ASSESSMENT REPORT
on
GEOLOGICAL MAPPING
ROCK & SOIL GEOCHEMISTRY
VLF-EM GEOPHYSICS

Loose Leg and Lead Leg Mineral Claims

Lewis Creek and Tracy Creek Area
Fort Steele Mining Division

TRIM 82G.072 & 082
599500 E 5517000 N

Operator
Ruby Red Resources
Suite 207 239 - 12th Ave SW
Calgary, Alberta, T2P 1H6

Owners
Ruby Red Resources
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1.00 INTRODUCTION

1.10 Location and Access

The Loose Leg property is located in the Fort Steele Mining Division approximately 25 km northeast of Cranbrook, B.C., between upper Lewis Creek and the Rocky Mountain Trench (Fig. 1). Access is via forestry roads up Lewis Creek and an old road up Tracy Creek.

1.20 Property

The Loose Leg property includes 38 claim units in the Loose Leg, Lead Leg, Lead Leg 2 and Lead Leg 3 mineral claims (Fig. 2). The claims are owned by Ruby Red Resources Inc. and Gregory Ewonus of Calgary, Alberta.

1.30 Physiography

The Loose Leg property is located east of the Rocky Mountain Trench in the Hughes Range of the Rocky Mountains and straddles the ridge between the north-flowing upper part of Lewis Creek and the trench. Topography is generally steep with mainly wooded and locally rocky slopes. Elevation ranges from 1060 to 2060 meters. Forest cover includes mainly pine, fir and larch. Small parts of the claim block have been logged and are in various stages of regeneration.

1.40 History

A number of old workings are present on the the claim block, developed mainly on poly-metallic but mainly galena-bearing quartz veins. In 2002 a program of prospecting and rock geochemistry was conducted on the claims (Rodgers and Kennedy, 2002) with anomalous gold detected at a number of localities. In 2003 minor geologic mapping was completed and one area was explored with three lines of contour soil geochemistry (Klewchuk, 2004)

1.50 Purpose of Exploration Program

In 2004 work was focused on and near the Tracy Creek drainage. A series of UTEM geophysics anomalies previously detected by Cominco Ltd. were surveyed in more detail using VLF-EM, to determine the continuity and near-surface variability of the anomalies. Four soil lines were sampled, one on each side of Tracy Creek and two across the Fort Steele Formation north of Tracy Creek, to evaluate these areas for bedrock mineralization.

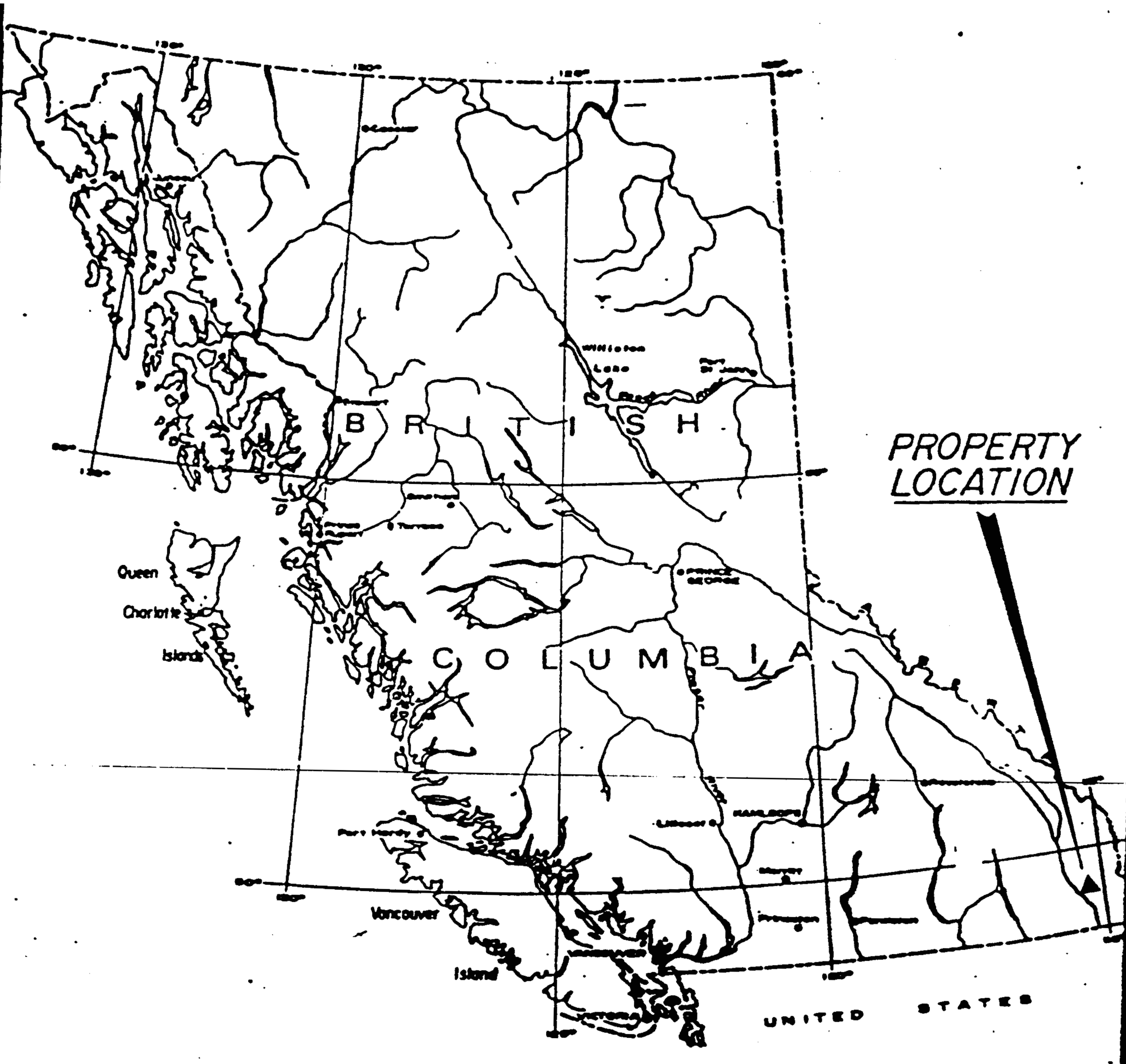

Figure 1
Loose Leg Property Location

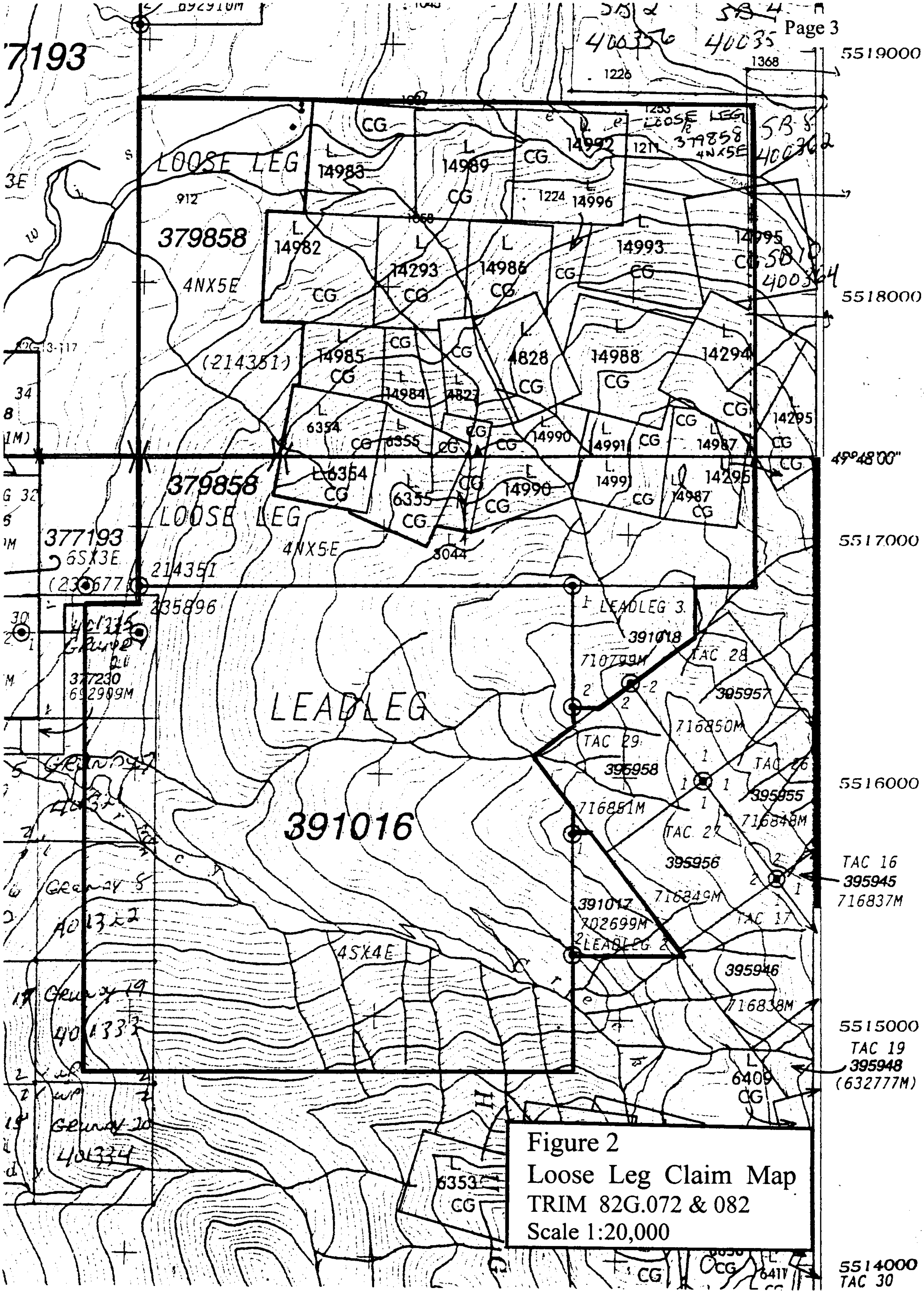

Figure 2
Loose Leg Claim Map
TRIM 82G.072 & 082
Scale 1:20,000

2.00 GEOLOGY

Stratigraphy

The Loose Leg property is underlain by mesoproterozoic Purcell Supergroup rocks of the Fort Steele and Aldridge Formations. These rocks are described by Hoy (1993):

> Purcell Supergroup rocks in Fernie west-half are exposed in the Purcell Mountains and the Hughes, Lizard and Galton ranges east of the trench. Throughout the Purcell Mountains , formations are generally thick, contacts between them are gradational, and lateral facies or thickness changes are gradual. However in the northern Hughes Range the lower part of the Purcell Supergroup is markedly different, with predominantly fluvial, alluvial fan and deltaic deposits at the base, overlain by a relatively thin and heterogeneous Aldridge succession. Facies and thickness changes within the Aldridge Formation are pronounced here indicating influence of syndepositional faults or growth faults. A thick succession of turbidites, interlayered with gabbroic sills, was deposited to the south and west. The transition between these contrasting facies marks the edge of the Purcell basin in early Purcell time. The tectonic disturbance recorded in these rocks continued intermittently near the basin edge during deposition of younger, generally shallow-water sediments.

The Fort Steele Formation is exposed along the western edge of the Loose Leg property and is described by Hoy as:

> The Fort Steele Formation comprises predominantly cross-bedded and massive quartz arenite, quartz and feldspathic wacke and siltstone, interpreted to be primarily deposits of a braided fluvial system. The formation is characterized by thick sections of massive and crossbedded quartz arenite and a number of large fining-upward cycles, termed megacycles, that are several hundred meters thick. Fine-grained siltstone and argillite facies are not abundant, comprising less than 10 per cent of the total exposed succession. These are interpreted to be alluvial fan and fan-delta deposits.

The Aldridge Formation overlies the Fort Steele Formation on the Loose Leg property. The lower part of the Aldridge Formation is divided by Hoy (1993) into six distinctive units, A1a to A1f. These units are further described by Hoy:

> The basal member of unit A1 (A1a) ... consists of medium to dark grey to black, finely laminated argillite and siltstone. Flaser and lenticular bedding occur occasionally and graded siltstone-argillite couplets up to 3 centimeters thick may define bedding. Its basal part is generally coarser grained and may include minor quartz wacke, siltstone and wacke with dolomitic cement.

A1b is a conspicuous unit, from 20 to more than 100 meters thick, characterized by abundant carbonate and referred to as the "carbonate marker unit". It consists primarily of interlayered silty or argillaceous dolomite, dolomitic argillite or siltstone interbedded on a 2 to 3 meter scale. Dolomitic layers are brown weathering, commonly finely laminated and may contain isolated mound-shaped stromatolites or cryptal algal mat deposits. Lenticular beds, crossbeds, scours and ripple marks are common within siltstone or dolomitic siltstone. Grey limestone, interbedded with dolomite, is prominent near the top of Unit A1b just north of Wasa Creek; thinly interbedded chert and dolomite, and pods of brown-weathering dolomite in siltstone are occasionally present.

Unit A1b grades upward into A1c, a succession of interbedded argillite and siltstone. South of Lewis Creek, A1c can be subdivided into three subunits. These include a massive to faintly laminated black graphitic argillite, overlain by a lighter coloured grey, greenish grey or tan, finely laminated siltstone or silty argillite and, finally, a medium to dark grey, rusty weathering, massive to faintly laminated argillite. Rusty weathering dolomite pods, minor calcareous argillite and rare, thin silty quartzite layers occur locally within the two upper subunits.

Unit A1d is a distinctive unit south of Lewis Creek that hosts both the Kootenay King and Estella lead-zinc deposits. It consists largely of buff-weathering dolomitic siltstone interlayered with buff to grey, finely laminated argillite. Sedimentary structures, including lenticular bedding, flaser bedding, tangential crossbedding and graded siltstone-argillite couplets, commonly with flame or load casts at their base, are conspicuous. To the south, the unit becomes a coarser grained tan siltstone or wacke with only minor argillite or dolomitic siltstone. To the north it changes to a dark, finely laminated argillite with only minor interbedded siltstone. Contacts with underlying argillite of unit A1c and overlying, generally dolomite-free siltstone and argillite of Unit A1f are gradational across many tens of meters.

Unit A1f comprises siltstone and argillite with minor dolomitic siltstone and occasional wacke and quartz arenite beds. Graded bedding is common and ripple crosslaminations, lenticular bedding and mud-chip breccias occur in the middle and upper parts of the unit. The contact with the overlying middle Aldridge is placed at the base of the first, prominent, thick-bedded quartz wacke turbidite sequence.

A number of thick, massive to faintly laminated quartz arenite or quartz wacke beds (referred to as 'quartzites' and mapped as Unit A1e) occur within A1d and less commonly within A1c.

Middle Aldridge Formation rocks exposed in the southwest corner of the claim block include grey to rusty weathering quartz wacke and siltstone interbedded with silty argillite.

Geologic mapping in 2003 was focused on the northern portion of the claim block (i.e. mainly on the Loose Leg mineral claim). A normal stratigraphic sequence is present with Fort Steele Formation quartzites and siltstones at the northern and northeastern edges of the property. Overlying A1 stratigraphy occurs above the Fort Steele Formation with middle Aldridge turbidites present on the Estella Mine road north of Tracy Creek. In 2004 mapping focused on the upper contact of the Fort Steele Formation, where a fault is interpreted north of Tracy Creek.

Structure

Limited geologic mapping and poor bedrock exposure has hindered understanding structure of the Loose Leg property in detail. What appears to be a low angle fault occurs along the eastern boundary of the Loose Leg mineral claim. Two adits are developed in or near this structure, and have galena and chalcopyrite -bearing quartz veining in the dump material. Seven samples collected from the adits in2003 have up to 713 ppb Au / tonne and a sample from a large fault zone about 230 m south of the adits returned 706 ppb Au (Klewchuk, 2004). A number of northwest-striking high angle faults recognized on the property host galena-bearing quartz veining which has been the focus of previous exploration activity in the form of numerous adits. In some cases bedrock exposures are insufficient to place confidence in defining a specific geologic unit and local unresolved structural complexities may well be present. The northwest-striking faults offset units of stratigraphy but with apparent minor vertical displacement.

Mapping in the Tracy Creek area in 2003 identified a fault between Fort Steele Formation and overlying Aldridge Formation. The fault is indicated by local folding within the eastern-most exposed Fort Steele rocks just north of Tracy Creek. More recessive middle Aldridge stratigraphy to the east is poorly exposed. The fault zone is also supported by a limited VLF-EM survey, also done in 2004. East-west bedding immediately north of Tracy Creek near 598250E may be related to the Tracy Creek Fault.

It appears the area of the Loose Leg property has been tectonically active in both Proterozoic and Cretaceous times.

Intrusions

Narrow Proterozoic age gabbroic Moyie Sills or dikes occur within the upper units of Aldridge A1 stratigraphy. Two small gabbro sills (dikes?) were mapped in 2003 along the Estella road. Gabbro float was noted at a few other localities indicating there are a number of small gabbro intrusions present.

Cretaceous age felsic intrusions, which appear to be syenites, intrude the sedimentary rocks on the Loose Leg property as narrow dikes and sills, and as matrix to breccias. Earlier prospecting defined widespread breccias on the property but geologic mapping has covered only a few of these occurrences although syenite float was observed in a number of localities (see Klewchuk, 2004) including areas underlain by Fort Steele Formation quartzites within the drainage of Tracy Creek. The bulk of the syenite float occurs near the contact of Fort Steele Formation and overlying Aldridge A1 stratigraphy. The competency contrast between the massive and brittle

Fort Steele Formation quartzites and overlying more distinctly bedded A1a sediments may have focused this felsic intrusion activity. Some syenite float was also noted near the A1b - A1c boundary near 9400E 7430N. Felsic intrusions may be related to the Estella stock (a short distance south of the Loose Leg claim group) which has been dated at 115 Ma (Hoy, 1993). The presence of syenite and felsite float just above and north of Tracy Creek indicates that these felsic intrusions are associated with the Tracy Creek Fault

Anomalous gold which is present near syenite intrusions suggests a genetic relationship between the syenites and gold.

