





**DIAMOND DRILLING REPORT**

**AND**

**RESOURCE DEFINITION**

**FOR THE**

**LODESTONE PROPERTY**

**SIMILKAMEEN MINING DIVISION**

**SOUTHWESTERN B.C.**

**NTS 92 H7**

**For**

**SARGOLD RESOURCE CORPORATION**

**May 04, 2004**

**Nils von Fersen P.Geol.**

GEOLOGICAL SURVEY BRANCH  
ASSESSMENT REPORT  
27520

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## 1.0 SUMMARY

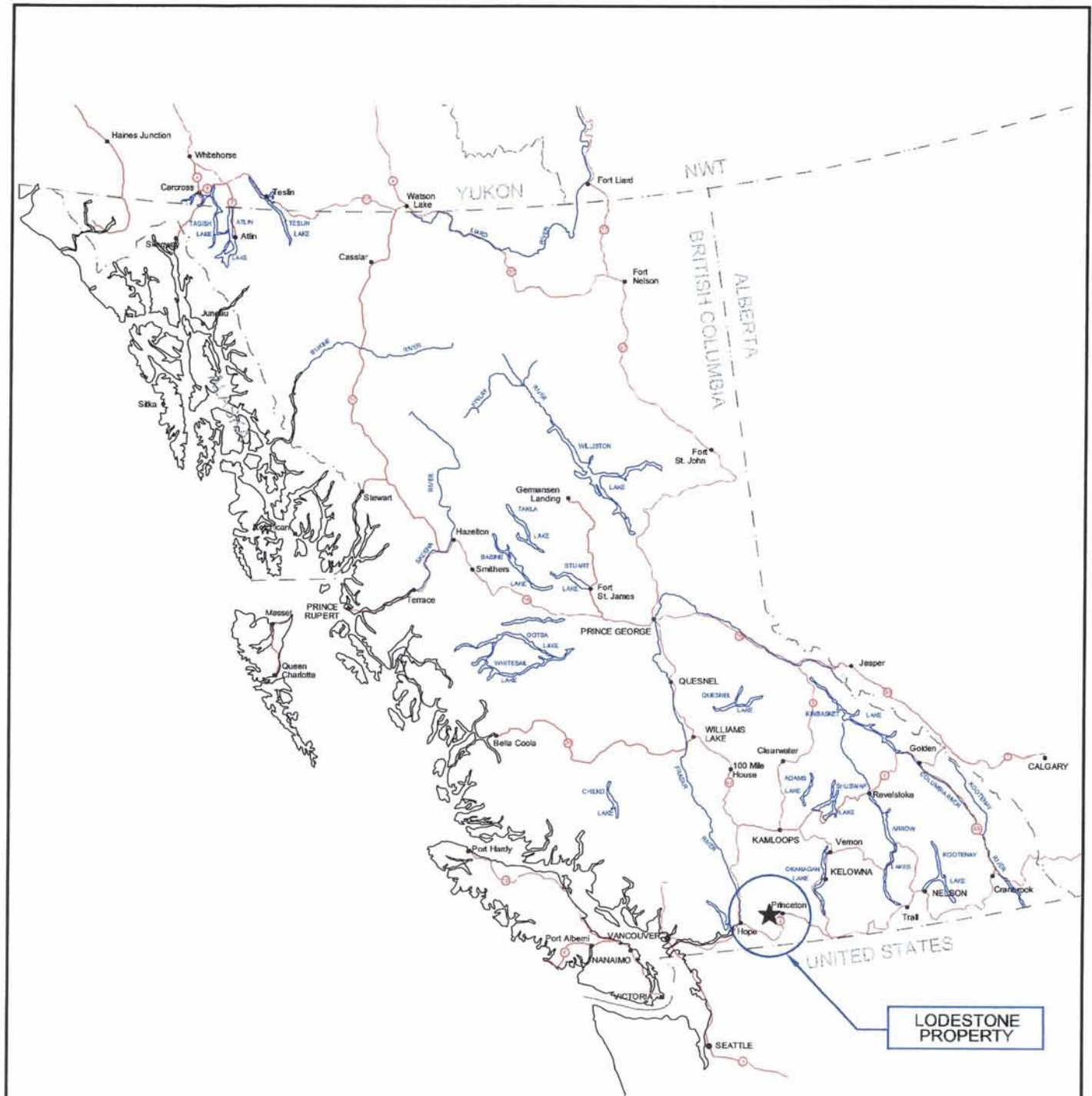
This report describes the results of a diamond drilling program conducted on the Lodestone Property on behalf of Sargold Resource Corporation. The objective of the program was to obtain sufficient, closely spaced, data regarding the average magnetite content in the host clinopyroxenite unit to support a resource calculation acceptable under the provisions of NI 43-101.

The Lodestone property is situated in the Similkameen Mining Division, approximately 25 km west of the town of Princeton, or 175 km east-northeast of Vancouver, in southwestern British Columbia (Figure 1). The property lies within the Tulameen Ultramafic Complex, on Lodestone Mountain, comprising four contiguous, modified grid system claims that total 50 units approximating 1,140 hectares, or 2,816 acres.

Since the presence of magnetite on Lodestone Mountain was discovered in the early 1900's, the area has been staked numerous times and has been the target of extensive exploration efforts which ranged from early surface trenches to detailed prefeasibility studies in 1969-1973.

The principal mafic and ultramafic units of the Tulameen Ultramafic Complex comprise dunite/peridotite, olivine clinopyroxenite, hornblende clinopyroxenite, and gabbroic to dioritic rocks. The Lodestone property is underlain by all of the major rock units of the Complex, with the exception of dunite and peridotite; however significant magnetite concentrations are only found in the clinopyroxenite unit. The Lodestone magnetite mineralization occurs in a poorly constrained zone that appears to vary between 100 meters and 400 meters in width, and trends northwesterly for a minimum of 700 meters. Vertical drill holes located in the center of the clinopyroxenite have reached a maximum depth of 186 meters (618 feet) without encountering the bottom of the magnetite mineralization. The true thickness of the zone has not been determined to date.

Sargold Resource Corporation contracted Beaupre Diamond Drilling Ltd., of Princeton, B.C., to carry out a diamond drilling program consisting of 15 vertically oriented diamond drill holes, aggregating 1,069 meters of NQ diameter core. The drill program was conducted between November 17<sup>th</sup> and December 13, 2003. Holes were located in a rectangular grid pattern with a nominal 25 meter spacing between holes, in an area defined by previous drill programs as containing high magnetite concentrations. All 15 holes of the current drill program encountered medium to coarse grained magnetite bearing hornblende clinopyroxenite throughout their length. Good core recoveries were achieved, only two holes returned recoveries below 90%. Visual estimates of magnetite content ranged from 10 to 25%, with occasional short sections of +/- 50%. No significant amounts of pyrite or pyrrhotite were noted in the clinopyroxenite. Results of the Davis Tube analyses completed at the University of British Columbia were very encouraging, providing weighted average percent magnetite contents per drill hole ranging from 19.54% to 27.25%.



# LODESTONE PROPERTY

## LOCATION MAP

SCALE 1:1,000,000 (APPROX.)  
 0 100 200 400 600 km

FILE NAME LODESTONE_LOCATION.DWG	MADE MT	SCALE: approx 1:1,000,000	DATE: June 5, 2003	FIG 1
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Specific gravity determinations conducted on 32 samples by Vison Scitec Ltd., provided an average specific gravity factor for the clinopyroxenite host rock of 3.34.

A revised resource calculation, compliant with regulations under National Instrument 43-101 and based on the results of the closely spaced diamond drilling program recommended by M. Tindall and J. Miller-Tait, has defined a measured resource of 2.035 million tonnes grading 24.33% magnetite.

## **2.0 INTRODUCTION and TERMS OF REFERENCE**

This report was prepared at the request of Sargold Resource Corporation, and is written in compliance with reporting and disclosure requirements under National Instrument 43-101. The author's mandate was to conduct a diamond drilling program on the Lodestone Property and to prepare a new resource calculation conforming to the requirements of National Instrument 43-101. The program was based on recommendations in a Qualifying Report for Canley Developments Inc. (renamed Sargold Resource Corporation) entitled Geological Report for the Lodestone Property, Similkameen Mining Division, M. Tindall P. Geo., J. Miller- Tait P. Geo., June 5, 2003.

Information relating to items 6 to 11 under Form 43-101 has been largely excerpted from the above report. The author supervised the diamond drilling and sampling programs, and logged all of the core, between November 11 and December 17, 2003.

Substantial exploration efforts between 1962 and the early 1990's on the Lodestone property included considerable diamond and percussion drilling as well as preliminary feasibility studies. This work defined a large area of magnetite rich hornblende clinopyroxenite averaging approximately 14% magnetic iron. The historical resource estimates determined for the Lodestone Property do not conform to the requirements of National Instrument 43-101. A diamond drilling program of closely spaced holes on a nominal 25 meter grid was recommended to provide sufficient data for a new resource estimate compliant with NI 43-101.

## **3.0 DISCLAIMER**

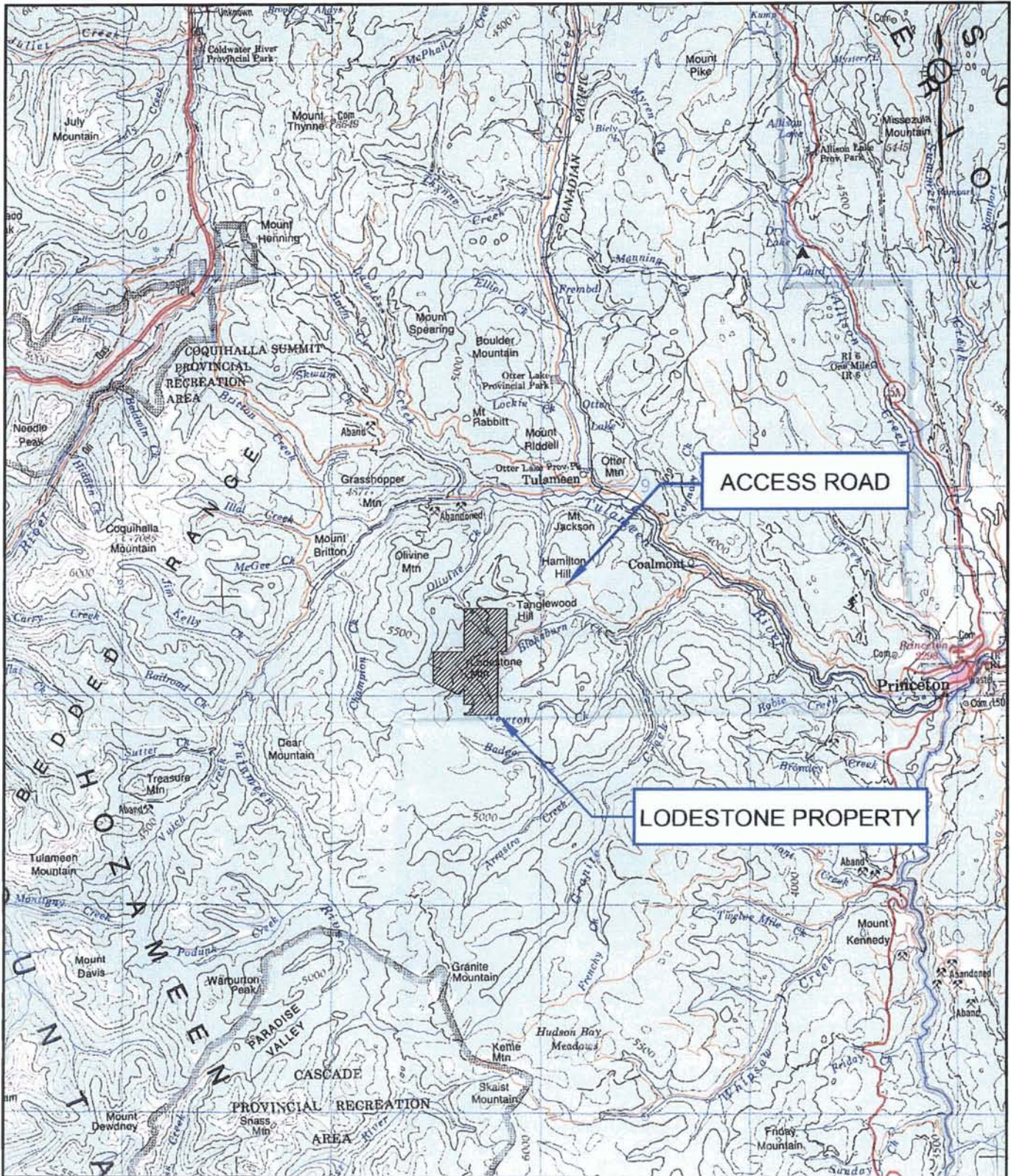
Title to the claims was investigated on March 18, 2004 on the website provided by the Ministry of Sustainable Resource Development for the Province of British Columbia. The website indicates that the four claims discussed in this report are owned by 651030 B.C. Ltd., a company controlled by Richard Warke. The sale of 651030 B.C. to Sargold Resource Corporation closed September 2, 2003. Richard Warke is also President and CEO of Sargold Resource Corporation, the company that commissioned this report. The ministry website showed all four claims to be in good standing until October 4, 2004. The author of this report is not aware of any encumbrances, royalties or contracts that may encumber the property. A legal review of property title was not part of the scope of this report.

## **4.0 PROPERTY DESCRIPTION AND LOCATION**

The Lodestone property is situated in the Similkameen Mining Division, approximately 25 km west of the town of Princeton, or 175 km east-northeast of Vancouver, in southwestern British Columbia (Figure 1). The property is centered at 49°28' north latitude and 122°50' west longitude on NTS map sheet 92H/7.

Access to the property is obtained from the village of Coalmont on the Tulameen River, via a good mainline logging access road that follows Blakeburn Creek (Figure 2).





SOURCE:  
 B.C. MINISTRY OF SUSTAINABLE RESOURCE  
 DEVELOPMENT CLAIM MAP M092H046 & NTS MAP 92H

SCALE 1:250,000 (APPROX.)



## LODESTONE PROPERTY

### LOCATION AND ACCESS MAP

FILE NAME	MADE	SCALE: approx	DATE:	FIG
LODESTONE_LOCATIONACCESS.DWG	MT	1:250,000	JUNE 5, 2003	2

The Lodestone property is located on Crown land and is comprised of four contiguous, modified grid system claims that total 50 units and cover an area approximating 1,140 hectares, or 2,816 acres (Figure 3).

A review of the land tenure information provided on the Ministry of Mines and Energy website on March 18, 2004 indicates the claims are recorded as being 100% owned by 651030 B.C. Ltd. All four claims are shown to be in good standing until October 4, 2004. Table 3.0.1 lists a summary of the claim information.

**Table 3.0.1**

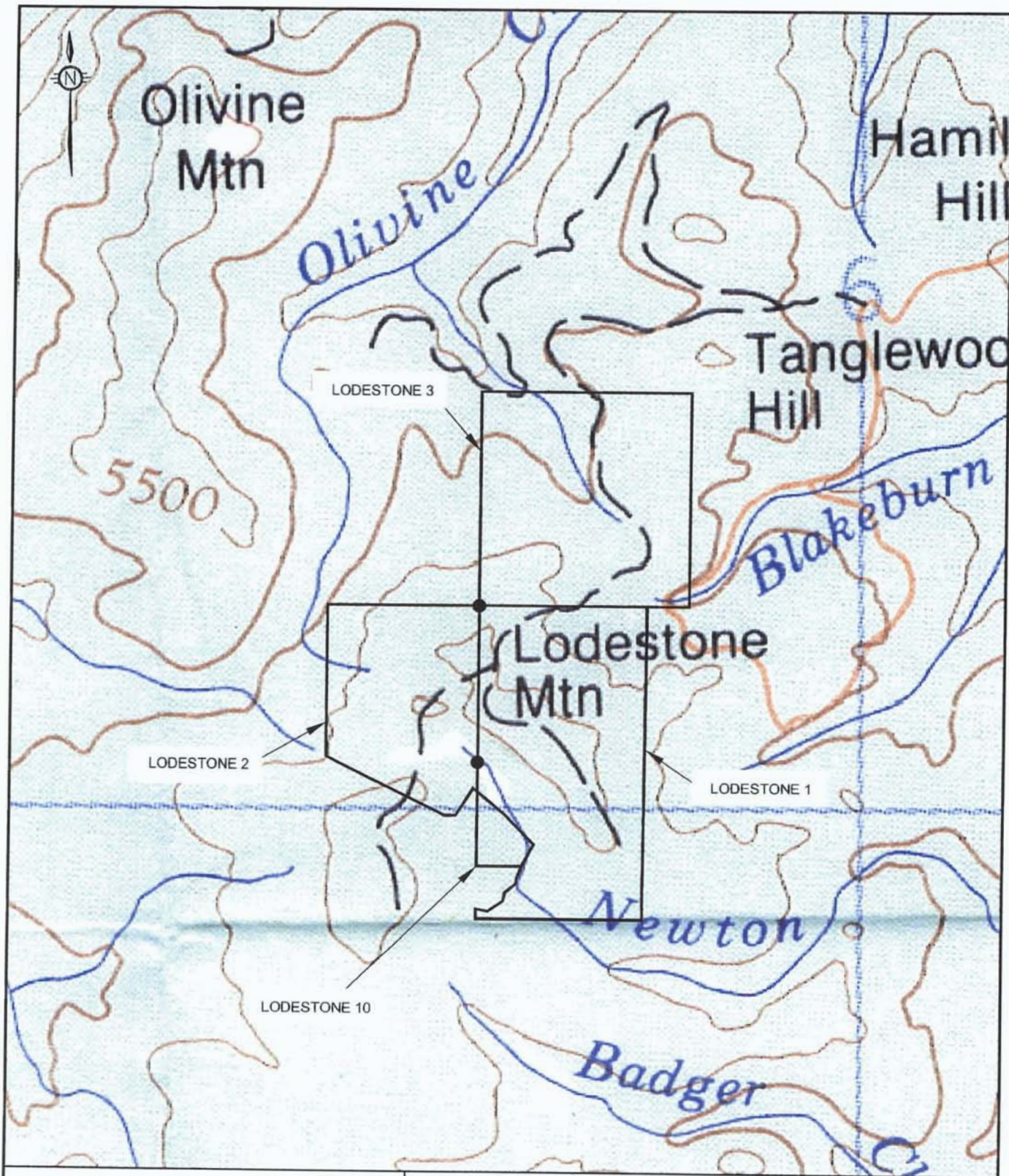
Claim Name	Tenure No.	Owner	Valid to	No of Units	Tag No.
Lodestone 1	248685	651030 BC Ltd	10/04/2004	18	43807
Lodestone 2	248686	651030 BC Ltd	10/04/2004	12	43808
Lodestone 3	248687	651030 BC Ltd	10/04/2004	16	43809
Lodestone 10	305919	651030 BC Ltd	10/04/2004	4	200427

The Lodestone property covers Lodestone Mountain and lies between elevations of 1,525 and 1,895 meters above sea level. In general, topography is gently rolling to moderately steep. Outcrop is abundant along the northwestern trending ridge that forms the crest of Lodestone Mountain. This zone of outcrop conforms to the area of magnetite mineralization that was the target of previous exploration efforts. Outcrop is scarce to non-existent elsewhere on the property.

The area surrounding the property is covered by mature fir forest, and is being actively logged. Widely spaced, sub-alpine spruce, juniper and open grassy areas characterize the summit of Lodestone Mountain. Regionally, forested areas are generally underlain by glacial till. Glacio-fluvial deposits also occur at lower elevations in the river valley.

The region lies in a transition zone between the Cascade Mountains to the west and the Interior Plateau, located further to the east. The climate is transitional between that of the dry southern interior and the much moister Cascade and Coast Mountain ranges located to the west. Summers are hot and dry while winters are cold with heavy snowfall at high elevations. Patches of snow can remain on the plateau areas of Olivine, Grasshopper and Lodestone Mountains until early June, and snowfalls can take place as early as mid-September. The climate of the Princeton – Coalmont area is moderate with temperatures ranging from the low 30's Celsius in summer to -15° Celsius in winter. Annual average rainfall is 218 mm. at Princeton and snowfall averages 150 cm.

Supplies and services are available in Princeton, a distance of approximately 40 km by road from the property. Sufficient water for exploration purposes is available at Lodestone Lake, approximately 750 meters west of Lodestone Peak, and immediately adjacent to the zone of magnetite mineralization.

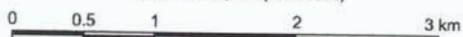


**LEGEND**

● LEGAL CONERPOST

SOURCE:  
B.C. MINISTRY OF SUSTAINABLE RESOURCE  
DEVELOPMENT; CLAIM MAP M092H046 & NTS MAP 92H

SCALE 1:50,000 (APPROX.)



**LODESTONE  
PROPERTY**

**CLAIM MAP**

FILE NAME LODESTONE_CLAIMMAP.DWG	MADE MT	SCALE: approx 1:50,000	DATE: JUNE 5, 2003	FIG 3
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## 5.0 HISTORY

During the late 1800's the Tulameen District was the most important producer of platinum in North America. Platinum was recovered along with the placer gold from the Tulameen River and its tributaries. The platinum occurred as a fine, hard, silver-white lustrous metal with a high specific gravity in the sluice boxes and gold pans, along with the gold and heavy concentrations of black sands (magnetite and chromitite). Total platinum production from the alluvial operations was estimated to be approximately 20,000 ounces from the area between 1885 and 1934 (O'Neil and Gunning, 1934).

Preliminary geological investigations by government agencies in the Tulameen area included work by Kemp (1902), Camsell (1913), Rice (1948), Findlay (1969), St. Louis (1982, 1986), Rublee (1986,1994). Nixon and Rublee (1987) classified the Tulameen Alaskan-type ultramafic complex as potential hosts for commercially exploitable deposits of platinum metals.

Since the presence of magnetite on Lodestone Mountain was discovered in the early 1900's, the area has been staked numerous times and early, unrecorded, exploration is indicated by many old trenches on the property.

