+75E	201 202	2	2.72	4	1760	24	255	0.42	48	< 10	42				
L72+00N 26+00E	201 202	1	1.60	10	960	14	221	0.34	76	< 10	82				
L72+00N 26+25E	201 202	1	2.48	7	500	16	250	0.41	59	< 10	82				
L72+50N 23+25E	201 202	< 1	1.71	21	870	18	272	0.34	72	< 10	54				
L72+50N 23+50E	201 202	< 1	2.07	9	880	18	250	0.37	71	< 10	68				
L72+50N 23+75E	201 202	< 1	1.91	16	830	14	259	0.31	66	< 10	60				
L72+50N 24+00E	201 202	< 1	2.13	16	600	14	265	0.28	59	< 10	38				
L72+50N 24+25E	201 202	< 1	1.95	26	1010	24	295	0.51	106	< 10	146				
L72+50N 24+50E	201 202	1	2.05	10	880	14	222	0.32	56	< 10	72				
L72+50N 24+75E	201 202	< 1	1.88	25	580	30	242	0.55	107	< 10	222				
L72+50N 25+00E	201 202	1	1.61	22	820	22	207	0.31	73	< 10	62				
L72+50N 25+50E	201 202	1	2.03	11	520	54	246	0.41	87	< 10	156				
L72+50N 25+75E	201 202	< 1	2.23	6	770	22	237	0.34	57	< 10	72				
L72+50N 26+00E	201 202	1	3.12	1	410	8	319	0.32	33	< 10	46				
L72+50N 26+25E	201 202	< 1	1.67	11	500	16	273	0.31	100	< 10	40				
L72+50N 26+50E	201 202	1	1.69	13	340	20	240	0.42	98	< 10	60				
L73+00N 23+50E	201 202	< 1	2.19	10	960	14	289	0.35	66	< 10	62				
L73+00N 23+75E	201 202	1	1.87	8	600	24	237	0.51	79	< 10	80				
L73+00N 24+00E	201 202	< 1	2.64	8	360	14	311	0.40	56	< 10	54				
L73+00N 24+50E	201 202	< 1	2.22	10	440	18	277	0.36	72	< 10	62				
L73+00N 24+75E	201 202	< 1	2.43	9	480	14	276	0.39	61	< 10	52				
L73+00N 25+00E	201 202	< 1	1.99	19	1820	18	305	0.47	110	< 10	86				
L73+00N 25+50E	201 202	< 1	2.36	6	580	20	244	0.45	68	< 10	58				
L73+00N 25+75E	201 202	< 1	2.79	3	530	10	293	0.29	38	< 10	40				
L73+00N 26+00E	201 202	1	2.11	7	1170	20	235	0.35	59	< 10	78				
L73+00N 26+25E	201 202	1	2.23	6	710	28	220	0.29	54	< 10	58				
L73+00N 26+50E	201 202	< 1	1.79	7	300	20	236	0.34	70	< 10	26				
L73+50N 23+50E	201 202	< 1	2.07	13	390	18	269	0.32	62	< 10	52				
L73+50N 23+75E	201 202	3	1.83	17	600	22	255	0.38	76	< 10	66				
L73+50N 24+00E	201 202	< 1	2.34	9	530	16	318	0.44	74	< 10	50				
L73+50N 24+25E	201 202	1	2.31	12	410	16	307	0.39	72	< 10	76				
L73+50N 24+50E	201 202	< 1	2.13	11	620	24	263	0.43	80	< 10	96				

CERTIFICATION: _____



ALS Chemex

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GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

Page: 2-A
 Total Pages: 3
 Certificate Date: 31-OCT-2000
 Invoice No.: 10031747
 P.O. Number:
 Account: CYO

Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

CERTIFICATE OF ANALYSIS A0031747

SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
L73+50N 24+75E	201 202	< 0.2	7.60	560	3.5	< 2	1.22	< 0.5	6	33	8	2.28	2.04	0.50	355
L73+50N 25+00E	201 202	< 0.2	8.24	450	2.5	< 2	1.02	< 0.5	7	28	12	2.87	1.47	0.40	305
L73+50N 25+50E	201 202	< 0.6	7.53	420	2.0	< 2	1.61	< 0.5	12	37	19	4.56	1.20	0.73	720
L73+50N 25+75E	201 202	< 0.2	7.98	630	2.5	< 2	1.38	< 0.5	9	28	13	2.68	1.69	0.60	460
L73+50N 26+00E	201 202	< 0.2	7.85	570	1.5	2	1.08	< 0.5	7	31	19	2.92	1.77	0.50	430
L73+50N 26+25E	201 202	< 0.2	8.74	460	2.0	< 2	0.70	< 0.5	7	35	13	3.11	1.36	0.29	530
L73+50N 26+50E	201 202	< 0.2	6.31	700	1.5	< 2	0.89	< 0.5	3	27	8	1.09	1.95	0.23	205
L74+00N 23+50E	201 202	< 0.2	8.01	520	2.0	< 2	1.82	< 0.5	7	24	15	2.27	1.65	0.56	445
L74+00N 23+75E	201 202	< 0.2	8.31	460	2.0	< 2	1.89	< 0.5	9	21	16	2.52	1.39	0.65	470
L74+00N 24+00E	201 202	< 0.2	7.55	600	2.0	< 2	1.40	< 0.5	8	31	18	2.62	1.76	0.47	365
L74+00N 24+25E	201 202	< 0.2	7.42	530	2.0	< 2	1.37	< 0.5	6	40	11	4.17	1.54	0.54	445
L74+00N 24+50E	201 202	< 0.2	7.08	500	2.5	< 2	2.67	< 0.5	19	66	12	4.68	1.55	1.33	675
L74+00N 24+75E	201 202	1.4	8.17	530	2.0	< 2	1.18	< 0.5	6	27	14	3.02	1.62	0.38	340
L74+00N 25+00E	201 202	2.4	7.52	580	3.0	< 2	1.25	< 0.5	9	51	12	3.17	1.76	0.60	375
L74+00N 25+25E	201 202	1.6	7.87	500	2.5	< 2	1.54	< 0.5	5	20	9	2.37	1.50	0.50	365
L74+00N 25+50E	201 202	< 0.2	7.51	490	2.5	< 2	1.47	< 0.5	11	31	14	2.83	1.40	0.49	570
L74+00N 25+75E	201 202	< 0.2	8.69	600	2.0	< 2	1.27	< 0.5	7	26	15	2.71	1.60	0.45	460
L74+00N 26+00E	201 202	< 0.2	8.32	380	1.5	< 2	2.09	< 0.5	16	56	22	3.56	1.18	0.87	610
L74+00N 26+25E	201 202	< 0.2	8.11	590	2.0	< 2	1.10	< 0.5	8	36	11	2.43	1.68	0.39	480
L74+00N 26+50E	201 202	< 0.2	6.44	650	2.0	< 2	1.02	0.5	5	27	8	2.07	1.74	0.34	270
L74+50N 23+50E	201 202	< 0.2	7.74	620	2.0	< 2	1.37	< 0.5	8	32	14	3.04	1.80	0.67	415
L74+50N 23+75E	201 202	< 0.2	7.79	390	1.5	< 2	1.85	< 0.5	7	14	8	2.34	1.33	0.59	425
L74+50N 24+00E	201 202	< 0.2	7.91	540	2.5	< 2	1.21	< 0.5	7	31	12	2.75	1.51	0.44	345
L74+50N 24+25E	201 202	< 0.2	7.13	680	2.0	< 2	1.36	< 0.5	4	24	23	1.75	1.92	0.41	420
L74+50N 24+50E	201 202	< 0.2	7.86	590	3.0	< 2	1.31	< 0.5	11	50	22	3.74	1.65	0.64	390
L74+50N 24+75E	201 202	< 0.2	8.61	460	2.5	< 2	1.32	< 0.5	8	22	10	2.85	1.35	0.52	420
L74+50N 25+00E	201 202	< 0.2	7.34	570	3.0	< 2	1.48	< 0.5	7	32	9	2.54	1.66	0.61	390
L74+50N 25+25E	201 202	< 0.2	7.08	550	4.0	< 2	1.34	< 0.5	6	44	12	3.19	1.59	0.48	330
L74+50N 25+75E	201 202	< 0.2	7.62	590	2.0	< 2	0.99	0.5	11	46	12	3.73	1.74	0.53	410
L74+50N 26+00E	201 202	< 0.2	7.91	470	1.5	< 2	0.91	< 0.5	4	22	8	2.32	1.50	0.26	410
L74+50N 26+25E	201 202	< 0.2	7.92	390	1.5	< 2	1.59	< 0.5	6	10	9	2.03	1.35	0.52	520
L74+50N 26+50E	201 202	< 0.2	8.10	530	2.0	< 2	1.11	< 0.5	4	24	9	2.47	1.56	0.34	275
VNA 5+25B	201 202	< 0.2	8.80	420	1.5	< 2	1.21	< 0.5	4	15	7	2.07	1.44	0.35	380
VNA 5+50B	201 202	< 0.2	7.31	520	2.0	< 2	1.08	< 0.5	7	29	8	2.39	1.68	0.39	590
VNA 5+75B	201 202	< 0.2	8.34	540	2.0	< 2	0.88	< 0.5	5	29	10	2.32	1.64	0.36	310
VNA 6+00B	201 202	< 0.2	7.12	600	2.5	< 2	1.13	< 0.5	10	46	15	2.86	2.15	0.70	455
VNA 6+25B	201 202	< 0.2	7.80	580	2.5	< 2	1.10	< 0.5	9	45	13	3.15	1.76	0.57	440
VNA 6+25C	201 202	< 0.2	7.64	520	2.0	< 2	1.25	< 0.5	7	23	10	2.31	1.54	0.42	510
VNA 6+50B	201 202	< 0.2	9.00	600	2.5	< 2	1.00	< 0.5	7	34	14	2.77	1.82	0.38	325
VNA 6+75B	201 202	< 0.2	8.32	670	2.0	< 2	0.97	< 0.5	9	35	11	2.42	2.05	0.47	330

CERTIFICATION:



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GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

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 Total Pages: 3
 Certificate Date: 31-OCT-2000
 Invoice No.: 10031747
 P.O. Number:
 Account: CYO

CERTIFICATE OF ANALYSIS A0031747

SAMPLE	PREP CODE	Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)			
L73+50N 24+75E	201 202	< 1	2.31	8	370	22	263	0.35	66	< 10	100			
L73+50N 25+00E	201 202	< 1	1.91	8	990	18	221	0.30	64	< 10	54			
L73+50N 25+50E	201 202	< 1	2.13	10	1640	18	255	0.57	110	< 10	90			
L73+50N 25+75E	201 202	< 1	2.19	10	720	16	288	0.34	64	< 10	72			
L73+50N 26+00E	201 202	< 2	2.21	9	1620	16	256	0.38	73	< 10	50			
L73+50N 26+25E	201 202	< 1	1.36	6	840	30	172	0.29	67	< 10	66			
L73+50N 26+50E	201 202	< 1	1.74	4	300	16	247	0.32	50	< 10	20			
L74+00N 23+50E	201 202	< 3	2.67	15	610	10	326	0.34	49	< 10	60			
L74+00N 23+75E	201 202	< 1	2.46	10	870	10	344	0.31	55	< 10	86			
L74+00N 24+00E	201 202	< 1	2.16	7	830	18	286	0.40	72	< 10	60			
L74+00N 24+25E	201 202	< 2	2.38	10	1060	22	275	0.70	114	< 10	84			
L74+00N 24+50E	201 202	< 1	2.15	23	1350	16	311	1.16	146	< 10	150			
L74+00N 24+75E	201 202	< 1	2.42	6	720	18	267	0.37	64	< 10	52			
L74+00N 25+00E	201 202	< 1	1.97	16	930	14	274	0.35	77	< 10	78			
L74+00N 25+25E	201 202	< 1	2.53	5	590	14	314	0.32	52	< 10	54			
L74+00N 25+50E	201 202	< 1	2.25	12	840	18	239	0.46	70	< 10	268			
L74+00N 25+75E	201 202	< 1	2.41	7	860	12	274	0.35	62	< 10	70			
L74+00N 26+00E	201 202	< 1	1.80	23	1540	14	188	0.49	105	< 10	78			
L74+00N 26+25E	201 202	< 1	2.14	8	1000	16	255	0.33	56	< 10	100			
L74+00N 26+50E	201 202	< 1	1.68	6	350	12	258	0.31	61	< 10	34			
L74+50N 23+50E	201 202	< 1	2.14	8	530	16	293	0.35	74	< 10	72			
L74+50N 23+75E	201 202	< 1	2.78	5	340	8	340	0.34	45	< 10	44			
L74+50N 24+00E	201 202	< 1	2.13	9	550	16	252	0.35	57	< 10	72			
L74+50N 24+25E	201 202	< 1	2.85	5	360	14	312	0.40	56	< 10	68			
L74+50N 24+50E	201 202	< 1	2.06	15	880	18	280	0.46	90	< 10	158			
L74+50N 24+75E	201 202	< 1	2.55	8	1060	16	281	0.40	58	< 10	90			
L74+50N 25+00E	201 202	< 1	2.40	10	640	16	310	0.42	66	< 10	92			
L74+50N 25+25E	201 202	< 1	1.86	14	1140	16	268	0.37	76	< 10	70			
L74+50N 25+75E	201 202	< 1	1.77	17	950	18	236	0.37	82	< 10	98			
L74+50N 26+00E	201 202	< 1	2.20	3	1170	24	210	0.35	55	< 10	40			
L74+50N 26+25E	201 202	< 1	2.92	3	990	6	318	0.29	35	< 10	46			
L74+50N 26+50E	201 202	< 1	2.15	5	750	12	267	0.27	52	< 10	40			
VNA 5+25B	201 202	< 1	2.37	3	570	16	255	0.29	43	< 10	52			
VNA 5+50B	201 202	< 1	1.79	8	2070	22	237	0.26	53	< 10	70			
VNA 5+75B	201 202	< 1	1.86	6	740	14	215	0.28	51	< 10	74			
VNA 6+00B	201 202	< 1	1.96	20	670	62	271	0.34	68	< 10	220			
VNA 6+25B	201 202	< 1	1.71	15	1140	56	246	0.32	65	< 10	316			
VNA 6+25C	201 202	< 1	2.35	6	1160	18	278	0.30	52	< 10	128			
VNA 6+50B	201 202	< 1	2.12	8	770	62	253	0.31	60	< 10	326			
VNA 6+75B	201 202	< 1	2.07	11	550	18	259	0.33	60	< 10	114			

CERTIFICATION:



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GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

Project: PROJECT #86
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 Invoice No.: I0031747
 P.O. Number :
 Account : CYO

CERTIFICATE OF ANALYSIS A0031747

SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
VNA 7-00B	201 202	1.8	8.36	540	2.5	< 2	0.98	< 0.5	8	38	12	3.49	1.65	0.47	330
VNA 7-00C	201 202	< 0.2	7.54	690	2.5	< 2	1.17	< 0.5	8	38	14	2.50	2.06	0.66	365
VNA 7-25B	201 202	< 0.2	8.49	630	2.5	< 2	1.09	0.5	10	34	10	2.60	2.00	0.44	380
VNA 7-50B	201 202	0.4	8.84	620	2.5	< 2	1.09	< 0.5	10	40	12	2.45	1.87	0.44	360

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Client: GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
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CERTIFICATE OF ANALYSIS

A0031747

SAMPLE	PREP CODE	Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)				
VNA 7+00B	201 202	< 1	1.52	11	1060	14	242	0.24	70	< 10	118				
VNA 7+00C	201 202	< 1	1.93	14	590	14	299	0.24	64	< 10	98				
VNA 7+25B	201 202	< 1	1.76	9	770	12	277	0.24	59	< 10	78				
VNA 7+50B	201 202	< 1	2.03	12	630	14	262	0.30	58	< 10	128				

CERTIFICATION: _____



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To: GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
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Project: PROJECT #86
Comments: ATTN: WARNER GRUENWALD

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Total: 5
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CERTIFICATE OF ANALYSIS A0031990

SAMPLE	PREP CODE		Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
	L42+00N 11+00E	201	202	< 0.2	8.09	660	3.0	< 2	0.77	< 0.5	8	51	13	3.71	2.46	0.67
L42+00N 11+30E	201	202	< 0.2	8.25	710	2.5	< 2	0.81	< 0.5	9	46	20	2.54	3.02	0.71	425
L42+00N 11+30E B	201	202	< 0.2	7.24	490	2.0	< 2	0.54	< 0.5	4	34	8	2.99	1.95	0.37	245
L42+00N 11+50E	201	202	0.4	6.97	380	1.5	< 2	0.63	0.5	4	28	10	3.31	1.80	0.30	235
L42+00N 11+75E	201	202	< 0.2	7.43	510	1.5	< 2	0.88	0.5	4	23	7	2.34	2.17	0.35	290
L42+00N 12+00E	201	202	0.2	6.78	470	1.5	< 2	1.10	< 0.5	5	22	9	2.71	1.71	0.39	290
L42+00N 12+25E	201	202	0.2	7.40	480	2.0	< 2	0.76	< 0.5	4	24	8	2.37	1.92	0.32	305
L43+00N 11+00E	201	202	0.4	8.33	500	2.0	< 2	0.63	< 0.5	5	38	11	2.76	2.05	0.48	345
L43+00N 11+00E C	201	202	< 0.2	8.09	700	3.0	< 2	0.79	< 0.5	10	45	19	2.47	2.93	0.70	470
L43+00N 11+25	201	202	0.2	7.76	520	2.0	< 2	0.68	< 0.5	4	25	6	2.70	2.00	0.30	260
L43+00N 11+50E	201	202	0.2	7.50	540	2.0	12	0.62	< 0.5	7	40	14	3.92	2.20	0.54	295
L43+00N 11+75E	201	202	0.2	8.10	480	2.0	< 2	0.85	< 0.5	7	38	15	2.76	1.70	0.39	360
L43+00N 12+00E	201	202	0.2	7.81	390	1.5	< 2	1.02	< 0.5	5	28	9	3.12	1.54	0.39	300
L43+00N 12+25E	201	202	0.2	7.46	400	2.0	< 2	0.65	< 0.5	4	25	5	3.93	2.51	0.26	270
L45+00N 09+75E	201	202	0.4	7.88	510	2.0	< 2	0.61	< 0.5	5	43	9	3.24	1.97	0.41	280
L45+00N 10+00E	201	202	0.2	8.07	540	2.0	< 2	0.68	< 0.5	7	44	10	3.01	1.87	0.43	460
L45+00N 10+25E	201	202	< 0.2	7.41	400	1.5	< 2	0.86	< 0.5	10	39	19	3.61	1.10	0.80	1035
L45+00N 10+50E	201	202	0.2	7.51	430	2.5	< 2	0.85	< 0.5	6	37	9	3.51	1.68	0.39	295
L45+00N 10+75E	201	202	0.2	9.39	630	5.0	< 2	1.17	< 0.5	11	67	31	4.09	2.18	0.82	545
L45+00N 11+00E	201	202	< 0.2	7.71	570	3.0	< 2	0.97	< 0.5	7	45	13	2.72	2.32	0.59	430
L45+00N 11+25E	201	202	< 0.2	7.10	450	2.0	< 2	1.00	< 0.5	8	48	13	3.86	1.73	0.46	510
L45+00N 11+50E	201	202	< 0.2	8.17	460	1.5	< 2	1.08	< 0.5	5	16	12	2.26	1.41	0.34	285
L45+00N 11+75E	201	202	0.2	7.57	370	2.0	< 2	0.75	< 0.5	4	25	8	2.61	1.72	0.31	295
L45+00N 12+00E	201	202	< 0.2	7.71	350	2.0	< 2	0.59	< 0.5	4	25	7	2.34	1.48	0.26	215
L45+00N 12+25E	201	202	< 0.2	7.23	530	2.0	< 2	0.82	< 0.5	4	32	8	3.31	2.07	0.38	275
L45+00N 12+50E	201	202	0.2	7.38	380	1.5	< 2	0.70	< 0.5	3	22	11	3.02	1.34	0.27	220
L45+00N 12+75E	201	202	< 0.2	8.26	510	2.0	< 2	0.84	< 0.5	4	29	8	2.89	1.93	0.38	290
L45+00N 13+00E	201	202	< 0.2	7.02	470	1.5	< 2	1.11	< 0.5	5	24	6	2.57	1.82	0.49	390
L45+00N 13+50E	201	202	< 0.2	7.09	580	1.5	< 2	1.11	< 0.5	4	12	10	1.49	2.12	0.38	345
L45+00N 14+00E	201	202	< 0.2	7.39	520	1.5	< 2	1.48	< 0.5	7	7	13	1.81	1.76	0.55	690
L45+00N 14+50E	201	202	1.0	7.79	400	1.0	< 2	0.98	< 0.5	4	8	13	3.09	1.20	0.33	275
L45+00N 15+00E	201	202	0.2	7.42	490	1.5	< 2	1.22	< 0.5	5	9	9	1.93	1.57	0.41	335
L45+00N 15+50E	201	202	< 0.2	6.87	560	1.5	< 2	1.22	< 0.5	5	9	7	1.55	2.00	0.49	380
L45+00N 16+00E	201	202	< 0.2	6.74	450	1.5	< 2	1.05	< 0.5	5	29	9	2.72	1.79	0.41	330
L45+00N 16+50E	201	202	0.8	7.53	470	2.5	< 2	1.66	1.5	8	25	47	2.67	1.71	0.57	660
L45+00N 17+00E	201	202	0.2	7.35	490	2.5	< 2	1.36	< 0.5	7	30	16	3.59	1.59	0.49	345
L45+00N 17+50E	201	202	< 0.2	7.11	590	2.0	< 2	0.88	< 0.5	4	24	8	1.93	2.07	0.35	280
L45+00N 18+00E	201	202	< 0.2	6.99	600	2.5	< 2	0.90	< 0.5	6	35	10	1.78	2.23	0.55	370
L45+00N 18+50E	201	202	< 0.2	7.09	570	2.0	< 2	0.70	< 0.5	6	35	11	2.61	2.10	0.43	295
L45+00N 19+00E	201	202	< 0.2	6.86	610	2.0	< 2	0.90	< 0.5	5	32	12	2.31	2.21	0.50	370

CERTIFICATION:



ALS Chemex

Aurora Laboratory Services Ltd.
 Analytical Chemists * Geochemists * Registered Assayers
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o: GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

Page: 1-B
 Total Pages: 5
 Certificate Date: 28-OCT-2000
 Invoice No.: I0031990
 P.O. Number:
 Account: CYO

CERTIFICATE OF ANALYSIS A0031990

SAMPLE	PREP CODE	Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)				
L42+00N 11+00E	201 202	1	1.67	17	370	30	228	0.35	76	< 10	96				
L42+00N 11+30E	201 202	< 1	1.97	20	610	28	251	0.27	59	< 10	62				
L42+00N 11+30E B	201 202	< 1	1.32	7	800	22	170	0.24	57	< 10	38				
L42+00N 11+50E	201 202	< 1	1.60	6	1650	30	171	0.27	58	< 10	34				
L42+00N 11+75E	201 202	< 1	2.18	5	530	26	231	0.39	54	< 10	38				
L42+00N 12+00E	201 202	2	2.18	6	610	28	244	0.44	59	< 10	42				
L42+00N 12+25E	201 202	< 1	1.97	5	1190	26	203	0.34	49	< 10	50				
L43+00N 11+00E	201 202	< 1	1.52	12	950	24	196	0.23	52	< 10	80				
L43+00N 11+00E C	201 202	1	1.96	17	490	30	246	0.28	58	< 10	64				
L43+00N 11+25	201 202	< 1	1.78	4	760	24	205	0.28	50	< 10	52				
L43+00N 11+50E	201 202	< 1	1.48	11	730	32	183	0.37	78	< 10	86				
L43+00N 11+75E	201 202	< 1	1.84	13	700	350	200	0.35	60	< 10	270				
L43+00N 12+00E	201 202	< 1	1.96	8	490	22	219	0.26	48	< 10	48				
L43+00N 12+25E	201 202	< 1	1.87	5	790	38	184	0.26	73	< 10	42				
L45+00N 09+75E	201 202	< 1	1.49	10	540	30	183	0.27	60	< 10	66				
L45+00N 10+00E	201 202	< 1	1.43	14	880	24	184	0.27	57	< 10	88				
L45+00N 10+25E	201 202	< 1	1.63	41	2080	20	185	0.39	69	< 10	50				
L45+00N 10+50E	201 202	< 1	1.55	8	720	28	176	0.35	71	< 10	92				
L45+00N 10+75E	201 202	< 1	1.67	34	910	44	239	0.44	82	< 10	168				
L45+00N 11+00E	201 202	1	1.90	13	720	32	229	0.35	63	< 10	80				
L45+00N 11+25E	201 202	1	1.90	11	3510	48	205	0.52	82	< 10	182				
L45+00N 11+50E	201 202	< 1	2.34	3	680	24	240	0.37	44	< 10	50				
L45+00N 11+75E	201 202	< 1	2.00	6	660	30	194	0.30	48	< 10	40				
L45+00N 12+00E	201 202	< 1	1.57	5	750	28	158	0.22	41	< 10	40				
L45+00N 12+25E	201 202	< 1	1.95	7	580	30	214	0.41	80	< 10	44				
L45+00N 12+50E	201 202	3	1.79	5	740	26	169	0.38	64	< 10	36				
L45+00N 12+75E	201 202	< 1	1.97	7	480	30	214	0.41	73	< 10	72				
L45+00N 13+00E	201 202	1	2.42	6	690	26	246	0.37	61	< 10	44				
L45+00N 13+50E	201 202	< 1	2.86	1	360	24	276	0.40	42	< 10	38				
L45+00N 14+00E	201 202	< 1	3.04	3	1690	16	316	0.30	36	< 10	46				
L45+00N 14+50E	201 202	1	2.26	5	800	16	222	0.39	51	< 10	34				
L45+00N 15+00E	201 202	1	2.80	1	340	16	268	0.40	44	< 10	40				
L45+00N 15+50E	201 202	< 1	3.09	2	360	16	279	0.32	40	< 10	38				
L45+00N 16+00E	201 202	< 1	2.07	6	890	22	223	0.38	58	< 10	44				
L45+00N 16+50E	201 202	< 1	2.25	14	1220	26	296	0.32	51	< 10	186				
L45+00N 17+00E	201 202	4	1.89	8	1010	24	249	0.40	61	< 10	98				
L45+00N 17+50E	201 202	< 1	2.01	3	510	20	244	0.33	48	< 10	46				
L45+00N 18+00E	201 202	1	1.90	12	790	22	254	0.27	48	< 10	46				
L45+00N 18+50E	201 202	< 1	1.69	11	570	20	213	0.23	47	< 10	40				
L45+00N 19+00E	201 202	< 1	1.94	11	530	24	239	0.31	55	< 10	40				

CERTIFICATION:



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GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
VERNON, BC
V1B 3M9

Project: PROJECT #86
Comments: ATTN: WARNER GRUENWALD

Page 1 of 2-A
Total F: 5
Certificate Date: 26-OCT-2000
Invoice No.: I0031990
P.O. Number:
Account: CYO

CERTIFICATE OF ANALYSIS A0031990

SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
L45+00N 19+50E	201 202	0.8	7.44	540	2.5	< 2	0.92	< 0.5	11	34	16	3.33	1.90	0.49	1210
L45+00N 20+00E	201 202	0.2	7.20	610	2.0	< 2	0.90	< 0.5	10	37	13	2.79	2.10	0.54	615
L45+00N 20+50E	201 202	0.6	7.19	520	1.5	< 2	1.22	< 0.5	5	22	18	1.68	1.72	0.47	340
L45+00N 21+00E	201 202	< 0.2	7.04	670	2.5	< 2	0.76	< 0.5	8	44	12	2.62	2.45	0.64	335
L45+00N 21+50E	201 202	< 0.2	7.25	520	1.5	< 2	1.22	< 0.5	4	22	10	1.88	1.66	0.42	340
L45+00N 22+00E	201 202	0.2	6.43	440	2.0	< 2	1.42	< 0.5	5	35	11	3.26	1.57	0.42	375
L45+00N 22+50E	201 202	< 0.2	6.57	540	1.5	< 2	1.18	< 0.5	4	27	9	2.26	1.76	0.38	315
L45+00N 23+00E	201 202	< 0.2	6.68	580	1.5	< 2	1.06	< 0.5	1	25	5	0.86	2.05	0.26	225
L45+00N 23+50E	201 202	0.2	6.41	610	1.5	< 2	0.97	< 0.5	3	10	11	1.29	1.91	0.28	305
L45+00N 24+00E	201 202	< 0.2	6.42	510	2.0	< 2	1.25	< 0.5	5	23	10	2.32	1.84	0.40	345
L45+00N 24+50E	201 202	< 0.2	7.10	510	2.0	< 2	0.97	< 0.5	4	32	10	2.56	1.66	0.36	285
L45+00N 25+00E	201 202	< 0.2	6.94	550	1.5	< 2	1.07	< 0.5	5	26	14	2.71	1.75	0.33	365
L48+00N 17+00E	201 202	< 0.2	6.81	600	2.0	< 2	1.18	< 0.5	2	25	6	1.60	2.25	0.24	325
L48+00N 17+50E	201 202	< 0.2	6.74	430	1.5	< 2	0.55	< 0.5	5	24	10	3.36	1.35	0.22	255
L48+00N 18+00E	201 202	< 0.2	7.22	470	1.5	< 2	0.82	< 0.5	3	16	6	2.64	2.07	0.29	275
L48+00N 19+00E	201 202	< 0.2	7.98	460	2.5	< 2	0.90	< 0.5	5	42	13	2.97	1.69	0.48	315
L48+00N 20+00E	201 202	< 0.2	6.49	560	2.5	< 2	0.90	< 0.5	10	32	10	2.91	2.11	0.44	445
L48+00N 20+50E	201 202	< 0.2	8.01	680	2.5	< 2	1.02	< 0.5	8	52	20	3.01	2.62	0.82	370
L48+00N 21+00E	201 202	0.2	6.88	570	2.5	< 2	0.81	< 0.5	9	42	34	3.57	2.04	0.62	510
L48+00N 21+50E	201 202	0.4	7.47	580	2.0	< 2	1.23	< 0.5	12	27	18	2.64	1.94	0.58	570
L48+00N 22+00E	201 202	< 0.2	7.30	510	1.5	< 2	1.19	< 0.5	5	26	9	3.25	1.72	0.51	375
L48+00N 22+50E	201 202	0.2	8.35	560	2.0	< 2	1.31	< 0.5	8	35	21	2.56	1.87	0.54	440
L48+00N 23+00E	201 202	< 0.2	6.23	620	2.0	< 2	1.17	< 0.5	7	34	12	2.57	2.12	0.47	335
L48+00N 24+50E	201 202	< 0.2	7.35	690	2.0	< 2	0.74	0.5	9	54	18	3.21	2.55	0.71	365
L48+00N 25+00E	201 202	0.2	7.78	670	2.0	< 2	1.17	< 0.5	9	30	15	2.94	2.18	0.64	550
L48+00N 25+50E	201 202	0.2	7.22	590	2.0	< 2	1.95	0.5	8	35	25	2.48	2.00	0.55	365
L52+00N 23+00E	201 202	< 0.2	6.85	440	2.0	< 2	1.78	< 0.5	6	16	11	2.77	1.40	0.42	370
L52+00N 24+00E	201 202	< 0.2	6.72	610	2.0	< 2	0.80	< 0.5	4	29	10	2.63	2.11	0.42	350
L52+00N 24+50E	201 202	< 0.2	7.06	530	2.0	< 2	1.52	< 0.5	5	24	9	2.07	1.85	0.49	375
L54+00N 17+00E	201 202	0.2	7.01	470	2.0	< 2	1.71	< 0.5	7	31	13	3.61	1.82	0.53	395
L54+00N 17+50E	201 202	< 0.2	7.17	440	1.5	< 2	0.81	< 0.5	3	13	4	1.14	2.69	0.21	245
L54+00N 18+00E	201 202	< 0.2	7.19	460	1.5	< 2	1.51	< 0.5	6	11	6	1.63	1.73	0.52	370
L54+00N 18+50E	201 202	< 0.2	6.77	490	1.5	< 2	0.87	< 0.5	1	13	13	2.28	1.53	0.25	315
L54+00N 19+00E	201 202	< 0.2	7.05	450	1.5	< 2	0.57	< 0.5	3	17	9	2.29	1.54	0.18	210
L54+00N 19+50E	201 202	< 0.2	8.26	430	2.5	< 2	1.28	< 0.5	5	24	8	3.85	1.75	0.44	310
L54+00N 20+00E	201 202	0.2	6.64	530	1.5	< 2	1.22	< 0.5	3	14	12	1.88	1.69	0.35	315
L54+00N 20+50E	201 202	0.4	6.70	440	1.5	< 2	0.85	< 0.5	3	16	12	2.77	1.37	0.24	240
L54+00N 21+00E	201 202	1.2	6.86	500	1.5	< 2	1.31	< 0.5	4	14	15	2.46	1.66	0.38	310
L54+00N 21+50E	201 202	< 0.2	7.30	470	2.0	< 2	1.02	< 0.5	9	55	13	4.06	1.58	0.46	495
L54+00N 22+00E	201 202	< 0.2	6.49	680	2.0	< 2	0.98	< 0.5	4	18	7	1.27	2.23	0.29	395

CERTIFICATION:



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BY GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
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Project : PROJECT #86
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Page : 2-B
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CERTIFICATE OF ANALYSIS A0031990