A series of narrow carbonate-altered mafic dikes, which are probably Cretaceous in age, have been identified across much of the property and are commonly within northwest structures. Similar intrusions are known to be present on nearby claims where anomalous gold is also present, supporting a genetic relationship between these mafic dikes and gold mineralization. These mafic dikes tend to be elevated in cobalt and nickel and may reflect a deep parent magma. Widespread elevated cobalt and nickel values in rocks and soils collected on nthe property probably reflect the presence of these dikes.

Mineralization

Anomalous gold mineralization has been identified at a number of localities and within different host rocks on the Loose Leg property. Gold occurs with quartz veins, quartz-dolomite veins, base metal -bearing quartz veins, in fault zones and in limonite breccia. Some of these occurrences are exposed by old workings which typically were driven on base metal (lead, zinc and copper) - bearing quartz veins and are hosted by Fort Steele Formation quartzites, A1b and A1c stratigraphy . The adits appear to be close to fault structures which have not been exposed by the workings. Quartz veins and quartz vein breccia zones exposed in the workings tend to be developed parallel or sub-parallel to the host stratigraphy. Many of the quartz veins and quartz vein breccia zones observed are lensey in character. Most of the workings have visible galena and chalcopyrite with less common sphalerite. Anomalous molybdenum, silver and gold are also present. These workings were sampled during a prospecting program in 2002 and were reported on by Rodgers and Kennedy (2002).

3.00 GEOCHEMISTRY

3.10 Rock Geochemistry

Twenty-three rock samples were collected as part of the 2003 field program. Rock samples were shipped to ACME Analytical Laboratories at 852 East Hastings Street, Vancouver, B.C., V6A 1R6, and analyzed for a 30 element ICP package and geochemical gold. Sample locations with gold values in ppb and copper in ppm are given in Figure 3; lead, zinc and silver are shown in Figure 4; descriptions of the rock samples are given in Appendix 1 and complete geochemical analyses are in Appendix 2.

Sampling of bedding and cleavage -parallel quartz veinlets and limonitic fractures shows that some of these veins and fractures are mineralized. Cleavage on the property is related to development of a large nappe style fold and the mineralization present in both cleavage and bedding -parallel quartz veins and limonitic fractures suggests mineralization occurred during development of this fold. Larger dilatent zones which developed during the folding are thus prospective targets for finding larger concentrations of mineralization.

Follow-up evaluation of high gold in soils on line 'FS' located a narrow bedding-parallel quartz vein with over 2 grams/tonne gold. This vein may be related to the fault on the eastern margin of the Fort Steele Formation on the property.

Low anomalous gold occurs within a NNW oriented (157/85NE) limonitic fracture zone within Fort Steele quartzites (sample L-32). This zone is parallel to the small stream gullies on the south side of Tracy Creek and, as these may be mineralized structures, additional soils were collected at the small stream gullies but no anomalous gold was detected.

3.20 Soil Geochemistry

A total of 314 soil samples were collected in 2004 on four 'contour' lines; two are roughly N-S lines covering the Fort Steele Formation on the west side of the Loose Leg claim at ~1130m and ~1420m elevation (Lines '1150' and 'FS', respectively. The other two lines roughly parallel Tracy Creek on the north (line 'NT') and south (Line 'ST') sides of the drainage. Lines were run using hand-held GPS for control and sample intervals at 25 meters were measured using a hip-chain. Additional soil samples were collected at stream gulleys on the Line ST south of Tracy Creek.

Soils were collected from the 'B' horizon at an approximate depth of 15 cm, placed in Kraft paper bags, dried and then shipped to ACME Analytical Laboratories at 852 East Hastings Street, Vancouver, B.C., V6A 1R6, and analyzed for a 30 element ICP package and geochemical gold by standard analytical techniques. Soil sample contour lines are shown on Figures 3 & 4; sample sites are marked and values for copper and gold are shown in Figure 3, and lead, zinc and silver values are shown in Figure 4. Results for the three contour lines completed in 2003 are also shown. Complete geochemical analyses for the 2004 soil samples are provided in Appendix 3.

Results for Gold

Gold values in soils are generally below 10ppb, similar to results obtained in 2003. Scattered values above 10ppb are present on all the lines sampled, with local clusters of elevated gold. The soil line north of Tracy Creek has relatively few anomalous gold values with the higher values (70, 78 and 79ppb) associated with the Fort Steele Formation quartzites and its hangingwall fault contact.The line south of Tracy Creek also has scattered lower anomalous gold values with most of these occurring between elevations of 1450 and 1650m. This area includes the upper contact of the Fort Steele Formation quartzites.

The two contour soil lines north of Tracy Creek similarly have widespread weaker anomalous gold values. The upper contour line which is closer to the eastern (fault) contact of the Fort Steele Formation has gold values up to 158 ppb. Higher gold values in this area coincide with some elevated copper, lead, zinc and silver values and may reflect poly-metallic quartz veins like those exposed in old workings about one kilometer northeast of the higher soil values.

Results for Copper

Regionally in the Aldridge Formation a 'threshold' value for copper is about 32 ppm. Weak to moderate anomalous copper occurs in places on the Tracy Creek lines and on contour line 1150 (Fig. 3). Higher copper values on these lines rarely coincide with higher gold values. Higher copper values near the upper part of the south Tracy Creek line do coincide roughly with a broader area of anomalous lead and zinc here.

The highest copper values occur on Line 1150 within the northern third of the line, from about 5516850N to 5517350N. These high copper values correspond with a few higher gold values and an area of high lead, zinc and silver. The soil line here crosses a NW-striking altered young mafic dike, a narrow NE-striking quartz vein breccia with anomalous gold (sample L-03-1 with 596 ppb Au; Klewchuk, 2004), and a syenite dike / breccia complex developed in the upper exposed portion of the Fort Steele Formation quartzites. These features were mapped in 2003. Based on the contour soil sampling done in both 2003 and 2004, this area is more anomalous than that where a suite of historic adits and trenches were dug on base and precious metals ('poly-metallic') -bearing quartz veins near 5517700N 599450E. Further evaluation of this area of anomalous soils on Line 1150 is warranted. The upper contact of the Fort Steele Formation is only a short distance above this soil contour line. The soil geochemistry coverage should be expanded to delineate the uphill extent of the anomaly and resolve whether the source is the Fort Steele Formation quartzites, the overlying Aldridge Formation sedimentary rocks, or a fault at the contact.

Results for Lead, Zinc and Silver

Threshold value for lead within the Aldridge is about 50 ppm with significant anomalous level at about 100 ppm. For zinc, threshold is about 150 ppm and for silver, about 0.2 ppm.

Two areas of anomalous soils are present on the lines sampled in 2004.

One is at the upper end of both lines which parallel Tracy Creek, approximately above 1600m elevation (Fig. 4). On the south side of Tracy Creek this corresponds approximately with the hangingwall (fault?) Contact of the Fort Steele Formation. The Estella ore body is developed along and proximal to a shear / fault zone which strikes northwest and dips southwest. Much of the ore also occurred in sub-parallel, more westerly-striking 'shear strands' in the footwall of the main structure. The anomalous soils of the upper Tracy Creek lines may reflect the northwest extension of the mineralized Estella Fault Zone and its associated footwall structures.

The second area of anomalous Pb-Zn-Ag is on contour line 'FS', at ~1420 m elevation, between about 1400N and 2300N (Fig.4). The highest lead value (9978 ppm), zinc value (420 ppm) and silver value (22.7 ppm) occur within this anomaly. This is the area of the altered mafic dike, quartz vein breccia and syenite matrix breccia mapped in 2003 and indicated above. The altered mafic dike strikes northwest and may be fault-controlled. A short distance to the northeast is the area of workings developed on flat-lying, roughly bedding-parallel 'poly-metallic' quartz veins mapped in 2003. These quartz veins appear to be developed adjacent to NW structures which are similar to the attitude of the Estella ore body and they could be an indicator of Estella-type lead-zinc-silver mineralization. Some of the original workings at the Estella were developed on quartz veins.

4.00 VLF-EM GEOPHYSICS

4.10 Introduction

In 1989 Cominco Ltd. did a UTEM survey in the Tracy Creek area, part of a three year program of UTEM surveying in the Estella area (AR 19,671). Their target was SEDEX mineralization at some depth below surface. Cominco's survey lines were oriented at about 020^0 and spaced approximately 200m apart. The survey detected a series of shallow, moderate to strong UTEM anomalies on both sides of Tracy Creek. The anomalous responses appeared compatible with conductors trending parallel to Tracy Creek. Historic mapping had recognized a WNW-trending fault within and paralleling Tracy Creek, roughly parallel to the Estella fault / shear to the southeast. This fault or any of Cominco's apparently WNW-trending UTEM anomalies could be a host structure for an Estella-type base metal sulfide vein thus a VLF-EM survey was initiated in Tracy Creek to more accurately locate the anomalies and delineate and evaluate them.

Cominco's old UTEM lines were located and, where feasible, were used for the VLF-EM survey. Additional lines were surveyed at 50m spacings, also at an azimuth of 020^0. As the survey progressed, some lines were also surveyed at right angles, at 110^0 (Fig. 5). In addition, the old road paralleling Tracy Creek was also surveyed and results are in Figure 6. A total of 7.1 kilometers of line were surveyed.

4.20 VLF-EM Survey

4.21 Instrumentation and Survey Procedure

The VLF-EM (**V**ery **L**ow **F**requency **E**lectro**m**agnetics) method uses powerful radio transmitters set up in different parts of the world for military communication and navigation. In radio communication terminology, VLF means very low frequency, about 15 to 25 kHz. However, relative to frequencies generally used in geophysical exploration, the VLF technique actually uses very high frequencies.

A Crone Radem VLF-EM receiver, manufactured by Crone Geophysics Ltd. of Mississauga, Ontario, was used for the VLF-EM survey. Seattle, Washington, transmitting at 24.8 kHz and at an approximate azimuth of 247° from the survey area, was used as the transmitting station.

In all electromagnetic prospecting, a transmitter produces an alternating magnetic (primary) field by a strong alternating current usually through a coil of wire. If a conductive mass such as a sulfide body is within this magnetic field, a secondary alternating current is induced within it, which in turn induces a secondary magnetic field that distorts the primary magnetic field. The VLF-EM receiver measures the resultant field of the primary and secondary fields, and measures this as the tilt or 'dip angle'. The Crone Radem VLF-EM receiver measures both the total field strength and the dip angle.

The VLF-EM uses a frequency range from about 15 to 28 kHz, whereas most EM instruments use frequencies ranging from a few hundred to a few thousand Hz. Because of its relatively high frequency, the VLF-EM can detect zones of relatively lower conductivity. This results in it being a useful tool for geologic mapping in areas of overburden but it also often results in detection of weak anomalies that are difficult to explain. However the VLF-EM can also detect sulfide bodies that have too low a conductivity for other EM methods to pick up.

Survey lines on the grid were initially located by using a Garmin 76 hand-held GPS, then run by compass. All survey lines were measured with a hip-chain with VLF-EM readings (field strength and dip angle) taken at 25 meter spacings. Sufficient GPS readings were taken during VLF-EM surveying to provide confidence in plotting all survey lines on the base map.

Results were reduced by applying the Fraser Filter and both dip angle and Fraser Filter values are shown on the survey lines in Figure 5 & 6.

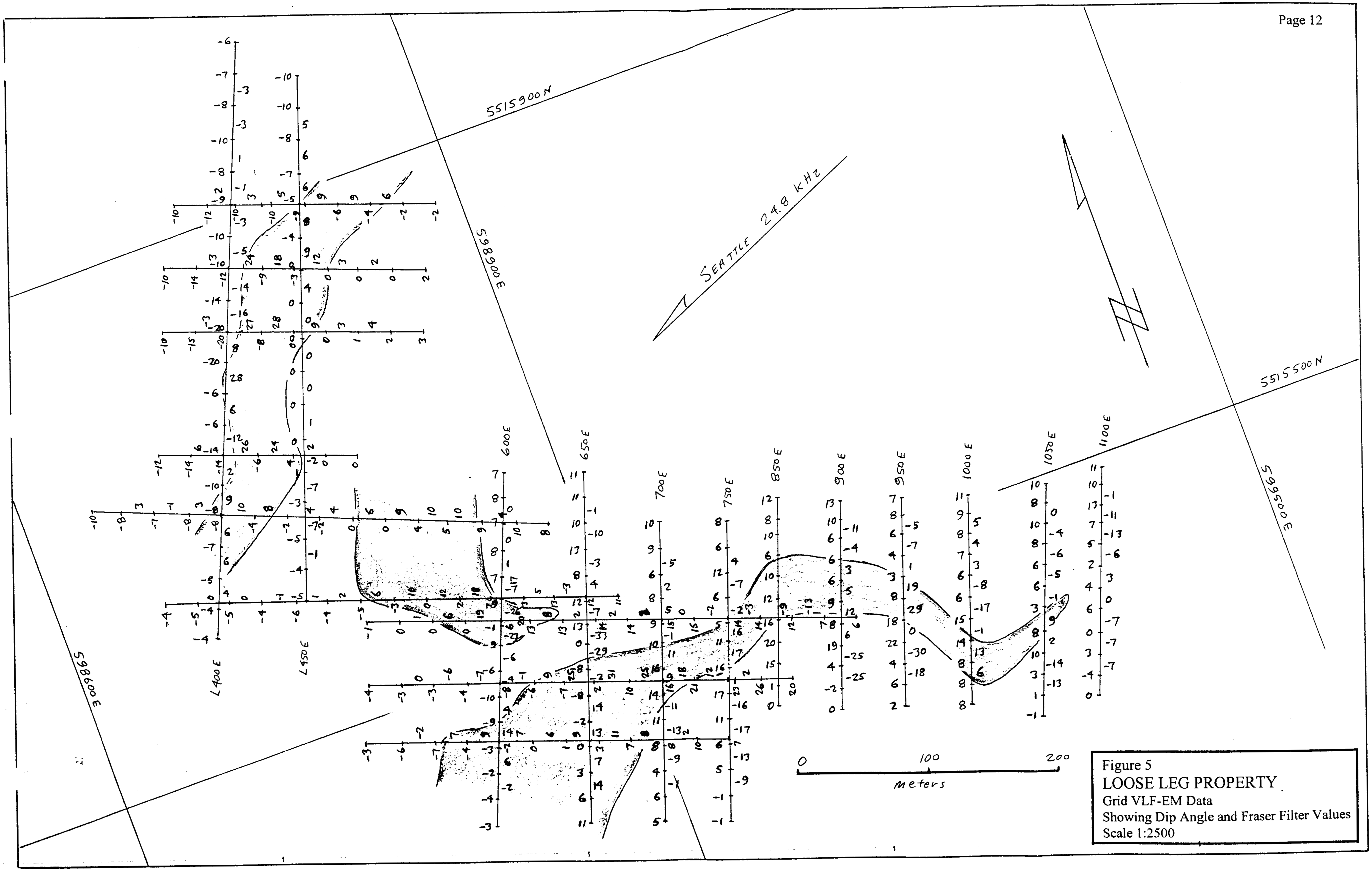

Figure 5
LOOSE LEG PROPERTY
Grid VLF-EM Data
Showing Dip Angle and Fraser Filter Values
Scale 1:2500

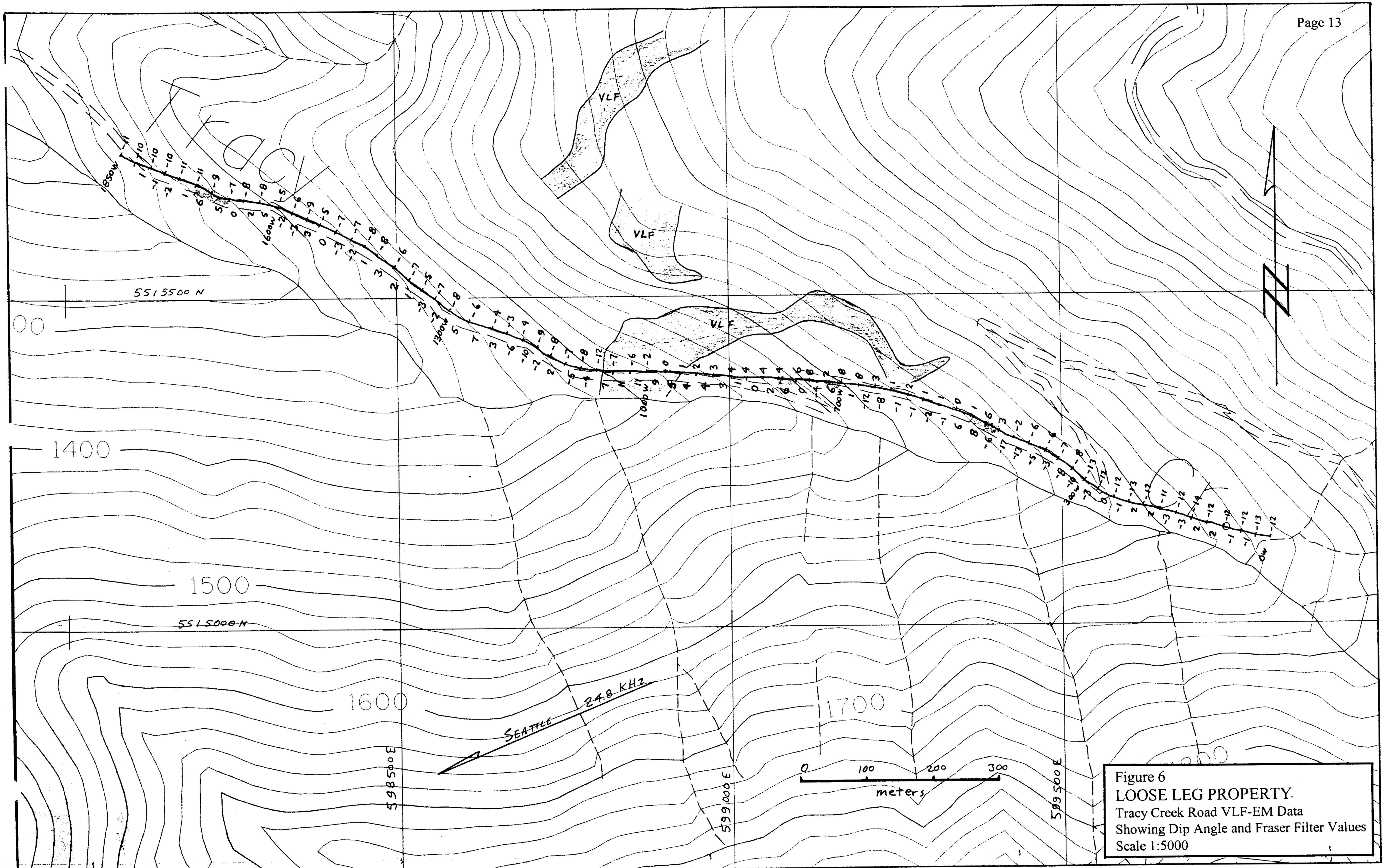

Figure 6
LOOSE LEG PROPERTY
Tracy Creek Road VLF-EM Data
Showing Dip Angle and Fraser Filter Values
Scale 1:5000

The Fraser Filter is essentially a 4-point difference operator which transforms zero crossings into peaks, and a low pass operator which induces the inherent high frequency noise in the data. Thus the noisy, often non-contourable data are transformed into less noisy, contourable data. Another advantage of this filter is that a conductor which does not show up as a zero crossover in the unfiltered data quite often shows up in the filtered data.

