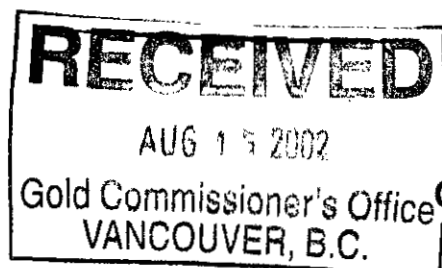


REPORT FOR ASSESSMENT
CARIBOO GOLD PROJECT - WELLS, B.C.



Cariboo Mining Division
N.T.S. Map Area 93H/4E
Latitude: 53° 06' North
Longitude: 121° 34' West

prepared for:

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GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT

August 14th, 2002

26,906

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1.0 INTRODUCTION

The Cariboo Gold Project is located around the town of Wells, British Columbia, 74km east of Quesnel British Columbia and 8km from the Barkerville Historic Town site. Site of the 1860's Cariboo gold rush, this region is estimated to have produced 2.6 million ounces of placer gold and from 1933 to 1987 has produced 1.23 million ounces of lode gold. The primary mines on the property are the Cariboo Gold Quartz, Island Mountain, Aurum, Mosquito Creek Gold mines, and the Hardscrabble Mountain tungsten/gold mine as well as dozens of smaller workings and showings.

The Cariboo Gold Project consists of properties owned by the Cariboo Gold group of companies, which includes International Wayside Gold Mines Ltd ("Wayside"), Island Mountain Gold Mines Ltd, and Golden Cariboo Resources Ltd.

The size of property, with its long history of lode and placer gold production, presents a favorable environment for further exploration and discovery of gold. Geophysical, and diamond drilling work programs have been carried out in the year 2001 with the intention of uncovering new targets and showings around the historic workings. The discovery of the Bonanza Ledge Zone by Robert Reid while drilling the BC Vein in early 2000 exemplifies the prospective nature of this area and has renewed interest by the mining community, spurring the largest staking rush in British Columbia since the discovery of Eskay Creek.

The historical maps and plans of the camp are measured in imperial units, and as Wayside has most of the original working plans, imperial measurements have been used with minor exceptions throughout the program. Coordinates contained in this report are on the original Cariboo Gold Quartz Mine (CGQM) grid system. Figures and maps include NAD 83 Metric UTM Grids as well as the imperial CGQM grid.

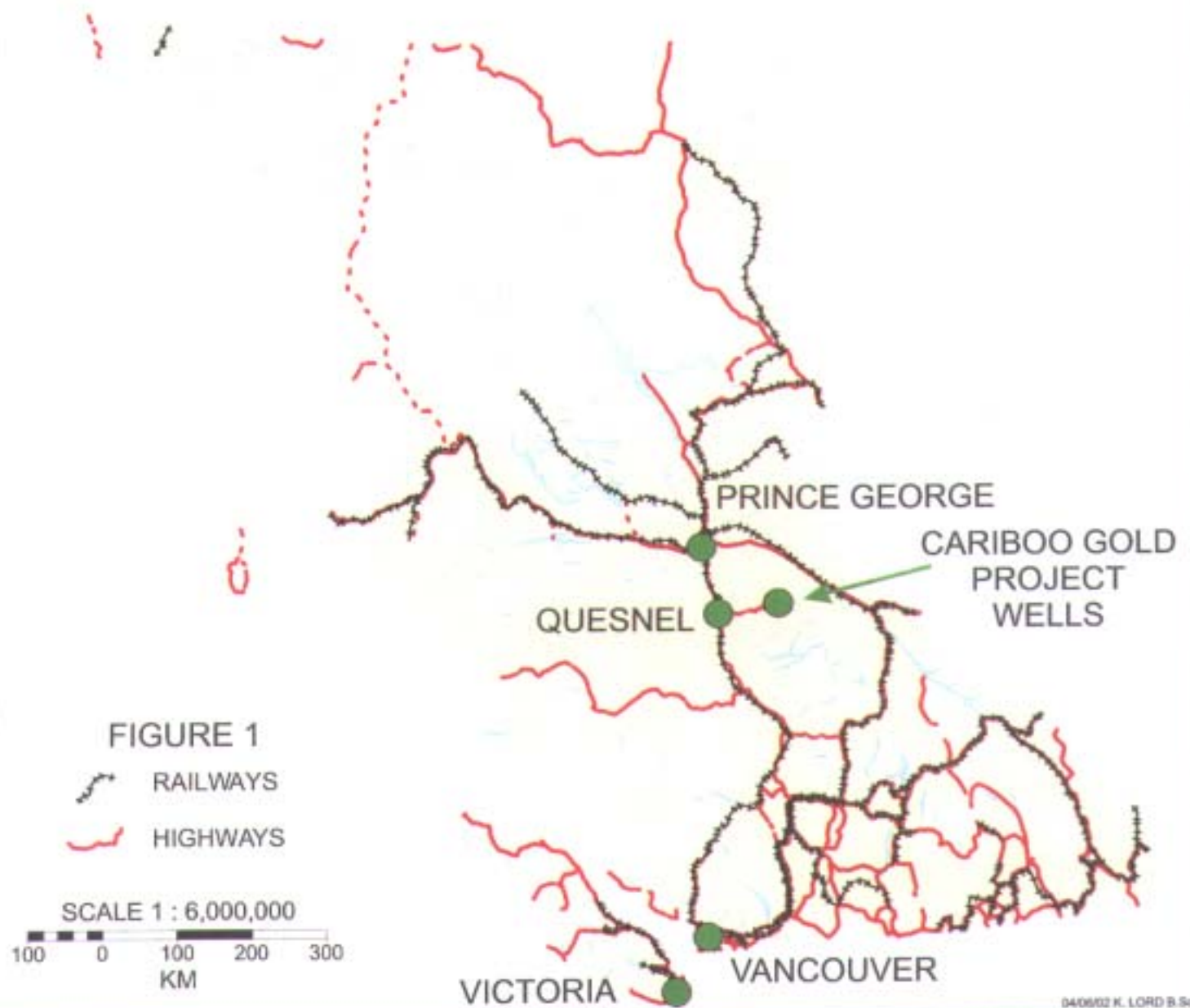
The purpose of this report is to provide documentation of geophysical and diamond drilling work filed for assessment on up to the end of 2001.

2.0 PROPERTY DESCRIPTION, ACCESSIBILITY AND OWNERSHIP

The area of assessment within the Cariboo Gold Project includes the Bonanza Ledge zone, BC shaft and Cariboo Gold Quartz mine, at Wells, British Columbia. Wells is situated in the Quesnel Highlands on the edge of the Interior Plateau at 53° 06' North Latitude and 121° 34' West Longitude, within NTS map 93H/04E and the Cariboo Mining District.

Wells is 46 miles (74 kilometers) due east of Quesnel along the paved Highway 26 to Barkerville Historic Town (Figure 1 – Location Map). Access from Wells to the work areas is by 4X4 truck, all terrain vehicle or snowmobile depending on the

BRITISH COLUMBIA



season, through a network of trails and roads accessible from Wells and Barkerville Historic Town, some of which date back to the nineteenth century.

The property is located above an elevation of 4,000 feet, shows local relief of 2,000 feet and is forested with spruce and balsam. As the Wells area has high annual accumulations of snow, claims are snow-free for about five months of the year. Arctic inflows with temperatures of the range of minus 30 to 40 degrees centigrade occur for periods of several weeks during the winter. Fair weather is most common in the late spring and early fall.

Mineral holdings (Figure 2 – Land Holdings / Access) for the purpose of this assessment consist of 66 Crown-granted mineral claims and 280 units within two and four post mineral claims. Mosquito Consolidated Gold Mines Limited owns 64 of the Crown granted mineral claims (Cariboo Gold Quartz Property). Wayside has earned a 50% interest in these crown grants and is presently in an option agreement to purchase the remaining 50% interest. The other two crown grants (lots 2F and 42F) are owned outright by Wayside. The IPO 1-22 claims have been optioned from Samuel D. Skiber. The remaining two and four-post mineral claims have been either staked or purchased by Wayside over the last several years (Table 1).

In addition, work is also being credited to the Myrtle and Proserpine crown granted mineral claims held by Gold City Industries Ltd. (45 lots) where International Wayside Gold Mines has just finalized an agreement to earn 50% in this land.

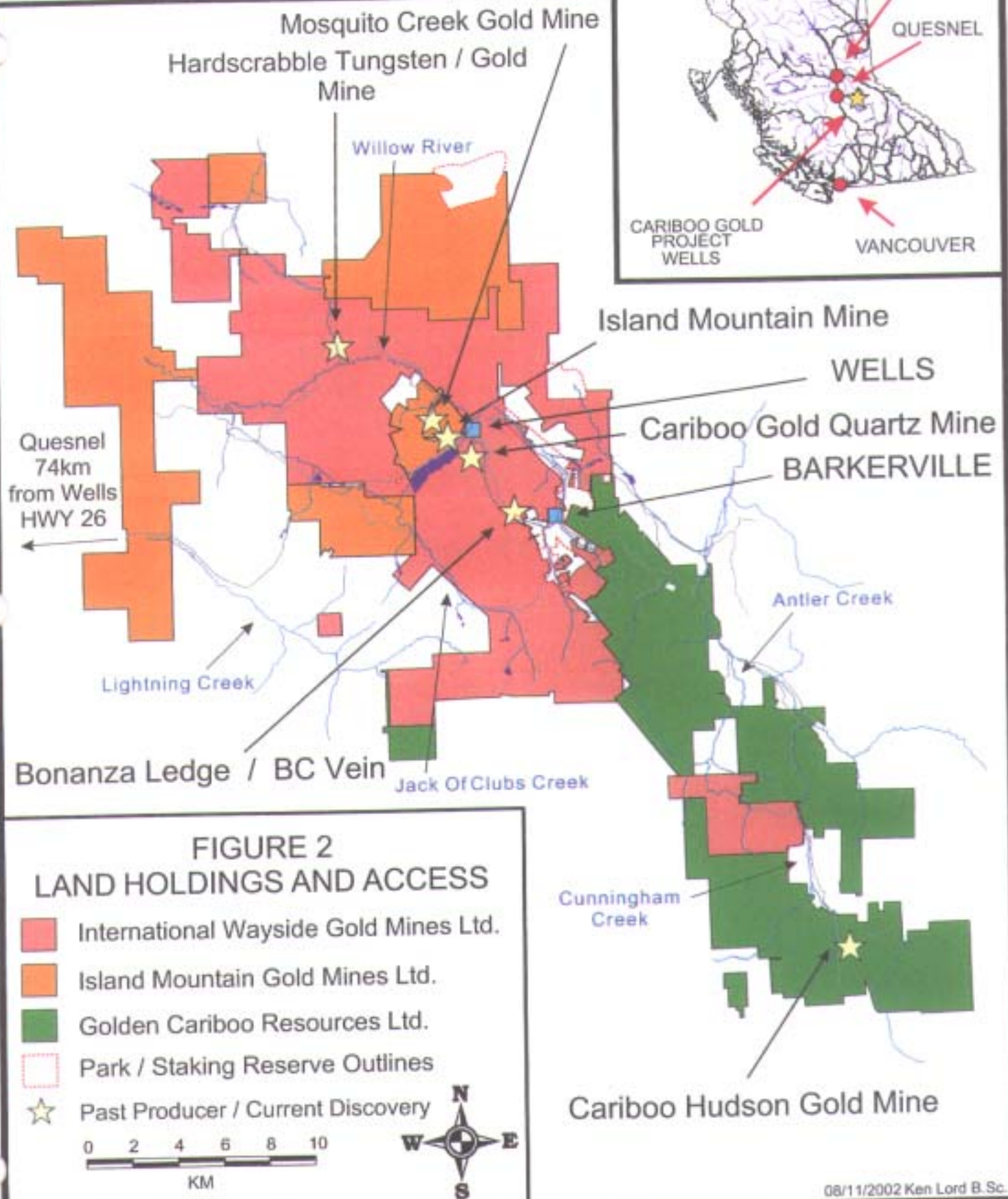
All groundwork performed during this program was carried out primarily on Crown granted mineral claims. A small portion of the work was carried out on the two/four post claims. The claims and work locations are shown on Figure 5.

TABLE 1 – IWA Property holdings for the purpose of assessment.

IWA Group of Crown-granted Mineral Claims

Claim Name	Lot No.	Date Crown Granted
BLACK BULL	2F	November 26, 1874
WAOMING	42F	May 20, 1876
AMERICAN	92	March 1, 1889
CARIBOO	93	March 1, 1889
ST. LAURENT	94	March 1, 1889
GOLDFINCH NO.2	301	October 7, 1901
EAGLE FRACTION	302	October 7, 1901
GLADSTONE	303	October 7, 1901
GOLDFINCH	318	April 28, 1898
PINKERTON	353	April 28, 1898
OLYMPIC NO. 5	5862	August 19, 1936
OLYMPIC NO. 3	5863	August 19, 1936
OLYMPIC NO. 1	5864	August 19, 1936
OLYMPIC NO. 4	5865	September 30, 1936

CARIBOO GOLD PROJECT



Claim Name	Lot No.	Date Crown Granted
OLYMPIC NO. 2	5866	August 19, 1936
CARIBOO NO. 7	5867	August 19, 1936
TELLURIDE FRACTION	5868	September 30, 1936
OLYMPIC NO. 12	5869	August 19, 1936
EMMA FRACTION	5870	September 30, 1936
EMMA	5871	August 19, 1936
BULL MOOSE	5872	August 19, 1936
SNOW STORM	5873	August 31, 1936
CAMERON	5874	August 19, 1936
CARIBOO TRAIL	5875	August 19, 1936
APEX FRACTION	5876	September 30, 1936
OLYMPIC FRACTION	5877	September 30, 1936
OLYMPIC NO. 6	5878	September 30, 1936
OLYMPIC NO. 7	5879	August 19, 1936
OLYMPIC NO. 13	5880	September 30, 1936
OLYMPIC NO. 14	5881	September 13, 1936
OLYMPIC NO. 11	5882	August 19, 1936
OLYMPIC NO. 9	5883	August 19, 1936
OLYMPIC NO. 8	5884	August 19, 1936
OLYMPIC NO. 17	5885	September 13, 1936
OLYMPIC NO. 10	5886	August 19, 1936
OLYMPIC NO. 16	5887	September 30, 1936
OLYMPIC NO. 15	5888	May 29, 1935
CARIBOO NO. 2 FRACTION	5889	September 30, 1936
GOLD STANDARD FRACTION	5890	December 9, 1936
BULLION	5891	December 10, 1938
GOLD BOOM	5892	December 10, 1938
GOLD STANDARD	5893	December 12, 1938
GOLD STANDARD NO. 1	5894	December 12, 1938
GOLD STANDARD NO. 2	5895	December 12, 1938
GOLD STANDARD NO. 3	5896	December 12, 1938
APEX	5897	September 13, 1936
PINKERTON FRACTION	5898	September 13, 1936
BROOKFORD NO. 2	5899	February 1, 1936
CARIBOO FRACTION	5919	December 12, 1938
DOLLY GREY FRACTION	7793	May 29, 1935
RAINBOW	7794	May 29, 1935
DOLLY VARDEN	7795	May 29, 1936
LAKEVIEW	7796	May 29, 1935
JACK OF CLUBS	7797	May 29, 1935
TELLURIDE	7798	May 29, 1936
TELLURIDE NO. 2	7799	May 29, 1935
TELLURIDE NO. 3	7800	May 29, 1936
CARIBOO NO. 1	7801	May 29, 1935
CARIBOO NO. 2	7802	May 29, 1935
MOTHER LODE	7803	May 29, 1935
RAINBOW FRACTION	7804	May 29, 1935
CARIBOO NO. 3	7805	May 29, 1935
GOLDBRICK	7806	May 29, 1935
MUCHO ORO	10026	September 18, 1925

Claim Name	Lot No.	Date Crown Granted
BROOKFORD NO. 1	10351	February 1, 1936
INIT. FRACTION	11227	July 28, 1939

IWA Group of Two/Four-post Mineral Claims

Mineral Claims	Tenure number	Date Staked	Assessment Due
L423 (RCG)	206856	March 22, 1990	March 22, 2002
FRANK 1-12	339130-339141	August 18, 1995	August 18, 2002
LAKE 1-4	355141-355144	April 4, 1997	April 4, 2002
FRANK 13-17	355124-355128	April 5, 1997	April 5, 2002
FRANK 18-27	355129-355138	April 17, 1997	April 17, 2002
CLUB 1-7	355152-355158	April 5, 1997	April 5, 2002
CLUB 8-17	355159-355168	April 6, 1997	April 6, 2002
CLUB 18-21	355169-355172	April 18, 1997	April 18, 2002
CLUB 22-31	355173-355182	April 17, 1997	April 17, 2002
FIELD 1-6	355085-355090	April 16, 1997	April 16, 2002
FIELD 8-12	355092-355096	April 16, 1997	April 16, 2002
WATSON 1-5	355080-355084	April 6, 1997	April 6, 2002
WALKER 1-6	355145-355150	April 7, 1997	April 7, 2002
EMORY 1-5	355997-355101	April 6, 1997	April 6, 2002
EMORY 6-11	355102-355107	April 16, 1997	April 16, 2002
EMORY 12-25	355108-355121	April 17, 1997	April 17, 2002
L.S. # 1-4	366281-366284	November 9, 1998	Nov 9, 2003
LIBERTY	375059	March 26, 2000	March 26, 2002
GOLD 4,5,3,1	375061-375064	March 28, 2000	March 28, 2002
NED 5-12	375120-375127	March 30, 2000	March 30, 2002
IPO 17-22	375339-375344	April 10, 2000	April 10, 2002
IPO 1-16	375347-375362	April 7, 2000	April 7, 2002
RAVEN # 1-6	375444-375449	April 16, 2000	April 16, 2002
WING 6-17	376090-376100	April 30, 2000	April 30, 2002
WING 4-5	376101-376102	April 30, 2000	April 30, 2002
FRANK 7-9	377533-377535	May 22, 2000	May 22, 2002
BUD 8	377537	May 28, 2000	May 28, 2002
KING FRACTION	375060		Dec 31 2002
DWM 1-7,11-13	385640-385649		Dec 31 2002

IWA Group of Crown Granted Mineral Claims

(held by Gold City Industries Ltd -Joint venture with Wayside earning 50% interest)

Claim Name	Lot No.
Wilkinson	177
Proserpine	430
Proserpine South	431
Proserpine West	2044
	2044
Proserpine East	2046
Conklin	2047
	7535
Shamrock No.4	10377
Shamrock No.5	10378

Claim Name	Lot No.
Shamrock No.6	10379
Shamrock No.7	10380
Progress No.8	10387
Progress No.7	10388
Progress No.6	10389
Lone Fraction	10404
	10471
	10472
	10473
Mint	10474
	10475
	10476
Myrtle	10501
Marie	10502
	10503
	10504
	10505
	10506
Y Fraction	10507
Martha	10508
Mabel	10509
	10510
Florence	10511
Cariboo	10512
Z Fraction	10513
N.M. No.5 Fraction	10514
Pan 1	10590
Pan 1 South	10591
San Juan Extension	10592
North Star	10593
Boom	10595
	11239
Princess Fraction	11240
Stephanie Fraction	11453
Noisy Enemy Fraction	11454
	11543

3.0 HISTORY OF THE PROPERTIES -After Hall (1997)

3.1 Cariboo Gold Belt

The Cariboo gold belt in south-central British Columbia was a world-class producer of gold. Total production of placer gold from the Cariboo goldfields is estimated to be approximately 2.6 million ounces. 90 percent of the placer gold was recovered from Late Pleistocene, pre-glacial and interglacial gravels in buried paleochannels of modern stream valleys. Greater than 60 percent of production is associated with rock strata of the upper Paleozoic Downey and Hardscrabble Mountain

successions, as mapped by Struick (1988), over a strike length of 30 miles (50km) from Big Valley Creek to the Cariboo River.

The distributions of drainages with high-recorded yield of placer gold, north of Mount Agnes clearly defines the trend of lode mineralization developed at Wells. Other trends parallel to the mine trend established at Wells are also indicated. Bowman (1889) first recognized that the rich gold-placers of the Wells-Barkerville area were associated with a trend of quartz veins in outcrop extending from Mt. Proserpine to Island Mountain. Prominent strike veins of the camp were mined at several periods prior to the lode-gold rush at Wells in the 1930's.

The bimodal distribution in fineness of placer gold from the Stanley-Wells-Barkerville goldfields, as reported by Knight and McTaggart (1989), reflect the two varieties of lode ore mined at Wells. Alternate sources of gold mineralization (potentially including the Bonanza Ledge Zone) are inferred for a third population showing enrichments in mercury content.

3.2 Wells Mining Camp

70 years after the Cariboo gold rush, hardrock gold mines were developed at Wells. The Wells camp ranks 5th in production of lode gold in British Columbia, Schroeter and Lane (1991). Mining was focused along a mineralized trend developed underground over a strike length of 3.5 miles, vertical range of 2,000 feet and width of about 700 feet. The Baker-Rainbow contact, mapped on surface by Hanson (1935) over a strike length of 12 miles from the Willow River to Antler Creek, was the principal guide to ore in the camp.

As zones of quartz stockworks mined underground extend to surface, opportunities for open-pit mining exist on Cow Mountain and Island Mountain. As early as 1948, A.C. Skerl recommended testing the open-pit potential of the Rainbow zone above the Rainbow fault. Development of open-pit gold reserves was the primary objective of exploration programs completed by Wharf Resources Ltd. (1980-1981), Pan Orvana Resources Inc. (1983-1990) and International Wayside Gold Mines Ltd. (1995-1997) on the Cariboo Group.

TABLE 2 – Past Lode and Placer Production, Cariboo Gold Belt

Mine	Time Frame	Tons	Grade-oz/ton	Ounces
Cariboo Gold Quartz	1933 - 1959	1,681,951	0.37	626,755
Island Mountain	1934 - 1967	1,245,295	0.46	569,528
Mosquito Creek	1980 - 1987	103,148	0.33	34,281
Total	1933 - 1987	3,030,394	0.41	1,230,564
Placer/Hydraulic Mining	1860 - Present			2,600,000

3.3 Cariboo Exploration & Development

Following the peak in placer production in 1863, early hard-rock miners worked weathered and gold-enriched tops of prominent strike veins using arrastras and stamp mills to process ore. Increased exploration activity during the periods 1877-1878 and 1886-1891 followed the geological surveys of G.M. Dawson and A.A. Bowman, respectively, of the Geological surveys of Canada. The Proserpine, Perkins, Black Jack, Bonanza, Steadman, Pinkerton, Enterprise and Island Mountain veins date from this early period.

Within the present Wayside Group and during the late 1870's and 1880's, the B.C. Mining and Milling Company worked the B.C. (Bonanza) vein and the Victoria Company worked the Enterprise and Pinkerton veins (both on the Pinkerton Crown-grant). A.W. Sanders located the Rainbow claims in the 1920's and mined auriferous vein showings at an elevation of about 4,800 feet on a spur of Cow Mountain. These latter workings were close to the core of the Sanders zone where snipers have been active during recent decades.

3.4 Cariboo Gold Quartz Mine (CGQM)

Fred Wells purchased the Rainbow group of claims from A.W. Sanders and incorporated the Cariboo Gold Quartz Mining Company Limited in 1927 for the purpose of exploring these veins. The first adit (1100 level adit) was driven in 1927 from an elevation of 4,375 feet on Lowhee Creek to cut the down dip projection of veins on the Rainbow claims but failed to reach target. The 1500 level adit, driven in 1931 from an elevation of 4,000 feet on the Telluride Crown grant near Jack of Clubs Lake, cut four zones of auriferous quartz veins and made the mine (Guiguet, 1961). Milling operations began at a rate of 50-60 tons per day in 1933, increased to 100 tons per day in 1935 and reached a peak of 350 tons per day in 1941. Early operations were favored by an increase in the price of gold from \$20.67(US) to \$35.00(US) in 1934.

3.4.1 Pre-war Production

The Cariboo Gold Quartz mine (No.1 mine) consists of 36 miles of underground development on 13 levels (900 to 2100 levels) between elevations of about 4,800 and 3,350 feet. Spacing of Levels is 108 feet. The 1500 level, main haulage, extends 10,500 feet to the B.C. shaft. Raises on +70 degrees from the 1500 level and adits on the 1200 level (4300 feet) and 1000 level (4,500 feet) provided access to upper levels of the mine. Three shafts sunk internally from the 1500 level, the No.1 shaft in the No.1 zone, No.2 shaft in the Rainbow zone and the No.3 shaft in the Sanders zone accessed the lower levels. Mineralized zones were interconnected by underground workings by the late 1940's.

By 1941, the productive section of the mine was developed over a strike length of 5,000 feet to the Lowhee fault. Pre-war production was mainly from the No.1,

Rainbow and Sanders zones between the 1500 level and surface. Total production in the No.1 mine for the period 1933 to 1942 was 305,146 ounces from 766,640 tons of quartz-type ore. An average of about 10 tons of quartz-type ore was mined per foot of total development completed during this period.

In 1940-41, the main haulage was extended 5,500 feet to the B.C. vein at the southeast boundary of the Cariboo Group and a -68 degree inclined shaft deepened to 950 feet to meet it. With the exception of the highly productive 15-52 and 15-53A&B stopes in the hanging wall of the Goldfinch fault, little exploration, development or mining was carried out in this drift extension.

In October of 1942, gold mining was classified as a non-war industry by the Federal government and received no priority for labour or supplies. As a result, gold mines in British Columbia were unable to hire replacement labour for the duration of the war. The mine operation never recovered from loss of revenue due to a 50 percent reduction in production and depletion of reserves due to no exploration drilling and minor development during this period. In 1944, the first pyrite-type ore body was found by accident in the Rainbow zone.

3.4.2 Post-war Production

Post-war development was concentrated in the No.1 and Tailings zones below the 1500 level through the No.1-No.2 shaft connection; in the Sanders zone through the No.3 shaft; and in the Pinkerton zone. In 1946, new management failed in an attempt to apply less selective mining methods in the Pinkerton zone, diluted mill feed and wrote off the reserve inventory for this zone.

In 1948, the No. 1 shaft was widened and deepened to the 2100 level and selective stoping of quartz-type ore resumed. A major pyrite-type replacement ore body (172R-B stope; 34,394 tons of 0.70 ounces gold per ton) was discovered in the Tailings zone in 1950 while drilling to determine height of backs below Jack of Clubs Lake. Following purchase of the Island Mountain mine in 1954, the Cariboo Gold Quartz Mining Company Limited focused on development of higher quality pyrite-type replacement ore. Subsequent activities in the No.1 mine were mainly confined to the No.1 and Tailings zones until closure of the No.1 mine on August 31, 1959.

Reserves of 105,010 tons of ore, including a 1952 reserve write down of 46,600 tons of 0.27 ounces gold per ton and an additional 58,410 tons of 0.37 ounces gold per ton scattered in 51 ore remnants through 13 levels and across a distance of 10,500 feet are reported (33rd Annual Report of the Cariboo Gold Quartz Mining Company Limited, 1959).

3.4.3 Mill Tailings

The Cariboo Gold Quartz mill continued operation-using feed from the Aurum mine until March 1967. During 34 years of operation, a total of 2.9 million tons of mill tailings were dumped into the northeast end of Jack of Clubs Lake, significantly altering the original shoreline. The tailings are intercalated with placer tailings, are locally 250 feet thick and comprise the flat area adjacent to the lake and southwest perimeter of the town. The average recovery for the history of the mill was 95.3%.

3.5 Subsequent Exploration Programs

3.5.1 Cariboo Gold Quartz Mining Company Limited (1968)

In 1968, Dolmage Campbell & Associates Ltd. Carried out a 3.1 mile (5km), bulldozer-trenching program on behalf of the Cariboo Gold Quartz Mining Company Limited. The objective of the program was to find surface replacement ore in the Aurum limestone unit. The Baker-Rainbow contact was explored over a strike length of 2.5 miles (4km) with cross-trenches on Island Mountain, Cow Mountain and two long trenches on Barkerville Mountain, located the Baker-Rainbow contact but failed to find the 339 (Aurum) limestone unit at this contact.

17 trenches, 8 to 16 feet deep, were cut across the Baker-Rainbow contact over a strike length of 1 mile (1.6km) on Island Mountain. Pyrite-type mineralization (20 feet in length and 3 feet in width) was discovered in Trench J.

3.5.2 Wharf Resources Ltd. (1980-1981)

Wharf Resources Ltd. carried out surface drilling programs in 1980 and 1981 to search for near-surface ore on the Cariboo and Island Mountain groups. A total of 23,000 feet (7010m) of percussion drilling and 4,000 feet (1220m) of diamond drilling were completed in 1980 and 1981 (Bolin, 1984). The open-pit potential in the Sanders zone was the main focus of work.

3.5.3 Blackberry Gold Resources Inc. (1988)

In 1987, Blackberry Gold Resources Inc. completed several exploration programs on the Arch 1-4 claim group located on Cow Mountain and Richfield mountains. The objective of the work was discovery of gold mineralization in association with the system of northerly striking fault structures. Ground VLF geophysical surveys were used to define conductors inferred to represent the strike extension of major faults on the Cariboo Group of Crown-granted mineral claims. Four strong conductive trends were tested along six fences of percussion drill holes comprising a total of 7,956 feet of drilling in 79 holes. This was followed by 8,089 feet of diamond drilling in 19 holes.

3.5.4 Pan Orvana Resources Inc. (1989-1991)

Pan Orvana Resources Inc. developed an integrated program of surface exploration including the following (Table 2):

TABLE 3 - Pan Orvana Resources Inc. Exploration History

Activity	Quantity	
grid lines	8.0 miles	(12,920m)
road construction	1.5 miles	(2,350m)
surface trenches (20 trenches)	1.4 miles	(2,269m)
diamond drilling (4 holes)	1155 feet	(353m)
ground geophysical surveys:		
IP	13.9 miles	(22.2km)
Radiometric	33.9 miles	(54.5km)
VLF	5.0 miles	(8.0km)
	Total: 63 miles	(84.7km)
geochemistry:		
1988 grid	40m x 200, grid of property	
1989 grid fill in	200	
soil profiles	29	
geological mapping:		
trenches	1:500 scale	
ore zones	1:1,000 scale	
property	1:2,000 scale	

Trenching and sampling in the Sanders zone defined a northerly striking zone with an average grade of 0.119 ounces gold per ton across an average width of 66 feet and over a length of 270 feet (Table 3). Pan Orvana Resources Inc. also explored the Wells trend, defined by >225 ppb gold and associated base metal anomalies in soils, within the B.C. argillite unit or footwall section of stratigraphy.

TABLE 4 - Trench Results of Pan Orvana Resources Inc. in the Sanders Zone

Trench	Grade (ounces gold per ton)	Width (feet)
3	0.137	46
1A	0.120	66
4	0.085	85
2A	0.149	66

3.5.5 Gold City Mining Corporation, Welbar Project (1995)

In 1994 and 1995, Gold City Mining Corporation assembled a large mineral land position consisting of 32,000 acres (13,000 hectares) between Mount Tom and the Cariboo Hudson mine. This involved seven option agreements including one with Mosquito Creek, Island Mountain, and Cariboo groups. The latter was subject to the Cariboo Option Agreement between Mosquito Consolidated Gold Mines Ltd.

and International Wayside Gold Mines Ltd. Intera Information Technologies Corporation flew a synthetic aperture radar survey covering 1,000 square kilometers in July 1995. Dighern I Power completed a regional radiometrics-magnetics-electromagnetic, airborne geophysical survey consisting of 795 line miles (1,280 line kilometers) in surveys, as well as trenching and diamond drilling on some of their properties, including one hole on the Mosquito Creek Group.

3.5.6 International Wayside Gold Mines Ltd. (1995-2000)

Between 1995 and 1998, IWA completed 225 holes totaling 37,724 feet (11,500m) of drilling on Cow Mountain to further test the potential of an open pit resource over the Rainbow, Sanders, and Pinkerton zones. About half of this drilling consisted of underground long-hole percussion drilling from the 1200 level adit of the Cariboo Gold Quartz Mine that had been rehabilitated in 1996. A compilation of this data and all available past work produced a measured resource of 8.6 million tons grading 0.1 ounces of gold per ton as reported by S. M. Dykes (January 19, 1999)

In 1998 and 1999 a secondary target of the Cariboo Gold Project, the BC Vein, was explored over a strike length of 1260 feet (384m) by 31 drill holes from surface, totaling 7366 feet (2245m) with the goal to find high-grade ore shoots of the kind located by the Cariboo Gold Quartz Mining Company in the 1940's. Significant gold values were intersected in nearly every hole.

In the year 2000, air photo covering 10km by 43km at a scale of 1:116000, line cutting, and subsequent geochemical, geophysical and diamond drilling programs were completed on the Cariboo Gold Project property for the purpose of exploring the Bonanza Ledge Zone and BC Vein, and to find new targets of Bonanza Ledge type mineralization away from the initial discovery. A narrow base line staggered along three CGQM grid Northings, totaling 13,200 feet (4km) in length was cut across the property from the northwest side of Cow Mountain to Stout's Gulch hydraulic pit, controlled by a theodolite / EDM ground survey with control points located every 200 feet (60.95m). 46.6km of cross lines were cut to provide control for ground surveys.

The entire grid generated during the line-cutting program was covered by a soil geochemistry survey. Grid lines between 9600E and 13000E were sampled at 100-foot (30.48m) intervals on lines spaced 400 feet (121.91m) apart. Between 13000E and 22800E samples were collected at 50-foot (15.24m) intervals on lines spaced 200 feet (60.95m) apart. An initial orientation survey conducted at the start of the line-cutting program over the Bonanza Ledge zone was sampled every 25 or 50 feet (7.62 to 15.24m) in undisturbed places on lines separated by 100 feet (30.48m).

In addition to the 2,437 samples collected in 2000 by IWA, several other soil geochemistry programs have been carried out previously over Cow and Barkerville mountains. The data from three of these programs have been located within the CGQM grid system (by GPS and ground survey) and compiled into one database. These programs include the 1998 Goldfinch grid (IWA, 90 samples; previously unreported,

assay certificates in Appendix IX, part 5), the 1997 Ditchline survey (IWA, 904 samples; Lord, Reid (1997)), and the 1988-89 Pan Orvana grid (1,484 samples; Laird (1988, 1989)).

Of the 4,915 compiled soil samples, the 90 Goldfinch samples, and 36 of the 2000 IWA samples were only analyzed for gold. Only gold data could be located for 656 samples of Pan Orvana's data (south east area of the Pan Orvana grid). An estimated additional 500 to 1000 samples are known to have been collected on infill lines on the Pan Orvana grid in 1989 but could not be compiled due to the exclusion of Assay Certificates from Laird (1989).

The geophysics program consisted of three parts: a Self Potential survey carried out on an orientation grid, a total field Magnetometer and VLF-EM survey, and an Induced Polarization survey. The Mag, VLF, and IP surveys were contracted out to Scott Geophysics Ltd. of Vancouver B.C. while field assistant Angelique Justason and the author conducted the SP survey. 11,000 feet (3.35km) of grid over the Bonanza Ledge zone was tested in the Self Potential survey.

Between October 19th – 24th 2000, 108,000 feet (32.9km) of magnetometer and VLF-EM survey were completed at 50-foot intervals along the cut lines. Two Scintrex ENVI magnetometer / VLF-EM field units with an operator each took the readings which were corrected for diurnal variations referencing a Scintrex ENVI base station magnetometer.

60,750 feet (18.5km) of IP survey was completed between October 11th and November 1st 2000, using the pole-dipole array with an electrode spacing of 50 feet (15.24m) at "n" separations of 1 to 6. The cut lines at 20200E, 20400E and 20600E were surveyed at "n" separations of 1 to 11. The on current electrode was to the south of the potential electrodes on all survey lines.

Between January 18th and November 20th 2000, 48 diamond drill holes were drilled on the BC Vein and Bonanza Ledge zone for a total of 20,431 feet (6227m) of drilling.

4.0 REGIONAL GEOLOGY - After Hall (1997)

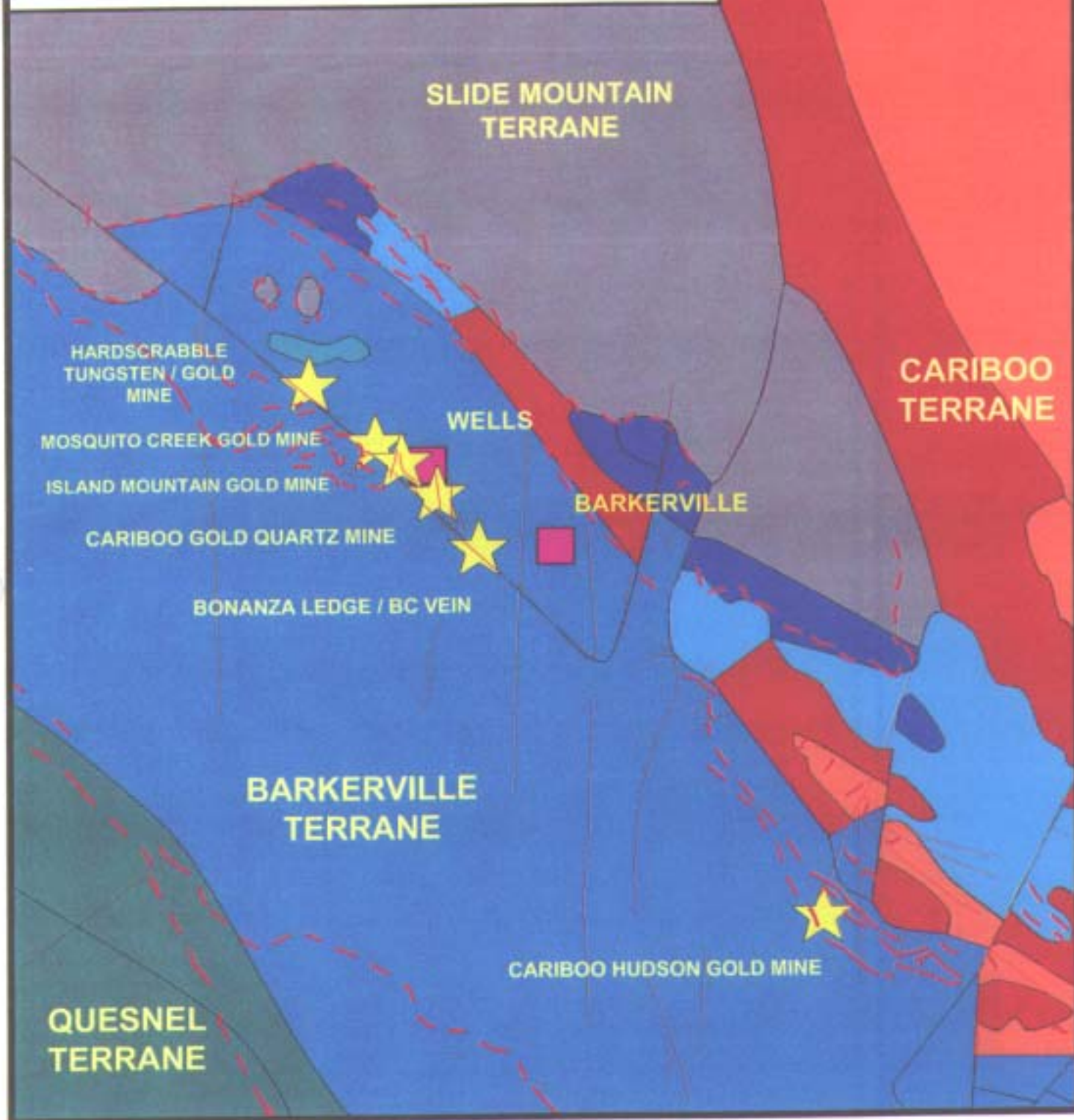
Reports and maps by Bowman (1889, 1895), Johnston and Uglow (1926), Hansen (1935), Sutherland Brown (1957), Struick (1988), and Levson and Giles (1993) are the main geological references for the Cariboo gold mining district. The Cariboo mining district is located in the south central part of the Omineca morpho-geological belt of the Canadian Cordillera (Figure 3) where the following tectonic terranes are recognized.

1. Quesnel Terrane - Early Mesozoic island arc assemblage of basaltic and andesitic pyroclastics, volcanoclastics, greywacke and other sedimentary rocks.
2. Slide Mountain Terrane - Late Paleozoic, rift related oceanic assemblage of submarine pillowed basalt, diorite and chert including some blue schist metamorphic remnants.

CARIBOO GOLD PROJECT

FIGURE 3

REGIONAL GEOLOGY



3. Kootenay (Barkerville) Terrane - Late Proterozoic and Paleozoic sequence of continental shelf and slope deposits including siliceous clastics, lesser volcanics and carbonates.
4. Cassiar (Cariboo) Terrane - Late Proterozoic and Paleozoic sequence of continental shelf clastics and carbonates.

4.1 Barkerville Subterrane

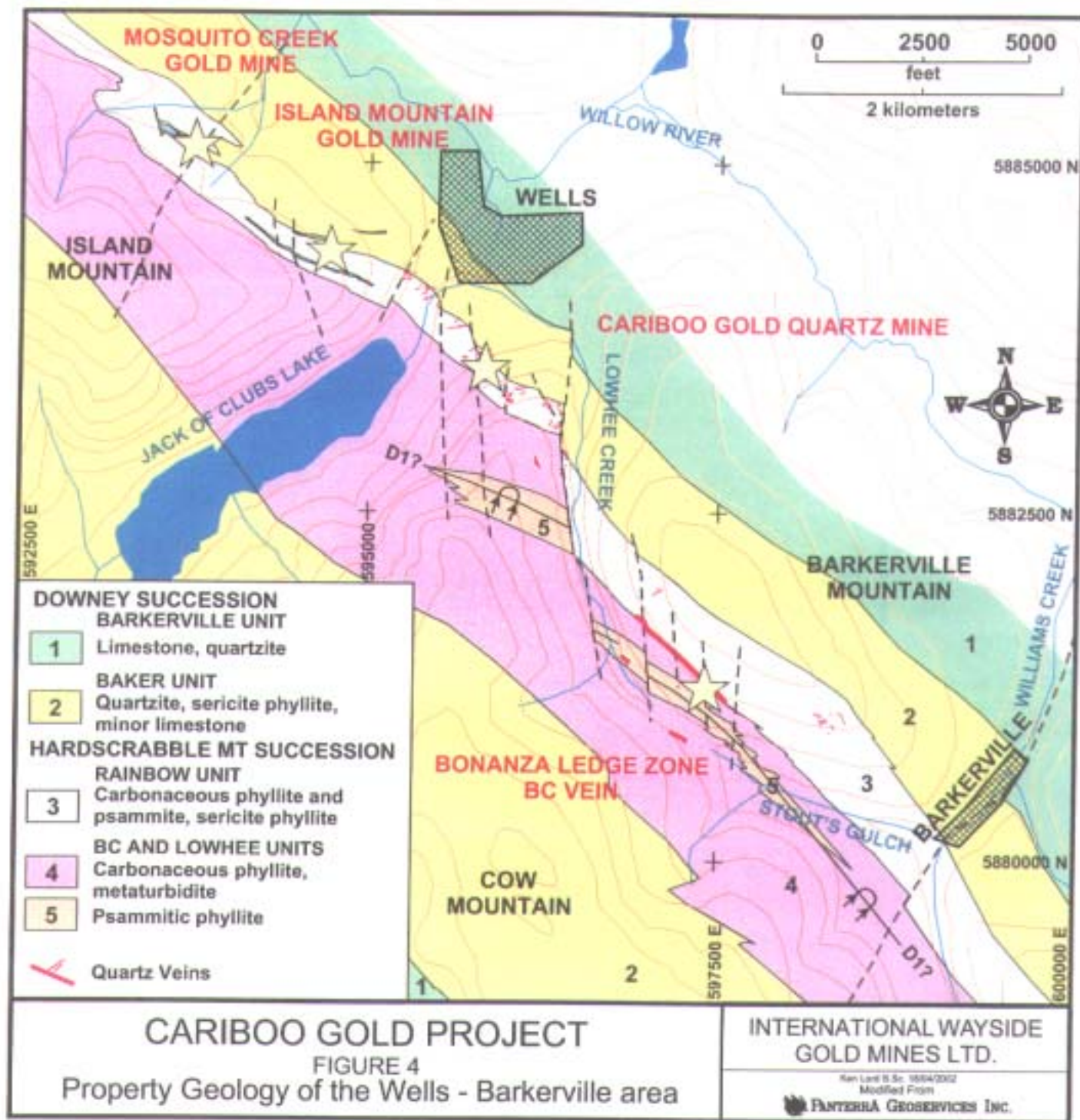
Barkerville subterrane, structurally the lowest exposed stratigraphic sequence, is more deformed and metamorphosed than adjacent terranes. Quesnel, Slide Mountain and Cariboo terranes overlie the Barkerville subterrane above the Eureka, Pundata and Pleasant Valley thrusts, respectively. Westward directed thrusting prior to the eastward-directed emplacement of Slide Mountain Terrane in post-Permian time amalgamated Cariboo and Barkerville subterrane. Klippe of Island Mountain Amphibolite, similar to the Crooked Amphibolite of Slide Mountain Terrane, cap Island Mountain at Wells.

Barkerville subterrane is comprised of possibly Precambrian to Permian metamorphosed grit, quartzite, black and green pelite, lesser limestone and volcanoclastics rocks assigned to the Snowshoe Group. The Downey succession, an approximately 150 meter thick stratigraphic interval within the upper Snowshoe Group constitutes the heart of the Cariboo gold belt. The Cariboo gold belt lies within a lower greenschist facies, metamorphic low characterized by phyllites and the development of pyrite, dolomite and chloritoid porphyroblasts in rocks of appropriate bulk composition.

The Snowshoe Group of Barkerville subterrane has been correlated with Eagle Bay Formation near Adams Lake and the Lardeau Group near Kootenay Lake (Struick, 1986). Correlation with Yukon-Tanana Terrane in Yukon is also likely. All of these have high potential for precious metal-enriched, massive sulfide deposits.

Bedrock was deeply eroded and weathered during Tertiary time. Glacial deposits associated with two phases of advance (125,000 - 60,000; 30,000 - 10,000 YBP) of the Wisconsin Cordilleran Ice Sheet (Fraser glaciation) overlap tectonic terranes. A unit of gray coloured till associated with the late Wisconsin glacial period is widely distributed in the Cariboo Gold Belt. An older, brown-weathered till unit has been identified locally. Valleys are filled with glacial sediments and alluvium to about the 4,000-foot contour. Near Wells, the ice moved to the northwest.

The property geology is primarily governed by the contact between the Rainbow and Baker units that has controlled the exploration and production in the area. The Rainbow is known as the Hardscrabble and the Baker is known as the Downey. The property geology is outlined in figure 4 for the immediate area around the mines at Mosquito Creek, Island Mountain and Cariboo Quartz Gold Mines.



5.0 PROGRAM AND RESULTS

The program in 2001 consisted of 16,883 feet of diamond drilling in 25 drill holes, 20.03 line kilometers of Induced Polarization (IP) data was collected along 22 lines on Cow Mountain, 24.32 kilometers of grid line was completed with Self Potential and 7.19 kilometers of brushing out of lines was completed for the IP survey on 11 lines. These areas of work are all outlined on Figure 5, which shows the claims and crown grants with respect to the areas worked.

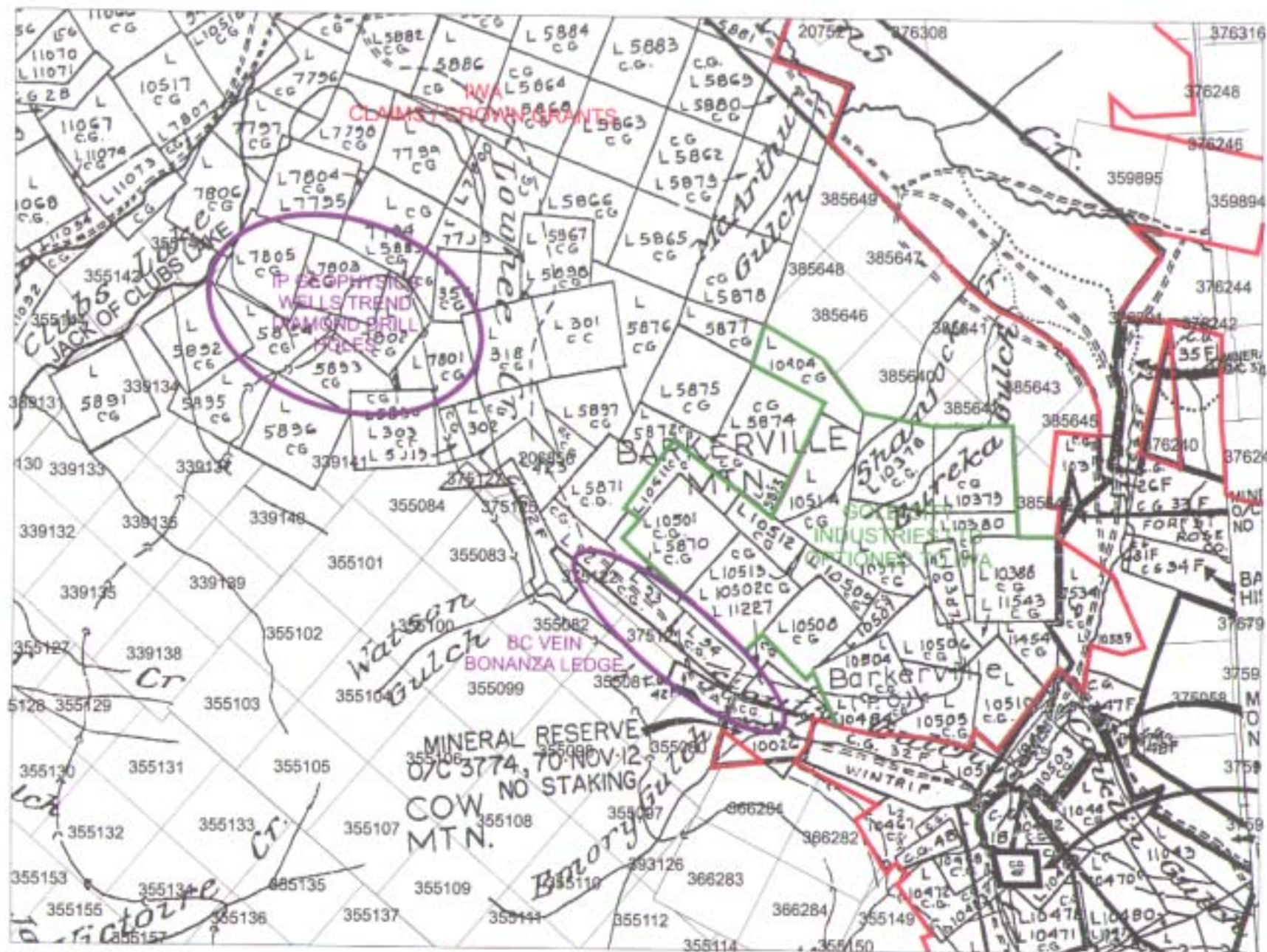
5.1 Diamond drilling

A total of 25 diamond drill holes were completed from April 12 to December 23rd 2001 on Crown Grants 42F, 92, 93, 94, 7802, 7803 and 356. The total footage for the drill holes was 16,883 feet as outlined with the survey information on table 5. Copies of the drill hole logs are attached in Appendix 1. The logs include all of the data collected from the core such as lithology, alteration type and styles, quartz veins and stringers, faults and sulphide content. This data has been combined with assay data from core samples and sludge samples for the holes.

Standard Drilling using a Longyear 38 drilled the holes. Core was collected using a wire line NQ system and placed in NQ core boxes. Lids were secured with nails and the boxes were transported to a secure drill compound where it was logged and sampled. Samples were marked by the geologist logging the core and based upon parameter seen in the core. The sampler who uses a diamond saw to cut the core so that ½ can be sent for assay and ½ can be retained on site for future calculation then takes the core. The remaining core is stored in a weatherproof building erected in the compound. All samples were then shipped to Acme laboratories in Vancouver for analysis. The assay certificates and the assaying procedure are shown in Appendix 6.

The purpose of the 2001 program was to establish the on strike extension of the BC vein and Bonanza Ledge mineralization and understand the timing and style of the mineralization form. Once an understanding of the deposits was established then it would be easier to locate more mineralized bodies like the Bonanza Ledge. In reviewing previous workers reports from present to the 1860's and logging of the entire old core, the following interpretations have been made:

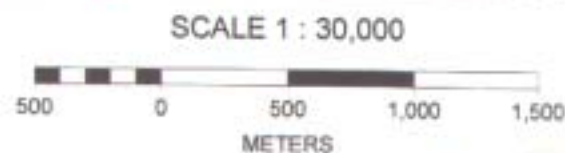
1. Mineralization is associated with a crustal scale fault or break. This is supported by the linear alignment of deposits (Hardscrabble Mine, Mosquito Mine, Island Mountain mine, Cariboo Gold Quartz Mine.), main quartz veins and significant placer production creeks.
2. Bonanza Ledge is a replacement style deposit in calcareous and carbonaceous mudstone and siltstone.
3. Bonanza Ledge has a rod like morphology and is comprised of multiple lenses, which are almost horizontal.



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CARIBOO GOLD PROJECT

FIGURE 5
2001 CLAIMS / CROWN GRANTS
WORK LOCATIONS

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↑
TS 093H04W



4. Bonanza Ledge appears to follow the F2 or L2 just like the replacement mineralization at Island Mountain. The Lineation has been measured by Rhys and is almost horizontal.
5. The quartz veins at Island Mountain and Mosquito act as feeders to the replacement ore zones.
6. The quartz veins occur in the more competent rocks of the Rainbow-quartz rich siltstone, arenites and the replacement zones occur in the more chemically reactive units of the Baker and Lowhee Stratigraphy.
7. The apparent sequence of mineralizing events is the breaking of the competent rocks (Rainbow) allowing fluids to move upward through the units and then outward to create replacement zones in the Baker rocks when the veins intersect the limestones in the Baker unit.
8. Gold in the Bonanza Ledge is located on the edge of pyrite grains and in fractures in the pyrite grains. It suggests gold is emplaced late in the mineralizing sequence.
9. Quartz veins appear to be concentrated around the northerly striking faults, with the veins reducing in size away from the faults. The northerly faults are one of the controls for the localization of the mineralization.
10. Northerly Faulting has occurred early and in some cases after mineralization.
11. The replacement bodies at Bonanza Ledge are larger because of the host rock at Bonanza are calcareous mudstones and siltstones as opposed to the limestones at Island Mountain.
12. The expectations are that veins can be followed across the Rainbow unit to the chemically active Baker or Lowhee units to locate the replacement zones. This model suggests that the mineralized area is approximately 1000 feet across by 4 miles in length with mineralization focused near the northerly faults.
13. Continuity of mineralization is clearly demonstrated in the mined stopes at Island Mountain, Mosquito Mines and Cariboo Gold Quartz mines. The rod shape bodies follow the plunge of the F2 (-22° to the Northwest) and continuity along that plunge is very good.
14. The alteration consists of introduction of K (muscovite), Mg (dolomite, ankerite), Fe (ankerite, pyrite) and Si (flooding and veins).
15. Pyrrhotite appears to have a negative correlation with gold. The Pyrrhotite is either early, at the same time or later than the mineralization. It is the interpretation of the author that the Pyrrhotite is early and is possibly early in the metamorphic sequence.
16. Mineralization may be related to peak metamorphism. This is based upon the dating of sericite.
17. The main gold area is in the greenschist facies metamorphic grade as opposed to the biotite grade metamorphism that is seen to the south of Quesnel Lake and to the North.
18. The different fineness and trace elements seen in the placer gold in the area suggests that there could be several gold mineralizing events.

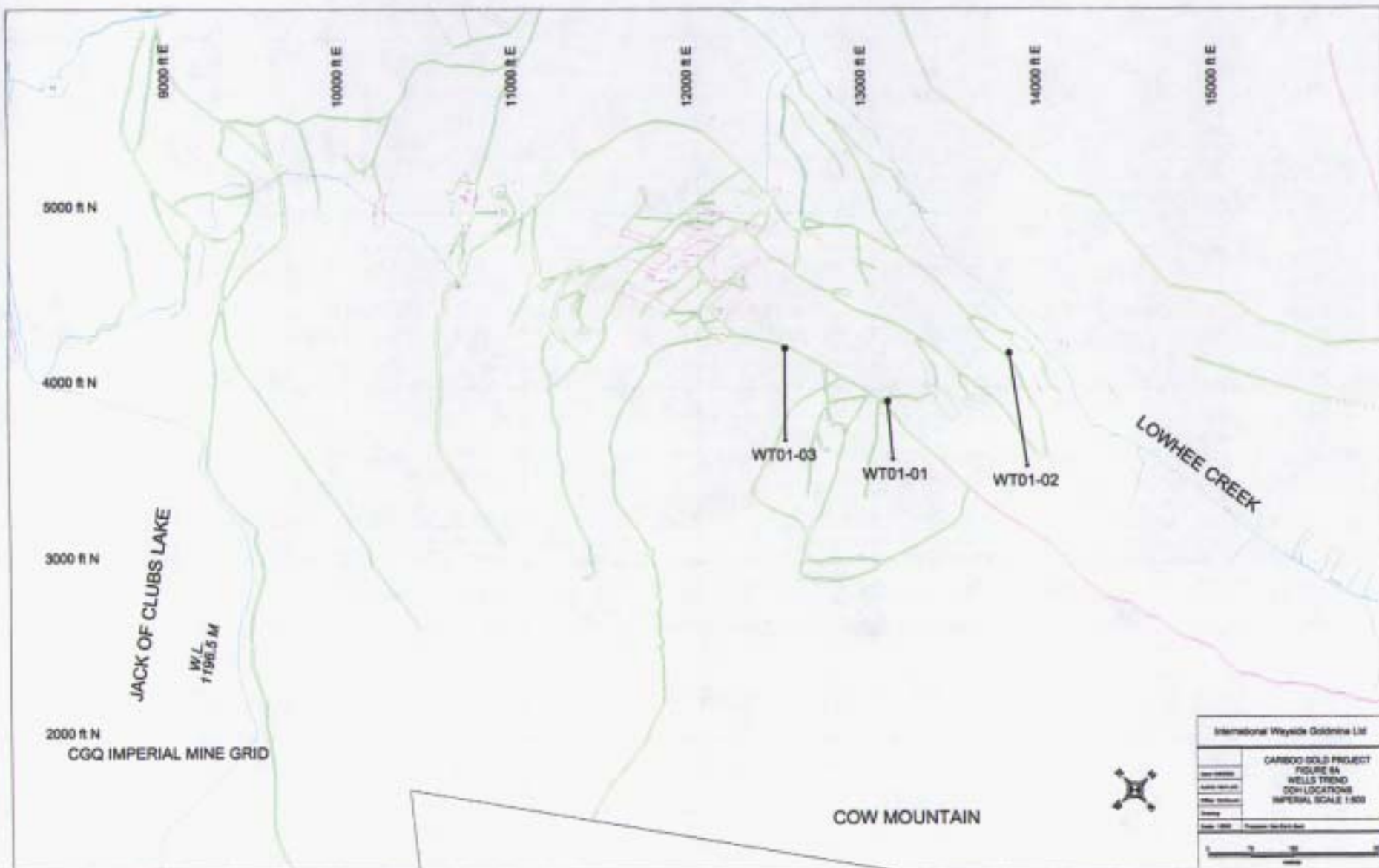
Table 6 outlines the significant assays obtained in the 2001-drilling program. The drill hole intersections were obtained from the BC Vein and Bonanza Ledge area. An

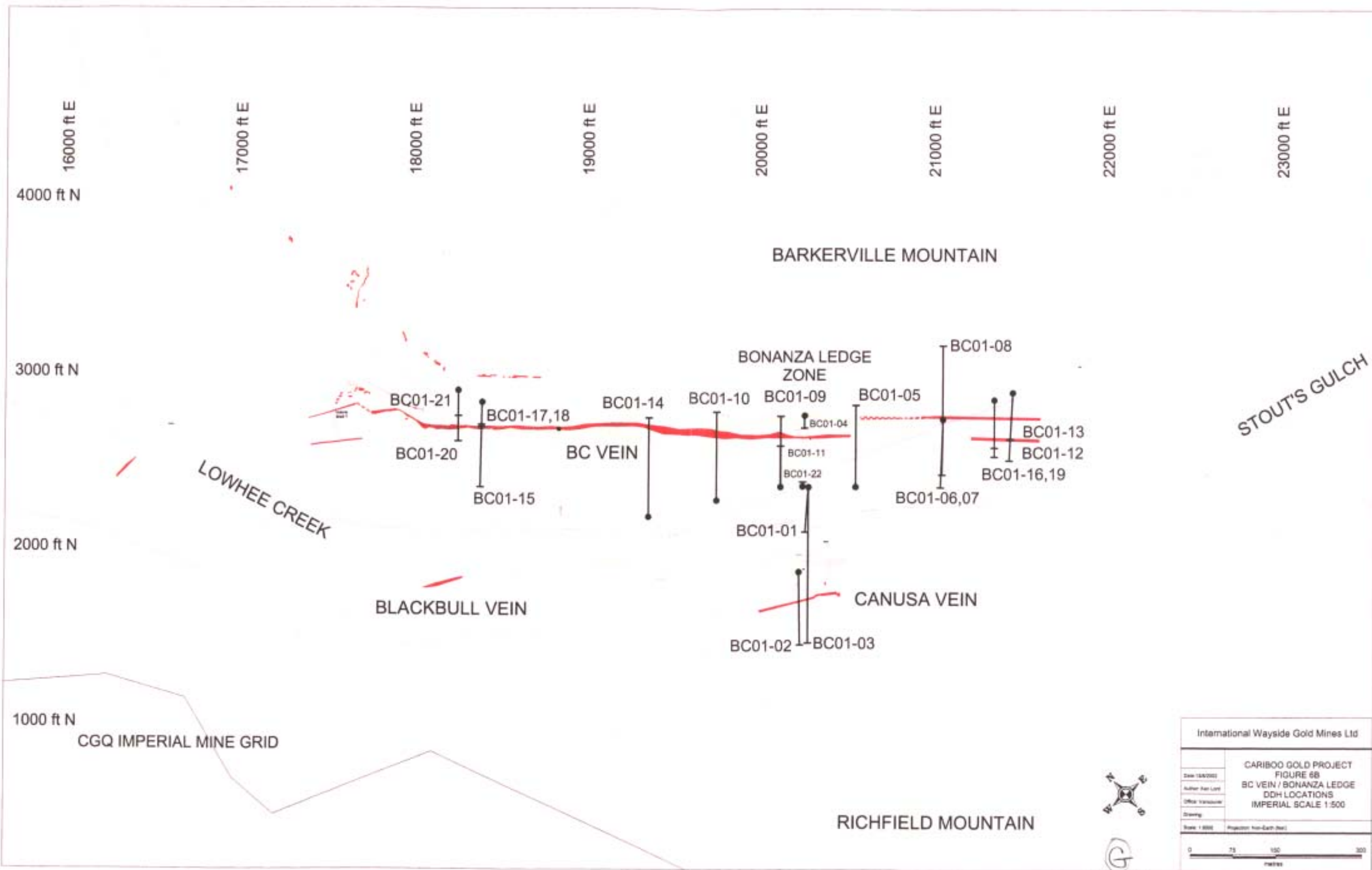
TABLE 5 - Drill Hole Survey Data

CGQM GRID		B C	VEIN	BONANZA	LEDGE	WELLS	TREND			
DRILL	TRUE	GRID			COORD COLLAR			COORD TAIL		
HOLE	AZIMUTH	BEARING	INCL	LENGTH	NORTHING	EASTING	ELEV	NORTHING	EASTING	ELEV
BC01-01	227	184	-69	720	2391	20229	4773	2134	20211	4101
BC01-02	223	180	-45	1260	2390	20229	4773	1499	20229	3882
BC01-03	222	179	-45	590	1906	20176	4718	1489	20183	4301
BC01-04	223	180	-80	410	2801	20206	4849	2730	20206	4445
BC01-05	43	0	-38	590	2396	20500	4756	2861	20500	4393
BC01-06	225	182	-49	590	2778	21000	4786	2391	20986	4341
BC01-07	224	181	-70	920	2778	21000	4786	2463	20995	3921
BC01-08	43	0	-50	640	2791	20999	4786	3202	20999	4296
BC01-09	43	0	-60	805	2395	20070	4784	2798	20070	4087
BC01-10	43	0	-60	1010	2316	19701	4789	2821	19701	3914
BC01-11	43	0	-52	377	2394	20068	4785	2626	20068	4488
BC01-12	226	183	-42.5	530	2934	21401	4787	2544	21381	4429
BC01-13	226	183	-60	537	2935	21401	4787	2667	21387	4322
BC01-14	43	0	-45	800	2219	19306	4782	2785	19306	4216
BC01-15	224	181	-41	637	2869	18341	4973	2388	18333	4555
BC01-16	223	180	-45	463	2893	21295	4787	2566	21295	4460
BC01-17	224	181	-60	250	2872	18341	4973	2747	18339	4756
BC01-18	224	181	-80	800	2874	18341	4973	2735	18339	4185
BC01-19	223	180	-62	589	2894	21295	4787	2617	21295	4267
BC01-20	223	180	-65	690	2940	18205	4990	2648	18205	4365
BC01-21	223	180	-80	840	2940	18205	4990	2794	18205	4163
BC01-22	46	3	-88	690	2398	20195	4776	2422	20197	4086
WT01-01	218	175	-45	475	3925	13085	4794	3590	13114	4458
WT01-02	214	171	-45	925	4199	13777	4655	3553	13879	4001
WT01-03	223	180	-45	745	4228	12497	4801	3701	12497	4274
			Total	16,883						

TABLE 6 - 2001 Drill Hole Intersections

Drill Hole	From (ft)	To (ft)	Length (ft)	Au g/tonne	Au oz/ton
3 [#]	75.7	76.7	1	38.84	1.133
#	294.0	295.7	1.7	5.37	0.157
5	101.8	103.8	2	13.04	0.38
6	165.0	195.0	30	0.42	0.012
7	763.0	764.0	1	1.43	0.042
8*	35.0	50.0	15	15.51	0.452
9	203.7	269.0	65.3	3.29	0.096
11	209.6	234.6	25	7.32	0.213
12	130.2	137.0	6.8	1.75	0.051
	193.3	205.9	12.6	3.15	0.092
13	93.0	97.0	4	8.64	0.252
15*	142.8	186.0	43.2	5.97	0.188
16	198.4	200.3	1.9	3.07	0.09
17*	163.1	170.5	7.4	2.0	0.056
	187.5	189.2	1.7	1.39	0.041
18	69.6	70.8	1.2	10.43	0.304
*	228.1	234.4	6.3	1.24	0.036
	238.2	253.7	15.5	7.27	0.212
20	254.3	281.4	27.1	8.0	0.233
21	362.6	378.5	15.9	4.44	0.129
WT-02	447.7	449.5	1.8	22.83	0.666
WT-03	422.7	430.3	7.6	3.03	0.088





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International Wayside Gold Mines Ltd	
CARIBOO GOLD PROJECT FIGURE 6B BC VEIN / BONANZA LEDGE DDH LOCATIONS IMPERIAL SCALE 1:500	
Date: 15/05/2001	
Author: Dan Lott	
Office: Vancouver	
Drawing:	
Scale: 1:500	Projection: UTM (Zone 18N)

additional 22 intersections were obtained to extend the mineralized area to 3500 feet in strike with it still open in all directions. All of these intersections are within 300 feet of the surface, which could be extracted in a long pit. There are now 104 drill holes into the BC Vein and Bonanza mineralized bodies with 88 significant intersections over the last four years.

5.2 Induced Polarization Survey

SJ Geophysics completed a total of 22 lines of Induced Potential (IP) survey on Cow Mountain. A report on the survey and the pseudosections for each line showing the chargeability and resistivity values and modeling of that data using the UBC Inversion technique are presented in Appendix 2.

The IP survey was completed on the Wells trend area to complete the IP coverage south of Jack of Clubs Lake. It was found in 2000 that IP located the Bonanza Ledge Discovery zone because of the increased sulphide content (up to 70%). Outside of the initial discovery area there were more graphite horizons, faults and sulphides not related to the mineralization that caused problems along the length of the BC Vein.

The survey completed in 2001 covered the Wells Trend as outlined in Figure 7. The Wells trend is interpreted to be the northwest extension of the Bonanza Ledge stratigraphy. Within the survey an argillite cap was outlined on Cow Mountain, which was not possible to have the current go below the cap. The lines were extended to see if some current could be pushed into the underlying sediments, however the argillite cap was too conductive, more meaningful data was collected either southeast or northwest survey from the argillite cap.

Some targets have been outlined on the IP profiles as shown in Appendix 3. They correlate well with the targets outlined in the Self Potential report by Ms. A. Justason in Appendix 4.

5.3 Self Potential Survey

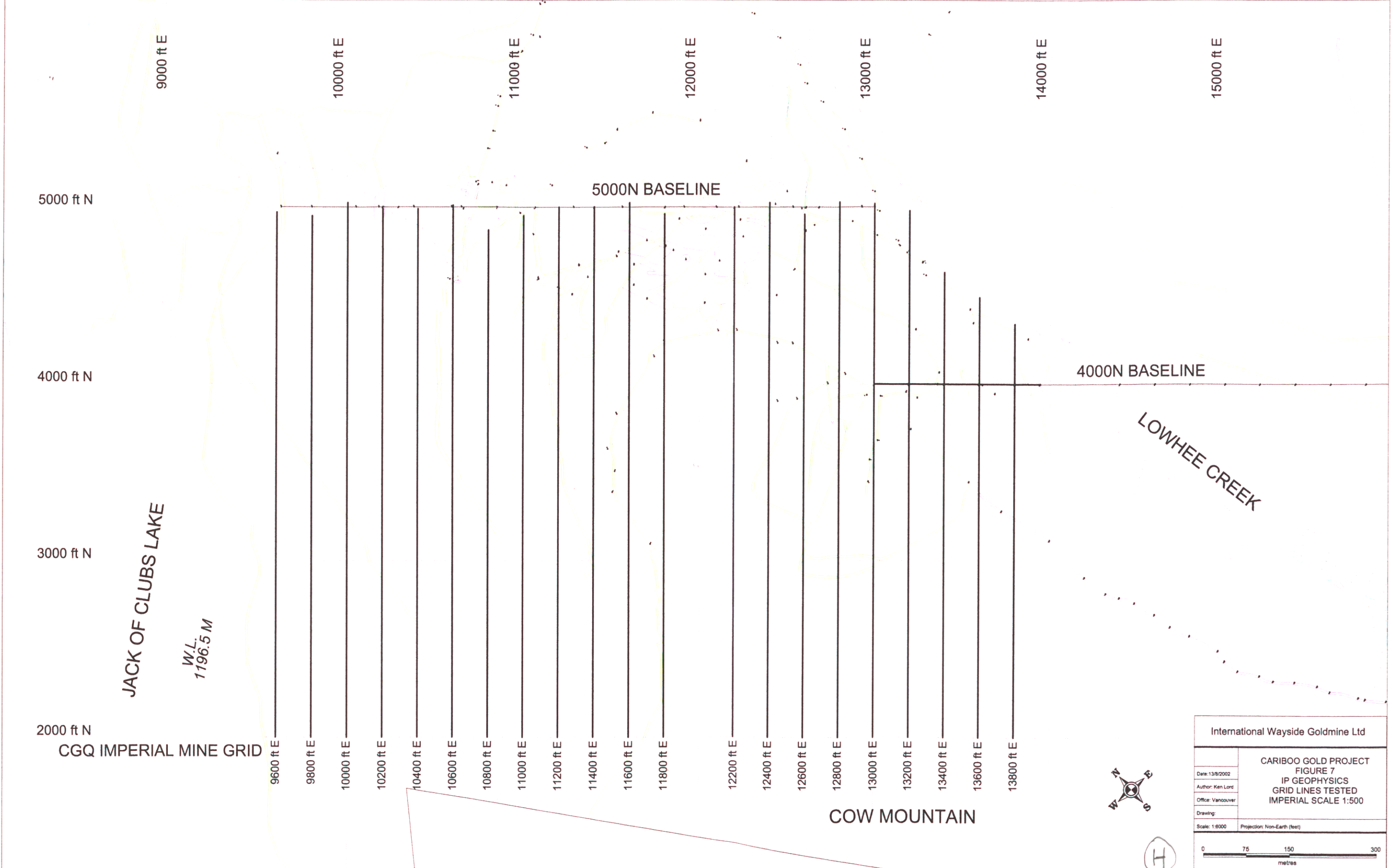
The self potential (SP) work soon completed by Ms. Justason and is summarized in her report in Appendix 4. She identifies several targets as outlined on the map for further follow up.

The SP appears to provide a similar response to the IP data however it cannot penetrate to the same depth. SP survey are easier to operate and can be completed by company personnel.

6.0 CONCLUSION

The drilling continues to outline more gold along the BC Vein and Bonanza Ledge area. It is encouraging to be able to continue drilling more intersections along this major structure. The Company has been drilling the Bonanza Ledge and BC Vein for 4 consecutive years. All of the intersections are shallow and could be extracted in an open pit.

Further drilling in 2002 is warranted along strike to determine the extent of the mineralization. Infill drilling will be required to provide better continuity estimates, however that will not be completed until an estimate has been made of the resource currently defined by the four years of drilling.



International Wayside Goldmine Ltd	
Date: 13/8/2002	CARIBOO GOLD PROJECT FIGURE 7 IP GEOPHYSICS GRID LINES TESTED IMPERIAL SCALE 1:500
Author: Ken Lord	
Office: Vancouver	
Drawing:	
Scale: 1:5000	Projection: Non-Earth (feet)

0 75 150 300
metres



(H)
26906

The IP and SP surveys have outlined more targets for follow up drilling, prospecting and geological mapping. The combined work indicates that there is a structural corridor where there is a good opportunity to intersect gold mineralization either in replacement bodies or in quartz veins. The styles of mineralization appear to be related to the host lithology i.e. potentially replacement style or brittle.

The project is encouraging and further drilling is warranted to determine the extent of the mineralization and locate other bodies of mineralized rock.

7.0 STATEMENT OF EXPENDITURES

The statement of accounts show in Appendix 5 covers the costs for the diamond drilling and geophysical surveys carried out in 2001. The work that was carried out was 7.19 kilometers of line brushing out, 20.03 kilometers of ground Induced Polarization and 24.32 line kilometers of Self Potential. The total cost of the program was \$763,403.21CAN.

APPENDIX 1 - Drill Hole Logs

BC01-01
BC01-02
BC01-03
BC01-04
BC01-05
BC01-06
BC01-07
BC01-08
BC01-09
BC01-10
BC01-11
BC01-12
BC01-13
BC01-14
BC01-15
BC01-16
BC01-17
BC01-18
BC01-19
BC01-20
BC01-21
BC01-22
WT01-01
WT01-02
WT01-03

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[illegible]

D.D.H. BC01-01

Page 3 of 3

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
386.2-402.0	strongly sericitized								
414.0-483.0	chloritized								
450.0-472.0	quartz stringers								
483.0-488.5	strongly sericitized and weakly dolomitized								
488.5-503.0	chloritized								
495.6-502.8	quartz stringers								
502.8-710.0	Arenite								
	medium to thin layering								
503.0-584.0	strongly dolomitized								
570.0-592.0	quartz stringers								
584.0-595.5	chloritized								
592.0-596.0	fault								
602.5-603.5	fault								
613.5-655.5	chloritized								
682.9-698.0	fault								
					698.0-720.0		1.0		
698.8-711.0	chloritized								
710.0-720.0	Grit								
	thin layering								
712.0-713.5	quartz stringers								
714.5-720.0	fault								
720.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-02

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: March 21, 2001
 Date Completed: April 11, 2001
 Final Depth: **1260 feet (384.0 m)**

Collar Grid Coordinates
 Northing Easting Elevation
 Mine Grid 2390.0 ft. 20229.0 ft. 4772.6 ft.

Logged by: J. Pautler and R.D. Hall

Depth	Azimuth	Dip
collar	223°	-45°
650.0 ft.	223°	-40°
1260.0 ft.	223°	-41°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-60.0	Overburden								
60.0-240.0	Arenite medium layering								
		60.4-76.5	0.5						
			344045	core	60.4	64.3	<0.01	<0.001	3.9
			344046	core	64.3	68.6	<0.01	<0.001	4.3
		76.5-89.8	1.0						
		89.8-100.0	0.5						
		100.0-105.5	1.0						
		105.5-140.0	0.5						
		140.0-160.0	1.0						
		160.0-186.4	0.5						
167.3-168.0	fault		344047	core	167.3	171.5	<0.01	<0.001	4.2
171.5-175.7	strongly sericitized and moderately dolomitized		344048	core	171.5	175.7	<0.01	<0.001	4.2
175.7-186.4	strongly dolomitized and moderately chloritized		344049	core	175.7	180.5	<0.01	<0.001	4.8
177.6-177.7	fault		344050	core	180.5	186.4	<0.01	<0.001	5.9
183.0-183.1	fault								
		186.4-208.1	trace						
186.4-208.1	strongly sericitized and moderately dolomitized								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
201.3-201.6 203.6-216.3	fault quartz stringers		344051	core	186.4	190.4	0.01	<0.001	4.0
			344052	core	190.4	195.1	<0.01	<0.001	4.7
			344053	core	195.1	199.1	0.01	<0.001	4.0
			344054	core	199.1	203.6	<0.01	<0.001	4.5
208.1-265.4	strongly dolomitized and moderately chloritized	0.5	344055	core	203.6	208.1	<0.01	<0.001	4.5
			344056	core	208.1	212.1	<0.01	<0.001	4.0
			344057	core	212.1	216.3	<0.01	<0.001	4.2
230.5-294.9	fault	1.0	344058	core	224.9	225.9	0.02	0.001	1.0
			344059	core	230.5	236.0	<0.01	<0.001	5.5
			344060	core	236.0	240.0	<0.01	<0.001	4.0
240.0-331.9	Grit medium layering fault								
			344061	core	250.0	255.3	0.01	<0.001	5.3
			344062	core	255.3	260.0	<0.01	<0.001	4.7
			344063	core	260.0	265.4	0.01	<0.001	5.4
290.9-294.9	quartz stringers								
294.9-300.2	quartz stringers	4.0	344064	core	290.9	295.3	<0.01	<0.001	4.4
			344065	core	295.3	300.0	0.03	0.001	4.7
300.2-393.8	quartz stringers	1.0	344066	core	300.0	304.7	<0.01	<0.001	4.7
			344067	LG Standard			1.67	0.049	
			344068	HG Standard			6.66	0.194	
317.6-318.4	fault								
317.6-318.4	quartz stringers								
318.4-331.9	quartz stringers								
322.0-336.8	strongly dolomitized								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
331.9-336.4	quartz stringers								
331.9-393.8	Calcareous Arenite medium layering								
			344069	core	331.9	336.5	<0.01	<0.001	4.6
			344070	core	336.5	341.9	0.01	<0.001	5.4
336.8-385.8	strongly sericitized and moderately dolomitized								
			344071	core	341.9	346.6	<0.01	<0.001	4.7
			344072	core	346.6	351.7	<0.01	<0.001	5.1
348.7-349.6	fault								
			344079	core	351.7	360.0	<0.01	<0.001	8.3
			344080	core	360.0	365.0	0.01	<0.001	5.0
			344081	core	365.0	370.0	<0.01	<0.001	5.0
			344082	core	370.0	375.0	<0.01	<0.001	5.0
			344083	core	375.0	380.0	<0.01	<0.001	5.0
			344084	core	380.0	385.0	<0.01	<0.001	5.0
			344085	core	385.0	390.0	0.01	<0.001	5.0
			344073	core	390.0	393.6	<0.01	<0.001	3.6
			344074	core	393.6	395.7	1.29	0.038	2.1
		5.0							
393.8-395.7	quartz vein								
393.8-486.3	Grit medium layering								
		1.0							
			344075	core	395.7	398.3	<0.01	<0.001	2.6
			344076	core	404.2	405.2	0.01	<0.001	1.0
			344077	core	405.2	408.2	<0.01	<0.001	3.0
419.4-419.7	fault								
424.4-429.6	fault								
457.0-460.0	quartz stringers								
			344078	core	457.0	460.0	0.01	<0.001	3.0
			344087	core	HG Standard		7.02	0.205	
			344088	core	LG Standard		1.70	0.050	
463.0-465.0	fault								
473.0-479.0	fault								
482.7-486.3	chloritized								
484.6-487.6	quartz stringers								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
763.7-766.1	quartz stringers								
		770.5-772.0	0.5						
771.5-781.5	chloritized								
		772.0-776.0	2.0						
772.0-776.0	quartz vein								
		776.0-1020.0	0.5						
790.1-792.0	Pelite very thin layering								
792.0-812.2	Calcareous Arenite thin layering								
794.9-800.8	quartz stringers								
812.2-813.5	Pelite very thin layering								
813.5-897.3	Calcareous Arenite thin layering								
823.8-879.3	strongly dolomitized and moderately chloritized								
837.0-849.0	quartz stringers								
897.3-910.5	quartz stringers								
897.3-910.5	strongly dolomitized								
897.3-1048.2	Arenite thin layering								
931.5-978.8	quartz stringers								
931.5-978.8	strongly dolomitized and moderately chloritized								
1000.0-1024.0	quartz stringers								
		1020.0-1048.2	1.0						
		1048.2-1260.0	trace						
1048.2-1055.0	Calcareous Arenite thin layering								
1055.0-1087.0	strongly dolomitized								
1055.0-1087.0	Arenite thin layering								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
1061.5-1069.5	quartz stringers								
1087.0-1101.0	Calcareous Arenite thin layering								
1101.0-1110.5	quartz stringers								
1101.0-1114.0	strongly dolomitized and moderately chloritized								
1101.0-1238.3	Arenite thin layering								
1169.9-1170.9	quartz stringers								
1238.3-1260.0	Graphitic Pelite very thin layering								
1260.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-03

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: March 12, 2001
 Date Completed: March 20, 2001
 Final Depth: **590 feet (179.8 m)**

Collar Grid Coordinates

Northing	Eastng	Elevation
1906.0 ft.	20176.0 ft.	4718.0 ft.

 Mine Grid

Logged by: R.D. Hall and J. Pautler

Depth	Azimuth	Dip
collar	222°	-45°
150.0 ft.	216°	-44°
590.0 ft.	224°	-41°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-14.0	Overburden								
14.0-219.6	Arenite and Pelite								
14.0-46.2	very thin layering strongly dolomitized								
		14.0-30.5	1.0						
			344001	core	15.5	16.5	<0.01	<0.001	1.0
			344002	core	24.3	27.3	<0.01	<0.001	3.0
		30.5-46.2	0.0						
			344003	core	42.8	46.2	0.17	0.005	3.4
46.2-48.5	quartz vein	46.2-48.5	5.0						
			344004	core	46.2	48.5	0.07	0.002	2.3
		48.5-62.3	0.0						
			344005	core	48.5	51.5	0.05	0.001	3.0
51.0-51.4	quartz vein								
62.3-107.9	strongly dolomitized								
		62.3-76.0	1.0						
			344006	core	73.7	75.7	0.09	0.003	2.0
			344007	core	75.7	76.7	38.84	1.133	1.0
76.0-76.5	quartz vein	76.0-76.5	50.0						
		76.5-82.4	1.0						
			344008	core	76.7	78.6	0.03	0.001	1.9

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
82.4-83.5	quartz vein		344009	core	78.6	82.1	0.04	0.001	3.5
			344010	core	82.1	84.5	0.03	0.001	2.4
		82.4-83.5	0.0						
		83.5-93.0	1.0						
		93.0-99.0	0.0						
104.7-105.9	quartz vein	99.0-104.7	1.0						
		104.7-105.9	10.0						
			344011	core	104.7	105.9	0.01	<0.001	1.2
		105.9-121.8	1.0						
			344012	core	105.9	107.9	<0.01	<0.001	2.0
121.8-123.3	fault								
124.2-125.0	quartz vein	121.8-124.2	1.5						
			344013	core	123.3	125.3	<0.01	<0.001	2.0
		124.2-125.0	0.0						
129.2-130.8	quartz stringers	125.0-144.0	1.5						
			344014	core	138.7	143.3	<0.01	<0.001	4.6
			344015	core	143.3	150.8	<0.01	<0.001	7.5
144.0-150.8	fault								
160.0-170.0	chloritized								
183.0-195.0	fault								
190.0-190.3	quartz vein		344016	core	183.0	191.0	<0.01	<0.001	8.0
		190.0-190.3	0.0						
		190.3-413.2	0.5						
213.4-213.5	fault								
218.2-218.3	fault								
219.6-295.7	Arenite								
	medium layering								
257.7-260.0	quartz stringers								
			344017	core	257.7	263.9	<0.01	<0.001	6.2
261.6-263.8	quartz stringers								
270.8-286.2	quartz stringers								

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From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
286.2-294.0	quartz vein		344018	core	284.5	286.2	<0.01	<0.001	1.7
			344019	core	286.2	290.0	<0.01	<0.001	3.8
			344020	core	290.0	291.7	0.01	<0.001	1.7
			344021	core	291.7	294.0	0.01	<0.001	2.3
294.0-295.7	quartz vein								
			344022	core	294.0	295.7	5.37	0.157	1.7
295.7-341.8	Grit medium layering								
295.7-308.0	quartz stringers								
			344023	core	295.7	298.4	0.03	0.001	2.7
			344024	LG Standard			1.71	0.050	
			344025	HG Standard			6.73	0.196	
329.6-340.5	quartz stringers								
341.8-343.0	Pelite very thin layering								
343.0-345.0	Grit medium layering								
345.0-356.0	Arenite thin layering								
353.3-396.5	strongly dolomitized								
356.0-395.5	Calcareous Arenite thin layering								
395.5-440.8	Arenite and Pelite medium layering								
403.2-403.8	fault								
411.2-413.2	quartz vein								
					413.2-414.0		3.0		
414.0-415.4	quartz vein								
					414.0-421.8		0.5		
421.8-423.3	quartz vein								
					421.8-423.3		1.0		

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
		423.3-524.6	0.5						
440.8-471.2	Grit and Pelite thick layering								
460.0-462.5	quartz stringers								
462.5-463.0	quartz stringers								
462.5-463.0	fault								
463.0-467.0	quartz stringers								
467.0-468.0	quartz stringers								
467.0-468.0	fault								
471.2-570.1	Arenite and Pelite medium layering								
505.1-505.6	fault								
524.6-525.9	quartz vein								
		524.6-525.9	3.0						
		525.9-533.9	0.5						
532.3-541.5	fault								
533.9-536.5	quartz vein								
		533.9-536.5	5.0						
		536.5-575.6	0.5						
569.0-575.4	chloritized								
570.1-573.5	Grit thick layering								
571.7-573.5	quartz vein								
573.5-575.4	Arenite and Pelite medium layering								
575.4-590.0	Graphitic Pelite very thin layering								
		575.6-590.0	1.0						
590.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-04

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: March 4, 2001
 Date Completed: March 7, 2001
 Final Depth: **410 feet (125.0 m)**

Collar Grid Coordinates

Mine Grid

Northing	Easting	Elevation
2801.0 ft.	20206.0 ft.	4849.0 ft.

Logged by: R.D. Hall

Depth	Azimuth	Dip
collar	223°	-80°
180.0 ft.	236°	-79°
400.0 ft.	232°	-79°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-10.0	Overburden								
10.0-141.0	Magnetite-bearing Pelite								
	very thin layering								
10.0-30.0	chloritized								
					10.0-242.3		0.5		
30.0-39.0	strongly sericitized								
38.0-40.0	fault								
39.0-81.0	chloritized								
48.5-50.0	fault								
81.0-102.0	strongly dolomitized								
86.8-93.3	quartz stringers								
102.0-141.0	chloritized								
141.0-153.2	Pelite								
	very thin layering								
141.0-153.2	strongly dolomitized								
153.2-155.7	Arenite and Lesser Graphitic Pelite								
	very thin layering								
155.7-221.0	Magnetite-bearing Pelite								
	very thin layering								
155.7-182.5	strongly sericitized and moderately dolomitized								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
304.5-354.0	strongly sericitized and moderately dolomitized								
			1962	core	304.5	310.0	0.06	0.002	5.5
			1963	core	310.0	315.0	0.31	0.009	5.0
			1964	core	315.0	320.0	0.05	0.001	5.0
			1965	core	320.0	325.0	0.29	0.008	5.0
			1966	core	325.0	329.5	0.02	<0.001	4.5
329.5-352.5		10.0							
			1967	core	329.5	335.0	0.08	0.002	5.5
			1968	core	335.0	340.0	0.02	<0.001	5.0
			1969	core	340.0	345.0	0.01	<0.001	5.0
			1970	core	345.0	350.0	0.01	<0.001	5.0
			1971	core	350.0	354.0	0.03	0.001	4.0
352.5-354.0		1.0							
354.0-377.0	Arenite and Lesser Graphitic Pelite very thin layering								
354.0-358.0		3.0							
			1972	core	354.0	358.0	0.01	<0.001	4.0
358.0-377.0		1.0							
			1973	core	358.0	369.5	0.04	0.001	11.5
377.0-387.5	Arenite medium layering								
377.0-386.0	strongly sericitized and moderately dolomitized								
381.1-382.7	quartz stringers								
386.0-410.0	quartz stringers								
377.0-381.1		3.0							
381.1-382.7		1.0							
382.7-386.0		3.0							
386.0-410.0		1.0							
387.5-410.0	Arenite and Lesser Graphitic Pelite thin to very thin layering								
410.0	E.O.H.								

Diamond Drill Log

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: April 28, 2001
 Date Completed: May 8, 2001
Final Depth: 590 feet (179.8 m)

	Northing	Easting	Elevation
Mine Grid	2396.0 ft.	20500.0 ft.	4756.0 ft.

Logged by: J. Pautler

Depth	Azimuth	Dip
collar	43°	-38°
110.0 ft.	41°	-38°
480.0 ft.	37°	-36°
590.0 ft.	41°	-36°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-50.0	Overburden								
50.0-177.7	Arenite thin layering								
		50.0-100.7	1.0						
51.0-81.8	fault		344093	core	99.2	100.7	0.01	<0.001	1.5
100.7-107.8	quartz vein	100.7-102.6	5.0						
			344094	core	100.7	101.8	0.01	<0.001	1.1
			344095	core	101.8	103.8	13.04	0.380	2.0
		102.6-103.0	60.0						
103.0-109.0	fault								
		103.0-108.6	7.0						
			344096	core	103.8	107.1	0.37	0.011	3.3
			344097	core	107.1	108.0	0.15	0.004	0.9
			344098	core	108.0	136.5	0.02	0.001	28.5
		108.6-138.5	2.0						
130.0-142.0	fault		344099	core	136.5	138.5	0.02	0.001	2.0
		138.5-159.0	8.0						
			344100	core	138.5	143.0	0.02	0.001	4.5
			6001	core	143.0	149.2	0.01	<0.001	6.2
			6002	core	149.2	154.0	0.02	0.001	4.8

(

Length
ft.

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
234.4-324.0	Arenite								
234.4-248.2	medium layering								
	strongly dolomitized and moderately sericitized								
234.4-236.1		10.0							
236.1-238.8	quartz stringers								
236.1-249.7		2.0							
			6019	core	236.1	238.8	0.01	<0.001	2.7
			6020	core	238.8	243.6	0.01	<0.001	4.8
			6021	core	243.6	247.3	0.01	<0.001	3.7
247.4-247.7	quartz vein								
248.2-254.0	chloritized								
249.7-256.0		8.0							
			6022	core	249.7	252.2	0.01	<0.001	2.5
			6023	core	252.2	255.7	0.01	<0.001	3.5
254.0-275.5	strongly sericitized and moderately dolomitized								
254.0-261.3	fault								
			6024	core	255.7	260.0	0.01	<0.001	4.3
256.0-261.3		3.0							
			6025	core	260.0	265.7	0.01	<0.001	5.7
261.3-265.7		6.0							
265.7-270.6		4.0							
270.6-294.9		2.0							
275.0-277.0	fault								
275.5-276.3	chloritized								
276.3-287.8	strongly sericitized and moderately dolomitized								
287.8-290.6	chloritized								
290.6-294.9	strongly sericitized and moderately dolomitized								
294.9-298.6	chloritized								
294.9-298.6		3.0							
298.6-324.0	strongly sericitized and moderately dolomitized								
298.6-305.4		2.0							
305.4-317.1		4.0							
			6026	core	305.4	309.8	0.01	<0.001	4.4
			6027	core	309.8	313.8	0.01	<0.001	4.0
			6028	core	313.8	317.1	0.01	<0.001	3.3
317.1-318.4	quartz stringers								
317.1-318.4		1.0							
			6029	core	317.1	318.4	0.01	<0.001	1.3

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
318.4-324.0		1.0							
320.0-324.0	fault		6030	core	318.4	324.0	0.01	<0.001	5.6
324.0-391.5	Calcareous Arenite and Lesser Grit medium layering								
324.0-363.0	strongly dolomitized								
324.0-328.7		2.0							
			6031	core	324.0	328.7	0.01	<0.001	4.7
328.7-333.9		1.0							
			6032	core	328.7	330.7	0.02	0.001	2.0
333.9-336.9		10.0							
			6033	core	333.9	336.9	0.03	0.001	3.0
336.9-408.2		1.0							
			6034	core	340.0	343.0	0.12	0.004	3.0
			6035	core	343.0	347.4	0.01	<0.001	4.4
			6036	core	347.4	350.0	0.01	<0.001	2.6
347.6-391.5	fault								
			6037	core	360.0	364.8	0.01	<0.001	4.8
363.0-391.5	strongly dolomitized and moderately sericitized								
			6038	core	364.8	366.8	0.01	<0.001	2.0
			6039	core	366.8	370.0	0.01	<0.001	3.2
391.5-408.2	Graphitic Pelite very thin layering								
391.5-409.2	fault								
408.2-419.2	Calcareous Arenite medium layering								
408.2-438.7		1.0							
409.2-419.2	strongly dolomitized and moderately sericitized								
409.2-419.2	fault								
			6040	core	413.0	418.6	0.01	<0.001	5.6
			6041	core	418.6	424.4	0.01	<0.001	5.8
419.2-438.7	Graphitic Pelite very thin layering								
419.2-438.7	fault								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
			6042	core	424.4	430.0	0.02	0.001	5.6
			6043	core	430.0	438.8	0.01	<0.001	8.8
438.7-471.8	Calcareous Arenite medium layering								
438.7-460.6	strongly dolomitized and moderately sericitized								
		438.7-471.6	6.0						
			6044	core	438.8	444.1	0.28	0.008	5.3
			6045	core	444.1	450.0	0.09	0.003	5.9
			6046	core	450.0	454.2	0.05	0.001	4.2
			6047	core	454.2	460.0	0.09	0.003	5.8
			6048	core	460.0	463.5	0.96	0.028	3.5
460.6-471.6	strongly sericitized								
460.6-471.6	fault								
			6049	core	463.5	467.7	0.04	0.001	4.2
			6050	core	467.7	471.8	0.06	0.002	4.1
471.8-489.6	BC Vein Structure								
471.6-475.8	quartz vein								
471.6-475.8	fault								
		471.6-489.6	4.0						
			6051	core	471.8	475.8	1.01	0.029	4.0
475.8-485.8	quartz vein								
			6053	core	475.8	478.1	0.07	0.002	2.3
			6054	core	478.1	482.0	0.44	0.013	3.9
			6055	core	482.0	485.8	0.55	0.016	3.8
485.8-489.5	quartz vein								
485.8-489.5	fault								
			6056	core	485.8	489.6	0.38	0.011	3.8
489.6-529.0	Dolomite Porphyroblastic Pelite								
				core	478.1	489.6	0.46	0.013	11.5
		489.6-590.0	0.1						
				core	471.8	489.6	0.53	0.015	17.8
			6057	core	489.6	493.1	0.01	<0.001	3.5
497.3-529.0	very thin layering strongly sericitized and moderately chloritized								

D.D.H. BC01-05

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From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
529.0-590.0	Magnetite-bearing Pelite								
	very thin layering								
529.0-590.0	chloritized								
590.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-06

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: May 13, 2001
 Date Completed: May 27, 2001
Final Depth: 590 feet (179.8 m)

Collar Grid Coordinates
Northing Easting Elevation
 Mine Grid **2778.0 ft. 21000.0 ft. 4786.0 ft.**

Logged by: D. Hladky

Depth	Azimuth	Dip
collar	225°	-49°
0.0 ft.	225°	-49°
200.0 ft.	203°	-47°
580.0 ft.	216°	-49°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-46.0	Overburden								
46.0-165.0	Arenite								
	very thin layering								
46.0-115.3	strongly sericitized and dolomitized								
		2.0							
		5.0							
			6058	core	52.0	60.0	0.01	<0.001	8.0
		0.1							
115.3-120.3	chloritized								
		3.0							
			6059	core	115.3	120.0	0.01	<0.001	4.7
120.3-149.0	strongly sericitized and dolomitized								
123.5-125.0	fault		6060	core	130.0	139.3	0.01	<0.001	9.3
		5.0							
		0.1							
		10.0							
			6061	core	139.3	145.0	0.01	<0.001	5.7
145.0-171.0	quartz stringers		6062	core	145.0	150.0	0.02	<0.001	5.0
149.0-188.0	strongly sericitized								
		2.0							
			6063	core	150.0	156.1	0.01	<0.001	6.1

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
156.1-165.7	quartz vein								
156.1-156.4	fault								
		156.1-165.0	3.0						
			6064	core	156.1	165.0	0.02	0.001	8.9
165.0-478.0	Arenite and Lesser Pelite thin layering								
		165.0-195.0	10.0						
			6065	core	165.0	171.0	0.49	0.014	6.0
166.4-166.6	fault								
			6066	core	171.0	180.0	0.48	0.014	9.0
			6067	core	180.0	190.0	0.31	0.009	10.0
187.8-200.3	quartz stringers								
			6068	core	190.0	195.0	0.43	0.013	5.0
				core	165.0	195.0	0.42	0.012	30.0
		195.0-241.1	3.0						
			6069	core	195.0	200.0	0.04	0.001	5.0
			6070	core	200.0	210.0	0.07	0.002	10.0
			6071	core	210.0	220.0	0.07	0.002	10.0
215.5-219.3	quartz vein								
			6072	core	220.0	230.0	0.05	0.001	10.0
224.4-229.0	quartz stringers								
			6073	core	230.0	241.1	0.01	<0.001	11.1
241.1-245.6	strongly sericitized								
		241.1-245.6	2.0						
			6074	core	241.1	245.6	0.01	<0.001	4.5
		245.6-286.1	1.0						
263.4-263.8	quartz vein								
286.1-290.5	strongly sericitized								
		286.1-290.5	10.0						
			6075	core	286.1	290.5	0.01	<0.001	4.4
		290.5-297.7	0.1						
297.7-306.6	strongly sericitized								
		297.7-306.6	4.0						
			6076	core	297.7	306.6	0.01	<0.001	8.9
302.0-302.1	fault								
306.6-313.7	strongly sericitized								
		306.6-478.0	1.0						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
314.6-315.3	quartz vein								
345.2-346.2	quartz stringers								
362.0-393.5	quartz stringers								
413.0-418.5	quartz stringers								
416.4-418.3	fault								
457.0-469.0	quartz stringers								
461.5-462.2	fault								
478.0-528.9	Grit and Lesser Arenite								
	medium layering								
478.0-492.6	strongly dolomitized								
		478.0-590.0	0.1						
492.6-510.0	strongly sericitized and moderately dolomitized								
			6079	core	492.6	500.0	0.01	<0.001	7.4
			6080	core	500.0	510.2	0.01	<0.001	10.2
528.9-590.0	Grit								
	thick layering								
542.0-555.0	quartz stringers								
571.0-576.5	quartz stringers								
582.0-585.5	quartz stringers								
587.5-588.5	fault								
590.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-07

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: May 28, 2001
 Date Completed: June 4, 2001
 Final Depth: **920 feet (280.4 m)**

Collar Grid Coordinates
 Northing Easting Elevation
 Mine Grid 2778.0 ft. 21000.0 ft. 4786.0 ft.

Logged by: D. Hladky

Depth	Azimuth	Dip
collar	224°	-70°
0.0 ft.	224°	-70°
600.0 ft.	224°	-69°
910.0 ft.	224°	-67°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-20.0	Overburden								
20.0-421.2	Arenite and Lesser Pelite								
	very thin layering								
20.0-99.0	strongly sericitized and moderately dolomitized								
		20.0-32.5	3.0						
			6081	core	20.0	30.0	0.02	0.001	10.0
			6082	core	30.0	34.8	0.01	<0.001	4.8
		32.5-34.8	12.0						
		34.8-67.5	2.0						
			6083	core	34.8	40.0	0.01	<0.001	5.2
			6084	core	40.0	50.0	0.01	<0.001	10.0
43.7-45.5	quartz stringers								
			6085	core	50.0	60.0	0.01	<0.001	10.0
52.0-53.2	quartz stringers								
			6086	core	60.0	67.5	0.01	<0.001	7.5
		67.5-123.1	0.1						
88.9-89.5	quartz stringers								
99.0-125.5	chloritized, moderately sericitized and dolomitized								
103.4-108.7	quartz stringers								
120.8-122.5	fault								
		123.1-128.4	1.0						
			6087	core	123.1	128.4	0.01	<0.001	5.3
125.5-142.5	strongly sericitized and moderately dolomitized								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
126.1-131.8	quartz stringers								
					128.4-131.8				
		0.1							
			6088	core	128.4	136.6	0.01	<0.001	8.2
					131.8-136.6				
		2.0							
					136.6-137.0				
		4.0							
			6089	core	136.6	140.0	0.01	<0.001	3.4
					137.0-144.8				
		2.0							
			6090	core	140.0	144.8	0.01	<0.001	4.8
142.5-144.2	chloritized and moderately dolomitized								
144.2-150.3	strongly sericitized and moderately dolomitized								
					144.8-145.0				
		5.0							
			6092	core	144.8	150.3	0.01	<0.001	5.5
					145.0-149.5				
		2.0							
					149.5-150.3				
		4.0							
150.3-153.4	strongly sericitized and moderately chloritized								
					150.3-170.3				
		3.0							
			6093	core	150.3	160.0	0.01	<0.001	9.7
153.4-153.9	chloritized and moderately dolomitized								
153.9-179.3	strongly sericitized, moderately dolomitized and slightly chloritized								
			6094	core	160.0	170.3	0.01	<0.001	10.3
					170.3-170.9				
		3.0							
			6095	core	170.3	174.4	0.01	<0.001	4.1
					170.9-171.3				
		7.0							
					171.3-173.1				
		3.0							
					173.1-174.4				
		10.0							
					174.4-179.3				
		4.0							
			6096	core	174.4	179.3	0.01	<0.001	4.9
179.3-197.8	silicified								
					179.3-347.0				
		2.0							
			6097	core	179.3	190.0	0.01	<0.001	10.7
190.0-191.2	quartz vein								
			6098	core	190.0	197.8	0.01	<0.001	7.8
199.5-201.7	quartz vein								
219.4-220.0	quartz vein								
225.3-226.5	quartz vein								
227.5-228.2	fault								
229.1-230.4	quartz vein								
236.7-244.9	silicified								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
241.8-243.4	quartz vein								
245.9-246.1	fault								
249.2-273.1	silicified								
257.6-258.9	quartz vein								
258.3-258.5	fault								
260.1-261.0	quartz vein								
261.6-261.9	quartz vein								
262.2-263.0	quartz vein								
263.4-264.5	quartz vein								
265.4-266.7	quartz vein								
266.5-256.2	quartz vein								
270.0-270.5	quartz vein								
270.5-271.0	fault								
273.1-273.3	fault								
275.0-275.5	quartz vein								
275.3-276.3	fault								
277.1-277.6	quartz vein								
278.5-278.9	quartz vein								
280.4-280.9	quartz vein								
282.9-283.3	quartz vein								
286.4-320.0	silicified								
287.3-288.0	quartz vein								
288.6-290.2	quartz vein								
291.9-292.9	quartz vein								
294.9-295.4	quartz vein								
301.8-303.0	quartz vein								
305.3-320.0	quartz vein								
321.1-321.9	quartz vein								
326.1-326.7	quartz vein								
			6099	core	326.1	332.8	0.01	<0.001	6.7
328.0-328.6	quartz vein								
330.0-331.5	quartz vein								
336.6-347.0	silicified and moderately dolomitized								
342.0-344.0	quartz vein								
344.5-345.1	fault								
346.0-346.2	fault								
347.0-356.3	silicified and moderately sericitized								
		3.0							
		347.0-350.1							

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
			6100	core	347.0	350.1	0.08	0.002	3.1
		25.0							
			6101	core	350.1	356.3	0.06	0.002	6.2
		3.0							
			6102	core	356.3	363.1	0.04	0.001	6.8
363.1-368.4	strongly sericitized and moderately silicified								
			6103	core	363.1	368.4	0.15	0.004	5.3
		10.0							
		1.0							
368.4-372.1	strongly dolomitized								
369.7-369.8	fault								
372.1-374.2	strongly sericitized and moderately chloritized								
372.2-372.5	fault								
		5.0							
			6105	core	373.2	376.6	0.15	0.004	3.4
		2.0							
374.2-375.3		20.0							
375.3-375.5		2.0							
375.5-376.1		20.0							
376.1-376.6		2.0							
376.6-421.1		2.0							
			6106	core	376.6	381.3	0.09	0.003	4.7
379.3-380.0	fault								
381.3-421.2	silicified and moderately dolomitized								
			6107	core	381.3	390.0	0.09	0.003	8.7
384.6-385.1	fault								
421.2-661.9	Arenite, Lesser Pelite and Minor Grit thin layering								
		1.0							
441.0-478.5	quartz stringers								
		25.0							
			6108	core	480.2	485.5	0.02	0.001	5.3
		7.0							
			6109	core	485.5	490.4	0.01	<0.001	4.9
490.4-511.3	strongly sericitized and moderately dolomitized								
		6.0							
			6110	core	490.4	494.3	0.01	<0.001	3.9

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
493.3-494.3	quartz stringers		6112	core	494.3	498.4	0.01	<0.001	4.1
497.8-498.4	fault		6113	core	498.4	505.6	0.01	<0.001	7.2
505.6-511.3	strongly dolomitized	3.0							
511.3-589.7		2.0							
522.9-523.1	fault								
528.8-529.4	fault								
557.7-558.6	fault								
557.7-558.6	quartz stringers								
560.7-589.7	silicified and moderately dolomitized								
571.6-571.8	fault								
589.7-590.0	fault								
589.7-748.5		1.0							
594.5-594.7	quartz vein								
602.5-603.6	fault								
611.9-612.2	fault								
616.8-618.3	fault								
631.9-644.3	silicified and moderately dolomitized								
643.1-643.4	fault								
661.9-678.3	Pelite and Lesser Arenite								
	very thin layering								
672.2-672.4	fault								
678.3-804.7	Arenite, Lesser Grit and Minor Pelite								
	thin layering								
678.3-699.0	strongly dolomitized								
720.2-722.5	quartz stringers								
747.0-748.5	quartz stringers								
748.0-748.5	fault		6114	core	748.0	750.2	0.76	0.022	2.2
748.5-750.2	quartz vein	8.0							
750.2-750.8	fault								
750.2-763.1	quartz stringers	1.0							

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
755.5-756.8	fault		6115	core	763.0	764.0	1.11	0.032	1.0
763.1-763.4	quartz vein								
763.4-768.0	quartz stringers								
768.0-769.7	quartz vein								
		769.1-769.3	8.0						
		769.3-920.0	1.0						
769.7-770.0	quartz stringers								
770.0-770.5	quartz vein								
770.5-783.0	quartz stringers								
780.2-780.7	fault								
797.0-800.1	quartz stringers								
801.7-802.0	fault								
804.7-920.0	Grit, Lesser Arenite and Minor Pelite thin layering								
818.0-830.4	strongly dolomitized								
830.4-840.4	silicified and moderately chloritized								
839.0-839.5	fault								
841.0-847.4	strongly dolomitized								
847.4-852.0	silicified and moderately chloritized								
852.0-865.2	strongly dolomitized and moderately chloritized								
865.2-903.3	chloritized								
869.9-908.5	quartz stringers								
895.8-895.9	fault								
908.1-908.2	fault								
911.6-912.0	quartz stringers								
912.0-920.0	chloritized								
917.6-920.0	quartz stringers								
920.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-08

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: June 5, 2001
 Date Completed: June 11, 2001
 Final Depth: **640 feet (195.1 m)**

Collar Grid Coordinates
 Northing Easting Elevation
 Mine Grid 2791.0 ft. 20999.0 ft. 4786.0 ft.

Logged by: D. Hladky

Depth	Azimuth	Dip
collar	43°	-50°
0.0 ft.	43°	-49°
250.0 ft.	45°	-47°
630.0 ft.	49°	-45°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-14.0	Overburden very thin layering								
14.0-50.0	Fault Zone - Pelite and Vein Quartz very thin layering								
14.0-35.0	quartz vein								
35.0-50.0	strongly sericitized								
35.0-92.4	fault								
		35.0-50.0	4.0						
			6116	core	35.0	40.0	11.21	0.327	5.0
			6117	core	40.0	42.5	18.35	0.535	2.5
			6118	core	42.5	46.5	8.98	0.262	4.0
45.5-45.9	quartz vein								
			6119	core	46.5	50.0	27.09	0.790	3.5
50.0-92.4	Graphitic Pelite thin layering								
				core	35.0	50.0	15.51	0.452	15.0
		50.0-92.4	2.0						
			6120	core	50.0	60.0	0.42	0.012	10.0
			6121	core	60.0	70.0	0.15	0.004	10.0
61.4-256.2	quartz stringers								
			6122	core	70.0	80.0	0.19	0.006	10.0
			6123	core	80.0	86.5	0.20	0.006	6.5

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
			6124	core	86.5	92.4	0.21	0.006	5.9
92.4-109.4	Arenite and Lesser Graphitic Pelite thin layering								
		92.4-122.6	0.1						
109.4-149.3	Arenite and Pelite thin layering								
109.4-136.5	strongly dolomitized and moderately silicified								
		122.6-143.5	1.0						
125.0-125.2	fault								
136.5-259.2	strongly sericitized and moderately chloritized								
		143.5-150.0	2.0						
149.3-233.0	Pelite and Lesser Arenite thin layering								
		150.0-172.6	0.1						
		172.6-224.4	2.0						
			6126	core	190.0	200.0	0.01	<0.001	10.0
			6127	core	206.0	207.5	0.01	<0.001	1.5
			6128	core	211.1	216.7	0.01	<0.001	5.6
		224.4-233.0	0.1						
233.0-248.8	Magnetite-bearing Pelite and Arenite thin layering								
		233.0-248.6	3.0						
248.8-327.0	Pelite and Lesser Arenite thin layering								
		248.6-259.8	2.0						
			6129	core	255.0	260.0	0.07	0.002	5.0
256.2-256.6	quartz vein								
256.6-279.0	quartz stringers								
259.2-270.3	chloritized and moderately dolomitized								
		259.8-286.2	1.0						
270.3-295.3	strongly sericitized and moderately chloritized								
279.0-399.4	quartz stringers								
		286.2-327.0	0.1						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
286.7-287.0	fault								
295.3-315.4	chloritized								
315.4-344.6	strongly sericitized and moderately dolomitized								
327.0-365.0	Magnetite-bearing Pelite								
	thin layering								
		327.0-376.6	4.0						
342.5-342.6	fault								
344.6-360.0	chloritized								
360.0-364.6	strongly sericitized and moderately chloritized								
			6130	core	361.4	363.9	0.13	0.004	2.5
364.6-512.2	chloritized								
365.0-386.9	Pelite								
	thin layering								
		376.6-386.9	1.0						
386.9-410.4	Magnetite-bearing Pelite								
	thin layering								
		386.9-410.4	3.0						
399.4-400.0	quartz vein								
400.0-403.1	quartz stringers								
403.1-403.6	quartz vein								
403.6-410.9	quartz stringers								
410.4-569.7	Pelite								
	thin layering								
		410.4-513.3	0.1						
410.9-411.3	quartz vein								
411.3-445.8	quartz stringers								
445.8-446.3	quartz vein								
446.3-513.3	quartz stringers								
512.2-513.5	strongly sericitized								
			6132	core	512.2	513.5	0.36	0.011	1.3
513.3-513.4	quartz vein								
		513.3-513.4	40.0						
513.4-523.3	quartz stringers								
		513.4-569.7	0.1						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
513.5-589.4	chloritized								
523.3-523.9	quartz vein								
523.9-577.9	quartz stringers								
529.4-530.0	fault								
569.7-631.0	Magnetite-bearing Pelite thin layering								
		569.7-631.0	1.0						
577.9-578.5	quartz vein								
578.5-601.0	quartz stringers								
589.4-589.7	strongly sericitized								
589.7-640.0	chloritized								
			6133	core	592.7	594.2	0.16	0.005	1.5
601.0-603.5	quartz vein								
603.5-619.7	quartz stringers								
605.2-605.6	fault								
617.0-622.0	Fault Zone								
619.7-620.3	quartz vein								
620.3-624.6	quartz stringers								
624.6-625.0	quartz vein								
625.0-636.7	quartz stringers								
625.0-625.6	fault								
626.0-627.9	fault								
631.0-640.0	Pelite thin layering								
		631.0-640.0	0.1						
631.6-632.0	fault								
636.7-639.3	quartz vein								
639.3-640.0	quartz stringers								
640.0	E.O.H.								

International Wayside Gold Mines Ltd.
Diamond Drill Log

D.D.H. BC01-09

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: June 11, 2001
 Date Completed: June 21, 2001
 Final Depth: **805 feet (245.4 m)**

Collar Grid Coordinates
Northing Easting Elevation
 Mine Grid 2395.0 ft. 20070.0 ft. 4784.0 ft.

Logged by: D. Hladky

Depth	Azimuth	Dip
collar	43°	-60°
0.0 ft.	43°	-60°
250.0 ft.	43°	-57°
545.0 ft.	43°	-57°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-30.0	Overburden								
30.0-90.7	Arenite, Lesser Pelite and Grit								
	thin layering								
30.0-56.2	strongly sericitized and moderately silicified								
30.0-186.9		2.0							
30.4-30.7	quartz vein								
31.5-33.2	quartz vein								
50.0-52.0	Fault Zone								
56.2-109.6	silicified								
58.3-59.6	Fault Zone								
90.7-112.3	Grit, Lesser Arenite and Pelite								
	thin layering								
98.3-98.4	fault								
105.3-107.0	fault								
109.6-116.0	silicified and moderately sericitized								
109.6-111.0	Fault Zone								
112.3-114.4	Conglomerate								
	thick layering								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
114.4-185.4	Grit, Lesser Arenite and Pelite thin layering								
116.0-119.0	strongly sericitized and moderately silicified								
119.0-138.5	silicified								
138.3-138.5	fault								
138.5-157.3	silicified and moderately sericitized								
157.3-157.5	fault								
164.2-164.7	fault								
185.4-236.6	Graphitic Pelite, Lesser Arenite and Grit thin layering								
186.9-215.1	quartz stringers								
		186.9-203.7	3.0						
			6138	core	193.7	203.7	0.04	0.001	10.0
		203.7-206.8	25.0						
			6139	core	203.7	206.8	5.13	0.150	3.1
		206.8-213.1	4.0						
			6140	core	206.8	212.0	1.12	0.033	5.2
207.7-208.7	fault								
			6141	core	212.0	215.1	2.81	0.082	3.1
		213.1-213.6	20.0						
		213.6-226.2	4.0						
215.1-236.6	strongly sericitized and moderately silicified								
			6142	core	215.1	220.0	2.09	0.061	4.9
			6143	core	220.0	225.0	7.50	0.219	5.0
			6144	core	225.0	230.0	9.23	0.269	5.0
		226.2-226.8	15.0						
		226.8-245.9	4.0						
236.0-252.3	quartz stringers								
236.6-668.7	Pelite thin layering								
236.6-289.8	strongly sericitized and moderately chloritized								
			6145	core	230.0	236.6	1.68	0.049	6.6
				core	203.7	236.6	4.12	0.120	32.9
			6146	core	236.6	244.2	0.63	0.018	7.6
			6147	core	244.2	249.0	10.78	0.314	4.8
		245.9-246.5	12.0						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
252.3-253.9	fault	4.0							
			6148	core	249.0	253.9	0.10	0.003	4.9
		25.0							
			6149	core	253.9	257.7	3.03	0.088	3.8
		4.0							
			6150	core	257.7	263.4	0.67	0.020	5.7
		10.0							
			6151	core	263.4	269.0	1.30	0.038	5.6
		4.0							
289.8-530.4	strongly sericitized and moderately dolomitized	10.0							
		4.0							
				core	203.7	269.0	3.29	0.096	65.3
		4.0							
			6152	core	269.0	275.4	0.23	0.007	6.4
		8.0							
		4.0							
			6153	core	275.4	281.0	0.03	0.001	5.6
		9.0							
295.7-296.5	quartz vein	3.0							
			6154	core	281.0	289.8	0.01	<0.001	8.8
			6155	core	289.8	295.5	0.05	0.001	5.7
		11.0							
		4.0							
			6156	core	295.5	300.0	0.02	0.001	4.5
		18.0							
			6157	core	300.0	304.0	0.01	<0.001	4.0
321.0-321.6	Fault Zone		6158	core	304.0	308.3	0.01	<0.001	4.3
		3.0							
			6159	core	308.3	319.0	0.01	<0.001	10.7
			6160	core	319.0	330.0	0.01	<0.001	11.0
			6162	core	330.0	340.0	0.01	<0.001	10.0
			6163	core	340.0	350.0	0.01	<0.001	10.0
			6165	core	350.0	360.0	0.01	<0.001	10.0

From-To (ft)	Description		% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
358.2-358.4	quartz vein									
		360.0-363.2	20.0							
				6166	core	360.0	363.2	0.01	<0.001	3.2
		363.2-365.8	8.0							
				6167	core	363.2	366.6	0.01	<0.001	3.4
		365.8-366.6	2.0							
		366.6-369.2	16.0							
				6168	core	366.6	369.2	0.01	<0.001	2.6
		369.2-377.8	5.0							
				6169	core	369.2	373.9	0.01	<0.001	4.7
				6170	core	373.9	380.7	0.01	<0.001	6.8
		377.8-378.4	12.0							
		378.4-384.0	6.0							
				6171	core	380.7	387.4	0.01	<0.001	6.7
		384.0-394.0	2.0							
				6172	core	387.4	394.0	0.01	<0.001	6.6
		394.0-394.3	8.0							
				6173	core	394.0	396.7	0.01	<0.001	2.7
		394.3-396.3	2.0							
		396.3-396.7	8.0							
		396.7-421.7	2.0							
				6175	core	396.7	406.0	0.01	<0.001	9.3
403.4-404.5	fault									
				6176	core	406.0	410.0	0.01	<0.001	4.0
408.2-410.0	quartz stringers									
				6177	core	410.0	415.0	0.01	<0.001	5.0
				6178	core	415.0	420.0	0.01	<0.001	5.0
				6179	core	420.0	426.0	0.01	<0.001	6.0
		421.7-422.3	10.0							
		422.3-429.4	3.0							
425.2-425.6	quartz vein									
				6180	core	426.0	430.0	0.01	<0.001	4.0
		429.4-437.7	8.0							
				6181	core	430.0	434.0	0.01	<0.001	4.0
				6182	core	434.0	437.7	0.01	<0.001	3.7
		437.7-480.3	3.0							
				6183	core	437.7	443.0	0.01	<0.001	5.3

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
445.0-453.9	quartz stringers		6184	core	443.0	450.0	0.01	<0.001	7.0
			6186	core	450.0	460.0	0.01	<0.001	10.0
			6187	core	460.0	470.0	0.01	<0.001	10.0
			6188	core	470.0	480.0	0.01	<0.001	10.0
478.1-485.0	quartz stringers		6189	core	480.0	485.0	0.01	<0.001	5.0
		480.3-481.4	6.0						
		481.4-491.0	2.0						
			6190	core	485.0	491.6	0.01	<0.001	6.6
488.2-539.4	quartz stringers								
		491.0-491.6	7.0						
		491.6-530.4	2.0						
			6191	core	491.6	500.0	0.01	<0.001	8.4
530.4-539.4	chloritized and moderately dolomitized		6192	core	500.0	510.0	0.01	<0.001	10.0
			6193	core	510.0	520.0	0.01	<0.001	10.0
			6194	core	530.0	535.0	0.01	<0.001	5.0
		530.4-530.8	18.0						
539.4-594.3	strongly sericitized and moderately dolomitized	530.8-537.6	1.0						
		537.6-539.0	4.0						
			6195	core	537.6	541.8	0.01	<0.001	4.2
		539.0-541.8	1.0						
543.5-545.0	strongly sericitized and moderately dolomitized	541.8-543.5	5.0						
			6196	core	541.8	547.1	0.01	<0.001	5.3
		543.5-545.0	1.0						
		545.0-547.1	7.0						
547.1-555.5	quartz stringers	547.1-555.5	1.0						
		555.5-740.1	0.1						
582.2-582.6	quartz vein								
583.5-584.7	quartz vein								
585.7-587.6	quartz stringers								
587.6-588.2	quartz vein								
594.3-638.3	strongly dolomitized and moderately sericitized		6198	core	590.0	595.7	0.01	<0.001	5.7
			6199	core	595.7	600.0	0.01	<0.001	4.3

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
596.5-610.0	quartz stringers		6200	core	615.0	620.0	0.01	<0.001	5.0
615.5-616.3	quartz vein								
625.1-667.3	quartz stringers								
638.3-641.1	chloritized and moderately dolomitized								
641.1-668.7	strongly dolomitized and moderately sericitized								
668.7-805.0	Arenite and Lesser Graphitic Pelite								
	thin layering								
668.7-670.1	fault								
673.7-674.0	calcite vein								
681.7-682.0	calcite vein								
684.7-684.8	quartz vein								
719.8-726.5	silicified and moderately sericitized								
730.1-805.0	quartz stringers								
			740.1-755.4	3.0					
754.4-762.4	silicified								
			755.4-805.0	0.1					
805.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-10

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: June 29, 2001
 Date Completed: July 25, 2001
 Final Depth: **1010 feet (307.8 m)**

Collar Grid Coordinates
 Northing Easting Elevation
 Mine Grid **2316.0 ft. 19701.0 ft. 4789.0 ft.**

Logged by: D. Hladky

Depth	Azimuth	Dip
collar	43°	-60°
150.0 ft.	39°	-60°
500.0 ft.	43°	-59°
1010.0 ft.	44°	-58°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-36.0	Overburden								
36.0-62.5	Arenite, Lesser Grit and Graphitic Pelite thin to very thin layering								
36.0-58.5	silicified, moderately dolomitized and weakly sericitized								
		1.0							
41.5-42.0	fault								
47.9-48.8	quartz vein								
48.8-51.4	quartz stringers								
51.4-54.3	quartz vein								
55.4-56.4	quartz vein								
56.4-58.7	quartz stringers								
58.5-72.1	silicified, moderately sericitized and weakly dolomitized								
		0.4							
58.7-59.7	quartz vein								
62.2-62.5	Fault Zone								
62.5-78.4	Grit, Lesser Arenite and Graphitic Pelite thin to very thin layering								
63.3-65.5	quartz stringers								
72.1-78.4	silicified, moderately dolomitized and weakly sericitized								
72.1-74.6	quartz stringers								
74.6-77.3	quartz vein								
77.3-78.8	quartz stringers								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
78.4-85.0	Arenite, Lesser Graphitic Pelite and Grit very thin to thin layering								
		78.4-92.5	1.2						
78.8-78.9	fault								
80.0-82.2	quartz stringers								
82.2-82.3	strongly sericitized, moderately bleached and weakly dolomitized								
85.0-92.5	Grit, Lesser Arenite and Graphitic Pelite thin layering								
85.0-92.5	silicified, moderately sericitized and weakly dolomitized								
90.4-92.1	quartz stringers								
92.5-95.8	Arenite, Lesser Graphitic Pelite and Grit very thin to thin layering								
92.5-95.8	strongly dolomitized and moderately bleached								
		92.5-94.1	2.0						
94.1-95.8	quartz vein								
		94.1-95.8	26.0						
			6203	core	94.1	95.8	3.79	0.111	1.7
95.8-100.0	Arenite, Lesser Grit and Graphitic Pelite thin layering								
95.8-103.9	silicified, moderately sericitized and weakly dolomitized								
		95.8-100.7	0.7						
97.0-100.0	quartz stringers								
100.0-108.2	Grit, Lesser Arenite and Graphitic Pelite thin to medium layering								
		100.7-103.9	1.5						
103.4-103.9	quartz stringers								
103.9-106.9	silicified and moderately dolomitized								
		103.9-106.9	0.7						
106.9-110.0	silicified, moderately sericitized and weakly dolomitized								
		106.9-110.0	1.5						
108.2-127.5	Arenite, Lesser Grit and Graphitic Pelite thin layering								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
110.0-118.2	silicified and moderately dolomitized	1.0							
118.2-125.0	silicified, moderately sericitized and weakly dolomitized	1.5							
125.0-138.8	silicified and moderately dolomitized	1.0							
127.5-149.0	Grit, Lesser Arenite and Graphitic Pelite thin to medium layering								
127.5-128.4	quartz vein	2.5							
129.5-136.0	quartz stringers	1.0							
136.0-136.4	quartz vein	26.0							
			6204	core	136.0	137.0	0.94	0.027	1.0
138.8-139.9	silicified, moderately sericitized and weakly dolomitized	2.0							
139.9-145.4	silicified and moderately dolomitized	1.0							
145.4-146.5	silicified, moderately sericitized and weakly dolomitized								
146.5-149.0	silicified and moderately dolomitized								
147.0-147.7	quartz stringers								
147.7-149.0	quartz vein	2.5							
149.0-150.2	Graphitic Pelite, Lesser Arenite and Grit thin to very thin layering								
149.0-154.0	quartz stringers	0.4							
150.2-154.2	Arenite, Lesser Grit and Graphitic Pelite thin to very thin layering								
150.2-155.1	silicified, moderately dolomitized and weakly sericitized								
150.9-151.0	fault								
154.2-158.7	Grit, Lesser Arenite and Graphitic Pelite thin to very thin layering								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
155.1-155.7	silicified, moderately sericitized and weakly dolomitized								
155.7-165.2	silicified, moderately dolomitized and weakly sericitized								
158.0-158.5	quartz stringers								
158.7-173.9	Arenite, Lesser Grit and Graphitic Pelite								
	thin to very thin layering								
160.3-167.0	quartz stringers								
165.2-165.6	silicified, moderately sericitized and weakly dolomitized								
165.6-168.8	silicified, moderately dolomitized and weakly sericitized								
165.8-165.9	fault								
168.8-173.9	silicified, moderately sericitized and weakly dolomitized								
170.0-192.0	quartz stringers								
173.9-195.0	Grit, Lesser Arenite and Graphitic Pelite								
	thin to medium layering								
173.9-201.9	silicified and moderately dolomitized								
180.8-180.1	Fault Zone								
195.0-203.3	Arenite, Lesser Grit and Graphitic Pelite								
	thin to medium layering								
197.6-202.0	quartz stringers								
197.6-198.4	Fault Zone								
201.9-203.3	silicified, moderately sericitized and weakly dolomitized								
203.3-207.7	Arenite, Lesser Graphitic Pelite and Grit								
	thin to medium layering								
203.3-209.5	quartz stringers								
					203.3-218.6		2.0		
204.6-204.7	fault								
207.7-281.6	Grit, Lesser Arenite and Graphitic Pelite								
	thin to medium layering								
210.5-212.7	quartz stringers								
210.5-211.5	Fault Zone								
213.5-215.8	quartz stringers								
217.0-218.6	quartz stringers								
218.6-218.9	quartz stringers								
					218.6-246.2		0.6		

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
218.9-232.2	silicified and moderately dolomitized								
219.6-220.0	quartz vein								
220.1-220.8	quartz vein								
220.7-220.8	fault								
220.8-222.2	quartz stringers								
222.2-223.0	Fault Zone								
227.0-228.5	quartz stringers								
228.2-228.4	Fault Zone								
230.1-232.2	quartz stringers								
237.0-246.2	silicified and moderately dolomitized								
239.2-239.5	quartz vein								
246.2-258.3	silicified, moderately sericitized and weakly dolomitized								
					246.2-246.4	3.0			
					246.4-252.2	1.5			
248.0-249.0	quartz stringers								
250.8-258.6	quartz stringers								
					252.2-252.7	5.0			
					252.7-260.0	0.7			
260.0-263.6	quartz stringers								
					260.0-273.0	1.0			
263.1-265.3	Fault Zone								
264.9-265.1	quartz stringers								
265.5-265.9	Fault Zone								
266.0-266.3	fault								
272.4-278.3	quartz stringers								
272.9-281.6	strongly dolomitized and moderately bleached								
					273.0-283.8	0.7			
281.6-300.0	Arenite, Lesser Grit and Graphitic Pelite thin layering								
282.8-285.4	quartz stringers								
					283.8-289.3	2.5			
285.4-286.6	quartz vein								
289.3-289.4	fault								
					289.3-300.0	1.5			
290.5-293.0	silicified								
290.5-294.0	quartz stringers								
293.2-294.0	fault								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
343.6-358.0	strongly sericitized, moderately dolomitized and weakly chloritized								
350.4-352.3	quartz stringers								
353.2-353.7	quartz vein								
		2.5							
			6209	core	353.7	358.0	0.01	<0.001	4.3
		7.0							
		4.0							
358.0-360.9	strongly sericitized and moderately dolomitized								
359.1-359.5	quartz vein								
359.5-360.2	quartz stringers								
		12.0							
360.7-360.9	Pelite								
	thin layering								
360.9-417.3	Arenite, Lesser Graphitic Pelite and Grit								
		2.0							
	thin to medium layering								
360.9-387.0	strongly sericitized, moderately dolomitized and weakly chloritized								
		18.0							
			6210	core	363.2	364.6	0.01	<0.001	1.4
		1.5							
368.3-369.4	quartz stringers								
		13.0							
		3.5							
		8.0							
			6211	core	375.4	379.2	0.02	0.001	3.8
			6212	1/4 core	375.4	379.2	0.01	<0.001	3.8
378.4-389.2	quartz stringers								
		2.0							
		6.0							
387.0-608.4	strongly sericitized and moderately dolomitized								
		1.5							
390.0-290.2	quartz stringers								
		12.5							
			6213	core	390.6	392.9	0.01	<0.001	2.3
		4.0							
		9.0							

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
392.9-393.4		2.0							
393.3-396.3	quartz stringers		6214	core	392.9	396.2	0.01	<0.001	3.3
		393.4-394.0	7.0						
		394.0-394.9	2.0						
		394.9-399.5	25.0						
399.5-400.0	quartz stringers		6215	core	396.2	399.5	0.01	<0.001	3.3
		400.0-401.5	18.0						
		401.5-405.0	1.5						
		405.0-405.3	26.0						
409.0-409.1	quartz vein	405.3-409.0	12.0						
		409.0-409.1	15.0						
			6217	core	409.0	412.3	0.01	<0.001	3.3
		409.1-409.3	1.5						
411.7-412.3	quartz stringers	409.3-409.8	27.0						
		409.8-410.4	12.0						
		410.4-419.1	3.5						
417.3-450.0	Arenite, Lesser Grit and Graphitic Pelite thin layering								
		419.1-420.2	55.0						
			6218	core	419.1	420.2	0.01	<0.001	1.1
		420.2-422.5	2.0						
		422.5-425.2	18.0						
426.3-427.3	quartz vein		6219	core	422.5	425.2	0.01	<0.001	2.7
		425.2-429.5	4.5						
		429.5-430.8	16.0						
			6220	core	429.5	430.8	0.01	<0.001	1.3
		430.8-433.1	2.5						
		433.1-434.4	8.0						
		434.4-436.0	3.0						
		436.0-436.2	30.0						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
436.2-438.6		5.0							
438.6-439.5		21.0							
			6221	core	438.6	442.0	0.01	<0.001	3.4
			6222	LG Standard			1.69	0.049	
439.5-440.6		5.0							
440.6-442.0		17.0							
442.0-444.8		5.0							
444.8-445.6		12.0							
			6223	core	444.8	450.0	0.01	<0.001	5.2
445.6-446.5		2.0							
446.5-450.0		8.5							
450.0-529.2	Arenite, Lesser Graphitic Pelite and Grit thin layering								
450.0-453.9		4.0							
453.9-455.3		8.0							
455.3-459.6		2.5							
459.6-460.0		20.0							
			6224	core	459.6	461.7	0.01	<0.001	2.1
460.0-461.3		10.0							
461.3-461.7		33.0							
461.7-464.2		9.0							
464.2-465.0		21.0							
			6225	core	464.2	465.0	0.02	0.001	0.8
465.0-468.6		15.0							
			6226	core	465.0	468.6	0.01	<0.001	3.6
468.6-471.0		5.0							
471.0-478.0		17.0							
			6227	core	471.0	474.0	0.01	<0.001	3.0
			6228	core	474.0	478.0	0.01	<0.001	4.0
478.0-480.7		4.0							
			6229	core	480.5	484.3	0.01	<0.001	3.8
480.7-484.3		12.0							
484.3-486.0		35.0							
			6230	core	484.3	486.0	0.01	<0.001	1.7
486.0-489.8		24.0							
			6231	core	486.0	489.8	0.02	0.001	3.8
489.8-497.2		1.5							

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
		497.2-500.4	3.0						
498.0-498.2	quartz stringers								
		500.4-511.5	1.5						
		511.5-521.5	3.5						
		521.5-528.0	1.5						
		528.0-529.0	3.5						
529.2-557.4	Arenite, Lesser Grit and Graphitic Pelite								
	thin layering	529.0-578.7	1.5						
534.3-535.3	quartz stringers								
537.4-537.6	quartz stringers								
538.7-539.0	quartz stringers								
541.0-544.9	quartz stringers								
557.4-616.0	Arenite, Lesser Graphitic Pelite and Grit								
	thin to medium layering								
562.9-563.2	quartz stringers								
		578.7-581.6	4.5						
580.7-580.9	quartz stringers								
		581.6-602.2	0.5						
		602.2-605.3	7.0						
			6232	core	602.2	605.3	0.03	0.001	3.1
			6233	duplicate	602.2	605.3	0.03	0.001	3.1
604.1-605.7	quartz stringers								
		605.3-615.3	0.5						
608.4-614.5	chloritized, moderately dolomitized and weakly sericitized								
614.5-616.5	strongly dolomitized, moderately chloritized and weakly sericitized								
614.7-616.0	quartz stringers								
		615.3-615.4	7.0						
		615.4-635.0	0.5						
616.0-624.1	Grit, Lesser Graphitic Pelite and Arenite								
	thin to medium layering								
616.5-624.2	strongly sericitized, moderately dolomitized and weakly chloritized								
624.1-645.5	Graphitic Pelite, Lesser Arenite and Grit								
	thin to medium layering								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
624.2-628.7	strongly dolomitized, moderately chloritized and weakly sericitized								
628.7-633.6	strongly sericitized, moderately dolomitized and weakly chloritized								
633.6-645.5	strongly dolomitized, moderately sericitized and weakly chloritized								
		635.0-635.9	4.0						
635.8-637.2	quartz stringers								
		635.9-643.4	0.5						
		643.4-652.1	1.0						
645.5-655.5	Grit, Lesser Graphitic Pelite and Arenite thin to medium layering								
645.5-656.6	strongly sericitized, moderately chloritized and weakly dolomitized	652.1-662.9	0.5						
655.5-662.9	Graphitic Pelite, Lesser Arenite and Grit thin to medium layering								
656.6-659.7	strongly sericitized, moderately dolomitized and weakly chloritized								
659.0-659.7	Fault Zone								
659.7-662.9	strongly dolomitized, moderately sericitized and weakly chloritized								
662.9-708.8	Grit, Lesser Graphitic Pelite and Arenite thin layering								
662.9-679.5	strongly sericitized, moderately dolomitized and weakly chloritized	662.9-663.1	1.5						
		663.1-672.9	0.5						
665.1-665.6	quartz stringers								
665.9-666.2	fault								
668.0-668.2	fault								
669.4-669.8	quartz stringers	672.9-686.0	1.0						
678.9-679.5	quartz stringers								
679.5-691.7	strongly dolomitized, moderately sericitized and weakly chloritized								
682.7-683.1	quartz stringers								
686.0-686.8	quartz stringers	686.0-686.8	4.0						
		686.8-689.8	2.0						
		689.8-690.9	3.0						
		690.9-693.9	1.0						
691.7-713.5	strongly sericitized, moderately dolomitized and weakly chloritized								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
		693.9-699.5	0.5						
696.5-697.7	fault								
698.8-699.5	Fault Zone								
		699.5-708.8	1.0						
704.0-704.2	quartz stringers								
706.7-707.2	fault								
708.8-718.6	Arenite, Lesser Pelite and Grit thin layering								
		708.8-750.0	0.5						
713.5-715.0	chloritized, moderately dolomitized and weakly sericitized								
715.0-719.3	strongly sericitized, moderately dolomitized and weakly chloritized								
718.6-740.8	Calcareous Grit, Arenite and Pelite thin layering								
719.3-721.9	strongly sericitized and moderately dolomitized								
721.7-722.4	calcite stringers								
721.9-736.0	strongly dolomitized, moderately sericitized and weakly chloritized								
736.0-827.6	strongly sericitized and moderately dolomitized								
736.0-740.8	strongly dolomitized, moderately chloritized and weakly sericitized								
736.0-736.5	calcite stringers								
740.8-741.6	Grit, Arenite and Pelite thin to medium layering								
740.8-741.6	strongly sericitized, moderately chloritized and weakly dolomitized								
741.6-783.0	Calcareous Conglomerate, Grit and Arenite thick to medium layering								
741.6-746.7	chloritized, moderately dolomitized and weakly sericitized								
746.7-755.7	strongly dolomitized, moderately sericitized and weakly chloritized								
		750.0-783.0	0.7						
754.0-797.1	calcite stringers								
755.7-767.5	strongly sericitized, moderately chloritized and weakly dolomitized								
767.5-774.0	strongly dolomitized, moderately chloritized and weakly sericitized								
771.3-771.5	fault								
772.6-773.4	Fault Zone								
774.0-783.0	chloritized, moderately dolomitized and weakly sericitized								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
783.0-797.5	Calcareous Grit, Conglomerate and Arenite thick to medium layering								
783.0-795.1	strongly dolomitized, moderately sericitized and weakly chloritized								
		783.0-795.1	4.0						
795.1-797.5	chloritized and moderately dolomitized								
		795.1-799.3	1.0						
797.1-797.2	calcite vein								
797.2-802.0	calcite stringers								
797.5-799.3	Calcareous Conglomerate and Grit medium layering								
797.5-799.3	strongly dolomitized, moderately chloritized and weakly sericitized								
799.3-800.0	Calcareous Arenite and Grit medium layering								
799.3-800.0	chloritized and moderately dolomitized								
		799.3-800.0	2.0						
800.0-801.3	Calcareous Grit, Conglomerate and Arenite medium layering								
800.0-801.3	strongly dolomitized, moderately sericitized and weakly chloritized								
		800.0-801.3	1.0						
801.3-802.0	Calcareous Conglomerate, Grit and Arenite medium layering								
801.3-802.0	strongly sericitized, moderately chloritized and weakly dolomitized								
		801.3-809.8	3.5						
802.0-809.8	Calcareous Grit and Arenite medium layering								
802.0-816.9	chloritized, moderately sericitized and weakly dolomitized								
802.0-802.3	calcite vein								
802.3-824.0	calcite stringers								
809.8-822.3	Calcareous Arenite and Pelite thick layering								
		809.8-816.9	1.5						
816.9-853.3	chloritized, moderately sericitized and weakly dolomitized								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
816.9-818.4	strongly sericitized, moderately chloritized and weakly dolomitized								
		816.9-827.6	2.0						
818.4-832.3	strongly sericitized, moderately chloritized and weakly dolomitized								
822.3-832.3	Calcareous Grit, Pelite and Arenite								
	medium layering								
827.6-923.9	calcite stringers								
		827.6-832.3	1.5						
832.3-926.3	Calcareous Pelite and Arenite								
	thin to medium layering								
		832.3-836.2	0.7						
		836.2-853.3	1.0						
853.3-859.1	strongly sericitized and moderately chloritized								
		853.3-859.1	1.5						
859.1-863.0	chloritized, moderately sericitized and weakly dolomitized								
		859.1-863.0	0.7						
863.0-865.5	strongly sericitized								
		863.0-865.5	1.0						
865.5-874.1	chloritized, moderately sericitized and weakly dolomitized								
		865.5-878.7	0.7						
874.1-874.7	strongly sericitized								
874.7-877.0	chloritized, moderately sericitized and weakly dolomitized								
877.0-836.2	chloritized								
877.0-877.8	strongly sericitized and moderately dolomitized								
877.8-878.7	chloritized								
878.7-882.7	strongly sericitized, moderately chloritized and weakly dolomitized								
		878.7-882.7	1.5						
882.7-884.6	chloritized and moderately sericitized								
		882.7-884.6	0.7						
884.6-888.3	strongly sericitized and moderately chloritized								
		884.6-888.3	2.0						
888.3-923.9	chloritized, moderately sericitized and weakly dolomitized								
		888.3-923.9	0.7						
923.9-929.2	chloritized								
		923.9-944.2	1.5						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
926.3-929.8	Calcareous Pelite and Arenite thick layering								
929.2-944.2	strongly sericitized, moderately chloritized and weakly dolomitized								
929.8-944.2	Grit, Arenite and Pelite thin to medium layering								
931.7-938.8	calcite stringers								
940.7-942.3	calcite stringers								
944.2-1010.0	Graphitic Arenite and Pelite thin layering								
944.2-958.5	strongly sericitized and moderately dolomitized								
		944.2-1000.0	3.5						
944.8-945.0	quartz stringers		6234	core	946.5	952.0	0.03	0.001	5.5
958.5-975.0	chloritized, moderately sericitized and weakly dolomitized								
975.0-983.5	silicified and moderately sericitized								
983.5-1001.5	strongly sericitized and moderately dolomitized								
1010.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-11

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: July 17, 2001
 Date Completed: July 23, 2001
 Final Depth: **377 feet (114.9 m)**

Collar Grid Coordinates
Northing Easting Elevation
 Mine Grid **2394.0 ft. 20068.0 ft. 4785.0 ft.**

Logged by: **D. Hladky**

Depth	Azimuth	Dip
collar	43°	-52°
0.0 ft.	43°	-52°
150.0 ft.	41°	-53°
357.0 ft.	42°	-52°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-35.0	Overburden								
35.0-73.0	Arenite and Graphitic Pelite thin to very thin layering								
39.7-58.0	silicified								
49.1-49.4	Fault Zone								
54.9-55.1	quartz vein								
55.1-58.0	quartz stringers								
58.0-61.1	strongly dolomitized and moderately silicified								
61.1-61.5	fault								
65.7-66.0	fault								
69.4-73.0	quartz stringers								
73.0-77.0	Graphitic Pelite and Arenite very thin to thin layering								
75.6-75.9	quartz vein								
77.0-83.2	Arenite, Graphitic Pelite and Grit thin to very thin layering								
79.9-81.2	quartz stringers								
80.6-84.8	strongly dolomitized and moderately sericitized								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
83.2-88.9	Grit, Arenite and Graphitic Pelite thin to very thin layering								
84.8-85.0	fault								
		86.5-90.2	1.5						
88.9-90.2	Graphitic Pelite and Arenite thin to very thin layering								
90.2-95.5	Grit, Graphitic Pelite and Arenite thin to medium layering								
		90.2-122.2	0.7						
95.5-117.5	Arenite, Graphitic Pelite and Grit thin to very thin layering								
100.0-100.4	strongly sericitized								
101.7-106.1	quartz stringers								
110.7-111.1	fault								
111.3-112.2	fault								
112.5-113.4	fault								
112.6-112.8	quartz stringers								
116.0-116.1	fault								
117.5-134.7	Grit, Arenite and Graphitic Pelite thin to medium layering								
118.0-118.3	quartz stringers								
118.1-118.8	fault								
122.2-122.8	quartz stringers								
		122.2-147.0	1.0						
124.4-124.7	quartz stringers								
134.7-139.8	Grit, Graphitic Pelite and Arenite thin to medium layering								
136.0-136.8	quartz stringers								
139.3-139.8	quartz stringers								
139.8-148.3	Grit, Arenite and Graphitic Pelite thin to medium layering								
142.9-143.5	quartz stringers								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
144.5-145.0	quartz stringers								
		147.0-169.8	0.7						
147.4-147.6	fault								
148.3-157.3	Grit and Arenite medium to thin layering								
148.3-148.5	fault								
148.5-148.7	quartz vein								
157.3-169.8	Grit, Arenite and Graphitic Pelite thin to medium layering								
166.4-168.5	quartz stringers								
167.1-168.5	silicified and moderately sericitized								
169.8-172.8	Graphitic Pelite and Arenite thin to very thin layering								
		169.8-179.0	1.5						
170.1-173.0	quartz stringers								
172.4-172.8	fault								
172.8-178.9	Arenite, Graphitic Pelite and Grit thin layering								
172.8-174.2	silicified, moderately sericitized and weakly dolomitized								
174.2-174.4	strongly sericitized								
174.4-175.8	silicified								
175.8-176.2	strongly sericitized and moderately silicified								
176.2-177.5	silicified								
177.5-178.2	quartz stringers								
178.9-208.3	Grit, Arenite and Graphitic Pelite thin to medium layering								
		179.0-205.3	0.7						
180.7-180.8	fault								
185.0-186.0	quartz stringers								
185.8-190.4	silicified and moderately sericitized								
192.1-199.5	strongly dolomitized, moderately sericitized and weakly silicified								
199.1-199.5	quartz stringers								
199.5-205.3	silicified and moderately sericitized								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
203.1-203.3	quartz vein								
205.2-209.5	quartz stringers								
		205.3-208.3	2.0						
208.3-266.3	Graphitic Pelite, Arenite and Grit thin layering								
		208.3-210.1	5.5						
209.5-210.1	fault		6426	core	209.6	212.0	2.79	0.081	2.4
209.7-238.8	strongly sericitized and moderately dolomitized								
		210.1-212.0	5.0						
210.8-211.0	fault								
		212.0-212.2	35.0						
			6235	core	212.0	217.0	14.73	0.430	5.0
		212.2-213.5	7.0						
212.4-214.2	quartz stringers								
		213.5-214.4	17.0						
		214.4-215.0	7.0						
215.0-215.3	quartz vein								
		215.0-216.3	3.0						
		216.3-217.0	7.0						
		217.0-223.1	1.5						
			6427	core	217.0	219.9	0.22	0.006	2.9
217.1-218.9	quartz stringers								
218.9-219.3	quartz vein								
219.3-221.5	quartz stringers								
			6428	core	219.9	223.1	0.33	0.010	3.2
		223.1-224.1	11.0						
			6236	core	223.1	224.8	43.64	1.273	1.7
		224.1-224.6	28.0						
224.6-224.8	fault								
		224.6-230.6	7.0						
			6237	core	224.8	230.9	0.61	0.018	6.1
225.7-226.2	fault								
227.5-229.5	quartz stringers								
		230.6-230.9	30.0						
		230.9-232.9	4.0						
231.6-231.8	fault								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
232.9-234.6		12.0							
233.5-237.0	quartz stringers		6238	core	232.9	234.6	12.90	0.376	1.7
				core	209.6	234.6	7.32	0.213	25.0
234.6-238.8		3.5							
238.0-239.0 238.8-242.8	quartz stringers strongly dolomitized and moderately sericitized		6429	core	230.9	232.9	0.51	0.015	2.0
			6430	core	234.6	237.5	0.03	0.001	2.9
			6239	core	237.5	238.8	0.09	0.003	1.3
238.8-239.5		8.0							
			6432	core	238.8	240.1	0.09	0.003	1.3
239.5-256.6		6.5							
242.8-377.0 243.1-246.7	strongly sericitized and moderately dolomitized quartz stringers								
			6240	core	248.0	253.0	0.08	0.002	5.0
251.5-251.7	fault								
253.0-254.5	quartz stringers								
256.6-257.9		8.0							
257.7-260.4	quartz stringers								
257.9-262.4		3.0							
			6242	core	262.0	267.0	0.04	0.001	5.0
262.4-263.1		6.0							
263.1-275.8		4.0							
266.3-312.2	Arenite, Grit and Graphitic Pelite thin to medium layering								
269.0-273.0	quartz stringers		6243	core	267.0	272.0	0.04	0.001	5.0
			6244	core	272.0	275.8	0.02	0.001	3.8
			6245	Standard			1.61	0.047	
275.8-279.7		8.0							
			6246	core	275.8	279.9	0.05	0.001	4.1
279.7-279.9		20.0							
279.9-285.5		1.5							
284.5-284.6	fault								
285.5-286.1		9.0							

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
286.0-286.7	fault		6247	core	285.5	288.0	0.02	0.001	2.5
		286.1-287.7	1.5						
		287.7-288.0	10.0						
		288.0-293.8	5.0						
289.0-289.2	fault		6248	core	288.0	293.8	0.02	0.001	5.8
		293.8-296.0	8.5						
			6249	core	293.8	298.9	0.01	<0.001	5.1
		296.0-299.8	2.0						
			6250	core	298.9	302.8	0.01	<0.001	3.9
		299.8-301.4	7.0						
		301.4-302.8	2.0						
		302.8-309.1	8.0						
			6251	core	302.8	309.1	0.01	<0.001	6.3
		309.1-312.2	2.0						
312.2-377.0	Grit, Arenite and Graphitic Pelite thin to medium layering								
		312.2-313.1	4.0						
			6252	core	312.2	316.9	0.04	0.001	4.7
		313.1-316.4	2.0						
315.2-315.5	fault								
		316.4-316.9	7.0						
		316.9-319.3	2.0						
		319.3-320.1	5.0						
			6253	core	319.3	322.6	0.02	0.001	3.3
		320.1-321.7	2.0						
		321.7-322.6	14.0						
		322.6-326.4	2.0						
		326.4-330.0	14.0						
			6254	core	326.4	330.0	0.03	0.001	3.6
332.8-335.5	quartz stringers	330.0-332.5	2.0						
		332.5-336.6	12.0						
			6255	core	332.5	337.8	0.03	0.001	5.3
336.5-337.0	quartz stringers	336.6-344.0	8.0						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
			6256	core	337.8	344.0	0.19	0.006	6.2
		3.0							
			6257	core	344.0	347.5	0.04	0.001	3.5
		8.0							
		1.5							
349.1-349.5	quartz vein								
351.0-351.2	quartz stringers								
		9.0							
			6258	core	351.5	356.4	0.01	<0.001	4.9
		1.5							
		10.0							
		2.0							
		20.0							
		3.0							
			6259	core	356.4	361.8	0.01	<0.001	5.4
		16.0							
357.4-357.9	quartz stringers								
		15.0							
		2.0							
			6260	core	361.8	365.3	0.02	0.001	3.5
		14.0							
		1.5							
		12.0							
		2.0							
373.0-375.0	quartz stringers								
377.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-12

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: July 24, 2001
 Date Completed: August 1, 2001
 Final Depth: **530 feet (161.5 m)**

Collar Grid Coordinates
 Northing Easting Elevation
 Mine Grid 2934.0 ft. 21401.0 ft. 4787.0 ft.

