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GEOLOGICAL AND GEOCHEMICAL REPORT ON THE STEWART PROPERTY

NELSON MINING DIVISION, BC
MAPSHEETS: 082F/3 and 82F/6
LATITUDE 49°16'N LONGITUDE 117°18'E

for

EMGOLD MINING CORPORATION
1400 - 570 GRANVILLE STREET
VANCOUVER, BC
V6C 3P1

by

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Consulting Geologist

May 2002

SUMMARY

The Stewart Property, containing several gold, molybdenum, zinc and tungsten prospects, is located near the town of Salmo in southeastern British Columbia. The property lies predominantly within lower Jurassic Elise Formation (Rossland Group) mafic volcanics and associated mid Jurassic and younger intrusive rocks.

The Stewart Property was worked by a number of operators from 1974 to 1998. Emgold Mining Corporation acquired the Stewart Property in 2001. Previous work on the property includes geology, geochemistry, geophysics, trenching and drilling. The drilling was concentrated on the Stewart Moly Zone, with smaller programs carried out on the North and South Craigtown Grids (formerly known as the Minnova north and south grids).

This report presents the results of the 2001 exploration program consisting of soil geochemical surveys over five grid areas defining zones of anomalous gold, zinc, molybdenum and tungsten.

For 2002, the recommended work program consists of detailed geological mapping and rock chip sampling, expanded soil geochemical surveys, and excavator trenching. This program is budgeted at $40,000.00.

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1) INTRODUCTION

The Stewart Property contains a number of gold, molybdenum, tungsten and zinc prospects, located near Salmo in southeastern British Columbia. Emgold Mining Corporation acquired the property from vendors Jack and Eric Denny in mid 2001.

Work done by Emgold in 2001 consisted of soil sampling five grid areas, and the results from this program show the need for expanded geochemical surveys and follow up geological mapping on the property. This report covers the details and results of the 2001 work program.

2) LOCATION AND ACCESS

The Stewart Property is located 7 kilometres north of Salmo, and directly west of Ymir, in the Nelson Mining Division of southeastern British Columbia (Figure 1). The claims are centred at latitude 49°16'N and longitude 117°18'E within mapsheets 82F/3 and 82F/6.

Access to the Stewart Property is either via the Erie Creek Road, 4 kilometres west of Salmo on Highway 3, or by the Stewart Creek Road, 4 kilometres north of Ymir on Highway 6. A number of logging and old mining roads provide access throughout the claims. These roads are in various conditions, some being maintained and others being overgrown with brush and alder.

3) PHYSIOGRAPHY

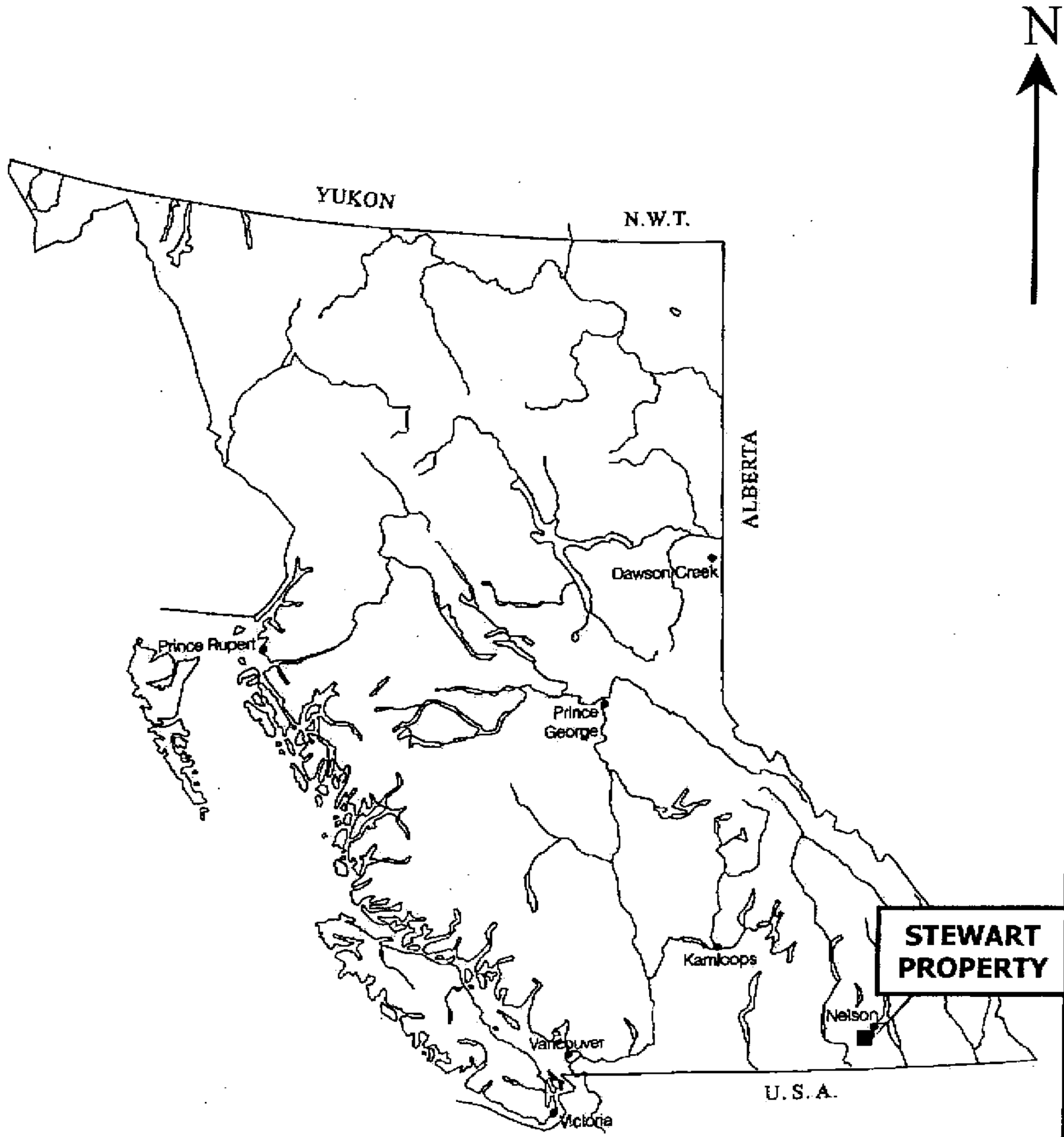
The Stewart Property is located in an area of rugged terrain. Topography on the property is steep with elevations ranging from 750 metres to 1,950 metres. Outcrop exposure is generally limited, but ridge crest outcrops are fairly common. The lower slopes and valley bottoms have extensive deposits of till.

Several portions of the claim area have been recently logged, with the remainder being covered with first and second growth forest consisting of dominantly conifer stands, but also some deciduous stands and minor brush fields.

The climate is moderate. Precipitation can occur throughout the year, but is lightest during the summer months. Most of the property is snow covered during December to April, with the highest regions not melting off until June or July. Temperatures typically range from –15° to 20° C annually.

4) HISTORY

The Stewart Property is located in an area of much early mining activity, with the Ymir, Erie, Sheep Creek and Nelson districts being sites of extensive exploration and production for over 100 years.



EMGOLD MINING CORPORATION

STEWART PROPERTY

NTS: 082F/6W NELSON MINING DIVISION

LOCATION MAP

BY: LD

DATE: MAY 2002

FIGURE: 1

1:1,000,000 SCALE

Recorded work on the Stewart Property began with surface exploration and development of the Arrow Tungsten showing by Premier Gold Mining Co. in 1942. Tungsten mineralization was identified over a 1000 foot (300 metre) strike length, with samples up to a few feet wide of over 1% WO_3. In the late 1960s and early 1970s, the property was explored for copper by Quintana and Copper Horn. Prospectors Eric and Jack Denny staked the property in 1978, and Shell Canada, followed by Selco, explored the property for molybdenum. Most of this work (including extensive drilling) was focused on the Stewart Moly and Breccia Summit areas. Large areas of the property were also soil sampled on a wide grid, and covered by airborne magnetic and impulse EM surveys.

From the mid 1980s to the mid 1990s, several groups explored the property for gold. US Borax and Lacana conducted geochemical surveys, concentrating in the Rest Creek area. Minnova, followed by Cameco, explored the Craigtown Creek area with geochemistry and geophysics (induced polarization and magnetics). Cameco drilled four core holes into one of the targets identified by this work. The found extensive anomalous gold in altered andesite, diorite and feldspar porphyry (values in the low 10s to 100s of ppb, maximum 24,854 ppb over 1 metre in a quartz-sulphide vein). In 1996, Orvana Minerals conducted geologic mapping, rock, soil and moss mat sampling, and a ground magnetic and VLF-EM survey.

The most recent work done on the property prior to Emgold's option was in 1997 by Orvana Minerals. The Craigtown Creek grid area was extended and covered by soil geochemistry and geological mapping. Also road construction to the ridge between the south and main forks of Craigtown creek was completed in order to access drill target areas defined by previous work.

5) WORK DONE BY EMGOLD MINING CORPORATION IN 2001

In 2001, Emgold Mining Corporation conducted soil geochemical surveys in five grid areas – the Arrow, Po, North and South Craigtown and Quartz Stockwork Grids. The grid locations can be seen on Figure 2. Fieldwork was carried out between July 22 and October 31, 2001 by a five person crew working out of the town of Salmo. Fieldwork was supervised by the author.

ARROW GRID

During 2001, a small grid was centred over the historic (1940s) Arrow Tungsten workings. Six grid lines of 500 metres length were put in at 100 metre spacings with samples collected along the grid lines at 25 metres stations.

PO GRID

The PO Grid covers mapped areas of mid Jurassic Silver King intrusive on the east and west sides of Highway 6. 11 grid lines spaced 200 metres apart were sampled at 50 metres stations where the underlying rock was believed to be the intrusive.

NORTH AND SOUTH CRAIGTOWN GRIDS

Prior work, in the 1990s, shows good gold soil geochemical anomalies in the north and south Craigtown Creek areas (formerly called the Minnova North and South anomalies). In 2001, Emgold extended these two grid areas. The North Craigtown Grid consists of five 100 metre spaced grid lines with sample stations at 25 metres along the lines. This grid was designed to expand and close off previously defined gold soil geochemical anomalies located to the north.

The South Craigtown Grid consists of six 200 metre spaced lines with samples collected at 25 metres stations along these lines. This grid was designed to expand the gold soil geochemical anomalies located to the west of this grid, and to cover previously defined induced polarization chargeability highs.

QUARTZ STOCKWORK GRID

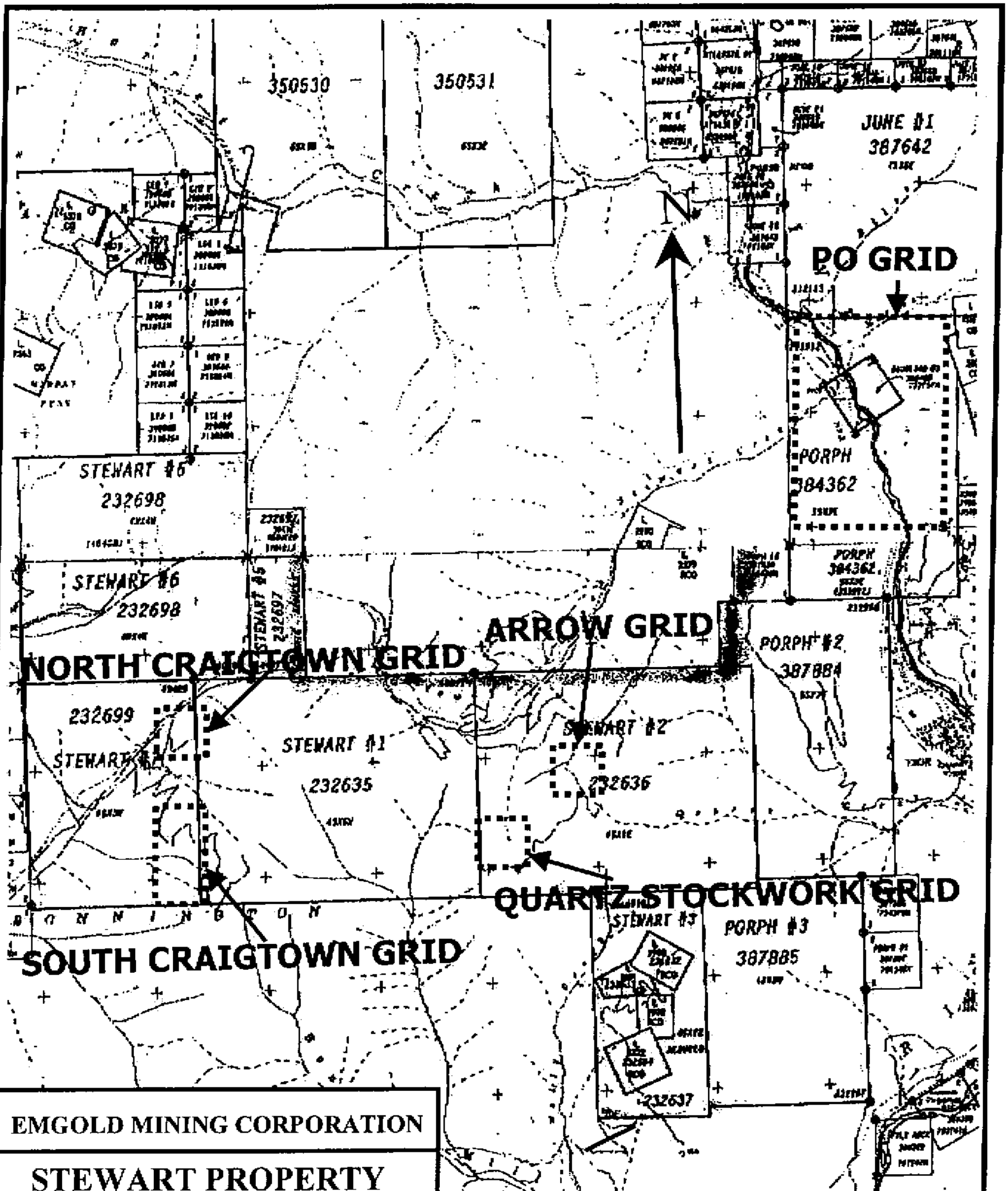
The Quartz Stockwork grid was put in over an area with limited outcrop exposure of altered intrusive rock containing abundant parallel and crosscutting quartz stockwork veinlets. Seven grid lines were put in at 100 metre spacings and samples were collected at 25 metre intervals along the lines. Also six rock chip samples were collected from outcrops exhibiting good quartz stockworking.

6) CLAIM INFORMATION

The Stewart Property is located within the Nelson Mining Division and consists of nine modified grid and six two post claims to total 127 units (Figure 2). Claim information is listed in Table I.

TABLE I
CLAIM INFORMATION

Claim Name	Units	Record No.	Anniversary (Expiry) Date
PORPH	15	384362	March 7 (2004)
PORPH 2	15	387884	July 6 (2004)
PORPH 3	12	387885	July 4 (2004)
PORPH 4	1	387886	July 3 (2004)
PORPH 5	1	387887	July 3 (2004)
PORPH 6	1	387888	July 10 (2004)
FAIRVIEW L2903	1	234612	March 15 (2004)
FREE SILVER L2902	1	232633	April 18 (2005)
ROYAL L5322	1	232634	April 18 (2005)
STEWART 1	20	232635	April 28 (2004)
STEWART 2	20	232636	April 28 (2004)
STEWART 3	8	232637	May 8 (2004)
STEWART 5	3	232697	November 28 (2004)
STEWART 6	16	232698	November 28 (2004)
STEWART 7	12	232699	November 28 (2004)



EMGOLD MINING CORPORATION

STEWART PROPERTY

NTS: 082F/6W NELSON MINING DIVISION

CLAIM MAP

BY: LD
DATE: MAY 2002

FIGURE: 2

1:50,000 SCALE

7) GEOLOGY

Geology and mineralization of the Stewart Property is well described by Fredericks and Thomson (1998), and is summarized below:

REGIONAL GEOLOGY

The immediate region is underlain in the east by Paleozoic clastic and carbonate sedimentary rocks of the Kootenay Terrane, and in the west by Mesozoic volcanic rocks of the Quesnel Terrane. In this region, the stratigraphy of both the Kootenay and Quesnel Terranes have been folded and faulted along an east-west compressional axis. They are intruded by felsic volcanic rocks that range in age from Jurassic to Tertiary. Coeval dioritic intrusions are common in the mafic andesitic volcanic rocks of the Jurassic Rossland Group. These tend to be relatively small bodies. Extensive late Mesozoic intrusive activity produced the widely distributed Nelson Group of intrusives of granitic to dioritic compositions. Eocene age, typically potassic (monzonite) intrusive rocks of the Coryell Group are also widely distributed in the region. Young (Tertiary) dykes and sills of rhyolite and felsite are common, and some small, more mafic intrusives are present. Much older clastic sedimentary rocks of the Proterozoic Aldridge (Belt) Supergroup outcrop extensively to the east.

PROPERTY GEOLOGY

The Stewart Property is underlain by sedimentary and volcanic rocks of the Jurassic Rossland Group, and by intrusive rocks of various younger ages (Figure 3). The oldest rocks are of the Elise Formation, the volcanic component of the Rossland Group. The Archibald Formation, which is the basal unit of the Rossland Group and composed of fine clastic sediments, outcrops west of the Stewart Property. The volcanic rocks of the Elise Formation are basaltic to andesitic in composition, tend to porphyritic flows, breccias, pyroclastics and subvolcanic intrusives. A fairly significant component of this formation includes fine-grained, equigranular to porphyritic/aphanitic diorite/andesite. Phenocrysts of feldspar, augite and hornblende are common in some of the units.

Overlying the Elise Formation is the Hall Formation (also Jurassic Rossland Group). These rocks are mostly argillite, siltstone, fine-grained sandstone and minor conglomerate. They are rarely limy, but are commonly siliceous. Compositionally, the rocks are very heterolithic, with a variety of clasts, including a high percentage of volcanic fragments. The Elise and Hall Formations are folded into a broad north-south trending syncline (Hall Creek Syncline) that runs through the property and extends both north and south over a 20 kilometre strike length. This north-south structural feature is the strongest one on the property.

A variety of intrusive rock types and ages have intruded the older rocks. These belong to three major groups. The older group consists of coeval diorite intrusives in the andesite pile of the Elise Formation. These tend to be fine to medium-grained, equigranular and weakly porphyritic. They range from very weakly to moderately magnetic. They probably are not very large, occurring as dykes or sills a few metres thick. Flow lineation in feldspar or hornblende phenocrysts is seen near the intrusive contacts in drill core.

After Hoy and Dunne, 1998

1:100,000 SCALE

EMGOLD MINING CORPORATION

STEWART PROPERTY

NTS: 082F/6W NELSON MINING DIVISION

GEOLOGY MAP

BY: LD
DATE: MAY 2002 **FIGURE: 3**

LEGEND

Tr	Rhyolite dykes
mEc	Biotite monzonite
mJp	Granite
mJsk	Plagioclase porphyry
lJh	Argillite, siltstone
lJe	Mafic flows, pyroclastics, tuffs

N

The next set of intrusive rocks is the Cretaceous Nelson intrusive suite, mostly quartz monzonite on the property, but also monzonite, granite and diorite. These tend to be large, in places composite, intrusive masses outcropping most extensively in the northern portion of the property, in the Stewart and Craigtown Creek drainages. Smaller stocks occur in the western portion of the property. Rocks of these intrusives are generally medium-grained, equigranular to porphyritic. They seem to range from weakly to fairly strongly magnetic. Porphyry molybdenum mineralization on the property is thought to be related to these intrusives.

Younger intrusives of the Coryell Suite (Eocene or later?) are also monzonitic, but tend to be a little more quartz-poor and alkaline than the Nelson rocks. They are typically biotitic. They may be equigranular or porphyritic. They occur in both the east central and west central portions of the property. What are probably the youngest intrusives are rhyolite, latite and minor basalt sills/dykes that intrude the older Rossland rocks and both Nelson and Coryell intrusives. These cross-cutting intrusives are aphanitic to weakly porphyritic (rhyolite and latite may have quartz eyes), generally strike north-south and are widely scattered on the property. The rhyolite intrusives commonly have distinct flow banding near their contacts with the country rock.

The dominant structural grain on the property is north-south. The Rossland Group stratigraphy generally strikes north-south, as does the Hall Creek Syncline. Northwest and northeast faults and shear zones are known on the property; they appear to be significant controls to mineralization. The common young rhyolite dykes and sills also strike north-south and dip steeply. All of these features indicate that the deformation occurred within a stress regime with an east-west compressional axis that was probably long lasting and contemporaneous with accretion onto the North American continent.

CRAIGTOWN CREEK AREA GEOLOGY

Orvana conducted mapping in 1996 and 1997 along road cuts and stream drainages in the Craigtown Creek area. The following geological summary is from Fredericks and Thomson, 1998, and is reproduced below as this area contains important gold mineralization.

The Elise (Jurassic age Rossland Group) Formation volcanics underlie a large portion of the Craigtown Creek area, and hosts a significant part of the known mineralization. They strike generally north-south and dip moderately to steeply east. Lithologies of the Elise Formation are texturally highly variable. The rocks constitute essentially an andesitic volcanic pile, but include flows, clastics and intrusives. Colour varies from light to dark grey, green or almost black. Most of the rocks are either porphyritic/aphanitic andesite flows or tuffs. Feldspar, hornblende and augite phenocrysts are common. The tuffs vary from ashes to lapilli or even cobble tuffs. Rarely, bedding is visible in ashy beds. Dioritic, porphyritic coeval dykes and/or sills are also common. These commonly have flow lineations preserved in the phenocrysts, near the contacts with the country rock. Compositionally, rocks of the Elise Formation are seen to vary from andesite to gabbro. Some of the rocks are basalt, containing up to 25% dark green to black augite phenocrysts. In the western portion of the area, a narrow belt of fine-grained tuffaceous volcanics is exposed in road cuts. These rocks lie between the granite and diorite intrusives, and are hornfelsed. They possibly represent a small sliver of the Archibald Formation (rather than the Elise Formation), otherwise not represented in the area, caught between two intrusives. Alteration in the Elise Formation is widespread and commonly consists of a propylitic assemblage, with less common potassic, carbonate and silicification.

Overlying the Elise Formation on the east are argillite, siltstone and tuffaceous rocks of the Hall Formation. These rocks also strike north-south and dip steeply. They are dark grey, tan to black and thinly bedded. They nave not been identified as calcareous in the Craigtown Creek area although they are in other areas of the property. They are often graphitic. Mineralization of these rocks in the study area seems to be restricted to the contact aureole around the "West Moly Intrusion", which is mostly further east. This mineralization is limited to disseminated pyrite/pyrrhotite and minor small quartz-sulphide veins. Alteration in this aureole includes silicification and hornfels (possible potassium metasomatism or silica flooding).

In the western portion of the area a variety of intrusive rocks occur. These probably represent in part a lobe of Nelson (Cretaceous) granite, quartz monzonite and diorite and extend eastward from the Bonnington pluton up Craigtown Creek. The granite is light speckled grey, pink and tan, medium to coarse-grained and unaltered. The diorite is medium to dark grey, medium to fine-grained, and tends to be more mafic in the west. It is generally unaltered to weakly propylitically altered. The monzonite and quartz monzonite outcrop extensively in the western portion of the grid area. This rock is medium to dark grey, medium-grained and generally equigranular to weakly porphyritic. It tends to be more quartz-rich in the southern portion of its distribution. It is generally unaltered or only weakly propylitically altered, except near its contact with the country rocks, where propylitic alteration is stronger. This rock intrudes the volcanic rocks of the Elise Formation.

Small monzonitic feldspar porphyry intrusive plugs occur in the Craigtown Creek area. These rocks were originally thought to belong to the Nelson intrusive group (Cretaceous). However, Hoy and Dunne (1988) suggest that rocks similar to these, including the Silver King porphyry, may be synvolcanic. One of these porphyries outcrops east of the 1996 grid on Anomaly Ridge, where Cameco drilled four holes. Other bodies are certain to underlie other areas, and the float is very common. These rocks are porphyritic, with 10-30% feldspar phenocrysts ¼ to 1 cm long, set in fine-grained, tannish grey groundmass. In places, anhedral quartz eyes constitute a few modal percent. Petrographic study indicates that the feldspar crystals are plagioclase. They are cream coloured and euhedral. In places they demonstrate a flow lineation. Mafics are mostly hornblende and minor biotite, and constitute a minor portion of the mode. The rocks often contain disseminated pyrite and in places are cut by stockwork quartz veinlets.

Fine-grained, felsic monzonitic intrusives occur in several portions of the Craigtown Creek area. These rocks may be from the same magmatic event as the feldspar porphyry intrusive described above, as they are compositionally similar. These rocks are light tan or grey, with pinkish hue in places, and contain only minor mafic minerals (generally 5% biotite). In places, especially near the ridge crest, brecciation is strong in these rocks. These appear to be intrusive breccias and show several cross-cutting relations. They are altered and mineralized, and are associated with anomalous Au and Cu geochemistry in both soils and rocks. Several percent magnetite is a common component, both as fine to medium-grained disseminations and as stockwork veinlets, with or without quartz. Potassium feldspar and quartz veining and flooding are present in places. These rocks probably represent elongate intrusives, perhaps 100 metres wide by 400 metres long, which were emplaced along the contact between the Elise Formation and the body of medium-grained monzonite. The strong northwest elongation implies structural control.

Latite and quartz latite dykes and small plugs occur in the Craigtown Creek area. They are probably Tertiary in age; they intrude the Rossland Group and the diorite and mozonite intrusives. The dykes are only a few metres in width and have strikes that range from northwest to northeast with steep dips. They are usually not altered or mineralized. However, a small plug of a trachytic latite and quartz latite porphyry with quartz veinlet stockwork and anomalous Au (>1 g/t) outcrops in the area. This plug was intruded along the same northwest striking zone of weakness that parallels the contact between the monzonite intrusives and the volcanics.

Rhyolite dykes are common on the Stewart Property, and a few of these traverse the Craigtown Creek area. They are also probably Tertiary, as they intrude the Rossland Group and the diorite and monzonite intrusives. They generally strike north-south and dip near vertically. They are a few metres in thickness. Texturally, the rhyolite is aphanitic, with minor quartz eyes in places. They have been mapped and logged as tuffs, flows or intrusives by other workers. Based on flow lineations, and chilled lower and upper contacts as seen in core, we believe that they are later intrusives. They are little altered except for some minor late quartz-carbonate veinlets. Some of them contain disseminated pyrite; in fact some earlier workers concluded that they are the source of the Au soil geochemical anomalies at Craigtown Creek. In our experience, they contain very little Au except where accompanied by quartz veinlet stockwork and pyrite.

Minor lamprophyre or porphyritic basaltic dykes, sills, and small plugs are present in the area. They are dark grayish brown, unaltered, not magnetic, and aphanitic, with minor biotite phenocrysts in places. They have distinct chill margins along both contacts in core. They also intrude the Rossland Group and the diorite and monzonite intrusives. They are probably late and unrelated to mineralization.

MINERALIZATION

The following mineralization summary is taken from Fredericks and Thomson (1998).

Mineralization on the property is widespread and varied. Included are porphyry Mo (and Cu?) with high grade breccia (Stewart Moly), contact/skarn related Mo and W (Arrow Tungsten), porphyry stockwork Au/Cu (Craigtown Creek), stratabound sediment hosted Au-rich sulphide (replacement manto or exhalative, i.e. Arlington Mine, Gold Hill?), quartz-pyrite-arsenopyrite stockwork in sediments (Trixi V), sediment hosted Ag-Zn-Pb

(Free Silver), and quartz-pyrite veins with gold (Craigtown Creek). Additionally, disseminated pyrite is common in several rock types, including andesite, argillite rhyolite and diorite/monzonite intrusives.

In the Craigtown Creek area, six types of mineralization are known. These include: 1) disseminated and fracture filling pyrite and/or pyrrhotite, +/- chalcopyrite, 2) quartz-magnetite veinlets, 3) quartz veinlet stockwork, 4) pyrite veinlets, 5) quartz-carbonate veins, and 6) quartz-sulphide veins. The first four types are associated with potentially economic, bulk tonnage style gold and copper mineralization. The last type could be associated with the same system that produced the former mineralization types, but is a distinctly different target type that also has economic potential.

Pyrite and pyrrhotite as disseminated grains and fracture fillings is common in the Craigtown Creek area. This type of mineralization is observed in all of the rock types mapped in the area, with the exception of the granite intrusive and basalt dykes. Traces of chalcopyrite are present in places with mineralization, where it occurs in intrusive or volcanic rocks, usually in association with shearing, brecciation or quartz veinlets. Propylitically altered quartz monzonite and diorite generally has only 0.5 to 2% sulphide. Andesite typically has more sulphide; 2-3% in propylitic rocks and 5-10% in silicified rocks, in relative proportion to the amount of alteration. Potassically altered intrusive and volcanic rocks have less sulphide, generally in the 0.5 to 4% range. This type of sulphide is also very common in feldspar porphyry. In one area of the grid, disseminated and fracture-filling pyrite and pyrrhotite in andesite tuff consistently yield 1-2 g/t gold in rock samples.

Quartz-magnetite veinlets are common in the north-northwest trending contact zone between the felsic monzonite intrusives and the Elise volcanics. This zone has strongly anomalous Au and Cu in soils. The host rocks are usually the intrusives and less commonly the volcanics. They are very rarely exposed in outcrop, mostly being seen in float or talus. The veinlets range from <1mm to 5mm in thickness, constitute 2-20% of the rocks and in places constitute a stockwork. Two or three stages of veining are visible in some hand samples; at least one stage is quartz only. Malachite stains are present in places, though the rocks rarely contain sulphide. Where sampled on the surface, rocks containing this type of mineralization contain anomalous Au (100 to 300 ppb range) and Cu (200 to 500ppm range).

Quartz and quartz-pyrite veinlet stockwork was observed in feldspar porphyry float in several places, and in the small latite plug mapped in the southern portion of the northwest striking zone of alteration and anomalous geochemistry that bisects the central portion of the grid. The rocks hosting this stockwork generally are moderately silicified, and contain several percent disseminated pyrite. Pyrite may also have been a component of the veinlets in some samples, but has been oxidized to limonite. This mineralization represents the potential for discovery of a large tonnage Au deposit, as several samples have returned Au values >1 g/t. This mineralization may represent more than one stage, as some rock samples contain high Au and low Cu; others have high Cu with high Au.

Pyrite veinlets in mafic andesite-basalt contain highly anomalous Au values in the central portion of Minnova's southern grid, east of Craigtown Creek. Dark green to black augite porphyritic mafic andesite or basalt is exposed in a few small outcrops, subcrop and float. Petrographic study indicates that this rock is propylitically altered and fragmental. It typically contains a few percent disseminated pyrite. In a couple of small outcrops, vague pyrite veinlets and clots are present. These vague veinlets have northeast orientations. Samples of this material have run in the 8 to10 g/t Au range.

Quartz-carbonate veinlets are present in both the Bonnington Pluton monzonite-diorite intrusive rocks and the Elise volcanics. They seem to occur in sheared, weakly altered (propylitic) outcrops. Shear directions are either northeast or north-south, with near vertical dips. Minor amounts of pyrite and or magnetite are present in the host rocks. Samples of these rocks have weakly anomalous Au and Cu.

Quartz-calcite-sulphide veins occurring in Elise volcanic rocks were intersected in one of the 1994 Cameco drill holes. They range from 10-30 cm wide and contain mostly white quartz and calcite, with 10-30% sulphide (pyrite, pyrrhotite and minor chalcopyrite). One of these veins contains 24,854 ppb Au. They appear to have high enough grade potential to be considered as targets, even in an underground mining situation. They are not known to outcrop anywhere. It is possible that the northeast striking Au in soil anomalies located on the grid north of Craigtown Creek are related to this type of mineralization. These anomalies are fairly narrow and linear appearing to be derived of relatively narrow veins or structures. Veins like this have been demonstrated to occur around porphyry type mineral systems in other important mining camps in British Columbia.