4.22 Discussion of Results

An arcuate, east-west oriented VLF-EM anomaly was detected along and north of the Tracy Creek 'road'. The anomaly appears to die out to the east and it broadens and turns to the south at its western, currently detected, extent.

At the northwestern edge of the VLF-EM survey area a NE-striking anomaly coincides approximately with the hangingwall contact of the Fort Steele Formation which here is interpreted to be a fault. This anomaly was traced for just over 500m and remains open at both ends.

Between the E-W and NNE VLF-EM anomalies, a third anomaly was detected; it appears to have a NW to NNE trend but is not well defined.

The two northern anomalies and the western portion of the southern anomaly are 'zero cross-over' anomalies where dip angle rises from negative to positive values. This type of anomaly may be due to an actual conductor rather than just a fault structure.

The soil geochemistry line on the north side of Tracy Creek crosses the southern VLF-EM anomaly; one anomalous gold value of 79ppb is present along with low anomalous copper, lead and zinc values.

The area surveyed by VLF-EM in Tracy Creek may be at the intersection of two structures; the east-west anomaly may be related to the Tracy Creek Fault; the northeast anomaly may be part of a fault structure at the top of the Fort Steele Formation. Additional work is warranted here to further delineate these anomalies and a small soil geochemistry survey should be completed to evaluate possible mineralization associated with the inferred structural intersection.

Two weaker anomalies which were detected on the Tracy Creek road survey should also be delineated because of their proximity to the Tracy Creek Fault.

5.00 CONCLUSIONS AND RECOMMENDATIONS

1. The 2004 soil geochemistry survey on the Loose Leg property identified a number of widespread, relatively isolated weak to moderate anomalies as well as two areas where anomalous copper, lead, zinc, silver and weaker gold are concentrated. Both these areas warrant additional work as the soil geochemistry results may reflect Estella-type vein sulfide mineralization.

2. Limited geologic mapping indicates a fault at the top of the Fort Steele Formation. This may be a low-angle structure that underlies a large portion of the Loose Leg claim block. Syenite breccias developed at the upper contact of the Fort Steele Formation in areas previously mapped on the property may also reflect this fault structure.

3. Multi-gram gold exists within bedding-parallel quartz veins within the Fort Steele Formation quartzites. Such veining may emanate from large fault structures such as the fault which forms the east contact of the Fort Steele Formation on the Loose Leg property.

4. VLF-EM surveying delineated three anomalies which may be at the intersection of two significant faults. The more detailed VLF-EM surveying completed in 2004 indicates that the picture is more complex than the simple one of WNW-oriented conductors provided by Cominco's earlier UTEM geophysics survey of the area . Further evaluation of these structures should be done as the higher grade gold seen in rock samples may be related to one of them.

6.00 REFERENCES

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Klewchuk, P., 2004, Assessment report on geologic mapping, rock and soil geochemistry, Loose Leg and Lead Leg mineral claims, Lewis Creek and Tracy Creek area, Fort Steele Mining Division, BC Assessment report #

Rodgers, G.M., and Kennedy, C., 2002, Prospecting and Geochemical report, Loose Leg and Lead Leg mineral claims,Wild Horse Creek area, Fort Steele Mining Division, BC Assessment Report #26976.

6.00 STATEMENT OF EXPENDITURES

Collection and analysis of 314 soil samples @ $19.81 / sample	$6220.00
Preparation and analysis of 23 rock samples @ $20.00	460.00
Field Work (Geol., geophys) 10 days @ $375.00 / day	3750.00
4X4 vehicle 10 days @ $85.00 / day	850.00
VLF-EM rental 5 days @ $30.00/day	150.00
Report 2 ½ days @ $375.00 / day	937.50
Report and field supplies	74.00
Total cost	$12,441.50

7.00 AUTHOR'S QUALIFICATIONS

As author of this report I, Peter Klewchuk, certify that:

1. I am an independent consulting geologist with offices at 246 Moyie Street, Kimberley, B.C.
2. I am a graduate geologist with a B.Sc. degree (1969) from the University of British Columbia and an M.Sc. degree (1972) from the University of Calgary.
3. I am a Fellow of the Geological Association of Canada and a member of the Association of Professional Engineers and Geoscientists of British Columbia.
4. I have been actively involved in mining and exploration geology, primarily in the province of British Columbia, for the past 29 years.
5. I have been employed by major mining companies and provincial government geological departments.

Dated at Kimberley, British Columbia, this 15th day of February, 2005.

Peter Klewchuk
P. Geo.

Appendix 1 Description of Rock Samples

Sample No.	UTM Coords	Description
L-20	599788E 5515284N	Chips of thin (½ to 3mm wide) cleavage-parallel granular QV with weathered out coarse pyrite (square pits).
L-21	599788E 5515284N	Irregular, vuggy and somewhat brecciated limonitic veins on bedding planes.
L-22	599605E 5515565N	Thin irregular band of limonite on bedding plane - thin breccia.
L-23	599688E 5515486N	Irregular bedding-parallel limonitic quartz vein breccia.
L-24	599668E 5515486N	Bedding-parallel quartz vein breccia, very limonitic. Sample is of float.
L-25	598826E 5515502N	Limonitic quartz breccia. Both orange and pink-red-brown more hematitic limonite present. Narrow breccia zone is parallel to 030/83W fracture cleavage. Near base of cliffs - more brecciation evident locally.
L-26	598845E 5515518N	Bedrock chips of silicified, argillic breccia with dissem py. Abundant QV, structural complexity.
L-27	598880E 5515512N	Composite of chips from footwall of fault (045/30NW). Limonitic QV with argillic, phyllitic and sericitic alteration.
L-28	598908E 5515513N	QV breccia with dissem py and limonitic-altered carbonate. East side of fault at top of FSQ.
L-29	598658E 5515722N	QV in FSQ. Orange-brown limonitic. Adjacent FSQ is brecciated and weakly to moderately limonitic. Est attitude is 025/60E.
L-30	598643E 5515722N	Limonite breccia at base of cliffs; may be some oxidized py. Very fractured - may be a proximal structure.
L-31	598460E 5516738N	Fracturing at 008/55W, sub-parallel to fault at east edge of FSQ, with massive siderite, possibly other limonite, crystalline quartz.
L-32	599048E 5515150N	Weaker limonite breccia / fracture zone in FSQ. Sample is grab of bits of more limonitic material.

L-33	598686E 5514570N	QV breccia with orange limonite, dissem euhedral py cubes.
L-34		Above soil line FS, 300N. Float quartz in talus in small draw. Abundant pyrite, no wallrock.
L-35		Above soil line FS at ~ 318N. Narrow bedding-parallel QV at base of cliffs. Mostly white quartz, pyrite on margins. Some open space crystals of quartz, local blebs of py.
L-36	598537E 5516080N	Bedding-parallel QV, brecciated with clots of chlorite. Dissem ox py in FSQ seds on margins of QV.
L-37	598590E 5516073N	QV in narrow fault zone at 015/60W. Brecciated quartz with few limonite spots.
L-38	598590E 5516073N	Near vertical (095/ ~90) limonitic fractures with crystalline quartz. Host FSQ is discolored pale yellow-orange.
L-39	598526E 5515761N	Carbonate veins in cleavage at ~112N on soil line FS.
L-40	598044E 5516319N	Float quartz with malachite. On talus. Dissem and patchy fine-grained cpy, mostly concentrated in one vague band in QV.
L-41	598083E 5516571N	Massive white, lensey, bedding-parallel quartz vein within thin bedded siltstone unit. Quartz is fractured at 116/86N. Some weak limonite, dissem py.
L-42	598170E 5515711N	QV-dolomite breccia in talus; float.

ACME AN TICAL LABORATORIES LTD. 852 E. HASTINGS ST. COUVER BC V6A 1R6 PHONE(604)253-3158 FAX(60 53-1716
(ISC 002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Ruby Red Resources Inc. PROJECT LOOSE LEG File # A403185
207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm.	Au* ppb
SI	<1	<1	<3	2	<.3	<1	<1	4	.08	<2	<8	<2	<2	5	<.5	<3	<3	<1	.27	<.001	<1	<1	<.01	6	<.01	<3	.01	1.05	.01	<2	<.5
L 33	2	42	<3	16	<.3	40	18	743	3.17	22	<8	<2	<2	128	<.5	<3	<3	16	5.90	.168	7	35	2.88	44	<.01	<3	.25	.05	.12	<2	1.9
L 34	4	3	4	69	<.3	29	20	493	4.02	2	<8	<2	2	31	.5	<3	<3	12	.16	.114	8	2	.03	41	<.01	<3	.23	.03	.07	2	2.5
L 35	4	214	101	6	3.8	6	4	62	2.22	<2	<8	<2	6	25	<.5	<3	<3	8	.03	.011	23	3	.02	1121	<.01	<3	.14	.01	.12	<2	2335.6
L 36	1	2	3	4	<.3	11	37	83	2.13	<2	<8	<2	3	10	<.5	<3	<3	3	.11	.046	3	1	.22	25	<.01	<3	.52	.11	.04	<2	11.4
L 37	2	5	<3	8	.3	5	2	97	1.00	<2	<8	<2	3	2	<.5	<3	<3	2	.01	.003	6	<1	.02	28	<.01	<3	.14	.01	.11	<2	28.8
L 38	5	170	7	15	<.3	20	1	320	7.09	5	<8	<2	3	6	<.5	<3	<3	8	.07	.054	6	7	.10	33	<.01	<3	.16	.01	.07	<2	4.2
RE L 38	6	170	6	14	<.3	20	1	319	7.08	4	<8	<2	3	6	<.5	<3	<3	8	.07	.055	6	7	.10	33	<.01	<3	.15	.01	.07	<2	3.8
L 39	<1	1	<3	2	<.3	3	2	4303	3.88	4	<8	<2	<2	143	<.5	<3	<3	<1	14.23	.010	6	11	6.74	46	<.01	<3	.06	.01	.06	<2	<.5
L 40	1	6893	42	2	1.1	6	11	16	1.28	2	<8	<2	<2	3	<.5	<3	<3	1	.02	.004	3	<1	.01	4	<.01	<3	.03	.02	<.01	<2	6.8
L 41	4	16	<3	6	<.3	16	5	246	.93	<2	<8	<2	<2	26	<.5	<3	<3	3	.84	.021	4	<1	.29	45	<.01	<3	.04	.01	.03	<2	18.1
L 42	<1	43	<3	13	<.3	18	15	2860	5.27	<2	<8	<2	<2	888	.9	<3	<3	7	10.59	.108	3	<1	4.73	47	<.01	<3	.08	.03	.02	2	10.1
STANDARD DS5/AU-R	13	141	24	135	.3	25	12	750	3.00	17	<8	<2	3	45	5.6	4	6	60	.73	.093	12	190	.67	135	.10	<3	1.98	.04	.14	6	478.0

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-171
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Ruby Red Resources Inc. PROJECT LOOSE LEG File # A401927
207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6 Submitted by: Peter Klewchuk

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L-20	11	337	34	123	3.6	29	11	554	36.20	<2	<8	<2	17	5	<.5	8	<3	15	.03	.181	<1	<1	.13	37	<.01	7	.90	.01	.10	3	89.3
L-21	8	134	41	92	.3	43	21	394	18.53	140	<8	<2	6	5	.5	<3	4	7	.05	.109	21	6	.08	40	<.01	<3	.68	.01	.13	<2	10.7
L-22	11	406	147	223	1.0	68	20	1063	19.88	5	<8	<2	21	29	.6	<3	8	13	.12	.208	12	16	.25	76	<.01	<3	1.11	.05	.18	<2	6.9
L-23	12	289	50	250	1.1	127	6	761	24.49	<2	<8	<2	8	8	<.5	<3	4	13	.03	.151	25	9	.13	24	<.01	<3	.66	.01	.11	<2	12.0
L-24	6	193	33	815	.8	45	6	703	22.26	243	<8	<2	7	8	<.5	<3	<3	4	.09	.080	4	5	.05	20	<.01	<3	.42	.01	.08	<2	8.1
L-25	3	9	9	16	<.3	16	11	459	1.29	<2	<8	<2	<2	4	<.5	<3	<3	6	.02	.020	5	11	.02	31	<.01	<3	.11	.03	.01	2	<.5
L-26	1	7	3	13	<.3	21	59	87	1.32	6	<8	<2	9	6	<.5	<3	<3	6	.09	.038	32	10	.18	12	<.01	4	.36	.06	.05	<2	<.5
L-27	2	10	18	10	<.3	33	37	279	3.80	3	<8	<2	5	9	<.5	<3	<3	8	.20	.047	22	9	.12	15	<.01	<3	.17	.04	.05	<2	6.1
L-28	1	5	4	6	<.3	11	23	295	1.64	<2	<8	<2	<2	24	<.5	<3	<3	6	1.64	.044	6	11	.78	14	<.01	<3	.10	.02	.03	<2	1.7
L-29	1	3	3	7	<.3	14	3	44	1.54	8	<8	<2	2	2	<.5	<3	<3	1	.01	.006	9	11	.03	8	<.01	3	.14	.01	.07	2	<.5
L-30	1	4	<3	14	<.3	15	4	56	2.19	<2	<8	<2	<2	3	<.5	<3	<3	<1	.02	.005	1	10	.04	9	<.01	3	.10	.01	.05	2	<.5
RE L-30	2	4	<3	15	<.3	16	4	57	2.26	2	<8	<2	<2	3	<.5	<3	<3	1	.02	.005	2	10	.04	9	<.01	3	.10	.01	.06	<2	<.5
L-31	7	3	<3	21	<.3	32	5	1327	12.42	8	<8	<2	4	17	1.2	<3	<3	18	7.01	.053	4	9	.51	82	<.01	<3	.18	<.01	.09	2	4.0
L-32	1	2	<3	24	<.3	11	5	131	1.71	3	<8	<2	2	3	<.5	<3	<3	2	.05	.006	6	8	.31	26	<.01	3	.68	<.01	.12	<2	30.3
STANDARD DS5/AU-R	13	146	24	137	.3	25	13	757	3.02	18	<8	<2	3	47	5.7	4	6	63	.76	.098	12	189	.70	141	.10	17	2.06	.04	.15	5	492.8

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK R150 60C AU* IGNITED, ACID LEACHED, ANALYZED BY ICP-MS. (15 gm)
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data ___ FA ___ DATE RECEIVED: MAY 7 2004 DATE REPORT MAILED: May 20/2004

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Ruby Red Resources Inc. PROJECT LOOSE LEG File # A401928 Page 1
207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6 Submitted by: Peter Klewchuk