**1954 - 1955** - United States Steel Corporation conducted a dip -needle survey and carried out an exploration program of drilling and trenching. The data from this work has been lost.

**1962 - 1970** - Imperial Metals and Power Limited conducted a series of exploration programs on the property. Imperial Metals completed a ground magnetometer survey, trenching, and a total of 11,600 feet of drilling in 60 holes. The majority of the drilling was done with a percussion machine on a drill pattern of 400 foot centers, on lines spaced 800 feet apart. Much of the specific data from these exploration programs is no longer available, and the location of drill core and percussion cuttings is unknown.

**1969** - Imperial Metals and Power commissioned Wright Engineers Ltd. to conduct a preliminary feasibility study. The prefeasibility study investigated mining iron at Lodestone Mountain, and coal at a nearby location. The two mine products would be used to produce metallized iron pellets (DRI) for the steel industry. The DRI plant was to be located at the town of Coalmont. The Wright report is all-encompassing and includes resource calculations, metallurgical studies, mine and plant designs, and financial projections.

**1973** - Dominion Foundries and Steel Ltd. (Dofasco) optioned the Lodestone property from Imperial Metals and Power. Dofasco completed nine diamond drill holes and 17 percussion holes for a total of 10,562 feet of drilling. The purpose of the drilling was to confirm the Wright Engineers reserves and to explore for increased reserves. Dofasco calculated new reserves, stripping ratios, and designed hypothetical pits. Dofasco concluded that the calculated "reserve" did not meet their requirement to support a 1,200,000 ton per year iron oxide pellet operation for a minimum 20 year mine life.

**1984** - The renamed Imperial Metals Corporation began to evaluate the platinum group element (PGE) potential of the property. Drill holes 73-3, 73-8 and 73-9 were re-logged and re-sampled. Ninety nine samples were collected and analyzed for 30 elements by atomic absorption. Twenty three of those samples were assayed for iron, copper and platinum. Results of the platinum assays were negative.

**1986** - The property was re-mapped and prospected. Eleven silt and concentrate samples were collected from streams draining the property and 37 rock samples were collected. All samples were assayed for platinum, palladium and gold with discouraging results. It was noted that mapping and prospecting were hampered by lack of outcrop in all areas of the claims except for Lodestone Ridge.

**1987** - Imperial Metals undertook a program of soil geochemistry. Sixty three kilometres of grid line were established and 1,221 soil samples were collected. Grid lines were spaced 200 metres and soil samples were collected at 50 metre intervals along the lines. Soil samples were fire assayed for gold, platinum, palladium and rhodium. Spotty, anomalous platinum group assays were returned from soils in the southern portion of the property in an area of no bedrock exposure.

**1989** - Tiffany Resources Inc. entered into an option agreement with Imperial Metals Corp. covering the Lodestone property. Six diamond drill holes totalling 612.7 metres were drilled by Tiffany and the drill core was analyzed for platinum group elements. The holes were drilled into the areas of anomalous PGE's in soil. No platinum group anomalies were detected in the drill core. It is of note that all six of the drill holes intersected long core intervals of pyroxenite containing strong magnetite mineralization. The core was not analyzed for iron content.

**1990** - An additional four diamond drill holes totalling 613.0 metres were completed by Tiffany. These drill holes also targeted the area of anomalous PGE's in soil. The drill core was analyzed for 30 elements by inductively coupled plasma methods (ICP) and was assayed for platinum. Platinum assays were discouraging. Again long intervals of magnetite bearing pyroxenite were intersected. Iron analyses varied between 1.8% and 13.25% for all of the core samples.

**1993** - PBK Engineering Ltd was contracted by Tiffany Resources and Prime Resources Group to complete a preliminary evaluation of the Lodestone iron deposit. The PBK report was based on the 1970 Wright Engineers report but was updated to 1991 costs and to allow for advances in mining and processing technology. Two scenarios were investigated based on production rates of 450,000 and 900,000 tons per year of direct reduced iron pellets (DRI). Iron carbide for the steel industry and magnetite concentrates for the coal industry were also briefly examined as possible products from the Lodestone mineralization. The PBK study investigated markets, examined available infrastructure, estimated capital and operating costs, produced a preliminary financial analysis and noted

additional work that would be required before a complete feasibility study could be undertaken

## 6.0 GEOLOGICAL SETTING

### 6.1 Regional Geology

The following description is condensed from Nixon and Hammock et al (1997). The regional geology is depicted in Figure 4, adapted from Nixon and Rublee (1988).

The Tulameen Ultramafic Complex is located in the southwestern Intermontane Belt, within the Quesnel Terrane, immediately east of the boundary with the Eagle Plutonic Complex. The mafic and ultramafic rocks were emplaced into metasedimentary and mafic to felsic metavolcanic rocks belonging to the Upper Triassic Nicola Group during a late Triassic deformational event. This volcanic assemblage evolved during the Late Triassic arc magmatism, and these rocks are considered to be comagmatic with the rocks of the Tulameen mafic-ultramafic suite. The Tulameen Complex and its host rocks are thought to be unconformably overlain by terrigenous sedimentary and volcanic assemblages of the Early Tertiary Princeton Group and Miocene plateau basalts.

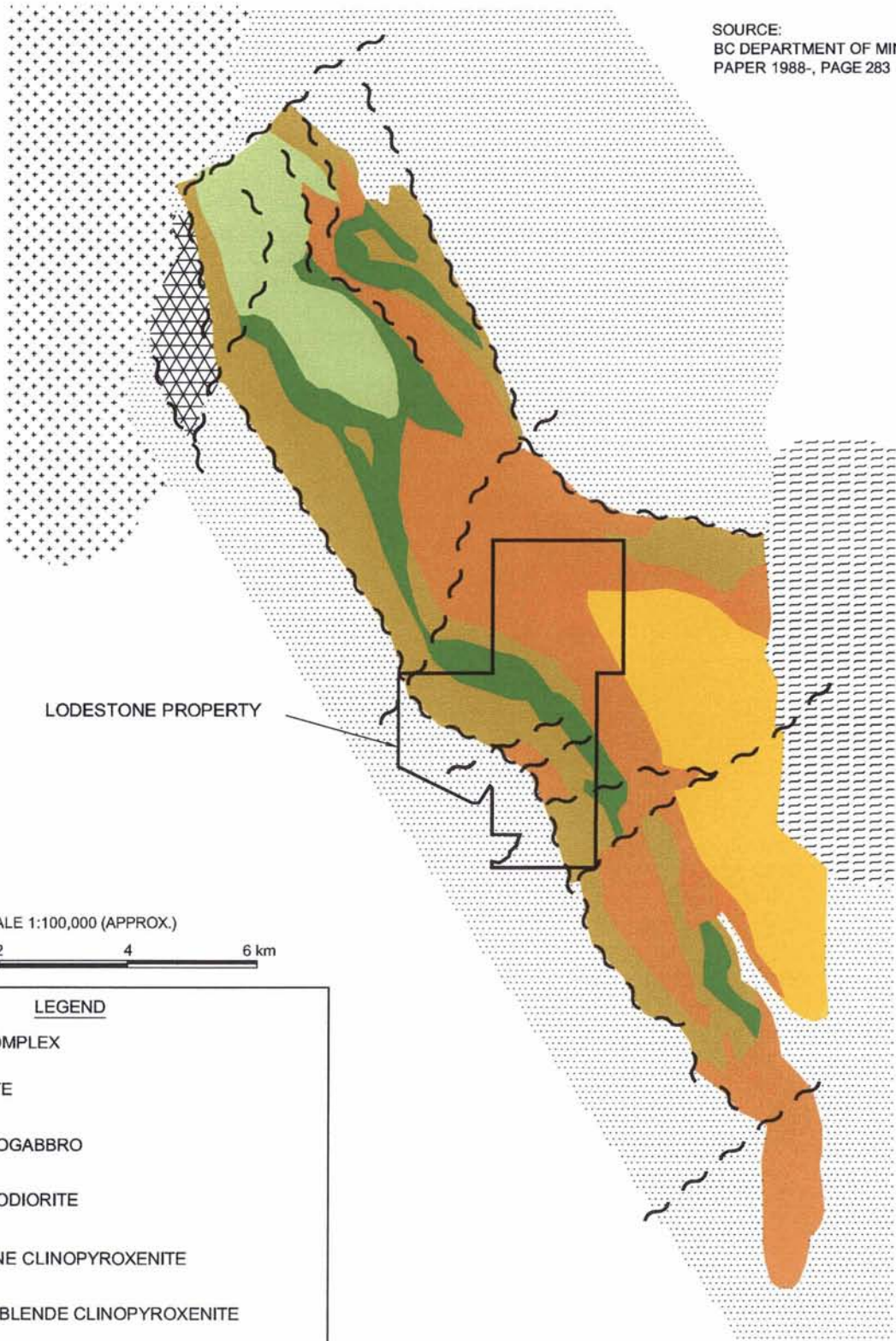
Regional structures trend roughly north-northwest and are characterized by southwest dipping foliation that parallels the eastern margin of the Eagle Plutonic Complex (Eagle Shear Zone). The Eagle Shear Zone is related to Middle - Late Jurassic contractional deformation. The Tulameen Complex forms an elongate body along the eastern margin of the shear zone and is concordant with the regional structural grain.

The principal mafic and ultramafic units of the Tulameen Ultramafic complex are comprised of dunite/peridotite, olivine clinopyroxenite, hornblende clinopyroxenite, and gabbroic to dioritic rocks, as depicted in Figure 4.

Dunite is generally restricted to the northern portion of the complex, at Grasshopper and Olivine Mountains. Concentrations of massive chromite appear to be randomly distributed within the dunite as discrete layers and irregular masses. Associated with the chromite are microscopic grains of platinum. Olivine pyroxenite envelops the dunite core and extends southwards along the central axis of the complex. Hornblende clinopyroxenite generally occurs at the periphery of the complex. This unit is continuous along the western margin of the complex but is more discontinuous along the east. Massive magnetite mineralization is associated with hornblende clinopyroxenite at Lodestone Mountain and at Tanglewood Hill, 3.4 km. north-northwest of Lodestone Mountain.

The main mass of gabbroic rocks is distributed on the eastern side of the complex. Gabbroic rocks are commonly in direct contact with olivine clinopyroxenite in the north. Syenodiorite is confined to the southwestern margin of the complex where it is unconformably overlain by Princeton Group sediments.

SOURCE:  
BC DEPARTMENT OF MINES  
PAPER 1988-, PAGE 283








LODESTONE PROPERTY

SCALE 1:100,000 (APPROX.)

0 2 4 6 km

LEGEND

TULAMEEN COMPLEX

-  DUNITE
-  SYENOGABBRO
-  SYENODIORITE
-  OLIVINE CLINOPYROXENITE
-  HORNBLLENDE CLINOPYROXENITE

 MYLONITIC ROCKS

 EAGLE GRANODIORITE

 PRINCETON GROUP

 NICOLA GROUP

 FAULT

LODESTONE  
PROPERTY

REGIONAL GEOLOGY

FILE NAME  
LODESTONE\_GEOLOGY.DWG

MADE  
MT

SCALE: approx  
1:100,000

DATE:  
JUNE 5, 2003

FIG  
4

## 6.2 Geology of the Lodestone Property

The Lodestone property is underlain by all of the major rock units of the Tulameen Ultramafic Complex with the exception of dunite and peridotite. Mapping is incomplete due to the extensive amount of overburden cover on the property, and much of the geology has been extrapolated from limited bedrock exposure. The geology of the Lodestone property is shown in Figure 5.

A central core of olivine pyroxenite trends northwesterly through the center of the property. The olivine pyroxenite is flanked on both sides by clinopyroxenite and hornblende clinopyroxenite. The clinopyroxenites are in turn flanked by gabbro. The gabbro unit on the northeast side forms a body about 2 km. in width, while the southwestern gabbro unit is narrow and discontinuous.

The western contact between the ultramafic complex and rocks of the Nicola Group is located immediately south of Lodestone Lake, where rusty quartz-biotite-chlorite schist is exposed.

The extensive overburden cover has also hampered structural mapping. Structures have been interpreted from northeasterly trending discontinuities indicated on the aeromagnetic map. These discontinuities coincide with photo linears and are generally less than 500 meters long.

## 6.3 Magnetite Mineralization

The southwestern hornblende clinopyroxenite body is host to the magnetite mineralization on the Lodestone property. This body has an inferred dip to the southwest between 30-50°. The magnetite is interpreted to be syngenetic with the formation of the clinopyroxenite.

Magnetite occurs principally as +/- 1 mm. disseminations interstitially between clinopyroxene and hornblende crystal intergrowths. Magnetite also forms semi-massive to massive lenses and vein-like bodies up to 0.6 meters wide. The quantity of magnetite is variable between 12% and 25% of the clinopyroxenite by volume.

The magnetite mineralization occurs in a poorly constrained zone that appears to vary between 100 meters and 400 meters in width, and trends northwesterly for a minimum of 700 meters. Vertical drill holes located in the center of the clinopyroxenite have penetrated as deep as 186 meters (618 feet) without exiting the magnetite mineralization. The true thickness of the zone has not been determined.



SOURCE:  
SOUTH HALF GEOLOGY & GEOCHEMISTRY MAP.  
B.C . MSRD ASSESSMENT REPORT #15458



LEGEND

TULAMEEN COMPLEX

-  MIXED LITHOLOGIES
-  SYENOGABBRO
-  SYENODIORITE
-  OLIVINE CLINOPYROXENITE
-  HORNBLLENDE CLINOPYROXENITE
-  NICOLA GROUP
-  FAULT

SCALE 1:30,000 (APPROX.)



**LODESTONE  
PROPERTY**

**PROPERTY GEOLOGY**

FILE NAME LODESTONE_PROPERTYGEOLOGY.DWG	MADE MT	SCALE: approx 1:30,000	DATE: JUNE 5, 2003	FIG 5
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## **7.0 2003 LODESTONE PROJECT DRILLING PROGRAM**

### **7.1 Introduction**

Sargold Resource Corporation contracted Beaupre Diamond Drilling Ltd., based in Princeton, B.C., to carry out a diamond drilling program on their Lodestone Mountain property. Vertically oriented drill holes were located in a rectangular grid at a nominal 25 meter spacing between holes, in an area defined by previous drill programs as containing elevated magnetite content (Figure 6). A total of 15 diamond drill holes aggregating 1,069 meters of NQ diameter core were completed between November 17<sup>th</sup> and December 13, 2003 (Figure 7). Fourteen of the fifteen holes were drilled to a nominal depth of 65.00 meters, and one was continued to a depth of 150 meters. Drill hole collars were marked by inserting a 3 meter length of PVC pipe into each hole.

### **7.2 Logistics and Procedures**

Beaupre Diamond Drilling supplied a Longyear 38 drill and a D-4 cat plus sufficient equipment and supplies to carry out the drill program. The equipment was mobilized on a flatbed trailer from Princeton to the Blakeburn Coal Mine, where it was offloaded. From this point the equipment was moved by cat for the remaining 15 kilometers to the top of Lodestone Mountain. Deep snow required the use of two cats, one to keep the access road open and the other to prepare drill-sites and move the drill rig. Drilling was conducted around the clock with two drill crews. Drill crews were based in Princeton, necessitating a one hour commute each way. On completion of each hole, debris and all materials used were removed from the pad. Due to the winter conditions prevalent during the program, final clean up and rehabilitation of the drill site was deferred until the snow has melted.

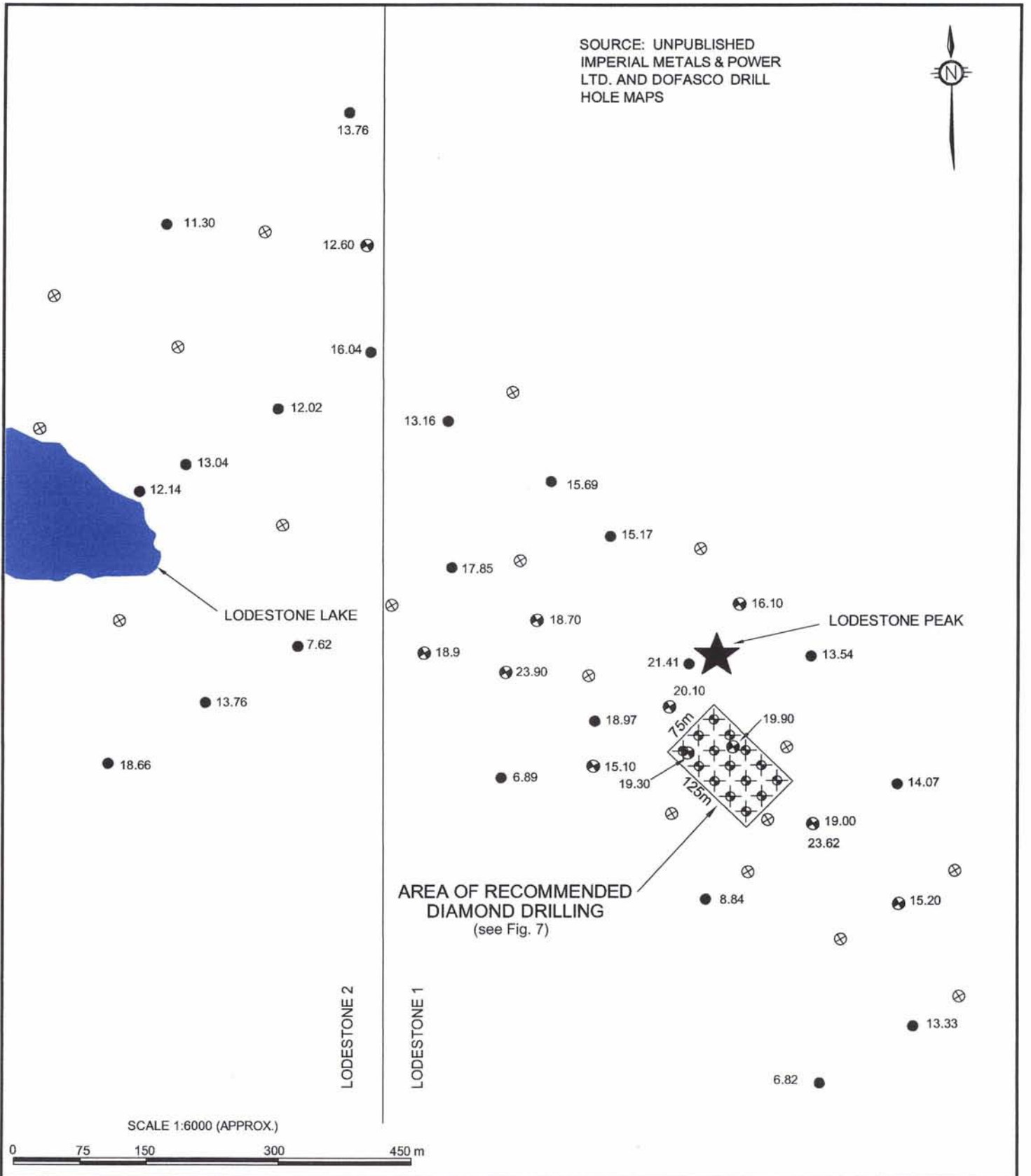
Due to strong magnetic interference at the site, drill hole locations were determined using a combination of GPS, surveyors prism, and metric tape. At the conclusion of the drill program the collar of each hole was surveyed using a Theodolite and Stadia Rod, with Lodestone Peak as a topographic marker (Figure 7).

Drill core was placed in wooden core boxes and transported to a core logging facility in Coalmont. At the facility, core was logged for RQD, photographed, and cut using a diamond saw before being logged for lithology. Core boxes were labeled indicating the project, drill hole and box number, and depths of core interval from surface. Lithological and geotechnical logs are presented in Appendix A and C.