ALTERATION

The following alteration summary is taken from Fredericks and Thomson (1998).

Various types of alteration are known on the Stewart Property. In the area of the porphyry molybdenum occurrences phyllic and potassic alterations are reported by earlier workers. Silicification is common in various rock types. Propylitic alteration of intrusive and volcanic rocks is widespread on the property. In the Craigtown Creek area, the focus of work in 1996 and 1997, alteration types observed include propylitic, silicification, carbonate, potassic and skarn.

In the Craigtown Creek area propylitic alteration is common in andesitic volcanic rocks of the Elise Formation. Patchy, pervasive epidote and chlorite tint the rocks green. Fractures in the Elise volcanics have fillings, coatings or selvages of these minerals. Intrusive rocks, including monzonite and diorite, also commonly display pervasive to fracture-controlled propylitic alteration, where mafic crystals have altered to chlorite and/or epidote. This alteration is not as ubiquitous in the intrusive as it is in the volcanic rocks. The propylitic alteration may be related to the margins of the Bonnington intrusive rocks that invade from the west, and the later fine-grained monzonite plugs that intrude the Elise/Bonnington contacts.

Silicification is intense within the Elise Formation andesite near Craigtown Creek. These rocks typically have a mottled, bleached colouration. Silicification is pervasive, and mafic minerals are entirely chloritized. The silicification is usually accompanied by disseminated pyrite or pyrrhotite. It is also coincident with anomalous soil and rock geochemistry (Au, Cu, As) in places, and therefore is assumed to be a function of the mineralization system. On the surface, these silicifed rocks tend for form small, iron-stained ridges and knobs with sparse vegetation. They appear to be associated primarily with northwest structures, also possibly intrusive contacts and northeast structures. On the ridge crest, silicified rocks appear to extend 100 metres east of the saddle where several northwest structures are mapped. This is also within 100 metres of an intrusive contact where potassic alteration is present.

Carbonate alteration is present in places in the andesite of the Elise Formation. This alteration can be either pervasive or veinlet/fracture controlled. Where pervasive, it tends to be apparent only when the rocks are subjected to HCl acid, or with petrography. Petrographic study indicates that most of the carbonate is ferroan dolomite and is generally a late alteration product. A few outcrops were located containing small veinlets of calcite, commonly associated with north-south or northeast shearing. In the north Minnova grid area, a northeast trending zone of carbonate alteration, bleaching and pervasive hematite/limonite traverses the hillside just downhill and east of the Cameco drill holes. This zone is approximately 20 metres wide.

Potassic alteration is present in places in brecciated and veined fine-grained felsic monzonite intrusive rocks along the Bonnington Pluton – Elise Formation contact. This alteration is fairly weak, and consists of pinkish to grayish flooding and veinlets of potassium feldspar. Quartz +/- magnetite veinlets are commonly associated with this alteration.

Skarn alteration was observed in two locations in the Craigtown Creek area. A small outcrop of green calc-silicate skarn was found just off the western end of the 1996 grid. This rock contains green pyroxene, brownish garnet, and black amphibole (+/- chlorite). Similar skarn was found in float near the east end of the old road running up the north side of the North Fork of Craigtown Creek. The protolith is probably andesitic fragmental volcanic rock.

ROCK SAMPLING TECHNIQUES

Chip samples were taken as continuous samples collected perpendicular to bedding or mineralizing structures wherever identifiable and consist of numerous 2 to 3 centimetre rock chips to total about 10 kilograms. Grab samples consist of 2 or 3 fist size pieces of rock representing a certain rock or mineralization type. All sample sites were marked with fluorescent flagging marked with the sample number.

Samples were placed in poly bags labelled with the corresponding sample number and were shipped to ACME Labs Ltd. in Vancouver for analyses. In the laboratory, samples were crushed to minus 200 mesh and fire assayed for gold, plus geochemically analyzed for 30 additional elements by the ICP method. One sample was selected to be assayed for tungsten by sodium fusion.

ROCK SAMPLE RESULTS

Certificates of Analysis for the rock sample results can be found in Appendix I. Table II summarizes the results from the surface rock grab and chip sampling program.

TABLE II
ROCK SAMPLE RESULTS

SAMPLE #	DESCRIPTION	Au (g/t)	Mo (ppm)	Zn (ppm)	W (ppm)
STEWART MOLY	dump grab	0.04	10350	<1	4
ARROW W	dump grab	0.01	123	40245	12600
ST4+05S 3+00E	chip	0.01	238	14	11
ST4+05S 4+30E	chip	0.01	36	23	4
ST4+10S 6+60E	chip	0.01	95	10	5
ST7+00S 2+50E	chip	0.01	4	33	13
ST7+90S 6+40E	chip	0.01	4	16	5
ST8+00S 4+30E	chip	0.01	3	49	5

The two grab samples in the above table were collected from the old Stewart Moly workings and from a partially collapsed trench at the Arrow Tungsten workings. The six chip samples were collected from the Quartz Stockwork grid during the course of soil sampling in areas where intense quartz stockworking in the intrusive rock was observed. The sample number coordinates for these samples correspond with the grid location from which they were taken.

The most significant results from these few rock samples is from the one collected from the Arrow Tungsten workings that returned 4.02% zinc and 1.26% tungsten. The sample collected from the Stewart Moly workings returned expected high grade molybdenum of 1.03% Mo. None of the samples taken from the Quartz Stockwork grid returned assays of any significance.

8) SOIL GEOCHEMISTRY

During the 2001 exploration program, a total of 608 soil samples were collected from five grid areas. These soil grids are named the Arrow, Po, Quartz Stockwork and the North and South Craigtown Grids. On the Po and South Craigtown Grids soil lines were put in at 200 metre spacings with samples collected at 50 metre stations on the Po Grid and at 25 metre stations on the South Craigtown Grid. On the Arrow, North Craigtown and Quartz Stockwork Grids lines were put in at 100 metre spacings and samples collected at 25 metre intervals along the lines.

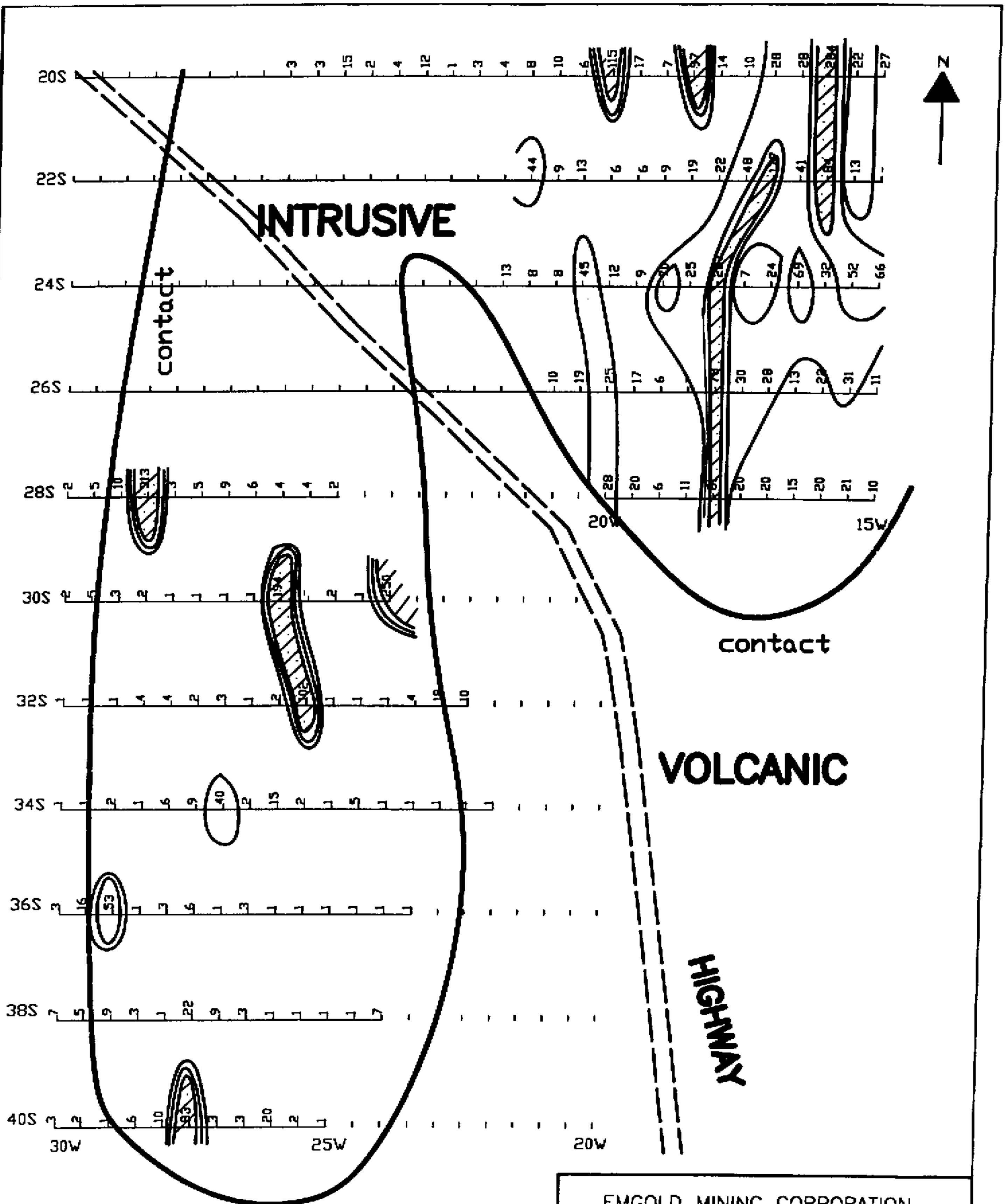
Samples were taken from the 'B' soil horizon whenever possible, and were collected using a mattock or shovel. Samples site were labelled with fluorescent flagging with the station number recorded on it, and soil was placed in correspondingly labelled Kraft soil bags. All soil samples were shipped to ACME Labs Ltd. in Vancouver for analyses. In the laboratory, samples were dried, sieved to –80 mesh and the fine fraction analyzed for gold by the wet geochemistry method and for 30 elements by the ICP method.

ACME Labs Ltd. Certificates of Analyses for the soil sample results can be seen in Appendix II. Figure 2 shows the location of the grids and Figures 4 to 15 show selected geochemical results for the various grids.

The Po Grid covers the southwestern extension of the mapped mid Jurassic Silver King intrusive unit which is known to contain porphyry style gold mineralization. The grid lies on either side of Highway 6 and the gold soil results are plotted on Figure 4. Scattered gold values can be seen on the west side of Highway 6, many of which represent single station anomalies. The highest gold value in this area is 313 ppb gold located at L28S, 28+50W. The northeast portion of the grid, on the east side of Highway 6 has a larger area of elevated gold values which appears to have a rough north-south trend. The best gold value in this area is 284 ppb located at L20S, 16+00W. This grid requires infill soil sampling of the anomalous areas at 100 metre spaced lines with 25 metre spaced stations. Geological mapping and chip sampling of outcrops in these anomalous areas is also recommended.

The North Craigtown Grid consists of five 100 metre spaced lines that extend to the southeast from the pre-existing Minnova north soil grid and was designed to follow the gold geochemistry anomaly found on that grid. Gold and zinc values for the North Craigtown Grid are plotted on Figure 5. Elevated gold values are predominantly confined to the northwest corner of the grid where the highest value of 84 ppb gold is located at L0S, 0+50E. Zinc values are fairly consistent throughout the grid area, with two stations returning greater than 300 ppm zinc at L2S, 3+50E and L3S, 1+50E. No follow up work in this grid area is recommended.

The South Craigtown Grid lies 600 metres south of the North Craigtown Grid and is an eastern extension of the pre-existing South Minnova soil grid. This grid covers an area of high geophysical (IP chargeability) responses. Gold, zinc and molybdenum soil values are plotted on Figures 6 to 8. All three soil maps show linear north-south trending anomalies running for the 1000 metre length of the grid. The gold anomaly is one to three stations in width and trends roughly along 3E. The highest gold value is 43 ppb gold located at L12S, 2+75E. The zinc soil anomaly roughly parallels the gold anomaly but widens out toward the east for the northern 400 metres of the grid. The best zinc soil value is 681 ppm located on L10S, 3+50E. The molybdenum soil values also roughly parallel the gold anomaly, but there appears to be a second, stronger anomaly trending along the eastern margin of the grid area. The best molybdenum value is 89 ppm located on L16S, 3+50E. Follow up work recommended for this area will consist of detailed mapping and outcrop sampling along the coincident gold, zinc and molybdenum trend running through the grid near 3E. If results of the surface mapping and sampling program are encouraging, excavator trenching will be done over the best target areas.



SCALE: 1:10,000

Au in soils (ppb)
25 ppb contours

>75 ppb Au

EMGOLD MINING CORPORATION

STEWART PROPERTY

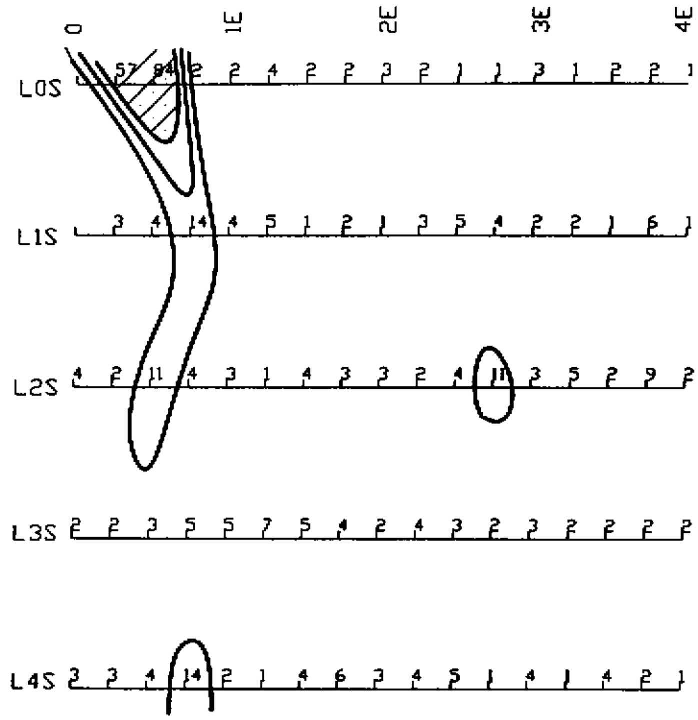
NTS: 082F/6W NELSON MINING DIVISION

PO GRID

GOLD IN SOILS

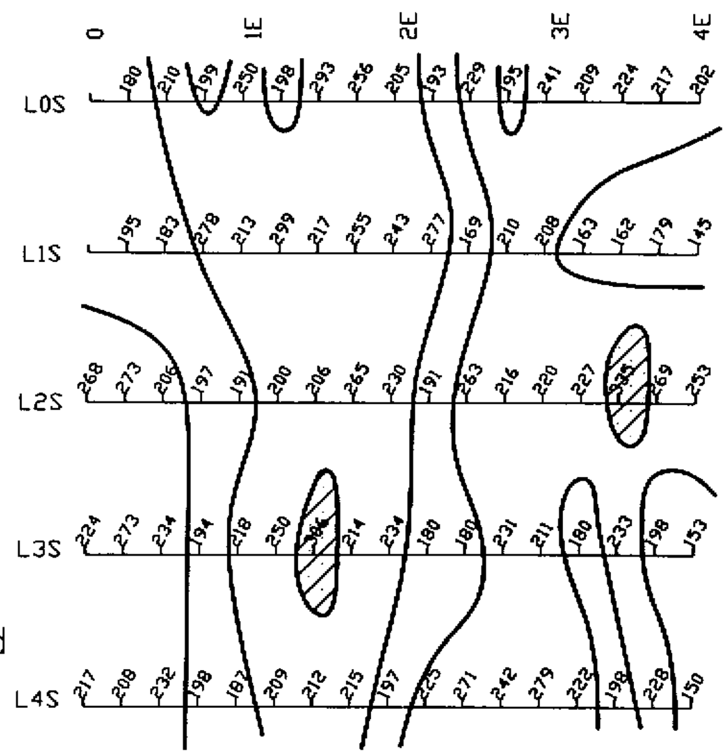
BY: PG
DATE: APRIL 2002

FIGURE 4



Au in soils (ppb)

>10 ppb contoured



Zn in soils (ppm)

>100 ppm contoured

SCALE: 1:5000

EMGOLD MINING CORPORATION

STEWART PROPERTY

NTS: 082F/6W NELSON MINING DIVISION

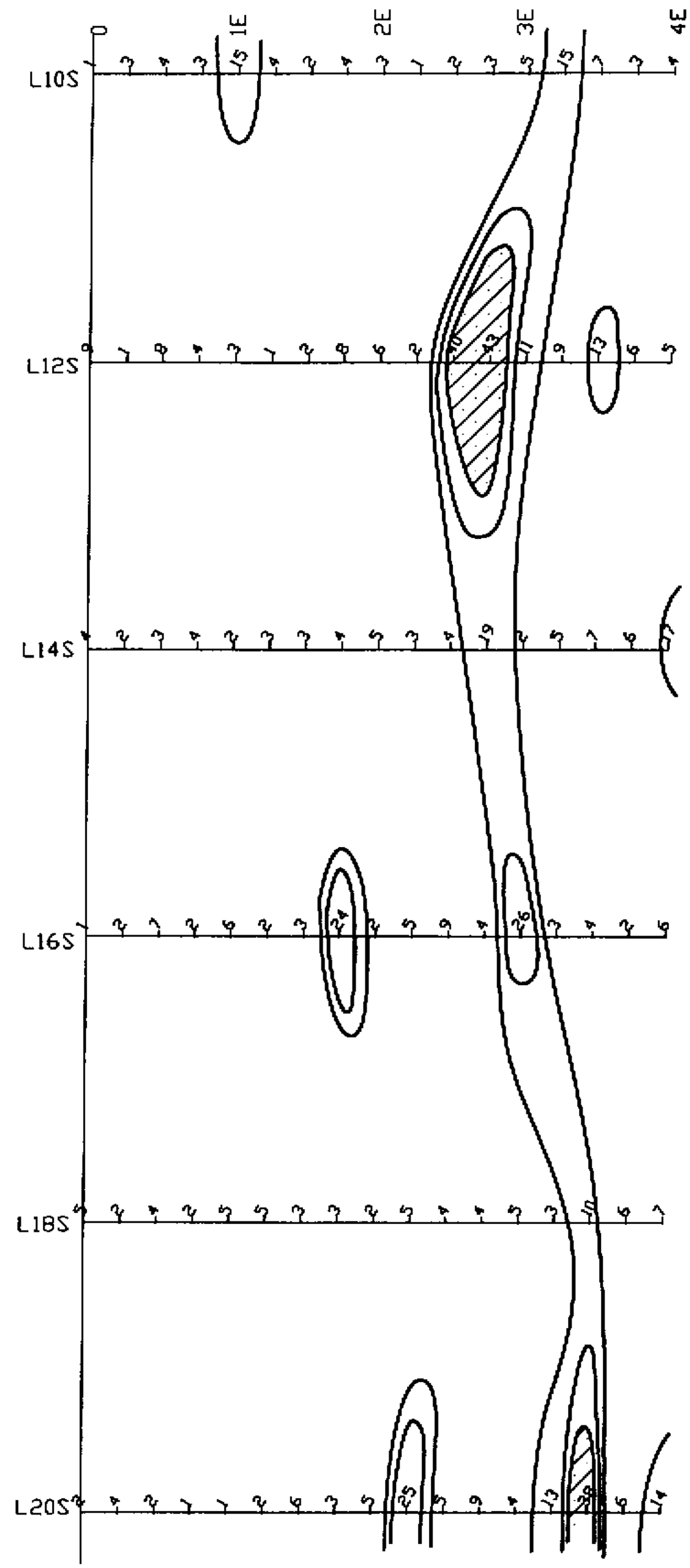
NORTH CRAIGTOWN GRID

GOLD AND ZINC IN SOILS

BY: LD

DATE: MAY 2002

FIGURE 5



SCALE: 1:5000

Au in soils (ppb)

10 ppb contours

>30 ppb gold

EMGOLD MINING CORPORATION

STEWART PROPERTY

NTS: 082F/6W NELSON MINING DIVISION

SOUTH CRAIGTOWN GRID

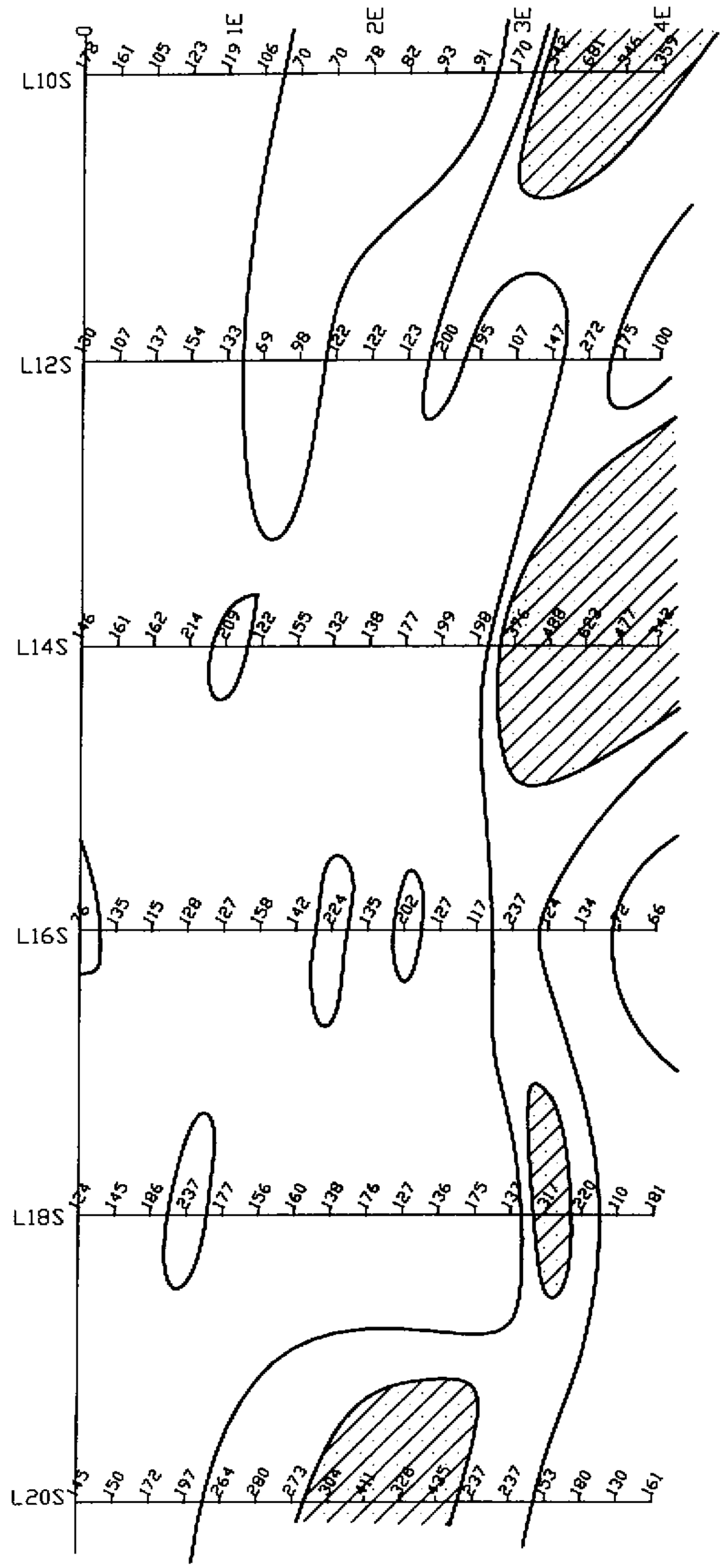
GOLD IN SOILS

BY: LD
DATE: MAY 2002

FIGURE 6

N

SCALE: 1:5000



Zn in soils (ppm)

100 ppm contours

>300 ppm zinc

EMGOLD MINING CORPORATION

STEWART PROPERTY

NTS: 082F/6W NELSON MINING DIVISION

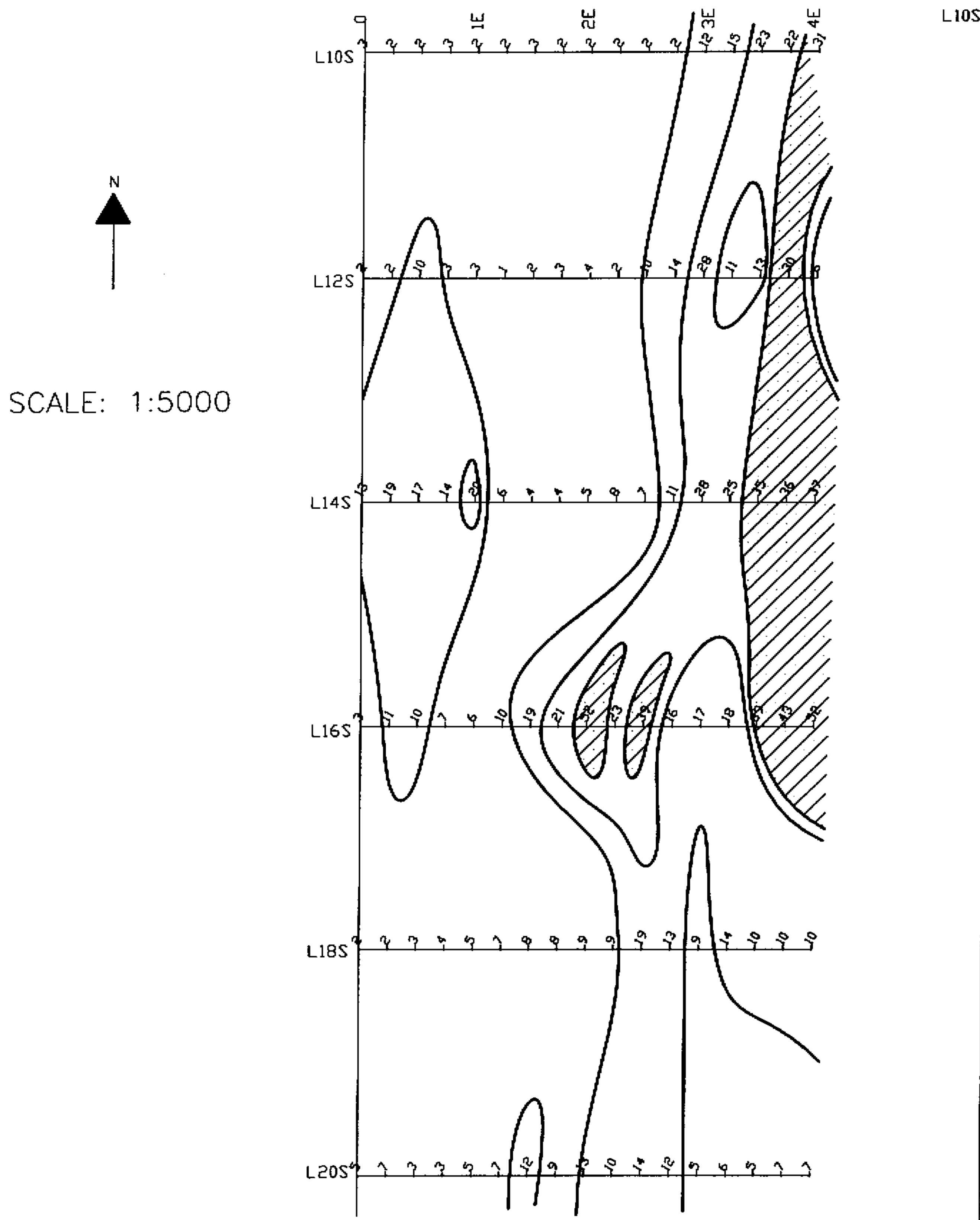
SOUTH CRAIGTOWN GRID

ZINC IN SOILS

BY: LD

DATE: MAY 2002

FIGURE 7



Mo in soils (ppm)

10 ppm contours

>30 ppm molybdenum

EMGOLD MINING CORPORATION

STEWART PROPERTY

NTS: 082F/6W NELSON MINING DIVISION

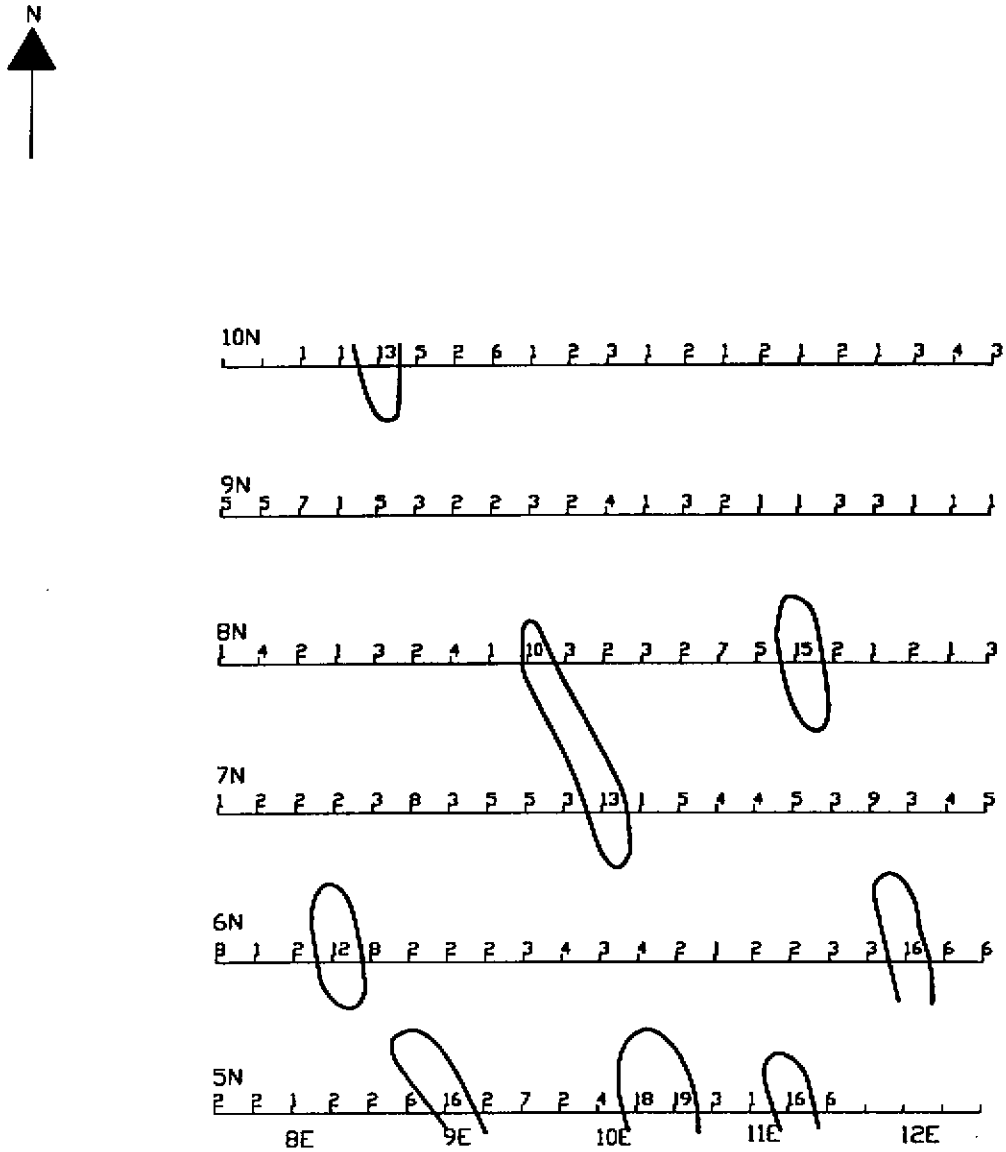
SOUTH CRAIGTOWN GRID

MOLYBDENUM IN SOILS

BY: LD

DATE: MAY 2002

FIGURE 8



SCALE: 1:5000

Au in soils (ppb)