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.3	2.1	2.1	36	<.1	3.9	3.4	448	1.58	<.5	1.8	1.1	4.1	69	<.1	<.1	.1	38	.53	.075	7	26.2	.47	190	.109	1	.82	.066	.47	.9	<.01	1.8	.3	<.05	4	<.5
NT 1850W	1.2	26.7	26.1	39	.1	18.3	11.0	392	1.92	7.6	.4	8.6	4.2	71	.2	.6	.4	12	8.11	.049	10	13.8	1.58	66	.019	3	.77	.007	.15	.1	.02	2.1	.1	.08	2	<.5
NT 1825W	1.1	29.9	26.7	37	.1	20.3	10.8	346	1.92	7.0	.4	10.8	4.1	71	.2	.5	.4	13	7.96	.053	11	18.9	1.57	61	.020	4	.94	.007	.15	.1	.02	2.0	.1	.08	2	<.5
NT 1800W	.6	86.9	22.2	87	.1	22.0	15.1	288	1.98	6.2	.4	4.3	3.9	19	.2	.3	.4	16	.26	.051	10	17.4	.36	203	.056	5	2.05	.014	.19	.1	.01	1.5	.1	<.05	5	<.5
NT 1775W	.5	34.9	22.4	64	<.1	21.9	12.9	552	1.81	3.0	.3	2.0	4.5	18	.2	.2	.3	14	.19	.045	11	18.5	.34	214	.049	4	1.71	.011	.30	.1	.01	2.3	.1	<.05	4	<.5
NT 1750W	.4	40.5	30.6	59	.1	21.7	14.3	1406	1.87	6.4	.5	11.1	6.5	26	.3	.2	.5	13	.40	.030	15	19.5	.33	369	.036	<1	1.32	.006	.28	.1	.02	2.0	.1	<.05	4	<.5
NT 1725W	.4	35.6	17.6	63	.1	18.8	8.8	310	1.47	5.8	.4	1.4	3.7	34	.2	.2	.3	12	.32	.074	9	11.3	.27	205	.062	4	1.77	.027	.24	.1	<.01	2.0	.1	<.05	5	<.5
NT 1700W	1.3	69.3	32.3	44	.1	28.8	14.5	117	2.83	8.5	.5	70.1	8.7	13	.1	.6	.5	21	.25	.054	23	22.2	.47	50	.018	2	1.14	.003	.27	.1	.01	3.6	.1	<.05	3	<.5
NT 1675W	.9	20.1	22.1	39	<.1	17.7	9.5	96	1.94	5.2	.5	6.2	6.6	10	<.1	.4	.4	16	.12	.019	18	15.8	.37	42	.031	3	.98	.004	.18	.1	.01	2.2	.1	<.05	3	<.5
NT 1650W	.9	26.1	27.9	41	.1	21.3	11.2	124	2.18	4.9	.4	11.5	7.2	9	.1	.5	.4	18	.28	.019	20	17.0	.52	50	.038	3	1.41	.005	.21	.2	.01	3.0	.1	<.05	4	<.5
NT 1625W	.4	14.0	20.8	77	.1	19.0	7.4	164	1.63	4.3	.5	2.1	3.5	24	.1	.1	.3	12	.24	.079	8	9.3	.22	216	.081	2	2.40	.021	.23	.1	.01	2.1	.1	<.05	7	<.5
NT 1600W	.5	18.9	15.7	65	.1	15.7	6.5	280	1.58	3.4	.3	77.5	3.1	23	.1	.1	.3	14	.25	.026	8	9.5	.25	225	.076	3	2.23	.019	.26	.1	.01	1.7	.1	<.05	6	<.5
NT 1575W	.7	11.9	16.5	51	<.1	17.3	7.6	127	1.80	3.7	.3	3.4	4.8	16	<.1	.3	.3	18	.20	.021	15	14.1	.39	62	.050	3	1.58	.010	.23	.1	.01	2.0	.1	<.05	4	<.5
NT 1550W	.4	9.9	10.5	45	.1	16.0	5.5	96	1.47	2.9	.3	2.3	2.7	27	.1	.2	.2	12	.28	.034	8	8.4	.22	153	.067	4	1.67	.028	.17	.1	<.01	1.8	.1	<.05	5	<.5
NT 1525W	.1	9.8	4.6	31	.1	8.3	3.0	109	.72	1.5	.1	.9	1.2	37	.1	.1	.1	11	.43	.044	4	4.6	.14	115	.046	3	1.08	.031	.15	.1	<.01	1.1	<.1	<.05	3	<.5
NT 1500W	.7	22.8	17.1	34	.1	18.4	8.5	138	2.10	5.0	.7	3.6	4.9	35	.1	.2	.3	23	.16	.025	9	10.0	.25	256	.096	2	3.30	.026	.09	.2	.03	2.4	.1	<.05	8	<.5
RE NT 1500W	.8	23.1	18.1	31	.1	19.0	8.1	134	1.96	5.0	.7	3.6	5.4	37	.1	.2	.3	20	.18	.024	10	9.9	.27	271	.099	1	3.20	.028	.10	.1	.03	2.5	.1	<.05	8	<.5
NT 1475W	.6	13.2	25.8	109	.2	26.9	9.0	633	2.17	3.5	.7	2.1	6.3	32	.2	.2	.3	20	.29	.038	14	11.9	.33	459	.104	4	3.09	.024	.22	.1	.03	2.5	.1	<.05	8	<.5
NT 1450W	.6	13.2	26.6	236	.1	25.5	10.6	1334	2.37	4.1	.7	4.2	7.6	34	.6	.2	.4	23	.36	.050	16	15.2	.42	698	.096	6	2.69	.026	.33	.1	.03	3.6	.2	<.05	7	<.5
NT 1425W	.4	14.2	11.5	61	.1	16.7	5.8	185	1.31	3.2	.4	5.6	3.1	35	.1	.2	.2	14	.31	.066	8	7.8	.24	237	.081	3	2.14	.040	.13	.1	.01	2.2	.1	<.05	7	<.5
NT 1400W	.9	24.7	26.0	65	.1	22.8	11.3	203	2.56	3.8	.3	6.8	7.0	12	.1	.4	.4	19	.18	.028	18	17.2	.53	120	.040	2	1.47	.006	.31	.1	.01	2.9	.1	<.05	5	<.5
NT 1375W	.6	12.4	17.0	72	.1	19.3	7.1	199	2.00	3.5	.7	2.3	4.6	27	.2	.3	.3	17	.35	.037	12	12.3	.33	220	.096	4	2.65	.023	.23	.1	.01	2.8	.1	<.05	7	<.5
NT 1350W	1.4	15.6	22.8	73	.1	23.9	10.7	815	2.27	5.7	.6	4.2	7.1	24	.3	1.1	.4	17	.33	.044	14	13.7	.42	233	.053	4	1.66	.013	.20	.1	.02	2.9	.1	<.05	5	<.5
NT 1325W	1.0	15.3	22.2	73	.1	26.7	9.7	130	2.28	5.2	.5	10.6	5.7	25	.1	.5	.4	15	.24	.060	9	9.9	.35	331	.085	3	2.55	.019	.23	.1	.01	2.7	.1	<.05	8	<.5
NT 1300W	1.2	17.2	23.6	69	.1	26.4	10.9	134	2.67	7.0	.6	1.7	5.5	29	.2	.4	.4	21	.34	.064	13	15.5	.41	238	.095	3	2.80	.016	.17	.1	.02	2.9	.1	<.05	8	<.5
NT 1275W	2.0	30.8	23.8	54	.1	27.1	14.4	129	2.93	8.1	.7	5.3	7.8	13	.1	.7	.5	21	.19	.051	21	19.8	.58	51	.022	1	1.19	.004	.20	.1	.01	3.4	.1	<.05	4	.5
NT 1250W	2.2	29.3	27.8	55	.1	23.1	13.5	131	2.47	7.7	.6	10.5	7.8	13	.1	.6	.5	21	.14	.042	22	17.9	.58	36	.027	3	1.13	.004	.24	.1	.01	2.6	.1	<.05	3	.5
NT 1225W	1.0	18.3	25.4	83	.2	20.4	9.7	525	2.10	4.3	1.0	2.6	5.4	16	.2	.3	.3	24	.13	.051	12	12.8	.31	226	.125	2	3.21	.024	.09	.1	.05	3.3	.2	<.05	8	<.5
NT 1200W	.3	10.5	13.1	90	.1	17.2	6.4	272	1.19	2.1	.4	.8	2.7	25	.2	.1	.2	14	.19	.081	7	6.7	.21	206	.078	4	1.82	.041	.11	.1	.02	2.3	.1	<.05	5	<.5
NT 1175W	.9	15.0	32.2	137	.1	25.4	14.6	647	1.93	6.6	.9	1.8	4.7	25	.3	.3	.4	23	.27	.075	10	10.4	.26	277	.114	3	2.78	.020	.11	.1	.06	3.3	.1	<.05	8	<.5
NT 1150W	.4	12.3	13.8	92	.1	22.0	8.4	103	1.29	4.3	.4	.9	3.5	34	.1	.2	.2	13	.31	.163	7	7.0	.24	167	.088	3	1.89	.027	.14	.1	.02	2.0	.1	<.05	7	<.5
NT 1125W	1.7	15.7	26.8	85	<.1	19.7	15.4	458	2.35	6.7	.4	4.9	5.3	10	.2	.5	.5	19	.13	.052	17	14.4	.48	98	.034	2	1.22	.006	.22	.1	.01	2.2	.1	<.05	4	<.5
NT 1100W	1.6	23.8	35.0	128	.1	28.8	20.3	788	2.84	5.8	.7	2.3	7.3	24	.3	.4	.6	23	.27	.043	19	15.6	.61	248	.057	5	2.08	.011	.25	.1	.01	3.7	.1	<.05	6	<.5
NT 1075W	2.1	21.6	29.1	79	<.1	20.9	12.4	298	2.66	8.0	.5	2.6	6.2	13	.1	.5	.5	21	.13	.026	17	15.5	.62	97	.036	2	1.31	.006	.19	.1	.01	2.3	.1	<.05	4	<.5
NT 1050W	3.9	49.4	44.8	95	.2	32.9	20.7	469	3.93	14.2	.9	79.3	9.7	16	.2	.9	.8	23	.18	.035	19	16.6	.77	60	.026	2	1.51	.008	.21	.1	.01	3.8	.1	.09	5	.5
STANDARD DS5	12.6	142.7	24.6	139	.3	25.1	12.0	729	2.95	18.0	6.1	41.7	2.6	44	5.7	3.9	6.2	57	.72	.082	12	169.6	.62	130	.091	16	1.88	.030	.14	5.6	.16	3.4	[illegible]	.05	7	4.8

GROUP 1DX - 15.0 GM SAMPLE LEACHED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 300 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILI
- SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data ✓ FA ____ DATE RECEIVED: MAY 7 2004 DATE REPORT MAILED: May 20/2004

BRITISH COLUMBIA CERTIFIED ASSAYER
Jacky Wang

Appendix 3. Geochemical Analyses of Soil Samples

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.6	2.9	2.1	39	<.1	3.5	3.4	465	1.59	<.5	1.7	<.5	3.7	82	<.1	<.1	.1	35	.50	.076	8	40.2	.46	192	.105	<1	.73	.062	.35	.7	<.01	1.7	.3	<.05	4	<.5
NT 1025W	4.1	46.1	54.0	81	.1	31.8	18.1	618	3.75	13.3	.9	10.9	8.9	21	.3	.7	.9	21	.24	.050	20	17.3	.97	58	.027	1	1.48	.010	.14	.1	.02	3.5	.1	<.05	5	.5
NT 1000W	1.9	20.7	30.3	84	.1	24.8	11.7	989	2.56	8.5	.7	2.7	6.8	36	.3	.3	.6	20	.38	.052	18	14.4	.70	212	.061	4	2.15	.014	.23	.1	.02	2.9	.1	<.05	6	<.5
NT 975W	2.3	26.8	28.4	79	.1	23.7	11.9	559	2.92	8.8	.8	3.7	7.3	28	.2	.4	.7	20	.23	.033	17	14.3	.67	151	.050	2	1.93	.012	.16	.1	.01	2.9	.1	<.05	5	.5
NT 950W	2.1	21.7	35.4	121	<.1	24.3	13.8	2064	2.79	7.9	.6	2.2	6.7	39	.7	.4	.6	18	.35	.059	19	12.8	.52	313	.042	3	1.64	.009	.23	.1	.02	2.5	.1	<.05	5	<.5
NT 925W	2.5	31.2	46.9	133	.1	28.3	18.4	2237	2.87	10.8	.7	1.7	6.5	44	.8	.5	.7	19	.50	.076	19	12.4	.49	270	.038	5	1.56	.008	.22	.1	.01	2.3	.1	<.05	4	<.5
NT 900W	2.0	27.7	29.3	90	.1	31.2	13.4	527	2.91	8.3	.9	2.8	7.2	31	.2	.4	.6	20	.24	.030	20	12.3	.46	225	.077	2	2.54	.018	.16	.1	.01	2.9	.1	<.05	7	<.5
NT 875W	3.1	39.8	32.4	88	.1	25.6	12.8	241	3.22	12.4	.8	2.9	7.8	16	.2	.6	.7	18	.18	.027	24	12.3	.51	79	.025	<1	1.18	.005	.12	.1	.01	2.3	.1	<.05	4	.5
NT 850W	2.8	37.5	37.5	88	<.1	27.7	13.7	391	3.31	13.9	.9	2.5	8.2	12	.1	.6	.7	18	.13	.042	22	13.8	.51	53	.025	2	1.17	.005	.17	.1	.02	2.1	.1	<.05	3	<.5
NT 825W	2.0	33.1	31.8	85	.1	31.1	13.1	281	3.01	10.0	1.0	3.4	7.4	24	.1	.4	.6	24	.21	.034	20	14.0	.51	158	.079	1	2.35	.015	.16	.1	.01	3.6	.1	<.05	7	<.5
NT 800W	2.2	26.8	27.8	85	.1	26.3	11.9	377	2.89	10.0	.6	7.2	6.6	22	.2	.4	.6	19	.29	.034	22	15.0	.60	110	.034	1	1.63	.008	.12	.1	.01	2.1	.1	<.05	5	.5
NT 775W	2.8	34.5	27.5	85	.1	26.8	13.7	497	2.78	12.0	.8	3.4	6.7	19	.2	.5	.5	18	.18	.061	21	14.0	.56	84	.033	2	1.32	.010	.13	.1	.01	2.3	.1	<.05	4	.6
NT 750W	3.1	37.7	24.2	71	.1	24.6	11.5	217	2.91	12.5	.9	2.9	7.3	14	.2	.5	.6	16	.12	.031	19	15.3	.64	33	.018	1	1.06	.007	.10	.1	.01	2.5	.1	<.05	3	<.5
NT 725W	2.6	30.6	23.9	71	.1	23.6	11.4	175	2.89	10.8	.8	2.2	7.0	17	.1	.5	.6	17	.14	.035	19	13.9	.56	50	.025	1	1.13	.007	.11	.1	<.01	2.1	.1	<.05	3	<.5
NT 700W	2.1	29.8	28.7	93	.1	25.3	12.7	414	2.52	11.0	.8	14.8	6.4	17	.2	.5	.5	17	.14	.061	22	13.0	.51	105	.041	1	1.47	.012	.14	.1	.01	2.3	.1	<.05	5	<.5
NT 675W	.6	16.0	11.0	76	.1	21.0	6.1	202	1.41	5.7	.8	.7	3.5	30	.2	.1	.2	15	.25	.162	9	6.5	.20	141	.107	3	2.42	.038	.08	.2	.02	2.1	.1	<.05	6	<.5
NT 650W	1.7	25.8	25.1	116	.1	27.3	12.2	725	2.28	8.4	.8	14.8	5.5	27	.2	.3	.5	18	.24	.120	14	10.6	.38	197	.073	2	2.00	.021	.12	.1	.01	2.1	.1	<.05	5	<.5
NT 625W	1.3	25.8	31.7	136	.1	27.5	10.7	1236	2.17	9.6	1.1	2.8	5.6	35	.4	.2	.5	20	.23	.173	12	10.1	.32	288	.108	3	2.56	.025	.12	.1	.02	2.4	.2	<.05	7	.5
NT 600W	1.7	26.8	44.6	248	.1	29.0	13.3	2624	2.62	11.4	1.2	3.0	6.3	56	.8	.3	.6	25	.46	.248	15	12.8	.41	526	.101	8	2.66	.021	.20	.1	.02	3.0	.2	<.05	8	.7
RE NT 575W	1.0	19.1	32.8	108	.1	15.8	7.4	1446	1.75	8.2	.9	2.9	3.3	51	.5	.3	.4	18	.35	.134	11	7.8	.23	323	.105	3	2.72	.034	.09	.1	.03	2.2	.2	<.05	7	<.5
NT 575W	.9	18.5	34.5	112	.1	17.3	8.0	1440	1.77	8.7	.9	2.4	3.5	54	.5	.3	.4	17	.36	.139	11	7.8	.23	338	.106	3	2.74	.034	.10	.1	.02	2.4	.2	<.05	7	.5
NT 550W	.5	24.3	19.7	68	.2	17.2	7.4	383	1.66	6.3	.9	1.8	3.2	36	.2	.1	.3	17	.23	.172	9	5.9	.18	183	.125	2	3.07	.031	.06	.1	.02	2.1	.1	<.05	8	<.5
NT 525W	.9	25.7	26.1	137	.2	22.7	9.9	1124	1.97	7.2	.9	3.5	5.2	43	.5	.2	.4	18	.32	.174	10	9.3	.25	229	.116	3	2.74	.040	.11	.1	.02	2.5	.1	<.05	7	<.5
NT 500W	2.2	25.4	31.2	101	.1	29.4	13.3	281	3.21	9.8	.7	21.4	6.2	36	.1	.4	.7	19	.22	.051	14	13.3	.41	85	.060	4	1.83	.017	.26	.1	.01	1.8	.1	<.05	5	<.5
NT 475W	5.3	59.1	33.1	97	.2	27.8	14.0	269	4.45	19.9	1.0	5.3	8.4	18	.2	.7	.9	13	.10	.042	25	12.5	.44	42	.015	1	.95	.005	.13	.1	.01	1.6	.1	<.05	3	.5
NT 450W	2.9	39.8	62.9	188	.2	37.2	19.1	1675	3.55	17.3	1.2	10.1	7.2	46	.7	.4	.9	27	.46	.171	16	14.9	.46	185	.073	4	2.42	.014	.14	.1	.03	2.5	.2	<.05	6	.6
NT 425W	2.9	27.9	61.4	241	.1	31.9	19.3	6760	3.40	14.8	1.0	5.3	4.6	51	1.3	.5	.9	26	.41	.166	17	13.2	.40	601	.069	2	2.44	.012	.14	.1	.04	2.5	.2	<.05	7	.6
NT 400W	1.0	33.1	28.5	110	.2	22.7	10.2	600	2.13	7.0	.8	2.6	4.1	48	.2	.3	.4	21	.25	.128	12	8.3	.24	238	.123	3	2.94	.033	.09	.1	.02	2.5	.1	<.05	8	.5
NT 375W	1.4	21.2	30.7	124	.1	22.7	10.1	894	2.32	7.9	.7	2.0	4.5	34	.3	.2	.5	18	.23	.097	10	9.0	.27	247	.097	3	2.53	.025	.12	.1	.03	2.0	.1	<.05	7	<.5
NT 350W	1.8	32.4	25.4	100	.1	24.6	10.7	223	2.48	10.3	.8	3.1	4.6	30	.2	.3	.5	17	.18	.091	11	8.5	.24	126	.084	1	1.99	.030	.08	.1	.02	2.1	.1	<.05	6	.7
NT 325W	3.0	36.5	35.8	130	.1	32.0	14.7	673	3.31	15.2	.7	2.8	5.7	18	.2	.4	.8	19	.12	.098	15	11.1	.32	155	.044	1	1.61	.011	.09	.1	.01	1.6	.1	<.05	5	.6
NT 300W	1.5	16.7	23.1	99	.1	25.2	10.6	293	1.99	7.1	.5	2.5	3.2	34	.2	.2	.4	19	.20	.031	9	8.4	.27	325	.089	3	2.66	.028	.13	.1	.02	1.4	.1	<.05	7	<.5
NT 275W	.5	11.5	14.3	45	.1	14.8	5.4	307	1.64	7.3	.5	2.2	2.8	33	.1	.1	.3	18	.27	.142	4	6.1	.13	101	.133	3	3.14	.032	.04	.1	.02	1.7	.1	<.05	8	<.5
NT 250W	.8	13.8	19.8	87	.1	17.9	7.9	502	1.75	7.3	.5	1.6	3.7	24	.2	.2	.3	19	.22	.160	6	7.6	.17	121	.117	2	2.81	.024	.05	.2	.03	1.6	.1	<.05	7	<.5
NT 225W	2.7	12.1	32.3	120	.1	19.6	13.6	918	2.61	11.4	.4	3.3	4.2	20	.2	.3	.6	20	.21	.062	14	10.7	.28	133	.033	2	1.31	.008	.10	.1	.02	1.4	.1	<.05	5	<.5
STANDARD D	13.2	142.2	24.7	130	.3	24.5	11.8	788	2.98	19.1	6.2	43.3	2.9	52	5.6	3.6	5.9	59	.71	.090	14	179.8	.66	148	.106	18	1.97	.033	.14	4.5	.16	3.6	1.2	<.05	7	5.3

