

REPORT ON THE 2004 DIAMOND DRILL PROGRAM

ON THE TODD CREEK PROPERTY

SKEENA MINING DIVISION,

STEWART GOLD CAMP,

NORTHWESTERN BRITISH COLUMBIA

LATITUDE 56° 15' NORTH

LONGITUDE 129° 46' WEST

NTS 104 A/5, 104 A/4

BY

GEOFINE EXPLORATION CONSULTANTS LTD.

FOR

LATEEGRA RESOURCES CORP.

DECEMBER 200

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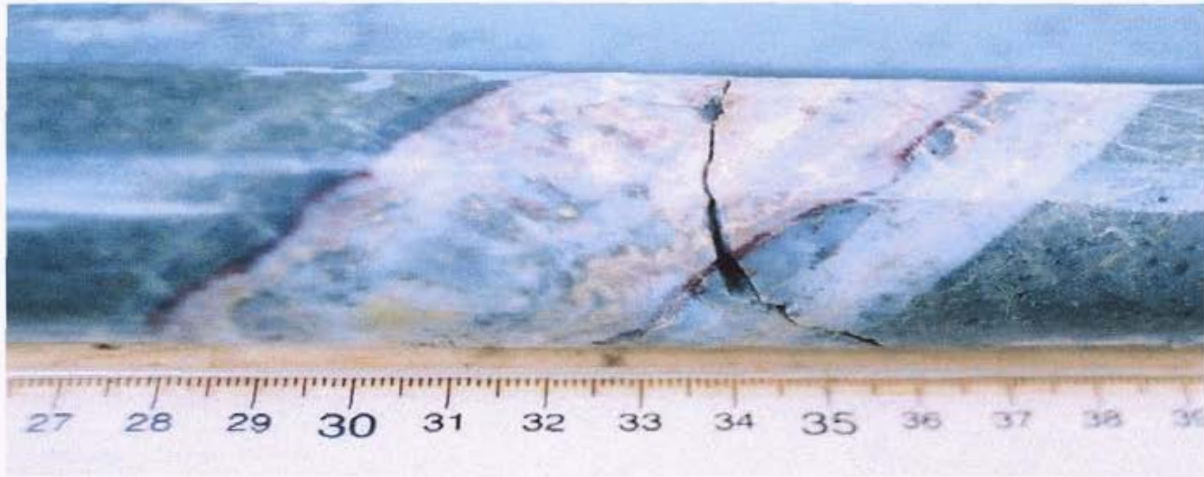
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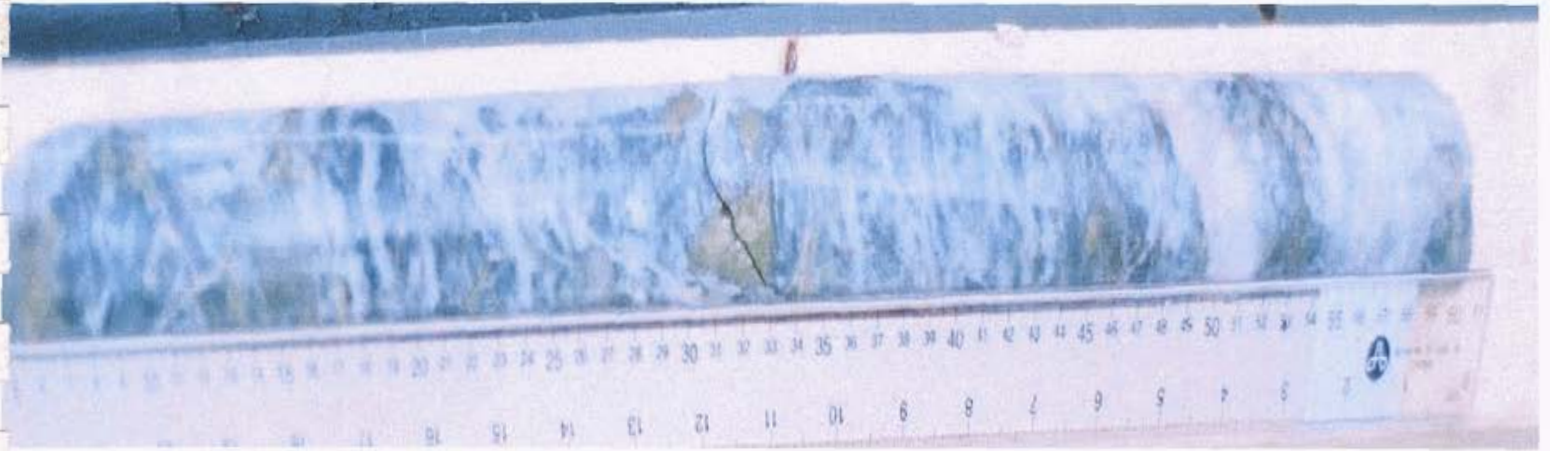
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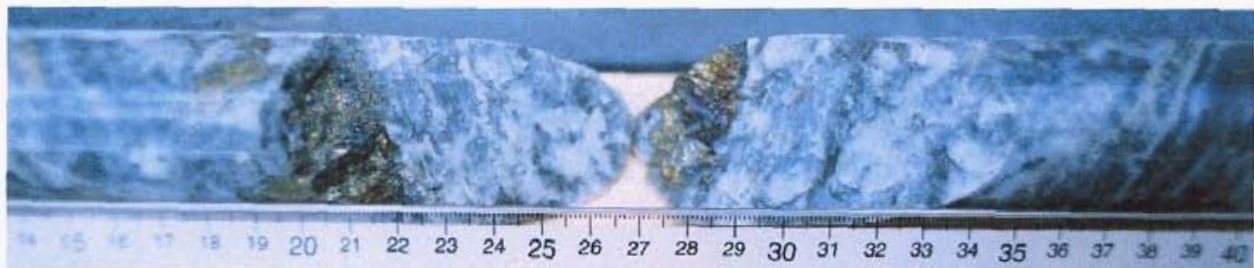
DECEMBER 2004



**BLEBBY CPY IN HEMATITE-QUARTZ MULTIPHASE BRECCIA VEIN,
(M TYPE MINERALIZATION) DDHSZD04-02A, SOUTH ZONE DEPOSIT**



M TYPE MINERALIZATION, SOUTH ZONE DEPOSIT, DDHSZD04-02A



**CLOSE UP OF M TYPE MINERALIZATION SHOWING
COARSE BLEBBY CPY**

FRONTSPIECE PHOTO 1

SUMMARY - 2004 TODD CREEK DRILL PROGRAM:

The Todd Creek Property is located in the historic Stewart Gold Camp and straddles the Todd Creek Valley, approximately 35 km northeast of Stewart, Northwestern British Columbia. The Property comprises 414 claim units in 24 mineral claims, which are registered in the name of Geofine Exploration Consultants Ltd. ("Geofine") on behalf of Geofund, a private investment group.

Lategra Resources Corp. ("LEG") holds the property under option from Geofine and can earn a 100% interest by fulfilling escalating option payments and work conditions. The LEG interest is subject to a Geofund 2.5% NSR.

The 2004 exploration program totalled about \$329,000 and consisted of a number of phases:

PHASE 1A: Drill Target Selection:

The historic database was reviewed in May to prioritize drill targets on the Todd Creek Property. Two priority drill target areas were identified: 1) the South Zone deposit and its apparent northern extensions i.e., the Gold Gully-MEXT and NEXT Zones; and, 2) the Fall Creek East F1 and North A Zones, located about 4 km north of the South Zone deposit.

The 2004 diamond drill program proposed by Geofine is shown in Table S1 and the exploration rationale is described below.

TABLE S1: PROPOSED 2004 DRILL PROGRAM, TODD CREEK PROPERTY:

AREA 1, SOUTH ZONE TARGET AREA:

TARGET:	HOLES:	METERS:
i. SOUTH ZONE DEPOSIT	4	755
ii. GOLD GULLY-MEXT ZONES	4	330
iii. NEXT ZONE	<u>1</u>	<u>175</u>
AREA 1, PHASE 1 TOTALS:	9	1260

AREA 2, FALL CREEK, ORANGE MOUNTAIN TARGET AREAS:

TARGET:	HOLES:	METERS:
i. FALL CREEK EAST F1 ZONE	3	255
ii. NORTH A ZONE	<u>2</u>	<u>280</u>
AREA 2, PHASE 1 TOTALS:	5	535

AREA 1. i) SOUTH ZONE DEPOSIT:

The South Zone deposit ("SZD") is hosted by the South Zone Structure ("SZS") and is reported to contain drill indicated reserves of 207,000 tonnes grading 5.48 g Au/t (Hemlo Gold Mines Inc., 1988 Annual Report), along with significant copper credits. The mineralization mainly comprises epithermal to mesothermal, multiphase hematite-quartz breccia veins containing coarse blebs of chalcopyrite ("M Type" mineralization; Frontpiece Photo 1). There is an apparent thickening of the SZD near the Camp Creek Fault and it is in this area that Noranda obtained some of its widest and highest grade drill intersections e.g., 6.12 g Au/t and 0.35% Cu over 6.1 m; 8.83 g Au/t and 0.45% Cu over 11.7 m; and, 3.61 g Au/t and 0.27% Cu over 29.75 m, including 6.91 g Au/t and 0.31% Cu over 8.15 m. These results, when plotted on Vertical Longitudinal Sections 1 and 1.1 ("VLS 1", "VLS 1.1" attached to this Summary) are interpreted as evidence of possible plunging ore shoot morphologies in which the higher-grade mineralization is concentrated. Geofine proposed four 2004 confirmation and step out holes on the SZD to evaluate the postulated shoots (Table S1).

AREA 1. ii) GOLD GULLY-MEXT ZONE, iii) NEXT ZONE:

The Gold Gully-MEXT ("GMZ") and NEXT Zones have never been evaluated with diamond drilling. They are located approximately 300 and 500 m north, respectively, of the northern most Noranda historic hole on the SZD. Exploration conducted by Geofine in 1999 discovered the GMZ and work in 2000 suggested that the SZD mineralization continues along strike to the north, to and beyond the NEXT Zone.

Some of the strongest gold-copper mineralization has been found to the north of the SZD in talus at the bottom of the cliff face in which the GMZ is located. The mineralization mainly comprises massive to disseminated specular hematite +/- pyrite and chalcopyrite in multiphase breccia veins ("Spec Type"); and, coarse disseminations of blebby chalcopyrite in multiphase quartz-hematite breccia veins (M Type). The orthogonal structural fabric, which includes the MEXT and NEXT Zone faults, is considered conducive to the development of plunging shoot morphologies. A total of 4 initial holes were proposed on the GMZ and one on the NEXT Zone (Table S1).

AREA 2. i) FALL CREEK EAST F1 ZONE:

The Fall Creek Target Area ("FCTA") is located about 4 km north of the NEXT Zone and straddles the east flowing Fall Creek. The area is of general interest because the Yellow Bowl Target Area is located south of the FCTA and the Orange Mountain Epithermal Target Area ("OMTA"), including the Amarillo Zone, is located immediately to the north.

The FCTA and southern part of the OMTA are characterized by numerous quartz-carbonate-chalcopyrite-pyrite +/- hematite, barite fuchsite multi-phase breccia veins (e.g., Fall Creek East F1 and West Zones, Ice Creek Zone, North A Zone, B Zone). As historic work has indicated, the veins can have significant gold and copper contents.

The East F1 Zone was discovered in 1986 as a follow-up of anomalous values returned in a soil

survey on the south side of Fall Creek. During 1986 to 1989 Noranda completed four holes totalling 368 m. Significant intersections include:

Hole 88-45: 0.43 g Au/t and 0.041% Cu over 48.7 m
incl. 6.72 g Au/t and 0.68% Cu over 1.45 m

Hole 88-46: 0.52 g Au/t and 0.058% Cu over 52.25 m
incl. 12.10 g Au/t and 0.58% Cu over 1.25 m

Hole 88-47: 1.24 g Au/t and 0.39% Cu over 31.5 m
incl. 3.14 g Au/t and 0.97% Cu over 11 m
incl. 5.96 g Au/t and 0.50% Cu over 7.9 m
incl. 24.14 g Au/t and 3.79% Cu over 1 m

Hole 88-48: 1.27 g Au/t and 0.12% Cu over 27.85 m
Incl. 3.94 g Au/t and 0.31% Cu over 7.90 m
incl. 4.71 g Au/t and 0.50% Cu over 4.75 m
incl. 15.22 g Au/t and 1.97% Cu over 1 m

IP and gold soil geochemical anomalies delineate the vein systems of the East and West Zones over a 900 by 450 m area. The East F1 Zone has an apparent strike length of over 800 m and a vertical extent of over 300 m. Noranda tested the zone with diamond drilling over a strike length of 100 m and to a depth of 50 m. Geofine proposed a Phase 1, three-hole 2004 diamond drill program comprising 255 m to follow-up the significant mineralization (Table S1).

AREA 2. ii) NORTH A ZONE:

The North A Zone is located in the OMTA on the north side of Fall Creek. It was a Newmont discovery and yielded significant results. The zone is described as northwest trending and vertically to steeply west dipping, up to 30 m wide and comprised of 0.1-2 m wide quartz, chalcopyrite, pyrite, hematite and breccia veins. The veins are commonly banded and brecciated and have been traced for 320 m. Trenching results ranged up to 3.8 g Au/t across 14.3 m.

Noranda tested the zone with 9 holes and the significant results include:

incl. 3.47 g Au/t, 0.75% Cu over 31.85 m
14.47 g Au/t, 2.06% Cu over 5.95 m
2.83 g Au/t, 0.58% Cu over 1.95 m
3.95 g Au/t, 0.22% Cu over 2.00 m
3.43 g Au/t, 0.73% Cu over 1.70 m
6.21 g Au/t, 0.60% Cu over 1.75 m

In 1990, Noranda drilled Hole 90-49 on an IP anomaly located about 85 m south of Fall Creek that appears to represent the along strike extension of the North A Zone. The hole returned anomalous copper, gold and zinc values over a core length of 16.4 m including 3.37 g Au/t and 0.27% Cu over a 2.85 m core length. The intersection, along with an IP anomaly located 100 m further south, suggest the North A Zone has a strike length of at least 500 m. The zone remains open to the southeast and also to the northwest, where Holes 88-43 and 88-44 returned a number of interesting assays including 2.74 g Au/t and 0.41% Cu over 3 m and 2.57 g Au/t over 3 m, respectively.