>10 ppb contoured

EMGOLD MINING CORPORATION

STEWART PROPERTY

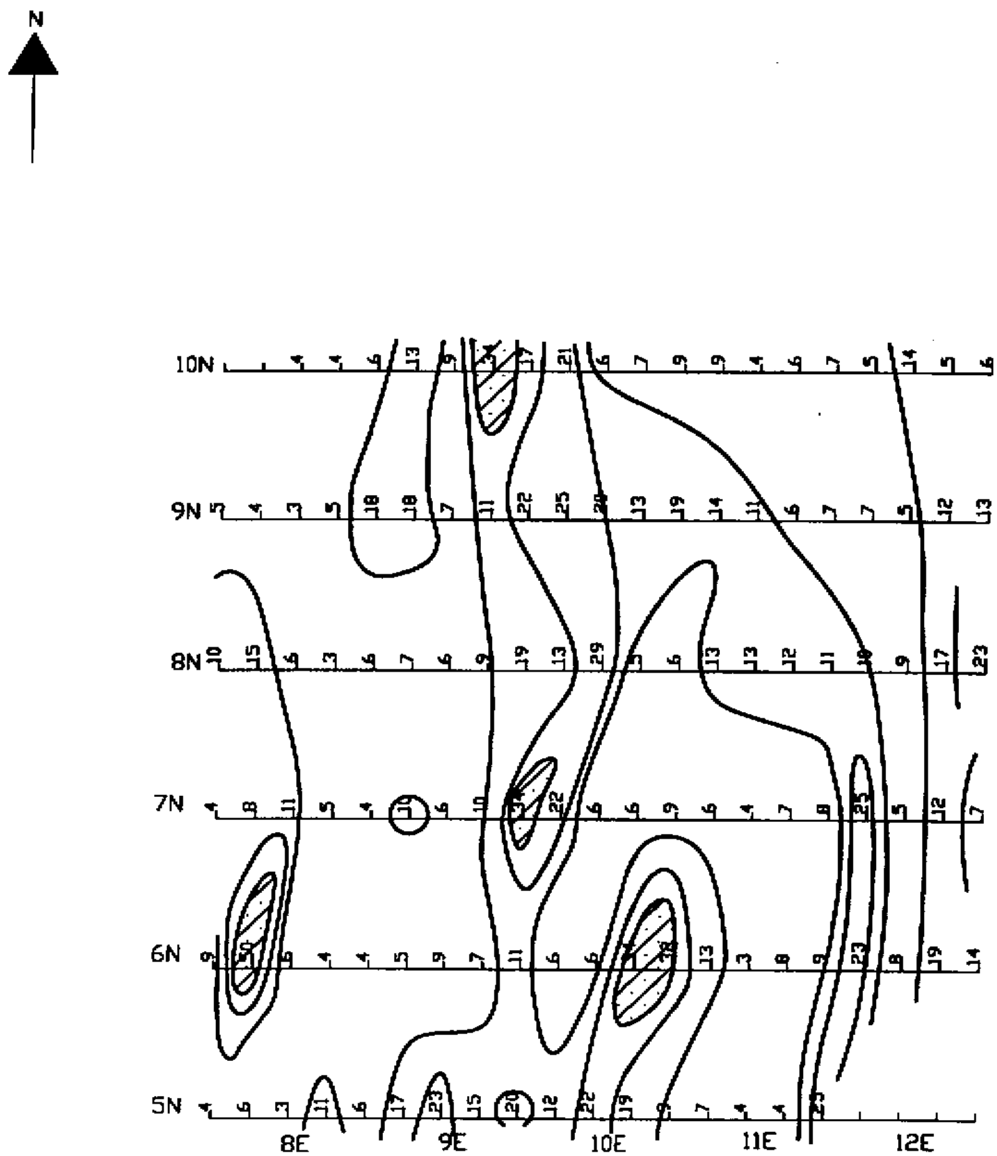
NTS: 082F/6W NELSON MINING DIVISION

ARROW GRID

GOLD IN SOILS

BY: PG
DATE: APRIL 2002

FIGURE 9



SCALE: 1:5000

Mo in soils (ppm)

10 ppm contours

>30 ppm Mo

EMGOLD MINING CORPORATION

STEWART PROPERTY

NTS: 082F/6W NELSON MINING DIVISION

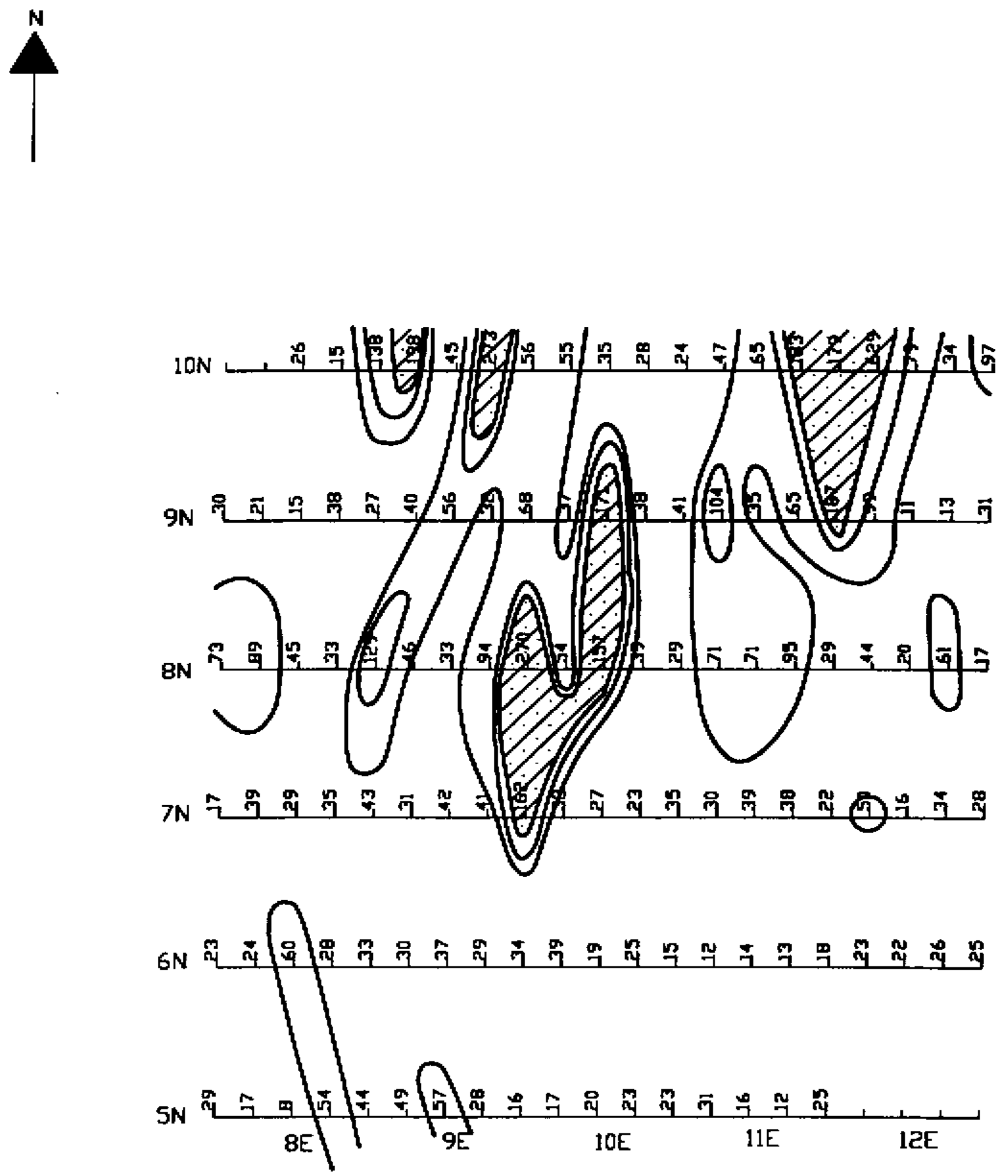
ARROW GRID

MOLYBDENUM IN SOILS

BY: PG

DATE: APRIL 2002

FIGURE 10



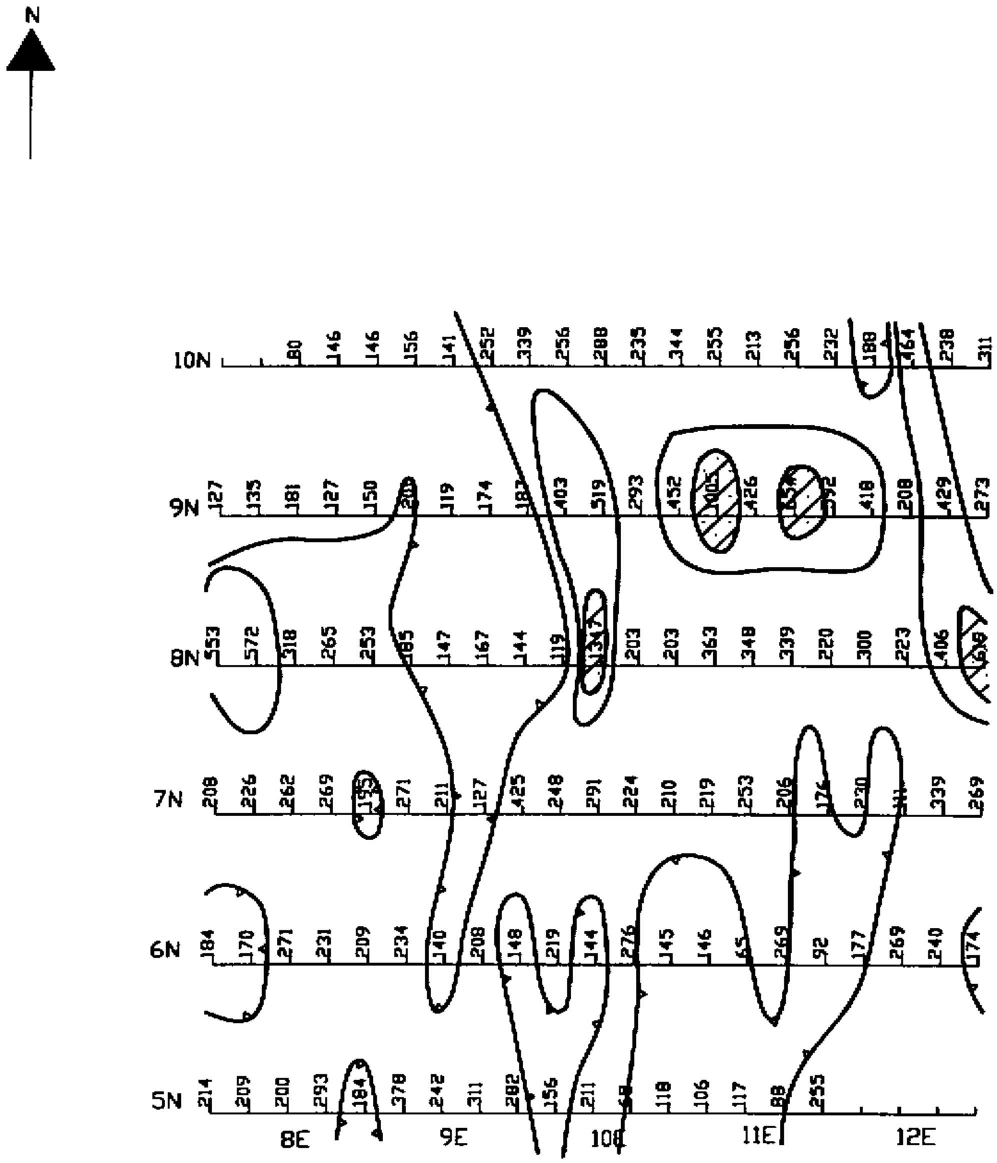
SCALE: 1:5000

As in soils (ppm)

50 ppm contoured

>150 ppm As

EMGOLD MINING CORPORATION
STEWART PROPERTY NTS: 082F/6W NELSON MINING DIVISION
ARROW GRID ARSENIC IN SOILS BY: PG DATE: APRIL 2002 FIGURE 11



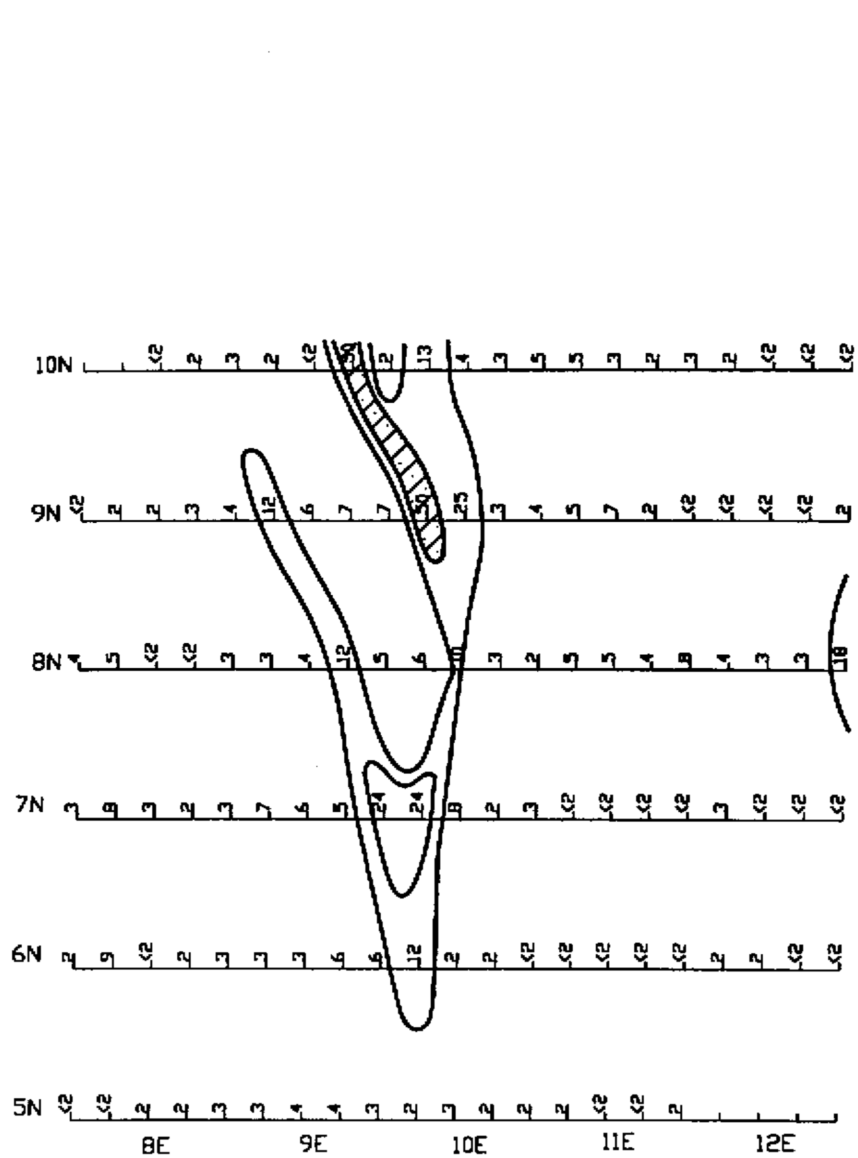
SCALE: 1:5000

Zn in soils (ppm)

200 ppm contours

>600 ppm Zn

EMGOLD MINING CORPORATION
STEWART PROPERTY NTS: 082F/6W NELSON MINING DIVISION
ARROW GRID ZINC IN SOILS BY: PG DATE: APRIL 2002 FIGURE 12



SCALE: 1:5000

W in soils (ppm)

10 ppm contours

>30 ppm W

EMGOLD MINING CORPORATION

STEWART PROPERTY

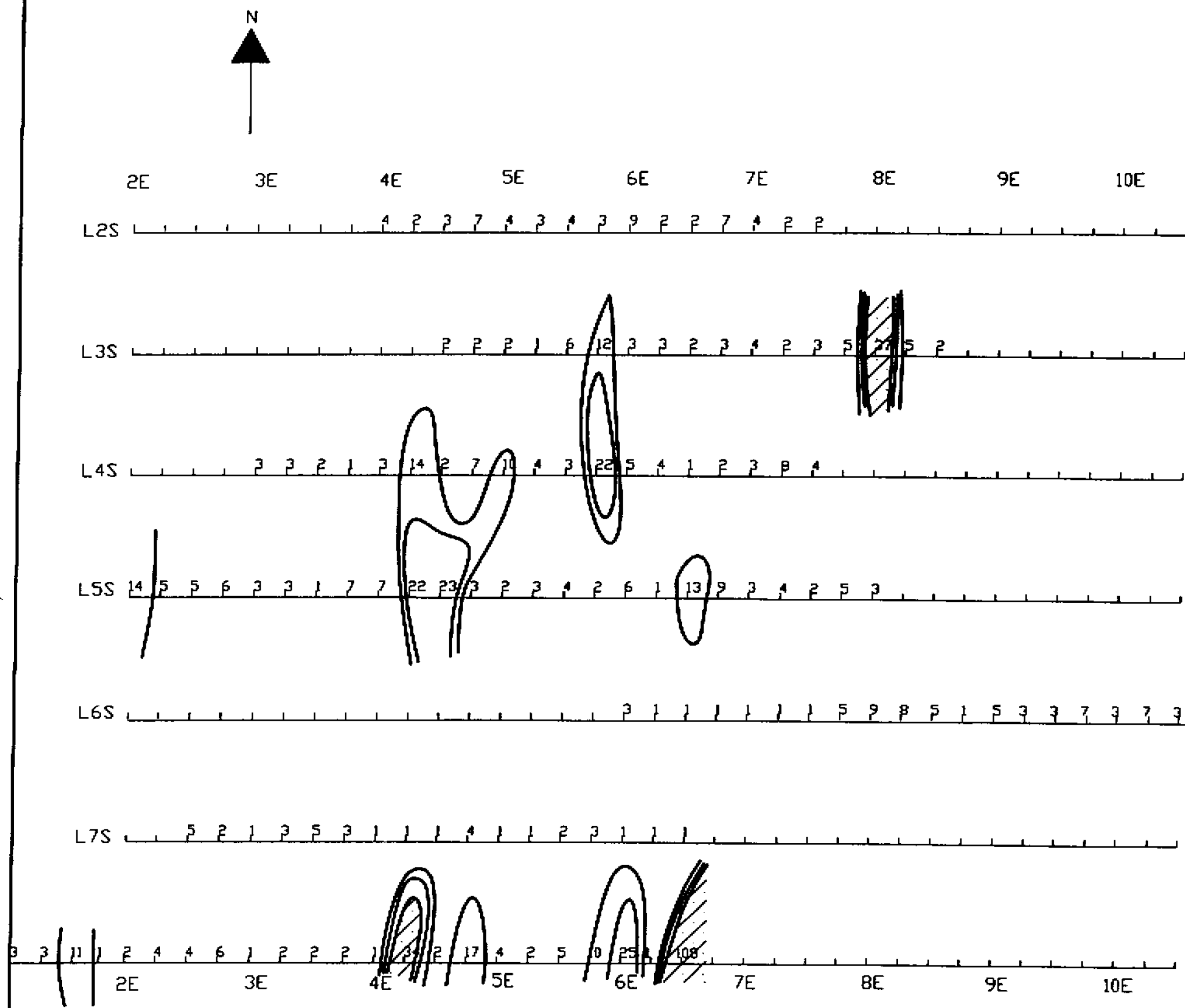
NTS: 082F/6W NELSON MINING DIVISION

ARROW GRID

TUNGSTEN IN SOILS

BY: PG
DATE: APRIL 2002

FIGURE 13



SCALE: 1:5000

Au in soils (ppb)

>10 ppb contoured

EMGOLD MINING CORPORATION

STEWART PROPERTY

NTS: 082F/6W NELSON MINING DIVISION

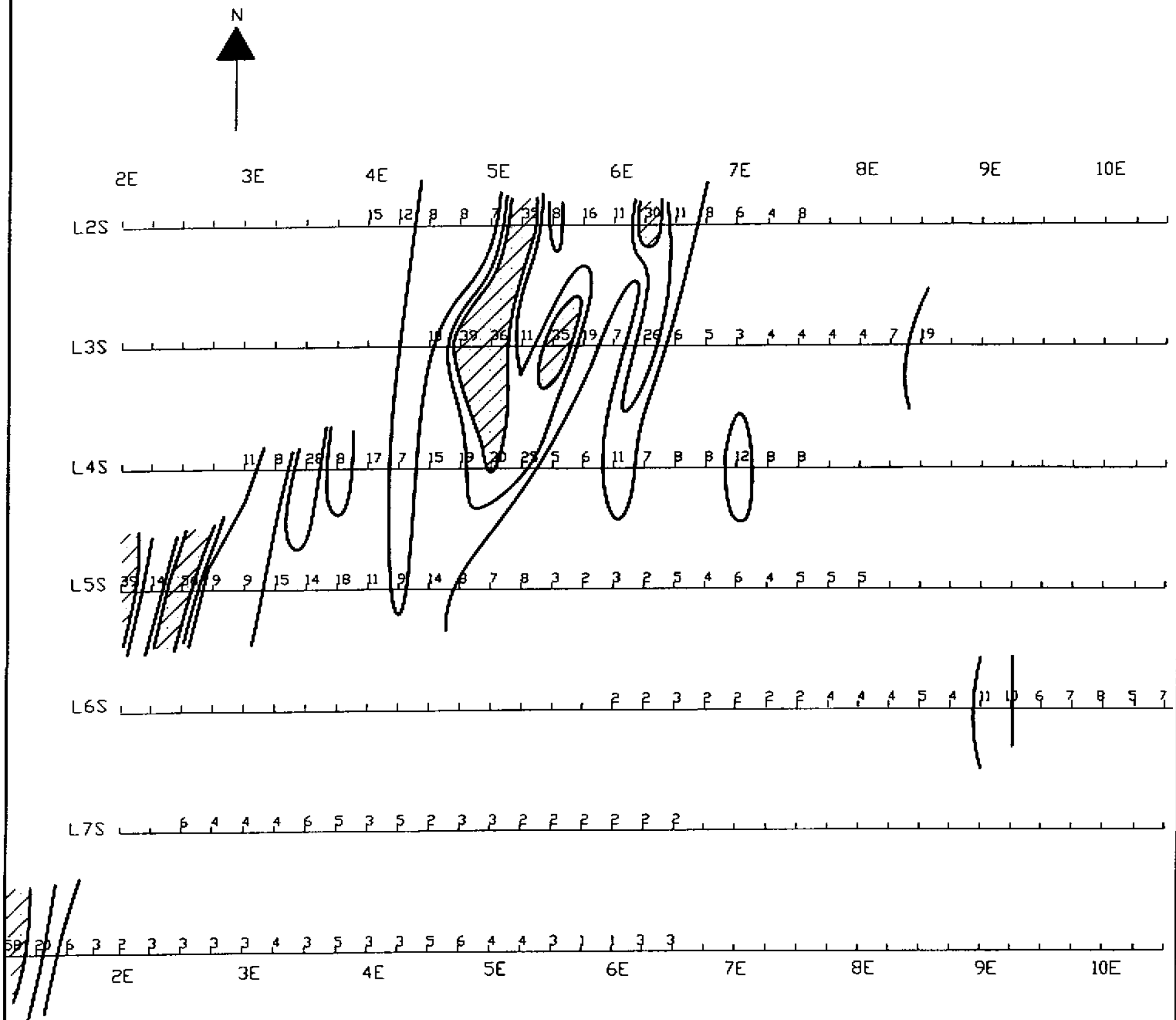
QUARTZ STOCKWORK GRID

GOLD IN SOILS

BY: LD

DATE: MAY 2002

FIGURE 14



SCALE: 1:5000

Mo in soils (ppm)

>10 ppm contoured

EMGOLD MINING CORPORATION

STEWART PROPERTY

NTS: 082F/6W NELSON MINING DIVISION

QUARTZ STOCKWORK GRID

MOLYBDENUM IN SOILS

BY: LD

DATE: MAY 2002

FIGURE 15

The Arrow Grid covers the historic Arrow Tungsten workings from the 1940s. Figures 9 through 13 show the gold, molybdenum, arsenic, zinc and tungsten soil geochemistry results for this grid. Gold values appear to be low and erratic with the highest value of 19 ppb gold occurring at L5N, 10+50E. Molybdenum shows a roughly linear anomalous area trending north-south through the center of the grid and smaller anomalous areas on either side of this main trend. The best molybdenum value of 50 ppm is located near the west side of the grid at L6N, 7+75E. Arsenic values are higher on the northern half of the grid area, with two main areas of concentrated highs – one near the center of the grid and one near the northeast corner. The highest arsenic value of 273 ppm is located at L10N, 9+25E. Zinc values are scattered, with some slightly higher values in the northeast quarter of the grid area. The highest zinc value of 1327 ppm occurs near the center of the grid, in the location of the old workings, at L8N, 10+00E. Tungsten is confined to the central portion of the grid area and lies directly above the trace of the known workings. The highest tungsten value of 50 ppm occurs at two stations L10N, 9+25E and L9N, 9+75E. Detailed mapping and rock chip sampling, followed by excavator trenching is recommended for the best anomalous areas on the Arrow Grid.

The Quartz Stockwork grid was put in over an area of low outcrop exposure, where the few exposed outcrops consist of intrusive rock with a high density of parallel and crosscutting quartz veinlets. On the Quartz Stockwork Grid, gold and molybdenum soil values have been plotted as Figures 14 and 15 respectively. Gold values are spotty and generally low. The highest gold soil value of 108 ppb gold occurs at the extreme southeast station on the grid at L8S, 6+50E. From the nature of the gold values it is recommended that the grid be extended to the south and east for an additional 300 metres in 2002. The molybdenum values trend across the grid area in a northeast-southwest direction. The highest molybdenum value of 58 ppm is found in the extreme southwest station on the grid at L8S, 1+00E.

9) CONCLUSIONS AND RECOMMENDATIONS

The Stewart Property lies within very prospective geology and hosts a variety of mineral occurrences. Previous work on the property defined zones of significant molybdenum and gold (+/- copper) mineralization. Emgold optioned the property in order to evaluate and expand the known gold mineralization and to test additional areas for gold, as many of the better molybdenum and tungsten anomalous areas were not historically tested for gold.

Work done by Emgold Mining Corporation in 2001 has led to the following conclusions and recommendations:

PO GRID

The Po Grid lies along the southern most mapped extent of mid Jurassic Silver King intrusive with lobes on either side of Highway 6. Silver King intrusive is known to host porphyry style gold mineralization on the Kena Property to the north. Several scattered gold soil geochemical anomalies were found on the west side of the grid, and a larger area of elevated gold soil values was found on the east side of the grid. Follow up work consisting of infill soil sampling and geological mapping accompanied by rock chip sampling is recommended to follow up these gold soil anomalies.

NORTH AND SOUTH CRAIGTOWN GRIDS

The North and South Craigtown grids were designed to expand and close off gold soil anomalies found by previous exploration work. The north grid was successful in limiting the extent of the gold soil anomaly that was found on the previous north Minnova grid. The south grid found an interesting linear soil anomaly for gold, zinc and molybdenum that runs for the 1000 metre length of the grid. The anomaly overlays an induced polarization chargeability anomaly found by previous property operators. Infill soil sampling, geological mapping and rock chip sampling is required to determine the source of this anomaly.

ARROW GRID

The Arrow grid was put in over historic tungsten workings in order to determine the limit of the tungsten mineralization and to test for other elements, most notably gold and zinc. Gold values are low and scattered, but good anomalous zones of zinc, arsenic and molybdenum trend throughout the grid. The tungsten soil anomaly appears to generally be confined to the area of known workings. A grab rock sample collected from one of the historic trenches returned very high zinc and tungsten values, and additional rock chip sampling is recommended in order to fully evaluate the potential of the historic workings.

QUARTZ STOCKWORK GRID

The Quartz Stockwork grid was put in over an area with outcrops of altered intrusive rock which contains abundant quartz stockworking. Scattered elevated gold values were found in soil samples throughout the grid, with the best anomalous area being in the extreme southeast corner of the grid. It is recommended to expand the soil grid to the south and east in order to better define this anomalous gold area. Several rock chip samples collected during the soil sampling program did not return any significant gold assay values.

OTHER AREAS

The regional geology map shows two sub-parallel belts of lower Jurassic Upper Elise Formation volcanic rocks trending through the Stewart Property. Small bodies of intrusive rocks occur throughout the volcanic belts and are known to be mineralized in this region. The westernmost belt of volcanics hosts the old Minnova north and south grids and our extensions to these grids, the North and South Craigtown Grids. This belt shows good gold soil geochemical response as has been discussed above.

The easternmost belt of these volcanic rocks has only been soil sampled in the most northerly extent of the claim holdings on the Po Grid and shows good gold soil geochemistry. Mapping of this belt of prospective volcanic rocks shows numerous associated intrusive rocks including Silver King Porphyry, Nelson intrusions (granite), Eocene mafic Coryell intrusives and Tertiary rhyolites. The volcanic belt trends south through the claims from the Po grid for 5 kilometres and it is recommended that the entire length of prospective rock units be soil sampled in 2002.

RECOMMENDED WORK PROGRAM

For 2002, an exploration program of detailed geological mapping and rock chip sampling, expanded soil geochemistry and excavator trenching is planned for the Stewart Property. This exploration program is budgeted at $40,000.00.

Respectfully submitted,

Linda Dandy, P.Geo.

10) REFERENCES

CARPENTER, T., and **GRANT, B.**, 1985; Stewart Project (10138) Report on Activities and Results from 1984: BC Ministry of Energy and Mines Assessment Report.

FREDERICKS, ROBERT, T., and **THOMSON, I.**, 1997; Report of 1996 Geological, Geochemical and Geophysical Exploration Program, Stewart Property, BC: BC Ministry of Energy and Mines Assessment Report.

FREDERICKS, ROBERT, T. and **THOMSON, I.**, 1998; Report of 1997 Geological, Geochemical, and Physical Work Program, Stewart Property, BC: BC Ministry of Energy and Mines Assessment Report.

HOY, T. and **ANDREW, K.**, 1989; Geology of the Nelson Map Area, Southeastern British Columbia: BC Ministry of Energy, Mines and Petroleum Resources, Open File 1989-11.

HOY, T. and **ANDREW, K.**, 1989; The Rossland Group, Nelson Map Area, Southeastern British Columbia: BC Ministry of Energy, Mines and Petroleum Resources, Geological Fieldwork, 1988, Paper 1989-1.

HUMPHREYS, N., 1992; Final Report on the Geology, Geochemistry and Trenching on the Denny Prospect, Cameco Corp.: BC Ministry of Energy and Mines Assessment Report #22829.

HUMPHREYS, N., 1993; Report on the Diamond Drilling on the Denny Prospect for Cameco Corp.: BC Ministry of Energy and Mines Assessment Report.

11) COST STATEMENT - 31 December 2001

GEOCHEMICAL SURVEY COST

SALARIES & WAGES: 5 pers., 30 mdays @ $214.33		$ 6,400.00
BENEFITS @ 20%		1,280.00
FOOD & ACCOMMODATION: 5 pers., 30 mdays @ $19.29		578.70
ASSAYS & ANALYSES – ACME LABS		
608 soils for Au & 32 element ICP @ $12.19	$7,409.87	
8 rocks for Au & 32 element ICP @ $19.34	154.68	
14 pulps for W @ $12.19	170.66	
	$7,735.21	7,735.21
SUPPLIES:		492.23
FUEL:		57.78
SHIPMENTS:		152.00
FIELD OFFICE:		250.00
4WD TRUCKS: 12 days @ $53.33		640.00
REPORT PREPARATION:		2,450.00
TOTAL GEOCHEMICAL SURVEY COST:		**$ 20,035.92**

12) QUALIFICATIONS

I, Linda Dandy, hereby certify that:

1. I am an independent Consulting Geologist with P&L Geological Services having an office at 3728 Ridgemont Road, Lac Le Jeune, British Columbia, V1S 1Y8.