Logged by: R.D. Hall

Depth	Azimuth	Dip
collar	226°	-43°
200.0 ft.	226°	-38°
520.0 ft.	236°	-36°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-25.0	Overburden								
25.0-42.6	Chlorite-bearing Pelite and Arenite very thin layering								
25.0-47.6	chloritized								
25.0-36.6	quartz stringers								
		25.0-42.6	0.5						
31.7-32.0	fault								
36.6-36.9	quartz vein								
			6261	core	36.6	41.7	0.01	<0.001	5.1
36.9-37.7	quartz stringers								
37.7-38.5	quartz vein								
38.5-41.1	quartz stringers								
41.1-41.7	quartz vein								
41.7-62.0	quartz stringers								
42.6-51.6	Magnetite- and Chlorite-bearing Pelite and Arenite very thin layering								
		42.6-51.3	2.0						
47.6-50.3	strongly sericitized and moderately dolomitized								
		51.3-61.2	0.7						
51.6-61.2	Biotite-bearing Pelite and Arenite very thin layering								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
61.2-71.8	Pelite and Arenite very thin layering								
61.2-135.4	strongly dolomitized and moderately sericitized								
		61.2-70.2	1.5						
			6262	core	61.2	67.0	0.02	0.001	5.8
64.0-67.0	quartz stringers								
			6263	core	67.0	70.2	0.03	0.001	3.2
		70.2-71.0	9.0						
			6264	core	70.2	72.0	0.31	0.009	1.8
		71.0-71.8	2.0						
71.8-87.4	Magnetite-bearing Pelite and Arenite very thin layering								
		71.8-87.4	2.5						
			6265	core	72.0	77.0	0.13	0.004	5.0
75.6-76.5	Fault Zone								
			6266	core	77.0	82.0	0.88	0.026	5.0
82.0-84.0	quartz stringers								
			6267	core	82.0	87.0	0.64	0.019	5.0
87.0-89.5	quartz stringers								
			6268	core	87.0	92.0	0.03	0.001	5.0
87.4-105.0	Pelite and Arenite very thin layering								
		87.4-105.0	1.5						
			6269	LG Standard			1.72	0.050	
105.0-111.6	Magnetite-bearing Pelite and Arenite very thin layering								
		105.0-111.6	2.0						
111.6-135.4	Dolomite Porphyroblastic Pelite and Arenite very thin layering								
		111.6-130.2	1.2						
112.5-113.1	quartz vein								
118.1-122.5	quartz vein								
125.8-125.9	fault								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
130.2-132.0	quartz vein		6270	core	127.0	130.2	0.30	0.009	3.2
		15.0							
130.2-131.9			6271	core	130.2	132.0	2.06	0.060	1.8
131.9-135.4		1.5							
			6272	core	132.0	135.5	0.11	0.003	3.5
135.4-190.0	Graphitic Pelite and Arenite very thin layering								
		35.0							
135.5-135.5	quartz stringers								
135.5-148.5	quartz vein								
135.5-136.8		9.0							
			6273	core	135.5	137.0	5.13	0.150	1.5
136.8-140.0		3.2							
137.0-161.6	Fault Zone			core	130.2	137.0	1.73	0.051	6.8
			6274	core	137.0	142.0	0.16	0.005	5.0
140.0-161.6		1.0							
			6275	core	142.0	147.0	0.07	0.002	5.0
			6276	core	147.0	152.0	0.04	0.001	5.0
148.5-200.0	quartz stringers								
			6277	core	161.2	165.4	0.02	0.001	4.2
			6278	1/4 core	161.2	165.4	0.02	0.001	4.2
161.6-165.4		0.5							
161.8-165.4	strongly dolomitized and moderately sericitized								
165.4-193.7		1.5							
167.4-168.0	Fault Zone								
169.1-169.6	fault								
178.5-178.6	fault								
188.7-188.8	fault								
189.3-200.0	fault								
			6279	core	188.7	193.3	0.35	0.010	4.6
190.0-250.0	Pelite and Arenite very thin layering strongly sericitized								
193.3-202.8			6280	core	193.3	196.2	2.72	0.079	2.9

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
193.7-194.2		2.2							
194.2-195.0		10.2							
195.0-195.8		55.2							
195.8-200.0		1.2							
			6281	core	196.2	200.0	0.03	0.001	3.8
200.0-202.8		1.0							
			6282	core	200.0	202.8	0.07	0.002	2.8
202.8-255.3	strongly sericitized and moderately dolomitized								
202.8-205.2		4.8							
			6283	core	202.8	205.3	0.09	0.003	2.5
205.2-205.9		30.0							
			6284	core	205.3	205.9	51.91	1.514	0.6
				core	193.3	205.9	3.14	0.092	12.6
205.9-214.3		4.8							
			6285	core	205.9	207.0	0.46	0.013	1.1
			6286	core	207.0	212.0	0.12	0.004	5.0
214.3-235.8		1.0							
			6287	core	232.0	235.8	0.01	<0.001	3.8
235.8-236.1	quartz vein								
235.8-245.5		5.0							
			6288	core	235.8	242.0	0.01	<0.001	6.2
236.1-236.7	quartz stringers								
236.7-239.3	quartz vein								
239.3-244.7	quartz stringers								
242.0-243.0	fault								
			6289	core	242.0	245.5	0.06	0.002	3.5
244.7-245.5	quartz vein								
245.5-253.0		3.2							
			6290	core	245.5	253.0	0.01	<0.001	7.5
247.4-248.0	fault								
250.0-376.0	Pelite and Arenite thin layering								
253.0-255.3		10.2							
			6291	core	253.0	255.3	0.02	0.001	2.3
253.8-254.0	quartz vein								
254.1-254.6	fault								
255.3-262.3	silicified and moderately sericitized								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
255.3-262.3		7.2							
			6292	core	255.3	262.3	0.13	0.004	7.0
256.0-256.2	fault								
260.5-267.0	quartz stringers								
262.3-267.0	strongly sericitized and moderately dolomitized								
262.3-279.3		5.2							
			6293	core	262.3	267.0	0.11	0.003	4.7
264.0-264.3	fault								
266.0-266.2	fault								
267.0-275.3	strongly sericitized								
267.0-279.3	quartz vein								
			6294	core	267.0	272.0	0.07	0.002	5.0
			6295	core	272.0	275.3	0.10	0.003	3.3
			6296	core	275.3	279.3	0.09	0.003	4.0
279.3-291.0	quartz stringers								
279.3-307.0		3.2							
			6297	core	279.3	288.8	0.01	<0.001	9.5
288.8-308.0	silicified								
			6298	core	288.8	297.0	0.01	<0.001	8.2
			6299	core	297.0	308.0	0.01	<0.001	11.0
304.0-304.5	fault								
307.0-313.0	quartz stringers								
307.0-314.0		2.0							
308.0-308.5	fault								
			6300	core	308.0	314.0	0.01	<0.001	6.0
309.5-309.6	fault								
314.0-318.7	silicified and moderately sericitized								
314.0-327.3		7.2							
			6301	core	314.0	318.7	0.01	<0.001	4.7
317.2-317.9	fault								
318.7-321.7	silicified								
			6302	core	318.7	321.7	0.01	<0.001	3.0
320.4-320.5	fault								
321.7-327.3	strongly sericitized and moderately silicified								
			6303	core	321.7	327.3	0.01	<0.001	5.6
327.3-329.0		3.0							
			6304	core	327.3	334.8	0.01	<0.001	7.5
329.0-368.5	silicified								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
329.0-334.9		5.0							
332.0-368.5	quartz stringers		6305	core	334.8	335.3	0.01	<0.001	0.5
334.9-335.3		30.0							
335.3-349.7		5.0	6306	core	335.3	342.0	0.01	<0.001	6.7
341.7-341.8	fault		6307	core	342.0	349.7	0.01	<0.001	7.7
349.7-376.2		1.0	6308	core	349.7	357.0	0.02	0.001	7.3
			6309	core	357.0	368.5	0.01	<0.001	11.5
361.8-362.1	fault		6310	core	368.5	375.4	0.01	<0.001	6.9
368.6-368.7	fault								
370.9-377.3	fault		6311	core	375.4	382.0	0.02	0.001	6.6
376.0-407.3	Graphitic Pelite thin layering								
376.2-407.3		5.0	6312	core	382.0	387.0	0.01	<0.001	5.0
382.5-382.7	fault		6313	core	387.0	392.0	0.01	<0.001	5.0
385.0-388.0	fault		6314	core	392.0	397.0	0.01	<0.001	5.0
389.0-389.8	fault		6315	core	397.0	407.0	0.01	<0.001	10.0
390.5-391.8	fault		6316	core	407.0	417.0	0.01	<0.001	10.0
406.6-406.9	fault								
407.3-435.0	Arenite and Pelite medium layering								
407.3-417.0		5.2							
408.0-435.0	silicified								
417.0-431.0	quartz stringers								
417.0-435.0		3.2	6317	core	417.0	427.0	0.01	<0.001	10.0

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
			6318	core	427.0	435.0	0.02	0.001	8.0
435.0-443.5	Graphitic Pelite and Arenite very thin layering								
		435.0-443.5	2.0						
443.2-444.2	fault								
443.5-510.8	Arenite and Pelite very thin layering								
		443.5-497.6	1.0						
449.0-452.0	quartz stringers								
463.5-464.0	fault								
465.0-473.0	quartz stringers								
472.0-482.0	strongly sericitized								
478.7-479.1	fault								
		497.6-510.8	0.8						
498.0-499.6	quartz stringers								
499.6-510.7	strongly dolomitized and moderately sericitized								
499.6-510.7	quartz and dolomite stringers								
			6319	core	499.6	507.0	0.01	<0.001	7.4
			6320	core	507.0	510.7	0.01	<0.001	3.7
510.8-525.9	Graphitic Pelite and Arenite very thin layering								
510.7-511.5	quartz stringers								
		510.8-525.9	3.0						
523.3-523.6	fault								
525.9-530.0	Arenite and Pelite medium layering								
		525.9-530.0	1.0						
526.5-530.0	quartz stringers								
530.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-13

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: August 1, 2001
 Date Completed: August 19, 2001
 Final Depth: **537 feet (163.7 m)**

Collar Grid Coordinates
 Northing Easting Elevation
 Mine Grid **2935.0 ft. 21401.0 ft. 4787.0 ft.**

Logged by: J. Kowalchuk

Depth	Azimuth	Dip
collar	226°	-60°
20.0 ft.	231°	-58°
150.0 ft.	228°	-57°
337.0 ft.	230°	-54°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-25.0	Overburden								
25.0-32.0	Magnetite- and Chlorite-bearing Pelite and Arenite very thin layering								
25.0-54.6	chloritized								
		25.0-61.8	10.0						
32.0-51.0	Chlorite-bearing Arenite and Pelite very thin layering								
39.0-40.4	quartz vein								
43.0-51.0	quartz stringers								
51.0-61.0	Magnetite- and Chlorite-bearing Arenite very thin layering								
54.6-141.4	strongly sericitized and moderately silicified								
61.0-85.0	Arenite very thin layering								
		61.8-97.0	0.5						
67.0-77.5	quartz stringers								
			6332	core	77.0	82.0	0.24	0.007	5.0
77.5-77.7	quartz vein								
77.7-87.0	quartz stringers								
			6333	core	82.0	87.0	0.05	0.001	5.0

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
85.0-97.0	Magnetite-bearing Arenite and Grit thin layering								
87.0-88.0	quartz vein								
88.0-154.5	quartz stringers								
			6334	core	93.0	97.0	8.63	0.252	4.0
97.0-107.0	Pelite and Arenite very thin layering								
		5.0							
107.0-112.0	Magnetite-bearing Pelite and Arenite very thin layering								
		0.5							
			6335	core	107.0	112.0	0.60	0.018	5.0
		5.0							
112.0-127.0	Arenite and Pelite medium layering								
			6336	core	112.0	117.0	0.59	0.017	5.0
			6337	core	117.0	122.0	0.23	0.007	5.0
			6338	core	122.0	127.0	0.27	0.008	5.0
		0.5							
127.0-135.0	Pelite and Arenite very thin layering								
			6339	core	127.0	132.0	0.11	0.003	5.0
			6340	core	132.0	137.0	0.17	0.005	5.0
135.0-154.5	Arenite and Grit thin layering								
		2.0							
			6341	core	137.0	142.0	0.19	0.006	5.0
141.4-154.5	silicified								
			6342	core	142.0	147.0	0.20	0.006	5.0
			6343	core	147.0	152.0	0.16	0.005	5.0
			6344	core	152.0	157.0	0.75	0.022	5.0

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
154.5-176.7	Arenite and Graphitic Pelite very thin layering								
154.5-176.7	carbonized								
154.5-155.0	fault								
		154.5-176.7	10.0						
			6345	core	157.0	162.0	0.21	0.006	5.0
			6346	core	162.0	169.0	0.68	0.020	7.0
166.0-176.7	fault								
			6347	core	169.0	177.0	0.17	0.005	8.0
176.7-218.0	Arenite and Grit thin layering								
176.7-219.3	strongly sericitized and moderately silicified								
		176.7-302.0	0.5						
217.0-237.0	quartz stringers								
218.0-269.0	Grit and Arenite medium layering								
219.3-247.0	chloritized and moderately silicified								
247.0-261.2	strongly sericitized and moderately silicified								
261.2-296.5	silicified and moderately sericitized								
269.0-309.5	Arenite and Pelite thin layering								
			6348	core	292.0	297.0	0.07	0.002	5.0
296.5-302.0	chloritized								
			6349	core	297.0	302.0	0.41	0.012	5.0
298.0-302.8	fault								
302.0-308.5	strongly sericitized								
		302.0-308.5	3.0						
			6350	core	302.0	308.5	0.04	0.001	6.5
304.0-327.0	quartz stringers								
308.5-334.0	carbonized								
		308.5-334.0	5.0						
			6351	core	308.5	312.0	0.02	0.001	3.5
309.5-318.0	Arenite and Pelite medium layering								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
318.0-362.0	Pelite and Arenite very thin layering		6352	core	312.0	317.0	0.02	0.001	5.0
			6353	core	317.0	322.0	0.08	0.002	5.0
			6354	core	322.0	327.0	0.17	0.005	5.0
			6355	core	327.0	332.0	0.02	0.001	5.0
334.0-405.3	strongly sericitized								
334.0-334.5	fault								
362.0-406.0	Pelite very thin layering								
367.0-368.5		5.0							
			6356	core	367.0	372.0	0.01	<0.001	5.0
368.5-368.8		20.0							
368.8-377.0		5.0							
			6357	core	372.0	377.0	0.01	<0.001	5.0
377.0-378.6		20.0							
			6358	core	377.0	379.0	0.03	0.001	2.0
378.6-392.0		0.5							
			6359	core	379.0	383.0	0.01	<0.001	4.0
			6360	core	383.0	388.0	0.01	<0.001	5.0
			6361	core	388.0	394.0	0.02	0.001	6.0
392.0-393.8		10.0							
393.8-395.3		25.0							
			6362	core	394.0	395.6	0.05	0.001	1.6
395.3-396.9		4.0							
			6363	core	395.6	397.0	0.01	<0.001	1.4
396.9-400.5		25.0							
			6364	core	397.0	401.0	0.04	0.001	4.0
400.5-405.3		1.0							
			6365	core	401.0	407.0	0.03	0.001	6.0
405.3-415.6		5.0							
406.0-427.0	Arenite and Graphitic Pelite very thin layering								
407.0-414.0	quartz stringers								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
			6366	core	407.0	412.0	0.06	0.002	5.0
			6367	core	412.0	417.0	0.05	0.001	5.0
		4.0							
			6368	core	417.0	422.0	0.02	0.001	5.0
		8.0							
			6369	core	422.0	427.0	0.02	0.001	5.0
426.0-427.0	fault								
427.0-458.5	Graphitic Arenite and Grit very thin layering								
			6370	core	427.0	432.0	0.10	0.003	5.0
		4.0							
			6371	core	432.0	437.0	0.03	0.001	5.0
			6372	HG Standard			3.37	0.098	
436.0-440.0	quartz stringers								
436.0-440.0	fault								
			6373	core	437.0	442.0	0.05	0.001	5.0
			6374	core	442.0	447.0	0.02	0.001	5.0
		5.0							
444.3-460.0	strongly sericitized								
		4.0							
			6375	core	447.0	452.0	0.01	<0.001	5.0
			6376	core	452.0	457.0	0.02	0.001	5.0
			6377	core	457.0	462.0	0.03	0.001	5.0
458.5-487.0	Pelite very thin layering								
		10.0							
460.0-463.2	strongly sericitized								
			6378	core	462.0	467.0	0.03	0.001	5.0
466.6-467.4	quartz vein								
			6379	core	467.0	472.0	0.01	<0.001	5.0
			6380	LG Standard			0.86	0.025	
468.6-469.5	quartz vein								
		2.0							
469.5-487.0	strongly sericitized								
			6381	core	472.0	477.0	0.01	<0.001	5.0
			6382	core	477.0	482.0	0.01	<0.001	5.0

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
			6383	core	482.0	487.0	0.01	<0.001	5.0
		25.0							
		2.0							
487.0-502.0	Graphitic Pelite and Arenite very thin layering								
		10.0							
			6384	core	487.0	492.0	0.01	<0.001	5.0
			6385	core	492.0	497.0	0.01	<0.001	5.0
			6386	core	497.0	502.0	0.01	<0.001	5.0
502.0-522.0	Arenite and Pelite very thin layering								
			6387	core	502.0	507.0	0.01	<0.001	5.0
502.4 520.0	strongly sericitized								
		1.0							
			6388	core	507.0	512.0	0.01	<0.001	5.0
			6389	core	512.0	517.0	0.01	<0.001	5.0
			6390	core	517.0	522.0	0.01	<0.001	5.0
		3.0							
522.0-537.0	Arenite, Graphitic Pelite and Lesser Grit very thin layering								
537.0	E.O.H.								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
96.1-100.4	strongly sericitized and moderately dolomitized								
98.5-99.1	quartz vein								
100.4-101.0	strongly dolomitized								
101.0-111.4	strongly sericitized and moderately dolomitized								
109.2-110.4	quartz stringers								
111.4-114.7	silicified and moderately dolomitized								
114.7-124.7	strongly sericitized and moderately dolomitized								
124.7-127.9	silicified and moderately dolomitized								
127.9-130.7	strongly sericitized and moderately dolomitized								
130.7-131.4	strongly dolomitized								
131.0-160.6	quartz stringers								
131.4-138.9	strongly sericitized and moderately dolomitized								
					131.9-137.3	2.0			
					137.3-158.4	0.5			
138.9-151.4	silicified and moderately dolomitized								
151.4-167.0	strongly sericitized and moderately dolomitized								
158.0-158.1	fault								
					158.4-159.0	3.5			
					159.0-167.0	1.0			
160.6-161.4	dolomite stringers								
161.4-165.5	quartz stringers								
167.0-178.4	strongly sericitized, moderately silicified and weakly dolomitized								
167.0-167.5	quartz stringers								
					167.0-203.0	0.6			
169.0-173.8	quartz stringers								
178.4-203.0	silicified and moderately dolomitized								
203.0-240.0	strongly dolomitized								
					203.0-203.4	8.0			
					203.4-241.1	0.7			
240.0-245.4	strongly sericitized and moderately dolomitized								
					241.1-246.0	3.5			
245.4-281.3	silicified and moderately dolomitized								
					246.0-414.7	0.5			
258.0-259.3	quartz stringers								
259.3-260.8	quartz vein								
260.8-261.2	dolomite stringers								
261.2-261.8	quartz stringers								
271.8-276.0	quartz stringers								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
280.9-284.1	quartz stringers								
281.3-284.0	strongly sericitized and moderately dolomitized								
284.0-304.2	silicified and moderately dolomitized								
284.1-284.3	quartz vein								
286.1-286.8	fault								
304.2-304.3	strongly sericitized								
304.3-318.0	silicified and moderately dolomitized								
312.6-315.2	quartz stringers								
315.2-315.4	quartz vein								
315.4-317.0	quartz stringers								
317.0-318.9	quartz vein								
318.0-322.9	carbonized and moderately dolomitized								
318.9-322.9	quartz stringers								
318.9-320.0	fault								
322.9-374.1	silicified and moderately dolomitized								
324.9-325.7	dolomite stringers								
335.9-338.3	quartz stringers								
364.4-368.6	quartz stringers								
374.1-381.8	silicified								
374.2-379.5	quartz stringers								
377.7-378.0	fault								
378.0-379.4	fault								
381.8-384.2	carbonized and moderately silicified								
381.8-388.6	quartz stringers								
381.8-382.8	fault								
383.4-384.2	fault								
384.2-390.0	silicified and moderately sericitized								
388.6-391.0	quartz vein								
389.6-390.0	fault								
390.0-417.4	strongly sericitized, moderately dolomitized and weakly silicified								
391.0-391.7	quartz stringers								
391.7-392.8	quartz vein								
392.8-414.4	quartz stringers								
407.7-408.8	fault								
409.1-409.5	fault								
410.0-414.0	fault								
414.4-415.0	quartz vein								
414.7-418.4		1.5							

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
415.0-418.4	quartz stringers								
417.4-560.9	Arenite, Lesser Pelite and Grit								
	thin to very thin layering								
417.4-422.1	carbonized								
417.4-418.4	fault								
418.4-421.2	quartz vein								
		0.5							
421.2-430.0	quartz stringers								
		2.0							
			6401	core	421.2	428.3	0.41	0.012	7.1
		5.0							
422.1-515.7	strongly sericitized and moderately dolomitized								
428.3-430.0	fault								
		1.5							
		2.5							
			6402	core	431.0	436.6	0.02	0.001	5.6
		1.5							
439.0-439.3	quartz vein								
		3.0							
		20.0							
		2.5							
445.6-449.5	quartz stringers								
		0.8							
		1.2							
		11.0							
		1.0							
454.1-460.5	quartz stringers								
		2.0							
		8.0							
		3.0							
464.5-464.6	fault								
		8.0							
		3.0							
		5.0							
			6403	core	468.2	471.3	0.01	<0.001	3.1
		2.0							
		9.5							

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
			6404	core	471.3	474.2	0.01	<0.001	2.9
474.2-475.4		2.0							
			6405	core	474.2	478.2	0.01	<0.001	4.0
475.4-476.0		6.5							
476.0-476.8		2.5							
476.8-478.0		12.0							
478.0-479.7		1.5							
479.7-480.5		4.0							
			6406	core	479.7	484.3	0.01	<0.001	4.6
480.5-481.0		1.5							
481.0-483.4		10.0							
483.4-484.3		3.0							
484.3-485.8		14.5							
			6407	core	484.3	488.4	0.01	<0.001	4.1
485.8-488.4	quartz stringers								
		1.5							
		4.5							
		2.0							
		5.5							
488.4-489.6	quartz vein								
			6408	core	488.4	489.6	0.03	0.001	1.2
489.6-495.9		1.5							
494.8-496.3	quartz stringers								
		2.5							
		4.0							
502.0-507.1	quartz stringers								
		1.0							
		7.0							
			6410	core	505.0	509.5	0.01	<0.001	4.5
506.5-507.2		1.5							
507.2-509.5		4.0							
509.5-515.0		3.5							
515.0-516.3		1.0							
515.7-528.1	strongly dolomitized and moderately sericitized								
		5.0							
		1.2							
		10.5							
			6411	core	527.2	529.0	0.02	0.001	1.8

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
528.1-531.0	strongly sericitized and moderately dolomitized								
		529.0-531.6	4.0						
			6412	core	529.0	533.1	0.02	0.001	4.1
531.0-535.7	strongly dolomitized and moderately sericitized								
		531.6-532.4	6.5						
		532.4-534.8	4.5						
			6413	core	533.1	536.7	0.01	<0.001	3.6
		534.8-535.7	1.5						
535.7-536.7	strongly sericitized and moderately dolomitized								
		535.7-536.7	3.5						
536.7-540.0	strongly sericitized and moderately dolomitized								
		536.7-556.3	1.5						
540.0-545.5	strongly dolomitized and moderately sericitized								
545.5-566.5	strongly sericitized and moderately dolomitized								
		556.3-560.9	1.8						
560.9-570.7	Grit, Lesser Arenite and Pelite thin to medium layering								
		560.9-561.7	1.5						
		561.7-566.3	2.5						
		566.3-578.3	1.6						
566.5-570.7	strongly sericitized, moderately dolomitized and weakly chloritized								
570.7-578.3	Arenite, Lesser Grit and Pelite thin to medium layering								
570.7-573.5	chloritized, moderately dolomitized and weakly sericitized								
573.5-578.3	silicified, moderately dolomitized and weakly chloritized								
578.3-581.5	Arenite, Lesser Grit and Pelite thin to medium layering								
578.3-581.5	strongly dolomitized, moderately sericitized and weakly chloritized								
		578.3-592.3	1.0						
581.5-594.7	Grit, Lesser Conglomerate and Arenite and Minor Pelite medium to thin layering								
581.5-586.5	chloritized, moderately sericitized and weakly dolomitized								
586.5-592.3	strongly dolomitized, moderately sericitized and weakly chloritized								
592.3-599.0	strongly sericitized, moderately dolomitized and weakly chloritized								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
592.3-594.7		2.0							
593.7-594.1	quartz stringers								
594.7-608.0	Grit, Lesser Arenite and Pelite thin to medium layering								
594.7-595.5		18.5							
595.5-599.0		2.0	6414	core	594.7	599.0	0.01	<0.001	4.3
599.0-601.6	strongly dolomitized, moderately sericitized and weakly chloritized								
601.6-604.0	strongly sericitized, moderately dolomitized and weakly chloritized								
604.0-625.3	strongly dolomitized and moderately sericitized								
605.0-606.2		8.0							
606.2-613.6		0.7	6415	core	605.0	606.2	0.03	0.001	1.2
608.0-627.7	Calcareous Arenite, Lesser Calcareous Grit and Pelite thin to medium layering								
611.0-633.0	calcite stringers								
613.6-616.0		4.5							
616.0-660.0		0.5							
625.3-627.7	strongly dolomitized and moderately chloritized								
627.7-660.0	Calcareous Grit, Lesser Calcareous Arenite, Pelite and Minor Conglomerate medium to thick layering								
627.7-629.8	strongly dolomitized and moderately sericitized								
629.8-631.5	strongly dolomitized, moderately chloritized and weakly sericitized								
631.5-642.3	strongly dolomitized and moderately sericitized								
633.0-648.0	quartz stringers								
641.2-642.1	fault								
642.3-647.0	strongly dolomitized								
647.0-660.0	chloritized and moderately dolomitized								
648.0-660.0	calcite stringers								
660.0-679.0	Calcareous Arenite, Lesser Calcareous Grit and Pelite medium to thin layering								
660.0-675.4	strongly dolomitized and moderately sericitized								
660.0-664.4	quartz stringers								

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From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
788.2-800.0	Calcareous Grit, Lesser Calcareous Arenite, Graphitic Pelite and Minor Conglomerate very thin to thin layering								
800.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-15

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: August 29, 2001
 Date Completed: September 7, 2001
 Final Depth: **637 feet (194.2 m)**

Collar Grid Coordinates
 Northing Easting Elevation
 Mine Grid 2869.0 ft. 18341.0 ft. 4973.0 ft.

Logged by: **D. Hladky**

Depth	Azimuth	Dip
collar	224°	-41°
60.0 ft.	226°	-43°
300.0 ft.	229°	-40°
630.0 ft.	231°	-37°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-14.0	Overburden								
14.0-14.5	Calcareous Arenite and Pelite								
	very thin to thin layering								
14.0-50.4	silicified, moderately sericitized and weakly dolomitized								
		14.0-54.6	0.8						
14.5-54.6	Dolomite Porphyroblastic Pelite and Arenite								
	very thin to thin layering								
			120001	sludge	20.0	30.0	0.01		
30.0-31.1	quartz vein								
			120002	sludge	30.0	40.0	0.08		
35.9-36.4	quartz stringers								
38.7-41.4	quartz stringers								
			120003	sludge	40.0	50.0	0.26		
43.0-43.7	quartz stringers								
48.2-48.4	quartz vein								
48.4-49.1	quartz stringers								
			120004	sludge	50.0	60.0	0.50		
50.1-50.4	quartz stringers								
50.4-54.6	strongly sericitized, moderately chloritized, weakly silicified and dolomitized								
51.4-52.6	quartz stringers								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
54.6-86.3	Magnetite-bearing, Dolomite Porphyroblastic Pelite and Arenite very thin to thin layering								
54.6-120.5	strongly sericitized, moderately silicified, weakly dolomitized and chloritized								
		54.6-86.3	2.0						
57.6-62.2	quartz stringers		120005	sludge	60.0	70.0	0.43		
63.4-63.7	quartz stringers								
66.1-66.6	quartz stringers								
68.2-68.8	quartz stringers		120006	sludge	70.0	80.0	0.56		
71.2-72.2	quartz stringers								
75.7-76.5	quartz stringers		120007	sludge	80.0	90.0	0.36		
80.4-80.8	quartz stringers								
81.2-103.2	quartz stringers								
82.6-82.8	fault								
86.3-207.3	Dolomite Porphyroblastic Arenite, Pelite and Lesser Grit very thin to thin layering								
86.3-86.4	fault								
		86.3-142.8	0.8						
88.8-89.0	fault								
89.6-90.3	fault		120008	sludge	90.0	100.0	0.65		
91.0-91.4	fault								
91.6-93.7	fault		120009	sludge	100.0	110.0	0.21		
103.0-103.7	Fault Zone								
105.9-106.2	Fault Zone								
106.2-106.8	quartz vein								
106.8-108.7	quartz stringers								
108.0-108.7	Fault Zone		120010	sludge	110.0	120.0	0.24		
111.5-112.0	quartz vein								
112.5-116.6	quartz stringers								
112.5-112.9	fault								
116.6-117.7	quartz vein								
118.5-118.8	quartz stringers								
120.0-120.5	fault								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
120.5-142.8	silicified, moderately sericitized and weakly dolomitized quartz vein		120011	sludge	120.0	130.0	0.60		
122.8-123.1									
			120012	sludge	130.0	140.0	0.32		
135.0-137.2	quartz vein								
137.2-142.8	quartz stringers		120013	sludge	140.0	150.0	1.91		
142.8-177.3	carbonized and moderately sericitized quartz vein								
142.8-145.5									
		142.8-146.0	2.0						
			6416	core	142.8	147.9	1.33	0.039	5.1
145.5-147.9	quartz stringers								
146.0-147.9	fault								
		146.0-147.9	3.5						
147.9-155.2	quartz vein								
		147.9-150.6	3.5						
			6417	core	147.9	150.6	0.69	0.020	2.7
			120014	sludge	150.0	160.0	15.77		
		150.6-160.4	7.5						
			6418	core	150.6	155.5	12.62	0.368	4.9
155.2-158.7	quartz stringers								
			6419	core	155.5	160.4	3.93	0.115	4.9
				core	150.6	160.4	8.28	0.241	9.8
158.7-160.4	quartz vein								
			120015	sludge	160.0	170.0	2.92		
160.4-161.5	quartz stringers								
		160.4-170.0	2.5						
			6420	core	160.4	165.7	0.24	0.007	5.3
161.5-161.7	quartz vein								
161.7-161.9	quartz stringers								
161.9-162.3	quartz vein								
162.3-164.5	quartz stringers								
164.5-164.8	quartz vein								
164.8-170.0	quartz stringers								
			6421	core	165.7	170.0	0.22	0.006	4.3
170.0-176.0	quartz vein								
		170.0-174.7	5.5						
			6422	core	170.0	173.7	7.29	0.213	3.7

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
202.6-202.8	quartz vein		6485	core	201.0	207.5	0.02	0.001	6.5
		202.6-202.8	6.5						
		202.8-207.3	1.5						
205.0-205.3	fault								
205.6-205.7	fault								
207.3-227.7	Mariposite-bearing Grit, Arenite and Lesser Pelite								
	thin layering								
207.3-227.7	strongly sericitized, moderately dolomitized and weakly silicified								
		207.3-227.8	0.6						
207.6-208.0	quartz vein								
210.0-218.6	quartz stringers								
			120020	sludge	210.0	220.0	0.44		
217.0-218.6	fault								
218.6-219.2	quartz vein								
219.2-225.8	quartz stringers								
			120021	sludge	220.0	230.0	0.39		
225.8-226.0	quartz vein								
227.7-241.4	Graphitic Pelite and Arenite								
	very thin to thin layering								
227.8-228.1	quartz vein								
		227.8-228.0	6.0						
		228.0-241.4	0.8						
228.1-241.9	quartz stringers								
			120022	sludge	230.0	240.0	0.32		
238.3-238.6	fault								
			120023	sludge	240.0	250.0	0.59		
241.4-292.0	Conglomerate, Grit, Arenite and Minor Graphitic Pelite								
	thin to medium layering								
241.4-244.8	silicified, moderately dolomitized and weakly sericitized								
		241.4-251.2	1.5						
244.8-255.2	strongly sericitized, moderately dolomitized, weakly chloritized and silicified								
			120024	sludge	250.0	260.0	0.15		
		251.2-271.3	0.8						
255.2-258.8	chloritized, moderately dolomitized and weakly sericitized								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
367.5-368.4	moderately dolomitized								
368.4-373.2	silicified, moderately chloritized, weakly dolomitized and sericitized								
			120036	sludge	370.0	380.0	0.09		
373.2-374.2	Mariposite-bearing Conglomerate, Grit and Graphitic Pelite								
	thin to medium layering								
373.2-374.1	moderately dolomitized								
374.2-418.2	Grit, Arenite and Lesser Graphitic Pelite								
	thin to medium layering								
374.1-374.2	strongly sericitized, moderately silicified and weakly dolomitized								
374.2-374.7	silicified, moderately dolomitized and weakly sericitized								
		374.3-403.7	0.8						
374.7-375.5	strongly sericitized and moderately dolomitized								
375.5-379.1	silicified and moderately dolomitized								
379.1-386.6	strongly dolomitized, moderately sericitized and weakly chloritized								
			120037	sludge	380.0	390.0	0.27		
386.6-387.9	chloritized, moderately dolomitized and weakly sericitized								
387.9-408.2	strongly dolomitized and moderately sericitized								
			120038	sludge	390.0	400.0	0.17		
390.2-390.8	quartz vein								
			120039	sludge	400.0	410.0	0.21		
403.7-403.9	quartz stringers								
		403.7-408.2	1.2						
408.2-412.2	strongly dolomitized, moderately sericitized and weakly chloritized								
		408.2-418.2	0.8						
			120040	sludge	410.0	420.0	0.05		
412.2-418.2	strongly dolomitized and moderately sericitized								
417.9-419.0	fault								
418.2-465.1	Graphitic Arenite and Pelite								
	very thin to thin layering								
418.2-422.0	carbonized								
418.2-431.0	quartz stringers								
		418.2-430.3	0.5						
419.6-419.7	fault								
419.8-420.0	fault								
			120041	sludge	420.0	430.0	0.05		

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
421.3-421.5	fault								
421.9-422.1	fault								
422.6-422.8	fault								
426.9-427.1	fault								
427.6-430.0	silicified and moderately sericitized								
427.6-427.8	fault								
428.6-430.3	fault								
			120042	sludge	430.0	440.0	0.13		
		2.5							
431.3-431.5	fault								
432.6-433.4	fault								
437.7-438.5	fault								
438.8-439.1	fault								
440.0-440.3	fault								
440.3-444.7	silicified and moderately sericitized								
441.0-446.0	quartz stringers								
444.1-444.2	fault								
444.7-446.2	carbonized								
444.7-445.2	fault								
		0.5							
445.4-446.2	fault								
446.2-452.9	moderately dolomitized								
446.7-447.2	fault								
447.5-447.6	fault								
452.4-452.6	quartz stringers								
452.4-452.6	fault								
452.9-454.2	carbonized								
454.2-461.0	moderately dolomitized								
456.9-457.3	quartz vein								
457.3-459.2	fault								
459.5-461.3	fault								
461.0-462.2	silicified and moderately sericitized								
461.3-461.7	quartz vein								
461.7-462.0	fault								
462.5-463.1	fault								
463.8-464.1	fault								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
465.1-480.2	Arenite and Grit and Graphitic Pelite								
	thin to very thin layering								
465.1-480.2	silicified and moderately sericitized								
465.6-466.3	fault								
466.8-470.5	fault								
					470.5-473.4	1.0			
473.4-473.8	quartz vein								
					473.4-587.2	1.1			
475.9-476.2	fault								
478.3-478.4	fault								
480.2-542.5	Arenite, Grit and Lesser Graphitic Pelite								
	thin to very thin layering								
480.2-502.5	strongly sericitized and moderately silicified								
481.4-481.5	fault								
484.3-484.7	fault								
490.0-500.0	quartz stringers								
502.5-516.0	silicified, moderately sericitized and weakly dolomitized								
516.0-542.5	strongly sericitized, moderately silicified and weakly dolomitized								
542.5-629.7	Grit, Arenite and Graphitic Pelite								
	medium to thin layering								
542.5-577.5	silicified, moderately dolomitized and weakly sericitized								
542.5-544.0	quartz stringers								
542.6-542.7	fault								
557.0-558.0	quartz stringers								
577.5-587.2	strongly dolomitized, moderately silicified and weakly sericitized								
578.5-579.0	quartz stringers								
578.5-578.7	fault								
578.9-579.0	fault								
581.4-581.7	fault								
586.5-586.8	fault								
587.2-596.9	strongly dolomitized, moderately sericitized and weakly silicified				587.2-596.9	1.5			
596.9-630.0	silicified, moderately dolomitized and weakly sericitized								
					596.9-630.0	0.5			
606.3-606.9	fault								
613.7-613.8	fault								

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From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
627.2-627.4	fault								
629.7-630.0	Grit, Arenite and Graphitic Pelite thin layering								
630.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-16

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: September 5, 2001
 Date Completed: September 5, 2001
 Final Depth: **463 feet (141.1 m)**

Collar Grid Coordinates
 Northing Easting Elevation
 Mine Grid 2893.0 ft. 21295.0 ft. 4787.0 ft.

Logged by: D. Hladky

Depth	Azimuth	Dip
collar	223°	-45°
66.0 ft.	230°	-44°
226.0 ft.	231°	-46°
446.0 ft.	231°	-49°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-10.0	Overburden								
10.0-50.7	Magnetite-bearing Pelite and Arenite thin to very thin layering								
10.0-48.3	strongly sericitized, moderately silicified and weakly dolomitized								
		10.0-59.3	1.1						
			120063	sludge	26.0	36.0	0.11		
			120064	sludge	46.0	56.0	0.04		
48.3-50.8	strongly sericitized, moderately silicified, weakly dolomitized and chloritized								
50.7-70.8	Dolomite Porphyroblastic Pelite and Arenite thin to very thin layering								
50.8-70.8	strongly sericitized, moderately silicified and weakly dolomitized								
54.9-55.0	fault								
			120065	sludge	56.0	66.0	0.05		
		59.3-65.0	1.6						
		65.0-70.8	0.8						
			120066	sludge	66.0	76.0	0.19		
70.8-101.8	Graphitic Pelite and Arenite very thin to thin layering								
70.8-73.5	quartz stringers								
		70.8-107.1	1.5						
			4516	core	70.8	76.0	0.10	0.003	5.2

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
73.5-74.3	quartz vein								
74.3-78.1	quartz stringers								
75.7-77.0	Fault Zone								
			4517	core	76.0	78.5	0.03	0.001	2.5
			120067	sludge	76.0	86.0	5.71		
78.1-78.5	quartz vein								
78.5-107.1	quartz stringers								
			4518	core	78.5	86.0	0.09	0.003	7.5
			4519	core	86.0	92.6	0.17	0.005	6.6
			120068	sludge	86.0	96.0	1.06		
86.4-104.1	carbonized								
86.4-97.1	Fault Zone								
			4520	core	92.6	96.0	0.15	0.004	3.4
			4521	core	96.0	100.0	0.05	0.001	4.0
			120069	sludge	96.0	106.0	0.82		
			4522	core	100.0	107.1	0.02	0.001	7.1
101.8-104.1	Graphitic Conglomerate, Pelite and Arenite thick layering								
104.1-145.2	Arenite, Graphitic Pelite and Grit very thin to thin layering								
106.0-107.1	fault								
			120070	sludge	106.0	116.0	0.31		
107.1-115.6	strongly sericitized and moderately dolomitized								
107.1-116.8	quartz stringers								
107.1-114.9		0.8							
109.6-109.9	fault								
111.9-112.1	fault								
114.9-115.6		2.0							
115.6-116.0	chloritized, moderately sericitized and weakly dolomitized								
115.6-123.5		0.8							
116.0-119.3	strongly sericitized and moderately dolomitized								
			120071	sludge	116.0	126.0	0.32		
119.0-129.0	quartz stringers								
119.3-120.0	chloritized, moderately sericitized and weakly dolomitized								
120.0-124.3	strongly sericitized and moderately dolomitized								
123.5-125.1		2.5							

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
124.3-125.1	chloritized, moderately sericitized and weakly dolomitized								
125.1-145.2	strongly sericitized and moderately dolomitized								
		125.1-156.0	0.8						
			120072	sludge	126.0	136.0	0.14		
134.6-149.1	quartz stringers								
			120073	sludge	136.0	146.0	0.17		
145.2-160.9	Arenite, Grit and Lesser Graphitic Pelite thin to medium layering								
145.2-155.9	strongly sericitized, moderately dolomitized and weakly silicified								
			120074	sludge	146.0	156.0	0.13		
149.1-149.5	quartz vein								
149.5-161.5	quartz stringers								
154.7-155.1	fault								
155.9-175.4	strongly sericitized and moderately dolomitized								
		156.0-158.0	3.2						
			120075	sludge	156.0	166.0	0.20		
		158.0-162.8	2.0						
160.9-348.5	Graphitic Arenite, Pelite and Grit very thin to thin layering								
160.9-161.3	fault								
162.5-162.8	fault								
		162.8-173.8	1.0						
			120076	sludge	166.0	176.0	0.15		
168.1-171.0	quartz stringers								
170.2-170.3	fault								
		173.8-198.4	0.5						
175.0-177.5	quartz stringers								
175.4-177.2	chloritized, moderately sericitized and weakly dolomitized								
			120077	sludge	176.0	186.0	0.07		
177.2-232.2	strongly sericitized, moderately dolomitized and weakly silicified								
			120078	sludge	186.0	196.0	0.10		
187.1-192.4	quartz stringers								
			6457	core	194.4	200.3	3.07	0.090	5.9
			120079	sludge	196.0	206.0	1.13		
197.2-198.4	quartz vein								
		198.4-199.0	7.2						

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From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
199.0-200.3		1.5							
200.3-204.3		2.0							
			6458	core	200.3	202.0	0.02	0.001	1.7
			6459	core	202.0	204.3	0.01	<0.001	2.3
			6468	LG Standard			1.81	0.053	
204.3-206.3	quartz vein								
		4.2							
204.3-206.8			120080	sludge	206.0	216.0	0.07		
206.8-207.6	quartz stringers								
		3.7							
206.8-218.2									
207.6-208.4	quartz vein								
208.4-211.2	quartz stringers								
211.2-212.2	quartz vein								
212.2-215.6	quartz stringers								
215.6-216.3	quartz vein								
			120081	sludge	216.0	226.0	0.18		
216.3-217.0	quartz stringers								
217.0-218.2	quartz vein								
218.2-222.8	quartz stringers								
		1.5							
218.2-223.2									
222.8-223.1	quartz vein								
223.1-232.4	quartz stringers								
		8.2							
223.2-223.4									
223.4-227.8		1.7							
			120082	sludge	226.0	236.0	0.12		
227.8-232.4		2.5							
232.2-290.7	silicified								
232.4-242.4	quartz vein								
		2.0							
232.4-242.4			120107	sludge	236.0	246.0	0.27		
242.4-246.0	quartz stringers								
		2.7							
242.4-283.7									
243.5-243.6	fault								
			120108	sludge	246.0	256.0	0.06		
			120109	sludge	256.0	266.0	0.17		
			120110	sludge	266.0	276.0	0.27		
			120111	sludge	276.0	286.0	0.15		
283.7-285.5		7.5							

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From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
285.5-288.5		1.0							
			120112	sludge	286.0	296.0	0.14		
288.5-316.7	quartz stringers								
		6.5							
290.3-290.7	fault								
290.7-296.6	silicified and moderately sericitized								
		1.7							
			120113	sludge	296.0	306.0	0.10		
			120114	sludge	306.0	316.0	0.06		
307.5-319.0	silicified, moderately sericitized and weakly dolomitized								
			120115	sludge	316.0	326.0	0.12		
316.7-319.0		3.0							
319.0-323.0	silicified and moderately sericitized								
		4.5							
322.4-322.6	fault								
323.0-348.5	moderately dolomitized								
		2.0							
			120116	sludge	326.0	336.0	0.06		
330.1-331.2		4.5							
331.2-334.6		2.0							
334.6-336.0		4.5							
336.0-338.6		0.8							
			120117	sludge	336.0	346.0	0.04		
337.5-342.0	quartz stringers								
		4.5							
338.6-341.8		0.5							
341.8-347.5			120118	sludge	346.0	356.0	0.08		
347.5-348.5	quartz stringers								
		5.5							
		1.0							
348.5-368.7	Arenite, Grit and Pelite								
348.3-348.5	fault								
	thin to medium layering								
348.5-366.3	silicified								
348.5-348.7	quartz vein								
		2.2							
348.7-358.0			120119	sludge	356.0	366.0	0.25		

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From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
358.0-361.5		5.0							
361.5-366.3		2.2							
			120120	sludge	366.0	376.0	0.06		
366.3-407.6		1.2							
368.7-402.4	Grit, Arenite and Pelite thin to medium layering								
			120121	sludge	376.0	386.0	0.07		
			120122	sludge	386.0	396.0	0.33		
			120123	sludge	396.0	406.0	0.40		
402.4-423.0	Graphitic Arenite, Pelite and Grit very thin to thin layering								
402.4-405.7	moderately sericitized								
			120124	sludge	406.0	416.0	0.12		
407.5-412.6	quartz stringers								
407.6-412.6		3.5							
412.4-412.6	fault								
412.6-416.6	moderately dolomitized								
412.6-422.6		7.0							
			120125	sludge	416.0	426.0	0.59		
416.6-422.6	strongly sericitized and moderately dolomitized								
			6497	core	416.6	418.8	0.01	<0.001	2.2
			6498	core	418.8	422.6	0.01	<0.001	3.8
422.6-426.3	silicified, moderately dolomitized and weakly sericitized								
422.6-426.3		1.5							
423.0-426.3	Graphitic Arenite, Pelite and Grit thin to medium layering								
			120126	sludge	426.0	436.0	0.10		
426.3-444.0	Graphitic Arenite, Grit and Pelite thin to very thin layering								
426.3-437.0		1.5							
			120127	sludge	436.0	446.0	0.04		
437.0-463.0		0.8							
438.0-444.0	silicified								

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From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
444.0-463.0	Graphitic Arenite, Pelite and Grit very thin to thin layering								
			120128	sludge	446.0	456.0	0.10		
			120129	sludge	456.0	466.0	0.03		
458.1-463.0	silicified and moderately sericitized								
463.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-17

Property: **Bonanza**
 Drilling Contractor: **Standard Drilling & Engineering Ltd.**
 Date Started: **September 10, 2001**
 Date Completed: **September 13, 2001**
Final Depth: 250 feet (76.2 m)

Collar Grid Coordinates
Northing Easting Elevation
 Mine Grid **2872.0 ft. 18341.0 ft. 4973.0 ft.**

Logged by: D. Hladky

Depth	Azimuth	Dip
collar	224°	-60°
100.0 ft.	229°	-60°
250.0 ft.	227°	-59°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-12.0	Overburden								
12.0-20.1	Graphitic, Calcareous Arenite and Pelite very thin to thin layering								
12.0-22.0	chloritized and moderately dolomitized								
		0.8							
			120083	sludge	12.0	20.0	0.02		
20.1-64.5	Dolomite Porphyroblastic Pelite and Arenite thin to medium layering								
			120084	sludge	20.0	30.0	0.21		
20.1-64.5	silicified, moderately sericitized and weakly dolomitized								
28.0-28.6	quartz vein								
			120085	sludge	30.0	40.0	0.03		
34.2-34.7	quartz vein								
34.8-35.0	fault								
35.8-38.0	quartz stringers								
			120086	sludge	40.0	50.0	0.58		
		2.0							
47.6-48.1	quartz vein								
		0.8							
49.6-51.1	quartz stringers								
			120087	sludge	50.0	60.0	0.18		
51.9-52.4	quartz vein								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
64.5-85.5	Magnetite-bearing, Dolomite Porphyroblastic Pelite medium to thin layering		120088	sludge	60.0	70.0	<0.01		
64.5-70.9	strongly sericitized, moderately silicified and weakly dolomitized	2.5							
69.1-95.0	quartz stringers		120089	sludge	70.0	80.0	<0.01		
70.9-84.2	chloritized, moderately sericitized and weakly silicified		120090	sludge	80.0	90.0	0.01		
84.2-85.5	strongly sericitized and moderately chloritized								
85.5-101.8	Pelite medium to thin layering								
85.5-95.7		0.8							
95.0-95.7	fault		120091	sludge	90.0	100.0	0.17		
95.7-97.0	chloritized and moderately sericitized								
97.0-98.0	strongly sericitized and moderately chloritized								
98.0-102.8	chloritized and moderately sericitized								
98.0-98.4	fault		120092	sludge	100.0	110.0	0.10		
101.8-128.3	Magnetite-bearing, Dolomite Porphyroblastic Pelite and Grit thin to very thin layering								
102.6-102.8	fault	1.0							
102.8-113.9	chloritized, moderately sericitized and weakly dolomitized								
102.8-113.9	quartz stringers		120093	sludge	110.0	120.0	0.20		
110.6-111.4		2.5							
111.4-129.3		2.5							
112.7-112.8	fault								
113.9-162.0	strongly sericitized, moderately silicified and weakly dolomitized								
114.9-115.5	Fault Zone		120094	sludge	120.0	130.0	1.21		
121.8-122.7	fault								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
122.7-130.6	quartz stringers								
128.3-161.9	Dolomite Porphyroblastic Pelite and Arenite thin to very thin layering								
		0.8							
			120095	sludge	130.0	140.0	1.04		
130.6-131.3	quartz vein								
131.3-140.0	quartz stringers								
		1.5							
			6440	core	131.3	133.0	0.91	0.027	1.7
		20.0							
		3.0							
			6441	core	133.0	137.0	0.90	0.026	4.0
133.2-133.6	fault								
				core	131.3	137.0	0.90	0.026	5.7
			6442	core	137.0	140.0	0.22	0.006	3.0
			6443	core	140.0	142.6	0.43	0.013	2.6
			120096	sludge	140.0	150.0	1.72		
		0.8							
			120097	sludge	150.0	160.0	1.35		
160.0-160.3	fault								
			120098	sludge	160.0	170.0	0.74		
161.9-170.5	Pelite and Arenite thin to very thin layering								
162.0-171.5	carbonized								
		1.0							
			6444	core	162.0	163.1	<0.01	<0.001	1.1
163.1-168.7	quartz stringers								
163.1-168.7	fault								
		2.0							
			6445	core	163.1	168.7	1.80	0.053	5.6
168.7-170.5	quartz vein								
		0.8							
			6446	core	168.7	170.5	2.24	0.065	1.8
			120099	sludge	170.0	180.0	2.69		

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
170.5-250.0	Dolomite Porphyroblastic Pelite and Arenite								
	thin to very thin layering			core	163.1	170.5	1.91	0.056	7.4
170.5-174.0	quartz stringers								
		2.5							
			6447	core	170.5	174.0	0.92	0.027	3.5
171.5-174.0	silicified								
173.2-174.4	fault								
174.0-235.9	strongly sericitized, moderately silicified and weakly dolomitized								
174.0-184.0	quartz stringers								
		1.5							
			6448	core	174.0	178.7	0.18	0.005	4.7
178.7-178.9	fault								
		1.0							
			120100	sludge	180.0	190.0	1.06		
181.5-181.9	Fault Zone								
184.6-186.5	Fault Zone								
		2.0							
			6449	core	187.5	189.2	1.39	0.041	1.7
		1.2							
			120101	sludge	190.0	200.0	0.49		
191.7-192.4	fault								
194.2-194.5	fault								
			120102	sludge	200.0	210.0	0.50		
204.5-213.5	quartz stringers								
208.0-209.3	Fault Zone								
			120103	sludge	210.0	220.0	0.68		
210.6-211.5	Fault Zone								
213.5-213.9	quartz vein								
		2.5							
			6450	core	213.5	215.4	0.35	0.010	1.9
215.1-215.4	quartz vein								
215.4-217.6	quartz stringers								
			6451	core	215.4	217.6	0.27	0.008	2.2
			6452	LG Standard			1.87	0.055	
217.6-218.1	quartz vein								
		0.8							
218.1-219.3	quartz stringers								
218.2-218.8	Fault Zone								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
219.3-219.6	quartz vein								
219.6-228.5	quartz stringers								
			120104	sludge	220.0	230.0	0.51		
		2.5							
			6453	core	221.0	223.2	0.36	0.011	2.2
221.7-222.1	Fault Zone								
223.2-225.0	Fault Zone								
			6454	core	223.2	226.9	0.14	0.004	3.7
226.9-227.0	fault								
		15.0							
		1.0							
227.7-227.9	fault								
229.1-229.8	Fault Zone								
			120105	sludge	230.0	240.0	0.36		
230.1-230.3	fault								
231.9-232.3	fault								
233.2-233.4	fault								
235.9-238.1	strongly sericitized, moderately dolomitized and weakly silicified								
238.1-241.5	strongly dolomitized and moderately sericitized								
			120106	sludge	240.0	250.0	0.38		
240.2-245.3	quartz stringers								
240.9-241.1	fault								
241.5-243.2	chloritized and moderately dolomitized								
242.8-243.2	fault								
243.2-244.1	strongly sericitized and moderately dolomitized								
244.1-250.0	strongly dolomitized, moderately sericitized and weakly silicified								
		5.0							
			6455	core	244.1	245.3	0.01	<0.001	1.2
		2.5							
245.3-249.4	quartz vein								
		3.0							
			6456	core	245.3	249.4	0.01	<0.001	4.1
		2.5							
250.0	E.O.H.								

D.D.H. BC01-18

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International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-18

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: September 13, 2001
 Date Completed: September 27, 2001
 Final Depth: **800 feet (243.8 m)**

Collar Grid Coordinates
 Northing Easting Elevation
 Mine Grid **2874.0 ft. 18341.0 ft. 4973.0 ft.**

Logged by: **D. Hladky**

Depth	Azimuth	Dip
collar	224°	-80°
36.0 ft.	207°	-80°
63.0 ft.	207°	-80°
413.0 ft.	193°	-77°
797.0 ft.	201°	-73°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-10.0	Overburden								
10.0-21.6	Calcareous Arenite and Pelite very thin to thin layering								
		10.0-41.9	0.8						
			120130	sludge	10.0	20.0	<0.01		
			120131	sludge	20.0	30.0	<0.01		
21.6-23.4	Calcareous Arenite thick layering								
23.4-25.1	Calcareous Arenite and Pelite very thin to thin layering								
25.1-101.4	Dolomite Porphyroblastic Pelite and Arenite thin to medium layering								
25.1-124.0	silicified, moderately dolomitized and weakly sericitized								
			120132	sludge	30.0	40.0	<0.01		
			120133	sludge	40.0	50.0	0.08		
41.9-43.1	quartz vein								
		41.9-44.9	1.2						
43.9-44.9	quartz stringers								
		44.9-51.0	0.8						
			120134	sludge	50.0	60.0	<0.01		

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
51.0-51.8		2.0							
51.4-51.8	quartz vein								
51.8-56.1		1.0							
55.3-56.1	quartz stringers								
56.1-69.6		0.8							
61.9-62.3	fault		120135	sludge	60.0	70.0	1.40		
64.8-80.6	quartz stringers								
69.6-70.8		8.0							
			6499	core	69.6	70.8	10.43	0.304	1.2
			120136	sludge	70.0	80.0	0.60		
70.8-80.6		1.0							
			120137	sludge	80.0	90.0	0.35		
80.6-81.5	quartz vein								
80.6-81.5		3.0							
81.5-82.2	quartz stringers								
81.5-82.2		2.0							
82.2-83.0	quartz vein								
82.2-83.0		1.0							
83.0-88.5	quartz stringers								
83.0-88.5		0.8							
88.5-89.2	quartz vein								
88.5-89.2		4.5							
89.2-96.7	quartz stringers								
89.2-95.5	Fault Zone								
89.2-95.9		1.0							
			120138	sludge	90.0	100.0	0.37		
95.9-96.2		15.0							
96.2-101.4		1.0							
96.7-97.0	quartz vein								
97.0-99.2	quartz stringers								
99.2-99.6	quartz vein								
99.2-99.4	fault								
99.6-121.0	quartz stringers								
			120139	sludge	100.0	110.0	0.12		
101.4-108.4	Magnetite-bearing, Dolomite Porphyroblastic Pelite and Arenite thin to medium layering								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
101.4-108.4		1.5							
108.4-124.0	Dolomite Porphyroblastic Pelite and Arenite thin to medium layering								
		0.8							
			120140	sludge	110.0	120.0	0.27		
		1.5							
		0.8							
			120141	sludge	120.0	130.0	0.23		
124.0-138.5	Magnetite-bearing, Dolomite Porphyroblastic Pelite and Arenite thin to medium layering								
124.0-150.3	strongly sericitized, moderately silicified and weakly dolomitized								
		2.5							
127.0-157.0	quartz stringers								
127.1-127.4	Fault Zone								
			120142	sludge	130.0	140.0	0.92		
138.5-140.0	Dolomite Porphyroblastic Pelite and Arenite thin to medium layering								
		0.8							
140.0-174.6	Magnetite-bearing, Dolomite Porphyroblastic Pelite, Arenite and Grit								
139.8-140.6	fault								
	thin to medium layering								
		1.5							
			120143	sludge	140.0	150.0	0.11		
			120144	sludge	150.0	160.0	0.09		
150.3-165.9	chloritized, moderately sericitized and weakly dolomitized								
157.0-157.8	quartz vein								
			120145	sludge	160.0	170.0	0.05		
160.4-165.9	quartz stringers								
165.9-208.8	strongly sericitized, moderately silicified and weakly dolomitized								
165.9-171.0	quartz stringers								
			120146	sludge	170.0	180.0	0.75		
171.8-174.6		2.5							

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
			4501	core	222.8	228.1	0.76	0.022	5.3
			4502	core	228.1	231.7	1.23	0.036	3.6
			120152	sludge	230.0	240.0	1.26		
			4503	core	231.7	234.4	1.24	0.036	2.7
233.5-234.1	quartz vein								
234.1-234.4	quartz stringers								
234.1-234.4	fault								
				core	228.1	234.4	1.23	0.036	6.3
234.4-238.2	quartz vein								
		234.4-236.0	3.5						
			4504	core	234.4	236.0	0.13	0.004	1.6
		236.0-238.2	0.8						
			4505	core	236.0	238.2	0.65	0.019	2.2
238.2-239.7	quartz stringers								
		238.2-244.2	3.5						
			4506	core	238.2	242.5	3.93	0.115	4.3
239.7-240.0	quartz vein								
240.0-242.6	quartz stringers								
240.0-242.6	Fault Zone								
			120153	sludge	240.0	250.0	5.22		
			4507	core	242.5	244.7	3.33	0.097	2.2
242.6-246.0	quartz vein								
243.0-243.2	fault								
244.2-244.7	fault								
		244.2-244.7	80.0						
				core	238.2	244.7	3.73	0.109	6.5
		244.7-248.1	5.5						
			4508	core	244.7	246.8	0.75	0.022	2.1
			4509	HG Standard			6.83	0.199	
246.0-248.1	quartz stringers								
246.0-248.1	Fault Zone								
			4510	core	246.8	248.1	38.90	1.135	1.3
248.1-250.0	quartz vein								
		248.1-249.1	75.0						
			4511	core	248.1	250.0	13.38	0.390	1.9
		249.1-250.0	1.8						
250.0-250.7	quartz stringers								
		250.0-253.7	20.0						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
250.7-252.0	quartz vein		4512	core	250.0	250.7	4.80	0.140	0.7
			120154	sludge	250.0	260.0	4.10		
			4513	core	250.7	253.7	2.52	0.074	3.0
252.0-261.0	silicified, moderately sericitized and weakly dolomitized								
252.0-252.6	quartz stringers								
252.6-253.7	quartz vein								
253.7-263.2	Dolomite Porphyroblastic Conglomerate and Pelite								
	very thin to thin layering								
				core	246.8	253.7	12.60	0.367	6.9
				core	238.2	253.7	7.27	0.212	15.5
253.7-258.8	quartz stringers								
		253.7-257.7	3.0						
			4514	core	253.7	257.7	0.64	0.019	4.0
		257.7-263.2	1.5						
			4515	core	257.7	261.0	0.47	0.014	3.3
258.8-260.1	quartz vein								
			120155	sludge	260.0	270.0	1.24		
260.4-263.2	quartz stringers								
261.0-263.2	carbonized								
263.2-284.9	Dolomite Porphyroblastic Arenite, Pelite and Grit								
	very thin to thin layering								
263.2-271.3	strongly sericitized, moderately silicified and weakly dolomitized								
263.2-269.3	quartz stringers								
		263.2-271.3	0.8						
269.3-269.6	quartz vein								
269.6-284.9	quartz stringers								
			120156	sludge	270.0	280.0	0.62		
271.3-284.9	silicified and moderately dolomitized								
		271.3-284.9	2.0						
279.4-280.8	Fault Zone								
			120157	sludge	280.0	290.0	0.21		
284.9-291.1	Dolomite Porphyroblastic Pelite and Arenite								
	very thin to thin layering								
284.9-291.1	carbonized								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
284.9-291.1	quartz stringers								
		284.9-291.1	1.5						
285.7-286.8	Fault Zone								
287.3-287.6	fault								
			120158	sludge	290.0	300.0	0.30		
291.1-303.3	Graphitic Pelite and Arenite								
	very thin to thin layering								
291.1-295.0	silicified and moderately dolomitized								
		291.1-293.8	0.8						
293.4-295.5	fault								
		293.8-303.3	1.5						
295.0-303.3	carbonized								
295.0-298.3	quartz stringers								
295.8-296.3	fault								
298.3-298.8	quartz vein								
298.8-304.0	quartz stringers								
			120159	sludge	300.0	310.0	0.82		
303.3-303.7	Dolomite Porphyroblastic Pelite and Conglomerate								
	very thin to thin layering								
303.3-303.7	silicified and moderately dolomitized								
		303.3-303.7	1.0						
303.7-306.3	Graphitic Pelite, Conglomerate and Grit								
	very thin to thin layering								
303.7-306.3	carbonized								
		303.7-306.3	1.5						
304.0-304.4	quartz vein								
304.4-305.5	quartz stringers								
305.5-305.7	quartz vein								
305.7-306.3	quartz stringers								
306.3-346.8	Arenite, Grit and Pelite								
	thin to very thin layering								
306.3-319.0	strongly sericitized, moderately dolomitized and weakly silicified								
306.3-309.0	quartz stringers								
		306.3-323.0	0.8						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
309.0-309.4	quartz vein								
309.4-321.8	quartz stringers								
			120160	sludge	310.0	320.0	0.26		
319.0-337.3	strongly dolomitized and moderately sericitized								
			120161	sludge	320.0	330.0	0.19		
321.8-322.8	quartz vein								
322.8-326.1	quartz stringers								
		323.0-323.1	2.0						
		323.1-332.9	0.8						
326.1-326.5	quartz vein								
326.5-343.0	quartz stringers								
			120162	sludge	330.0	340.0	0.68		
		332.9-333.3	1.0						
		333.3-340.4	0.8						
337.3-346.8	strongly sericitized and moderately dolomitized								
			120163	sludge	340.0	350.0	0.64		
		340.4-341.6	2.0						
		341.6-344.8	0.8						
343.0-343.1	quartz vein								
343.1-344.8	quartz stringers								
		344.8-346.8	2.5						
346.8-405.3	Graphitic Pelite and Arenite								
	very thin to thin layering								
346.8-347.8	silicified and moderately dolomitized								
		346.8-361.4	1.2						
347.8-348.1	quartz stringers								
348.1-348.2	quartz vein								
348.2-357.9	quartz stringers								
			120164	sludge	350.0	360.0	0.91		
357.9-358.2	quartz vein								
358.2-361.4	quartz stringers								
			4570	core	359.6	365.8	0.05	0.001	6.2
			120165	sludge	360.0	370.0	0.54		
361.4-361.7	quartz vein								
		361.4-364.3	7.5						
361.7-362.9	quartz stringers								
362.9-364.3	quartz vein								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
364.3-364.7	quartz stringers								
		364.3-370.2	1.0						
364.7-365.8	quartz vein								
365.8-370.2	quartz stringers								
			4571	core	365.8	370.1	0.38	0.011	4.3
			120166	sludge	370.0	380.0	0.72		
			4572	core	370.1	373.3	0.61	0.018	3.2
370.2-371.7	quartz vein								
		370.2-371.9	3.0						
371.7-372.3	quartz stringers								
		371.9-379.3	1.0						
372.3-373.3	quartz vein								
373.3-375.5	quartz stringers								
			4573	core	373.3	377.4	0.19	0.006	4.1
375.5-376.6	quartz vein								
376.6-381.3	quartz stringers								
			4574	core	377.4	381.3	0.05	0.001	3.9
		379.3-380.3	3.0						
			120167	sludge	380.0	390.0	0.64		
		380.3-388.5	1.0						
381.3-381.7	quartz vein								
381.7-386.2	quartz stringers								
386.2-386.5	quartz vein								
386.5-394.5	quartz stringers								
		388.5-393.9	2.5						
			120168	sludge	390.0	400.0	0.85		
		393.9-405.4	1.0						
394.5-394.7	quartz vein								
394.7-397.5	quartz stringers								
397.5-397.7	quartz vein								
397.7-407.5	quartz stringers								
			120169	sludge	400.0	410.0	0.39		
400.5-400.8	strongly sericitized and moderately dolomitized								
405.3-415.0	Graphitic Grit, Arenite and Pelite thin to very thin layering								
405.4-406.0	silicified and moderately dolomitized								
		405.4-406.0	2.0						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
406.0-407.5		1.0							
407.5-410.3	quartz vein								
407.5-409.7		0.5							
			4575	core	407.5	410.3	0.12	0.004	2.8
409.7-410.3		6.0							
			120170	sludge	410.0	420.0	0.66		
410.3-416.1	quartz stringers								
410.3-451.0		0.5							
410.6-412.7	strongly sericitized and moderately dolomitized								
412.7-445.7	moderately dolomitized								
415.0-428.2	Graphitic Pelite and Arenite very thin to thin layering								
416.1-416.6	quartz vein								
416.6-439.5	quartz stringers								
			120171	sludge	420.0	430.0	0.35		
428.2-451.4	Graphitic Pelite, Conglomerate and Arenite thin to very thin layering								
			120172	sludge	430.0	440.0	0.33		
439.5-439.6	quartz vein								
439.6-451.0	quartz stringers								
			120173	sludge	440.0	450.0	0.37		
445.7-450.2	silicified, moderately dolomitized and weakly chloritized								
			120174	sludge	450.0	460.0	0.35		
450.2-457.1	chloritized, moderately dolomitized and weakly sericitized								
451.0-483.4		0.5							
451.4-464.3	Dolomite Porphyroblastic Pelite and Arenite very thin to thin layering								
457.1-464.3	silicified, moderately chloritized and weakly dolomitized								
			120175	sludge	460.0	470.0	0.44		
464.3-484.3	Graphitic Pelite, Conglomerate and Arenite very thin to thin layering								
464.3-481.2	moderately dolomitized								
			120176	sludge	470.0	480.0	0.38		
471.0-473.0	quartz stringers								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
481.2-482.2	strongly sericitized and moderately dolomitized		120177	sludge	480.0	490.0	0.96		
482.2-483.4	silicified and moderately dolomitized								
483.4-484.2	strongly dolomitized and moderately silicified								
		483.4-506.4	1.5						
484.3-499.3	Grit, Arenite, Graphitic Pelite and Conglomerate very thin to thin layering								
484.2-485.4	strongly dolomitized and moderately sericitized								
485.4-485.6	strongly dolomitized								
			120178	sludge	490.0	500.0	0.38		
499.3-515.5	Conglomerate, Grit, Arenite and Minor Graphitic Pelite medium to thin layering								
501.5-510.3	strongly dolomitized, moderately silicified and weakly sericitized		120179	sludge	500.0	510.0	0.41		
510.3-565.4	strongly dolomitized, moderately sericitized and weakly silicified	506.4-515.5	0.5						
515.5-528.4	Grit, Arenite, Pelite and Conglomerate thin to very thin layering								
		515.5-519.5	1.5						
517.6-517.9	quartz vein								
		519.5-523.0	2.5						
522.8-523.0	quartz vein								
		523.0-569.9	0.5						
528.4-565.4	Grit, Conglomerate, Arenite and Pelite thin to very thin layering								
565.4-579.7	Grit, Arenite, Pelite and Conglomerate thin to very thin layering								
565.4-579.7	strongly sericitized, moderately dolomitized and weakly chloritized								
		569.9-577.5	2.0						
		577.5-579.7	12.5						
579.7-588.3	Dolomite Porphyroblastic Grit, Arenite and Pelite thin to medium layering								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
579.7-587.0	strongly sericitized, moderately dolomitized and weakly silicified								
		579.7-581.3	3.5						
		581.3-587.6	1.5						
587.0-589.0	silicified and moderately dolomitized								
		587.6-661.5	1.1						
588.3-630.2	Graphitic Arenite, Conglomerate, Grit and Pelite								
	very thin to thin layering								
589.0-589.3	quartz vein								
591.5-592.0	quartz vein								
595.0-598.8	quartz stringers								
598.2-598.8	fault								
604.0-605.1	quartz stringers								
604.9-605.1	fault								
605.1-605.3	quartz vein								
611.0-611.3	quartz stringers								
611.3-611.5	quartz vein								
614.7-614.9	quartz vein								
616.0-617.3	quartz stringers								
617.3-617.6	quartz vein								
617.6-619.6	quartz stringers								
621.9-623.5	moderately dolomitized								
623.5-625.1	strongly sericitized and moderately dolomitized								
625.1-627.0	moderately dolomitized								
628.8-628.9	quartz vein								
630.2-663.3	Graphitic Grit, Arenite, Pelite and Conglomerate								
	medium to thin layering								
638.4-638.9	quartz stringers								
653.9-656.1	silicified								
656.1-656.6	moderately dolomitized								
656.6-657.7	carbonized								
656.6-658.0	quartz stringers								
657.2-657.6	fault								
657.7-661.5	moderately dolomitized								
661.5-662.0	strongly sericitized and moderately dolomitized								
		661.5-662.0	1.5						
662.0-663.3	moderately dolomitized								
		662.0-663.3	0.5						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
663.3-800.0	Arenite, Grit and Pelite								
	medium to thin layering	0.5							
663.3-665.3	silicified and moderately dolomitized								
					663.3-670.0				
665.3-665.5	strongly sericitized and moderately dolomitized								
665.5-670.0	strongly dolomitized, moderately sericitized and weakly silicified								
666.8-678.4	quartz stringers	1.5							
670.0-690.9	strongly sericitized, moderately dolomitized and weakly silicified								
					670.0-719.0				
682.8-684.1	quartz stringers								
689.4-689.6	quartz vein								
690.9-691.4	chloritized and moderately sericitized	0.7							
691.4-710.0	strongly sericitized, moderately dolomitized and weakly silicified								
694.9-695.2	quartz stringers								
702.8-724.2	quartz stringers								
710.0-711.8	chloritized, moderately sericitized and weakly silicified								
711.8-720.0	strongly sericitized, moderately dolomitized and weakly silicified								
					719.0-734.7				
720.0-733.5	strongly sericitized and moderately dolomitized								
733.5-734.7	chloritized, moderately dolomitized, weakly sericitized and silicified								
734.7-742.3	strongly sericitized, moderately dolomitized and weakly silicified	1.5							
					734.7-737.9				
					737.9-770.0				
738.4-771.7	quartz stringers								
742.3-745.3	chloritized, moderately dolomitized and weakly sericitized	2.0							
745.3-749.8	strongly sericitized, moderately dolomitized and weakly chloritized	0.8							
749.8-754.2	strongly sericitized and moderately dolomitized								
754.2-755.3	chloritized, moderately dolomitized and weakly sericitized								
755.3-800.0	strongly sericitized and moderately dolomitized								
					770.0-771.7				
					771.7-800.0				
775.8-776.6	fault								
777.5-777.9	fault	1.5							
796.2-796.7	fault	0.8							
800.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-19

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: September 27, 2001
 Date Completed: October 2, 2001
 Final Depth: **589 feet (179.5 m)**

Collar Grid Coordinates
 Northing Easting Elevation
 Mine Grid **2894.0 ft. 21295.0 ft. 4787.0 ft.**

Logged by: D. Hladky

Depth	Azimuth	Dip
collar	223°	-62°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-15.0	Overburden								
15.0-35.0	Magnetite-bearing, Dolomite Porphyroblastic Pelite and Arenite thin to medium layering								
15.0-43.1	strongly sericitized and moderately silicified								
		15.0-50.0	1.0						
			120201	sludge	19.0	29.0	0.25		
			120202	sludge	29.0	39.0	0.29		
35.0-58.7	Magnetite-bearing Pelite and Arenite thick to thin layering								
			120203	sludge	39.0	49.0	0.04		
43.1-50.0	chloritized and moderately sericitized								
46.0-55.8	quartz stringers								
			120204	sludge	49.0	59.0	0.11		
50.0-54.0	strongly sericitized and moderately chloritized								
		50.0-54.0	2.5						
54.0-55.8	chloritized and moderately sericitized								
		54.0-55.8	0.8						
55.8-57.2	strongly sericitized and moderately chloritized								
		55.8-58.7	2.0						
57.2-60.0	strongly sericitized								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
58.7-63.0	Pelite and Arenite thick to thin layering								
		58.7-80.0	0.5	120205	sludge	59.0	69.0	<0.01	
60.0-63.0	chloritized and moderately sericitized								
63.0-67.8	Dolomite Porphyroblastic Pelite and Arenite thick to thin layering								
63.0-66.7	strongly sericitized and moderately chloritized								
63.0-80.0	quartz stringers								
66.7-80.0	strongly sericitized, moderately silicified and weakly dolomitized								
67.8-102.5	Graphitic Arenite, Pelite and Lesser Grit very thin to thin layering								
				120206	sludge	69.0	79.0	0.04	
71.6-71.8	fault								
				120207	sludge	79.0	89.0	0.08	
80.0-84.0	quartz stringers								
		80.0-102.5	0.8						
83.9-84.0	fault								
				120208	sludge	89.0	99.0	0.12	
95.0-101.5	quartz stringers								
				120209	sludge	99.0	109.0	0.13	
101.5-125.7	carbonized								
102.5-125.7	Graphitic Pelite and Arenite very thin to thin layering								
102.5-112.5	quartz stringers								
		102.5-112.5	1.5						
				4531	core	102.5	109.0	0.14	0.004
				4532	core	109.0	113.1	0.26	0.008
				120210	sludge	109.0	119.0	0.36	
112.5-113.1	quartz vein								
112.5-125.7	Fault Zone								
		112.5-113.1	2.0						
113.1-125.7	quartz stringers								
		113.1-163.5	1.5						
				4533	core	113.1	119.0	0.24	0.007
				4534	core	119.0	122.0	0.11	0.003

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
			120211	sludge	119.0	129.0	0.30		
			4535	core	122.0	125.7	0.61	0.018	3.7
125.7-389.4	Graphitic Arenite, Pelite and Grit very thin to thin layering								
125.7-126.4	strongly sericitized, moderately silicified and weakly dolomitized		4536	core	125.7	128.1	0.13	0.004	2.4
126.4-128.1	silicified and moderately dolomitized								
128.1-143.7	strongly sericitized and moderately dolomitized		4537	core	128.1	132.2	0.01	<0.001	4.1
			120212	sludge	129.0	139.0	0.26		
130.6-132.2	quartz stringers		4538	core	132.2	135.8	0.03	0.001	3.6
			4539	core	135.8	139.0	0.14	0.004	3.2
136.1-139.5	quartz stringers		120213	sludge	139.0	149.0	0.18		
140.5-143.2	quartz stringers								
143.7-148.8	chloritized, moderately dolomitized and weakly sericitized								
148.8-176.6	strongly sericitized and moderately dolomitized		120214	sludge	149.0	159.0	0.04		
153.7-160.6	quartz stringers								
158.3-158.6	fault		120215	sludge	159.0	169.0	0.06		
		163.5-168.9	0.8						
168.1-168.6	quartz stringers								
		168.9-171.6	1.5						
			120216	sludge	169.0	179.0	0.07		
171.6-172.3	fault								
		171.6-192.4	1.0						
176.6-178.0	chloritized, moderately dolomitized and weakly sericitized								
178.0-280.5	strongly sericitized and moderately dolomitized								
178.0-181.0	quartz stringers		120217	sludge	179.0	189.0	0.05		
			120218	sludge	189.0	199.0	0.13		
191.0-200.0	quartz stringers								
		192.4-196.7	1.2						
		196.7-198.7	1.5						
		198.7-202.8	1.2						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
			120219	sludge	199.0	209.0	0.71		
202.8-209.6		1.5							
			120220	sludge	209.0	219.0	0.62		
209.6-212.2		2.2							
212.2-213.0		40.0							
213.0-218.5		1.0							
218.5-220.0		5.0							
220.0-224.2		0.8							
224.2-224.9		5.0							
224.9-259.6		1.0							
			120222	sludge	229.0	239.0	0.17		
			120223	sludge	239.0	249.0	0.14		
			120224	sludge	249.0	259.0	0.13		
			120225	sludge	259.0	269.0	0.15		
259.6-265.4		1.5							
263.4-265.4	quartz stringers								
265.4-270.0		5.5							
			120226	sludge	269.0	279.0	0.15		
272.7-273.1	fault								
276.6-277.5	quartz stringers								
			120227	sludge	279.0	289.0	0.13		
280.5-285.9	silicified and moderately sericitized								
280.5-284.1	quartz stringers								
285.9-301.1	moderately sericitized								
285.9-286.9	quartz stringers								
286.9-289.8	quartz vein								
			120233	sludge	289.0	299.0	0.20		
289.8-294.6	quartz stringers								
294.6-299.1	quartz vein								
294.6-299.1		2.0							
			120234	sludge	299.0	309.0	0.52		
299.1-303.6	quartz stringers								
299.1-301.1		5.5							
301.1-303.6	silicified and moderately sericitized								
301.1-303.6		6.5							
303.6-319.2	moderately silicified								
303.6-307.1	quartz vein								
303.6-319.2		1.5							

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
307.1-311.7	quartz stringers								
307.4-307.6	fault		120235	sludge	309.0	319.0	0.20		
311.7-313.0	quartz vein								
313.0-319.2	quartz stringers								
317.8-318.4	fault		120236	sludge	319.0	329.0	0.09		
319.2-353.7	strongly sericitized and moderately dolomitized								
319.2-319.7	fault	319.2-341.8	1.2						
319.7-323.7	quartz stringers		120237	sludge	329.0	339.0	0.13		
337.6-337.8	fault		120238	sludge	339.0	349.0	0.10		
		341.8-342.4	6.2						
		342.4-345.4	30.0						
		345.4-351.5	3.0						
346.5-346.9	fault		120239	sludge	349.0	359.0	0.17		
		351.5-353.7	8.0						
351.7-351.8	quartz vein								
352.4-365.7	quartz stringers								
353.7-360.7	moderately silicified	353.7-375.0	2.5						
			120240	sludge	359.0	369.0	0.23		
360.7-360.9	strongly sericitized								
360.9-375.0	moderately silicified		120241	sludge	369.0	379.0	0.22		
372.3-378.0	quartz stringers								
375.0-379.2	strongly sericitized and moderately silicified	375.0-389.4	3.5						
			120242	sludge	379.0	389.0	0.25		
379.2-389.2	moderately silicified		120243	sludge	389.0	399.0	0.40		
389.4-397.1	Arenite, Grit and Pelite								
389.2-464.8	silicified								
	very thin to thin layering								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
389.4-414.7		2.5							
397.1-464.8	Graphitic Arenite, Grit, Pelite and Conglomerate very thin to thin layering								
409.5-417.0	quartz stringers		120254	sludge	409.0	419.0	0.57		
414.7-416.9		5.0							
416.9-426.3		2.0							
417.0-417.5	quartz vein								
417.5-425.1	quartz stringers								
425.1-425.5	quartz vein		120255	sludge	419.0	429.0	0.29		
425.5-432.1	quartz stringers								
426.3-464.8		1.5							
437.0-438.0	quartz stringers		120256	sludge	429.0	439.0	0.27		
444.3-444.6	fault								
446.0-446.5	fault								
449.3-450.3	quartz stringers		120257	sludge	439.0	449.0	0.20		
459.5-464.0	quartz stringers								
			120258	sludge	449.0	459.0	0.13		
			120259	sludge	459.0	469.0	0.11		
464.8-475.7	Graphitic Pelite and Arenite very thin layering								
467.7-467.8	fault								
470.0-474.8	quartz stringers		120260	sludge	469.0	479.0	0.12		
474.8-475.0		35.0							
475.0-475.7		7.0							
475.7-487.2	Arenite and Pelite very thin to thin layering								
475.7-478.6	strongly sericitized and moderately silicified								
475.7-477.8		2.5							
477.8-479.0		20.0							

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
478.6-487.2	strongly sericitized								
		479.0-492.0	2.5						
			120261	sludge	479.0	489.0	0.07		
487.2-490.2	Graphitic Pelite and Arenite very thin to thin layering								
488.6-495.1	quartz stringers								
			120262	sludge	489.0	499.0	0.19		
490.2-517.3	Calcareous Arenite and Pelite thin to very thin layering								
490.2-495.1	strongly sericitized and moderately dolomitized								
		492.0-492.7	15.0						
		492.7-495.1	2.5						
		495.1-517.3	1.5						
497.6-517.3	strongly sericitized and moderately dolomitized								
			120263	sludge	499.0	509.0	0.04		
			120264	sludge	509.0	519.0	0.27		
517.3-589.0	Graphitic Grit, Arenite, Pelite and Conglomerate thin to medium layering								
		517.3-589.0	0.8						
			120265	sludge	519.0	529.0	0.15		
			120266	sludge	529.0	539.0	0.11		
			120267	sludge	539.0	549.0	0.10		
540.2-540.4	strongly sericitized								
			120268	sludge	549.0	559.0	0.03		
			120269	sludge	559.0	569.0	0.04		
			120270	sludge	569.0	579.0	0.07		
			120271	sludge	579.0	589.0	0.05		
589.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-20

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: October 2, 2001
 Date Completed: October 16, 2001
 Final Depth: **690 feet (210.3 m)**

Collar Grid Coordinates
 Northing Easting Elevation
 Mine Grid 2940.1 ft. 18204.7 ft. 4989.9 ft.

Logged by: D. Hladky

Depth	Azimuth	Dip
collar	223°	-65°
100.0 ft.	224°	-64°
380.0 ft.	227°	-64°
680.0 ft.	230°	-61°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-16.0	Overburden								
16.0-31.5	Graphitic Pelite and Arenite very thin to thin layering								
		16.0-62.6	0.5						
31.5-41.4	Graphitic Arenite, Pelite and Grit very thin to thin layering								
39.0-41.4	quartz stringers								
41.4-49.7	Graphitic Pelite, Arenite and Grit very thin to thin layering								
49.7-57.8	Graphitic Arenite, Pelite and Grit very thin to thin layering								
54.5-54.6	fault								
54.7-55.0	quartz stringers								
57.8-96.4	Graphitic Pelite, Grit, Arenite and Conglomerate very thin to thin layering								
57.8-62.6	strongly sericitized								
60.0-69.0	quartz stringers								
62.6-62.9	fault								
		62.6-70.0	0.8						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
70.2-89.0	silicified and moderately sericitized	0.5							
75.2-77.5	fault								
81.1-84.3	Fault Zone								
86.0-90.1	quartz stringers								
88.0-88.9	Fault Zone								
90.1-96.4	quartz vein		4558	core	90.0	96.4	0.18	0.005	6.4
96.4-129.3	Graphitic, Dolomite Porphyroblastic Arenite, Pelite and Grit thin to very thin layering								
96.4-171.6	silicified, moderately sericitized and weakly dolomitized								
		4.0	4559	core	96.4	100.0	0.17	0.005	3.6
		0.5							
			120272	sludge	110.0	120.0	0.35		
			4560	core	120.0	124.6	0.13	0.004	4.6
			120273	sludge	120.0	130.0	6.56		
121.5-123.6	quartz stringers								
		1.5							
		0.5							
		1.5							
			4561	core	124.6	130.0	0.28	0.008	5.4
125.0-125.8	quartz stringers								
		0.5							
129.3-150.9	Magnetite-bearing, Dolomite Porphyroblastic Arenite, Pelite and Grit thin to very thin layering								
			4562	core	130.0	135.0	0.75	0.022	5.0
			120274	sludge	130.0	140.0	19.27		
130.3-131.4	quartz stringers								
		1.5							
		0.5							
			4576	core	135.0	140.0	0.35	0.010	5.0
136.9-142.5	quartz stringers								
			4577	core	140.0	145.0	0.02	0.001	5.0
			120275	sludge	140.0	150.0	5.07		
			4578	core	145.0	150.0	0.13	0.004	5.0

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
147.5-148.6	quartz stringers								
		1.5							
		0.5							
			4579	core	150.0	154.0	0.06	0.002	4.0
			120276	sludge	150.0	160.0	3.05		
150.9-166.0	Graphitic, Dolomite Porphyroblastic Arenite, Pelite and Grit thin to very thin layering								
150.9-152.7	quartz stringers								
154.0-156.4	quartz vein								
		8.5							
			4541	core	154.0	156.4	1.33	0.039	2.4
156.4-158.0		1.0							
			4580	core	156.4	160.0	0.01	<0.001	3.6
158.0-167.0		0.5							
			4581	core	160.0	165.0	0.01	<0.001	5.0
			120277	sludge	160.0	170.0	11.76		
			4582	core	165.0	170.0	0.76	0.022	5.0
165.7-171.6	quartz stringers								
166.0-183.1	Graphitic, Magnetite-bearing Pelite and Arenite thin to medium layering								
		1.5							
			4583	core	170.0	175.0	0.08	0.002	5.0
			120278	sludge	170.0	180.0	6.45		
171.6-181.1	strongly sericitized, moderately chloritized and weakly dolomitized								
173.5-176.5	quartz stringers								
			4584	core	175.0	180.0	0.01	<0.001	5.0
180.0-206.0	quartz stringers								
			4585	core	180.0	185.0	0.01	<0.001	5.0
			120279	sludge	180.0	190.0	0.92		
181.1-205.8	chloritized								
183.1-185.3	Graphitic Pelite and Arenite thin to medium layering								
			4586	core	185.0	190.0	0.01	<0.001	5.0

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
185.3-238.0	Magnetite-bearing Pelite and Arenite thin to medium layering								
			4587	core	190.0	195.0	0.01	<0.001	5.0
			120280	sludge	190.0	200.0	0.82		
			4588	core	195.0	200.0	0.01	<0.001	5.0
			4589	core	200.0	205.1	0.01	<0.001	5.1
			120281	sludge	200.0	210.0	3.23		
			4563	core	205.1	207.1	0.22	0.006	2.0
205.8-208.8	strongly sericitized								
206.0-206.4	quartz vein								
		20.0							
		1.5							
208.8-211.9	chloritized		4590	core	207.1	211.9	0.01	<0.001	4.8
			120282	sludge	210.0	220.0	0.18		
211.9-254.9	strongly sericitized and moderately silicified								
			4591	core	211.9	215.0	0.01	<0.001	3.1
			4592	core	215.0	220.0	0.16	0.005	5.0
217.9-222.5	quartz stringers								
217.9-218.5	Fault Zone								
219.2-219.8	fault								
			4593	core	220.0	225.0	0.39	0.011	5.0
			120283	sludge	220.0	230.0	0.17		
220.6-222.0	Fault Zone								
222.0-224.3	Fault Zone								
			4594	core	225.0	230.0	0.03	0.001	5.0
225.3-226.9	fault								
			4595	core	230.0	235.0	0.07	0.002	5.0
			120284	sludge	230.0	240.0	0.27		
			4596	core	235.0	240.0	0.01	<0.001	5.0
238.0-263.3	Dolomite Porphyroblastic, Arenite, Pelite and Grit thin to very thin layering								
			4597	core	240.0	245.0	0.35	0.010	5.0
			120285	sludge	240.0	250.0	11.39		
			4598	core	245.0	250.0	0.05	<0.001	5.0
			4599	core	250.0	254.9	0.03	0.001	4.9
			120286	sludge	250.0	260.0	0.77		
252.7-254.9	quartz vein								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
254.3-254.9		12.0							
254.9-263.3	silicified and moderately sericitized		4542	core	254.3	254.9	4.74	0.138	0.6
254.9-255.9	fault								
254.9-266.0		2.0							
257.2-257.6	quartz vein		4543	core	254.9	259.9	1.08	0.032	5.0
				core	254.3	259.9	1.47	0.043	5.6
			4544	core	259.9	261.7	0.15	0.004	1.8
			120287	sludge	260.0	270.0	2.74		
261.7-262.0	quartz vein								
			4545	core	261.7	264.0	0.61	0.018	2.3
263.3-264.0	Arenite, Conglomerate and Pelite								
	very thin to thin layering								
263.3-265.4	quartz stringers								
264.0-266.0	Dolomite Porphyroblastic Arenite, Pelite and Grit								
	thin to very thin layering								
264.0-266.0	silicified and moderately sericitized								
			4546	core	264.0	266.0	0.67	0.020	2.0
265.4-266.0	quartz vein								
266.0-281.4	Graphitic Pelite and Arenite								
	very thin to thin layering								
266.0-281.4	carbonized								
266.0-268.8	quartz stringers								
266.0-266.1	fault								
266.0-270.6		1.5							
			4547	core	266.0	270.7	2.36	0.069	4.7
268.8-270.6	quartz vein								
			120288	sludge	270.0	280.0	20.85		
270.6-271.2		40.0							
			4548	core	270.7	276.0	12.67	0.370	5.3
271.2-272.2	quartz vein								
271.2-277.5		1.2							
273.0-273.8	quartz vein								
			4600	core	276.0	277.5	7.35	0.214	1.5

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
277.5-280.8	quartz vein								
		20.0							
			4551	core	277.5	281.4	27.91	0.814	3.9
			120289	sludge	280.0	290.0	14.16		
		1.5							
281.4-291.0	Graphitic Arenite and Pelite								
	very thin to thin layering			core	266.0	281.4	12.86	0.375	15.4
				core	254.3	281.4	7.62	0.222	27.1
281.4-291.0	strongly sericitized and moderately silicified								
		0.8							
282.1-282.3	quartz vein		4601	core	281.4	285.0	0.31	0.009	3.6
			4602	core	285.0	290.0	0.08	0.002	5.0
286.9-287.2	quartz vein								
		1.5							
		0.5							
			4603	core	290.0	295.0	0.17	0.005	5.0
			120290	sludge	290.0	300.0	1.38		
291.0-293.3	Graphitic Pelite and Arenite								
	very thin layering								
291.0-293.3	carbonized								
293.3-298.4	Graphitic Arenite and Pelite								
	thin to very thin layering								
293.3-298.4	strongly sericitized and moderately dolomitized								
			4604	core	295.0	300.0	0.11	0.003	5.0
298.4-300.4	Magnetite- and Chlorite-bearing Arenite and Pelite								
	thin to very thin layering								
298.4-300.8	chloritized								
			4605	core	300.0	305.0	0.03	0.001	5.0
			120291	sludge	300.0	310.0	2.93		
300.4-314.6	Arenite and Grit								
	very thin to thin layering								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
300.8-314.6	strongly sericitized and moderately chloritized		4606	core	305.0	310.0	0.19	0.006	5.0
			4607	core	310.0	314.3	0.09	0.003	4.3
			120292	sludge	310.0	320.0	2.25		
311.0-318.6	quartz stringers								
		2.0							
314.0-318.2			4608	core	314.3	318.4	0.03	0.001	4.1
314.6-318.2	Graphitic Pelite and Arenite thin layering								
314.6-318.2	carbonized								
314.6-318.2	fault								
318.2-327.4	Grit and Arenite thin to medium layering								
318.2-327.4	chloritized								
		1.0							
			4609	core	318.4	321.7	0.05	0.001	3.3
			120293	sludge	320.0	330.0	2.43		
320.6-329.6	quartz stringers								
			4610	core	321.7	322.9	0.18	0.005	1.2
			4611	core	322.9	326.5	0.15	0.004	3.6
			4612	core	326.5	330.0	0.03	0.001	3.5
			4613	HG Standard			6.81	0.199	
327.4-329.8	Pelite and Arenite very thin to thin layering								
327.4-329.8	strongly sericitized								
		trace							
			4614	LG Standard			1.74	0.051	
329.8-332.2	Grit and Arenite medium to thin layering								
			4615	core	330.0	335.0	0.02	0.001	5.0
			120294	sludge	330.0	340.0	0.40		
332.2-336.3	Grit and Arenite medium to thin layering								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
332.2-359.5	strongly sericitized		4616	core	335.0	340.0	0.01	<0.001	5.0
336.3-340.6	Pelite and Arenite								
	thin to very thin layering								
338.0-338.2	quartz vein		4617	core	340.0	345.0	0.01	<0.001	5.0
			120295	sludge	340.0	350.0	5.29		
340.6-352.5	Grit, Arenite and Pelite								
	medium to thin layering		4618	core	345.0	350.0	0.01	<0.001	5.0
			4619	core	350.0	355.0	0.01	<0.001	5.0
			120296	sludge	350.0	360.0	3.35		
352.5-359.5	Arenite, Pelite and Grit								
	thin layering								
		352.5-359.5	0.5						
			4620	core	355.0	359.3	0.04	0.001	4.3
355.7-356.0	fault								
357.1-357.3	fault								
359.5-363.4	Pelite and Arenite								
	thin to very thin layering		4621	core	359.3	364.1	0.64	0.019	4.8
	carbonized								
359.5-369.8									
		359.5-363.4	0.8						
			120297	sludge	360.0	370.0	5.73		
360.6-361.4	quartz vein								
361.4-368.6	fault								
363.4-369.8	Arenite, Pelite and Grit								
	thin to very thin layering								
		363.4-421.3	trace						
			4622	core	364.1	370.0	0.06	0.002	5.9
369.8-377.0	Grit and Arenite								
	thin to very thin layering								

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From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
377.0-397.1	Pelite and Arenite								
369.8-377.0	strongly sericitized								
			4623	core	370.0	375.0	0.01	<0.001	5.0
			120298	sludge	370.0	380.0	3.77		
			4624	core	375.0	376.0	0.01	<0.001	1.0
			4625	core	376.0	380.0	0.01	<0.001	4.0
377.0-379.0	carbonized								
379.0-420.6	strongly sericitized								
			120299	sludge	380.0	390.0	0.88		
			120300	sludge	390.0	400.0	0.21		
397.1-406.3	Arenite, Grit and Pelite								
	thin to medium layering								
			195351	sludge	400.0	410.0	0.12		
406.3-425.3	Grit, Arenite and Pelite								
	thin to medium layering								
			195352	sludge	410.0	420.0	0.09		
			195353	sludge	420.0	430.0	0.24		
		421.3-441.8	0.5						
425.3-431.2	Pelite and Arenite								
	thin to medium layering								
428.0-430.0	fault								
			195354	sludge	430.0	440.0	0.10		
431.2-441.8	Grit and Arenite								
	thin to medium layering								
431.2-441.8	strongly sericitized								
			195355	sludge	440.0	450.0	0.23		
441.8-447.0	Conglomerate and Grit								
	medium to thick layering								
441.8-450.2	strongly sericitized								
441.8-447.0	quartz stringers								
		441.8-450.2	trace						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
447.0-450.2	Arenite and Pelite thin to medium layering								
450.2-481.0	Grit, Arenite and Pelite medium layering strongly sericitized		195356	sludge	450.0	460.0	0.20		
450.2-481.0		3.0							
			4552	core	450.2	454.0	0.02	0.001	3.8
			4553	core	454.0	458.0	0.01	<0.001	4.0
458.0-465.0		7.5							
			4554	core	458.0	462.0	0.01	<0.001	4.0
459.6-461.4	fault								
			195357	sludge	460.0	470.0	0.26		
			4555	core	462.0	465.0	0.01	<0.001	3.0
465.0-475.0		20.0							
			4556	core	465.0	470.0	0.02	0.001	5.0
			4557	core	470.0	475.0	0.05	0.001	5.0
			195358	sludge	470.0	480.0	0.20		
475.0-481.0		3.0							
			195359	sludge	480.0	490.0	0.20		
481.0-521.0	Arenite, Grit and Pelite thin to medium layering quartz stringers								
481.0-521.0		1.5							
			4626	core	485.0	490.0	0.01	<0.001	5.0
			4627	core	490.0	495.0	0.01	<0.001	5.0
			195360	sludge	490.0	500.0	1.18		
			4628	core	495.0	500.0	0.01	<0.001	5.0
			4629	core	500.0	505.0	0.01	<0.001	5.0
			195361	sludge	500.0	510.0	1.06		
			4630	core	505.0	510.0	0.01	<0.001	5.0
			195362	sludge	510.0	520.0	0.29		
515.3-515.7	fault								
516.9-517.2	quartz vein								
517.2-521.0	quartz stringers								
			195363	sludge	520.0	530.0	0.20		

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
521.0-557.5	Arenite and Pelite								
	medium layering								
521.0-549.0	strongly sericitized								
521.0-521.4	fault								
		5.0							
521.0-529.6			4564	core	521.6	526.6	0.08	0.002	5.0
			4565	core	526.6	530.0	0.02	0.001	3.4
529.6-540.0		0.5							
529.7-540.0	fault		195364	sludge	530.0	540.0	0.23		
540.0-540.6	quartz vein								
		1.0							
540.0-583.0			195365	sludge	540.0	550.0	0.30		
540.6-545.0	quartz stringers								
541.2-541.6	fault								
547.0-549.0	Fault Zone								
549.2-549.4	quartz vein								
551.1-551.2	quartz stringers								
552.7-552.9	quartz vein								
556.2-556.4	quartz vein								
557.5-590.0	Pelite and Arenite								
	thin layering								
			195366	sludge	560.0	570.0	0.30		
564.8-565.6	quartz vein								
566.3-567.2	quartz vein								
568.0-569.2	quartz vein								
			195367	sludge	570.0	580.0	0.11		
570.1-573.4	quartz vein								
574.2-574.4	quartz vein								
574.8-575.0	quartz vein								
575.4-576.8	quartz vein								
578.0-578.4	quartz vein								
			195368	sludge	580.0	590.0	0.17		
			4566	core	580.3	583.0	0.03	0.001	2.7
580.4-581.1	quartz vein								
581.3-583.1	fault								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
583.0-591.0		4.0							
			4567	core	583.0	588.0	0.02	0.001	5.0
			4568	core	588.0	591.0	0.01	<0.001	3.0
590.0-602.4	Arenite and Pelite very thin layering								
			195369	sludge	590.0	600.0	0.10		
591.0-593.0		0.5							
593.0-606.0		4.0							
			195370	sludge	600.0	610.0	0.27		
602.4-615.0	Pelite very thin layering								
606.0-617.6		1.0							
			195371	sludge	610.0	620.0	0.29		
612.2-612.6	fault								
615.0-624.2	Arenite and Pelite very thin to thin layering								
617.6-637.0		0.5							
618.9-619.8	quartz stringers								
			195372	sludge	620.0	630.0	0.24		
622.0-648.4	silicified								
622.2-623.5	quartz stringers								
624.2-648.6	Arenite thin to very thin layering								
			195373	sludge	630.0	640.0	0.37		
637.0-658.0		1.5							
			195374	sludge	640.0	650.0	0.86		
648.6-664.5	Arenite and Pelite								
648.4-664.6	moderately dolomitized very thin layering								
648.7-648.8	quartz vein								
			4631	core	650.0	653.6	0.05	0.001	3.6
			195375	sludge	650.0	660.0	1.25		
			4632	core	653.6	656.0	0.06	0.002	2.4

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
658.0-661.5			4633	core	656.0	658.0	0.02	0.001	2.0
		5.0							
			4569	core	658.0	661.5	0.78	0.023	3.5
661.0-661.5	quartz vein		195376	sludge	660.0	670.0	0.74		
661.5-668.6		0.8							
662.4-662.6	quartz vein								
663.7-664.2	quartz vein								
664.5-690.0	Arenite, Grit and Pelite thin to medium layering								
668.6-671.8	quartz vein		4634	core	668.3	672.2	0.02	0.001	3.9
668.6-671.8		trace							
671.8-690.0			195377	sludge	670.0	680.0	0.12		
		0.5							
673.5-673.9	quartz vein		4635	core	672.2	676.0	0.01	<0.001	3.8
675.6-675.7	quartz vein								
679.8-679.9	quartz vein		4636	core	676.0	680.0	0.01	<0.001	4.0
			4637	core	680.0	685.0	0.01	<0.001	5.0
			195378	sludge	680.0	690.0	1.32		
680.4-681.0	quartz vein								
681.3-681.6	quartz vein								
683.8-684.0	fault								
			4638	core	685.0	690.0	0.01	<0.001	5.0
690.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-21

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: October 17, 2001
 Date Completed: November 10, 2001
 Final Depth: **840 feet (256.0 m)**

Collar Grid Coordinates
 Northing Easting Elevation
 Mine Grid 2941.0 ft. 18204.7 ft. 4989.9 ft.

Logged by: K. Lord

Depth	Azimuth	Dip
collar	223°	-80°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-16.0	Overburden								
16.0-70.5	Pelite, Arenite and Grit thin layering								
		16.0-155.1	0.5						
			120301	sludge	16.0	30.0	0.01		
			120302	sludge	30.0	40.0	<0.01		
			120303	sludge	40.0	50.0	<0.01		
			120304	sludge	50.0	60.0	<0.01		
			120305	sludge	60.0	70.0	0.15		
69.0-69.8	quartz vein								
			120306	sludge	70.0	80.0	0.18		
70.5-120.0	Dolomite Porphyroblastic Pelite and Arenite very thin to thin layering								
			120307	sludge	80.0	90.0	<0.01		
			120308	sludge	90.0	100.0	0.02		
91.2-91.3	quartz vein								
92.5-92.7	dolomite vein								
			120309	sludge	100.0	110.0	0.05		
106.0-114.0	Fault Zone								
114.0-120.0	fault								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
120.0-163.0	Dolomite Porphyroblastic Pelite								
	very thin layering								
120.0-163.0	silicified								
120.0-132.0	Fault Zone		120311	sludge	120.0	130.0	0.28		
			120312	sludge	130.0	140.0	0.37		
136.6-136.8	quartz vein								
			120313	sludge	140.0	150.0	0.38		
			120314	sludge	150.0	160.0	0.16		
153.4-154.0	fault								
		5.0							
155.1-156.0		0.5							
156.0-173.0			120315	sludge	160.0	170.0	0.43		
163.0-366.0	Magnetite-bearing and Dolomite Porphyroblastic Pelite								
	very thin layering								
163.0-324.0	silicified and moderately chloritized								
165.3-165.6	fault								
			120316	sludge	170.0	180.0	0.55		
173.0-189.0	quartz stringers								
		1.0							
			120317	sludge	180.0	190.0	0.72		
		trace							
			120318	sludge	190.0	200.0	0.15		
195.8-196.4	quartz vein								
		2.0							
		0.5							
			120319	sludge	200.0	210.0	0.17		
			120320	sludge	210.0	220.0	0.51		
			120321	sludge	220.0	230.0	0.50		
			120322	sludge	230.0	240.0	0.62		
235.0-238.3	fault								
			120323	sludge	240.0	250.0	0.57		
			120324	sludge	250.0	260.0	0.29		
251.6-251.8	quartz and dolomite vein								
253.6-253.8	quartz vein								
254.7-255.4	quartz vein								
			120325	sludge	260.0	270.0	0.32		
266.6-266.7	quartz vein								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
290.6-290.7	quartz vein		120326	sludge	270.0	280.0	0.25		
			120327	sludge	280.0	290.0	0.45		
			120328	sludge	290.0	300.0	0.14		
			120329	sludge	300.0	310.0	3.59		
			120330	sludge	310.0	320.0	0.37		
307.8-314.5	quartz stringers		120331	sludge	320.0	330.0	3.13		
			4639	core	324.0	328.7	4.42		
324.5-326.0		1.0							
324.9-325.1	quartz vein								
325.8-326.4	quartz vein								
326.0-326.6		2.5							
326.6-328.5		2.0							
328.3-328.6	quartz vein								
328.5-328.7		5.0							
328.7-362.6		0.5							
362.5-363.1	quartz vein		120332	sludge	330.0	340.0	1.15		
			120333	sludge	340.0	350.0	0.67		
			120334	sludge	350.0	360.0	1.59		
			120335	sludge	360.0	370.0	21.69		
362.6-363.1		15.0							
			4640	core	362.6	364.4	2.11		
363.1-366.0		1.0							
			4641	core	364.4	366.0	0.64		
366.0-439.0	Graphitic Pelite								
	very thin layering								
366.0-439.0	carbonized								
366.0-379.0	quartz vein								
366.0-367.4		10.0							
			4642	core	366.0	369.0	2.37		
367.4-370.1		1.5							
			4643	core	369.0	371.7	0.90		
			120336	sludge	370.0	380.0	14.06		
370.1-375.0		10.0							
			4644	core	371.7	378.5	8.26	0.241	6.8

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
375.0-376.5		2.0							
376.5-378.5		10.0							
378.0-388.2	fault								
		1.0							
				core	362.6	378.5	4.44	0.129	15.9
			4645	core	378.5	383.5	0.26	0.008	5.0
379.7-386.8	quartz stringers								
			120337	sludge	380.0	390.0	1.78		
			4646	core	383.5	388.2	0.53	0.015	4.7
			4647	core	388.2	392.1	0.12	0.004	3.9
390.0-390.1	quartz vein								
			120338	sludge	390.0	400.0	0.62		
390.5-390.7	quartz vein								
392.1-393.8	quartz vein								
		3.0							
			4648	core	392.1	395.5	0.07	0.002	3.4
		0.5							
395.5-399.1	quartz vein								
			4649	core	395.5	399.1	0.11	0.003	3.6
396.5-396.8	fault								
397.5-399.1	fault								
			120339	sludge	400.0	410.0	0.27		
406.3-406.5	quartz vein								
407.6-407.8	quartz and dolomite vein								
409.8-410.0	quartz vein								
			120340	sludge	410.0	420.0	1.08		
			120341	sludge	420.0	430.0	1.04		
421.0-421.3	quartz vein								
		5.0							
422.0-439.0	Fault Zone								
			120342	sludge	430.0	440.0	0.88		
439.0-470.5	Mariposite-bearing Pelite and Arenite								
	thin layering								
439.0-470.2	strongly sericitized								
			120343	sludge	440.0	450.0	0.23		
			120344	sludge	450.0	460.0	0.30		
			120345	sludge	460.0	470.0	0.12		

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
468.2-468.3	quartz vein								
469.0-469.1	quartz vein								
470.0-470.0		0.8							
470.0-472.7		0.5							
			120346	sludge	470.0	480.0	0.56		
470.2-472.7	strongly sericitized and moderately dolomitized								
470.5-544.0	Calcareous Arenite, Grit and Pelite								
	thin layering								
472.7-538.8	strongly dolomitized and moderately sericitized								
472.7-497.7		1.0							
			120347	sludge	480.0	490.0	0.44		
			120348	sludge	490.0	500.0	0.18		
			4650	core	492.5	497.7	0.03	0.001	5.2
497.7-502.5		3.0							
			4651	core	497.7	502.5	0.01	<0.001	4.8
			120349	sludge	500.0	510.0	0.06		
502.5-518.4		1.0							
			4652	core	502.5	507.5	0.04	0.001	5.0
			4653	core	507.5	512.5	0.04	0.001	5.0
			120350	sludge	510.0	520.0	0.13		
512.0-514.1	fault								
			4654	core	512.5	518.0	0.05	0.001	5.5
			4655	core	518.0	520.0	0.05	0.001	2.0
518.4-518.6		5.0							
518.6-538.8		0.5							
			4656	core	520.0	525.0	0.04	0.001	5.0
			120351	sludge	520.0	530.0	0.34		
			4657	core	525.0	530.0	0.02	0.001	5.0
			4658	core	530.0	534.0	0.01	<0.001	4.0
			120352	sludge	530.0	540.0	0.09		
			4659	core	534.0	538.8	0.01	<0.001	4.8
538.8-555.5	silicified and moderately dolomitized								
538.8-543.5		5.0							
			4660	core	538.8	543.5	0.03	0.001	4.7
			120353	sludge	540.0	550.0	0.58		
543.5-577.8		0.5							
			4661	core	543.5	548.5	0.01	<0.001	5.0

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
544.0-555.5	Arenite and Grit thin to medium layering								
			120354	sludge	550.0	560.0	0.55		
555.5-568.9	Pelite thin layering								
557.0-561.5	Fault Zone								
			120355	sludge	560.0	570.0	0.48		
568.9-620.7	Pelite and Arenite thin to medium layering								
568.9-611.5	moderately silicified								
			120356	sludge	570.0	580.0	0.34		
573.1-573.8	fault								
		577.8-620.7	1.0						
			120357	sludge	580.0	590.0	0.17		
583.0-593.5	quartz stringers								
			120358	sludge	590.0	600.0	0.33		
595.7-595.8	quartz vein								
			120359	sludge	600.0	610.0	0.43		
			120360	sludge	610.0	620.0	0.06		
611.5-614.0	strongly sericitized								
614.0-620.7	silicified								
			120361	sludge	620.0	630.0	0.04		
620.7-642.0	Calcareous, Magnetite-bearing Arenite and Pelite thin to medium layering								
620.7-642.0	strongly sericitized								
620.7-636.7	quartz and calcite stringers								
		620.7-636.7	2.0						
			120362	sludge	630.0	640.0	0.07		
			4662	core	632.8	636.7	0.05	0.001	3.9
636.7-637.4	quartz vein								
		636.7-637.4	30.0						
			4663	core	636.7	640.0	0.26	0.008	3.3
637.4-638.8	quartz and calcite stringers								
		637.4-638.8	5.0						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
638.8-639.8	quartz vein								
		638.8-639.8	30.0						
		639.8-656.8	2.0						
			4664	core	640.0	645.0	0.02	0.001	5.0
			120363	sludge	640.0	650.0	0.82		
642.0-675.0	Arenite and Pelite								
	thin to medium layering								
642.0-678.8	strongly sericitized and moderately dolomitized								
			120364	sludge	650.0	660.0	0.26		
		656.8-664.5	4.0						
			4665	core	657.7	660.5	0.02	0.001	2.8
			120365	sludge	660.0	670.0	0.63		
			4666	core	660.5	664.5	0.06	0.002	4.0
		664.5-686.5	0.5						
666.2-666.4	quartz vein								
			120366	sludge	670.0	680.0	0.27		
675.0-692.7	Calcareous Arenite and Pelite								
	thin to medium layering								
678.8-700.0	strongly dolomitized								
			120367	sludge	680.0	690.0	0.18		
			4667	core	686.0	691.0	0.04	0.001	5.0
		686.5-691.3	4.0						
			120368	sludge	690.0	700.0	0.18		
			4668	core	691.0	692.0	0.01	<0.001	1.0
		691.3-691.8	10.0						
		691.8-695.0	4.0						
			4669	core	692.0	694.0	0.02	0.001	2.0
692.7-769.0	Magnetite-bearing Arenite, Pelite and Grit								
	thin to medium layering								
			4670	core	694.0	699.0	0.02	0.001	5.0
		695.0-703.5	3.0						
			4671	core	699.0	703.5	0.01	<0.001	4.5
700.0-720.0	strongly sericitized								
			120369	sludge	700.0	710.0	0.14		
703.5-710.3	quartz vein								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
703.5-710.3		7.5							
			4672	core	703.5	710.3	0.06	0.002	6.8
			120370	sludge	710.0	720.0	0.27		
710.3-717.8		5.0							
			4673	core	710.3	714.0	0.01	<0.001	3.7
			4674	core	714.0	717.8	0.01	<0.001	3.8
717.8-719.3	quartz vein								
717.8-719.3		10.0							
			4675	core	717.8	719.3	0.01	<0.001	1.5
719.3-725.7		2.0							
			4676	core	719.3	722.3	0.01	<0.001	3.0
720.0-773.5	strongly dolomitized and moderately sericitized		120371	sludge	720.0	730.0	0.15		
722.3-723.1	quartz vein		4677	core	722.3	726.5	0.01	<0.001	4.2
724.0-724.2	quartz vein								
725.7-725.9	quartz vein								
725.7-725.9		25.0							
725.9-729.0		1.0							
			4678	core	726.5	731.5	0.01	<0.001	5.0
729.0-748.5		5.0							
			120372	sludge	730.0	740.0	0.16		
			4679	core	731.5	736.5	0.01	<0.001	5.0
734.0-734.0	quartz vein		4680	core	736.5	741.5	0.01	<0.001	5.0
			120373	sludge	740.0	750.0	0.19		
			4681	core	741.5	746.5	0.01	<0.001	5.0
748.5-768.0		2.0							
			120374	sludge	750.0	760.0	0.13		
754.3-755.0	quartz vein								
768.0-777.8		3.0							
769.0-829.3	Calcareous, Magnetite-bearing Pelite and Arenite thin to medium layering								
773.5-829.3	strongly sericitized and moderately dolomitized								
777.8-777.9	quartz vein								
777.8-777.9		20.0							
777.9-787.8		4.0							

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From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
787.8-800.0		1.0							
800.0-810.4		2.0							
810.4-823.0		0.5							
823.0-840.0		1.5							
829.3-840.0	Arenite and Pelite thin layering								
829.3-840.0	strongly dolomitized								
840.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. BC01-22

Property: **Bonanza**
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: November 14, 2001
 Date Completed: November 23, 2001
 Final Depth: **690 feet (210.3 m)**

Collar Grid Coordinates
Northing Easting Elevation
 Mine Grid **2397.9 ft. 20195.3 ft. 4775.8 ft.**

Logged by: G. Walton

Depth	Azimuth	Dip
collar	46°	-88°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-22.0	Overburden								
22.0-121.6	Arenite								
	thin to medium layering								
22.0-55.0	limonitized								
		22.0-91.8	1.0						
			120375	sludge	22.0	30.0	<0.01		
			120376	sludge	30.0	40.0	<0.01		
			120377	sludge	40.0	50.0	<0.01		
			120378	sludge	50.0	60.0	<0.01		
55.0-121.6	strongly sericitized								
			120379	sludge	60.0	70.0	<0.01		
			120380	sludge	70.0	80.0	<0.01		
			120381	sludge	80.0	90.0	<0.01		
			120382	sludge	90.0	100.0	0.03		
91.8-97.0	quartz vein	91.8-97.0	10.0						
97.0-97.3	fault								
		97.0-100.0	4.0						
			120383	sludge	100.0	110.0	0.03		
			4682	core	101.9	105.5	0.07	0.002	3.6
102.0-104.0	quartz vein	102.0-104.0	10.0						
		104.0-121.6	1.0						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
121.6-157.0	Graphitic Pelite and Arenite thin to medium layering	2.0	120384	sludge	110.0	120.0	<0.01		
			120385	sludge	120.0	130.0	<0.01		
			120386	sludge	130.0	140.0	0.02		
			120387	sludge	140.0	150.0	0.02		
			120388	sludge	150.0	160.0	<0.01		
145.0-150.0	silicified								
145.0-150.0	quartz vein								
154.0-155.0	fault								
157.0-176.0	Arenite medium layering	2.0							
			120389	sludge	160.0	170.0	<0.01		
			120390	sludge	170.0	180.0	<0.01		
			4683	core	171.8	175.3	0.01	<0.001	3.5
172.0-174.0	strongly sericitized								
176.0-215.0	Pelite and Arenite thin layering	1.0							
			120391	sludge	180.0	190.0	<0.01		
			120392	sludge	190.0	200.0	<0.01		
			4684	core	200.0	203.5	0.01	<0.001	3.5
			120393	sludge	200.0	210.0	<0.01		
			4685	core	203.5	208.0	0.01	<0.001	4.5
201.0-204.0	quartz vein								
205.5-206.5	quartz vein								
208.5-210.0	strongly sericitized								
215.0-237.0	Arenite and Pelite medium layering		120394	sludge	210.0	220.0	0.02		

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
237.0-245.0	Graphitic Pelite and Arenite thin to medium layering	3.0	120395	sludge	220.0	230.0	<0.01		
			120396	sludge	230.0	240.0	0.02		
244.0-245.0	fault								
245.0-256.0	Arenite and Pelite medium to thin layering	2.0	120397	sludge	240.0	250.0	0.11		
245.0-256.0	strongly sericitized								
256.0-268.0	Graphitic Pelite and Arenite thin to medium layering	6.0	120398	sludge	250.0	260.0	0.09		
268.0-282.0	Arenite and Pelite medium layering	2.0	4689	core	255.0	260.0	0.03	0.001	5.0
			120399	sludge	260.0	270.0	7.10		
			4690	core	260.0	265.0	0.02	0.001	5.0
268.0-282.0	strongly sericitized								
282.0-310.0	Graphitic Pelite thin layering	7.0	4691	core	265.0	270.0	0.07	0.002	5.0
			120400	sludge	270.0	280.0	2.87		
			4692	core	270.0	275.0	<0.01	<0.001	5.0
309.0-315.0	fault		4693	core	275.0	280.0	<0.01	<0.001	5.0
			120401	sludge	280.0	290.0	0.47		
			4694	core	280.0	285.0	0.03	0.001	5.0
310.0-374.0	Arenite medium layering	2.0	120402	sludge	290.0	300.0	0.16		
			120403	sludge	300.0	310.0	0.23		
			120404	sludge	310.0	320.0	0.08		

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
355.0-356.0	quartz stringers		120405	sludge	320.0	330.0	0.06		
			120406	sludge	330.0	340.0	0.04		
			120407	sludge	340.0	350.0	0.07		
			120408	sludge	350.0	360.0	0.05		
			120409	sludge	360.0	370.0	0.04		
374.0-424.0	Graphitic Pelite thin layering	3.0	120410	sludge	370.0	380.0	0.04		
			120411	sludge	380.0	390.0	0.03		
			120412	sludge	390.0	400.0	0.04		
			120413	sludge	400.0	410.0	0.03		
			120414	sludge	410.0	420.0	0.04		
424.0-690.0	Arenite and Pelite medium layering		120415	sludge	420.0	430.0	0.05		
			120416	sludge	430.0	440.0	0.06		
			120417	sludge	440.0	450.0	0.03		
			120418	sludge	450.0	460.0	0.03		
			120419	sludge	460.0	470.0	0.03		
			120420	sludge	470.0	480.0	0.02		
			120421	sludge	480.0	490.0	0.02		
			120422	sludge	490.0	500.0	0.03		
			120423	sludge	500.0	510.0	0.03		
			120424	sludge	510.0	520.0	0.03		
			120425	sludge	520.0	530.0	0.03		
			120426	sludge	530.0	540.0	0.03		
536.5-540.0	quartz stringers		120427	sludge	540.0	550.0	0.04		
			120428	sludge	550.0	560.0	0.05		
554.0-556.0	quartz stringers								
557.0-566.0	quartz stringers								
566.0-570.0	strongly sericitized		120429	sludge	560.0	570.0	0.03		

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
566.0-570.0		10.0							
			4686	core	566.0	569.5	0.01	<0.001	3.5
570.0-641.0		1.0							
			120430	sludge	570.0	580.0	0.03		
574.0-516.0	fault								
576.0-578.0	silicified								
578.0-592.0	quartz stringers								
			120431	sludge	580.0	590.0	0.02		
582.0-620.0	chloritized								
			120432	sludge	590.0	600.0	0.01		
			120433	sludge	600.0	610.0	0.02		
			120434	sludge	610.0	620.0	0.03		
620.0-635.0	strongly sericitized								
			120435	sludge	620.0	630.0	0.03		
			4687	core	626.0	630.0	0.01	<0.001	4.0
			120436	sludge	630.0	640.0	0.03		
635.0-641.0	chloritized								
			120437	sludge	640.0	650.0	0.73		
641.0-646.0	strongly sericitized								
		3.0							
			4688	core	642.0	646.8	0.01	<0.001	4.8
646.0-690.0	chloritized								
			120438	sludge	650.0	660.0	0.03		
655.0-670.0	quartz stringers								
			120439	sludge	660.0	670.0	0.03		
			120440	sludge	670.0	680.0	0.03		
678.0-690.0	quartz stringers								
			120441	sludge	680.0	690.0	0.03		
690.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. WT01-01

Property: Wells Trend
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: July 25, 2001
 Date Completed: August 1, 2001
 Final Depth: 475 feet (144.8 m)

Collar Grid Coordinates
 Northing Easting Elevation
 Mine Grid 3925.0 ft. 13085.0 ft. 4794.0 ft.

Logged by: J. Kowalchuk

Depth	Azimuth	Dip
collar	218°	-45°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-15.0	Overburden								
15.0-54.0	Graphitic Pelite and Arenite very thin to thin layering								
		15.0-54.0	1.0						
28.5-43.0	fault								
30.0-75.0	quartz stringers, both parallel and orthogonal to the lineation								
45.5-46.5	fault								
54.0-183.5	Dolomite Porphyroblastic Arenite thin to very thin layering								
54.0-75.0	strongly sericitized and moderately dolomitized								
		54.0-62.0	2.0						
54.5-62.0	fault		6321	core	54.2	59.2	0.06	0.002	5.0
			6322	core	59.2	64.2	0.21	0.006	5.0
		62.0-77.6	0.5						
75.0-88.0	strongly dolomitized and moderately sericitized								
77.6-78.8	quartz vein parallel to the lineation								
		77.6-78.8	3.0						
			6323	core	77.6	78.8	0.72	0.021	1.2
78.8-88.0	quartz stringers parallel to the lineation								
78.8-79.5	fault								
		78.8-88.0	2.0						

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
87.5-93.5	fault		6324	core	85.8	90.8	0.08	0.002	5.0
88.0-100.0	quartz vein parallel to the lineation								
		5.0							
			6325	core	90.8	95.8	0.05	0.001	5.0
			6326	core	95.8	100.8	0.12	0.004	5.0
100.0-117.3	strongly sericitized and moderately dolomitized								
100.0-118.0	quartz stringers and calcite stringers parallel to the lineation								
		2.0							
			6327	core	100.8	105.8	0.01	0.000	5.0
			6328	core	105.8	110.8	0.01	0.000	5.0
			6329	core	110.8	115.8	0.01	0.000	5.0
117.3-133.0	strongly dolomitized and moderately sericitized								
		0.1							
120.4-121.0	quartz-calcite vein parallel to the lineation								
125.0-131.0	quartz stringers and calcite stringers, both parallel and orthogonal to the lineation								
133.0-136.0	strongly sericitized and moderately dolomitized								
		0.1							
136.0-183.5	strongly dolomitized and moderately sericitized								
		0.5							
138.5-183.5	quartz stringers and calcite stringers, both parallel and orthogonal to the lineation								
140.0-145.0	fault								
158.6-159.0	fault								
160.9-161.4	fault								
178.0-190.0	fault								
		1.0							
183.5-211.0	Graphitic Arenite and Pelite thin to very thin layering								
		5.0							
197.3-198.4	quartz-calcite vein orthogonal to the lineation								
199.2-199.6	quartz-calcite vein orthogonal to the lineation								
211.0-217.6	Arenite thin layering								
211.0-217.6	strongly sericitized								
		4.0							
			6330	core	211.0	217.8	0.57	0.017	6.8

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
214.0-215.0	quartz vein parallel to the lineation								
214.0-217.6	fault								
217.6-295.0	Graphitic Arenite and Pelite								
	very thin to thin layering								
227.2-234.0	quartz vein orthogonal to the lineation								
		227.6-234.0	0.1						
233.0-234.0	fault								
		234.0-295.0	4.0						
244.0-245.0	quartz vein parallel to the lineation								
244.0-246.0	fault								
285.0-294.0	quartz stringers and calcite stringers orthogonal to the lineation								
295.0-337.7	Chlorite, Dolomite Porphyroblastic Arenite and Pelite								
	thin to very thin layering								
295.0-301.0	chloritized and moderately dolomitized								
		295.0-302.0	2.0						
			6331	core	295.0	301.5	0.21	0.006	6.5
301.0-337.5	strongly dolomitized and moderately chloritized								
		302.0-337.0	0.5						
305.5-306.5	fault								
316.0-318.0	quartz stringers and calcite stringers diagonal to the lineation								
330.0-338.0	quartz stringers and calcite stringers diagonal to the lineation								
		337.0-345.0	4.0						
337.7-345.0	Graphitic, Calcareous Arenite and Grit ,								
	thin to medium layering								
345.0-363.6	Calcareous, Graphitic, Chlorite-bearing Grit and Arenite								
	thick layering								
345.0-363.0	quartz stringers and calcite stringers parallel to the lineation								
		345.0-363.0	0.1						
		363.0-475.0	4.0						
363.6-385.5	Graphitic, Calcareous Arenite								
	thin layering								

D.D.H. WT01-01

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From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
385.5-387.5	Calcareous, Graphitic Grit thick layering								
387.5-475.0	Graphitic, Calcareous Arenite and Grit medium to thick layering								
475.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. WT01-03

Property: Wells Trend
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: August 24, 2001
 Date Completed: August 31, 2001
 Final Depth: 745 feet (227.1 m)

Collar Grid Coordinates
 Northing Easting Elevation
 Mine Grid 4228.0 ft. 12497.0 ft. 4801.0 ft.