### **7.3 Drill Core Lithology**

As noted in section 5.2 above, the predominant rock type that underlies the area targeted by the drill program consists of magnetite bearing hornblende clinopyroxenite. Previous drilling programs have indicated this unit underlies an area measuring 100-400 meters in width, and at least 700 meters in length. The clinopyroxenite was previously tested to a

SOURCE: UNPUBLISHED  
 IMPERIAL METALS & POWER  
 LTD. AND DOFASCO DRILL  
 HOLE MAPS



**LEGEND**

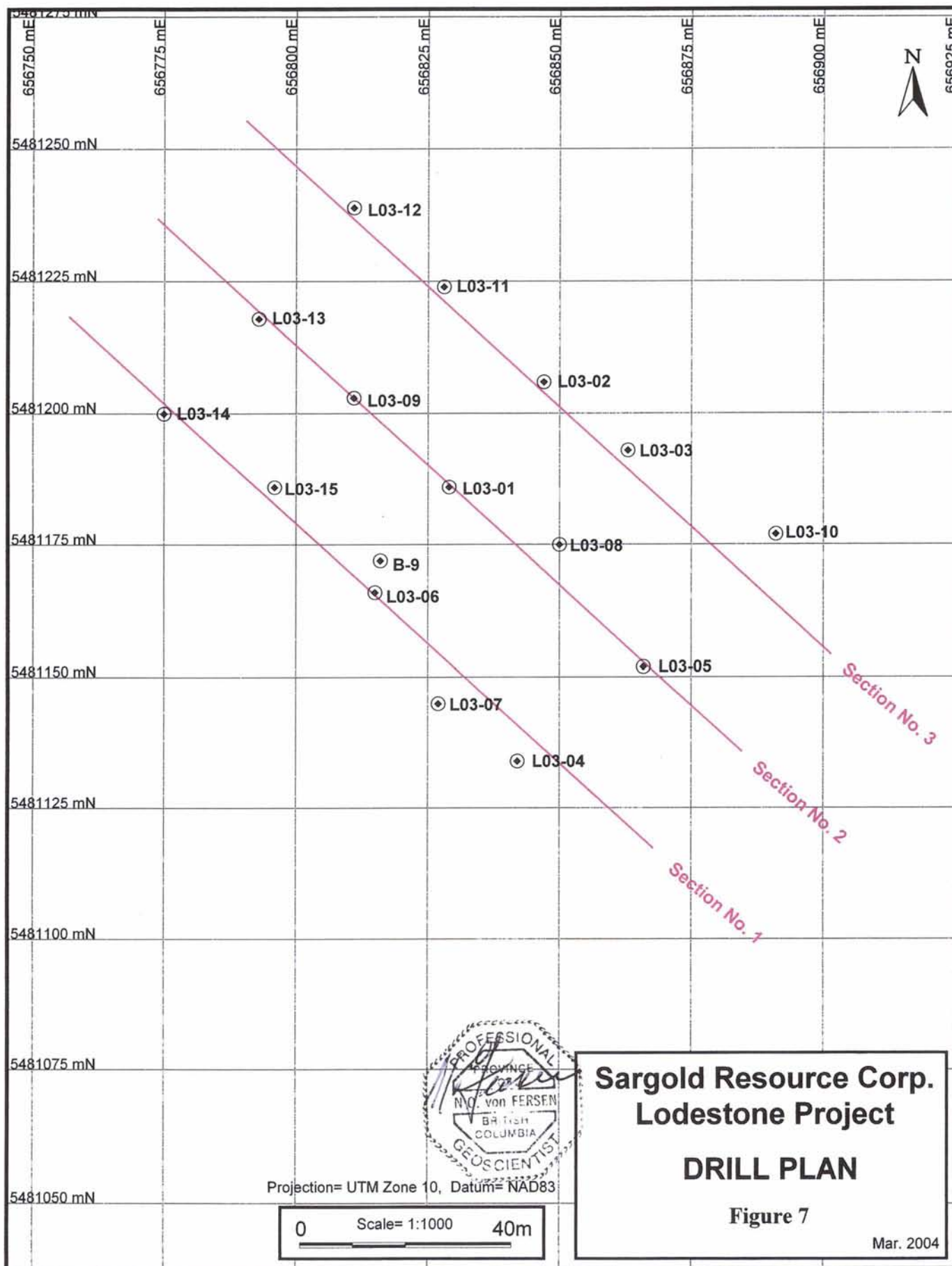
- IMPERIAL METALS PERCUSSION DRILL HOLE
- ⊕ IMPERIAL METALS DIAMOND DRILL HOLE
- ⊗ 1973 DOFASCO DRILL HOLE
- ⊕ RECOMMENDED DIAMOND DRILL HOLE
- 13.76 AVERAGE % SOLUBLE IRON FOR ENTIRE DRILL HOLE

NOTE: DRILL HOLE LOCATIONS ARE APPROXIMATE ONLY

**LODESTONE  
 PROPERTY**

**HISTORIC DRILLING**

FILE NAME LODESTONE_RECOMMENDEDDRILLING.DWG	MADE MT	SCALE: approx 1:6,000	DATE: JUNE 5, 2003	FIG 6
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maximum depth of 186 meters without encountering a change in rock type. All 15 holes of the current drill program encountered magnetite bearing hornblende clinopyroxenite throughout their length.

Hornblende clinopyroxenite is generally medium to coarse grained, dark greenish grey in colour, and equigranular. Clinopyroxene compositions consist primarily of diopsidic augite. Variable amounts of medium to coarse grained amphibole (hornblende), generally dark green to black, are scattered throughout the pyroxenite and are locally concentrated in narrow bands of hornblendite. Very coarse grained, clinopyroxene-hornblende intergrowths ( $\approx >1.0 \text{ cm} \times 0.5 \text{ cm}$ ) are relatively common and usually occur irregularly, over short 5 to 10 cm intervals. Magnetite occurs primarily as  $\approx 1.0 \text{ mm}$  grains, disseminated as interstitial intergrowths between medium to coarse grained clinopyroxenes, and less commonly, as irregular more massive segregations. The grain size of the magnetite is generally proportional to the grain size of the surrounding host rock.

#### **7.4 Alteration**

The hornblende clinopyroxenite exhibits broad, weak to moderate alteration characterized by phlogopite-biotite development of pyroxene, and actinolite alteration associated with hornblende. Fractures and veinlets developed within the unit are commonly filled with a combination of carbonate accompanied by lesser, fine grained quartz, sepiolite/talc, chlorite and serpentinite. Hematite is frequently developed on fractures and also occurs as hematite blotches surrounding larger aggregations of magnetite. In the latter case, phlogopite/biotite mica is closely associated with this alteration, suggesting it may not be wholly caused by circulating groundwaters. Rare trace amounts of fine grained pyrite are found in carbonate veinlets or associated with altered hornblendite.

#### **7.5 Rock Quality**

Geotechnical parameters of rock quality such as recovery, RQD length, hardness, weathering, number of joints, and joint condition were recorded on a geotechnical logging form and are presented in Appendix C.

Average recoveries per hole ranged from approximately 85% in drill hole L03-10 to 100%. Twelve of fifteen holes had core recoveries in excess of 90%. However, core is well fractured to strongly fractured for significant intervals in nearly all holes. A preliminary estimate of rock mass quality, or rock mass rating, using RQD, number of joints per interval and joint condition indicates a rating of fair.

#### **7.6 Sample Preparation and Analytical Procedures**

NQ core was cut using a diamond saw and half of the core was placed in standard plastic sample bags along with a numbered sample tag identifying the project, drill hole number, and the interval sampled. Sample bags were labelled with the drill hole number and the contained sample interval, and were sealed with a plastic zip lock strap. Several sample

bags were placed in a large rice bag for shipping. Rice bags were delivered to the Greyhound Courier Service in Princeton for delivery to the facilities of Vizon Scitech (formerly B.C. Research) for processing.

At the laboratory of Vizon Scitech each drill core sample was dried at room temperature, as required. The entire sample was passed through a jaw - crusher for an initial size reduction, and then fed through a cone crusher to further reduce the sample to  $\frac{3}{8}$  inches. A 150 gm. sub-sample was then taken using a knife-edge splitter with a  $\frac{1}{2}$  inch opening. Each 150 gm. sample was ground to 90% passing minus 325 mesh using a ring pulverizer.

The 150 gm. pulverized sub-samples were then sent to the University of British Columbia for Davis Tube testing, as follows:

A 20.00 gm. portion is weighed out from each 150 gm. sample and slurried in a 250 mL beaker. With the magnetic field of the Davis Tube activated, the slurried sample is washed into the tube through a funnel. The sample is fed into the oscillating Davis tube while the magnetic field is on and flooded with wash water. The continuous water flow washes all non-magnetic solids through the tube until the water discharging from the tube runs clear (generally about 2 minutes). The non-magnetic fraction is discarded. The magnetic field is then switched off and the retained magnetic solids are thoroughly washed out and collected. These solids are filtered, dried and weighed. This weight is the magnetite fraction, calculated as a percentage of the original 20 gram sample. A total of 340 samples were processed in this manner. Duplicate analyses were completed on 39 samples as a quality control measure, using the same pulverized split. Non-magnetic rejects from two tests were examined and contained a magnetic fraction of 0.11 and 0.18 grams. This represented 2 -3% of the total magnetite, and in both cases the small recovered fraction is lighter in colour than the normal magnetite products, suggesting that it is a weakly magnetic middling fraction, and not pure magnetite. Results of the Davis Tube analyses are presented in Appendix B.

### **7.7 Specific Gravity Determination**

A total of 32 samples were chosen for the purpose of determining the average specific gravity of the magnetite bearing clinopyroxenite. Two samples were selected from each of the short holes and four were taken from hole 14. The selected samples ranged in magnetite content from 17.1 to 34.5% and averaged 24.3%.

Specific Gravity determinations were conducted by Vizon Scitec Ltd. All drill core submitted for magnetite analysis had been previously crushed to  $\frac{3}{8}$  inch. A representative portion, weighing approximately 500 grams, was separated by riffle splitting from each bag of reject material representing the selected sample.

Each sample split was accurately weighed and slowly poured into a 500 mL graduated cylinder into which 250 mL of tap water had been added. After agitating the cylinder to

ensure that there were no entrained air-bubbles, the new solution level was recorded, with the increase in volume representing the displacement by the solids.

The specific gravity factor was calculated as the weight of sample in grams divided by the displaced volume of water in milliliters. Specific gravity factors ranged from 2.93 to 3.54, with an average of 3.34.

## **8.0 RESOURCE CALCULATION**

The diamond drilling program consisted of 15 vertical holes at a nominal spacing of 25 meters and a depth of 65 meters, with the exception of hole 15, which reached a depth of 150 meters. A revised resource calculation compliant with National Instrument 43-101 was performed utilizing three equidistant vertical sections 25 meters apart (Figure 7). Drill holes slightly off section were projected onto the sections (Figures 8-10). Each hole was assigned an area of influence equaling half the distance to the adjacent holes, and a constant depth of 65 meters. The weighted average percent magnetite content in each hole was calculated and assigned to the area of influence volume represented by each hole. The sum of the volumes per hole was multiplied by the average density of 3.34, to determine the tonnage for each block. Weighted average magnetite contents for each hole were summed and divided by the total number of holes providing the average grade for the 75x125x65 meter block defined by the drill program. Utilizing the above procedure a mineral resource of 2,035,000t grading 24.33% magnetite was defined by the drilling program.

The writer classifies the resource as a measured mineral resource based on the close drill hole spacing, the relatively uniform distribution of the magnetite within the clinopyroxenite unit tested by the current drilling, and the much larger, surrounding, extent of similar mineralization encountered in historic drilling.

Faulting is evident in core and is suggested by linears visible on airphotos. No fault offsets or lithological boundaries to the mineralized clinopyroxenite were encountered in the recent drilling. The writer is not aware of any factors that would limit an incremental expansion of the currently outlined measured resource, with the exception of natural grade variations.

## **9.0 MARKET ASSESSMENT**

Information concerning market factors for magnetite has been extracted from a report entitled Valuation and Related Fairness Opinion, Canley Developments Inc. July 2, 2003.

Magnetite is an important source of iron ore, and magnetite concentrates are also utilized in dense medium separation in coal preparation plants. Other possible markets for magnetite include: heavy aggregate for high density concrete, sand blasting abrasive, high density filter media, and radiation shielding aggregates.

Coal washing is the process of removing impurities, such as ash, sulphur based compounds, and heavier shale, from coal. In dense medium separation the coal is pre-

mixed with finely ground magnetite, and is fed to a cyclone separator under pressure. The separation of the lighter coal and heavier particles is achieved in the cyclone.

Estimated annual requirements for fine magnetite, used in heavy media separation of metallurgical coal by the major coal producers in western Canada, are 70,000-80,000 t/annum. Fording Coal and Luscar utilize approximately 52,000 tonnes annually.

Process Research Associates Ltd. conducted a scoping study of magnetite recovery on samples from the Lodestone property, and in a report dated January 8, 2002, concluded that the samples indicated the potential to produce a high grade magnetite concentrate suitable for use as a high density medium for the coal industry

The largest competitor to the Lodestone Property with respect to magnetite production is the Craigmont Mine, near Merritt, B.C., operated by M-Seven Industries Inc. The company produces between 60,000 and 70,000 tonnes of magnetite annually by processing the Craigmont mine tailings. M-Seven reports it is supplying most coal mines in western Canada with heavy media for their wash plants. No other supplier of magnetite is currently known in western Canada. Several of the coal producers have expressed a willingness to consider alternate sources of magnetite for future needs.

## **10.0 RESULTS AND CONCLUSIONS**

All fifteen holes drilled on the Lodestone Property encountered the magnetite rich hornblende clinopyroxenite unit. No other lithologies were noted in drill core, with the exception of a narrow porphyritic dike of intermediate composition in drill hole L03-14. Good core recoveries were achieved, only two holes returned recoveries below 90%. The pyroxenite unit is moderately to well fractured in all of the drill holes over the depths tested by the drill program. A number of structural linears noted on airphotos and topographic depressions in the Lodestone Mountain area support the interpretation of faulting. RQD data indicate a rock quality rating of fair. This would suggest that pit walls for any possible future mining scenario would likely require moderate slopes.

Results of the Davis Tube analyses were very encouraging, providing average percent magnetite contents per drill hole ranging from 19.54% to 27.25%. The average magnetite content for all holes to a nominal depth of 65 meters is 24.33%. The soluble iron method, employed in previous studies, required a conversion factor ( $\% \text{ soluble Fe} \times 1.1$ ) - 4.18 = % magnetic iron), and indicated an average of 14% magnetite over a larger area. Duplicate magnetite analyses representing 11% of the total number of samples analyzed, generally show good reproducibility. A graph indicating the correlation between original and duplicate samples is presented in Appendix B.

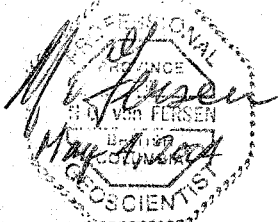
Magnetite is pervasively disseminated interstitially between clinopyroxene crystals and also occurs as larger amorphous segregations and irregular clots to nearly massive zones. Visual estimates ranged from 10 to 25%, with occasional short sections of +/- 50%. Interstitial magnetite has an approximate grain size +/- 1.0 mm. that varies with the grain size of the host rock. No significant amounts of pyrite or pyrrhotite were observed in the



core. Hematite alteration of magnetite is irregular and not pervasively developed in drill core. Locally, hematization of more massive magnetite concentrations near structural zones may result in a reduction of magnetite grades.

Although platinum and palladium mineralization has been primarily encountered in association with chromite lenses in dunites in the Tulameen Complex, it would be expedient to analyse selected composite samples from each of the fifteen holes for platinum group elements.

A revised resource calculation, compliant with the requirements of NI 43-101 and based on the results of the fifteen hole diamond drilling program recommended by Tindall and Miller-Tait, has defined a measured resource of 2.035 million tonnes grading 24.33% magnetite.



## REFERENCES

Nixon, G.T., Hammack, J.L., et al: (March 1997); Geology and Platinum-Group-Element Mineralization of Alaskan Type Ultramafic Complexes in British Columbia; Chapter 9; B.C. Ministry of Employment and Investment Bull. 93, 141p.

Tindall, M., Miller-Tait, J. (June 5, 2003); Geological Report for the Lodestone Property, Similkameen Mining Division.

Evans & Evans, Inc. (July 2, 2003); Valuation and Related Fairness Opinion, Canley Developments Inc.

Tse, Peter, (January 8, 2002); Scoping Study of Magnetite Recovery; Process Research Associates Ltd.

Certificate of Author

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**CERTIFICATE of AUTHOR**

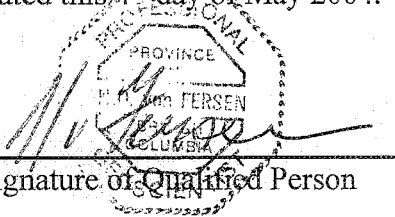
I Nils O. von Fersen, P.Geol., do hereby certify that:

1. I am a geological consultant.
2. I graduated with a degree of B.Sc. in Geology from the University of British Columbia, Vancouver, British Columbia in 1967.
3. I am a member of the Association of Professional Engineers and Geoscientists of British Columbia.
4. I have worked as a Geologist for a total of 36 years since my graduation from university.
5. I have read the definition of "Qualified Person" set out in National Instrument 43-101("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "Qualified Person" for the purposes of NI 43-101.
6. I am responsible for the preparation of all sections of the technical report titled DIAMOND DRILLING REPORT AND RESOURCE CALCULATION FOR THE LODESTONE PROPERTY, SIMILKAMEEN MINING DIVISION, and dated May 4, 2004 (the technical report). I worked on the property from November 12, 2003 to December 17, 2003 as the geologist responsible for the supervision of the diamond drilling program and the logging and sampling of the core.
7. I have not had prior involvement with the property that is the subject of the Technical Report.
8. I am not aware of any material fact or material change with respect to the subject matter of the Technical Report that is not reflected in the Technical Report, the omission to disclose which makes the Technical Report misleading.
9. I am independent of the issuer applying all the tests in section 1.5 of National Instrument 43-101.

10. I have read National Instrument 43-101 and Form 43-101F, and the Technical Report has been prepared in compliance with that instrument and form.

11. I consent to the filing of the Technical Report with any stock exchange and other regulatory authority and any publication by them for regulatory purposes, including electronic publication in the public company files on their websites accessible to the public, of the Technical Report.

Dated this 4<sup>th</sup> day of May 2004.

  
Signature of Qualified Person

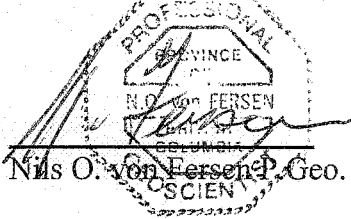
Nils O. von Fersen  
Name of Qualified Person

## CONSENT LETTER

With regard to the report I authored dated May 4, 2004, titled *Diamond Drilling Report and Resource Calculation for the Lodestone Property, Similkameen Mining Division, British Columbia*, for Sargold Resource Corporation.

I consent to having the report filed with any/all regulatory authorities including securities commissions, stock exchanges and I consent to the filing of the report in support of the disclosure in Santoy Resource Corporation's Annual Information Form.

Dated this 4<sup>th</sup> day of May 2004

  
Nils O. von Fersen, P. Geo.

**APPENDIX A**

**DRILL HOLE LOGS**

**L03-1 – L03-15**

## SARGOLD RESOURCES - LODESTONE PROJECT - DRILL LOG

<b>Hole ID:</b> L03-01	<b>Project:</b>	Lodestone Project	<b>Test</b>	Type:	Depth	Az.	Inc.
<b>Length</b> 66.14 m			1				
<b>Hole Azimuth:</b>	<b>Drill Company:</b>	Beaupre Drilling	2				
<b>Hole Inc:</b> Vertical	<b>Drill Start:</b>	Nov. 27/03	3				
<b>Core Size:</b> NQ	<b>Drill Finish:</b>	Nov. 27/03	4				
	<b>Logged By:</b>	N. von Fersen					

Main Unit			Geology	Sampling			Assay			
From	To	Length (m)	Comments	From	To	Length	Sample #			
0.00	4.57	4.57	<b>Casing</b>							
4.57	20.42	15.85	<b>Hornblende Clinopyroxenite</b> - dark greenish grey, mottled, medium to coarse grained, equigranular. Occasional short sections of very coarse hornblende/pyroxene intergrowths. Strongly magnetic, magnetite primarily occurs interstitial to pyroxene/hornblende and as irregular more concentrated blobs or segregations. Host rock is weakly to moderately altered, clinopyroxenes are serpentinized, biotite/vermiculite?, hornblende appears fresher. Stringers and veinlets of talc/sepiolite/carbonate. Serpentine/chlorite/carbonate common on fractures. Hematite stain on fractures near surface and associated with magnetite blobs. Occasional spec of pyrite associated with late stage carbonate/chlorite stringer. Magnetite content is difficult to estimate. Range 10-20%							
20.42	36.58	16.16	<b>as above</b> - medium grained with minor coarse grained sections. Clinopyroxene/hornblende crystal shapes are indistinct and irregular. Pyroxenes are altered to greenish colour, hornblendes are chloritized. Magnetite content is estimated at 10-20%							
36.58	52.73	16.15	<b>Hornblende Clinopyroxenite</b> - mottled greenish grey, medium grained, equigranular, massive. A few hairline stringers and veinlets of sepiolite/talc/carbonate with lesser quartz and chlorite, mainly oriented at 45-70 deg. To CA. Magnetite content estimated to range from 10-15%, disseminated							
52.73	66.14	13.41	<b>as above</b> - coarse grained sections at 53.50-54.25m, 56.16-56.46m, 58.58-63.90m.							
			<b>END OF HOLE</b>							































Hole ID: L03-14			Project:	Lodestone Project								
64.31	85.73	21.42	Hornblende Clinopyroxenite - medium - coarse grained, mottled, greenish, equigranular. Weak to moderately altered, rare, short interval of hornblendite partially altered to actinolite/biotite. Magnetite primarily interstitial with occasional blobs or semi-massive aggregates (5-10 cm). Occasional red hematite alteration spots in areas of larger concentrations. Hematite, carbonate, slickensides on fracture surfaces. Estimated magnetite content 15-20%.									
85.73	108.74	23.01	Hornblende Clinopyroxenite - 85.73-87.68m. as above with large blotches of hematite. 87.68-88.60m. very coarse grained 88.60-89.65m. fine to medium grained mafic dike. 89.65-94.70m. as above hornblende clinopyroxenite with moderate hematite									
108.74	131.07	22.33	as above - v.c.grained continues to 111.80m. Coarse to medium grained for the remainder of interval, interstitial magnetite with fewer amorphous segregations. Few carbonate stringers/veinlets, overall less altered than up-hole. Broken core continues to 117m. Strong hematite alteration dies off below 117m. Estimated magnetite concentration 15-20%									
131.07	142.24	11.17	Hornblende Clinopyroxenite - as above, minor hematite alteration, fractures II CA, slickensides to 139.11m. 139.11-143m. - fine grained intermediate porphyritic dike, narrow chill margins. Estimated magnetite content 10-15%									
142.24	150.57	8.33	Hornblende Clinopyroxenite - 143m to end of hole. Moderately altered and carbonate veined, c.-m. grained, some hematite staining of amorphous magnetite concentrations. Last 50 cm are very coarse grained. Estimated magnetite content 15-20%									
END OF HOLE				L03-14	Page 2							