2. I am a graduate of the University of British Columbia with the degree of Bachelor of Science in Geology (1981).

3. I am a member of the Association of Professional Engineers and Geoscientists of British Columbia (Registration No. 19236) and a Fellow of the Geological Association of Canada (Membership No. F5201).

4. I have practiced my profession in North America since 1981, having worked as an employee and consultant for Major Mining Corporations and Junior Resource Companies.

5. This report is based upon a personal examination of all available company and government reports pertinent to the subject property, and upon fieldwork undertaken on the property between July 22 and October 31, 2001.

Linda Dandy, P.Geo.
Consulting Geologist

May 7, 2002
Lac Le Jeune, B.C.

APPENDICES

APPENDIX I – ROCK CHIP SAMPLE RESULTS – CERTIFICATES OF ANALYSES

APPENDIX II – SOIL SAMPLE RESULTS – CERTIFICATES OF ANALYSES

APPENDIX I

ROCK CHIP SAMPLE RESULTS

CERTIFICATES OF ANALYSES

ACME ANALYT. L LABORATORIES LTD. 852 E. HASTINGS ST. VANC(ER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253 16
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Emgold Mining Corp. PROJECT ROZAN File # A102380

1400 - 570 Granville St., Vancouver BC V6C 3P1 Submitted by: Perry Grunenberg

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** gm/mt
STEWART MOLY	10350	32	16	<1	<.3	5	8	194	1.74	<2	<8	<2	8	28	<.2	<3	10	61	.15	.056	13	52	.26	59	.06	12	.46	.03	.17	4	.04
ARROW W	122	110	8	39185	<.3	23	20	3351	4.60	3	<8	<2	2	44	837.6	<3	<3	57	4.84	.060	3	33	.14	6	.01	5	.99	.01	.01	309	.01
RE ARROW W	123	113	3	40245	<.3	22	21	3450	4.74	<2	11	<2	2	46	864.2	<3	<3	59	5.21	.063	2	35	.14	5	.01	<3	1.02	.01	<.01	313	<.01
STANDARD C3	26	66	36	169	5.6	37	11	782	3.46	57	19	<2	21	28	23.7	15	24	79	.57	.090	19	165	.60	147	.10	24	1.84	.04	.16	20	-

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK R150 60C AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 26 2001 DATE REPORT MAILED: Aug 7/01 SIGNED BY C.L........ D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data ✓ FA ___

ACME ANALY AL LABORATORIES LTD. 852 E. HASTINGS ST. VAN(VER BC V6A 1R6 PHONE(604)253-3158 FAX(604)25)716
(ISO 9002 Accredited Co.)

ASSAY CERTIFICATE

Emgold Mining Corp. PROJECT ROZAN File # A102380R
1400 - 570 Granville St., Vancouver BC V6C 3P1 Submitted by: Perry Grunenberg

SAMPLE#	W %
ARROW W	1.26
STANDARD W-4	.75

W BY NA2O2 FUSION, ANALYSIS BY ASSAY ICP.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK PULP

DATE RECEIVED: AUG 3 2001 DATE REPORT MAILED: Aug 13/01 SIGNED BY C. L. D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data FA

ACME ANALY AL LABORATORIES LTD. 852 E. HASTINGS ST. VAN VER BC V6A 1R6 PHONE(604)253-3158 FAX(604)25 1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Emgold Mining Corp. PROJECT STEWART File # A103794
1400 - 570 Granville St., Vancouver BC V6C 3P1 Submitted by: Linda Dandy

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** gm/mt
SI	<1	5	<3	4	<.3	1	<1	4	.04	<2	<8	<2	<2	2	<.2	<3	<3	<1	.08	<.001	<1	3	<.01	2	<.01	<3	.01	.35	.01	<2	<.01
ST 4+05S 3+00E	238	24	8	14	<.3	2	1	244	1.30	<2	<8	<2	6	39	.2	<3	4	20	.24	.036	14	14	.13	86	.05	4	.36	.09	.10	11	.01
ST 4+05S 4+30E	36	43	5	23	<.3	2	1	151	1.09	<2	<8	<2	5	40	.2	<3	<3	14	.13	.028	12	10	.12	76	.05	<3	.46	.07	.13	4	.01
ST 4+10S 6+60E	95	16	8	10	<.3	2	<1	149	1.15	<2	<8	<2	6	46	<.2	<3	3	18	.13	.028	12	14	.07	38	.06	3	.28	.07	.09	5	<.01
ST 7+00S 2+50E	4	17	4	33	<.3	3	2	249	1.25	<2	<8	<2	5	27	<.2	<3	<3	18	.10	.014	8	14	.06	36	.01	4	.38	.03	.13	13	.01
ST 7+90S 6+40E	4	5	8	16	<.3	2	1	135	.63	2	<8	<2	4	28	<.2	<3	<3	11	.06	.014	8	16	.03	41	.02	<3	.23	.03	.12	5	.01
ST 8+00S 4+30E	3	8	5	49	<.3	4	1	142	.71	<2	<8	<2	4	38	<.2	<3	<3	12	.06	.012	9	15	.06	45	.02	3	.25	.04	.13	5	<.01
RE ST 8+00S 4+30E	3	9	5	61	<.3	4	1	138	.70	2	<8	<2	4	38	.5	<3	<3	12	.06	.011	9	14	.06	44	.02	4	.24	.04	.13	4	<.01
STANDARD DS3/AU-1	10	130	36	163	<.3	36	12	836	3.28	31	<8	<2	4	28	5.8	4	5	80	.55	.098	18	184	.62	147	.09	<3	1.73	.04	.17	4	3.37

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK R150 60C AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 25 2001 DATE REPORT MAILED: Nov5/01 SIGNED BY C.L........ D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data ___ FA ___

APPENDIX II

SOIL SAMPLE RESULTS

CERTIFICATES OF ANALYSES

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Emgold Mining Corp. PROJECT STEWART File # A103745 Page 1

1400 - 570 Granville St., Vancouver BC V6C 3P1 Submitted by: Linda Dandy

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	2	3	3	38	<.3	7	4	479	1.68	<2	<8	<2	4	69	<.5	<3	<3	37	.52	.083	7	21	.51	205	.12	<3	.94	.12	.55	2	.8
AR L10N 8+00E	4	47	11	80	.3	9	16	889	2.32	26	<8	<2	<2	11	1.0	<3	<3	33	.12	.117	7	10	.10	57	.10	<3	3.47	.01	.03	<2	1.3
AR L10N 8+25E	4	43	14	146	.4	16	23	1487	4.46	15	<8	<2	<2	16	.5	<3	<3	76	.14	.106	6	25	.24	112	.12	<3	2.99	.01	.05	2	.5
AR L10N 8+50E	6	65	16	146	.3	20	31	935	5.24	138	<8	<2	2	15	.5	<3	<3	98	.11	.150	6	36	.37	97	.13	<3	3.21	.01	.07	3	13.4
AR L10N 8+75E	13	97	14	156	.4	26	45	849	3.96	198	<8	<2	2	28	1.0	<3	<3	72	.24	.137	14	20	.34	58	.13	<3	4.56	.01	.07	2	4.6
AR L10N 9+00E	9	54	13	141	<.3	21	26	498	3.62	45	<8	<2	2	10	.7	<3	<3	67	.08	.099	7	21	.32	92	.14	<3	4.30	.01	.05	<2	2.3
AR L10N 9+25E	34	109	20	252	.5	37	70	2058	6.78	273	<8	<2	<2	38	2.8	<3	<3	77	.67	.235	9	21	.35	86	.04	<3	2.99	.01	.04	50	6.3
AR L10N 9+50E	16	66	18	339	.5	23	32	1574	5.26	55	<8	<2	<2	25	2.6	<3	<3	97	.32	.105	5	18	.44	105	.13	<3	2.28	.01	.04	2	1.3
RE AR L10N 9+50E	17	67	19	339	.5	23	31	1621	5.23	56	<8	<2	<2	25	2.7	<3	<3	100	.32	.104	5	17	.43	107	.13	<3	2.30	.01	.05	2	1.3
AR L10N 9+75E	21	62	24	256	.6	25	14	1216	3.74	55	<8	<2	<2	36	2.8	<3	<3	82	.36	.131	7	36	.24	97	.06	<3	2.18	.01	.05	13	1.8
AR L10N 10+00E	6	39	38	288	.6	31	17	1492	3.12	35	<8	<2	<2	18	2.1	<3	<3	69	.21	.098	6	34	.33	121	.07	<3	2.99	.01	.04	4	2.9
AR L10N 10+25E	7	29	28	235	.6	23	16	631	4.41	28	<8	<2	2	13	1.5	<3	<3	81	.10	.154	5	28	.20	112	.11	<3	2.92	.02	.04	3	.9
AR L10N 10+50E	9	45	27	344	.6	66	22	564	5.16	24	<8	<2	2	20	1.8	<3	<3	90	.19	.106	6	46	.43	112	.10	<3	3.40	.01	.04	5	1.6
AR L10N 10+75E	9	54	18	255	.3	63	21	617	5.21	47	<8	<2	3	12	.8	<3	<3	74	.11	.090	5	36	.37	98	.10	<3	3.37	.01	.05	5	.5
AR L10N 11+00E	4	40	20	213	<.3	41	17	2371	3.50	65	<8	<2	2	12	.8	<3	<3	73	.10	.115	7	34	.33	140	.09	<3	2.67	.02	.06	3	2.1
AR L10N 11+25E	6	36	17	256	.6	50	19	482	4.08	183	<8	<2	3	26	1.0	<3	<3	70	.21	.112	5	28	.28	163	.12	<3	3.57	.01	.05	2	.4
AR L10N 11+50E	7	60	32	232	.6	49	18	983	4.50	179	<8	<2	3	20	.9	<3	<3	94	.16	.084	7	38	.37	125	.07	<3	2.99	.01	.05	3	2.4
AR L10N 11+75E	5	54	14	188	.4	57	21	1563	4.56	629	<8	<2	2	16	.9	<3	<3	79	.14	.098	7	48	.63	122	.08	<3	2.45	.01	.05	2	1.0
AR L10N 12+00E	14	68	97	464	.6	71	18	642	4.42	79	<8	<2	3	32	1.4	<3	<3	94	.15	.127	7	29	.32	85	.08	<3	2.98	.01	.04	<2	3.0
AR L10N 12+25E	5	60	28	238	.4	42	15	973	3.37	34	<8	<2	3	15	1.0	<3	<3	71	.16	.111	8	42	.65	143	.06	<3	2.48	.01	.06	<2	4.4
AR L10N 12+50E	6	87	15	311	.3	75	24	702	5.17	97	<8	<2	3	20	1.4	<3	<3	76	.22	.142	7	44	.54	103	.07	<3	3.92	.01	.05	<2	2.8
AR L9N 7+50E	5	115	34	127	.4	27	32	1111	3.90	30	<8	<2	2	12	.8	<3	<3	64	.12	.202	12	32	.52	78	.09	<3	4.17	.01	.08	<2	5.4
AR L9N 7+75E	4	50	14	135	<.3	21	20	436	4.18	21	<8	<2	2	13	.5	<3	<3	83	.10	.093	6	31	.41	110	.11	<3	2.84	.02	.06	2	5.4
AR L9N 8+00E	3	52	17	181	<.3	16	41	2616	4.38	15	<8	<2	<2	14	.6	<3	<3	82	.12	.136	6	33	.42	89	.08	<3	2.21	.01	.07	2	6.5
AR L9N 8+25E	5	60	25	127	.4	16	27	1356	4.83	38	<8	<2	<2	17	.7	<3	<3	72	.13	.135	5	20	.23	117	.12	<3	2.25	.01	.06	3	1.1
AR L9N 8+50E	18	172	15	150	.5	25	124	3531	6.81	27	<8	<2	2	20	1.0	<3	<3	75	.22	.205	8	24	.29	91	.07	<3	3.12	.01	.08	4	5.4
AR L9N 8+75E	18	120	21	201	<.3	40	36	988	5.81	40	<8	<2	2	29	1.0	<3	<3	72	.24	.135	5	19	.43	84	.10	<3	3.61	.01	.06	12	2.6
AR L9N 9+00E	7	75	13	119	<.3	19	13	462	4.82	56	<8	<2	2	21	<.5	<3	<3	81	.21	.173	5	25	.37	99	.10	<3	2.92	.01	.06	6	2.1
AR L9N 9+25E	11	41	14	174	.8	19	11	1047	3.13	32	<8	<2	2	8	.6	<3	<3	60	.08	.163	5	22	.29	139	.12	<3	3.07	.01	.04	7	1.8
AR L9N 9+50E	22	52	15	187	.7	27	21	1524	3.51	68	<8	<2	2	14	.8	<3	<3	66	.18	.125	5	26	.36	103	.08	<3	2.86	.01	.05	7	3.1
AR L9N 9+75E	25	31	20	403	.6	27	14	1399	3.47	37	<8	<2	2	18	2.3	<3	<3	70	.18	.111	5	26	.30	88	.10	<3	3.44	.01	.04	50	2.4
AR L9N 10+00E	20	63	21	519	1.0	45	17	1167	4.26	171	<8	<2	2	15	4.5	<3	<3	82	.20	.156	8	36	.38	128	.06	<3	3.29	.01	.05	25	3.6
AR L9N 10+25E	13	53	30	293	.7	26	13	1168	3.85	38	<8	<2	<2	27	2.9	<3	<3	83	.30	.137	7	33	.31	160	.05	<3	1.77	.01	.05	3	<.2
AR L9N 10+50E	19	57	65	452	.4	35	22	1252	5.33	41	<8	<2	<2	66	3.1	<3	<3	79	.71	.138	9	34	.33	171	.05	<3	1.66	.01	.07	4	3.1
STANDARD DS3	9	129	35	149	.3	36	12	754	2.95	29	<8	<2	4	24	5.5	5	6	73	.52	.091	16	175	.57	145	.07	<3	1.62	.03	.16	4	21.4

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
- SAMPLE TYPE: SOIL SS80 60C AU* BY ACID LEACHED, ANALYZE BY ICP-MS. (10 gm)
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 22 2001 **DATE REPORT MAILED:** Oct 31/01 **SIGNED BY** ....D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	<3	39	<.3	4	4	461	1.46	<2	<8	<2	5	53	<.5	<3	<3	36	.49	.093	6	12	.42	184	.11	<3	.70	.05	.41	2	.2
AR L9N 10+75E	14	96	47	1005	1.2	99	19	965	3.72	104	9	<2	3	24	7.4	<3	<3	69	.23	.086	13	51	.32	84	.11	<3	3.92	.01	.05	5	2.1
AR L9N 11+00E	11	43	15	426	.5	46	22	895	4.68	35	<8	<2	2	28	4.3	<3	<3	90	.32	.062	9	39	.28	48	.06	<3	2.94	.01	.03	7	1.4
AR L9N 11+25E	6	19	26	654	.4	66	15	416	3.59	65	<8	<2	3	24	4.9	<3	<3	62	.32	.046	7	26	.20	90	.15	<3	3.68	.01	.04	2	.8
AR L9N 11+50E	7	93	153	592	2.1	69	31	1110	5.45	187	<8	<2	4	17	3.2	<3	<3	104	.14	.106	12	45	.54	117	.09	<3	3.63	.01	.06	<2	2.8
AR L9N 11+75E	7	79	81	418	1.2	63	23	827	4.72	99	<8	<2	3	21	1.8	<3	<3	94	.22	.105	7	35	.48	99	.08	<3	2.88	.01	.06	<2	3.0
AR L9N 12+00E	5	27	21	208	.4	21	11	630	3.60	11	<8	<2	<2	14	1.2	<3	<3	76	.08	.081	7	26	.26	99	.11	<3	2.00	.01	.05	<2	1.2
AR L9N 12+25E	12	54	18	429	.4	57	22	1170	6.07	13	<8	<2	2	26	1.7	<3	<3	112	.17	.107	7	32	.26	167	.11	<3	2.58	.01	.06	<2	.7
AR L9N 12+50E	13	71	20	273	.5	52	28	983	6.62	31	<8	<2	3	17	.8	<3	<3	112	.17	.155	6	40	.45	99	.09	<3	2.95	.01	.06	2	.8
AR L8N 7+50E	10	54	21	553	.3	44	28	1485	4.80	73	<8	<2	2	23	4.0	<3	<3	95	.23	.084	10	46	.61	162	.14	<3	2.89	.01	.08	4	1.0
AR L8N 7+75E	15	134	18	572	.5	52	38	2041	5.28	89	<8	<2	2	53	5.2	<3	<3	115	.60	.138	16	45	.77	149	.12	<3	2.95	.02	.13	5	3.8
AR L8N 8+00E	6	82	29	318	<.3	133	38	847	4.94	45	<8	<2	3	42	1.4	<3	<3	104	.54	.169	10	82	2.37	165	.23	<3	3.72	.01	.12	<2	1.6
AR L8N 8+25E	3	23	24	265	.3	15	17	582	3.51	33	<8	<2	2	22	2.1	<3	<3	71	.23	.200	4	21	.39	144	.17	<3	3.27	.01	.07	<2	.6
AR L8N 8+50E	6	120	18	253	.4	28	37	1286	6.84	129	<8	<2	2	36	1.5	<3	<3	126	.32	.199	8	30	.59	224	.13	<3	3.40	.01	.14	3	2.7
AR L8N 8+75E	7	89	24	185	.6	21	26	1381	7.35	46	<8	<2	2	26	1.0	<3	<3	110	.23	.195	6	27	.36	156	.11	<3	2.35	.01	.07	3	2.1
AR L8N 9+00E	6	54	26	147	<.3	23	13	634	4.27	33	<8	<2	2	16	.6	<3	<3	83	.12	.130	7	38	.53	98	.09	<3	2.05	.01	.06	4	3.6
RE AR L8N 9+00E	6	53	26	145	<.3	22	12	653	3.98	33	<8	<2	2	16	.6	<3	<3	77	.10	.128	7	37	.55	97	.08	<3	2.08	.01	.06	4	3.1
AR L8N 9+25E	9	32	21	167	.5	12	17	987	2.83	94	<8	<2	2	13	1.1	<3	<3	51	.12	.108	4	12	.15	96	.15	<3	2.72	.01	.04	12	1.4
AR L8N 9+50E	19	66	16	144	.3	21	10	309	3.29	270	<8	<2	3	13	.5	<3	<3	62	.13	.204	10	28	.43	61	.11	<3	4.09	.01	.06	5	10.2
AR L8N 9+75E	13	31	26	119	.4	20	8	322	3.88	54	<8	<2	2	17	.7	<3	<3	88	.16	.085	7	38	.43	81	.08	<3	2.22	.01	.05	6	3.4
AR L8N 10+00E	29	55	27	1347	.5	81	17	2982	3.44	157	<8	<2	<2	74	15.6	<3	<3	62	.80	.134	13	41	.49	141	.07	<3	2.70	.01	.07	10	1.5
AR L8N 10+25E	5	40	26	203	.7	25	12	884	3.43	36	<8	<2	<2	19	1.8	<3	<3	73	.17	.107	9	40	.45	137	.08	<3	2.73	.01	.06	3	3.1
AR L8N 10+50E	6	55	18	203	.5	27	15	1272	3.85	29	<8	<2	<2	16	1.6	<3	<3	88	.14	.169	9	42	.36	107	.06	<3	2.73	.01	.06	2	2.1
AR L8N 10+75E	13	65	36	363	.4	43	19	1128	4.24	71	<8	<2	3	29	1.6	<3	<3	91	.26	.132	14	48	.62	145	.07	<3	2.97	.01	.08	5	6.5
AR L8N 11+00E	13	63	39	348	.6	45	20	1052	4.22	71	<8	<2	2	36	1.6	<3	<3	91	.30	.138	12	47	.53	126	.07	<3	3.04	.01	.06	5	4.6
AR L8N 11+25E	12	64	121	339	2.1	45	22	1154	4.40	95	<8	<2	2	28	1.5	<3	<3	91	.26	.143	9	43	.52	104	.07	<3	2.99	.02	.06	4	14.5
AR L8N 11+50E	11	83	34	220	.5	56	27	876	5.13	29	<8	<2	2	32	1.2	<3	<3	89	.24	.138	7	46	.49	96	.06	<3	3.16	.02	.04	8	2.1
AR L8N 11+75E	10	43	21	300	.4	36	24	1761	4.00	44	<8	<2	<2	34	1.7	<3	<3	77	.39	.149	5	37	.34	195	.08	<3	2.70	.01	.06	4	.7
AR L8N 12+00E	9	58	24	223	.6	36	22	1163	4.40	20	<8	<2	<2	25	1.5	<3	<3	86	.20	.154	7	42	.40	153	.09	<3	2.57	.01	.04	3	2.0
AR L8N 12+25E	17	54	66	406	1.3	39	21	986	4.74	61	<8	<2	<2	44	2.7	<3	<3	113	.39	.072	6	48	.46	132	.06	<3	2.38	.01	.04	3	.9
AR L8N 12+50E	23	112	10	619	<.3	92	38	1160	6.58	17	<8	<2	3	43	1.7	<3	<3	80	.52	.125	5	32	2.36	84	.06	<3	4.83	.01	.04	18	2.6
AR L7N 7+50E	4	142	14	208	.6	19	44	1219	5.85	17	<8	<2	<2	37	1.2	<3	<3	110	.36	.152	5	20	.37	172	.16	<3	2.62	.02	.10	3	.5
AR L7N 7+75E	8	275	12	226	.4	38	66	1437	6.47	39	<8	<2	2	38	1.4	<3	<3	101	.31	.192	6	29	.55	129	.11	<3	3.55	.01	.13	8	2.2
AR L7N 8+00E	11	114	33	262	.3	29	64	1326	6.02	29	<8	<2	3	34	1.7	<3	<3	95	.33	.063	12	35	.41	139	.12	<3	2.39	.01	.09	3	2.0
STANDARD DS3	9	133	36	154	.3	36	12	762	2.96	31	<8	<2	4	26	5.8	5	6	77	.53	.097	17	182	.58	143	.08	<3	1.70	.03	.16	4	21.7

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	<3	41	<.3	6	4	519	1.78	<2	<8	<2	5	63	<.5	<3	<3	40	.46	.090	8	17	.51	199	.11	<3	.74	.06	.44	2	<.2
AR L7N 8+25E	5	48	20	269	.3	29	26	1754	4.22	35	<8	<2	3	28	1.1	<3	<3	78	.32	.156	9	50	.55	158	.10	<3	2.36	.01	.09	2	1.6
AR L7N 8+50E	4	38	18	195	.3	27	17	950	3.41	43	<8	<2	2	19	1.1	<3	<3	67	.18	.140	8	45	.57	113	.07	<3	2.37	.01	.06	3	3.2
AR L7N 8+75E	10	90	14	271	.7	27	24	1513	5.72	31	<8	<2	3	16	1.2	<3	<3	81	.13	.146	8	34	.40	113	.10	<3	3.16	.01	.06	7	7.7
AR L7N 9+00E	6	53	15	211	.3	24	19	1436	3.92	42	<8	<2	3	11	.9	<3	<3	69	.08	.139	8	32	.44	98	.11	<3	2.89	.01	.06	6	2.5
AR L7N 9+25E	10	87	12	127	.4	14	14	777	6.66	41	<8	<2	3	18	.8	<3	<3	96	.10	.198	8	30	.43	87	.10	<3	3.60	.01	.09	5	5.0
AR L7N 9+50E	34	50	24	425	.9	21	23	2178	4.47	162	<8	<2	2	22	2.5	<3	<3	83	.23	.070	8	32	.39	139	.08	<3	2.22	.01	.06	24	4.8
AR L7N 9+75E	22	35	30	248	.3	22	12	1073	3.23	32	<8	<2	2	20	1.4	<3	<3	70	.19	.078	8	33	.43	104	.08	<3	2.20	.01	.06	24	3.1
AR L7N 10+00E	6	31	20	291	.4	26	10	1039	3.23	27	<8	<2	2	20	1.4	<3	<3	73	.19	.089	9	40	.51	126	.09	<3	2.37	.01	.07	8	13.0
AR L7N 10+25E	6	26	20	224	.3	24	12	1909	3.14	23	<8	<2	2	20	1.2	<3	<3	69	.20	.115	7	33	.39	163	.08	<3	2.22	.01	.05	2	1.2
AR L7N 10+50E	9	35	28	210	.5	26	12	473	3.32	35	<8	<2	2	20	1.0	<3	<3	70	.18	.100	9	38	.44	120	.07	<3	2.87	.01	.05	3	4.8
AR L7N 10+75E	6	31	25	219	.7	23	12	1309	2.98	30	<8	<2	2	15	1.2	<3	<3	67	.12	.127	10	37	.47	127	.08	<3	2.69	.01	.06	<2	4.3
AR L7N 11+00E	4	30	32	253	1.5	26	12	1266	3.52	39	<8	<2	<2	24	1.2	<3	<3	73	.29	.175	7	39	.50	149	.06	<3	2.00	.01	.07	<2	3.5
AR L7N 11+25E	7	44	32	206	.9	25	11	1041	3.95	38	<8	<2	<2	19	1.1	<3	<3	83	.15	.136	9	45	.45	96	.06	<3	2.05	.01	.06	<2	4.8
AR L7N 11+50E	8	28	23	176	.9	22	8	361	3.65	22	<8	<2	2	14	.7	<3	<3	85	.10	.121	8	39	.40	98	.09	<3	2.34	.01	.05	<2	2.5
AR L7N 11+75E	25	40	107	230	.5	24	14	3589	2.85	50	<8	<2	<2	85	3.4	3	<3	64	.58	.111	15	33	.50	202	.05	<3	2.15	.01	.09	3	8.7
AR L7N 12+00E	5	22	20	111	.5	15	8	1488	3.14	16	<8	<2	<2	11	<.5	<3	<3	73	.07	.196	7	33	.37	109	.08	<3	1.55	.01	.05	<2	2.6
AR L7N 12+25E	12	41	64	339	2.1	31	14	1683	3.72	34	<8	<2	<2	16	1.2	<3	<3	97	.13	.172	10	48	.51	113	.07	<3	2.94	.01	.07	<2	4.0
AR L7N 12+50E	7	39	63	269	2.0	27	11	847	3.69	28	<8	<2	2	14	1.0	<3	<3	88	.12	.204	10	44	.49	114	.08	<3	3.16	.01	.07	<2	4.6
AR L6N 7+50E	9	129	12	184	.6	24	33	1751	5.54	23	<8	<2	2	20	.7	<3	<3	98	.16	.189	7	31	.55	115	.12	<3	3.07	.01	.11	2	8.0
AR L6N 7+75E	50	244	24	170	.5	12	31	2213	8.84	24	<8	<2	<2	29	.8	<3	<3	95	.25	.246	5	28	.22	122	.07	<3	1.15	.01	.07	9	.9
AR L6N 8+00E	6	62	20	271	.3	23	24	1460	3.92	60	<8	<2	<2	24	1.6	<3	<3	82	.22	.133	8	36	.47	142	.11	<3	1.92	.01	.07	<2	1.7
AR L6N 8+25E	4	55	14	231	.4	21	22	1291	4.91	28	<8	<2	2	17	1.2	<3	<3	127	.15	.165	7	35	.64	151	.19	<3	2.73	.01	.14	2	12.0
AR L6N 8+50E	4	39	16	209	.4	25	15	566	3.74	33	<8	<2	3	19	1.3	<3	<3	74	.17	.140	7	39	.57	113	.11	<3	3.12	.01	.07	3	2.4
RE AR L6N 8+50E	4	39	16	203	.4	24	15	524	3.53	32	<8	<2	3	18	1.2	<3	<3	71	.15	.136	7	39	.52	111	.11	<3	2.99	.01	.07	3	8.0
AR L6N 8+75E	5	63	14	234	.9	19	20	1738	5.43	30	<8	<2	2	19	1.1	<3	<3	103	.17	.178	8	29	.33	136	.11	<3	2.33	.01	.06	3	2.1
AR L6N 9+00E	9	106	17	140	.4	16	23	1654	8.71	37	<8	<2	2	20	.6	<3	<3	117	.12	.228	6	33	.35	99	.10	<3	2.35	.01	.06	3	2.0
AR L6N 9+25E	7	57	21	208	.4	20	16	2075	5.36	29	<8	<2	2	14	.8	<3	<3	100	.14	.193	7	33	.37	122	.12	<3	2.29	.01	.06	6	1.7
AR L6N 9+50E	11	68	16	148	.4	17	19	1429	7.37	34	<8	<2	2	12	.5	<3	<3	98	.16	.153	6	32	.32	70	.09	<3	1.70	.01	.05	6	2.5
AR L6N 9+75E	6	29	17	219	<.3	22	13	953	3.67	39	<8	<2	3	16	.6	<3	<3	75	.13	.117	8	30	.40	135	.10	<3	2.62	.01	.07	12	3.8
AR L6N 10+00E	6	29	17	144	.3	23	7	290	3.62	19	<8	<2	3	12	<.5	<3	<3	69	.11	.081	7	30	.36	79	.11	<3	3.33	.01	.05	2	3.0
AR L6N 10+25E	34	43	21	276	.8	31	15	1045	3.54	25	<8	<2	<2	28	1.9	<3	<3	69	.23	.085	13	38	.51	95	.07	<3	2.07	.01	.06	2	4.3
AR L6N 10+50E	32	101	15	145	.4	17	11	892	7.34	15	<8	<2	2	23	1.1	<3	<3	138	.09	.216	7	44	.27	120	.06	<3	2.53	.01	.05	<2	1.6
AR L6N 10+75E	13	41	19	146	<.3	19	9	989	4.09	12	<8	<2	2	14	.5	<3	<3	106	.10	.190	7	47	.52	117	.11	<3	2.00	.01	.07	<2	1.3
STANDARD DS3	9	133	35	156	.3	36	12	797	2.99	31	<8	<2	4	28	5.7	5	6	74	.51	.091	18	193	.54	146	.08	<3	1.63	.03	.17	4	20.1

