ASSESSMENT REPORT
on
GEOLOGY, GEOCHEMISTRY, GEOPHYSICS & TRENCHING

MW PROPERTY

Wycliffe area, SE B.C.

UTM 584000E 5501000N

TRIM 82G.061, 062, 071 & 072

For

SEDEX MINING CORP.
711 - 675 West Hastings Street
Vancouver, B.C.
V6B 1N2

By
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February, 2004

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1.00 INTRODUCTION

1.10 Location and Access

The MW claims are located in southeastern British Columbia on the western edge of the Rocky Mountain Trench with the property centered approximately 10 km ESE of Kimberley and near UTM coords. 584000E, 5501000N (Fig. 1).

Highway 95A bounds most of the claim block to the north (east of Kimberley) and to the south (SE of Kimberley). Numerous secondary roads cross the property and provide excellent road access.

1.20 Property

The MW property includes 206 claim units in 78 2- and 4-post mineral claims; MW 1-47, MW 50-71, MW 80 and MW 85-92 (Fig. 2). The claims are owned by Super Group Holdings Ltd. of Cranbrook, B.C. and Sedex Mining Corp. of Vancouver, B.C.

1.30 Physiography

The MW claims are situated along the western margin of the Rocky Mountain Trench, just north of the St. Mary River. Topography on the claim block is subdued and bedrock exposures are sparse (<1 %), although enough bedrock exists to demonstrate that only a thin veneer of glacial debris covers most of the claim area (compared to at least 600 meters of glacial debris cover locally on the east side of the Rocky Mountain Trench). Elevations range from about 870 to 970 meters. Vegetation reflects the low elevation and relatively dry climate and consists of grasslands, shrubs and sparse Yellow Pine, Douglas Fir and aspen. A few bedrock exposures are present above the widespread blanket of glacial overburden and in the post-glacial stream channels.

1.40 History

The MW claims cover a large block of ground not far southeast of the former producing world class Sullivan zinc-lead-silver deposit which was located just north of Kimberley. The property is also on the northwest flank of a very large aeromagnetic anomaly associated with a Cretaceous felsic (granodiorite to quartz monzonite) intrusion. Thus the MW property has potential for a Precambrian base metal deposit as well as a Cretaceous gold deposit. Previous exploration on what is now the MW property was for both base metal and gold mineralization.

Cominco has long held ground over what are now the MW claims as the eastern part of their large Sullivan Mine claim block. Their work included geologic mapping and small ground geophysics programs (eg. AR 2555). In the mid 1970's Esso Minerals controlled a large block of claims in the area. They conducted ground geophysical surveys and drilled a number of holes

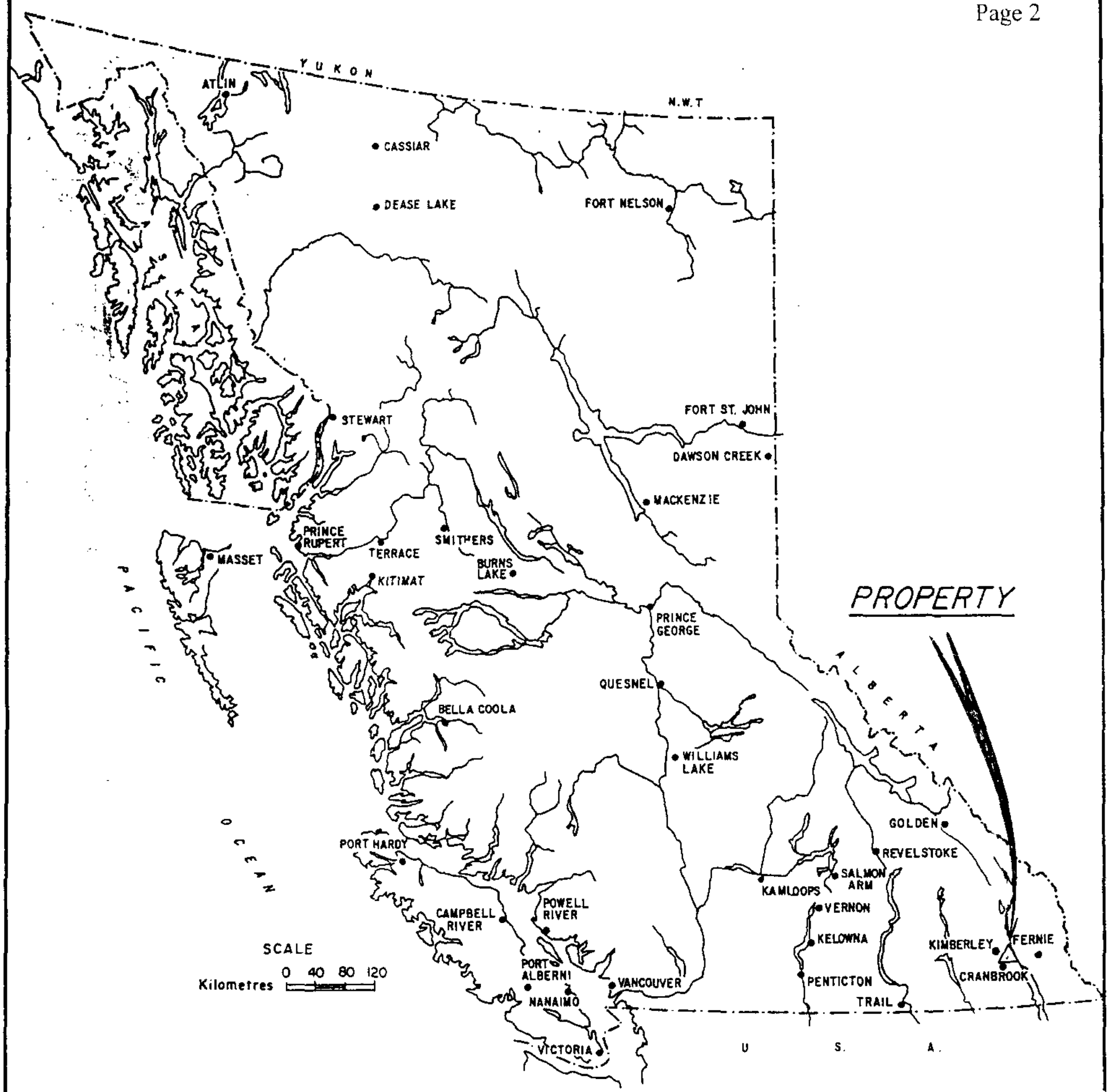

Figure 1
MW Property
Location Map

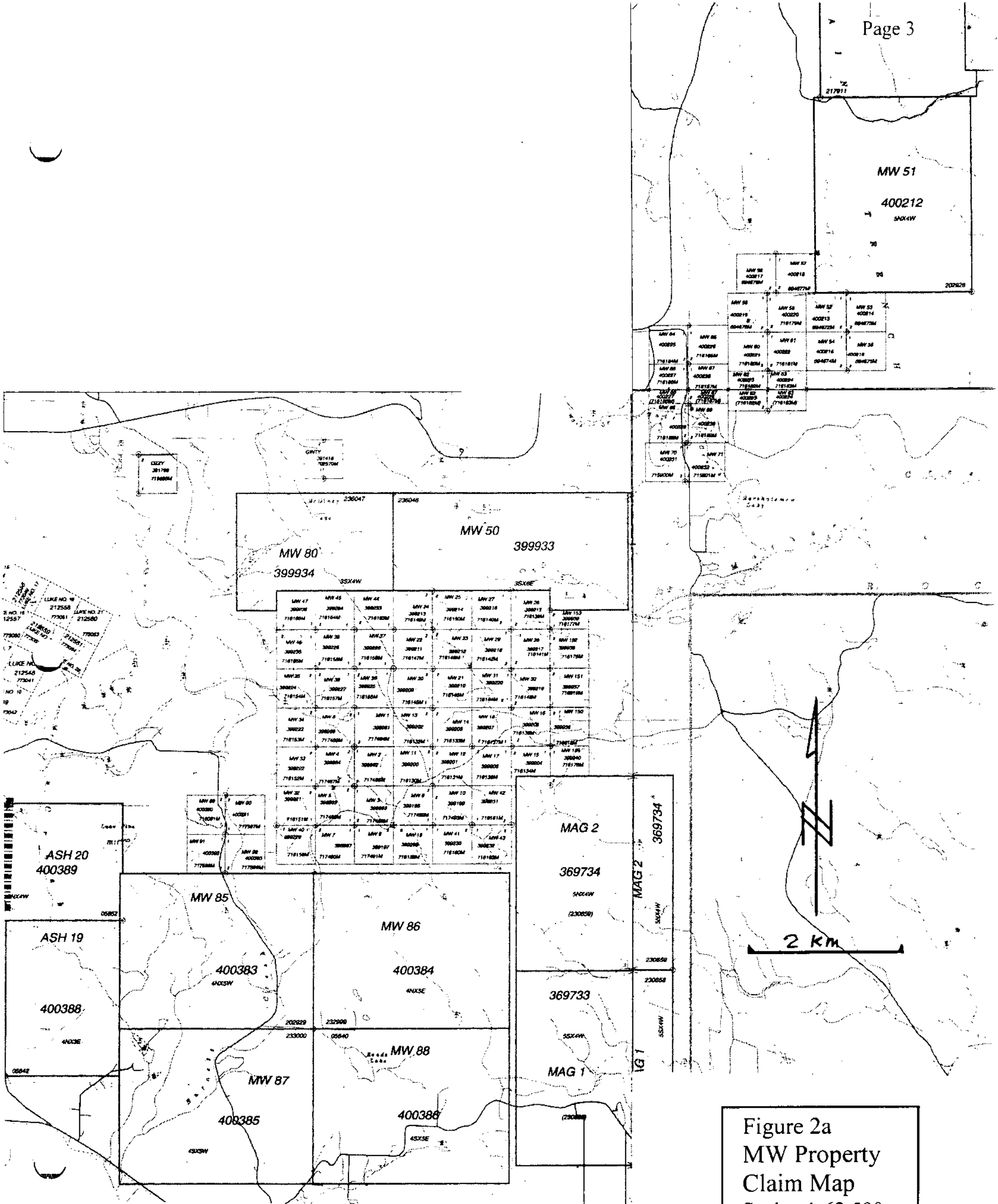

Figure 2a
MW Property
Claim Map
Scale ~1:62,500
TRIM 82G.061 ,062, 071, 072

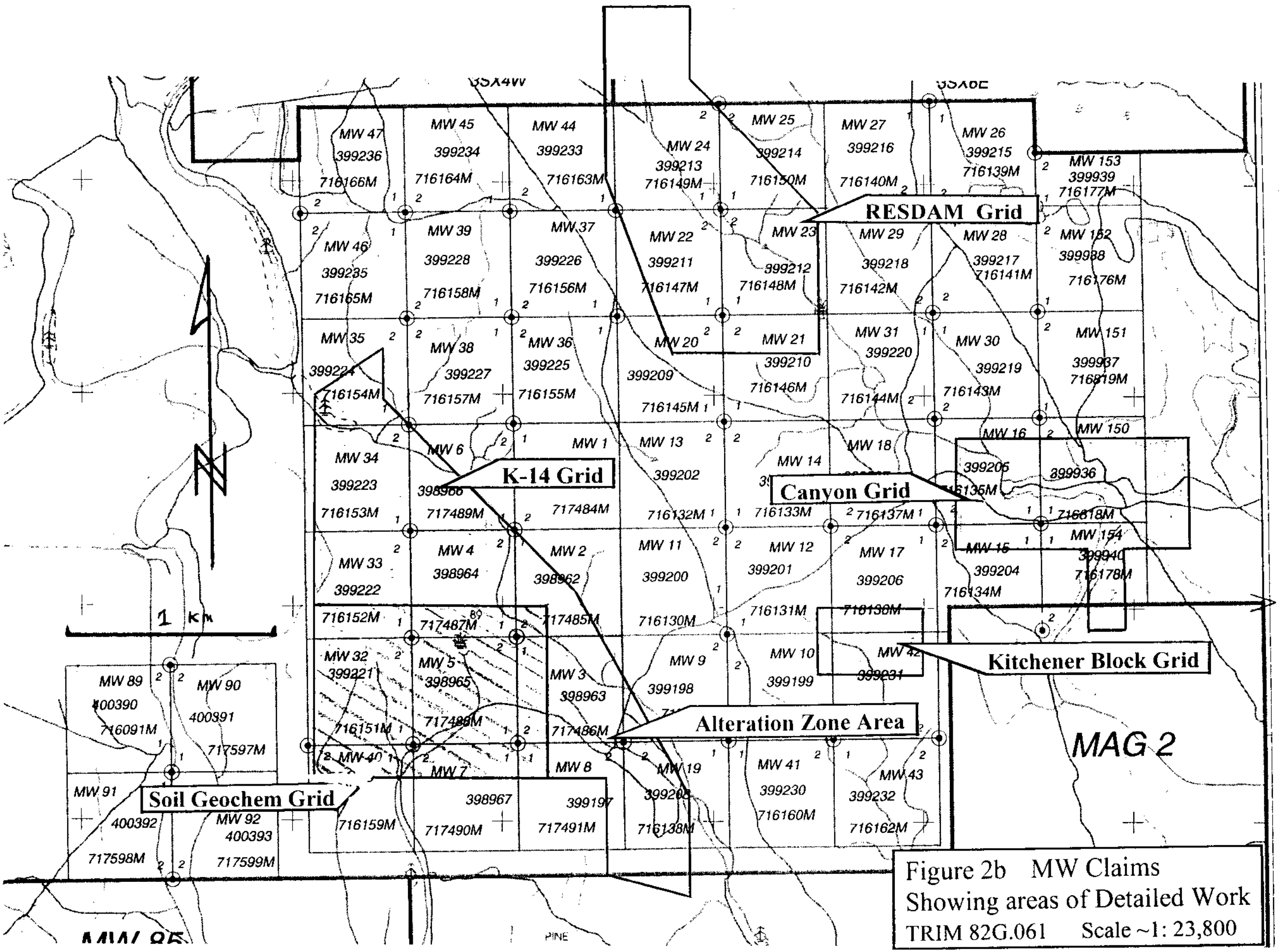

Figure 2b MW Claims
Showing areas of Detailed Work
TRIM 82G.061 Scale ~1: 23,800

searching for base metals (eg. AR's 05217, 05638, 05967, 06312). In the mid to late 1980's Normine Resources Ltd. controlled ground in the NE portion of the present MW claims. They did ground geophysics and diamond drilling searching for base metals. Some of their drilling intersected anomalous gold mineralization. Also in the mid to late 1980's Victoria Resource Corporation held ground in the present SE MW claim block area; their work included ground geophysics, soil and rock geochemistry and diamond drilling in a search for gold mineralization associated with the Cretaceous felsic intrusions (eg. AR's 16689, 22732).

In 1996 Sedex Mining Corp drilled one hole to follow up on the anomalous gold mineralization first encountered by Normine Resources Ltd. on what is now the NE portion of the MW claims (AR 24769). The most recent exploration work in the area was a diamond drilling program by Pathfinder Resources Ltd. on the MAG claims which are immediately east of the MW claims (Peters, 2001, AR 26506).

1.50 Scope of Present Program

Prospecting by C. Kennedy of Super Group Holdings Ltd. during the autumn of 2002 discovered significant gold mineralization in sparse bedrock exposures and led to staking of the MW claims. Subsequent preliminary evaluation of the property has included further rock geochemistry, soil geochemistry, geologic mapping, VLF-EM geophysical surveying and trenching.

2.00 GEOLOGY

The MW claim area is underlain by mesoproterozoic Purcell Supergroup rocks of the Aldridge, Creston and Kitchener Formations as well as overlying Cambrian Eager Formation. These are all mainly fine-grained clastic and carbonate lithologies and include quartzites, siltstones, argillites and dolomitic and calcareous siltstones. The Aldridge Formation is intruded by gabbroic composition Moyie sills and dikes and all units are intruded by Cretaceous granodiorite to monzonite felsic intrusions.

The MW property is situated within the Rocky Mountain Trench just west of a very large aeromagnetic anomaly and also covers parts of two major east-west faults, the St Mary and Kimberley Faults.

The claims are within an area of structural complexity with numerous fault-bounded blocks and significant rotation of some individual fault blocks. The level of structural deformation is greater on the MW property than in most adjacent areas. This can be attributed to a zone of intersection between strong northeast structure coinciding with the 'Kanasewich rift' (Kanasewich, 1968, Kanasewich et al, 1969) and a northwest-oriented flexure in the Rocky Mountain Trench.

Prospecting and rock geochemistry completed by Craig Kennedy in the fall of 2002 identified a number of previously unknown sites of anomalous gold mineralization. Gold occurs with narrow quartz veins, within northeast fault zones and within one larger zone of strong limonitic/manganese and siliceous alteration. Anomalous gold is hosted by different stratigraphies on the property including Middle Aldridge Formation, Aldridge - Creston transition and Creston Formation. Geology of the areas where detailed exploration activity was conducted in 2003 are shown in Figures 3a and 3b.

Gold values from the original sampling on the property range up to 10,660 ppb and significantly anomalous values obtained to date range over an area of 3 km by 2 km. Stronger gold values commonly are associated with elevated copper, lead, silver and zinc

3.00 VLF-EM GEOPHYSICS

3.10 Introduction

Bedrock exposures in the MW claim area are very sparse and, with gold mineralization believed related to structures, VLF-EM geophysical surveying was conducted to identify bedrock structures. Although overburden cover is extensive, the sparse exposures of bedrock suggest that bedrock is only shallowly buried over much of the claim block so VLF-EM is a suitable means of detecting conductors and structure in buried bedrock.

A reconnaissance VLF-EM survey was initially conducted over an area of widespread subcropping argillic and limonitic alteration where anomalous gold mineralization was present, near 5500700N, 582800E. Once a few anomalous responses were detected, a grid was surveyed and this was eventually expanded to a series of grids which were started where some anomalous gold had been earlier detected in bedrock or subcrop.

The areas of the VLF-EM survey are shown in Figure 2b and survey lines and survey data for individual areas are shown in Figures 4a to 4e. Survey lines were run mostly N-S although an area around the old Imperial Oil diamond drill hole K-14 was done with NW oriented lines, to cross ENE and NE anomalies. Lines were located using GPS and run by compass and measured with a hip-chain with VLF-EM readings taken at 25 meter spacings. Sufficient GPS readings were taken during VLF-EM surveying to provide confidence in plotting all survey lines on the base map. A total of just over 77 kilometers of line was surveyed.

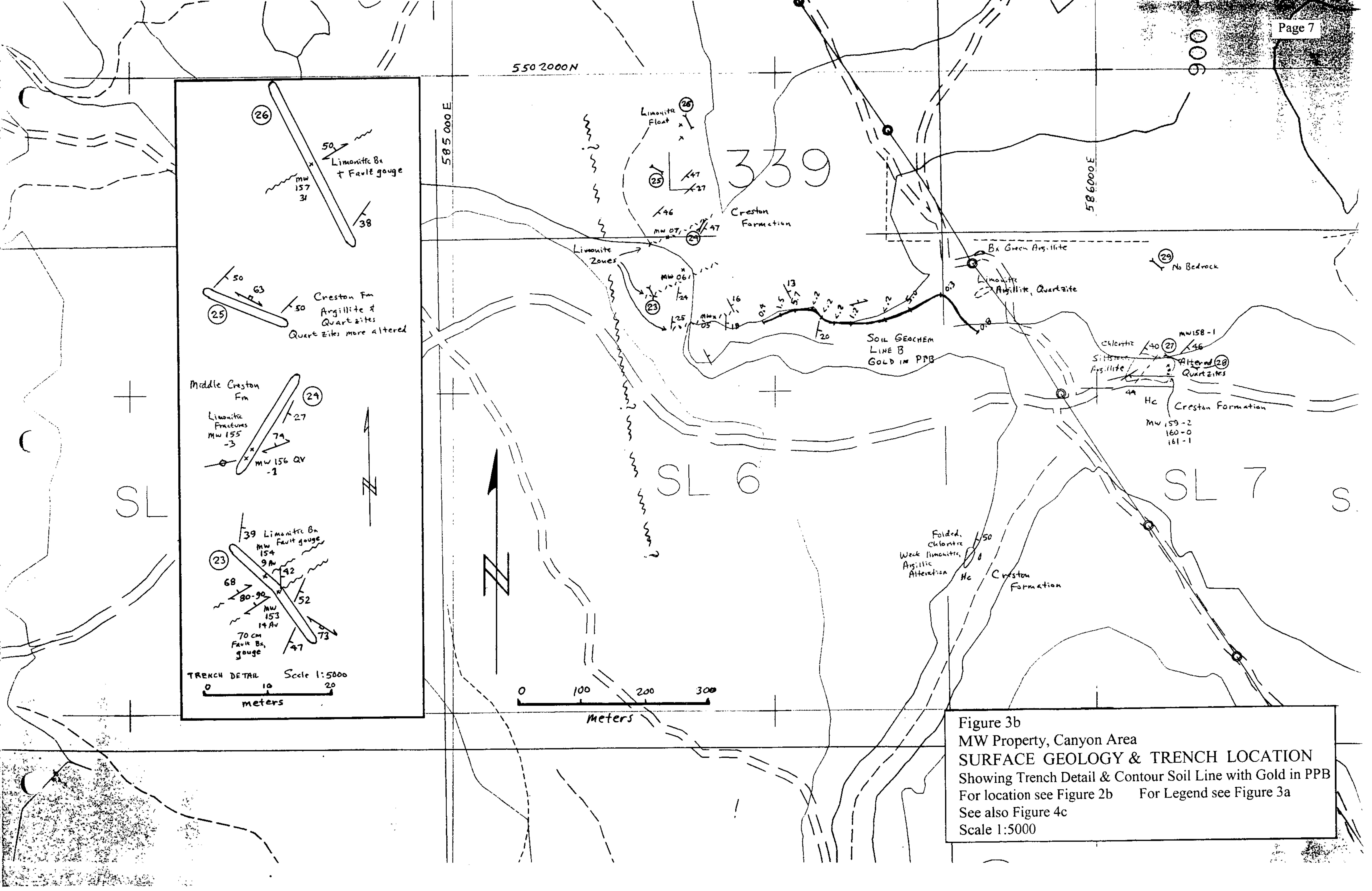

Figure 3b
MW Property, Canyon Area
SURFACE GEOLOGY & TRENCH LOCATION
Showing Trench Detail & Contour Soil Line with Gold in PPB
For location see Figure 2b For Legend see Figure 3a
See also Figure 4c
Scale 1:5000

3.20 VLF-EM Survey

3.21 Instrumentation and Survey Procedure

The VLF-EM (**V**ery **L**ow **F**requency **E**lectro**m**agnetics) method uses powerful radio transmitters set up in different parts of the world for military communication and navigation. In radio communication terminology, VLF means very low frequency, about 15 to 25 kHz. Relative to frequencies generally used in geophysical exploration, the VLF technique actually uses very high frequencies.

A Crone Radem VLF-EM receiver, manufactured by Crone Geophysics Ltd. of Mississauga, Ontario was used for the VLF-EM survey. Seattle, Washington, transmitting at 24.8 kHz and at an approximate azimuth of 247° from the survey area, was used as the transmitting station. This transmitting station is favorably located for detecting northeast-oriented structure, which is one of the primary controls of gold mineralization in the Cranbrook area. A few east-west oriented lines were surveyed using Annapolis, Maryland (21.4 kHz) as the transmitting station, located at an azimuth of ~ 124° from the survey area.

In all electromagnetic prospecting, a transmitter produces an alternating magnetic (primary) field by a strong alternating current usually through a coil of wire. If a conductive mass such as a sulfide body is within this magnetic field, a secondary alternating current is induced within it, which in turn induces a secondary magnetic field that distorts the primary magnetic field. The VLF-EM receiver measures the resultant field of the primary and secondary fields, and measures this as the tilt or 'dip angle'. The Crone Radem VLF-EM receiver measures both the total field strength and the dip angle.

The VLF-EM uses a frequency range from about 15 to 28 kHz, whereas most EM instruments use frequencies ranging from a few hundred to a few thousand Hz. Because of its relatively high frequency, the VLF-EM can detect zones of relatively lower conductivity. This results in it being a useful tool for geologic mapping in areas of overburden but it also often results in detection of weak anomalies that are difficult to explain. However the VLF-EM can also detect sulfide bodies that have too low a conductivity for other EM methods to pick up.

Results were reduced by applying the Fraser Filter and both dip angle and Fraser Filter values are shown on the survey lines in Figures 4a to 4e.

The Fraser Filter is essentially a 4-point difference operator which transforms zero crossings into peaks, and a low pass operator which induces the inherent high frequency noise in the data. Thus the noisy, often non-contourable data are transformed into less noisy, contourable data. Another advantage of this filter is that a conductor which does not show up as a zero crossover in the unfiltered data quite often shows up in the filtered data.

4.22 Discussion of Results

Southwest Area; Alteration Zone

This grid (Figs. 2a & 4a) which extends from about 582150E to 583900E and 549500N to 5501000N is a series of 50 to 100 meter spaced N-S lines, centered approximately on the Gas Pipeline. VLF-EM surveying detected 3 fairly distinct ~060° trending weak to moderate anomalies.

One of the larger areas of exposed bedrock on the MW claims occurs in the western portion of this grid. Middle Aldridge Formation metasedimentary rocks here strike NNE and dip moderately to steeply SE. Thus the VLF responses are oblique to bedding and are probably caused by structures which in turn may control the alteration and associated gold mineralization seen in the grid area. Subsequent trenching exposed considerable structure and it is apparent that the VLF anomalies do reflect structure. The 3 ENE-trending VLF-EM anomalies on this grid may define a broad deformation zone within which extensive brecciation, quartz veining, argillic and limonitic alteration are host to gold mineralization.

East of the pipeline a number of VLF-EM responses were detected. The most continuous of these trends northeasterly (centered at ~ 5500100N, 583700E) and is the strongest conductor detected in the entire MW property survey area to date. Trenching has not been done here yet. The other VLF-EM responses are mostly weak but some of them appear to reflect northwest structures although more detailed surveying is required to establish this.

Drill Hole K-14 Area (NW-oriented grid)

Initial surveying of this area (Figs. 2b & 4a) along lines extending northwest from the Alteration Zone area detected VLF-EM responses with a more NE to NNE orientation and, to provide better definition of these responses, a subsequent grid was established with NW-SE oriented lines.

A series of at least 4 NE to NNE oriented weak to moderate anomalous responses was detected on the K-14 grid. Sedimentary beds near DDH K-14 strike NNW and dip moderately east thus these VLF-EM responses are also oblique to bedding and probably represent cross-cutting structures of some kind. Some of the higher gold values from surface bedrock geochemistry are from near K-14 (~10 and 16 gram/tonne gold values in original prospecting) although host bedrock is relatively unaltered. These higher gold values may be with 'distal' quartz veins beyond areas of stronger hydrothermal alteration.

In the NW portion of the K-14 grid an ENE-trending quartz vein is hosted by NNE-striking / moderately east dipping middle Aldridge metasediments and is located between 2 VLF-EM anomalies. This vein was trenched (Trenches 17, 18, 19 and 37; Fig. 6b) and was found to have elevated gold values with coarse pyrite and galena.

Northeast 'RESDAM' Area

A northern VLF-EM grid, centered about 5503000N, 583900E (Figs. 2b & 4b) covers patchy bedrock exposures of thin bedded and laminated argillite and siltstone of the upper Aldridge Formation which may be a relatively unfavourable host for structurally-controlled gold mineralization. Original prospecting in this part of the property identified 1.54 and 2.16 gram/tonne gold values in subcropping material. VLF-EM surveying of the 'RESDAM' grid, with N-S oriented lines, detected a series of weak to moderate ENE to E-W and SE oriented responses. A gas pipeline crosses the area and interferes with the VLF responses. Two trenches were subsequently dug on the anomalous float but none of the VLF-EM anomalies here have been trenched. Bedding in this grid area strikes N-S and dips shallow to moderately east thus, again, the VLF responses are oblique to bedding and they probably represent cross-cutting structure.