SAMPLE	PREP CODE	Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)				
L45+00N 19+50E	201 202	< 1	1.90	10	1180	22	238	0.30	55	< 10	49				
L45+00N 20+00E	201 202	< 1	1.96	12	870	22	244	0.33	62	< 10	52				
L45+00N 20+50E	201 202	< 1	2.42	5	770	22	277	0.38	45	< 10	36				
L45+00N 21+00E	201 202	< 1	1.90	17	530	20	248	0.27	55	< 10	42				
L45+00N 21+50E	201 202	1	2.50	3	660	18	276	0.44	46	< 10	36				
L45+00N 22+00E	201 202	< 1	1.47	7	830	14	282	0.38	76	< 10	26				
L45+00N 22+50E	201 202	1	2.15	4	640	24	271	0.46	62	< 10	28				
L45+00N 23+00E	201 202	< 1	1.99	2	650	20	271	0.38	46	< 10	20				
L45+00N 23+50E	201 202	< 1	3.07	< 1	330	18	251	0.35	32	< 10	36				
L45+00N 24+00E	201 202	< 1	1.86	4	600	18	292	0.31	60	< 10	26				
L45+00N 24+50E	201 202	2	1.84	4	760	22	228	0.43	71	< 10	26				
L45+00N 25+00E	201 202	< 1	2.26	4	880	22	259	0.44	55	< 10	32				
L48+00N 17+00E	201 202	1	2.08	3	330	26	291	0.42	54	< 10	28				
L48+00N 17+50E	201 202	< 1	1.32	5	1210	26	153	0.32	66	< 10	30				
L48+00N 18+00E	201 202	< 1	2.09	3	420	30	222	0.26	39	< 10	52				
L48+00N 19+00E	201 202	< 1	1.47	12	430	20	215	0.27	53	< 10	50				
L48+00N 20+00E	201 202	< 1	1.76	10	560	22	251	0.25	55	< 10	66				
L48+00N 20+50E	201 202	< 1	1.78	20	500	28	280	0.30	73	< 10	76				
L48+00N 21+00E	201 202	< 1	1.52	17	980	32	219	0.30	66	< 10	60				
L48+00N 21+50E	201 202	1	2.32	16	940	28	283	0.36	59	< 10	68				
L48+00N 22+00E	201 202	< 1	2.14	6	690	24	265	0.40	60	< 10	46				
L48+00N 22+50E	201 202	3	2.27	10	1030	30	272	0.39	59	< 10	62				
L48+00N 23+00E	201 202	< 1	1.81	17	580	22	248	0.24	46	< 10	52				
L48+00N 24+50E	201 202	< 1	1.71	19	540	26	224	0.32	69	< 10	64				
L48+00N 25+00E	201 202	1	2.49	9	870	24	290	0.39	64	< 10	54				
L48+00N 25+50E	201 202	1	2.16	13	800	30	275	0.41	62	< 10	52				
L52+00N 23+00E	201 202	3	2.06	4	880	20	301	0.34	49	< 10	46				
L52+00N 24+00E	201 202	1	1.65	9	710	22	238	0.30	57	< 10	36				
L52+00N 24+50E	201 202	< 1	2.03	7	650	22	290	0.23	43	< 10	46				
L54+00N 17+00E	201 202	< 1	1.95	11	780	28	352	0.44	67	< 10	80				
L54+00N 17+50E	201 202	1	2.23	1	380	32	232	0.25	30	< 10	24				
L54+00N 18+00E	201 202	< 1	2.76	4	420	18	320	0.34	39	< 10	42				
L54+00N 18+50E	201 202	< 1	2.21	4	1070	32	211	0.45	42	< 10	32				
L54+00N 19+00E	201 202	< 1	1.39	3	830	24	179	0.24	41	< 10	26				
L54+00N 19+50E	201 202	< 1	1.98	6	440	32	267	0.41	75	< 10	66				
L54+00N 20+00E	201 202	< 1	2.68	3	840	22	269	0.44	49	< 10	42				
L54+00N 20+50E	201 202	4	2.00	1	900	30	206	0.42	64	< 10	30				
L54+00N 21+00E	201 202	< 1	2.44	7	550	22	263	0.37	44	< 10	38				
L54+00N 21+50E	201 202	< 1	1.57	15	1040	24	197	0.50	78	< 10	78				
L54+00N 22+00E	201 202	1	2.18	2	430	22	274	0.28	39	< 10	26				

CERTIFICATION:



ALS Chemex

Aurora Laboratory Services Ltd.
 Analytical Chemists * Geochemists * Registered Assayers
 212 Brooksbank Ave., North Vancouver
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D: GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

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 Certificate Date: 26-OCT-2000
 Invoice No.: I0031990
 P.O. Number :
 Account : CYO

Project : PROJECT #86
 Comments : ATTN: WARNER GRUENWALD

CERTIFICATE OF ANALYSIS A0031990

SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Ba ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
L54+00N 22+50E	201 202	< 0.2	6.41	620	2.0	< 2	0.90	< 0.5	4	30	13	2.80	2.10	0.38	365
L54+00N 23+00E	201 202	< 0.2	7.19	580	2.0	< 2	1.25	< 0.5	8	27	23	2.43	1.81	0.53	710
L54+00N 23+50E	201 202	< 0.2	7.81	590	2.0	< 2	1.38	< 0.5	11	37	49	3.22	1.93	0.56	635
L54+00N 24+00E	201 202	< 0.2	7.15	480	1.5	< 2	1.91	< 0.5	7	12	10	2.74	1.62	0.72	460
L54+00N 24+50E	201 202	< 0.2	7.86	660	2.0	< 2	0.96	< 0.5	7	51	11	3.39	2.62	0.71	340
L54+00N 25+00E	201 202	< 0.2	7.29	500	2.0	< 2	1.09	< 0.5	8	29	18	3.31	1.69	0.46	295
L56+00N 18+00E	201 202	< 0.2	6.75	580	1.5	< 2	1.18	< 0.5	5	29	6	1.97	1.94	0.49	325
L56+00N 18+50E	201 202	< 0.2	7.32	600	2.0	< 2	1.51	< 0.5	6	27	12	1.99	1.58	0.71	480
L56+00N 19+00E	201 202	< 0.2	6.78	640	1.5	< 2	1.44	< 0.5	6	8	7	1.97	2.23	0.65	455
L56+00N 19+50E	201 202	< 0.2	7.23	550	1.5	< 2	1.75	< 0.5	5	16	8	1.78	1.86	0.47	360
L56+00N 20+00E	201 202	< 0.2	7.16	380	1.0	< 2	1.50	< 0.5	9	36	14	3.88	1.24	0.42	830
L56+00N 20+50E	201 202	< 0.2	6.54	500	1.5	< 2	1.12	< 0.5	8	67	9	4.45	1.89	0.68	450
L56+00N 21+00E	201 202	< 0.2	8.14	390	2.0	< 2	1.56	< 0.5	8	45	15	4.01	1.26	0.40	335
L56+00N 21+50E	201 202	0.2	8.01	510	2.5	< 2	1.70	< 0.5	9	224	25	2.91	1.69	0.59	1105
L56+00N 22+00E	201 202	< 0.2	7.61	500	2.0	< 2	1.12	< 0.5	5	43	10	2.90	1.61	0.36	370
L56+00N 22+50E	201 202	< 0.2	6.63	530	2.5	< 2	1.49	< 0.5	8	36	24	2.07	2.09	0.47	625
L56+00N 23+00E	201 202	< 0.2	6.74	570	2.0	< 2	0.77	< 0.5	7	33	9	3.79	2.03	0.47	305
L56+00N 23+50E	201 202	0.2	6.60	550	2.0	< 2	1.36	< 0.5	5	26	10	1.92	1.90	0.43	465
L56+00N 24+00E	201 202	< 0.2	8.80	310	1.5	< 2	2.16	< 0.5	5	8	10	1.79	1.16	0.65	420
L56+00N 24+50E	201 202	< 0.2	6.75	540	2.0	< 2	0.83	< 0.5	5	31	7	3.96	1.78	0.41	300
L56+00N 25+00E	201 202	0.2	6.20	550	1.5	< 2	0.80	< 0.5	5	32	11	4.47	1.82	0.35	350
L58+00N 22+50E	201 202	< 0.2	7.03	650	2.0	< 2	1.11	< 0.5	5	35	9	2.57	2.29	0.42	330
L58+00N 23+00E	201 202	< 0.2	8.02	560	5.5	< 2	1.92	< 0.5	8	33	11	2.93	2.34	0.46	450
L58+00N 23+50E	201 202	< 0.2	8.29	410	3.0	< 2	2.16	< 0.5	13	95	22	3.94	1.81	1.11	550
L58+00N 24+00E	201 202	< 0.2	7.82	420	2.0	< 2	1.37	< 0.5	6	22	16	2.69	1.45	0.43	355
L58+00N 24+50E	201 202	< 0.2	8.48	380	4.5	< 2	1.78	< 0.5	17	50	21	3.78	1.87	0.68	645
L58+00N 25+50E	201 202	< 0.2	7.64	490	2.0	< 2	1.33	< 0.5	7	25	17	2.59	1.52	0.37	460
L58+00N 26+00E	201 202	< 0.2	6.57	500	1.5	< 2	0.89	< 0.5	4	24	12	3.32	1.54	0.32	285
L60+00N 22+00E	201 202	< 0.2	6.42	520	2.0	< 2	1.40	< 0.5	6	27	10	2.68	1.77	0.36	305
L60+00N 22+50E	201 202	< 0.2	8.04	570	2.5	< 2	1.22	< 0.5	7	35	10	2.58	2.04	0.50	385
L60+00N 23+00E	201 202	< 0.2	8.54	530	2.0	< 2	0.96	< 0.5	6	31	8	2.65	1.92	0.40	330
L60+00N 23+50E	201 202	< 0.2	7.98	520	2.0	< 2	0.91	< 0.5	4	21	13	2.25	1.86	0.29	430
L60+00N 24+00E	201 202	< 0.2	6.76	570	2.5	< 2	1.28	< 0.5	4	23	8	2.20	2.12	0.36	355
L60+00N 24+50E	201 202	< 0.2	6.53	560	2.0	< 2	0.97	< 0.5	5	23	9	2.55	1.81	0.30	335
L60+00N 25+00E	201 202	< 0.2	6.90	590	2.5	< 2	1.29	< 0.5	4	23	11	1.14	2.09	0.32	415
L60+00N 25+50E	201 202	< 0.2	6.50	510	2.5	< 2	1.47	< 0.5	9	24	7	2.74	1.75	0.42	860
L60+00N 26+00E	201 202	< 0.2	6.49	630	2.0	< 2	1.10	< 0.5	4	26	10	1.91	2.15	0.24	630
L62+00N 23+00E	201 202	< 0.2	6.23	560	2.0	< 2	0.85	< 0.5	6	31	9	2.80	1.89	0.40	285
L62+00N 23+50E	201 202	< 0.2	7.18	570	2.5	< 2	1.01	< 0.5	7	41	14	3.01	2.12	0.59	340
L62+00N 24+00E	201 202	< 0.2	7.34	520	2.5	< 2	0.67	< 0.5	5	25	17	2.86	2.54	0.40	320

CERTIFICATION:



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GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
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 V1B 3M9

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Project : PROJECT #86
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CERTIFICATE OF ANALYSIS A0031990

SAMPLE	PREP CODE		Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)			
L54+00N 22+50E	201	202	1	1.88	7	560	26	246	0.32	56	< 10	62			
L54+00N 23+00E	201	202	< 1	1.96	11	900	24	266	0.30	55	< 10	72			
L54+00N 23+50E	201	202	1	1.81	20	1190	28	268	0.35	61	< 10	104			
L54+00N 24+00E	201	202	1	2.85	7	740	18	355	0.38	57	< 10	56			
L54+00N 24+50E	201	202	< 1	1.87	14	340	24	265	0.32	77	< 10	60			
L54+00N 25+00E	201	202	3	1.83	8	780	20	252	0.34	62	< 10	46			
L56+00N 18+00E	201	202	< 1	2.21	6	490	24	287	0.40	62	< 10	32			
L56+00N 18+50E	201	202	1	2.70	11	990	28	373	0.49	55	< 10	52			
L56+00N 19+00E	201	202	< 1	3.11	5	330	18	309	0.32	55	< 10	46			
L56+00N 19+50E	201	202	< 1	2.68	3	410	20	353	0.38	45	< 10	40			
L56+00N 20+00E	201	202	2	1.70	11	1520	30	360	0.47	71	< 10	70			
L56+00N 20+50E	201	202	< 1	1.54	18	1090	36	228	0.52	121	< 10	54			
L56+00N 21+00E	201	202	< 1	1.55	10	1040	32	307	0.48	80	< 10	66			
L56+00N 21+50E	201	202	4	2.10	69	510	30	355	0.40	65	< 10	118			
L56+00N 22+00E	201	202	< 1	1.54	8	630	28	252	0.39	74	< 10	60			
L56+00N 22+50E	201	202	1	1.89	15	620	26	289	0.24	48	< 10	38			
L56+00N 23+00E	201	202	1	1.45	10	430	26	211	0.32	70	< 10	46			
L56+00N 23+50E	201	202	7	1.98	8	870	26	287	0.31	56	< 10	48			
L56+00N 24+00E	201	202	< 1	3.00	3	500	12	401	0.28	30	< 10	46			
L56+00N 24+50E	201	202	< 1	1.56	7	320	22	231	0.30	74	< 10	44			
L56+00N 25+00E	201	202	3	1.53	7	650	26	217	0.33	76	< 10	42			
L58+00N 22+50E	201	202	< 1	1.67	7	640	22	293	0.32	69	< 10	48			
L58+00N 23+00E	201	202	3	1.56	10	470	28	274	0.31	65	< 10	78			
L58+00N 23+50E	201	202	2	1.54	36	800	32	294	0.63	87	< 10	104			
L58+00N 24+00E	201	202	1	2.09	8	830	22	271	0.30	45	< 10	64			
L58+00N 24+50E	201	202	1	1.39	34	950	32	250	0.37	64	< 10	56			
L58+00N 25+50E	201	202	3	1.88	8	820	20	261	0.37	52	< 10	74			
L58+00N 26+00E	201	202	2	1.80	5	650	24	223	0.37	64	< 10	34			
L60+00N 22+00E	201	202	< 1	1.67	6	1050	16	280	0.31	59	< 10	36			
L60+00N 22+50E	201	202	< 1	1.75	9	600	22	293	0.30	61	< 10	70			
L60+00N 23+00E	201	202	< 1	1.89	6	760	22	248	0.28	56	< 10	50			
L60+00N 23+50E	201	202	1	2.14	4	1100	22	237	0.30	44	< 10	76			
L60+00N 24+00E	201	202	< 1	1.86	7	500	20	289	0.21	44	< 10	28			
L60+00N 24+50E	201	202	< 1	1.79	6	420	18	257	0.25	45	< 10	42			
L60+00N 25+00E	201	202	< 1	2.09	8	610	22	315	0.20	34	< 10	38			
L60+00N 25+50E	201	202	2	1.85	7	640	22	320	0.24	58	< 10	34			
L60+00N 26+00E	201	202	< 1	1.84	7	650	20	277	0.26	47	< 10	32			
L62+00N 23+00E	201	202	< 1	1.63	7	560	20	229	0.23	55	< 10	38			
L62+00N 23+50E	201	202	< 1	1.60	12	830	24	250	0.24	61	< 10	56			
L62+00N 24+00E	201	202	< 1	1.64	10	720	34	206	0.22	45	< 10	62			

CERTIFICATION: 



ALS Chemex

Aurora Laboratory Services Ltd.
 Analytical Chemists * Geochemists * Registered Assayers
 212 Brooksbank Ave., North Vancouver
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to: GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
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CERTIFICATE OF ANALYSIS A0031990

SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
L62+00N 24+50E	201 202	< 0.2	7.00	540	2.0	< 2	0.80	< 0.5	4	25	9	2.07	1.72	0.30	375
L62+00N 25+00E	201 202	< 0.2	6.81	570	2.0	< 2	0.99	< 0.5	5	24	11	2.46	1.70	0.35	470
L62+00N 25+50E	201 202	< 0.2	5.86	540	2.0	< 2	0.99	< 0.5	4	21	7	2.48	1.65	0.28	355
L62+00N 26+00E	201 202	< 0.2	7.17	500	2.5	< 2	0.88	0.5	5	28	15	2.87	1.48	0.26	320
L64+00N 23+00E	201 202	< 0.2	7.58	380	1.5	< 2	1.43	< 0.5	5	14	15	2.30	1.24	0.46	315
L64+00N 23+50E	201 202	< 0.2	7.15	600	2.5	< 2	0.84	< 0.5	5	29	11	2.39	1.84	0.42	315
L64+00N 24+00E	201 202	< 0.2	7.86	410	1.5	< 2	1.23	< 0.5	7	23	8	3.04	1.52	0.48	335
L64+00N 24+50E	201 202	< 0.2	7.01	670	2.0	< 2	0.90	< 0.5	5	29	8	1.99	2.12	0.46	355
L64+00N 25+00E	201 202	< 0.2	8.33	630	2.0	< 2	1.16	< 0.5	10	29	11	2.74	1.81	0.44	705
L64+00N 25+50E	201 202	< 0.2	7.12	660	2.5	< 2	1.36	< 0.5	7	30	14	2.29	2.10	0.47	440
L64+00N 25+75E	201 202	< 0.2	6.47	570	2.0	< 2	1.30	< 0.5	5	29	13	2.74	1.83	0.36	345
L66+00N 23+00E	201 202	< 0.2	7.18	640	2.5	< 2	1.30	< 0.5	7	31	10	2.33	2.18	0.55	355
L66+00N 23+05E	201 202	< 0.2	6.64	580	2.0	< 2	1.79	< 0.5	8	25	13	2.15	1.70	0.54	1440
L66+00N 23+50E	201 202	< 0.2	6.77	610	1.5	< 2	1.25	< 0.5	4	25	6	1.54	2.04	0.34	295
L66+00N 24+00E	201 202	< 0.2	7.18	530	2.0	< 2	0.78	0.5	4	22	13	2.18	1.74	0.26	310
L66+00N 24+50E A	201 202	< 0.2	7.29	620	2.5	< 2	1.24	< 0.5	8	35	23	2.78	1.99	0.46	360
L66+00N 24+50E B	201 202	< 0.2	8.09	660	2.0	< 2	1.09	< 0.5	6	31	9	2.29	2.03	0.42	430
L66+00N 25+25E	201 202	< 0.2	7.20	680	2.0	< 2	0.75	< 0.5	7	32	10	2.92	1.95	0.43	340
L66+00N 26+00E	201 202	< 0.2	6.48	520	2.0	< 2	0.69	< 0.5	4	28	8	2.46	1.59	0.33	285
L87+50N 22+50E A	201 202	< 0.2	9.42	620	2.5	< 2	1.06	< 0.5	20	32	27	2.86	1.88	0.49	335
L87+50N 22+50E B	201 202	0.2	9.29	660	2.5	< 2	1.25	< 0.5	11	48	23	3.50	2.23	0.64	330
L87+50N 22+75E	201 202	< 0.2	8.78	700	2.5	< 2	1.07	< 0.5	16	49	39	3.23	2.55	0.76	315
L87+50N 23+00E	201 202	< 0.2	8.95	690	2.5	< 2	1.15	< 0.5	12	47	36	3.59	2.48	0.70	380
L88+50N 21+00E	201 202	< 0.2	8.77	680	2.5	< 2	1.48	< 0.5	7	25	12	2.73	2.23	0.51	310
L88+50N 21+25E	201 202	< 0.2	9.14	410	2.0	< 2	1.56	< 0.5	8	15	9	2.88	1.33	0.52	445
L88+50N 21+50E	201 202	< 0.2	9.60	570	2.5	< 2	1.16	< 0.5	10	36	13	3.34	1.81	0.43	335
L88+50N 21+75E	201 202	< 0.2	8.99	570	2.5	< 2	1.53	< 0.5	8	21	15	2.79	1.94	0.48	330
L88+50N 22+00E	201 202	< 0.2	9.14	520	2.0	< 2	1.05	< 0.5	7	30	13	3.13	1.59	0.32	270
L89+00N 20+50E	201 202	< 0.2	7.77	620	3.0	< 2	1.72	< 0.5	9	31	17	2.59	2.22	0.65	390
L89+00N 20+75E	201 202	< 0.2	8.66	610	2.5	< 2	1.66	< 0.5	10	26	16	2.77	2.08	0.64	380
L89+00N 21+00E	201 202	< 0.2	7.83	630	2.5	< 2	1.56	< 0.5	7	23	10	2.41	2.24	0.49	290
L89+00N 21+25E	201 202	< 0.2	8.69	640	2.5	< 2	1.46	< 0.5	10	30	13	2.91	2.08	0.53	330
L89+00N 21+50E	201 202	< 0.2	7.99	710	2.5	< 2	1.57	< 0.5	8	31	14	2.55	2.59	0.64	360
L89+00N 21+75E	201 202	< 0.2	8.29	620	2.5	< 2	1.52	< 0.5	9	31	11	2.88	2.18	0.59	365
L89+00N 22+00E	201 202	< 0.2	8.29	670	3.0	< 2	1.76	< 0.5	9	29	14	2.67	2.61	0.76	380
L89+50N 19+50E	201 202	0.2	8.42	560	2.5	2	1.80	< 0.5	16	47	18	3.39	1.67	0.82	715
L89+50N 19+75E	201 202	< 0.2	8.40	460	2.5	< 2	2.76	< 0.5	29	66	68	5.88	1.51	1.73	835
L89+50N 20+25	201 202	< 0.2	8.86	660	2.5	< 2	1.63	< 0.5	8	27	10	2.69	2.14	0.53	325
L89+50N 20+50E	201 202	< 0.2	8.71	670	3.0	< 2	1.87	< 0.5	7	28	9	2.55	2.42	0.56	340
L89+50N 20+75E	201 202	< 0.2	8.52	680	3.0	< 2	1.86	< 0.5	10	26	7	2.53	2.35	0.57	370

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L62+00N 24+50E	201 202	1	1.59	5	870	18	222	0.22	42	< 10	56			
L62+00N 25+00E	201 202	< 1	1.88	7	860	14	253	0.29	50	< 10	46			
L62+00N 25+50E	201 202	1	1.61	5	340	18	270	0.24	45	< 10	24			
L62+00N 26+00E	201 202	< 1	1.57	5	700	20	224	0.32	56	< 10	40			
L64+00N 23+00E	201 202	1	2.30	4	780	16	285	0.28	40	< 10	40			
L64+00N 23+50E	201 202	< 1	1.64	8	760	20	234	0.23	47	< 10	38			
L64+00N 24+00E	201 202	< 1	2.00	5	920	18	262	0.30	63	< 10	42			
L64+00N 24+50E	201 202	< 1	1.87	7	650	18	260	0.23	47	< 10	36			
L64+00N 25+00E	201 202	< 1	1.87	8	550	26	269	0.33	58	< 10	144			
L64+00N 25+50E	201 202	1	1.88	10	500	24	286	0.26	51	< 10	88			
L64+00N 25+75E	201 202	3	1.78	8	660	26	270	0.31	60	< 10	130			
L66+00N 23+00E	201 202	< 1	1.82	9	480	22	335	0.25	60	< 10	40			
L66+00N 23+05E	201 202	< 1	1.78	10	1070	22	330	0.31	51	< 10	70			
L66+00N 23+50E	201 202	< 1	2.02	3	450	26	291	0.41	60	< 10	30			
L66+00N 24+00E	201 202	1	1.80	5	830	24	211	0.29	44	< 10	40			
L66+00N 24+50E A	201 202	2	1.70	13	630	26	265	0.31	61	< 10	46			
L66+00N 24+50E B	201 202	< 1	1.98	6	580	22	286	0.32	60	< 10	54			
L66+00N 25+25E	201 202	2	1.65	8	510	20	222	0.27	59	< 10	60			
L66+00N 26+00E	201 202	2	1.43	6	480	20	202	0.22	43	< 10	28			
L87+50N 22+50E A	201 202	< 1	2.07	40	950	32	257	0.39	64	< 10	156			
L87+50N 22+50E B	201 202	< 1	1.85	18	1010	26	284	0.39	95	< 10	106			
L87+50N 22+75E	201 202	< 1	1.65	30	640	28	272	0.34	87	< 10	90			
L87+50N 23+00E	201 202	< 1	1.72	29	780	22	293	0.33	87	< 10	106			
L88+50N 21+00E	201 202	< 1	1.96	9	1060	22	366	0.29	77	< 10	54			
L88+50N 21+25E	201 202	< 1	2.53	3	1570	18	316	0.36	63	< 10	78			
L88+50N 21+50E	201 202	1	1.92	13	1400	22	272	0.35	75	< 10	104			
L88+50N 21+75E	201 202	< 1	2.46	11	740	22	346	0.36	75	< 10	58			
L88+50N 22+00E	201 202	< 1	2.02	7	1850	26	230	0.44	72	< 10	70			
L89+00N 20+50E	201 202	< 1	2.07	23	490	26	369	0.30	80	< 10	86			
L89+00N 20+75E	201 202	< 1	2.27	13	570	26	373	0.32	77	< 10	82			
L89+00N 21+00E	201 202	< 1	2.01	6	880	20	370	0.29	77	< 10	40			
L89+00N 21+25E	201 202	< 1	2.04	11	700	22	338	0.33	81	< 10	128			
L89+00N 21+50E	201 202	< 1	1.94	18	630	22	374	0.26	80	< 10	72			
L89+00N 21+75E	201 202	< 1	1.83	10	1760	20	355	0.30	87	< 10	60			
L89+00N 22+00E	201 202	< 1	1.97	10	750	20	416	0.24	90	< 10	50			
L89+50N 19+50E	201 202	1	2.33	32	540	26	324	0.51	81	< 10	168			
L89+50N 19+75E	201 202	1	1.90	54	790	22	292	1.06	165	< 10	168			
L89+50N 20+25	201 202	< 1	2.06	10	1770	22	381	0.33	77	< 10	86			
L89+50N 20+50E	201 202	1	2.07	9	810	22	440	0.26	86	< 10	50			
L89+50N 20+75E	201 202	< 1	2.02	9	1210	22	426	0.29	82	< 10	102			

CERTIFICATION:



ALS Chemex

Aurora Laboratory Services Ltd.
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 212 Brooksbank Ave., North Vancouver
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: GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

Page 1 of 5-A
 Total F: 5
 Certificate Date: 26-OCT-2000
 Invoice No.: 10031990
 P.O. Number:
 Account: CYO

CERTIFICATE OF ANALYSIS A0031990

SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
L89+00N 21+00E	201 202	< 0.2	8.40	650	2.5	< 2	1.56	< 0.5	6	26	10	3.03	2.14	0.49	340
L90+00N 20+00E	201 202	< 0.2	7.45	650	2.5	< 2	1.80	< 0.5	9	35	14	2.62	2.32	0.64	375
L90+00N 20+25E	201 202	< 0.2	8.42	600	2.5	< 2	1.54	< 0.5	7	30	7	2.81	1.98	0.53	420
L90+00N 20+50E	201 202	< 0.2	9.21	610	2.5	< 2	1.59	< 0.5	10	30	9	3.08	2.14	0.54	430
L90+00N 20+75E	201 202	< 0.2	8.65	640	2.5	< 2	1.57	< 0.5	9	31	10	2.68	2.16	0.57	380
L90+00N 21+00E	201 202	< 0.2	8.80	550	2.5	< 2	1.49	< 0.5	6	25	10	2.53	1.90	0.44	370
L91+00N 20+50E	201 202	< 0.2	8.38	510	2.0	< 2	1.58	< 0.5	8	33	6	2.92	1.74	0.48	310
L91+00N 20+75E	201 202	< 0.2	8.47	630	2.5	< 2	1.76	< 0.5	7	23	7	2.68	2.18	0.53	360
L91+00N 21+00E	201 202	< 0.2	7.76	520	2.0	< 2	1.84	< 0.5	7	18	14	2.51	1.85	0.63	390
L92+00N 20+25E	201 202	< 0.2	9.21	560	4.5	< 2	1.79	< 0.5	20	36	30	3.91	1.65	0.80	390
L92+00N 20+50E	201 202	< 0.2	7.76	540	4.0	< 2	2.03	< 0.5	9	28	5	2.85	1.86	0.71	400
L92+00N 20+75E	201 202	< 0.2	8.26	490	2.0	< 2	1.63	< 0.5	7	23	7	3.03	1.65	0.51	320
L92+00N 21+00E	201 202	< 0.2	8.98	390	2.0	< 2	1.53	< 0.5	8	16	14	2.77	1.32	0.62	345
L93+00N 19+00E	201 202	0.2	8.05	540	2.5	< 2	1.78	< 0.5	7	30	7	2.67	1.84	0.64	355
L93+00N 19+25E	201 202	1.4	8.02	550	2.0	< 2	1.91	< 0.5	7	22	6	2.51	1.90	0.57	365
L93+00N 19+50E	201 202	0.4	7.69	640	2.5	< 2	1.79	< 0.5	11	37	9	2.65	2.13	0.68	450
L93+00N 19+75E	201 202	< 0.2	7.82	800	2.0	< 2	1.28	< 0.5	7	23	4	2.27	2.65	0.48	260
L93+00N 20+00E	201 202	< 0.2	7.73	770	2.5	< 2	1.25	< 0.5	5	22	5	2.03	2.63	0.46	255
L93+00N 20+25E	201 202	< 0.2	8.27	430	2.0	< 2	1.40	< 0.5	6	16	5	3.04	1.46	0.43	270
L93+00N 20+50E	201 202	2.0	7.96	780	2.5	< 2	1.28	< 0.5	5	22	7	2.27	2.71	0.50	280
L93+00N 20+75E	201 202	< 0.2	7.32	610	2.5	< 2	1.57	< 0.5	6	20	5	2.53	2.11	0.43	330
L93+00N 21+00E	201 202	< 0.2	8.69	710	3.0	< 2	1.24	< 0.5	9	27	14	2.54	2.42	0.59	325
75+00N 26+25E	201 202	< 0.2	6.83	680	2.0	< 2	1.08	< 0.5	7	39	7	2.99	2.20	0.57	475
MK 0+50E	201 202	< 0.2	9.14	410	2.5	< 2	1.13	< 0.5	10	44	15	3.26	1.33	0.50	420
MK 0+50EC	201 202	< 0.2	9.66	490	5.5	< 2	1.65	0.5	16	44	16	2.48	1.96	0.62	535
MK 1+50E	201 202	0.2	7.80	600	2.5	< 2	0.77	< 0.5	8	46	15	2.57	2.69	0.63	365
MK 1+50E C	201 202	< 0.2	8.26	570	2.5	< 2	0.65	< 0.5	8	45	15	3.46	2.25	0.58	310
MK 2+00E	201 202	< 0.2	7.09	530	2.0	< 2	0.75	< 0.5	8	45	18	3.63	2.34	0.62	370
MK 2+00E C	201 202	< 0.2	8.22	650	2.5	< 2	0.74	< 0.5	12	52	29	2.90	2.96	0.77	475
MK 2+50E	201 202	< 0.2	8.08	570	2.5	< 2	0.63	< 0.5	9	48	16	2.99	2.52	0.71	400
MK 2+50E C	201 202	< 0.2	7.74	680	2.5	< 2	0.73	< 0.5	7	39	20	2.34	2.75	0.68	430
MK 3+25E	201 202	< 0.2	7.16	530	2.0	< 2	0.77	0.5	4	30	11	3.08	1.75	0.41	270
MK 3+25E C	201 202	< 0.2	8.01	780	3.0	< 2	0.93	< 0.5	12	38	16	2.25	2.93	0.65	490

CERTIFICATION:



ALS Chemex

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GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

Page ar :5-B
 Total Pages :5
 Certificate Date: 26-OCT-2000
 Invoice No. :10031990
 P.O. Number :
 Account :CYO

CERTIFICATE OF ANALYSIS A0031990

SAMPLE	PREP CODE	Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)				
L89+50N 21+00E	201 202	1	1.89	7	1670	22	361	0.32	85	< 10	80				
L90+00N 20+00E	201 202	< 1	2.02	19	490	20	383	0.37	84	< 10	68				
L90+00N 20+25E	201 202	< 1	2.02	10	1240	20	351	0.32	76	< 10	108				
L90+00N 20+50E	201 202	1	1.88	7	1390	20	364	0.29	89	< 10	94				
L90+00N 20+75E	201 202	< 1	1.97	12	1070	20	352	0.30	74	< 10	96				
L90+00N 21+00E	201 202	< 1	2.04	6	1140	18	337	0.30	72	< 10	68				
L91+00N 20+50E	201 202	< 1	2.04	9	1250	22	308	0.38	75	< 10	70				
L91+00N 20+75E	201 202	< 1	2.21	5	980	22	419	0.31	81	< 10	78				
L91+00N 21+00E	201 202	< 1	2.35	7	480	18	387	0.33	67	< 10	56				
L92+00N 20+25E	201 202	< 1	1.69	49	490	34	287	0.38	85	< 10	110				
L92+00N 20+50E	201 202	< 1	2.14	10	370	24	365	0.37	82	< 10	118				
L92+00N 20+75E	201 202	< 1	2.08	7	970	20	337	0.32	80	< 10	98				
L92+00N 21+00E	201 202	< 1	2.37	10	680	18	299	0.30	56	< 10	84				
L93+00N 19+00E	201 202	< 1	2.22	13	610	20	379	0.36	72	< 10	60				
L93+00N 19+25E	201 202	< 1	2.27	8	730	20	397	0.32	73	< 10	50				
L93+00N 19+50E	201 202	< 1	2.07	19	660	22	388	0.38	81	< 10	68				
L93+00N 19+75E	201 202	< 1	2.09	8	520	20	370	0.24	69	< 10	38				
L93+00N 20+00E	201 202	< 1	2.14	7	400	20	363	0.23	63	< 10	32				
L93+00N 20+25E	201 202	< 1	2.07	5	840	18	304	0.28	74	< 10	38				
L93+00N 20+50E	201 202	< 1	2.17	7	890	22	364	0.22	67	< 10	34				
L93+00N 20+75E	201 202	< 1	2.04	4	2530	22	368	0.27	70	< 10	36				
L93+00N 21+00E	201 202	< 1	2.02	13	520	28	340	0.26	73	< 10	44				
75+00N 26+25E	201 202	< 1	1.75	10	1180	22	283	0.26	68	< 10	48				
MK 0+50E	201 202	< 1	1.55	28	690	22	185	0.35	64	< 10	96				
MK 0+50EC	201 202	< 1	1.85	32	1120	260	278	0.27	55	< 10	700				
MK 1+50E	201 202	< 1	1.80	18	790	36	216	0.24	57	< 10	128				
MK 1+50E C	201 202	1	1.51	14	1070	30	191	0.27	65	< 10	132				
MK 2+00E	201 202	< 1	1.67	16	1040	26	199	0.28	62	< 10	74				
MK 2+00E C	201 202	< 1	1.84	24	500	30	229	0.28	64	< 10	78				
MK 2+50E	201 202	< 1	1.57	17	420	28	186	0.28	66	< 10	116				
MK 2+50E C	201 202	< 1	1.85	16	390	24	244	0.25	57	< 10	50				
MK 3+25E	201 202	7	1.57	7	770	40	192	0.38	79	< 10	60				
MK 3+25E C	201 202	< 1	2.12	16	590	24	290	0.27	55	< 10	52				

CERTIFICATION:



ALS Chemex

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 212 Brooksbank Ave., North Vancouver
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To: GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

Page: 1-A
 Total Pages: 1
 Certificate Date: 24-OCT-2000
 Invoice No.: I0031429
 P.O. Number:
 Account: CYO

CERTIFICATE OF ANALYSIS A0031429

SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
VNA 0+50R	205 226	0.2	4.25	170	12.0	2	20.9	< 0.5	4	49	11	0.75	0.74	0.41	480
VNA 0+79R	205 226	0.4	8.13	60	13.5	118	4.88	< 0.5	11	63	222	7.41	0.99	1.77	1895
VNA 1+77R	205 226	0.6	6.09	150	9.0	130	2.65	3.5	21	111	451	9.36	2.17	0.42	990
VNA 2+05R	205 226	6.8	5.55	110	1.5	52	4.30	34.0	27	181	546	6.03	1.70	0.28	330
VNA 2+32R	205 226	0.2	4.96	140	1.5	4	0.36	< 0.5	32	136	226	5.01	2.39	0.04	65

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o: GEOQUEST CONSULTING LTD.