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	<3	40	<.3	6	4	486	1.64	<2	<8	<2	4	54	<.5	<3	<3	37	.46	.087	5	17	.52	216	.11	<3	.71	.05	.44	2	.2
AR L6N 11+00E	3	15	22	65	.3	10	4	180	2.70	14	<8	<2	2	7	<.5	<3	<3	64	.04	.074	4	27	.27	64	.07	<3	1.76	.01	.04	<2	2.4
AR L6N 11+25E	8	65	17	269	<.3	74	31	663	5.29	13	<8	<2	9	432	.5	<3	<3	127	1.08	.481	87	120	2.42	1320	.15	<3	3.47	.02	.43	<2	2.4
AR L6N 11+50E	9	25	26	92	.3	13	5	441	3.02	18	<8	<2	2	12	<.5	<3	<3	71	.09	.108	7	32	.38	77	.06	<3	1.84	.01	.05	<2	2.6
AR L6N 11+75E	23	31	49	177	.5	15	9	1296	3.14	23	<8	<2	2	38	1.4	<3	<3	67	.27	.075	14	27	.36	193	.07	<3	2.10	.01	.06	2	3.0
AR L6N 12+00E	8	36	30	269	.6	24	16	1889	4.04	22	<8	<2	3	19	1.1	<3	4	93	.23	.167	8	38	.49	185	.07	<3	2.53	.01	.07	2	15.7
AR L6N 12+25E	19	36	44	240	.5	24	13	1082	3.60	26	<8	<2	2	17	1.1	<3	<3	80	.14	.101	12	43	.58	164	.07	<3	2.43	.01	.06	<2	5.7
AR L6N 12+50E	14	40	32	174	.9	25	10	487	3.67	25	<8	<2	3	13	.7	<3	<3	84	.10	.149	10	42	.52	87	.08	<3	2.98	.01	.06	<2	6.1
AR L5N 7+50E	4	42	16	214	.3	16	18	2096	4.33	29	<8	<2	2	18	.7	<3	<3	102	.17	.149	7	35	.58	158	.12	<3	2.25	.01	.07	<2	2.2
AR L5N 7+75E	6	99	17	209	.7	20	34	3455	6.13	17	<8	<2	2	19	1.1	<3	<3	164	.16	.193	7	29	.94	207	.14	<3	2.69	.01	.10	<2	1.8
AR L5N 8+00E	3	58	11	200	.3	12	22	1740	6.23	8	<8	<2	2	13	.5	<3	<3	210	.15	.200	5	26	1.11	218	.28	<3	2.91	.01	.27	2	.9
AR L5N 8+25E	11	52	13	293	.4	19	23	1292	4.29	54	<8	<2	2	17	1.4	<3	<3	104	.16	.109	8	34	.62	141	.14	<3	2.61	.01	.09	2	1.5
AR L5N 8+50E	6	34	15	184	.3	16	15	1001	4.11	44	<8	<2	<2	14	.9	<3	<3	85	.12	.193	7	36	.41	102	.09	<3	2.13	.01	.06	3	1.9
AR L5N 8+75E	17	59	13	378	.4	19	23	996	4.58	49	<8	<2	<2	25	2.2	<3	<3	96	.19	.088	11	33	.51	121	.12	<3	2.59	.01	.10	3	6.3
AR L5N 9+00E	23	148	11	242	.5	18	26	1159	5.35	57	<8	<2	<2	19	1.2	<3	<3	74	.14	.156	8	30	.42	86	.06	<3	2.64	.01	.06	4	15.6
AR L5N 9+25E	15	60	14	311	.6	28	23	940	4.10	28	<8	<2	2	46	2.0	<3	<3	77	.41	.095	10	36	.63	143	.10	<3	2.48	.01	.08	4	1.6
AR L5N 9+50E	20	60	14	282	.4	24	26	717	4.48	16	<8	<2	2	22	1.2	<3	<3	88	.17	.101	9	35	.50	136	.11	<3	2.54	.01	.06	3	6.7
AR L5N 9+75E	12	40	13	156	.3	16	12	864	4.01	17	<8	<2	2	17	.5	<3	<3	81	.14	.141	7	34	.40	126	.10	<3	2.56	.01	.05	2	2.1
AR L5N 10+00E	22	40	16	211	.4	28	13	674	3.29	20	<8	<2	2	15	.9	<3	<3	72	.13	.069	8	35	.43	92	.10	<3	2.99	.01	.05	3	4.2
AR L5N 10+25E	19	41	17	68	.3	12	5	463	4.40	23	<8	<2	<2	15	.6	<3	<3	90	.09	.135	6	34	.30	73	.07	<3	1.43	.01	.05	2	17.5
AR L5N 10+50E	9	30	16	118	.3	17	10	1448	3.15	23	<8	<2	2	14	.5	<3	<3	72	.12	.122	8	36	.43	88	.05	<3	1.92	.01	.05	2	19.3
AR L5N 10+75E	7	27	19	106	.3	16	6	240	3.86	29	<8	<2	3	14	<.5	<3	<3	79	.10	.136	7	37	.36	93	.11	<3	3.05	.01	.05	2	2.2
RE AR L5N 10+75E	7	29	20	108	.3	16	7	260	3.99	31	<8	<2	3	14	<.5	<3	<3	79	.11	.142	7	37	.36	99	.11	<3	3.40	.01	.05	2	3.2
AR L5N 11+00E	4	26	16	117	.3	13	5	333	2.78	16	<8	<2	2	9	<.5	<3	<3	64	.07	.125	6	28	.31	70	.09	<3	2.91	.01	.04	<2	1.1
AR L5N 11+25E	4	30	15	88	.3	11	8	380	3.55	12	<8	<2	2	10	<.5	<3	<3	79	.06	.107	10	37	.38	80	.08	<3	2.83	.01	.05	<2	16.3
AR L5N 11+50E	25	41	31	255	.3	15	11	868	3.74	25	<8	<2	3	26	1.4	<3	<3	76	.22	.075	14	34	.44	153	.06	<3	2.11	.01	.06	2	5.5
CR L0S 0+25E	2	98	33	180	.6	21	22	1635	4.52	37	<8	<2	<2	53	2.2	<3	<3	89	.60	.145	10	40	.91	136	.10	<3	2.43	.01	.17	<2	56.8
CR L0S 0+50E	3	134	31	210	.6	24	20	1427	3.77	35	<8	<2	<2	40	2.2	<3	<3	86	.47	.177	11	38	.90	117	.08	<3	2.55	.01	.16	<2	83.5
CR L0S 0+75E	4	59	13	199	.6	28	15	811	3.27	14	<8	<2	<2	30	1.9	<3	<3	86	.36	.133	10	56	.81	90	.10	<3	3.02	.01	.08	<2	2.2
CR L0S 1+00E	2	45	23	250	.9	23	18	1477	3.55	16	<8	<2	<2	41	1.5	<3	<3	87	.53	.254	5	53	.75	162	.07	<3	2.17	.01	.06	<2	1.9
CR L0S 1+25E	4	68	15	198	.6	28	15	978	3.61	13	<8	<2	<2	25	1.5	<3	<3	81	.27	.130	8	51	.73	95	.07	<3	2.80	.01	.08	<2	3.9
CR L0S 1+50E	2	49	16	293	.9	32	20	1391	3.47	14	<8	<2	<2	36	3.3	<3	<3	75	.33	.271	8	51	.79	205	.09	<3	2.65	.01	.08	<2	1.6
CR L0S 1+75E	4	79	14	256	.8	48	22	921	4.08	18	<8	<2	<2	39	1.6	<3	<3	90	.46	.302	10	65	1.12	124	.09	<3	2.43	.01	.12	<2	1.9
CR L0S 2+00E	4	58	30	205	.4	25	18	1263	3.31	11	<8	<2	<2	40	2.4	<3	<3	74	.44	.185	10	48	.72	106	.06	<3	2.24	.01	.07	<2	2.7
STANDARD DS3	9	126	34	153	.3	34	12	724	2.94	30	<8	<2	4	29	5.5	5	6	75	.53	.087	17	193	.56	151	.08	<3	1.64	.03	.16	4	20.9

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	3	42	<.3	6	4	487	1.68	<2	<8	<2	5	65	<.5	<3	<3	41	.54	.094	8	17	.52	223	.12	<3	.81	.06	.45	2	<.2
CR L0S 2+25E	4	63	24	193	.6	29	22	1632	3.01	10	<8	<2	<2	42	3.5	<3	<3	81	.41	.153	17	50	.68	103	.07	<3	2.29	.01	.07	<2	1.6
CR L0S 2+50E	2	34	15	229	.8	24	15	815	3.26	14	<8	<2	2	31	1.8	<3	<3	80	.31	.171	8	42	.60	143	.11	<3	2.94	.01	.06	<2	.7
CR L0S 2+75E	3	37	18	195	.7	26	16	730	3.57	11	<8	<2	2	28	1.3	<3	<3	95	.27	.156	8	51	.67	170	.13	<3	2.66	.01	.08	<2	1.0
CR L0S 3+00E	4	68	15	241	.5	37	21	803	4.05	14	<8	<2	2	27	1.0	<3	<3	114	.26	.257	8	69	.94	190	.11	<3	2.58	.01	.08	<2	2.5
CR L0S 3+25E	7	72	14	209	.5	41	23	1441	4.00	9	<8	<2	<2	28	1.4	<3	<3	116	.25	.125	10	57	.87	178	.11	<3	2.71	.01	.11	<2	1.4
CR L0S 3+50E	4	59	16	224	.3	40	22	1538	4.40	12	<8	<2	2	29	1.2	<3	<3	123	.30	.167	8	67	1.05	200	.10	<3	2.55	.01	.12	<2	1.8
CR L0S 3+75E	4	50	16	217	.5	31	20	719	4.09	17	<8	<2	3	15	.9	<3	<3	110	.13	.294	7	54	.79	133	.12	<3	3.38	.01	.08	<2	1.9
CR L0S 4+00E	3	46	17	202	.6	30	20	864	3.66	10	<8	<2	2	18	1.0	<3	<3	100	.16	.126	7	53	.80	156	.11	<3	2.52	.01	.08	<2	1.1
CR L1S 0+25E	4	73	14	195	1.1	30	18	745	3.69	17	<8	<2	2	18	1.6	<3	<3	84	.17	.289	8	49	.66	114	.07	<3	2.60	.01	.06	<2	2.8
CR L1S 0+50E	4	56	15	183	.6	28	16	1008	3.61	15	<8	<2	<2	20	1.7	<3	<3	97	.17	.236	9	50	.69	120	.08	<3	2.73	.01	.07	<2	3.8
CR L1S 0+75E	6	79	27	278	.6	45	24	1261	4.90	18	<8	<2	<2	56	1.6	<3	<3	129	.60	.170	9	62	.96	195	.11	<3	2.67	.01	.12	<2	14.1
CR L1S 1+00E	4	68	14	213	.7	41	20	720	3.32	13	<8	<2	2	27	1.4	<3	<3	102	.30	.182	9	57	.92	152	.11	<3	2.88	.01	.09	<2	3.5
CR L1S 1+25E	4	77	18	299	.7	41	26	1268	4.39	16	<8	<2	2	43	1.3	<3	<3	122	.43	.227	8	71	1.15	173	.11	<3	2.65	.01	.08	<2	4.7
CR L1S 1+50E	4	45	18	217	.7	29	20	1406	3.55	10	<8	<2	2	26	2.1	<3	<3	96	.24	.168	9	51	.65	164	.11	<3	2.58	.01	.07	<2	1.0
CR L1S 1+75E	4	64	14	255	.6	36	23	1026	4.62	16	<8	<2	2	29	2.0	<3	<3	131	.25	.238	8	62	.87	199	.13	<3	2.66	.01	.12	<2	1.8
CR L1S 2+00E	4	53	14	243	.6	32	21	1375	3.49	10	<8	<2	2	28	2.0	<3	<3	91	.36	.158	9	49	.70	141	.13	<3	3.03	.01	.07	<2	1.0
CR L1S 2+25E	3	63	16	277	.5	43	23	1497	4.16	11	<8	<2	2	29	2.0	<3	<3	120	.31	.152	7	67	.97	217	.14	<3	2.89	.02	.10	<2	3.2
CR L1S 2+50E	4	46	18	169	.4	24	17	875	3.18	10	<8	<2	2	25	1.4	<3	<3	86	.21	.158	10	44	.53	124	.13	<3	3.71	.01	.09	<2	4.7
RE CR L1S 2+50E	4	44	18	157	.4	24	17	824	3.15	9	<8	<2	2	24	1.5	<3	<3	85	.22	.150	10	40	.54	122	.12	<3	3.60	.01	.09	<2	1.9
CR L1S 2+75E	4	60	16	210	.5	36	19	916	3.70	12	<8	<2	2	25	1.5	<3	<3	98	.29	.176	10	55	.74	134	.11	<3	3.36	.01	.09	<2	4.0
CR L1S 3+00E	3	49	23	208	.7	28	17	1539	3.54	11	<8	<2	<2	20	1.6	<3	<3	94	.17	.117	9	53	.67	141	.12	<3	2.52	.01	.07	<2	2.3
CR L1S 3+25E	5	59	18	163	.5	28	19	1105	3.77	11	<8	<2	2	21	.9	<3	<3	107	.20	.113	9	57	.67	100	.13	<3	2.64	.01	.07	<2	2.3
CR L1S 3+50E	4	46	14	162	.8	28	15	932	3.51	10	<8	<2	2	18	.7	<3	<3	95	.16	.120	8	53	.73	106	.12	<3	2.40	.01	.07	<2	1.4
CR L1S 3+75E	5	54	18	179	.4	22	20	1028	3.73	12	<8	<2	2	14	.9	<3	<3	90	.11	.239	7	39	.45	121	.11	<3	3.06	.01	.06	<2	5.7
CR L1S 4+00E	5	41	13	145	.3	22	13	948	2.68	8	<8	<2	2	24	.8	<3	<3	73	.21	.194	7	30	.39	108	.12	<3	3.57	.01	.05	<2	1.0
CR L2S 0+00E	8	93	20	268	<.3	59	24	964	4.67	21	<8	<2	2	29	2.0	3	<3	103	.29	.150	18	60	1.10	134	.09	<3	2.24	.01	.10	<2	3.6
CR L2S 0+25E	4	61	13	273	.9	45	21	785	3.78	14	<8	<2	2	19	2.1	<3	<3	92	.18	.175	13	52	.81	136	.12	<3	3.34	.01	.08	<2	2.0
CR L2S 0+50E	4	61	16	206	.5	29	17	757	3.74	11	<8	<2	2	40	1.6	<3	<3	109	.29	.382	10	53	.75	198	.11	<3	3.11	.01	.09	<2	10.5
CR L2S 0+75E	5	75	17	197	.9	28	23	1861	4.26	8	<8	<2	<2	40	2.2	<3	<3	112	.33	.129	12	45	.65	149	.12	<3	2.58	.01	.09	<2	4.0
CR L2S 1+00E	7	84	15	191	.5	36	23	893	4.54	12	<8	<2	3	28	1.3	<3	<3	115	.24	.143	11	48	.71	142	.13	<3	3.88	.01	.10	2	3.3
CR L2S 1+25E	3	50	14	200	.6	27	16	1382	3.21	9	<8	<2	<2	24	1.6	<3	<3	92	.24	.133	8	45	.59	143	.12	<3	2.66	.01	.08	<2	1.3
CR L2S 1+50E	9	110	31	206	<.3	46	27	1262	4.75	12	<8	<2	3	46	1.4	<3	<3	138	.45	.181	12	59	.93	181	.14	3	2.95	.02	.25	3	4.2
CR L2S 1+75E	4	68	24	265	.7	37	23	1245	4.03	11	<8	<2	2	34	2.7	<3	<3	108	.36	.176	9	54	.75	164	.12	<3	2.91	.01	.09	<2	2.7
STANDARD DS3	9	125	35	159	.3	35	12	775	2.96	30	<8	<2	4	29	5.6	5	5	81	.51	.092	19	193	.53	150	.08	<3	1.72	.03	.16	3	19.7

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	<3	38	<.3	6	4	497	1.63	<2	<8	<2	5	55	<.5	<3	<3	39	.44	.084	7	17	.50	203	.11	<3	.74	.05	.43	2	<.2
CR L2S 2+00E	5	74	16	230	.3	49	22	884	4.67	17	<8	<2	2	27	1.1	<3	<3	121	.32	.230	8	76	.89	131	.11	<3	3.14	.01	.12	<2	3.4
CR L2S 2+25E	3	54	17	191	.6	33	20	996	4.29	13	<8	<2	2	24	1.1	<3	<3	111	.24	.201	7	71	.84	117	.10	<3	2.61	.01	.07	<2	1.8
CR L2S 2+50E	4	50	33	263	.4	29	19	5721	3.34	8	<8	<2	<2	26	3.0	<3	<3	89	.25	.144	7	45	.57	299	.10	<3	1.79	.01	.08	<2	4.1
CR L2S 2+75E	7	104	14	216	.7	44	28	1142	4.75	12	<8	<2	2	25	1.7	<3	<3	133	.26	.141	12	64	.84	141	.12	<3	3.30	.01	.11	2	10.5
CR L2S 3+00E	8	64	19	220	.6	25	19	1034	4.40	12	<8	<2	2	26	1.2	<3	<3	106	.29	.134	8	41	.61	117	.13	<3	2.68	.01	.09	2	3.2
CR L2S 3+25E	7	77	28	227	.4	30	23	1406	4.05	11	<8	<2	<2	33	1.6	<3	<3	104	.33	.143	10	45	.67	109	.11	<3	2.47	.01	.09	2	4.7
CR L2S 3+50E	6	56	44	335	.5	28	25	2515	4.20	12	<8	<2	<2	38	1.8	<3	<3	104	.41	.169	8	45	.64	178	.11	<3	2.28	.01	.08	<2	2.1
CR L2S 3+75E	10	131	15	269	.4	59	33	1183	6.08	13	<8	<2	3	31	1.4	<3	<3	174	.33	.163	12	67	1.05	212	.13	<3	3.71	.01	.13	3	8.7
CR L2S 4+00E	7	81	20	253	.6	28	24	1436	5.18	9	<8	<2	2	21	1.5	<3	<3	137	.20	.165	9	50	.64	174	.13	<3	2.22	.01	.08	2	2.3
CR L3S 0+00E	4	52	17	224	.4	32	23	1479	3.75	15	<8	<2	<2	71	2.3	<3	<3	83	.80	.133	13	50	.71	160	.09	3	2.18	.01	.10	<2	1.6
CR L3S 0+25E	5	75	19	273	.5	34	26	1829	4.41	10	<8	<2	<2	43	3.1	<3	<3	109	.42	.153	12	53	.71	142	.12	<3	2.68	.01	.09	<2	1.7
CR L3S 0+50E	5	64	17	234	.4	31	26	1781	4.18	11	<8	<2	2	35	2.7	<3	<3	108	.33	.153	11	51	.67	158	.13	3	2.52	.01	.10	2	2.8
CR L3S 0+75E	6	84	14	194	.4	35	24	1081	4.30	11	<8	<2	2	26	1.3	<3	<3	110	.25	.166	17	51	.74	106	.13	<3	3.71	.01	.11	2	4.5
CR L3S 1+00E	5	73	14	218	.4	37	25	1444	3.97	10	<8	<2	2	21	2.6	<3	<3	117	.22	.136	12	53	.70	124	.12	<3	2.82	.01	.08	2	5.0
CR L3S 1+25E	5	70	20	250	.4	37	24	1436	4.15	14	<8	<2	2	52	2.8	<3	<3	117	.61	.231	9	50	.69	182	.12	<3	2.67	.01	.09	2	7.4
CR L3S 1+50E	3	48	14	306	.3	31	23	2682	3.72	10	<8	<2	2	43	2.7	<3	<3	100	.51	.240	9	51	.64	261	.12	<3	2.65	.01	.07	<2	4.6
CR L3S 1+75E	5	76	15	214	<.3	42	21	842	4.20	12	<8	<2	2	26	1.2	<3	<3	113	.30	.159	9	59	.80	140	.13	<3	3.34	.01	.10	2	3.8
CR L3S 2+00E	4	46	21	234	.3	30	20	1682	3.87	11	<8	<2	2	46	2.5	<3	<3	95	.48	.161	7	48	.61	221	.11	<3	2.51	.01	.09	<2	2.1
CR L3S 2+25E	5	82	16	180	.5	35	23	1049	4.18	11	<8	<2	3	29	1.2	<3	<3	110	.31	.188	11	49	.70	131	.11	<3	3.59	.01	.09	2	4.0
CR L3S 2+50E	4	57	30	180	.6	26	18	983	3.74	10	<8	<2	2	27	1.2	<3	<3	103	.29	.179	7	48	.57	140	.11	<3	2.24	.01	.08	<2	3.1
CR L3S 2+75E	5	67	16	220	.4	31	23	1810	4.07	11	<8	<2	2	32	1.1	<3	<3	108	.31	.241	8	49	.67	172	.12	<3	2.75	.01	.08	<2	2.3
RE CR L3S 2+75E	5	67	15	231	.4	30	24	1794	4.24	11	<8	<2	2	32	1.1	<3	<3	107	.31	.245	8	49	.65	169	.12	<3	2.67	.01	.09	<2	2.2
CR L3S 3+00E	5	60	19	211	.3	30	23	1843	3.95	9	<8	<2	2	23	1.1	<3	<3	106	.17	.159	7	54	.73	143	.10	<3	2.35	.01	.08	<2	2.9
CR L3S 3+25E	4	64	15	180	.6	27	20	1274	3.68	10	<8	<2	2	22	1.0	<3	<3	96	.21	.220	8	50	.67	113	.12	<3	2.84	.01	.08	<2	2.0
CR L3S 3+50E	5	53	13	233	.6	28	21	978	3.51	10	<8	<2	2	20	.9	<3	<3	93	.18	.205	7	45	.67	117	.13	<3	3.29	.01	.06	<2	1.8
CR L3S 3+75E	6	74	14	198	.6	25	23	1343	3.84	9	<8	<2	2	17	.8	<3	<3	94	.17	.202	7	38	.61	118	.14	<3	2.99	.01	.08	3	1.8
CR L3S 4+00E	10	72	66	153	.6	17	14	1475	4.11	14	<8	<2	<2	31	1.3	<3	<3	91	.26	.152	7	29	.48	150	.10	<3	2.21	.01	.08	8	2.4
CR L4S 0+00E	3	51	16	217	.4	30	21	1396	3.39	10	<8	<2	2	49	1.7	<3	<3	83	.47	.150	9	52	.64	169	.11	<3	2.75	.01	.09	<2	2.9
CR L4S 0+25E	4	55	19	208	.5	32	20	1311	3.54	10	<8	<2	<2	38	1.9	<3	<3	98	.40	.136	10	47	.69	154	.12	<3	2.69	.01	.10	<2	3.1
CR L4S 0+50E	4	73	15	232	.4	37	24	1467	3.67	9	<8	<2	2	34	2.4	<3	<3	107	.33	.169	11	50	.69	212	.11	<3	3.07	.01	.10	<2	4.1
CR L4S 0+75E	6	71	18	198	.4	36	24	1281	4.06	14	<8	<2	2	31	1.2	<3	<3	100	.27	.173	9	45	.72	161	.11	<3	3.02	.01	.09	2	14.4
CR L4S 1+00E	3	42	18	187	.3	26	19	1619	3.42	12	<8	<2	2	21	1.8	<3	<3	91	.17	.135	8	44	.59	128	.12	<3	2.45	.01	.07	<2	1.7
CR L4S 1+25E	3	53	15	209	.5	28	19	1310	3.57	10	<8	<2	2	18	1.4	<3	<3	96	.14	.120	8	55	.73	123	.12	<3	2.47	.01	.07	<2	1.2
STANDARD DS3	9	130	35	158	.3	37	13	770	3.05	31	<8	<2	4	29	5.6	5	6	80	.51	.094	19	194	.58	145	.09	<3	1.64	.03	.17	4	20.3

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

ACME ANALYTICAL

Emgold Mining Corp. PROJECT STEWART FILE # A103745

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	<3	39	<.3	6	4	510	1.65	<2	<8	<2	5	59	<.5	<3	<3	39	.48	.098	7	17	.56	208	.12	<3	.83	.06	.44	2	<.2
CR L4S 1+50E	3	56	13	212	.8	31	20	1578	3.77	10	<8	<2	<2	21	1.6	<3	<3	98	.17	.262	8	66	.77	163	.11	<3	2.97	.01	.07	<2	4.1
CR L4S 1+75E	5	73	16	215	.5	34	25	1744	3.68	10	<8	<2	<2	16	1.4	<3	<3	101	.14	.162	10	61	.97	87	.10	<3	3.39	.01	.07	<2	5.7
CR L4S 2+00E	5	73	12	197	.8	36	21	775	4.23	10	<8	<2	2	17	1.3	<3	<3	111	.15	.124	10	67	1.01	89	.13	<3	3.63	.01	.07	<2	2.9
CR L4S 2+25E	5	66	14	225	.4	33	21	983	3.93	10	<8	<2	2	18	1.0	<3	<3	113	.16	.280	7	63	.96	149	.11	<3	3.38	.01	.07	<2	4.3
CR L4S 2+50E	4	47	14	271	<.3	33	20	1063	3.94	12	<8	<2	2	20	1.3	<3	<3	103	.18	.302	7	58	.85	201	.14	<3	3.52	.01	.08	<2	4.5
CR L4S 2+75E	5	57	17	242	.3	31	27	2261	3.91	11	<8	<2	2	21	1.2	<3	<3	111	.19	.223	7	61	.75	155	.12	<3	2.76	.01	.06	<2	1.3
CR L4S 3+00E	6	104	14	279	.4	45	35	924	4.58	17	<8	<2	2	29	1.1	<3	<3	124	.32	.278	7	84	1.14	141	.13	<3	3.93	.01	.07	2	4.2
CR L4S 3+25E	4	42	16	222	.5	23	16	1021	3.33	11	<8	<2	2	21	.9	<3	<3	88	.23	.234	6	44	.58	128	.15	<3	4.22	.01	.08	<2	1.4
CR L4S 3+50E	4	44	14	198	.4	26	17	960	3.18	10	<8	<2	2	13	.7	<3	<3	91	.12	.236	6	45	.64	111	.13	<3	4.33	.01	.07	<2	3.7
CR L4S 3+75E	6	56	18	228	.3	29	22	1489	3.60	12	<8	<2	2	14	.7	<3	<3	95	.12	.235	7	49	.74	126	.13	<3	4.10	.01	.07	2	1.8
CR L4S 4+00E	9	59	21	150	.4	17	15	884	4.07	13	<8	<2	2	13	.6	<3	<3	97	.08	.126	6	31	.51	95	.13	<3	3.04	.01	.06	5	.9
CR L10S 0+00E	3	42	14	178	.5	21	17	1112	3.18	10	<8	<2	2	12	.7	<3	<3	83	.11	.131	6	47	.55	132	.13	<3	3.87	.01	.05	<2	1.3
CR L10S 0+25E	2	47	30	161	.7	26	14	926	3.63	7	<8	<2	<2	19	.6	<3	<3	91	.18	.132	5	61	.78	95	.14	<3	2.72	.01	.09	<2	3.3
CR L10S 0+50E	2	35	44	108	.6	18	13	1313	3.29	10	<8	<2	2	12	.5	<3	<3	92	.08	.142	6	43	.61	121	.13	<3	1.84	.01	.07	<2	4.1
CR L10S 0+75E	3	50	18	123	<.3	22	16	902	3.96	7	<8	<2	3	16	<.5	<3	<3	105	.11	.346	7	52	.86	133	.13	<3	3.36	.01	.08	<2	2.8
CR L10S 1+00E	2	59	26	119	.3	22	13	626	3.95	13	<8	<2	3	12	<.5	<3	<3	91	.11	.193	7	49	.77	76	.14	<3	3.68	.01	.08	2	14.7
CR L10S 1+25E	2	52	14	106	.4	17	12	494	3.36	6	<8	<2	3	14	<.5	<3	<3	82	.09	.159	7	32	.65	86	.14	<3	4.69	.01	.08	<2	4.0
CR L10S 1+50E	3	28	15	70	<.3	8	7	669	2.52	4	<8	<2	2	10	<.5	<3	<3	74	.08	.094	5	16	.32	69	.14	<3	3.27	.01	.06	<2	1.6
CR L10S 1+75E	2	32	13	70	<.3	12	10	446	3.31	4	<8	<2	3	10	<.5	<3	<3	82	.08	.094	8	25	.44	61	.14	<3	3.82	.01	.06	<2	3.4
RE CR L10S 1+75E	2	29	13	69	<.3	11	10	447	3.16	4	<8	<2	3	10	<.5	<3	<3	79	.07	.094	8	25	.44	62	.15	<3	3.66	.01	.06	<2	3.5
CR L10S 2+00E	2	28	16	78	<.3	10	8	520	3.02	5	<8	<2	2	11	<.5	<3	<3	73	.08	.095	6	21	.40	67	.13	<3	3.77	.01	.06	<2	3.0
CR L10S 2+25E	2	22	20	82	<.3	9	8	2709	2.81	4	<8	<2	2	13	<.5	<3	<3	66	.12	.099	6	19	.34	98	.12	<3	2.03	.01	.06	<2	1.4
CR L10S 2+50E	2	36	76	93	<.3	11	9	421	3.14	17	<8	<2	2	12	<.5	<3	<3	67	.10	.076	5	20	.40	56	.11	<3	2.93	.01	.06	<2	2.1
CR L10S 2+75E	2	14	56	91	.3	7	6	666	2.83	5	<8	<2	<2	9	<.5	<3	<3	71	.10	.053	6	16	.18	40	.11	<3	1.40	.01	.05	<2	2.6
CR L10S 3+00E	12	49	22	170	.3	18	12	676	3.40	12	<8	<2	2	11	.5	<3	<3	87	.08	.128	6	32	.53	61	.10	<3	3.66	.01	.05	<2	5.4
CR L10S 3+25E	15	59	19	342	.4	26	13	701	3.83	11	<8	<2	<2	21	1.1	<3	<3	89	.14	.130	7	31	.63	138	.10	<3	3.67	.01	.07	<2	14.7
CR L10S 3+50E	23	63	22	681	.3	52	22	1504	3.93	15	<8	<2	<2	35	3.2	<3	<3	93	.42	.085	15	41	.61	51	.08	<3	2.45	.01	.06	4	6.8
CR L10S 3+75E	22	43	26	346	<.3	19	19	1571	3.53	10	<8	<2	<2	59	4.5	<3	<3	86	.54	.093	17	30	.55	83	.10	<3	2.28	.01	.08	<2	2.9
CR L10S 4+00E	31	89	26	359	.3	39	28	1675	4.72	10	<8	<2	<2	29	2.2	<3	<3	108	.29	.100	13	36	.70	88	.06	<3	2.57	.01	.08	6	3.8
CR L12S 0+00E	2	56	20	130	.5	20	18	1907	3.34	7	<8	<2	2	21	.5	<3	<3	86	.15	.164	7	37	.72	115	.11	<3	3.02	.01	.10	<2	9.1
CR L12S 0+25E	2	50	16	107	.3	15	14	904	2.88	7	<8	<2	3	13	<.5	<3	<3	68	.11	.193	7	24	.50	85	.15	<3	4.19	.01	.08	<2	1.3
CR L12S 0+50E	10	74	16	137	<.3	19	14	492	3.54	7	<8	<2	3	12	<.5	<3	<3	74	.07	.132	7	24	.55	68	.10	<3	3.79	.01	.08	<2	8.2
CR L12S 0+75E	3	68	19	154	.3	26	20	1113	3.55	10	<8	<2	4	9	<.5	<3	<3	84	.06	.219	10	43	.82	83	.14	<3	4.22	.01	.10	<2	4.3
STANDARD DS3	9	128	34	154	.3	36	13	769	3.03	30	<8	<2	4	28	5.7	6	6	77	.49	.096	18	185	.62	141	.09	<3	1.71	.03	.17	4	20.9