Standard is STANDARD DS5. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm
NT 200W	1.9	22.2	35.5	71	.3	15.5	9.2	530	1.77	6.7	1.2	2.2	2.0	99	.4	.2	.4	20
NT 175W	3.4	11.2	45.9	125	.2	20.5	14.3	531	2.39	7.7	1.1	3.1	5.0	57	.3	.3	.6	29
NT 150W	3.4	11.7	57.0	85	.1	13.8	11.9	1430	2.18	15.2	.8	1.2	3.8	30	.3	.2	.6	30
NT 125W	1.7	7.9	44.1	101	.1	17.8	9.0	337	2.37	8.6	.5	1.3	3.2	39	.3	.3	.6	33
NT 100W	2.2	10.5	50.2	106	.1	15.4	9.7	805	2.17	8.3	.8	4.2	3.2	39	.3	.3	.8	32
NT 75W	6.4	34.1	74.2	142	.1	29.7	16.4	772	3.15	12.8	.7	27.2	5.6	28	.4	.5	1.1	32
NT 50W	8.2	30.9	64.3	161	.1	26.3	14.3	698	2.91	12.1	.6	3.3	4.8	51	.4	.5	1.1	28
NT 25W	5.3	46.5	127.8	285	.2	23.0	19.5	5983	2.73	16.1	.9	18.8	3.7	69	2.5	.7	1.3	26
NT 0W	4.2	41.0	68.6	190	.1	22.7	18.2	2912	2.83	9.8	1.1	1.6	5.7	115	1.7	.5	1.0	25
STANDARD	12.5	143.0	25.4	138	.3	24.6	12.1	744	2.86	17.9	6.3	41.2	2.7	47	5.6	3.9	5.9	58

SAMPLE#	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
NT 200W	1.05	.038	8	10.6	.39	97	.047	2	1.78	.034	.08	.1	.02	1.9	.1	.08	4	1.5
NT 175W	.40	.026	15	15.3	.45	134	.068	2	2.24	.023	.09	.1	.03	2.6	.2	<.05	7	.8
NT 150W	.24	.026	8	11.0	.30	125	.106	3	2.60	.025	.07	.2	.03	2.0	.1	<.05	8	.6
NT 125W	.40	.048	4	9.8	.26	87	.151	5	3.45	.027	.07	.2	.03	1.5	.1	<.05	9	<.5
NT 100W	.29	.033	7	11.2	.34	158	.125	2	2.35	.021	.09	.1	.03	1.8	.1	<.05	8	.5
NT 75W	.24	.042	14	12.0	.49	240	.088	3	2.60	.014	.13	.1	.03	2.1	.2	<.05	8	.5
NT 50W	.49	.065	14	11.2	.48	247	.077	2	2.47	.013	.14	.1	.02	2.0	.2	<.05	7	.5
NT 25W	.91	.067	14	12.7	.41	521	.037	3	1.44	.011	.09	.2	.09	2.5	.2	<.05	5	.6
NT 0W	1.16	.045	14	12.3	.52	379	.032	2	1.37	.008	.10	.1	.06	2.6	.1	<.05	5	.9
STANDARD	.71	.091	13	179.3	.68	138	.098	16	1.94	.034	.12	4.8	.16	3.4	1.1	<.05	7	5.0

Standard is STANDARD DS5.

Data FA

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Ruby Red Resources Inc. PROJECT LOOSE LEG File # A402220 Page 1

207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6 Submitted by: Peter Klewchuk

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
G-1	1.4	2.2	1.9	39	<.1	3.5	3.4	425	1.52	<.5	1.7	.5	4.1	74	<.1	<.1	.1	32	.47	.073	6	27.2	.45	201	.102	1	.72	.072	.37	.8	<.01	1.5	.3	<.05	4	<.5	15.0
FS 1525N	1.5	42.3	237.0	116	.7	11.6	32.8	2033	1.55	8.3	.6	14.7	1.5	47	.6	.9	.5	14	.72	.076	9	10.7	.19	354	.026	4	1.21	.008	.11	.1	.07	1.2	.1	<.05	4	<.5	15.0
FS 1500N	1.0	12.7	121.1	87	.2	10.5	7.7	1298	1.50	4.5	.6	7.2	3.9	24	.4	.5	.3	13	.25	.049	11	9.0	.21	270	.031	4	1.46	.010	.12	.1	.05	1.3	.1	<.05	4	<.5	15.0
FS 1475N	1.3	9.8	60.5	45	.2	11.3	5.9	133	1.69	3.8	.4	7.8	4.5	20	.1	.6	.4	19	.29	.016	11	10.5	.23	138	.041	3	1.97	.008	.07	.1	.03	1.4	.1	<.05	7	<.5	15.0
FS 1450N	1.7	15.4	204.3	45	.3	11.9	8.5	964	1.69	5.3	.5	31.3	5.4	28	.4	.9	.4	14	.59	.025	11	11.0	.22	220	.020	4	1.14	.004	.13	.1	.05	1.9	.1	<.05	4	<.5	15.0
FS 1425N	1.4	22.5	169.6	54	.6	12.2	10.2	653	1.88	4.7	.5	157.9	10.9	18	.5	.8	.5	15	.45	.017	17	11.0	.24	133	.019	4	1.08	.003	.23	.1	.04	1.8	.1	<.05	3	<.5	15.0
FS 1400N	.7	26.1	74.3	70	.1	13.3	19.0	1476	2.11	4.4	.4	5.7	6.1	21	.1	.5	.6	10	.61	.031	16	12.7	.48	284	.026	5	1.40	.008	.25	.1	.03	2.6	.1	.07	4	.5	7.5
FS 1375N	.6	10.0	16.2	57	<.1	14.2	6.0	167	1.40	4.2	.3	2.4	2.8	24	.1	.2	.2	13	.28	.116	7	9.4	.21	136	.045	6	1.64	.019	.09	.1	.01	1.3	.1	<.05	5	<.5	15.0
FS 1350N	.8	7.9	20.8	39	<.1	14.1	7.5	254	1.79	3.1	.3	1.9	3.4	15	<.1	.3	.3	16	.16	.016	11	11.0	.24	184	.056	1	1.97	.013	.09	.1	.01	1.5	.1	<.05	6	<.5	15.0
FS 1325N	.8	8.1	32.9	72	.1	13.3	7.2	1564	1.58	2.4	.3	.6	3.1	28	.2	.2	.2	14	.39	.031	9	10.9	.22	415	.055	6	1.68	.016	.17	.1	.02	1.6	.1	.07	5	<.5	15.0
FS 1300N	.9	10.0	54.4	44	.2	13.9	7.0	304	1.85	3.0	.5	2.4	4.5	23	.1	.4	.3	17	.26	.013	12	11.7	.26	218	.059	4	1.89	.012	.10	.1	.01	1.9	.1	<.05	5	<.5	15.0
FS 1275N	.9	8.2	46.1	45	.1	14.4	9.0	1402	1.93	2.5	.5	3.0	4.9	25	.2	.4	.3	17	.32	.015	12	10.8	.25	419	.056	3	1.82	.010	.19	.1	.03	2.0	.1	<.05	5	<.5	15.0
FS 1250N	1.3	8.6	15.2	38	.1	16.5	7.8	852	2.89	4.9	.5	23.5	8.8	27	.1	.4	.2	12	.60	.077	13	8.3	.27	223	.019	5	1.07	.005	.26	.1	.03	2.1	.1	<.05	4	<.5	15.0
FS 1225N	.7	12.0	16.4	66	.1	14.7	9.2	1238	2.14	3.5	.5	4.6	5.8	29	.1	.3	.2	13	.37	.044	16	9.4	.25	343	.041	5	1.54	.011	.27	.1	.02	2.6	.1	<.05	4	<.5	15.0
FS 1200N	1.1	25.1	25.5	80	.1	14.7	7.4	252	1.95	5.5	.5	5.8	3.6	21	.1	.4	.3	21	.25	.035	11	12.0	.31	147	.050	2	2.04	.014	.09	.1	.03	1.5	.1	<.05	6	<.5	15.0
FS 1175N	1.1	13.6	24.7	53	.2	16.2	7.4	81	1.95	4.4	.6	21.1	4.2	24	.1	.4	.3	19	.28	.020	14	11.1	.30	145	.050	1	1.96	.010	.09	.1	.02	1.8	.1	<.05	6	<.5	15.0
FS 1150N	1.2	19.4	36.7	46	.1	19.4	11.6	305	2.42	5.6	.6	4.4	6.6	14	.1	.5	.3	16	.36	.019	19	14.3	.36	135	.028	<1	1.50	.005	.13	.1	.03	3.7	.1	<.05	4	<.5	15.0
FS 1100N	.7	14.8	19.5	57	<.1	16.2	9.7	1535	1.97	2.3	.5	.7	5.9	27	.1	.3	.3	14	.38	.019	15	13.7	.38	310	.051	5	1.81	.013	.21	.1	.03	2.6	.1	<.05	6	<.5	7.5
RE FS 1100N	.8	14.3	19.9	56	<.1	15.6	9.4	1492	1.93	2.1	.5	1.1	5.9	28	.2	.3	.3	13	.37	.018	15	13.0	.35	303	.050	4	1.77	.013	.21	.1	.02	2.5	.1	<.05	6	<.5	7.5
FS 1075N	.5	7.5	13.8	55	.2	11.7	6.3	650	1.57	2.9	1.1	8.6	9.2	27	.1	.3	.2	10	.46	.038	21	10.7	.24	264	.031	5	1.45	.008	.26	.1	.03	1.9	.1	<.05	4	<.5	15.0
FS 1050N	1.1	11.3	18.0	94	.1	16.5	7.9	2130	2.02	3.3	.6	3.1	6.1	38	.2	.3	.3	16	.50	.050	14	13.8	.28	619	.049	4	2.05	.013	.22	.1	.02	1.9	.1	<.05	7	<.5	15.0
FS 1025N	1.3	8.7	20.5	55	.1	15.3	9.2	1279	2.13	3.5	.6	1.1	4.4	12	.1	.4	.3	17	.12	.027	17	13.6	.25	202	.040	3	1.81	.007	.16	.1	.03	1.9	.1	<.05	5	<.5	15.0
FS 1000N	1.1	12.7	27.6	74	.1	18.8	10.0	1658	2.12	4.4	.7	1.7	6.0	26	.3	.3	.3	20	.26	.033	15	17.6	.29	384	.060	<1	2.24	.012	.17	.1	.03	2.3	.1	<.05	7	<.5	15.0
FS 975N	1.1	20.3	25.2	66	.2	21.6	13.4	1480	2.32	3.1	.6	4.4	5.7	32	.3	.3	.3	28	.36	.031	16	26.6	.43	382	.050	4	2.03	.008	.18	.5	.04	2.8	.1	<.05	6	<.5	7.5
FS 925N	.8	66.2	22.7	45	.1	27.0	16.4	203	2.31	4.3	.6	3.8	7.7	26	.1	.5	.3	21	.35	.020	19	42.2	.46	131	.037	2	1.63	.011	.20	.1	.01	3.9	.1	<.05	5	<.5	15.0
FS 900N	.8	25.3	14.6	31	.1	27.5	14.5	130	2.19	3.0	.6	15.3	12.0	20	.1	1.0	.3	15	.54	.027	19	26.1	.42	76	.009	4	1.08	.003	.25	.1	.01	2.5	.1	<.05	3	<.5	15.0
FS 875N	.4	63.1	18.6	54	.1	139.6	30.3	474	4.96	3.3	.2	1.2	3.9	28	.1	.2	.4	86	.49	.015	10	450.5	2.62	152	.068	4	3.96	.011	.24	.1	.03	14.5	.1	<.05	12	<.5	15.0
FS 850N	.9	18.4	15.8	67	<.1	22.6	10.6	2342	1.74	3.5	.3	<.5	2.3	40	.4	.1	.3	18	.60	.117	8	40.8	.42	507	.046	4	1.56	.015	.21	.1	.02	2.4	.1	<.05	5	<.5	15.0
FS 825N	.7	10.1	22.1	51	<.1	15.0	7.6	376	1.88	2.4	.3	1.3	4.0	16	.1	.2	.3	12	.28	.025	12	18.0	.31	126	.040	3	1.43	.010	.22	.1	.01	2.2	.1	<.05	4	<.5	15.0
FS 800N	.3	7.6	14.7	112	.1	11.0	7.7	1297	1.74	1.8	.2	8.5	2.8	27	.1	.1	.3	11	.43	.057	8	12.1	.25	287	.059	11	1.68	.015	.32	.1	.01	2.0	.1	<.05	5	<.5	15.0
FS 775N	.9	18.7	24.3	62	.1	23.6	12.3	1271	2.51	4.9	.7	2.5	9.6	27	.3	.6	.4	21	.40	.039	18	16.2	.46	316	.056	3	1.93	.009	.30	.1	.03	2.8	.1	<.05	6	<.5	15.0
FS 750N	1.1	21.7	25.8	63	.1	20.9	12.1	1191	2.48	6.2	.9	13.1	8.0	17	.3	.5	.4	27	.20	.026	19	17.6	.38	266	.055	<1	1.77	.006	.16	.1	.04	2.8	.1	<.05	5	<.5	15.0
FS 725N	1.1	20.0	19.9	57	.1	21.7	11.7	878	2.54	5.2	.7	4.2	8.1	16	.2	.4	.4	21	.25	.018	19	17.9	.44	212	.037	<1	1.42	.005	.16	.1	.01	2.7	.1	<.05	4	<.5	15.0
FS 700N	1.1	20.3	24.8	46	.2	20.0	8.9	209	2.58	4.7	1.0	5.8	9.1	21	.1	.6	.3	18	.34	.017	16	16.0	.43	151	.052	3	1.98	.017	.16	.1	.02	3.2	.1	<.05	6	.5	15.0
FS 675N	1.0	34.3	23.3	68	.1	26.7	15.2	692	3.28	5.8	.5	10.1	8.7	24	.2	.5	.3	25	.62	.038	20	27.9	.63	183	.040	4	1.58	.005	.37	.1	.03	4.3	.1	<.05	5	<.5	15.0
STANDARD DS5	13.3	148.1	25.1	141	.3	26.0	12.8	791	3.02	19.0	6.1	43.6	2.7	45	5.7	3.9	6.2	61	.72	.090	12	197.4	.68	144	.094	16	1.99	.032	.13	4.9	.19	3.4	1.0	<.05	7	5.2	15.0

GROUP 1DX - 15.0 GM SAMPLE LEACHED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 300 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data ƒ FA ____ DATE RECEIVED: MAY 21 2004 DATE REPORT MAILED: June 1/04