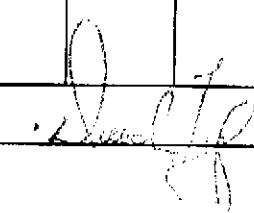
8055 ASPEN RD.
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Project : PROJECT #86
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 Total : 1
 Certificate Date: 24-OCT-2000
 Invoice No. : I0031429
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CERTIFICATE OF ANALYSIS A0031429

SAMPLE	PREP CODE		Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)				
VNA 0+50R	205	226	< 1	1.15	6	400	12	1835	0.08	14	< 10	42				
VNA 0+79R	205	226	< 1	2.87	10	1120	8	501	0.16	47	140	252				
VNA 1+77R	205	226	3	2.08	8	770	36	249	0.08	21	30	234				
VNA 2+05R	205	226	10	0.53	108	2280	7960	156	0.34	100	< 10	>10000				
VNA 2+32R	205	226	8	1.93	4	110	46	166	0.01	3	< 10	74				

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to: GEOQUEST CONSULTING LTD.

8055 ASPEN RD.
 VERNON, BC
 V1B 3M9

Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

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 Total Pages : 1
 Certificate Date: 26-OCT-2000
 Invoice No. : 10031548
 P.O. Number :
 Account : CYO

CERTIFICATE OF ANALYSIS A0031548

SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
VNA 22+26R	205 226	3.0	2.52	30	0.5	24	5.41	119.0	122	96	1850	17.20	0.07	0.22	925
VNR-05	205 226	< 0.2	7.52	2220	2.5	< 2	11.20	16.5	17	184	23	4.09	2.00	0.78	1220
VNR-06	205 226	< 0.2	6.28	30	0.5	4	6.37	295	78	138	164	6.51	1.80	0.77	975
VNR-07	205 226	< 0.2	9.27	70	1.0	< 2	1.50	43.5	49	141	509	6.13	4.26	1.31	370
VNR-08	205 226	6.2	0.40	70	< 0.5	6	20.7	69.5	6	98	44	0.60	0.10	0.35	105
VNR-09	205 226	< 0.2	7.79	1140	2.5	< 2	3.02	4.0	10	103	17	2.54	1.94	0.82	310
VNR-10	205 226	7.4	7.50	430	3.0	32	1.88	1.5	5	152	100	5.41	2.64	0.32	185
VNR-11	205 226	11.2	2.44	140	< 0.5	70	4.55	113.5	36	185	111	5.76	0.27	0.17	620
VNR-12	205 226	0.2	5.21	600	8.0	8	8.42	0.5	8	161	10	2.31	0.89	0.37	480
VNR-13	205 226	< 0.2	7.34	720	1.5	< 2	1.05	1.5	3	92	18	1.11	2.70	0.16	80

CERTIFICATION: _____



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 Total: 1
 Certificate Date: 25-OCT-2000
 Invoice No.: I0031548
 P.O. Number:
 Account: CYO

CERTIFICATE OF ANALYSIS **A0031548**

SAMPLE	PREP CODE	Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)				
VNA 22+26R	205 226	10	0.01	399	4490	2620	113	0.15	42	< 10	>10000				
VNR-05	205 226	< 1	0.43	35	1510	54	576	0.31	82	< 10	>10000				
VNR-06	205 226	< 1	1.06	112	910	942	292	0.30	80	< 10	>10000				
VNR-07	205 226	1	2.95	95	360	1590	288	0.55	122	< 10	4820				
VNR-08	205 226	< 1	0.02	6	600	>10000	183	< 0.01	9	< 10	>10000				
VNR-09	205 226	1	2.36	12	700	376	420	0.37	48	< 10	2350				
VNR-10	205 226	3	0.20	10	700	3510	52	0.27	84	< 10	2200				
VNR-11	205 226	1	0.12	42	1300	6720	70	0.11	39	< 10	>10000				
VNR-12	205 226	< 1	0.26	23	750	102	188	0.30	59	< 10	1105				
VNR-13	205 226	< 1	3.18	5	230	328	291	0.08	8	< 10	1480				

CERTIFICATION:



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 VERNON, BC
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 Comments: ATTN: WARNER GRUENWALD

Page Number: 1-A
 Total Pages: 1
 Certificate Date: 25-OCT-2000
 Invoice No.: I0031748
 P.O. Number:
 Account: CYO

CERTIFICATE OF ANALYSIS A0031748

SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
VNR-01	205 226	1.2	8.74	700	3.0	6	1.14	4.0	20	162	62	5.03	2.99	1.14	620
VNR-02	205 226	8.4	5.81	40	9.5	44	5.52	90.5	25	180	128	5.40	0.36	0.35	1530
VNR-03	205 226	< 0.2	5.09	430	3.0	< 2	5.75	83.5	20	173	34	4.82	1.53	1.10	845
VNR-04	205 226	< 0.2	8.30	1250	11.5	10	12.40	5.5	13	162	< 1	3.99	1.14	0.85	1140
VNA 6+53R	205 226	3.6	6.35	130	3.0	46	1.77	35.0	17	169	155	4.45	1.54	0.71	455
VNA 16+97R	205 226	< 0.2	5.56	350	1.5	< 2	0.61	< 0.5	12	213	25	2.86	1.57	0.90	285
VNA 19+64R	205 226	< 0.2	8.27	1190	3.0	< 2	6.81	< 0.5	18	154	41	3.63	1.77	2.16	665

CERTIFICATION: _____



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 Total Pages: 1
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CERTIFICATE OF ANALYSIS

A0031748

SAMPLE	PREP CODE	Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)				
VNR-01	205 226	< 1	2.42	36	610	696	159	0.55	107	< 10	2790				
VNR-02	205 226	1	0.72	52	1390	6450	215	0.26	67	< 10	>10000				
VNR-03	205 226	1	1.38	25	1070	82	368	0.33	50	< 10	>10000				
VNR-04	205 226	< 1	0.99	27	860	70	623	0.28	75	< 10	2570				
VNA 6+53R	205 226	8	2.11	56	610	2090	236	0.35	67	< 10	>10000				
VNA 16+97R	205 226	1	1.56	19	290	14	133	0.29	62	< 10	108				
VNA 19+64R	205 226	2	1.04	36	770	14	503	0.37	101	< 10	110				

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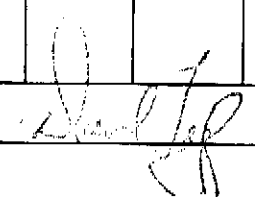
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 Certificate Date: 25-OCT-2000
 Invoice No. :10031796
 P.O. Number :
 Account :CYO

CERTIFICATE OF ANALYSIS A0031796

SAMPLE	PREP CODE	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Co ppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)	Mn ppm (ICP)
MKR-01	205 226	< 0.2	3.47	20	13.0	4	3.88	352	36	146	262	8.95	0.08	0.30	2110
MKR-02	205 226	< 0.2	9.69	790	4.5	4	1.27	< 0.5	9	143	123	6.34	2.84	1.14	705
VNA 4+78R	205 226	11.0	1.62	10	0.5	112	5.90	250	38	175	73	8.50	0.09	0.12	575
VNR 14	205 226	< 0.2	9.67	30	9.0	10	3.22	0.5	18	63	153	7.65	0.46	1.58	1850
VNR 15	205 226	< 0.2	6.12	140	1.5	< 2	0.07	< 0.5	< 1	169	5	0.56	2.77	0.07	155
VNR 16	205 226	< 0.2	6.77	330	3.5	< 2	7.37	0.5	18	219	41	3.17	2.05	0.60	560
VNR 17	205 226	< 0.2	6.40	200	4.5	< 2	14.10	< 0.5	13	137	21	3.11	1.14	1.24	770
L69N 24+70E (R)	205 226	< 0.2	6.40	110	5.5	2	7.53	< 0.5	20	88	148	7.35	0.88	3.11	1705

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Page 1 of 1
 Total : 1
 Certificate Date: 25-OCT-2000
 Invoice No. : I0031796
 P.O. Number :
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CERTIFICATE OF ANALYSIS A0031796

SAMPLE	PREP CODE	Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)				
MKR-01	205 226	< 1	0.62	49	1160	90	119	0.21	60	< 10	>10000				
MKR-02	205 226	7	3.15	8	340	224	311	0.60	131	< 10	390				
VNA 4+78R	205 226	10	0.01	84	960	>10000	66	0.12	50	< 10	>10000				
VNR 14	205 226	1	3.00	8	950	92	395	0.28	69	< 10	630				
VNR 15	205 226	< 1	2.04	1	100	42	86	0.01	2	< 10	102				
VNR 16	205 226	1	0.57	38	570	64	826	0.36	97	< 10	336				
VNR 17	205 226	1	1.43	25	860	24	771	0.35	68	< 10	188				
L69N 24+70E (R)	205 226	4	1.98	15	1270	12	189	1.01	235	< 10	150				

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Page Number : 1
 Total Pages : 1
 Certificate Date: 25-OCT-2000
 Invoice No. : I0032221
 P.O. Number :
 Account : CYO

CERTIFICATE OF ANALYSIS	A0032221
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SAMPLE	PREP CODE	Au ppb FA+AA	Zn %							
VNA 2+05R	212 --	< 5	1.06							

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Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

Page: 1 of 1
 Total: 1
 Certificate Date: 27-OCT-2000
 Invoice No.: I0032460
 P.O. Number:
 Account: CYO

CERTIFICATE OF ANALYSIS	A0032460
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SAMPLE	PREP CODE	Au ppb FA+AA	Pb %	Zn %						
VNA 22+26R	212 --	< 5	-----	7.10						
VNR-05	212 --	-----	-----	1.29						
VNR-06	212 --	-----	-----	15.95						
VNR-07	212 --	< 5	-----	-----						
VNR-08	212 --	-----	4.07	6.57						
VNR-11	212 --	-----	-----	6.53						

CERTIFICATION: *Angela Green*



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Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

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 Total F : 1
 Certificate Date: 27-OCT-2000
 Invoice No. : I0032485
 P.O. Number :
 Account : CYO

CERTIFICATE OF ANALYSIS	A0032485
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SAMPLE	PREP CODE	Zn %								
VNR-02	212 --	5.55								
VNR-03	212 --	2.51								
VNA 6+53R	212 --	2.32								

CERTIFICATION: *Warner Gruenwald*



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Project: PROJECT #86
 Comments: ATTN: WARNER GRUENWALD

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 Total 1
 Certificate Date: 27-OCT-2000
 Invoice No.: I0032486
 P.O. Number:
 Account: CYO

CERTIFICATE OF ANALYSIS	A0032486
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SAMPLE	PREP CODE	Pb %	Zn %							
MKR-01 VNA 4+78R	212 -- 212 --	----- 3.83	19.55 21.5							

CERTIFICATION: *Warner Gruenwald*

APPENDIX II
ROCK DESCRIPTIONS (W. GRUENWALD, P.GEO.)

**VISTA NAVAN
PRELIMINARY ROCK SAMPLE DATA**

Sample No.	Co-ordinates	Description	Ag ppm	Bi ppm	Cu ppm	Pb ppm	Zn ppm
L69N 24+70E	Grid	Not collected by WG	<0.2	2	148	12	150
MKR-01	~42+60E;11+00E	"Mike Showing" - grab sample of 2m mineralization from till bank along road. Zn associated with dark green skarn, gneiss and pegmatite host.	<0.2	4	262	90	19.55%
MKR-02	~42+30N;11+10E	Grab from 0.3m subangular boulder in glacial till. Consists of calc-silicate with trace sphalerite.	<0.2	4	123	224	390
VNA 0+50R	Grid co-ordinate 71+00N;25+68E 50m @345°m from bridge at Fowler L	Grab sample from 10 length of marble/minor calc-silicate along road cut.	0.2	2	11	12	42
VNA 0+79R	Grid co-ordinate 71+30N;25+55E 29 m @ 348° from bridge	Grab sample of angular, rusty calc-silicate, local source. Disseminated py-po, trace cpy.	0.4	118	222	8	252
VNA 1+77R	Grid co-ordinate 72+25N;25+25E	Float cobble (ferricrete) with 10% semi-stratified py, minor cpy in a siliceous matrix. Rock is angular and 2m deep in till cover.	0.6	130	451	36	234
VNA 2+05R	Grid co-ordinate 72+55N;25+25E	Angular, rusty and vary angular quartz rich gneiss with noteable ga, sph and cpy. Suspect this is from zone proximal to massive sulphides.	6.8	52	546	7960	1.06%
VNA 2+32R	Grid co-ordinate 72+82N;25+25E	15 cm cobble of quartz rich "granular" looking rock with 5-10% disseminated py, trace cpy.	0.2	4	226	46	74
VNA 4+78R	Grid co-ordinate est. 75+15N; 25+13E <i>25+85E</i>	NAVAN I SHOWING grab composite of fine grained massive sulphide fragments over ~7m length of road cut. Collected to identify litho geochemistry as well as Zn content.	11.0	112	73	3.83%	21.50%
VNA 6+53R	Grid co-ordinate est. 77+00N; 25+10E <i>25+85E</i>	Angular, limonitic 30 cm boulder. Contains 2 cm band of fine grained dense sphalerite similar to Navan I showing. Contains >cpy than Navan I	3.6	46	155	2090	2.32%
VNA 16+97R	Grid co-ordinate est. 83+00N;26+00E <i>APPROX</i>	Random grab across 5 m of limonitic, platy, feldspar. Quartz-biotite gneiss with disseminated py	<0.2	<2	25	14	108
VNA 19+64R	Grid co-ordinate est. 83+30N;24+20E	Chip sample across 2.0 m of calc-silicate	<0.2	<2	41	14	110
VNA 22+26R	Grid co-ordinate est. 83+50N;22+30E	Sphalerite bearing float (~15-20cm) below road cut.	3.0	24	1850	2620	7.10%
VNR-01	Grid co-ordinate est. 76+70N; 25+10E 617m from bridge <i>25+85E</i>	NAVAN II SHOWING - chip sample across 4.0 m of rusty qtz-fs-bio gneiss with disseminated py-po and minor sph.	1.2	6	62	696	2790
VNR-02	Grid co-ordinate est. 76+70N; 25+10E 617m from bridge <i>25+85E</i>	Sample of blocks of skarn material on hanging wall of schist (VNR-01). Est., a 0.3 m zone with irregular clots of sph, minor ga.	8.4	44	128	6450	5.55%

**VISTA NAVAN
PRELIMINARY ROCK SAMPLE DATA**

Sample No.	Co-ordinates	Description	Ag ppm	Bi ppm	Cu ppm	Pb ppm	Zn ppm
VNR-03	Grid co-ordinate ~83+50N;21+95E Road co-ordinate 22+83 from bridge	VISTA II SHOWING - uppermost sample across 0.2m of green-gray calc-silicate. Lower 5 cm contains modest amounts of coarse sphalerite.	<0.2	<2	34	82	2.51%
VNR-04	Grid co-ordinate ~83+50N;21+95E Road co-ordinate 22+83 from bridge	Lower sample across 1.4 m of mottled white, green and pinkish skarn, minor sphalerite.	<0.2	10	<1	70	2570
VNR-05	Grid co-ordinate 83+60N;21+80E Road co-ordinate 22+87	Chip sample across 0.5 m of green and pink massive skarn with minor disseminated sph near VNR-06 sample.	<0.2	<2	23	54	1.29%
VNR-06	Grid co-ordinate 83+60N;21+80E Road co-ordinate 22+88	Across 0.3m (true width) of semi to massive f.g. sphalerite with irregular clots of skarn.	<0.2	4	164	942	15.95%
VNR-07	Grid co-ordinate 83+60N;21+80E Road co-ordinate 22+89	Estimated width of 0.2 m of dark grey gneiss with disseminated py, sph, go.	<0.2	<2	509	1590	4820
VNR-08	Grid co-ordinate est. 87+80N;21+65E Road co-ordinate 22+98	Orange weathered siliceous (qtz vein) zone on top of skarn horizon. Sample along 0.9m strike length and average width of 8 cm. Modest amounts of galena and sphalerite present.	6.2	6	44	4.07%	6.57%
VNR-09	Grid co-ordinate est. 87+80N;21+65E Road co-ordinate 22+98	Chip sample across 0.25m of hanging wall gneiss adjacent to VNR-08	<0.2	<2	17	376	2350
VNR-10	Grid co-ordinate est. 87+80N;21+65E Road co-ordinate 23+01 to 23+02	Sample across 0.85m of rusty fault zone with local quartz and gouge 020°/85°W°±. Normal fault displacement	7.4	32	100	3510	2200
VNR-11	Grid co-ordinate est. 87+85N;21+60E Road co-ordinate 23+06	VISTA I type mineralization. Chip sample across 0.3m. Upper 15 cm is quartz with disseminated sph. Zone pinches out to west in 0.75m to a narrow "cataclastic" zone	11.2	70	111	6720	6.53%
VNR-12	Grid co-ordinate est. 87+85N;21+60E Road co-ordinate 23+06	Chip sample across 0.75m of hanging wall skarn	0.2	8	10	102	1105
VNR-13	Grid co-ordinate est. 87+85N;21+60E Road co-ordinate 23+06	Chip sample across 0.40m footwall pegmatite	<0.2	<2	18	328	1480
VNR-14	032° and 28m from B/L25E;70+00N	Rusty float in road bank	<0.2	10	153	92	630
VNR-15	Grid co-ordinate est. 89+55N;20+90E Road co-ordinate 25+20	Sample across 2.0m fault zone in pegmatite area	<0.2	<2	5	42	102
VNR-16	Grid co-ordinate est. 89+75N;20+80E Road co-ordinate 25+39	Sample across 2.30m fault zone near contact between pegmatite and calc-silicate. Suspect trace sph.	<0.2	<2	41	64	336
VNR-17	Grid co-ordinate est. 90+64N;21+05E Road co-ordinate 26+10	Grab sample of skarn/calc-silicate/marble.	<0.2	<2	21	24	188

APPENDIX III

GRAVITY SURVEY - DISCOVERY GEOPHYSICS LTD.

**GEOPHYSICAL REPORT ON A
GRAVITY SURVEY**

BROKEN HILL PROJECT

AVOLA, BRITISH COLUMBIA

**LATITUDE: 51°50.1'N LONGITUDE: 119°15.0'W
NTS: 82M/14 UTM: 345,000E 5,745,000N**

by

**Wes K. Kubo, B.Sc.
Dennis V. Woods, Ph.D., P.Eng.
Consulting Geophysicists**

for

**CASSIDY GOLD CORP.
220-141 Victoria Street
Kamloops, B.C., Canada V2C 1Z5**

DATE OF WORK: 1-17 December 2000

DATE OF REPORT: 23 February 2001

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INTRODUCTION

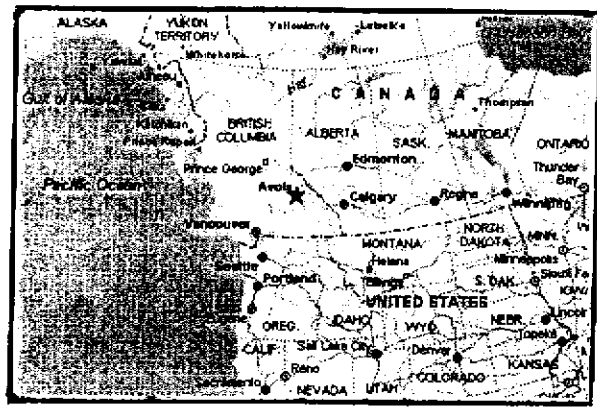
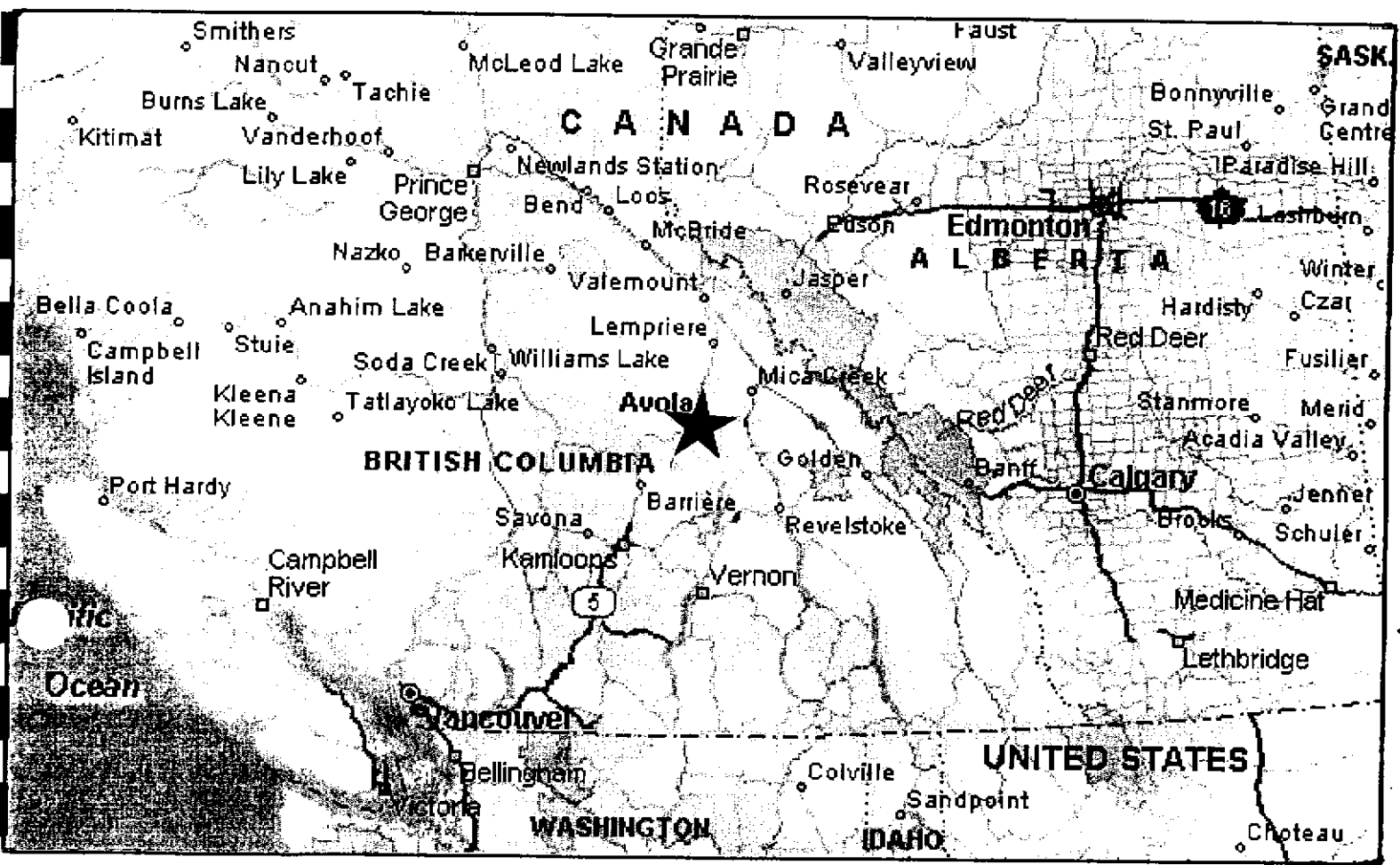
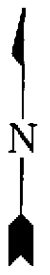
During the period 1 to 17 December 2000, Discovery Geophysics Inc. carried out a gravity survey on the Broken Hill property of Cassidy Gold Corp. near Avola, British Columbia. The survey was carried out as a follow-up investigation to previous sampling and geochemical studies on the property. Of particular interest were the Navan and Vista showings, two high-grade zinc discoveries within the survey area. The survey was the first geophysics done on the property. Wes Kubo and Alain Cotnoir recorded a total of 350 stations on 20 lines over 14 days of surveying.

A LaCoste & Romberg model G gravity meter was used for the gravity readings. A GDD hydrostatic chain level was used to determine relative elevation differences between successive stations and between adjacent survey lines. These relative elevations were converted to absolute elevations by tying into a benchmark elevation obtained with a handheld GPS unit. Station locations were determined by interpolating and extrapolating from GPS fixed locations on a chained grid. Clinometer readings were taken at every station in order to map detailed topography around the stations so that near-station terrain corrections could be made.

The results of this survey are presented in this report along with a technical description of the gravity survey method, survey procedures, and data processing and presentation. The results from the survey are discussed in detail and the report concludes with a review of the interpretations and recommendations for further work. The data are presented in tabular form in Appendix A and as gridded, contoured, colour maps in Appendix B. All map plots are overlain on a digital topographic base showing hydrography and elevation contours.

SURVEY LOCATION, ACCESS AND PHYSIOGRAPHY

The Broken Hill property is located on NTS map sheet 82M/14 near Avola in eastern British Columbia (Figure 1). The town of Avola, where there are minimal facilities, is located 2 km south of the entrance to the property. Accommodations and meals were provided in Blue River, approximately 35 km north of the property on the Yellowhead Highway (Hwy 5). Travel time to the property was approximately half an hour on the highway, 15 minutes up a snow-covered



200 KM

CASSIDY GOLD CORP.

BROKEN HILL PROJECT
AVOLA, B.C.
LOCATION MAP

Instrument: LaCoats & Romberg Model G Gravity Meter

Surveyed By: W. Kubo, A. Colnar	Survey Date: Dec 2000
Processed & Plotted by: Wes Kubo	Date: 23 Feb 2001

DISCOVERY GEOPHYSICS INC.

149 Commercial Rd., Springdale, Nfld. Box 223 A0J 1T0
 tel: (709)673-5359 fax: (709)673-5359 email: horizon@thezone.net

logging road and a further 45 minutes up the logging road on snowmobile.

The topography in the survey area varies from gently rolling in the centre of the survey grid to very steep on the northeast and southwest boundaries of the grid. There is a 120 m range in elevation over the survey area. A large cliff lies to the southwest and the northeast edge of the grid sits on a steep mountain slope. Fowler Lake lies at the southern end of the grid. There are numerous creeks and ravines which made surveying difficult (Figure 2). As well, the ground in certain areas was swampy. While the main blockages were cleared off of the grid, there was much underbrush blocking the lines. It was anticipated that the snow would have covered the brush by the time the survey commenced, however this was not the case. Traversing grid lines was often difficult due to an abundance of brush and steep, slippery slopes.

SURVEY METHODOLOGY

The gravity method is conceptually one of the simplest of the geophysical methods. This potential field method uses the measured gravity response to find variations in subsurface structure due to small changes in density. A body that has a density that is greater than the surrounding rock will exert a larger gravitational pull at the surface, which is measured by the gravity meter. Similarly, a density low such as a void will result in decreased gravitational pull at the surface. Gravity measurements are sensitive to many factors including latitude, elevation, topography, earth tides and the quantity of interest, subsurface density variations. The former four factors must be accounted for before a meaningful result can be obtained. For a comprehensive resource on the gravity method, the reader is referred to Applied Geophysics (Telford et al., 1990, pp. 6-61).

The gravity meter measures changes in the gravitational pull due to variations in subsurface density. Gravity meters are essentially a fine mechanical balance consisting of a mass supported by a spring. Changes in gravity pull the mass against the restoring force of the spring. The amount of adjustment necessary to bring the spring back to its null position is an indicator of the strength of the gravity field. The LaCoste & Romberg gravimeter uses a zero-length spring, which theoretically collapses to a length of zero in the absence of any outside forces, i.e. the tension is directly proportional to the length of the spring.

SURVEY PROCEDURES

Gravity readings were taken at 25 m intervals on lines 7650N to 8600N (50 m line spacing) using a LaCoste & Romberg Model G Gravity Meter (see "INSTRUMENT SPECIFICATIONS"). Readings were taken as close as possible to flagged grid markers, which were generally tied to trees. The gravity meter was placed on a concave, long-legged, base-plate tripod, whose legs were sunk into the ground for stability. The gravity meter reading and the time of each reading were entered into a logbook. The height of the edge of the plate was measured and recorded as the instrument height. In the event that a station needed to be reoccupied, a 20 - 30 cm circle with a dot in the centre was spray-painted (fluorescent orange) on the ground to mark the station. The occasional station had to be relocated along the grid line or skipped entirely due to terrain complications. Such complications included swampy ground where a steady reading couldn't be taken, steep ground where there was no convenient spot to place the gravimeter, and creeks where it was unsafe to take a reading. A base station reading in the clearing in the southern end of the grid at 7900N/2550E was repeated at the beginning and end of each survey day to monitor *instrument drift*. A few stations were also re-read for additional drift monitoring or to check for *tares* (sudden shifts in the readings due to the gravity meter receiving a slight knock during the course of the survey). Note that the baseline at 2500E was not surveyed. Details of the survey coverage are listed below in Table 1 and the survey grid is shown in Figure 2.

Some difficulties were encountered during the course of the survey. Originally, the survey plan included up to 120 stations on Fowler Lake. However, the lake surface only froze over toward the end of the survey period after an intense cold snap, and although the thickness of ice was sufficient to walk on (carefully) and a survey grid was hence flagged in across the lake, the ice thickness was not great enough to obtain a gravity reading. Any slight vertical movement of the ice surface, due for instance, to wind action across the surface, is enough to cause wild fluctuations in the gravity meter reading and hence no useful data could be obtained. Ice thickness of over a foot, and preferably over two feet, are required to obtain a reasonably stable gravity reading. An additional complication arose during an extremely cold day on 15 December, when thick frost formed inside the gravity meter and rendered the levels and thermometer unreadable.



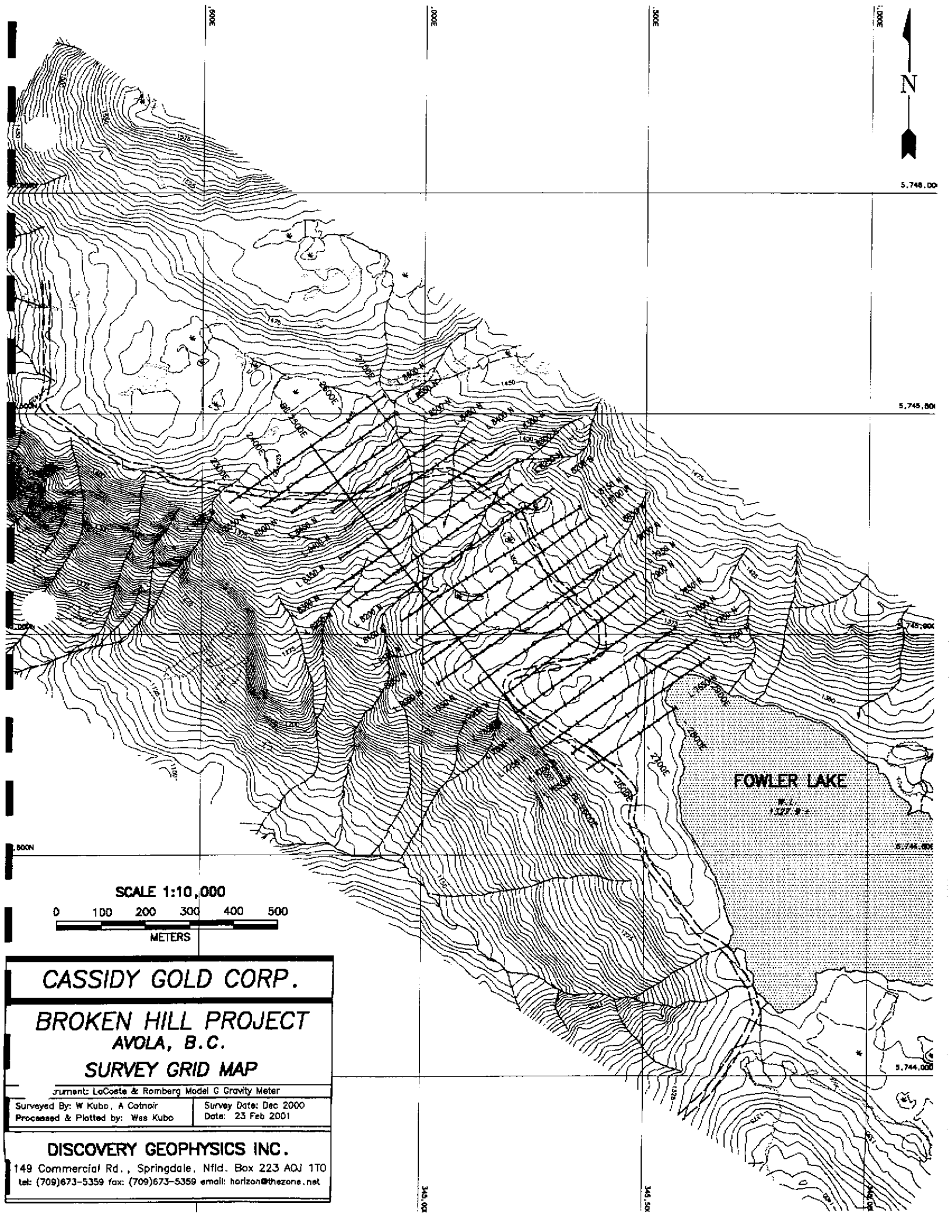
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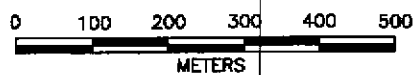
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SCALE 1:10,000



CASSIDY GOLD CORP.

**BROKEN HILL PROJECT
AVOLA, B.C.**

SURVEY GRID MAP

Instrument: LaCoste & Romberg Model G Gravity Meter

Surveyed By: W Kubo, A Colnoir

Survey Date: Dec 2000

Processed & Plotted by: Was Kubo

Date: 23 Feb 2001

DISCOVERY GEOPHYSICS INC.