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	<3	42	<.3	6	4	514	1.67	<2	<8	<2	4	56	<.5	<3	<3	38	.47	.094	7	15	.51	207	.12	<3	.80	.05	.47	2	.2
CR L12S 1+00E	3	68	17	133	.3	20	16	1055	3.50	7	<8	<2	3	10	<.5	<3	<3	91	.08	.189	7	35	.79	82	.15	<3	4.45	.01	.11	<2	2.6
CR L12S 1+25E	1	30	21	69	<.3	8	9	4409	2.54	3	<8	<2	<2	12	<.5	<3	<3	68	.11	.076	6	15	.27	92	.10	<3	1.72	.01	.07	<2	.7
CR L12S 1+50E	2	45	17	98	.7	10	10	976	2.70	5	<8	<2	3	8	<.5	<3	<3	61	.06	.159	7	13	.43	83	.16	<3	4.42	.01	.08	<2	2.4
CR L12S 1+75E	3	62	12	122	<.3	15	18	861	4.19	5	<8	<2	3	15	<.5	<3	<3	120	.10	.140	7	21	1.09	140	.17	<3	4.56	.01	.45	<2	7.6
CR L12S 2+00E	4	44	27	122	<.3	16	12	836	3.06	9	<8	<2	4	11	<.5	<3	<3	63	.11	.175	6	20	.42	62	.15	<3	4.55	.01	.08	<2	6.3
CR L12S 2+25E	2	46	16	123	.3	17	15	958	3.27	9	<8	<2	2	15	<.5	<3	<3	78	.15	.234	6	28	.59	116	.14	<3	4.02	.01	.08	<2	2.4
CR L12S 2+50E	10	70	34	200	.3	30	15	1050	3.12	14	<8	<2	3	9	.7	<3	<3	68	.08	.201	8	29	.54	56	.14	<3	4.62	.01	.08	<2	39.6
CR L12S 2+75E	14	56	22	195	.3	30	16	772	3.80	8	<8	<2	3	10	<.5	<3	<3	87	.08	.119	7	31	.43	72	.13	<3	3.35	.01	.06	<2	42.9
CR L12S 3+00E	28	80	13	107	.3	10	8	727	4.94	6	<8	<2	<2	37	<.5	<3	<3	129	.16	.258	8	20	1.07	167	.14	<3	3.02	.01	.33	<2	11.4
CR L12S 3+25E	11	75	13	147	.4	25	14	903	3.67	7	<8	<2	3	11	<.5	<3	<3	79	.10	.194	7	35	.56	64	.11	<3	3.78	.01	.07	<2	8.7
CR L12S 3+50E	13	76	16	272	.3	39	14	528	3.85	9	<8	<2	4	11	<.5	<3	<3	96	.09	.149	10	38	.57	68	.09	<3	4.00	.01	.07	<2	12.6
CR L12S 3+75E	30	61	32	175	.6	22	10	712	4.89	10	<8	<2	2	8	.5	<3	3	96	.06	.203	8	34	.41	59	.03	<3	2.60	<.01	.09	<2	6.1
CR L12S 4+00E	6	29	18	100	<.3	14	6	380	4.38	8	<8	<2	4	7	<.5	<3	<3	77	.06	.117	7	38	.43	51	.14	<3	3.54	.01	.08	<2	5.0
CR L14S 0+00E	13	88	19	146	.7	25	20	1755	4.03	7	<8	<2	2	22	.6	<3	<3	96	.15	.117	13	29	.67	154	.11	<3	2.82	.01	.09	<2	3.8
CR L14S 0+25E	19	87	28	161	.8	30	18	1484	4.13	11	<8	<2	<2	22	1.0	<3	<3	94	.17	.221	9	28	.50	105	.06	<3	2.86	.01	.10	2	2.1
CR L14S 0+50E	17	97	17	162	.7	27	17	1347	3.64	8	<8	<2	<2	18	.6	<3	<3	93	.16	.121	11	28	.59	86	.08	<3	3.47	.01	.09	<2	3.4
CR L14S 0+75E	14	132	77	214	.3	19	32	3634	4.29	12	<8	<2	<2	58	2.5	<3	<3	107	.48	.193	7	22	.85	194	.10	<3	2.85	.01	.20	2	4.4
CR L14S 1+00E	20	139	72	209	.3	18	34	3804	3.91	10	<8	<2	<2	51	2.9	<3	<3	94	.49	.200	7	18	.65	161	.09	<3	2.75	.01	.14	<2	2.4
CR L14S 1+25E	6	72	13	122	<.3	14	16	1223	3.59	5	<8	<2	<2	18	<.5	<3	<3	96	.23	.163	7	18	.70	97	.11	<3	3.18	.01	.13	<2	3.4
CR L14S 1+50E	4	45	29	155	.3	14	14	1358	3.42	7	<8	<2	2	22	.8	<3	<3	88	.18	.118	7	19	.54	108	.13	<3	2.69	.01	.11	<2	2.7
CR L14S 1+75E	4	52	12	132	<.3	15	15	1157	3.31	6	<8	<2	2	17	<.5	<3	<3	87	.16	.150	7	22	.59	86	.14	<3	3.65	.01	.10	<2	3.9
RE CR L14S 1+75E	4	53	12	129	<.3	15	14	1108	3.41	5	<8	<2	2	17	<.5	<3	<3	88	.15	.148	7	22	.61	85	.13	<3	3.58	.01	.10	<2	2.3
CR L14S 2+00E	5	52	14	138	<.3	15	15	1095	3.45	5	<8	<2	<2	16	.5	<3	<3	93	.17	.108	6	18	.64	78	.11	<3	2.76	.01	.11	<2	5.0
CR L14S 2+25E	8	65	13	177	<.3	20	16	693	3.38	7	<8	<2	2	14	<.5	<3	<3	88	.15	.107	7	21	.66	69	.12	<3	3.60	.01	.11	<2	2.9
CR L14S 2+50E	7	57	22	199	<.3	20	17	1179	3.37	9	<8	<2	2	15	.7	<3	<3	83	.15	.160	7	22	.54	88	.11	<3	3.22	.01	.09	<2	4.3
CR L14S 2+75E	11	46	21	198	.4	16	15	1561	3.70	6	<8	<2	<2	15	.8	<3	<3	79	.16	.134	6	21	.37	93	.09	<3	2.02	.01	.08	<2	18.7
CR L14S 3+00E	28	117	30	376	.4	34	29	2425	4.17	10	<8	<2	<2	25	2.6	<3	<3	79	.27	.161	11	23	.51	114	.05	<3	2.94	.01	.08	<2	2.3
CR L14S 3+25E	25	166	25	488	.7	60	40	2006	4.54	8	<8	<2	2	29	2.9	<3	<3	90	.31	.193	10	29	.55	202	.08	<3	2.92	.01	.11	2	4.5
CR L14S 3+50E	35	121	37	623	.4	62	36	2470	4.76	10	<8	<2	<2	37	3.7	<3	<3	92	.38	.118	15	32	.54	172	.05	<3	2.69	.01	.09	2	7.1
CR L14S 3+75E	36	88	40	477	.7	28	23	2282	4.01	11	<8	<2	<2	19	2.8	<3	3	71	.18	.128	20	24	.51	162	.02	<3	2.59	.01	.11	2	5.9
CR L14S 4+00E	37	69	31	342	.5	17	14	2614	3.73	13	<8	<2	<2	15	2.0	<3	<3	65	.17	.146	14	22	.34	203	.02	<3	2.20	.01	.12	<2	16.8
CR L16S 0+00E	3	53	13	76	.6	13	8	259	2.90	6	<8	<2	3	9	<.5	<3	<3	67	.07	.087	6	20	.46	76	.14	<3	4.32	.01	.06	<2	1.3
CR L16S 0+25E	11	96	18	135	.3	24	16	575	3.87	12	<8	<2	3	15	.5	<3	<3	86	.12	.150	8	26	.71	94	.13	<3	4.04	.01	.08	2	2.2
STANDARD DS3	9	125	36	156	.3	36	12	816	3.26	30	<8	<2	4	27	5.8	5	6	79	.55	.096	19	185	.64	149	.09	<3	1.74	.03	.16	4	21.6

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	<3	43	<.3	6	4	554	1.64	<2	<8	<2	5	65	<.5	<3	<3	41	.51	.107	8	17	.62	223	.11	<3	.88	.06	.51	2	<.2
CR L16S 0+50E	10	51	13	115	<.3	17	13	956	3.35	7	<8	<2	2	15	<.5	<3	<3	94	.13	.104	7	22	.61	82	.13	<3	2.84	.01	.10	2	6.5
CR L16S 0+75E	7	58	15	128	<.3	18	12	593	3.86	7	<8	<2	2	14	<.5	<3	<3	97	.13	.108	7	26	.66	79	.14	<3	3.55	.01	.10	2	1.6
CR L16S 1+00E	6	74	15	127	<.3	18	15	990	3.47	12	<8	<2	2	16	<.5	<3	<3	96	.15	.208	7	27	.72	72	.11	<3	3.38	.01	.11	2	5.8
CR L16S 1+25E	10	97	15	158	.3	28	18	923	4.01	12	<8	<2	2	19	.5	<3	<3	98	.18	.147	8	32	.71	91	.11	<3	3.73	.01	.10	4	2.4
CR L16S 1+50E	19	114	17	142	.5	23	14	1049	4.64	16	<8	<2	2	17	<.5	<3	<3	109	.16	.213	6	36	.74	74	.12	<3	3.90	.01	.09	8	2.5
CR L16S 1+75E	21	83	24	224	<.3	38	15	1314	3.44	13	<8	<2	3	17	.9	<3	<3	98	.17	.164	8	29	.54	74	.12	<3	3.87	.01	.09	4	24.4
CR L16S 2+00E	52	97	16	135	.4	27	29	1780	3.65	7	<8	<2	<2	21	.7	<3	<3	82	.18	.175	10	25	.47	80	.10	<3	3.02	.01	.11	6	2.1
CR L16S 2+25E	23	113	23	202	.7	25	21	1004	4.07	13	<8	<2	2	10	<.5	<3	<3	81	.08	.173	9	29	.51	65	.10	<3	3.82	.01	.07	3	5.0
CR L16S 2+50E	39	130	28	127	.8	15	12	995	4.10	11	<8	<2	<2	9	.5	<3	3	87	.07	.155	8	24	.55	47	.07	<3	3.11	.01	.07	6	8.5
CR L16S 2+75E	16	53	15	117	.3	16	8	1086	3.50	6	<8	<2	2	8	<.5	<3	<3	89	.07	.106	8	27	.39	67	.11	<3	2.95	.01	.07	3	4.2
CR L16S 3+00E	17	73	14	237	.4	31	15	947	3.60	10	<8	<2	3	9	.5	<3	<3	112	.11	.147	10	42	.44	69	.08	<3	3.86	.01	.06	2	26.1
CR L16S 3+25E	18	28	20	124	.3	11	8	772	4.83	11	<8	<2	2	15	<.5	<3	<3	99	.10	.238	9	33	.31	79	.11	<3	2.58	.01	.08	<2	3.3
CR L16S 3+50E	89	120	10	134	.4	25	13	619	4.63	7	<8	<2	3	14	<.5	<3	<3	89	.10	.182	10	37	.39	71	.11	<3	4.72	.01	.07	<2	3.8
CR L16S 3+75E	43	58	10	72	.5	11	4	407	3.60	6	<8	<2	3	11	<.5	<3	<3	76	.08	.175	6	24	.22	55	.12	<3	4.26	.01	.06	3	1.9
CR L16S 4+00E	52	112	12	66	.3	13	6	299	5.28	6	<8	<2	4	10	<.5	<3	<3	103	.06	.154	9	39	.30	54	.14	<3	4.01	.01	.07	2	5.7
CR L18S 0+00E	2	27	17	124	.3	11	11	760	3.28	11	<8	<2	2	11	<.5	<3	<3	72	.09	.161	7	18	.53	99	.12	<3	3.36	.01	.11	<2	5.1
CR L18S 0+25E	2	52	17	145	.4	13	15	602	3.17	10	<8	<2	3	15	<.5	<3	<3	81	.15	.143	7	19	.57	82	.14	<3	4.03	.01	.10	<2	2.4
RE CR L18S 0+25E	2	49	17	140	.4	13	14	635	3.05	10	<8	<2	3	14	<.5	<3	<3	84	.14	.142	7	19	.55	79	.14	<3	4.01	.01	.12	<2	2.3
CR L18S 0+50E	3	72	25	186	.6	16	15	639	3.48	15	<8	<2	3	17	.5	<3	<3	93	.14	.172	7	20	.75	91	.14	<3	4.34	.01	.14	2	4.0
CR L18S 0+75E	4	62	21	237	.3	18	19	1011	3.32	16	<8	<2	3	17	1.1	<3	<3	82	.18	.160	11	20	.63	132	.15	<3	3.99	.02	.12	3	1.9
CR L18S 1+00E	5	94	19	177	.3	22	22	1276	3.61	20	<8	<2	2	16	.6	<3	<3	87	.16	.236	10	23	.68	98	.11	<3	3.95	.01	.12	5	5.1
CR L18S 1+25E	7	96	16	156	.3	24	19	626	3.51	14	<8	<2	3	14	<.5	<3	<3	80	.13	.140	9	23	.60	91	.13	<3	3.91	.01	.11	7	5.1
CR L18S 1+50E	8	66	19	160	.3	23	19	1054	3.63	21	<8	<2	2	17	<.5	<3	<3	84	.15	.199	8	27	.55	89	.12	<3	3.13	.01	.10	5	3.2
CR L18S 1+75E	8	81	23	138	<.3	28	17	736	3.57	15	<8	<2	3	19	<.5	<3	<3	82	.15	.218	13	30	.59	121	.14	<3	3.75	.01	.13	6	3.2
CR L18S 2+00E	9	91	24	176	.3	24	17	1272	3.95	41	<8	<2	2	14	<.5	<3	<3	83	.10	.149	11	26	.62	119	.09	<3	3.05	.01	.10	6	2.0
CR L18S 2+25E	9	85	17	127	.3	22	17	853	3.25	23	<8	<2	3	11	<.5	<3	<3	67	.09	.190	8	21	.46	67	.13	<3	4.03	.01	.08	3	4.8
CR L18S 2+50E	19	87	18	136	.3	23	16	1152	3.63	15	<8	<2	3	14	<.5	<3	<3	75	.09	.184	10	26	.44	68	.12	<3	3.96	.01	.08	4	3.9
CR L18S 2+75E	13	93	26	175	.3	31	21	1946	3.40	10	<8	<2	2	15	.7	<3	<3	77	.10	.195	11	28	.53	76	.10	<3	3.61	.01	.09	3	3.4
CR L18S 3+00E	9	67	20	137	.4	22	12	529	3.14	9	<8	<2	3	11	<.5	<3	<3	76	.09	.121	7	24	.49	76	.12	<3	3.76	.01	.07	3	4.8
CR L18S 3+25E	14	98	15	317	.3	38	29	1270	3.64	12	<8	<2	3	12	.9	<3	<3	91	.06	.166	10	28	.37	70	.13	<3	4.48	.01	.07	5	3.1
CR L18S 3+50E	10	44	21	220	.4	23	10	917	3.60	23	<8	<2	3	10	.6	<3	<3	100	.07	.147	8	31	.42	77	.11	<3	2.85	.01	.08	5	10.1
CR L18S 3+75E	10	54	12	110	.3	18	10	582	2.69	7	<8	<2	4	7	<.5	<3	<3	67	.05	.206	8	19	.25	29	.15	<3	5.18	.01	.06	2	5.6
CR L18S 4+00E	10	60	20	181	.3	21	11	722	2.90	10	<8	<2	2	8	<.5	<3	<3	60	.06	.159	13	20	.39	65	.08	<3	3.27	.01	.10	3	7.4
STANDARD DS3	9	124	35	159	.3	36	11	799	2.95	33	<8	<2	4	27	5.8	5	6	75	.53	.100	18	171	.61	140	.08	<3	1.72	.03	.16	4	19.7

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	<3	40	<.3	6	4	501	1.67	<2	<8	<2	5	58	<.5	<3	<3	38	.52	.090	7	16	.53	201	.12	<3	.80	.06	.42	2	.4
CR L20S 0+00E	5	69	43	145	.3	12	21	2000	3.58	9	<8	<2	<2	59	.6	<3	<3	101	.83	.159	9	16	.95	81	.09	<3	2.94	.03	.19	<2	2.0
CR L20S 0+25E	7	75	34	150	.3	13	24	2522	3.54	16	<8	<2	<2	50	.7	<3	<3	87	.72	.138	8	16	.70	96	.07	3	3.28	.02	.12	2	3.8
CR L20S 0+50E	3	39	27	172	<.3	12	17	1885	3.29	11	<8	<2	2	19	.7	<3	<3	81	.20	.199	6	16	.48	112	.13	<3	3.22	.01	.09	<2	2.1
CR L20S 0+75E	3	56	21	197	.4	15	20	1561	3.40	9	<8	<2	2	19	1.1	<3	<3	90	.17	.175	8	18	.62	110	.13	<3	3.99	.01	.11	<2	1.3
CR L20S 1+00E	5	62	23	264	.4	23	20	1638	3.68	10	<8	<2	3	17	.9	<3	<3	98	.15	.178	9	25	.72	121	.16	<3	4.01	.01	.11	<2	1.3
CR L20S 1+25E	7	66	17	280	.3	26	21	1720	3.39	14	<8	<2	<2	32	1.3	<3	<3	88	.36	.188	10	24	.70	108	.11	<3	3.53	.01	.12	<2	1.6
CR L20S 1+50E	12	71	24	273	<.3	27	24	1758	3.64	19	<8	<2	<2	25	1.2	<3	<3	95	.33	.212	12	28	.71	58	.07	<3	3.40	.01	.13	<2	6.0
CR L20S 1+75E	9	69	42	304	<.3	28	26	2025	3.46	22	<8	<2	<2	50	2.3	<3	<3	89	.80	.158	12	29	.74	75	.08	<3	2.45	.02	.13	2	3.1
CR L20S 2+00E	13	79	22	411	.3	39	29	1022	4.34	25	<8	<2	3	35	1.5	<3	<3	103	.49	.112	13	37	.80	83	.14	<3	3.50	.01	.09	3	4.9
CR L20S 2+25E	10	66	47	326	<.3	31	30	1850	3.47	24	<8	<2	<2	65	4.1	<3	<3	80	1.08	.195	10	35	.69	96	.05	3	2.21	.02	.10	3	24.6
CR L20S 2+50E	14	75	19	435	.3	35	22	1362	3.72	22	<8	<2	<2	50	3.2	<3	<3	91	.76	.110	12	44	.67	70	.08	<3	2.43	.02	.07	3	5.0
CR L20S 2+75E	12	91	24	237	.3	31	21	1428	3.75	18	<8	<2	<2	15	.7	<3	<3	82	.18	.214	10	29	.54	72	.07	<3	3.13	.01	.07	2	9.0
CR L20S 3+00E	5	63	14	237	.4	28	13	638	3.67	13	<8	<2	3	12	.5	<3	<3	90	.12	.226	10	29	.55	97	.13	<3	3.55	.01	.08	2	3.5
RE CR L20S 3+00E	5	63	14	235	.4	28	13	650	3.58	13	<8	<2	3	12	.5	<3	<3	90	.15	.229	10	29	.53	97	.12	<3	3.48	.01	.08	2	3.8
CR L20S 3+25E	6	80	14	153	.3	24	17	1034	3.39	10	<8	<2	<2	13	<.5	<3	<3	83	.14	.195	10	29	.61	75	.11	<3	3.56	.01	.11	2	13.0
CR L20S 3+50E	5	102	33	180	<.3	32	22	1705	3.50	11	<8	<2	<2	17	.7	<3	<3	95	.15	.180	11	35	.73	100	.10	<3	3.36	.01	.11	2	38.3
CR L20S 3+75E	7	135	22	130	.3	25	22	1096	4.14	9	<8	<2	2	14	<.5	<3	<3	80	.10	.211	9	24	.54	74	.11	<3	3.55	.01	.09	11	6.0
CR L20S 4+00E	7	96	17	161	.3	26	18	761	3.82	9	<8	<2	2	16	<.5	<3	<3	86	.11	.187	10	28	.60	88	.14	<3	3.91	.01	.11	5	13.6
PO L20S 26+00W	<1	38	15	91	<.3	25	15	693	2.71	6	<8	<2	3	37	<.5	<3	<3	58	.38	.235	8	41	.62	185	.16	3	3.43	.02	.09	<2	3.0
PO L20S 25+50W	<1	43	18	102	<.3	28	15	845	2.69	8	<8	<2	4	38	.6	<3	<3	60	.45	.223	13	49	.68	185	.14	<3	3.23	.02	.10	<2	2.8
PO L20S 25+00W	<1	41	21	144	.3	25	13	567	2.73	7	<8	<2	4	28	<.5	<3	<3	54	.29	.262	9	42	.59	117	.15	<3	4.10	.01	.07	<2	15.3
PO L20S 24+50W	1	24	21	72	<.3	19	12	1805	2.46	6	<8	<2	2	27	<.5	<3	<3	48	.25	.158	8	37	.52	179	.13	<3	2.24	.01	.07	<2	2.4
PO L20S 24+00W	1	36	14	76	<.3	22	12	433	2.75	6	<8	<2	3	36	<.5	<3	<3	54	.33	.215	11	40	.54	101	.15	<3	3.30	.01	.06	<2	4.4
PO L20S 23+50W	<1	64	14	83	<.3	26	15	489	2.87	7	<8	<2	4	38	<.5	<3	<3	60	.35	.102	10	46	.71	109	.16	<3	3.17	.01	.07	<2	12.0
PO L20S 23+00W	1	36	16	98	<.3	23	16	2432	2.86	6	<8	<2	3	29	<.5	<3	<3	55	.26	.254	8	36	.56	204	.13	<3	2.77	.01	.07	<2	.8
PO L20S 22+50W	1	36	27	115	<.3	22	15	4202	2.55	8	<8	<2	2	66	1.0	<3	<3	49	.54	.316	7	30	.53	531	.14	3	2.90	.02	.11	<2	2.7
PO L20S 22+00W	<1	129	22	106	<.3	31	21	1661	3.14	6	<8	<2	3	59	.6	<3	<3	71	.50	.142	10	53	1.14	197	.16	<3	2.92	.01	.09	<2	3.7
PO L20S 21+50W	1	48	15	87	<.3	28	15	1228	2.88	7	<8	<2	3	44	<.5	<3	<3	61	.33	.135	7	41	.74	151	.13	3	2.76	.01	.09	<2	7.8
PO L20S 21+00W	1	63	9	76	<.3	34	19	762	3.18	8	<8	<2	2	53	<.5	<3	<3	67	.49	.118	9	41	1.03	145	.11	<3	2.08	.01	.11	<2	10.1
PO L20S 20+50W	1	83	14	67	<.3	54	19	1455	3.22	16	<8	<2	3	51	<.5	<3	<3	63	.52	.243	9	49	.92	207	.12	3	2.86	.01	.10	<2	5.8
PO L20S 20+00W	1	63	20	96	.3	21	16	3521	3.54	11	<8	<2	4	41	.7	<3	<3	50	.51	.322	16	28	.59	323	.11	3	3.16	.01	.09	2	114.7
PO L20S 19+50W	1	54	11	61	.3	44	18	738	3.01	6	<8	<2	2	45	<.5	<3	<3	69	.36	.058	9	62	.82	175	.14	<3	2.48	.01	.08	<2	17.0
PO L20S 19+00W	1	22	15	67	<.3	22	12	863	2.59	6	<8	<2	3	35	<.5	<3	<3	46	.26	.142	7	26	.41	192	.15	<3	2.75	.01	.08	<2	7.1
STANDARD DS3	9	124	36	153	.3	36	12	752	2.90	30	<8	<2	4	26	5.3	5	5	77	.55	.096	18	174	.59	142	.09	<3	1.76	.03	.14	4	20.5

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	<3	39	<.3	5	4	497	1.71	<2	<8	<2	5	59	<.5	<3	<3	37	.41	.102	8	17	.48	210	.13	<3	.78	.06	.45	2	<.2
PO L20S 18+50W	<1	37	12	61	<.3	20	16	639	2.85	10	<8	<2	3	53	<.5	<3	<3	56	.37	.228	9	32	.54	188	.14	<3	2.63	.01	.09	<2	97.0
PO L20S 18+00W	1	26	12	71	<.3	17	12	964	2.61	8	<8	<2	3	49	<.5	<3	<3	46	.33	.343	9	27	.44	226	.13	3	2.54	.01	.09	<2	14.2
PO L20S 17+50W	1	34	21	66	<.3	17	14	1210	2.69	9	<8	<2	3	39	<.5	<3	<3	53	.30	.199	11	29	.47	183	.14	<3	2.86	.01	.09	<2	9.5
PO L20S 17+00W	1	106	13	78	<.3	69	26	1274	3.49	24	<8	<2	2	48	.5	<3	<3	70	.36	.135	11	70	.93	190	.13	<3	2.30	.01	.14	<2	28.0
PO L20S 16+50W	1	27	16	67	<.3	15	15	1219	2.99	9	<8	<2	2	47	<.5	<3	<3	58	.26	.269	7	32	.53	192	.11	<3	1.81	.01	.07	<2	27.7
PO L20S 16+00W	1	94	16	70	<.3	23	17	653	3.21	16	<8	<2	3	43	<.5	<3	<3	61	.34	.308	10	31	.74	136	.14	4	3.43	.01	.12	<2	284.0
PO L20S 15+50W	1	54	11	56	<.3	29	16	623	2.97	16	<8	<2	2	59	<.5	<3	<3	61	.48	.143	11	51	.90	168	.10	<3	2.07	.01	.10	<2	22.3
PO L20S 15+00W	1	47	7	62	<.3	15	15	525	3.33	7	<8	<2	2	55	<.5	<3	<3	66	.35	.155	7	33	.92	110	.09	<3	1.78	.01	.09	<2	27.3
PO L22S 21+50W	1	37	22	105	<.3	64	22	2211	3.36	18	<8	<2	2	47	.7	<3	<3	67	.33	.196	8	72	.97	225	.15	<3	2.44	.01	.13	<2	43.9
PO L22S 21+00W	1	29	31	107	<.3	29	13	1346	2.74	22	<8	<2	2	42	1.1	<3	<3	44	.36	.426	9	27	.33	190	.13	<3	3.42	.01	.08	<2	8.7
PO L22S 20+50W	1	30	16	80	<.3	21	13	1207	2.77	10	<8	<2	3	30	<.5	<3	<3	51	.21	.278	9	33	.45	191	.15	<3	3.04	.01	.08	<2	13.3
PO L22S 20+00W	1	26	13	89	<.3	21	13	1072	2.59	7	<8	<2	3	36	<.5	<3	<3	51	.34	.207	9	32	.46	275	.15	3	2.93	.01	.09	<2	5.6
PO L22S 19+50W	1	27	19	124	<.3	21	13	1795	2.82	10	<8	<2	3	33	.6	<3	<3	50	.30	.303	8	27	.44	275	.17	4	3.33	.01	.09	<2	5.8
PO L22S 19+00W	1	36	13	79	<.3	23	15	622	3.16	13	<8	<2	3	42	<.5	<3	<3	59	.32	.292	8	35	.56	182	.16	3	2.71	.01	.11	<2	8.5
PO L22S 18+50W	5	35	12	47	.3	39	19	1403	2.59	30	<8	<2	4	86	<.5	<3	<3	40	.74	.056	15	63	.57	154	.17	<3	3.77	.03	.08	<2	19.2
PO L22S 18+00W	1	25	64	189	<.3	20	15	4186	2.96	9	<8	<2	3	43	2.1	<3	<3	50	.33	.234	10	30	.32	381	.16	<3	2.36	.01	.11	<2	22.3
PO L22S 17+50W	1	53	14	82	<.3	28	19	1820	3.26	17	<8	<2	3	48	.6	<3	<3	60	.33	.288	9	44	.58	254	.13	<3	2.89	.01	.09	<2	48.2
PO L22S 17+00W	1	31	27	84	<.3	19	19	2493	3.24	13	<8	<2	2	67	.7	<3	<3	54	.53	.297	8	34	.43	236	.12	3	1.99	.01	.08	<2	177.0
RE PO L22S 17+00W	1	29	27	83	<.3	19	18	2516	3.10	13	<8	<2	2	67	.6	<3	<3	53	.55	.299	7	32	.41	232	.11	<3	1.93	.01	.08	<2	54.3
PO L22S 16+50W	1	37	16	80	<.3	26	18	1113	3.06	14	<8	<2	3	37	.5	<3	<3	56	.24	.214	8	34	.51	177	.14	<3	2.72	.01	.09	<2	41.2
PO L22S 16+00W	1	27	12	67	<.3	14	13	2097	2.67	8	<8	<2	2	59	<.5	<3	<3	43	.40	.367	10	26	.43	338	.10	<3	2.32	.01	.10	<2	83.6
PO L22S 15+50W	1	43	9	64	<.3	20	14	732	2.94	7	<8	<2	2	50	<.5	<3	<3	59	.34	.150	10	32	.66	138	.12	<3	2.40	.01	.13	<2	26.3
PO L24S 22+00W	1	75	11	68	<.3	33	18	335	3.02	12	<8	<2	4	31	<.5	<3	<3	62	.28	.103	10	58	.81	90	.13	<3	2.60	.01	.09	<2	13.3
PO L24S 21+50W	3	22	22	43	.3	39	12	386	2.88	11	<8	<2	2	36	<.5	<3	<3	56	.32	.062	9	46	.35	104	.16	<3	3.03	.01	.07	<2	8.3
PO L24S 21+00W	1	41	11	97	<.3	30	19	822	3.77	17	<8	<2	3	26	<.5	<3	<3	108	.28	.295	7	47	1.26	114	.16	<3	4.13	.01	.13	<2	7.9
PO L24S 20+50W	4	140	18	57	.4	30	15	1311	3.15	36	10	<2	3	75	<.5	<3	<3	50	.79	.089	13	54	.39	123	.16	<3	3.45	.02	.06	2	44.8
PO L24S 20+00W	1	28	16	89	<.3	24	16	537	3.04	13	<8	<2	4	31	<.5	<3	<3	53	.25	.340	8	34	.39	131	.16	<3	3.70	.01	.07	<2	11.6
PO L24S 19+50W	1	30	14	78	<.3	23	13	341	2.80	8	<8	<2	4	29	<.5	<3	<3	46	.23	.180	7	31	.39	143	.17	3	4.08	.01	.09	<2	9.0
PO L24S 19+00W	1	22	18	61	<.3	21	12	584	2.97	17	<8	<2	2	38	<.5	<3	<3	56	.35	.098	7	42	.42	115	.16	<3	2.65	.01	.08	<2	70.4
PO L24S 18+50W	1	28	13	72	<.3	17	13	493	2.63	7	<8	<2	3	38	<.5	<3	<3	45	.31	.218	10	30	.43	181	.12	<3	2.48	.01	.07	<2	24.7
PO L24S 18+00W	1	26	29	108	<.3	40	18	3191	3.03	10	<8	<2	2	62	1.2	<3	<3	51	.55	.349	13	40	.59	406	.12	<3	2.63	.02	.12	<2	226.9
PO L24S 17+50W	1	35	14	79	<.3	38	19	943	3.44	7	<8	<2	5	51	<.5	<3	<3	65	.50	.285	22	24	.85	300	.20	<3	4.44	.03	.15	<2	7.0
PO L24S 17+00W	1	47	17	81	<.3	50	26	2462	3.79	6	<8	<2	5	86	.7	<3	<3	84	.96	.253	28	28	1.27	595	.21	4	3.72	.03	.22	<2	24.0
STANDARD DS3	9	125	36	156	.3	35	13	798	3.17	32	<8	<2	4	27	5.8	5	6	85	.53	.099	20	188	.55	148	.09	<3	1.71	.03	.18	4	22.1