Logged by: D. Hladky

Depth	Azimuth	Dip
collar	223°	-45°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-10.0	Overburden								
10.0-236.7	Graphitic Pelite and Arenite very thin to thin layering								
19.8-20.6	quartz stringers orthogonal to the lineation								
20.6-20.9	quartz vein parallel to the lineation								
20.9-21.7	quartz stringers								
24.2-27.7	quartz stringers								
32.3-35.2	quartz stringers								
35.2-35.6	quartz vein								
35.6-36.5	quartz stringers								
44.6-44.9	fault								
53.5-53.6	fault								
84.8-88.9	quartz stringers								
108.8-112.4	quartz stringers								
125.9-126.3	quartz stringers								
132.4-133.1	quartz vein								
133.4-133.5	fault								
134.8-134.9	fault								
138.3-139.3	quartz vein								
139.3-144.5	quartz stringers								
144.5-145.3	quartz vein								
145.3-150.9	quartz stringers								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
150.9-151.3	quartz vein								
153.1-155.8	quartz stringers								
155.8-157.3	quartz vein								
		155.8-156.0	10.0						
		156.0-228.6	1.5						
157.3-166.2	quartz stringers								
168.9-171.9	quartz stringers								
169.3-169.6	fault								
171.0-171.2	fault								
173.8-174.1	fault								
175.5-176.2	quartz stringers								
176.2-176.8	quartz vein								
176.8-180.0	quartz stringers								
180.0-180.4	quartz vein								
180.4-201.1	quartz stringers								
202.1-202.7	quartz vein								
203.6-205.0	quartz stringers								
205.0-205.5	quartz vein								
209.9-228.6	quartz stringers								
228.6-228.7	quartz vein								
		228.6-228.7	8.0						
228.7-230.9	quartz stringers								
		228.7-338.0	1.5						
230.9-231.7	quartz vein								
230.9-231.0	fault								
231.7-234.8	quartz stringers								
235.4-236.2	quartz vein								
236.2-242.3	quartz stringers								
236.7-506.2	Graphitic, Dolomite Porphyroblastic Pelite, Arenite and Grit								
	very thin to thin layering								
242.3-242.6	quartz vein								
242.6-254.5	quartz stringers								
252.6-253.3	fault								
254.5-255.0	quartz vein								
255.0-262.7	quartz stringers								
262.7-262.9	quartz vein								
262.9-264.7	quartz stringers								

D.D.H. WT01-03

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From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
264.7-265.9	quartz stringers								
265.9-268.2	quartz stringers								
267.1-267.4	fault								
290.3-291.5	quartz vein								
301.8-303.8	quartz stringers								
338.0-338.5	quartz vein								
		338.0-338.5	6.0						
338.5-340.3	quartz stringers								
		338.5-375.0	0.5						
355.3-355.8	quartz vein								
364.7-366.5	quartz vein								
367.1-375.0	quartz stringers								
367.1-384.7	fault								
		375.0-384.7	1.5						
384.5-393.1	quartz stringers								
		384.7-406.3	1.0						
393.1-395.0	quartz vein								
395.0-403.9	quartz stringers								
406.3-410.6	strongly silicified and moderately dolomitized								
		406.3-422.7	0.5						
410.6-411.0	carbonized								
410.6-411.0	fault								
411.0-430.3	strongly silicified and moderately dolomitized								
417.4-419.0	quartz stringers								
421.4-422.7	quartz stringers								
422.7-430.3	quartz vein								
		422.7-430.3	15.0						
			4001	core	422.7	426.5	1.29	0.038	3.8
			4002	core	426.5	430.3	4.76	0.139	3.8
430.3-435.2	quartz stringers								
		430.3-434.2	2.5						
			4003	core	430.3	433.7	0.25	0.007	3.4
433.7-438.7	strongly silicified, moderately dolomitized and slightly sericitized								
		434.2-455.0	1.0						
437.2-440.4	quartz stringers								
438.7-454.1	strongly silicified and moderately dolomitized								
449.2-452.4	quartz stringers								
454.1-484.6	strongly silicified, moderately dolomitized and slightly chloritized								

D.D.H. WT01-03

Page 4 of 6

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
		455.0-460.0	2.0						
455.4-469.0	quartz stringers								
		460.0-481.6	1.0						
472.5-478.1	quartz stringers								
	pyrrhotite and lesser pyrite	481.6-496.0	1.0						
484.1-485.0	quartz vein								
484.6-491.5	strongly silicified and moderately dolomitized								
485.0-491.0	quartz stringers								
491.0-496.0	quartz stringers								
491.5-494.9	strongly silicified								
494.9-496.0	chloritized, moderately silicified, slightly dolomitized and sericitized								
496.0-528.3	quartz stringers								
		496.0-651.0	0.5						
505.0-506.2	fault								
506.2-611.3	Graphitic Pelite, Conglomerate, Arenite and Grit								
	very thin to thin layering								
526.9-528.2	fault								
530.1-534.0	moderately dolomitized								
531.7-533.9	quartz stringers								
565.0-573.8	quartz stringers								
593.5-611.3	quartz stringers								
611.3-612.2	Chlorite-bearing Pelite and Arenite								
	very thin to thin layering								
611.3-612.2	chloritized and moderately dolomitized								
612.2-612.3	Graphitic Pelite, Conglomerate and Arenite								
612.3-613.4	Calcareous Arenite and Pelite								
	very thin to thin layering								
	very thin to thin layering								
613.4-651.0	Chlorite-bearing Pelite and Arenite								
	very thin to thin layering								
613.4-613.6	strongly sericitized and moderately dolomitized								
613.6-693.7	chloritized and moderately dolomitized								
626.3-634.8	quartz and dolomite stringers								

D.D.H. WT01-03

Page 5 of 6

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
635.5-651.7	quartz stringers								
635.6-636.2	fault								
651.0-667.2	Magnetite- and Chlorite-bearing Pelite and Arenite thin to medium layering								
					651.0-667.2		1.5		
656.5-662.3	quartz stringers								
667.2-728.9	Chlorite-bearing Pelite and Arenite very thin to medium layering								
					667.2-742.3		0.5		
668.0-668.4	fault								
676.5-677.4	quartz stringers								
677.4-677.6	quartz stringers								
679.3-680.0	quartz stringers								
689.0-689.3	quartz stringers								
693.1-693.7	fault								
693.7-728.9	chloritized, moderately dolomitized and slightly silicified								
704.7-716.3	quartz stringers								
707.2-707.7	fault								
709.9-712.6	Fault Zone								
713.6-714.6	fault								
716.9-717.3	Fault Zone								
720.2-720.6	fault								
721.9-722.3	quartz stringers								
727.9-741.5	quartz stringers								
728.9-735.1	Graphitic Pelite and Arenite very thin to thin layering								
728.9-730.8	strongly silicified, moderately chloritized and slightly dolomitized								
735.1-741.5	Graphitic Arenite and Pelite								
734.9-735.1	fault								
	very thin to thin layering								
741.5-745.0	Graphitic Grit, Pelite and Arenite thin to very thin layering								
741.5-742.0	strongly sericitized and moderately silicified								

D.D.H. WT01-03

Page 6 of 6

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
741.5-745.0	quartz stringers								
741.5-742.3	fault								
		742.3-744.7	1.5						
			4004	core	744.0	745.0	0.01	0.000	1.0
744.5-745.0	strongly sericitized and moderately silicified								
		744.7-745.0	8.0						
745.0	E.O.H.								

International Wayside Gold Mines Ltd.

Diamond Drill Log

D.D.H. WT01-02

Property: Wells Trend
 Drilling Contractor: Standard Drilling & Engineering Ltd.
 Date Started: August 3, 2001
 Date Completed: August 17, 2001
 Final Depth: 925 feet (281.9 m)

Collar Grid Coordinates
 Northing Easting Elevation
 Mine Grid 4199.0 ft. 13777.0 ft. 4655.0 ft.

Logged by: J. Kowalchuk

Depth	Azimuth	Dip
collar	214°	-45°

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
0.0-10.0	Overburden								
10.0-248.0	Graphitic, Chlorite-bearing Arenite and Grit thin to very thin layering								
		10.0-248.0	4.0						
77.0-81.0	fault								
80.0-81.0	quartz vein diagonal to the lineation								
156.0-156.1	quartz stringers diagonal to the lineation								
176.0-190.0	quartz stringers diagonal to the lineation								
196.0-203.0	quartz stringers diagonal to the lineation								
215.0-225.0	fault								
246.0-246.2	fault								
246.2-255.6	quartz stringers diagonal to the lineation								
248.0-297.0	Chlorite, Dolomite Porphyroblastic Arenite thin layering								
248.0-262.0	strongly sericitized and moderately chloritized								
		248.0-256.7	2.0						
256.7-259.0	quartz vein parallel to the lineation		6391	core	256.0	260.1	0.09	0.003	4.1
		256.7-259.0	2.0						
	pyrrhotite and lesser pyrite	259.0-297.0	2.0						
259.4-262.7	quartz stringers parallel to the lineation								
266.0-267.3	strongly sericitized								

D.D.H. WT01-02

Page 2 of 5

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
267.3-282.6	strongly sericitized and moderately chloritized								
283.0-289.3	strongly sericitized and moderately dolomitized								
289.3-297.0	chloritized and moderately sericitized								
297.0-367.0	Arenite								
	thin layering								
297.0-325.0	strongly sericitized and moderately dolomitized								
	pyrrhotite	2.0							
325.0-332.0	strongly dolomitized and moderately sericitized								
	pyrrhotite and lesser pyrite	1.0							
325.7-329.2	quartz stringers and calcite stringers diagonal to the lineation								
			6392	core	326.2	326.9	0.01	0.000	0.7
			6393	core	329.0	329.6	0.03	0.001	0.6
332.0-334.5	strongly sericitized and moderately dolomitized								
334.5-367.0	strongly dolomitized, moderately chloritized and slightly sericitized								
347.0-347.2	fault								
367.0-392.1	Graphitic, Calcareous Arenite and Pelite								
	thin to very thin layering								
					369.0-392.1				
384.0-385.1	fault								
392.1-445.0	Dolomite Porphyroblastic Arenite								
	medium layering								
392.0-477.6	strongly dolomitized								
					392.1-445.0				
406.0-406.2	fault								
445.0-453.6	Dolomite Porphyroblastic Arenite								
	medium layering								
					445.0-447.2				
	pyrrhotite and lesser pyrite	5.0			447.2-449.2				
447.7-449.2	quartz-calcite vein parallel to the lineation								
			6394	core	447.7	449.5	22.83	0.666	1.8
					449.2-453.6				
453.0-453.9	fault								

From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
453.6-477.6	Dolomite Porphyroblastic Arenite medium layering								
		453.6-477.6	0.1						
477.6-491.5	Graphitic Arenite and Pelite thin to very thin layering								
		477.6-491.5	0.1						
491.5-569.0	Graphitic, Calcareous Arenite and Pelite thin to very thin layering								
		491.5-569.0	5.0						
495.0-528.0	quartz stringers and calcite stringers diagonal to the lineation								
569.0-574.0	Dolomite Porphyroblastic Pelite thick layering								
		569.0-630.1	2.0						
574.0-583.0	Calcareous, Dolomite Porphyroblastic Arenite thin layering								
574.0-630.1	calcite stringers parallel to the lineation								
583.0-584.2	Graphitic Arenite and Pelite thin to very thin layering								
584.2-587.5	Calcareous, Dolomite Porphyroblastic Arenite thin layering								
		6395	core		585.0	590.0	0.01	0.000	5.0
587.5-588.2	Graphitic Arenite and Pelite thin to very thin layering								
588.2-589.0	Calcareous, Dolomite Porphyroblastic Arenite thin layering								
589.0-592.0	Graphitic Arenite and Pelite thin to very thin layering								
		6396	core		590.0	595.0	0.01	0.000	5.0

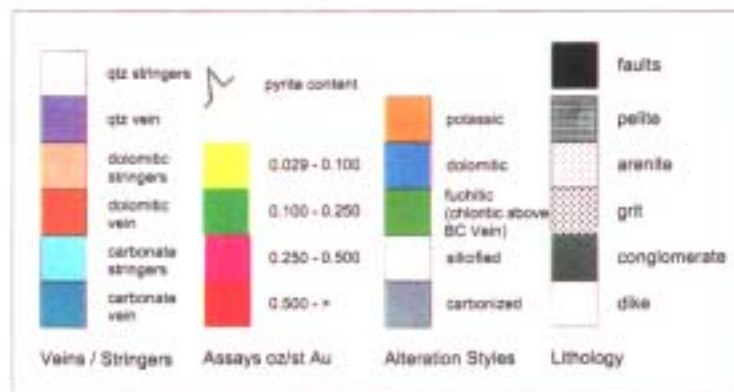
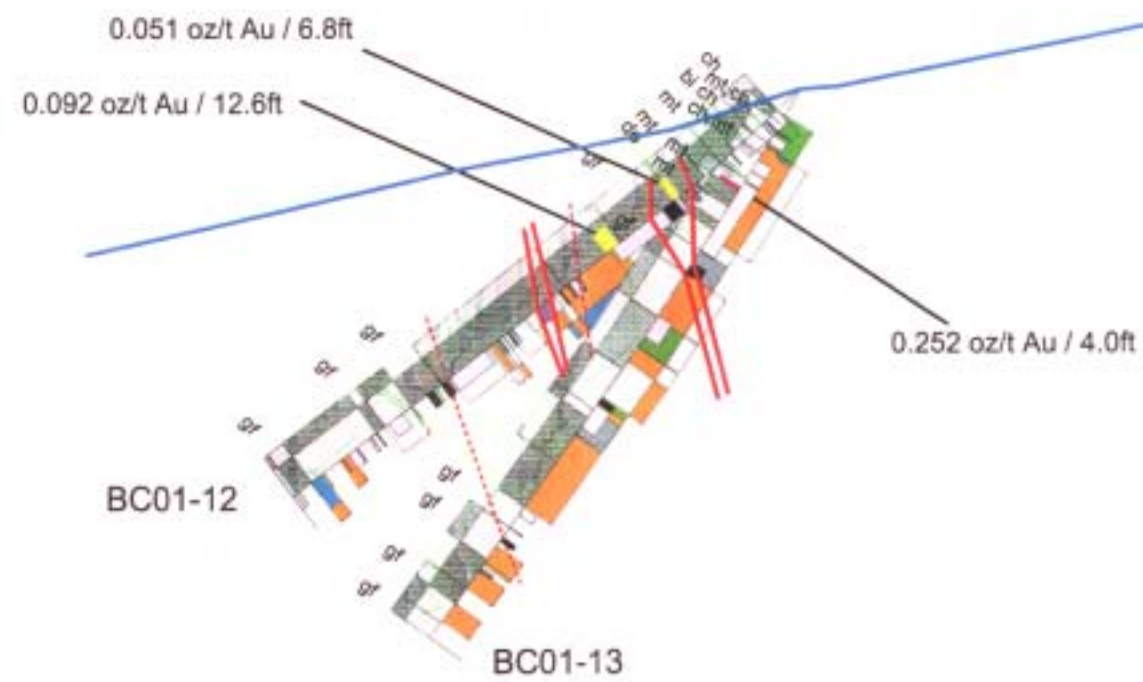
From-To (ft)	Description	% sulph	Sample No.	Type	From (ft)	To (ft)	Au g/t	Au oz./ton	Length ft.
592.0-630.0	Calcareous, Dolomite Porphyroblastic Arenite thin layering								
600.0-601.0	calcite vein parallel to the lineation								
630.0-666.8	Dolomite Porphyroblastic Arenite and Pelite thick layering								
		630.1-666.8	2.0						
			6397	core	635.0	640.0	0.06	0.002	5.0
636.1-666.8	strongly sericitized								
			6398	core	640.0	645.0	0.03	0.001	5.0
			6399	core	645.0	650.0	0.02	0.001	5.0
660.0-677.6	calcite stringers, both parallel and diagonal to the lineation								
666.8-677.6	Calcareous Arenite thin layering								
		666.8-677.6	0.5						
677.6-730.0	Dolomite Porphyroblastic Arenite and Pelite thick layering								
677.6-705.0	strongly sericitized								
		677.6-705.0	1.5						
			6400	core	677.6	680.2	0.02	0.001	2.6
695.0-697.0	calcite stringers diagonal to the lineation								
698.3-700.4	calcite vein diagonal to the lineation								
		705.0-730.0	0.1						
730.0-752.0	Calcareous, Chlorite-bearing Arenite t-thick layering								
730.0-752.0	chloritized								
730.0-758.5	calcite stringers parallel to the lineation								
		730.0-752.0	3.0						
752.0-758.3	Dolomite Porphyroblastic, Calcareous Pelite and Arenite thick layering								
		752.0-758.3	2.0						
758.3-802.8	Calcareous, Mariposite-bearing Arenite thin layering								

APPENDIX 2 – CROSS SECTIONS

5000 ft Elev

2000 ft N

3000 ft N



4000 ft Elev

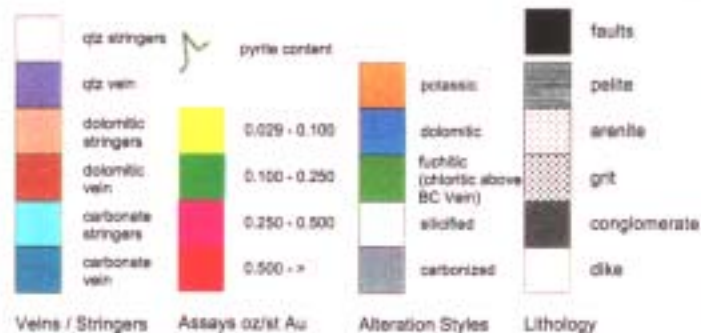
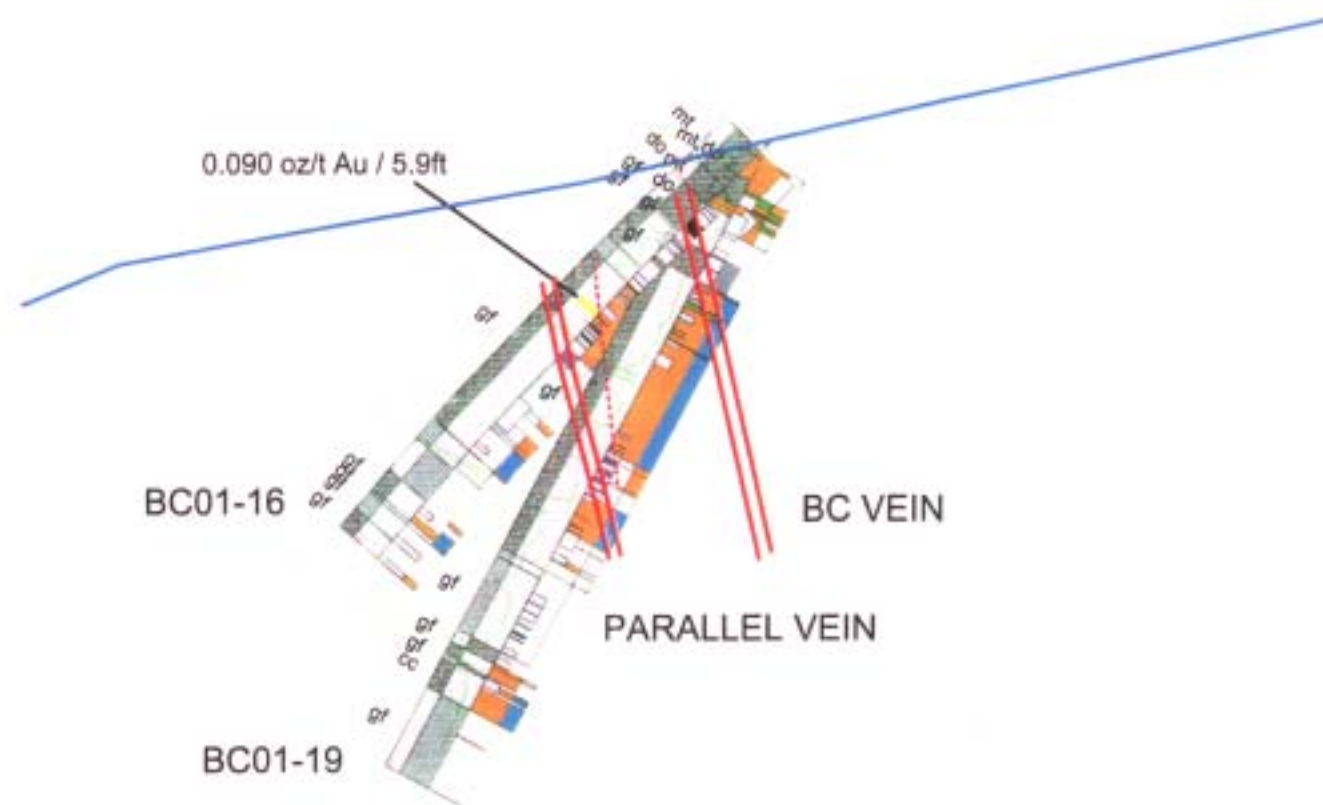
International Wayside Gold Mines Ltd.	
Date: 14/05/2000 Author: Ken Lord Officer: Mike BC Drawing: Scale: 1:1000 Projection: Non-Geoth (NAD)	CARIBOO GOLD PROJECT BC VEIN / BONANZA LEDGE DCH SECTION 21400 EAST FACING NORTHWEST IMPERIAL SCALE 1:150

26906

5000 ft Elev

2000 ft N

3000 ft N



4000 ft Elev

26906

International Wayside Gold Mines Ltd.	
Date: 14/01/2002	CARIBOO GOLD PROJECT
Author: Stan Lord	BC VEIN / BONANZA LEDGE
Office: Wye BC	DDH SECTION 21300 EAST
Drawing:	FACING NORTHWEST
Scale: 1:150	IMPERIAL SCALE 1:150
Projection: Transverse Mercator	

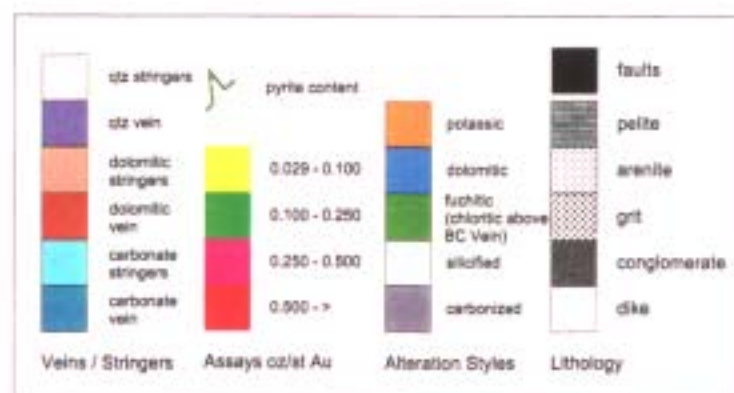
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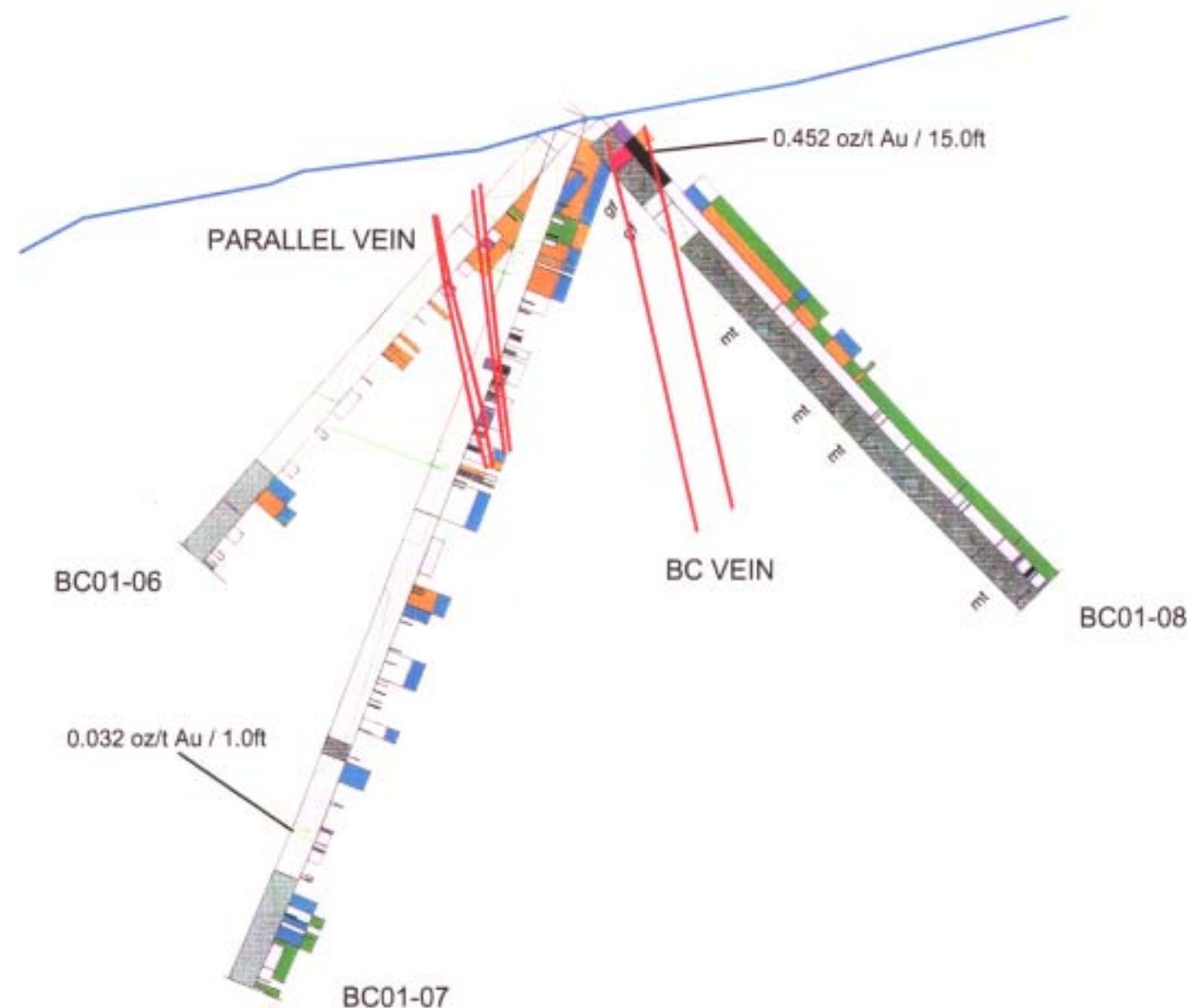
5000 ft Elev

2000 ft N

3000 ft N



4000 ft Elev



26906

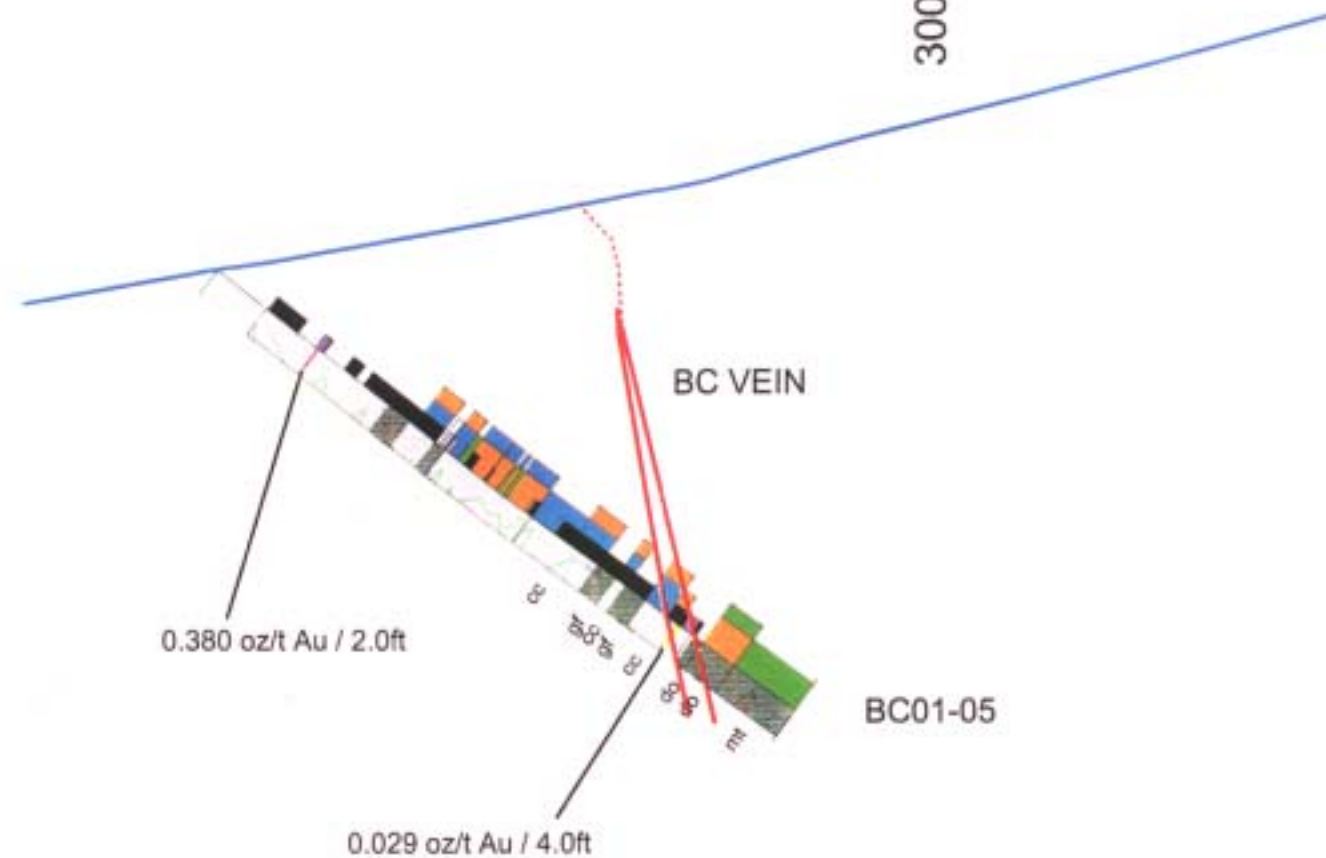
International Wayside Gold Mines Ltd.	
Date: 1/18/2005	CARIBOO GOLD PROJECT
Author: Kim Lott	BC VEIN / BONANZA LEDGE
Client: Wayside BC	DDH SECTION 21000 EAST
Drawing:	FACING NORTHWEST
Scale: 1:150	IMPERIAL SCALE 1:150
Projection: Non-South (West)	

0 20 40 80
meters

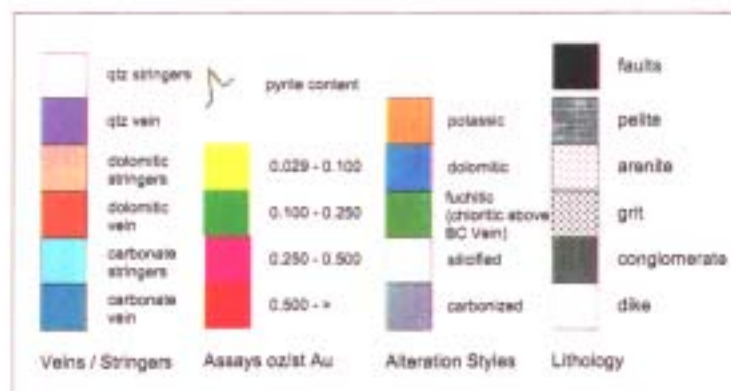
5000 ft Elev

2000 ft N

3000 ft N



4000 ft Elev



26906

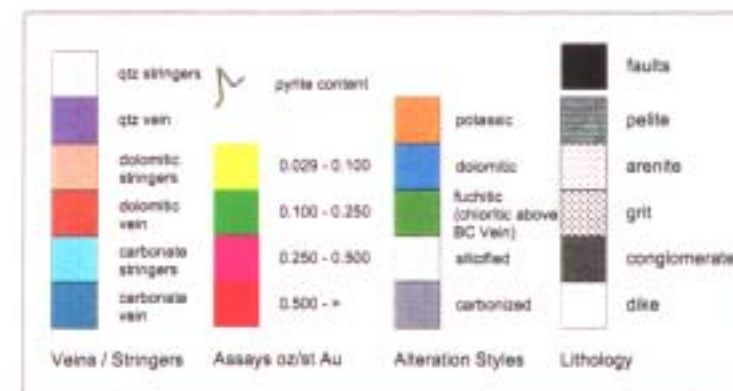
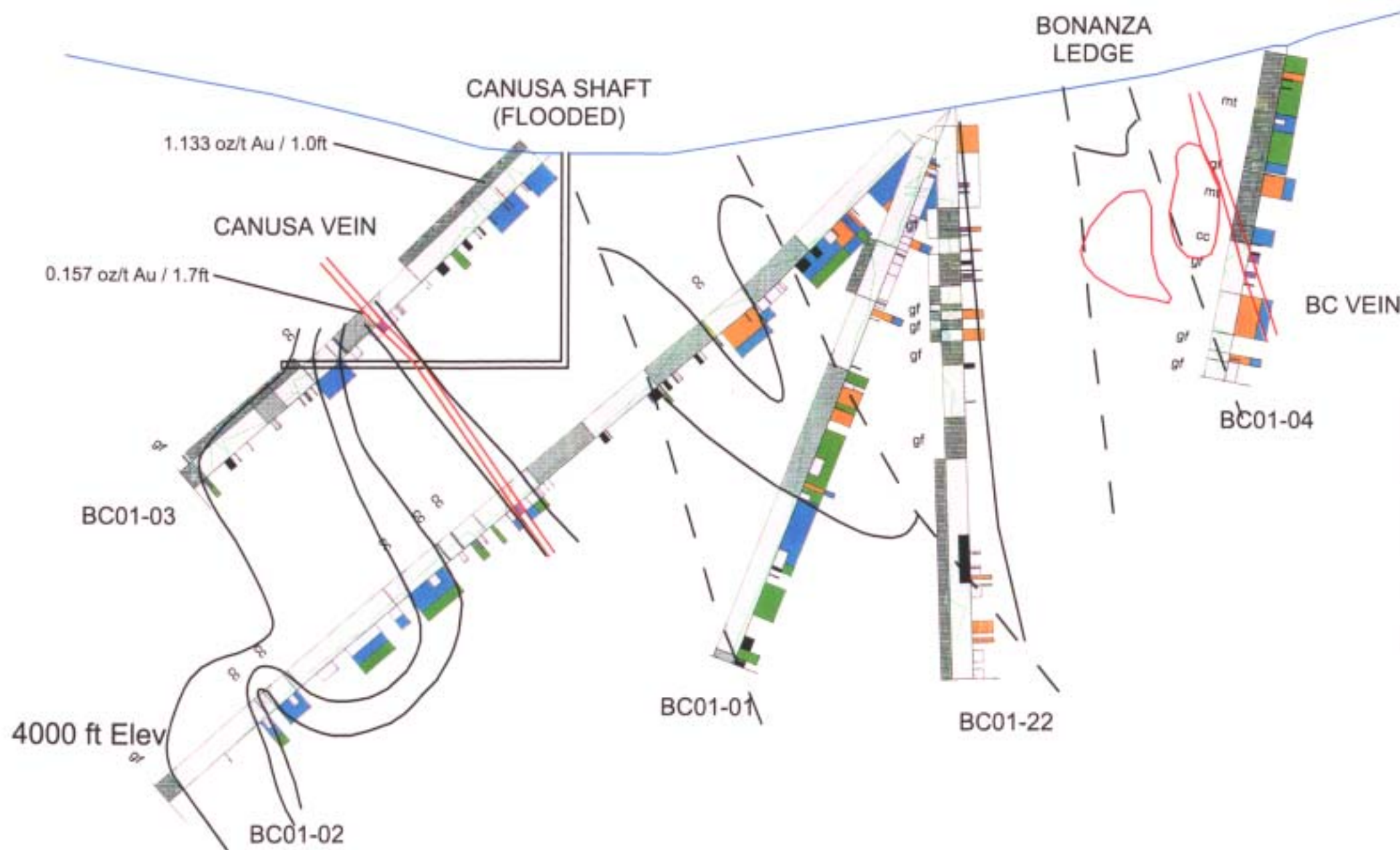
International Wayside Gold Mines Ltd.	
Date: 14/03/2011	CARIBOO GOLD PROJECT BC VEIN / BONANZA LEDGE DDH SECTION 20500 EAST FACING NORTHWEST IMPERIAL SCALE 1:150
Author: Neil Laid	
Office: Wye BC	
Drawing:	
Scale: 1:1500	Projection: North (NAD 83)

0 20 40 60
metres

5000 ft Elev

2000 ft N

3000 ft N



26906 (M)

International Wayside Gold Mines Ltd.

CARIBOO GOLD PROJECT
BC VEIN / BONANZA LEDGE
DDH SECTION 20200 EAST
FACING NORTHWEST
IMPERIAL SCALE 1:150

0 20 40 80
metres

5000 ft Elev

2000 ft N

3000 ft N

BONANZA LEDGE

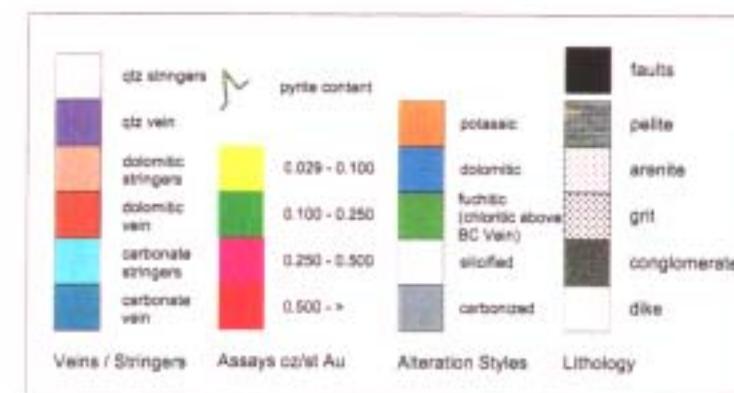
BC VEIN

0.213 oz/t Au / 25.0ft

0.096 oz/t Au / 65.3ft

BC01-11

BC01-09

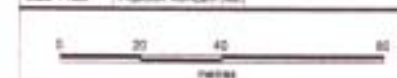


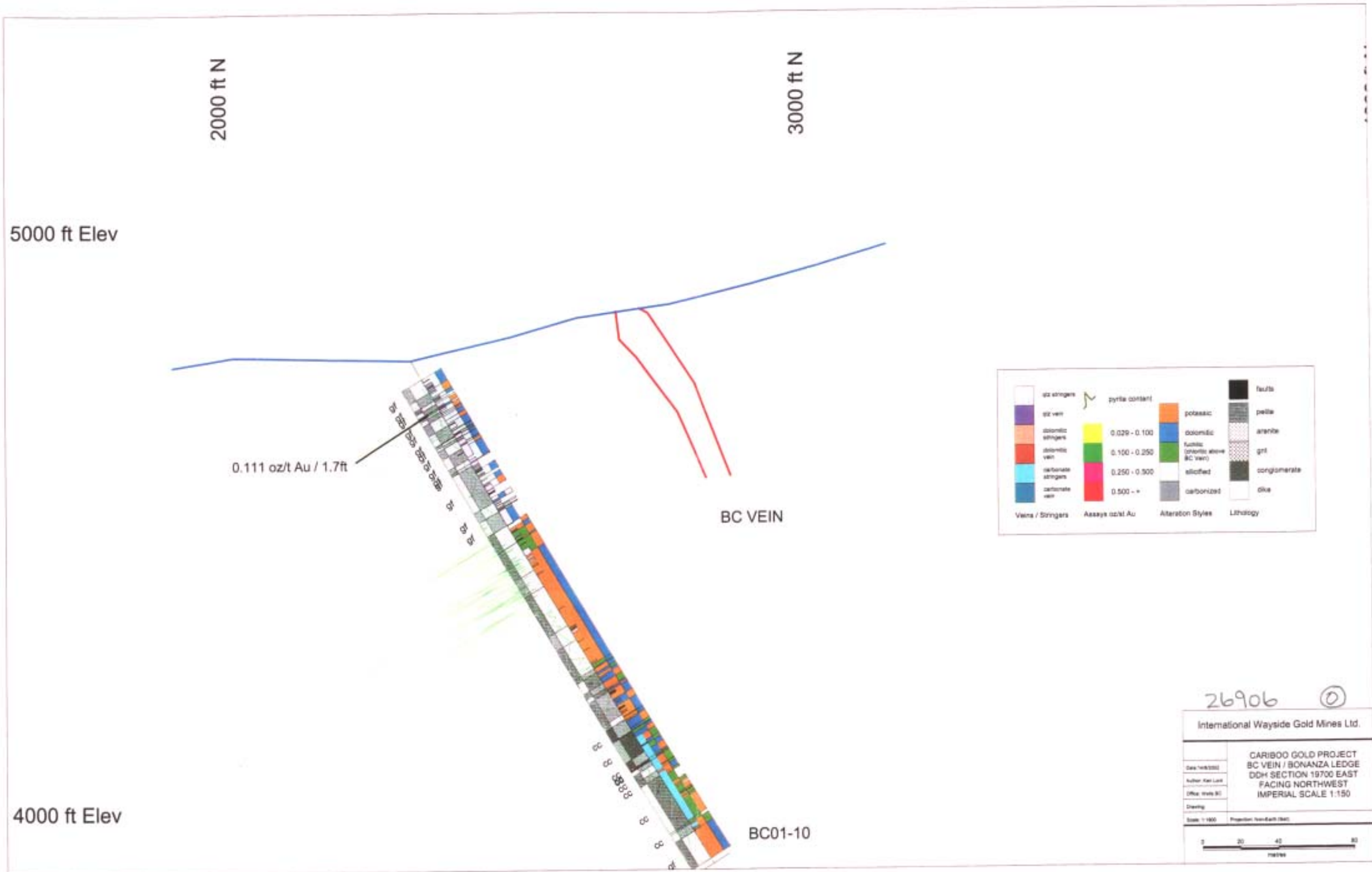
4000 ft Elev

26906 (N)

International Wayside Gold Mines Ltd.

CARIBOO GOLD PROJECT
BC VEIN / BONANZA LEDGE
DDH SECTION 20070 EAST
FACING NORTHWEST
IMPERIAL SCALE 1:150



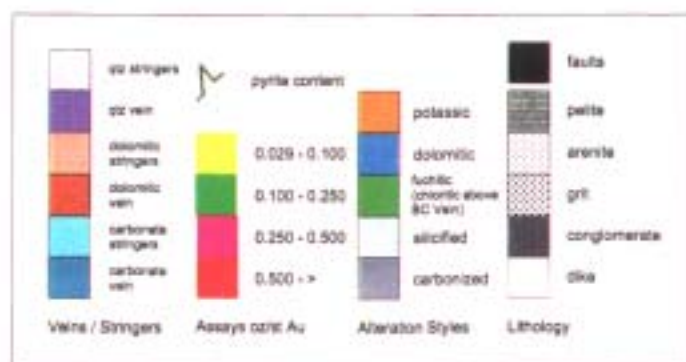
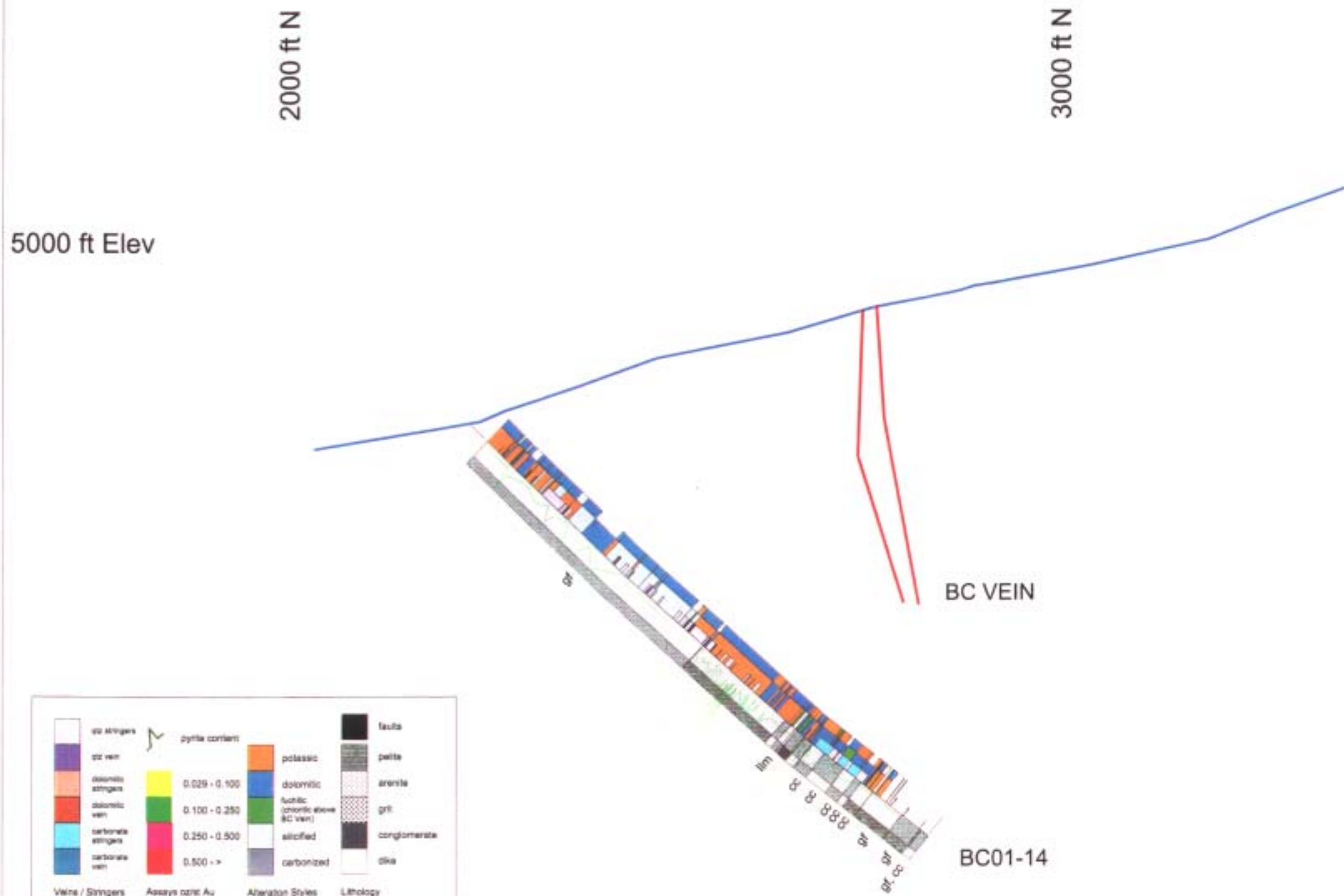


26906 ①

International Wayside Gold Mines Ltd.

Date: 10/1/2000	CARIBOO GOLD PROJECT BC VEIN / BONANZA LEDGE DDH SECTION 19700 EAST FACING NORTHWEST IMPERIAL SCALE 1:150
Author: Ken Lord	
Office: White BC	
Drawing	
Scale: 1:1500	Projection: North (NAD83)

0 20 40 80
metres



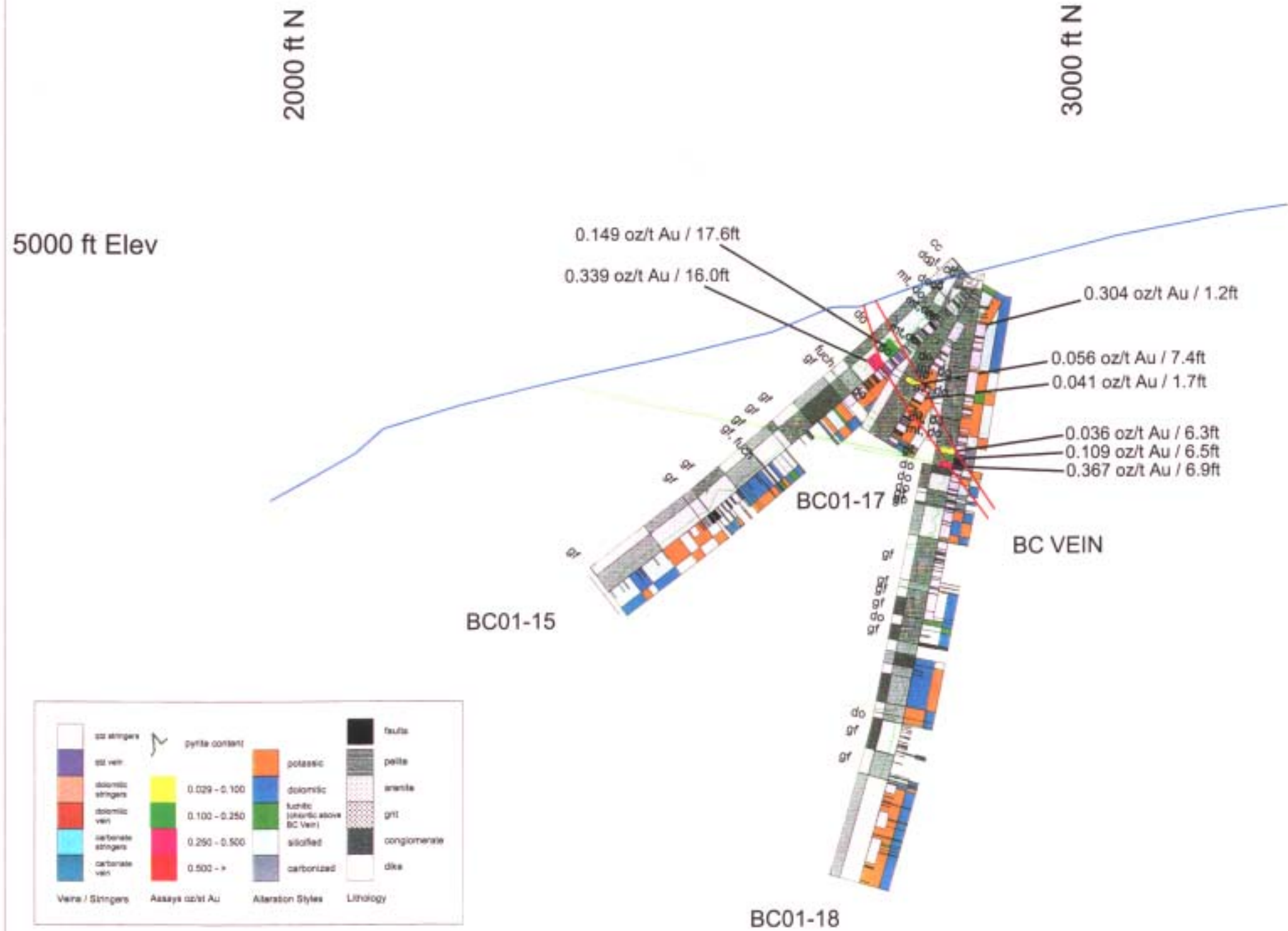
26906 (P)

International Wayside Gold Mines Ltd.

CARIBOO GOLD PROJECT
BC VEIN / BONANZA LEDGE
DDH SECTION 19300 EAST
FACING NORTHWEST
IMPERIAL SCALE 1:150

Scale 1:150 Projection Non-Earth (NAD)

0 20 40 80
metres



4000 ft Elev

26906 Q

International Wayside Gold Mines Ltd.

Date 14/03/00	CARIBOO GOLD PROJECT BC VEIN / BONANZA LEDGE DDH SECTION 18400 EAST FACING NORTHWEST IMPERIAL SCALE 1:150
Author Ken Lark	
Office Mike BC	
Drawing	
Scale 1:150	Projection North (True)

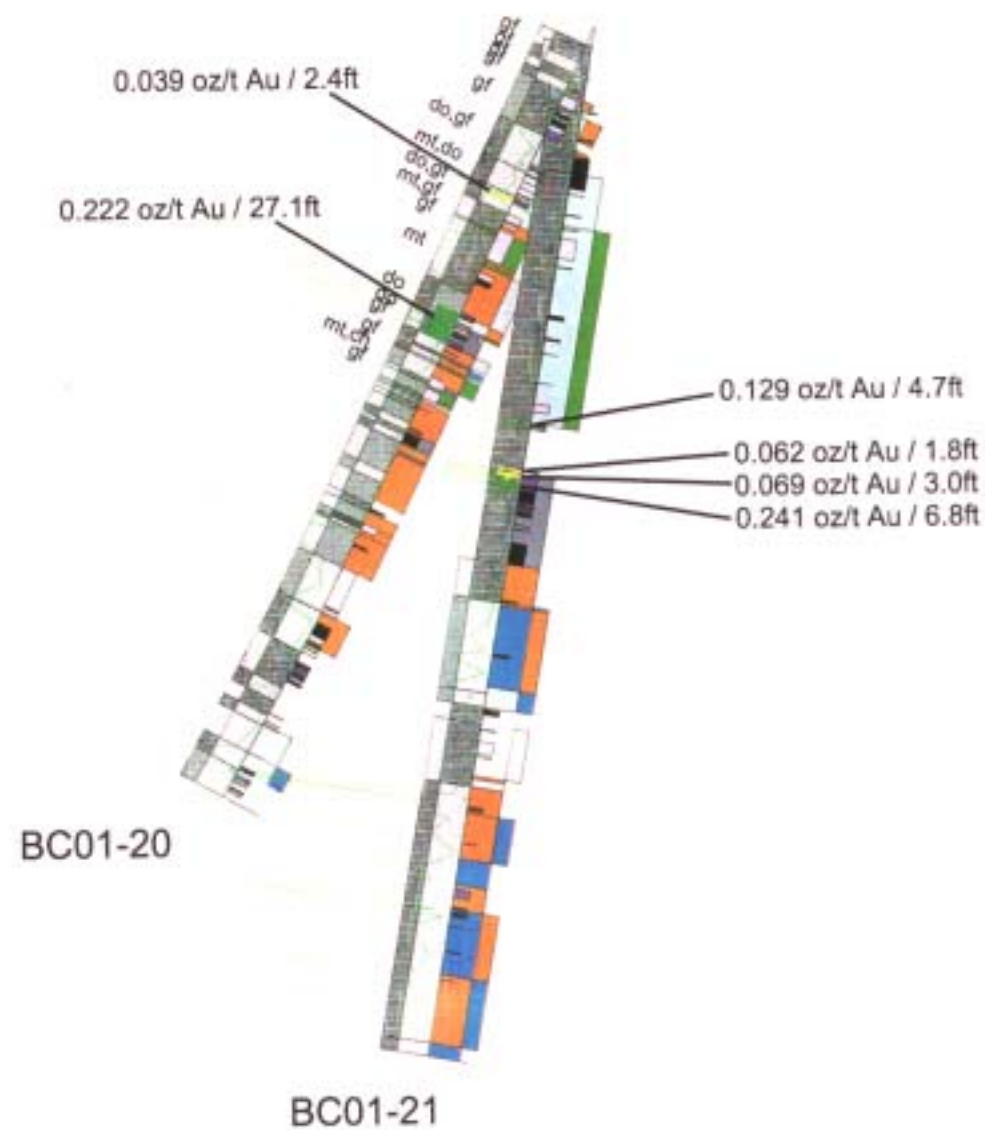
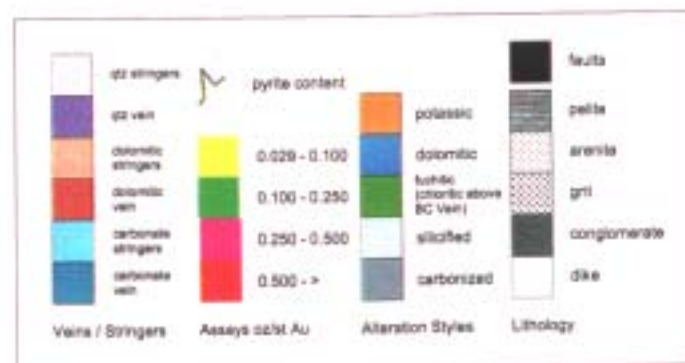
0 20 40 60
metres

5000 ft Elev

4000 ft Elev

2000 ft N

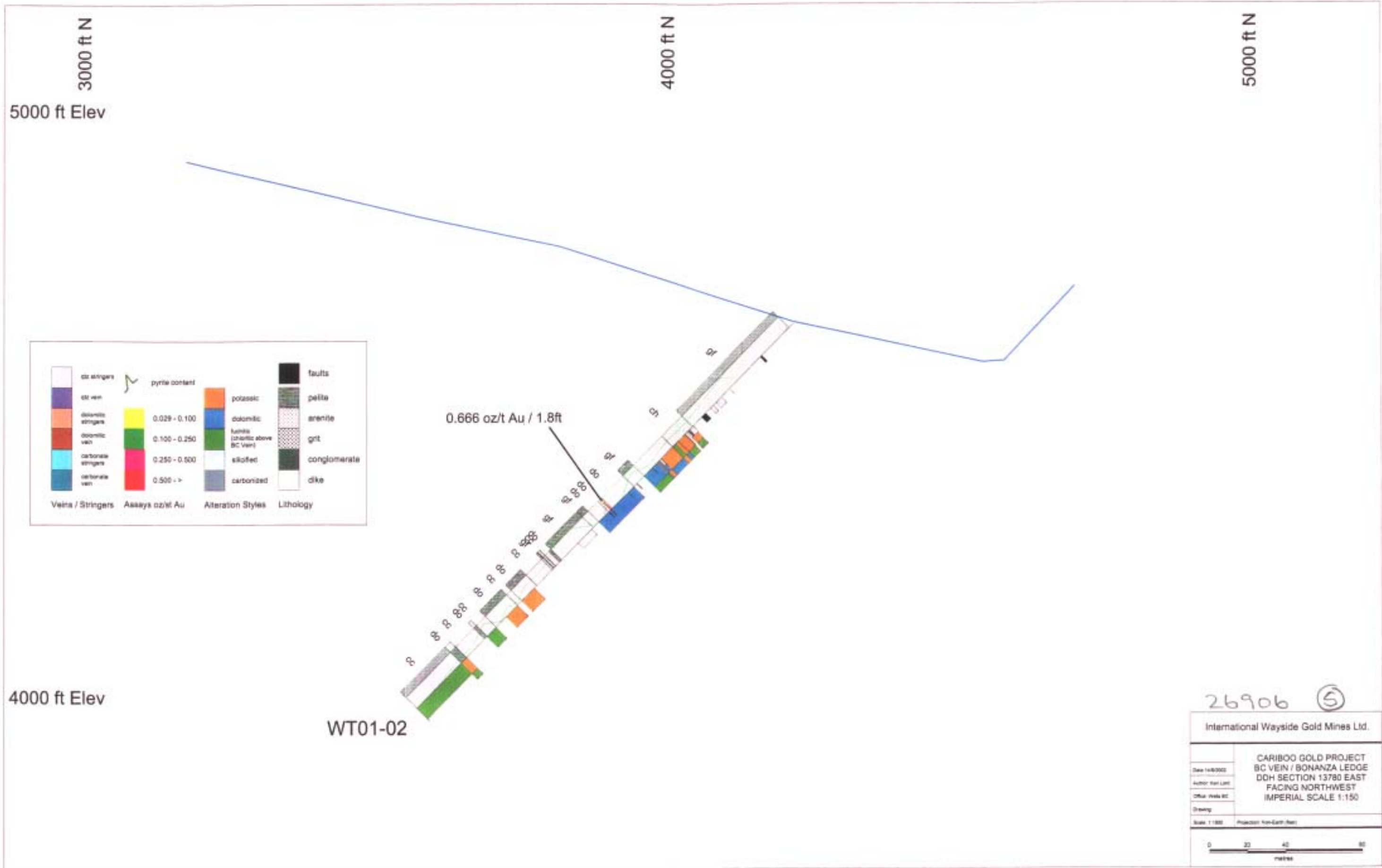
3000 ft N



26906 (R)

International Wayside Gold Mines Ltd.

CARIBOO GOLD PROJECT BC VEIN / BONANZA LEDGE DDH SECTION 18200 EAST FACING NORTHWEST IMPERIAL SCALE 1:150	
Date: 1/18/2002	
Author: Ron Lamb	
Office: Pella BC	
Drawing:	
Scale: 1:1500	Projection: North (NAD)

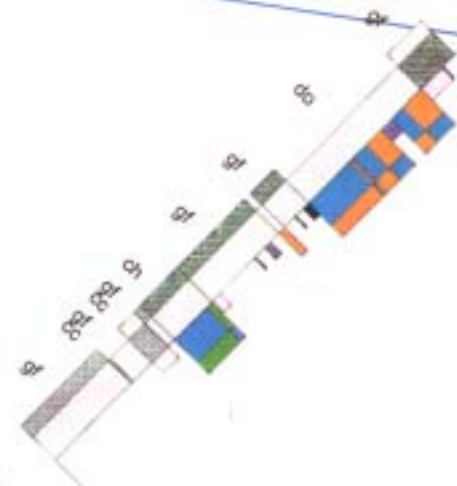


3000 ft N
5000 ft Elev

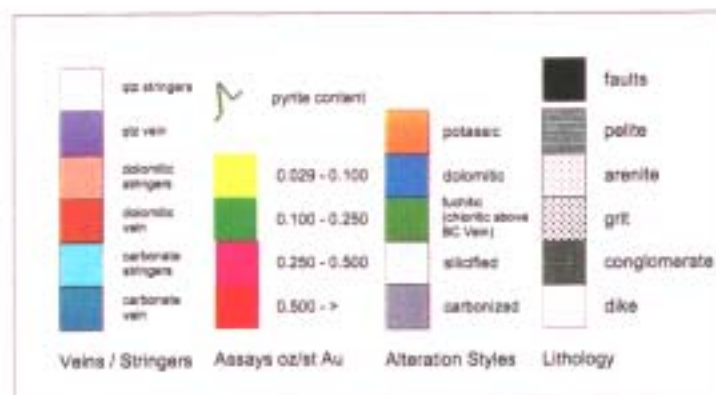
4000 ft N

5000 ft N

WT01-01



4000 ft Elev



26906 (T)

International Wayside Gold Mines Ltd.

CARIBOO GOLD PROJECT
WELLS TREND
DDH SECTION 13085 EAST
FACING NORTHWEST
IMPERIAL SCALE 1:150

Scale: 1:1500 Projection: True-Shape (NAD)

0 20 40 80
metres

3000 ft N
5000 ft Elev

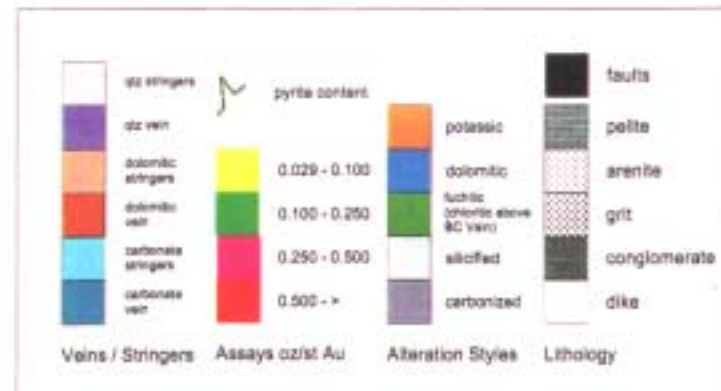
4000 ft N

5000 ft N

WT01-03

0.088 oz/t Au / 7.6ft

4000 ft Elev



26906 (TB)

International Wayside Gold Mines Ltd.	
Date: 14/03/2012	CARIBOO GOLD PROJECT
Author: Sam Lott	BC VEIN / BONANZA LEDGE
Officer: Mike BC	DDH SECTION 13780 EAST
Drawing	FACING NORTHWEST
Scale: 1:150	IMPERIAL SCALE 1:150
Projection: North (dist)	

APPENDIX 3 – INDUCED POLARIZATION REPORT

By SJ Geophysics



SJ Geophysics Ltd.

S.J.V. Consultants Ltd.



11762-94th Avenue,
Delta BC V4C 3R7 CANADA

Bus: (604) 582-1100
E-mail: tr@nt@sjgeophysics.com

Fax: (604) 589-7466
www.sjgeophysics.com

International Wayside Gold Mines Ltd. Induced Polarization Survey Cow Mountain Project, Wells Area, B.C.

December 14, 2001

The following pages contain colour cross-sectional images of the IP results gathered along 22 lines (14200E to 9600E) on the Cow Mountain Project. Two sets of three images are presented for each line: the first for the resistivity component and the second for the chargeability component.

In the first image of the set, the apparent resistivity (or chargeability) data is presented in a standard pseudosection format, with plotting locations adjusted for elevation and true electrode positioning. The second and third images present the interpreted (inverted) resistivity (or chargeability) data as coloured depth sections. The second image uses a customized colour distribution, calculated from the range of values noted along the line. This representation most clearly displays the variations in the measured parameters along each line. The third image uses a standardized colour distribution: 1 to 50,000 ohm-m for the resistivity and 0 to 120 milliseconds for the chargeability. These representations allows for a better line to line comparison of the results across the survey grid.

The survey grid was established using the original mine grid, which used imperial units (feet) however some work, including this IP survey, used the metric system. All of the maps created have been registered to the NAD 83, Zone 10, UTM coordinate system, to be consistent with the autocad base maps provided by Wayside. Lines (9600E to 14200E) and stations (2000N to 5000N) have retained the imperial numbering scheme on all plots. However, the depths and stations labeled on the pseudosection and depthsections included in

this document are in metres. The horizontal locations posted on these sections are the horizontal distance (in metres) referenced from station location 2000N. Therefore, location 2000N on these plots coincides with station 2000N on the map. However, grid location 3000N (station) on the plan map will coincide with location 2304.8 on the section plots (2000 + 304.8m (1000 feet = 304.8m)).

The pseudosections and depthsections included in this document can be generated as larger, scaled plots if required.

The inversion results can also be presented as colour contoured plan maps for selected depths. Data files for these results at 15, 50 and 100 metre depths from surface have been generated.

List of Lines

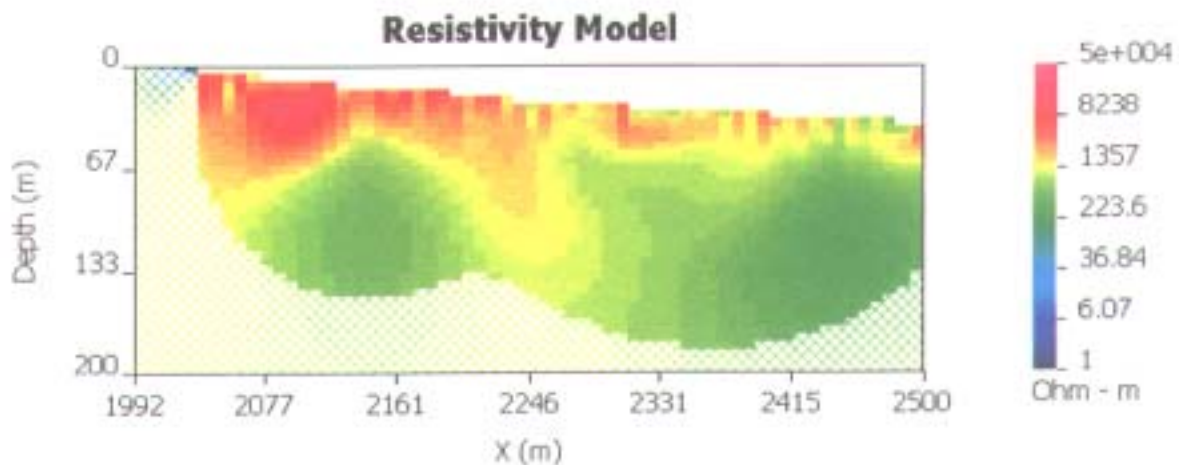
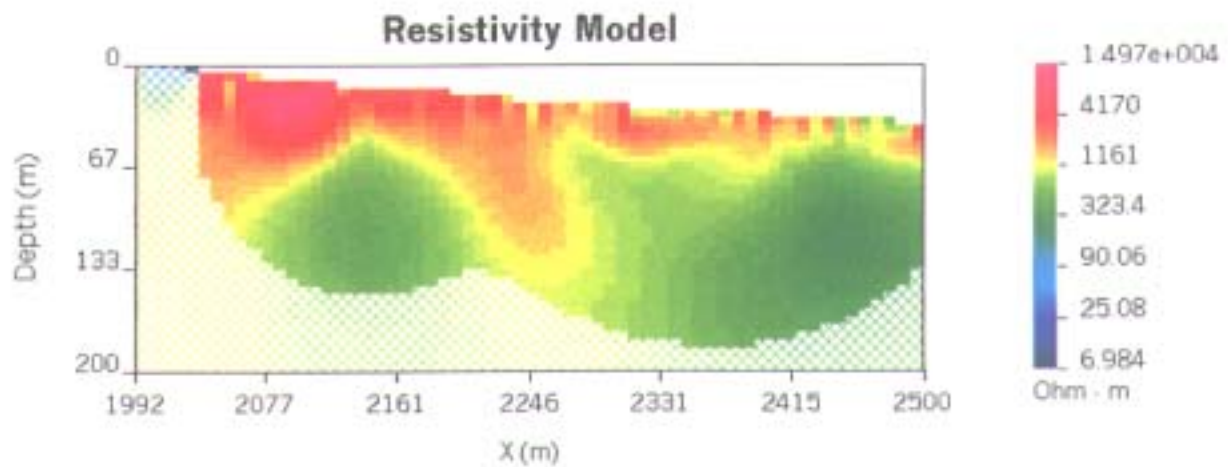
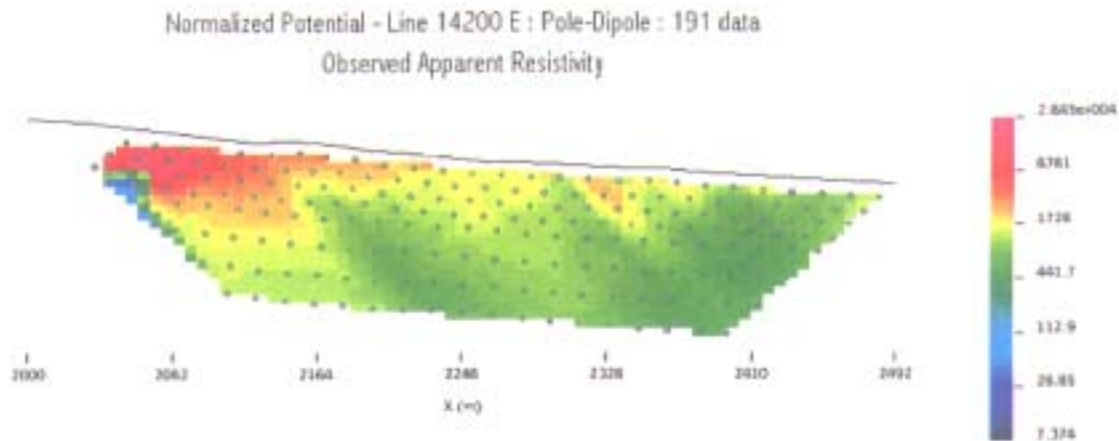
Page

Line 14200E Resistivity	4
Line 14200E Chargeability.....	5
Line 14000E Resistivity	6
Line 14000E Chargeability.....	7
Line 13800E Resistivity	8
Line 13800E Chargeability.....	9
Line 13600E Resistivity	10
Line 13600E Chargeability.....	11
Line 13400E Resistivity	12
Line 13400E Chargeability.....	13
Line 13200E Resistivity	14
Line 13200E Chargeability.....	15
Line 13000E Resistivity	16
Line 13000E Chargeability.....	17
Line 12800E Resistivity	18
Line 12800E Chargeability.....	19
Line 12600E Resistivity	20

Line 12600E Chargeability.....	21
Line 12200E Resistivity	22
Line 12200E Chargeability.....	23
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Line 14200E Resistivity

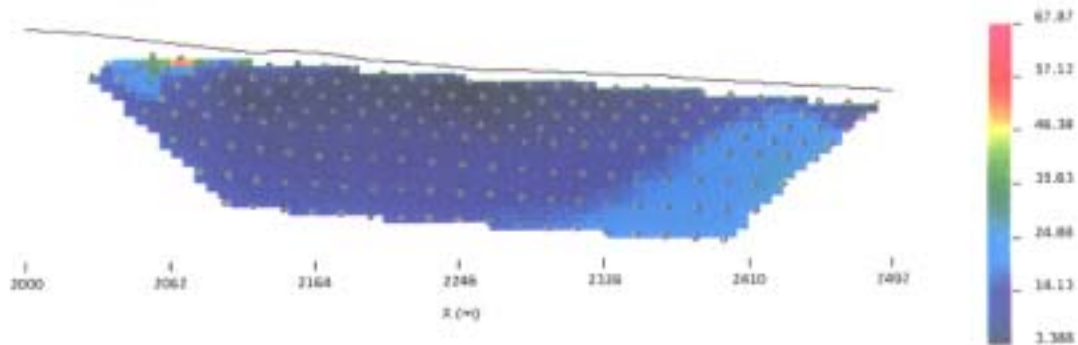
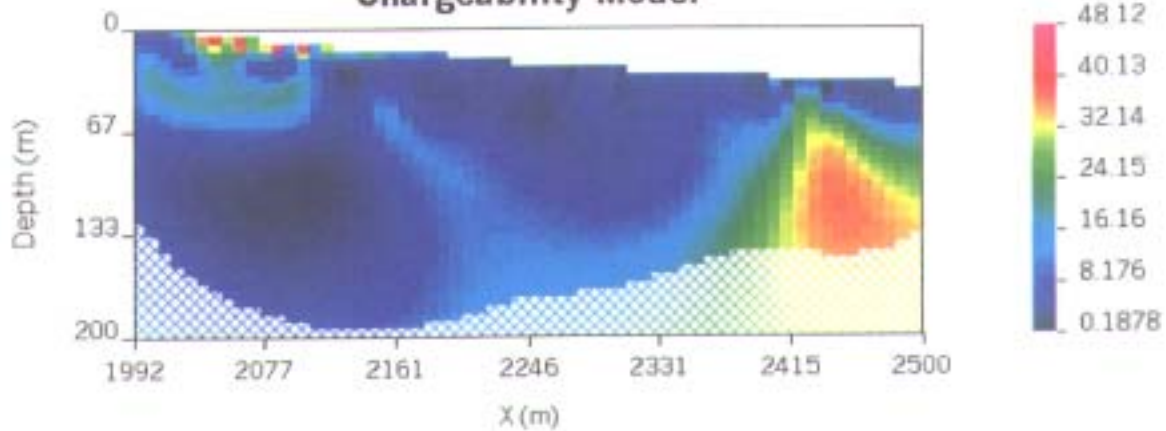
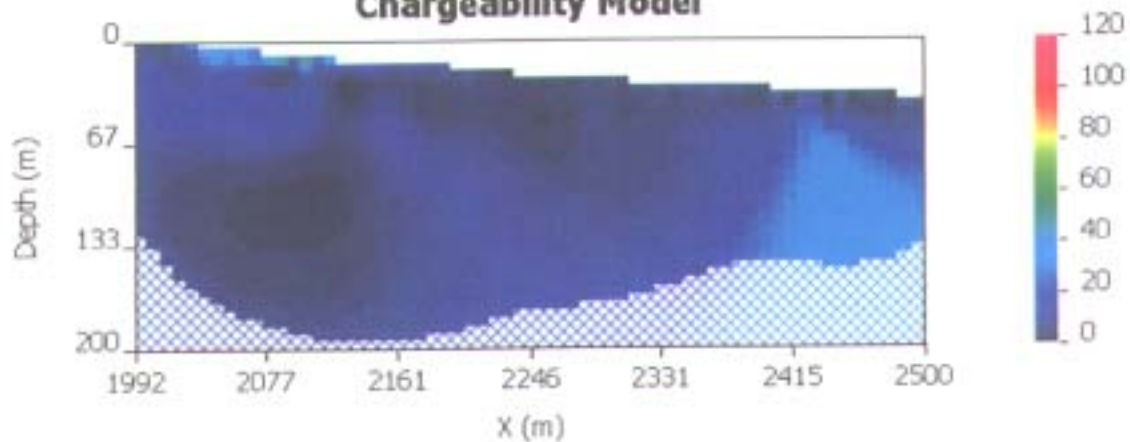
Pseudosection



Line 14200E Chargeability

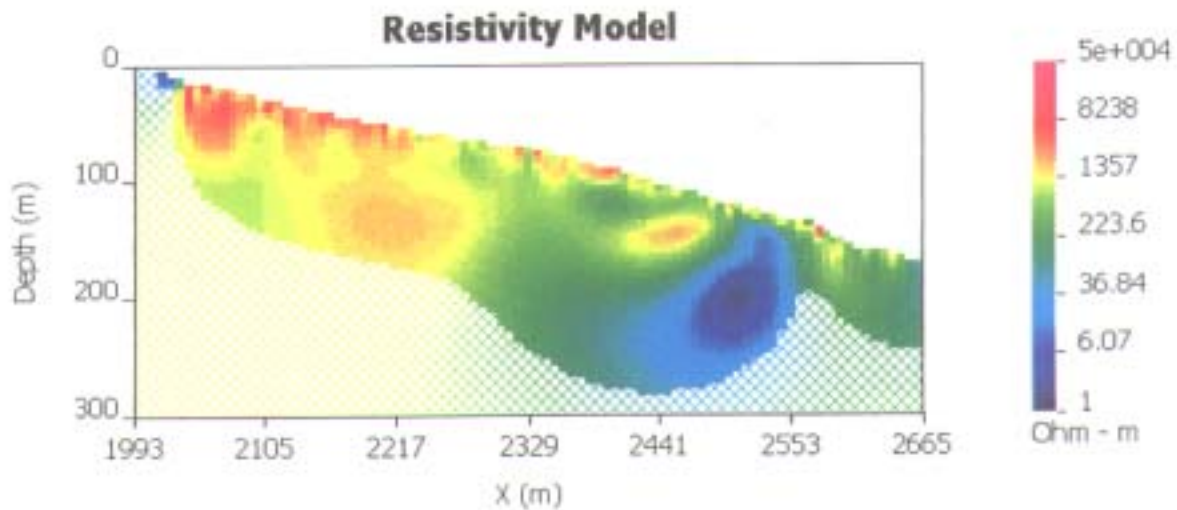
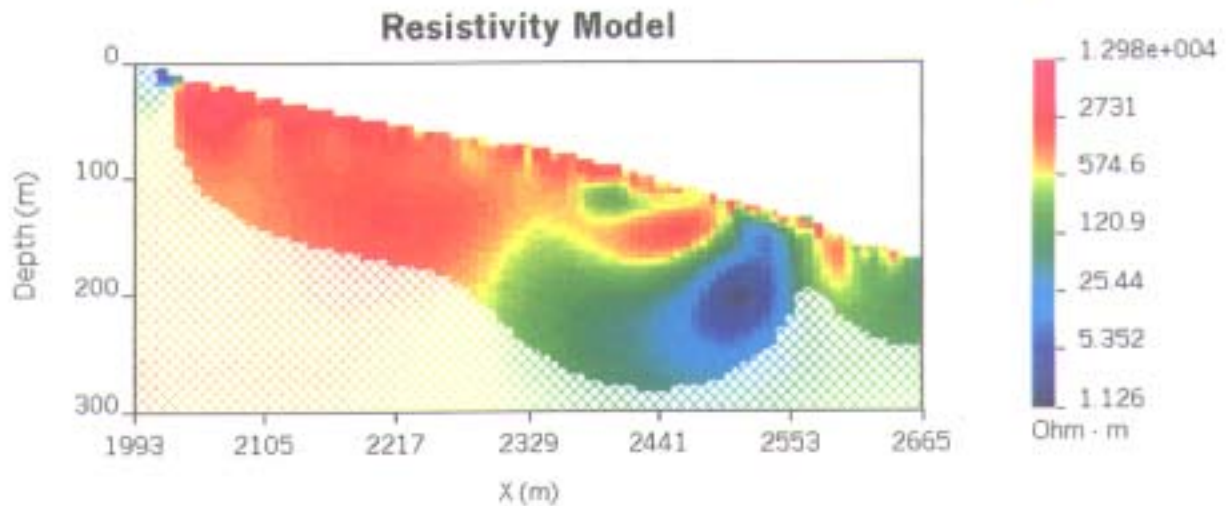
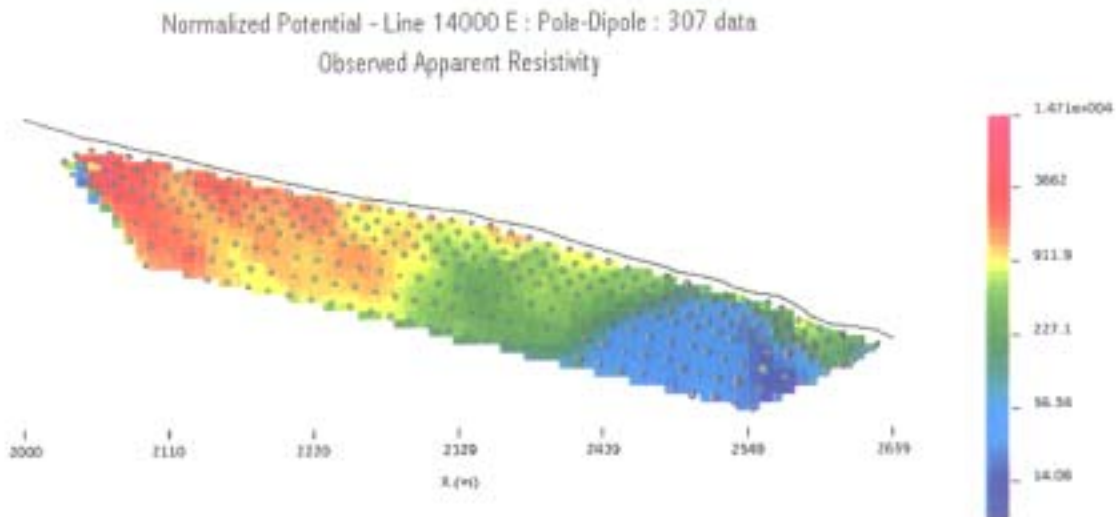
Pseudosection:

Mx Chargeability - Line 14200 E : Pole-Dipole : 188 data
Observed Apparent Chargeability

**Chargeability Model****Chargeability Model**

Line 14000E Resistivity

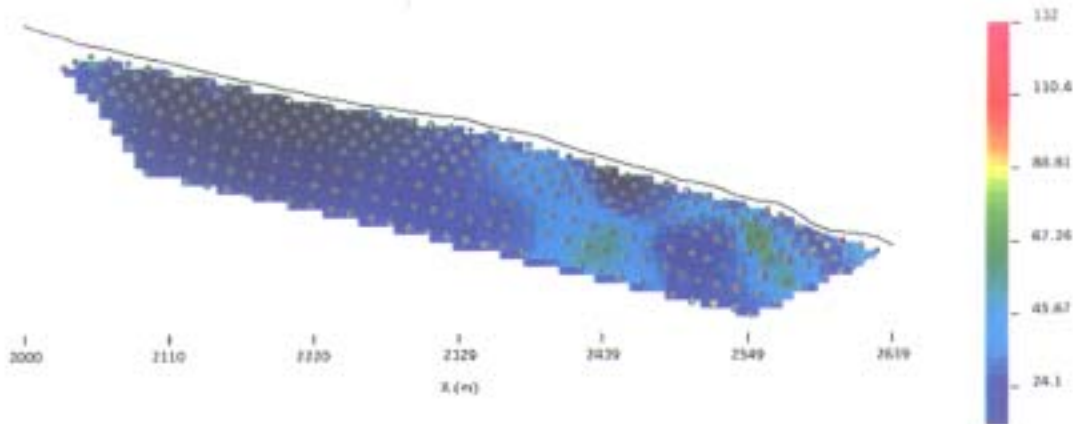
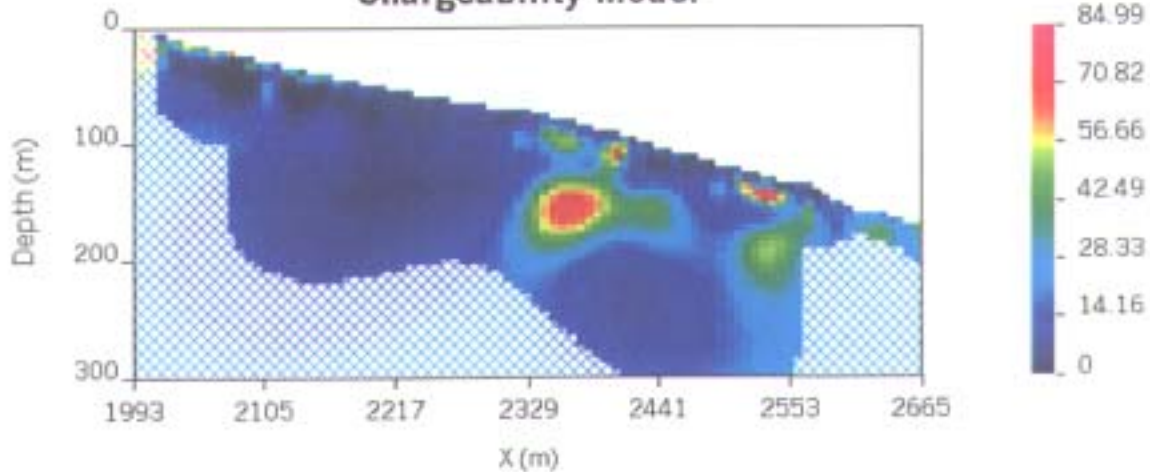
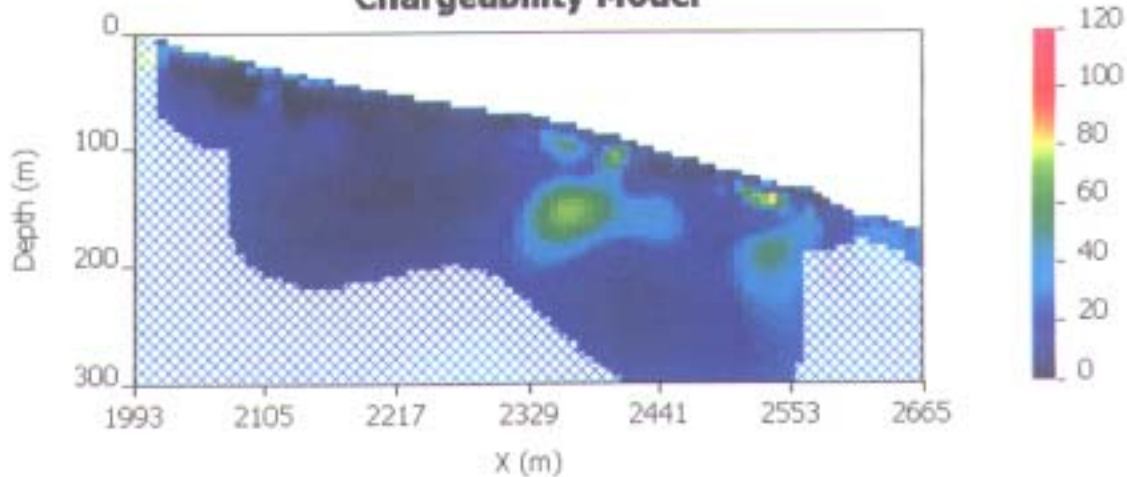
Pseudosection



Line 14000E Chargeability

Pseudosection

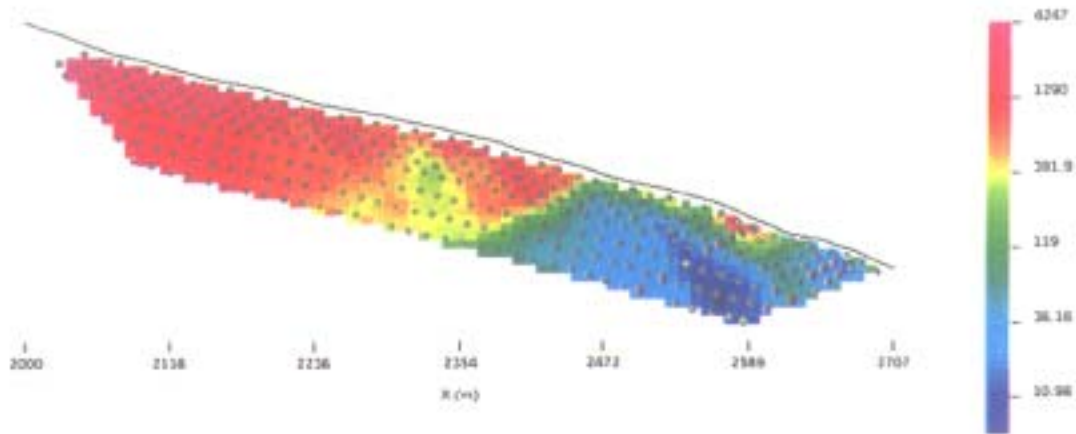
Mx Chargeability - Line 14000 E : Pole-Dipole : 305 data
Observed Apparent Chargeability

**Chargeability Model****Chargeability Model**

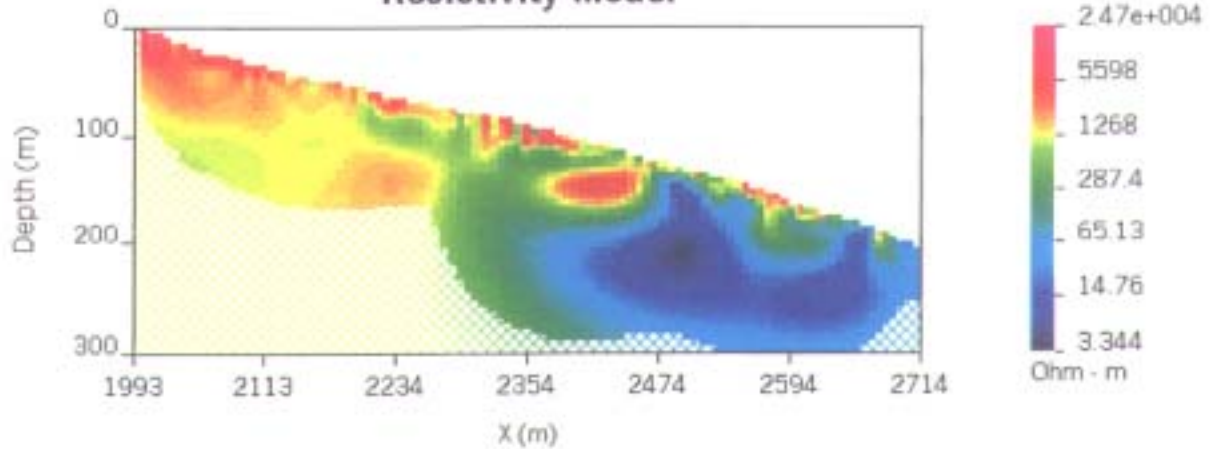
Line 13800E Resistivity

Pseudosection

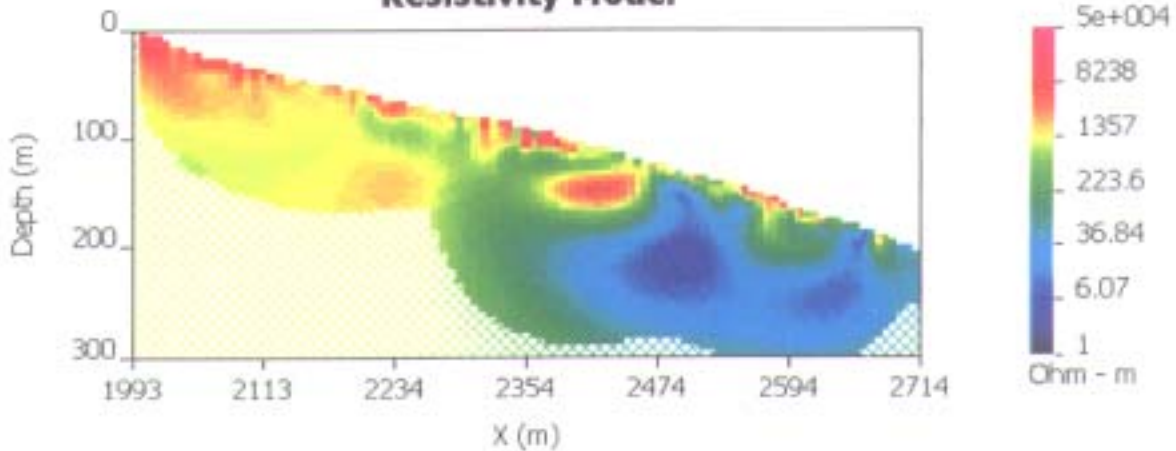
Normalized Potential - Line 13800 E : Pole-Dipole : 350 data
Observed Apparent Resistivity



Resistivity Model



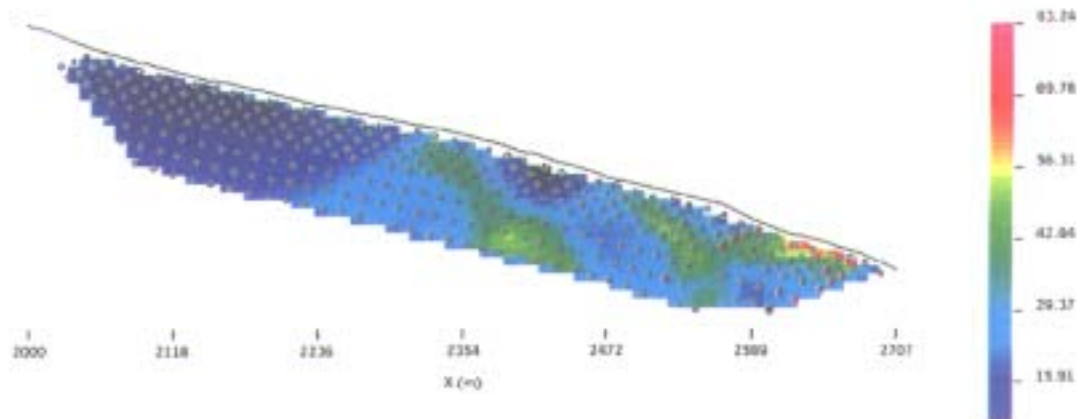
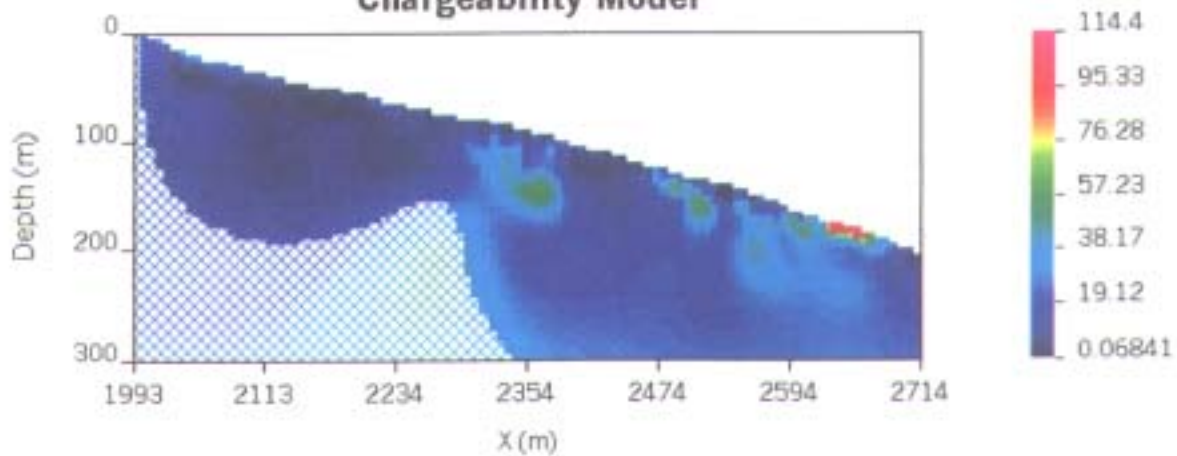
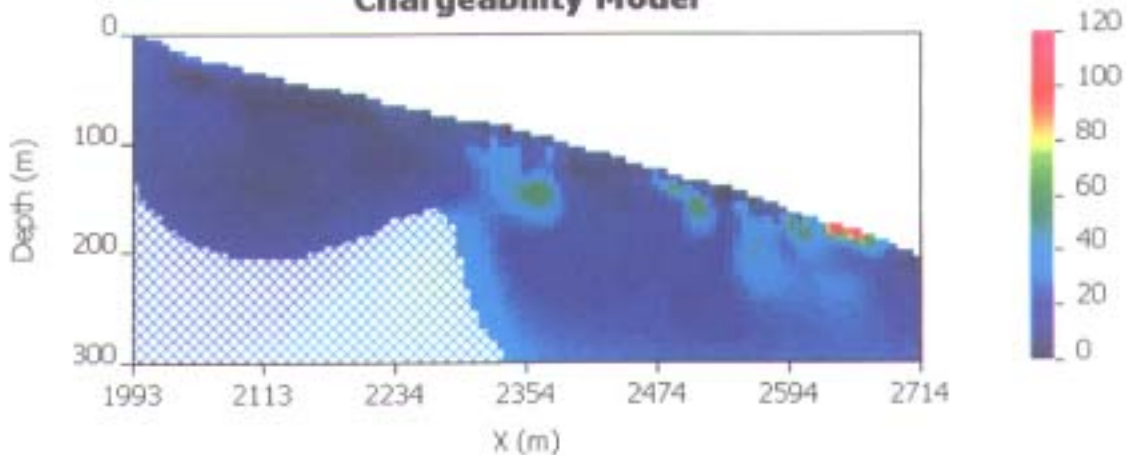
Resistivity Model



Line 13800E Chargeability

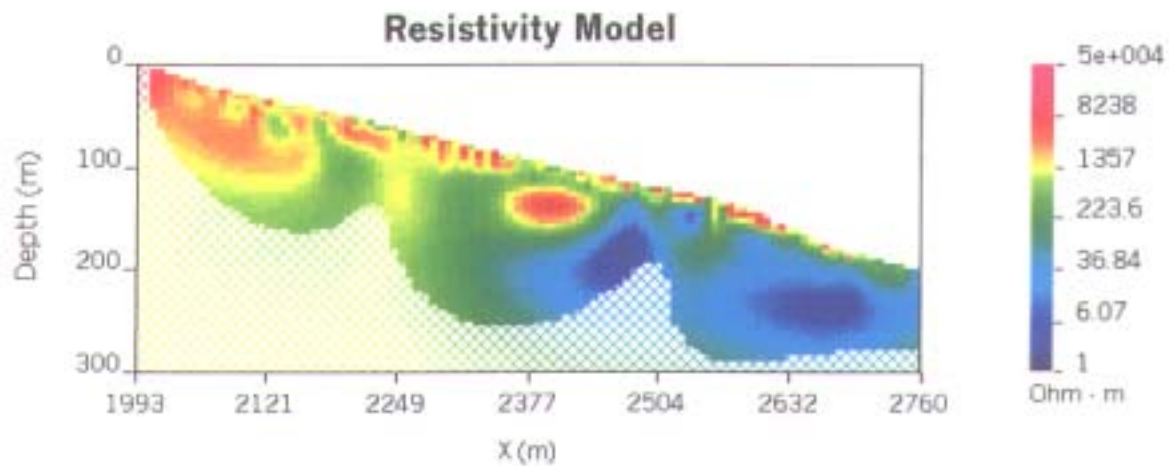
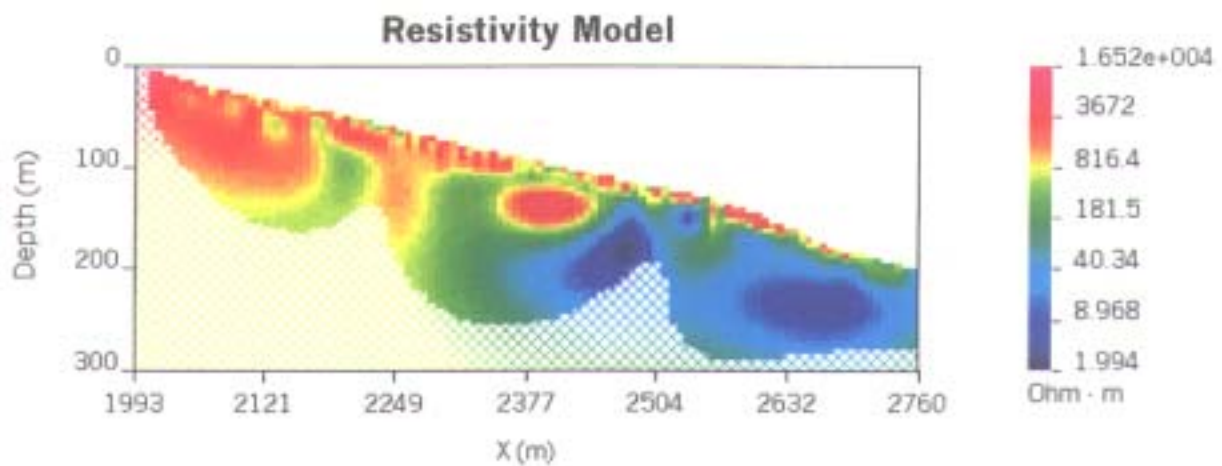
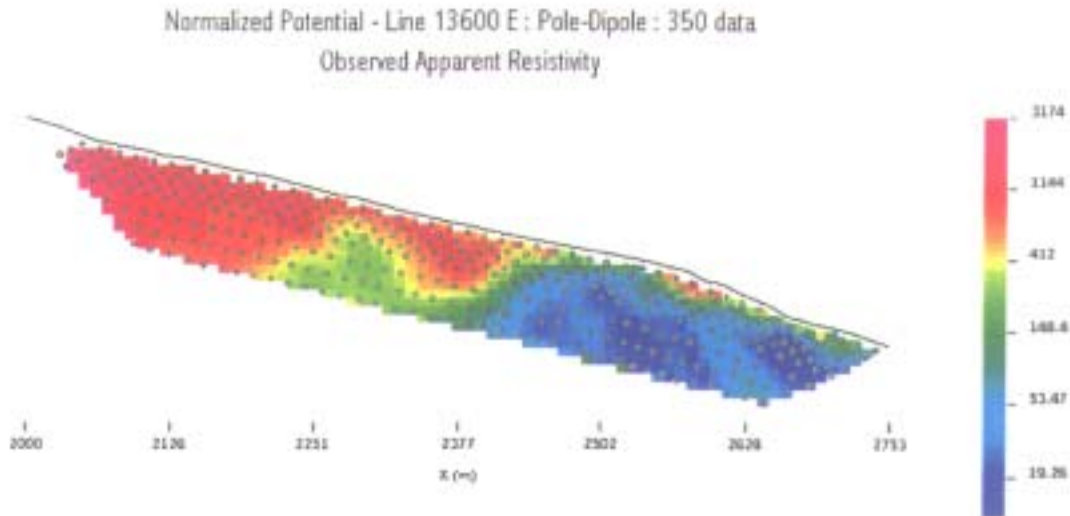
Pseudosection

Mx Chargeability - Line 13800 E : Pole-Dipole : 341 data
Observed Apparent Chargeability

**Chargeability Model****Chargeability Model**

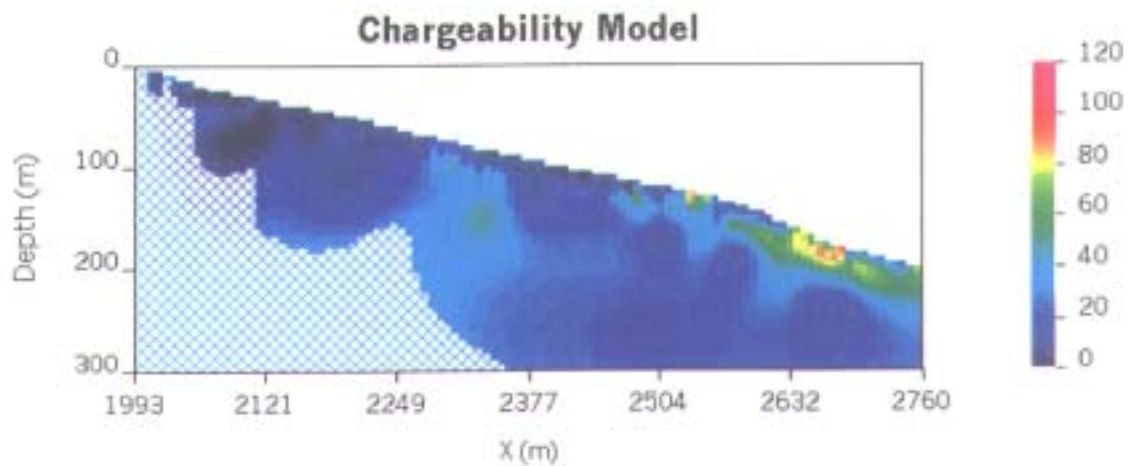
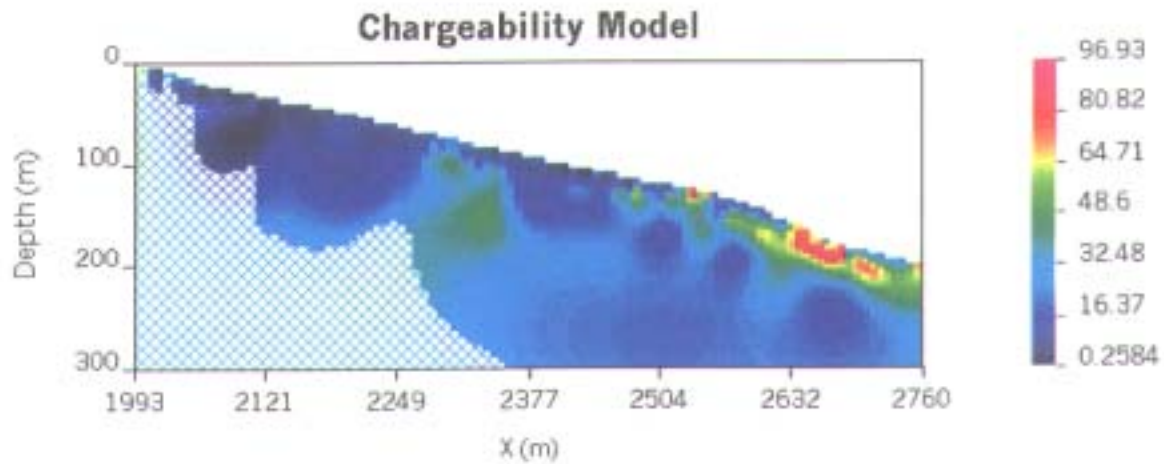
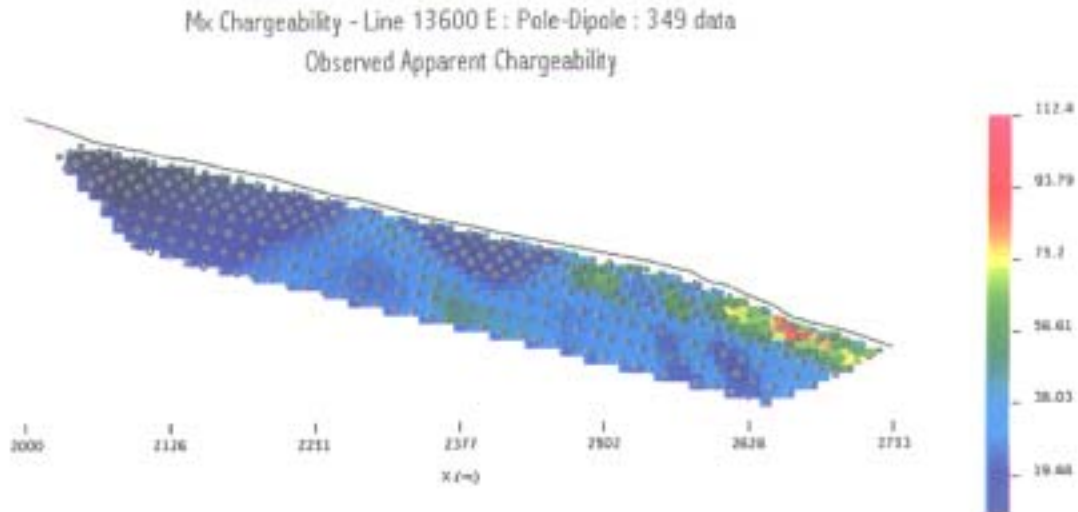
Line 13600E Resistivity

Pseudosection



Line 13600E Chargeability

Pseudosection

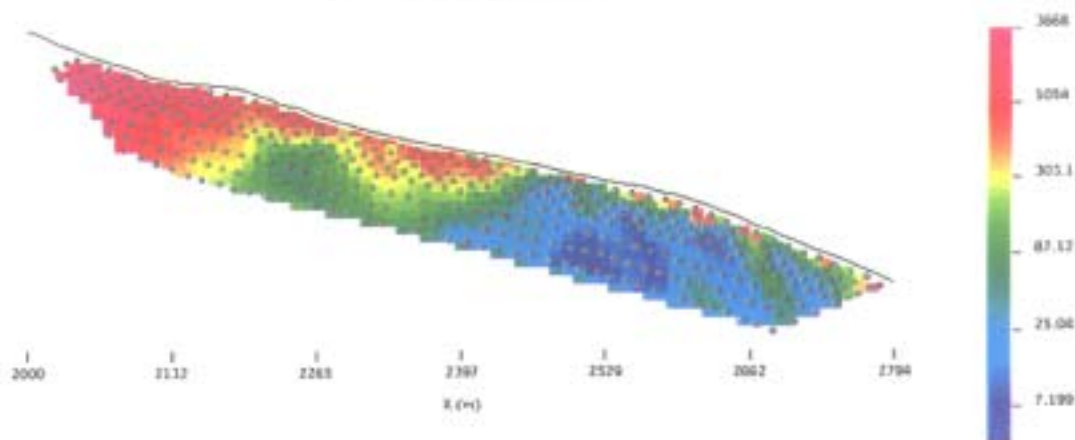
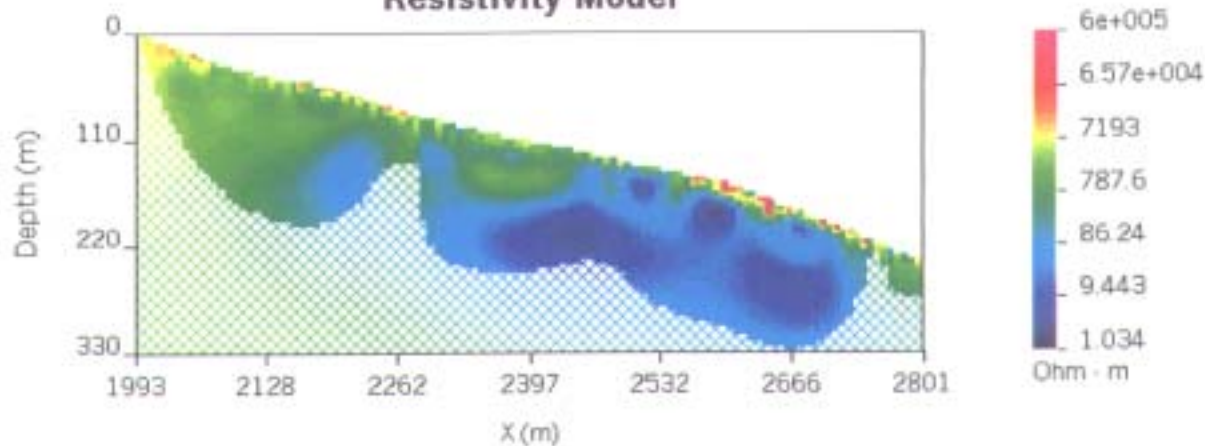
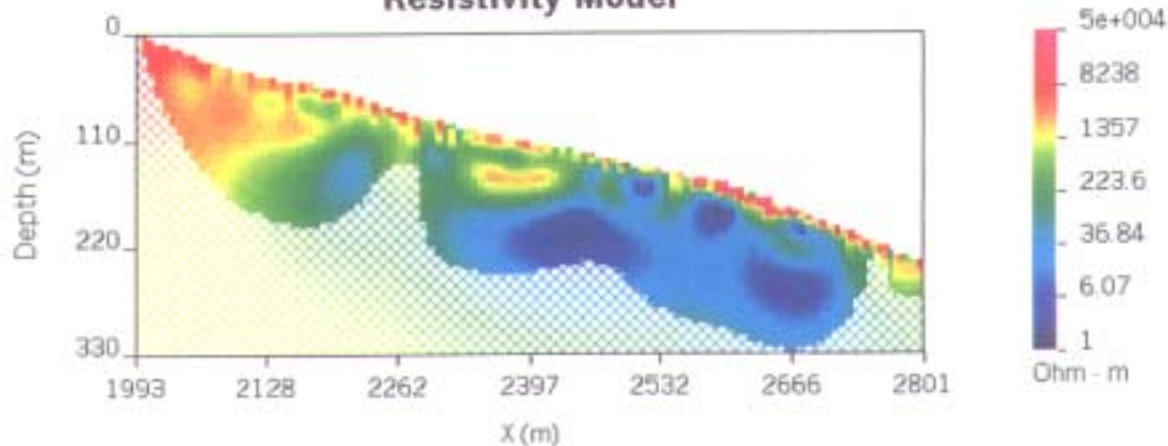


Line 13400E Resistivity

Pseudosection

Normalized Potential - Line 13400 E : Pole-Dipole : 389 data

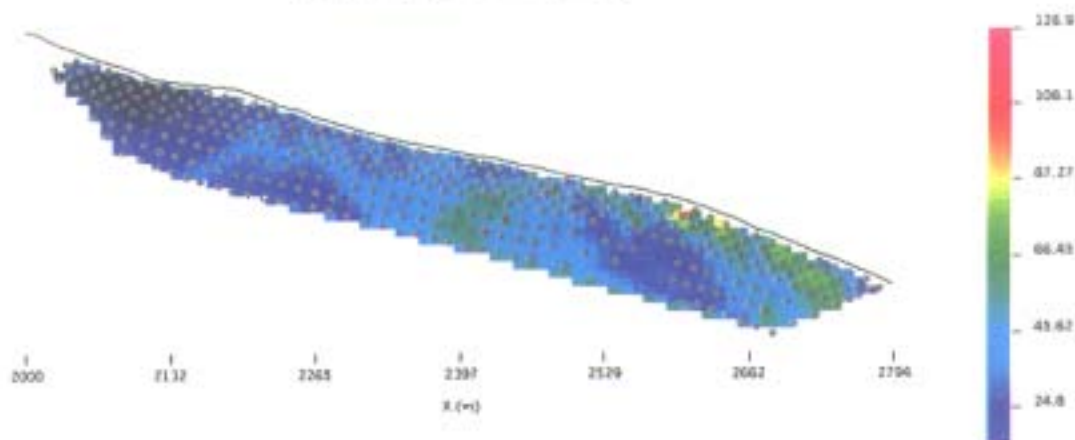
Observed Apparent Resistivity

**Resistivity Model****Resistivity Model**

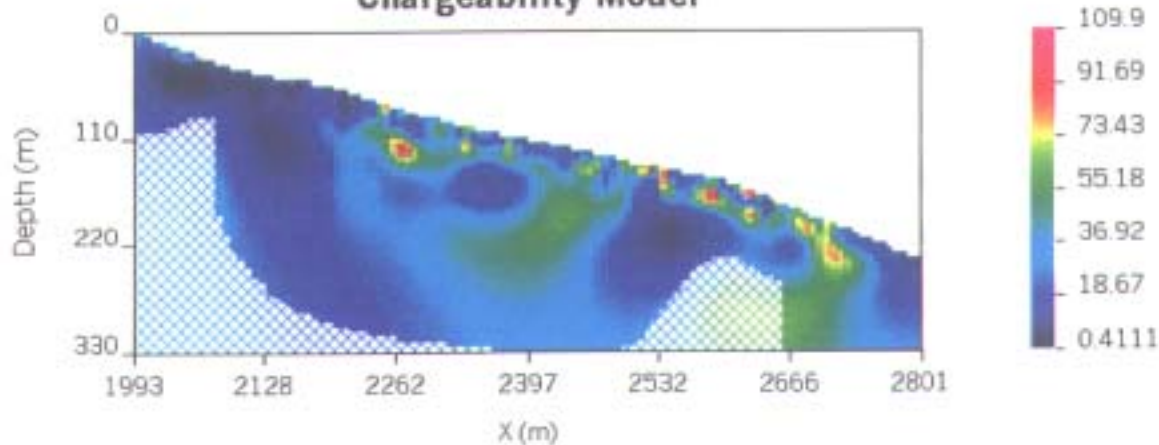
Line 13400E Chargeability

Pseudosection

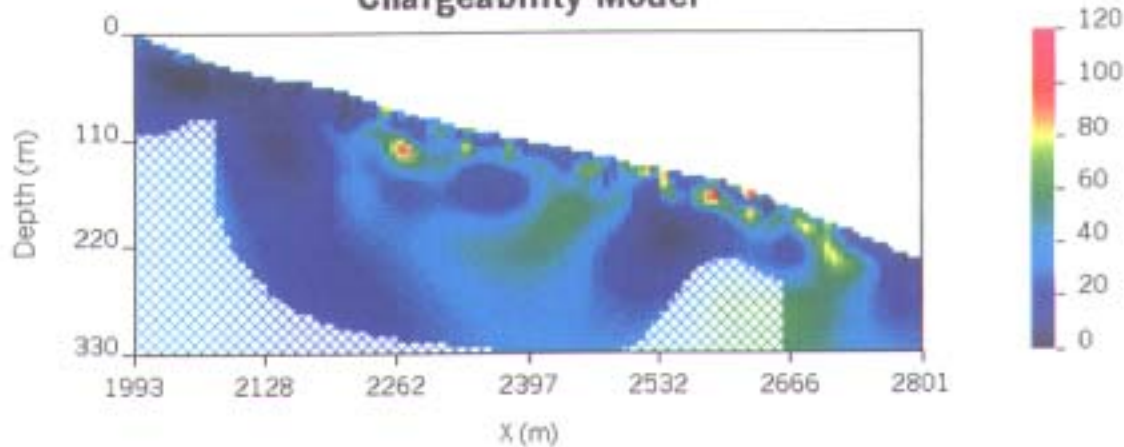
Mx Chargeability - Line 13400 E : Pole-Dipole : 368 data
Observed Apparent Chargeability



Chargeability Model



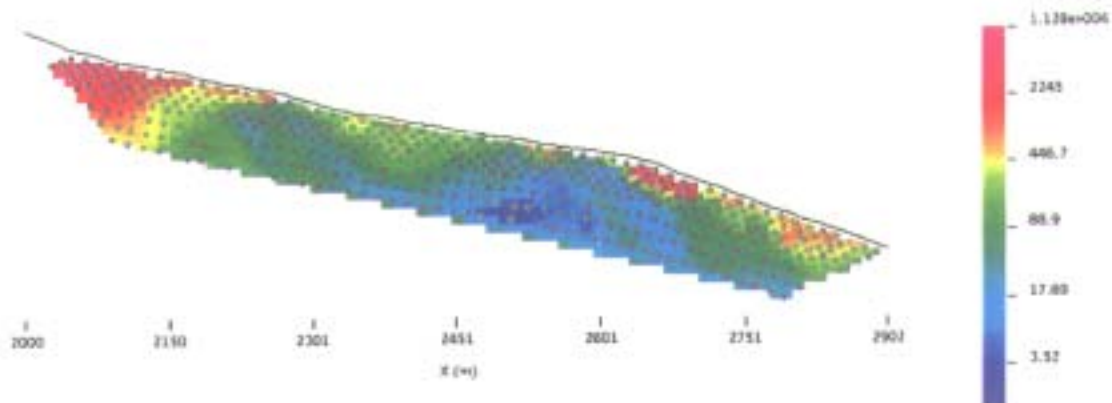
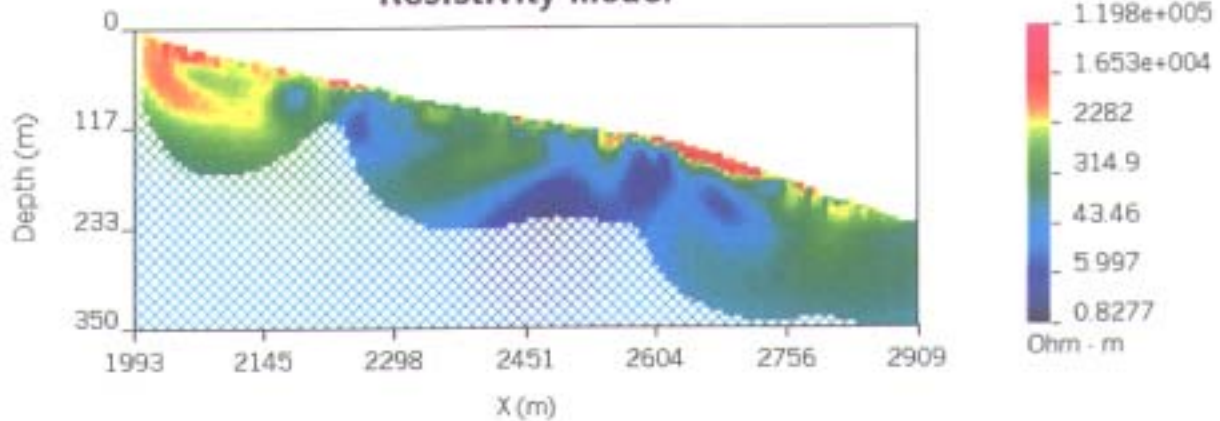
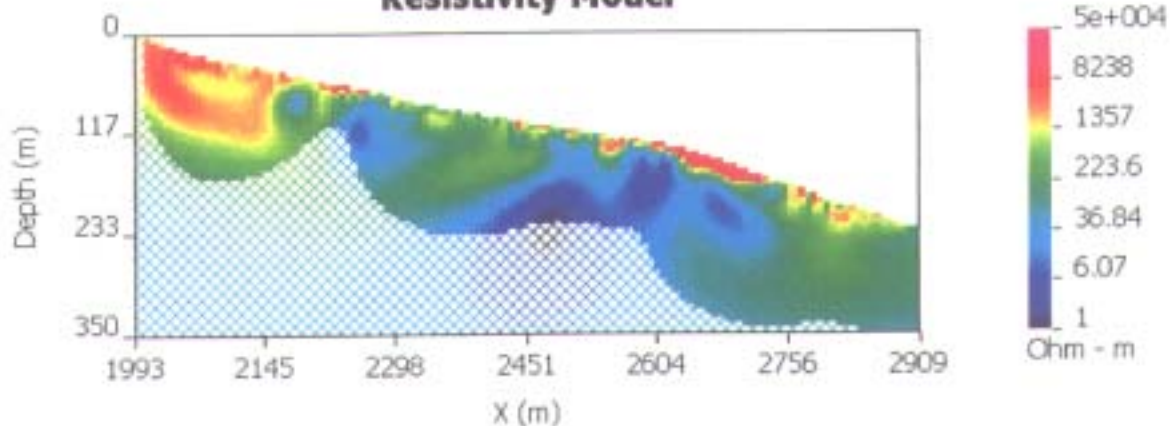
Chargeability Model



Line 13200E Resistivity

Pseudosection

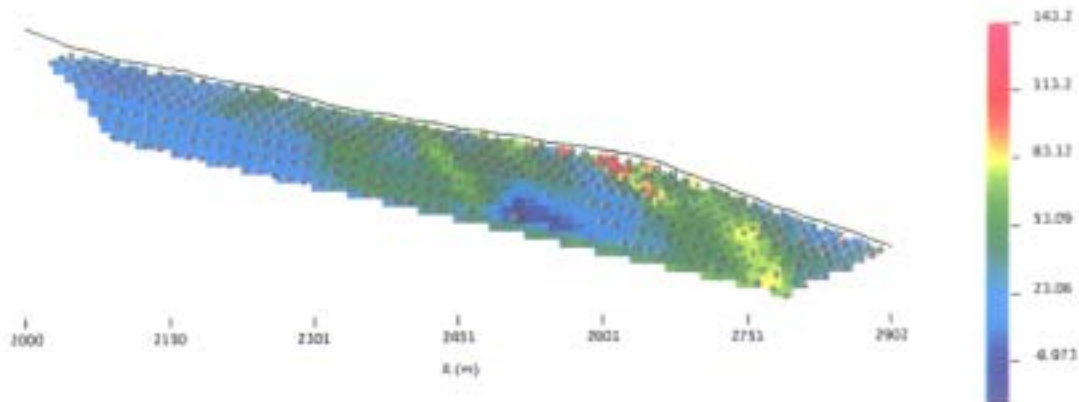
Normalized Potential - Line 13200 E : Pole-Dipole : 434 data
Observed Apparent Resistivity

**Resistivity Model****Resistivity Model**

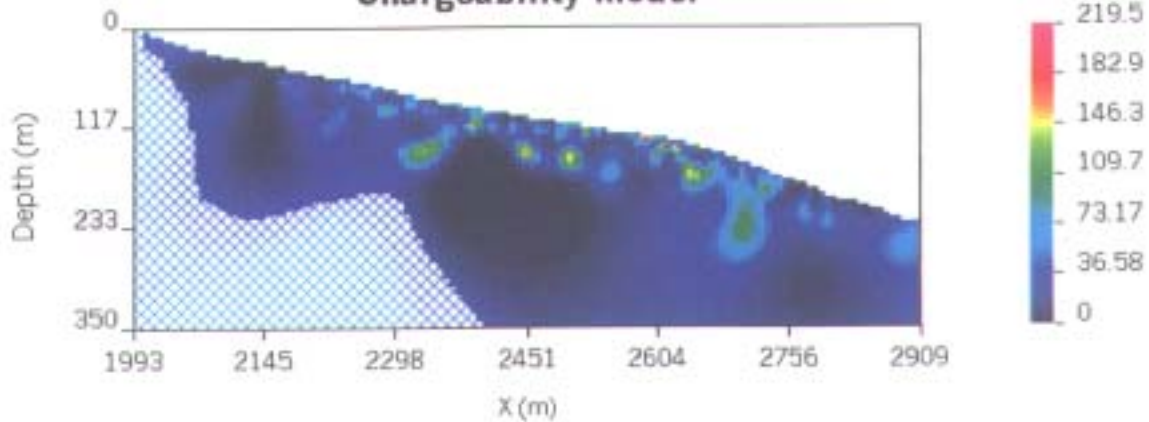
Line 13200E Chargeability

Pseudosection

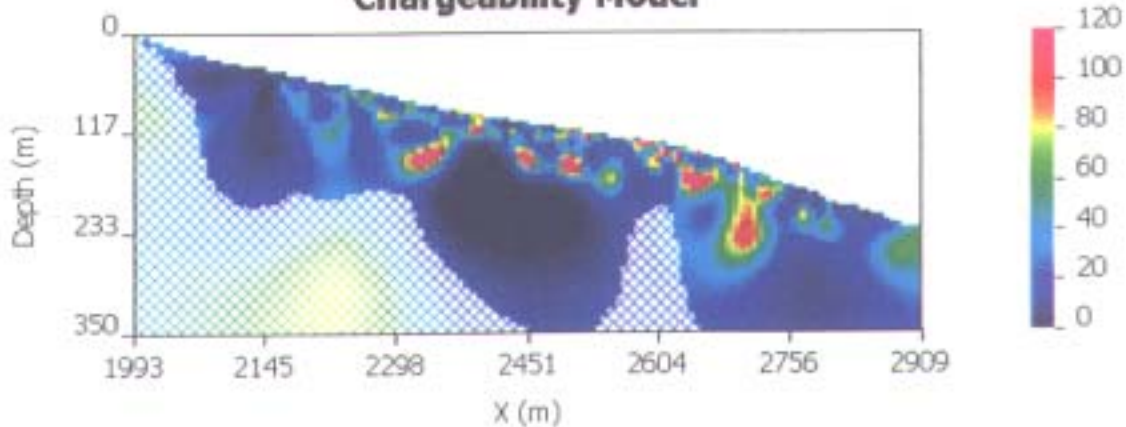
Mx Chargeability - Line 13200 E : Pole-Dipole : 414 data
Observed Apparent Chargeability



Chargeability Model



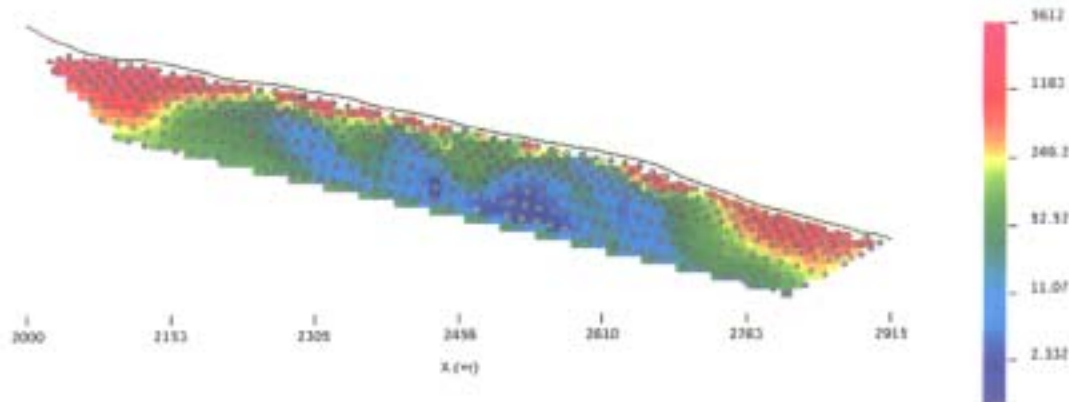
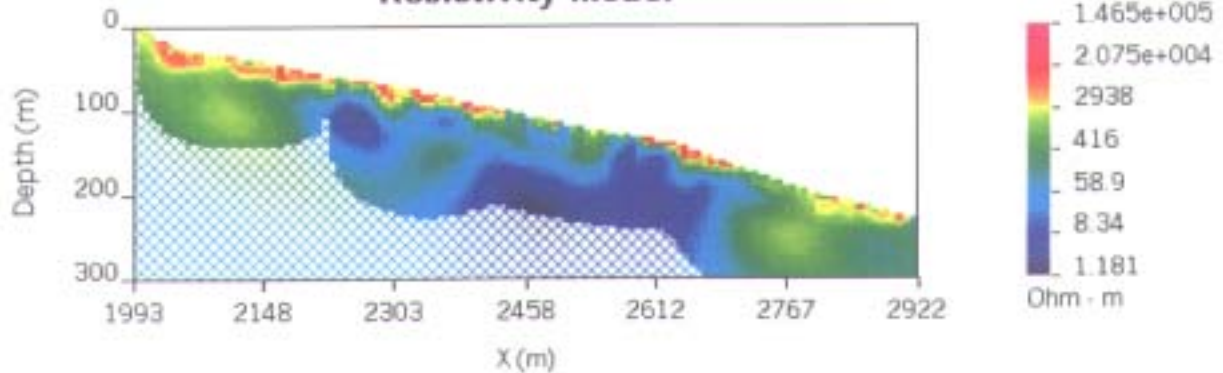
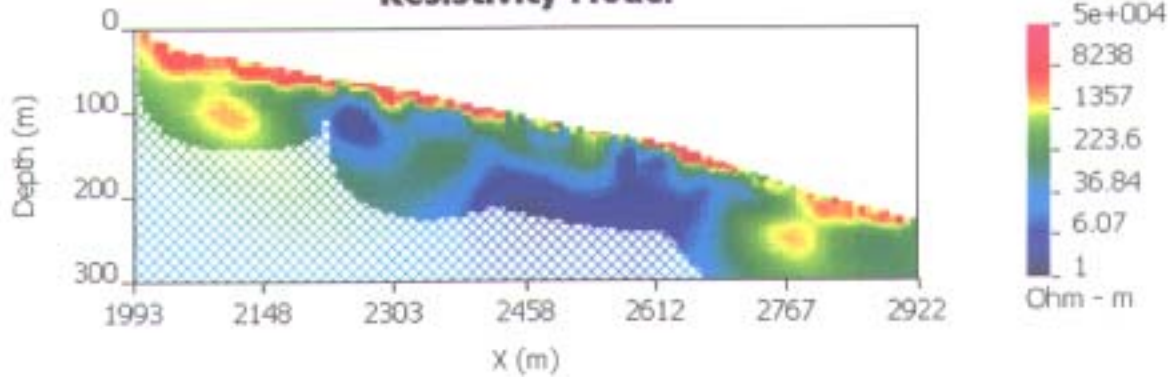
Chargeability Model



Line 13000E Resistivity

Pseudosection

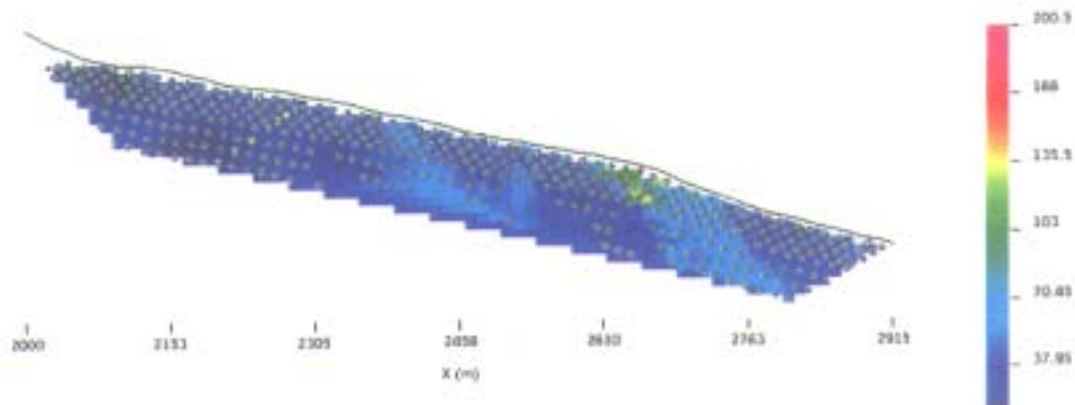
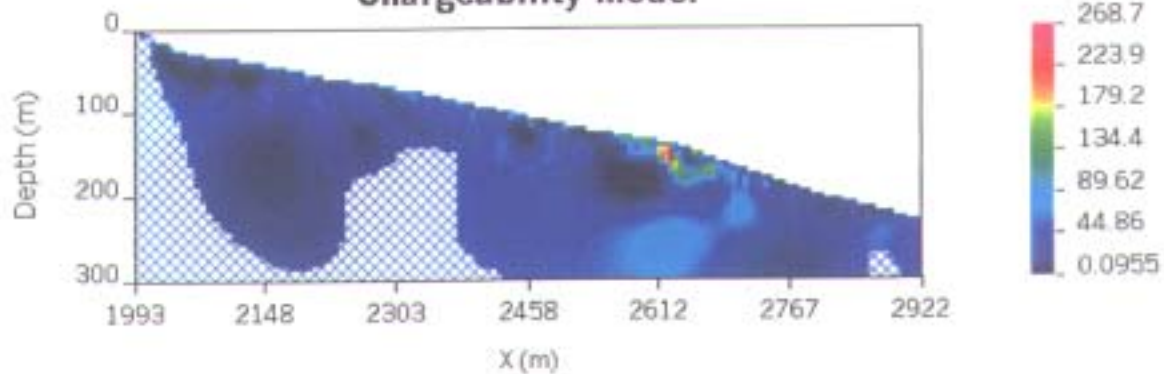
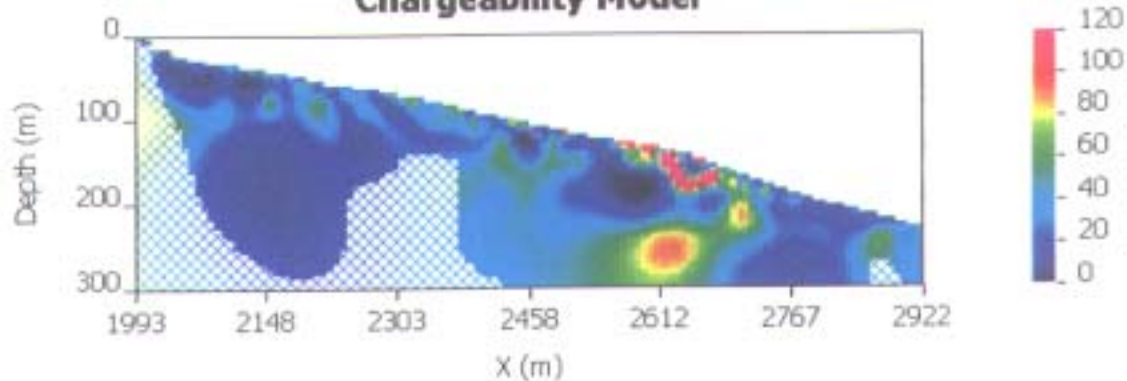
Normalized Potential - Line 13000 E : Pole-Dipole : 437 data
Observed Apparent Resistivity

**Resistivity Model****Resistivity Model**

Line 13000E Chargeability

Pseudosection

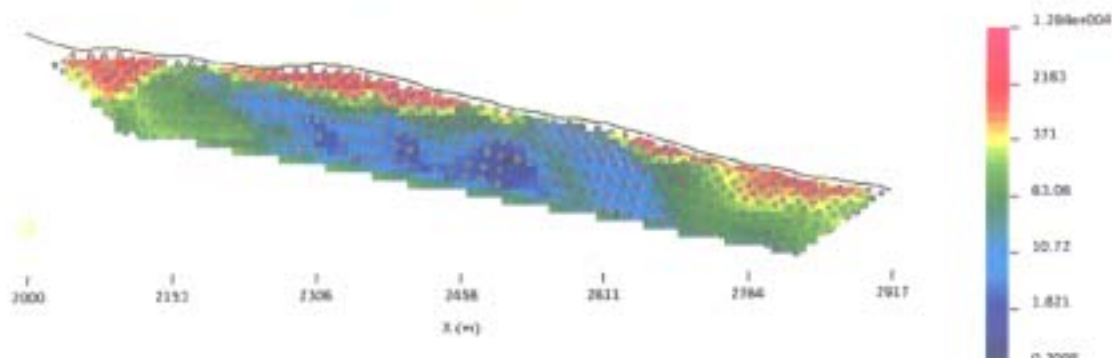
Mx Chargeability - Line 13000 E : Pole-Dipole : 395 data
Observed Apparent Chargeability

**Chargeability Model****Chargeability Model**

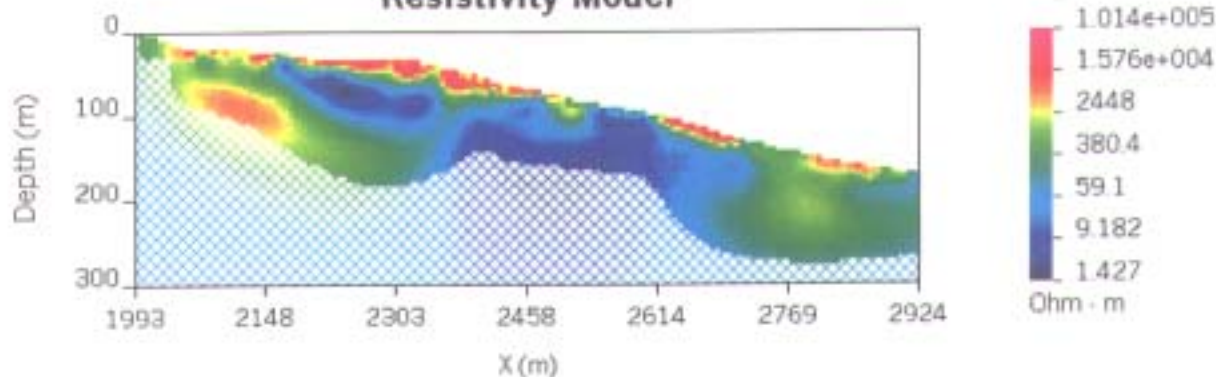
Line 12800E Resistivity

Pseudosection

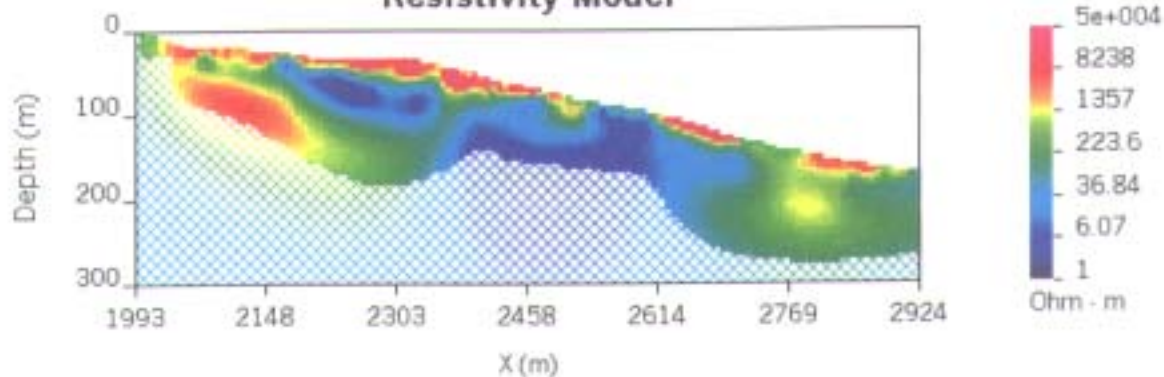
Normalized Potential – Line 12800 E : Pole-Dipole : 421 data
Observed Apparent Resistivity