149 Commercial Rd., Springdale, Nfld. Box 223 A0J 1T0
tel: (709)673-5359 fax: (709)673-5359 email: horizon@thezone.net

345,00

345,00

345,00

TABLE 1: Gravity survey coverage

Line	Stations	Length (m)
7650N	2558E to 2800E	242.5
7700N	2550E to 2925E	375.0
7750N	2500E to 2925E	425.0
7800N	2500E to 2900E	400.0
7850N	2500E to 2900E	400.0
7900N	2500E to 2900E	400.0
7950N	2450E to 2900E	450.0
8000N	2400E to 2900E	500.0
8050N	2400E to 2900E	500.0
8100N	2425E to 2900E	475.0
8150N	2425E to 2900E	475.0
8200N	2450E to 2875E	425.0
8250N	2350E to 2825E	475.0
8300N	2350E to 2850E	500.0
8350N	2400E to 2850E	450.0
8400N	2450E to 2800E	350.0
8450N	2450E to 2750E	300.0
8500N	2375E to 2700E	325.0
8550N	2325E to 2700E	375.0
8600N	2275E to 2700E	425.0

	Total	8.3 km

A total of 13 station locations and elevations (spread over the survey area) in NAD83 UTM were determined using a handheld GPS. All other station locations were determined by numerically interpolating and extrapolating from these 13 points. The station elevations were surveyed using a GDD hydrostatic chain level (see "INSTRUMENT SPECIFICATIONS"). This level measures the relative elevation between two points by sensing hydrostatic pressure within an oil filled tube and survey chain. Since the GDD level only measures relative elevations, every reading has to be tied to the network of stations, in order to calculate an elevation that is relative to a common point with a known elevation. The benchmark point was chosen as 7900N/2525E. Also, to correct for cumulative errors due to instrument drift, all readings must be taken in closed loops that are tied into the network of known elevation points. The elevation control network was established at stations on every survey line close to the road crossing using the same looping technique, before

the gravity survey was carried out on these lines. The elevation surveyor worked ahead of the gravity operator, setting up and marking the station and taking slope measurements. When the gravity reading was complete, an elevation reading was recorded and the survey proceeded to the next station.

In order to map the near station terrain, the level operator took four slope readings at each station. A clinometer was used to sight the slope in the grid north, east, south and west directions. These readings were input for a near-station terrain correction using the sloping-wedge technique (Barrows and Fett 1991).

DATA PROCESSING AND PRESENTATION

Station locations are determined from the 13 handheld GPS control points located on the chained grid. The Geosoft XYFILL program is used to interpolate and extrapolate UTM locations for the entire grid. The relative elevations from the GDD electronic level are entered into a spreadsheet at the end of each survey day. The relative elevation at each point in a loop is first determined relative to the starting point on the road by adding individual relative elevations. When the loop is closed off, the summed elevation for the loop is generally non-zero due to errors and instrument drift. This is corrected by dividing the loop error by the number of stations and then cumulatively adjusting each station elevation by that amount, thus bringing the summed elevation for the loop back to zero. The corrected relative elevations are then tied into the entire network through the road control points. This provides an absolute elevation at every point with a relative average accuracy of ± 2 cm. Note that the GPS benchmark elevation of 1400 m at 7900N/2525E was changed to 1348 m to better match the DEM derived elevation. This resulted in a mean difference between DEM and gravity elevations that was as close to zero as possible.

The slope measurements are input into a spreadsheet routine that calculates the gravitational effect of a quarter wedge of uniform slope θ out to radius R (Barrows and Fett, 1991).

$$g_w = \frac{1}{2} \pi G \rho R (1 - \cos \theta)$$

where G is the gravitational constant and ρ is the density of the terrain.

These near-station terrain corrections ranged from 0.01 to 0.31 mGals over the survey area for the selected radius of 25 m.

A digital elevation model (DEM) was prepared using orthophoto techniques by Eagle Mapping Services Ltd. This model consisted of elevation data at a 25 m interval over a 1.5 km x 3 km area covering the survey grid. In addition, there was elevation data at a regular 50 m interval (plus along hydrological features) extending approximately 2 km past the more detailed area. The coloured and contoured DEM is shown in a 1:5000 scale map in Appendix B.

An accurate DEM allows a precise terrain correction to be calculated for every station using "RasterTC", a DEM-based, integrated-surface, terrain correction program (Cogbill, 1990). RasterTC performs terrain corrections over two zones, deemed the inner and outer zone. The inner zone extends from 25 to 250 m out from the station and the outer zone extends from 250 to 2500 m from the station. The supplied DEM is used to calculate an elevation surface in each of the zones. Terrain corrections are calculated independently for every station. The actual elevations of the gravity stations are not used. Instead, the elevation on the surface at the station location is used, thus avoiding any bias that may exist between actual and DEM elevations.

The RasterTC terrain corrections over the survey area are depicted in a colour gridded and contoured map in Appendix B. The combined inner and outer zone terrain corrections ranged from 2.18 to 7.57 mGals over the survey area, which is some ten times the expected amplitude from a real geologic body. Hence, in this mountainous area, the terrain effect can produce false anomalies that are greater in size and amplitude than a real geological feature, and in this case at least, have the appropriate shape of the gravity field from a real geologic target.

All gravity data processing was carried out using a specialized application from LaCoste & Romberg and Geotools Corp. called "GravMaster". This program uses MS-Excel spreadsheets for data input and output (see Appendix A). The program first converts the gravity meter readings from arbitrary units to mGals using the scale factor chart supplied with the instrument. Earth tide corrections are then determined for each reading using the recorded date and time and the UTM

station locations. The tide corrected gravity readings are then corrected for instrument drift and tares using the base station and repeat station readings, linearly interpolating any differences in these repeat readings over the time interval between readings. The station elevations, copied into the spreadsheet from the GDD level processing output, are used to determine the combined free-air and Bouguer slab, elevation corrections. The Bouguer correction is determined for a range of slab densities from 2.5 to 2.8 g/cm³ in order to determine the optimal density for the survey area (i.e. the density that results in the least correlation between final corrected gravity and elevation).

The corrected, relative, gravity readings are then converted to absolute gravity values by inputting into GravMaster the known absolute gravity value of 980965.31 mGals at the control station at the Sandman Inn in Blue River (Canadian Gravity Standardization Net Station No. 9051-82). As a result, the corrected, absolute gravity values at the Broken Hill property can be tied into the GSC regional gravity grid of Canada.

The final step of the gravity processing procedure is to calculate the theoretical gravity at every station using an internationally accepted formula for the gravity field of the World Geodetic System (1984) reference ellipsoid: i.e. the US National Imagery and Mapping Agency (1998) formula (Blakely, 1995, pg. 135). The gravity stations locations were used to calculate the theoretical gravity at each station.

The “simple Bouguer gravity” is calculated by subtracting the theoretical ellipsoid gravity from the observed and corrected absolute gravity at each station. The “complete Bouguer gravity” is found by adding the near-station wedge, and inner and outer zone DEM terrain corrections at each station to the simple Bouguer gravity. By comparing the complete Bouguer gravity to the elevation map, it was determined that a density of 2.7 g/cm³ showed the least correlation between Bouguer gravity and terrain features. The final accumulated error of the complete Bouguer gravity is estimated to be about ±0.03 mGals (reading error: 0.005 mGals; drift correction: 0.002 mGals; elevation correction: 0.008 mGals; terrain correction: 0.015 mGals; all other corrections have negligible errors).

The complete Bouguer gravity are listed in Appendix A and displayed as a colour gridded and contoured map in Appendix B.

DISCUSSION OF RESULTS

After adding the terrain effect to the Bouguer gravity, we are left with a fairly flat gravity field over most of the survey grid except for an area of elevated gravity from line 8200N to line 8500N, plus additional gravity highs at a few locations along the edges of the survey grid. The latter anomalies are likely due to residual terrain effects which were not completely eliminated by the terrain correction routine; probably because of minor inaccuracies in the DEM. Note that they generally occur where the terrain is steepest.

The 300 m by 300 m area between line 8200N and 8500N with elevated gravity values of about 0.4 mGals above background should be considered geologically anomalous. The relatively abrupt edges and flat top of this gravity high suggest that it is due to a relatively shallow geologic formation with sharp boundaries – possibly faulted. The anomalous area does not appear to be due to a deeply buried massive body. The anomaly is consistent with a bounded, flat-lying to gently dipping, high density, stratigraphic formation, such as a sedex massive sulphide deposit. However, other high density formations such as a mafic sill or an iron/magnesium-rich exhalite could be causing the anomaly.

The undulating character of the gravity high suggests that the causative formation is not laterally uniform. Small peaks in the gravity field may indicate areas where the formation has greater density, presumably due to increased concentrations of high-density mineralization, or to areas where the formation is thicker. In either case, these areas should receive first priority for drill testing.


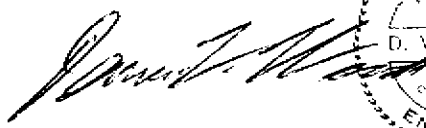
CONCLUSION AND RECOMMENDATIONS

After careful correction and processing of the survey data, especially the determination of an accurate terrain correction, the gravity survey on the Broken Hill property has resulted in the definition of an anomalous zone of higher residual gravity over the northern portion of the survey grid from line 8200N to line 8500N. This area of higher gravity of order 0.4 mGals is interpreted to be due to a fault-bounded, flat-lying to gently dipping, high-density, stratigraphic formation. A sedex massive sulphide deposit is one of many possible high-density formations that could be

causing this zone of elevated gravity. The undulating character of the gravity high suggests that the causative formation is not laterally uniform but may consist of pockets of greater density and/or thicker formation. It is recommended that some of these slightly elevated gravity highs should receive highest priority for follow-up drilling. Additional isolated gravity anomalies along the edges of the survey area are probably due to residual terrain correction effects due to imprecise DEM near abrupt changes in topographic slope.

The anomalous gravity zone is not coincident with the highest zinc geochemical anomalies, which occur immediately northwest of the survey area (the Vista prospect), and at the west end of lines 7700N, 7650N and further south (the Navan prospect). However, there is a single, isolated zinc geochemical anomaly at the west end of line 8400N that is in close proximity to the observed gravity anomaly. There is a very weak gravity high centred at 125E on line 7700N close to the Navan prospect, which could be targeted for drill testing. The north limit of the survey towards the Vista prospect may also have anomalously high gravity. However, additional gravity data should be collected both to the south and to the north of the present survey to better define any possible gravity features in these areas.

Respectfully submitted,



A circular professional seal for a Professional Engineer in the Province of Columbia. The seal contains the text: "PROFESSIONAL", "ENGINEER", "OF", "COLUMBIA", "PROVINCE". The name "D. V. WOODS" is stamped across the center of the seal.

Dennis V. Woods, Ph.D., P.Eng.
Consulting Geophysicist

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- Barrows, L.J., and Fett, J.D.: A sloping wedge technique for calculating gravity terrain corrections, *Geophysics*, vol. 56, no. 7, pp. 1061-1063, 1991.
- Blakely, R.J.: *Potential Theory in Gravity and Magnetics Applications*, Cambridge University Press, 1995.
- Cogbill, A.H.: Gravity terrain corrections calculated using Digital Elevation Models, *Geophysics*, vol. 55, no. 1, pp. 102-106, 1990.
- Telford, W.M., Geldarti, L.P. and Sheriff, R.E.: *Applied Geophysics Second Edition*, Cambridge University Press, 1990.

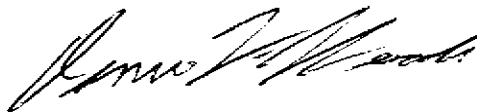
CERTIFICATE OF QUALIFICATIONS:

Dennis V. Woods

I, Dennis V. Woods of the municipality of Surrey, in the province of British Columbia, hereby certify as follows:

1. I am a Consulting Geophysicist with an office at #4 - 2320 King George Highway, Surrey, B.C., V4A 5A5.
2. I hold the following university degrees: Bachelor of Science, Applied Geology, Queen's University, 1973; Master of Science, Applied Geophysics, Queen's University, 1975; Doctor of Philosophy, Geophysics, Australian National University, 1979.
3. I am a registered professional engineer with The Association of Professional Engineers and Geoscientists of the Province of British Columbia (registration number 15,745), and of the Province of Newfoundland (registration number 03551).
4. I am an active member of the Society of Exploration Geophysicists, the Canadian Society of Exploration Geophysicists and the Australian Society of Exploration Geophysicists.
5. I have practised my profession as a field geologist (1971-1975), a research geoscientist (1974-1986), and a geophysical consultant (1979 to the present).
6. I have no direct interest in Cassidy Gold Corp. or the above described properties and projects, which are the subject of this report, nor do I intend to have any direct interest.

Dated at Surrey, in the Province of British Columbia, this 23rd day of February, 2001.



Dennis V. Woods, Ph.D., P.Eng.
Consulting Geophysicist



THE CHAIN+LEVEL

**The Fastest Way to Do
Surveys Without Visual
Contact. Period.**

The Chain+Level Is a Real Productivity Booster

Have you ever dreamed of surveying elevation profiles or road sections up to 5 times faster than with a total station without even cutting trees? It is now possible with the Chain+Level.

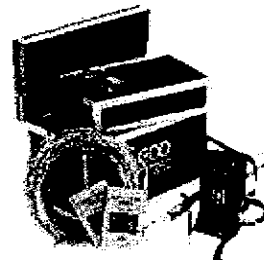
The Chain+Level, model D, is a true alternative to total stations and GPS (Global Positioning System) used to measure the difference of elevation between two points in woody or hilly areas. The Chain+Level gives additional flexibility to do fast and inexpensive topographic surveys in such environments.

Unique advantages of the Chain+Level

- No need to cut vegetation : time and cost savings.
- Field applications so far indicate a productivity improved by 200 to 500 % compared to total station surveys as there is no permit nor line cutting required.
- Faster surveys, less errors as the storage of the coordinates are transferred from the optional datalogger to the office computer at the end of each day.
- The high precision of the elevation

CONTENTS

- The Chain+Level**
- Operation**
- Specifications**
- Purchase - Rental**
- Testimonials**



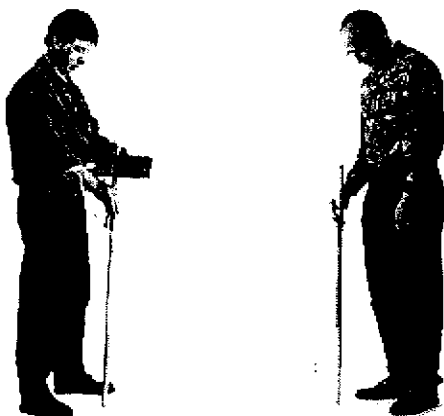
obtained (Z) from the Chain+Level can be combined with the coordinates (XY) from a relational GPS. With the Chain+Level, one can level between benchmarks spotted with a high-precision GPS or total station at every kilometer or so.

Successful applications so far include:

- Staking out longitudinal profiles and measuring cross-sections on roads, power lines, etc.
- Staking out flood basins, such as for hydroelectric dams.
- Topographic surveys, especially in woody areas.
- Geophysical surveys: gravity, seismic, electromagnetic, etc.
- Drill hole collars and geological section surveys.

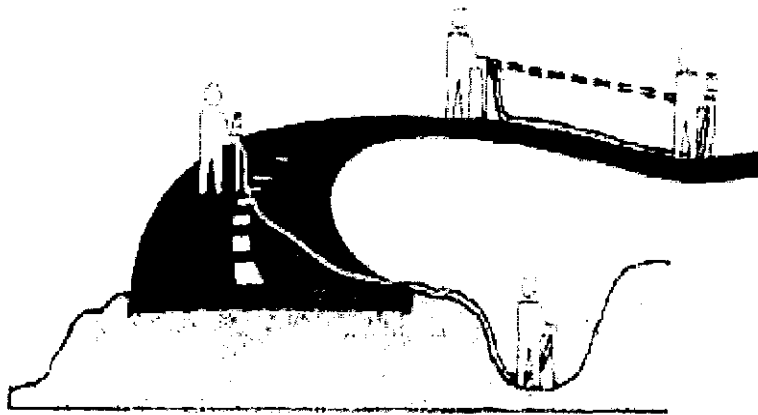
The Chain+Level is Really Fast and Simple to Operate

The GDD Chain+Level consists of a digital reading unit and two pressure sensors connected by a flexible 25 or 50-meter chaining cable containing a special fluid. Three other sensors measure temperature and density variations in the fluid. Readings are quick, and the meter indicates true elevation differences with high precision at any outside temperature.



The sensor rods at each end of the cable are placed on the points to be measured. The digital reading of the difference of elevation, V , is obtained instantly just by pressing one key. The rods are then transferred to new positions to read successive differences in elevation. No

visual contact is ever needed between the points to be measured.



Road survey crews report that they are at least three times more productive with a GDD Chain+Level than with a total station. They especially like the fact that it is so simple to operate.

Precision

For a one-kilometer profile, typical closure errors are less than 10 cm. The error on each station is less than 2 cm (0.1 foot).

For sections or profiles, the Chain+Level can measure a difference of elevation of ~15 meters in millimeters in a single reading with a precision of 0.2 %. The reading precision gives an immediate feedback of the reading quality the operator.

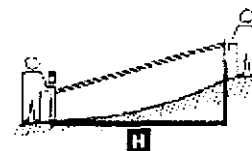
The reading unit with a cable, combined to the optional datalogger and the Multi-Carnet software for advanced surveys, allow to relate total station data or transform the data obtained to make them compatible with any COGO software. Users can use the datalogger with the Multi-Carnet software, choose the Chain+Level driver and later change the driver to work with almost any total stations on the market.

Operating the instrument

The operator presses the slope distance button and is given the exact slope distance (S) he must chain for a preset horizontal interval (H).

The slope distance (S) is chained. The two stations are now exactly H meters or feet apart horizontally. The pickets are driven in or a reference point is marked on the ground.

With sensor supports on top of the pickets, the



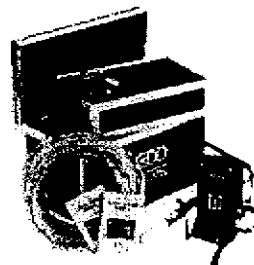
exact elevation difference between the two points is read instantly by pressing the vertical distance button.



Whether it is used by itself or jointly with a GPS or a total station, the Chain+Level is designed to suit your own requirements. You just have to choose between these options:

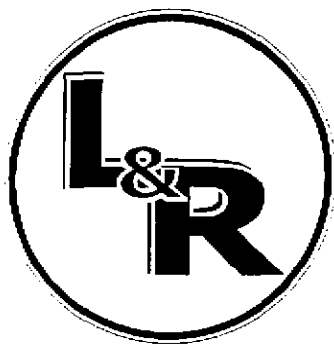
- The reading unit with a cable (the easiest way to use it)
- The reading unit with a cable, plus the optional datalogger and the GDD Chain+Level software enabling the recording and transferring of data to a computer in ASCII format at the end of the day. The ASCII format is a universal standard.

Specifications



Standard Components	
<ul style="list-style-type: none"> • Reading unit with leather case and cable • Battery charger (110 VAC, 220 VAC) • Extra bottle of fluid for the cable • Spare screws and screwdriver • Springs for gravimeter table • Instructions manual • Calibration tape • Shipping case 	
Options	<ul style="list-style-type: none"> - 6 aluminium sensor rods - Portable debubbling vacuum pump - Electronic notebook: Multi-Carnet (PC9000-MEMO4) - Extra 25 or 50-m cable (100 or 200 ft) - Special cable lengths available upon request
Measurements	
Range	± 15 m (± 50 ft)
Reading resolution	1 mm (0.005 ft)
Calibration stability	$\pm 0.2\%$ (less than a 2-cm error per 10-m elevation)
Typical closure error	<10 cm (4 in) on a 1-km (3/4 mile) traverse

(sigma)	
Elevation precision per station	<1 cm (0.04 in) on a 1-km (3/4 mile) traverse
Tested temperature range	-40°C to 40°C (-40°F to 104°F)
Reading Unit	
Size	25.7 x 11.1 x 12 cm (10 x 4.25 x 4.75 in)
Weight	2.5 kg (5.5 lb)
Case	Aluminum, shock resistant
Display	Adjustable contrast, backlight dot matrix (LCD)
Power source	12-V rechargeable battery
Usage	1.2 watt (100 mA)
Battery life	Up to 12 hours
Battery charger	110 VAC, 220 VAC
Cable	
Standard lengths	25 m and 50 m (100 and 200 ft)
Weight	2 kg / 30 m (4.5 lb / 100 ft)
Chaining cable	Robust, shock resistant, waterproof
Cable chained	At every 0.1 m (12 in)



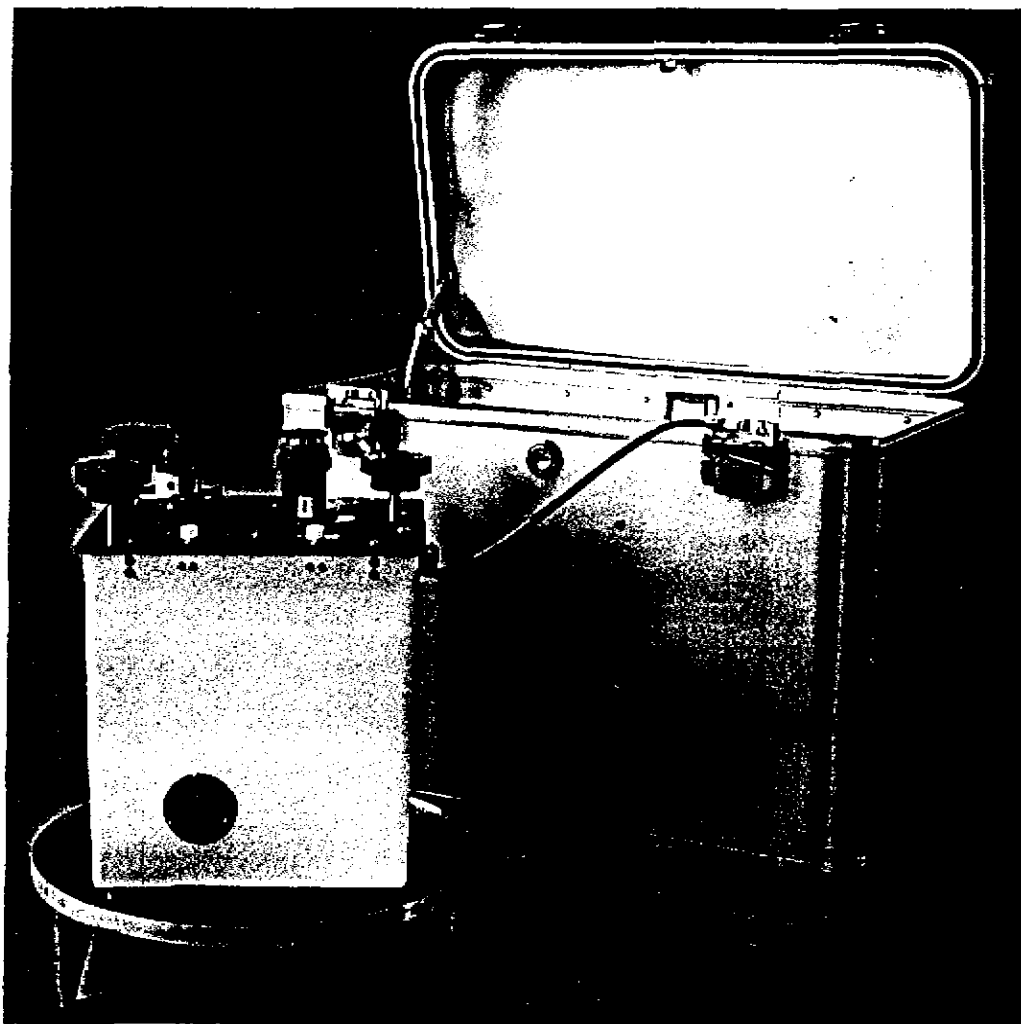
LaCoste & Romberg LLC

The first name in gravity since 1939

Land Gravity Meters

LaCoste & Romberg, manufacturer of high precision gravity meters since 1939, introduced the world's first worldwide range gravity meter — the Model G meter — in 1959. A more sensitive version — the Model D meter — was introduced in 1968. LaCoste & Romberg land gravity meters have become the standard by which all other gravity meters are currently measured. They have a proven record of reliability and ruggedness, so much so that virtually all L&R meters manufactured to date are still in use.

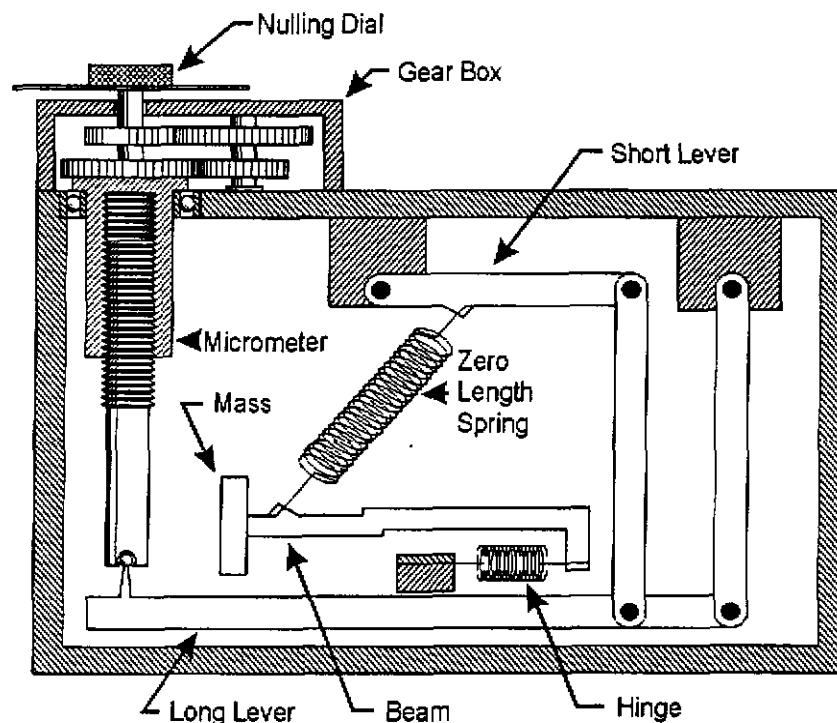
The two types of land gravity meters — the Model G (geodetic) meter and the Model D (microgal) meter — both use the famous patented L&R zero-length™ spring suspension system. The Model G meter has been the standard of the industry for almost 40 years. We estimate that more than 10 million gravity stations have been observed with this meter on every continent. The Model D meter is the preferred instrument for microgravity applications. The main difference is that the Model D meter has two screws - a coarse screw that gives the meter worldwide range, and a limited range fine screw that has greater accuracy than the single screw in the Model G meter.



TECHNICAL FEATURES

Accuracy: Both the Model G and the Model D have a reading precision of 0.001 mGal (1 μ Gal) using the standard optical system. Reading precision using the optional MVR system is 0.0001 mGal (0.1 μ Gal). The measurement repeatability of the Model G is under 0.01 mGal, while the repeatability of the Model D with its fine adjustment system is under 0.005 mGal (5 μ Gal). By reading the beam position with an optional electronic system, the Model G's repeatability can be improved to under 0.005 mGal (5 μ Gal). The LaCoste & Romberg sensor uses a 12 g tungsten proof mass (unlike light-weight quartz sensors whose proof masses are under a 0.1 g). Our denser metal sensor is fundamentally capable of higher system accuracies than any other portable gravity sensor. In one study, the thermal noise floor of the L&R sensor was shown to be under 0.014 μ Gal. While this level of accuracy is not yet achievable in field measurements, it shows that the LaCoste & Romberg meter is extremely well-designed for the task of measuring remarkably small variations in the earth's gravity.

Reliability: The basic LaCoste & Romberg sensor has been manufactured since 1939. The Model G Meter has been manufactured since 1959 and the Model D Meter since 1968. Both meters have undergone gradual evolution in design details that have improved their accuracies and reliability. New meters employ components that are designed for long life and require little maintenance. Some meters have undergone automobile and airplane accidents without sustaining any sensor damage whatsoever. Our sensors contain rugged metal components which can reliably withstand extreme field conditions, unlike quartz spring instruments which rely upon delicate glass parts. L&R meters improve with age, unlike quartz meters which tend to become more fragile with age. In fact our land meters are so robust, NASA chose to take a modified LaCoste & Romberg Model G Meter to the moon on Apollo 17.



Schematic diagram showing L&R's famous patented zero-length spring suspension system. This system, developed over 60 years, has a thermal noise floor of less than 0.014 μ Gal.

Range: The G-Meter has a worldwide range of 7,000 mGal without resetting. The Model D has a fine adjustment range of 200 mGal, which is adequate for most microgravity applications. A course adjustment screw allows the Model D to be re-ranged to any location worldwide.

Drift: Gravity meter drift for a new meter is less than 1 mGal per month. As a LaCoste & Romberg meter ages, the drift often improves to rates of less than 0.5 mGal per month. Our sensors are manufactured entirely of metal. Once initial expansions have taken place, the sensor does not radically change its characteristics with time, in fact they become more stable. By contrast, quartz spring sensors, because they are made of glass, tend to flow, devitrify, or crystallize with time. Because these are changes in state of the fundamental sensor, their drift rates can exceed 30 mGal per month and only degrade with time.



Model G meter with MVR digital feedback system.

Stable Factory Calibration: The calibration depends on a hardened micrometer screw and metal lever system. It is stable over the life of the meter and is not affected by loss of operating temperature. Our comprehensive calibration procedure takes place in two stages. In the first stage, a computer-operated testing apparatus simulates the full worldwide gravity range by

systematically applying different proof masses to the beam. In the final stage, we rigorously field test our instruments over the highest precision gravity calibration range in the world, located in New Mexico.



Ease of use and rugged reliability are the reasons why L&R's land gravity meters have surveyed more gravity stations than any other meter.

Sensor Environment: The sensor is sealed in a dry nitrogen atmosphere. The housing is temperature controlled and protected from magnetic fields. Because the sensor is permanently sealed, it is unaffected by changes in humidity. The sensors have a built-in fail-safe pressure compensation system. If the pressure seals fail for any reason during a survey, reasonable accuracy can be maintained until the meter is serviced.

RELIABLE FACTORY SERVICE

LaCoste & Romberg's famous reliable factory service stands behind every gravity meter we produce. Our trained technicians have many years of experience at building and maintaining gravity meters. There are three basic types of factory service: Targeted Service, General Service and Comprehensive Service (recommended every eight years).

OPTIONS

Electronic Readout: A Capacitive Positioning Indicator (CPI) system used to read the beam without using the optical system. Improves the meter repeatability to below 0.005 mGal.

MVR: High accuracy electronic feedback system which keeps the beam at null. Produces a high accuracy gravity reading through the use of its feedback voltage. Electronic levels and dial clamp options are recommended.

Pendulum Levels: High accuracy electronic level indicator system.

Ceramic Levels: A resistive liquid electronic level indicator system.

Variable Damping: A special adjustment allowing the user to change the beam damping in cases where vibrations or ground motions are a problem.

Nulling Dial Clamp: Used to prevent the dial from being moved during measurements. Recommended in cases where meter is used to observe earth tides or for the MVR option.

High Speed Crank: Useful for resetting the counter over a large interval between surveys.

Extended Range (Model D only): The fine adjustment screw can be built with a 300 mGal range rather than the standard 200 mGal range.

Calibrated Course Screw (Model D only): The course adjustment screw can be calibrated like a Model G meter with a worldwide range.

TIDEAQ: A 16 bit data acquisition system for digitizing and recording land meter output for earth tide monitoring applications.

LAND METER SPECIFICATIONS

System Performance

G Meter System Precision 0.001 mGal
G Meter System Repeatability 0.01 mGal
G Meter Accuracy 0.04 mGal or better

D Meter System Precision 0.001 mGal
D Meter System Repeatability 0.005 mGal
D Meter Accuracy 0.01 mGal or better

G Meter MVR option System Precision 0.0001 mGal
G Meter MVR option System Repeatability 0.005 mGal
G Meter MVR option Accuracy 0.01 mGal or better

Drift: 1.0 mGal (or better) per month new,
0.5 mGal (or better) per month after 2 years

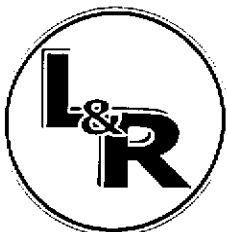
Range: G Meter - 7,000 mGals (worldwide),
D Meter - 200 mGals, resetable for worldwide use

Size and Weight

Size: 7.75 x 7.0 x 9.875 inch; 19.7 x 17.8 x 25.1 cm
Weight of meter: 7 lbs; 3.2 kg
Weight of battery: 5 lbs; 2.3 kg
Weight of meter, battery and carrying case: 22 lbs; 10.0 kg

Warranty

All new land gravity meters come with a one-year warranty on parts and labor.



