ASSESSMENT REPORT

on

GEOLOGY, GEOCHEMISTRY & TRENCHING

EDDY PROPERTY

Weaver Creek area, SE B.C.

UTM 569000E 5473000N

TRIM 82F.040 & 82F.050

For

RUBY RED RESOURCES LTD.
Suite 207, 239 12th Ave. SW
Calgary, Alberta
T2R 1H6

By
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March, 2004

TABLE OF CONTENTS

LIST OF ILLUSTRATIONS

1.00 INTRODUCTION

1.10 Location and Access

The Eddy property is located in southeastern British Columbia, approximately 25 kilometers southwest of Cranbrook, centered at UTM coords. 569000E, 5473000N on Weaver Creek, a major east-flowing tributary of the Moyie River (Figs. 1 & 2).

The eastern portion of the claims is accessed by road south of Cranbrook, using the Lumberton and Moyie Forest Service Roads and tributary roads in Noke, Weaver, North Moyie and Ryder Creeks. The Western portion of the claims is in Galway Creek and is accessed by the Perry Creek forest road system.

1.20 Property

The Eddy property includes 149 claim units in one 20 unit 4-post claim and 126 2-post claims (Fig. 2). Many of the claims have duplicate names:

Claim name and No.	Tenure numbers
Eddy	387078
Eddy1-6 inclusive	387079-84 inclusive
Eddy 7, 8	387776, 77
Eddy 9-12 "	387833-36 "
Eddy 13, 14	387778, 79
Eddy 15	393225 20 units
Eddy 15-18 "	395123-26 inclusive
Eddy 20-26 "	395271-77 "
Eddy 16-43 "	395294-321 "
Eddy 27-31 "	395322-26 "
Eddy 44	395344
Eddy 32-41 "	395754-63 "
Eddy 42-63 "	396088-109 "
Nelly 1-4 "	387670-73 "
L3772A	210255
L3773	210256
L3774	210257
ED 1S to ED 14S	403032-045 "
EDDY NE-1 to EDDY NE-7	403056-062 "
ED NE-8 to ED-NE16	403504-512 "

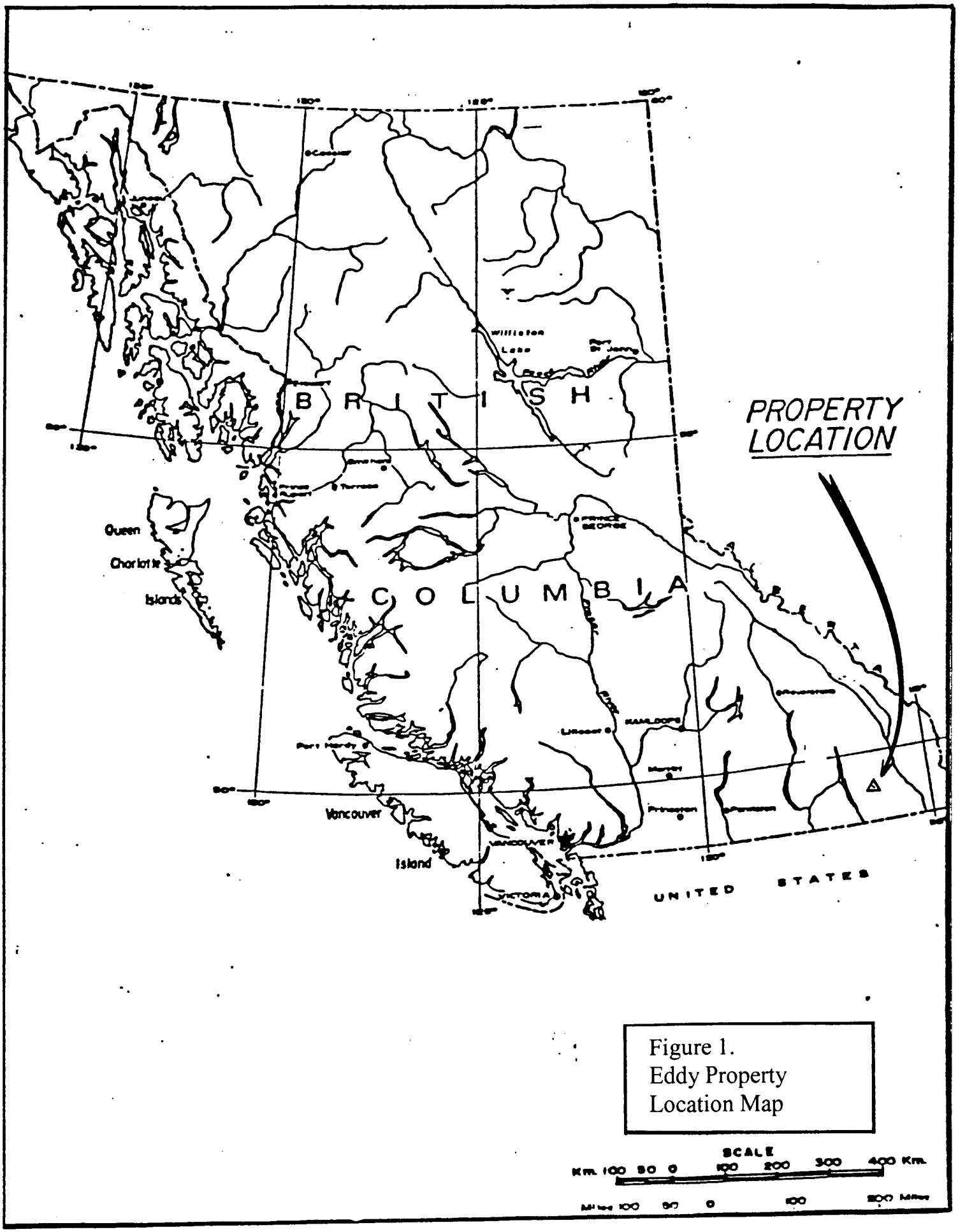


Figure 1.
Eddy Property
Location Map

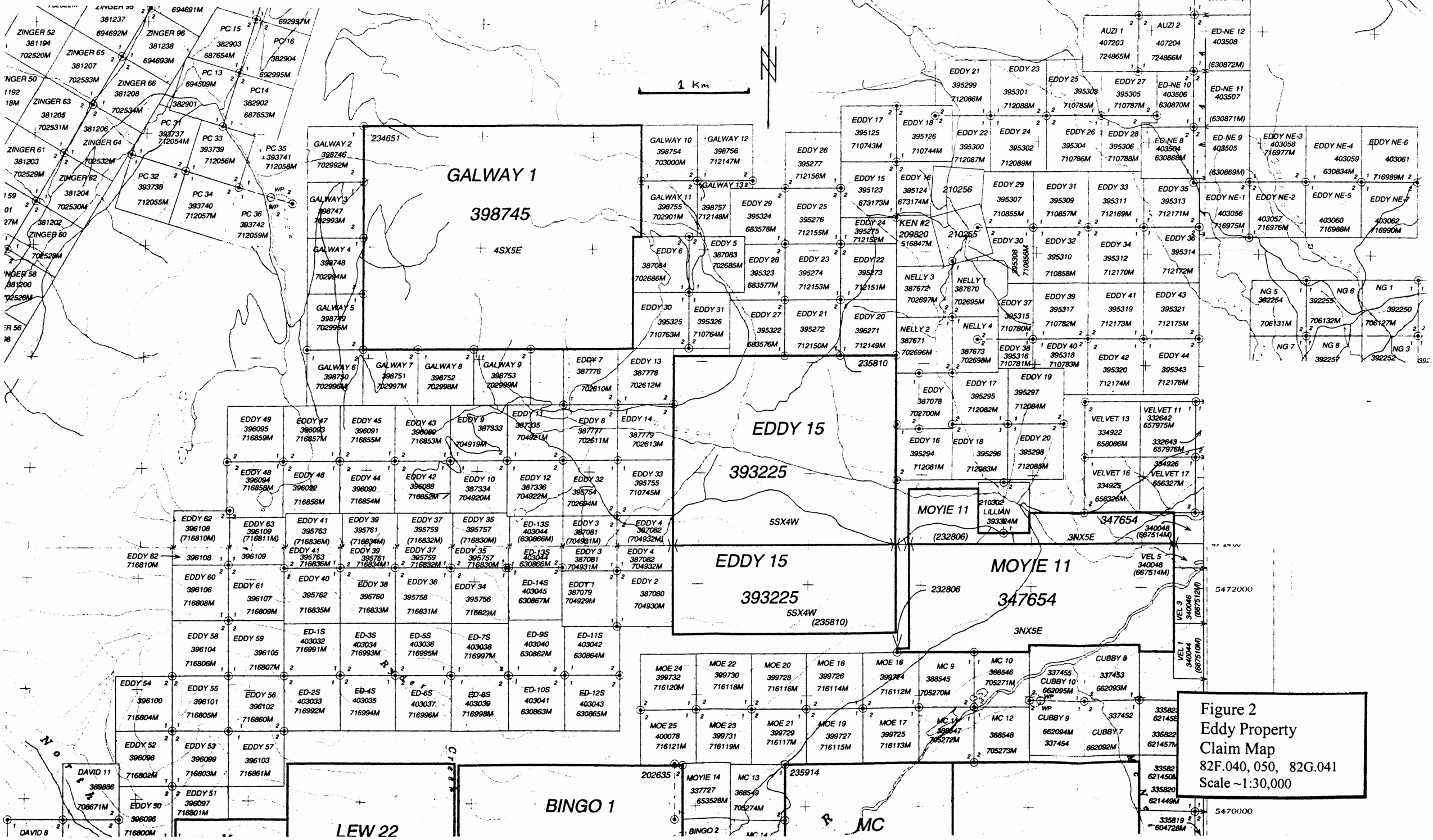


Figure 2
Eddy Property
Claim Map
82F.040, 050, 82G.041
Scale ~1:30,000

1.30 Physiography

The Eddy claim area is part of the Purcell Mountain Range. Elevations on the property range from 1460 to 2210 meters and topography varies from gentle and moderate wooded slopes to steep rocky slopes. Forest cover includes mainly pine, fir and larch. Areas within the claim block have been clear-cut logged within the past 30 years and are in various stages of regeneration.

1.40 History

The Moyie River is one of three main placer gold drainages in the Cranbrook area and Weaver Creek has had considerable placer gold produced from it. During the time of extensive placer gold production in the late 1800 and early to mid 1900's, prospecting for lode gold sources of the placers in the Cranbrook area was widespread. Numerous quartz veins were tested, some were found to be auriferous, and a few had minor production. No significant lode gold production is known from the area of the present Eddy claims. Two workings in the Prospector's Dream area may date back to the 1890's.

Building of logging roads in the Weaver Creek drainage in 1981 exposed gold-bearing quartz veins and led to staking of mineral claims. Early exploration on the property consisted of road building and trenching with minor geologic and geochemical work.

In 1984 a program of prospecting, geological mapping and soil and rock geochemistry was conducted. Encouraging gold values were obtained by reconnaissance soil sampling in a few areas. In 1987 a program of more soil sampling, trenching and diamond drilling further tested these areas (Morris, 1987). Three holes were drilled at the Hill Vein, three at the MC2 Shear area (Old Baldy Fault) and nine at the Galena Vein.

In 1989 an exploration program of prospecting, heavy mineral sampling in selected tributary drainages, soil and rock geochemistry, VLF-EM and magnetic geophysical surveying, geological mapping and trenching was conducted (Klewchuk and Kennedy, 1990). Emphasis continued to be on areas that were known to contain gold but the importance of the Old Baldy Fault as a control for gold mineralization was recognized. A small program in 1990 focused on a galena-bearing quartz vein hosted by gabbro south of the MC2 area.

In 2002, Ruby Red Resources conducted prospecting and rock geochemistry with favourable results (Rodgers, 2002).

1.50 Scope of Present Program

In 2003 exploration work on the Eddy claims included geologic mapping, rock geochemistry (49 samples), contour soil geochemistry (250 samples) and trenching (17 trenches).

2.00 GEOLOGY

2.1 Regional Geology

Mapping by Reesor (1981), Hoy and Diakow (1982) and Hoy (1984) has developed a good understanding of the geology and structure of the Cranbrook area of southeastern British Columbia. This area, which includes the Eddy claims, is part of the Purcell Anticlinorium, a geological sub-province which lies between the Rocky Mountain Thrust and Fold Belt to the east and the Kootenay Arc to the west.

The mesoproterozoic Purcell Supergroup which occurs within the core of the anticlinorium includes up to 11 kilometers of dominantly fine-grained clastic and carbonate rocks.

The Eddy claims are underlain by parts of the two lowermost units of the Purcell Supergroup, namely the Aldridge and Creston Formations. Both formations are comprised of fine-grained clastic sedimentary rocks; the Aldridge is a thick succession of predominantly impure quartzites and siltstones of turbidite affinity while the Creston Formation is a shallower water sequence of cleaner quartzites but with considerable siltstone and argillite. The Aldridge Formation is intruded by a series of gabbro to diorite composition sills and dikes which are called the Moyie Intrusions; a few dikes extend into the Creston Formation.

In a broad regional manner, structure of the Cranbrook area is dominated by a series of NNE oriented faults, at least some of which are believed to have been active during sedimentation in the Precambrian and thus have locally modified the type, distribution and thickness of late Proterozoic and Paleozoic rocks (Leech, 1958; Lis and Price, 1976).

The Eddy claims sit within an area of increased structural complexity which is more or less centered on the three prominent placer gold streams in the Cranbrook area, namely Perry Creek and the Moyie and Wild Horse Rivers. A series of NNE to NE oriented shear zones and a series of east to NE oriented transverse faults create the structurally complex, block-faulted area within which the placer gold occurs.

Cretaceous intrusions of granodiorite to syenite composition are scattered through the general area of placer gold occurrence near Cranbrook. These young rocks are probably the eastern limit of the Nelson Batholith complex. Some of the syenite and quartz monzonite stocks carry appreciable pyrite, pyrrhotite and chalcopyrite and tend to be associated with anomalous gold.

2.20 Property Geology

Regional mapping by federal and provincial government geologists provides only a basic framework of the geology of the Eddy claims. The claim block is underlain by Aldridge and Creston Formation rocks. The only major intrusions in the claim block are Precambrian gabbro and diorite sills and dikes. Minor occurrences of younger, Cretaceous or early Tertiary felsic

intrusive activity have been recognized by previous work and new occurrences were identified during the 2004 work.

Bedding typically strikes northeasterly with moderate to steep west dips. The Old Baldy Fault is the dominant structure on the claim block. It strikes northeasterly with moderate to steep northwest dip. Within the claim area the Old Baldy Fault has a more easterly trend than its typical NNE strike and this may be a factor in the association of gold with this structure on the claim block. The Old Baldy Fault where it has been mapped on the property is entirely within the Aldridge Formation, suggesting there is little if any vertical displacement on the structure. A short distance to the northwest of the Old Baldy Fault is a narrower fault that separates middle Aldridge Formation on the southeast from Creston Formation to the northwest. This structure was first recognized in 1989 and termed the AC fault (for Aldridge / Creston); in the MC2 and Galena Vein areas it has at least 350 meters of vertical displacement. Trenching of the AC Fault in 1989 found high grade gold-bearing quartz veining within the structure.

The Eddy property sits between the Cranbrook and Moyie transverse faults which may also be major controls of gold mineralization. No east-west oriented cross faults are known on the Eddy claims but the strong east-west linears of Weaver Creek and the North Moyie River suggest both of these drainages may reflect such structures.

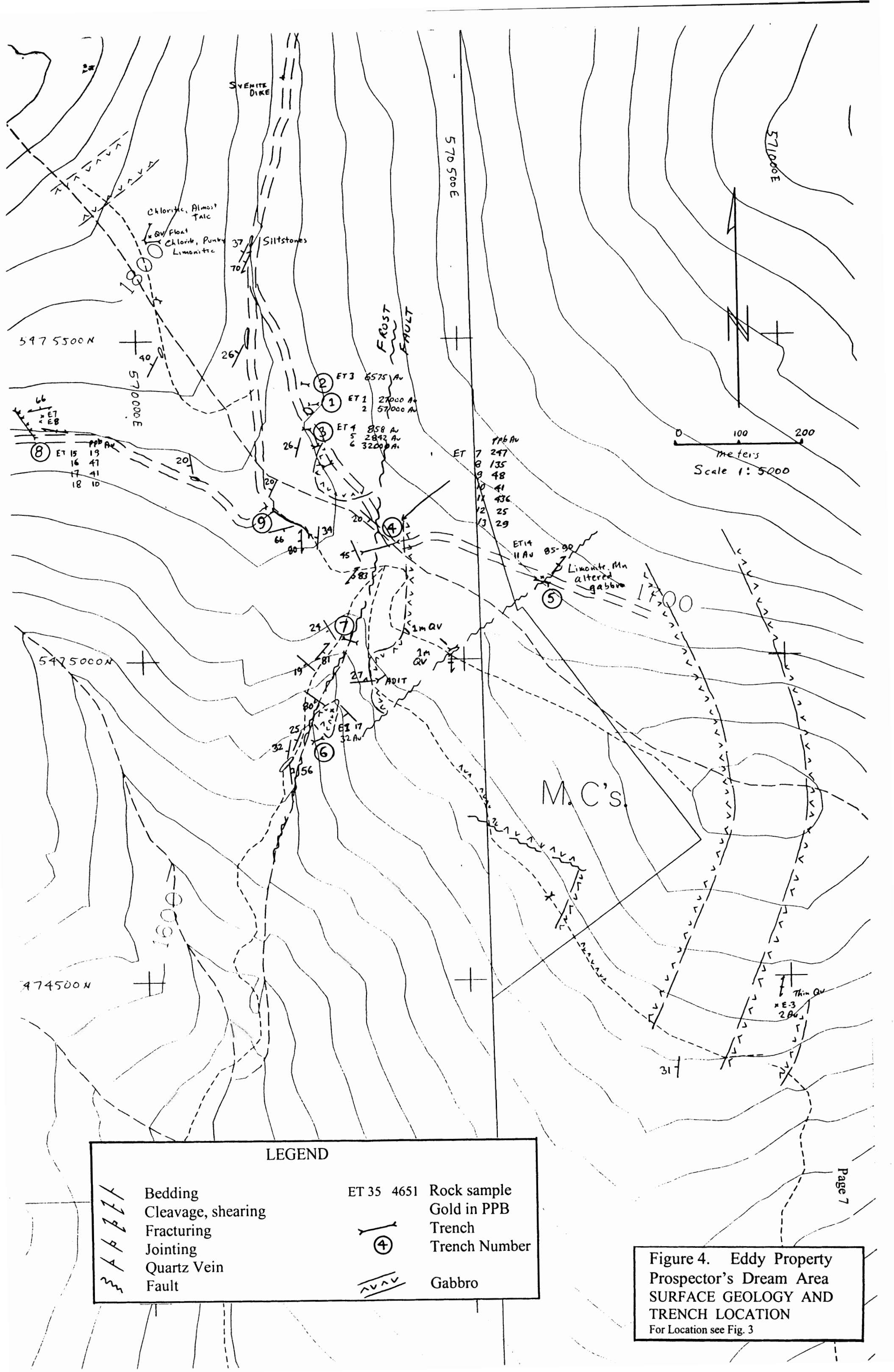
In 2004, a few days of geologic mapping were spent on each of four areas:

1. Prospector's Dream
2. Old Baldy Fault NW of Prospector's Dream
3. Hill Vein
4. MC2 area

1. Prospector's Dream

The Prospector's Dream area (Figs. 3 & 4) is underlain by middle Aldridge stratigraphy which is intruded by at least 2 fairly thick gabbro sills. A strong NNE striking 'Frost' Fault cuts through the small saddle at 5475150N 570400E. Two historic relatively flat-lying gold-bearing quartz vein prospects occur on opposite sides of this fault and may be related to it. Trenching crossed the Frost Fault in the saddle and established that anomalous gold mineralization (best value of 436 ppb over 25 cm.) occurs with brecciation, quartz veining and limonitic alteration within the structure. Additional trenching of the fault structure was attempted but was unsuccessful due to thick overburden.

There is widespread limonitic and manganese alteration with brecciation in the Prospector's Dream area and it is developed in a non-uniform manner, indicating structural control.



LEGEND

Bedding	ET 35 4651 Rock sample
Cleavage, shearing	Gold in PPB
Fracturing	Trench
Jointing	④ Trench Number
Quartz Vein	
Fault	Gabbro

Figure 4. Eddy Property
Prospector's Dream Area
SURFACE GEOLOGY AND
TRENCH LOCATION
For Location see Fig. 3

2. Old Baldy Fault NW of Prospector's Dream

A few exposures of the Old Baldy Fault occur along a steep sidehill northwest of the Prospector's Dream area, notably near 547600N 569150E (Fig. 3). The fault is a fairly wide zone of sheared middle Aldridge Formation quartzites, siltstones and argillites. The zone is variably silicified with fine disseminated pyrite as well as thin lensey quartz veins. Rock geochemistry done in 2002 apparently did not detect any significant gold mineralization. The Old Baldy Fault can be traced in float and sparse outcrop easterly to about 570000E where sample E4 returned only 0.2 ppb Au. To the west the position of the fault is uncertain across the ridge at ~568900E although there is considerable limonitic-altered float and some quartz vein breccia float near 1980-2000 m elevation on the ridge. Further west there is abundant quartz vein and altered float just east of the north fork of Weaver Creek near 568250E, 5475550N, suggesting the fault comes through here. Further to the southwest the fault zone is partially exposed by previous roadbuilding and trenching in the Galena Vein area. Rock sampling of sheared, silicified and pyritic fault zone material in 2002 from the Galena Vein area returned up to 3878 ppb Au from grab samples (Rodgers, 2002).

This limited rock sampling along the Old Baldy Fault NW of the Prospector's Dream area indicates gold mineralization is present within the fault structure but is not consistently developed.

West of the north fork of Weaver Creek, a parallel-trending but narrower fault zone separates middle Aldridge Formation rocks to the southeast from Creston Formation rocks to the northwest. This AC (Aldridge / Creston) Fault parallels the Old Baldy Fault from the MC2 area (~565500E 5472900N) to the north fork of Weaver Creek and possibly further east toward Noke Creek. Anomalous gold was identified within the AC Fault in 1989 (Klewchuk and Kennedy, 1989) and it remains a potential structural control of gold across much of the Eddy property.

3 Hill Vein Area

The Hill Vein (Figs. 3 & 5) is a north-striking, relatively flat west-dipping gold-bearing quartz vein with about 500 m of known strike length and up to ~1 m thick, that was discovered in the early 1980's by road building for logging. The vein appears to be related to a north striking 'Hill Vein' fault on its west margin. Initial work included extensive bulldozer trenching and the resulting rubble cover has masked details of the geology. A few days of geologic mapping in 2003 established that the vein occurs between 2 thick middle Aldridge gabbroic Moyie sills - the same sills that occur at the Prospector's Dream area. Favourable-looking quartz vein breccia and limonitic float SE of the Hill Vein and anomalous soil geochemistry north of the Hill Vein suggest the gold mineralization has more continuity than was recognized in the past. Trenching on the Hill Vein in 2004 crossed the north-striking western fault which has considerable brecciation, limonitic alteration, quartz veining and possible felsic intrusions associated with it. Trenching near the northern known extent of the Hill Vein encountered a series of flat-lying

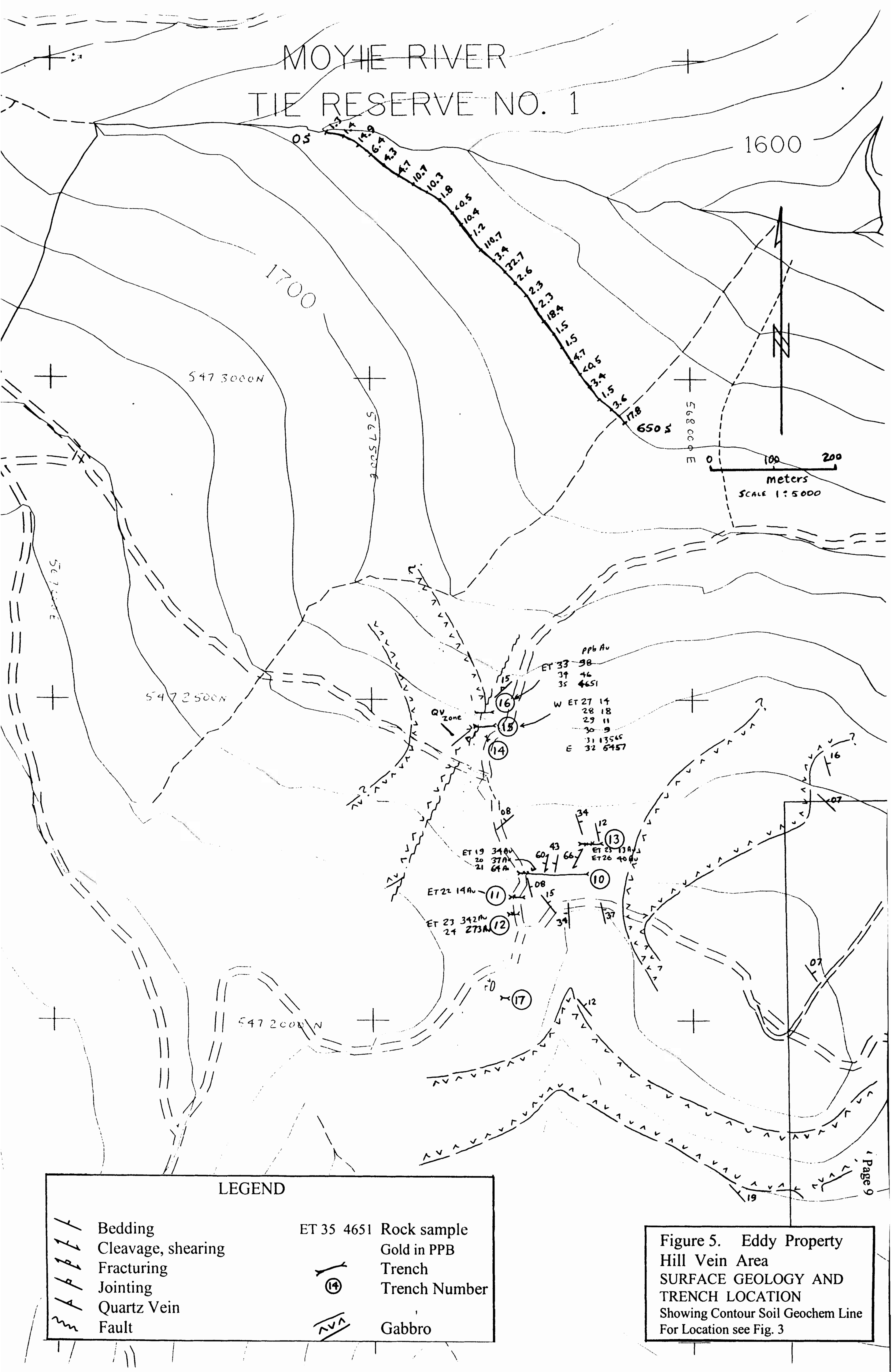


Figure 5. Eddy Property
Hill Vein Area
SURFACE GEOLOGY AND
TRENCH LOCATION
Showing Contour Soil Geochem Line
For Location see Fig. 3

auriferous quartz veins which appear related to the Hill Vein Fault. Further evaluation of the Hill Vein area is warranted. The fault structure should be traced and soil geochemistry can be used to identify areas of anomalous gold mineralization which can then be trenched and drilled.

4. MC2 area

Minimal geologic mapping was done in this area in 2003. Considerable trenching was done here in 1989 and widespread anomalous gold was detected; prospecting and rock geochemistry done in 2002 supports the presence of high gold values (Rodgers, 2002). Although no specific drill targets were identified in the MC2 area in the past, the area warrants continuing work to define such drill targets.

3.00 SOIL AND ROCK GEOCHEMISTRY

3.10 Soil Geochemistry

Soil samples were collected from 3 contour lines in two areas. Two lines are north and NW of the Prospector's Dream area and cover parts of the Old Baldy Fault zone while the third line is north of the Hill Vein prospect (Fig. 3). A total of 250 soil samples were collected; soils were taken from the B Horizon at an approximate depth of 15 cm, placed in Kraft paper bags, dried and shipped to Acme Analytical Laboratories Ltd. at 852 East Hastings Street, Vancouver, B.C., where they were analyzed for a 30 element ICP package and geochemical gold by standard analytical techniques. Soil contour lines are shown on Figure 3; lines, sample sites and gold values in ppb are shown in Figures 5 and 6. Complete geochemical analyses are provided in Appendix 2.

Anomalous gold occurs on all 3 lines sampled. The anomalous gold on the 2 northern lines indicates there is gold associated with the Old Baldy Fault in this area and anomalous values north of the Hill Vein indicate the Hill Vein mineralization may extend northward to this location. Both areas warrant follow-up exploration.

Old Baldy Fault Area

The two northern soil geochem lines, at approximate elevations of 1860 and 1940 meters (Figs. 3 and 6) cross the Old Baldy Fault in places. Elevated gold is present only at a few places along the soil lines. Where the Old Baldy Fault is crossed at the eastern end of the soil lines, gold values are consistently low with only rare isolated anomalous values. More consistent anomalous gold is present on both sides of the ridge east of the north fork of Weaver Creek, apparently

within the footwall area of the Old Baldy Fault. Further west, anomalous gold values are present in soils where the lines cross the Old Baldy Fault, as indicated by abundant anomalous quartz veining and limonitic alteration. This apparent irregular association of gold with the Old Baldy Fault may be due to other factors such as interfering structures. Further work should try to identify other controlling features such as intersecting structure.