**APPENDIX B**

**DAVIS TUBE MAGNETITE ANALYSES**

**AND**

**SPECIFIC GRAVITY RESULTS**

LODESTONE PROJECT

DUPLICATE ANALYSES

Sample #	Sample wt g	Mag Tare g	Mag Gross g	Mag Net g	Original	Duplicate
					Total Mag %	Total Mag %
22122	20.00	0.96	7.22	6.26	31.3	30.4
22102	20.00	0.55	6.47	5.92	29.6	28.9
22136	20.00	1.22	4.53	3.31	16.6	16.5
22160	20.00	1.19	9.70	8.51	42.6	40.5
22181	20.00	1.14	4.56	3.42	17.1	16.6
22171	20.00	1.15	5.99	4.84	24.2	23.7
22196	20.00	1.23	5.75	4.52	22.6	22.2
22212	20.00	1.11	3.90	2.79	14.0	13.4
22249	20.00	1.01	5.93	4.92	24.6	23.0
22264	20.00	1.07	7.34	6.27	31.4	28.2
22273	20.00	1.00	5.11	4.11	20.6	19.5
22296	20.00	1.14	3.88	2.74	13.7	13.6
22303	20.00	1.08	4.18	3.10	15.5	15.1
22316	20.00	1.25	5.25	4.00	20.0	17.8
22328	20.00	1.23	12.09	10.86	54.3	54.4
22336	20.00	1.24	6.21	4.97	24.9	26.8
22362	20.00	1.06	8.28	7.22	36.1	34.1
22394	20.00	1.03	4.80	3.77	18.9	20.0
22405	20.00	1.02	3.09	2.07	10.4	11.4
22432	20.00	1.11	7.02	5.91	29.6	28.2
22358	20.00	1.08	6.30	5.22	26.1	26.1
22382	20.00	1.04	4.27	3.23	16.2	16.3
22400	20.00	1.04	3.49	2.45	12.3	12.4
22422	20.00	1.03	5.35	4.32	21.6	21.7
22440	20.00	0.98	6.07	5.09	25.5	25.5
22294	20.00	1.18	6.75	5.57	27.9	28.5
22299	20.00	1.08	6.30	5.22	26.1	26.8
22305	20.00	1.25	5.41	4.16	20.8	21.3
22323	20.00	1.12	5.70	4.58	22.9	23.1
22345	20.00	1.18	5.41	4.23	21.2	21.1
22236	20.00	1.11	5.15	4.04	20.2	20.0
22239	20.00	1.09	6.41	5.32	26.6	26.5
22268	20.00	1.07	5.36	4.29	21.5	21.5
22179	20.00	1.14	5.58	4.44	22.2	21.9
22200	20.00	1.21	6.10	4.89	24.5	23.5
22223	20.00	1.11	5.18	4.07	20.4	19.4
22126	20.00	0.99	6.25	5.26	26.3	25.4
22150	20.00	1.25	6.35	5.10	25.5	23.9
22157	20.00	1.10	5.79	4.69	23.5	22.4

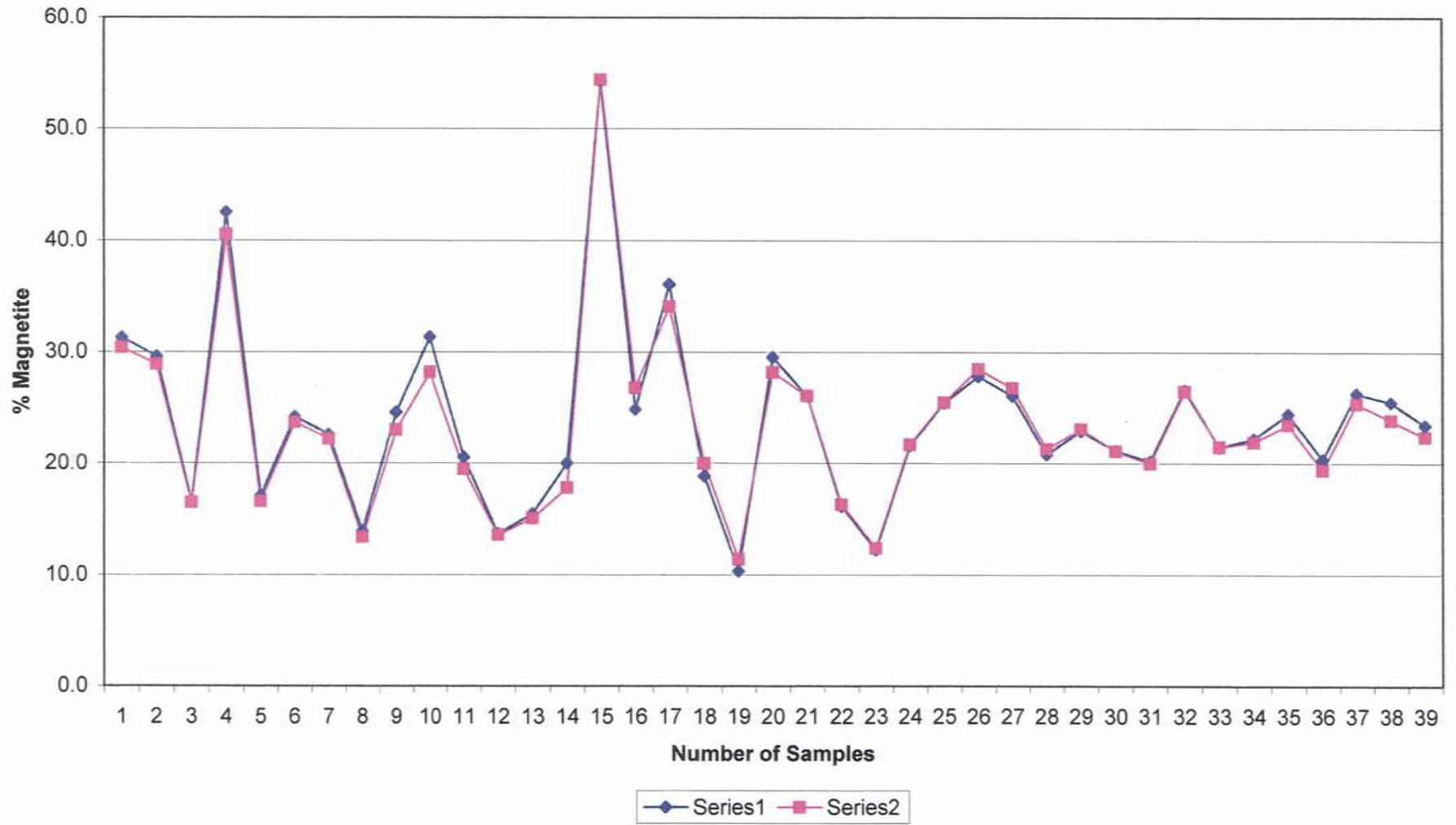
# LODESTONE PROJECT

## Specific Gravity Determinations

Sample #	Split Wt. (grams)	Volume (mL)	S. G.	% Mag
22110	513.1	150	3.42	26.00
22122	507.0	144	3.52	31.30
22130	503.1	146	3.45	27.90
22139	511.6	156	3.28	20.90
22153	499.2	144	3.47	26.50
22165	510.4	161	3.17	23.60
22173	506.5	147	3.45	26.10
22181	507.2	163	3.11	17.10
22196	507.8	150	3.39	22.60
22207	498.7	150	3.32	18.70
22214	505.4	153	3.30	29.20
22230	514.1	152	3.38	20.40
22237	511.2	147	3.48	24.50
22247	503.6	151	3.34	23.80
22255	504.8	148	3.41	30.70
22266	502.9	146	3.44	24.40
22278	509.0	146	3.49	25.30
22286	503.1	149	3.38	26.20
22297	504.0	172	2.93	26.70
22308	499.5	161	3.10	19.10
22317	512.3	148	3.46	25.60
22324	506.3	143	3.54	34.50
22336	505.9	150	3.37	24.90
22345	516.1	159	3.25	21.20
22358	512.3	152	3.37	26.10
22369	520.2	169	3.08	17.30
22378	503.7	150	3.36	26.70
22394	504.5	152	3.32	18.90
22414	514.2	155	3.32	22.80
22419	508.6	155	3.28	19.60
22424	511.3	153	3.34	21.10
22436	503.4	147	3.42	27.30



### Lodestone Project Magnetite Analysis original vs. duplicate



SARGOLD RESOURCE CORP

LODESTONE PROJECT - DAVIS TUBE RESULTS

Hole #	From	To	Length	Sample #	Sample wt	Mag Tare	Mag Gross	Mag Net	Total Mag	L x Mag%	Av. Grade
	(m)	(m)	(m)		g	g	g	g	%		
L03-01	4.57	5.18	0.61	22101	20.00	0.56	4.86	4.30	21.5	13.12	
	5.18	8.23	3.05	22102	20.00	0.55	6.47	5.92	29.6	90.28	
	8.23	11.28	3.05	22103	20.00	0.54	4.86	4.32	21.6	65.88	
	11.28	14.33	3.05	22104	20.00	0.57	6.16	5.59	28.0	85.25	
	14.33	17.37	3.04	22105	20.00	0.56	5.18	4.62	23.1	70.22	
	17.37	20.42	3.05	22106	20.00	0.98	6.18	5.20	26.0	79.30	
	20.42	23.47	3.05	22107	20.00	0.97	4.90	3.93	19.7	59.93	
	23.47	24.99	1.52	22108	20.00	0.98	6.45	5.47	27.4	41.57	
	24.99	26.52	1.53	22109	20.00	0.97	7.19	6.22	31.1	47.58	
	26.52	29.57	3.05	22110	20.00	0.97	6.17	5.20	26.0	79.30	
	29.57	31.70	2.13	22111	20.00	1.00	6.05	5.05	25.3	53.78	
	31.70	33.80	2.10	22112	20.00	1.03	5.78	4.75	23.8	49.88	
	33.80	36.58	2.78	22113	20.00	0.97	5.08	4.11	20.6	57.13	
	36.58	40.54	3.96	22114	20.00	0.96	5.35	4.39	22.0	86.92	
	40.54	42.88	2.34	22115	20.00	0.96	5.51	4.55	22.8	53.24	
	42.88	44.81	1.93	22116	20.00	0.98	5.14	4.16	20.8	40.14	
	44.81	47.85	3.04	22117	20.00	0.96	5.41	4.45	22.3	67.64	
	47.85	50.90	3.05	22118	20.00	0.98	5.91	4.93	24.7	75.18	
	50.90	52.73	1.83	22119	20.00	0.98	6.81	5.83	29.2	53.34	
	52.73	55.78	3.05	22120	20.00	0.98	5.71	4.73	23.7	72.13	
	55.78	58.83	3.05	22121	20.00	0.97	6.72	5.75	28.8	87.69	
	58.83	61.87	3.04	22122	20.00	0.96	7.22	6.26	31.3	95.15	
	61.87	64.31	2.44	22123	20.00	0.97	6.46	5.49	27.5	66.98	
	64.31	66.14	1.83	22124	20.00	0.96	6.79	5.83	29.2	53.34	
										1544.98	25.09

Hole #	From	To	Length	Sample #	Sample wt	Mag Tare	Mag Gross	Mag Net	Total Mag	L x Mag%	Av. Grade
	(m)				g	g	g	g	%		
L03-02	4.57	7.62	3.05	22125	20.00	0.97	5.65	4.68	23.4	71.37	
	7.62	10.06	2.44	22126	20.00	0.99	6.25	5.26	26.3	64.17	
	10.06	14.33	4.27	22127	20.00	1.18	5.92	4.74	23.7	101.20	
	14.33	17.37	3.04	22128	20.00	1.20	7.25	6.05	30.3	91.96	
	17.37	20.42	3.05	22129	20.00	1.11	6.73	5.62	28.1	85.71	
	20.42	23.47	3.05	22130	20.00	1.24	6.81	5.57	27.9	84.94	
	23.47	26.52	3.05	22131	20.00	1.15	5.89	4.74	23.7	72.29	
	26.52	29.57	3.05	22132	20.00	1.19	7.65	6.46	32.3	98.52	
	29.57	32.61	3.04	22133	20.00	1.12	6.57	5.45	27.3	82.84	
	32.61	35.97	3.36	22134	20.00	1.14	5.21	4.07	20.4	68.38	
	35.97	38.71	2.74	22135	20.00	1.16	5.63	4.47	22.4	61.24	
	38.71	41.75	3.04	22136	20.00	1.22	4.53	3.31	16.6	50.31	
	41.75	44.81	3.06	22137	20.00	1.12	5.22	4.10	20.5	62.73	
	44.81	47.85	3.04	22138	20.00	1.25	5.07	3.82	19.1	58.06	
	47.85	50.90	3.05	22139	20.00	1.17	5.35	4.18	20.9	63.74	
	50.90	53.45	2.55	22140	20.00	1.22	5.77	4.55	22.8	58.01	
	53.45	57.00	3.55	22141	20.00	1.13	7.03	5.90	29.5	104.73	
	57.00	59.44	2.44	22142	20.00	1.24	5.71	4.47	22.4	54.53	
	59.44	61.26	1.82	22143	20.00	1.16	5.87	4.71	23.6	42.86	
	61.26	64.01	2.75	22144	20.00	1.18	6.84	5.66	28.3	77.83	
	64.01	66.14	2.13	22145	20.00	1.13	5.41	4.28	21.4	45.58	
										1500.99	24.38

Hole #	From (m)	To	Length	Sample #	Sample wt g	Mag Tare g	Mag Gross g	Mag Net g	Total Mag %	L x Mag%	Av. Grade
L03-03	4.57	7.92	3.35	22146	20.00	1.24	6.76	5.52	27.6	92.46	
	7.92	10.14	2.22	22147	20.00	1.17	6.92	5.75	28.8	63.83	
	10.14	13.10	2.96	22148	20.00	1.22	6.08	4.86	24.3	71.93	
	13.10	15.56	2.46	22149	20.00	1.13	6.36	5.23	26.2	64.33	
	15.56	17.38	1.82	22150	20.00	1.25	6.35	5.10	25.5	46.41	
	17.38	19.84	2.46	22151	20.00	1.15	6.55	5.40	27.0	66.42	
	19.84	23.47	3.63	22152	20.00	1.19	6.35	5.16	25.8	93.65	
	23.47	26.52	3.05	22153	20.00	1.12	6.41	5.29	26.5	80.67	
	26.52	29.57	3.05	22154	20.00	1.24	6.02	4.78	23.9	72.90	
	29.57	32.61	3.04	22155	20.00	1.15	6.22	5.07	25.4	77.06	
	32.61	34.75	2.14	22156	20.00	1.19	6.27	5.08	25.4	54.36	
	34.75	37.19	2.44	22157	20.00	1.10	5.79	4.69	23.5	57.22	
	37.19	38.71	1.52	22158	20.00	1.23	6.52	5.29	26.5	40.20	
	38.71	42.06	3.35	22159	20.00	1.16	5.94	4.78	23.9	80.07	
	42.06	44.81	2.75	22160	20.00	1.19	9.70	8.51	42.6	117.01	
	44.81	47.85	3.04	22161	20.00	1.10	6.96	5.86	29.3	89.07	
	47.85	49.68	1.83	22162	20.00	1.24	7.38	6.14	30.7	56.18	
	49.68	51.51	1.83	22163	20.00	1.16	6.07	4.91	24.6	44.93	
	51.51	53.95	2.44	22164	20.00	1.19	5.65	4.46	22.3	54.41	
	53.95	57.00	3.05	22165	20.00	1.14	5.85	4.71	23.6	71.83	
	57.00	60.05	3.05	22166	20.00	1.24	5.29	4.05	20.3	61.76	
	60.05	62.48	2.43	22167	20.00	1.18	7.06	5.88	29.4	71.44	
	62.48	65.34	2.86	22168	20.00	1.18	5.83	4.65	23.3	66.50	
										1594.63	26.24

**SARGOLD RESOURCE CORP**

**LODESTONE PROJECT - DAVIS TUBE RESULTS**

Hole #	From	To	Length (m)	Sample #	Sample wt g	Mag Tare g	Mag Gross g	Mag Net g	Total Mag %	L x Mag % Av. Grade
L03-04	5.57	8.23	2.66	22169	20.00	1.12	8.37	7.25	36.3	96.43
	8.23	11.28	3.05	22170	20.00	1.22	8.85	7.63	38.2	116.36
	11.28	14.33	3.05	22171	20.00	1.15	5.99	4.84	24.2	73.81
	14.33	17.37	3.04	22172	20.00	1.16	5.42	4.26	21.3	64.75
	17.37	20.42	3.05	22173	20.00	1.11	6.32	5.21	26.1	79.45
	20.42	23.47	3.05	22174	20.00	1.23	6.03	4.80	24.0	73.20
	23.47	26.52	3.05	22175	20.00	1.16	6.78	5.62	28.1	85.71
	26.52	29.57	3.05	22176	20.00	1.18	6.16	4.98	24.9	75.95
	29.57	32.61	3.04	22177	20.00	1.10	5.95	4.85	24.3	73.72
	32.61	35.66	3.05	22178	20.00	1.24	4.94	3.70	18.5	56.42
	35.66	38.71	3.05	22179	20.00	1.14	5.58	4.44	22.2	67.71
	38.71	41.76	3.05	22180	20.00	1.17	5.23	4.06	20.3	61.91
	41.76	44.81	3.05	22181	20.00	1.14	4.56	3.42	17.1	52.16
	44.81	47.55	2.74	22182	20.00	1.22	5.43	4.21	21.1	57.68
	47.55	49.99	2.44	22183	20.00	1.14	5.61	4.47	22.4	54.53
	49.99	52.73	2.74	22184	20.00	1.18	5.79	4.61	23.1	63.16
	52.73	55.74	3.01	22185	20.00	1.12	5.36	4.24	21.2	63.81
	55.74	57.00	1.26	22186	20.00	1.24	5.60	4.36	21.8	27.47
	57.00	60.05	3.05	22187	20.00	1.15	6.48	5.33	26.7	81.28
	60.05	62.79	2.74	22188	20.00	1.19	6.06	4.87	24.4	66.72
62.79	65.53	2.74	22189	20.00	1.12	7.05	5.93	29.7	81.24	
										1473.46
										24.57

Hole #	From	To	Length (m)	Sample #	Sample wt g	Mag Tare g	Mag Gross g	Mag Net g	Total Mag %	L x Mag %	Av. Grade
L03-05	3.66	7.62	3.96	22190	20.00	1.21	5.51	4.30	21.5	85.14	
	7.62	10.67	3.05	22191	20.00	1.14	5.39	4.25	21.3	64.81	
	10.67	14.33	3.66	22192	20.00	1.16	5.49	4.33	21.7	79.24	
	14.33	17.37	3.04	22193	20.00	1.12	5.38	4.26	21.3	64.75	
	17.37	20.12	2.75	22194	20.00	1.23	5.15	3.92	19.6	53.90	
	20.12	23.47	3.35	22195	20.00	1.14	5.39	4.25	21.3	71.19	
	23.47	26.52	3.05	22196	20.00	1.23	5.75	4.52	22.6	68.93	
	26.52	29.57	3.05	22197	20.00	1.16	5.83	4.67	23.4	71.22	
	29.57	32.61	3.04	22198	20.00	1.15	6.14	4.99	25.0	75.85	
	32.61	35.66	3.05	22199	20.00	1.13	6.05	4.92	24.6	75.03	
	35.66	38.71	3.05	22200	20.00	1.21	6.10	4.89	24.5	74.57	
	38.71	40.84	2.13	22201	20.00	1.14	5.44	4.30	21.5	45.80	
	40.84	44.50	3.66	22202	20.00	1.16	4.46	3.30	16.5	60.39	
	44.50	47.85	3.35	22203	20.00	1.14	5.21	4.07	20.4	68.17	
	47.85	50.90	3.05	22204	20.00	1.22	6.35	5.13	25.7	78.23	
	50.90	53.64	2.74	22205	20.00	1.16	5.83	4.67	23.4	63.98	
	53.64	57.00	3.36	22206	20.00	0.99	4.98	3.99	20.0	67.03	
	57.00	60.05	3.05	22207	20.00	1.06	4.80	3.74	18.7	57.03	
	60.05	63.09	3.04	22208	20.00	1.08	6.12	5.04	25.2	76.61	
	63.09	65.53	2.44	22209	20.00	1.02	5.56	4.54	22.7	55.39	
										1357.26	21.93

Hole #	From	To	Length (m)	Sample #	Sample wt g	Mag Tare g	Mag Gross g	Mag Net g	Total Mag %	L x Mag % Av. Grade
L03-05	3.66	7.62	3.96	22190	20.00	1.21	5.51	4.30	21.5	85.14
	7.62	10.67	3.05	22191	20.00	1.14	5.39	4.25	21.3	64.81
	10.67	14.33	3.66	22192	20.00	1.16	5.49	4.33	21.7	79.24
	14.33	17.37	3.04	22193	20.00	1.12	5.38	4.26	21.3	64.75
	17.37	20.12	2.75	22194	20.00	1.23	5.15	3.92	19.6	53.90
	20.12	23.47	3.35	22195	20.00	1.14	5.39	4.25	21.3	71.19
	23.47	26.52	3.05	22196	20.00	1.23	5.75	4.52	22.6	68.93
	26.52	29.57	3.05	22197	20.00	1.16	5.83	4.67	23.4	71.22
	29.57	32.61	3.04	22198	20.00	1.15	6.14	4.99	25.0	75.85
	32.61	35.66	3.05	22199	20.00	1.13	6.05	4.92	24.6	75.03
	35.66	38.71	3.05	22200	20.00	1.21	6.10	4.89	24.5	74.57
	38.71	40.84	2.13	22201	20.00	1.14	5.44	4.30	21.5	45.80
	40.84	44.50	3.66	22202	20.00	1.16	4.46	3.30	16.5	60.39
	44.50	47.85	3.35	22203	20.00	1.14	5.21	4.07	20.4	68.17
	47.85	50.90	3.05	22204	20.00	1.22	6.35	5.13	25.7	78.23
	50.90	53.64	2.74	22205	20.00	1.16	5.83	4.67	23.4	63.98
	53.64	57.00	3.36	22206	20.00	0.99	4.98	3.99	20.0	67.03
	57.00	60.05	3.05	22207	20.00	1.06	4.80	3.74	18.7	57.03
	60.05	63.09	3.04	22208	20.00	1.08	6.12	5.04	25.2	76.61
	63.09	65.53	2.44	22209	20.00	1.02	5.56	4.54	22.7	55.39
									1357.26	21.93