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APPENDIX A

Tabulation of Gravity Data

GravMaster Input

Line	Station	Comment	ID	X	Y	Elev (m)	Time	Date	Instv	InstH (m)
base	base	base out	000	345221.2	5744890	1348.231	12:46	12/3/00	4249.90	0.39
7900N	2550	v.shaky	083	345221.2	5744890	1348.231	12:46	12/3/00	4249.90	0.39
7900N	2575		084	345239.4	5744904	1348.826	13:32	12/3/00	4249.99	0.45
7900N	2600		085	345257.6	5744919	1349.579	13:45	12/3/00	4250.04	0.48
7900N	2625		086	345275.8	5744933	1349.892	13:56	12/3/00	4250.11	0.44
7900N	2650		087	345294.0	5744947	1349.434	14:05	12/3/00	4250.29	0.42
7900N	2675		088	345312.2	5744961	1347.779	14:15	12/3/00	4250.66	0.50
7900N	2700		089	345330.4	5744975	1346.201	14:25	12/3/00	4251.00	0.43
7900N	2725		090	345348.6	5744989	1346.978	14:37	12/3/00	4250.74	0.46
7900N	2750	shaky	091	345366.8	5745003	1349.447	14:48	12/3/00	4250.31	0.37
7900N	2775		092	345385.0	5745017	1353.579	14:58	12/3/00	4249.37	0.46
7900N	2800		093	345403.2	5745031	1356.559	15:10	12/3/00	4248.77	0.43
7900N	2825	shaky	094	345421.4	5745045	1360.866	15:21	12/3/00	4247.87	0.41
7900N	2850		095	345439.6	5745060	1367.763	15:29	12/3/00	4246.55	0.40
base	base	base in	000	345221.2	5744890	1348.231	15:53	12/3/00	4249.91	0.38
base	base	base out	000	345221.2	5744890	1348.231	9:17	12/4/00	4249.82	0.36
7900N	2875		096	345457.8	5745074	1375.219	10:03	12/4/00	4244.98	0.48
7900N	2900		097	345476.0	5745088	1382.509	10:15	12/4/00	4243.52	0.46
7850N	2900	new line	080	345538.5	5745053	1383.906	10:32	12/4/00	4243.22	0.45
7850N	2875	shaky	079	345518.0	5745039	1375.397	10:46	12/4/00	4244.93	0.49
7850N	2850		078	345497.6	5745024	1367.205	10:53	12/4/00	4246.64	0.49
7850N	2825		077	345477.1	5745010	1359.724	11:00	12/4/00	4248.11	0.48
7850N	2800	shaky	076	345456.6	5744995	1354.378	11:08	12/4/00	4249.22	0.44
7850N	2775		075	345436.2	5744981	1351.311	11:15	12/4/00	4249.89	0.45
7850N	2750	no marker	074	345415.7	5744966	1349.838	11:22	12/4/00	4250.20	0.46
7850N	2725		073	345395.2	5744952	1349.968	11:28	12/4/00	4250.19	0.45
7850N	2700		072	345374.8	5744937	1350.386	11:34	12/4/00	4250.14	0.47
7850N	2675		071	345354.3	5744923	1351.036	11:42	12/4/00	4249.99	0.45
7850N	2650	shaky	070	345333.8	5744908	1352.517	11:50	12/4/00	4249.62	0.45
7850N	2625	v. shaky	069	345313.3	5744894	1352.218	12:00	12/4/00	4249.67	0.42
7850N	2600		068	345292.9	5744879	1352.204	12:08	12/4/00	4249.43	0.44
7850N	2575		067	345272.4	5744865	1350.576	12:15	12/4/00	4249.53	0.42
7850N	2550		066	345251.9	5744850	1348.895	12:22	12/4/00	4249.53	0.48
7850N	2525		065	345231.5	5744836	1345.791	12:48	12/4/00	4249.82	0.48
7850N	2500	steep!!	064	345211.0	5744821	1335.642	13:06	12/4/00	4251.43	0.50
7900N	2500		081	345182.5	5744862	1343.325	13:22	12/4/00	4249.96	0.44
7900N	2525		082	345203.0	5744876	1348.015	13:29	12/4/00	4249.41	0.51
base	base	Base in	000	345221.2	5744890	1348.231	13:35	12/4/00	4249.80	0.36
base	base	Base out	000	345221.2	5744890	1348.231	13:35	12/4/00	4249.80	0.36
7800N	2550		049	345280.4	5744810	1345.717	13:44	12/4/00	4249.97	0.45
7800N	2575	shaky	050	345300.9	5744825	1348.443	13:52	12/4/00	4249.82	0.44
7800N	2600		051	345321.4	5744839	1353.520	13:59	12/4/00	4248.99	0.47
7800N	2625		052	345341.8	5744854	1355.212	14:06	12/4/00	4248.91	0.45
7800N	2650	shaky	053	345362.3	5744868	1356.533	14:16	12/4/00	4248.74	0.48
7800N	2675		054	345382.8	5744883	1356.165	14:22	12/4/00	4248.99	0.42
7800N	2700		055	345403.3	5744897	1352.615	14:29	12/4/00	4249.77	0.47
7800N	2725	v. shaky	056	345423.7	5744912	1351.722	14:37	12/4/00	4249.98	0.42
7800N	2750		057	345444.2	5744926	1352.666	14:45	12/4/00	4249.70	0.49
7800N	2775		058	345464.7	5744941	1351.694	14:51	12/4/00	4249.86	0.40
7800N	2800		059	345485.1	5744955	1350.765	14:59	12/4/00	4249.95	0.47
7800N	2825		060	345505.6	5744970	1349.716	15:05	12/4/00	4250.01	0.43
7800N	2850	steep	061	345526.1	5744984	1355.246	15:16	12/4/00	4248.86	0.42
7800N	2875	steep	062	345546.5	5744999	1360.529	15:23	12/4/00	4247.78	0.45
base	base	Base In/hard to read	000	345221.2	5744890	1348.321	15:42	12/4/00	4249.88	0.36
base	base	Base Out	000	345221.2	5744890	1348.321	9:08	12/5/00	4249.78	0.36
7800N	2900		063	345567.0	5745013	1369.110	9:43	12/5/00	4245.97	0.51
7750N	2925	v. steep	046	345616.0	5744987	1363.193	10:05	12/5/00	4247.03	0.50
7750N	2900	steep	045	345595.5	5744972	1352.973	10:16	12/5/00	4249.04	0.45
7750N	2875	v. shaky	044	345575.0	5744958	1347.058	10:23	12/5/00	4250.21	0.45
7750N	2850		043	345554.6	5744943	1343.581	10:29	12/5/00	4251.00	0.46
7750N	2825		042	345534.1	5744929	1343.369	10:36	12/5/00	4251.15	0.47
7750N	2800	shaky	041	345513.6	5744914	1343.213	10:43	12/5/00	4251.32	0.42
7750N	2775	v. shaky	040	345493.2	5744900	1345.600	10:50	12/5/00	4250.91	0.45
7750N	2750		039	345472.7	5744885	1350.416	11:00	12/5/00	4250.05	0.40
7750N	2725		038	345452.2	5744871	1353.225	11:08	12/5/00	4249.53	0.42
7750N	2700		037	345431.8	5744856	1354.381	11:15	12/5/00	4249.22	0.48
7750N	2675		036	345411.3	5744842	1354.277	11:21	12/5/00	4249.30	0.47
7750N	2650	v. shaky	035	345390.8	5744827	1356.478	11:29	12/5/00	4248.71	0.42
7750N	2625		034	345370.3	5744813	1354.783	11:37	12/5/00	4248.89	0.45
7750N	2600		033	345349.9	5744798	1351.395	11:43	12/5/00	4249.35	0.44
7750N	2600	tare check	033	345349.9	5744798	1351.395	11:50	12/5/00	4249.37	0.42
7750N	2575		032	345329.4	5744784	1346.004	11:57	12/5/00	4250.28	0.44
7750N	2550		031	345308.9	5744769	1345.265	12:05	12/5/00	4249.79	0.44

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7750N	2525	v. steep	030	345288.5	5744755	1334.928	12:20	12/5/00	4251.51	0.43
7750N	2500	v. steep	029	345268.0	5744740	1325.169	12:34	12/5/00	4253.23	0.47
7800N	2500	steep	047	345239.5	5744781	1332.761	12:47	12/5/00	4251.81	0.46
7800N	2525	steep	048	345260.0	5744796	1340.142	13:01	12/5/00	4250.58	0.42
7800N	2550	R12/04/00	049	345280.4	5744810	1345.717	13:10	12/5/00	4249.96	0.46
7700N	2575		014	345357.9	5744744	1343.938	13:39	12/5/00	4250.65	0.46
7700N	2600		015	345378.4	5744758	1345.735	13:45	12/5/00	4250.68	0.45
7700N	2625		016	345398.8	5744773	1347.766	13:51	12/5/00	4250.46	0.45
7700N	2650	shaky	017	345419.3	5744787	1348.192	13:59	12/5/00	4250.50	0.39
7700N	2675		018	345439.8	5744802	1349.517	14:05	12/5/00	4250.29	0.36
7700N	2700		019	345460.3	5744816	1349.335	14:12	12/5/00	4250.33	0.40
7700N	2725	shaky	020	345480.7	5744831	1346.373	14:19	12/5/00	4250.90	0.42
7700N	2750		021	345501.2	5744845	1345.048	14:25	12/5/00	4251.06	0.45
7700N	2775		022	345521.7	5744860	1338.393	14:32	12/5/00	4252.28	0.47
7700N	2800		023	345542.1	5744874	1334.571	14:40	12/5/00	4252.95	0.48
7700N	2825		024	345562.6	5744889	1332.305	14:48	12/5/00	4253.25	0.45
7700N	2850	shaky	025	345583.1	5744903	1329.745	14:56	12/5/00	4253.63	0.43
7700N	2875		026	345603.5	5744918	1333.981	15:04	12/5/00	4252.68	0.40
7700N	2900		027	345624.0	5744932	1339.801	15:14	12/5/00	4251.57	0.45
7700N	2925	E.O.L.	028	345644.5	5744947	1347.368	15:21	12/5/00	4250.16	0.39
base	base	Base In	000	345221.2	5744890	1348.321	16:47	12/5/00	4249.82	0.34
base	base	Base Out	000	345221.2	5744890	1348.321	9:12	12/6/00	4249.81	0.34
7650N	2795	nr lake/v shaky/bad reading	011	345566.5	5744830	1328.592	10:39	12/6/00	4253.88	0.49
7650N	2775	shaky	010	345550.2	5744819	1334.530	10:49	12/6/00	4252.99	0.48
7650N	2750	shaky	009	345529.7	5744804	1340.718	10:57	12/6/00	4251.77	0.49
7650N	2725		008	345509.2	5744790	1341.828	11:04	12/6/00	4251.74	0.43
7650N	2700		007	345488.8	5744775	1344.002	11:11	12/6/00	4251.31	0.42
7650N	2675		006	345468.3	5744761	1344.861	11:18	12/6/00	4251.09	0.49
7650N	2650		005	345447.8	5744746	1345.378	11:25	12/6/00	4251.10	0.45
7650N	2625		004	345427.3	5744732	1348.246	11:31	12/6/00	4250.30	0.47
7650N	2600		003	345406.9	5744717	1348.438	11:39	12/6/00	4250.04	0.42
7650N	2575	road	002	345386.4	5744703	1345.297	11:48	12/6/00	4250.27	0.48
7650N	2557	E.O.L.	001	345371.7	5744692	1339.701	11:57	12/6/00	4250.99	0.42
7700N	2550	steep	013	345337.4	5744729	1340.382	12:10	12/6/00	4250.83	0.44
7700N	2575	hard to read/R12/05/00	014	345357.9	5744744	1343.938	12:20	12/6/00	4250.62	0.46
7950N	2775		110	345374.2	5745064	1354.710	14:19	12/6/00	4249.06	0.47
7950N	2800	v. shaky	111	345394.7	5745078	1359.896	14:27	12/6/00	4247.90	0.50
7950N	2825		112	345415.2	5745093	1365.322	14:33	12/6/00	4246.90	0.46
7950N	2850		113	345435.7	5745107	1371.657	14:42	12/6/00	4245.68	0.47
7950N	2875		114	345456.2	5745122	1377.090	14:49	12/6/00	4244.58	0.47
7950N	2900	v.steep/E.O.L.	115	345476.7	5745136	1386.608	15:07	12/6/00	4242.66	0.33
8000N	2900		136	345442.4	5745178	1387.460	15:21	12/6/00	4242.44	0.46
8000N	2875		135	345421.9	5745164	1382.001	15:27	12/6/00	4243.61	0.38
8000N	2850		134	345401.5	5745149	1376.770	15:32	12/6/00	4244.68	0.50
8000N	2825		133	345381.0	5745135	1370.132	15:38	12/6/00	4246.02	0.52
base	base	Base In	000	345221.2	5744890	1348.321	15:50	12/6/00	4249.79	0.35
base	base	Base Out	000	345221.2	5744890	1348.321	9:52	12/7/00	4249.76	0.33
8000N	2800		132	345360.5	5745120	1364.852	10:09	12/7/00	4246.99	0.42
8000N	2775		131	345340.1	5745106	1360.003	10:15	12/7/00	4247.98	0.43
8000N	2750		130	345319.6	5745091	1355.145	10:21	12/7/00	4248.96	0.46
8000N	2725	shaky	129	345299.1	5745077	1347.242	10:30	12/7/00	4250.53	0.45
8000N	2700		128	345278.7	5745062	1346.829	10:35	12/7/00	4250.61	0.46
8000N	2675		127	345258.2	5745048	1346.695	10:41	12/7/00	4250.58	0.46
8000N	2650	shaky	126	345237.7	5745033	1344.116	10:48	12/7/00	4250.99	0.45
8000N	2625		125	345217.3	5745019	1337.925	10:54	12/7/00	4252.21	0.39
8000N	2600	near creek	124	345196.8	5745004	1335.956	11:01	12/7/00	4252.49	0.45
8000N	2575	v. shaky!!	123	345176.3	5744990	1335.624	11:10	12/7/00	4252.48	0.43
7950N	2475	Grav only	099	345128.2	5744890	1345.673	11:18	12/7/00	4249.23	0.44
8000N	2550	road	122	345155.8	5744975	1335.693	11:25	12/7/00	4252.30	0.46
8000N	2550	tare check	122	345155.8	5744975	1335.693	11:27	12/7/00	4252.30	0.46
8000N	2525		121	345135.4	5744961	1335.427	11:36	12/7/00	4252.23	0.43
8000N	2500		120	345114.9	5744946	1336.092	11:41	12/7/00	4251.81	0.45
8000N	2475		119	345094.4	5744932	1335.623	11:46	12/7/00	4251.70	0.38
8000N	2450		118	345074.0	5744917	1331.366	11:53	12/7/00	4252.22	0.45
8000N	2425		117	345053.5	5744903	1323.950	12:00	12/7/00	4253.37	0.44
8000N	2400	E.O.L.	116	345033.0	5744888	1316.212	12:08	12/7/00	4254.59	0.43
7950N	2450		098	345107.7	5744875	1339.251	12:37	12/7/00	4250.11	0.46
7950N	2475	R120700	099	345128.2	5744890	1345.673	12:45	12/7/00	4249.32	0.46
7950N	2500		100	345148.7	5744904	1345.805	13:03	12/7/00	4249.66	0.46
7950N	2525		101	345169.2	5744919	1344.948	13:09	12/7/00	4250.20	0.41
7950N	2550		102	345189.7	5744933	1344.351	13:14	12/7/00	4250.58	0.48
7950N	2575		103	345210.2	5744948	1343.943	13:20	12/7/00	4250.88	0.40
7950N	2600		104	345230.7	5744962	1343.302	13:26	12/7/00	4251.08	0.37
7950N	2625		105	345251.2	5744977	1342.322	13:32	12/7/00	4251.40	0.40

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7950N	2650		106	345271.7	5744991	1342.637	13:40	12/7/00	4251.42	0.41
7950N	2675		107	345292.2	5745006	1342.666	13:47	12/7/00	4251.46	0.38
7950N	2700		108	345312.7	5745020	1342.853	13:54	12/7/00	4251.39	0.44
7950N	2750		109	345353.7	5745049	1346.504	14:10	12/7/00	4250.62	0.46
7950N	2775	R120600	110	345374.2	5745064	1354.710	14:25	12/7/00	4249.03	0.42
8050N	2750		151	345286.1	5745133	1355.178	14:32	12/7/00	4248.95	0.47
8050N	2775		152	345306.6	5745148	1362.477	14:41	12/7/00	4247.49	0.47
8050N	2800		153	345327.1	5745162	1366.702	14:47	12/7/00	4246.72	0.48
8050N	2825		154	345347.6	5745177	1371.431	14:54	12/7/00	4245.76	0.44
8050N	2850		155	345368.1	5745191	1376.627	15:00	12/7/00	4244.73	0.39
8050N	2875		156	345388.6	5745206	1381.747	15:06	12/7/00	4243.76	0.43
8050N	2900	E.O.L.	157	345409.1	5745220	1386.153	15:11	12/7/00	4242.88	0.47
base	base	Base In	000	345221.2	5744890	1348.321	15:25	12/7/00	4249.79	0.33
base	base	Base Out	000	345221.2	5744890	1348.321	9:21	12/8/00	4249.78	0.33
8100N	2900	steep/shaky	176	345374.8	5745262	1388.003	10:02	12/7/00	4242.17	0.42
8100N	2875		175	345354.3	5745248	1383.098	10:08	12/8/00	4243.22	0.47
8100N	2850	shaky	174	345333.9	5745233	1377.235	10:16	12/8/00	4244.45	0.35
8100N	2825		173	345313.4	5745219	1372.402	10:24	12/8/00	4245.33	0.45
8100N	2800		172	345292.9	5745204	1366.827	10:30	12/8/00	4246.53	0.42
8100N	2775		171	345272.5	5745190	1361.266	10:36	12/8/00	4247.66	0.44
8100N	2750		170	345252.0	5745175	1356.364	10:43	12/8/00	4248.67	0.45
8100N	2725		169	345231.5	5745161	1349.029	10:49	12/8/00	4250.11	0.41
8100N	2700		168	345211.1	5745146	1346.799	10:56	12/8/00	4250.59	0.38
8100N	2675		167	345190.6	5745132	1345.151	11:01	12/8/00	4250.87	0.46
8100N	2650		166	345170.1	5745117	1342.883	11:07	12/8/00	4251.29	0.43
8100N	2625	shaky	165	345149.7	5745103	1340.882	11:15	12/8/00	4251.61	0.48
8100N	2575		164	345108.7	5745074	1334.707	11:26	12/8/00	4252.63	0.45
8100N	2550		163	345088.3	5745059	1334.218	11:33	12/8/00	4252.59	0.40
8050N	2575	other line	144	345142.6	5745032	1334.606	11:41	12/8/00	4252.69	0.47
8100N	2525	road	162	345067.8	5745045	1330.801	11:46	12/8/00	4253.17	0.48
8100N	2500	BL2500E	161	345047.3	5745030	1327.042	11:52	12/8/00	4253.80	0.47
8100N	2475		160	345026.8	5745016	1324.449	11:58	12/8/00	4254.18	0.44
8100N	2450		159	345006.4	5745001	1321.976	12:04	12/8/00	4254.37	0.44
8100N	2425	E.O.L.	158	344985.9	5744987	1311.776	12:20	12/8/00	4256.27	0.46
8050N	2400		137	344999.1	5744930	1309.445	12:35	12/8/00	4256.32	0.43
8050N	2425		138	345019.6	5744945	1317.872	12:42	12/8/00	4254.96	0.43
8050N	2450		139	345040.1	5744959	1321.901	12:48	12/8/00	4254.47	0.35
8050N	2475		140	345060.6	5744974	1323.806	12:55	12/8/00	4254.25	0.42
8050N	2500	BL2500E	141	345081.1	5744988	1324.535	13:01	12/8/00	4254.36	0.48
8050N	2525		142	345101.6	5745003	1326.655	13:07	12/8/00	4254.09	0.50
8050N	2550		143	345122.1	5745017	1330.980	13:13	12/8/00	4253.28	0.46
8050N	2575	R120800	144	345142.6	5745032	1334.606	13:32	12/8/00	4252.66	0.49
8050N	2600		145	345163.1	5745046	1340.707	13:39	12/8/00	4251.54	0.45
8050N	2625		146	345183.6	5745061	1343.255	13:46	12/8/00	4251.21	0.46
8050N	2650		147	345204.1	5745075	1349.356	13:51	12/8/00	4250.09	0.45
8050N	2675		148	345224.6	5745090	1348.102	13:57	12/8/00	4250.41	0.45
8050N	2700	v. shaky!!	149	345245.1	5745104	1347.682	14:07	12/8/00	4250.33	0.39
8050N	2725		150	345265.6	5745119	1349.163	14:13	12/8/00	4250.16	0.46
8050N	2750	R120700	151	345286.1	5745133	1355.178	14:19	12/8/00	4248.98	0.48
8150N	2750		190	345225.0	5745205	1359.870	14:27	12/8/00	4247.96	0.47
8150N	2775		191	345246.2	5745218	1364.846	14:40	12/8/00	4246.95	0.44
8150N	2800		192	345267.4	5745232	1367.266	14:46	12/8/00	4246.58	0.46
8150N	2825	on top of 4 m ridge	193	345288.7	5745245	1373.065	14:52	12/8/00	4245.29	0.43
8150N	2850		194	345309.9	5745258	1374.012	14:57	12/8/00	4245.12	0.41
8150N	2875		195	345331.1	5745271	1376.470	15:04	12/8/00	4244.53	0.44
8150N	2900		196	345352.3	5745285	1381.324	15:09	12/8/00	4243.44	0.35
base	base	Base In	000	345221.2	5744890	1348.321	15:20	12/8/00	4249.84	0.33
base	base	Base Out	000	345221.2	5744890	1348.321	9:30	12/9/00	4249.84	0.33
8200N	2875	steep/shaky	214	345291.0	5745329	1378.478	10:10	12/9/00	4243.90	0.43
8200N	2850		213	345270.6	5745314	1372.395	10:16	12/9/00	4245.13	0.42
8200N	2825		212	345250.1	5745300	1367.532	10:22	12/9/00	4246.21	0.48
8200N	2800	frozen creek/swamp	211	345229.6	5745285	1365.204	10:28	12/9/00	4246.74	0.50
8200N	2775		210	345209.2	5745271	1364.551	10:34	12/9/00	4246.88	0.46
8200N	2750	road	209	345188.7	5745256	1360.931	10:42	12/9/00	4247.55	0.47
8200N	2725	frozen swamp	208	345168.2	5745242	1353.237	10:54	12/9/00	4249.09	0.52
8200N	2700	swamp/shaky	207	345147.8	5745227	1348.756	11:01	12/9/00	4249.98	0.46
8200N	2675	shaky	206	345127.3	5745213	1346.062	11:07	12/9/00	4250.52	0.49
8200N	2650	shaky	205	345106.8	5745198	1340.741	11:13	12/9/00	4251.35	0.48
8200N	2625	near creek	204	345086.3	5745184	1334.731	11:20	12/9/00	4252.46	0.44
8200N	2600	near creek	203	345065.9	5745169	1330.650	11:28	12/9/00	4253.15	0.44
8200N	2575	near creek	202	345045.4	5745155	1327.530	11:37	12/9/00	4253.64	0.45
8200N	2540	near creek	201	345016.8	5745134	1321.351	11:52	12/9/00	4254.76	0.54
8200N	2525	near creek	200	345004.5	5745126	1318.918	12:00	12/9/00	4255.12	0.38
8200N	2500	near creek	199	344984.0	5745111	1314.696	12:09	12/9/00	4255.82	0.43

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8200N	2475	near creek	198	344963.5	5745097	1311.578	12:16	12/9/00	4256.40	0.42
8200N	2450	E.O.L.	197	344943.1	5745082	1306.956	12:27	12/9/00	4257.12	0.52
8150N	2425		177	344952.0	5745030	1309.046	13:06	12/9/00	4256.74	0.42
8150N	2450		178	344872.5	5745044	1314.548	13:12	12/9/00	4255.83	0.45
8150N	2475		179	344893.0	5745058	1319.124	13:21	12/9/00	4255.03	0.48
8150N	2500	BL2500E	180	345013.5	5745072	1321.827	13:28	12/9/00	4254.61	0.46
8150N	2525		181	345034.0	5745086	1324.048	13:35	12/9/00	4254.27	0.45
8150N	2550		182	345055.2	5745099	1328.840	13:42	12/9/00	4253.44	0.52
8150N	2575		183	345076.4	5745113	1332.028	13:48	12/9/00	4253.00	0.36
8150N	2600	shaky	184	345097.7	5745126	1336.131	13:55	12/9/00	4252.28	0.36
8150N	2625		185	345118.9	5745139	1340.770	14:02	12/9/00	4251.45	0.44
8150N	2650		186	345140.1	5745152	1342.473	14:08	12/9/00	4251.21	0.46
8150N	2675		187	345161.3	5745166	1345.940	14:14	12/9/00	4250.63	0.37
8150N	2700		188	345182.6	5745179	1348.862	14:20	12/9/00	4250.05	0.39
8150N	2725		189	345203.8	5745192	1353.482	14:28	12/9/00	4249.14	0.45
8150N	2750	R120800	190	345225.0	5745205	1359.870	14:37	12/9/00	4247.86	0.50
8250N	2775		232	345179.2	5745310	1361.390	2:46	12/9/00	4247.45	0.49
8250N	2800		233	345199.6	5745324	1366.844	2:51	12/9/00	4246.33	0.45
8250N	2825	E.O.L.	234	345220.1	5745339	1371.762	2:58	12/9/00	4245.27	0.44
base	base	Base In	000	345221.2	5744890	1348.321	3:24	12/9/00	4249.79	0.35
base	base	Base Out	000	345221.2	5744890	1348.321	10:10	12/10/00	4249.81	0.35
8300N	2850		255	345211.2	5745392	1377.329	10:27	12/10/00	4243.99	0.47
8300N	2825		254	345190.7	5745378	1371.651	10:33	12/10/00	4245.09	0.35
8300N	2800		253	345170.2	5745363	1370.190	10:40	12/10/00	4245.78	0.45
8300N	2775		252	345149.7	5745349	1367.888	10:45	12/10/00	4246.18	0.48
8300N	2750		251	345129.2	5745334	1362.220	10:52	12/10/00	4247.23	0.45
8300N	2725		250	345108.7	5745320	1358.826	10:59	12/10/00	4247.91	0.42
8300N	2700		249	345088.2	5745305	1355.218	11:05	12/10/00	4248.63	0.41
8300N	2675		248	345067.7	5745291	1352.327	11:11	12/10/00	4249.22	0.49
8300N	2650		247	345047.2	5745276	1350.642	11:18	12/10/00	4249.55	0.35
8300N	2625		246	345026.7	5745262	1348.496	11:24	12/10/00	4249.86	0.48
8300N	2600		245	345006.2	5745247	1345.019	11:31	12/10/00	4250.47	0.41
8300N	2575	steep	244	344985.7	5745233	1344.020	11:38	12/10/00	4250.48	0.44
8300N	2550	near creek	243	344965.2	5745218	1334.624	11:51	12/10/00	4252.13	0.50
8300N	2525		242	344944.7	5745204	1339.197	12:11	12/10/00	4251.23	0.41
8300N	2500		241	344924.2	5745189	1339.265	12:17	12/10/00	4251.15	0.44
8300N	2475		240	344903.7	5745175	1334.601	12:22	12/10/00	4251.92	0.47
8300N	2450		239	344883.2	5745160	1329.515	12:28	12/10/00	4252.78	0.45
base	base	Base In	000	345221.2	5744890	1348.321	9:15	12/11/00	4250.08	0.35
base	base	Base Out	000	345221.2	5744890	1348.321	9:15	12/11/00	4250.08	0.35
8300N	2425	redo	238	344862.7	5745146	1325.655	9:33	12/11/00	4253.64	0.48
8300N	2400	redo	237	344842.2	5745131	1320.887	9:38	12/11/00	4254.43	0.51
8300N	2375	redo	236	344821.7	5745117	1316.950	9:43	12/11/00	4255.11	0.50
8300N	2350	redo	235	344801.2	5745102	1312.977	9:47	12/11/00	4255.75	0.49
8250N	2350	redo	215	344831.2	5745063	1307.222	9:53	12/11/00	4257.08	0.50
8250N	2375	redo	216	344851.7	5745078	1309.912	9:58	12/11/00	4256.70	0.51
8250N	2400	redo	217	344872.1	5745092	1316.160	10:03	12/11/00	4255.58	0.46
8250N	2425	back on track	218	344892.6	5745107	1318.930	10:11	12/11/00	4255.11	0.49
8250N	2450		219	344913.1	5745121	1322.849	10:17	12/11/00	4254.46	0.51
8250N	2475		220	344933.5	5745136	1326.480	10:23	12/11/00	4253.92	0.48
8250N	2500	BL2500E	221	344954.0	5745150	1327.597	10:30	12/11/00	4253.78	0.47
8250N	2525	on creek	222	344974.5	5745165	1324.303	10:37	12/11/00	4254.48	0.49
8250N	2550		223	344994.9	5745179	1335.200	10:50	12/11/00	4252.47	0.45
8250N	2575		224	345015.4	5745194	1338.608	10:57	12/11/00	4251.99	0.47
8250N	2600		225	345035.9	5745208	1342.805	11:04	12/11/00	4251.23	0.42
8250N	2625		226	345056.3	5745223	1346.255	11:11	12/11/00	4250.70	0.44
8250N	2650	shaky	227	345076.8	5745237	1346.991	11:18	12/11/00	4250.53	0.48
8250N	2675		228	345097.3	5745252	1348.839	11:24	12/11/00	4250.11	0.45
8250N	2700		229	345117.8	5745266	1349.849	11:30	12/11/00	4249.79	0.47
8250N	2725		230	345138.2	5745281	1351.180	11:37	12/11/00	4249.79	0.49
8250N	2750		231	345158.7	5745295	1356.690	11:47	12/11/00	4248.68	0.46
8250N	2775	R120900	232	345179.2	5745310	1361.390	11:54	12/11/00	4247.78	0.47
8350N	2725		269	345078.6	5745359	1370.843	14:41	12/11/00	4245.88	0.51
8350N	2750		270	345099.1	5745373	1377.836	14:50	12/11/00	4244.43	0.46
8350N	2775		271	345119.6	5745388	1384.660	14:55	12/11/00	4243.08	0.40
8350N	2800		272	345140.0	5745402	1392.479	15:02	12/11/00	4241.49	0.46
8350N	2825		273	345160.5	5745417	1398.903	15:08	12/11/00	4240.22	0.45
8350N	2850	E.O.L.	274	345181.0	5745431	1402.915	15:14	12/11/00	4239.97	0.46
base	base	Base In	000	345221.2	5744890	1348.321	15:27	12/11/00	4250.10	0.36
control	9999	Sand Ctrl. St: 980956.44	999	341732.9	5775310.24	631.350	8:08	12/12/00	4389.23	0.47
base	base	Base Out	000	345221.2	5744890	1348.321	9:36	12/12/00	4250.49	0.36
8400N	2800		289	345110.7	5745441	1402.230	10:22	12/12/00	4240.01	0.45
8400N	2775		288	345090.2	5745427	1395.062	10:27	12/12/00	4241.49	0.49
8400N	2750		287	345069.7	5745412	1388.596	10:32	12/12/00	4242.73	0.46

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8400N	2725		286	345049.2	5745398	1381.954	10:37	12/12/00	4244.09	0.50
8400N	2700		285	345028.7	5745383	1378.887	10:44	12/12/00	4244.72	0.47
8400N	2675		284	345008.2	5745369	1377.314	10:51	12/12/00	4245.04	0.47
8400N	2650		283	344987.7	5745354	1373.616	10:56	12/12/00	4245.58	0.44
8400N	2625		282	344967.2	5745340	1369.790	11:01	12/12/00	4246.18	0.38
8400N	2600		281	344946.7	5745325	1365.993	11:08	12/12/00	4246.72	0.49
8400N	2575	v. steep	280	344926.2	5745311	1371.611	11:17	12/12/00	4245.42	0.42
8400N	2550		279	344905.7	5745296	1371.268	11:25	12/12/00	4245.33	0.49
8400N	2525		278	344885.2	5745282	1366.926	11:31	12/12/00	4246.00	0.43
8400N	2500	BL2500E	277	344864.7	5745267	1361.314	11:39	12/12/00	4246.81	0.42
8400N	2475	v. steep	276	344844.2	5745253	1359.968	11:47	12/12/00	4246.91	0.40
8400N	2450	E.O.L.	275	344823.7	5745238	1361.808	12:00	12/12/00	4246.15	0.36
8350N	2400		256	344812.5	5745170	1332.323	12:24	12/12/00	4252.40	0.46
8350N	2425		257	344833.0	5745185	1338.663	12:44	12/12/00	4251.38	0.41
8350N	2450		258	344853.5	5745199	1340.827	12:51	12/12/00	4251.04	0.40
8350N	2475		259	344873.9	5745214	1343.834	12:56	12/12/00	4250.75	0.42
8350N	2500	BL2500E	260	344894.4	5745228	1347.361	13:01	12/12/00	4250.22	0.52
8350N	2525		261	344914.9	5745243	1350.581	13:07	12/12/00	4249.69	0.48
8350N	2550		262	344935.3	5745257	1353.717	13:12	12/12/00	4249.18	0.38
8350N	2575	near creek	263	344955.8	5745272	1345.621	13:21	12/12/00	4250.71	0.45
8350N	2600	steep	264	344976.3	5745286	1354.279	13:30	12/12/00	4249.22	0.46
8350N	2625	steep	265	344996.8	5745301	1360.519	13:38	12/12/00	4248.03	0.44
8350N	2650	shaky	266	345017.2	5745315	1363.429	13:48	12/12/00	4247.52	0.42
8350N	2675	new battery	267	345037.7	5745330	1367.004	13:58	12/12/00	4246.91	0.45
8350N	2700		268	345058.2	5745344	1368.972	14:03	12/12/00	4246.57	0.48
8350N	2725	R121100	269	345078.6	5745359	1370.843	14:13	12/12/00	4246.24	0.47
8450N	2525		293	344855.4	5745321	1389.761	14:21	12/12/00	4241.58	0.40
8450N	2550		294	344875.8	5745335	1389.973	14:33	12/12/00	4241.73	0.48
8450N	2575		295	344896.3	5745350	1391.427	14:42	12/12/00	4241.64	0.50
8450N	2600		296	344916.8	5745364	1388.286	14:52	12/12/00	4242.38	0.45
8450N	2625		297	344937.3	5745379	1389.356	15:02	12/12/00	4242.19	0.46
8450N	2650		298	344957.7	5745393	1386.475	15:08	12/12/00	4242.95	0.45
base	base	Base In	000	345221.2	5744890	1348.321	15:20	12/12/00	4250.45	0.34
base	base	Base Out	000	345221.2	5744890	1348.321	9:10	12/13/00	4250.66	0.34
8450N	2675	fluctuating	299	344978.2	5745408	1391.595	10:27	12/13/00	4242.18	0.46
8450N	2700		300	344998.7	5745422	1397.519	10:37	12/13/00	4241.08	0.45
8450N	2725		301	345019.1	5745437	1399.442	10:43	12/13/00	4240.74	0.50
8450N	2750	E.O.L.	302	345039.6	5745451	1403.984	10:50	12/13/00	4239.82	0.43
8500N	2700		316	344969.1	5745461	1412.167	11:03	12/13/00	4238.16	0.46
8500N	2675		315	344948.6	5745447	1407.425	11:10	12/13/00	4239.20	0.43
8500N	2650		314	344928.1	5745432	1406.383	11:23	12/13/00	4239.25	0.40
8500N	2625		313	344907.7	5745418	1408.255	11:29	12/13/00	4238.77	0.41
8500N	2600		312	344887.2	5745403	1404.323	11:35	12/13/00	4239.52	0.49
8500N	2575		311	344866.7	5745389	1405.715	11:42	12/13/00	4239.08	0.50
8500N	2550	shaky	310	344846.3	5745374	1405.536	11:50	12/13/00	4239.03	0.49
8500N	2525	fluctuating still	309	344825.8	5745360	1409.557	11:58	12/13/00	4237.95	0.48
8500N	2500	BL2500E	308	344805.3	5745345	1407.620	12:08	12/13/00	4238.21	0.49
8500N	2475		307	344784.8	5745331	1409.223	12:15	12/13/00	4237.59	0.57
8500N	2450		306	344764.4	5745316	1408.630	12:23	12/13/00	4237.47	0.54
8500N	2425		305	344743.9	5745302	1405.322	12:31	12/13/00	4238.03	0.53
8500N	2400		304	344723.4	5745287	1405.549	12:37	12/13/00	4237.63	0.49
8500N	2375		303	344703.0	5745273	1404.425	13:04	12/13/00	4237.38	0.50
8450N	2450		290	344794.0	5745277	1398.723	13:21	12/13/00	4239.13	0.46
8450N	2475		291	344814.4	5745292	1394.704	13:28	12/13/00	4240.27	0.46
8450N	2500	BL2500E	292	344834.9	5745306	1392.050	13:35	12/13/00	4241.13	0.47
8450N	2525	R121200	293	344855.4	5745321	1389.761	13:40	12/13/00	4241.81	0.48
8550N	2350		318	344653.1	5745299	1409.049	13:54	12/13/00	4236.44	0.48
8550N	2375		319	344673.6	5745314	1412.374	14:00	12/13/00	4236.04	0.41
8550N	2400		320	344694.0	5745328	1412.494	14:07	12/13/00	4236.41	0.54
8550N	2425		321	344714.5	5745343	1413.431	14:15	12/13/00	4236.51	0.47
8550N	2450		322	344735.0	5745357	1414.351	14:23	12/13/00	4236.65	0.42
8550N	2475		323	344755.4	5745372	1415.878	14:31	12/13/00	4236.50	0.45
8550N	2500		324	344775.9	5745386	1416.617	14:40	12/13/00	4236.53	0.47
8550N	2525		325	344796.4	5745401	1419.194	14:48	12/13/00	4236.15	0.49
8550N	2550		326	344816.8	5745415	1419.417	14:55	12/13/00	4236.34	0.46
8550N	2575		327	344837.3	5745430	1418.480	15:02	12/13/00	4236.75	0.48
8550N	2600		328	344857.8	5745444	1417.631	15:08	12/13/00	4237.03	0.43
base	base	Base In	000	345221.2	5744890	1348.321	15:31	12/13/00	4250.71	0.34
base	base	Base Out	000	345221.2	5744890	1348.321	9:22	12/14/00	4251.02	0.34
7650N	2800E	lake shore	012	345570.6	5744833	1328.592	10:16	12/14/00	4255.37	0.52
8550N	2625	swamp/shaky	329	344878.3	5745459	1416.368	11:48	12/14/00	4237.86	0.30
8550N	2650		330	344898.7	5745473	1418.118	11:53	12/14/00	4237.49	0.46
8550N	2675		331	344919.2	5745488	1420.369	12:00	12/14/00	4237.06	0.45
8550N	2700	E.O.L.	332	344939.7	5745502	1418.524	12:07	12/14/00	4237.66	0.46