North of Hill Vein

One soil line at 1640 m elevation ('Line 1690') was sampled about 700 m north of the Hill Vein and just south of Weaver Creek (Figs. 3 and 5). The line was intended to cross the inferred northerly strike of the Hill Vein Fault. Gold values on the line are mostly low but do range up to 110.7 ppb and support the extension of a mineralized Hill Vein Fault structure to the north.

3.20 Rock Geochemistry

Fourteen rock samples were collected during the course of geologic mapping in selected areas of the propert and an additional 35 rock samples were collected from trenches. Rock samples were shipped to Acme Analytical Laboratories Ltd. at 852 East Hastings Street, Vancouver, B.C., and analyzed for a 30 element ICP package and geochemical gold by standard analytical techniques. Rock sample sites are shown on Figures 3, 4 and 5 with sample descriptions in Appendix 1 and complete geochemical analyses in Appendix 3.

Only a few of the field rock samples have anomalous gold. Weak gold is present with minor copper mineralization in quartz veins in gabbro south of the Prospector's Dream area (sample E1, Fig. 4). Stronger gold mineralization is present in limonite breccia and quartz vein breccia in the inferred footwall area of the Old Baldy Fault on the ridge east of the north fork of Weaver Creek (samples E5 and E6, Fig. 3). These rock samples are close to anomalous contour soils.

In the trench sampling (see also section 4.00) anomalous gold is present in almost every sample. The flat-lying quartz vein of the 'Shaft' prospect west of the Frost Fault at the Prospector's Dream area returned very high values with analyses of 57000, 32000 and 27000 ppb Au. High values are also present at the Hill Vein area, again within fairly flat-lying quartz veins.

Anomalous gold occurs with elevated Mo, Cu, Pb, Zn, As, and Ag at the Prospector's Dream area. A similar but weaker association is evident in some of the other trench samples.

4.00 TRENCHING

4.10 Prospector's Dream area

Three trenches (trench 1, 2 & 3: Figs. 4 & 7) were dug on the 'Shaft prospect' on the west side of the Frost Fault, where an inclined shaft was formerly excavated on a north-striking, moderate west-dipping auriferous quartz vein. The bedding-parallel quartz vein was exposed in the 3 trenches over a north-south strike length of ~ 68 m, and in the trenches ranges in thickness from ~ 15 cm to 75 cm. The vein is discrete in the northern 2 trenches with minor wall rock alteration but in the southern trench the zone is a composite of brecciated limonitic wallrock and a series of thin veinlets with the widest quartz vein only 15 cm thick. Gold values are very high with 6575 ppb over 40 cm in the northern trench, 57000 ppb over 40 cm and 27000 ppb over 75 cm in the middle trench (location of the original inclined shaft), and an average of 17420 ppb over 1.2 m of thin quartz veins and brecciated wallrock in the southern trench (Fig. 7).

The control for this quartz vein is unknown but the Frost Fault, which should be only 10 or 15 m to the east, is a likely candidate. The intersection of this high grade quartz vein system and the Frost Fault is eroded but other similar quartz vein systems could occur along strike along the fault to the north or south, or at depth along the fault structure.

Trench 4 was located across the saddle where the Frost Fault was inferred (Figs. 4 & 8). The fault was intersected in the trench on the west side of the saddle. Previous trenching had been done here and there is considerable limonitic, liesegang-altered / stained rubble on surface. The fault zone in the trench is an 8 meter wide north-striking zone of complex brecciation. Fracturing and shearing in the zone dip 53° to 60° west. Sampling of the more limonitic and quartz vein-rich zones in the fault returned anomalous gold values up to 436 ppb. To the east of the fault, a peripheral zone of brecciation and quartz veins trending NE also carries weak gold, with values up to 247 ppb. Although no high grade gold values were seen in the Frost Fault, exposing the structure and seeing anomalous gold within the structure and in peripheral thin quartz veins and altered, brecciated wallrock strongly supports the idea of this structure being an important control of gold mineralization.

Trench 5 crossed a fault zone in gabbro at ~ 5475100N, 570600E (Fig. 4) which strikes NE and dips steeply NW. The gabbro is decomposed and limonitic, typical of hydrothermal activity related to the gold mineralizing process. This structure may be related to the Frost Fault; a NE striking quartz vein in the trench has only very weak gold (11 ppb; sample ET-14).

Trench 6 was an attempt to cross the Frost Fault near 5474850N, 570300E but bedrock could not be reached.

Trench 7 was another attempt at crossing the Frost Fault near 5475030N, 570300E. Although the trench started adjacent to a small cliff of bedrock to the west, again bedrock could not be reached in the trench.

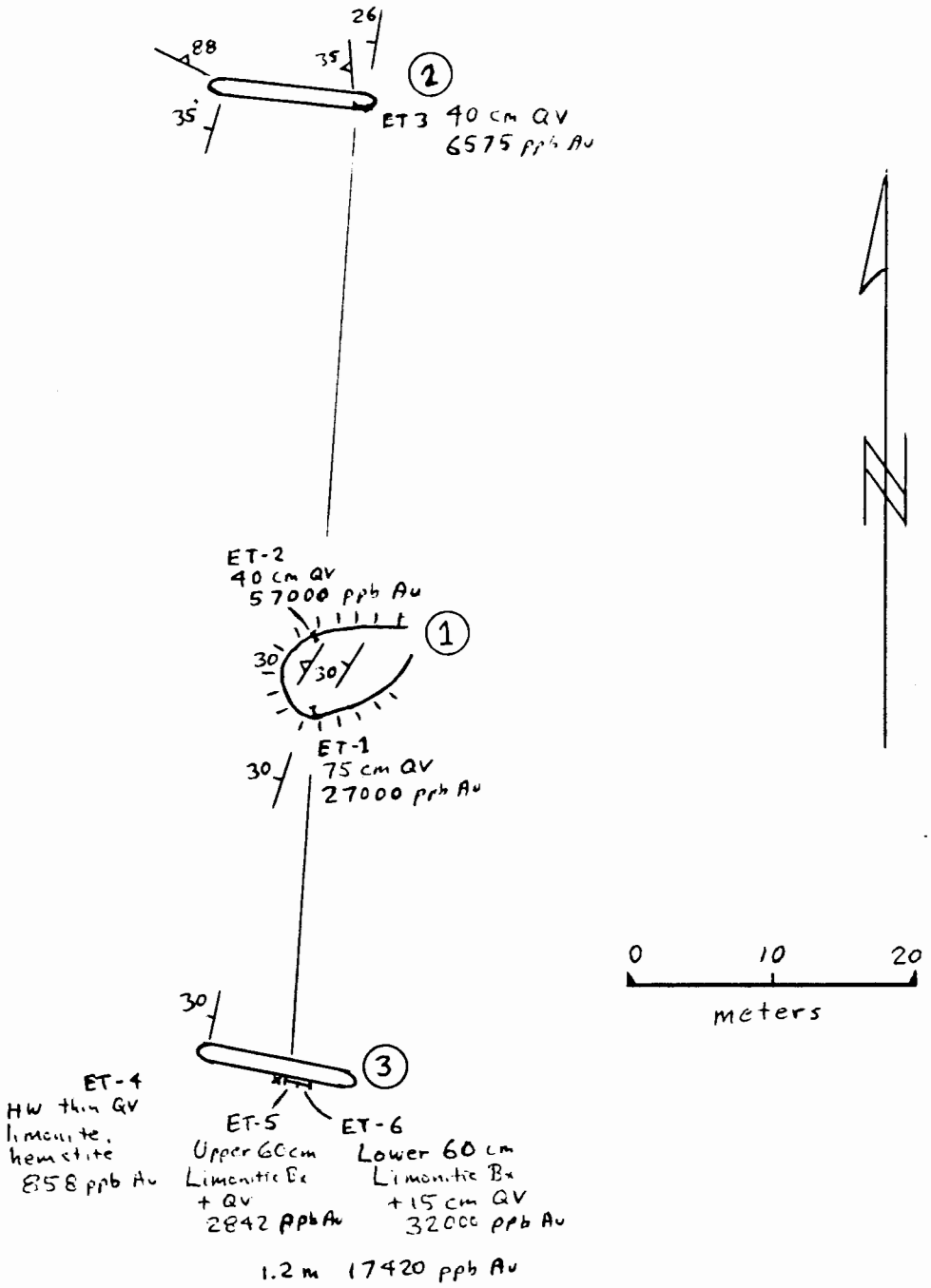


Figure 7. Eddy Property
Detail of Trenches 1, 2 & 3
Scale 1;500
For Location see Figs. 3 & 4.

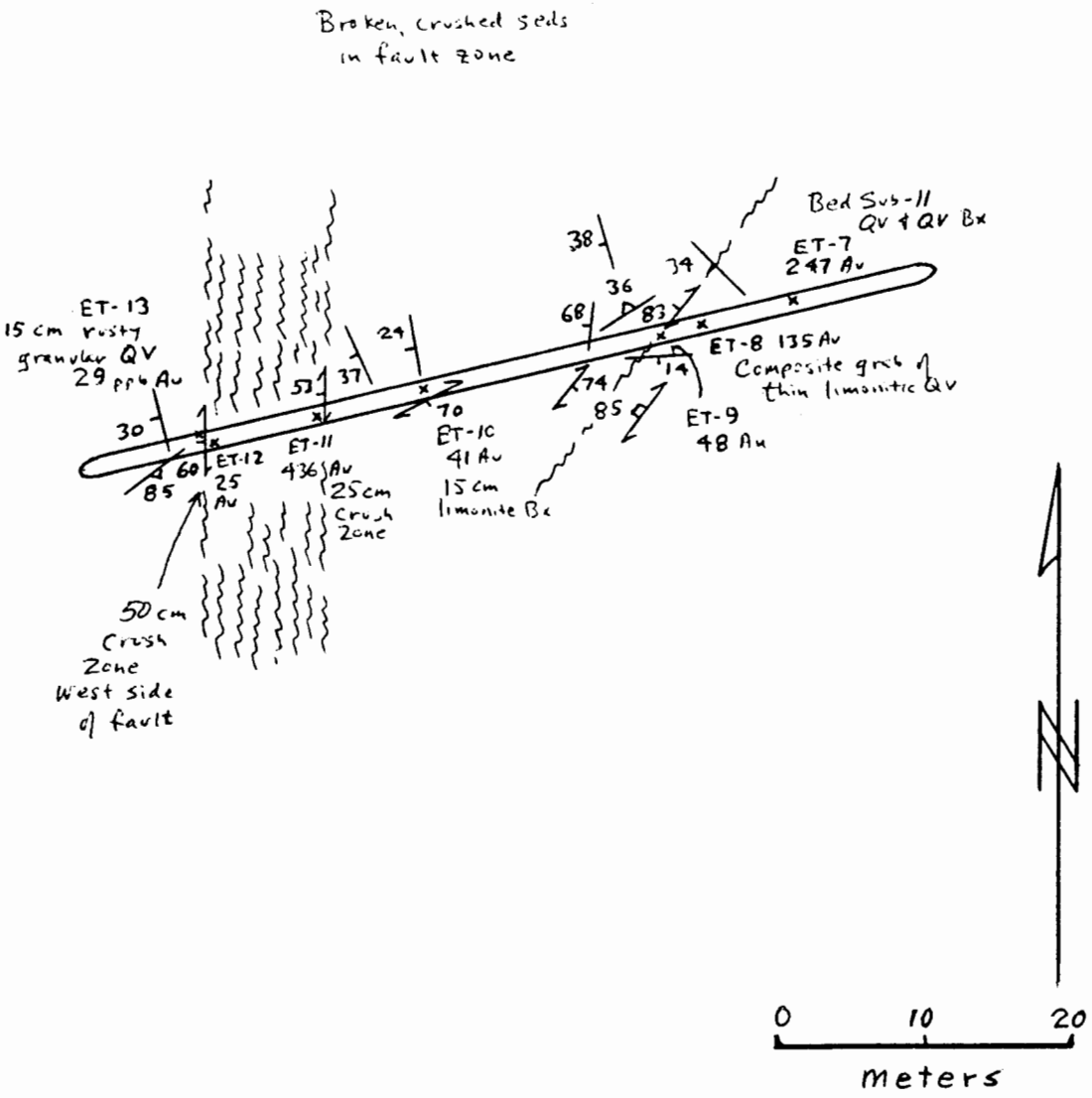


Figure 8. Eddy Property
Detail of Trench 4
Scale 1;500
For Location see Figs. 3 & 4.

Trench 8 was located at 5475400N, 568800E (Fig. 4) near a possible bedrock exposure of quartz vein breccia. The quartz vein breccia was not seen in the trench but the entire trench was in punky, limonitic and manganese altered siltstone with extensive vertical fracturing and scattered narrow near-vertical crush zones with limonite breccia and minor quartz veining. Four samples, ET-15 to 18 returned low anomalous gold values from 10 to 47 ppb. The strong alteration suggests there is a nearby favourable structure.

Trench 9 was dug along a central road adjacent to quartz vein float and to look for an extension of the Shaft zone quartz vein seen in trenches 1, 2 & 3. Bedrock in the trench is very shallow and relatively unaltered with only a few narrow zones of weaker brecciation and limonite. Small scale folding is present indicating the presence of structural deformation.

4.20 Hill Vein Area

Trench 10 crossed the axis of a gentle anticline on the east side of the Hill Vein Fault near 5472200N, 567800E (Fig. 5) and just north of rock samples collected in 2002 which had multi-gram gold values (Rodgers, 2002). Bedrock at the west end is very hard, possibly silicified and could not be very well exposed but no quartz veining or significant alteration was noted. A few minor faults with weak limonitic brecciation were encountered; three samples returned 34, 37 and 64 ppb Au (samples ET 19-21), the latter over a 70 cm width. Similar narrow limonitic faults were crossed near the east end of the trench and trench 13 was dug to the north, to cross these narrow zones again. Similar low gold values were obtained (Samples ET 25, 26 with 13, 40 ppb Au). These results show the widespread nature of weak gold mineralization in the Hill Vein area.

Trenches 11 and 12 are both near 5472200N, 567700E and were dug to try and expose part of the Hill Vein. No larger quartz veins were seen in trench 11 (14 ppb Au in limonite breccia at the west end; sample ET-22). A larger quartz vein exposed in trench 12 ran 273 ppb Au over 1 meter, while a hangingwall breccia zone (ET-23) ran 342 ppb Au. Previous workers have described the Hill Vein as a relatively flat-lying structure bounded on the west by a steep fault zone. Extensive former trenching and subsequent recontouring of the trench debris has left no exposures of the quartz vein.

Trenches 14, 15 and 16 were dug near the northern edge of the known extent of the Hill Vein system (Figs. 5 & 9). Trench 14 was a dig-out of an existing trench that had sloughed in, leaving no bedrock exposure. A thick quartz vein exposed only in the west wall has an over-all shallow northwesterly dip. To the north, trenches 15 and 16 are at a lower elevation and below the projection of the vein seen in trench 14. Both trenches 15 and 16 started in altered gabbro on their west end, crossed a NNE-striking fault with steep (but both NW and SE) dip. This structure appears to be the 'Hill Vein Fault' although further south it is inferred to strike more N-S. Both trenches east of the fault zone cut into complex zones of brecciation and quartz veining with strong sub-horizontal 'crush zones'. The picture is complicated by the presence of old trenching in the area. Gold values in the thick quartz veins, which appear to be a series of separate veins,

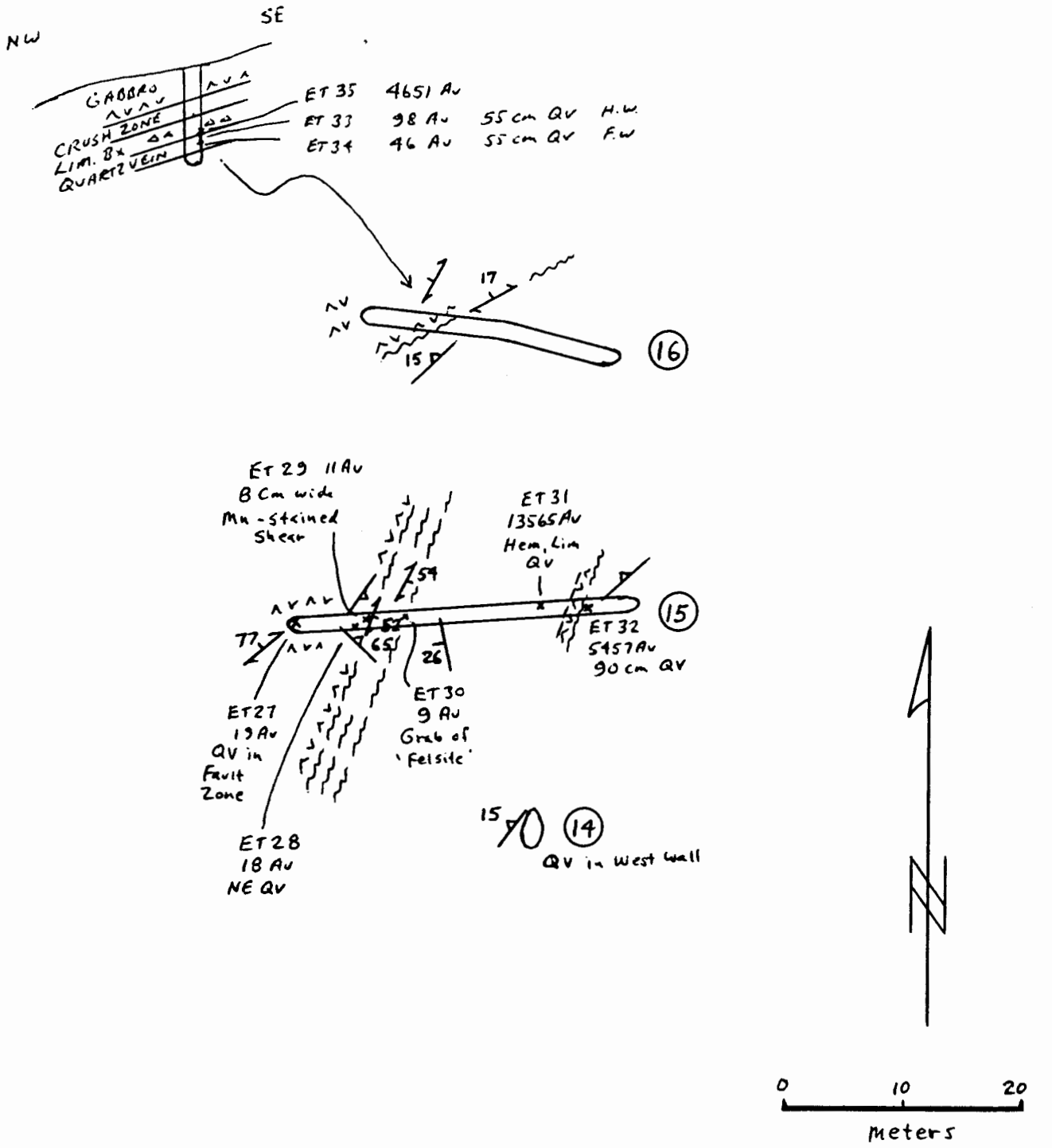


Figure 9. Eddy Property
Detail of Trenches 14, 15 & 16
Scale 1;500
For Location see Figs. 3 & 5.

range from 46 to 13565 ppb (Fig. 9). Although the zones are complex, it appears that a series of gold-bearing quartz veins and brecciation are developed on the immediate eastern side of the 'Hill Vein Fault'.

Trench 17 was dug further south, on an old trench, in the vicinity of abundant blocky quartz vein rubble from previous trenching; the intent was to expose the Hill Vein in this area and sample a bedrock exposure. No quartz vein was seen in the trench. The upper part of the trench was in siltstone rubble and the only bedrock was gabbro at some depth.

5.00 CONCLUSIONS

1. Geologic mapping and trenching at the Prospector's Dream confirmed this area to be structurally complex in detail. The north striking 'Frost Fault' carries anomalous gold and could be an important structural control. Three trenches on the Shaft zone just west of the Frost Fault exposed the gold-bearing quartz vein over a strike length of about 68 m and returned very high gold values with 57000 ppb Au over a 40 cm quartz vein, 27000 ppb Au over a 75 cm quartz vein and 17420 ppb Au over 1.2 m of a composite of thin quartz veins and brecciated, limonitic siltstones.

2. Trenching at the Hill Vein area indicates a series of irregular, relatively flat-lying, lensey gold-bearing quartz veins are developed in association with a northerly to NE striking fault zone. Extensive historic trenching has left most of the 500 m strike length of the Hill Vein covered with rubble. Anomalous gold in one contour soil geochemistry line about 700 m north of the Hill Vein suggests the gold mineralization may have a much greater strike length than was previously indicated.

3. The gold-bearing systems of relatively flat-lying quartz veins with associated sub-horizontal brecciation and alteration developed alongside the fault zones at both the Prospector's Dream and Hill Vein areas are important targets to explore as they may be quite large. To date only very short strike lengths of the fault structures have been trenched and no drilling has tested these targets.

4. Gabbros at both the Prospector's Dream and Hill Vein areas are strongly limonitic altered and decomposed where they are cut by faults. This alteration is evidently a product of the hydrothermal alteration associated with the gold mineralizing process and it can be used as an exploration guide.

5. Contour soil lines which tested the Old Baldy Fault between the north fork of Weaver Creek and Noke Creek defined areas of anomalous gold which require careful follow-up exploration.

6. Although the MC2 area received little attention in 2003 it remains a prime target on the property because of high gold values previously detected by surface rock geochemistry, soil geochemistry and trenching programs.

7. In addition to local higher gold values in the flat-lying quartz veins and larger fault zones, weaker gold is present in many limonitic fault breccia zones and shows that a strong, widespread gold mineralizing system exists on the Eddy claim group.

6.00 REFERENCES

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7.00 STATEMENT OF COSTS

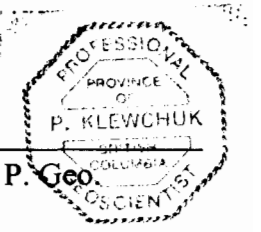
Geologist (P. Klewchuk) 19 days, field work & office, @ $321/day	$6099.00
4x4 truck 14 days @ $100/day, includes mileage	$1400.00
Rock geochemistry 49 samples @ $22/sample	1078.00
Soil geochemistry 250 samples @ $22/sample	5050.00
Trenching	3050.00
Report 3 ½ days @ $321/day	1123.50
Project administration and supervision (G. Turner) includes travel costs from Calgary 5 days @ $450/day	2250.00
Drafting, Kevin Franck and Associates	166.00
Total Cost	**$20,216.50**

8.00 AUTHOR'S QUALIFICATIONS

As author of this report I, Peter Klewchuk, certify that:

1. I am an independent consulting geologist with offices at 246 Moyie Street, Kimberley, B.C.
2. I am a graduate geologist with a B.Sc. degree (1969) from the University of British Columbia and an M.Sc. degree (1972) from the University of Calgary.
3. I am a Fellow of the Geological Association of Canada and a member of the Association of Professional Engineers and Geoscientists of British Columbia.
4. I have been actively involved in mining and exploration geology, primarily in the province of British Columbia, for the past 25 years.
5. I have been employed by major mining companies and provincial government geological departments.

Dated at Kimberley, British Columbia, this 15th day of March, 2004.



Peter Klewchuk, P. Geo.

Appendix 1. Description of Rock Samples

Sample Number	Description
E-1	White granular quartz vein, 30 to 70 cm wide, in gabbro; weathering cpy with malachite stain.
E-2	Pink hematite and limonite stained quartz veins in limonitic argillite.
E-3	Limonitic quartz in locally bleached, altered gabbro; small darker limonitic vugs.
E-4	"Bedding-parallel" quartz vein lens; vuggy and rusty with chloritic margins.
E-5	Argillic altered, liesegang stained zone with minor quartz; limonitic breccia.
E-6	Quartz vein breccia float. Lighter orange-brown limonitic siltstone with cross-cutting light gray QV.
E-7	Strongly limonitic QV breccia, pink, brown and reddish limonite. Sample from 1-2 m diam exposure (2 of them) with 'conformable' attitude but may be float.
E-8	Similar to E-7.
E-9	Thin rusty QV 092/85°S with minor QV breccia adjacent.
E-10	Bedding and cleavage parallel QV. Vuggy cavities on margins of QV are limonitic - dark reddish black to pink hematite. Seds are a bit brecciated with angular elongate fragments in QV. Vein is lensey, to 8 cm wide.
E-11	Quartz vein with thin, vuggy, very rusty streaks (sulfides leached out?). Patch of chloritic seds in immediate FW.
E-12	Thin rusty QV at argillite-quartzite contact.
E-13	Narrow bedding-parallel sheared quartz vein zone with some strong limonite.
E-14	4 m NE of E-13. Same zone.
ET-1	Chip sample over 75 cm of quartz vein on south edge of trench.
ET-2	40 cm chip of QV on north wall of trench; about 4 m north of ET-1. About 1 m of HW seds are limonite breccia.
ET-3	Chip of 40 cm QV. Granular at top, limonitic, vuggy in middle, less limonitic at base.
ET-4	Grab sample of thin hangingwall veinlets. Some with hematite, all with limonite.
ET-5	60 cm chip of upper half of composite zone of limonite breccia and quartz veins. QV are irregular but quite srongly developed.
ET-6	Footwall 60 cm chip of 'main' QV of 15 cm + limonite breccia, limonitic rubble.
ET-7	Bedding sub-parallel QV and QV breccia with pink-brown (dolomite?) And pastel green (argillic) alteration with pyrite and specular hematite.
ET-8	Composite grab of limonitic QV in 038/85W fractures.
ET-9	Chip over 45-50 cm of fault zone. Mainly limonite breccia, very little QV. 040/83W.
ET-10	15 cm wide limonite bx zone at 063/70S. Zone cross-cuts bedding - sub-parallel fractures in wallrock which are both N and S dipping.
ET-11	25 cm crush zone on east edge of larger fault zone. East half more limonite breccia, west half more orange-brown colored with broken QV.
ET-12	50 cm chip of west side of large fault zone; limonite breccia.

ET-13	15 cm wide rusty granular QV. Some marginal bx creating local pods to 30 cm wide.
ET-14	QV at 029/90 in altered gabbro.
ET-15	Limonitic clay gouge zone 077/66N 15-30 cm wide but anastomosing.
ET-16	Near-vertical clay gouge zone. Very irregular with thin rusty broken QV. Mn on vertical fractures.
ET-17	Narrow rusty, chloritic gouge zone 1-2 cm wide at 102/wavy 70N-70S. More rusty than most of rock - see no quartz.
ET-18	Siliceous, rusty part of anastomosing crush zone.
ET-19	Thin QV at 117/73S, bit rusty.
ET-20	Grab of more intense limonite breccia with thin light gray QV in orange-white limonite altered breccia.
ET-21	70 cm chip of fault, QV bx zone at 022/72W. Yellowish limonite with thin light gray QV
ET-22	Grab of limonite breccia with thin lensey QV.
ET-23	Grab of darker limonite breccia adjacent to QV on north wall.
ET-24	1 m chip across crushed quartz of Hill Vein. No sulfides recognized.
ET-25	Grab of stronger limonite breccia, weak QV bx.
ET-26	Grab of ~80 cm wide limonite breccia / fault zone. No obvious QV. 027/66W.
ET-27	QV in fault zone at west end of trench, in limonitic, decomposed gabbro, ~050/77NW.
ET-28	Sample of 036/45SE rusty QV in south wall; part of limonite & Mn stained QV zone.
ET-29	Rusty, Mn-stained shear ~8 cm wide, at 024/52SE.
ET-30	Grab of irregular whitish patch of gritty, probable felsite.
ET-31	Grab of vuggy, hematitic, limonitic quartz; quartz is broken up but may be ~2.5 m thick.
ET-32	Chip of 90 cm thick QV near contact with gabbro dike
ET-33	Top 55 cm of QV, mostly massive whitish quartz with minor limonite.
ET-34	Bottom 55 cm of QV.
ET-35	Grab of HW contact of QV. Limonitic, brecciated, silicified siltstone or quartzite.