A series of E-W oriented lines were surveyed across parts of the RESDAM area (fig. 4c) to test for a northeast fault that separates Middle Aldridge Formation on the west from Creston Formation on the east. This fault is inferred from geology in the Alteration Zone area and is tentatively located by terminations in VLF-EM anomalies. This NNE fault may terminate the E-W VLF-EM anomaly at 2400N on the RESDAM grid, and may coincide with a weak NE anomaly at 4200E, 2900N (Fig. 4b). Surveying on the east-west lines failed to detect any anomaly near 2400N, 4000E but confirmed the original response at 4200E, 2900N. If the fault passes through here it is only locally a weak 'conductor', and thus may not be a factor in the deposition of gold mineralization.

Eastern 'Canyon' Area

An eastern or 'Canyon' VLF-EM grid (Figs. 2a & 4d) of N-S lines is centered approximately at 5501500N, 585700E. A NNW-oriented electrical Power Line crosses this grid and interferes with the VLF response locally. A central ENE-oriented moderate VLF-EM response crosses the grid area; additional surveying in the central portion of the grid area is needed to confirm the continuity of the anomaly across the grid area. This anomaly appears to end abruptly at ~ 585275E, possibly along a northerly-striking fault. Other anomalies present on the grid are of moderate to weak strength. Their currently established strike length is short and orientations appear to be E-W to ENE and WNW.

Bedding in the grid area strikes NE to N-S with shallow to moderate SE to E dips. Generally the VLF anomalies cross bedding suggesting they represent cross-cutting structures. Further work is needed here to better delineate some of the anomalies, with additional surveying needed on both intermediate and peripheral lines.

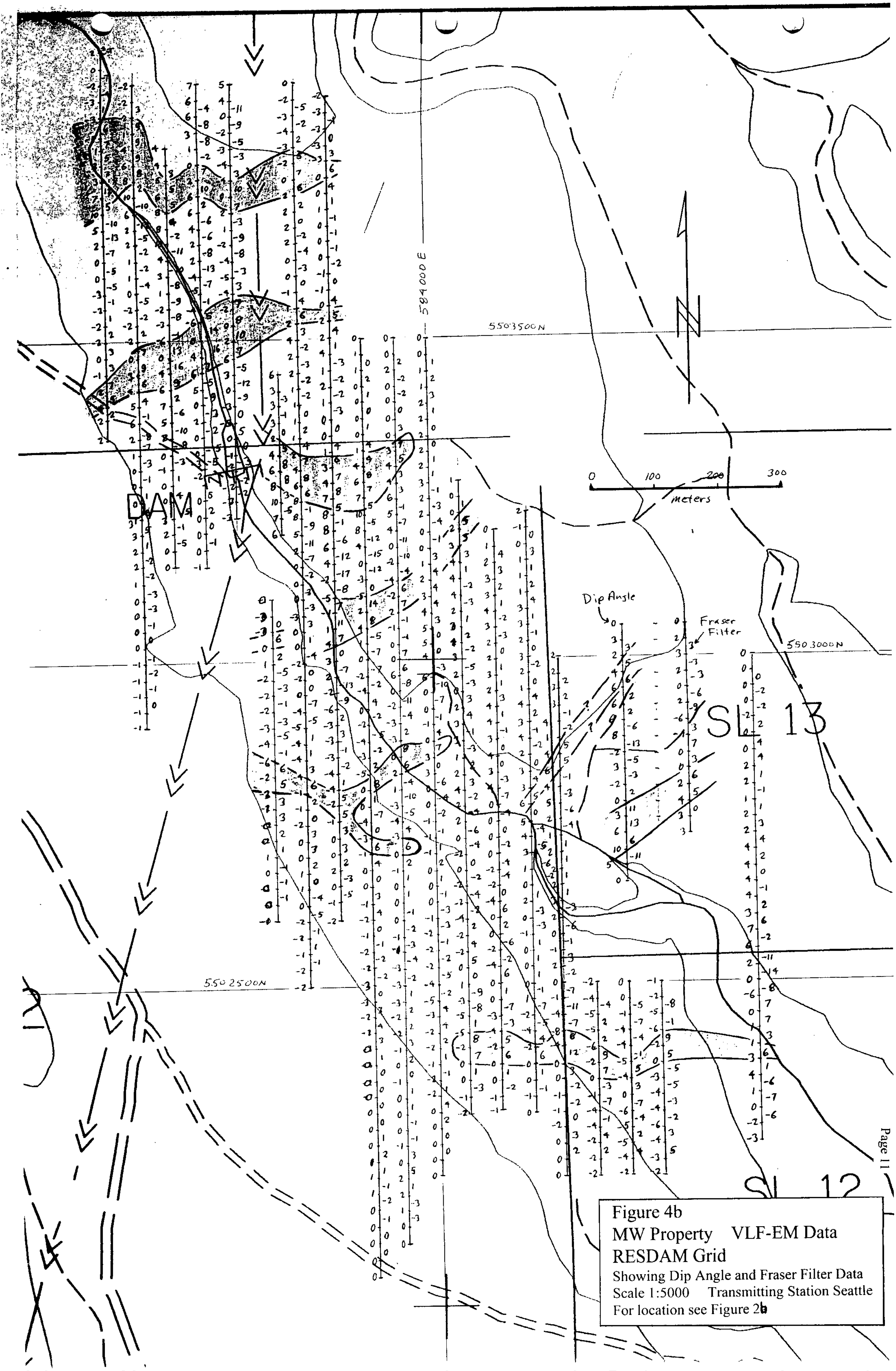

Figure 4b
MW Property VLF-EM Data
RESDAM Grid
Showing Dip Angle and Fraser Filter Data
Scale 1:5000 Transmitting Station Seattle
For location see Figure 2b

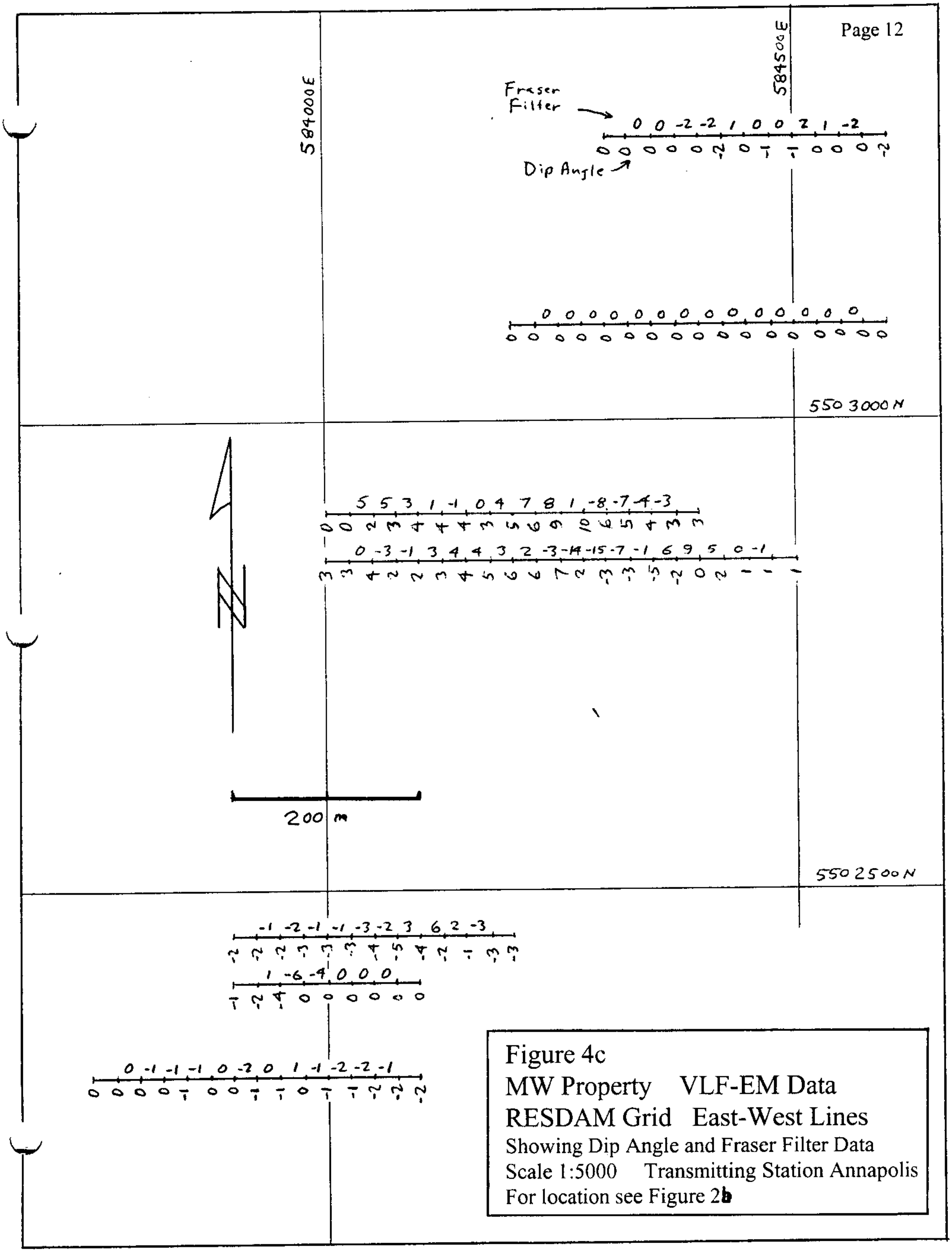

Figure 4c
MW Property VLF-EM Data
RESDAM Grid East-West Lines
Showing Dip Angle and Fraser Filter Data
Scale 1:5000 Transmitting Station Annapolis
For location see Figure 2b

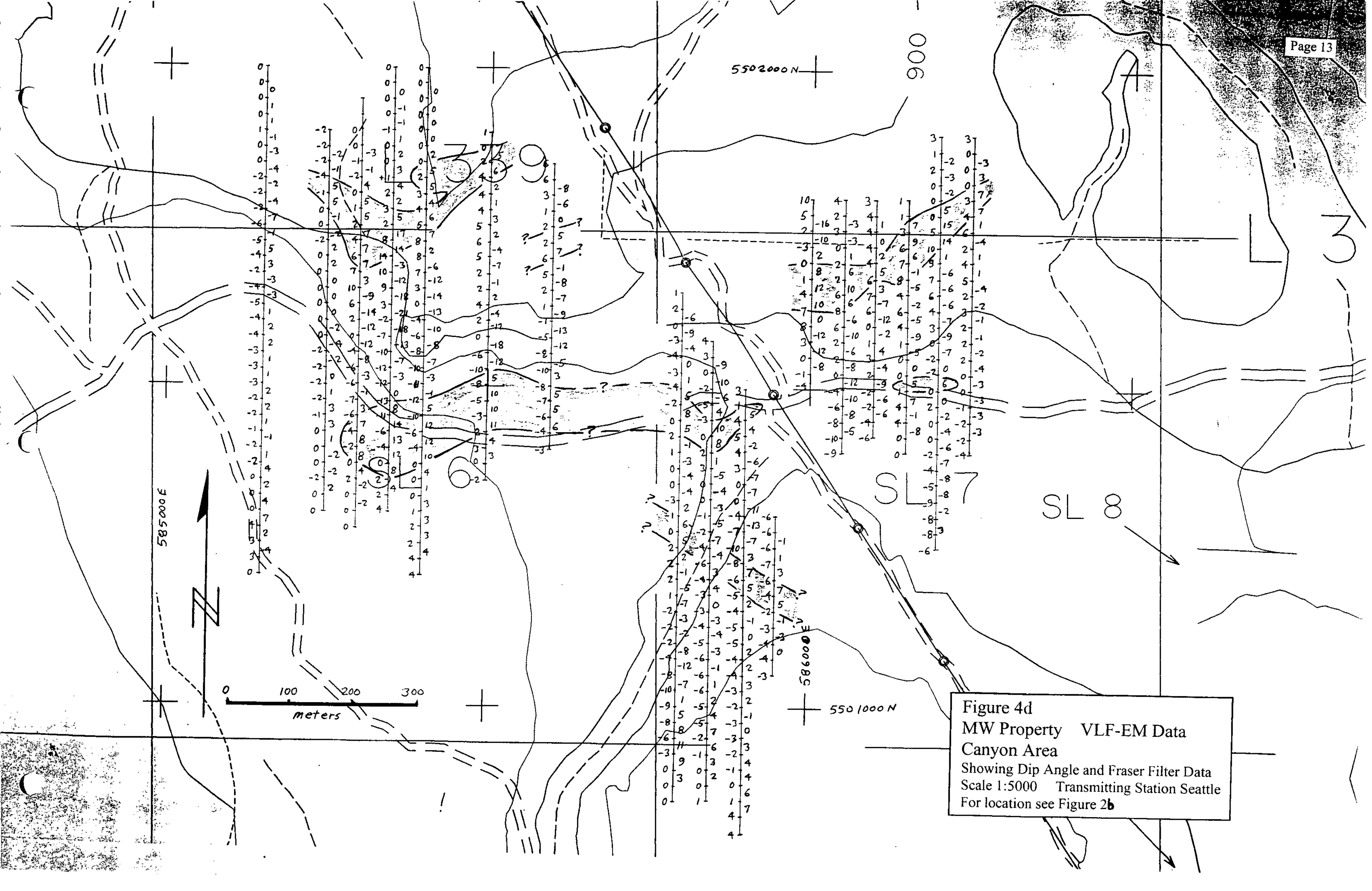

Figure 4d
MW Property VLF-EM Data
Canyon Area
Showing Dip Angle and Fraser Filter Data
Scale 1:5000 Transmitting Station Seattle
For location see Figure 2b

Southeast, Kitchener Block area

Four 100 m spaced east-west VLF-EM lines were surveyed in an area where prospecting had indicated a fault block of Kitchener Formation was present (Figs 2b and 4e). The purpose of the VLF here was to detect any bounding faults on this block. The minimal VLF-EM surveying detected 2 NNE-trending anomalies.

4.00 SOIL AND ROCK GEOCHEMISTRY

4.10 Soil Geochemistry

Much of the bedrock on the MW property is covered by glacial and glacio-fluvial deposits and the topography is subdued thus soil geochemistry could be expected to not work well. One soil grid and 3 'reconnaissance contour' lines were sampled as a test.

The soil grid covers the large alteration zone, centered at ~ 550500N 582700E, where anomalous gold is present in subcropping argillic and limonitic altered middle Aldridge Formation sediments. The soil geochemistry grid comprises 12 north-south lines, spaced at 100 meters with samples taken at 50 m intervals (Figure 4). The survey was controlled using GPS. Soil samples were collected from the 'B' horizon at an average depth of about 15 cm, placed in Kraft paper bags, then dried and shipped to Acme Analytical Laboratories Ltd. at 852 East Hastings Street, Vancouver, B.C., where they were analyzed for a 30 element ICP package and geochemical gold by standard analytical techniques.

The three contour lines (Lines A, B & C; Figs. 3a and 3b) were located near the base of post-glacial stream channels where previous work had identified some anomalous gold mineralization or favourable alteration. The contour lines were controlled with GPS. These samples were treated similarly to the grid soils but analyses were just for gold (Appendix 2).

Results

The soil grid (Fig. 5) barely detected the gold mineralization of the Alteration Zone, with a single value of 6.9 ppb Au at 5500750N on line 582800E. Two other weak gold values were detected in the very northwest portion of the grid (14.4 and 6.8 ppb Au), near where northwest-striking quartz-carbonate veins are present.

Only 2 anomalous gold values were detected by the 3 contour soil lines, both on Line C (Fig. 3a). At 325 S a sample was collected from altered material near the site of rock samples MW 08 and MW 09 (2160 and 5140 ppb Au respectively). This sample returned a value of 62.4 ppb Au. A second sample site at 775 S returned a value of 58.7 ppb Au. Subsequent follow-up prospecting identified a concentration of limonitic float material which appears to be subcrop and associated with an ENE trend of fairly weak limonite alteration.

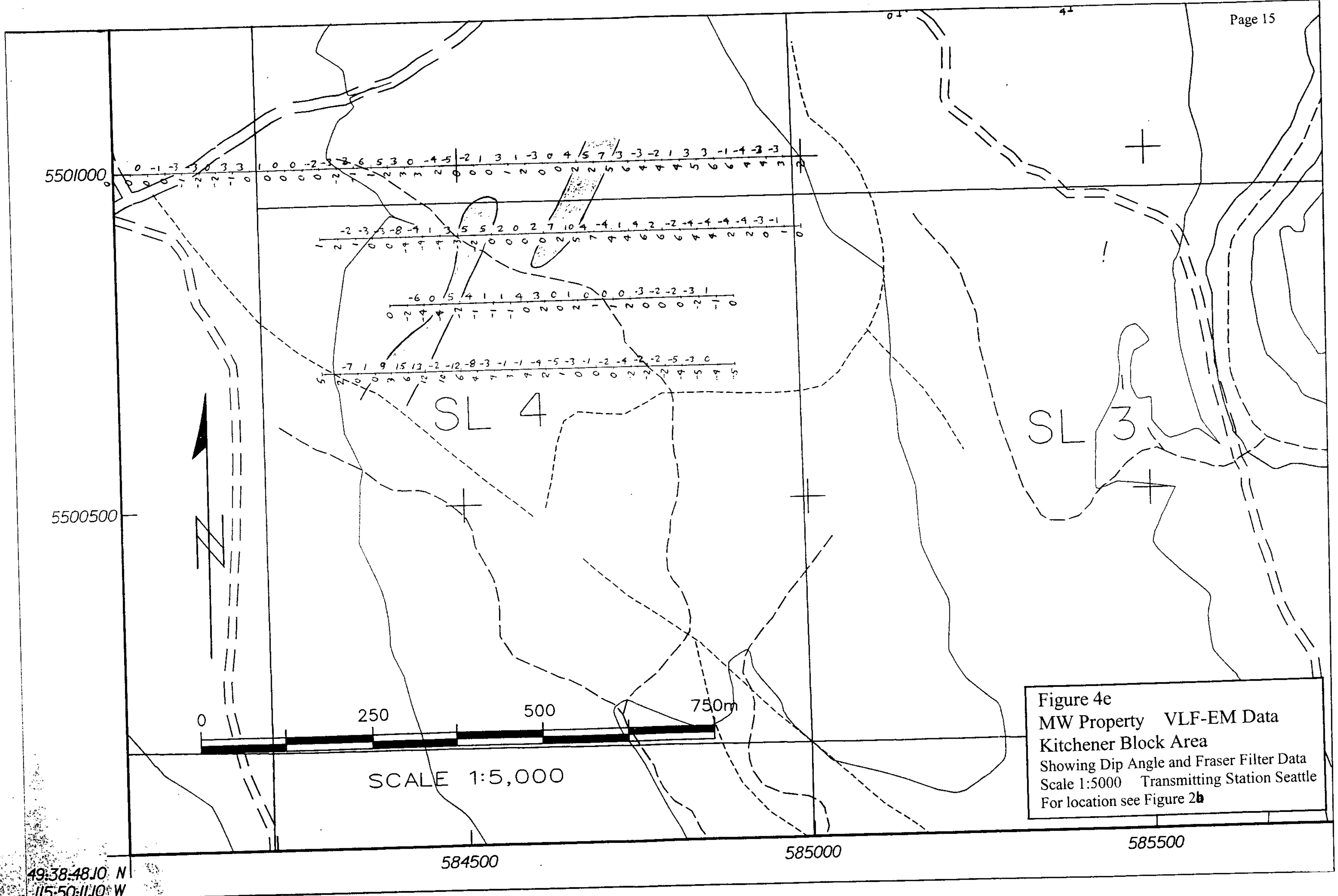

Figure 4e
MW Property VLF-EM Data
Kitchener Block Area
Showing Dip Angle and Fraser Filter Data
Scale 1:5000 Transmitting Station Seattle
For location see Figure 2b

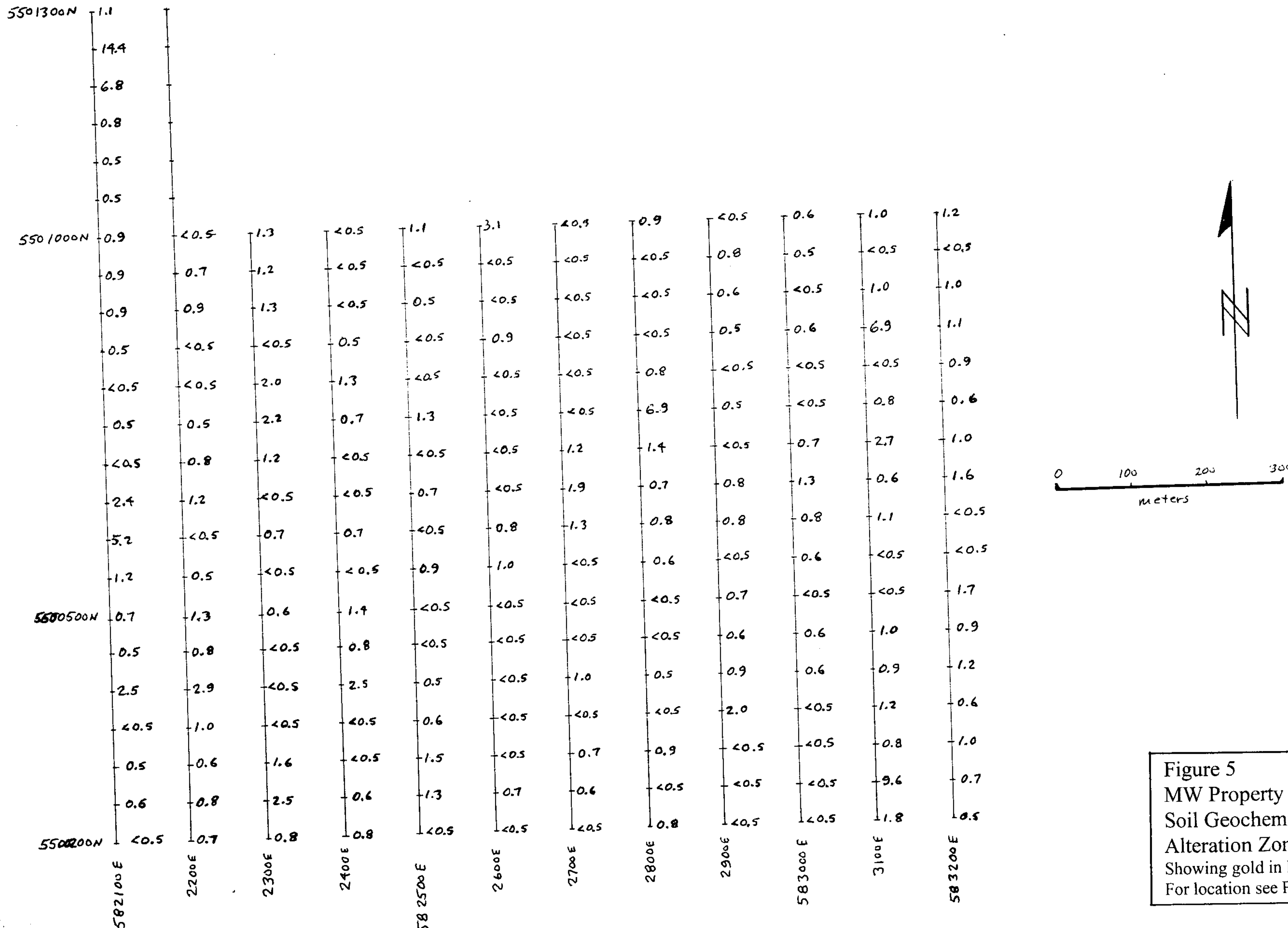

Figure 5
MW Property
Soil Geochemistry
Alteration Zone Area
Showing gold in PPB
For location see Figure 2b

4.20 Rock Geochemistry

The original prospecting done by C. Kennedy of Super Group Holdings Ltd. discovered significant widespread gold mineralization within very sparse bedrock exposure. The original rock sampling and geochemical analyses (samples MW 1 to 37) were completed before claims were staked. The data are included here for completeness although the costs associated with this work are not part of the assessment credit. A second phase of prospecting in the spring of 2003 expanded the original work somewhat, with continued favourable results. Rock samples collected during prospecting and subsequently from trenches were shipped to Acme Analytical Laboratories Ltd. at 852 East Hastings Street, Vancouver, B.C., and analyzed for a 30 element ICP package and geochemical gold by standard analytical techniques. Rock sample sites are shown on the geology maps (Figs. 3a & 3b) with complete geochemical analyses provided in Appendix 1 and sample descriptions in Appendix 3.

Anomalous gold is present in quartz and quartz-carbonate veins and with limonite breccias and in fault gouge. Much of the gold seen to date on the MW claims is associated with anomalous copper, lead, zinc and silver.

5.00 TRENCHING

Bedrock exposure on the MW claims is very limited yet only a thin layer of glacial overburden is present in some areas thus trenching was used to expose bedrock in selected places to better understand local geology and to expose gold-bearing structures.

Two phases of trenching were completed using a tracked excavator, with a total of 41 trenches dug in total. Trenches were mapped and sampled and were backfilled shortly thereafter. Most of the trenching was carried out in the area of the Alteration Zone and are shown in detail in Figure 6a. Other trenches are shown in Figures 3a, 3b and 6b. A total of 290 rock samples were collected during the trenching programs. Most of these are grab samples with some being chip samples. Samples were shipped to Acme Analytical Laboratories Ltd. at 852 East Hastings Street, Vancouver, B.C., and analyzed for a 30 element ICP package and geochemical gold by standard analytical techniques. Sample locations are shown on the various maps along with gold values in ppb; complete geochemical analyses are in Appendix 1 and sample descriptions are provided in Appendix 3.

Trenching demonstrated that considerable structural deformation is present across all of the area trenched. At the Alteration Zone, extensive brecciation of middle Aldridge Formation stratigraphy is associated with limonitic and manganese alteration as well as argillic alteration and silicification. The prominent structure appears to be ENE, striking at an azimuth of close to 060°. Within this strike orientation, tectonic cleavage, fracturing and quartz veining is mainly shallow to moderately SE dipping but there are also steep NW dips. There is also a fairly strong NW fabric developed across most of the area. This was apparent as well from surface mapping, with widespread NW striking quartz veins. Considerable structural fabric within the trenches of the Alteration Zone area is relatively flat lying, indicating the presence of sub-horizontal or thrust faulting. Strong manganese tends to be developed along near-vertical fracturing which is prominent in areas of more intense brecciation.

Weak gold mineralization was detected in most of the trenches. Gold is typically present in quartz veins of all orientations seen and is with limonite breccias developed in association with ENE fault zones. Considerable very thin quartz veining is commonly present in many of the breccia zones but these are not always very apparent because of the rubbly nature of much of the limonite-altered breccias.

Higher gold values were detected within a zone central to the large Alteration Zone, associated with a strong ENE striking, moderately SE dipping fault zone which carries pink hematite. Within this area, quartz veins of different attitudes and limonite breccia and fault gouge all contain significant gold. Scattered elevated gold values are also present elsewhere within the Alteration Zone area. Initially, trenching was directed to following higher gold numbers that had been established by prospecting. Because the Alteration Zone appears bounded by ENE trending VLF-EM anomalies that parallel the trend of the prominent structure and cross the attitude of bedding, trenching was also directed to evaluating the VLF-EM anomalies. Trench 38 crossed the northern of 3 ENE trending VLF-EM anomalies in the Alteration Zone area and established the presence of a strong, wide fault structure. Considerable oxidixed disseminated pyrite is associated with vuggy, irregularly developed quartz seams and masses within the fault structure. The entire fault structure could not be exposed by the trench as groundwater was encountered in the low portion of the old stream channel where the trench was located. Gold values were disappointingly low from this structure but the presence of some gold demonstrates this orientation of structure is important for the localization of gold in the MW claim area.

At the SE edge of the trenched area within the larger Alteration Zone area, another ENE fault was trenched at the locality of the middle ENE trending VLF-EM anomaly (Trench 40; Fig. 6a). Weak gold is also associated with this structure. At the south end of this trench an unusual massive, chloritic fault breccia, without any internal fabric, was encountered. Because no attitude was obtained on this feature, it's relationship to the overall geologic picture is unknown.