**SARGOLD RESOURCE CORP**

**LODESTONE PROJECT - DAVIS TUBE RESULTS**

Hole #	From	To	Length	Sample #	Sample wt	Mag Tare	Mag Gross	Mag Net	Total Mag	L x Mag %	Av. Grade
					g	g	g	g	%		
L03-07	3.35	6.71	3.36	22230	20.00	1.05	7.02	5.97	29.9	100.30	
	6.71	9.75	3.04	22231	20.00	1.08	5.57	4.49	22.5	68.25	
	9.75	12.80	3.05	22232	20.00	1.08	5.77	4.69	23.5	71.52	
	12.80	15.29	2.49	22233	20.00	0.99	5.00	4.01	20.1	49.92	
	15.29	17.37	2.08	22234	20.00	1.05	5.98	4.93	24.7	51.27	
	17.37	20.62	3.25	22235	20.00	1.06	6.22	5.16	25.8	83.85	
	20.62	24.08	3.46	22236	20.00	1.11	5.15	4.04	20.2	69.89	
	24.08	27.05	2.97	22237	20.00	1.03	5.93	4.90	24.5	72.77	
	27.05	30.78	3.73	22238	20.00	1.04	5.97	4.93	24.7	91.94	
	30.78	32.61	1.83	22239	20.00	1.09	6.41	5.32	26.6	48.68	
	32.61	35.66	3.05	22240	20.00	1.10	6.11	5.01	25.1	76.40	
	35.66	37.80	2.14	22241	20.00	1.01	7.55	6.54	32.7	69.98	
	37.80	40.54	2.74	22242	20.00	1.06	5.93	4.87	24.4	66.72	
	40.54	43.59	3.05	22243	20.00	1.07	5.96	4.89	24.5	74.57	
	43.59	46.94	3.35	22244	20.00	1.07	5.59	4.52	22.6	75.71	
	46.94	50.90	3.96	22245	20.00	1.00	4.84	3.84	19.2	76.03	
	50.90	54.25	3.35	22246	20.00	1.08	5.92	4.84	24.2	81.07	
	54.25	57.30	3.05	22247	20.00	1.07	5.83	4.76	23.8	72.59	
	57.30	59.44	2.14	22248	20.00	1.07	5.88	4.81	24.1	51.47	
	59.44	62.48	3.04	22249	20.00	1.01	5.93	4.92	24.6	74.78	
62.48	65.23	2.75	22250	20.00	1.07	5.52	4.45	22.3	61.19		
										<b>1,488.91</b>	<b>24.06</b>



Hole #	From	To	Length	Sample #	Sample wt g	Mag Tare g	Mag Gross g	Mag Net g	Total Mag %	L x Mag % Av. Grade
L03-08	4.88	8.23	3.35	22251	20.00	1.10	5.19	4.09	20.5	68.51
	8.23	10.67	2.44	22252	20.00	1.08	5.82	4.74	23.7	57.83
	10.67	13.72	3.05	22253	20.00	1.00	5.55	4.55	22.8	69.39
	13.72	16.76	3.04	22254	20.00	1.03	6.29	5.26	26.3	79.95
	16.76	19.81	3.05	22255	20.00	1.11	7.24	6.13	30.7	93.48
	19.81	22.86	3.05	22256	20.00	1.06	5.90	4.84	24.2	73.81
	22.86	25.91	3.05	22257	20.00	1.02	5.95	4.93	24.7	75.18
	25.91	28.96	3.05	22258	20.00	1.06	6.54	5.48	27.4	83.57
	28.96	32.02	3.06	22259	20.00	1.09	6.00	4.91	24.6	75.12
	32.02	35.04	3.02	22260	20.00	1.09	6.32	5.23	26.2	78.97
	35.04	38.10	3.06	22261	20.00	1.02	6.12	5.10	25.5	78.03
	38.10	41.45	3.35	22262	20.00	1.06	6.13	5.07	25.4	84.92
	41.45	44.50	3.05	22263	20.00	1.09	6.68	5.59	28.0	85.25
	44.50	47.55	3.05	22264	20.00	1.07	7.34	6.27	31.4	95.62
	47.55	50.60	3.05	22265	20.00	1.00	5.96	4.96	24.8	75.64
	50.60	53.68	3.08	22266	20.00	1.05	5.93	4.88	24.4	75.15
	53.68	56.70	3.02	22267	20.00	1.11	5.82	4.71	23.6	71.12
	56.70	59.75	3.05	22268	20.00	1.07	5.36	4.29	21.5	65.42
	59.75	62.80	3.05	22269	20.00	1.02	5.62	4.60	23.0	70.15
	62.80	64.92	2.12	22270	20.00	1.07	6.76	5.69	28.5	60.31
									1,517.43	25.27

Hole #	From	To	Length	Sample #	Sample wt g	Mag Tare g	Mag Gross g	Mag Net g	Total Mag %	L x Mag % Av. Grade
L03-09	4.88	7.92	3.04	22271	20.00	1.09	5.86	4.77	23.9	72.50
	7.92	10.97	3.05	22272	20.00	1.08	6.69	5.61	28.1	85.55
	10.97	14.13	3.16	22273	20.00	1.00	5.11	4.11	20.6	64.94
	14.13	17.37	3.24	22274	20.00	1.09	6.87	5.78	28.9	93.64
	17.37	20.42	3.05	22275	20.00	1.10	6.98	5.88	29.4	89.67
	20.42	23.57	3.15	22276	20.00	1.07	5.96	4.89	24.5	77.02
	23.57	26.52	2.95	22277	20.00	1.01	7.43	6.42	32.1	94.70
	26.52	29.57	3.05	22278	20.00	1.07	6.13	5.06	25.3	77.17
	29.57	32.00	2.43	22279	20.00	1.08	4.89	3.81	19.1	46.29
	32.00	35.05	3.05	22280	20.00	1.09	6.12	5.03	25.2	76.71
	35.05	38.10	3.05	22281	20.00	1.04	5.40	4.36	21.8	66.49
	38.10	41.18	3.08	22282	20.00	1.07	5.40	4.33	21.7	66.68
	41.18	44.54	3.36	22283	20.00	1.08	5.41	4.33	21.7	72.74
	44.54	47.85	3.31	22284	20.00	1.09	5.76	4.67	23.4	77.29
	47.85	50.60	2.75	22285	20.00	1.03	5.51	4.48	22.4	61.60
	50.60	53.64	3.04	22286	20.00	1.07	6.30	5.23	26.2	79.50
	53.64	56.69	3.05	22287	20.00	1.20	4.05	2.85	14.3	43.46
	56.69	60.05	3.36	22288	20.00	1.13	5.97	4.84	24.2	81.31
	60.05	63.09	3.04	22289	20.00	1.17	6.07	4.90	24.5	74.48
	63.09	65.53	2.44	22290	20.00	1.21	6.23	5.02	25.1	61.24
									1,462.98	24.12

SARGOLD RESOURCE CORP.

LODESTONE PROJECT - DAVIS TUBE RESULTS

Hole #:	From	To	Length	Sample #	Sample wt g	Mag Tare g	Mag Gross g	Mag Net g	Total Mag %	L x Mag%	Av. Grade
LJ3-10	4.15	7.32	3.17	22291	20.00	1.09	5.81	4.72	23.6	74.81	
	7.32	9.75	2.43	22292	20.00	1.13	6.26	5.13	25.7	62.33	
	9.75	12.80	3.05	22293	20.00	1.21	5.81	4.60	23.0	70.15	
	12.80	15.85	3.05	22294	20.00	1.18	6.75	5.57	27.9	84.94	
				22294d	20.00	1.15	6.85	5.70	28.5	0.00	
	15.85	20.42	4.57	22295	20.00	1.08	6.42	5.34	26.7	122.02	
	20.42	23.47	3.05	22296	20.00	1.14	3.88	2.74	13.7	41.79	
	23.47	26.52	3.05	22297	20.00	1.23	6.57	5.34	26.7	81.44	
	26.52	29.57	3.05	22298	20.00	1.17	5.85	4.68	23.4	71.37	
	29.57	32.61	3.04	22299	20.00	1.08	6.30	5.22	26.1	79.34	
				22299d	20.00	1.09	6.45	5.36	26.8	0.00	
	32.61	35.66	3.05	22300	20.00	1.10	6.54	5.44	27.2	82.96	
	35.66	38.71	3.05	22301	20.00	1.21	4.83	3.62	18.1	55.21	
	38.71	41.76	3.05	22302	20.00	1.18	5.51	4.33	21.7	66.03	
	41.76	44.81	3.05	22303	20.00	1.08	4.18	3.10	15.5	47.28	
	44.81	47.55	2.74	22304	20.00	1.13	4.04	2.91	14.6	39.87	
	47.55	50.90	3.35	22305	20.00	1.25	5.41	4.16	20.8	69.68	
				22305d	20.00	1.11	5.36	4.25	21.3	0.00	
	50.90	53.95	3.05	22306	20.00	1.17	6.42	5.25	26.3	80.06	
	53.95	57.00	3.05	22307	20.00	1.10	5.46	4.36	21.8	66.49	
57.00	60.05	3.05	22308	20.00	1.12	4.93	3.81	19.1	58.10		
60.05	63.09	3.04	22309	20.00	1.24	5.22	3.98	19.9	60.50		
63.09	66.14	3.05	22310	20.00	1.18	5.17	3.99	20.0	60.85		
									1375.21	22.18	

Hole #	From	To	Length	Sample #	Sample wt g	Mag Tare g	Mag Gross g	Mag Net g	Total Mag %	L x Mag% Av. Grade
L03-11	3.05	7.01	3.96	22311	20.00	1.08	4.84	3.76	18.8	74.45
	7.01	10.06	3.05	22312	20.00	1.24	6.91	5.67	28.4	86.47
	10.06	13.11	3.05	22313	20.00	1.15	5.79	4.64	23.2	70.76
	13.11	16.46	3.35	22314	20.00	1.09	5.80	4.71	23.6	78.89
	16.46	19.51	3.05	22315	20.00	1.13	5.73	4.60	23.0	70.15
	19.51	22.56	3.05	22316	20.00	1.25	5.25	4.00	20.0	61.00
	22.56	25.61	3.05	22317	20.00	1.17	6.28	5.11	25.6	77.93
	25.61	28.66	3.05	22318	20.00	1.09	7.03	5.94	29.7	90.59
	28.66	32.00	3.34	22319	20.00	1.13	4.19	3.06	15.3	51.10
	32.00	35.14	3.14	22320	20.00	1.23	5.58	4.35	21.8	68.30
	35.14	38.21	3.07	22321	20.00	1.16	5.65	4.49	22.5	68.92
	38.21	41.51	3.30	22322	20.00	1.09	5.65	4.56	22.8	75.24
	41.51	44.81	3.30	22323	20.00	1.12	5.70	4.58	22.9	75.57
	44.81	47.85	3.04	22324	20.00	1.26	8.15	6.89	34.5	104.73
	47.85	50.60	2.75	22325	20.00	1.18	6.41	5.23	26.2	71.91
	50.60	53.64	3.04	22326	20.00	1.10	9.33	8.23	41.2	125.10
	53.64	56.39	2.75	22327	20.00	1.12	7.39	6.27	31.4	86.21
	56.39	59.45	3.06	22328	20.00	1.23	12.09	10.86	54.3	166.16
59.45	62.50	3.05	22329	20.00	1.17	9.67	8.50	42.5	129.63	
62.50	66.14	3.64	22330	20.00	1.10	5.85	4.75	23.8	86.45	
									1719.54	27.25

Hole #	From	To	Length	Sample #	Sample wt g	Mag Tare g	Mag Gross g	Mag Net g	Total Mag %	L x Mag% Av. Grade
L03-12	3.35	6.40	3.05	22331	20.00	1.12	6.54	5.42	27.1	82.66
	6.40	9.18	2.78	22332	20.00	1.23	5.94	4.71	23.6	65.47
	9.18	12.25	3.07	22333	20.00	1.17	6.42	5.25	26.3	80.59
	12.25	15.30	3.05	22334	20.00	1.08	6.07	4.99	25.0	76.10
	15.30	18.29	2.99	22335	20.00	1.11	6.33	5.22	26.1	78.04
	18.29	21.30	3.01	22336	20.00	1.24	6.21	4.97	24.9	74.80
	21.30	24.34	3.04	22337	20.00	1.17	5.90	4.73	23.7	71.90
	24.34	27.13	2.79	22338	20.00	1.10	5.28	4.18	20.9	58.31
	27.13	30.19	3.06	22339	20.00	1.14	5.59	4.45	22.3	68.09
	30.19	32.61	2.42	22340	20.00	1.24	4.98	3.74	18.7	45.25
	32.61	35.66	3.05	22341	20.00	1.16	5.02	3.86	19.3	58.86
	35.66	38.97	3.31	22342	20.00	1.09	5.75	4.66	23.3	77.12
	38.97	42.24	3.27	22343	20.00	1.13	4.70	3.57	17.9	58.37
	42.24	45.33	3.09	22344	20.00	1.23	5.24	4.01	20.1	61.95
	45.33	48.41	3.08	22345	20.00	1.18	5.41	4.23	21.2	65.14
	48.41	51.82	3.41	22346	20.00	1.10	6.20	5.10	25.5	86.96
	51.82	55.17	3.35	22347	20.00	1.13	5.85	4.72	23.6	79.06
	55.17	58.22	3.05	22348	20.00	1.24	6.22	4.98	24.9	75.94
	58.22	61.30	3.08	22349	20.00	1.17	7.88	6.71	33.6	103.33
	61.30	65.23	3.93	22350	20.00	1.07	6.10	5.03	25.2	98.84
									1466.78	23.70

SARGOLD RESOURCE CORP

LODESTONE PROJECT - DAVIS TUBE RESULTS

Hole #	From	To	Length	Sample #	Sample wt g	Mag Tare g	Mag Gross g	Mag Net g	Total Mag %	Lx%Mag.	Av. Grade
L03-13	3.35	6.71	3.36	22351	20.00	1.10	6.87	5.77	28.9	96.94	
	6.71	9.76	3.05	22352	20.00	1.23	5.45	4.22	21.1	64.36	
	9.76	12.77	3.01	22353	20.00	1.18	5.67	4.49	22.5	67.57	
	12.77	15.84	3.07	22354	20.00	1.08	7.07	5.99	30.0	91.95	
	15.84	18.90	3.06	22355	20.00	1.09	7.57	6.48	32.4	99.14	
	18.90	21.95	3.05	22356	20.00	1.08	5.56	4.48	22.4	68.32	
	21.95	25.00	3.05	22357	20.00	1.11	5.42	4.31	21.6	65.73	
	25.00	28.05	3.05	22358	20.00	1.08	6.30	5.22	26.1	79.61	
			0.00	22358d	20.00	0.97	6.18	5.21	26.1	0.00	
	28.05	31.05	3.00	22359	20.00	1.04	6.60	5.56	27.8	83.40	
	31.05	34.05	3.00	22360	20.00	1.04	6.97	5.93	29.7	88.95	
	34.05	37.09	3.04	22361	20.00	0.98	6.13	5.15	25.8	78.28	
	37.09	40.14	3.05	22362	20.00	1.06	8.28	7.22	36.1	110.11	
	40.14	43.20	3.06	22363	20.00	1.05	6.52	5.47	27.4	83.69	
	43.20	46.25	3.05	22364	20.00	0.96	5.93	4.97	24.9	75.79	
	46.25	49.30	3.05	22365	20.00	1.04	6.08	5.04	25.2	76.86	
	49.30	52.36	3.06	22366	20.00	1.04	4.92	3.88	19.4	59.36	
	52.36	55.30	2.94	22367	20.00	1.05	4.68	3.63	18.2	53.36	
	55.30	58.40	3.10	22368	20.00	0.97	6.31	5.34	26.7	82.77	
	58.40	61.45	3.05	22369	20.00	1.05	4.50	3.45	17.3	52.61	
61.45	64.01	2.56	22370	20.00	1.05	6.71	5.66	28.3	72.45		
64.01	65.84	1.83	22371	20.00	1.04	11.68	10.64	53.2	97.36		
									1648.60	26.38	

Hole #	From	To	Length	Sample #	Sample wt g	Mag Tare g	Mag Gross g	Mag Net g	Total Mag %	Lx%Mag.	Av. Grade
L03-14	3.48	6.14	2.66	22372	20.00	0.96	7.97	7.01	35.1	93.23	
	6.14	9.11	2.97	22373	20.00	1.04	6.11	5.07	25.4	75.29	
	9.11	11.28	2.17	22374	20.00	1.05	5.95	4.90	24.5	53.17	
	11.28	14.33	3.05	22375	20.00	1.03	5.44	4.41	22.1	67.25	
	14.33	17.37	3.04	22376	20.00	0.95	5.49	4.54	22.7	69.01	
	17.37	20.42	3.05	22377	20.00	1.03	5.86	4.83	24.2	73.66	
	20.42	23.47	3.05	22378	20.00	1.04	6.38	5.34	26.7	81.43	
	23.47	26.52	3.05	22379	20.00	1.02	6.15	5.13	25.7	78.23	
	26.52	29.57	3.05	22380	20.00	0.95	5.91	4.96	24.8	75.64	
	29.57	31.70	2.13	22381	20.00	1.02	5.66	4.64	23.2	49.42	
	31.70	34.75	3.05	22382	20.00	1.04	4.27	3.23	16.2	49.26	
			0.00	22382d	20.00	0.97	4.23	3.26	16.3	0.00	
	34.75	37.80	3.05	22383	20.00	1.05	5.73	4.68	23.4	71.37	
	37.80	40.54	2.74	22384	20.00	0.95	5.88	4.93	24.7	67.54	
	40.54	43.60	3.06	22385	20.00	1.05	7.07	6.02	30.1	92.11	
	43.60	46.66	3.06	22386	20.00	1.06	5.91	4.85	24.3	74.20	
	46.66	49.70	3.04	22387	20.00	0.96	6.30	5.34	26.7	81.17	
	49.70	52.91	3.21	22388	20.00	1.04	5.77	4.73	23.7	75.92	
	52.91	56.39	3.48	22389	20.00	1.03	3.90	2.87	14.4	49.94	
	56.39	59.45	3.06	22390	20.00	1.05	4.44	3.39	17.0	51.87	
	59.45	62.50	3.05	22391	20.00	0.95	4.49	3.54	17.7	53.98	av. to 65m
	62.50	65.60	3.10	22392	20.00	1.05	5.11	4.06	20.3	62.93	22.05
	65.60	68.88	3.28	22393	20.00	1.05	4.61	3.56	17.8	58.38	
68.88	71.94	3.06	22394	20.00	1.03	4.80	3.77	18.9	57.68		
71.94	74.84	2.90	22395	20.00	0.93	4.41	3.48	17.4	50.46		
74.84	77.72	2.88	22396	20.00	1.05	4.60	3.55	17.8	51.12		
77.72	80.55	2.83	22397	20.00	0.99	4.07	3.08	15.4	43.58		

Hole #	From	To	Length	Sample #	Sample wt g	Mag Tare g	Mag Gross g	Mag Net g	Total Mag %	Lx%Mag. Av. Grade
L03-14	80.55	83.82	3.27	22398	20.00	1.02	5.71	4.69	23.5	76.68
	83.82	86.88	3.06	22399	20.00	0.94	3.32	2.38	11.9	36.41
	86.88	89.92	3.04	22400	20.00	1.04	3.49	2.45	12.3	37.24
			0.00	22400d	20.00	0.97	3.44	2.47	12.4	0.00
	89.92	92.94	3.02	22401	20.00	1.01	3.60	2.59	13.0	39.11
	92.94	96.00	3.06	22402	20.00	1.03	6.45	5.42	27.1	82.93
	96.00	99.26	3.26	22403	20.00	0.94	3.73	2.79	14.0	45.48
	96.26	102.41	6.15	22404	20.00	1.04	2.68	1.64	8.2	50.43
	102.41	105.46	3.05	22405	20.00	1.02	3.09	2.07	10.4	31.57
	105.46	108.74	3.28	22406	20.00	1.04	3.65	2.61	13.1	42.80
	108.74	111.77	3.03	22407	20.00	0.96	4.53	3.57	17.9	54.09
	111.77	114.96	3.19	22408	20.00	1.04	4.03	2.99	15.0	47.69
	114.96	117.96	3.00	22409	20.00	1.04	3.81	2.77	13.9	41.55
	117.96	121.01	3.05	22410	20.00	1.05	5.04	3.99	20.0	60.85
	121.01	124.05	3.04	22411	20.00	0.95	4.94	3.99	20.0	60.65
	124.05	127.12	3.07	22412	20.00	1.03	4.79	3.76	18.8	57.72
	127.10	130.15	3.05	22413	20.00	1.03	4.72	3.69	18.5	56.27
	130.15	133.20	3.05	22414	20.00	1.05	5.61	4.56	22.8	69.54
	133.20	136.25	3.05	22415	20.00	0.95	5.42	4.47	22.4	68.17
	136.25	139.29	3.04	22416	20.00	1.03	4.87	3.84	19.2	58.37
0.00			22417	no sample						0.00
143.00	144.78	1.78	22418	20.00	1.01	5.18	4.17	20.9	37.11	
144.78	147.83	3.05	22419	20.00	1.05	4.96	3.91	19.6	59.63	
147.83	150.57	2.74	22420	20.00	0.93	4.70	3.77	18.9	51.65	av. for all
									2873.76	19.54