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GEOCHEMICAL ANALYSIS CERTIFICATE

Ruby Red Resources Inc. PROJECT EDDY File # A305301 Page 1

207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6 Submitted by: Glen Rodgers

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.6	2.6	2.3	44	<.1	4.2	4.0	561	1.90	<.5	2.1	1.3	4.6	98	<.1	<.1	.1	39	.54	.079	10	13.7	.54	238	.144	1	.92	.087	.54	2.3	.01	2.1	.4	.07	5	<.5
L1690 0SE	.5	16.4	19.0	31	.2	8.1	3.5	191	1.32	1.5	.5	1.4	1.6	10	.1	.1	.5	25	.10	.022	10	7.9	.25	79	.138	2	1.15	.017	.04	.1	.03	1.4	.1	.08	11	.5
L1690 25SE	.2	15.2	8.1	17	.1	4.3	2.7	172	.70	.6	.7	14.9	.5	6	.2	.1	.2	10	.06	.021	21	5.3	.20	50	.017	1	.64	.005	.03	<.1	.03	.9	<.1	<.05	3	<.5
L1690 75SE	.4	11.0	11.8	27	.1	6.5	5.6	670	1.49	2.5	.5	6.4	1.3	6	.2	.2	.4	24	.05	.038	13	8.4	.21	61	.036	1	.86	.006	.03	.1	.05	1.1	.1	.07	5	<.5
L1690 100SE	.7	16.8	10.4	33	.1	8.5	7.0	235	1.35	1.8	.6	4.3	.8	11	.2	.1	.3	22	.15	.027	20	10.1	.39	57	.029	<1	1.26	.008	.03	.1	.03	1.4	.1	<.05	6	<.5
L1690 125SE	1.1	49.5	55.0	58	.5	10.8	23.1	413	1.56	4.9	2.6	4.7	.4	30	1.4	.4	.4	24	.33	.134	38	37.2	.23	122	.019	1	2.56	.009	.06	.1	.14	2.1	.1	.14	5	1.5
L1690 150SE	.3	7.4	11.1	18	.1	3.9	2.2	97	1.13	2.2	.3	10.7	1.3	6	.1	.1	.3	28	.07	.018	15	8.4	.16	46	.067	<1	.64	.009	.03	.1	.03	1.1	<.1	.08	7	<.5
L1690 175SE	.2	6.7	9.5	15	.1	2.8	2.3	291	.45	.8	.4	10.3	.9	4	.1	<.1	.3	9	.05	.016	22	5.4	.14	45	.022	<1	.54	.005	.03	<.1	.01	.7	<.1	<.05	4	<.5
L1690 200SE	.9	45.0	29.2	25	.2	8.3	8.3	312	1.78	3.0	1.0	1.8	2.4	12	.3	.1	.5	34	.09	.032	16	10.9	.24	70	.118	<1	1.66	.018	.05	.2	.05	2.4	.1	.06	10	<.5
L1690 225SE	.6	28.0	21.9	21	.1	6.4	4.6	270	1.33	2.3	.9	<.5	1.2	13	.2	.1	.4	22	.10	.028	18	7.5	.18	61	.081	<1	1.25	.016	.04	.1	.04	1.7	.1	<.05	10	<.5
L1690 250SE	.5	23.4	14.4	32	.1	11.2	6.9	215	1.66	2.0	.7	10.4	1.6	8	.2	.1	.3	30	.07	.023	24	12.9	.50	57	.044	<1	1.46	.009	.04	.1	.03	1.6	.1	<.05	6	<.5
L1690 275SE	.7	31.9	19.8	25	.2	7.3	4.0	99	1.53	2.2	.7	1.2	3.0	6	.2	.1	.3	25	.05	.027	20	9.9	.29	57	.050	<1	1.51	.009	.04	.1	.04	1.8	.1	<.05	7	<.5
L1690 300SE	.8	19.7	12.9	41	.1	8.7	5.6	133	3.00	4.6	.9	110.7	4.0	5	.2	.2	.3	45	.07	.060	13	14.3	.32	50	.058	<1	3.17	.007	.03	.1	.12	2.5	.1	<.05	10	<.5
L1690 325SE	1.0	67.6	31.4	55	.2	21.1	37.1	1295	3.11	6.2	1.9	3.4	2.7	15	.3	.3	.5	56	.15	.081	26	20.8	.55	185	.045	1	3.17	.009	.07	.1	.05	3.8	.1	<.05	9	<.5
L1690 350SE	.3	12.2	16.4	22	.1	5.0	2.9	101	1.14	1.7	.4	32.7	1.6	15	.1	.1	.3	29	.18	.017	17	6.6	.20	82	.083	<1	.71	.013	.03	.1	.01	1.1	.1	<.05	7	<.5
L1690 375SE	.6	11.3	11.8	27	.1	7.6	4.1	95	2.94	4.6	.4	2.6	3.4	6	.1	.2	.3	76	.10	.042	20	11.8	.31	47	.052	<1	1.04	.007	.04	.1	.03	1.6	.1	<.05	8	<.5
L1690 400SE	.6	10.3	16.0	28	.2	5.3	2.6	97	1.67	3.0	.6	2.3	3.1	10	.1	.2	.3	40	.13	.045	16	8.9	.21	60	.094	<1	1.71	.013	.04	.1	.04	1.9	.1	<.05	11	<.5
RE L1690 400SE	.6	10.9	14.9	30	.2	5.0	2.8	100	1.83	3.4	.5	3.8	2.7	9	.1	.1	.3	40	.12	.042	13	8.1	.18	57	.087	<1	1.62	.011	.04	.1	.05	1.6	.1	<.05	12	<.5
L1690 425SE	.2	8.0	5.0	15	<.1	4.2	1.7	52	.72	1.3	.3	2.3	1.2	10	.1	.1	.1	19	.11	.011	19	6.5	.16	40	.025	<1	.43	.006	.04	<.1	.01	.9	<.1	<.05	3	<.5
L1690 450SE	.4	14.7	9.2	23	.1	7.3	4.1	174	1.61	2.5	.4	18.4	2.6	8	.1	.1	.2	36	.11	.027	23	9.6	.34	52	.030	1	1.03	.006	.03	.1	.03	1.1	.1	<.05	5	<.5
L1690 475SE	.8	59.5	41.2	64	.4	15.5	35.3	1425	2.95	3.9	1.3	1.5	1.7	25	.4	.2	.5	55	.30	.079	26	17.8	.38	119	.079	4	2.96	.017	.06	.1	.09	3.4	.1	.07	12	.6
L1690 500SE	.6	12.3	25.0	23	.1	4.0	3.5	87	.92	1.1	.5	1.5	1.2	11	.1	.1	.4	23	.12	.018	11	5.5	.12	68	.107	<1	.83	.016	.03	.1	.02	1.1	.1	<.05	9	<.5
L1690 525SE	.4	16.7	8.5	40	<.1	10.8	5.9	226	2.33	3.5	.5	4.7	4.7	3	.1	.1	.3	45	.07	.025	20	13.6	.54	38	.033	1	1.10	.005	.04	.1	.02	1.9	<.1	<.05	5	<.5
L1690 550SE	.2	4.0	9.0	17	.1	.8	.5	128	.19	<.5	.1	<.5	.3	6	.1	.1	.3	9	.06	.012	9	2.5	.03	44	.053	<1	.26	.015	.03	<.1	.03	.5	<.1	<.05	4	<.5
L1690 575SE	.7	105.0	36.5	28	.4	9.9	6.2	189	1.75	3.1	2.7	3.4	.8	11	.4	.1	.3	34	.12	.058	30	11.0	.20	60	.064	1	2.57	.015	.04	.1	.12	3.1	.1	<.05	10	.6
L1690 600SE	.6	34.3	31.5	40	.4	9.8	10.2	853	1.33	3.3	1.0	1.5	.5	26	.5	.2	.3	27	.27	.049	33	11.4	.33	122	.050	<1	1.32	.012	.05	.1	.08	1.7	.1	.10	7	<.5
L1690 625SE	1.2	24.3	22.2	65	.1	8.1	38.6	3455	2.67	4.4	.9	3.6	1.5	12	.6	.2	.3	61	.17	.058	25	10.9	.32	172	.038	<1	1.31	.007	.04	.1	.04	2.7	.2	<.05	5	.5
L1690 650SE	.7	39.1	27.7	50	.2	14.0	12.8	871	2.28	4.6	1.2	17.8	2.6	20	.6	.3	.5	44	.15	.046	48	15.4	.36	183	.066	<1	1.92	.010	.06	.1	.12	4.0	.1	.07	10	.7
L1860 0S	1.1	9.3	10.6	22	<.1	6.2	2.5	54	4.20	6.6	.6	1.8	6.0	3	.1	.3	.4	45	.03	.052	13	15.7	.24	18	.073	1	1.98	.006	.03	.2	.04	1.3	.1	<.05	11	.5
L1860 25S	.9	5.7	6.0	14	.1	5.4	2.5	44	1.74	3.4	.5	<.5	4.2	4	.1	.1	.3	19	.04	.027	22	7.7	.24	28	.024	<1	1.17	.004	.02	.1	.04	.8	.1	<.05	6	<.5
L1860 50S	.9	3.7	3.6	13	<.1	4.9	2.1	54	1.18	2.8	.5	2.3	4.7	3	<.1	.2	.3	16	.04	.025	28	5.3	.28	24	.013	<1	.63	.003	.02	.1	.01	.5	<.1	<.05	4	<.5
L1860 75S	1.2	6.3	6.2	22	<.1	10.5	3.6	57	3.38	4.2	.8	1.8	7.4	2	.1	.2	.3	28	.02	.054	26	18.3	.57	27	.018	2	1.85	.003	.03	.1	.04	1.4	<.1	<.05	6	<.5
L1860 100S	.7	6.1	5.8	23	.1	7.1	2.4	54	2.17	3.4	.5	1.7	5.0	1	.1	.1	.2	23	.01	.028	20	11.2	.43	17	.022	<1	1.30	.003	.02	.1	.03	1.2	<.1	<.05	6	.5
L1860 125S	1.0	7.2	9.6	39	.2	10.5	6.8	253	2.47	4.6	.8	1.6	6.1	4	.2	.2	.3	30	.05	.058	17	16.1	.44	48	.043	1	2.42	.007	.05	.1	.09	2.0	.1	<.05	7	.5
L1860 150S	.8	3.6	5.6	14	.1	4.3	1.9	47	1.77	2.7	.4	1.0	5.1	3	.1	.2	.3	29	.02	.018	27	8.6	.22	21	.034	<1	.81	.004	.02	.1	.02	.9	.1	<.05	8	<.5
STANDARD DS5	13.5	148.6	24.1	142	.3	24.8	12.6	774	3.00	19.4	6.7	41.8	3.1	51	5.9	3.8	6.6	63	.76	.100	14	191.6	.68	138	.095	18	2.15	.034	.14	4.9	.16	3.4	1.2	<.05	7	5.0

GROUP 1DX - 15.0 GM SAMPLE LEACHED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 300 ML, ANALYSED BY ICP-MS.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
- SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 23 2003 DATE REPORT MAILED: Nov 7/03 SIGNED BY. C. Leong .D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Data L FA

Appendix 2. Soil Geochem Analyses

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.5	2.4	2.2	43	<.1	4.3	4.1	510	1.98	.7	2.0	.8	4.6	96	<.1	<.1	.1	46	.59	.081	11	15.0	.63	251	.140	<1	.99	.090	.50	2.2	.01	2.3	.4	.10	5	<.5
L1860 175S	1.3	3.6	6.6	21	<.1	5.8	2.9	79	2.63	3.5	.4	1.9	5.1	3	.1	.2	.4	44	.02	.035	25	12.1	.33	24	.046	6	1.06	.003	.04	.2	.02	1.2	.1	.13	10	<.5
L1860 200S	.8	6.1	8.2	24	<.1	7.2	4.6	49	2.43	3.6	.5	3.2	4.5	3	.1	.2	.3	37	.02	.049	19	14.4	.41	36	.040	<1	2.19	.003	.03	.1	.10	1.7	.1	.08	7	<.5
L1860 225S	.6	2.3	3.9	8	<.1	4.1	1.6	29	1.50	2.5	.3	1.3	3.9	2	<.1	.1	.2	25	.01	.024	25	8.3	.29	17	.017	<1	.92	.003	.02	.1	.04	1.0	<.1	.07	6	<.5
L1860 250S	1.2	5.3	10.3	20	<.1	8.5	3.6	47	2.83	4.9	.6	3.5	5.6	3	.1	.3	.4	42	.02	.044	20	12.8	.47	30	.085	<1	1.99	.006	.03	.2	.04	1.4	.1	.08	11	<.5
L1860 275S	.8	8.2	8.5	18	.1	4.6	2.7	50	1.73	3.0	.9	1.7	3.6	4	.1	.2	.3	33	.03	.088	7	7.7	.16	32	.100	2	2.98	.012	.02	.1	.07	1.6	<.1	<.05	9	<.5
L1860 300S	1.2	10.0	8.3	24	.1	9.5	5.5	64	1.90	5.0	1.0	3.0	4.9	4	.1	.1	.2	26	.04	.085	13	10.0	.42	39	.059	1	3.02	.008	.03	.1	.06	2.0	<.1	.06	7	<.5
L1860 325S	.9	12.3	11.4	25	.2	7.9	7.0	60	2.00	4.9	1.2	2.6	4.4	5	.1	.1	.2	33	.05	.108	8	8.9	.23	52	.098	2	3.55	.014	.03	.2	.11	2.8	.1	.07	9	.6
L1860 350S	.8	11.3	10.3	28	<.1	7.9	5.2	129	2.17	6.0	1.0	2.7	4.1	5	.1	.2	.3	32	.04	.141	4	9.8	.11	37	.124	<1	5.33	.015	.02	.2	.09	2.4	<.1	.06	10	.5
L1860 375S	1.4	7.1	12.9	30	.1	7.2	5.9	251	2.26	5.6	.7	15.4	4.5	6	.1	.3	.3	38	.05	.089	8	10.7	.18	58	.067	1	3.01	.008	.03	.2	.06	1.5	.1	<.05	9	<.5
L1860 400S	1.3	6.7	12.6	40	<.1	11.1	10.1	187	2.26	6.7	.8	2.3	5.2	6	.1	.2	.4	36	.03	.057	14	11.5	.37	63	.054	<1	2.44	.007	.05	.1	.04	1.8	.1	<.05	8	<.5
L1860 425S	1.5	7.3	19.1	31	<.1	14.5	12.2	185	2.48	6.9	1.0	2.1	7.4	5	<.1	.2	.4	30	.03	.044	19	12.2	.65	67	.048	<1	2.48	.006	.05	.1	.04	2.0	.1	<.05	7	<.5
L1860 450S	.9	6.3	13.5	31	<.1	10.4	9.6	108	2.28	5.5	.6	2.5	4.5	7	.1	.2	.3	32	.06	.057	10	10.2	.28	74	.067	1	2.77	.008	.04	.1	.07	1.3	.1	<.05	9	<.5
L1860 475S	1.2	6.2	15.8	38	<.1	14.4	16.8	520	2.68	8.0	1.2	2.4	7.0	5	.1	.3	.4	29	.04	.046	20	13.2	.63	64	.046	1	1.86	.004	.06	.2	.03	1.5	.1	<.05	8	<.5
L1860 500S	1.6	6.4	16.3	42	<.1	19.9	19.4	210	3.31	8.2	.9	2.3	7.8	5	.1	.3	.4	35	.05	.037	19	17.5	.68	95	.061	<1	2.69	.005	.05	.2	.05	1.8	.1	<.05	10	<.5
RE L1860 500S	1.6	6.4	15.4	41	<.1	18.6	20.2	197	3.20	7.9	.9	1.7	7.7	6	.1	.2	.4	37	.05	.041	18	16.2	.68	97	.061	3	2.95	.005	.06	.1	.05	1.7	.1	<.05	10	<.5
L1860 525S	1.5	6.8	17.9	40	.1	16.0	15.5	217	2.87	9.6	.8	2.2	6.3	6	.1	.3	.4	39	.06	.040	17	14.0	.58	67	.062	<1	2.32	.006	.06	.1	.04	1.7	.1	<.05	9	<.5
L1860 550S	1.4	8.1	150.4	56	.1	26.5	34.3	214	2.95	7.2	1.6	75.5	8.9	5	.1	.2	.4	31	.03	.036	19	15.4	.66	50	.057	<1	2.11	.004	.05	.1	.04	1.7	.1	<.05	7	<.5
L1860 575S	2.1	5.7	16.8	44	<.1	16.5	10.8	147	3.42	9.3	.7	2.6	7.7	4	.1	.3	.5	42	.03	.033	20	19.6	.70	62	.050	<1	2.62	.004	.05	.1	.04	2.1	.1	<.05	11	<.5
L1860 600S	1.7	4.8	28.8	41	.1	15.7	9.8	278	2.95	8.1	.5	8.0	5.8	7	.1	.3	.5	41	.05	.030	21	16.9	.65	76	.037	<1	1.89	.004	.05	.1	.04	1.8	.1	<.05	9	.5
L1860 625S	1.9	7.9	148.1	78	.1	26.4	27.2	170	3.49	8.2	1.7	13.2	11.0	5	.1	.2	.6	26	.03	.039	26	18.4	.88	56	.020	<1	2.18	.003	.05	.1	.04	2.3	.1	<.05	6	.5
L1860 650S	2.1	45.7	622.0	161	.3	24.6	35.3	386	2.85	8.1	2.2	12.7	9.5	4	.3	.4	.5	34	.04	.045	22	16.8	.74	54	.048	<1	2.49	.006	.05	.1	.04	2.3	.1	<.05	8	<.5
L1860 675S	1.5	12.5	162.4	148	.1	12.4	8.8	166	2.56	9.6	.8	61.3	6.1	4	.4	1.5	.4	33	.03	.047	14	13.2	.47	68	.060	4	3.22	.008	.04	.6	.07	1.9	.1	<.05	7	<.5
L1860 700S	1.0	7.5	49.8	110	.5	11.0	9.2	260	2.09	3.0	.4	6.3	4.0	5	.8	.2	.4	30	.05	.046	14	11.0	.30	72	.058	3	2.21	.011	.05	.3	.04	1.3	.1	<.05	8	<.5
L1860 725S	1.3	8.8	32.4	66	.1	10.4	6.2	127	2.24	4.2	.9	7.0	5.7	5	.2	.3	.3	36	.04	.058	12	11.5	.32	54	.072	<1	2.81	.010	.04	.5	.07	2.0	.1	<.05	8	<.5
L1860 750S	1.1	22.5	12.3	58	.1	12.7	10.0	181	2.35	5.0	.5	20.7	5.2	6	.3	.3	.3	40	.07	.041	17	10.9	.55	46	.047	<1	1.74	.007	.05	.1	.03	2.0	.1	<.05	7	.5
L1860 775S	1.4	9.6	21.1	78	.2	14.6	11.2	260	2.48	4.7	1.0	8.3	6.8	7	.3	.4	.4	27	.07	.040	18	12.7	.52	81	.053	3	2.30	.007	.05	.2	.06	1.5	.1	<.05	7	<.5
L1860 800S	1.0	7.0	61.1	124	.6	15.9	16.1	144	2.22	4.0	.7	8.6	5.5	7	.3	.5	.3	27	.06	.048	16	11.7	.42	62	.053	<1	2.56	.008	.05	.2	.05	1.4	.1	<.05	7	<.5
L1860 825S	1.1	55.0	10.7	53	.1	14.2	17.4	444	2.39	5.5	.7	.9	4.2	8	.2	.2	.3	45	.08	.087	7	10.1	.25	44	.103	<1	3.85	.016	.05	.2	.05	2.0	.1	<.05	9	<.5
L1860 850S	1.1	26.9	9.7	40	.1	14.6	12.3	378	2.36	4.7	.6	1.7	5.4	6	.1	.2	.4	31	.06	.031	18	11.9	.45	74	.047	<1	1.84	.005	.06	.1	.03	1.3	.1	<.05	7	.6
L1860 875S	.9	11.4	14.0	39	<.1	11.7	8.1	539	2.15	4.4	.5	1.0	4.7	5	.1	.2	.4	30	.06	.032	18	11.5	.36	57	.044	1	1.94	.005	.06	.1	.05	1.4	.1	<.05	7	.7
L1860 900S	1.3	5.2	29.2	60	.1	11.3	7.1	111	2.48	5.2	.5	1.8	5.1	4	.1	.6	.5	31	.04	.024	20	11.1	.32	54	.034	<1	1.66	.004	.05	.1	.01	1.3	.1	<.05	7	<.5
L1860 925S	.7	7.4	58.2	41	.1	10.0	9.5	176	1.59	4.8	1.0	1.0	5.7	4	.1	.5	.3	13	.02	.022	25	8.4	.39	32	.014	<1	1.06	.002	.03	.1	.02	.9	<.1	<.05	4	<.5
L1860 950S	1.4	8.1	17.2	40	.3	13.7	10.1	141	1.90	5.5	.7	2.9	5.9	6	.1	.2	.3	24	.04	.027	18	10.4	.29	74	.041	<1	2.04	.006	.04	.1	.05	1.3	.1	<.05	6	<.5
L1860 975S	1.2	7.2	9.2	29	<.1	10.9	8.4	161	1.84	3.6	.6	1.4	5.3	6	.1	.2	.3	22	.05	.027	16	8.9	.25	81	.041	<1	2.21	.006	.05	.1	.03	1.3	.1	<.05	6	.6
STANDARD DS5	12.2	136.6	25.6	138	.2	24.3	11.7	740	2.96	18.6	6.2	44.0	2.9	51	5.4	3.9	6.4	62	.77	.080	14	190.0	.66	137	.103	19	2.15	.033	.15	4.5	.16	3.6	1.0	<.05	7	5.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.7	2.9	2.5	50	<.1	4.6	4.3	625	2.09	<.5	2.1	.5	5.4	105	<.1	<.1	.1	56	.65	.082	10	16.1	.67	273	.148	<1	1.12	.103	.55	2.5	<.01	2.3	.4	.13	6	<.5
L1860 1000S	.9	12.9	12.7	30	<.1	14.9	17.1	190	2.09	3.3	1.5	1.0	8.1	5	.1	.2	.3	32	.04	.035	15	11.2	.32	89	.071	<1	2.87	.008	.06	.2	.04	1.8	.1	.11	8	<.5
L1860 1025S	.7	12.5	9.9	33	<.1	14.8	14.9	271	1.93	3.3	.8	3.3	5.0	8	.1	.2	.3	33	.07	.035	13	10.3	.25	100	.090	<1	3.00	.011	.07	.1	.03	1.8	.1	.06	8	<.5
L1860 1050S	.9	9.1	10.1	31	<.1	11.9	8.4	272	2.33	3.9	.8	2.4	6.4	6	<.1	.2	.3	29	.04	.031	19	10.4	.37	67	.040	<1	2.24	.006	.05	.1	.03	1.3	.1	.09	7	<.5
L1860 1075S	.9	6.2	9.5	34	<.1	8.6	6.5	208	2.20	3.4	.4	55.0	5.0	4	.1	.2	.4	31	.03	.019	19	10.3	.28	75	.032	<1	1.54	.004	.05	.1	.03	1.0	.1	<.05	7	<.5
L1860 1100S	.9	7.6	11.8	29	<.1	10.1	7.0	405	1.98	3.2	.7	.6	4.0	10	.1	.2	.3	29	.10	.075	9	9.3	.18	91	.075	3	2.89	.010	.06	.2	.04	1.4	.1	.07	8	<.5
L1860 1125S	.8	6.4	10.4	32	<.1	8.2	5.3	140	1.78	2.5	.6	.7	4.6	6	.1	.2	.3	29	.03	.040	14	9.4	.25	66	.046	1	1.70	.007	.04	.1	.04	1.2	.1	<.05	7	<.5
L1860 1150S	1.2	9.6	16.7	62	<.1	12.2	9.0	384	2.53	6.8	.8	<.5	5.8	6	.1	.3	.4	36	.04	.080	10	12.8	.23	71	.076	<1	2.97	.010	.06	.1	.06	1.5	.1	<.05	10	<.5
L1860 1175S	1.3	8.8	14.5	36	<.1	7.8	5.1	283	2.47	4.6	.6	<.5	4.3	6	.1	.3	.4	39	.06	.069	8	10.2	.13	64	.091	<1	3.11	.011	.05	.2	.07	1.4	.1	<.05	11	<.5
L1860 1200S	1.3	7.6	14.5	40	<.1	8.2	4.2	143	2.46	5.4	.6	.6	4.9	5	.1	.4	.4	36	.04	.080	7	10.6	.18	46	.095	<1	2.76	.011	.07	.2	.04	1.3	.1	<.05	10	<.5
L1860 1225S	1.0	12.8	20.1	49	<.1	11.3	7.7	238	2.49	4.8	.8	.8	5.1	8	.1	.4	.4	36	.06	.069	12	12.2	.27	98	.086	<1	3.15	.010	.05	.2	.04	1.9	.1	<.05	9	<.5
L1860 1250S	1.0	6.6	12.5	35	.1	6.5	3.4	272	1.66	2.2	.4	<.5	2.9	6	.1	.2	.4	31	.06	.026	14	8.8	.15	51	.045	<1	1.08	.008	.06	.1	.02	1.0	.1	<.05	7	<.5
L1860 1275S	.4	5.0	9.3	26	<.1	4.8	2.0	105	1.20	2.4	.5	1.9	4.6	5	.1	.1	.4	26	.06	.023	20	7.0	.13	48	.027	1	.96	.004	.05	.1	.02	1.1	.1	<.05	6	<.5
L1860 1300S	1.0	10.9	24.4	31	.1	12.8	10.6	299	2.33	4.1	2.0	<.5	4.3	29	.1	.2	.7	33	.21	.027	28	12.0	.38	72	.041	<1	1.79	.007	.06	.1	.02	1.3	.1	<.05	8	<.5
L1860 1325S	1.4	9.0	18.6	35	.1	6.8	3.6	142	2.98	3.7	.5	<.5	4.5	8	.1	.3	.6	47	.06	.048	13	12.0	.18	53	.085	2	1.72	.007	.04	.1	.04	1.2	.1	<.05	12	<.5
L1860 1350S	1.2	12.4	17.7	50	.1	12.7	6.7	186	3.00	5.3	1.0	.7	6.6	7	.1	.3	.6	38	.07	.043	21	14.1	.47	76	.055	3	2.05	.005	.07	.2	.04	1.7	.1	<.05	9	<.5
L1860 1425S	.8	15.0	25.5	37	.1	13.8	11.1	383	2.23	4.4	1.9	1.7	2.4	26	.2	.3	.5	32	.26	.047	25	15.2	.42	72	.026	<1	2.11	.007	.08	.1	.03	1.5	.1	<.05	7	<.5
L1860 1450S	.8	15.6	15.7	41	.1	16.6	15.6	226	2.66	5.3	1.4	.9	6.6	8	.1	.2	.4	27	.06	.059	20	15.1	.44	88	.041	1	2.72	.006	.07	.1	.03	1.7	.1	<.05	7	<.5
L1860 1475S	.6	9.5	11.1	39	.1	7.1	5.4	278	1.79	2.8	.7	1.1	2.3	9	.1	.1	.4	24	.06	.097	16	9.1	.18	89	.038	<1	1.42	.006	.05	.1	.03	.9	.1	<.05	6	<.5
L1860 1500S	1.0	11.0	12.2	54	.1	11.4	7.1	277	2.58	6.4	.8	3.5	5.4	6	.1	.2	.4	30	.04	.077	16	12.3	.32	70	.062	<1	2.31	.006	.06	.2	.05	1.4	.1	<.05	8	<.5
RE L1860 1500S	.9	11.3	12.7	55	.1	10.9	7.5	271	2.64	6.3	.9	2.1	5.3	7	.1	.3	.4	33	.04	.075	17	12.9	.32	71	.066	1	2.32	.007	.05	.2	.04	1.4	.1	<.05	8	<.5
L1860 1525S	.7	11.6	8.5	44	.1	10.6	6.8	161	2.28	6.7	1.0	4.9	6.9	4	.1	.2	.3	26	.03	.053	19	10.4	.33	56	.055	2	2.21	.006	.04	.1	.04	1.5	.1	<.05	7	<.5
L1860 1550S	1.3	13.8	12.9	45	.1	18.2	11.6	264	2.62	8.6	.9	2.6	6.9	5	.1	.2	.4	29	.03	.035	15	12.3	.34	86	.044	<1	2.48	.005	.05	.1	.06	1.4	.1	<.05	8	<.5
L1860 1575S	1.0	7.9	9.0	27	.1	14.8	9.4	178	2.32	6.4	.7	4.1	5.4	7	<.1	.2	.4	24	.08	.031	18	10.3	.32	63	.040	<1	1.92	.005	.05	.1	.02	1.0	.1	<.05	7	<.5
L1860 1600S	.8	6.9	10.0	35	.1	9.4	8.2	536	1.98	6.2	.5	3.6	4.6	5	.1	.2	.4	27	.04	.031	15	8.7	.20	86	.059	5	1.60	.009	.05	.1	.03	1.3	.1	<.05	7	<.5
L1860 1625S	.6	5.9	6.8	23	<.1	5.6	3.8	201	1.88	5.8	.4	13.0	4.6	3	<.1	.2	.4	23	.03	.020	22	7.7	.20	38	.021	2	1.20	.004	.04	.1	.01	.8	.1	<.05	6	<.5
L1860 1650S	.9	12.0	11.3	41	.1	17.0	11.2	303	2.06	5.4	1.1	4.0	5.7	6	.1	.3	.3	26	.04	.041	12	9.8	.23	110	.089	3	2.67	.009	.05	.2	.04	1.8	.1	<.05	7	<.5
L1860 1675S	.6	6.0	11.2	30	<.1	8.3	6.8	341	1.72	4.8	.5	4.0	4.5	5	<.1	.2	.3	27	.05	.033	15	8.9	.22	65	.051	2	1.57	.007	.05	.1	.02	1.0	.1	<.05	6	<.5
L1860 1700S	.8	10.3	12.8	35	.1	14.1	10.5	491	2.13	5.8	1.1	4.3	5.2	13	.1	.2	.4	32	.14	.033	19	11.8	.29	81	.053	3	2.03	.010	.06	.1	.02	1.4	.1	<.05	8	.5
L1860 1725S	.5	6.2	14.5	46	.1	6.3	4.4	119	1.84	4.2	.4	.9	3.8	4	.1	.2	.4	30	.04	.026	15	9.7	.21	49	.038	2	1.51	.006	.05	<.1	.02	1.0	.1	<.05	7	<.5
L1860 1750S	.5	8.6	16.7	50	.1	10.2	7.1	158	2.04	3.3	.8	1.2	4.7	7	.2	.2	.3	26	.07	.065	7	10.5	.20	66	.069	4	2.81	.009	.06	.1	.04	1.6	.1	<.05	8	<.5
L1860 1775S	.5	12.7	18.3	34	.1	14.5	10.7	744	2.04	3.2	1.0	16.9	5.2	15	.1	.2	.4	26	.18	.020	21	16.2	.74	61	.028	<1	1.80	.007	.05	.1	.01	1.7	.1	<.05	6	<.5
L1860 1800S	.9	10.1	11.2	51	.1	11.3	9.4	242	2.26	6.1	.7	9.6	6.2	5	.1	.2	.3	30	.04	.056	15	9.9	.23	70	.078	5	2.52	.009	.05	.2	.03	1.5	.1	<.05	7	<.5
L1860 1825S	.9	8.8	15.4	48	.1	9.3	7.3	290	2.32	5.6	.5	51.3	5.6	4	.1	.3	.5	32	.04	.036	20	10.7	.26	62	.054	2	1.64	.007	.06	.2	.03	1.2	.1	<.05	7	<.5
L1860 1850S	.6	6.2	12.3	52	.1	7.8	6.1	436	1.59	3.4	.4	10.4	3.5	5	<.1	.2	.3	22	.06	.024	15	8.2	.20	88	.049	2	1.38	.006	.06	.1	.02	.9	.1	<.05	6	<.5
STANDARD DS5	12.6	150.9	26.0	146	.2	25.8	12.3	757	3.02	18.9	6.4	44.8	2.8	50	5.7	3.9	6.6	65	.74	.086	13	194.4	.69	136	.099	18	2.11	.033	.15	5.0	.17	3.3	1.1	<.05	7	5.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
L1860 1875S	.7	14.0	19.5	69	.1	10.2	7.5	326	2.49	3.8	.6	5.6	4.0	5	.1	.3	.3	48	.07	.078	10	10.4	.29	85	.104	<1	2.67	.012	.08	.1	.05	1.8	.1	.12	9	.6
L1860 1900S	.5	15.2	14.0	69	.1	12.3	9.8	482	2.43	3.4	.7	6.1	5.4	6	.1	.2	.2	42	.06	.067	9	9.8	.23	81	.113	1	2.99	.014	.07	.1	.03	1.7	.1	.06	8	.7
L1860 1925S	.6	14.3	12.3	83	.1	9.1	9.5	276	2.84	2.6	.4	14.8	3.3	5	.1	.2	.3	59	.11	.051	13	8.6	.27	93	.099	<1	1.68	.012	.14	.1	.02	2.0	.2	.08	9	<.5
L1860 1950S	.8	36.8	14.2	77	.1	14.8	14.1	246	3.31	5.1	.8	19.9	6.6	6	.1	.2	.3	53	.08	.045	20	11.4	.46	98	.084	1	2.21	.010	.17	.1	.04	2.4	.2	<.05	7	<.5
L1860 1975S	.7	21.0	10.3	63	.1	9.9	10.4	181	3.26	2.9	.4	39.4	3.8	5	.1	.2	.3	58	.11	.048	16	9.4	.32	85	.093	3	1.81	.011	.14	.1	.03	2.3	.2	<.05	9	.7
L1860 2000S	.6	61.9	12.6	47	.1	10.2	10.6	134	2.80	2.9	.4	2.8	2.8	6	.1	.2	.3	87	.14	.034	12	9.0	.29	85	.077	3	1.91	.013	.08	.1	.02	2.3	.1	<.05	8	<.5
L1860 2025S	.7	24.3	12.6	63	.1	12.3	11.7	258	2.51	3.7	.6	5.2	4.6	5	.1	.2	.3	58	.09	.040	15	9.9	.34	73	.063	2	2.14	.010	.09	.1	.02	2.4	.1	<.05	8	<.5
L1860 2050S	.6	20.5	10.5	75	.2	9.6	8.5	199	2.26	3.1	.6	8.9	4.7	6	.1	.1	.3	28	.07	.057	17	9.7	.31	69	.050	3	2.18	.008	.07	.1	.03	1.7	.1	<.05	6	<.5
L1860 2075S	.6	33.7	11.7	108	.3	12.2	17.0	530	2.55	3.3	.7	2.9	3.8	6	.1	.1	.3	46	.09	.088	9	9.7	.25	75	.103	3	3.14	.017	.09	.2	.04	3.0	.2	<.05	8	.6
L1860 2100S	.4	70.2	7.9	77	.3	11.1	12.7	338	3.20	2.9	.4	6.0	3.3	6	.1	.2	.2	101	.13	.082	10	7.4	.45	67	.102	3	1.95	.015	.10	.1	.03	3.9	.2	<.05	7	.5
L1860 2125S	.5	137.5	9.7	117	.2	15.8	17.2	764	3.15	3.6	.4	2.7	2.1	9	.2	.2	.2	131	.21	.077	6	7.3	.36	65	.132	2	2.55	.021	.10	.1	.06	3.6	.2	<.05	9	.6
L1860 2150S	.7	110.1	12.6	88	.2	15.3	13.0	555	3.02	5.2	.6	106.6	3.3	8	.1	.2	.2	89	.13	.133	5	9.7	.28	59	.138	4	4.13	.015	.08	.2	.08	3.5	.1	<.05	10	.5
L1860 2175S	.6	71.8	11.6	102	.3	11.7	11.4	706	2.40	3.9	.4	.8	2.5	8	.3	.2	.2	50	.13	.098	6	8.5	.21	62	.104	2	2.80	.015	.07	.1	.05	2.1	.1	<.05	8	<.5
L1860 2200S	.4	21.3	13.1	75	.2	8.1	9.3	1330	1.85	3.0	.4	2.1	2.2	9	.3	.2	.3	41	.13	.106	6	8.0	.15	65	.116	4	2.42	.017	.05	.1	.03	1.9	.1	<.05	8	<.5
L1860 2225S	.8	62.4	12.8	83	.4	10.7	9.6	499	1.90	4.3	1.2	1.7	3.3	9	.3	.2	.2	39	.08	.142	8	8.3	.16	66	.149	4	4.13	.021	.04	.2	.05	3.9	.1	<.05	11	.7
L1860 2250S	.6	23.3	9.9	90	.3	16.7	13.7	373	2.72	2.6	.5	2.7	2.6	9	.2	.1	.2	71	.19	.080	6	9.6	.35	69	.110	<1	2.80	.024	.09	.1	.03	3.6	.1	<.05	8	<.5
L1860 2275S	.6	12.8	14.4	77	.1	12.8	11.9	925	2.35	3.1	.3	1.2	2.0	10	.1	.3	.3	58	.16	.090	5	10.4	.24	67	.121	1	2.89	.018	.05	.1	.06	1.9	.1	<.05	9	.5
L1860 2300S	1.0	38.3	12.5	70	.2	12.1	10.4	908	2.39	4.1	.9	2.1	3.3	6	.1	.2	.3	51	.10	.115	7	11.0	.24	58	.133	<1	3.84	.013	.07	.2	.06	3.3	.2	<.05	10	.5
RE L1860 2300S	1.0	41.1	13.2	78	.2	13.3	11.0	900	2.41	4.4	1.0	2.1	3.5	7	.1	.2	.3	46	.10	.125	8	11.0	.25	66	.137	2	4.17	.015	.08	.2	.07	3.0	.2	<.05	11	.7
L1860 2325NW	.5	26.0	11.3	82	.1	13.4	12.0	1117	2.23	3.2	.5	1.4	2.7	11	.2	.2	.2	48	.13	.084	6	9.8	.22	87	.140	<1	3.18	.020	.06	.1	.03	2.3	.1	<.05	10	<.5
L1860 2350NW	.6	34.3	14.4	122	.1	20.7	16.4	1814	3.40	4.5	.4	1.9	2.4	11	.2	.3	.2	71	.17	.084	7	12.2	.43	87	.129	<1	3.00	.016	.08	.1	.04	2.6	.1	<.05	10	<.5
L1860 2375NW	.6	42.7	13.3	107	.2	16.5	19.3	1009	2.94	3.4	.5	5.2	2.7	7	.2	.2	.3	55	.12	.087	7	12.2	.26	90	.134	<1	3.05	.013	.09	.1	.05	2.6	.2	<.05	11	<.5
L1860 2400NW	.6	63.4	13.1	70	.1	14.7	13.5	316	2.90	3.7	.6	17.9	4.0	7	.1	.2	.3	62	.13	.053	11	9.1	.32	79	.105	<1	2.45	.014	.07	.2	.04	2.7	.1	<.05	8	<.5
L1860 2425NW	.7	92.0	12.3	54	.1	14.9	14.9	325	2.78	4.4	.9	15.5	4.9	8	.1	.2	.2	60	.12	.081	12	9.9	.35	74	.117	<1	3.41	.016	.07	.1	.04	3.6	.1	<.05	8	<.5
L1860 2450NW	.4	46.6	26.7	84	.2	11.4	10.6	1038	2.19	3.5	.3	4.4	2.8	13	.3	.4	.3	47	.20	.095	11	8.9	.23	111	.096	2	1.76	.016	.09	.1	.02	2.1	.1	<.05	7	<.5
L1860 2475NW	.7	73.2	11.3	72	.1	17.5	13.1	273	2.45	3.5	.6	5.3	3.9	9	.1	.2	.2	51	.14	.080	11	9.9	.31	100	.111	<1	2.57	.015	.11	.2	.02	2.8	.1	<.05	7	.5
L1860 2500NW	.8	96.0	12.1	81	.2	17.2	14.3	881	2.82	3.9	.5	9.6	3.5	9	.2	.2	.3	58	.09	.063	14	11.1	.29	100	.100	<1	2.39	.011	.06	.2	.03	2.0	.1	<.05	10	<.5
L1860 2525NW	.8	42.8	12.9	68	.1	16.0	10.8	451	2.53	4.8	.4	19.2	3.9	7	.1	.3	.3	49	.09	.061	15	10.2	.34	78	.087	<1	2.33	.012	.08	.2	.02	2.2	.1	<.05	8	<.5
L1860 2550NW	.8	25.5	17.5	59	.1	11.6	9.4	260	2.26	4.4	.9	3.5	4.6	9	.2	.2	.3	35	.10	.120	5	9.0	.13	53	.138	<1	4.47	.018	.04	.2	.04	1.6	.1	<.05	10	.5
L1860 2575NW	.8	13.4	14.8	76	.2	9.7	7.8	282	2.28	4.1	.6	4.0	3.9	12	.2	.2	.3	39	.12	.124	8	10.1	.17	81	.121	<1	3.51	.015	.06	.2	.04	1.7	.1	<.05	10	<.5
L1860 2600NW	.8	12.3	17.7	76	.1	9.0	7.1	295	1.96	3.0	.5	2.1	3.5	7	.1	.2	.3	32	.07	.112	8	9.6	.14	89	.109	<1	2.63	.013	.05	.1	.03	1.4	.1	<.05	9	<.5
L1860 2625NW	.9	11.5	14.9	53	.1	7.3	6.3	247	2.06	3.4	.5	1.5	2.9	5	.1	.2	.4	39	.06	.082	8	9.2	.14	56	.122	2	2.12	.015	.05	.2	.02	1.4	.1	.07	10	.5
L1860 2650NW	.7	13.9	11.8	56	.1	9.6	7.0	358	1.93	2.6	.4	5.2	3.4	7	.1	.1	.3	29	.09	.079	17	9.3	.25	71	.063	<1	1.51	.009	.05	.1	.03	1.3	.1	.06	7	<.5
L1860 2675NW	.8	13.8	14.2	61	.1	9.2	6.9	283	2.00	4.0	.5	8.1	3.7	6	.1	.2	.3	27	.06	.136	9	8.7	.16	56	.082	<1	2.37	.013	.05	.2	.04	1.2	.1	<.05	7	<.5
STANDARD DS5	11.7	142.9	24.5	128	.3	24.2	12.1	776	3.02	18.1	5.8	40.2	2.8	50	5.4	3.7	5.7	61	.75	.093	13	185.4	.65	130	.095	17	2.13	.033	.15	4.8	.18	3.4	1.0	<.05	7	5.1