BRITISH COLUMBIA CERTIFIED ASSAYER
Clarence Leong

ACME ANALYTICAL

Ruby Red Resources Inc. PROJECT LOOSE LEG FILE # A402220

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
G-1	1.4	2.7	1.9	41	<.1	3.6	3.8	506	1.80	.6	1.8	<.5	4.4	74	<.1	<.1	.1	33	.53	.078	6	29.1	.47	204	.108	3	.73	.072	.42	.8	<.01	1.7	.3	<.05	5	<.5	15.0
FS 650N	.5	15.2	19.6	66	.1	16.6	9.5	1117	2.28	2.9	.4	4.1	6.1	24	.2	.2	.3	14	.43	.030	13	15.9	.37	300	.066	6	1.93	.015	.29	.1	.02	3.0	.1	<.05	7	.6	15.0
FS 625N	.6	15.5	17.1	49	.1	17.0	9.9	315	2.39	3.0	.5	3.2	6.1	16	<.1	.2	.3	15	.26	.021	15	17.3	.43	156	.062	5	1.79	.012	.29	.1	.01	3.6	.1	<.05	6	.5	15.0
FS 600N	.8	17.5	21.1	76	.1	17.4	9.8	1122	2.26	4.4	.2	2.6	5.4	22	.2	.3	.3	12	.59	.058	15	13.5	.41	247	.031	5	1.34	.006	.34	.1	.02	2.7	.1	<.05	4	<.5	15.0
FS 575N	.5	12.3	16.6	45	.1	14.0	7.8	373	2.07	3.1	.4	1.3	4.9	24	.1	.2	.3	13	.35	.017	11	12.1	.29	245	.065	3	1.92	.021	.28	.1	.01	2.8	.1	<.05	5	<.5	15.0
FS 550N	.8	11.4	19.0	48	<.1	14.9	9.0	325	2.23	4.0	.4	.7	6.1	10	.1	.3	.3	13	.23	.022	16	14.0	.34	120	.031	1	1.28	.004	.20	.1	.02	2.6	.1	<.05	4	.5	15.0
FS 525N	1.1	21.8	23.4	48	.1	18.5	11.3	283	2.38	5.8	.5	2.4	7.3	10	.1	.6	.4	20	.22	.016	19	16.2	.45	125	.028	<1	1.21	.004	.16	.1	.03	2.6	.1	<.05	4	.5	15.0
FS 500N	1.1	25.8	34.7	79	.1	19.0	13.1	2355	2.51	6.0	.4	9.1	5.8	21	.5	.5	.4	25	.38	.041	17	18.8	.46	339	.038	3	1.18	.004	.22	.1	.03	3.2	.1	<.05	4	.6	15.0
FS 475N	.8	14.5	26.1	40	<.1	17.7	10.2	1098	2.29	4.1	.4	11.5	10.2	11	.2	.4	.3	13	.35	.019	23	14.9	.41	181	.012	1	1.07	.004	.25	.1	.03	2.5	.1	<.05	3	.5	15.0
FS 450N	.8	11.2	17.8	60	<.1	16.1	8.3	886	2.33	4.0	.7	7.4	8.8	23	.2	.3	.3	16	.36	.023	16	11.0	.27	277	.049	2	1.79	.009	.24	.1	.02	2.1	.1	<.05	5	<.5	15.0
FS 425N	.9	16.5	36.4	82	.2	12.6	9.7	2272	1.95	5.3	.5	39.6	4.2	37	.6	.5	.4	12	.76	.068	16	9.8	.26	500	.026	2	1.14	.007	.24	.1	.06	2.0	.1	<.05	3	.6	15.0
FS 400N	.8	15.3	18.8	49	.1	16.5	9.5	395	2.59	3.3	.7	12.9	8.3	20	.2	.3	.4	13	.34	.021	16	10.8	.32	264	.050	3	1.84	.011	.23	.1	.01	2.9	.1	<.05	5	.5	15.0
FS 375N	1.3	24.8	28.1	89	.1	17.8	11.1	1983	2.16	7.9	.4	19.4	3.4	25	.5	.5	.4	13	.65	.069	13	10.2	.37	290	.030	3	1.14	.010	.15	.1	.05	1.9	.1	<.05	3	.5	15.0
FS 350N	2.0	20.8	36.1	71	.4	21.7	17.3	1293	3.29	11.0	2.4	19.0	7.6	32	.4	.7	.6	14	.55	.085	20	15.1	.33	150	.015	2	1.15	.005	.16	.1	.10	2.1	.1	<.05	4	.7	15.0
FS 325N	1.6	16.4	56.6	68	.3	22.1	13.3	1944	2.91	3.9	.7	36.6	9.0	56	.5	.4	.4	21	.90	.041	19	15.3	.25	622	.031	5	1.73	.009	.18	.1	.06	2.8	.1	<.05	5	.6	15.0
FS 300N	1.7	22.6	52.2	90	.2	21.2	14.6	3080	2.78	5.6	1.8	66.2	9.0	49	.9	.6	.3	11	.69	.106	19	7.2	.15	554	.013	3	.80	.006	.16	.1	.03	2.5	.1	.06	2	.6	15.0
RE FS 475N	.7	13.8	24.8	40	<.1	16.0	9.1	1027	2.16	4.1	.4	8.7	9.9	11	.1	.5	.3	13	.34	.019	21	13.3	.38	180	.011	3	1.03	.003	.24	.1	.02	2.4	.1	<.05	3	.5	15.0
FS 275N	1.4	14.8	35.3	65	.3	14.5	10.9	2124	2.34	5.8	1.2	10.9	8.8	28	.6	.3	.4	11	.46	.076	17	8.8	.27	320	.014	1	.96	.006	.18	.1	.05	1.4	.1	<.05	3	<.5	7.5
FS 250N	.9	23.4	48.9	226	.2	18.5	11.8	2677	2.07	4.7	.6	9.8	5.2	79	.9	.3	.4	14	.88	.062	11	10.8	.26	672	.046	6	1.55	.015	.17	.1	.05	2.1	.1	<.05	5	.5	15.0
FS 225N	1.7	20.1	31.9	94	.1	26.5	13.8	365	2.91	5.2	1.1	1.7	6.6	29	.2	.3	.6	25	.29	.062	14	15.7	.46	239	.059	1	2.48	.015	.14	.2	.02	2.3	.1	<.05	7	.5	15.0
FS 200N	2.3	22.9	25.2	65	.1	24.1	12.4	201	2.85	10.8	.7	.6	6.0	17	.1	.7	.7	21	.15	.034	16	14.4	.48	92	.034	1	1.36	.007	.11	.1	.03	1.7	.1	<.05	5	.5	15.0
FS 175N	1.6	14.1	25.0	80	.1	21.2	11.7	928	2.43	4.3	.8	7.2	5.6	33	.1	.3	.4	18	.38	.032	11	12.6	.33	335	.049	3	2.09	.013	.15	.1	.04	2.2	.1	<.05	6	<.5	7.5
FS 150N	1.0	11.5	17.3	55	.1	15.8	8.3	234	2.26	3.7	.5	5.8	4.8	27	.1	.6	.3	20	.40	.025	16	14.9	.35	147	.035	2	1.96	.012	.10	.1	.03	2.2	.1	<.05	5	<.5	15.0
FS 125N	1.3	14.1	16.6	45	.1	18.6	8.3	158	2.48	5.1	.8	2.8	5.3	14	.1	1.2	.3	19	.21	.034	26	13.6	.30	86	.032	1	1.93	.007	.12	.1	.03	1.7	.1	<.05	6	.5	7.5
FS 100N	1.6	14.3	25.6	86	.1	17.0	10.5	2651	2.30	5.5	.6	2.4	5.2	35	.3	.6	.4	18	.51	.033	14	12.4	.32	489	.046	2	1.75	.008	.13	.1	.05	2.1	.1	<.05	5	.5	15.0
FS 75N	1.2	10.6	18.5	47	<.1	16.7	7.9	333	2.10	3.7	.3	.7	4.2	13	<.1	.3	.4	21	.20	.013	12	14.6	.36	165	.038	3	1.50	.006	.09	.1	.02	1.5	.1	<.05	5	<.5	15.0
FS 50N	1.7	13.5	27.2	50	.1	18.5	11.8	1197	2.41	4.4	.4	3.3	5.4	19	.2	.4	.5	21	.31	.017	14	16.1	.44	221	.047	2	1.53	.008	.21	.1	.02	2.2	.1	<.05	5	.5	15.0
FS 25N	1.0	11.7	19.8	54	<.1	17.4	9.1	852	2.18	4.0	.4	2.6	5.5	15	.2	.4	.4	21	.24	.016	14	14.3	.39	183	.046	2	1.47	.006	.20	.1	.01	2.3	.1	<.05	5	<.5	15.0
FS 0N	.9	10.8	16.3	50	<.1	14.5	7.5	616	1.96	3.9	.3	3.1	5.1	12	.1	.3	.3	18	.18	.014	15	14.7	.40	133	.037	2	1.21	.005	.21	.1	.02	1.9	.1	<.05	4	<.5	15.0
STANDARD DS5	13.0	149.9	24.8	142	.3	25.0	12.7	818	3.06	19.2	6.2	43.0	2.9	45	5.5	3.7	6.3	59	.76	.098	11	195.4	.67	141	.097	17	1.97	.032	.14	4.7	.18	3.5	1.1	<.05	7	4.8	15.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data ___ FA ___

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Ruby Red Resources Inc. PROJECT LOOSE LEG File # A403184 Page 1

207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
FS 2500N	2	77	38	55	<.3	37	37	532	4.06	6	<8	<2	10	18	<.5	<3	<3	19	.26	.024	21	13	.45	130	.02	<3	1.67	.01	.17	<2	47.8
FS 2475N	2	100	21	47	<.3	33	33	556	4.08	8	<8	<2	14	18	<.5	<3	<3	20	.26	.028	22	13	.48	129	.02	<3	2.35	.01	.17	<2	11.1
FS 2450N	1	20	26	37	<.3	29	15	519	2.19	8	<8	<2	4	20	<.5	<3	<3	22	.15	.022	11	1	.25	158	.07	<3	2.26	.03	.13	<2	6.9
FS 2425N	1	7	28	40	<.3	16	10	983	1.85	4	<8	<2	3	30	<.5	<3	<3	19	.37	.021	11	1	.24	253	.05	<3	1.73	.02	.11	<2	14.1
FS 2400N	1	12	37	32	<.3	18	10	146	2.06	7	<8	<2	4	8	<.5	<3	<3	20	.08	.020	17	1	.28	98	.02	<3	1.55	.01	.08	<2	24.3
FS 2375N	2	20	70	52	.3	29	12	228	2.23	10	<8	<2	4	21	<.5	<3	<3	22	.21	.026	12	2	.26	230	.06	<3	2.22	.02	.11	<2	13.2
NT 2350N	1	9	33	27	<.3	17	11	435	1.62	6	<8	<2	2	20	<.5	<3	<3	18	.24	.032	7	<1	.18	136	.07	<3	2.18	.03	.11	<2	1.1
NT 2325N	1	13	44	37	<.3	17	11	609	1.55	10	<8	<2	3	23	<.5	<3	<3	18	.26	.021	11	<1	.21	218	.04	<3	1.58	.02	.08	<2	3.8
NT 2300N	1	18	44	45	.4	20	12	214	2.05	6	<8	<2	4	15	<.5	<3	<3	24	.15	.035	12	<1	.27	178	.06	<3	2.13	.02	.11	<2	36.6
NT 2275N	1	13	121	187	.4	17	11	380	1.84	10	<8	<2	3	19	1.0	<3	<3	23	.20	.037	8	<1	.22	149	.09	<3	2.34	.03	.10	3	15.4
NT 2250N	1	30	59	61	<.3	22	14	181	2.19	10	<8	<2	5	18	<.5	<3	<3	22	.13	.043	12	2	.31	205	.06	3	2.36	.02	.09	<2	9.2
NT 2225N	<1	14	38	38	<.3	18	9	183	2.00	7	<8	<2	3	26	<.5	<3	<3	17	.29	.020	12	4	.26	274	.06	<3	2.24	.03	.10	<2	3.3
NT 2200N	1	10	50	58	<.3	13	17	315	2.17	6	<8	<2	6	14	<.5	<3	<3	23	.16	.084	14	2	.22	131	.03	<3	1.35	.01	.13	<2	14.1
NT 2175N	1	14	60	63	<.3	19	12	136	2.22	3	<8	<2	4	25	<.5	<3	<3	26	.23	.030	12	3	.33	258	.06	<3	2.53	.02	.11	<2	1.8
RE NT 2175N	1	15	61	64	.3	20	12	134	2.23	5	<8	<2	4	25	<.5	<3	<3	27	.24	.030	13	4	.33	261	.06	<3	2.56	.02	.11	<2	4.0
NT 2150N	<1	16	44	35	<.3	15	11	299	1.98	6	<8	<2	7	9	<.5	<3	<3	13	.16	.013	22	1	.34	91	.02	<3	.95	<.01	.16	<2	6.9
NT 2125N	1	45	46	45	<.3	17	17	689	2.65	7	<8	<2	7	19	<.5	<3	<3	21	.29	.011	20	20	.57	198	.04	3	1.74	.01	.30	<2	24.5
NT 2100N	2	50	79	95	<.3	33	32	381	4.63	10	<8	<2	6	22	<.5	3	<3	48	.37	.015	18	92	1.22	128	.06	<3	1.89	.01	.17	2	40.6
NT 2075N	3	86	411	215	.4	21	77	2020	2.42	9	<8	<2	6	65	2.4	6	<3	18	.80	.018	13	9	.28	433	.04	<3	1.59	.02	.15	<2	15.3
NT 2050N	5	122	648	332	.5	30	90	1275	3.35	17	<8	<2	8	32	2.1	11	<3	20	.49	.024	18	3	.38	249	.03	3	1.42	.01	.17	<2	41.1
NT 2025N	3	85	260	160	1.2	34	106	1516	3.40	19	<8	<2	13	32	1.0	10	<3	23	.45	.025	20	10	.30	468	.04	3	2.07	.01	.16	3	57.0
NT 2000N	1	32	207	70	.7	16	36	280	2.14	13	<8	<2	10	8	<.5	7	<3	16	.10	.042	20	<1	.25	118	.02	4	1.00	.01	.10	<2	29.8
NT 1975N	5	328	9978	252	22.7	24	50	3174	3.58	29	<8	<2	6	55	1.6	11	<3	20	.65	.148	14	7	.40	304	.03	3	1.59	.01	.19	<2	111.7
NT 1950N	2	26	284	420	.6	18	21	894	3.02	12	<8	<2	7	36	1.2	<3	<3	18	.52	.075	15	9	.36	215	.02	<3	1.44	.01	.11	<2	40.0
NT 1925N	2	28	81	103	<.3	26	24	1128	3.34	12	<8	<2	9	47	.5	<3	<3	24	.69	.047	16	11	.41	268	.03	<3	2.13	.01	.19	2	20.6
TN 1900N	<1	34	27	53	<.3	19	4	679	.71	4	<8	<2	<2	177	.8	<3	<3	3	20.69	.103	3	4	.54	126	.01	10	.48	.02	.05	<2	3.3
TN 1875N	1	22	17	47	<.3	24	14	295	2.12	7	<8	<2	3	24	<.5	<3	<3	24	.24	.028	11	1	.36	200	.05	3	2.29	.02	.09	<2	6.6
TN 1850N	1	29	15	38	<.3	17	10	379	1.65	9	<8	<2	3	22	<.5	<3	<3	18	.23	.127	8	<1	.21	230	.08	<3	2.19	.03	.07	<2	.6
TN 1825N	<1	11	27	36	<.3	16	9	361	1.73	6	<8	<2	3	20	<.5	<3	<3	18	.20	.036	11	<1	.27	226	.04	<3	1.81	.02	.08	<2	.7
TN 1800N	1	15	38	44	<.3	20	12	588	2.29	7	<8	<2	5	19	<.5	<3	<3	20	.24	.015	15	2	.33	233	.05	5	2.25	.01	.15	<2	8.1
TN 1775N	<1	44	73	88	<.3	19	20	999	2.33	7	<8	<2	3	18	<.5	<3	<3	22	.22	.054	13	6	.33	176	.05	4	2.42	.02	.15	<2	1.0
TN 1750N	1	13	45	68	<.3	19	21	475	2.11	8	<8	<2	5	21	<.5	<3	<3	22	.24	.030	12	5	.31	218	.06	5	2.23	.02	.16	<2	.8
TN 1725N	1	14	32	58	<.3	19	12	252	2.10	7	<8	<2	4	14	<.5	<3	<3	23	.16	.032	14	1	.35	176	.05	<3	2.11	.01	.13	<2	1.2
TN 1700N	<1	21	75	132	<.3	19	19	696	2.16	7	<8	<2	5	25	.6	<3	<3	19	.25	.030	14	4	.33	395	.07	<3	2.56	.02	.13	<2	2.0
STANDARD DS5	13	144	23	132	.3	24	12	748	2.96	24	9	<2	3	46	5.7	5	7	59	.77	.092	11	180	.68	137	.10	15	1.97	.04	.15	6	45.0

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: SOIL SS80 60C AU* BY ACID LEACHED, ANALYZED BY ICP-MS. (15 gm)
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA ____ DATE RECEIVED: JUN 29 2004 DATE REPORT MAILED: July 16/04...