GravMaster Input

8600N	2700		350	344910.3	5745542	1424.444	12:20	12/14/00	4236.45	0.46
8600N	2675		349	344889.8	5745528	1423.519	12:26	12/14/00	4236.56	0.51
8600N	2650		348	344869.3	5745513	1423.370	12:31	12/14/00	4236.47	0.45
8600N	2625		347	344848.8	5745499	1423.251	12:36	12/14/00	4236.44	0.50
8600N	2600		346	344828.4	5745484	1423.865	12:43	12/14/00	4236.26	0.49
8600N	2575		345	344807.9	5745470	1424.995	12:49	12/14/00	4235.90	0.44
8600N	2550		344	344787.4	5745455	1426.151	12:55	12/14/00	4235.41	0.48
8600N	2525		343	344767.0	5745441	1425.085	13:01	12/14/00	4235.42	0.50
8600N	2500		342	344746.5	5745426	1420.655	13:08	12/14/00	4236.23	0.46
8600N	2475		341	344726.0	5745412	1420.052	13:32	12/14/00	4236.17	0.48
8600N	2450		340	344705.6	5745397	1420.233	13:37	12/14/00	4235.91	0.39
8600N	2425		339	344685.1	5745383	1423.531	13:44	12/14/00	4234.80	0.42
8600N	2400		338	344664.6	5745368	1424.894	13:50	12/14/00	4234.17	0.54
8600N	2375		337	344644.2	5745354	1427.040	13:56	12/14/00	4233.23	0.45
8600N	2350		336	344623.7	5745339	1417.589	14:07	12/14/00	4235.09	0.51
8600N	2325		335	344603.2	5745325	1411.116	14:13	12/14/00	4236.16	0.56
8600N	2300		334	344582.8	5745310	1405.993	14:20	12/14/00	4236.97	0.49
8600N	2275	E.O.L.	333	344562.3	5745296	1401.632	14:27	12/14/00	4237.45	0.40
8550N	2325		317	344632.6	5745285	1406.421	14:41	12/14/00	4236.66	0.48
8550N	2350	R121300	318	344653.1	5745299	1409.049	14:51	12/14/00	4236.74	0.47
base	base	Base In	000	345221.2	5744890	1348.321	15:05	12/14/00	4250.92	0.35

GravMaster Output

ID	X	Y	Line	Station	Elev (m)	Boug2.5	Boug2.6	Boug2.7	Boug2.8
0	345221.2	5744890	7900N	2550	1348.231	-145.58	-151.23	-156.89	-162.54
1	345371.7	5744892	7650N	2557	1339.701	-145.95	-151.57	-157.19	-162.81
2	345386.4	5744703	7650N	2575	1345.297	-145.54	-151.18	-156.82	-162.46
3	345406.9	5744717	7650N	2600	1348.438	-145.16	-150.81	-156.47	-162.12
4	345427.3	5744732	7650N	2625	1348.246	-144.93	-150.58	-156.24	-161.89
5	345447.8	5744746	7650N	2650	1345.378	-144.72	-150.36	-156.00	-161.64
6	345468.3	5744761	7650N	2675	1344.861	-144.83	-150.47	-156.11	-161.75
7	345488.8	5744775	7650N	2700	1344.002	-144.82	-150.45	-156.09	-161.72
8	345509.2	5744790	7650N	2725	1341.828	-144.83	-150.46	-156.09	-161.71
9	345529.7	5744804	7650N	2750	1340.718	-145.02	-150.64	-156.26	-161.89
10	345550.2	5744819	7650N	2775	1334.530	-145.06	-150.65	-156.25	-161.84
11	345566.5	5744830	7650N	2795	1328.592	-145.37	-150.94	-156.51	-162.08
12	345570.6	5744833	7650N	2800	1328.592	-145.07	-150.64	-156.21	-161.78
13	345337.4	5744729	7700N	2550	1340.382	-146.00	-151.62	-157.24	-162.86
14	345357.9	5744744	7700N	2575	1343.938	-145.50	-151.13	-156.77	-162.40
15	345378.4	5744758	7700N	2600	1345.735	-145.11	-150.75	-156.40	-162.04
16	345398.8	5744773	7700N	2625	1347.766	-144.93	-150.59	-156.24	-161.89
17	345419.3	5744787	7700N	2650	1348.192	-144.84	-150.49	-156.14	-161.80
18	345439.8	5744802	7700N	2675	1349.517	-144.80	-150.46	-156.12	-161.78
19	345460.3	5744816	7700N	2700	1349.335	-144.80	-150.46	-156.11	-161.77
20	345480.7	5744831	7700N	2725	1346.373	-144.83	-150.47	-156.12	-161.76
21	345501.2	5744845	7700N	2750	1345.048	-144.94	-150.58	-156.22	-161.86
22	345521.7	5744860	7700N	2775	1338.393	-145.06	-150.67	-156.28	-161.90
23	345542.1	5744874	7700N	2800	1334.571	-145.17	-150.76	-156.36	-161.96
24	345562.6	5744889	7700N	2825	1332.305	-145.35	-150.93	-156.52	-162.10
25	345583.1	5744903	7700N	2850	1329.745	-145.50	-151.07	-156.65	-162.22
26	345603.5	5744918	7700N	2875	1333.981	-145.62	-151.21	-156.81	-162.40
27	345624.0	5744932	7700N	2900	1339.801	-145.55	-151.17	-156.79	-162.41
28	345644.5	5744947	7700N	2925	1347.368	-145.47	-151.12	-156.77	-162.42
29	345268.0	5744740	7750N	2500	1325.169	-146.68	-152.24	-157.79	-163.35
30	345288.5	5744755	7750N	2525	1334.928	-146.46	-152.06	-157.66	-163.25
31	345308.9	5744769	7750N	2550	1345.265	-146.11	-151.75	-157.39	-163.03
32	345329.4	5744784	7750N	2575	1346.004	-145.47	-151.11	-156.76	-162.40
33	345349.9	5744798	7750N	2600	1351.395	-145.32	-150.98	-156.65	-162.32
34	345370.3	5744813	7750N	2625	1354.783	-145.11	-150.79	-156.47	-162.15
35	345390.8	5744827	7750N	2650	1356.478	-144.96	-150.65	-156.34	-162.03
36	345411.3	5744842	7750N	2675	1354.277	-144.81	-150.48	-156.16	-161.84
37	345431.8	5744856	7750N	2700	1354.381	-144.87	-150.55	-156.23	-161.91
38	345452.2	5744871	7750N	2725	1353.225	-144.82	-150.50	-156.17	-161.85
39	345472.7	5744885	7750N	2750	1350.416	-144.88	-150.55	-156.21	-161.87
40	345493.2	5744900	7750N	2775	1345.600	-144.99	-150.63	-156.27	-161.91
41	345513.6	5744914	7750N	2800	1343.213	-145.07	-150.71	-156.34	-161.97
42	345534.1	5744929	7750N	2825	1343.369	-145.21	-150.84	-156.47	-162.11
43	345554.6	5744943	7750N	2850	1343.581	-145.33	-150.96	-156.60	-162.23
44	345575.0	5744958	7750N	2875	1347.058	-145.44	-151.09	-156.73	-162.38
45	345595.5	5744972	7750N	2900	1352.973	-145.43	-151.10	-156.78	-162.45
46	345616.0	5744987	7750N	2925	1363.193	-145.38	-151.10	-156.81	-162.53
47	345239.5	5744781	7800N	2500	1332.761	-146.61	-152.20	-157.79	-163.38
48	345260.0	5744796	7800N	2525	1340.142	-146.38	-152.00	-157.62	-163.24
49	345280.4	5744810	7800N	2550	1345.717	-145.86	-151.50	-157.14	-162.79
50	345300.9	5744825	7800N	2575	1348.443	-145.45	-151.11	-156.76	-162.42
51	345321.4	5744839	7800N	2600	1353.520	-145.27	-150.95	-156.62	-162.30
52	345341.8	5744854	7800N	2625	1355.212	-145.03	-150.71	-156.39	-162.08
53	345362.3	5744868	7800N	2650	1356.533	-144.94	-150.63	-156.32	-162.01
54	345382.8	5744883	7800N	2675	1356.165	-144.80	-150.49	-156.17	-161.86
55	345403.3	5744897	7800N	2700	1352.615	-144.73	-150.40	-156.07	-161.75
56	345423.7	5744912	7800N	2725	1351.722	-144.73	-150.40	-156.07	-161.74
57	345444.2	5744926	7800N	2750	1352.666	-144.82	-150.49	-156.16	-161.84
58	345464.7	5744941	7800N	2775	1351.694	-144.90	-150.57	-156.23	-161.90
59	345485.1	5744955	7800N	2800	1350.765	-144.99	-150.66	-156.32	-161.98
60	345505.6	5744970	7800N	2825	1349.716	-145.17	-150.83	-156.49	-162.15
61	345526.1	5744984	7800N	2850	1355.246	-145.23	-150.92	-156.60	-162.28
62	345546.5	5744999	7800N	2875	1360.529	-145.26	-150.97	-156.67	-162.38
63	345567.0	5745013	7800N	2900	1369.110	-145.26	-151.00	-156.74	-162.48
64	345211.0	5744821	7850N	2500	1335.642	-146.40	-152.00	-157.60	-163.20
65	345231.5	5744836	7850N	2525	1345.791	-145.99	-151.63	-157.27	-162.92
66	345251.9	5744850	7850N	2550	1348.895	-145.67	-151.32	-156.98	-162.63
67	345272.4	5744865	7850N	2575	1350.576	-145.35	-151.02	-156.68	-162.34
68	345292.9	5744879	7850N	2600	1352.204	-145.13	-150.80	-156.47	-162.14
69	345313.3	5744894	7850N	2625	1352.218	-144.90	-150.57	-156.24	-161.91
70	345333.8	5744908	7850N	2650	1352.517	-144.90	-150.57	-156.24	-161.91
71	345354.3	5744923	7850N	2675	1351.036	-144.84	-150.50	-156.17	-161.83
72	345374.8	5744937	7850N	2700	1350.386	-144.82	-150.48	-156.15	-161.81

GravMaster Output

73	345395.2	5744952	7850N	2725	1349.968	-144.88	-150.54	-156.20	-161.86
74	345415.7	5744966	7850N	2750	1349.838	-144.90	-150.56	-156.22	-161.88
75	345436.2	5744981	7850N	2775	1351.311	-144.93	-150.60	-156.26	-161.93
76	345456.6	5744995	7850N	2800	1354.378	-145.00	-150.68	-156.36	-162.04
77	345477.1	5745010	7850N	2825	1359.724	-145.04	-150.74	-156.44	-162.14
78	345497.6	5745024	7850N	2850	1367.205	-145.01	-150.75	-156.48	-162.21
79	345518.0	5745039	7850N	2875	1375.397	-145.09	-150.86	-156.63	-162.40
80	345538.5	5745053	7850N	2900	1383.906	-145.12	-150.92	-156.73	-162.53
81	345182.5	5744862	7900N	2500	1343.325	-146.37	-152.00	-157.64	-163.27
82	345203.0	5744876	7900N	2525	1348.015	-145.96	-151.62	-157.27	-162.92
83	345221.2	5744890	7900N	2550	1348.231	-145.58	-151.23	-156.89	-162.54
84	345239.4	5744904	7900N	2575	1348.826	-145.37	-151.02	-156.68	-162.33
85	345257.6	5744919	7900N	2600	1349.579	-145.17	-150.83	-156.48	-162.14
86	345275.8	5744933	7900N	2625	1349.892	-145.06	-150.72	-156.38	-162.04
87	345294.0	5744947	7900N	2650	1349.434	-144.99	-150.64	-156.30	-161.96
88	345312.2	5744961	7900N	2675	1347.779	-144.93	-150.59	-156.24	-161.89
89	345330.4	5744975	7900N	2700	1346.201	-144.94	-150.59	-156.23	-161.88
90	345348.6	5744989	7900N	2725	1346.976	-145.05	-150.70	-156.35	-162.00
91	345366.8	5745003	7900N	2750	1349.447	-145.02	-150.68	-156.34	-162.00
92	345385.0	5745017	7900N	2775	1353.579	-145.12	-150.80	-156.47	-162.15
93	345403.2	5745031	7900N	2800	1356.559	-145.14	-150.83	-156.52	-162.21
94	345421.4	5745045	7900N	2825	1360.866	-145.20	-150.90	-156.61	-162.31
95	345439.6	5745060	7900N	2850	1367.763	-145.15	-150.88	-156.62	-162.35
96	345457.8	5745074	7900N	2875	1375.219	-145.11	-150.87	-156.64	-162.41
97	345476.0	5745088	7900N	2900	1382.509	-145.12	-150.92	-156.72	-162.51
98	345107.7	5744875	7950N	2450	1339.251	-147.03	-152.64	-158.26	-163.87
99	345128.2	5744890	7950N	2475	1345.673	-146.57	-152.22	-157.86	-163.50
100	345148.7	5744904	7950N	2500	1345.805	-146.18	-151.82	-157.46	-163.11
101	345169.2	5744919	7950N	2525	1344.948	-145.83	-151.47	-157.11	-162.75
102	345189.7	5744933	7950N	2550	1344.351	-145.56	-151.20	-156.83	-162.47
103	345210.2	5744948	7950N	2575	1343.943	-145.38	-151.01	-156.65	-162.28
104	345230.7	5744962	7950N	2600	1343.302	-145.32	-150.96	-156.59	-162.22
105	345251.2	5744977	7950N	2625	1342.322	-145.20	-150.83	-156.46	-162.09
106	345271.7	5744991	7950N	2650	1342.637	-145.13	-150.76	-156.39	-162.02
107	345292.2	5745006	7950N	2675	1342.666	-145.10	-150.73	-156.36	-161.99
108	345312.7	5745020	7950N	2700	1342.853	-145.13	-150.76	-156.39	-162.02
109	345353.7	5745049	7950N	2750	1346.504	-145.19	-150.83	-156.48	-162.12
110	345374.2	5745064	7950N	2775	1354.710	-145.14	-150.82	-156.50	-162.18
111	345394.7	5745078	7950N	2800	1359.896	-145.25	-150.96	-156.66	-162.36
112	345415.2	5745093	7950N	2825	1365.322	-145.19	-150.91	-156.64	-162.36
113	345435.7	5745107	7950N	2850	1371.657	-145.14	-150.89	-156.64	-162.40
114	345456.2	5745122	7950N	2875	1377.090	-145.16	-150.94	-156.71	-162.48
115	345476.7	5745136	7950N	2900	1386.608	-145.22	-151.03	-156.85	-162.66
116	345033.0	5744888	8000N	2400	1316.212	-147.19	-152.70	-158.22	-163.74
117	345053.5	5744903	8000N	2425	1323.950	-146.85	-152.41	-157.96	-163.51
118	345074.0	5744917	8000N	2450	1331.366	-146.52	-152.10	-157.68	-163.27
119	345094.4	5744932	8000N	2475	1335.623	-146.21	-151.81	-157.41	-163.01
120	345114.9	5744946	8000N	2500	1336.092	-145.99	-151.60	-157.20	-162.80
121	345135.4	5744961	8000N	2525	1335.427	-145.72	-151.32	-156.92	-162.52
122	345155.8	5744975	8000N	2550	1335.693	-145.59	-151.20	-156.80	-162.40
123	345176.3	5744990	8000N	2575	1335.624	-145.44	-151.05	-156.65	-162.25
124	345196.8	5745004	8000N	2600	1335.956	-145.37	-150.97	-156.57	-162.18
125	345217.3	5745019	8000N	2625	1337.925	-145.28	-150.89	-156.50	-162.11
126	345237.7	5745033	8000N	2650	1344.116	-145.25	-150.89	-156.52	-162.16
127	345258.2	5745048	8000N	2675	1346.695	-145.15	-150.80	-156.45	-162.09
128	345278.7	5745062	8000N	2700	1346.829	-145.10	-150.75	-156.40	-162.05
129	345299.1	5745077	8000N	2725	1347.242	-145.12	-150.77	-156.41	-162.06
130	345319.6	5745091	8000N	2750	1355.145	-145.11	-150.79	-156.47	-162.15
131	345340.1	5745106	8000N	2775	1360.003	-145.13	-150.84	-156.54	-162.24
132	345360.5	5745120	8000N	2800	1364.852	-145.16	-150.89	-156.61	-162.33
133	345381.0	5745135	8000N	2825	1370.132	-145.09	-150.84	-156.58	-162.33
134	345401.5	5745149	8000N	2850	1376.770	-145.12	-150.89	-156.67	-162.44
135	345421.9	5745164	8000N	2875	1382.001	-145.19	-150.99	-156.78	-162.58
136	345442.4	5745178	8000N	2900	1387.460	-145.26	-151.08	-156.89	-162.71
137	344999.1	5744930	8050N	2400	1309.445	-146.87	-152.36	-157.85	-163.34
138	345019.6	5744945	8050N	2425	1317.872	-146.55	-152.08	-157.60	-163.13
139	345040.1	5744959	8050N	2450	1321.901	-146.26	-151.81	-157.35	-162.89
140	345060.6	5744974	8050N	2475	1323.806	-146.09	-151.64	-157.19	-162.74
141	345081.1	5744988	8050N	2500	1324.535	-145.83	-151.38	-156.93	-162.49
142	345101.6	5745003	8050N	2525	1326.655	-145.68	-151.24	-156.80	-162.37
143	345122.1	5745017	8050N	2550	1330.980	-145.64	-151.22	-156.81	-162.39
144	345142.6	5745032	8050N	2575	1334.606	-145.52	-151.11	-156.71	-162.30
145	345163.1	5745046	8050N	2600	1340.707	-145.46	-151.08	-156.70	-162.33
146	345183.6	5745061	8050N	2625	1343.255	-145.29	-150.92	-156.55	-162.18

GravMaster Output

147	345204.1	5745075	8050N	2650	1349.356	-145.20	-150.86	-156.51	-162.17
148	345224.6	5745090	8050N	2675	1348.102	-145.14	-150.79	-156.45	-162.10
149	345245.1	5745104	8050N	2700	1347.682	-145.34	-150.99	-156.64	-162.29
150	345265.6	5745119	8050N	2725	1349.163	-145.20	-150.86	-156.52	-162.17
151	345286.1	5745133	8050N	2750	1355.178	-145.18	-150.86	-156.54	-162.22
152	345306.6	5745148	8050N	2775	1362.477	-145.18	-150.89	-156.61	-162.32
153	345327.1	5745162	8050N	2800	1366.702	-145.11	-150.84	-156.57	-162.30
154	345347.6	5745177	8050N	2825	1371.431	-145.14	-150.90	-156.65	-162.40
155	345368.1	5745191	8050N	2850	1376.627	-145.16	-150.93	-156.70	-162.47
156	345388.6	5745206	8050N	2875	1381.747	-145.10	-150.89	-156.69	-162.48
157	345409.1	5745220	8050N	2900	1386.153	-145.09	-150.90	-156.72	-162.53
158	344985.9	5744987	8100N	2425	1311.776	-146.48	-151.98	-157.48	-162.98
159	345006.4	5745001	8100N	2450	1321.976	-146.34	-151.89	-157.43	-162.97
160	345026.8	5745016	8100N	2475	1324.449	-146.04	-151.60	-157.15	-162.70
161	345047.3	5745030	8100N	2500	1327.042	-145.90	-151.47	-157.03	-162.59
162	345067.8	5745045	8100N	2525	1330.801	-145.78	-151.36	-156.94	-162.52
163	345088.3	5745059	8100N	2550	1334.218	-145.71	-151.30	-156.90	-162.49
164	345108.7	5745074	8100N	2575	1334.707	-145.56	-151.16	-156.76	-162.35
165	345149.7	5745103	8100N	2625	1340.882	-145.35	-150.97	-156.60	-162.22
166	345170.1	5745117	8100N	2650	1342.883	-145.29	-150.93	-156.56	-162.19
167	345190.6	5745132	8100N	2675	1345.151	-145.26	-150.90	-156.54	-162.18
168	345211.1	5745146	8100N	2700	1346.799	-145.24	-150.89	-156.54	-162.19
169	345231.5	5745161	8100N	2725	1349.029	-145.28	-150.94	-156.59	-162.25
170	345252.0	5745175	8100N	2750	1356.364	-145.24	-150.93	-156.62	-162.31
171	345272.5	5745190	8100N	2775	1361.266	-145.29	-150.99	-156.70	-162.41
172	345292.9	5745204	8100N	2800	1366.827	-145.32	-151.05	-156.78	-162.51
173	345313.4	5745219	8100N	2825	1372.402	-145.40	-151.16	-156.91	-162.66
174	345333.9	5745233	8100N	2850	1377.235	-145.35	-151.13	-156.90	-162.68
175	345354.3	5745248	8100N	2875	1383.098	-145.38	-151.18	-156.98	-162.78
176	345374.8	5745262	8100N	2900	1388.003	-145.47	-151.29	-157.11	-162.93
177	344952.0	5745030	8150N	2425	1309.046	-146.63	-152.11	-157.60	-163.09
178	344972.5	5745044	8150N	2450	1314.548	-146.43	-151.94	-157.46	-162.97
179	344993.0	5745058	8150N	2475	1319.124	-146.32	-151.85	-157.38	-162.91
180	345013.5	5745072	8150N	2500	1321.827	-146.21	-151.75	-157.30	-162.84
181	345034.0	5745086	8150N	2525	1324.048	-146.12	-151.67	-157.22	-162.77
182	345055.2	5745099	8150N	2550	1328.840	-145.98	-151.55	-157.12	-162.69
183	345076.4	5745113	8150N	2575	1332.028	-145.84	-151.42	-157.01	-162.59
184	345097.7	5745126	8150N	2600	1336.131	-145.74	-151.34	-156.94	-162.54
185	345118.9	5745139	8150N	2625	1340.770	-145.63	-151.25	-156.87	-162.49
186	345140.1	5745152	8150N	2650	1342.473	-145.53	-151.16	-156.79	-162.42
187	345161.3	5745166	8150N	2675	1345.940	-145.45	-151.10	-156.74	-162.38
188	345182.6	5745179	8150N	2700	1348.862	-145.45	-151.11	-156.76	-162.42
189	345203.8	5745192	8150N	2725	1353.482	-145.43	-151.10	-156.78	-162.45
190	345225.0	5745205	8150N	2750	1359.870	-145.37	-151.07	-156.77	-162.48
191	345246.2	5745218	8150N	2775	1364.846	-145.35	-151.08	-156.80	-162.52
192	345267.4	5745232	8150N	2800	1367.266	-145.24	-150.97	-156.71	-162.44
193	345288.7	5745245	8150N	2825	1373.065	-145.39	-151.15	-156.90	-162.66
194	345309.9	5745258	8150N	2850	1374.012	-145.39	-151.15	-156.91	-162.67
195	345331.1	5745271	8150N	2875	1376.470	-145.49	-151.26	-157.03	-162.80
196	345352.3	5745285	8150N	2900	1381.324	-145.64	-151.43	-157.23	-163.02
197	344943.1	5745082	8200N	2450	1306.956	-146.67	-152.15	-157.63	-163.11
198	344963.5	5745097	8200N	2475	1311.578	-146.50	-152.00	-157.50	-163.00
199	344984.0	5745111	8200N	2500	1314.696	-146.46	-151.97	-157.48	-163.00
200	345004.5	5745126	8200N	2525	1318.918	-146.34	-151.87	-157.40	-162.93
201	345016.8	5745134	8200N	2540	1321.351	-146.16	-151.70	-157.24	-162.78
202	345045.4	5745155	8200N	2575	1327.530	-146.08	-151.65	-157.22	-162.78
203	345065.9	5745169	8200N	2600	1330.650	-145.96	-151.54	-157.12	-162.70
204	345086.3	5745184	8200N	2625	1334.731	-145.84	-151.44	-157.03	-162.63
205	345106.8	5745198	8200N	2650	1340.741	-145.74	-151.36	-156.98	-162.60
206	345127.3	5745213	8200N	2675	1346.062	-145.51	-151.15	-156.79	-162.44
207	345147.8	5745227	8200N	2700	1348.758	-145.53	-151.18	-156.84	-162.49
208	345168.2	5745242	8200N	2725	1353.237	-145.51	-151.18	-156.86	-162.53
209	345188.7	5745256	8200N	2750	1360.931	-145.53	-151.24	-156.95	-162.65
210	345209.2	5745271	8200N	2775	1364.551	-145.49	-151.21	-156.93	-162.66
211	345229.6	5745285	8200N	2800	1365.204	-145.50	-151.22	-156.95	-162.67
212	345250.1	5745300	8200N	2825	1367.532	-145.58	-151.32	-157.05	-162.78
213	345270.6	5745314	8200N	2850	1372.395	-145.72	-151.47	-157.23	-162.98
214	345291.0	5745329	8200N	2875	1378.478	-145.74	-151.52	-157.30	-163.08
215	344831.2	5745063	8250N	2350	1307.222	-146.91	-152.39	-157.87	-163.35
216	344851.7	5745078	8250N	2375	1309.912	-146.75	-152.25	-157.74	-163.23
217	344872.1	5745092	8250N	2400	1316.160	-146.64	-152.16	-157.68	-163.20
218	344892.6	5745107	8250N	2425	1318.930	-146.56	-152.09	-157.62	-163.15
219	344913.1	5745121	8250N	2450	1322.849	-146.42	-151.97	-157.52	-163.06
220	344933.5	5745136	8250N	2475	1326.480	-146.25	-151.82	-157.38	-162.94

GravMaster Output

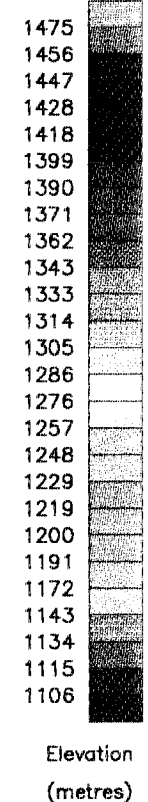
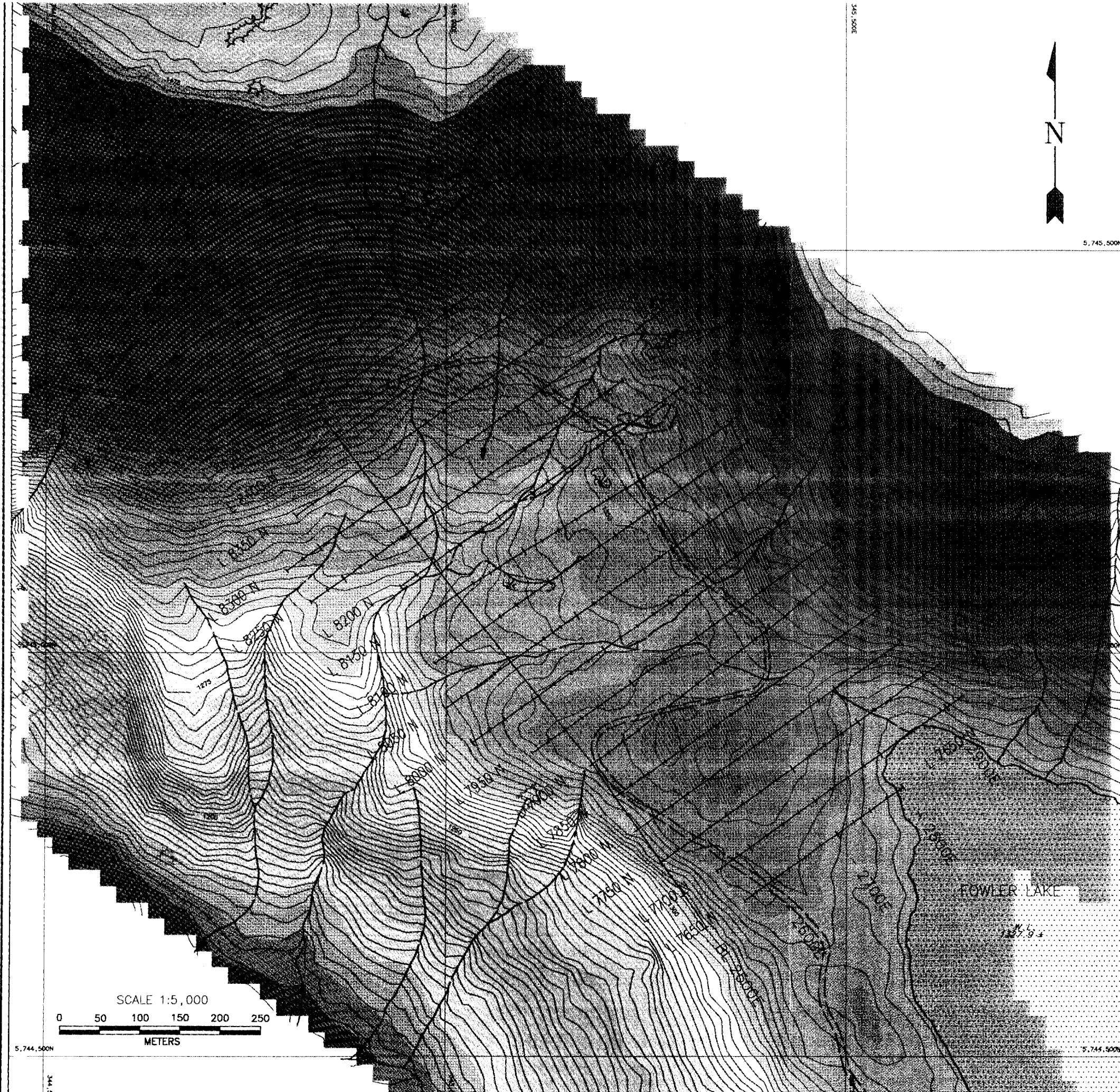
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223	344994.9	5745179	8250N	2550	1335.200	-145.99	-151.59	-157.19	-162.79
224	345015.4	5745194	8250N	2575	1338.608	-145.79	-151.40	-157.02	-162.63
225	345035.9	5745208	8250N	2600	1342.805	-145.73	-151.36	-156.99	-162.62
226	345056.3	5745223	8250N	2625	1346.255	-145.57	-151.22	-156.86	-162.51
227	345076.8	5745237	8250N	2650	1346.991	-145.60	-151.24	-156.89	-162.54
228	345097.3	5745252	8250N	2675	1348.839	-145.67	-151.32	-156.98	-162.63
229	345117.8	5745266	8250N	2700	1349.849	-145.79	-151.45	-157.11	-162.77
230	345138.2	5745281	8250N	2725	1351.180	-145.53	-151.19	-156.86	-162.52
231	345158.7	5745295	8250N	2750	1356.690	-145.55	-151.24	-156.93	-162.62
232	345179.2	5745310	8250N	2775	1361.390	-145.53	-151.24	-156.95	-162.66
233	345199.6	5745324	8250N	2800	1366.844	-145.60	-151.33	-157.07	-162.80
234	345220.1	5745339	8250N	2825	1371.762	-145.70	-151.45	-157.20	-162.95
235	344801.2	5745102	8300N	2350	1312.977	-147.12	-152.62	-158.13	-163.63
236	344821.7	5745117	8300N	2375	1316.950	-146.97	-152.49	-158.01	-163.53
237	344842.2	5745131	8300N	2400	1320.887	-146.87	-152.40	-157.94	-163.48
238	344862.7	5745146	8300N	2425	1325.655	-146.72	-152.28	-157.83	-163.39
239	344883.2	5745160	8300N	2450	1329.515	-146.58	-152.15	-157.73	-163.30
240	344903.7	5745175	8300N	2475	1334.601	-146.42	-152.01	-157.61	-163.21
241	344924.2	5745189	8300N	2500	1339.265	-146.27	-151.88	-157.50	-163.12
242	344944.7	5745204	8300N	2525	1339.197	-146.22	-151.84	-157.45	-163.07
243	344965.2	5745218	8300N	2550	1334.624	-146.22	-151.81	-157.41	-163.01
244	344985.7	5745233	8300N	2575	1344.020	-146.01	-151.64	-157.28	-162.91
245	345006.2	5745247	8300N	2600	1345.019	-145.83	-151.47	-157.11	-162.75
246	345026.7	5745262	8300N	2625	1348.496	-145.73	-151.39	-157.04	-162.70
247	345047.2	5745276	8300N	2650	1350.642	-145.66	-151.32	-156.99	-162.65
248	345067.7	5745291	8300N	2675	1352.327	-145.62	-151.29	-156.96	-162.63
249	345088.2	5745305	8300N	2700	1355.218	-145.67	-151.35	-157.03	-162.71
250	345108.7	5745320	8300N	2725	1358.826	-145.67	-151.37	-157.06	-162.76
251	345129.2	5745334	8300N	2750	1362.220	-145.67	-151.38	-157.09	-162.80
252	345149.7	5745349	8300N	2775	1367.888	-145.58	-151.32	-157.05	-162.79
253	345170.2	5745363	8300N	2800	1370.190	-145.54	-151.29	-157.03	-162.78
254	345190.7	5745378	8300N	2825	1371.651	-145.99	-151.74	-157.49	-163.24
255	345211.2	5745392	8300N	2850	1377.329	-145.92	-151.69	-157.47	-163.24
256	344812.5	5745170	8350N	2400	1332.323	-147.02	-152.61	-158.20	-163.78
257	344833.0	5745185	8350N	2425	1338.663	-146.79	-152.41	-158.02	-163.63
258	344853.5	5745199	8350N	2450	1340.827	-146.71	-152.33	-157.95	-163.58
259	344873.9	5745214	8350N	2475	1343.834	-146.40	-152.03	-157.67	-163.30
260	344894.4	5745228	8350N	2500	1347.361	-146.20	-151.85	-157.50	-163.15
261	344914.9	5745243	8350N	2525	1350.581	-146.10	-151.77	-157.43	-163.09
262	344935.3	5745257	8350N	2550	1353.717	-146.02	-151.70	-157.38	-163.05
263	344955.8	5745272	8350N	2575	1345.621	-146.11	-151.75	-157.40	-163.04
264	344976.3	5745286	8350N	2600	1354.279	-145.87	-151.55	-157.22	-162.90
265	344996.8	5745301	8350N	2625	1360.519	-145.82	-151.53	-157.23	-162.94
266	345017.2	5745315	8350N	2650	1363.429	-145.76	-151.48	-157.20	-162.91
267	345037.7	5745330	8350N	2675	1367.004	-145.66	-151.39	-157.12	-162.85
268	345058.2	5745344	8350N	2700	1368.972	-145.60	-151.34	-157.08	-162.82
269	345078.6	5745359	8350N	2725	1370.843	-145.57	-151.32	-157.07	-162.81
270	345099.1	5745373	8350N	2750	1377.836	-145.64	-151.42	-157.20	-162.98
271	345119.6	5745388	8350N	2775	1384.660	-145.66	-151.46	-157.27	-163.07
272	345140.0	5745402	8350N	2800	1392.479	-145.67	-151.51	-157.35	-163.19
273	345160.5	5745417	8350N	2825	1398.903	-145.67	-151.53	-157.40	-163.26
274	345181.0	5745431	8350N	2850	1402.915	-145.11	-151.00	-156.88	-162.76
275	344823.7	5745238	8400N	2450	1361.808	-147.45	-153.16	-158.87	-164.58
276	344844.2	5745253	8400N	2475	1359.968	-147.06	-152.76	-158.46	-164.16
277	344864.7	5745267	8400N	2500	1361.314	-146.89	-152.60	-158.31	-164.01
278	344885.2	5745282	8400N	2525	1366.926	-146.58	-152.31	-158.04	-163.77
279	344905.7	5745296	8400N	2550	1371.268	-146.37	-152.12	-157.87	-163.62
280	344926.2	5745311	8400N	2575	1371.611	-146.25	-152.00	-157.75	-163.50
281	344946.7	5745325	8400N	2600	1365.993	-146.06	-151.79	-157.52	-163.25
282	344967.2	5745340	8400N	2625	1369.790	-145.88	-151.63	-157.37	-163.12
283	344987.7	5745354	8400N	2650	1373.616	-145.71	-151.47	-157.23	-162.99
284	345008.2	5745369	8400N	2675	1377.314	-145.51	-151.28	-157.06	-162.83
285	345028.7	5745383	8400N	2700	1378.887	-145.53	-151.31	-157.09	-162.87
286	345049.2	5745398	8400N	2725	1381.954	-145.54	-151.34	-157.13	-162.93
287	345069.7	5745412	8400N	2750	1388.596	-145.60	-151.42	-157.24	-163.06
288	345090.2	5745427	8400N	2775	1395.062	-145.54	-151.39	-157.24	-163.09
289	345110.7	5745441	8400N	2800	1402.230	-145.61	-151.49	-157.37	-163.25
290	344794.0	5745277	8450N	2450	1398.723	-147.28	-153.14	-159.01	-164.87
291	344814.4	5745292	8450N	2475	1394.704	-146.95	-152.80	-158.65	-164.50
292	344834.9	5745306	8450N	2500	1392.050	-146.63	-152.47	-158.30	-164.14
293	344855.4	5745321	8450N	2525	1389.761	-146.43	-152.25	-158.08	-163.91
294	344875.8	5745335	8450N	2550	1389.973	-146.23	-152.05	-157.88	-163.71