Resistivity Model



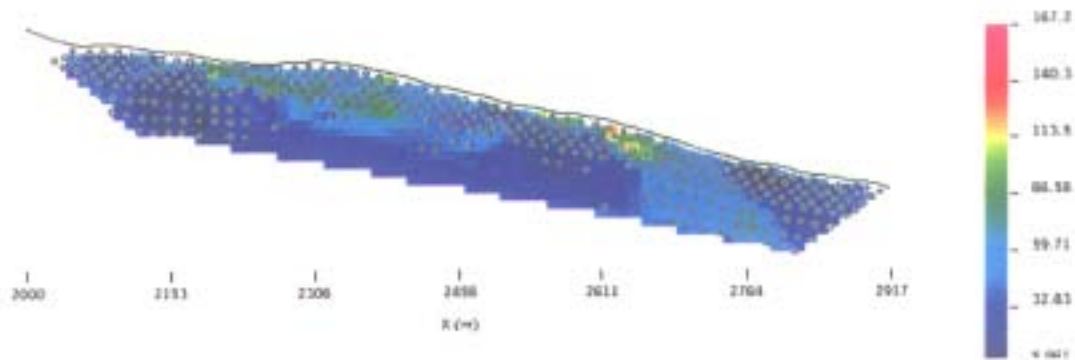
Resistivity Model



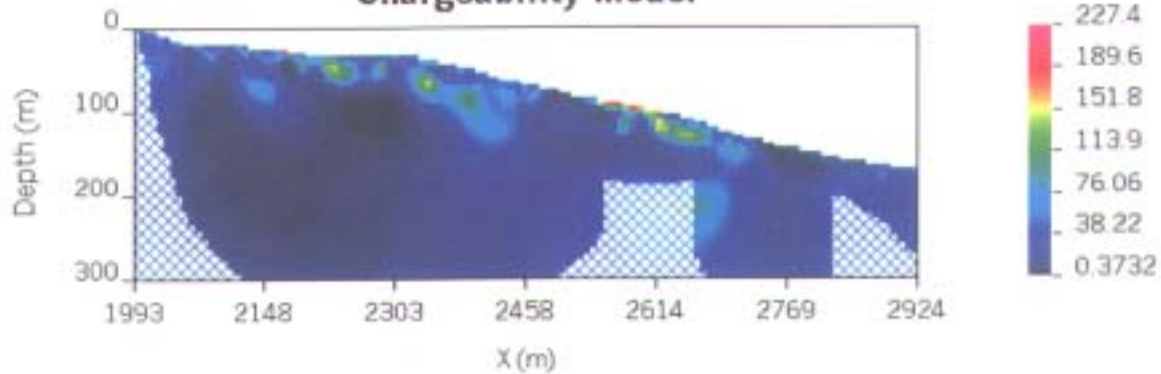
Line 12800E Chargeability

Pseudosection

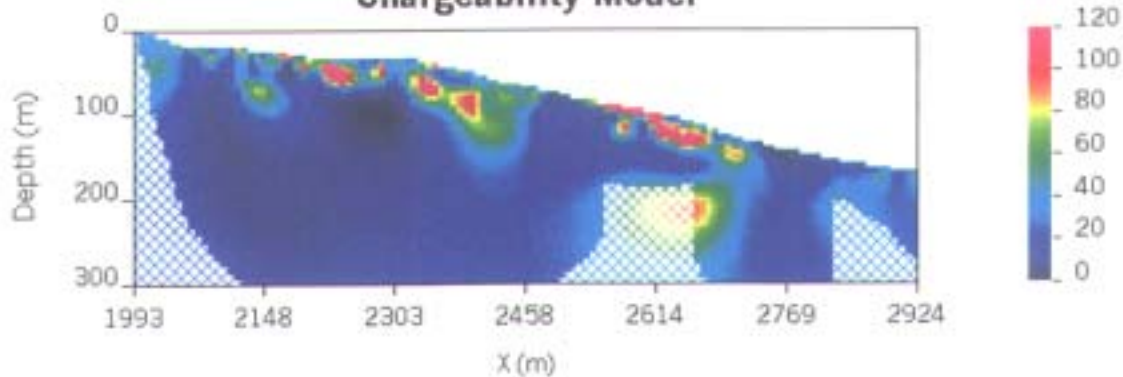
Mx Chargeability - Line 12800 E : Pole-Dipole : 350 data
Observed Apparent Chargeability



Chargeability Model

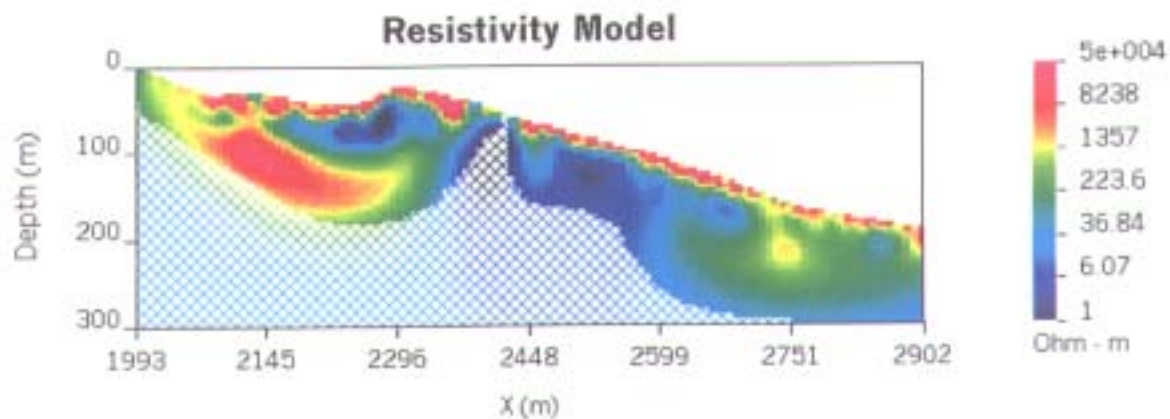
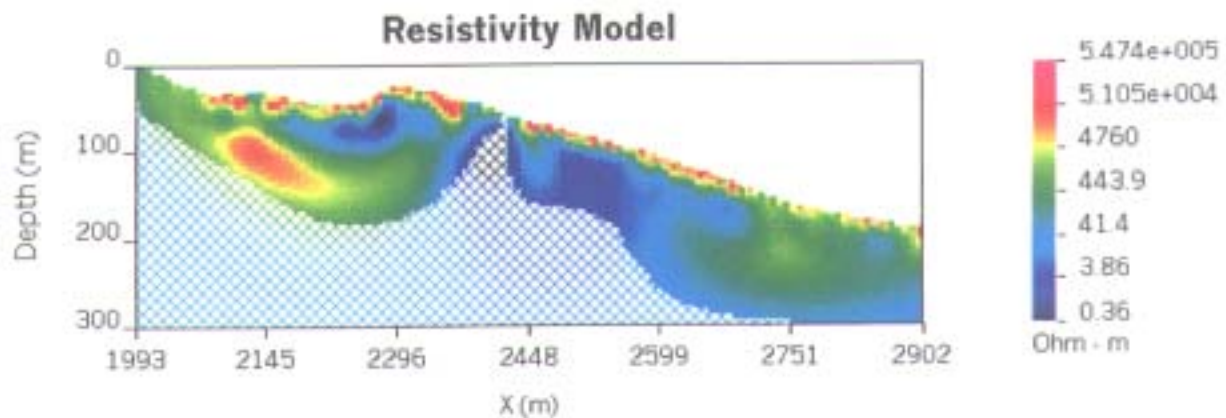
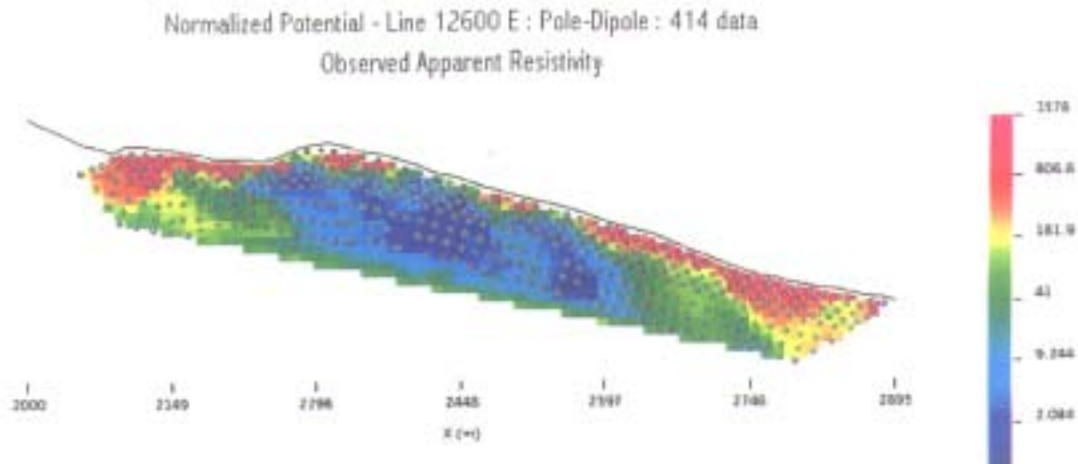


Chargeability Model



Line 12600E Resistivity

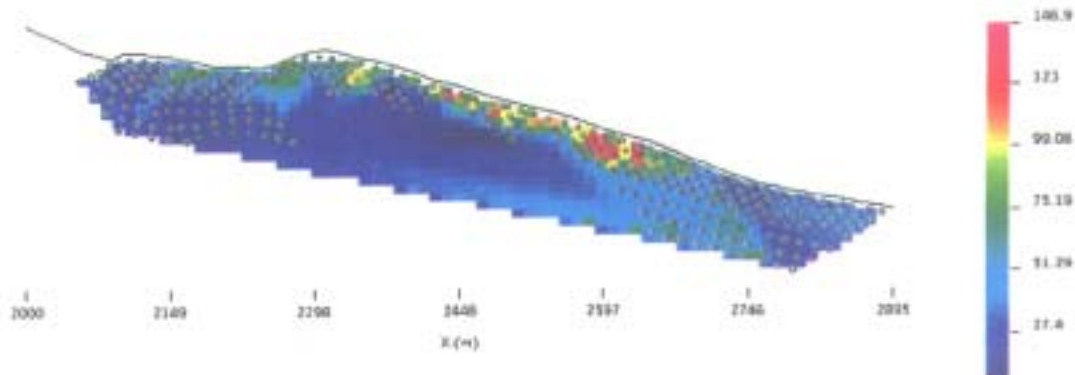
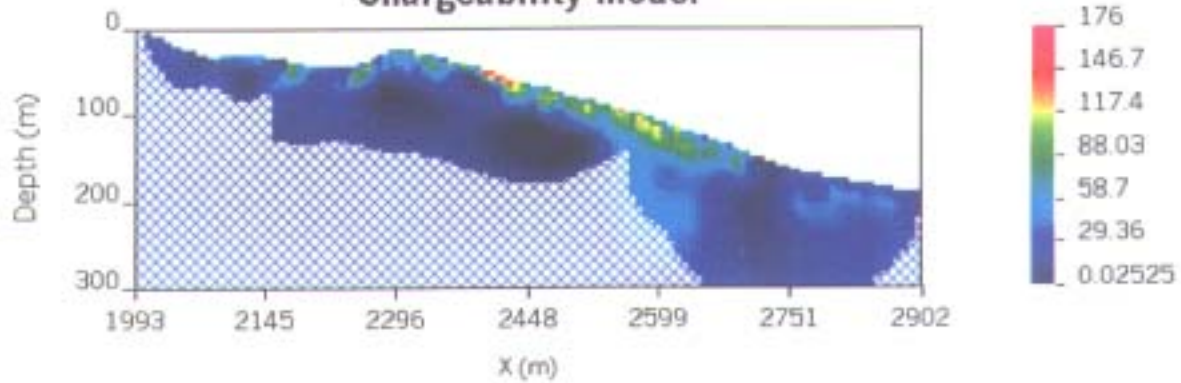
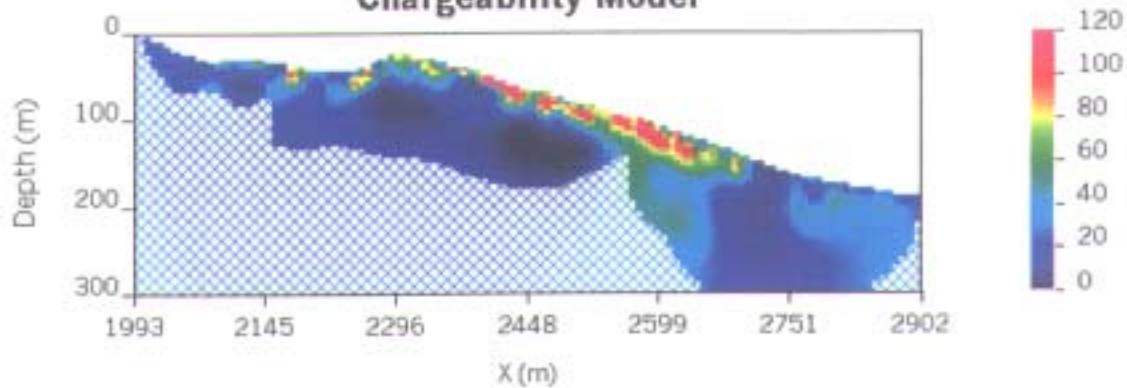
Pseudosection



Line 12600E Chargeability

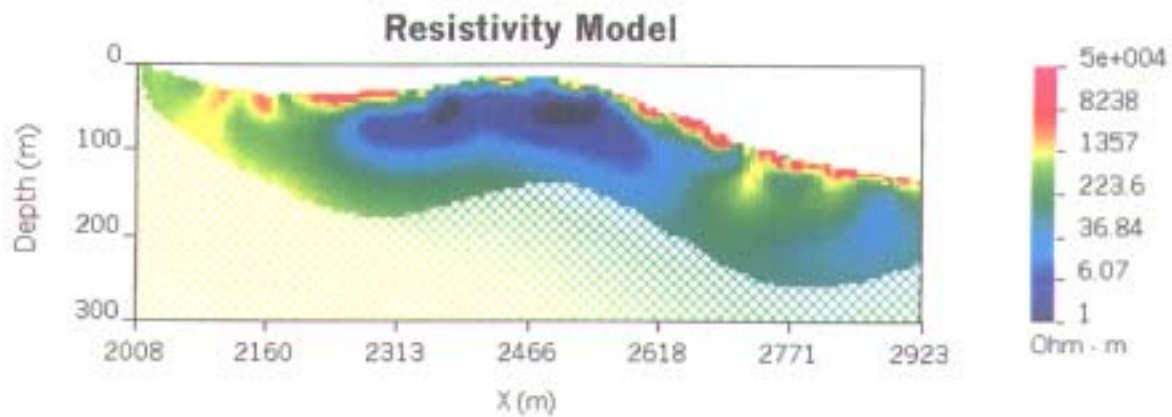
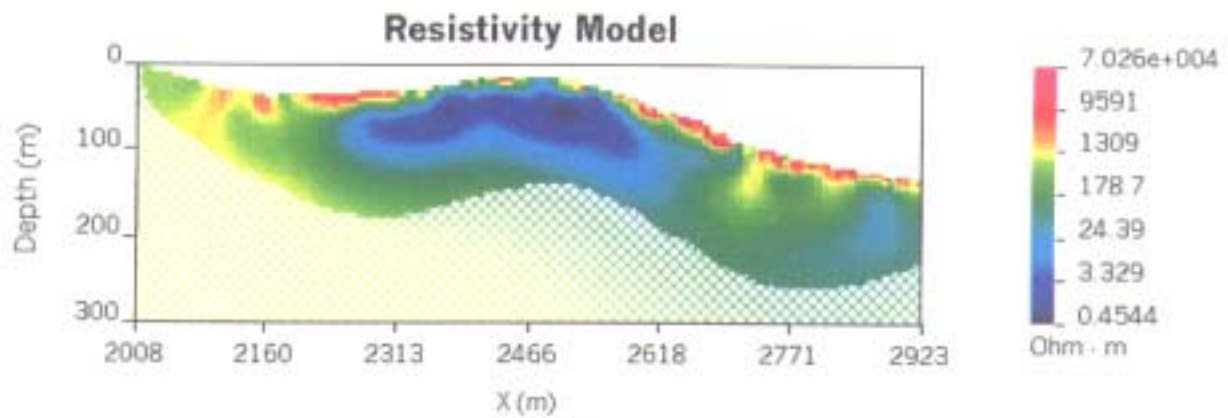
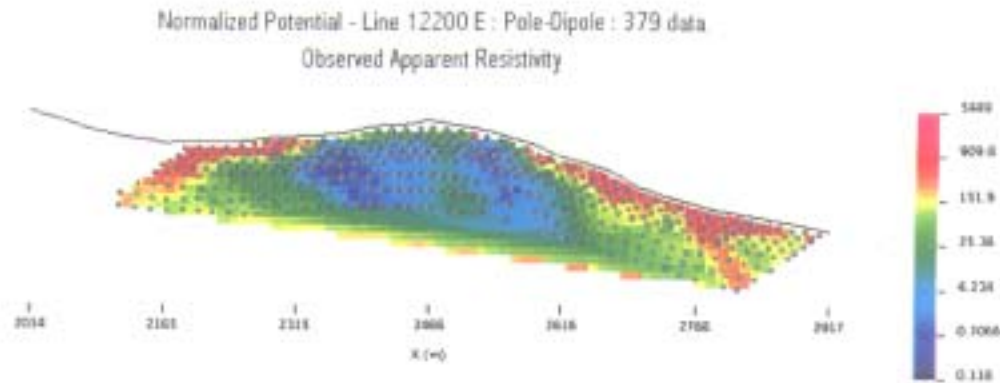
Pseudosection

Mx Chargeability - Line 12600 E : Pole-Dipole : 302 data
Observed Apparent Chargeability

**Chargeability Model****Chargeability Model**

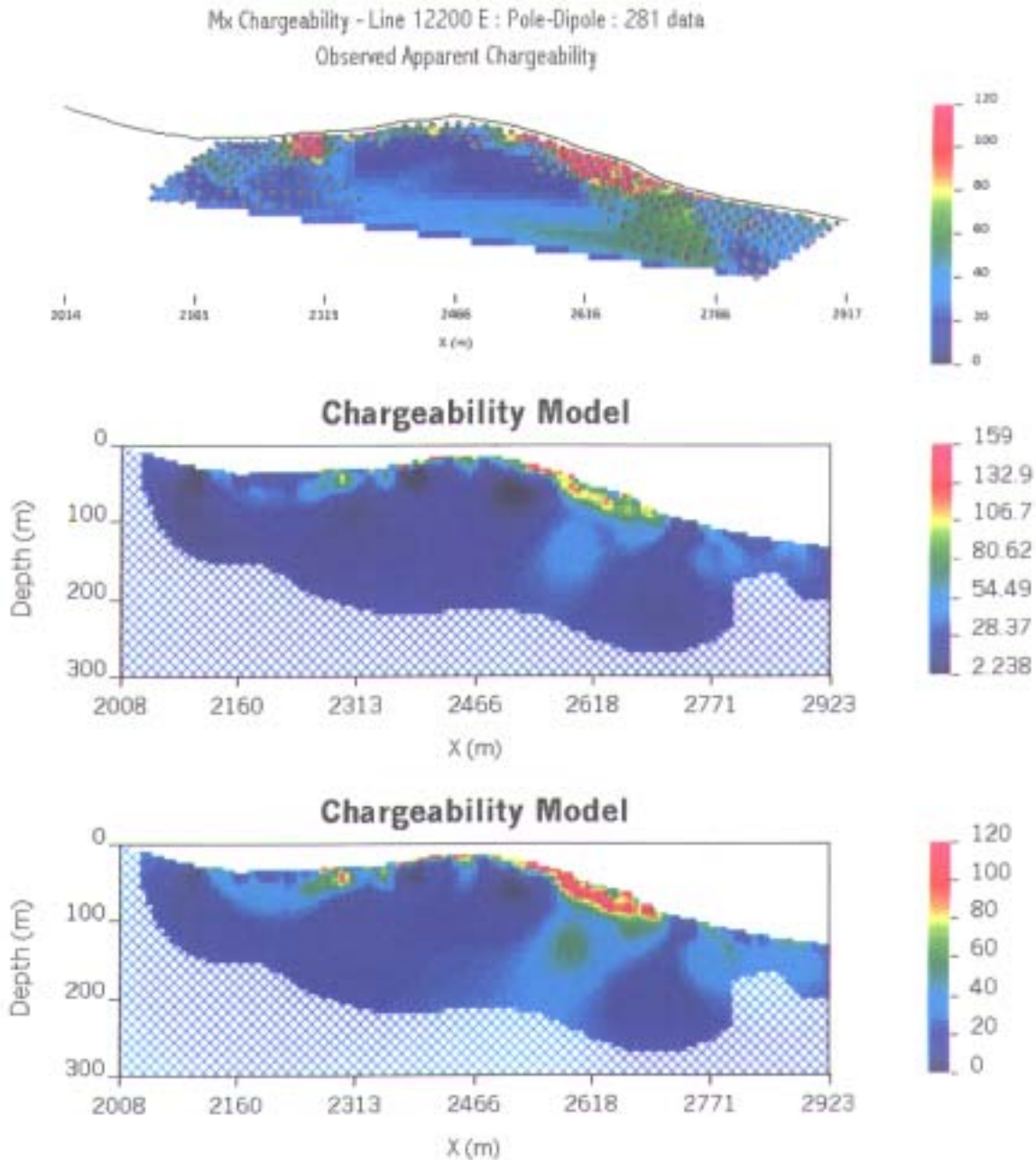
Line 12200E Resistivity

Pseudosection



Line 12200E Chargeability

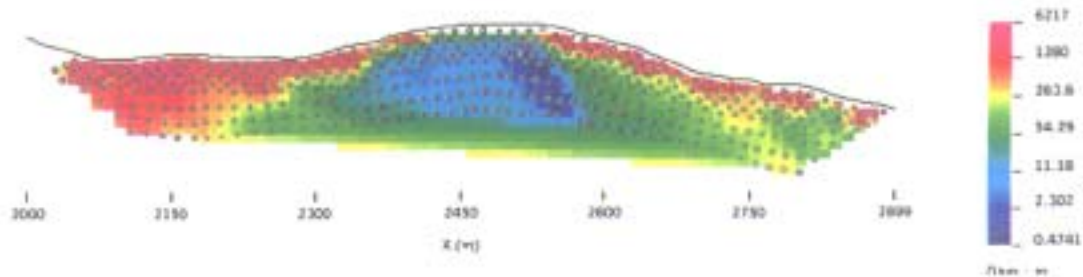
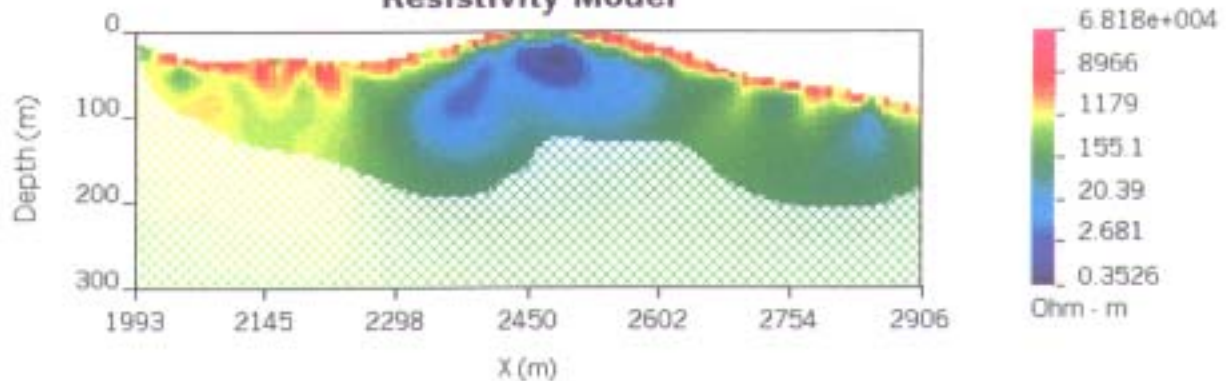
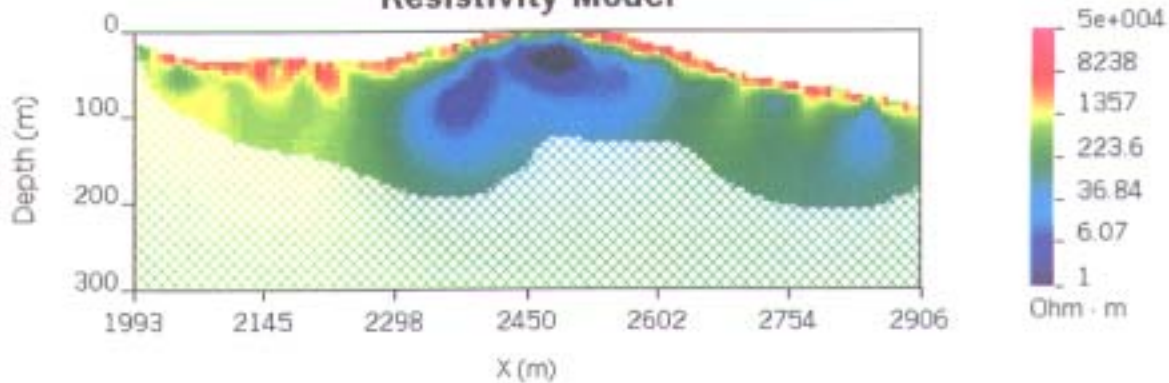
Pseudosection



Line 11800E Resistivity

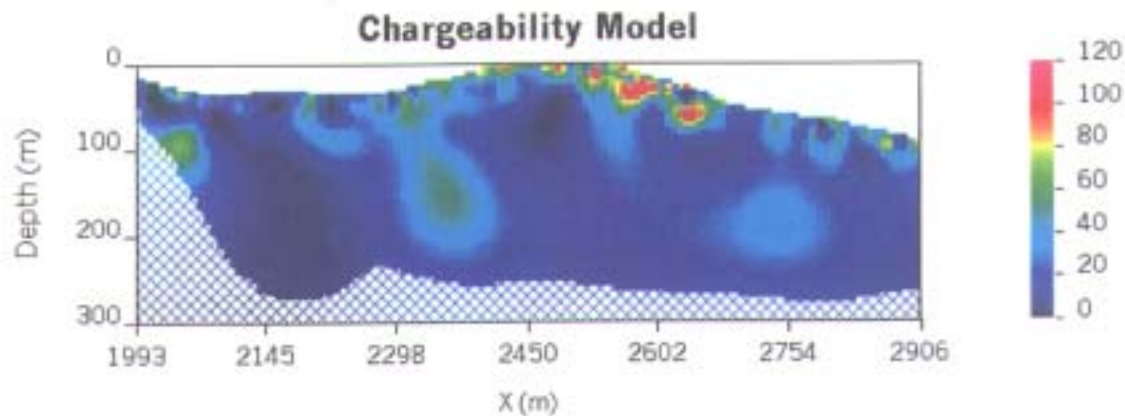
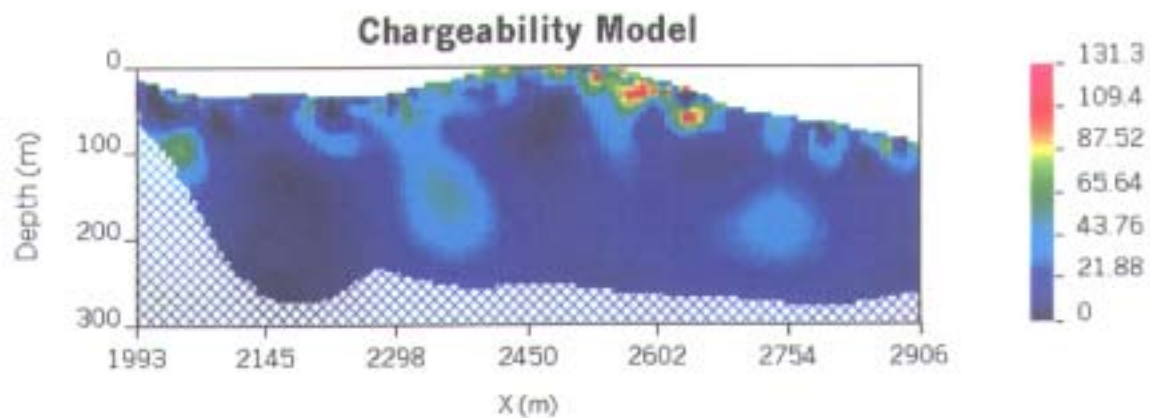
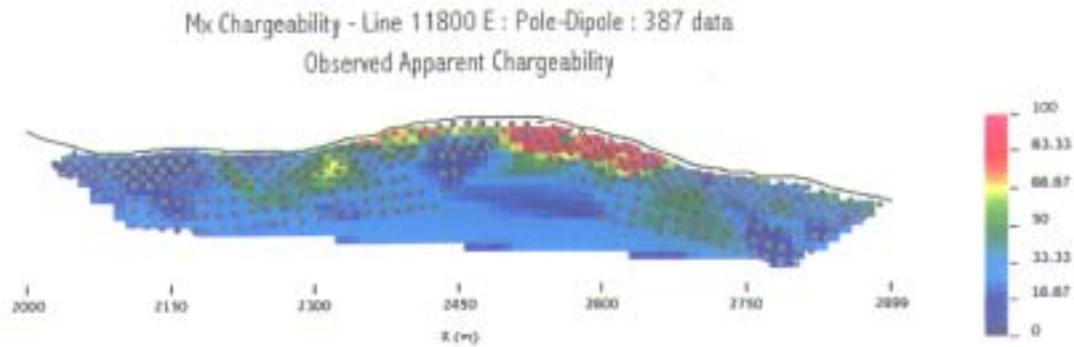
Pseudosection

Normalized Potential - Line 11800 E : Pole-Dipole : 438 data
Observed Apparent Resistivity

**Resistivity Model****Resistivity Model**

Line 11800E Chargeability

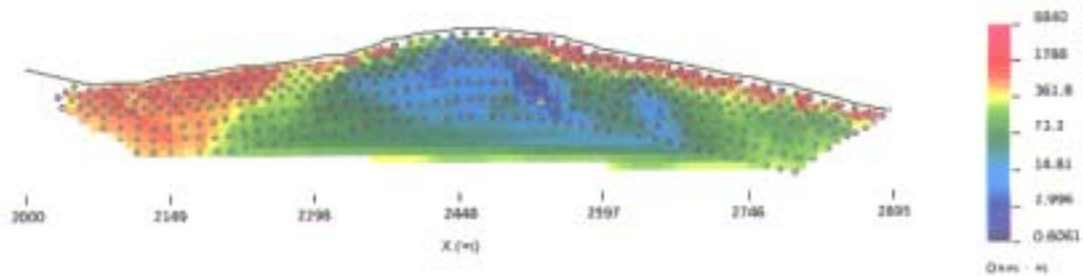
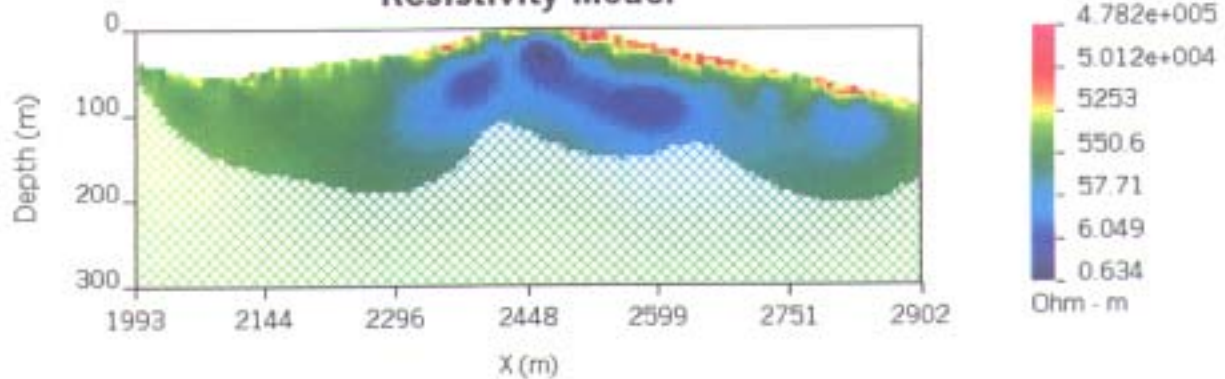
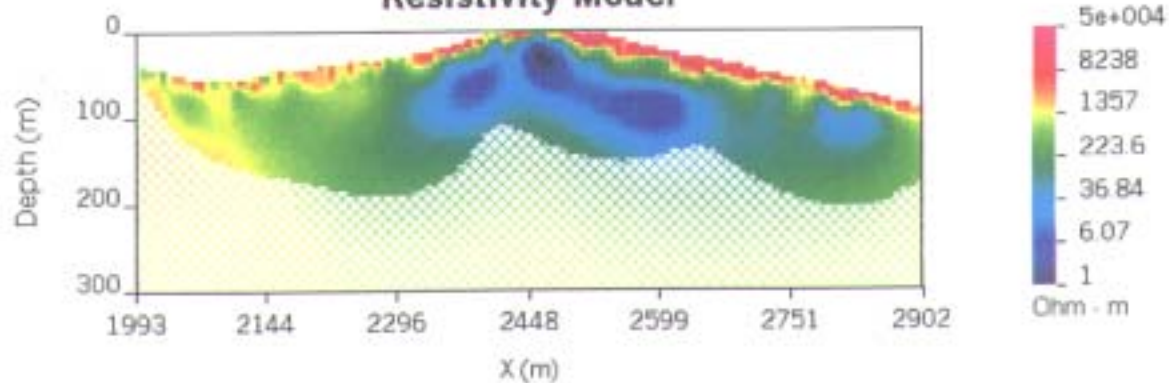
Pseudosection



Line 11600E Resistivity

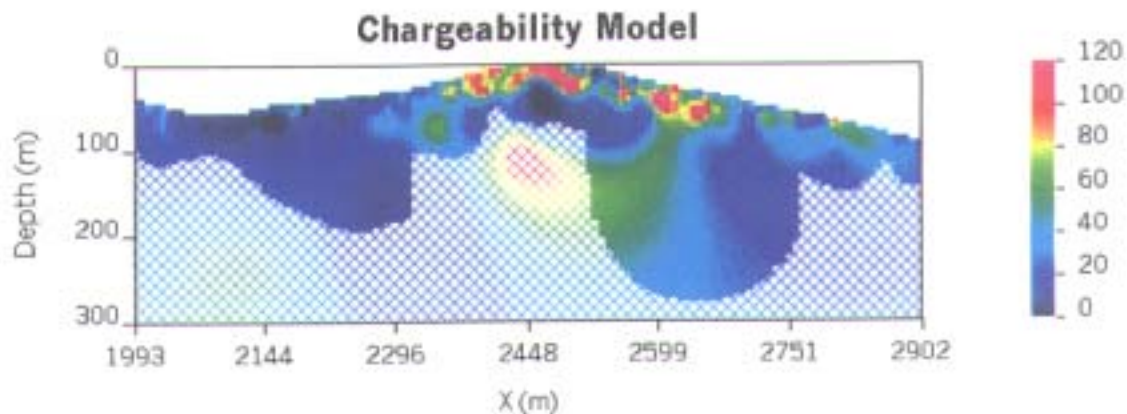
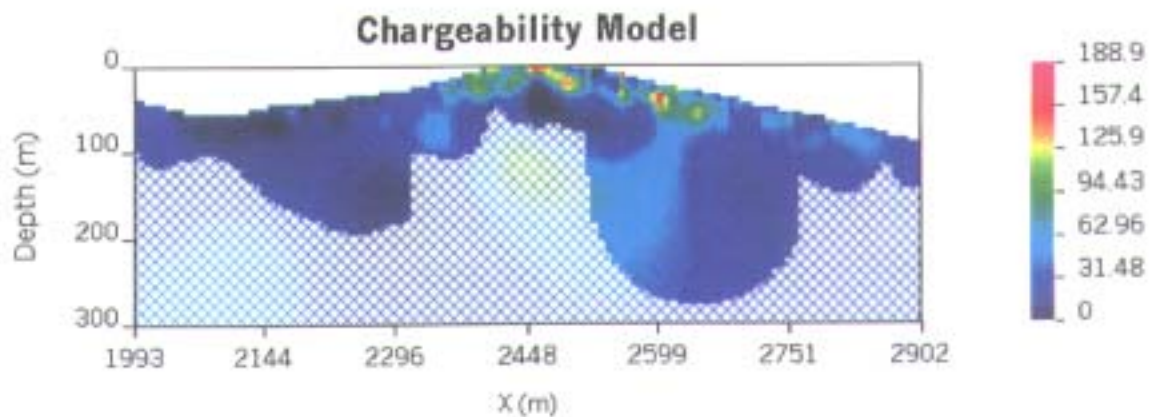
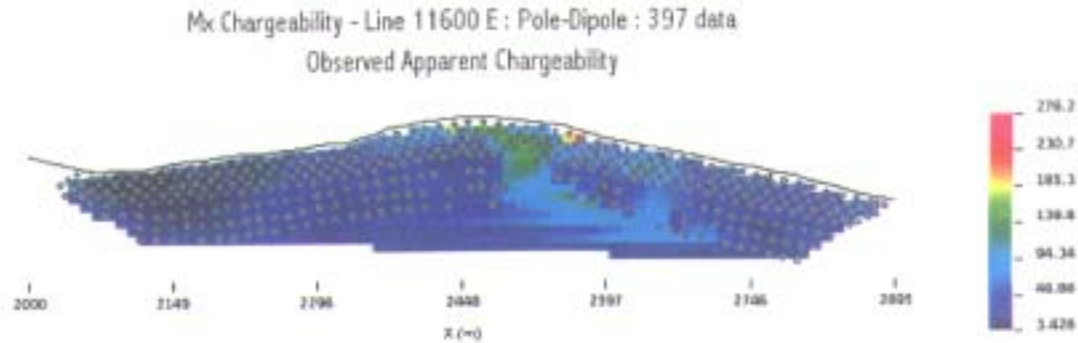
Pseudosection

Normalized Potential - Line 11600 E : Pole-Dipole : 431 data
Observed Apparent Resistivity

**Resistivity Model****Resistivity Model**

Line 11600E Chargeability

Pseudosection

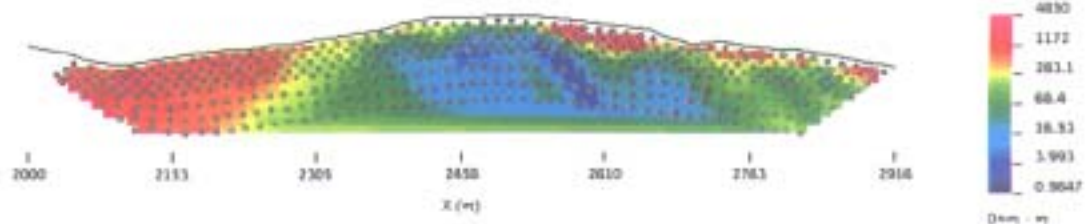
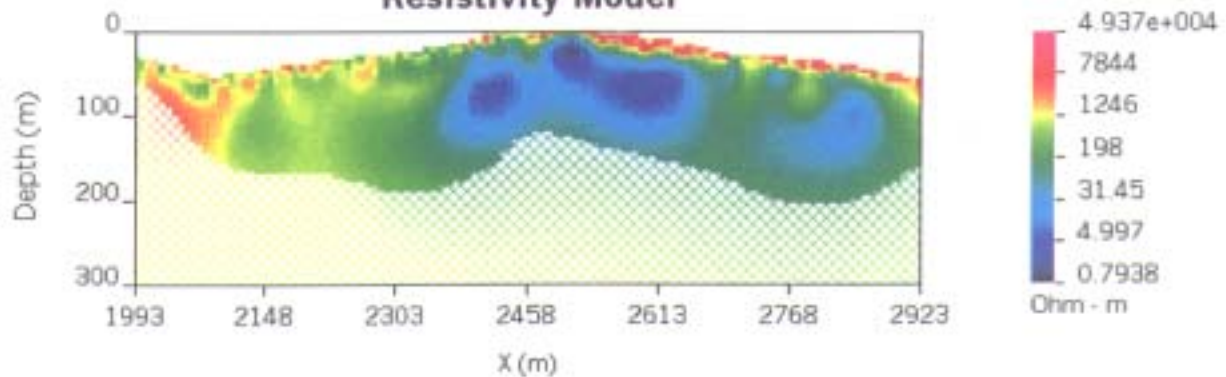
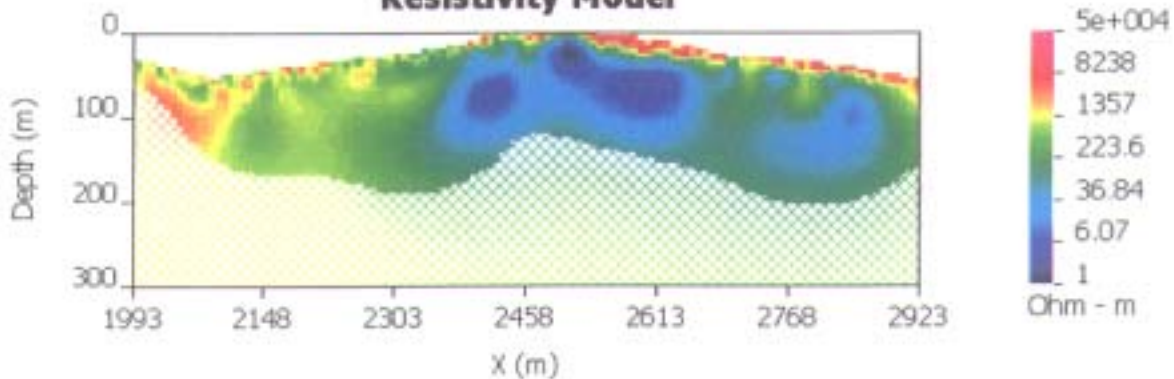


Line 11400E Resistivity

Pseudosection

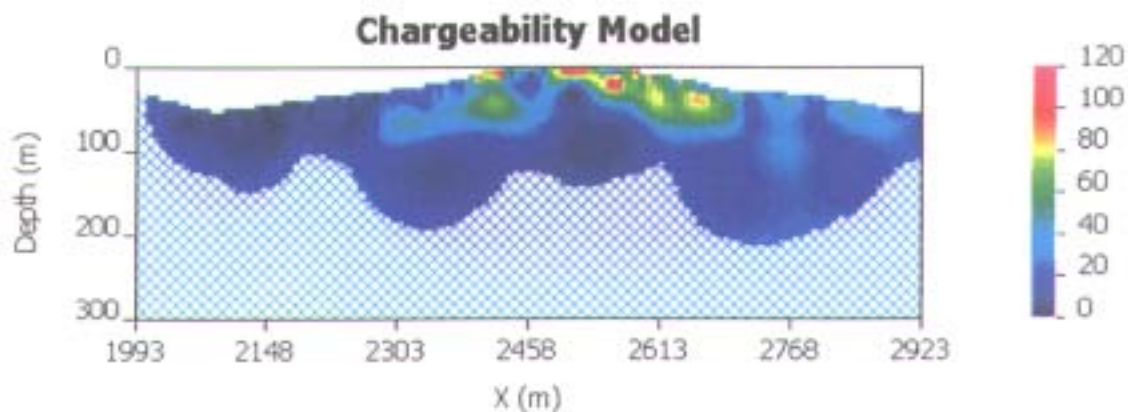
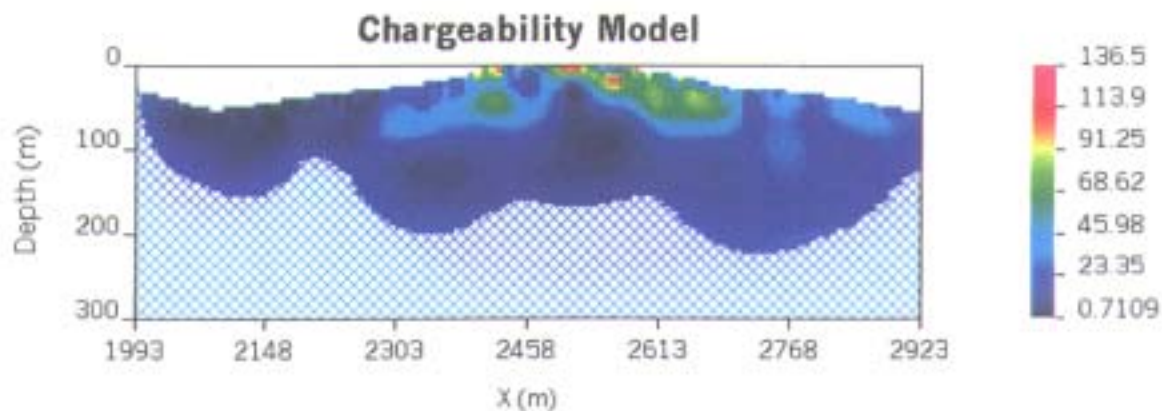
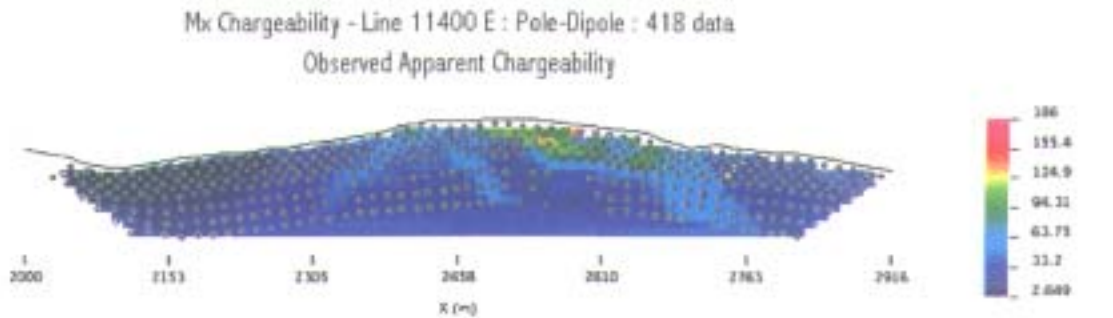
Normalized Potential - Line 11400 E : Pole-Dipole : 439 data

Observed Apparent Resistivity

**Resistivity Model****Resistivity Model**

Line 11400E Chargeability

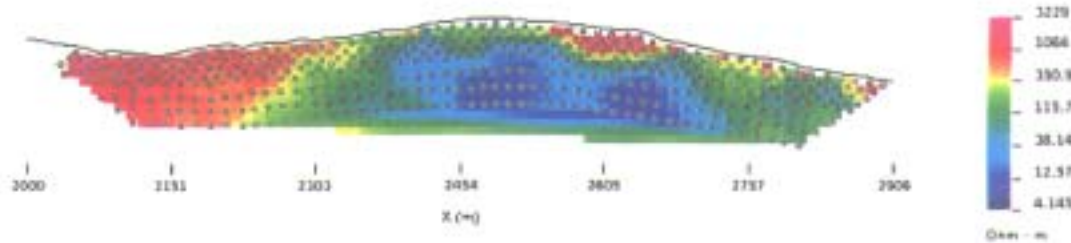
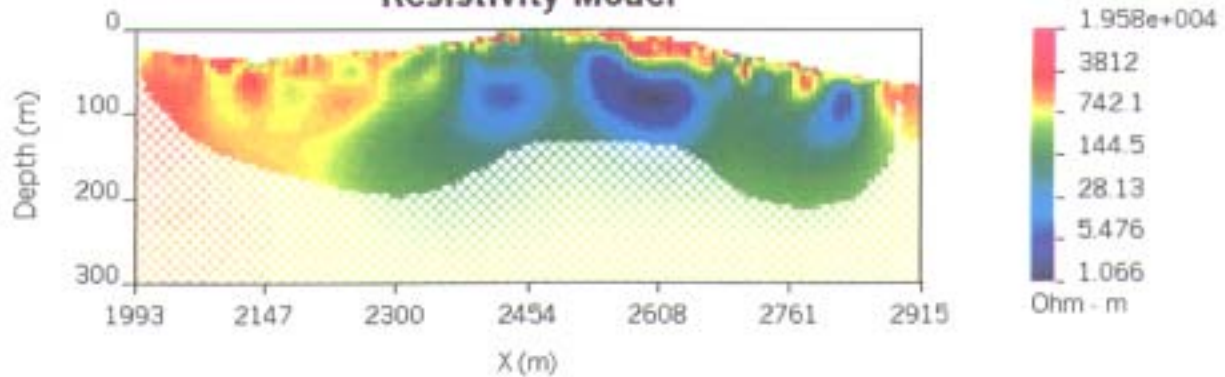
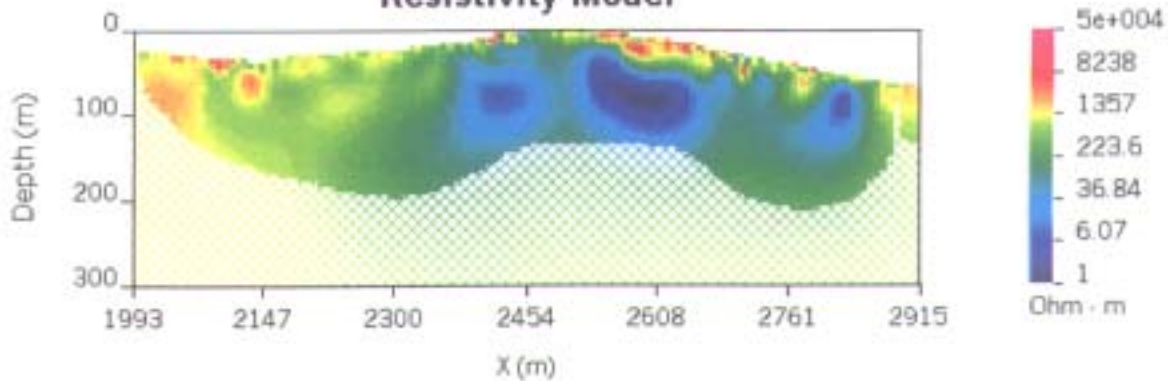
Pseudosection



Line 11200E Resistivity

Pseudosection

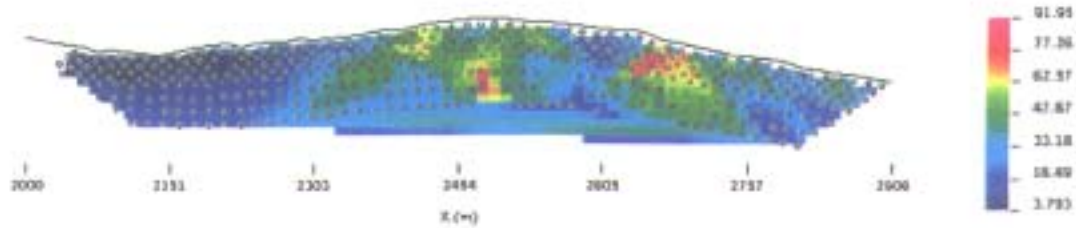
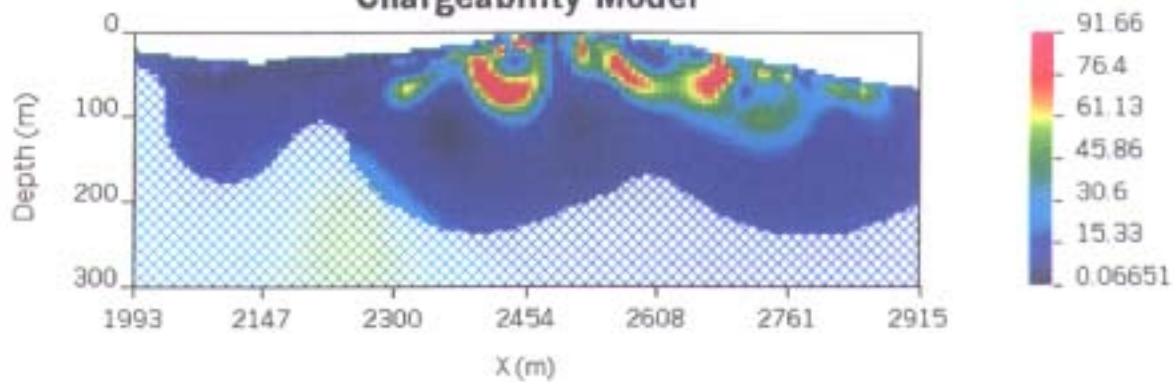
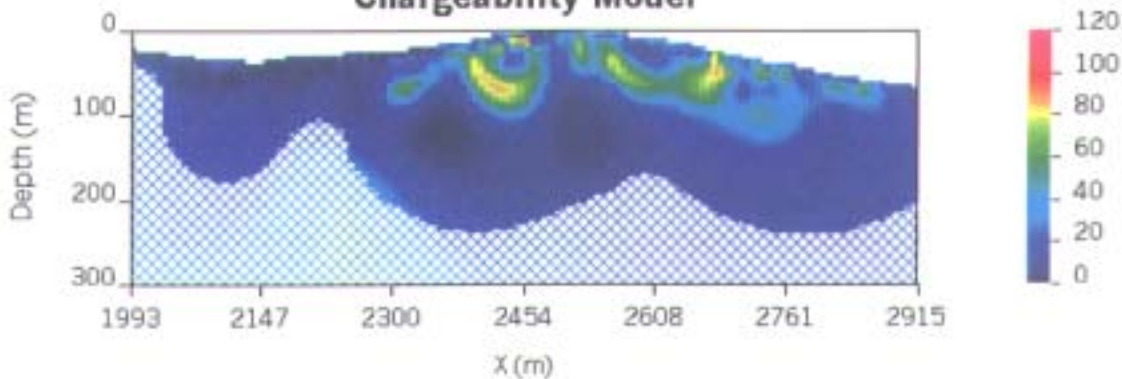
Normalized Potential - Line 11200 E : Pole-Dipole : 430 data
Observed Apparent Resistivity

**Resistivity Model****Resistivity Model**

Line 11200E Chargeability

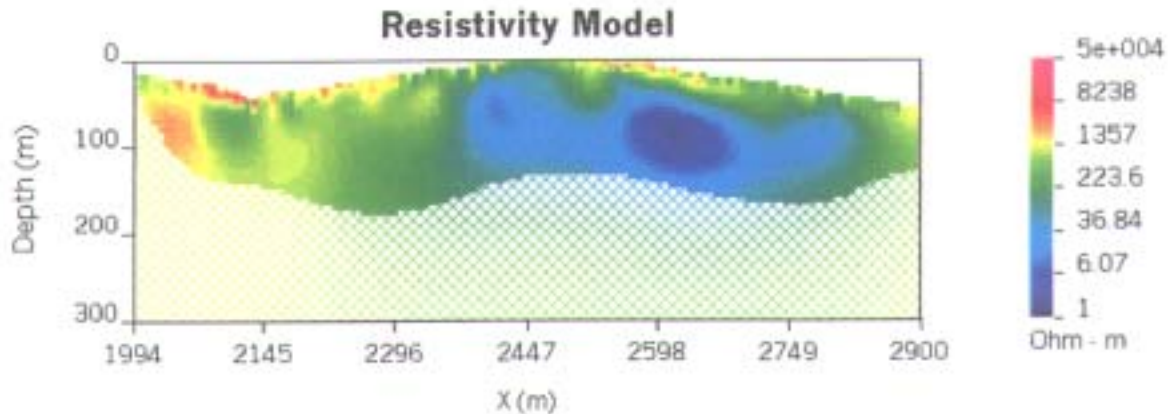
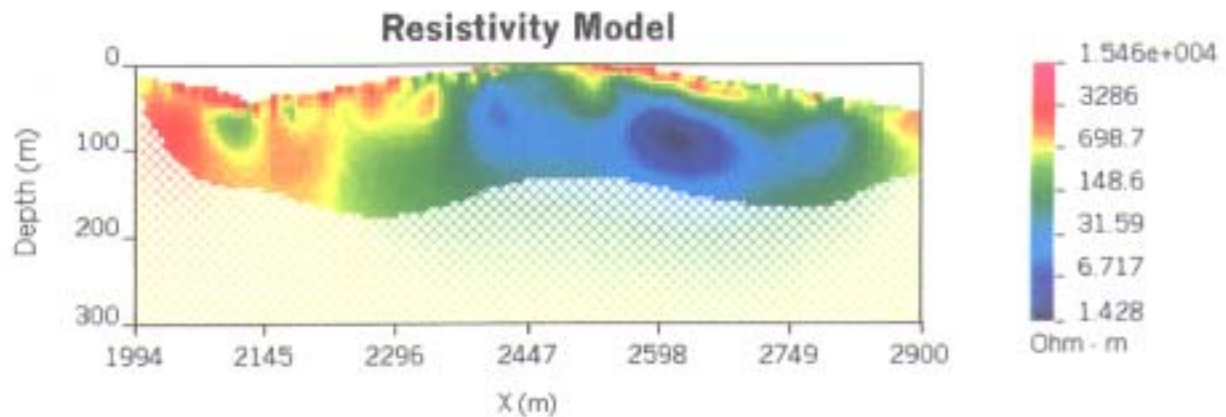
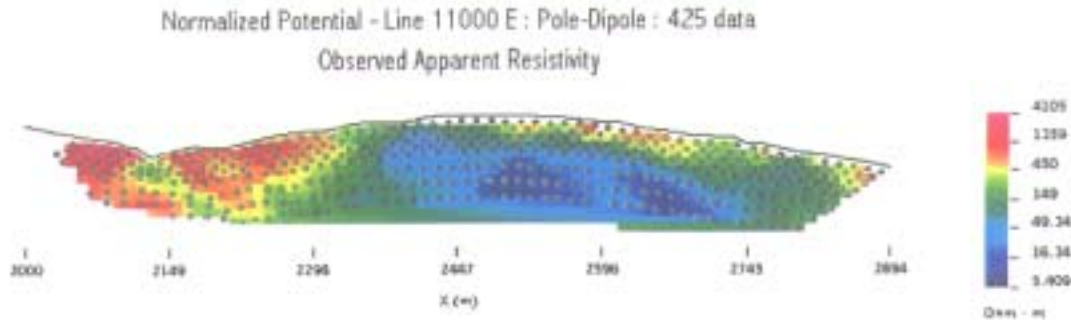
Pseudosection

Mx Chargeability - Line 11200 E : Pole-Dipole : 411 data
Observed Apparent Chargeability

**Chargeability Model****Chargeability Model**

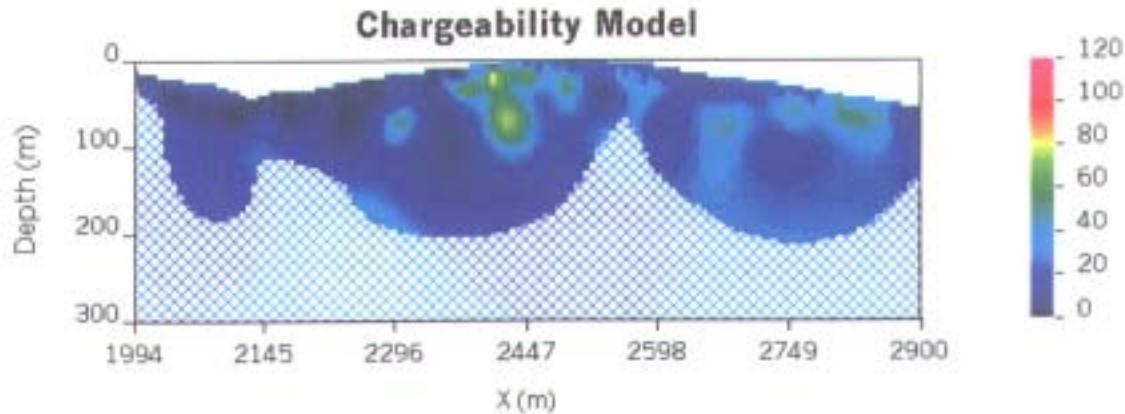
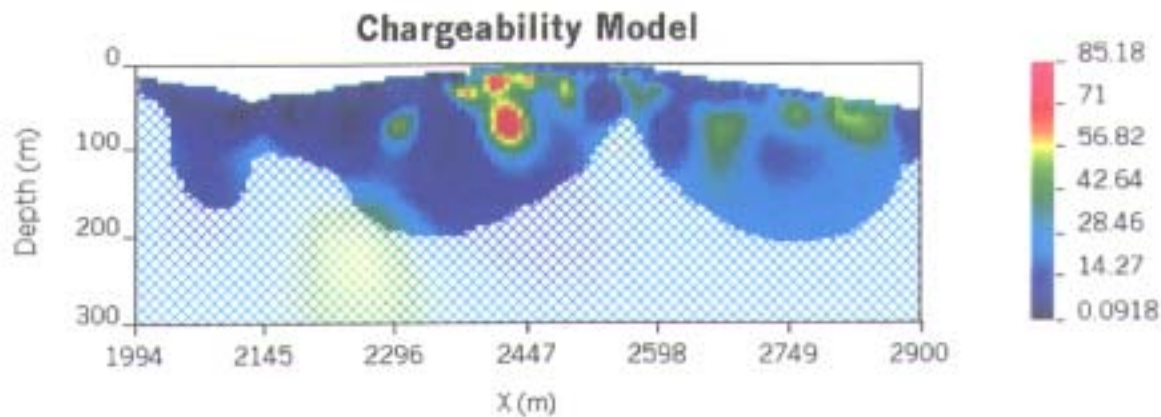
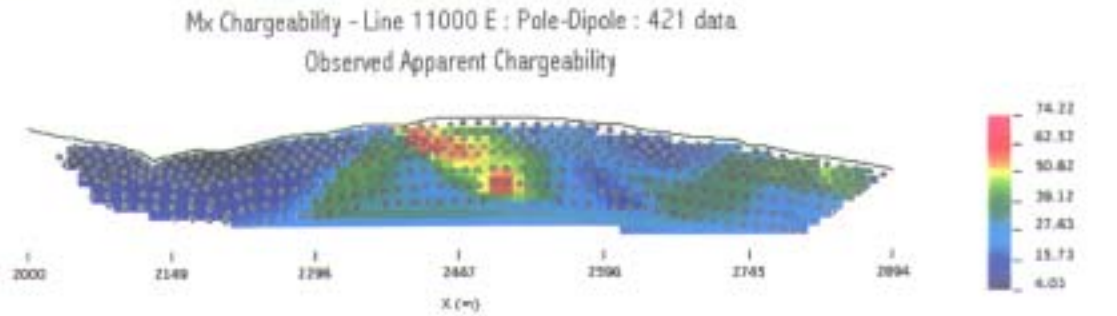
Line 11000E Resistivity

Pseudosection



Line 11000E Chargeability

Pseudosection

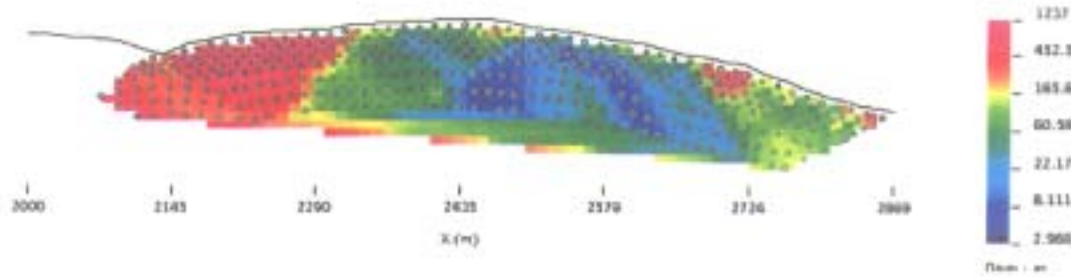
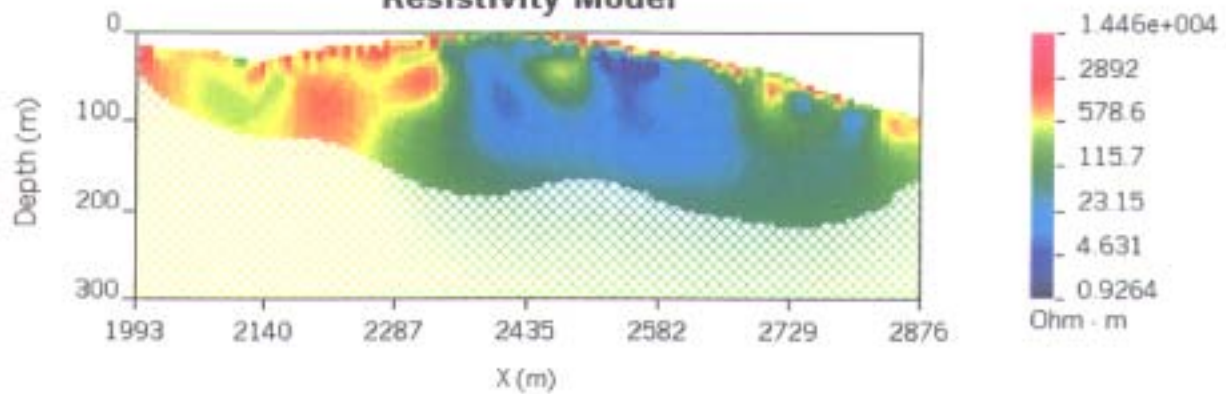
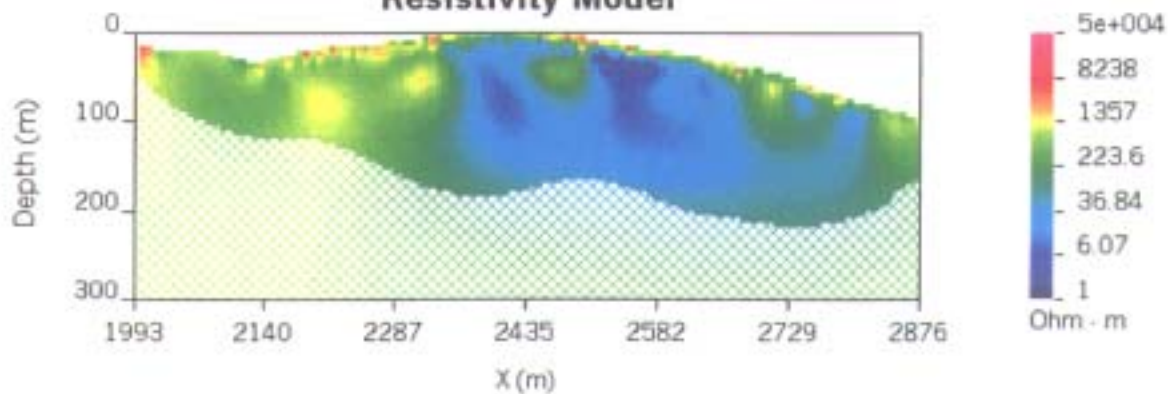


Line 10800E Resistivity

Pseudosection

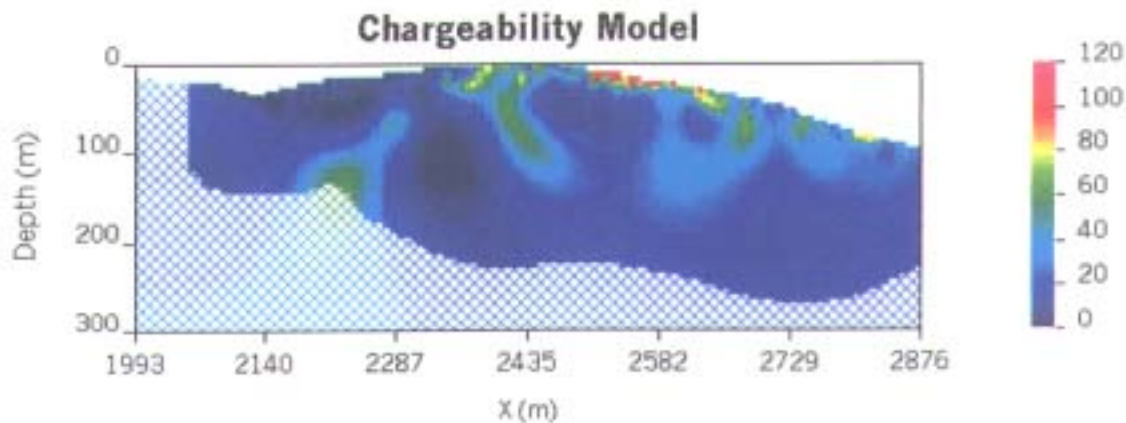
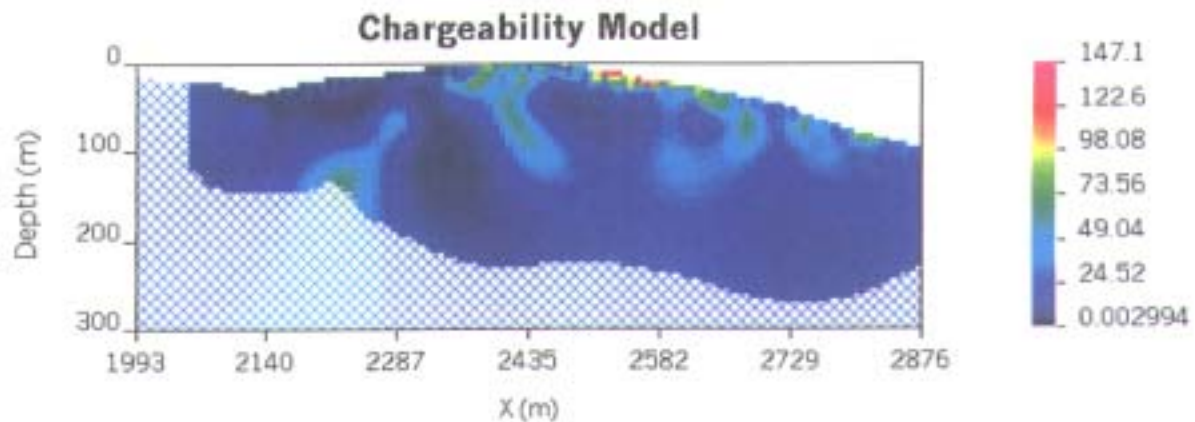
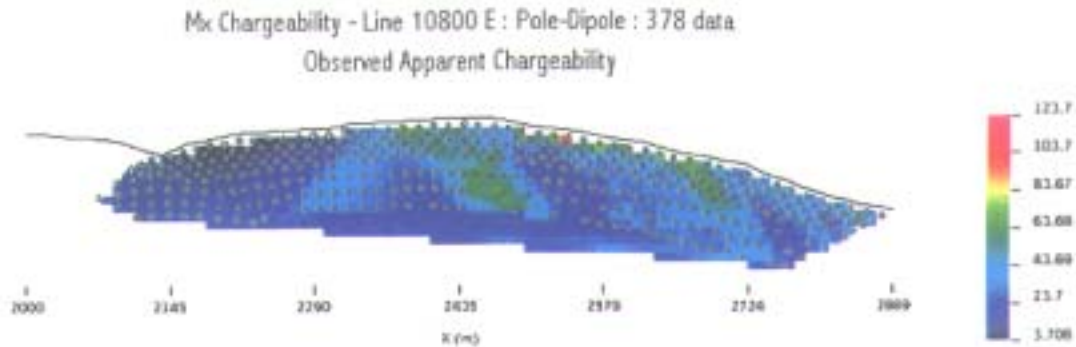
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Observed Apparent Resistivity

**Resistivity Model****Resistivity Model**

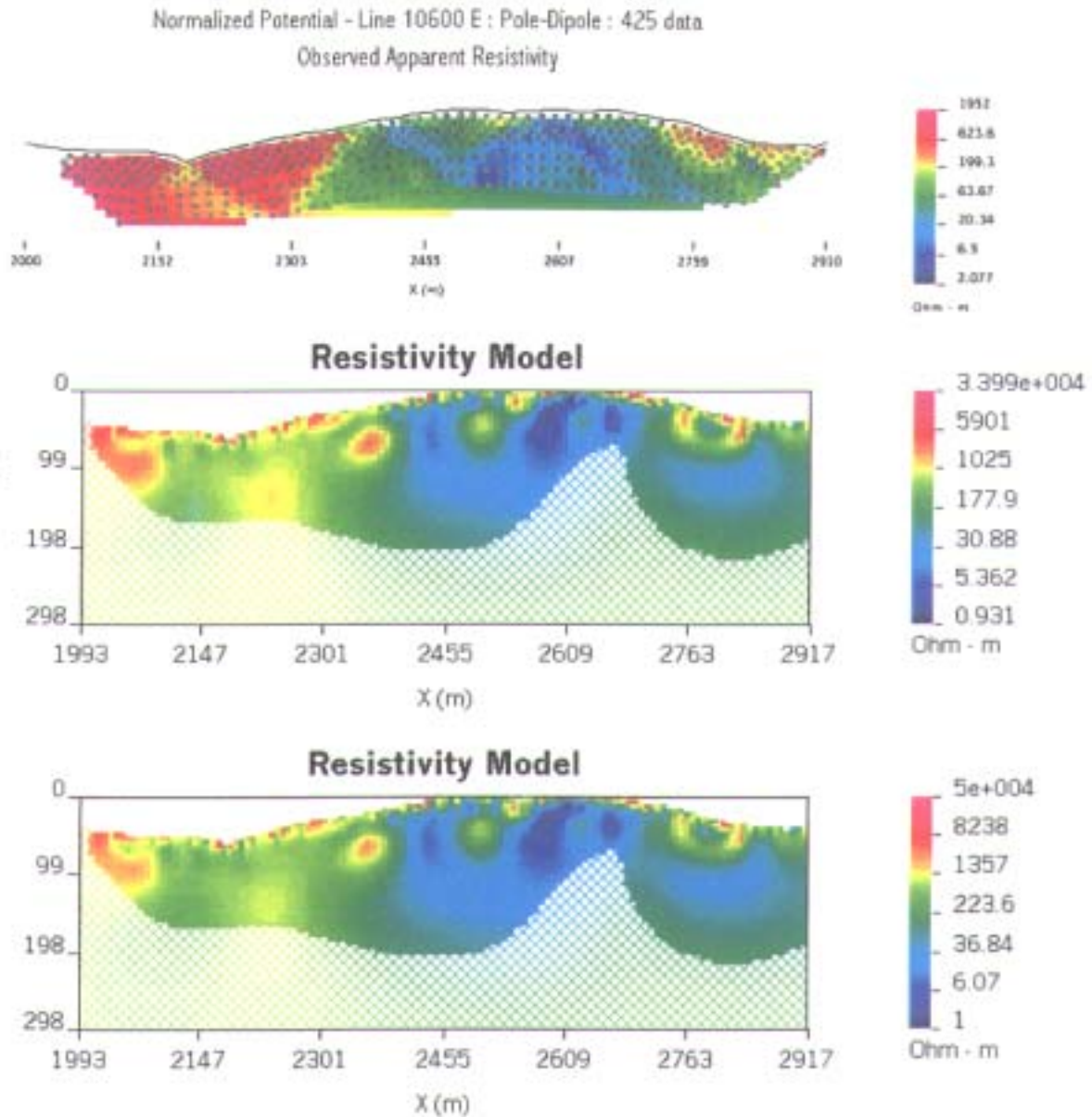
Line 10800E Chargeability

Pseudosection



Line 10600E Resistivity

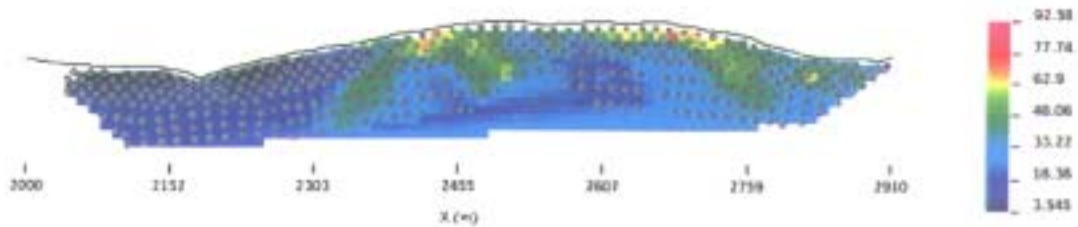
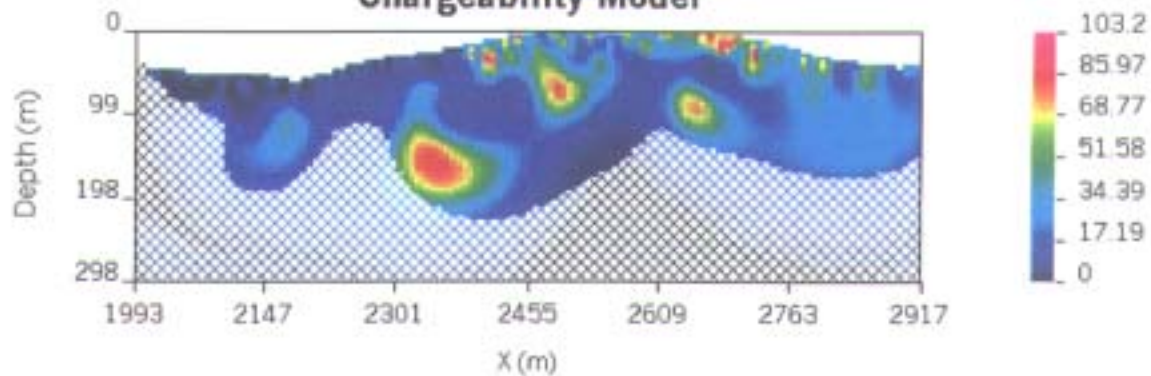
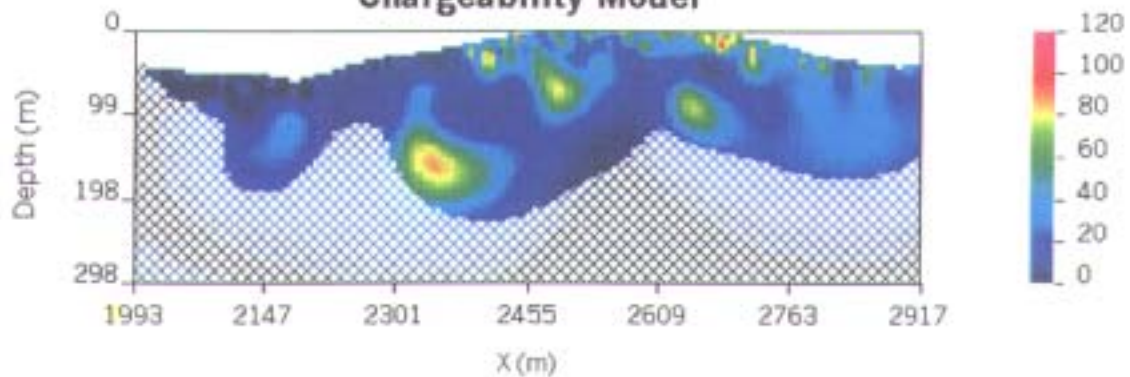
Pseudosection



Line 10600E Chargeability

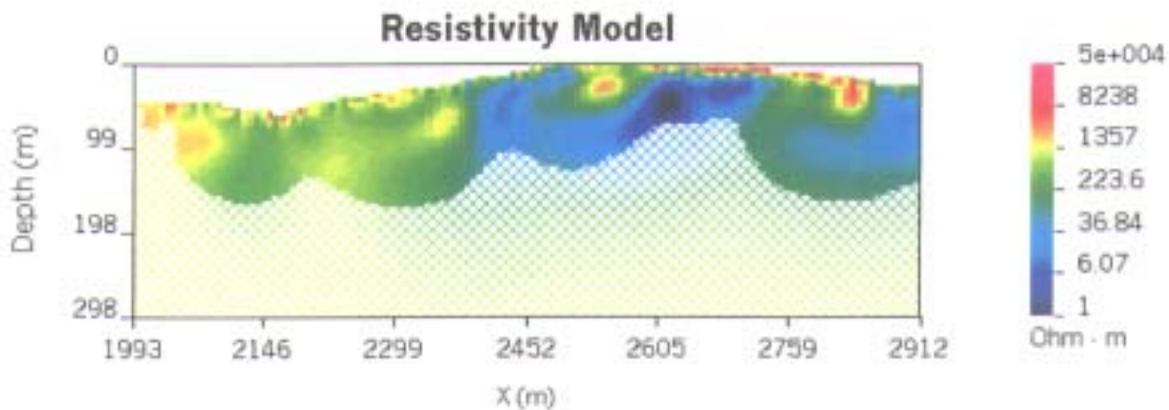
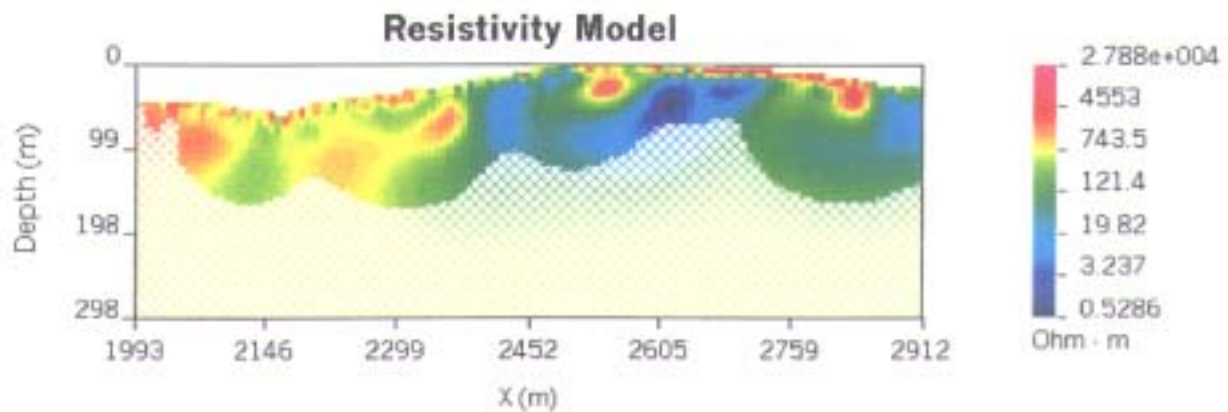
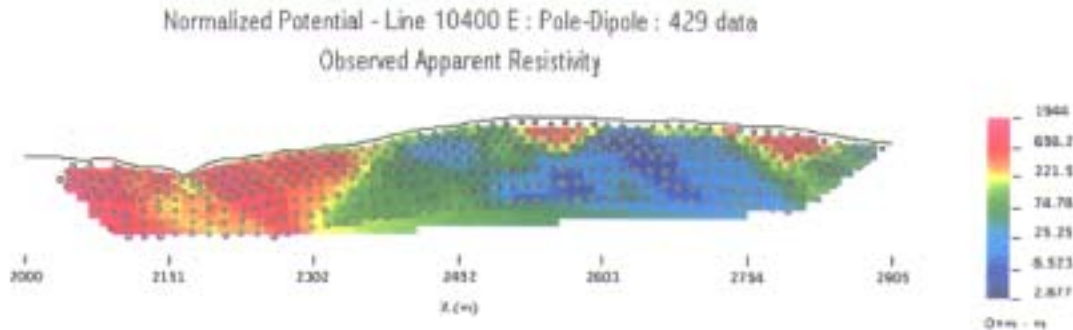
Pseudosection

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Observed Apparent Chargeability

**Chargeability Model****Chargeability Model**

Line 10400E Resistivity

Pseudosection

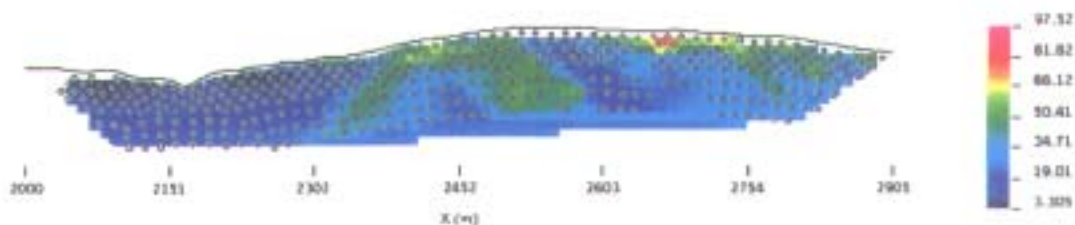


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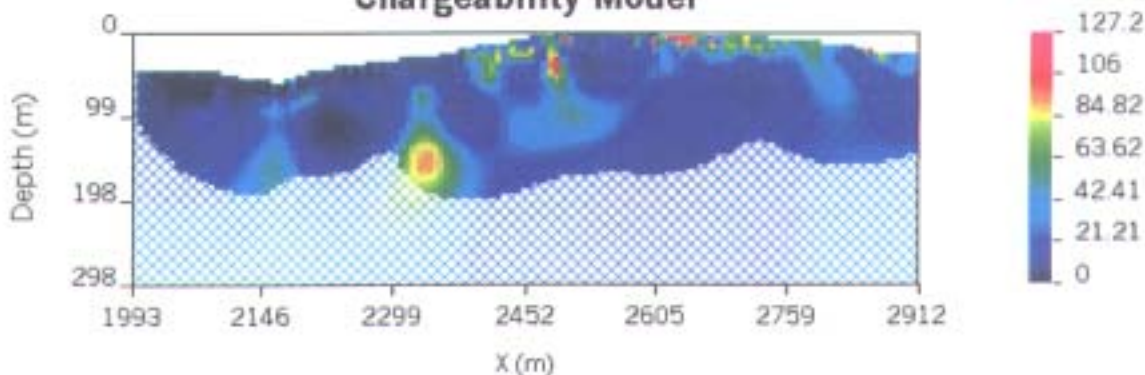
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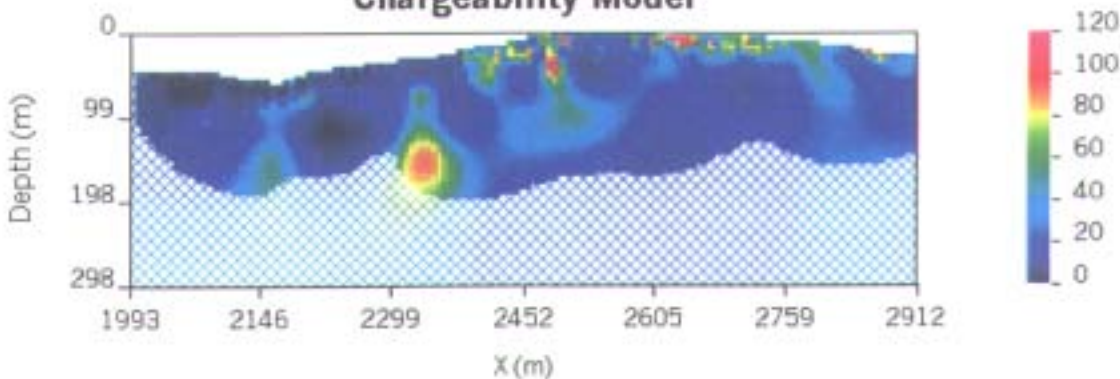
Observed Apparent Chargeability



Chargeability Model



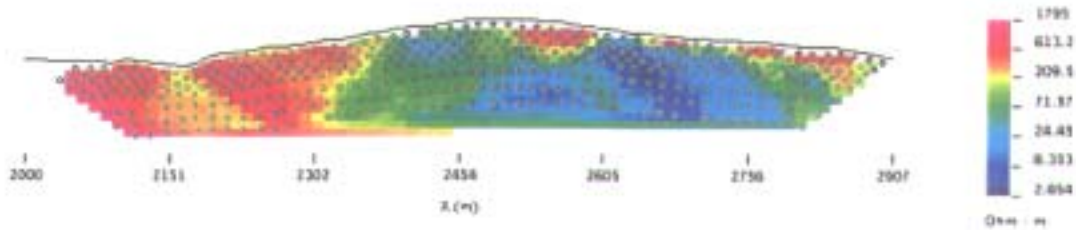
Chargeability Model



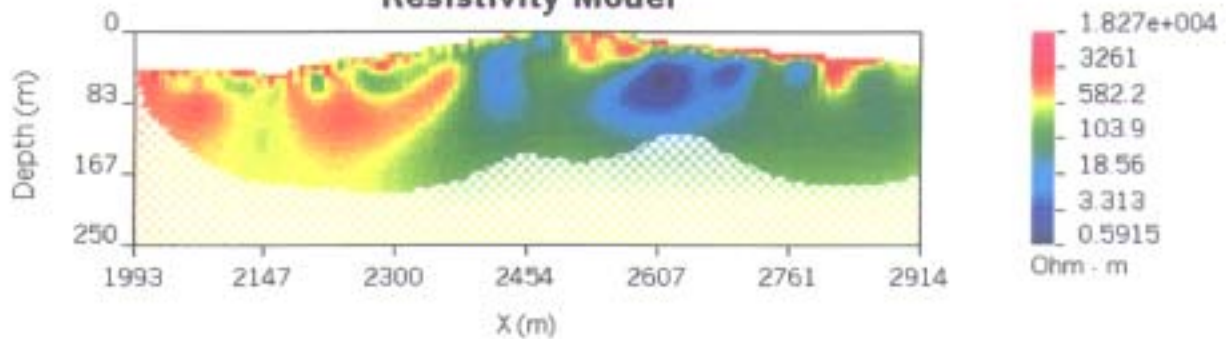
Line 10200E Resistivity

Pseudosection

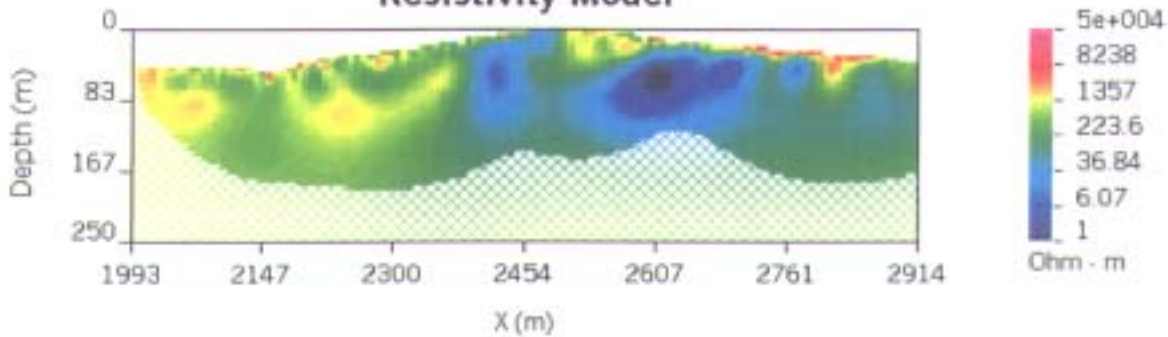
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Observed Apparent Resistivity



Resistivity Model

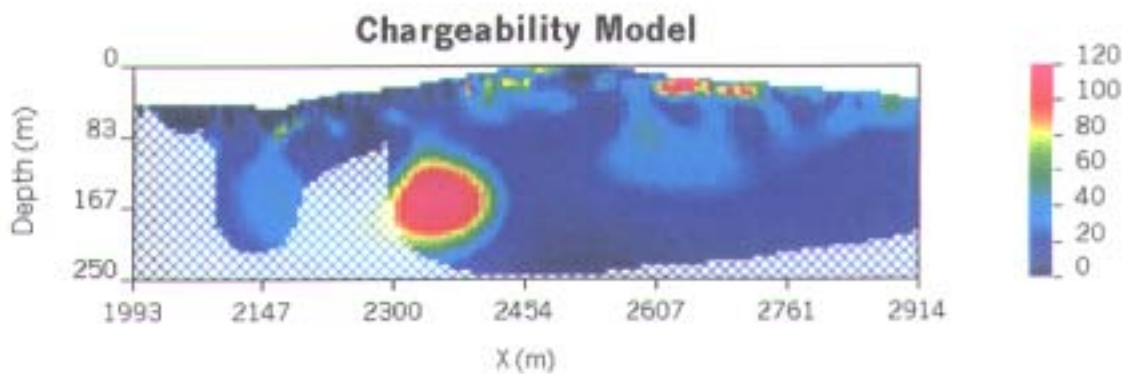
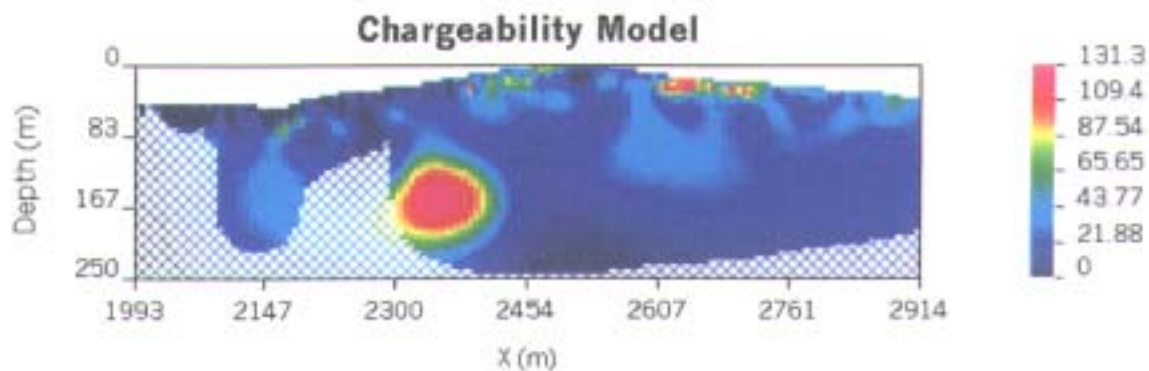
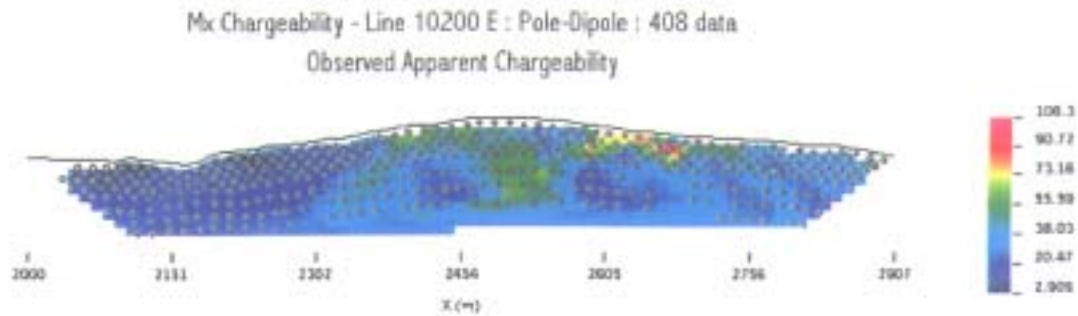


Resistivity Model



Line 10200E Chargeability

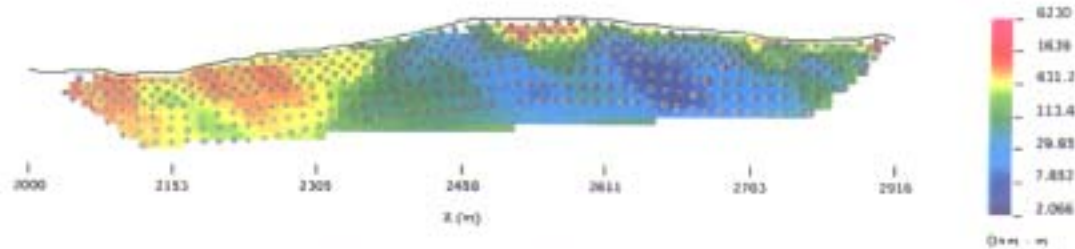
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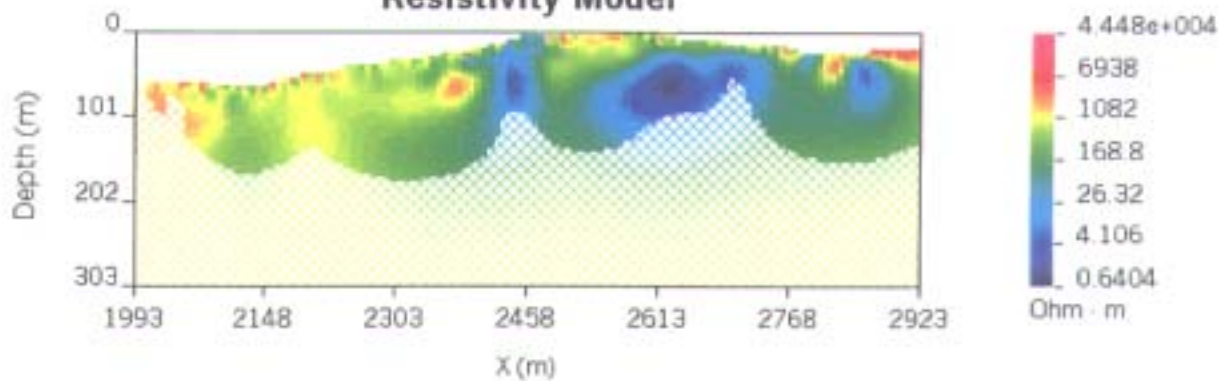
Line 10000E Resistivity

Pseudosection

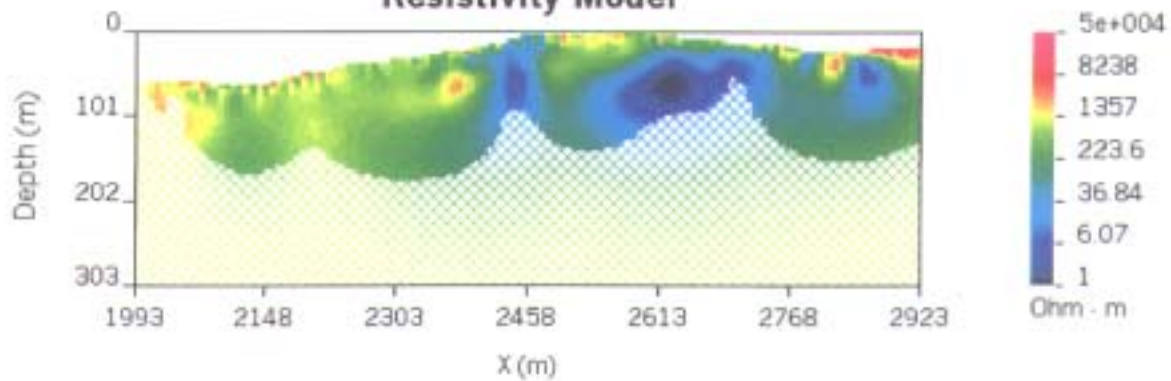
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Observed Apparent Resistivity



Resistivity Model

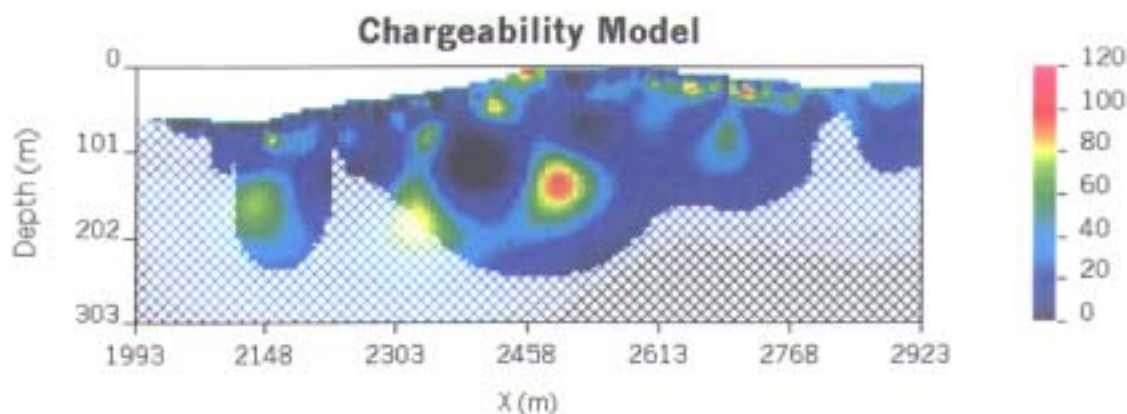
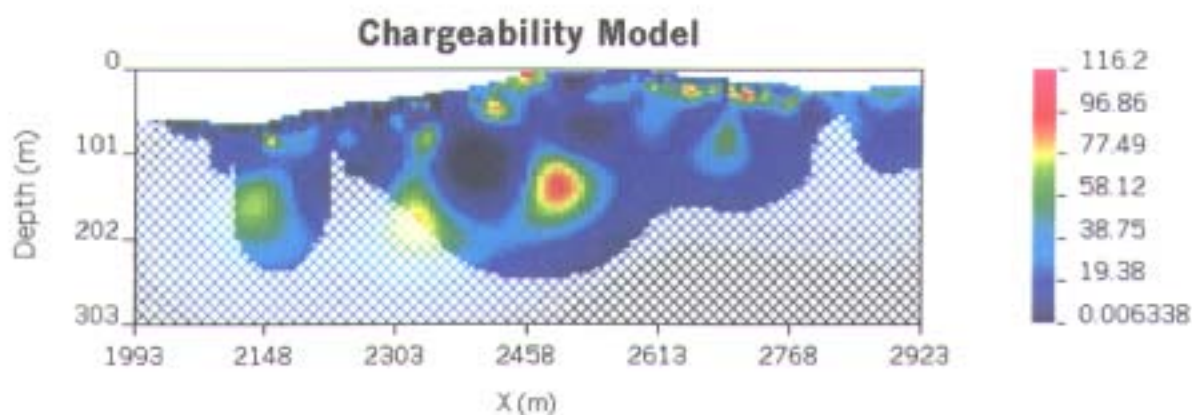
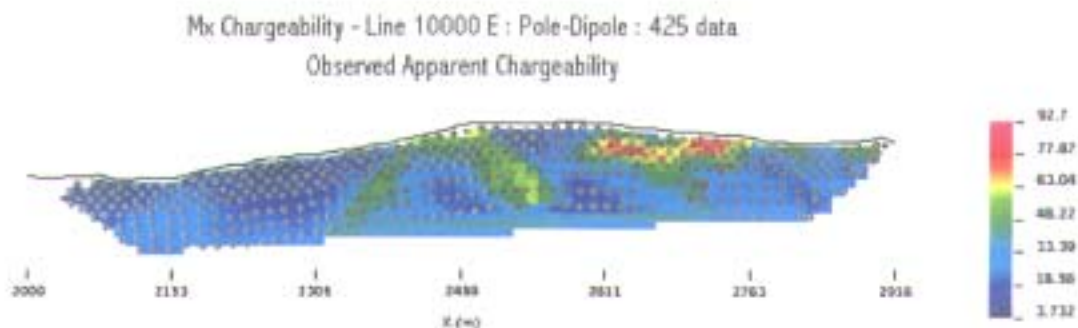


Resistivity Model



Line 10000E Chargeability

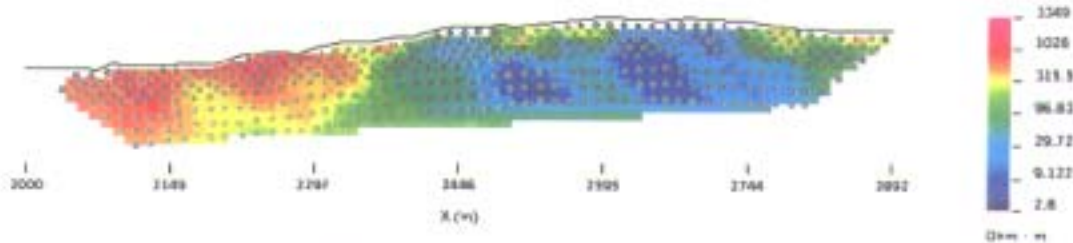
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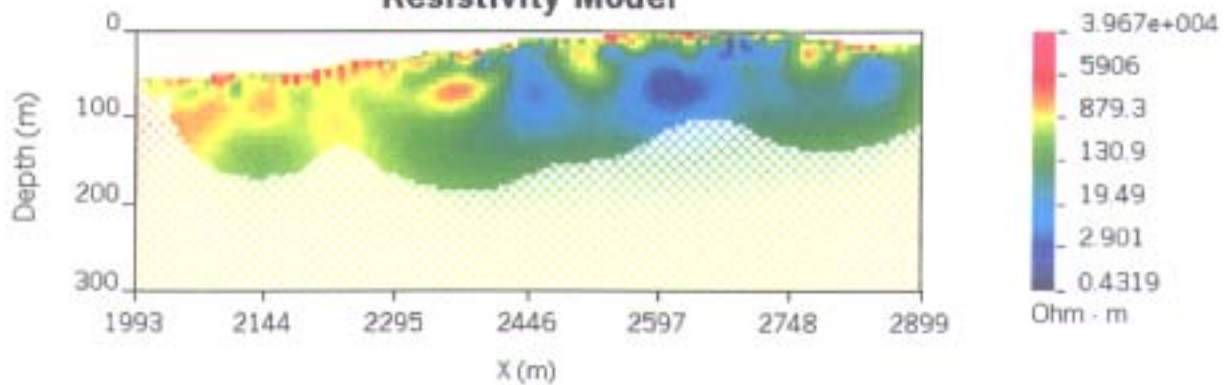
Line 9800E Resistivity

Pseudosection

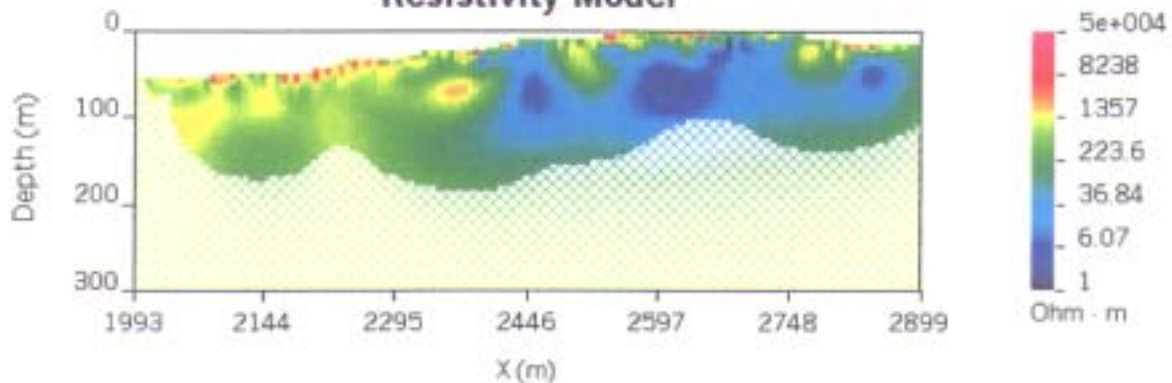
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Observed Apparent Resistivity



Resistivity Model



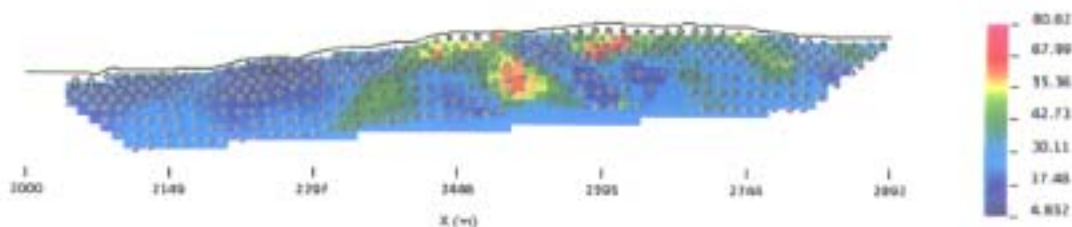
Resistivity Model



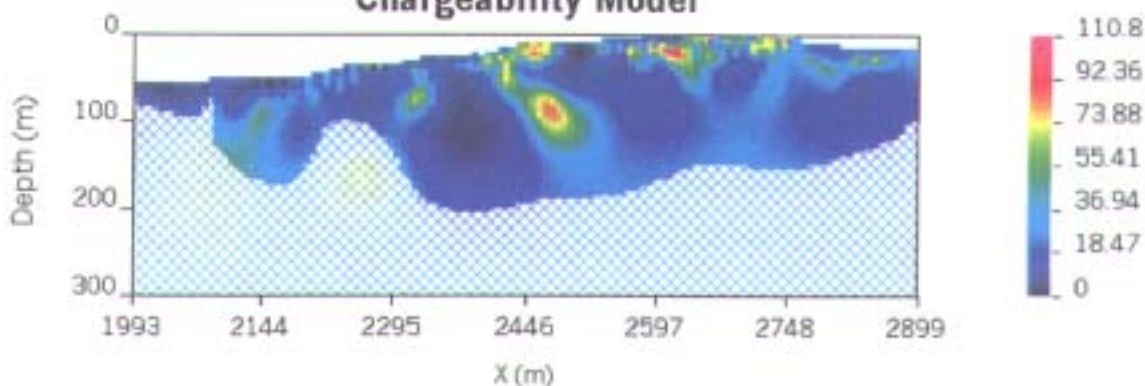
Line 9800E Chargeability

Pseudosection

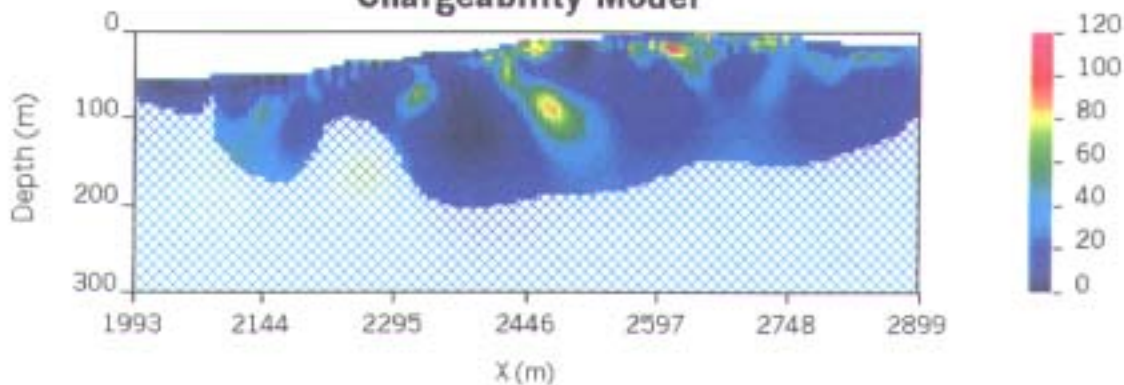
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Observed Apparent Chargeability



Chargeability Model

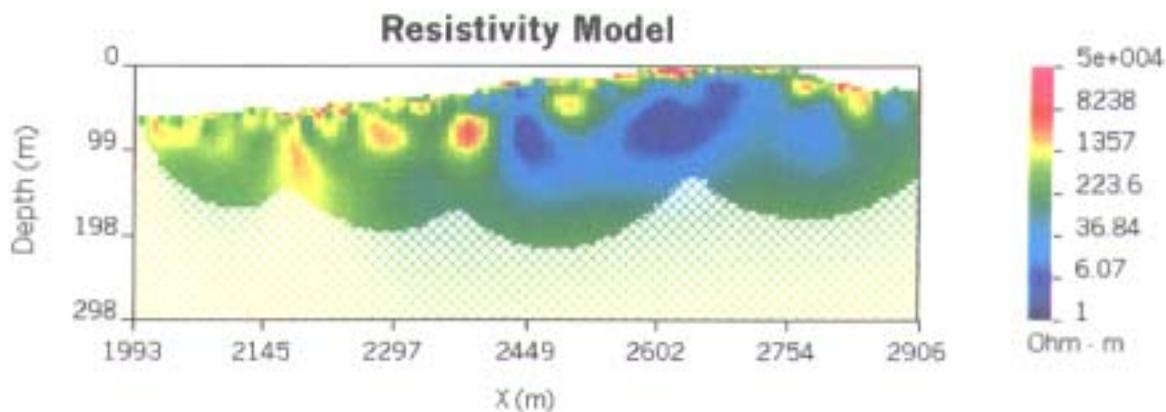
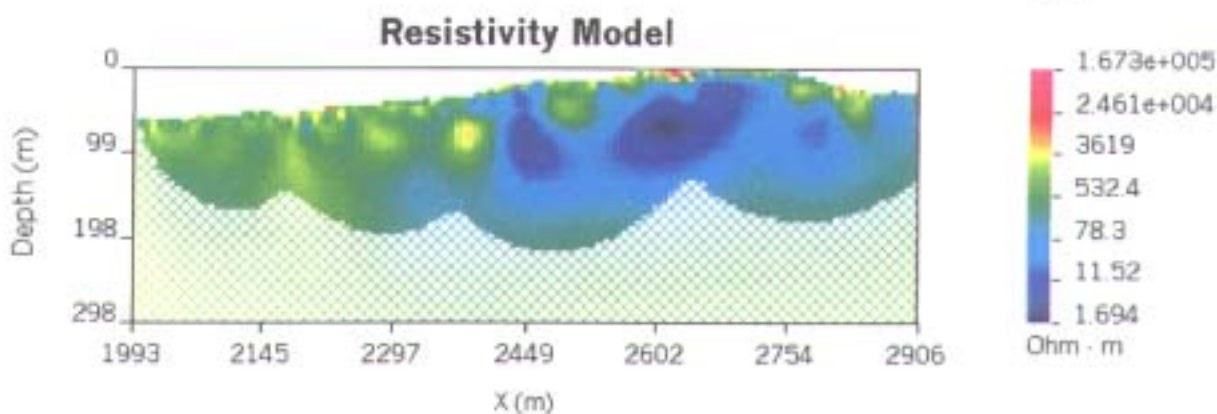
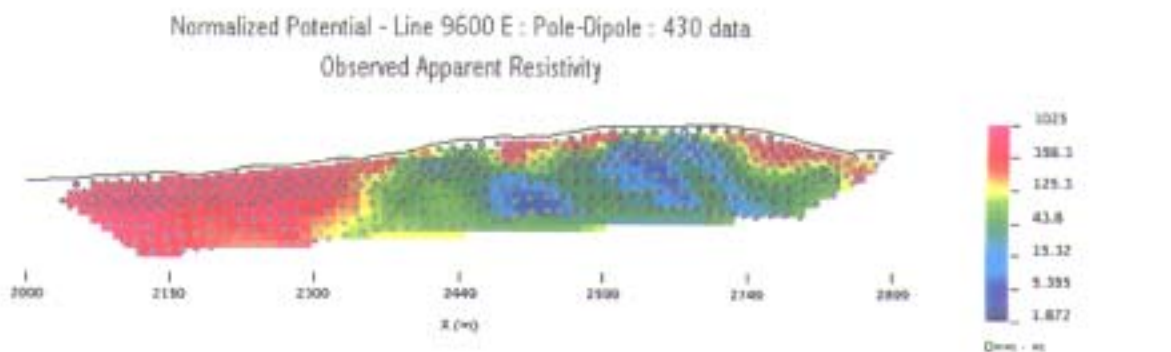


Chargeability Model



Line 9600E Resistivity

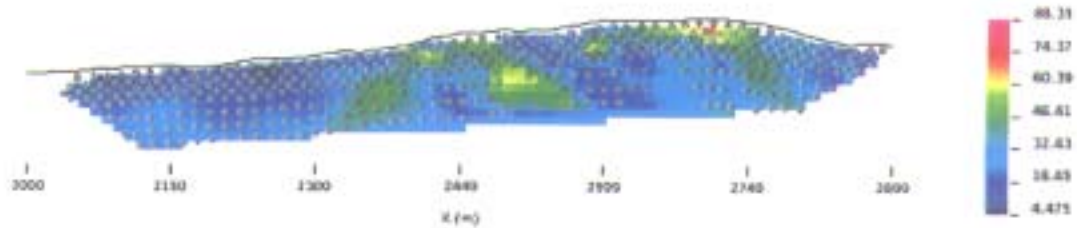
Pseudosection



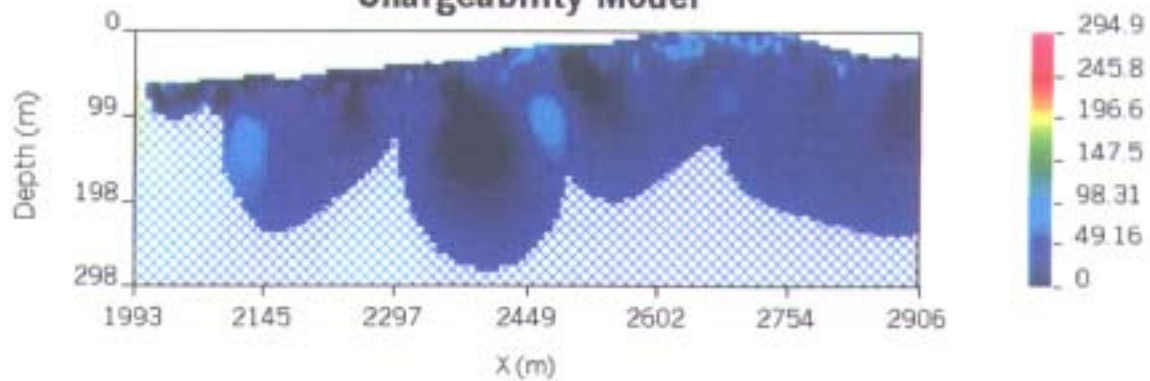
Line 9600E Chargeability

Pseudosection

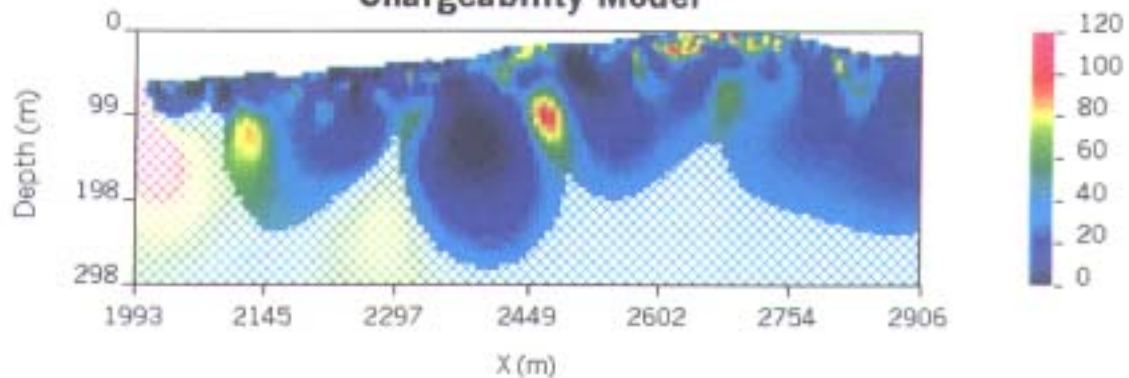
Mx Chargeability - Line 9600 E : Pole-Dipole : 406 data
Observed Apparent Chargeability



Chargeability Model



Chargeability Model



APPENDIX 4 – SELF POTENTIAL REPORT
By A. Justason.

2001 SUMMARY REPORT
on
BARKERVILLE MOUNTAIN AND COW MOUNTAIN
SELF-POTENTIAL GEOPHYSICAL PROGRAM
WELLS, BRITISH COLUMBIA

Prepared for

International Wayside Gold Mines Ltd.

Wells Field Office

PO Box 247

12422 Barkerville Hwy

Wells, B.C.

V0K 2R0

by

Angelique Justason

University of Victoria

July 2002

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APPENDICES

APPENDIX I: 2001 Self-potential Data and Related Notes for Barkerville Mountain and Cow Mountain

APPENDIX II: 2001 Self-potential Profiles, including Bonanza Ledge Zone Profiles

APPENDIX III: Map of Self-potential Geophysics Point Values

APPENDIX IV: Map of Self-potential Geophysics 100mV Contours

1.0 INTRODUCTION

In 2000, a Self-potential program proved successful in outlining the New Discovery Zone, commonly known as Bonanza Ledge, and warranted further exploration in 2001 for Bonanza Ledge type mineralization in the vicinity. As a result, a self-potential geophysical program was conducted by International Wayside Gold Mines Limited during the 2001 field season on Barkerville Mountain and extended to Cow Mountain, adjacent to Wells, British Columbia in search of geophysical signatures similar to that found at the Bonanza Ledge Zone.

2.0 STUDY AREA

International Wayside Gold Mines concentrated self-potential geophysical studies on the existing mine grid located on Barkerville and Cow Mountains on NTS map sheet 093H3. Angelique Justason (author) operated the equipment and managed the data while Megan Broswick, Keith Montgomery, Benoît Landry, Shawn Rust and Ken Lord cheerfully assisted throughout the season.

Approximately 92000 feet, or 28 kilometers, of gridline was investigated in 2001 for geophysical signatures using the Self Potential method on the existing Cariboo Gold Quartz mine grid. The baseline strikes 47° west of north, or 313°, and the cross lines run perpendicular to the baseline at 43° east of north. Line spacing on Barkerville Mountain was 200 feet, except the area nearest the Bonanza Ledge where line spacing was 100 feet. Cow Mountain, however, had a line spacing of 400 feet at the time the geophysical survey was conducted and was tied in and corrected to correlate with data from Barkerville Mountain. Measurements were taken every twenty five feet along the lines and each data point was tied in and corrected to represent a value relative to the base station located at 20200E and 2800N.

3.0 EQUIPMENT

Field equipment used in the gathering of raw data consisted of 800 feet of 14 gauge wire, a *RadioShack* 35-range auto ranging digital multimeter, two ¾ glazed, porous, ceramic *Scintrex* pots with copper electrodes and a cork seal, and two hand held radios for communication.

4.0 PROCEDURE

Two methods of gathering field data were used: the roving pot method and the leap frog method.

The roving pot method involves leaving the negative pot at a stationary point while the positive pot is moved forward along the grid at points where readings are to be taken until the length of wire on the reel is at its maximum or the area of interest is covered. This method is best used when two persons are available: one person stays at the negative pot and takes the meter readings, while the second person moves the positive pot forward along the grid.

The leap frog method, on the other hand, uses a fixed length of wire, 30 feet in this case, between the negative and positive pots. At the start of each line, the positive pot is the forward pot, however, in order to move along the line after the initial reading, the negative pot is 'leap-

frogged' past the positive pot to the next station. A reading is taken but because the negative pot is now the forward pot, the sign of the reading taken with the voltmeter must be reversed, as such with every time the negative pot is the forward pot. The leap frog method can be used with just one person. It is good to use when a small area of detail is required and no help is available; but, it is a very tedious and time consuming method as much walking back and forth to leap frog the pots is required and calculations are slightly more involved than the roving pot method.

Soil surveys conducted during the previous 2000 field season left behind holes that allowed easy access to the soil's B-horizon. Where possible these holes were cleared of debris and used to set the self-potential (SP) pot firmly in the ground. Where holes were not of good quality or non-existent, the ground was cleared of moss, rocks and roots and dug to a sufficient depth to allow for the most accurate measurement. Holes were consistently dug to a depth where the pots could be placed in the B-horizon. Rarely was it necessary to skip a station due to subcropping or outcropping of the country rock.

Control stations were established where each outline crossed the baseline. The measurement taken at each control station was corrected to represent a value relative to the original base station located at 20200E 2800N which was given an arbitrary value of zero millivolts. For example, first we assume that the base station has a value of zero and every measurement taken from this point is relative to this base station value. Next, we take a measurement to the control station at the next adjacent outline. Let's say this is a value of +5mV. After establishing this, we can set up our equipment at this point and take measurements along that cross line. We must remember, though, that each value now measured from this first control station must have a value of +5mV added to it in order for it to be compared to the value of zero mV at the base station. After this cross line is finished we must take a measurement to the next control station at the next cross line before we set up on it. Let's assume that this has a value of +10mV. Now we can set up on the second control station. However, every single measurement taken from this second control station must now have +5mV + (+10mV), or +15mV, added to it. The next control station would have the third control station value plus the last two control station values added to it, and so on. This method of tying in each station was used throughout the field season. Furthermore, upon each return to the study area, a half dozen or so stations were remeasured and checked against the values taken during the previous day to insure the data was accurate and the equipment was in proper working order.

5.0 ANALYSIS OF FIELD DATA

After raw data was collected in the field, it was entered into an Excel spreadsheet and corrected in order to analyze the values in relation to the base station 20200E 2800N located just north of the Bonanza Ledge Zone. Formulas such as that described above were created in Excel and were used to produce a final self-potential value that was relative to the base station. A separate table was also created in Excel showing only the Easting, Northing and corresponding final self-potential values in millivolts. The latter table was used to create profiles for each line and was contoured using MapInfo Version 5.5 before it was finally overlayed on a plan map of the study area.

5.1 Barkerville Mountain

Barkerville Mountain has been a focus of mineral exploration for over one hundred years and with the discovery of the Bonanza Ledge Zone in 2000, a search for similar anomalous zones has been ongoing across the region.

5.1a Bonanza Ledge Anomaly

The Bonanza Ledge Zone is highlighted extremely well using the self-potential method. It is not masked by the graphitic BC Unit and shows up as an oblong east/west trending anomaly on the mine grid, outlined by the -100mV contour. International Wayside Gold Mines' 2000 drill program on Bonanza Ledge established a pattern between the SP values and gold hits originating within the bands of massive to finely disseminated pyrite. Gold mineralization in the Bonanza Ledge occurs in discrete zones of intense pyrite mineralization comprising 10-80% pyrite, as folded pyrite veinlets, bedding and S1 parallel lamina of fine grained pyrite and bands of semi-massive pyrite up to 80 feet thick (Rhys and Ross, 2001). It was discovered that the gold hits within the Bonanza Ledge occurred where self-potential readings were between -300mV and -100mV. Gold values have yet to be hit outside this interval unless it occurs in a vein or at a depth of greater than about 300 feet: research has indicated that the equipment used for self-potential surveys reach a maximum depth of about 300 feet (Burr, 1982).

5.1b Magnetite Phyllite Signature

Another common pattern has been established within the Rainbow#4 unit, or the magnetite phyllite unit, which bounds the north side of the Bonanza Ledge. This greyish green to tan magnetite phyllite forms a distinct lithological and geophysical marker which can be used to trace lithologies and prospective stratigraphy throughout the area. The geologic contact of the magnetite phyllite typically has self-potential readings of about zero millivolts and up; furthermore, these positive self-potential values correlate well with chargeability lows and magnetic highs as should be expected.

5.1c East Anomaly - East of Waoming Fault

A significant self-potential anomaly is centered at approximately 21300E 2800N, about 700 feet grid east and 200 feet grid north of the Bonanza Ledge Zone. The oblong anomaly trends east/west on the mine grid, is about 700 feet by 300 feet in size and is possibly cut off on the west side by the Waoming Fault. The center of the anomaly has a thin, elongate band of Self Potential values reaching below -400mV, suggesting a graphitic zone exists near the center of the anomaly: this could be a fault zone or possibly a continuation of the BC Vein structure. The anomaly also appears to be in the same stratigraphic section as the Bonanza Ledge. The new anomaly occurs within the BC and Lowhee units and is bound to the north by the Rainbow#4 unit.

5.1d Strike Vein Signatures

Repeating bands of alternating high and low self-potential values are a prominent feature observed within the BC and Lowhee units of Barkerville Mountain. Observations of rock fragments found in soils and subcrops exposed along road cuts suggest that the high negative self-potential values were produced by black graphitic argillite or carbonaceous phyllite which may or may not contain sulphide bearing quartz veins. These repeating bands may be entirely separate anomalous zones or may represent tight multiple folding of the BC and Lowhee units. It is possible that the tight folding of the region produced graphitic zones along the hinge of the folds, therefore producing high negative self-potential values along the hinge of each fold, but further investigation is needed.

One historically important strike vein in the study area is the BC vein/fault structure. The BC vein is a northeast dipping, fault hosted, gold bearing quartz vein that has been traced 4100 feet as of June 2002 (*pers.comm.*, Lord, 2002). Furthermore, the vein and fault are localized in carbonaceous phyllite of the BC unit. The vein generally contains >2% sulphides, either as clots or disseminations in gold bearing area, and locally contains >50% pyrite and/or base metals (Rhys and Ross, 2001). The self-potential geophysical signature for the BC vein/fault structure is a distinct feature on the plan map. The anomalous signature of the structure, typically outlined by the -600mV contour, appears grid north of the Bonanza Ledge at approximately 19700E 2675N and continues 1400 feet grid east until it is laterally offset 200 feet grid northwest by the Goldfinch fault. As of July 2002, exploration and drilling has confirmed that the BC vein/fault structure continues grid east of the Goldfinch fault for about 500 feet (*pers.comm.*, Lord, 2002). However, the plan view of the contoured self-potential data suggests that the BC vein/fault structure extends 800 feet grid west from about 17800E 2800N to 17000E 2700N before it appears to be cut off, possibly by another north striking fault. An anomaly identical to that of the BC vein/fault structure also exists between 18000E 2750N and 17600E 2675N. Further drilling or surface exploration should be completed along the length of these anomalies to confirm if they are a western extension of the gold bearing BC vein.

Interesting observations were made during the gathering of self-potential data on lines 15200E and 15400E. A significant amount of argillite rubble and subcrop was observed from 3500N to 3600N along the 15200E cutline before, finally, a large hole or trench was noted at 3600N. This may be from the historic exploration for mineralized quartz veins. Grid east along the 15400E cutline, field observations state that one of the strike vein structures exists between 3525N and 3625N. Graphitic argillite and orange weathered quartz were commonly found along this one hundred foot section of the 15400E line, with self-potential values peaking at -554mV. Self-potential signatures also support that a strike vein exists here and is possibly truncated to the grid east by an unnamed fault, and it is assumed to be cut off to the west by Lowhee fault.

5.1e Butts Zone Anomaly

The Butts Zone is located along the edge of Lowhee Gulch just north of the 4000N baseline. This auriferous zone which has been previously mined underground shows up very well using

the self-potential method. The Butts Zone anomaly is outlined by the -200 mV contour interval and peaks at -700mV. Because underground work was conducted here in the past, it is important to consider that the anomaly might also be so strong partly due to standing water, oxidizing rails or other equipment located below the surface. The grid east extent of the anomaly appears to be truncated by an unnamed, north striking fault at about 15300E 4050N and is truncated grid west by the Lowhee Gulch.

5.1f Baker/Rainbow Anomaly

Another area of interest is outlined by the anomalous self-potential values which trend at least 1300 feet east from 15200E 4500N along the mine grid. Historically, this has been mapped as the geologic contact between the Baker and Rainbow units (*pers comm*, Hall, 2002) and has been used in the past as the principle guide to ore in the Wells mining camp (Lord and Hall, 2001). The contact is quite distinctive on the self-potential profiles produced for lines 15200E to 16400E. The profiles reveal that the anomaly shows up suddenly and subsides more gradually as it approaches north. This would suggest that the contact dips to the north. It was also noted in the field that the ground in this vicinity was typically quite wet or marshy; therefore, it should also be assumed that the self-potential values may be slightly skewed to the positive.

5.1g Fault Zones

The repeating bands of high negative self-potential readings have also been useful in outlining previously known and unknown fault zones in the area. Apparent lateral offsets are best observed on the plan view of the self-potential data.

The Waoming fault lies in grid east end of the study area, between the Bonanza Ledge and the 'east anomaly'. The Waoming fault has been mapped as a north striking, east dipping fault. The western edge of the new self-potential anomaly appears to be cut off by the fault, however, this needs to be confirmed by drilling.

The Goldfinch fault is also a north striking, east dipping fault that shows an apparent dextral displacement of approximately 200 feet. The offset of the Rainbow#4 and BC units along the Goldfinch fault can be readily observed on the self-potential map between about 18000E 2800N and 17400E 3250N.

About 300 feet grid east of the Goldfinch fault along the 2800E baseline, another less prominent fault occurs. A small, northeast/southwest striking, apparently dextral fault with an offset of about 175 feet cuts through the -700mV self-potential contour interval which outlines the BC vein self-potential anomaly.

Initial analysis of the plan map of the self-potential data also suggests the possibility that a large fault, previously unmapped, is centered between the Goldfinch and Lowhee faults. This possible fault appears to be parallel with the Goldfinch fault and has a strike length of at least 2600 feet with an apparent dextral displacement of 400-1400 feet. There is also the possibility that numerous, smaller faults exist here instead, making the plan view of the self-potential data appear as if one single large fault exists. Further detailed exploration through prospecting or

drilling needs to be conducted here in order to determine the true structure and its implications on the geology between it and Lowhee Gulch (i.e. BC Vein exploration).

Lowhee fault has been previously mapped as the dominant fault in the study area, having an apparent dextral displacement of 1000-2000 feet. In order to interpret the Lowhee fault with the self-potential method, the self-potential data needs to be more complete along the fault itself, perhaps where Lowhee fault does not exist within the gulch. Lowhee Gulch not only proved difficult to navigate with the self-potential equipment, but, also, the washed gravel and cobbles, and absence of the soil's B-horizon made it difficult to take reliable self-potential readings. Furthermore, where readings could be taken along the gulch, self-potential values were skewed to the positive because of the topographic low and the presence of water along the creek. A self-potential study might be more useful in highlighting the Lowhee fault on the terrain south of the gulch between 15000E and 19000E.

5.2 Cow Mountain

Cow Mountain has also been an important point of interest in the mining community. The Cariboo Gold Quartz Mine had underground exploration and mining operations which concentrated on zones of quartz stockworks. As these zones have been found to extend to surface, an opportunity for open-pit mining currently exists on Cow Mountain (Lord and Hall, 2001).

In July of 2001, self-potential geophysics was conducted on the mine grid between Lowhee Creek and line 10600E. At the time the survey was carried out, cut lines were spaced at 400 feet apart from one another. This made for loss of some detail that would have otherwise been seen but was sufficient to serve as a quick reconnaissance of the ground and helped to outline some good initial relationships between the known geology and the plan map created from the self-potential readings.

5.2a BC Argillite Anomaly

The most significant observation was that of the BC Argillite which caps the knoll of Cow Mountain south of the Sanders Zone. Readings on this knoll peaked at upwards of -900 millivolts relative to the base station. It was expected to have a high negative value within this unit of argillite as it is quite graphitic and also because it occurs along a topographic high. The south westerly edge of the BC Unit anomaly on Cow Mountain appears to be truncated to the west by the Rainbow Fault, but this may in part be a function of topography.

5.2b New Replacement Zones

Prospecting in the area, to date, has turned up some interesting discoveries on both the easterly and westerly edges of the argillite anomaly capping Cow Mountain. A fold nose and oxidized zone was discovered near 11400E 3300N, about 200 feet east of a replacement showing discovered in July of 2001. The self-potential profile of 11400E presents an anomalous zone ranging from -100mV to -276mV, peaking at 3375N. Another replacement zone was also discovered on the east side of Cow Mountain along the upper ditch line road near 13200E;

however, an accurate correlation can not be made with the self-potential profile as the showing occurred between the widely spaced cross lines upon which the self-potential data was derived. The discovery of the replacement ore bodies cut by sulfide bearing quartz veins is promising but further detailed work is required to determine their extent.

5.2c Other Correlations

Although the plan view of the self-potential data does not provide much detail, further interpretation can be made with the self-potential profiles. Noticeable correlations can be made when comparing the profiles to the known geology of the area. The 12600E profile, for example, shows a topographic high and a graphitic signature from about 2600N to 3900N. Values rise slightly between 3900N and 4150N before they sharply drop again to about -650mV within another graphitic zone, possibly the BC Unit. The east dipping Sanders fault is highlighted by a sharp rise in the self-potential profile between 4150N and 4500N before values begin to drop again slightly within the south extent of the Sanders Zone. Correlations such as these can be made between the known geology along each grid line and the corresponding self-potential profiles.

It should also be noted that mapping of the alteration zones conducted in 2000 by Panterra Geoservices Inc. also appear to correlate with the profiles produced from the 2001 self-potential data. A sharp peak with a range of -100mV to -150mV exists on either side of the topographic high and graphite anomaly on 12600E. These two peaks correlate directly with the alteration zones mapped the previous year. The profile of line 13800E also has two peaks with a range of -200mV between 3500N and 3950N that correlate perfectly with the alteration zones mapped along that line. Further detail is needed to confirm if such a correlation is valid for this area, but it does appear, initially, that a pattern does exist.

It is recommended that future self-potential geophysics be conducted on in-fill cut lines, with a spacing of 200 feet, to gain a better understanding of the self-potential geophysical signatures on Cow Mountain and to give good drill targets.

6.0 CONSIDERATIONS IN ANALIZING SP DATA

6.1 Geology

The self-potential method is most commonly used to outline sulphide bodies which contain pyrite, pyrrhotite and/or chalcopyrite. The equipment responds to good conducting sulphides, both oxidized and unoxidized bodies, graphite and nonconducting, disseminated sulphides if these sulphides are oxidizing. Another feature of the self-potential method is its ability to differentiate between anomalies caused by sulphides and anomalies caused by graphite. Sulphides produce a range of up to 350mV between the most positive and the most negative self-potential readings (Burr, 1982); while graphitic zones have a larger range between its most positive and its most negative values. The self-potential method was also found to be useful in highlighting geologic contacts and fault zones in the study area. It was also discovered that certain lithological units produced a certain range of self-potential signatures; for example, the

Rainbow#4 marker unit consistently produced self-potential values ranging from 0mV to about +20mV.

6.2 Telluric Currents

Geomagnetic storms, induced by activity originating from the sun, greatly diminish the reliability of self-potential readings. It is, however, easy to detect when such a storm is taking place while conducting a self-potential survey. It was observed in the field that if self-potential readings were taken while a significant geomagnetic storm was active, readings would fluctuate sporadically with no commonly recurring value. It was observed to have jumped around up to a range of plus or minus 40 millivolts at any given point during an active storm.

Reliable self-potential readings are next to impossible to obtain during such solar activity. When it was discovered that readings were taken in the field while a less significant storm was taking place, and readings were much less sporadic, data values were later rechecked. In one case, they were completely redone. Values taken during a smaller storm consistently produced values more positive than when the values were taken during a quiet period. A pattern did not necessarily develop between the fluctuating self-potential values and class of storm, but another important correlation had been found.

Each day before leaving for the field and upon return, real-time solar activity data was observed at www.spaceweather.com. The solar wind data, velocity and proton density, presented on spaceweather.com is updated every 10 minutes and was very useful during the geophysical program. The solar wind data is derived from real-time information transmitted to Earth from the ACE spacecraft and reported by the NOAA Space Environment Center. The ACE spacecraft is located at a point between the earth and the sun which enables it to give about a one hour advance warning of impending geomagnetic activity. Upon further investigation, it was discovered that there is in fact a correlation between the sporadic self-potential values and the density of protons per cubic centimeter. A pattern had been established and the density of protons per cubic centimeter was carefully observed before and after each self-potential survey. It was revealed that if there were more than the mid-teens of protons/cm³, a self-potential survey would be unreliable and put on hold until the density of protons bombarding the Earth's atmosphere subsided. If readings were found to be sporadic while in the field, after checking all wire contacts, ground contacts, and checking the pots for any cracks, communication was made with base camp to confirm if there was any significant solar activity. If so, the geophysical gear was packed up and the field crew returned to base camp until such time where the solar activity subsided. This was usually the next day, however, it is possible to have to wait several days. When returning to the field after such solar activity, all the values for the line worked on the previous field day were rechecked and corrected to confirm the accuracy of the data before work on subsequent lines commenced.

6.3 Radio Transmissions

Use of hand held radios for communication between the field crew is very important while conducting a self-potential survey using the long wire method; however, it can also impede the survey or corrupt the raw data gathered in the field. Self-potential readings must not be taken

while transmitting over a hand held radio. The radio transmission interferes with the multimeter and skews the values. The person taking the readings can however receive a transmission without skewing the data but it is very important for this person not to transmit while taking the readings.

6.4 Ground Conditions

It is very important to note features encountered in the field that may affect the interpretation of the final self-potential data. This may be ground disturbances, presence of oxidizing metal objects, subcropping of rocks, a high water table, or even thick moss. Each can affect self-potential readings taken in the field. Ground disturbances made by man may skew reading either to the positive or to the negative; for example, the pile of oxidizing tailing found south of the BC Shaft has self-potential values skewed slightly to the negative creating a rounded anomaly in plan view around the pile. The varying depth of subcrop below surface is also important to consider. A graphitic unit, for example, located 20 feet below overburden will have a stronger negative self-potential reading than that of the same unit found at a depth of 200 feet. The clay content in the ground also affects self-potential readings. Clay has a natural tendency to hold a large amount of water, thus skewing self-potential reading to the positive. Any area encountered in the field with a significant water content should be noted as it will invariably cause reading to be more positive than if the water was not present. It is also important to consistently remove the moss from the ground at each station in order to take a reliable measurement. Moss and rotting debris found in the varying thickness of the A-horizon also has a tendency to hold some amount of water also varying from one place to another. Trial measurements were taken to determine the importance of removing moss from each station and it was found that self-potential values were skewed up to +30mV than if the moss were removed. It was also discovered that on a second run of the same stations on the moss, the values were not the same. This seemed to be a function of how much the moss pushed down while the forward pot was placed and held on the ground. In conclusion, solid contact with the B-horizon must be insured at each station and ground conditions should be noted to make for the most reliable measurements and further interpretation.

6.5 Topographic Effect

Topographic highs and lows must be considered when interpreting the self-potential data. Topographic lows or flat lying areas may have a high water table and even be marshy. Such areas tend to produce strong positive values. If an anomalous zone should occur here it may not be as apparent. In contrast, a topographic high or a very low water table tends to produce strong negative values. An example can be seen on top of Cow Mountain where not only is it capped by graphitic argillite, but the topographic high has elevated the negative values to nearly -1000mV.

It is, however, possible to dampen the effects of topography on self-potential readings. The two prepared pots must be placed in two separate canvas bags filled with damp loam or sawdust. Both pots are then in contact with medium of constant pH and the influence of varying acidity is strongly attenuated. As a result, readings become more uniform, the background displays a

narrower range, anomalies in swamps are better defined and anomalies on hills are less negative and less exaggerated (Burr, 1982). Although this method of dampening the effects of topography was not used during the 2001 field season, the topographic highs, lows and marshy areas were carefully considered in the final interpretation of the self-potential data.

7.0 CONCLUSION

The self-potential geophysical method is a useful way of outlining zones containing pyrite and other conductive or oxidizing sulphides. It has been instrumental in outlining the Bonanza Ledge Zone of Barkerville Mountain near Wells, British Columbia, and warranted further self-potential geophysical exploration of the area. In 2001, International Wayside Gold Mines Ltd. conducted self-potential studies on approximately 28 line kilometers along the existing Cariboo Gold Quartz mine grid located on Barkerville and Cow Mountains between 22500E and 10600E.

The 2001 self-potential geophysical program proved successful in establishing relationships between certain self-potential signatures and the known geology of the area:

- Numerous bands of grid east/west trending, high negative self-potential values correlate well with known strike veins of the area, including the BC vein/fault structure. This correlation may be helpful in exploring for the western extent of the BC vein/fault structure.
- The Rainbow#4 unit, which has been used as a marker unit for tracing lithologies and prospective stratigraphy throughout the area, was found to consistently produce thin bands of self-potential values of zero to +20mV.
- Offsets and the cutting off of anomalous self-potential zones have been useful in mapping fault zones.
- The Baker/Rainbow contact was outlined by the anomalous self-potential values which trend at least 1300 feet east from 15200E 4500N along the mine grid.
- It was also discovered that the very high negative anomalous zone on Cow Mountain represents a unit of graphitic argillite capping the knoll. This high negative anomaly likely masks other possible anomalous zones around and structurally below it. The data gathered on Cow Mountain was gathered with a line spacing of 400 feet and made final interpretation of the data difficult. Future self-potential work is recommended on Cow Mountain with a final line spacing of 200 feet to better understand the anomalous areas located on Cow Mountain.
- Most significantly, an anomalous zone, comparable to that of the Bonanza Ledge self-potential anomaly, was discovered 700 feet grid east of the Bonanza Ledge. The new 'East Anomaly', centered at about 21300E 2800N, is approximately 700 feet by 300 feet in size. It is bound to the north by the Rainbow#4 unit and truncated to the west by the Waoming fault. This anomalous zone should be studied further by conducting a half-day more of detailed self-potential geophysics over the anomaly at a line spacing of 100 feet. This new 'East Anomaly' may prove to host Bonanza Ledge type mineralization.

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<http://www.microgeo.com/service/sp/sp.html>

<http://www.spaceweather.com>

APPENDIX I

2001 Self-potential Data and Related Notes
for
Barkerville Mountain and Cow Mountain

CONTROL STATION

13400E, 3400N

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
		0.0					
13400	2525	-112.9	0.0	-112.9	-50.4	-163.3	
13400	2550	-130.4	0.0	-130.4	-50.4	-180.8	
13400	2575	-127.7	0.0	-127.7	-50.4	-178.1	
13400	2600	-144.2	0.0	-144.2	-50.4	-194.6	
13400	2625	-150.6	0.0	-150.6	-50.4	-201.0	lots of sticks
13400	2650	-146.9	0.0	-146.9	-50.4	-197.3	lots of sticks
13400	2675	-141.3	0.0	-141.3	-50.4	-191.7	
13400	2700	-131.5	0.0	-131.5	-50.4	-181.9	
13400	2725	-108.7	0.0	-108.7	-50.4	-159.1	
13400	2750	-99.3	0.0	-99.3	-50.4	-149.7	
13400	2775	-92.0	0.0	-92.0	-50.4	-142.4	
13400	2800	-90.6	0.0	-90.6	-50.4	-141.0	
13400	2825	-83.8	0.0	-83.8	-50.4	-134.2	rooty
13400	2850	-71.9	0.0	-71.9	-50.4	-122.3	
13400	2875	-36.5	0.0	-36.5	-50.4	-86.9	
13400	2900	-40.8	0.0	-40.8	-50.4	-91.2	
13400	2925	-48.1	0.0	-48.1	-50.4	-98.5	
13400	2950	-81.9	0.0	-81.9	-50.4	-132.3	
13400	2975	-104.5	0.0	-104.5	-50.4	-154.9	
13400	3000	-123.5	0.0	-123.5	-50.4	-173.9	
13400	3025	-187.4	0.0	-187.4	-50.4	-237.8	
13400	3050	-252.7	0.0	-252.7	-50.4	-303.1	
13400	3075	-248.0	0.0	-248.0	-50.4	-298.4	rooty
13400	3100	-248.2	0.0	-248.2	-50.4	-298.6	
13400	3125	-232.2	0.0	-232.2	-50.4	-282.6	
13400	3150	-220.5	0.0	-220.5	-50.4	-270.9	rooty
13400	3175	-183.0	0.0	-183.0	-50.4	-233.4	
13400	3200	-125.7	0.0	-125.7	-50.4	-176.1	next to road
13400	3225	-69.2	0.0	-69.2	-50.4	-119.6	
13400	3250	-46.1	0.0	-46.1	-50.4	-96.5	
13400	3275	-46.3	0.0	-46.3	-50.4	-96.7	
13400	3300	-35.1	0.0	-35.1	-50.4	-85.5	
13400	3325	-28.0	0.0	-28.0	-50.4	-78.4	
13400	3350	-23.3	0.0	-23.3	-50.4	-73.7	
13400	3375	-17.6	0.0	-17.6	-50.4	-68.0	
13400	3400	0.0	0.0	0.0	-50.4	-50.4	Cow Mountain base station
13400	3450	-35.4	0.0	-35.4	-50.4	-85.8	
13400	3500	-73.2	0.0	-73.2	-50.4	-123.6	rocky
13400	3525	-19.4	0.0	-19.4	-50.4	-69.8	
13400	3550	-239.3	0.0	-239.3	-50.4	-289.7	middle of road
13400	3575	-287.9	0.0	-287.9	-50.4	-338.3	
13400	3600	-337.8	0.0	-337.8	-50.4	-388.2	
13400	3625	-317.4	0.0	-317.4	-50.4	-367.8	
13400	3650	-309.1	0.0	-309.1	-50.4	-359.5	rooty
13400	3675	-430.0	0.0	-430.0	-50.4	-480.4	
13400	3700	-338.5	0.0	-338.5	-50.4	-388.9	
13400	3725	-273.9	0.0	-273.9	-50.4	-324.3	
13400	3750	-200.9	0.0	-200.9	-50.4	-251.3	
13400	3775	-114.5	0.0	-114.5	-50.4	-164.9	
13400	3800	-34.0	0.0	-34.0	-50.4	-84.4	
13400	3825	7.3	0.0	7.3	-50.4	-43.1	
13400	3850	-25.1	0.0	-25.1	-50.4	-75.5	
13400	3875	-74.2	0.0	-74.2	-50.4	-124.6	
13400	3900	-122.6	0.0	-122.6	-50.4	-173.0	
13400	3925	-184.9	0.0	-184.9	-50.4	-235.3	very rocky
13400	3950	-9.3	0.0	-9.3	-50.4	-59.7	
13400	3975	-356.4	0.0	-356.4	-50.4	-406.8	
13400	4000	-478.0	0.0	-478.0	-50.4	-528.4	
13400	4025	-472.0	0.0	-472.0	-50.4	-522.4	rooty
13400	4050	-431.0	0.0	-431.0	-50.4	-481.4	rooty
13400	4075	-449.0	0.0	-449.0	-50.4	-499.4	
13400	4100	-521.0	0.0	-521.0	-50.4	-571.4	
13400	4125	-531.0	0.0	-531.0	-50.4	-581.4	
13400	4150	-459.0	0.0	-459.0	-50.4	-509.4	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
13400	4175	-382.0	0.0	-382.0	-50.4	-432.4	10-12' drop
13400	4200	-209.3	0.0	-209.3	-50.4	-259.7	rocky
13400	4225	-244.6	0.0	-244.6	-50.4	-295.0	
13400	4250	-382.9	0.0	-382.9	-50.4	-433.3	
13400	4275	-301.5	0.0	-301.5	-50.4	-351.9	
13800E, 3400N		-2.7					
13800	2525	7.5	-2.7	4.8	-50.4	-45.6	
13800	2550	12.6	-2.7	9.9	-50.4	-40.5	
13800	2575	33.8	-2.7	31.1	-50.4	-19.3	argillite in hole
13800	2600	10.4	-2.7	7.7	-50.4	-42.7	
13800	2625	11.0	-2.7	8.3	-50.4	-42.1	
13800	2650	16.7	-2.7	14.0	-50.4	-36.4	
13800	2675	22.0	-2.7	19.3	-50.4	-31.1	
13800	2700	28.8	-2.7	26.1	-50.4	-24.3	
13800	2725	31.9	-2.7	29.2	-50.4	-21.2	lt grey phyl rx in soil
13800	2750	35.8	-2.7	33.1	-50.4	-17.3	
13800	2775	27.3	-2.7	24.6	-50.4	-25.8	
13800	2800	38.2	-2.7	35.5	-50.4	-14.9	
13800	2825	43.9	-2.7	41.2	-50.4	-9.2	
13800	2850	36.0	-2.7	33.3	-50.4	-17.1	
13800	2875	45.5	-2.7	42.8	-50.4	-7.6	
13800	2900	55.7	-2.7	53.0	-50.4	2.6	
13800	2925	52.9	-2.7	50.2	-50.4	-0.2	
13800	2950	49.1	-2.7	46.4	-50.4	-5.0	
13800	2975	50.6	-2.7	47.9	-50.4	-2.5	
13800	3000	36.6	-2.7	33.9	-50.4	-16.5	
13800	3025	28.9	-2.7	26.2	-50.4	-24.2	
13800	3050	39.5	-2.7	36.8	-50.4	-13.6	
13800	3075	25.0	-2.7	22.3	-50.4	-28.1	
13800	3100	16.6	-2.7	13.9	-50.4	-36.5	
13800	3125	-11.4	-2.7	-14.1	-50.4	-64.5	
13800	3150	-8.2	-2.7	-10.9	-50.4	-61.3	
13800	3175	-1.9	-2.7	-4.6	-50.4	-55.0	
13800	3200	-13.8	-2.7	-16.5	-50.4	-66.9	
13800	3225	-5.9	-2.7	-8.6	-50.4	-59.0	on pile of dirt or down side of ditch line
13800	3250	7.8	-2.7	5.1	-50.4	-45.3	
13800	3275	-11.7	-2.7	-14.4	-50.4	-64.8	
13800	3300	8.2	-2.7	5.5	-50.4	-44.9	
13800	3325	-3.5	-2.7	-6.2	-50.4	-56.6	
13800	3350	2.5	-2.7	-0.2	-50.4	-50.6	
13800	3375	-23.6	-2.7	-26.3	-50.4	-76.7	
13800	3400	-2.7	0.0	-2.7	-50.4	-53.1	
13800	3450	-22.7	-2.7	-25.4	-50.4	-75.8	
13800	3475	-42.3	-2.7	-45.0	-50.4	-95.4	
13800	3500	-46.5	-2.7	-49.2	-50.4	-99.6	
13800	3525	-84.2	-2.7	-86.9	-50.4	-137.3	
13800	3550	-131.5	-2.7	-134.2	-50.4	-184.6	
13800	3575	-190.0	-2.7	-192.7	-50.4	-243.1	
13800	3600	-281.8	-2.7	-284.5	-50.4	-334.9	
13800	3625	-355.5	-2.7	-358.2	-50.4	-408.6	
13800	3650	-338.5	-2.7	-341.2	-50.4	-391.6	
13800	3675	-299.1	-2.7	-301.8	-50.4	-352.2	
13800	3700	-263.0	-2.7	-265.7	-50.4	-316.1	rocky roadcut
13800	3725	-239.4	-2.7	-242.1	-50.4	-292.5	
13800	3750	-204.4	-2.7	-207.1	-50.4	-257.5	
13800	3775	-154.3	-2.7	-157.0	-50.4	-207.4	
13800	3800	-106.2	-2.7	-108.9	-50.4	-159.3	side of road
13800	3825	-142.4	-2.7	-145.1	-50.4	-195.5	rocky
13800	3850	-262.7	-2.7	-265.4	-50.4	-315.8	
13800	3875	-380.8	-2.7	-383.5	-50.4	-433.9	
13800	3900	-226.3	-2.7	-229.0	-50.4	-279.4	
13800	3925	-187.2	-2.7	-189.9	-50.4	-240.3	
13800	3950	-142.6	-2.7	-145.3	-50.4	-195.7	
13800	3975	-174.5	-2.7	-177.2	-50.4	-227.6	
13800	4000	-229.8	-2.7	-232.5	-50.4	-282.9	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
13800	4025	-275.8	-2.7	-278.5	-50.4	-328.9	
13800	4050	-315.6	-2.7	-318.3	-50.4	-368.7	
13800	4075	-296.0	-2.7	-298.7	-50.4	-349.1	
13800	4100	-168.0	-2.7	-170.7	-50.4	-221.1	
13800	4125	-129.8	-2.7	-132.5	-50.4	-182.9	just abv rd @ wif's place
13800	4150	-157.5	-2.7	-160.2	-50.4	-210.6	lwhe camp/on rd, rusty jeep
13800	4175	-127.7	-2.7	-130.4	-50.4	-180.8	Lowhee camp
13800	4200	-282.3	-2.7	-285.0	-50.4	-335.4	Lowhee camp
13800	4225	-364.3	-2.7	-367.0	-50.4	-417.4	Lowhee camp
13800	4250	-406.0	-2.7	-408.7	-50.4	-459.1	lowhee camp. Lots of old metal lying around
13800	4275	-382.2	-2.7	-384.9	-50.4	-435.3	
14000E, 3400N	-	-9.3					
14000	2525	7.4	-12.0	-4.6	-50.4	-55.0	
14000	2550	46.3	-12.0	34.3	-50.4	-18.1	
14000	2575	49.0	-12.0	37.0	-50.4	-13.4	
14000	2600	61.2	-12.0	49.2	-50.4	-1.2	
14000	2625	48.3	-12.0	36.3	-50.4	-14.1	
14000	2650	72.7	-12.0	60.7	-50.4	10.3	
14000	2675	62.8	-12.0	50.8	-50.4	0.4	
14000	2700	86.4	-12.0	74.4	-50.4	24.0	
14000	2725	67.8	-12.0	55.8	-50.4	5.4	
14000	2750	80.4	-12.0	68.4	-50.4	18.0	
14000	2775	73.7	-12.0	61.7	-50.4	11.3	
14000	2800	84.9	-12.0	72.9	-50.4	22.5	
14000	2825	87.3	-12.0	75.3	-50.4	24.9	very wet soil
14000	2850	89.0	-12.0	77.0	-50.4	26.6	
14000	2875	83.4	-12.0	71.4	-50.4	21.0	
14000	2900	92.6	-12.0	80.6	-50.4	30.2	
14000	2925	75.0	-12.0	63.0	-50.4	12.6	
14000	2950	88.8	-12.0	76.8	-50.4	26.4	
14000	2975	86.0	-12.0	74.0	-50.4	23.6	
14000	3000	93.0	-12.0	81.0	-50.4	30.6	
14000	3025	87.3	-12.0	75.3	-50.4	24.9	
14000	3050	89.7	-12.0	77.7	-50.4	27.3	
14000	3075	74.6	-12.0	62.6	-50.4	12.2	
14000	3100	62.2	-12.0	50.2	-50.4	-0.2	on ditch line
14000	3125	65.3	-12.0	53.3	-50.4	2.9	
14000	3150	65.0	-12.0	53.0	-50.4	2.6	
14000	3175	57.1	-12.0	45.1	-50.4	-5.3	
14000	3200	65.1	-12.0	53.1	-50.4	2.7	
14000	3225	45.4	-12.0	33.4	-50.4	-17.0	
14000	3250	53.9	-12.0	41.9	-50.4	-8.5	
14000	3275	25.3	-12.0	13.3	-50.4	-37.1	
14000	3300	37.1	-12.0	25.1	-50.4	-25.3	
14000	3325	-15.6	-12.0	-27.6	-50.4	-78.0	
14000	3350	-42.2	-12.0	-54.2	-50.4	-104.6	
14000	3375	-32.5	-12.0	-44.5	-50.4	-94.9	
14000	3400	-9.3	-2.7	-12.0	-50.4	-62.4	
14000	3425	-13.7	-12.0	-25.7	-50.4	-78.1	
14000	3450	11.9	-12.0	-0.1	-50.4	-50.5	
14000	3475	7.1	-12.0	-4.9	-50.4	-55.3	
14000	3500	7.9	-12.0	-4.1	-50.4	-54.5	
14000	3525	-29.1	-12.0	-41.1	-50.4	-91.5	
14000	3550	-37.9	-12.0	-49.9	-50.4	-100.3	
14000	3575	-71.2	-12.0	-83.2	-50.4	-133.6	
14000	3600	-106.9	-12.0	-118.9	-50.4	-169.3	
14000	3625	-169.4	-12.0	-181.4	-50.4	-231.8	
14000	3650	-194.8	-12.0	-206.8	-50.4	-257.2	
14000	3675	-238.3	-12.0	-250.3	-50.4	-300.7	
14000	3700	-249.5	-12.0	-261.5	-50.4	-311.9	
14000	3725	-255.2	-12.0	-267.2	-50.4	-317.6	
14000	3750	-273.4	-12.0	-285.4	-50.4	-335.8	
14000	3775	-322.9	-12.0	-334.9	-50.4	-385.3	
14000	3800	-384.6	-12.0	-396.6	-50.4	-447.0	
14000	3825	-362.1	-12.0	-374.1	-50.4	-424.5	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
14000	3850	-182.1	-12.0	-194.1	-50.4	-244.5	
14000	3875	-103.3	-12.0	-115.3	-50.4	-165.7	
14000	3900	-59.3	-12.0	-71.3	-50.4	-121.7	
14000	3925	-18.3	-12.0	-30.3	-50.4	-80.7	
14000	3950	27.9	-12.0	15.9	-50.4	-34.5	
14000	3975	36.1	-12.0	24.1	-50.4	-26.3	no more northing measurements (Lowhee hydraulicked area: cliff)
13000E, 3400N		-620.5					
13000	2525	233.4	-620.5	-387.1	-50.4	-437.5	
13000	2550	207.4	-620.5	-413.1	-50.4	-463.5	some rx
13000	2575	176.1	-620.5	-444.4	-50.4	-494.8	
13000	2600	131.8	-620.5	-488.7	-50.4	-539.1	
13000	2625	94.0	-620.5	-526.5	-50.4	-576.9	
13000	2650	85.2	-620.5	-535.3	-50.4	-585.7	
13000	2675	52.9	-620.5	-567.6	-50.4	-618.0	
13000	2700	10.2	-620.5	-610.3	-50.4	-660.7	
13000	2725	31.3	-620.5	-589.2	-50.4	-639.6	
13000	2750	23.1	-620.5	-597.4	-50.4	-647.8	
13000	2775	21.0	-620.5	-599.5	-50.4	-649.9	
13000	2800	-40.7	-620.5	-661.2	-50.4	-711.6	
13000	2825	-76.5	-620.5	-697.0	-50.4	-747.4	
13000	2850	-27.4	-620.5	-647.9	-50.4	-698.3	lots roots
13000	2875	130.7	-620.5	-489.8	-50.4	-540.2	
13000	2900	284.0	-620.5	-336.5	-50.4	-386.9	
13000	2925	315.4	-620.5	-305.1	-50.4	-255.5	
13000	2950	287.7	-620.5	-332.8	-50.4	-383.2	
13000	2975	202.9	-620.5	-417.6	-50.4	-468.0	
13000	3000	121.3	-620.5	-499.2	-50.4	-549.6	lots bluey rx, grey soil
13000	3025	15.9	-620.5	-604.6	-50.4	-655.0	on rd
13000	3050	-10.2	-620.5	-630.7	-50.4	-681.1	lots rocks
13000	3075	-72.7	-620.5	-693.2	-50.4	-743.6	lots rocks
13000	3100	-90.1	-620.5	-710.6	-50.4	-761.0	
13000	3125	-117.8	-620.5	-738.3	-50.4	-788.7	
13000	3150	-159.2	-620.5	-779.7	-50.4	-830.1	a bit rocky
13000	3175	-147.1	-620.5	-767.6	-50.4	-818.0	
13000	3200	-137.5	-620.5	-758.0	-50.4	-808.4	lots roots
13000	3225	-138.5	-620.5	-759.0	-50.4	-809.4	roots
13000	3250	-145.0	-620.5	-765.5	-50.4	-815.9	rocky
13000	3275	-111.6	-620.5	-732.1	-50.4	-782.5	
13000	3300	-90.6	-620.5	-711.1	-50.4	-761.5	
13000	3325	-26.7	-620.5	-647.2	-50.4	-697.6	
13000	3350	-11.8	-620.5	-632.3	-50.4	-682.7	rooty
13000	3375	-5.1	-620.5	-625.6	-50.4	-676.0	
13000	3400	-620.5	0.0	-620.5	-50.4	-670.9	rocky
13000	3425	-124.6	-620.5	-745.1	-50.4	-795.5	rocky
13000	3450	-104.2	-620.5	-724.7	-50.4	-775.1	
13000	3475	-70.8	-620.5	-691.3	-50.4	-741.7	
13000	3500	-26.0	-620.5	-646.5	-50.4	-696.9	
13000	3525	71.8	-620.5	-548.7	-50.4	-599.1	
13000	3550	334.5	-620.5	-286.0	-50.4	-336.4	lots roots
13000	3575	470.0	-620.5	-150.5	-50.4	-200.9	
13000	3600	583.0	-620.5	-37.5	-50.4	-87.9	
13000	3625	681.0	-620.5	10.5	-50.4	-39.9	on rd/rocky
13000	3650	259.8	-620.5	-360.7	-50.4	-411.1	on rd/rocky
13000	3675	256.0	-620.5	-264.5	-50.4	-314.9	on rd/rocky
13000	3700	655.0	-620.5	34.5	-50.4	-15.9	
13000	3725	865.0	-620.5	44.5	-50.4	-5.9	rooty
13000	3750	836.0	-620.5	15.5	-50.4	-34.9	
13000	3775	588.0	-620.5	-32.5	-50.4	-82.9	
13000	3800	479.0	-620.5	-141.5	-50.4	-191.9	
13000	3825	289.0	-620.5	-331.5	-50.4	-381.9	
13000	3850	161.2	-620.5	-459.3	-50.4	-509.7	
13000	3875	210.3	-620.5	-410.2	-50.4	-460.6	rooty/rocky
13000	3900	41.9	-620.5	-578.6	-50.4	-629.0	
13000	3925	-27.0	-620.5	-647.5	-50.4	-697.9	
13000	3950	21.5	-620.5	-569.0	-50.4	-649.4	on road

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
13000	3975	-8.1	-820.5	-828.6	-50.4	-877.0	
13000	4000	-28.8	-820.5	-849.3	-50.4	-899.7	rooty/at outline
13000	4025	-93.7	-820.5	-714.2	-50.4	-764.6	
13000	4050	-93.4	-820.5	-713.9	-50.4	-764.3	
13000	4075	-41.6	-820.5	-682.1	-50.4	-712.5	roots
13000	4100	155.2	-820.5	-465.3	-50.4	-515.7	
13000	4125	285.9	-820.5	-334.6	-50.4	-385.0	
13000	4150	268.4	-820.5	-352.1	-50.4	-402.5	
13000	4175	210.5	-820.5	-410.0	-50.4	-460.4	roots
13000	4200	215.7	-820.5	-404.8	-50.4	-455.2	
13000	4225	246.0	-820.5	-374.5	-50.4	-424.9	
13000	4250	216.9	-820.5	-403.6	-50.4	-454.0	
13000	4275	206.0	-820.5	-414.5	-50.4	-464.9	
12600E, 3400N		-198.3					
12600	2550	242.8	-818.8	-576.0	-50.4	-626.4	
12600	2575	148.2	-818.8	-670.6	-50.4	-721.0	back to argillite again
12600	2600	13.0	-818.8	-805.8	-50.4	-856.2	lots roots
12600	2625	-12.1	-818.8	-830.9	-50.4	-881.3	
12600	2650	-1.6	-818.8	-820.4	-50.4	-870.8	
12600	2675	39.5	-818.8	-779.3	-50.4	-829.7	
12600	2700	135.5	-818.8	-683.3	-50.4	-733.7	def. Different rx
12600	2725	135.0	-818.8	-683.8	-50.4	-734.2	
12600	2750	117.1	-818.8	-761.7	-50.4	-722.1	
12600	2775	-14.7	-818.8	-833.5	-50.4	-883.9	
12600	2800	-40.8	-818.8	-859.6	-50.4	-910.0	change in rock comp
12600	2825	-76.6	-818.8	-895.4	-50.4	-945.8	
12600	2850	-79.9	-818.8	-898.7	-50.4	-949.1	
12600	2875	-71.6	-818.8	-890.4	-50.4	-940.8	
12600	2900	-79.9	-818.8	-898.7	-50.4	-949.1	
12600	2925	-79.4	-818.8	-898.2	-50.4	-948.6	really rocky
12600	2950	-53.4	-818.8	-872.2	-50.4	-922.6	lots rock still
12600	2975	-54.5	-818.8	-873.3	-50.4	-923.7	by tower on top of hill
12600	3000	-80.0	-818.8	-898.8	-50.4	-949.2	still very rocky
12600	3025	-79.2	-818.8	-898.0	-50.4	-948.4	next to rd/ rocky
12600	3050	-78.0	-818.8	-898.8	-50.4	-947.2	rocky/rd
12600	3075	-55.7	-818.8	-874.5	-50.4	-924.9	rocky
12600	3100	-61.3	-818.8	-880.1	-50.4	-930.5	
12600	3125	-53.8	-818.8	-872.6	-50.4	-923.0	really rocky
12600	3150	-73.0	-818.8	-891.8	-50.4	-942.2	
12600	3175	-80.4	-818.8	-899.2	-50.4	-949.6	lots qtz in hole
12600	3200	-81.6	-818.8	-900.4	-50.4	-950.8	lots roots
12600	3225	-50.1	-818.8	-868.9	-50.4	-919.3	many rocks
12600	3250	-15.3	-818.8	-834.1	-50.4	-884.5	at road. Many rocks
12600	3275	-74.9	-818.8	-893.7	-50.4	-944.1	rocky blk phyll/graph/arg
12600	3300	-61.5	-818.8	-880.3	-50.4	-930.7	
12600	3325	-90.4	-818.8	-909.2	-50.4	-959.6	
12600	3350	-68.6	-818.8	-887.4	-50.4	-937.8	rocky
12600	3375	-78.7	-818.8	-897.5	-50.4	-947.9	
12600	3400	-198.3	-820.5	-618.8	-50.4	-869.2	argillite
12600	3425	-66.3	-818.8	-885.1	-50.4	-935.5	
12600	3450	-86.5	-818.8	-905.3	-50.4	-955.7	
12600	3475	-76.2	-818.8	-895.0	-50.4	-945.4	
12600	3500	-70.7	-818.8	-889.5	-50.4	-939.9	argillite
12600	3525	-16.7	-818.8	-835.5	-50.4	-885.9	argillite
12600	3550	-24.0	-818.8	-842.8	-50.4	-893.2	
12600	3575	-21.1	-818.8	-839.9	-50.4	-890.3	
12600	3600	-27.2	-818.8	-846.0	-50.4	-896.4	roots
12600	3625	-5.6	-818.8	-824.4	-50.4	-874.8	
12600	3650	20.5	-818.8	-798.3	-50.4	-848.7	roots
12600	3675	15.5	-818.8	-803.3	-50.4	-853.7	
12600	3700	4.9	-818.8	-813.9	-50.4	-864.3	a few roots
12600	3725	6.8	-818.8	-812.0	-50.4	-862.4	
12600	3750	35.5	-818.8	-783.3	-50.4	-833.7	
12600	3775	71.2	-818.8	-747.6	-50.4	-798.0	lots roots

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
12600	3800	98.5	-818.8	-720.3	-50.4	-770.7	argillite
12600	3825	9.8	-818.8	-809.0	-50.4	-859.4	
12600	3850	5.8	-818.8	-813.0	-50.4	-863.4	
12600	3875	-13.4	-818.8	-832.2	-50.4	-882.6	rocky
12600	3900	-4.4	-818.8	-823.2	-50.4	-873.6	
12600	3925	117.3	-818.8	-701.5	-50.4	-751.9	
12600	3950	193.6	-818.8	-625.2	-50.4	-675.6	rooty
12600	3975	216.8	-818.8	-602.0	-50.4	-652.4	
12600	4000	221.0	-818.8	-597.8	-50.4	-648.2	
12600	4025	215.6	-818.8	-603.2	-50.4	-653.6	
12600	4050	236.8	-818.8	-582.2	-50.4	-632.6	rooty
12600	4075	323.7	-818.8	-495.1	-50.4	-545.5	
12600	4100	400.0	-818.8	-418.8	-50.4	-469.2	
12600	4125	444.0	-818.8	-374.8	-50.4	-425.2	
12600	4150	442.0	-818.8	-375.8	-50.4	-427.2	
12600	4175	408.0	-818.8	-410.8	-50.4	-461.2	many rocks
12600	4200	340.8	-818.8	-478.0	-50.4	-528.4	north side of road. Rocky
12600	4225	222.8	-818.8	-596.0	-50.4	-846.4	
12600	4250	215.9	-818.8	-602.9	-50.4	-853.3	
12200E, 3400N		-50.2					
12200	2525	512.0	-869.0	-357.0	-50.4	-407.4	lots willow roots
12200	2535	524.0	-869.0	-345.0	-50.4	-395.4	lots willow roots
12200	2550	471.0	-869.0	-398.0	-50.4	-448.4	some willow roots
12200	2575	408.0	-869.0	-461.0	-50.4	-511.4	
12200	2600	392.6	-869.0	-476.5	-50.4	-526.9	alternating brown and black rocks
12200	2625	375.9	-869.0	-493.1	-50.4	-543.5	willow roots
12200	2650	370.9	-869.0	-498.1	-50.4	-548.5	
12200	2675	386.9	-869.0	-482.1	-50.4	-532.5	
12200	2700	393.1	-869.0	-475.9	-50.4	-526.3	alt. Bm, blk rx in subcrop
12200	2725	359.2	-869.0	-509.8	-50.4	-560.2	alt. Bm, blk rx in subcrop
12200	2750	337.5	-869.0	-531.5	-50.4	-581.9	lts willow roots
12200	2775	309.6	-869.0	-559.4	-50.4	-609.8	lighter looking rx
12200	2800	194.6	-869.0	-674.4	-50.4	-724.8	willow rts
12200	2825	170.3	-869.0	-698.7	-50.4	-749.1	
12200	2850	66.7	-869.0	-802.3	-50.4	-852.7	back to black argillite rocks
12200	2875	10.5	-869.0	-858.5	-50.4	-908.9	
12200	2900	5.2	-869.0	-863.8	-50.4	-914.2	rock change again?
12200	2925	-11.5	-869.0	-880.5	-50.4	-930.9	
12200	2950	-0.7	-869.0	-889.7	-50.4	-920.1	some willow rts
12200	2975	-10.6	-869.0	-879.6	-50.4	-930.0	
12200	3000	0.7	-869.0	-868.3	-50.4	-918.7	
12200	3025	0.7	-869.0	-868.3	-50.4	-918.7	
12200	3050	25.1	-869.0	-843.9	-50.4	-894.3	many rocks
12200	3075	-0.3	-869.0	-869.3	-50.4	-919.7	
12200	3100	2.3	-869.0	-866.7	-50.4	-917.1	
12200	3125	-22.9	-869.0	-891.9	-50.4	-942.3	lots willow rts
12200	3150	-12.3	-869.0	-881.3	-50.4	-931.7	blk dk grey arg. some rx in hole
12200	3175	-3.9	-869.0	-872.9	-50.4	-923.3	
12200	3200	-5.4	-869.0	-874.4	-50.4	-924.8	
12200	3225	-2.6	-869.0	-871.6	-50.4	-922.0	
12200	3250	-4.3	-869.0	-873.3	-50.4	-923.7	willow, lts roots
12200	3275	-18.6	-869.0	-887.8	-50.4	-938.0	
12200	3300	-3.2	-869.0	-872.2	-50.4	-922.6	lots roots
12200	3325	-14.0	-869.0	-883.0	-50.4	-933.4	rocky
12200	3350	-8.1	-869.0	-877.1	-50.4	-927.5	
12200	3375	-15.0	-869.0	-884.0	-50.4	-934.4	
12200	3400	-50.2	-818.8	-889.0	-50.4	-919.4	
12200	3425	11.0	-869.0	-858.1	-50.4	-908.5	
12200	3450	8.3	-869.0	-860.7	-50.4	-911.1	
12200	3475	-6.2	-869.0	-875.2	-50.4	-925.6	a bit rocky on little knob
12200	3500	-6.4	-869.0	-875.4	-50.4	-925.8	
12200	3525	-26.6	-869.0	-895.6	-50.4	-948.0	
12200	3550	-22.5	-869.0	-891.5	-50.4	-941.9	lots of rocks
12200	3575	-26.6	-869.0	-895.6	-50.4	-946.0	
12200	3600	-20.9	-869.0	-889.9	-50.4	-940.3	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
12200	3625	-7.4	-869.0	-876.4	-50.4	-926.8	
12200	3650	-16.1	-869.0	-885.1	-50.4	-935.5	
12200	3675	-28.1	-869.0	-897.1	-50.4	-947.5	lots of rocks
12200	3700	-23.3	-869.0	-892.3	-50.4	-942.7	rx change to north
12200	3725	-12.4	-869.0	-881.4	-50.4	-931.8	roots
12200	3750	-7.2	-869.0	-878.2	-50.4	-928.6	more roots
12200	3775	-17.0	-869.0	-888.0	-50.4	-938.4	
12200	3800	-26.1	-869.0	-895.1	-50.4	-945.5	
12200	3825	-30.3	-869.0	-899.3	-50.4	-949.7	
12200	3850	-22.0	-869.0	-891.0	-50.4	-941.4	
12200	3875	-13.8	-869.0	-882.8	-50.4	-933.2	
12200	3900	-0.7	-869.0	-869.7	-50.4	-920.1	
12200	3925	26.4	-869.0	-842.6	-50.4	-893.0	rocky
12200	3950	108.1	-869.0	-760.9	-50.4	-811.3	
12200	3975	147.2	-869.0	-721.8	-50.4	-772.2	
12200	4000	179.7	-869.0	-689.3	-50.4	-739.7	quite rocky
12200	4025	165.7	-869.0	-703.3	-50.4	-753.7	still rocky
12200	4050	138.5	-869.0	-730.5	-50.4	-780.9	roots
12200	4075	209.6	-869.0	-659.4	-50.4	-709.8	rocky
12200	4100	171.2	-869.0	-697.8	-50.4	-748.2	lots roots
12200	4125	163.9	-869.0	-705.1	-50.4	-755.5	rocky
12200	4150	199.2	-869.0	-669.8	-50.4	-720.2	
12200	4175	249.7	-869.0	-619.3	-50.4	-669.7	
12200	4200	310.3	-869.0	-558.7	-50.4	-609.1	
12200	4225	376.5	-869.0	-490.1	-50.4	-540.5	
12200	4238	431.0	-869.0	-438.0	-50.4	-488.4	
12200	4250	478.0	-869.0	-391.0	-50.4	-441.4	
11800E, 3390N							
11800	2525	26.3	-842.7	-119.7	-50.4	-170.1	lots roots
11800	2550	708.0	-842.7	-134.7	-50.4	-185.1	lots roots
11800	2575	710.0	-842.7	-132.7	-50.4	-183.1	
11800	2600	728.0	-842.7	-114.7	-50.4	-165.1	
11800	2625	710.0	-842.7	-132.7	-50.4	-183.1	
11800	2650	714.0	-842.7	-128.7	-50.4	-179.1	
11800	2675	710.0	-842.7	-132.7	-50.4	-183.1	lots willow roots
11800	2700	694.0	-842.7	-148.7	-50.4	-199.1	
11800	2725	698.0	-842.7	-144.7	-50.4	-195.1	lots roots
11800	2750	691.0	-842.7	-151.7	-50.4	-202.1	
11800	2775	685.0	-842.7	-157.7	-50.4	-208.1	rocky
11800	2800	700.0	-842.7	-142.7	-50.4	-193.1	
11800	2825	679.0	-842.7	-163.7	-50.4	-214.1	
11800	2850	684.0	-842.7	-158.7	-50.4	-209.1	
11800	2875	667.0	-842.7	-175.7	-50.4	-226.1	
11800	2900	675.0	-842.7	-187.7	-50.4	-218.1	
11800	2925	639.0	-842.7	-203.7	-50.4	-254.1	
11800	2950	571.0	-842.7	-271.7	-50.4	-322.1	rocky
11800	2975	533.0	-842.7	-309.7	-50.4	-360.1	
11800	3000	568.0	-842.7	-274.7	-50.4	-325.1	
11800	3025	425.0	-842.7	-417.7	-50.4	-468.1	
11800	3050	343.3	-842.7	-499.4	-50.4	-549.8	lots roots
11800	3075	268.6	-842.7	-574.1	-50.4	-624.5	
11800	3100	246.3	-842.7	-596.4	-50.4	-646.8	
11800	3125	149.2	-842.7	-693.5	-50.4	-743.9	
11800	3150	142.2	-842.7	-700.5	-50.4	-750.9	
11800	3175	122.0	-842.7	-720.7	-50.4	-771.1	
11800	3200	91.5	-842.7	-751.2	-50.4	-801.6	
11800	3225	24.6	-842.7	-818.1	-50.4	-868.5	many rocks
11800	3250	36.9	-842.7	-805.8	-50.4	-856.2	
11800	3275	-0.3	-842.7	-843.0	-50.4	-893.4	
11800	3300	-6.5	-842.7	-836.2	-50.4	-886.6	
11800	3325	-3.9	-842.7	-846.6	-50.4	-897.0	
11800	3350	9.5	-842.7	-833.2	-50.4	-883.6	
11800	3375	2.4	-842.7	-840.3	-50.4	-890.7	
11800	3390	26.3	-869.0	-842.7	-50.4	-893.1	
11800	3425	-33.1	-842.7	-875.8	-50.4	-926.2	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
11800	3450	-29.9	-842.7	-872.6	-50.4	-923.0	
11800	3475	14.4	-842.7	-828.3	-50.4	-878.7	
11800	3500	-28.4	-842.7	-871.1	-50.4	-921.5	
11800	3525	-36.7	-842.7	-879.4	-50.4	-929.8	
11800	3550	-25.6	-842.7	-868.3	-50.4	-918.7	
11800	3575	-23.2	-842.7	-865.9	-50.4	-916.3	
11800	3600	-11.6	-842.7	-854.3	-50.4	-904.7	
11800	3625	-14.9	-842.7	-857.6	-50.4	-908.0	
11800	3650	-17.9	-842.7	-860.6	-50.4	-911.0	
11800	3675	-21.4	-842.7	-864.1	-50.4	-914.5	
11800	3700	-19.3	-842.7	-862.0	-50.4	-912.4	
11800	3725	-6.3	-842.7	-849.0	-50.4	-899.4	
11800	3750	14.3	-842.7	-828.4	-50.4	-878.8	some roots
11800	3775	33.7	-842.7	-809.0	-50.4	-859.4	rocky and some roots
11800	3800	43.1	-842.7	-799.6	-50.4	-850.0	
11800	3825	82.3	-842.7	-760.4	-50.4	-810.8	
11800	3850	132.2	-842.7	-710.5	-50.4	-760.9	
11800	3875	171.4	-842.7	-671.3	-50.4	-721.7	
11800	3900	207.5	-842.7	-635.2	-50.4	-685.6	rocky
11800	3925	225.3	-842.7	-617.4	-50.4	-667.8	rocky
11800	3950	211.4	-842.7	-631.3	-50.4	-681.7	
11800	3975	194.8	-842.7	-647.9	-50.4	-698.3	
11800	4000	158.2	-842.7	-684.5	-50.4	-734.9	rocky
11800	4025	141.8	-842.7	-700.9	-50.4	-751.3	
11800	4050	160.6	-842.7	-673.1	-50.4	-723.5	rocky and rocky inlie
11800	4075	190.4	-842.7	-652.3	-50.4	-702.7	
11800	4100	240.1	-842.7	-602.6	-50.4	-653.0	blk, brn rx + qtz
11800	4125	279.7	-842.7	-563.0	-50.4	-613.4	few rx/ lots willow rts
11800	4150	319.4	-842.7	-523.3	-50.4	-573.7	lots willows
11800	4175	438.0	-842.7	-404.7	-50.4	-455.1	
11800	4200	486.0	-842.7	-356.7	-50.4	-407.1	above rd to south
11800	4225	635.0	-842.7	-207.7	-50.4	-258.1	really rky N side rd
11800	4250	705.0	-842.7	-137.7	-50.4	-188.1	lots argillite
11800	4260	731.0	-842.7	-111.7	-50.4	-162.1	lots roots, rx
upperditchlineRdat 4200N .0							
-850	11760	2613	400.0	-481.0	-81.0	-562.0	
-825	11761	2638	401.0	-481.0	-80.0	-561.0	
-800	11762	2664	424.0	-481.0	-57.0	-538.0	
-775	11756	2691	448.0	-481.0	-33.0	-514.0	
-750	11754	2714	488.0	-481.0	7.0	-474.0	
-725	11756	2740	470.0	-481.0	-11.0	-492.0	
-700	11767	2765	477.0	-481.0	-4.0	-505.0	
-675	11767	2788	477.0	-481.0	-4.0	-505.0	
-650	11752	2813	467.0	-481.0	-14.0	-525.0	rock change
-625	11757	2837	468.0	-481.0	-13.0	-534.0	
-600	11756	2862	468.0	-481.0	-15.0	-546.0	muddy
-575	11753	2888	466.0	-481.0	-15.0	-556.0	
-550	11747	2912	479.0	-481.0	-2.0	-563.0	out of mud (some water)
-525	11744	2937	487.0	-481.0	-14.0	-595.0	mud
-500	11741	2961	453.0	-481.0	-28.0	-609.0	mud
-475	11734	2985	431.0	-481.0	-50.0	-632.0	mud
-450	11725	3012	425.0	-481.0	-56.0	-637.0	mud
-425	11718	3037	415.0	-481.0	-66.0	-647.0	muddy from hoe
-400	11708	3063	390.8	-481.0	-90.2	-671.2	
-375	11700	3087	341.7	-481.0	-139.3	-621.3	
-350	11687	3123	230.1	-481.0	-250.9	-531.9	
-325	11674	3131	116.8	-481.0	-364.2	-447.4	
-300	11659	3153	18.9	-481.0	-462.1	-443.2	
-275	11646	3172	-83.1	-481.0	-564.1	-481.0	
-250	11631	3197	-182.0	-481.0	-663.0	-514.0	
-225	11618	3216	-209.4	-481.0	-690.4	-541.4	
-200	11606	3235	-196.7	-481.0	-677.7	-526.7	
-175	11588	3258	-150.1	-481.0	-631.1	-481.0	
-150	11572	3278	-106.7	-481.0	-587.7	-434.0	
-125	11559	3300	-73.8	-481.0	-554.8	-401.0	

CONTROL STATION	SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
	EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
-100	11543	3316	-61.6	-481.0	-542.6	-50.4	-593.0	
-75	11531	3331	-40.3	-481.0	-521.3	-50.4	-571.7	
-50	11519	3366	0.0	-481.0	-481.0	-50.4	-531.4	
-25	11525	3388	27.4	-481.0	-453.6	-50.4	-504.0	
0	11525	3413	361.7	-842.7	-481.0	-50.4	-531.4	
25	11506	3432	-8.8	-481.0	-489.8	-50.4	-540.2	
50	11505	3463	-20.8	-481.0	-501.8	-50.4	-552.2	
75	11504	3488	-147.6	-481.0	-628.6	-50.4	-679.0	
100	11504	3513	-244.7	-481.0	-725.7	-50.4	-776.1	
125	11505	3538	-267.6	-481.0	-748.6	-50.4	-799.0	
150	11506	3561	-291.0	-481.0	-772.0	-50.4	-822.4	
175	11504	3587	-287.6	-481.0	-768.6	-50.4	-819.0	
200	11496	3614	-281.7	-481.0	-762.7	-50.4	-813.1	
225	11489	3638	-265.2	-481.0	-746.2	-50.4	-796.6	
250	11488	3664	-266.1	-481.0	-747.1	-50.4	-797.5	
275	11488	3689	-274.4	-481.0	-755.4	-50.4	-805.8	
300	11497	3713	-267.4	-481.0	-748.4	-50.4	-798.8	
325	11505	3738	-227.4	-481.0	-708.4	-50.4	-758.8	
350	11511	3761	-207.9	-481.0	-688.9	-50.4	-739.3	
375	11516	3785	-180.2	-481.0	-661.2	-50.4	-711.6	
400	11527	3812	-183.5	-481.0	-664.5	-50.4	-714.9	
425	11537	3833	-151.1	-481.0	-632.1	-50.4	-682.5	
450	11545	3858	-76.0	-481.0	-557.0	-50.4	-607.4	
475	11556	3876	-35.3	-481.0	-516.3	-50.4	-566.7	
500	11571	3900	14.6	-481.0	-466.4	-50.4	-516.8	
525	11585	3920	64.7	-481.0	-416.3	-50.4	-466.7	
550	11600	3943	85.7	-481.0	-395.3	-50.4	-445.7	
575	11613	3961	92.8	-481.0	-388.2	-50.4	-438.6	
600	11626	3983	74.3	-481.0	-406.7	-50.4	-457.1	
625	11640	4007	75.3	-481.0	-405.7	-50.4	-456.1	
650	11654	4025	92.7	-481.0	-388.3	-50.4	-438.7	
675	11666	4049	82.7	-481.0	-398.3	-50.4	-448.7	
700	11680	4071	92.3	-481.0	-388.7	-50.4	-439.1	
725	11694	4090	115.3	-481.0	-365.7	-50.4	-416.1	
750	11704	4113	190.3	-481.0	-290.7	-50.4	-341.1	big piece of metal on NW side of rd
775	11706	4138	214.2	-481.0	-266.8	-50.4	-317.2	
800	11708	4163	266.8	-481.0	-214.2	-50.4	-264.6	
825	11727	4181	295.6	-481.0	-185.4	-50.4	-235.8	
11400E, 3400N			309.2					
	11400	2525	240.0	-171.8	68.2	-50.4	17.8	
	11400	2550	237.9	-171.8	66.1	-50.4	15.7	
	11400	2575	232.1	-171.8	60.3	-50.4	9.9	lots of roots
	11400	2600	236.1	-171.8	64.3	-50.4	13.9	
	11400	2625	220.3	-171.8	48.5	-50.4	-1.9	
	11400	2650	246.9	-171.8	75.1	-50.4	24.7	
	11400	2675	227.8	-171.8	56.0	-50.4	5.6	
	11400	2700	249.8	-171.8	78.0	-50.4	27.6	
	11400	2725	243.9	-171.8	72.1	-50.4	21.7	
	11400	2750	252.1	-171.8	80.3	-50.4	29.9	
	11400	2775	264.0	-171.8	92.2	-50.4	41.8	
	11400	2800	281.4	-171.8	109.6	-50.4	59.2	
	11400	2825	281.2	-171.8	109.4	-50.4	59.0	
	11400	2850	274.9	-171.8	103.1	-50.4	52.7	brown weathered rock
	11400	2875	279.8	-171.8	108.0	-50.4	57.6	
	11400	2900	297.3	-171.8	125.5	-50.4	75.1	
	11400	2925	288.7	-171.8	105.3	-50.4	54.9	tent value corrected
	11400	2950	300.8	-171.8	129.0	-50.4	78.8	on W side of road (lower ditchline)
	11400	2975	273.7	-171.8	101.9	-50.4	51.5	
	11400	3000	297.3	-171.8	125.5	-50.4	75.1	
	11400	3025	289.3	-171.8	117.5	-50.4	67.1	
	11400	3050	284.8	-171.8	113.0	-50.4	62.6	
	11400	3075	285.5	-171.8	113.7	-50.4	63.3	
	11400	3100	279.6	-171.8	107.8	-50.4	57.4	
	11400	3125	257.6	-171.8	85.8	-50.4	35.4	
	11400	3150	256.6	-171.8	84.8	-50.4	34.4	lots roots

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
11400	3175	253.0	-171.8	81.2	-50.4	30.8	
11400	3200	255.7	-171.8	83.9	-50.4	33.5	
11400	3225	230.5	-171.8	58.7	-50.4	8.3	
11400	3250	165.0	-171.8	-6.8	-50.4	-57.2	
11400	3275	45.1	-171.8	-126.7	-50.4	-177.1	
11400	3300	-30.8	-171.8	-202.6	-50.4	-253.0	
11400	3325	-40.1	-171.8	-211.9	-50.4	-262.3	
11400	3350	-28.6	-171.8	-200.4	-50.4	-250.8	qtz in hole
11400	3375	-53.6	-171.8	-225.4	-50.4	-275.8	
11400	3400	309.2	-481.0	-171.8	-50.4	-222.2	
11400	3425	40.2	-171.8	-131.6	-50.4	-182.0	
11400	3450	108.9	-171.8	-62.9	-50.4	-113.3	
11400	3475	132.1	-171.8	-39.7	-50.4	-90.1	
11400	3500	65.0	-171.8	-106.8	-50.4	-157.2	fault?
11400	3525	-143.2	-171.8	-315.0	-50.4	-365.4	
11400	3550	-411.0	-171.8	-582.8	-50.4	-633.2	
11400	3575	-520.0	-171.8	-691.8	-50.4	-742.2	
11400	3600	-553.0	-171.8	-724.8	-50.4	-775.2	
11400	3625	-570.0	-171.8	-741.8	-50.4	-792.2	
11400	3650	-596.0	-171.8	-767.8	-50.4	-818.2	
11400	3675	-585.0	-171.8	-756.8	-50.4	-807.2	
11400	3700	-612.0	-171.8	-783.8	-50.4	-834.2	
11400	3725	-621.0	-171.8	-792.8	-50.4	-843.2	lots of roots
11400	3750	-604.0	-171.8	-775.8	-50.4	-826.2	blk rocky sub crop
11400	3775	-546.0	-171.8	-717.8	-50.4	-768.2	
11400	3800	-500.0	-171.8	-671.8	-50.4	-722.2	
11400	3825	-484.0	-171.8	-655.8	-50.4	-706.2	
11400	3850	-480.0	-171.8	-651.8	-50.4	-702.2	
11400	3875	-483.0	-171.8	-654.8	-50.4	-705.2	
11400	3900	-467.0	-171.8	-638.8	-50.4	-689.2	lots of roots
11400	3925	-452.0	-171.8	-623.8	-50.4	-674.2	
11400	3950	-415.0	-171.8	-586.8	-50.4	-637.2	rocky
11400	3975	-392.0	-171.8	-563.8	-50.4	-614.2	
11400	4000	-385.7	-171.8	-557.5	-50.4	-607.9	
11400	4025	-403.0	-171.8	-574.8	-50.4	-625.2	
11400	4050	-388.0	-171.8	-559.8	-50.4	-610.2	
11400	4075	-386.0	-171.8	-557.8	-50.4	-608.2	
11400	4100	-312.5	-171.8	-484.3	-50.4	-534.7	
11400	4125	-284.5	-171.8	-436.3	-50.4	-486.7	
11400	4150	-165.4	-171.8	-337.2	-50.4	-387.6	
11400	4175	-70.1	-171.8	-241.9	-50.4	-292.3	
11400	4200	62.3	-171.8	-118.3	-50.4	-168.7	tentvaluecorrected to corr w duplicate station from lower DL road averaged
11400	4225	93.5	-171.8	-78.3	-50.4	-128.7	
11400	4250	126.5	-171.8	-45.3	-50.4	-95.7	
lowerDitchLineRd@3400N		344.8	-136.2				
-500	11400	2925	229.8	-136.2	105.3	-50.4	54.9 tent value corrected
-475	11394	2925	241.7	-136.2	105.5	-50.4	55.1
-450	11387	2975	238.8	-136.2	102.6	-50.4	52.2
-425	11379	2999	243.7	-136.2	107.5	-50.4	57.1
-400	11369	3023	250.9	-136.2	114.7	-50.4	64.3 on road again over grown
-375	11360	3042	242.0	-136.2	105.8	-50.4	55.4 in dirt mound by ditch line
-350	11353	3062	241.1	-136.2	104.9	-50.4	54.5 in dirt mound by ditch line
-325	11344	3088	245.0	-136.2	108.8	-50.4	58.4 in dirt mound by ditch line
-300	11334	3114	234.5	-136.2	98.3	-50.4	47.9 in dirt mound by ditch line
-275	11325	3131	241.2	-136.2	105.0	-50.4	54.6 in dirt mound by ditch line
-250	11314	3166	234.0	-136.2	97.8	-50.4	47.4 in dirt mound by ditch line
-225	11310	3188	237.2	-136.2	101.0	-50.4	50.6 in dirt mound by ditch line
-200	11300	3210	226.7	-136.2	90.5	-50.4	40.1
-175	11290	3233	212.9	-136.2	76.7	-50.4	26.3
-150	11284	3257	200.7	-136.2	64.5	-50.4	14.1
-125	11275	3282	162.1	-136.2	25.9	-50.4	-24.5
-100	11267	3305	99.4	-136.2	-36.8	-50.4	-87.2
-75	11256	3331	-10.3	-136.2	-146.5	-50.4	-196.9
-50	11250	3355	-74.9	-136.2	-211.1	-50.4	-261.5
-25	11241	3379	-45.8	-136.2	-182.0	-50.4	-232.4

CONTROL STATION

	SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
	EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
0	11238	3400	344.8	-481.0	-136.2	-50.4	-186.6	
25	11234	3437	-16.1	-136.2	-152.3	-50.4	-202.7	
50	11237	3463	3.1	-136.2	-133.1	-50.4	-183.5	
75	11237	3499	111.7	-136.2	-24.5	-50.4	-74.9	
100	11239	3527	167.3	-136.2	31.1	-50.4	-19.3	
125	11244	3563	161.4	-136.2	25.2	-50.4	-25.2	
150	11246	3599	156.5	-136.2	20.3	-50.4	-30.1	
175	11248	3631	119.7	-136.2	-18.5	-50.4	-66.9	
200	11241	3662	30.2	-136.2	-108.0	-50.4	-158.4	
225	11256	3691	-51.4	-136.2	-187.8	-50.4	-238.0	
250	11262	3722	-107.0	-136.2	-243.2	-50.4	-293.8	
275	11267	3750	-159.3	-136.2	-295.5	-50.4	-345.9	
300	11275	3768	-186.5	-136.2	-322.7	-50.4	-373.1	
325	11281	3794	-193.7	-136.2	-329.9	-50.4	-380.3	muddy
350	11287	3819	-183.5	-136.2	-319.7	-50.4	-370.1	muddy
375	11295	3842	-185.4	-136.2	-321.6	-50.4	-372.0	muddy
400	11301	3861	-179.8	-136.2	-316.0	-50.4	-366.4	muddy
425	11306	3883	-185.7	-136.2	-321.9	-50.4	-372.3	
450	11315	3915	-164.5	-136.2	-300.7	-50.4	-351.1	
475	11323	3940	-175.4	-136.2	-311.6	-50.4	-362.0	
500	11328	3964	-211.0	-136.2	-347.2	-50.4	-397.6	
525	11338	3987	-212.9	-136.2	-349.1	-50.4	-399.5	
550	11344	4010	-252.7	-136.2	-388.9	-50.4	-439.3	
575	11350	4036	-257.8	-136.2	-394.0	-50.4	-444.4	
600	11359	4059	-269.5	-136.2	-405.7	-50.4	-456.1	
625	11363	4081	-232.8	-136.2	-369.0	-50.4	-419.4	
650	11367	4106	-193.9	-136.2	-330.1	-50.4	-380.5	
675	11376	4131	-102.1	-136.2	-238.3	-50.4	-288.7	fork in road
700	11385	4153	-45.8	-136.2	-182.0	-50.4	-232.4	main road goes to NE
725	11392	4175	-23.4	-136.2	-159.6	-50.4	-210.0	
750	11400	4200	9.1	-136.2	-118.3	-50.4	-168.7	tentative corrected to corr w duplicate station from lower DL road...averaged
775	11416	4218	61.1	-136.2	-75.1	-50.4	-125.5	
800	11427	4238	107.0	-136.2	-29.2	-50.4	-79.6	
825	11444	4259	140.9	-136.2	4.7	-50.4	-45.7	
11000E, 3400N			194.7					
	11000	2525	27.4	58.5	85.9	-50.4	35.5	blk rocky ground
	11000	2550	10.2	58.5	68.7	-50.4	18.3	
	11000	2575	18.6	58.5	77.1	-50.4	26.7	
	11000	2600	20.5	58.5	79.0	-50.4	28.6	
	11000	2625	2.2	58.5	60.7	-50.4	10.3	
	11000	2650	12.8	58.5	71.3	-50.4	20.9	
	11000	2675	31.9	58.5	90.3	-50.4	39.9	
	11000	2700	39.8	58.5	97.3	-50.4	46.9	
	11000	2725	35.1	58.5	93.6	-50.4	43.2	
	11000	2750	31.1	58.5	89.6	-50.4	39.2	
	11000	2775	20.6	58.5	79.1	-50.4	28.7	
	11000	2800	48.0	58.5	106.5	-50.4	56.1	
	11000	2825	19.2	58.5	77.7	-50.4	27.3	
	11000	2850	33.0	58.5	91.5	-50.4	41.1	
	11000	2875	27.0	58.5	85.5	-50.4	35.1	
	11000	2900	48.4	58.5	108.9	-50.4	58.5	
	11000	2925	25.6	58.5	84.1	-50.4	33.7	
	11000	2950	64.5	58.5	123.0	-50.4	72.6	some roots
	11000	2975	40.0	58.5	98.5	-50.4	48.1	
	11000	3000	33.5	58.5	92.0	-50.4	41.6	
	11000	3025	43.7	58.5	102.2	-50.4	51.8	
	11000	3050	57.5	58.5	116.0	-50.4	65.6	lots of roots
	11000	3075	62.3	58.5	120.8	-50.4	70.4	
	11000	3100	62.6	58.5	121.0	-50.4	70.8	fluctuating plus/minus 3
	11000	3125	63.7	58.5	122.2	-50.4	71.8	
	11000	3150	56.4	58.5	114.9	-50.4	64.5	
	11000	3175	61.6	58.5	120.1	-50.4	69.7	creek
	11000	3200	60.6	58.5	119.1	-50.4	68.7	
	11000	3225	54.7	58.5	113.2	-50.4	62.8	
	11000	3250	44.2	58.5	102.7	-50.4	52.3	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
11000	3275	40.2	58.5	98.7	-50.4	48.3	
11000	3300	46.1	58.5	104.6	-50.4	54.2	
11000	3325	33.7	58.5	92.2	-50.4	41.8	
11000	3350	15.5	58.5	74.0	-50.4	23.6	
11000	3375	-4.3	58.5	54.2	-50.4	3.8	
11000	3400	194.7	58.5	58.5	-50.4	8.1	
11000	3425	3.2	58.5	61.7	-50.4	11.3	
11000	3450	11.3	58.5	69.6	-50.4	19.4	
11000	3475	5.9	58.5	64.4	-50.4	14.0	lots of roots
11000	3500	7.7	58.5	66.2	-50.4	15.8	
11000	3525	-3.5	58.5	55.0	-50.4	4.6	
11000	3550	-17.1	58.5	41.4	-50.4	-9.0	
11000	3575	-21.3	58.5	37.2	-50.4	-13.2	
11000	3600	-0.4	58.5	58.1	-50.4	7.7	
11000	3625	-18.1	58.5	40.4	-50.4	-10.0	
11000	3650	-27.2	58.5	31.3	-50.4	-19.1	
11000	3675	-51.4	58.5	7.1	-50.4	-43.3	
11000	3700	-90.8	58.5	-32.3	-50.4	-82.7	
11000	3725	-140.9	58.5	-82.4	-50.4	-132.8	
11000	3750	-190.3	58.5	-131.8	-50.4	-182.2	
11000	3775	-235.1	58.5	-176.6	-50.4	-227.0	
11000	3800	-325.9	58.5	-267.4	-50.4	-317.8	
11000	3825	-514.0	58.5	-455.5	-50.4	-505.9	
11000	3850	-664.0	58.5	-605.5	-50.4	-655.9	
11000	3875	-641.0	58.5	-582.5	-50.4	-632.5	
11000	3900	-610.0	58.5	-551.5	-50.4	-601.9	
11000	3925	-570.0	58.5	-511.5	-50.4	-561.9	
11000	3950	-518.0	58.5	-459.5	-50.4	-509.9	lots of roots
11000	3975	-482.0	58.5	-423.5	-50.4	-473.9	
11000	4000	-482.0	58.5	-423.5	-50.4	-473.9	
11000	4025	-436.0	58.5	-377.5	-50.4	-427.9	
11000	4050	-398.0	58.5	-339.5	-50.4	-389.9	
11000	4075	-363.6	58.5	-305.1	-50.4	-355.5	
11000	4100	-335.1	58.5	-276.6	-50.4	-327.0	
11000	4125	-293.8	58.5	-235.3	-50.4	-285.7	
11000	4150	-277.5	58.5	-219.0	-50.4	-269.4	lots of roots
11000	4175	-253.9	58.5	-195.4	-50.4	-245.8	
11000	4200	-227.2	58.5	-168.7	-50.4	-219.1	
11000	4225	-219.7	58.5	-161.2	-50.4	-211.6	lots of black rocks
11000	4250	-197.6	58.5	-139.1	-50.4	-189.5	
11000	4275	-186.9	58.5	-128.4	-50.4	-178.8	
10600E, 3400N							
10600	3400	-74.6	-16.1	-16.1	-50.4	-66.5	
10600	3425	-68.9	-16.1	-85.0	-50.4	-135.4	
10600	3450	-52.1	-16.1	-68.2	-50.4	-118.6	blk argillite, weathered orange lying around
10600	3475	-32.3	-16.1	-48.4	-50.4	-98.8	
10600	3500	-28.1	-16.1	-44.2	-50.4	-84.6	
10600	3525	-134.1	-16.1	-150.2	-50.4	-200.6	
10600	3550	-231.5	-16.1	-247.6	-50.4	-298.0	
10600	3575	-261.7	-16.1	-277.8	-50.4	-328.2	
10600	3600	-368.6	-16.1	-382.7	-50.4	-433.1	
10600	3625	-502.0	-16.1	-518.1	-50.4	-568.5	
10600	3650	-357.4	-16.1	-373.5	-50.4	-423.9	
10600	3675	-214.4	-16.1	-230.5	-50.4	-280.9	
10600	3700	-322.9	-16.1	-339.0	-50.4	-389.4	black argillite rocks
10600	3725	-586.0	-16.1	-602.1	-50.4	-652.5	
10600	3750	-471.0	-16.1	-487.1	-50.4	-537.5	
10600	3775	-303.9	-16.1	-320.0	-50.4	-370.4	
10600	3800	-286.0	-16.1	-302.1	-50.4	-352.5	
10600	3825	-422.0	-16.1	-438.1	-50.4	-488.5	
10600	3850	-389.0	-16.1	-405.1	-50.4	-455.5	
10600	3875	-273.5	-16.1	-289.6	-50.4	-340.0	
10600	3900	-297.2	-16.1	-313.3	-50.4	-363.7	
10600	3925	-479.0	-16.1	-495.1	-50.4	-545.5	
10600	3950	-661.0	-16.1	-677.1	-50.4	-727.5	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
10600	3975	-668.0	-18.1	-684.1	-50.4	-734.5	
10600	4000	-608.0	-18.1	-624.1	-50.4	-674.5	change to grey phyllitic rocks
10600	4025	-588.0	-18.1	-604.1	-50.4	-654.5	
10600	4050	-544.0	-18.1	-560.1	-50.4	-610.5	
10600	4075	-380.4	-18.1	-378.5	-50.4	-426.9	
10600	4100	-331.7	-18.1	-347.8	-50.4	-398.2	
10600	4125	-215.2	-18.1	-231.3	-50.4	-281.7	
10600	4150	-92.7	-18.1	-108.8	-50.4	-158.2	
10600	4175	-86.3	-18.1	-102.4	-50.4	-152.8	
10600	4200	-188.3	-18.1	-204.4	-50.4	-254.8	
10600	4225	-262.7	-18.1	-278.8	-50.4	-329.2	
10600	4250	-170.6	-18.1	-188.7	-50.4	-237.1	
10600	4275	-80.5	-18.1	-96.6	-50.4	-147.0	
10200E, 3400N		33.4					
		33.4	58.5	91.9	-50.4	41.5	TAKEN FROM 11000E, 3400N

Wed Aug 22, 2001
20800E, 2800N

20800	2400	0.1					
20800	2425	-17.4	0.1	-17.3	0.0	-17.3	
20800	2450	-5.1	0.1	-5.0	0.0	-5.0	
20800	2475	0.8	0.1	0.9	0.0	0.9	
20800	2475	-13.6	0.1	-13.5	0.0	-13.5	
20800	2500	2.4	0.1	2.5	0.0	2.5	
20800	2525	-4.6	0.1	-4.5	0.0	-4.5	
20800	2550	3.8	0.1	3.9	0.0	3.9	
20800	2575	-21.4	0.1	-21.3	0.0	-21.3	
20800	2600	-25.1	0.1	-25.0	0.0	-25.0	
20800	2625	-29.0	0.1	-28.9	0.0	-28.9	
20800	2650	-70.3	0.1	-70.2	0.0	-70.2	
20800	2675	-21.8	0.1	-21.7	0.0	-21.7	
20800	2695	-17.6	0.1	-17.5	0.0	-17.5	
20800	2725	-11.4	0.1	-11.3	0.0	-11.3	road
20800	2750	-0.3	0.1	-0.2	0.0	-0.2	road fill
20800	2775	-17.0	0.1	-16.9	0.0	-16.9	
20800	2800	0.1	0.1	0.1	0.0	0.1	
20800	2825	-17.0	0.1	-16.9	0.0	-16.9	
20800	2850	14.5	0.1	14.6	0.0	14.6	
20800	2875	5.0	0.1	5.1	0.0	5.1	
20800	2900	24.4	0.1	24.5	0.0	24.5	
20800	2925	-10.1	0.1	-10.0	0.0	-10.0	
20800	2950	-51.8	0.1	-51.7	0.0	-51.7	
20800	2975	-141.1	0.1	-141.0	0.0	-141.0	
20800	3000	-96.1	0.1	-96.0	0.0	-96.0	gravelly
20800	3025	-44.5	0.1	-44.4	0.0	-44.4	
20800	3050	-20.5	0.1	-20.4	0.0	-20.4	platey, lt coloured gravel. Gravel > soil
20800	3075	-36.8	0.1	-36.7	0.0	-36.7	
20800	3100	-23.8	0.1	-23.7	0.0	-23.7	
20800	3125	-5.5	0.1	-5.4	0.0	-5.4	
20800	3150	-10.2	0.1	-10.1	0.0	-10.1	
20800	3175	-15.3	0.1	-15.2	0.0	-15.2	
20800	3200	-56.5	0.1	-56.4	0.0	-56.4	

21000E, 2807N

21000	2000	-103.9					
21000	2025	-204.3	-104.0	100.3	0.0	100.3	hydraulicked area of gulch
21000	2050	-209.7	-104.0	105.7	0.0	105.7	hydraulicked area of gulch, near small creek
21000	2075	178.9	-104.0	74.9	0.0	74.9	hydraulicked area of gulch
21000	2100	171.4	-104.0	67.4	0.0	67.4	hydraulicked area of gulch
21000	2125	179.7	-104.0	75.7	0.0	75.7	hydraulicked area of gulch
21000	2150	185.1	-104.0	81.1	0.0	81.1	hydraulicked area of gulch
21000	2175	180.7	-104.0	76.7	0.0	76.7	hydraulicked area of gulch
21000	2200	166.9	-104.0	62.9	0.0	62.9	hydraulicked area of gulch
21000	2225	181.4	-104.0	77.4	0.0	77.4	hydraulicked area of gulch
21000	2250	168.7	-104.0	64.7	0.0	64.7	hydraulicked area of gulch
21000	2275	157.5	-104.0	53.5	0.0	53.5	hydraulicked area of gulch
21000	2300	117.1	-104.0	13.1	0.0	13.1	edge of hydraulicked area
21000	2325	122.6	-104.0	18.6	0.0	18.6	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
21000	2325	116.2	-104.0	12.2	0.0	12.2	old cabin here
21000	2350	122.0	-104.0	18.0	0.0	18.0	
21000	2375	105.7	-104.0	1.7	0.0	1.7	
21000	2400	101.6	-104.0	-2.4	0.0	-2.4	
21000	2425	78.8	-104.0	-25.2	0.0	-25.2	
21000	2450	87.9	-104.0	-16.1	0.0	-16.1	
21000	2475	88.3	-104.0	-15.7	0.0	-15.7	
21000	2500	82.8	-104.0	-21.2	0.0	-21.2	swampy
21000	2525	84.4	-104.0	-39.6	0.0	-39.6	swampy
21000	2550	62.7	-104.0	-41.3	0.0	-41.3	
21000	2575	32.1	-104.0	-71.9	0.0	-71.9	
21000	2600	50.4	-104.0	-53.6	0.0	-53.6	
21000	2625	30.1	-104.0	-73.9	0.0	-73.9	
21000	2650	44.5	-104.0	-59.5	0.0	-59.5	
21000	2675	28.9	-104.0	-75.1	0.0	-75.1	
21000	2700	32.2	-104.0	-71.8	0.0	-71.8	
21000	2725	19.4	-104.0	-84.6	0.0	-84.6	
21000	2750	5.5	-104.0	-98.5	0.0	-98.5	on south side of the ditch line
21000	2775	7.5	-104.0	-96.5	0.0	-96.5	in road
21000	2807	-103.9	0.1	-104.0	0.0	-104.0	
21000	2825	34.1	-104.0	-69.9	0.0	-69.9	
21000	2850	97.6	-104.0	-6.4	0.0	-6.4	
21000	2875	91.5	-104.0	-12.5	0.0	-12.5	
21000	2900	130.0	-104.0	26.0	0.0	26.0	
21000	2925	87.7	-104.0	8.3	0.0	8.3	
21000	2950	103.0	-104.0	-1.0	0.0	-1.0	
21000	2975	53.6	-104.0	-50.4	0.0	-50.4	
21000	3000	-12.8	-104.0	-116.8	0.0	-116.8	
21000	3025	11.5	-104.0	-92.5	0.0	-92.5	
21000	3050	60.5	-104.0	-43.5	0.0	-43.5	
21000	3075	102.1	-104.0	-1.9	0.0	-1.9	11:40 am fluctuating abit
21000	3100	111.8	-104.0	7.8	0.0	7.8	fluctuating a lot ... plus/minus 10mV
21000	3125	80.8	-104.0	-23.2	0.0	-23.2	11:48am fluctuating A LOT.. plus/minus 25mV
21000	3150	90.4	-104.0	-13.6	0.0	-13.6	
21000	3175	51.2	-104.0	-52.8	0.0	-52.8	
21000	3200	-22.1	-104.0	-126.1	0.0	-126.1	
21000	3225	-157.6	-104.0	-261.6	0.0	-261.6	
21000	3250	-95.5	-104.0	-199.5	0.0	-199.5	
21000	3275	-127.0	-104.0	-231.0	0.0	-231.0	
21000	3300	-50.9	-104.0	-154.9	0.0	-154.9	
21000	3325	-12.5	-104.0	-116.5	0.0	-116.5	
21000	3350	-15.1	-104.0	-119.1	0.0	-119.1	
21000	3375	-42.0	-104.0	-146.0	0.0	-146.0	
21000	3400	-60.7	-104.0	-164.7	0.0	-164.7	
21000	3425	-80.0	-104.0	-184.0	0.0	-184.0	
21000	3450	-211.7	-104.0	-315.7	0.0	-315.7	
21000	3475	-22.1	-104.0	-126.1	0.0	-126.1	
21000	3500	43.6	-104.0	-60.4	0.0	-60.4	
21000	3525	68.3	-104.0	-35.7	0.0	-35.7	
21000	3550	92.1	-104.0	-11.9	0.0	-11.9	
21000	3575	72.2	-104.0	-31.8	0.0	-31.8	angled metal in ground
21000	3600	78.9	-104.0	-27.1	0.0	-27.1	
21200E, 2800N		-231.4					
21200	2000	400.0	-335.4	64.6	0.0	64.6	
21200	2025	384.1	-335.4	48.7	0.0	48.7	
21200	2050	399.0	-335.4	63.6	0.0	63.6	
21200	2075	385.4	-335.4	60.0	0.0	60.0	
21200	2100	392.4	-335.4	57.0	0.0	57.0	
21200	2125	383.2	-335.4	47.8	0.0	47.8	
21200	2150	375.0	-335.4	39.6	0.0	39.6	North side of road
21200	2175	365.2	-335.4	29.8	0.0	29.8	
21200	2200	399.0	-335.4	63.6	0.0	63.6	
21200	2225	371.1	-335.4	35.7	0.0	35.7	
21200	2250	370.6	-335.4	35.2	0.0	35.2	
21200	2275	360.1	-335.4	24.7	0.0	24.7	bottom of hyd pit.

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
21200	2300	410.0	-335.4	74.6	0.0	74.6	25 feet south of edge of hyd pit
21200	2325	334.7	-335.4	-0.7	0.0	-0.7	edge of hydraulicked pit
21200	2350	390.0	-335.4	54.6	0.0	54.6	
21200	2375	376.3	-335.4	40.9	0.0	40.9	
21200	2400	371.9	-335.4	36.4	0.0	36.4	
21200	2425	347.8	-335.4	12.4	0.0	12.4	
21200	2450	344.2	-335.4	8.8	0.0	8.8	fluct $\pm$ 4 mV
21200	2475	308.8	-335.4	-26.6	0.0	-26.6	fluct $\pm$ 2mV
21200	2500	330.6	-335.4	-4.8	0.0	-4.8	fluct $\pm$ 0.5 mV
21200	2525	303.5	-335.4	-31.9	0.0	-31.9	
21200	2550	248.5	-335.4	-86.9	0.0	-86.9	
21200	2575	247.2	-335.4	-88.2	0.0	-88.2	
21200	2600	246.0	-335.4	-89.4	0.0	-89.4	
21200	2625	217.6	-335.4	-117.8	0.0	-117.8	
21200	2650	222.8	-335.4	-112.6	0.0	-112.6	
21200	2675	208.9	-335.4	-126.5	0.0	-126.5	
21200	2700	199.6	-335.4	-135.8	0.0	-135.8	
21200	2725	164.4	-335.4	-171.0	0.0	-171.0	
21200	2750	132.7	-335.4	-202.7	0.0	-202.7	
21200	2775	47.6	-335.4	-287.8	0.0	-287.8	
21200	2800	-231.4	-104.0	-335.4	0.0	-335.4	on ditch line trail
21200	2825	74.9	-335.4	-260.5	0.0	-260.5	
21200	2850	215.6	-335.4	-119.8	0.0	-119.8	south side of road
21200	2875	241.5	-335.4	-93.9	0.0	-93.9	
21200	2900	276.8	-335.4	-58.6	0.0	-58.6	
21200	2925	294.1	-335.4	-41.3	0.0	-41.3	
21200	2950	321.7	-335.4	-13.7	0.0	-13.7	
21200	2975	319.4	-335.4	-16.0	0.0	-16.0	
21200	3000	326.2	-335.4	-9.2	0.0	-9.2	
21200	3025	306.6	-335.4	-28.8	0.0	-28.8	
21200	3050	327.6	-335.4	-7.6	0.0	-7.6	
21200	3075	331.7	-335.4	-3.7	0.0	-3.7	
21200	3100	333.0	-335.4	-2.4	0.0	-2.4	
21200	3125	318.3	-335.4	-17.1	0.0	-17.1	
21200	3150	318.2	-335.4	-17.2	0.0	-17.2	
21200	3175	301.8	-335.4	-33.6	0.0	-33.6	
21200	3200	297.4	-335.4	-38.0	0.0	-38.0	
21200	3225	315.5	-335.4	-19.9	0.0	-19.9	
21200	3250	278.0	-335.4	-59.4	0.0	-59.4	
21200	3275	205.7	-335.4	-129.7	0.0	-129.7	
21200	3300	177.6	-335.4	-157.8	0.0	-157.8	
21200	3325	209.6	-335.4	-125.8	0.0	-125.8	
21200	3350	220.5	-335.4	-114.9	0.0	-114.9	
21200	3375	223.9	-335.4	-111.5	0.0	-111.5	
21200	3400	243.3	-335.4	-92.1	0.0	-92.1	
21200	3425	249.2	-335.4	-86.2	0.0	-86.2	
21200	3450	281.1	-335.4	-54.3	0.0	-54.3	
21200	3475	289.7	-335.4	-45.7	0.0	-45.7	
21200	3500	329.8	-335.4	-5.6	0.0	-5.6	
21200	3525	341.6	-335.4	6.2	0.0	6.2	
21200	3550	342.0	-335.4	6.6	0.0	6.6	
21200	3575	336.9	-335.4	1.5	0.0	1.5	
21200	3600	312.8	-335.4	-22.6	0.0	-22.6	
Fri Aug 24 ..leapfrog method							
21175	2800	64.9	0.0	64.9	0.0	64.9	
21200	2775	59.3	64.9	124.2	0.0	124.2	
21200	2750	57.0	124.2	181.2	0.0	181.2	
21200	2725	31.7	181.2	212.9	0.0	212.9	by old trenches
21200	2700	28.1	212.9	241.0	0.0	241.0	
21200	2675	21.0	241.0	262.0	0.0	262.0	
21200	2650	7.4	262.0	269.4	0.0	269.4	
21225	2800	-40.0	0.0	-40.0	0.0	-40.0	South side of ditch pile
21250	2800	-42.2	-40.0	-82.2	0.0	-82.2	
21275	2800	-15.8	-82.2	-98.0	0.0	-98.0	
21300	2800	-13.0	-98	-111.0	0.0	-111.0	
21325	2800	58.5	-111	-52.5	0.0	-52.5	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
21350	2800	12.0	-52.5	-40.5	0.0	-40.5	
21375	2800	14.1	-40.5	-26.4	0.0	-26.4	
21400	2800	52.9	-26.4	26.5	0.0	26.5	
21425	2800	-23.9	26.5	2.6	0.0	2.6	
21450	2800	4.1	2.6	6.7	0.0	6.7	
21475	2800	42.0	6.7	48.7	0.0	48.7	oxidizing rocks and grey soil
21400	2775	-103.8	48.7	-103.8	0.0	-103.8	
21400	2750	12.3	-103.8	-91.5	0.0	-91.5	angular black shale in gravel
21400	2725	64.3	-91.5	-27.2	0.0	-27.2	
21400	2700	86.1	-27.2	58.9	0.0	58.9	
21400	2675	18.7	58.9	77.6	0.0	77.6	
21400	2650	81.6	77.6	159.2	0.0	159.2	
21400	2625	-4.5	159.2	154.7	0.0	154.7	
21400	2600	44.2	154.7	198.9	0.0	198.9	
21400	2825	78.2	198.9	78.2	0.0	78.2	
21400	2850	82.2	78.2	160.4	0.0	160.4	
21400	2875	15.9	160.4	176.3	0.0	176.3	on South side of ditch line
Sat Aug 25							
21300	2800	-94.6	-335.4	-430.0	0.0	-430.0	
21400E, 2800N							
21400	2200	352.0	-299.5	52.5	0.0	52.5	cobbly and platy rocks
21400	2225	334.2	-299.5	34.7	0.0	34.7	
21400	2250	328.5	-299.5	29.0	0.0	29.0	
21400	2275	290.0	-299.5	-9.5	0.0	-9.5	
21400	2300	268.8	-299.5	-30.7	0.0	-30.7	
21400	2325	279.6	-299.5	-19.9	0.0	-19.9	muddy and rocky. Side of pit
21400	2350	265.1	-299.5	-34.4	0.0	-34.4	10 feet north from edge of hyd pit
21400	2375	268.5	-299.5	-31.0	0.0	-31.0	
21400	2400	263.5	-299.5	-36.0	0.0	-36.0	
21400	2425	271.6	-299.5	-27.9	0.0	-27.9	
21400	2450	278.9	-299.5	-20.6	0.0	-20.6	12:22pm. fluct ±2mV
21400	2475	258.4	-299.5	-41.1	0.0	-41.1	
21400	2500	263.5	-299.5	-36.0	0.0	-36.0	
21400	2525	250.9	-299.5	-48.6	0.0	-48.6	
21400	2550	224.8	-299.5	-74.7	0.0	-74.7	
21400	2575	219.8	-299.5	-79.7	0.0	-79.7	
21400	2600	208.2	-299.5	-91.3	0.0	-91.3	
21400	2625	161.2	-299.5	-138.3	0.0	-138.3	12:18pm
21400	2650	157.7	-299.5	-141.8	0.0	-141.8	
21400	2675	83.1	-299.5	-216.4	0.0	-216.4	
21400	2700	67.5	-299.5	-232.0	0.0	-232.0	
21400	2725	-28.7	-299.5	-328.2	0.0	-328.2	
21400	2750	-82.7	-299.5	-382.2	0.0	-382.2	
21400	2775	-107.8	-299.5	-407.3	0.0	-407.3	
21400	2800	35.9	-335.4	-299.5	0.0	-299.5	
21400	2825	99.2	-299.5	-200.3	0.0	-200.3	
21400	2850	168.8	-299.5	-130.7	0.0	-130.7	
21400	2875	195.0	-299.5	-104.5	0.0	-104.5	
21400	2900	232.7	-299.5	-66.8	0.0	-66.8	8C01-12/13 drill rods in the ground
21400	2925	221.8	-299.5	-77.7	0.0	-77.7	south side of road
21400	2950	264.0	-299.5	-35.5	0.0	-35.5	north side of road
21400	2975	292.5	-299.5	-8.9	0.0	-8.9	
21400	3000	809.9	-299.5	10.4	0.0	10.4	
21400	3025	296.9	-299.5	-2.6	0.0	-2.6	
21400	3050	322.5	-299.5	23.0	0.0	23.0	
21400	3075	309.9	-299.5	10.4	0.0	10.4	
21400	3100	275.9	-299.5	-23.6	0.0	-23.6	
21400	3125	190.7	-299.5	-108.8	0.0	-108.8	
21400	3150	125.7	-299.5	-173.8	0.0	-173.8	
21400	3175	67.6	-299.5	-231.9	0.0	-231.9	
21400	3200	179.6	-299.5	-119.9	0.0	-119.9	
21400	3225	256.0	-299.5	-43.5	0.0	-43.5	few small fragments of black rock
21400	3250	286.8	-299.5	-12.7	0.0	-12.7	
21400	3275	287.5	-299.5	-12.0	0.0	-12.0	
21400	3300	296.5	-299.5	-3.0	0.0	-3.0	very wet ground
21400	3325	281.7	-299.5	-17.8	0.0	-17.8	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
21400	3350	275.0	-299.5	-24.5	0.0	-24.5	
21400	3375	188.4	-299.5	-110.1	0.0	-110.1	
21400	3400	56.5	-299.5	-243.0	0.0	-243.0	gravel size black rocks in hole
21400	3425	43.5	-299.5	-256.0	0.0	-256.0	
21400	3450	268.8	-299.5	-30.7	0.0	-30.7	still black rocks in hole. fluct ±1mV
21400	3475	307.4	-299.5	7.9	0.0	7.9	fluct ±15mV. 11:26am. Solar Flare?
21400	3500	322.4	-299.5	22.9	0.0	22.9	
21400	3525	319.4	-299.5	19.9	0.0	19.9	
21400	3550	323.5	-299.5	24.0	0.0	24.0	
21400	3575	328.9	-299.5	29.4	0.0	29.4	fluctuating LOTS and quickly ±5mV
21400	3600	315.4	-299.5	15.9	0.0	15.9	11:36am
21500	2800	48.7	-299.5	-250.8	0.0	-250.8	
21600E, 2800N		116.8					
21600	2200	244.3	-182.7	61.6	0.0	61.6	
21600	2225	239.5	-182.7	56.8	0.0	56.8	by creek
21600	2250	247.1	-182.7	64.4	0.0	64.4	
21600	2275	225.3	-182.7	42.6	0.0	42.6	
21600	2300	156.7	-182.7	-26.0	0.0	-26.0	lots of rocks
21600	2325	174.2	-182.7	-8.5	0.0	-8.5	
21600	2350	193.1	-182.7	10.4	0.0	10.4	
21600	2375	195.9	-182.7	13.2	0.0	13.2	
21600	2400	199.7	-182.7	17.0	0.0	17.0	
21600	2425	189.4	-182.7	6.7	0.0	6.7	2:04 PM
21600	2450	182.4	-182.7	-0.3	0.0	-0.3	
21600	2475	165.6	-182.7	-17.1	0.0	-17.1	
21600	2500	154.1	-182.7	-28.6	0.0	-28.6	
21600	2525	141.8	-182.7	-40.9	0.0	-40.9	
21600	2550	136.1	-182.7	-46.6	0.0	-46.6	edge of bank
21600	2575	111.6	-182.7	-71.1	0.0	-71.1	
21600	2600	96.5	-182.7	-86.2	0.0	-86.2	
21600	2625	87.1	-182.7	-95.6	0.0	-95.6	1:56 PM
21600	2650	80.1	-182.7	-102.6	0.0	-102.6	
21600	2675	32.5	-182.7	-150.2	0.0	-150.2	
21600	2700	11.1	-182.7	-171.6	0.0	-171.6	
21600	2725	-7.2	-182.7	-189.9	0.0	-189.9	
21600	2750	0.9	-182.7	-181.8	0.0	-181.8	
21600	2775	17.0	-182.7	-165.7	0.0	-165.7	rocky ground
21600	2800	116.8	-299.5	-182.7	0.0	-182.7	
21600	2825	86.1	-182.7	-96.6	0.0	-96.6	
21600	2850	103.4	-182.7	-79.3	0.0	-79.3	
21600	2875	135.7	-182.7	-47.0	0.0	-47.0	
21600	2900	175.2	-182.7	-7.5	0.0	-7.5	
21600	2925	196.4	-182.7	13.7	0.0	13.7	
21600	2950	222.1	-182.7	39.4	0.0	39.4	
21600	2975	196.1	-182.7	13.4	0.0	13.4	by ditch line
21600	3000	231.5	-182.7	48.8	0.0	48.8	
21600	3025	234.8	-182.7	52.1	0.0	52.1	South side of road
21600	3050	205.3	-182.7	22.6	0.0	22.6	
21600	3075	111.6	-182.7	-71.1	0.0	-71.1	
21600	3100	-87.7	-182.7	-270.4	0.0	-270.4	
21600	3125	-59.1	-182.7	-241.8	0.0	-241.8	black rocks
21600	3150	-81.5	-182.7	-101.2	0.0	-101.2	
21600	3175	117.2	-182.7	-65.5	0.0	-65.5	
21600	3200	154.6	-182.7	-28.1	0.0	-28.1	
21600	3225	184.2	-182.7	1.5	0.0	1.5	
21600	3250	188.8	-182.7	6.1	0.0	6.1	
21600	3275	197.4	-182.7	14.7	0.0	14.7	
21600	3300	203.3	-182.7	20.6	0.0	20.6	1:17 PM
21600	3325	193.0	-182.7	10.3	0.0	10.3	
21600	3350						
21600	3375						
21600	3400	188.1	-182.7	5.4	0.0	5.4	
21600	3425	168.1	-182.7	-14.6	0.0	-14.6	
21600	3450	171.3	-182.7	-11.4	0.0	-11.4	
21600	3475	174.5	-182.7	-8.2	0.0	-8.2	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
21600	3500	152.9	-182.7	-29.9	0.0	-29.9	most northern extent of cutline
21600	3525	135.1	-182.7	-47.6	0.0	-47.6	
21600	3550	179.9	-182.7	-2.8	0.0	-2.8	
21600	3575	185.9	-182.7	3.2	0.0	3.2	
21600	3600	191.7	-182.7	9.0	0.0	9.0	
21700	2800	110.3	-182.7	-72.4	0.0	-72.4	E side of small trench coming off ditch line that runs downhill. Water table is only 1 foot down. Quite wet.
21800E, 2800N		131.7					
21800	2425	53.1	-51.0	2.1	0.0	2.1	
21800	2450	74.2	-51.0	23.2	0.0	23.2	
21800	2475	49.0	-51.0	-2.0	0.0	-2.0	
21800	2500	60.2	-51.0	9.2	0.0	9.2	
21800	2525	21.3	-51.0	-29.7	0.0	-29.7	
21800	2550	28.6	-51.0	-24.4	0.0	-24.4	
21800	2575	12.4	-51.0	-38.6	0.0	-38.6	
21800	2600	11.0	-51.0	-40.0	0.0	-40.0	
21800	2625	-22.4	-51.0	-73.4	0.0	-73.4	
21800	2650	-22.1	-51.0	-73.1	0.0	-73.1	
21800	2675	-54.7	-51.0	-105.7	0.0	-105.7	
21800	2700	-48.8	-51.0	-97.8	0.0	-97.8	
21800	2725	-34.3	-51.0	-85.3	0.0	-85.3	
21800	2750	-4.6	-51.0	-55.6	0.0	-55.6	
21800	2775	-8.4	-51.0	-57.4	0.0	-57.4	
21800	2800	131.7	-182.7	-51.0	0.0	-51.0	marshy
21800	2825	12.2	-51.0	-38.8	0.0	-38.8	
21800	2850	17.4	-51.0	-33.6	0.0	-33.6	
21800	2875	20.6	-51.0	-30.4	0.0	-30.4	
21800	2900	31.8	-51.0	-19.2	0.0	-19.2	
21800	2925	32.8	-51.0	-18.2	0.0	-18.2	
21800	2950	42.5	-51.0	-8.5	0.0	-8.5	
21800	2975	239.2	-51.0	188.2	0.0	188.2	
21800	3000	166.9	-51.0	115.9	0.0	115.9	
21800	3025	92.5	-51.0	41.5	0.0	41.5	
21800	3050	-45.2	-51.0	-96.2	0.0	-96.2	
21800	3075	-145.3	-51.0	-196.3	0.0	-196.3	
21800	3100	-118.7	-51.0	-169.7	0.0	-169.7	by ditch line
21800	3125	97.4	-51.0	46.4	0.0	46.4	
21800	3150	154.6	-51.0	103.6	0.0	103.6	North side of road
21800	3175	-107.1	-51.0	-158.1	0.0	-158.1	
21800	3200	-2.7	-51.0	-53.7	0.0	-53.7	Argillite rocks again
21800	3225	40.4	-51.0	-10.6	0.0	-10.6	
21800	3250	65.7	-51.0	14.7	0.0	14.7	
21800	3275	33.3	-51.0	-17.7	0.0	-17.7	
21800	3300	78.7	-51.0	27.7	0.0	27.7	
21800	3325	67.6	-51.0	16.6	0.0	16.6	
21800	3350	72.9	-51.0	21.9	0.0	21.9	
21800	3375	71.1	-51.0	20.1	0.0	20.1	
21800	3400	81.6	-51.0	30.6	0.0	30.6	
21800	3425	84.8	-51.0	33.8	0.0	33.8	
21800	3450	90.8	-51.0	39.6	0.0	39.6	
21800	3475	79.6	-51.0	28.6	0.0	28.6	
21800	3500	-86.6	-51.0	-35.6	0.0	-35.6	
21800	3525	75.5	-51.0	24.5	0.0	24.5	
21800	3550	57.6	-51.0	6.6	0.0	6.6	
21800	3575	54.2	-51.0	3.2	0.0	3.2	
21800	3600	226.4	-51.0	175.4	0.0	175.4	
21800	3625	194.2	-51.0	143.2	0.0	143.2	
21900	2800	8.6	-51.0	-42.4	0.0	-42.4	
22000E, 2800N		10.2					
22000	2550	1.8	-40.8	-39.1	0.0	-39.1	top of cliff. Fluct ±4mV
22000	2575	-25.5	-40.8	-66.3	0.0	-66.3	
22000	2600	-34.8	-40.8	-75.6	0.0	-75.6	
22000	2625	-63.5	-40.8	-104.3	0.0	-104.3	
22000	2650	-69.0	-40.8	-109.8	0.0	-109.8	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
22000	2675	-86.1	-40.8	-126.9	0.0	-126.9	
22000	2700	-81.5	-40.8	-122.4	0.0	-122.4	
22000	2725	-71.0	-40.8	-111.8	0.0	-111.8	
22000	2750	-43.8	-40.8	-84.6	0.0	-84.6	
22000	2775	-14.3	-40.8	-55.1	0.0	-55.1	
22000	2800	10.2	-51.0	-40.8	0.0	-40.8	
22100	2800	0.5	-51.0	-50.5	0.0	-50.5	
22200	2800	22.1	-40.8	-18.7	0.0	-18.7	
22300	2800	60.4	-40.8	19.6	0.0	19.6	
22400	2800	88.8	-40.8	48.0	0.0	48.0	
22500	2800	110.1	-40.8	69.3	0.0	69.3	
22200e, 2800n							
22200	2675	-58.5	-18.7	-77.2	0.0	-77.2	
22200	2700	-38.7	-18.7	-57.4	0.0	-57.4	
22200	2725	-32.0	-18.7	-50.7	0.0	-50.7	
22200	2750	-17.2	-18.7	-35.9	0.0	-35.9	
22200	2775	9.5	-18.7	-9.2	0.0	-9.2	
22200	2800	22.1	-40.8	-18.7	0.0	-18.7	
22200	2825	32.7	-18.7	14.0	0.0	14.0	
22200	2850	62.8	-18.7	44.1	0.0	44.1	
22200	2875	53.5	-18.7	34.8	0.0	34.8	
22200	2900	74.7	-18.7	56.0	0.0	56.0	
22200	2925	60.5	-18.7	41.8	0.0	41.8	
22200	2950	72.1	-18.7	53.4	0.0	53.4	
22200	2975	77.4	-18.7	58.7	0.0	58.7	
22200	3000	71.7	-18.7	53.0	0.0	53.0	
22200	3025	88.0	-18.7	69.3	0.0	69.3	
22200	3050	93.7	-18.7	75.0	0.0	75.0	
22200	3075	80.9	-18.7	62.2	0.0	62.2	
22200	3100	87.1	-18.7	68.4	0.0	68.4	
22200	3125	80.8	-18.7	62.1	0.0	62.1	
22200	3150	108.6	-18.7	89.9	0.0	89.9	
22200	3175	219.0	-18.7	200.3	0.0	200.3	
22200	3200	180.7	-18.7	162.0	0.0	162.0	
22200	3225	78.6	-18.7	59.9	0.0	59.9	
22200	3250	197.0	-18.7	178.3	0.0	178.3	
22200	3275	165.9	-18.7	147.2	0.0	147.2	
22200	3300	168.7	-18.7	150.0	0.0	150.0	
Tues Aug 28							
22100	2775	10.7	-50.5	-39.8	0.0	-39.8	
22100	2750	-43.3	-39.8	-83.1	0.0	-83.1	
22100	2725	-15.6	-83.1	-98.7	0.0	-98.7	
22100	2700	-24.5	-98.7	-123.2	0.0	-123.2	
22100	2675	21.7	-123.2	-101.5	0.0	-101.5	
22100	2650	5.1	-101.5	-96.4	0.0	-96.4	took an average of 2 measurements taken in 2 separate holes spaced 1 foot away from each other. Ground not good here.
22100	2625	16.9	-96.4	-79.5	0.0	-79.5	edge of pit
21900	2775	-32.5	-42.4	-74.9	0.0	-74.9	
21900	2750	53.7	-74.9	-21.2	0.0	-21.2	
21900	2725	13.2	-21.2	-8.0	0.0	-8.0	
21900	2700	-8.8	-8	-16.8	0.0	-16.8	
21900	2675	10.5	-16.8	-6.3	0.0	-6.3	crossed a small stream
21900	2650	7.7	-6.3	1.4	0.0	1.4	grey soil with rusty/oxidized patches
21900	2625	47.0	1.4	48.4	0.0	48.4	40% gravel in grey clay
21900	2600	-6.1	48.4	42.3	0.0	42.3	no good contact with B-horizon
21700	2775	5.8	-72.4	-66.6	0.0	-66.6	east side of slough
21700	2750	-37.9	-66.6	-104.5	0.0	-104.5	
21700	2725	5.8	-104.5	-98.9	0.0	-98.9	wet, mossy, bareish hillside, gravel soil. Possibly OLD overgrown pile of gravel from
21700	2700	15.9	-98.9	-83.0	0.0	-83.0	exploration in years past
21700	2675	9.4	-83.0	-73.6	0.0	-73.6	Gravel hill covered in <2inch thick moss and ,40 year old trees
21700	2650	0.5	-73.6	-73.1	0.0	-73.1	Gravel hill covered in <2inch thick moss and ,40 year old trees
21700	2625	8.5	-73.1	-64.6	0.0	-64.6	Gravel hill covered in <2inch thick moss and ,40 year old trees

CONTROL STATION

aug30, 2001: leap frog method

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
21700	2600	-18.6	-84.8	-83.2	0.0	-83.2	
21700	2575	36.4	-83.2	-46.8	0.0	-46.8	
21225	2150	11.9	39.8	51.5	0.0	51.5	
21250	2145	-12.4	51.5	39.1	0.0	39.1	
21273	2138	18.7	39.1	57.8	0.0	57.8	
21298	2127	-16.6	57.8	41.2	0.0	41.2	
21324	2119	5.1	41.2	48.3	0.0	48.3	
21347	2111	-2.3	48.3	44.0	0.0	44.0	
21372	2102	23.3	44.0	67.3	0.0	67.3	
21400	2092	17.7	67.3	85.0	0.0	85.0	
		17.5	85.0	102.5	0.0	102.5	
		-16.0	102.5	86.5	0.0	86.5	
		4.3	86.5	90.8	0.0	90.8	
		-7.1	90.8	83.7	0.0	83.7	
		17.6	83.7	101.3	0.0	101.3	
21535	2103	-16.4	101.3	84.9	0.0	84.9	
		20.0	84.9	104.9	0.0	104.9	
		-17.7	104.9	87.2	0.0	87.2	
21588	2125	11.1	87.2	98.3	0.0	98.3	
21622	2125	-7.9	98.3	90.4	0.0	90.4	
21652	2125	10.8	90.4	101.2	0.0	101.2	
21685	2123	-15.0	101.2	86.2	0.0	86.2	
		12.7	86.2	98.9	0.0	98.9	
21750	2120	-7.0	98.9	91.9	0.0	91.9	
21780	2120	11.1	91.9	103.0	0.0	103.0	
21808	2121	-14.2	103.0	88.8	0.0	88.8	
21832	2122	3.5	88.8	92.3	0.0	92.3	
		-8.0	92.3	84.3	0.0	84.3	
		8.6	84.3	92.9	0.0	92.9	
		-13.7	92.9	79.2	0.0	79.2	
19775	2325	-3.5	-111.6	-115.1	0.0	-115.1	
19750	2314	-9.0	-115.1	-124.1	0.0	-124.1	
19725	2312	-3.8	-124.1	-127.9	0.0	-127.9	
19695	2300	-28.5	-127.9	-156.4	0.0	-156.4	
19670	2292	0.6	-156.4	-155.9	0.0	-155.9	
19637	2287	-2.3	-155.9	-158.2	0.0	-158.2	
19610	2280	32.5	-158.2	-125.7	0.0	-125.7	
19591	2275	17.4	-125.7	-108.3	0.0	-108.3	
		29.5	-108.3	-78.8	0.0	-78.8	
		10.5	-78.8	-68.3	0.0	-68.3	
19509	2250	12.0	-68.3	-56.3	0.0	-56.3	
		5.1	-56.3	-51.2	0.0	-51.2	
		12.8	-51.2	-38.4	0.0	-38.4	
		6.2	-38.4	-30.2	0.0	-30.2	
19410	2225	12.0	-30.2	-18.2	0.0	-18.2	
		13.3	-18.2	-4.9	0.0	-4.9	
19358	2213	3.7	-4.9	-1.2	0.0	-1.2	
		-0.3	-1.2	-1.5	0.0	-1.5	
19300	2193	6.9	-1.5	5.4	0.0	5.4	At BC01-13. Very wet area
19275	2185	-2.1	5.4	3.3	0.0	3.3	
		-0.7	3.3	2.6	0.0	2.6	
		-16.1	2.6	-13.5	0.0	-13.5	
19190	2170	-5.4	-13.5	-18.9	0.0	-18.9	
		0.0					
19700	2400	-124.5	-4.0	-128.5	0.0	-128.5	
19700	2425	-149.4	-4.0	-153.4	0.0	-153.4	
19700	2450	-157.9	-4.0	-161.9	0.0	-161.9	
19700	2475	-210.2	-4.0	-214.2	0.0	-214.2	
19700	2500	-226.0	-4.0	-230.0	0.0	-230.0	
19700	2520	-231.2	-4.0	-235.2	0.0	-235.2	
19700	2540	-182.7	-4.0	-186.7	0.0	-186.7	
19700	2560	-213.5	-4.0	-217.5	0.0	-217.5	
19700	2580	-188.7	-4.0	-192.7	0.0	-192.7	
19700	2600	-186.0	-4.0	-190.0	0.0	-190.0	North side of road

SEPT 1, 2001 regular method
19700E, 2800N

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
19700	2617	-223.4	-4.0	-227.4	0.0	-227.4	
19700	2634	-323.1	-4.0	-327.1	0.0	-327.1	road located 50 feet to south
19700	2651	-467.0	-4.0	-461.0	0.0	-461.0	BC Vein
19700	2668	-528.0	-4.0	-532.0	0.0	-532.0	BC Vein
19700	2685	-417.0	-4.0	-421.0	0.0	-421.0	BC Vein?
19700	2700	-317.3	-4.0	-321.3	0.0	-321.3	near end of new road
19700	2725	-261.2	-4.0	-265.2	0.0	-265.2	
19700	2750	-140.7	-4.0	-144.7	0.0	-144.7	
19700	2775	-35.9	-4.0	-39.9	0.0	-39.9	
19700	2800	0.0		-4.0	0.0	-4.0	
19700	2825	2.7	-4.0	-1.3	0.0	-1.3	
19700	2850	-17.4	-4.0	-21.4	0.0	-21.4	
19700	2875	-27.8	-4.0	-31.8	0.0	-31.8	
19700	2900	-73.6	-4.0	-77.6	0.0	-77.6	
19700	2925	-355.3	-4.0	-359.3	0.0	-359.3	
19700	2950	-726.0	-4.0	-730.0	0.0	-730.0	
19700	2975	-232.7	-4.0	-236.7	0.0	-236.7	
19700	3000	-154.6	-4.0	-158.6	0.0	-158.6	
19700	3025	-104.3	-4.0	-108.3	0.0	-108.3	
19700	3050	-52.5	-4.0	-56.5	0.0	-56.5	
19700	3075	-131.9	-4.0	-135.9	0.0	-135.9	
19700	3100	-517.0	-4.0	-521.0	0.0	-521.0	
19700	3125	-600.0	-4.0	-604.0	0.0	-604.0	
19700	3150	-470.0	-4.0	-474.0	0.0	-474.0	
19700	3175	-589.0	-4.0	-593.0	0.0	-593.0	
19700	3200	-488.0	-4.0	-492.0	0.0	-492.0	
19700	3225	-115.4	-4.0	-119.4	0.0	-119.4	
19700	3250	-80.7	-4.0	-84.7	0.0	-84.7	
19700	3275	-50.3	-4.0	-54.3	0.0	-54.3	
19700	3300	-95.5	-4.0	-99.5	0.0	-99.5	
19594E, 2800N							
		-1.1					
19600	2025	23.6	-5.1	18.5	0.0	18.5	edge of hydraulicked pit
19600	2050	19.2	-5.1	14.1	0.0	14.1	
19600	2075	13.7	-5.1	8.6	0.0	8.6	
19600	2100	23.5	-5.1	18.4	0.0	18.4	
19600	2125	3.2	-5.1	-1.9	0.0	-1.9	fluct±4mV
19600	2150	5.1	-5.1	0.0	0.0	0.0	
19600	2175	-9.5	-5.1	-14.6	0.0	-14.6	
19600	2200	-9.1	-5.1	-14.2	0.0	-14.2	
19600	2225	-44.9	-5.1	-50.0	0.0	-50.0	
19600	2250	-69.1	-5.1	-74.2	0.0	-74.2	
19600	2275	-108.6	-5.1	-113.7	0.0	-113.7	
19600	2300	-125.2	-5.1	-130.3	0.0	-130.3	North side of road
19600	2325	-122.8	-5.1	-127.9	0.0	-127.9	
19600	2350	-105.7	-5.1	-110.8	0.0	-110.8	
19600	2375	-99.7	-5.1	-104.8	0.0	-104.8	
19600	2400	-90.4	-5.1	-95.5	0.0	-95.5	
19600	2425	-111.1	-5.1	-116.2	0.0	-116.2	
19600	2450	-117.9	-5.1	-123.0	0.0	-123.0	
19600	2475	-159.4	-5.1	-164.5	0.0	-164.5	
19600	2500	-167.7	-5.1	-172.8	0.0	-172.8	
19600	2525	-156.6	-5.1	-161.7	0.0	-161.7	
19600	2550	-105.9	-5.1	-111.0	0.0	-111.0	
19600	2575	-117.6	-5.1	-122.7	0.0	-122.7	
19600	2600	-156.7	-5.1	-161.8	0.0	-161.8	
19600	2625	-222.8	-5.1	-227.7	0.0	-227.7	
19600	2650	-312.6	-5.1	-317.7	0.0	-317.7	
19600	2675	-450.0	-5.1	-455.1	0.0	-455.1	
19600	2700	-384.4	-5.1	-389.5	0.0	-389.5	
19600	2725	-321.5	-5.1	-326.6	0.0	-326.6	
19600	2750	-278.8	-5.1	-283.9	0.0	-283.9	
19600	2775	-54.2	-5.1	-59.3	0.0	-59.3	
19594	2800	-1.1	-4.0	-5.1	0.0	-5.1	
19600	2825	1.1	-5.1	-4.0	0.0	-4.0	
19600	2850	-25.8	-5.1	-30.9	0.0	-30.9	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
19600	2875	-58.0	-5.1	-63.1	0.0	-63.1	
19600	2900	-304.4	-5.1	-309.5	0.0	-309.5	
19600	2925	-180.2	-5.1	-185.3	0.0	-185.3	
19600	2950	-301.2	-5.1	-306.3	0.0	-306.3	
19600	2975	-177.7	-5.1	-182.8	0.0	-182.8	
19600	3000	-22.9	-5.1	-28.0	0.0	-28.0	
19600	3025	-24.4	-5.1	-29.5	0.0	-29.5	
19600	3050	-37.2	-5.1	-42.3	0.0	-42.3	
19600	3075	-120.8	-5.1	-125.9	0.0	-125.9	
19600	3100	-231.3	-5.1	-236.4	0.0	-236.4	
19600	3125	-341.5	-5.1	-346.6	0.0	-346.6	
19600	3150	-809.0	-5.1	-814.1	0.0	-814.1	
19600	3175	-260.5	-5.1	-265.6	0.0	-265.6	
19600	3200	-109.8	-5.1	-114.9	0.0	-114.9	
19600	3225	-44.9	-5.1	-50.0	0.0	-50.0	
19600	3250	-48.0	-5.1	-53.1	0.0	-53.1	
19600	3275	-152.8	-5.1	-157.9	0.0	-157.9	
19600	3300	-696.0	-5.1	-701.1	0.0	-701.1	
19600	3325	-635.0	-5.1	-640.1	0.0	-640.1	
19600	3350	-738.0	-5.1	-743.1	0.0	-743.1	
19600	3375	-739.0	-5.1	-744.1	0.0	-744.1	
19600	3400	-628.0	-5.1	-633.1	0.0	-633.1	at the road... also 4+50E 60N (Newmont/Goldcity grid??)
19600	3425	-423.0	-5.1	-428.1	0.0	-428.1	
19600	3450	-139.9	-5.1	-144.0	0.0	-144.0	
19600	3475	-40.9	-5.1	-46.0	0.0	-46.0	
19600	3500	-18.7	-5.1	-23.8	0.0	-23.8	
19600	3525	-0.9	-5.1	-6.0	0.0	-6.0	
19600	3550	15.0	-5.1	9.9	0.0	9.9	
19600	3575	31.9	-5.1	26.8	0.0	26.8	
19600	3600	34.2	-5.1	29.1	0.0	29.1	
19500	2800	-50.3	-5.1	-55.4	0.0	-55.4	
19400E, 2800E							
19400	2000	-73.4	-78.5	36.4	0.0	36.4	
19400	2025	112.9	-78.5	44.5	0.0	44.5	
19400	2050	121.0	-78.5	51.4	0.0	51.4	
19400	2075	127.9	-78.5	45.6	0.0	45.6	
19400	2100	122.1	-78.5	37.5	0.0	37.5	
19400	2125	114.0	-78.5	19.6	0.0	19.6	5 feet away is old rusty hyd pipe
19400	2150	96.3	-78.5	15.9	0.0	15.9	
19400	2175	92.4	-78.5	8.3	0.0	8.3	
19400	2200	84.8	-78.5	8.9	0.0	8.9	
19400	2225	83.4	-78.5	6.4	0.0	6.4	
19400	2250	84.9	-78.5	-5.2	0.0	-5.2	north side of road
19400	2275	73.3	-78.5	-32.8	0.0	-32.8	
19400	2300	45.7	-78.5	-20.6	0.0	-20.6	
19400	2325	57.9	-78.5	-47.0	0.0	-47.0	
19400	2350	31.5	-78.5	-43.4	0.0	-43.4	
19400	2375	35.1	-78.5	-99.4	0.0	-99.4	
19400	2400	-20.9	-78.5	-83.5	0.0	-83.5	
19400	2425	-5.0	-78.5	-165.8	0.0	-165.8	
19400	2450	-87.3	-78.5	-158.9	0.0	-158.9	
19400	2475	-80.4	-78.5	-234.6	0.0	-234.6	
19400	2500	-156.1	-78.5	-276.0	0.0	-276.0	
19400	2525	-197.5	-78.5	-315.9	0.0	-315.9	
19400	2550	-237.4	-78.5	-268.5	0.0	-268.5	
19400	2575	-190.0	-78.5	-291.3	0.0	-291.3	
19400	2600	-212.8	-78.5	-336.4	0.0	-336.4	
19400	2625	-257.9	-78.5	-448.9	0.0	-448.9	South side of road. Old drill location
19400	2650	-370.4	-78.5	-631.5	0.0	-631.5	
19400	2700	-553.0	-78.5	-728.5	0.0	-728.5	no station... quartz subcrop
19400	2725	-850.0	-78.5	-782.5	0.0	-782.5	by BC Vein outcrop
19400	2750	-884.0	-78.5	-578.5	0.0	-578.5	8 feet north of BC Vein outcrop
19400	2775	-500.0	-78.5	-222.6	0.0	-222.6	75 feet north of BC Vein outcrop
19400	2800	-144.1	-5.1	-78.5	0.0	-78.5	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
19400	2825	16.4	-78.5	-62.1	0.0	-62.1	
19400	2850	21.5	-78.5	-57.0	0.0	-57.0	
19400	2875	-21.3	-78.5	-99.8	0.0	-99.8	
19400	2900	-211.7	-78.5	-290.2	0.0	-290.2	
19400	2925	-216.3	-78.5	-294.8	0.0	-294.8	
19400	2950	-251.8	-78.5	-330.3	0.0	-330.3	
19400	2975	-94.0	-78.5	-172.5	0.0	-172.5	
19400	3000	48.7	-78.5	-29.8	0.0	-29.8	
19400	3025	32.0	-78.5	-46.5	0.0	-46.5	
19400	3050	6.7	-78.5	-71.8	0.0	-71.8	
19400	3075	10.4	-78.5	-68.1	0.0	-68.1	south side of road
19400	3100	50.0	-78.5	-28.5	0.0	-28.5	
19400	3125	37.2	-78.5	-41.3	0.0	-41.3	
19400	3150	71.6	-78.5	-6.9	0.0	-6.9	
19400	3175	63.3	-78.5	-15.2	0.0	-15.2	
19400	3200	72.5	-78.5	-6.0	0.0	-6.0	
19400	3225	59.0	-78.5	-19.5	0.0	-19.5	
19400	3250	27.0	-78.5	-51.5	0.0	-51.5	
19400	3275	-205.9	-78.5	-284.4	0.0	-284.4	
19400	3300	-655.0	-78.5	-733.5	0.0	-733.5	
19400	3325	-704.0	-78.5	-782.5	0.0	-782.5	
19400	3350	-630.0	-78.5	-708.5	0.0	-708.5	
19400	3375	-377.3	-78.5	-455.8	0.0	-455.8	
19400	3400	-167.5	-78.5	-246.0	0.0	-246.0	
19400	3425	-18.8	-78.5	-87.3	0.0	-87.3	
19400	3450	-26.2	-78.5	-104.7	0.0	-104.7	
19400	3475	61.7	-78.5	-16.8	0.0	-16.8	
19400	3500	89.3	-78.5	10.8	0.0	10.8	
19400	3525	92.1	-78.5	13.6	0.0	13.6	
19400	3550	119.9	-78.5	41.4	0.0	41.4	LMST unit???
19400	3575	118.1	-78.5	39.6	0.0	39.6	LMST unit???
19400	3600	127.6	-78.5	49.1	0.0	49.1	
19300	2800	-90.7	-78.5	-189.2	0.0	-189.2	
19200E, 2800N		-105.9					
19200	2100	199.2	-184.4	14.8	0.0	14.8	
19200	2125	178.8	-184.4	-5.6	0.0	-5.6	
19200	2150	175.8	-184.4	-8.6	0.0	-8.6	
19200	2175	184.2	-184.4	-0.2	0.0	-0.2	
19200	2200	164.1	-184.4	-20.3	0.0	-20.3	
19200	2225	183.2	-184.4	-21.2	0.0	-21.2	
19200	2250	145.9	-184.4	-38.5	0.0	-38.5	
19200	2275	131.6	-184.4	-52.8	0.0	-52.8	
19200	2300	107.8	-184.4	-76.6	0.0	-76.6	
19200	2325	47.4	-184.4	-137.0	0.0	-137.0	
19200	2350	-3.3	-184.4	-187.7	0.0	-187.7	
19200	2375	-57.3	-184.4	-241.7	0.0	-241.7	
19200	2400	-70.1	-184.4	-254.5	0.0	-254.5	
19200	2425	-71.1	-184.4	-255.5	0.0	-255.5	
19200	2450	2.6	-184.4	-181.8	0.0	-181.8	
19200	2475	5.8	-184.4	-178.6	0.0	-178.6	
19200	2500	14.5	-184.4	-169.9	0.0	-169.9	
19200	2525	42.2	-184.4	-226.6	0.0	-226.6	
19200	2550	-104.2	-184.4	-288.6	0.0	-288.6	
19200	2575	-353.3	-184.4	-537.7	0.0	-537.7	
19200	2600	-555.0	-184.4	-739.4	0.0	-739.4	
19200	2625	-619.0	-184.4	-803.4	0.0	-803.4	
19200	2650	-583.0	-184.4	-767.4	0.0	-767.4	
19200	2675	-574.0	-184.4	-758.4	0.0	-758.4	
19200	2700	-558.0	-184.4	-742.4	0.0	-742.4	
19200	2725	-525.0	-184.4	-709.4	0.0	-709.4	
19200	2763	-350.4	-184.4	-534.8	0.0	-534.8	
19200	2775	-97.9	-184.4	-282.3	0.0	-282.3	
19200	2800	-105.9	-78.5	-184.4	0.0	-184.4	west side of road
19200	2825	43.2	-184.4	-141.2	0.0	-141.2	
19200	2850	41.7	-184.4	-142.7	0.0	-142.7	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
19200	2875	-281.4	-184.4	-465.8	0.0	-465.8	
19200	2900	-439.0	-184.4	-623.4	0.0	-623.4	
19200	2925	-465.0	-184.4	-649.4	0.0	-649.4	
19200	2950	-359.2	-184.4	-543.6	0.0	-543.6	
19200	2975	-349.3	-184.4	-533.7	0.0	-533.7	
19200	3000	-139.3	-184.4	-323.7	0.0	-323.7	
19200	3025	-113.4	-184.4	-297.8	0.0	-297.8	
19200	3050	37.2	-184.4	-147.2	0.0	-147.2	
19200	3075	36.2	-184.4	-148.2	0.0	-148.2	
19200	3100	57.0	-184.4	-127.4	0.0	-127.4	
19200	3125	130.4	-184.4	-54.0	0.0	-54.0	
19200	3150	14.9	-184.4	-169.5	0.0	-169.5	
19200	3175	166.0	-184.4	-18.4	0.0	-18.4	
19200	3200	150.4	-184.4	-34.0	0.0	-34.0	
19200	3225	110.8	-184.4	-73.6	0.0	-73.6	
19200	3250	-162.2	-184.4	-346.6	0.0	-346.6	
19200	3275	-597.0	-184.4	-781.4	0.0	-781.4	
19200	3300	-847.0	-184.4	-831.4	0.0	-831.4	last most northern picket on cutline
19200	3325	-557.0	-184.4	-741.4	0.0	-741.4	
19200	3350	-277.5	-184.4	-461.9	0.0	-461.9	
19200	3375	-60.2	-184.4	-244.6	0.0	-244.6	
19200	3400	35.2	-184.4	-149.2	0.0	-149.2	
19200	3425	108.6	-184.4	-75.8	0.0	-75.8	
19200	3450	156.2	-184.4	-28.2	0.0	-28.2	
19200	3475	190.5	-184.4	5.1	0.0	5.1	
19200	3500	199.7	-184.4	15.3	0.0	15.3	
19200	3525	213.3	-184.4	28.9	0.0	28.9	northern extent of cutline
19200	3550	225.5	-184.4	41.1	0.0	41.1	
19200	3575	225.9	-184.4	41.5	0.0	41.5	
19200	3600	236.2	-184.4	51.8	0.0	51.8	
19100	2800	44.9	-184.4	-139.5	0.0	-139.5	
Sun Sept 2 19000E,2800N							
19000	2100	79.0					
19000	2125	65.4	-105.4	-40.0	0.0	-40.0	edge of pit
19000	2150	44.6	-105.4	-60.9	0.0	-60.9	
19000	2175	51.2	-105.4	-54.2	0.0	-54.2	
19000	2200	2.3	-105.4	-103.1	0.0	-103.1	
19000	2225	-7.7	-105.4	-113.1	0.0	-113.1	on ditch line road
19000	2250	-56.7	-105.4	-162.1	0.0	-162.1	
19000	2275	-88.2	-105.4	-193.6	0.0	-193.6	
19000	2300	-254.5	-105.4	-359.9	0.0	-359.9	
19000	2325	-383.0	-105.4	-488.4	0.0	-488.4	
19000	2350	-504.0	-105.4	-609.4	0.0	-609.4	
19000	2375	-466.0	-105.4	-571.4	0.0	-571.4	to side of an old depression
19000	2400	-362.5	-105.4	-467.9	0.0	-467.9	
19000	2425	-194.9	-105.4	-300.3	0.0	-300.3	
19000	2450	-169.8	-105.4	-275.2	0.0	-275.2	
19000	2475	-212.0	-105.4	-317.4	0.0	-317.4	
19000	2500	-249.3	-105.4	-354.7	0.0	-354.7	
19000	2525	-285.1	-105.4	-390.5	0.0	-390.5	
19000	2550	-462.0	-105.4	-567.4	0.0	-567.4	
19000	2575	-614.0	-105.4	-719.4	0.0	-719.4	
19000	2600	-650.0	-105.4	-755.4	0.0	-755.4	
19000	2625	-596.0	-105.4	-701.4	0.0	-701.4	
19000	2650	-662.0	-105.4	-767.4	0.0	-767.4	
19000	2675	-606.0	-105.4	-711.4	0.0	-711.4	
19000	2700	-497.0	-105.4	-602.4	0.0	-602.4	
19000	2725	-422.0	-105.4	-527.4	0.0	-527.4	South side of road
19000	2750	-459.0	-105.4	-564.4	0.0	-564.4	
19000	2775	-447.0	-105.4	-552.4	0.0	-552.4	good valid reading. South side of road
19000	2800	-115.2	-105.4	-220.6	0.0	-220.6	north side of road
19000	2825	79.0	-184.4	-105.4	0.0	-105.4	
19000	2850	-7.2	-105.4	-112.6	0.0	-112.6	
19000	2875	-47.1	-105.4	-152.5	0.0	-152.5	
19000	2900	-174.4	-105.4	-279.8	0.0	-279.8	
19000	2925	-393.4	-105.4	-498.8	0.0	-498.8	changed multimeter battery and rechecked reading. No change

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
19000	2925	-379.6	-105.4	-485.0	0.0	-485.0	
19000	2950	-460.0	-105.4	-565.4	0.0	-565.4	
19000	2975	-313.9	-105.4	-419.3	0.0	-419.3	
19000	3000	-173.2	-105.4	-278.6	0.0	-278.6	
19000	3025	-231.6	-105.4	-337.0	0.0	-337.0	
19000	3050	-197.8	-105.4	-303.2	0.0	-303.2	
19000	3075	17.5	-105.4	-87.9	0.0	-87.9	
19000	3100	58.1	-105.4	-46.3	0.0	-46.3	
19000	3125	37.5	-105.4	-67.9	0.0	-67.9	
19000	3150	20.9	-105.4	-84.5	0.0	-84.5	on old road
19000	3175	3.1	-105.4	-102.3	0.0	-102.3	
19000	3200	-28.5	-105.4	-133.9	0.0	-133.9	
19000	3225	-52.6	-105.4	-158.0	0.0	-158.0	
19000	3250	-49.2	-105.4	-154.6	0.0	-154.6	
19000	3275	-578.0	-105.4	-683.4	0.0	-683.4	argillite zone?
19000	3300	-485.0	-105.4	-590.4	0.0	-590.4	argillite zone?
19000	3325	-188.4	-105.4	-293.8	0.0	-293.8	
19000	3350	22.3	-105.4	-83.1	0.0	-83.1	
19000	3375	61.1	-105.4	-44.3	0.0	-44.3	
19000	3400	80.8	-105.4	-24.6	0.0	-24.6	cut line ends
19000	3425	97.6	-105.4	-7.8	0.0	-7.8	
19000	3450	86.5	-105.4	-18.9	0.0	-18.9	
19000	3475	115.2	-105.4	9.8	0.0	9.8	
19000	3500	117.9	-105.4	12.5	0.0	12.5	
18900	2800	-58.9	-105.4	-164.3	0.0	-164.3	
18800	2150	166.2	-310.9	-144.7	0.0	-144.7	by piled up mag. phyllite
18800	2175	188.5	-310.9	-122.4	0.0	-122.4	
18800	2200	131.4	-310.9	-179.5	0.0	-179.5	
18800	2225	84.1	-310.9	-226.8	0.0	-226.8	North side of road
18800	2250	-81.8	-310.9	-392.7	0.0	-392.7	disturbed ground
18800	2275	-373.2	-310.9	-684.1	0.0	-684.1	
18800	2300	-353.9	-310.9	-664.8	0.0	-664.8	
18800	2325	-365.1	-310.9	-676	0.0	-676	
18800	2350	-245.3	-310.9	-558.2	0.0	-558.2	
18800	2375	-169.1	-310.9	-480	0.0	-480	
18800	2400	-229	-310.9	-539.9	0.0	-539.9	
18800	2425	-275.8	-310.9	-586.7	0.0	-586.7	
18800	2450	-33.2	-310.9	-344.1	0.0	-344.1	
18800	2525	-299.8	-310.9	-610.7	0.0	-610.7	cobble and boulder sized tailings. No station
18800	2550	-437	-310.9	-747.9	0.0	-747.9	cobble and boulder sized tailings No station
18800	2575	-425	-310.9	-735.9	0.0	-735.9	south side of BC shaft tailings dump
18800	2600	-443	-310.9	-753.9	0.0	-753.9	
18800	2625	-413	-310.9	-723.9	0.0	-723.9	
18800	2650	-408	-310.9	-718.9	0.0	-718.9	
18800	2675	-442	-310.9	-752.9	0.0	-752.9	NE side of BC shaft dump
18800	2700	-476	-310.9	-786.9	0.0	-786.9	south side of road
18800	2740	-429	-310.9	-739.9	0.0	-739.9	10 feet south of BC vein outcrop
18800	2763	-206.6	-310.9	-517.5	0.0	-517.5	
18800	2775	-22.9	-310.9	-333.8	0.0	-333.8	
18800	2800	-205.5	-105.4	-310.9	0.0	-310.9	North of BC Shaft and Vein
18800	2825	-2.1	-310.9	-313	0.0	-313	
18800	2850	-54.1	-310.9	-365	0.0	-365	
18800	2875	-62.1	-310.9	-373	0.0	-373	
18800	2900	-195	-310.9	-505.9	0.0	-505.9	
18800	2925	-231.1	-310.9	-542	0.0	-542	SW corner of old cabin
18800	2950	-277.3	-310.9	-588.2	0.0	-588.2	NW corner of old cabin
18800	2975	-288	-310.9	-598.9	0.0	-598.9	
18800	3000	-293.5	-310.9	-604.4	0.0	-604.4	
18800	3025	-325.2	-310.9	-636.1	0.0	-636.1	
18800	3050	-132.5	-310.9	-443.4	0.0	-443.4	
18800	3075	9.5	-310.9	-301.4	0.0	-301.4	
18800	3100	182.8	-310.9	-128.1	0.0	-128.1	
18800	3125	221	-310.9	-89.9	0.0	-89.9	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
18800	3150	281.5	-310.9	-29.4	0.0	-29.4	
18800	3175	292.3	-310.9	-18.6	0.0	-18.6	
18800	3200	294.3	-310.9	-16.6	0.0	-16.6	
18800	3225	272.3	-310.9	-38.6	0.0	-38.6	
18800	3250	38	-310.9	-272.9	0.0	-272.9	
18800	3275	-328.9	-310.9	-639.8	0.0	-639.8	
18800	3300	-268.4	-310.9	-579.3	0.0	-579.3	
18800	3325	-82.9	-310.9	-393.8	0.0	-393.8	
18800	3350	72.6	-310.9	-238.3	0.0	-238.3	
18800	3375	185.1	-310.9	-125.8	0.0	-125.8	
18800	3400	234.5	-310.9	-76.4	0.0	-76.4	end of cutline
18800	3425	252.8	-310.9	-58.1	0.0	-58.1	
18800	3450	282.8	-310.9	-28.1	0.0	-28.1	
18800	3475	269.4	-310.9	-41.5	0.0	-41.5	
18800	3500	294.7	-310.9	-16.2	0.0	-16.2	
18700	2800	150.2	-310.9	-160.7	0.0	-160.7	
18600	2050	62.2	-91.2	-29	0.0	-29	edge of pit. Fluctuating slightly
18600	2075	32.7	-91.2	-58.5	0.0	-58.5	Fluctuating slightly
18600	2100	31.9	-91.2	-59.3	0.0	-59.3	
18600	2125	3.7	-91.2	-87.5	0.0	-87.5	
18600	2150	-19.6	-91.2	-110.8	0.0	-110.8	south side of road. Fluctuating
18600	2175	-91.9	-91.2	-183.1	0.0	-183.1	
18600	2200	-219.3	-91.2	-310.5	0.0	-310.5	
18600	2225	-461	-91.2	-552.2	0.0	-552.2	
18600	2250	-559	-91.2	-650.2	0.0	-650.2	
18600	2275	-482	-91.2	-573.2	0.0	-573.2	
18600	2300	-354.3	-91.2	-445.5	0.0	-445.5	
18600	2325	-261.6	-91.2	-352.8	0.0	-352.8	
18600	2350	-249.3	-91.2	-340.5	0.0	-340.5	
18600	2375	-360.4	-91.2	-451.6	0.0	-451.6	
18600	2400	-632	-91.2	-723.2	0.0	-723.2	
18600	2425	-435	-91.2	-526.2	0.0	-526.2	
18600	2450	-211.3	-91.2	-302.5	0.0	-302.5	
18600	2475	-217.3	-91.2	-308.5	0.0	-308.5	
18600	2500	-404	-91.2	-495.2	0.0	-495.2	too rocky. Argillite. No station
18600	2550	-631	-91.2	-722.2	0.0	-722.2	
18600	2575	-537	-91.2	-628.2	0.0	-628.2	
18600	2600	-671	-91.2	-762.2	0.0	-762.2	
18600	2625	-636	-91.2	-727.2	0.0	-727.2	
18600	2650	-621	-91.2	-712.2	0.0	-712.2	
18600	2675	-622	-91.2	-713.2	0.0	-713.2	
18600	2700	-688	-91.2	-779.2	0.0	-779.2	south side of road
18600	2725	-665	-91.2	-758.2	0.0	-758.2	north side of road
18600	2750	-297.5	-91.2	-388.7	0.0	-388.7	
18600	2775	-75.1	-91.2	-166.3	0.0	-166.3	
18600	2800	219.7	-310.9	-91.2	0.0	-91.2	on road
18600	2850	31.8	-91.2	-59.6	0.0	-59.6	too rocky here for a station. Phyllite exposed in roadcut nearby
18600	2875	-47.4	-91.2	-138.6	0.0	-138.6	
18600	2900	-233.7	-91.2	-324.9	0.0	-324.9	
18600	2925	-706	-91.2	-797.2	0.0	-797.2	rocky hole: graphitic argillite
18600	2950	-733	-91.2	-824.2	0.0	-824.2	
18600	2975	-678	-91.2	-769.2	0.0	-769.2	
18600	3000	-486	-91.2	-577.2	0.0	-577.2	
18600	3025	-379.5	-91.2	-470.7	0.0	-470.7	
18600	3050	-804	-91.2	-695.2	0.0	-695.2	
18600	3075	-579	-91.2	-670.2	0.0	-670.2	
18600	3100	-460	-91.2	-551.2	0.0	-551.2	
18600	3125	-293.1	-91.2	-384.3	0.0	-384.3	
18600	3150	-253.8	-91.2	-345	0.0	-345	
18600	3175	-187.6	-91.2	-278.8	0.0	-278.8	north side of road
18600	3200	-23.8	-91.2	-115	0.0	-115	
18600	3225	11.1	-91.2	-80.1	0.0	-80.1	fluctuating slightly

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
18600	3250	-67.2	-91.2	-158.4	0.0	-158.4	
18600	3275	-301.1	-91.2	-392.3	0.0	-392.3	
18600	3300	-392.9	-91.2	-484.1	0.0	-484.1	end of cut line
18600	3325	-398	-91.2	-489.2	0.0	-489.2	
18600	3350	-393	-91.2	-484.2	0.0	-484.2	
18600	3375	-349	-91.2	-440.2	0.0	-440.2	
18600	3400	-196.7	-91.2	-287.9	0.0	-287.9	
18600	3425	-47.9	-91.2	-139.1	0.0	-139.1	
18600	3450	12.2	-91.2	-79	0.0	-79	
18500	2900	-23.3	-91.2	-114.5	0.0	-114.5	
18400	2125	99.8	-99.9	-0.1	0.0	-0.1	edge of pit
18400	2150	81.4	-99.9	-18.5	0.0	-18.5	
18400	2175	71.3	-99.9	-28.6	0.0	-28.6	north side of road
18400	2200	38.3	-99.9	-61.6	0.0	-61.6	minimal fluctuation in reading
18400	2225	9.9	-99.9	-90	0.0	-90	
18400	2250	-13.5	-99.9	-113.4	0.0	-113.4	
18400	2275	-65.5	-99.9	-165.4	0.0	-165.4	
18400	2300	-114.5	-99.9	-214.4	0.0	-214.4	
18400	2325	-192.3	-99.9	-292.2	0.0	-292.2	
18400	2350	-293.7	-99.9	-393.6	0.0	-393.6	
18400	2375	-396.2	-99.9	-496.1	0.0	-496.1	
18400	2400	-386.2	-99.9	-486.1	0.0	-486.1	
18400	2425	-365.6	-99.9	-465.5	0.0	-465.5	
18400	2450	-381.1	-99.9	-481	0.0	-481	
18400	2475	-415	-99.9	-514.9	0.0	-514.9	
18400	2500	-508	-99.9	-607.9	0.0	-607.9	
18400	2525	-503	-99.9	-602.9	0.0	-602.9	
18400	2550	-372.4	-99.9	-472.3	0.0	-472.3	
18400	2575	-520	-99.9	-619.9	0.0	-619.9	
18400	2600	-623	-99.9	-722.9	0.0	-722.9	
18400	2625	-635	-99.9	-734.9	0.0	-734.9	
18400	2650	-588	-99.9	-687.9	0.0	-687.9	
18400	2675	-539	-99.9	-638.9	0.0	-638.9	
18400	2700	-571	-99.9	-670.9	0.0	-670.9	
18400	2725	-543	-99.9	-642.9	0.0	-642.9	north side of road
18400	2750	-168.6	-99.9	-268.5	0.0	-268.5	
18400	2775	-59.6	-99.9	-159.5	0.0	-159.5	
18400	2800	-8.7	-91.2	-99.9	0.0	-99.9	near BC01-15
18300	2800	-73.7	-99.9	-173.6	0.0	-173.6	
18200	2025	163.6	-102.5	61.1	0.0	61.1	edge of pit
18200	2050	166.3	-102.5	63.8	0.0	63.8	
18200	2075	159.9	-102.5	57.4	0.0	57.4	
18200	2100	157.7	-102.5	55.2	0.0	55.2	
18200	2125	156.9	-102.5	54.4	0.0	54.4	south side of road
18200	2150	133.9	-102.5	31.4	0.0	31.4	north side of road
18200	2175	113.4	-102.5	10.9	0.0	10.9	
18200	2200	119.8	-102.5	17.3	0.0	17.3	
18200	2225	97.6	-102.5	-4.9	0.0	-4.9	
18200	2250	89.1	-102.5	-13.4	0.0	-13.4	
18200	2275	51.9	-102.5	-50.6	0.0	-50.6	
18200	2300	39.6	-102.5	-62.9	0.0	-62.9	
18200	2325	-6.1	-102.5	-108.6	0.0	-108.6	
18200	2350	-29.1	-102.5	-131.64	0.0	-131.64	
18200	2375	-124.6	-102.5	-227.1	0.0	-227.1	
18200	2400	-198.7	-102.5	-301.2	0.0	-301.2	
18200	2425	-368.9	-102.5	-471.4	0.0	-471.4	
18200	2450	-502.0	-102.5	-604.5	0.0	-604.5	
18200	2475	-588.0	-102.5	-688.5	0.0	-688.5	
18200	2500	-481.0	-102.5	-583.5	0.0	-583.5	
18200	2525	-388.0	-102.5	-490.5	0.0	-490.5	
18200	2550	-357.5	-102.5	-480	0.0	-480	
18200	2575	-433.0	-102.5	-535.5	0.0	-535.5	
18200	2600	-423.0	-102.5	-525.5	0.0	-525.5	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
18200	2625	-329.9	-102.5	-432.4	0.0	-432.4	
18200	2650	-236.4	-102.5	-338.9	0.0	-338.9	
18200	2675	-485.0	-102.5	-588.5	0.0	-588.5	
18200	2700	-496.0	-102.5	-598.5	0.0	-598.5	
18200	2725	-601.0	-102.5	-703.5	0.0	-703.5	alternating argillite and phyllite (mag--> dol?). North side of bottom road
18200	2750	-437.0	-102.5	-539.5	0.0	-539.5	alternating argillite and phyllite (mag--> dol?). North side of road
18200	2775	-185.5	-102.5	-288	0.0	-288	alternating argillite and phyllite (mag--> dol?)
18200	2800	-2.6	-99.9	-102.5	0.0	-102.5	
18200	2825	36.6	-102.5	-65.9	0.0	-65.9	
18200	2850	72.9	-102.5	-29.6	0.0	-29.6	
18200	2875	78.8	-102.5	-23.7	0.0	-23.7	
18200	2900	13.0	-102.5	-89.5	0.0	-89.5	
18200	2925	-279.7	-102.5	-382.2	0.0	-382.2	
18200	2950	-242.9	-102.5	-345.4	0.0	-345.4	south side of road
18200	2975	-292.8	-102.5	-395.3	0.0	-395.3	
18200	3000	-384.8	-102.5	-487.1	0.0	-487.1	
18200	3025	-502.0	-102.5	-604.5	0.0	-604.5	
18200	3050	-612.0	-102.5	-714.5	0.0	-714.5	
18200	3075	-624.0	-102.5	-726.5	0.0	-726.5	
18200	3100	-396.7	-102.5	-499.2	0.0	-499.2	
18200	3125	-165.3	-102.5	-267.8	0.0	-267.8	
18200	3150	23.0	-102.5	-79.5	0.0	-79.5	
18200	3175	104.7	-102.5	2.2	0.0	2.2	
18200	3200	100.9	-102.5	-1.8	0.0	-1.8	
18200	3225	88.3	-102.5	-14.2	0.0	-14.2	
18200	3250	-11.5	-102.5	-114	0.0	-114	black rocky shale hole
18200	3275	-23.9	-102.5	-126.4	0.0	-126.4	
18200	3300	-257.0	-102.5	-359.5	0.0	-359.5	end of cutline
18200	3325	-427.0	-102.5	-529.5	0.0	-529.5	
18200	3350	-554.0	-102.5	-656.5	0.0	-656.5	
18200	3375	-446.0	-102.5	-548.5	0.0	-548.5	
18200	3400	-198.1	-102.5	-300.6	0.0	-300.6	
Mon Sept 3							
18000	2000	182.7	-126.0	56.7	0.0	56.7	
18000	2025	174.6	-126.0	48.6	0.0	48.6	
18000	2050	185.1	-126.0	59.1	0.0	59.1	
18000	2075	181.4	-126.0	55.4	0.0	55.4	
18000	2100	168.9	-126.0	42.9	0.0	42.9	
18000	2125	161.0	-126.0	35	0.0	35	
18000	2150	156.3	-126.0	30.3	0.0	30.3	north side of road
18000	2175	135.6	-126.0	9.6	0.0	9.6	
18000	2200	127.9	-126.0	1.9	0.0	1.9	
18000	2225	96.5	-126.0	-27.5	0.0	-27.5	
18000	2250	84.7	-126.0	-41.3	0.0	-41.3	
18000	2275	54.3	-126.0	-71.7	0.0	-71.7	
18000	2300	34.5	-126.0	-91.5	0.0	-91.5	
18000	2325	-2.9	-126.0	-128.9	0.0	-128.9	
18000	2350	-53.4	-126.0	-179.4	0.0	-179.4	
18000	2375	-147.2	-126.0	-273.2	0.0	-273.2	)
18000	2400	-317.0	-126.0	-443	0.0	-443	fluctuating plus/minus 3mV
18000	2425	-423.0	-126.0	-549	0.0	-549	
18000	2450	-398.0	-126.0	-524	0.0	-524	
18000	2475	-419.0	-126.0	-545	0.0	-545	
18000	2500	-419.0	-126.0	-545	0.0	-545	
18000	2525	-412.0	-126.0	-538	0.0	-538	
18000	2550	-282.1	-126.0	-408.1	0.0	-408.1	
18000	2575	-251.7	-126.0	-377.7	0.0	-377.7	
18000	2600	-455.0	-126.0	-581	0.0	-581	
18000	2625	-609.0	-126.0	-735	0.0	-735	on old road
18000	2650	-559.0	-126.0	-685	0.0	-685	
18000	2675	-478.0	-126.0	-604	0.0	-604	
18000	2700	-355.7	-126.0	-481.7	0.0	-481.7	
18000	2725	-183.0	-126.0	-309	0.0	-309	
18000	2750	-163.4	-126.0	-289.4	0.0	-289.4	
18000	2775	-54.5	-126.0	-180.5	0.0	-180.5	outcrop below
18000	2800	-23.5	-102.5	-126	0.0	-126	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
18000	2825	26.8	-126.0	-99.2	0.0	-99.2	
18000	2850	-70.2	-126.0	-196.2	0.0	-196.2	
18000	2875	-356.5	-126.0	-482.5	0.0	-482.5	
18000	2900	-259.0	-126.0	-385	0.0	-385	
18000	2925	-285.1	-126.0	-411.1	0.0	-411.1	
18000	2950	-74.9	-126.0	-200.9	0.0	-200.9	
18000	2975	-4.5	-126.0	-130.5	0.0	-130.5	in ditchline
18000	3000	-203.4	-126.0	-329.4	0.0	-329.4	
18000	3025	-488.0	-126.0	-614	0.0	-614	
18000	3050	-624.0	-126.0	-750	0.0	-750	south side of road
18000	3075	-589.0	-126.0	-715	0.0	-715	
18000	3100	-344.7	-126.0	-470.7	0.0	-470.7	
18000	3125	-66.7	-126.0	-192.7	0.0	-192.7	
18000	3150	53.3	-126.0	-72.7	0.0	-72.7	
18000	3175	8.6	-126.0	-117.4	0.0	-117.4	
18000	3200	36.6	-126.0	-89.4	0.0	-89.4	on old road
18000	3225	84.8	-126.0	-41.2	0.0	-41.2	
18000	3250	-175.6	-126.0	-301.6	0.0	-301.6	
18000	3275	-386.0	-126.0	-512	0.0	-512	
18000	3300	-414.0	-126.0	-540	0.0	-540	
18000	3325	-247.9	-126.0	-373.9	0.0	-373.9	fluctuating plus/minus 3mV
18000	3350	-36.3	-126.0	-162.3	0.0	-162.3	
18000	3375	67.5	-126.0	-58.5	0.0	-58.5	
18000	3400	118.1	-126.0	-7.9	0.0	-7.9	fluctuating lots
18000	3425	127.3	-126.0	1.3	0.0	1.3	
18000	3450	150.0	-126.0	24	0.0	24	
18000	3475	153.1	-126.0	27.1	0.0	27.1	
18000	3500	173.8	-126.0	47.8	0.0	47.8	
18000	3525	186.3	-126.0	60.3	0.0	60.3	
18000	3550	196.0	-126.0	70	0.0	70	
18000	3575	196.4	-126.0	72.4	0.0	72.4	
18000	3600	208.3	-126.0	82.3	0.0	82.3	
17900	2800	-290.8	-126.0	-416.8	0.0	-416.8	
17800	2150	696.0	-689.0	7	0.0	7	edge of pit
17800	2175	673.0	-689.0	-16	0.0	-16	north side of road
17800	2200	671.0	-689.0	-18	0.0	-18	
17800	2225	646.0	-689.0	-43	0.0	-43	
17800	2250	616.0	-689.0	-73	0.0	-73	
17800	2275	580.0	-689.0	-109	0.0	-109	
17800	2300	535.0	-689.0	-154	0.0	-154	
17800	2325	489.0	-689.0	-200	0.0	-200	
17800	2350	438.0	-689.0	-251	0.0	-251	
17800	2375	337.6	-689.0	-351.4	0.0	-351.4	
17800	2400	363.0	-689.0	-326	0.0	-326	
17800	2425	188.9	-689.0	-500.1	0.0	-500.1	
17800	2450	214.2	-689.0	-474.8	0.0	-474.8	
17800	2475	227.7	-689.0	-461.3	0.0	-461.3	
17800	2500	271.5	-689.0	-417.5	0.0	-417.5	
17800	2525	189.3	-689.0	-499.7	0.0	-499.7	
17800	2550	28.4	-689.0	-660.6	0.0	-660.6	
17800	2575	293.8	-689.0	-782.8	0.0	-782.8	
17800	2600	197.9	-689.0	-786.9	0.0	-786.9	
17800	2625	-414.4	-689.0	-803.4	0.0	-803.4	
17800	2650	-40.7	-689.0	-729.7	0.0	-729.7	
17800	2675	148.1	-689.0	-542.9	0.0	-542.9	
17800	2700	-40.9	-689.0	-729.9	0.0	-729.9	
17800	2725	138.1	-689.0	-550.9	0.0	-550.9	
17800	2750	345.8	-689.0	-343.2	0.0	-343.2	
17800	2775	176.2	-689.0	-512.8	0.0	-512.8	
17800	2800	-563.0	-126.0	-689	0.0	-689	in old trench running N/S on grid. Looks like from early exploration of BC Vein
17800	2825	-67.6	-689.0	-756.6	0.0	-756.6	
17800	2850	431.1	-689.0	-287.9	0.0	-287.9	
17800	2875	601.0	-689.0	-88	0.0	-88	
17800	2900	572.0	-689.0	-117	0.0	-117	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
17800	2925	686.0	-689.0	-3	0.0	-3	in middle of road
17800	2950	668.0	-689.0	-21	0.0	-21	
17800	2975	365.3	-689.0	-323.7	0.0	-323.7	
17800	3000	77.3	-689.0	-611.7	0.0	-611.7	
17800	3025	135.7	-689.0	-553.3	0.0	-553.3	
17800	3050	198.6	-689.0	-490.4	0.0	-490.4	
17800	3075	356.8	-689.0	-332.2	0.0	-332.2	in ditchline
17800	3100	283.6	-689.0	-405.4	0.0	-405.4	
17800	3125	434.0	-689.0	-255	0.0	-255	
17800	3150	474.0	-689.0	-215	0.0	-215	south side of road
17800	3175	558.0	-689.0	-131	0.0	-131	
17800	3200	459.0	-689.0	-230	0.0	-230	
17800	3225	453.0	-689.0	-236	0.0	-236	
17800	3250	390.0	-689.0	-299	0.0	-299	
17800	3275	368.1	-689.0	-320.9	0.0	-320.9	
17800	3300	449.0	-689.0	-240	0.0	-240	
17800	3325	514.0	-689.0	-175	0.0	-175	
17800	3350	586.0	-689.0	-103	0.0	-103	
17800	3375	613.0	-689.0	-76	0.0	-76	
17800	3400	678.0	-689.0	-11	0.0	-11	
17800	3425	680.3	-689.0	-8.7	0.0	-8.7	
17800	3450	701.5	-689.0	12.5	0.0	12.5	
17800	3475	709.3	-689.0	20.3	0.0	20.3	
17800	3500	738.0	-689.0	49	0.0	49	
17800	3525	750.5	-689.0	61.5	0.0	61.5	
17800	3550	789.0	-689.0	100	0.0	100	
17700	2800	148.7	-689.0	-540.3	0.0	-540.3	
17600	2125	723.0	-726.9	-3.9	0.0	-3.9	edge of pit
17600	2150	729.0	-726.9	2.1	0.0	2.1	
17600	2175	704.0	-726.9	-22.9	0.0	-22.9	
17600	2200	682.0	-726.9	-44.9	0.0	-44.9	south side of road
17600	2225	682.0	-726.9	-44.9	0.0	-44.9	
17600	2250	635.0	-726.9	-91.9	0.0	-91.9	
17600	2275	573.0	-726.9	-153.9	0.0	-153.9	
17600	2300	498.0	-726.9	-228.9	0.0	-228.9	
17600	2325	413.0	-726.9	-313.9	0.0	-313.9	
17600	2350	334.1	-726.9	-392.8	0.0	-392.8	
17600	2375	238.9	-726.9	-488	0.0	-488	
17600	2400	200.7	-726.9	-526.2	0.0	-526.2	
17600	2425	197.9	-726.9	-529	0.0	-529	
17600	2450	268.8	-726.9	-458.1	0.0	-458.1	
17600	2475	230.4	-726.9	-496.5	0.0	-496.5	
17600	2500	129.9	-726.9	-597	0.0	-597	
17600	2525	1.7	-726.9	-725.2	0.0	-725.2	
17600	2550	-32.2	-726.9	-759.1	0.0	-759.1	
17600	2575	-37.8	-726.9	-764.7	0.0	-764.7	
17600	2600	11.5	-726.9	-715.4	0.0	-715.4	
17600	2625	64.4	-726.9	-662.5	0.0	-662.5	
17600	2650	308.2	-726.9	-418.7	0.0	-418.7	
17600	2675	386.0	-726.9	-340.9	0.0	-340.9	
17600	2700	353.0	-726.9	-373.9	0.0	-373.9	
17600	2725	290.4	-726.9	-436.5	0.0	-436.5	
17600	2750	219.7	-726.9	-507.2	0.0	-507.2	
17600	2775	57.0	-726.9	-669.9	0.0	-669.9	
17600	2800	-37.9	-689.0	-726.9	0.0	-726.9	argillite fill in hole, some quartz
17600	2825	251.2	-726.9	-475.7	0.0	-475.7	
17600	2850	665.0	-726.9	-61.9	0.0	-61.9	
17600	2875	684.0	-726.9	-42.9	0.0	-42.9	
17600	2900	680.0	-726.9	-46.9	0.0	-46.9	
17600	2925	623.0	-726.9	-103.9	0.0	-103.9	
17600	2950	183.0	-726.9	-583.9	0.0	-583.9	
17600	2975	326.2	-726.9	-400.7	0.0	-400.7	
17600	3000	516.0	-726.9	-210.9	0.0	-210.9	
17600	3025	298.0	-726.9	-428.9	0.0	-428.9	
17600	3050	456.0	-726.9	-270.9	0.0	-270.9	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
17600	3075	392.9	-726.9	-334	0.0	-334	
17600	3100	403.0	-726.9	-323.9	0.0	-323.9	
17600	3125	479.0	-726.9	-247.9	0.0	-247.9	
17600	3150	574.0	-726.9	-152.9	0.0	-152.9	
17600	3175	510.0	-726.9	-216.9	0.0	-216.9	
17600	3200	443.0	-726.9	-283.9	0.0	-283.9	
17600	3225	323.6	-726.9	-403.3	0.0	-403.3	in ditchline south side of road
17600	3250	227.2	-726.9	-499.7	0.0	-499.7	
17600	3275	230.9	-726.9	-496	0.0	-496	
17600	3300	574.0	-726.9	-152.9	0.0	-152.9	
17600	3325	541.0	-726.9	-85.9	0.0	-85.9	
17600	3350	702.0	-726.9	-24.9	0.0	-24.9	
17600	3375	696.0	-726.9	-30.9	0.0	-30.9	
17600	3400	735.0	-726.9	8.1	0.0	8.1	
17600	3425	720.0	-726.9	-6.9	0.0	-6.9	
17600	3450	753.0	-726.9	26.1	0.0	26.1	
17600	3475	746.0	-726.9	19.1	0.0	19.1	
17600	3500	775.0	-726.9	48.1	0.0	48.1	
17600	3525	782.0	-726.9	55.1	0.0	55.1	
17600	3550	816.0	-726.9	89.1	0.0	89.1	
17600	3575	824.0	-726.9	97.1	0.0	97.1	
17600	3600	850.0	-726.9	123.1	0.0	123.1	
17500	2800	122.4	-726.9	-604.5	0.0	-604.5	
17400	2200	720	-762.1	-42.1	0.0	-42.1	edge of pit
17400	2225	690	-762.1	-72.1	0.0	-72.1	
17400	2250	668	-762.1	-94.1	0.0	-94.1	
17400	2275	624	-762.1	-138.1	0.0	-138.1	
17400	2300	609	-762.1	-153.1	0.0	-153.1	
17400	2325	544	-762.1	-218.1	0.0	-218.1	
17400	2350	504	-762.1	-258.1	0.0	-258.1	
17400	2375	494	-762.1	-268.1	0.0	-268.1	
17400	2400	452	-762.1	-310.1	0.0	-310.1	
17400	2425	402	-762.1	-360.1	0.0	-360.1	
17400	2450	380	-762.1	-382.1	0.0	-382.1	
17400	2475	233.5	-762.1	-528.6	0.0	-528.6	
17400	2500	134.6	-762.1	-627.5	0.0	-627.5	
17400	2525	116.2	-762.1	-645.9	0.0	-645.9	
17400	2550	315.8	-762.1	-446.3	0.0	-446.3	
17400	2575	339.1	-762.1	-423	0.0	-423	
17400	2600	267.7	-762.1	-494.4	0.0	-494.4	
17400	2625	126	-762.1	-636.1	0.0	-636.1	
17400	2650	77.2	-762.1	-684.9	0.0	-684.9	
17400	2675	24.3	-762.1	-737.8	0.0	-737.8	
17400	2700	32.9	-762.1	-729.2	0.0	-729.2	
17400	2725	-17.9	-762.1	-780	0.0	-780	
17400	2750	-34.2	-762.1	-796.3	0.0	-796.3	
17400	2775	-28.5	-762.1	-790.6	0.0	-790.6	black shaley hole in old road
17400	2800	-35.2	-726.9	-762.1	0.0	-762.1	in road fill on side of old road that runs down the hill
17400	2825	333.7	-762.1	-428.4	0.0	-428.4	
17400	2850	626.0	-762.1	-136.1	0.0	-136.1	
17400	2875	726.0	-762.1	-36.1	0.0	-36.1	
17400	2900	755.0	-762.1	-7.1	0.0	-7.1	
17400	2925	757.0	-762.1	-5.1	0.0	-5.1	
17400	2950	753.0	-762.1	-9.1	0.0	-9.1	
17400	2975	891.0	-762.1	-71.1	0.0	-71.1	
17400	3000	863.0	-762.1	-99.1	0.0	-99.1	
17400	3025	485.0	-762.1	-297.1	0.0	-297.1	
17400	3050	302.1	-762.1	-460	0.0	-460	south side of road
17400	3075	236.3	-762.1	-525.8	0.0	-525.8	
17400	3100	236.1	-762.1	-526	0.0	-526	
17400	3125	312.3	-762.1	-449.8	0.0	-449.8	
17400	3150	312.4	-762.1	-449.7	0.0	-449.7	
17400	3175	459.0	-762.1	-303.1	0.0	-303.1	
17400	3200	444.0	-762.1	-318.1	0.0	-318.1	

CONTROL STATION	SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
	EASTING	NORTHING	[mV]	[mV]	[mv]	[mV]	[mV]	
	17400	3225	426.0	-762.1	-336.1	0.0	-336.1	
	17400	3250	463.0	-762.1	-299.1	0.0	-299.1	
	17400	3275	240.7	-762.1	-521.4	0.0	-521.4	
	17400	3300	432.0	-762.1	-330.1	0.0	-330.1	
	17400	3325	633.0	-762.1	-129.1	0.0	-129.1	
	17400	3350	699.0	-762.1	-63.1	0.0	-63.1	south side of road
	17400	3375	770.0	-762.1	7.9	0.0	7.9	
	17400	3400	805.0	-762.1	42.9	0.0	42.9	
	17400	3425	813.0	-762.1	50.9	0.0	50.9	
	17400	3450	816.0	-762.1	53.9	0.0	53.9	
	17400	3475	818.0	-762.1	55.9	0.0	55.9	
	17400	3500	818.0	-762.1	55.9	0.0	55.9	
	17400	3525	819.0	-762.1	56.9	0.0	56.9	
	17400	3550	843.0	-762.1	80.9	0.0	80.9	
	17400	3575	859.0	-762.1	96.9	0.0	96.9	
	17400	3600	887.0	-762.1	124.9	0.0	124.9	
	17300	2800	32.7	-762.1	-729.4	0.0	-729.4	
Sat sept 8, leap frog								
22400E, 2800N								
	22400	2785	48.0		59.1	0.0	59.1	
	22400	2770	11.1	48	47.8	0.0	47.8	
	22400	2750	-11.3	59.1	60.7	0.0	60.7	
	22400	2725	12.9	47.8	58.0	0.0	58.0	on side of pit
	22400	2700	-2.7	60.7	55.3	0.0	55.3	muddy
	22400	2675	10.3	55	62.6	0.0	62.6	still on side of pit
	22400	2650	-5.7	68.3	78.1	0.0	78.1	
	22400	2625	15.5	62.6	73.0	0.0	73.0	still on side of hill. Gravelly
	22400	2600	-5.1	78.1	91.4	0.0	91.4	at bottom of hill. Gravelly
	22400	2570	18.4	73	88.9	0.0	88.9	flat topography. Marsh
	22400	2550	-2.5	91.4	98.3	0.0	98.3	flat topography. Gravelly
	22400	2525	9.4	88.9	61.9	0.0	61.9	flat topography. Muddy
	22400	2500	-36.4	98.3	60.5	0.0	60.5	
	22400	2475	-1.4	61.9				
	22400	2825	29.7	48	77.7	0.0	77.7	
	22400	2800	-31.3	77.7	46.4	0.0	46.4	
	22400	2775	21.7	46.4	68.1	0.0	68.1	
	22400	2900	-3.3	68.1	64.8	0.0	64.8	
21000E, 2807N								
	21025	2800	-104.0		-148.5	0.0	-148.5	
	21050	2800	-44.5	-104	-191.9	0.0	-191.9	middle of muddy road
	21075	2805	-15.9	-148.5	-207.8	0.0	-207.8	on muddy road
	20975	2800	19.8	-191.9		0.0	0.0	
	20975	2800	19.8	-104	-84.2	0.0	-84.2	
21350E, 2800N								
	21350	2775	-375.9		-445.0	0.0	-445.0	
	21350	2750	-69.1	-375.9	-384.9	0.0	-384.9	
	21350	2725	60.1	-445	-289.2	0.0	-289.2	
	21375	2725	95.7	-384.9	-310.9	0.0	-310.9	rusty gravel
	21350	2825	-21.7	-289.2				
	21350	2825	121.5	-375.9	-254.4	0.0	-254.4	
	21350	2850	87.2	-254.4	-167.2	0.0	-167.2	3 feet south of path on ditchline
21300E, 2800N								
	21300	2775	-448.4		-471.5	0.0	-471.5	
	21300	2750	-25.1	-448.4	-539.8	0.0	-539.8	
	21300	2725	-68.3	-471.5	-424.2	0.0	-424.2	
	21300	2725	115.6	-539.8				
21200E, 2800N								
	21225	2800	-335.4		-370.8	0.0	-370.8	duplicate
	21250	2800	-35.4	-335.4	-414.4	0.0	-414.4	duplicate
	21275	2800	-43.6	-370.8	-422.5	0.0	-422.5	duplicate
	21275	2800	-8.1	-414.4				

CONTROL STATION

Sun Sept 9

17200E, 2800N

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
17300	2800	32.7	-762.1	-729.4	0.0	-729.4	
					0.0	0.0	
		242.1					
17200	2350	269.7	-487.3	-217.6	0.0	-217.6	top edge of pit
17200	2375	173.9	-487.3	-313.4	0.0	-313.4	
17200	2400	97.3	-487.3	-390.0	0.0	-390.0	
17200	2425	94.2	-487.3	-393.1	0.0	-393.1	
17200	2450	78.3	-487.3	-409.0	0.0	-409.0	
17200	2475	92.3	-487.3	-395.0	0.0	-395.0	
17200	2500	158.1	-487.3	-329.2	0.0	-329.2	
17200	2525	244.8	-487.3	-242.5	0.0	-242.5	rooty
17200	2550	259.5	-487.3	-227.8	0.0	-227.8	rooty
17200	2575	214.6	-487.3	-272.7	0.0	-272.7	
17200	2600	98.9	-487.3	-388.4	0.0	-388.4	
17200	2625	156.7	-487.3	-330.6	0.0	-330.6	rocky
17200	2650	-190.6	-487.3	-677.9	0.0	-677.9	
17200	2675	-293.6	-487.3	-780.9	0.0	-780.9	rocky
17200	2700	-254.2	-487.3	-741.5	0.0	-741.5	
17200	2725	-248.3	-487.3	-735.6	0.0	-735.6	
17200	2750	-272.2	-487.3	-759.5	0.0	-759.5	
17200	2775	-213.9	-487.3	-701.2	0.0	-701.2	
17200	2800	242.1	-729.4	-487.3	0.0	-487.3	
17200	2825	256.4	-487.3	-230.9	0.0	-230.9	
17200	2850	363.2	-487.3	-124.1	0.0	-124.1	
17200	2875	396.2	-487.3	-91.1	0.0	-91.1	
17200	2900	395.4	-487.3	-91.9	0.0	-91.9	
17200	2925	293.4	-487.3	-193.9	0.0	-193.9	
17200	2950	111.2	-487.3	-376.1	0.0	-376.1	
17200	2975	-11.0	-487.3	-498.3	0.0	-498.3	
17200	3000	-60.2	-487.3	-547.5	0.0	-547.5	
17200	3025	-50.8	-487.3	-537.9	0.0	-537.9	
17200	3050	82.4	-487.3	-404.9	0.0	-404.9	
17200	3075	32.1	-487.3	-455.2	0.0	-455.2	
17200	3100	-0.5	-487.3	-487.8	0.0	-487.8	
17200	3125	108.1	-487.3	-379.2	0.0	-379.2	
17200	3150	136.0	-487.3	-351.3	0.0	-351.3	reading taken in middle of the road
17200	3175	129.8	-487.3	-357.5	0.0	-357.5	
17200	3200	334.8	-487.3	-152.5	0.0	-152.5	
17200	3225	364.7	-487.3	-122.6	0.0	-122.6	maybe near a creek. Ground is dewy wet
17200	3250	380.8	-487.3	-106.5	0.0	-106.5	
17200	3275	456.0	-487.3	-31.3	0.0	-31.3	
17200	3300	532.0	-487.3	44.7	0.0	44.7	
17200	3325	563.0	-487.3	65.7	0.0	65.7	some roots in hole
17200	3350	570.0	-487.3	82.7	0.0	82.7	
17200	3375	593.0	-487.3	105.7	0.0	105.7	
17200	3400	611.0	-487.3	123.7	0.0	123.7	
17200	3425	611.0	-487.3	123.7	0.0	123.7	
17200	3450	627.0	-487.3	139.7	0.0	139.7	
17200	3475	648.0	-487.3	160.7	0.0	160.7	
17200	3500	629.0	-487.3	141.7	0.0	141.7	
17200	3525	632.0	-487.3	144.7	0.0	144.7	
17200	3550	652.0	-487.3	164.7	0.0	164.7	
17200	3575	649.0	-487.3	161.7	0.0	161.7	
17200	3600	665.0	-487.3	177.7	0.0	177.7	
17100	2800	149.3	-487.3	-338.0	0.0	-338.0	
		331.3					
17000E, 2800N							
17000	2430	-72.9	-156.0	-228.9	0.0	-228.9	on side of hill/hyd pit
17000	2450	-89.7	-156.0	-245.7	0.0	-245.7	edge of hyd pit
17000	2475	-64.1	-156.0	-220.1	0.0	-220.1	
17000	2500	-8.6	-156.0	-184.6	0.0	-184.6	
17000	2525	-3.7	-156.0	-159.7	0.0	-159.7	
17000	2550	-73.4	-156.0	-229.4	0.0	-229.4	
17000	2575	-246.7	-156.0	-402.7	0.0	-402.7	
17000	2600	-412.0	-156.0	-568.0	0.0	-568.0	rocky

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
17000	2625	-461.0	-156.0	-617.0	0.0	-617.0	
17000	2650	-458.0	-156.0	-614.0	0.0	-614.0	
17000	2675	-502.0	-156.0	-658.0	0.0	-658.0	
17000	2700	-536.0	-156.0	-692.0	0.0	-692.0	
17000	2725	-575.0	-156.0	-731.0	0.0	-731.0	
17000	2750	-563.0	-156.0	-719.0	0.0	-719.0	
							fallen trees... No station
17000	2800	331.3	-487.3	-156.0	0.0	-156.0	
17000	2825	121.7	-156.0	-34.3	0.0	-34.3	
17000	2850	119.2	-156.0	-36.8	0.0	-36.8	rooty
17000	2875	114.8	-156.0	-41.2	0.0	-41.2	
							FOR FUTURE REFERENCE: bear den located here with many markings on surrounding trees up to 100' away
17000	2900	37.8	-156.0	-118.2	0.0	-118.2	
17000	2925	-170.3	-156.0	-326.3	0.0	-326.3	
17000	2950	-286.4	-156.0	-442.4	0.0	-442.4	
17000	2975	-346.3	-156.0	-502.3	0.0	-502.3	
17000	3000	-257.8	-156.0	-413.8	0.0	-413.8	
17000	3025	-257.0	-156.0	-413.0	0.0	-413.0	
17000	3050	-264.9	-156.0	-420.9	0.0	-420.9	
17000	3075	-437.0	-156.0	-593.0	0.0	-593.0	
17000	3100	-453.0	-156.0	-609.0	0.0	-609.0	
17000	3125	-356.5	-156.0	-512.5	0.0	-512.5	
17000	3150	-207.9	-156.0	-363.9	0.0	-363.9	
17000	3175	-127.0	-156.0	-283.0	0.0	-283.0	
17000	3200	-17.7	-156.0	-173.7	0.0	-173.7	
17000	3225	27.9	-156.0	-128.1	0.0	-128.1	
17000	3250	-31.7	-156.0	-187.7	0.0	-187.7	rocky and next to stream
17000	3275	109.5	-156.0	-46.5	0.0	-46.5	rocky
17000	3300	181.0	-156.0	25.0	0.0	25.0	
17000	3325	252.1	-156.0	96.1	0.0	96.1	
17000	3350	257.5	-156.0	101.5	0.0	101.5	rocky
17000	3375	271.1	-156.0	115.1	0.0	115.1	rocky
17000	3400	305.9	-156.0	149.9	0.0	149.9	
17000	3425	304.8	-156.0	148.8	0.0	148.8	
17000	3450	325.4	-156.0	169.4	0.0	169.4	
17000	3475	321.0	-156.0	165.0	0.0	165.0	
17000	3500	332.6	-156.0	176.6	0.0	176.6	
17000	3525	340.0	-156.0	184.0	0.0	184.0	
17000	3550	339.0	-156.0	183.0	0.0	183.0	
17000	3575	344.1	-156.0	188.1	0.0	188.1	
17000	3600	336.7	-156.0	180.7	0.0	180.7	
16900	2800	75.3	-156.0	-80.7	0.0	-80.7	
16800E, 2800N		80.8					
16800	2600	75.4	-75.2	0.2	0.0	0.2	
16800	2625	49.0	-75.2	-26.2	0.0	-26.2	
16800	2650	1.6	-75.2	-73.6	0.0	-73.6	
16800	2675	-78.6	-75.2	-153.8	0.0	-153.8	
16800	2700	-143.1	-75.2	-218.3	0.0	-218.3	
16800	2725	-202.7	-75.2	-277.9	0.0	-277.9	
16800	2750	-137.7	-75.2	-212.9	0.0	-212.9	
16800	2775	-54.6	-75.2	-129.8	0.0	-129.8	
16800	2800	80.8	-156.0	-75.2	0.0	-75.2	30' mine grid Northwest of claim post
16800	2825	32.5	-75.2	-42.7	0.0	-42.7	
16800	2850	29.3	-75.2	-45.9	0.0	-45.9	
16800	2875	-41.4	-75.2	-116.6	0.0	-116.6	
16800	2900	-206.6	-75.2	-281.8	0.0	-281.8	
16800	2925	-295.6	-75.2	-370.8	0.0	-370.8	
16800	2950	-377.9	-75.2	-453.1	0.0	-453.1	
16800	2975	-363.4	-75.2	-438.6	0.0	-438.6	
16800	3000	-324.7	-75.2	-399.9	0.0	-399.9	
16800	3025	-354.2	-75.2	-429.4	0.0	-429.4	
16800	3050	-413.0	-75.2	-488.2	0.0	-488.2	rocky
16800	3075	-203.8	-75.2	-279.0	0.0	-279.0	
16800	3100	-76.8	-75.2	-151.6	0.0	-151.6	
16800	3125	-208.2	-75.2	-283.4	0.0	-283.4	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
16800	3150	-208.7	-75.2	-283.9	0.0	-283.9	
16800	3175	-126.1	-75.2	-201.3	0.0	-201.3	
16800	3200	-97.5	-75.2	-172.7	0.0	-172.7	
16800	3225	-192.2	-75.2	-267.4	0.0	-267.4	
16800	3250	-204.2	-75.2	-279.4	0.0	-279.4	
16800	3275	-282.7	-75.2	-357.9	0.0	-357.9	
16800	3300	-80.4	-75.2	-155.6	0.0	-155.6	
16800	3325	98.5	-75.2	23.3	0.0	23.3	
16800	3350	157.6	-75.2	82.4	0.0	82.4	
16800	3375	200.7	-75.2	125.5	0.0	125.5	on road
16800	3400	212.3	-75.2	137.1	0.0	137.1	
16800	3425	227.9	-75.2	152.7	0.0	152.7	
16800	3450	216.0	-75.2	140.8	0.0	140.8	
16800	3475	219.5	-75.2	144.3	0.0	144.3	
16800	3500	237.1	-75.2	161.9	0.0	161.9	
16800	3525	237.7	-75.2	162.5	0.0	162.5	
16800	3550	254.1	-75.2	178.9	0.0	178.9	rocky
16700	2800	7.0	-75.2	-68.2	0.0	-68.2	
16600E, 2800N		15.2					
16600	2750	21.6	-60.0	-38.4	0.0	-38.4	
16600	2775	37.6	-60.0	-22.4	0.0	-22.4	going downhill, towards edge of pit
16600	2800	15.2	-75.2	-60.0	0.0	-60.0	
16600	2825	-0.1	-60.0	-60.1	0.0	-60.1	
16600	2850	-6.6	-60.0	-66.6	0.0	-66.6	
16600	2875	-77.3	-60.0	-137.3	0.0	-137.3	
16600	2900	-138.4	-60.0	-198.4	0.0	-198.4	
16600	2925	-167.9	-60.0	-227.9	0.0	-227.9	
16600	2950	-185.1	-60.0	-245.1	0.0	-245.1	
16600	2975	-202.8	-60.0	-262.8	0.0	-262.8	
16600	3000	-186.4	-60.0	-246.4	0.0	-246.4	
16600	3025	-214.0	-60.0	-274.0	0.0	-274.0	
16600	3050	-81.4	-60.0	-141.4	0.0	-141.4	
16600	3075	-114.5	-60.0	-174.5	0.0	-174.5	
16600	3100	-275.1	-60.0	-335.1	0.0	-335.1	
16600	3125	-284.9	-60.0	-344.9	0.0	-344.9	
16600	3150	-229.0	-60.0	-289.0	0.0	-289.0	
16600	3175	-137.3	-60.0	-197.3	0.0	-197.3	
16600	3200	-93.2	-60.0	-153.2	0.0	-153.2	
16600	3225	-162.1	-60.0	-222.1	0.0	-222.1	
16600	3250	-134.4	-60.0	-194.4	0.0	-194.4	
16600	3275	-30.4	-60.0	-90.4	0.0	-90.4	
16600	3300	108.9	-60.0	48.9	0.0	48.9	
16600	3325	140.9	-60.0	80.9	0.0	80.9	
16600	3350	167.7	-60.0	107.7	0.0	107.7	
16600	3375	190.7	-60.0	130.7	0.0	130.7	
16600	3400	206.6	-60.0	146.6	0.0	146.6	
16600	3425	209.8	-60.0	149.8	0.0	149.8	
16600	3450	211.7	-60.0	151.7	0.0	151.7	
16600	3475	227.1	-60.0	167.1	0.0	167.1	on road
16600	3500	215.0	-60.0	155.0	0.0	155.0	
16600	3525	214.2	-60.0	154.2	0.0	154.2	
16600	3550	216.8	-60.0	156.8	0.0	156.8	
16600	3575	201.8	-60.0	141.8	0.0	141.8	
16575	2800	-24.9	-60.0	-35.1	0.0	-35.1	edge of pit and most western end of 2800N baseline
Sept 12 leap frog 21200E, 2850N		-119.8					
21195	2844	-22.4	-119.8	-142.2	0.0	-142.2	center of road
21175	2839	-24.9	-142.2	-167.1	0.0	-167.1	center of road
21148	2830	-9.7	-167.1	-176.8	0.0	-176.8	center of road
21123	2823	-19.7	-176.8	-196.5	0.0	-196.5	center of road
21100	2814	-1.2	-196.5	-197.7	0.0	-197.7	center of road
21075	2805	-16.9	-197.7	-214.6	0.0	-214.6	center of road
21100E, 2814N		-197.7					

CONTROL STATION	SURVEY STATION		READING [mV]	CORRECTION VALUE [mV]	TENTATIVE VALUE [mV]	NORMALIZER [mV]	FINAL VALUE [mV]	COMMENTS
	EASTING	NORTHING						
	21100	2839	71.5	-197.7	-126.2	0.0	-126.2	gravelly, grey soil. Near old orange flagging that says 65E 2600N. Looks like old trench or road was here
	21100	2864	40.7	-126.2	-85.5	0.0	-85.5	
	21100	2863	56.2	-85.5	-30.3	0.0	-30.3	
21195E, 2844N			-142.2					muddy close to muddy waterhole in road
	21218	2859	18.8	-142.2	-123.4	0.0	-123.4	
	21218	2853	-0.3	-123.4	-123.7	0.0	-123.7	
21250E, 2800N			-417.6					
	21250	2775	52.3	-417.6	-365.3	0.0	-365.3	
	21250	2750	61.4	-365.3	-303.9	0.0	-303.9	
	21250	2725	43.9	-303.9	-260.0	0.0	-260.0	
21300E, 2725N			-424.2					rocky and rooty..... NOTE: I think drill rods in the ground at 21300E, and drilling south on grid, is affecting the SP readings. These 21300E values are skewed and will not be included with the final data. all values along 16600E from 3525N to 4800N were completely redone at a later date, Sept 21, as it was later found that sporadic readings were a result of Solar Flare activity which made SP values 20-30mV more positive than they should have been. Other lines completed on Sept 15 were also rechecked but did not need to be redone as values remained about the same as when originally taken.
	21300	2700	68.3	-424.2	-355.9	0.0	-355.9	
	21300	2675	31.7	-355.9	-324.2	0.0	-324.2	
SEPT 15 regular 16600E, 3500N			155.0					
	16600	3525	-12.9	155.0	142.1	0.0	142.1	
	16600	3550	-32.8	155.0	122.2	0.0	122.2	
	16600	3600	-10.0	155.0	145.0	0.0	145.0	
	16600	3625	-20.7	155.0	134.3	0.0	134.3	
	16600	3650	1.3	155.0	156.3	0.0	156.3	
	16600	3675	-8.1	155.0	148.9	0.0	148.9	
	16600	3700	-10.9	155.0	144.1	0.0	144.1	
	16600	3733	-32.6	155.0	122.4	0.0	122.4	
	16600	3767	-4.7	155.0	150.3	0.0	150.3	
	16600	3800	29.7	155.0	184.7	0.0	184.7	
	16600	3825	31.8	155.0	186.8	0.0	186.8	
	16600	3850	45.7	155.0	200.7	0.0	200.7	
	16600	3875						
	16600	3900	40.2	155.0	195.2	0.0	195.2	
	16600	3925	50.2	155.0	205.2	0.0	205.2	
	16600	3950	45.5	155.0	200.5	0.0	200.5	
	16600	3975	51.9	155.0	208.9	0.0	208.9	
	16600	4000	52.9	155.0	207.9	0.0	207.9	thick overburden
16600E, 4000N			207.9					
	16600	4025	-2.4	207.9	205.5	0.0	205.5	
	16600	4050	4.3	207.9	212.2	0.0	212.2	
	16600	4075	-11.4	207.9	196.5	0.0	196.5	
	16600	4100	8.0	207.9	215.9	0.0	215.9	
	16600	4125						
	16600	4150	20.3	207.9	228.2	0.0	228.2	
	16600	4175	-1.5	207.9	206.4	0.0	206.4	
	16600	4200	1.6	207.9	209.5	0.0	209.5	
	16600	4225	-13.9	207.9	194.0	0.0	194.0	
	16600	4250	-13.1	207.9	194.8	0.0	194.8	
	16600	4275						
	16600	4300						south side of road
	16600	4332	9.4	207.9	217.3	0.0	217.3	
	16600	4350	-15.3	207.9	192.6	0.0	192.6	
	16600	4375	-10.8	207.9	197.1	0.0	197.1	
	16600	4400	-14.9	207.9	193.0	0.0	193.0	
	16600	4425	-22.7	207.9	185.2	0.0	185.2	
	16600	4450	2.8	207.9	210.8	0.0	210.8	
	16600	4475	8.6	207.9	216.5	0.0	216.5	
	16600	4500	15.6	207.9	223.5	0.0	223.5	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
16600	4525	4.8	207.9	212.7	0.0	212.7	
16600	4550	9.2	207.9	217.1	0.0	217.1	
16600	4575	20.8	207.9	228.5	0.0	228.5	
16600	4600	20.2	207.9	228.1	0.0	228.1	
16600	4625	8.8	207.9	216.7	0.0	216.7	Baker fm? Rocky
16600	4650	10.4	207.9	218.3	0.0	218.3	
16600	4675	-6.9	207.9	201.0	0.0	201.0	
16600	4700	-1.8	207.9	206.1	0.0	206.1	
16600	4725	-14.8	207.9	193.1	0.0	193.1	
16600	4750	-14.3	207.9	193.6	0.0	193.6	fluct slightly
16600	4775	-24.5	207.9	183.4	0.0	183.4	lighty color, rocky (Baker)
16600	4800	-23.9	207.9	184.0	0.0	184.0	light color (Baker)
16400E, 4000N							
16400	4000	-32.0	207.9	175.9	0.0	175.9	
16400	3975	0.9	175.9	176.8	0.0	176.8	
16400	3950	-9.6	175.9	166.3	0.0	166.3	
16400	3925	-2.7	175.9	173.2	0.0	173.2	
16400	3900	-1.3	175.9	174.6	0.0	174.6	
16400	3875	-5.3	175.9	170.6	0.0	170.6	
16400	3850	-12.0	175.9	163.9	0.0	163.9	
16400	3825	-19.8	175.9	156.1	0.0	156.1	
16400	3800	-13.9	175.9	162.0	0.0	162.0	
16400	3775	-41.3	175.9	134.6	0.0	134.6	
16400	3750	-47.3	175.9	128.6	0.0	128.6	
16400	3725	-90.8	175.9	85.1	0.0	85.1	
16400	3700	-76.2	175.9	99.7	0.0	99.7	
16400	3675	-93.7	175.9	82.2	0.0	82.2	
16400	3650	-108.8	175.9	67.1	0.0	67.1	
16400	3625	-76.3	175.9	99.6	0.0	99.6	
16400	3600	-96.5	175.9	79.4	0.0	79.4	
16400	3575	-99.3	175.9	76.6	0.0	76.6	
16400	3550	-93.2	175.9	82.7	0.0	82.7	
16400	3525	-81.0	175.9	94.9	0.0	94.9	
16400	3500	-89.6	175.9	86.3	0.0	86.3	
16400	3475	-91.5	175.9	84.4	0.0	84.4	
16400	3450	-106.5	175.9	69.4	0.0	69.4	
16400	3425	-100.9	175.9	75.0	0.0	75.0	
16400	3400	-93.4	175.9	82.5	0.0	82.5	
16400	3350	-106.8	175.9	69.1	0.0	69.1	
16400	3300	-146.2	175.9	29.7	0.0	29.7	
16400	3275	-240.0	175.9	-64.1	0.0	-64.1	
16400	3250	-420.7	175.9	-244.8	0.0	-244.8	
16400	3225	-591.7	175.9	-415.8	0.0	-415.8	
16400	3200	-523.0	175.9	-347.1	0.0	-347.1	
16400	3175	-298.2	175.9	-122.3	0.0	-122.3	hyd pit about 150' to south
16200	4000	-58.0	207.9	149.9	0.0	149.9	
16000	4000	-37.5	207.9	170.4	0.0	170.4	
16000E, 4000N							
16000	3950	-1.0	170.4	169.4	0.0	169.4	
16000	3900	19.4	170.4	189.8	0.0	189.8	
16000	3850	-7.7	170.4	162.7	0.0	162.7	
16000	3800	-36.8	170.4	133.6	0.0	133.6	
16000	3750	-13.2	170.4	157.2	0.0	157.2	
16000	3700	-134.4	170.4	36.0	0.0	36.0	
16000	3675	-242.5	170.4	-72.1	0.0	-72.1	
16000	3650	-101.1	170.4	69.3	0.0	69.3	
16000	3625	-91.1	170.4	79.3	0.0	79.3	
16000	3600	-103.0	170.4	67.4	0.0	67.4	
16000	3575	-118.1	170.4	52.3	0.0	52.3	
16000	3550	-167.1	170.4	3.3	0.0	3.3	
16000	3525	-137.1	170.4	33.3	0.0	33.3	
16000	3500	-220.5	170.4	-50.1	0.0	-50.1	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
16000	3475	-276.0	170.4	-105.6	0.0	-105.6	
16000	3450	-315.1	170.4	-144.7	0.0	-144.7	
16000	3425	-423.0	170.4	-252.6	0.0	-252.6	
16000	3400	-499.0	170.4	-328.6	0.0	-328.6	
16000	3375	-590.5	170.4	-420.1	0.0	-420.1	
16000	3350	-635.0	170.4	-464.6	0.0	-464.6	
16000	3325	-665.5	170.4	-495.1	0.0	-495.1	
16000	3300	-677.5	170.4	-507.1	0.0	-507.1	BC Vein/ graphitic anomaly??
16000	3275	-738.5	170.4	-568.1	0.0	-568.1	BC Vein/ graphitic anomaly??
16000	3250	-808.0	170.4	-637.6	0.0	-637.6	BC Vein/ graphitic anomaly??
16000	3225	-862.0	170.4	-691.6	0.0	-691.6	BC Vein/ graphitic anomaly??
16000	3200	-885.5	170.4	-715.1	0.0	-715.1	
15805	3992	-1.6	207.9	160.5	0.0	160.5	
15600	4000	-8.3	170.4	162.1	0.0	162.1	
15600	3975	-7.0	162.1	155.1	0.0	155.1	4:40 PM
15600	3950	-9.5	162.1	152.6	0.0	152.6	
15600	3925	-2.8	162.1	159.3	0.0	159.3	
15600	3900	-8.4	162.1	153.7	0.0	153.7	
15600	3875	-29.7	162.1	132.4	0.0	132.4	
15600	3850	-11.7	162.1	150.4	0.0	150.4	
15600	3825	-25.3	162.1	136.8	0.0	136.8	
15600	3800	-28.6	162.1	133.5	0.0	133.5	
15600	3775	-33.2	162.1	128.9	0.0	128.9	
15600	3750	-45.2	162.1	115.9	0.0	115.9	
15600	3725	-29.0	162.1	133.1	0.0	133.1	
15600	3700	-70.0	162.1	92.1	0.0	92.1	
15600	3675	-89.6	162.1	72.5	0.0	72.5	
15600	3650	-99.3	162.1	62.8	0.0	62.8	
15600	3625	-152.0	162.1	10.1	0.0	10.1	
15600	3600	-238.3	162.1	-76.2	0.0	-76.2	
15600	3575	-444.0	162.1	-281.9	0.0	-281.9	
15600	3550	-502.0	162.1	-339.9	0.0	-339.9	
15600	3525	-599.0	162.1	-436.9	0.0	-436.9	
15600	3500	-513.0	162.1	-350.9	0.0	-350.9	
15600	3475	-379.8	162.1	-217.7	0.0	-217.7	
15600	3450	-377.5	162.1	-215.4	0.0	-215.4	
15600	3425	-521.5	162.1	-359.4	0.0	-359.4	5:14 PM
15600	3400	-525.0	162.1	-362.9	0.0	-362.9	
15600	3375	-519.0	162.1	-356.9	0.0	-356.9	
15600	3350	-482.0	162.1	-319.9	0.0	-319.9	
15600	3325	-527.0	162.1	-364.9	0.0	-364.9	
15600	3300	-539.0	162.1	-376.9	0.0	-376.9	
15600	3275	-568.0	162.1	-405.9	0.0	-405.9	
15600	3250	-588.0	162.1	-425.9	0.0	-425.9	
15600	3225	-582.0	162.1	-419.9	0.0	-419.9	
15600	3200	-561.0	162.1	-398.9	0.0	-398.9	very edge of pit
15406	4000	-30.3	162.1	131.8	0.0	131.8	
15194	4000	-291.5	162.1	-129.4	0.0	-129.4	
15000	4000	-286.7	162.1	-124.6	0.0	-124.6	taken in linear old dirt mound from an old trench that is parallel to mine grid N/S
15000	4025	-26.0	-124.6	-150.6	0.0	-150.6	
15000	4050	-66.5	-124.6	-191.2	0.0	-191.2	
15000	4075	-164.6	-124.6	-279.2	0.0	-279.2	
15000	4100	-180.9	-124.6	-305.5	0.0	-305.5	
15000	4125	-183.8	-124.6	-308.4	0.0	-308.4	
15000	4150	-118.8	-124.6	-243.4	0.0	-243.4	
15000	4175	-34.4	-124.6	-159.0	0.0	-159.0	
15000	4200	-8.5	-124.6	-133.1	0.0	-133.1	
15000	4225	-32.2	-124.6	-156.8	0.0	-156.8	
15000	4250	6.5	-124.6	-118.1	0.0	-118.1	
15000	4275	46.5	-124.6	-78.1	0.0	-78.1	
15000	4300	119.5	-124.6	-5.1	0.0	-5.1	
15000	4325	155.7	-124.6	31.1	0.0	31.1	
15000	4350	173.0	-124.6	48.4	0.0	48.4	
15000	4375	183.0	-124.6	58.4	0.0	58.4	
15000	4400	207.5	-124.6	82.9	0.0	82.9	

15-Sep

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
15000	4425	222.7	-124.6	98.1	0.0	98.1	marshy
15000	4450	224.8	-124.6	100.2	0.0	100.2	marshy
15000	4475	209.6	-124.6	85.0	0.0	85.0	
			-124.6				no station: in dirt pile on side of road
15000	4525	220.8	-124.6	96.2	0.0	96.2	on road
15000	4550	217.5	-124.6	92.9	0.0	92.9	
15000	4575	226.7	-124.6	102.1	0.0	102.1	
15000	4600	246.0	-124.6	121.4	0.0	121.4	
15000	4625	245.4	-124.6	120.8	0.0	120.8	
15000	4650	252.5	-124.6	127.9	0.0	127.9	
15000	4675	243.5	-124.6	118.9	0.0	118.9	
15000	4700	246.1	-124.6	121.5	0.0	121.5	
15000	4725	234.0	-124.6	109.4	0.0	109.4	
15000	4750	268.9	-124.6	144.3	0.0	144.3	12:30 PM
15000	4775	248.6	-124.6	124.0	0.0	124.0	
15000	4800	285.9	-124.6	161.3	0.0	161.3	
15000	3975	-51.0	-124.6	-175.6	0.0	-175.6	
15000	3950	-53.5	-124.6	-178.1	0.0	-178.1	
15000	3925	53.4	-124.6	-71.2	0.0	-71.2	
15000	3900	170.3	-124.6	45.7	0.0	45.7	
15000	3875	167.1	-124.6	42.5	0.0	42.5	
15000	3850	194.4	-124.6	69.8	0.0	69.8	
15000	3825	188.4	-124.6	63.8	0.0	63.8	
15000	3800	189.7	-124.6	65.1	0.0	65.1	
15000	3775	146.4	-124.6	21.8	0.0	21.8	
15000	3750	144.4	-124.6	19.8	0.0	19.8	
15000	3725	127.2	-124.6	2.6	0.0	2.6	
15000	3700	127.3	-124.6	2.7	0.0	2.7	
15000	3675	78.8	-124.6	-47.8	0.0	-47.8	
15000	3650	6.9	-124.6	-117.7	0.0	-117.7	
15000	3625	-75.5	-124.6	-200.1	0.0	-200.1	
15000	3600	-337.6	-124.6	-462.2	0.0	-462.2	
15000	3575	-495.0	-124.6	-619.6	0.0	-619.6	
15000	3550	-472.0	-124.6	-596.6	0.0	-596.6	
15000	3525	-342.0	-124.6	-466.6	0.0	-466.6	edge of hydraulicked pit
14800	4000	96.9	-124.6	-27.7	0.0	-27.7	
14600	4000	-76.7	-124.6	-201.3	0.0	-201.3	
14400	4000	-148.2	-124.6	-272.8	0.0	-272.8	
14400	4025	-86.0	-272.8	-358.8	0.0	-358.8	
14400	4050	-142.9	-272.8	-415.7	0.0	-415.7	
14400	4075	-196.7	-272.8	-469.5	0.0	-469.5	
14400	4100	-208.8	-272.8	-481.6	0.0	-481.6	
14400	4125	-295.4	-272.8	-568.2	0.0	-568.2	
14400	4150	-330.2	-272.8	-603.0	0.0	-603.0	
14400	4175	-399.2	-272.8	-672.0	0.0	-672.0	
14400	4200	-405.0	-272.8	-677.8	0.0	-677.8	
14400	4225	-427.0	-272.8	-699.8	0.0	-699.8	
14400	4250	-360.8	-272.8	-633.6	0.0	-633.6	
14400	4275	-263.5	-272.8	-536.3	0.0	-536.3	
14400	4300	-157.5	-272.8	-430.3	0.0	-430.3	
14400	4325	-11.0	-272.8	-283.8	0.0	-283.8	
14400	4350	52.0	-272.8	-220.8	0.0	-220.8	
14400	4375	105.8	-272.8	-167.0	0.0	-167.0	
14400	4400	-183.4	-272.8	-89.4	0.0	-89.4	
14400	4425	-232.8	-272.8	-40.0	0.0	-40.0	
14400	4450	268.9	-272.8	-3.9	0.0	-3.9	
14400	4475	285.6	-272.8	12.8	0.0	12.8	
14400	4500	311.0	-272.8	38.2	0.0	38.2	
14400	4525	321.8	-272.8	49.0	0.0	49.0	
14400	4550	332.9	-272.8	60.1	0.0	60.1	
14400	4575	372.5	-272.8	99.7	0.0	99.7	
14400	4600	393.8	-272.8	121.0	0.0	121.0	
14400	4625	408.0	-272.8	135.2	0.0	135.2	
14400	4650	404.0	-272.8	131.2	0.0	131.2	
14400	4675	404.0	-272.8	131.2	0.0	131.2	
14400	4700	413.0	-272.8	140.2	0.0	140.2	

CONTROL STATION

	SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
	EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
14400	4725		410.0	-272.8	137.2	0.0	137.2	
	4750		410.0	-272.8	137.2	0.0	137.2	
	4775		416.0	-272.8	143.2	0.0	143.2	
	4800		421.0	-272.8	148.2	0.0	148.2	
14600E, 4000N			-201.3					
	14600	4025	-113.4	-201.3	-314.7	0.0	-314.7	
	14600	4050	-191.0	-201.3	-392.3	0.0	-392.3	
	14600	4075	-239.6	-201.3	-440.9	0.0	-440.9	
	14600	4100	-239.3	-201.3	-440.6	0.0	-440.6	
	14600	4125	-278.6	-201.3	-479.9	0.0	-479.9	
	14600	4150	-335.8	-201.3	-537.1	0.0	-537.1	
	14600	4175	-323.7	-201.3	-525.0	0.0	-525.0	
	14600	4200	-358.9	-201.3	-560.2	0.0	-560.2	
	14600	4225	-433.0	-201.3	-634.3	0.0	-634.3	
	14600	4250	-395.7	-201.3	-597.0	0.0	-597.0	by old telegraph road
	14600	4275	-301.9	-201.3	-503.2	0.0	-503.2	
	14600	4300	-150.9	-201.3	-352.2	0.0	-352.2	
	14600	4325	-2.3	-201.3	-203.6	0.0	-203.6	
	14600	4350	117.2	-201.3	-84.1	0.0	-84.1	
	14600	4375	186.6	-201.3	-14.7	0.0	-14.7	
	14600	4400	224.2	-201.3	22.9	0.0	22.9	
	14600	4425	262.3	-201.3	61.0	0.0	61.0	
	14600	4450	290.9	-201.3	89.6	0.0	89.6	
	14600	4475	301.6	-201.3	100.3	0.0	100.3	
	14600	4500	319.7	-201.3	118.4	0.0	118.4	
	14600	4525	303.4	-201.3	102.1	0.0	102.1	
	14600	4550	317.4	-201.3	116.1	0.0	116.1	
	14600	4575	335.1	-201.3	133.8	0.0	133.8	
	14600	4600	339.7	-201.3	138.4	0.0	138.4	
	14600	4625	353.2	-201.3	151.9	0.0	151.9	
	14600	4650	365.9	-201.3	164.6	0.0	164.6	
	14600	4675	371.2	-201.3	169.9	0.0	169.9	on the road
	14600	4700						
	14600	4725						
	14600	4750						
	14600	4775	363.3	-201.3	162.0	0.0	162.0	
	14600	4800						
	14600	3975	39.0	-201.3	-162.3	0.0	-162.3	
	14600	3950	105.9	-201.3	-95.4	0.0	-95.4	edge of pit
14800E, 4000N			-27.7					
	14800	3975	8.5	-27.7	-19.2	0.0	-19.2	
	14800	3954	22.9	-27.7	-4.8	0.0	-4.8	creek
	14800	3925	26.2	-27.7	-1.5	0.0	-1.5	creek
	14800	3900	21.3	-27.7	-6.4	0.0	-6.4	creek
	14800	3875	32.5	-27.7	4.8	0.0	4.8	
	14800	3850	16.5	-27.7	-11.2	0.0	-11.2	
	14800	3825	-18.4	-27.7	-46.1	0.0	-46.1	
	14800	3800	10.9	-27.7	-16.8	0.0	-16.8	
	14800	3775	6.8	-27.7	-20.9	0.0	-20.9	
	14800	3750	38.6	-27.7	10.9	0.0	10.9	
	14800	3725	35.4	-27.7	7.7	0.0	7.7	
	14800	3700	53.8	-27.7	26.1	0.0	26.1	edge of pit
Mon Sept 17 14800 E, 4000N			-27.7					
	14800	4025	-33.1	-27.7	-60.8	0.0	-60.8	
	14800	4050	-69.9	-27.7	-97.6	0.0	-97.6	
	14800	4075	-116.7	-27.7	-144.4	0.0	-144.4	rocky
	14800	4100	-241.9	-27.7	-269.6	0.0	-269.6	orangy brown rock
	14800	4125	-235.8	-27.7	-263.5	0.0	-263.5	
	14800	4150	-200.8	-27.7	-228.5	0.0	-228.5	
	14800	4175	-197.7	-27.7	-225.4	0.0	-225.4	
	14800	4200	-245.3	-27.7	-273.0	0.0	-273.0	
	14800	4225	-304.0	-27.7	-331.7	0.0	-331.7	very rocky. Old stream bed?

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
14800	4275	-149.6	-27.7	-177.2	0.0	-177.2	
14800	4300	-72.2	-27.7	-99.9	0.0	-99.9	
14800	4325	-18.4	-27.7	-44.1	0.0	-44.1	
14800	4350	35.6	-27.7	7.9	0.0	7.9	
14800	4375	70.2	-27.7	42.5	0.0	42.5	
14800	4400	83.7	-27.7	56.0	0.0	56.0	
14800	4425	95.7	-27.7	68.0	0.0	68.0	
14800	4450	93.8	-27.7	66.1	0.0	66.1	marsh. Hole filling quickly with water
14800	4475	121.2	-27.7	93.5	0.0	93.5	18' wise old stream? Cave in? trench? Strikes downhill
14800	4500	131.3	-27.7	103.6	0.0	103.6	
14800	4525	129.9	-27.7	102.2	0.0	102.2	
14800	4550	133.9	-27.7	106.2	0.0	106.2	
14800	4575	154.6	-27.7	126.9	0.0	126.9	north side of the road, on the road
14800	4600	163.8	-27.7	136.1	0.0	136.1	black wet peat
14800	4625	166.1	-27.7	138.4	0.0	138.4	black wet peat
14800	4650	168.4	-27.7	140.7	0.0	140.7	black wet peat
14800	4675	176.2	-27.7	148.5	0.0	148.5	black wet peat
14800	4700	179.1	-27.7	151.4	0.0	151.4	good hole, no peat
14800	4725	178.6	-27.7	150.9	0.0	150.9	
14800	4750	179.1	-27.7	151.4	0.0	151.4	
14800	4775	183.2	-27.7	155.5	0.0	155.5	
14800	4800	173.6	-27.7	145.9	0.0	145.9	
15194E, 4000N		-129.4					
15200	3975	-61.0	-129.4	-190.4	0.0	-190.4	
15200	3950	-60.8	-129.4	-190.2	0.0	-190.2	
15200	3925	-1.2	-129.4	-130.6	0.0	-130.6	
15200	3900	68.3	-129.4	-61.1	0.0	-61.1	
15200	3875	167.0	-129.4	37.6	0.0	37.6	
15200	3850	207.4	-129.4	78.0	0.0	78.0	
15200	3825	201.5	-129.4	72.1	0.0	72.1	lots of willow roots
15200	3800	212.7	-129.4	83.3	0.0	83.3	
15200	3775	198.9	-129.4	69.5	0.0	69.5	
15200	3750	192.9	-129.4	63.5	0.0	63.5	
15200	3725	162.8	-129.4	33.4	0.0	33.4	
15200	3700	140.8	-129.4	11.4	0.0	11.4	
15200	3675	107.8	-129.4	-21.6	0.0	-21.6	
15200	3650	90.9	-129.4	-38.5	0.0	-38.5	
15200	3625	-15.2	-129.4	-144.6	0.0	-144.6	
15200	3560	-505.0	-129.4	-634.4	0.0	-634.4	shaley soil and shale subcrop from here to next measured station
15200	3475	-368.4	-129.4	-497.8	0.0	-497.8	
15200	3450	-442.0	-129.4	-571.4	0.0	-571.4	gravelly hole
15200	3425	-249.8	-129.4	-379.2	0.0	-379.2	clay soil
15200	3400	-141.3	-129.4	-270.7	0.0	-270.7	
15200	3375	-157.3	-129.4	-286.7	0.0	-286.7	edge of pit
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15194	4000		-129.4	-129.4			
15200	4025	115.3	-129.4	-14.1	0.0	-14.1	
15200	4050	101.0	-129.4	-28.4	0.0	-28.4	
15200	4075	42.3	-129.4	-87.1	0.0	-87.1	
15200	4100	-39.5	-129.4	-168.9	0.0	-168.9	
15200	4125	-119.1	-129.4	-248.5	0.0	-248.5	
15200	4150	-51.4	-129.4	-180.8	0.0	-180.8	
15200	4175	27.6	-129.4	-101.8	0.0	-101.8	
15200	4200	72.4	-129.4	-57.0	0.0	-57.0	
15200	4225	115.5	-129.4	-13.9	0.0	-13.9	
15200	4250	128.1	-129.4	-1.3	0.0	-1.3	
15200	4275	141.0	-129.4	11.6	0.0	11.6	
15200	4300	213.3	-129.4	83.9	0.0	83.9	
15200	4325	244.5	-129.4	115.1	0.0	115.1	
15200	4350	259.0	-129.4	129.6	0.0	129.6	rooty
15200	4375	260.2	-129.4	130.8	0.0	130.8	south side of road
15200	4400	248.0	-129.4	118.6	0.0	118.6	north side of road in sand > gravel road fill
15200	4425	225.8	-129.4	96.4	0.0	96.4	
15200	4450	210.5	-129.4	81.1	0.0	81.1	
15200	4475	162.6	-129.4	53.2	0.0	53.2	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
15200	4500	142.7	-129.4	13.3	0.0	13.3	
15200	4525	93.9	-129.4	-35.6	0.0	-35.6	
15200	4550	121.7	-129.4	-7.7	0.0	-7.7	
15200	4575	152.9	-129.4	23.5	0.0	23.5	
15200	4600	181.8	-129.4	52.4	0.0	52.4	
15200	4625	187.1	-129.4	57.7	0.0	57.7	
15200	4650	189.0	-129.4	59.6	0.0	59.6	
15200	4675	209.7	-129.4	80.3	0.0	80.3	
15200	4700	230.4	-129.4	101.0	0.0	101.0	gravelly
15200	4725	238.2	-129.4	108.8	0.0	108.8	
15200	4750	250.2	-129.4	120.8	0.0	120.8	rocks and roots on hole
15200	4775	244.0	-129.4	114.6	0.0	114.6	
15406	4000			131.8			
15400	4025	-3.0	131.8	128.8	0.0	128.8	
15400	4050	-9.5	131.8	122.3	0.0	122.3	
15400	4075	-15.8	131.8	116.0	0.0	116.0	
15400	4100	-32.2	131.8	99.6	0.0	99.6	
15400	4125	-7.0	131.8	124.8	0.0	124.8	
15400	4150	10.8	131.8	142.6	0.0	142.6	
15400	4175	10.6	131.8	142.4	0.0	142.4	
15400	4200	8.1	131.8	139.9	0.0	139.9	
15400	4225	12.6	131.8	144.4	0.0	144.4	
15400	4250	19.6	131.8	151.4	0.0	151.4	fine gravel
15400	4275	17.2	131.8	149.0	0.0	149.0	
15400	4300	18.3	131.8	150.1	0.0	150.1	south side of road
15400	4325	19.2	131.8	151.0	0.0	151.0	north side of road
15400	4350	4.0	131.8	135.8	0.0	135.8	
15400	4375	4.5	131.8	136.3	0.0	136.3	
15400	4400	-2.6	131.8	129.2	0.0	129.2	
15400	4425	-17.7	131.8	114.1	0.0	114.1	
15400	4450	-23.1	131.8	108.7	0.0	108.7	
15400	4475	-36.1	131.8	95.7	0.0	95.7	
15400	4500	-59.4	131.8	72.5	0.0	72.5	
15400	4525	-85.9	131.8	45.9	0.0	45.9	
15400	4550	-88.5	131.8	43.3	0.0	43.3	
15400	4575	-92.6	131.8	39.2	0.0	39.2	
15400	4600	-67.2	131.8	64.6	0.0	64.6	
15400	4625	-67.2	131.8	64.6	0.0	64.6	
15400	4650	-64.1	131.8	67.8	0.0	67.8	
15400	4675	-45.3	131.8	86.6	0.0	86.6	
15400	4700	-46.6	131.8	85.3	0.0	85.3	
15400	4725	-46.2	131.8	85.6	0.0	85.6	
15400	4750	-31.1	131.8	100.8	0.0	100.8	
15400	4775	-34.8	131.8	97.0	0.0	97.0	
15400	4800	-38.5	131.8	93.3	0.0	93.3	
15400	3975	-18.8	131.8	113.0	0.0	113.0	on north side of old telegraph road
15400	3950	-28.6	131.8	103.2	0.0	103.2	
15400	3925	-36.5	131.8	95.3	0.0	95.3	
15400	3900	-39.1	131.8	92.7	0.0	92.7	
15400	3875	-49.3	131.8	82.5	0.0	82.5	
15400	3850	-39.5	131.8	92.3	0.0	92.3	
15400	3825	-43.2	131.8	88.6	0.0	88.6	
15400	3800	-47.8	131.8	84.0	0.0	84.0	
15400	3775	-38.0	131.8	93.8	0.0	93.8	
15400	3750	-54.6	131.8	77.2	0.0	77.2	
15400	3725	-81.5	131.8	50.3	0.0	50.3	
15400	3700	-102.5	131.8	29.3	0.0	29.3	
15400	3675	-125.4	131.8	6.4	0.0	6.4	
15400	3650	-183.2	131.8	-51.4	0.0	-51.4	
15400	3625	-339.4	131.8	-207.6	0.0	-207.6	orange weathered quartz hole. BC Vein structure??
15400	3600	-674.0	131.8	-542.2	0.0	-542.2	argillite > quartz. BC Vein structure??
15400	3575	-686.0	131.8	-554.2	0.0	-554.2	clean hole
15400	3550	-599.0	131.8	-487.2	0.0	-487.2	lots argillite. BC Vein structure??
15400	3525	-499.0	131.8	-367.2	0.0	-367.2	clean hole
15400	3500	-427.0	131.8	-285.2	0.0	-285.2	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
15400	3475	-416.0	131.8	-284.2	0.0	-284.2	soil has changed to a fine gr light brown colored soil with phyllitic rocks mag phyll??
15400	3450	-498.0	131.8	-366.2	0.0	-366.2	
15400	3425	-488.0	131.8	-356.2	0.0	-356.2	
15400	3400	-525.0	131.8	-393.2	0.0	-393.2	
15400	3375	-539.0	131.8	-407.2	0.0	-407.2	
15400	3350	-559.0	131.8	-427.2	0.0	-427.2	edge of hyd pit
15600	4000			162.1			
15600	4025	-13.9	162.1	148.2	0.0	148.2	
15600	4050	-18.0	162.1	144.1	0.0	144.1	
15600	4075	-13.0	162.1	149.1	0.0	149.1	
15600	4100	-12.3	162.1	149.8	0.0	149.8	
15600	4125	0.5	162.1	162.6	0.0	162.6	
15600	4150	-11.2	162.1	150.9	0.0	150.9	a bit of gravel
15600	4175	-6.9	162.1	155.2	0.0	155.2	
15600	4200	-4.4	162.1	157.7	0.0	157.7	
15600	4220	0.3	162.1	162.4	0.0	162.4	side of road
15600	4250	15.0	162.1	177.1	0.0	177.1	muddy, north side of road
15600	4275	8.3	162.1	170.4	0.0	170.4	
15600	4300	8.3	162.1	170.4	0.0	170.4	
15600	4325	11.6	162.1	173.7	0.0	173.7	
15600	4350	-5.7	162.1	156.4	0.0	156.4	
15600	4375	1.5	162.1	163.6	0.0	163.6	
15600	4400	14.4	162.1	176.5	0.0	176.5	marsh, wet
15600	4425	-5.7	162.1	156.4	0.0	156.4	
15600	4450	-9.5	162.1	152.7	0.0	152.7	
15600	4475	-38.6	162.1	123.5	0.0	123.5	
15600	4500	-52.6	162.1	109.5	0.0	109.5	
15600	4525	-64.1	162.1	98.0	0.0	98.0	
15600	4550	-100.8	162.1	61.3	0.0	61.3	
15600	4585	-210.0	162.1	-47.9	0.0	-47.9	marsh at 4575N
15600	4600	-224.7	162.1	-62.6	0.0	-62.6	
15600	4625	-181.6	162.1	0.5	0.0	0.5	
15600	4650	-85.3	162.1	76.9	0.0	76.9	
15600	4675	-72.3	162.1	89.8	0.0	89.8	
15600	4700	-78.2	162.1	83.9	0.0	83.9	
15600	4725	-81.3	162.1	80.8	0.0	80.8	gravelly
15600	4750	-37.9	162.1	124.2	0.0	124.2	
15600	4775	-71.5	162.1	90.6	0.0	90.6	
20-Sep							
15805	3992			160.5			
15800	4025	-9.7	160.5	150.8	0.0	150.8	
15800	4050	1.3	160.5	161.8	0.0	161.8	
15800	4075	-9.8	160.5	150.7	0.0	150.7	
15800	4100	3.5	160.5	164.0	0.0	164.0	
15800	4125	12.4	160.5	172.9	0.0	172.9	
15800	4150	9.6	160.5	170.1	0.0	170.1	
15800	4175	5.5	160.5	166.0	0.0	166.0	
15800	4200	21.2	160.5	181.7	0.0	181.7	
15800	4225	23.0	160.5	183.5	0.0	183.5	gravel
15800	4250	28.9	160.5	189.4	0.0	189.4	lots gravel, South side of road
15800	4275	15.6	160.5	176.1	0.0	176.1	
15800	4300	16.0	160.5	176.5	0.0	176.5	
15800	4325	7.6	160.5	168.1	0.0	168.1	
15800	4350	36.1	160.5	196.6	0.0	196.6	
15800	4375	20.1	160.5	180.6	0.0	180.6	
15800	4400	23.1	160.5	183.6	0.0	183.6	
15800	4425	19.2	160.5	179.7	0.0	179.7	
15800	4450	20.0	160.5	180.5	0.0	180.5	
15800	4475	15.2	160.5	175.7	0.0	175.7	North side of creek. Wet, marshy ground
15800	4500	3.5	160.5	164.0	0.0	164.0	
15800	4525	-20.9	160.5	139.6	0.0	139.6	
15800	4550	-48.1	160.5	112.4	0.0	112.4	
15800	4575	-136.8	160.5	23.7	0.0	23.7	
15800	4600	-473.0	160.5	-312.5	0.0	-312.5	crossed Goldfinch Fault?

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
15800	4625	-448.0	160.5	-285.5	0.0	-285.5	
15800	4650	-175.1	160.5	-14.6	0.0	-14.6	
15800	4675	-105.4	160.5	55.1	0.0	55.1	
15800	4700	-72.2	160.5	88.3	0.0	88.3	
15800	4725	-57.5	160.5	103.0	0.0	103.0	
15800	4750	-52.3	160.5	108.2	0.0	108.2	
15800	4775	-52.1	160.5	108.4	0.0	108.4	
15850	4600	-374.8	160.5	-214.3	0.0	-214.3	
15750	4600	-558.0	160.5	-397.5	0.0	-397.5	
15850	4575	-233.6	160.5	-73.1	0.0	-73.1	
15750	4575	-148.1	160.5	12.4	0.0	12.4	
15800	3975	-19.0	160.5	141.5	0.0	141.5	11:15 AM
15800	3950	-23.6	160.5	136.9	0.0	136.9	
15800	3925	-36.4	160.5	124.1	0.0	124.1	
15800	3900	-41.3	160.5	119.2	0.0	119.2	
15800	3875	-34.0	160.5	126.5	0.0	126.5	
15800	3850	-22.3	160.5	138.2	0.0	138.2	
15800	3825	-40.8	160.5	119.7	0.0	119.7	
15800	3800	-48.2	160.5	112.3	0.0	112.3	
15800	3775	-56.5	160.5	105.0	0.0	105.0	
15800	3750	-51.6	160.5	108.9	0.0	108.9	
15800	3725	-65.5	160.5	95.0	0.0	95.0	
15800	3700	-72.9	160.5	87.6	0.0	87.6	
15800	3675	-79.2	160.5	81.3	0.0	81.3	
15800	3650	-81.2	160.5	79.3	0.0	79.3	
15800	3625	-105.8	160.5	54.7	0.0	54.7	
15800	3600	-139.7	160.5	20.8	0.0	20.8	
15800	3575	-210.9	160.5	-50.4	0.0	-50.4	
15800	3550	-415.0	160.5	-254.5	0.0	-254.5	
15800	3525	-625.0	160.5	-464.5	0.0	-464.5	
15800	3500	-678.0	160.5	-517.5	0.0	-517.5	
15800	3475	-655.0	160.5	-494.5	0.0	-494.5	
15800	3450	-568.0	160.5	-407.5	0.0	-407.5	
15800	3425	-499.0	160.5	-338.5	0.0	-338.5	
15800	3400	-644.0	160.5	-483.5	0.0	-483.5	
15800	3375	-658.0	160.5	-497.5	0.0	-497.5	
15800	3350	-562.0	160.5	-401.5	0.0	-401.5	
15800	3325	-541.0	160.5	-380.5	0.0	-380.5	
15800	3300	-569.0	160.5	-408.5	0.0	-408.5	
15800	3275	-642.0	160.5	-481.5	0.0	-481.5	
15800	3250	-619.0	160.5	-458.5	0.0	-458.5	
15800	3225	-562.0	160.5	-401.5	0.0	-401.5	
15800	3200	-558.0	160.5	-397.5	0.0	-397.5	
16000	4000			170.4			
16000	4025	-13.6	170.4	156.8	0.0	156.8	
16000	4050	-5.2	170.4	165.2	0.0	165.2	
16000	4075	-21.3	170.4	149.1	0.0	149.1	
16000	4100	-1.1	170.4	169.3	0.0	169.3	
16000	4125	-0.5	170.4	169.9	0.0	169.9	
16000	4150	12.8	170.4	183.2	0.0	183.2	
16000	4175	11.4	170.4	181.8	0.0	181.8	
16000	4200	11.7	170.4	182.1	0.0	182.1	
16000	4225	11.1	170.4	181.5	0.0	181.5	
16000	4250	20.5	170.4	190.9	0.0	190.9	on road
16000	4275	21.3	170.4	191.7	0.0	191.7	
16000	4300	28.8	170.4	199.2	0.0	199.2	
16000	4325	23.0	170.4	193.4	0.0	193.4	
16000	4350	28.5	170.4	198.9	0.0	198.9	
16000	4375	32.9	170.4	203.3	0.0	203.3	
16000	4400	40.8	170.4	211.2	0.0	211.2	
16000	4425	31.6	170.4	202.0	0.0	202.0	
16000	4450	38.6	170.4	209.0	0.0	209.0	
16000	4475	30.0	170.4	200.4	0.0	200.4	
16000	4500	36.1	170.4	206.5	0.0	206.5	
16000	4525	19.2	170.4	189.6	0.0	189.6	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
16000	4550	12.1	170.4	182.5	0.0	182.5	
16000	4575	-26.0	170.4	144.4	0.0	144.4	
16000	4600	-66.5	170.4	103.9	0.0	103.9	
16000	4625	-214.1	170.4	-43.7	0.0	-43.7	
16000	4650	-144.7	170.4	25.7	0.0	25.7	
16000	4675	-100.8	170.4	69.6	0.0	69.6	lots quartz here. Dk grey rock with 1/2" qtz stringer, orange weath
16000	4700	-70.7	170.4	99.7	0.0	99.7	
16000	4725	-65.9	170.4	104.5	0.0	104.5	more qtz, red weath.
16000	4750	-47.7	170.4	122.7	0.0	122.7	on old road
16000	4775	-40.5	170.4	129.9	0.0	129.9	on old road
16000	4800	-39.8	170.4	130.6	0.0	130.6	on old road
16200	4000		149.9	149.9			
16200	4025	-8.1	149.9	141.8	0.0	141.8	
16200	4050	-4.3	149.9	145.6	0.0	145.6	
16200	4075	2.5	149.9	152.4	0.0	152.4	
16200	4100	7.1	149.9	157.0	0.0	157.0	
16200	4125	-2.3	149.9	147.6	0.0	147.6	
16200	4150	-6.2	149.9	143.7	0.0	143.7	
16200	4175	17.6	149.9	167.5	0.0	167.5	
16200	4200	27.1	149.9	177.0	0.0	177.0	
16200	4225	23.3	149.9	173.2	0.0	173.2	
16200	4250	34.1	149.9	184.0	0.0	184.0	
16200	4275	39.0	149.9	188.9	0.0	188.9	
16200	4300	40.9	149.9	190.8	0.0	190.8	
16200	4325	33.6	149.9	183.5	0.0	183.5	
16200	4350	53.9	149.9	203.8	0.0	203.8	on road
16200	4375	52.1	149.9	202.0	0.0	202.0	
16200	4400	60.4	149.9	210.3	0.0	210.3	
16200	4425	50.3	149.9	200.2	0.0	200.2	
16200	4450	59.6	149.9	209.5	0.0	209.5	
16200	4475	50.9	149.9	200.8	0.0	200.8	
16200	4525	57.0	149.9	206.9	0.0	206.9	
16200	4550	48.9	149.9	198.8	0.0	198.8	
16200	4575	35.0	149.9	184.9	0.0	184.9	
16200	4600	12.2	149.9	162.1	0.0	162.1	
16200	4625	-153.0	149.9	-3.1	0.0	-3.1	
16200	4650	-188.3	149.9	-38.4	0.0	-38.4	
16200	4675	-112.4	149.9	37.5	0.0	37.5	
16200	4700	-69.0	149.9	80.9	0.0	80.9	subcropping of bluegrey silicified rock with quartz and disseminated pyrite
16200	4725	-54.8	149.9	95.1	0.0	95.1	subcropping of bluegrey silicified rock with quartz and disseminated pyrite
16200	4750	-56.2	149.9	94.7	0.0	94.7	subcropping of bluegrey silicified rock with quartz and disseminated pyrite
16200	4775	-47.7	149.9	102.2	0.0	102.2	subcropping of bluegrey silicified rock with quartz and disseminated pyrite
16200	3975	-7.8	149.9	142.1	0.0	142.1	
16200	3950	-2.5	149.9	147.4	0.0	147.4	
16200	3925	-18.4	149.9	131.5	0.0	131.5	
16200	3900	-6.4	149.9	143.5	0.0	143.5	
16200	3875	-21.8	149.9	128.1	0.0	128.1	
16200	3850	-13.7	149.9	136.2	0.0	136.2	
16200	3825	-22.1	149.9	127.8	0.0	127.8	
16200	3800	-22.5	149.9	127.4	0.0	127.4	
16200	3775	-52.3	149.9	97.6	0.0	97.6	
16200	3750	-83.9	149.9	66.0	0.0	66.0	
16200	3725	-136.5	149.9	13.4	0.0	13.4	
16200	3675	-181.2	149.9	-31.3	0.0	-31.3	
16200	3650	-154.3	149.9	-4.4	0.0	-4.4	on road
16200	3625	-163.4	149.9	-13.5	0.0	-13.5	
16200	3600	-126.3	149.9	23.6	0.0	23.6	
16200	3575	-114.9	149.9	35.0	0.0	35.0	
16200	3550	-93.8	149.9	56.1	0.0	56.1	
16200	3525	-105.0	149.9	44.9	0.0	44.9	
16200	3500	-82.8	149.9	57.1	0.0	57.1	
16200	3475	-107.6	149.9	42.3	0.0	42.3	
16200	3450	-96.9	149.9	53.0	0.0	53.0	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
16200	3425	-106.7	149.9	43.2	0.0	43.2	
16200	3400	-101.0	149.9	48.9	0.0	48.9	
16200	3375	-118.6	149.9	31.3	0.0	31.3	
16200	3350	-133.6	149.9	16.3	0.0	16.3	
16200	3325	-156.9	149.9	-7.0	0.0	-7.0	
16200	3300	-165.5	149.9	-15.6	0.0	-15.6	
16200	3275	-187.3	149.9	-37.4	0.0	-37.4	
16200	3250	-167.2	149.9	-17.3	0.0	-17.3	
16200	3225	-173.6	149.9	-23.7	0.0	-23.7	
16200	3200	-207.5	149.9	-57.6	0.0	-57.6	
16400	4000	-32.0	207.9	175.9	0.0	175.9	
16400	4025	-11.5	175.9	164.4	0.0	164.4	
16400	4050	-1.4	175.9	174.5	0.0	174.5	
16400	4075	-4.6	175.9	171.3	0.0	171.3	
16400	4100	2.1	175.9	178.0	0.0	178.0	
			175.9				marsh
16400	4150	17.6	175.9	193.5	0.0	193.5	
16400	4175	14.4	175.9	190.3	0.0	190.3	
16400	4200	18.4	175.9	194.3	0.0	194.3	
16400	4225	-23.0	175.9	152.9	0.0	152.9	
16400	4250	16.8	175.9	192.7	0.0	192.7	
16400	4275	20.1	175.9	196.0	0.0	196.0	
16400	4300	35.9	175.9	211.8	0.0	211.8	
16400	4325	29.2	175.9	205.1	0.0	205.1	
16400	4350	39.7	175.9	215.6	0.0	215.6	
16400	4375	28.4	175.9	204.3	0.0	204.3	south side of road
16400	4400	46.8	175.9	222.7	0.0	222.7	north side of road
16400	4425	39.0	175.9	214.9	0.0	214.9	
16400	4450	45.5	175.9	221.4	0.0	221.4	
16400	4475	41.5	175.9	217.4	0.0	217.4	
16400	4500	30.6	175.9	206.5	0.0	206.5	
16400	4525	45.8	175.9	221.7	0.0	221.7	
16400	4550	48.1	175.9	224.0	0.0	224.0	
16400	4575	32.4	175.9	208.3	0.0	208.3	
16400	4600	28.2	175.9	204.1	0.0	204.1	
16400	4625	0.7	175.9	176.6	0.0	176.6	
16400	4650	-83.4	175.9	92.5	0.0	92.5	
16400	4675	-354.6	175.9	-178.7	0.0	-178.7	
16400	4700	-124.7	175.9	51.2	0.0	51.2	
16400	4725	-59.5	175.9	116.4	0.0	116.4	
16400	4750	-57.3	175.9	118.6	0.0	118.6	
16400	4775	-35.5	175.9	140.4	0.0	140.4	
16400	4800	-25.1	175.9	150.8	0.0	150.8	
21-Sep							
16600	4200		207.9	207.9			
16600	4225	-13.9	207.9	194.0	0.0	194.0	
16600	4250	-13.1	207.9	194.8	0.0	194.8	
16600	4332	9.4	207.9	217.3	0.0	217.3	
16600	4350	-15.3	207.9	192.6	0.0	192.6	
16600	4375	-10.8	207.9	197.1	0.0	197.1	
16600	4400	-14.9	207.9	193.0	0.0	193.0	
16600	4425	-22.7	207.9	185.2	0.0	185.2	
16600	4450	2.9	207.9	210.8	0.0	210.8	
16600	4475	8.6	207.9	216.5	0.0	216.5	
16600	4500	15.6	207.9	223.5	0.0	223.5	
16600	4525	4.8	207.9	212.7	0.0	212.7	
16600	4550	9.2	207.9	217.1	0.0	217.1	
16600	4575	20.6	207.9	228.5	0.0	228.5	
16600	4600	20.2	207.9	228.1	0.0	228.1	
16600	4625	8.8	207.9	216.7	0.0	216.7	
16600	4650	10.4	207.9	218.3	0.0	218.3	
16600	4675	-6.9	207.9	201.0	0.0	201.0	
16600	4700	-1.8	207.9	206.1	0.0	206.1	
16600	4725	-14.8	207.9	193.1	0.0	193.1	
16600	4750	-14.3	207.9	193.6	0.0	193.6	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
16600	4775	-24.5	207.9	183.4	0.0	183.4	
16600	4800	-23.9	207.9	184.0	0.0	184.0	
16600	4825	-37.0	207.9	170.9	0.0	170.9	very rocky
16600	4850	-47.9	207.9	160.1	0.0	160.1	black shale, very rocky, little soil
16600	4875	-56.1	207.9	151.8	0.0	151.8	good hole
16600	4900	-65.6	207.9	142.3	0.0	142.3	10:22 AM
16600	4925	-68.5	207.9	139.4	0.0	139.4	
16600	4950	-42.9	207.9	165.0	0.0	165.0	
16600	4975	-49.5	207.9	158.4	0.0	158.4	rocky
16600	5000	-43.8	207.9	164.1	0.0	164.1	rocky
18400	2800			-99.9			
18400	2825	-28.2	-99.9	-128.1	0.0	-128.1	in sump
18400	2850	-77.0	-99.9	-176.9	0.0	-176.9	on south side of road
18400	2875	-346.2	-99.9	-446.1	0.0	-446.1	north side of road on embankment
18400	2900	-514.0	-99.9	-613.9	0.0	-613.9	
18400	2925	-631.0	-99.9	-730.9	0.0	-730.9	
18400	2950	-636.0	-99.9	-735.9	0.0	-735.9	
18400	2975	-499.0	-99.9	-598.9	0.0	-598.9	
18400	3000	-401.0	-99.9	-500.9	0.0	-500.9	
18400	3025	-374.9	-99.9	-474.8	0.0	-474.8	
18400	3050	-405.0	-99.9	-504.9	0.0	-504.9	
18400	3075	-484.0	-99.9	-583.9	0.0	-583.9	
18400	3100	-690.0	-99.9	-789.9	0.0	-789.9	
18400	3125	-567.0	-99.9	-666.9	0.0	-666.9	
18400	3150	-144.8	-99.9	-244.7	0.0	-244.7	
18400	3175	42.3	-99.9	-57.6	0.0	-57.6	
18400	3200	78.2	-99.9	-21.7	0.0	-21.7	
18400	3225	74.0	-99.9	-25.9	0.0	-25.9	
18400	3250	82.1	-99.9	-17.8	0.0	-17.8	
18400	3275	-55.1	-99.9	-155.0	0.0	-155.0	
18400	3300	-266.8	-99.9	-366.7	0.0	-366.7	end of cutline
18400	3325	-412.0	-99.9	-511.9	0.0	-511.9	
18400	3350	-496.0	-99.9	-595.9	0.0	-595.9	
18400	3375	-190.9	-99.9	-290.8	0.0	-290.8	
18400	3400	-57.9	-99.9	-157.8	0.0	-157.8	
18400	3425	17.2	-99.9	-82.7	0.0	-82.7	
18400	3450	83.5	-99.9	-16.4	0.0	-16.4	
18400	3475	107.3	-99.9	7.4	0.0	7.4	by old trench/ shaft tying Cow Mountain to Bonanza Ledge base station
22-Sep	14400	4000		-272.8			
	14350	4000	-272.8	-323.1	0.0	-323.1	about 240' lower elevation than negative pot. East side of creek
	14150	4000	-272.8	70.5	0.0	70.5	West side of creek
	14135	4000	-272.8	66.3	0.0	66.3	on east side of Wilf's Island
	14105	3975	-272.8	31.3	0.0	31.3	west side of Wilf's Island
	14075	3975	-272.8	31.3	0.0	31.3	25' west of last reading
	14028	4000	-272.8	18.2	0.0	18.2	
	14000	4000	-272.8	0.9	0.0	0.9	
	14000	3950	-272.8	-29.6	0.0	-29.6	
	14000	3900	-272.8	-82.0	0.0	-82.0	
	13975	4000	-272.8	-38.7	0.0	-38.7	
	13944	4000	-272.8	-72.1	0.0	-72.1	at survey pin 2K-112. Rocky
	13868	4000	-272.8	-114.8	0.0	-114.8	on old road
	13800	4000	-272.8	-277.2	0.0	-277.2	
Sun Sept 23	14400	4000		-272.8			
	14400	3950	-272.8	-232.1	0.0	-232.1	side of Lowhee pit
	14400	3875	-272.8	-128.8	0.0	-128.8	side of Lowhee pit
	15800	3200		-397.5			
	15800	3175	-397.5	-429.6	0.0	-429.6	
	15800	3150	-397.5	-413.6	0.0	-413.6	
	15800	3125	-397.5	-436.9	0.0	-436.9	
	15800	3100	-397.5	-394.2	0.0	-394.2	top edge of pit
	15800	3075	-397.5	-368.7	0.0	-368.7	side of pit

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
16000	3200			-715.1			
16000	3175	-0.2	-715.1	-715.3	0.0	-715.3	
16000	3150	4.9	-715.1	-710.2	0.0	-710.2	
16000	3125	41.0	-715.1	-674.1	0.0	-674.1	
16000	3100	171.5	-715.1	-543.6	0.0	-543.6	in old or seasonal stream bed
16000	3075	257.6	-715.1	-457.5	0.0	-457.5	
16000	3050	372.0	-715.1	-343.1	0.0	-343.1	
16000	3025	404.0	-715.1	-311.1	0.0	-311.1	
16000	3000	464.0	-715.1	-251.1	0.0	-251.1	
16000	2975	470.0	-715.1	-245.1	0.0	-245.1	
16200	3200			-57.6			wet, soft ground
16200	3170	71.6	-57.6	14.0	0.0	14.0	
16200	3150	37.4	-57.6	-20.2	0.0	-20.2	
16200	3125	10.5	-57.6	-47.1	0.0	-47.1	
16200	3100	-12.0	-57.6	-69.6	0.0	-69.6	
16200	3075	-66.4	-57.6	-124.0	0.0	-124.0	
16200	3050	-130.8	-57.6	-188.4	0.0	-188.4	
16200	3025	-195.2	-57.6	-252.8	0.0	-252.8	
16200	3000	-232.2	-57.6	-289.8	0.0	-289.8	
16200	2975	-222.0	-57.6	-279.6	0.0	-279.6	fluct ± 3 mV
16200	2950	-232.0	-57.6	-289.6	0.0	-289.6	
16200	2925	-237.3	-57.6	-294.9	0.0	-294.9	
16200	2900	-235.0	-57.6	-292.6	0.0	-292.6	fluct ±2mV
16400	3200			-347.1			
16400	3175	224.8	-347.1	-122.3	0.0	-122.3	
16400	3150	222.4	-347.1	-124.7	0.0	-124.7	
16400	3125	328.5	-347.1	-18.6	0.0	-18.6	
16400	3100	347.0	-347.1	-0.1	0.0	-0.1	
16400	3075	333.0	-347.1	-14.1	0.0	-14.1	
16400	3050	234.9	-347.1	-112.2	0.0	-112.2	
16400	3025	129.3	-347.1	-217.8	0.0	-217.8	
16400	3000	-33.9	-347.1	-381.0	0.0	-381.0	
16400	2975	-20.6	-347.1	-367.7	0.0	-367.7	
16400	2950	9.9	-347.1	-337.3	0.0	-337.3	
16400	2925	41.1	-347.1	-306.0	0.0	-306.0	
16400	2900	50.5	-347.1	-296.6	0.0	-296.6	
16400	2875	74.4	-347.1	-272.7	0.0	-272.7	edge of pit
17800	2200			-18.0			
17800	2175	2.0	-18.0	-18.0	0.0	-18.0	
17800	2150	25.0	-18.0	7.0	0.0	7.0	
17800	2130	34.9	-18.0	16.9	0.0	16.9	
17800	2000	102.5	-18.0	84.5	0.0	84.5	
17800	1900	123.0	-18.0	105.0	0.0	105.0	
17800	1875	108.4	-18.0	90.4	0.0	90.4	North side of road
13800	4000			-277.2			
13800	3900	6.8	-277.2	-270.4	0.0	-270.4	
13800	3800	125.3	-277.2	-151.9	0.0	-151.9	
13800	3700	-38.0	-277.2	-315.2	0.0	-315.2	
13800	3600	-55.0	-277.2	-332.2	0.0	-332.2	
13800	3500	183.4	-277.2	-93.8	0.0	-93.8	
13800	3400	224.5	-277.2	-52.7	0.0	-52.7	
13800	3400			-52.7			set up
13400	3400	2.3	-52.7	-50.4	0.0	-50.4	Correction / Normalizing Value for all points on Cow Mtn to be tied to Bonanza Ledge Base Station at 20200E 2800N
14000	2800			-26.6			set up
14400	2793	19.3	-26.6	-7.3	0.0	-7.3	on ditch line
14400	2850	34.7	-26.6	8.1	0.0	8.1	
14400	2850			8.1			set up

25-Sep

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
14400	2900	17.7	8.1	25.8	0.0	25.8	soft, black, wet soil. Possibly still A-horizon
14400	2925	12.1	8.1	20.2	0.0	20.2	brown soil
14400	2950	10.8	8.1	18.9	0.0	18.9	
1:32 pm. Voltmeter readings jumping A LOT. Spaceweather.com says 250protons/cm ³ . Was only at 5 when we left for the field this morning. Solar storm still in progress and affecting readings. Must wait No solar interference expected today. Solar wind up high (~400-500km/s) but protons/cm ³ is very low							
14400	2150	-72.5	8.1	-64.4			
14400	2200	-48.2	8.1	-40.1	0.0	-40.1	gravelly
14400	2225	-91.4	8.1	-83.3	0.0	-83.3	very rocky
14400	2275	-72.1	8.1	-64.0	0.0	-64.0	very rocky
14400	2325	-80.2	8.1	-72.1	0.0	-72.1	
14400	2350	-57.9	8.1	-49.8	0.0	-49.8	lots of gravel
14400	2375	-87.4	8.1	-79.3	0.0	-79.3	
14400	2400	-66.0	8.1	-57.9	0.0	-57.9	
14400	2450	-54.1	8.1	-46.0	0.0	-46.0	
14400	2475	-43.9	8.1	-35.8	0.0	-35.8	
14400	2500	-26.4	8.1	-18.3	0.0	-18.3	
14400	2525	-43.6	8.1	-35.5	0.0	-35.5	
14400	2550	-29.4	8.1	-21.3	0.0	-21.3	
14400	2575	-42.7	8.1	-34.6	0.0	-34.6	
14400	2600	-58.1	8.1	-50.0	0.0	-50.0	
14400	2625	-48.0	8.1	-39.9	0.0	-39.9	
14400	2650	-29.1	8.1	-21.0	0.0	-21.0	
14400	2675	-33.1	8.1	-25.0	0.0	-25.0	
14400	2700	-7.3	8.1	0.8	0.0	0.8	
14400	2793	-15.4	8.1	-7.3	0.0	-7.3	
14400	2850	20.2	-12.1	8.1	0.0	8.1	
14400	2900	13.7	8.1	21.8			
14400	2925	12.1	8.1	20.2	0.0	20.2	
14400	2950	10.8	8.1	18.9	0.0	18.9	
14400	3000	10.5	8.1	18.6	0.0	18.6	
14400	3025	6.2	8.1	14.3	0.0	14.3	
14400	3050	13.6	8.1	21.7	0.0	21.7	
14400	3075	0.2	8.1	8.3	0.0	8.3	
14400	3100	-10.9	8.1	-2.8	0.0	-2.8	
14400	3125	-11.0	8.1	-2.9	0.0	-2.9	
14400	3175	-8.4	8.1	-0.3	0.0	-0.3	
14400	3200	-4.9	8.1	3.2	0.0	3.2	
14400	3225	-5.3	8.1	2.9	0.0	2.9	No B-horizon. Marshy
14400	3300	-8.6	8.1	-0.5	0.0	-0.5	No B-horizon. Marshy
14400	3375	-36.6	8.1	-28.5	0.0	-28.5	No B-horizon. Edge of Lowtree pit. A bit wet
14400	3400	-20.2	8.1	-12.1	0.0	-12.1	gravelly
14600	2050	-56.9	-33.9	-90.8			
14600	2100	-35.5	-33.9	-69.4	0.0	-69.4	
14600	2150	-26.0	-33.9	-59.9	0.0	-59.9	gravelly
14600	2200	-29.3	-33.9	-63.2	0.0	-63.2	
14600	2250	-22.4	-33.9	-56.3	0.0	-56.3	
14600	2300	-25.3	-33.9	-59.2	0.0	-59.2	
14600	2350	-30.9	-33.9	-64.8	0.0	-64.8	gravelly
14600	2400	-29.7	-33.9	-63.6	0.0	-63.6	
14600	2450	-12.5	-33.9	-46.4	0.0	-46.4	gravelly
14600	2500	-6.6	-33.9	-40.5	0.0	-40.5	
14600	2550	-2.9	-33.9	-36.8	0.0	-36.8	
14600	2600	-7.2	-33.9	-41.1	0.0	-41.1	
14600	2650	9.9	-33.9	-24.0	0.0	-24.0	12:54pm
14600	2694	-0.4	-33.9	-34.3	0.0	-34.3	on ditch line
14600	2750	-6.3	-33.9	-40.2	0.0	-40.2	gravelly
14600	2800	-42.0	8.1	-33.9	0.0	-33.9	
14600	2850	-10.7	-33.9	-44.6	0.0	-44.6	
14600	2900	6.1	-33.9	-27.8	0.0	-27.8	
14600	2950	13.2	-33.9	-20.7	0.0	-20.7	reading jumped. 12:30pm
14600	3000	10.7	-33.9	-23.2	0.0	-23.2	
14600	3050	52.9	-33.9	19.0	0.0	19.0	

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
14600	3100	7.3	-33.9	-26.7	0.0	-26.7	excellent hole. Uniform soil. No gravel
14600	3150	10.7	-33.9	-23.2	0.0	-23.2	
14600	3200	11.5	-33.9	-22.4	0.0	-22.4	
14600	3250	12.4	-33.9	-21.6	0.0	-21.6	
14800	2850	21.7	-33.9	-12.2	0.0	-12.2	very old road below ditchline. Numerous 4 foot diameter rusty flumes lying around
14800	2240	-50.2	-12.2	-62.4	0.0	-62.4	lots of grey phyllitic rocks nearby. Gravelly hole
14800	2350	-40.9	-12.2	-53.1	0.0	-53.1	
14800	2450	-34.0	-12.2	-46.2	0.0	-46.2	
14800	2500	-19.6	-12.2	-31.8	0.0	-31.8	crossed the ditchline
14800	2530	-34.5	-12.2	-46.7	0.0	-46.7	
14800	2600	0.2	-12.2	-12.0	0.0	-12.0	top edge of pit
14800	2625	-3.8	-12.2	-16.0	0.0	-16.0	
14800	2750	-3.3	-12.2	-15.5	0.0	-15.5	
14800	2850	21.7	-33.9	-12.2	0.0	-12.2	
14800	2900	-27.8	-12.2	-40.0	0.0	-40.0	
14800	2950	-9.6	-12.2	-21.8	0.0	-21.8	
14800	3000	-25.9	-12.2	-38.1	0.0	-38.1	
14800	3050	-21.9	-12.2	-34.1	0.0	-34.1	
14800	3100	-23.2	-12.2	-35.4	0.0	-35.4	
14800	3150	-4.8	-12.2	-17.0	0.0	-17.0	
14800	3250	-2.5	-12.2	-14.7	0.0	-14.7	
15000	2800	5.7	-12.2	-6.5	0.0	-6.5	Extremely windy day. Storm too dangerous to remain on this side of Cow Mtn near the gulch. Branches falling
12200	4025			-753.7			graphitic argillite close to surface
12200	4050	-27.2	-753.7	-780.9	0.0	-780.9	
12200	4075	43.9	-753.7	-709.8	0.0	-709.8	South side of road. Argillite outcrop nearby
12200	4100	5.5	-753.7	-748.2	0.0	-748.2	
12200	4125	-1.8	-753.7	-755.5	0.0	-755.5	
12200	4150	33.5	-753.7	-720.2	0.0	-720.2	
12200	4175	84.0	-753.7	-669.7	0.0	-669.7	
12200	4200	144.6	-753.7	-609.1	0.0	-609.1	
12200	4225	213.2	-753.7	-540.5	0.0	-540.5	
12200	4238	265.3	-753.7	-488.4	0.0	-488.4	
12200	4250	250.5	-753.7	-503.2	0.0	-503.2	
12200	4300	549.0	-753.7	-204.7	0.0	-204.7	black and brown rocks on old road. Rocky hole
12200	4325	495.0	-753.7	-258.7	0.0	-258.7	
12200	4350	581.0	-753.7	-192.7	0.0	-192.7	
12200	4375	633.0	-753.7	-120.7	0.0	-120.7	
12200	4400	721.0	-753.7	-32.7	0.0	-32.7	
12200	4425	677.0	-753.7	-76.7	0.0	-76.7	
12200	4450	585.0	-753.7	-168.7	0.0	-168.7	
12200	4475	489.0	-753.7	-264.7	0.0	-264.7	
12200	4500	523.0	-753.7	-230.7	0.0	-230.7	
12200	4525	562.0	-753.7	-191.7	0.0	-191.7	on a road
12200	4550	597.0	-753.7	-158.7	0.0	-158.7	
12200	4575	595.0	-753.7	-158.7	0.0	-158.7	
12200	4625	663.0	-753.7	-90.7	0.0	-90.7	
12200	4650	641.0	-753.7	-112.7	0.0	-112.7	
12200	4675	606.0	-753.7	-147.7	0.0	-147.7	
12200	4700	593.0	-753.7	-160.7	0.0	-160.7	
12200	4725	592.0	-753.7	-161.7	0.0	-161.7	
12200	4750	557.0	-753.7	-196.7	0.0	-196.7	
12200	4800	281.1	-753.7	-472.8	0.0	-472.8	
13000	4175	-460.4		-460.4			on a road
13000	4200	35.2	-460.4	-425.2	0.0	-425.2	
13000	4225	37.2	-460.4	-423.2	0.0	-423.2	
13000	4250	17.2	-460.4	-443.2	0.0	-443.2	
13000	4275	14.5	-460.4	-445.9	0.0	-445.9	
13000	4300	6.1	-460.4	-454.3	0.0	-454.3	

Sat Sept 23

CONTROL STATION

SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
13000	4325	58.3	-480.4	-402.1	0.0	-402.1	
13000	4350	306.0	-480.4	-154.4	0.0	-154.4	BIG change in readings. Crossed fault or other contact?
13000	4375	430.0	-480.4	-30.4	0.0	-30.4	
13000	4400	515.0	-480.4	54.6	0.0	54.6	on a road
13000	4425	493.0	-480.4	32.6	0.0	32.6	
13000	4450	507.0	-480.4	46.6	0.0	46.6	
13000	4475	522.0	-480.4	61.6	0.0	61.6	
13000	4500	543.0	-480.4	82.6	0.0	82.6	
13000	4525	514.0	-480.4	53.6	0.0	53.6	
13000	4550	538.0	-480.4	77.6	0.0	77.6	
13000	4575	530.0	-480.4	69.6	0.0	69.6	
13000	4600	542.0	-480.4	81.6	0.0	81.6	
13000	4625	495.0	-480.4	34.6	0.0	34.6	
13000	4650	497.0	-480.4	36.6	0.0	36.6	end of a road
13000	4675	504.0	-480.4	43.6	0.0	43.6	
13000	4700	480.0	-480.4	19.6	0.0	19.6	
13000	4725	469.0	-480.4	8.6	0.0	8.6	
13000	4750	429.0	-480.4	-31.4	0.0	-31.4	
13000	4775	415.0	-480.4	-45.4	0.0	-45.4	
13000	4800	412.0	-480.4	-48.4	0.0	-48.4	
13000	4825	418.0	-480.4	-42.4	0.0	-42.4	by a road
13000	4850	362.8	-480.4	-97.7	0.0	-97.7	
13000	4875	332.3	-480.4	-128.1	0.0	-128.1	
13000	4900	340.0	-480.4	-120.4	0.0	-120.4	
13000	4925	315.0	-480.4	-145.4	0.0	-145.4	
13400	4300			-71.7			on an old overgrown road
13400	4325	-68.6	-71.7	-140.3	0.0	-140.3	goosey hole
13400	4350	3.4	-71.7	-68.3	0.0	-68.3	
13400	4375	94.8	-71.7	23.1	0.0	23.1	at lower ditchline
13400	4400	160.9	-71.7	89.2	0.0	89.2	
13400	4425	209.0	-71.7	137.3	0.0	137.3	
13400	4450	265.5	-71.7	193.8	0.0	193.8	
13400	4475	319.2	-71.7	247.5	0.0	247.5	
13400	4500	423.0	-71.7	351.3	0.0	351.3	
13400	4525	449.0	-71.7	377.3	0.0	377.3	
13400	4550	453.0	-71.7	381.3	0.0	381.3	
13400	4575	490.0	-71.7	418.3	0.0	418.3	
13400	4600	488.0	-71.7	416.3	0.0	416.3	
13400	4625	509.0	-71.7	437.3	0.0	437.3	
13400	4650	475.0	-71.7	403.3	0.0	403.3	
13400	4675	450.0	-71.7	378.3	0.0	378.3	end of line. Edge of Lowhee pit
13400	4700	456.0	-71.7	384.3	0.0	384.3	side of Lowhee pit
13400	4725	448.0	-71.7	376.3	0.0	376.3	
13400	4750	400.0	-71.7	328.3	0.0	328.3	
13400	4775	348.2	-71.7	276.5	0.0	276.5	
13400	4800	389.8	-71.7	318.1	0.0	318.1	
13400	4825	402.0	-71.7	330.3	0.0	330.3	
13400	4900	437.0	-71.7	365.3	0.0	365.3	
13400	4925	540.0	-71.7	468.3	0.0	468.3	
13400	4950	550.0	-71.7	478.3	0.0	478.3	
Sun Sept 30							
13800	4000			-277.2			
13800	4025	-51.7	-277.2	-328.9	0.0	-328.9	
13800	4050	-82.3	-277.2	-359.5	0.0	-359.5	
13800	4075	-71.9	-277.2	-349.1	0.0	-349.1	
13800	4100	74.8	-277.2	-202.4	0.0	-202.4	in trench, very rocky
13800	4125	94.3	-277.2	-182.9	0.0	-182.9	South side of road
13800	4150	67.4	-277.2	-209.8	0.0	-209.8	North side of road
13800	4175	99.5	-277.2	-177.7	0.0	-177.7	
13800	4200	-58.2	-277.2	-335.4	0.0	-335.4	Lowhee camp
13800	4225	-140.2	-277.2	-417.4	0.0	-417.4	Lowhee camp
13800	4250	-181.9	-277.2	-459.1	0.0	-459.1	
13800	4275	-158.1	-277.2	-435.3	0.0	-435.3	
13800	4300	-292.6	-277.2	-569.8	0.0	-569.8	

CONTROL STATION

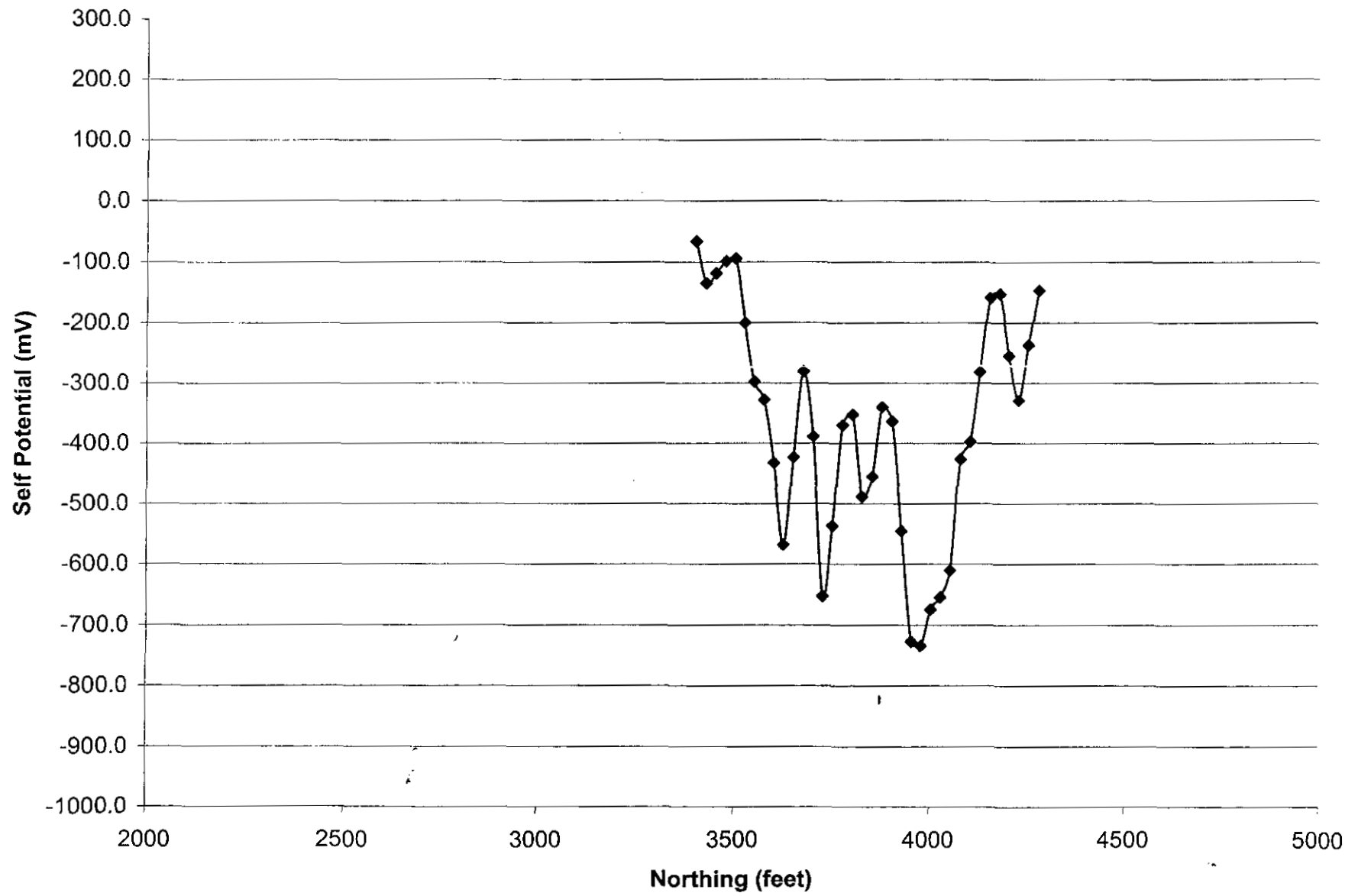
SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
13800	4350	-372.0	-277.2	-649.2	0.0	-649.2	
13800	4400	163.6	-277.2	-113.6	0.0	-113.6	South side of Lowhee creek
13800	4430	292.9	-277.2	15.7	0.0	15.7	North side of Lowhee creek. 5 feet north of creek
13800	4455	337.6	-277.2	60.4	0.0	60.4	
14000	3750			-335.8			
14000	3775	-36.4	-335.8	-372.2	0.0	-372.2	
14000	3800	-104.3	-335.8	-440.1	0.0	-440.1	
14000	3825	-88.7	-335.8	-424.5	0.0	-424.5	
14000	3850	91.3	-335.8	-244.5	0.0	-244.5	
14000	3875	170.1	-335.8	-165.7	0.0	-165.7	
14000	3900	214.1	-335.8	-121.7	0.0	-121.7	
14000	3925	265.1	-335.8	-70.7	0.0	-70.7	
14000	3950	306.2	-335.8	-29.6	0.0	-29.6	
14000	3975	309.5	-335.8	-26.3	0.0	-26.3	
14000	4000	336.7	-335.8	0.9	0.0	0.9	in a pile of dirt
14000	4100	261.1	-335.8	-74.7	0.0	-74.7	
14000	4150	246.3	-335.8	-89.6	0.0	-89.6	
12600	4000			-648.2			
12600	4025	-5.4	-648.2	-653.6	0.0	-653.6	
12600	4050	15.6	-648.2	-632.6	0.0	-632.6	
12600	4075	102.7	-648.2	-545.5	0.0	-545.5	
12600	4100	179.0	-648.2	-469.2	0.0	-469.2	
12600	4125	223.0	-648.2	-425.2	0.0	-425.2	
12600	4150	221.0	-648.2	-427.2	0.0	-427.2	
12600	4175	187.0	-648.2	-461.2	0.0	-461.2	
12600	4190	149.5	-648.2	-498.7	0.0	-498.7	middle of road
12600	4200	119.8	-648.2	-528.4	0.0	-528.4	
12600	4225	1.8	-648.2	-646.4	0.0	-646.4	
12600	4250	-5.1	-648.2	-653.3	0.0	-653.3	
12600	4275	11.9	-648.2	-636.3	0.0	-636.3	
12600	4300	159.9	-648.2	-488.3	0.0	-488.3	
12600	4325	305.6	-648.2	-342.6	0.0	-342.6	
12600	4350	456.0	-648.2	-192.2	0.0	-192.2	rocky
12600	4375	536.0	-648.2	-112.2	0.0	-112.2	
12600	4400	630.0	-648.2	-18.2	0.0	-18.2	
12600	4425	636.0	-648.2	-12.2	0.0	-12.2	
12600	4450	647.0	-648.2	-1.2	0.0	-1.2	
12600	4475	621.0	-648.2	-27.2	0.0	-27.2	
12600	4500	621.0	-648.2	-27.2	0.0	-27.2	
12600	4525	587.0	-648.2	-61.2	0.0	-61.2	
12600	4550	527.0	-648.2	-121.2	0.0	-121.2	
12600	4575	498.0	-648.2	-150.2	0.0	-150.2	
12600	4600	545.0	-648.2	-103.2	0.0	-103.2	
12600	4625	529.0	-648.2	-119.2	0.0	-119.2	side of a road
12600	4650	466.0	-648.2	-182.2	0.0	-182.2	
12600	4675	444.0	-648.2	-204.2	0.0	-204.2	
12600	4700	468.0	-648.2	-180.2	0.0	-180.2	
11400	4200			-168.7			on lower ditchline road
11400	4225	40.0	-168.7	-128.7	0.0	-128.7	
11400	4250	73.0	-168.7	-95.7	0.0	-95.7	
11400	4275	86.4	-168.7	-102.3	0.0	-102.3	
11400	4300	124.9	-168.7	-43.8	0.0	-43.8	
11400	4325	141.7	-168.7	-27.0	0.0	-27.0	
11400	4350	75.4	-168.7	-93.3	0.0	-93.3	
11400	4375	-51.9	-168.7	-220.6	0.0	-220.6	
11400	4400	-130.2	-168.7	-298.9	0.0	-298.9	
11400	4425	-303.2	-168.7	-471.9	0.0	-471.9	
11400	4450	-442.0	-168.7	-610.7	0.0	-610.7	
11400	4475	-498.0	-168.7	-664.7	0.0	-664.7	
11400	4500	-478.0	-168.7	-644.7	0.0	-644.7	
11400	4550	-458.0	-168.7	-626.7	0.0	-626.7	
11400	4575	-312.3	-168.7	-481.0	0.0	-481.0	
11400	4600	-221.2	-168.7	-389.9	0.0	-389.9	

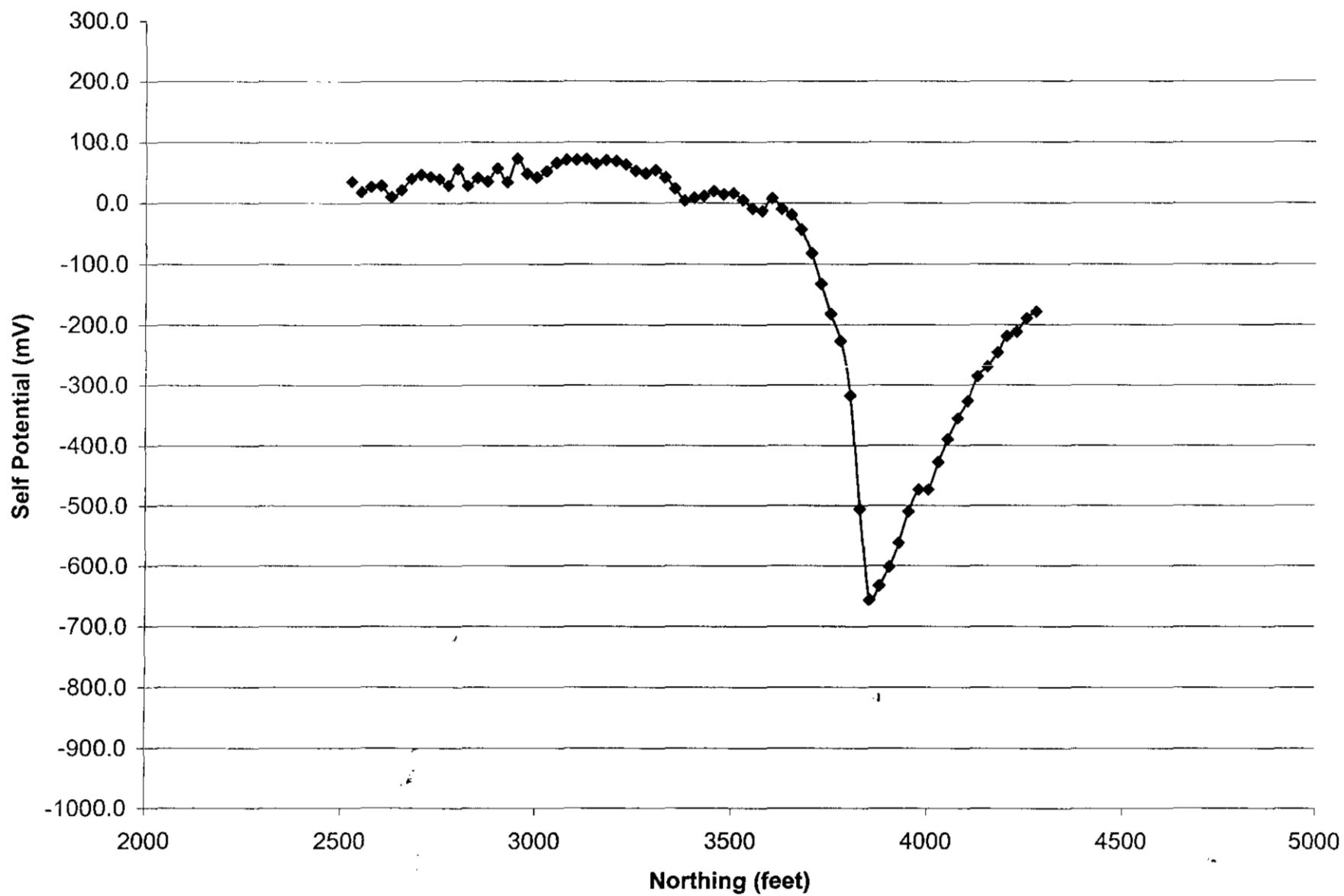
CONTROL STATION

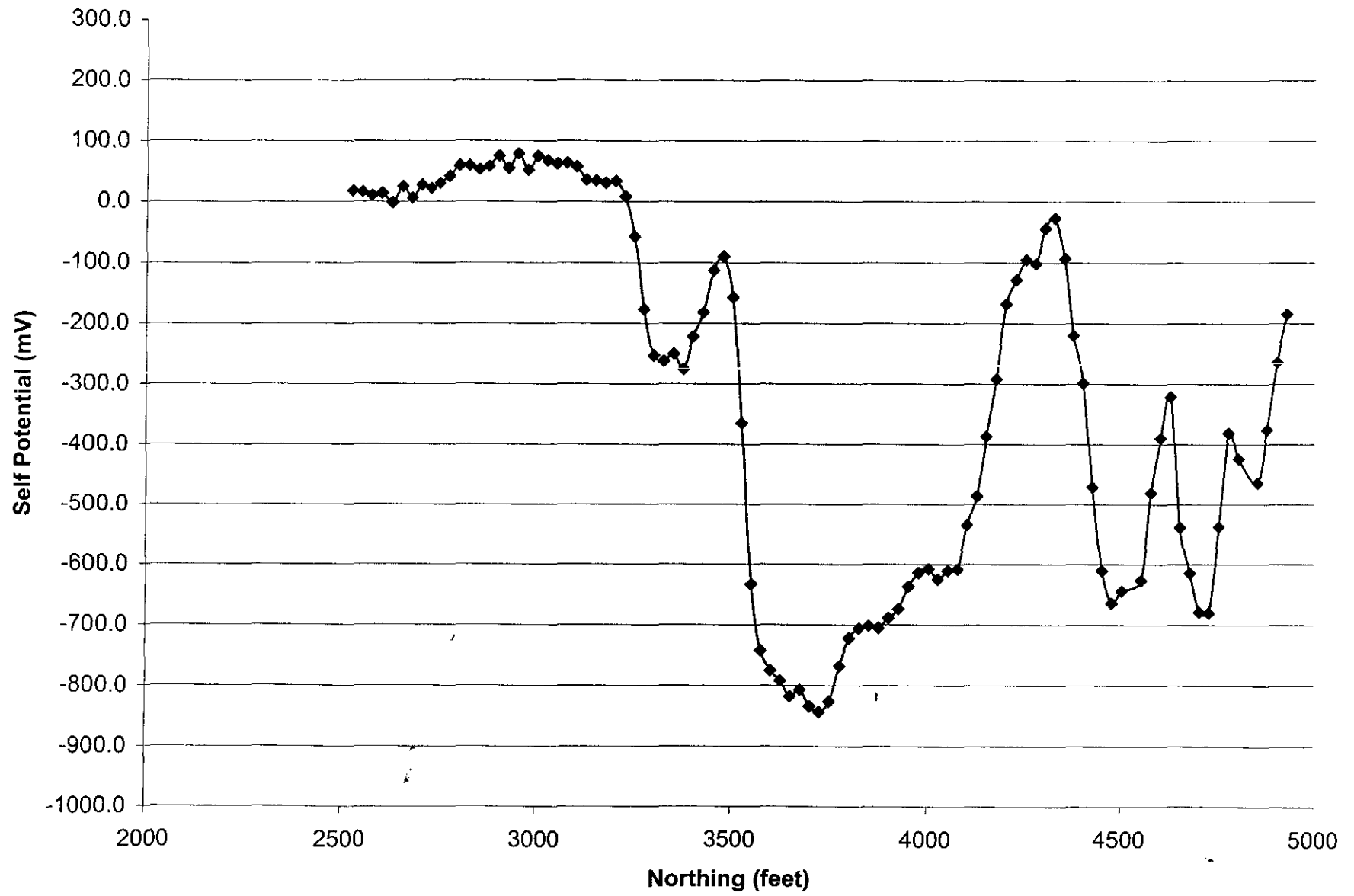
SURVEY STATION		READING	CORRECTION VALUE	TENTATIVE VALUE	NORMALIZER	FINAL VALUE	COMMENTS
EASTING	NORTHING	[mV]	[mV]	[mV]	[mV]	[mV]	
11400	4625	-152.4	-168.7	-321.1	0.0	-321.1	on a road: may be driveable
11400	4650	-370.3	-168.7	-539.0	0.0	-539.0	
11400	4675	-446.0	-168.7	-614.7	0.0	-614.7	
11400	4700	-511.0	-168.7	-679.7	0.0	-679.7	
11400	4725	-512.0	-168.7	-680.7	0.0	-680.7	
11400	4750	-369.0	-168.7	-537.7	0.0	-537.7	
11400	4775	-213.2	-168.7	-381.9	0.0	-381.9	
11400	4800	-256.1	-168.7	-424.8	0.0	-424.8	
11400	4850	-295.9	-168.7	-464.6	0.0	-464.6	
11400	4875	-207.9	-168.7	-376.6	0.0	-376.6	
11400	4900	-95.8	-168.7	-264.5	0.0	-264.5	
11400	4925	-16.5	-168.7	-185.2	0.0	-185.2	

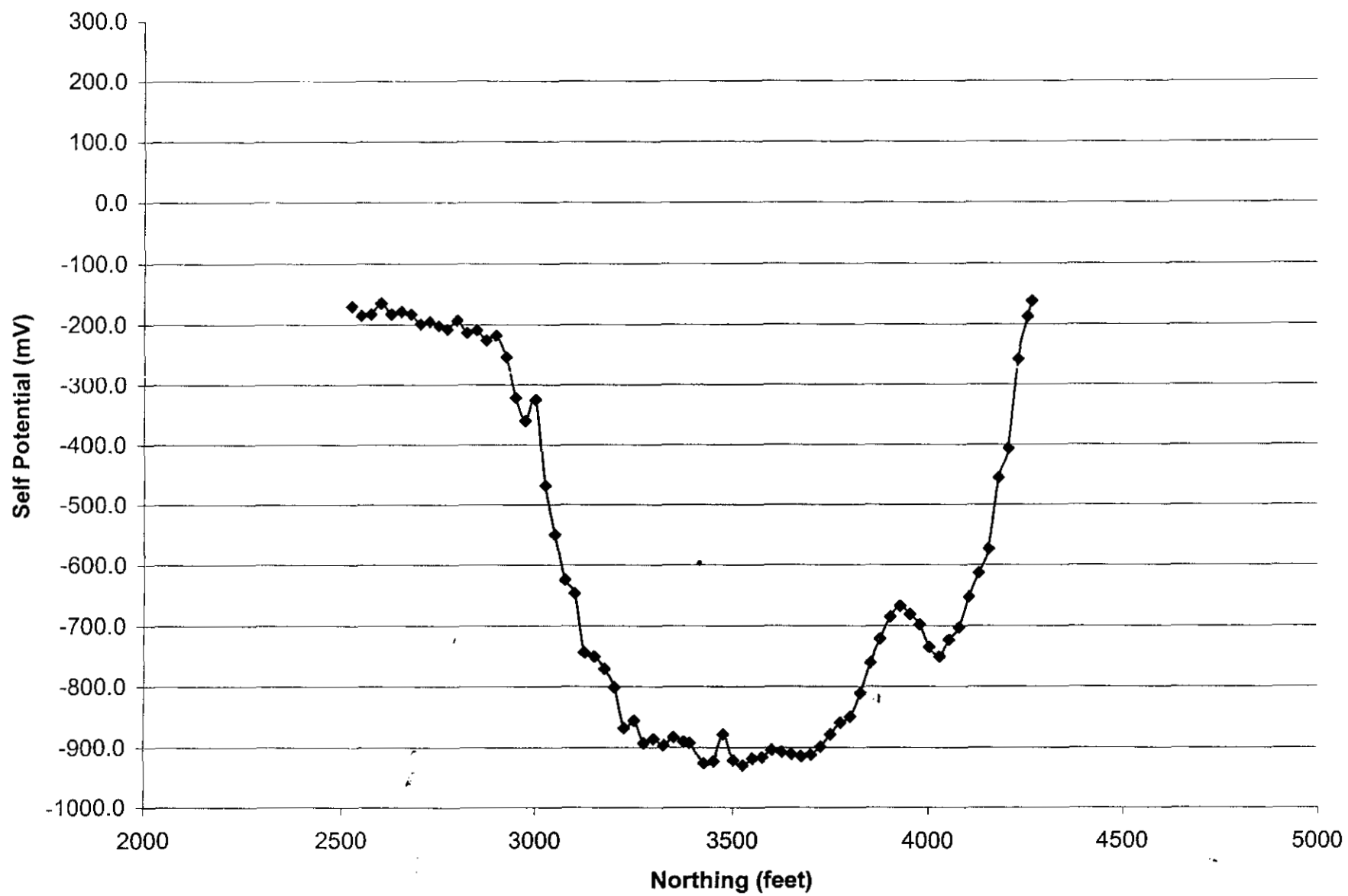
APPENDIX II

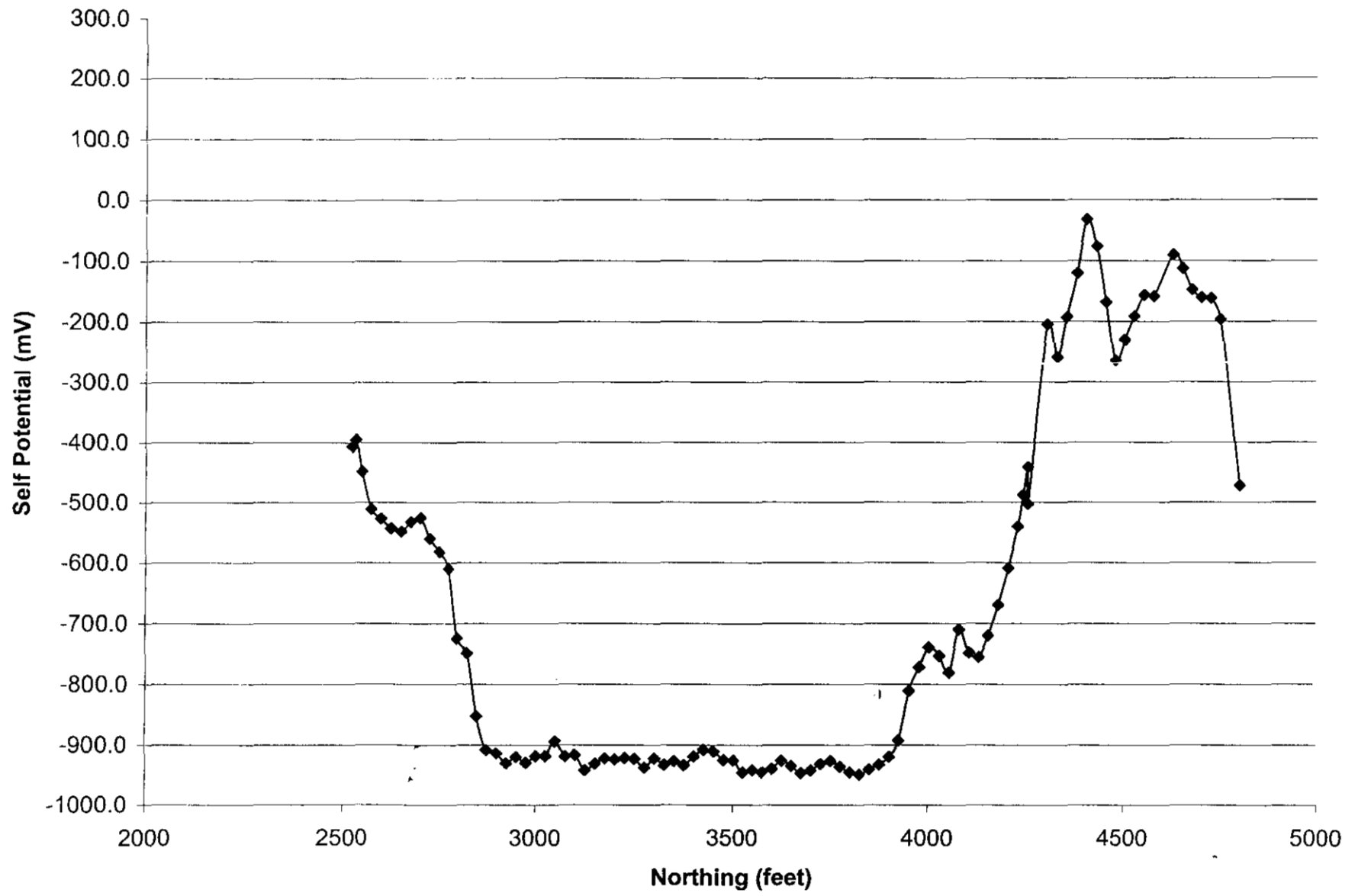
2001 Self-potential Profiles
including
Bonanza Ledge Zone Profiles

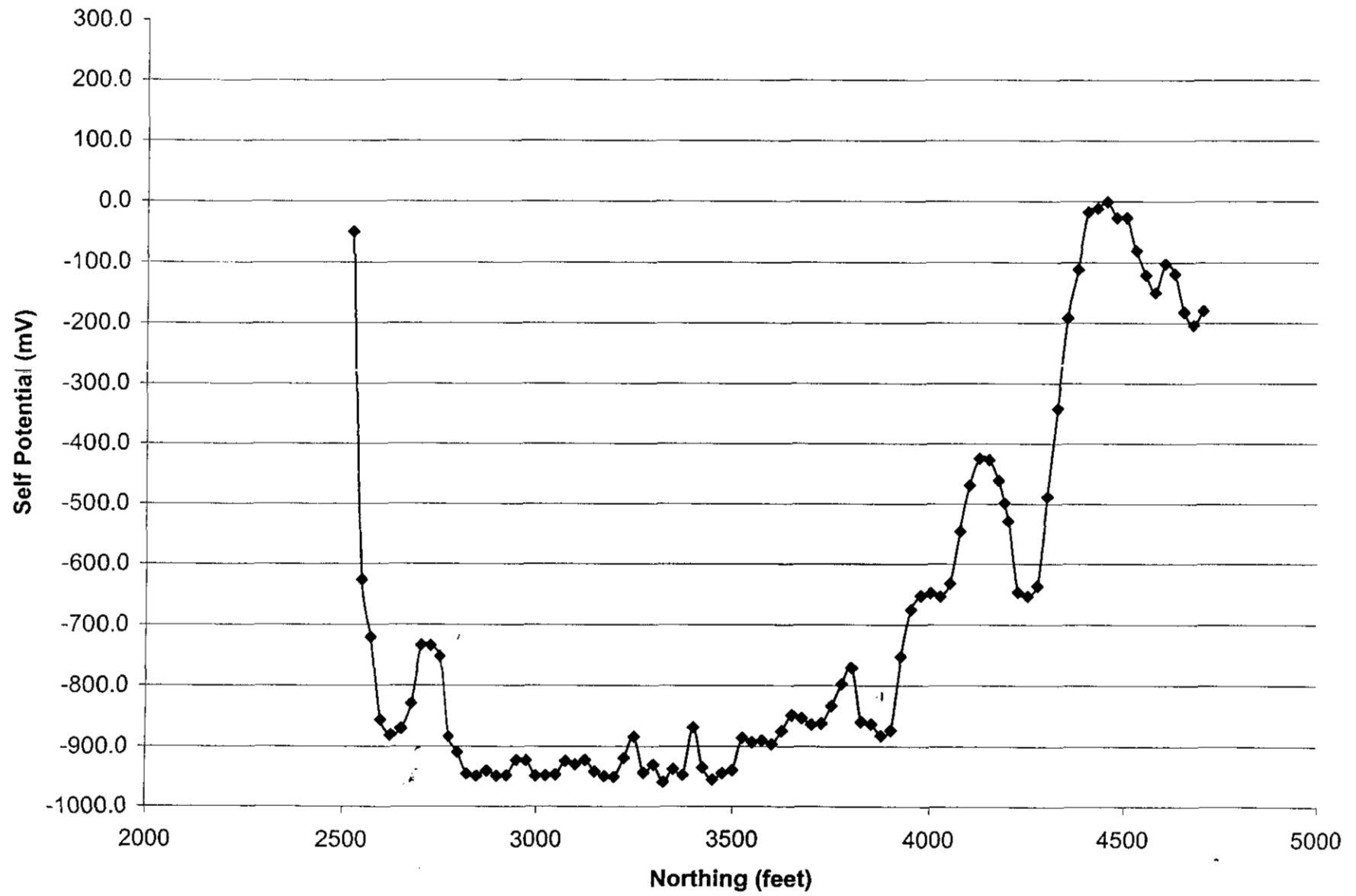


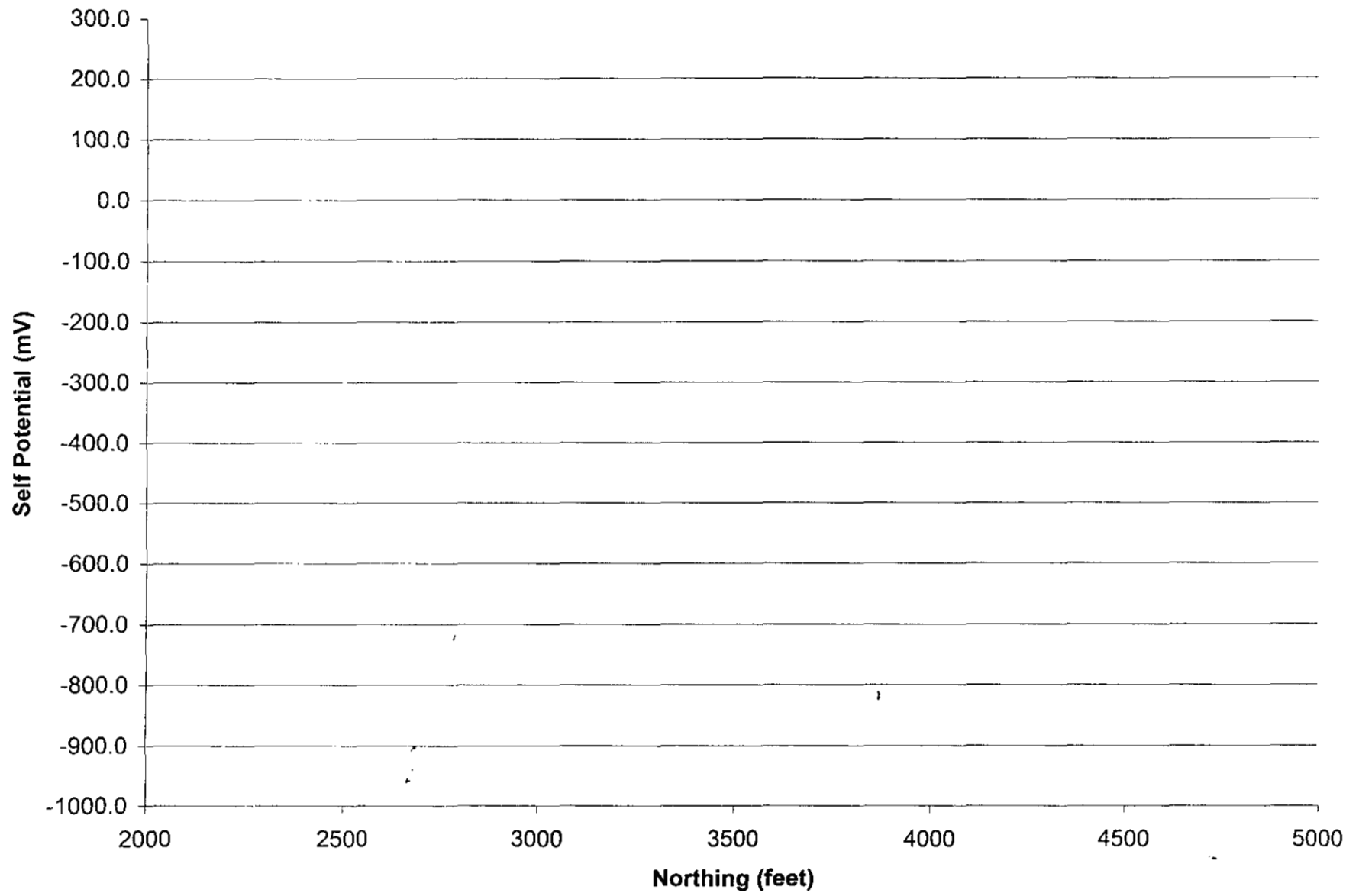


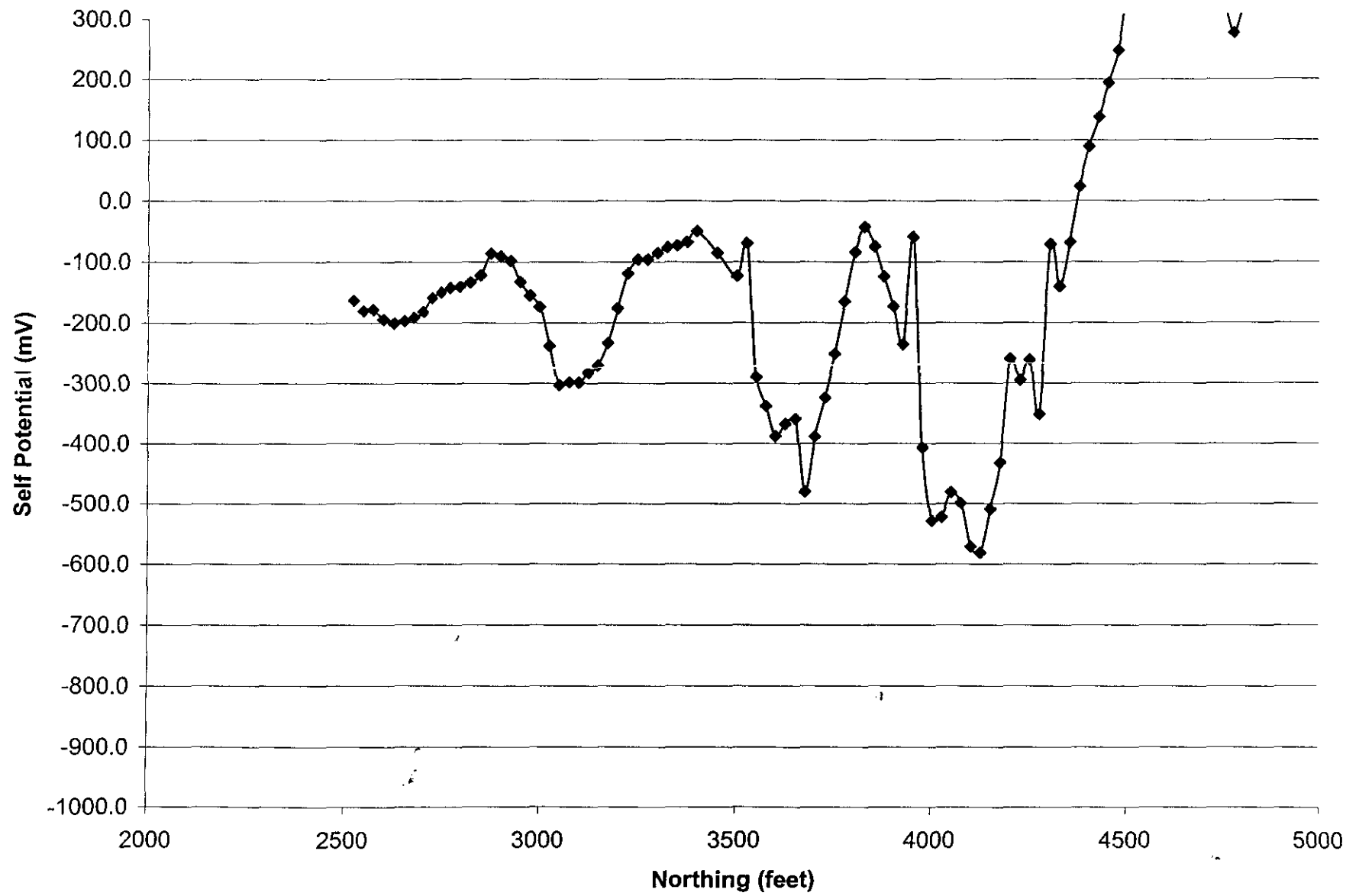


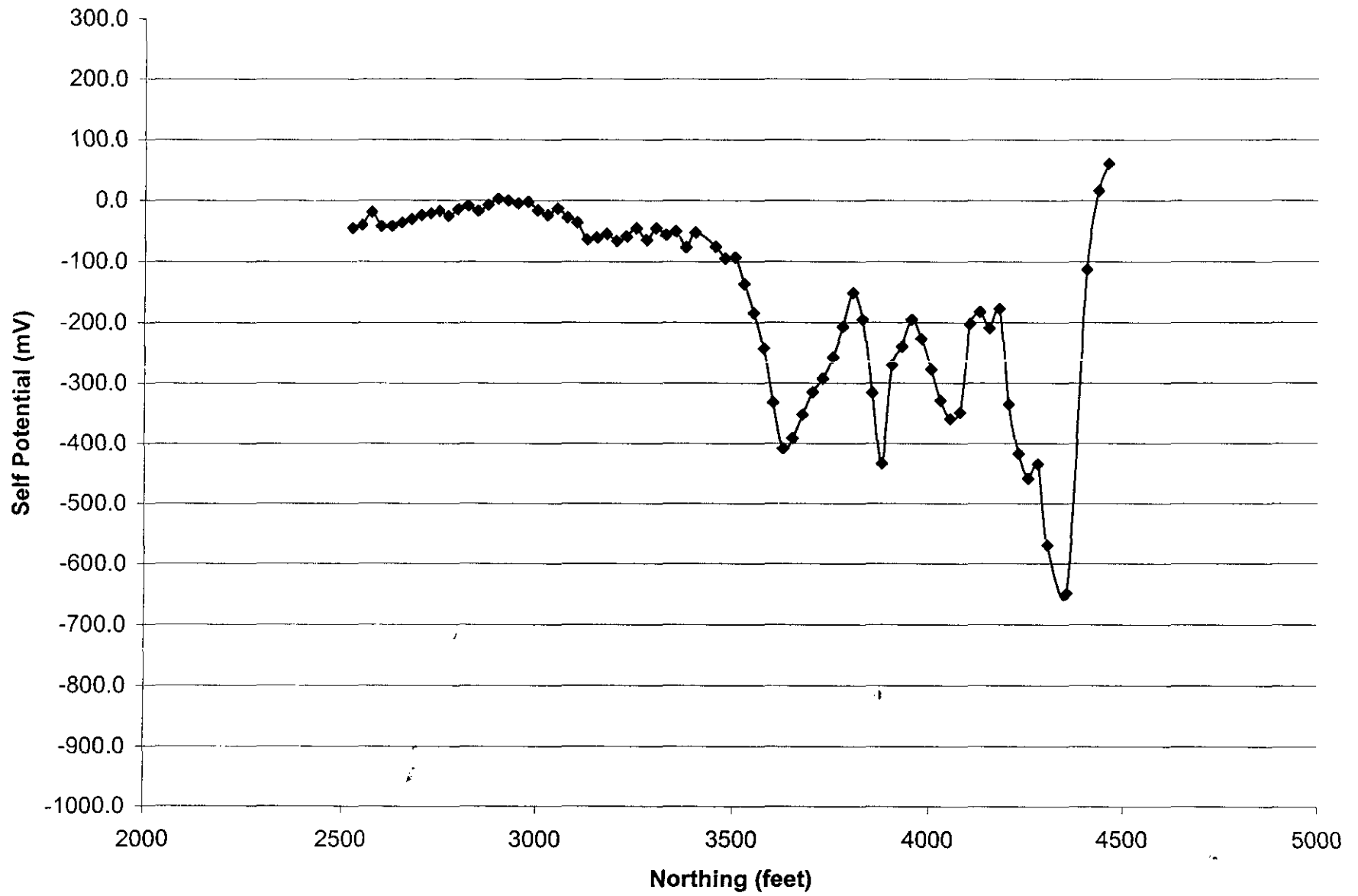


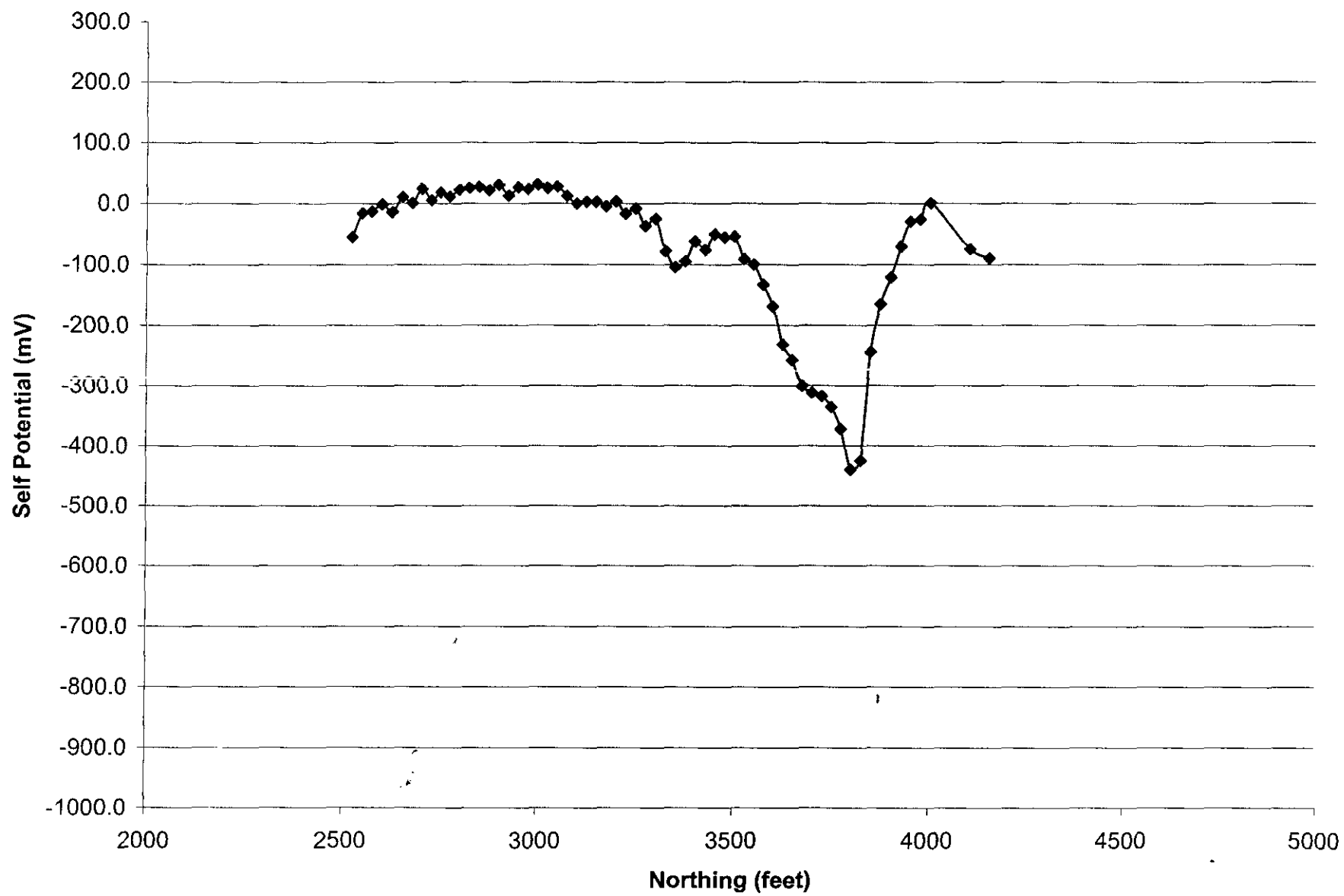


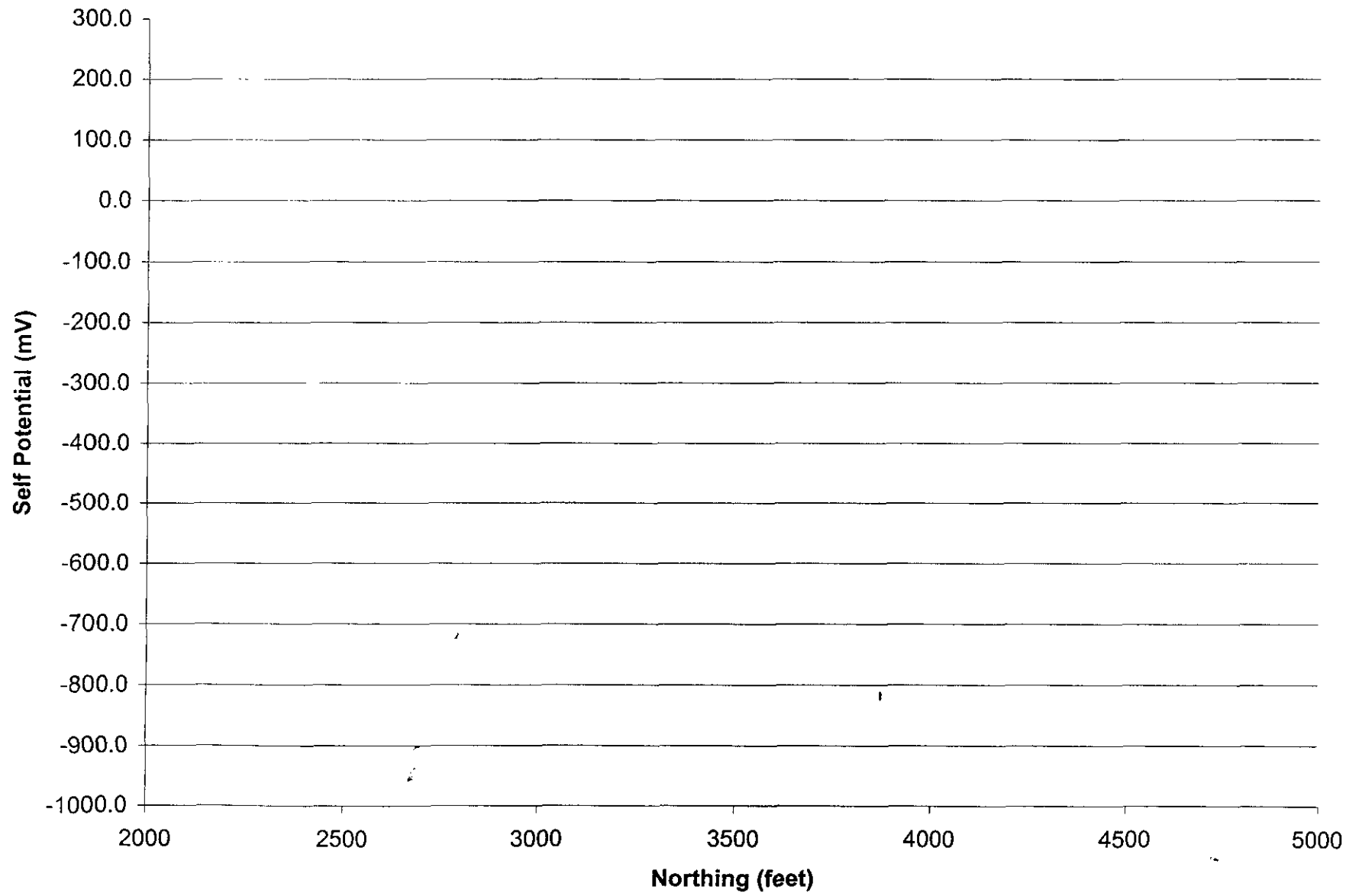


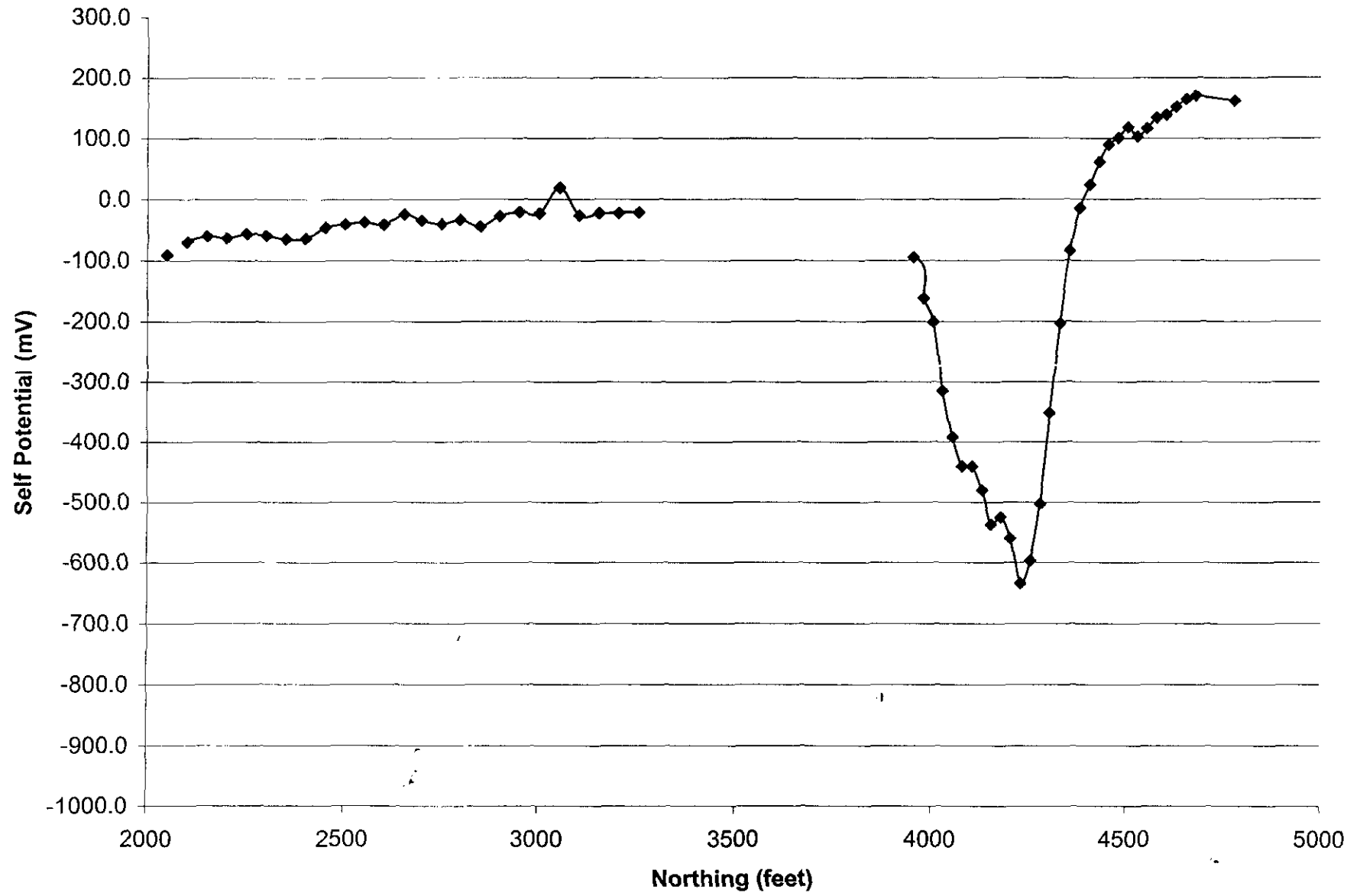


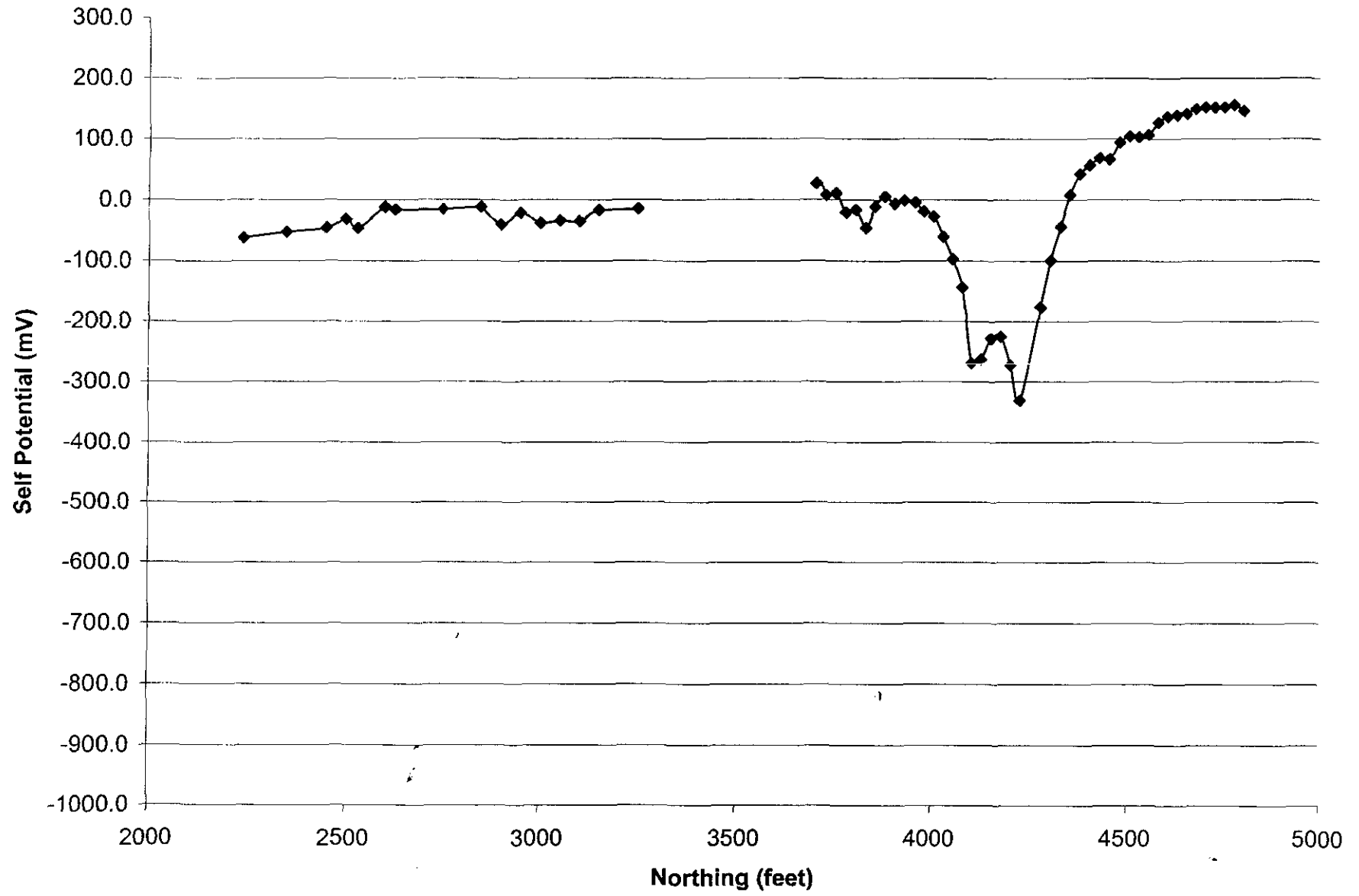


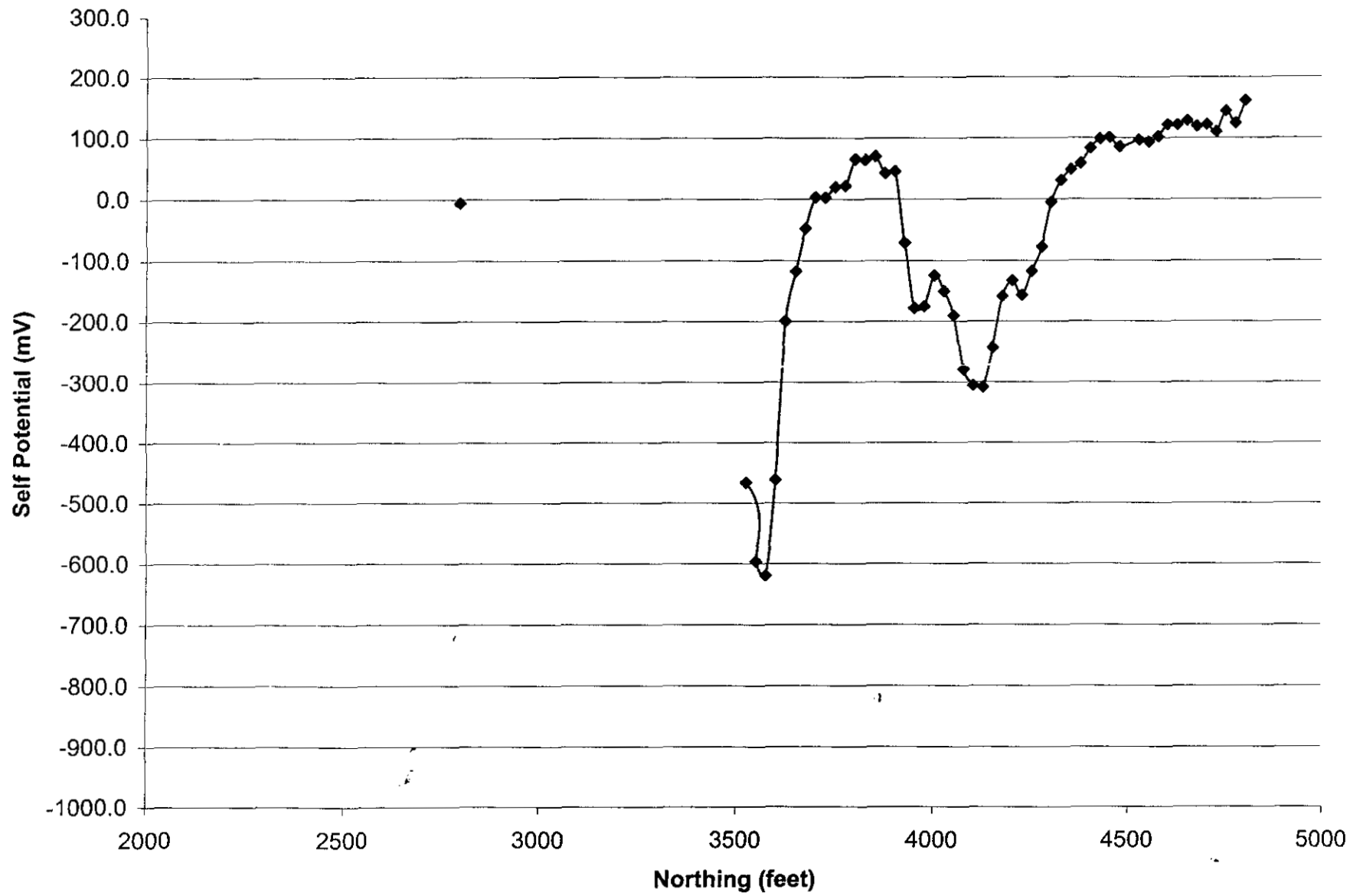


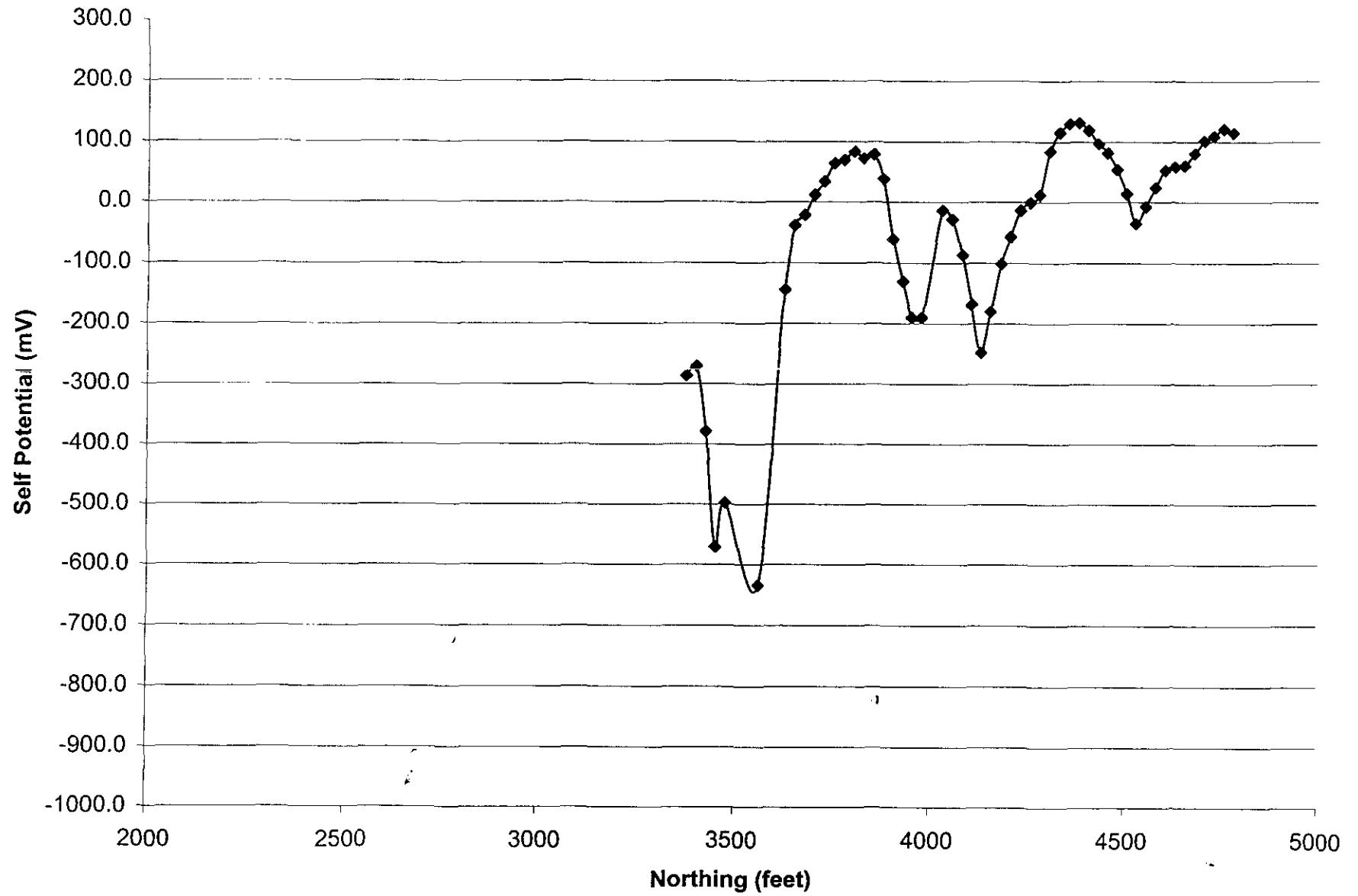


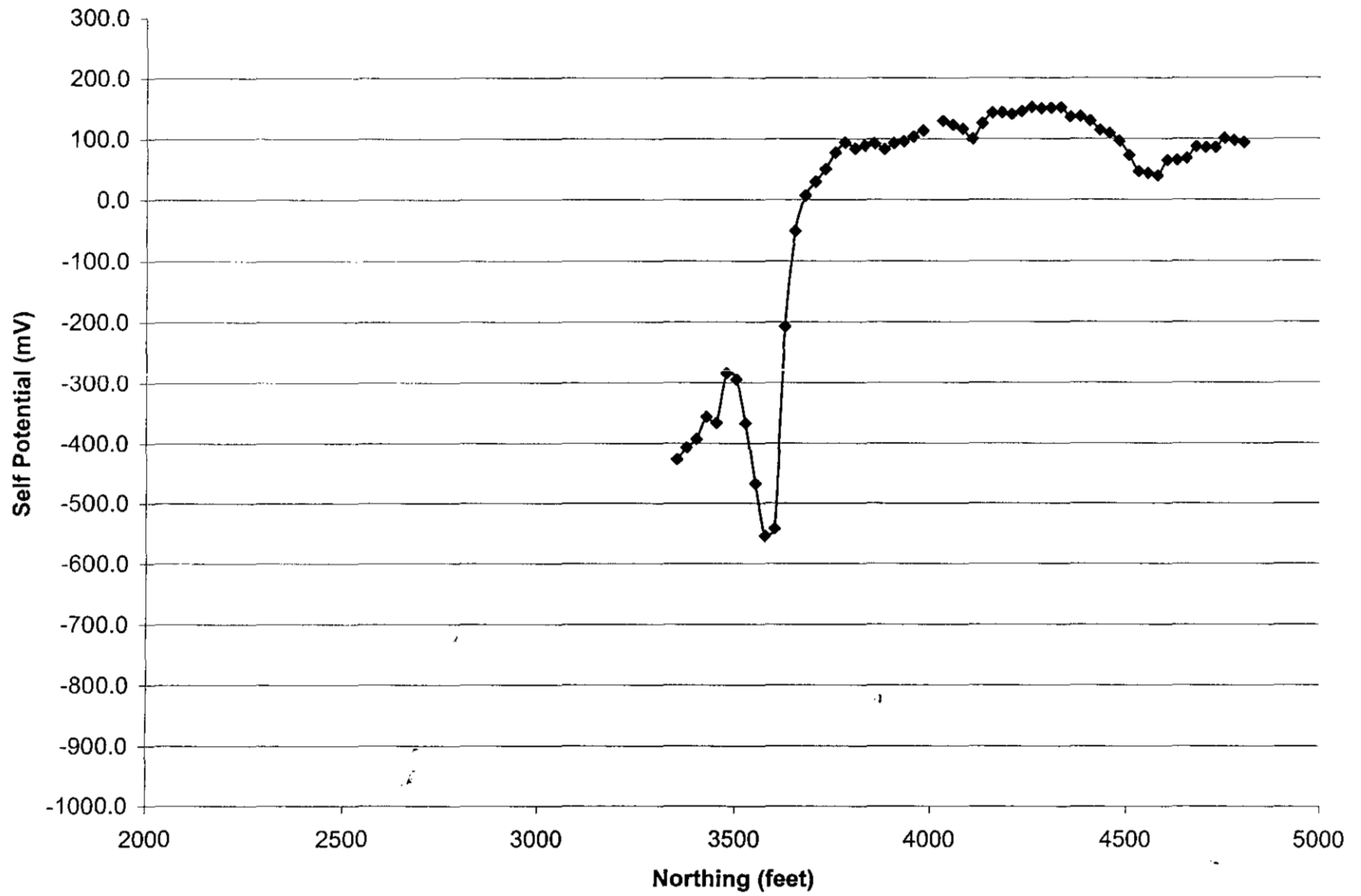


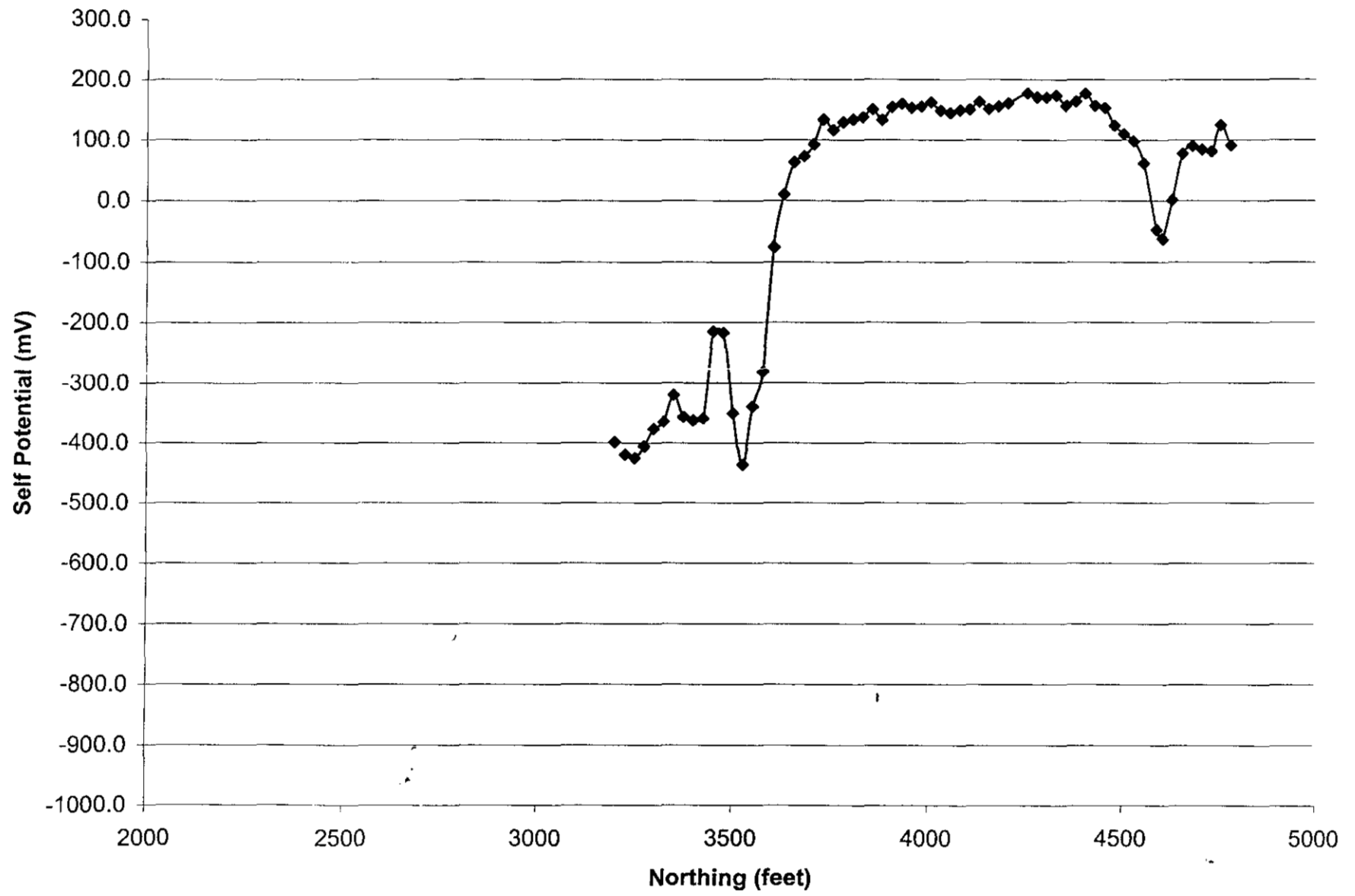


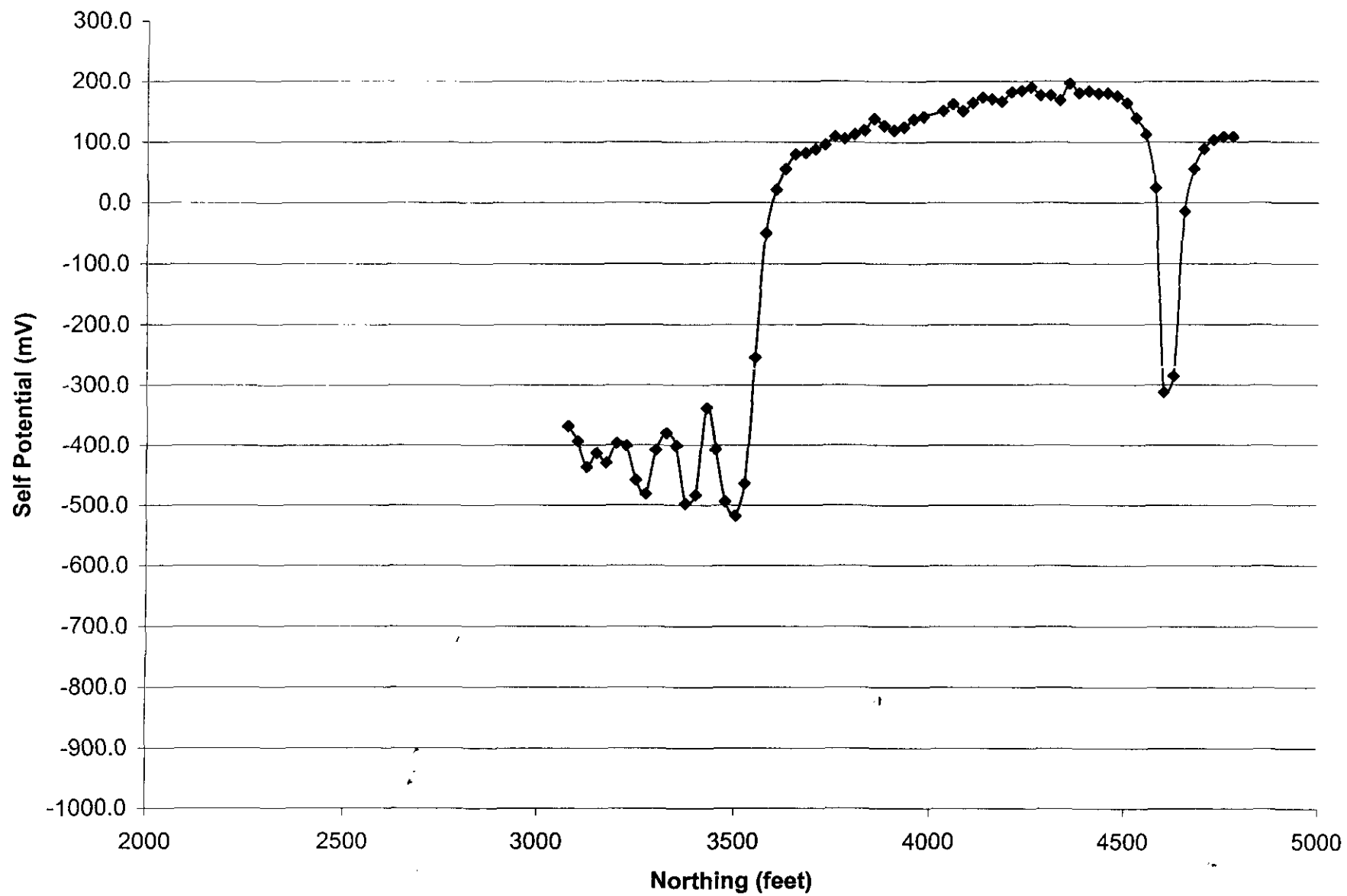


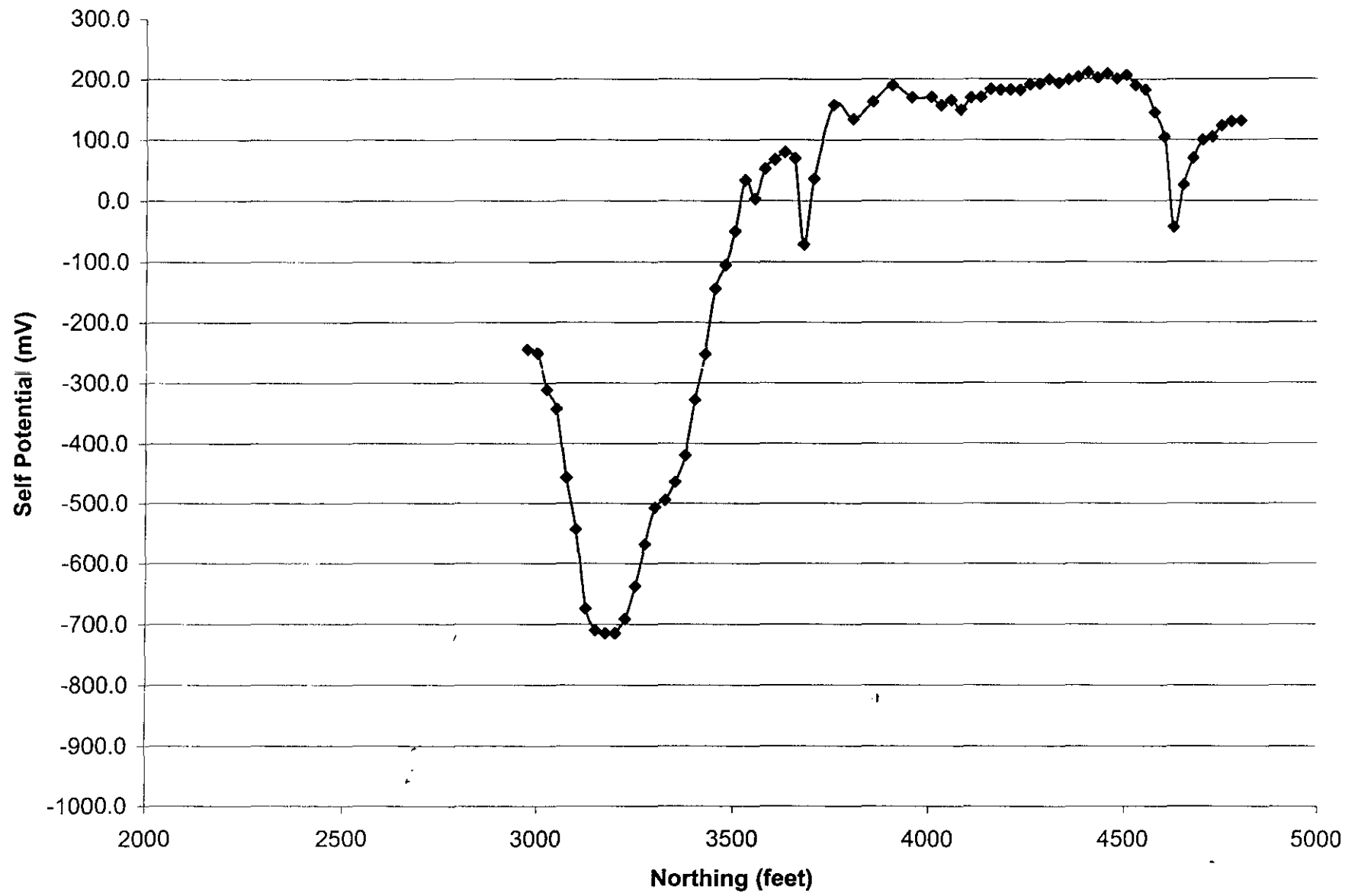


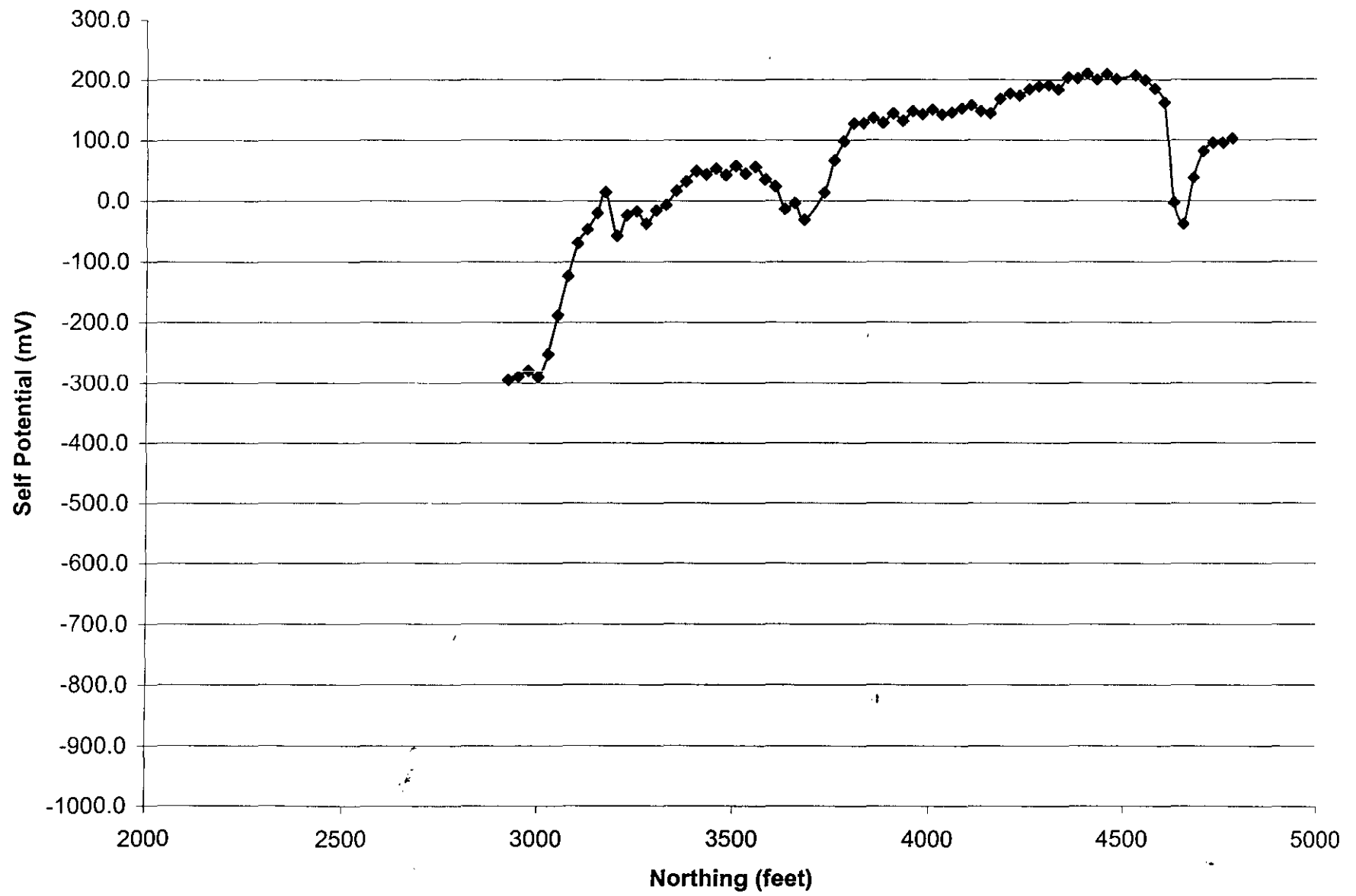


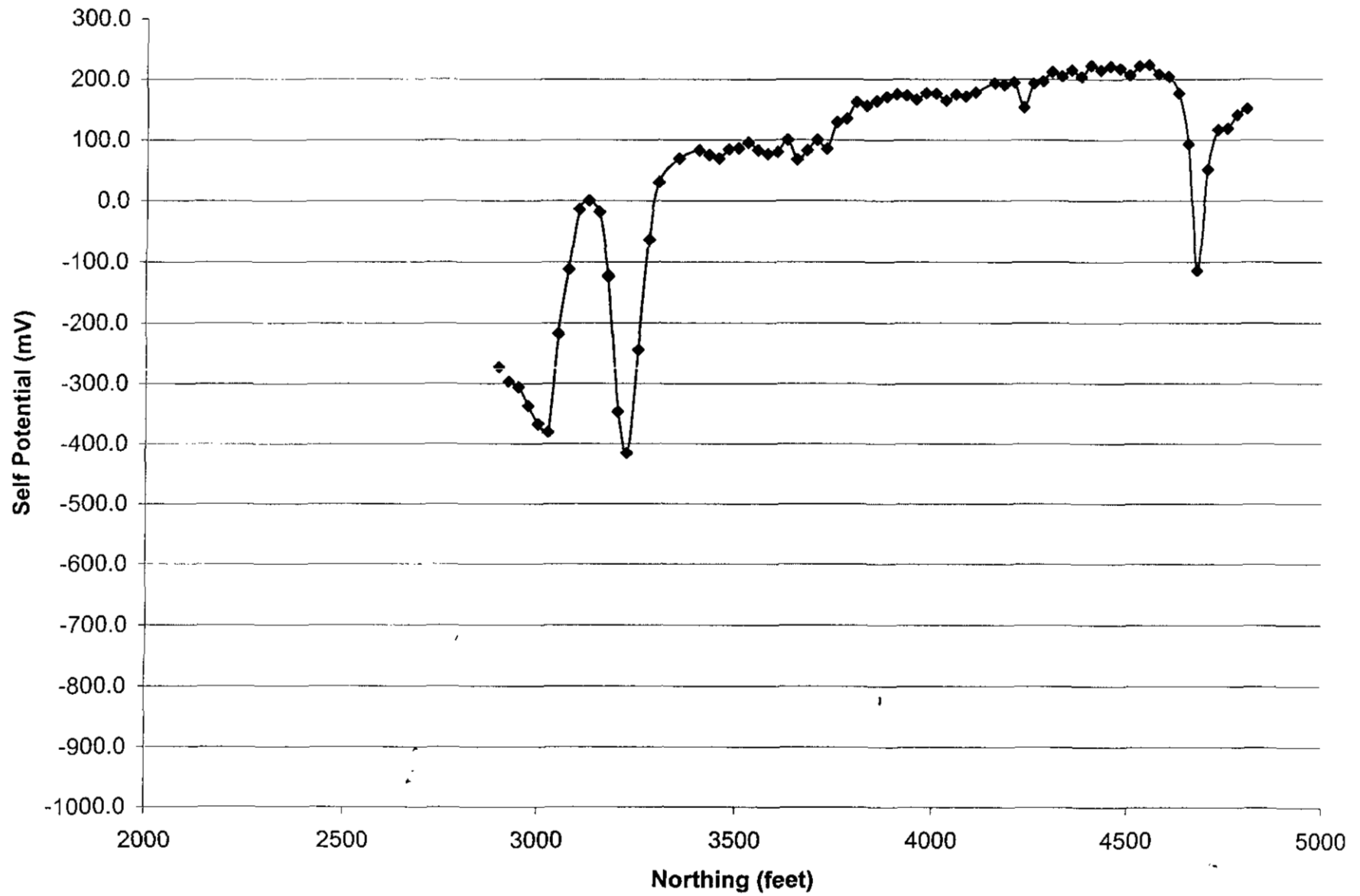


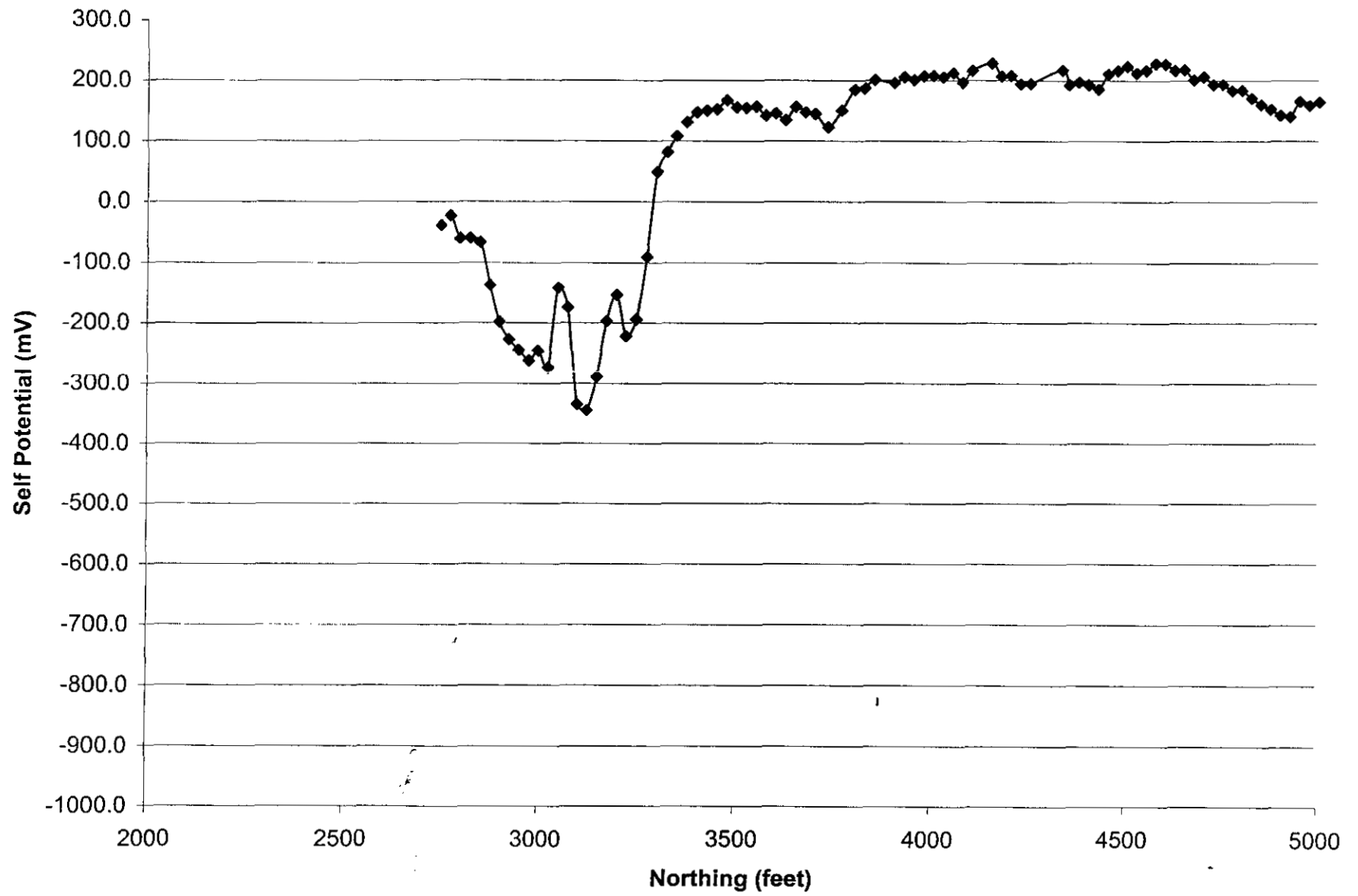


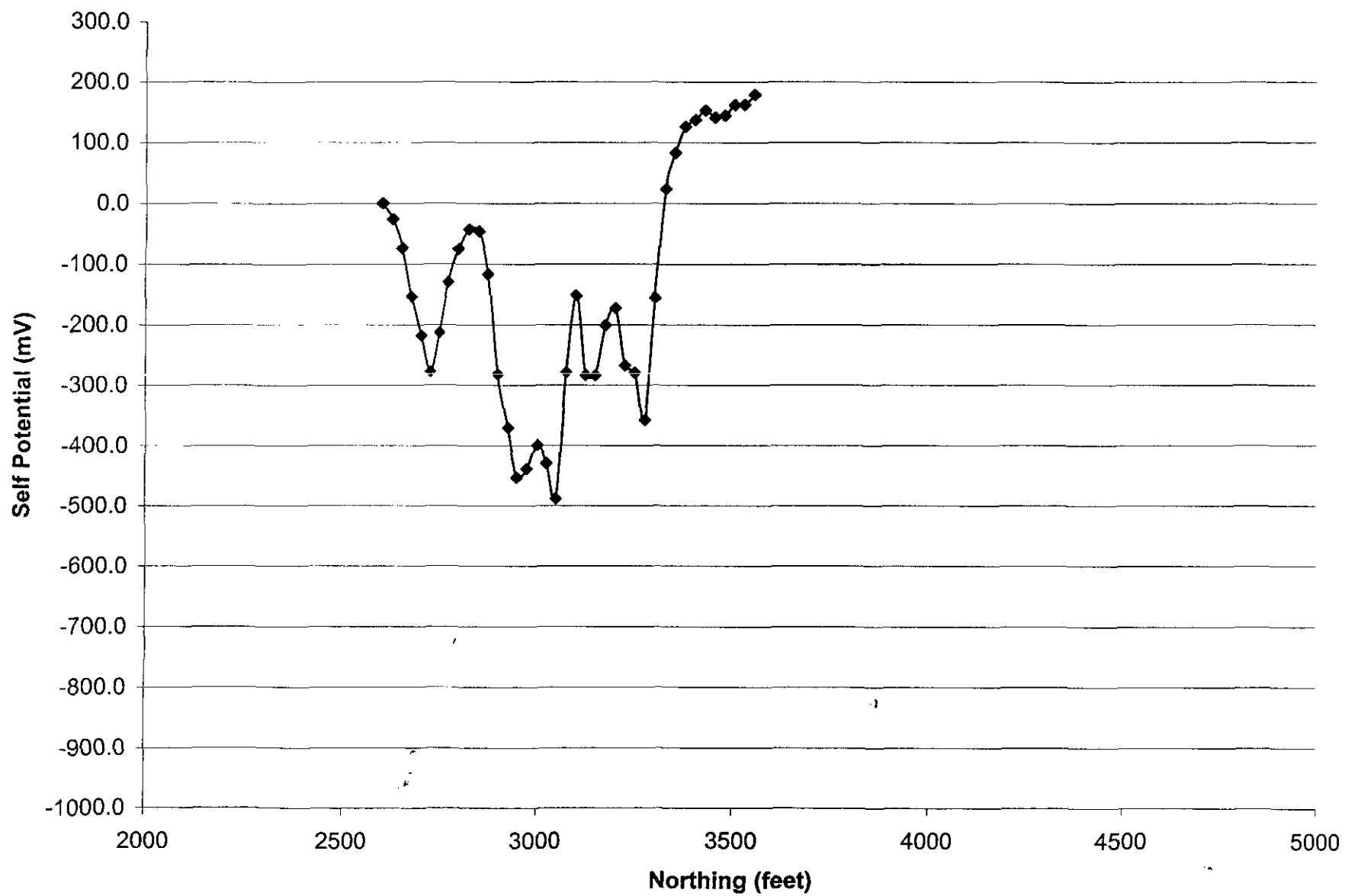


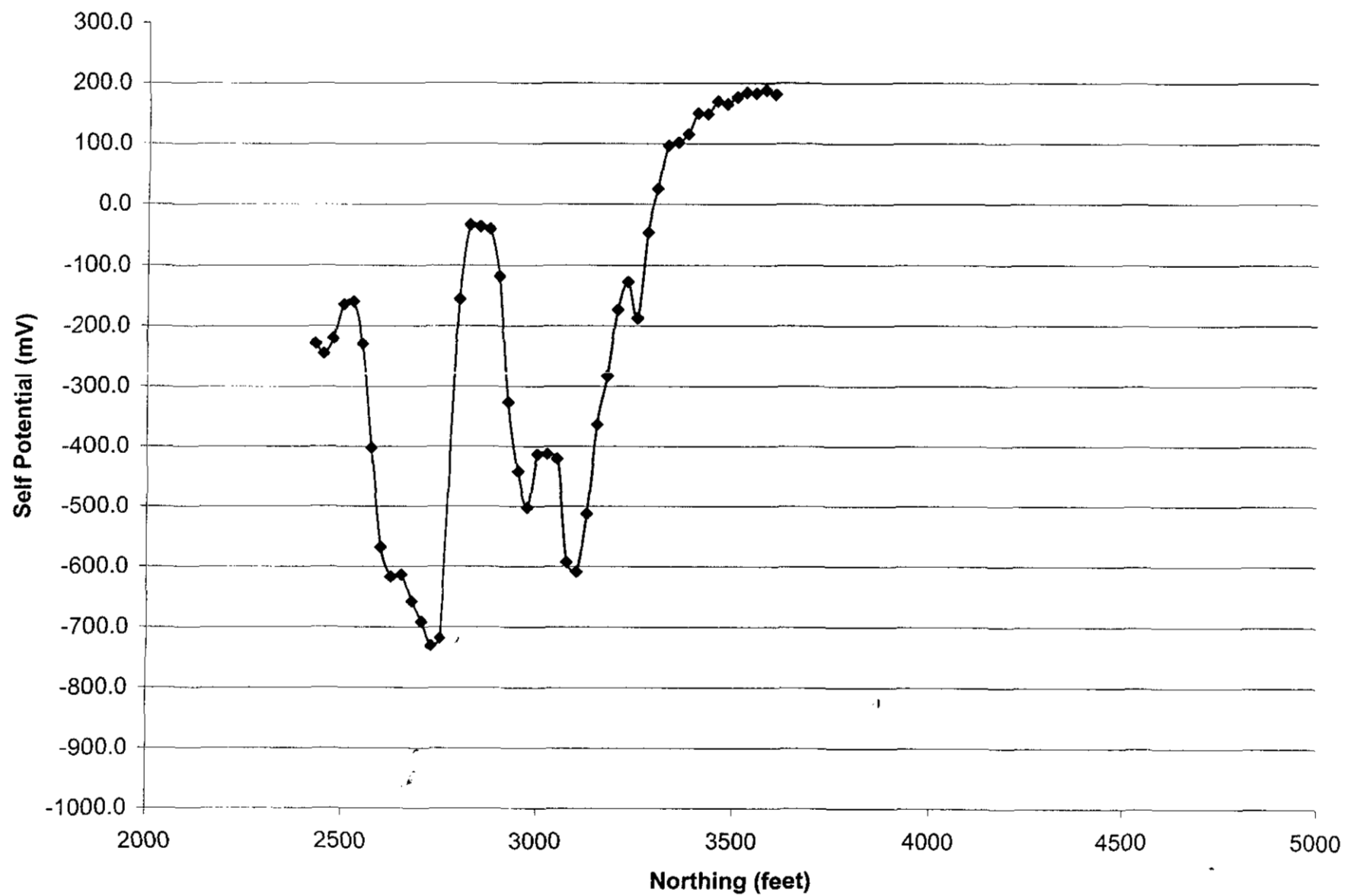


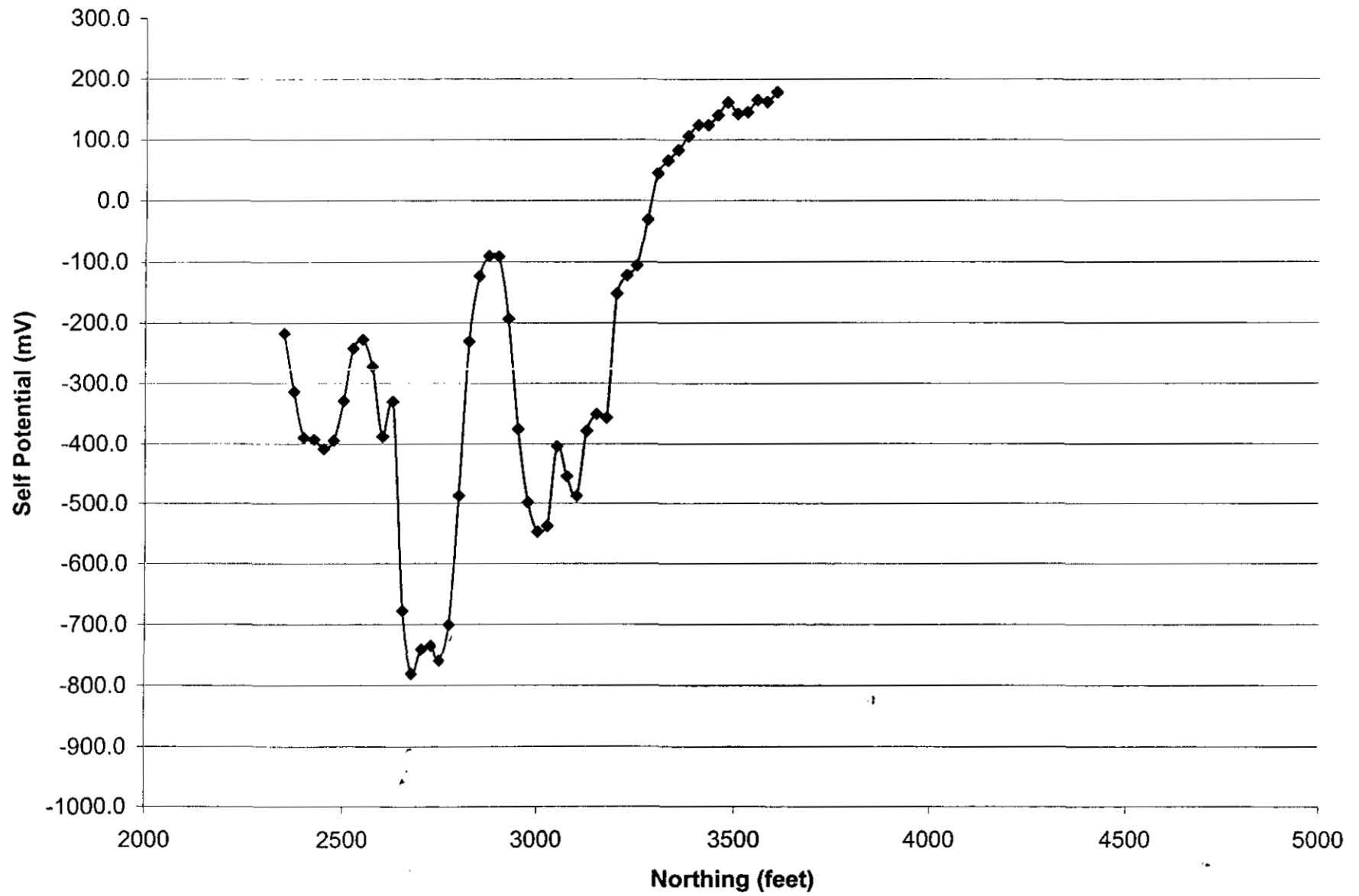


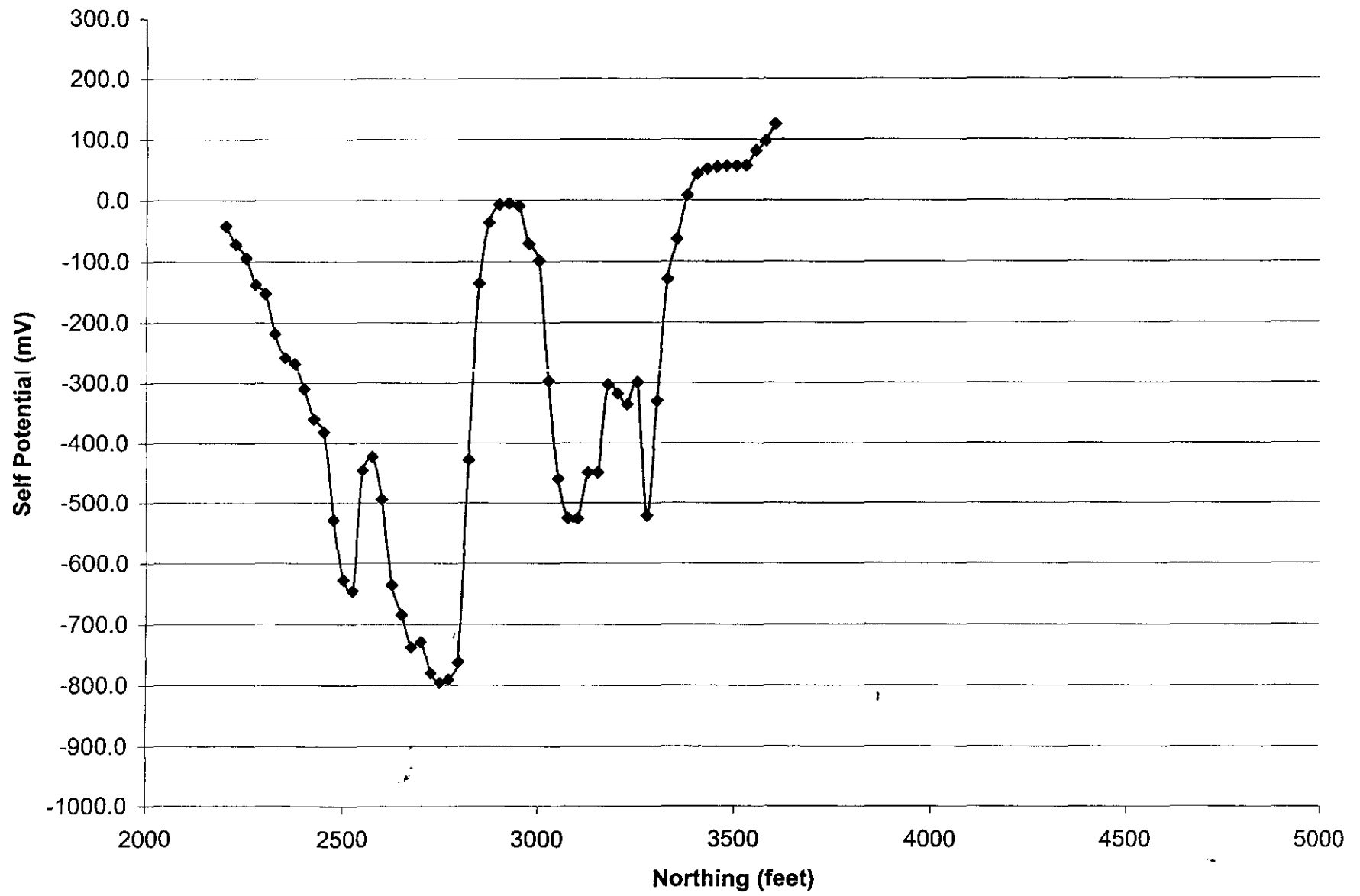


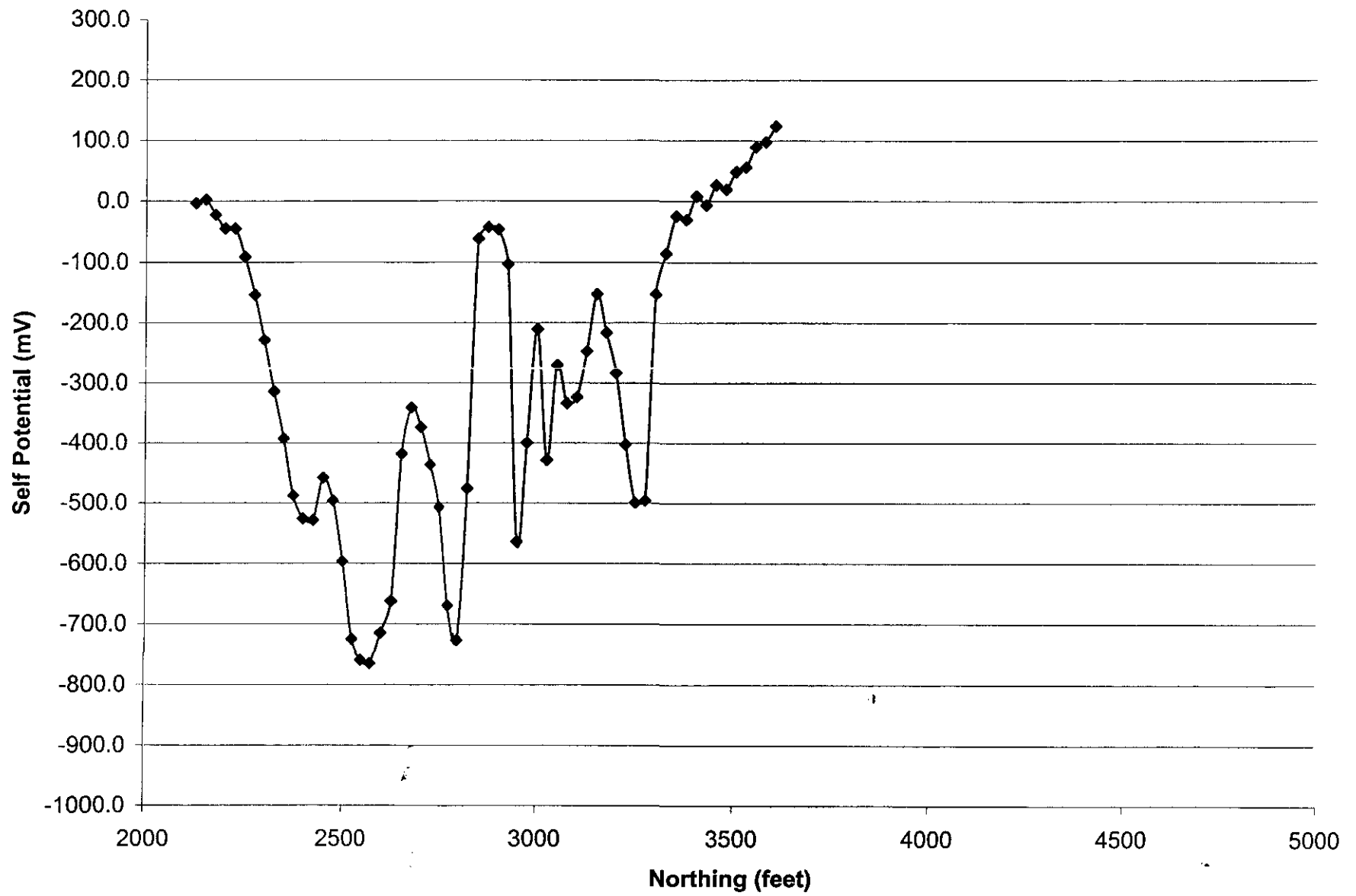


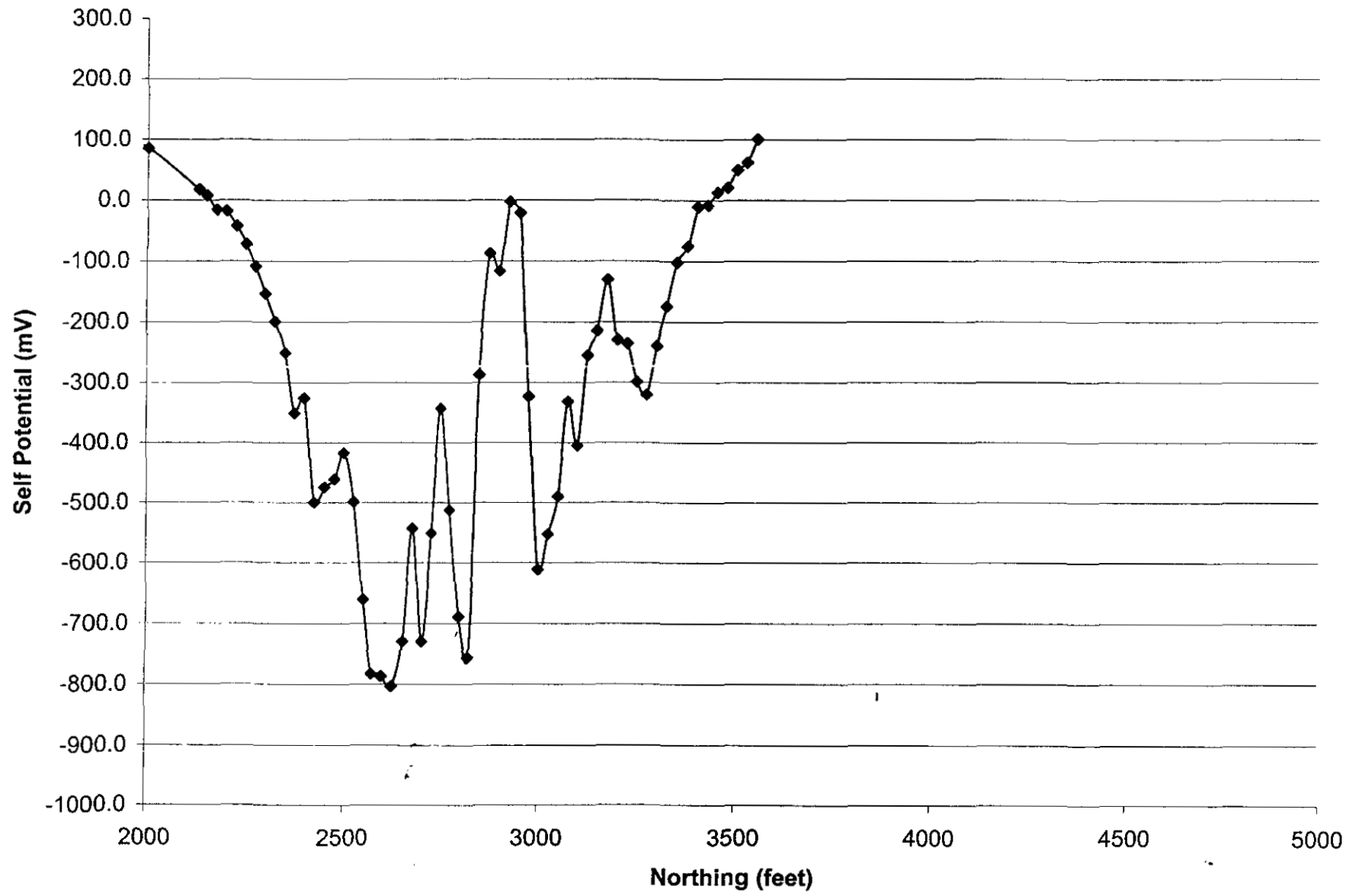


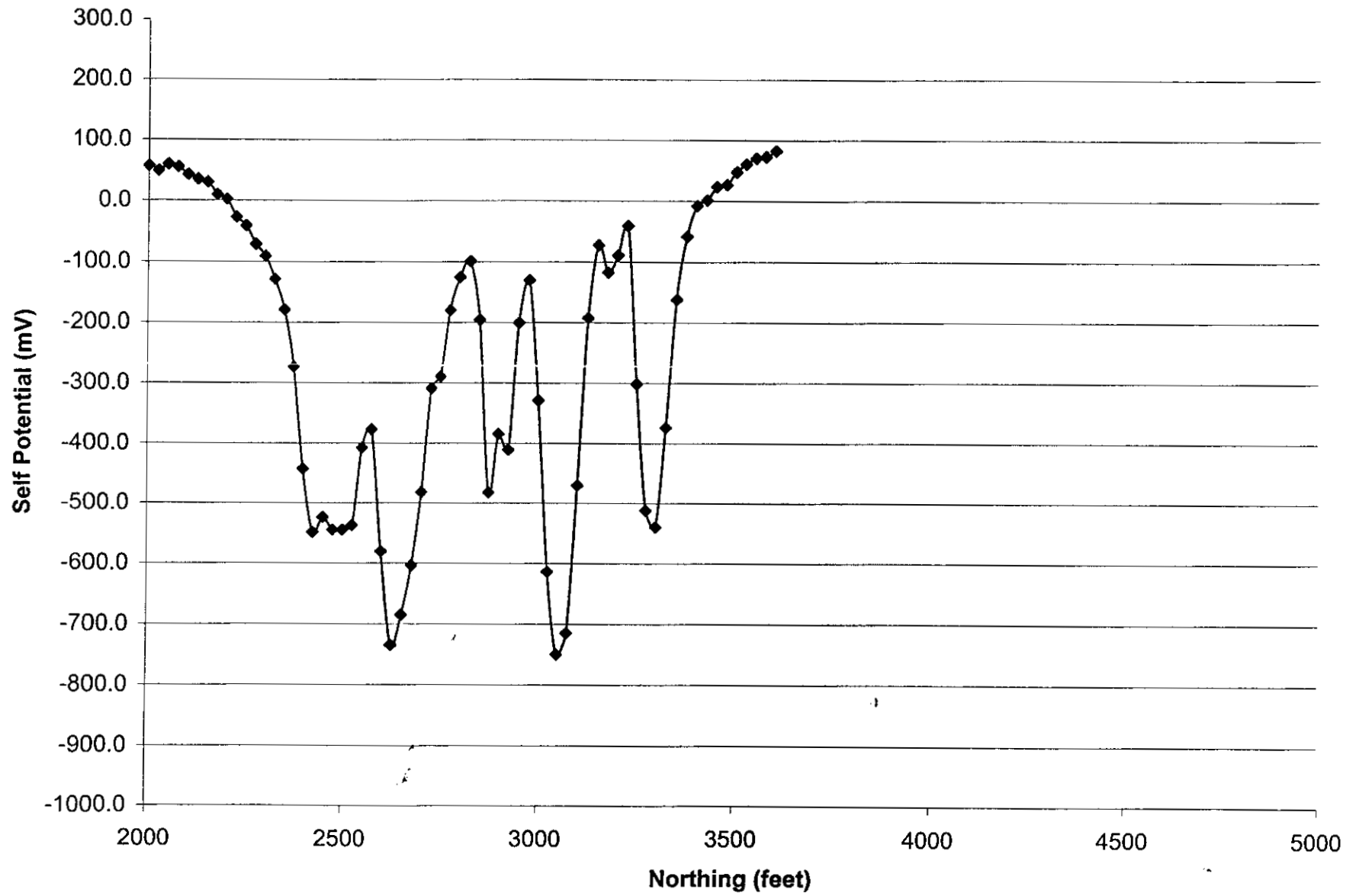


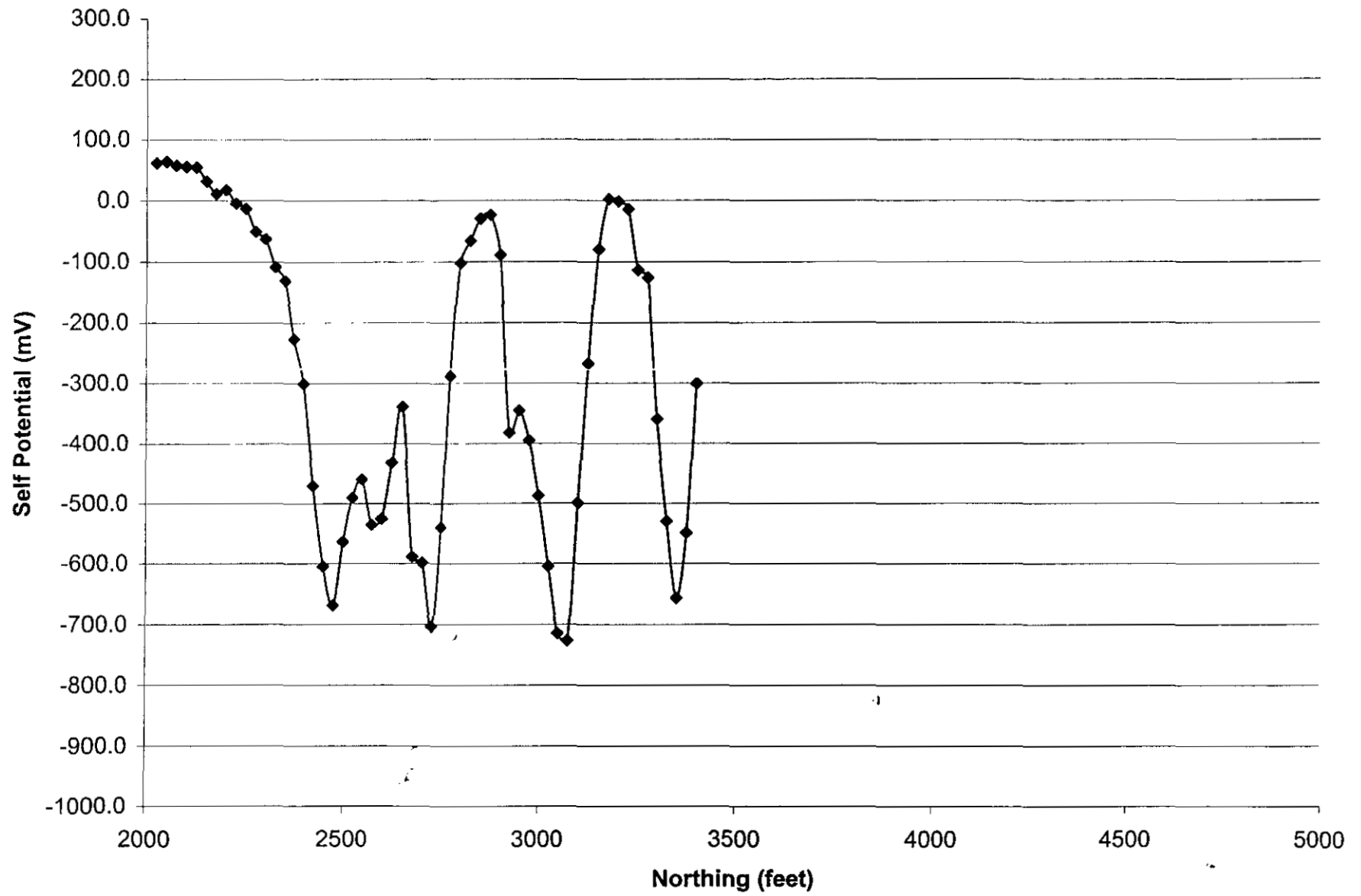


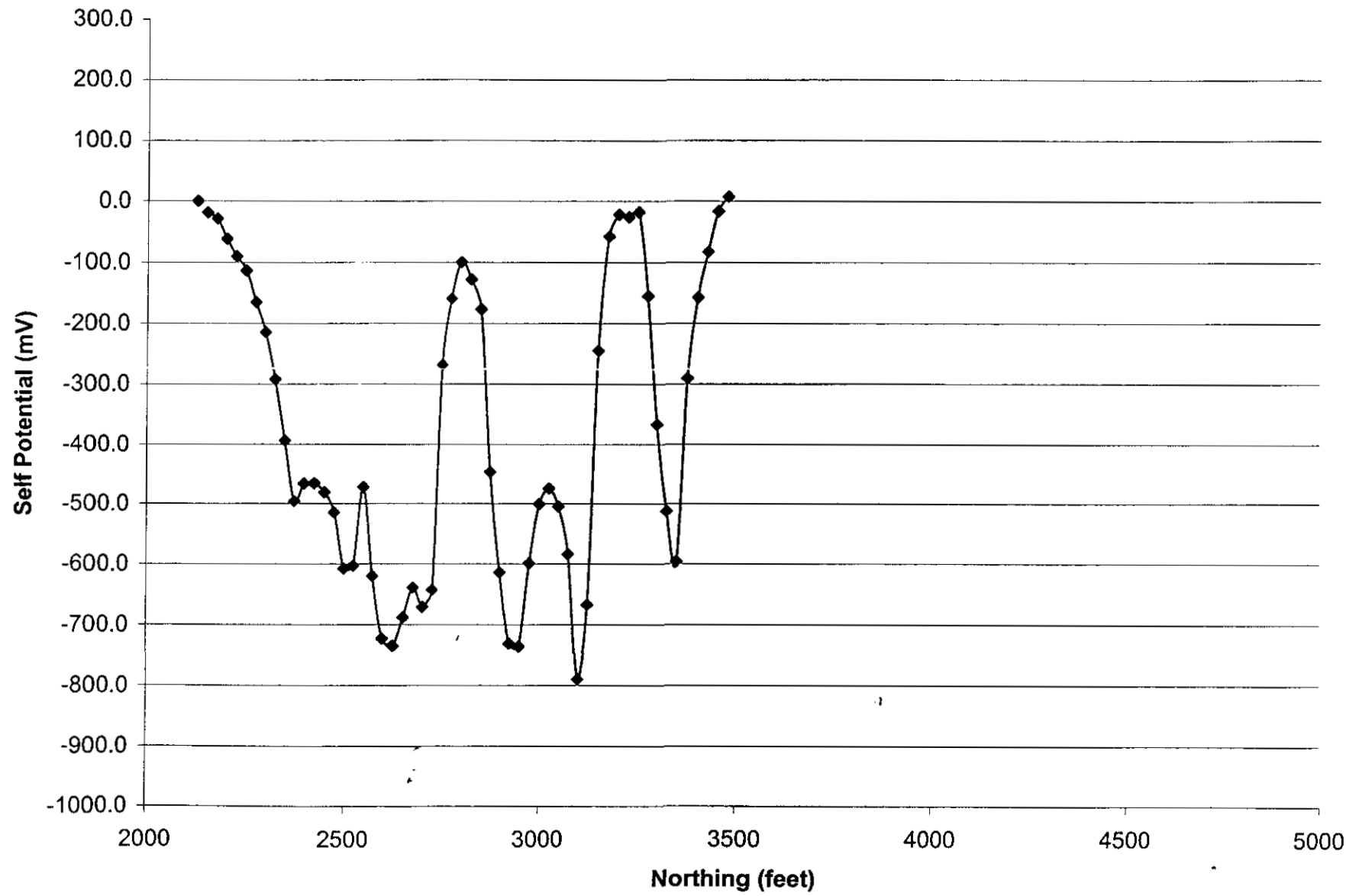


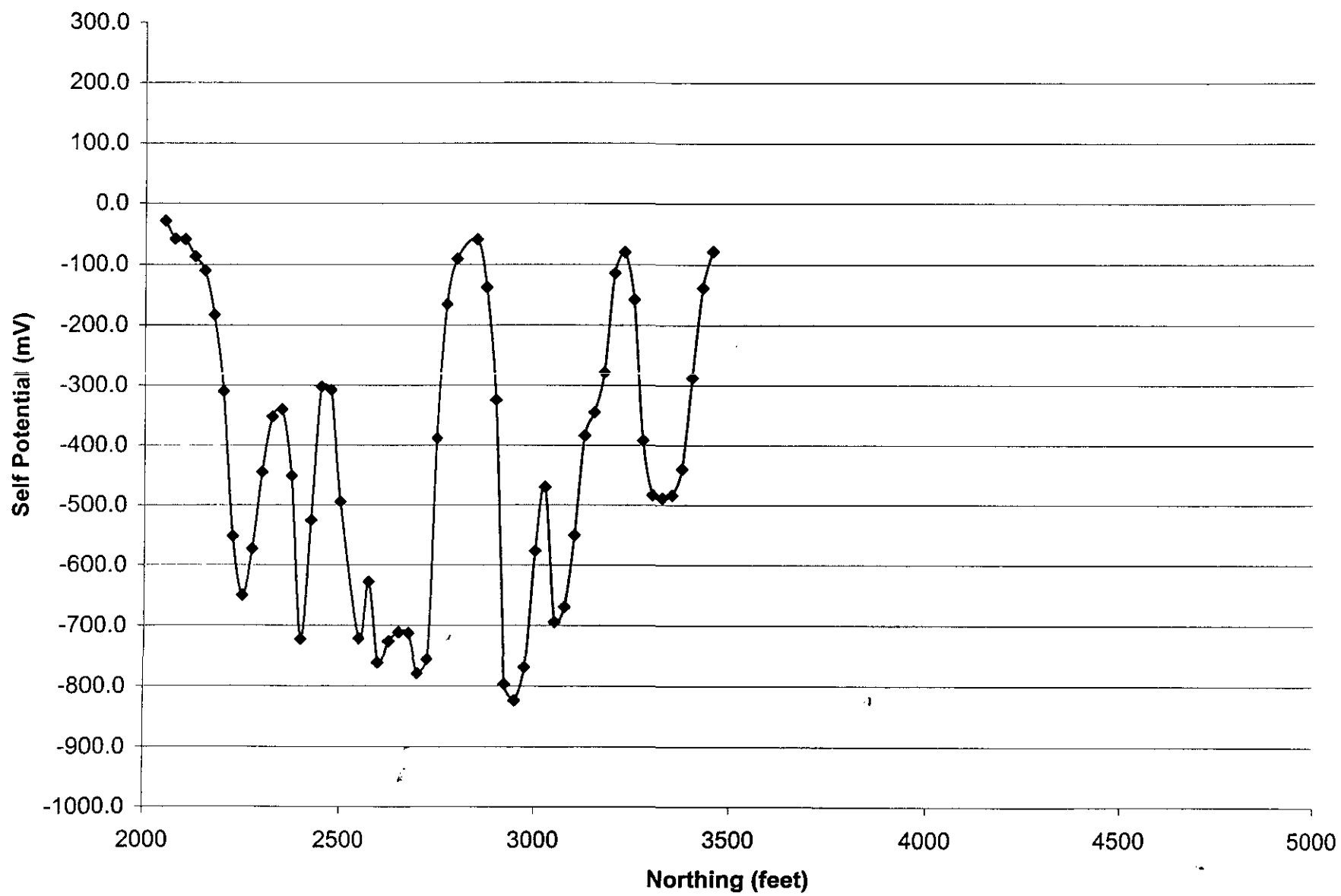


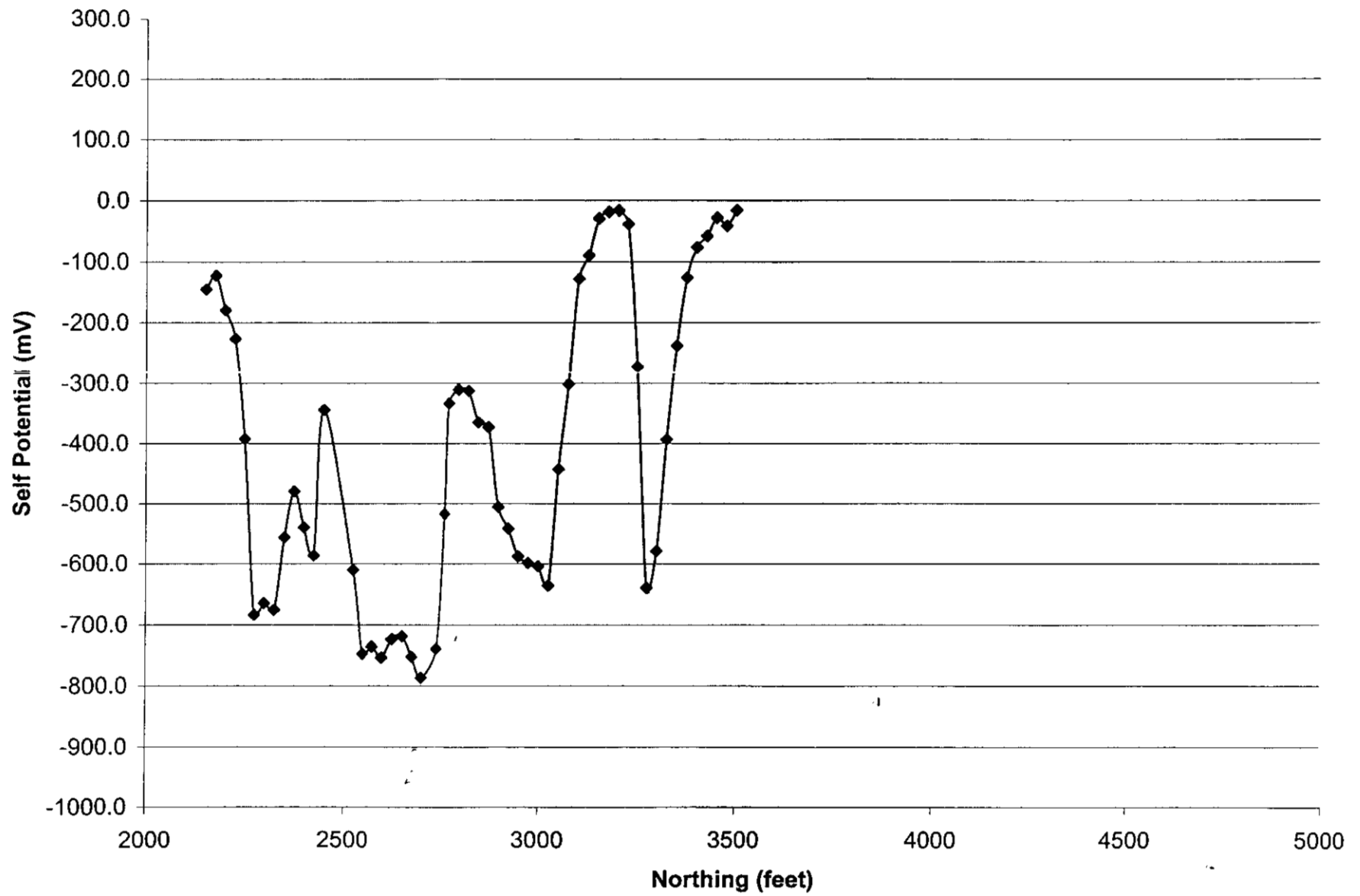


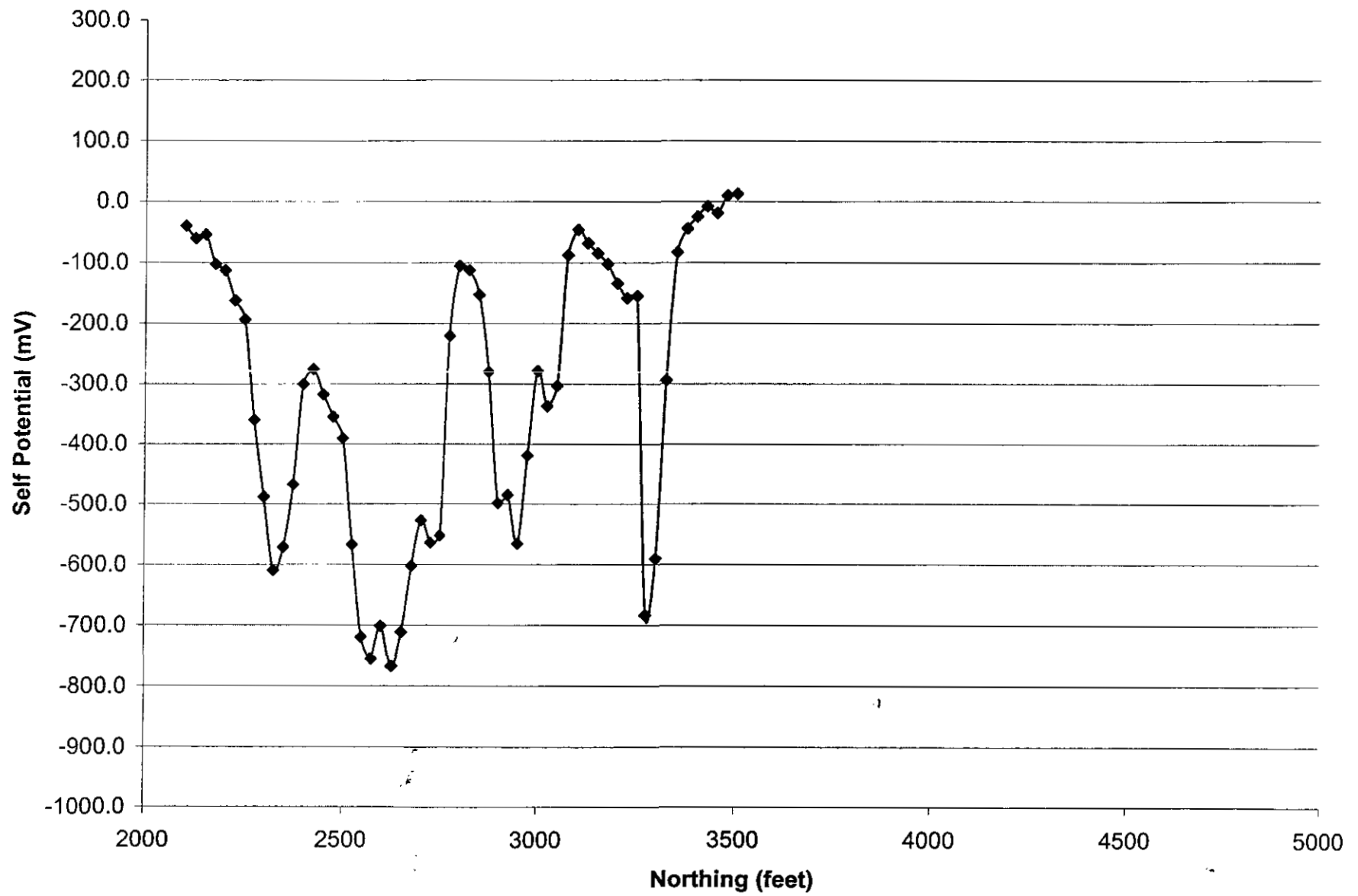


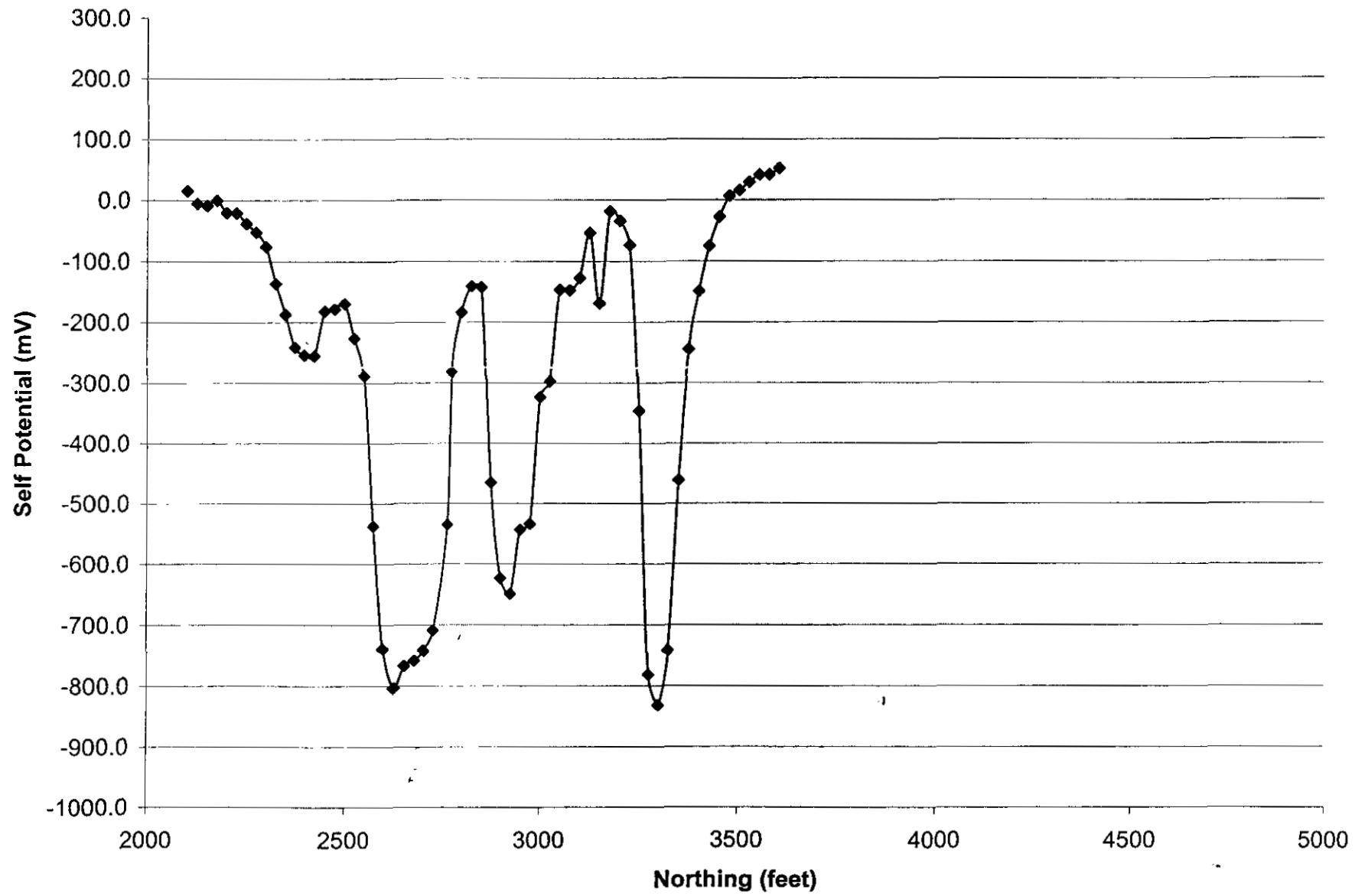


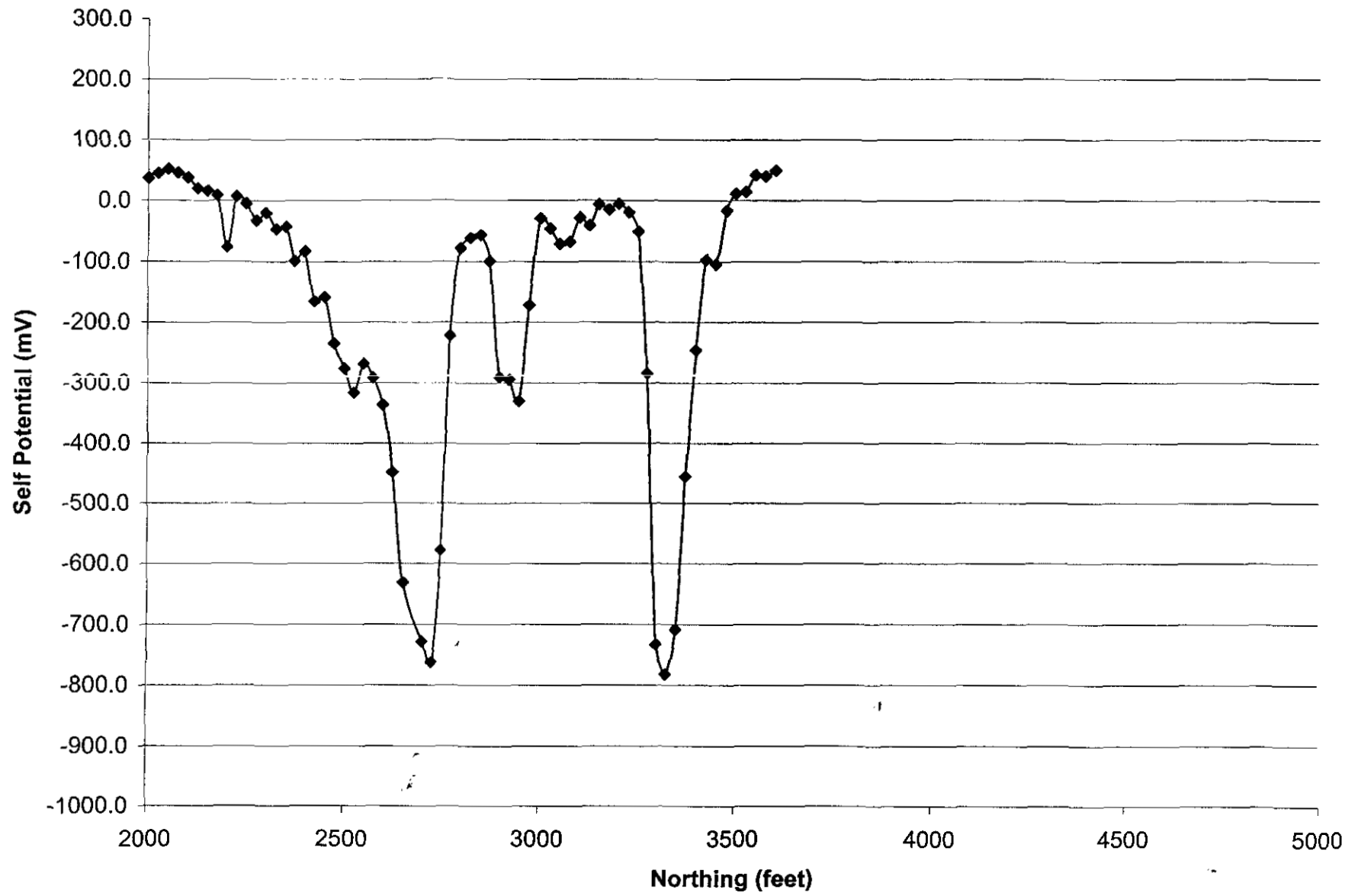


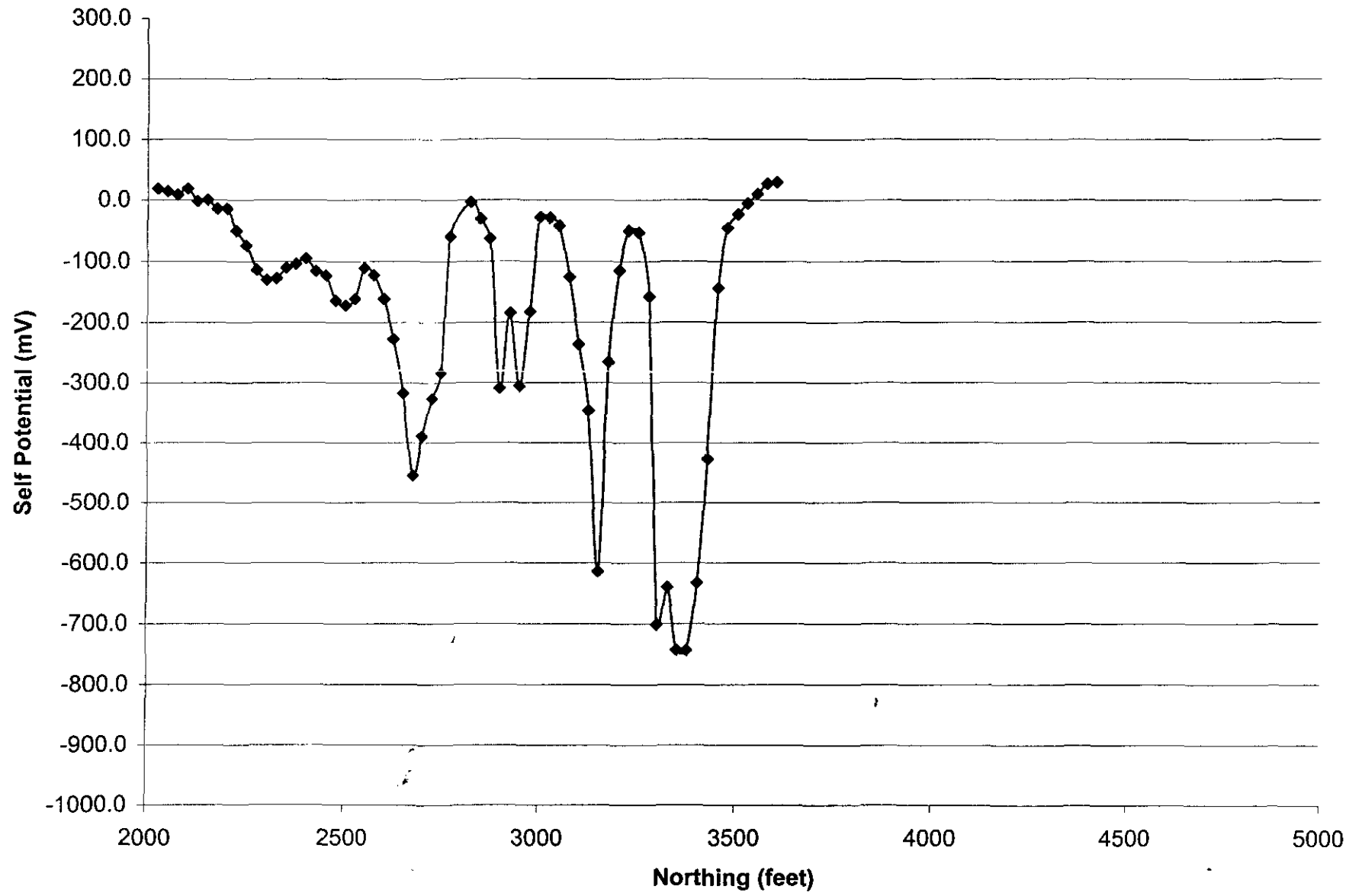


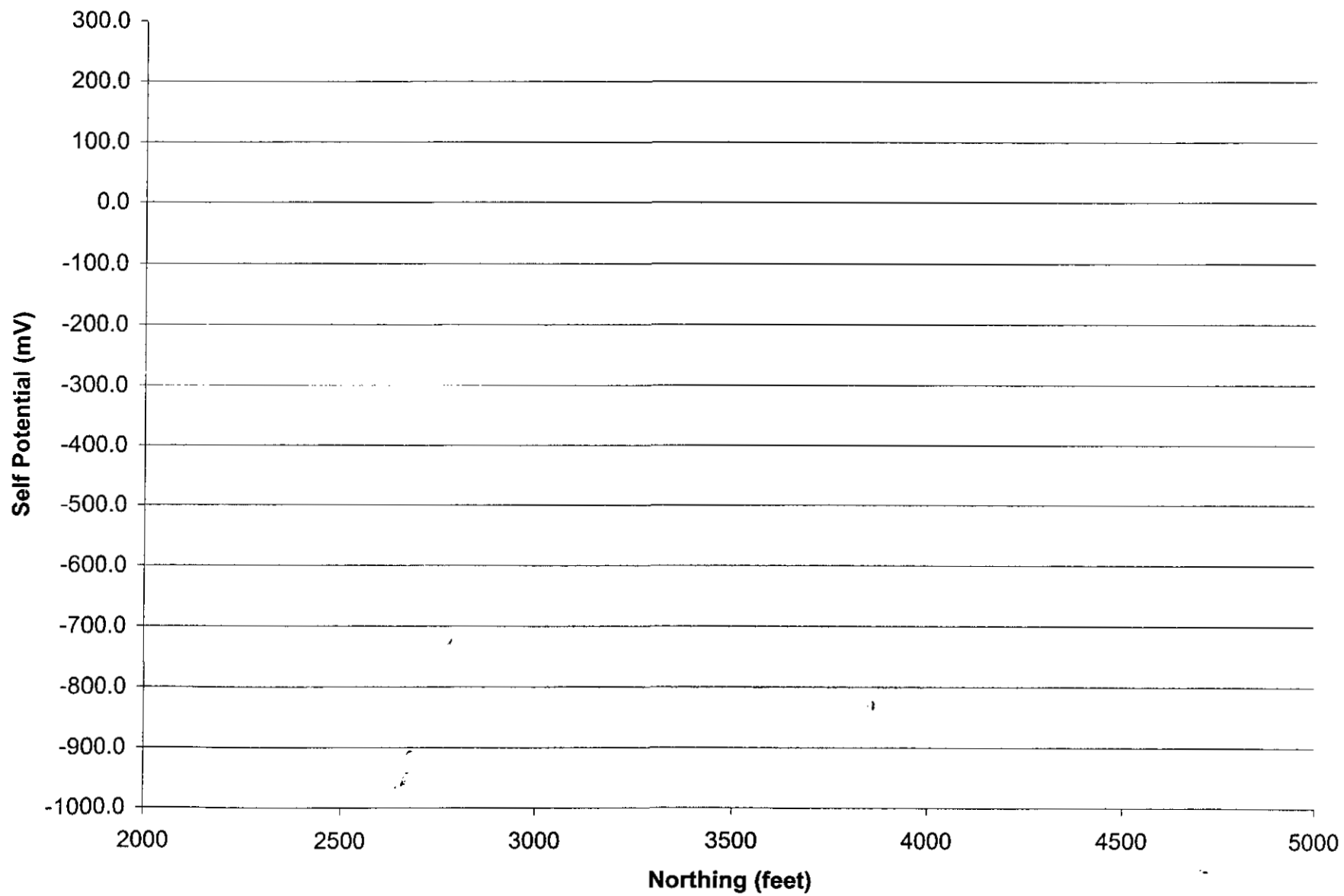


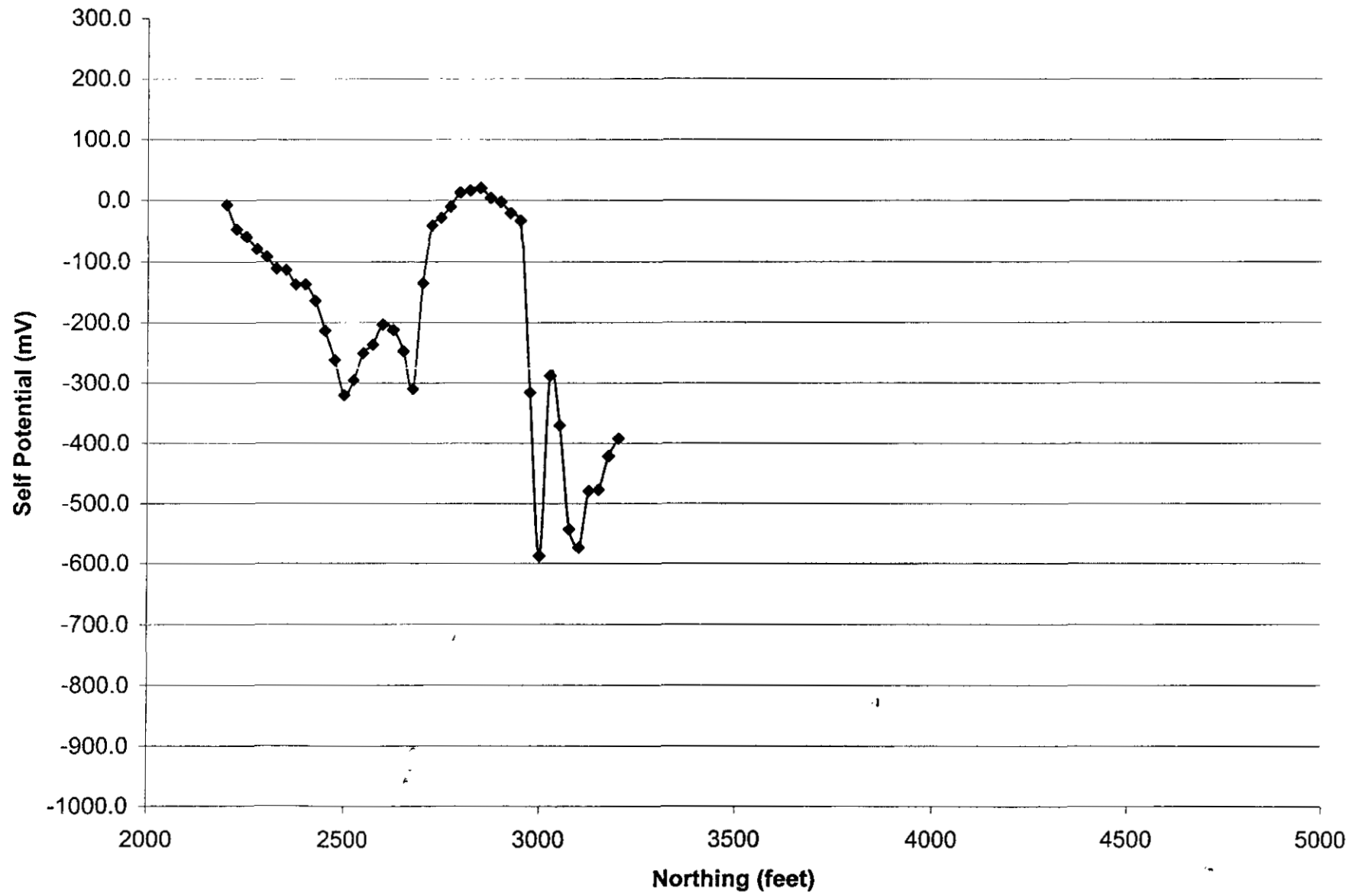


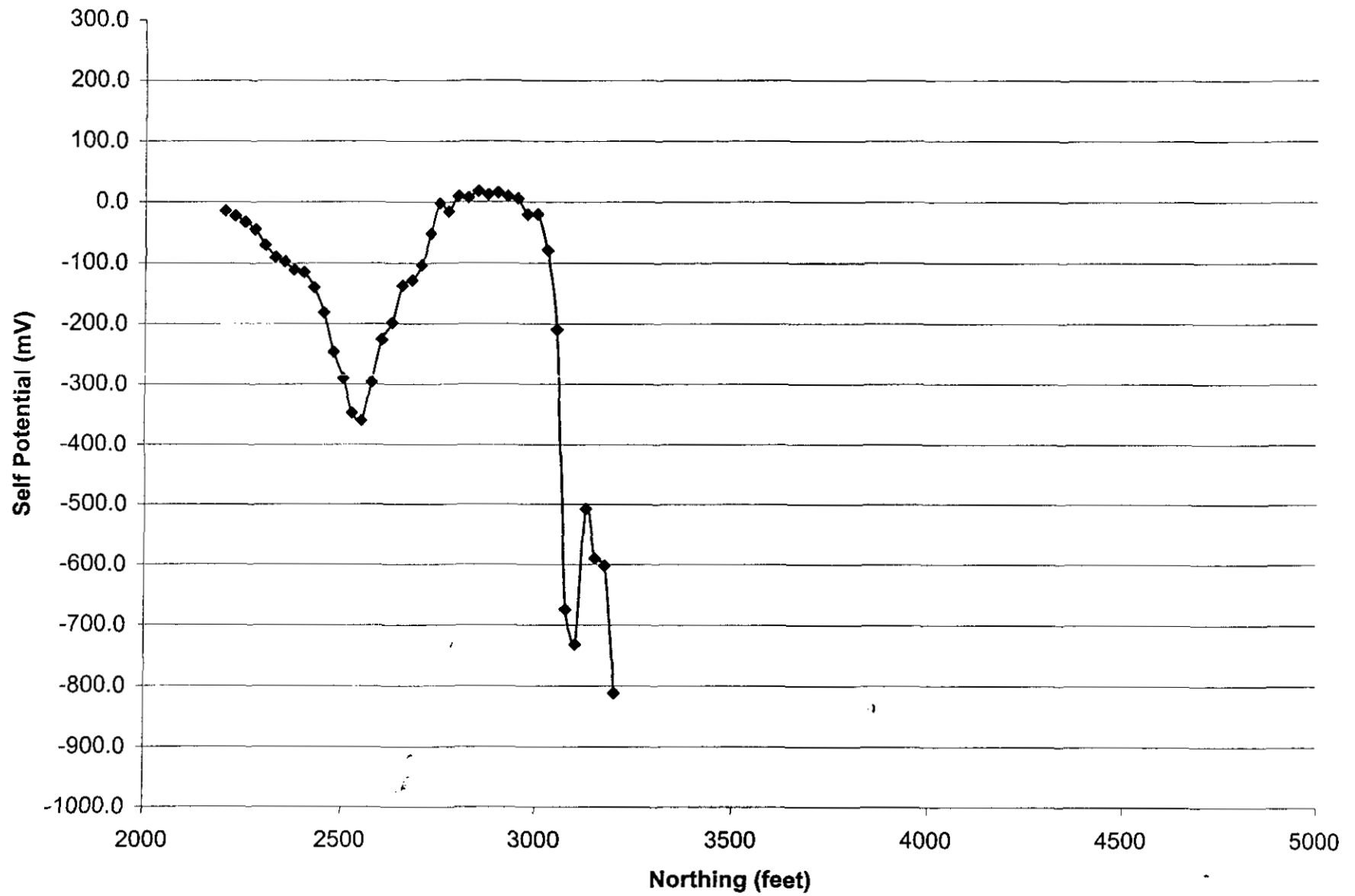


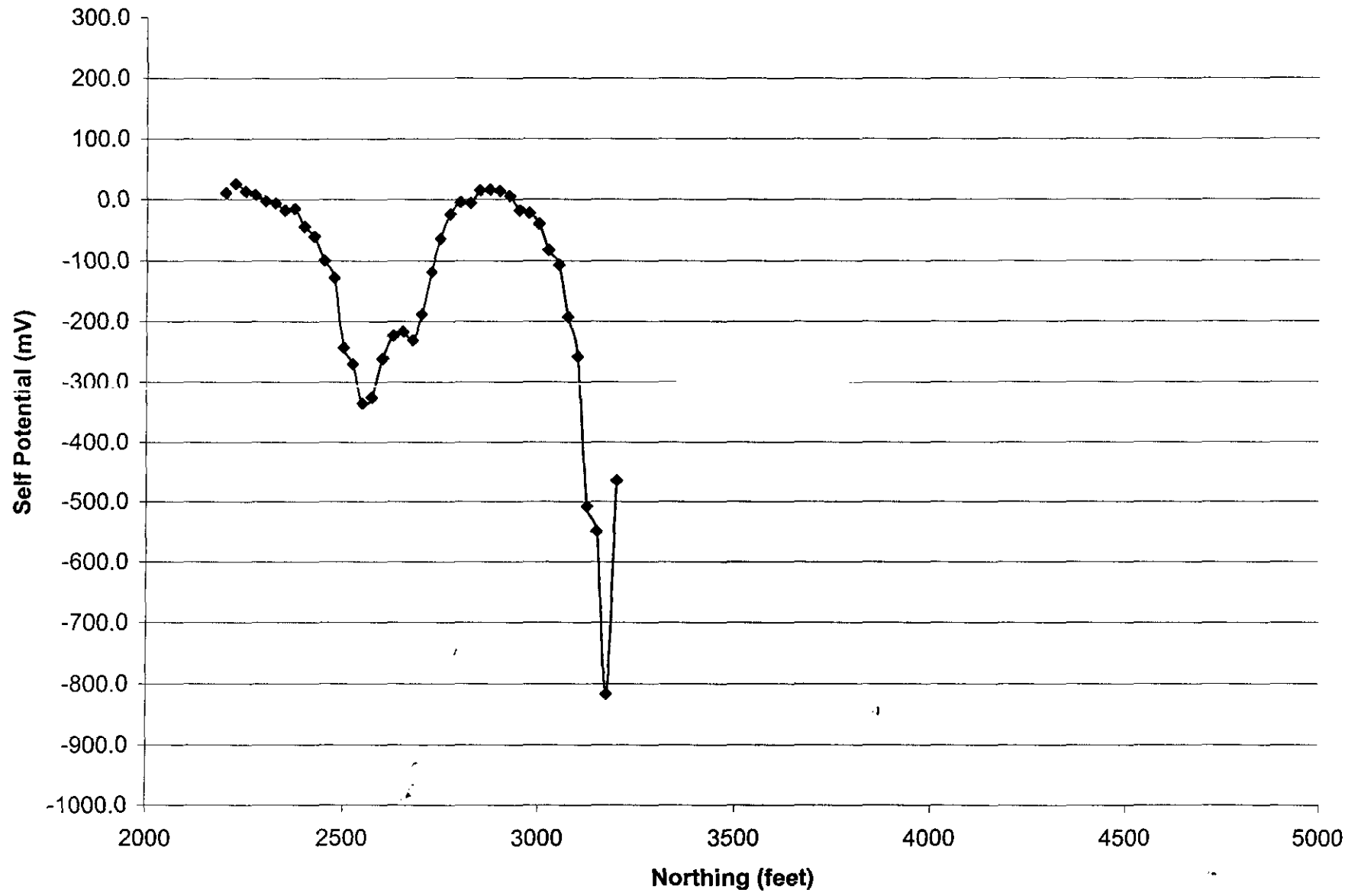


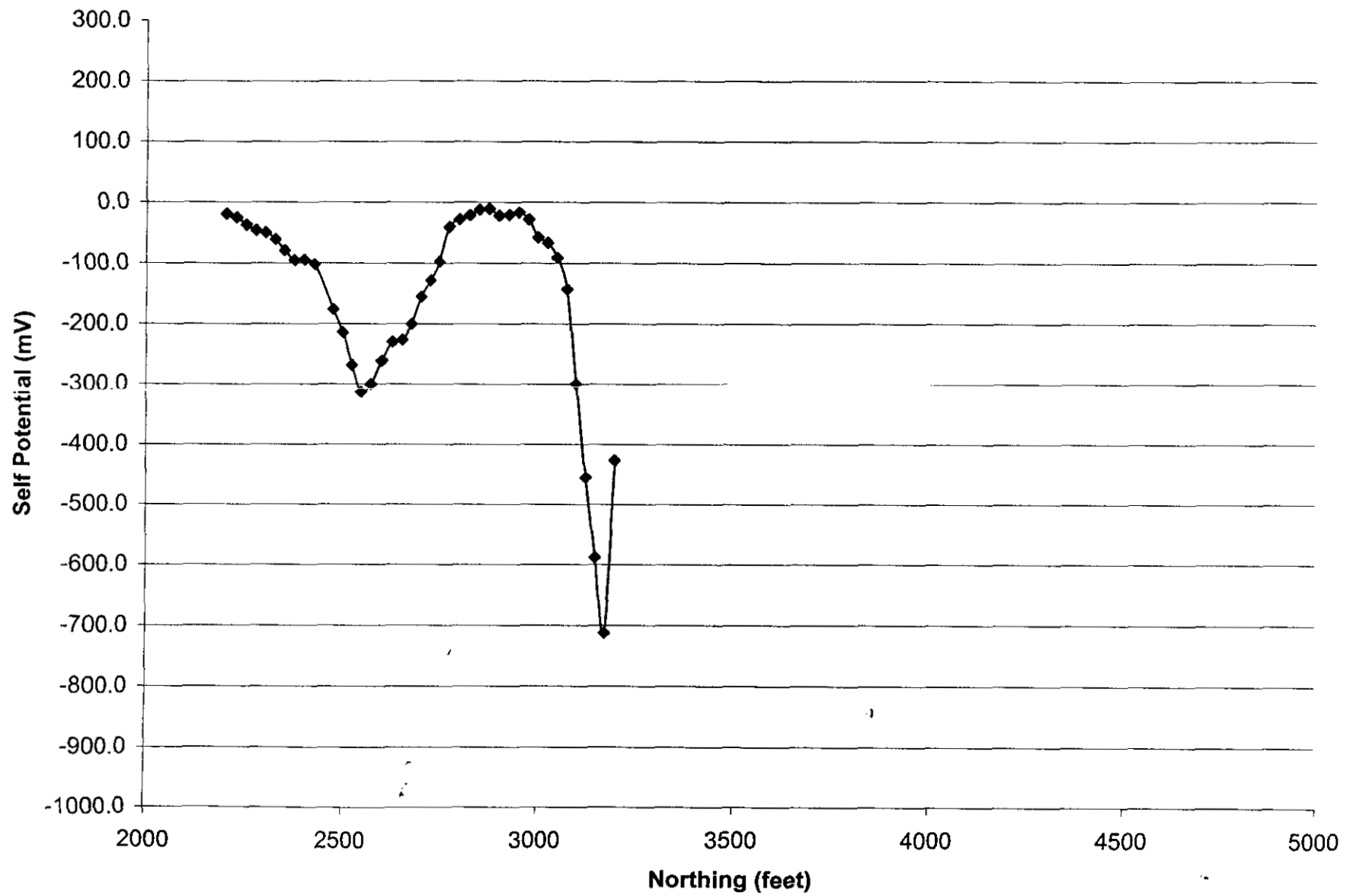


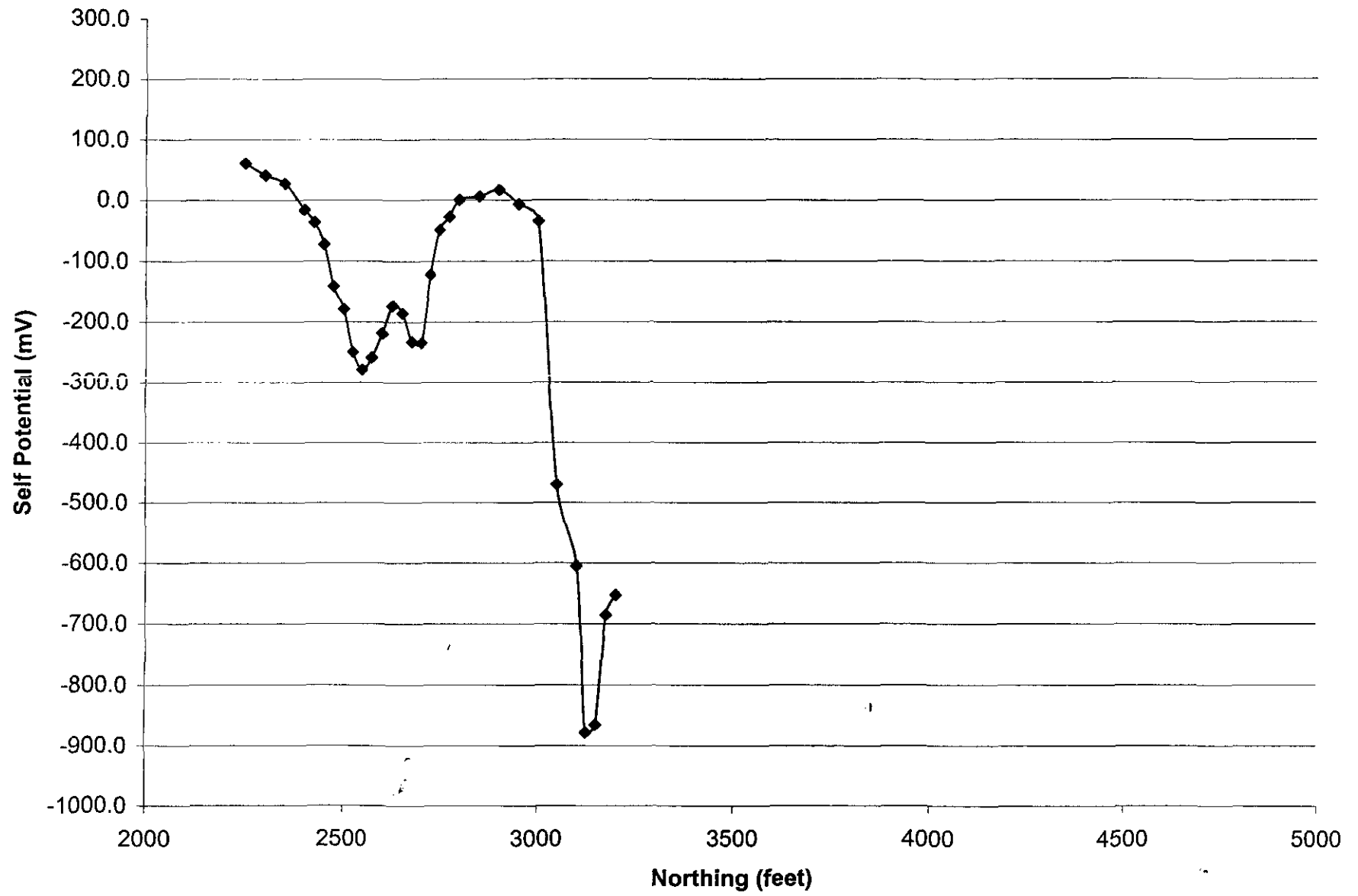


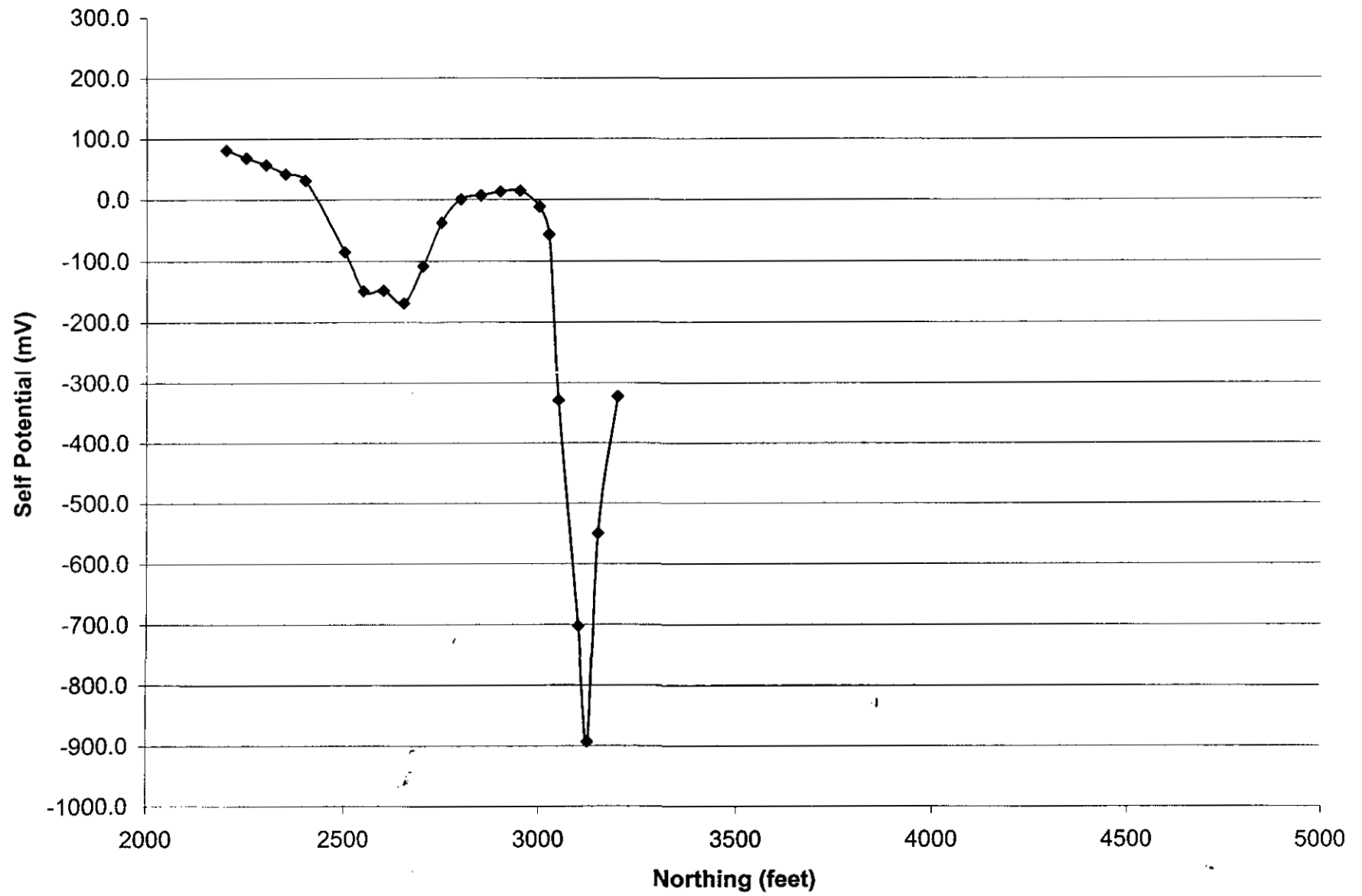


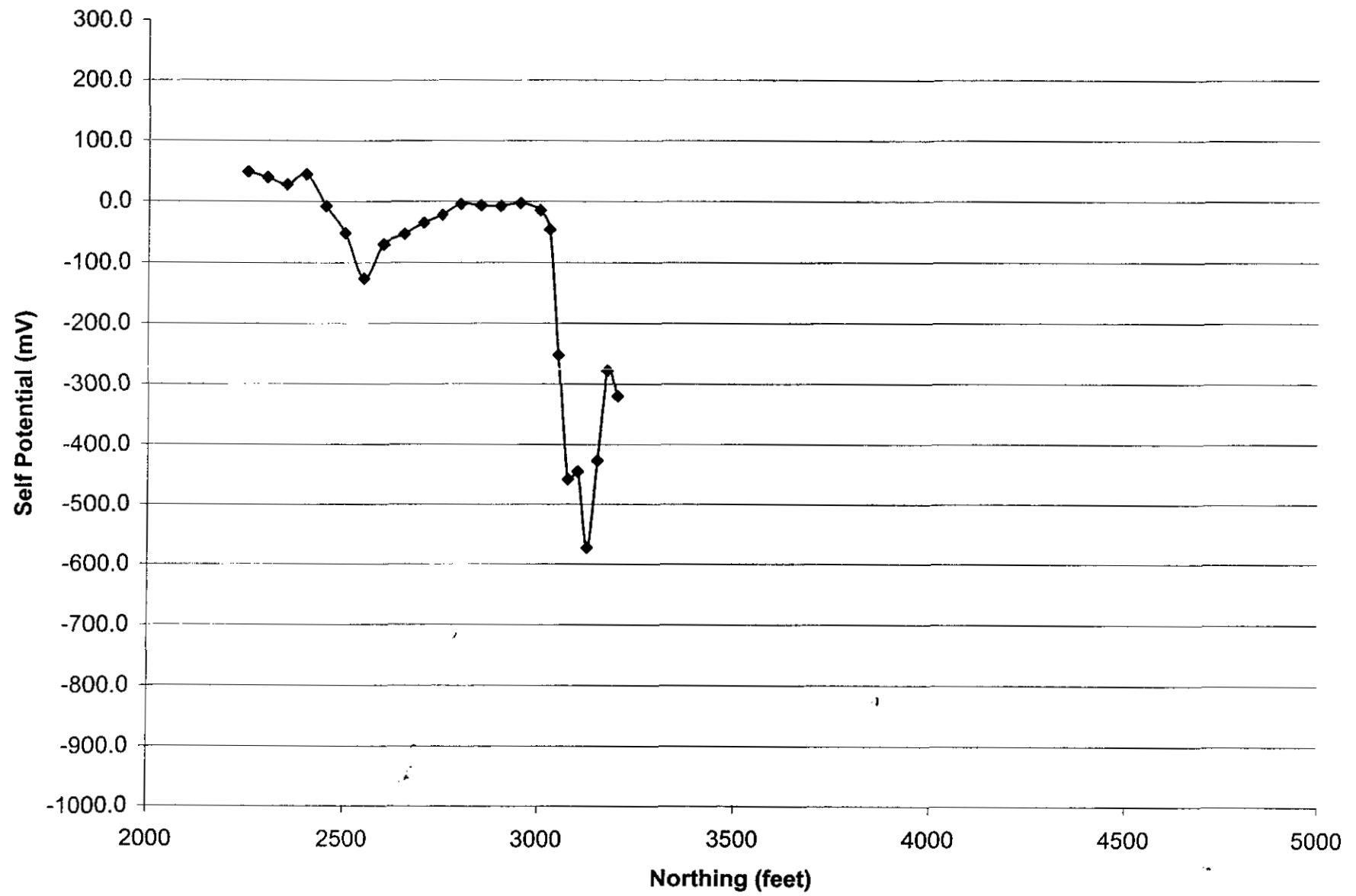


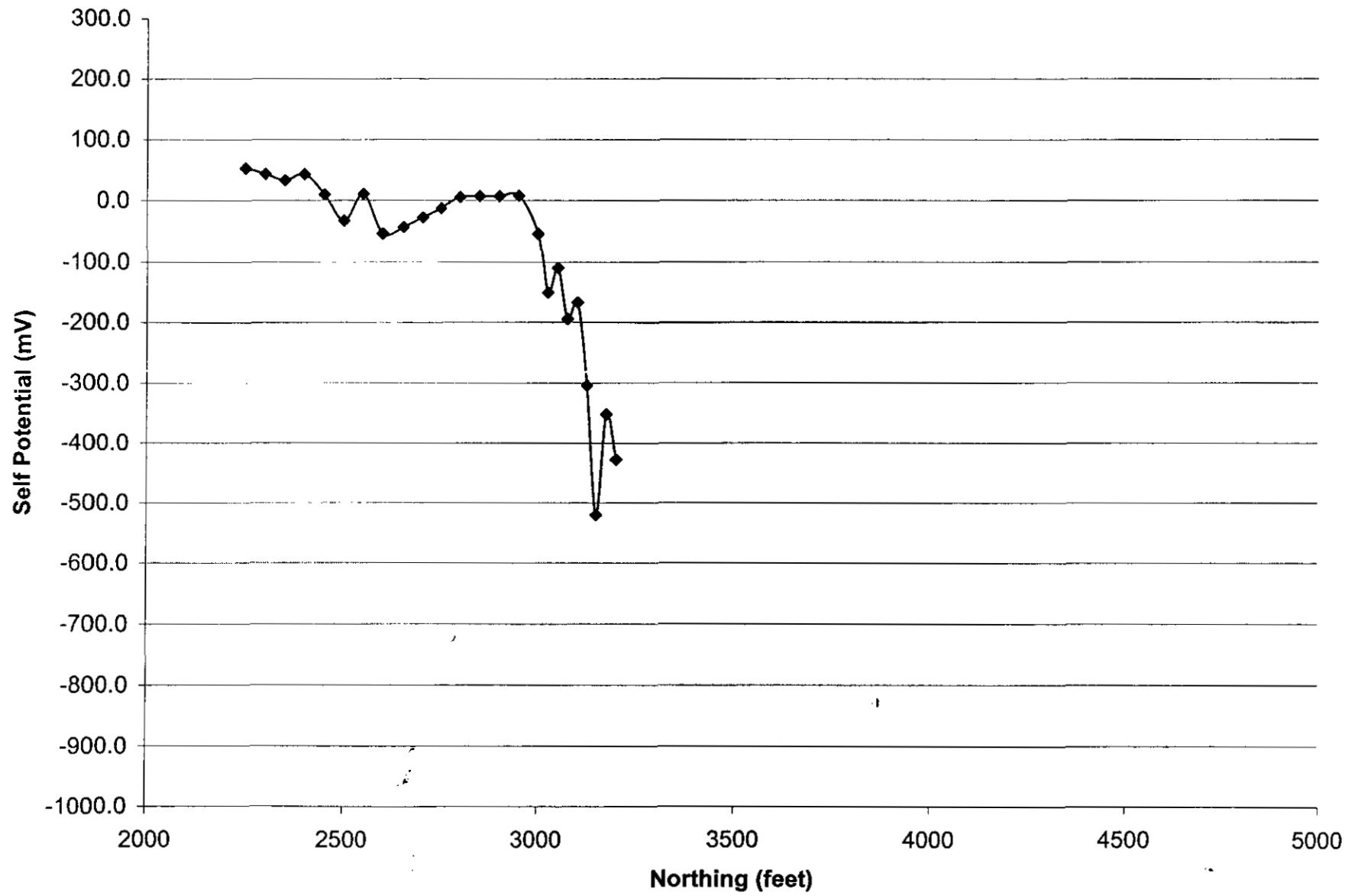


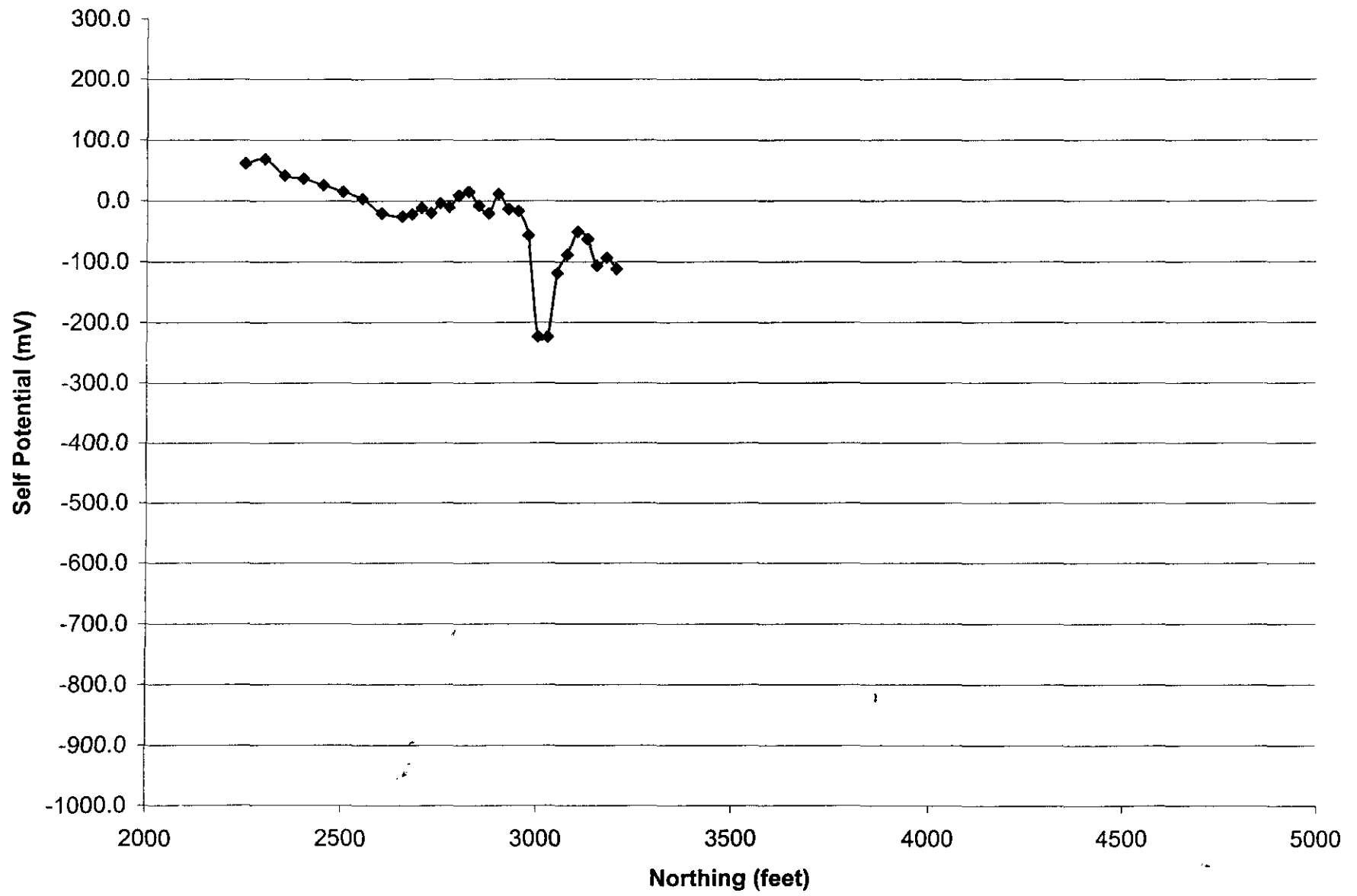


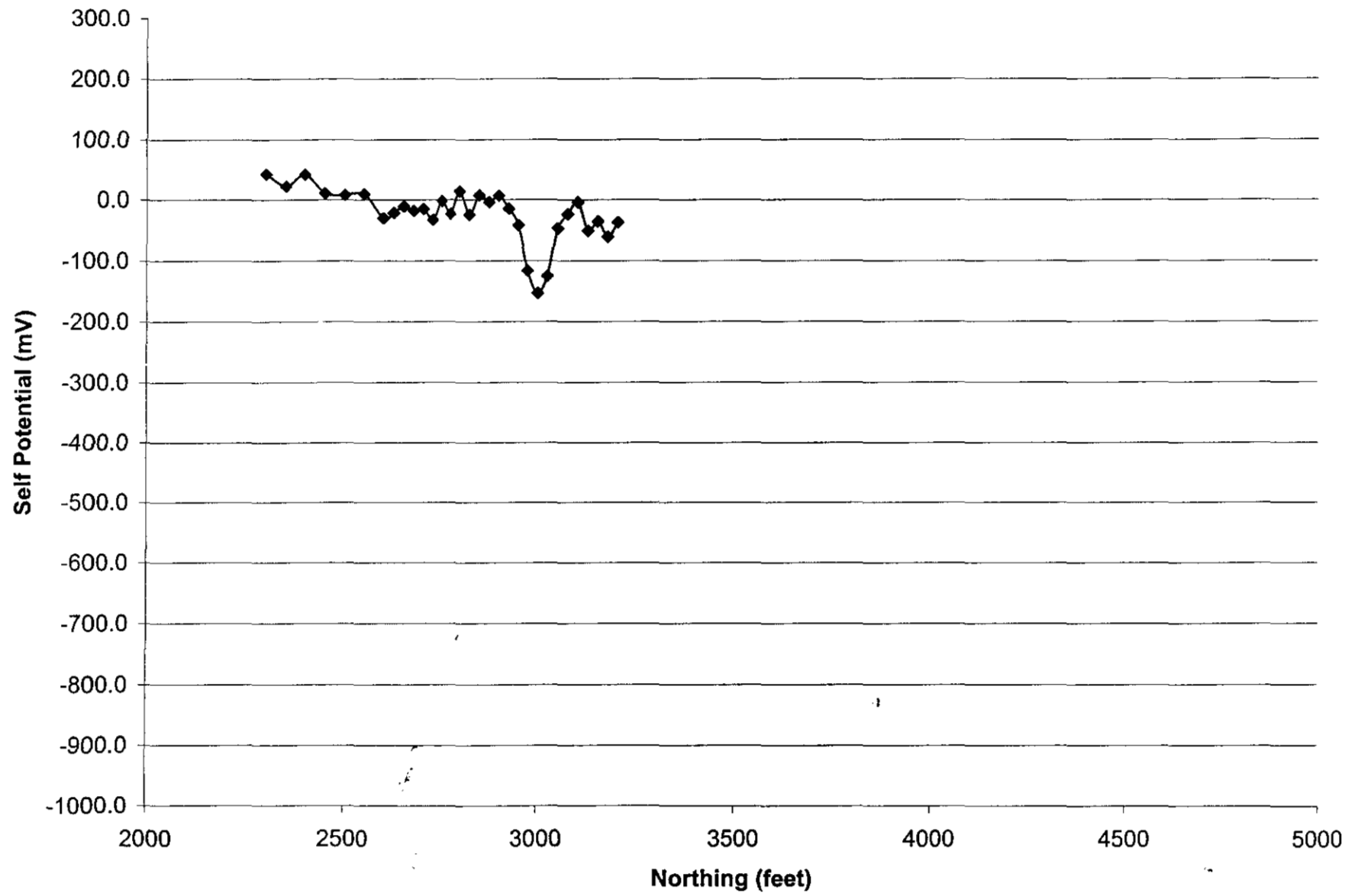


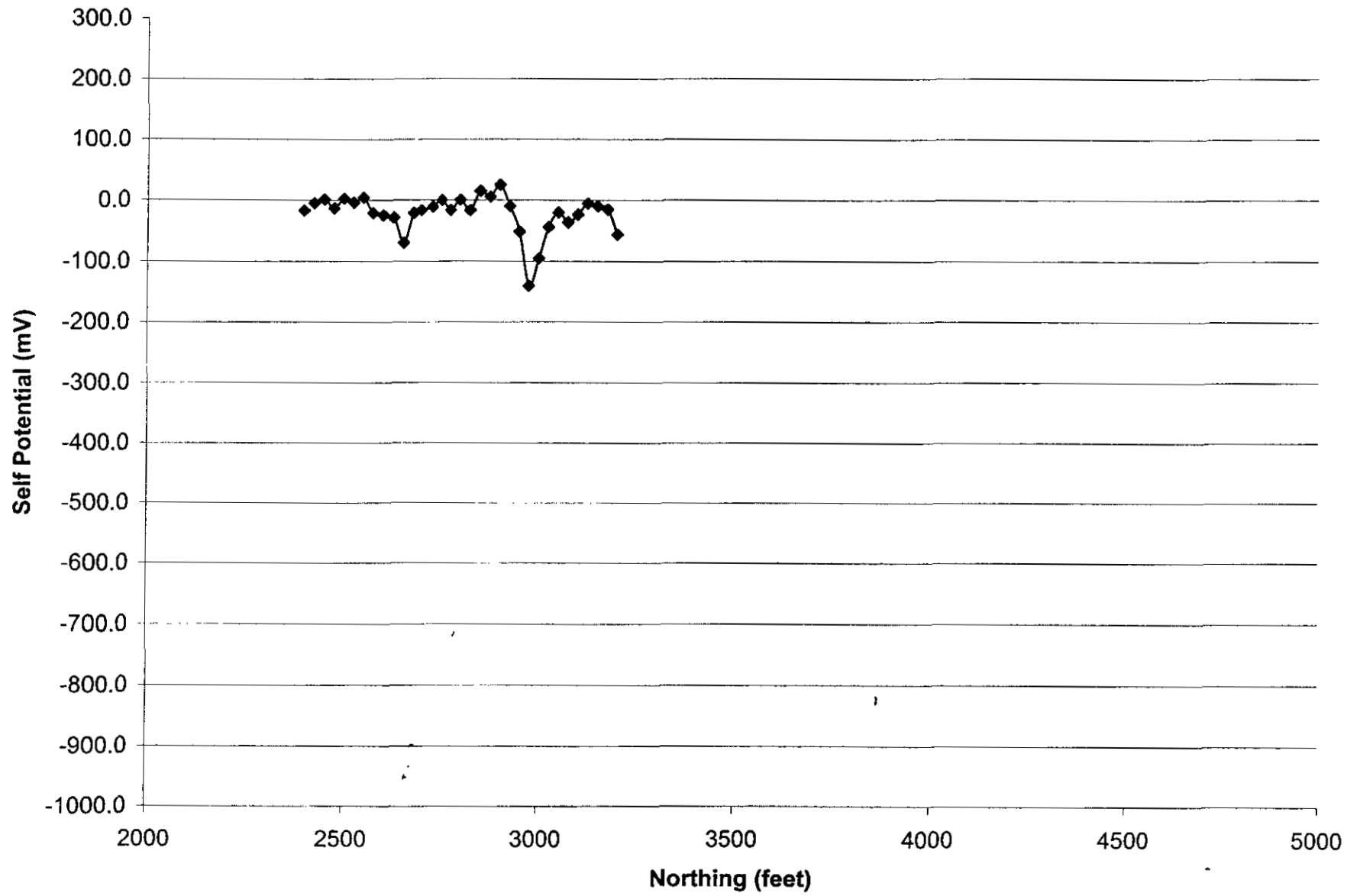


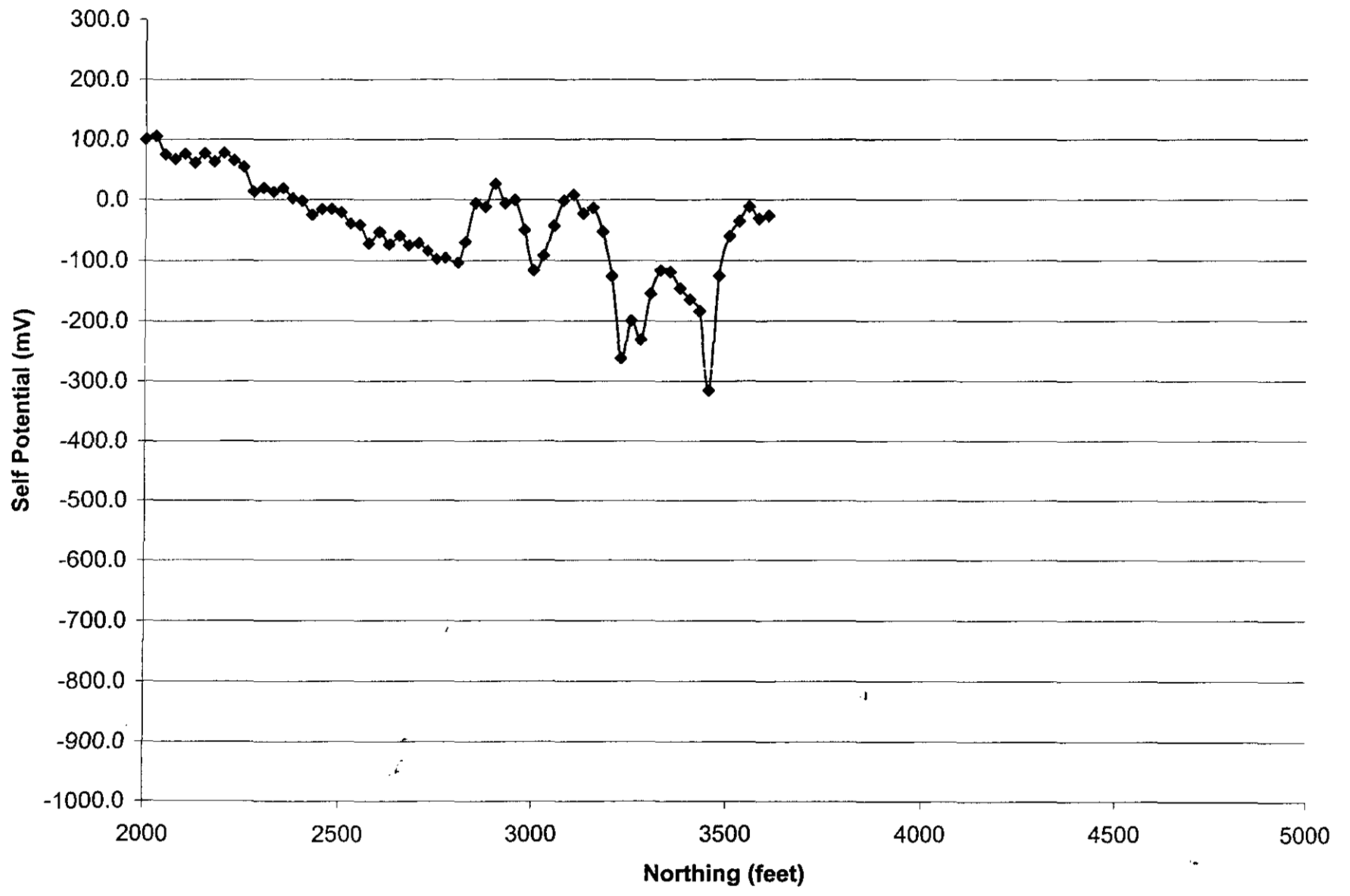


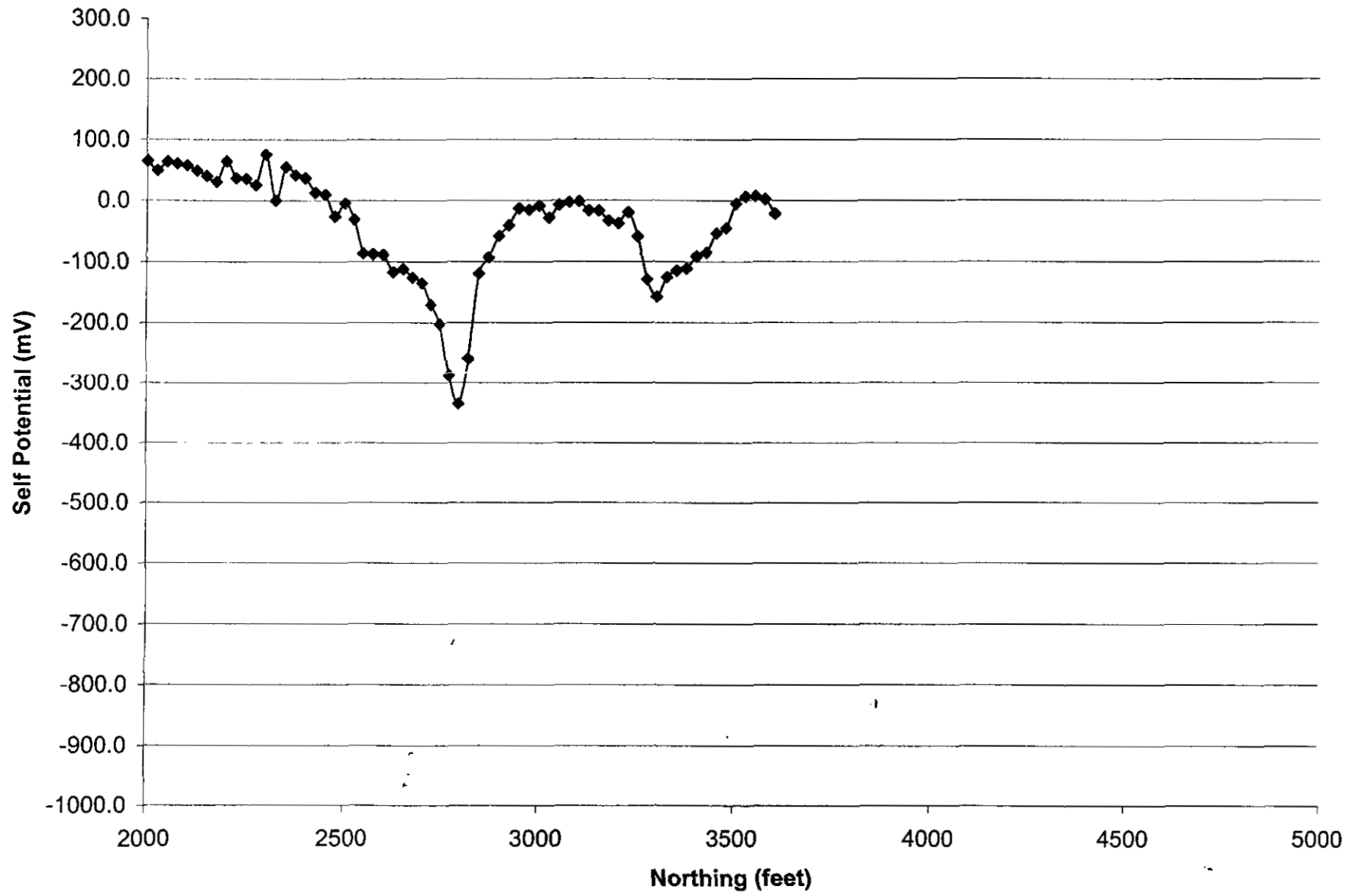


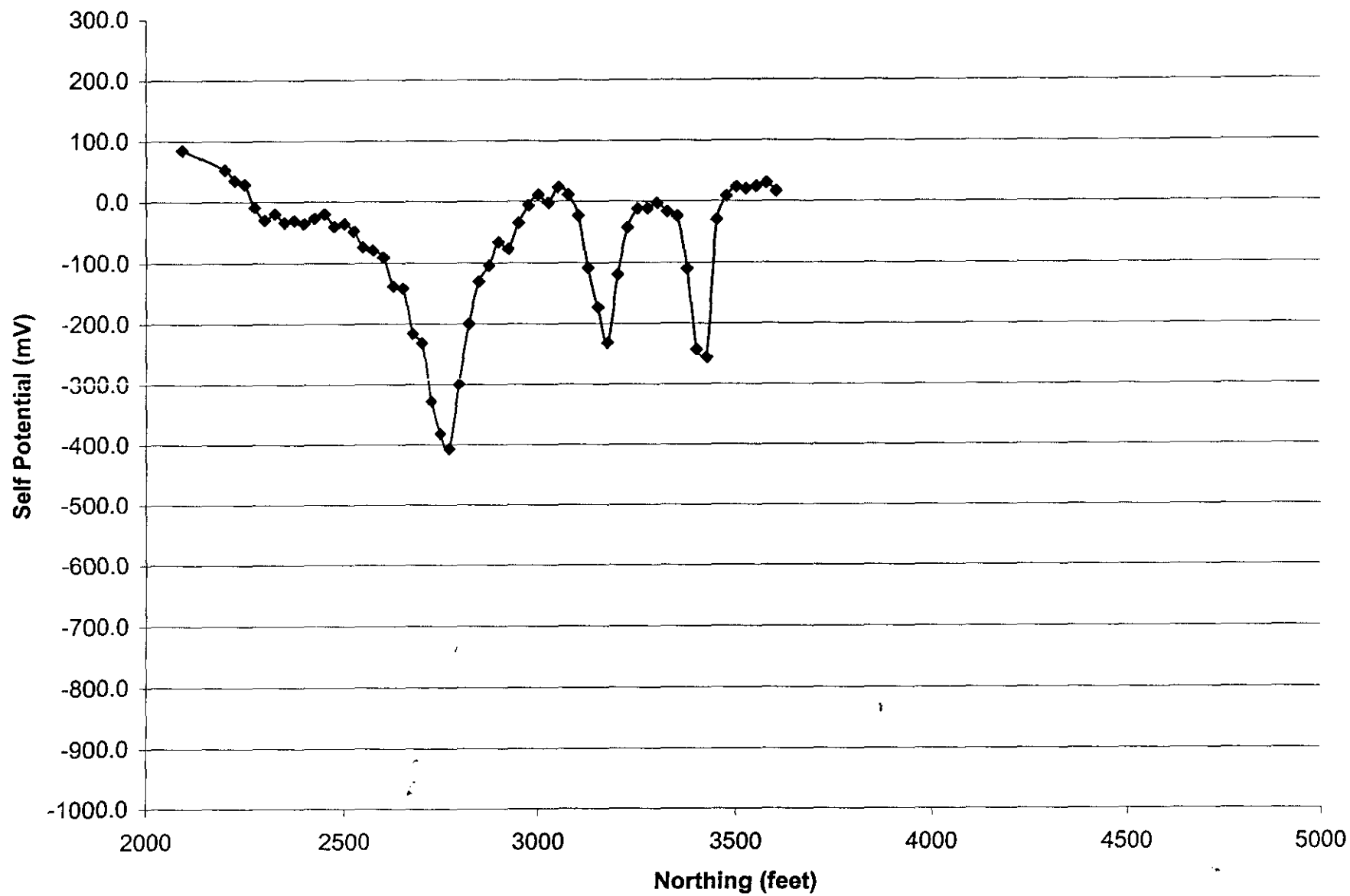


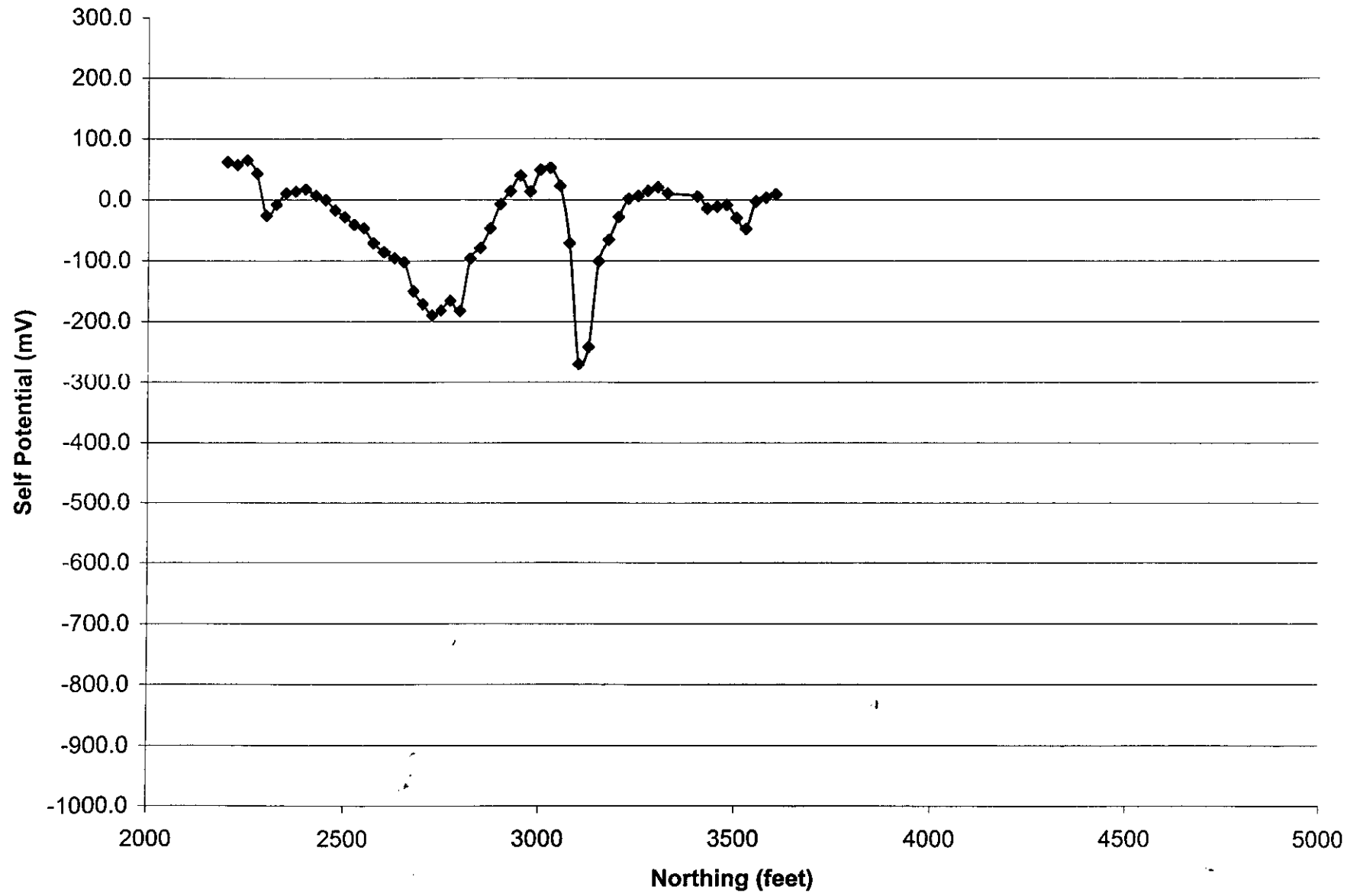


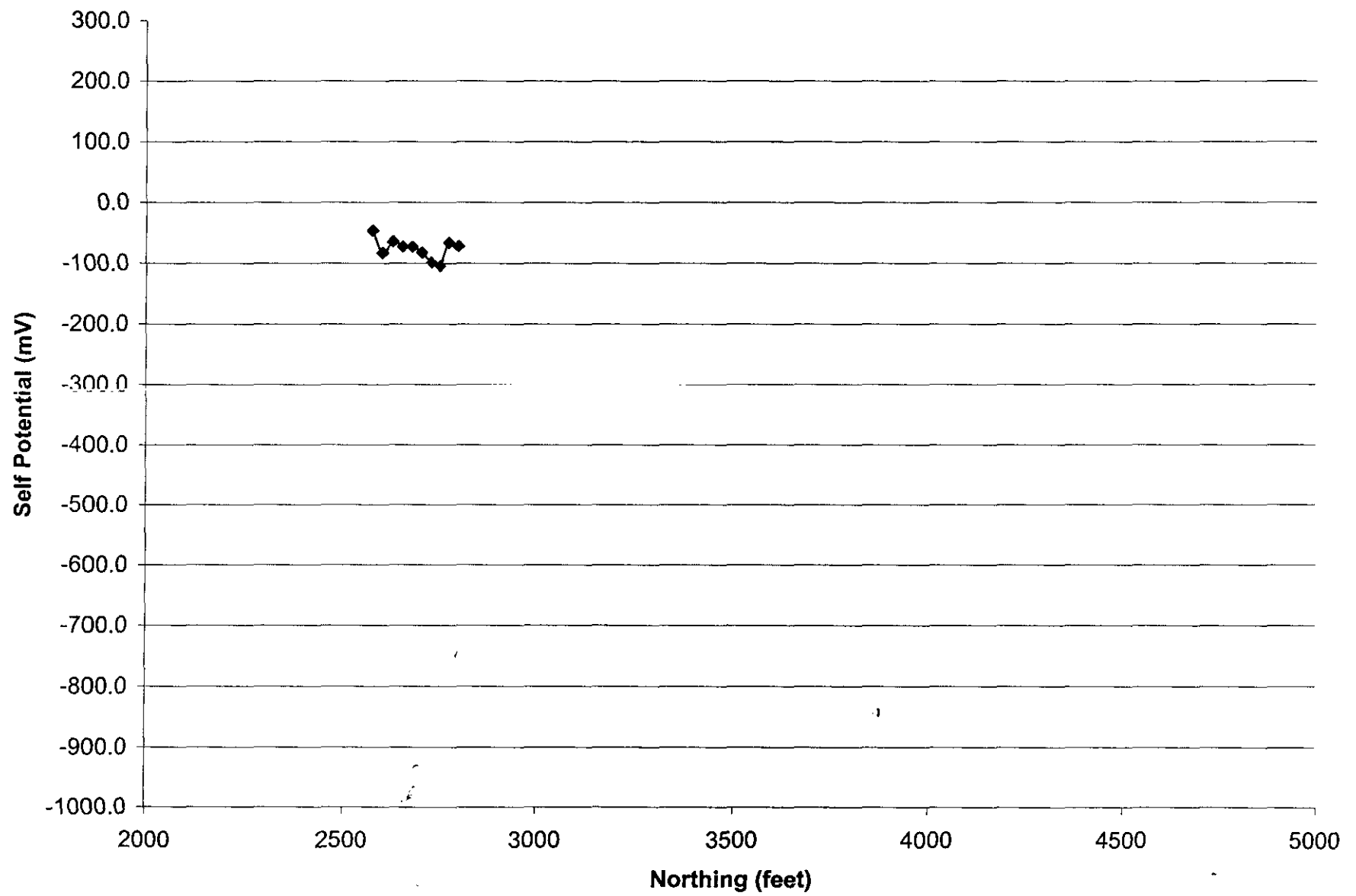


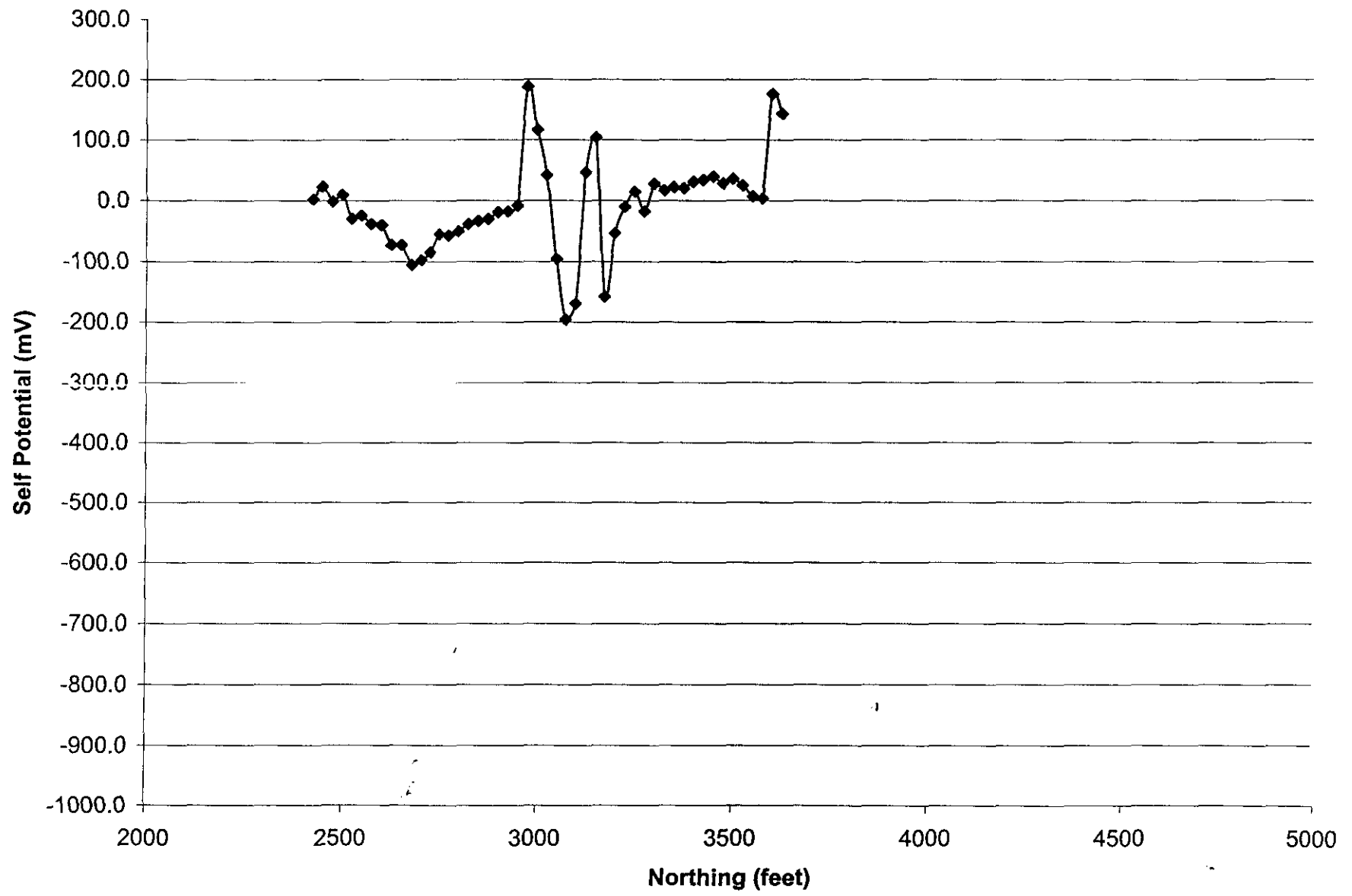


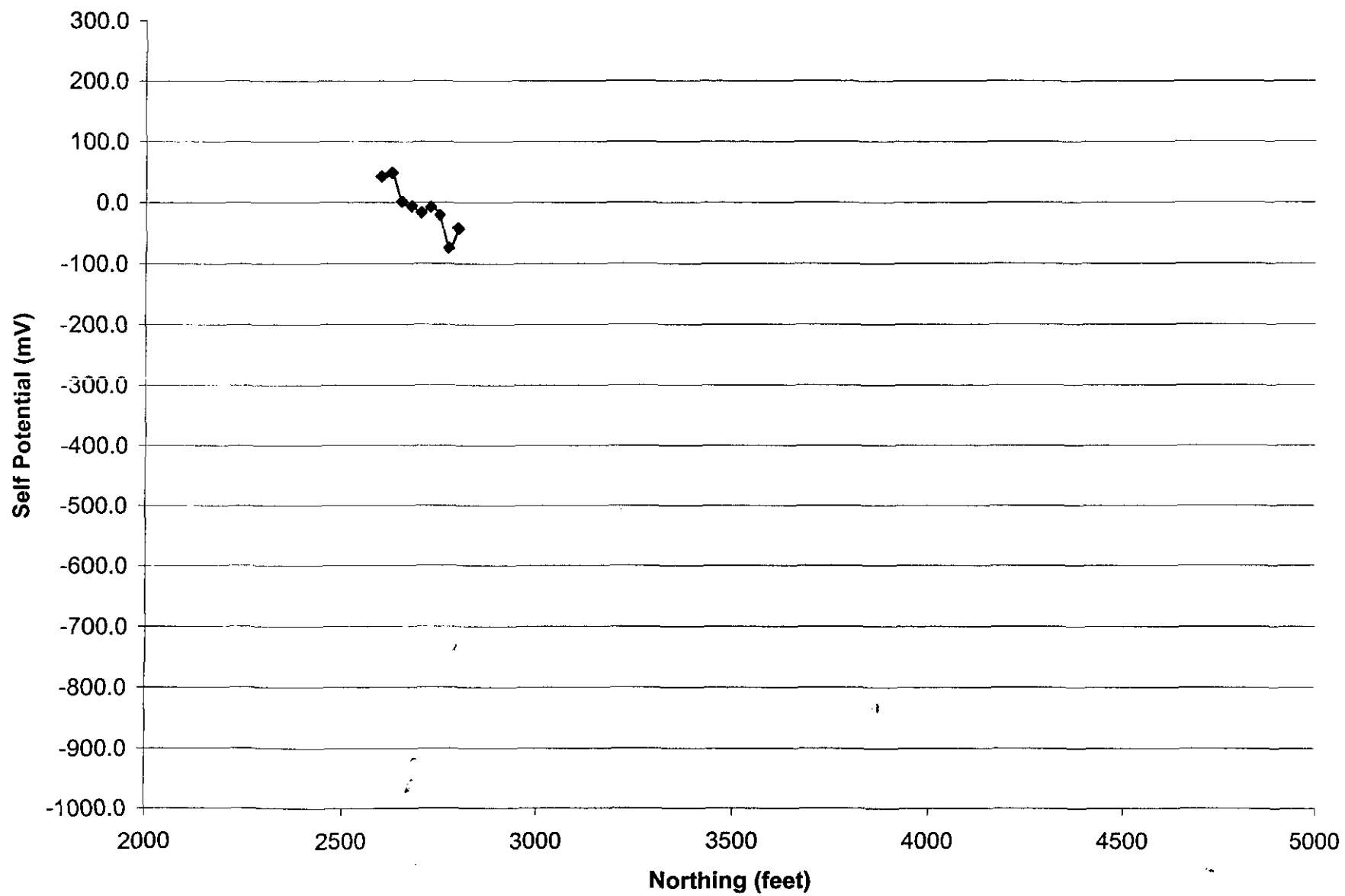


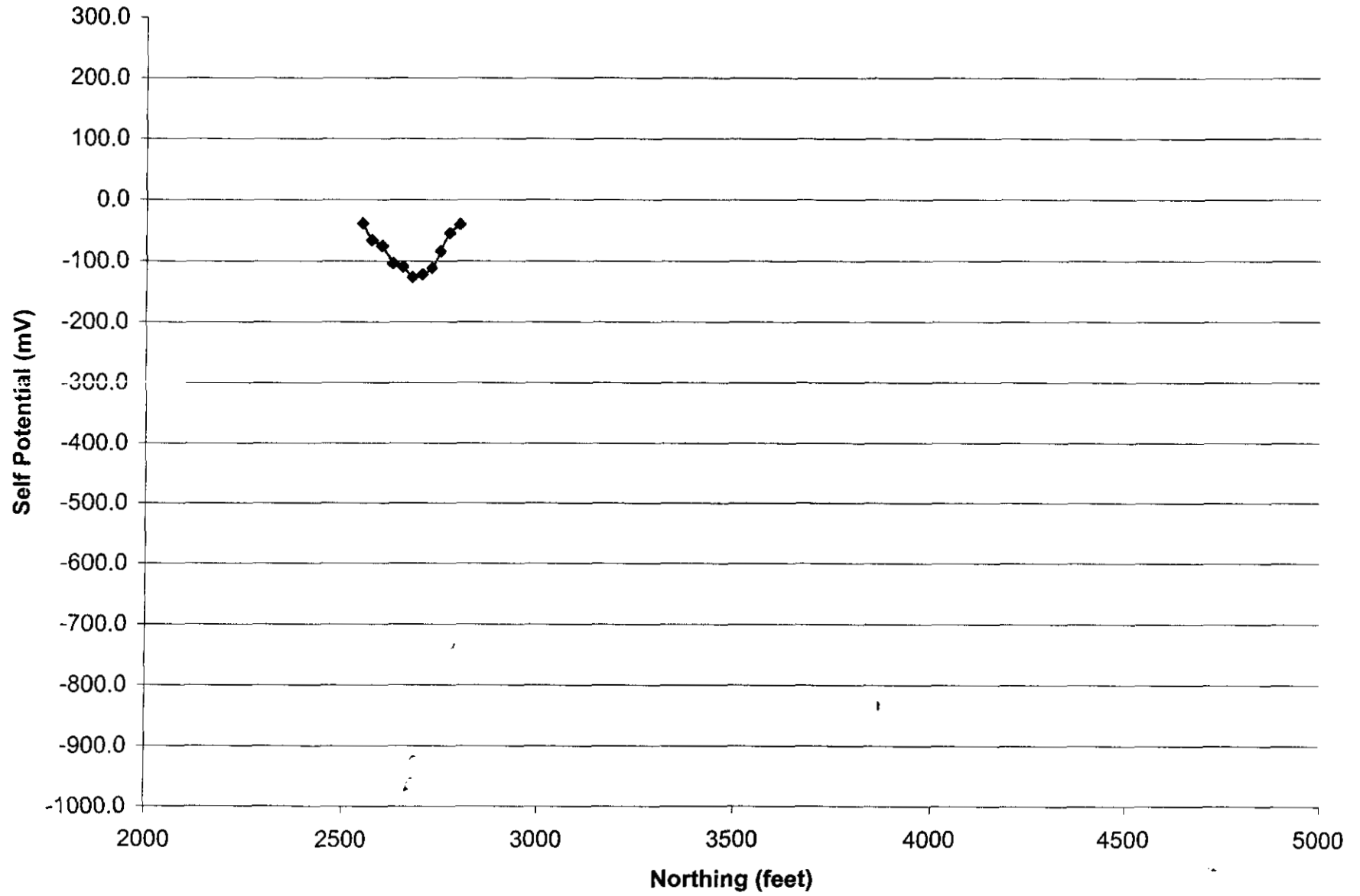


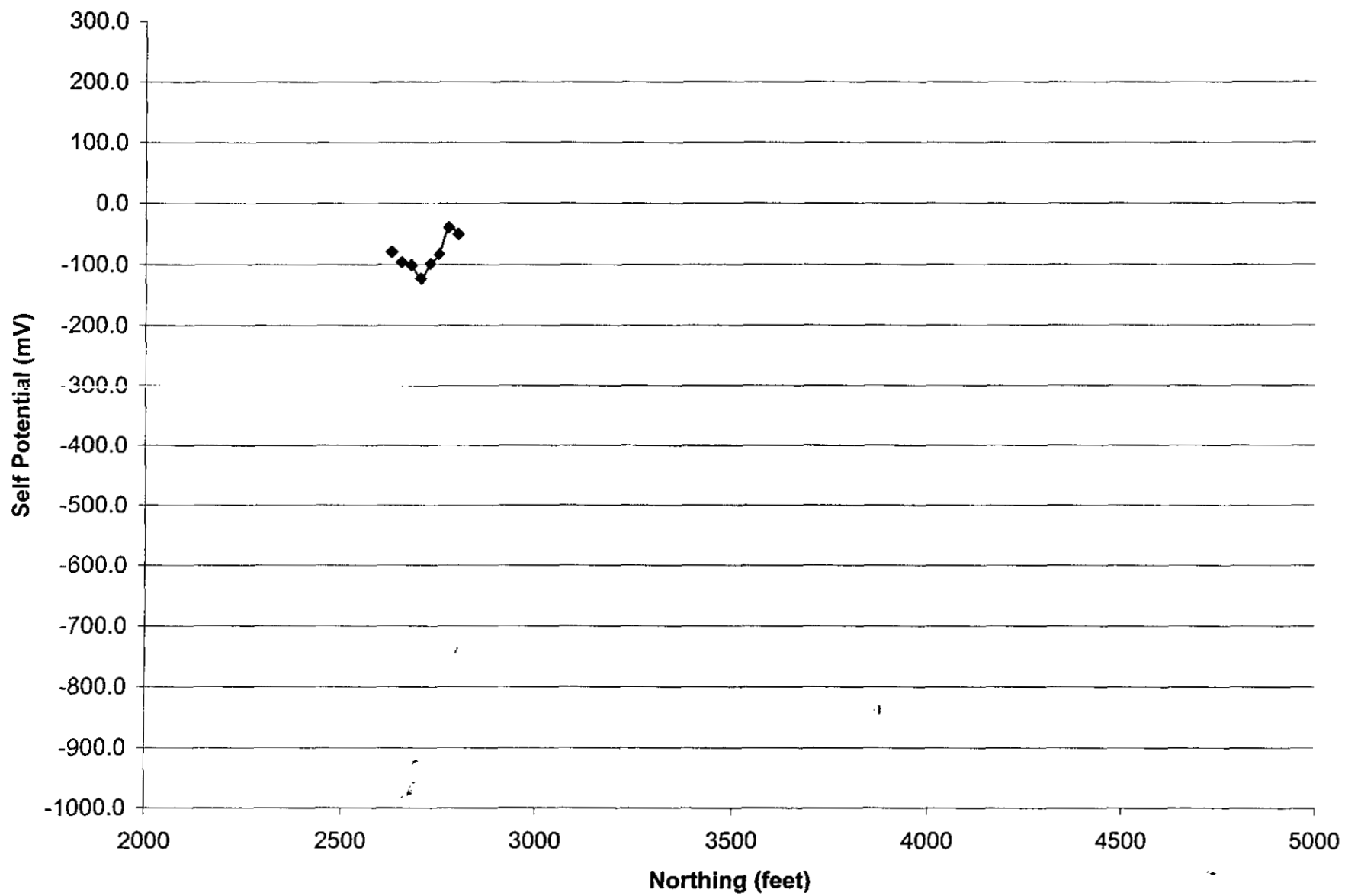


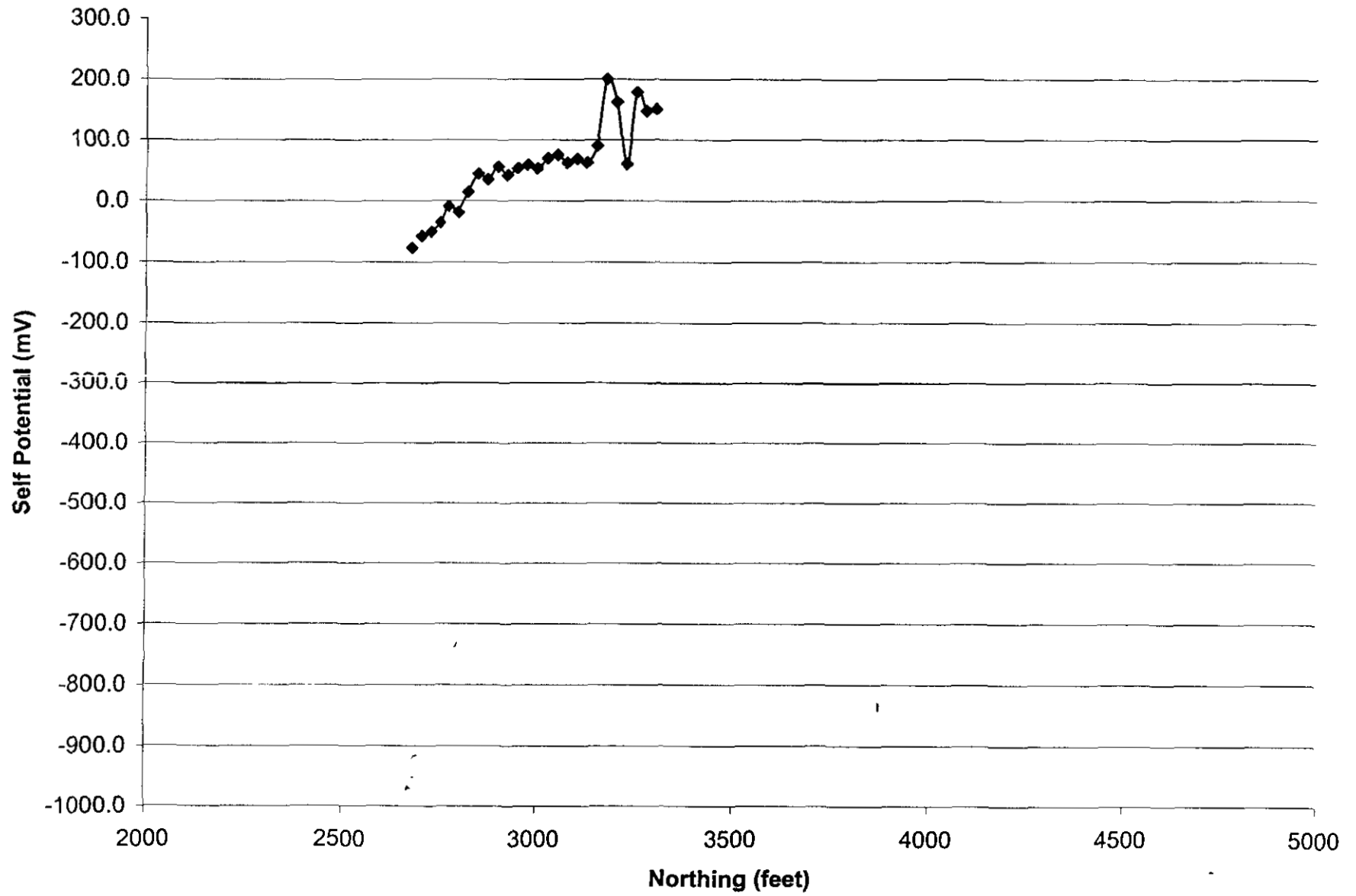


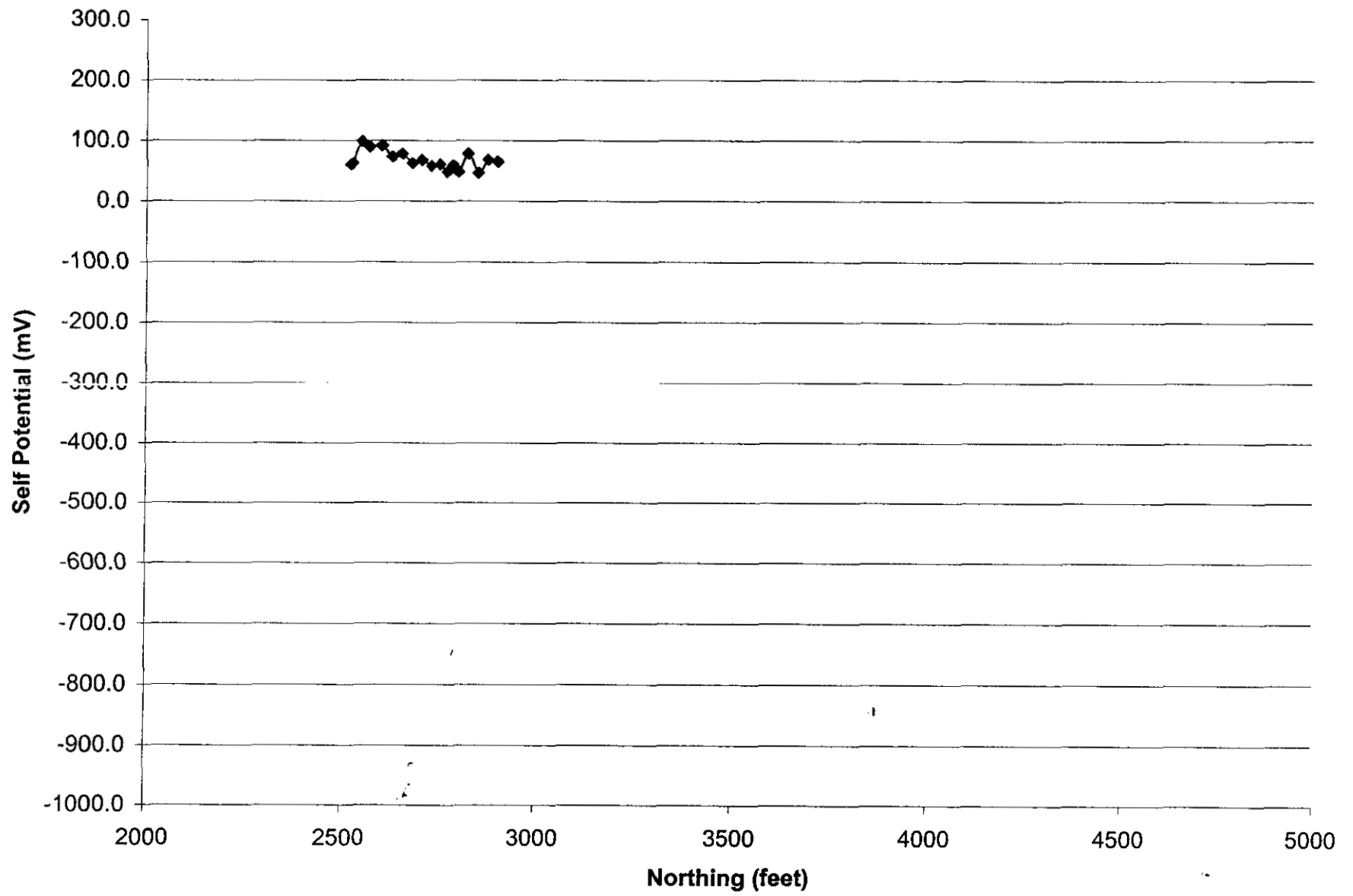












APPENDIX III

Map of Self-potential Geophysics Point Values

APPENDIX IV

Map of Self-potential Geophysics 100mV Contours

**APPENDIX 5 – STATEMENT OF EXPENDITURES AND
STATEMENT OF WORK EVENT # 3175109**

International Wayside Gold Mines - Financial Statement for January - December 2001

[illegible]

1

International Wayside Gold Mines - Financial Statement for January - December 2001

	W	X	Y	Z	AA	AB	AC
1							
2	380	381	382	383	384	386	TOTALS
3	Surf Expl	Reclama-	Travel	Salaries &	UG Expl	Site	
4	& Drill WT	tion		Benefits	& Drilling	Maint.	
5			\$16.50			\$12.83	\$36,991.51
6						\$11.93	\$41,627.12
7				\$132.45		\$400.00	\$16,620.26
8				\$247.85		\$80.00	\$23,128.59
9				\$291.53		\$114.91	\$24,191.28
10				\$1,306.30		\$57.17	\$40,393.86
11			\$1,016.50	\$1,424.50		\$60.00	\$26,079.02
12			\$1,493.72	\$1,372.67		\$756.13	\$53,929.86
13	\$3,312.18			\$523.72	\$615.00	\$119.63	\$58,314.22
14	\$4,236.89		\$6,400.00	\$1,072.79		\$358.58	\$46,845.09
15		\$700.00		\$2,000.26		\$783.27	\$41,420.78
16	\$3,379.91	\$815.00	\$76.50	\$1,334.16		\$31.00	\$40,197.69
17	\$4,967.43			\$1,753.95			\$23,642.54
18	\$3,441.10			\$1,293.59			\$35,040.50
19	\$5,318.68			\$3,600.52		\$12.50	\$38,195.44
20	\$4,301.96			\$1,206.71		\$40.00	\$29,066.87
21				\$1,758.34		\$74.21	\$28,646.22
22				\$845.20		\$648.66	\$20,037.29
23				\$1,290.83		\$20.00	\$33,461.12
24				\$1,493.09		\$16.03	\$21,646.19
25				\$547.54			\$21,505.67
26				\$1,390.15		\$500.00	\$62,422.09
27	\$28,958.15	\$1,515.00	\$9,003.22	\$24,886.15	\$615.00	\$4,096.85	\$763,403.21
28							

APPENDIX 6 – ASSAY CERTIFICATES
Acme Laboratories

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A104202 Page 1

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Ken Lord

SAMPLE#	Au** gm/mt
SI	<.01
4639	4.42
4640	2.11
4641	.64
4642	2.37
4643	.90
4644	8.26
4645	.26
4646	.53
4647	.12
4648	.07
4649	.11
4650	.03
4651	<.01
4652	.04
4653	.04
4654	.05
4655	.05
4656	.04
4657	.02
4658	<.01
RE 4658	<.01
RRE 4658	<.01
4659	<.01
4660	.03
4661	<.01
4662	.05
4663	.26
4664	.02
4665	.02
4666	.06
4667	.04
4668	.01
4669	.02
4670	.02
4671	<.01
STANDARD AU-1	3.41

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: CORE R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns

DATE RECEIVED: NOV 29 2001 DATE REPORT MAILED: Dec 7/01 SIGNED BY: D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data FA VIK



SAMPLE#	Au** gm/mt
4672	.06
4673	<.01
4674	<.01
4675	<.01
4676	<.01
4677	.01
4678	<.01
4679	<.01
4680	<.01
4681	.01
4682	.07
4683	<.01
RE 4683	<.01
RRE 4683	<.01
4684	<.01
4685	<.01
4686	<.01
4687	<.01
4688	<.01
STANDARD AU-1	3.38

Sample type: CORE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

AA

GEOCHEM PRECIOUS METALS ANALYSIS

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A104134 Page 1

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Ken Lord

AA

SAMPLE#	Au** ppb
SI	<2
C 120375	3
C 120376	2
C 120377	3
C 120378	<2
C 120379	2
C 120380	4
C 120381	9
C 120382	32
C 120383	31
C 120384	3
C 120385	6
C 120386	17
C 120387	20
C 120388	7
C 120389	7
C 120390	9
RE C 120390	5
C 120391	4
C 120392	6
C 120393	6
C 120394	24
C 120395	5
C 120396	23
C 120397	107
C 120398	94
C 120399	7098
C 120400	2868
C 120401	473
C 120402	158
C 120403	226
C 120404	76
C 120405	59
C 120406	39
C 120407	71
STANDARD AU-R	491

GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.
- SAMPLE TYPE: SLUDGE R150 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: NOV 23 2001 DATE REPORT MAILED: Dec 3/01 SIGNED BY: C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



SAMPLE#	Au** ppb
C 120408	52
C 120409	39
C 120410	44
C 120411	32
C 120412	40
C 120413	32
C 120414	38
C 120415	45
C 120416	64
C 120417	28
C 120418	25
C 120419	28
C 120420	17
RE C 120420	20
C 120421	19
C 120422	32
C 120423	29
C 120424	31
C 120425	33
C 120426	34
C 120427	37
C 120428	54
C 120429	25
C 120430	25
C 120431	21
C 120432	10
C 120433	23
C 120434	33
C 120435	26
C 120436	34
C 120437	730
C 120438	28
C 120439	32
C 120440	29
C 120441	32
STANDARD AU-R	487

Sample type: SLUDGE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A104133 Page 1

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Ken Lord

SAMPLE#	Au** gm/mt
SI	<.01
4576	.35
4577	.02
4578	.13
4579	.06
4580	<.01
4581	<.01
4582	.76
4583	.08
4584	<.01
4585	<.01
4586	<.01
4587	<.01
4588	<.01
4589	<.01
4590	<.01
RE 4590	<.01
RRE 4590	<.01
4591	<.01
4592	.16
4593	.39
4594	.03
4595	.07
4596	<.01
4597	.35
4598	.05
4599	.03
4600	7.35
4601	.31
4602	.08
4603	.17
4604	.11
4605	.03
4606	.19
4607	.09
STANDARD AU-1	3.37

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: CORE R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: NOV 23 2001 DATE REPORT MAILED: Dec 3 / 01 SIGNED BY: C. Leong, D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data LFA YIN



SAMPLE#	Au** gm/mt
4608	.03
4609	.06
4610	.18
4611	.16
4612	.03
4613 PULP	6.81
4614 PULP	1.74
4615	.02
4616	<.01
4617	<.01
4618	<.01
4619	<.01
4620	.04
RE 4620	.04
RRE 4620	.04
4621	.64
4622	.06
4623	<.01
4624	<.01
4625	<.01
4626	<.01
4627	<.01
4628	<.01
4629	<.01
4630	<.01
4631	.05
4632	.06
4633	.02
4634	.02
4635	<.01
4636	<.01
4637	<.01
4638	.01
STANDARD AU-1	3.43

Sample type: CORE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A104133R Page 1

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Godfrey Walton

SAMPLE#	Au** gm/mt
SI	<.01
4576	.33
4577	.02
4578	.07
4579	.06
4580	<.01
4581	<.01
4582	.57
4583	.55
4584	<.01
4597	.14
4598	.02
4599	.03
4600	6.58
RE 4600	6.61
4601	.34
4602	.07
4603	.20
4604	.60
4605	.02
4606	.19
4607	.08
4608	.02
4609	.05
4610	.15
4611	.14
4612	.04
4615	.03
4616	<.01
4617	<.01
4618	<.01
4619	.01
4620	.05
4621	.87
4622	.04
4623	<.01
STANDARD AU-1	3.33

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: CORE REJ.

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: DEC 4 2001 DATE REPORT MAILED: Dec 7/01 SIGNED BY: [Signature] D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



SAMPLE#	Au** gm/mt
4624	<.01
4625	<.01

Sample type: CORE REJ..

ACME
(13)YTICAL LABORATORIES LTD.
9002 Accredited Co.)

852 E. HASTINGS ST.

VANCOUVER BC V6A 1R6

PHONE (604) 253-3158 FAX (604) 253-1716

153-1716

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A104133R2

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Ken Lord

SAMPLE#	S.Wt gm	NAu mg	-Au gm/mt	DupAu gm/mt	TotAu gm/mt
4576	516	.05	.20	-	.30
4577	525	<.01	.01	-	.01
4578	513	<.01	.14	-	.14
4579	542	<.01	.07	-	.07
4580	527	<.01	<.01	-	<.01
4581	518	<.01	<.01	-	<.01
4582	543	.07	.32	-	.45
4583	534	<.01	.12	-	.12
4584	529	<.01	<.01	-	<.01
4585	482	<.01	<.01	-	<.01
4586	531	<.01	<.01	<.01	<.01
4587	549	<.01	<.01	-	<.01
4588	544	<.01	<.01	-	<.01
4589	516	<.01	<.01	-	<.01
4590	523	<.01	<.01	-	<.01

-AU : -150 AU BY FIRE ASSAY FROM 1 A.T. SAMPLE. DUPAU: AU DUPLICATED FROM -150 MESH. NAU - NATIVE GOLD, TOTAL SAMPLE FIRE ASSAY.
- SAMPLE TYPE: CORE REJ.

DATE RECEIVED: DEC 14 2001

DATE REPORT MAILED:

SIGNED BY: C. Leong

TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. File # A104019 Page 1
P.O. Box 247, 2422 Barker, Wells BC V0K 2R0

SAMPLE# Au**
gm/mt

SI	<.01
4541	1.33
4542	4.74
4543	1.08
4544	.15
4545	.61
4546	.67
4547	2.36
4548	12.67
4549	.43
4550 PULP	1.69
4551	27.91
4552	.02
RE 4552	.02
RRE 4552	.02
4553	.01
4554	<.01
4555	<.01
4556	.02
4557	.05
4558	.18
4559	.17
4560	.13
4561	.28
4562	.75
4563	.22
4564	.08
RE 4564	.08
RRE 4564	.08
4565	.02
4566	.03
4567	.02
4568	<.01
4569	.78
4570	.05
STANDARD AU-1	3.32

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.
- SAMPLE TYPE: CORE R150 60C
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: NOV 14 2001 DATE REPORT MAILED: Nov 21/01 SIGNED BY: C. Leong D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data LFA VINS



Int'l Wayside Gold Mines Ltd.

FILE # A104019

Page 2



SAMPLE#	Au** gm/mt
4571	.08
4572	.61
4573	.18
4574	.05
4575	.12
RE 4575	.15

Sample type: CORE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. File # A104019R
 P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Godfrey Walton

SAMPLE#	Au** gm/mt
SI	<.01
4541	2.83
4542	5.19
4543	.91
4544	.12
4545	.42
4546	.53
4547	2.55
4548	13.71
RE 4548	13.44
4549	.48
4551	28.61
4560	.29
4561	.22
4562	.63
STANDARD AU-1	3.32

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.
 - SAMPLE TYPE: CORE REJ.
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: DEC 4 2001 DATE REPORT MAILED: *Dec 7/01* SIGNED BY: *C. Leong* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ACME ANALYTICAL LABORATORIES LTD.
(IL 9002 Accredited Co.)

852 B. HASTINGS ST. VANCOUVER BC V6A 1R6

PHONE (604) 253-3158 FAX (604) 253-1716

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. File # A104019R2
P.O. Box 247, 2422 Barker, Wells BC V0K 2R0

SAMPLE#	S.Wt gm	NAu mg	-Au gm/mt	TotAu gm/mt
4541	540	.61	1.28	2.41
4560	514	.03	.25	.31
4561	552	.16	.54	.83
4562	535	.33	.58	1.20

-AU : -150 AU BY FIRE ASSAY FROM 1 A.T. SAMPLE. DUPAU: AU DUPLICATED FROM -150 MESH. NAU - NATIVE GOLD, TOTAL SAMPLE FIRE ASSAY.
- SAMPLE TYPE: CORE REJ.

DATE RECEIVED: DEC 14 2001 DATE REPORT MAILED: Dec 20/01 SIGNED BY: C. Leong D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

GEOCHEM PRECIOUS METALS ANALYSIS

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103985 Page 1

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: A. Justason

SAMPLE#	Au** ppb
SI	<2
C 120301	10
C 120302	5
C 120303	2
C 120304	7
C 120305	151
C 120306	182
C 120307	9
C 120308	21
C 120309	50
C 120311	281
C 120312	365
C 120313	383
C 120314	158
C 120315	428
C 120316	549
C 120317	718
C 120318	150
C 120319	170
C 120320	509
RE C 120320	478
C 120321	500
C 120322	622
C 120323	571
C 120324	285
C 120325	321
C 120326	247
C 120327	450
C 120328	138
C 120329	1587
C 120330	370
C 120331	3130
C 120332	1145
C 120333	672
C 120334	1591
STANDARD AU-R	495

GROUP 38 - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.
 - SAMPLE TYPE: SLUDGE R150 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: NOV 13 2001 DATE REPORT MAILED: Nov 21/01 SIGNED BY: C. L. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data FA VMS



SAMPLE#	Au** ppb
C 120335	21690
C 120336	14061
C 120337	1778
C 120338	619
C 120339	274
C 120340	1083
C 120341	1041
C 120342	877
C 120343	227
C 120344	301
C 120345	121
RE C 120345	137
C 120346	558
C 120347	439
C 120348	181
C 120349	63
C 120350	134
RE C 120350	154
C 120351	339
C 120352	91
C 120353	575
C 120354	545
C 120355	484
C 120356	341
C 120357	173
C 120358	331
C 120359	426
C 120360	55
C 120361	42
C 120362	74
C 120363	818
C 120364	260
C 120365	630
C 120366	269
C 120367	183
C 120368	183
STANDARD AU-R	472

Sample type: SLUDGE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Au** ppb
C 120369	144
C 120370	265
C 120371	147
C 120372	58
C 120373	193
C 120374	133
RE C 120374	229
STANDARD AU-R	486

Sample type: SLUDGE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

GEOCHEMICAL ANALYSIS CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT H. HERRICK File # A103761

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: A. Justason

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga	Au*
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	%	ppm	ppm	ppm	ppm	%	ppm	ppb
SI	.7	<1	<2	1	<.1	<1	<1	4	.04	<1	<1	<2	<1	2	<.2	<.5	<.5	<1	.07	<.001	<1	6	<.01	2	<.001	<1	<.01	.273	<.01	<1	<1	<.1	<1	<.02	<1	<.2
C 121281	3.8	10	9	26	<.1	14	5	532	1.21	1	<1	<2	4	14	<.2	<.5	<.5	3	.07	.012	18	88	.05	21	.001	<1	.21	.013	.07	2	<1	1.2	<1	<.02	<1	<.2
C 121282	1.3	9	12	12	<.1	13	6	431	1.89	2	1	<2	8	848	<.2	<.5	<.5	3	17.12	.025	27	65	.16	22	.001	<1	.18	.016	.10	1	<1	1.8	<1	<.02	<1	<.2
C 121283	4.4	62	20	91	.1	27	18	619	4.75	3	3	<2	20	10	.2	<.5	.6	25	.10	.050	61	54	1.11	54	.002	<1	2.05	.009	.18	<1	<1	1.1	<1	<.02	6	2.1
C 121284	6.1	39	27	106	.3	46	30	1609	4.78	4	3	<2	20	11	.3	<.5	.5	36	.06	.040	56	92	1.44	60	.004	<1	2.21	.009	.19	1	<1	1.4	<1	<.02	7	<.2
C 121285	3.7	46	18	101	.1	43	21	1162	4.06	3	2	<2	18	7	.3	<.5	<.5	25	.02	.031	52	59	1.00	69	.002	<1	1.89	.008	.18	<1	<1	1.1	<1	<.02	6	1.5
C 121286	3.0	55	19	114	.1	54	23	1399	4.39	4	3	<2	20	9	.3	<.5	.5	33	.01	.036	53	71	1.00	118	.002	<1	2.03	.011	.23	<1	<1	1.2	<1	<.02	6	<.2
C 121287	2.7	12	10	24	<.1	9	4	348	1.01	2	<1	<2	7	6	<.2	<.5	<.5	4	.15	.027	21	65	.14	54	.002	<1	.36	.009	.14	1	<1	.5	<1	<.02	1	.7
C 121288	4.6	62	10	69	<.1	145	51	1590	7.55	4	<1	<2	1	187	.3	<.5	<.5	32	5.81	.184	11	134	1.86	55	.021	<1	.92	.037	.11	<1	<1	4.2	<1	.22	3	<.2
RE C 121288	4.5	65	10	72	<.1	149	51	1645	7.92	4	<1	<2	1	186	.3	<.5	<.5	32	5.64	.185	12	135	1.93	51	.022	1	.96	.037	.11	<1	<1	4.2	<1	.21	3	1.0
STANDARD DS3	9.7	129	34	162	.3	34	13	841	3.31	32	7	<2	4	29	5.7	5.5	6.0	76	.54	.098	19	187	.58	147	.092	<1	1.66	.029	.16	4	<1	2.7	1	.02	7	20.3

GROUP 1DX - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
- SAMPLE TYPE: ROCK R150 60C AU* IGNITION BY ACID LEACHED, ANALYZE BY ICP-MS. (10 gm)
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 23 2001 DATE REPORT MAILED: Nov 5/01 SIGNED BY: C. Leong, J. Wang; CERTIFIED B.C. ASSAYERS

GEOCHEM PRECIOUS METALS ANALYSIS

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103709

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: A. Justason

SAMPLE#

Au**
ppb

SI	11
C 120297	5732
C 120298	3770
C 120299	878
C 120300	212
E 195351	122
E 195352	92
E 195353	239
E 195354	102
E 195355	225
E 195356	196
E 195357	258
E 195358	204
E 195359	202
E 195360	1176
RE E 195360	1257
E 195361	1063
E 195362	286
E 195363	195
E 195364	227
E 195365	297
E 195366	113
E 195367	259
E 195368	167
E 195369	101
E 195370	272
E 195371	283
E 195372	241
E 195373	366
E 195374	864
E 195375	1249
E 195376	744
E 195377	120
E 195378	1323
STANDARD AU-R	519

GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.
- SAMPLE TYPE: SLUDGE R150 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 18 2001 DATE REPORT MAILED: Oct 29/01 SIGNED BY: C. Leong TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

AA
LL

ASSAY CERTIFICATE

AA
LL

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103708

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: D. Hladky

SAMPLE#	Au** gm/mt
SI	<.01
4501	.76
4502	1.23
4503	1.24
4504	.13
4505	.65
4506	3.93
4507	3.33
4508	.75
4509 PULP	6.83
4510	38.90
4511	13.38
4512	4.80
4513	2.52
4514	.64
4515	.47
RE 4515	.47
RRE 4515	.48
4531	.14
4532	.26
4533	.24
4534	.11
4535	.61
4536	.13
4537	.01
4538	.03
4539	.14
4540 PULP	1.81
6499	10.43
6500	.43
STANDARD AU-1	3.37

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: CORE R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 18 2001 DATE REPORT MAILED: Oct 24/01 SIGNED BY: C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

GEOCHEM PRECIOUS METALS ANALYSIS

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103644

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: D. Hickey

SAMPLE#

Au**
ppb

SI

<2

C 120272

349

C 120273

6561

C 120274

19271

C 120275

5071

C 120276

3045

C 120277

11758

C 120278

6451

C 120279

915

C 120280

824

C 120281

3234

C 120282

180

C 120283

171

C 120284

271

C 120285

11391

RE C 120286

661

C 120286

768

C 120287

2741

C 120288

20846

C 120289

14164

C 120290

1379

C 120291

2926

C 120292

2252

C 120293

2427

C 120294

403

C 120295

5286

C 120296

3348

STANDARD AU-R

488

GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.

- SAMPLE TYPE: SLUDGE R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 15 2001 DATE REPORT MAILED: Oct 23/01 SIGNED BY: C. H. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

AA
LL

ASSAY CERTIFICATE

AA
LL

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103644R

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Godfrey Walton

SAMPLE#	Au** gm/mt
SI	<.01
C 120273	.68
* C 120274	12.41
C 120276	7.14
* C 120277	8.70
* C 120279	3.64
C 120282	.18
* C 120288	20.74
STANDARD AU-1	3.32

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.
- SAMPLE TYPE: SLUDGE REJ.

DATE RECEIVED: DEC 4 2001

DATE REPORT MAILED:

Dec 7/01

SIGNED BY: C. Long

D. TOYE, C. LEONG, J. WANG, CERTIFIED B.C. ASSAYERS

* Sample rerun from original pulps, no rejects left.

GEOCHEM PRECIOUS METALS ANALYSIS

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103608

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: D. Hladky

SAMPLE#

Au**
ppb

SI	2
C 120254	566
C 120255	292
C 120256	267
C 120257	200
C 120258	125
C 120259	105
C 120260	124
C 120261	72
C 120262	191
C 120263	40
C 120264	266
C 120265	148
RE C 120265	220
C 120266	111
C 120267	102
C 120268	33
C 120269	40
C 120270	72
C 120271	45
STANDARD AU-R	481

GROUP 38 - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.
 - SAMPLE TYPE: SLUDGE R150 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 11 2001 DATE REPORT MAILED: Oct 22/01 SIGNED BY: C. H. D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103607 Page 1

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: D. Hladky

SAMPLE#	Au** gm/mt
SI	<.01
4516	.10
4517	.03
4518	.09
4519	.17
4520	.15
4521	.05
4522	.02
4523	<.01
4524	.65
4525	.42
4526	.01
RE 4526	.04
RRE 4526	<.01
4527	.05
4528	.15
4529	.14
4530	.02
6440	.91
6441	.90
6442	.22
6443	.43
6444	.04
6445	1.80
6446	2.24
6447	.92
6448	.18
RE 6448	.16
RRE 6448	.17
6449	1.39
6450	.35
6451	.27
6452 PULP	1.87
6453	.36
6454	.14
STANDARD AU-1	3.26

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: CORE R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 11 2001 DATE REPORT MAILED: Oct 22/01 SIGNED BY: C. Leong D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data LFA YW



SAMPLE#	Au** gm/mt
6455	<.01
6456	.01
6457	3.07
6458	.02
6459	.01
6468 PULP	1.81
6497	<.01
6498	.01
RE 6498	<.01
STANDARD AU-1	3.40

Sample type: CORE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



GEOCHEM PRECIOUS METALS ANALYSIS



Int'l Wayside Gold Mines Ltd. PROJECT WELLS TREND File # A103514

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: A. Justason

SAMPLE#	Au** ppb

C 121280	5439

GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.
- SAMPLE TYPE: SOIL SS80 60C

DATE RECEIVED: OCT 4 2001 DATE REPORT MAILED: Oct 12/01 SIGNED BY: *C. Leong* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Assay recommend for gold > 1000 ppb.



GEOCHEMICAL ANALYSIS CERTIFICATE



Int'l Wayside Gold Mines Ltd. PROJECT WELLS TREND File # A103513

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: A. Justason

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au**
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	%	ppm	ppb
SI	1	<1	3	1	<.3	2	<1	6	.05	<2	9	<2	<2	3	<.2	<3	<3	1	.14	<.001	<1	9	<.01	4	<.01	<3	.01	.64	.01	<2	<2
C 121274	7	68	16	72	<.3	30	3	63	3.95	71	<8	<2	4	12	.4	<3	5	15	.01	.110	17	90	.01	73	<.01	4	.28	.01	.15	2	39
C 121275	4	9	8	8	<.3	10	1	41	.69	5	<8	<2	<2	1	<.2	<3	<3	5	.01	.010	<1	119	<.01	3	<.01	<3	.02	.01	.01	3	2
C 121276	10	871	23489	666	175.7	17	<1	75	22.33	5070	<8	3	<2	8	1.6	34	440	7	.01	.492	1	42	.02	38	<.01	<3	.37	.01	.14	18	5678
C 121277	6	668	25863	250	136.6	12	1	58	2.98	152	<8	<2	<2	4	1.8	21	177	8	.01	.195	2	145	.01	29	<.01	<3	.19	<.01	.05	5	711
C 121278	8	249	29140	182	97.0	8	1	45	2.10	91	<8	<2	<2	4	1.9	10	119	6	.01	.127	<1	122	.01	15	<.01	<3	.11	<.01	.03	3	200
C 121279	6	289	27635	351	119.1	13	1	57	3.83	136	<8	<2	<2	8	3.2	23	145	5	.01	.222	<1	105	.01	13	<.01	<3	.12	<.01	.05	7	167
RE C 121279	6	284	29300	360	117.1	13	1	57	3.82	134	<8	<2	<2	8	3.2	20	143	6	.01	.227	1	108	.01	13	<.01	<3	.13	<.01	.05	7	161
STANDARD DS3/AU-R	10	123	33	159	<.3	36	12	804	3.17	31	<8	<2	4	28	5.5	4	5	81	.54	.094	19	192	.60	147	.09	4	1.77	.04	.17	4	503

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK R150 60C AU** GROUP 3B - 30.00 GM SAMPLE ANALYSIS BY FA/ICP.
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 4 2001 DATE REPORT MAILED: Oct 17/01 SIGNED BY: C. Leong D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

AA

GEOCHEM PRECIOUS METALS ANALYSIS

AA

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103512

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted By: D. Hladky

SAMPLE#	Au** ppb
SI	<2
C 120233	197
C 120234	524
C 120235	195
C 120236	94
C 120237	133
C 120238	104
C 120239	171
C 120240	233
C 120241	213
C 120242	253
C 120243	396
C 120244	5
RE C 120244	6
C 120245	4
C 120246	4
C 120247	9
C 120248	23
C 120249	12
C 120250	190
C 120251	755
C 120252	268
C 120253	324
STANDARD AU-R	475

GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.
- SAMPLE TYPE: SLUDGE R150 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 4 2001 DATE REPORT MAILED: Oct 15/01 SIGNED BY: C. Leong TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ACME ANALYTICAL LABORATORIES LTD.
(ISO 9002 Accredited Co.)

852 E. HASTINGS ST.

VANCOUVER BC V6A 1R6

PHONE (604) 253-3158 FAX (604) 253-1716

GEOCHEM PRECIOUS METALS ANALYSIS

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103480

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: A. Justason

SAMPLE#

Au**
ppb

SI

<2

C 121268

8

C 121269

159

C 121270

147

C 121271

7

C 121272

11

C 121273

2

RE C 121273

<2

STANDARD AU-R

485

GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.

- SAMPLE TYPE: ROCK R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED:

OCT 2 2001

DATE REPORT MAILED:

Oct 12/01

SIGNED BY:

C. Leong

B. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



GEOCHEM PRECISION METALS ANALYSIS



Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103479

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: D. Hladky

SAMPLE#	Au** ppb
SI	3
C 120195	415
C 120196	416
C 120197	372
C 120198	357
C 120199	287
C 120200	334
C 120228	114
RE C 120228	102
C 120229	51
C 120230	105
C 120231	126
C 120232	76
STANDARD AU-R	475

GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.
- SAMPLE TYPE: SLUDGE R150 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 2 2001 DATE REPORT MAILED: Oct 12/01 SIGNED BY: *C. Leong* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103478

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: D. Hladky

SAMPLE#	Au** gm/mt	Au** gm/mt
SI	<.01	-
6416	1.33	-
6417	.69	-
6418	12.62	-
6419	3.93	-
6420	.24	-
6421	.22	-
6422	7.29	-
6423 PULP	6.78	-
6424	50.41	32.94
6425	6.75	-
6479	2.21	-
6480	.50	-
RE 6480	.55	-
RRE 6480	.50	-
6481	4.83	-
6482	.02	-
6483	.02	-
6484	<.01	-
6485	.02	-
STANDARD AU-1	3.33	-

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: CORE R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 2 2001 DATE REPORT MAILED: Oct 12/01 SIGNED BY: C. Leong TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

AA
LL

GEOCHEM PRECISION METALS ANALYSIS

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103410 Page 1

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: A. Justason

AA
LL

SAMPLE#

Au**
ppb

SI	<2
C 120130	6
C 120131	2
C 120132	2
C 120133	84
C 120134	6
C 120135	1400
C 120136	603
C 120137	349
C 120138	372
C 120139	118
C 120140	266
C 120141	229
C 120142	922
C 120143	107
C 120144	92
C 120145	45
RE C 120145	75
C 120146	749
C 120147	556
C 120148	221
C 120149	211
C 120150	2170
C 120151	2941
C 120152	1264
C 120153	5216
C 120154	4101
C 120155	1236
C 120156	617
C 120157	213
C 120158	297
C 120159	824
C 120160	256
C 120161	193
C 120162	675

STANDARD AU-R 488

GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.
- SAMPLE TYPE: SULDGE R150 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: SEP 28 2001 DATE REPORT MAILED: Oct 11/01 SIGNED BY: C. Leong D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data FA

SAMPLE#	Au** ppb
C 120163	640
C 120164	906
C 120165	543
C 120166	715
C 120167	636
C 120168	846
C 120169	393
C 120170	659
C 120171	351
C 120172	333
C 120173	373
C 120174	350
C 120175	443
RE C 120175	428
C 120176	380
C 120177	962
C 120178	380
C 120179	408
C 120180	196
C 120181	182
C 120182	261
C 120183	960
C 120184	909
C 120185	567
C 120186	353
C 120187	238
C 120188	193
C 120189	152
C 120190	138
C 120191	578
C 120192	136
C 120193	431
C 120194	149
STANDARD AU-R	485

Sample type: SULDGE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Au** ppb
C 120201	246
C 120202	289
C 120203	39
C 120204	114
C 120205	4
C 120206	43
C 120207	78
C 120208	119
C 120209	127
C 120210	358
C 120211	299
C 120212	260
RE C 120212	246
C 120213	183
C 120214	43
C 120215	61
C 120216	66
C 120217	51
C 120218	132
C 120219	713
C 120220	620
C 120222	169
C 120223	139
C 120224	131
C 120225	146
C 120226	146
C 120227	130
STANDARD AU-R	479

Sample type: SULDGE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

AA
LL

GEOCHEM PRECIOUS METALS ANALYSIS

AA
LL

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103334

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: A. Justason

SAMPLE#	Au** ppb
SI	<2
C 120107	.268
C 120108	59
C 120109	169
C 120110	267
C 120111	148
C 120112	138
C 120113	103
C 120114	60
C 120115	117
C 120116	58
C 120117	43
C 120118	81
C 120119	251
C 120120	63
RE C 120120	69
C 120121	72
C 120122	333
C 120123	397
C 120124	123
C 120125	588
C 120126	103
C 120127	36
C 120128	102
C 120129	26
STANDARD AU-R	495

GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.
- SAMPLE TYPE: SULFIDE R150 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: SEP 25 2001

DATE REPORT MAILED:

Oct 5/01

SIGNED BY:

D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

AA
11

GEOCHEM PRECIOUS METALS ANALYSIS

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103153 Page 1

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: D. Hladky

AA
11

SAMPLE#	Au** ppb
SI	5
C 120063	113
C 120064	37
C 120065	48
C 120066	186
C 120067	5708
C 120068	1064
C 120069	820
C 120070	308
C 120071	322
C 120072	143
C 120073	174
C 120074	133
C 120075	203
RE C 120075	191
C 120076	147
C 120077	68
C 120078	98
C 120079	1131
C 120080	74
C 120081	182
C 120082	123
C 120083	20
C 120084	212
C 120085	28
C 120086	578
C 120087	183
C 120088	6
C 120089	8
C 120090	12
C 120091	173
C 120092	100
C 120093	198
C 120094	1208
C 120095	1036
STANDARD AU-R	476

GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.
- SAMPLE TYPE: SLUDGE R150 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: SEP 14 2001 DATE REPORT MAILED: *Sept 24/01* SIGNED BY: *C. Leong* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data *1* FA *YIN*

SAMPLE#	Au** ppb
C 120096	1716
C 120097	1351
C 120098	738
C 120099	2685
C 120100	1055
C 120101	485
C 120102	499
RE C 120102	476
C 120103	682
C 120104	505
C 120105	357
C 120106	380
STANDARD AU-R	471

Sample type: SLUDGE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

AA

GEOCHEM PRECISION METALS ANALYSIS

AA

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103110

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: D. Hladky

SAMPLE#	Au** ppb
C 120043	416
C 120044	615
C 120045	659
C 120046	849
C 120047	572
C 120048	232
C 120049	719
C 120050	409
C 120051	374
C 120052	648
C 120053	356
C 120054	657
RE C 120054	645
C 120055	370
C 120056	524
C 120057	296
C 120058	240
C 120059	116
C 120060	130
C 120061	155
C 120062	65
STANDARD AU-R	474

GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.

- SAMPLE TYPE: SLUDGE R150 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: SEP 7 2001 DATE REPORT MAILED: Sept 18/01 SIGNED BY: C. H. D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. File # A103109
P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: D. Hladky

SAMPLE#	Au** gm/mt
4001	1.29
4002	4.76
4003	.25
4004	.01
RE 4004	<.01

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: CORE R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: SEP 11 2001 DATE REPORT MAILED: Sept 21/01 SIGNED BY: [Signature] D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



ASSAY CERTIFICATE



Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103108

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: D. Hladky

SAMPLE#	Au** gm/mt
6426	2.79
6427	.22
6428	.33
6429	.51
6430	.03
6431 PULP	7.38
6432	.09
6433	.02
6434	.06
RE 6434	.07
RRE 6434	.11
6435	.04
6436	<.01
6437	<.01
6438	.03
6439	1.50
STANDARD AU-1	3.36

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: CORE R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: SEP 11 2001 DATE REPORT MAILED: Sept 21/01 SIGNED BY: C. Leong D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

GEOCHEM PRECISION METALS ANALYSIS

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A103075 Page 1

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: D. Hladky

SAMPLE#	Au** ppb
C 120001	11
C 120002	78
C 120003	260
C 120004	497
C 120005	428
C 120006	556
C 120007	355
C 120008	648
C 120009	209
C 120010	235
C 120011	596
C 120012	319
C 120013	1912
C 120014	15774
C 120015	2922
RE C 120015	2982
C 120016	7353
C 120017	4407
C 120018	1537
C 120019	633
C 120020	442
C 120021	389
C 120022	322
C 120023	592
C 120024	150
C 120025	236
C 120026	133
C 120027	114
C 120028	200
C 120029	170
C 120030	250
C 120031	413
C 120032	127
C 120033	87
STANDARD AU-R	478

GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.

- SAMPLE TYPE: SLUDGE R150 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: SEP 7 2001 DATE REPORT MAILED: Sept 20/01 SIGNED BY: C. Leong, J. Wang; CERTIFIED B.C. ASSAYERS

ASSAY RECOMMENDED for gold > 1000 ppb

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data FA VIK



SAMPLE#	Au** ppb
C 120034	213
C 120035	88
C 120036	94
C 120037	270
C 120038	172
C 120039	207
C 120040	53
C 120041	52
C 120042	133
RE C 120042	171
STANDARD FA-10R	483

Sample type: SLUDGE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. File # A103074
P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: D. Hladky

SAMPLE#

Au**
gm/mt

6401	.41
6402	.02
6403	<.01
6404	<.01
6405	<.01
6406	<.01
6407	<.01
6408	.03
6409 PULP	1.83
6410	.01
RE 6410	.02
RRE 6410	.02
6411	.02
6412	.01
6413	<.01
6414	.01
6415	.03
STANDARD AU-1	3.31

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.
- SAMPLE TYPE: CORE R150 60C
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: SEP 7 2001 DATE REPORT MAILED: *Sept 18/01* SIGNED BY: *C. Leong* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. File # A102961 Page 1

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0

SAMPLE#	Au** gm/mt	Au2 gm/mt
6332	.24	-
6333	.05	-
6334	8.63	8.80
6335	.60	-
6336	.59	-
6337	.23	-
6338	.27	-
6339	.11	-
6340	.17	-
6341	.19	-
6342	.20	-
RE 6342	.19	-
RRE 6342	.20	-
6343	.16	-
6344	.75	-
6345	.21	-
6346	.68	-
6347	.17	-
6348	.07	-
6349	.41	-
6350	.04	-
6351	.02	-
6352	.02	-
6353	.08	-
6354	.17	-
RE 6354	.16	-
RRE 6354	.18	-
6355	.02	-
6356	<.01	-
6357	<.01	-
6358	.03	.01
6359	<.01	<.01
6360	<.01	<.01
6361	.02	<.01
STANDARD AU-1	3.39	-

REVISED COPY

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

AU2 - 2nd ANALYSIS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: CORE R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 31 2001 DATE REPORT MAILED: Sept 11/01 SIGNED BY: C. Leong D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

SAMPLE#	Au** gm/mt	Au2 gm/mt
6362	.05	.03
6363	<.01	<.01
6364	.04	.03
6365	.03	<.01
6366	.06	.05
6367	.05	.03
6368	.02	<.01
6369	.02	.02
6370	.10	.09
6371	.03	.02
6372 PULP	6.74	6.47
6373	.05	-
6374	.02	-
RE 6374	.01	-
RRE 6374	.02	-
6375	.01	-
6376	.02	-
6377	.03	-
6378	.03	-
6379	<.01	-
6380 PULP	1.71	-
6381	<.01	-
6382	<.01	-
6383	<.01	-
6384	.01	-
RE 6384	.01	-
RRE 6384	.02	-
6385	.01	-
6386	<.01	-
6387	<.01	-
6388	<.01	-
6389	<.01	-
6390	<.01	-
6394	10.53	-
STANDARD AU-1	3.38	-

Sample type: CORE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

REVISED COPY

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A102937

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: D. Hladky

SAMPLE#	Au** gm/mt
6391	.09
6392	<.01
6393	.03
6394	22.83
6395	<.01
6396	<.01
RE 6396	<.01
RRE 6396	<.01
6397	.06
6398	.03
6399	.02
6400	.02
STANDARD AU-1	3.35

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: CORE R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 30 2001 DATE REPORT MAILED: Sept 7/01 SIGNED BY: C. Leong D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



ASSAY CERTIFICATE



Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A102777

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Ken Load

SAMPLE#	Au** gm/mt
6321	.06
6322	.21
6323	.72
6324	.08
6325	.05
6326	.12
6327	.01
RE 6327	<.01
RRE 6327	<.01
6328	<.01
6329	<.01
6330	.57
6331	.21
STANDARD AU-1	3.38

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: CORE R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 20 2001 DATE REPORT MAILED: *Aug 27/2001* SIGNED BY: *[Signature]* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ACME
(1)ANALYTICAL LABORATORIES LTD.
9002 Accredited Co.)

852 E. HASTINGS ST.

VANCOUVER BC V6A 1R6

PHONE (604) 253-3158 FAX (604)

253-1716

AA

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A102656 Page 1

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: R. Hall

AA

SAMPLE#	Au** gm/mt
6261	<.01
6262	.02
6263	.03
6264	.31
6265	.13
6266	.88
6267	.64
6268	.03
6269 PULP	1.72
6270	.30
RE 6270	.24
RRE 6270	.30
6271	2.06
6272	.11
6273	5.13
6274	.16
6275	.07
6276	.04
6277	.02
6278	.02
6279	.35
6280	2.72
6281	.03
6282	.07
RE 6282	.07
RRE 6282	.13
6283	.09
6284	51.91
6285	.46
6286	.12
6287	<.01
6288	<.01
6289	.06
6290	.01
STANDARD AU-1	3.30

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: CORE R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 13 2001 DATE REPORT MAILED: Aug 27/01 SIGNED BY: C. L. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data: HFA YHS

SAMPLE#	Au** gm/mt
6291	.02
6292	.13
6293	.11
6294	.07
6295	.10
6296	.09
6297	<.01
6298	<.01
6299	<.01
6300	<.01
6301	.01
6302	<.01
RE 6302	.01
RRE 6302	<.01
6303	<.01
6304	<.01
6305	<.01
6306	<.01
6307	<.01
6308	.02
6309	<.01
6310	.01
6311	.02
6312	<.01
6313	.01
6314	.01
RE 6314	<.01
RRE 6314	.01
6315	.01
6316	<.01
6317	<.01
6318	.02
6319	<.01
6320	.01
STANDARD AU-1	3.34

Sample type: CORE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A102655

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0

SAMPLE#

Au**
gm/mt

6235	14.73
6236	43.64
6237	.61
6238	12.90
6239	.09
6240	.08
6241	.03
6242	.04
6243	.04
6244	.02
6245 PULP	1.61
6246	.05
6247	.02
6248	.02
RE 6248	.03
RRE 6248	.02
6249	.01
6250	.01
6251	.01
6252	.04
6253	.02
6254	.03
6255	.03
6256	.19
6257	.04
6258	<.01
6259	.01
6260	.02
STANDARD AU-1	3.35

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: CORE R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 13 2001

DATE REPORT MAILED:

Aug 17/01

SIGNED BY:

C. L.

D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT Cow Mountain File # A102489

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Gary Polischuk

SAMPLE#	Au** gm/mt
C 121251	.05
C 121252	.78
C 121253	.06
C 121254	.23
C 121255	.07
C 121256	.84
C 121257	.45
C 121258	.35
C 121259	.15
C 121260	.13
C 121261	.17
C 121262	.27
RE C 121262	.34
C 121263	.08
C 121264	.03
C 121265	.63
C 121266	<.01
C 121267	<.01
STANDARD AU-1	3.28

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: ROCK R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 30 2001 DATE REPORT MAILED: Aug 9/01 SIGNED BY: C. L. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. File # A102488

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Gary Polischuk

SAMPLE#

Au**
gm/mt

C 121983	<.01
C 121985	<.01
C 121987	.09
C 121988	.19
C 121989	<.01

C 121990	<.01
RE C 121990	<.01
C 121991	<.01
C 121992	<.01
C 121993	<.01

C 121994	.32
STANDARD AU-1	3.40

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: ROCK R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 30 2001

DATE REPORT MAILED:

SIGNED BY: *C. Long*

D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

GEOCHEM PRECIOUS METALS ANALYSIS

Int'l Wayside Gold Mines Ltd. File # A102487
P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Gary Polischuk

SAMPLE#

Au**
ppb

C 121984
C 121986
RE C 121986

9
38
77

GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.
- SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 30 2001 DATE REPORT MAILED: *Aug 9/01* SIGNED BY: *C. Leong* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A102486

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Gary Polischuk

SAMPLE#	Au** gm/mt
C 121951	<.01
C 121952	<.01
C 121953	.04
C 121954	.18
C 121981	<.01
C 121982	<.01
RE C 121982	<.01
STANDARD AU-1	3.34

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: ROCK R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 30 2001 DATE REPORT MAILED: Aug 9/01 SIGNED BY: C. Leong, J. Wang; CERTIFIED B.C. ASSAYERS

GEOCHEM PRECIOUS METALS ANALYSIS

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A102485

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Gary Polischuk

SAMPLE#

Au**
ppb

C 121130
C 121955
RE C 121955
STANDARD AU-S

5
73
97
46

GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.

- SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 30 2001 DATE REPORT MAILED: Aug 9/01 SIGNED BY: C. Leong, J. Wang; CERTIFIED B.C. ASSAYERS

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A102484 Page 1

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0

SAMPLE#	Au** gm/mt
6203	3.79
6204	.94
6205	.03
6206	<.01
6207	.02
6208	.02
6209	.01
6210	.01
6211	.02
6212	<.01
6213	.01
6214	<.01
RE 6214	<.01
RRE 6214	<.01
6215	<.01
6216	<.01
6217	<.01
6218	<.01
6219	<.01
6220	<.01
6221	<.01
6222 PULP	1.69
6223	<.01
6224	.01
6225	.02
6226	<.01
RE 6226	<.01
RRE 6226	<.01
6227	.01
6228	<.01
6229	<.01
6230	<.01
6231	.02
6232	.03
STANDARD AU-1	3.27

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: CORE R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 30 2001 DATE REPORT MAILED: Aug 10/01 SIGNED BY: C. Leong TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



SAMPLE#	Au** gm/mt
6233	.03
6234	.03
RE 6234	.02

Sample type: CORE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ACME ANALYTICAL LABORATORIES LTD.
(9002 Accredited Co.)

852 E. HASTINGS ST. VANCOUVER BC V6A 1R6

PHONE (604) 253-3158 FAX (604) 253-1716

AA
11

GEOCHEM PRECIOUS METALS ANALYSIS

AA
11

Int'l Wayside Gold Mines Ltd. PROJECT Wayside File # A102342

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Gary Polischuk

SAMPLE#	Au** ppb
C 121975	88
C 121976	39
C 121980	17
RE C 121976	30

GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.

- SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 24 2001 DATE REPORT MAILED: *July 27/01* SIGNED BY: *C. Leong* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



ASSAY CERTIFICATE



Int'l Wayside Gold Mines Ltd. PROJECT Wayside File # A102341

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Gary Polischuk

SAMPLE#	Au** gm/mt
C 121956	<.01
C 121957	.04
C 121958	.19
C 121959	.10
C 121960	.08
C 121961	.02
C 121962	.15
C 121963	<.01
C 121964	<.01
C 121965	<.01
C 121966	.02
C 121967	<.01
C 121968	<.01
C 121969	.02
C 121970	<.01
RE C 121970	<.01
C 121971	<.01
C 121972	<.01
C 121973	<.01
C 121974	.01
C 121977	<.01
C 121978	.03
C 121979	<.01
STANDARD AU-1	3.43

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: ROCK R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 24 2001 DATE REPORT MAILED: July 27/01 SIGNED BY: C. Leong, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

GEOCHEMICAL ANALYSIS CERTIFICATE

Int'l Wayside Gold Mines Ltd. File # A102260

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted By: Jean Poutier

SAMPLE#

Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Tl	Hg	Au**
ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	%	%	ppm	ppm	ppm	ppb

C 121698	2	81	<3	43	<.3	24	6	247	2.21	5	<8	<2	5	10	<.2	<3	<3	18	.13	.032	15	71	.77	874	.06	8	.93	.02	.30	3	<5	<1	<2
C 121699	2	10	6	59	<.3	3	1	358	2.53	<2	<8	<2	8	12	<.2	<3	<3	6	.02	.021	34	25	.95	55	<.01	6	1.31	.03	.14	<2	<5	<1	5
C 121700	4	53	14	64	<.3	27	11	279	3.33	<2	<8	<2	7	14	<.2	<3	<3	6	.05	.030	15	36	.79	76	<.01	6	1.21	.03	.12	2	<5	1	17
RE C 121700	4	52	16	63	<.3	26	11	278	3.33	<2	<8	<2	7	14	<.2	<3	<3	7	.05	.030	15	39	.79	76	<.01	7	1.20	.03	.13	2	<5	<1	22
STANDARD C3	25	66	32	159	5.9	36	10	756	3.25	54	24	3	18	28	22.7	15	22	80	.54	.083	19	164	.59	146	.09	25	1.81	.04	.15	19	<5	1	-
STANDARD G-2	1	5	3	42	<.3	8	3	521	1.99	<2	<8	<2	4	66	<.2	<3	<3	40	.60	.090	7	73	.58	215	.13	7	.88	.07	.43	4	<5	<1	-

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.

UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.

ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB

- SAMPLE TYPE: ROCK R150 60C AU** GROUP 3B - 30.00 GM SAMPLE ANALYSIS BY FA/ICP.

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 19 2001 DATE REPORT MAILED: July 30/01 SIGNED BY: C. Leong D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT Bonanza Ledge File # A102102
P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: A. Justason

SAMPLE#	Au** gm/mt
6201	.70
6202	.01
RE 6202	<.01

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.
- SAMPLE TYPE: CORE R150 60C
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 11 2001 DATE REPORT MAILED: *July 16/01* SIGNED BY: *C. Leong* TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

GEOCHEMICAL ANALYSIS CERTIFICATE

Int'l Wayside Gold Mines Ltd. File # A101956

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: G. Polischuk

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
C 121124	4	66	17	114	.3	48	12	6285	14.38	8	<8	<2	3	10	<2	<3	<3	59	.19	.109	25	42	.52	183	.08	<3	1.59	.01	.03	<2	2.0
C 121125	11	100	128	195	.5	143	65	2606	7.19	20	<8	<2	9	21	<2	<3	<3	40	.38	.288	110	31	.46	419	<.01	<3	1.53	.01	.11	<2	4.6
C 121128	3	114	32	165	2.9	520	139	4240	12.24	653	<8	<2	2	160	1.3	<3	<3	44	2.74	.161	7	142	1.79	228	.01	<3	.75	.01	.02	<2	3.6
C 121133	4	38	29	109	.3	15	16	1278	8.77	7	<8	<2	4	8	<2	<3	<3	79	.09	.310	20	12	.81	114	.01	<3	2.15	.01	.02	<2	1.1
RE C 121133	4	39	22	104	.3	18	16	1228	8.60	<2	<8	<2	4	8	<2	<3	3	79	.08	.307	21	16	.80	110	.01	<3	2.13	.01	.03	<2	.8
STANDARD DS3	10	120	32	153	.6	39	12	801	3.13	28	<8	<2	4	28	5.0	5	6	79	.53	.094	18	197	.60	144	.10	<3	1.74	.04	.17	4	21.5

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO₃-H₂O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
- SAMPLE TYPE: SOIL SS80 60C AU* BY ACID LEACHED, ANALYZE BY ICP-MS. (10 gm)
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 4 2001 DATE REPORT MAILED: *July 16/01* SIGNED BY: *C. Leong* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

AA

GEOCHEM PRECIOUS METALS ANALYSIS

Int'l Wayside Gold Mines Ltd. File # A101955

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: G. Potischuk

AA

SAMPLE#	Au** ppb
C 121121	<2
C 121122	25
C 121123	<2
C 121126	4
C 121127	7
C 121129	4
C 121130 not received	-
C 121131	25
C 121132	2
C 121134	<2
RE C 121134	<2
STANDARD AU-R	454

GROUP 38 - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.
- SAMPLE TYPE: ROCK R150 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 4 2001 DATE REPORT MAILED: *July 10/01* SIGNED BY: *C. Leong* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT Cariboo Gold File # A101876 Page 1

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0

SAMPLE#

Au**
gm/mt

6138	.04
6139	5.13
6140	1.12
6141	2.81
6142	2.09
6143	7.50
6144	9.23
6145	1.68
6146	.63
6147	10.78
6148	.10
RE 6148	.10
RRE 6148	.12
6149	3.03
6150	.67
6151	1.30
6152	.23
6153	.03
6154	.01
6155	.05
6156	.02
6157	<.01
6158	.01
6159	<.01
6160	<.01
RE 6160	<.01
RRE 6160	<.01
6161 PULP	7.08
6162	<.01
6163	<.01
6164	.52
6165	<.01
6166	<.01
6167	<.01
STANDARD AU-1	3.47

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.
 - SAMPLE TYPE: CORE R150 60C
 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUN 26 2001 DATE REPORT MAILED: July 5/01 SIGNED BY: C. Leong, J. Wang; CERTIFIED B.C. ASSAYERS

SAMPLE#	Au** gm/mt
6168	.02
6169	<.01
6170	<.01
6171	<.01
6172	<.01
6173	<.01
6174	<.01
6175	<.01
6176	<.01
6177	<.01
6178	<.01
RE 6178	<.01
RRE 6178	<.01
6179	<.01
6180	<.01
6181	<.01
6182	<.01
6183	<.01
6184	<.01
6185 PULP	6.99
6186	<.01
6187	<.01
6188	<.01
6189	<.01
6190	<.01
RE 6190	<.01
RRE 6190	<.01
6191	<.01
6192	<.01
6193	<.01
6194	<.01
6195	<.01
6196	<.01
6197	<.01
6198	<.01
STANDARD AU-1	3.46

Sample type: CORE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Au** gm/mt
6199	<.01
6200	<.01
RE 6200	<.01

Sample type: CORE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. File # A101713
P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Ken Lord

SAMPLE#	Au** gm/mt
6116	11.21
6117	18.35
6118	8.98
6119	27.09
6120	.42
6121	.15
6122	.19
6123	.20
6124	.21
6125 PULP	6.93
6126	.01
6127	<.01
6128	<.01
RE 6128	<.01
RRE 6128	<.01
6129	.07
6130	.13
6131	.16
6132	.36
6133	.16
STANDARD AU-1	3.46

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.
- SAMPLE TYPE: CORE R150 60C
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUN 15 2001 DATE REPORT MAILED: June 26/01 SIGNED BY: C. Leong, J. Wang; CERTIFIED B.C. ASSAYERS

GEOCHEM PRECIOUS METALS ANALYSIS

Int'l Wayside Gold Mines Ltd. File # A101685

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: G. Polischuk

SAMPLE#

Au**
ppb

C 121001	1677
C 121005	26
C 121006	259
C 121007	12
C 121008	4
C 121012	<2
C 121013	<2
RE C 121013	<2

GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.

- SAMPLE TYPE: ROCK R150 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUN 13 2001 DATE REPORT MAILED: June 22/01 SIGNED BY: C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ASSAY RECOMMENDED for gold > 1000 ppb

GEOCHEMICAL ANALYSIS CERTIFICATE

Int'l Wayside Gold Mines Ltd. File # A101684

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: G. Potischuk

SAMPLE#

Au*
ppb

C 121002 34.9
C 121003 15.4
C 121004 200.9
C 121009 14.4
C 121010 21.2

C 121011 12.9
RE C 121011 23.0
STANDARD DS3 19.9

AU* BY ACID LEACHED, ANALYSIS BY ICP-MS. (10 gm)

- SAMPLE TYPE: SOIL SS80 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUN 13 2001 DATE REPORT MAILED: June 20/01 SIGNED BY: C. Leong D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT Caribou Gold File # A101683 Page 1

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Ken Lord

SAMPLE#

Au**
gm/mt

6081	.02
6082	.01
6083	<.01
6084	<.01
6085	<.01
6086	.01
6087	<.01
6088	<.01
6089	<.01
6090	<.01
6091 PULP	6.75
6092	<.01
RE 6092	.01
RRE 6092	<.01
6093	<.01
6094	<.01
6095	<.01
6096	<.01
6097	.01
6098	.01
6099	.09
6100	.08
6101	.06
6102	.04
6103	.15
6104	.05
RE 6104	.08
RRE 6104	.06
6105	.15
6106	.09
6107	.09
6108	.02
6109	.01
6110	<.01
STANDARD AU-1	3.40

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: CORE R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUN 13 2001 DATE REPORT MAILED: June 25/01 SIGNED BY: C. Leong D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data FA



SAMPLE#	Au** gm/mt
6111 PULP	1.77
6112	<.01
6113	<.01
6114	.76
6115	1.11
RE 6115	1.75

Sample type: CORE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. PROJECT Caribou Gold File # A101662

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0 Submitted by: Ken Lord

SAMPLE#

Au**
gm/mt

6058	.01
6059	.01
6060	<.01
6061	<.01
6062	.02
6063	.01
6064	.02
6065	.49
6066	.48
6067	.31
6068	.43
6069	.04
6070	.07
RE 6070	.07
RRE 6070	.06
6071	.07
6072	.05
6073	<.01
6074	<.01
6075	<.01
6076	.01
6077	<.01
6078 PULP	1.77
6079	<.01
6080	<.01
STANDARD AU-1	3.42

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.
 - SAMPLE TYPE: CORE R150 60C
 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUN 12 2001 DATE REPORT MAILED: June 22/01 SIGNED BY: C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ASSAY CERTIFICATE

Int'l Wayside Gold Mines Ltd. File # A101326 Page 1

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0

SAMPLE#

Au**
gm/mt

344093	<.01
344094	.01
344095	13.04
344096	.37
344097	.15
344098	.02
344099	.02
344100	.02
6001	.01
6002	.02
6003	<.01
6004	.03
RE 6004	.03
RRE 6004	.04
6005	.02
6006	.02
6007	.05
6008	.09
6009	.17
6010	.43
6011	.20
6012	.07
6013	<.01
6014	<.01
6015	<.01
6016	<.01
RE 6016	.02
RRE 6016	.01
6017	<.01
6018	<.01
6019	<.01
6020	<.01
6021	<.01
6022	.01
STANDARD AU-1	3.39

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.

- SAMPLE TYPE: CORE R150 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: MAY 15 2001 DATE REPORT MAILED: May 22/01 SIGNED BY: C. L. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Date FA YIN



SAMPLE#	Au** gm/mt
6023	<.01
6024	<.01
6025	<.01
6026	<.01
6027	<.01
6028	<.01
6029	<.01
6030	<.01
6031	<.01
6032	.02
6033	.03
6034	.12
RE 6034	.11
RRE 6034	.05
6035	<.01
6036	<.01
6037	<.01
6038	<.01
6039	<.01
6040	<.01
6041	<.01
6042	.02
6043	<.01
6044	.28
6045	.09
6046	.05
RE 6046	.05
RRE 6046	.04
6047	.09
6048	.96
6049	.04
6050	.06
6051	1.01
6052 not received	-
6053	.07
STANDARD AU-1	3.40

Sample type: CORE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Au** gm/mt
6054	.44
6055	.55
6056	.38
6057	.01
RE 6057	<.01
STANDARD AU-1	3.46

Sample type: CORE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

GEOCHEMICAL ANALYSIS CERTIFICATE

Int'l Wayside Gold Mines Ltd. File # A101089 Page 1

P.O. Box 247, 2422 Barker, Wells BC V0K 2R0



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Tl	Hg	Au**
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	%	ppm	ppm	ppm	gm/mt
344045	1	26	16	75	.5	38	19	1379	4.17	3	<8	<2	10	12	.2	<3	<3	6	.24	.041	28	43	.04	76	<.01	6	.34	.02	.18	2	<5	<1	<.01
344046	3	28	12	67	<.3	35	18	1119	4.43	5	<8	<2	9	16	<.2	<3	<3	1	.35	.034	22	9	.27	66	<.01	<3	.38	.03	.20	<2	<5	<1	<.01
344047	1	27	6	51	<.3	35	14	602	3.44	8	<8	<2	5	76	<.2	<3	<3	<1	1.44	.044	13	40	1.04	50	<.01	<3	.29	.02	.15	2	<5	1	<.01
344048	<1	56	<3	67	<.3	72	28	1275	7.44	22	<8	<2	<2	272	.2	<3	<3	6	6.12	.134	7	16	2.71	57	<.01	<3	.30	.03	.15	<2	<5	<1	<.01
344049	2	35	11	85	.4	40	16	683	4.44	7	<8	<2	6	49	.2	3	3	<1	.92	.045	14	46	1.18	55	<.01	4	.32	.02	.17	3	<5	1	<.01
344050	3	28	18	72	<.3	40	15	607	3.76	4	<8	<2	3	106	<.2	<3	<3	<1	2.15	.033	10	13	1.37	64	<.01	<3	.41	.02	.19	2	<5	<1	<.01
344051	1	53	7	76	<.3	102	34	1194	7.99	48	<8	<2	<2	294	.3	4	<3	29	6.52	.105	6	74	3.38	45	<.01	<3	.67	.02	.09	<2	<5	1	.01
344052	<1	68	<3	73	<.3	145	42	1270	7.64	61	<8	<2	<2	323	.4	<3	<3	16	7.18	.103	6	39	3.21	58	<.01	4	.41	.03	.12	2	<5	<1	<.01
344053	<1	55	<3	105	.6	165	41	1206	7.77	77	<8	<2	<2	277	.5	3	<3	33	6.52	.106	5	94	3.23	516	<.01	<3	.95	.01	.08	2	<5	<1	.01
344054	4	57	5	133	.6	130	31	991	6.33	48	<8	<2	<2	335	.3	3	<3	11	8.18	.078	5	35	2.91	46	<.01	<3	.63	.03	.09	2	<5	2	<.01
RE 344054	3	60	12	138	.8	132	30	1013	6.47	44	<8	<2	2	342	.3	3	<3	10	8.36	.081	6	41	2.97	48	<.01	<3	.63	.03	.10	2	<5	<1	<.01
RRE 344054	2	56	4	110	<.3	127	32	987	6.28	47	<8	<2	<2	332	.4	4	<3	8	8.15	.078	5	54	2.91	37	<.01	<3	.59	.02	.07	2	<5	2	<.01
344055	1	34	4	55	.5	88	23	889	4.82	34	<8	<2	4	201	<.2	<3	<3	5	5.33	.081	10	25	2.17	46	<.01	4	.37	.03	.13	<2	<5	1	<.01
344056	2	40	11	77	.5	33	13	492	3.85	<2	<8	<2	5	30	<.2	<3	3	2	.64	.033	14	46	.94	42	<.01	4	.29	.02	.15	2	<5	<1	<.01
344057	3	30	16	39	<.3	23	9	447	2.79	<2	<8	<2	4	65	<.2	<3	<3	<1	1.50	.021	11	15	.87	40	<.01	<3	.28	.02	.14	2	<5	<1	<.01
344058	3	71	12	47	<.3	24	23	1155	6.80	<2	<8	<2	<2	100	.2	3	<3	<1	3.06	.170	7	30	1.76	48	<.01	<3	.29	.03	.14	<2	<5	<1	.02
344059	1	42	13	81	<.3	40	19	625	4.48	10	<8	<2	5	54	<.2	<3	<3	2	1.48	.038	14	12	1.19	46	<.01	<3	.53	.02	.16	<2	<5	<1	<.01
344060	1	32	4	88	<.3	41	15	546	4.56	7	<8	<2	5	55	<.2	3	<3	5	1.38	.041	12	49	1.17	34	<.01	<3	1.42	.02	.15	2	<5	<1	<.01
344061	1	32	20	77	.4	37	15	776	4.28	17	<8	<2	5	62	<.2	<3	<3	<1	1.10	.067	15	8	1.11	87	<.01	<3	.73	.01	.15	<2	<5	<1	.01
344062	1	24	38	76	.3	31	12	652	4.25	8	<8	<2	6	49	<.2	<3	<3	1	.96	.033	14	43	1.09	87	<.01	<3	.82	.01	.13	<2	<5	<1	<.01
344063	1	28	11	85	.3	34	15	608	3.73	12	<8	<2	8	39	<.2	3	<3	4	.93	.035	19	15	.91	54	<.01	4	.61	.01	.17	<2	<5	1	.01
344064	2	19	19	61	<.3	31	11	605	3.44	<2	<8	<2	4	100	<.2	<3	<3	<1	1.70	.033	9	36	1.12	46	<.01	<3	.26	.02	.16	<2	<5	<1	<.01
344065	1	37	37	50	<.3	37	14	872	4.49	31	<8	<2	2	188	.2	<3	<3	<1	3.00	.030	5	7	1.55	48	<.01	<3	.27	.01	.17	<2	<5	<1	.03
344066	2	32	18	55	<.3	35	12	702	3.90	9	<8	<2	4	101	<.2	<3	<3	<1	1.68	.034	9	42	1.20	47	<.01	3	.29	.01	.17	<2	<5	<1	<.01
RE 344066	2	29	25	54	<.3	34	12	696	3.87	12	<8	<2	5	99	<.2	<3	<3	<1	1.66	.034	8	40	1.19	46	<.01	6	.29	.01	.17	2	<5	<1	<.01
RRE 344066	1	27	19	56	<.3	36	12	712	3.95	11	<8	<2	5	101	<.2	<3	<3	<1	1.69	.034	9	13	1.22	48	<.01	<3	.30	.01	.17	2	<5	<1	<.01
344067 PULP	6	36	23	58	<.3	10	<1	69	3.02	1389	<8	2	8	28	<.2	60	3	11	.04	.017	22	53	.03	87	<.01	7	.67	.02	.24	2	<5	<1	1.67
344068 PULP	2	64	22	93	1.2	150	21	1337	4.35	5367	<8	6	13	64	<.2	6	4	61	.81	.023	25	262	1.21	64	.16	4	3.17	.11	.95	10	<5	<1	6.66
344069	<1	3	53	70	<.3	27	6	866	3.76	9	<8	<2	3	459	<.2	<3	<3	<1	11.37	.024	6	26	4.41	63	<.01	<3	.17	.02	.10	3	<5	<1	<.01
344070	<1	23	5	70	.3	50	15	769	3.66	5	<8	<2	5	222	.2	<3	<3	<1	6.26	.060	8	14	1.94	88	<.01	3	.31	.01	.17	<2	<5	<1	.01
344071	<1	20	<3	51	<.3	77	22	1759	7.14	31	<8	<2	<2	474	.5	<3	<3	14	15.41	.041	3	34	4.76	174	<.01	3	.18	.02	.08	<2	<5	<1	<.01
344072	<1	47	6	46	<.3	301	80	1160	5.73	217	<8	<2	<2	462	.5	<3	<3	17	13.97	.056	2	76	4.45	262	<.01	<3	.24	.02	.12	<2	<5	<1	<.01
344073	<1	<1	8	51	<.3	56	14	1675	6.76	53	<8	<2	<2	574	.4	<3	<3	9	16.58	.029	6	39	5.47	184	<.01	<3	.14	.03	.09	<2	<5	<1	<.01
344074	2	<1	36	<1	.5	16	10	266	5.49	221	<8	<2	<2	44	<.2	<3	35	<1	1.20	.004	<1	17	.42	15	<.01	<3	.05	<.01	.03	3	<5	<1	1.29
STANDARD C3/AU-1	24	61	31	159	6.0	34	10	738	3.37	55	20	2	19	25	21.8	14	21	78	.55	.085	18	163	.60	137	.09	20	1.82	.04	.15	15	<5	1	3.46
STANDARD G-2	1	2	<3	39	<.3	8	4	509	2.01	<2	<8	<2	4	62	<.2	<3	<3	38	.63	.090	7	76	.59	201	.13	3	.91	.06	.44	3	<5	1	-

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: CORE R150 60C AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.
Samples beginning 'RE' are Retuns and 'RRE' are Reject Retuns.

DATE RECEIVED: APR 23 2001 DATE REPORT MAILED: May 4/01 SIGNED BY: [Signature] TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data FA

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Tl	Hg	Au**
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	%	ppm	ppm	ppm	gm/mt
344075	<1	3	5	59	<3	35	7	2021	5.90	24	<8	<2	2	459	.3	<3	<3	<1	11.32	.121	5	1	3.44	82	<.01	3	.24	.01	.16	<2	<5	<1	<.01
344076	4	15	24	36	<3	19	7	481	2.42	<2	<8	<2	3	153	<.2	<3	<3	<1	2.94	.019	6	46	1.21	51	<.01	<3	.24	.01	.14	<2	<5	<1	.01
344077	3	9	16	36	<3	20	7	427	1.93	6	<8	<2	6	133	<.2	<3	<3	<1	2.42	.030	13	13	1.10	60	<.01	<3	.30	.01	.18	<2	<5	<1	<.01
344078	5	7	19	15	<3	15	3	1503	2.16	7	<8	<2	6	156	<.2	3	<3	<1	3.51	.029	11	71	1.16	46	<.01	3	.21	.01	.17	3	<5	<1	.01
344079	<1	71	<3	71	<3	219	45	1351	8.17	65	<8	<2	<2	272	.2	<3	<3	9	6.87	.136	4	30	3.16	89	<.01	4	.49	.01	.14	<2	<5	<1	<.01
344080	2	76	<3	55	<3	304	68	1790	8.89	157	<8	<2	<2	374	.2	<3	<3	12	10.09	.100	2	65	3.19	101	<.01	<3	.29	.01	.16	<2	<5	<1	.01
344081	1	95	<3	56	.5	171	44	1483	8.31	73	<8	<2	<2	244	<.2	<3	<3	16	6.64	.132	5	17	2.24	85	<.01	<3	.31	.03	.18	<2	<5	<1	<.01
344082	<1	81	<3	53	<3	157	48	1444	7.70	97	<8	<2	<2	385	.5	<3	<3	15	10.09	.089	2	54	3.23	116	<.01	<3	.31	.02	.14	<2	<5	<1	<.01
RE 344082	1	81	5	53	<3	158	48	1447	7.74	94	<8	<2	<2	384	<.2	<3	<3	14	10.13	.089	2	51	3.25	116	<.01	5	.31	.02	.15	<2	<5	<1	<.01
RRE 344082	<1	85	<3	52	<3	161	47	1459	7.80	92	<8	<2	<2	385	.2	<3	<3	13	10.13	.092	2	39	3.26	122	<.01	5	.34	.02	.16	<2	<5	<1	<.01
344083	<1	<1	12	42	<3	73	24	1431	6.16	84	<8	<2	2	495	.2	<3	3	13	15.14	.020	5	63	5.32	204	<.01	5	.17	.03	.08	<2	<5	<1	<.01
344084	1	1	17	39	<3	73	21	1396	5.70	84	<8	<2	<2	475	<.2	<3	<3	10	12.90	.032	5	44	4.25	160	<.01	3	.17	.02	.09	<2	<5	<1	<.01
344085	2	12	11	45	.3	102	25	1866	6.78	129	<8	<2	<2	532	.4	<3	<3	15	15.45	.041	3	55	5.30	173	<.01	4	.16	.03	.10	<2	<5	<1	.01
344086 not received	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
344087 PULP	1	63	23	101	1.8	157	23	1387	4.55	5835	<8	7	14	67	<.2	8	<3	64	.85	.026	27	261	1.28	66	.17	15	3.26	.12	1.02	9	<5	<1	7.02
344088 PULP	6	35	23	58	.3	10	<1	68	3.04	1489	<8	5	8	29	<.2	60	4	11	.04	.018	23	51	.03	92	<.01	12	.67	.02	.26	<2	<5	<1	1.70
344089	2	32	16	49	.3	26	12	602	3.45	15	<8	<2	10	57	<.2	<3	<3	<1	1.00	.033	15	15	.71	65	<.01	9	.47	.01	.25	<2	<5	<1	<.01
344090	4	2	<3	1	.3	7	1	154	.74	26	<8	<2	<2	6	<.2	<3	<3	2	.20	.001	2	51	.07	13	<.01	6	.06	<.01	.04	5	<5	<1	.89
344091	5	2	4	3	.5	3	1	467	.88	21	<8	<2	<2	15	<.2	<3	<3	1	.56	.001	3	22	.17	15	<.01	6	.06	<.01	.05	<2	<5	1	.03
344092	2	22	6	50	<3	26	11	581	3.11	21	10	<2	11	97	<.2	3	<3	1	1.76	.053	13	60	.68	63	<.01	6	.38	.01	.23	2	<5	<1	.01
STANDARD C3/AU-1	25	61	31	159	6.4	34	10	753	3.37	55	22	<2	18	26	22.9	14	22	73	.54	.090	18	157	.60	144	.09	22	1.83	.04	.16	15	<5	<1	3.49
STANDARD G-2	3	<1	<3	39	<3	7	4	527	2.06	<2	<8	<2	5	66	<.2	<3	<3	39	.64	.096	8	73	.60	214	.13	<3	.92	.07	.48	<2	<5	<1	<.01

Sample type: CORE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



ALS Chemex

Aurora Laboratory Services Ltd.
Analytical Chemists * Geochemists * Registered Assayers
212 Brooksbank Ave., North Vancouver
British Columbia, Canada V7J 2C1
PHONE: 604-984-0221 FAX: 604-984-0218

To: INTERNATIONAL WAYSIDE GOLD MINES

BOX 247
WELLS, BC
V0K 2R0

Project: CARIBOO GOLD
Comments: ATTN: RICHARD HALLKEN LORD

Page: 1
Total: 1
Certificate Date: 23-MAR-2001
Invoice No.: I0113678
P.O. Number:
Account: JLI

CERTIFICATE OF ANALYSIS

A0113678

SAMPLE	PREP CODE	Au ppb FA+AA										
1951	205 226	420										
1952	205 226	240										
1953	205 226	150										
1954	205 226	130										
1955	205 226	115										
1956	205 226	105										
1957	205 226	60										
1958	205 226	280										
1959	205 226	125										
1960	205 226	35										
1961	205 226	45										
1962	205 226	55										
1963	205 226	310										
1964	205 226	50										
1965	205 226	290										
1966	205 226	15										
1967	205 226	75										
1968	205 226	15										
1969	205 226	< 5										
1970	205 226	< 5										
1971	205 226	25										
1972	205 226	< 5										
1973	205 226	35										
1974	225 --	1685										

CERTIFICATION: *Angela Yuen*



To: INTERNATIONAL WAYSIDE GOLD MINES

Project : CARIBOO GOLD
Comments: ATTN: KEN LORD/RICHARD HALL

Page 1 of 2
Total : 2
Certificate Date: 06-APR-2001
Invoice No. : I0114552
P.O. Number :
Account : JLI

A0114552

CERTIFICATION:



ALS Chemex

Aurora Laboratory Services Ltd.
 Analytical Chemists * Geochemists * Registered Assayers
 212 Brooksbank Ave., North Vancouver
 British Columbia, Canada V7J 2C1
 PHONE: 604-984-0221 FAX: 604-984-0218

To: INTERNATIONAL WAYSIDE GOLD MINES

BOX 247
 WELLS, BC
 V0K 2R0

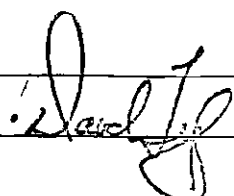
Project: CARIBOO GOLD
 Comments: ATTN: RICHARD HALL/KEN LORD

Page: 1-B
 Total: 1
 Certificate Date: 09-APR-2001
 Invoice No.: 10114312
 P.O. Number:
 Account: JLI

CERTIFICATE OF ANALYSIS

A0114312

SAMPLE	PREP CODE	Mo ppm	Na %	Ni ppm	P ppm	Pb ppm	S %	Sb ppm	Sc ppm	Sr ppm	Ti %	Tl ppm	U ppm	V ppm	W ppm	Zn ppm
1951	244 229	9	0.02	56	950	24	1.55	< 2	6	137	< 0.01	< 10	< 10	48	< 10	120
1952	244 229	5	< 0.01	49	1000	18	1.87	4	5	123	< 0.01	< 10	< 10	38	< 10	98
1953	244 229	7	0.01	51	1180	6	1.65	< 2	5	128	< 0.01	< 10	< 10	27	< 10	74
1954	244 229	8	0.01	88	1860	4	1.29	< 2	5	232	< 0.01	< 10	< 10	29	< 10	62
1955	244 229	3	< 0.01	55	1610	26	0.84	< 2	3	103	< 0.01	< 10	< 10	31	< 10	90
1956	244 229	4	0.01	53	1340	16	1.41	2	5	133	< 0.01	< 10	< 10	38	< 10	92
1957	244 229	3	< 0.01	46	1100	28	1.07	< 2	5	111	< 0.01	< 10	< 10	31	< 10	114
1958	244 229	4	0.01	62	1010	24	3.07	< 2	6	127	< 0.01	< 10	< 10	29	< 10	142
1959	244 229	7	0.01	47	1120	8	0.93	< 2	4	133	< 0.01	< 10	< 10	25	< 10	118
1960	244 229	10	0.01	87	2490	4	1.59	< 2	5	279	< 0.01	< 10	< 10	21	< 10	46
1961	244 229	15	0.01	103	4100	4	1.12	< 2	8	442	< 0.01	< 10	< 10	23	< 10	50
1962	244 229	5	0.01	139	1980	6	1.16	< 2	12	430	< 0.01	< 10	< 10	18	< 10	48
1963	244 229	7	0.01	188	1210	16	4.40	4	13	489	< 0.01	< 10	< 10	18	< 10	82
1964	244 229	7	< 0.01	102	740	8	2.01	2	8	379	< 0.01	< 10	< 10	9	< 10	56
1965	244 229	11	0.01	132	1530	24	4.06	< 2	10	443	< 0.01	< 10	< 10	16	< 10	96
1966	244 229	8	0.01	93	1310	2	1.27	2	9	410	< 0.01	< 10	< 10	14	< 10	82
1967	244 229	7	0.02	51	2600	10	4.18	4	5	199	< 0.01	< 10	< 10	13	< 10	140
1968	244 229	7	0.01	27	1150	6	2.24	< 2	5	200	< 0.01	< 10	< 10	10	< 10	86
1969	244 229	4	< 0.01	34	760	6	1.84	< 2	3	103	< 0.01	< 10	< 10	8	< 10	68
1970	244 229	3	< 0.01	27	700	6	2.63	< 2	3	68	< 0.01	< 10	< 10	6	< 10	84
1971	244 229	6	0.02	67	1600	12	4.18	< 2	6	188	< 0.01	< 10	< 10	14	< 10	114
1972	244 229	< 1	0.02	32	380	2	0.71	< 2	3	43	< 0.01	< 10	< 10	4	< 10	96
1973	244 229	4	0.01	39	690	18	1.04	2	2	141	< 0.01	< 10	< 10	8	< 10	140
1974	244 229	6	0.02	11	170	22	0.01	96	6	29	< 0.01	< 10	< 10	11	< 10	64

CERTIFICATION: 



ALS Chemex

Aurora Laboratory Services Ltd.

Analytical Chemists * Geochemists * Registered Assayers

212 Brooksbank Ave., North Vancouver
British Columbia, Canada V7J 2C1
PHONE: 604-984-0221 FAX: 604-984-0218

To: INTERNATIONAL WAYSIDE GOLD MINES

BOX 247
WELLS, BC
V0K 2R0

Project: CARIBOO GOLD
Comments: ATTN: RICHARD HALL/KEN LORD

Page: 1-A
Total: 1
Certificate Date: 09-APR-2001
Invoice No.: I0114312
P.O. Number:
Account: JLI

CERTIFICATE OF ANALYSIS

A0114312

SAMPLE	PREP CODE	Ag ppm	Al %	As ppm	B ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cd ppm	Co ppm	Cr ppm	Cu ppm	Fe %	Ga ppm	Hg ppb	K %	La ppm	Mg %	Mn ppm
1951	244 229	0.4	0.50	118	< 10	70	0.5	< 2	4.47	1.0	12	61	33	3.70	< 10	10	0.22	< 10	1.50	935
1952	244 229	0.2	0.41	124	< 10	80	0.5	< 2	2.91	0.5	9	98	34	2.97	< 10	10	0.18	< 10	1.02	585
1953	244 229	0.2	0.38	142	< 10	100	0.5	< 2	2.82	0.5	13	91	36	2.93	< 10	< 10	0.20	< 10	1.02	650
1954	244 229	0.2	0.48	218	< 10	120	0.5	< 2	4.57	0.5	22	80	33	3.11	< 10	< 10	0.26	< 10	1.62	1085
1955	244 229	0.2	0.34	122	< 10	130	< 0.5	< 2	2.24	0.5	9	150	36	1.84	< 10	< 10	0.17	< 10	0.73	455
1956	244 229	0.2	0.40	138	< 10	70	0.5	< 2	2.42	0.5	11	134	38	2.44	< 10	< 10	0.18	< 10	0.82	610
1957	244 229	0.2	0.27	94	< 10	90	< 0.5	< 2	2.39	0.5	9	99	36	2.08	< 10	< 10	0.13	< 10	0.81	550
1958	244 229	< 0.2	0.36	272	< 10	50	0.5	< 2	2.01	0.5	17	66	43	3.68	< 10	10	0.19	< 10	0.74	450
1959	244 229	< 0.2	0.35	90	< 10	160	0.5	< 2	3.39	0.5	11	68	41	2.61	< 10	10	0.17	< 10	1.34	570
1960	244 229	< 0.2	0.46	212	< 10	140	0.5	< 2	4.61	0.5	16	16	4	3.11	< 10	< 10	0.26	< 10	1.57	1105
1961	244 229	< 0.2	0.43	232	< 10	120	0.5	< 2	7.59	2.0	23	16	3	4.42	< 10	< 10	0.25	< 10	2.67	1660
1962	244 229	< 0.2	0.39	312	< 10	100	0.5	< 2	8.42	2.0	44	23	5	5.44	< 10	< 10	0.24	< 10	3.26	1850
1963	244 229	0.8	0.25	236	< 10	90	0.5	< 2	10.55	2.5	46	29	20	8.08	< 10	10	0.16	< 10	4.66	2030
1964	244 229	0.4	0.18	116	< 10	70	< 0.5	< 2	10.30	2.0	26	13	19	5.49	< 10	10	0.11	< 10	3.59	1605
1965	244 229	0.8	0.32	172	< 10	50	0.5	< 2	9.91	2.5	52	19	20	7.84	< 10	60	0.19	< 10	4.06	1660
1966	244 229	0.6	0.34	104	< 10	170	0.5	< 2	10.35	2.5	33	16	35	5.74	< 10	10	0.18	< 10	4.14	1765
1967	244 229	0.2	0.45	66	< 10	70	< 0.5	< 2	4.41	1.0	35	28	92	7.56	< 10	40	0.21	< 10	1.77	770
1968	244 229	0.2	0.40	22	< 10	70	< 0.5	< 2	5.87	< 0.5	25	13	81	6.33	< 10	30	0.14	< 10	1.81	880
1969	244 229	0.2	0.37	16	< 10	50	< 0.5	< 2	2.55	1.0	22	13	51	3.63	< 10	50	0.08	< 10	1.80	550
1970	244 229	< 0.2	0.71	16	< 10	30	< 0.5	< 2	1.77	< 0.5	22	10	55	4.95	< 10	270	0.07	< 10	0.72	405
1971	244 229	< 0.2	0.93	136	< 10	100	0.5	< 2	3.41	0.5	45	19	105	8.43	< 10	290	0.20	< 10	1.89	1170
1972	244 229	< 0.2	0.43	26	< 10	150	< 0.5	< 2	0.73	< 0.5	15	36	24	3.63	< 10	30	0.23	< 10	0.91	310
1973	244 229	0.4	0.35	34	< 10	150	< 0.5	< 2	3.96	1.5	12	50	38	3.25	< 10	10	0.21	< 10	1.51	495
1974	244 229	< 0.2	0.65	1465	< 10	100	0.5	< 2	0.05	< 0.5	1	44	39	3.09	< 10	50	0.26	10	0.03	70

CERTIFICATION:

RERUNS from A0113678



ALS Chemex

Aurora Laboratory Services Ltd.
Analytical Chemists * Geochemists * Registered Assayers
212 Brooksbank Ave., North Vancouver
British Columbia, Canada V7J 2C1
PHONE: 604-984-0221 FAX: 604-984-0218

To: INTERNATIONAL WAYSIDE GOLD MINES

BOX 247
WELLS, BC
V0K 2R0

Project : CARIBOO GOLD
Comments: ATTN: KEN LORD/RICHARD HALL

Page : 1
Total : 2
Certificate Date: 06-APR-2001
Invoice No. : I0114552
P.O. Number :
Account : JLI

CERTIFICATE OF ANALYSIS

A0114552

SAMPLE	PREP CODE	Au ppb FA+AA	Au FA g/t								
344001	205 226	< 5	-----								
344002	205 226	< 5	-----								
344003	205 226	170	-----								
344004	205 226	70	-----								
344005	205 226	45	-----								
344006	205 226	90	-----								
344007	205 226	>10000	38.84								
344008	205 226	25	-----								
344009	205 226	35	-----								
344010	205 226	30	-----								
344011	205 226	5	-----								
344012	205 226	< 5	-----								
344013	205 226	< 5	-----								
344014	205 226	< 5	-----								
344015	205 226	< 5	-----								
344016	205 226	< 5	-----								
344017	205 226	< 5	-----								
344018	205 226	< 5	-----								
344019	205 226	< 5	-----								
344020	205 226	10	-----								
344021	205 226	5	-----								
344022	205 226	5370	-----								
344023	205 226	30	-----								
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344025	225 --	6730	-----								
344026	205 226	< 5	-----								
344027	205 226	10	-----								
344028	205 226	30	-----								
344029	205 226	10	-----								
344030	205 226	20	-----								
344031	205 226	90	-----								
344032	205 226	< 5	-----								
344033	205 226	< 5	-----								
344034	205 226	5	-----								
344035	205 226	10	-----								
344036	205 226	10	-----								
344037	205 226	< 5	-----								
344038	205 226	5	-----								
344039	205 226	40	-----								
344040	205 226	80	-----								

CERTIFICATION:

Angela [Signature]

APPENDIX 7 – List of References

Published References

Bowman, A.

1889: Report on the geology of the mining district of Cariboo, British Columbia; Geological Survey of Canada, Annual Report for 1887-1888, v. 3, pt. 1, p. 1-49c.

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CERTIFICATION

I, Godfrey J. Walton, resident of North Vancouver, British Columbia, Canada hereby certify as follows:

- 1) I am a Consulting Geologist with an office located at 5463 Cortez Crescent, North Vancouver, British Columbia.
- 2) I also act as a Contract Vice president of Exploration for International Wayside Gold Mines Ltd.
- 3) I graduated with a Honours degree of Bachelor of Science in Geology from the University of Alberta in 1974 and a degree of Masters of Science in Geology, from Queen's University in 1978.
- 4) I have practiced my profession on a continuous basis for 28 years.
- 5) I am registered as a Professional Geoscientist (No. 19961) by the Association of Professional Engineers and Geoscientists of the Province of British Columbia since December 15th 1992.
- 6) I am knowledgeable and experienced in surface and underground exploration for gold.
- 7) I held the position of mine manager as defined in the Mines Act on behalf of International Wayside Gold Mines Ltd. for approved work programs in the BC vein area (Permit Number MX-11-113) during the period May 15th to December 15th, 2001. This included supervision of personnel and contractors involved in exploration work as scheduled by the directors of International Wayside Gold Mines Ltd.
- 8) I have hold shares in International Wayside Gold Mines and option to purchase shares in this company.
- 9) This certification is for the purposes of the "Report for Assessment, Cariboo Gold Project – Wells, B.C.", written by myself dated August 15th, 2002

Dated at North Vancouver, Province of British Columbia, Canada this 14th day of August, 2002.



Godfrey J. Walton, P. Geo