BRITISH COLUMBIA CERTIFIED ASSAYER
Clarence Leong

Ruby Red Resources Inc. PROJECT LOOSE LEG FILE # A403184 Page 2

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
TN 1675N	2	25	45	51	<.3	16	15	334	2.13	7	<8	<2	7	11	<.5	<3	<3	17	.19	.014	21	2	.32	113	.04	4	1.37	.01	.12	<2	3.2
TN 1650N	2	34	49	70	<.3	19	22	990	2.30	7	<8	<2	8	15	<.5	<3	<3	19	.28	.021	20	1	.30	206	.04	<3	1.46	.01	.15	2	5.5
TN 1625N	2	40	40	79	<.3	18	110	735	2.09	8	<8	<2	10	18	.5	<3	<3	16	.33	.034	18	<1	.22	109	.03	<3	1.15	.01	.18	<2	17.4
NT 1600N	2	42	59	59	<.3	18	18	468	2.21	5	<8	<2	11	10	<.5	<3	<3	14	.46	.011	26	2	.37	130	.02	4	1.22	.01	.22	<2	10.1
NT 1575N	4	138	1215	180	1.4	22	70	1177	2.56	8	<8	<2	12	42	.9	<3	<3	13	1.16	.115	22	2	.34	239	.02	8	1.21	.01	.39	3	100.2
NT 1550N	1	29	164	176	.4	18	46	2423	2.35	5	<8	<2	7	32	1.1	<3	<3	21	.39	.079	16	6	.31	501	.05	<3	1.94	.02	.23	2	5.2
NT 1125N	<1	6	17	39	<.3	13	8	348	2.05	<2	<8	<2	6	13	<.5	<3	<3	14	.20	.012	18	<1	.34	124	.03	3	1.24	.01	.25	<2	1.4
NT 950N	1	15	32	61	<.3	22	13	1733	2.12	<2	<8	<2	6	26	<.5	<3	<3	21	.33	.018	15	21	.37	371	.05	5	1.56	.01	.23	<2	1.3
ST 2125W	1	30	42	71	<.3	21	11	1064	2.26	5	<8	<2	4	25	<.5	<3	<3	18	1.54	.039	10	11	.54	208	.05	7	1.60	.01	.16	<2	9.5
ST 2100W	3	19	44	89	<.3	22	10	222	2.54	3	<8	<2	5	18	<.5	<3	<3	24	.22	.020	12	5	.47	129	.06	<3	1.85	.02	.13	<2	3.1
ST 2075W	2	9	17	123	<.3	17	7	230	1.49	2	<8	<2	2	19	<.5	<3	<3	16	.18	.045	7	<1	.28	153	.05	<3	1.61	.03	.10	2	2.4
ST 2050W	1	10	25	71	<.3	19	8	224	2.09	<2	<8	<2	4	15	<.5	<3	<3	19	.18	.013	11	4	.35	106	.06	<3	1.71	.02	.11	<2	7.0
ST 2025W	1	8	15	112	<.3	10	5	618	1.16	<2	<8	<2	2	14	<.5	<3	<3	13	.18	.024	8	<1	.24	151	.04	<3	1.04	.01	.11	<2	<.5
ST 2000W	1	9	21	47	<.3	15	7	234	2.08	6	<8	<2	3	16	<.5	<3	<3	17	.20	.014	11	2	.38	163	.05	<3	1.79	.02	.14	<2	2.2
ST 1975W	1	9	21	43	<.3	17	7	146	1.87	<2	<8	<2	3	14	<.5	<3	<3	18	.16	.012	10	3	.36	126	.05	<3	1.74	.02	.10	<2	2.2
ST 1950W	1	9	23	50	<.3	22	9	171	2.09	5	<8	<2	2	17	<.5	<3	<3	21	.16	.020	9	4	.35	164	.07	<3	2.10	.02	.14	<2	3.7
ST 1925W	<1	9	23	49	<.3	19	8	178	2.18	3	<8	<2	4	17	<.5	<3	<3	19	.19	.022	11	5	.37	102	.06	3	1.76	.02	.14	<2	2.8
ST 1900W	2	21	22	44	<.3	21	10	113	2.53	6	<8	<2	5	10	<.5	<3	<3	18	.13	.018	14	4	.45	40	.03	<3	1.06	.01	.09	<2	9.9
ST 1875W	3	12	22	33	<.3	19	9	107	2.28	5	<8	<2	4	9	<.5	<3	<3	20	.14	.012	16	8	.44	61	.03	<3	1.23	.01	.08	<2	3.3
RE ST 1875W	1	13	21	35	<.3	19	9	109	2.31	5	<8	<2	5	9	<.5	<3	<3	21	.14	.013	17	10	.46	62	.03	<3	1.28	.01	.09	<2	7.0
ST 1850W	2	12	28	56	<.3	18	8	179	2.37	2	<8	<2	4	14	<.5	<3	<3	20	.22	.026	13	5	.43	84	.05	3	1.90	.01	.15	<2	8.2
ST 1840W	1	14	25	57	<.3	14	8	848	1.92	6	<8	<2	4	14	<.5	<3	<3	14	.27	.028	13	3	.42	107	.04	<3	.96	.01	.18	<2	4.0
ST 1825W	1	17	27	41	<.3	20	9	177	2.32	5	<8	<2	5	11	<.5	<3	<3	18	.15	.012	15	4	.48	67	.06	<3	1.63	.01	.13	<2	3.4
ST 1800W	<1	13	18	64	<.3	22	8	145	2.15	7	<8	<2	4	19	<.5	<3	<3	22	.15	.089	9	2	.31	111	.07	<3	2.32	.03	.10	<2	4.6
ST 1775W	2	14	24	50	<.3	19	10	238	2.09	5	<8	<2	3	9	<.5	<3	<3	19	.11	.024	16	5	.41	69	.03	<3	1.20	.01	.09	<2	23.2
ST 1750W	2	11	24	59	<.3	20	9	167	2.20	6	<8	<2	3	11	<.5	<3	<3	21	.12	.035	15	5	.45	99	.05	<3	1.76	.01	.08	2	5.5
ST 1725W	1	9	32	67	<.3	13	11	435	1.81	6	<8	<2	3	10	<.5	<3	<3	17	.12	.035	13	3	.35	106	.03	<3	.86	.01	.12	<2	3.3
ST 1708W	1	12	23	38	<.3	19	8	113	2.16	2	<8	<2	4	10	<.5	<3	<3	20	.10	.017	14	6	.42	63	.04	<3	1.26	.01	.09	<2	7.5
ST 1700W	<1	12	23	81	<.3	20	7	291	1.93	6	<8	<2	3	30	<.5	<3	<3	20	.25	.218	6	<1	.25	146	.08	<3	2.31	.03	.11	<2	3.8
ST 1675W	1	12	20	114	<.3	23	8	341	2.01	5	<8	<2	3	21	<.5	<3	<3	20	.20	.104	9	2	.33	162	.05	<3	2.03	.02	.10	<2	2.2
ST 1650W	2	13	19	62	<.3	20	8	162	1.95	6	<8	<2	3	16	<.5	<3	<3	19	.16	.036	12	<1	.34	126	.05	<3	1.62	.02	.08	2	5.8
ST 1625W	1	19	22	68	<.3	24	11	622	2.29	7	<8	<2	4	17	<.5	<3	<3	23	.15	.059	13	2	.39	178	.05	<3	1.95	.01	.09	<2	3.2
ST 1600W	1	90	23	82	<.3	26	13	158	2.10	8	<8	<2	3	22	<.5	<3	<3	22	.22	.051	9	<1	.32	118	.08	<3	2.36	.03	.11	<2	3.0
ST 1575W	2	13	30	63	<.3	22	8	165	2.25	4	<8	<2	4	17	<.5	<3	<3	23	.17	.024	11	<1	.32	139	.07	<3	2.18	.02	.12	<2	3.7
STANDARD DS5	12	147	26	138	.4	26	12	833	3.10	18	10	<2	3	47	5.6	4	6	62	.76	.099	12	189	.71	144	.10	16	2.09	.04	.16	5	44.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

ACME ANALYTICAL

Ruby Red Resources Inc. PROJECT LOOSE LEG FILE # A403184

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
ST 1550W	1	35	34	68	<.3	28	12	134	2.46	6	<8	<2	3	11	<.5	<3	<3	22	.08	.025	13	3	.38	188	.06	<3	2.14	.02	.10	<2	2.2
ST 1525W	1	18	24	62	<.3	22	10	142	2.24	8	<8	<2	3	9	<.5	<3	3	20	.09	.018	18	2	.47	64	.04	<3	1.20	.01	.11	<2	7.0
ST 1500W	2	16	22	82	<.3	22	10	183	2.12	7	<8	<2	3	9	<.5	<3	<3	20	.10	.025	15	<1	.42	115	.05	<3	1.52	.01	.09	<2	12.1
ST 1475W	1	15	26	82	<.3	25	8	167	1.99	6	<8	<2	3	24	<.5	<3	<3	22	.22	.055	9	1	.29	140	.08	<3	2.28	.03	.09	<2	2.0
ST 1450W	3	23	35	70	<.3	25	11	175	2.77	7	<8	<2	4	11	<.5	<3	<3	22	.11	.024	20	5	.55	120	.04	<3	1.56	.01	.11	<2	17.6
ST 1425W	2	22	34	62	<.3	24	11	147	2.63	8	<8	<2	5	10	<.5	<3	4	19	.13	.027	19	5	.48	88	.04	<3	1.40	.01	.11	<2	8.2
ST 1400W	1	10	23	106	<.3	23	10	363	1.74	6	<8	<2	2	19	<.5	<3	<3	22	.19	.116	6	1	.23	194	.08	<3	2.28	.03	.09	2	.6
ST 1375W	1	10	27	121	<.3	18	12	435	1.83	3	<8	<2	2	15	<.5	<3	<3	22	.17	.040	11	3	.33	175	.04	<3	1.43	.01	.12	<2	1.8
ST 1350W	2	10	33	77	<.3	21	11	497	1.94	5	<8	<2	2	18	<.5	<3	<3	21	.15	.046	10	1	.30	188	.06	<3	1.92	.02	.09	<2	3.6
ST 1325W	2	14	30	90	<.3	28	12	231	2.51	9	<8	<2	3	12	<.5	<3	<3	23	.11	.078	13	6	.42	216	.06	<3	1.99	.02	.10	<2	25.6
ST 1300W	2	20	54	64	<.3	29	10	129	2.22	6	<8	<2	3	25	<.5	<3	<3	18	.22	.061	11	2	.41	172	.06	3	2.19	.03	.10	<2	2.7
ST 1275W	<1	16	28	69	<.3	23	8	167	1.84	6	<8	<2	3	25	<.5	<3	<3	20	.28	.109	6	<1	.24	141	.09	3	2.43	.04	.09	<2	1.2
RE ST 1275W	1	16	26	69	<.3	23	8	164	1.84	6	<8	<2	2	24	<.5	<3	<3	20	.27	.108	6	<1	.24	141	.09	4	2.41	.04	.09	<2	1.2
ST 1250W	2	12	27	67	<.3	25	9	276	1.91	4	<8	<2	2	22	<.5	<3	<3	18	.31	.106	9	<1	.38	189	.06	3	2.04	.03	.15	2	3.1
ST 1225W	3	21	78	59	<.3	32	12	167	2.52	6	<8	<2	4	23	<.5	<3	<3	19	.20	.039	12	2	.52	188	.06	<3	2.23	.02	.12	<2	1.4
ST 1200W	3	15	36	65	<.3	26	12	311	2.69	7	<8	<2	4	9	<.5	<3	<3	25	.08	.058	15	4	.50	200	.04	4	2.04	.01	.09	<2	4.7
ST 1175W	2	10	24	62	<.3	24	8	307	2.03	4	<8	<2	3	16	<.5	<3	<3	18	.15	.132	9	1	.34	200	.07	<3	2.06	.02	.10	<2	2.5
ST 1150W	2	14	23	64	<.3	22	10	272	2.10	5	<8	<2	2	15	<.5	<3	<3	17	.22	.081	15	1	.51	114	.04	3	1.67	.01	.13	<2	4.1
ST 1125W	2	17	30	78	<.3	32	10	174	2.40	6	<8	<2	4	19	<.5	<3	<3	21	.19	.072	13	<1	.42	193	.06	6	2.25	.02	.13	<2	2.5
ST 1100W	4	33	50	92	.4	30	16	421	3.16	10	<8	<2	7	21	<.5	<3	<3	16	.17	.037	22	2	.49	113	.03	3	1.53	.02	.11	<2	21.9
ST 1075W	3	14	52	78	<.3	35	12	158	2.55	8	<8	<2	4	14	<.5	<3	<3	28	.13	.074	12	5	.33	188	.07	4	2.39	.02	.13	<2	2.4
ST 1050W	2	12	46	74	<.3	32	10	151	2.14	6	<8	<2	3	23	<.5	<3	3	22	.16	.047	11	1	.32	177	.07	<3	2.38	.02	.11	2	2.6
ST 1025W	1	11	19	65	<.3	20	6	203	1.57	6	<8	<2	2	29	<.5	<3	<3	19	.27	.249	4	<1	.18	175	.11	<3	2.51	.04	.06	<2	1.9
ST 1000W	2	23	42	61	<.3	26	11	201	2.29	7	<8	<2	4	19	<.5	<3	<3	22	.12	.050	15	2	.34	198	.07	<3	2.15	.02	.08	<2	7.9
ST 975W	5	25	37	54	<.3	23	11	170	2.76	10	<8	<2	7	7	<.5	<3	<3	24	.06	.031	27	4	.38	88	.02	3	1.42	.01	.08	<2	12.1
ST 950W	3	21	52	90	<.3	28	16	242	2.91	6	<8	<2	6	11	<.5	<3	<3	25	.14	.033	21	7	.45	114	.04	3	1.98	.01	.13	2	5.8
ST 940W	4	30	40	59	<.3	30	18	661	3.61	13	<8	<2	5	22	.5	<3	<3	17	.68	.044	17	4	.74	79	.03	4	1.54	.01	.10	<2	6.8
ST 925W	4	32	34	90	<.3	47	19	433	3.03	8	<8	<2	7	14	<.5	3	<3	24	.24	.043	22	11	.47	134	.04	4	1.80	.01	.13	<2	32.7
ST 900W	3	17	31	65	<.3	35	13	142	2.72	6	<8	<2	4	14	<.5	<3	<3	28	.13	.024	15	4	.52	190	.07	3	2.19	.01	.10	<2	8.2
ST 875W	3	12	19	49	<.3	27	9	210	1.99	4	<8	<2	2	25	<.5	<3	<3	22	.22	.069	8	<1	.25	201	.11	<3	2.65	.03	.08	<2	18.3
ST 850W	2	11	15	35	<.3	30	9	113	1.65	3	<8	<2	4	28	<.5	<3	<3	18	.17	.086	9	<1	.23	183	.09	6	2.29	.04	.08	<2	16.0
ST 825W	6	19	32	77	<.3	34	15	192	3.51	7	<8	<2	7	12	<.5	<3	<3	35	.09	.062	18	16	.52	183	.06	3	2.52	.01	.09	2	7.9
ST 800W	4	12	30	52	<.3	23	10	129	3.43	8	<8	<2	6	6	<.5	<3	<3	37	.04	.054	17	10	.43	107	.05	<3	2.21	.01	.07	<2	4.6
ST 775W	3	10	19	42	<.3	19	8	155	2.91	8	<8	<2	5	7	<.5	<3	<3	33	.04	.042	15	2	.30	87	.06	<3	1.90	.01	.07	<2	8.5
STANDARD DS5	13	144	25	135	.4	25	12	756	3.17	19	8	<2	3	46	5.6	4	6	60	.74	.092	12	177	.69	140	.10	13	2.00	.04	.15	6	44.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

ACME ANALYTICAL

Ruby Red Resources Inc. PROJECT LOOSE LEG FILE # A403184

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
ST 750W	4	9	16	50	<.3	16	6	92	2.65	7	<8	<2	6	8	<.5	<3	<3	26	.06	.021	17	2	.35	51	.02	6	1.31	.01	.08	2	28.0
ST 725W	2	15	38	57	<.3	43	12	438	3.35	6	<8	<2	9	50	<.5	<3	<3	27	.68	.024	19	15	.55	87	.07	<3	3.16	.02	.09	<2	14.1
ST 700W	3	18	33	70	<.3	25	11	102	2.97	10	<8	<2	5	13	<.5	<3	<3	27	.08	.021	15	2	.44	118	.04	<3	2.06	.01	.07	<2	6.1
ST 683W	3	11	38	51	<.3	18	15	436	2.62	7	<8	<2	3	16	<.5	<3	<3	29	.22	.028	12	2	.34	87	.05	<3	1.34	.02	.11	<2	3.4
ST 675W	<1	15	23	43	.3	21	9	171	1.75	5	<8	<2	4	20	<.5	<3	<3	20	.15	.042	5	<1	.18	113	.09	5	2.48	.04	.06	<2	3.0
ST 650W	3	19	33	53	<.3	19	9	133	3.18	11	<8	<2	7	7	<.5	<3	<3	31	.03	.044	15	4	.40	99	.04	5	2.14	.01	.06	<2	13.3
ST 625W	2	17	33	52	<.3	21	12	149	2.45	5	<8	<2	5	16	<.5	<3	<3	27	.09	.037	9	<1	.27	167	.08	<3	2.69	.02	.07	<2	7.2
ST 600W	3	24	43	59	<.3	22	12	132	3.03	10	<8	<2	7	15	<.5	<3	<3	29	.08	.055	12	6	.33	123	.07	<3	2.63	.02	.08	<2	36.5
ST 575W	3	12	20	50	<.3	29	12	157	2.67	7	<8	<2	4	19	<.5	<3	<3	28	.15	.076	7	1	.25	140	.10	<3	3.64	.03	.06	<2	6.7
ST 550W	4	27	52	91	<.3	23	23	1675	3.67	8	<8	<2	4	20	<.5	<3	<3	31	.24	.054	17	7	.31	109	.05	<3	1.62	.01	.10	<2	.7
ST 525W	8	20	43	52	<.3	27	14	124	4.60	12	<8	<2	9	7	<.5	<3	<3	32	.03	.055	17	10	.42	67	.02	<3	1.86	.01	.07	<2	9.6
ST 500W	12	26	38	69	<.3	26	14	133	4.14	15	<8	<2	8	10	<.5	<3	<3	28	.08	.034	19	6	.36	75	.01	<3	1.52	.01	.07	<2	18.7
ST 475W	7	15	28	64	<.3	33	17	115	3.78	13	<8	<2	7	10	<.5	<3	<3	23	.04	.036	16	11	.51	100	.02	3	1.90	.01	.07	<2	15.7
ST 450W	6	30	31	76	<.3	34	15	140	4.66	24	<8	<2	9	9	<.5	<3	<3	16	.02	.041	19	7	.49	37	<.01	<3	1.16	.01	.05	<2	10.8
ST 425W	6	27	355	337	.4	45	28	285	5.57	19	<8	<2	6	16	1.2	<3	<3	29	.09	.036	14	12	.28	133	.03	<3	1.67	.01	.10	<2	64.3
ST 400W	4	31	47	131	<.3	74	23	198	4.17	19	<8	<2	5	19	<.5	<3	<3	25	.13	.078	8	1	.25	123	.06	<3	2.13	.02	.09	<2	27.5
ST 375W	2	17	35	146	<.3	38	17	647	3.45	14	<8	<2	5	19	<.5	<3	<3	30	.17	.043	12	7	.37	133	.06	<3	1.93	.01	.12	2	1.1
ST 350W	2	16	32	152	<.3	43	16	432	2.70	8	<8	<2	5	15	<.5	<3	<3	26	.15	.048	9	<1	.27	94	.08	<3	2.36	.02	.10	3	1.9
ST 325W	5	46	52	169	<.3	48	25	1418	4.80	22	<8	<2	7	30	<.5	<3	<3	22	.42	.062	14	11	.42	139	.03	<3	1.60	.01	.12	2	1.0
ST 313W	2	61	113	190	<.3	35	19	986	3.63	12	<8	<2	3	37	.5	<3	<3	31	1.83	.062	14	28	1.81	61	.06	<3	1.82	.01	.07	3	10.6
ST 300W	4	38	131	193	.4	43	26	933	4.70	15	<8	<2	5	16	<.5	<3	<3	30	.22	.060	13	14	.44	78	.06	<3	2.24	.02	.08	3	1.8
RE ST 300W	5	37	129	189	<.3	41	26	913	4.60	14	<8	<2	5	15	<.5	<3	<3	29	.21	.058	13	13	.43	75	.05	<3	2.21	.02	.08	3	2.8
ST 275W	14	88	33	147	<.3	62	25	335	7.87	34	<8	<2	9	8	<.5	<3	<3	20	.04	.052	14	11	.41	68	.01	<3	1.67	.01	.06	3	1.7
ST 250W	1	11	10	65	<.3	45	10	248	2.09	5	<8	<2	4	19	<.5	<3	<3	22	.15	.040	5	<1	.15	59	.12	<3	3.44	.04	.05	<2	1.3
ST 225W	5	48	27	104	<.3	33	13	164	4.35	23	<8	<2	7	7	<.5	<3	<3	22	.04	.028	18	7	.46	49	.01	<3	1.35	<.01	.07	2	2.1
ST 200W	2	12	17	101	<.3	36	13	280	2.46	6	<8	<2	3	15	<.5	<3	<3	30	.12	.034	6	<1	.20	66	.12	<3	2.84	.03	.06	<2	2.9
ST 175W	5	30	39	336	<.3	38	18	317	4.36	15	<8	<2	4	11	<.5	<3	<3	42	.08	.033	14	18	.56	88	.04	<3	1.95	.01	.07	<2	3.4
ST 150W	2	15	27	187	<.3	54	13	472	2.66	4	<8	<2	4	17	<.5	<3	<3	26	.13	.080	8	1	.25	91	.10	<3	2.51	.03	.09	2	2.6
ST 125W	5	40	56	201	<.3	54	21	312	5.18	17	<8	<2	6	17	<.5	<3	<3	24	.15	.070	12	12	.34	58	.04	<3	1.84	.01	.08	2	5.8
ST 120W	8	41	67	178	<.3	34	24	587	5.80	18	<8	<2	7	14	<.5	<3	<3	35	.13	.060	16	16	.32	93	.03	<3	1.58	.01	.09	3	4.0
ST 100W	2	21	35	236	<.3	43	16	432	3.35	7	<8	<2	4	22	.5	<3	<3	31	.25	.068	10	2	.28	88	.08	<3	2.35	.02	.10	<2	1.8
ST 75W	<1	11	20	77	<.3	29	11	672	2.34	6	<8	<2	3	22	<.5	<3	<3	23	.25	.111	5	<1	.16	98	.12	<3	3.98	.03	.05	<2	1.1
ST 50W	3	20	47	147	<.3	40	21	452	3.86	12	<8	<2	4	13	<.5	<3	<3	30	.11	.042	15	10	.35	96	.05	<3	2.15	.01	.09	2	2.1
ST 25W	1	17	33	174	<.3	44	18	410	3.25	9	<8	<2	4	17	<.5	<3	<3	30	.18	.048	9	5	.28	111	.07	<3	2.49	.02	.08	2	2.2
STANDARD DS5	12	145	25	131	<.3	26	12	774	3.20	18	<8	<2	3	49	5.6	4	6	62	.74	.091	11	189	.69	143	.10	15	2.03	.04	.15	6	45.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
ST 00W	3	15	29	232	<.3	41	13	181	2.98	9	<8	<2	3	16	.8	<3	<3	28	.10	.055	10	8	.32	73	.07	<3	2.67	.02	.07	<2	2.0
L1150 1100N	<1	7	23	85	<.3	16	11	800	2.09	<2	<8	<2	4	25	<.5	<3	<3	14	.29	.024	13	6	.36	473	.06	<3	1.81	.02	.25	<2	2.4
L1150 1075N	<1	7	12	29	<.3	12	6	197	1.81	<2	<8	<2	3	27	<.5	<3	<3	12	.33	.016	9	3	.25	277	.10	<3	2.71	.03	.16	<2	3.4
L1150 1050N	<1	7	18	56	<.3	12	6	289	1.80	<2	<8	<2	4	23	<.5	<3	<3	11	.30	.023	14	7	.36	204	.06	<3	1.75	.01	.23	<2	1.4
L1150 1025N	<1	8	12	253	<.3	13	5	470	1.44	4	<8	<2	2	51	<.5	<3	<3	14	.47	.083	8	1	.25	446	.06	8	1.73	.03	.25	<2	1.8
L1150 1000N	<1	7	12	80	<.3	12	5	364	1.55	<2	<8	<2	3	38	<.5	<3	<3	12	.37	.043	7	<1	.23	333	.08	6	1.96	.03	.21	<2	1.4
L1150 975N	<1	10	18	41	<.3	13	7	138	1.71	4	<8	<2	4	23	<.5	<3	<3	10	.27	.049	11	<1	.27	183	.05	6	1.58	.02	.20	<2	4.8
L1150 950N	<1	25	22	27	<.3	22	12	161	2.35	6	<8	<2	6	23	<.5	<3	<3	16	.89	.032	18	11	.60	97	.03	<3	1.18	.01	.20	<2	36.2
L1150 925N	<1	10	14	41	<.3	12	7	130	1.78	<2	<8	<2	4	28	<.5	<3	<3	10	.38	.025	11	<1	.27	107	.06	7	1.65	.02	.30	<2	22.2
L1150 850N	<1	9	13	32	<.3	14	7	97	1.84	<2	<8	<2	5	28	<.5	<3	<3	10	.30	.023	13	1	.30	190	.06	6	1.72	.02	.21	<2	1.8
L1150 825N	<1	12	43	36	<.3	19	12	167	2.37	4	<8	<2	6	30	<.5	<3	<3	15	.41	.016	15	4	.35	189	.07	<3	2.28	.02	.29	<2	3.8
L1150 800N	1	13	40	44	<.3	19	16	605	2.48	7	<8	<2	7	23	<.5	<3	<3	13	.35	.033	19	6	.46	150	.05	<3	1.59	.01	.37	<2	9.6
L1150 775N	1	29	66	44	<.3	26	15	291	2.58	8	<8	<2	8	18	<.5	<3	<3	16	.66	.027	21	11	.56	156	.02	<3	1.10	<.01	.17	<2	22.3
L1150 750N	<1	11	100	60	<.3	18	13	436	2.27	2	<8	<2	6	29	<.5	<3	<3	12	.37	.033	15	1	.28	229	.06	5	1.86	.02	.24	<2	3.8
L1150 725N	1	13	27	46	<.3	23	17	792	2.27	6	<8	<2	8	24	<.5	<3	<3	12	.24	.020	18	1	.33	241	.06	<3	1.68	.02	.24	<2	16.5
L1150 700N	1	14	31	49	<.3	23	17	859	2.24	2	<8	<2	8	26	<.5	<3	<3	13	.30	.015	16	3	.35	272	.07	<3	1.82	.02	.29	<2	5.4
L1150 675N	<1	22	34	54	<.3	26	15	735	2.59	3	<8	<2	6	26	<.5	<3	<3	14	.35	.041	17	10	.48	369	.05	<3	1.65	.01	.42	<2	7.2
RE L1150 675N	<1	23	35	53	<.3	27	15	742	2.60	3	<8	<2	7	26	<.5	<3	<3	14	.36	.041	17	14	.48	371	.05	<3	1.68	.01	.42	<2	5.4
L1150 625N	2	15	26	58	<.3	19	10	944	1.95	<2	<8	<2	7	26	<.5	<3	<3	15	.35	.025	18	6	.34	261	.05	<3	1.55	.01	.24	<2	5.3
L1150 600N	<1	47	36	88	<.3	23	18	700	2.28	<2	<8	<2	7	30	<.5	<3	<3	13	.45	.046	16	7	.37	415	.04	4	1.64	.02	.38	<2	7.0
L1150 575N	1	12	22	49	<.3	19	12	371	2.49	<2	<8	<2	7	17	<.5	<3	<3	14	.30	.015	17	7	.44	198	.05	5	1.90	.01	.32	<2	6.8
L1150 550N	1	31	29	42	<.3	24	15	149	2.59	5	<8	<2	10	16	<.5	<3	<3	16	.32	.019	22	11	.48	112	.04	3	1.51	.01	.21	<2	20.0
L1150 525N	<1	23	43	59	<.3	28	17	359	2.61	4	<8	<2	9	13	<.5	<3	<3	14	.23	.019	19	9	.47	147	.04	<3	1.61	.01	.30	<2	17.3
L1150 500N	<1	29	38	47	<.3	24	16	596	2.57	5	<8	<2	7	16	<.5	<3	<3	14	1.02	.033	18	10	.59	167	.03	<3	1.29	.01	.32	<2	8.1
L1150 475N	<1	36	35	40	<.3	23	14	650	2.35	6	<8	<2	5	32	<.5	<3	<3	12	3.85	.045	14	15	.64	202	.02	4	1.11	.01	.25	<2	11.6
L1150 450N	1	34	30	42	<.3	23	15	454	2.32	7	<8	<2	4	45	<.5	<3	<3	11	3.38	.055	13	15	1.17	181	.02	4	.94	.01	.17	<2	19.7
L1150 425N	2	34	10	20	.4	24	10	318	1.39	9	<8	<2	<2	163	.5	3	<3	5	15.39	.130	4	13	2.06	84	.01	17	.46	.01	.13	<2	31.4
L1150 400N	<1	13	20	44	<.3	22	12	578	2.75	2	<8	<2	6	16	<.5	<3	<3	17	.38	.019	17	19	.61	154	.07	<3	1.77	.01	.39	<2	2.6
L1150 375N	2	51	15	31	<.3	41	17	563	2.62	7	<8	<2	2	87	.6	3	<3	27	9.20	.101	7	107	1.67	165	.05	10	1.23	.01	.37	<2	16.1
L1150 350N	<1	8	21	39	<.3	17	9	254	2.22	2	<8	<2	5	13	<.5	<3	<3	15	.24	.013	15	9	.47	145	.05	<3	1.70	.01	.23	<2	5.2
L1150 325N	<1	12	25	34	<.3	23	10	168	2.43	2	<8	<2	6	15	<.5	<3	<3	16	.27	.031	17	21	.54	117	.05	4	1.71	.01	.33	<2	3.9
L1150 300N	<1	19	26	47	<.3	41	14	279	2.90	4	<8	<2	5	11	<.5	<3	<3	26	.28	.015	16	83	.74	125	.06	4	1.70	.01	.31	<2	4.8
L1150 275N	<1	16	24	44	<.3	23	11	656	2.64	6	<8	<2	6	11	<.5	<3	<3	15	.40	.016	19	18	.63	146	.04	<3	1.42	.01	.29	<2	14.1
L1150 250N	<1	17	29	37	<.3	26	12	383	2.71	3	<8	<2	6	15	<.5	<3	<3	19	.31	.018	17	28	.57	141	.06	<3	1.80	.01	.32	<2	1.7
STANDARD DS5	12	141	25	132	.3	26	12	754	3.00	18	<8	<2	3	46	5.3	<3	6	60	.75	.091	12	189	.68	137	.10	16	2.01	.04	.15	6	45.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data ___ FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L1150 225N	2	24	27	33	<.3	34	16	349	2.69	6	<8	<2	7	14	<.5	<3	<3	22	.36	.018	19	38	.74	106	.04	7	1.40	.01	.19	<2	2.8
L1150 200N	3	10	18	46	<.3	16	8	508	2.08	4	<8	<2	5	12	<.5	<3	<3	16	.25	.013	15	8	.43	130	.05	5	1.32	.01	.15	<2	4.7
L1150 175N	1	20	26	35	<.3	22	11	202	2.61	3	<8	<2	7	10	<.5	<3	<3	16	.45	.010	22	10	.64	103	.04	4	1.44	.01	.12	<2	2.3
L1150 150N	<1	37	29	33	<.3	32	15	354	2.37	6	<8	<2	5	19	<.5	<3	<3	21	3.07	.032	14	49	.91	92	.02	4	1.00	<.01	.14	<2	9.8
L1150 125N	<1	53	15	36	<.3	37	126	749	1.98	33	<8	<2	6	57	<.5	3	<3	11	3.02	.086	11	19	.82	124	.01	15	.87	.01	.18	<2	2.7
L1150 100N	1	16	24	34	<.3	20	10	203	2.67	6	<8	<2	7	10	<.5	<3	<3	16	.44	.014	18	12	.58	107	.03	5	1.46	.01	.13	<2	32.5
RE L1150 100N	2	15	20	35	<.3	20	10	200	2.68	7	<8	<2	8	10	<.5	<3	<3	17	.43	.015	19	14	.59	106	.03	7	1.46	.01	.13	<2	3.0
L1150 75N	2	11	18	48	<.3	19	9	386	2.70	3	<8	<2	6	11	<.5	<3	<3	16	.32	.012	16	11	.51	202	.06	6	2.16	.01	.22	<2	1.0
L1150 50N	1	12	19	41	<.3	19	10	302	2.63	2	<8	<2	6	12	<.5	<3	<3	16	.29	.011	16	12	.51	153	.05	<3	1.77	.01	.18	<2	.9
L1150 25N	1	15	21	41	<.3	20	10	262	2.74	4	<8	<2	7	12	<.5	<3	<3	16	.34	.011	18	12	.57	161	.05	3	1.73	.01	.17	<2	2.6
L1150 00N	2	12	19	42	<.3	17	9	266	2.22	5	<8	<2	5	9	<.5	<3	<3	16	.22	.016	17	8	.43	94	.04	<3	1.35	<.01	.11	<2	1.8
STANDARD DS5	13	142	24	133	.3	25	12	751	3.00	18	8	<2	3	46	5.6	4	5	59	.74	.092	12	188	.68	137	.10	14	1.98	.04	.15	7	45.5

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA


Creek
L 7656
Lewis
Sand and Gravel
M.C.'s
M.C.
Tracy
Creek
Fault
Line NT
Line ST
Fort Steele Formation Quartzites
Lower Aldridge Formation
Grundy
6855
LEGEND
LOWER ALDRIDGE FORMATION
A1d Buff-weathering dolomitic siltstone
A1c Interbedded argillite and siltstone. Black, grey and greenish grey
A1b Carbonate marker unit. Dolomitic argillite or siltstone
A1a Medium to dark grey to black, finely laminated argillite and siltstone
FORT STEELE FORMATION
Massive to faintly banded quartzite, interbedded darker grey siltstone
Mafic Dikes Green, brown where carbonate-altered
Syenite White to pale green, slightly pink. Coarse feldspars common
Gabbro Dark green, coarse to medium grained
Adit
Trench
Rock Sample (eg.L-32)
Bedding
Cleavage
Fracture cleavage
Jointing
Quartz vein
GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT
27,651
Ruby Red Resources Inc.
LOOSE LEG PROPERTY
GEOLOGY
ROCK & CONTOUR SOIL GEOCHEMISTRY
GOLD (ppb) & COPPER (ppm) VALUES
Figure: 3


Creek
Lewis
L 7656
Sand and Gravel
M.C.'s
M.C.
L 142
L 6855
Grundy
Line ST
Line NT
Line FS
L12
L13
L14
27.651
GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT
Ruby Red Resources Inc.
LOOSE LEG PROPERTY
ROCK & CONTOUR SOIL GEOCHEMISTRY
LEAD, ZINC & SILVER VALUES (in ppm)
Scale: 1:5,000
Date:
Mapsheets: 082G072/82
Figure: 4
Datum: Nad 83