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data A FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.6	2.2	2.2	44	<.1	3.9	4.2	582	2.01	.7	1.8	1.0	3.9	88	<.1	<.1	.1	44	.52	.084	12	14.1	.54	246	.115	<1	.89	.084	.47	2.3	<.01	2.1	.3	.10	5	<.5
L1860 2700NW	.7	14.0	11.8	66	.1	10.8	8.3	252	2.04	3.8	.6	17.7	4.3	6	.1	.2	.4	34	.08	.109	18	7.5	.26	74	.060	3	1.97	.009	.06	.2	.02	1.6	.1	.09	6	<.5
L1860 2825NW	.9	9.8	12.6	42	.1	12.8	9.7	310	2.39	4.0	.5	17.9	4.8	8	.1	.2	.4	35	.09	.044	20	10.4	.30	105	.058	6	2.30	.008	.08	.1	.03	1.6	.1	.06	7	<.5
L1860 2850NW	.9	11.6	16.2	50	.1	15.2	9.2	435	2.67	4.2	.5	9.5	4.9	7	.1	.3	.5	38	.12	.032	28	12.9	.40	92	.043	5	1.83	.006	.08	.1	.02	1.8	.1	.08	8	<.5
L1860 2875NW	1.9	37.2	42.8	84	.2	30.9	19.2	2642	3.14	8.0	3.3	15.6	6.1	28	.6	.4	.8	29	.40	.074	55	13.4	.51	126	.031	1	2.35	.010	.10	.1	.05	3.3	.1	.13	6	<.5
L1860 2900NW	1.2	23.0	28.5	61	.1	17.2	12.0	386	2.43	7.2	1.7	20.3	6.6	11	.1	.2	.6	25	.18	.022	36	10.7	.45	61	.015	<1	1.61	.005	.07	.1	.01	1.9	.1	<.05	5	<.5
L1860 2925NW	1.6	33.1	24.1	83	.1	26.6	13.7	257	3.29	6.4	1.6	27.6	7.2	11	.1	.3	.7	37	.15	.031	30	15.8	.51	68	.043	3	2.47	.008	.09	.1	.01	2.2	.1	<.05	6	<.5
L1860 2950NW	1.9	33.0	41.7	118	.1	20.9	22.3	2319	3.24	9.7	1.2	24.9	5.5	11	.6	.5	.9	35	.15	.074	31	13.5	.47	135	.059	8	1.83	.007	.09	.2	.06	1.6	.1	<.05	7	<.5
L1860 2975NW	1.7	27.0	22.8	82	.1	19.0	17.2	1039	3.37	8.5	1.1	9.3	6.5	11	.2	.3	.6	39	.14	.076	21	13.1	.43	144	.105	6	2.76	.011	.10	.2	.05	2.1	.1	<.05	10	<.5
L1860 3000NW	1.2	18.6	15.7	66	.1	16.5	14.0	877	2.83	6.7	.8	16.4	5.8	12	.1	.3	.6	35	.14	.046	24	11.5	.40	166	.071	3	2.12	.009	.08	.1	.05	1.9	.1	<.05	8	<.5
L1860 3025NW	1.2	18.0	20.2	101	.2	17.8	17.3	1259	2.94	5.0	.9	84.5	6.4	12	.3	.3	.6	39	.19	.070	23	13.4	.44	194	.087	4	2.73	.013	.13	.1	.05	2.6	.1	<.05	9	<.5
L1860 3050NW	1.3	11.3	14.4	69	.2	12.3	11.4	365	2.70	4.1	.6	25.9	4.0	18	.2	.2	.4	40	.27	.085	10	9.9	.18	160	.123	4	2.84	.022	.07	.2	.05	1.8	.1	<.05	11	<.5
L1860 3075NW	1.1	10.3	16.1	48	.2	11.6	11.1	1621	2.80	4.2	.6	112.1	5.1	10	.2	.2	.6	38	.18	.060	32	10.3	.38	140	.050	4	1.25	.007	.10	.1	.02	1.9	.1	<.05	7	<.5
L1860 3100NW	1.2	14.6	12.3	54	.1	22.4	19.6	503	3.13	4.7	1.0	93.5	5.9	8	<.1	.3	.5	43	.07	.078	15	14.1	.43	106	.093	<1	3.29	.011	.07	.2	.06	2.4	.1	<.05	10	<.5
L1860 3125NW	1.5	7.1	10.0	37	.1	17.1	32.9	1457	2.98	3.8	.7	7.8	4.8	9	.1	.2	.5	43	.12	.033	24	12.1	.49	154	.037	1	1.82	.006	.09	.1	.02	2.5	.1	<.05	7	<.5
L1860 3150NW	1.9	9.9	9.9	39	.1	21.4	27.0	248	3.61	5.2	.8	10.7	5.1	6	.1	.3	.6	54	.05	.048	20	12.3	.77	72	.046	<1	2.27	.006	.07	.1	.03	3.2	.1	<.05	8	<.5
L1860 3175NW	1.5	9.0	12.7	46	.1	13.5	19.1	330	2.95	3.5	.6	16.4	4.2	9	.1	.2	.5	48	.06	.052	15	13.0	.39	129	.092	4	2.12	.011	.06	.1	.04	2.3	.1	<.05	11	<.5
L1860 3200NW	1.5	11.1	11.4	42	.1	15.5	20.3	249	2.46	5.7	1.2	2.6	5.2	11	.1	.3	.3	34	.10	.225	7	9.7	.20	76	.132	1	4.28	.021	.05	.2	.09	2.2	.1	<.05	11	<.5
RE L1860 3200NW	1.5	10.5	11.5	39	<.1	14.7	19.6	233	2.28	4.9	1.2	2.9	5.5	10	.1	.3	.3	32	.09	.207	7	8.8	.19	70	.126	1	4.12	.019	.05	.3	.09	2.2	.1	<.05	10	<.5
L1860 3225NW	1.4	10.5	12.2	50	.1	15.1	19.1	674	2.69	6.3	1.2	3.9	6.5	8	.1	.3	.4	32	.07	.073	14	11.7	.35	122	.072	2	2.58	.010	.06	.2	.05	1.8	.1	<.05	8	<.5
L1860 3250NW	1.4	10.7	14.1	45	.1	11.1	11.2	182	2.45	6.5	1.3	3.2	5.0	13	.2	.4	.3	33	.14	.128	5	9.9	.16	86	.132	4	4.03	.018	.04	.2	.10	2.1	.1	<.05	11	.5
L1860 3275NW	1.3	6.5	12.7	28	.1	12.9	12.2	172	2.47	4.0	.6	1.4	4.0	9	.1	.2	.4	38	.08	.077	11	9.8	.18	89	.103	3	2.93	.016	.05	.2	.03	1.5	.1	<.05	12	<.5
L1860 3300NW	1.0	11.3	20.0	31	.1	18.2	14.9	453	2.37	4.7	3.2	1.5	7.7	21	.1	.2	.5	22	.17	.029	34	13.6	.35	101	.036	2	2.27	.009	.06	.1	.04	2.3	.1	<.05	8	.5
L1860 3325NW	.8	5.6	9.6	26	<.1	7.6	6.1	115	2.10	4.8	.6	<.5	4.5	6	.1	.2	.3	26	.06	.063	25	10.2	.26	67	.040	1	1.61	.007	.04	.1	.05	1.3	.1	<.05	6	<.5
L1860 3350NW	.4	5.3	9.5	22	.1	6.1	3.1	111	1.53	2.4	.4	<.5	3.5	5	<.1	.1	.3	22	.04	.036	26	6.6	.17	59	.037	5	1.02	.006	.04	.1	.02	1.1	.1	<.05	7	<.5
L1860 3375NW	.4	6.6	18.1	25	.1	6.8	4.3	525	1.19	2.2	.4	1.9	1.7	16	.2	.1	.4	16	.14	.022	26	7.3	.25	109	.020	1	1.01	.007	.08	.1	.02	.9	.1	<.05	5	<.5
L1860 3400NW	.4	6.8	9.3	34	<.1	8.2	5.4	154	1.65	2.5	.5	3.4	4.9	5	.1	.1	.3	17	.04	.021	33	8.5	.36	43	.027	<1	1.07	.004	.04	.1	<.01	.7	<.1	<.05	5	<.5
L1940 0S	.7	10.1	12.0	28	.1	6.3	3.0	58	1.71	4.3	.8	<.5	5.3	3	<.1	.2	.3	18	.01	.024	23	9.1	.21	26	.021	2	1.51	.003	.03	.1	.04	1.4	.1	<.05	5	<.5
L1940 25S	.6	4.5	11.3	12	.1	2.7	1.0	35	2.03	3.0	.4	<.5	3.1	3	<.1	.2	.4	24	.02	.021	20	6.4	.08	19	.045	<1	.96	.006	.03	.1	.03	.7	.1	<.05	7	.5
L1940 50S	.8	9.7	10.3	21	.1	3.9	2.0	52	2.18	3.7	.9	<.5	4.7	5	.1	.2	.2	32	.05	.054	10	10.2	.10	27	.076	<1	3.90	.013	.03	.2	.06	1.8	.1	<.05	8	<.5
L1940 75S	.6	6.3	9.8	22	.1	3.7	1.7	45	1.98	3.6	.5	<.5	3.1	3	.1	.3	.4	25	.03	.026	22	8.3	.13	27	.032	2	1.11	.004	.04	.1	.03	.9	.1	<.05	7	<.5
L1940 100S	.4	6.1	9.0	42	.1	8.7	4.4	120	1.68	3.4	.7	<.5	5.7	3	.1	.1	.2	19	.02	.026	21	9.8	.28	31	.021	4	1.55	.002	.04	.1	.03	1.0	.1	<.05	4	<.5
L1940 125S	.6	8.0	10.2	26	.1	5.3	2.9	112	1.65	3.3	.7	<.5	4.1	4	<.1	.2	.3	23	.03	.047	15	7.2	.17	35	.050	5	1.99	.009	.04	.1	.04	1.0	.1	<.05	8	<.5
L1940 150S	1.0	6.1	8.2	24	.1	5.3	3.0	63	1.57	3.6	.7	<.5	4.7	3	<.1	.2	.4	25	.02	.025	24	8.0	.17	31	.031	<1	1.44	.005	.03	.1	.03	1.1	.1	<.05	6	<.5
L1940 175S	.6	7.0	8.1	24	<.1	6.7	2.9	60	1.78	4.6	.8	<.5	5.5	2	<.1	.2	.3	19	.02	.026	25	9.5	.26	26	.026	2	1.24	.003	.03	.1	.03	1.2	.1	<.05	5	<.5
STANDARD DS5	13.1	143.0	25.6	141	.3	24.6	13.1	775	3.15	19.2	5.9	42.0	3.1	50	5.6	3.8	6.3	65	.78	.104	16	184.5	.70	143	.098	18	2.03	.034	.15	4.7	.19	3.6	1.1	<.05	7	4.8

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data A FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.5	2.5	2.7	46	<.1	4.6	4.7	572	1.98	.8	1.8	1.2	4.5	104	<.1	<.1	.1	47	.59	.082	9	14.4	.52	234	.128	<1	.96	.096	.52	2.0	<.01	2.6	.3	.17	5	.5
L1940 200S	.8	12.8	10.7	30	.1	6.4	3.6	73	2.19	3.7	.9	2.7	5.3	5	.1	.2	.3	35	.04	.073	7	10.8	.13	35	.064	<1	2.75	.010	.05	.1	.05	1.9	.1	.17	8	<.5
L1940 225S	1.1	11.6	11.2	35	.1	6.7	4.5	129	2.50	4.9	.9	1.8	6.2	4	.1	.3	.4	40	.03	.064	9	11.9	.18	36	.082	2	2.88	.009	.04	.2	.05	1.7	.1	.08	9	.6
L1940 250S	2.0	8.0	13.4	38	.1	7.1	4.5	141	4.86	6.8	.7	2.6	5.9	4	.1	.5	.6	57	.03	.079	10	17.7	.18	45	.093	<1	2.41	.007	.05	.2	.07	1.5	.1	.09	14	.6
L1940 275S	2.1	11.3	8.7	20	.1	7.6	3.6	69	3.32	5.7	.7	4.1	7.2	3	<.1	.4	.5	32	.02	.052	16	15.1	.31	30	.022	2	2.02	.004	.03	.1	.04	1.4	.1	.08	8	<.5
L1940 300S	3.0	19.6	12.0	38	.1	11.6	7.1	131	2.89	4.8	.8	1.5	5.4	8	.1	.4	.4	39	.04	.049	13	14.3	.31	47	.042	1	2.21	.006	.03	.1	.03	1.7	.1	<.05	8	<.5
L1940 325S	1.3	12.9	10.3	37	<.1	17.7	14.4	150	2.85	6.5	.8	1.2	6.2	6	.1	.3	.4	35	.04	.044	15	15.6	.53	57	.030	1	2.20	.004	.04	.2	.03	1.9	.1	.10	6	1.0
L1940 350S	1.6	10.7	13.1	33	<.1	11.6	7.9	226	2.90	5.6	1.0	.5	6.0	7	.1	.3	.4	38	.06	.062	7	12.3	.20	64	.093	<1	3.67	.010	.04	.2	.08	2.1	.1	.07	11	.5
L1940 375S	1.2	10.3	12.4	40	.1	12.0	6.5	482	3.16	4.1	.5	<.5	4.8	12	.1	.3	.5	48	.10	.061	14	21.2	.29	73	.088	1	2.14	.008	.06	.2	.05	2.0	.1	.08	10	.5
L1940 400S	1.5	16.1	14.6	44	.1	14.8	12.5	424	2.70	6.9	1.1	1.5	5.8	6	.2	.3	.5	35	.04	.063	11	13.7	.33	65	.078	4	2.95	.009	.05	.2	.06	2.1	.1	<.05	9	.6
L1940 425S	1.3	13.4	14.2	44	<.1	11.7	9.4	346	3.01	5.8	.8	1.1	5.3	8	.1	.3	.4	41	.06	.076	8	12.9	.21	80	.098	<1	3.18	.010	.06	.2	.05	1.9	.1	.08	11	.5
L1940 450S	1.2	16.9	12.2	38	.1	12.9	10.6	215	2.55	5.5	1.0	1.3	5.3	7	.1	.3	.3	37	.06	.063	8	12.6	.28	62	.104	<1	3.53	.011	.05	.2	.08	2.2	.1	.09	9	.6
L1940 475S	1.2	12.7	13.9	43	.1	12.3	10.3	349	2.91	5.9	.5	1.9	4.4	7	.1	.4	.4	37	.05	.049	12	13.1	.29	65	.077	<1	2.48	.009	.05	.2	.05	1.6	.1	.07	10	<.5
L1940 500S	2.3	19.9	24.9	54	.1	28.2	25.6	384	3.29	6.2	.9	<.5	5.1	12	.1	.4	.6	44	.09	.043	12	18.3	.29	62	.109	4	2.18	.009	.09	.2	.04	2.1	.1	<.05	11	.7
L1940 525S	1.4	11.7	12.9	40	<.1	12.8	11.4	674	2.30	4.9	.6	<.5	4.1	7	.1	.3	.4	32	.06	.026	16	12.4	.24	88	.057	3	1.61	.008	.06	.1	.03	1.2	.1	<.05	7	<.5
L1940 550S	1.4	10.5	18.9	45	<.1	10.5	7.6	582	2.16	6.8	.6	<.5	4.4	7	.1	.3	.4	30	.06	.035	13	11.3	.21	82	.042	2	1.66	.007	.06	.1	.03	1.3	.1	.06	7	<.5
L1940 575S	1.1	9.7	23.5	46	.1	8.5	6.0	643	1.60	4.6	.5	1.3	3.1	14	.2	.3	.4	23	.14	.046	9	7.9	.14	82	.064	5	1.55	.010	.07	.1	.03	1.3	.1	<.05	6	<.5
L1940 600S	.9	9.4	13.8	40	.1	8.7	5.0	244	1.93	3.9	.5	1.3	3.7	12	.1	.2	.4	30	.05	.037	12	10.5	.17	94	.059	1	1.54	.008	.05	.1	.03	1.3	.1	<.05	7	<.5
L1940 625S	1.4	12.0	14.2	46	.1	8.7	7.2	166	2.13	4.7	1.0	1.1	5.7	7	.1	.3	.3	29	.05	.066	10	11.3	.19	76	.064	1	2.90	.010	.05	.2	.05	1.7	.1	<.05	8	.7
L1940 650S	1.1	10.1	17.9	57	.1	8.8	6.7	773	1.93	4.4	.7	1.9	3.8	12	.2	.3	.3	29	.10	.080	8	9.6	.14	96	.087	2	2.55	.012	.05	.1	.04	1.5	.1	<.05	7	<.5
L1940 675S	1.3	11.6	16.7	59	.1	10.5	7.5	255	2.05	5.1	.9	1.4	4.2	9	.2	.3	.3	30	.08	.107	5	8.9	.12	81	.120	4	3.77	.015	.04	.2	.07	2.1	.1	<.05	10	.7
L1940 700S	2.0	11.1	20.7	68	.1	10.4	7.8	392	2.49	8.1	.6	1.5	4.4	8	.1	.3	.4	33	.08	.063	8	11.9	.17	73	.103	4	2.44	.012	.07	.1	.05	1.6	.1	<.05	10	<.5
RE L1940 700S	1.8	10.9	19.1	68	.1	10.6	7.0	404	2.39	7.9	.6	1.1	4.2	9	.2	.3	.4	34	.10	.067	8	11.7	.17	72	.105	<1	2.51	.012	.07	.2	.07	1.8	.1	.06	9	.5
L1940 725S	1.6	17.7	20.3	63	.1	12.1	8.4	181	2.37	5.3	.9	1.8	5.5	6	.1	.3	.4	35	.05	.041	11	11.8	.21	110	.096	3	2.54	.010	.07	.2	.05	1.9	.1	<.05	9	.6
L1940 750S	.8	74.6	15.4	56	.1	15.5	13.5	499	2.84	5.7	.9	<.5	5.4	10	.1	.3	.4	52	.10	.070	16	11.8	.50	94	.059	<1	1.88	.005	.08	.1	.02	3.1	.1	<.05	8	.8
L1940 775S	2.1	17.1	17.9	41	.1	15.8	16.8	315	3.30	7.2	.7	2.2	4.3	12	.2	.3	.7	41	.08	.047	14	14.0	.35	88	.070	1	2.31	.008	.06	.1	.04	1.7	.1	.06	10	<.5
L1940 800S	1.1	14.1	19.3	41	.3	11.7	14.5	618	2.39	4.9	1.6	.8	2.6	35	.4	.2	.5	28	.30	.053	15	11.9	.29	126	.061	3	1.84	.009	.08	.1	.05	1.6	.1	<.05	8	<.5
L1940 825S	.9	13.2	31.0	58	.1	15.7	13.9	912	2.13	3.8	1.6	2.4	3.3	20	.4	.2	.5	27	.18	.065	20	12.3	.37	134	.055	1	2.24	.007	.09	.1	.04	1.8	.1	.07	7	.7
L1940 850S	.9	12.3	12.5	56	.1	9.9	6.4	311	2.97	4.0	1.0	2.3	6.7	5	.1	.2	.5	39	.03	.058	20	15.3	.32	67	.060	2	1.99	.005	.06	.1	.04	1.9	.1	.07	9	.6
L1940 875S	1.0	11.8	13.8	53	.1	9.6	6.7	406	2.69	5.5	.9	2.0	5.2	4	.1	.3	.4	28	.04	.056	17	12.3	.30	60	.036	<1	1.71	.004	.05	.1	.04	1.8	.1	<.05	7	.5
L1940 900S	1.4	16.4	24.8	64	.2	18.3	14.0	169	3.36	5.6	1.4	2.5	7.7	7	.2	.2	.6	39	.06	.051	13	17.3	.38	92	.080	<1	3.50	.009	.08	.1	.07	2.3	.1	.08	12	.5
L1940 925S	1.6	24.4	21.5	62	.1	17.5	14.3	280	3.35	5.7	2.0	3.5	8.9	5	.2	.4	.5	32	.04	.063	18	15.1	.42	52	.071	1	2.64	.005	.06	.1	.08	2.5	.1	.08	9	.8
L1940 950S	.9	15.6	15.0	61	.2	13.0	9.4	199	2.66	4.9	1.0	4.6	7.1	6	.1	.3	.4	32	.05	.046	14	14.8	.32	77	.072	<1	2.66	.007	.07	.1	.06	2.1	.1	.09	9	.8
L1940 975S	.8	5.7	9.7	25	.1	6.1	3.6	86	1.59	2.7	.5	4.1	3.6	4	.1	.1	.3	26	.03	.020	16	9.0	.18	42	.031	1	1.05	.006	.05	.1	.01	1.0	.1	<.05	6	<.5
L1940 1000S	1.1	9.5	13.4	31	.1	7.3	3.6	104	2.05	4.4	.7	4.8	4.4	8	.1	.2	.4	31	.06	.046	9	10.6	.14	60	.064	<1	2.45	.010	.05	.1	.04	1.7	.1	.07	8	<.5
STANDARD DS5	13.1	139.6	26.0	137	.3	24.0	12.7	778	3.03	19.2	6.0	43.0	2.8	52	5.7	4.1	6.3	62	.79	.101	12	188.9	.68	145	.097	17	1.99	.034	.15	4.7	.18	3.7	1.0	.06	6	5.1