A second area of high gold values was encountered about 400 m NW of DDH K-14. Initial trenching was on an ENE striking quartz vein which returned values of about 300 ppb Au. Trenching of the quartz vein returned slightly higher gold values (Fig. 6b) but also exposed a swarm of quartz veins and quartz vein breccias with higher gold values and anomalous lead, copper, zinc and silver values. Much of the structure associated with the higher gold values is northerly striking but alteration is not strong, although some of the rocks are pervasively sericitically altered. A follow-up trench (37) dug during the second phase of trenching failed to expose any significant quartz veining, although rocks within this trench are also sericitically altered.

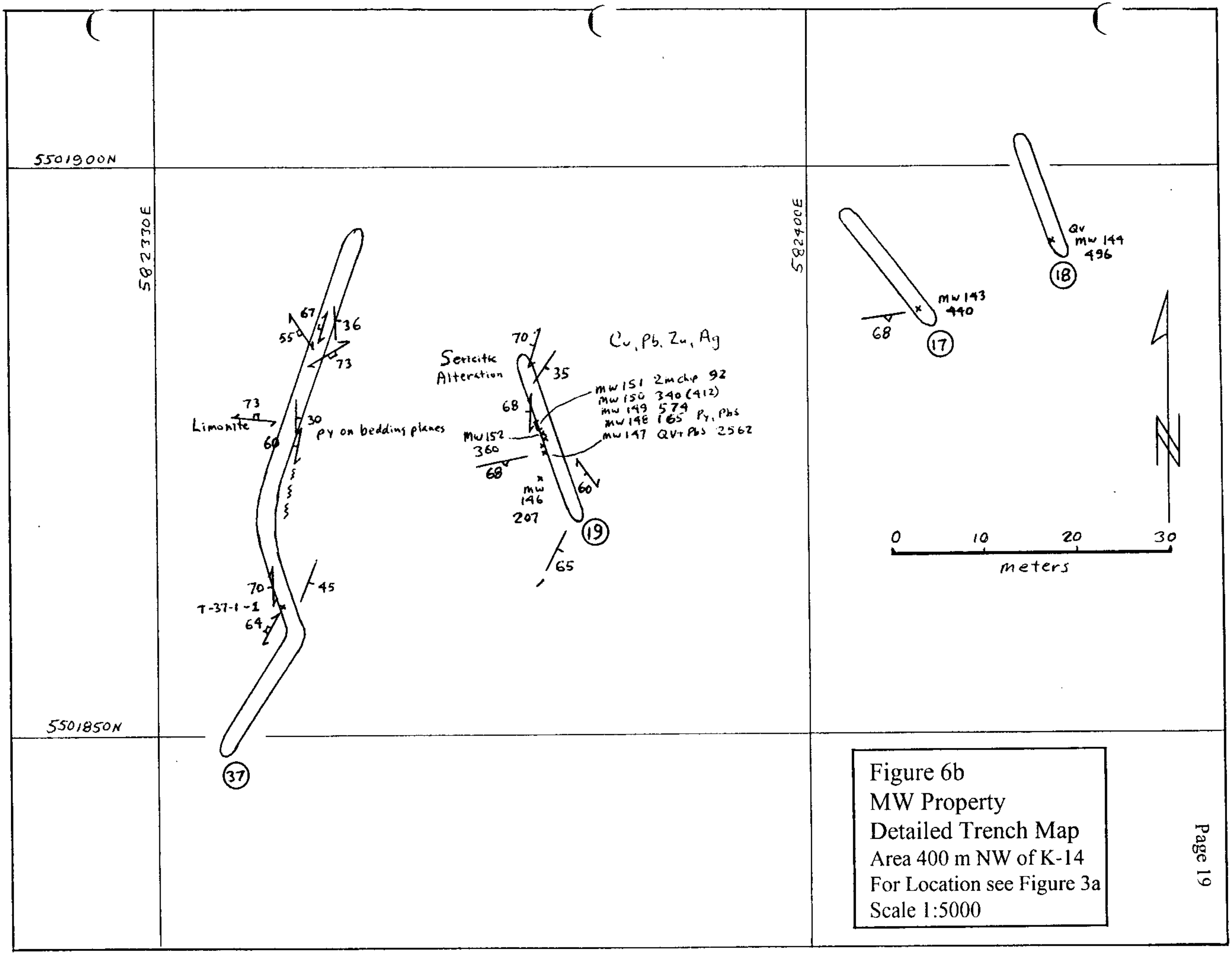

Figure 6b
MW Property
Detailed Trench Map
Area 400 m NW of K-14
For Location see Figure 3a
Scale 1:5000

Other trenches, such as at the Canyon area (Fig. 3b.) Exposed favourable fault structures but with little quartz veining and only low gold values. Limonite breccias are present and gold is associated with them but no high values were detected. Further east 3 trenches were attempted near an exposure of altered Creston Formation quartzites but overburden thickness prevented getting to bedrock except for one small exposure.

6.00 CONCLUSIONS

Widespread anomalous gold on the MW claims is structurally-controlled and associated with anomalous copper, lead, silver and zinc. Prominent structural controls are ENE and NW. Gold occurs within limonite breccias, fault gouge and quartz veins within these structures. Gold-bearing quartz veins which strike ENE dip shallowly, moderately and steeply SE and steeply to the NW. Northwest-striking quartz veins dip steeply to both NE and SW.

One concentration of gold mineralization which is central to the large Alteration Zone and associated with a pink hematite -bearing ENE fault warrants further evaluation by diamond drilling. Because of the complexity of gold-bearing structure, vertical holes are probably best suited for an initial drill program.

VLF-EM surveying detected numerous ENE to NE trending weak to moderate anomalies which generally cross bedding. Subsequent trenching established there is considerable tectonic structure parallel to the VLF-EM anomalies and trenching of specific VLF-EM anomalies established that the anomalies are fault structures, some of which carry anomalous gold. Because of the extensive overburden cover on the property, VLF-EM surveying is an effective method of identifying structures on the property which might host gold mineralization.

Soil geochemistry detected areas of anomalous gold but this method of exploration is probably not cost effective on the MW claims because of the extensive cover of glacial debris.

7.00 REFERENCES

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8.00 STATEMENT OF COSTS

Geologic mapping, VLF-EM surveying, trench supervision, mapping and sampling	
28 days @ $300/day	$8400.00
Truck 28 days @ $75.00/day	2100.00
VLF-EM rental 21 days @ $25/day	525.00
Trenching Phase 1 Quesnell	7285.00
Trenching Phase 2 Price	5922.50
Geochemical analyses 287 soils, 218 rocks	6606.66
Report 4 days @ $300/day	1200.00
Sub-total	$32039.16
15% Administration	4805.87
Total Expenditure	**$36,845.87**

9.00 AUTHOR'S QUALIFICATIONS

As author of this report I, Peter Klewchuk, certify that:

1. I am an independent consulting geologist with offices at 246 Moyie Street, Kimberley, B.C.
2. I am a graduate geologist with a B.Sc. degree (1969) from the University of British Columbia and an M.Sc. degree (1972) from the University of Calgary.
3. I am a Fellow of the Geological Association of Canada and a member of the Association of Professional Engineers and Geoscientists of British Columbia.
4. I have been actively involved in mining and exploration geology, primarily in the province of British Columbia, for the past 25 years.
5. I have been employed by major mining companies and provincial government geological departments.

Dated at Kimberley, British Columbia, this 25th day of February, 2004.

Peter Klewchuk, P. Geo.

PROFESSIONAL PROVINCE OF P. KLEWCHUK BRITISH COLUMBIA GEOSCIENTIST

Super Group Holdings Ltd. File # A205541 Page 1
1805 - 13th Ave South, Cranbrook BC V1C 5Y1 Submitted by: Craig Kennedy

SAMPLE#	Note	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
SI		<1	2	<3	4	<.3	2	<1	29	.09	5	<8	<2	<2	2	<.5	<3	<3	1	.07	.001	<1	2	.01	21	<.01	<3	.01	.33	<.01	<2	<.2
MW-01		1	6	5	13	<.3	7	3	299	.85	5	<8	<2	3	5	<.5	<3	3	4	.03	.014	24	13	.03	71	<.01	3	.20	.01	.16	4	79.5
MW-02	Altered	1	4	6	22	<.3	9	6	238	1.31	3	<8	<2	8	8	<.5	<3	5	3	.10	.041	22	6	.07	105	<.01	3	.52	.01	.33	2	417.0
MW-03	Creston	1	4	6	66	<.3	17	15	405	1.43	<2	<8	<2	12	6	<.5	<3	<3	6	.02	.018	50	12	.39	77	<.01	<3	.94	.01	.36	<2	19.9
MW-04	I.R.	2	8	<3	25	<.3	12	4	327	1.26	2	<8	<2	3	5	<.5	<3	4	4	.01	.047	18	16	.15	103	<.01	3	.43	.01	.19	9	2.3
MW-05	by	1	8	<3	30	<.3	15	6	725	1.68	7	<8	<2	<2	6	<.5	<3	<3	5	.03	.019	7	14	.04	102	<.01	<3	.21	.01	.11	5	1.8
MW-06		1	6	<3	21	<.3	10	5	957	1.91	<2	<8	<2	6	8	<.5	<3	3	3	.03	.020	30	10	.04	126	<.01	<3	.42	.01	.27	3	.9
MW-07		1	14	55	45	<.3	15	7	480	1.69	20	<8	<2	6	4	<.5	<3	<3	3	.02	.018	36	13	.03	89	.01	<3	.32	.01	.23	4	995.2
MW-08	UA Shear	3	21	22	225	1.1	34	12	662	8.41	44	<8	4	6	7	<.5	<3	4	4	.05	.057	10	6	.05	53	.01	4	.59	.02	.30	3	2159.7
MW-09	Dam	2	12	20	237	.4	36	12	504	8.01	41	<8	<2	4	6	.6	<3	<3	3	.03	.062	11	8	.04	37	<.01	4	.51	.02	.24	2	1540.3
MW-10	Pseudo	2	9	38	111	<.3	11	7	184	.83	9	<8	<2	3	23	.5	<3	5	1	.65	.026	10	15	.27	47	<.01	3	.23	.02	.20	9	21.7
MW-11	T° Shear	2	31	613	12	6.0	4	1	38	1.09	27	<8	10	<2	5	<.5	108	5	1	.01	.008	1	14	<.01	44	<.01	<3	.03	.01	.06	5	10660.0
MW-12		5	9	147	24	.5	5	1	128	.99	3	<8	<2	<2	6	<.5	5	<3	1	.02	.006	1	19	.01	40	<.01	<3	.09	.01	.09	12	1232.5
MW-13		2	222	187	94	25.8	12	7	813	1.99	12	<8	<2	8	94	.7	186	<3	66	1.34	.039	45	13	.69	56	<.01	<3	.31	<.01	.29	2	122.7
MW-14	45° Shear	2	79	16	34	<.3	18	7	134	4.09	37	<8	<2	7	11	<.5	<3	<3	8	.09	.052	14	19	.26	65	.01	<3	.60	.05	.31	7	<.2
MW-15	MA	6	30	179	94	2.5	16	8	345	2.33	26	<8	<2	6	23	.8	3	<3	15	.02	.031	17	15	.02	42	<.01	<3	.21	.01	.22	4	224.9
MW-16		1	11	<3	402	1.3	53	100	2976	10.64	42	<8	<2	9	17	1.4	5	<3	5	.07	.218	27	7	.05	320	.01	3	.55	.03	.33	5	11.4
MW-17		1	9	<3	276	.7	47	50	1999	10.12	77	<8	<2	8	9	1.5	<3	<3	6	.03	.136	38	7	.05	91	<.01	3	.49	.02	.35	3	9.2
MW-18		4	42	115	48	9.2	7	3	91	3.81	17	<8	<2	6	5	<.5	15	<3	9	.01	.030	22	11	.02	60	<.01	3	.44	.02	.30	5	344.1
MW-19		2	24	9	48	.3	17	6	149	2.29	8	<8	<2	5	5	<.5	<3	<3	3	.02	.020	25	13	.03	41	<.01	<3	.33	.02	.18	3	8.1
MW-20	Large	1	70	16	132	<.3	44	15	402	10.03	41	<8	<2	7	4	<.5	<3	<3	5	.01	.094	26	7	.02	72	<.01	<3	.53	.02	.32	<2	3.0
MW-21		2	67	437	71	40.5	3	2	127	1.17	13	<8	<2	6	3	<.5	27	3	4	<.01	.020	22	11	.02	46	<.01	<3	.35	.02	.25	3	311.6
MW-22	Alteration	2	10	26	35	3.9	13	17	285	3.24	30	<8	<2	10	5	<.5	<3	<3	6	.02	.023	33	7	.03	101	<.01	3	.52	.02	.38	2	24.6
MW-23		1	12	7	26	.3	6	3	133	4.65	25	<8	<2	10	26	<.5	<3	<3	10	.05	.046	79	14	.02	82	<.01	<3	.46	.06	.11	2	4.5
MW-24	Zone	3	24	7	64	<.3	30	18	133	4.71	19	<8	<2	4	5	<.5	4	<3	6	.04	.049	14	14	.02	30	<.01	<3	.28	.02	.12	8	116.0
RE MW-24	MA	2	24	6	62	<.3	29	17	124	4.62	17	<8	<2	4	5	<.5	3	<3	5	.04	.049	13	14	.02	28	<.01	3	.26	.01	.11	7	129.3
MW-25		1	33	13	148	.7	54	19	152	6.29	25	<8	<2	11	20	.7	7	<3	43	.26	.159	41	10	.06	114	<.01	4	.66	.02	.34	<2	1272.5
MW-26		2	11	3	34	.4	12	32	797	1.68	2	<8	<2	7	12	<.5	<3	<3	3	.07	.057	30	11	.01	125	<.01	<3	.36	.04	.15	5	19.4
MW-27		2	14	8	24	1.1	7	2	70	1.53	26	<8	<2	5	7	<.5	<3	3	6	.02	.013	20	11	.02	60	<.01	4	.35	.02	.19	4	255.8
MW-28		9	19	11	14	3.2	5	2	115	2.51	18	<8	<2	6	7	<.5	3	<3	10	.01	.013	26	18	.01	45	<.01	<3	.18	<.01	.11	10	465.1
MW-29		1	13	4	17	<.3	9	5	80	1.57	<2	<8	<2	9	11	<.5	<3	<3	7	.05	.031	38	11	.07	131	<.01	3	1.05	.03	.61	<2	30.9
MW-30		1	10	3	34	<.3	9	8	316	1.79	4	<8	<2	7	8	<.5	<3	<3	2	.05	.035	27	8	.02	79	<.01	<3	.36	.03	.18	4	4.8
MW-31		8	68	21	26	<.3	8	4	110	4.44	7	<8	<2	10	12	<.5	3	<3	17	.08	.078	43	22	.69	72	.02	<3	1.29	.01	.51	<2	3.8
MW-32		3	11	13	145	<.3	57	14	1347	15.33	10	<8	<2	6	12	<.5	<3	4	2	.06	.186	22	7	.04	182	<.01	<3	.42	.03	.19	<2	5.0
MW-33		5	137	719	53	>200	3	1	40	2.10	30	<8	<2	4	6	<.5	67	3	7	.01	.020	16	12	.01	47	<.01	<3	.26	.01	.17	4	1349.1
MW-34		1	65	607	56	4.5	3	1	48	1.50	11	<8	<2	6	8	<.5	10	<3	5	.02	.026	24	7	.02	53	<.01	3	.34	.03	.19	3	710.1
MW-35		2	30	55	112	2.1	21	4	108	5.65	20	<8	<2	5	6	<.5	11	<3	7	.04	.079	28	11	.02	37	<.01	3	.31	.02	.13	3	154.9
MW-36		<1	19	37	80	.3	47	6	205	11.72	19	<8	<2	8	8	<.5	<3	6	5	.01	.054	30	6	.03	66	<.01	<3	.53	.04	.31	2	10.8
MW-37		<1	26	3	33	<.3	19	14	964	3.51	9	<8	<2	8	5	<.5	<3	<3	6	.01	.020	37	6	.03	118	<.01	3	.42	.02	.30	<2	.5
STANDARD DS4/AU-R		7	120	32	158	.5	33	12	792	3.16	23	11	<2	4	27	5.0	5	6	75	.52	.091	16	165	.58	147	.09	3	1.74	.04	.16	4	456.4

Sample type: ROCK R150 60C.

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Hastings Management Corp. File # A302125 Page 1
711 - 675 W. Hastings St., Vancouver BC V6B 1N2 Submitted by: Craig Kennedy

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
SI	<1	<1	<3	<1	<.3	<1	<1	<2	.01	2	<8	<2	<2	2	<.5	<3	<3	<1	.07	<.001	<1	<1	.01	2	<.01	<3	<.01	.39	.01	<2	<.2
MW-50	<1	73	10	185	.3	327	49	2300	7.78	66	<8	<2	<2	182	.7	<3	3	191	4.14	.133	17	606	4.52	106	.01	<3	3.83	.02	.09	3	3.4
MW-51	1	45	10	94	8.7	15	4	54	4.55	20	<8	<2	10	4	<.5	6	<3	4	.03	.034	37	10	.05	41	<.01	6	.50	.01	.30	2	3.5
MW-52	4	10	9	29	<.3	12	3	188	1.41	10	<8	<2	4	14	<.5	<3	<3	3	.05	.027	18	26	.07	75	<.01	3	.46	.02	.21	7	1.6
MW-53	1	38	16	15	<.3	6	3	131	1.72	13	8	<2	<2	3	<.5	<3	<3	3	.01	.011	6	2	.11	22	<.01	4	.22	.01	.07	<2	3.4
MW-54	5	11	<3	63	<.3	10	2	294	1.62	7	<8	<2	<2	3	<.5	<3	<3	1	.03	.021	4	21	.01	29	<.01	<3	.12	<.01	.05	11	1.2
MW-55	1	18	15	11	.8	8	5	28	1.78	13	<8	<2	<2	8	<.5	3	<3	1	.01	.023	12	4	.01	30	<.01	4	.19	.02	.07	<2	21.5
MW-56	3	8	17	43	<.3	24	7	934	5.11	13	<8	<2	7	8	<.5	<3	3	2	.03	.017	30	15	.27	96	<.01	3	.79	.03	.30	2	1.6
MW-57	<1	9	10	32	<.3	5	3	504	1.20	2	<8	<2	<2	64	<.5	<3	<3	<1	1.62	.009	6	4	.69	22	<.01	<3	.09	.02	.05	<2	2.0
MW-58	6	37	359	224	5.0	38	19	561	4.70	48	<8	<2	5	9	1.4	3	<3	18	.06	.051	24	19	.04	64	<.01	5	.35	.01	.29	3	687.2
MW-59	2	16	45	177	3.2	33	15	553	2.93	31	<8	<2	5	5	2.1	3	<3	15	.05	.036	26	7	.03	59	<.01	3	.31	.01	.24	3	260.6
MW-60	1	46	86	518	.4	27	17	436	3.85	27	<8	<2	8	7	1.4	<3	<3	5	.11	.044	25	15	.15	84	<.01	4	.55	.02	.33	3	11.7
MW-61	1	58	12	477	2.0	9	7	401	2.13	10	<8	<2	10	6	2.1	<3	<3	5	.03	.022	26	3	.02	47	<.01	<3	.32	.02	.08	<2	27.1
MW-62	4	4	7	123	1.1	5	2	163	1.06	7	<8	<2	7	4	<.5	<3	<3	6	.03	.025	24	17	.02	58	<.01	<3	.22	.01	.16	8	11.6
MW-63	1	22	32	14	<.3	3	1	69	1.45	6	<8	<2	<2	3	<.5	<3	<3	1	.01	.016	1	1	<.01	10	<.01	<3	.04	.01	<.01	<2	6.7
MW-64	4	36	34	181	<.3	10	5	363	3.63	5	<8	<2	7	6	<.5	<3	<3	16	.04	.043	21	26	1.19	71	.04	<3	1.40	.01	.62	3	1.2
MW-65	1	18	12	21	<.3	5	2	65	1.39	25	<8	<2	10	4	<.5	<3	<3	6	.03	.027	31	8	.13	43	<.01	<3	.57	.05	.16	<2	1.0
MW-66	7	7	22	3	37.8	3	<1	43	.91	22	<8	<2	<2	3	<.5	49	<3	3	.01	.004	5	25	.01	60	.01	<3	.09	.01	.16	10	378.7
MW-67	2	374	1387	88	67.5	3	1	26	1.87	38	<8	<2	6	27	.9	391	<3	4	.01	.036	30	3	.03	126	<.01	<3	.31	.02	.41	<2	298.4
MW-68	6	131	365	62	49.3	5	1	65	1.52	27	<8	<2	2	22	<.5	194	<3	2	.01	.016	11	29	.01	117	<.01	<3	.17	.01	.16	9	669.6
MW-69	2	66	833	67	137.3	1	<1	10	1.81	44	<8	15	3	37	<.5	278	<3	3	<.01	.022	21	2	.01	141	<.01	<3	.07	.03	.28	<2	16570.6
RE MW-69	2	67	845	67	139.1	1	<1	11	1.83	43	<8	21	4	38	<.5	283	<3	2	<.01	.023	21	2	.01	143	<.01	<3	.08	.02	.24	<2	18463.6
MW-70	6	116	627	81	26.3	3	1	47	2.01	23	<8	<2	3	11	<.5	133	<3	4	.01	.014	11	27	.01	87	<.01	<3	.16	.02	.18	6	240.3
MW-71	1	12	63	23	2.9	2	1	45	.77	4	<8	<2	4	6	<.5	8	<3	11	.01	.016	21	3	.02	76	.01	<3	.21	<.01	.18	<2	192.0
STANDARD DS4/AU-R	7	128	30	160	<.3	34	12	797	3.20	24	<8	<2	4	28	5.4	6	5	75	.52	.091	17	165	.57	148	.08	<3	1.81	.04	.14	4	462.9

Sample type: ROCK R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK R150 60C AU* IGNITED, ACID LEACHED, ANALYZED BY ICP-MS. (15 gm)
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUN 19 2003 DATE REPORT MAILED: July 2/03 SIGNED BY. D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data FA

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

<u>Sedex Mining Corp.</u> File # A304772 Page 1
711 - 675 W. Hastings St., Vancouver BC V6B 1N2 Submitted by: Peter Klewchuk

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
SI	<1	1	<3	1	<.3	<1	<1	2	.07	<2	<8	<2	<2	3	<.5	<3	<3	<1	.10	<.001	<1	1	<.01	1	<.01	<3	.01	.53	.01	<2	<.2
MW-101	2	43	47	19	.8	8	4	68	1.83	272	<8	<2	10	8	<.5	5	3	4	.01	.014	28	9	.05	63	<.01	<3	.25	.02	.16	<2	65.4
MW-102	8	64	38	64	.5	33	17	1298	5.62	18	<8	<2	15	10	<.5	4	3	9	.24	.045	31	12	.79	52	<.01	<3	1.22	.02	.16	<2	2.0
MW-103	9	64	563	326	5.7	25	14	1012	4.72	43	<8	<2	15	19	3.3	3	<3	22	.14	.042	51	6	.09	54	<.01	<3	.36	<.01	.21	<2	452.0
MW-104	3	14	7	14	.3	19	5	919	2.95	5	<8	<2	12	9	<.5	<3	<3	5	.11	.048	35	4	.06	53	.01	<3	.32	.01	.25	2	3.9
MW-105	2	51	18	13	.4	44	35	908	4.12	19	<8	<2	14	10	<.5	<3	<3	4	.58	.051	22	4	.08	54	<.01	<3	.31	.01	.24	<2	8.1
MW-106	<1	32	408	78	.7	11	5	103	2.68	7	<8	<2	14	9	<.5	<3	<3	4	.10	.040	35	2	.03	38	<.01	<3	.24	<.01	.19	2	71.9
MW-107	<1	16	22	31	.6	5	4	56	1.53	4	<8	<2	9	3	<.5	<3	<3	2	.02	.011	29	2	.02	27	<.01	<3	.20	<.01	.14	<2	19.6
MW-108	1	29	10	198	.5	20	17	415	8.76	2	<8	<2	12	5	<.5	<3	<3	3	.02	.086	27	3	.02	39	<.01	<3	.19	.01	.12	<2	49.4
MW-109	<1	16	27	53	.7	13	30	421	2.59	2	<8	<2	13	6	<.5	3	<3	3	.15	.029	27	3	.06	48	<.01	<3	.51	<.01	.11	2	19.0
MW-110	1	15	9	68	.3	15	18	388	2.74	<2	<8	<2	11	4	1.8	<3	<3	2	.10	.076	28	5	.02	45	<.01	<3	.21	<.01	.17	2	1.0
MW-111	<1	53	20	86	1.6	3	1	36	6.36	27	<8	2	19	12	<.5	6	<3	19	.04	.042	40	5	.02	53	<.01	<3	.30	.01	.19	<2	2436.8
MW-112	1	52	118	45	4.2	2	<1	24	4.47	16	<8	<2	7	4	<.5	7	3	8	.02	.015	24	5	.02	25	<.01	<3	.22	.01	.13	<2	367.8
MW-113	1	101	9	103	<.3	47	20	79	6.84	13	<8	<2	13	5	<.5	<3	<3	6	.06	.054	38	4	.05	41	<.01	<3	.31	.01	.18	<2	19.0
MW-114	<1	34	7	43	<.3	18	13	177	3.03	10	<8	<2	6	6	<.5	<3	<3	2	.07	.007	18	3	.06	47	<.01	<3	.47	.01	.06	<2	5.9
MW-115	2	26	26	9	.8	2	1	16	1.10	4	<8	<2	11	4	<.5	5	<3	4	.02	.006	30	3	.02	35	<.01	<3	.21	.01	.17	<2	29.6
MW-116	2	36	101	19	1.3	6	4	31	.83	<2	<8	<2	7	5	<.5	<3	<3	5	.06	.012	39	4	.04	26	<.01	<3	.24	<.01	.03	<2	45.8
MW-117	1	14	3	66	<.3	21	1	349	8.36	17	<8	<2	8	9	<.5	5	<3	3	.12	.092	19	4	.06	44	<.01	<3	.18	.01	.07	<2	2.7
MW-118	<1	59	<3	285	7.3	80	254	>9999	5.78	45	<8	<2	11	61	2.0	4	<3	5	.31	.040	18	4	.15	150	<.01	<3	.34	.03	.11	<2	1.9
RE MW-118	<1	59	4	281	7.2	79	250	>9999	5.72	45	<8	<2	11	61	2.1	5	4	4	.30	.040	18	4	.15	149	<.01	<3	.34	.03	.11	<2	3.1
MW-119	6	113	10	195	.4	93	46	687	15.16	63	<8	<2	13	34	<.5	3	<3	11	.52	.224	52	11	.16	90	<.01	<3	.46	.02	.07	<2	2.0
MW-120	<1	118	468	74	41.7	5	5	454	1.72	9	<8	3	2	6	<.5	49	<3	2	.06	.027	2	5	.02	26	<.01	<3	.11	.01	.03	<2	1636.7
MW-121	1	202	1620	169	10.2	8	25	5349	2.04	11	<8	<2	<2	11	.8	6	<3	2	.09	.029	2	5	.03	130	<.01	<3	.11	.01	.02	<2	163.6
MW-122	1	85	349	280	1.7	40	50	3230	8.92	<2	<8	<2	13	11	<.5	4	<3	4	.37	.023	43	5	.12	2329	<.01	<3	.39	.01	.17	<2	56.2
MW-123	2	181	187	513	2.3	15	9	253	11.47	74	<8	4	21	12	<.5	9	4	26	.13	.084	41	17	.17	113	<.01	<3	.67	.01	.21	<2	3624.9
MW-124	<1	56	97	95	2.0	5	<1	75	8.60	17	<8	<2	14	8	<.5	5	<3	20	.04	.053	37	4	.02	42	<.01	<3	.30	.01	.17	<2	569.6
MW-125	<1	29	4	55	<.3	21	10	157	3.92	24	<8	<2	4	5	<.5	3	3	4	.05	.040	10	6	.02	21	<.01	<3	.16	<.01	.05	2	28.7
MW-126	<1	20	8	43	.4	14	4	137	2.81	12	<8	<2	4	4	<.5	<3	<3	4	.02	.015	8	4	.02	21	<.01	<3	.20	.01	.09	<2	166.2
MW-127	<1	31	42	69	.7	36	30	523	4.67	14	<8	<2	13	9	<.5	<3	<3	7	.13	.038	42	6	.09	124	<.01	<3	.48	.02	.16	<2	276.1
MW-128	1	7	6	21	.6	10	5	122	1.24	5	<8	<2	5	3	<.5	<3	<3	3	.02	.008	15	7	.02	19	<.01	<3	.13	.02	.06	<2	12.2
MW-129	1	20	6	59	.8	27	6	257	4.46	12	<8	<2	5	22	<.5	<3	<3	11	.40	.114	24	9	.07	97	<.01	3	.46	.01	.12	<2	1037.6
MW-130	2	29	5	117	.4	60	19	1312	8.57	45	<8	<2	2	17	<.5	<3	<3	9	.34	.170	13	8	.08	81	<.01	<3	.20	.01	.04	<2	255.7
MW-131	3	47	84	81	2.4	46	26	2923	7.50	38	<8	<2	12	19	<.5	<3	<3	12	.21	.061	43	18	.10	122	<.01	<3	.37	.01	.15	<2	1234.4
MW-132	<1	47	<3	66	<.3	28	9	387	3.75	14	<8	<2	11	9	<.5	<3	<3	3	.12	.027	32	4	.06	46	<.01	<3	.31	.02	.10	<2	10.0
MW-133	1	58	<3	37	.4	23	7	234	10.04	10	<8	<2	5	5	<.5	<3	<3	4	.05	.046	16	9	.02	26	<.01	<3	.17	.01	.04	<2	38.0
STANDARD DS5/AU-R	12	142	24	132	.3	25	12	745	2.93	18	<8	<2	3	47	5.3	4	7	59	.72	.092	12	188	.66	137	.09	17	2.06	.03	.13	4	466.5

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK R150 60C AU* IGNITED, ACID LEACHED, ANALYZED BY ICP-MS. (15 gm)
<u>Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.</u>

DATE RECEIVED: OCT 3 2003 DATE REPORT MAILED: Oct 20/2003 SIGNED BY ....D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

 Data A FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
MW-134	<1	47	72	331	<.3	6	4	48	3.69	35	<8	<2	22	13	<.5	3	6	7	.02	.055	57	4	.02	57	<.01	<3	.30	.02	.19	4	17.6
MW-135	3	22	216	42	3.9	3	1	41	3.54	21	<8	<2	10	11	<.5	3	<3	10	.04	.019	33	4	.07	73	<.01	<3	.33	.05	.27	<2	149.0
MW-136	2	26	48	37	1.2	4	1	33	6.56	41	<8	<2	9	13	<.5	<3	<3	12	.04	.028	16	4	.03	91	<.01	<3	.20	.07	.21	2	207.3
MW-137	20	23	86	12	2.9	2	<1	16	2.73	23	<8	<2	7	6	<.5	24	4	17	.02	.010	34	7	.01	20	<.01	<3	.12	.01	.06	<2	526.8
MW-138	2	28	103	23	5.4	3	<1	14	5.35	20	<8	<2	8	14	<.5	6	4	15	.14	.017	20	5	.03	78	<.01	<3	.24	.10	.21	<2	793.2
MW-139	3	48	22	24	2.8	9	1	152	2.99	18	<8	<2	12	6	<.5	<3	<3	4	.11	.009	39	5	.09	37	<.01	<3	.47	.01	.15	<2	8.9
MW-140	<1	32	90	9	1.1	2	1	14	.67	7	<8	<2	<2	1	<.5	23	<3	<1	<.01	.002	1	6	<.01	9	<.01	<3	.02	.01	.01	<2	1890.8
MW-141	3	835	256	655	24.6	37	17	1341	2.61	21	<8	<2	<2	36	4.8	91	<3	12	.02	.024	6	9	.04	158	<.01	<3	.27	.01	.03	5	629.2
MW-142	1	52	43	82	1.7	28	14	684	4.53	18	<8	<2	13	9	<.5	10	<3	13	.20	.036	38	9	.43	78	<.01	<3	1.05	.01	.25	<2	48.0
MW-143	1	12	10	9	3.7	2	1	34	.77	31	<8	<2	6	4	<.5	<3	<3	6	.08	.004	18	11	.01	36	<.01	<3	.12	.01	.12	<2	440.1
MW-144	6	10	148	37	5.4	<1	<1	21	.70	15	<8	<2	4	5	<.5	6	<3	4	<.01	.005	13	8	.01	51	<.01	<3	.08	.01	.15	<2	495.7
MW-145	2	63	99	828	<.3	28	11	735	3.01	6	<8	<2	9	5	7.7	21	<3	7	.12	.048	31	10	.15	56	<.01	<3	.47	.02	.25	<2	18.1
MW-146	3	182	72	47	8.0	8	4	79	3.15	20	<8	<2	7	11	<.5	94	<3	4	.01	.022	33	7	.02	68	<.01	<3	.16	.01	.15	<2	207.2
MW-147	4	2516	>9999	535	190.9	2	<1	28	3.89	479	<8	4	<2	45	41.9	>2000	18	3	<.01	.017	12	4	<.01	60	<.01	<3	.07	.01	.14	<2	2561.6
MW-148	1	146	1945	109	26.9	2	1	41	.65	14	<8	<2	<2	8	1.0	96	<3	1	.02	.004	2	7	.01	24	<.01	<3	.03	.01	.02	<2	165.0
MW-149	2	387	1950	552	132.0	4	1	45	1.89	38	<8	<2	6	22	5.3	563	<3	5	.01	.027	21	7	.02	57	<.01	<3	.16	.01	.15	7	573.5
MW-150	1	370	1815	577	46.3	2	1	24	1.86	25	<8	<2	6	41	5.7	258	<3	4	.01	.026	17	6	.01	100	<.01	<3	.13	.01	.14	7	340.1
RE MW-150	2	368	1838	580	45.0	2	1	21	1.88	24	<8	<2	6	42	5.6	258	<3	3	.01	.027	19	7	.01	102	<.01	<3	.13	.01	.15	6	412.1
MW-151	1	57	232	116	3.2	5	2	142	2.14	9	<8	<2	8	16	<.5	21	<3	5	.57	.031	26	9	.17	55	<.01	<3	.38	.02	.16	4	91.6
MW-152	1	641	5690	5657	31.9	2	1	70	.97	13	<8	<2	<2	21	66.1	179	3	1	.11	.019	4	3	.04	40	<.01	<3	.04	.01	.04	5	359.8
MW-153	1	7	52	35	<.3	28	15	372	2.44	4	<8	<2	24	16	<.5	<3	<3	4	.09	.028	69	8	.22	73	<.01	<3	.57	.01	.20	<2	14.4
MW-154	1	11	41	57	<.3	18	15	678	3.10	26	<8	<2	13	11	<.5	3	3	18	.04	.020	57	6	.09	98	<.01	<3	.39	.01	.19	<2	9.2
MW-155	<1	3	27	15	.4	9	6	278	1.21	4	<8	<2	9	5	<.5	<3	<3	4	.05	.006	29	7	.03	39	<.01	<3	.40	.01	.12	<2	2.5
MW-156	<1	3	10	14	.3	3	2	668	.74	2	<8	<2	<2	2	<.5	<3	<3	1	.01	.014	2	7	.01	76	<.01	<3	.05	.01	.02	<2	.5
MW-157	<1	28	40	38	.5	31	14	194	1.25	15	<8	<2	7	11	<.5	<3	<3	3	.49	.010	30	6	.05	51	<.01	<3	.41	.03	.16	2	31.4
MW-158	1	21	10	19	<.3	5	4	564	.87	4	<8	<2	<2	2	<.5	<3	<3	1	.02	.004	9	8	.01	52	<.01	<3	.06	<.01	.04	<2	1.0
MW-159	1	3	45	5	.6	3	1	51	.40	<2	<8	<2	<2	1	<.5	3	<3	<1	.01	.002	2	11	<.01	9	<.01	<3	.04	.01	.02	<2	2.0
MW-160	<1	3	8	20	<.3	2	2	110	1.10	2	<8	<2	<2	<1	<.5	<3	<3	1	<.01	.017	2	7	<.01	6	<.01	<3	.02	.01	.02	<2	<.2
MW-161	1	9	22	8	.3	2	1	240	.53	<2	<8	<2	<2	1	<.5	<3	<3	1	.04	.003	1	9	<.01	21	<.01	<3	.01	.01	<.01	<2	.9
STANDARD DS5/AU-R	12	142	25	132	.4	24	12	759	3.01	17	<8	<2	4	48	5.4	5	7	58	.72	.094	12	188	.67	139	.09	18	2.11	.04	.14	4	465.9

Sample type: ROCK R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Sedex Mining Corp. PROJECT MW File # A306161 Page 1
711 - 675 W. Hastings St., Vancouver BC V6B 1N2 Submitted by: Peter Klewchuk

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
SI	<1	2	<3	3	<.3	<1	<1	4	.04	<2	<8	<2	<2	4	<.5	<3	<3	<1	.14	<.001	<1	1	.01	4	<.01	<3	.01	.60	.01	<2	<.2
T30-01	3	274	245	881	1.9	77	43	1464	23.47	189	<8	<2	7	14	.9	17	<3	10	.20	.372	13	5	.09	334	.01	<3	.60	.02	.17	<2	6.5
T30-02	1	42	21	99	.3	23	12	437	3.34	16	<8	<2	7	8	<.5	<3	<3	5	.05	.048	32	4	.04	73	.01	<3	.44	.03	.24	<2	3.7
T30-03	1	38	25	86	.5	25	14	302	3.65	19	<8	<2	6	9	<.5	<3	<3	4	.07	.035	43	5	.05	76	.01	<3	.43	.03	.23	<2	2.1
T30-04	1	33	16	101	1.4	27	21	1398	3.71	15	<8	<2	8	11	<.5	<3	<3	4	.07	.034	37	3	.05	137	<.01	<3	.45	.03	.26	<2	2.4
T30-05	1	39	5	147	2.4	38	53	2643	5.31	23	<8	<2	10	10	.6	3	<3	3	.05	.060	28	6	.04	76	<.01	<3	.42	.02	.26	<2	7.4
T30-06	1	32	<3	45	3.2	22	34	3278	2.43	10	<8	<2	5	8	.5	<3	<3	5	.06	.014	20	4	.05	58	<.01	<3	.32	.01	.18	<2	78.5
T30-07	2	37	<3	280	3.1	54	77	3745	11.81	43	<8	<2	9	11	1.1	<3	<3	3	.05	.186	48	5	.04	88	<.01	<3	.46	.02	.28	<2	8.8
T30-08	1	22	3	114	<.3	38	26	764	5.22	13	<8	<2	9	7	<.5	<3	3	5	.03	.057	32	4	.03	72	.01	<3	.48	.02	.28	<2	13.7
T30-09	1	20	8	116	<.3	31	12	161	4.56	11	<8	<2	9	6	<.5	<3	<3	6	.03	.047	31	5	.03	52	.01	<3	.46	.02	.27	<2	70.1
T30-10	3	31	7	231	<.3	52	13	114	7.97	26	<8	<2	9	6	<.5	4	<3	6	.01	.127	42	5	.03	52	<.01	<3	.51	.02	.28	<2	7.1
T30-11	1	22	53	144	.4	32	13	261	4.50	12	<8	<2	9	11	<.5	<3	<3	10	.08	.053	47	6	.07	86	<.01	<3	.63	.02	.29	<2	231.9
T30-12	2	33	74	172	<.3	29	15	142	5.65	13	<8	<2	9	9	<.5	4	<3	11	.06	.063	29	4	.04	65	<.01	<3	.58	.02	.27	<2	648.8
T30-13	2	46	22	153	<.3	37	10	86	8.20	18	9	<2	11	7	<.5	11	<3	7	.04	.079	49	6	.03	65	.01	<3	.54	.02	.27	<2	193.2
T30-14	1	18	43	127	<.3	24	5	88	4.78	18	<8	<2	10	8	<.5	4	<3	11	.04	.057	35	4	.03	64	<.01	<3	.49	.02	.28	<2	439.3
T30-15	2	90	15	212	.4	45	19	311	9.19	54	<8	3	12	7	<.5	4	<3	30	.04	.059	24	7	.04	60	<.01	<3	.48	.02	.25	<2	2351.7
T30-16	2	59	5	160	.8	29	18	1183	6.31	26	<8	<2	9	12	.8	3	<3	8	.04	.072	33	4	.06	109	.01	<3	.51	.02	.28	<2	104.9
T30-17	3	28	4	21	.3	5	4	82	2.21	9	<8	<2	9	9	<.5	<3	<3	5	.02	.014	23	9	.02	98	.01	<3	.42	.03	.21	2	14.4
RE T30-17	3	27	4	19	<.3	4	4	81	2.11	9	<8	<2	9	9	<.5	3	<3	4	.02	.013	22	8	.02	96	<.01	<3	.39	.03	.20	2	12.2
T31-01	<1	15	4	13	.4	3	1	33	.75	2	<8	<2	9	10	<.5	<3	<3	3	.08	.006	34	4	.03	42	<.01	<3	.39	.03	.21	<2	63.1
T31-02	2	15	3	30	.3	6	2	156	1.38	4	<8	<2	2	8	<.5	<3	<3	1	.22	.011	9	20	.06	30	.01	<3	.22	.02	.09	6	9.8
T31-03	<1	18	5	19	<.3	4	2	137	.65	2	8	<2	5	10	<.5	<3	<3	2	.10	.012	82	4	.03	32	.01	<3	.41	.03	.18	<2	9.5
T31-04	1	34	8	100	1.1	5	1	64	3.84	8	<8	<2	8	7	<.5	4	<3	3	.13	.025	29	7	.03	42	.01	<3	.39	.02	.19	<2	154.0
T31-05	1	8	3	15	<.3	2	1	114	1.03	2	<8	<2	8	5	<.5	<3	<3	3	.03	.016	39	3	.03	52	<.01	<3	.42	.02	.26	<2	106.8
T31-06	5	28	5	20	1.7	4	1	73	3.44	15	<8	<2	8	12	<.5	4	<3	25	.05	.036	26	16	.04	44	<.01	<3	.35	.01	.14	5	149.6
T31-07	3	22	15	191	1.3	24	10	420	14.51	37	<8	<2	10	9	<.5	10	<3	14	.07	.131	21	5	.05	72	<.01	<3	.62	.01	.12	<2	318.2
T31-08	3	44	5	25	1.3	6	3	91	4.29	11	<8	<2	10	8	<.5	<3	<3	9	.03	.023	43	9	.03	53	<.01	<3	.46	.02	.27	<2	77.7
T31-09	3	80	218	34	5.6	1	<1	13	6.68	28	<8	<2	6	19	<.5	33	<3	29	.04	.013	11	5	.04	50	.01	<3	.33	.02	.18	<2	503.2
T31-10	5	64	116	71	3.3	5	<1	36	7.96	20	<8	<2	9	10	<.5	9	<3	30	.06	.031	35	11	.04	53	.01	<3	.35	.02	.18	2	573.0
T31-11	<1	5	6	47	<.3	10	6	405	4.44	8	<8	<2	7	17	<.5	<3	<3	3	.16	.070	27	4	.04	65	<.01	<3	.34	.02	.19	<2	5.8
T31-12	3	34	44	205	1.2	33	14	240	13.40	24	<8	<2	10	8	<.5	8	<3	16	.05	.122	26	7	.04	60	<.01	<3	.49	.02	.20	<2	150.3
T31-13	<1	28	16	24	.7	2	2	9	1.89	7	<8	<2	8	11	<.5	<3	<3	4	.01	.016	56	5	.02	84	<.01	<3	.49	.02	.31	<2	13.5
T32-01	1	55	55	92	.5	28	17	251	4.07	24	11	<2	9	10	<.5	13	<3	4	.15	.020	68	8	.10	92	<.01	<3	.56	.02	.25	<2	11.7
T32-02	1	33	462	333	.8	15	8	741	2.55	7	<8	<2	4	8	<.5	10	<3	5	.08	.016	15	4	.07	55	<.01	<3	.22	.02	.08	<2	20.0
T32-03	6	634	1296	1283	85.2	26	10	240	7.62	59	<8	4	7	10	1.2	190	<3	12	.14	.046	18	13	.07	87	<.01	<3	.52	.02	.17	<2	3652.8
STANDARD DS5/AU-R	12	145	23	128	<.3	23	11	762	2.85	18	<8	<2	3	45	5.6	3	5	57	.68	.089	11	178	.64	137	.08	16	1.94	.03	.13	5	471.1

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK R150 60C AU* IGNITED, ACID LEACHED, ANALYZED BY ICP-MS. (15 gm)
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: DEC 15 2003 DATE REPORT MAILED: Dec 31/03 SIGNED BY C.L. D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

 Data / FA

ACME ANALYTICAL

Sedex Mining Corp. PROJECT MW FILE # A306161

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
T32-04	2	40	18	96	.6	39	11	500	7.98	<2	<8	<2	8	9	.7	3	<3	3	.07	.051	29	5	.06	89	<.01	<3	.48	.04	.23	<2	19.3
T32-05	2	82	61	344	.9	31	10	973	3.30	5	<8	<2	<2	6	<.5	4	<3	4	.14	.011	6	11	.06	76	<.01	<3	.25	.01	.03	3	17.2
T32-06	1	44	22	100	<.3	18	7	1016	2.54	5	<8	<2	7	7	<.5	<3	<3	3	.09	.014	21	5	.05	108	<.01	<3	.49	.02	.12	<2	5.0
T32-07	1	32	20	88	<.3	13	6	491	1.58	2	<8	<2	7	8	<.5	3	<3	2	.05	.010	44	7	.03	72	<.01	3	.42	.04	.20	2	2.6
T32-08	1	15	13	51	.4	17	9	1607	2.73	12	<8	<2	<2	4	<.5	3	<3	5	.04	.014	5	7	.03	103	<.01	<3	.10	.01	.02	2	7.6
T32-09	1	57	71	96	.4	24	10	914	2.21	6	<8	<2	11	9	<.5	<3	<3	5	.15	.009	35	11	.08	121	<.01	<3	.54	.03	.16	2	13.5
T32-10	1	24	33	85	<.3	25	17	881	2.46	8	<8	<2	7	8	<.5	<3	<3	4	.06	.013	45	6	.05	99	<.01	3	.40	.03	.16	<2	8.9
T32-11	1	99	403	465	.7	12	7	107	1.76	5	<8	<2	5	8	<.5	14	<3	3	.05	.014	76	7	.05	56	<.01	3	.41	.03	.20	<2	6.5
T32-12	1	19	928	253	1.2	7	5	95	1.53	2	<8	<2	7	9	<.5	3	<3	10	.06	.028	33	6	.05	85	<.01	<3	.59	.01	.17	<2	97.2
T32-13	1	100	37	67	<.3	15	7	323	1.63	5	<8	<2	8	9	<.5	3	<3	3	.06	.010	38	9	.05	68	<.01	<3	.38	.03	.19	<2	5.0
T32-14	1	95	164	241	<.3	67	38	1647	6.05	44	<8	<2	6	10	1.0	8	<3	7	.16	.041	66	6	.10	168	<.01	<3	.52	.02	.25	<2	44.2
T32-15	1	42	102	119	.4	38	26	797	3.11	20	<8	<2	11	9	<.5	5	<3	5	.11	.020	55	8	.07	122	<.01	3	.55	.03	.29	2	13.9
RE T32-15	1	42	102	118	<.3	37	26	787	3.05	21	<8	<2	10	9	<.5	5	<3	5	.10	.019	55	7	.06	121	<.01	3	.54	.02	.29	<2	19.1
T33-01	1	16	8	22	<.3	10	5	180	5.08	3	<8	<2	2	5	<.5	<3	<3	3	.02	.018	13	4	.01	23	<.01	<3	.23	.02	.07	2	13.0
T33-02	2	24	6	25	<.3	12	4	154	5.46	2	<8	<2	4	9	<.5	<3	<3	5	.05	.044	19	11	.02	45	<.01	<3	.38	.02	.12	3	44.5
T33-03	1	18	13	12	<.3	9	6	216	3.21	2	<8	<2	4	5	<.5	<3	<3	5	.03	.022	13	5	.02	42	<.01	<3	.27	.01	.08	<2	9.2
T33-04	2	38	101	35	.4	13	23	589	4.99	7	<8	<2	5	10	<.5	<3	<3	5	.03	.027	31	11	.03	67	<.01	<3	.41	.02	.14	2	30.3
T33-05	1	43	6	21	<.3	14	11	303	5.59	6	<8	<2	5	7	<.5	<3	<3	4	.03	.033	19	6	.03	40	<.01	<3	.36	.02	.12	<2	34.1
T33-06	4	17	8	11	.6	3	2	67	1.54	5	<8	<2	6	8	<.5	<3	<3	6	.02	.020	20	14	.02	41	<.01	<3	.29	.01	.15	3	587.4
T33-07	2	14	5	14	<.3	6	4	119	3.31	3	<8	<2	7	7	<.5	<3	<3	2	.02	.012	30	11	.01	35	<.01	<3	.34	.02	.16	2	13.9
T33-08	<1	34	9	16	<.3	7	4	59	1.44	7	<8	<2	10	7	<.5	<3	<3	4	.03	.013	50	5	.02	66	<.01	<3	.50	.02	.29	<2	11.1
T34-01	1	9	8	29	<.3	19	7	142	3.84	8	<8	<2	6	6	<.5	<3	<3	3	.01	.029	32	8	.03	44	<.01	3	.46	.02	.22	2	11.8
T34-02	1	24	11	30	<.3	16	5	117	2.90	12	<8	<2	12	9	<.5	<3	<3	6	.05	.027	56	7	.06	58	<.01	3	.57	.02	.29	<2	19.8
T34-03	2	29	7	33	2.8	14	67	828	2.53	6	<8	<2	6	8	<.5	<3	<3	3	.03	.050	38	9	.01	76	<.01	<3	.38	.02	.16	2	31.7
T34-04	1	52	14	51	.5	9	11	524	3.23	15	<8	<2	11	9	<.5	5	<3	21	.06	.035	39	7	.03	90	<.01	3	.54	.02	.26	2	730.1
T34-05	2	16	8	36	1.1	21	10	684	4.89	<2	8	<2	6	15	.6	<3	<3	5	.25	.161	16	9	.03	73	<.01	<3	.42	.03	.17	2	44.8
T34-06	1	24	8	30	.5	22	22	1103	6.00	6	<8	<2	7	14	.9	<3	<3	7	.20	.176	23	6	.04	112	<.01	<3	.49	.03	.19	<2	172.9
T34-07	1	9	5	14	<.3	17	12	467	2.10	2	<8	<2	7	34	<.5	<3	<3	2	.69	.316	30	8	.02	112	<.01	3	.54	.04	.22	2	4.5
T34-08	<1	6	4	10	.8	4	8	335	.58	<2	<8	<2	11	15	<.5	<3	<3	3	.20	.086	40	6	.02	69	<.01	3	.48	.03	.23	<2	1.6
T34-09	1	46	25	83	<.3	38	6	244	4.07	14	<8	<2	10	8	<.5	<3	<3	6	.08	.047	38	4	.03	63	<.01	<3	.49	.02	.22	2	43.3
T34-10	1	40	9	32	.3	20	8	168	1.78	12	<8	<2	6	8	<.5	<3	4	4	.08	.034	51	8	.04	70	<.01	3	.48	.02	.25	<2	5.1
T34-11	2	42	6	167	9.3	35	23	1711	6.88	16	<8	<2	<2	9	1.3	5	<3	2	.13	.082	7	6	.03	56	<.01	<3	.15	.01	.04	<2	9.2
T34-12	1	18	8	52	2.0	20	14	867	2.43	11	<8	<2	6	12	<.5	<3	<3	2	.16	.069	20	9	.03	92	<.01	<3	.51	.02	.25	2	14.8
T34-13	1	21	8	43	4.2	18	4	246	2.06	13	<8	<2	4	8	<.5	<3	<3	4	.11	.036	13	7	.06	55	<.01	<3	.30	.02	.14	<2	224.8
STANDARD DS5/AU-R	12	142	24	130	<.3	24	12	743	2.84	19	<8	<2	3	46	5.6	5	6	58	.70	.090	12	184	.66	137	.09	16	1.95	.04	.13	5	473.5

Sample type: ROCK R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
T34-14	<1	31	7	47	2.0	15	4	386	3.39	6	<8	<2	7	7	<.5	<3	<3	3	.07	.008	33	4	.04	66	<.01	<3	.42	.02	.22	<2	12.5
T34-15	4	14	10	36	.6	21	11	1910	2.09	4	<8	<2	11	11	<.5	<3	<3	3	.08	.023	46	9	.03	228	<.01	<3	.42	.03	.20	<2	8.8
T34-16	1	20	20	80	.4	31	8	280	3.23	22	<8	<2	9	9	<.5	4	3	5	.10	.033	35	4	.06	71	<.01	<3	.51	.02	.23	<2	81.1
T34-17	2	51	10	155	.5	74	23	679	6.18	17	<8	<2	9	13	<.5	3	<3	5	.32	.119	33	7	.07	83	<.01	<3	.56	.03	.22	2	7.7
T34-18	3	38	8	235	3.2	87	47	5116	9.90	20	<8	<2	12	19	1.3	4	<3	3	.32	.186	33	3	.05	117	<.01	<3	.44	.03	.17	<2	1.5
T34-19	6	60	12	214	8.7	110	147	8295	7.28	16	<8	<2	10	27	1.8	3	<3	2	.32	.128	29	6	.08	122	<.01	<3	.46	.03	.17	<2	1.8
T34-20	1	29	5	64	.9	42	21	500	3.34	13	<8	<2	9	11	<.5	<3	<3	3	.19	.041	34	3	.08	67	<.01	<3	.51	.03	.23	<2	5.3
T34-21	1	21	5	66	.5	28	11	449	2.69	10	<8	<2	8	10	<.5	<3	<3	3	.14	.019	27	8	.07	56	<.01	<3	.41	.02	.18	2	2.2
T34-22	1	24	7	84	.6	35	10	662	3.45	14	<8	<2	7	13	<.5	<3	3	3	.23	.053	25	3	.10	70	<.01	<3	.47	.03	.19	<2	1.3
T34-23	1	26	7	82	.3	38	17	710	4.02	9	<8	<2	13	11	<.5	<3	<3	4	.20	.038	36	7	.10	102	<.01	<3	.55	.02	.27	<2	10.0
T34-24	<1	25	4	68	.4	32	8	478	3.51	9	<8	<2	10	16	<.5	3	3	4	.30	.074	39	5	.11	85	<.01	<3	.56	.02	.29	<2	22.0
T34-25	1	62	10	127	.9	51	11	244	5.34	8	<8	<2	11	13	<.5	<3	<3	6	.20	.100	32	4	.07	67	<.01	<3	.51	.02	.27	<2	9.0
T34-26	<1	34	8	54	<.3	24	7	115	2.20	8	<8	<2	11	12	<.5	<3	3	4	.16	.048	56	4	.09	63	<.01	<3	.52	.02	.28	<2	6.3
RE T34-26	<1	33	10	52	.3	23	6	110	2.15	6	<8	<2	11	12	<.5	<3	<3	3	.15	.047	56	4	.09	61	<.01	<3	.51	.02	.28	<2	6.8
T35-01	9	100	50	262	6.2	126	95	9706	11.34	21	<8	<2	10	31	2.7	4	<3	12	.71	.204	24	6	.15	232	<.01	<3	.70	.03	.22	2	35.6
T35-02	6	77	19	285	3.5	114	47	5637	14.77	19	<8	<2	9	21	1.5	4	<3	7	.54	.182	22	4	.14	162	<.01	<3	.54	.02	.17	<2	8.6
T35-03	4	49	17	189	2.8	63	42	3985	8.58	9	<8	<2	9	20	.9	4	<3	6	.59	.096	30	8	.14	145	<.01	<3	.63	.03	.19	<2	12.9
T35-04	1	25	7	50	.3	34	13	303	4.15	3	<8	<2	9	9	<.5	3	<3	3	.10	.029	34	3	.05	57	<.01	<3	.42	.03	.19	<2	2.0
T35-05	1	36	5	84	<.3	43	11	258	7.99	4	<8	<2	12	10	<.5	5	<3	5	.31	.054	32	6	.07	69	<.01	<3	.49	.03	.23	<2	.4
T35-06	<1	19	13	21	.4	13	9	458	1.60	<2	<8	<2	5	14	<.5	<3	3	3	.43	.047	40	5	.04	70	<.01	<3	.42	.03	.20	<2	1.4
T35-07	2	24	6	36	1.0	17	8	978	1.56	3	<8	<2	8	9	<.5	<3	3	2	.21	.014	38	7	.03	74	<.01	<3	.38	.03	.19	<2	2.4
T35-08	4	15	7	14	.3	13	7	2148	2.78	12	<8	<2	7	13	<.5	<3	<3	7	.19	.016	24	6	.26	247	<.01	<3	.58	.04	.19	<2	2.6
T36-01	2	30	7	56	.6	37	8	656	5.84	11	<8	<2	9	20	<.5	<3	5	3	2.28	.071	29	7	.10	74	<.01	<3	.43	.04	.16	<2	4.5
T36-02	3	96	7	108	5.3	99	77	3723	5.32	12	<8	<2	8	16	1.3	3	<3	7	.50	.045	34	3	.07	161	<.01	<3	.51	.04	.19	<2	2.3
T36-03	3	139	7	119	.5	86	19	464	9.40	15	<8	<2	5	26	.8	10	4	5	2.81	.148	29	9	.19	76	<.01	<3	.47	.03	.14	2	3.1
T36-04	<1	17	5	43	<.3	17	8	224	1.95	2	<8	<2	10	9	<.5	<3	4	3	.18	.013	41	4	.04	61	<.01	<3	.40	.04	.19	<2	.4
T36-05	1	47	4	76	1.0	46	76	1238	4.89	9	<8	<2	8	14	<.5	<3	<3	4	.19	.086	32	8	.07	127	<.01	<3	.53	.04	.18	<2	1.0
T36-06	1	32	5	87	.3	57	74	775	7.02	15	<8	<2	9	9	<.5	<3	3	4	.09	.061	28	4	.05	71	<.01	<3	.50	.03	.21	<2	1.8
T36-07	2	22	6	58	.3	47	54	2336	8.13	8	<8	<2	9	10	<.5	4	<3	3	.24	.055	25	6	.11	100	<.01	<3	.48	.03	.19	<2	2.0
T36-08	3	31	5	98	<.3	37	24	2488	10.07	13	<8	<2	8	27	.6	3	<3	6	.90	.290	21	5	.13	147	<.01	<3	.67	.04	.24	<2	2.9
T36-09	2	34	5	33	.3	21	13	460	3.39	12	<8	<2	9	15	<.5	<3	<3	5	.78	.052	28	10	.08	57	<.01	<3	.50	.03	.15	2	1.4
T36-10	<1	44	8	123	.5	44	78	1355	7.32	5	<8	<2	6	10	<.5	<3	<3	2	.11	.034	26	3	.07	66	<.01	<3	.39	.03	.11	<2	<.2
T36-11	2	32	4	66	.4	40	35	3874	12.80	9	14	<2	8	32	1.1	3	<3	4	1.00	.406	17	7	.19	136	<.01	<3	.69	.03	.20	<2	1.5
T36-12	1	73	9	112	.5	42	70	1026	6.35	3	<8	<2	6	9	<.5	<3	<3	2	.14	.035	27	4	.07	64	<.01	<3	.43	.03	.11	<2	1.6
STANDARD DS5/AU-R	12	145	24	131	.3	24	12	746	2.88	18	<8	<2	3	46	5.6	5	5	58	.71	.094	12	188	.66	138	.09	16	1.96	.04	.14	4	471.3

Sample type: ROCK R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
T36-13	3	23	<3	274	.6	65	61	5611	26.24	39	<8	<2	8	20	.8	7	<3	3	.47	.254	14	5	.27	134	<.01	<3	.54	.02	.17	3	.5
T37-01	2	8	91	125	<.3	7	2	335	1.77	2	<8	<2	7	7	<.5	4	<3	8	.31	.046	50	9	.17	89	<.01	<3	.54	.04	.28	2	.2
T38-01	1	30	14	26	1.5	16	25	3741	3.06	6	<8	<2	11	16	<.5	<3	<3	3	.06	.026	63	6	.04	118	<.01	3	.47	.01	.32	2	.3
T38-02	2	105	24	92	1.4	19	14	5425	4.78	23	<8	<2	5	21	.7	<3	<3	2	.13	.063	26	3	.04	90	<.01	<3	.28	.01	.18	3	.7
T38-03	2	75	122	461	<.3	199	66	9624	19.79	<2	<8	<2	6	51	7.1	<3	<3	4	.30	.037	31	3	.19	110	<.01	<3	1.43	.01	.15	<2	<.2
T38-04	2	21	33	53	.9	15	7	2624	1.55	15	<8	<2	4	6	<.5	<3	<3	1	.04	.014	38	8	.02	64	<.01	<3	.25	<.01	.16	4	.2
T38-05	<1	3	83	21	.6	11	10	268	1.77	<2	<8	<2	4	34	<.5	<3	<3	1	.74	.316	15	4	.03	95	<.01	3	.42	.01	.22	2	1.4
T38-06	3	226	285	552	6.1	262	154	7041	19.30	44	<8	<2	10	17	16.0	21	<3	7	.31	.156	34	5	.12	353	<.01	<3	.36	.01	.22	3	5.1
T38-07	3	43	232	302	.8	130	32	1806	22.30	17	<8	<2	6	30	2.7	13	3	5	.48	.225	13	5	.12	100	<.01	<3	.26	<.01	.16	4	3.3
T38-08	1	89	609	171	7.6	52	51	6172	4.81	51	<8	<2	6	21	7.2	5	<3	4	.45	.072	27	4	.09	414	<.01	<3	.40	.01	.26	3	5.3
T38-09	1	39	314	201	2.4	29	28	1862	4.02	11	<8	<2	10	13	2.4	4	<3	3	.76	.066	30	4	.06	150	<.01	3	.36	.01	.21	2	1.0
T38-10	1	50	487	604	1.1	43	19	991	8.73	30	11	<2	12	8	2.9	7	<3	19	.05	.037	60	6	.06	80	<.01	3	.44	.01	.26	2	12.0
T38-11	<1	51	225	151	7.1	22	23	671	2.94	9	9	<2	11	10	1.0	3	<3	8	.05	.014	71	6	.05	69	<.01	3	.41	<.01	.27	2	7.8
T38-12	1	126	559	801	.8	45	27	2417	4.69	37	<8	<2	10	8	5.1	3	<3	7	.04	.031	33	4	.05	176	<.01	3	.47	<.01	.30	3	7.1
T38-13	1	46	233	203	.5	41	22	949	2.94	8	<8	<2	10	7	1.7	3	<3	8	.04	.011	30	4	.05	96	<.01	3	.44	.01	.28	2	18.6
T38-14	2	40	263	101	.9	20	17	630	2.50	8	<8	<2	6	7	1.5	<3	<3	5	.10	.048	24	7	.04	91	<.01	<3	.36	<.01	.22	3	4.5
T38-15	2	22	126	44	1.0	11	13	379	1.89	2	<8	<2	6	5	.5	<3	<3	4	.05	.013	24	5	.04	66	<.01	<3	.32	<.01	.21	2	2.8
T38-16	1	9	20	18	<.3	5	2	100	.85	2	<8	<2	8	4	<.5	<3	<3	2	.01	.006	28	6	.02	47	<.01	<3	.34	<.01	.24	2	2.9
RE T38-16	1	9	19	18	<.3	4	2	95	.86	<2	<8	<2	8	3	<.5	<3	<3	2	.01	.006	28	6	.02	46	<.01	<3	.34	<.01	.23	2	1.3
T38-17	1	67	18	35	<.3	11	3	165	2.22	3	<8	<2	8	8	<.5	<3	<3	6	.43	.030	38	6	.27	56	<.01	<3	.54	.01	.27	2	2.5
T38-18	1	70	15	47	<.3	14	5	246	3.34	7	<8	<2	8	4	<.5	<3	4	5	.02	.023	37	7	.04	62	<.01	<3	.46	<.01	.29	2	4.1
T38-19	2	59	4	60	3.3	26	19	2708	3.87	14	<8	<2	5	7	1.0	<3	3	3	.05	.023	43	5	.04	199	<.01	<3	.33	<.01	.21	3	<.2
T38-20	1	37	7	62	1.8	17	23	2809	4.01	5	<8	<2	7	8	.6	<3	<3	2	.07	.046	17	10	.03	106	<.01	<3	.30	.01	.16	3	.7
T38-21	1	21	4	37	1.1	14	12	739	2.08	8	<8	<2	5	3	<.5	<3	<3	1	.01	.010	23	6	.02	39	<.01	<3	.23	<.01	.15	2	<.2
T39-01	1	33	35	97	1.0	32	30	2287	3.36	13	<8	<2	10	9	.8	<3	4	4	.16	.077	29	8	.04	80	<.01	3	.53	.01	.30	3	4.9
T39-02	<1	117	724	226	8.2	72	60	7753	5.57	53	<8	<2	8	11	4.5	5	3	8	.13	.059	41	4	.06	137	<.01	3	.55	.01	.28	3	8.8
T39-03	2	104	36	83	.3	29	25	762	3.80	10	<8	<2	8	5	<.5	5	<3	5	.04	.026	29	6	.04	95	<.01	<3	.42	.01	.25	2	3.5
T39-04	1	66	22	123	.8	27	23	1070	4.69	11	<8	<2	7	4	.8	6	4	5	.02	.021	34	5	.03	73	<.01	<3	.36	.01	.22	2	4.6
T39-05	1	40	26	79	.3	27	23	787	3.34	12	<8	<2	9	6	<.5	4	<3	5	.08	.047	30	5	.03	71	<.01	<3	.45	.01	.27	2	2.8
T40-01	1	23	7	73	.4	26	8	1326	2.58	13	<8	<2	9	13	.6	<3	3	4	.46	.025	39	3	.09	124	<.01	<3	.53	.01	.25	2	2.0
T40-02	1	36	4	66	.4	20	9	287	2.37	11	<8	<2	11	7	<.5	<3	3	4	.08	.028	56	4	.06	71	<.01	<3	.61	<.01	.28	2	9.6
T40-03	4	51	7	168	14.5	111	94	>9999	6.93	52	<8	<2	8	31	1.8	<3	3	8	.39	.039	40	2	.12	988	<.01	<3	.64	.01	.24	2	38.3
T40-04	1	29	12	78	1.1	30	9	813	3.36	19	<8	<2	9	17	.5	<3	4	6	2.35	.014	43	3	.16	114	<.01	<3	.68	.01	.25	2	3.5
T40-05	1	52	53	63	1.0	28	21	968	3.71	14	<8	<2	10	8	<.5	<3	3	9	.29	.016	51	8	.12	159	<.01	<3	.84	<.01	.24	2	6.9
STANDARD DS5/AU-R	13	146	25	136	.3	25	12	782	3.02	19	<8	<2	3	47	5.8	4	7	60	.72	.096	12	190	.68	141	.10	17	1.99	.03	.14	5	466.4

<u>Sample type: ROCK R150 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.</u>

Data ✓ FA

ACME ANALYTICAL

Sedex Mining Corp. PROJECT MW FILE # A306161

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
T40-06	<1	19	10	81	.3	25	15	481	3.45	7	<8	<2	11	9	.5	<3	<3	8	.18	.023	41	11	.23	135	<.01	<3	1.16	.01	.31	<2	2.6
T40-07	<1	34	11	70	1.0	43	21	1240	4.83	10	9	<2	7	7	.8	<3	<3	7	.09	.014	55	6	.14	142	<.01	<3	.86	.01	.23	<2	2.8
T40-08	<1	36	16	65	<.3	30	19	535	2.64	9	<8	<2	8	6	<.5	<3	<3	6	.10	.009	44	9	.17	138	<.01	<3	.95	<.01	.22	<2	3.3
STANDARD DS5/AU-R	12	151	23	133	.3	24	11	747	2.96	19	<8	<2	3	47	5.7	4	6	60	.70	.095	13	189	.68	141	.10	17	1.92	.03	.14	5	460.0

Sample type: ROCK R150 60C.

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Sedex Mining Corp. PROJECT MP File # A302141 Page 1

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.2	2.9	2.4	40	<.1	4.2	4.0	515	1.83	<.5	2.8	.9	4.1	68	<.1	<.1	.1	39	.58	.083	8	27.7	.54	180	.130	2	.83	.063	.38	1.0	.01	1.8	.3	<.05	5	<.5
L21E 1300N	.6	11.0	10.8	74	<.1	11.9	6.1	746	1.69	3.8	.5	1.1	3.7	18	.1	.1	.2	14	.25	.061	14	10.3	.37	257	.068	5	1.96	.017	.24	.1	.02	2.4	.1	<.05	5	<.5
L21E 1250N	.5	11.7	11.6	56	.1	13.0	6.5	655	1.94	3.9	.7	14.4	4.3	15	.1	.2	.2	17	.23	.043	17	12.0	.42	235	.081	2	2.21	.015	.24	.2	.04	2.9	.1	<.05	6	<.5
L21E 1200N	.5	14.9	10.7	47	.2	12.2	6.9	569	1.84	3.8	.6	6.8	4.0	16	.1	.3	.2	15	.26	.040	17	11.4	.39	184	.063	2	1.88	.013	.21	.1	.01	2.6	.1	<.05	5	<.5
L21E 1150N	.5	21.5	12.2	44	.1	13.9	7.3	488	2.02	4.7	.5	.8	5.0	12	<.1	.3	.2	19	.27	.043	21	13.8	.53	168	.060	6	1.69	.011	.29	.1	.05	2.6	.1	<.05	5	<.5
L21E 1100N	.5	15.9	11.0	66	.1	14.3	7.0	624	1.84	4.0	.7	.5	3.8	22	.1	.2	.2	18	.30	.075	16	11.3	.41	257	.079	3	2.28	.015	.19	.1	.03	2.7	.1	<.05	7	<.5
L21E 1050N	.2	11.1	9.4	40	<.1	11.2	5.3	301	1.75	3.4	.6	.5	4.3	13	<.1	.2	.2	16	.20	.025	18	10.8	.38	178	.070	2	1.85	.014	.19	.1	.03	2.5	.1	<.05	6	<.5
L21E 1000N	.4	11.8	9.7	50	<.1	12.2	6.1	406	1.81	3.2	.6	.9	4.7	12	.1	.2	.2	17	.24	.032	20	12.4	.43	140	.064	3	1.70	.011	.26	.1	.03	2.8	.1	<.05	5	<.5
L21E 950N	.5	15.1	10.4	63	<.1	14.5	6.8	646	1.83	3.7	.5	.9	4.2	18	.1	.2	.2	17	.24	.038	17	12.5	.40	231	.070	3	1.95	.017	.21	.2	.04	2.7	.1	<.05	6	<.5
L21E 900N	.3	9.0	9.7	52	<.1	12.6	5.3	434	1.76	2.9	.6	.9	4.1	16	.1	.2	.2	15	.20	.035	17	10.8	.37	220	.082	3	2.23	.017	.21	.1	.03	2.7	.1	<.05	6	<.5
L21E 850N	.6	9.1	11.0	54	.1	13.5	5.4	486	1.66	3.0	.6	.5	3.8	16	<.1	.1	.2	16	.21	.041	16	10.6	.37	261	.087	3	2.26	.020	.20	.2	.04	2.7	.1	<.05	6	<.5
L21E 800N	1.0	29.8	13.0	71	.1	15.9	7.1	709	2.01	4.9	.6	<.5	3.8	19	.2	.3	.2	22	.28	.052	20	15.2	.46	191	.075	3	2.14	.014	.23	.2	.04	3.4	.1	.06	6	<.5
L21E 750N	.5	12.2	10.1	63	.1	12.3	6.1	622	1.69	3.5	.6	.5	3.5	19	.1	.2	.2	17	.27	.041	16	11.2	.37	235	.077	3	2.10	.018	.21	.1	.03	2.4	.1	<.05	6	<.5
L21E 700N	.6	26.6	12.6	71	.1	14.9	8.2	576	2.06	5.6	.8	<.5	4.0	16	.1	.3	.2	24	.23	.058	19	14.8	.47	215	.073	1	2.12	.014	.13	.1	.02	3.1	.1	<.05	6	<.5
L21E 650N	.5	22.1	16.3	61	.2	17.0	7.9	656	2.04	4.3	.7	2.4	4.1	19	.1	.6	.2	21	.36	.040	20	13.2	.43	196	.075	3	2.10	.015	.28	.1	.03	3.0	.1	<.05	6	<.5
L21E 600N	.6	17.6	18.0	91	.2	18.2	8.1	875	2.01	4.8	.9	1.2	3.6	25	.2	.5	.2	20	.35	.075	20	12.5	.39	258	.084	4	2.49	.020	.26	.1	.03	3.0	.1	<.05	7	<.5
L21E 550N	.7	29.0	18.3	79	.1	13.2	7.5	1069	1.94	4.2	.6	1.2	2.5	23	.2	.3	.2	21	.53	.073	16	11.7	.38	202	.058	3	1.92	.013	.22	.2	.03	3.1	.1	<.05	5	<.5
L21E 500N	.4	18.2	12.9	54	.1	12.1	7.4	642	1.82	3.3	.4	.7	3.1	18	.1	.3	.2	16	.43	.054	19	10.6	.44	166	.049	4	1.56	.011	.25	.2	.02	2.3	.1	<.05	5	<.5
L21E 450N	.7	16.4	11.7	55	.1	13.2	6.8	710	1.67	3.5	.5	.5	1.9	32	.2	.3	.2	17	.45	.059	17	9.7	.35	194	.051	2	1.56	.012	.21	.2	.01	1.9	.1	.07	5	<.5
L21E 400N	.4	17.5	11.8	48	.1	13.1	7.0	585	1.73	4.0	.4	1.3	3.0	19	.1	.3	.2	15	.45	.058	19	10.1	.42	147	.047	4	1.46	.011	.22	.3	.02	2.0	.1	<.05	4	<.5
RE L21E 400N	.4	18.1	11.8	52	.1	13.3	7.4	626	1.84	4.3	.5	2.3	3.0	19	.1	.4	.2	16	.49	.062	20	10.4	.43	158	.049	7	1.58	.011	.22	.2	.03	2.1	.1	.07	4	<.5
L21E 350N	.7	23.3	14.8	64	.1	16.2	8.8	706	2.07	4.8	.6	<.5	3.5	23	.2	.4	.2	18	.45	.068	20	12.1	.46	170	.057	6	1.70	.011	.26	.3	.01	2.5	.1	<.05	5	<.5
L21E 300N	1.4	25.5	19.4	128	.1	19.0	8.8	1248	1.88	4.3	.9	.5	.9	36	.4	.3	.3	16	.49	.115	16	9.8	.34	250	.047	3	1.93	.013	.18	.1	.03	1.6	.1	<.05	5	<.5
L21E 250N	.6	24.9	13.3	53	.1	17.0	8.8	555	2.16	5.3	.6	.6	3.8	18	.1	.4	.3	19	.47	.071	23	14.5	.55	169	.067	4	1.77	.009	.37	.2	.03	2.9	.1	.07	5	<.5
L21E 200N	.7	18.4	12.5	67	.1	15.2	8.1	695	1.72	3.6	1.0	<.5	1.2	31	.3	.2	.2	16	.62	.090	17	10.4	.43	196	.061	3	1.73	.012	.22	.2	.05	1.6	.1	.07	5	<.5
L22E 1000N	.4	8.2	12.4	59	<.1	12.2	5.5	634	1.66	3.4	.5	<.5	3.4	16	.1	.2	.2	15	.20	.043	15	9.9	.35	213	.079	2	2.02	.018	.21	.2	.02	2.3	.1	.11	6	<.5
L22E 950N	.3	8.9	12.4	77	<.1	11.7	5.7	716	1.66	2.9	.4	.7	3.5	15	.2	.2	.2	13	.31	.042	16	10.6	.39	196	.067	4	1.81	.013	.24	.3	.03	2.3	.1	<.05	5	<.5
L22E 900N	.5	10.1	15.9	75	<.1	10.6	5.8	739	1.66	4.5	.4	.9	3.3	18	.2	.3	.2	14	.29	.044	16	11.2	.37	214	.067	3	1.86	.015	.21	.2	.03	2.3	.1	<.05	5	<.5
L22E 850N	1.3	11.0	10.7	50	.1	13.7	6.8	532	1.87	4.1	.6	<.5	3.7	15	.1	.2	.2	17	.24	.035	17	11.4	.40	176	.077	3	2.15	.013	.21	.2	.04	2.9	.1	.14	5	<.5
L22E 800N	.9	22.0	34.7	151	.1	19.3	10.0	1579	2.12	7.1	.9	<.5	1.7	29	.4	.6	.3	17	.68	.158	16	10.6	.38	257	.063	5	2.29	.016	.16	.2	.03	2.1	.1	.07	7	<.5
L22E 750N	1.2	12.7	19.4	117	.1	11.9	5.8	1180	1.52	5.4	.4	.5	1.8	27	.3	.2	.2	15	.43	.112	12	8.8	.29	243	.065	1	1.88	.017	.18	.1	.04	1.8	.1	<.05	5	<.5
L22E 700N	.6	24.3	16.7	62	.1	13.8	7.6	675	1.94	3.6	.5	.8	4.2	17	.2	.3	.2	19	.43	.050	18	12.8	.44	165	.063	5	1.79	.010	.29	.2	.01	2.7	.1	<.05	5	<.5
L22E 650N	.6	14.9	21.9	91	.1	11.6	6.0	856	1.62	4.2	.5	1.2	2.1	27	.3	.3	.2	14	.57	.064	14	9.8	.33	232	.055	4	1.65	.011	.23	.1	.03	2.2	.1	.08	4	<.5
L22E 600N	.6	22.4	25.1	109	.1	17.4	9.2	845	2.02	5.1	.7	<.5	3.6	23	.3	.5	.3	18	.44	.069	18	12.5	.42	173	.059	4	1.84	.010	.26	.2	.01	2.5	.1	.09	5	<.5
L22E 550N	.9	25.6	16.3	123	.2	21.3	9.9	1390	1.96	5.7	.7	.5	1.9	45	.3	.5	.2	17	.68	.129	17	10.1	.34	236	.058	3	1.96	.015	.18	.1	.03	2.2	.1	.07	6	<.5
STANDARD DS4	6.9	129.4	30.5	160	.4	35.9	12.7	780	3.23	23.2	6.6	26.6	4.0	29	5.3	4.6	5.0	78	.56	.089	17	174.5	.61	143	.103	2	1.73	.030	.17	3.9	.28	3.9	1.2	<.05	6	1.2

GROUP 1DX - 15.0 GM SAMPLE LEACHED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 300 ML, ANALYSED BY ICP-MS.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
- SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUN 20 2003 DATE REPORT MAILED: July 2/03 SIGNED BY ... D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Sedex Mining Corp. PROJECT MW FILE # A302141

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.3	1.9	2.0	39	<.1	4.8	4.4	474	1.84	.5	2.6	<.5	3.7	64	<.1	<.1	.1	38	.52	.089	6	30.8	.52	193	.124	1	.88	.062	.41	.7	.01	1.8	.3	<.05	4	<.5
L22E 500N	1.4	29.6	21.0	102	.1	20.4	11.1	1294	2.38	6.4	.9	1.3	2.4	35	.3	.6	.3	15	.55	.109	16	8.9	.37	169	.046	4	1.04	.009	.18	.1	.03	2.1	.1	.07	4	<.5
L22E 450N	1.6	25.7	26.0	129	.1	19.9	9.7	1230	2.00	6.1	1.0	.8	1.3	45	.5	.4	.3	17	.69	.106	14	10.8	.43	216	.050	3	2.01	.012	.16	.2	.04	1.7	.1	.07	6	<.5
L22E 400N	.7	17.5	15.5	74	.1	12.4	6.8	827	1.59	4.2	.4	2.9	1.5	31	.2	.3	.2	13	.56	.065	15	8.5	.36	199	.038	3	1.45	.008	.18	.2	.04	1.4	.1	.06	4	<.5
L22E 350N	.8	17.5	15.6	68	.1	11.6	6.6	737	1.62	3.8	.5	1.0	2.1	30	.2	.3	.2	13	.57	.063	14	8.5	.35	196	.042	2	1.51	.010	.21	.2	.03	1.7	.1	<.05	4	<.5
L22E 300N	.5	15.5	15.6	55	.1	12.0	6.2	592	1.65	4.1	.5	.6	2.3	22	.2	.4	.2	12	.44	.063	15	9.0	.35	168	.042	2	1.49	.008	.19	.1	.04	1.6	.1	<.05	4	<.5
L22E 250N	.7	17.1	16.2	64	.1	11.4	6.5	657	1.63	4.7	.5	.8	2.4	24	.1	.4	.2	13	.47	.061	16	9.6	.37	171	.043	3	1.49	.010	.19	.1	.02	1.8	.1	<.05	4	<.5
L22E 200N	.7	18.9	15.8	57	.1	12.6	6.7	670	1.67	4.8	.4	.7	2.0	22	.2	.3	.2	14	.60	.073	16	9.8	.38	168	.041	2	1.49	.011	.18	.2	.02	1.8	.1	<.05	4	<.5
L23E 1000N	.5	9.3	10.9	62	<.1	10.9	6.0	677	1.75	3.4	.6	1.3	3.4	15	.1	.2	.2	14	.28	.040	17	9.6	.36	205	.064	4	2.00	.012	.25	.2	.01	2.4	.1	<.05	5	<.5
L23E 950N	.5	14.6	11.4	75	.1	14.3	6.9	810	1.83	4.7	.8	1.2	2.2	25	.2	.2	.2	17	.31	.070	18	10.5	.34	274	.072	2	2.34	.016	.16	.1	.02	2.3	.1	<.05	6	<.5
L23E 900N	.6	11.7	9.1	85	<.1	15.6	6.3	854	1.59	3.2	.5	1.3	2.4	25	.1	.1	.2	14	.28	.068	14	9.1	.31	263	.067	2	2.08	.019	.17	.2	.02	2.1	.1	<.05	5	<.5
L23E 850N	.3	11.9	8.8	47	<.1	11.2	6.5	468	1.79	3.3	.4	<.5	3.7	10	<.1	.2	.2	12	.22	.045	18	10.3	.39	124	.046	3	1.48	.009	.26	.1	.02	2.4	.1	<.05	4	<.5
L23E 800N	.5	16.8	10.6	78	.1	12.8	6.6	705	1.66	4.0	.6	2.0	2.0	20	.2	.2	.2	15	.36	.102	16	10.3	.37	192	.052	2	1.79	.013	.19	.1	.02	1.9	.1	<.05	5	<.5
L23E 750N	1.1	26.3	32.4	289	.3	23.8	12.0	1295	2.18	7.1	1.2	2.2	1.8	32	2.3	.5	.3	21	.29	.140	18	12.6	.38	251	.078	2	2.81	.015	.11	.2	.02	2.5	.1	<.05	7	<.5
L23E 700N	.8	15.4	13.8	89	.1	16.0	7.4	922	1.78	4.8	.6	1.2	1.1	25	.1	.2	.2	16	.47	.098	15	10.6	.35	235	.030	2	2.03	.014	.15	.1	.02	1.7	.1	<.05	5	<.5
L23E 650N	.6	19.5	15.0	68	.1	14.1	7.3	589	1.78	4.4	.4	<.5	2.6	21	.2	.4	.2	13	.49	.058	20	10.1	.44	152	.039	3	1.45	.009	.20	.2	.03	2.0	.1	<.05	4	<.5
L23E 600N	.5	17.6	11.6	51	.1	13.8	7.2	529	1.77	4.4	.4	.7	2.9	16	.1	.3	.2	14	.41	.054	20	9.9	.42	129	.041	3	1.53	.007	.21	.2	.02	2.0	.1	<.05	4	<.5
L23E 550N	.7	18.0	13.4	65	.1	14.4	7.5	747	1.84	4.2	.6	<.5	3.1	23	.1	.3	.2	16	.40	.056	20	10.4	.39	201	.054	3	1.81	.009	.20	.2	.02	2.3	.1	<.05	4	<.5
L23E 500N	1.3	28.3	18.1	112	.1	23.9	10.6	1037	2.21	5.5	.9	.6	3.0	33	.3	.6	.3	16	.55	.087	20	11.1	.41	197	.054	4	2.04	.010	.22	.2	.03	2.3	.1	<.05	5	<.5
L23E 450N	.6	18.0	16.0	52	.1	12.1	7.3	532	1.68	5.3	.4	<.5	2.7	17	.1	.3	.2	13	.40	.069	20	9.7	.44	117	.037	2	1.27	.008	.18	.2	.02	1.8	.1	<.05	3	<.5
L23E 400N	.8	17.1	11.8	65	.1	13.6	7.0	764	1.71	4.0	.6	<.5	1.4	27	.2	.2	.2	15	.47	.079	18	9.4	.36	208	.050	3	1.81	.012	.19	.2	.02	1.8	.1	<.05	5	<.5
L23E 350N	.7	19.5	11.4	56	.1	13.8	7.5	646	1.81	4.2	.5	<.5	2.6	21	.1	.3	.2	15	.52	.074	20	10.4	.45	171	.040	4	1.51	.009	.20	.1	.02	2.0	.1	<.05	4	<.5
L23E 300N	.6	26.3	14.1	58	.1	15.0	9.1	644	2.10	4.5	.5	1.6	3.9	19	.1	.4	.2	19	.39	.052	23	13.0	.53	169	.048	3	1.73	.009	.25	.2	.02	2.5	.1	<.05	4	<.5
RE L23E 300N	.5	26.5	13.9	58	.1	15.8	8.6	645	2.13	5.1	.5	.5	4.0	18	.1	.3	.2	20	.39	.052	23	13.2	.53	168	.049	3	1.70	.008	.26	.3	.02	2.6	.1	<.05	4	<.5
L23E 250N	.4	19.6	11.4	53	.1	13.9	7.6	603	1.80	4.8	.3	2.5	2.6	18	.2	.4	.2	16	.49	.061	21	10.7	.48	153	.040	6	1.47	.009	.22	.2	.02	2.1	.1	<.05	4	<.5
L23E 200N	.9	21.6	12.4	72	.1	16.7	8.6	851	1.93	4.5	.8	.8	2.2	30	.1	.2	.3	17	.47	.080	18	11.5	.41	216	.052	3	1.81	.011	.18	.2	.01	2.1	.1	<.05	5	<.5
L24E 1000N	.4	15.2	11.4	66	.1	16.7	6.5	614	1.79	3.5	.5	<.5	3.2	18	.1	.2	.2	15	.30	.055	19	11.7	.41	198	.055	3	1.79	.010	.24	.2	.01	2.4	.1	<.05	5	<.5
L24E 950N	.5	19.5	12.1	89	.1	15.9	7.6	803	1.85	4.6	.7	<.5	2.2	28	.2	.2	.2	17	.43	.084	19	11.1	.39	236	.058	4	2.00	.011	.20	.2	.04	2.3	.1	<.05	5	<.5
L24E 900N	.7	21.4	12.7	107	.1	16.5	8.2	1052	1.74	5.2	.6	<.5	.6	34	.2	.2	.2	16	.43	.128	17	10.8	.37	274	.043	3	1.86	.014	.19	.1	.03	1.5	.1	<.05	5	<.5
L24E 850N	.6	15.7	11.2	59	.1	13.4	6.6	633	1.77	3.8	.7	.5	1.9	22	.2	.2	.2	15	.35	.068	18	10.1	.40	176	.045	3	1.70	.010	.16	.2	.01	2.1	.1	<.05	4	<.5
L24E 800N	1.6	20.7	22.1	152	.1	23.8	11.0	1735	2.20	6.5	1.0	1.1	1.3	29	.4	.3	.3	21	.34	.131	19	13.1	.44	267	.059	2	2.59	.009	.12	.1	.04	2.2	.1	<.05	7	<.5
L24E 750N	1.6	30.1	26.9	174	.2	26.7	9.8	1606	2.06	7.3	.8	.7	1.1	53	.6	.6	.3	14	1.03	.135	15	10.2	.43	214	.043	5	1.85	.016	.20	.1	.03	1.4	.1	<.05	5	<.5
L24E 700N	.7	29.9	24.6	125	.1	26.6	11.2	1190	1.98	5.1	.7	<.5	1.4	48	.3	.3	.4	15	.90	.145	14	10.8	.43	223	.060	6	2.08	.020	.28	.1	.02	1.7	.1	<.05	5	<.5
L24E 650N	1.1	25.9	23.5	118	.1	19.9	8.6	1236	1.79	5.1	.9	<.5	1.4	42	.4	.6	.2	16	.80	.119	14	9.3	.37	200	.064	4	2.21	.019	.20	.1	.06	1.7	.1	<.05	5	<.5
L24E 600N	.8	19.2	14.7	54	.1	16.5	8.4	725	2.05	5.6	.9	.7	2.8	22	.1	.3	.3	19	.33	.078	21	12.0	.45	221	.063	1	2.08	.015	.14	.2	.02	2.9	.1	<.05	5	<.5
STANDARD DS4	6.9	126.3	30.7	163	.4	35.8	12.2	775	3.27	22.7	6.6	26.7	3.9	28	5.3	4.7	5.1	78	.55	.095	18	170.6	.60	147	.093	2	1.82	.030	.16	4.0	.28	3.9	1.2	<.05	6	1.2

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ACME ANALYTICAL

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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.3	2.2	2.5	37	<.1	3.9	3.5	499	1.80	<.5	2.8	<.5	4.0	67	<.1	<.1	.1	39	.56	.086	8	21.4	.56	190	.130	2	.81	.059	.39	.9	<.01	1.8	.3	<.05	4	<.5
L24E 550N	.8	20.3	17.4	58	.1	17.4	8.5	789	1.88	4.9	.8	<.5	4.0	31	.1	.4	.3	17	.37	.065	20	8.8	.42	201	.061	3	1.85	.017	.18	.1	.02	2.4	.2	<.05	5	<.5
L24E 500N	.6	19.9	16.1	47	.1	13.7	7.4	551	1.91	3.9	.5	1.4	4.1	16	.1	.4	.3	18	.36	.053	20	9.6	.48	146	.067	4	1.46	.009	.24	.2	.02	2.3	.1	<.05	4	<.5
L24E 450N	.6	20.3	12.0	52	.1	12.7	7.3	571	1.74	4.1	.4	.8	2.9	16	.1	.4	.3	16	.38	.071	20	9.4	.49	155	.039	4	1.46	.010	.21	.2	.01	1.9	.1	<.05	4	.6
L24E 400N	.4	19.0	12.4	50	.1	13.2	6.7	526	1.75	4.2	.4	2.5	2.9	18	.1	.3	.2	18	.40	.067	19	10.0	.49	141	.038	5	1.36	.010	.22	.2	.01	2.0	.1	<.05	4	.5
L24E 350N	.6	20.1	13.3	58	.1	16.1	7.8	639	1.86	3.9	.7	<.5	3.3	23	.2	.5	.2	20	.35	.059	22	9.7	.47	196	.056	6	1.68	.008	.24	.2	.02	2.4	.1	<.05	5	<.5
L24E 300N	.8	20.8	17.4	93	.1	21.5	10.3	916	2.18	4.8	1.1	<.5	2.6	36	.3	.4	.3	23	.40	.091	18	11.0	.45	277	.078	4	2.49	.016	.14	.1	.03	2.6	.1	<.05	7	<.5
L24E 250N	1.5	26.7	19.1	94	.1	23.7	11.7	1043	2.21	5.4	1.4	.6	2.5	32	.4	.5	.3	24	.30	.084	18	10.2	.45	270	.086	2	2.79	.014	.15	.2	.03	2.7	.1	<.05	8	<.5
L24E 200N	1.3	29.7	15.1	86	.1	15.9	7.8	1088	1.62	4.4	.9	.8	.5	48	.3	.3	.2	16	.70	.189	13	7.5	.36	273	.038	5	2.15	.017	.14	.1	.03	1.1	.1	<.05	6	<.5
L25E 1000N	.4	13.1	12.2	54	.1	13.9	6.3	709	1.73	4.1	.6	1.1	3.7	20	.1	.2	.2	17	.29	.049	18	9.9	.42	256	.068	4	2.03	.016	.26	.2	.03	2.5	.1	<.05	5	<.5
L25E 950N	.6	13.8	11.4	67	.1	15.8	6.9	905	1.72	3.8	.7	<.5	2.6	28	.1	.2	.2	16	.32	.059	18	9.3	.36	383	.071	3	2.29	.018	.16	.2	.03	2.3	.1	<.05	5	<.5
L25E 900N	.7	19.6	11.5	173	.1	17.1	7.6	1404	1.61	4.3	.6	.5	1.4	40	.3	.2	.2	14	.49	.242	14	9.0	.32	341	.059	4	2.15	.019	.16	.1	.05	1.8	.1	<.05	6	<.5
L25E 850N	.7	23.6	28.2	118	.1	21.4	9.7	1247	2.06	6.1	.9	<.5	2.2	43	.3	.4	.4	19	.60	.099	18	12.5	.48	258	.084	5	2.79	.019	.24	.1	.03	2.3	.1	<.05	7	<.5
L25E 800N	1.2	23.1	36.4	185	.2	27.8	11.4	1451	2.00	6.5	.9	<.5	1.7	53	.8	.5	.3	16	.60	.156	14	10.6	.40	254	.063	3	2.38	.017	.13	.1	.04	1.8	.1	<.05	6	<.5
L25E 750N	.7	16.0	16.6	147	.2	16.4	8.2	1109	1.85	4.8	.9	1.3	2.2	34	.5	.3	.2	19	.35	.129	14	10.9	.38	272	.090	2	2.66	.023	.11	.1	.05	2.3	.1	<.05	7	<.5
L25E 700N	.7	17.3	19.7	95	.1	17.3	7.8	1097	2.00	5.0	.8	<.5	1.9	30	.2	.3	.3	18	.41	.089	20	12.4	.49	334	.067	3	2.36	.015	.16	.2	.03	2.7	.1	<.05	6	<.5
L25E 650N	.7	14.3	13.0	68	.1	14.4	7.4	823	1.89	3.8	.8	.7	3.3	27	.1	.3	.2	19	.33	.055	18	11.0	.41	273	.079	2	2.25	.018	.12	.1	.02	2.7	.1	<.05	6	<.5
L25E 600N	.6	15.5	12.7	67	.1	14.3	7.5	1016	1.83	4.3	.8	<.5	1.4	30	.1	.3	.2	19	.46	.102	17	11.1	.41	305	.066	3	2.33	.019	.22	.1	.08	2.2	.1	<.05	5	<.5
RE L25E 600N	.6	15.6	12.9	65	.1	13.0	7.0	968	1.81	4.2	.7	.7	1.6	30	.2	.2	.2	17	.44	.102	17	10.5	.41	308	.066	3	2.25	.020	.20	.2	.07	2.4	.1	<.05	5	<.5
L25E 550N	.6	20.0	13.5	51	.1	13.1	7.3	703	1.63	4.2	.6	.9	1.9	25	.2	.3	.2	15	.50	.093	17	9.7	.43	195	.046	2	1.62	.013	.16	.2	.06	1.9	.1	<.05	4	<.5
L25E 500N	.9	17.7	14.2	56	.1	12.5	7.4	818	1.57	4.1	.6	<.5	2.6	26	.2	.3	.2	12	.57	.066	17	10.0	.50	176	.036	3	1.25	.009	.18	.2	.03	2.0	.1	<.05	3	<.5
L25E 450N	.8	17.8	13.5	68	.1	14.9	7.8	981	1.91	4.2	.8	<.5	1.8	29	.2	.3	.2	19	.48	.108	18	12.1	.43	305	.065	4	2.15	.015	.16	.1	.06	2.6	.1	<.05	5	<.5
L25E 400N	.4	15.0	12.3	44	<.1	13.0	7.6	583	1.82	4.4	.6	.5	3.4	16	<.1	.3	.2	18	.29	.060	21	11.6	.49	151	.056	3	1.62	.010	.15	.2	.03	2.5	.1	<.05	4	<.5
L25E 350N	.3	19.0	13.0	56	.1	12.2	7.7	711	1.82	3.7	.3	.6	2.6	61	.1	.3	.2	14	1.68	.063	17	11.4	.66	188	.045	9	1.60	.014	.28	.1	.03	2.1	.1	<.05	4	<.5
L25E 300N	.8	17.2	20.3	76	.1	19.2	9.5	751	2.30	5.3	1.1	1.5	3.9	27	.1	.4	.3	19	.39	.054	23	12.4	.52	227	.070	4	2.21	.017	.19	.1	.05	3.0	.1	<.05	6	<.5
L25E 250N	.3	8.6	18.6	61	.1	12.4	5.2	177	1.74	1.3	2.7	1.3	3.5	31	.1	.1	.2	11	.48	.026	15	10.2	.49	141	.091	3	2.53	.021	.20	.1	.03	2.9	.1	<.05	6	.5
L25E 200N	.3	18.8	9.9	49	.1	10.4	6.3	661	1.46	3.3	.7	<.5	.7	87	.2	.2	.2	13	3.29	.101	11	9.7	.63	260	.034	6	1.56	.023	.20	.1	.04	1.3	.1	.07	4	.9
L26E 1000N	.5	24.3	17.2	102	<.1	16.4	9.8	1540	1.95	6.8	.6	3.1	3.7	25	.3	.2	.3	17	.54	.109	22	13.4	.54	392	.060	4	1.98	.016	.25	.1	.04	3.0	.1	<.05	5	<.5
L26E 950N	.4	16.2	12.4	67	.1	14.5	7.3	710	1.90	3.9	.6	<.5	4.0	18	.1	.2	.2	16	.32	.054	21	12.0	.48	222	.063	3	2.01	.012	.28	.2	.03	2.7	.1	<.05	5	<.5
L26E 900N	1.0	17.3	13.9	164	.1	20.6	9.3	1318	1.87	4.6	.9	<.5	1.2	36	.4	.3	.2	18	.36	.086	16	10.3	.40	295	.063	4	2.36	.016	.14	.1	.05	2.0	.1	<.05	6	<.5
L26E 850N	1.3	15.9	13.9	89	.1	17.8	8.4	955	2.01	4.1	.9	.9	1.6	25	.1	.2	.2	20	.30	.090	18	12.3	.45	277	.069	3	2.45	.015	.14	.1	.01	2.3	.1	<.05	6	<.5
L26E 800N	1.1	16.0	11.7	103	.1	17.8	8.9	1036	1.70	4.7	.9	<.5	.9	27	.2	.2	.2	17	.34	.140	16	10.4	.36	272	.064	3	2.48	.019	.11	.1	.06	1.8	.1	<.05	6	<.5
L26E 750N	.5	18.8	12.5	98	.1	16.8	8.4	1195	2.04	6.2	.7	<.5	2.3	30	.2	.2	.2	19	.56	.124	17	13.6	.51	389	.074	4	2.47	.017	.17	.2	.05	2.7	.1	<.05	6	<.5
L26E 700N	.7	17.2	19.3	116	<.1	14.8	7.7	1275	1.88	6.0	.7	<.5	1.6	28	.2	.2	.2	17	.45	.139	16	12.2	.42	422	.069	3	2.44	.017	.15	.1	.03	2.3	.1	<.05	6	<.5
L26E 650N	.4	21.1	15.4	84	.1	17.7	8.8	810	2.24	6.6	.7	<.5	3.5	27	.1	.2	.2	20	.47	.073	19	14.2	.55	385	.082	3	2.66	.018	.17	.1	.03	3.3	.1	<.05	6	<.5
STANDARD DS4	6.9	127.5	31.1	161	.3	36.3	11.8	810	3.16	22.0	6.6	28.1	4.2	28	5.5	4.9	5.0	77	.52	.093	18	162.6	.60	142	.093	3	1.79	.031	.16	4.2	.29	3.8	1.2	<.05	6	1.4

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ACME ANALYTICAL

Sedex Mining Corp. PROJECT MW FILE # A302141

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.0	3.1	2.1	46	<.1	4.5	4.1	516	1.78	<.5	2.6	<.5	3.8	73	<.1	<.1	.1	42	.53	.088	8	29.7	.55	194	.131	2	.88	.069	.38	.8	<.01	1.9	.3	.07	5	<.5
L26E 600N	.6	15.2	13.8	94	.1	15.9	7.6	873	2.05	5.5	.9	.8	2.2	26	.2	.2	.2	20	.37	.110	17	10.7	.46	410	.075	4	2.54	.016	.14	.2	.04	2.6	.1	<.05	7	<.5
L26E 550N	.5	16.5	12.8	84	.1	14.3	7.0	899	1.72	4.2	.6	1.0	.9	29	.1	.2	.2	17	.67	.097	14	9.5	.39	279	.047	4	1.93	.014	.18	.2	.02	1.6	.1	.10	5	<.5
L26E 500N	.5	20.8	18.3	74	.1	16.3	8.6	893	2.10	6.3	.9	<.5	3.0	26	.1	.6	.2	20	.43	.087	20	12.2	.49	297	.069	2	2.27	.011	.17	.2	.02	3.3	.1	<.05	6	<.5
L26E 450N	.6	22.3	18.1	83	.1	16.5	9.3	1038	1.99	5.0	.8	<.5	2.3	29	.2	.6	.3	20	.52	.092	19	11.2	.43	304	.062	4	1.96	.011	.20	.2	.04	2.5	.1	<.05	6	<.5
L26E 400N	.6	20.2	15.9	85	.1	15.5	8.5	996	2.00	5.6	1.0	<.5	1.1	33	.1	.3	.2	20	.48	.126	19	11.2	.45	332	.061	4	2.49	.014	.12	.2	.04	2.2	.1	.06	6	<.5
L26E 350N	.6	22.3	16.4	90	.1	17.1	9.2	1093	2.11	5.5	1.1	<.5	1.2	30	.2	.3	.2	21	.51	.132	19	11.6	.50	262	.063	6	2.41	.015	.14	.1	.04	2.3	.1	<.05	7	<.5
L26E 300N	.1	9.1	14.8	42	<.1	8.8	5.7	287	1.57	1.9	.2	<.5	3.5	23	.1	.2	.2	10	.39	.021	13	9.4	.47	231	.036	3	1.49	.020	.17	.1	.04	2.1	.1	<.05	4	<.5
L26E 250N	.4	13.8	14.5	56	.1	11.5	5.9	589	1.65	4.4	.6	.7	2.5	22	.1	.3	.2	14	.39	.056	17	8.3	.41	230	.049	4	1.71	.010	.21	.2	.03	2.1	.1	<.05	4	<.5
L26E 200N	.3	15.2	10.7	50	.1	11.6	6.8	572	1.69	3.8	.5	<.5	2.6	20	.1	.2	.2	15	.34	.050	18	9.4	.43	200	.047	3	1.71	.011	.19	.1	.02	2.1	.1	<.05	5	<.5
L27E 1000N	.4	17.8	15.5	85	.1	15.3	8.2	1011	1.93	5.9	.7	<.5	2.0	23	.2	.2	.2	18	.39	.155	16	10.4	.41	299	.067	3	2.31	.016	.16	.4	.06	2.4	.1	<.05	7	<.5
L27E 950N	.5	20.0	14.4	74	.1	14.9	8.2	906	1.87	4.9	1.0	<.5	1.3	30	.1	.2	.3	20	.46	.111	17	10.8	.43	314	.065	4	2.33	.016	.14	.1	.06	2.3	.1	<.05	6	<.5
L27E 900N	.7	16.6	19.3	86	.1	13.4	7.3	947	1.75	5.0	.9	<.5	1.0	35	.3	.3	.2	18	.59	.106	16	10.6	.44	326	.054	5	2.07	.013	.17	.1	.04	1.9	.1	<.05	6	<.5
L27E 850N	.8	20.0	14.8	74	.1	16.9	9.0	977	2.07	5.5	1.0	<.5	1.9	32	.2	.2	.3	20	.62	.098	18	11.6	.49	319	.063	3	2.46	.013	.18	.2	.05	2.5	.1	<.05	6	<.5
L27E 800N	.5	15.3	12.3	68	.1	14.7	7.2	851	1.86	3.9	.7	<.5	2.2	29	.2	.2	.2	19	.47	.069	17	11.4	.41	323	.067	3	2.30	.014	.15	.2	.04	2.6	.1	<.05	6	<.5
L27E 750N	.5	16.8	11.9	77	.1	15.5	8.3	911	1.90	5.1	.8	<.5	2.1	27	.2	.2	.2	19	.34	.096	16	11.6	.39	369	.080	3	2.49	.020	.15	.2	.03	2.8	.1	<.05	7	<.5
L27E 700N	.4	15.5	14.3	61	.1	13.9	7.3	790	1.94	3.5	.5	1.2	3.2	24	.1	.3	.3	14	.42	.082	17	10.6	.46	277	.072	3	2.22	.017	.24	.1	.06	2.9	.1	<.05	5	<.5
L27E 650N	.4	17.3	12.5	60	<.1	15.6	8.0	783	1.95	4.3	.6	1.9	3.7	26	.1	.2	.2	19	.29	.033	16	11.7	.43	288	.082	3	2.17	.015	.21	.2	.03	3.1	.1	<.05	6	<.5
L27E 600N	.4	22.3	14.1	60	.1	15.5	9.1	626	2.08	4.1	.6	1.3	3.7	21	.1	.3	.3	21	.41	.034	21	15.5	.52	223	.082	4	1.87	.011	.30	.2	.02	3.0	.1	<.05	5	<.5
L27E 550N	.4	16.1	11.2	53	.1	12.4	7.8	667	1.75	4.1	.3	<.5	1.7	29	.1	.2	.2	15	.87	.063	16	10.5	.54	194	.043	4	1.56	.016	.18	.2	.05	1.9	.1	<.05	4	<.5
L27E 500N	.6	18.5	16.1	77	.1	15.9	8.3	865	2.09	5.6	1.0	<.5	2.3	33	.2	.3	.2	22	.36	.096	20	13.5	.45	345	.082	3	2.54	.017	.15	.2	.05	3.0	.1	<.05	6	<.5
L27E 450N	.5	19.1	16.4	78	.1	14.8	8.8	977	2.06	5.5	.9	<.5	1.5	31	.3	.3	.2	21	.42	.100	20	12.9	.48	320	.068	3	2.23	.015	.14	.1	.05	2.6	.1	<.05	6	<.5
L27E 400N	.6	23.4	18.8	82	.1	19.9	10.1	1141	2.53	6.2	1.0	1.0	2.4	32	.1	.3	.3	23	.49	.106	23	16.4	.56	348	.065	3	2.45	.010	.14	.2	.04	3.5	.1	<.05	6	<.5
L27E 350N	.7	20.7	16.7	106	.1	18.1	10.1	1105	2.17	5.4	.9	<.5	3.4	24	.2	.2	.3	19	.36	.140	18	14.5	.47	375	.075	2	2.40	.014	.15	.2	.05	3.2	.1	<.05	6	<.5
L27E 300N	.2	11.9	10.5	33	.1	11.1	5.8	287	1.67	3.6	.4	.7	4.4	12	.1	.2	.2	13	.26	.031	21	9.5	.45	113	.039	3	1.23	.007	.19	.2	.01	2.2	.1	<.05	4	<.5
RE L27E 300N	.3	12.4	10.4	33	.1	11.2	6.3	302	1.66	3.7	.4	<.5	4.3	12	.1	.2	.2	15	.27	.031	21	11.3	.45	119	.062	3	1.26	.007	.19	.2	.02	2.5	.1	.06	3	<.5
L27E 250N	.5	12.8	11.7	67	<.1	10.7	6.1	597	1.61	4.0	.4	.6	2.2	22	.1	.2	.2	14	.48	.072	16	10.0	.43	178	.042	5	1.60	.008	.19	.1	.03	2.0	.1	<.05	4	<.5
L27E 200N	.5	13.3	10.7	42	<.1	10.6	5.9	541	1.59	3.1	.4	<.5	2.6	20	.1	.3	.2	14	.43	.061	18	10.1	.41	183	.046	4	1.46	.009	.22	.2	.02	2.1	.1	<.05	4	<.5
L28E 1000N	.6	19.9	14.2	85	.1	17.0	9.2	1026	2.07	5.0	1.0	.9	.9	34	.2	.3	.2	21	.53	.112	18	12.4	.48	306	.067	3	2.57	.017	.12	.1	.04	2.1	.1	.06	6	<.5
L28E 950N	.9	18.3	18.2	90	.1	15.2	8.5	1042	2.01	6.0	.9	<.5	.8	31	.3	.3	.3	22	.56	.125	16	12.4	.47	308	.060	3	2.66	.015	.11	.2	.07	1.8	.1	.10	7	<.5
L28E 900N	.7	19.0	17.5	161	.1	14.9	8.1	1232	1.90	4.9	.8	<.5	.8	60	.4	.3	.3	19	.67	.129	15	11.1	.43	331	.055	3	2.30	.016	.13	.2	.04	1.8	.1	<.05	6	<.5
L28E 850N	.5	17.8	15.9	58	.1	15.4	8.3	599	2.17	4.6	.7	<.5	5.1	21	.1	.3	.3	20	.32	.044	22	14.0	.53	170	.062	2	1.99	.009	.26	.2	.02	3.3	.1	<.05	5	<.5
L28E 800N	.3	18.3	11.7	48	.1	11.4	6.6	533	1.55	3.8	.3	.8	2.4	49	.1	.2	.2	16	.58	.051	13	10.1	.50	288	.059	4	1.76	.024	.20	.1	.03	2.4	.1	<.05	4	<.5
L28E 750N	.8	17.0	11.9	90	.8	21.7	13.3	817	1.57	6.0	1.2	6.9	2.4	38	.1	.3	.3	15	.41	.239	10	7.5	.21	345	.085	3	2.23	.024	.31	.2	.04	2.5	.1	<.05	5	<.5
L28E 700N	.6	28.4	19.7	343	.1	17.8	8.6	2532	1.50	7.1	.5	1.4	2.0	62	.9	.5	.2	13	.57	.259	10	7.9	.25	970	.062	2	1.76	.015	.13	.1	.06	1.8	.1	<.05	4	<.5
STANDARD DS4	6.8	130.3	31.1	163	.3	35.6	11.8	790	3.20	23.0	6.5	29.9	4.0	27	5.7	5.0	5.0	78	.52	.095	18	167.5	.58	140	.094	2	1.74	.031	.15	4.1	.29	3.7	1.1	.07	6	1.3