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	<3	40	<.3	7	4	518	1.68	<2	<8	<2	5	60	<.5	<3	<3	38	.48	.101	7	20	.51	210	.11	<3	.80	.05	.55	2	.3
PO L24S 16+50W	1	34	14	76	<.3	21	15	2388	2.80	8	<8	<2	2	37	.5	<3	<3	52	.31	.253	11	31	.51	227	.11	<3	2.88	.01	.10	<2	68.6
PO L24S 16+00W	1	45	10	72	.3	22	15	753	3.10	8	<8	<2	2	39	<.5	<3	<3	54	.35	.150	11	36	.72	145	.10	<3	2.45	.01	.12	<2	31.8
PO L24S 15+50W	1	43	10	62	<.3	18	13	1032	2.78	6	<8	<2	3	33	<.5	<3	<3	49	.24	.159	14	29	.60	192	.12	<3	3.06	.01	.11	<2	51.5
PO L24S 15+00W	1	80	10	62	<.3	23	19	643	3.34	13	<8	<2	3	43	<.5	<3	<3	64	.35	.094	9	46	.92	103	.11	<3	2.11	.01	.16	<2	65.7
PO L26S 21+00W	1	31	12	84	<.3	31	16	436	2.80	8	<8	<2	4	29	<.5	<3	<3	51	.27	.148	9	45	.53	170	.13	<3	3.64	.01	.10	<2	9.7
PO L26S 20+50W	5	35	10	45	<.3	36	24	1333	3.04	12	<8	<2	2	60	<.5	<3	<3	60	.51	.030	10	62	.75	186	.12	<3	2.31	.01	.11	<2	19.4
PO L26S 20+00W	1	26	13	66	<.3	29	16	296	2.92	11	<8	<2	3	30	<.5	<3	<3	59	.21	.055	10	48	.50	122	.14	<3	2.95	.01	.08	<2	25.2
PO L26S 19+50W	1	38	13	99	<.3	28	16	865	2.89	12	<8	<2	4	30	<.5	<3	<3	53	.25	.215	10	40	.66	162	.14	<3	3.24	.01	.11	<2	17.1
PO L26S 19+00W	1	34	12	95	<.3	37	20	1929	3.21	6	<8	<2	4	41	<.5	<3	<3	64	.39	.239	18	34	.80	235	.18	<3	3.66	.02	.13	<2	6.4
PO L26S 18+00W	1	36	32	115	<.3	20	22	4178	3.24	12	<8	<2	3	55	1.3	<3	<3	46	.47	.359	17	27	.59	404	.12	3	3.42	.01	.17	<2	78.4
PO L26S 17+50W	1	40	14	87	<.3	21	15	2131	3.06	9	<8	<2	2	49	<.5	<3	<3	52	.35	.307	13	34	.57	205	.11	<3	2.76	.01	.11	<2	29.6
PO L26S 17+00W	1	28	21	92	<.3	20	14	2853	2.97	8	<8	<2	2	40	.7	<3	<3	53	.34	.211	13	33	.54	322	.12	<3	2.79	.01	.11	<2	27.7
PO L26S 16+50W	1	25	30	88	<.3	16	10	5152	2.52	7	<8	<2	2	48	1.0	<3	<3	40	.44	.319	12	22	.40	609	.11	<3	3.13	.02	.13	<2	12.9
PO L26S 16+00W	1	36	13	63	<.3	20	14	1592	2.91	7	<8	<2	3	32	<.5	<3	<3	56	.24	.172	12	30	.52	216	.14	<3	2.94	.01	.09	<2	21.9
PO L26S 15+50W	1	33	12	66	<.3	19	13	963	2.61	8	<8	<2	3	24	<.5	<3	<3	48	.19	.237	12	26	.45	214	.14	<3	3.39	.01	.08	<2	31.0
PO L26S 15+00W	1	31	15	81	<.3	19	15	1729	2.89	9	<8	<2	3	38	.5	<3	<3	53	.29	.223	9	28	.52	218	.13	<3	2.80	.01	.10	<2	11.1
PO L28S 30+00W	1	32	15	185	.5	29	14	901	2.98	7	<8	<2	3	22	1.2	<3	<3	61	.19	.224	10	39	.57	199	.13	<3	3.25	.01	.12	<2	2.4
PO L28S 29+50W	1	21	16	121	<.3	24	14	940	2.98	6	<8	<2	2	27	.5	<3	<3	65	.19	.161	7	37	.52	196	.13	<3	2.84	.01	.10	<2	5.2
PO L28S 29+00W	1	33	13	111	<.3	28	15	699	3.07	5	<8	<2	2	36	.5	<3	<3	84	.31	.093	7	56	.80	149	.14	<3	2.50	.01	.15	<2	10.4
RE PO L28S 29+00W	1	32	13	106	<.3	28	14	654	2.97	5	<8	<2	2	32	<.5	<3	<3	77	.24	.087	6	51	.82	142	.12	<3	2.36	.01	.14	<2	1.1
PO L28S 28+50W	1	40	15	107	<.3	34	15	375	2.98	6	<8	<2	2	29	.5	<3	<3	81	.22	.083	6	55	.75	148	.15	<3	2.71	.01	.14	<2	312.9
PO L28S 28+00W	1	23	11	145	.3	29	12	791	2.43	5	<8	<2	3	27	.9	<3	<3	56	.20	.262	7	40	.54	142	.12	<3	2.53	.02	.14	<2	2.9
PO L28S 27+50W	2	70	23	173	.3	39	20	1019	3.60	23	<8	<2	3	36	1.4	<3	<3	95	.41	.160	12	75	1.15	157	.12	<3	2.51	.01	.21	<2	5.2
PO L28S 27+00W	1	39	15	80	<.3	25	13	520	2.87	7	<8	<2	3	31	<.5	<3	<3	76	.34	.102	12	51	.80	113	.11	<3	1.84	.01	.21	<2	9.3
PO L28S 26+50W	1	31	12	166	.3	37	15	362	2.87	4	<8	<2	3	25	1.2	<3	<3	64	.22	.176	8	48	.72	168	.15	<3	3.35	.01	.14	<2	6.0
PO L28S 26+00W	1	45	14	103	.3	31	15	626	3.00	5	<8	<2	2	39	.5	<3	<3	82	.36	.104	13	65	1.19	150	.14	<3	2.19	.01	.31	<2	4.2
PO L28S 25+50W	1	28	17	152	<.3	25	13	746	2.49	7	<8	<2	3	24	.8	<3	<3	64	.23	.316	9	43	.68	161	.13	<3	2.73	.01	.15	<2	3.7
PO L28S 25+00W	1	27	15	116	.3	23	12	588	2.61	5	<8	<2	3	21	.7	<3	<3	65	.19	.225	8	45	.64	128	.11	<3	2.51	.01	.12	<2	2.1
PO L28S 20+00W	1	26	18	81	<.3	24	13	792	2.74	9	<8	<2	3	15	<.5	<3	<3	50	.10	.235	5	39	.46	171	.17	<3	4.17	.01	.06	<2	27.5
PO L28S 19+50W	1	37	12	44	<.3	24	12	231	2.66	71	<8	<2	2	78	<.5	<3	<3	46	1.22	.064	27	132	.56	132	.13	<3	3.46	.03	.07	<2	19.7
PO L28S 19+00W	1	16	15	108	<.3	16	10	1663	2.50	13	<8	<2	3	24	<.5	<3	<3	36	.20	.522	8	20	.23	193	.16	<3	4.16	.01	.07	<2	5.8
PO L28S 18+50W	<1	22	17	217	<.3	23	11	742	2.59	6	<8	<2	4	71	.5	<3	<3	37	.55	.702	11	31	.50	597	.13	<3	3.21	.01	.21	<2	11.0
PO L28S 18+00W	<1	30	15	103	<.3	19	13	2172	2.80	5	<8	<2	3	35	.9	<3	<3	49	.28	.232	14	25	.44	366	.15	<3	3.66	.01	.10	<2	80.5
STANDARD DS3	9	120	36	155	.3	36	12	770	3.12	30	<8	<2	4	27	5.7	5	6	73	.53	.099	18	186	.61	142	.08	<3	1.68	.03	.17	4	23.5

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	<3	41	<.3	7	4	491	1.49	<2	<8	<2	6	64	<.5	<3	<3	37	.50	.107	8	19	.55	210	.12	<3	.80	.05	.44	2	<.2
PO L28S 17+50W	1	29	14	61	<.3	20	12	1374	2.31	5	<8	<2	3	32	<.5	<3	<3	46	.32	.133	11	27	.54	228	.14	<3	2.65	.01	.08	<2	19.8
PO L28S 17+00W	1	28	15	80	<.3	16	11	2103	2.33	7	<8	<2	3	55	<.5	<3	<3	40	.66	.287	14	23	.46	350	.12	3	3.32	.01	.10	<2	20.3
PO L28S 16+50W	1	23	14	88	<.3	17	11	1760	2.57	7	<8	<2	3	55	<.5	<3	<3	38	.57	.353	11	26	.51	304	.10	3	2.88	.01	.13	<2	15.4
PO L28S 16+00W	1	34	14	71	<.3	25	14	1264	2.94	10	<8	<2	2	48	<.5	<3	<3	44	.40	.242	11	34	.60	227	.08	<3	2.48	.01	.12	<2	19.7
PO L28S 15+50W	1	28	10	62	<.3	18	12	822	2.44	7	<8	<2	2	35	<.5	<3	<3	38	.37	.189	9	25	.50	175	.08	<3	2.00	.01	.09	<2	21.1
PO L28S 15+00W	1	19	11	78	<.3	19	12	1932	2.41	3	<8	<2	2	45	<.5	<3	<3	38	.45	.184	10	26	.42	313	.11	<3	2.59	.01	.09	<2	9.9
PO L30S 30+00W	1	50	22	167	.3	26	15	666	3.20	11	<8	<2	3	25	1.3	<3	<3	64	.29	.273	10	46	.68	177	.13	<3	3.15	.01	.12	<2	1.6
PO L30S 29+50W	3	50	28	222	<.3	39	18	868	2.98	34	<8	<2	2	61	2.7	<3	<3	72	.93	.166	13	67	1.06	140	.08	<3	1.85	.01	.14	2	5.3
PO L30S 29+00W	1	87	15	103	.3	25	16	1089	3.46	8	<8	<2	4	24	.5	<3	<3	54	.26	.314	11	39	.62	174	.11	<3	3.53	.01	.09	<2	2.5
PO L30S 28+50W	1	30	15	93	<.3	22	12	571	2.56	6	<8	<2	3	24	.5	<3	<3	66	.23	.189	9	42	.62	133	.12	<3	2.33	.01	.09	<2	1.9
PO L30S 28+00W	1	17	13	89	<.3	19	12	560	2.55	5	<8	<2	3	25	<.5	<3	<3	60	.24	.146	6	35	.55	126	.13	<3	2.32	.01	.09	<2	1.3
PO L30S 27+50W	1	22	18	155	<.3	23	14	534	2.79	10	<8	<2	4	21	.7	<3	<3	55	.17	.358	7	33	.49	137	.14	<3	3.54	.01	.09	<2	<.2
PO L30S 27+00W	1	29	19	153	.3	26	14	361	2.64	14	<8	<2	3	23	.9	<3	<3	53	.29	.176	7	32	.48	154	.14	<3	3.36	.01	.08	<2	1.3
PO L30S 26+50W	1	24	55	141	<.3	18	13	4551	2.42	8	<8	<2	2	37	1.3	<3	<3	51	.45	.115	9	32	.35	411	.12	<3	2.03	.01	.11	<2	1.1
PO L30S 26+00W	1	25	25	143	<.3	22	14	597	3.42	12	<8	<2	4	24	.6	<3	<3	57	.25	.178	11	31	.47	174	.12	<3	3.23	.01	.09	<2	194.3
PO L30S 25+00W	1	39	20	111	<.3	24	15	992	2.88	14	<8	<2	3	31	<.5	<3	<3	61	.37	.152	8	37	.51	198	.14	<3	3.09	.01	.07	<2	1.7
PO L30S 24+50W	1	30	19	108	<.3	22	12	1043	2.38	9	<8	<2	4	16	.5	<3	<3	51	.19	.217	12	28	.39	159	.17	<3	4.08	.01	.07	<2	1.2
PO L30S 24+00W	1	49	20	130	.4	24	14	466	2.60	13	<8	<2	4	17	.5	<3	<3	54	.14	.139	14	32	.54	155	.18	<3	3.65	.01	.08	<2	249.8
PO L32S 30+00W	1	26	26	90	<.3	18	12	1322	2.81	24	<8	<2	3	23	<.5	<3	<3	55	.20	.231	7	29	.45	249	.13	<3	2.70	.01	.08	<2	.7
PO L32S 29+50W	3	40	24	128	.4	43	31	2058	4.67	46	<8	<2	2	10	.5	<3	<3	65	.07	.202	7	41	.47	156	.12	<3	2.41	.01	.06	<2	1.0
RE PO L32S 29+50W	3	41	24	121	.4	43	31	1964	4.13	46	<8	<2	2	10	.5	<3	<3	69	.07	.206	7	40	.48	159	.12	<3	2.47	.01	.06	<2	1.2
PO L32S 29+00W	2	45	38	161	<.3	69	17	2670	2.99	71	<8	<2	4	38	.9	<3	<3	63	.36	.172	13	119	.79	230	.17	<3	3.44	.02	.11	<2	1.4
PO L32S 28+50W	2	24	18	91	<.3	17	15	1087	2.95	6	<8	<2	2	14	<.5	<3	<3	57	.12	.147	14	31	.53	100	.14	<3	2.30	.01	.09	<2	3.8
PO L32S 28+00W	1	25	21	118	<.3	18	12	2803	2.83	5	<8	<2	3	14	.5	<3	<3	51	.14	.163	10	25	.34	205	.17	<3	3.22	.01	.06	<2	3.7
PO L32S 27+50W	1	25	22	98	<.3	18	12	932	2.78	6	<8	<2	2	14	.5	<3	<3	56	.14	.180	8	32	.46	150	.13	<3	3.18	.01	.08	<2	1.7
PO L32S 27+00W	1	30	24	102	<.3	21	12	1992	3.03	7	<8	<2	2	29	.6	<3	<3	60	.30	.159	10	36	.61	213	.13	<3	2.93	.01	.11	<2	3.1
PO L32S 26+50W	1	19	21	90	<.3	18	12	1917	2.79	5	<8	<2	2	30	.5	<3	<3	53	.39	.140	8	29	.41	201	.16	<3	2.81	.01	.11	<2	.5
PO L32S 26+00W	1	27	26	116	<.3	22	13	2327	2.68	6	<8	<2	3	25	.6	<3	<3	54	.33	.146	14	32	.51	198	.15	<3	3.40	.01	.10	<2	2.3
PO L32S 25+50W	1	19	51	148	<.3	13	15	10081	4.04	7	<8	<2	3	55	1.6	<3	<3	43	.70	.129	26	17	.42	660	.10	<3	2.28	.01	.14	<2	102.2
PO L32S 25+00W	1	33	100	210	<.3	22	13	1199	2.87	7	<8	<2	7	50	.8	<3	<3	50	.51	.281	16	30	.51	272	.13	<3	3.04	.01	.13	<2	1.2
PO L32S 24+50W	1	29	23	164	<.3	24	14	2770	3.05	7	<8	<2	3	34	.9	<3	<3	60	.41	.142	10	37	.61	260	.14	<3	2.65	.01	.12	<2	.7
PO L32S 24+00W	1	32	22	158	<.3	24	15	1677	2.98	11	<8	<2	3	22	.6	<3	<3	73	.19	.254	8	45	.63	184	.12	<3	2.92	.01	.10	<2	.4
PO L32S 23+50W	1	40	12	119	<.3	27	16	656	3.11	7	<8	<2	2	30	<.5	<3	<3	66	.30	.217	7	55	.80	153	.10	<3	2.56	.01	.11	<2	4.1
STANDARD DS3	9	121	35	154	.3	37	13	834	2.92	30	<8	<2	4	26	5.9	5	6	73	.54	.096	17	190	.59	143	.09	<3	1.71	.03	.17	4	21.3

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

Emgold Mining Corp. PROJECT STEWART FILE # A103745

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	3	44	<.3	7	4	540	1.65	<2	<8	<2	6	65	<.5	<3	<3	40	.51	.092	9	21	.60	220	.12	<3	.85	.06	.44	2	.4
PO L32S 23+00W	5	180	42	161	.8	41	52	2897	6.13	30	<8	<2	2	20	.7	<3	<3	121	.16	.146	12	48	1.73	176	.16	<3	3.57	.01	.30	<2	18.2
PO L32S 22+50W	1	24	30	139	<.3	18	13	4875	3.13	12	<8	<2	2	40	1.4	<3	<3	44	.43	.243	9	23	.43	361	.13	<3	3.29	.01	.11	<2	9.8
PO L34S 30+00W	2	59	13	143	<.3	34	23	1220	4.65	20	<8	<2	2	19	.5	<3	<3	121	.23	.162	5	72	1.31	249	.21	<3	2.98	.01	.13	<2	.9
PO L34S 29+50W	3	35	33	175	.3	24	20	2384	3.38	100	<8	<2	4	61	1.1	<3	<3	45	.80	.156	15	37	.38	265	.15	<3	3.39	.01	.07	<2	.7
PO L34S 29+00W	2	34	16	81	<.3	21	9	464	2.99	226	<8	<2	3	33	<.5	<3	<3	50	.60	.197	5	36	.44	131	.17	<3	4.57	.01	.07	<2	1.8
PO L34S 28+50W	2	41	24	136	<.3	106	23	814	3.67	57	<8	<2	5	29	<.5	<3	<3	71	.33	.161	13	182	1.64	182	.17	<3	3.36	.01	.12	<2	.8
PO L34S 28+00W	2	21	24	130	<.3	37	14	1377	3.49	52	<8	<2	3	27	.5	<3	<3	54	.28	.177	8	59	.59	171	.15	<3	3.08	.01	.09	<2	5.7
PO L34S 27+50W	2	51	27	116	<.3	38	15	1405	3.50	81	<8	<2	4	74	.9	<3	<3	54	.91	.081	26	104	.72	234	.18	<3	3.80	.03	.12	<2	8.8
PO L34S 27+00W	1	15	24	122	<.3	17	9	941	2.55	18	<8	<2	3	30	.5	<3	<3	40	.31	.297	10	27	.27	208	.16	<3	3.06	.02	.08	<2	39.5
PO L34S 26+50W	1	16	16	74	<.3	21	11	512	3.02	17	<8	<2	2	30	<.5	<3	<3	60	.29	.126	7	45	.55	136	.14	<3	2.31	.01	.08	<2	1.5
PO L34S 26+00W	1	14	16	77	<.3	17	11	1057	3.05	10	<8	<2	3	27	<.5	<3	<3	53	.22	.112	10	30	.41	166	.13	<3	2.76	.01	.09	<2	14.9
PO L34S 25+50W	1	23	16	119	<.3	26	11	979	2.91	26	<8	<2	3	33	.5	<3	<3	50	.36	.165	11	40	.43	167	.16	<3	3.74	.02	.09	<2	1.2
RE PO L34S 25+50W	1	24	17	125	<.3	28	12	1021	2.93	27	<8	<2	4	36	<.5	<3	<3	53	.38	.174	12	43	.42	184	.17	3	3.80	.02	.08	<2	1.5
PO L34S 25+00W	1	16	21	125	<.3	22	11	700	2.72	17	<8	<2	3	31	<.5	<3	<3	62	.31	.109	8	40	.46	140	.14	<3	2.57	.01	.08	<2	1.3
PO L34S 24+50W	1	28	31	116	<.3	18	11	963	2.76	9	<8	<2	4	26	.5	<3	<3	50	.28	.153	8	34	.41	167	.13	<3	3.12	.01	.08	<2	4.6
PO L34S 24+00W	1	21	17	129	<.3	19	10	620	2.93	9	<8	<2	3	32	<.5	<3	<3	51	.30	.169	9	37	.44	140	.15	<3	3.62	.01	.07	<2	1.1
PO L34S 23+50W	1	23	28	187	<.3	21	12	470	2.95	17	<8	<2	4	37	.5	<3	<3	59	.33	.272	7	37	.44	124	.18	<3	4.69	.01	.06	<2	.9
PO L34S 23+00W	1	54	29	149	.6	33	15	929	3.28	16	8	<2	3	75	.9	<3	<3	72	.70	.105	11	68	.75	160	.17	<3	3.24	.02	.07	<2	1.1
PO L34S 22+50W	1	18	23	115	<.3	14	9	1150	2.64	9	<8	<2	3	23	<.5	<3	<3	47	.22	.220	7	26	.31	180	.12	<3	2.85	.01	.07	<2	1.0
PO L34S 22+00W	3	47	17	159	<.3	33	19	1208	4.06	18	<8	<2	3	27	.9	<3	<3	115	.24	.159	6	50	.82	196	.20	<3	3.48	.01	.12	<2	1.1
PO L36S 30+00W	2	32	15	140	<.3	30	18	1053	3.64	31	<8	<2	2	19	.6	<3	<3	83	.19	.102	6	66	.69	203	.20	<3	2.72	.01	.08	<2	3.3
PO L36S 29+50W	3	37	13	93	<.3	26	15	427	3.06	20	<8	<2	3	20	<.5	<3	<3	71	.20	.129	7	44	.59	105	.13	<3	3.20	.01	.08	<2	16.2
PO L36S 29+00W	3	28	14	100	<.3	22	14	664	2.71	42	<8	<2	2	21	<.5	<3	<3	62	.21	.134	8	41	.53	121	.15	<3	2.97	.01	.07	<2	52.5
PO L36S 28+50W	1	34	13	157	<.3	72	17	579	3.09	16	<8	<2	3	19	<.5	<3	<3	69	.17	.165	7	80	.76	159	.14	<3	3.10	.01	.10	<2	1.3
PO L36S 28+00W	1	28	15	83	<.3	22	13	574	2.95	9	<8	<2	3	16	<.5	<3	<3	66	.12	.139	8	41	.50	140	.14	<3	3.11	.01	.06	<2	2.5
PO L36S 27+50W	1	26	20	87	<.3	21	11	1225	2.62	7	<8	<2	4	26	<.5	<3	<3	57	.24	.137	14	34	.51	194	.16	<3	3.30	.01	.10	<2	5.7
PO L36S 27+00W	1	21	24	94	<.3	18	13	1019	3.27	9	<8	<2	2	22	<.5	<3	<3	66	.21	.185	9	47	.52	178	.16	<3	2.21	.01	.07	<2	1.1
PO L36S 26+50W	1	26	18	87	<.3	20	11	685	3.04	7	<8	<2	3	20	<.5	<3	<3	60	.19	.132	9	34	.57	110	.14	<3	3.08	.01	.08	<2	2.6
PO L36S 26+00W	<1	32	14	45	<.3	11	6	189	1.97	6	<8	<2	4	21	<.5	<3	<3	35	.21	.196	5	12	.14	95	.21	<3	5.83	.02	.04	<2	<.2
PO L36S 25+50W	1	63	18	166	.3	21	18	1071	3.72	11	<8	<2	3	24	.6	<3	<3	82	.24	.372	5	25	.88	171	.22	<3	4.04	.02	.10	<2	<.2
PO L36S 25+00W	1	45	19	234	.3	27	29	895	5.14	14	<8	<2	2	20	.5	<3	<3	146	.18	.196	4	55	1.35	215	.25	<3	3.47	.01	.12	<2	<.2
PO L36S 24+50W	1	56	73	231	<.3	22	20	1885	4.06	6	<8	<2	7	39	.6	<3	<3	106	.39	.154	10	37	1.08	298	.21	<3	3.24	.01	.16	<2	.8
PO L36S 24+00W	1	98	9	81	<.3	101	25	541	3.66	8	<8	<2	2	33	<.5	<3	<3	102	.36	.066	7	217	1.74	160	.16	<3	2.40	.01	.13	<2	1.4
STANDARD DS3	10	123	34	158	.3	36	12	732	2.95	31	<8	<2	4	28	5.4	5	6	79	.52	.098	19	191	.59	148	.09	<3	1.76	.03	.18	4	20.9

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	<3	39	<.3	6	4	444	1.53	<2	<8	<2	5	53	<.5	<3	<3	33	.49	.082	6	17	.52	207	.10	<3	.74	.04	.43	2	.3
PO L36S 23+50W	2	49	11	78	<.3	22	24	457	3.63	5	<8	<2	2	15	<.5	<3	<3	56	.11	.152	6	33	.49	137	.08	<3	2.16	.01	.06	<2	.8
PO L38S 30+00W	2	34	12	127	.3	26	16	601	3.41	44	<8	<2	2	27	.7	<3	<3	74	.28	.114	7	51	.72	124	.09	<3	2.44	.01	.10	<2	6.9
PO L38S 29+50W	2	47	13	147	.3	27	16	568	3.13	34	<8	<2	3	21	.7	<3	<3	72	.18	.096	8	49	.70	116	.12	<3	2.99	.01	.08	<2	5.4
PO L38S 29+00W	3	53	11	105	<.3	27	15	403	3.18	91	<8	<2	3	29	.5	<3	<3	70	.34	.184	9	51	.84	105	.10	<3	2.49	.01	.10	<2	9.3
PO L38S 28+50W	1	19	12	81	<.3	14	10	341	2.54	8	<8	<2	2	12	<.5	<3	<3	56	.10	.133	6	31	.37	107	.12	<3	2.18	.01	.04	<2	2.8
PO L38S 28+00W	1	25	22	111	<.3	22	12	1071	2.86	8	<8	<2	3	21	.5	<3	<3	57	.23	.137	8	38	.46	226	.13	<3	3.29	.01	.07	<2	1.2
PO L38S 27+50W	1	28	44	123	<.3	16	14	3531	3.30	10	<8	<2	<2	32	1.1	<3	<3	57	.34	.141	11	37	.52	210	.09	<3	1.80	.01	.08	<2	22.0
PO L38S 27+00W	1	35	41	127	<.3	19	15	2902	3.11	8	<8	<2	<2	35	1.3	<3	<3	60	.38	.142	14	43	.57	177	.08	<3	2.12	.01	.08	<2	8.7
PO L38S 26+50W	1	28	20	80	<.3	24	14	1090	3.10	9	<8	<2	3	24	<.5	<3	<3	61	.25	.119	8	34	.47	252	.14	<3	3.67	.01	.07	<2	3.2
PO L38S 26+00W	1	32	16	110	<.3	17	15	1138	2.82	5	<8	<2	2	24	<.5	<3	<3	60	.23	.187	6	37	.60	246	.12	<3	2.36	.01	.07	<2	.7
PO L38S 25+50W	1	41	21	122	<.3	17	14	1327	2.85	8	<8	<2	2	21	<.5	<3	<3	64	.16	.211	6	35	.61	174	.12	<3	2.33	.01	.08	<2	.7
PO L38S 25+00W	1	44	57	198	<.3	19	22	2819	4.04	9	<8	<2	2	51	1.4	<3	<3	111	.44	.146	7	37	1.02	442	.17	<3	2.35	.01	.14	<2	.9
PO L38S 24+50W	1	37	38	129	<.3	19	16	1018	3.61	15	<8	<2	8	30	<.5	<3	<3	88	.44	.300	5	44	.98	360	.19	<3	2.79	.01	.15	<2	1.0
PO L38S 24+00W	1	99	54	130	.4	20	25	578	4.50	15	<8	<2	3	24	<.5	<3	<3	145	.26	.077	7	41	1.97	300	.27	<3	3.64	.01	.51	<2	6.7
RE PO L38S 24+00W	1	94	57	129	.4	19	25	592	4.63	15	<8	<2	3	24	<.5	<3	<3	141	.28	.074	7	41	2.05	305	.27	<3	3.67	.01	.52	<2	4.3
PO L40S 30+00W	4	60	15	424	.6	29	16	1149	3.41	261	10	<2	2	35	4.0	<3	<3	65	.51	.103	14	54	.65	104	.10	<3	2.46	.01	.09	<2	3.1
PO L40S 29+50W	3	56	20	490	.3	30	16	1138	3.23	412	10	<2	3	42	4.3	<3	<3	61	.59	.072	15	58	.71	104	.12	<3	2.88	.02	.10	<2	2.0
PO L40S 29+00W	1	27	12	196	<.3	23	13	727	2.89	62	<8	<2	2	25	1.0	<3	<3	63	.26	.138	8	40	.53	178	.11	<3	2.48	.01	.07	<2	1.1
PO L40S 28+50W	1	18	31	122	<.3	14	9	482	2.87	17	<8	<2	2	14	.5	<3	<3	58	.11	.192	6	32	.37	128	.13	<3	1.97	.01	.05	<2	6.1
PO L40S 28+00W	2	28	53	132	<.3	18	18	4175	4.42	12	<8	<2	2	23	1.2	<3	<3	64	.22	.115	15	46	.54	393	.09	<3	2.32	.01	.10	<2	10.2
PO L40S 27+50W	1	35	31	130	<.3	22	15	1915	3.64	10	<8	<2	2	24	.7	<3	<3	65	.24	.150	13	49	.66	207	.12	<3	2.57	.01	.10	<2	82.8
PO L40S 27+00W	1	38	16	83	<.3	22	14	1430	3.27	7	<8	<2	2	41	.5	<3	<3	61	.45	.086	14	39	.64	232	.13	<3	3.33	.01	.09	<2	3.3
PO L40S 26+50W	1	54	12	97	.3	21	18	1598	3.57	6	<8	<2	2	29	<.5	<3	<3	73	.37	.087	8	38	.75	159	.14	<3	2.36	.01	.09	<2	2.9
PO L40S 26+00W	1	42	15	80	<.3	23	14	918	2.87	8	<8	<2	3	24	<.5	<3	<3	63	.22	.142	8	38	.63	195	.12	<3	2.73	.01	.07	<2	20.4
PO L40S 25+50W	1	52	13	77	<.3	23	15	824	3.02	8	<8	<2	3	28	<.5	<3	<3	72	.31	.084	9	42	.73	133	.14	<3	2.77	.01	.08	<2	2.2
PO L40S 25+00W	1	92	104	366	.3	34	33	2249	5.90	67	<8	<2	3	56	2.8	<3	<3	167	.52	.152	12	50	1.57	420	.20	<3	3.35	.01	.34	<2	1.1
STANDARD DS3	9	124	35	164	.3	35	12	768	3.28	31	<8	<2	4	26	5.7	5	6	72	.51	.090	17	181	.58	154	.09	<3	1.66	.03	.15	4	20.8

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

ACME ANALYT AL LABORATORIES LTD. 852 E. HASTINGS ST. VANC ER BC V6A 1R6 PHONE(604)253-3158 FAX(604)25 716
(ISO 90 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Emgold Mining Corp. PROJECT STEWART File # A103745R
1400 - 570 Granville St., Vancouver BC V6C 3P1 Submitted by: Linda Dandy

SAMPLE#	W ppm
AR L10N 9+25E	70
AR L10N 9+75E	30
AR L9N 8+75E	21
AR L9N 9+75E	83
AR L9N 10+00E	47
AR L8N 9+25E	18
AR L8N 10+00E	30
AR L8N 12+50E	29
AR L7N 9+50E	57
RE AR L7N 9+50E	53
AR L7N 9+75E	41
AR L6N 7+75E	22
AR L6N 9+75E	23
CR L20S 3+75E	23
STANDARD SO-17	10

GROUP 4B - REE - LiBO2 FUSION, ICP/MS FINISHED.
- SAMPLE TYPE: SOIL PULP
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: NOV 9 2001 DATE REPORT MAILED: Nov 19/01 SIGNED BY .... D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data FA

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Emgold Mining Corp. PROJECT STEWART File # A103793 Page 1
1400 - 570 Granville St., Vancouver BC V6C 3P1 Submitted by: Linda Dandy