Hole #	From	To	Length	Sample #	Sample wt g	Mag Tare g	Mag Gross g	Mag Net g	Total Mag %	Lx%Mag. Av. Grade
L03-15	3.05	6.10	3.05	22421	20.00	1.02	5.35	4.33	21.7	66.03
	6.10	9.14	3.04	22422	20.00	1.03	5.35	4.32	21.6	65.66
			0.00	22422d	20.00	0.98	5.32	4.34	21.7	0.00
	9.14	12.28	3.14	22423	20.00	1.04	5.51	4.47	22.4	70.18
	12.28	15.33	3.05	22424	20.00	0.94	5.15	4.21	21.1	64.20
	15.33	18.50	3.17	22425	20.00	1.00	5.64	4.64	23.2	73.54
	18.50	21.64	3.14	22426	20.00	1.02	6.18	5.16	25.8	81.01
	21.64	24.38	2.74	22427	20.00	1.05	5.84	4.79	24.0	65.62
	24.38	27.13	2.75	22428	20.00	1.02	5.72	4.70	23.5	64.63
	27.13	30.78	3.65	22429	20.00	1.06	5.52	4.46	22.3	81.40
	30.78	33.83	3.05	22430	20.00	0.96	5.75	4.79	24.0	73.05
	33.83	36.89	3.06	22431	20.00	1.05	5.51	4.46	22.3	68.24
	36.89	39.97	3.08	22432	20.00	1.11	7.02	5.91	29.6	91.01
	39.97	43.09	3.12	22433	20.00	1.19	6.59	5.40	27.0	84.24
	43.09	46.13	3.04	22434	20.00	1.08	6.35	5.27	26.4	80.10
	46.13	49.07	2.94	22435	20.00	1.05	6.25	5.20	26.0	76.44
	49.07	52.10	3.03	22436	20.00	1.11	6.56	5.45	27.3	82.57
	52.10	55.17	3.07	22437	20.00	1.10	6.02	4.92	24.6	75.52
	55.17	57.91	2.74	22438	20.00	1.06	7.76	6.70	33.5	91.79
	57.91	60.93	3.02	22439	20.00	1.00	6.43	5.43	27.2	81.99
60.93	63.09	2.16	22440	20.00	0.98	6.07	5.09	25.5	54.97	
		0.00	22440d	20.00	0.96	6.05	5.09	25.5	0.00	
63.09	65.23	2.14	22441	20.00	0.96	5.71	4.75	23.8	50.83	
									1543.03	24.82

**APPENDIX C**

**GEOTECHNICAL LOGS**

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Nov. 29/03

**HOLE #** L 03-01 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:** 66.14 m

**CORE SIZE:** NQ

Depth m		Recovery			Lithology	RQD (>4")		Rock	Weathering	Joint Cond.	
From	To	Length	Length	Rec. %		Length	%	Hardness	Core	# Joints	Condition
0.00	4.57	4.57			Casing						
4.57	5.18	0.61	0.61	100.00		0.30	49.18	R1	MW	24	12
5.18	8.23	3.05	3.05	100.00		0.95	31.15	R2	MW	22	6
8.23	11.28	3.05	3.05	100.00		2.25	73.77	R2	MW	18	12
11.28	14.33	3.05	3.05	100.00		1.58	51.80	R2	MW	22	12
14.33	17.37	3.04	3.04	100.00		2.44	80.26	R2	MW	14	12
17.37	20.42	3.05	3.05	100.00		1.26	41.31	R2	MW	28	6
20.42	23.47	3.05	2.70	88.52		1.70	55.74	R2	SW	21	12
23.47	24.99	1.52	1.52	100.00		0.62	40.79	R2	SW	23	20
24.99	26.52	1.52	2.13	140.13		0.68	44.74	R2	SW	19	20
26.52	29.57	3.05	2.52	82.62		1.58	51.80	R2	SW	32	20
29.57	31.09	1.52	1.45	95.39		0.00	0.00	R2	SW	24	20
31.09	31.70	0.61	0.61	100.00		0.28	45.90	R2	SW	17	20
31.70	32.92	1.22	0.90	73.77		0.00	0.00	R2	SW	23	20
32.92	33.83	0.91	1.40	153.85		0.49	53.85	R2	SW	14	20
33.83	34.44	0.61	0.61	100.00		0.23	37.70	R2	SW	27	20
34.44	36.58	2.14	2.14	100.00		0.85	39.72	R2	SW	23	20

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 13/03

**HOLE #** L 03-01 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:** 66.14 m

**CORE SIZE:** NQ

From	Depth m		Recovery		Lithology	RQD (>4")		Rock Hardness	Weathering Core	Joint Cond.	
	To	Length	Length	Rec. %		Length	%			# Joints	Condition
36.58	37.49	0.91	0.75	82.42		0.15	16.48	R2	SW	26	12
37.49	40.54	3.05	3.05	100.00		2.35	77.05	R2	SW	18	12
40.54	41.76	1.22	1.32	108.20		1.03	84.43	R2	SW	24	12
41.76	44.81	3.05	2.95	96.72		2.27	74.43	R2	SW	21	12/6
44.81	47.85	3.04	3.03	99.67		2.07	68.09	R2	SW	20	12
47.85	50.90	3.05	3.05	100.00		3.00	98.36	R2	SW	14	20
50.90	52.73	1.83	1.83	100.00		1.17	63.93	R2	SW	19	20
52.73	55.78	3.05	3.05	100.00		2.26	74.10	R2	SW	20	20
55.78	58.83	3.05	3.05	100.00		2.63	86.23	R2	SW	22	20
58.83	61.87	3.04	3.10	101.97		3.00	98.68	R2	SW	18	20
61.87	64.31	2.44	2.44	100.00		1.75	71.72	R2	SW	22	20
64.31	66.14	1.83	1.81	98.91		1.56	85.25	R2	SW	19	20

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Nov 30/03

**HOLE #** L03-02 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:** 66.14 m

**CORE SIZE:** NQ

From	Depth m		Recovery			Lithology	RQD (>4")		Rock Hardness	Weathering Core	Joint Cond.	
	To	Length	Length	Rec. %	Length		%	# Joints			Condition	
0.00	4.57					CASING						
4.57	7.62	3.05	3.05	100.00		2.65	86.89	R2	SW	16/20	25	
7.62	10.06	2.44	2.44	100.00		1.61	65.98	R2	SW	26/20	20	
10.06	11.28	1.22	1.22	100.00		0.97	79.51	R2	SW	8/20	25	
11.28	14.33	3.05	3.05	100.00		2.03	66.56	R2	SW	26/20	25	
14.33	17.37	3.04	3.04	100.00		2.70	88.82	R2	FR	14/20	25	
17.37	20.42	3.05	3.05	100.00		2.13	69.84	R2	FR	30	20/25	
20.42	23.47	3.05	3.05	100.00		2.60	85.25	R2	FR	22	25	
23.47	26.51	3.04	3.04	100.00		2.60	85.53	R2	FR	19	25	
26.51	29.57	3.06	3.06	100.00		1.70	55.56	R2	FR	29	25	
29.57	32.61	3.04	3.04	100.00		2.10	69.08	R2	FR	26	25	
32.61	35.05	2.44	2.44	100.00		0.97	39.75	R2	FR	30	12	
35.05	35.97	0.92	0.92	100.00		0.35	38.04	R2	FR	14	12	
35.97	38.71	2.74	2.64	96.35		1.87	68.25	R2	FR	15	20	
38.71	41.75	3.04	3.04	100.00		2.55	83.88	R2	FR	16	20/25	
41.75	44.81	3.06	3.06	100.00		2.33	76.14	R2	FR	26	25	
44.81	47.85	3.04	3.04	100.00		2.38	78.29	R2	FR	22	25	



**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Nov 30 - Dec 1/03

**HOLE #** L03-03

**NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:** 65.34

**CORE SIZE:** NQ

Depth m		Recovery			Lithology	RQD (>4")		Rock	Weathering	Joint Cond.	
From	To	Length	Length	Rec. %		Length	%	Hardness	Core	# Joints	Condition
0.00	4.57	0.00			CASING	0.00					
4.57	7.92	3.35	2.90	86.57		0.97	28.96	R2	SW	>30	6
7.92	8.84	0.92	0.92	100.00		0.39	42.39	R2	SW	11	6\12
8.84	11.28	2.44	2.44	100.00		1.85	75.82	R2	SW	19	6\12
11.28	13.10	1.82	1.82	100.00		0.85	46.70	R2	SW	16	12
13.10	14.33	1.23	1.23	100.00		1.04	84.55	R2	SW	7	12
14.33	17.37	3.04	3.04	100.00		2.36	77.63	R2	SW	15	12
17.37	19.81	2.44	2.44	100.00		0.88	36.07	R2	SW	27	6
19.81	22.56	2.75	2.60	94.55		1.80	65.45	R2	SW	19	12
22.56	23.47	0.91	1.01	110.99		0.80	87.91	R2	SW	7	12
23.47	26.52	3.05	3.05	100.00		2.12	69.51	R2	SW	20	12
26.52	29.57	3.05	3.05	100.00		2.30	75.41	R2	SW	20	12
29.57	32.61	3.04	3.04	100.00		1.95	64.14	R2	SW	31	6\12
32.61	34.75	2.14	2.14	100.00		0.87	40.65	R2	SW	25	6\12
34.75	37.19	2.44	2.44	100.00		1.50	61.48	R2	SW	22	12
37.19	38.71	1.52	1.52	100.00		0.80	52.63	R2	SW	18	12
38.71	41.45	2.74	2.74	100.00		1.16	42.34	R2	SW	29	6\12

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Nov 30/03 & Dec 1/03

**HOLE #** L03-03

**NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:** 65.34

**CORE SIZE:** NQ

Depth		Recovery			Lithology	RQD (>4")		Rock Hardness	Weathering Core	Joint Cond.	
From	To	Length	Length	Rec. %		Length	%			# Joints	Condition
41.45	42.06	0.61	0.61	100.00		0.00	0.00	R2	SW	~30	6
42.06	44.81	2.75	2.65	96.36		1.96	71.27	R2	SW	15	12
44.81	47.85	3.04	3.04	100.00		1.05	34.54	R2	SW	36	6
47.85	49.68	1.83	1.83	100.00		0.20	10.93	R2	SW	33	6
49.68	51.51	1.83	1.83	100.00		1.00	54.64	R2	SW	25	6
51.51	53.95	2.44	2.23	91.39		1.60	65.57	R2	SW	7	6
53.95	57.00	3.05	3.05	100.00		2.87	94.10	R2	SW	2	12
57.00	60.05	3.05	3.05	100.00		2.37	77.70	R2	SW	14	12
60.05	62.48	2.43	2.43	100.00		1.70	69.96	R2	SW	22	12
62.48	65.34	2.86	2.86	100.00		1.68	58.74	R2	SW	27	12



**GEOTECHNICAL LOGGING FORM**

PROJECT: Lodestone

LOGGER: N. von Fersen

DATE: Dec 1/03

HOLE # L03-04 NORTHING:

EASTING:

ELEVATION:

AZIMUTH/DIP & DIRECTION:

LENGTH: 65.53 m

CORE SIZE: NQ

From	Depth m		Recovery		Lithology	RQD (>4")		Rock Hardness	Weathering Core	Joint Cond.	
	To	Length	Length	Rec. %		Length	%			# Joints	Condition
0	4.57	4.57	4.57	0	Casing						
4.57	8.23	3.66	3.66	100.00		1.33	36.34	R2	SW	24	12
8.23	11.28	3.05	3.05	100.00		2.51	82.30	R2	SW	15	12
11.28	14.33	3.05	3.05	100.00		2.55	83.61	R2	SW	14	20
14.33	17.37	3.05	3.05	100.00		2.67	87.54	R2	SW	14	20
17.37	20.42	3.05	3.05	100.00		2.79	91.48	R2	SW	13	20
20.42	23.47	3.05	3.05	100.00		2.26	74.10	R2	SW	16	20
23.47	26.52	3.05	3.05	100.00		1.80	59.02	R2	SW	22	20
26.52	29.57	3.05	3.05	100.00		2.18	71.48	R2	SW	18	20
29.57	32.61	3.04	3.04	100.00		2.88	94.74	R2	SW	11	20
32.61	35.66	3.05	3.05	100.00		2.00	65.57	R2	SW	20	20
35.66	38.71	3.05	3.05	100.00		1.92	62.95	R2	SW	23	20
38.71	41.76	3.05	3.05	100.00		1.87	61.31	R2	SW	27	12/20
41.76	44.81	3.05	2.80	91.80		1.62	53.11	R2	SW	>30	12/6
44.81	47.55	2.74	2.60	94.89		0.48	17.52	R2	SW	shattered/numorous	6
47.55	49.99	2.44	1.78	72.95		0.60	24.59	R2	SW	31	6
49.99	52.73	2.74	2.14	78.10		1.17	42.70	R2	SW	~30	6
52.73	55.47	2.74	2.74	100.00		1.90	69.34	R2	SW	26	6

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 1/03

**HOLE #** L-03-04 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:** 65.53 m

**CORE SIZE:** NQ

Depth		Recovery			Lithology	RQD (>4")		Rock Hardness	Weathering Joint Cond.		
From	To	Length	Length	Rec. %		Length	%		Core	# Joints	Condition
55.47	57.00	1.53	1.56	101.96		1.35	88.24	R2	SW	9	12
57.00	60.05	3.05	3.05	100.00		1.94	63.61	R2	SW	30	12
60.05	62.79	2.74	2.65	96.72		1.35	49.27	R2	SW	23	12/6
62.79	65.53	2.74	2.74	100.00		2.54	92.70	R2	SW	13	12/6

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 1/03

**HOLE #** L-03-05 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:** 65.53 m

**CORE SIZE:** NQ

Depth m		Recovery			Lithology	RQD (>4")	Rock	Weathering Joint Cond.			
From	To	Length	Length	Rec. %		Length	%	Hardness	Core	# Joints	Condition
0	3.66	3.66	0	0	Casing						
3.66	5.18	1.52	1.12	73.68		0.84	55.26	R2	SW	10	6
5.18	7.62	2.44	1.40	57.38		0.00	0.00	R2	SW	Shattered	6
7.62	10.67	3.05	2.88	94.43		1.67	54.75	R2	SW	26	6
10.67	11.28	0.61	0.60	98.36		0.43	70.49	R2	SW	4	12
11.28	14.33	3.05	3.05	100.00		2.50	81.97	R2	SW	17	12
14.33	17.37	3.04	3.04	100.00		2.00	65.79	R2	SW	18	12
17.37	20.12	2.75	2.55	92.73		1.90	69.09	R2	SW	16	12
20.12	21.95	1.83	1.73	94.54		0.83	45.36	R2	SW	18	12
21.95	23.47	1.52	1.72	113.16		1.53	100.66	R2	SW	8	12
23.47	26.52	3.05	3.05	100.00		2.24	73.44	R2	SW	14	20
26.52	29.57	3.05	3.05	100.00		2.78	91.15	R2	SW	5	25
29.57	32.61	3.04	3.04	100.00		2.50	82.24	R2	SW	16	12
32.61	35.66	3.05	3.05	100.00		1.99	65.25	R2	SW	27	12
35.66	38.71	3.05	3.05	100.00		1.80	59.02	R2	SW	26	12
38.71	40.84	2.13	2.03	97.65		1.67	78.40	R2	SW	9	12
40.84	43.28	2.44	2.30	94.26	Fault or fracture zone 41.74 45.11m	1.04	42.62	R2-1	HW	Shattered	6
43.28	44.50	1.12	0.55	49.11		0.00	0.00	R1-0	HW	Shattered	6\0

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 1/03

**HOLE #** L-03-05 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:** 65.53 m

**CORE SIZE:** NQ

From	Depth m		Recovery		Lithology	RQD (>4")		Rock Hardness	Weathering Joint Cond.		
	To	Length	Length	Rec. %		Length	%		Core	# Joints	Condition
44.50	45.11	0.61	0.61	100.00		0.00	0.00	R1-0	HW	>25	0
45.11	47.85	2.74	2.52	91.97		1.90	69.34	R1	H-MW	25	6
47.85	50.90	3.05	3.05	100.00		2.18	71.48	R1-R2	HW-SW	35	6
50.90	53.64	2.74	2.65	96.72		1.95	71.17	R2	SW	14	12
53.64	55.47	1.83	1.60	87.43		0.96	52.46	R2	SW	25	12/6
55.47	56.39	0.92	1.06	115.22		0.84	91.30	R2	SW-MW	20	12/6
56.39	57.00	0.61	0.61	100.00	fract. ll/ca	0.00	0.00	R1	MW	-	6
57.00	60.05	3.05	2.98	97.70		2.43	79.67	R2	SW	17	12
60.05	63.09	3.04	3.00	98.68		1.87	61.51	R2	SW	27	20
63.09	65.53	2.44	2.40	98.36		1.52	62.30	R2	SW	24	20

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 5/03

**HOLE #** L-03-06 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:** 64.92 m

**CORE SIZE:** NQ

Depth m		Recovery			Lithology	RQD (>4")		Rock Hardness	Weathering Core	Joint Cond.	
From	To	Length	Length	Rec. %		Length	%			# Joints	Condition
0	3.66	3.66	0	0	Casing						
3.66	5.18	1.52	1.20	78.95		0.72	60.00	R2	SW	20	6
5.18	6.40	1.22	0.77	63.11		0.70	90.91	R2	SW	8	12
6.40	7.32	0.92	0.92	100.00		0.44	47.83	R2	SW	17	12
7.32	8.23	0.91	0.80	87.91		0.24	30.00	R2	SW	21	12
8.23	10.36	2.13	1.60	75.12		0.56	35.00	R2	SW	27	12
10.36	12.19	1.83	1.53	83.61		0.70	45.75	R1-2	S-MW	21	6
12.19	14.02	1.83	1.85	101.09		0.44	23.78	R2	SW	31	6
14.02	14.63	0.61	0.32	52.46		0.00	0.00	R1-2	S-MW	9	12
14.63	16.15	1.52	1.16	76.32		0.00	0.00	R1-2	S-MW	17	6
16.15	19.20	3.05	2.86	93.77		1.25	43.71	R2	SW	29	12
19.20	21.64	2.44	2.44	100.00		1.47	60.25	R2	SW	26	12
21.64	23.47	1.83	1.45	79.23		0.98	67.59	R2	SW	25	12
23.47	25.30	1.83	1.83	100.00		0.53	28.96	R1-2	SW	30	6
25.30	25.91	0.61	0.54	88.52		0.10	18.52	R2	SW	7	12
25.91	28.65	2.74	2.64	96.35		2.10	79.55	R2	SW	17	12
28.65	29.57	0.92	0.92	100.00		0.50	54.35	R2	SW	11	12
29.57	32.61	3.04	2.85	93.75		1.52	53.33	R2	SW	29	12

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 5/03

**HOLE #** L-03-06 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:** 64.92 m

**CORE SIZE:** NQ

Depth		Recovery			Lithology	RQD (>4")		Rock Hardness	Weathering Core	Joint Cond.	
From	To	Length	Length	Rec. %		Length	%			# Joints	Condition
32.61	35.66	3.05	3.05	100.00		2.00	65.57	R2	SW	29	12
35.66	38.10	2.44	2.44	100.00		1.52	62.30	R2	SW	22	12
38.10	39.93	1.83	1.70	92.90		0.82	48.24	R2	SW	19	12
39.93	41.76	1.83	1.20	65.57		1.00	83.33	R2	SW	14	12
41.76	44.20	2.44	3.05	125.00		2.50	81.97	R2	SW	20	12
44.20	47.24	3.04	2.95	97.04		2.37	80.34	R2	SW	20	12
47.24	49.99	2.75	2.75	100.00		2.13	77.45	R2	SW	24	12
49.99	52.43	2.44	2.35	96.31		1.53	65.11	R2	SW	26	12
52.43	53.95	1.52	1.52	100.00		1.18	77.63	R2	SW	23	12
53.95	55.78	1.83	1.43	78.14	Str. Fract Zone	0.30	20.98	R2	SW	30	12
55.78	56.39	0.61	0.50	81.97	Fractured Zone	0.00	0.00	R2	SW	20	12
56.39	59.44	3.05	3.00	98.36		2.70	90.00	R2	SW	17	12
59.44	61.87	2.43	2.40	98.77		1.82	75.83	R2	SW	16	12
61.87	64.92	3.05	3.05	100.00		2.08	68.20	R2	SW	19	12

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 5/03

**HOLE #** L-03-07 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:**

**CORE SIZE:** NQ

From	Depth		Recovery		Lithology	RQD (>4")		Rock Hardness	Weathering Core	Joint Cond.	
	To	Length	Length	Rec. %		Length	%			# Joints	Condition
0.00	3.35	3.35	0.00	0	Casing						
3.35	5.18	1.83	1.20	65.57		0.65	35.52	R1-2	SW	15	6
5.18	6.71	1.53	0.80	52.29		0.00	0.00	R1-2	SW	20	6
6.71	8.53	1.82	0.75	41.21	Str Fr Zone	0.00	0.00	R1-2	SW	-	6
8.53	9.75	1.22	0.80	65.57	Str Fr Zone	0.12	9.84	R2	SW	-	6
9.75	11.89	2.14	1.85	86.45		1.04	48.60	R2	SW	26	12
11.89	12.80	0.91	0.91	100.00		0.30	32.97	R2	SW	18	12
12.80	13.72	0.92	0.90	97.83	Fr Zone	0.13	14.13	R2	SW	-	12
13.72	14.63	0.91	0.90	98.90	Fr Zone	0.14	15.38	R2	SW	-	12
14.63	17.37	2.74	2.60	94.89		1.61	58.76	R2	SW	22	12
17.37	20.12	2.75	2.20	80.00	Fr ll/ca Fr Zone	0.49	17.82	R2	SW	-	12
20.12	21.64	1.52	1.48	97.37	Fr Zone ll/ca - 60 deg.	0.45	29.61	R2	SW	-	12
21.64	24.08	2.44	1.80	73.77	Fr Zone	0.32	13.11	R2	SW	-	12
24.08	26.52	2.44	2.50	102.46		1.98	81.15	R2	SW	18	12
26.52	28.96	2.41	2.28	94.61		1.16	48.13	R2	SW	25	12
28.96	30.78	1.82	1.65	90.66		0.56	30.77	R2	SW	21	12
30.78	32.61	1.83	1.80	98.36		0.44	24.04	R2	SW	33	12