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data A FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.6	2.5	2.2	41	<.1	4.5	4.2	557	1.96	.6	1.8	<.5	4.1	93	<.1	<.1	.1	51	.64	.081	9	13.2	.51	256	.139	2	.95	.090	.43	2.2	<.01	2.5	.3	.14	5	<.5
L1940 1025S	1.3	11.5	14.6	42	.1	9.4	6.5	153	1.99	4.3	.9	2.6	5.0	7	.1	.3	.3	36	.06	.064	7	8.9	.17	69	.087	<1	2.93	.011	.05	.2	.04	1.6	.1	.06	10	<.5
L1940 1050S	1.4	12.8	15.4	49	.1	9.9	7.0	257	2.45	5.1	.7	2.6	4.4	6	.1	.2	.4	41	.05	.059	9	9.2	.21	73	.099	<1	2.58	.012	.05	.2	.06	1.6	.1	.11	10	<.5
L1940 1075S	1.4	15.2	15.4	60	.2	7.6	4.9	214	2.33	5.5	.9	2.6	4.2	14	.2	.3	.4	43	.16	.099	7	10.1	.16	76	.119	2	2.93	.014	.06	.3	.08	1.5	.1	.12	10	<.5
L1940 1100S	.8	12.6	12.8	49	.1	9.5	5.2	134	2.25	4.6	.7	2.5	5.6	5	.1	.2	.3	38	.04	.084	12	11.2	.25	66	.060	<1	2.61	.010	.04	.1	.05	1.9	.1	<.05	8	<.5
L1940 1125S	.9	17.8	9.8	45	<.1	12.9	6.9	180	2.25	5.7	.8	2.9	5.9	4	.1	.3	.3	31	.03	.058	16	13.3	.38	57	.024	1	2.23	.004	.03	.1	.03	1.7	.1	<.05	5	<.5
L1940 1150S	1.0	9.1	10.8	32	<.1	7.3	4.0	184	2.11	4.4	.4	2.2	4.6	5	.1	.2	.4	34	.04	.030	20	10.0	.21	58	.044	1	1.71	.006	.05	.2	.04	1.4	.1	<.05	8	<.5
L1940 1175S	1.1	15.9	13.4	52	.1	11.0	6.6	283	2.38	4.4	.6	3.4	4.6	6	.1	.2	.4	39	.05	.069	11	11.8	.23	91	.098	1	2.83	.010	.06	.2	.03	2.1	.1	<.05	10	<.5
L1940 1200S	.9	13.5	11.9	39	.1	9.2	5.9	364	1.93	3.9	.6	2.4	3.8	5	.1	.2	.4	36	.04	.059	10	8.8	.17	66	.087	<1	2.36	.011	.04	.1	.06	1.4	.1	.06	9	<.5
L1940 1225S	1.0	18.3	13.3	53	.1	10.3	8.0	449	2.45	5.1	.7	3.5	5.0	5	.1	.2	.5	42	.04	.076	11	11.3	.19	75	.098	<1	2.69	.011	.06	.1	.05	1.9	.1	.06	9	.5
L1940 1250S	1.4	18.9	12.9	44	.1	14.3	10.5	272	2.96	9.8	1.0	28.5	7.1	5	.1	.5	.6	35	.04	.049	20	10.8	.35	71	.046	<1	2.07	.004	.04	.2	.04	1.8	.1	<.05	8	<.5
L1940 1275S	1.2	20.8	11.9	40	.1	15.9	12.0	209	2.81	7.4	1.1	45.4	8.0	5	.1	.3	.5	30	.03	.049	20	11.7	.33	65	.039	<1	2.08	.004	.04	.1	.04	1.4	.1	<.05	5	<.5
L1940 1300S	1.0	10.7	12.3	45	.1	10.7	9.9	578	2.74	6.3	.6	18.5	5.3	5	.1	.3	.5	35	.05	.037	19	10.5	.20	67	.059	3	1.60	.006	.04	.1	.06	1.4	.1	<.05	8	<.5
L1940 1325S	1.1	12.1	12.6	42	.1	12.7	10.0	385	2.76	5.3	.6	67.4	6.3	7	.1	.2	.5	40	.07	.052	18	12.1	.19	105	.075	1	2.20	.008	.05	.2	.04	1.6	.1	<.05	8	<.5
L1940 1350S	1.1	9.1	13.5	40	.2	10.4	7.1	336	2.80	4.6	.6	8.8	5.6	5	.1	.3	.5	38	.05	.053	18	11.9	.19	72	.065	<1	1.74	.007	.05	.2	.06	1.3	.1	<.05	9	<.5
L1940 1375S	.8	10.5	14.8	51	.1	11.3	8.3	410	2.24	6.7	.6	191.2	5.6	7	.2	.3	.5	27	.05	.048	21	9.3	.23	67	.055	<1	1.80	.007	.04	.1	.03	1.2	.1	<.05	7	<.5
L1940 1400S	1.6	11.9	20.0	53	.1	15.7	13.7	341	3.12	8.3	1.1	80.9	7.3	5	.1	.3	.7	36	.05	.059	19	11.4	.25	102	.083	3	2.27	.008	.06	.2	.04	1.9	.1	<.05	9	<.5
L1940 1425S	.9	23.7	21.6	83	.1	15.7	9.4	1138	2.52	5.2	1.0	37.4	6.7	4	.1	.3	.5	26	.04	.046	19	15.1	.53	87	.057	1	2.11	.005	.03	.1	.03	1.8	.1	.06	6	<.5
L1940 1450S	1.5	18.9	34.3	107	.3	13.8	15.9	2206	2.71	5.6	.6	13.3	2.2	12	.4	.5	.5	34	.11	.061	15	10.3	.22	88	.083	<1	1.65	.008	.07	.1	.06	1.2	.2	<.05	8	<.5
L1940 1475S	1.7	20.3	41.3	118	.2	13.4	15.7	3448	2.75	4.8	.6	3.8	3.2	14	.4	.5	.6	41	.19	.059	14	14.3	.30	136	.101	2	1.76	.014	.08	.1	.07	1.6	.2	<.05	9	<.5
L1940 1500S	.8	14.4	21.2	130	.1	12.3	10.5	2930	2.16	3.3	.5	4.2	3.1	11	.5	.2	.4	37	.12	.072	9	9.6	.15	132	.121	<1	2.36	.015	.05	.2	.04	1.5	.2	<.05	10	<.5
RE L1940 1500S	.8	13.9	21.8	127	.2	11.2	10.2	3062	2.00	3.1	.6	2.5	3.1	11	.5	.3	.4	32	.11	.071	10	9.0	.15	146	.116	2	2.27	.013	.05	.1	.05	1.3	.2	<.05	9	<.5
L1940 1525NW	.7	12.5	20.4	97	.2	9.8	8.8	772	2.25	4.2	.6	1.3	2.6	7	.2	.3	.4	38	.07	.073	7	9.9	.14	74	.124	1	2.38	.011	.06	.1	.05	1.5	.1	<.05	10	<.5
L1940 1550NW	1.1	32.6	36.1	121	.4	21.7	12.8	1295	2.38	4.6	1.2	16.2	5.3	9	.4	.3	.4	31	.10	.085	13	12.4	.28	99	.108	<1	3.10	.010	.07	.2	.07	2.1	.1	<.05	8	<.5
L1940 1575NW	1.2	15.7	23.9	134	.4	15.0	9.9	1702	2.68	4.4	.8	2.5	3.9	8	.2	.3	.5	35	.07	.087	12	12.5	.24	103	.105	4	2.57	.009	.08	.2	.05	1.3	.2	<.05	9	<.5
L1940 1600NW	1.1	18.2	23.6	127	.1	17.1	14.8	1960	2.46	4.5	.7	3.2	3.3	19	.3	.3	.5	31	.19	.089	15	12.6	.32	119	.078	6	2.38	.007	.12	.2	.05	1.4	.2	<.05	8	<.5
L1940 1625NW	1.2	18.1	19.9	90	.2	16.6	11.4	693	2.37	5.0	.9	4.7	5.2	8	.2	.2	.5	31	.06	.067	12	11.9	.25	121	.104	1	3.18	.010	.06	.1	.06	1.8	.2	<.05	8	.5
L1940 1650NW	.9	18.9	23.2	118	.1	22.8	13.3	1472	2.52	4.9	.8	2.4	4.8	23	.4	.3	.4	33	.26	.090	13	12.6	.30	159	.127	4	3.15	.014	.10	.2	.03	1.8	.2	<.05	9	.5
L1940 1675NW	.7	19.7	20.8	113	.1	22.8	12.2	294	2.44	2.9	.6	10.1	5.8	10	.1	.2	.4	25	.10	.045	19	14.4	.44	92	.079	<1	2.11	.007	.09	.1	.01	1.5	.2	<.05	7	<.5
L1940 1700NW	1.1	25.7	25.4	155	.1	25.2	17.8	3983	2.77	3.8	.8	13.8	3.4	17	.4	.3	.5	34	.19	.084	18	13.0	.36	246	.094	4	2.74	.012	.12	.1	.06	1.7	.2	.08	9	.6
L1940 1725NW	1.2	20.5	40.2	180	.2	24.4	18.6	3418	2.63	5.3	1.0	3.6	4.0	18	.6	.5	.5	36	.22	.119	13	13.4	.28	163	.124	7	2.85	.012	.10	.1	.06	1.7	.2	<.05	10	<.5
L1940 1750NW	1.4	12.2	21.2	194	.1	21.7	13.6	1229	2.49	3.1	.7	1.9	3.3	15	.3	.3	.5	35	.19	.072	11	12.5	.27	157	.122	1	3.20	.013	.08	.1	.07	1.4	.2	.08	10	<.5
L1940 1775NW	1.3	17.4	29.7	139	.2	20.4	15.3	1348	2.47	3.4	.9	1.8	4.1	20	.5	.2	.5	33	.18	.066	14	11.7	.31	188	.108	3	2.56	.011	.09	.1	.06	1.8	.2	<.05	8	<.5
L1940 1800NW	1.4	17.2	22.0	133	.2	21.4	14.2	542	2.49	4.6	1.0	3.4	5.4	8	.1	.3	.5	30	.07	.068	13	11.4	.30	108	.118	<1	3.34	.011	.06	.2	.07	1.7	.1	<.05	9	<.5
L1940 1825NW	1.1	14.5	20.3	143	.1	20.6	13.7	259	3.12	4.9	.8	3.2	5.2	7	.1	.3	.5	36	.10	.089	14	13.6	.33	81	.107	<1	2.73	.009	.07	.2	.04	1.4	.1	<.05	10	<.5
STANDARD DS5	12.4	139.4	24.3	131	.3	23.2	11.9	770	2.88	18.0	6.1	43.1	2.8	52	5.7	4.0	6.3	61	.75	.099	12	179.2	.68	137	.101	16	2.07	.034	.14	4.6	.17	3.2	1.0	<.05	7	4.7

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data A FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.6	2.7	2.1	42	<.1	4.6	4.1	563	2.00	<.5	1.8	<.5	4.2	87	<.1	<.1	.1	39	.54	.074	10	15.3	.51	251	.126	1	.93	.090	.45	2.3	<.01	2.3	.3	<.05	4	<.5
L1940 1850NW	1.3	6.8	17.6	54	.1	7.8	4.7	143	2.01	2.6	.4	3.5	3.5	6	.1	.2	.4	31	.08	.024	13	8.6	.15	63	.060	1	1.39	.008	.05	.1	.02	1.1	.1	<.05	8	<.5
L1940 1875NW	1.0	11.0	11.2	81	.2	9.3	8.0	845	1.95	3.0	.8	2.4	4.0	6	.2	.1	.3	30	.05	.178	8	9.9	.16	105	.112	2	3.03	.019	.05	.2	.05	2.3	.1	<.05	9	<.5
L1940 1900NW	1.2	8.2	12.8	59	.1	9.3	5.6	388	2.29	3.3	.4	41.0	3.8	8	.1	.2	.5	36	.06	.045	16	11.7	.23	87	.099	2	1.36	.010	.06	.2	.04	1.6	.1	<.05	10	<.5
L1940 1925NW	1.5	5.4	9.8	29	.1	5.9	3.9	119	1.81	2.1	.3	3.0	3.8	7	.1	.2	.4	27	.09	.025	19	8.4	.18	50	.026	<1	1.16	.006	.04	.1	.02	1.1	.1	<.05	6	<.5
L1940 1950NW	.6	12.9	10.1	37	<.1	11.7	6.8	161	2.00	3.8	.9	18.6	7.2	3	<.1	.2	.3	11	.02	.028	21	8.9	.34	54	.020	1	1.24	.003	.04	.1	.02	1.1	<.1	<.05	4	<.5
L1940 1975NW	1.3	12.7	14.2	55	.1	11.9	8.3	492	2.51	4.6	.7	8.2	4.6	6	.1	.3	.4	28	.07	.041	18	11.4	.29	82	.064	<1	1.99	.009	.06	.1	.03	1.5	.1	<.05	9	<.5
L1940 2000NW	1.4	12.5	11.4	45	.1	13.2	7.6	166	2.18	5.2	.8	8.7	5.8	5	.1	.2	.3	25	.04	.069	13	10.5	.26	74	.079	1	3.16	.010	.05	.2	.05	1.9	.1	<.05	7	<.5
L1940 2025NW	1.0	14.3	10.7	47	.1	14.0	10.8	292	2.29	4.4	.9	4.8	6.5	5	.1	.2	.3	21	.04	.059	15	10.0	.31	90	.051	<1	2.72	.009	.04	.2	.04	2.0	.1	<.05	7	<.5
L1940 2050NW	.7	9.9	9.6	41	<.1	15.2	11.8	281	1.55	1.8	.8	42.2	4.8	8	<.1	.1	.3	14	.05	.016	21	8.7	.32	66	.023	<1	1.24	.007	.04	.1	.01	1.0	<.1	<.05	4	<.5
L1940 2075NW	.9	12.2	9.5	38	.1	11.4	9.1	112	1.89	3.8	.7	1.3	4.6	5	.1	.2	.3	21	.04	.051	10	9.1	.21	95	.071	1	2.50	.012	.04	.2	.05	1.8	.1	<.05	7	<.5
L1940 2100NW	1.0	10.0	12.7	35	.1	8.1	6.0	208	2.23	5.2	.7	6.6	4.7	6	.1	.2	.4	30	.04	.065	9	9.9	.15	75	.081	1	2.73	.012	.04	.1	.05	1.7	.1	<.05	9	<.5
RE L1940 2100NW	1.0	9.6	12.6	34	.1	7.8	5.8	192	2.11	5.2	.6	3.2	4.6	6	.1	.3	.3	29	.04	.071	9	9.9	.16	74	.083	1	2.84	.013	.05	.2	.05	1.8	.1	<.05	9	<.5
L1940 2125NW	1.2	15.4	11.7	34	.1	7.1	4.8	195	2.23	4.4	1.2	2.0	3.9	6	.1	.3	.3	35	.05	.119	4	9.0	.10	62	.148	2	4.38	.017	.03	.2	.06	2.7	<.1	<.05	11	<.5
L1940 2150NW	.4	7.4	7.4	47	<.1	8.7	5.6	106	1.51	1.6	.6	1.4	5.6	2	<.1	.1	.2	13	.02	.029	22	9.1	.31	53	.015	<1	1.37	.003	.04	.1	.02	1.2	<.1	<.05	3	<.5
L1940 2175NW	.8	9.5	11.3	38	.1	6.4	4.0	188	1.84	2.7	.5	5.5	3.5	5	.1	.2	.3	31	.04	.057	11	8.2	.11	89	.045	1	1.97	.011	.04	.1	.03	1.6	.1	<.05	8	<.5
L1940 2200NW	.9	9.3	11.1	42	.1	8.5	4.7	112	3.00	4.3	.7	1.7	5.4	3	.1	.2	.3	28	.03	.076	14	12.5	.22	44	.049	<1	2.14	.007	.04	.2	.04	1.6	.1	<.05	8	<.5
L1940 2225NW	1.2	8.9	18.8	38	.2	8.1	4.2	118	2.38	4.2	.8	2.6	4.5	7	.1	.2	.4	37	.06	.064	9	10.9	.16	83	.080	<1	2.47	.010	.05	.2	.07	2.0	.1	<.05	11	<.5
L1940 2250NW	.5	5.5	14.1	35	<.1	7.7	5.6	152	1.35	1.6	.4	3.7	3.6	7	<.1	.1	.3	17	.07	.015	19	9.4	.26	70	.023	<1	1.06	.006	.04	.1	.01	1.1	.1	<.05	4	<.5
L1940 2275NW	.7	8.7	14.3	53	.1	10.6	6.7	274	2.34	3.1	.6	.7	4.7	8	.1	.1	.4	29	.07	.039	19	13.2	.30	96	.043	<1	1.53	.006	.06	.1	.01	1.3	.1	<.05	7	<.5
L1940 2300NW	.8	8.3	14.0	49	.1	9.8	5.3	134	2.44	4.1	.7	3.6	4.8	7	.1	.2	.3	26	.05	.042	22	12.3	.32	71	.029	<1	1.62	.004	.05	.1	.02	1.4	.1	.06	7	<.5
L1940 2325NW	.4	7.9	12.0	37	.1	8.6	5.4	119	1.57	1.7	.6	1.0	4.0	7	.1	.1	.3	19	.05	.016	23	10.7	.31	68	.023	<1	1.14	.006	.04	.1	.01	1.2	.1	<.05	5	<.5
STANDARD DS5	13.1	142.0	24.7	140	.3	24.7	11.7	795	3.02	18.8	6.2	44.3	2.7	51	6.1	3.8	6.0	61	.72	.093	13	177.5	.65	147	.097	16	2.09	.034	.13	5.0	.17	3.7	1.0	<.05	7	5.1

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data A FA ___

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Ruby Red Resources Inc. PROJECT EDDY/LOOSE LEG File # A303291

207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6 Submitted by: Peter Klewchuk

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
SI	<1	<1	3	<1	<.3	3	<1	<2	.06	<2	<8	<2	<2	2	<.5	<3	<3	<1	.10	<.001	<1	1	.01	2	<.01	<3	<.01	.46	<.01	<2	<.2
E-1	1	11821	14	27	6.6	25	30	113	3.88	19	<8	<2	<2	2	.7	4	<3	30	.02	.002	1	3	.71	4	<.01	<3	.59	.02	<.01	2	32.0
E-2	2	280	21	46	.3	15	12	1555	8.05	25	<8	<2	8	11	1.0	4	3	49	.02	.099	21	13	.13	67	<.01	<3	.87	.01	.17	<2	1.5
E-3	<1	188	7	7	.7	7	5	70	1.11	26	<8	<2	<2	39	<.5	<3	<3	35	.97	.015	1	9	.04	9	.11	<3	.78	<.01	.01	<2	2.0
E-4	1	6	7	10	<.3	9	3	46	1.89	4	<8	<2	8	2	<.5	<3	<3	9	.03	.018	24	9	.49	13	<.01	<3	.90	.02	.05	<2	.2
E-5	<1	13	<3	11	<.3	7	4	116	1.60	<2	<8	<2	8	1	<.5	<3	<3	2	.02	.015	26	3	.04	16	<.01	<3	.28	.02	.07	<2	267.8
E-6	<1	58	8	10	<.3	8	21	35	2.06	4	<8	<2	8	1	<.5	3	3	2	.01	.023	85	4	.03	19	<.01	<3	.40	.02	.05	29	1490.2
E-7	1	6	5	2	<.3	7	8	23	2.05	5	<8	<2	2	3	<.5	<3	<3	3	<.01	.033	42	4	<.01	12	<.01	<3	.11	<.01	.07	3	19.9
E-8	2	3	15	14	<.3	7	10	40	4.31	12	<8	<2	7	1	<.5	<3	4	9	<.01	.073	24	3	.01	18	<.01	<3	.22	.01	.12	<2	10.1

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Ruby Red Resources Inc. PROJECT LOOSE LEG File # A303665

207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6 Submitted by: Peter Klewchuk

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
E-9	3	10	42	19	<.3	14	16	709	8.01	26	<8	<2	4	7	<.5	3	5	13	.04	.025	31	11	.66	14	<.01	<3	.90	.01	.06	2	<.2
E-10	1	2	6	21	<.3	15	9	124	3.61	<2	<8	<2	4	3	<.5	<3	<3	13	.02	.026	4	13	1.25	16	<.01	<3	1.40	<.01	.08	<2	<.2
E-11	<1	2	6	6	<.3	3	4	32	7.49	5	<8	<2	2	3	<.5	<3	3	19	.01	.025	5	11	.28	36	<.01	<3	.55	.01	.07	<2	2.3
E-12	14	6	12	34	<.3	16	12	1527	6.86	<2	<8	<2	6	5	<.5	<3	<3	11	.02	.123	7	13	.93	58	<.01	<3	1.32	.01	.11	<2	<.2
E-13	1	4	6	13	<.3	8	13	84	4.61	<2	<8	<2	8	4	<.5	<3	<3	7	.01	.037	5	11	.40	36	<.01	<3	.73	.01	.13	<2	<.2
E-14	1	4	20	14	<.3	4	5	166	7.22	<2	<8	<2	7	2	<.5	<3	4	9	.01	.034	10	11	.22	32	<.01	<3	.67	.01	.12	<2	4.4
STANDARD DS5/AU-R	12	137	24	131	.3	24	12	735	2.85	17	<8	<2	3	47	5.4	4	6	58	.71	.092	12	182	.65	137	.10	17	2.01	.03	.13	3	466.0

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK R150 60C AU* IGNITED, ACID LEACHED, ANALYZED BY ICP-MS. (15 gm)

DATE RECEIVED: AUG 25 2003 DATE REPORT MAILED: Sept 9/03 SIGNED BY. . . . . D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ACME ANALYTICAL LABORATORIES LTD. (ISO 9002 Accredited Co.) 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Ruby Red Resources Inc. PROJECT EDDY File # A304921 Page 1

207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6 Submitted by: Peter Klewchuk

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
SI	<1	2	3	2	<.3	<1	<1	9	.10	<2	<8	<2	<2	6	<.5	<3	<3	<1	.11	<.001	<1	2	<.01	112	<.01	<3	.01	.50	<.01	<2	.2
ET-1	51	192	1837	296	11.0	23	16	21	14.92	1938	<8	30	<2	2	1.1	<3	<3	3	.01	.043	2	13	.01	17	<.01	<3	.09	<.01	.04	<2	27000.0
ET-2	72	219	5046	543	23.2	22	14	127	15.98	3098	<8	77	3	3	9.3	<3	8	6	.02	.063	5	8	.03	22	<.01	<3	.21	<.01	.06	<2	57000.0
ET-3	15	460	1082	402	1.9	15	20	320	5.97	698	<8	8	<2	1	6.6	<3	<3	9	.01	.033	4	13	.04	15	<.01	<3	.23	<.01	.05	<2	6574.9
ET-4	6	77	660	235	.6	14	18	1003	3.72	86	<8	2	2	3	5.3	<3	<3	14	.02	.046	9	8	.09	30	.01	<3	.42	.01	.15	<2	858.2
ET-5	11	141	4876	804	1.2	15	13	363	6.00	220	<8	4	5	6	4.7	<3	<3	11	.05	.091	21	8	.15	21	.01	<3	.87	.02	.20	<2	2842.1
ET-6	206	225	6731	809	14.9	22	13	95	15.07	1805	<8	30	6	5	8.9	13	6	9	.04	.092	14	10	.11	23	.01	<3	.75	<.01	.13	<2	32000.0
ET-7	11	174	381	230	.3	16	12	856	3.39	32	<8	<2	4	3	2.5	<3	3	7	.03	.043	14	11	.13	39	.01	<3	.43	.03	.11	<2	246.9
ET-8	10	83	659	621	<.3	15	10	1186	4.48	18	<8	<2	4	3	10.1	<3	<3	7	.03	.044	13	6	.05	26	<.01	<3	.31	.01	.07	<2	134.8
ET-9	1	12	128	404	<.3	21	11	387	4.36	2	<8	<2	8	19	3.6	<3	<3	17	.24	.046	21	17	1.38	53	.01	3	2.40	.02	.25	<2	48.4
ET-10	2	19	105	91	<.3	40	30	2533	7.54	2	<8	<2	9	19	<.5	7	3	26	.16	.068	67	17	.91	29	.02	<3	2.75	.01	.10	<2	40.7
ET-11	16	13	34	51	<.3	13	10	156	2.78	75	<8	<2	7	6	<.5	<3	<3	7	.02	.022	22	8	.17	24	<.01	<3	.99	<.01	.10	<2	435.9
ET-12	1	11	15	28	<.3	9	5	144	1.77	5	<8	<2	9	13	<.5	<3	<3	6	.11	.020	30	6	.42	19	<.01	<3	1.26	<.01	.08	<2	25.0
ET-13	4	32	233	327	<.3	15	7	950	4.51	13	<8	<2	5	6	<.5	<3	<3	18	.06	.047	29	13	.59	19	<.01	<3	1.15	.01	.09	<2	28.6
ET-14	<1	90	12	21	<.3	13	13	195	1.99	<2	<8	<2	<2	9	<.5	<3	<3	55	.16	.014	3	24	1.27	9	.06	<3	1.28	<.01	<.01	<2	11.1
ET-15	2	23	52	83	.4	50	18	3075	9.40	31	17	<2	10	18	<.5	5	<3	130	.24	.040	25	17	.86	133	.01	<3	2.35	<.01	.11	<2	19.4
ET-16	<1	27	22	61	<.3	30	12	1962	4.51	9	<8	<2	11	13	<.5	<3	<3	39	.20	.024	35	9	.75	96	<.01	<3	1.74	<.01	.16	<2	47.3
ET-17	3	11	81	84	.4	60	8	>9999	15.16	16	<8	<2	4	50	.6	<3	<3	121	.61	.071	25	15	2.51	331	.01	<3	2.94	<.01	.05	<2	41.3
ET-18	1	13	293	88	<.3	38	18	3506	5.14	5	<8	<2	4	22	<.5	<3	<3	65	.36	.028	34	11	2.02	132	.01	<3	2.64	.01	.07	<2	9.9
RE ET-18	1	13	286	86	<.3	36	17	3412	5.01	2	<8	<2	5	22	<.5	4	<3	63	.35	.028	32	12	1.98	130	.01	<3	2.58	.01	.08	<2	9.0
ET-19	1	16	227	15	<.3	4	3	87	.91	4	<8	<2	6	3	<.5	<3	<3	9	.01	.022	21	9	.07	23	<.01	<3	.43	.01	.06	<2	34.3
ET-20	1	18	21	27	<.3	3	1	36	1.61	4	<8	<2	6	4	<.5	<3	<3	10	.01	.025	38	7	.06	24	.01	<3	.52	.03	.14	<2	37.0
ET-21	1	61	14	44	<.3	13	11	52	7.52	11	<8	<2	14	5	<.5	4	<3	19	.03	.069	46	12	.12	28	.01	<3	1.78	.02	.10	<2	64.2
ET-22	1	43	39	81	<.3	13	12	459	4.73	4	<8	<2	10	9	<.5	<3	<3	6	.06	.027	42	5	.11	126	<.01	<3	1.13	<.01	.21	<2	13.6
ET-23	4	157	17	108	.9	38	49	2689	12.21	16	35	<2	3	6	.6	<3	5	24	.02	.105	15	13	.05	125	<.01	<3	.84	<.01	.23	<2	342.4
ET-24	<1	37	13	6	<.3	3	2	119	.59	<2	<8	<2	<2	1	<.5	<3	<3	4	.01	.005	4	5	.02	22	<.01	<3	.26	<.01	.03	<2	272.8
ET-25	1	15	117	85	<.3	15	7	173	2.44	13	<8	<2	7	7	<.5	<3	<3	16	.05	.025	24	17	.50	45	.04	<3	1.18	.04	.13	<2	13.3
ET-26	1	21	24	47	<.3	12	12	77	3.79	5	<8	<2	12	5	<.5	3	<3	57	.02	.050	69	20	.52	42	.01	<3	2.15	.04	.38	<2	40.1
ET-27	1	102	8	11	<.3	10	13	492	2.09	3	<8	<2	3	6	<.5	<3	<3	34	.03	.015	8	11	.28	21	.03	<3	.97	.01	.05	<2	18.5
ET-28	<1	118	9	7	.4	24	76	628	2.63	12	<8	<2	<2	4	<.5	<3	<3	42	.01	.020	2	12	.16	32	.01	<3	.63	.01	.01	<2	18.4
ET-29	1	82	8	16	<.3	36	192	3307	10.85	16	15	<2	3	7	<.5	<3	6	106	.07	.083	24	30	.52	97	.01	<3	1.86	<.01	.17	<2	11.4
ET-30	<1	4	4	5	<.3	5	4	758	1.72	<2	<8	<2	6	6	<.5	<3	<3	16	.02	.028	51	6	.11	84	<.01	<3	1.16	.03	.04	<2	9.2
ET-31	3	44	11	4	.9	2	1	69	1.44	<2	<8	10	<2	2	<.5	<3	<3	4	<.01	.014	4	16	.01	14	.01	<3	.19	<.01	.03	2	13565.3
ET-32	1	42	18	7	1.4	2	1	75	.84	2	<8	4	<2	1	<.5	<3	3	3	.01	.008	3	15	.01	13	<.01	<3	.13	<.01	.02	<2	5457.0
ET-33	1	50	86	9	<.3	2	2	174	.58	<2	<8	<2	<2	1	<.5	<3	<3	4	<.01	.005	7	14	.01	21	<.01	<3	.12	<.01	.06	2	98.4
STANDARD DS5/AU-R	12	140	27	131	.3	24	12	754	2.88	18	<8	<2	3	46	5.7	5	7	58	.72	.095	13	180	.65	136	.09	17	2.04	.03	.13	4	470.0

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK R150 60C AU* IGNITED, ACID LEACHED, ANALYZED BY ICP-MS. (15 gm)
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 9 2003 DATE REPORT MAILED: Oct 27/2003 SIGNED BY ..D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
ET-34	<1	18	61	3	.4	1	1	191	.48	2	<8	<2	<2	1	<.5	<3	<3	2	.01	.003	1	11	.01	18	<.01	<3	.06	.01	.01	<2	46.0
ET-35	5	202	220	23	4.9	6	4	55	4.40	7	<8	6	9	5	<.5	<3	3	13	.01	.038	26	12	.03	99	.01	<3	.54	.02	.15	<2	4650.8
STANDARD DS5/AU-R	13	145	25	134	.3	25	12	783	2.94	19	<8	2	3	47	5.7	4	7	58	.72	.097	12	186	.66	140	.09	18	2.06	.03	.12	4	460.0

Sample type: ROCK R150 60C.

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Ruby Red Resources Inc. PROJECT EDDY File # A305301 Page 1

207 - 239 - 12th Ave S.W., Calgary AB T2R 1N6 Submitted by: Glen Rodgers

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.6	2.6	2.3	44	<.1	4.2	4.0	561	1.90	<.5	2.1	1.3	4.6	98	<.1	<.1	.1	39	.54	.079	10	13.7	.54	238	.144	1	.92	.087	.54	2.3	.01	2.1	.4	.07	5	<.5
L1690 0SE	.5	16.4	19.0	31	.2	8.1	3.5	191	1.32	1.5	.5	1.4	1.6	10	.1	.1	.5	25	.10	.022	10	7.9	.25	79	.138	2	1.15	.017	.04	.1	.03	1.4	.1	.08	11	.5
L1690 25SE	.2	15.2	8.1	17	.1	4.3	2.7	172	.70	.6	.7	14.9	.5	6	.2	.1	.2	10	.06	.021	21	5.3	.20	50	.017	1	.64	.005	.03	<.1	.03	.9	<.1	<.05	3	<.5
L1690 75SE	.4	11.0	11.8	27	.1	6.5	5.6	670	1.49	2.5	.5	6.4	1.3	6	.2	.2	.4	24	.05	.038	13	8.4	.21	61	.036	1	.86	.006	.03	.1	.05	1.1	.1	.07	5	<.5
L1690 100SE	.7	16.8	10.4	33	.1	8.5	7.0	235	1.35	1.8	.6	4.3	.8	11	.2	.1	.3	22	.15	.027	20	10.1	.39	57	.029	<1	1.26	.008	.03	.1	.03	1.4	.1	<.05	6	<.5
L1690 125SE	1.1	49.5	55.0	58	.5	10.8	23.1	413	1.56	4.9	2.6	4.7	.4	30	1.4	.4	.4	24	.33	.134	38	37.2	.23	122	.019	1	2.56	.009	.06	.1	.14	2.1	.1	.14	5	1.5
L1690 150SE	.3	7.4	11.1	18	.1	3.9	2.2	97	1.13	2.2	.3	10.7	1.3	6	.1	.1	.3	28	.07	.018	15	8.4	.16	46	.067	<1	.64	.009	.03	.1	.03	1.1	<.1	.08	7	<.5
L1690 175SE	.2	6.7	9.5	15	.1	2.8	2.3	291	.45	.8	.4	10.3	.9	4	.1	<.1	.3	9	.05	.016	22	5.4	.14	45	.022	<1	.54	.005	.03	<.1	.01	.7	<.1	<.05	4	<.5
L1690 200SE	.9	45.0	29.2	25	.2	8.3	8.3	312	1.78	3.0	1.0	1.8	2.4	12	.3	.1	.5	34	.09	.032	16	10.9	.24	70	.118	<1	1.66	.018	.05	.2	.05	2.4	.1	.06	10	<.5
L1690 225SE	.6	28.0	21.9	21	.1	6.4	4.6	270	1.33	2.3	.9	<.5	1.2	13	.2	.1	.4	22	.10	.028	18	7.5	.18	61	.081	<1	1.25	.016	.04	.1	.04	1.7	.1	<.05	10	<.5
L1690 250SE	.5	23.4	14.4	32	.1	11.2	6.9	215	1.66	2.0	.7	10.4	1.6	8	.2	.1	.3	30	.07	.023	24	12.9	.50	57	.044	<1	1.46	.009	.04	.1	.03	1.6	.1	<.05	6	<.5
L1690 275SE	.7	31.9	19.8	25	.2	7.3	4.0	99	1.53	2.2	.7	1.2	3.0	6	.2	.1	.3	25	.05	.027	20	9.9	.29	57	.050	<1	1.51	.009	.04	.1	.04	1.8	.1	<.05	7	<.5
L1690 300SE	.8	19.7	12.9	41	.1	8.7	5.6	133	3.00	4.6	.9	110.7	4.0	5	.2	.2	.3	45	.07	.060	13	14.3	.32	50	.058	<1	3.17	.007	.03	.1	.12	2.5	.1	<.05	10	<.5
L1690 325SE	1.0	67.6	31.4	55	.2	21.1	37.1	1295	3.11	6.2	1.9	3.4	2.7	15	.3	.3	.5	56	.15	.081	26	20.8	.55	185	.045	1	3.17	.009	.07	.1	.05	3.8	.1	<.05	9	<.5
L1690 350SE	.3	12.2	16.4	22	.1	5.0	2.9	101	1.14	1.7	.4	32.7	1.6	15	.1	.1	.3	29	.18	.017	17	6.6	.20	82	.083	<1	.71	.013	.03	.1	.01	1.1	.1	<.05	7	<.5
L1690 375SE	.6	11.3	11.8	27	.1	7.6	4.1	95	2.94	4.6	.4	2.6	3.4	6	.1	.2	.3	76	.10	.042	20	11.8	.31	47	.052	<1	1.04	.007	.04	.1	.03	1.6	.1	<.05	8	<.5
L1690 400SE	.6	10.3	16.0	28	.2	5.3	2.6	97	1.67	3.0	.6	2.3	3.1	10	.1	.2	.3	40	.13	.045	16	8.9	.21	60	.094	<1	1.71	.013	.04	.1	.04	1.9	.1	<.05	11	<.5
RE L1690 400SE	.6	10.9	14.9	30	.2	5.0	2.8	100	1.83	3.4	.5	3.8	2.7	9	.1	.1	.3	40	.12	.042	13	8.1	.18	57	.087	<1	1.62	.011	.04	.1	.05	1.6	.1	<.05	12	<.5
L1690 425SE	.2	8.0	5.0	15	<.1	4.2	1.7	52	.72	1.3	.3	2.3	1.2	10	.1	.1	.1	19	.11	.011	19	6.5	.16	40	.025	<1	.43	.006	.04	<.1	.01	.9	<.1	<.05	3	<.5
L1690 450SE	.4	14.7	9.2	23	.1	7.3	4.1	174	1.61	2.5	.4	18.4	2.6	8	.1	.1	.2	36	.11	.027	23	9.6	.34	52	.030	1	1.03	.006	.03	.1	.03	1.1	.1	<.05	5	<.5
L1690 475SE	.8	59.5	41.2	64	.4	15.5	35.3	1425	2.95	3.9	1.3	1.5	1.7	25	.4	.2	.5	55	.30	.079	26	17.8	.38	119	.079	4	2.96	.017	.06	.1	.09	3.4	.1	.07	12	.6
L1690 500SE	.6	12.3	25.0	23	.1	4.0	3.5	87	.92	1.1	.5	1.5	1.2	11	.1	.1	.4	23	.12	.018	11	5.5	.12	68	.107	<1	.83	.016	.03	.1	.02	1.1	.1	<.05	9	<.5
L1690 525SE	.4	16.7	8.5	40	<.1	10.8	5.9	226	2.33	3.5	.5	4.7	4.7	3	.1	.1	.3	45	.07	.025	20	13.6	.54	38	.033	1	1.10	.005	.04	.1	.02	1.9	<.1	<.05	5	<.5
L1690 550SE	.2	4.0	9.0	17	.1	.8	.5	128	.19	<.5	.1	<.5	.3	6	.1	.1	.3	9	.06	.012	9	2.5	.03	44	.053	<1	.26	.015	.03	<.1	.03	.5	<.1	<.05	4	<.5
L1690 575SE	.7	105.0	36.5	28	.4	9.9	6.2	189	1.75	3.1	2.7	3.4	.8	11	.4	.1	.3	34	.12	.058	30	11.0	.20	60	.064	1	2.57	.015	.04	.1	.12	3.1	.1	<.05	10	.6
L1690 600SE	.6	34.3	31.5	40	.4	9.8	10.2	853	1.33	3.3	1.0	1.5	.5	26	.5	.2	.3	27	.27	.049	33	11.4	.33	122	.050	<1	1.32	.012	.05	.1	.08	1.7	.1	.10	7	<.5
L1690 625SE	1.2	24.3	22.2	65	.1	8.1	38.6	3455	2.67	4.4	.9	3.6	1.5	12	.6	.2	.3	61	.17	.058	25	10.9	.32	172	.038	<1	1.31	.007	.04	.1	.04	2.7	.2	<.05	5	.5
L1690 650SE	.7	39.1	27.7	50	.2	14.0	12.8	871	2.28	4.6	1.2	17.8	2.6	20	.6	.3	.5	44	.15	.046	48	15.4	.36	183	.066	<1	1.92	.010	.06	.1	.12	4.0	.1	.07	10	.7
L1860 0S	1.1	9.3	10.6	22	<.1	6.2	2.5	54	4.20	6.6	.6	1.8	6.0	3	.1	.3	.4	45	.03	.052	13	15.7	.24	18	.073	1	1.98	.006	.03	.2	.04	1.3	.1	<.05	11	.5
L1860 25S	.9	5.7	6.0	14	.1	5.4	2.5	44	1.74	3.4	.5	<.5	4.2	4	.1	.1	.3	19	.04	.027	22	7.7	.24	28	.024	<1	1.17	.004	.02	.1	.04	.8	.1	<.05	6	<.5
L1860 50S	.9	3.7	3.6	13	<.1	4.9	2.1	54	1.18	2.8	.5	2.3	4.7	3	<.1	.2	.3	16	.04	.025	28	5.3	.28	24	.013	<1	.63	.003	.02	.1	.01	.5	<.1	<.05	4	<.5
L1860 75S	1.2	6.3	6.2	22	<.1	10.5	3.6	57	3.38	4.2	.8	1.8	7.4	2	.1	.2	.3	28	.02	.054	26	18.3	.57	27	.018	2	1.85	.003	.03	.1	.04	1.4	<.1	<.05	6	<.5
L1860 100S	.7	6.1	5.8	23	.1	7.1	2.4	54	2.17	3.4	.5	1.7	5.0	1	.1	.1	.2	23	.01	.028	20	11.2	.43	17	.022	<1	1.30	.003	.02	.1	.03	1.2	<.1	<.05	6	.5
L1860 125S	1.0	7.2	9.6	39	.2	10.5	6.8	253	2.47	4.6	.8	1.6	6.1	4	.2	.2	.3	30	.05	.058	17	16.1	.44	48	.043	1	2.42	.007	.05	.1	.09	2.0	.1	<.05	7	.5
L1860 150S	.8	3.6	5.6	14	.1	4.3	1.9	47	1.77	2.7	.4	1.0	5.1	3	.1	.2	.3	29	.02	.018	27	8.6	.22	21	.034	<1	.81	.004	.02	.1	.02	.9	.1	<.05	8	<.5
STANDARD DS5	13.5	148.6	24.1	142	.3	24.8	12.6	774	3.00	19.4	6.7	41.8	3.1	51	5.9	3.8	6.6	63	.76	.100	14	191.6	.68	138	.095	18	2.15	.034	.14	4.9	.16	3.4	1.2	<.05	7	5.0

GROUP 1DX - 15.0 GM SAMPLE LEACHED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 300 ML, ANALYSED BY ICP-MS.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
- SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 23 2003 DATE REPORT MAILED: Nov 7/03 SIGNED BY. C.D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only. Data FA

Appendix 2. Soil Geochem Analyses

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.5	2.4	2.2	43	<.1	4.3	4.1	510	1.98	.7	2.0	.8	4.6	96	<.1	<.1	.1	46	.59	.081	11	15.0	.63	251	.140	<1	.99	.090	.50	2.2	.01	2.3	.4	.10	5	<.5
L1860 175S	1.3	3.6	6.6	21	<.1	5.8	2.9	79	2.63	3.5	.4	1.9	5.1	3	.1	.2	.4	44	.02	.035	25	12.1	.33	24	.046	6	1.06	.003	.04	.2	.02	1.2	.1	.13	10	<.5
L1860 200S	.8	6.1	8.2	24	<.1	7.2	4.6	49	2.43	3.6	.5	3.2	4.5	3	.1	.2	.3	37	.02	.049	19	14.4	.41	36	.040	<1	2.19	.003	.03	.1	.10	1.7	.1	.08	7	<.5
L1860 225S	.6	2.3	3.9	8	<.1	4.1	1.6	29	1.50	2.5	.3	1.3	3.9	2	<.1	.1	.2	25	.01	.024	25	8.3	.29	17	.017	<1	.92	.003	.02	.1	.04	1.0	<.1	.07	6	<.5
L1860 250S	1.2	5.3	10.3	20	<.1	8.5	3.6	47	2.83	4.9	.6	3.5	5.6	3	.1	.3	.4	42	.02	.044	20	12.8	.47	30	.085	<1	1.99	.006	.03	.2	.04	1.4	.1	.08	11	<.5
L1860 275S	.8	8.2	8.5	18	.1	4.6	2.7	50	1.73	3.0	.9	1.7	3.6	4	.1	.2	.3	33	.03	.088	7	7.7	.16	32	.100	2	2.98	.012	.02	.1	.07	1.6	<.1	<.05	9	<.5
L1860 300S	1.2	10.0	8.3	24	.1	9.5	5.5	64	1.90	5.0	1.0	3.0	4.9	4	.1	.1	.2	26	.04	.085	13	10.0	.42	39	.059	1	3.02	.008	.03	.1	.06	2.0	<.1	.06	7	<.5
L1860 325S	.9	12.3	11.4	25	.2	7.9	7.0	60	2.00	4.9	1.2	2.6	4.4	5	.1	.1	.2	33	.05	.108	8	8.9	.23	52	.098	2	3.55	.014	.03	.2	.11	2.8	.1	.07	9	.6
L1860 350S	.8	11.3	10.3	28	<.1	7.9	5.2	129	2.17	6.0	1.0	2.7	4.1	5	.1	.2	.3	32	.04	.141	4	9.8	.11	37	.124	<1	5.33	.015	.02	.2	.09	2.4	<.1	.06	10	.5
L1860 375S	1.4	7.1	12.9	30	.1	7.2	5.9	251	2.26	5.6	.7	15.4	4.5	6	.1	.3	.3	38	.05	.089	8	10.7	.18	58	.067	1	3.01	.008	.03	.2	.06	1.5	.1	<.05	9	<.5
L1860 400S	1.3	6.7	12.6	40	<.1	11.1	10.1	187	2.26	6.7	.8	2.3	5.2	6	.1	.2	.4	36	.03	.057	14	11.5	.37	63	.054	<1	2.44	.007	.05	.1	.04	1.8	.1	<.05	8	<.5
L1860 425S	1.5	7.3	19.1	31	<.1	14.5	12.2	185	2.48	6.9	1.0	2.1	7.4	5	<.1	.2	.4	30	.03	.044	19	12.2	.65	67	.048	<1	2.48	.006	.05	.1	.04	2.0	.1	<.05	7	<.5
L1860 450S	.9	6.3	13.5	31	<.1	10.4	9.6	108	2.28	5.5	.6	2.5	4.5	7	.1	.2	.3	32	.06	.057	10	10.2	.28	74	.067	1	2.77	.008	.04	.1	.07	1.3	.1	<.05	9	<.5
L1860 475S	1.2	6.2	15.8	38	<.1	14.4	16.8	520	2.68	8.0	1.2	2.4	7.0	5	.1	.3	.4	29	.04	.046	20	13.2	.63	64	.046	1	1.86	.004	.06	.2	.03	1.5	.1	<.05	8	<.5
L1860 500S	1.6	6.4	16.3	42	<.1	19.9	19.4	210	3.31	8.2	.9	2.3	7.8	5	.1	.3	.4	35	.05	.037	19	17.5	.68	95	.061	<1	2.69	.005	.05	.2	.05	1.8	.1	<.05	10	<.5
RE L1860 500S	1.6	6.4	15.4	41	<.1	18.6	20.2	197	3.20	7.9	.9	1.7	7.7	6	.1	.2	.4	37	.05	.041	18	16.2	.68	97	.061	3	2.95	.005	.06	.1	.05	1.7	.1	<.05	10	<.5
L1860 525S	1.5	6.8	17.9	40	.1	16.0	15.5	217	2.87	9.6	.8	2.2	6.3	6	.1	.3	.4	39	.06	.040	17	14.0	.58	67	.062	<1	2.32	.006	.06	.1	.04	1.7	.1	<.05	9	<.5
L1860 550S	1.4	8.1	150.4	56	.1	26.5	34.3	214	2.95	7.2	1.6	75.5	8.9	5	.1	.2	.4	31	.03	.036	19	15.4	.66	50	.057	<1	2.11	.004	.05	.1	.04	1.7	.1	<.05	7	<.5
L1860 575S	2.1	5.7	16.8	44	<.1	16.5	10.8	147	3.42	9.3	.7	2.6	7.7	4	.1	.3	.5	42	.03	.033	20	19.6	.70	62	.050	<1	2.62	.004	.05	.1	.04	2.1	.1	<.05	11	<.5
L1860 600S	1.7	4.8	28.8	41	.1	15.7	9.8	278	2.95	8.1	.5	8.0	5.8	7	.1	.3	.5	41	.05	.030	21	16.9	.65	76	.037	<1	1.89	.004	.05	.1	.04	1.8	.1	<.05	9	.5
L1860 625S	1.9	7.9	148.1	78	.1	26.4	27.2	170	3.49	8.2	1.7	13.2	11.0	5	.1	.2	.6	26	.03	.039	26	18.4	.88	56	.020	<1	2.18	.003	.05	.1	.04	2.3	.1	<.05	6	.5
L1860 650S	2.1	45.7	622.0	161	.3	24.6	35.3	386	2.85	8.1	2.2	12.7	9.5	4	.3	.4	.5	34	.04	.045	22	16.8	.74	54	.048	<1	2.49	.006	.05	.1	.04	2.3	.1	<.05	8	<.5
L1860 675S	1.5	12.5	162.4	148	.1	12.4	8.8	166	2.56	9.6	.8	61.3	6.1	4	.4	1.5	.4	33	.03	.047	14	13.2	.47	68	.060	4	3.22	.008	.04	.6	.07	1.9	.1	<.05	7	<.5
L1860 700S	1.0	7.5	49.8	110	.5	11.0	9.2	260	2.09	3.0	.4	6.3	4.0	5	.8	.2	.4	30	.05	.046	14	11.0	.30	72	.058	3	2.21	.011	.05	.3	.04	1.3	.1	<.05	8	<.5
L1860 725S	1.3	8.8	32.4	66	.1	10.4	6.2	127	2.24	4.2	.9	7.0	5.7	5	.2	.3	.3	36	.04	.058	12	11.5	.32	54	.072	<1	2.81	.010	.04	.5	.07	2.0	.1	<.05	8	<.5
L1860 750S	1.1	22.5	12.3	58	.1	12.7	10.0	181	2.35	5.0	.5	20.7	5.2	6	.3	.3	.3	40	.07	.041	17	10.9	.55	46	.047	<1	1.74	.007	.05	.1	.03	2.0	.1	<.05	7	.5
L1860 775S	1.4	9.6	21.1	78	.2	14.6	11.2	260	2.48	4.7	1.0	8.3	6.8	7	.3	.4	.4	27	.07	.040	18	12.7	.52	81	.053	3	2.30	.007	.05	.2	.06	1.5	.1	<.05	7	<.5
L1860 800S	1.0	7.0	61.1	124	.6	15.9	16.1	144	2.22	4.0	.7	8.6	5.5	7	.3	.5	.3	27	.06	.048	16	11.7	.42	62	.053	<1	2.56	.008	.05	.2	.05	1.4	.1	<.05	7	<.5
L1860 825S	1.1	55.0	10.7	53	.1	14.2	17.4	444	2.39	5.5	.7	.9	4.2	8	.2	.2	.3	45	.08	.087	7	10.1	.25	44	.103	<1	3.85	.016	.05	.2	.05	2.0	.1	<.05	9	<.5
L1860 850S	1.1	26.9	9.7	40	.1	14.6	12.3	378	2.36	4.7	.6	1.7	5.4	6	.1	.2	.4	31	.06	.031	18	11.9	.45	74	.047	<1	1.84	.005	.06	.1	.03	1.3	.1	<.05-	7	.6
L1860 875S	.9	11.4	14.0	39	<.1	11.7	8.1	539	2.15	4.4	.5	1.0	4.7	5	.1	.2	.4	30	.06	.032	18	11.5	.36	57	.044	1	1.94	.005	.06	.1	.05	1.4	.1	<.05	7	.7
L1860 900S	1.3	5.2	29.2	60	.1	11.3	7.1	111	2.48	5.2	.5	1.8	5.1	4	.1	.6	.5	31	.04	.024	20	11.1	.32	54	.034	<1	1.66	.004	.05	.1	.01	1.3	.1	<.05	7	<.5
L1860 925S	.7	7.4	58.2	41	.1	10.0	9.5	176	1.59	4.8	1.0	1.0	5.7	4	.1	.5	.3	13	.02	.022	25	8.4	.39	32	.014	<1	1.06	.002	.03	.1	.02	.9	<.1	<.05	4	<.5
L1860 950S	1.4	8.1	17.2	40	.3	13.7	10.1	141	1.90	5.5	.7	2.9	5.9	6	.1	.2	.3	24	.04	.027	18	10.4	.29	74	.041	<1	2.04	.006	.04	.1	.05	1.3	.1	<.05	6	<.5
L1860 975S	1.2	7.2	9.2	29	<.1	10.9	8.4	161	1.84	3.6	.6	1.4	5.3	6	.1	.2	.3	22	.05	.027	16	8.9	.25	81	.041	<1	2.21	.006	.05	.1	.03	1.3	.1	<.05	6	.6
STANDARD DS5	12.2	136.6	25.6	138	.2	24.3	11.7	740	2.96	18.6	6.2	44.0	2.9	51	5.4	3.9	6.4	62	.77	.080	14	190.0	.66	137	.103	19	2.15	.033	.15	4.5	.16	3.6	1.0	<.05	7	5.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

ACME ANALYTICAL

Ruby Red Resources Inc. PROJECT EDDY FILE # A305301

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.7	2.9	2.5	50	<.1	4.6	4.3	625	2.09	<.5	2.1	.5	5.4	105	<.1	<.1	.1	56	.65	.082	10	16.1	.67	273	.148	<1	1.12	.103	.55	2.5	<.01	2.3	.4	.13	6	<.5
L1860 1000S	.9	12.9	12.7	30	<.1	14.9	17.1	190	2.09	3.3	1.5	1.0	8.1	5	.1	.2	.3	32	.04	.035	15	11.2	.32	89	.071	<1	2.87	.008	.06	.2	.04	1.8	.1	.11	8	<.5
L1860 1025S	.7	12.5	9.9	33	<.1	14.8	14.9	271	1.93	3.3	.8	3.3	5.0	8	.1	.2	.3	33	.07	.035	13	10.3	.25	100	.090	<1	3.00	.011	.07	.1	.03	1.8	.1	.06	8	<.5
L1860 1050S	.9	9.1	10.1	31	<.1	11.9	8.4	272	2.33	3.9	.8	2.4	6.4	6	<.1	.2	.3	29	.04	.031	19	10.4	.37	67	.040	<1	2.24	.006	.05	.1	.03	1.3	.1	.09	7	<.5
L1860 1075S	.9	6.2	9.5	34	<.1	8.6	6.5	208	2.20	3.4	.4	55.0	5.0	4	.1	.2	.4	31	.03	.019	19	10.3	.28	75	.032	<1	1.54	.004	.05	.1	.03	1.0	.1	<.05	7	<.5
L1860 1100S	.9	7.6	11.8	29	<.1	10.1	7.0	405	1.98	3.2	.7	.6	4.0	10	.1	.2	.3	29	.10	.075	9	9.3	.18	91	.075	3	2.89	.010	.06	.2	.04	1.4	.1	.07	8	<.5
L1860 1125S	.8	6.4	10.4	32	<.1	8.2	5.3	140	1.78	2.5	.6	.7	4.6	6	.1	.2	.3	29	.03	.040	14	9.4	.25	66	.046	1	1.70	.007	.04	.1	.04	1.2	.1	<.05	7	<.5
L1860 1150S	1.2	9.6	16.7	62	<.1	12.2	9.0	384	2.53	6.8	.8	<.5	5.8	6	.1	.3	.4	36	.04	.080	10	12.8	.23	71	.076	<1	2.97	.010	.06	.1	.06	1.5	.1	<.05	10	<.5
L1860 1175S	1.3	8.8	14.5	36	<.1	7.8	5.1	283	2.47	4.6	.6	<.5	4.3	6	.1	.3	.4	39	.06	.069	8	10.2	.13	64	.091	<1	3.11	.011	.05	.2	.07	1.4	.1	<.05	11	<.5
L1860 1200S	1.3	7.6	14.5	40	<.1	8.2	4.2	143	2.46	5.4	.6	.6	4.9	5	.1	.4	.4	36	.04	.080	7	10.6	.18	46	.095	<1	2.76	.011	.07	.2	.04	1.3	.1	<.05	10	<.5
L1860 1225S	1.0	12.8	20.1	49	<.1	11.3	7.7	238	2.49	4.8	.8	.8	5.1	8	.1	.4	.4	36	.06	.069	12	12.2	.27	98	.086	<1	3.15	.010	.05	.2	.04	1.9	.1	<.05	9	<.5
L1860 1250S	1.0	6.6	12.5	35	.1	6.5	3.4	272	1.66	2.2	.4	<.5	2.9	6	.1	.2	.4	31	.06	.026	14	8.8	.15	51	.045	<1	1.08	.008	.06	.1	.02	1.0	.1	<.05	7	<.5
L1860 1275S	.4	5.0	9.3	26	<.1	4.8	2.0	105	1.20	2.4	.5	1.9	4.6	5	.1	.1	.4	26	.06	.023	20	7.0	.13	48	.027	1	.96	.004	.05	.1	.02	1.1	.1	<.05	6	<.5
L1860 1300S	1.0	10.9	24.4	31	.1	12.8	10.6	299	2.33	4.1	2.0	<.5	4.3	29	.1	.2	.7	33	.21	.027	28	12.0	.38	72	.041	<1	1.79	.007	.06	.1	.02	1.3	.1	<.05	8	<.5
L1860 1325S	1.4	9.0	18.6	35	.1	6.8	3.6	142	2.98	3.7	.5	<.5	4.5	8	.1	.3	.6	47	.06	.048	13	12.0	.18	53	.085	2	1.72	.007	.04	.1	.04	1.2	.1	<.05	12	<.5
L1860 1350S	1.2	12.4	17.7	50	.1	12.7	6.7	186	3.00	5.3	1.0	.7	6.6	7	.1	.3	.6	38	.07	.043	21	14.1	.47	76	.055	3	2.05	.005	.07	.2	.04	1.7	.1	<.05	9	<.5
L1860 1425S	.8	15.0	25.5	37	.1	13.8	11.1	383	2.23	4.4	1.9	1.7	2.4	26	.2	.3	.5	32	.26	.047	25	15.2	.42	72	.026	<1	2.11	.007	.08	.1	.03	1.5	.1	<.05	7	<.5
L1860 1450S	.8	15.6	15.7	41	.1	16.6	15.6	226	2.66	5.3	1.4	.9	6.6	8	.1	.2	.4	27	.06	.059	20	15.1	.44	88	.041	1	2.72	.006	.07	.1	.03	1.7	.1	<.05	7	<.5
L1860 1475S	.6	9.5	11.1	39	.1	7.1	5.4	278	1.79	2.8	.7	1.1	2.3	9	.1	.1	.4	24	.06	.097	16	9.1	.18	89	.038	<1	1.42	.006	.05	.1	.03	.9	.1	<.05	6	<.5
L1860 1500S	1.0	11.0	12.2	54	.1	11.4	7.1	277	2.58	6.4	.8	3.5	5.4	6	.1	.2	.4	30	.04	.077	16	12.3	.32	70	.062	<1	2.31	.006	.06	.2	.05	1.4	.1	<.05	8	<.5
RE L1860 1500S	.9	11.3	12.7	55	.1	10.9	7.5	271	2.64	6.3	.9	2.1	5.3	7	.1	.3	.4	33	.04	.075	17	12.9	.32	71	.066	1	2.32	.007	.05	.2	.04	1.4	.1	<.05	8	<.5
L1860 1525S	.7	11.6	8.5	44	.1	10.6	6.8	161	2.28	6.7	1.0	4.9	6.9	4	.1	.2	.3	26	.03	.053	19	10.4	.33	56	.055	2	2.21	.006	.04	.1	.04	1.5	.1	<.05	7	<.5
L1860 1550S	1.3	13.8	12.9	45	.1	18.2	11.6	264	2.62	8.6	.9	2.6	6.9	5	.1	.2	.4	29	.03	.035	15	12.3	.34	86	.044	<1	2.48	.005	.05	.1	.06	1.4	.1	<.05	8	<.5
L1860 1575S	1.0	7.9	9.0	27	.1	14.8	9.4	178	2.32	6.4	.7	4.1	5.4	7	<.1	.2	.4	24	.08	.031	18	10.3	.32	63	.040	<1	1.92	.005	.05	.1	.02	1.0	.1	<.05	7	<.5
L1860 1600S	.8	6.9	10.0	35	.1	9.4	8.2	536	1.98	6.2	.5	3.6	4.6	5	.1	.2	.4	27	.04	.031	15	8.7	.20	86	.059	5	1.60	.009	.05	.1	.03	1.3	.1	<.05	7	<.5
L1860 1625S	.6	5.9	6.8	23	<.1	5.6	3.8	201	1.88	5.8	.4	13.0	4.6	3	<.1	.2	.4	23	.03	.020	22	7.7	.20	38	.021	2	1.20	.004	.04	.1	.01	.8	.1	<.05	6	<.5
L1860 1650S	.9	12.0	11.3	41	.1	17.0	11.2	303	2.06	5.4	1.1	4.0	5.7	6	.1	.3	.3	26	.04	.041	12	9.8	.23	110	.089	3	2.67	.009	.05	.2	.04	1.8	.1	<.05	7	<.5
L1860 1675S	.6	6.0	11.2	30	<.1	8.3	6.8	341	1.72	4.8	.5	4.0	4.5	5	<.1	.2	.3	27	.05	.033	15	8.9	.22	65	.051	2	1.57	.007	.05	.1	.02	1.0	.1	<.05	6	<.5
L1860 1700S	.8	10.3	12.8	35	.1	14.1	10.5	491	2.13	5.8	1.1	4.3	5.2	13	.1	.2	.4	32	.14	.033	19	11.8	.29	81	.053	3	2.03	.010	.06	.1	.02	1.4	.1	<.05	8	.5
L1860 1725S	.5	6.2	14.5	46	.1	6.3	4.4	119	1.84	4.2	.4	.9	3.8	4	.1	.2	.4	30	.04	.026	15	9.7	.21	49	.038	2	1.51	.006	.05	<.1	.02	1.0	.1	<.05	7	<.5
L1860 1750S	.5	8.6	16.7	50	.1	10.2	7.1	158	2.04	3.3	.8	1.2	4.7	7	.2	.2	.3	26	.07	.065	7	10.5	.20	66	.069	4	2.81	.009	.06	.1	.04	1.6	.1	<.05	8	<.5
L1860 1775S	.5	12.7	18.3	34	.1	14.5	10.7	744	2.04	3.2	1.0	16.9	5.2	15	.1	.2	.4	26	.18	.020	21	16.2	.74	61	.028	<1	1.80	.007	.05	.1	.01	1.7	.1	<.05	6	<.5
L1860 1800S	.9	10.1	11.2	51	.1	11.3	9.4	242	2.26	6.1	.7	9.6	6.2	5	.1	.2	.3	30	.04	.056	15	9.9	.23	70	.078	5	2.52	.009	.05	.2	.03	1.5	.1	<.05	7	<.5
L1860 1825S	.9	8.8	15.4	48	.1	9.3	7.3	290	2.32	5.6	.5	51.3	5.6	4	.1	.3	.5	32	.04	.036	20	10.7	.26	62	.054	2	1.64	.007	.06	.2	.03	1.2	.1	<.05	7	<.5
L1860 1850S	.6	6.2	12.3	52	.1	7.8	6.1	436	1.59	3.4	.4	10.4	3.5	5	<.1	.2	.3	22	.06	.024	15	8.2	.20	88	.049	2	1.38	.006	.06	.1	.02	.9	.1	<.05	6	<.5
STANDARD DS5	12.6	150.9	26.0	146	.2	25.8	12.3	757	3.02	18.9	6.4	44.8	2.8	50	5.7	3.9	6.6	65	.74	.086	13	194.4	.69	136	.099	18	2.11	.033	.15	5.0	.17	3.3	1.1	<.05	7	5.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
L1860 1875S	.7	14.0	19.5	69	.1	10.2	7.5	326	2.49	3.8	.6	5.6	4.0	5	.1	.3	.3	48	.07	.078	10	10.4	.29	85	.104	<1	2.67	.012	.08	.1	.05	1.8	.1	.12	9	.6
L1860 1900S	.5	15.2	14.0	69	.1	12.3	9.8	482	2.43	3.4	.7	6.1	5.4	6	.1	.2	.2	42	.06	.067	9	9.8	.23	81	.113	1	2.99	.014	.07	.1	.03	1.7	.1	.06	8	.7
L1860 1925S	.6	14.3	12.3	83	.1	9.1	9.5	276	2.84	2.6	.4	14.8	3.3	5	.1	.2	.3	59	.11	.051	13	8.6	.27	93	.099	<1	1.68	.012	.14	.1	.02	2.0	.2	.08	9	<.5
L1860 1950S	.8	36.8	14.2	77	.1	14.8	14.1	246	3.31	5.1	.8	19.9	6.6	6	.1	.2	.3	53	.08	.045	20	11.4	.46	98	.084	1	2.21	.010	.17	.1	.04	2.4	.2	<.05	7	<.5
L1860 1975S	.7	21.0	10.3	63	.1	9.9	10.4	181	3.26	2.9	.4	39.4	3.8	5	.1	.2	.3	58	.11	.048	16	9.4	.32	85	.093	3	1.81	.011	.14	.1	.03	2.3	.2	<.05	9	.7
L1860 2000S	.6	61.9	12.6	47	.1	10.2	10.6	134	2.80	2.9	.4	2.8	2.8	6	.1	.2	.3	87	.14	.034	12	9.0	.29	85	.077	3	1.91	.013	.08	.1	.02	2.3	.1	<.05	8	<.5
L1860 2025S	.7	24.3	12.6	63	.1	12.3	11.7	258	2.51	3.7	.6	5.2	4.6	5	.1	.2	.3	58	.09	.040	15	9.9	.34	73	.063	2	2.14	.010	.09	.1	.02	2.4	.1	<.05	8	<.5
L1860 2050S	.6	20.5	10.5	75	.2	9.6	8.5	199	2.26	3.1	.6	8.9	4.7	6	.1	.1	.3	28	.07	.057	17	9.7	.31	69	.050	3	2.18	.008	.07	.1	.03	1.7	.1	<.05	6	<.5
L1860 2075S	.6	33.7	11.7	108	.3	12.2	17.0	530	2.55	3.3	.7	2.9	3.8	6	.1	.1	.3	46	.09	.088	9	9.7	.25	75	.103	3	3.14	.017	.09	.2	.04	3.0	.2	<.05	8	.6
L1860 2100S	.4	70.2	7.9	77	.3	11.1	12.7	338	3.20	2.9	.4	6.0	3.3	6	.1	.2	.2	101	.13	.082	10	7.4	.45	67	.102	3	1.95	.015	.10	.1	.03	3.9	.2	<.05	7	.5
L1860 2125S	.5	137.5	9.7	117	.2	15.8	17.2	764	3.15	3.6	.4	2.7	2.1	9	.2	.2	.2	131	.21	.077	6	7.3	.36	65	.132	2	2.55	.021	.10	.1	.06	3.6	.2	<.05	9	.6
L1860 2150S	.7	110.1	12.6	88	.2	15.3	13.0	555	3.02	5.2	.6	106.6	3.3	8	.1	.2	.2	89	.13	.133	5	9.7	.28	59	.138	4	4.13	.015	.08	.2	.08	3.5	.1	<.05	10	.5
L1860 2175S	.6	71.8	11.6	102	.3	11.7	11.4	706	2.40	3.9	.4	.8	2.5	8	.3	.2	.2	50	.13	.098	6	8.5	.21	62	.104	2	2.80	.015	.07	.1	.05	2.1	.1	<.05	8	<.5
L1860 2200S	.4	21.3	13.1	75	.2	8.1	9.3	1330	1.85	3.0	.4	2.1	2.2	9	.3	.2	.3	41	.13	.106	6	8.0	.15	65	.116	4	2.42	.017	.05	.1	.03	1.9	.1	<.05	8	<.5
L1860 2225S	.8	62.4	12.8	83	.4	10.7	9.6	499	1.90	4.3	1.2	1.7	3.3	9	.3	.2	.2	39	.08	.142	8	8.3	.16	66	.149	4	4.13	.021	.04	.2	.05	3.9	.1	<.05	11	.7
L1860 2250S	.6	23.3	9.9	90	.3	16.7	13.7	373	2.72	2.6	.5	2.7	2.6	9	.2	.1	.2	71	.19	.080	6	9.6	.35	69	.110	<1	2.80	.024	.09	.1	.03	3.6	.1	<.05	8	<.5
L1860 2275S	.6	12.8	14.4	77	.1	12.8	11.9	925	2.35	3.1	.3	1.2	2.0	10	.1	.3	.3	58	.16	.090	5	10.4	.24	67	.121	1	2.89	.018	.05	.1	.06	1.9	.1	<.05	9	.5
L1860 2300S	1.0	38.3	12.5	70	.2	12.1	10.4	908	2.39	4.1	.9	2.1	3.3	6	.1	.2	.3	51	.10	.115	7	11.0	.24	58	.133	<1	3.84	.013	.07	.2	.06	3.3	.2	<.05	10	.5
RE L1860 2300S	1.0	41.1	13.2	78	.2	13.3	11.0	900	2.41	4.4	1.0	2.1	3.5	7	.1	.2	.3	46	.10	.125	8	11.0	.25	66	.137	2	4.17	.015	.08	.2	.07	3.0	.2	<.05	11	.7
L1860 2325NW	.5	26.0	11.3	82	.1	13.4	12.0	1117	2.23	3.2	.5	1.4	2.7	11	.2	.2	.2	48	.13	.084	6	9.8	.22	87	.140	<1	3.18	.020	.06	.1	.03	2.3	.1	<.05	10	<.5
L1860 2350NW	.6	34.3	14.4	122	.1	20.7	16.4	1814	3.40	4.5	.4	1.9	2.4	11	.2	.3	.2	71	.17	.084	7	12.2	.43	87	.129	<1	3.00	.016	.08	.1	.04	2.6	.1	<.05	10	<.5
L1860 2375NW	.6	42.7	13.3	107	.2	16.5	19.3	1009	2.94	3.4	.5	5.2	2.7	7	.2	.2	.3	55	.12	.087	7	12.2	.26	90	.134	<1	3.05	.013	.09	.1	.05	2.6	.2	<.05	11	<.5
L1860 2400NW	.6	63.4	13.1	70	.1	14.7	13.5	316	2.90	3.7	.6	17.9	4.0	7	.1	.2	.3	62	.13	.053	11	9.1	.32	79	.105	<1	2.45	.014	.07	.2	.04	2.7	.1	<.05	8	<.5
L1860 2425NW	.7	92.0	12.3	54	.1	14.9	14.9	325	2.78	4.4	.9	15.5	4.9	8	.1	.2	.2	60	.12	.081	12	9.9	.35	74	.117	<1	3.41	.016	.07	.1	.04	3.6	.1	<.05	8	<.5
L1860 2450NW	.4	46.6	26.7	84	.2	11.4	10.6	1038	2.19	3.5	.3	4.4	2.8	13	.3	.4	.3	47	.20	.095	11	8.9	.23	111	.096	2	1.76	.016	.09	.1	.02	2.1	.1	<.05	7	<.5
L1860 2475NW	.7	73.2	11.3	72	.1	17.5	13.1	273	2.45	3.5	.6	5.3	3.9	9	.1	.2	.2	51	.14	.080	11	9.9	.31	100	.111	<1	2.57	.015	.11	.2	.02	2.8	.1	<.05	7	.5
L1860 2500NW	.8	96.0	12.1	81	.2	17.2	14.3	881	2.82	3.9	.5	9.6	3.5	9	.2	.2	.3	58	.09	.063	14	11.1	.29	100	.100	<1	2.39	.011	.06	.2	.03	2.0	.1	<.05	10	<.5
L1860 2525NW	.8	42.8	12.9	68	.1	16.0	10.8	451	2.53	4.8	.4	19.2	3.9	7	.1	.3	.3	49	.09	.061	15	10.2	.34	78	.087	<1	2.33	.012	.08	.2	.02	2.2	.1	<.05	8	<.5
L1860 2550NW	.8	25.5	17.5	59	.1	11.6	9.4	260	2.26	4.4	.9	3.5	4.6	9	.2	.2	.3	35	.10	.120	5	9.0	.13	53	.138	<1	4.47	.018	.04	.2	.04	1.6	.1	<.05	10	.5
L1860 2575NW	.8	13.4	14.8	76	.2	9.7	7.8	282	2.28	4.1	.6	4.0	3.9	12	.2	.2	.3	39	.12	.124	8	10.1	.17	81	.121	<1	3.51	.015	.06	.2	.04	1.7	.1	<.05	10	<.5
L1860 2600NW	.8	12.3	17.7	76	.1	9.0	7.1	295	1.96	3.0	.5	2.1	3.5	7	.1	.2	.3	32	.07	.112	8	9.6	.14	89	.109	<1	2.63	.013	.05	.1	.03	1.4	.1	<.05	9	<.5
L1860 2625NW	.9	11.5	14.9	53	.1	7.3	6.3	247	2.06	3.4	.5	1.5	2.9	5	.1	.2	.4	39	.06	.082	8	9.2	.14	56	.122	2	2.12	.015	.05	.2	.02	1.4	.1	.07	10	.5
L1860 2650NW	.7	13.9	11.8	56	.1	9.6	7.0	358	1.93	2.6	.4	5.2	3.4	7	.1	.1	.3	29	.09	.079	17	9.3	.25	71	.063	<1	1.51	.009	.05	.1	.03	1.3	.1	.06	7	<.5
L1860 2675NW	.8	13.8	14.2	61	.1	9.2	6.9	283	2.00	4.0	.5	8.1	3.7	6	.1	.2	.3	27	.06	.136	9	8.7	.16	56	.082	<1	2.37	.013	.05	.2	.04	1.2	.1	<.05	7	<.5
STANDARD DS5	11.7	142.9	24.5	128	.3	24.2	12.1	776	3.02	18.1	5.8	40.2	2.8	50	5.4	3.7	5.7	61	.75	.093	13	185.4	.65	130	.095	17	2.13	.033	.15	4.8	.18	3.4	1.0	<.05	7	5.1

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data A FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.6	2.2	2.2	44	<.1	3.9	4.2	582	2.01	.7	1.8	1.0	3.9	88	<.1	<.1	.1	44	.52	.084	12	14.1	.54	246	.115	<1	.89	.084	.47	2.3	<.01	2.1	.3	.10	5	<.5
L1860 2700NW	.7	14.0	11.8	66	.1	10.8	8.3	252	2.04	3.8	.6	17.7	4.3	6	.1	.2	.4	34	.08	.109	18	7.5	.26	74	.060	3	1.97	.009	.06	.2	.02	1.6	.1	.09	6	<.5
L1860 2825NW	.9	9.8	12.6	42	.1	12.8	9.7	310	2.39	4.0	.5	17.9	4.8	8	.1	.2	.4	35	.09	.044	20	10.4	.30	105	.058	6	2.30	.008	.08	.1	.03	1.6	.1	.06	7	<.5
L1860 2850NW	.9	11.6	16.2	50	.1	15.2	9.2	435	2.67	4.2	.5	9.5	4.9	7	.1	.3	.5	38	.12	.032	28	12.9	.40	92	.043	5	1.83	.006	.08	.1	.02	1.8	.1	.08	8	<.5
L1860 2875NW	1.9	37.2	42.8	84	.2	30.9	19.2	2642	3.14	8.0	3.3	15.6	6.1	28	.6	.4	.8	29	.40	.074	55	13.4	.51	126	.031	1	2.35	.010	.10	.1	.05	3.3	.1	.13	6	<.5
L1860 2900NW	1.2	23.0	28.5	61	.1	17.2	12.0	386	2.43	7.2	1.7	20.3	6.6	11	.1	.2	.6	25	.18	.022	36	10.7	.45	61	.015	<1	1.61	.005	.07	.1	.01	1.9	.1	<.05	5	<.5
L1860 2925NW	1.6	33.1	24.1	83	.1	26.6	13.7	257	3.29	6.4	1.6	27.6	7.2	11	.1	.3	.7	37	.15	.031	30	15.8	.51	68	.043	3	2.47	.008	.09	.1	.01	2.2	.1	<.05	6	<.5
L1860 2950NW	1.9	33.0	41.7	118	.1	20.9	22.3	2319	3.24	9.7	1.2	24.9	5.5	11	.6	.5	.9	35	.15	.074	31	13.5	.47	135	.059	8	1.83	.007	.09	.2	.06	1.6	.1	<.05	7	<.5
L1860 2975NW	1.7	27.0	22.8	82	.1	19.0	17.2	1039	3.37	8.5	1.1	9.3	6.5	11	.2	.3	.6	39	.14	.076	21	13.1	.43	144	.105	6	2.76	.011	.10	.2	.05	2.1	.1	<.05	10	<.5
L1860 3000NW	1.2	18.6	15.7	66	.1	16.5	14.0	877	2.83	6.7	.8	16.4	5.8	12	.1	.3	.6	35	.14	.046	24	11.5	.40	166	.071	3	2.12	.009	.08	.1	.05	1.9	.1	<.05	8	<.5
L1860 3025NW	1.2	18.0	20.2	101	.2	17.8	17.3	1259	2.94	5.0	.9	84.5	6.4	12	.3	.3	.6	39	.19	.070	23	13.4	.44	194	.087	4	2.73	.013	.13	.1	.05	2.6	.1	<.05	9	<.5
L1860 3050NW	1.3	11.3	14.4	69	.2	12.3	11.4	365	2.70	4.1	.6	25.9	4.0	18	.2	.2	.4	40	.27	.085	10	9.9	.18	160	.123	4	2.84	.022	.07	.2	.05	1.8	.1	<.05	11	<.5
L1860 3075NW	1.1	10.3	16.1	48	.2	11.6	11.1	1621	2.80	4.2	.6	112.1	5.1	10	.2	.2	.6	38	.18	.060	32	10.3	.38	140	.050	4	1.25	.007	.10	.1	.02	1.9	.1	<.05	7	<.5
L1860 3100NW	1.2	14.6	12.3	54	.1	22.4	19.6	503	3.13	4.7	1.0	93.5	5.9	8	<.1	.3	.5	43	.07	.078	15	14.1	.43	106	.093	<1	3.29	.011	.07	.2	.06	2.4	.1	<.05	10	<.5
L1860 3125NW	1.5	7.1	10.0	37	.1	17.1	32.9	1457	2.98	3.8	.7	7.8	4.8	9	.1	.2	.5	43	.12	.033	24	12.1	.49	154	.037	1	1.82	.006	.09	.1	.02	2.5	.1	<.05	7	<.5
L1860 3150NW	1.9	9.9	9.9	39	.1	21.4	27.0	248	3.61	5.2	.8	10.7	5.1	6	.1	.3	.6	54	.05	.048	20	12.3	.77	72	.046	<1	2.27	.006	.07	.1	.03	3.2	.1	<.05	8	<.5
L1860 3175NW	1.5	9.0	12.7	46	.1	13.5	19.1	330	2.95	3.5	.6	16.4	4.2	9	.1	.2	.5	48	.06	.052	15	13.0	.39	129	.092	4	2.12	.011	.06	.1	.04	2.3	.1	<.05	11	<.5
L1860 3200NW	1.5	11.1	11.4	42	.1	15.5	20.3	249	2.46	5.7	1.2	2.6	5.2	11	.1	.3	.3	34	.10	.225	7	9.7	.20	76	.132	1	4.28	.021	.05	.2	.09	2.2	.1	<.05	11	<.5
RE L1860 3200NW	1.5	10.5	11.5	39	<.1	14.7	19.6	233	2.28	4.9	1.2	2.9	5.5	10	.1	.3	.3	32	.09	.207	7	8.8	.19	70	.126	1	4.12	.019	.05	.3	.09	2.2	.1	<.05	10	<.5
L1860 3225NW	1.4	10.5	12.2	50	.1	15.1	19.1	674	2.69	6.3	1.2	3.9	6.5	8	.1	.3	.4	32	.07	.073	14	11.7	.35	122	.072	2	2.58	.010	.06	.2	.05	1.8	.1	<.05	8	<.5
L1860 3250NW	1.4	10.7	14.1	45	.1	11.1	11.2	182	2.45	6.5	1.3	3.2	5.0	13	.2	.4	.3	33	.14	.128	5	9.9	.16	86	.132	4	4.03	.018	.04	.2	.10	2.1	.1	<.05	11	.5
L1860 3275NW	1.3	6.5	12.7	28	.1	12.9	12.2	172	2.47	4.0	.6	1.4	4.0	9	.1	.2	.4	38	.08	.077	11	9.8	.18	89	.103	3	2.93	.016	.05	.2	.03	1.5	.1	<.05	12	<.5
L1860 3300NW	1.0	11.3	20.0	31	.1	18.2	14.9	453	2.37	4.7	3.2	1.5	7.7	21	.1	.2	.5	22	.17	.029	34	13.6	.35	101	.036	2	2.27	.009	.06	.1	.04	2.3	.1	<.05	8	.5
L1860 3325NW	.8	5.6	9.6	26	<.1	7.6	6.1	115	2.10	4.8	.6	<.5	4.5	6	.1	.2	.3	26	.06	.063	25	10.2	.26	67	.040	1	1.61	.007	.04	.1	.05	1.3	.1	<.05	6	<.5
L1860 3350NW	.4	5.3	9.5	22	.1	6.1	3.1	111	1.53	2.4	.4	<.5	3.5	5	<.1	.1	.3	22	.04	.036	26	6.6	.17	59	.037	5	1.02	.006	.04	.1	.02	1.1	.1	<.05	7	<.5
L1860 3375NW	.4	6.6	18.1	25	.1	6.8	4.3	525	1.19	2.2	.4	1.9	1.7	16	.2	.1	.4	16	.14	.022	26	7.3	.25	109	.020	1	1.01	.007	.08	.1	.02	.9	.1	<.05	5	<.5
L1860 3400NW	.4	6.8	9.3	34	<.1	8.2	5.4	154	1.65	2.5	.5	3.4	4.9	5	.1	.1	.3	17	.04	.021	33	8.5	.36	43	.027	<1	1.07	.004	.04	.1	<.01	.7	<.1	<.05	5	<.5
L1940 0S	.7	10.1	12.0	28	.1	6.3	3.0	58	1.71	4.3	.8	<.5	5.3	3	<.1	.2	.3	18	.01	.024	23	9.1	.21	26	.021	2	1.51	.003	.03	.1	.04	1.4	.1	<.05	5	<.5
L1940 25S	.6	4.5	11.3	12	.1	2.7	1.0	35	2.03	3.0	.4	<.5	3.1	3	<.1	.2	.4	24	.02	.021	20	6.4	.08	19	.045	<1	.96	.006	.03	.1	.03	.7	.1	<.05	7	.5
L1940 50S	.8	9.7	10.3	21	.1	3.9	2.0	52	2.18	3.7	.9	<.5	4.7	5	.1	.2	.2	32	.05	.054	10	10.2	.10	27	.076	<1	3.90	.013	.03	.2	.06	1.8	.1	<.05	8	<.5
L1940 75S	.6	6.3	9.8	22	.1	3.7	1.7	45	1.98	3.6	.5	<.5	3.1	3	.1	.3	.4	25	.03	.026	22	8.3	.13	27	.032	2	1.11	.004	.04	.1	.03	.9	.1	<.05	7	<.5
L1940 100S	.4	6.1	9.0	42	.1	8.7	4.4	120	1.68	3.4	.7	<.5	5.7	3	.1	.1	.2	19	.02	.026	21	9.8	.28	31	.021	4	1.55	.002	.04	.1	.03	1.0	.1	<.05	4	<.5
L1940 125S	.6	8.0	10.2	26	.1	5.3	2.9	112	1.65	3.3	.7	<.5	4.1	4	<.1	.2	.3	23	.03	.047	15	7.2	.17	35	.050	5	1.99	.009	.04	.1	.04	1.0	.1	<.05	8	<.5
L1940 150S	1.0	6.1	8.2	24	.1	5.3	3.0	63	1.57	3.6	.7	<.5	4.7	3	<.1	.2	.4	25	.02	.025	24	8.0	.17	31	.031	<1	1.44	.005	.03	.1	.03	1.1	.1	<.05	6	<.5
L1940 175S	.6	7.0	8.1	24	<.1	6.7	2.9	60	1.78	4.6	.8	<.5	5.5	2	<.1	.2	.3	19	.02	.026	25	9.5	.26	26	.026	2	1.24	.003	.03	.1	.03	1.2	.1	<.05	5	<.5
STANDARD DS5	13.1	143.0	25.6	141	.3	24.6	13.1	775	3.15	19.2	5.9	42.0	3.1	50	5.6	3.8	6.3	65	.78	.104	16	184.5	.70	143	.098	18	2.03	.034	.15	4.7	.19	3.6	1.1	<.05	7	4.8