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

 Data FA

ACME ANALYTICAL

Sedex Mining Corp. PROJECT MW FILE # A302141 Page 5

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm
G-1	1.1	2.7	2.5	42	<.1	4.3	3.8	499	1.84	<.5	2.7	.5	3.7	66	<.1	<.1	.1
L28E 650N	.5	18.0	16.8	82	.1	17.9	9.2	842	2.21	6.0	1.2	.7	4.6	20	.2	.3	.3
L28E 600N	.7	19.0	22.7	77	.1	16.3	8.7	840	2.29	5.8	1.0	.8	3.2	23	.2	.3	.3
L28E 550N	.6	18.4	14.8	74	.1	14.6	8.4	818	2.06	5.7	1.0	.6	1.8	28	.1	.3	.2
L28E 500N	.6	35.8	36.0	79	.1	18.1	8.9	781	2.31	8.3	.9	<.5	4.5	20	.3	1.6	.3
L28E 450N	.6	16.7	19.3	103	.1	13.0	7.6	1011	1.85	4.9	.7	<.5	2.9	20	.2	.3	.3
L28E 400N	.3	13.8	10.9	32	<.1	11.4	5.9	261	1.73	3.9	.6	.5	4.9	10	.1	.3	.2
L28E 350N	.4	16.0	14.4	53	.1	10.6	6.8	552	1.72	4.6	.3	<.5	2.6	22	.2	.3	.2
L28E 300N	.4	15.8	10.4	45	<.1	10.9	6.1	543	1.62	3.4	.3	.9	1.9	21	.2	.2	.2
L28E 250N	.5	13.7	11.3	43	.1	11.7	6.2	804	1.77	3.4	.6	<.5	2.4	24	.1	.2	.2
L28E 200N	.5	13.4	12.2	51	<.1	9.9	5.3	553	1.65	3.4	.5	.8	2.6	27	.2	.2	.2
L29E 1000N	.9	9.9	14.8	98	.1	12.8	4.9	1150	1.44	3.8	.5	<.5	2.3	24	.2	.2	.2
L29E 950N	.6	14.6	15.5	63	<.1	16.4	7.9	799	2.12	4.0	.9	.8	4.7	22	.2	.3	.3
L29E 900N	.7	14.5	17.5	93	<.1	13.8	6.9	1010	2.04	4.6	.9	.6	2.9	27	.2	.3	.2
L29E 850N	.6	18.7	13.8	96	.1	14.3	8.0	1070	2.06	4.4	1.0	.5	1.1	29	.2	.2	.2
L29E 800N	.6	17.9	17.6	97	.1	14.4	7.6	1137	1.99	5.3	.8	<.5	2.0	28	.2	.3	.3
L29E 750N	.4	21.2	16.1	61	.1	13.2	7.5	652	1.98	5.3	.3	.5	3.5	16	.1	.3	.3
L29E 700N	.7	18.9	20.6	129	<.1	16.1	9.2	1291	2.11	6.6	.8	<.5	2.9	23	.2	.3	.3
L29E 650N	.1	14.8	5.9	46	.1	5.0	3.4	602	.83	1.7	.2	.8	.3	278	.2	.2	.1
L29E 600N	.2	18.6	10.8	64	.1	8.6	5.0	643	1.33	3.3	.4	.8	.9	125	.3	.3	.2
L29E 550N	.5	14.2	19.4	80	.1	14.4	8.1	853	2.01	4.9	1.1	<.5	3.4	37	.2	.3	.3
L29E 500N	.4	17.1	10.3	76	.1	13.0	6.3	639	1.69	3.4	.7	.7	3.1	26	.1	.1	.2
L29E 450N	.4	21.1	14.1	67	.1	14.2	8.6	861	1.94	4.6	.5	.6	3.2	24	.1	.3	.3
L29E 400N	.4	18.5	14.9	54	<.1	15.7	7.7	754	2.05	4.1	.8	.9	4.0	26	.1	.2	.2
L29E 350N	.3	22.1	18.4	49	.1	14.0	8.0	504	2.00	6.1	.4	2.0	4.2	15	.1	.6	.3
L29E 300N	.3	17.4	18.1	56	<.1	10.3	6.3	709	1.51	3.6	.2	<.5	2.7	37	.3	.3	.2
RE L29E 300N	.4	16.8	19.9	49	<.1	10.2	6.1	690	1.55	3.4	.2	<.5	2.6	36	2	.3	.2
L29E 250N	.5	15.2	14.0	73	.1	13.9	7.3	701	1.86	6.4	.7	.6	3.2	21	.1	.3	.2
L29E 200N	.6	20.7	14.9	82	.1	14.2	7.8	1055	1.92	5.0	.9	<.5	2.0	37	.1	.2	.3
L30E 1000N	.3	14.7	13.1	44	<.1	12.7	7.0	564	1.81	4.2	.4	.6	4.3	11	.1	.3	.2
L30E 950N	.4	13.8	13.1	61	<.1	14.2	7.7	533	1.87	4.0	1.0	.5	5.0	16	.2	.2	.2
L30E 900N	.9	21.6	16.8	120	.7	21.2	6.8	536	1.93	5.8	.6	<.5	3.4	27	.4	.4	.3
L30E 850N	.4	18.9	16.6	90	.1	13.8	7.8	935	1.81	6.2	.7	.6	3.2	33	.3	.2	.3
L30E 800N	.5	18.6	19.4	77	.1	11.9	6.4	1043	1.58	4.7	.6	<.5	1.2	28	.3	.3	.2
L30E 750N	.5	19.4	27.5	82	.1	16.6	8.1	932	2.09	6.5	.7	<.5	3.0	22	.3	.3	.3
STANDARD DS4	6.8	124.4	32.3	161	.3	34.7	11.9	802	3.24	22.7	6.9	28.9	4.2	28	5.5	5.0	5.2

SAMPLE#	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	39	.65	.085	8	22.7	.55	202	.129	3	.86	.063	.39	.9	<.01	2.0	.3	.09	5	<.5
L28E 650N	22	.28	.077	18	11.5	.47	278	.085	4	2.51	.019	.18	.2	.02	3.2	.2	<.05	5	<.5
L28E 600N	22	.31	.068	19	11.6	.48	331	.079	3	2.39	.014	.15	.2	.04	3.2	.1	<.05	7	<.6
L28E 550N	22	.40	.087	18	10.4	.44	288	.066	4	2.30	.016	.15	.2	.05	2.7	.1	<.05	6	<.5
L28E 500N	20	.33	.057	19	12.1	.55	247	.065	4	2.07	.012	.21	.2	.06	3.4	.1	<.05	5	<.5
L28E 450N	16	.39	.111	13	10.1	.46	388	.062	4	1.95	.013	.14	.1	.08	2.4	.1	<.05	5	<.6
L28E 400N	16	.20	.032	18	9.7	.47	123	.048	2	1.44	.008	.19	.2	.04	2.3	.1	<.05	4	<.5
L28E 350N	13	.46	.079	16	9.5	.46	172	.036	5	1.41	.010	.22	.2	.03	1.9	.1	<.05	4	<.5
L28E 300N	14	.51	.057	16	8.4	.43	185	.040	4	1.52	.010	.21	.2	.04	1.8	.1	<.05	4	<.5
L28E 250N	17	.40	.064	17	9.6	.44	226	.052	3	1.84	.011	.23	.2	.04	2.3	.1	<.05	5	<.5
L28E 200N	14	.40	.051	16	8.2	.43	227	.052	4	1.79	.012	.24	.3	.03	2.1	.1	<.05	5	<.6
L29E 1000N	13	.34	.138	10	7.6	.28	347	.071	2	2.01	.021	.13	.2	.02	1.9	.1	<.05	5	<.5
L29E 950N	20	.33	.033	17	11.5	.43	333	.093	3	2.47	.017	.22	.3	.02	3.3	.1	<.05	6	<.5
L29E 900N	21	.34	.066	17	10.3	.42	385	.086	3	2.43	.017	.21	.2	.03	3.0	.1	<.05	7	<.5
L29E 850N	20	.43	.114	18	11.2	.44	364	.068	3	2.72	.019	.13	.1	.03	2.2	.1	.06	7	<.6
L29E 800N	19	.50	.121	17	11.4	.43	422	.070	3	2.27	.014	.14	.2	.03	2.7	.1	<.05	6	<.5
L29E 750N	15	.60	.060	18	12.1	.57	195	.041	4	1.43	.009	.23	.3	.02	2.2	.1	<.05	4	<.5
L29E 700N	19	.41	.129	19	13.0	.48	327	.069	4	2.18	.014	.21	.2	.03	2.8	.1	<.05	6	<.5
L29E 650N	6	7.80	.076	6	4.6	2.43	273	.024	7	1.00	.035	.14	<.1	.01	.7	<.1	.17	3	.7
L29E 600N	11	5.15	.077	10	7.8	.91	259	.045	6	1.66	.029	.17	.1	.03	1.7	.1	.17	4	.5
L29E 550N	20	.42	.048	15	11.2	.42	336	.087	3	2.64	.025	.14	.1	.03	3.1	.1	.07	6	<.5
L29E 500N	16	.34	.106	13	9.9	.35	301	.080	4	2.20	.025	.23	.1	.02	2.8	.1	<.05	6	<.5
L29E 450N	15	.59	.065	18	11.5	.51	211	.050	3	1.62	.014	.16	.1	.03	2.9	.1	.06	4	<.5
L29E 400N	17	.36	.036	18	11.7	.44	270	.085	3	2.41	.020	.18	.2	.03	3.5	.1	<.05	6	<.6
L29E 350N	15	1.02	.062	17	13.0	.79	87	.032	3	1.11	.008	.15	.2	.02	2.5	.1	.08	3	<.6
L29E 300N	13	.95	.054	15	9.5	.48	199	.042	4	1.27	.013	.23	2	.03	2.2	.1	.09	4	<.6
RE L29E 300N	12	.98	053	13	9.2	.46	189	.040	4	1.31	.012	.24	.2	.02	2.0	<.1	<.05	3	<.5
L29E 250N	17	.33	.080	17	11.5	.43	251	.073	3	2.09	.018	.19	.2	.03	2.8	.1	.06	6	<.5
L29E 200N	18	.54	.101	16	11.4	.43	303	.067	4	2.23	.019	.17	.2	.05	2.8	.1	.08	6	<.5
L30E 1000N	12	.20	.029	19	10.2	.46	158	.050	3	1.46	.009	.23	.2	.02	2.7	.1	<.05	4	<.5
L30E 950N	15	.26	.033	20	12.3	.56	153	.049	2	1.57	.032	.19	.2	.01	2.5	.1	<.05	4	<.5
L30E 900N	17	.25	.139	14	11.3	.36	382	.072	3	2.17	.017	.13	.1	.02	1.6	.1	<.05	6	<.5
L30E 850N	17	.64	.136	15	11.0	.48	395	.078	3	2.24	.026	.12	.2	.04	2.7	.1	<.05	6	<.6
L30E 800N	15	.59	.115	14	9.4	.37	305	.051	2	1.77	.017	.14	.2	.02	1.8	.1	<.05	5	<.5
L30E 750N	17	.47	.073	18	12.7	.50	298	.064	2	1.90	.014	.17	.2	.03	2.8	.1	<.05	6	<.6
STANDARD DS4	78	.52	.093	18	166.1	.58	148	.098	2	1.80	.032	.16	3.9	.29	3.8	1.2	<.05	6	1.5

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

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ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.2	4.5	2.2	40	<.1	4.7	4.3	528	1.72	<.5	2.5	<.5	3.7	67	<.1	<.1	.1	35	.52	.081	8	30.8	.56	216	.131	2	.87	.070	.41	.7	<.01	1.8	.3	<.05	4	<.5
L30E 700N	.6	17.0	15.6	60	.1	15.8	7.6	619	2.10	5.2	.9	.7	3.4	22	.1	.3	.2	18	.32	.058	18	12.5	.46	300	.071	2	2.28	.016	.15	.1	.03	3.0	.1	<.05	6	<.5
L30E 650N	.4	16.5	15.9	73	.1	15.2	8.6	861	2.18	4.6	1.0	1.3	4.4	24	.1	.3	.3	20	.29	.049	19	13.4	.46	362	.095	3	2.77	.020	.16	.2	.02	3.4	.1	<.05	7	<.5
L30E 600N	.5	17.4	15.0	81	.1	16.1	8.4	928	2.10	5.7	.9	.8	2.1	22	.1	.3	.3	19	.31	.103	18	12.8	.45	304	.075	3	2.48	.017	.15	.2	.03	2.6	.1	<.05	6	<.5
L30E 550N	.4	16.2	12.6	76	.2	14.8	7.3	857	1.81	6.5	.8	.6	2.9	20	.1	.2	.2	19	.35	.117	17	11.6	.44	292	.077	3	2.36	.021	.13	.2	.01	2.6	.1	<.05	6	<.5
L30E 500N	.4	16.9	13.5	62	.1	13.1	7.8	805	1.88	4.8	.9	<.5	3.7	21	.1	.3	.2	19	.23	.052	17	11.1	.42	283	.076	3	2.24	.018	.16	.2	.02	2.9	.1	<.05	5	<.5
L30E 450N	.8	13.0	15.1	84	.1	15.0	7.5	866	1.99	4.3	.9	.6	2.2	18	.1	.2	.3	17	.28	.118	17	11.5	.43	316	.087	3	3.01	.016	.21	.2	.03	2.9	.1	<.05	7	<.5
L30E 400N	.5	15.4	12.8	66	.1	13.9	7.7	743	1.95	4.6	1.0	.6	2.7	26	.1	.3	.2	19	.37	.059	19	11.6	.42	319	.072	3	2.26	.016	.12	.2	.02	2.8	.1	<.05	6	<.5
L30E 350N	.8	21.4	16.1	82	.1	16.2	8.6	1074	2.11	5.0	.9	<.5	3.2	28	.1	.3	.3	19	.49	.076	20	13.2	.49	344	.084	3	2.49	.016	.16	.2	.05	3.3	.1	<.05	6	<.5
L30E 300N	.5	14.6	12.2	67	<.1	10.9	6.5	614	1.57	6.2	.6	<.5	3.1	27	.1	.3	.2	13	.58	.088	14	9.4	.40	254	.039	4	1.46	.010	.14	.1	.03	1.6	<.1	<.05	4	<.5
L30E 250N	.7	19.6	14.0	78	.1	12.6	7.2	1135	1.68	4.3	.8	<.5	.5	31	.2	.3	.2	16	.55	.142	15	9.8	.39	311	.043	4	2.25	.016	.15	.1	.04	1.3	.1	<.05	6	<.5
L30E 200N	.7	20.8	16.9	70	.1	17.1	8.9	1093	2.13	5.2	1.1	<.5	2.8	34	.2	.2	.2	20	.58	.082	19	12.7	.50	328	.077	4	2.51	.018	.19	.1	.04	3.1	.1	<.05	6	<.5
L31E 1000N	.5	27.5	23.2	91	.1	20.3	12.1	1275	2.47	6.3	.9	1.0	3.7	20	.3	.3	.3	21	.59	.088	23	15.8	.61	357	.086	3	2.59	.016	.23	.1	.06	3.5	.2	.06	6	<.5
L31E 950N	.5	19.8	14.5	82	.1	13.7	8.3	927	1.87	5.1	.8	<.5	2.6	27	.2	.3	.3	16	.45	.091	19	11.3	.50	323	.063	4	2.20	.019	.25	.2	.03	2.6	.1	<.05	5	<.5
L31E 900N	.7	28.1	16.0	89	.1	19.1	10.6	1084	2.18	7.1	1.1	1.0	5.1	27	.1	.3	.3	19	.39	.049	21	12.6	.51	407	.082	4	2.37	.019	.21	.2	.02	3.6	.1	<.05	6	<.5
L31E 850N	.7	17.8	14.4	78	.2	18.4	8.1	951	1.84	6.5	1.0	6.9	2.8	28	.2	.3	.2	17	.27	.114	18	10.5	.39	274	.079	2	2.33	.021	.12	.1	.06	2.6	.1	<.05	6	<.5
L31E 800N	1.0	15.2	14.0	88	.1	17.5	8.1	1067	1.85	5.1	.8	<.5	2.3	19	.2	.2	.2	19	.25	.117	15	11.0	.37	290	.089	3	2.64	.022	.16	.2	.04	2.5	.1	<.05	7	<.5
L31E 750N	.4	19.1	16.5	70	.1	16.5	9.2	959	2.33	5.4	.9	.8	5.0	21	.1	.3	.3	20	.39	.053	22	14.4	.58	316	.092	4	2.75	.018	.24	.2	.03	3.8	.1	<.05	6	<.5
L31E 700N	.4	15.0	21.8	71	<.1	12.8	6.8	1024	1.67	5.2	.5	2.7	3.4	22	.1	.3	.2	14	.35	.044	16	10.4	.43	264	.068	3	1.95	.015	.17	.2	.02	2.7	.1	<.05	5	<.5
RE L31E 700N	.4	15.6	21.7	69	<.1	14.0	6.7	1013	1.66	5.5	.4	.9	3.5	22	.2	.2	.2	15	.34	.045	17	10.0	.43	283	.068	4	1.91	.014	.16	.2	.03	2.7	.1	<.05	5	<.5
L31E 650N	.4	18.3	17.2	75	.1	18.0	8.8	1082	2.15	4.7	.8	.6	3.5	27	.1	.3	.2	19	.51	.053	21	12.9	.55	364	.091	4	2.61	.020	.15	.1	.02	3.7	.1	<.05	6	<.5
L31E 600N	.4	17.2	17.2	72	<.1	17.4	8.6	758	2.26	5.7	.8	1.1	5.5	18	.1	.3	.3	20	.36	.052	22	14.2	.56	228	.088	4	2.57	.016	.20	.1	.03	3.7	.1	<.05	6	<.5
L31E 550N	.3	16.2	20.1	67	<.1	14.7	7.8	855	2.07	4.8	.5	<.5	5.0	19	.2	.3	.3	16	.34	.037	20	12.3	.53	287	.077	3	2.24	.017	.20	.1	.02	3.7	.1	<.05	5	<.5
L31E 500N	.5	12.0	11.2	56	<.1	13.5	6.8	714	1.86	4.3	.7	<.5	4.0	16	.1	.2	.2	17	.20	.053	18	11.4	.43	240	.077	2	2.08	.017	.17	.2	.02	2.8	.1	<.05	5	<.5
L31E 450N	.4	13.2	11.2	54	.1	13.2	6.4	777	1.63	4.0	.6	1.0	2.1	23	.2	.2	.2	16	.40	.083	16	10.2	.40	237	.059	4	1.82	.014	.19	.1	.01	2.0	.1	<.05	4	<.5
L31E 400N	.4	16.5	12.0	48	.1	11.8	6.7	656	1.72	4.5	.4	.9	2.8	19	.1	.2	.2	15	.48	.056	18	11.2	.48	207	.048	4	1.47	.011	.21	.2	.02	2.1	.1	<.05	4	<.5
L31E 350N	.4	15.6	11.6	44	.1	12.9	7.4	630	1.92	4.6	.7	1.2	3.2	18	.1	.3	.2	18	.33	.044	21	10.9	.46	223	.062	2	1.79	.013	.14	.2	.02	2.7	.1	<.05	5	<.5
L31E 300N	.5	19.6	21.3	72	.1	16.3	8.6	1003	2.15	5.4	.9	.8	3.6	22	.2	.3	.3	19	.35	.058	22	12.7	.53	319	.082	2	2.46	.014	.12	.2	.04	3.5	.1	<.05	6	<.5
L31E 250N	.5	19.1	15.0	69	.1	14.0	8.1	1078	1.79	4.6	.6	9.6	1.5	28	.1	.3	.2	17	.64	.086	16	11.0	.44	356	.059	2	2.03	.017	.15	.1	.04	2.3	.1	.10	5	<.5
L31E 200N	.4	14.7	10.2	40	.1	11.9	6.7	604	1.74	4.5	.5	1.8	3.7	16	.1	.3	.2	16	.28	.035	18	10.9	.45	188	.050	3	1.55	.012	.16	.2	.03	2.4	.1	.08	4	<.5
L32E 1000N	.5	16.3	17.5	70	<.1	16.5	8.9	899	2.29	6.4	.8	1.2	4.8	17	.2	.3	.3	20	.29	.055	21	14.5	.50	273	.087	4	2.67	.017	.20	.2	.03	4.0	.1	<.05	6	<.5
L32E 950N	.4	11.7	11.3	39	<.1	9.3	5.8	759	1.55	2.8	.3	<.5	3.4	16	.1	.2	.2	11	.41	.034	19	8.8	.42	170	.037	3	1.12	.007	.18	.2	.03	2.1	.1	<.05	3	<.5
L32E 900N	1.3	32.6	19.4	88	.1	27.8	17.9	1271	2.51	8.8	1.9	1.0	3.9	41	.2	.5	.4	16	.60	.143	18	10.4	.49	296	.086	7	2.51	.025	.20	.1	.03	2.7	.1	<.05	5	<.5
L32E 850N	1.1	21.2	22.3	97	.1	18.1	9.2	1167	2.17	6.6	.8	1.1	1.9	26	.3	.3	.3	20	.48	.117	17	12.3	.49	332	.069	3	2.47	.017	.15	.1	.06	2.6	.1	<.05	6	<.5
L32E 800N	1.0	28.1	20.5	113	.1	17.9	10.5	1510	2.07	6.8	.8	.9	1.6	34	.3	.3	.3	21	.64	.185	17	12.7	.46	338	.069	3	2.38	.022	.17	.2	.06	2.8	.1	.07	6	<.5
STANDARD DS4	6.9	129.7	31.3	159	.3	35.8	12.5	827	3.20	22.7	6.7	27.8	4.0	29	5.3	4.9	4.9	76	.53	.083	18	164.6	.59	147	.102	2	1.78	.033	.18	4.0	.26	3.8	1.1	<.05	6	1.4

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

 Data FA

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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm
G-1	1.3	2.5	2.3	38	<.1	3.7	3.9	483	1.94	<.5	2.6	1.1	4.1	70	<.1	<.1	.1
L32E 750N	.7	22.3	15.3	87	.1	14.7	9.1	1010	2.12	6.1	.8	.6	1.2	26	.2	.3	.3
L32E 700N	.6	21.2	15.8	73	.1	17.3	9.5	982	2.41	7.0	1.0	1.0	2.1	25	.1	.4	.3
L32E 650N	1.7	14.8	13.8	84	<.1	13.5	7.6	1061	1.81	5.5	.6	1.6	2.1	19	.2	.3	.2
L32E 600N	.6	13.7	14.6	86	.1	15.0	7.5	1008	2.03	5.7	.7	<.5	2.6	19	.1	.3	.3
L32E 550N	.3	13.9	17.1	41	<.1	13.2	6.7	356	1.95	5.4	.6	<.5	4.6	8	.1	.4	.2
L32E 500N	.4	13.6	10.7	56	<.1	11.9	6.3	733	1.80	3.9	.5	1.7	3.7	16	.1	.3	.2
L32E 450N	.3	11.0	9.9	39	<.1	11.2	6.3	676	1.80	3.4	.4	.9	4.0	14	.1	.2	.2
L32E 400N	.3	12.7	11.1	56	.1	12.1	5.7	486	1.81	4.3	.5	1.2	4.3	15	<.1	.2	.2
L32E 350N	.4	9.2	9.5	43	<.1	12.0	6.0	583	1.85	3.5	.5	.6	4.2	13	<.1	.2	.2
L32E 300N	.3	11.0	11.0	42	<.1	11.4	6.0	583	1.85	3.9	.5	1.0	4.1	14	.1	.2	.2
RE L32E 300N	.3	12.0	11.5	43	<.1	12.4	6.3	614	1.86	3.9	.5	.6	4.2	14	.1	.3	.2
L32E 250N	.5	12.1	12.1	45	<.1	13.0	6.5	625	1.96	4.0	.6	.7	4.0	17	.1	.2	.2
L32E 200N	.5	12.8	13.7	54	<.1	10.8	6.1	793	1.77	4.0	.3	.5	3.2	26	.2	.3	.2
STANDARD DS4	6.8	129.3	30.6	162	.3	35.7	12.0	782	3.28	23.8	6.5	29.0	3.8	27	5.4	4.9	5.0

SAMPLE#	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	40	.57	.086	8	32.2	.53	187	.130	1	.84	.065	.41	.8	<.01	1.9	.3	<.05	5	<.5
L32E 750N	19	.42	.163	16	11.4	.42	265	.058	3	2.17	.015	.13	.2	.03	2.1	.1	<.05	6	<.5
L32E 700N	23	.37	.088	18	12.6	.49	310	.076	2	2.52	.017	.14	.2	.03	2.8	.2	.07	7	<.5
L32E 650N	14	.31	.253	12	10.3	.36	216	.058	3	1.96	.016	.13	.1	.02	2.1	.1	<.05	5	<.5
L32E 600N	20	.29	.111	14	12.3	.38	307	.079	3	2.37	.024	.13	.1	.04	2.4	.1	<.05	6	<.5
L32E 550N	16	.16	.040	18	11.8	.45	108	.040	1	1.30	.006	.13	.1	.02	2.5	.1	<.05	3	<.5
L32E 500N	15	.28	.049	15	10.4	.39	211	.058	2	1.73	.052	.18	.2	.02	2.5	.1	<.05	5	<.5
L32E 450N	13	.28	.037	17	10.7	.39	158	.054	3	1.59	.010	.22	.2	.02	2.5	.1	<.05	5	<.5
L32E 400N	14	.35	.050	18	10.3	.41	137	.047	3	1.44	.009	.21	.1	.02	2.3	.1	<.05	4	<.5
L32E 350N	15	.19	.040	16	9.8	.37	169	.056	3	1.70	.010	.19	.3	.02	2.4	.1	<.05	4	<.5
L32E 300N	15	.26	.033	17	9.6	.39	172	.053	2	1.61	.010	.19	.2	.02	2.3	.1	<.05	4	<.5
RE L32E 300N	15	.27	.033	18	9.9	.40	177	.055	2	1.64	.011	.20	.2	.02	2.6	.1	<.05	5	<.5
L32E 250N	18	.26	.034	17	10.8	.40	214	.069	2	2.02	.013	.23	.2	.02	2.9	.1	.07	6	<.5
L32E 200N	13	.50	.045	16	9.2	.47	199	.048	6	1.50	.011	.25	.1	.02	2.2	.1	<.05	4	<.5
STANDARD DS4	78	.54	.093	17	167.4	.61	140	.093	2	1.74	.029	.16	4.1	.28	3.8	1.2	.08	6	1.4

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
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GEOCHEMICAL ANALYSIS CERTIFICATE

Sedex Mining Corp. File # A302448
711 - 675 W. Hastings St., Vancouver BC V6B 1N2 Submitted by: Peter Klewchuk

SAMPLE#	Au* ppb
G-1	<.2
LA 0E	<.2
LA 40E	1.0
LA 80E	.2
LA 120E	<.2
LA 160E	<.2
LA 200E	.3
LA 250E	.8
LA 300E	.2
LA 350E	<.2
LA 400E	<.2
LA 450E	.2
LA 500E	<.2
LA 550E	<.2
LA 600E	1.5
RE LA 600E	<.2
LB 300W	.4
LB 275W	1.5
LB 250W	5.7
LB 225W	<.2
LB 200W	<.2
LB 180W	<.2
LB 160W	1.2
LB 120W	<.2
LB 80W	5.0
LB 45W	.3
LB 0W	.8
STANDARD DS5	42.0

AU* BY ACID LEACHED, ANALYZED BY ICP-MS. (15 gm)
- SAMPLE TYPE: SOIL SS80 60C
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 8 2003 **DATE REPORT MAILED:** July 18/03 **SIGNED BY**.......D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data FA

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Sedex Mining Corp. PROJECT MW File # A302812 Page 1

711 - 675 W. Hastings St., Vancouver BC V6B 1N2 Submitted by: Peter Klewchuk

SAMPLE#	Au* ppb
G-1	.7
LC 0S	.5
LC 25S	.8
LC 50S	.6
LC 75S	.4
LC 100S	<.2
LC 175S	.7
LC 200S	.8
LC 225S	1.2
LC 275S	.7
LC 325S	62.4
LC 350S	.8
LC 375S	.6
LC 400S	.7
RE LC 400S	.3
LC 425S	.6
LC 450S	.3
LC 475S	.7
LC 500S	1.0
LC 525S	1.2
LC 550S	.2
LC 575S	3.8
LC 625S	3.5
LC 650S	.3
LC 675S	9.9
LC 700S	58.7
LC 725S	1.7
LC 750S	2.0
LC 775S	<.2
LC 825S	.7
LC 850S	.7
LC 875S	.2
LC 900S	.4
LC 950S	.7
LC 975S	1.3
STANDARD DS5	42.0

AU* BY ACID LEACHED, ANALYZED BY ICP-MS. (15 gm)
- SAMPLE TYPE: SOIL SS80 60C

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 23 2003 DATE REPORT MAILED: Aug 1/03 SIGNED BY..........D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data FA

SAMPLE#	Au* ppb
G-1	.2
LC 1000S	.6
LC 1025S	2.0
LC 1050S	1.1
LC 1075S	.7
LC 1100S	.7
LC 1125S	.7
LC 1150S	.4
LC 1175S	1.4
LC 1200S	.6
LC 1225S	.4
LC 1250S	.8
LC 1275S	.4
LC 1300S	.8
LC 1325S	.7
LC 1350S	1.3
RE LC 1350S	1.4
LC 1375S	.5
LC 1400S	.9
LC 1425S	1.2
LC 1450S	3.6
STANDARD DS5	44.7

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data ✓ FA ___

Appendix 3 Description of Rock Samples

MW 50	Intrusive? Narrow quartz-carbonate veins with some limonite.
MW 51	Liesegange breccia float. Sericite and limonite -altered. Rubble from gas line excavation.
MW 52	North side of pipeline. Same as above. More quartzite.
MW 53	Narrow quartz veins with vugs and limonite.
MW 54	Quartzite rubble - narrow quartz veins with hematite and limonite.
MW 55	Same as above.
MW 56	Liesegange altered, some pyrite gashes, narrow quartz veins with limonite.
MW 57	Angular pieces of quartzite float. Narrow vuggy quartz veins with limonite.
MW 58	Brecciated grey-black siltstone. Narrow quartz veins with limonite and carbonate.
MW 59	Same as above.
MW 60	Brecciated silicified silts and quartzite. Some narrow carbonate veins with weak limonite.
MW 61	Same as above. Stronger alteration.
MW 62	Narrow (½ cm) quartz veins. Some vugs with weak limonite staining.
MW 63	Narrow NW trending QV in quartzite. Some vugs, patchy limonitic staining.
MW 64	Weak breccia. Same as 61. Quartzite unit contacting silts.
MW 65	Weak breccia. Narrow quartz vein.
MW 66	Float E-W to ENE QV.
MW 67	Similar to 66, minor PbS.
MW 68	Similar to 68.
MW 69	10-15 cm ENE trending QV, steeply south dipping.
MW 70	Thin ENE trending QV.
MW 71	Thin ENE trending QV.
MW 101	3845E 0149N Weak limonitic breccia, fracture-parallel 2-3 cm wide QV, fine dissem. pyrite on fractures.
MW 102	Trench 2. Limonitic fracture at 045/36SE in thin & med bedded silts and argillites.
MW 103	Trench 3. Fault zone at 055/60SE. Narrow zone of clay gouge and limonitic rubble.
MW104	Trench 3. Brecciated dark blue-gray argillite; fractures coated with limonite
MW 105	Trench 3. Similar limonite breccia in blue-gray argillite. No obvious quartz veins - may be very thin QV.
MW106	Trench 3. 50 cm chip sample across narrow fault zone. Limonitic, brecciated yellow-orange-gray, mottled. Darker reddish brown limonite seams, few colloidal-looking QV, irregular, wavy.
MW107	Trench 3. Limonitic breccia at west contact of felsic dike.
MW108	Trench 3. Limonite breccia from east side of felsic dike
MW109	Trench 3. Possible felsic dike. White to light gray, fine to med. grained, massive but with limonite-coated fractures. Representative sample of dike material.
MW110	Trench 4. Limonite breccia in blue-gray argillite. Grab sample.
MW111	Trench 5. Grab of poorly exposed limonite breccia.
MW112	Trench 5. 50 cm chip sample. Limonitic, brecciated quartzites.