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	<3	41	<.3	4	4	488	1.50	<2	<8	<2	6	55	<.5	<3	<3	37	.42	.092	8	13	.52	202	.12	<3	.79	.05	.41	3	.6
ST L2S 4+00E	15	14	18	59	<.3	10	4	178	2.96	17	<8	<2	2	16	<.5	<3	<3	92	.11	.076	7	26	.29	54	.11	<3	1.16	.01	.05	12	3.5
ST L2S 4+25E	12	18	22	103	.3	12	6	415	3.08	15	<8	<2	3	10	<.5	<3	<3	77	.05	.091	6	28	.28	90	.14	<3	3.02	.01	.05	3	2.2
ST L2S 4+50E	8	27	16	86	.4	12	6	373	3.08	16	<8	<2	3	9	<.5	<3	<3	70	.06	.092	8	31	.37	69	.09	<3	3.01	.01	.05	2	3.3
ST L2S 4+75E	8	31	42	121	<.3	20	8	551	2.98	27	<8	<2	4	15	.6	<3	<3	69	.11	.152	9	36	.56	76	.09	<3	2.14	.01	.08	3	7.0
ST L2S 5+00E	7	30	18	97	<.3	17	7	353	3.06	19	<8	<2	3	10	<.5	<3	<3	71	.06	.136	8	35	.50	64	.09	<3	2.67	.01	.06	2	3.9
ST L2S 5+25E	35	18	35	42	<.3	7	3	148	2.95	13	<8	<2	2	8	.5	<3	<3	82	.04	.060	8	18	.16	49	.10	<3	1.27	<.01	.04	2	3.2
ST L2S 5+50E	8	25	38	63	.4	10	5	246	2.84	17	<8	<2	<2	12	.7	<3	<3	73	.07	.123	10	23	.29	60	.08	<3	1.88	.01	.05	<2	4.0
ST L2S 5+75E	16	17	20	66	.3	10	5	212	2.53	11	<8	<2	2	9	<.5	<3	<3	61	.06	.060	11	22	.24	77	.11	<3	2.34	.01	.04	<2	2.5
ST L2S 6+00E	11	15	20	60	.3	10	4	230	3.26	17	<8	<2	2	13	<.5	<3	<3	86	.08	.072	8	28	.30	58	.09	<3	1.72	.01	.05	<2	9.4
ST L2S 6+25E	30	12	25	45	<.3	5	3	105	1.71	7	<8	<2	<2	10	.8	<3	<3	59	.05	.043	7	12	.10	41	.09	<3	.71	.01	.05	<2	1.6
ST L2S 6+50E	11	20	35	46	<.3	6	2	127	1.61	9	<8	<2	<2	11	1.0	<3	<3	50	.05	.040	9	12	.13	54	.05	<3	1.00	.01	.05	2	1.7
ST L2S 6+75E	8	40	24	119	.5	19	7	284	3.14	26	<8	<2	4	14	.6	<3	<3	73	.10	.122	10	35	.51	68	.10	<3	3.53	.01	.06	2	7.1
ST L2S 7+00E	6	16	28	55	<.3	8	4	272	3.34	21	<8	<2	3	7	<.5	3	<3	83	.04	.142	8	24	.20	52	.14	<3	2.35	.01	.05	<2	4.0
ST L2S 7+25E	4	21	20	75	.3	10	5	329	2.79	12	<8	<2	3	8	<.5	<3	<3	69	.05	.073	6	25	.27	76	.10	<3	3.12	.01	.04	<2	1.9
ST L2S 7+50E	8	37	26	118	.3	15	16	1970	2.93	11	<8	<2	2	11	.7	<3	<3	67	.06	.170	14	26	.37	93	.07	<3	2.32	.01	.06	<2	2.1
ST L3S 4+50E	10	32	23	72	.6	13	14	530	3.04	16	<8	<2	<2	11	1.0	<3	<3	60	.07	.192	12	26	.29	76	.09	<3	2.35	.01	.06	2	2.2
ST L3S 4+75E	39	32	18	57	.4	9	5	421	4.23	10	<8	<2	4	11	<.5	<3	<3	67	.04	.114	11	20	.28	70	.13	<3	1.91	.01	.06	2	2.3
ST L3S 5+00E	36	30	27	59	<.3	10	4	200	3.05	14	<8	<2	3	14	<.5	<3	<3	71	.06	.073	13	21	.25	74	.13	<3	1.86	.01	.07	3	2.3
ST L3S 5+25E	11	33	20	53	.4	9	4	162	2.71	9	<8	<2	4	7	<.5	<3	<3	65	.04	.072	10	22	.22	64	.13	<3	3.60	.01	.04	<2	1.4
ST L3S 5+50E	35	23	19	77	.3	12	5	235	3.73	14	<8	<2	3	10	<.5	<3	<3	86	.06	.070	9	29	.30	64	.12	<3	2.20	.01	.05	<2	6.2
ST L3S 5+75E	19	25	18	93	.3	18	6	227	2.89	15	<8	<2	2	15	<.5	<3	<3	68	.09	.072	12	28	.41	84	.12	<3	2.45	.01	.05	<2	1.9
RE ST L3S 5+75E	18	24	17	87	.3	17	6	221	2.87	15	<8	<2	2	14	<.5	<3	<3	67	.09	.078	12	26	.40	86	.12	<3	2.39	.01	.05	<2	12.1
ST L3S 6+00E	7	29	18	81	.3	14	7	339	2.89	19	<8	<2	<2	16	.5	<3	<3	76	.11	.115	10	32	.38	73	.08	<3	2.27	.01	.05	<2	3.4
ST L3S 6+25E	26	29	16	83	.5	20	11	791	2.69	11	<8	<2	<2	18	.6	<3	<3	61	.11	.073	19	34	.46	129	.09	<3	2.20	.01	.06	<2	3.4
ST L3S 6+50E	6	18	15	60	.5	8	4	203	2.96	12	<8	<2	2	9	<.5	<3	<3	65	.06	.106	6	24	.23	61	.11	<3	3.28	.01	.04	<2	2.4
ST L3S 6+75E	5	19	16	85	<.3	13	5	284	3.09	15	<8	<2	3	16	<.5	<3	<3	72	.09	.121	6	29	.34	69	.12	<3	2.89	.01	.05	2	3.3
ST L3S 7+00E	3	23	18	88	.4	13	6	362	2.99	17	<8	<2	3	11	<.5	<3	<3	74	.07	.123	8	31	.37	58	.13	<3	3.58	.01	.05	<2	3.9
ST L3S 7+25E	4	21	19	123	.8	10	5	2041	2.49	8	<8	<2	2	10	.5	<3	<3	63	.06	.114	7	20	.26	177	.13	<3	2.33	.01	.06	<2	1.9
ST L3S 7+50E	4	24	16	75	.5	11	5	222	2.60	12	<8	<2	3	6	<.5	<3	<3	60	.04	.113	6	24	.25	51	.11	<3	3.72	.01	.04	<2	2.5
ST L3S 7+75E	4	24	35	110	.3	14	6	485	3.27	19	<8	<2	3	10	.7	<3	<3	81	.07	.095	7	33	.37	75	.09	<3	2.58	.01	.07	<2	4.7
ST L3S 8+00E	4	26	22	101	.6	12	7	504	2.89	13	<8	<2	2	8	<.5	<3	<3	74	.06	.127	8	30	.32	81	.08	<3	2.83	.01	.05	<2	36.7
ST L3S 8+25E	7	22	22	81	.5	11	7	298	3.00	15	<8	<2	3	7	<.5	<3	<3	70	.04	.134	8	26	.27	63	.12	<3	3.20	.01	.05	<2	5.1
ST L3S 8+50E	19	18	22	108	.4	12	5	222	3.03	12	<8	<2	2	15	.6	<3	<3	71	.08	.050	9	27	.33	152	.10	<3	1.84	.01	.05	<2	2.2
STANDARD DS3	9	130	36	159	.3	35	12	829	3.07	31	<8	<2	4	29	5.9	5	6	79	.56	.100	18	190	.58	146	.09	<3	1.73	.03	.14	4	22.1

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
- SAMPLE TYPE: SOIL SS80 60C AU* BY ACID LEACHED, ANALYZE BY ICP-MS. (10 gm)
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 25 2001 DATE REPORT MAILED: Nov 5/01 SIGNED BY............D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data FA

ACME ANALYTICAL

Emgold Mining Corp. PROJECT STEWART FILE # A103793

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	<3	41	<.3	5	4	528	1.72	<2	<8	<2	5	56	<.5	<3	<3	36	.46	.103	7	12	.54	219	.11	<3	.79	.04	.51	3	.4
ST L4S 3+00E	11	24	28	71	.3	9	6	438	3.08	13	<8	<2	2	9	<.5	<3	<3	61	.07	.062	13	20	.23	77	.06	<3	2.64	.01	.05	4	2.9
ST L4S 3+25E	8	24	17	65	<.3	10	4	167	3.41	23	<8	<2	3	12	<.5	<3	<3	60	.10	.118	6	25	.25	46	.11	<3	4.02	.01	.05	8	2.6
ST L4S 3+50E	28	31	19	51	.6	7	4	226	3.49	10	<8	<2	4	7	<.5	<3	<3	62	.04	.140	7	16	.17	70	.08	<3	2.92	.01	.05	2	2.3
ST L4S 3+75E	8	22	17	24	.4	6	3	80	2.67	7	<8	<2	2	6	<.5	<3	<3	50	.04	.117	9	14	.10	39	.13	<3	3.67	.01	.03	<2	.8
ST L4S 4+00E	17	34	23	64	.3	11	4	235	3.02	14	<8	<2	4	7	<.5	<3	<3	50	.04	.125	10	21	.25	54	.09	<3	4.17	.01	.06	3	2.6
ST L4S 4+25E	7	36	17	69	<.3	13	8	391	2.64	15	<8	<2	<2	10	<.5	<3	<3	56	.08	.161	10	27	.35	70	.07	<3	2.51	.01	.06	2	14.2
ST L4S 4+50E	15	31	20	89	<.3	14	6	530	3.06	17	<8	<2	3	14	.5	<3	<3	63	.09	.175	9	27	.44	89	.08	<3	2.59	<.01	.07	3	2.2
ST L4S 4+75E	19	27	23	81	.3	14	6	250	4.00	23	<8	<2	3	10	<.5	<3	<3	81	.06	.180	11	30	.39	76	.11	<3	2.98	.01	.06	3	6.5
ST L4S 5+00E	30	35	19	79	.3	13	7	457	3.49	19	<8	<2	2	10	.7	<3	<3	62	.07	.247	11	24	.35	61	.08	<3	3.01	.01	.07	2	9.7
ST L4S 5+25E	25	36	18	60	<.3	10	6	267	3.18	15	<8	<2	<2	9	1.0	<3	<3	59	.06	.098	11	20	.21	57	.09	<3	2.28	.01	.04	<2	3.6
ST L4S 5+50E	5	25	33	64	.3	13	10	380	3.81	18	<8	<2	2	8	.5	<3	<3	54	.05	.111	8	21	.35	67	.14	<3	2.06	.01	.06	2	3.1
ST L4S 5+75E	6	25	25	66	.3	15	6	248	3.58	32	<8	<2	2	12	1.0	<3	<3	79	.08	.086	7	35	.40	58	.10	<3	2.50	.01	.06	<2	21.8
ST L4S 6+00E	11	23	21	50	<.3	7	3	162	2.67	11	<8	<2	2	9	.7	<3	<3	62	.04	.074	10	16	.18	67	.10	<3	1.41	.01	.06	2	4.8
ST L4S 6+25E	7	26	18	90	.4	13	5	284	3.13	12	<8	<2	4	10	<.5	<3	<3	60	.06	.109	8	22	.27	92	.11	<3	3.67	.01	.06	<2	3.6
ST L4S 6+50E	8	36	15	106	<.3	19	7	274	3.00	15	<8	<2	5	9	<.5	<3	<3	59	.06	.110	9	31	.45	66	.10	<3	4.76	.01	.07	2	1.2
ST L4S 6+75E	8	25	18	82	.3	10	5	864	2.92	6	<8	<2	3	7	<.5	<3	<3	60	.04	.135	9	19	.21	84	.10	<3	3.16	.01	.06	<2	2.2
ST L4S 7+00E	12	26	16	93	.3	16	6	444	3.10	12	<8	<2	3	13	<.5	<3	<3	66	.08	.089	10	28	.47	79	.08	3	2.43	.01	.07	3	3.2
ST L4S 7+25E	8	33	18	127	<.3	18	8	1185	3.28	18	<8	<2	4	14	<.5	<3	<3	70	.10	.149	9	34	.54	111	.09	<3	2.89	.01	.08	3	8.0
ST L4S 7+50E	8	26	23	132	.4	14	8	831	3.48	17	<8	<2	3	16	.6	<3	<3	74	.11	.183	10	31	.52	159	.08	<3	2.49	.01	.08	2	3.5
ST L5S 2+00E	39	41	21	133	1.0	17	13	787	3.44	28	<8	<2	<2	16	1.1	<3	<3	81	.16	.090	11	25	.51	121	.09	<3	2.11	.01	.08	3	13.7
RE ST L5S 2+00E	39	40	20	133	1.0	17	13	727	3.34	28	<8	<2	<2	17	1.1	<3	<3	76	.15	.099	12	26	.56	130	.08	<3	2.17	.01	.08	3	8.7
ST L5S 2+25E	14	20	23	57	<.3	8	4	227	3.46	20	<8	<2	3	7	<.5	<3	<3	77	.06	.104	6	18	.26	61	.12	<3	2.33	.01	.05	2	4.8
ST L5S 2+50E	56	54	19	147	<.3	22	10	541	4.00	38	<8	<2	3	16	.5	<3	<3	85	.13	.115	9	36	.75	114	.11	<3	2.31	.01	.11	3	5.3
ST L5S 2+75E	9	33	25	85	<.3	12	6	308	2.99	13	<8	<2	5	10	<.5	<3	<3	58	.08	.089	9	20	.33	100	.10	<3	3.67	.01	.07	4	6.1
ST L5S 3+00E	9	32	16	64	<.3	11	5	244	3.34	17	<8	<2	3	11	<.5	<3	<3	61	.09	.102	9	23	.34	69	.10	<3	3.39	.01	.06	4	3.0
ST L5S 3+25E	15	18	27	53	<.3	8	4	520	2.52	20	<8	<2	<2	9	.6	<3	<3	58	.06	.080	8	16	.20	81	.08	<3	1.13	.01	.05	4	2.9
ST L5S 3+50E	14	21	21	42	<.3	7	3	139	3.15	11	<8	<2	3	9	<.5	<3	<3	67	.05	.080	8	19	.16	69	.12	<3	2.67	.01	.04	2	1.2
ST L5S 3+75E	18	35	18	91	<.3	16	6	266	3.55	25	<8	<2	4	11	<.5	<3	<3	81	.07	.132	10	31	.43	58	.12	<3	3.11	.01	.07	5	7.0
ST L5S 4+00E	11	27	26	86	<.3	14	6	253	3.57	18	<8	<2	3	10	<.5	<3	<3	70	.06	.141	9	25	.39	72	.09	<3	2.34	.01	.07	9	6.8
ST L5S 4+25E	9	51	26	75	.3	13	9	276	3.25	13	<8	<2	3	8	<.5	<3	<3	60	.05	.249	12	23	.33	97	.12	<3	3.40	.01	.07	7	22.1
ST L5S 4+50E	14	28	27	73	<.3	13	6	399	3.81	20	<8	<2	3	9	<.5	<3	<3	81	.05	.157	10	24	.31	89	.09	<3	2.17	.01	.07	19	22.5
ST L5S 4+75E	8	23	24	57	<.3	9	7	295	2.85	15	<8	<2	<2	8	.7	<3	<3	50	.05	.105	11	20	.25	65	.07	<3	2.45	.01	.06	2	3.1
ST L5S 5+00E	7	27	20	58	.4	10	5	253	2.50	13	<8	<2	2	9	.5	<3	<3	50	.05	.093	10	18	.27	61	.10	<3	2.09	.01	.05	<2	2.4
STANDARD DS3	9	135	37	156	.3	37	12	806	3.28	31	<8	<2	4	29	5.7	5	6	77	.55	.094	19	179	.57	145	.08	<3	1.71	.03	.17	4	23.3

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	3	45	<.3	6	4	559	2.06	<2	<8	<2	6	63	<.5	<3	<3	42	.61	.104	8	16	.56	227	.12	<3	1.02	.06	.54	3	<.2
ST L5S 5+25E	8	35	17	58	.5	11	6	179	2.44	9	<8	<2	2	7	.6	<3	<3	48	.04	.047	16	21	.26	71	.11	<3	2.40	.01	.05	<2	2.7
ST L5S 5+50E	3	32	24	54	.3	10	9	257	2.64	12	<8	<2	<2	9	2.1	<3	<3	42	.04	.076	13	19	.27	72	.06	<3	1.75	.01	.07	<2	3.9
ST L5S 5+75E	2	17	15	60	.4	9	4	233	2.75	14	<8	<2	2	7	<.5	<3	<3	60	.04	.086	6	23	.24	48	.10	<3	3.34	.01	.05	<2	2.1
ST L5S 6+00E	3	18	18	74	.3	12	5	260	3.31	15	<8	<2	3	8	<.5	<3	<3	71	.07	.085	5	30	.29	61	.09	<3	3.16	.01	.06	<2	6.1
ST L5S 6+25E	2	15	11	45	.4	6	3	178	2.68	10	<8	<2	4	4	<.5	<3	<3	41	.03	.121	4	20	.14	37	.12	<3	5.62	.01	.03	<2	1.1
ST L5S 6+50E	5	59	14	114	<.3	26	9	290	2.76	25	<8	<2	4	13	<.5	<3	<3	62	.10	.092	9	39	.68	60	.05	<3	2.32	.01	.07	2	13.2
ST L5S 6+75E	4	24	14	71	.3	12	5	238	2.90	13	<8	<2	5	9	<.5	<3	<3	52	.07	.134	6	32	.32	51	.10	<3	5.40	.01	.06	<2	8.8
ST L5S 7+00E	6	35	18	121	<.3	19	7	410	3.17	17	<8	<2	5	10	<.5	<3	<3	63	.07	.115	8	35	.48	73	.09	<3	4.00	.01	.07	3	2.9
ST L5S 7+25E	4	26	22	109	.5	14	8	592	2.98	11	<8	<2	2	31	1.0	<3	<3	63	.14	.124	11	29	.38	420	.06	<3	1.81	.01	.08	2	4.4
ST L5S 7+50E	5	25	19	128	<.3	21	11	898	3.17	10	<8	<2	2	17	.7	<3	<3	68	.10	.089	11	39	.51	212	.08	<3	2.01	.01	.07	2	1.7
ST L5S 7+75E	5	29	25	122	.5	17	8	375	3.58	17	<8	<2	3	12	<.5	<3	<3	83	.10	.117	9	44	.49	108	.08	<3	2.79	.01	.07	<2	4.6
ST L5S 8+00E	5	25	21	123	.6	15	8	437	3.39	16	<8	<2	3	11	.5	<3	<3	78	.07	.106	8	34	.39	103	.08	<3	2.41	.01	.07	<2	3.2
ST L6S 6+00E	2	25	24	83	<.3	14	6	270	2.61	14	<8	<2	4	12	.5	<3	<3	61	.08	.049	8	27	.36	71	.08	<3	2.49	.01	.07	<2	2.8
ST L6S 6+25E	2	21	18	65	<.3	8	4	251	2.53	6	<8	<2	5	8	<.5	<3	<3	44	.04	.073	8	17	.21	54	.06	<3	3.38	.01	.07	3	1.3
ST L6S 6+50E	3	15	13	53	<.3	10	4	330	2.33	10	<8	<2	2	9	<.5	<3	<3	76	.04	.080	8	17	.16	68	.13	<3	1.12	.01	.07	<2	1.3
ST L6S 6+75E	2	14	19	57	<.3	7	3	436	2.69	5	<8	<2	4	9	<.5	<3	<3	56	.03	.047	9	15	.17	46	.10	<3	3.20	.01	.06	<2	.8
ST L6S 7+00E	2	19	15	49	.3	8	4	238	2.21	7	<8	<2	4	6	<.5	<3	<3	42	.03	.079	6	14	.15	52	.14	<3	4.93	.01	.05	<2	1.0
ST L6S 7+25E	2	12	19	49	<.3	6	4	336	2.36	4	<8	<2	3	9	<.5	<3	<3	60	.04	.029	9	15	.16	76	.09	<3	1.39	.01	.06	<2	1.1
ST L6S 7+50E	2	21	22	103	<.3	42	14	2135	2.96	4	<8	<2	3	19	<.5	<3	<3	56	.13	.066	8	40	.74	235	.15	<3	2.61	.01	.09	<2	.9
ST L6S 7+75E	4	35	18	137	<.3	23	9	286	3.07	17	<8	<2	3	10	<.5	<3	<3	63	.09	.150	9	36	.57	96	.08	<3	3.33	.01	.07	<2	4.7
ST L6S 8+00E	4	28	19	133	<.3	20	9	583	3.10	13	<8	<2	3	15	<.5	<3	<3	73	.11	.130	12	38	.48	107	.07	<3	3.05	.01	.08	<2	9.2
ST L6S 8+25E	4	29	21	125	.3	17	6	328	2.91	16	<8	<2	4	9	<.5	<3	<3	67	.08	.150	8	32	.39	86	.11	<3	4.08	.01	.08	<2	7.5
RE ST L6S 8+25E	4	27	20	127	<.3	17	7	306	3.05	15	<8	<2	4	8	<.5	<3	<3	66	.07	.144	8	31	.38	79	.10	<3	3.86	.01	.07	<2	3.9
ST L6S 8+50E	5	31	25	119	<.3	17	8	410	3.35	16	<8	<2	4	9	<.5	<3	<3	76	.07	.099	9	35	.36	94	.09	<3	3.08	.01	.07	<2	4.6
ST L6S 8+75E	4	21	20	99	.4	13	6	689	3.06	15	<8	<2	3	10	.5	<3	<3	76	.09	.185	7	25	.26	98	.10	<3	2.72	.01	.07	<2	1.2
ST L6S 9+00E	11	90	52	320	.8	52	20	1546	3.95	40	<8	<2	2	25	1.2	<3	<3	126	.29	.137	10	51	.65	226	.06	<3	2.65	.01	.14	3	5.1
ST L6S 9+25E	10	69	29	221	.9	40	14	589	3.81	30	<8	<2	2	13	1.1	<3	<3	117	.14	.109	12	49	.53	124	.08	<3	2.75	.01	.09	2	3.3
ST L6S 9+50E	6	50	21	201	.4	27	14	1476	3.11	24	<8	<2	2	30	1.6	<3	3	88	.32	.141	11	35	.50	223	.05	<3	1.94	.01	.09	2	2.7
ST L6S 9+75E	7	62	23	211	.5	30	16	987	3.20	27	<8	<2	2	39	1.5	<3	3	99	.40	.174	13	43	.50	238	.05	<3	2.05	.01	.14	3	6.9
ST L6S 10+00E	8	56	22	229	.6	28	14	1507	3.08	22	11	<2	<2	85	1.6	<3	<3	80	.47	.144	12	41	.47	813	.04	<3	1.80	.01	.10	2	3.4
ST L6S 10+25E	5	72	25	198	.4	33	19	1069	3.64	36	<8	<2	<2	46	1.1	<3	3	101	.48	.189	8	43	.82	256	.05	<3	2.18	.01	.17	3	6.6
ST L6S 10+50E	7	57	24	146	.6	23	13	1092	3.30	24	<8	<2	<2	13	1.1	<3	3	90	.11	.090	9	35	.53	114	.06	<3	2.25	.01	.13	3	3.2
ST L7S 2+50E	6	27	14	74	<.3	10	5	264	2.59	11	<8	<2	4	10	<.5	<3	<3	49	.08	.095	9	17	.23	60	.11	<3	3.36	.01	.06	4	4.9
STANDARD DS3	9	129	36	161	.3	36	13	802	3.07	31	<8	<2	4	28	5.8	5	6	78	.54	.084	18	188	.56	148	.09	<3	1.72	.03	.17	4	22.6

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

ACME ANALYTICAL

Emgold Mining Corp. PROJECT STEWART FILE # A103793

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	<3	43	<.3	5	5	533	1.84	<2	<8	<2	6	65	<.5	<3	<3	41	.56	.108	8	15	.61	216	.11	<3	.84	.06	.46	3	.4
ST L7S 2+75E	4	23	21	49	<.3	8	4	206	2.83	7	<8	<2	4	6	<.5	<3	<3	63	.04	.103	12	17	.22	58	.15	<3	2.89	.01	.07	2	1.7
ST L7S 3+00E	4	15	20	53	<.3	8	3	163	3.47	12	<8	<2	4	8	<.5	<3	<3	65	.06	.151	6	21	.19	53	.14	<3	3.15	.01	.06	5	.9
ST L7S 3+25E	4	25	17	96	<.3	13	6	363	2.86	16	<8	<2	4	10	.5	<3	<3	56	.08	.154	11	26	.39	67	.11	<3	3.53	.01	.07	7	2.5
ST L7S 3+50E	6	31	16	99	.3	15	8	296	3.17	19	<8	<2	3	12	.5	<3	<3	73	.09	.083	20	32	.43	76	.11	<3	2.60	.01	.06	6	4.9
ST L7S 3+75E	5	25	14	87	.4	13	5	276	2.60	20	<8	<2	2	8	.6	<3	<3	63	.06	.092	7	29	.31	70	.10	<3	3.22	.01	.06	5	3.1
ST L7S 4+00E	3	18	12	48	<.3	8	6	263	2.88	13	<8	<2	2	6	.8	<3	<3	46	.05	.121	10	17	.18	40	.14	<3	3.27	.01	.04	<2	1.4
ST L7S 4+25E	5	27	18	94	<.3	15	7	264	3.57	20	<8	<2	4	9	<.5	<3	<3	92	.07	.068	9	35	.43	63	.14	<3	3.48	.01	.06	2	1.2
ST L7S 4+50E	2	17	10	39	.3	6	3	146	2.16	8	<8	<2	3	4	<.5	<3	<3	38	.03	.100	6	15	.15	35	.13	<3	5.24	.01	.03	<2	1.2
RE ST L7S 4+50E	2	18	11	40	<.3	7	3	165	2.21	8	<8	<2	3	5	<.5	<3	<3	40	.04	.105	6	15	.15	36	.14	<3	5.49	.01	.03	<2	1.3
ST L7S 4+75E	3	17	16	116	<.3	13	5	389	2.69	10	<8	<2	3	12	<.5	<3	<3	54	.09	.116	8	22	.32	70	.10	<3	3.19	.01	.07	3	4.1
ST L7S 5+00E	3	17	16	71	<.3	10	5	542	2.58	9	<8	<2	3	9	<.5	<3	<3	63	.06	.074	8	20	.28	71	.08	<3	1.61	.01	.06	2	1.1
ST L7S 5+25E	2	13	18	31	<.3	5	2	89	2.95	7	<8	<2	3	6	<.5	<3	<3	57	.03	.070	8	14	.10	54	.16	<3	3.09	.01	.04	<2	.7
ST L7S 5+50E	2	16	17	70	<.3	10	4	172	2.52	8	<8	<2	3	8	<.5	<3	<3	53	.04	.046	8	20	.21	53	.09	<3	2.60	.01	.05	<2	2.4
ST L7S 5+75E	2	15	18	52	<.3	9	3	172	2.46	10	<8	<2	3	7	<.5	<3	<3	64	.04	.072	7	21	.23	50	.09	<3	2.41	.01	.05	<2	3.1
ST L7S 6+00E	2	17	14	52	<.3	9	4	156	2.39	9	<8	<2	4	5	<.5	<3	<3	46	.04	.077	5	18	.22	37	.12	<3	4.03	.01	.04	<2	.6
ST L7S 6+25E	2	15	16	78	<.3	10	5	438	2.66	7	<8	<2	4	7	<.5	<3	<3	54	.04	.062	6	19	.22	73	.13	<3	4.05	.01	.06	<2	1.0
ST L7S 6+50E	2	14	16	79	<.3	10	4	182	2.26	6	<8	<2	5	7	<.5	<3	<3	48	.04	.058	5	15	.21	64	.13	<3	3.89	.01	.06	<2	.6
ST L8S 1+00E	58	103	15	73	.5	11	11	791	4.74	18	<8	<2	2	11	<.5	<3	8	118	.09	.142	7	25	.47	60	.09	<3	1.82	.01	.08	18	3.2
ST L8S 1+25E	20	54	26	80	<.3	15	10	1072	4.25	66	<8	<2	2	14	.7	3	<3	121	.12	.156	9	32	.59	74	.15	<3	1.49	.01	.10	9	3.1
ST L8S 1+50E	6	38	15	74	.3	12	7	298	3.08	21	<8	<2	2	10	<.5	<3	<3	82	.08	.099	7	28	.37	61	.09	<3	2.50	.01	.07	2	11.2
ST L8S 1+75E	3	19	11	30	.5	5	3	176	2.45	9	<8	<2	3	4	<.5	<3	<3	44	.03	.174	4	17	.12	27	.13	<3	4.37	.01	.03	<2	.7
ST L8S 2+00E	2	22	14	51	<.3	9	4	326	2.71	11	<8	<2	3	6	<.5	<3	<3	57	.05	.111	5	18	.22	61	.14	<3	3.87	.01	.04	<2	1.5
ST L8S 2+25E	3	27	23	75	.5	10	4	174	2.72	16	<8	<2	5	7	<.5	<3	<3	55	.04	.131	7	29	.30	51	.14	<3	3.70	.01	.06	2	3.5
ST L8S 2+50E	3	18	35	46	.3	8	4	181	3.29	18	<8	<2	3	6	<.5	<3	<3	71	.03	.091	10	15	.18	53	.18	<3	2.02	.01	.07	2	4.2
ST L8S 2+75E	3	19	16	62	<.3	10	4	162	2.76	12	<8	<2	4	7	<.5	<3	<3	55	.04	.063	9	19	.23	47	.11	<3	2.86	.01	.05	4	6.4
ST L8S 3+00E	3	16	17	73	<.3	10	4	163	3.03	11	<8	<2	5	7	<.5	<3	<3	60	.04	.069	7	19	.24	49	.13	<3	2.63	.01	.06	3	.8
ST L8S 3+25E	4	24	17	61	.3	8	5	227	3.09	9	<8	<2	4	5	<.5	<3	<3	55	.03	.112	13	19	.22	58	.14	<3	4.72	.01	.05	2	1.7
ST L8S 3+50E	3	21	20	81	<.3	11	5	288	3.00	13	<8	<2	4	8	<.5	<3	<3	72	.06	.095	7	23	.28	63	.15	<3	3.19	.01	.06	4	2.0
ST L8S 3+75E	5	25	20	69	.3	12	6	247	3.28	15	<8	<2	3	8	<.5	<3	<3	74	.05	.089	9	27	.27	64	.13	<3	2.84	.01	.06	2	1.9
ST L8S 4+00E	3	21	15	52	.3	10	4	155	2.72	12	<8	<2	4	6	<.5	<3	<3	54	.05	.174	7	21	.23	43	.14	<3	4.35	.01	.04	<2	1.0
ST L8S 4+25E	3	24	24	113	<.3	18	9	1317	2.56	18	<8	<2	<2	14	.6	<3	<3	61	.10	.166	8	29	.46	86	.05	<3	2.02	.01	.07	2	34.0
ST L8S 4+50E	5	25	22	90	<.3	15	7	311	3.20	17	<8	<2	2	9	<.5	<3	<3	75	.07	.156	10	26	.41	71	.12	<3	2.45	.01	.07	2	2.3
ST L8S 4+75E	6	32	18	100	<.3	20	8	356	2.81	22	<8	<2	2	11	<.5	<3	<3	66	.07	.133	12	35	.52	56	.08	<3	2.51	.01	.07	2	16.7
STANDARD DS3	9	128	35	161	.3	37	12	819	2.95	31	<8	<2	4	27	5.7	5	6	80	.54	.101	18	183	.63	142	.09	<3	1.68	.03	.16	4	20.3

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

Emgold Mining Corp. PROJECT STEWART FILE # A103793

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
G-1	1	2	<3	38	<.3	5	4	530	1.61	<2	<8	<2	5	56	<.5	<3	<3	36	.52	.095	8	15	.55	204	.11	<3	.71	.04	.44	2	<.2
ST L8S 5+00E	4	18	22	52	.3	9	5	275	2.54	8	<8	<2	<2	8	<.5	<3	<3	47	.07	.189	10	19	.22	68	.07	<3	1.75	.01	.05	<2	3.5
ST L8S 5+25E	4	28	24	63	.4	12	5	198	2.81	10	<8	<2	2	8	.5	<3	<3	58	.06	.120	11	25	.36	78	.14	<3	2.35	.01	.07	<2	2.1
ST L8S 5+50E	3	17	23	71	<.3	11	5	327	3.04	13	<8	<2	3	9	<.5	<3	<3	61	.06	.117	9	26	.31	63	.10	<3	2.32	.01	.06	<2	4.8
ST L8S 5+75E	1	8	19	30	<.3	5	2	239	1.64	5	<8	<2	<2	8	<.5	<3	<3	52	.06	.031	8	12	.13	64	.08	<3	.76	.01	.04	<2	9.6
ST L8S 6+00E	1	16	15	45	<.3	7	4	286	2.46	6	<8	<2	3	9	<.5	<3	<3	48	.08	.061	6	18	.14	65	.13	<3	3.40	.01	.04	<2	25.2
ST L8S 6+25E	3	15	24	72	<.3	10	5	406	2.64	7	<8	<2	2	8	<.5	<3	<3	52	.06	.101	9	20	.28	63	.10	<3	2.06	.01	.07	<2	1.2
ST L8S 6+50E	3	20	21	100	<.3	13	7	536	2.33	13	<8	<2	3	9	<.5	<3	<3	46	.06	.111	10	23	.34	59	.08	<3	2.44	.01	.07	<2	108.4
RE ST L8S 6+50E	3	22	21	101	<.3	14	7	494	2.44	13	<8	<2	3	9	<.5	<3	<3	46	.07	.116	10	23	.32	63	.08	<3	2.49	.01	.07	<2	3.3
STANDARD DS3	9	122	36	154	.3	35	13	822	3.06	31	<8	<2	4	27	5.6	5	6	75	.53	.100	18	190	.63	141	.09	<3	1.62	.03	.15	4	20.3

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA