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PROSPECTING AND DRILLING REPORT
ON THE

TOMMY JACK PROPERTY

MINERAL CLAIMS
Au 1 to 4, Tom, and Sic 1 to 6
(68 units)

OMINECA MINING DIVISION
BRITISH COLUMBIA, CANADA

Latitude: 56° 08' 03" N Longitude: 127° 36' 57" W

N.T.S 94 D/4E

Owner: Lorne Warren
825 Lower Viewmount Road
Smithers, BC V0J2N0

Operator: Kodiak Exploration Ltd.
Suite 520 - 885 Dunsmuir Street
Vancouver, BC V6C 1N5

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Consulting Geologist

GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT

27,314

December 15, 2003

SUMMARY

The Tommy Jack Property consists of 68 contiguous claim units and is located within the Omineca Mining Division, approximately 95 km northeast of the town of Hazelton British Columbia, Canada. Road access is ~ 16 km away but a new road is planned along Tommy Jack Creek. Topography is mountainous and most of the property is below tree line in primary growth hemlock, fir and spruce forest.

Noranda worked on the property in the mid-1980's, conducting extensive soil and geophysical surveys and drilled 35 short drill holes. Noranda returned the property to the current owner's wife and the Warren's have held the core claims in good standing until present. Subsequent to the results from the 2002 field programme Kodiak entered into a five-year option agreement with Lorne Warren, at which time Kodiak will have earned 100% ownership. Fieldwork continued in 2003 consisting of prospecting, sampling of Noranda drill core, ~ 20 km of induced polarization geophysical surveying, and 1035.9 m of diamond drilling.

Tommy Jack is underlain by the Bowser Lake Group a clastic sedimentary rock assemblage, which overlies Stikine, Cache Creek, and Quesnel Terrane rocks. Bowser Lake Group rocks are intruded by the Upper Cretaceous Bulkley Intrusions that are directly related to the mineral occurrences in the area. Most of the Bowser Lake sedimentary rocks are Fe-carbonate and clay altered and locally silicified on the Tommy Jack Property. Dacite dykes cut the Bowser Group rocks and silicification and alteration tends to be more intense in the vicinity of these dykes. Quartz-carbonate veins are common throughout and gold and silver bearing quartz-carbonate-sulphide (sphalerite-galena-pyrite+/-arsenopyrite) veins occur locally.

The 2003 field programme identified a 150x1000 m high chargeability anomaly, which coincides with previously discovered Au-Ag soil anomalies and Au-Ag mineralization intersected by drilling in 1986 and 1987. Drilling during the 2003 programme tested the Camp Showing to depth and along strike and the northernmost chargeability high, encountering several zones of Ag mineralization and weak gold mineralization.

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1.0 INTRODUCTION

This report is intended to disclose the results of the prospecting, induced polarization geophysical surveying and drilling programme conducted by Kodiak Exploration Ltd during the 2003 field season on the Tommy Jack Property. The work programme was designed to (1) find the strike extents of the discovery showing on Tommy Jack Creek through prospecting and IP surveying and (2) to drill test gold-silver mineralization on Tommy Jack Creek and test geophysical anomalies.

Field activities were conceived, supervised, conducted and the data interpreted by the author and Acme Analytical Laboratories provided all geochemical analyses presented below.

2.0 PROPERTY DESCRIPTION AND LOCATION

The Tommy Jack Property consists of 68 contiguous claim units, covering an area of 14.5 km^2 within the Omineca Mining Division, British Columbia, Canada (Figures 1 and 2). It is located at 56° 08' 03" N latitude and 127° 36' 57" W longitude, in NTS map sheet 094D/04 E. Currently, these claim blocs have not been legally surveyed. Table 1 lists the claims, claim numbers, current expiry dates and their ownership status for the claim blocs that comprise the Tommy Jack Property.

Claim Name	Tenure #	Expiry Date	Owner	Ownership
AU 1	238791	June 12, 2006	Lorne Warren	100%
AU 2	238792	June 12, 2006	Lorne Warren	100%
AU 3	238793	June 12, 2006	Lorne Warren	100%
AU 4	238794	June 12, 2006	Lorne Warren	100%
TOM	238907	October 24, 2003	Lorne Warren	100%
SIC 1	395459	July 25, 2006	Int. Kodiak Res.	100%
SIC 2	395460	July 25, 2006	Int. Kodiak Res.	100%
SIC 3	395461	July 26, 2006	Int. Kodiak Res.	100%
SIC 4	395462	July 26, 2006	Int. Kodiak Res.	100%
SIC 5	395463	July 26, 2006	Int. Kodiak Res.	100%
SIC 6	395464	July 26, 2006	Int. Kodiak Res.	100%

Table 1: Tommy Jack Property claims, expiry dates, and ownership.

Lorne Warren owns the core claims to the Tommy Jack Property and has entered into an option agreement with International Kodiak Resources Ltd. Under this option agreement Kodiak may earn 100% interest in the Au 1 to 4 and Tom claims after making a series of cash and stock payments over a period of five years.

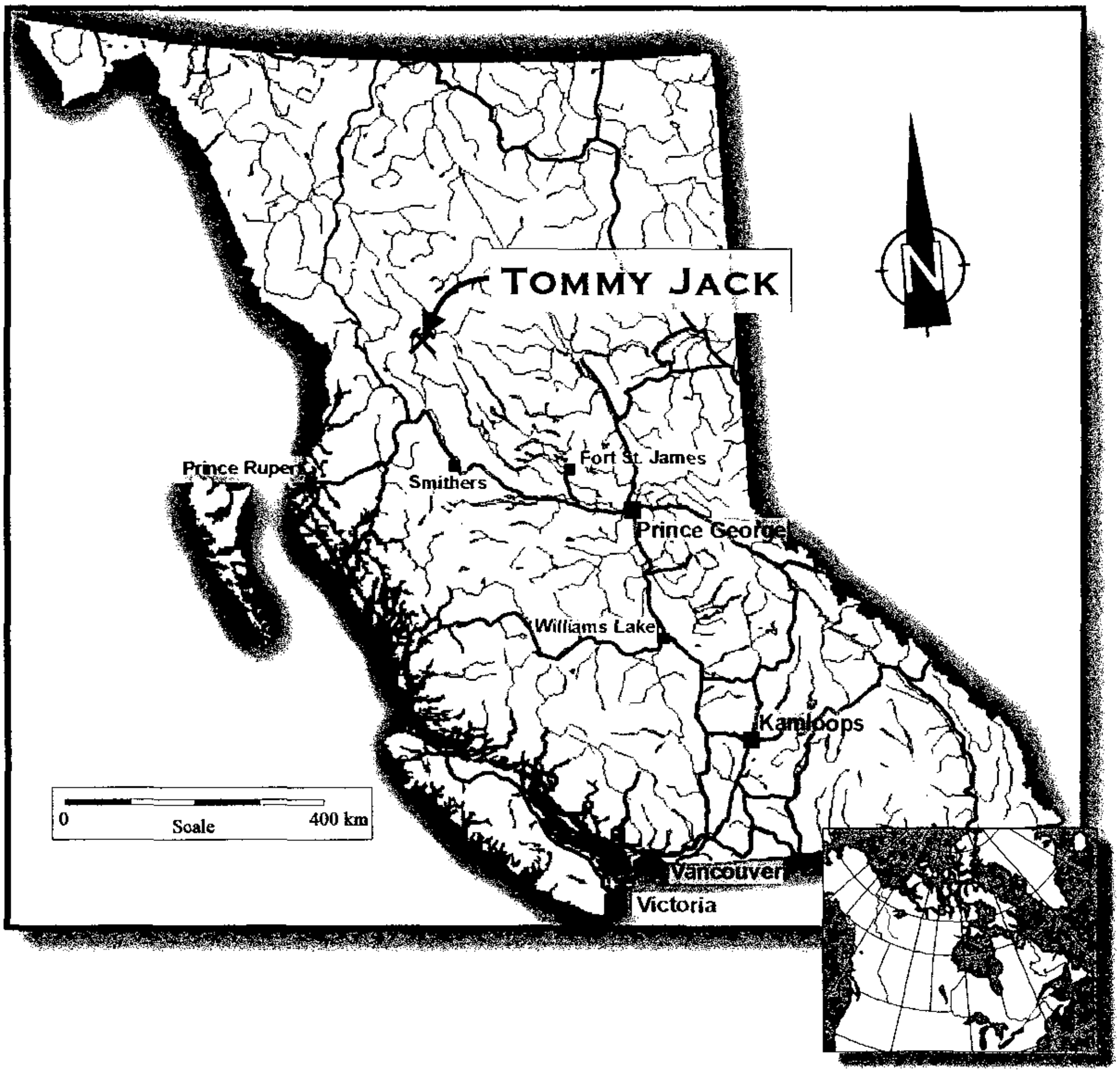

Figure 1: Map of British Columbia, Canada depicting the location of the Tommy Jack Property with respect to major towns, cities and highways.

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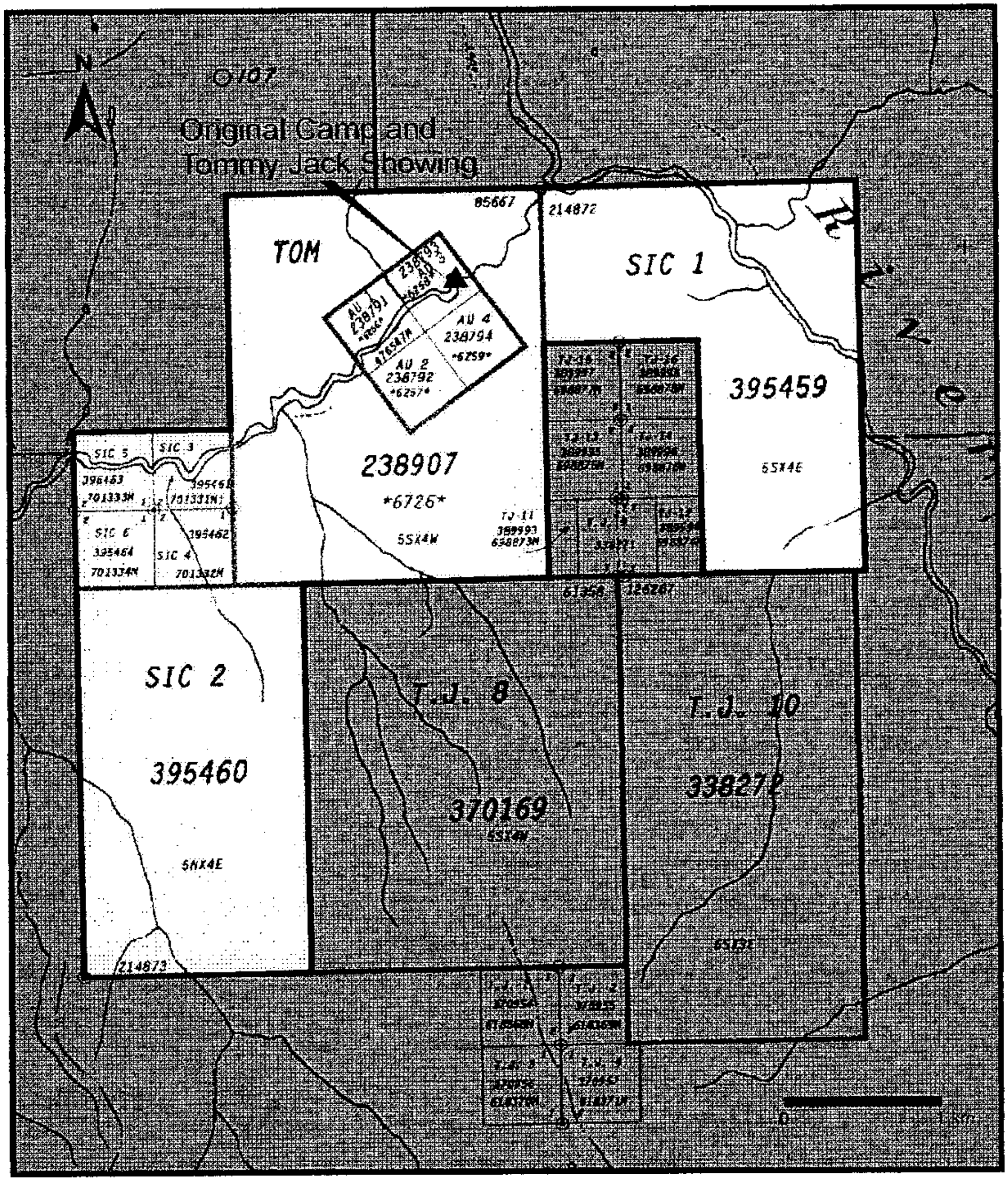

Figure 2: Claim map (as of November 20, 2003) depicting the claims in the Tommy Jack area; Kodiak owns the highlighted claims Sic 1-6, Tom, and Au 1-4. Also, the location of the Tommy Jack "Camp Showing" is denoted by a triangle.

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Outcrop of the mineralization occurs in a cut bank on the side of Tommy Jack Creek and its strike extents appear to continue up the hillside away from the creek. Tommy Jack Creek is not specified as a protected watershed area. There are no parks/nature reserves in the area around or over the Tommy Jack Property.

3.0 ACCESS, CLIMATE, INFRASTRUCTURE, AND PHYSIOGRAPHY

Elevations on the Tommy Jack Property range from 730 m at the junction of Tommy Jack Creek and the Sicintine River to 1700 m above mean sea level. Most of the property is covered by dense, primary growth hemlock, spruce and fir forest and above 1600 m vegetative cover is dominated by scrubby spruce, heather, moss and grass. The topography consists of rugged mountains, which descend 1000 m into the main drainages with slope grades commonly, 20 to 40%.

Tommy Jack is 95 km north of the Yellowhead Highway (Hwy 16) and the community of Hazelton, British Columbia. Currently access is by helicopter. The nearest road access is located approximately 16 km south-southwest of the property with a new road slated to go through the property within the next two years. This new road is intended to be the new haul road for the Kemess Au-Cu mine (owned by Northgate Exploration), which is 110 km northeast of the Tommy Jack Property.

Precipitation in the area is high (~ 1300 mm) with snow falling in October and remaining until late May or June. Fall is often subject to heavy valley fogs and poor weather, which closes down the field season by October and doesn't allow for safe flying until late December. Groundwork is therefore limited to the summer months between late June and October, although drilling and some geophysical surveying is possible in the winter.

4.0 HISTORY

The first discovery of the Tommy Jack Showing was by native trappers and two prospectors apparently worked the in the area between the 1930's and 40's (Myers, 1988). Kerr and Glen Huck staked the property in either 1962 or 1963 (Myers, 1988) and Canex Aerial Exploration recorded the first work on the property in 1964. Canex's publicly recorded work consisted of a 1460 by 1650 m soil grid but they also did trenching and drilling around the showing in 1967, which is written up in a unpublished company report.

Most of the work done on the Tommy Jack Property was by Noranda Exploration between the years of 1985 and 1987 (Table 3). Noranda had optioned the ground from a prospector based in Smithers, BC. They conducted a large soil geochemical survey (2004 samples over a 2.8 by 2.0 km area) and followed it up in 1986 by drilling 10 holes totaling 762 metres. After/during the first round of drilling Noranda completed 55.5 km of ground magnetometer surveying, 4 km of VLF-EM surveying, prospecting, silt sampling and assayed their soils taken in 1985 for Au. In 1987, they completed another

25 drill holes totaling 1690.5 metres and subsequent to the results decided to return the property to its owner, Joyce Warren.

Year	Report #	Company	Work Done	$ Spent	$ Spent (2002 $'s)
1963/64	574	Cancx	827 soils	$9,000.00	$52,000.00
1967	n/r	Canex	trenching; 3 drill holes (not assayed)	n/a	n/a
1985	13778	Noranda	45 soils; 2 silts; 12 rocks	$3,623.00	$6,069.00
1985	14631	Noranda	2004 soils	$15,146.56	$87,347.00
1986	15515	Noranda	10 DDH's, 762 m; 191	$120,755.00	$198,610.00
1987	16062	Noranda	re-analyzed 543 soils from 1985	$2,384.50	$3,785.00
1987	16943	Noranda	25 DDH's, 1690.5 m; 338 samples	$209,032.00	$331,797.00
1986/87	n/r	Noranda	55.5 km of mag; 4 km of VLF-EM, 115 rocks; 92 silts	n/a	n/a
1989	19581	Intertech	28 rocks; 5 silts; 746 soil; 23.2 km VLF-EM	$63,208.18	$91,872.00
1995	24589	A. Raven	15 rocks; 132 soils	$15,660.00	$19,716.00
2000	26197	A. Raven	35 rocks; 4.3 km SP survey; 12 m trenching	$24,804.00	$25,973.00
2002	27175	Kodiak	27 rocks; 12 chips; 36 core samples	$34,655.20	$34,655.20
				Total	**$851,824.20**

Table 2: Summary of recorded work on the Tommy Jack Property.

Intertech Minerals Corp. optioned the Tommy Jack Property from Joyce Warren in 1989 and completed a geochemical soil survey (south of the Noranda grid), a 23.2 km of VLF-EM survey and prospecting programme. They recommended further work including drilling but failed to follow-up on this work and gave the property back to Joyce Warren.

Since 1989, little work has occurred and Joyce Warren has signed the title of the central 20 unit bloc and 4 two post claims to her husband Lorne Warren, which they have kept in good standing since 1989.

The area south of the Warren ground (Figure 2) was staked and is currently held by Alan Raven (formerly a contactor for Noranda). Alan Raven has conducted a small geochemical soil survey, a self-potential geophysical survey, and minor trenching on his ground. In May of 2002, Alan Raven optioned his property to Gold City Industries who is currently the operator.

In 2002, International Kodiak Resources Ltd (now Kodiak Exploration Ltd) optioned the Tommy Jack Property and completed a work programme consisting of prospecting, geochemical rock and drill core sampling to evaluate the Tommy Jack Property.

5.0 GEOLOGY

The Tommy Jack Property lies in the Intermontane Belt of the British Columbia Cordillera. It is within a geological feature called the Bowser Basin, which is characterized by the Middle to Upper Jurassic Bowser Lake Group, a large sedimentary overlap assemblage that covers rocks of the Stikine, Quesnel and Cache Creek Terranes (Figure 3; after Wheeler and McFeely, 1991). Intruding the Bowser Lake Group are the

Upper Cretaceous Bulkley Intrusions, which form high-level granodiorite, quartz monzonite to monzodiorite mountain massifs in the area (Evenchick and Porter, 1993). These intrusions impart wide hornfelsed alteration zones within the Bowser Group sedimentary rocks, up to 1000 m from the intrusion contacts. Felsic dykes are also common around the massifs. The Bulkley Intrusions appear to be directly related to mineral occurrences in the area (Richards, 1978).

On the Tommy Jack Property, Bowser Lake Group sedimentary rocks are generally shallowly dipping, medium to fine grained arenite intercalated with minor siltstone, shale and conglomerate. The sedimentary rocks are cut by near vertical 1 to 5 m wide quartz-feldspar porphyry dacite to rhyolite dykes. Moderately dipping, graphitic NE to SE trending faults cut the Bowser Lake Group rocks along Tommy Jack Creek.

Most of the Bowser Lake Group rocks on the property have been subjected to weak to moderate Fe-carbonate and sericite/clay alteration. Quartz-carbonate veins without sulphide minerals are common throughout the property, with Ag+/-Au mineralization associated with the presence of sulphides, which occur within veins locally. At least three type of veins occur within the property: (1) barren, 1 mm to 10 cm wide calcite +/- gypsum and rare quartz veins, (2) massive, 1 mm to 20 cm wide quartz-calcite-galena-sphalerite-pyrite+/-arsenopyrite+/-tetrahedrite veins, and (3) 5 to 50 cm thick, banded, gold and silver bearing quartz-Fe-carbonate-arsenopyrite-argentite?-sphalerite-galena-tetrahedrite veins. Fe-carbonate-sericite-clay alteration and silicification envelopes the sulphide bearing quartz veins and is most intense at the contacts with the felsic dykes.

Mineralization encountered by drilling appears to show dominantly low-grade (1-2 gpt Ag) silver mineralization with negligible gold grades over wide zones 10-60 m near Tommy Jack Creek. These wide zones consist of sericite/clay altered arenite and siltstone with a widely spaced (10 to 30 cm) stockwork of 1 to 10 mm quartz-carbonate-sulphide (pyrite+/-sphalerite+/-galena+/-arsenopyrite) veins. Approximately 600 m south of Tommy Jack Creek historical Noranda drill holes encountered low-grade Au and Ag mineralization (1-2 gpt Au and 1-30 gpt Ag) over widths of 10-25 m.

6.0 DEPOSIT TYPES

The Tommy Jack prospect does not fall nicely within most epithermal Au-Ag deposits models although it falls within the broad grouping of low-sulphidation epithermal deposit type by White and Hedenquist (1995). It is classified as "Type I05 – Polymetallic Ag-Pb-Zn (+/- Au, Cu) Veins" by the BC Geological Survey and not as an epithermal deposit. This classification includes Pachuca – Real del Monte (Mexico), Silverton District and Creede (Colorado). Both, Pachuca and Creede/Silverton, which are considered Epithermal Vein deposits by the US Geological Survey classification scheme. Corbett (2002) may have a better deposit model that describes the Tommy Jack deposit in his low-sulphidation epithermal deposit sub-division "Carbonate-base metal gold".

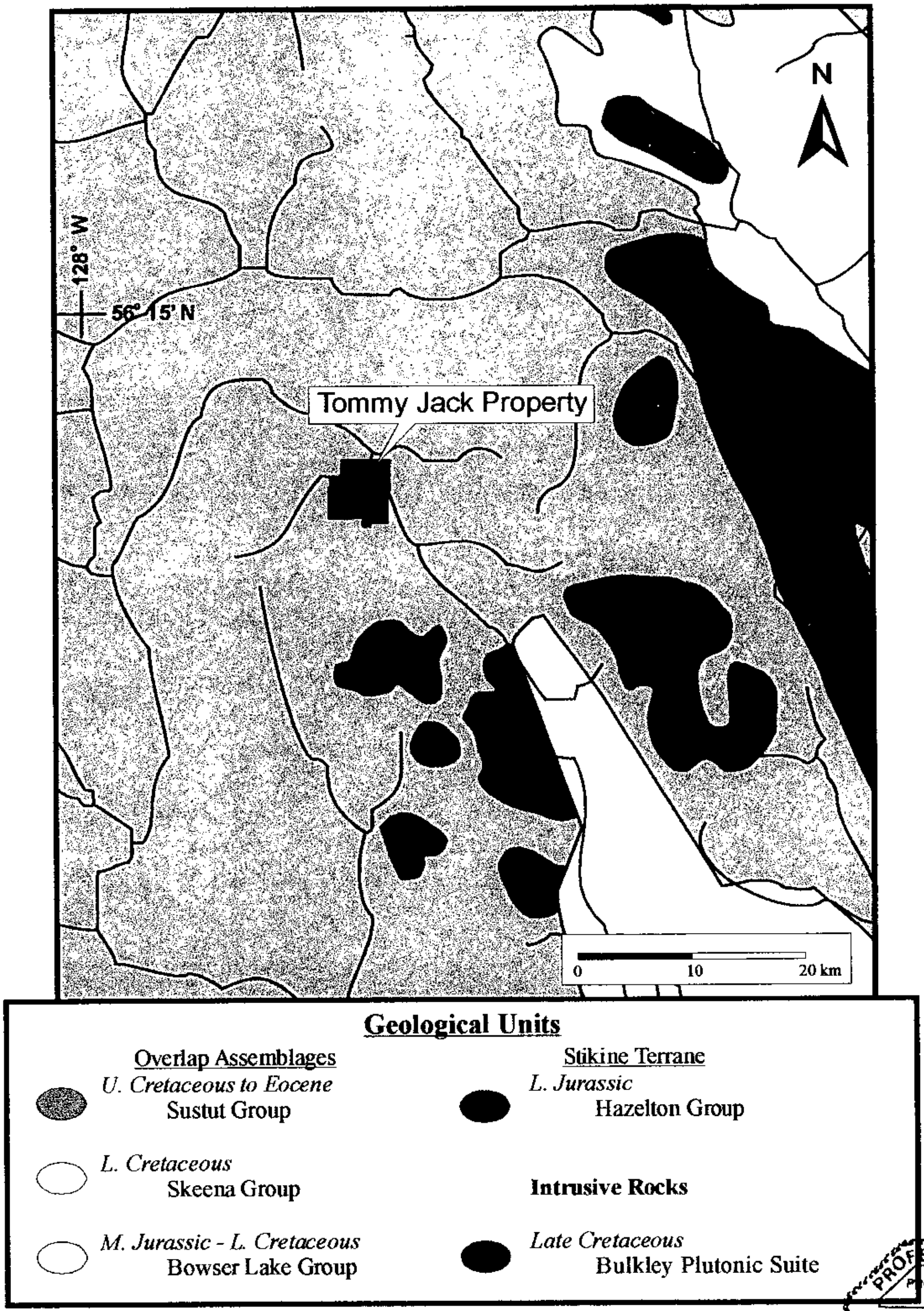

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Figure 3: Regional geology surrounding the Tommy Jack Property *(after Wheeler and McFeely, 1991).*

The "Carbonate-base metal gold" model described by Corbett (2002) is typified by chlorite-sericite to illite-smectite alteration, carbonate-quartz-pyrite-sphalerite-galena-chalcopyrite veins, breccias or fractures, gold and silver mineralization, and disseminated or fissure vein deposits. Tommy Jack contains similar gangue minerals and proportions of gangue minerals and is a disseminated fracture vein system with clay to sericite alteration.

7.0 MINERALIZATION

The main surface exposure of gold-silver mineralization occurs in the banks of Tommy Jack Creek below an area used as a camp by Noranda and Canex during their work programmes. This exposure extends for approximately 135 m N-S along the creek, and the veins strike 135 and dip 30-35 degrees to the southwest. A true thickness for the zone is roughly calculated to be 40 to 55 m however the extents along strike and to depth is unknown. Ten 1 m chip samples collected across this zone, perpendicular to the attitude of the zone averaged 1.1 gpt Au, 276 gpt Ag, 0.1% Cu, 0.8 % Pb and 1.6 % Zn. Grab samples from the Camp Showing range from 0.02 to 10.56 gpt gold and 10.9 to 1824.7 gpt Ag. Of the eleven grab samples taken six returned > 1gpt gold and five samples >100 gpt silver.

Fe-carbonate/clay altered arenite, silicified arenite and siltstone, quartz filled breccia with soft clay altered arenite fragments, and banded sulphide and gold bearing quartz veins typify the rocks in the Camp Showing. Veins are 5 to 50 cm wide and are comprised of banded quartz-Fe-carbonate-arsenopyrite-argentite?-sphalerite-galena-tetrahedrite. These veins generally return assay values between 1.13 and 10.56 gpt gold. The Camp Showing and Bowser Lake Group rocks elsewhere along Tommy Jack Creek are cut by numerous steep to moderately dipping dip-slip faults. The relationship between the faults and the timing of quartz vein generation is uncertain.

Drilling by Noranda failed to intersect the banded veins observed in the Camp Showing, as the nearest holes were collared more than ½ km to the south (Figure 4). However, several zones of disseminated low-grade gold and silver mineralized zones and local high-grade veins were encountered by these holes. Generally, the most impressive gold and silver values in the drill holes come from quartz-galena-sphalerite-pyrite veins, which are usually 1 to 3 metres from the contact of a felsic dyke or locally within the chilled margins of the dyke. Intertech Minerals reported the following as the "best drill intersections" from the Noranda drilling:

Drill Hole	Width	Gold		Silver	
	metres	gpt	opt	gpt	opt
86-5	6.6	4.3	0.125	83.6	2.43
87-14	0.6	31.05	0.3	129.0	3.76
87-23	1.3	14.69	0.42	36.3	1.06

It is important to note that Noranda sampled about 16.5% of the core that they drilled and representative sampling of the un-split core, by Kodiak, revealed interesting results

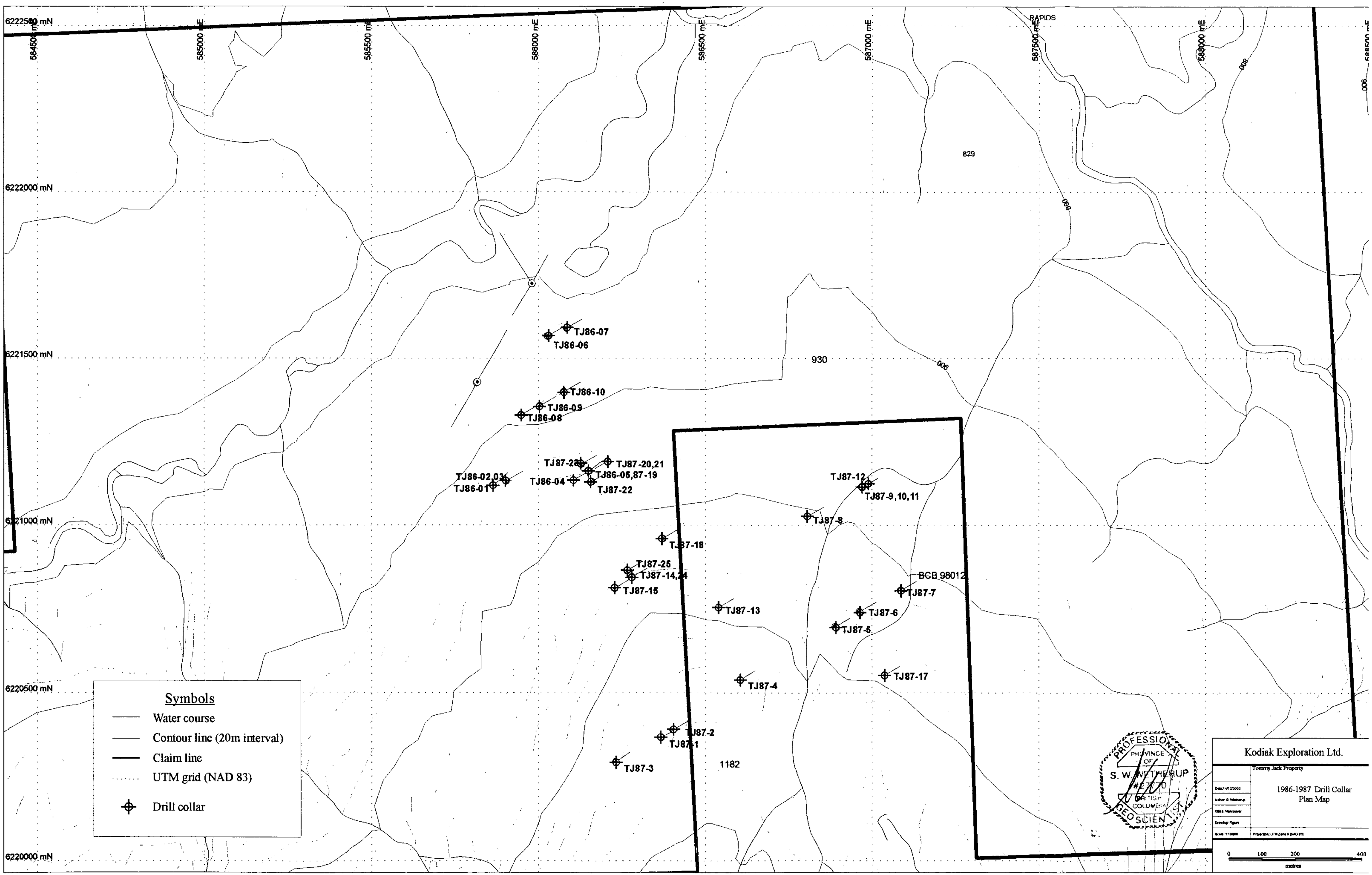

Figure 4: 1986-1987 Noranda drill collar plan.

including a 38.3 gpt Au over 0.2 m sample from hole 87-14. This 38.3 gpt Au sample was approximately 25 m below the interval reported by Intertech Minerals in hole 87-14 (above).

8.0 EXPLORATION AND RESULTS

Fieldwork occurred during July 1 to 18, 2003 and August 15 to September 5, 2003. The programme was conceived, supervised, and conducted by the author on behalf of Kodiak Exploration Ltd. The first phase of fieldwork consisted of sampling the remaining Noranda drill core, prospecting, line-cutting, and 10 km of induced polarization surveying. Approximately 1000 m of drilling and 10 more km of IP surveying constituted the second phase of work during the 2003 field season.

8.1 Prospecting

Outcrop is very limited on the property and is generally found along the creek gullies and along Tommy Jack Creek, which hampered the prospecting significantly. Prospecting on the property in 2003 concentrated on looking for strike extents of the Camp Showing and looking for other mineralized zones along Tommy Jack Creek.

The Camp Showing was originally reported to only exist on the south side of Tommy Jack Creek but in 2003 prospecting demonstrated that the mineralized system continues north of the creek (Figure 5), except that the veins contain more silver and lower gold values than at the Camp Showing. Also, several float boulders were found in Beaver and Unnamed Creeks, which were gold and silver mineralized suggesting possible extensions or separate mineralized zones not previously discovered (Figure 5; Appendix II; assay certificates in Appendix VII).

8.2 Sampling Noranda Drill Core

Approximately half of the drill core was present at the storage site with all of the holes represented by at least one box of core. Samples were taken from sections that were not sampled previously and from zones in which their meterage and hole number were still clearly marked. The highest gold fire assays were 0.45 gpt over 1.2 m and 0.45 gpt over 1.5 m and the highest silver assay 17.4 gpt over 1.1 m. Of the 144 samples taken seventeen retuned highly anomalous gold values >/=0.2 gpt and 50 samples >/=1 gpt silver (Appendix III; assay certificates in Appendix VII).

8.3 Induced Polarization Geophysical Surveying

Over 20 line kilometers of IP surveying were completed on the Tommy Jack Property (Figure 6). From this survey, a large high chargeability anomaly was discovered extending north and south from the camp showing and appears to be offset by several faults (see Appendix IV for a complete report of the results).

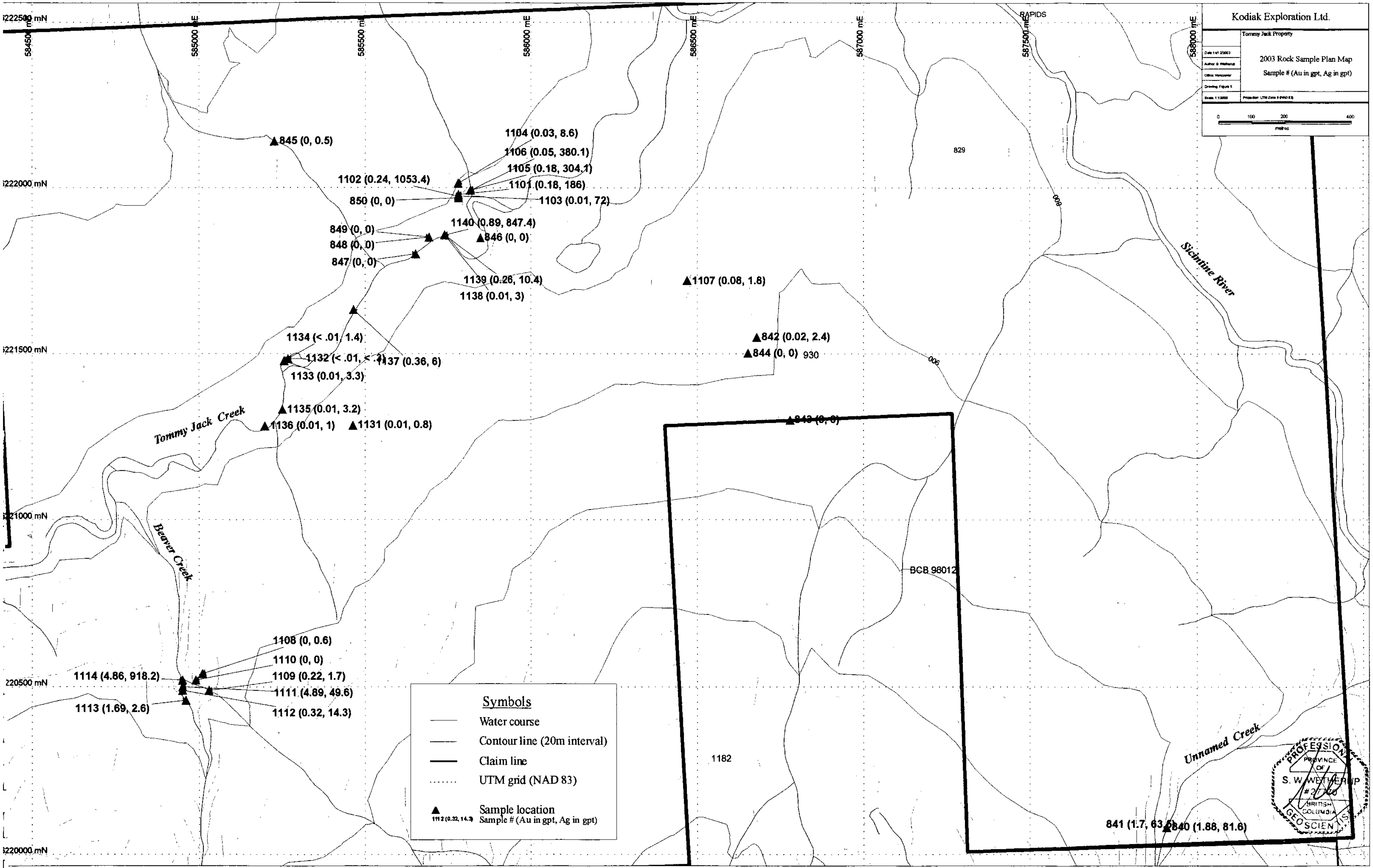

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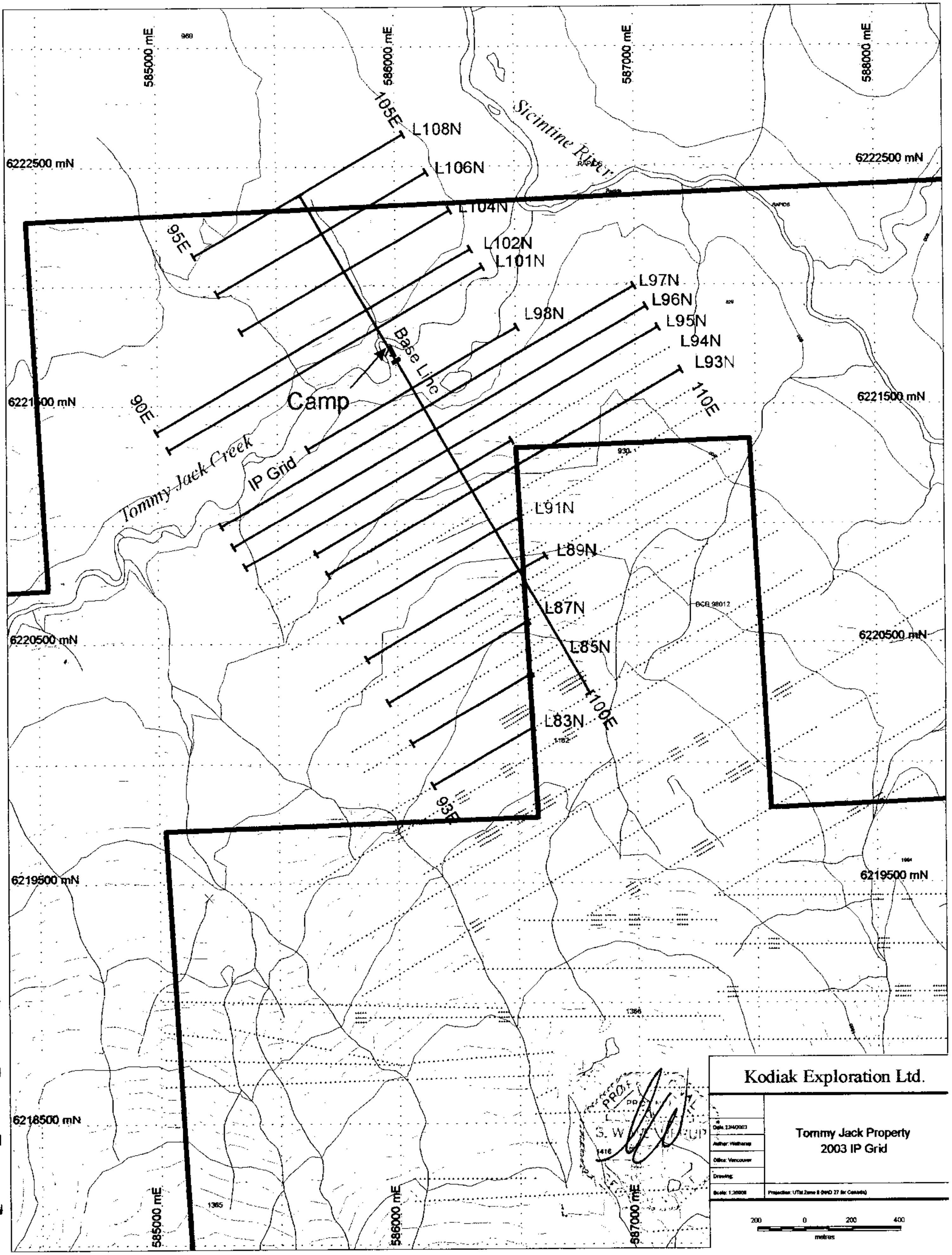
Figure 5: Prospecting grab sample plan.



Kodiak Exploration Ltd.

Tommy Jack Property
2003 IP Grid

Date: 22/4/2003
Author: Wetherup
Office: Vancouver
Drawing:
Scale: 1:20000
Projection: UTM Zone 9 (NAD 27 for Canada)

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8.4 Diamond Drilling

Five diamond drill holes totalling 1035.9 m tested the Camp Showing to depth, possible strike extents southeast and southwest of the Camp Showing, and the northernmost chargeability high (Figure 7). Below is a summary of the results and a complete drill log is in Appendix V, drill sections in Appendix VI, and assay certificates in Appendix VII.

Table 3: Summary highlights from 2003 drilling.

DDH#	From (m)	To (m)	Length	Au (gpt)	Ag (gpt)	Comments
TJ03-01	109.5	136.0	**26.5 m**	**0.11**	**14.3**	
TJ03-02	43.1	66.0	**22.9 m**	**0.32**	**40.1**	incl. 3.9 m of 0.49 gpt Au and 129.7 gpt Ag
TJ03-02	123.0	145.3	**22.3 m**	**0.10**	**50.4**	incl. 0.3 m of 2.6 gpt Au and 2321.5 gpt Ag
TJ03-02	210.0	241.4	**31.4 m**	**0.04**	**8.4**	incl. 10.0 m of 15.9 gpt Ag
TJ03-03	24.0	34.2	**10.2 m**	**2.04**	**138.5**	incl. 1.8 m of 9.38 gpt Au and 580.3 gpt Ag
TJ03-04	156.5	160.8	**4.3 m**	**1.07**	**4.8**	
TJ03-05	107.0	108.1	**1.1 m**	**2.76**	**21.9**	
TJ03-05	68.0	69.2	**1.2 m**	**0.93**	**31.7**	

Quartz-sulphide veins in the Camp Showing are oriented ~135 and dip moderately southwest. TJ03-01 was drilled to intersect possible strike and down-dip mineralization extensions from the Camp Showing and cut 26.5 m of weak gold and silver mineralization (Table 2). Most of the rock in TJ03-01 is arenite with lesser amounts of interbedded siltstone and minor coal, which is weakly to moderately clay/carbonate altered and contains many 1 to 10 mm carbonate+/-quartz veins. Vein mineralogy changes in the hole from carbonate+/-gypsum at the top of the hole and changing to quartz-carbonate near the bottom with local zones with quartz-carbonate-sulphide (pyrite-galena-sphalerite-arsenopyrite-chalcopyrite) veins. Three nearly orthogonal vein sets occur in TJ03-01 at 70°, 20° and 45° to the core axis. Of these veins the 70° set are planar and the most dominant, with the 20° set parallel to and within shears/faults and the 45° set occurring as tension gashes or wispy veins that terminate at veins oriented at 70° to the core axis.

Hole TJ03-02 was collared at the same location as the TJ03-01 collar and went directly below the Camp Showing. It encountered several silver with minor gold mineralized zones and contains three orthogonal vein sets much like hole TJ03-01. In hole TJ03-02, the most dominant quartz-carbonate+/-sulphide vein set are planar and 20-30° to the core axis and are mineralized. A 50-70° to core axis vein set is also mineralized but are less frequent, wispy, and parallel to a tensional joint set. The third vein set is parallel to the core axis, are locally mineralized and occur within shears/faults.

Figure 7: 2003 Drill collar and drill trace plan with chargeability contour map.

The highest gold and silver grades of the 2003 drilling programme were encountered at the top of hole TJ03-03. The third hole drilled was collared in the same location as holes TJ03-01 and TJ03-02 but was drilled to the southwest to intersect the northernmost chargeability high. Again, there are three orthogonal carbonate+/-quartz+/-sulphide vein sets, a mineralized sub-parallel to 20° to core axis set, a wispy, tensional, 60-80° to core axis set, and a 35-45° to core axis set, which are commonly within shear zones. Within the mineralized zone at the top of the hole the widest quartz-carbonate-pyrite-sphalerite-galena veins are 0-20° to the core axis and occur with many 1 mm to 10 mm 70-80° veins. This mineralized zone occurs adjacent to a dacite dyke. Below the mineralized zone the vein mineralogy is dominated by carbonate with lesser amounts of quartz and rare sulphide minerals.

Hole TJ03-04 was drilled north-northeast into the northern chargeability high. It intersected 1-5%, 1-10 mm quartz-carbonate-sulphide veins and weak Ag mineralization (>1 gpt Ag over >60 m) throughout most of the hole. The sulphide content of the rock explains the chargeability anomaly. Vein sets are at 80°, 30-45° (parallel to shear zones), and sub-parallel to core axis, with the 80° vein set being the most common and the sub-parallel veins occurring as tensional veins between the 80° veins. Red sphalerite, galena, and pyrite are common throughout and occur in all vein sets.

From the same drill pad hole TJ03-05 as drilled 180° from hole TJ03-04 to the south-southwest. Vein concentration is less in TJ03-05 than in TJ03-04 and carbonate-quartz+/-sulphide veins occur near parallel, 45°,and 80° to the core axis. Most shear zones are sub-parallel to 45° to the core axis including a broken and fault gouge zone between 75.3 to 92.0 m.

9.0 SAMPLING METHODS

Prospecting samples were given unique five digit sample numbers that were recorded in field books and on the sample bag before sealing it. Grab samples were collected, given a sample number, placed in a plastic sample bag, and sealed. Also, a hand sample was collected, a GPS coordinate taken (using a Garmin XL 12 hand held GPS) and a brief geological description of the sample was recorded into a field notebook.

Drill core was measured and logged for rock type, vein orientation, and mineralogy. Sample intervals were marked, measured, given a unique sample number, and their locations (i.e. hole number and meterage/footage) were recorded along with a short geological description. These intervals were then split using a core splitter, with half of the core placed back into the core box and half into a plastic sample bag. Core was logged and is stored on the TJ03-01,02,03 drill site.

10.0 SAMPLE PREPARATION, ANALYSES AND SECURITY

All samples were transported by helicopter to base camp, packed into the field vehicle, and delivered to Acme Laboratories, in Vancouver by Canadian Freightways and Greyhound.

Acme Analytical Laboratories is located at 852 East Hastings Street, Vancouver, BC and is an ISO 9002 accredited analytical laboratory. Acme conducted all of the analytical work on the samples including the crushing and splitting. Kodiak requested that all samples be analyzed for 36 elements by ICP-MS using an aqua-regia digestion and fire assay for Au and Ag.

Sample preparation for the ICP-MS method constituted crushing up to 4 kg of sample to –10 mesh (70%), followed by splitting to a 250 g aliquot that was then pulverized to –150 mesh (95%). From there the 250 g aliquot was split to a 30 g aliquot, subjected to an aqua-regia digestion and then analyzed by an Inductively Coupled Plasma Mass Spectrometer (ICP-MS) apparatus for 36 elements. Also, a classical, lead collection, fire assay was performed on 29.2 g of sample pulp and the dore bead analyzed by ICP-ES for Au and Ag.

11.0 DATA VERIFICATION

Verification of the data has relied upon ISO 9002 certified Acme Analytical Laboratories' data verification procedures. Acme Labs verifies data in three ways, by running (1) blanks to test for carry-over affects, (2) duplicates to test for precision, and (3) standards which are cross checked at other laboratories to ensure accuracy. The author received the data directly from the laboratory and any inaccuracies with the data would be due to unforeseen problems at the lab.

The 2003 fieldwork programme was small and running a cross-laboratory check is not justified, especially as Acme Analytical Laboratories runs regular cross-laboratory checks of its own.

12.0 INTERPRETATION AND CONCLUSIONS

12.1 Summary of 2003 Fieldwork

Fieldwork in 2003 consisted mainly of 20 line kilometers of induced polarization geophysical surveying and approximately 1000m of diamond drilling. The IP survey delineated a NW trending, 2.1 km long and 100 to 300 m wide high chargeability anomaly, which appears to be offset into three sections by two or more east trending fault structures. This chargeability anomaly coincides with many of the gold and silver mineralized drill intersections by the Noranda drill programmes in 1987 and 1986.

Diamond drilling in 2003 was initiated to test the main showing on Tommy Jack Creek to depth and along strike and to test the northernmost section of the high chargeability anomaly mentioned above. Geochemical analyses of the drill core by Acme Analytical Laboratories using standard fire assay methods showed many zones of low (1 to 5 gpt) to moderate (5 to 100 gpt) silver mineralization and nine gold assays greater than 1 gpt.

12.2 Geological Interpretation

Ag-Au (Zn-Pb-Cu) mineralization and Fe-carbonate-sericite+/-chlorite+/-clay alteration on the Tommy Jack Property best approximates the Low-Sulphidation Epithermal Au-Ag deposit model. The low-sulphidation model encompasses a broad spectrum of alteration mineral and metal assemblages and has subsequently been subdivided. Corbett (2002) describes many low-sulphidation sub-types, of which his "Carbonate-base metal gold" mineralization model bears a strong resemblance to Tommy Jack. This deposit type includes deposits such as Porgera, Hidden Valley, Kermenge, Kelian, and Mt Leyshon.

The Carbonate-base metal gold deposit model suggests that the silver dominated mineralization, gangue mineral and alteration mineral assemblages observed in the 2003 Kodiak drill programme were deposited at higher crustal levels than the gold-silver mineralization encountered by the Noranda drill holes to the south. Hence, the northernmost chargeability anomaly is probably too high in the system to deposit gold and explains why the Noranda drill holes to the south have more gold.

The central and southernmost chargeability highs are over 1 km in strike length and have been tested directly or along its periphery by several Noranda drill holes, which returned significant Ag-Au mineralized intersections.

13.0 RECOMMENDATIONS

Previous soil surveys produced Au-Ag anomalies that coincide with the chargeability high discovered in the 2003 programme. These soil anomalies extend beyond the scope of the IP survey and suggest there may be more zones yet to be tested by drilling. Hence, increasing the area of the IP survey to the south and west is suggested to investigate the possibility of more mineralized zones existing beyond the area of historical work.

Previous workers appeared to be focus on the high-grade Au-Ag intersections and ignored the low-grade bulk tonnage potential of the Tommy Jack Property. Attempts by Noranda to reproduce high-grade assays with closely spaced drilling were mostly unsuccessful, which indicates that these zones are probably small and discontinuous making them difficult exploration targets. However, low-grade zones are a much better target as they are 10-25 m wide, tabular, and appears to be detectable by induced polarization surveys.

From the alteration and mineralization observed on the Tommy Jack Property, it appears to be a Low-Sulphidation Carbonate-base metal gold prospect. Drilling, thus far, has shown that the central and southernmost chargeability highs correspond to wide zones (9-25 m) of low-grade gold-silver mineralization. Furthermore, Carbonate-base metal gold deposits tend to be large low-grade deposits (eg. Porgera ~58 Mt @ 3.5 gpt, Place Dome website, 2003; http://www.placerdome.com/operations/porgera/porgera.html) with up to 1 km in vertical extent and therefore further drilling is required on Tommy Jack to test the strike extents of the chargeability anomaly and to test the mineralization to depth.

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Statement of Qualifications

I, Stephen William Wetherup of 635 East 45th Avenue, Vancouver, British Columbia, certify that:

1. I am a graduate of the University of Manitoba with a BSc. Honours in Geology, in 1995,
2. I have practiced my profession as an mineral exploration geologist with Fox Geological Services, Phelps Dodge Corp. of Canada and as a geological consultant, for 5 years,
3. I have been operating a business as a geological consultant under my own name since June, 2001,
4. I am a member of the Society of Economic Geologists, Geological Association of Canada, and the Vancouver Mining Exploration Group,
5. I am a Professional Geoscientist registered with the Association of Professional Geoscientists and Engineers of British Columbia,
6. I last visited the Tommy Jack Property between ~~July~~ Aug 23 and ~~July 28~~ Sept 5, 2003,
7. I am the author of this report,
8. I am not aware of any material facts or change in facts at the time this certification is dated.
9. I have no monetary interest in the property nor do I own or expect to receive interest in the company who is currently operating on the property,
10. I have had no previous involvement with the Tommy Jack Property,
11. I have read the TSX Venture Exchange policy documents, National Instrument 43-101, Companion Policy 43-101CP, and Form 43-101F1.

S. W. WETHERUP

Stephen William Wetherup,
BSc., P.Geo.

Vancouver, British Columbia
Dated this 20 day of
December, 2003

APPENDIX I

2003 Field Expenses

Tommy Jack Property
2003 Project Expenses
Appendix I

Expense Item	Vendor	Units	Rate	Amount	Totals
Field Labour					
Geologist	Stephen Wetherup	38.75 days	$321/day	$ 12,438.75	
Cook	Dorrie Williams	34 days	$330/day	$ 10,890.00	
First Aid attendant	Dorrie Williams	34 days	$33/day	$ 1,089.00	
Labourer	Sam Raymond	17 days	$236.50/day	$ 3,547.50	
Linecutter	Sam Watling	20 days	$330/day	$ 6,600.00	
Carpenter	John Anderson	3 days	$330/day	$ 990.00	
Linecutter	Graham Scammells	17 days	$330/day	$ 5,610.00	
Linecutter	Barney Middleton	17 days	$330/day	$ 5,610.00	
Linecutter	Jerry Mencl	6 days	$330/day	$ 1,980.00	
Prospector	Lorne Warren	9 days	$423.50/day	$ 3,811.50	
Labourer	Bill Garner	3 days	$250/day	$ 825.00	
Labourer	Dennis Symington	20 days	$200/day	$ 4,000.00	
Labourer	Jason Chornobay	34 days	$200/day	$ 6,800.00	
Labourer	Linda Wetherup	19 days	$165/day	$ 3,135.00	
Labourer	Mark Henley	15 days	$200/day	$ 3,000.00	
					$ 70,326.75
Accomodations and Board					
Acc and Board	CJL Enterprises	307 mandays	$65/manday	$ 19,955.00	
Transportation of food to camp	CJL Enterprises	2 days	$ 265/day	$ 530.00	
Acc and board	Expenses			$ 3,304.28	
					$ 23,789.28
Contractors					
Camp Set up	CJL Enterprises			$ 7,302.16	
Geophysical Surveying	Scott Geophysics			$ 4,000.00	
Geophysical Surveying	Scott Geophysics			$ 13,029.59	
Geophysical Surveying	Scott Geophysics			$ 1,792.25	
Geophysical Surveying	Scott Geophysics			$ 11,751.28	
Geophysical Surveying	Scott Geophysics			$ 4,000.00	
Diamond Drilling	Britton Bros.			$ 67,068.35	
					$ 101,641.47
Geochemical Assaying					
Assays	Acme Labs	9 Core		$ 319.28	
Assays	Acme Labs	23 Rock		$ 638.82	
Assays	Acme Labs	135 Core		$ 3,794.07	
Assays	Acme Labs	295 Core		$ 7,641.16	
Assays	Acme Labs	186 Core		$ 4,786.00	
Assays	Acme Labs	17 Rocks		$ 425.53	
					$ 17,604.86
Transportation					
Helicopter	Interior Helicopters			$ 23,774.42	
Helicopter	Highland Helicopters	25.7 hrs		$ 25,622.14	
Helicopter fuel	Highland Helicopters			$ 1,914.07	
Truck Rental	CJL Enterprises			$ 4,919.97	
Plane Fare	Air Canada			$ 503.50	

Truck Rental	Stephen Wetherup	5 days	$80.25/day	$	401.25		
Truck Rental	Stephen Wetherup	18 days	$80.25/day	$	1,444.50		
Truck Rental	Stephen Wetherup	21 days	$80.25/day	$	1,685.25		
Fuel	Stephen Wetherup			$	1,905.01		
						$	**56,734.09**
Miscellaneous							
Rock cutting	Vancouver Petrographics			$	138.61		
Shipping Rocks	Greyhound			$	43.78		
Equipment rental	CJL Enterprises			$	4,807.00		
Satellite Phone	CJL Enterprises			$	2,266.14		
Satellite Phone	Global Star			$	121.32		
Satellite Phone	Global star			$	487.27		
Satellite Phone	Global star			$	1,206.60		
Data Entry	Bart Jaworski			$	775.75		
Data Compilation	Stephen Wetherup			$	4,092.75		
Field Preparation	Stephen Wetherup			$	802.50		
Report Writing and Data Entry	Stephen Wetherup			$	7,043.81		
Miscellaneous Expenses	Stephen Wetherup			$	3,993.60		
						$	**21,785.53**

Total Expenses for 2003 **$** **291,881.98**

APPENDIX II

Prospecting Sample Descriptions and Selected Element Assays

Tommy Jack Property

Prospecting Sample Summary Descriptions and Selected Elements

Appendix II

ample No.	Date	Sample Type	Material	Colour	Easting	Northing	Zone	Datum	Comments	Cu (ppm)	Pb (ppm)	Zn (ppm)	Mn (ppm)	As (ppm)	Sb (ppm)	Bi (ppm)	Mg (%)	W (ppm)	Hg (ppm)	Ag (gpt)*	Au (gpt)*	Method
840	7/5/03	Rock	Float, Talus	red	587910	6220080	9V	Nad 83	Qtz-py boulder	690.1	182.8	4892	13	3845.1	55	70.4	0	3.3	0.28	**81.6**	**1.88**	ICP-MS/AR
841	7/5/03	Rock	Bedrock	orange	587910	6220080	9V	Nad 83	3-4 cm qtz-py-cabonate vein	789.5	149.7	99	1025	199.5	29.3	62.3	0.03	0.1	0.04	**63.5**	**1.7**	ICP-MS/AR
842	7/6/03	Rock	Bedrock	orange	586680	6221550	9V	Nad 83	Arenite with qtz veining	50.7	10.2	144	489	35.1	0.9	1.7	0.45	5.9	0	**2.4**	**0.02**	ICP-MS/AR
843	7/6/03	Rock	Bedrock	orange	586780	6221300	9V	Nad 83	Clay altered siltstone with 1-5% carbonate veins	13.9	7.9	23	1634	34.9	0.7	0.4	0.33	0.3	0	**0**	**0**	ICP-MS/AR
844	7/6/03	Rock	Float	green, white	586654	6221502	9V	Nad 83	Arenite with 25% qtz-carbonate+/- py vein and stockwork	16.9	3.9	38	690	8.8	0.3	0.1	1.08	3.8	0	**0**	**0**	ICP-MS/AR
845	7/7/03	Rock	Bedrock	orange	585226	6222140	9V	Nad 83	Arenite with abundant carbonate-qtz veins	18.4	9.8	56	1401	23.1	3.6	0.1	0.88	0.6	0.05	**0.5**	**0**	ICP-MS/AR
846	7/9/03	Rock	Bedrock	brown	585846	6221849	9V	Nad 83	Brown siltstone with 1% carbonate veins	62.3	7.6	93	659	2.5	0.1	0.1	0.89	0.3	0	**0**	**0**	ICP-MS/AR
847	7/9/03	Rock	Float	orange	585652	6221800	9V	Nad 83	Fe-carbonate breccia with shale fragments	14.9	2.9	39	2891	23.6	1.4	0	2.7	0.3	0	**0**	**0**	ICP-MS/AR
848	7/9/03	Rock	Bedrock	grey	585692	6221851	9V	Nad 83	Altered arenite with trace to 1% py	40.7	7.2	90	1078	2.6	0.1	0.1	2.03	0.3	0	**0**	**0**	ICP-MS/AR
849	7/9/03	Rock	Bedrock	white	585692	6221851	9V	Nad 83	Bedding parallel carbonate vein with trace py and cpy	26.3	3.4	27	1615	3.9	0.1	0	0.85	0.1	0	**0**	**0**	ICP-MS/AR
850	7/9/03	Rock	Talus	orange	585780	6221970	9V	Nad 83	Altered arenite with ~ 5% carbonate veining	48.7	9.3	27	483	30.3	2.7	0.1	0.66	0.5	0	**0**	**0**	ICP-MS/AR
1101	7/9/03	Rock	Bedrock	red	585780	6221980	9V	Nad 83	Fault zone with qtz-carbonate-gal-sph-cpy vein	477.6	1364.4	304	486	25.8	77.3	0.1	0.59	5.4	0.31	**186**	**0.18**	ICP-MS/AR
1102	7/9/03	Rock	Bedrock	grey	585780	6221975	9V	Nad 83	Fault zone with qtz-carbonate-gal-sph-cpy vein	2435.6	10000	40958	808	59.5	995.9	0.1	0.29	29.3	62.23	**1053.4**	**0.24**	ICP-MS/AR
1103	7/9/03	Rock	Bedrock	brown, orange	585780	6221975	9V	Nad 83	Qtz-carbonate-gal-sph-cpy breccia	179.8	1916.7	8579	1487	14	76.5	0.1	1.1	>200	32.5	**72**	**0.01**	ICP-MS/AR
1104	7/9/03	Rock	Bedrock	brown, orange	585779	6222014	9V	Nad 83	Arenite and siltstone with Fe-carbonate veins	54.4	33.9	164	1376	18.9	3.8	0	0.98	3	0.15	**8.6**	**0.03**	ICP-MS/AR
1105	7/9/03	Rock	Talus	orange	585816	6221993	9V	Nad 83	Fe-carbonate-calcite-cpy-sph-tetrahedrite vein within a clay altered arenite	16121	281.5	202	3721	542.9	255.1	0.8	2.39	1.7	0.13	**304.1**	**0.18**	ICP-MS/AR
1106	7/9/03	Rock	Talus	orange	585816	6221993	9V	Nad 83	Angular qtz-Fe-carbonate cobble	5070.9	10000	6576	3340	152.7	287.3	1.2	2.2	1.7	0.81	**380.1**	**0.05**	ICP-MS/AR
1107	7/10/03	Rock	Float	white	586470	6221720	9V	Nad 83	Angular qtz-Fe-carbonate cobble	41.6	113.3	40	342	8.4	2.8	0	0.04	6.4	0.02	**1.8**	**0.08**	ICP-MS/AR
1108	7/11/03	Rock	Float	orange	585010	6220540	9V	Nad 83	Siltstone cobble with a 4 cm wide calcite-Fe-carbonate-qtz vein	10.5	2.1	113	2727	2.1	0.1	0.1	3.71	0.5	0.04	**0.6**	**0**	ICP-MS/AR
1109	7/11/03	Rock	Float	white	585030	6220490	9V	Nad 83	Qtz vein cobble	11.2	86.2	13	325	340.6	1.6	0.1	0.02	150.4	0.01	**1.7**	**0.22**	ICP-MS/AR
1110	7/11/03	Rock	Float	grey	584990	6220520	9V	Nad 83	Siltstone with 10-15% qtz-Fe-carbonate stockwork and veins	6.7	2.9	11	341	4.6	2.1	0.1	0.07	6	0	**0**	**0**	ICP-MS/AR
1111	7/11/03	Rock	Float	red, white	584950	6220500	9V	Nad 83	Rusty qtz rounded cobble	166.3	10000	6512	30	1402.3	112.7	4.4	0	6.6	4.25	**49.6**	**4.89**	ICP-MS/AR
1112	7/11/03	Rock	Float	orange	584950	6220490	9V	Nad 83	Carbonate altered arentie with a 1cm wide qtz-py-gal-Fe-carbonate vein	140.3	5765.7	8657	6795	156.2	16	0.2	1.43	>200	1.6	**14.3**	**0.32**	ICP-MS/AR
1113	7/11/03	Rock	Float	white	584960	6220460	9V	Nad 83	Qtz breccia with fragments of siltstone	5.5	64.1	82	516	46.3	0.7	0	0.1	11	0.04	**2.6**	**1.69**	ICP-MS/AR
1114	7/11/03	Rock	Float	white	584950	6220520	9V	Nad 83	Qtz-py-gal-sph vein with graphite	1458.9	10000	63490	102	7948.3	1175.5	0	0.01	4.3	21.59	**918.2**	**4.86**	ICP-MS/AR
1131	8/20/03	Rock	Talus	orange	585464	6221284	9V	Nad 83	Fe-carbonate-calcite+/-sph vein within a fault zone.	32	9	30	1961	7	< 3	< 3	0.66	< 2		**0.8**	**0.01**	ICP/AR
1132	8/20/03	Rock	Bedrock	orange	585267	6221485	9V	Nad 83	Carbonate altered dacite with few Fe-carbonate+/-calcite+/-qtz+/- py veinlets	3	3	49	740	13	< 3	< 3	0.63	< 2		**< .3**	**< .01**	ICP/AR
1133	8/20/03	Rock	Bedrock	orange	585255	6221478	9V	Nad 83	Calcite-Fe-carbonate-qtz veins within a sheared dacite dyke	37	5	45	1479	3	13	< 3	3.27	< 2		**3.3**	**0.01**	ICP/AR

1134	8/20/03	Rock	Bedrock	orange	585255	6221479	9V	Nad 83	Argillic alteration of dacite/adesite dyke.	337	< 3	42	1439	2	8	< 3	3.06	< 2		**1.4**	< .01	ICP/AR
1135	8/20/03	Rock	Float	orange	585250	6221332	9V	Nad 83	Carbonate and brecciated arenite with 50-60% cal+Fe-carbonate material.	16	4	24	2566	8	4	< 3	2.9	< 2		**3.2**	**0.01**	ICP/AR
1136	8/20/03	Rock	Bedrock	orange	585198	6221282	9V	Nad 83	A fault zone with abundant cal-Fe-carbonate+/-qtz+/-cpy veins	33	3	59	2003	9	4	< 3	0.64	< 2		**1**	**0.01**	ICP/AR
1137	8/20/03	Rock	Bedrock	Red	585466	6221632	9V	Nad 83	Two small fault zones with 2-5cm of qtz-cb-py-sph veining within them; ft 162/40, ft 168/66	7	17	30	197	50	29	< 3	0.17	< 2		**6**	**0.36**	ICP/AR
1138	8/20/03	Rock	Bedrock	orange	585739	6221858	9V	Nad 83	Altereed arenite with calcite/Fe-carbonate +/- pyrite and galena	25	19	44	2575	15	6	< 3	2.39	2		**3**	**0.01**	ICP/AR
1139	8/20/03	Rock	Bedrock	white	585739	6221858	9V	Nad 83	Qtz-bx vein with trace to 10% pyrite within a siltstone	86	240	5027	3132	236	6	< 3	0.54	< 2		**10.4**	**0.26**	ICP/AR
1140	8/20/03	Rock	Bedrock	white	585739	6221858	9V	Nad 83	Qtz-gal-py-sph-tet+/-apy vein in arenite	436	>9999	7025	378	>9999	632	< 3	0.11	2		**847.4**	**0.89**	ICP/AR

APPENDIX III

Noranda Drill Core Sample Descriptions
and
Selected Assay Results

Tommy Jack Property

Summary and Selected Elements from Sampling Un-split Noranda Drill Core

Appendix III

Analyses from Acme Analytical Laboratories analyzed by ICP (* Au and Ag analyzed by fire assay)

Drill Hole	Easting	Northing	Zone	From (m)	To (m)	Sample No.	Cu (ppm)	Pb (ppm)	Zn (ppm)	As (ppm)	Sb (ppm)	Bi (ppm)	Hg (ppm)	Ag (gpt)*	Au (gpt)*
87-14	586278	6220845	9V	4.0	5.5	C 158001	92.4	11.5	99	293.8	0.7	0.1	0.02	1.4	0.14
87-14	586278	6220845	9V	5.5	7.0	C 158002	67.7	6.6	73	54.6	0.3	0.1	0	0	0.01
87-14	586278	6220845	9V	7.0	8.5	C 158003	73.1	103.9	152	187.6	0.5	0.1	0.02	0.8	0.05
87-14	586278	6220845	9V	8.5	10.1	C 158004	74.7	43	104	214.3	0.4	0.2	0.03	0.6	0.09
87-14	586278	6220845	9V	10.1	11.6	C 158005	58.5	11.3	83	42.3	0.4	0.1	0.01	0.6	0.01
87-14	586278	6220845	9V	11.6	13.1	C 158006	46.5	21.7	41	123.9	1.2	0.1	0.01	1.6	0.06
87-14	586278	6220845	9V	13.1	14.6	C 158007	93.2	124.2	1149	94.3	1	0.1	0.24	1.4	0.1
87-14	586278	6220845	9V	14.6	16.2	C 158008	78.2	303.7	148	338.4	1.6	0.1	0.03	2.3	0.23
87-14	586278	6220845	9V	16.2	17.7	C 158009	62.4	85.4	41	317.4	3.4	0.1	0.01	1.5	0.17
87-14	586278	6220845	9V	35.4	36.0	C 158010	73.7	10.6	37	108.5	0.5	0.1	0	0.4	0.22
87-14	586278	6220845	9V	36.6	38.3	C 158011	79.5	8.2	44	130.9	0.6	0.1	0	0.8	0.14
87-14	586278	6220845	9V	39.0	41.1	C 158012	103.8	27.8	59	225.1	0.8	0.1	0	0.9	0.37
87-14	586278	6220845	9V	46.3	48.2	C 158013	79.5	32.4	97	131.6	0.6	0.1	0.01	0.7	0.21
87-14	586278	6220845	9V	48.2	49.7	C 158014	67.7	11	31	147.9	0.7	0.1	0	0.6	0.06
87-14	586278	6220845	9V	49.7	51.2	C 158015	71.2	9.3	48	81.2	0.5	0.1	0	0	0.03
87-14	586278	6220845	9V	51.2	52.7	C 158016	86.9	15.1	45	113	0.7	0.1	0.01	0.6	0.05
87-14	586278	6220845	9V	52.7	54.3	C 158017	94.2	40.3	58	361.4	0.6	0.1	0	0.9	0.3
87-14	586278	6220845	9V	54.3	55.8	C 158018	57.4	41.3	25	193.8	0.9	0.1	0	0.9	0.1
87-14	586278	6220845	9V	55.8	57.3	C 158019	55.6	16.5	68	77.8	0.5	0.1	0.02	0.5	0.06
87-14	586278	6220845	9V	57.3	59.1	C 158020	51.4	9.5	23	101.3	0.3	0.1	0	0.4	0.02
87-14	586278	6220845	9V	61.6	63.1	C 158021	80.5	71	90	489.6	1.8	0.1	0	2.3	0.22
87-14	586278	6220845	9V	63.1	64.9	C 158022	55.7	6.9	25	82.5	0.5	0.1	0	0.5	0.04
87-14	586278	6220845	9V	64.9	66.4	C 158023	52.5	4.2	27	61.7	0.2	0.1	0	0	0.01
87-14	586278	6220845	9V	66.4	68.0	C 158024	52.4	4.2	24	55.1	0.2	0.1	0	0.3	0.04
87-14	586278	6220845	9V	68.0	68.9	C 158025	55.2	3.3	34	51.8	0.2	0.1	0	0	0
86-01	585862	6221119	9V	6.4	7.3	C 158026	81	38.5	111	91	0.6	0.1	0.02	1	0.02
86-01	585862	6221119	9V	7.6	8.5	C 158027	83.1	13.4	113	47.7	0.3	0.2	0.01	0.9	0.01
86-01	585862	6221119	9V	8.8	10.1	C 158028	90.8	7.5	88	140.4	0.7	0.1	0	1.7	0.02
86-01	585862	6221119	9V	10.4	11.3	C 158029	79.3	8.1	95	41.2	0.7	0.1	0.01	0.9	0.01
86-01	585862	6221119	9V	11.6	13.1	C 158030	67.1	12	83	43.2	0.4	0.1	0	1.1	0.21
86-01	585862	6221119	9V	13.1	14.6	C 158031	62.8	5.4	70	48.8	0.3	0.1	0	0.6	0.02
86-01	585862	6221119	9V	14.6	16.2	C 158032	63.6	5.2	84	56.5	0.3	0.1	0.01	0.9	0.11
86-01	585862	6221119	9V	16.2	17.4	C 158033	42.3	32.8	81	96	0.7	0.1	0.01	1.2	0.03
86-01	585862	6221119	9V	18.0	19.2	C 158034	68.7	80.8	192	58.9	0.8	0.1	0.01	2.8	0.17
86-01	585862	6221119	9V	19.2	20.7	C 158035	52.4	9.9	89	38.1	0.6	0.1	0.01	1	0.02

Tommy Jack Property

Summary and Selected Elements from Sampling Un-split Noranda Drill Core

Appendix III

Analyses from Acme Analytical Laboratories analyzed by ICP (* Au and Ag analyzed by fire assay)

Drill Hole	Easting	Northing	Zone	From (m)	To (m)	Sample No.	Cu (ppm)	Pb (ppm)	Zn (ppm)	As (ppm)	Sb (ppm)	Bi (ppm)	Hg (ppm)	Ag (gpt)*	Au (gpt)*
86-01	585862	6221119	9V	20.7	22.3	C 158036	41.7	14.8	89	36.6	1.2	0	0.01	1.3	0.01
86-01	585862	6221119	9V	22.3	23.8	C 158037	38.7	6.4	76	36.8	0.8	0	0	0.8	0.01
86-01	585862	6221119	9V	26.2	28.2	C 158038	65.1	7.1	89	52.4	0.5	0.1	0	1	0.1
86-02	585903	6221132	9V	3.0	3.7	C 158039	46.7	5.8	91	49.3	0.7	0	0.01	0.8	0
86-02	585903	6221132	9V	6.1	7.0	C 158040	64.2	20.4	60	53.6	1.2	0.1	0.01	1.7	0.01
86-02	585903	6221132	9V	7.0	8.5	C 158041	49.2	10.3	57	58.5	0.4	0.1	0.01	1.4	0.04
86-02	585903	6221132	9V	8.5	10.1	C 158042	2.4	23.1	42	21.2	0.2	0	0	0.8	0.02
86-02	585903	6221132	9V	10.1	11.0	C 158043	18.2	8	50	18.8	0.2	0	0.01	0.9	0.02
86-02	585903	6221132	9V	20.1	22.3	C 158044	65.1	6.8	87	8.5	0.1	0	0.01	0.8	0.01
86-02	585903	6221132	9V	22.3	24.1	C 158045	61.6	4.1	83	14.1	0.2	0	0	0	0.01
86-02	585903	6221132	9V	25.0	26.8	C 158046	57.9	5.2	85	29.9	0.5	0	0	0.7	0
86-02	585903	6221132	9V	26.8	28.3	C 158047	57.1	7.4	74	29.8	0.6	0	0	0.5	0.01
86-02	585903	6221132	9V	28.3	30.8	C 158048	48.4	30.2	129	35.6	0.4	0	0.01	0	0.01
86-02	585903	6221132	9V	75.6	77.1	C 158049	43.8	98.8	139	218.7	1.1	0	0.01	1.7	0.21
86-02	585903	6221132	9V	77.1	78.6	C 158050	33.8	10.8	71	54.2	1	0	0.01	1	0.01
86-02	585903	6221132	9V	78.6	80.2	C 158051	33.8	19.2	129	53.8	1.2	0	0.01	0.7	0.02
86-02	585903	6221132	9V	80.2	81.7	C 158052	56.4	20.2	90	143.2	2.8	0	0	2.1	0.12
86-03	585903	6221132	9V	2.7	4.3	C 158053	26.3	13.2	94	48.9	1.6	0	0.01	1.3	0.01
86-03	585903	6221132	9V	5.5	6.7	C 158054	65.2	3.7	68	40.6	0.4	0	0.01	0.5	0.02
86-03	585903	6221132	9V	6.7	7.9	C 158055	41.8	10.9	93	18.1	0.6	0	0	0.3	0.01
86-03	585903	6221132	9V	7.9	9.4	C 158056	65.5	31.9	117	64.3	1.2	0.1	0.01	4.7	0.01
86-03	585903	6221132	9V	15.8	17.4	C 158057	50	8.2	88	12.8	0.5	0	0.01	1.2	0.01
86-03	585903	6221132	9V	17.4	18.9	C 158058	61.4	5.6	89	4.7	0.3	0	0	0.5	0.01
86-03	585903	6221132	9V	18.9	19.8	C 158059	62.9	4.2	97	8.4	0.3	0	0	0.4	0.01
86-03	585903	6221132	9V	24.7	25.9	C 158060	26	20.3	101	37.4	0.8	0	0	0.7	0.01
86-03	585903	6221132	9V	26.2	27.7	C 158061	31.3	7.9	104	38.1	0.8	0	0.01	0.5	0.01
86-03	585903	6221132	9V	28.0	29.6	C 158062	27.6	4.6	93	33.5	0.3	0	0.01	0.3	0.01
86-03	585903	6221132	9V	29.6	30.2	C 158063	30.7	3.2	89	26.4	0.2	0	0	0	0.01
86-04	586105	6221135	9V	6.1	6.7	C 158064	42.4	5	82	32	0.1	0	0	0.7	0.01
86-04	586105	6221135	9V	7.0	8.2	C 158065	56.4	8.8	84	37.5	0.1	0.1	0	0.4	0
86-04	586105	6221135	9V	8.5	9.1	C 158066	37.1	17.6	67	44.2	0.2	0	0	0.7	0.01
86-04	586105	6221135	9V	9.4	10.1	C 158067	46.9	9.5	59	54.6	0.2	0.1	0	0.7	0.01
86-04	586105	6221135	9V	31.4	32.9	C 158068	48.5	5.9	73	51	0.4	0	0.01	0.5	0
86-04	586105	6221135	9V	32.9	34.4	C 158069	48.8	20	106	65.3	0.6	0.1	0.01	0.7	0
86-04	586105	6221135	9V	34.4	36.0	C 158070	41.9	42.4	94	47.7	0.3	0	0	0.4	0

Tommy Jack Property

Summary and Selected Elements from Sampling Un-split Noranda Drill Core

Appendix III

Analyses from Acme Analytical Laboratories analyzed by ICP (* Au and Ag analyzed by fire assay)

Drill Hole	Easting	Northing	Zone	From (m)	To (m)	Sample No.	Cu (ppm)	Pb (ppm)	Zn (ppm)	As (ppm)	Sb (ppm)	Bi (ppm)	Hg (ppm)	Ag (gpt)*	Au (gpt)*
86-04	586105	6221135	9V	36.0	37.5	C 158071	48.9	6.9	71	32.3	0.3	0	0	0.6	0
86-04	586105	6221135	9V	48.8	50.3	C 158072	36.9	17.6	57	58.6	0.3	0	0	0.7	0.01
86-04	586105	6221135	9V	50.3	51.8	C 158073	62.5	10.5	90	44.5	0.9	0.1	0	0.8	0
86-04	586105	6221135	9V	51.8	53.3	C 158074	48.4	8.5	82	44.5	0.4	0.1	0.01	0.3	0
86-04	586105	6221135	9V	53.3	54.9	C 158075	71.2	7.2	93	48.3	0.8	0.1	0.01	0.4	0
86-04	586105	6221135	9V	54.9	56.4	C 158076	72.4	33.4	132	49.4	0.5	0.1	0.02	1.2	0.22
86-04	586105	6221135	9V	56.4	57.6	C 158077	60.1	8.4	80	49.8	0.5	0.1	0.01	0.4	0
86-04	586105	6221135	9V	57.6	58.8	C 158078	41.7	16.2	122	338.6	0.7	0	0.17	0.7	0.02
86-04	586105	6221135	9V	58.8	60.4	C 158079	31.7	126.7	202	44.3	0.8	0	0.02	1.1	0
86-04	586105	6221135	9V	66.4	67.4	C 158080	89.4	6.9	73	288.7	0.5	0.1	0.02	0.9	0.03
86-04	586105	6221135	9V	68.0	69.2	C 158081	81.5	37.9	643	762.8	0.5	0	0.06	1.6	0.45
86-04	586105	6221135	9V	69.5	70.7	C 158082	74.6	3.9	77	50	0.1	0	0.01	0.8	0
86-04	586105	6221135	9V	71.0	72.2	C 158083	66.1	3.7	84	62.7	0.3	0	0	0.6	0
87-01	586365	6220367	9V	4.0	5.5	C 158084	55.6	2.6	46	44.9	0.2	0	0	0.3	0
87-01	586365	6220367	9V	5.5	7.0	C 158085	57.7	2.4	63	43.7	0.2	0	0	0	0
87-01	586365	6220367	9V	7.0	8.5	C 158086	57.7	3.1	80	44.6	0.2	0	0.01	0.4	0
87-01	586365	6220367	9V	24.4	25.6	C 158087	41.4	13	53	48.1	0.4	0	0.02	0.5	0
87-01	586365	6220367	9V	25.9	27.1	C 158088	65.9	27.2	175	44.5	0.2	0	0.01	0.5	0.02
87-01	586365	6220367	9V	27.1	28.3	C 158089	61.7	5.7	75	50.1	0.4	0	0	0.6	0
87-01	586365	6220367	9V	28.3	29.9	C 158090	68.3	4.4	79	46.5	0.5	0	0	0.7	0
87-01	586365	6220367	9V	29.9	31.4	C 158091	70	4.4	46	49.4	2	0.1	0	5.8	0
87-01	586365	6220367	9V	31.4	32.9	C 158092	76	6.9	66	50.1	0.4	0	0	1.1	0.03
87-01	586365	6220367	9V	32.9	34.4	C 158093	58.8	19	108	47.3	0.4	0.2	0	0.9	0.01
87-01	586365	6220367	9V	34.4	35.4	C 158094	88	33.9	62	139.9	0.5	0.3	0.01	1.6	0.19
87-01	586365	6220367	9V	39.0	40.5	C 158095	35.6	24.2	71	64.3	0.3	0	0	0.6	0.01
87-01	586365	6220367	9V	40.5	41.1	C 158096	50.1	26.9	111	43.2	1.9	0	0.01	4	0
87-01	586365	6220367	9V	46.6	48.2	C 158097	41.1	7.7	96	29.5	0.7	0	0.01	0	0
87-01	586365	6220367	9V	48.2	49.7	C 158098	76.3	28.8	98	62.6	0.8	0.1	0.01	1.7	0.03
87-01	586365	6220367	9V	49.7	51.2	C 158099	48	12.3	92	45.9	0.5	0	0.01	0	0
87-01	586365	6220367	9V	51.2	52.7	C 158100	50.5	11.7	65	49.3	0.9	0	0.01	0.9	0.01
87-01	586365	6220367	9V	52.7	54.3	C 158101	63.9	3	36	54.7	0.5	0	0	0.5	0
87-01	586365	6220367	9V	54.3	55.8	C 158102	63	9.2	22	319.9	0.8	0	0	1.1	0.33
87-01	586365	6220367	9V	55.8	57.3	C 158103	87.5	22.2	94	182	1.1	0	0.02	2.4	0.35
87-01	586365	6220367	9V	57.3	58.8	C 158104	63.5	3.4	64	92.6	0.4	0	0	0.9	0.02
87-01	586365	6220367	9V	63.1	64.3	C 158105	98.7	5.1	25	229.4	1.7	0	0.01	3	0.32

Tommy Jack Property

Summary and Selected Elements from Sampling Un-split Noranda Drill Core

Appendix III

Analyses from Acme Analytical Laboratories analyzed by ICP (* Au and Ag analyzed by fire assay)

Drill Hole	Easting	Northing	Zone	From (m)	To (m)	Sample No.	Cu (ppm)	Pb (ppm)	Zn (ppm)	As (ppm)	Sb (ppm)	Bi (ppm)	Hg (ppm)	Ag (gpt)*	Au (gpt)*
87-01	586365	6220367	9V	64.3	64.9	C 158106	71.8	3.8	61	64.2	0.3	0.1	0.01	0.6	0.01
87-01	586365	6220367	9V	64.9	66.4	C 158107	67.9	5	97	45.4	0.2	0	0	0.7	0
87-01	586365	6220367	9V	66.4	68.0	C 158108	68	4.3	87	44.6	0.3	0	0.01	0	0
87-01	586365	6220367	9V	68.0	69.8	C 158109	55.3	6.1	57	45	0.1	0	0	0.7	0.01
87-01	586365	6220367	9V	69.5	71.0	C 158110	49.5	11.5	90	35.3	0.4	0	0.01	0	0
87-01	586365	6220367	9V	71.0	72.5	C 158111	75.5	5.5	95	37.3	0.1	0	0	0.7	0
87-01	586365	6220367	9V	72.5	74.1	C 158112	53.3	15.1	90	37.2	0.2	0	0	0.3	0
87-01	586365	6220367	9V	74.1	75.6	C 158113	70.1	14.1	95	36.6	0.3	0.1	0	0.5	0.01
87-01	586365	6220367	9V	75.6	77.1	C 158114	69.7	26	92	46.3	0.4	0	0	0.8	0.01
86-05	586151	6221162	9V	4.3	4.9	C 158115	44.7	12.5	78	45	1.2	0	0.01	1.5	0.01
86-05	586151	6221162	9V	10.7	12.2	C 158116	48.3	80.9	69	1028.3	1.4	0	0.01	1.7	0.2
86-05	586151	6221162	9V	12.2	13.7	C 158117	50.3	62.8	152	423.6	1.2	0	0.01	0.6	0.06
86-05	586151	6221162	9V	13.7	15.2	C 158118	46.4	11.5	73	206.2	0.7	0	0	0.9	0.03
86-05	586151	6221162	9V	15.2	16.8	C 158119	45.6	72.6	341	54.2	1.1	0	0.04	0.7	0.03
86-05	586151	6221162	9V	73.2	74.7	C 158120	79.6	22.3	63	68.5	1.2	0	0.01	0.7	0.09
86-05	586151	6221162	9V	74.7	76.2	C 158121	116.6	10.7	399	132.2	1.1	0	0.05	1.3	0.07
86-05	586151	6221162	9V	76.2	77.7	C 158122	67.8	19.7	99	66.3	1.2	0	0.01	1	0.02
86-05	586151	6221162	9V	77.7	79.2	C 158123	52.5	9	76	50.5	1.5	0	0	2	0
87-15	586227	6220812	9V	4.9	7.0	C 158124	76.4	26.4	58	145	1.5	0	0	2.4	0.22
87-15	586227	6220812	9V	7.0	8.5	C 158125	86.8	25.3	80	113.3	0.9	0	0	1.5	0.07
87-15	586227	6220812	9V	8.5	10.1	C 158126	80	5.8	76	47.5	0.5	0	0	1	0.02
87-15	586227	6220812	9V	10.1	10.7	C 158127	64.5	4.4	69	44.9	0.3	0	0	0.4	0.03
87-15	586227	6220812	9V	72.2	74.1	C 158128	41.5	21.7	131	76.9	0.4	0	0	0.6	0.01
87-15	586227	6220812	9V	74.1	75.6	C 158129	54.1	16.2	74	79.2	0.7	0.1	0	1.1	0.1
87-15	586227	6220812	9V	75.6	77.7	C 158130	94.5	4148	492	151.1	17.6	0.1	0.2	17.4	0.35
87-15	586227	6220812	9V	77.7	78.6	C 158131	7	63.3	51	111.4	0.5	0.1	0.01	0.5	0.09
87-15	586227	6220812	9V	78.6	80.2	C 158132	1.8	74.3	49	37.7	0.2	0	0.01	0	0.04
87-15	586227	6220812	9V	80.2	81.7	C 158133	18.2	443.6	580	40.1	0.6	0.2	0.06	1.7	0.17
87-15	586227	6220812	9V	81.7	83.4	C 158134	20.8	394.2	449	48.1	0.7	0.2	0.05	1	0.16
87-15	586227	6220812	9V	83.4	84.7	C 158135	76.7	21	60	55.8	0.5	0.1	0	0.9	0.02
87-17	587038	6220552	9V	17.7	19.2	C 158148	31.9	197.2	295	64.8	0.4	0.1	0.02	1.1	0.06
87-17	587038	6220552	9V	16.2	17.7	C 158149	23.1	9.2	59	48.1	0.3	0.1	0	0.3	0
87-17	587038	6220552	9V	19.2	20.7	C 158150	42.8	27.8	143	347.3	0.6	0.2	0.01	1.1	0.03
87-17	587038	6220552	9V	20.7	22.3	C 158151	31.8	73.8	561	259.7	0.4	0.5	0.08	1	0.02
87-13	586539	6220754	9V	1.5	3.0	C 158152	39.3	103.4	59	1522.4	2.5	0.1	0.01	5.4	0.45

Tommy Jack Property

Summary and Selected Elements from Sampling Un-split Noranda Drill Core

Appendix III

Analyses from Acme Analytical Laboratories analyzed by ICP (* Au and Ag analyzed by fire assay)

Drill Hole	Easting	Northing	Zone	From (m)	To (m)	Sample No.	Cu (ppm)	Pb (ppm)	Zn (ppm)	As (ppm)	Sb (ppm)	Bi (ppm)	Hg (ppm)	Ag (gpt)*	Au (gpt)*
87-19	586148	6221163	9V	26.2	27.7	C 158153	11.2	118.3	150	59.1	0.6	0	0.01	0.8	0.02
87-19	586148	6221163	9V	27.7	29.3	C 158154	11.4	170.3	171	60	0.9	0	0.02	1.3	0.02
87-19	586148	6221163	9V	29.3	30.8	C 158155	4.2	60.2	111	195.2	0.5	0.1	0.01	0.4	0.06
87-19	586148	6221163	9V	30.8	31.7	C 158156	6.9	79.2	510	103	0.5	0	0.05	0.9	0.04

APPENDIX IV

Induced Polarization Report

LOGISTICAL REPORT

INDUCED POLARIZATION SURVEY

TOMMY JACK PROPERTY

HAZELTON AREA, BRITISH COLUMBIA

on behalf of

KODIAK EXPLORATION LTD.
Suite 520 – 885 Dunsmuir Street
Vancouver, B.C. V6C 1N5

Survey performed: July 9 to 19 and August 21 to 29, 2003

by

Alan Scott, Geophysicist
SCOTT GEOPHYSICS LTD.
4013 West 14th Avenue
Vancouver, B.C. V6R 2X3

September 2, 2003

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Appendix

Accompanying Maps

Accompanying Data Files

1. INTRODUCTION

An induced polarization (IP) survey was performed at the Tommy Jack Property, Hazelton Area, British Columbia, within the period August 21- 29, 2003. The survey was performed by Scott Geophysics Ltd. on behalf of Kodiak Exploration Ltd.. The survey was an extension of a survey performed in the period July 9-19, 2003, by Scott Geophysics Ltd. on behalf of GCP Mining Corporation. This report describes the instrumentation and procedures, and presents the results of both surveys.

2. SURVEY COVERAGE AND PROCEDURES

A total of 19.7 line km of IP survey was performed at the Tommy jack Property, 10.3 km in the July survey and 9.4 km on the August survey. The pole dipole array was used for the survey, with an "a" spacing of 25m and "n" separations of 1 to 5 (25/1-5). The online current electrode was located to the west of the potential electrodes on all survey lines, except line 10000E, for which it was located to the south.

All survey data is archived to the accompanying floppy disk.

3. PERSONNEL

Ken Moir was the crew chief on the survey on behalf of Scott Geophysics Ltd. Stephen Wetherup was the representative on behalf of Kodiak Exploration Ltd..

4. INSTRUMENTATION

A Scintrex IPR12 receiver and IPC7 transmitter were used for the IP survey. Readings were taken in the time domain using a 2 second on/2 second off alternating square wave. The chargeability values plotted on the accompanying pseudosections and plan maps are for the interval 690 to 1050 msec after shutoff.

Respectfully Submitted,

Alan Scott, Geophysicist

Statement of Qualifications

for

Alan Scott, Geophysicist

of

4013 West 14th Avenue
Vancouver, B.C. V6R 2X3

I, Alan Scott, hereby certify the following statements regarding my qualifications and involvement in the program of work on behalf of Kodiak Exploration Ltd. at the Tommy Jack Property, Hazelton Area, British Columbia, as presented in this report of September 2, 2003.

I have no material interest in the property under consideration in this report.

The work was performed by individuals sufficiently trained and qualified for its performance.

I graduated from the University of British Columbia with a Bachelor of Science degree (Geophysics) in 1970, and with a Master of Business Administration in 1982.

I am a member of the Association of Professional Engineers and Geoscientists of the Province of British Columbia.

I have been practicing my profession as a Geophysicist in the field of Mineral Exploration since 1970.

Respectfully submitted,

Alan Scott, P.Geo.

APPENDIX V

2003 Diamond Drill Hole Logs

Tommy Jack Property

2003 Diamond Drill Hole Logs

Appendix IV

Hole #: TJ03-01

Purpose: To test the possible strike extent of the camp showing to the SE.

Logged By: S. Wetherup, August 25, 2003

Project: 202.0
Azimuth: 30.0
Dip: -45.0
Easting: 585979
Northing 6221725

Date Commenced: August 23, 2003; 7:00 PM
Date Finished: August 24, 2003; 7:00 PM
Total Depth: 143.6 m
Core Size: BTW

From	To	Rock Description	Sample #	From	To	Comments	Qtz	FeCb	Cb	Py	Apy	Cpy	Gal	Sph	Au (gpt)	Ag (gpt)
0.0	18.3	Casing														
18.3	100.5	Intercalated medium grained arenite, fine grained arenite and siltstone. Arenite is light grey to dark grey, contains 30-60% feldspar (plagioclase) and 40-70% dark to light grey lithic fragments. Siltstone is dark grey to black, aphanitic, with rare fine grained disseminated or irregular masses (up to 1cm in diameter) of pyrite. Arenite and siltstone are soft as feldspar grains are waxy and appear to be mostly sericite or clay and the arenite often contains carbonate replaced clasts (i.e. carbonate/Fe-carbonate altered). Local zones of clay alteration and bleaching occur locally within arenite units. Veining is uncommon but rare calcite or gypsum veins occur within this zone with little to no quartz or sulphide minerals. Few graphitic shear zones/faults.	158251	18.3	21.0				tr						0.01	0.0
			158252	21.0	24.0				tr						0.00	0.0
			158253	24.0	26.5				tr						0.00	0.0
			158254	26.5	28.5				1						0.00	0.0
			158255	28.5	31.2	fault gouge 29.6 and 30.9			tr						0.00	0.0
			158256	31.2	34.0	Siltstone			tr						0.00	0.0
			158257	34.0	36.4	Siltstone			tr						0.00	0.0
			158258	36.4	40.0	Arenite to 37.3 then Siltstone			tr						0.00	0.0
			158259	40.0	43.3	Siltstone; broken throughout			tr						0.02	5.9
			158260	43.3	45.0	arenite with few wispy calcite veins; 50 deg. to CA			tr						0.00	2.0
			158261	45.0	45.3	Quartz within a graphitic gouge zone.			1						1.82	14.6
			158262	45.3	48.0	Arenite with veins at 20 deg. to CA.			1						0.00	0.0
			158263	48.0	51.0	Clay altered arenite to 48.7 m			tr						0.01	0.0
			158264	51.0	54.0	Clay altered arenite			tr						0.01	0.0
			158265	54.0	57.0	Clay altered arenite with gypsum veins			tr						0.00	0.0
			158266	57.0	60.1	Arenite with gypsum veins between 59.5 to 60.1			tr						0.00	0.0
			158267	60.1	63.0	Bedding 60 deg. to CA; broken at end of run.			tr						0.00	0.0
			158268	63.0	66.3	Joint set 45 deg. to CA; fg arenite			tr						0.00	0.0
			158269	66.3	69.0	Fg arenite; joints 50 deg. to CA			tr						0.00	0.0
			158270	69.0	72.0	Fg arenite to siliceous siltstone									0.00	0.0
			158271	72.0	75.0	Fg arenite to siliceous siltstone; fault parallel to CA			tr						0.00	0.0
			158272	75.0	78.0	Bedding 50 deg. to CA; fault 76.7m; vein set 70 deg. to CA			tr						0.00	0.0

			158273	78.0	81.0	Fg arenite and siltstone			tr	tr					0.00	0.0
			158274	81.0	83.9	Arenite			tr						0.01	0.0
			158275	83.9	87.0	Siltstone; 1mm veins 35 deg. to CA			tr						0.00	0.0
			158276	87.0	90.0	Fg arenite			tr						0.00	0.0
			158277	90.0	93.0	92.3-93.0 siltstone;1 cm calcite/quartz/pyrite vein 92.7m 20 deg. to CA			tr	tr					0.02	0.0
			158278	93.0	95.9	Bedding 60 deg. to CA			tr						0.00	0.0
			158279	95.9	96.7	SZ 20 deg. to CA with quartz-carbonate veins	tr	tr	2	tr		tr			0.00	0.0
			158280	96.7	100.5	Arenite with rare calcite veins			1						0.00	0.0
100.5	130.0	Intertcalated arenite and siltstone with an increase in veining. Also, veins consist of quartz-Fe-carbonate-calcite and commonly contain pyrite, galena,sphalerite, arsenopyrite, and possibly tetrahedrite. Veins cut CA @ 70 deg., 20 deg., 45 deg. and small graphitic and chloritic shearz cut the core @ 45 deg..	158281	100.5	101.5	Quartz vein and szs 50 deg. and 80 deg. to CA	1		1	tr					0.03	4.7
			158282	101.5	102.5	1% veins 80 deg.	tr		tr						0.00	0.0
			158283	102.5	103.5	1% veins 80 deg. and lenses 45 deg.	tr		tr						0.00	0.0
			158284	103.5	104.5	Broken with chloritic and graphitic shears	tr		tr						0.01	0.0
			158285	104.5	105.5	Siltstone	tr		tr						0.01	0.0
			158286	105.5	106.5	Siltstone; bedding 50-60 deg.	tr		tr	tr					0.00	0.0
			158287	106.5	107.5	Siltstone with chloritic and graphitic shears.	tr		tr	tr					0.00	0.0
			158288	107.5	108.5	Broken core.	tr		tr	tr					0.01	0.0
			158289	108.5	109.5	Broken siltstone	tr		tr	tr					0.01	0.0
			158290	109.5	110.5		tr		tr	tr					0.18	18.7
			158291	110.5	111.5	Siltstone with chloritic fractures	tr		tr	tr					0.01	2.2
			158292	111.5	113.0	Clay altered arenite	tr		tr	tr					0.12	5.5
			158293	113.0	114.3	Sericite altered arenite with Fe-carbonate	1	1	2	1				tr	0.01	0.0
			158294	114.3	115.7	Fe-carbonate and sericite altered arenite	1	2	1	1					0.45	17.5
			158295	115.7	118.0	Fe-carbonate and sericite altered arenite	1	2	1	tr			tr	tr	0.02	5.9
			158296	118.0	119.0	Silicified shear zone 118.0-118.6	3	1	3	1	tr	tr	tr	tr	0.29	30.6
			158297	119.0	120.0	Siltstone with 3 mm pyrite-quartz veins	1	1	1	2		tr	tr	tr	0.41	37.4
			158298	120.0	121.0	Siltstone; En echelon veins 1 to 10 mm ~ 5 to 20 cm apart	1	1	tr	tr			tr	tr	0.04	4.8
			158299	121.0	122.0	Siltstone; En echelon veins 1 to 10 mm ~ 5 to 20 cm apart	1	1	tr	tr			tr	tr	0.05	3.7
			158300	122.0	123.0	Siltstone; En echelon veins 1 to 10 mm ~ 5 to 20 cm apart	1	1	1	tr			tr	tr	0.10	3.6
			158301	123.0	124.0	Siltstone; En echelon veins 1 to 10 mm ~ 5 to 20 cm apart	1	1	1	tr			tr	tr	0.02	3.0
			158302	124.0	125.0	Altered arenite with quartz-Fe-carbonate veins	tr	tr	tr	tr			tr	tr	0.01	2.2
			158303	125.0	126.0	Altered arenite with quartz-Fe-carbonate veins	tr	tr	tr	tr			tr	tr	0.02	2.8
			158304	126.0	127.0	5 cm quartz vein 30 deg. to CA 127.0m	2	1	1	1	tr		tr	tr	0.26	11.8
			158305	127.0	128.0	Arenite; veins 45 deg., I 1 to 4 mm wide and 1 to 10 cm apart	1	1	1	tr					0.01	0.0

			158306	128.0	129.0	Arenite; veins 45 deg., ! 1 to 4 mm wide and 1 to 10 cm apart	1	1	1	tr					0.01	0.0
			158307	129.0	130.0	Fg arenite to siltstone	1	1	1	tr	tr	tr	tr	tr	0.26	5.5
130.0	143.6	Bleached and clay altered arenite.Veins are quartz-Fe-Carbonate and sulphide bearing; most veins are en echelon @ 45 deg. to the core axis.	158308	130.0	131.0	Two 1-2 cm veins in arenite	tr	tr	tr	tr	tr		tr	tr	0.17	4.6
			158309	131.0	132.0	Altered (clay) arenite	tr	tr	tr	tr					0.02	5.2
			158310	132.0	133.0	Altered (clay) arenite	tr	tr	tr	tr					0.02	0.0
			158311	133.0	134.0	Altered (clay) arenite	tr	tr	tr	tr	tr		tr	tr	0.09	5.4
			158312	134.0	135.0	Fault 134.4 (lost circulation)	tr		tr						0.01	0.0
			158313	135.0	136.0		tr	tr	tr	tr			tr	tr	0.07	189.9
			158314	136.0	139.0		tr	tr	tr	tr					0.01	0.0
			158315	139.0	142.0		tr	tr	tr	tr					0.01	0.0
			158316	142.0	143.6		tr	tr	tr	tr					0.00	0.0
					EOH											

tr=trace amounts
1 = tr to 1%
2 = 1 to 2%
3 = 2 to 5%
4 = 5 to 10%
5 = 10 to 25%
6 = > 25%

Tommy Jack Property

2003 Diamond Drill Hole Logs

Appendix IV

Hole #: TJ03-02

Purpose: To test the main showing to depth.

Logged By: S. Wetherup, August 27, 2003

Project: 202.0
Azimuth: 327.5
Dip: -44.0
Easting: 585979
Northing 6221725

Date Commenced: August 24, 2003; 9:00 PM
Date Finished: August 27, 2003; 5:00 PM
Total Depth: 252.1 m
Core Size: BTW

		Rock Description														
From	To		Sample #	From	To	Comments	Qtz	FeCb	Cb	Py	Apy	Cpy	Gal	Sph	Au (gpt)	Ag (gpt)
0.0	15.2	Casing														
15.2	39.0	Intercalated medium grained arenite, fine grained arenite and siltstone with trace Fe-carbonate-carbonate-quartz +/-sulphide minerals. Sulphide content of the veins increases near base of this unit. Locally sulphide minerals asre disseminated within the wall rock adjacent to sulphide bearing veins.	158157	15.2	18.0	Siltstone	tr		tr						0.00	0.0
			158158	18.0	21.0	Siltstone to 20.8 then Arenite	tr		tr						0.01	0.0
			158159	21.0	24.0	Arenite; veins 45 degrees	tr		tr						0.00	0.0
			158160	24.0	27.0	Arenite to 24.3 then siltstone; bedding 20 degrees	tr		tr	tr					0.00	0.0
			158161	27.0	30.0	Arenite			tr						0.00	0.0
			158162	30.0	33.0	Arenite; slightly clay altered	tr		tr						0.00	0.0
			158163	33.0	36.0	Arenite; Fe-carbonate altered	tr		tr	tr					0.00	2.0
39.0	45.2	Quartz-Fe-Carbonate veins contain from trace to 20-30% pyrite, sphalerite, galena, arsenopyrite, and chalcopyrite. This zone also contains abundant graphitic shears (with quartz sulphide veining) @ 30-35 degrees to CA.	158164	36.0	39.0	Pyritic zone 37.4 m; pyrite vein 30-40 degrees to CA.	tr	tr	tr	1					0.01	8.4
			158165	39.0	40.0	Quartz-Fe-carbonate breccia with 10% pyrite-sphalerite-galena; 30 degrees to CA.	2	2	2	1			tr	tr	0.07	25.7
			158166	40.0	42.7	One vein parallel to CA	1	1	1	tr			tr	tr	0.00	8.8
			158167	42.7	43.1		tr		tr	tr					0.00	3.0
			158168	43.1	44.2	Massive quartz-pyrite-chalcopyrite within a graphitic shear zone	5	3	2	3	tr	tr	tr	tr	1.20	71.2
			158169	44.2	45.8	Quartz stockwork and veins within bleached arenite	3	3	3	2	tr	tr	1	1	0.11	17.9
45.8	72.3	Approximately 1-2% quartz-Fe-carbonate-pyrite-galena-sphalerite veining throughout. Wall rock also contains disseminated pyrite, galena and sphalerite within a few centimeters of a sulphide bearing vein. Veinsets occur @ 30 and 60 degrees to CA. The veins @ 60 degrees to CA generally originate and terminate at the 30-35 degree veins	158170	45.8	48.0		3	2	2	3	tr	tr	1	1	0.33	24.4
			158171	48.0	50.0	V. 40 degrees to CA	3	2	2	3	tr	tr	1	1	0.50	48.0
			158172	50.0	52.0	Siltstone	2	1	1	2	tr	tr	tr	tr	0.07	7.2
			158173	52.0	54.0	Arenite	1	1	1	2	tr	tr	tr	tr	0.19	19.6
			158174	54.0	56.0	V. 30 degrees to CA; bedding 40 degrees	1	1	1	1	tr	tr	tr	tr	0.10	6.0
			158175	56.0	59.0		tr	tr	tr	tr	tr	tr	tr	tr	0.20	8.4
			158176	59.0	60.0	1-2 cm wide veins with sulphide 59.3 m and a shear zone 59.6 m and 35 degrees	3	3	3	3	tr	tr	1	1	0.75	28.6
			158177	60.0	62.1	Siltstone	tr	tr	tr	tr	tr	tr	tr	tr	0.08	17.7
			158178	62.1	63.0	Arenite; three 1 cm wide veins 30 degrees	2	2	2	3	tr	tr	1	1	0.84	111.5

			158179	63.0	66.0	Few gash veins 50 degrees	2	2	2	3	tr	tr	1	1	0.39	135.2
			158180	66.0	69.3	Arenite	1	1	1	2	tr	tr	tr	tr	0.10	16.5
			158181	69.3	72.3	Fg arenite with siltstone	1	1	1	2	tr	tr	tr	tr	0.13	10.8
72.3	118.6	Trace quartz-carbonate veining and rare sulphide minerals in the veins. Chlorite is common along veins in this section. Rock is intact with little breakage; it is carbonate altered with feldspars in the artenite alteredd to sericite and some of the mafics replaced by Fe-carbonate locally. The dominant vein orientation is 40-55 degrees to CA and some sub-parallel to the core axis.	158182	72.3	75.0	Arenite cut by veins 35 degrees	tr	tr	tr	1	tr	tr	tr	tr	0.11	6.6
			158183	75.0	78.0	Bedding 40-45 degrees	tr	tr	tr	tr					0.19	6.0
			158184	78.0	81.0	Arenite weakly clay altered	tr	tr	tr	tr					0.01	2.2
			158185	81.0	84.0	Broken between 82.0 and 83.0m	tr	tr	tr	tr					0.02	2.0
			158186	84.0	87.0	Siltstone	tr	tr	tr	tr					0.00	3.1
			158187	87.0	90.0	Arenite to 89.0m; Siltstone to 90.0	tr	tr	tr	tr					0.01	0.0
			158188	90.0	93.0	Arenite; shear zone between 91.3-92.8; dominant veins 45-50 degrees	tr	tr	tr	tr					0.00	0.0
			158189	93.0	96.0	Arenite	2	2	2	tr					0.01	2.6
			158190	96.0	99.0	Arenite	1	1	1	tr					0.00	0.0
			158191	99.0	102.0	Arenite to 100.0; silstone to 102.0	1	1	1	tr					0.01	6.5
			158192	102.0	104.9	Broken and sheared siltstone	1	1	1	tr					0.03	11.2
			158193	104.9	108.0	Arenite; bedding 20 degrees; veins 30 degrees	1	1	1	tr					0.01	0.0
			158194	108.0	111.4	veins 35-40 degrees	1	1	1	tr					0.01	0.0
			158195	111.4	114.0	112.5-112.6 quartz vein; 113.1-113.4 shear zone	2	2	2	tr					0.01	0.0
			158196	114.0	117.0	Chloritic arenite	1	1	1	tr					0.01	0.0
			158197	117.0	118.6	veins 30-35 degrees	2	2	2	1					0.01	2.3
118.6	145.3	Quartz-Fe-Carbonate veins occur in slightly higher abundances (~1%) and accessory mineralogy consists predominantly of pyrite-sphalerite-and galena and little chlorite. Sulphide minerals occur finely disseminated within the wall rock (arenite and lesser siltstone). This section contains some wider veins (1 cm to 40 cm) than the typical hairline to 1 cm thick veins observed elsewhere. Conjugate vein sets occur at 20-30 degrees, 50-70 degrees and parallel to the core axis. The 20-30 degree veins are the most dominant and the 50-70 degree veins in lesser abundance seem to occur with a joint set which ranges from 45 to 70 degrees to the core axis.	158198	118.6	120.0	veins 30 and 50 degrees with sulphides	1	1	1	1			tr	tr	0.01	3.2
			158199	120.0	121.0	Arenite; with sub-parallel veins; and 70 degree veins	2	2	2	tr					0.00	0.0
			158200	121.0	122.0	Arenite with 70 degree veins	2	2	2	tr					0.00	0.0
			158341	122.0	123.0	Two 50 degree veins 0.5 to 2 cm	3	3	3	1			1	1	0.01	4.9
			158317	123.0	124.1	Two 50 degree veins	3	3	3	1			1	1	0.04	45.3
			158318	124.1	125.0	Two 50 degree veins	3	3	3	1					0.05	79.0
			158319	125.0	126.0	Few shear zones in last 50 cm 20-30 degrees to CA	1	1	1	tr					0.01	6.8
			158320	126.0	127.0	Two 50 degree veins	3	3	3	2	tr	tr	1	1	0.05	17.3
			158321	127.0	128.0	Arenite	1	1	1	tr					0.01	5.3
			158322	128.0	129.0		1	1	1	tr					0.01	3.7
			158323	129.0	129.8	Wall rock with pyrite veinlets parallel to CA	1	1	1	2			tr	tr	0.02	10.9
			158324	129.8	130.1	Quartz-sphalerite-galenalpyrite-arsenopyrite-chalcopyrite vein	5	4	2	3	1	1	3	3	2.63	2321.5
			158325	130.1	130.7	Wall rock with pyrite stringers	3	3	3	3			tr	tr	0.61	104.0
			158326	130.7	132.0	Arenite; veins 20 degrees	2	2	2	tr			tr	tr	0.04	25.1

			158327	132.0	133.0		1	1	1	tr					0.02	7.5
			158328	133.0	135.0	Arenite	tr	tr	tr	tr					0.00	0.0
			158329	135.0	136.0	1 cm vein 135.9 m	2	2	2	tr			tr	tr	0.11	110.5
			158330	136.0	137.0	Arenite	1	1	1	tr			tr	tr	0.00	3.6
			158331	137.0	138.0	Arenite	2	2	2	tr			tr	tr	0.01	6.8
			158332	138.0	139.0	Arenite with few sub-parallel veins	2	2	2	tr			tr	tr	0.01	10.5
			158333	139.0	140.0	Few veins/ stringers 45 degrees	1	1	1	tr			tr	tr	0.02	7.2
			158334	140.0	141.1	Few 45 to 60 degree and sub parallel veins	2	2	2	1			1	1	0.01	30.2
			158335	141.1	142.3	Veins 40 degrees	2	2	2	1			1	1	0.02	13.0
			158336	142.3	142.7	Quartz-sphalerite-galenalpyrite-arsenopyrite-chalcopyrite vein	6	5	3	3	1	1	3	3	1.60	19.6
			158337	142.7	144.2	Many 20-30 degree and 40-50 degree veins with abundant sulphides	3	3	3	3	tr	tr	1	1	0.06	12.2
			158338	144.2	145.3	Arenite	3	3	3	3	tr	tr	1	1	0.04	13.7
145.3	183.8	Weakly altered arenite andf siltstone with few wispy to planar hairline to 2mm calcite =/- gypsum+/-Fe-carbonate+/-quartz veinlets. Sulphide minerals rare to non-existant except near the base of this section (within 1m). Chlorite is common along vein selveges.	158339	145.3	148.0	Arenite; Veins 20-25 degrees	2	2	2	1			tr	tr	0.00	6.8
			158340	148.0	151.0	Arenite	tr	tr	tr	tr					Not Sampled	
			158342	151.0	154.0	Arenite	tr	tr	tr	tr					0.00	0.0
			158343	154.0	157.0	Arenite; veins 45 degrees	tr	tr	tr	tr					Not Sampled	
			158344	157.0	160.0	Small ptygmatic vein; joint set 45 degrees	tr	tr	tr						0.02	0.5
			158345	160.0	163.0	Shear zone between 160.9-162.1 cutting siltstone 20 degrees to CA.	tr	1	1	tr				tr	0.02	6.5
			158346	163.0	166.0	Shear zone between 164.5-164.8 cutting siltstone 20 degrees to CA.	tr	1	1	1					0.03	12.6
			158347	166.0	169.0	Arenite	tr	tr	tr	tr					0.02	0.7
			158348	169.0	172.0	Arenite (minor siltstone)	tr	1	1	tr					0.02	0.0
			158349	172.0	175.0	Arenite	tr	tr	tr						0.02	0.0
			158350	175.0	178.0	Arenite; veins 25 degrees	tr	tr	tr						0.02	0.3
			158201	178.0	181.0	Arenite; veins 40 degrees; siltstone from 178.9 to 181.0	tr	tr	1	tr					0.01	0.0
			158202	181.0	183.8	Arenite	tr	1	1	tr			tr	tr	0.09	16.7
183.8	207.7	Veins comprised of quartz-Fe-carbonate-calcite and usually pyrite, galena, sphalerite+/-arsenopyrite+/-tetrahedrite(?). Vein density is still low ~1% with local concentrations up to 3%. Also, arenite and siltstone contains wispy Fe-carbonate alteration locally.	158203	183.8	184.5	Siltstone; shear zone with abundant quartz-Fe-carbonate veins 20 degrees	2	3	3	2	1		1	1	0.01	2.3
			158204	184.5	188.0	Veins mostly 25 degrees and lesser amounts 60 degrees	1	1	1	tr			tr	tr	0.00	0.0
			158205	188.0	191.0	Veins mostly 25 degrees and lesser amounts 60 degrees and sub-parallel evins	1	1	1	tr					0.00	0.0
			158206	191.0	194.0	Siltstone	tr	tr	tr	tr			tr	tr	0.00	0.0
			158207	194.0	196.7	Siltstone few 45 and 90 degree veins	tr	tr	tr	tr					0.00	0.0
			158208	196.7	197.2	Two 1 cm arseonpyrite bearing quartz veins 20 and 45 degrees	3	3	3	1	1				0.00	0.0
			158209	197.2	200.0	1 cm arsenopyrite-quartz veins	1	tr	1	tr	tr				0.01	0.0
			158210	200.0	203.0	Most veins 60 degrees to CA	1	tr	1	tr			tr	tr	0.00	0.0

			158211	203.0	207.7	Shear zone 207.7 20 degrees to CA	tr	tr	tr	tr					0.00	0.0
207.7	241.4	Vein density increases below the 20 cm shear zone which occurs immediately above this unit. Veins contain more Fe-carbonate and far less chlorite (if any). Veins often have cocks comb/drusy quartz and open spaces within them. Sulphide accessory minerals are common. Open space veins are generally @ 10-25 degrees to CA and contain sulphides.	158212	207.7	210.0	Arenite; bedding 35 degrees; veins 25 degrees	tr	tr	tr	tr					0.00	0.0
			158213	210.0	212.5	Arenite; veins 45 degrees to CA which are also perpendicular to bedding (40 degrees to CA)	1	1	1	tr			tr	tr	0.02	5.5
			158214	212.5	215.5	Open space veins 0-20 degrees to CA	1	1	1	tr			tr	tr	0.01	6.9
			158215	215.5	217.5		tr	tr	tr	tr			tr	tr	0.00	3.3
			158216	217.5	219.0	Very few veinlets	tr	tr	tr						0.00	6.4
			158217	219.0	221.0	Bleached arenite; veins 30 degrees	1	1	1						0.01	6.2
			158218	221.0	222.0	Bleached arenite; veins 30 degrees and 60-90 degress to CA and a few 10 degrees to CA	3	3	3	tr					0.01	6.0
			158219	222.0	223.0	Bleached arenite; veins 30 degrees and 60-90 degress to CA and a few 10 degrees to CA	3	3	3	tr					0.01	10.0
			158220	223.0	224.0	Bleached arenite; veins 30 degrees and 60-90 degress to CA and a few 10 degrees to CA	3	3	3	1					0.33	6.5
			158221	224.0	225.0	Bleached arenite; veins 45 degrees and perpendicular to bedding (35 degrees)	3	3	3	1			tr	tr	0.14	12.7
			158222	225.0	226.0	Seven 1-2 cm veins 20 degrees	4	4	4	tr			tr	tr	0.20	20.9
			158223	226.0	227.0	Sub-parallel veins 226.2-226.6m	4	4	4	tr			tr	tr	0.04	5.5
		Note: Sampling error with 158343 and 158340 so no analyses.	158224	227.0	228.0	Siltstone	1	1	1	1			tr	tr	0.17	49.9
			158225	228.0	231.0	Siltstone; shear zone and banded quartz-graphite veins 231.7-231.9 m	tr	tr	tr	tr					0.02	8.3
			158226	231.0	232.0	Siltstone; veins 30 degrees	2	2	2	1			tr	tr	0.06	16.9
			158227	232.0	232.9	Siltstone; shear zone 232.3-232.8 m	1	1	1	1					0.01	12.7
			158228	232.9	234.0	Siltstone and arenitearallel and 30 degree to CA veins.	2	2	2	tr					0.04	15.3
			158229	234.0	235.0	Parallel to CA banded quartz vein	3	3	3	tr			tr		0.04	5.4
			158230	235.0	236.0		1	1	1	tr			tr	tr	0.01	4.3
			158231	236.0	237.0	Shear zone 236.5-236.9 20 to 30 degrees	2	2	2	tr					0.00	2.7
			158232	237.0	239.0		tr	tr	tr				tr		0.02	0.0
			158233	239.0	240.0	Open space drusy veins parallel to 20 degrees to CA	3	3	3	tr			tr		0.01	2.8
			158234	240.0	241.4	20 and 10 degree veins	2	2	2	1					0.01	3.5
241.4	252.1	Similar amounts of quartz-Fe-carbonate veins but there is very little sulphides. The most common veins are 20-25 degrees to CA and are orthogonal to a less abundant 45 degree set of veins.	158235	241.4	244.0		tr	tr	tr	tr					0.01	0.0
			158236	244.0	247.0	25 and 45 degree veins	tr	tr	tr	tr					0.01	0.0
			158237	247.0	250.0		tr	tr	tr	tr					0.01	0.0
			158238	250.0	252.1		tr	tr	tr	tr					0.02	0.0
					EOH											

tr=trace amounts
1 = tr to 1%
2 = 1 to 2%
3 = 2 to 5%
4 = 5 to 10%

5 = 10 to 25%
6 = > 25%

Tommy Jack Property
2003 Diamond Drill Hole Logs
Appendix IV

Hole #: TJ03-03

Purpose: To test to northernmost chargeability anomaly

Logged By: S. Wetherup, August 27, 2003

Project: 202.0
Azimuth: 211.0
Dip: -44.0
Easting: 585979
Northing 6221725

Date Commenced: August 27, 2003; 7:00 PM
Date Finished: August 28, 2003; 5:00 PM
Total Depth: 157.3
Core Size: BTW

From	To	Rock Description	Sample #	From	To	Comments	Qtz	FeCb	Cb	Py	Apy	Cpy	Gal	Sph	Au (gpt)	Ag (gpt)
0.0	9.2	Casing														
9.2	34.2	Arenite and siltstone with abundant quartz-Fe-carbonate-calcite-pyrite-galena-sphalerite-arsenopyrite veins. At base of this unit, intermediate dyke material is fractured, sheared and cut by numerous quartz-Fe-carbonate veins. Veins contain 2-20% sulphide minerals and upo to 80% locally. Vein sets in this section cut the core @ 35-45 (hairline to 4 cm wide), wispy veins cut the core @ 60-80 degrees and many tension fracture/gash veins occur sub-parallel to the core axis. Locally sulphide minerals are disseminated within the arenite/siltstone wall rock directly adjacent to sulphide bearing veins within 1 to 40 mm. The base of this unit is a fault breccia containing 30% quartz-carbonate, 30-40% graphite/coal, and 20-30% pyrite+/-sphalerite+/-galena.	158239	9.2	12.0	Arenite; veins 10-20 degrees and 70 degrees	tr	tr	tr	tr					0.00	0.0
			158240	12.0	15.0	Arenite; veins 10-20 degrees and 70 degrees	1	1	1	tr					0.00	0.0
			158241	15.0	16.7	Arenite; bedding 35 degrees									0.00	0.0
			158242	16.7	18.0	Siltstone; few shear zones 45 degrees	2	2	2	1			tr	tr	0.01	3.0
			158243	18.0	20.0	Arenite; broken with few shear zones; a 10 cm quartz vein 40 degrees	3	3	3	1					0.28	12.0
			158244	20.0	21.0	Most veins 40 degrees	2	2	2	1			tr	tr	0.13	33.0
			158245	21.0	22.0	Arenite; stockwork of quartz veins most 40 degrees	3	3	3	1			tr	tr	0.03	14.9
			158246	22.0	23.2	Arenite; veins 40 degrees and 80 degrees	4	4	4	1	tr		tr	tr	0.20	9.1
			158247	23.2	24.0		1	1	1	tr					0.04	23.0
			158248	24.0	25.0	Sub-parallel and 2 80 degrees veins	3	3	3	1			tr	tr	1.41	207.8
			158249	25.0	26.0	2cm vein @40 degrees	2	2	2	tr					0.02	9.9
			158250	26.0	26.8		2	2	2	tr					0.11	19.7
			158351	26.8	27.2	Several 80 degrees veins with arsenopyrite and pyrite; and sub-parallel veins.	3	3	3	3	2		tr	1	0.94	35.2
			158352	27.2	28.0	Several sub-parallel veins and 70 o veins in arenite	2	2	2	2			tr	tr	0.49	34.5
			158353	28.0	29.0	Siltstone	2	2	2	1					0.71	18.4
			158354	29.0	30.0	Siltstone; ends a 30 degrees shear zone	1	1	1	tr					0.06	18.0
			158355	30.0	31.0	Bleached intermiediate porphyritic dyke withfew quartz veins	3	3	3	tr					0.03	1.3
			158356	31.0	32.8	Quartz and sulphide zone.	5	5	5	4	tr	tr	4	4	9.38	580.3
			158357	32.8	34.2	Shear zone with sheared and bleached intermediate dyke and graphitic gouge.	2	2	2	2			tr	tr	0.60	39.3
34.2	37.1	Intermediate feldspar-hornblende porphyry dyke; 15-20% chloritized (euhedral?) hornblende and feldspar phenocrysts 5-10 mm long and 1-3 mm wide; few pyroxene pseudomorphs; matrix is light pistachio green with 1-2% disseminated pyrite/pyrrhotite.	158358	34.2	37.1	One 1cm wide vein 20 degrees to CA contains ruby silver? And arsenopyrite.				2	tr				0.03	1.0
			158359	37.1	40.0	Siltstone	tr	tr	tr	tr					0.01	0.0
			158360	40.0	43.0	Arenite				tr					0.02	0.0

			158361	43.0	46.0	Arenite and 20% siltstone									0.02	0.0
37.1	157.3	Arenite and siltstone with few coal seams; very few veins mostly containing calcite and lesser amounts of Fe-carbonate and usually< 25% quartz; sulphide minerals are uncommon; Locally arenite units are pervasively Fe-carbonate altered with feldspar grains altered to sericite and mafics to Fe-carbonate. Alteration is commonly in wispy zones parallel to the core axis; locally veins contain gypsum.	158362	46.0	49.0	Siltstone; bedding 30 degrees									0.01	0.3
			158363	49.0	52.0	Siltstone; bedding 35 degrees									0.02	0.0
			158364	52.0	55.0	Arenite and siltstone	tr	tr	tr						0.02	0.0
			158365	55.0	58.0	Veins 45 degrees	tr	1	1						0.01	0.3
			158366	58.0	61.0	Arenite; bedding 15 degrees									0.02	0.3
			158367	61.0	64.0	Sub parallel veinlets	tr	tr	tr	tr					0.01	0.0
			158368	64.0	67.0	Arenite	tr	tr	tr						0.02	0.4
			158369	67.0	70.0	Arenite	tr	tr	tr						0.03	0.7
			158370	70.0	73.0	Arenite; sub-parallel veins	tr	tr	tr						0.01	0.4
			158371	73.0	76.0	Arenite; sub-parallel veins	tr	tr	tr						0.01	0.4
			158372	76.0	79.0	Arenite									0.02	0.0
			158373	79.0	82.0	Arenite; few veins 70 degrees and 30 degrees	1	1	1	tr					0.01	0.0
			158374	82.0	85.0	Arenite; parallel and 70 degrees; shear zone 20 degrees	1	1	1	tr					0.01	1.0
			158375	85.0	88.0	Siltstone; bedding 5-10 degrees	tr	tr	tr	1					0.01	0.9
			158376	88.0	91.0	Siltstone; bedding 5 degrees to parallel	tr	tr	tr	1					0.00	1.4
			158377	91.0	94.0	Arenite and siltstone	1	1	1	tr					0.00	0.8
			158378	94.0	97.0	Broken arenite and siltstone; shear zone 20 degrees to parallel between 95.5 and 97.0 m	1	1	1	tr					0.00	0.9
			158379	97.0	100.0	Shear zone 97.0-97.5; bedding parallel to 5 degrees	tr	1	1	tr					0.00	0.9
			158380	100.0	103.0	Arenite; breccia zone @100.8	1	2	2	tr					0.01	1.4
			158381	103.0	106.0	Arenite and siltstone; 20 degrees veins	tr	1	1	tr					0.00	0.8
			158382	106.0	109.0	Arenite and siltstone; small 45 degrees shear zone				tr					0.00	0.6
			158383	109.0	112.0	Arenite and siltstone; 20 degrees veins				tr					0.00	0.0
			158384	112.0	115.0	Arenite and siltstone	tr	1	1	tr					0.00	0.3
			158385	115.0	118.0	Arenite	tr	1	1	tr					0.00	0.0
			158386	118.0	121.0	Arenite and siltstone; bedding 20 degrees	tr	1	1	tr					0.01	0.0
			158387	121.0	124.0	1 mm veins 10 degrees and 70 degrees within siltstone	tr	tr	tr	tr					0.00	0.0
			158388	124.0	127.0	Siltstone; broken between 124.4 and 126.0	tr	tr	tr	tr					0.00	0.0
			158389	127.0	130.0	Siltstone; veins 20-25 degrees	tr	1	1	tr					0.00	0.4
			158390	130.0	133.0	Siltstone; 1mm strngers 25 degrees to CA	tr	tr	1	tr					0.00	0.0
			158391	133.0	136.0	Arenite; sub-parallel veins; bedding 45 degrees	tr	1	1	tr					0.00	0.0
			158392	136.0	139.0	Arenite; bedding @70-80 degrees	tr	1	1	tr					0.00	0.0
			158393	139.0	142.0	Arenite	tr	1	2	tr					0.00	0.3

			158394	142.0	145.0	Coal 143.8m within arenite	tr	1	2	1					0.00	0.7
			158395	145.0	148.0	Siltstone	tr	1	1	tr					0.00	0.0
			158396	148.0	151.0	Siltstone; broken and graphitic slicks on surfaces	tr	1	1	tr					0.00	0.0
			158397	151.0	154.0	Siltstone; broken and graphitic slicks on surfaces; shear zone 20 degrees	tr	2	2	tr					0.00	0.0
			158398	154.0	157.3	Broken core; veins 70-80 degrees and parallel to CA.	tr	2	2	tr					0.00	0.7
					EOH											

tr=trace amounts
1 = tr to 1%
2 = 1 to 2%
3 = 2 to 5%
4 = 5 to 10%
5 = 10 to 25%
6 = > 25%

Tommy Jack Property

2003 Diamond Drill Hole Logs

Appendix IV

Hole #: TJ03-04

Purpose: To test to northernmost chargeability anomaly; cutting it to the NE

Logged By: S. Wetherup, August 30, 2003

Project: 202.0
Azimuth: 30.0
Dip: -45.0
Easting: 585813
Northing 6221427

Date Commenced: August 29, 2003; 11:00 PM
Date Finished: August 31, 2003; 3:00PM
Total Depth: 261.3
Core Size: BTW

From	To	Rock Description	Sample #	From	To	Comments	Qtz	FeCb	Cb	Py	Apy	Cpy	Gal	Sph	Au (gpt)	Ag (gpt)
0.0	9.2	Casing														
9.2	56.9	Arenite and 20% siltstone with carbonized plant fragments, and a few thin coal seams (<1cm); Slight sericite alteration (and Fe-carbonate?) most evident in the arenite but probably within the siltstone as well; scant verining ~1-2% with local zone of more intense veining ~5-10%; veins mostly Fe-carbonate, some calcite and minor quartz with a locallized zones where veins contain 1-10% sulphides; veins mostly cut the core 80 degrees, with a lesser abundance of veins 30-45 degrees and rare sub-parallel veins. A small intermediate porphyritic dyke occurs near the top of this section; it contains chloritized and clay altered horblende and feldspar phenocrysts, and ~1-2% pyrite.	158399	9.2	12.0	Siltstone to 10.1; clay gouge for 20cm then altered intermediate porphyry	tr	tr	tr	1					0.00	0.0
			158400	12.0	13.5	Altered intermediate porphyry til 12.9m then arenite.	tr	tr	tr	11					0.04	1.5
			158401	13.5	14.5	Quartz veins 30 degrees, sub-parallel and 50 degrees	3	3	3	1			tr	tr	0.04	1.5
			158402	14.5	15.5	Shear zone between 14.9-15.5 55-60 degrees; siltstone	3	3	3	2			tr	tr	0.09	1.9
			158403	15.5	16.5	Shear zone between 14.9-15.5; 55-60 degrees to CA; siltstone	3	3	3	2			tr	tr	0.02	11.8
			158404	16.5	19.0	Arenite; sub paralle shears (1mm wide); veins 70 and 20 degrees	2	2	2	tr					0.02	0.8
			158405	19.0	22.0	Arenite; shears and veins 80 degrees with perpendicular veins 30 degrees to CA	2	2	2	tr					0.00	0.4
			158406	22.0	25.0	Arenite	2	2	2	tr			tr	tr	0.00	1.0
			158407	25.0	28.0	Arenite	tr	tr	tr	tr					0.00	0.9
			158408	28.0	31.0	Arenite; bedding 70 degrees; few sub-parallel veins	tr	tr	tr						0.01	0.8
			158409	31.0	34.0	Siltstone last 2.5 m	tr	tr	tr						0.01	1.0
			158410	34.0	37.0	Siltstone									0.00	0.6
			158411	37.0	40.0	Arenite	1	1	1						0.01	0.0
			158412	40.0	43.0	Arenite; graphitic shear zone 42.8-45.5m 60-80 degrees	tr	tr	tr	tr					0.00	1.0
			158413	43.0	46.0	Arenite	tr	tr	tr						0.24	4.0
			158414	46.0	49.0	Arenite; veins 45 and 80 degrees	1	1	1						0.01	0.4
			158415	49.0	52.0	One CA parallel vein; arenite	1	1	1						0.00	0.0
			158416	52.0	55.6	Shear zone top tio bottom	2	2	2	tr					0.04	0.9
			158417	55.6	56.9	Siltstone	tr	tr	tr						0.19	1.9
56.9	66.2	Siltstone with several shear zones and 5-10% quartz-pyrite-Fe carbonate+/-chalcopyrite+/-arsenopyrite+/-sphalerite+/-galena veins; the largest most mineralized veins are @ 70-80 degrees to core axis and parallel to the shear zones that cut the core; lesser amounts of veins occur @ 45 degrees to core axis and splay off of the dominant veins set; these 45 degree veins are ~	158418	56.9	58.0	Arsenopyrite vein 70 degrees to CA	3	3	3	1	tr	tr	tr	tr	0.08	3.8
			158419	58.0	59.0	Shear zone between 58.5-59.0 m 70-80 degrees	3	3	3	1	tr	tr	tr	tr	0.09	2.9
			158420	59.0	60.0	Broken and graphitic	tr	tr	tr	tr					0.20	4.2

		perpendicular to the 70-80 degree veins; a few wispy 20 degree veins occur as well.	158421	60.0	61.0	20 degrees and sub-parallel veins with sulphides	2	2	2	tr	tr	tr	tr	tr	0.14	3.5
			158422	61.0	62.0	few 70-80 degrees veins	3	3	3	2	tr	tr	tr	tr	0.33	3.3
			158423	62.0	63.0	Wispy veinlets and stockwork	3	3	3	tr	tr	tr	tr	tr	0.12	3.8
			158424	63.0	64.0	Arenite; stockwork	4	4	4	1					0.27	5.4
			158425	64.0	65.0	Arenite	2	2	2	1					0.21	9.2
			158426	65.0	66.2	Shear zone; 80-70 degrees and sub-parallel deformation.	4	4	4	2	tr	tr	tr	tr	0.81	6.7
66.2	141.3	Arenite generally with minor siltstone; the three veins sets (70-80, 45, and sub-parallel) occur in this section but abundance is generally lower (~1-5%) with local zones up to 25% vein material; local small shear zones that are highly silicified and sulphide bearing. Core axis parallel veins usually sinuous and originate and terminate @ 45 degree or 80 degree veins.	158427	66.2	69.0	Arenite	tr	tr	tr	tr					0.02	1.1
			158428	69.0	72.0	Arenite; bedding 30 degrees	tr	tr	tr	tr				tr	0.01	0.3
			158429	72.0	75.0	Siltstone; with minor arenite	tr	tr	tr	tr					0.00	0.8
			158430	75.0	78.0	Siltstone	1	1	1	tr					0.00	1.2
			158431	78.0	81.0	Siltstone and arenite; Fe-carbonate altered; 80 degrees veins	1	1	1	tr	tr	tr			0.01	0.8
			158432	81.0	83.0	Arenite; 80 degrees veins	1	1	1	tr	tr				0.01	0.3
			158433	83.0	85.0	Arenite	2	2	2	1	1			tr	0.02	0.6
			158434	85.0	87.0	Arenite	tr	tr	tr	tr					0.01	0.8
			158435	87.0	89.0	Siltstone	tr	tr	tr	tr					0.01	0.3
			158436	89.0	91.0	Siltstone; sub-parallel vein	2	2	2	tr	tr			tr	0.01	1.8
			158437	91.0	93.0	Arenite; veins @80 and 35 o	1	2	1	tr					0.00	2.1
			158438	93.0	95.0	Shear zone 80 degrees	1	1	1	1					0.05	4.3
			158439	95.0	97.0	Long sub-parallel shear/vein	3	3	3	1					0.04	2.9
			158440	97.0	99.0	Arenite	2	2	2	1	tr	tr	tr	tr	0.02	4.2
			158441	99.0	101.0	Arenite; 80 and 40 degrees veins	2	3	2	1	tr	tr	tr	tr	0.02	2.7
			158442	101.0	103.0	Arenite; 80 degrees veins	1	2	1	tr					0.01	1.2
			158443	103.0	105.0	Arenite; 80 degrees veins	1	2	2	tr					0.01	1.3
			158444	105.0	107.0	Arenite; bedding sub-parallel to CA	2	3	2	1	tr	tr	tr	tr	0.06	0.8
			158445	107.0	111.0	Arenite; mostly 80 degrees veins	2	2	2	1					0.04	1.6
			158446	111.0	112.1	Arenite; mostly 80 degrees veins	2	2	2	1					0.01	1.2
			158447	112.1	113.4	Shear zone 70 and 90 degrees to CA	4	4	4	1		tr		tr	0.07	3.9
			158448	113.4	115.0	Arenite; 45 and 70 degrees veins; bedding sub-parallel	2	2	2	tr	tr	tr		tr	0.01	16.2
			158449	115.0	117.0	Arenite	1	2	1	tr					0.01	20.8
			158450	117.0	119.0	Arenite	2	3	2	tr				tr	0.00	10.7
			158451	119.0	120.0	Arenite; sub-parallel vein and a 2 cm wide vein 80 degrees	4	4	4	1	1			1	0.01	1.4
			158452	120.0	121.0	Arenite	2	2	2	tr					0.01	1.5
			158453	121.0	122.1	20cm quartz breccia 121.2	3	4	3	1					0.00	2.2

			158454	122.1	123.3	Bedding 10 degrees to CA	tr	tr	tr	tr					0.00	1.6
			158455	123.3	124.1	Chloritic gouge 124.1m 40 degrees to CA	3	3	3	1					0.04	16.2
			158456	124.1	126.0	Arenite	2	2	2	tr				tr	0.00	3.6
			158457	126.0	128.0	Arenite; 3cm wide 40 degrees vein and 2 cm wide 80 degrees vein	3	3	3	tr	tr			tr	0.01	3.3
			158458	128.0	130.0	Arenite	2	2	2	tr				tr	0.01	7.0
			158459	130.0	132.5	Arenite	1	1	1	tr					0.01	3.0
			158460	132.5	133.5	Arenite	4	4	4	1	tr	tr		tr	0.04	2.6
			158461	133.5	134.5	Arenite	3	3	3	1					0.02	3.1
			158462	134.5	135.5	Arenite; 20 degrees vein and 45 vein; bedding 0 degrees to CA	4	4	4	2	1			tr	0.05	4.3
			158463	135.5	137.0	Arenite	1	1	1	tr	tr				0.00	2.5
			158464	137.0	139.0	Arenite	2	2	2	1					0.01	3.2
			158465	139.0	141.3	Siltstone; 45 and 10 degrees veins	1	1	1	tr	tr				0.01	2.9
141.3	161.6	Coal seams within arenite and siltstone; coal zones often sheared and contains graphite; also these zones oftewn contain quartz-carbonate zones with~10-20% pyrite in the veins and stockworks; trace amounts of chalcopyrite, arsenopyrite, sphalerite, and galena occur in the veins.	158466	141.3	142.7	Coal zone with shearing and quartz veins	3	3	3	1					0.04	3.5
			158467	142.7	144.8	Arenite; veins70 and 30 degrees	3	3	3	1					0.05	2.7
			158468	144.8	147.0	Graphitic shear zone 40 degrees to CA	tr	tr	tr	1					0.04	4.1
			158469	147.0	149.0	Arenite	tr	tr	tr	tr					0.04	2.1
			158470	149.0	151.5	Arenite	1	tr	1	tr					0.08	3.1
			158471	151.5	153.0	Arenite; shear zone20 degrees to CA	3	1	3	1					0.10	2.8
			158472	153.0	154.0	Siltstone	tr	tr	2	1					0.15	3.3
			158473	154.0	154.8	Siltstone; disseminated pyrite throughout	1	tr	1	1					0.06	1.6
			158474	154.8	155.5	Veins 80 degrees and 40 degrees; shear zonelast 20cm 40 degrees to CA.	3	tr	3	3					0.08	3.0
			158475	155.5	156.5	Arenite	1	tr	1	tr					0.01	1.5
			158476	156.5	157.5	Arenite; quartz stockwork	4	tr	4	2					0.86	7.2
			158477	157.5	158.5	Arenite; veins 80 degrees, sub-parallel and 20 degrees to CA	4	tr	4	3					1.42	10.8
			158478	158.5	159.0	Veins 30 degrees to CA	4	tr	4	3					2.20	3.9
			158479	159.0	160.0	Coal zone and shearz 20 degrees to CA	1	tr	1	1					0.71	5.4
			158480	160.0	160.8	Arenite; quartz beccia zone	4	tr	tr	1					0.63	3.2
			158481	160.8	161.6	Siltstone; small shear 40 degrees 160.8-161.0m	1	tr	1	tr					0.01	1.7
161.6	234.0	Arenite with quartz-Fe carbonate-calcite veins; rare sulphides in the veins and disseminated within the host rock; very few shear zones or coal seamsIn this section; arenite is Fe-carbonate altered in most sections; local zones of more intense veining up to 5-7%.	158482	161.6	165.0	Arenite	1	1	1	tr					0.01	0.8
			158483	165.0	168.0	Arenite	1	1	1	tr				tr	0.00	0.9
			158484	168.0	171.0	Arenite	tr	tr	tr	tr				tr	0.00	0.7
			158485	171.0	174.0	Arenite; Fe-carbonate altered; bedding 10 degrees	2	3	1	tr				tr	0.00	0.0
			158486	174.0	177.0	Arenite; Fe-carbonate altered	tr	3	tr	tr					0.01	0.8

			158487	177.0	180.0	Arenite; Fe-carbonate altered	2	2	tr	tr				tr	0.00	0.0
			158488	180.0	183.0	Arenite and siltstone; broken section; fault gouge 40 degrees to CA 181.5 m	2	2	2	tr					0.00	0.0
			158489	183.0	186.0	Arenite; veins 30 degrees and 80 degrees to CA	2	2	2	tr					0.01	0.0
			158490	186.0	189.0	Arenite; shear with quartz 20 degrees to CA	2	2	2	tr					0.01	0.6
			158491	189.0	192.0	Siltstone	2	2	2	tr					0.01	0.0
			158492	192.0	195.0	Arenite; open space quartz cocks comb breccia 193.3-193.4	2	2	2	tr				tr	0.03	0.8
			158493	195.0	198.0	Arenite; bedding 10 degrees to Sub-parallel to CA	1	1	1	tr					0.00	0.0
			158494	198.0	201.0	Arenite	1	1	1	tr					0.02	0.5
			158495	201.0	204.0	Arenite; bedding sub-parallel to CA	tr	tr	tr	tr					0.01	0.7
			158496	204.0	207.0	Arenite	tr	tr	tr	tr					0.00	0.7
			158497	207.0	210.0	Arenite; cross-bedded 40-30 degrees to CA; most bedding sub-parallel to CA	tr	tr	tr						0.01	1.2
			158498	210.0	211.0	Arenite;20 degrees and 80 degrees veins	3	3	3	1					0.00	0.3
			158499	211.0	212.0	Arenite;20 degrees and 80 degrees veins	tr	tr	tr	tr					0.02	0.6
			158500	212.0	213.0	Arenite; gouge 40 degrees	tr	tr	tr	tr					0.00	1.6
			158501	213.0	214.0	45 and 20 degrees veins	3	1	3	tr				tr		
			158502	214.0	215.0		2	1	2	tr					0.01	0.6
			158503	215.0	216.0	Arenite; sub-parallel and 80 degrees veins	2	1	2	1				tr	0.05	0.0
			158504	216.0	219.0	Arenite	1	tr	1	tr					0.00	0.0
			158505	219.0	222.0	Arenite; bedding sub-parallel to CA									0.01	0.0
			158506	222.0	225.0	Arenite									0.01	0.5
			158507	225.0	228.0	Arenite; bedding sub-parallel to CA									0.00	0.4
			158508	228.0	231.0	Broken; shear zone 229.4; 30 degrees to CA	1		1	tr					0.01	0.8
			158509	231.0	234.0		2	1	2	tr			tr	tr	0.00	1.1
234.0	242.4	Graphitic shear zone with quartz-carbonate-pyrite-galena-sphalerite stringers extending several meters above and below veinsa in the shear zones; shear zones @ 80 degrees and 45 degrees; 45 degree shears are most common and locally a few sub-parallel shears occur.	158510	234.0	235.0	Arenite; several 80 degrees veins 1mm to 2 cm wide	3	tr	3	1			tr	tr	0.16	1.8
			158511	235.0	236.0	Arenite; 80 degrees veins	2	1	2	1			tr	tr	0.21	2.6
			158512	236.0	237.0	Arenite	3	1	3	1			tr	tr	0.28	3.6
			158513	237.0	238.0	Arenite up to 237.2 m then shear zone	4	1	4	2			tr	tr	0.87	15.2
			158514	238.0	239.4	Shear zone	4	1	4	2			tr	tr	0.98	13.6
			158515	239.4	240.4	Siltstone and arenite	1	1	1	tr					0.02	1.7
			158516	241.4	241.4		2	2	2	1			tr	tr	0.02	1.3
242.4	261.3	Arenite with scant (trace-1%) quartz-Fe carbonate-carbonate veins +/-pyrite.	158517	242.4	242.4	Veins @45 ans 80 degrees	2	2	2	1			tr	tr	0.04	2.1
			158518	246.0	246.0	Gouge 244.1-244.3	tr	tr	tr	1					0.00	0.9
			158519	249.0	249.0	Arenite	tr	tr	tr	tr					0.01	0.0

			158520	252.0	252.0	Arenite	tr	tr	tr	tr					0.01	0.7
			158521	255.0	255.0	Arenite	1	1	1	tr			tr	tr	0.00	0.4
			158522	258.0	258.0	Arenite and siltstone; graphitic shear zone 257.7-258.0m; 40 degrees the CA	1	1	1	tr					0.01	1.1
			158523	261.3	261.3	Fault gouge 259.6 m									0.01	0.6
					EOH											

tr=trace amounts
1 = tr to 1%
2 = 1 to 2%
3 = 2 to 5%
4 = 5 to 10%
5 = 10 to 25%
6 = > 25%

Tommy Jack Property

2003 Diamond Drill Hole Logs

Appendix IV

Hole #: TJ03-05

Purpose: To test the western chargeability anomaly; cutting it to the SW

Logged By: S. Wetherup, September 2, 2003

Project: 202.0
Azimuth: 150.0
Dip: -45.0
Easting: 585816
Northing 6221429

Date Commenced: August 31, 2003; 5:00 PM
Date Finished: September 1, 2003; 11:00 PM
Total Depth: 221.6
Core Size: BTW

From	To	Rock Description	Sample #	From	To	Comments	Qtz	FeCb	Cb	Py	Apy	Cpy	Gal	Sph	Au (gpt)	Ag (gpt)
0.0	6.1	Casing														
6.1	18.4	Siltstone and arenite with a few small graphitic shears; 1-5% quartz-Fe carbonate-carbonate-pyrite veining.	158524	6.1	8.0	Arenite	1	1	1	tr					0.00	0.0
			158525	8.0	10.0	Arenite; small banded quartz vein @ 9.8 m; 20 degrees to CA	2	2	2	tr					0.00	0.0
			158526	10.0	12.0	Siltstone	tr	tr	tr	tr					0.01	0.0
			158527	12.0	14.0	Siltstone with some coal zones; shear zone 40 degrees to CA	tr	tr	tr	tr					0.00	0.4
			158528	14.0	16.0	Arenite; veins 60 degrees to CA	2	2	2	tr					0.01	0.0
			158529	16.0	18.4	Arenite; veins 50 degrees to CA	3	3	3	1			tr	tr	0.05	1.3
18.4	22.5	Fault zone cuts core at 5 degrees; core mostly broken with clayey-graphitic gouge and quartz breccia containing orangy brown sphalerite and pyrite.	158530	18.4	20.5	Gouge and quartz breccia	5	5	5	1			tr	1	0.08	2.9
			158531	20.5	22.5	Arenite; with disseminated pyrite	2	2	2	1					0.02	2.0
22.5	24.4	Intermediate porphyritic dyke; sericite/clay altered phenocrysts; ~ 2-3% disseminated pyrite throughout and several 70 and 45 degree to core axis quartz-Fe-carbonate veins.	158532	22.5	24.4	Dyke	3	3	3	3				tr	Not sampled	
			158533	24.4	25.5	Arenite; quartz vein 10-20 degrees to CA	3	3	3	1				1	0.46	20.2
24.4	40.8	Arenite and minor intercalated siltstone with 2-5% quartz-Fe-carbonate veins; few shear zones; arenite is generally sericite altered and light grey in colour.	158534	25.5	28.0	Arenite	2	2	2	1				tr	0.02	1.9
			158535	28.0	30.0	Arenite	2	2	2	tr					0.01	1.5
			158536	30.0	32.0	Arenite	1	1	1	tr					0.01	0.9
			158537	32.0	34.0	Arenite	1	1	1	tr					0.01	1.1
			158538	34.0	36.0	Arenite	tr	tr	tr	tr					0.00	0.5
			158539	36.0	37.0	Arenite	tr	tr	tr	tr					0.01	1.3
			158540	37.0	37.7	Quartz breccia zone; 30 degrees to CA	5	5	5	2			tr	tr	0.07	2.3
			158541	37.7	38.8	Arenite	tr	tr	tr	tr					0.01	0.5
			158542	38.8	40.0	Arenite; quartz vein sub-parallel to CA	3	3	3	tr				tr	0.01	0.9
			158543	40.0	40.8	Arenite	tr	tr	tr	tr					0.01	0.9
40.8	42.5	Intermediate porphyritic dyke.	158544	40.8	42.5	Dyke	2	2	2	3				tr	0.06	1.3
42.5	60.6	Arenite; 1-10% quartz-Fe carbonate-carbonate with rare pyrite-sphalerite-galena veins; veins 80 and 45 degrees to CA and sub-parallel veins occur as	158545	42.5	43.5	Arenite; shear zone 20 degrees to CA @ 43.1 m	3	3	3	tr					0.01	0.8

		well; sericite alteration occurs locally.	158546	43.5	44.5	Arenite	2	2	2	tr					0.00	0.0
			158547	44.5	45.5	Arenite	4	4	4	tr					0.00	0.4
			158548	45.5	46.5	Arenite	2	2	2	tr					0.00	0.5
			158549	46.5	48.0	Arenite; sericite altered	1	1	1	tr					0.00	0.0
			158550	48.0	50.0	Arenite; sericite altered	3	3	3	tr					0.01	0.7
			158551	50.0	52.0	Arenite; sericite altered	tr	tr	tr	tr					0.00	2.2
			158552	52.0	54.0	Arenite; sericite altered	3	3	3	tr				tr	0.11	0.9
			158553	54.0	56.0	Arenite; sericite altered	3	3	3	tr					0.01	0.6
			158554	56.0	57.3	Arenite; sericite altered	3	3	3	tr					0.00	0.4
			158555	57.3	60.0	Arenite; sericite altered; a 1 cm near parallel to CA quartz vein runs for 1 m	3	3	3	tr					0.00	0.3
			158556	60.0	60.6	Arenite; sericite altered	2	2	2	tr					0.01	0.4
60.6	86.0	Siltstone with few shear zones and quartz veins with common pyrite; shear zones are graphitic and occur sub-parallel, 20-30 and 60-70 degrees to core axis.	158564	60.6	62.0	Siltstone	2	2	2	tr					0.00	1.0
			158557	62.0	64.0	Siltstone	tr	tr	tr	1					0.01	1.3
			158558	64.0	66.0	Siltstone	tr	tr	tr	2					0.00	1.5
			158559	66.0	68.0	Shears 20 and 45 degrees to CA	2	2	2	2					0.15	2.4
			158560	68.0	69.2	Siltstone; quartz breccia 20 degrees to CA	4	4	4	3					0.93	31.7
			158561	69.2	70.0	Siltstone	2	2	2	3					0.40	11.3
			158562	70.0	72.0	Siltstone; broken core	tr	tr	tr	2					0.03	1.1
			158563	72.0	74.8	Siltstone; broken core	tr	tr	tr	1					0.05	1.5
			158565	74.8	75.3	Siltstone	tr	1	1	1					0.12	2.2
			158566	75.3	78.3	Siltstone; shear zone 76.7 to 77.9; 20 degrees to CA	tr	tr	tr	tr					0.01	1.5
			158567	78.3	80.0	Arenite; broken; veins 45 degrees to CA	2	2	2	1					0.14	3.3
			158568	80.0	82.0	Gouge 45 degrees to near parallel to CA	tr	tr	tr	1					0.03	1.9
			158569	82.0	84.0	Gouge	tr	tr	tr	1					0.01	1.1
			158570	84.0	86.0	Gouge	tr	tr	tr	1					0.10	0.6
86.0	97.3	Arenite with rare quartz-Fe carbonate-carbonate veins with trace sulphides; veins 30 and 80 degrees to core axis and sub-parallel.	158571	86.0	88.0	Arenite	1	1	1	tr					0.00	0.4
			158572	88.0	90.0	Arenite; broken	tr	tr	tr	tr					0.00	0.0
			158573	90.0	92.0	Arenite; broken	tr	tr	tr	tr					0.00	0.6
			158574	92.0	94.0	Arenite	1	1	1	tr					0.01	0.8
			158575	94.0	96.0	Arenite; shear @ 96.0 m (10cm) 80 degrees to CA	tr	tr	tr	tr					0.14	5.3
			158576	96.0	97.3		tr	tr	tr	tr			1	1	0.03	1.7
97.3	98.6	Arenite with 2-5% quartz-Fe carbonate-pyrite-galena-sphalerite veins (~ 25-50% of veins comprised of sulphide minerals)	158577	97.3	98.6	Parallel veins with pyrite-sphalerite-galena	2	2	2	1				tr	0.24	5.0
			158578	98.6	100.1	Parallel veins with pyrite-sphalerite-galena in dyke material	2	2	2	3					0.02	0.0

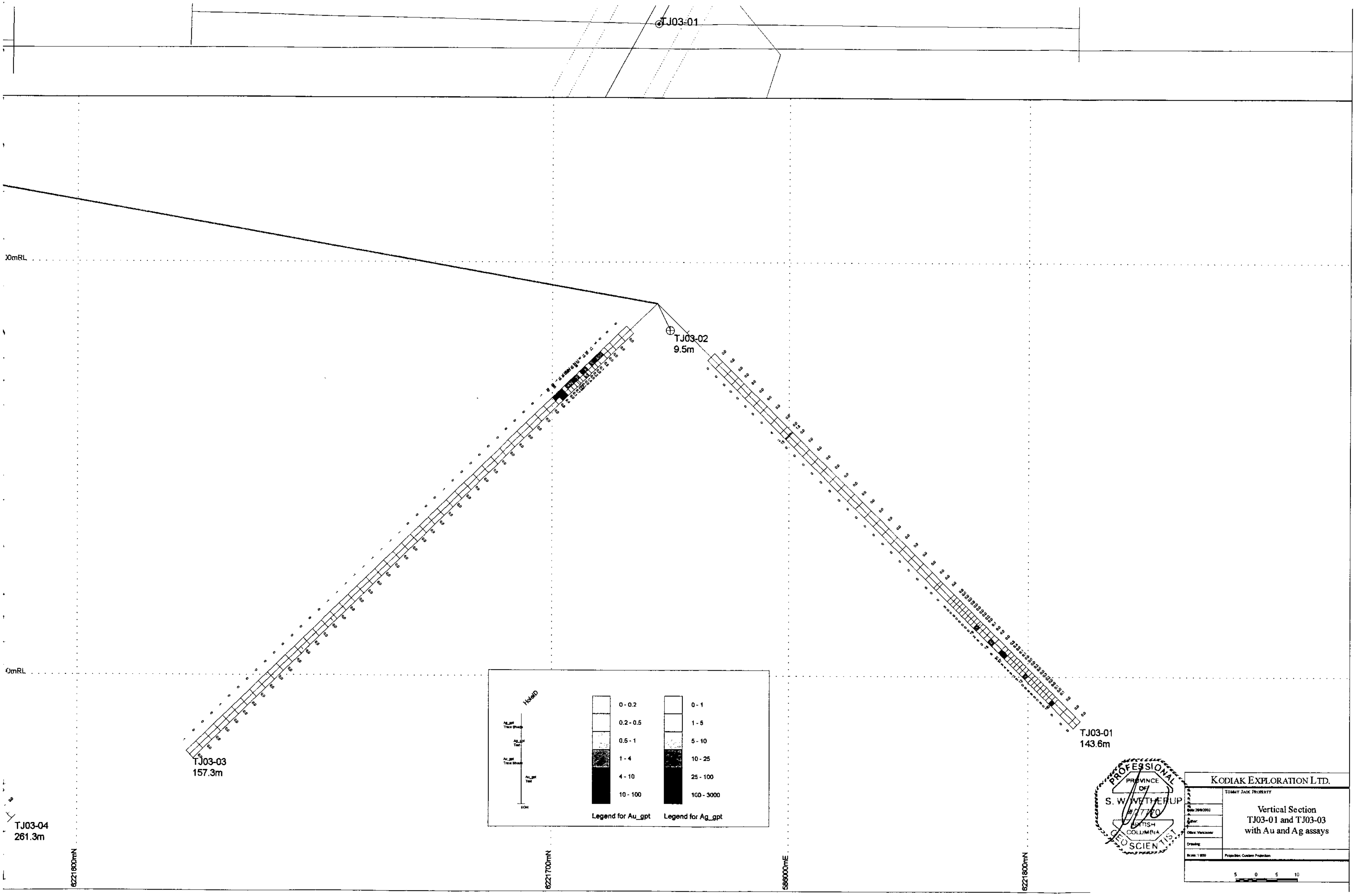
98.6	100.1	Intermediate prophyritic dyke; clay altered with disseminated pyrite	158579	100.1	101.0	Veins sub-parallel to 10 degrees to CA	2	2	2	3			tr	tr	0.07	2.3
100.1	109.0	Arenite with 2-5% quartz-Fe carbonate-pyrite-galena-sphalerite veins (~ 25-50% of vein comprised of sulphide minerals)	158580	101.0	103.0	Arenite; sericite altered	1	1	1	1					0.01	0.6
			158581	103.0	105.0	Arenite; sub-parallel and 80 degrees to CA veins	1	1	1	tr					0.04	0.9
			158582	105.0	106.0	Arenite; sub-parallel and 80 degrees to CA veins	1	1	1	tr			1	1	0.19	0.8
			158583	106.0	107.0	Arenite; one 1 cm vein	1	1	1	1			2	2	0.23	4.5
			158584	107.0	108.1	Arenite; two 3 cm veins	4	4	4	3					2.76	21.9
			158585	108.1	109.0	Sub-parallel veins	1	1	1	tr					0.02	2.0
109.0	139.7	Arenite with very little sulphide minerals in quartz-Fe-carbonate veins and little veining (<0.5%)	158586	109.0	111.0										0.02	0.5
			158587	111.0	113.0	Two veins 10 degrees to CA	tr	tr	tr	tr			tr	tr	0.02	1.0
			158588	113.0	115.0		1	1	1	tr					0.26	5.4
			158589	115.0	117.0		tr	tr	tr						0.02	2.0
			158590	117.0	119.0	Veins 45 degrees quartz pyrite veins; disseminated pyrite within arenite	1	1	1	2					0.01	1.2
			158591	119.0	120.0	Shear zone @ 119.0-119.3 m; 80 degrees to CA	3	3	3	2			1	1	0.18	3.0
			158592	120.0	121.0	20 degrees vein with sulphides	1	1	1	1			tr	tr	0.29	2.8
			158593	121.0	123.0	Veins 20 degrees to CA	1	1	1	tr			tr	tr	0.06	2.3
			158594	123.0	125.0		1	1	1	tr			tr	tr	0.03	2.6
			158595	125.0	127.0	Shear zone @ 125.3-125.6 m; 20 degrees to CA	3	3	3	1			tr	tr	0.02	2.8
			158596	127.0	129.0		tr	tr	tr	tr			tr	tr	0.05	1.8
			158597	129.0	131.0		tr	tr	tr	tr			tr	tr	0.04	1.2
			158598	131.0	133.0		tr	tr	tr						0.00	0.3
			158599	133.0	135.0	Shear zone 10 degrees to CA; between 135.4-135.9									0.00	1.0
			158600	135.0	137.0		1	1	1	tr			tr	tr	0.04	0.8
			158601	137.0	139.7		1	1	1	tr					0.01	0.5
139.7	140.7	Shear zone with quartz-pyrite-galena-sphalerite veining	158602	139.7	140.7		5	5	5	3			1	1	0.77	6.6
140.7	202.0	Arenite with scant veins generally below 0.5%; Up to 5-10% veins occur locally.	158603	140.7	143.0	Arenite; veins 80 degrees to CA	2	2	2	tr					0.01	1.7
			158604	143.0	146.0	Arenite; veins 45 degrees to CA	3	3	3	tr					0.02	1.7
			158605	146.0	149.0		tr	tr	tr						0.00	0.0
			158606	149.0	152.0	Bedding 70 degrees to CA	tr	tr	tr						0.00	0.0
			158607	152.0	155.0	Arenite	tr	tr	tr						0.04	0.3
			158608	155.0	156.0	Arenite									0.00	1.2
			158609	156.0	157.0	Arenite; 10cm vein 45 degrees to CA	4	4	4	2			1	1	0.62	12.6
			158610	157.0	160.0										0.01	0.4
			158611	160.0	163.0		tr	tr	tr						0.01	0.5

			158612	163.0	164.8		tr	tr	tr	tr					0.01	0.4
			158613	164.8	165.1	Arenite; pyrite pod ~ 6cm in diameter	1	tr	tr	5					0.04	1.6
			158614	165.1	168.0		tr	tr	tr	tr					0.01	0.4
			158615	168.0	171.0		tr	tr	tr	tr					0.03	0.7
			158616	171.0	172.8		tr	tr	tr	tr					0.02	0.6
			158617	172.8	174.0	Arenite; shear zone @ 173.6-174.0	3	1	3	tr					0.32	9.7
			158618	174.0	177.0		tr	tr	tr	tr					0.03	0.9
			158619	177.0	180.0	45 degrees veins	1	tr	1	tr					0.00	0.8
			158620	180.0	183.0	Veins 10-80 degrees to CA	tr	1	1	tr					0.01	0.4
			158621	183.0	186.0		1	2	2	tr					0.01	0.0
			158622	186.0	189.0		tr	tr	tr	1					0.06	0.0
			158623	189.0	190.0	Veins 10-30 degrees to CA	2	2	2	1			tr	tr	0.46	0.9
			158624	190.0	192.0		1	1	1	tr					0.01	0.9
			158625	192.0	194.1	Veins sub-parallel to CA	1	1	1	tr			tr	tr	0.90	1.4
			158626	194.1	197.0		1	1	1	tr					0.05	1.1
			158627	197.0	200.0		tr	tr	tr	tr					0.01	0.5
			158628	200.0	201.5	Siltstone	1	1	1	tr					0.03	1.4
			158629	201.5	202.0	Siltstone	3	3	3	3					0.84	8.3
202.0	205.4	Intermediate prophyritic dyke; clay altered with disseminated pyrite	158630	202.0	203.0	Contact ~ 80 degrees to CA; sheared contact; dyke	2	2	2	4					0.03	0.8
			158631	203.0	204.0	Veins 90 degrees to 10 degrees to CA	2	2	2	4					0.11	0.8
			158632	204.0	205.4		2	2	2	4					0.05	1.4
205.4	221.6	Arenite with scant veins generally below 0.5%; Up to 5-10% veins occur locally.	158633	205.4	206.4	Arenite	tr	tr	tr	tr					0.05	1.7
			158634	206.4	209.4	Siltstone	2	2	2	tr					0.03	1.3
			158635	209.4	212.0	Vein 45 degrees to CA	2	2	2	tr					0.01	0.9
			158636	212.0	214.0	Veins 20-30 degrees to CA	3	3	3	tr					0.01	0.0
			158637	214.0	215.0		3	3	3	1			tr	tr	0.02	3.5
			158638	215.0	216.5		1	1	1	tr					0.11	2.1
			158639	216.5	219.0		1	1	1	tr					0.01	0.5
			158640	219.0	221.6	Veins 20 degrees to CA	2	2	2	tr					0.01	1.0
					EOH											

tr=trace amounts
1 = tr to 1%
2 = 1 to 2%

APPENDIX VI

2003 Drill Sections



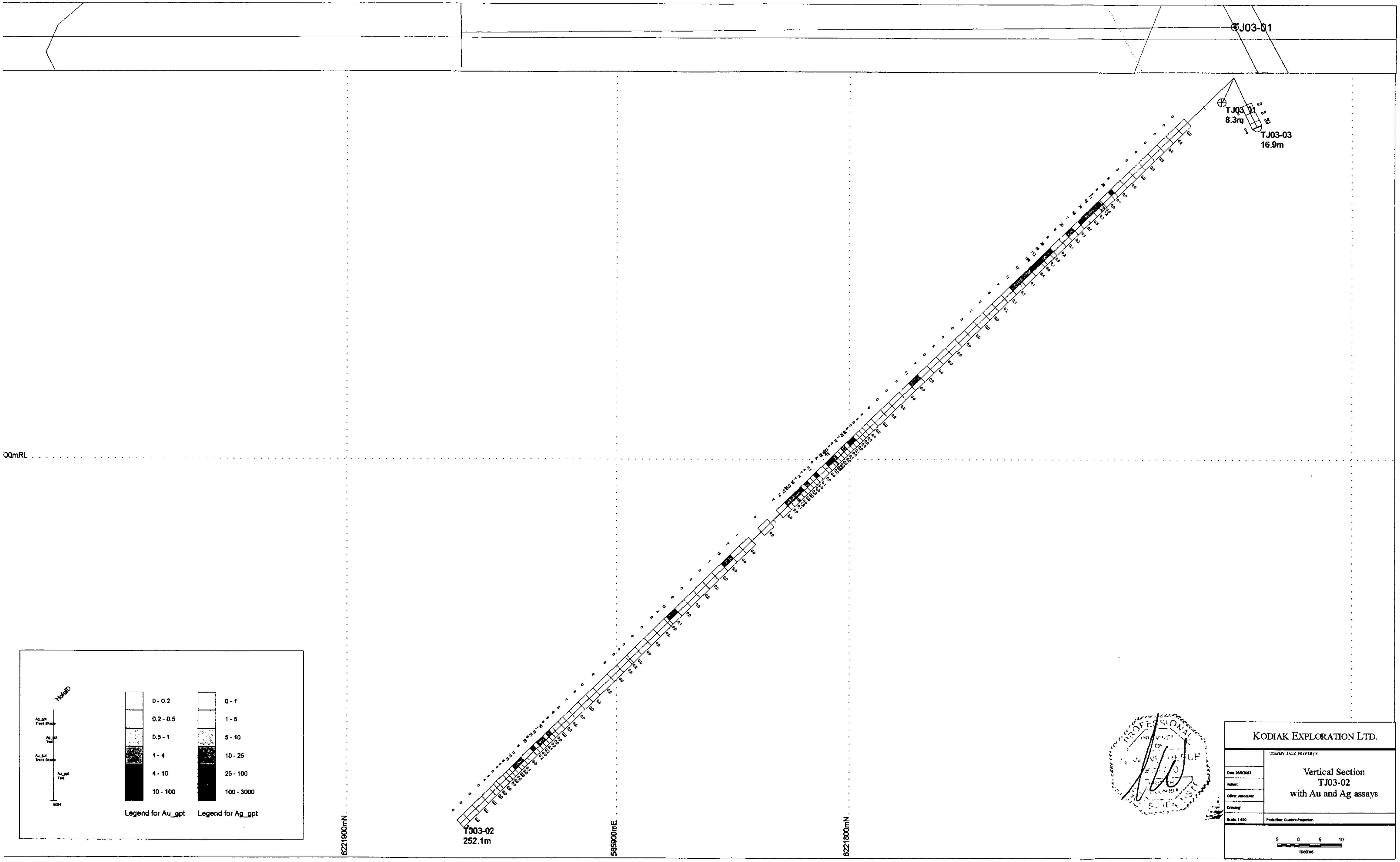
S. W. WETHERUP

KODIAK EXPLORATION LTD.

TOMMY JACK PROPERTY

Vertical Section
TJ03-01 and TJ03-03
with Au and Ag assays

Date: 26/9/2003
Author:
Office: Vancouver
Drawing:
Scale: 1:1000
Projection: Custom Projection



KODIAK EXPLORATION LTD.

TOMMY JACK PROPERTY

Vertical Section
TJ03-02
with Au and Ag assays

Date 26/9/2003

Author:

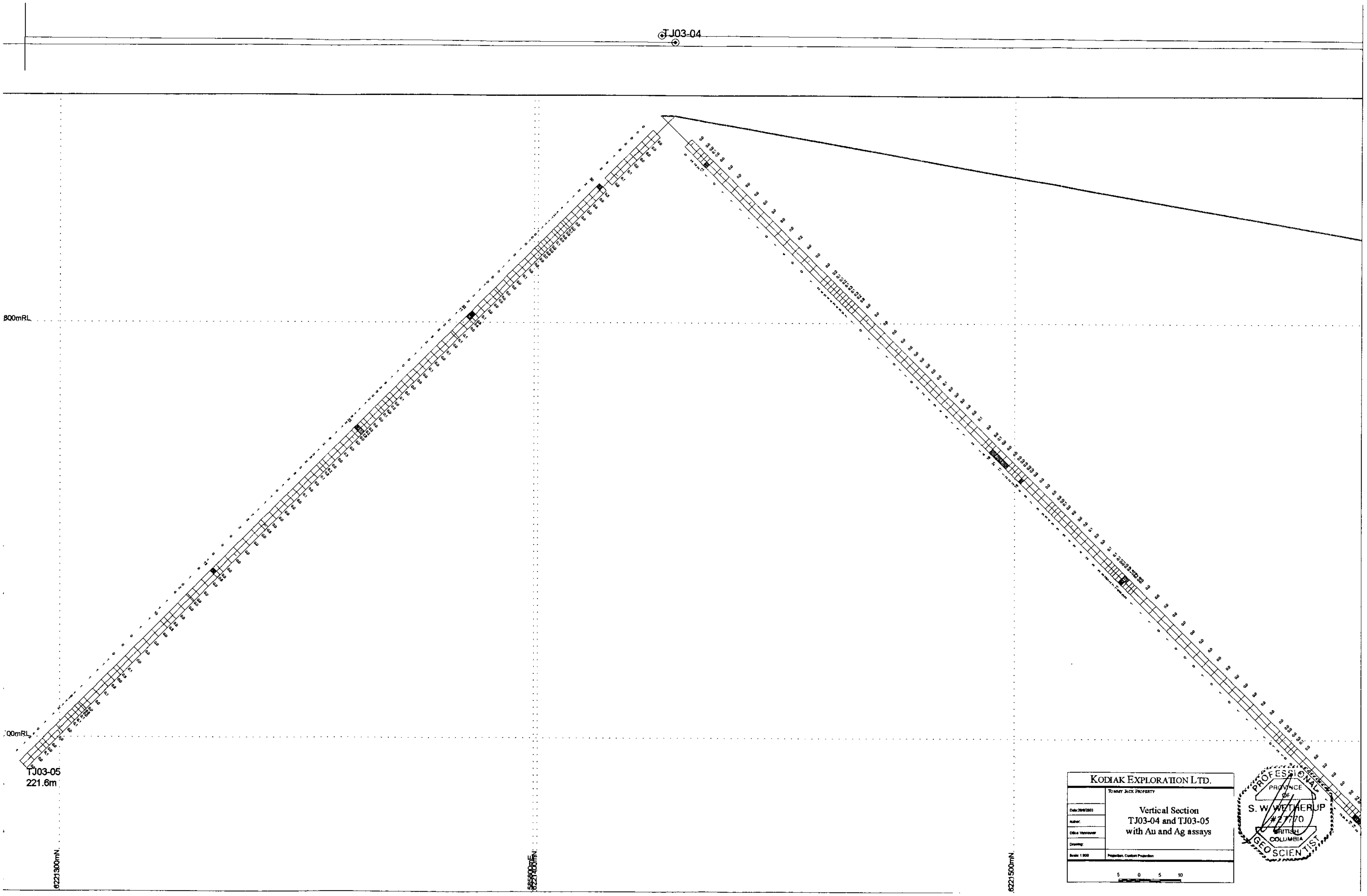
Office: Vancouver

Drawing:

Scale: 1:800

Projection: Custom Projection

5 0 5 10
metres



KODIAK EXPLORATION LTD.

TOMMY JACK PROPERTY

Vertical Section TJ03-04 and TJ03-05 with Au and Ag assays

Date:29/9/2003

Author:

Office: Vancouver

Drawing:

Scale: 1:800

Projection. Custom Projection

5 0 5 10

S. W. WETHERUP
#27770

APPENDIX VII

Assay Certificates

ACME ANALYTICAL LABORATORIES LTD. 8 E. H ING . V OUVE 1R6 PH (60 3-3 FAX 1)25 716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Kodiak Exploration Ltd. PROJECT 202 File # A302761

704 - 525 Seymour St., Vancouver BC V6B 3H7 Submitted by: S. Wetherup

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga	Se	Ag**	Au**	Sample
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppb	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	ppm	ppm	ppm	%	ppm	ppm	gm/mt	gm/mt	gm
S1	.5	1.2	.5	2	<.1	.3	.1	6	.09	.8	<.1	<.5	<.1	3	<.1	<.1	<.1	1	.11	.001	<1	2.0	.01	3	.003	1	.01	.529	.01	.1	<.01	.2	<.1	<.05	<1	<.5	.2	<.01	-
01108	.9	10.5	2.1	113	<.1	5.8	11.3	2727	7.55	2.1	.1	<.5	.3	301	.2	.1	.1	29	12.98	.035	7	3.3	3.71	66	<.001	2	.57	.007	.04	.5	.04	2.6	<.1	.07	2	<.5	.6	<.01	1700
01109	.8	11.2	86.2	13	.8	2.2	.6	325	.79	340.6	<.1	128.9	<.1	6	.1	1.6	.1	2	.09	.002	<1	9.5	.02	16	.001	1	.05	.010	.01	150.4	.01	.7	<.1	.14	<1	<.5	1.7	22	700
01110	5.8	6.7	2.9	11	.1	4.3	1.3	341	1.56	4.6	<.1	.7	<.1	49	.1	2.1	.1	3	.76	.143	2	15.8	.07	22	.001	2	.09	.007	<.01	6.0	<.01	.7	<.1	<.05	<1	<.5	<.1	<.01	1500
01111	.9	166.3	>9999	6512	49.2	2.8	1.0	30	7.17	1402.3	<.1	3638.9	<.1	5	78.4	112.7	4.4	<1	.01	.001	<1	10.1	<.01	7	<.001	<1	.04	.001	.02	6.6	4.25	.1	<.1	8.16	<1	.7	49.6	4.89	800
01112	2.4	140.3	5765.7	8657	15.1	7.1	10.8	6795	5.00	156.2	.1	145.0	.6	149	99.1	16.0	.2	23	5.44	.082	6	11.7	1.43	42	<.001	3	.40	.024	.20	>200	1.60	10.7	.1	.80	1	.6	14.3	.32	1300
01113	4.0	5.5	64.1	82	1.0	8.3	6.4	516	2.35	46.3	<.1	745.7	.2	41	.8	.7	<.1	2	.60	.023	1	14.7	.10	58	.001	2	.18	.007	.11	11.0	.04	1.9	<.1	1.23	<1	<.5	2.6	1.69	1000
01114	1.0	1458.9	>9999	63490	>200	3.7	3.7	102	3.84	7948.3	<.1	3351.4	<.1	5	742.2	1175.5	<.1	1	.06	.004	<1	7.2	.01	10	.001	<1	.08	.009	.03	4.3	21.59	.5	<.1	6.99	2	<.5	918.2	4.86	1900
01115	1.3	14.7	57.5	311	5.6	6.6	6.4	2320	6.70	27.2	.1	13.6	.4	685	3.0	9.7	<.1	48	11.23	.023	10	10.8	2.61	33	.001	<1	.34	.008	.03	1.3	.16	5.1	<.1	.05	1	<.5	6.6	.02	1600
01116	11.2	118.5	44.0	134	7.8	12.9	9.9	70	1.81	13.2	<.1	3721.2	<.1	8	1.6	4.3	66.4	4	.13	.003	<1	13.0	.03	92	.002	<1	.08	.003	.06	4.1	.01	.6	<.1	.81	<1	.9	6.4	1.57	1000
01117	8.3	2302.0	5.5	45	2.8	33.6	44.0	5448	5.55	3.9	.1	300.9	.1	36	.4	.5	13.6	35	2.78	.034	2	24.8	.46	28	.007	1	.96	.005	.21	2.4	.02	3.9	.1	1.69	3	<.5	3.3	.40	1200
01118	6.7	30171.4	6.7	53	25.9	65.5	59.1	752	6.85	7.2	<.1	635.1	<.1	70	.5	.6	63.6	6	.04	.006	<1	7.8	.05	9	.001	<1	.17	.002	.06	2.9	.03	.9	<.1	5.33	1	.9	26.0	2.17	1800
01119	7.9	588.7	7.9	11	12.2	2.3	.8	64	7.06	13.5	.2	5796.2	.2	8	<.1	5.8	1796.1	4	.02	.097	1	13.3	.02	445	.003	<1	.32	.002	.17	1.7	.03	1.1	<.1	<.05	1	2.3	13.2	5.47	1500
01120	4.1	1948.4	17.5	19	18.6	2.1	2.2	61	17.43	10.5	.4	10456.7	.5	15	.1	4.5	277.4	9	.02	.114	2	3.4	.02	868	.003	<1	.56	.001	.20	.8	.07	1.7	.1	<.05	5	4.2	13.9	7.34	1600
RE 01120	3.9	1951.6	17.6	21	12.7	1.8	2.2	60	17.52	10.8	.4	7551.7	.5	15	<.1	4.5	288.3	9	.01	.110	2	4.4	.02	866	.003	<1	.56	.003	.19	.9	.08	1.6	.1	<.05	4	4.2	16.7	8.56	-
01121	3.6	14.1	1.8	99	.1	2.6	4.2	558	2.72	1.2	.3	5.0	1.1	7	.1	.1	3.6	10	.18	.071	10	8.1	.95	297	.119	1	1.21	.093	.59	1.0	.01	11.4	.2	<.05	8	<.5	<.1	.01	1400
01122	16.1	15.2	2.0	114	.1	2.3	4.4	647	2.44	.9	.4	2.0	1.1	7	<.1	.1	.7	10	.14	.059	10	4.7	.79	233	.077	1	1.16	.076	.40	.9	<.01	9.5	.1	<.05	8	<.5	.1	<.01	1500
01123	3.5	396.5	12.1	7	4.0	1.8	.3	54	5.63	4.1	.2	1325.8	.4	1	<.1	2.4	246.4	5	.01	.053	1	9.7	.02	71	.005	<1	.39	.007	.23	1.0	.01	1.2	.1	<.05	2	9	5.9	2.82	1700
01124	.4	1052.4	6.2	135	84.9	4.5	3.3	1146	1.11	22.7	.3	6.0	.3	21	8.2	50.4	2.3	4	1.49	.015	2	4.9	.16	1423	.002	5	.39	.010	.19	1.3	1.71	3.2	.1	<.05	1	.6	83.3	.02	1400
01125	3.4	65.5	8.8	96	1.4	5.5	3.8	1065	1.48	4.8	.1	3.0	.1	41	9.2	14.3	1.2	5	1.82	.006	1	12.3	.26	1782	.002	2	.20	.013	.10	1.7	.06	3.3	<.1	.09	1	<.5	2.9	.01	1700
01126	.6	1535.0	6.7	220	84.5	2.1	1.1	393	.54	109.9	.4	6.0	.2	15	17.9	350.0	.5	2	.46	.023	3	6.1	.11	384	.002	5	.33	.030	.13	2.0	6.70	2.4	1	<.05	1	<.5	80.5	.01	1300
01127	1.4	27.0	15.4	84	.5	6.1	18.8	987	4.34	30.0	.1	3.0	.3	17	.1	1.8	.2	121	.48	.061	3	9.3	1.95	23	.154	1	2.27	.093	.03	.7	.05	5.5	.1	.43	9	<.5	2.7	<.01	1600
01128	.8	22.5	4.7	56	.7	4.7	16.9	1190	3.90	106.2	.1	1.1	.4	17	.1	1.5	.1	118	.27	.060	4	9.0	1.46	25	.119	2	2.14	.074	.11	.8	<.01	9.0	.1	.20	9	<.5	1.8	<.01	1400
01129	42.1	6.7	34.9	89	.2	2.3	4.2	176	4.44	731.4	.6	2.0	1.4	10	.2	4.8	.6	39	.18	.071	4	12.1	.08	15	.017	1	.66	.066	.09	1.9	.01	3.1	.3	2.26	5	.8	.5	<.01	1400
01130	2.2	16.7	8.3	35	.1	1.6	3.0	658	2.88	22.4	.6	.8	1.3	20	<.1	1.6	.2	17	.47	.097	9	5.4	.21	48	.140	1	.77	.092	.16	1.6	<.01	7.7	.3	.58	5	<.5	.9	<.01	1700
STANDARD DS5/R-2/AU-1	11.9	143.1	23.9	134	.3	24.7	12.0	768	2.94	17.7	5.6	39.6	2.5	49	5.7	3.3	6.0	58	.73	.095	12	183.3	.64	134	.094	17	2.04	.035	.14	4.8	.15	3.3	1.0	<.05	6	5.0	156.5	3.42	-

GROUP 1DX - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-MS.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
AG** & AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.
- SAMPLE TYPE: ROCK R150 60C   Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 22 2003 **DATE REPORT MAILED:** Aug 5/03 **SIGNED BY**.......... D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data FA

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Kodiak Exploration Ltd. File # A304170
704 - 525 Seymour St., Vancouver BC V6B 3H7 Submitted by: S. Wetherup

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Ag**	Au**	Sample
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	gm/mt	gm/mt	gm
SI	<1	1	<3	1	<.3	1	<1	3	.08	2	<8	<2	<2	3	<.5	<3	<3	<1	.11	<.001	<1	1	<.01	5	<.01	<3	.01	.49	.01	<2	<.3	.02	-
01131	<1	32	9	30	<.3	11	22	1961	7.07	7	<8	<2	<2	232	.5	<3	<3	22	12.07	.024	6	3	.66	127	<.01	<3	.36	.03	.07	<2	.8	.01	1000
01132	1	3	3	49	<.3	2	7	740	2.83	13	<8	<2	<2	126	<.5	<3	<3	43	4.06	.155	14	5	.63	57	<.01	<3	.69	.03	.13	<2	<.3	<.01	1100
01133	1	37	5	45	<.3	87	34	1479	6.72	3	<8	<2	<2	532	.6	13	<3	107	8.65	.098	6	68	3.27	82	<.01	<3	.65	.02	.04	<2	3.3	.01	1000
01134	<1	337	<3	42	<.3	187	41	1439	5.28	2	<8	<2	2	443	<.5	8	<3	123	5.76	.145	12	130	3.06	1006	<.01	<3	.79	.01	.05	<2	1.4	<.01	1100
01135	<1	16	4	24	<.3	7	6	2566	7.26	8	<8	<2	<2	619	.7	4	<3	33	13.03	.016	2	7	2.90	42	<.01	<3	.53	<.01	.02	<2	3.2	.01	1100
01136	<1	33	3	59	<.3	17	15	2003	3.67	9	<8	<2	<2	298	<.5	4	<3	43	8.72	.038	15	10	.64	42	<.01	<3	.73	.01	.02	<2	1.0	.01	1300
01137	<1	7	17	30	6.6	10	5	197	12.44	50	10	<2	<2	46	.5	29	<3	30	1.02	.025	1	6	.17	10	<.01	<3	.42	.01	.03	<2	6.0	.36	1200
01138	<1	25	19	44	3.2	7	2	2575	7.80	15	<8	<2	<2	189	.8	6	<3	21	9.64	.027	1	4	2.39	67	<.01	<3	.49	.01	.05	2	3.0	.01	1100
01139	<1	86	240	5027	7.5	3	4	3132	5.09	236	<8	<2	<2	430	42.4	6	<3	15	9.26	.011	4	<1	.54	35	<.01	<3	.98	.01	.02	<2	10.4	.26	1600
01140	<1	436	>9999	7025	>200	8	7	378	3.31	>9999	<8	<2	<2	13	62.1	632	<3	5	.33	.009	1	4	.11	19	<.01	<3	.18	.01	.04	2	847.4	.89	1400
																																	1200
																																	1000
																																	-
																																	1500
																																	1600
																																	2000
																																	1400
																																	2500
STANDARD	12	137	23	130	.3	24	12	747	2.82	18	<8	<2	3	47	5.3	3	7	58	.72	.092	12	177	.64	137	.09	17	1.99	.04	.11	4	155.9	3.33	-

Standard is STANDARD DS5/R-2/AU-1.

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
AG** & AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK R150 60C <u>Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.</u>

DATE RECEIVED: SEP 5 2003 DATE REPORT MAILED: Sep24/2003 SIGNED BY ....D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data___ FA ____

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Kodiak International Ltd. PROJECT 202 File # A302564 Page 1

704 - 525 Seymour St., Vancouver BC V6B 3H7 Submitted by: S. Wetherup

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga	Se	Ag**	Au**	Sample
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppb	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	ppm	ppm	ppm	%	ppm	ppm	gm/mt	gm/mt	gm
SI	.2	.6	.6	<1	<.1	.2	.1	5	.05	<.5	<.1	<.5	<.1	2	<.1	<.1	<.1	<1	.08	<.001	<1	1.1	<.01	2	<.001	<1	.01	.412	<.01	<.1	<.01	<.1	<.1	<.05	<1	<.5	<.3	<.01	-
C 158001	.2	92.4	11.5	99	1.3	17.0	17.6	1642	4.27	293.8	.1	78.6	.8	75	.7	.7	.1	15	2.34	.064	3	3.5	.87	59	<.001	2	.34	.022	.18	.2	.02	9.8	.1	.54	1	<.5	1.4	.14	2000
C 158002	.2	67.7	6.6	73	.7	17.5	19.1	1085	4.63	54.6	.1	3.8	1.1	90	.3	.3	.1	20	2.53	.073	7	6.7	1.27	52	<.001	4	.43	.031	.20	<.1	<.01	10.7	.1	<.05	1	<.5	<.3	.01	2800
C 158003	.2	73.1	103.9	152	1.0	15.8	17.2	1319	4.59	187.6	.1	30.9	1.0	87	1.1	.5	.1	18	2.56	.065	5	4.6	1.23	41	<.001	2	.39	.023	.19	<.1	.02	8.9	.1	.10	1	<.5	.8	.05	3300
C 158004	.4	74.7	43.0	104	1.0	14.0	16.4	1343	4.69	214.3	.1	26.7	1.2	86	.7	.4	.2	15	2.67	.072	5	3.9	1.27	38	<.001	3	.40	.028	.21	<.1	.03	9.3	.1	.15	1	<.5	.6	.09	2500
C 158005	.7	58.5	11.3	83	.8	13.6	16.7	1042	4.57	42.3	.2	1.1	1.0	92	.4	.4	.1	12	2.38	.069	6	2.7	1.26	33	<.001	1	.33	.013	.19	<.1	.01	10.0	.1	.06	1	.6	6	.01	3500
C 158006	2.0	46.5	21.7	41	1.1	15.4	20.0	1228	4.62	123.9	.2	17.3	1.1	90	.3	1.2	.1	11	2.61	.087	3	2.4	1.07	33	<.001	2	.36	.025	.20	.2	.01	8.0	.1	.67	1	1.7	1.6	.06	3000
C 158007	2.2	93.2	124.2	1149	1.5	11.1	16.8	1239	4.26	94.3	.1	29.3	1.2	92	15.5	1.0	.1	14	2.91	.156	6	3.4	1.13	34	<.001	1	.44	.031	.21	21.0	.24	8.6	.1	.29	1	.5	1.4	.10	3000
C 158008	1.2	78.2	303.7	148	2.5	10.0	14.0	1901	3.98	338.4	.1	143.1	.8	91	2.0	1.6	.1	9	3.35	.054	3	2.4	.97	25	<.001	2	.29	.022	.18	.8	.03	9.4	.1	.90	1	.7	2.3	.23	2900
C 158009	1.8	62.4	85.4	41	1.8	14.6	17.5	2342	3.93	317.4	.2	36.8	1.1	103	.4	3.4	.1	13	3.81	.060	3	2.0	.99	28	<.001	2	.33	.022	.19	1.0	.01	9.9	.1	.87	1	.6	1.5	.17	3500
C 158010	.4	73.7	10.6	37	.5	15.3	16.6	1575	4.17	108.5	.1	85.5	.8	73	.3	.5	.1	12	2.43	.049	5	3.1	1.03	37	<.001	3	.33	.022	.20	.7	<.01	9.7	.1	.29	1	.5	.4	.22	900
C 158011	.3	79.5	8.2	44	.7	14.7	16.9	1424	4.13	130.9	.1	30.1	.8	98	.3	.6	.1	11	2.51	.052	6	2.9	1.04	41	.001	2	.34	.019	.21	.7	<.01	9.3	.1	<.05	1	.5	.8	.14	3000
C 158012	.4	103.8	27.8	59	1.0	14.7	17.1	1913	3.88	225.1	.1	71.0	.6	87	.6	.8	.1	10	2.67	.039	4	2.6	.96	39	.001	2	.33	.016	.22	.9	<.01	8.8	.1	.61	1	.5	.9	.37	3000
C 158013	.4	79.5	32.4	97	1.0	14.7	16.8	1334	4.53	131.6	.1	46.9	.7	99	.9	.6	.1	16	2.66	.056	4	2.7	1.00	43	<.001	2	.37	.020	.22	.4	.01	10.8	.1	.42	1	.9	.7	.21	3500
C 158014	.6	67.7	11.0	31	.9	18.7	21.8	1514	4.22	147.9	.1	6.0	1.0	98	.2	.7	.1	14	2.92	.050	5	2.9	1.01	45	<.001	1	.35	.018	.22	.9	<.01	10.6	.1	.32	1	.5	.6	06	4000
C 158015	.7	71.2	9.3	48	.6	18.4	21.6	1163	4.44	81.2	.1	2.4	.9	104	.4	.5	.1	12	2.71	.065	6	3.2	1.07	48	<.001	1	.34	.026	.22	.6	<.01	9.4	.1	.20	1	.8	<.3	.03	3500
C 158016	.2	86.9	15.1	45	.6	11.9	14.3	1361	3.68	113.0	.1	1.9	.5	90	.3	.7	.1	9	2.98	.036	4	1.9	.98	63	<.001	2	.32	.021	.22	.6	.01	8.7	.1	.33	1	.6	.6	.05	3200
C 158017	1.0	94.2	40.3	58	.9	16.1	18.6	1201	2.88	361.4	.1	14.9	.6	87	.5	.6	.1	9	2.48	.056	3	1.6	.67	43	<.001	1	.30	.017	.20	.7	<.01	8.6	<.1	.99	1	.6	.9	.30	3000
C 158018	2.2	57.4	41.3	25	1.2	10.6	12.8	1602	3.65	193.8	.1	18.8	.6	157	.2	.9	.1	12	3.84	.056	3	2.7	.98	31	<.001	2	.31	.019	.17	.6	<.01	9.2	.1	.76	1	.5	.9	10	4000
C 158019	2.8	55.6	16.5	68	.6	11.1	14.3	1170	3.53	77.8	.1	4.0	.6	127	.6	.5	.1	9	3.21	.044	4	1.7	.89	28	<.001	1	.28	.020	.16	.4	.02	7.6	<.1	.24	1	<.5	.5	06	3500
C 158020	2.4	51.4	9.5	23	.5	13.2	16.0	1218	3.79	101.3	.1	2.4	.6	139	.2	.3	.1	15	3.28	.042	5	3.6	.97	33	<.001	1	.32	.021	.16	.6	<.01	8.2	.1	.24	1	<.5	.4	.02	4100
RE C 158020	2.9	52.1	9.5	20	.5	12.0	14.8	1225	3.82	96.6	.1	1.7	.7	139	.1	.3	.1	15	3.29	.039	5	3.1	.97	32	<.001	3	.32	.024	.18	.6	<.01	8.9	.1	.19	1	<.5	.4	.02	-
RRE C 158020	2.6	53.8	13.6	20	.4	12.4	15.6	1212	3.83	101.1	.1	4.8	.7	137	.1	.3	.1	14	3.27	.045	5	2.8	.97	34	<.001	<1	.32	.024	.16	.6	<.01	8.7	.1	.19	1	<.5	.6	.03	-
C 158021	1.1	80.5	71.0	90	2.5	11.5	14.6	1507	4.10	489.6	.1	11.8	.7	155	.7	1.8	.1	13	3.80	.048	4	2.9	1.06	36	<.001	2	.33	.022	.18	.5	<.01	8.6	.1	.63	1	.5	2.3	.22	3500
C 158022	.7	55.7	6.9	25	.6	14.8	17.5	1355	4.22	82.5	.1	4.9	.8	141	.2	.5	.1	11	3.23	.042	5	1.8	1.06	47	<.001	2	.32	.028	.20	.4	<.01	8.5	.1	.22	1	<.5	.5	.04	4000
C 158023	.8	52.5	4.2	27	.4	15.8	19.6	1119	4.17	61.7	.1	3.7	.8	142	.2	.2	.1	8	2.94	.052	5	2.9	1.06	42	<.001	2	.33	.028	.19	.1	<.01	7.2	.1	.30	1	<.5	< 3	.01	3500
C 158024	.3	52.4	4.2	24	.4	11.9	14.9	1186	4.20	55.1	.1	9.3	1.1	143	.2	.2	.1	11	3.04	.063	5	2.4	1.04	42	<.001	1	.35	.024	.19	.3	<.01	7.5	.1	.21	1	<.5	.3	.04	2800
C 158025	.9	55.2	3.3	34	.4	16.2	20.0	1264	4.53	51.8	.1	<.5	1.0	137	.2	.2	.1	10	2.66	.047	7	3.4	1.10	40	<.001	1	.31	.023	.20	.4	<.01	8.3	.1	<.05	1	<.5	<.3	<.01	2500
C 158026	1.2	81.0	38.5	111	1.3	18.3	19.6	1144	4.27	91.0	.1	17.7	.7	234	.4	.6	.1	33	3.27	.062	5	5.9	.86	53	.001	1	1.79	.026	.19	.2	.02	9.8	.1	.53	4	.9	1.0	.02	2000
C 158027	.2	83.1	13.4	113	1.1	18.0	18.2	783	4.88	47.7	.1	.8	.7	156	.4	.3	.2	33	1.69	.063	6	8.4	1.04	81	<.001	<1	2.03	.025	.18	.2	.01	10.2	.1	.34	5	.5	.9	.01	1900
C 158028	.7	90.8	7.5	88	1.5	18.3	20.5	669	4.85	140.4	.1	3.5	.7	130	.2	.7	.1	41	1.11	.090	5	9.5	1.07	56	<.001	1	2.18	.033	.19	.2	<.01	7.7	.1	.40	4	.7	1.7	.02	1900
C 158029	.8	79.3	8.1	95	1.3	19.2	22.5	1636	5.01	41.2	.1	1.3	.7	240	.2	.7	.1	39	3.99	.055	7	8.3	1.02	54	<.001	<1	2.16	.022	.17	.2	.01	8.2	.1	.31	5	.6	.9	.01	2500
C 158030	.4	67.1	12.0	83	1.0	15.5	19.3	1009	4.88	43.2	.1	4.9	.8	219	.2	.4	.1	40	2.81	.081	6	6.7	1.07	53	<.001	1	2.18	.030	.16	.2	<.01	9.4	.1	.32	5	.9	1.1	21	3500
C 158031	.6	62.8	5.4	70	.8	15.4	18.8	969	4.54	48.8	.1	6.8	.8	229	.1	.3	.1	41	2.98	.086	6	8.4	.95	47	<.001	<1	2.00	.037	.17	.1	<.01	10.0	.1	.37	4	.6	.6	.02	3000
C 158032	.4	63.6	5.2	84	.8	14.8	19.9	1121	6.08	56.5	<.1	12.9	.6	245	.3	.3	.1	49	2.98	.057	5	8.3	1.07	54	<.001	1	2.22	.034	.17	.1	.01	10.2	.1	.24	5	.5	.9	.11	3200
STANDARD DS5/R-2/AU-1	12.4	141.7	24.2	138	.3	24.4	11.9	792	3.00	18.1	5.6	43.6	2.5	52	5.4	3.6	6.4	61	.78	.093	12	186.7	.68	139	.099	16	2.10	.034	.17	4.4	.16	3.5	1.0	<.05	6	5.1	156.7	3.32	-

GROUP 1DX - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-MS.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
AG** & AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.
- SAMPLE TYPE: CORE R150 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 14 2003 **DATE REPORT MAILED:** July 29/03 **SIGNED BY**..........D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ✓ FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Ag** gm/mt	Au** gm/mt	Sample gm
C 158033	1.0	42.3	29.5	81	1.0	15.1	18.4	1129	4.41	76.8	.1	5.1	.6	187	.3	.7	.1	41	2.77	.097	4	6.3	.90	41	.001	1	1.80	.038	.12	.2	.01	8.4	.1	.56	3	.5	1.2	.03	2500
C 158034	1.2	68.7	72.7	192	2.0	14.0	16.2	1014	4.66	47.1	.1	39.2	.7	142	1.2	.8	.1	37	1.57	.055	6	6.6	1.04	58	<.001	1	2.14	.031	.15	.1	.01	9.1	.1	.21	4	.8	2.8	.17	2800
C 158035	1.6	52.4	8.9	89	.9	11.8	16.8	919	4.53	30.5	.1	4.1	.8	176	.3	.6	.1	41	2.53	.156	7	6.8	1.03	63	<.001	<1	2.10	.037	.13	.3	.01	9.0	.1	.25	4	.5	1.0	.02	3000
C 158036	.8	41.7	13.3	89	.7	14.3	20.3	1305	4.45	29.3	.1	4.6	.8	249	.1	1.2	<.1	57	3.85	.069	7	10.7	1.24	51	<.001	<1	2.29	.036	.08	.1	.01	10.0	.1	.17	5	<.5	1.3	.01	3300
C 158037	.5	38.7	5.8	76	.6	15.2	19.3	1279	4.73	29.4	.1	1.0	.8	214	.1	.8	<.1	61	3.29	.082	8	11.7	1.59	51	<.001	<1	2.67	.029	.08	.1	<.01	8.1	.1	.19	5	<.5	.8	.01	3500
C 158038	.4	65.1	6.4	89	.8	14.6	18.7	859	5.17	41.9	.1	2.9	.7	158	.2	.5	.1	32	2.34	.119	6	5.3	1.07	57	<.001	<1	2.12	.017	.16	.3	<.01	11.6	.1	.50	4	<.5	1.0	.10	4000
C 158039	.9	46.7	5.2	91	.2	16.7	16.2	1033	4.87	39.4	.2	<.5	1.0	69	.4	.7	<.1	30	2.49	.084	7	7.4	1.02	37	<.001	<1	1.67	.025	.15	.2	.01	9.9	.1	.19	3	<.5	.8	<.01	1300
C 158040	.8	64.2	18.4	60	1.2	15.3	18.4	1076	4.02	42.9	.1	<.5	.8	77	.2	1.2	.1	18	2.15	.067	6	4.1	.86	64	<.001	<1	1.39	.025	.15	.2	.01	11.2	.1	<.05	2	<.5	1.7	.01	2500
C 158041	.5	49.2	9.3	57	.7	11.6	15.1	1105	4.68	46.8	.1	.8	.8	113	.3	.4	.1	23	2.09	.060	6	5.9	.96	46	.001	1	1.83	.019	.17	.2	.01	9.5	.1	.13	3	<.5	1.4	.04	3700
C 158042	.1	2.4	20.8	42	.3	<.1	4.9	1583	2.29	17.0	.2	9.7	1.3	162	.2	.2	<.1	5	3.39	.076	9	<1	.62	43	<.001	<1	.96	.014	.20	.2	<.01	2.3	.1	.46	2	<.5	.8	.02	3000
C 158043	4.6	18.2	7.2	50	.3	4.0	7.3	1217	2.96	15.0	.2	3.0	1.1	158	.2	.2	<.1	18	2.58	.071	9	5.2	.74	42	<.001	1	1.43	.024	.20	.1	.01	4.2	.1	.20	3	<.5	.9	.02	2100
C 158044	.3	65.1	6.1	87	.1	18.9	19.9	1056	5.27	6.8	.1	<.5	.8	145	.1	.1	<.1	54	2.17	.075	7	18.9	1.21	48	.001	<1	2.35	.050	.13	.1	.01	12.0	.1	.15	7	<.5	.8	.01	4000
C 158045	.5	61.6	3.7	83	.1	18.8	19.9	1264	5.64	11.3	.1	<.5	.8	128	.1	.2	<.1	58	2.18	.067	8	20.0	1.36	49	<.001	<1	2.40	.058	.12	.1	<.01	13.0	.1	<.05	6	<.5	<.3	.01	2500
C 158046	.8	57.9	4.7	85	.3	21.0	21.5	1128	6.46	23.9	.1	.8	.9	135	.1	.5	<.1	62	1.62	.090	7	20.4	1.34	51	<.001	<1	2.67	.040	.11	.2	<.01	12.8	.1	.21	7	.5	.7	<.01	2000
C 158047	.7	57.1	6.7	74	.2	17.8	18.5	1341	4.91	23.8	.1	<.5	.7	152	.1	.6	<.1	44	2.48	.069	6	14.0	1.16	50	<.001	<1	2.03	.051	.12	.1	<.01	11.8	.1	<.05	4	<.5	.5	.01	2500
C 158048	.8	48.4	27.2	129	.2	18.2	18.6	1871	5.20	28.5	.1	<.5	.7	176	.2	.4	<.1	45	4.70	.077	6	15.8	1.35	42	<.001	<1	1.66	.038	.12	.1	.01	11.8	.1	.15	4	.6	<.3	.01	3500
C 158049	1.5	43.8	88.9	139	1.2	15.8	17.0	1920	4.72	175.0	.2	91.2	.9	129	1.3	1.1	<.1	26	2.64	.115	4	7.5	1.20	51	.001	<1	1.74	.020	.13	.3	.01	7.5	.1	.42	3	<.5	1.7	.21	2500
C 158050	.7	33.8	9.7	71	.4	12.8	17.6	1512	4.52	43.4	.2	3.5	1.0	130	.2	1.0	<.1	28	2.55	.083	6	5.3	1.31	54	.001	<1	1.70	.027	.14	.3	.01	8.2	.1	<.05	3	<.5	1.0	.01	3000
RE C 158050	.8	37.4	11.2	79	.5	16.5	19.7	1574	4.74	40.4	.2	1.7	.9	128	.3	1.0	<.1	28	2.66	.096	6	6.0	1.37	57	.001	<1	1.80	.031	.13	.3	<.01	8.1	.1	.12	3	<.5	1.0	.01	-
RRE C 158050	1.0	36.5	11.9	81	.5	15.1	19.4	1496	4.67	45.0	.2	2.8	.9	125	.3	1.0	<.1	29	2.55	.091	6	6.7	1.36	51	.001	<1	1.80	.027	.13	.2	<.01	7.7	.1	<.05	3	<.5	.9	.01	-
C 158051	.6	33.8	17.3	129	.4	14.2	18.6	1596	4.08	43.0	.1	18.5	.8	130	.8	1.2	<.1	18	3.03	.071	5	4.0	1.27	61	<.001	1	1.12	.037	.14	.2	.01	9.2	.1	<.05	2	<.5	.7	.02	3300
C 158052	.9	56.4	18.2	90	1.5	18.6	22.5	1947	4.51	114.6	.1	56.9	.8	107	.5	2.8	<.1	25	2.82	.086	4	5.8	1.25	46	<.001	1	1.29	.019	.15	.2	<.01	7.9	.1	.48	3	<.5	2.1	.12	3200
C 158053	1.2	26.3	11.9	94	.8	12.8	20.0	1657	4.69	39.1	.1	2.2	.6	201	.2	1.6	<.1	33	4.07	.041	4	5.4	.93	40	<.001	<1	1.64	.029	.12	.1	.01	10.6	.1	.25	3	<.5	1.3	.01	3100
C 158054	1.0	65.2	3.3	68	.4	18.5	22.6	969	5.02	32.5	.1	<.5	.8	141	.1	.4	<.1	47	2.05	.072	7	12.5	1.09	78	<.001	<1	2.40	.025	.14	.1	.01	9.6	.1	.08	5	<.5	.5	.02	2500
C 158055	.6	41.8	9.8	93	.2	20.9	19.2	3150	4.34	14.5	.2	<.5	.7	188	.2	.6	<.1	48	8.21	.077	7	15.8	1.02	45	<.001	<1	1.57	.028	.13	.1	<.01	10.0	.1	.06	4	<.5	.3	.01	3200
C 158056	3.6	65.5	28.7	117	3.9	16.0	19.3	947	4.35	51.4	.1	<.5	.6	139	.5	1.2	.1	20	3.00	.048	5	4.7	.87	51	.001	1	1.22	.021	.16	.2	.01	10.9	.1	.13	2	<.5	4.7	.01	3000
C 158057	.4	50.0	7.4	88	.5	12.8	13.7	702	4.64	10.2	.1	<.5	.8	140	.2	.5	<.1	48	1.66	.045	7	11.9	1.06	36	.001	1	2.28	.033	.11	.1	.01	8.5	.1	.10	6	<.5	1.2	.01	2500
C 158058	.3	61.4	5.0	89	.1	14.7	17.1	803	5.19	3.8	.1	<.5	.7	141	.2	.3	<.1	47	1.90	.041	8	13.4	1.14	49	.001	1	2.42	.034	.11	.1	<.01	10.8	.1	<.05	7	<.5	.5	.01	3000
C 158059	.3	62.9	3.8	97	.3	22.4	20.9	1305	5.09	6.7	.1	<.5	.7	207	.1	.3	<.1	53	3.32	.053	6	18.4	1.07	154	.001	<1	2.47	.031	.11	.1	<.01	10.0	.1	<.05	8	.5	.4	.01	1000
C 158060	1.3	26.0	18.3	101	.2	11.5	16.5	2379	4.46	29.9	.1	<.5	.7	182	.4	.8	<.1	31	5.84	.049	4	4.8	.83	45	<.001	1	1.08	.028	.11	.1	<.01	10.7	.1	.10	2	<.5	.7	.01	3200
C 158061	2.4	31.3	7.1	104	.3	12.2	20.5	1587	4.98	30.5	.2	<.5	.9	169	.1	.8	<.1	61	3.94	.065	4	12.5	.80	58	<.001	<1	1.79	.036	.10	.1	.01	10.4	.1	.15	3	<.5	.5	.01	2300
C 158062	4.3	27.6	4.1	93	.2	12.1	17.5	957	4.92	26.8	.2	<.5	.8	166	.2	.3	<.1	72	2.40	.073	5	17.0	.91	43	.001	<1	2.08	.037	.10	.1	.01	10.1	.1	.10	5	<.5	.3	.01	2500
C 158063	.7	30.7	2.9	89	.3	13.2	16.3	966	5.76	21.1	.1	<.5	.7	195	.1	.2	<.1	84	2.29	.068	4	15.8	.95	39	.001	1	2.59	.039	.10	.1	<.01	10.1	.1	.17	8	<.5	<.3	.01	2800
C 158064	.9	42.4	4.5	82	.3	13.0	14.8	1077	4.44	25.6	.1	<.5	1.0	131	.3	.1	<.1	39	2.48	.102	8	8.0	.86	106	<.001	<1	1.87	.049	.11	.1	<.01	10.3	.1	.14	3	<.5	.7	.01	1900
STANDARD DS5	13.2	149.6	25.0	139	.3	25.7	12.0	814	3.02	18.1	5.9	39.0	2.3	52	5.6	3.7	6.2	61	.77	.091	13	182.8	.68	146	.098	19	2.05	.039	.14	4.8	.18	3.6	1.2	<.05	7	4.8	155.5	3.28	-

Standard is STANDARD DS5/R-2/AU-1. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Ag** gm/mt	Au** gm/mt	Sample gm
C 158065	.7	56.4	8.8	84	.5	17.3	21.5	932	5.96	37.5	.1	<.5	1.0	120	.3	.1	.1	44	1.83	.104	11	7.0	1.25	49	.001	<1	2.73	.039	.15	.2	<.01	11.7	.1	<.05	5	<.5	.4	<.01	2500
C 158066	1.0	37.1	17.6	67	.8	12.8	18.4	1065	4.98	44.2	.1	<.5	.9	117	.3	.2	<.1	25	3.06	.107	6	5.4	1.03	36	<.001	1	1.57	.031	.13	.2	<.01	11.5	.1	.25	2	<.5	.7	.01	1400
C 158067	1.3	46.9	9.5	59	.6	17.3	21.5	798	5.04	54.6	.1	.7	1.2	74	.2	.2	.1	42	1.45	.079	11	8.7	1.15	41	<.001	1	2.23	.026	.15	.3	<.01	11.2	.1	<.05	4	<.5	.7	.01	1100
C 158068	.6	48.5	5.9	73	.4	16.9	18.6	1026	4.94	51.0	.2	.6	1.3	90	.2	.4	<.1	26	2.31	.099	8	9.6	1.31	48	<.001	<1	.91	.039	.15	.2	.01	11.4	.1	.08	2	.7	.5	<.01	3000
C 158069	.3	48.8	20.0	106	.5	17.7	19.6	1484	4.30	65.3	.1	3.2	1.0	110	.6	.6	.1	21	3.20	.064	6	5.0	1.26	44	<.001	<1	.91	.021	.15	.2	.01	10.7	.1	.13	1	<.5	.7	<.01	2800
C 158070	.6	41.9	42.4	94	.4	17.4	18.1	1764	3.55	47.7	.1	<.5	.8	163	.3	.3	<.1	22	5.49	.078	6	6.5	1.07	32	<.001	<1	.61	.043	.10	.2	<.01	11.0	<.1	.11	1	<.5	.4	<.01	3200
C 158071	.3	48.9	6.9	71	.3	17.0	17.9	987	3.91	32.3	.1	1.7	.8	102	.1	.3	<.1	25	2.92	.073	6	7.3	1.02	57	<.001	1	1.03	.053	.11	.1	<.01	9.7	.1	.08	2	<.5	.6	<.01	2500
C 158072	.9	36.9	17.6	57	.5	11.0	15.9	962	4.42	58.6	.1	<.5	.6	99	.2	.3	<.1	28	2.53	.045	3	5.2	1.13	43	<.001	2	1.33	.022	.17	.2	<.01	12.1	.1	.16	2	.9	.7	.01	2000
C 158073	.3	62.5	10.5	90	1.1	14.6	23.0	579	5.02	44.5	.1	1.5	.9	48	.4	.9	.1	35	.97	.114	9	6.4	1.10	40	<.001	2	2.13	.023	.17	.3	<.01	12.0	.1	<.05	4	.5	.8	<.01	3000
C 158074	.5	48.4	8.5	82	.4	14.7	21.7	752	5.36	44.5	.1	<.5	1.2	70	.2	.4	.1	37	1.46	.081	7	7.5	1.17	43	<.001	2	1.97	.026	.20	.2	.01	14.3	.1	.11	3	.5	.3	<.01	2500
C 158075	.3	71.2	7.2	93	.4	16.5	24.0	817	4.99	48.3	.1	.6	.7	87	.2	.8	.1	26	1.44	.053	5	4.4	1.01	64	<.001	<1	1.30	.031	.21	.1	.01	11.1	.1	.11	2	.5	.4	<.01	2200
C 158076	.4	72.4	33.4	132	1.1	15.4	19.1	967	5.14	49.4	.1	69.1	.6	81	.5	.5	.1	27	1.72	.044	3	5.9	1.08	54	<.001	2	1.55	.022	.15	.3	.02	11.0	.1	.55	3	.7	1.2	.22	2600
C 158077	1.4	60.1	8.4	80	.4	14.3	23.0	863	4.60	49.8	.1	1.1	.9	82	.4	.5	.1	27	1.97	.090	4	4.2	1.03	36	<.001	1	1.67	.025	.17	.3	.01	10.7	.1	.09	3	<.5	.4	<.01	2600
C 158078	2.2	41.7	16.2	122	.6	11.8	17.4	1198	4.45	338.6	.1	7.5	.5	108	.8	.7	<.1	23	2.84	.050	4	4.6	1.12	29	<.001	1	1.24	.023	.14	.4	.17	10.0	.1	.09	3	<.5	.7	.02	3000
RE C 158078	2.0	39.3	16.1	119	.6	12.0	18.1	1175	4.36	332.3	.1	7.8	.5	107	.9	.7	<.1	22	2.77	.055	4	5.2	1.10	27	<.001	<1	1.23	.023	.12	.3	.17	9.5	.1	.09	2	.6	.6	.03	-
RRE C 158078	1.2	36.4	11.7	78	.6	10.7	17.6	1278	4.36	247.9	.1	5.6	.7	115	.6	.9	<.1	22	2.89	.052	4	2.5	1.10	31	<.001	<1	1.19	.022	.14	.4	.07	10.5	.1	.10	2	.5	.5	.02	-
C 158079	.8	31.7	126.7	202	1.5	12.2	17.6	1682	3.75	44.3	.1	.6	.8	103	2.0	.8	<.1	14	3.51	.103	7	3.7	.92	26	<.001	1	.55	.024	.13	.4	.02	8.4	.1	.09	1	<.5	1.1	<.01	2500
C 158080	.3	89.4	6.9	73	1.0	18.3	19.0	1116	4.50	288.7	.1	10.7	.6	92	.5	.5	.1	16	2.62	.071	4	3.2	.99	39	<.001	1	.92	.021	.18	.3	.02	10.5	.1	.31	2	.7	.9	.03	1800
C 158081	.5	81.5	37.9	643	1.4	16.0	23.8	1343	4.37	762.8	.1	192.6	.6	84	8.1	.5	<.1	17	2.24	.031	4	3.9	.84	36	<.001	1	.96	.018	.16	.4	.06	10.7	.1	.98	2	.5	1.6	.45	2500
C 158082	.3	74.6	3.9	77	.7	13.9	19.8	1029	4.85	50.0	.1	4.9	.9	99	.4	.1	<.1	19	2.47	.071	9	4.1	1.09	40	<.001	<1	1.03	.022	.21	.2	.01	12.3	.1	.06	2	<.5	.8	<.01	3300
C 158083	.6	66.1	3.7	84	.7	18.9	23.5	834	4.70	62.7	.1	<.5	.9	97	.2	.3	<.1	26	2.18	.066	11	6.0	1.05	45	<.001	1	1.58	.023	.20	.2	<.01	12.1	.1	<.05	3	.7	.6	<.01	2500
C 158084	.7	55.6	2.6	46	.4	12.7	14.4	1068	4.28	44.9	.1	<.5	1.1	69	.3	.2	<.1	19	2.52	.134	8	4.3	.86	46	<.001	1	.54	.032	.21	.2	<.01	10.9	.1	<.05	1	.6	.3	<.01	2500
C 158085	.5	57.7	2.4	63	.4	14.2	17.3	1018	4.62	43.7	.1	.7	1.0	67	.4	.2	<.1	17	2.52	.124	8	4.3	1.04	41	<.001	1	.45	.032	.16	.2	<.01	10.1	.1	<.05	1	<.5	<.3	<.01	3500
C 158086	.9	57.7	3.1	80	.3	15.3	18.1	992	4.44	44.6	.1	<.5	1.0	76	.4	.2	<.1	16	2.25	.096	8	4.2	.98	47	<.001	1	.50	.037	.22	.3	.01	11.4	.1	<.05	1	<.5	.4	<.01	4500
C 158087	.7	41.4	13.0	53	.7	19.8	17.8	1056	4.26	48.1	.2	<.5	1.2	85	.3	.4	<.1	28	2.64	.069	7	6.2	.92	37	<.001	<1	.44	.020	.14	.3	.02	8.7	.1	.08	1	<.5	.5	<.01	3000
C 158088	1.1	65.9	27.2	175	.8	15.8	19.2	1032	4.26	44.5	.1	3.4	1.2	97	1.6	.2	<.1	20	2.35	.097	6	5.8	.92	45	<.001	<1	.55	.032	.23	.4	.01	11.1	.1	.18	1	.5	.5	.02	3500
C 158089	.5	61.7	5.7	75	.8	16.5	18.8	1001	3.59	50.1	.1	<.5	1.0	97	.4	.4	<.1	15	2.76	.083	6	3.5	.92	32	<.001	1	.40	.023	.16	.1	<.01	9.9	.1	.08	1	<.5	.6	<.01	3000
C 158090	.8	68.3	4.4	79	.9	14.8	17.1	1061	4.36	46.5	.1	1.1	1.2	106	.3	.5	<.1	20	2.59	.082	5	3.1	.94	37	<.001	<1	.46	.025	.19	.3	<.01	11.5	.1	.34	1	<.5	.7	<.01	4000
C 158091	1.0	70.0	4.4	46	4.8	13.9	17.9	1305	4.06	49.4	.1	<.5	1.4	114	.4	2.0	.1	14	2.93	.160	8	2.2	1.00	41	<.001	1	.47	.025	.22	.2	<.01	11.3	.1	.09	1	<.5	5.8	<.01	4000
C 158092	.7	76.0	6.9	66	1.0	12.9	14.5	1236	3.74	50.1	.1	3.3	.8	102	.3	.4	<.1	12	2.67	.105	4	3.2	.89	41	<.001	<1	.43	.023	.20	.5	<.01	9.2	.1	.24	1	.6	1.1	.03	3700
C 158093	.6	58.8	19.0	108	1.1	15.0	13.0	1046	3.49	47.3	.1	1.7	.9	112	.7	.4	.2	11	2.61	.063	5	3.1	.83	41	<.001	1	.46	.024	.22	.2	<.01	8.2	.1	.10	1	<.5	.9	.01	4100
C 158094	2.6	88.0	33.9	62	2.0	16.8	20.0	1549	3.10	139.9	.1	7.4	.7	111	.5	.5	.3	9	2.79	.056	3	3.8	.75	45	<.001	1	.42	.020	.24	.5	.01	6.9	.1	.58	1	<.5	1.6	.19	2000
C 158095	.7	35.6	24.2	71	.8	14.2	14.6	1260	3.88	64.3	.1	<.5	.9	148	.4	.3	<.1	17	3.34	.083	5	4.1	1.09	38	<.001	1	.48	.029	.19	.5	<.01	9.1	.1	.25	1	<.5	.6	.01	3900
C 158096	1.0	50.1	26.9	111	4.2	14.0	15.6	1151	4.24	43.2	.1	<.5	1.1	125	.7	1.9	<.1	15	3.26	.069	7	4.8	1.02	46	<.001	2	.76	.028	.24	.3	.01	9.8	.1	.06	1	<.5	4.0	<.01	1600
STANDARD DS5	13.1	144.4	25.1	137	.3	24.4	12.1	786	3.01	18.4	5.7	40.1	2.6	51	5.5	3.4	6.0	59	.75	.098	12	190.5	.68	141	.092	16	2.12	.035	.15	4.7	.18	3.8	1.1	<.05	7	4.9	155.2	3.33	-

Standard is STANDARD DS5/R-2/AU-1. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ___ FA ___

ACME ANALYTICAL

Kodiak International Ltd. PROJECT 202 FILE # A302564

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Ag** gm/mt	Au** gm/mt	Sample gm
C 158097	.7	41.1	7.7	96	.2	15.3	17.5	1262	5.96	29.5	.2	.9	1.3	118	.1	.7	<.1	63	2.50	.125	6	16.6	1.30	41	.001	2	1.87	.063	.16	.4	.01	12.4	.1	<.05	4	<.5	<.3	<.01	2800
C 158098	1.3	76.3	28.8	98	1.4	18.3	21.1	1211	4.64	62.6	.1	.9	.9	120	.6	.8	.1	17	2.71	.105	6	5.3	1.10	57	<.001	1	.69	.050	.27	.4	.01	9.7	.1	.24	1	<.5	1.7	.03	3700
C 158099	.6	48.0	12.3	92	.3	15.7	18.0	1022	4.97	45.9	.1	<.5	.8	114	.4	.5	<.1	19	2.72	.095	3	4.8	1.08	47	<.001	2	.62	.051	.22	.4	.01	10.3	.1	.09	1	<.5	<.3	<.01	3800
C 158100	1.2	50.5	11.7	65	.9	15.6	17.6	1240	4.34	49.3	.1	2.3	.6	128	.4	.9	<.1	17	3.06	.075	3	5.5	.99	45	<.001	2	.54	.037	.21	.5	.01	9.0	.1	.08	1	<.5	.9	.01	3400
C 158101	.7	63.9	3.0	36	.6	17.5	21.4	1209	5.36	54.7	.1	.7	1.0	78	.1	.5	<.1	17	2.01	.068	7	4.3	1.04	41	<.001	1	.55	.028	.24	.3	<.01	11.8	.1	<.05	1	<.5	.5	<.01	3700
C 158102	1.3	63.0	9.2	22	1.4	18.4	18.8	1775	4.93	319.9	.1	39.5	.6	101	.2	.8	<.1	17	2.51	.078	3	4.7	.91	49	<.001	1	.72	.027	.24	.7	<.01	9.8	.1	1.18	2	.5	1.1	.33	2900
C 158103	.9	87.5	22.2	94	2.7	16.5	19.3	1307	5.15	182.0	.1	46.2	.5	151	.7	1.1	<.1	22	2.44	.060	4	4.0	.94	54	<.001	1	.92	.021	.21	.5	.02	10.3	.1	.88	2	.5	2.4	.35	2900
C 158104	.8	63.5	3.4	64	.6	16.1	18.2	1009	4.56	92.6	<.1	1.8	.8	110	.5	.4	<.1	17	2.02	.076	6	3.8	.89	43	<.001	1	.57	.022	.23	.4	<.01	10.4	.1	.21	1	<.5	.9	.02	2800
C 158105	.7	98.7	5.1	25	3.7	15.0	18.8	1794	4.42	229.4	.1	45.4	.7	131	.2	1.7	<.1	17	2.84	.076	4	3.1	.92	45	<.001	1	.75	.020	.24	.3	.01	11.9	.1	.62	2	<.5	3.0	.32	2100
C 158106	.8	71.8	3.8	61	.5	19.7	26.3	808	4.95	64.2	.1	1.0	1.0	92	.2	.3	.1	15	1.94	.068	8	3.5	.98	59	<.001	1	.62	.028	.24	.2	.01	12.3	.1	<.05	2	<.5	.6	.01	1600
C 158107	.5	67.9	5.0	97	.5	17.4	19.7	752	4.63	45.4	.1	<.5	.9	77	.1	.2	<.1	21	2.12	.076	6	4.9	.93	57	.001	<1	.99	.021	.22	.1	<.01	10.9	.1	.19	2	<.5	.7	<.01	3200
C 158108	.6	68.0	4.3	87	.3	18.2	25.4	904	5.05	44.6	.1	<.5	1.0	107	.2	.3	<.1	33	2.55	.103	7	10.4	1.04	60	.001	2	1.74	.028	.25	.2	.01	13.4	.1	<.05	4	<.5	<.3	<.01	3400
C 158109	.6	55.3	6.1	57	.4	15.9	18.1	943	4.99	45.0	.1	<.5	.8	159	.1	.1	<.1	41	2.35	.072	5	11.6	.97	50	.001	1	2.01	.024	.18	.1	<.01	10.7	.1	.27	5	<.5	.7	.01	3500
C 158110	3.0	49.5	11.5	90	.3	20.0	22.1	1109	5.28	35.3	.2	1.0	1.2	126	.1	.4	<.1	76	2.96	.079	8	26.9	1.04	62	.002	<1	1.80	.041	.17	.2	.01	10.7	.1	<.05	5	<.5	<.3	<.01	3300
RE C 158110	3.2	52.2	9.2	93	.3	22.4	23.6	1106	5.26	36.2	.2	<.5	1.2	125	.2	.4	<.1	76	2.96	.093	8	28.5	1.04	61	.002	<1	1.80	.042	.17	.4	.01	10.9	.1	.14	5	<.5	<.3	.01	-
RRE C 158110	2.7	50.3	10.0	104	.3	21.9	23.1	1081	5.23	37.9	.2	<.5	1.2	130	.2	.4	<.1	75	2.91	.083	8	27.8	1.03	60	.003	<1	1.80	.041	.17	.1	<.01	11.3	.1	<.05	5	<.5	<.3	<.01	-
C 158111	.7	75.5	5.5	95	.5	19.5	21.7	787	4.62	37.3	.1	.7	1.2	139	.3	.1	<.1	35	1.89	.074	10	11.3	.91	104	.001	1	1.60	.032	.21	.1	<.01	11.4	.1	<.05	4	<.5	.7	<.01	3000
C 158112	.5	53.3	15.1	90	.3	19.1	19.7	1026	5.44	37.2	.1	2.3	1.2	145	.2	.2	<.1	42	2.60	.085	8	11.5	1.12	65	.002	2	1.31	.027	.19	.1	<.01	11.4	.1	.17	3	.5	.3	<.01	3000
C 158113	3.6	70.1	14.1	95	.5	14.6	17.8	903	4.10	36.6	.2	1.6	.8	111	.4	.3	.1	21	1.78	.079	6	5.3	.89	81	<.001	1	.76	.029	.23	.3	<.01	9.4	.2	.12	2	<.5	.5	.01	3400
C 158114	.8	69.7	26.0	92	.7	12.9	18.6	1035	4.76	46.3	.1	<.5	.9	143	.5	.4	<.1	27	1.72	.093	8	3.8	.93	57	<.001	2	.69	.020	.23	.7	<.01	11.0	.1	.07	2	<.5	.8	.01	3100
C 158115	.9	44.7	12.5	78	1.1	17.4	17.3	765	2.79	45.0	.1	3.5	.6	77	.6	1.2	<.1	12	2.70	.061	4	2.8	.70	53	.001	2	.52	.023	.20	.6	.01	9.0	.2	.17	1	<.5	1.5	.01	1500
C 158116	.8	48.3	80.9	69	1.7	16.1	17.0	1764	3.69	1028.3	.1	52.1	.9	167	.6	1.4	<.1	20	4.05	.076	4	4.6	1.11	52	.001	3	.54	.026	.20	.9	.01	8.8	.1	.71	1	<.5	1.7	.20	2100
C 158117	.4	50.3	62.8	152	1.1	18.9	20.1	1364	5.09	423.6	.1	39.4	1.2	115	.8	1.2	<.1	24	2.82	.100	9	6.9	1.61	41	.001	2	.60	.032	.24	.6	.01	12.1	.1	.15	1	<.5	.6	.06	3200
C 158118	.4	46.4	11.5	73	.6	20.8	21.7	1359	5.08	206.2	.1	22.2	1.0	126	.2	.7	<.1	31	3.04	.099	8	8.3	1.62	30	.001	2	1.21	.023	.18	.5	<.01	10.1	.1	.11	2	<.5	.9	.03	3100
C 158119	.5	45.6	72.6	341	1.1	15.5	17.9	1950	4.31	54.2	.1	19.5	1.0	135	3.7	1.1	<.1	23	3.47	.094	8	5.3	1.47	37	.001	2	.62	.029	.22	.4	.04	10.6	.1	.11	1	<.5	.7	.03	3100
C 158120	.1	79.6	22.3	63	1.1	16.4	18.5	965	4.77	68.5	.1	19.2	1.1	125	.3	1.2	<.1	12	2.10	.053	9	3.3	1.01	68	<.001	3	.50	.023	.24	.5	.01	11.8	.1	.29	1	<.5	.7	.09	2800
C 158121	.4	116.6	10.7	399	1.2	18.3	21.1	1426	3.94	132.2	.1	24.5	.9	165	4.0	1.1	<.1	16	2.80	.070	6	3.9	.99	50	.002	2	.52	.025	.22	.5	.05	10.4	.1	.26	1	<.5	1.3	.07	2800
C 158122	1.0	67.8	19.7	99	.9	16.7	20.0	1031	4.44	66.3	.1	4.0	.8	187	.6	1.2	<.1	15	2.12	.057	6	3.7	.98	50	<.001	2	.49	.021	.24	.4	.01	11.1	.2	.27	1	.5	1.0	.02	2900
C 158123	.8	52.5	9.0	76	1.6	19.5	20.7	1080	4.99	50.5	.1	<.5	.9	177	.4	1.5	<.1	21	2.47	.079	5	5.8	1.15	60	<.001	<1	.58	.023	.26	.5	<.01	11.4	.2	.35	1	.6	2.0	<.01	2800
C 158124	.4	76.4	26.4	58	2.5	15.0	16.6	1253	4.78	145.0	.1	60.1	.7	112	.3	1.5	<.1	21	2.33	.064	3	4.0	1.01	46	<.001	2	.59	.015	.26	.7	<.01	8.7	.1	1.07	1	<.5	2.4	.22	4400
C 158125	.4	86.8	25.3	80	1.4	17.0	18.5	1197	4.53	113.3	.1	7.5	.8	116	.5	.9	<.1	25	2.41	.058	4	3.8	.94	52	<.001	1	.62	.018	.28	.5	<.01	10.1	.1	.71	2	<.5	1.5	.07	4000
C 158126	.5	80.0	5.8	76	.8	18.5	20.3	1026	4.83	47.5	.1	1.3	.8	122	.3	.5	<.1	29	2.62	.066	5	6.5	1.01	50	<.001	1	.70	.024	.27	.3	<.01	9.8	.1	.37	2	<.5	1.0	.02	2500
C 158127	.3	64.5	4.4	69	.6	16.3	17.7	1173	4.73	44.9	.2	11.4	1.1	123	.2	.3	<.1	24	2.84	.071	5	6.4	1.15	42	.001	2	.66	.024	.24	.2	<.01	9.9	.1	.28	1	<.5	.4	.03	1200
C 158128	1.7	41.5	21.7	131	.4	22.1	23.4	1217	4.47	76.9	.2	4.0	1.4	100	.9	.4	<.1	26	3.10	.082	8	7.6	.89	66	.001	3	.66	.033	.31	.4	<.01	9.8	.1	.23	1	<.5	.6	.01	4100
STANDARD DS5	12.5	136.1	24.4	130	.3	24.2	11.9	743	2.95	18.3	5.9	43.0	2.6	51	5.4	3.5	6.0	59	.76	.092	12	183.6	.69	133	.094	20	2.06	.035	.16	4.8	.15	3.6	1.1	<.05	6	4.9	154.4	3.38	-

Standard is STANDARD DS5/R-2/AU-1. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Kodiak Exploration Ltd. PROJECT TOMMY JACK File # A302768

704 - 525 Seymour St., Vancouver BC V6B 3H7 Submitted by: John Bakers

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Ag** gm/mt	Au** gm/mt	Sample gm
S1	.5	.5	.4	1	<.1	.2	.1	3	.05	2.5	<.1	<.5	<.1	3	<.1	<.1	<.1	<1	.12	<.001	<1	1.1	<.01	3	<.001	<1	.01	.553	<.01	.1	<.01	<.1	<.1	<.05	<1	<.5	<.1	<.01	-
C 158148	.5	31.9	197.2	295	.8	9.5	12.9	1201.	3.74	64.8	.2	7.5	1.5	147	2.1	.4	.1	28	2.88	.058	7	4.9	.87	61	<.001	2	1.34	.025	.21	.3	.02	7.0	.1	.19	3	<.5	1.1	.06	2100
C 158149	1.4	23.1	9.2	59	.2	13.1	16.0	785	3.88	48.1	.1	<.5	1.1	108	.2	.3	.1	23	2.61	.060	7	6.5	.88	50	.002	2	1.11	.049	.21	.3	<.01	8.0	.1	.09	2	<.5	.3	<.01	2900
C 158150	3.3	42.8	27.8	143	.8	7.3	11.1	1038	2.86	347.3	.2	3.3	1.1	138	1.2	.6	.2	16	2.89	.070	5	2.9	.63	76	.001	3	.72	.034	.21	.5	.01	4.7	.1	.27	2	<.5	1.1	.03	2800
C 158151	1.1	31.8	73.8	561	.8	.9	6.5	1657	2.37	259.7	.3	25.4	1.1	153	5.8	.4	.5	8	3.36	.068	7	3.7	.57	115	.001	2	.59	.024	.26	.6	.08	2.6	.1	.25	1	<.5	1.0	.02	2700
C 158152	.6	39.3	103.4	59	3.5	6.6	12.8	991	3.40	1522.4	.1	170.3	.7	99	.5	2.5	.1	15	2.30	.059	5	2.9	.77	47	.001	3	.54	.025	.21	1.0	.01	4.9	.1	.81	1	<.5	5.4	.45	2600
C 158153	1.2	11.2	118.3	150	.7	1.6	8.6	1471	2.75	59.1	.1	24.6	.8	115	1.4	.6	<.1	8	3.15	.083	5	4.1	.76	66	.001	3	.66	.020	.26	.8	.01	3.3	.1	.51	1	<.5	.8	.02	2600
C 158154	.2	11.4	170.3	171	.8	1.6	6.2	1959	2.75	60.0	.1	18.2	.8	173	1.7	.9	<.1	7	4.23	.079	6	1.7	.87	67	<.001	3	.57	.021	.24	.6	.02	3.4	.1	.29	1	<.5	1.3	.02	2300
C 158155	1.2	4.2	60.2	111	.3	2.0	9.3	1428	3.11	195.2	.2	47.6	.7	149	.6	.5	.1	8	3.31	.082	4	4.9	.76	65	.004	4	.64	.023	.26	.9	.01	3.4	.1	1.06	1	<.5	.4	.06	2100
C 158156	.2	6.9	79.2	510	.6	1.3	9.5	1477	2.95	103.0	.1	31.3	.7	137	4.5	.5	<.1	8	2.99	.083	4	1.9	.80	121	<.001	3	.84	.021	.25	.8	.05	2.8	.1	.80	2	<.5	.9	.04	1800
STANDARD	12.5	144.6	24.3	145	.2	24.7	11.9	761	2.89	17.5	6.3	42.9	2.6	47	5.7	3.4	6.0	58	.72	.089	12	185.4	.67	134	.098	20	2.04	.032	.13	4.8	.16	3.6	1.0	<.05	6	4.9	156.5	3.26	-

Standard is STANDARD DS5/R-2/AU-1.
GROUP 1DX - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-MS.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
AG** & AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.
- SAMPLE TYPE: CORE R150 60C

DATE RECEIVED: JUL 22 2003 **DATE REPORT MAILED:** Aug 5/03 **SIGNED BY**.........D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data FA ____

ACME ANALYTICAL LABORATORIES LTD.   852 E. HASTINGS ST. VANCOUVER BC   V6A 1R6   PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Kodiak Exploration Ltd.   File # A304091   Page 1
704 - 525 Seymour St., Vancouver BC V6B 3H7   Submitted by: S. Wetherup

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Ag** gm/mt	Au** gm/mt	Sample gm
SI	<1	10	<3	4	<.3	<1	<1	11	.05	<2	<8	<2	<2	4	<.5	<3	<3	1	.13	.001	1	3	.01	4	<.01	<3	.02	.58	.01	<2	<2	<.01	-
C 158157	<1	70	14	95	<.3	18	24	1018	6.46	67	<8	<2	2	76	<.5	<3	<3	39	2.06	.153	7	10	1.21	140	<.01	<3	1.20	.04	.16	2	<2	<.01	3300
C 158158	<1	83	5	73	.4	13	20	959	5.24	22	<8	<2	2	78	<.5	<3	<3	22	1.58	.125	11	5	1.10	133	<.01	<3	.65	.03	.20	2	<2	.01	5200
C 158159	<1	52	<3	52	1.0	11	15	1099	5.60	13	<8	<2	<2	95	<.5	<3	<3	22	2.16	.065	7	6	1.19	101	<.01	<3	.69	.03	.18	2	<2	<.01	3800
C 158160	<1	61	7	62	<.3	12	17	914	4.31	14	<8	<2	<2	123	<.5	<3	<3	20	2.14	.043	9	5	.99	118	<.01	<3	.65	.04	.20	<2	<2	<.01	3700
C 158161	<1	74	7	89	<.3	14	18	966	5.05	13	<8	<2	2	137	<.5	3	<3	23	2.05	.158	13	6	1.08	120	<.01	<3	.66	.04	.23	<2	<2	<.01	4300
C 158162	<1	62	7	75	.3	18	20	1029	5.21	28	<8	<2	<2	136	<.5	<3	<3	23	2.48	.085	9	7	1.10	133	<.01	<3	.69	.03	.21	2	<2	<.01	4700
C 158163	<1	71	22	110	1.9	12	17	1005	4.72	20	<8	<2	2	117	.5	3	<3	18	1.73	.048	9	4	.96	91	<.01	<3	.56	.03	.20	2	2.0	<.01	6000
C 158164	<1	82	81	124	8.4	11	16	818	4.80	139	<8	<2	<2	135	.8	5	<3	37	1.27	.046	5	9	.94	48	<.01	<3	1.82	.02	.18	<2	8.4	.01	4900
C 158165	1	146	488	504	26.5	15	19	1522	5.06	107	<8	<2	<2	201	4.6	21	<3	37	2.75	.078	3	10	1.06	65	<.01	<3	1.68	.01	.16	<2	25.7	.07	1600
C 158166	1	30	21	85	8.3	10	16	1053	4.25	11	<8	<2	<2	142	.6	9	<3	22	2.09	.060	4	5	.88	44	<.01	<3	.63	.03	.19	<2	8.8	<.01	2900
C 158167	<1	16	12	56	4.0	9	11	735	4.35	13	<8	<2	<2	113	<.5	6	<3	32	1.46	.053	2	8	.75	36	<.01	<3	1.64	.02	.17	<2	3.0	<.01	500
C 158168	4	170	1970	4936	71.5	20	21	651	5.40	5797	<8	<2	<2	118	43.0	70	<3	16	1.27	.080	2	5	.35	32	<.01	<3	.92	.01	.16	11	71.2	1.20	2700
C 158169	<1	92	85	136	20.8	30	25	1921	5.25	1057	<8	<2	<2	235	.8	16	<3	51	3.80	.076	5	18	2.02	46	<.01	<3	2.46	.02	.13	2	17.9	.11	2200
C 158170	<1	89	490	936	24.6	16	16	1511	4.54	5383	<8	<2	<2	140	10.4	23	<3	23	1.45	.050	3	7	.84	78	<.01	<3	.78	.02	.17	<2	24.4	.33	3400
RE C 158170	<1	91	489	961	24.5	16	16	1524	4.60	5384	<8	<2	<2	142	10.6	22	<3	23	1.46	.051	3	7	.85	78	<.01	<3	.79	.02	.18	<2	25.0	.32	-
RRE C 158170	<1	86	488	907	23.0	15	16	1513	4.56	5280	<8	<2	<2	140	10.1	20	<3	23	1.45	.051	3	6	.84	77	<.01	<3	.81	.02	.19	<2	22.4	.32	-
C 158171	<1	302	1072	4579	48.0	16	18	1614	4.57	5439	<8	<2	2	148	54.5	52	<3	22	2.36	.119	5	4	.93	77	<.01	<3	.61	.03	.19	<2	48.0	.50	3400
C 158172	<1	113	271	442	7.6	15	18	1634	5.00	375	<8	<2	2	172	4.6	4	<3	22	2.18	.136	6	5	1.16	67	<.01	<3	.63	.03	.22	<2	7.2	.07	3600
C 158173	<1	92	143	1965	20.2	16	22	1403	5.06	1063	<8	<2	<2	168	22.3	11	<3	29	1.90	.054	6	6	1.21	81	<.01	<3	.91	.03	.21	<2	19.6	.19	3100
C 158174	1	64	99	213	7.5	16	18	1726	4.62	682	<8	<2	2	160	1.8	3	<3	32	2.43	.104	7	8	1.14	56	<.01	<3	.88	.03	.19	<2	6.0	.10	3000
C 158175	1	84	153	555	7.2	14	16	1661	4.73	838	<8	<2	<2	166	5.6	5	<3	29	2.83	.079	6	7	1.10	75	<.01	<3	1.09	.03	.18	<2	8.4	.20	5000
C 158176	1	70	433	2279	28.0	12	15	2156	4.95	>9999	<8	<2	<2	218	26.5	21	<3	26	3.55	.053	3	4	.85	44	<.01	<3	1.15	.03	.15	<2	28.6	.75	1700
C 158177	<1	59	94	244	17.8	15	18	1944	4.32	2136	<8	<2	<2	164	2.2	9	<3	30	2.51	.062	4	7	1.03	81	<.01	<3	.70	.04	.19	<2	17.7	.08	3400
C 158178	1	154	1662	1196	110.5	16	16	1887	5.14	4659	<8	<2	<2	147	10.7	80	<3	28	2.34	.065	4	9	1.06	100	<.01	<3	.61	.03	.16	<2	111.5	.84	1500
C 158179	<1	115	823	1630	132.1	16	17	1683	4.35	3629	<8	<2	<2	151	18.3	64	<3	21	1.90	.057	4	4	.92	89	<.01	<3	.54	.03	.18	<2	135.2	.39	5000
C 158180	1	104	751	1427	16.9	13	16	1662	3.72	709	<8	<2	2	161	16.0	13	<3	23	2.87	.106	5	5	.96	47	<.01	<3	.58	.03	.15	<2	16.5	.10	4700
C 158181	<1	76	183	514	9.1	15	26	1279	5.39	849	<8	<2	2	135	5.0	8	<3	21	1.39	.046	6	5	1.11	73	<.01	<3	.66	.04	.21	<2	10.8	.13	3400
C 158182	<1	99	472	1088	6.5	17	18	1340	4.96	277	<8	<2	<2	171	11.6	3	<3	30	2.03	.053	6	8	1.18	109	<.01	<3	1.41	.03	.19	<2	6.6	.11	4000
C 158183	<1	104	90	527	6.3	19	25	1199	5.81	2740	<8	<2	<2	173	5.0	5	3	47	1.64	.068	5	10	1.22	70	<.01	<3	2.23	.04	.18	<2	6.0	.19	4400
C 158184A	1	71	11	90	1.8	17	21	1037	4.96	119	<8	<2	2	230	.6	<3	<3	43	1.68	.112	10	10	1.21	62	<.01	<3	2.29	.04	.15	2	2.2	.01	2200
C 158184B	<1	75	11	82	2.1	20	22	833	5.34	103	<8	<2	2	153	.7	<3	<3	50	.80	.090	6	13	1.45	54	<.01	<3	2.54	.03	.15	2	<2	.01	3200
C 158185	<1	74	119	103	2.3	18	21	1014	5.64	98	<8	<2	2	197	.7	3	<3	47	1.69	.075	7	12	1.45	69	<.01	<3	2.59	.03	.15	2	2.0	.02	4400
C 158186	<1	76	17	69	2.2	21	24	900	4.68	75	<8	<2	<2	181	.6	<3	<3	41	1.47	.074	8	9	1.17	111	<.01	<3	2.24	.05	.21	2	3.1	<.01	4900
C 158187	<1	57	31	128	1.2	22	22	1620	5.56	57	<8	<2	2	353	.8	<3	<3	64	3.36	.099	8	20	1.46	153	<.01	<3	3.02	.06	.16	3	<2	.01	5200
STANDARD DS5	12	140	24	131	.3	23	11	741	2.85	20	<8	<2	2	48	5.3	4	6	57	.72	.094	12	183	.64	140	.09	16	1.99	.04	.13	4	159.0	3.32	-

Standard is STANDARD DS5/R-2/AU-1.

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
AG** & AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: CORE R150 60C   Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: SEP 5 2003   **DATE REPORT MAILED:** Sept 19/03   **SIGNED BY**.......... D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data___ FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Ag** gm/mt	Au** gm/mt	Sample gm
C 158188	<1	67	25	94	1.4	21	20	1085	4.60	41	<8	<2	2	216	<.5	<3	<3	49	2.85	.059	7	19	1.32	162	<.01	<3	2.18	.08	.13	2	<2	<.01	4100
C 158189	<1	59	34	71	2.9	21	21	1723	4.37	40	<8	<2	<2	286	<.5	3	<3	37	4.72	.074	4	13	1.39	129	<.01	<3	1.40	.08	.16	2	2.6	.01	5000
C 158190	1	50	19	140	2.0	27	22	1624	5.44	78	<8	<2	<2	265	.5	4	<3	55	4.15	.077	6	19	1.76	115	<.01	<3	2.18	.08	.17	2	<2	<.01	4800
C 158191	3	62	39	109	7.5	20	20	1001	3.48	129	<8	<2	2	183	.6	<3	<3	36	2.24	.063	3	9	.89	98	<.01	<3	1.60	.07	.16	<2	6.5	.01	4900
C 158192	1	76	20	129	11.5	18	20	1164	4.32	359	<8	<2	<2	148	.7	6	<3	40	1.72	.056	3	8	1.00	91	<.01	<3	1.95	.06	.16	2	11.2	.03	4500
C 158193	<1	70	6	95	1.3	18	19	1005	4.87	44	<8	<2	<2	196	<.5	<3	<3	44	3.19	.101	4	10	1.20	138	<.01	<3	1.82	.11	.16	2	<2	.01	5700
C 158194	<1	73	9	88	1.0	14	17	983	4.47	41	<8	<2	<2	208	<.5	<3	<3	38	2.88	.045	4	8	1.13	136	<.01	<3	1.85	.10	.17	2	<2	.01	5700
C 158195	<1	59	<3	101	.9	25	23	1040	5.93	53	<8	<2	<2	174	<.5	<3	<3	65	2.39	.064	6	17	1.48	115	<.01	<3	2.48	.09	.14	2	<2	.01	4600
C 158196	<1	61	8	75	1.0	20	20	885	4.24	44	<8	<2	<2	180	<.5	3	<3	33	2.51	.061	7	10	1.14	134	<.01	<3	1.70	.11	.14	2	<2	.01	4700
C 158197	<1	54	162	163	1.4	22	21	1918	6.02	55	<8	<2	<2	150	.8	<3	<3	59	3.60	.063	7	19	1.76	89	<.01	<3	2.26	.07	.17	2	2.3	.01	3000
C 158198	<1	47	317	547	2.6	20	18	2970	5.54	56	<8	<2	<2	162	4.3	<3	<3	53	5.02	.071	5	14	1.97	68	<.01	<3	1.72	.05	.15	<2	3.2	.01	2200
C 158199	<1	48	39	295	1.1	28	26	1394	6.24	71	<8	<2	2	114	1.0	<3	<3	74	2.40	.066	8	23	1.77	71	<.01	<3	2.54	.05	.17	<2	<2	<.01	1700
C 158200	<1	46	11	97	1.2	21	21	1291	5.07	57	<8	<2	<2	125	<.5	3	<3	43	2.57	.069	7	11	1.65	70	<.01	<3	2.09	.05	.16	2	<2	<.01	1500
RE C 158200	<1	46	13	93	1.0	21	21	1283	5.04	54	<8	<2	<2	124	<.5	<3	<3	42	2.55	.069	7	11	1.64	69	<.01	<3	2.07	.05	.16	2	<2	.01	-
RRE C 158200	<1	46	14	88	1.0	22	21	1210	5.03	54	<8	<2	<2	120	<.5	<3	<3	43	2.41	.069	7	11	1.63	70	<.01	<3	2.07	.05	.16	2	<2	.01	-
C 158201	<1	86	10	103	.5	16	20	1028	5.41	34	<8	<2	<2	169	<.5	<3	<3	42	2.50	.141	11	9	1.16	118	<.01	<3	2.27	.08	.21	<2	<2	.01	5200
C 158202	1	66	97	260	16.1	17	19	1579	4.86	530	<8	<2	3	154	1.7	9	<3	21	2.76	.083	6	5	1.00	188	<.01	<3	.70	.14	.18	<2	16.7	.09	5000
C 158203	1	84	75	136	3.8	17	23	1258	4.42	95	<8	<2	2	169	.7	9	<3	23	2.97	.169	8	5	.97	153	<.01	<3	1.24	.10	.19	2	2.3	.01	1700
C 158204	<1	58	5	71	.9	18	20	998	5.42	33	<8	<2	2	139	.5	<3	<3	45	1.69	.072	9	12	1.13	95	<.01	<3	2.35	.09	.16	2	<2	<.01	5800
C 158205	<1	63	10	75	<.3	14	17	1137	4.16	22	<8	<2	<2	157	<.5	<3	<3	22	3.40	.074	8	6	.92	129	<.01	<3	1.09	.11	.16	<2	<2	<.01	4300
C 158206	1	66	24	139	1.4	16	19	1111	4.93	30	<8	<2	<2	139	1.0	7	<3	22	2.42	.086	9	5	1.01	147	<.01	<3	.99	.10	.22	2	<2	<.01	4600
C 158207	<1	69	12	109	.7	15	19	695	5.53	20	<8	<2	2	158	<.5	<3	<3	51	1.07	.072	12	12	1.18	140	<.01	<3	2.85	.08	.20	2	<2	<.01	4100
C 158208	<1	104	6	98	.8	15	13	1154	5.57	18	<8	<2	<2	327	.5	<3	<3	48	3.96	.072	6	10	1.03	149	<.01	<3	2.60	.08	.20	<2	<2	<.01	500
C 158209	<1	86	7	77	.9	19	21	830	5.45	32	<8	<2	2	224	<.5	3	<3	49	1.83	.079	9	12	1.07	153	<.01	<3	2.70	.09	.19	2	<2	.01	4500
C 158210	<1	63	7	113	.5	31	28	1959	6.31	29	<8	<2	<2	238	.5	3	<3	110	5.20	.069	8	39	1.29	119	<.01	<3	2.89	.07	.15	2	<2	<.01	4300
C 158211	1	60	8	84	.6	15	18	886	4.80	37	<8	<2	3	147	<.5	4	<3	26	2.37	.052	6	6	.99	134	<.01	<3	1.03	.09	.18	2	<2	<.01	7900
C 158212	1	59	6	73	.4	14	17	826	4.45	34	<8	<2	<2	145	<.5	<3	<3	23	2.26	.049	6	6	.92	132	<.01	<3	.94	.09	.17	<2	<2	<.01	3900
C 158213	1	55	21	69	5.3	20	34	1107	4.42	85	<8	<2	<2	172	<.5	6	<3	27	2.97	.063	6	6	1.03	109	<.01	<3	1.25	.08	.17	2	5.5	.02	3600
C 158214	<1	69	46	140	7.7	12	16	987	4.76	16	<8	<2	<2	157	.9	4	3	26	2.67	.055	7	6	1.14	96	<.01	<3	1.55	.07	.15	<2	6.9	.01	5300
C 158215	<1	40	79	241	3.9	12	15	1155	4.37	34	<8	<2	2	167	2.0	<3	<3	27	2.90	.069	6	6	1.14	104	<.01	<3	1.52	.08	.14	<2	3.3	<.01	3900
C 158216	<1	49	54	134	6.3	17	21	1104	4.47	43	<8	<2	2	146	1.0	6	<3	21	2.38	.055	9	5	1.17	111	<.01	<3	.85	.09	.16	<2	6.4	<.01	3500
C 158217	<1	52	63	359	5.6	15	21	1188	4.73	22	<8	<2	<2	161	3.1	4	<3	31	2.51	.063	7	7	1.25	95	<.01	<3	1.48	.07	.15	<2	6.2	.01	2700
C 158218	<1	35	141	339	5.6	16	22	1330	5.17	22	<8	<2	2	148	2.8	10	<3	35	2.80	.071	8	9	1.24	86	<.01	<3	1.90	.07	.16	<2	6.0	.01	1900
C 158219	1	56	49	174	10.5	15	20	1499	4.48	20	<8	<2	<2	283	1.5	28	<3	26	4.01	.110	7	7	1.29	75	<.01	<3	1.25	.06	.15	2	10.0	.01	2300
STANDARD DS5	12	138	23	130	.4	23	12	739	2.83	17	11	<2	3	47	5.2	<3	6	58	.70	.088	12	180	.64	134	.09	16	1.99	.03	.13	4	155.6	3.43	-

Standard is STANDARD DS5/R-2/AU-1. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Ag** gm/mt	Au** gm/mt	Sample gm
C 158220	1	31	42	188	7.7	18	20	1602	5.44	94	<8	<2	2	155	1.6	7	<3	36	2.63	.080	6	13	1.42	78	<.01	<3	1.46	.07	.23	<2	6.5	.33	1300
C 158221	1	73	113	522	12.0	14	17	1947	4.69	856	<8	<2	2	200	5.0	19	<3	21	4.46	.064	4	6	1.40	75	<.01	<3	.56	.06	.16	<2	12.7	.14	1600
C 158222	1	46	19	66	19.2	11	16	1828	3.47	35	<8	<2	2	303	.8	19	<3	20	4.60	.069	4	9	1.25	56	<.01	<3	.51	.05	.19	15	20.9	.20	1700
C 158223	<1	14	6	38	5.7	14	18	1662	4.86	87	<8	<2	2	224	.5	3	<3	24	3.90	.064	4	7	1.44	71	<.01	<3	.60	.06	.18	<2	5.5	.04	1700
C 158224	1	101	999	1525	50.0	14	20	1249	3.97	202	<8	<2	2	166	17.4	31	3	17	2.43	.071	4	5	.99	127	<.01	<3	.50	.09	.21	<2	49.9	.17	2000
C 158225	1	72	22	178	7.8	13	16	1127	4.34	33	<8	<2	2	163	2.0	<3	<3	21	2.80	.069	6	6	1.10	142	<.01	<3	.71	.09	.22	<2	8.3	.02	4700
C 158226	1	59	17	87	16.8	11	16	979	3.92	75	<8	<2	2	194	1.1	6	<3	23	3.26	.063	5	5	1.02	97	<.01	<3	1.00	.07	.19	<2	16.9	.06	1700
C 158227	1	53	9	60	12.6	13	19	781	4.31	19	<8	<2	<2	136	.7	6	<3	27	2.02	.053	7	6	1.07	104	<.01	<3	1.38	.08	.19	<2	12.7	.01	1500
C 158228	1	49	6	63	14.6	11	14	856	3.63	17	<8	<2	<2	191	.9	9	<3	17	2.49	.054	6	4	.93	123	<.01	<3	.55	.08	.20	<2	15.3	.04	2000
C 158229	<1	59	160	237	6.3	14	18	994	4.63	23	<8	<2	2	132	2.5	4	<3	30	1.85	.075	6	7	1.13	108	<.01	<3	1.65	.07	.21	<2	5.4	.04	1700
C 158230	<1	42	32	111	3.2	17	20	1040	6.48	37	<8	<2	2	152	1.0	3	4	57	2.10	.069	7	15	1.47	106	<.01	<3	2.51	.08	.16	<2	4.3	.01	1300
C 158231	1	53	26	52	3.6	16	24	843	4.26	43	<8	<2	<2	152	.6	<3	<3	29	2.22	.067	6	7	1.02	114	<.01	<3	1.65	.08	.19	<2	2.7	<.01	1200
C 158232	1	63	7	118	.9	13	17	856	4.12	31	<8	<2	<2	153	.9	<3	<3	22	2.51	.086	9	5	1.01	116	<.01	<3	.84	.09	.21	<2	<2	.02	3600
C 158233	<1	41	29	162	2.7	19	20	1293	6.04	43	<8	<2	<2	190	1.2	9	<3	35	2.57	.105	7	8	1.45	170	<.01	<3	.65	.07	.19	<2	2.8	.01	2000
C 158234	<1	83	67	97	4.0	16	19	1122	5.03	33	<8	<2	2	128	.7	4	<3	29	2.15	.056	7	6	1.14	108	<.01	<3	1.02	.07	.21	<2	3.5	.01	2200
C 158235	<1	81	7	108	.4	15	19	904	5.07	31	<8	<2	<2	127	.5	<3	<3	24	1.72	.065	8	4	1.07	137	<.01	<3	.77	.09	.22	<2	<2	.01	3700
C 158236	<1	70	7	81	.3	15	18	793	4.20	34	<8	<2	2	145	.5	<3	<3	21	2.51	.080	8	5	.93	154	<.01	<3	.68	.10	.22	<2	<2	.01	5900
C 158237	<1	52	21	107	1.3	20	21	1504	5.89	75	<8	<2	2	140	.6	<3	<3	36	2.47	.084	7	9	1.26	120	<.01	<3	1.19	.09	.18	<2	<2	.01	5100
C 158238	<1	56	8	102	.8	22	27	1060	6.26	54	<8	<2	2	136	<.5	<3	<3	48	2.04	.077	7	13	1.47	98	<.01	<3	2.52	.09	.15	<2	<2	.02	1900
C 158239	<1	62	<3	33	.3	13	15	896	4.15	31	<8	<2	<2	72	<.5	<3	<3	22	2.10	.051	8	4	.92	111	<.01	<3	.85	.03	.20	<2	<2	<.01	2700
C 158240	<1	69	9	70	.3	16	22	931	4.01	31	<8	<2	<2	122	<.5	<3	<3	22	2.00	.049	8	5	.87	124	<.01	<3	.71	.03	.22	<2	<2	<.01	4900
RE C 158240	<1	71	11	71	.6	16	23	935	4.02	30	<8	<2	<2	122	<.5	<3	<3	22	2.01	.049	8	5	.88	124	<.01	<3	.71	.03	.22	<2	2.3	.02	-
RRE C 158240	<1	71	10	69	.4	16	23	927	4.02	32	<8	<2	<2	121	<.5	<3	<3	22	2.02	.048	8	5	.87	127	<.01	<3	.71	.03	.22	<2	<2	<.01	-
C 158241	<1	59	7	100	.6	21	21	1508	5.41	33	<8	<2	3	148	.6	<3	<3	33	3.22	.092	5	9	1.15	76	<.01	<3	1.56	.03	.21	<2	<2	<.01	2500
C 158242	1	65	106	85	3.0	15	18	1037	4.40	66	<8	<2	2	142	.7	<3	<3	40	2.44	.061	5	7	.92	53	<.01	<3	1.89	.02	.19	<2	3.0	.01	1900
C 158243	<1	65	288	1688	11.9	14	17	1128	4.60	933	<8	<2	<2	120	17.9	4	<3	40	1.95	.062	4	10	.87	52	<.01	<3	1.88	.02	.20	<2	12.0	.28	2600
C 158244	<1	82	183	207	34.2	17	17	2572	4.18	1321	<8	<2	3	137	1.9	17	<3	38	3.48	.062	4	8	1.19	62	<.01	<3	1.34	.03	.19	<2	33.0	.13	1500
C 158245	<1	36	197	525	12.8	14	15	2920	3.60	146	<8	<2	2	131	4.1	4	<3	31	3.71	.058	3	9	1.12	45	<.01	<3	1.07	.03	.18	<2	14.9	.03	1500
C 158246	<1	46	108	136	9.4	14	15	2179	4.08	1870	<8	<2	2	143	1.2	6	<3	28	2.82	.079	3	6	1.02	58	<.01	<3	1.31	.03	.17	<2	9.1	.20	1700
C 158247	<1	85	6	38	23.7	17	18	1457	4.44	305	<8	<2	2	114	.6	9	<3	39	1.93	.122	6	8	1.26	63	<.01	<3	1.85	.02	.19	<2	23.0	.04	1500
C 158248	<1	208	2754	3797	199.2	18	21	1490	5.63	>9999	<8	<2	<2	114	24.0	94	<3	33	1.71	.091	4	4	.98	69	<.01	<3	1.73	.02	.18	<2	207.8	1.41	1500
C 158249	<1	80	39	157	10.6	21	21	1684	4.75	215	<8	<2	2	142	1.6	5	<3	39	2.19	.057	7	7	1.21	84	<.01	<3	2.06	.03	.19	<2	9.9	.02	1800
C 158250	<1	99	172	148	20.1	18	20	1487	4.53	942	<8	<2	2	130	1.5	9	<3	45	1.16	.087	5	9	1.13	77	<.01	<3	2.20	.02	.20	<2	19.7	.11	1200
C 158251	<1	68	6	94	<.3	15	16	894	5.02	11	<8	<2	2	80	<.5	<3	<3	42	1.49	.037	8	12	1.10	126	<.01	<3	1.58	.04	.18	<2	<2	.01	2800
STANDARD DS5	12	137	23	131	<.3	24	12	744	2.84	19	<8	<2	3	47	5.5	3	6	58	.71	.092	11	185	.63	137	.08	16	1.98	.04	.12	4	156.3	3.37	-

Standard is STANDARD DS5/R-2/AU-1. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Ag** gm/mt	Au** gm/mt	Sample gm
C 158252	<1	64	5	85	<.3	16	18	1041	4.47	5	<8	<2	<2	100	<.5	<3	<3	26	2.15	.102	9	8	.99	108	<.01	3	.90	.05	.20	<2	<2	<.01	5000
C 158253	1	75	5	86	<.3	13	16	1024	3.92	7	<8	<2	2	100	<.5	7	3	19	1.86	.058	11	5	.80	107	<.01	<3	.84	.03	.24	<2	<2	<.01	3400
C 158254	1	56	4	72	<.3	20	25	1205	4.42	24	<8	<2	<2	102	<.5	11	<3	31	2.35	.054	8	8	.97	110	<.01	<3	1.61	.04	.19	<2	<2	<.01	3400
C 158255	1	78	20	103	1.1	12	16	970	4.34	19	<8	<2	2	109	.6	<3	<3	26	2.11	.218	12	6	.86	129	<.01	3	.96	.03	.28	2	<2	<.01	3500
C 158256	2	71	6	87	<.3	15	19	931	4.49	22	<8	<2	3	97	<.5	<3	<3	21	1.58	.058	10	6	.90	110	<.01	<3	.67	.04	.22	<2	<2	<.01	3400
C 158257	2	70	8	94	<.3	15	18	1492	4.44	29	<8	<2	<2	139	<.5	<3	<3	26	4.61	.209	11	6	.93	267	.01	<3	.77	.04	.25	2	<2	<.01	3700
C 158258	1	65	12	88	.5	16	18	978	4.45	43	<8	<2	2	103	<.5	3	<3	22	1.91	.064	10	6	.89	128	<.01	3	.57	.04	.20	2	<2	<.01	5700
C 158259	1	57	74	165	5.7	19	21	972	3.93	115	<8	<2	2	95	1.4	8	<3	20	1.94	.073	5	5	.76	76	<.01	<3	.61	.03	.21	<2	5.9	.02	4300
C 158260	1	58	21	104	1.8	21	23	940	3.99	70	<8	<2	<2	105	.7	<3	<3	19	2.26	.057	8	5	.83	73	<.01	<3	.56	.04	.21	<2	2.0	<.01	3900
C 158261	3	66	1083	1634	13.0	19	18	863	5.19	911	<8	<2	2	87	14.7	12	<3	25	2.34	.037	2	7	.59	46	<.01	<3	1.01	.02	.12	<2	14.6	1.82	400
C 158262	1	71	<3	93	.3	31	24	1879	5.96	19	<8	<2	2	134	<.5	<3	<3	78	3.76	.065	7	28	1.69	63	<.01	<3	2.39	.05	.11	2	<2	<.01	2200
C 158263	<1	65	8	101	<.3	25	23	2439	4.52	15	<8	<2	<2	168	<.5	<3	<3	66	5.21	.069	6	19	1.87	50	<.01	<3	1.44	.07	.09	<2	<2	.01	4500
C 158264	<1	71	3	99	<.3	29	23	1218	5.10	<2	<8	<2	<2	118	.6	<3	<3	115	2.74	.076	6	37	2.22	44	<.01	<3	2.70	.09	.07	<2	<2	.01	4200
C 158265	<1	66	<3	78	<.3	25	21	1231	4.74	4	<8	<2	2	125	<.5	<3	<3	101	3.28	.073	6	30	2.28	38	<.01	<3	2.39	.08	.06	<2	<2	<.01	4400
C 158266	<1	60	<3	89	<.3	30	25	1933	5.16	4	<8	<2	<2	133	<.5	<3	<3	109	4.32	.078	8	35	2.35	38	<.01	<3	2.48	.07	.07	2	<2	<.01	5300
C 158267	1	77	3	92	.8	16	17	892	4.01	30	<8	<2	3	155	<.5	4	<3	28	3.14	.077	9	7	1.21	135	.01	<3	.80	.08	.17	2	<2	<.01	5300
C 158268	1	75	6	89	.9	15	17	867	3.86	50	<8	<2	<2	155	<.5	<3	<3	25	2.12	.054	6	5	1.01	88	<.01	<3	.69	.07	.20	2	<2	<.01	3200
C 158269	<1	66	3	89	.3	18	18	873	4.31	33	<8	<2	2	190	<.5	<3	<3	29	2.49	.063	7	7	1.09	77	<.01	<3	.81	.08	.15	<2	<2	<.01	4400
C 158270	<1	99	5	91	.3	18	19	847	5.02	15	<8	<2	2	173	<.5	<3	<3	48	2.06	.063	11	14	1.27	105	.01	<3	2.41	.06	.19	2	<2	<.01	3700
RE C 158270	<1	99	<3	91	<.3	18	19	861	5.09	11	<8	<2	<2	175	<.5	<3	<3	49	2.07	.064	10	13	1.28	107	<.01	<3	2.45	.06	.19	<2	<2	<.01	-
RRE C 158270	<1	94	<3	87	<.3	17	18	804	4.85	8	<8	<2	2	166	<.5	<3	<3	46	1.96	.061	11	13	1.23	98	<.01	<3	2.31	.05	.18	2	<2	<.01	-
C 158271	1	74	5	91	<.3	16	18	1108	4.60	12	<8	<2	2	198	<.5	<3	<3	50	3.27	.098	7	14	1.18	92	<.01	<3	2.10	.06	.15	<2	<2	<.01	4800
C 158272	5	60	3	84	<.3	15	17	1274	4.45	14	<8	<2	2	242	<.5	3	<3	51	3.79	.086	8	14	1.14	82	<.01	<3	2.14	.06	.15	2	<2	<.01	4500
C 158273	<1	73	4	92	<.3	17	19	924	4.68	13	<8	<2	2	198	<.5	<3	<3	52	2.08	.070	10	16	1.15	117	<.01	<3	2.56	.06	.18	<2	<2	<.01	4500
C 158274	<1	48	3	88	<.3	16	18	937	4.01	7	<8	<2	2	194	<.5	<3	<3	69	2.77	.121	7	18	1.01	86	<.01	<3	2.17	.09	.15	<2	<2	.01	5000
C 158275	<1	69	5	109	<.3	15	20	807	5.53	<2	<8	<2	2	140	<.5	<3	<3	61	1.20	.038	8	15	1.31	121	.01	<3	3.08	.04	.22	<2	<2	<.01	4300
C 158276	<1	73	8	93	<.3	19	20	968	5.01	11	<8	<2	2	151	<.5	<3	<3	64	1.60	.067	8	20	1.17	119	<.01	<3	2.64	.07	.20	<2	<2	<.01	3900
C 158277	<1	68	80	175	1.9	22	24	1023	5.54	1424	<8	<2	2	165	.9	4	<3	70	1.65	.075	5	19	.97	108	<.01	<3	2.54	.06	.17	<2	<2	.02	4000
C 158278	1	66	15	127	.5	16	19	1124	4.46	125	<8	<2	2	189	<.5	3	<3	52	2.64	.066	8	13	1.02	134	<.01	<3	2.01	.09	.16	2	<2	<.01	3500
C 158279	3	42	47	72	1.7	15	17	1887	4.40	39	<8	<2	<2	372	<.5	3	<3	36	5.60	.053	3	9	1.36	92	<.01	<3	1.38	.07	.11	2	<2	<.01	1700
C 158280	1	49	<3	88	<.3	25	21	1543	4.92	27	<8	<2	<2	135	<.5	<3	<3	84	3.11	.082	8	27	1.52	98	<.01	<3	2.23	.08	.14	2	<2	<.01	6600
C 158281	2	59	64	99	4.7	24	20	1896	5.31	385	<8	<2	<2	234	.9	5	<3	63	4.79	.080	4	20	1.82	65	<.01	<3	2.34	.04	.15	2	4.7	.03	1600
C 158282	<1	69	5	97	<.3	17	18	1029	4.42	47	<8	<2	<2	194	<.5	<3	<3	37	2.83	.088	7	8	.97	129	<.01	<3	1.78	.11	.19	2	<2	<.01	1900
C 158283	<1	74	4	78	.6	19	21	1185	4.78	46	<8	<2	2	221	<.5	<3	<3	37	3.12	.088	9	9	1.03	150	<.01	<3	2.07	.10	.22	2	<2	<.01	1700
STANDARD DS5	12	140	23	131	<.3	24	12	742	2.82	19	<8	<2	3	46	5.5	3	6	58	.71	.092	12	186	.64	135	.09	16	2.02	.03	.13	4	155.1	3.38	-

Standard is STANDARD DS5/R-2/AU-1. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Ag**	Au**	Sample
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	gm/mt	gm/mt	gm
C 158284	<1	71	<3	85	.4	17	20	835	4.75	33	<8	<2	2	179	<.5	<3	<3	40	2.10	.194	13	9	1.03	131	<.01	<3	2.25	.08	.18	<2	<2	.01	1200
C 158285	<1	67	7	77	1.0	18	20	858	4.81	41	<8	<2	<2	154	<.5	3	<3	37	1.88	.069	4	9	1.04	130	<.01	<3	2.02	.09	.17	2	<2	.01	1400
C 158286	<1	61	11	83	.9	16	18	1041	4.92	39	<8	<2	2	210	<.5	<3	<3	31	3.18	.139	7	9	1.21	175	.01	<3	1.26	.12	.15	<2	<2	<.01	1300
C 158287	<1	61	6	153	.8	17	19	1121	5.65	32	<8	<2	2	204	<.5	<3	<3	39	3.18	.092	5	10	1.28	147	.01	<3	1.89	.10	.14	<2	<2	<.01	1300
C 158288	<1	69	6	84	.9	16	18	1008	4.98	34	<8	<2	2	187	<.5	<3	<3	33	2.46	.079	3	8	1.10	146	.01	<3	1.26	.10	.11	2	<2	.01	1200
C 158289	<1	72	5	87	1.0	20	22	865	3.89	48	<8	<2	<2	168	<.5	5	<3	39	1.99	.090	2	7	.79	136	<.01	<3	1.17	.10	.13	<2	<2	.01	1300
C 158290	<1	82	46	61	16.1	15	17	1457	3.91	2794	<8	<2	<2	148	<.5	15	<3	33	2.30	.070	3	7	.86	112	<.01	<3	.84	.08	.14	<2	18.7	.18	1700
C 158291	<1	67	7	68	2.4	17	18	1145	4.33	55	<8	<2	<2	178	<.5	4	<3	27	2.62	.066	3	6	.99	149	<.01	<3	.86	.11	.14	<2	2.2	.01	1700
C 158292	<1	44	84	70	5.3	20	20	1702	6.25	1939	<8	<2	<2	134	.5	8	<3	45	3.30	.077	4	12	1.16	78	.01	<3	1.91	.06	.11	<2	5.5	.12	2100
C 158293	2	35	12	125	.9	23	22	2611	5.08	62	<8	<2	<2	275	<.5	3	<3	61	6.82	.076	5	15	1.03	74	<.01	<3	1.86	.06	.11	<2	<2	.01	2500
C 158294	<1	94	1019	994	17.4	17	18	2476	5.53	706	<8	<2	<2	266	9.1	13	<3	49	4.15	.061	4	10	1.09	79	<.01	3	2.07	.05	.15	<2	17.5	.45	2200
C 158295	<1	64	287	521	6.6	23	20	2896	4.60	194	<8	<2	<2	159	4.7	7	<3	33	3.74	.074	4	9	1.11	82	<.01	3	1.17	.05	.17	<2	5.9	.02	3500
C 158296	1	82	166	140	28.5	17	24	2138	4.65	3924	<8	<2	<2	106	1.4	31	<3	25	1.88	.031	1	3	.72	83	<.01	<3	.75	.04	.17	<2	30.6	.29	1900
C 158297	<1	144	443	352	34.5	14	18	1653	4.84	8833	<8	<2	<2	103	3.0	39	<3	19	1.41	.032	1	3	.55	84	.01	<3	.60	.05	.18	<2	37.4	.41	1800
C 158298	1	56	33	59	4.9	13	17	2389	4.02	708	<8	<2	2	117	<.5	5	<3	24	1.99	.144	4	4	.84	121	<.01	<3	.57	.06	.21	<2	4.8	.04	1600
C 158299	<1	80	39	95	3.2	15	18	1801	4.51	259	<8	<2	<2	116	.5	5	<3	21	1.84	.062	4	4	.92	125	<.01	<3	.51	.06	.18	<2	3.7	.05	1900
C 158300	<1	76	136	60	3.5	14	16	2197	4.29	872	<8	<2	<2	121	.5	7	<3	17	1.97	.066	4	4	.84	133	<.01	<3	.46	.07	.18	<2	3.6	.10	1700
RE C 158300	<1	80	142	61	3.5	14	16	2285	4.44	919	<8	<2	<2	126	<.5	6	<3	19	2.03	.068	4	3	.87	138	<.01	<3	.47	.07	.18	<2	3.1	.10	-
RRE C 158300	<1	76	123	63	3.6	13	16	2263	4.42	883	<8	<2	<2	122	.5	6	<3	17	2.01	.068	4	4	.86	135	<.01	<3	.49	.07	.20	<2	3.1	.10	-
C 158301	<1	50	10	27	3.1	14	17	1434	3.84	95	<8	<2	<2	143	<.5	<3	<3	24	3.08	.067	5	5	.98	104	<.01	<3	.55	.06	.16	<2	3.0	.02	2000
C 158302	<1	64	22	97	2.7	15	18	1467	4.36	39	<8	<2	<2	141	.8	3	<3	27	2.99	.068	5	6	1.07	99	<.01	<3	.85	.06	.16	<2	2.2	.01	1900
C 158303	<1	71	35	105	3.0	16	20	1707	4.43	118	<8	<2	<2	138	.9	7	<3	25	2.89	.064	9	7	1.07	122	<.01	<3	.52	.06	.17	<2	2.8	.02	2000
C 158304	<1	80	491	342	11.6	16	16	1611	4.29	1380	<8	<2	<2	122	3.6	13	<3	21	2.68	.048	4	5	.99	119	<.01	<3	.53	.07	.15	<2	11.8	.26	2000
C 158305	<1	63	19	86	1.9	15	18	1265	4.41	41	<8	<2	2	120	<.5	<3	<3	23	2.36	.055	7	5	1.09	154	<.01	<3	.49	.07	.17	<2	<2	.01	2300
C 158306	<1	75	47	501	1.2	16	21	1499	4.66	43	<8	<2	<2	123	4.3	3	<3	27	2.48	.062	7	5	1.16	162	<.01	<3	.56	.07	.17	<2	<2	.01	1600
C 158307	1	75	1039	1567	5.7	14	18	1430	4.17	1152	<8	<2	<2	125	17.2	4	<3	24	2.94	.174	7	4	1.06	155	<.01	<3	.54	.07	.18	<2	5.5	.26	2300
C 158308	<1	88	700	2213	5.4	15	16	2088	4.42	140	<8	<2	<2	97	23.2	7	<3	24	2.54	.063	5	4	1.18	110	<.01	<3	.40	.05	.18	<2	4.6	.17	1600
C 158309	<1	87	272	929	5.7	18	20	2115	4.92	23	<8	<2	<2	126	9.7	7	<3	29	2.77	.072	5	6	1.35	98	<.01	<3	.54	.05	.19	<2	5.2	.02	1700
C 158310	<1	48	27	208	1.6	19	20	1814	5.39	15	<8	<2	<2	140	1.6	<3	<3	42	3.51	.065	8	10	1.66	87	<.01	<3	1.75	.06	.15	<2	<2	.02	1500
C 158311	<1	45	47	121	7.7	16	18	1682	4.38	273	<8	<2	2	162	.7	4	<3	28	3.99	.056	5	7	1.29	92	<.01	<3	.97	.07	.14	<2	5.4	.09	2000
C 158312	<1	47	5	77	1.2	17	20	1242	5.56	15	<8	<2	<2	135	<.5	<3	<3	45	2.57	.066	9	12	1.49	101	<.01	<3	2.01	.07	.14	<2	<2	.01	1900
C 158313	<1	110	735	162	192.1	16	17	1298	3.87	839	<8	<2	<2	172	1.0	92	<3	26	3.44	.057	5	6	1.24	135	<.01	<3	.91	.08	.13	<2	189.9	.07	1000
C 158314	<1	48	10	88	.8	19	23	1210	4.76	30	<8	<2	<2	148	<.5	<3	<3	56	2.88	.075	8	13	1.47	97	<.01	<3	1.76	.07	.13	<2	<2	.01	4800
C 158315	1	43	14	98	1.3	16	20	1715	4.36	25	<8	<2	2	213	<.5	<3	<3	47	4.34	.082	7	11	1.41	81	.01	<3	1.53	.06	.13	<2	<2	.01	5100
STANDARD DS5	12	140	24	134	.3	24	12	752	2.88	19	<8	<2	3	46	5.4	4	6	58	.71	.090	12	190	.65	139	.09	18	2.06	.03	.13	3	156.4	3.38	-

Standard is STANDARD DS5/R-2/AU-1. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Ag** gm/mt	Au** gm/mt	Sample gm
C 158316	1	42	25	97	.9	18	20	1078	5.07	28	<8	<2	2	111	<.5	<3	<3	59	2.14	.094	7	15	1.69	74	<.01	<3	2.06	.05	.15	<2	<2	<.01	2400
C 158317	1	64	2853	1016	45.2	20	19	3437	3.44	193	<8	<2	<2	151	10.6	20	15	21	4.54	.096	6	5	1.15	68	<.01	<3	.70	.06	.16	<2	45.3	.04	1500
C 158318	1	84	1842	2005	82.1	15	15	2823	4.67	538	<8	<2	2	195	19.8	42	<3	21	5.64	.078	4	4	1.63	59	<.01	<3	.94	.05	.15	<2	79.0	.05	1200
C 158319	1	56	319	144	4.8	15	17	1407	4.52	71	<8	<2	2	162	.8	3	<3	28	3.32	.106	5	6	1.24	79	<.01	<3	1.60	.06	.17	<2	6.8	.01	1800
C 158320	<1	76	231	306	17.7	16	17	1630	4.51	1190	<8	<2	<2	176	2.2	11	<3	28	3.02	.045	3	7	1.03	131	<.01	<3	1.49	.08	.20	<2	17.3	.05	2000
C 158321	<1	76	111	160	6.5	18	19	1303	5.03	124	<8	<2	2	149	1.0	<3	<3	28	2.47	.050	7	7	1.21	144	<.01	<3	1.13	.09	.21	<2	5.3	.01	1700
C 158322	<1	59	30	62	4.9	19	20	1131	5.29	56	<8	<2	2	136	<.5	<3	<3	47	2.36	.069	4	14	1.39	104	<.01	<3	1.85	.07	.19	<2	3.7	.01	1900
C 158323	<1	43	120	40	10.6	24	23	1579	5.25	320	<8	<2	2	133	<.5	8	<3	48	2.87	.067	3	11	1.24	81	<.01	<3	1.48	.06	.18	2	10.9	.02	1500
C 158324	1	2585	>9999	55194	>200	8	3	471	5.59	>9999	<8	2	<2	16	582.3	>2000	<3	4	.54	.005	<1	<1	.17	7	<.01	<3	.12	.02	.03	<2	2321.5	2.63	600
C 158325	<1	140	1778	3040	109.5	20	21	1217	6.20	8324	<8	<2	3	98	28.8	83	<3	25	1.58	.088	2	6	.58	38	<.01	<3	.78	.06	.18	<2	104.0	.61	1100
C 158326	1	67	580	339	27.1	17	20	1959	4.86	797	<8	<2	2	131	3.2	18	<3	27	2.18	.142	4	6	1.12	129	<.01	<3	.68	.08	.23	<2	25.1	.04	2400
C 158327	1	67	96	490	6.8	17	18	1447	4.95	254	<8	<2	<2	158	4.4	6	<3	28	2.44	.117	5	6	1.21	129	<.01	<3	.70	.09	.20	<2	7.5	.02	1500
C 158328	<1	49	43	102	1.4	17	17	1309	4.87	39	<8	<2	2	125	<.5	<3	<3	28	2.22	.069	9	6	1.34	102	<.01	<3	.53	.07	.19	<2	<2	<.01	3100
C 158329	<1	141	2584	587	113.6	20	18	2052	5.53	439	<8	<2	2	126	5.5	66	<3	37	2.63	.100	6	12	1.52	96	<.01	<3	.58	.07	.20	<2	110.5	.11	1800
C 158330	<1	62	41	105	3.4	14	15	1481	4.22	41	<8	<2	<2	160	.6	5	<3	24	3.18	.114	8	6	1.17	119	<.01	<3	.56	.09	.18	<2	3.6	<.01	1700
RE C 158330	1	61	43	99	3.2	14	15	1466	4.19	43	<8	<2	2	158	.6	4	<3	24	3.17	.113	8	6	1.16	118	<.01	<3	.56	.09	.20	<2	3.1	<.01	-
RRE C 158330	1	57	51	89	3.2	14	15	1426	4.07	32	<8	<2	2	154	<.5	4	<3	24	3.10	.111	9	6	1.13	116	<.01	<3	.56	.09	.19	<2	2.7	.01	-
C 158331	<1	56	33	47	7.6	14	17	1364	4.14	40	<8	<2	2	164	<.5	8	<3	26	2.83	.107	8	6	1.08	104	<.01	<3	.78	.09	.17	<2	6.8	.01	1500
C 158332	<1	54	240	189	9.9	13	16	1502	4.40	133	<8	<2	<2	163	1.5	9	<3	26	2.75	.062	7	7	1.13	97	<.01	<3	.93	.08	.16	<2	10.5	.01	1800
C 158333	<1	36	1126	415	6.6	15	16	1298	4.68	170	<8	<2	<2	162	3.0	8	<3	33	2.76	.055	5	8	1.14	99	<.01	<3	1.39	.08	.16	<2	7.2	.02	2000
C 158334	<1	72	550	2863	29.8	17	18	2328	4.40	72	<8	<2	2	155	22.4	16	<3	34	4.07	.064	4	8	1.40	78	<.01	<3	1.04	.07	.14	<2	30.2	.01	1600
C 158335	1	41	138	86	12.9	23	23	1658	4.77	469	<8	<2	2	129	.7	9	<3	47	2.47	.076	3	11	1.12	79	<.01	<3	1.62	.06	.16	<2	13.0	.02	1400
C 158336	<1	27	429	33	18.2	10	7	1842	5.66	>9999	<8	<2	<2	110	<.5	57	<3	10	3.50	.027	<1	5	.78	32	<.01	<3	.22	.02	.06	10	19.6	1.60	1100
C 158337	<1	53	75	100	12.3	19	22	1278	4.39	1052	<8	<2	<2	132	.8	7	<3	32	2.30	.084	4	8	.93	113	<.01	<3	1.35	.08	.17	<2	12.2	.06	2700
C 158338	<1	56	107	90	14.3	18	19	1607	4.83	462	<8	<2	<2	170	.8	8	<3	43	2.74	.099	5	11	1.15	87	<.01	<3	1.88	.07	.17	<2	13.7	.04	2000
C 158339	1	52	31	91	5.9	18	18	1140	4.12	48	<8	<2	<2	136	.6	<3	<3	27	2.57	.080	7	7	.98	95	<.01	<3	1.36	.08	.18	5	6.8	<.01	4500
C 158341	1	41	112	245	5.9	28	24	2141	4.17	154	<8	<2	<2	139	2.1	4	<3	33	3.46	.081	6	8	1.33	62	<.01	<3	1.32	.05	.15	<2	4.9	.01	2200
C 158342	1	65	19	83	1.4	19	21	1254	4.82	40	<8	<2	2	139	.5	3	<3	26	2.09	.118	9	7	1.14	116	<.01	<3	.87	.09	.17	<2	<2	<.01	4500
STANDARD DS5/R-2/AU-1	12	139	25	132	<.3	23	12	741	2.83	18	<8	<2	3	46	5.4	4	6	58	.72	.092	12	179	.64	137	.09	15	1.98	.03	.12	4	157.2	3.37	-

Sample type: CORE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA ____

E A TIC LAB ORI TD. 85 . H NGS VA JVE V .R6 PH .604 -31 AX( )25 16
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Kodiak Exploration Ltd. File # A304169 Page 1
704 - 525 Seymour St., Vancouver BC V6B 3H7 Submitted by: S. Wetherup

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Ag** gm/mt	Au** gm/mt	Sample gm
SI	<1	1	<3	1	<.3	<1	<1	4	.02	<2	<8	<2	<2	3	<.5	<3	<3	<1	.12	<.001	<1	<1	<.01	2	<.01	<3	.01	.53	<.01	<2	.6	.01	-
C 158344	<1	97	8	94	.5	18	22	944	4.94	37	9	<2	<2	150	<.5	3	<3	22	1.48	.092	5	4	1.23	179	<.01	<3	.72	.11	.21	<2	.5	.02	4200
C 158345	<1.	66	48	149	5.9	16	20	1208	5.21	208	<8	<2	<2	138	.9	10	3	35	1.24	.156	4	6	1.04	176	<.01	<3	1.13	.11	.23	<2	6.5	.02	4600
C 158346	8	81	59	370	12.2	16	19	1189	4.54	264	9	<2	<2	118	2.2	23	<3	24	1.06	.062	2	5	.76	149	<.01	<3	.63	.09	.18	<2	12.6	.03	5500
C 158347	<1	60	6	101	.7	18	20	874	4.49	37	<8	<2	2	147	<.5	<3	<3	23	1.96	.058	4	6	.96	212	<.01	<3	.82	.14	.17	<2	.7	.02	4400
C 158348	<1	82	4	91	<.3	15	18	932	5.13	24	<8	<2	<2	151	<.5	<3	<3	30	2.09	.037	9	7	1.15	175	<.01	<3	1.26	.12	.16	<2	<.3	.02	4700
C 158349	<1	67	6	80	<.3	15	16	839	3.87	23	<8	<2	<2	157	<.5	<3	<3	24	2.39	.061	8	7	.90	156	<.01	<3	1.21	.14	.14	<2	<.3	.02	4000
C 158350	<1	70	18	87	.3	16	20	1039	5.63	34	10	<2	<2	166	<.5	4	<3	53	1.94	.136	9	11	1.32	124	.01	<3	2.45	.08	.19	<2	.3	.02	4500
C 158351	1	74	426	272	32.9	20	22	1335	4.67	>9999	<8	<2	<2	98	2.6	35	<3	24	1.23	.063	2	6	.64	55	.01	<3	1.17	.02	.18	<2	35.2	.94	600
C 158352	<1	106	761	1275	38.3	16	16	1752	4.08	3498	<8	<2	<2	110	14.3	22	<3	26	1.84	.060	3	6	.85	51	<.01	<3	1.22	.02	.16	<2	34.5	.49	1500
C 158353	<1	99	234	722	13.4	15	17	1875	5.04	4803	9	<2	<2	130	7.6	12	<3	36	2.09	.085	3	8	1.26	43	.01	<3	1.62	.01	.13	<2	18.4	.71	2200
C 158354	1	83	190	455	15.0	18	22	1470	4.44	389	<8	<2	<2	131	4.7	11	<3	33	2.05	.077	3	7	1.04	51	<.01	<3	1.43	.01	.11	<2	18.0	.06	2000
C 158355	1	4	14	125	1.4	3	7	1782	3.29	23	<8	<2	<2	326	1.0	4	<3	39	4.75	.148	13	8	1.38	41	<.01	<3	2.07	.01	.15	<2	1.3	.03	1800
C 158356	1	807	>9999	18835	>200	8	5	1472	9.46	>9999	12	<2	3	141	236.2	515	3	10	3.62	.009	1	8	.28	19	<.01	<3	.38	.01	.04	114	580.3	9.38	3100
C 158357	2	126	1716	631	37.6	8	10	2021	6.58	741	10	<2	<2	239	6.7	28	<3	37	5.03	.086	4	6	2.27	47	<.01	<3	2.17	.01	.11	2	39.3	.60	800
C 158358	1	11	39	105	1.1	4	9	809	3.14	28	10	<2	<2	186	.5	3	<3	41	3.04	.144	17	9	1.34	370	<.01	<3	1.82	.04	.17	<2	1.0	.03	4800
C 158359	<1	55	3	58	<.3	15	19	845	4.07	41	<8	<2	2	204	<.5	<3	<3	24	2.13	.038	4	5	.95	66	<.01	<3	.77	.03	.08	<2	<.3	.01	4000
C 158360	<1	71	<3	81	<.3	17	17	924	4.94	19	10	<2	2	198	<.5	<3	3	50	2.52	.097	10	17	1.40	76	<.01	<3	2.14	.07	.11	<2	<.3	.02	4500
C 158361	<1	84	10	97	<.3	18	19	1017	5.15	25	10	<2	2	193	<.5	<3	<3	50	2.75	.121	11	15	1.44	136	<.01	<3	2.27	.06	.11	<2	<.3	.02	4200
C 158362	<1	96	5	86	<.3	17	19	830	4.94	14	<8	<2	2	185	<.5	<3	<3	49	1.68	.043	7	15	1.40	132	<.01	<3	2.47	.08	.14	<2	.3	.01	4100
RE C 158362	<1	102	5	92	<.3	18	20	888	5.28	16	8	<2	2	198	<.5	<3	<3	52	1.80	.045	8	17	1.47	136	<.01	<3	2.65	.09	.15	2	<.3	.02	-
RRE C 158362	<1	98	16	99	.4	16	18	838	5.00	29	<8	<2	2	187	<.5	<3	<3	47	1.71	.043	8	16	1.41	119	<.01	<3	2.40	.08	.11	<2	.3	.01	-
C 158363	<1	90	8	85	<.3	16	18	1024	4.93	19	8	<2	2	161	<.5	<3	3	50	1.99	.077	10	14	1.43	151	<.01	<3	2.42	.11	.15	<2	<.3	.02	4800
C 158364	<1	87	7	93	<.3	18	24	1002	5.12	28	8	<2	<2	161	<.5	<3	<3	49	2.03	.062	10	13	1.44	156	<.01	<3	2.40	.11	.13	<2	<.3	.02	4600
C 158365	1	60	7	87	<.3	17	20	1060	4.58	28	<8	<2	<2	158	<.5	3	<3	44	2.71	.081	6	13	1.35	163	<.01	<3	1.66	.11	.09	<2	.3	.01	4500
C 158366	<1	57	<3	83	<.3	15	16	1043	4.40	18	<8	<2	<2	150	.5	<3	<3	50	2.61	.098	7	15	1.33	156	<.01	<3	1.91	.15	.10	<2	.3	.02	4800
C 158367	1	63	4	81	<.3	15	18	1012	4.79	24	<8	<2	2	173	.5	3	<3	47	2.69	.125	8	13	1.38	148	<.01	<3	2.03	.12	.09	<2	<.3	.01	4900
C 158368	2	67	4	82	.6	17	18	922	4.82	30	8	<2	2	174	<.5	3	<3	55	1.82	.078	8	16	1.33	130	<.01	<3	2.50	.12	.12	<2	.4	.02	4700
C 158369	1	49	<3	71	.6	18	18	1332	5.04	21	8	<2	2	147	<.5	3	<3	56	2.78	.068	6	21	1.38	111	.01	<3	2.01	.10	.09	<2	.7	.03	4300
C 158370	1	49	9	85	.5	19	19	1858	4.62	29	14	<2	2	195	<.5	<3	<3	48	5.56	.106	7	16	1.37	128	<.01	<3	1.51	.11	.11	<2	.4	.01	5000
C 158371	1	45	13	124	.4	30	26	2934	5.16	44	<8	<2	<2	195	.6	<3	<3	87	7.62	.097	7	38	1.51	103	<.01	<3	1.28	.07	.08	<2	.4	.01	5800
C 158372	1	39	19	106	.3	17	16	3334	3.40	34	<8	<2	<2	263	.5	3	<3	29	11.37	.086	7	8	1.11	112	<.01	<3	.70	.09	.10	<2	<.3	.02	4500
C 158373	1	50	7	85	<.3	21	19	1545	4.72	26	<8	<2	<2	206	<.5	<3	<3	48	4.17	.081	8	17	1.34	134	<.01	<3	1.78	.11	.09	<2	<.3	.01	4700
C 158374	1	48	6	61	1.3	17	19	1297	4.49	38	<8	<2	<2	226	<.5	3	<3	30	3.80	.082	6	8	1.21	138	<.01	<3	1.60	.12	.10	<2	1.0	.01	4500
C 158375	2	68	<3	84	1.4	14	18	847	4.88	44	<8	<2	<2	187	.6	<3	<3	44	1.43	.103	7	8	1.31	122	<.01	<3	2.41	.09	.10	<2	.9	.01	4400
STANDARD DS5/R-2/AU-1	12	140	23	131	<.3	23	12	758	2.92	18	11	<2	3	48	5.3	5	7	58	.73	.096	12	185	.65	142	.09	16	2.05	.03	.11	4	153.7	3.39	-

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
AG** & AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: CORE R150 60C <u>Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.</u>

DATE RECEIVED: SEP 5 2003 **DATE REPORT MAILED:** Sep 24/2003 **SIGNED BY** ....D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data ✓ FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Ag** gm/mt	Au** gm/mt	Sample gm
C 158376	<1	80	4	112	1.3	16	18	765	4.54	57	<8	<2	<2	204	1.0	<3	<3	49	1.13	.069	6	10	1.28	151	<.01	<3	2.53	.13	.12	<2	1.4	<.01	4500
C 158377	<1	67	<3	58	.8	19	18	1026	4.58	52	<8	<2	<2	248	.6	<3	<3	40	2.15	.091	8	9	1.25	151	.01	<3	2.48	.13	.13	<2	.8	<.01	4700
C 158378	<1	69	3	80	.9	17	18	973	4.38	40	<8	<2	<2	244	.5	<3	3	42	2.05	.065	6	10	1.26	141	<.01	<3	2.44	.12	.12	<2	.9	<.01	4200
C 158379	1	66	4	70	.9	16	17	918	4.27	46	<8	<2	<2	257	<.5	<3	3	37	2.43	.077	8	8	1.24	141	<.01	<3	2.32	.12	.12	<2	.9	<.01	4700
C 158380	6	62	5	62	1.4	14	16	787	4.21	30	<8	<2	2	229	<.5	5	<3	42	1.69	.063	5	10	1.27	130	<.01	<3	2.40	.12	.10	<2	1.4	.01	5000
C 158381	<1	71	<3	76	.8	16	17	850	4.44	36	<8	<2	2	248	<.5	<3	3	45	2.26	.071	11	11	1.16	155	<.01	<3	2.47	.13	.13	<2	.8	<.01	4000
C 158382	1	57	5	81	.6	19	20	1001	4.87	40	<8	<2	2	230	.5	4	<3	52	3.04	.104	6	17	1.36	186	<.01	<3	2.37	.18	.14	<2	.6	<.01	4800
C 158383	1	59	<3	94	.3	18	20	1017	4.77	33	<8	<2	2	199	<.5	<3	<3	51	2.84	.101	8	18	1.34	172	<.01	<3	2.14	.17	.12	<2	<.3	<.01	5400
C 158384	1	60	5	81	.6	14	16	1037	4.41	22	<8	<2	2	257	.5	3	<3	52	2.76	.067	8	14	1.27	129	<.01	<3	2.50	.14	.10	<2	.3	<.01	4900
C 158385	1	54	4	83	<.3	16	16	1434	4.39	12	<8	<2	2	214	<.5	<3	<3	60	4.56	.077	7	20	1.27	118	<.01	<3	2.26	.15	.11	<2	<.3	<.01	4000
C 158386	1	66	5	88	<.3	15	17	968	4.59	10	<8	<2	<2	138	<.5	<3	<3	54	2.22	.087	8	16	1.35	132	<.01	<3	2.23	.16	.12	<2	<.3	.01	4200
C 158387	<1	91	5	85	<.3	16	16	899	4.82	7	<8	<2	<2	174	<.5	<3	<3	54	1.90	.061	10	14	1.40	123	.01	<3	2.46	.15	.13	<2	<.3	<.01	5500
C 158388	1	77	4	86	<.3	17	17	1035	5.01	10	<8	<2	<2	232	.5	<3	4	55	3.44	.332	10	15	1.43	111	<.01	<3	2.51	.14	.13	<2	<.3	<.01	4400
C 158389	<1	68	<3	89	.3	21	19	955	4.81	22	<8	<2	2	240	.6	3	<3	56	2.63	.060	6	15	1.35	115	<.01	<3	2.42	.16	.11	<2	.4	<.01	4500
C 158390	<1	75	4	92	<.3	16	16	994	4.48	6	<8	<2	<2	169	<.5	<3	<3	54	2.36	.094	12	16	1.42	108	<.01	<3	2.19	.16	.11	<2	<.3	<.01	4000
RE C 158390	<1	73	8	91	<.3	16	16	986	4.44	7	<8	<2	2	167	<.5	5	<3	54	2.33	.093	12	16	1.41	109	<.01	<3	2.17	.16	.11	<2	.3	<.01	-
RRE C 158390	<1	75	5	93	<.3	17	16	1016	4.54	5	<8	<2	<2	175	.5	<3	3	55	2.41	.093	12	18	1.44	115	<.01	<3	2.28	.17	.12	<2	<.3	<.01	-
C 158391	<1	66	7	86	<.3	16	16	1012	4.48	8	<8	<2	<2	161	.6	<3	<3	48	2.26	.071	10	15	1.45	106	<.01	<3	2.11	.15	.12	<2	<.3	<.01	4100
C 158392	<1	71	4	92	<.3	23	19	1324	5.12	4	<8	<2	<2	190	.5	<3	3	60	3.19	.095	10	20	1.53	121	<.01	<3	2.17	.15	.12	<2	<.3	<.01	4500
C 158393	<1	75	3	95	.5	21	20	1047	4.87	24	<8	<2	<2	265	.6	<3	<3	56	2.69	.052	6	16	1.40	95	<.01	<3	2.51	.12	.10	<2	.3	<.01	4300
C 158394	3	62	<3	86	.7	25	24	865	5.03	39	<8	<2	2	207	.5	6	4	71	1.86	.064	5	20	1.29	102	<.01	<3	2.70	.13	.11	2	.7	<.01	4000
C 158395	1	75	4	103	.3	19	20	805	5.09	13	<8	<2	<2	174	.5	<3	3	76	1.51	.100	7	22	1.06	101	<.01	<3	2.88	.13	.12	<2	<.3	<.01	4100
C 158396	1	71	5	95	.6	18	20	915	4.90	10	<8	<2	<2	200	.5	<3	<3	70	1.97	.158	8	19	1.06	103	<.01	<3	2.83	.13	.12	<2	<.3	<.01	4100
C 158397	2	69	3	100	.3	18	21	917	4.92	13	<8	<2	2	196	.5	<3	<3	61	1.79	.106	11	16	1.18	113	<.01	<3	2.67	.13	.12	<2	<.3	<.01	3500
C 158398	<1	65	4	96	.6	20	22	1068	4.89	29	<8	<2	2	209	.5	<3	<3	55	2.40	.068	8	14	1.04	134	<.01	<3	2.44	.14	.14	<2	.7	<.01	5200
C 158399	<1	30	24	86	.3	10	12	1523	3.43	17	<8	<2	<2	153	.5	<3	<3	37	4.00	.083	8	11	1.00	73	<.01	<3	1.57	.03	.14	<2	<.3	<.01	3000
C 158400	4	30	141	225	1.1	6	11	1656	2.85	62	<8	<2	<2	119	2.0	<3	<3	16	3.61	.086	8	5	.86	73	<.01	<3	.91	.03	.20	<2	1.5	.04	3100
C 158401	<1	60	10	74	1.7	15	17	1005	3.53	1509	<8	<2	<2	72	.6	10	<3	28	2.17	.077	5	7	.80	75	<.01	<3	1.51	.03	.14	<2	1.5	.04	1500
C 158402	<1	42	13	94	2.1	21	20	1257	5.17	1122	<8	<2	<2	88	.8	5	<3	46	2.38	.080	4	13	1.41	49	<.01	<3	2.27	.02	.14	<2	1.9	.09	1400
C 158403	<1	66	6	29	12.2	14	16	2123	4.66	140	<8	<2	<2	185	.5	8	<3	32	5.15	.053	3	5	1.47	59	<.01	<3	1.78	.02	.14	<2	11.8	.02	1100
C 158404	<1	45	14	75	.8	20	20	1517	4.72	76	<8	<2	<2	163	.6	<3	<3	46	3.82	.083	8	13	1.48	42	<.01	<3	2.40	.02	.14	<2	.8	.02	2700
C 158405	<1	40	4	69	.4	21	20	1606	4.77	53	<8	<2	<2	113	<.5	<3	<3	47	3.74	.087	7	12	1.60	41	<.01	<3	1.61	.03	.12	<2	.4	<.01	5400
C 158406	1	42	24	98	.5	21	20	1990	4.29	58	9	<2	<2	181	<.5	4	<3	38	4.42	.081	7	10	1.60	47	<.01	<3	1.51	.03	.13	<2	1.0	<.01	5500
C 158407	<1	63	3	77	.6	19	20	1007	4.68	64	<8	<2	<2	119	<.5	<3	<3	32	2.05	.063	6	9	1.32	83	<.01	<3	2.07	.04	.17	<2	.9	<.01	5200
STANDARD DS5	12	143	23	134	.3	25	12	768	2.94	18	<8	<2	3	49	5.7	6	6	61	.75	.094	12	191	.64	140	.10	14	2.09	.04	.11	4	151.0	3.32	-

Standard is STANDARD DS5/R-2/AU-1. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Ag** gm/mt	Au** gm/mt	Sample gm
C 158408	<1	63	8	91	<.3	17	18	928	4.53	37	<8	<2	<2	115	<.5	<3	<3	21	2.12	.082	8	6	1.10	89	<.01	<3	1.28	.04	.13	<2	.8	.01	4900
C 158409	<1	83	8	102	.6	16	17	764	5.11	161	<8	<2	2	110	<.5	<3	3	25	1.27	.067	8	7	1.27	103	<.01	<3	1.96	.02	.14	<2	1.0	.01	4800
C 158410	<1	94	10	91	<.3	22	23	844	4.49	48	<8	<2	<2	168	<.5	<3	<3	20	2.06	.063	10	5	1.12	89	<.01	<3	1.35	.02	.15	<2	.6	<.01	5000
C 158411	1	49	22	98	<.3	17	19	1039	4.90	45	<8	<2	<2	217	.6	<3	3	31	3.07	.108	7	7	1.16	49	<.01	<3	1.83	.03	.12	<2	<.3	.01	5500
C 158412	1	75	5	84	.8	17	18	828	4.52	53	<8	<2	<2	190	<.5	3	<3	26	2.44	.106	6	6	1.04	54	<.01	<3	1.63	.03	.13	<2	1.0	<.01	5100
C 158413	1	83	360	277	3.5	18	19	1010	4.58	710	<8	<2	<2	194	2.5	6	3	35	2.70	.070	3	8	1.00	91	<.01	<3	1.85	.06	.12	<2	4.0	.24	3500
C 158414	<1	58	6	70	<.3	15	16	711	3.96	34	<8	<2	<2	132	<.5	<3	<3	22	1.45	.056	6	5	.87	42	<.01	<3	1.30	.01	.10	<2	.4	.01	4000
C 158415	1	56	3	108	<.3	17	19	1027	5.14	28	<8	<2	2	221	.7	3	<3	37	2.76	.111	6	10	1.26	64	<.01	<3	2.24	.02	.11	<2	<.3	<.01	4100
C 158416	4	63	53	149	.8	12	15	1401	4.30	29	<8	<2	<2	222	.9	<3	<3	34	3.61	.049	6	7	1.01	74	<.01	<3	1.89	.02	.11	<2	.9	.04	3900
C 158417	<1	64	59	73	2.2	18	21	987	5.33	67	<8	<2	<2	162	.6	4	<3	49	1.44	.063	7	12	1.34	61	<.01	<3	2.49	.02	.11	<2	1.9	.19	1500
C 158418	3	34	65	1661	2.9	22	25	1446	4.46	114	<8	<2	<2	244	13.9	9	<3	39	3.68	.062	3	6	1.07	36	<.01	<3	1.85	.02	.10	3	3.8	.08	1200
C 158419	2	66	12	274	2.3	14	16	1212	3.13	60	<8	<2	<2	222	2.6	<3	<3	35	2.78	.083	6	7	.94	52	<.01	<3	1.72	.03	.11	<2	2.9	.09	1500
C 158420	4	65	40	105	4.1	13	16	1545	4.63	129	<8	<2	<2	238	.9	4	<3	42	3.34	.056	3	6	1.25	49	<.01	<3	1.97	.02	.09	<2	4.2	.20	1700
C 158421	5	50	7	28	2.8	14	17	875	4.28	54	<8	<2	<2	175	<.5	3	<3	41	1.66	.078	5	8	1.12	48	<.01	<3	2.00	.02	.09	<2	3.5	.14	1400
C 158422	2	85	84	36	3.5	17	20	1296	4.63	350	<8	<2	<2	218	.5	8	3	34	3.20	.069	3	7	.95	47	<.01	<3	1.70	.01	.11	<2	3.3	.33	1500
C 158423	<1	54	33	64	3.6	18	21	1371	4.44	87	<8	<2	<2	187	.6	3	<3	40	2.51	.058	3	9	1.08	35	<.01	<3	1.89	.01	.09	<2	3.8	.12	1800
C 158424	<1	50	46	99	5.2	16	17	1918	3.86	332	<8	<2	<2	209	1.0	6	<3	38	2.97	.070	4	8	1.14	38	<.01	<3	1.80	.01	.11	<2	5.4	.27	2000
C 158425	<1	62	87	121	9.8	22	23	1775	4.29	1632	<8	<2	<2	182	1.1	14	<3	39	2.33	.095	5	9	1.07	24	<.01	<3	1.74	.01	.10	<2	9.2	.21	2100
C 158426	<1	94	187	76	6.9	16	19	1207	4.45	857	<8	<2	<2	176	.8	8	<3	31	2.09	.094	3	6	.78	60	<.01	4	1.57	.01	.12	<2	6.7	.81	5400
RE C 158426	1	97	177	64	7.1	17	19	1224	4.52	871	<8	<2	<2	179	.7	10	<3	32	2.12	.093	3	7	.79	60	<.01	<3	1.58	.01	.12	<2	7.3	.87	-
RRE C 158426	<1	98	168	51	6.7	17	19	1173	4.37	852	<8	<2	<2	170	.5	9	<3	30	2.04	.089	3	6	.75	57	<.01	<3	1.52	.01	.12	<2	7.0	.89	-
C 158427	<1	58	4	75	.7	17	19	1136	4.92	105	<8	<2	<2	188	<.5	<3	<3	44	2.58	.110	6	10	1.20	53	<.01	<3	1.85	.02	.11	<2	1.1	.02	2500
C 158428	<1	56	6	71	<.3	16	17	1049	4.73	37	<8	<2	<2	184	<.5	<3	<3	34	2.99	.132	6	7	1.23	50	<.01	<3	1.31	.03	.13	<2	.3	.01	5800
C 158429	<1	72	7	30	.8	17	19	934	4.45	64	<8	<2	<2	184	<.5	<3	<3	34	2.51	.081	6	6	1.14	60	<.01	<3	1.69	.02	.11	<2	.8	<.01	6100
C 158430	<1	77	7	73	1.4	16	20	816	4.71	61	<8	<2	2	158	.6	<3	<3	40	1.46	.065	9	7	1.25	99	<.01	<3	2.12	.02	.11	<2	1.2	<.01	5400
C 158431	<1	71	6	24	.9	19	20	920	4.34	48	<8	<2	2	186	<.5	<3	<3	38	2.09	.054	6	8	1.14	62	<.01	<3	1.91	.02	.12	<2	.8	.01	6100
C 158432	<1	53	5	47	.5	18	19	706	4.48	46	<8	<2	2	147	<.5	<3	<3	46	1.42	.078	8	10	1.23	86	<.01	<3	2.16	.02	.11	<2	.3	.01	3500
C 158433	<1	54	4	25	1.0	13	15	1202	4.72	50	<8	<2	<2	185	<.5	<3	<3	36	3.02	.104	5	7	1.22	55	<.01	<3	1.88	.02	.11	<2	.6	.02	4000
C 158434	<1	56	25	120	.5	21	21	1655	5.18	68	<8	<2	<2	182	.6	<3	<3	49	3.59	.088	6	11	1.28	36	<.01	<3	1.75	.02	.13	<2	.8	.01	3500
C 158435	<1	71	<3	61	.3	17	19	1049	4.47	53	<8	<2	2	152	<.5	<3	<3	31	2.43	.092	6	6	1.01	57	<.01	<3	1.37	.02	.12	<2	.3	.01	3400
C 158436	<1	93	46	44	1.3	14	17	1064	4.27	33	<8	<2	<2	186	<.5	3	<3	25	3.30	.052	5	4	1.20	73	<.01	<3	1.10	.02	.12	<2	1.8	.01	3600
C 158437	<1	64	10	31	2.2	18	18	1048	4.26	75	<8	<2	<2	187	<.5	4	<3	27	3.15	.076	4	6	1.09	48	<.01	<3	1.18	.02	.12	<2	2.1	<.01	3800
C 158438	<1	40	22	36	4.5	19	21	1278	4.31	1270	<8	<2	<2	148	<.5	9	<3	26	2.63	.103	3	5	.79	46	<.01	<3	1.10	.02	.13	<2	4.3	.05	3700
C 158439	1	53	10	32	3.3	16	19	1547	4.55	898	<8	<2	<2	150	<.5	11	<3	31	2.64	.085	1	6	1.00	45	<.01	<3	1.36	.02	.12	2	2.9	.04	3500
STANDARD DS5	12	143	23	131	<.3	25	12	756	2.89	20	<8	<2	3	49	5.6	4	6	58	.72	.093	12	186	.65	135	.09	16	2.05	.04	.11	4	153.8	3.35	-

Standard is STANDARD DS5/R-2/AU-1. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Ag** gm/mt	Au** gm/mt	Sample gm
C 158440	8	45	14	31	4.6	13	16	1107	3.41	78	<8	<2	<2	137	<.5	5	<3	30	1.71	.073	3	7	.79	34	<.01	<3	1.44	.02	.12	<2	4.2	.02	3800
C 158441	1	38	10	22	3.1	17	19	1466	4.76	63	<8	<2	<2	176	<.5	4	<3	35	2.71	.111	4	9	1.14	36	<.01	<3	1.58	.03	.12	<2	2.7	.02	3900
C 158442	2	41	19	71	1.6	16	18	1472	4.30	64	<8	<2	<2	172	.5	<3	<3	26	3.76	.302	6	6	1.07	61	<.01	<3	.96	.03	.23	<2	1.2	.01	3700
C 158443	1	42	7	45	.9	16	19	1367	4.21	53	<8	<2	<2	129	<.5	4	<3	25	2.76	.119	6	6	.97	65	<.01	<3	.78	.04	.12	<2	1.3	.01	4300
C 158444	2	53	8	20	1.1	15	18	1660	4.26	398	<8	<2	<2	127	<.5	5	<3	21	2.74	.077	5	6	.97	81	<.01	<3	.55	.05	.13	<2	.8	.06	6600
C 158445	6	60	28	37	1.6	14	17	1337	3.43	127	<8	<2	<2	134	<.5	4	<3	19	2.70	.070	4	5	.79	56	<.01	<3	.86	.05	.12	<2	1.6	.04	2000
C 158446	<1	30	12	27	1.0	13	17	1376	4.14	41	<8	<2	<2	151	<.5	<3	<3	24	3.76	.049	4	6	1.01	56	<.01	<3	1.18	.04	.12	<2	1.2	.01	2100
C 158447	<1	21	67	94	3.8	12	14	1932	5.65	96	<8	<2	<2	267	.8	3	<3	34	4.87	.071	2	8	1.33	36	<.01	<3	1.58	.02	.10	<2	3.9	.07	2000
C 158448	<1	73	61	985	15.4	17	17	1327	4.93	36	<8	<2	<2	222	7.1	7	<3	40	2.80	.082	7	10	1.11	56	<.01	<3	2.30	.04	.11	<2	16.2	.01	2500
C 158449	<1	84	71	505	20.8	16	18	1448	5.04	35	<8	<2	<2	217	3.4	<3	<3	29	3.08	.072	6	8	1.26	61	<.01	<3	2.02	.05	.11	<2	20.8	.01	3500
C 158450	<1	59	65	379	8.9	17	16	1213	4.45	45	<8	<2	2	190	3.1	3	<3	27	2.59	.075	7	8	.95	72	<.01	<3	1.89	.05	.12	<2	10.7	<.01	3700
C 158451	2	15	60	503	1.3	9	9	4336	5.33	26	<8	<2	<2	552	3.7	<3	<3	39	8.38	.171	9	8	1.69	59	<.01	<3	2.22	.03	.07	<2	1.4	.01	1900
C 158452	1	59	124	228	1.7	23	20	1570	4.16	74	<8	2	2	236	1.6	<3	<3	42	3.35	.076	6	12	.97	71	<.01	<3	1.94	.05	.11	<2	1.5	.01	1700
C 158453	1	31	20	31	1.9	16	17	2038	3.99	55	<8	<2	<2	179	<.5	<3	<3	22	4.43	.056	4	5	1.07	58	<.01	<3	1.01	.05	.09	<2	2.2	<.01	2100
C 158454	<1	41	8	71	1.6	18	17	1256	4.68	46	<8	<2	2	122	.6	<3	<3	27	2.51	.067	6	8	1.02	63	<.01	<3	1.56	.05	.12	<2	1.6	<.01	1500
C 158455	<1	77	48	48	15.4	16	14	2406	5.39	57	<8	<2	<2	250	.5	5	<3	40	5.36	.054	3	9	1.24	50	<.01	<3	1.99	.03	.09	<2	16.2	.04	2200
C 158456	1	41	229	619	2.9	17	19	2235	3.64	48	<8	<2	<2	251	4.4	<3	<3	30	4.87	.108	7	9	.96	67	<.01	<3	1.44	.04	.10	<2	3.6	<.01	3200
C 158457	1	38	182	544	2.7	13	13	3127	4.38	33	<8	<2	<2	276	3.7	<3	<3	29	6.46	.110	6	7	1.43	67	<.01	<3	1.35	.04	.11	<2	3.3	.01	3300
C 158458	<1	38	222	2090	7.7	16	17	2001	4.79	53	<8	<2	2	212	14.8	4	<3	39	3.75	.112	5	8	1.31	55	<.01	<3	1.99	.03	.11	2	7.0	.01	3000
C 158459	<1	53	40	219	3.0	17	20	1242	4.55	47	<8	<2	<2	165	1.5	<3	<3	35	2.32	.060	6	9	1.02	80	<.01	<3	2.02	.04	.12	<2	3.0	.01	3800
C 158460	<1	30	88	233	2.3	14	14	1456	5.13	63	11	<2	<2	207	1.9	<3	<3	39	2.98	.058	4	9	1.03	78	<.01	<3	1.99	.05	.12	<2	2.6	.04	1500
RE C 158460	<1	33	83	241	2.9	15	14	1446	5.07	59	<8	<2	2	204	1.8	<3	<3	38	2.97	.058	3	8	1.02	78	<.01	<3	1.96	.05	.12	<2	3.1	.04	-
RRE C 158460	<1	39	99	222	3.0	16	15	1521	5.18	67	<8	<2	<2	213	1.9	3	<3	39	3.21	.056	3	8	1.03	81	<.01	<3	1.98	.04	.12	<2	2.7	.04	-
C 158461	<1	39	204	106	2.7	14	16	912	4.06	82	8	<2	<2	139	.8	<3	<3	30	1.63	.013	3	6	.71	108	<.01	<3	1.72	.06	.14	<2	3.1	.02	1700
C 158462	<1	69	102	127	3.9	15	14	1221	4.05	138	8	<2	<2	196	1.1	4	<3	29	3.28	.060	3	6	.78	71	<.01	<3	1.59	.04	.10	<2	4.3	.05	2100
C 158463	1	51	26	40	2.1	14	15	823	2.81	46	<8	<2	2	178	<.5	<3	<3	29	2.41	.081	6	7	.78	100	<.01	<3	1.42	.06	.12	<2	2.5	<.01	3000
C 158464	1	65	78	504	2.2	15	15	762	3.44	105	<8	<2	<2	134	4.2	<3	<3	29	1.76	.078	4	7	.78	94	<.01	3	1.55	.05	.13	<2	3.2	.01	3100
C 158465	<1	73	45	227	2.7	16	17	794	4.09	51	<8	<2	<2	111	1.7	<3	<3	33	1.31	.077	6	7	.86	94	<.01	<3	1.79	.05	.14	<2	2.9	.01	3800
C 158466	1	55	20	55	3.0	15	13	2662	3.56	278	<8	<2	<2	287	.5	6	<3	25	5.02	.013	3	5	.94	96	<.01	<3	1.69	.05	.11	<2	3.5	.04	3400
C 158467	<1	68	10	56	2.4	17	17	1343	4.70	189	<8	<2	<2	131	<.5	<3	<3	38	2.34	.056	4	9	1.04	115	<.01	<3	1.91	.06	.11	<2	2.7	.05	3600
C 158468	3	22	49	57	3.5	24	36	1074	3.42	338	<8	<2	<2	125	<.5	11	<3	34	2.38	.042	1	5	.90	31	<.01	<3	1.27	.02	.02	<2	4.1	.04	2000
C 158469	3	71	5	87	1.9	20	22	726	5.24	84	<8	<2	<2	126	.5	3	<3	46	.94	.048	5	9	1.20	152	<.01	<3	2.18	.08	.13	<2	2.1	.04	3000
C 158470	2	80	4	93	2.4	14	17	1193	4.99	81	9	<2	<2	188	<.5	<3	<3	44	2.20	.050	4	10	1.20	140	<.01	<3	2.09	.07	.11	<2	3.1	.08	4600
C 158471	3	48	19	102	2.8	20	22	1234	3.48	321	9	<2	2	182	.5	7	<3	30	2.65	.041	4	5	.89	98	<.01	<3	1.44	.05	.09	<2	2.8	.10	2500
STANDARD DS5/R-2/AU-1	12	138	21	130	<.3	24	12	736	2.86	17	<8	<2	3	47	5.3	4	5	58	.72	.088	12	180	.64	136	.09	15	2.01	.04	.11	3	156.2	3.30	-

Sample type: CORE R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data___ FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Ag** gm/mt	Au** gm/mt	Sample gm
C 158472	<1	102	13	47	3.2	12	7	543	3.70	447	<8	<2	<2	106	<.5	5	<3	23	.72	.012	4	4	.63	119	<.01	<3	1.28	.06	.16	<2	3.3	.15	1400
C 158473	<1	71	18	94	2.1	17	17	961	4.70	223	<8	<2	<2	124	.6	<3	<3	39	1.43	.045	4	9	.93	116	<.01	<3	1.99	.06	.19	<2	1.6	.06	1200
C 158474	<1	85	13	67	3.0	13	16	1023	3.94	180	<8	<2	<2	154	.5	4	<3	23	2.07	.009	3	4	.72	111	<.01	<3	1.52	.05	.16	<2	3.0	.08	1800
C 158475	<1	73.	6	57	1.5	13	14	798	4.45	114	<8	<2	2	98	<.5	6	<3	33	.89	.008	11	7	1.05	124	<.01	<3	2.08	.06	.17	<2	1.5	.01	2000
C 158476	<1	103	61	51	7.3	16	16	1815	5.67	2048	<8	<2	<2	256	.7	7	<3	29	3.93	.147	4	5	.73	80	<.01	<3	1.58	.05	.18	<2	7.2	.86	1700
C 158477	<1	103	108	40	11.8	17	18	1473	5.52	3456	<8	<2	2	176	<.5	8	<3	31	2.35	.154	4	6	.71	65	.01	3	1.66	.06	.25	<2	10.8	1.42	1900
C 158478	1	32	64	16	3.9	15	14	1723	4.43	7276	<8	<2	<2	235	<.5	6	4	18	3.51	.029	2	3	.52	75	<.01	<3	.96	.05	.14	<2	3.9	2.20	600
C 158479	3	66	42	28	4.7	17	19	1516	3.95	838	<8	<2	2	254	<.5	7	<3	28	3.99	.035	2	4	.69	92	<.01	<3	1.31	.04	.14	<2	5.4	.71	1500
C 158480	1	74	65	30	3.2	15	17	1352	3.98	1266	<8	<2	2	212	<.5	5	<3	29	3.08	.170	5	6	.66	95	<.01	<3	1.43	.05	.16	<2	3.2	.63	1100
C 158481	31	67	48	25	2.2	29	43	1158	3.68	102	<8	<2	<2	206	<.5	6	<3	44	2.86	.064	8	9	.95	108	<.01	<3	1.90	.06	.16	<2	1.7	.01	600
C 158482	4	65	5	87	.8	17	21	840	4.61	56	<8	<2	<2	158	.6	4	<3	37	2.07	.068	7	8	1.00	148	<.01	<3	1.77	.07	.16	<2	.8	.01	4900
C 158483	1	61	8	112	.9	19	22	881	4.34	48	<8	<2	<2	171	.5	<3	<3	40	2.48	.055	6	9	.96	139	<.01	<3	1.68	.07	.19	<2	.9	<.01	4300
C 158484	1	72	7	85	.7	17	18	881	4.89	33	<8	<2	2	159	<.5	<3	<3	36	2.26	.220	9	9	1.02	192	<.01	3	1.77	.08	.25	<2	.7	<.01	4700
RE C 158484	1	70	6	86	.4	15	17	861	4.80	32	<8	<2	<2	155	<.5	<3	<3	34	2.22	.217	9	8	.99	188	<.01	<3	1.75	.08	.24	<2	.4	<.01	-
RRE C 158484	1	68	7	82	.4	17	17	848	4.73	32	<8	<2	2	154	<.5	<3	<3	32	2.23	.230	9	8	.98	172	<.01	<3	1.58	.07	.19	<2	.4	<.01	-
C 158485	<1	68	8	126	<.3	16	18	998	4.38	60	<8	<2	<2	172	<.5	<3	<3	29	2.78	.049	5	7	.98	155	<.01	<3	1.68	.08	.19	<2	<.3	<.01	4600
C 158486	<1	57	16	103	.7	16	17	956	3.68	122	<8	<2	<2	165	<.5	3	<3	24	3.04	.115	5	6	.93	156	<.01	<3	1.04	.08	.16	<2	.8	.01	4700
C 158487	<1	53	11	97	<.3	19	18	1222	4.57	49	<8	<2	<2	170	.5	<3	<3	41	3.17	.066	8	11	1.14	133	<.01	<3	1.68	.07	.17	<2	<.3	<.01	5100
C 158488	<1	55	9	79	.3	18	17	944	4.45	45	<8	<2	2	138	<.5	5	<3	38	2.00	.073	9	9	1.08	112	<.01	3	2.01	.06	.13	<2	<.3	<.01	4000
C 158489	<1	51	8	86	<.3	23	23	1405	5.73	60	<8	<2	<2	202	.5	<3	<3	43	3.28	.125	7	13	1.22	125	<.01	<3	2.34	.06	.19	<2	<.3	.01	5200
C 158490	1	51	5	72	.6	17	19	1158	5.48	48	<8	<2	2	212	.5	4	<3	39	2.64	.147	7	11	1.26	117	<.01	<3	2.47	.06	.14	<2	.6	.01	5100
C 158491	<1	63	10	41	.9	18	18	946	5.09	41	<8	<2	2	166	<.5	3	<3	40	2.07	.085	10	10	1.13	126	<.01	<3	2.26	.07	.18	<2	<.3	.01	4500
C 158492	<1	60	13	50	.8	14	14	1075	4.02	39	8	<2	2	184	<.5	<3	<3	29	2.94	.079	7	7	1.00	119	<.01	<3	1.74	.08	.17	<2	.8	.03	5100
C 158493	<1	55	7	81	<.3	18	19	1113	4.99	36	<8	<2	<2	209	<.5	<3	<3	32	2.89	.067	7	8	1.12	116	<.01	<3	2.14	.07	.14	<2	<.3	<.01	3700
C 158494	<1	53	4	78	.5	15	18	1169	4.60	36	<8	<2	<2	222	<.5	<3	<3	31	2.78	.067	8	8	1.07	136	<.01	<3	2.09	.08	.19	<2	.5	.02	4100
C 158495	<1	54	<3	83	.7	18	19	1160	4.99	39	<8	<2	2	213	<.5	3	<3	34	2.66	.074	8	11	1.17	131	<.01	<3	2.09	.08	.13	<2	.7	.01	4700
C 158496	2	54	6	76	.7	16	17	965	4.10	33	<8	<2	<2	184	<.5	<3	<3	33	2.53	.075	8	8	1.03	147	<.01	<3	1.71	.09	.16	<2	.7	<.01	4600
C 158497	<1	57	15	82	.8	15	16	1239	3.72	52	<8	<2	2	172	<.5	4	<3	26	3.17	.075	7	6	1.00	158	<.01	<3	1.28	.08	.13	<2	1.2	.01	4000
C 158498	<1	51	7	45	.5	16	16	1502	4.27	95	<8	<2	<2	160	<.5	<3	<3	25	3.30	.071	7	6	1.11	180	<.01	<3	1.32	.09	.17	<2	.3	<.01	1400
C 158499	<1	45	10	78	1.9	20	18	2219	4.91	414	<8	<2	<2	239	.6	3	<3	38	4.47	.078	5	10	1.39	114	<.01	<3	2.13	.06	.12	<2	.6	.02	3800
C 158500/C 158501	<1	74	6	78	1.1	15	15	1968	3.40	40	<8	<2	<2	347	.6	<3	<3	29	5.13	.048	8	6	.96	129	<.01	<3	1.81	.07	.10	<2	1.6	<.01	1500
C 158502	1	56	<3	60	.6	17	20	1776	4.92	64	<8	<2	<2	237	.5	<3	<3	43	3.19	.102	8	11	1.11	164	<.01	<3	2.45	.09	.16	<2	.6	.01	1800
C 158503	1	52	12	89	<.3	19	21	1745	4.85	276	<8	<2	2	184	.6	<3	<3	32	3.56	.107	7	10	1.18	161	<.01	<3	1.63	.08	.13	<2	<.3	.05	2100
C 158504	1	41	20	84	<.3	15	17	2957	3.68	39	<8	<2	<2	267	<.5	<3	<3	26	7.83	.108	9	6	.99	164	<.01	<3	1.27	.09	.14	<2	<.3	<.01	4700
STANDARD DS5/R-2/	12	133	24	128	<.3	23	11	706	2.78	18	<8	<2	3	46	5.3	4	6	57	.72	.087	11	178	.62	133	.08	16	1.94	.04	.13	3	155.0	3.38	-

Standard is STANDARD DS5/R-2/AU-1. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Ag** gm/mt	Au** gm/mt	Sample gm
C 158505	<1	65	<3	71	<.3	19	22	1174	4.56	32	<8	<2	2	162	<.5	<3	<3	29	2.78	.083	10	9	1.18	158	<.01	<3	1.60	.11	.11	<2	<.3	.01	5500
C 158506	<1	68	3	77	.4	20	21	1202	4.61	39	<8	<2	2	175	<.5	<3	<3	24	2.80	.074	9	7	1.13	181	<.01	<3	1.38	.11	.09	<2	.5	.01	4200
C 158507	<1	65	<3	81	.3	18	19	1168	4.63	40	<8	<2	2	148	<.5	<3	<3	22	2.45	.099	11	6	1.03	203	<.01	<3	1.16	.13	.12	<2	.4	<.01	5000
C 158508	<1	61	7	85	.8	16	17	1026	5.18	37	<8	<2	2	157	<.5	5	<3	33	1.85	.051	7	8	1.33	151	<.01	<3	2.28	.09	.10	<2	.8	.01	3800
C 158509	<1	66	11	91	1.4	18	21	791	4.97	42	8	<2	2	137	<.5	<3	<3	42	1.49	.185	8	10	1.30	140	<.01	<3	2.21	.08	.12	<2	1.1	<.01	3600
C 158510	<1	88	96	575	2.3	16	16	1316	3.78	469	<8	<2	<2	149	6.0	4	<3	23	2.56	.083	5	6	.83	133	<.01	<3	1.05	.08	.12	<2	1.8	.16	3000
C 158511	<1	69	118	460	2.8	18	19	1501	5.18	528	<8	<2	<2	138	5.0	4	<3	35	2.13	.070	4	8	1.19	109	<.01	<3	1.78	.07	.10	<2	2.6	.21	1700
C 158512	<1	101	683	1224	4.1	22	22	1804	4.90	346	<8	<2	2	119	12.0	5	<3	56	2.16	.060	3	14	1.04	88	<.01	<3	1.60	.05	.10	<2	3.6	.28	1600
C 158513	<1	110	329	491	15.2	12	11	951	3.94	1908	<8	<2	<2	125	5.5	8	<3	12	1.55	.017	1	2	.35	64	<.01	<3	.59	.05	.11	<2	15.2	.87	1700
C 158514	<1	56	873	616	14.0	12	13	1008	4.72	2691	<8	<2	<2	129	5.9	11	<3	13	1.32	.015	1	4	.30	45	<.01	<3	.71	.05	.09	<2	13.6	.98	2400
C 158515	<1	82	46	203	1.8	16	19	988	5.06	69	<8	<2	2	197	1.2	3	<3	38	1.87	.047	4	8	1.15	157	<.01	<3	2.18	.09	.13	<2	1.7	.02	1700
C 158516	<1	58	38	123	1.7	21	20	1088	5.24	507	8	<2	<2	223	.7	3	<3	38	2.07	.072	3	10	1.01	167	<.01	<3	2.21	.10	.12	<2	1.3	.02	2000
C 158517	1	53	109	247	1.8	18	18	2675	4.81	284	<8	<2	<2	310	1.5	4	<3	30	5.27	.136	4	7	1.49	113	<.01	<3	1.48	.08	.11	<2	2.1	.04	1900
C 158518	1	49	22	95	.9	16	16	2362	3.72	37	8	<2	<2	243	<.5	3	<3	23	5.84	.118	6	4	1.17	124	<.01	<3	1.05	.10	.09	<2	.9	<.01	5700
C 158519	1	61	6	73	.3	18	19	1437	4.63	44	10	<2	<2	229	<.5	<3	<3	28	3.97	.104	8	7	1.16	158	<.01	<3	1.39	.13	.10	<2	<.3	.01	5100
C 158520	<1	72	9	88	.7	17	20	1085	4.47	56	<8	<2	2	226	<.5	3	<3	30	3.08	.067	6	7	1.04	178	<.01	<3	1.47	.13	.08	<2	.7	.01	5300
C 158521	<1	64	5	90	.4	16	16	993	5.01	35	<8	<2	<2	195	<.5	<3	<3	35	2.37	.072	8	10	1.12	176	<.01	<3	1.88	.14	.09	<2	.4	<.01	5000
C 158522	2	65	10	135	1.1	14	19	674	4.48	48	<8	<2	2	194	<.5	3	<3	37	1.32	.047	5	7	.97	163	<.01	<3	2.05	.12	.09	<2	1.1	.01	5200
RE C 158522	2	62	10	155	.9	14	18	689	4.54	46	<8	<2	<2	197	.6	<3	<3	38	1.34	.047	4	8	.99	165	<.01	<3	2.08	.12	.09	<2	1.2	<.01	-
RRE C 158522	<1	59	6	92	.7	11	19	872	4.72	47	<8	<2	2	177	<.5	6	<3	30	1.83	.046	3	6	1.07	187	<.01	<3	1.44	.13	.11	<2	.4	.01	-
C 158523	<1	61	7	105	.6	12	19	920	4.87	44	<8	<2	<2	182	<.5	3	<3	29	1.80	.054	4	6	1.08	198	<.01	<3	1.42	.14	.11	<2	.6	.01	6000
C 158524	<1	52	9	89	<.3	17	18	901	4.55	26	<8	<2	<2	93	<.5	5	<3	29	2.91	.116	6	8	1.09	76	<.01	<3	1.45	.03	.12	<2	<.3	<.01	4100
C 158525	1	68	20	86	<.3	15	17	750	4.44	27	<8	<2	<2	122	<.5	5	<3	31	3.05	.097	4	7	1.04	90	<.01	<3	1.53	.03	.11	<2	<.3	<.01	3900
C 158526	1	104	10	91	<.3	19	26	744	4.60	40	<8	<2	<2	89	<.5	7	<3	34	2.14	.081	6	7	1.00	108	<.01	<3	1.66	.02	.13	<2	<.3	.01	3700
C 158527	<1	105	15	111	.4	20	24	820	4.90	53	<8	<2	2	123	<.5	7	<3	29	2.50	.063	7	5	1.22	122	<.01	<3	1.76	.02	.12	<2	.4	<.01	3800
C 158528	<1	55	11	146	<.3	12	15	1122	4.17	36	<8	<2	<2	200	<.5	4	<3	25	4.67	.043	6	5	.98	131	<.01	<3	1.43	.03	.10	<2	<.3	.01	3600
C 158529	<1	58	40	163	1.4	15	18	878	4.61	92	<8	<2	2	148	1.3	<3	<3	37	2.06	.083	5	10	1.12	54	<.01	<3	2.13	.02	.11	<2	1.3	.05	4500
C 158530	<1	11	430	5975	3.7	2	6	2037	2.49	130	<8	<2	<2	401	52.6	5	3	11	7.76	.064	4	<1	.66	66	<.01	<3	1.07	.01	.09	3	2.9	.08	4100
C 158531	<1	9	168	219	1.5	1	8	1467	2.91	23	<8	<2	<2	225	1.9	3	<3	11	4.29	.085	5	3	.92	49	<.01	<3	1.22	.02	.11	<2	2.0	.02	3000
C 158533	1	25	7671	2893	20.2	11	12	1497	3.59	2362	<8	<2	<2	195	23.3	25	<3	28	3.95	.048	3	5	.87	41	<.01	<3	1.33	.01	.09	<2	20.2	.46	2100
C 158534	<1	20	160	102	2.0	7	11	1060	2.82	215	<8	<2	<2	145	.6	4	<3	19	2.61	.069	5	4	.88	51	<.01	<3	1.05	.02	.11	<2	1.9	.02	3500
C 158535	<1	34	32	62	1.6	16	18	1550	4.47	147	<8	<2	<2	186	.5	3	<3	36	3.89	.087	6	7	1.60	42	<.01	<3	1.61	.02	.09	<2	1.5	.01	3200
C 158536	<1	45	27	82	.9	14	18	1352	4.94	47	<8	<2	<2	203	.6	<3	<3	36	3.34	.095	8	7	1.73	39	<.01	<3	2.44	.02	.09	<2	.9	.01	3200
C 158537	<1	47	23	93	1.1	16	20	1357	5.10	50	<8	<2	2	183	.5	<3	<3	38	3.33	.097	8	8	1.77	29	<.01	<3	2.45	.02	.10	<2	1.1	.01	3100
STANDARD DS5	13	141	24	132	.3	25	12	748	2.90	19	<8	<2	3	47	5.4	5	6	59	.72	.093	12	189	.64	137	.10	14	2.03	.04	.11	3	152.8	3.29	-

Standard is STANDARD DS5/R-2/AU-1. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Ag** gm/mt	Au** gm/mt	Sample gm
C 158538	<1	41	6	75	.5	15	19	967	4.21	45	<8	<2	2	203	<.5	3	<3	41	3.35	.091	9	9	1.66	28	<.01	<3	2.29	.02	.08	<2	.5	<.01	2700
C 158539	<1	45	21	115	1.5	19	22	1262	5.28	70	<8	<2	<2	175	.5	3	<3	48	2.44	.074	6	11	1.48	42	<.01	<3	2.63	.02	.13	2	1.3	.01	2600
C 158540	<1	27	77	88	2.2	11	16	1116	3.72	116	<8	<2	2	171	.5	4	<3	37	3.16	.077	3	8	1.09	28	<.01	<3	1.65	.01	.08	<2	2.3	.07	1200
C 158541	<1	41	13.	54	.8	13	17	977	3.99	36	<8	<2	<2	223	<.5	<3	3	32	3.39	.087	7	6	1.57	26	<.01	<3	2.26	.02	.08	<2	.5	.01	1700
C 158542	1	18	14	288	.7	14	19	1160	3.61	63	<8	<2	<2	214	1.5	<3	4	35	3.40	.059	4	8	1.24	61	<.01	<3	1.64	.01	.10	<2	.9	.01	1600
C 158543	1	36	10	73	.8	18	22	1424	4.87	91	<8	<2	<2	184	<.5	<3	<3	44	2.81	.075	5	10	1.53	52	<.01	<3	2.30	.02	.12	<2	.9	.01	800
C 158544	<1	13	138	176	1.2	3	8	1351	2.91	62	<8	<2	<2	193	1.3	<3	3	13	3.45	.087	5	1	.92	64	<.01	<3	1.16	.02	.14	<2	1.3	.06	3200
C 158545	1	38	16	253	.8	23	26	1565	4.72	122	<8	<2	<2	266	.6	<3	<3	53	4.47	.070	5	12	1.61	88	<.01	<3	1.92	.02	.11	<2	.8	.01	1700
C 158546	<1	40	7	79	<.3	19	20	1017	4.22	55	<8	<2	<2	167	<.5	<3	<3	48	3.05	.078	7	12	1.37	65	<.01	<3	1.44	.03	.09	<2	<.3	<.01	2000
C 158547	<1	33	12	74	<.3	14	18	1683	4.28	46	<8	<2	<2	260	<.5	<3	<3	36	5.05	.089	8	7	1.97	102	<.01	<3	1.48	.03	.08	<2	.4	<.01	1500
C 158548	<1	37	6	63	.5	15	18	1241	4.00	294	<8	<2	<2	225	<.5	<3	<3	35	3.43	.092	8	7	1.55	96	<.01	<3	1.90	.02	.08	<2	.5	<.01	1500
C 158549	<1	36	3	71	<.3	14	17	1176	3.96	46	<8	<2	<2	192	<.5	<3	<3	40	2.87	.092	9	8	1.58	43	<.01	<3	2.08	.03	.08	<2	<.3	<.01	2100
C 158550	<1	37	12	75	.7	13	18	1293	3.99	36	<8	<2	2	210	<.5	4	<3	45	3.23	.099	7	9	1.61	39	<.01	<3	2.15	.02	.09	<2	.7	.01	3500
RE C 158550	<1	40	12	69	.7	13	17	1296	3.99	31	<8	<2	<2	211	<.5	3	<3	45	3.24	.099	7	8	1.61	39	<.01	<3	2.15	.02	.09	<2	.9	.03	-
RRE C 158550	1	37	12	75	.6	13	18	1265	3.91	32	<8	<2	<2	207	<.5	<3	<3	44	3.17	.096	7	9	1.60	39	<.01	<3	2.12	.03	.09	<2	.6	.02	-
C 158551	<1	37	8	75	2.8	15	17	1142	4.22	37	<8	<2	<2	181	<.5	<3	<3	48	2.72	.093	7	9	1.71	35	<.01	<3	2.35	.04	.08	<2	2.2	<.01	3300
C 158552	<1	42	5	110	.8	16	19	1085	4.29	36	<8	<2	<2	147	<.5	<3	<3	56	1.95	.096	8	12	1.66	52	<.01	<3	2.44	.03	.08	<2	.9	.11	3000
C 158553	<1	35	6	69	.5	16	18	1102	3.99	36	<8	<2	2	181	<.5	<3	<3	45	2.58	.093	8	10	1.53	60	<.01	<3	2.19	.03	.09	<2	.6	.01	3200
C 158554	<1	38	4	66	.3	15	19	1276	3.92	40	<8	<2	2	212	<.5	<3	<3	44	3.17	.097	9	11	1.47	47	<.01	<3	2.10	.04	.09	<2	.4	<.01	2100
C 158555	<1	41	10	81	.3	14	16	1182	4.38	68	<8	<2	<2	210	<.5	<3	<3	38	2.51	.089	8	8	1.50	170	<.01	<3	2.31	.04	.09	<2	.3	<.01	4500
C 158556	2	44	4	92	.5	13	17	1124	4.81	64	<8	<2	2	228	<.5	<3	<3	42	3.14	.098	10	8	1.55	48	<.01	<3	2.35	.04	.09	<2	.4	.01	1000
C 158557	<1	54	33	123	1.3	19	18	1015	5.05	64	<8	<2	<2	157	.6	<3	<3	42	2.34	.055	6	11	1.27	103	<.01	<3	2.15	.04	.12	<2	1.3	.01	3200
C 158558	6	62	10	83	1.1	16	17	711	3.91	88	<8	<2	<2	177	<.5	3	<3	30	1.91	.077	5	7	.84	99	<.01	<3	1.62	.06	.13	<2	1.5	<.01	3000
C 158559	1	61	23	102	1.9	17	18	997	4.29	1131	<8	<2	2	159	.5	<3	<3	34	1.57	.085	5	8	.88	93	<.01	<3	1.82	.05	.10	<2	2.4	.15	2800
C 158560	<1	86	4188	4237	30.1	16	17	1221	4.25	7059	<8	2	<2	110	51.0	32	3	17	1.76	.045	2	2	.58	58	<.01	<3	.75	.03	.11	<2	31.7	.93	1800
C 158561	<1	69	1041	111	10.6	15	18	794	4.19	2276	<8	<2	<2	109	1.2	9	<3	21	1.04	.048	1	5	.49	56	<.01	3	1.07	.04	.12	<2	11.3	.40	1500
C 158562	<1	73	126	550	.9	13	16	1272	4.82	75	<8	<2	2	155	5.8	<3	<3	36	2.28	.130	6	7	1.03	91	<.01	3	1.98	.04	.13	<2	1.1	.03	2600
C 158563	<1	61	40	83	1.4	14	19	844	4.98	87	<8	<2	2	122	<.5	4	<3	41	1.03	.067	8	8	1.14	94	<.01	<3	2.25	.03	.14	<2	1.5	.05	3200
C 158564	2	65	23	82	1.0	14	18	757	3.85	47	<8	<2	<2	161	<.5	4	<3	26	2.11	.039	7	6	1.04	135	<.01	<3	1.56	.03	.12	<2	1.0	<.01	2500
C 158565	1	56	13	61	2.2	12	18	1522	5.15	618	<8	<2	<2	159	<.5	3	<3	38	2.60	.128	2	7	1.20	77	<.01	3	1.80	.02	.14	<2	2.2	.12	2000
C 158566	1	57	24	78	.9	17	21	1419	4.51	93	<8	<2	2	159	<.5	3	<3	35	2.70	.085	6	8	.99	61	<.01	<3	1.36	.03	.12	<2	1.5	.01	5400
C 158567	1	64	38	101	2.8	15	16	1609	4.60	762	<8	<2	<2	162	.9	5	<3	34	3.31	.066	4	8	1.08	46	<.01	<3	1.54	.02	.12	<2	3.3	.14	3000
C 158568	1	71	177	243	2.6	19	19	1296	4.26	97	<8	<2	2	163	2.1	7	<3	39	2.80	.074	6	9	1.03	71	<.01	<3	1.72	.02	.13	<2	1.9	.03	2900
C 158569	<1	81	19	94	1.0	20	19	1325	4.27	83	<8	<2	2	143	.7	<3	<3	35	2.53	.076	6	9	1.32	56	<.01	<3	1.95	.03	.14	<2	1.1	.01	3000
STANDARD DS5	12	141	23	134	.3	24	12	761	2.92	18	<8	<2	3	49	5.5	3	6	59	.73	.093	12	190	.64	135	.09	16	2.10	.04	.11	3	153.4	3.35	-

Standard is STANDARD DS5/R-2/AU-1. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Ag** gm/mt	Au** gm/mt	Sample gm
C 158570	<1	58	12	75	.5	18	16	1318	4.43	99	<8	<2	2	127	.5	<3	<3	34	2.30	.075	7	9	1.48	34	<.01	<3	2.00	.03	.11	<2	.6	.10	3200
C 158571	<1	52	13	83	.4	15	14	2090	3.99	42	<8	<2	2	183	<.5	3	<3	23	4.68	.064	6	6	1.41	43	<.01	<3	1.39	.03	.11	<2	.4	<.01	4000
C 158572	<1	66	9	96	<.3	19	19	1420	4.69	37	<8	<2	<2	164	<.5	<3	<3	34	2.95	.110	10	8	1.52	43	<.01	<3	2.05	.02	.12	<2	<.3	<.01	3000
C 158573	<1	68	24	108	.5	23	22	2040	4.54	79	<8	<2	<2	213	.7	<3	<3	29	4.62	.070	7	7	1.45	50	<.01	<3	1.53	.02	.14	<2	.6	<.01	3300
C 158574	<1	69	25	137	.8	17	19	1433	4.60	343	<8	<2	<2	141	1.3	<3	<3	35	2.76	.070	8	8	1.39	57	<.01	<3	1.81	.02	.14	<2	.8	.01	3500
C 158575	<1	77	815	373	3.3	16	15	1854	4.46	938	<8	<2	<2	161	4.1	3	<3	36	3.11	.069	4	9	1.36	59	<.01	<3	1.72	.03	.12	<2	5.3	.14	3400
C 158576	<1	80	42	49	1.3	19	20	1750	4.20	107	<8	<2	<2	133	<.5	<3	<3	19	3.08	.060	6	5	1.28	67	<.01	<3	.66	.04	.14	<2	1.7	.03	2600
C 158577	1	245	674	2544	5.3	24	19	2145	4.09	893	<8	<2	<2	116	25.4	<3	<3	25	2.69	.095	4	6	1.01	74	<.01	<3	.92	.03	.14	<2	5.0	.24	2700
C 158578	<1	6	76	141	<.3	<1	5	1719	2.30	28	<8	<2	<2	120	1.3	<3	<3	5	3.17	.088	10	1	.65	52	<.01	<3	.45	.02	.21	<2	<.3	.02	3600
C 158579	<1	71	36	66	1.7	18	19	1777	3.97	186	<8	<2	<2	139	.8	6	<3	29	3.20	.061	3	7	1.21	73	<.01	<3	.87	.04	.11	<2	2.3	.07	3200
C 158580	1	43	13	95	.6	22	24	1843	4.72	73	<8	<2	2	134	.8	6	<3	41	3.31	.082	6	11	1.59	65	<.01	<3	.77	.04	.13	<2	.6	.01	3200
C 158581	<1	54	197	350	.9	21	22	2478	4.00	188	<8	<2	<2	153	3.3	4	<3	26	4.18	.084	6	6	1.50	69	<.01	<3	.42	.04	.12	<2	.9	.04	4000
C 158582	<1	82	14	318	.8	21	21	2278	4.41	400	<8	<2	<2	138	3.3	<3	<3	25	3.60	.103	5	7	1.49	71	<.01	<3	.57	.04	.15	<2	.8	.19	1900
C 158583	<1	101	25	386	3.2	16	19	1594	4.55	188	<8	<2	2	112	4.4	4	<3	19	2.28	.077	4	5	1.16	109	<.01	<3	.42	.06	.15	<2	4.5	.23	2000
C 158584	<1	215	2308	519	21.0	13	15	1043	6.20	1404	<8	<2	<2	85	7.8	17	<3	10	1.68	.041	2	5	.49	47	<.01	<3	.32	.04	.09	<2	21.9	2.76	1500
C 158585	1	60	27	89	1.5	20	24	1354	5.10	70	<8	<2	2	132	.8	4	<3	31	2.69	.071	5	8	1.25	93	<.01	<3	.90	.05	.12	<2	2.0	.02	1700
C 158586	<1	73	9	90	.5	13	15	982	4.40	31	<8	<2	<2	125	.7	<3	<3	17	2.03	.088	8	4	.98	131	<.01	<3	.50	.07	.15	<2	.5	.02	3000
C 158587	<1	60	41	130	.8	14	17	1009	4.45	85	<8	<2	2	119	.9	<3	<3	15	1.92	.077	8	3	1.01	125	<.01	<3	.44	.07	.15	<2	1.0	.02	3200
C 158588	<1	206	49	120	4.8	22	19	1391	6.34	1720	<8	<2	<2	125	1.5	6	<3	36	2.37	.075	3	9	1.11	98	<.01	<3	1.30	.06	.12	<2	5.4	.26	3400
C 158589	2	64	13	68	1.3	11	14	1346	4.51	45	<8	<2	<2	139	.8	3	<3	21	2.49	.217	10	4	1.06	121	<.01	<3	.76	.07	.18	<2	2.0	.02	3000
C 158590	<1	105	10	127	1.1	17	22	1113	5.61	83	<8	<2	<2	119	.9	<3	<3	18	1.39	.055	10	3	1.26	131	<.01	<3	.61	.07	.15	<2	1.2	.01	3300
RE C 158590	<1	107	9	119	1.0	17	22	1116	5.63	85	<8	<2	<2	120	.9	<3	<3	17	1.40	.055	10	3	1.27	133	<.01	<3	.61	.07	.15	<2	1.0	.01	-
RRE C 158590	<1	105	10	135	1.0	16	22	1098	5.58	85	<8	<2	<2	117	1.0	<3	<3	17	1.37	.055	9	3	1.25	129	<.01	<3	.61	.07	.14	<2	1.4	.02	-
C 158591	2	43	84	70	2.6	17	21	2157	5.02	413	<8	<2	<2	146	.8	4	<3	17	3.53	.062	4	5	1.27	84	<.01	<3	.62	.05	.12	<2	3.0	.18	1700
C 158592	<1	45	496	184	3.3	19	21	1881	5.78	3506	<8	<2	<2	128	1.8	7	<3	38	3.11	.090	5	10	1.36	72	<.01	<3	1.40	.04	.14	<2	2.8	.29	1400
C 158593	1	60	1121	1672	3.9	18	20	4441	4.20	149	<8	<2	<2	157	16.1	4	<3	22	4.96	.077	5	3	1.39	73	<.01	<3	.45	.04	.14	<2	2.3	.06	3100
C 158594	<1	51	723	1208	2.2	18	18	3852	4.05	80	<8	<2	<2	166	11.8	<3	<3	28	5.15	.085	7	5	1.35	68	<.01	<3	.90	.03	.12	<2	2.6	.03	3000
C 158595	1	56	17	48	1.1	16	19	1302	4.62	140	<8	<2	<2	154	.5	<3	<3	36	2.67	.221	8	7	1.18	97	<.01	<3	1.72	.05	.16	<2	2.8	.02	3100
C 158596	<1	101	14	90	1.3	22	25	1282	5.98	185	<8	<2	2	106	.9	3	<3	55	1.76	.045	6	15	1.31	97	<.01	<3	1.75	.05	.14	<2	1.8	.05	3300
C 158597	<1	85	13	58	1.2	21	24	1036	4.66	529	<8	<2	2	129	.6	3	<3	43	2.28	.081	7	12	1.00	106	<.01	<3	1.49	.06	.14	<2	1.2	.04	3000
C 158598	<1	71	13	102	.3	16	20	844	4.69	39	<8	<2	2	117	.5	<3	<3	20	1.88	.074	11	4	1.00	124	<.01	<3	.71	.07	.15	<2	.3	<.01	3100
C 158599	1	79	9	81	1.0	16	18	857	4.70	53	<8	<2	<2	128	.7	<3	<3	30	1.86	.076	7	6	1.05	114	<.01	<3	1.46	.06	.15	<2	1.0	<.01	3000
C 158600	1	72	21	82	.8	20	22	1015	4.68	142	<8	<2	<2	131	.5	<3	<3	29	2.43	.068	5	8	.99	117	<.01	<3	1.28	.07	.14	<2	.8	.04	2900
C 158601	<1	51	27	134	.5	14	17	1542	4.27	43	<8	<2	<2	181	.6	<3	<3	27	4.45	.075	6	6	1.28	92	<.01	<3	1.17	.06	.14	<2	.5	.01	2700
STANDARD DS5	12	140	25	133	<.3	24	12	762	2.90	18	<8	<2	3	48	5.5	4	7	58	.73	.095	12	184	.66	141	.10	17	2.04	.04	.11	3	152.6	3.33	-

Standard is STANDARD DS5/R-2/AU-1. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Ag** gm/mt	Au** gm/mt	Sample gm
C 158602	5	64	1059	320	5.0	18	18	1097	4.37	789	<8	<2	<2	152	3.2	6	<3	19	2.94	.054	2	6	.83	78	.01	<3	.80	.04	.15	<2	6.6	.77	2800
C 158603	<1	71	15	79	1.9	21	20	1008	4.39	47	10	<2	<2	134	<.5	5	<3	21	2.13	.049	5	8	1.13	81	.01	<3	.63	.05	.16	2	1.7	.01	4000
C 158604	<1	59	16	106	1.7	23	19	1474	4.78	39	10	<2	2	157	<.5	5	<3	23	3.10	.075	6	8	1.48	67	.01	<3	.72	.04	.15	<2	1.7	.02	4700
C 158605	<1	67	9	75	<.3	15	15	966	3.89	29	<8	<2	<2	147	<.5	4	<3	16	2.49	.074	7	5	1.21	85	<.01	<3	1.10	.06	.13	<2	<.3	<.01	4900
C 158606	<1	55	8	80	.6	14	14	1051	3.83	28	<8	<2	<2	152	<.5	3	<3	17	2.87	.072	6	4	1.29	92	<.01	<3	.69	.06	.16	<2	<.3	<.01	5200
C 158607	1	64	3	98	.3	14	14	897	4.03	35	<8	<2	2	114	<.5	3	<3	17	2.18	.091	8	4	1.16	109	<.01	<3	.60	.07	.18	<2	.3	.04	5700
C 158608	1	58	4	62	1.2	14	17	998	3.78	51	<8	<2	2	105	<.5	3	<3	19	2.43	.080	7	5	.97	97	<.01	<3	.78	.06	.16	<2	1.2	<.01	1800
C 158609	9	93	2773	261	11.6	14	16	1269	4.92	464	<8	<2	<2	103	3.2	9	<3	25	2.03	.056	3	4	.94	87	<.01	<3	1.35	.05	.19	<2	12.6	.62	2000
C 158610	<1	64	9	82	.5	16	16	947	4.74	43	<8	<2	<2	131	<.5	3	<3	34	2.34	.067	7	10	1.15	117	.01	<3	1.72	.07	.18	2	.4	.01	5600
C 158611	<1	88	3	84	.5	16	18	831	4.84	39	<8	<2	2	130	<.5	5	<3	29	1.95	.085	10	8	1.22	107	.01	<3	1.84	.06	.15	2	.5	.01	6100
C 158612	<1	84	<3	81	.4	15	16	809	4.56	29	<8	<2	2	120	<.5	3	<3	20	1.77	.098	10	5	1.14	139	<.01	<3	1.06	.07	.22	<2	.4	.01	3100
C 158613	2	53	68	43	1.6	22	35	720	10.80	276	<8	<2	<2	112	<.5	12	<3	11	2.06	.059	1	3	.78	24	<.01	<3	.56	.06	.11	3	1.6	.04	500
C 158614	2	65	5	80	.4	16	17	888	4.47	33	8	<2	2	122	<.5	3	<3	18	2.26	.091	6	5	1.13	122	<.01	<3	.99	.08	.19	<2	.4	.01	5200
C 158615	<1	66	7	92	.7	15	17	1115	4.25	51	<8	<2	2	127	<.5	<3	<3	18	2.79	.080	7	5	1.16	107	<.01	<3	1.06	.06	.15	<2	.7	.03	5500
C 158616	1	48	7	95	.6	14	15	1098	4.20	43	<8	<2	2	107	.6	<3	<3	15	2.72	.063	7	4	1.06	96	<.01	<3	.55	.06	.12	<2	.6	.02	3600
C 158617	2	113	122	52	10.7	14	16	1612	4.64	1353	<8	<2	<2	122	.6	6	<3	30	3.35	.060	3	7	1.09	69	<.01	<3	1.54	.04	.12	2	9.7	.32	1600
C 158618	<1	66	9	81	.9	15	18	920	4.06	82	<8	<2	2	126	<.5	<3	<3	24	2.23	.062	7	6	1.07	131	.01	<3	1.61	.07	.20	<2	.9	.03	4500
C 158619	<1	46	3	81	.6	16	19	900	4.60	40	<8	<2	2	135	<.5	3	<3	39	2.08	.097	7	10	1.24	92	.01	<3	1.98	.06	.12	<2	.8	<.01	4300
C 158620	1	31	5	75	.4	16	18	1036	4.32	39	<8	<2	<2	178	<.5	6	<3	42	2.57	.096	5	10	1.13	81	<.01	<3	1.94	.07	.12	2	.4	.01	4600
RE C 158620	<1	30	<3	73	.4	15	18	1028	4.31	37	<8	<2	2	178	<.5	<3	<3	42	2.57	.095	5	9	1.13	80	<.01	<3	1.93	.07	.12	<2	.6	.01	-
RRE C 158620	<1	31	3	78	.6	16	19	1087	4.52	40	<8	<2	<2	184	<.5	<3	<3	43	2.71	.100	4	10	1.18	80	<.01	<3	1.94	.06	.10	<2	.5	<.01	-
C 158621	1	29	8	52	.5	15	18	1231	4.28	43	<8	<2	<2	168	<.5	3	<3	35	2.95	.083	4	9	1.14	92	<.01	<3	1.78	.08	.14	<2	<.3	.01	5400
C 158622	2	36	8	92	.4	19	20	1160	4.59	302	<8	<2	<2	119	<.5	<3	<3	54	2.51	.059	5	16	1.15	72	<.01	<3	1.77	.07	.13	<2	<.3	.06	4100
C 158623	1	42	28	155	.9	15	18	1238	4.40	807	<8	<2	<2	141	1.0	3	<3	34	2.82	.080	3	9	1.07	69	<.01	<3	1.41	.06	.10	<2	.9	.46	1600
C 158624	1	48	23	113	.8	16	19	1035	4.64	50	<8	<2	2	162	.5	<3	<3	44	2.18	.116	6	11	1.11	69	<.01	<3	2.18	.05	.11	2	.9	.01	3800
C 158625	<1	91	38	103	1.4	18	17	1232	5.24	2982	<8	<2	2	160	<.5	3	<3	31	2.77	.074	3	10	1.13	95	<.01	<3	1.72	.07	.17	<2	1.4	.90	3600
C 158626	1	78	12	101	1.0	17	20	1090	4.73	65	<8	<2	<2	166	.5	<3	<3	33	2.41	.063	5	9	1.21	98	<.01	<3	2.01	.07	.19	<2	1.1	.05	4200
C 158627	<1	60	<3	78	.5	19	20	1038	4.90	55	<8	<2	<2	159	.5	3	<3	34	2.49	.074	6	9	1.12	85	.01	<3	1.99	.06	.16	2	.5	.01	4400
C 158628	<1	78	5	84	1.1	15	17	1062	4.51	98	8	<2	2	117	.6	<3	<3	33	1.64	.074	7	7	.99	100	<.01	<3	1.93	.07	.24	<2	1.4	.03	2000
C 158629	5	154	563	2066	9.2	19	28	790	4.32	879	<8	<2	<2	105	20.4	6	3	24	1.32	.049	3	3	.56	91	<.01	<3	1.45	.03	.34	<2	8.3	.84	800
C 158630	1	24	70	121	.8	3	9	1787	2.82	104	<8	<2	<2	315	1.1	<3	<3	13	4.34	.089	4	2	.80	87	<.01	<3	1.29	.03	.20	<2	.8	.03	1300
C 158631	<1	16	167	249	.8	3	9	1924	3.00	102	<8	<2	2	241	2.5	<3	<3	14	3.58	.092	5	2	.87	97	<.01	<3	1.26	.04	.24	<2	.8	.11	1600
C 158632	<1	25	155	188	1.4	3	9	1567	2.96	58	<8	<2	<2	269	2.2	3	<3	15	3.56	.089	5	2	.84	95	<.01	<3	1.59	.04	.22	<2	1.4	.05	1800
C 158633	2	67	94	122	1.7	23	23	1295	5.32	162	<8	<2	<2	180	1.0	3	<3	46	2.67	.072	6	13	1.09	101	<.01	<3	2.56	.05	.30	2	1.7	.05	1900
STANDARD DS5	12	137	23	128	.4	24	11	739	2.85	20	<8	<2	3	47	5.2	5	6	57	.71	.094	11	185	.64	140	.09	13	1.99	.03	.13	5	152.1	3.35	-

Standard is STANDARD DS5/R-2/AU-1. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Ag** gm/mt	Au** gm/mt	Sample gm
C 158634	<1	68	25	87	1.0	19	19	957	4.93	206	<8	<2	<2	147	<.5	<3	<3	38	2.00	.063	6	8	1.08	102	<.01	<3	2.19	.07	.22	<2	1.3	.03	4600
C 158635	<1	59	14	60	.8	18	20	1022	4.39	89	<8	<2	<2	154	<.5	<3	<3	39	2.69	.051	7	9	1.29	101	<.01	<3	1.98	.08	.20	<2	.9	.01	4000
C 158636	1	42	4	70	<.3	18	20	866	3.67	37	<8	<2	2	129	<.5	<3	<3	43	2.47	.100	9	10	1.36	78	<.01	<3	1.61	.09	.12	<2	<.3	.01	3900
C 158637	4	48	26	53	3.2	18	20	1080	3.84	49	<8	<2	2	199	.5	<3	<3	33	3.01	.090	5	7	1.12	83	<.01	<3	1.74	.07	.13	<2	3.5	.02	2800
C 158638	<1	47	32	54	2.1	17	18	1364	4.09	565	<8	<2	2	219	<.5	3	<3	37	3.04	.074	6	8	1.24	89	<.01	<3	1.93	.05	.18	<2	2.1	.11	2000
C 158639	<1	40	30	119	.5	17	19	1397	4.18	62	<8	<2	<2	187	.6	<3	<3	31	3.57	.075	7	8	1.57	84	<.01	<3	1.70	.06	.18	<2	.5	.01	3700
C 158640	1	43	14	70	1.0	20	21	1399	3.66	78	<8	<2	2	138	<.5	5	<3	24	3.87	.085	6	6	1.32	84	.01	<3	.99	.07	.15	<2	1.0	.01	3900
STANDARD DS5	12	138	22	131	.3	24	12	741	2.88	18	<8	<2	3	47	5.4	4	6	58	.72	.091	12	187	.65	138	.09	14	2.04	.03	.14	3	-	-	-

Sample type: CORE R150 60C.

Data FA

KODIAK EXPLORATION LTD.

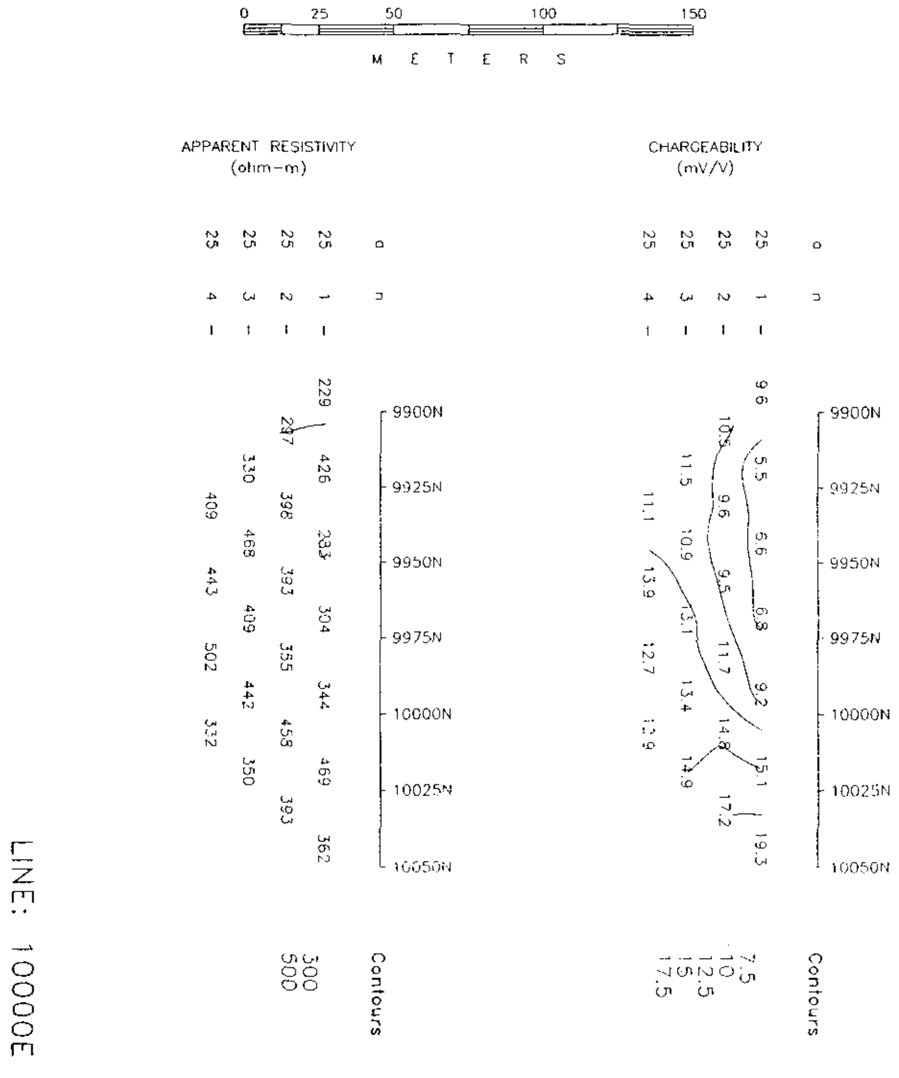
TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 10000E

INDUCED POLARIZATION SURVEY	Pole–Dipole Array
SCOTT GEOPHYSICS LTD.	SCINTREX IPR12
August/03	Pulse Rate: 2 sec

current electrode south of potential electrodes (array heading N)

Mx chargeability = 690–1050 msec after shutoff (mid point 870 msec)



GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT

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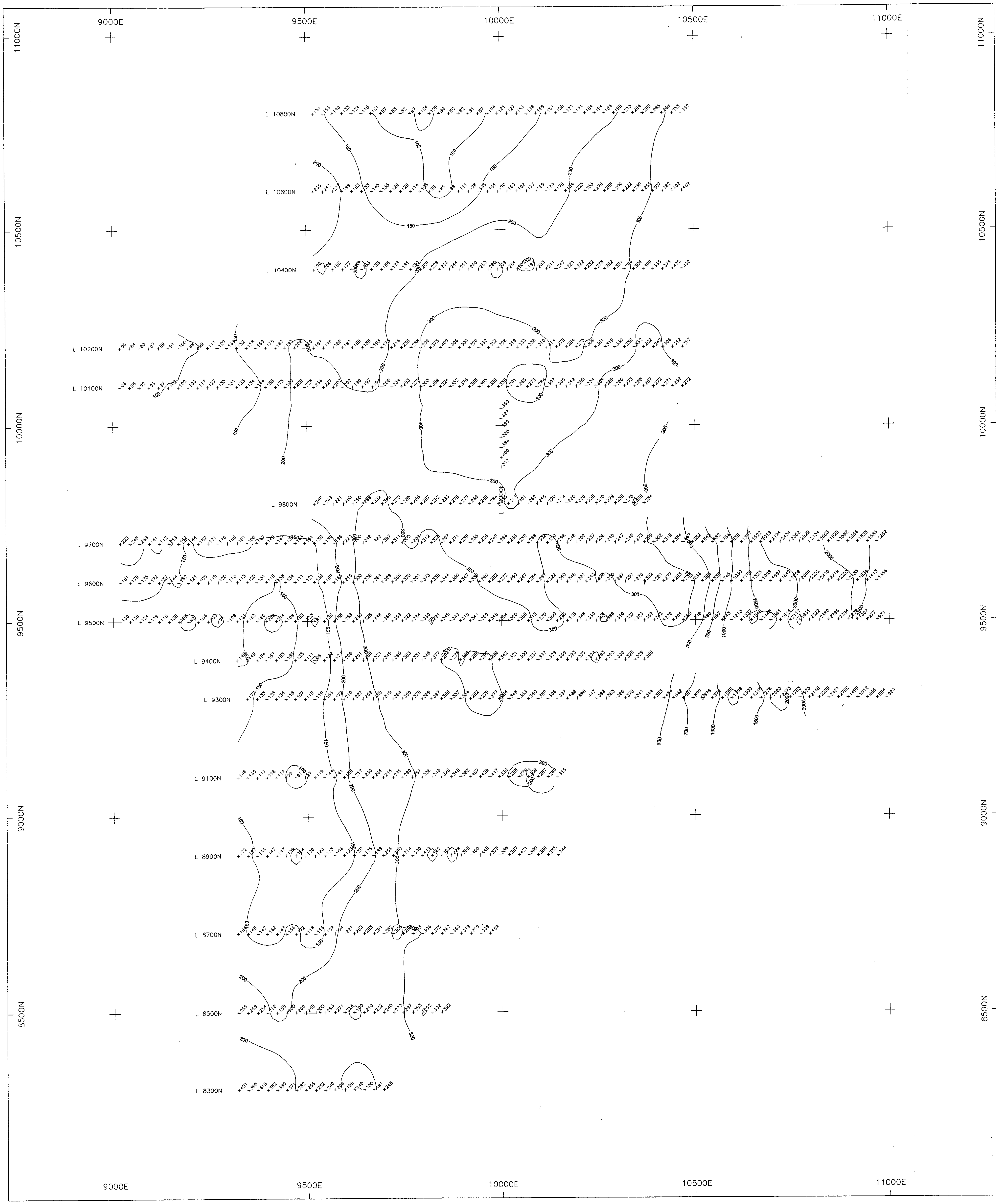

SURVEY SPECIFICATIONS

survey performed	August/03
receiver	Scintrex IPR12
transmitter	Scintrex IPC7
pulse time	2 seconds
Mx receive window	690-1050 msecs
array	pole dipole
a spacing	25 metres
n separations	1, 2, 3, 4, 5
Contoured value	Filtered chargeability
Filtered values	n = 1 to 5

Contour intervals:
2.5, 5.0, 7.5, 10.0, 12.5, 15.0,
17.5, 20.0, 25.0, 30.0 (mV/V)

Note: The filter applied to this data is the standard Fraser triangular filter whereby one value is selected at n=1, two values at n=2, three values at n=3, etc. The plotted value is the average of the average values of the n separations and is plotted at the n=1 data point. The filtered values give only general trends. The pseudosections must be referred to to assess specific features.

GEOLOGICAL SURVEY BRANCH
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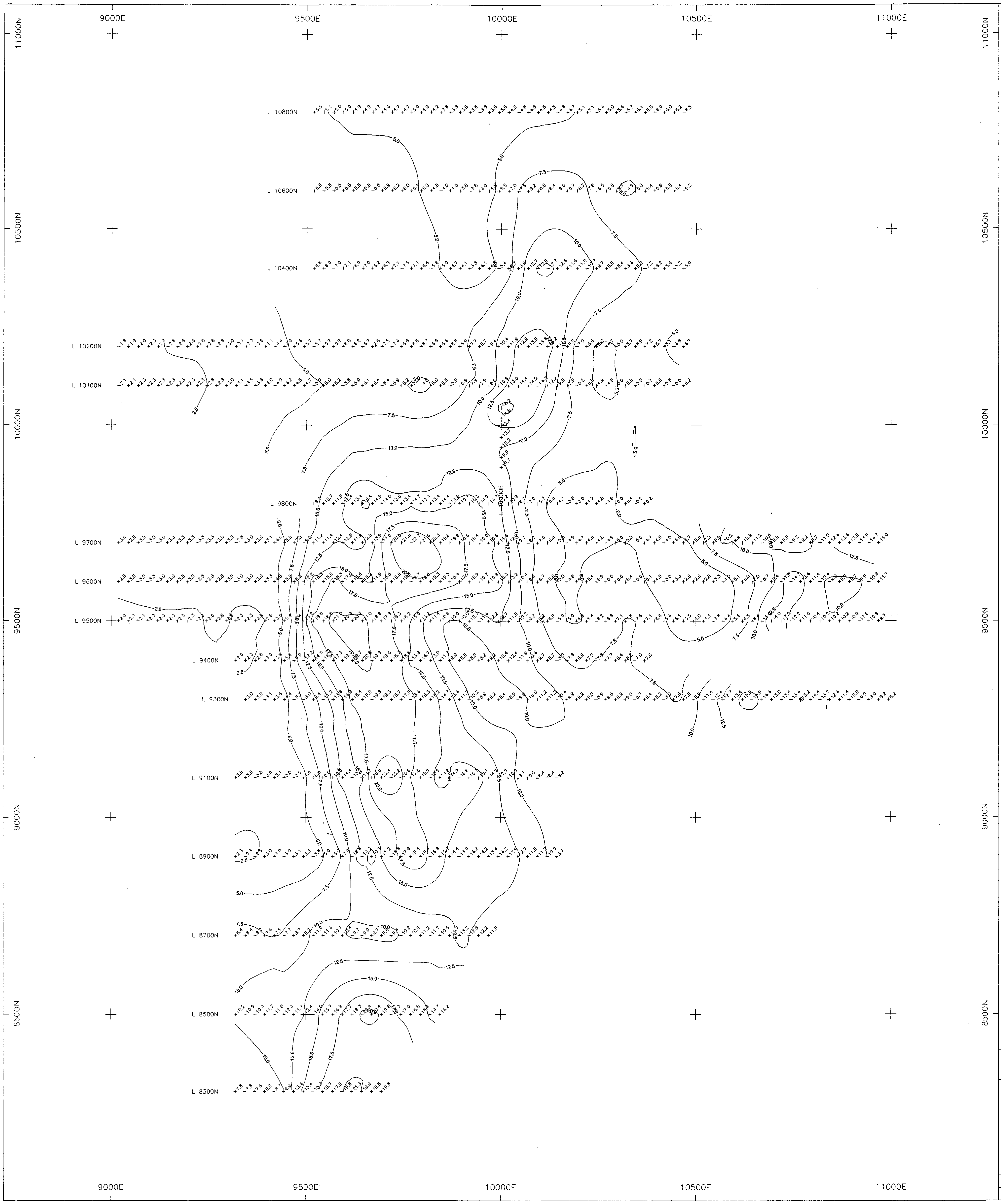
(M1)

0 100 200 300 400
METERS

KODIAK EXPLORATION LTD.

TOMMY JACK PROPERTY
HAZELTON AREA, B.C.
Resistivity Contour Plan
Triangular Filtered Values
First to Fifth Separations

DRAWN BY: ars | DATE: Aug/03
SCOTT GEOPHYSICS LTD.

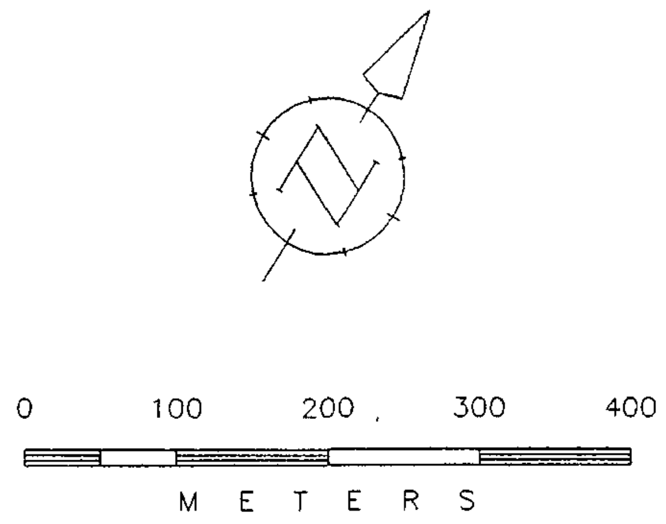


SURVEY SPECIFICATIONS

survey performed	August/03
receiver	Scintrex IPR12
transmitter	Scintrex IPC7
pulse time	2 seconds
Mx receive window	690-1050 msecs
array	pole dipole
a spacing	25 metres
n separations	1, 2, 3, 4, 5
Contoured value	Filtered chargeability
Filtered values	n = 1 to 5

Contour intervals:
2.5, 5.0, 7.5, 10.0, 12.5, 15.0,
17.5, 20.0, 25.0, 30.0 (mV/V)

Note: The filter applied to this data is the standard Fraser triangular filter whereby one value is selected at n=1, two values at n=2, three values at n=3, etc. The plotted value is the average of the average values of the n separations and is plotted at the n=1 data point. The filtered values give only general trends. The pseudosections must be referred to to assess specific features.



KODIAK EXPLORATION LTD.

TOMMY JACK PROPERTY

HAZELTON AREA, B.C.
Chargeability Contour Plan
Triangular Filtered Values
First to Fifth Separations

DRAWN BY: ars
DATE: Aug/03
SCOTT GEOPHYSICS LTD.

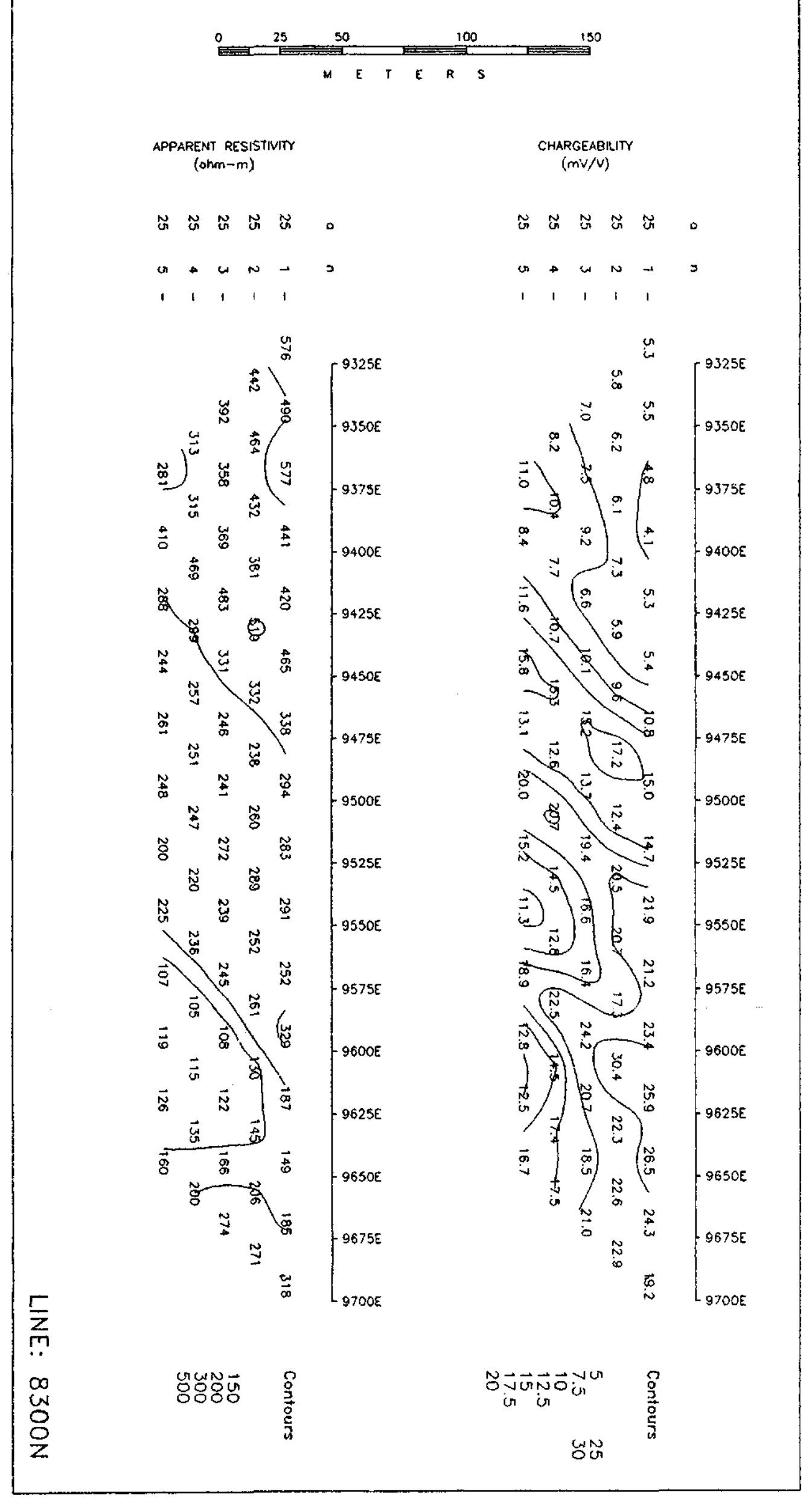
KODIAK EXPLORATION LTD.

TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 8300N

INDUCED POLARIZATION SURVEY — Pole–Dipole Array
SCOTT GEOPHYSICS LTD. — SCINTREX IPR12
August/03 — Pulse Rate: 2 sec

current electrode west of potential electrodes (array heading E)
Mx chargeability = 690–1050 msec after shutoff (mid point 870 msec)



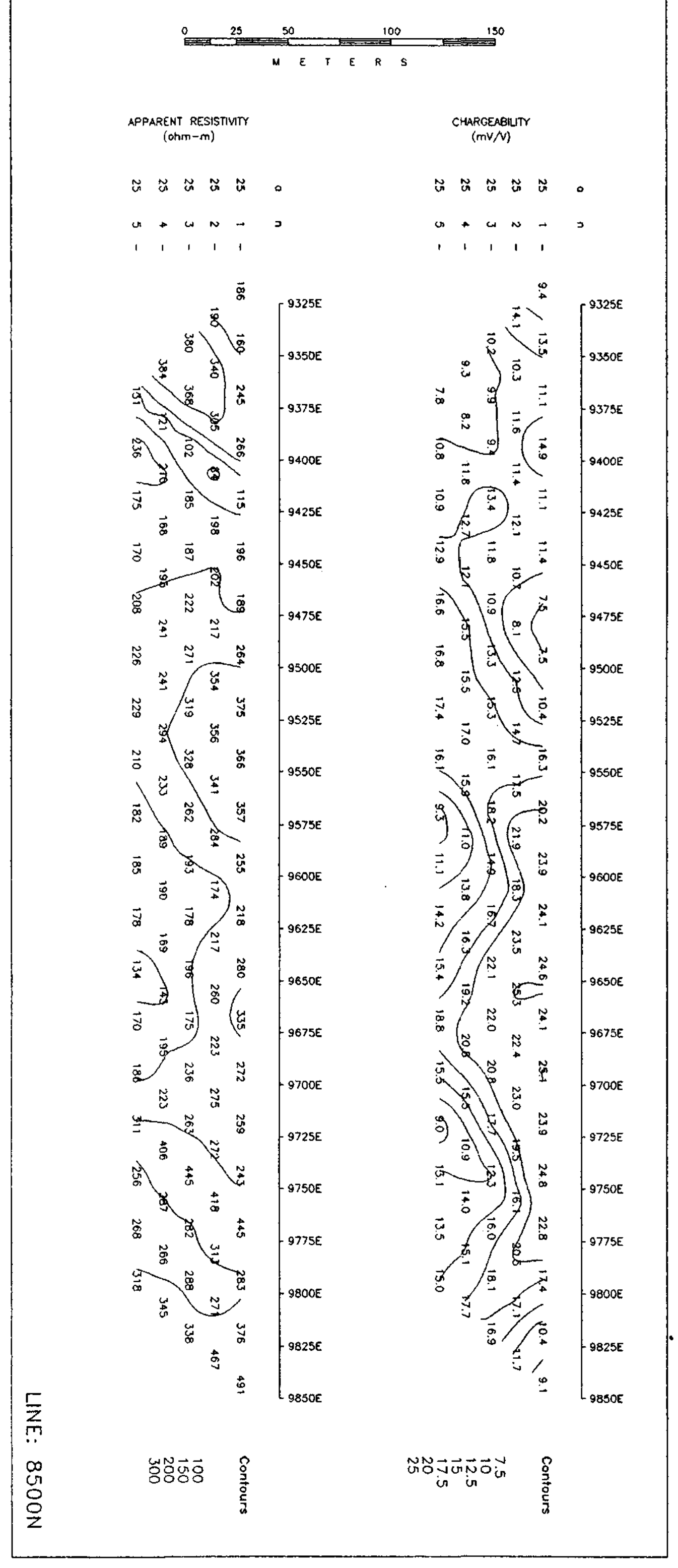
KODIAK EXPLORATION LTD.

TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 8500N

INDUCED POLARIZATION SURVEY — Pole–Dipole Array
SCOTT GEOPHYSICS LTD. — SCINTREX IPR12
August/03 — Pulse Rate: 2 sec

current electrode west of potential electrodes (array heading E)
Mx chargeability = 690–1050 msec after shutoff (mid point 870 msec)



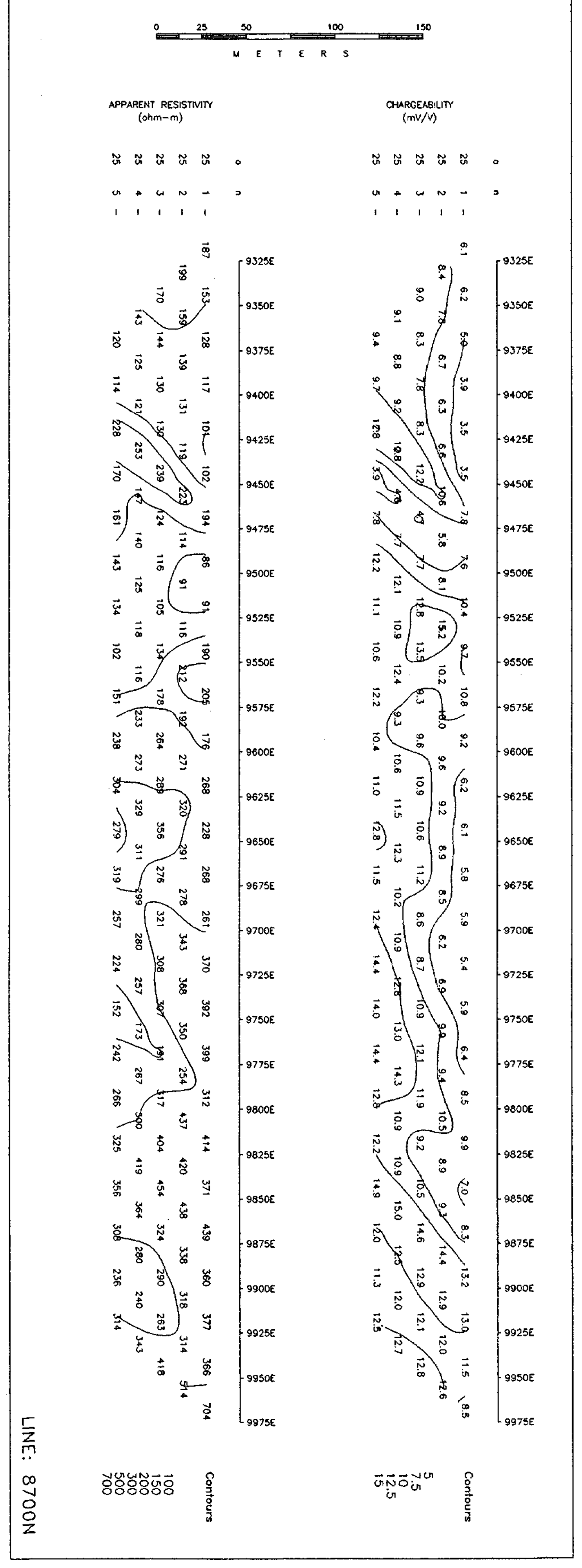
KODIAK EXPLORATION LTD.

TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 8700N

INDUCED POLARIZATION SURVEY — Pole–Dipole Array
SCOTT GEOPHYSICS LTD. — SCINTREX IPR12
August/03 — Pulse Rate: 2 sec

current electrode west of potential electrodes (array heading E)
Mx chargeability = 690–1050 msec after shutoff (mid point 870 msec)



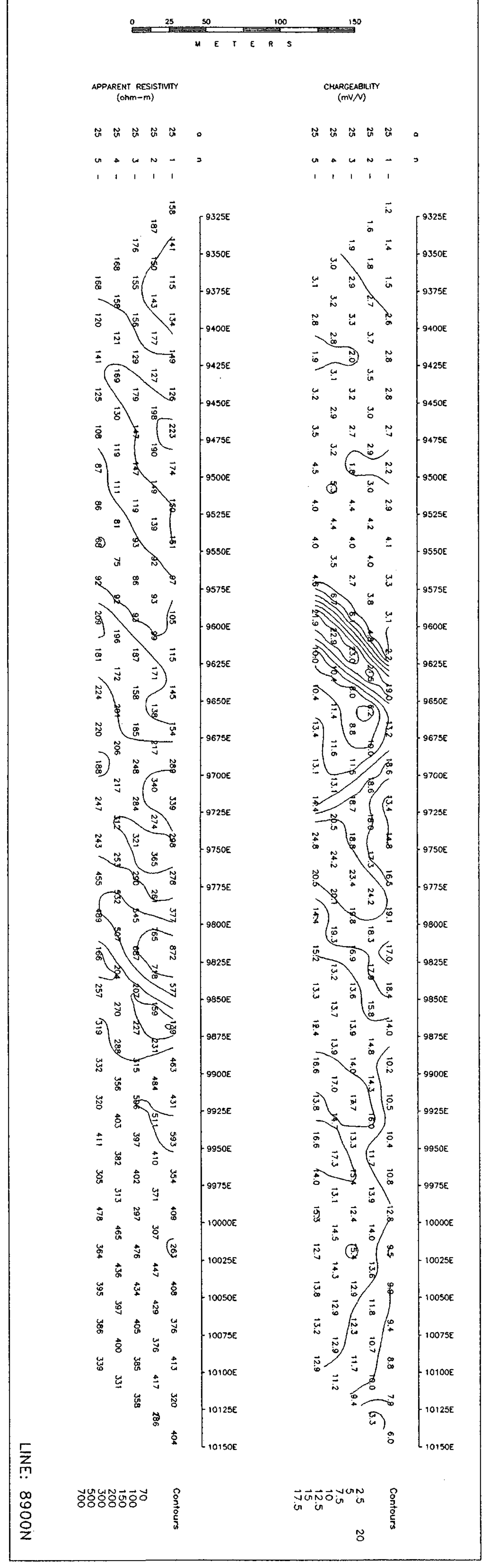
KODIAK EXPLORATION LTD.

TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 8900N

INDUCED POLARIZATION SURVEY — Pole–Dipole Array
SCOTT GEOPHYSICS LTD. — SCINTREX IPR12
August/03 — Pulse Rate: 2 sec

current electrode west of potential electrodes (array heading E)
Mx chargeability = 690–1050 msec after shutoff (mid point 870 msec)



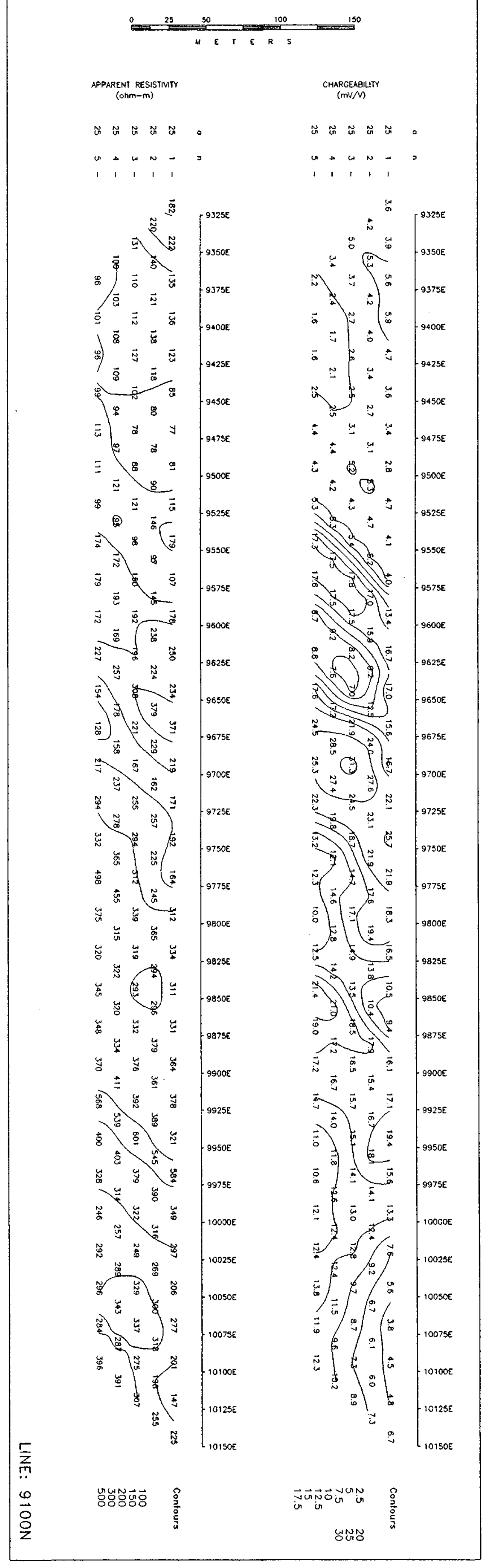
KODIAK EXPLORATION LTD.

TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 9100N

INDUCED POLARIZATION SURVEY — Pole–Dipole Array
SCOTT GEOPHYSICS LTD. — SCINTREX IPR12
August/03 — Pulse Rate: 2 sec

current electrode west of potential electrodes (array heading E)
Mx chargeability = 690–1050 msec after shutoff (mid point 870 msec)



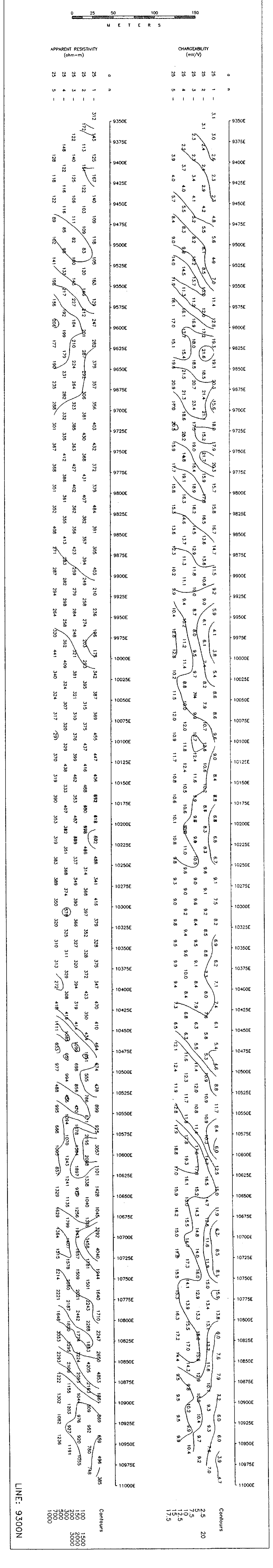
KODIAK EXPLORATION LTD.

TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 9300N

INDUCED POLARIZATION SURVEY — Pole–Dipole Array
SCOTT GEOPHYSICS LTD. — SCINTREX IPR12
August/03 — Pulse Rate: 2 sec

current electrode west of potential electrodes (array heading E)
Mx chargeability = 690–1050 msec after shutoff (mid point 870 msec)



KODIAK EXPLORATION LTD.

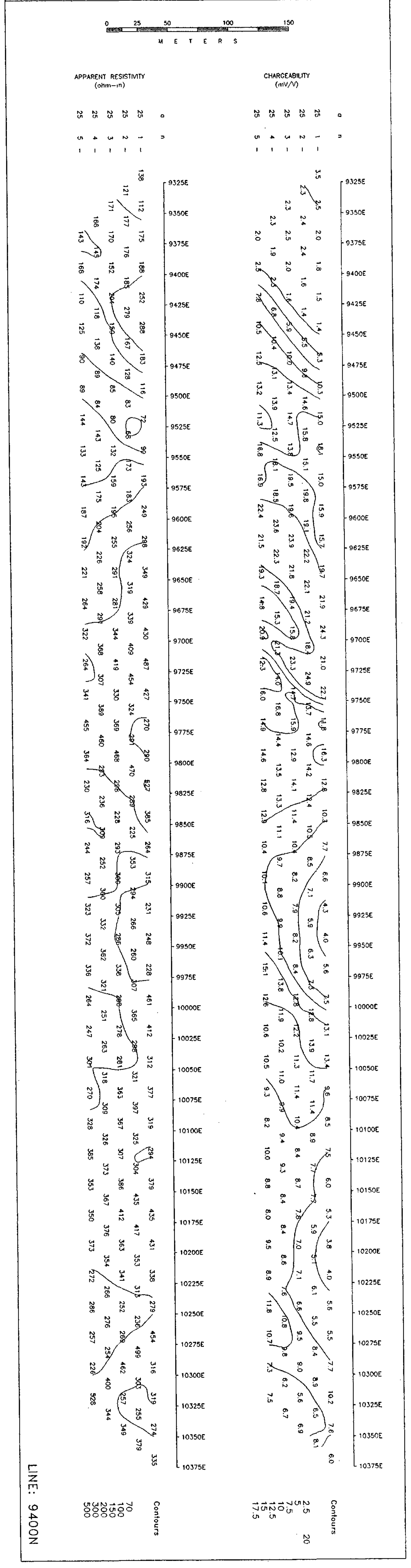
TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 9400N

INDUCED POLARIZATION SURVEY
SCOTT GEOPHYSICS LTD.
August/03

Pole-Dipole Array
SCINTREX IPR12
Pulse Rate: 2 sec

current electrode west of potential electrodes (array heading E)
Mx chargeability = 690-1050 msec after shutoff (mid point 870 msec)



KODIAK EXPLORATION LTD.

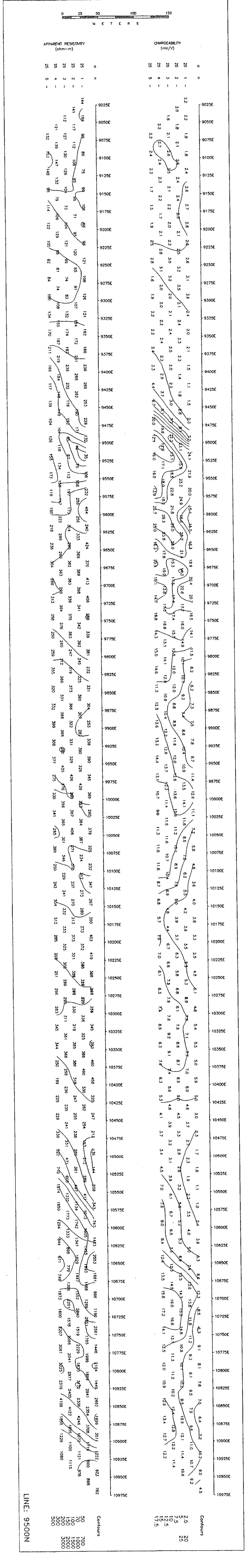
TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 9500N

INDUCED POLARIZATION SURVEY
SCOTT GEOPHYSICS LTD.
August/03

Pole-Dipole Array
SCINTREX IPR12
Pulse Rate: 2 sec

current electrode west of potential electrodes (array heading E)
Mx chargeability = 690-1050 msec after shutoff (mid point 870 msec)



KODIAK EXPLORATION LTD.

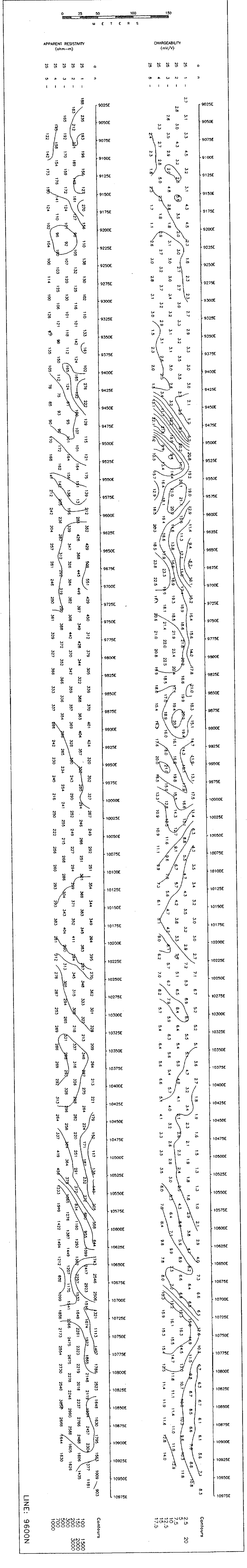
TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 9600N

INDUCED POLARIZATION SURVEY
SCOTT GEOPHYSICS LTD.
August/03

Pole-Dipole Array
SCINTREX IPR12
Pulse Rate: 2 sec

current electrode west of potential electrodes (array heading E)
Mx chargeability = 690-1050 msec after shutoff (mid point 870 msec)



KODIAK EXPLORATION LTD.

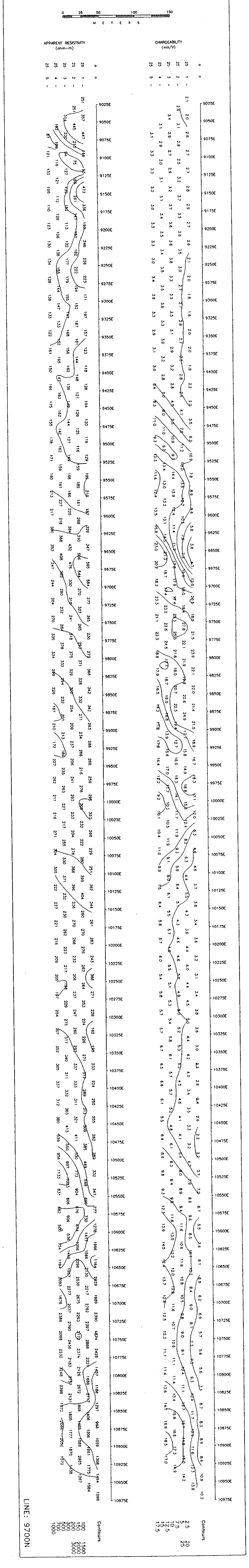
TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 9700N

INDUCED POLARIZATION SURVEY
SCOTT GEOPHYSICS LTD.
August/03

Pole-Dipole Array
SCINTREX IPR12
Pulse Rate: 2 sec

current electrode west of potential electrodes (array heading E)
Mx chargeability = 690-1050 msec after shutoff (mid point 870 msec)



KODIAK EXPLORATION LTD.

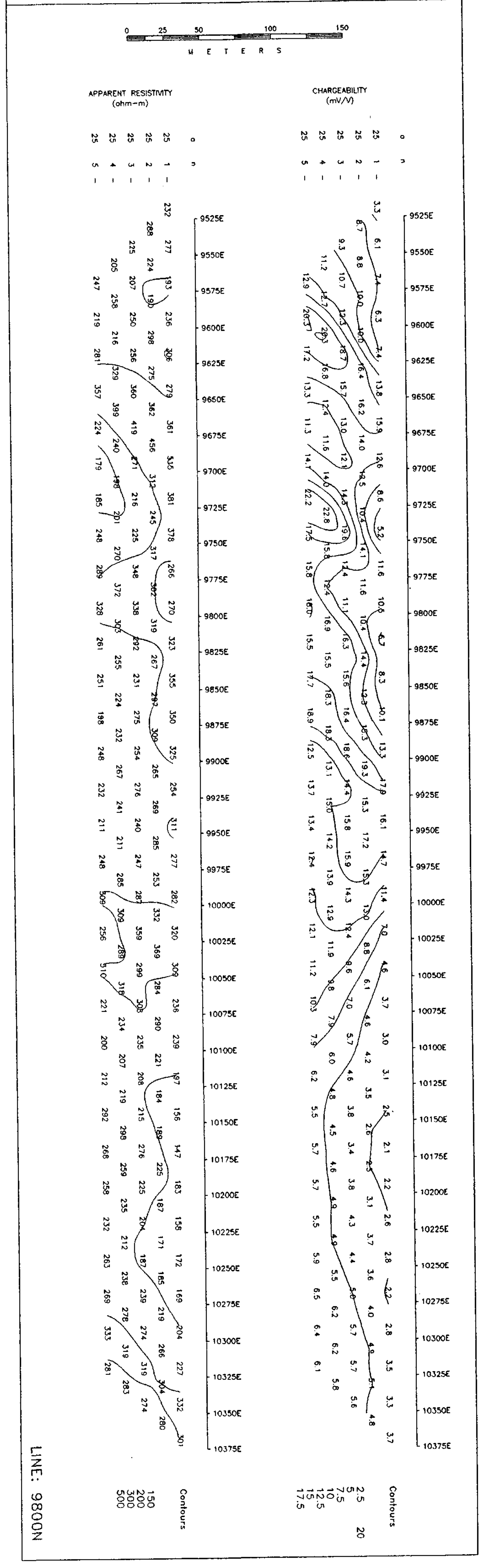
TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 9800N

INDUCED POLARIZATION SURVEY
SCOTT GEOPHYSICS LTD.
August/03

Pole-Dipole Array
SCINTREX IPR12
Pulse Rate: 2 sec

current electrode west of potential electrodes (array heading E)
Mx chargeability = 690-1050 msec after shutoff (mid point 870 msec)



M4

GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT

27,314 (M5)

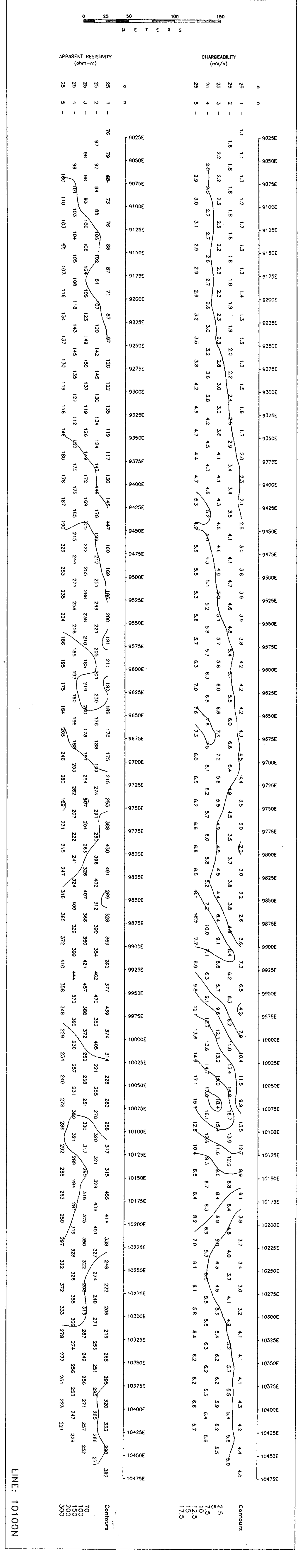
KODIAK EXPLORATION LTD.

TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 10100N

INDUCED POLARIZATION SURVEY — Pole–Dipole Array
SCOTT GEOPHYSICS LTD. — SCINTREX IPR12
August/03 — Pulse Rate: 2 sec

current electrode west of potential electrodes (array heading E)
Mx chargeability = 690–1050 msec after shutoff (mid point 870 msec)



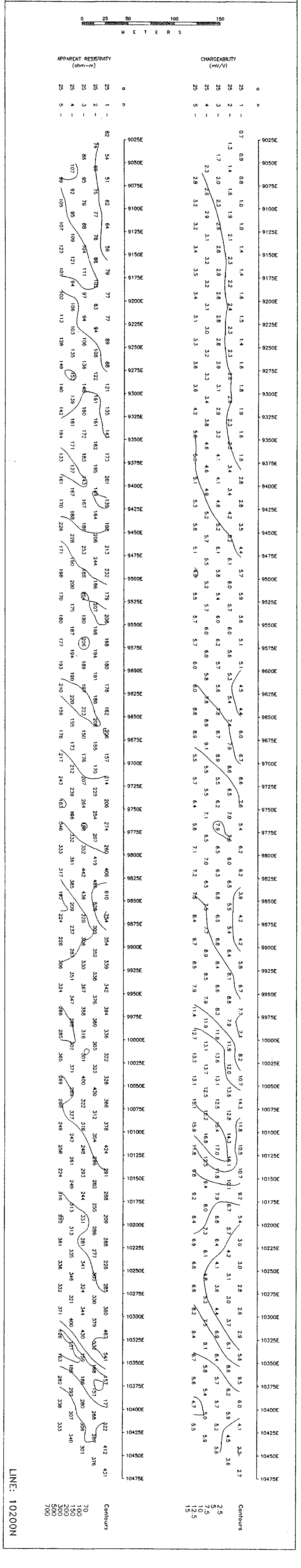
KODIAK EXPLORATION LTD.

TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 10200N

INDUCED POLARIZATION SURVEY — Pole–Dipole Array
SCOTT GEOPHYSICS LTD. — SCINTREX IPR12
August/03 — Pulse Rate: 2 sec

current electrode west of potential electrodes (array heading E)
Mx chargeability = 690–1050 msec after shutoff (mid point 870 msec)



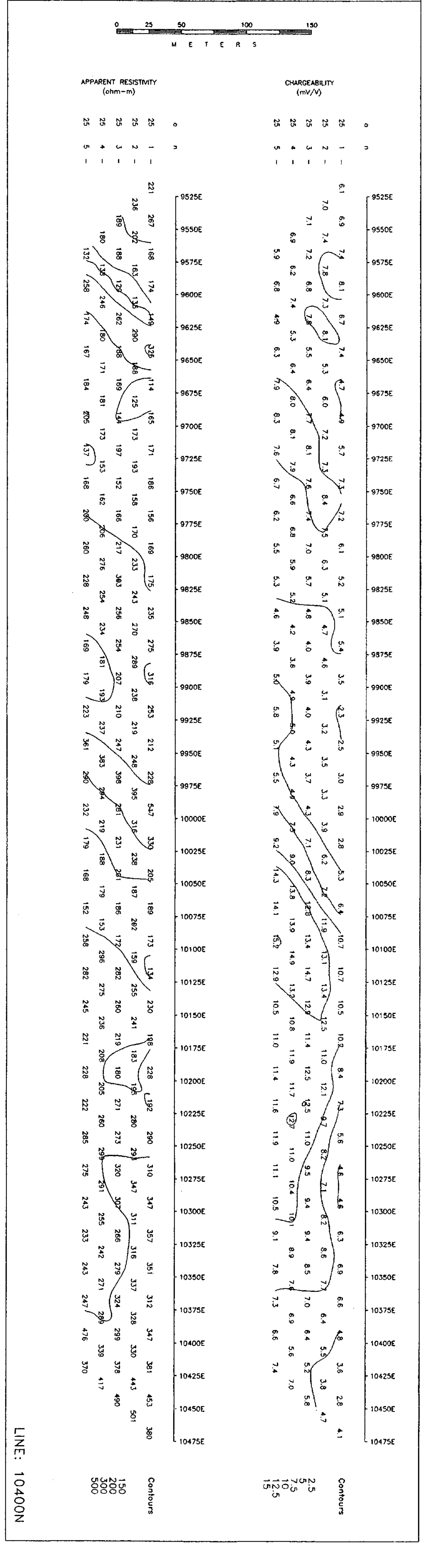
KODIAK EXPLORATION LTD.

TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 10400N

INDUCED POLARIZATION SURVEY — Pole–Dipole Array
SCOTT GEOPHYSICS LTD. — SCINTREX IPR12
August/03 — Pulse Rate: 2 sec

current electrode west of potential electrodes (array heading E)
Mx chargeability = 690–1050 msec after shutoff (mid point 870 msec)



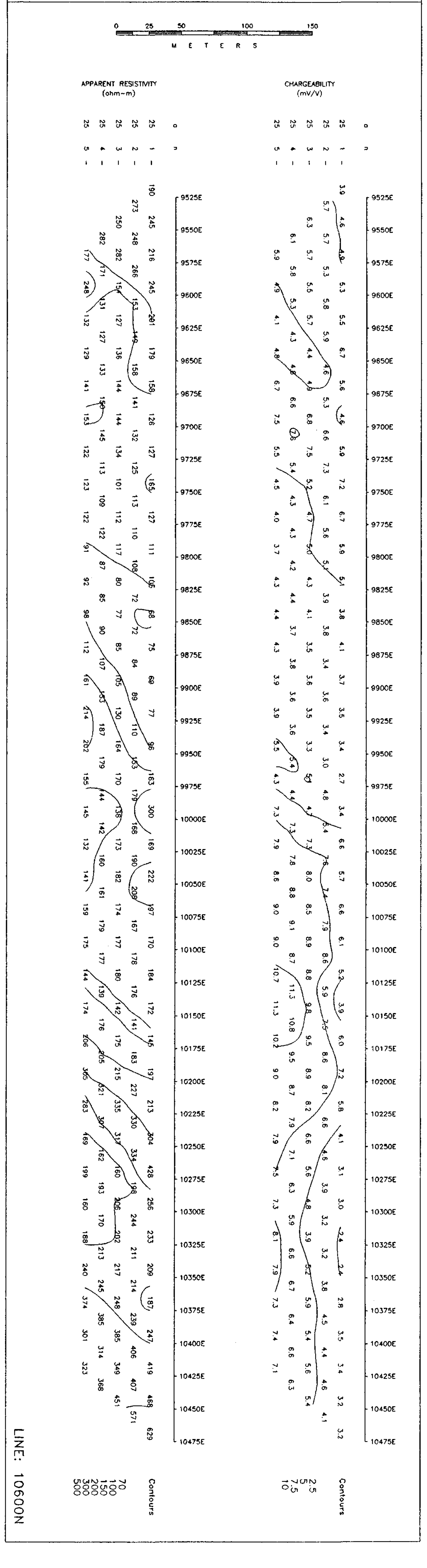
KODIAK EXPLORATION LTD.

TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 10600N

INDUCED POLARIZATION SURVEY — Pole–Dipole Array
SCOTT GEOPHYSICS LTD. — SCINTREX IPR12
August/03 — Pulse Rate: 2 sec

current electrode west of potential electrodes (array heading E)
Mx chargeability = 690–1050 msec after shutoff (mid point 870 msec)



KODIAK EXPLORATION LTD.

TOMMY JACK PROPERTY, HAZELTON AREA, B.C.

LINE: 10800N

INDUCED POLARIZATION SURVEY — Pole–Dipole Array
SCOTT GEOPHYSICS LTD. — SCINTREX IPR12
August/03 — Pulse Rate: 2 sec

current electrode west of potential electrodes (array heading E)
Mx chargeability = 690–1050 msec after shutoff (mid point 870 msec)