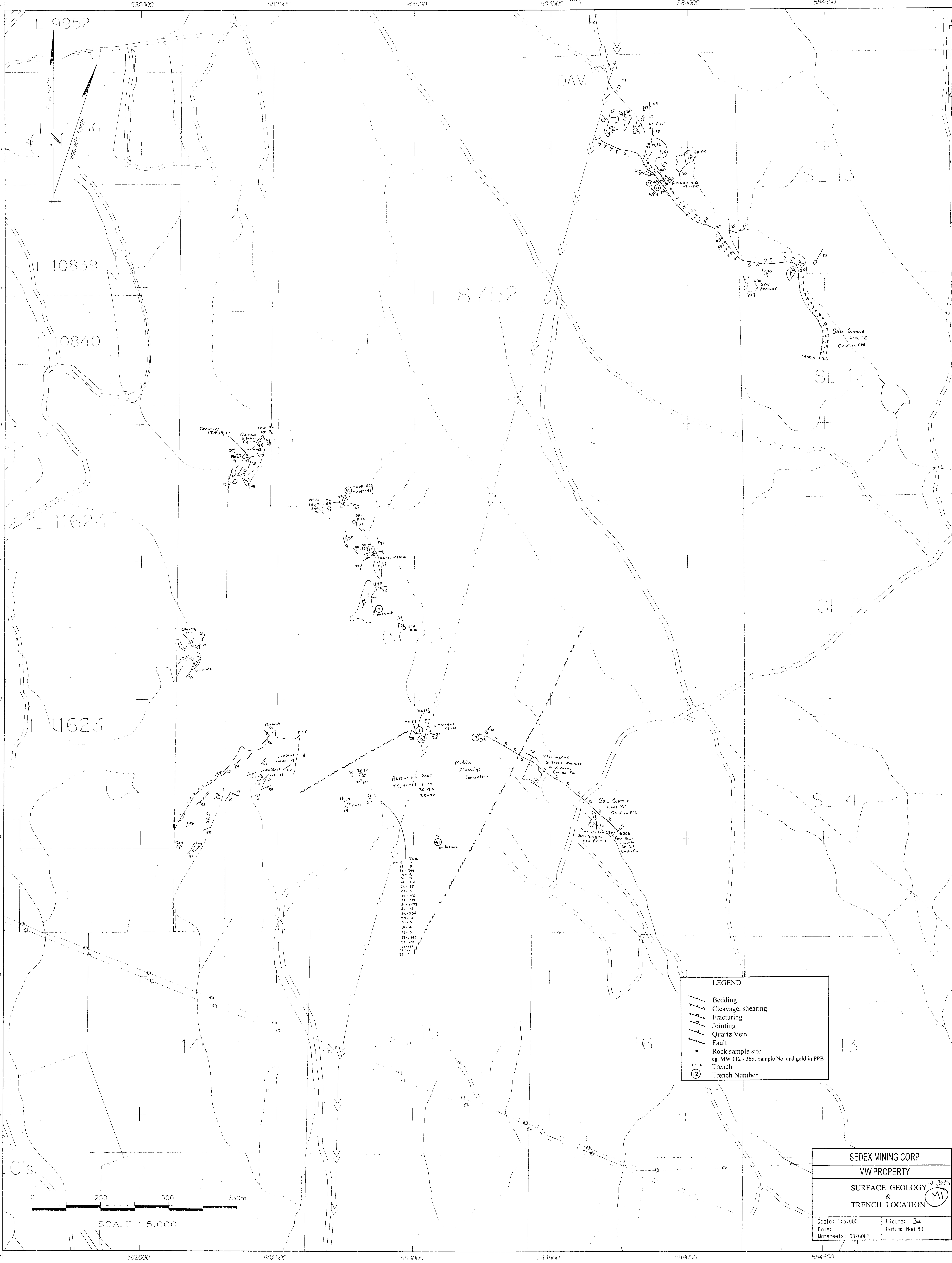
MW113	Trench 5. Limonitic seam - narrow shear, at 060/83SE.
MW114	Trench 5. Limonitic fractures at 141/87N (roughly parallel to trench). Argillic-altered sediments - gritty, like felsic dike material.
MW115	Trench 6. Ochre red fault breccia at 040/20SE, within a fairly 'dry' looking fault zone.
MW116	Trench 6. Grab of 2-3 cm banded QV at 043/60SE.
MW117	Trench 6. Grab of brecciated quartzite with limonitic fractures.
MW118	Trench 6. Limonite / manganese coated fractures - local more intense alteration in much wider, weaker breccia.
MW119	Trench 6. Grab of brecciated seds with NW oriented limonitic fractures at 130/75-80S.
MW120	Trench 5. (Extended west end of trench.) 30 cm chip sample on 25-40 cm wide quartz vein at 029/48SE. Vuggy, rusty to just weakly rusty quartz. Local strong limonite and manganese.
MW121	Trench 5. Mn and limonite -rich 20 cm wide part of same QV.
MW122	Trench 5. 10-15 cm limonitic shear immediately east of QV, at 140/42SW. Not obvious if the shear is related to or offsets quartz vein.
MW123	Trench 5. Poorly exposed fault with gouge at base of trench, at 145/65SW. Grab sample of fault gouge with some pink hematite.
MW124	Trench 5. Limonite breccia with thin QV.
MW125	Trench 7. Grab of narrow vuggy QV, 1-2 cm wide, at 150/70SW.
MW126	Trench 7. Grab of limonitic brecciated quartzites; may be some thin QV. Sample is within a larger breccia system.
MW127	Trench 7. Shallow fault zone ~15 cm wide, at 130/25NE, within larger breccia.
MW128	Trench 7. Grab of quartz vein. 4.5 m from SE end of trench.
MW129	Trench 8. Altered quartzites with limonite and thin quartz veins. Sample 2-3 m from NW end of trench, of flat (105/15S) and NW (142/65S) QV; in altered quartz vein breccia.
MW130	Trench 8. QV at 3.2 m from NW end of trench, at 139/85SW. Very rusty, crumbly, rodded quartz vein ~ 5 cm wide.
MW131	Trench 8. At 4.3 m from NW end of trench; grab sample of wavy, limonitic seam immediately below gravel overburden. 088/82S.
MW132	Trench 8. Limonitic seams at 074/78S. Some gritty, poorly developed quartz.
MW133	Trench 9. 3 cm wide very rusty, vuggy QV on NW fractures (142/84-90NE). 2.5 m from NW end of trench.
MW134	Trench 10. Grab of limonitic breccia, mostly argillite. Orange and pink limonite.
MW135	Trench 10. 60 cm chip of more fractured zone, possible fault, at 040/55SE. Seams of yellow, orange, pink and red limonite. 8.8 m from north end of trench.
MW136	Trench 10. Grab of yellow and reddish 'ochre-like' limonite. Seams are up to 10 cm wide, at 040/55SE. 8.8 m from north end of trench.
MW137	Trench 10. 3 cm wide QV within larger 'Ochre' fault zone. 11 m from north end of trench.
MW138	Trench 10. Chip across ~75 cm of 'Ochre' fault zone; yellow, red and white clay gouge with minor QV (MW137) and fractured argillite.
MW139	Trench 11. Near pipeline. Grab of very weakly limonitic fault breccia. Dry type of breccia, no obvious fabric in trench.

MW140	Trench 15. 50 cm chip across quartz vein 062/50NW. (Previous surface grab was 10 g). This is a 'cross-cutting' quartz vein as most ENE structure seen is SE dipping.
MW141	Trench 16. North of old DDH K-14. Grab of 10-15 cm wide QV at 110/40SE. Vuggy QV with abundant reddish limonite.
MW142	Trench 16. Grab of limonitic fractures, some with clay-limonite gouge.
MW143	Trench 17. 20 cm QV at 082/68S.
MW144	Trench 18. Grab sample of thin QV in argillite. Extension of vein MW143. Very minor limonite, no obvious sulfides.
MW145	Trench 19. Limonitic fractures at 170/70W, with very thin QV. Sericitic and dolomitic(?) altered seds.
MW146	Trench 19. Vuggythin QV. Grab off trenched material. Crystalline, vuggy.
MW147	Trench 19. Thin QV ~2 cm wide, at 078/68S. Very abundant PbS.
MW148	Trench 19. Grab of more massive quartz, some quartz vein breccia, py and PbS.
MW149	Trench 19. Quartz vein breccia. Coarse, wavy, vuggy, rusty, lensey anastomosing veins. No sulfides noted.
MW150	Sericite (and dolomite?) -altered QV breccia. Vuggy quartz veins. No sulfides noted.
MW151	Trench 19. 2 m chip sample across limonitic quartz vein breccia, from north side of quartz vein to clay seam. 004/68W fracturing at north end of sample.
MW152	Trench 19. Grab of thinner 145° QV in immediate footwall zone of larger quartz vein. Very close to MW149 sample.
MW 153	Trench 23. 70 cm chip across yellow-brown-orange limonitic fault breccia and gouge. Mostly fragments of sediment with no obvious QV.
MW154	Trench 23. 20 cm wide fault zone ~3 m to north of MW153. 060/68N. Darker brown limonitic breccia; fragmented seds with strong limonite on fractures.
MW155	Trench 24. Grab of more intense limonite alteration, sheared at 071/74N, mostly argillite, within local stronger fracture zone.
MW156	Trench 24. Grab of 080/90 QV; vuggy, granular, reddish limonitic, hematitic.
MW157	Trench 26. Grab of minor fault zone at 060/50NW. Limonitic fragments and fault gouge.
MW158	Trench 27. Grab of altered limonitic quartzite from trench.
MW159	Surface sample of altered quartzites (near trench 28), with irregular quartz veins. QV have a few vugs,medium brown-orange limonite like weak iron carbonate weathering.
MW160	Surface sample; grab from outcrop of brown-orange-pink limonitic-altered quartzite and irregular QV. QV are rusty with leached sulfide of Fe carbonate (?).
MW161	Surface sample, grab from outcrop. Similar to MW160.
T30-01	Goethite-rich zone with Mn,~1 cm wide, in silty argillite.
T30-02	Limonite and argillic-altered, Mn-stained silty argillite. Composite sample over 30 cm.
T30-03	15 cm composite sample. Fractured, limonite and Mn-altered quartzite, or silicified siltstone.
T30-04	Same as 03. A grab of more limonitic material.
T30-05	Same as 03 and 04.

T30-06	Clay gouge zone. Composite limonite zones with Mn.
T30-07	060° zone, narrow breccia, good limonite. Dips steeply west. Abundant Mn on fractures.
T30-08	Different zone, similar to 07.
T30-09	Brecciated siltstone. Limonite and Mn stained fractures.
T30-10	Same as 09. More argillic alteration, less iron.
T30-11	Same as 09.
T30-12	More limonitic breccia, abundant Mn.
T30-13	Liomonitic breccia (fairly weak), in siltstone.
T30-14	Brecciated, argillic-altered siltstone, some more intense limonite.
T30-15	Limonite-rich brecciated siltstone.
T30-16	Same as 15.
T30-17	Same as 15.
T31-01	Weak breccia in quartzite, liesegange stained / weathered, some limonite.
T31-02	Quartz vein. Vuggy with limonite and Mn. White bull quartz.
T31-03	Very good limonite-altered quartzite. Liesegange.
T31-04	Same as 03.
T31-05	Less intensely brecciated; micro veins with fractures, limonitic with Mn.
T31-06	More argillic, favourable-looking breccia with limonite and Mn.
T31-07	Same as 06.
T31-08	Weaker looking zone in argillic siltstone, some Mn and limonite on fractures.
T31-09	Vuggy quartz with limonite and red hematite; good looking alteration.
T31-10	Red zone with narrow quartz veins; abundant limonite.
T31-11	Good looking breccia; quartz with vugs, abundant limonite.
T31-12	Limonitic vein with quartz in liesegange-stained breccia.
T-31-13	Less altered breccia, some limonite and Mn.
T32-01	Quartz breccia with limonite and manganese in black argillaceous siltstone.
T32-02	Vuggy quartz vein breccia with limonite and manganese.
T32-03	Composite of 3 & 4 cm wide QV; vuggy with limonite.
T32-04	Quartz breccia with limonite and manganese, argillic alteration.
T32-05	NW (120°) trending limonite rich 2 cm QV.
T32-06	NW (120°) trending limonite rich 1 cm QV.
T32-07	Quartz breccia zone, vuggy, in silty argillite.
T32-08	NW trending limonite and Mn rich QV in argillic alteration.
T32-09	Series of NW trending QV with limonite and Mn.
T32-10	Composite of 4 narrow NW trending veins spread across 1 m, with limonite and Mn.
T32-11	Quartz breccia zone. Limonite and Mn. Narrow vuggy veins.
T32-12	Vuggy NW QV with quartz breccia and limonite. 20 cm wide.
T32-13	Quartz vein and breccia, 15 cm wide. Limonite, vugs and Mn.
T32-14	Limonite & Mn rich gouge zone, some quartz; crushed zone.
T32-15	Brecciated, silicified(?) Siltstone. Small vuggy QV, limonite and MN.
T33-01	1 cm wide NW trending QV, steeply east-dipping. Vuggy with limonite and Mn.

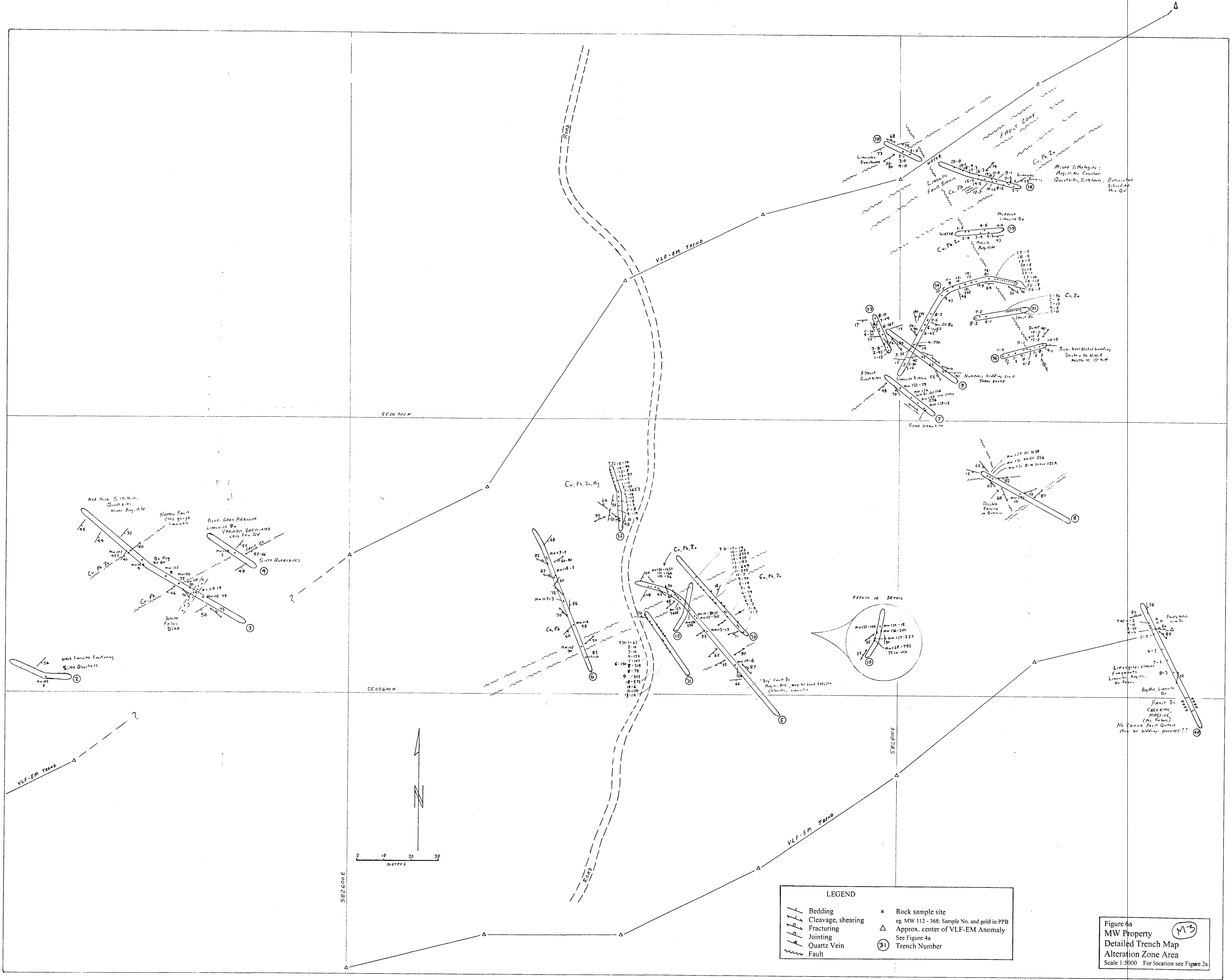
T33-02	Similar to 01, different QV.
T33-03	Same as above. (May be 01 vein, 3 m along strike to north?).
T33-04	Same as above. Veins appear to pod out into small breccia zones. Pink hematite.
T33-05	Similar to above, with pink hematite coloration
T33-06	East-west 3 cm wide QV. Flat north dip. Vugs and limonite. With breccia chips and argillite partings. Could be an 'older' vein.
T33-07	NW QV, steep SE dip.
T33-08	Black argillite, some rusty zones. A little vuggy. 'Common' looking.
T34-01	Liesegange altered, weathered siltstone with narrow vuggy, limonitic quartz veins.
T34-02	Rotten, argillic-altered siltstone, argillite. Weak limonite, no quartz.
T34-03	Vuggy, limonitic 160° 1 cm QV in liesegange altered siltstone.
T34-04	East-west QV in black argillite; vuggy with Mn and limonite. ~1 cm wide.
T34-05	1 cm wide NW QV with vugs, limonite.
T34-06	Same as 05
T34-07	Narrow QV in breccia zone. Vuggy, limonitic, liesegange altered.
T34-08	Quartz vein breccia in quartzites. 30 cm composite.
T34-09	50 cm chip. Liesegange-altered silts, thin QV.
T34-10	Breccia with narrow QV, limonite and Mn.
T34-11	10 cm NW QV. Vugs & limonite.
T34-12	20 cm chip. Same zone as above. Limonite and vugs.
T34-13	Breccia vein material. Some vugs, limonite and Mn.
T34-14	Liesegange breccia, vugs. Abundant limonite and Mn.
T34-15	Mn rich clots in liesegange siltstone.
T34-16	Fault zone; limonitic, argillic quartz chips. 0.5m.
T34-17	Fault zone; 1.2 m chip, same as 16.
T34-18	Fault zone; 0.3m, limonite rich.
T34-19	Fault zone; 0.75m, quartz and limonite.
T-34-20 to 26	Main fault zone; rubbly, argillic alteration with quartz, limonite, shearing. Samples ~ 1.0m each. Fault zone includes clay zones and NW striking limonitic QV.
T35-01	0.70m chip of limonite rich fault zone.
T35-02	0.70m chip. Similar to 01, limonitic gouge zone.
T35-03	0.8m chip. Alteration not as strong as 01 and 02 above.
T35-04	1.5m chip. Liesegang altered seds, some narrow QV.
T35-05	0.6m chip. Similar to 04.
T35-06	Liesegange siltstone. 1cm QV, vugs and limonite.
T35-07	Liesegange seds, 30cm composite. Mn and limonite.
T35-08	Mn rich argillic zone. Some limonite and liesegange.
T36-01	Brecciated seds, argillic altered with micro QV, limonite and Mn.
T36-02	Same as above.
T36-03	Same as above.
T36-04 to 09	Varying amounts of narrow crush zones soaked with limonite. Narrow limonitic veins (reddish and orange limonite). Different types of clay alteration. Argillites are phyllitic with slickensides on fracture surfaces.

T36-10	Grab sample off pile. Quartzite breccia with limonite.
T36-11	" Same as above.
T36-12	" Same as above
T36-13	Narrow crush breccia. 40° trend, abundant limonite.
T37-01	Narrow quartz-carbonate vein 'zone'. 040°/NW dip. Some limonite, carbonate and Mn on fractures.
T38-01	Altered limonitic quartzite. Abundant sericite.
T38-02	Limonite and Mn rich breccia.
T38-03	Narrow Mn and limonite rich zone at 078/35S.
T38-04	Narrow quartz vein in quartzite. Limonite and Mn. Near sample 02.
T38-05	Altered quartzite between argillite-siltstone beds. Very vuggy, limonitic.
T38-06	Brecciated quartzite with limonite and vugs.
T38-07	Crushed quartzite, abundant limonite.
T38-08	Brecciated quartzite and siltstone. Sericite and limonite alteration. Possible very thin QV.
T38-09	"
T38-10	"
T38-11	Limonitic breciated siltstone and quartzite.
T38-12	"
T38-13	"
T38-14	No description.
T38-15	Narrow quartz vein with limonitic, brecciated quartzite 130°/dip NE.
T38-16	Brecciated quartzite, vuggy, limonitic.
T38-17	Limonitic altered zones in argillic siltstone.
T38-18	Same as 17.
T38-19	Altered quartzite. Vugs and limonite.
T38-20	Altered quartzite. Few small vugs, limonite.
T38-21	Vuggy altered quartzite. Few microveinlets of quartz. Sericite and limonite.
T39-01	Altered quartzite. Some microveining. Limonite and Mn.
T39-02	Vuggy quartzite with limonite and Mn.
T39-03	Limonite altered siltstone, some breccia and crushing, Mn.
T39-04	"
T39-05	"
T40-01	Limonitic breccia zone.
T40-02	Brecciated siltstone. Liesegange, limonite, vugs.
T40-03	Limonitic NW fracture zone.
T40-04	Limonitic, vuggy fracture zone at 065°/N dip.
T40-05	138°/steep NE limonitic breccia zone in siltstones. Narrow zone.
T40-06	Very argillic, bleached siltstone. Stronger zones of limonite veining. Some Mn.
T40-07	"
T40-08	"



L 9952
True North
Magnetic North
N
DAM
SL 13
SL 12
SL 5
SL 4
L 10839
L 10840
L 11624
L 11623
L 8762
14
15
16
13
C's.
Soil Contour Line 'C' Gold in PPB
Soil Contour Line 'A' Gold in PPB
Alteration Zone Trenches 1-10 30-36 38-40
Middle Aldridge Formation
582000
582500
583000
583500
584000
584500
5503000
5502500
5502000
5501500
5501000
5500500
5500000
5499500
0
250
500
750m
SCALE 1:5,000
LEGEND
Bedding
Cleavage, shearing
Fracturing
Jointing
Quartz Vein
Fault
Rock sample site
eg. MW 112 - 368; Sample No. and gold in PPB
Trench
Trench Number
SEDEX MINING CORP
MW PROPERTY
SURFACE GEOLOGY & TRENCH LOCATION
Scale: 1:5,000
Date:
Mapsheets: 082G061
Figure: 3a
Datum: Nad 83
M1

SEDEX MINING CORP
MW Property VLF-EM Data
Alteration Zone & K-14 Grid Areas
Showing Dip Angle and Fraser Filter Data
Scale 1:5000 Transmitting Station Seattle
For location see Figure 2b
Scale: 1:5,000
Date:
Mapsheets: 082G061
Figure: 4a
Datum: Nad 83
SCALE 1:5,000
0
250
500
750m
True North
Magnetic North
N
DAM
L 8752
L 10839
L 10840
L 11624
L 11623
L 6623
SL 13
SL 12
SL 5
SL 4
15
14
13
C's
Dip Angle
Fraser Filter
M2
582000
582500
583000
583500
584000
584500
5503000
5502500
5502000
5501500
5501000
5500500
5500000
5499500
49:40:40.90 N
115:49:18.50 W
49:40:21.50 N
115:44:19.60 W



ROAD
VLF-EM TREND
FAULT ZONE
5500700N
5500600N
582600E
582700E
0 10 20 30
meters
N
TRENCH 10 DETAIL
LEGEND
Bedding
Cleavage, shearing
Fracturing
Jointing
Quartz Vein
Fault
Rock sample site
eg. MW 112 - 368; Sample No. and gold in PPB
Approx. center of VLF-EM Anomaly
See Figure 4a
Trench Number
Figure 6a
MW Property
Detailed Trench Map
Alteration Zone Area
Scale 1:5000 For location see Figure 2a
M3