GravMaster Output

295	344896.3	5745350	8450N	2575	1391.427	-146.03	-151.86	-157.70	-163.53
296	344916.8	5745364	8450N	2600	1388.286	-145.94	-151.76	-157.58	-163.41
297	344937.3	5745379	8450N	2625	1389.356	-145.93	-151.75	-157.58	-163.40
298	344957.7	5745393	8450N	2650	1386.475	-145.76	-151.57	-157.38	-163.20
299	344978.2	5745408	8450N	2675	1391.595	-145.73	-151.57	-157.40	-163.24
300	344998.7	5745422	8450N	2700	1397.519	-145.66	-151.52	-157.38	-163.24
301	345019.1	5745437	8450N	2725	1399.442	-145.61	-151.48	-157.34	-163.21
302	345039.6	5745451	8450N	2750	1403.984	-145.65	-151.54	-157.42	-163.31
303	344703.0	5745273	8500N	2375	1404.425	-147.87	-153.76	-159.65	-165.54
304	344723.4	5745287	8500N	2400	1405.549	-147.40	-153.30	-159.19	-165.08
305	344743.9	5745302	8500N	2425	1405.322	-147.04	-152.94	-158.83	-164.72
306	344764.4	5745316	8500N	2450	1408.630	-146.95	-152.85	-158.76	-164.66
307	344784.8	5745331	8500N	2475	1409.223	-146.71	-152.61	-158.52	-164.43
308	344805.3	5745345	8500N	2500	1407.620	-146.44	-152.34	-158.24	-164.15
309	344825.8	5745360	8500N	2525	1409.557	-146.32	-152.23	-158.14	-164.05
310	344846.3	5745374	8500N	2550	1405.538	-146.05	-151.95	-157.84	-163.73
311	344866.7	5745389	8500N	2575	1405.715	-145.98	-151.87	-157.76	-163.66
312	344887.2	5745403	8500N	2600	1404.323	-145.83	-151.72	-157.60	-163.49
313	344907.7	5745418	8500N	2625	1408.255	-145.82	-151.73	-157.63	-163.54
314	344928.1	5745432	8500N	2650	1406.383	-145.73	-151.63	-157.53	-163.42
315	344948.6	5745447	8500N	2675	1407.425	-145.57	-151.48	-157.38	-163.28
316	344969.1	5745461	8500N	2700	1412.167	-145.67	-151.59	-157.51	-163.43
317	344632.6	5745285	8550N	2325	1406.421	-148.46	-154.36	-160.26	-166.15
318	344653.1	5745299	8550N	2350	1409.049	-147.89	-153.79	-159.70	-165.61
319	344673.6	5745314	8550N	2375	1412.374	-147.68	-153.60	-159.52	-165.45
320	344694.0	5745328	8550N	2400	1412.494	-147.25	-153.18	-159.10	-165.02
321	344714.5	5745343	8550N	2425	1413.431	-147.00	-152.92	-158.85	-164.78
322	344735.0	5745357	8550N	2450	1414.351	-146.70	-152.63	-158.56	-164.49
323	344755.4	5745372	8550N	2475	1415.878	-146.54	-152.48	-158.42	-164.35
324	344775.9	5745386	8550N	2500	1416.617	-146.37	-152.31	-158.25	-164.19
325	344796.4	5745401	8550N	2525	1419.194	-146.24	-152.19	-158.14	-164.09
326	344816.8	5745415	8550N	2550	1419.417	-146.02	-151.97	-157.92	-163.88
327	344837.3	5745430	8550N	2575	1418.480	-145.80	-151.75	-157.70	-163.65
328	344857.8	5745444	8550N	2600	1417.631	-145.72	-151.66	-157.61	-163.55
329	344878.3	5745459	8550N	2625	1416.368	-145.48	-151.42	-157.35	-163.29
330	344898.7	5745473	8550N	2650	1418.118	-145.46	-151.40	-157.35	-163.29
331	344919.2	5745488	8550N	2675	1420.369	-145.45	-151.40	-157.36	-163.31
332	344939.7	5745502	8550N	2700	1418.524	-145.22	-151.17	-157.12	-163.06
333	344562.3	5745296	8600N	2275	1401.632	-148.67	-154.55	-160.42	-166.30
334	344582.8	5745310	8600N	2300	1405.993	-148.26	-154.15	-160.05	-165.94
335	344603.2	5745325	8600N	2325	1411.116	-148.03	-153.94	-159.86	-165.78
336	344623.7	5745339	8600N	2350	1417.589	-147.82	-153.77	-159.71	-165.65
337	344644.2	5745354	8600N	2375	1427.040	-147.82	-153.80	-159.79	-165.77
338	344664.6	5745368	8600N	2400	1424.894	-147.29	-153.26	-159.24	-165.21
339	344685.1	5745383	8600N	2425	1423.531	-146.98	-152.95	-158.92	-164.89
340	344705.6	5745397	8600N	2450	1420.233	-146.55	-152.50	-158.46	-164.41
341	344726.0	5745412	8600N	2475	1420.052	-146.31	-152.26	-158.22	-164.17
342	344746.5	5745426	8600N	2500	1420.655	-146.15	-152.11	-158.06	-164.02
343	344767.0	5745441	8600N	2525	1425.085	-146.07	-152.05	-158.02	-164.00
344	344787.4	5745455	8600N	2550	1426.151	-145.88	-151.86	-157.84	-163.82
345	344807.9	5745470	8600N	2575	1424.995	-145.65	-151.63	-157.60	-163.58
346	344828.4	5745484	8600N	2600	1423.865	-145.51	-151.48	-157.45	-163.42
347	344848.8	5745499	8600N	2625	1423.251	-145.47	-151.44	-157.40	-163.37
348	344869.3	5745513	8600N	2650	1423.370	-145.44	-151.41	-157.38	-163.35
349	344889.8	5745528	8600N	2675	1423.519	-145.32	-151.28	-157.25	-163.22
350	344910.3	5745542	8600N	2700	1424.444	-145.27	-151.24	-157.21	-163.19

APPENDIX B

Maps



PROCESSING HISTORY

note: steps 1-5 were performed using the GravMaster™ software package.

- 1) Instrument value converted to milliGals and shifted to absolute gravity (980984.31 mGals at control station #9051-82 in Blue River, B.C.)
- 2) Add tide correction based on the program of W. Dewhurst.
- 3) Subtract drift correction based on differences in repeat gravity observations.
- 4) Subtract theoretical gravity from each station using 1998 NIMA formula.
- 5) Add free air correction and subtract Bouguer correction based on density 2.70 g/cm³. This step also accounts for instrument height.
- 6) Add near-station terrain corrections using field slope measurements with sloping wedge technique (Barrows and Fett, 1991).
- 7) Add inner and outer zone terrain corrections using Cogbill (1990)² DEM, integrated surface, terrain correction algorithm.
- 8) Gridded using Geosoft RANGRID program.
- 9) Contoured using Muir-GMS CONTUR.
 1. Barrows, L.J. and Fett, J.D., 1991, A sloping wedge technique for calculating gravity terrain corrections, *Geophysics*, Vol. 56, No. 7, p.1061-1063.
 2. Cogbill, A.H., 1990, Gravity terrain corrections using digital elevation models, *Geophysics*, Vol. 55, No. 1, p.102-108.

CASSIDY GOLD CORP.

BROKEN HILL PROJECT
AVOLA, B.C.

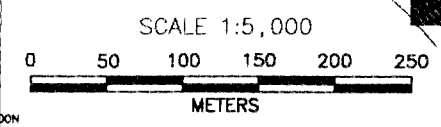
DIGITAL ELEVATION MODEL

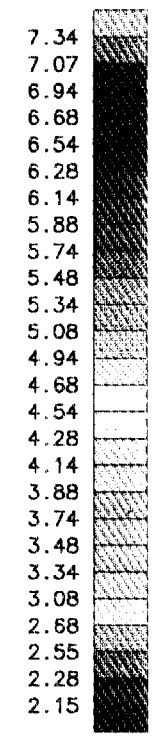
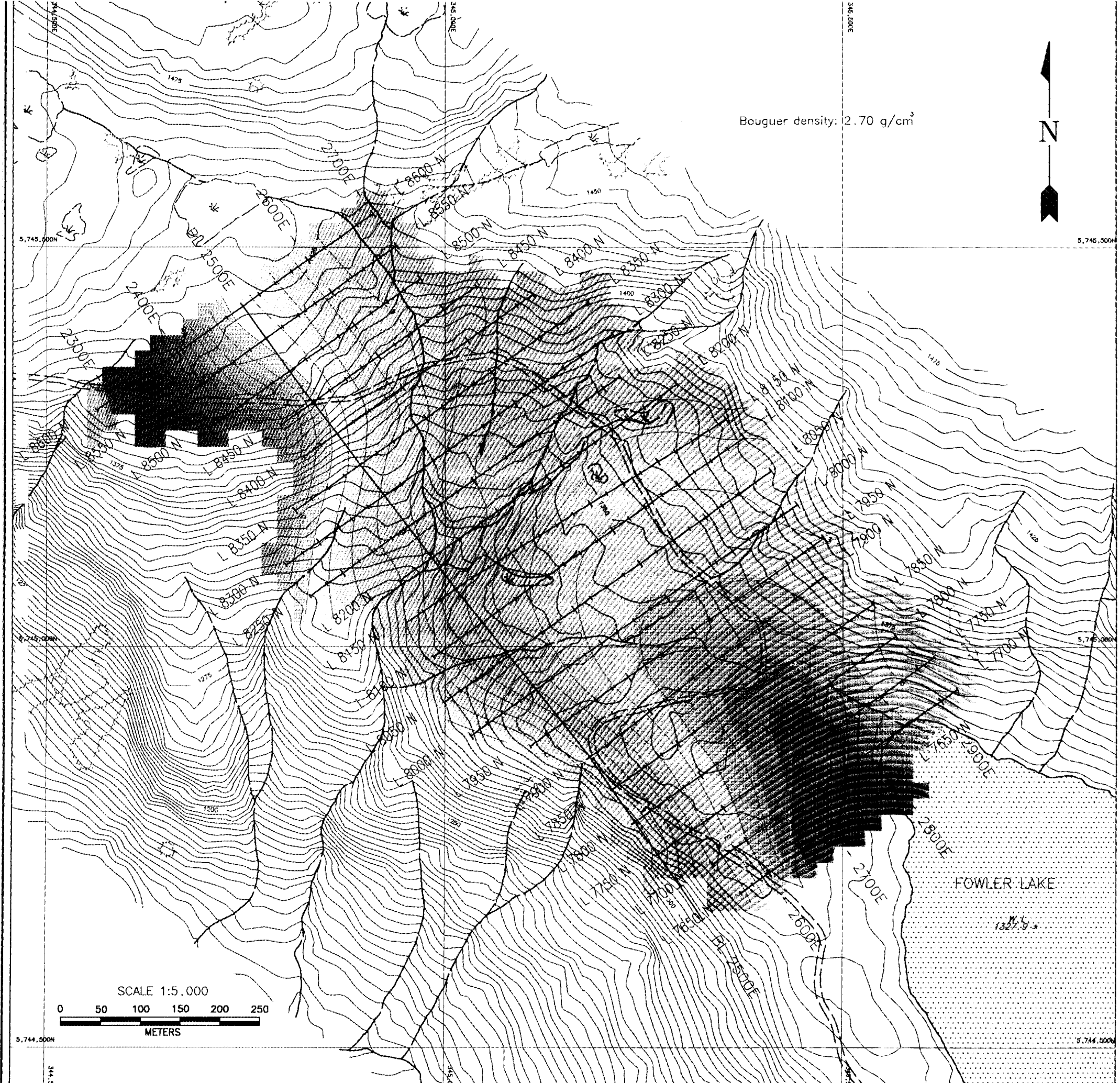
Instrument: LaCoste & Romberg Model G Gravity Meter

Surveyed By: W Kubo, A Colnair	Survey Date: Dec 2000
Processed & Plotted by: Wes Kubo	Date: 23 Feb 2001

DISCOVERY GEOPHYSICS INC.

149 Commercial Rd., Springdale, Nfld. Box 223 A0J 1T0
tel: (709)673-5359 fax: (709)673-5359 email: horizon@thezone.net





Terrain Correction (mgals)

PROCESSING HISTORY

note: steps 1-5 were performed using the GravMaster™ software package.

- 1) Instrument value converted to millGals and shifted to absolute gravity (980984.31 mGals at control station #9051-82 in Blue River, B.C.)
- 2) Add tide correction based on the program of W. Dewhurst.
- 3) Subtract drift correction based on differences in repeat gravity observations.
- 4) Subtract theoretical gravity from each station using 1998 NIMA formula.
- 5) Add free air correction and subtract Bouguer correction based on density 2.70 g/cm³. This step also accounts for instrument height.
- 6) Add near-stations terrain corrections using field slope measurements with sloping wedge technique (Barrows and Fett, 1991).
- 7) Add inner and outer zone terrain corrections using Cogbill (1990)² DEM, integrated surface, terrain correction algorithm.
- 8) Gridded using Geosoft RANGRID program.
- 9) Contoured using Muir-GMS CONTUR.
 1. Barrows, L.J. and Fett, J.D., 1991. A sloping wedge technique for calculating gravity terrain corrections. *Geophysics*, Vol. 56, No. 7, p. 1061-1063.
 2. Cogbill, A.H., 1990. Gravity terrain corrections using digital elevation models. *Geophysics*, Vol. 55, No. 1, p. 102-106.

CASSIDY GOLD CORP.

BROKEN HILL PROJECT
AVOLA, B.C.

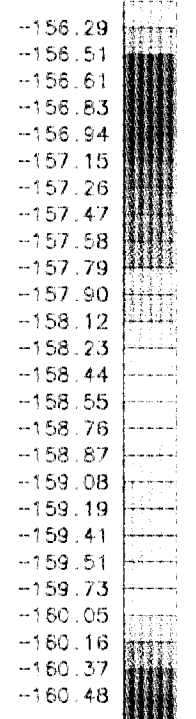
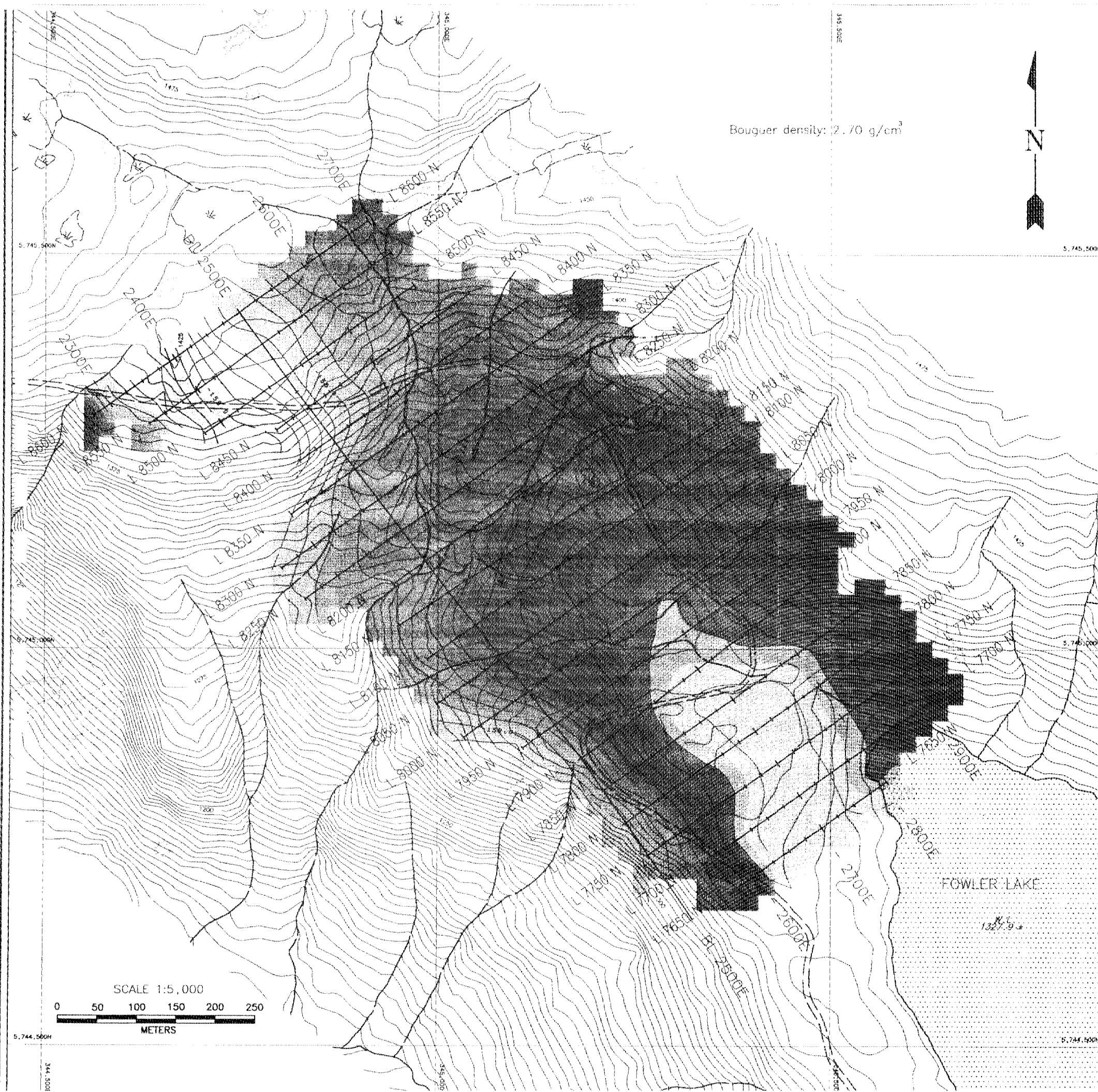
DEM TERRAIN CORRECTION

Instrument: LaCoste & Romberg Model G Gravity Meter

Surveyed By: W. Kubo, A. Colnair	Survey Date: Dec 2000
Processed & Plotted by: Wes Kubo	Date: 23 Feb 2001

DISCOVERY GEOPHYSICS INC.

149 Commercial Rd., Springdale, Nfld. Box 223 A0J 1T0
tel: (709)673-5359 fax: (709)673-5359 email: horizon@thezone.net

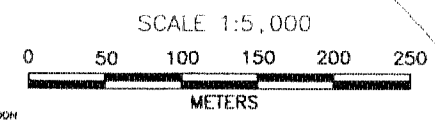


Bouguer Gravity (mgals)

PROCESSING HISTORY

note: steps 1-5 were performed using the GravMaster software package.

- 1) Instrument value converted to milligals and shifted to absolute gravity (980956.31 mgals at control station #9051-B2 in Blue River, B.C.)
- 2) Add tide correction based on the program of W. Dewhurst.
- 3) Subtract drift correction based on differences in repeat gravity observations.
- 4) Subtract theoretical gravity from each station using 1998 NIMA formula.
- 5) Add free air correction and subtract Bouguer correction based on density 2.70 g/cm³. This step also accounts for instrument height.
- 6) Gridded using Geosoft RANGRID program.
- 7) Contoured using Muir-GMS CONTOUR.



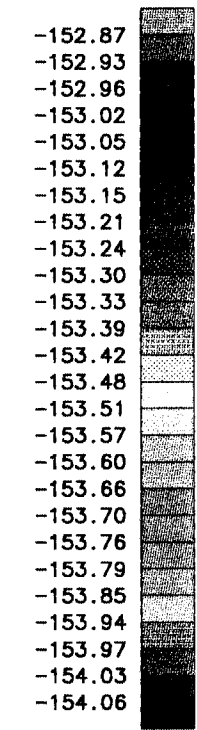
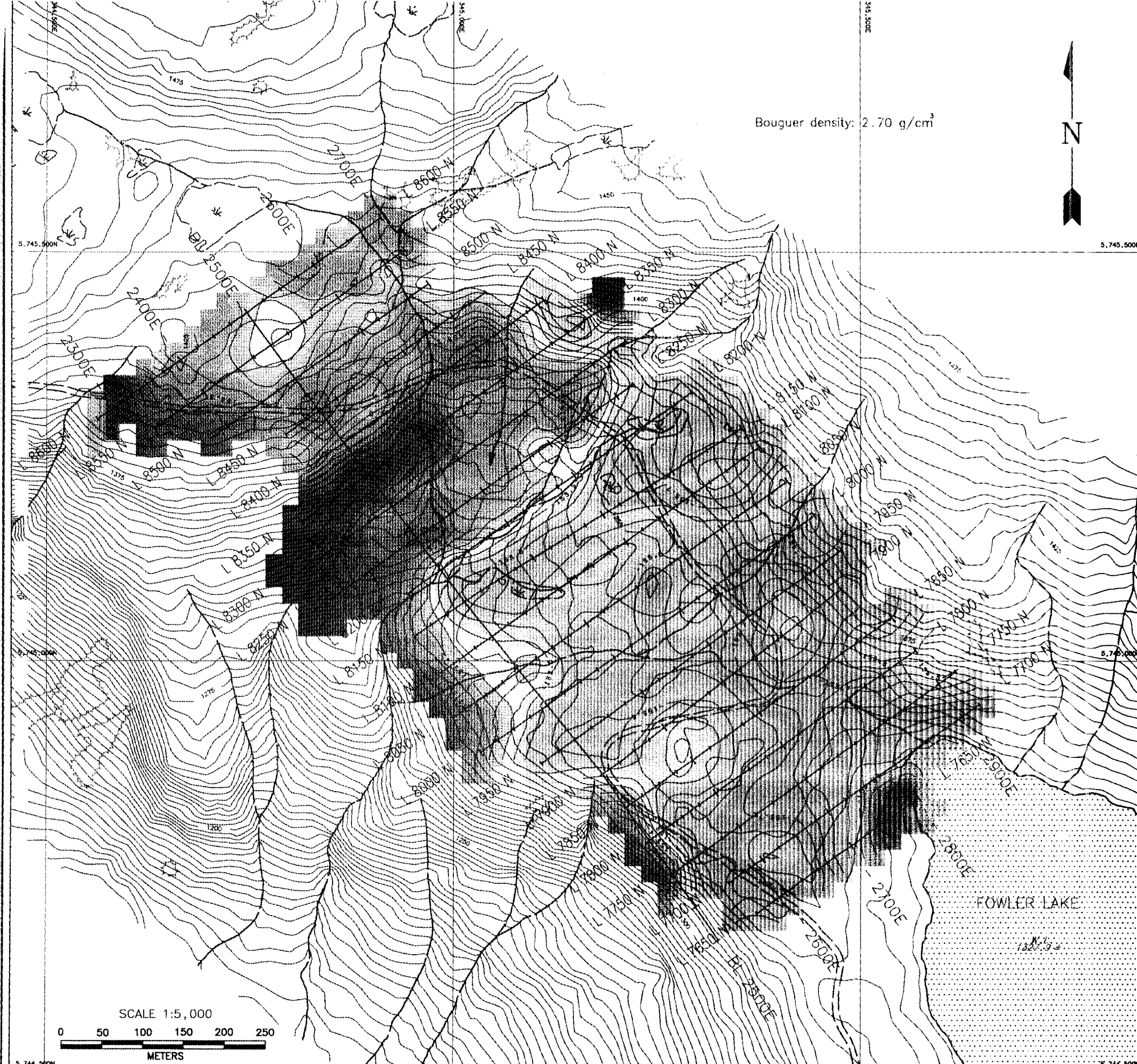
CASSIDY GOLD CORP.

BROKEN HILL PROJECT
AVOLA, B.C.

SIMPLE BOUGUER GRAVITY

Instrument: LaCoste & Romberg Model G Gravity Meter
 Surveyed By: W Kubo, A Colnar Survey Date: Dec 2000
 Processed & Plotted by: Wes Kubo Date: 23 Feb 2001

DISCOVERY GEOPHYSICS INC.
 149 Commercial Rd., Springdale, Nfld. Box 223 A0J 1T0
 tel: (709)673-5359 fax: (709)673-5359 email: horizon@thezone.net



Bouguer Gravity (mgals)

PROCESSING HISTORY

note: steps 1-5 were performed using the GravMaster™ software package.

- 1) Instrument value converted to milliGals and shifted to absolute gravity (980984.31 mGals at control station #9051-82 in Blue River, B.C.)
- 2) Add tide correction based on the program of W. Dewhurst.
- 3) Subtract drift correction based on differences in repeat gravity observations.
- 4) Subtract theoretical gravity from each station using 1998 NIMA formula.
- 5) Add free air correction and subtract Bouguer correction based on density 2.70 g/cm³. This step also accounts for instrument height.
- 6) Add near-station terrain corrections using field slope measurements with sloping wedge technique (Barrows and Fett, 1991).
- 7) Add inner and outer zone terrain corrections using Cogbill (1990) DEM, integrated surface, terrain correction algorithm.
- 8) Gridded using Geosoft RANGRID program.
- 9) Contoured using Muir-GMS CONTUR.
 1. Barrows, L.J. and Fett, J.D., 1991, A sloping wedge technique for calculating gravity terrain corrections, *Geophysics*, Vol. 56, No. 7, p. 1061-1063.
 2. Cogbill, A.H., 1990, Gravity terrain corrections using digital elevation models, *Geophysics*, Vol. 55, No. 1, p. 102-106.

CASSIDY GOLD CORP.

**BROKEN HILL PROJECT
AVOLA, B.C.**

COMPLETE BOUGUER GRAVITY

Instrument: LaCoste & Romberg Model G Gravity Meter

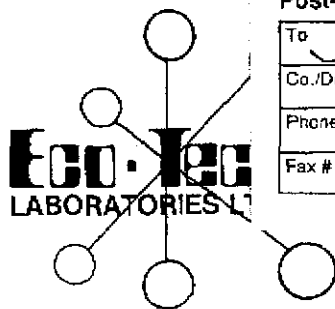
Surveyed By: W Kubo, A Cotnoir	Survey Date: Dec 2000
Processed & Plotted by: Wes Kubo	Date: 23 Jan 2001

DISCOVERY GEOPHYSICS INC.

149 Commercial Rd., Springdale, Nfld. Box 223 ADJ 1T0
tel: (709)673-5359 fax: (709)673-5359 email: horizon@thezone.net

APPENDIX IV

GEOCHEMICAL PROCEDURE AND RESULTS



Post-it™ Fax Note	7671E	Date	# of pages 2
To	Jim Gillis	From	
Co./Dept.		Co.	
Phone #		Phone #	
Fax #		Fax #	828-2269

**ASSAYING
GEOCHEMISTRY
ANALYTICAL CHEMISTRY
ENVIRONMENTAL TESTING**

#2, Kamloops, B.C. V2C 6T4
73-5700 Fax (250) 573-4557
email: ecotech@mail.wkpowerlink.com

Analytical Procedure Assessment Report

MULTI ELEMENT ICP ANALYSIS

Samples are catalogued and dried. Soil samples are screened to obtain a -80 mesh sample. Samples unable to produce adequate -80 mesh material are screened at a coarser fraction. These samples are flagged with the relevant mesh. Rock samples are 2 stage crushed to minus 10 mesh and pulverized on a ring mill pulverizer to minus 140 mesh, rolled and homogenized.

A 0.5 gram sample is digested with aqua regia which contains beryllium which acts as an internal standard. The sample is analyzed on a Jarrell Ash ICP unit.

Results are collated by computer and are printed along with accompanying quality control data (repeats and standards). Results are printed on a laser printer and are faxed and/or mailed to the client.

K:Methods/methicp



ASSAYING
GEOCHEMISTRY
ANALYTICAL CHEMISTRY
ENVIRONMENTAL TESTING

10041 E. Trans Canada Hwy., R.R. #2, Kamloops, B.C. V2C 6T4
Phone (250) 573-5700 Fax (250) 573-4557
email: ecotech@mail.wkpowerlink.com

Analytical Procedure Assessment Report

GEOCHEMICAL GOLD ANALYSIS

Samples are catalogued and dried. Soils are prepared by sieving through an 80 mesh screen to obtain a minus 80 mesh fraction. Samples unable to produce adequate minus 80 mesh material are screened at a coarser fraction. These samples are flagged with the relevant mesh. Rock samples are 2 stage crushed to minus 10 mesh and a 250 gram subsample is pulverized on a ring mill pulverizer to -140 mesh. The subsample is rolled, homogenized and bagged in a prenumbered bag.

The sample is weighed to 10/15/30 grams and fused along with proper fluxing materials. The bead is digested in aqua regia and analyzed on an atomic absorption instrument. Over-range values for rocks are re-analyzed using gold assay methods.

Appropriate reference materials accompany the samples through the process allowing for quality control assessment. Results are entered and printed along with quality control data (repeats and standards). The data is faxed and/or mailed to the client.