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data A FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.5	2.5	2.7	46	<.1	4.6	4.7	572	1.98	.8	1.8	1.2	4.5	104	<.1	<.1	.1	47	.59	.082	9	14.4	.52	234	.128	<1	.96	.096	.52	2.0	<.01	2.6	.3	.17	5	.5
L1940 200S	.8	12.8	10.7	30	.1	6.4	3.6	73	2.19	3.7	.9	2.7	5.3	5	.1	.2	.3	35	.04	.073	7	10.8	.13	35	.064	<1	2.75	.010	.05	.1	.05	1.9	.1	.17	8	<.5
L1940 225S	1.1	11.6	11.2	35	.1	6.7	4.5	129	2.50	4.9	.9	1.8	6.2	4	.1	.3	.4	40	.03	.064	9	11.9	.18	36	.082	2	2.88	.009	.04	.2	.05	1.7	.1	.08	9	.6
L1940 250S	2.0	8.0	13.4	38	.1	7.1	4.5	141	4.86	6.8	.7	2.6	5.9	4	.1	.5	.6	57	.03	.079	10	17.7	.18	45	.093	<1	2.41	.007	.05	.2	.07	1.5	.1	.09	14	.6
L1940 275S	2.1	11.3	8.7	20	.1	7.6	3.6	69	3.32	5.7	.7	4.1	7.2	3	<.1	.4	.5	32	.02	.052	16	15.1	.31	30	.022	2	2.02	.004	.03	.1	.04	1.4	.1	.08	8	<.5
L1940 300S	3.0	19.6	12.0	38	.1	11.6	7.1	131	2.89	4.8	.8	1.5	5.4	8	.1	.4	.4	39	.04	.049	13	14.3	.31	47	.042	1	2.21	.006	.03	.1	.03	1.7	.1	<.05	8	<.5
L1940 325S	1.3	12.9	10.3	37	<.1	17.7	14.4	150	2.85	6.5	.8	1.2	6.2	6	.1	.3	.4	35	.04	.044	15	15.6	.53	57	.030	1	2.20	.004	.04	.2	.03	1.9	.1	.10	6	1.0
L1940 350S	1.6	10.7	13.1	33	<.1	11.6	7.9	226	2.90	5.6	1.0	.5	6.0	7	.1	.3	.4	38	.06	.062	7	12.3	.20	64	.093	<1	3.67	.010	.04	.2	.08	2.1	.1	.07	11	.5
L1940 375S	1.2	10.3	12.4	40	.1	12.0	6.5	482	3.16	4.1	.5	<.5	4.8	12	.1	.3	.5	48	.10	.061	14	21.2	.29	73	.088	1	2.14	.008	.06	.2	.05	2.0	.1	.08	10	.5
L1940 400S	1.5	16.1	14.6	44	.1	14.8	12.5	424	2.70	6.9	1.1	1.5	5.8	6	.2	.3	.5	35	.04	.063	11	13.7	.33	65	.078	4	2.95	.009	.05	.2	.06	2.1	.1	<.05	9	.6
L1940 425S	1.3	13.4	14.2	44	<.1	11.7	9.4	346	3.01	5.8	.8	1.1	5.3	8	.1	.3	.4	41	.06	.076	8	12.9	.21	80	.098	<1	3.18	.010	.06	.2	.05	1.9	.1	.08	11	.5
L1940 450S	1.2	16.9	12.2	38	.1	12.9	10.6	215	2.55	5.5	1.0	1.3	5.3	7	.1	.3	.3	37	.06	.063	8	12.6	.28	62	.104	<1	3.53	.011	.05	.2	.08	2.2	.1	.09	9	.6
L1940 475S	1.2	12.7	13.9	43	.1	12.3	10.3	349	2.91	5.9	.5	1.9	4.4	7	.1	.4	.4	37	.05	.049	12	13.1	.29	65	.077	<1	2.48	.009	.05	.2	.05	1.6	.1	.07	10	<.5
L1940 500S	2.3	19.9	24.9	54	.1	28.2	25.6	384	3.29	6.2	.9	<.5	5.1	12	.1	.4	.6	44	.09	.043	12	18.3	.29	62	.109	4	2.18	.009	.09	.2	.04	2.1	.1	<.05	11	.7
L1940 525S	1.4	11.7	12.9	40	<.1	12.8	11.4	674	2.30	4.9	.6	<.5	4.1	7	.1	.3	.4	32	.06	.026	16	12.4	.24	88	.057	3	1.61	.008	.06	.1	.03	1.2	.1	<.05	7	<.5
L1940 550S	1.4	10.5	18.9	45	<.1	10.5	7.6	582	2.16	6.8	.6	<.5	4.4	7	.1	.3	.4	30	.06	.035	13	11.3	.21	82	.042	2	1.66	.007	.06	.1	.03	1.3	.1	.06	7	<.5
L1940 575S	1.1	9.7	23.5	46	.1	8.5	6.0	643	1.60	4.6	.5	1.3	3.1	14	.2	.3	.4	23	.14	.046	9	7.9	.14	82	.064	5	1.55	.010	.07	.1	.03	1.3	.1	<.05	6	<.5
L1940 600S	.9	9.4	13.8	40	.1	8.7	5.0	244	1.93	3.9	.5	1.3	3.7	12	.1	.2	.4	30	.05	.037	12	10.5	.17	94	.059	1	1.54	.008	.05	.1	.03	1.3	.1	<.05	7	<.5
L1940 625S	1.4	12.0	14.2	46	.1	8.7	7.2	166	2.13	4.7	1.0	1.1	5.7	7	.1	.3	.3	29	.05	.066	10	11.3	.19	76	.064	1	2.90	.010	.05	.2	.05	1.7	.1	<.05	8	.7
L1940 650S	1.1	10.1	17.9	57	.1	8.8	6.7	773	1.93	4.4	.7	1.9	3.8	12	.2	.3	.3	29	.10	.080	8	9.6	.14	96	.087	2	2.55	.012	.05	.1	.04	1.5	.1	<.05	7	<.5
L1940 675S	1.3	11.6	16.7	59	.1	10.5	7.5	255	2.05	5.1	.9	1.4	4.2	9	.2	.3	.3	30	.08	.107	5	8.9	.12	81	.120	4	3.77	.015	.04	.2	.07	2.1	.1	<.05	10	.7
L1940 700S	2.0	11.1	20.7	68	.1	10.4	7.8	392	2.49	8.1	.6	1.5	4.4	8	.1	.3	.4	33	.08	.063	8	11.9	.17	73	.103	4	2.44	.012	.07	.1	.05	1.6	.1	<.05	10	<.5
RE L1940 700S	1.8	10.9	19.1	68	.1	10.6	7.0	404	2.39	7.9	.6	1.1	4.2	9	.2	.3	.4	34	.10	.067	8	11.7	.17	72	.105	<1	2.51	.012	.07	.2	.07	1.8	.1	.06	9	.5
L1940 725S	1.6	17.7	20.3	63	.1	12.1	8.4	181	2.37	5.3	.9	1.8	5.5	6	.1	.3	.4	35	.05	.041	11	11.8	.21	110	.096	3	2.54	.010	.07	.2	.05	1.9	.1	<.05	9	.6
L1940 750S	.8	74.6	15.4	56	.1	15.5	13.5	499	2.84	5.7	.9	<.5	5.4	10	.1	.3	.4	52	.10	.070	16	11.8	.50	94	.059	<1	1.88	.005	.08	.1	.02	3.1	.1	<.05	8	.8
L1940 775S	2.1	17.1	17.9	41	.1	15.8	16.8	315	3.30	7.2	.7	2.2	4.3	12	.2	.3	.7	41	.08	.047	14	14.0	.35	88	.070	1	2.31	.008	.06	.1	.04	1.7	.1	.06	10	<.5
L1940 800S	1.1	14.1	19.3	41	.3	11.7	14.5	618	2.39	4.9	1.6	.8	2.6	35	.4	.2	.5	28	.30	.053	15	11.9	.29	126	.061	3	1.84	.009	.08	.1	.05	1.6	.1	<.05	8	<.5
L1940 825S	.9	13.2	31.0	58	.1	15.7	13.9	912	2.13	3.8	1.6	2.4	3.3	20	.4	.2	.5	27	.18	.065	20	12.3	.37	134	.055	1	2.24	.007	.09	.1	.04	1.8	.1	.07	7	.7
L1940 850S	.9	12.3	12.5	56	.1	9.9	6.4	311	2.97	4.0	1.0	2.3	6.7	5	.1	.2	.5	39	.03	.058	20	15.3	.32	67	.060	2	1.99	.005	.06	.1	.04	1.9	.1	.07	9	.6
L1940 875S	1.0	11.8	13.8	53	.1	9.6	6.7	406	2.69	5.5	.9	2.0	5.2	4	.1	.3	.4	28	.04	.056	17	12.3	.30	60	.036	<1	1.71	.004	.05	.1	.04	1.8	.1	<.05	7	.5
L1940 900S	1.4	16.4	24.8	64	.2	18.3	14.0	169	3.36	5.6	1.4	2.5	7.7	7	.2	.2	.6	39	.06	.051	13	17.3	.38	92	.080	<1	3.50	.009	.08	.1	.07	2.3	.1	.08	12	.5
L1940 925S	1.6	24.4	21.5	62	.1	17.5	14.3	280	3.35	5.7	2.0	3.5	8.9	5	.2	.4	.5	32	.04	.063	18	15.1	.42	52	.071	1	2.64	.005	.06	.1	.08	2.5	.1	.08	9	.8
L1940 950S	.9	15.6	15.0	61	.2	13.0	9.4	199	2.66	4.9	1.0	4.6	7.1	6	.1	.3	.4	32	.05	.046	14	14.8	.32	77	.072	<1	2.66	.007	.07	.1	.06	2.1	.1	.09	9	.8
L1940 975S	.8	5.7	9.7	25	.1	6.1	3.6	86	1.59	2.7	.5	4.1	3.6	4	.1	.1	.3	26	.03	.020	16	9.0	.18	42	.031	1	1.05	.006	.05	.1	.01	1.0	.1	<.05	6	<.5
L1940 1000S	1.1	9.5	13.4	31	.1	7.3	3.6	104	2.05	4.4	.7	4.8	4.4	8	.1	.2	.4	31	.06	.046	9	10.6	.14	60	.064	<1	2.45	.010	.05	.1	.04	1.7	.1	.07	8	<.5
STANDARD DS5	13.1	139.6	26.0	137	.3	24.0	12.7	778	3.03	19.2	6.0	43.0	2.8	52	5.7	4.1	6.3	62	.79	.101	12	188.9	.68	145	.097	17	1.99	.034	.15	4.7	.18	3.7	1.0	.06	6	5.1

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data A FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.6	2.5	2.2	41	<.1	4.5	4.2	557	1.96	.6	1.8	<.5	4.1	93	<.1	<.1	.1	51	.64	.081	9	13.2	.51	256	.139	2	.95	.090	.43	2.2	<.01	2.5	.3	.14	5	<.5
L1940 1025S	1.3	11.5	14.6	42	.1	9.4	6.5	153	1.99	4.3	.9	2.6	5.0	7	.1	.3	.3	36	.06	.064	7	8.9	.17	69	.087	<1	2.93	.011	.05	.2	.04	1.6	.1	.06	10	<.5
L1940 1050S	1.4	12.8	15.4	49	.1	9.9	7.0	257	2.45	5.1	.7	2.6	4.4	6	.1	.2	.4	41	.05	.059	9	9.2	.21	73	.099	<1	2.58	.012	.05	.2	.06	1.6	.1	.11	10	<.5
L1940 1075S	1.4	15.2	15.4	60	.2	7.6	4.9	214	2.33	5.5	.9	2.6	4.2	14	.2	.3	.4	43	.16	.099	7	10.1	.16	76	.119	2	2.93	.014	.06	.3	.08	1.5	.1	.12	10	<.5
L1940 1100S	.8	12.6	12.8	49	.1	9.5	5.2	134	2.25	4.6	.7	2.5	5.6	5	.1	.2	.3	38	.04	.084	12	11.2	.25	66	.060	<1	2.61	.010	.04	.1	.05	1.9	.1	<.05	8	<.5
L1940 1125S	.9	17.8	9.8	45	<.1	12.9	6.9	180	2.25	5.7	.8	2.9	5.9	4	.1	.3	.3	31	.03	.058	16	13.3	.38	57	.024	1	2.23	.004	.03	.1	.03	1.7	.1	<.05	5	<.5
L1940 1150S	1.0	9.1	10.8	32	<.1	7.3	4.0	184	2.11	4.4	.4	2.2	4.6	5	.1	.2	.4	34	.04	.030	20	10.0	.21	58	.044	1	1.71	.006	.05	.2	.04	1.4	.1	<.05	8	<.5
L1940 1175S	1.1	15.9	13.4	52	.1	11.0	6.6	283	2.38	4.4	.6	3.4	4.6	6	.1	.2	.4	39	.05	.069	11	11.8	.23	91	.098	1	2.83	.010	.06	.2	.03	2.1	.1	<.05	10	<.5
L1940 1200S	.9	13.5	11.9	39	.1	9.2	5.9	364	1.93	3.9	.6	2.4	3.8	5	.1	.2	.4	36	.04	.059	10	8.8	.17	66	.087	<1	2.36	.011	.04	.1	.06	1.4	.1	.06	9	<.5
L1940 1225S	1.0	18.3	13.3	53	.1	10.3	8.0	449	2.45	5.1	.7	3.5	5.0	5	.1	.2	.5	42	.04	.076	11	11.3	.19	75	.098	<1	2.69	.011	.06	.1	.05	1.9	.1	.06	9	.5
L1940 1250S	1.4	18.9	12.9	44	.1	14.3	10.5	272	2.96	9.8	1.0	28.5	7.1	5	.1	.5	.6	35	.04	.049	20	10.8	.35	71	.046	<1	2.07	.004	.04	.2	.04	1.8	.1	<.05	8	<.5
L1940 1275S	1.2	20.8	11.9	40	.1	15.9	12.0	209	2.81	7.4	1.1	45.4	8.0	5	.1	.3	.5	30	.03	.049	20	11.7	.33	65	.039	<1	2.08	.004	.04	.1	.04	1.4	.1	<.05	5	<.5
L1940 1300S	1.0	10.7	12.3	45	.1	10.7	9.9	578	2.74	6.3	.6	18.5	5.3	5	.1	.3	.5	35	.05	.037	19	10.5	.20	67	.059	3	1.60	.006	.04	.1	.06	1.4	.1	<.05	8	<.5
L1940 1325S	1.1	12.1	12.6	42	.1	12.7	10.0	385	2.76	5.3	.6	67.4	6.3	7	.1	.2	.5	40	.07	.052	18	12.1	.19	105	.075	1	2.20	.008	.05	.2	.04	1.6	.1	<.05	8	<.5
L1940 1350S	1.1	9.1	13.5	40	.2	10.4	7.1	336	2.80	4.6	.6	8.8	5.6	5	.1	.3	.5	38	.05	.053	18	11.9	.19	72	.065	<1	1.74	.007	.05	.2	.06	1.3	.1	<.05	9	<.5
L1940 1375S	.8	10.5	14.8	51	.1	11.3	8.3	410	2.24	6.7	.6	191.2	5.6	7	.2	.3	.5	27	.05	.048	21	9.3	.23	67	.055	<1	1.80	.007	.04	.1	.03	1.2	.1	<.05	7	<.5
L1940 1400S	1.6	11.9	20.0	53	.1	15.7	13.7	341	3.12	8.3	1.1	80.9	7.3	5	.1	.3	.7	36	.05	.059	19	11.4	.25	102	.083	3	2.27	.008	.06	.2	.04	1.9	.1	<.05	9	<.5
L1940 1425S	.9	23.7	21.6	83	.1	15.7	9.4	1138	2.52	5.2	1.0	37.4	6.7	4	.1	.3	.5	26	.04	.046	19	15.1	.53	87	.057	1	2.11	.005	.03	.1	.03	1.8	.1	.06	6	<.5
L1940 1450S	1.5	18.9	34.3	107	.3	13.8	15.9	2206	2.71	5.6	.6	13.3	2.2	12	.4	.5	.5	34	.11	.061	15	10.3	.22	88	.083	<1	1.65	.008	.07	.1	.06	1.2	.2	<.05	8	<.5
L1940 1475S	1.7	20.3	41.3	118	.2	13.4	15.7	3448	2.75	4.8	.6	3.8	3.2	14	.4	.5	.6	41	.19	.059	14	14.3	.30	136	.101	2	1.76	.014	.08	.1	.07	1.6	.2	<.05	9	<.5
L1940 1500S	.8	14.4	21.2	130	.1	12.3	10.5	2930	2.16	3.3	.5	4.2	3.1	11	.5	.2	.4	37	.12	.072	9	9.6	.15	132	.121	<1	2.36	.015	.05	.2	.04	1.5	.2	<.05	10	<.5
RE L1940 1500S	.8	13.9	21.8	127	.2	11.2	10.2	3062	2.00	3.1	.6	2.5	3.1	11	.5	.3	.4	32	.11	.071	10	9.0	.15	146	.116	2	2.27	.013	.05	.1	.05	1.3	.2	<.05	9	<.5
L1940 1525NW	.7	12.5	20.4	97	.2	9.8	8.8	772	2.25	4.2	.6	1.3	2.6	7	.2	.3	.4	38	.07	.073	7	9.9	.14	74	.124	1	2.38	.011	.06	.1	.05	1.5	.1	<.05	10	<.5
L1940 1550NW	1.1	32.6	36.1	121	.4	21.7	12.8	1295	2.38	4.6	1.2	16.2	5.3	9	.4	.3	.4	31	.10	.085	13	12.4	.28	99	.108	<1	3.10	.010	.07	.2	.07	2.1	.1	<.05	8	<.5
L1940 1575NW	1.2	15.7	23.9	134	.4	15.0	9.9	1702	2.68	4.4	.8	2.5	3.9	8	.2	.3	.5	35	.07	.087	12	12.5	.24	103	.105	4	2.57	.009	.08	.2	.05	1.3	.2	<.05	9	<.5
L1940 1600NW	1.1	18.2	23.6	127	.1	17.1	14.8	1960	2.46	4.5	.7	3.2	3.3	19	.3	.3	.5	31	.19	.089	15	12.6	.32	119	.078	6	2.38	.007	.12	.2	.05	1.4	.2	<.05	8	<.5
L1940 1625NW	1.2	18.1	19.9	90	.2	16.6	11.4	693	2.37	5.0	.9	4.7	5.2	8	.2	.2	.5	31	.06	.067	12	11.9	.25	121	.104	1	3.18	.010	.06	.1	.06	1.8	.2	<.05	8	.5
L1940 1650NW	.9	18.9	23.2	118	.1	22.8	13.3	1472	2.52	4.9	.8	2.4	4.8	23	.4	.3	.4	33	.26	.090	13	12.6	.30	159	.127	4	3.15	.014	.10	.2	.03	1.8	.2	<.05	9	.5
L1940 1675NW	.7	19.7	20.8	113	.1	22.8	12.2	294	2.44	2.9	.6	10.1	5.8	10	.1	.2	.4	25	.10	.045	19	14.4	.44	92	.079	<1	2.11	.007	.09	.1	.01	1.5	.2	<.05	7	<.5
L1940 1700NW	1.1	25.7	25.4	155	.1	25.2	17.8	3983	2.77	3.8	.8	13.8	3.4	17	.4	.3	.5	34	.19	.084	18	13.0	.36	246	.094	4	2.74	.012	.12	.1	.06	1.7	.2	.08	9	.6
L1940 1725NW	1.2	20.5	40.2	180	.2	24.4	18.6	3418	2.63	5.3	1.0	3.6	4.0	18	.6	.5	.5	36	.22	.119	13	13.4	.28	163	.124	7	2.85	.012	.10	.1	.06	1.7	.2	<.05	10	<.5
L1940 1750NW	1.4	12.2	21.2	194	.1	21.7	13.6	1229	2.49	3.1	.7	1.9	3.3	15	.3	.3	.5	35	.19	.072	11	12.5	.27	157	.122	1	3.20	.013	.08	.1	.07	1.4	.2	.08	10	<.5
L1940 1775NW	1.3	17.4	29.7	139	.2	20.4	15.3	1348	2.47	3.4	.9	1.8	4.1	20	.5	.2	.5	33	.18	.066	14	11.7	.31	188	.108	3	2.56	.011	.09	.1	.06	1.8	.2	<.05	8	<.5
L1940 1800NW	1.4	17.2	22.0	133	.2	21.4	14.2	542	2.49	4.6	1.0	3.4	5.4	8	.1	.3	.5	30	.07	.068	13	11.4	.30	108	.118	<1	3.34	.011	.06	.2	.07	1.7	.1	<.05	9	<.5
L1940 1825NW	1.1	14.5	20.3	143	.1	20.6	13.7	259	3.12	4.9	.8	3.2	5.2	7	.1	.3	.5	36	.10	.089	14	13.6	.33	81	.107	<1	2.73	.009	.07	.2	.04	1.4	.1	<.05	10	<.5
STANDARD DS5	12.4	139.4	24.3	131	.3	23.2	11.9	770	2.88	18.0	6.1	43.1	2.8	52	5.7	4.0	6.3	61	.75	.099	12	179.2	.68	137	.101	16	2.07	.034	.14	4.6	.17	3.2	1.0	<.05	7	4.7

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data K FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.6	2.7	2.1	42	<.1	4.6	4.1	563	2.00	<.5	1.8	<.5	4.2	87	<.1	<.1	.1	39	.54	.074	10	15.3	.51	251	.126	1	.93	.090	.45	2.3	<.01	2.3	.3	<.05	4	<.5
L1940 1850NW	1.3	6.8	17.6	54	.1	7.8	4.7	143	2.01	2.6	.4	3.5	3.5	6	.1	.2	.4	31	.08	.024	13	8.6	.15	63	.060	1	1.39	.008	.05	.1	.02	1.1	.1	<.05	8	<.5
L1940 1875NW	1.0	11.0	11.2	81	.2	9.3	8.0	845	1.95	3.0	.8	2.4	4.0	6	.2	.1	.3	30	.05	.178	8	9.9	.16	105	.112	2	3.03	.019	.05	.2	.05	2.3	.1	<.05	9	<.5
L1940 1900NW	1.2	8.2	12.8	59	.1	9.3	5.6	388	2.29	3.3	.4	41.0	3.8	8	.1	.2	.5	36	.06	.045	16	11.7	.23	87	.099	2	1.36	.010	.06	.2	.04	1.6	.1	<.05	10	<.5
L1940 1925NW	1.5	5.4	9.8	29	.1	5.9	3.9	119	1.81	2.1	.3	3.0	3.8	7	.1	.2	.4	27	.09	.025	19	8.4	.18	50	.026	<1	1.16	.006	.04	.1	.02	1.1	.1	<.05	6	<.5
L1940 1950NW	.6	12.9	10.1	37	<.1	11.7	6.8	161	2.00	3.8	.9	18.6	7.2	3	<.1	.2	.3	11	.02	.028	21	8.9	.34	54	.020	1	1.24	.003	.04	.1	.02	1.1	<.1	<.05	4	<.5
L1940 1975NW	1.3	12.7	14.2	55	.1	11.9	8.3	492	2.51	4.6	.7	8.2	4.6	6	.1	.3	.4	28	.07	.041	18	11.4	.29	82	.064	<1	1.99	.009	.06	.1	.03	1.5	.1	<.05	9	<.5
L1940 2000NW	1.4	12.5	11.4	45	.1	13.2	7.6	166	2.18	5.2	.8	8.7	5.8	5	.1	.2	.3	25	.04	.069	13	10.5	.26	74	.079	1	3.16	.010	.05	.2	.05	1.9	.1	<.05	7	<.5
L1940 2025NW	1.0	14.3	10.7	47	.1	14.0	10.8	292	2.29	4.4	.9	4.8	6.5	5	.1	.2	.3	21	.04	.059	15	10.0	.31	90	.051	<1	2.72	.009	.04	.2	.04	2.0	.1	<.05	7	<.5
L1940 2050NW	.7	9.9	9.6	41	<.1	15.2	11.8	281	1.55	1.8	.8	42.2	4.8	8	<.1	.1	.3	14	.05	.016	21	8.7	.32	66	.023	<1	1.24	.007	.04	.1	.01	1.0	<.1	<.05	4	<.5
L1940 2075NW	.9	12.2	9.5	38	.1	11.4	9.1	112	1.89	3.8	.7	1.3	4.6	5	.1	.2	.3	21	.04	.051	10	9.1	.21	95	.071	1	2.50	.012	.04	.2	.05	1.8	.1	<.05	7	<.5
L1940 2100NW	1.0	10.0	12.7	35	.1	8.1	6.0	208	2.23	5.2	.7	6.6	4.7	6	.1	.2	.4	30	.04	.065	9	9.9	.15	75	.081	1	2.73	.012	.04	.1	.05	1.7	.1	<.05	9	<.5
RE L1940 2100NW	1.0	9.6	12.6	34	.1	7.8	5.8	192	2.11	5.2	.6	3.2	4.6	6	.1	.3	.3	29	.04	.071	9	9.9	.16	74	.083	1	2.84	.013	.05	.2	.05	1.8	.1	<.05	9	<.5
L1940 2125NW	1.2	15.4	11.7	34	.1	7.1	4.8	195	2.23	4.4	1.2	2.0	3.9	6	.1	.3	.3	35	.05	.119	4	9.0	.10	62	.148	2	4.38	.017	.03	.2	.06	2.7	<.1	<.05	11	<.5
L1940 2150NW	.4	7.4	7.4	47	<.1	8.7	5.6	106	1.51	1.6	.6	1.4	5.6	2	<.1	.1	.2	13	.02	.029	22	9.1	.31	53	.015	<1	1.37	.003	.04	.1	.02	1.2	<.1	<.05	3	<.5
L1940 2175NW	.8	9.5	11.3	38	.1	6.4	4.0	188	1.84	2.7	.5	5.5	3.5	5	.1	.2	.3	31	.04	.057	11	8.2	.11	89	.045	1	1.97	.011	.04	.1	.03	1.6	.1	<.05	8	<.5
L1940 2200NW	.9	9.3	11.1	42	.1	8.5	4.7	112	3.00	4.3	.7	1.7	5.4	3	.1	.2	.3	28	.03	.076	14	12.5	.22	44	.049	<1	2.14	.007	.04	.2	.04	1.6	.1	<.05	8	<.5
L1940 2225NW	1.2	8.9	18.8	38	.2	8.1	4.2	118	2.38	4.2	.8	2.6	4.5	7	.1	.2	.4	37	.06	.064	9	10.9	.16	83	.080	<1	2.47	.010	.05	.2	.07	2.0	.1	<.05	11	<.5
L1940 2250NW	.5	5.5	14.1	35	<.1	7.7	5.6	152	1.35	1.6	.4	3.7	3.6	7	<.1	.1	.3	17	.07	.015	19	9.4	.26	70	.023	<1	1.06	.006	.04	.1	.01	1.1	.1	<.05	4	<.5
L1940 2275NW	.7	8.7	14.3	53	.1	10.6	6.7	274	2.34	3.1	.6	.7	4.7	8	.1	.1	.4	29	.07	.039	19	13.2	.30	96	.043	<1	1.53	.006	.06	.1	.01	1.3	.1	<.05	7	<.5
L1940 2300NW	.8	8.3	14.0	49	.1	9.8	5.3	134	2.44	4.1	.7	3.6	4.8	7	.1	.2	.3	26	.05	.042	22	12.3	.32	71	.029	<1	1.62	.004	.05	.1	.02	1.4	.1	.06	7	<.5
L1940 2325NW	.4	7.9	12.0	37	.1	8.6	5.4	119	1.57	1.7	.6	1.0	4.0	7	.1	.1	.3	19	.05	.016	23	10.7	.31	68	.023	<1	1.14	.006	.04	.1	.01	1.2	.1	<.05	5	<.5
STANDARD DS5	13.1	142.0	24.7	140	.3	24.7	11.7	795	3.02	18.8	6.2	44.3	2.7	51	6.1	3.8	6.0	61	.72	.093	13	177.5	.65	147	.097	16	2.09	.034	.13	5.0	.17	3.7	1.0	<.05	7	5.1

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data A FA ___

49:26:32.80 N
116:38:10.20 W

563500 564500 565500 566500 567500 568500 569500 570500 571500

5476000 5475000 5474000 5473000 5472000 5471000 5470000

49:26:28.80 N
115:59:59.70 W

True North
Magnetic North

OLD BALDY MOUNTAIN

Galloway Creek

Weaver Creek

Contour Soil Geochem Lines
1940
1860

OLD BALDY FAULT

AC FAULT

Prospector's Dream Area

M.C.'s.

Blk. D
MOYIE RIVER
TIE RESERVE NO. 1

Contour Soil Geochem Line 1650'

HILL VEIN FAULT

SL 10

Creek

REC5080

MC2 Area

Hill Vein Area

Weaver Cr.

Ryder Creek

Moyie River

Moyie Creek

0 500 1000 1500m
SCALE 1:10,000

LEGEND

	Bedding	Hc	Creston Formation
	Cleavage, shearing	Ha	Aldridge Formation
	Fracturing		Gabbro
	Jointing		Trench
	Quartz Vein		Fault

Ruby Red Resources Inc.

EDDY PROJECT

SURFACE GEOLOGY
Showing location of
Contour Soil Geochem Lines

Scale: 1:10,000	Figure: 3
Date:	Datum: Nad 83
Mapsheets: 082F040/50	

49:22:13.80 N
116:00:14.5

568500 569000 569500 570000 570

568000 5476000N

True North

Magnetic North

547 5500 N

5475000N

5474500 N

2000 1900 1800 1700 1600

LINE 1940

LINE 1860

Weaver

0 100 200 300
meters

Figure 6. Eddy Property
Contour Soil Geochem Lines
SHOWING GOLD IN PPB
Scale 1;5000
For Location see Fig. 3