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 5/03

**HOLE #** L-03-07 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:** 65.53 m

**CORE SIZE:** NQ

From	Depth		Recovery		Lithology	RQD (>4")		Rock Hardness	Weathering Core	Joint Cond.	
	To	Length	Length	Rec. %		Length	%			# Joints	Condition
32.61	35.66	3.05	3.05	100.00		2.40	78.69	R2	SW	21	
35.66	37.80	2.14	2.10	98.13		1.25	58.41	R2	SW	33	6
37.80	40.54	2.74	2.65	96.72		2.04	74.45	R2	SW	16	6
40.54	43.59	3.05	2.92	95.74		1.50	49.18	R2	SW	31	6
43.59	44.81	1.22	1.20	98.36		0.28	22.95	R2	SW	21	6
44.81	46.94	2.13	1.60	75.12		0.83	38.97	R2	SW	30	12
46.94	48.46	1.52	1.37	90.13		0.33	21.71	R2	SW	25	12
48.46	50.90	2.44	2.38	97.54		0.75	30.74	R2	SW	26	6
50.90	53.04	2.14	2.14	100.00	Fr Sub II ca	0.70	32.71	R2	SW	32	12
53.04	54.25	1.21	1.20	99.17		0.50	41.32	R2	SW	15	12
54.25	55.17	0.92	0.60	65.22		0.12	13.04	R2	SW	11	12
55.17	56.39	1.22	1.22	100.00	Fr zone sub II to -30/ca	0.37	30.33	R2	SW	17	12
56.39	59.44	3.05	2.96	97.05		2.74	89.84	R2	SW	19	12
59.44	62.48	3.04	2.95	97.04		2.47	81.25	R2	SW	16	20
62.48	65.53	3.05	3.02	99.02		2.62	85.90	R2	SW	14	20



**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 6/03

**HOLE #** L-03-08 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:** 64.92 m

**CORE SIZE:** NQ

From	Depth m		Recovery		Lithology	RQD (>4")		Rock Hardness	Weathering Core	Joint Cond.	
	To	Length	Length	Rec. %		Length	%			# Joints	Condition
0.00	4.88	4.88	0.00	0	Casing						
4.88	6.40	1.52	1.50	98.68	Str Fractured	0.12	7.89	R1	MW		6
6.40	8.23	1.83	1.83	100.00		1.62	88.52	R2	SW	13	12
8.23	10.67	2.44	2.44	100.00	Fr Sub ll/ca	1.42	58.20	R1	SW	13	12
10.67	13.72	3.05	3.05	100.00		2.27	74.43	R2	SW	16	12
13.72	16.76	3.04	3.05	100.33		2.40	78.95	R2	SW	18	12
16.76	19.81	3.05	3.05	100.00		2.28	74.75	R2	SW	22	12
19.81	22.86	3.05	3.05	100.00		2.52	82.62	R2	SW	19	12
22.86	25.91	3.05	3.05	100.00		2.20	72.13	R2	SW	26	12
25.91	26.52	0.61	0.47	77.05		0.21	34.43	R2	SW	8	12
26.52	28.65	2.13	2.13	100.00	Fr Zone	0.70	32.86	R2	SW	~40	12
28.65	30.48	1.83	1.76	96.17		1.30	71.04	R2	SW	11	12
30.48	32.61	2.13	1.87	87.79		1.34	62.91	R2	SW	14	12
32.61	34.44	1.83	1.83	100.00		1.43	78.14	R2	SW	17	12
34.44	36.27	1.83	1.83	100.00	Fr Zone	0.82	44.81	R2	SW	33	12
36.27	38.10	1.83	1.80	98.36		1.18	64.48	R2	SW	18	12
*38.10	41.45	3.35	3.35	100.00	Fr 10-45/ca	2.36	70.45	R2	SW	27	12



**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone      **LOGGER:** N. von Fersen      **DATE:** Dec 7/03

**HOLE #** L-03-09    **NORTHING:**      **EASTING:**      **ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**      **LENGTH:** 65.53 m      **CORE SIZE:** NQ

Depth m		Recovery			Lithology	RQD (>4")		Rock	Weathering	Joint Cond.	
From	To	Length	Length	Rec. %		Length	%	Hardness	Core	# Joints	Condition
0.00	4.88	4.88			Casing			R2	SW		
4.88	5.49	0.61	0.70	114.75		0.23	32.86	R2	SW	16	6
5.49	7.32	1.83	1.70	92.90		0.80	47.06	R2	SW	25	6
7.32	7.92	0.60	0.60	100.00		0.15	25.00	R2	SW	11	12
7.92	10.97	3.05	2.92	95.74		1.97	67.47	R2	SW	27	12
10.97	13.11	3.04	2.33	76.64		1.22	52.36	R2	SW	28	12
13.11	14.33	1.22	1.20	98.36		0.71	59.17	R2	SW	9	12
14.33	17.37	3.04	3.00	98.68		1.64	54.67	R2	SW	24	12
17.37	20.42	3.05	3.05	100.00		1.70	55.74	R2	SW	39	12
20.42	22.86	2.44	2.44	100.00		0.85	34.84	R2	SW	35	12
22.86	23.77	1.17	0.95	81.20		0.24	25.26	R2	SW	20	12
23.77	25.30	1.53	1.50	98.04		0.48	32.00	R2	SW	22	12
25.30	26.52	1.22	1.22	100.00		0.73	59.84	R2	SW	13	12
26.52	29.57	3.05	3.05	100.00		2.24	73.44	R2	SW	24	12
29.57	32.00	2.43	2.35	96.71		1.86	79.15	R2	SW	16	12
32.00	35.05	3.05	2.94	96.39		2.44	82.99	R2	SW	20	12
35.05	36.58	1.53	1.64	107.19		1.05	64.02	R2	SW	16	12

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 7/03

**HOLE #** L-03-09 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:** 65.53 m

**CORE SIZE:** NQ

From	Depth		Recovery		Lithology	RQD (>4")		Rock Hardness	Weathering Core	Joint Cond.	
	To	Length	Length	Rec. %		Length	%			# Joints	Condition
36.58	38.10	1.52	1.52	100.00		0.95	62.50	R2	SW	14	12
38.10	39.32	1.22	1.20	98.36		0.78	65.00	R2	SW	15	12
39.32	41.76	2.44	2.40	98.36		1.48	61.67	R2	SW	26	12
41.76	44.81	3.05	3.05	100.00		2.59	84.92	R2	SW	17	12
44.81	47.85	3.04	2.98	98.03		1.95	65.44	R2	SW	22	12
*47.85	50.60	2.75	2.98	108.36		1.48	49.66	R2	SW	34	12
50.60	53.64	3.04	2.85	93.75	Well Fractured zones	1.43	50.18	R2	SW	>35	12
*53.64	56.39	2.75	2.50	90.91		2.18	87.20	R2	SW	15	12
56.39	59.44	3.05	3.05	100.00		2.50	81.97	R2	SW	19	12
59.44	60.05	0.61	0.61	100.00	Fractured zone	0.00	0.00	R2	SW	20	12
60.05	63.09	3.04	2.95	97.04		1.18	40.00	R2	SW	10	12
63.09	65.53	2.44	2.44	100.00		1.82	74.59	R2	SW	15	12

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 8/03

**HOLE # L-03-10 NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:** 66.14 m

**CORE SIZE:** NQ

Depth m		Recovery		Lithology	RQD (>4")		Rock Hardness	Weathering Core	Joint Cond.		
From	To	Length	Length		Rec. %	Length			%	# Joints	Condition
0.00	4.15			Casing						12	
4.15	6.10	1.95	1.95	100.00	Top of hole broken core	0.47	24.10	R2	SW	-	12
6.10	7.32	1.22	1.00	81.97	Strongly Fractured	0.00	0.00	R2	SW	-	6
7.32	7.62	0.30	0.44	146.67		0.00	0.00	R1-2	SW	-	6
7.62	9.75	2.13	2.13	100.00		0.67	31.46	R2	SW	38	6
9.75	11.28	1.53	1.30	84.97	Strongly Fractured	0.00	0.00	R1-2	SW	-	6
11.28	12.80	1.52	0.85	55.92	Strongly Fractured	0.00	0.00	R1-2	SW	-	6
12.80	14.33	1.53	0.87	56.86	Strongly Fractured	0.25	16.34	R1-2	SW	-	6
14.33	15.24	0.91	0.65	71.43	Strongly Fractured	0.10	10.99	R1-2	SW	-	6
15.24	16.46	1.22	1.22	100.00		0.19	15.57	R1	MW	-	6
16.46	18.59	2.13	1.85	86.85	Mod well Fr	0.43	20.19	R2	SW	-	6
18.59	20.42	1.83	0.53	28.96		0.00	0.00	R1	MW	-	6
20.42	23.47	3.05	2.95	96.72		2.17	71.15	R2	SW	17	12
23.47	24.38	0.91	0.76	83.52		0.45	49.45	R2	SW	11	12
24.38	25.91	1.53	1.00	65.36	Broken ground	0.00	0.00	R1-2	MW	-	6
25.91	26.52	0.60	0.40	66.67	Broken ground	0.00	0.00	R1-2	MW	-	6
26.52	27.74	1.22	0.60	49.18	Broken ground	0.00	0.00	R1-2	MW	-	6

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 8/03

**HOLE # L-03-10 NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:**

**CORE SIZE:** NQ

Depth		Recovery		Lithology	RQD (>4")		Rock Hardness	Weathering Core	Joint Cond.		
From	To	Length	Length		Rec. %	Length			%	# Joints	Condition
27.74	29.57	1.83	1.54	84.15	1.02	55.74	R2	SW	19	12	
29.57	30.48	0.91	0.60	65.93	Shattered Core	0.00	0.00	R2	SW	-	12
30.48	30.78	0.30	0.14	46.67	Shattered Core	0.00	0.00	R2	SW	-	12
30.78	32.00	1.22	0.90	73.77		0.50	40.98	R2	SW	12	12
32.00	32.61	0.61	0.61	100.00	Shattered	0.17	27.87	R2	SW	>25	12
32.61	34.75	2.14	1.70	79.44	Shattered	0.29	13.55	R2	SW	-	12
34.75	35.66	0.91	0.91	100.00	Shattered	0.00	0.00	R2	SW	-	12
35.66	38.71	3.05	3.05	100.00	Shattered Sub 11 ca	1.15	37.70	R2	SW	-	12
38.71	40.54	1.83	1.63	89.07	Strongly Fractured	0.39	21.31	R2	SW	30	12
40.54	41.76	1.22	1.02	83.61	Broken Section	0.43	35.25	R2	MW	20	12
41.76	44.87	3.11	3.11	100.00	Broken Section	0.80	25.72	R1-2	SW-MW	59	12/6
44.87	47.55	2.68	2.30	85.82		1.12	41.79	R2	SW-MW	37	12/6
47.55	49.38	1.83	1.83	100.00	Shattered Section	0.72	39.34	R2	SW	34	12/6
49.38	50.29	0.91	0.75	82.42	Shattered	0.21	23.08	R2	SW	>25	12
50.29	50.90	0.61	0.47	77.05		0.45	73.77	R2	MW	4	12
50.90	53.95	3.05	2.99	98.03		2.22	72.79	R2	MW	17	12
53.95	54.86	0.91	0.91	100.00	Shattered	0.31	34.07	R2	MW	25	12



**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone      **LOGGER:** N. von Fersen      **DATE:** Dec 9/03

**HOLE #** L-03-11    **NORTHING:**      **EASTING:**      **ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**      **LENGTH:** 66.14 m      **CORE SIZE:** NQ

Depth m		Recovery			Lithology	RQD (>4")		Rock Hardness	Weathering Joint Cond.	
From	To	Length	Length	Rec. %		Length	%		Core	# Joints
0.00	3.05	3.05	0.00		Casing					
3.05	5.18	2.13	1.35	63.38	Well Fractured	0.22	10.33	R2-1	SW-MW	>30    6
5.18	5.79	0.61	0.50	81.97		0.14	22.95	R2	SW	15    12
5.79	7.01	1.22	0.92	75.41	Well Fractured	0.12	9.84	R1	MW	>30    6
7.01	10.06	3.05	3.05	100.00		1.25	40.98	R2	SW	37    12
10.06	11.28	1.22	1.22	100.00		0.40	32.79	R2	SW	21    12
11.28	13.41	2.13	1.95	91.55		0.00	0.00	R2-1	SW>MW	36    12/6
13.41	16.46	3.05	2.80	91.80	Well Fractured	0.52	17.05	R2	SW	54    12
16.46	18.59	2.13	2.13	100.00		0.86	40.38	R2	SW	30    12
18.59	20.42	1.83	1.83	100.00		1.33	72.68	R2	SW	13    12
20.42	22.86	2.44	2.40	98.36		1.42	58.20	R2	SW	22    12
22.86	25.91	3.05	3.05	100.00		2.19	71.80	R2	SW	22    12
25.91	27.13	1.22	1.22	100.00		0.59	48.36	R2	SW	17    12
27.13	28.96	1.83	1.76	96.17		1.30	71.04	R2	SW	13    12
28.96	32.00	3.04	3.04	100.00		2.50	82.24	R2	SW	15    12
32.00	32.92	0.92	0.92	100.00		0.63	68.48	R2	SW	7    12
32.92	35.66	2.74	2.67	97.45		2.04	74.45	R2	SW	13    12
35.66	38.71	3.05	3.05	100.00		2.67	87.54	R2	SW	18    12





**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone      **LOGGER:** N. von Fersen      **DATE:** Dec 9/03

**HOLE #** L-03-12    **NORTHING:**      **EASTING:**      **ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**      **LENGTH:** 65.23 m      **CORE SIZE:** NQ

Depth m		Recovery			Lithology	RQD (>4")		Rock	Weathering	Joint Cond.	
From	To	Length	Length	Rec. %		Length	%	Hardness	Core	# Joints	Condition
0.00	3.35	3.35			Casing						
3.35	4.27	0.92	0.75	81.52	Top of hole-rubble	0.00	0.00	R2-1	SW-MW	-	6
4.27	5.18	0.91	0.32	35.16	Top of hole-rubble	0.00	0.00	R2-1	SW-MW	-	6
5.18	6.40	1.22	0.65	53.28	Shattered	0.00	0.00	R1-2	MW-SW	-	6
6.40	6.71	0.31	0.31	100.00		0.23	74.19	R1-2	SW	19	6
6.71	8.23	1.52	1.40	92.11		0.47	30.92	R2	SW	24	12
8.23	9.14	0.91	0.65	71.43	Shattered	0.00	0.00	R2-1	SW-MW	20	6
9.14	10.67	1.53	0.80	52.29	Shattered	0.00	0.00	R1-2	SW-MW	>25	6
10.67	11.58	0.91	0.91	100.00		0.26	28.57	R2	SW	24	12
11.58	14.33	2.75	2.75	100.00		1.23	44.73	R2	SW	35	12
14.33	14.94	0.61	0.55	90.16	Some Fr sub 11/ca	0.00	0.00	R2	SW-MW	15	6
14.94	16.46	1.52	1.52	100.00	Some Fr sub 11/ca	0.66	43.42	R2	SW	20	12/6
16.46	18.29	1.83	1.73	94.54		1.10	60.11	R2	SW	15	12
18.29	20.42	2.13	1.73	81.22		1.18	55.40	R2-1	SW	15	12/6
20.42	22.25	1.83	1.80	98.36		0.68	37.16	R2	SW	28	12
22.25	23.47	1.22	1.04	85.25		0.28	22.95	R2	SW	17	12
23.47	24.69	1.22	1.05	86.07		0.35	28.69	R2	SW	14	12
24.69	25.30	0.61	0.61	100.00		0.00	0.00	R2	SW	16	12

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 9/03

**HOLE #** L-03-12 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:**

**CORE SIZE:** NQ

Depth		Recovery			Lithology	RQD (>4")		Rock Hardness	Weathering Joint Cond.		
From	To	Length	Length	Rec. %		Length	%		Core	# Joints	Condition
25.30	26.52	1.22	0.80	65.57		0.00	0.00	R2	SW	28	12
26.52	27.13	0.61	0.55	90.16		0.16	26.23	R2	SW	11	12
27.13	28.96	1.83	1.73	94.54		1.12	61.20	R2	SW	20	12
28.96	29.57	0.61	0.75	122.95		0.40	65.57	R2	SW	25	12
29.57	32.61	3.05	2.78	91.15		2.22	72.79	R2	SW	18	12
32.61	35.66	3.05	2.05	67.21		2.89	94.75	R2	SW	13	12
35.66	36.88	1.22	0.95	77.87		0.50	40.98	R2	SW	19	12
36.88	38.40	1.52	1.52	100.00		0.87	57.24	R2	SW	25	12
38.40	40.84	2.44	2.05	84.02	Fr zone Sub ll/ca	1.01	41.39	R2-1	SW-MW	25	12\6
40.84	43.59	2.75	2.45	89.09		1.70	61.82	R2	SW	13	12
43.59	46.33	2.74	2.70	98.54		1.90	69.34	R2	SW	23	12
46.33	47.85	1.52	1.45	95.39		0.75	49.34	R2	SW	17	12
47.85	49.07	1.22	1.14	93.44		0.63	51.64	R2	SW	11	12
49.07	51.82	2.75	2.45	89.09		1.40	50.91	R2	SW	26	12
51.82	52.43	0.61	0.60	98.36		0.10	16.39	R2	SW	17	12
52.43	53.95	1.52	1.45	95.39		0.25	16.45	R2	SW	33	12
53.95	55.17	1.22	1.00	81.97		0.17	13.93	R2	SW	23	12
55.17	58.22	3.05	2.05	67.21		1.51	49.51	R2	SW	35	12



**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 11/03

**HOLE #** L-03-13 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:** 65.84 m

**CORE SIZE:** NQ

Depth m		Recovery		Lithology	RQD (>4")		Rock	Weathering	Joint Cond.		
From	To	Length	Length		Rec. %	Length			%	Hardness	Core
0.00	3.55	3.55									
3.55	4.88	1.33	1.25	93.98	Casing	0.30	22.56	R1-2	S-MW	35	6
4.88	6.71	1.83	1.83	100.00	Dominant Fr 45-70 ca, occ fract 15-20 deg/ca	0.42	22.95	R2-1	SW	30	6
6.71	8.23	1.52	1.52	100.00	"	0.70	46.05	R2	SW	16	12
8.23	11.28	3.05	3.05	100.00	"	2.50	81.97	R2	SW	18	12
11.28	14.33	3.05	3.05	100.00	"	1.95	63.93	R2	SW	21	12
14.33	17.37	3.04	3.00	98.68	incr in fract sub ll/ca	1.03	33.88	R2	SW	34	6
17.37	20.12	2.75	2.75	100.00	sub ll/ca 15-25	1.34	48.73	R2	SW	18	12
20.12	21.64	1.52	1.52	100.00	sub ll/ca 15-25	1.03	67.76	R2	SW	11	12
21.64	23.47	1.83	1.55	84.70	Dominant Fr 40-60 ca, occ. sub ll/ca	0.90	49.18	R2	SW	11	12
23.47	26.52	3.05	3.04	99.67	as above	1.87	61.31	R2	SW	23	12
26.52	29.57	3.05	3.05	100.00	as above	1.33	43.61	R2	SW	40	12
29.57	32.61	3.04	3.00	98.68	fr sub ll/ca + 20 to 45/ca	0.90	29.61	R2	SW	30	12
32.61	35.05	2.44	2.44	100.00	as above	1.45	59.43	R2	SW	19	12
35.05	37.49	2.44	2.44	100.00	dom. Fract 30-60/ca	1.15	47.13	R2	SW	20	12
37.49	37.80	0.31	0.30	96.77	str fract	0.00	0.00	R2	SW	15	12
37.80	39.62	1.82	1.80	98.90	well fr, sub ll/ca	0.39	21.43	R2	SW	36	12
39.62	41.76	2.14	2.14	100.00	sub ll/ca + 20-45	1.08	50.47	R2		31	12

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 11/03

**HOLE #** L-03-13 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:**

**CORE SIZE:** NQ

Depth		Recovery			Lithology	RQD (>4")		Rock	Weathering	Joint Cond.	
From	To	Length	Length	Rec. %		Length	%	Hardness	Core	# Joints	Condition
41.76	43.59	1.83	1.80	98.36	Dom Fr ~ 20/ca	1.03	56.28	R2	SW	15	12
43.59	44.81	1.22	1.52	124.59	Fr 20-45 ca	0.85	69.67	R2	SW	16	12
44.81	47.85	3.04	2.50	82.24	Fr 20-45 ca	1.08	35.53	R2	SW	31	12
47.85	49.07	1.22	1.22	100.00	Fr 20-45 ca	0.37	30.33	R2	SW	21	12
49.07	50.90	1.83	1.49	81.42	Fr 20-45 ca	0.40	21.86	R2	SW	21	12
50.90	53.04	2.14	1.75	81.78	Dom Fr 30-70	0.56	26.17	R2	SW	23	12
53.04	54.25	1.21	1.21	100.00	Dom Fr 25-90	0.80	66.12	R2	SW	16	12
54.25	55.78	1.53	1.45	94.77	Dom Fr 25-90	0.58	37.91	R2	SW	19	12
55.78	57.00	1.22	0.98	80.33	Dom Fr 25-90	0.55	45.08	R2	SW	16	12
57.00	57.61	0.61	0.92	150.82	Dom Fr 25-90	0.59	96.72	R2	SW	9	12
57.61	60.05	2.44	1.94	79.51	Dom Fr 25-90	0.77	31.56	R2	SW	26	12
60.05	60.96	0.91	0.80	87.91	Dom Fr 25-90	0.11	12.09	R2	SW	19	12
60.96	63.09	2.13	1.84	86.38	Dom Fr 70-Sub II/ca	0.55	25.82	R2	SW	34	12
63.09	64.01	0.92	0.57	61.96	Dom Fr 45-65	0.27	29.35	R2	SW	12	12
64.01	65.84	1.83	2.10	114.75	Dom 45- Sub II/ca	1.20	65.57	R2	SW	26	12

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone      **LOGGER:** N. von Fersen      **DATE:** Dec 12/03

**HOLE #** L-03-14    **NORTHING:**      **EASTING:**      **ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**      **LENGTH:** 150.57 m      **CORE SIZE:** NQ