K:Methods/geoauana



ASSAYING
GEOCHEMISTRY
ANALYTICAL CHEMISTRY
ENVIRONMENTAL TESTING

10041 Dallas Drive, Kamloops, B.C. V2C 6T4
Phone (250) 573-5700 Fax (250) 573-4557
email: ecotech@direct.ca

CERTIFICATE OF ASSAY AK 2001- 004

CASSIDY GOLD CORP.
#220, 141 Victoria Street
KAMLOOPS, BC
V2C 1Z5

8-Feb-01

ATTENTION: JAMES T. GILLIS, President

No. of samples received: 12

Sample type: Core

Project #: None Given

Shipment #: None Given

Samples submitted by: J. Pautler

ET #.	Tag #	Pb (%)	Zn (%)
1	131301	-	2.83
2	131302	0.82	2.96
4	131304	-	3.92
6	131306	-	3.65

QC DATA:

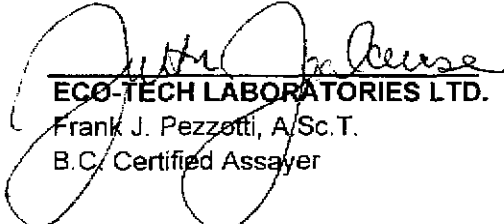
Resplit:

1 131301 2.79

Standard:

CCU-1a 0.35 2.87

XLS/00


ECO-TECH LABORATORIES LTD.
Frank J. Pezzotti, A.Sc.T.
B.C. Certified Assayer



ASSAYING
GEOCHEMISTRY
ANALYTICAL CHEMISTRY
ENVIRONMENTAL TESTING

10041 Dallas Drive, Kamloops, B.C. V2C 6T4
Phone: (250) 573-5700 Fax: (250) 573-4557
email: ecotech@direct.ca

CERTIFICATE OF ASSAY AK 2001- 003

CASSIDY GOLD CORP.
#220, 141 Victoria Street
KAMLOOPS, BC
V2C 1Z5

6-Feb-01

ATTENTION: JAMES T. GILLIS, President

No. of samples received: 40

Sample type: Core

Project #: None Given

Shipment #: 2001-01

Samples submitted by: J. Pautler

ET #.	Tag #	Zn (%)
2	131856	1.69
4	131858	1.58
26	131880	1.19

QC DATA:

Standard:

Mpl

19.01

XLS/00


ECO-TECH LABORATORIES LTD.

Frank J. Pezzotti, A.Sc.T.
B.C. Certified Assayer

8 Feb-01

ECO-TECH LABORATORIES LTD.
10041 Dallas Drive
KAMLOOPS, B.C.
V2C 6T4

ICP CERTIFICATE OF ANALYSIS AK 2001-004

CASSIDY GOLD CORP.
#220, 141 Victoria Street
KAMLOOPS, BC
V2C 1Z5

Phone: 250-573-5700
Fax : 250-573-4557

ATTENTION: JAMES T. GILLIS, President

No. of samples received: 12
Sample type: Core
Project #: None Given
Shipment #: None Given
Samples submitted by: J. Pautler


Values in ppm unless otherwise reported

Et #.	Tag #	Au(ppb)	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
1	131301	-	<0.2	0.61	<5	10	<5	5.67	98	30	90	19	1.62	20	0.13	443	<1	0.01	44	>10000	22	<5	<20	74	0.03	<10	18	<10	24	>10000
2	131302	<5	1.6	0.37	<5	80	10	6.25	54	12	122	171	2.76	<10	0.05	253	<1	0.08	49	5090	8812	<5	<20	68	<0.01	<10	13	<10	3	>10000
3	131303	-	<0.2	1.10	<5	10	10	3.98	<1	3	72	3	0.74	<10	0.11	387	<1	0.02	9	800	22	<5	<20	29	0.06	<10	12	<10	16	162
4	131304	<5	1.1	0.44	<5	15	5	3.45	87	17	87	39	1.80	<10	0.08	409	<1	0.02	26	3230	300	<5	<20	66	0.03	<10	9	<10	<1	>10000
5	131305	-	<0.2	0.37	<5	10	<5	1.30	1	5	99	4	0.77	<10	0.16	171	<1	0.03	13	890	10	<5	<20	36	0.12	<10	9	<10	13	505
6	131306	<5	<0.2	0.59	<5	25	<5	2.04	90	20	95	17	1.50	<10	0.21	297	<1	0.02	22	2160	32	<5	<20	39	0.05	<10	13	<10	<1	>10000
7	131895	<5	<0.2	0.41	<5	15	<5	1.09	<1	3	64	4	0.77	10	0.20	131	<1	0.04	2	270	6	<5	<20	24	0.04	<10	7	<10	7	66
8	131896	<5	<0.2	0.22	<5	15	<5	1.49	<1	1	71	4	0.42	<10	0.07	104	2	0.03	2	260	18	<5	<20	89	0.01	<10	2	<10	7	52
9	131897	<5	0.3	1.03	<5	<5	5	>10	<1	4	34	5	0.63	<10	0.30	415	<1	0.07	11	500	52	5	<20	1103	0.03	<10	10	<10	10	74
10	131898	<5	<0.2	1.97	<5	90	10	0.38	<1	18	79	48	4.58	10	1.05	753	<1	0.05	15	650	<2	<5	<20	21	0.24	<10	72	<10	21	105
11	131899	<5	<0.2	0.38	<5	10	<5	0.32	<1	<1	72	8	0.45	<10	0.06	109	1	0.06	2	270	4	<5	<20	25	0.01	<10	2	<10	13	14
12	131900	-	<0.2	0.98	<5	85	<5	0.74	2	20	60	48	4.86	20	0.17	447	2	0.01	47	920	10	<5	<20	12	0.04	<10	38	<10	1	534

QC DATA:

Resplit:																															
1	131301		<0.2	0.63	<5	10	<5	5.51	94	28	92	20	1.58	20	0.12	433	<1	0.01	40	>10000	24	<5	<20	78	0.03	<10	18	<10	26	>10000	
Repeat:																															
1	131301		<0.2	0.87	<5	10	<5	5.71	98	30	92	20	1.63	20	0.13	468	<1	0.01	44	>10000	20	<5	<20	82	0.03	<10	20	<10	27	>10000	
Standard:																															
GEO'00		120	1.5	1.68	50	170	<5	1.52	<1	18	47	89	3.37	10	0.95	669	<1	0.02	22	650	4	<5	<20	66	0.08	<10	72	<10	10	73	

df/4
XLS/00


 ECO-TECH LABORATORIES LTD.
 Jutta Jealous
 B.C. Certified Assayer

6-Feb-01

ICP CERTIFICATE OF ANALYSIS AK 2001-003

CASSIDY GOLD CORP.

Et #.	Tag #	Au(ppb)	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Tl %	U	V	W	Y	Zn
26	131880	-	1.4	0.98	<5	100	10	0.59	17	13	90	55	2.53	20	0.41	280	<1	0.05	27	220	1216	<5	<20	20	0.10	<10	21	<10	17	>10000
27	131881	-	<0.2	2.10	<5	220	5	0.48	1	27	148	40	4.77	20	1.07	502	<1	0.07	34	840	8	<5	<20	11	0.39	<10	91	<10	31	136
28	131882	-	0.3	1.24	<5	10	10	4.74	<1	5	72	3	0.81	<10	0.21	339	<1	0.02	9	990	16	<5	<20	35	0.12	<10	20	<10	13	113
29	131883	-	0.4	0.99	<5	20	<5	4.85	<1	8	90	24	1.68	20	0.34	389	<1	0.05	13	370	38	<5	<20	159	0.07	<10	14	<10	24	75
30	131884	5	0.4	0.23	<5	15	<5	0.84	<1	3	93	6	0.79	<10	0.15	266	3	0.02	8	170	44	<5	<20	30	<0.01	<10	1	<10	4	31
31	131885	<5	0.3	6.02	<5	150	<5	4.39	<1	35	114	106	4.20	10	1.12	347	<1	0.19	69	1380	20	<5	<20	624	0.23	<10	62	<10	14	72
32	131886	<5	0.2	0.72	<5	25	<5	1.08	<1	6	89	19	1.85	10	0.34	483	2	0.03	12	560	18	<5	<20	31	0.03	<10	14	<10	14	49
33	131887	<5	<0.2	0.22	<5	10	<5	0.39	<1	<1	85	9	0.46	<10	0.04	132	2	0.04	3	120	10	<5	<20	11	<0.01	<10	<1	<10	5	11
34	131888	65	<0.2	2.01	<5	25	15	2.53	2	10	65	30	1.81	10	0.40	677	<1	0.16	36	1170	<2	<5	<20	73	0.07	<10	29	70	12	338
35	131889	<5	<0.2	0.19	<5	5	<5	0.14	<1	<1	104	3	0.28	<10	0.01	90	2	0.04	4	40	<2	<5	<20	5	<0.01	<10	<1	<10	<1	16
36	131890	5	<0.2	1.29	<5	50	5	2.31	<1	14	70	16	2.79	20	0.77	1015	<1	0.04	24	1030	4	<5	<20	37	0.08	<10	36	<10	17	373
37	131891	<5	<0.2	0.26	<5	15	<5	0.84	<1	3	77	13	1.00	<10	0.05	520	2	0.03	7	200	24	<5	<20	39	<0.01	<10	2	<10	10	58
38	131892	<5	<0.2	0.29	<5	10	<5	0.41	<1	1	80	7	0.55	<10	0.04	218	2	0.04	5	150	12	<5	<20	18	<0.01	<10	1	<10	11	49
39	131893	5	<0.2	0.18	<5	<5	<5	0.10	<1	<1	99	6	0.44	<10	0.02	242	2	0.04	3	180	<2	<5	<20	3	<0.01	<10	<1	<10	6	12
40	131894	<5	<0.2	0.30	<5	15	<5	1.15	<1	<1	74	7	0.57	10	0.02	171	2	0.03	3	280	12	<5	<20	34	<0.01	<10	<1	<10	12	28

QC DATA:

Resplit:

1	131855	<5	<0.2	3.99	<5	45	<5	5.90	<1	8	102	13	1.15	20	0.35	161	<1	0.23	15	4610	4	<5	<20	587	0.07	<10	25	<10	36	56
36	131890	5	<0.2	1.33	<5	50	<5	2.30	<1	15	82	15	2.90	20	0.77	1049	<1	0.04	30	1040	8	<5	<20	32	0.09	<10	38	<10	18	374


Repeat:

1	131855	<5	<0.2	3.85	10	45	<5	5.99	<1	8	81	13	1.19	20	0.35	183	<1	0.22	15	4550	4	5	<20	573	0.07	<10	24	<10	34	52
10	131864	-	0.4	0.31	<5	15	<5	2.04	<1	3	120	9	0.71	<10	0.08	456	3	0.01	7	100	38	<5	<20	91	<0.01	<10	1	<10	7	20
18	131872	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
19	131873	-	<0.2	0.29	15	35	<5	2.07	<1	9	94	23	2.07	10	0.40	300	3	<0.01	20	610	24	<5	<20	109	<0.01	<10	4	<10	6	65
35	131889	<5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
36	131890	-	<0.2	1.29	<5	50	<5	2.31	<1	14	72	16	2.88	20	0.77	1057	<1	0.04	27	1070	8	<5	<20	32	0.08	<10	38	<10	17	366

Standard:

GEO'00	125	1.4	1.83	50	175	<5	1.68	<1	20	56	87	3.79	20	0.99	718	<1	0.03	28	750	14	<5	<20	65	0.11	<10	79	<10	10	76
GEO'00	-	1.4	1.84	55	175	<5	1.71	1	20	58	89	3.85	20	0.99	726	<1	0.02	29	740	12	<5	<20	65	0.12	<10	81	<10	11	80

d1/3
XLS/00


 ECO-TECH LABORATORIES LTD.
 Jutta Jealous
 B.C. Certified Assayer

6-Feb-01

ECO-TECH LABORATORIES LTD.
10041 Dallas Drive
KAMLOOPS, B.C.
V2C 6T4

ICP CERTIFICATE OF ANALYSIS AK 2001-003

CASSIDY GOLD CORP.
#220, 141 Victoria Street
KAMLOOPS, BC
V2C 1Z5

Phone: 250-573-5700
Fax : 250-573-4557

ATTENTION: JAMES T. GILLIS, President

No. of samples received: 40

Sample type: Core

Project #: None Given

Shipment #: 2001-01

Samples submitted by: J. Pautler

Values in ppm unless otherwise reported

Et #.	Tag #	Au(ppb)	Ag	Al %	As	Ba	Bi	Ca %	Cd	Co	Cr	Cu	Fe %	La	Mg %	Mn	Mo	Na %	Ni	P	Pb	Sb	Sn	Sr	Ti %	U	V	W	Y	Zn
1	131855	<5	<0.2	4.00	<5	50	<5	5.88	<1	8	81	14	1.14	20	0.36	158	<1	0.23	16	4770	<2	<5	<20	601	0.07	<10	25	<10	33	48
2	131856	5	<0.2	0.56	<5	15	<5	4.15	61	11	95	15	1.36	10	0.13	484	<1	0.02	20	9440	194	<5	<20	78	0.03	<10	17	<10	19	>10000
3	131857	<5	0.3	0.27	<5	<5	<5	1.43	2	<1	139	7	0.38	70	0.03	85	2	0.06	9	4760	6	<5	<20	34	0.03	<10	6	<10	52	467
4	131858	-	0.4	0.86	<5	20	<5	3.39	51	15	110	14	2.39	30	0.50	538	<1	0.05	31	990	98	<5	<20	108	0.07	<10	11	<10	8	>10000
5	131859	-	0.3	0.64	<5	25	<5	2.50	<1	12	63	28	2.12	30	0.46	428	<1	0.04	35	150	12	5	<20	58	0.18	<10	11	<10	22	351
6	131860	<5	<0.2	1.63	<5	45	<5	3.11	1	21	108	38	4.33	20	1.25	1010	4	0.02	30	660	14	<5	<20	189	0.01	<10	38	<10	7	186
7	131861	<5	<0.2	0.26	<5	20	<5	0.77	<1	2	84	5	0.61	<10	0.05	164	2	0.01	14	200	68	<5	<20	40	<0.01	<10	2	<10	4	97
8	131862	<5	<0.2	1.12	<5	45	5	9.06	1	22	69	35	4.29	20	0.80	1490	3	0.01	38	900	8	<5	<20	590	0.02	<10	25	<10	16	206
9	131863	5	<0.2	0.77	<5	45	<5	6.52	2	22	67	60	4.60	20	0.37	1187	3	0.01	41	730	14	<5	<20	322	<0.01	<10	21	<10	13	174
10	131864	<5	0.3	0.34	<5	20	<5	1.95	<1	3	116	10	0.70	<10	0.08	445	3	0.01	9	180	36	<5	<20	100	<0.01	<10	2	<10	7	20
11	131865	-	<0.2	1.24	<5	10	10	>10	2	4	36	10	1.43	<10	0.54	1287	<1	0.04	6	610	12	5	<20	801	0.02	<10	14	<10	25	228
12	131866	-	0.3	1.29	<5	10	5	7.59	<1	5	67	2	1.26	<10	0.72	523	<1	0.03	8	700	28	5	<20	192	0.04	<10	13	<10	19	232
13	131867	-	0.3	0.36	<5	20	<5	0.52	<1	1	88	4	0.54	20	0.09	110	2	0.05	3	630	6	<5	<20	22	0.02	<10	4	<10	19	14
14	131868	-	0.2	0.14	<5	10	<5	0.15	<1	1	86	6	0.35	<10	0.02	70	3	0.03	3	150	12	<5	<20	4	<0.01	<10	<1	<10	7	12
15	131869	-	<0.2	1.19	<5	80	5	0.55	<1	12	94	16	2.64	10	0.58	352	<1	0.03	19	290	8	<5	<20	20	0.10	<10	28	<10	7	73
16	131870	-	<0.2	0.79	<5	55	<5	0.58	<1	10	101	15	2.23	20	0.35	320	2	0.03	17	200	4	<5	<20	34	0.04	<10	16	<10	8	107
17	131871	70	0.3	0.22	60	15	<5	0.33	<1	<1	125	6	0.51	<10	0.02	112	2	0.01	4	170	14	<5	<20	12	<0.01	<10	<1	<10	2	22
18	131872	16	0.3	0.24	<5	10	<5	1.06	<1	<1	95	5	0.38	<10	0.01	147	2	0.01	2	300	32	<5	<20	65	<0.01	<10	<1	<10	6	13
19	131873	-	<0.2	0.26	10	30	<5	2.12	<1	8	96	23	2.06	10	0.39	303	3	<0.01	20	590	22	<5	<20	107	<0.01	<10	3	<10	6	60
20	131874	65	<0.2	0.26	80	20	<5	0.14	<1	<1	87	6	0.36	<10	0.01	273	2	<0.01	5	70	30	<5	<20	5	<0.01	<10	<1	<10	7	156
21	131875	<5	<0.2	1.26	<5	75	<5	2.31	2	17	125	33	3.53	30	0.69	398	<1	0.04	30	760	6	<5	<20	77	0.14	<10	47	<10	32	413
22	131876	-	<0.2	4.75	<5	80	<5	3.55	1	32	193	38	3.26	<10	1.21	647	<1	0.32	80	780	10	<5	<20	309	0.14	<10	107	<10	7	295
23	131877	-	<0.2	2.36	<5	145	10	0.31	1	26	139	29	5.17	20	1.19	525	<1	0.05	44	280	14	<5	<20	10	0.33	<10	85	<10	17	220
24	131878	-	<0.2	0.89	<5	25	<5	0.81	<1	6	70	11	1.93	50	0.44	305	2	0.05	3	440	12	<5	<20	17	0.08	<10	28	<10	24	34
25	131879	<5	<0.2	1.55	<5	105	10	0.99	<1	13	99	23	2.68	20	0.66	358	<1	0.06	24	450	30	<5	<20	36	0.11	<10	35	<10	12	94

APPENDIX V

DIAMOND DRILL LOGS - J. PAUTLER, P. Geo.

TABLE OF LITHOLOGICAL UNITS AND LEGEND

TERTIARY:

T Unit 6 Tertiary mafic dykes: The dykes are very fine grained, dioritic in composition and contain 1-2mm phenocrysts of pyroxene.

CRETACEOUS - TERTIARY:

xx Unit 5 Pegmatite: Pegmatite occurs primarily as sills but locally crosscuts as dykes and consists of quartz, feldspar and biotite. Occasionally muscovite dominates over biotite.

Gdi Unit 4 Granodiorite: Minor dykes of weakly foliated generally medium grained granodiorite of uncertain age are evident.

PROTEROZOIC to PALEOZOIC: Shuswap Metamorphic Complex

c/s Unit 3 Calc-silicate: This unit grades from a fine grained, banded pale green and pink calc-silicate to coarser grained skarn (**SK**) containing calcite, quartz, diopside, lesser garnet, actinolite, and tremolite. May contain beds and pods of white crystalline or grey banded marble (**Mb**) and chert.

- - Unit 2: Biotite Gneiss: Unit 2 consists of quartz-feldspar-biotite gneiss (**Gn**) with lesser schist. Commonly weathers gossanous due to the presence of trace pyrite and pyrrhotite and high iron content. Narrow quartzite beds may be present (**Qte**).

v v Unit 1: Amphibolite Gneiss: Unit 1 exhibits a dark, often green, medium grained groundmass dominated by amphiboles with lesser amounts of biotite and plagioclase. Laminae with almandine garnets, 0.5 to 1 cm in size, are common. May contain narrow bands of calc-silicate and larger bands of biotite gneiss.

py pyrite

po pyrrhotite

sp sphalerite

ga galena

DEPTH (metres) From To	GRAPHIC	DESCRIPTION	REMARKS	STRUCTURE		ALTERATION	METALLIC MINERALS (%)	SAMPLE DATA				RESULTS			
				Angles	Veins			SAMPLE No.	FROM	TO	LENGTH				
26.8 - 29.2		calc-sil with up to 0.5m bands of Mb. with w-s lim, vugs, very minor ^{9°} ply also with m.lim.		0-10°	fract	w-s lim	tr po	13165	27.9	29.2	1.3				
								13166	29.2	30.5	1.3				
29.2 - 32.8		peg - assimilating cis horizon; Calc sil remnants, more siliceous cherty zone @ 32.2-32.3 @ 32.6-33.8 - new lim grading into lower cherty zone.													
33.8 - 38.7		siliceous unit - grades from sil k.w. Gneiss to 34.1-34.7 - cherty zone - dk grey-purplest - more limic peg through section cherty zone has more calc sil development near base of section		55°	contact										
				70° CH	Soln banding in chert	possible related to D-200 structures		13178	33.8	34.1	0.3				
				20° CH				13167	34.1	34.7	0.6				
								13168	34.7	35.8	0.9				
				70° CA	Arch in Gneiss			13169	35.8	37.7	1.9				
								13170	37.7	38.7	1.0				
38.7 - 41.9	X F	Pegmatite - good granitic texture coarse crystalline ± w.lim @ 38.7-41.9 - Fault Zone		10° CA	fault	w-sil	12% Pyro								
	X X	@ 38.9-39.1 - s sil zone, lim vugs				w lim on fract									
49.1	X X	w 47.8-49.1 vuggy sil zone in peg				5% apy, m (8) imp		13181	38.7	39.7	1.0				
	X X	clean qtz				w-s-s-l									
				85°	lower contact	m.lim. s.sil		13182	47.4	48.5	1.1				

HOLE No. ^{BH} DDH 01-2

DIAMOND DRILL LOG

COMPANY Cassidy Gold
 PROJECT Bickell Hill
 PROPERTY _____

NTS RJM/14
 CLAIM _____
 ELEVATION 1410 m
 GRID COORD 8550 N / 2350 E
 NORTHING _____
 EASTING _____

DATE: Collared 27/01/01 PM
 Completed 28/01/01
 Logged 30/01/01
 LOGGED BY: J. Faulter
 CORE SIZE: NQ

DEPTH	DIP	AZ.
	0	-90

LENGTH: 84.177
 DEPTH of OVB: 3.7m
 CASING REMAINING: _____
 WATERLINE LENGTH: _____
 PROBLEMS: _____

DEPTH (metres) From To	GRAPHIC	DESCRIPTION	RECOVERY	STRUCTURE		ALTERATION	METALLIC MINERALS (%)	SAMPLE DATA				RESULTS				
				Angles	Veins			SAMPLE No	FROM	TO	LENGTH m					
0 - 3.7m		Casing 6.0" dia 4.0" dia GROSS														
3.7m - 14.2m	C/S	act. diap. gnt calc silicate with minor peg dys 2-10" of section, minor bio Gneiss - rusty zones 49-54m and 123-125m now bio Gneiss sections		75° 05°	thin fol'n fractures	m limb's fault	tr po	13176	44	54	1.0m					
								13177	12.1	12.6	0.5m					
								13182	12.4	12.5	0.6					
14.2 - 23.8m	X Y Y X	Peg Gneiss gneiss in section to km greyish-white grades coarse down section, some bio Gneiss remnants (lots of py, calc in pegs to 1cm (some mafic Gneiss remnants (lots) with po as well) mafic Gneiss => "pepiled" big pegs)		5-20°	fract	Wren	tr po									
23.8m - 31.3m	C/S M/S	green-pink calc-silicate with 50% gnt banded massive minor peg dys in section straight dys		70° 45°	anding contact		5% po at base of section									

concrete cube with minerals → ...

DEPTH (metres) From To	GRAPE-C	DESCRIPTION	RECOVERY	STRUCTURE		ALTERATION	METALLIC MINERALS (%)	SAMPLE DATA				RESULTS					
				Angles	Vains			SAMPLE No.	FROM	TO	LENGTH	ppm Zn	% Zn				
89- 131	x x x	Pegmatite of some xls to 5cm. minor grey banded gtz, occ. gnt, occ. slabs of ^{py and} pegmatite - fine grained towards bottom of section; 1.2% subalt?	100%				pg = 1/2% py = 1/2%										
131- 171	-- -- --	White pegmatite ^{matrix} Gneiss - green grading near margin, 10% hb - more greenish layers, some porphyroblasts		53°CA	contact												
171- 25.9	++ ++ +	Pegmatite - large clots of brown biotite ^{throughout} top of section local zones up to 30cm with remnants of bio-Gneiss, local clots of py ^{in upper half} - some warner sections of Peg (5-7cm xls)					py = 1/2%										
25.9- 26.5	4/5 *	CALC SILICATE - SKARN gtz - w/ - diap - ^{cherty} Flom - gnt, ^{at} Flom with 15% sphal over 5cm @ 26.1m as stringers and tr. gnt ^{isolated ilmenite in crs} in remainder of section		70°CA 65-60 65°	contact folia sp str.		sp, tr gnt	131856	25.9	26.5	0.6	1.69%					
26.5- 26.8	x x	Peg 0.5cm green size up to 1cm															
26.8- 27.5	e/s *	CALC SILICATE ad-flom - wall - calc-gtz calc-silicate to skin with pe; minor peg ^{veins to 2cm wide} @ 26.9m - 1cm band of sp		45°CA	contact		sp, tr gnt py 1/2%	131857 131858 131859	26.5 26.8 27.0	26.8 27.0 27.5	0.3 0.8 0.5	467 1.58					

1.22% Zn / 1.1%

HOLE No. ^{BH} DDH 01-2

PAGE 1 of

DIAMOND DRILL LOG

COMPANY Cassidy Gold
 PROJECT Bickers Hill
 PROPERTY _____

NTS 82m/14
 CLAIM _____
 ELEVATION 1410 m
 GRID COORD 8550N/2350E
 NORTHING _____
 EASTING _____

DATE: Collared 27/01/01 PM
 Completed 28/01/01
 Logged 30/01/01
 LOGGED BY: J. Pautler
 CORE SIZE: AK2

DEPTH	DIP	AZ.
<u>0</u>	<u>-00</u>	<u>—</u>

LENGTH: 84.4m
 DEPTH of OVB.: 3.7m
 CASING REMAINING: _____
 WATERLINE LENGTH: _____
 PROBLEMS: _____

DEPTH (metres) From To	GRAPHIC	DESCRIPTION	LITHOLOGY	STRUCTURE		ALTERATION	METALLIC MINERALS (%)	SAMPLE DATA				RESULTS						
				Angles	Veins			SAMPLE No.	FROM	TO	LENGTH							
0 - 3.7m		CASING 60% peg 40% bio Gneiss																
3.7m - 14.2m	C/S	act. drop-gnt calc silicate with minor peg dys 3-10% of section, minor bio Gneiss - rusty zones 4.4-5.4m and 12.3-12.5m more bio Gneiss sections		75° 0.5°	thin film fracture	m.l.m. s. fault	tr. pa.	131876	4.4	5.4	1.0m							
								131877	12.1	12.6	0.5m							
								131882	12.4	12.5	0.6							
14.2 - 23.8m	X	Peg from gneiss 2-0.5cm to 1cm greyish-white granules coarse down section, some bio Gneiss remnants		5-20°	fract	W ser.	tr. pa.											
	X	clots of peg. 20m peg to 1cm (some mafic Gneiss remnants (clots) with po as well) mafic Gneiss => replaced by po.					tr. pa.											
	X						tr. pa.											
23.8m - 31.3m	C/S	gran-pink calc-silicate with 50% quartz banded mafic minor peg dys in section { biog. dys		70° 45°	banding contact													

coarse calc-silicate minerals -> thin

DIAMOND DRILL LOG

COMPANY Cassidy Gold
 PROJECT Broken Hill
 PROPERTY _____

NTS E2M/14 DATE: Collared 29/01/01 pm DEPTH 0 DIP -90 AZ. _____ LENGTH: 81.4m
 CLAIM _____ Completed 30/01/01 am DEPTH 0 DIP -90 AZ. _____ DEPTH of OVB.: 6.1m
 ELEVATION 1354m Logged 1/02/01 CASING REMAINING: _____
 GRID COORD 7070N/2600E LOGGED BY: J Pautler WATERLINE LENGTH: _____
 NORTHING _____ CORE SIZE: NØ PROBLEMS: _____
 EASTING _____

DEPTH (metres) From To	GRAPHIC	DESCRIPTION	BUCKYMETRE	STRUCTURE		ALTERATION	METALLIC MINERALS (%)	SAMPLE DATA				RESULTS					
				Angles	Veins			SAMPLE No.	FROM	TO	LENGTH						
0-6.1		CASING - PEGMATITE, very much b.o. Gneiss															
6.1-11.1	X Y	Pegmatite - gnt rich calc sil and bio Gneiss sections				w/c lay, w. some w/lim.	tr py, po										
11.1-18.9	-	Biotite Gneiss on calc sil development of 1.5cm layers, 2.5' in reg. in section		50° CA 60"	contact fol'n		tr po										
	F	Rubbly zone from 133 to 14.6 m - fault	85%														
14.3-31.1	-	Pegmatite - some gnt @ 20.4 - 21.0 fault		15° CA	in fault	w. some m.l.m. w/ clay, w. chert	1% py	13884	20.4	21.1	0.7						
21.1-23.7	C/S	Calc-silicate gnt rich diop-sil, some gnt & cal - some bio Gn sections		65°	banding		1/2 po										
23.7-28.6	X Y	Bio Gneiss with 60° N Reg.		15° CA 65°	contact fol'n contacts		1/2 to po in py tr po in Gn										
28.6-		Calc-silicate light green-pink diop gnt @ 29.3 - 29.8 2-3% po - grades		55° CA	contact		1/2 to po										
31.3		to Bio Gneiss from 30.3 - 31.3					5% po	13885	29.3	29.8	0.5						

DIAMOND DRILL LOG

HOLE No. BH-DDH01-8

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COMPANY Cassidy Gold
 PROJECT Broken Hill
 PROPERTY _____

NTS 80 M/14
 CLAIM _____
 ELEVATION 1345m
 GRID COORD 7720N/25+65E
 NORTHING _____
 EASTING _____

DATE: Collared 31/01/01
 Completed 1/02/01
 Logged 2/02/01
 LOGGED BY: J Painter
 CORE SIZE: 1/02/01

DEPTH	DIP	AZ.
0	-60	235

LENGTH: 997m
 DEPTH of OVB.: 6.1m
 CASING REMAINING: _____
 WATERLINE LENGTH: _____
 PROBLEMS: _____

DEPTH (metres) From To	GRAPHIC	DESCRIPTION	RECOVERY	STRUCTURE		ALTERATION	METALLIC MINERALS (%)	SAMPLE DATA				RESULTS						
				Angles	Veins			SAMPLE No	FROM	TO	LENGTH m							
0 - 6.1		CASING - drop-out - gat stem pegmatite blue Gneiss																
6.1 - 7.1	C/S	Calc silicate grading to minor biotite Gneiss - 10cm vuggy peg at start with s. lim; some mgk in sections of calc-sil/Gn notably at 6.2 and 7.1m near peg contacts - light green to tan pink calc sil.		55° CA	banding in cfs	f tr mgk, pe		131870	6.1	7.1	1.0							
7.1 - 8.4		Pegmatite - very fract, broken from 7.1 - 8.6 appears silicified 9.3-9.4m		35° CA	fract	± w-melag, s lim + m-s sil, m lim	+ r po, py 42% po	131891	7.1	8.4	1.5							
8.4 - 12.2		Fault @ 14.6 - 17.4 higher mass, ser alt'd peg with py, po		0-15° N	fault	→ S. rb, m lim, w lim M ser	1/2 - 1% po 1-2% py, po	131892	8.6	9.8	1.2							
12.2 - 17.9		@ 14.2 - 1m zone blue Gn faulting from 14.4 - 17.9m		30° CA	contact													
17.9 - 26.6		→ remnant Mb zone 25.9 - 26.6m in peg		75° CA 25° CA	folia			131894	25.9	26.7	0.9							

DIAMOND DRILL LOG

HOLE No. BH DDH 01-13

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COMPANY Cassidy Gold Corp.
PROJECT Broken Hill
PROPERTY

NTS 32m/14 DATE: Collared 3/02/01
 CLAIM _____ Completed 3/02/01
 ELEVATION 7407m 1406m Logged 4/02/01
 GRID COORD 8490N/2450E
 NORTHING _____ LOGGED BY: J. Pautler
 EASTING _____ CORE SIZE: _____

DEPTH	DIP	AZ	LENGTH:
0	-45	085°	41.8m
			DEPTH of OVB.: 5.5m
			CASING REMAINING: _____
			WATERLINE LENGTH: _____
			PROBLEMS: _____

DEPTH (metres) From To	GRADE	DESCRIPTION	RECOVERY	STRUCTURE		ALTERATION	METALLIC MINERALS (%)	SAMPLE DATA				RESULTS		
				Angles	Veins			SAMPLE No.	FROM	TO	LENGTH m	PPM Zn	% Zn	% Pb
0-5.5		CASING												
5.5-10.7		Pegmatite m-cg. avg 1cm xls, some gnts @ 7.0-7.3m - cherty zone @ 13.0m weak fault - fracturing		20° fault 24,60 fractures		w. rsk lim 2-12% py								
10.7-21.1		Pegmatite with what appears to be remnant Bio Grains sections making up to 30% of section, some remnant frags of mafics in py => chl, po		62° CA fold contacts		tr chl	tr po							
21.1-28.4		Calc-silicate stain gnt rich - gnt - deep-gnt - act - hem-cal @ 21.3 - 10cm fault zone young, py, po - some buff-oliv bands top: @ 23.5 - 24.0 - act hem @ 24.5 - 24.4 dissem and sp bands in calc sil stain to cherty exhalite? cherty exch from 24.9 - 25.5m - sp in bands? trgn and some		40° contact 33° banding 45° fault			1% sp dissem 2-3% sp + trgn 10% py, po, trgn	131301	24.5	24.9	0.7	2.83		
				40° banding 30° bands in chert		very siliceous cherty exch		131302	24.9	25.5	0.6	2.94	0.82	2.50% 3.9%
								131303	25.5	26.3	0.8	10.2		
									25.5	26.3	0.8	10.2		

HOLE No. BH-DDH 01-13

DEPTH (metres) From To	GRAPHIC	DESCRIPTION	RECOVERY	STRUCTURE		ALTERATION	METALLIC MINERALS (%)	SAMPLE DATA				RESULTS					
				Angles	Veins			SAMPLE No.	FROM	TO	LENGTH M	ppm Zn	% Zn				
21.1 - 28.4		ga in fractures - barren calc-sil skarn zones from 25.5-26.3 and 27.5-27.8 m @ 26.3m 3-5cm wide band of sp (15-20% / 5cm) @ 28.4 - 1-3cm band of sp.		30°	sp. band		7-10% sp	13204	26.3	27.5	0.2						
				48°	sp band		5-8% sp	13305	27.5	27.8	0.3	505		392			
				30° CA	contact												
28.4 - 33.7		Bio Gneiss with ≈ 25% pyromatite dykes, minor calc silicate @ 29.7 - 29.9 m		45° CA	fault												
				40° CA	contacts		≈ 4% sp in calc silicate										
				50° CA	contact												
33.7 - 39.6		Pyromatite - generally m.s. @ 37.1 - minor fault @ 37.8 - 38.5 - calc silicate zone in peg top bio X ₂ near bottom of peg section.		15° CA	fault												
				30°	contact												
				45-50	banding												
				30°	contact												
39.6 - 41.8		Biotite Gneiss @ 40.2 - 40.5 - parasitic folding evident with axes "b. fold"		35°	fold and minor fold axes												
41.8 - 404																	