From	Depth m		Recovery		Lithology	RQD (>4")		Rock Hardness	Weathering Core	Joint Cond.	
	To	Length	Length	Rec. %		Length	%			# Joints	Condition
0.00	3.48	3.48			Casing			R2	SW		
3.48	3.96	0.58	0.58	100.00	Fr 15-60	0.00	0.00	R2	SW	23	12
3.96	5.18	1.22	1.00	81.97	Fr sub II-80	0.00	0.00	R2	SW	31	12
5.18	5.79	0.61	0.51	83.61	Fr 45-65	0.12	19.67	R2	SW	22	12
5.79	7.62	1.83	1.58	86.34	Fr sub II to 45-65	0.88	48.09	R2	SW	25	12
7.62	9.45	1.83	1.22	66.67	Fr 45-65	0.57	31.15	R2	SW	15	12
9.45	11.28	1.83	1.83	100.00	Fr sub II-75	0.33	18.03	R2	SW	35	12
11.28	14.33	3.05	3.05	100.00	Fr sub II-60	1.70	55.74	R2	SW	30	12
14.33	17.37	3.04	3.05	100.33	Fr sub II-75	1.24	40.79	R2-1	SW-MW	41	12/6
17.37	20.42	3.05	3.05	100.00	Fr 15-60	2.45	80.33	R2	SW	23	12
20.42	23.47	3.05	2.98	97.70	Fr 30-75	2.05	67.21	R2	SW	22	12
23.47	26.52	3.05	2.95	96.72	Fr 30-75	2.06	67.54	R2	SW	22	12
26.52	29.57	3.05	3.05	100.00	Fr 20-65	1.05	34.43	R2-1	SW-MW	54	12/6
29.57	31.70	2.13	1.90	89.20	Fr 20-65	1.12	52.58	R2	SW	16	12
31.70	34.75	3.05	3.05	100.00	Fr 15-70	2.26	74.10	R2	SW	22	12
34.75	37.80	3.05	2.90	95.08	Fr 45-80	2.36	77.38	R2	SW	18	12
37.80	40.54	2.74	2.68	97.81	Fr 25-80	2.08	75.91	R2	SW	19	12
40.54	41.76	1.22	1.22	100.00	Fr 25-80	0.87	71.31	R2	SW	10	12

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 12/03

**HOLE #** L-03-14 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

**LENGTH:** 150

**CORE SIZE:**

Depth		Recovery			Lithology	RQD (>4")		Rock	Weathering	Joint Cond.	
From	To	Length	Length	Rec. %		Length	%	Hardness	Core	# Joints	Condition
41.76	44.81	3.05	3.05	100.00	Fr Sub II-60	0.79	25.90	R2-1	SW-MW	47	12\6
44.81	47.85	3.04	2.40	78.95	Str Fr 10-45	0.90	29.61	R2	SW	~64	12
47.85	49.07	1.22	1.20	98.36	Fr 20-60	0.84	68.85	R2	SW	16	12
49.07	50.90	1.83	1.73	94.54	Fr 20-60	1.18	64.48	R2	SW	14	12
50.90	53.34	2.44	2.44	100.00	Fr 20-60	1.95	79.92	R2	SW	20	12
53.34	56.39	3.05	3.05	100.00	Fr 20-60	1.06	34.75	R2	SW	27	12
56.39	58.83	2.44	2.20	90.16	Fr sub II-60	1.09	44.67	R2	SW	21	12
58.83	60.05	1.22	1.15	94.26	Fr sub II-60	0.50	40.98	R2	SW	14	12
60.05	60.96	0.91	0.81	89.01	Fr sub II-60	0.11	12.09	R2	SW	14	12
60.96	63.09	2.13	1.76	82.63	Fr 20-80	0.71	33.33	R2	SW	26	12
63.09	64.31	1.22	0.95	77.87	Fr 15-60	0.53	43.44	R2	SW	13	12
64.31	65.23	0.92	1.05	114.13	Fr 15-45	0.30	32.61	R2	SW	22	12
65.23	66.75	1.52	1.25	82.24	Fr 25-55	0.58	38.16	R2	SW	20	12
66.75	67.67	0.92	0.70	76.09	Fr 25-55	0.10	10.87	R2	SW	20	12
67.67	68.88	1.21	1.21	100.00	Fr 35-65	0.39	32.23	R2	SW	22	12
68.88	69.49	0.61	0.61	100.00	Fr 15-65	0.00	0.00	R2	SW	16	12
69.49	70.71	1.22	0.70	57.38	Fr 15-65	0.13	10.66	R1	MW	18	12
70.71	73.15	2.44	2.14	87.70	Fr 25-65	1.36	55.74	R1-2	SW	23	12



**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone      **LOGGER:** N. von Fersen      **DATE:** Dec 12/03

**HOLE #** L-03-14    **NORTHING:**      **EASTING:**      **ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**      **LENGTH:** 150      **CORE SIZE:**

From	Depth		Recovery		Lithology	RQD (>4")		Rock Hardness	Weathering Core	Joint Cond.	
	To	Length	Length	Rec. %		Length	%			# Joints	Condition
73.15	73.76	0.61	0.60	98.36	Fr 25-85	0.13	21.31	R2	SW	10	12
73.76	75.90	2.14	2.10	98.13	Fr 25-65	1.60	74.77	R2	SW	20	12
75.90	77.72	1.82	1.72	94.51	Fr 15-65	0.88	48.35	R2	SW	16	12
77.72	80.16	2.44	2.28	93.44	Fr 25-60	1.49	61.07	R2	SW	21	12
80.16	81.08	0.92	0.82	89.13	Well Fract 30-60	0.22	23.91	R2-1	SW	~30	12
81.08	83.82	2.74	2.68	97.81	Fr sub II-60	1.61	58.76	R2	SW	21	12
83.82	85.34	1.52	1.46	96.05	Fr sub II-60	0.30	19.74	R2	SW	28	12
85.34	87.48	2.14	2.05	95.79	Fr sub II-60	1.22	57.01	R2	SW	19	12
87.48	89.31	1.83	1.69	92.35	Fr 50-90	0.98	53.55	R2	SW	18	12
89.31	91.14	1.83	0.89	48.63	Fr 50-90 poss F.Z.	0.10	5.46	R1	S-MW	26	6
91.14	92.05	0.91	0.91	100.00	Fr 15-65	0.54	59.34	R2	SW	17	12
92.05	94.79	2.74	2.70	98.54	Fr 30-80	2.37	86.50	R2	SW	15	12
94.79	97.23	2.44	2.70	110.66	Fr 30-80	1.37	56.15	R2	SW	27	12
97.23	99.67	2.44	2.09	85.66	Fr 30-80	1.48	60.66	R2	SW	18	12
99.67	102.41	2.74	2.74	100.00	Fr 20-85	1.21	44.16	R2	SW	28	12
102.41	103.94	1.53	1.60	104.58	Fr 20-65	0.85	55.56	R2	SW	18	12
103.94	106.98	3.04	2.77	91.12	Fr 30-70	1.59	52.30	R2-1	S-MW	21	12
106.98	108.81	1.83	1.50	81.97	Fr sub II-65	0.69	37.70	R1	MW	22	12/6
108.81	110.34	1.53	1.53	100.00	Fr 20-60	1.07	69.93	R2-1	SW	10	12

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone      **LOGGER:** N. von Fersen      **DATE:** Dec 12/03

**HOLE #** L-03-14    **NORTHING:**      **EASTING:**      **ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**      **LENGTH:** 150.57 m      **CORE SIZE:**

Depth m		Recovery			Lithology	RQD (>4")		Rock	Weathering	Joint Cond.	
From	To	Length	Length	Rec. %		Length	%	Hardness	Core	# Joints	Condition
110.34	112.17	1.83	1.83	100.00	Fr sub II-65	0.72	39.34	R2	SW	20	12
112.17	114.91	2.74	2.40	87.59	Fr 20-80	1.97	71.90	R2	SW	15	12
114.91	117.96	3.05	3.05	100.00	Fr 20-80	1.65	54.10	R2	SW	30	12
117.96	121.01	3.05	3.05	100.00	Fr 20-80	2.59	84.92	R2	SW	18	12
121.01	124.05	3.04	3.05	100.33	Fr 30-80	2.30	75.66	R2	SW	21	12
124.05	127.10	3.05	3.00	98.36	Fr 20-80	1.97	64.59	R2	SW	28	12
127.10	130.15	3.05	3.05	100.00	Fr 50-80	2.50	81.97	R2	SW	23	12
130.15	133.20	3.05	3.05	100.00	Fr 10-80	1.87	61.31	R2	SW	28	12
133.20	136.25	3.05	3.05	100.00	Fr 20-80	2.62	85.90	R2	SW	18	12
136.25	139.29	3.04	3.04	100.00	Fr 30-85	2.17	71.38	R2	SW	25	12
139.29	142.34	3.05	3.05	100.00	Fr 30-85, Dike1	2.56	83.93	R2	SW	17	12
142.34	144.78	2.44	2.40	98.36	Fr 45-90, 60cm Dike	2.37	97.13	R2	SW	7	12
144.78	147.83	3.05	3.00	98.36	Fr 25-80	2.36	77.38	R2	SW	22	12
147.83	150.57	2.74	2.92	106.57	Fr 35-85	2.68	97.81	R2	SW	14	12

**GEOTECHNICAL LOGGING FORM**

PROJECT: Lodestone

LOGGER: N. von Fersen

DATE: Dec 13/03

HOLE # L-03-15 NORTHING:

EASTING:

ELEVATION:

AZIMUTH/DIP & DIRECTION:

LENGTH: 65.23 m

CORE SIZE: NQ

From	Depth m		Recovery		Lithology	RQD (>4")		Rock Hardness	Weathering Core	Joint Cond.	
	To	Length	Length	Rec. %		Length	%			# Joints	Condition
0.00	3.05	3.05			Casing						
3.05	4.88	1.83	0.45	24.59	Rubble	0.00	0.00	R1	MW		6
4.88	6.10	1.22	1.10	90.16	Fr 25-75	0.34	27.87	R2	SW	17	12
6.10	7.92	1.82	2.00	109.89	Fr 30-85	1.25	68.68	R2	SW	18	12
7.92	9.14	1.22	1.18	96.72	Fr 30-85	0.34	27.87	R2	SW	22	12
9.14	9.75	0.61	0.54	88.52	Fr II/ca - 55	0.15	24.59	R2	SW	14	12
9.75	11.28	1.53	1.23	80.39	Fr II/ca - 55	0.55	35.95	R2	SW	28	12
11.28	13.11	1.83	1.83	100.00	Fr II/ca - 55	0.86	46.99	R2	SW	35	12
13.11	14.63	1.52	1.30	85.53	Fr II/ca - 55	0.33	21.71	R2	SW	21	12
14.63	16.76	2.13	2.13	100.00	Fr sub II-75	1.06	49.77	R2	SW	27	12
16.76	18.90	2.14	2.10	98.13	Fr sub II-85	0.80	37.38	R2	SW	32	12
18.90	19.81	0.91	0.91	100.00	Fr 20-70	0.15	16.48	R2	SW	24	12
19.81	21.64	1.83	1.37	74.86	Fr 30-65	0.67	36.61	R2	SW	17	12
21.64	24.38	2.74	2.55	93.07	Fr sub II-65	1.20	43.80	R2	SW	23	12
24.38	24.99	0.61	0.61	100.00	Fr sub II-65	0.00	0.00	R2	SW	14	12
24.99	26.52	1.53	1.37	89.54	Fr sub II-65	0.59	38.56	R2	SW	27	12
26.52	27.14	0.61	0.59	96.72	Fr sub II-65 shattered	0.00	0.00	R2	SW	>30	12
27.14	28.04	0.91	0.74	81.32	Fr sub II-85	0.10	10.99	R2	SW	21	12

**GEOTECHNICAL LOGGING FORM**

**PROJECT:** Lodestone

**LOGGER:** N. von Fersen

**DATE:** Dec 13/03

**HOLE #** L-03-15 **NORTHING:**

**EASTING:**

**ELEVATION:**

**AZIMUTH/DIP & DIRECTION:**

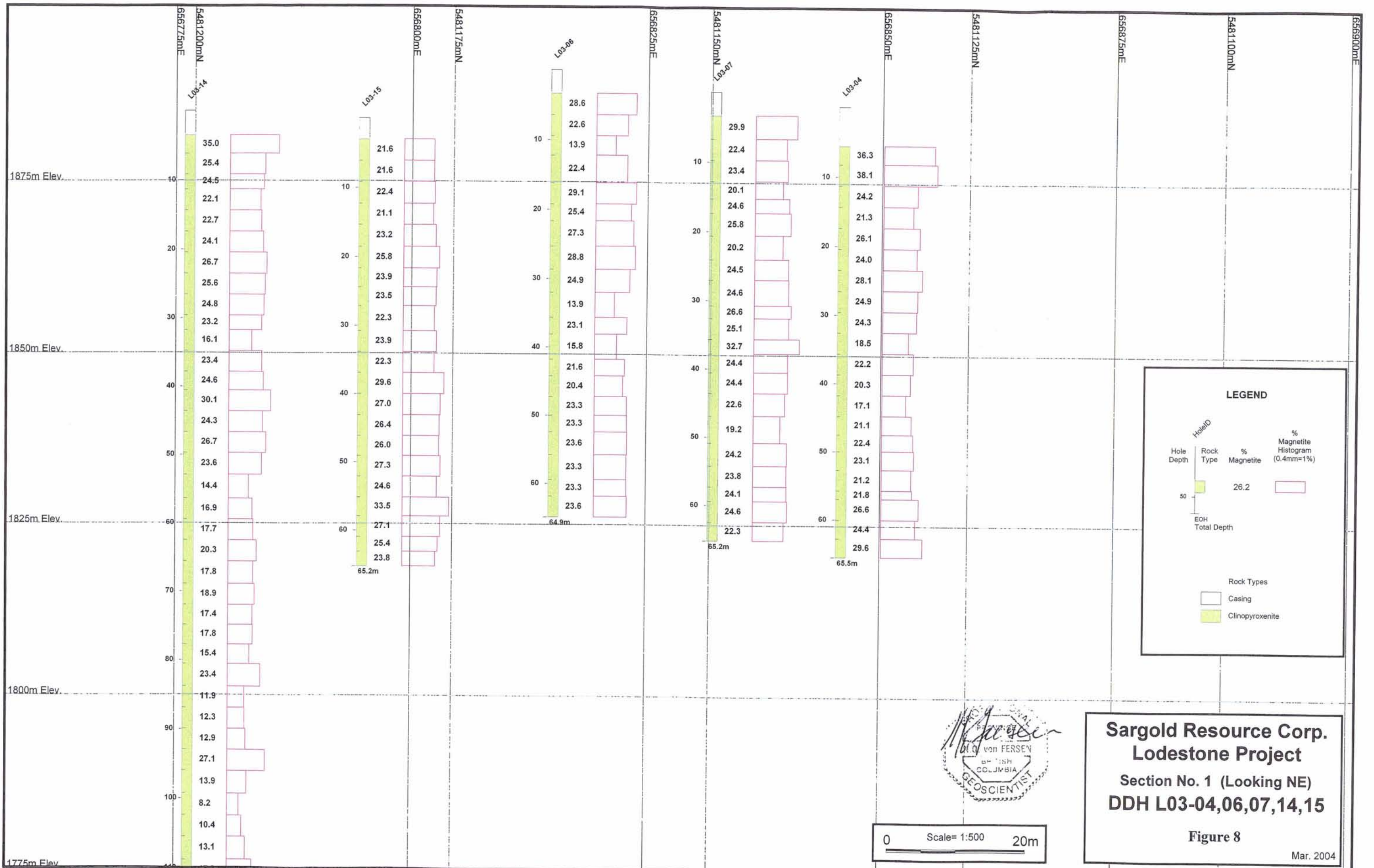
**LENGTH:** 65.23 m

**CORE SIZE:** NQ

Depth m		Recovery			Lithology	RQD (>4")		Rock	Weathering	Joint Cond.	
From	To	Length	Length	Rec. %		Length	%	Hardness	Core	# Joints	Condition
28.04	29.57	1.53	1.33	86.93	Fr 30-70	0.39	25.49	R2	SW	26	12
29.57	29.87	0.30	0.26	86.67	Fr sub II-65	0.00	0.00	R2	SW	12	12
29.87	30.78	0.91	0.69	75.82	Fr sub II-65	0.32	35.16	R2	SW	11	12
30.78	33.22	2.44	2.28	93.44	Fr s II-65 F.Z 33.22	1.22	50.00	R2-1	SW-MW	21	12/6
33.22	33.83	0.61	0.61	100.00	Fr sub II-60	0.20	32.79	R2	SW	11	12
33.83	35.97	2.14	2.10	98.13	Fr sub II-65	0.96	44.86	R2	SW	32	12
35.97	37.80	1.83	1.63	89.07	Fr 30-85	1.02	55.74	R2	SW	19	12
37.80	40.84	3.04	2.80	92.11	Fr 30-85	1.79	58.88	R2	SW	28	12
40.84	42.67	1.83	1.83	100.00	Fr sub II-60	0.69	37.70	R2	SW	33	12
42.67	44.81	2.14	2.24	104.67	Fr 20-65	1.50	70.09	R2	SW	18	12
44.81	46.33	1.52	1.52	100.00	Fr 20-65	1.01	66.45	R2	SW	22	12
46.33	49.07	2.74	2.72	99.27	Fr sub II-60	1.88	68.61	R2	SW	19	12
49.07	50.90	1.83	1.80	98.36	Fr sub II-70	1.46	79.78	R2	SW	11	12
50.90	53.34	2.44	2.55	104.51	Fr sub II-70	1.60	65.57	R2	SW	31	12
53.34	55.78	2.44	2.40	98.36	Fr sub II-70	1.38	56.56	R2	SW	25	12
55.78	57.91	2.13	2.03	95.31	Fr 20-70	1.34	62.91	R2	SW	25	12
57.91	60.05	2.14	2.14	100.00	Fr 10-60	1.42	66.36	R2	SW	18	12
60.05	63.09	3.04	3.04	100.00	Fr 10-60	1.58	51.97	R2	SW	27	12
63.09	65.23	2.14	2.14	100.00	Fr 10-60	1.27	59.35		SW	23	12/6

**APPENDIX D**

**DRILL HOLE SECTIONS**





**LEGEND**

Hole ID

Hole Depth

Rock Type

% Magnetite

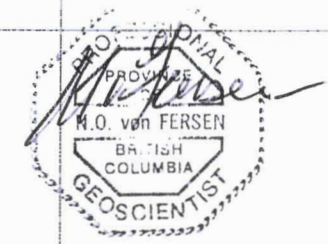
% Magnetite Histogram (0.4mm=1%)

ECH Total Depth

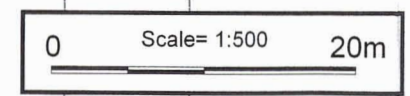
Rock Types

Casing

Clinopyroxenite



**Sargold Resource Corp.**  
**Lodestone Project**  
 Section No. 2 (Looking NE)  
 DDH L03-01,05,08,09,13  
 Figure 9  
 Mar. 2004



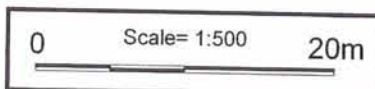
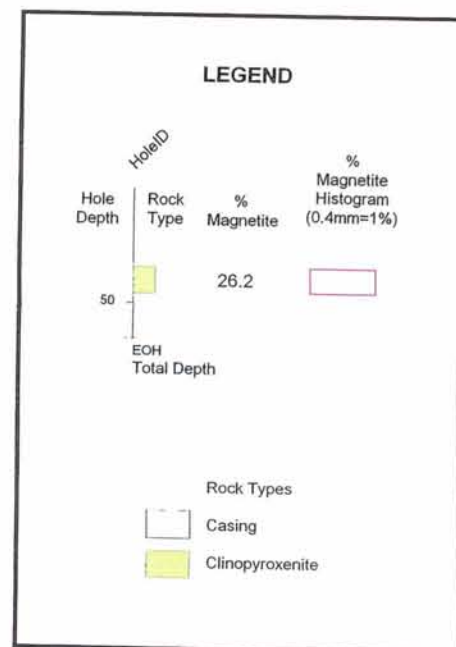
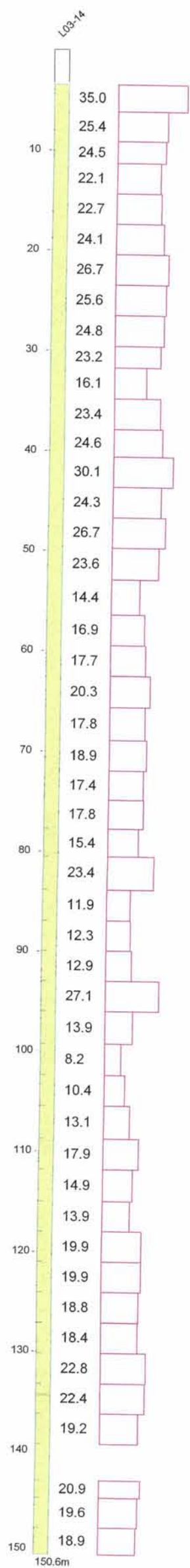
1775m Elev.



0 Scale= 1:500 20m

**Sargold Resource Corp.**  
**Lodestone Project**  
 Section No. 3 (Looking NE)  
 DDH L03-02,03,10,11,12  
 Figure 10  
 Mar. 2004





**Sargold Resource Corp.**  
**Lodestone Project**  
**DDH L03-14**  
**Figure 11**  
 Mar. 2004

**APPENDIX E**

**SUMMARY OF EXPENDITURES**

**Sargold Resource Corporation  
Lodestone Property  
Diamond Drilling Program**

<b>Item Description</b>	<b>Cost</b>
Diamond drilling	\$ 78,538.97
Core boxes / lids	1,964.60
Cat time for set-ups / snow removal	25,813.76
Sample analysis @ \$50/s	15,029.19
Project geologist @ \$450/d	17,200.00
Geologist	2,650.00
Assistant @ \$150/d	5,300.00
Room & board	1,589.74
Truck rental	5,067.33
Fuel	647.03
Field supplies (core saw, bags, tags, etc.)	3,732.30
Drafting	437.50
Final report	4,500.00
Miscellaneous	1,242.43
<b>Total expenditures</b>	<b><u><u>\$ 163,712.85</u></u></b>