In 1997, Geofine located the southern extension of the North A Zone, south of Fall Creek. Contiguous chip samples over a 13.5 m width averaged 330 ppb Au and 0.40% Cu, including 3 m averaging 2.16 g Au/t, 8.7 g Ag/t, 1.28% Cu, and 0.15% Zn. A 1 m chip sample from the zone north of Fall Creek returned 44.81 g Au/t and 3.28% Cu. In 1999, the outcrop was re-sampled with an expanded width and returned 44.18 g Au/t and 3.30% Cu over 2 m. The next outcrop, located about 2 m to the south, was evaluated with three contiguous samples that returned 1.58 g Au/t and 1.20% Cu over 2 m; 20.14 g Au/t and 0.48% Cu over 2 m; and 0.63 g Au/t and 0.28% Cu over 2 m.

The Phase 1 2004 diamond drilling activities proposed by Geofine on the North A Zone contemplated the drilling of two holes totalling about 280 m. DDHAZ04-01 was proposed to follow-up the wide intersection of 1.51 g Au/t and 0.34% Cu over 16.75 m in DDH 88-41; the outcrop sample near Trench 5, which returned 44.18 g gold/t and 3.30% copper over 2 m; and, the gold values in additional outcrop samples, which ranged up to 4.04 g Au/t

DDHAZ04-02 was proposed to provide additional information on the strong intersection in DDH88-22 i.e., 3.47 g Au/t and 0.75% Cu over 31.85 m, including 14.47 g Au/t, 2.06% Cu over 5.95 m. The hole would be continued to evaluate the mineralization intersected near the bottom of DDH88-40 i.e., 1.64 g Au/t and 0.45% Cu over 8.9 m.

PHASE 1B: 2004 FIELD PROGRAM:

The 2004 field program was carried out mainly from July 8 to August 9, 2004 and was supervised by David Molloy, P. Geo. (APGO, BCAPEG) and David Kennedy, P. Geo. (BCAPEG). The work included grid restoration, topographic surveys, hole spotting, camp installation, diamond drilling, core logging and sampling, the collection of 3 large composite samples of mineralized talus and reclamation. The 6 confirmation and step out drill holes are described in Table D1 and comprise 761 m. Five of the holes were drilled on the South Zone deposit (SZD) in the vicinity of the highest-grade Noranda historic holes and one of these (DDHSZD04-02) was abandoned in overburden. The NEXT Zone was tested with one hole (DDHNEXT04-01).

The program was hindered by on-going mechanical breakdowns experienced by the drill contractor. As a result, only about 60% of the South Zone Target Area program was carried out and it required about the twice the time originally allocated for the complete program. Moreover, the MEXT Zone was not tested, since the drill and camp had been contracted to another project commencing in

August.

The results of the program are shown in Table D1 and on Vertical Longitudinal Section 1 (VLS 1). All the holes intersected favourable alteration and mineralization over core lengths ranging between 20 to 36 m. Such stratigraphies i.e., the South Zone Deposit Stratigraphy ("SZDS") and NEXT Zone Stratigraphy ("NZS") are the visual components of the drill core with the strongest alteration and apparent auriferous mineralization. The stratigraphies are generally signatred by elevated Au and Cu values along with some elevated amounts of Bi, Fe, Mn, Mo, Pb, S, Sb and some Na and K depletion.

DDHNEXT04-01 constitutes a 500 m step out from the most northerly Noranda historic hole (VLS 1). The hole was successful in intersecting the NZS over a 36 m core length that includes five multiphase quartz breccia veins, usually mineralized with hematite, pyrite and blebby chalcopyrite and hosted by silicified and sulfidized, crackled crystal tuff. The veins returned up to 1.68 Au/t and 0.49% Cu over a 7.02 m core length, including 4.18 g Au/t and 0.92% Cu over a 1.5 m core length (Table D1). The mineralization was intersected precisely as planned, at about 56 m below the collar location. The intersection is considered a further indication of the along strike and down dip continuity of the South Zone Structure (SZS) over a one km strike length that remains open at depth and to the north and south.

DDHSZD04-04 is the deepest hole ever drilled on the SZD and intersected a 22 m core length of the SZDS. The SZD mineralization was intersected at a vertical depth of about 182 m and returned 3.09 g Au/t and 0.29% Cu over a core length of 10 m, including 10.51 g Au/t and 0.88% Cu over a core length of 2.22 m. The intersection is important evidence of the continuity of the mineralization at depth, were it remains strong and completely open (VLS 1, 1.1).

Holes DDHSZD04-01, -02A and -03 were drilled in proximity to the historic Noranda higher-grade intersections as an attempt to confirm the apparent wide, higher-grade target. All holes hit the SZDS where planned, over core lengths ranging between 20 and 25 m. However, the grades and widths in DDHSZD04-01 and DDHSZD04-03 were less than expected (Table D1). DDHSZD04-02A provided the best indication of a wide zone, returning 1.08 g Au/t and 0.18% Cu over a 18.34 m core length, including 5.39 g Au/t and 0.88% Cu over a 2.3 m core length.

The relevance of the 2004 drill program and the importance of the SZS mineralization is further discussed and interpreted herein via reference to VLS 1 and VLS 2 and other components of the historic database. As referenced above, the deposit is hosted by the SZS and is reported to contain drill indicated reserves of 207,000 tonnes grading 5.48 g Au/t, along with significant copper credits.

As illustrated on VLS 1, the 32 historic and the five 2004 drill holes have all intersected various strengths of the SZD mineralization. As shown in Table D2, the overall average grade of all these holes is 3.57 g Au/t and 0.34% Cu over an average core length of 4.61 m or over an estimated true width of 3.23 m. Using a cutoff of 3 g Au/t and an 8.2 gram meter product, the resulting average grade from the remaining 16 holes is 4.8 g Au/t and 0.43% Cu over an average core length of 6.4 m or an estimated true width of 4.5 m (Table D3). Approximately 43% of the holes meet the cut-off

			TABLE D1				Nov 30/04		
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			ANALYTICAL RESULTS, 2004 DIAMOND DRILL PROGRAM						
			TODD CREEK PROPERTY						
			<u>NEXT ZONE</u>						
								Estimated	
HOLE NUMBER	SECTION (N), STATION (E) ELEVATION (m)	Hole Length (m)	Au (g/t)	Cu (%)	Core Interval (m)	Core Length: (m)	True Width (m)		
DDHNEXT04-01	10700N, 10190E 1033 m	154.53	7.28	0.76	94.70-94.91	0.21	0.1		
			2.6	0.26	107.00-108.00	1.00	0.46		
			1.68	0.49	114.98-122.00	7.02	3.25		
			incl. 2.48	0.6	118.70-122.00	3.30			
			incl. 4.18	0.92	118.70-120.20	1.50			
			<u>SOUTH ZONE DEPOSIT</u>						
DDHSZD04-01	10115N, 9934E 1135 m	125.00	3.51	0.09	102.27-102.77	0.50	0.45		
			2.02	0.23	105.97-107.42	1.45	1.38		
DDHSZD04-02	10075N, 9950E 1132 m	6.09	Abandoned in overburden						
DDHSZD04-02A	10075N, 9930E 1132 m	121.64	1.08	0.18	101.66-120.00	18.34	13.75		
			incl. 1.35	0.2	101.66-115.42	13.76			
			incl. 2.65	0.44	101.66-107.28	5.62			
			incl. 5.39	0.88	104.98-107.28	2.30			
			incl. 7.02	1.16	104.98-106.58	1.60			
DDHSZD04-03	10100N, 9900E 1131 m	154.27	8.55	0.67	142.43-143.75	1.32	1.25		
DDHSZD04-04	10050N, 9925E 1132 m	199.39	3.09	0.29	180.90-190.90	10.00	5.25		
			incl. 4.04	0.35	180.90-187.13	6.23			
			incl. 10.51	0.88	180.90-183.12	2.22			
	TOTAL METERS DRILLED	760.92							

TABLE D2						
						20-Dec-04
SOUTH ZONE DEPOSIT & NEXT ZONE: TODD CREEK PROPERTY						
AU & CU ANALYTICAL RESULTS FROM HISTORIC &						
2004 DIAMOND DRILL HOLES						
SECTION (N)	HOLE NO.	Au g/t	%Cu	CORE LENGTH (m)	GMP	
					Au	Cu
9832	87-1	0.420	0.12	2.13	0.895	0.26
9868	87-2	4.10	0.25	2.00	8.20	0.50
9868	87-3	5.86	0.40	0.72	4.22	0.29
9868	88-16	1.91	0.17	2.05	3.91	0.35
9927	87-4	1.41	0.06	0.53	0.75	0.03
9927	87-5	11.93	1.50	1.73	20.64	2.60
9927	88-15	1.53	0.11	2.60	3.98	0.29
9959	87-6	3.53	0.34	0.50	1.77	0.17
9959	87-7	4.00	0.23	1.50	6.00	0.35
9959	88-14	7.65	0.97	0.15	1.15	0.15
9996	87-8	6.85	0.23	6.15	42.10	1.41
9996	87-9	2.24	0.27	9.93	22.21	2.68
9996	88-13	4.17	0.62	4.25	17.72	2.64
10021	88-10A	4.25	0.38	5.64	23.97	2.14
10021	88-11	4.35	0.56	0.40	1.74	0.22
10021	88-12	2.59	0.46	3.95	10.24	1.82
10044	88-39	5.62	0.67	1.35	7.59	0.90
10050	04-04	3.09	0.29	10.00	30.90	2.90
10075	88-17	1.95	0.19	6.20	12.06	1.18
10075	88-18	2.26	0.13	4.25	9.61	0.55
10075	88-19	3.61	0.27	29.75	107.40	8.03
10075	04-02A	1.08	0.18	18.34	19.81	3.30
10075	88-38	2.02	0.20	1.40	2.83	0.28
10100	88-33	4.59	0.88	0.90	4.13	0.79
10100	88-34	3.66	0.66	3.35	12.26	2.21
10100	88-35	8.61	0.45	11.70	100.74	5.27
10100	88-37	6.12	0.35	6.10	37.33	2.14
10100	04-03	8.55	0.67	1.32	11.29	0.88
10116	88-26	4.65	0.74	6.15	28.60	4.55
10116	88-27	3.09	0.50	8.25	25.50	4.13
10116	04-01	2.02	0.23	1.45	2.93	0.33
10116	88-28	5.97	1.30	0.25	1.49	0.33
10154	88-29	1.98	0.16	3.00	5.93	0.48
10154	88-30	5.04	0.54	0.85	4.28	0.46
10200	88-31	2.19	0.34	1.75	3.83	0.60
10200	88-32	0.03	0.06	3.00	0.10	0.18
10700	N04-01	1.68	0.49	7.02	11.79	3.44
Total	37	144.59	15.97	170.61	609.90	58.80
	Ave Au g/t	3.57				
	Ave %Cu		0.34			
	Ave Core Length m			4.61		
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criteria. Although the parameters of its calculation are not known, the grade referenced by Noranda (207,000 tonnes grading 5.48 g Au/t) could be obtained by increasing the cutoff parameters.

As shown on VLS 1, there is some indication that plunging shoot morphologies control the distribution of the higher-grade mineralization. For example, most of the higher-grade mineralization is located in proximity to a number of postulated orthogonal plunge axes (i.e., at elevation 1125 m, south plunging axes at about 10050N and 10150N and the north plunging axis at 10000N). As contemplated on VSL 1, such axes often have a regular periodicity of distribution (e.g., as at the Golden Patricia Mine in Northwestern Ontario) and can provide strong rationale for the orchestration of an ore discovery drill program.

The physical characteristics of the sulfide mineralization in the SZD are another important consideration in the interpretation of the drill results. The disseminated, generally coarse, blebby chalcopyrite associated with the M Type mineralization can constitute a “nugget effect”, such that a drill hole could pass through a well-mineralized zone and return low-grade gold and copper values over narrow widths. This “one in three effect” was experienced at the Golden Patricia Mine, where the distribution of coarse grains of visible gold in a cherty exhalite required closely spaced drilling to partially outline the ore shoots. Only one in three holes in such ore shoots commonly returned ore grade values.

In view of the factors referenced above it is concluded that the SZD and its northern extensions continue to offer significant exploration potential. As indicated by VLS 1 and the historical database, the SZS target is large. To date it has been delineated over a 1 km strike length and it may extend another 3 km to the south to the Mylonite Zone. It may also extend another 4 km to the north to the Knob Zone, located at the junction of Fall Creek and Todd Creek. As shown on VLS 1, about 60% of the known strike length of the SZS has yet to be drill tested. As shown on VLS 1 and 1.1, the area that has been tested remains open at depth.

One of the most apparently prospective areas of the SZS, the GMZ, is located where the four proposed intercepts (PM05-01, -02, -03, -04) of the recommended 2005 holes are shown on VLS 1. Composite samples taken in 2004 of the rather abundant mineralized talus at the base of cliff in which the GMZ outcrops continue to confirm the importance of the target. A composite sample of Spec Type mineralization returned 6.77 g Au/t and 0.31% Cu and a composite of M Type material returned 5.76 g/Au t and 2.33% Cu. The composites were prepared from two larger samples each weighing approximately 75 kg.

It is recommended that a 2005 diamond drill program of sufficient scope and size be carried out to attempt to determine if the SZS has potential for hosting a significant orebody. Four initial holes totalling about 1200 m are thus proposed to evaluate the SZD at depth; one hole totalling about 300 m to evaluate the NEXT Zone at depth; and, 4 holes totalling about 350 m to initially test the GMZ.

The projection points of the proposed intersections of the holes on the SZD (PSZD05-01 to -04), of those proposed on the GMZ (PM05-01 to -04) and of the proposed hole on the NEXT Zone (PN05-01) are shown on VLS 1. The four proposed holes on the SZD are planned to intersect the SZS at

the 925 m elevation, approximately 200 m below the collars of the holes. The first hole would be drilled 25 m under DDHSZD04-04 to intersect the SZS along the postulated south plunge axis shown on VLS 1. The three other SZD holes are also proposed to intersect the SZS in the vicinity of the south plunging axes shown on VSL 1. For example, the projection point of the PSZD05-02 intersection shown on VLS 1 and VLS 1.1 is 70 m down plunge of that in Noranda hole DDH88-14 and that of the PSZD05-04 intersection is about 270 m down plunge of the GMZ. The rationale of the SZD drill program is to test the deposit down dip/plunge where it remains open and in the vicinity of where the higher-grade mineralization is postulated to occur.

JVX Ltd. of Toronto has proposed that borehole Spectral IP be utilized, if warranted, in 3 or 4 deep holes drilled on the SZD. Such geophysical methods could map the sulfide mineralization associated with the SZS at depth in order to maximize the on-going drill targeting process. The deeper holes would have to be drilled about 60 m beyond the mineralized zone to facilitate the geophysical survey.

The four holes proposed on the GMZ (VLS 1) would evaluate the apparent higher-grade gold-copper mineralization located in proximity to the structural junction of the MEXT Fault and the SZS. The potential of the auriferous oxide or Spec Type mineralization apparently was not recognized until 1999, when discovered by Geofine in the GMZ target area. As noted by Geofine in 2000, the GMZ is currently deemed to offer one of the highest priority drill targets on the property. An initial target grade of greater than 6 g Au/t and 1% Cu is considered reasonable, with the expectation that tonnage and grade components can be enhanced by substantial, plunging ore shoot morphologies.

The strong NZS intersected in DDHNEXT04-01 would be followed by a hole proposed to intersect the NEXT Zone at the 925 m elevation (VLS 1) i.e., about 50 m vertically below that of DDHNEXT04-01. The hole would total about 300 m.

A follow-up drill program is also recommended on the F1 Zone in the Fall Creek Target Area that would entail three holes totalling about 255 m. The prospective target is similar to the M Type mineralization in the SZD. It is located in steeper topography but has been delineated by an IP anomaly over an 800 m strike length.

IP surveying could prove very useful elsewhere on the Todd Creek Property. For example, the large Amarillo Zone covers a high-level epithermal system with a very strong polymetallic geochemical signature. Although a number of drill targets have been spotted historically, IP surveying could provide the definition required to prioritize specific targets. The Spectral IP survey technique could also be invaluable at the south end of the South Zone deposit to evaluate its southern strike extension under the glacial fluvial deposits of the Todd Creek Valley.

The proposed 2005 Phase 1 drill program is summarized in Table S2 and would entail 12 holes comprising about 2100 m of diamond drilling. The Phase 1 program does not include any of the aforementioned IP surveying, which could be part of a Phase 2 program. The on site helicopter and camp supported drill program is estimated to total about \$716,000 or about \$649,000 net of GST and refundable reclamation bond (Table S3). The estimated cost is subject to contractor bids and permitting requirements. The program would take about 40 days to complete. If the helicopter was

TABLE S2:

PROPOSED 2005 DRILL PROGRAM, TODD CREEK PROPERTY

AREA 1, SOUTH TARGET AREA:

TARGET:	HOLES:	METERS:
i. SOUTH ZONE DEPOSIT	4	1200
ii. GOLD GULLY-MEXT ZONES	4	350
iii. NEXT Zone	<u>1</u>	<u>300</u>
AREA 1, PHASE 1 TOTALS:	9	1850

AREA 2, FALL CREEK TARGET AREA:

TARGET:	HOLES:	METERS:
i. FALL CREEK EAST F1 ZONE	<u>3</u>	<u>255</u>
AREA 2, PHASE 1 TOTALS:	<u>3</u>	<u>255</u>
2005 PROPOSED DRILL PROGRAM	12	2105

TABLE S3: PROPOSED PHASE 1 BUDGET, 2005 FINAL WORK
PROGRAM: 2100 M DIAMOND DRILLING PROGRAM*:

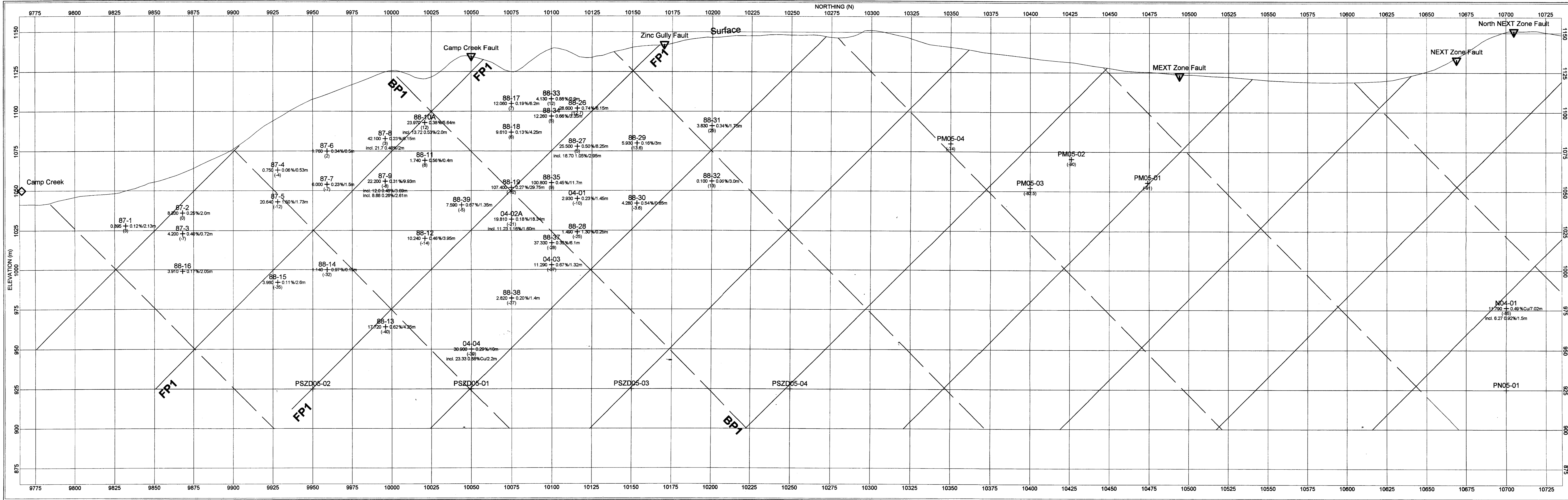
<u>ITEM</u>	<u>ESTIMATED COST</u>
	(\$)
i) Property, assessment work research	
ii) Project permitting, planning, gov't bond	28000
iii) Geochemical signature analyses	
iv) Property Compensation	
v) Structural fabric studies, airphotos, mag maps	
vi) Field equipment, supp incl standards, coresplit	5500
vii) Mob-demob	10000
viii) Ground transport, shipping, GF helicopter	25000
ix) Analyses, assays 250 @ \$40	10000
x) Linecutting	
xi) Geophys surveys: 12 days, travel mob, report	
xii) Land surveys	
xiii) Food, sustenance, accommodation	4500
xiv) Communications - in field (sat phone, fax)	2500
xv) Compilations, drafting, reporting, assess. rpts, quality assurance, data verification	12500
Government filing fees	15000
xvi) Land acquisition payments, option payments	
xvii) Legal fees	
xviii) Licences	
xix) Salaries: local labour, geological crew	60000
Workers Comp Ins.	
\$1200/day @ 50 days;	
xx) Diamond drilling: 2100m @210/m	441000
incl mob/demob, camp & maint, drill pads, cook, heli support	
xxi) Contingency:	44000
Subtotal	658000
xxii) Geofine Overhead @3%	19000
xxiii) GST	39000
ESTIMATED TODD 2005 PROPOSED BUDGET*	\$716000
NET OF RECLAM BOND AND GST:	649000
ESTIMATED TODD 2005 PROPOSED BUDGET**	\$646000
NET OF RECLAM BOND AND GST:	581000

*Subject to contractor bids and permit requirements. Assumes an on site helicopter.

**If helicopter is allowed to do other work as in 2004, cost of helicopter support may be about 40% less than budgeted.

POCKET S1

VLS 1, VLS 1.1



- LEGEND**
- + Projected intercept point
 - 88-30 Diamond drill hole number
 - 4.28 + 0.54%/1m GMP Au + %Cu/core length
 - (-5) Distance projected to section from west
 - (5) Distance projected to section from east
 - + PM05-01 Proposed intercept of 2005 diamond drill hole
 - Interpreted main South plunge axis of mineralized shoot
 - Interpreted north (back) plunge axis of mineralized shoot

N

20 20 40
metres

27

DAVID E. MOLLOY
PRACTISING MEMBER
0817
ONTARIO

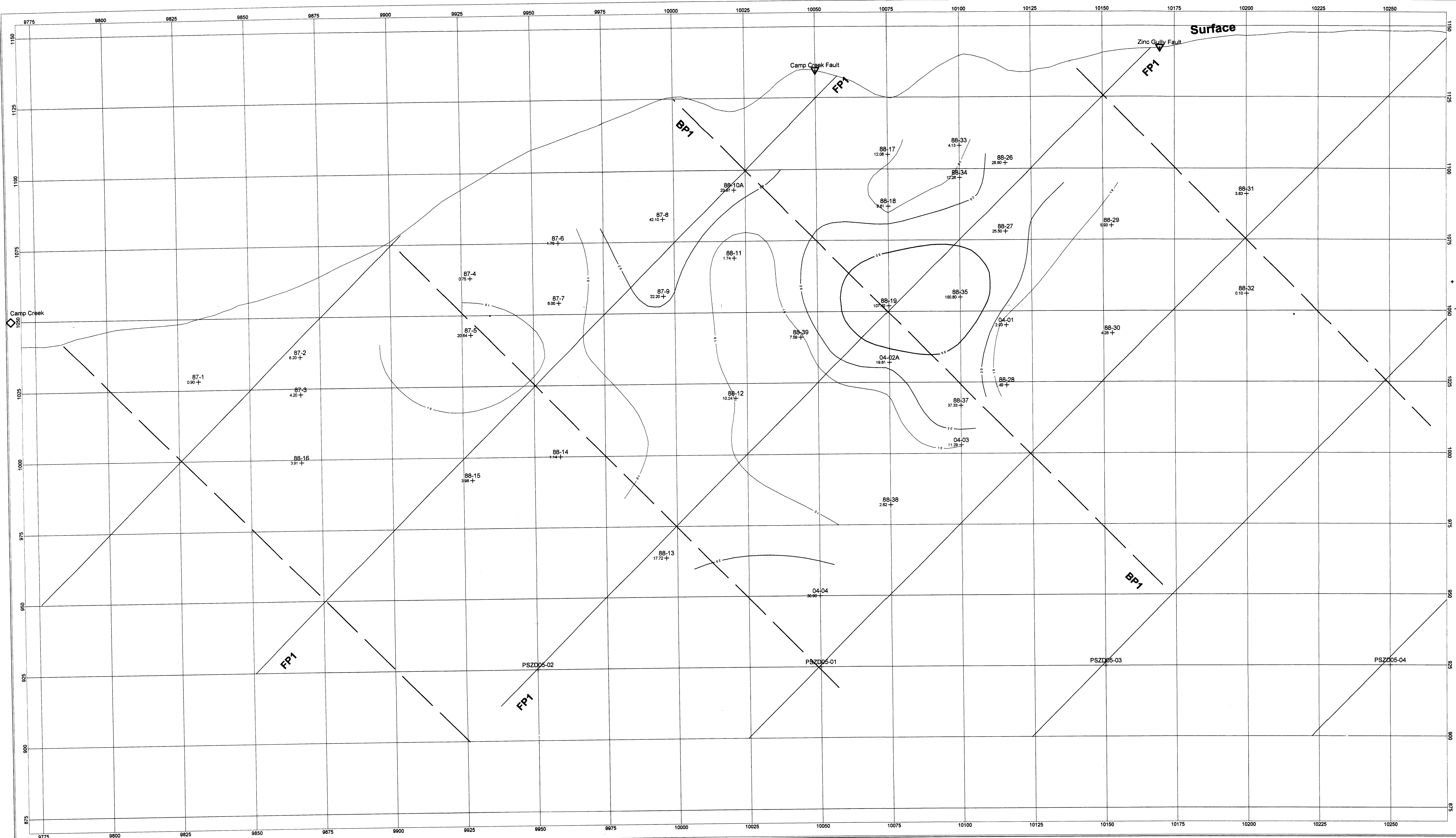
27 David E. Molloy Geo.

VERTICAL LONGITUDINAL SECTION 1

Projected to BL 10000E
Looking 280 degrees

TODD CREEK PROPERTY
SOUTH ZONE DEPOSIT

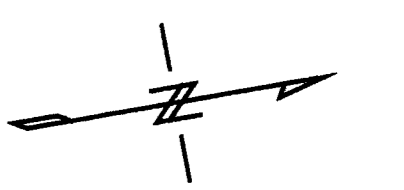
Geofine Exploration Consultants Ltd. Jan. 2005



LEGEND

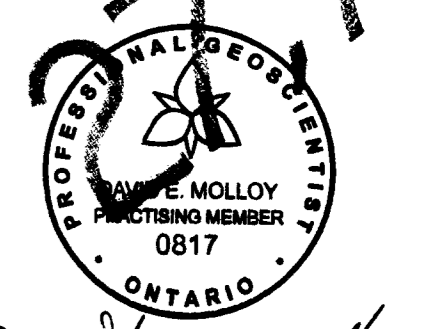
4.28 + GMP AU AND INTERCEPT POINT
 88-30 Diamond drill hole number
 + PSZD05-01 Proposed intercept of 2005 diamond drill hole
 ———— Interpreted main South plunge axis of mineralized shoot
 - - - - - Interpreted north (back) plunge axis of mineralized shoot

CONTOUR INTERVALS OF GMP
 ~~~~~ 10  
 ~~~~~ 20  
 ~~~~~ 50



Scale 1:500  
 0 10 20 30  
 metres

GEOLOGICAL SURVEY BRANCH  
 REPORT



David E. Molloy, P. Geol.

VERTICAL LONGITUDINAL SECTION 1.1  
 Projected to BL 10000E  
 Looking 280 degrees  
 TODD CREEK PROPERTY  
 SOUTH ZONE DEPOSIT  
 Geofine Exploration Consultants Ltd. Jan. 2005

allowed to undertake additional work when not required on the property, it is estimated the program cost would drop to about \$646,000 or about \$581,000 net of GST and refundable reclamation bond.

The program could also be carried out in a number of phases. For example, a Phase 1A program could contemplate testing the Gold Gully – MEXT Zone, the NEXT Zone, the Fall Creek East FI Zone and one deep hole on the South Zone deposit. This program would total about 1200 m. A Phase 1B program could continue with the three remaining holes proposed on the South Zone deposit or as specifically warranted by the results of the Phase 1A program.

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**REPORT ON THE 2004 DIAMOND DRILL PROGRAM**  
**CARRIED OUT ON THE TODD CREEK PROPERTY,**  
**STEWART GOLD CAMP, SKEENA MINING DIVISION,**  
**NORTHWESTERN BRITISH COLUMBIA**

**1. INTRODUCTION:**

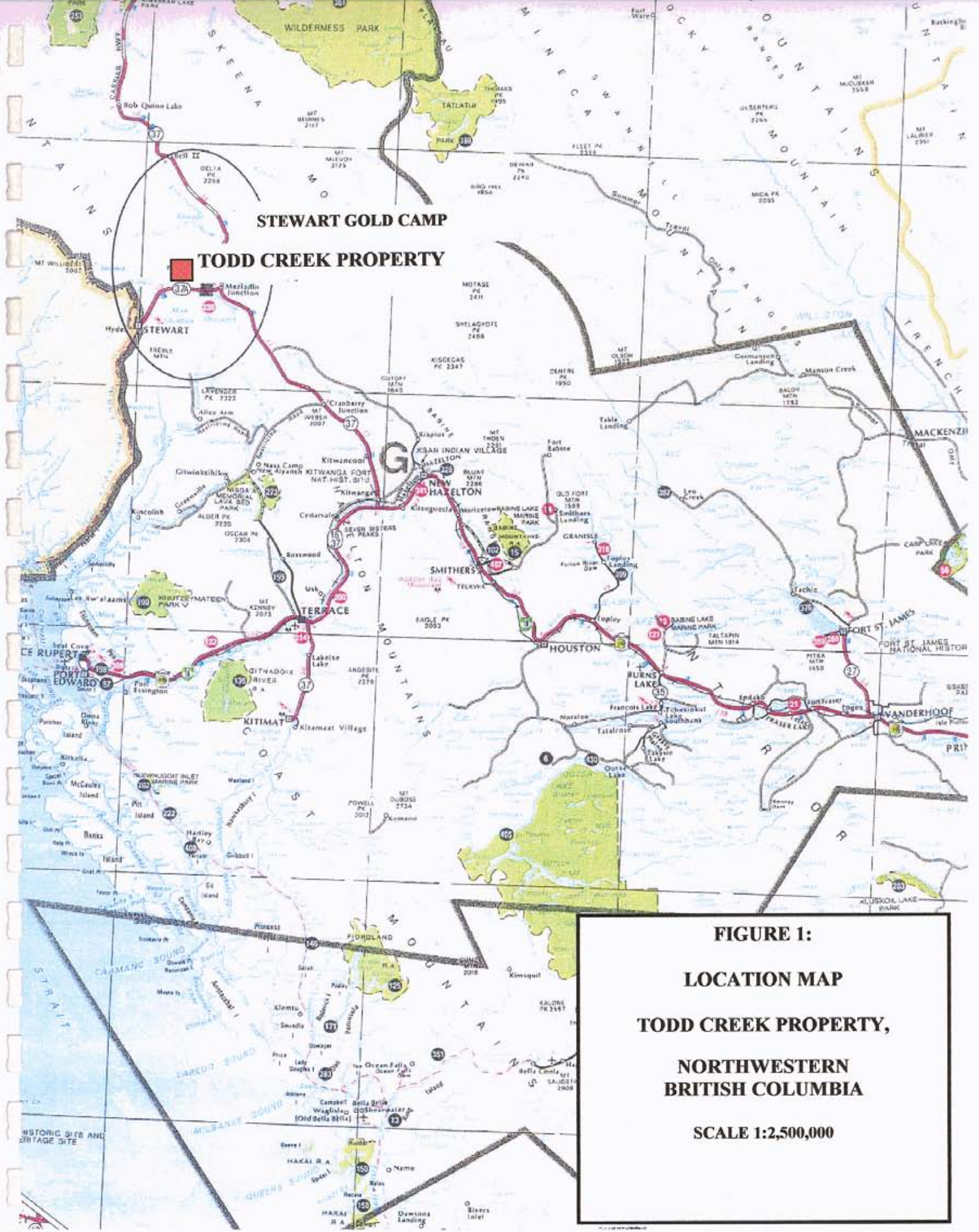
This report reviews the results of the 2004, helicopter supported drill program carried out on the Todd Creek Property (Maps 1, 2, 2A) by Geofine Exploration Consultants Ltd. ("Geofine") on behalf of Lateegra Resources Corp. ("LEG"). The property is located in the Stewart Gold Camp of Northwestern British Columbia (Figures 1, 2, 3) and straddles the Todd Creek Valley, about 35 km northeast of Stewart, British Columbia.

The work comprised 6 drill holes totalling about 761 m (Table D1) and was carried out mainly in July and August. The confirmation and step out holes were drilled on the South Zone deposit ("SZD") and a component of its northern extension, the NEXT Zone (Maps 3, 4, 4A, 4B), to follow-up the historic drill results obtained by Noranda and the 1999 and 2000 exploration results obtained by Geofine.

The Todd Creek Property is dominated by Jurassic Age pyroclastic rocks of the Unuk River Formation, which hosts most of the significant mineralization in the Stewart Camp (Figure 2). The exploration target is structurally controlled epithermal - mesothermal mineralization: M Type i.e., hematite-quartz multiphase breccia veins that contain blebby, auriferous chalcopyrite (Frontspiece Photo 1); and, Spec Type i.e., massive to disseminated auriferous specular hematite and hematite-chalcopyrite veins associated with the South Zone Structure ("SZS"). The orthogonal structural fabric is considered conducive to the development of ore shoot morphologies along the SZS, e.g., at the Gold Gully-NEXT Zone ("GMZ") and in the vicinity of the Camp Creek Fault at the SZS (Maps 1, 2A, 4).

A large, strong gold-copper hydrothermal system(s) exists on the Todd Creek Property and the mineralization, as demonstrated by the SZD and its northern extensions, exhibits very good along strike and down dip continuity. Similar M Type mineralization exists 4 km to the north in the Fall Creek and North A Zones, on the flank of the high-level epithermal system in the Orange Mountain Target Area "OMTA". It is postulated that this epithermal system, as evidenced at the Amarillo Zone, is underlain by a porphyry hydrothermal system and that the intrusion, the resulting deformation, formation of the structurally hosted, gold-copper multiphase breccia veins and mineralogical and alteration zoning are closely related spatially, temporally and genetically. Moreover, it is contemplated that more than one such porphyry system is associated with the aforementioned mineralization i.e., one in the OMTA and one at depth near the GMZ. The SZS target is large, possibly extending over 7 km from the Mylonite Zone to the south to the SZD and to the Knob Zone located at the junction of the Fall Creek Fault and SZS. The exploration target is a gold-copper orebody most likely to be discovered along the SZS or in the OMTA, in proximity to the aforementioned porphyry hydrothermal system(s).





**STEWART GOLD CAMP**

**TODD CREEK PROPERTY**

**FIGURE 1:  
LOCATION MAP  
TODD CREEK PROPERTY,  
NORTHWESTERN  
BRITISH COLUMBIA**

**SCALE 1:2,500,000**



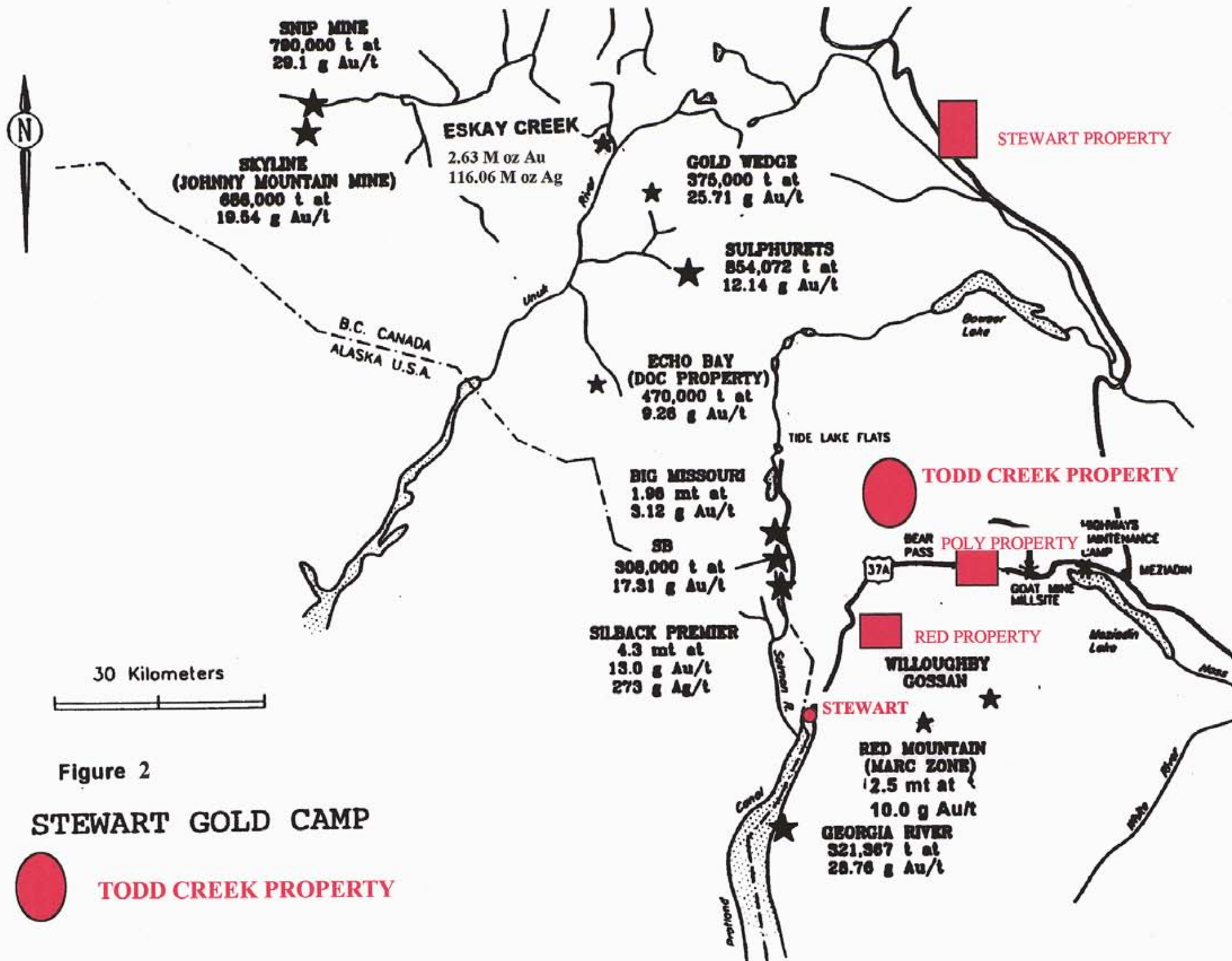
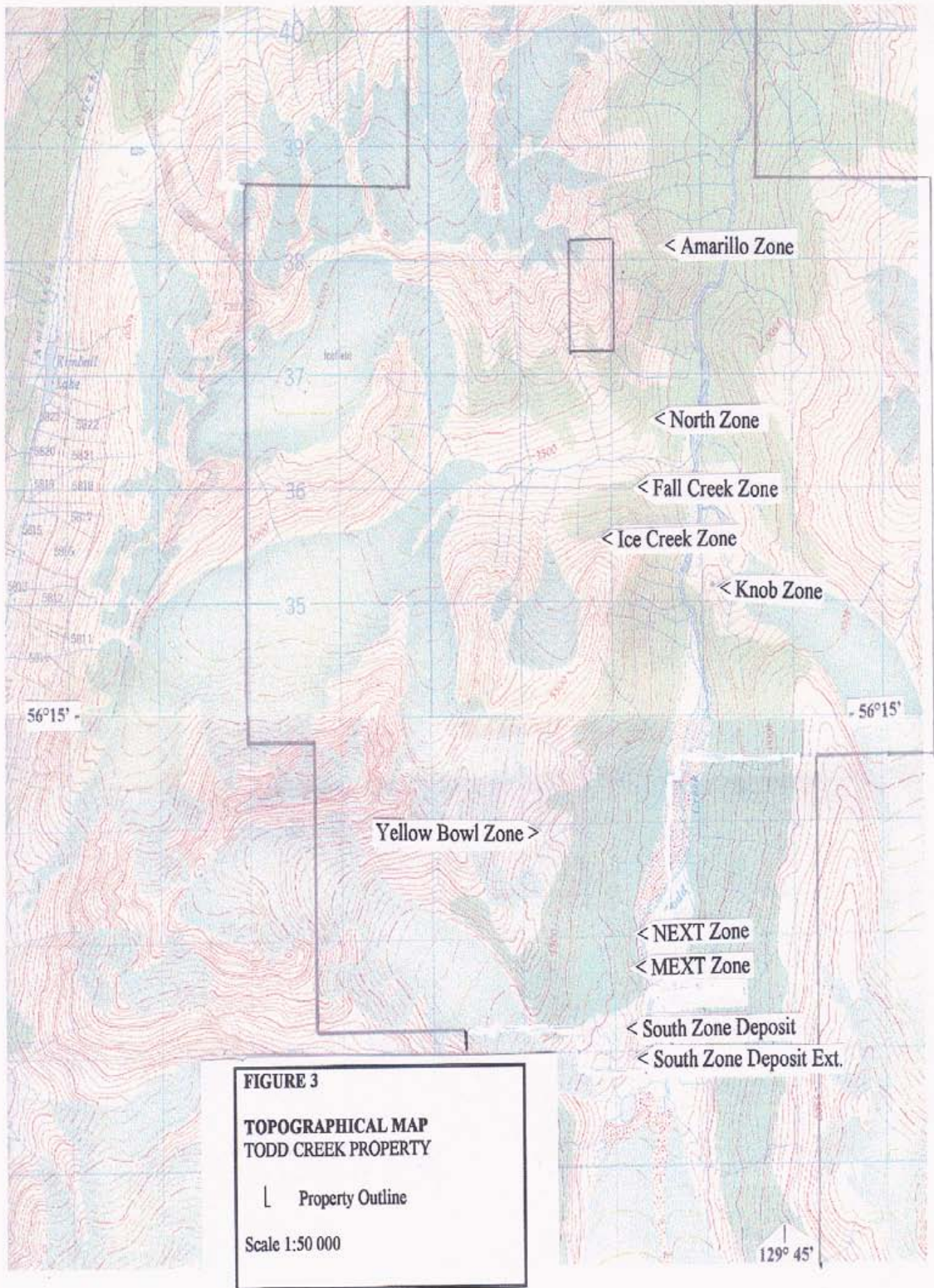


Figure 2

STEWART GOLD CAMP

 TODD CREEK PROPERTY





**FIGURE 3**  
**TOPOGRAPHICAL MAP**  
**TODD CREEK PROPERTY**

| Property Outline

Scale 1:50 000

## **2. PROPERTY, OWNERSHIP, OPTION AGREEMENTS:**

The Todd Creek Property consists of 24 claims i.e., Todd 1-8, Todd 11-13 and Todd 18 Claims; the Pat 4-5 Claims; the Pat 20-24 claims; and, the Benji 8-12 Claims (Table 1; Map 1) that comprise 414 claim units and cover about 104 square km. The claims are located on British Columbia Mineral Titles Maps 104A04E, 104A04W, 104A05E and 104A05W (Map 1).

The claims are registered in the name of Geofine Exploration Consultants Ltd, as agent of Geofund. Geofund is the owner of the property and is a private investment group that funds the research, acquisition, exploration and marketing of mineral targets. Lateegra Resources Corp. ("LEG") holds the property under option from Geofine and can earn a 100% interest by fulfilling escalating option payments and work conditions. The LEG interest is subject to a Geofund 2.5% NSR.

## **3. LOCATION AND ACCESS:**

The Todd Creek Property is situated in the Skeena Mining Division, about 35 km northeast of the town of Stewart, Northwestern British Columbia (Figures 1, 2). The property is located on NTS Map Sheets 104/A4 and 104/A5 and centred at about Latitude 56° 15', Longitude 129° 46' (Figure 3). The claims straddle the Todd Creek Valley, approximately 10 km north of the Stewart Highway 37A (Figures 2- 4).

In view of the mountainous terrain, helicopter access is currently required, either from the Prism Helicopter base in Stewart or from staging areas near American Creek; or, from the Bowser Lake access road off the Stewart-Cassiar Highway (Figure 2). The most logical land route to facilitate the development of an ore body is probably north along Todd Creek to the Bowser River, east to Bowser Lake and east by barge across the lake where lumber roads lead to the Stewart-Cassiar Highway 37. A 9 km tunnel driven north to the property from the Rufus Creek area on Highway 37A would provide the most direct and all season route to the port of Stewart, and to the historic Westmin mill. The discovery of a major ore body, which is the on-going exploration objective, could justify the expense of such a tunnel.

## **4. TOPOGRAPHY, DRAINAGE, CLIMATE, WILDLIFE & VEGETATION:**

The Todd Creek Property is located within the Boundary Ranges of the northern British Columbia Coastal Mountains (Figure 4). The regional topography is characterized by the Todd Creek Valley, which has an elevation of between about 600 to 900 m on the property (Map 2). East and west of Todd Creek, the valley rises steeply to elevations over 2000 m. Young, deep valleys hosting tributaries, which drain into Todd Creek and which facilitate geological and geochemical surveys characterize the mountainous topography (Figure 3). The heads of the valleys are often occupied by glaciers, which are currently receding at a rate of tens of metres per year. Approximately 20% of the property is covered by glaciers and ice fields (Figure 3).

**TABLE 1: MINERAL CLAIMS, TODD PROPERTY,  
SKEENA MINING DIVISION:**

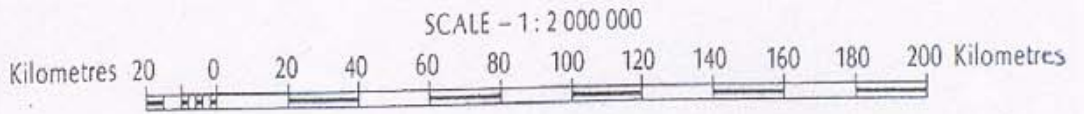
**NTS: 104A04E/W & 104A05E/W**

| <b>NAME</b>    | <b>TAG</b>       | <b>TENURE</b> | <b>UNITS</b>     | <b>STAKED</b> | <b>EXPIRY*</b> |
|----------------|------------------|---------------|------------------|---------------|----------------|
| Todd 1         | 230148           | 325164        | 20               | Apr 17/94     | May 12/2005    |
| Todd 2         | 230149           | 325165        | 20               | Apr 17/94     | May 12/2005    |
| Todd 3         | 230150           | 325166        | 20               | Apr 17/94     | May 12/2005    |
| Todd 4         | 230151           | 325167        | 20               | Apr 17/94     | May 12/2005    |
| Todd 5         | 230152           | 325168        | 20               | Apr 17/94     | May 12/2005    |
| Todd 6         | 230153           | 325169        | 20               | Apr 17/94     | May 12/2005    |
| Todd 7         | 230154           | 325170        | 20               | Apr 17/94     | May 12/2005    |
| Todd 8         | 230155           | 325171        | 20               | Apr 17/94     | May 12/2005    |
| Todd 11        | 230158           | 325174        | 20               | Apr 17/94     | May 12/2005    |
| Todd 12        | 230159           | 325175        | 10               | Apr 17/94     | May 12/2005    |
| Todd 13        | 231613           | 354785        | 18               | Apr 10/97     | May 12/2005    |
| Todd 18        | 220191           | 370599        | 2                | Aug 13/99     | May 12/2006    |
| Pat 4          | 219260           | 329969        | 20               | Aug 17/94     | May 12/2005    |
| Pat 5          | 229769           | 329970        | 20               | Aug 17/94     | May 12/2005    |
| Pat 20         | 231609           | 354781        | 20               | Apr 10/97     | May 12/2005    |
| Pat 21         | 231610           | 354782        | 20               | Apr 10/97     | May 12/2005    |
| Pat 22         | 218219           | 355287        | 15               | Apr 20/97     | May 12/2005    |
| Pat 23         | 231612           | 354784        | 20               | Apr 10/97     | May 12/2005    |
| Pat 24         | 218220           | 355288        | 5                | Apr 20/97     | May 12/2005    |
| Benji 8        | 239519           | 378752        | 20               | July 17/00    | July 15/06     |
| Benji 9        | 239520           | 378753        | 20               | July 17/00    | July 15/06     |
| Benji 10       | 239521           | 378754        | 20               | July 17/00    | July 15/06     |
| Benji 11       | 239530           | 379525        | 12               | August 2/00   | July 15/06     |
| Benji 12       | 239529           | 379526        | 12               | August 2/00   | July 15/05     |
| <b>Totals:</b> | <b>24 Claims</b> |               | <b>414 Units</b> |               |                |

**\*The filing of 2004 work credits to extend all the claims for three additional years is pending.**

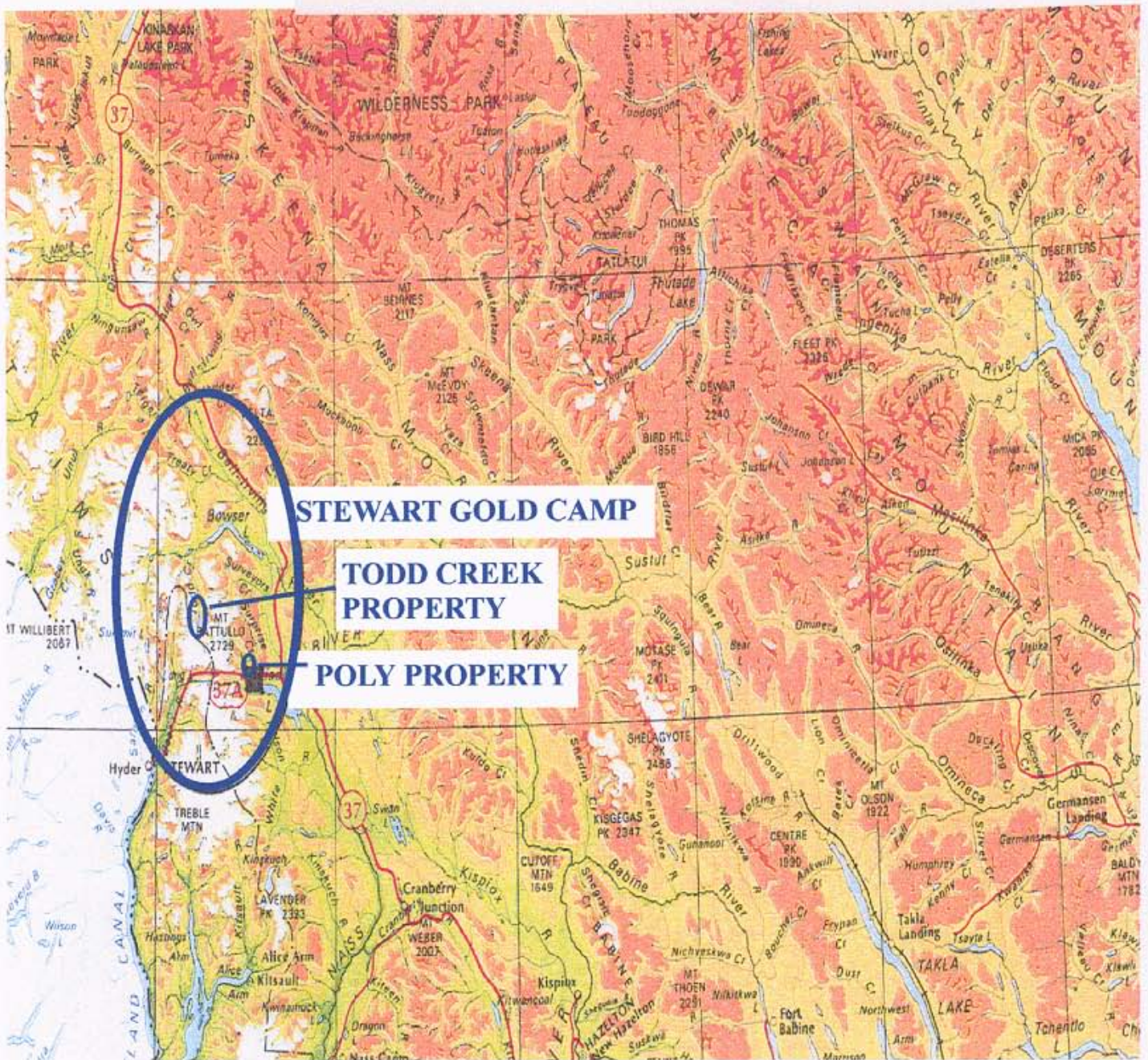
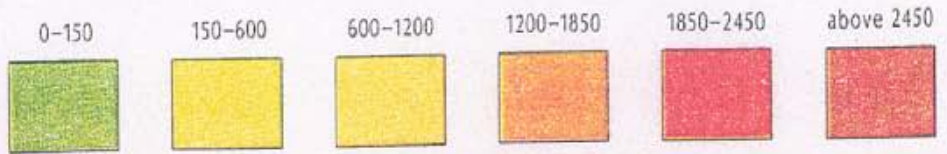
**C:\TODD CLAIMS**





**FIGURE 4:  
RELIEF MAP**

ELEVATION IN METRES ABOVE SEA LEVEL



The exploration field season generally extends from late June to October. In 2004, the Stewart area experienced one of the warmest summers in history, with daily temperatures often exceeding 30°C. Summers are usually characterized by long hours of daylight and pleasant temperatures. Although winters have been getting milder and glaciers have been rapidly receding, snow can cover higher elevations in early September and accumulations can total several metres in a 24-hour period. Recorded mean annual snowfalls in the area range from 520 cm at Stewart (sea level) to 1,500 cm at Tide Lake Flats (915 m elevation). The proximity to the ocean and relatively high mountains can make for highly changeable weather, including dense morning fog along the coast. Stewart is located on the Portland Canal (Figures 1, 2) and has the distinction of being Canada's most northerly, ice-free seaport.

Wildlife in the area consists of mountain goats, foxes, grizzly bears, black bears, wolves, marmots, martins and ptarmigan. Vegetation in the Todd Valley ranges from dense tag alders to small areas of spruce forest, to sub-alpine spruce thickets, with heather and alpine meadows. Above tree line at approximately 1,200 m, bare rock, talus slopes and glaciers with occasional islands of alpine meadow prevail.

## **5. EXPLORATION HISTORY:**

The central area of the Stewart Camp was prospected at the close of the 19th century, mainly for visible gold in quartz veins. The showings were generally located on Crown granted claims, but very little of this work was documented.

The most prominent early discovery was the historic Silbak-Premier gold-silver mine, which produced 56,000 kg of gold and 1,281,400 kg of silver in its original lifetime from 1918 to 1976. The mine was re-opened by Westmin in 1988 with reserves quoted at 5.9 million tonnes grading 2.16 g gold/t and 80.23 g silver/t (Randall, 1988). The mine closed in 1998 and the 2500 t/d mill facility was put up for sale.

The Camp (Figure 2), after more recent discoveries that include the recently closed Snip Mine (total deposit size of 1,055,105 ounces of gold contained in 1.3 M tonnes); the Eskay Creek Mine (total deposit size of about 7.1 M ounces gold equivalent); and, Red Mountain (with reserves of about 1 M ounces of gold), continues to be regarded as a very prospective environment where discoveries of rich, gold/silver/base metal deposits can be made.

Historical exploration activities on the Todd Creek Property evolved around the 12 mineral showings that are located on and in the vicinity of the property and that are referenced in the BC government's mineral records ("Minfile"). The showings are briefly described below and are located on Map 1 according to Minfile Number.



**a. Minfile 001: South Zone Deposit on Todd 13:**

The South Zone deposit is located on the Todd 13 Mineral Claim, north of the new Benji 9 and 10 Claims (Map 1). The South Zone was discovered by Newmont Mining Corporation in 1959, and was held by Noranda Exploration Company, Limited and Goldnev Resources Inc. as the Toc 10 Claim, until the spring of 1997. Geofine staked the South Zone deposit as part of the Todd Creek Property.

According to Government Assessment Report 18800, the South Zone is the most significant target area located on the Toc 10 and 11 claims. Drilling in 1987 tested the southern 175 m strike length of the zone and significant results include:

11.93 g gold/t over 1.73 m  
4.10 g gold/t over 2.00 m  
4.01 g gold/t over 1.50 m  
3.25 g gold/t over 3.69 m  
3.36 g gold/t over 2.61 m

Drilling in 1988 tested the down dip extension and strike continuity of the zone for an additional 200 m to the north. Intersections ranged from 1-30 m and significant values include:

6.91 g gold/t over 8.15 m  
6.86 g gold/t over 2.00 m  
6.53 g gold/t over 2.05 m  
4.65 g gold/t over 6.15 m  
8.83 g gold/t over 11.70 m  
6.12 g gold/t over 6.10 m

The zone has been tested by 34 holes comprising 3186 m. The zone was reported by Noranda to be hosted by altered feldspar porphyry exposed over an area of 950 by 500 m. Quartz-pyrite is the principal alteration, but near the mineralization, quartz-sericite is the dominant type. The mineralization consists of chalcopyrite, pyrite, specular hematite and malachite. The mineralization is hosted by a 5 to 15 m wide, northeast trending, fracture zone that dips west. The area is underlain by Upper Triassic to Lower Jurassic rocks of the Unuk River Formation, which is part of the Hazelton Group (Figure 5).

The South Zone is reported to contain drill indicated reserves of 207,000 tonnes grading 5.48 g Au/t (Hemlo Gold Mines Inc., 1988 Annual Report).

**b. Minfile 111: Mid Zone on Todd 12:**

The Mid Zone was discovered by Noranda in 1986. It comprises an area about 500 by 250 m encompassing several west-southwest to northwest trending quartz-pyrite-chalcopyrite veins. The veins are 0.01 to 6.0 metres wide and 1 to 108 metres long. Grab samples assayed up to 1.68% copper with negligible molybdenum, lead, zinc, silver, arsenic, cadmium, antimony, and gold values.



The mineralization is apparently hosted by altered felsic rocks composed of quartz-sericite-pyrite.

**c. Minfile 110: Ridge Showing on Todd 12:**

Noranda discovered the Ridge Showing in 1987. The showing consists of several mineralized outcrops that cover an area about 300 by 200 m. Mineralization comprises pyrite, chalcopyrite and malachite. North-northwest trending andesite flows and agglomerates are reported to be interbedded with feldspar porphyry (intrusive?) and rhyolite flows and tuffs. Grab samples assayed up to 0.34 g gold/t, 5.2 g silver/t, and 14.14% copper. The mineralization appears to be hosted by mafic volcanics that lie immediately west of a large gossan apparently associated with feldspar porphyry. Approximately 200 m north of the showing, a sample from outcrop assayed 12.7g silver/t, 1.17% lead and 1.71% zinc.

**d. Minfile 109: Knob 1 Showing on Todd 3:**

The Knob 1 showing was discovered by Noranda in 1987. The showing comprises several 1-10 cm wide pyrite +/- chalcopyrite veins that occur in a large, prominent gossan. The gossan includes extensive areas of quartz-sericite-pyrite alteration. A grab sample from one of the veins assayed 0.37% copper. The mineralization occurs in pervasively altered, northwest trending andesite flows and breccias, which are intruded by fine grained mafic dykes.

**e. Minfile 108: Toc 9 Showing on Todd 4:**

Noranda discovered the Toc 9 Showing in 1986. Mineralization consists of narrow chalcopyrite veins that occur in 1-2 m wide discontinuous, north-northwest trending shear zones. The zones are reported to be hosted by altered feldspar porphyry composed of quartz, sericite and pyrite. Grab samples assayed up to 32.9 g gold/t and 3.08% copper.

**f. Minfile 107: F1 Zone or Fall Creek East Zone on Todd 3:**

The F1 Zone was discovered by Noranda in 1987 as a follow-up of anomalous values returned in a soil survey on the south side of Fall Creek. During 1986 to 1989 Noranda completed geological mapping, silt and soil geochemical surveys and four holes totalling 368 m on the zone. Significant intersections include:

- 6.72 g gold/t over 1.45 m
- 12.10 g gold/t over 1.25 m
- 2.73 g gold/t and 0.59% copper over 13.00 m
- incl. 5.41 g gold/t and 0.50% copper over 5.25 m
- 4.34 g gold/t over 2.00 m
- 3.94 g gold/t over 7.90 m
- incl. 4.71 g gold/t over 4.75 m

The mineralization is associated with pervasively altered andesites that contain quartz-sericite-pyrite

zones and that are cut by mineralized structures with a variety of orientations. The main zone of interest is associated with quartz-pyrite-chalcopyrite-barite veins that have been traced for 400 m along strike and 300 m vertically. The drilling tested the zone over a strike length of 100 m and to a depth of 50 m.

IP and gold soil geochemistry delineated an anomalous area 900 by 450 m, which encompasses the F1 zone and several other mineralized outcrop and float occurrences. In 1990, Golden Nevada Resources Inc. drill tested a number of the IP targets with 10 holes that did return some significant results including 1.35 g gold/t over 15.35 m (Baerg, 1991). The encouraging results were never followed up.

**g. Minfile 106: North A Zone on Todd 2:**

The North A Zone on the Todd 2 claim was a Newmont discovery and yielded significant results. The zone is described as northwest trending and vertically to steeply west dipping, comprising 0.1-2 m wide quartz, chalcopyrite, pyrite, hematite and breccia veins. The veins are commonly banded and brecciated and have been traced for 320 m. Trenching results ranged up to 3.8 g gold/t across 14.3 m.

The zone was tested with 9 holes and a Mise-a-la-masse survey. The drilling and geophysics suggest that the zone is discontinuous and poddy along strike and down dip. Widths on the zone range from 1-32 m. The zone was tested over a strike length of 150 m. Significant drill values include the following:

incl. 3.47 g gold/t, 0.75% copper over 31.85 m  
14.47 g gold/t, 2.06% copper over 5.95 m  
2.83 g gold/t, 0.58% copper over 1.95 m  
3.95 g gold/t, 0.22% copper over 2.00 m  
3.43 g gold/t, 0.73% copper over 1.70 m  
6.21 g gold/t, 0.60% copper over 1.75 m

Another zone located 200 to 550 m east of the above zone contains identical mineralization except for the absence of stringer mineralization. Chip sampling on this zone produced assay values up to 9.53 g gold/t and 0.35% copper across 1 m.

**h. Minfile 105: North East Zone on Todd 2:**

Noranda discovered the showing in the course the follow-up of a geochemical survey. The host rocks are propylitically altered green volcanics, green to buff agglomerates/flow breccias and tuff. Alteration consists of chlorite, carbonate, sericite and pyrite (2-5%). A feldspar porphyry dyke is exposed near the showing. Mineralization consists of a west-northwest trending barite-quartz-galena vein, which cuts the feldspar porphyry body. Samples assayed up to 39.30 g silver/t, 12% lead, and 6.2% zinc, with negligible copper and gold values.

**i. Minfile 104: Orange Mt. Showing on Woodcock's Todd Claim (2 units) within Todd 1 and Todd 2:**

The showing is hosted by altered volcanics within an alteration zone some 1500 m by 1200 m. A barite jasper zone lies within the alteration zone and is the locus of the showing. Mineralization comprises pyrite, barite, and galena. Abundant jarosite is noted in the intensely altered area. Chip samples ranging up to 232.5 g silver/t and 12.8% lead across 0.7 m were reported. Approximately 190 m east northeast of the showing, grab samples assayed up to 199.5 g silver/t and 27.7% lead. Approximately 250 m northeast of the showing grab samples assayed up to greater than 100 g silver/t, 0.22% copper, and 0.28% lead.

**j. Minfile 103: Bow 31 Showing on Todd 2:**

Brucejack Gold Ltd. outlined an area of anomalous gold and silver values in 1987-1988. Marlin Developments analyzed the previously collected samples for base metals. The showing consists of massive to weakly foliated, fine-grained tuff that contains 7 to 10% finely disseminated pyrite. A grab sample assayed 175.9 g silver/t, 0.41% lead, and 0.52% zinc.

**k. Minfile 102: Bow 32 Showing on Todd 2:**

Brucejack Gold in conjunction with Marlin Developments found the zone in the follow-up of a geochemical survey. Mineralized outcrops occur on both sides of Todd Creek over a distance of about 200 m. Silver values from the outcrops typically range from 34 to 343 g/t. The highest-grade mineralization occurs on the east bank of the creek and is hosted in a hematite-chlorite altered felsic tuff. It consists of a 20 to 30 cm wide stock work of quartz, barite and carbonate containing 15% pyrite as disseminations and stringers. A sample of this mineralization assayed 2262.9 g silver/t. Immediately west of the showing on the west bank of the creek, a grab sample assayed 0.14 g gold/t, 233.1 g silver/t and 0.54% lead.

In 1994, Geofund staked the Todd Creek Property and, under an option agreement with Oracle Minerals Inc., carried out a \$200,000, Phase 1 exploration program (Molloy, 1994). The work included compilations of historical data; an Aerodat helicopterborne conventional EM and gradiometer survey (Map 2; Woolham, 1994); and, reconnaissance geological and geochemical surveys on a number of the most prospective targets, including the Fall Creek, North and Amarillo Zones. Based on the work, a \$600,000, 1997 follow-up program was recommended that included an 1800 m drill program (Molloy, 1994). The historical Noranda gold and copper intersections on the East and West Fall Creek Zones and on the North A Zone were the main focus of the proposed drill program.

In 1997, Geofund optioned the property to Island-Arc Resources Ltd. Geofund carried out a \$215,000 detailed follow-up program on the Amarillo, North, Yellow Bowl and South Zones; and reconnaissance surveys on the East Target Area and the Mylonite Zone. As a result, an \$850,000 exploration program was proposed that included further target prioritization and about 2600 m of diamond drilling on the South, Amarillo and Fall Creek, and North Grids (Molloy, 1997).

In 1999, Okak Bay Resources Ltd. funded an \$85,000 exploration program, which was carried out by Geofine. The work included the discovery of the Zinc Zone; and, the MEXT and NEXT Zones. Detailed follow-up work was carried out on the North, Fall Creek and the Amarillo Zones. The historic Noranda drill holes on the South Zone were located and tied into the new 9950E Base Line. Fourteen proposed holes were spotted on the South, NEXT, North and Amarillo Zones and a drill program comprising at least 1200 m was recommended (Molloy, 1999).

In 2000, Island Arc Mining Corporation funded a \$125,000 geological and geochemical program to mainly evaluate the apparent northern extension of the South Zone deposit ("SZD"; Molloy, 2000). The work included the staking of the Benji 8-12 Claims (Map 1, Table 1), mainly to cover the postulated southern and northern extensions of the SZD; the taking and interpretation of air photos of the South Zone to precisely locate the South Zone Structure ("SZS") and its possible extensions; the refurbishing of parts of the historic Noranda/Geofine South Zone Grid and the re-spotting of the drill holes located in 1999 on the SZD; the extension of the 1999 South Zone Base Line to 8925N and 10550N; and, the installation of control lines i.e., the By Glacier Control Line; the Southern Projection Line of the SZD; the Todd Valley Control Line (C Line) from the southern area of the SZD to north of the NEXT Zone; the MEXT/NEXT Zone Control Lines on the cliff above the MEXT and NEXT Zones; and, the Knob Zone Control Lines. The program also included the refurbishing of part of the Amarillo Grid and the re-spotting of drill holes spotted in 1999, as snow conditions allowed. Some detailed grid lines were also over the Barite and North Barite Zones. In view of extensive snow cover in 2000, only minimal work could be carried out on the Yellow Bowl Zone.

Geological and geochemical surveys on the aforementioned control and grid lines included some hand stripping and the collection of 368 rock (talus, float, sub crop, panel, glacial boulders), soil, stream sediment and check samples. SZS mineralization types were classified; and, 343 of the samples were analyzed by FA/AA for gold, and by 34 element ICP. Some additional whole rock, tungsten, tin and quality assurance analyses were carried out. Seven drill holes were spotted and topographic surveys run on drill section lines.

## 6. REGIONAL GEOLOGY:

The Todd Creek property is situated in a broad, north-northwest trending volcanogenic-plutonic belt consisting of the Upper Triassic Stuhini Group and the Upper Triassic to Lower Middle Jurassic Hazelton Group. This belt has been termed the "Stewart Complex" (Figures 5, 6) by Grove (1986) and forms part of the Stikinia Terrane. The Stikinia Terrane, together with the Cache Creek and Quesnel Terranes, constitute the Intermontaine Superterrane, which was accreted to North America in Middle Jurassic time (Monger et al, 1982). To the west, the Stewart Complex is bordered by the Coast Plutonic Complex. Sedimentary rocks of the Middle to Upper Jurassic Bowser Lake Group overlay the Stewart Complex in the east.

The Jurassic stratigraphy was established by Grove (1986, Figure 5) during regional mapping conducted from 1964 to 1968. Formational subdivisions have been made and are currently being modified and refined as regional work continues, most notably by the Geological Survey Branch of the British Columbia Ministry of Energy, Mines and Petroleum Resources (Alldrick, 1984, 1985, 1989); and, by the Geological Survey of Canada (Anderson, 1989; Anderson and Thorkelson, 1990; Lewis, et al, 1992; Creig, et al, 1995). The sedimentological, structural, and stratigraphic framework of the area is being established with some degree of precision. The Hazelton Group represents an evolving (alkalic/calc-alkalic) island arc complex, capped by a thick turbidite succession (Bowser Lake Group). Grove (1986) divided the Hazelton into four litho-stratigraphic units (time intervals defined by Alldrick et al, 1987):

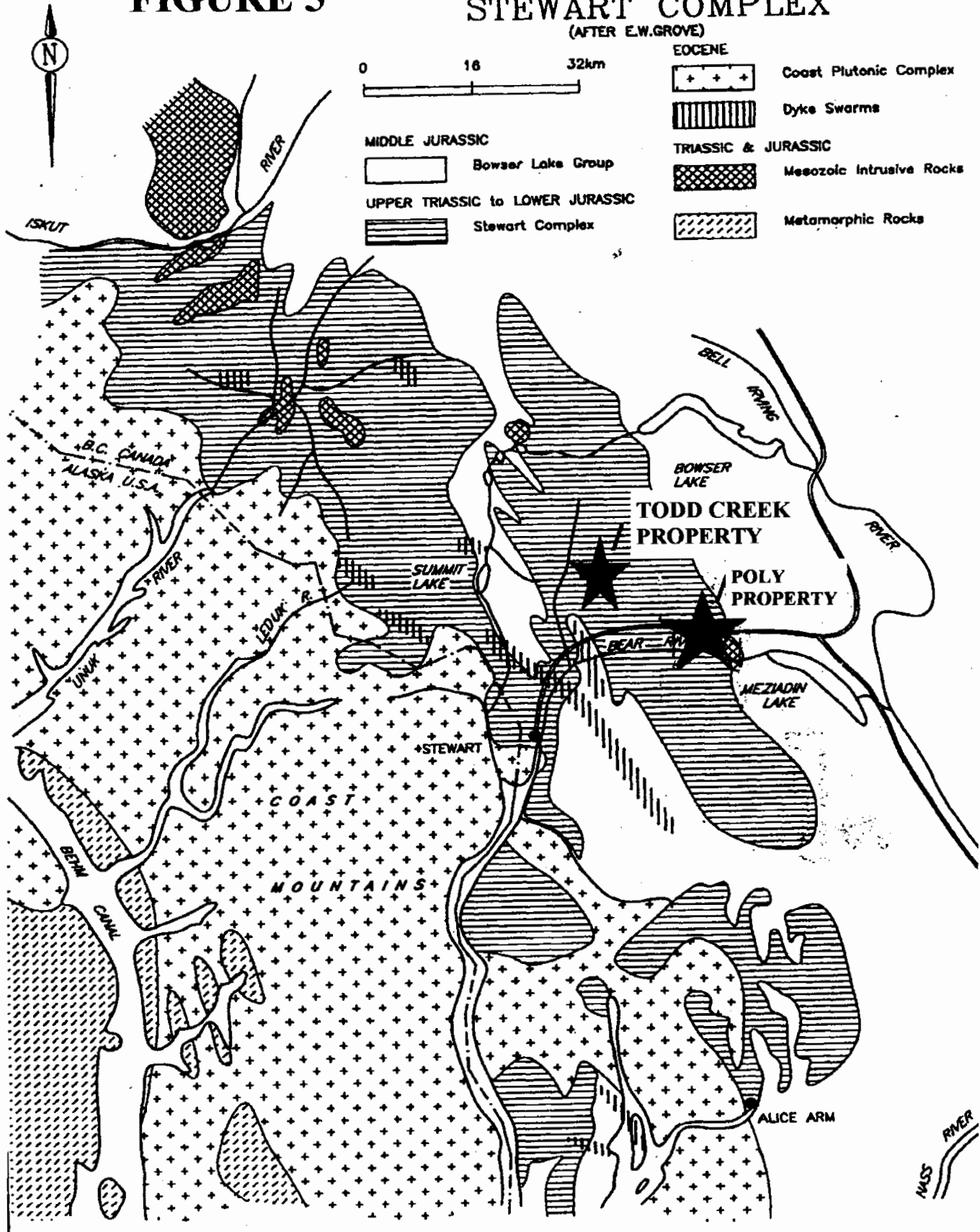
1. The Upper Triassic to Lower Jurassic Unuk River Formation (Norian to Pliensbachian).
2. The Middle Jurassic Betty Creek Formation (Pliensbachian to Toarcian).
3. The Middle Jurassic Salmon River Formation (Toarcian to Bajocian).
4. The Middle to Upper Jurassic Nass Formation (Toarcian to Oxfordian - Kimmeridgian).

Alldrick assigned formational status (Mt. Dilworth Formation, Figure 7) to a Toarcian rhyolite unit (Monitor Rhyolite) overlying the Betty Creek Formation. Rocks of the Salmon River Formation are transitional between the mostly volcanic Hazelton Group and the wholly sedimentary Bowser Lake Group and are presently regarded as the uppermost formation of the Hazelton or the basal formation of the Bowser Lake Group.

The Unuk River Formation (Figure 7), a thick sequence of andesite flows and pyroclastic rocks with minor interbedded sedimentary rocks, hosts a number of major gold deposits in the Stewart Camp (Figure 2). The unit is unconformably overlain by heterogeneous, maroon to green, epiclastic volcanic conglomerates, breccias, greywackes and finer grained clastic rocks of the Betty Creek Formation. Felsic flows, tuffs and tuff breccias characterize the Mt. Dilworth Formation (Figure 7). This formation represents the climatic and penultimate volcanic event of the Hazelton Group volcanism and forms an important regional marker horizon. The overlying Salmon River Formation has been subdivided in the Iskut area into an Upper Lower Jurassic and a Lower Middle Jurassic member (Anderson and Thorkelson, 1990). The upper member has been further subdivided into three north trending facies belts: the eastern Troy Ridge facies (starved basin), the medial Eskay Creek

# FIGURE 5

## REGIONAL GEOLOGY STEWART COMPLEX (AFTER E.W.GROVE)





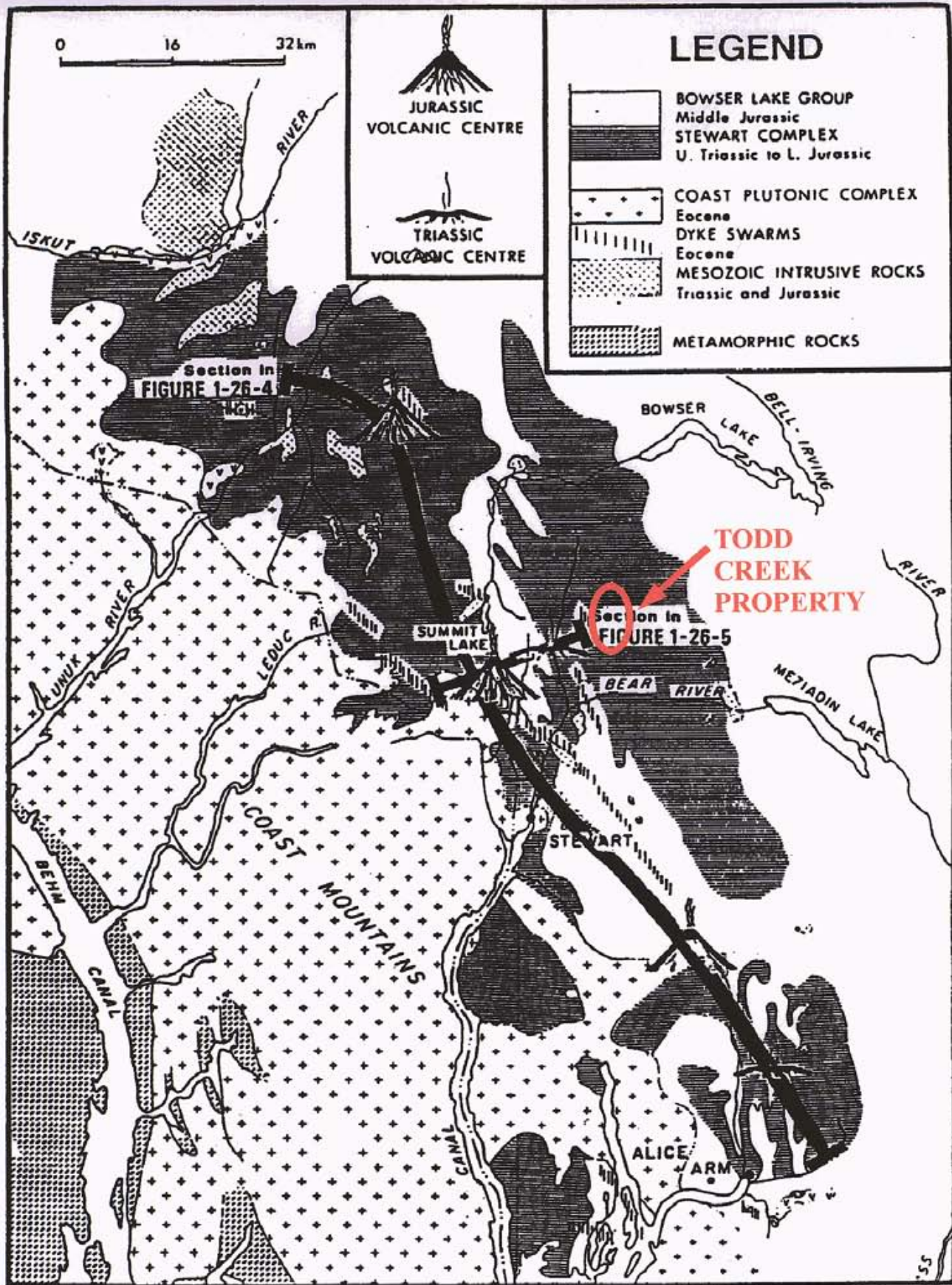


Figure 1-27-3. Distribution of the Stewart complex showing the locations of section lines for Figures 1-27-4 and 1-27-5.

**FIGURE 6**

**STEWART VOLCANIC BELT**



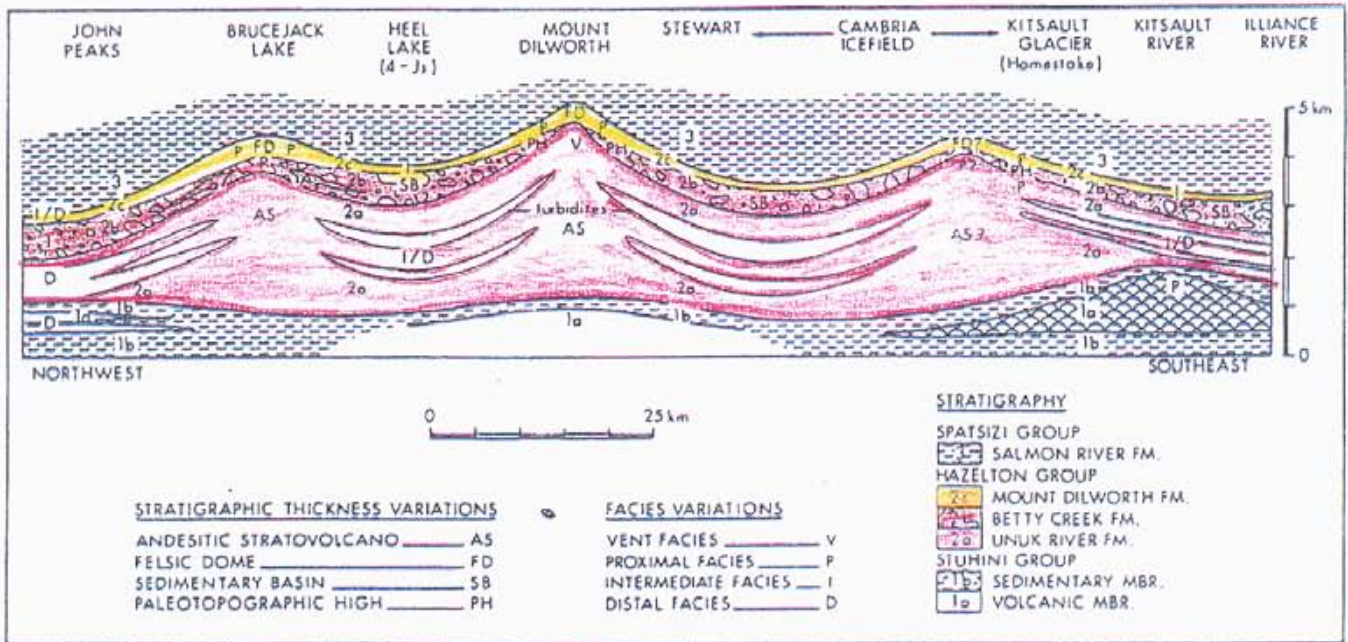


Figure 1-27-4. North-south schematic reconstruction through the Stewart complex.

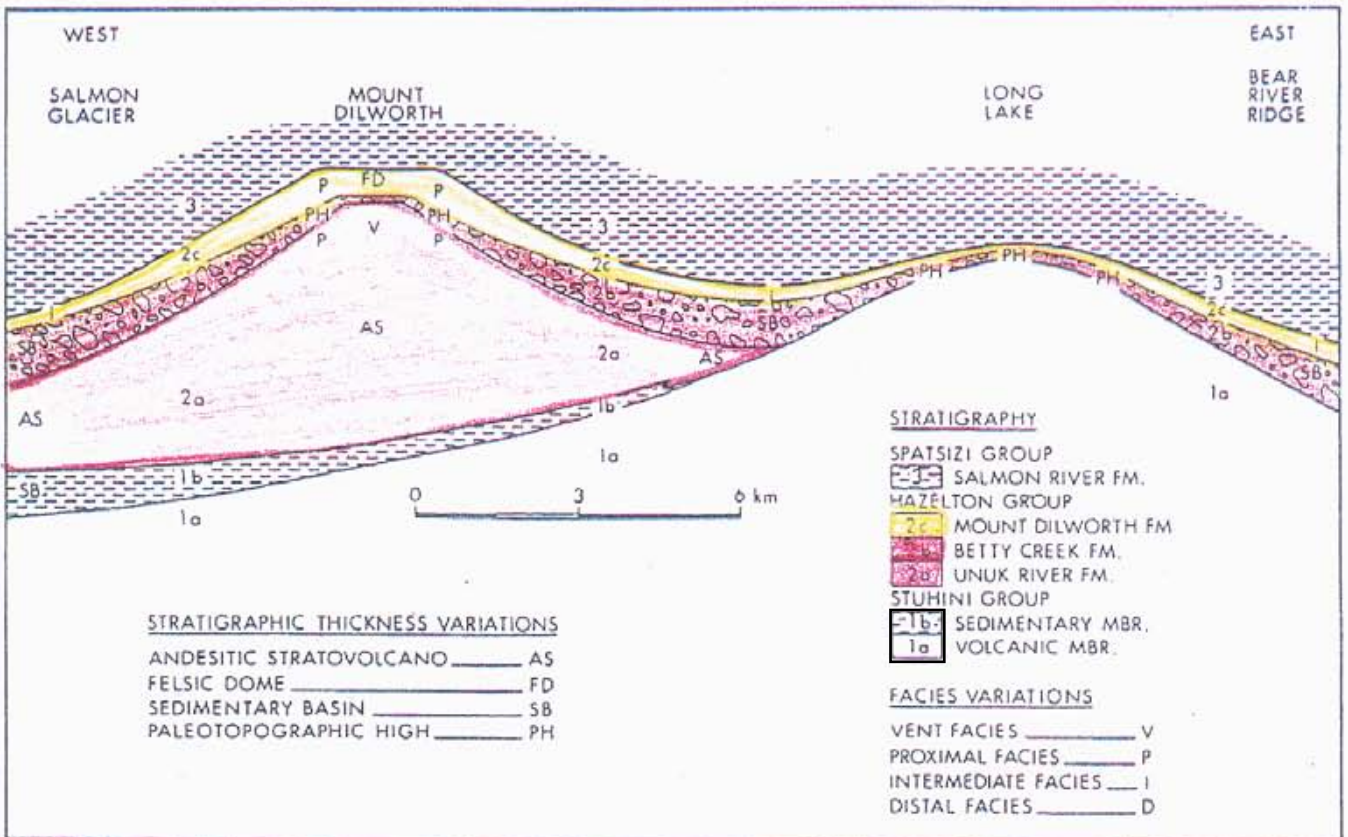


Figure 1-27-5. West-east schematic reconstruction through the Stewart complex.

## FIGURE 7

### DILWORTH FORMATION IN STEWART COMPLEX STRATIGRAPHY



facies (back-arc basin) and the western Snippaker Mountain facies (volcanic arc). Sediments of the Bowser Lake Group rest unconformably on the Hazelton Group rocks and they include shales, argillites, silt and mudstones, greywackes and conglomerates. The contact between the Bowser Lake Group and Hazelton Group passes between Strohn Creek in the north and White River in the south. The contact appears to be a thrust zone with the Bowser Lake Group sediment "slices" occurring within and overlying the Hazelton Group pyroclastics to the west.

Two main intrusive episodes occurred in the Stewart Area: a Lower Jurassic suite of diorite to granodiorite porphyries (Texas Creek Suite) that are comagmatic with extrusive rocks of the Hazelton Group; and, an Upper Cretaceous to Early Tertiary intrusive complex (Coast Plutonic Complex and satellite intrusions). The early Jurassic suite is characterized by the occurrence of coarse hornblende, orthoclase and plagioclase and phenocrysts and locally potassium feldspar megacrysts. The Eocene Hyder quartz-monzonite, comprising a main batholith, several smaller plugs and a widespread dyke phase, represents the Coast Plutonic Complex.

Middle Cretaceous regional metamorphism (Alldrick et al., 1987) is predominantly of the lower greenschist facies. This metamorphic event seems to be related to compression and concomitant crustal thickening at the Intermontaine - Insular superterrane boundary (Rubin et al., 1990). Biotite hornfels zones are associated with a majority of the quartz monzonite and granodiorite stocks.

## 7. REGIONAL MINERALIZATION AND EXPLORATION ACTIVITIES:

The Stewart Complex is the setting for the Stewart (Silbak-Premier, Silver Butte, Big Missouri, Red Mountain), Iskut (Snip, Johnny Mountain, Eskay Creek) Sulphurets, and Kitsalt (Alice Arm) gold/silver mining camps (Figure 2). Mesothermal to epithermal, depth persistent gold-silver veins form one of the most significant types of economic deposit. There appears to be a spatial as well as a temporal association of gold deposits to Lower Jurassic calc-alkaline intrusions and volcanic centres (Figures 8, 8A, 8B). In the Stewart area, the main regional trend of mineralization corresponds with the trend of the Jurassic Stewart Volcanic Belt (Figures 6, 8B). A second volcanic belt and associated regional linear trend of mineralization is postulated to extend from south of the area of the Red Mountain deposit north through the Todd Creek area (Figure 8 B). The intrusions are often characterized by 1-2 cm sized, potassium feldspar megacrysts and correspond to the top of the Unuk River Formation.

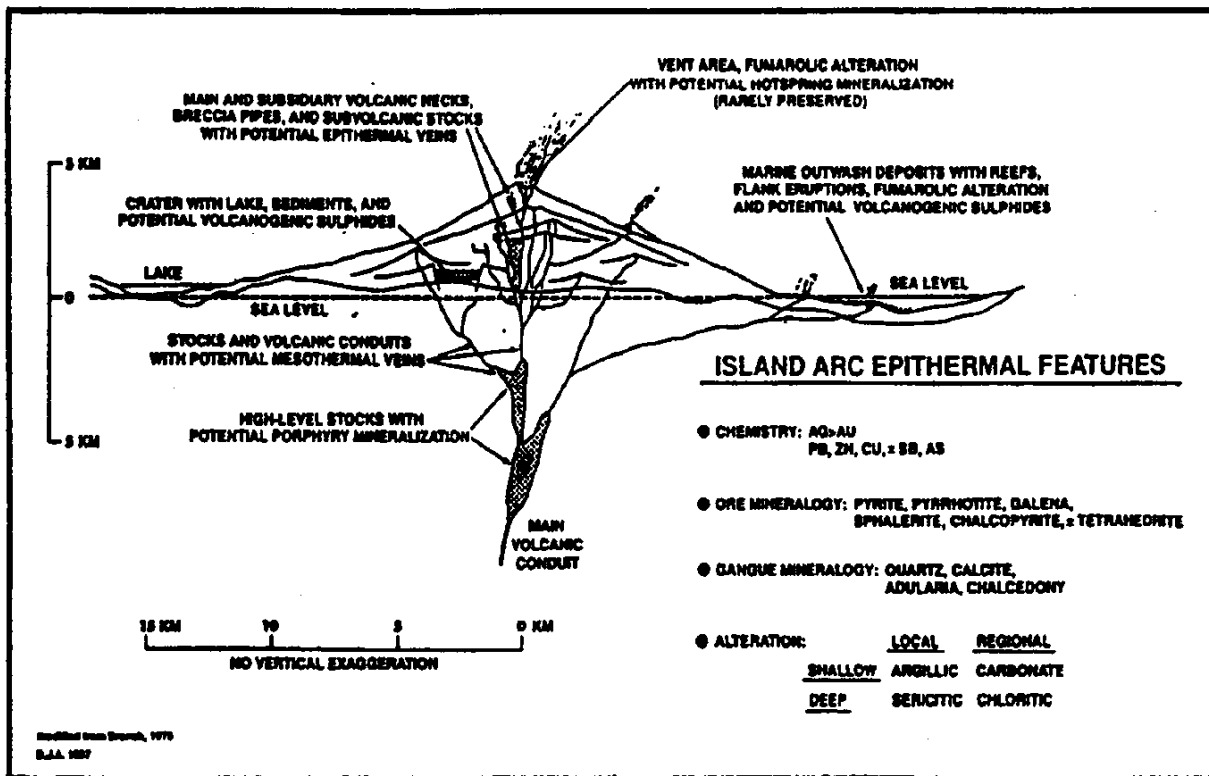
The most prominent example of this type of mineralization is the historic Silbak-Premier gold-silver mine, which is located in the main, Stewart volcanic belt (Figure 2). The mine produced 56,000 kg of gold and 1,281,400 kg of silver in its original lifetime from 1918 to 1976. The mine was re-opened by Westmin in 1988 with reserves quoted at 5.9 million tonnes grading 2.16 g gold/t and 80.23 g silver/t (Randall, 1988). The mine was closed in the summer of 1997 and the mill was put up for sale.

The ore is hosted by Unuk River Formation andesites and comagmatic Texas Creek porphyritic dacite sills and dykes. The ore bodies comprise a series of en echelon lenses, which are developed over a strike length of 180 m and through a vertical range of 600 m (Grove, 1986; McDonald, 1988). The mineralization is controlled by northwesterly and northeasterly trending structures and their intersections but also occurs locally concordant with andesitic flows and breccias.

Two main vein types occur: silica-rich, low-sulfide precious metal veins and sulfide-rich base metal veins. The precious metal veins are more prominent in the upper levels of the deposit and contain polybasite, pyrargyrite, argentiferous tetrahedrite, native silver, electrum and argentite. Combined sulfides of pyrite, sphalerite, chalcopyrite and galena are generally less than 5%. The base metal veins crosscut the precious metal veins and increase in abundance with depth. They contain 25 to 45% combined pyrite, sphalerite, chalcopyrite and galena, with minor amounts of pyrrhotite, argentiferous tetrahedrite, native silver, electrum and arsenopyrite.

Quartz is the main gangue mineral, with lesser amounts of calcite, barite, and some adularia being present. The mineralization is associated with strong silicification, feldspathization, and pyritization. A temperature range of 250 to 260 degrees C has been determined for the deposition of the base and precious metals (McDonald, 1988).

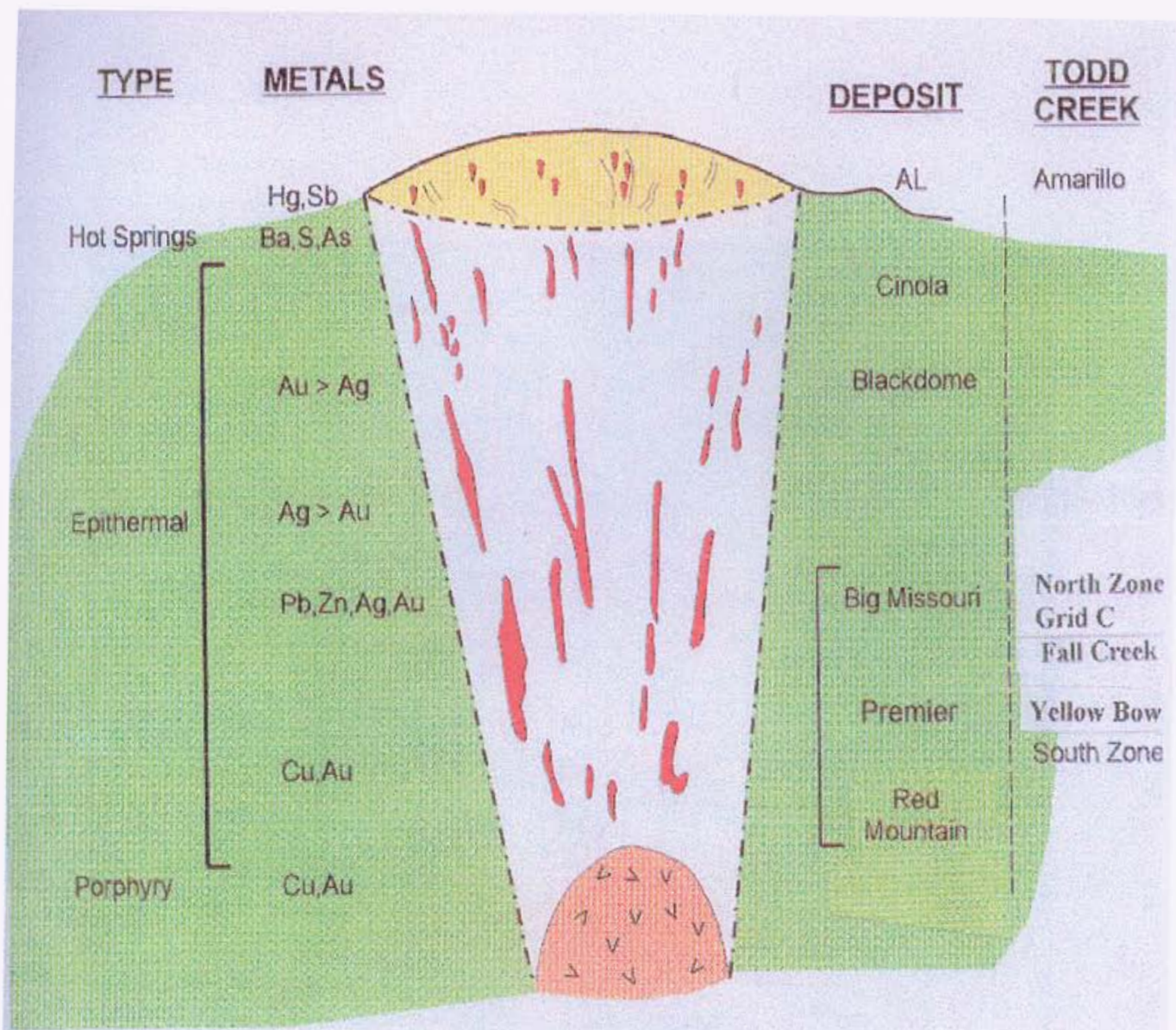
Middle Eocene silver-lead-zinc veins are characterized by high silver to gold ratios and by spatial association with molybdenum and/or tungsten occurrences. They are structurally controlled and lie within north, northwest, and east trending faults. This mineralization has been less significant in economic terms.



Distribution of ore deposits within a stratovolcano (modified from Branch, 1976).

## FIGURE 8

### MINERALIZATION TYPES STEWART CAMP



(after Panteleyev, 1986 and others)

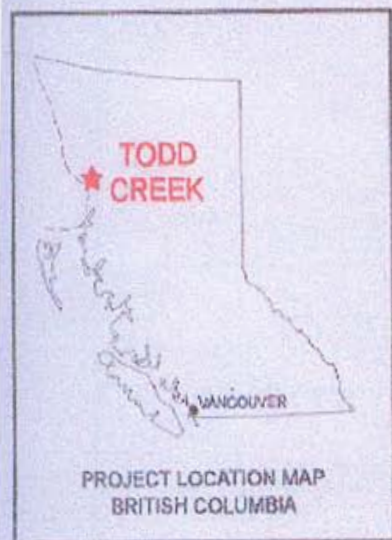
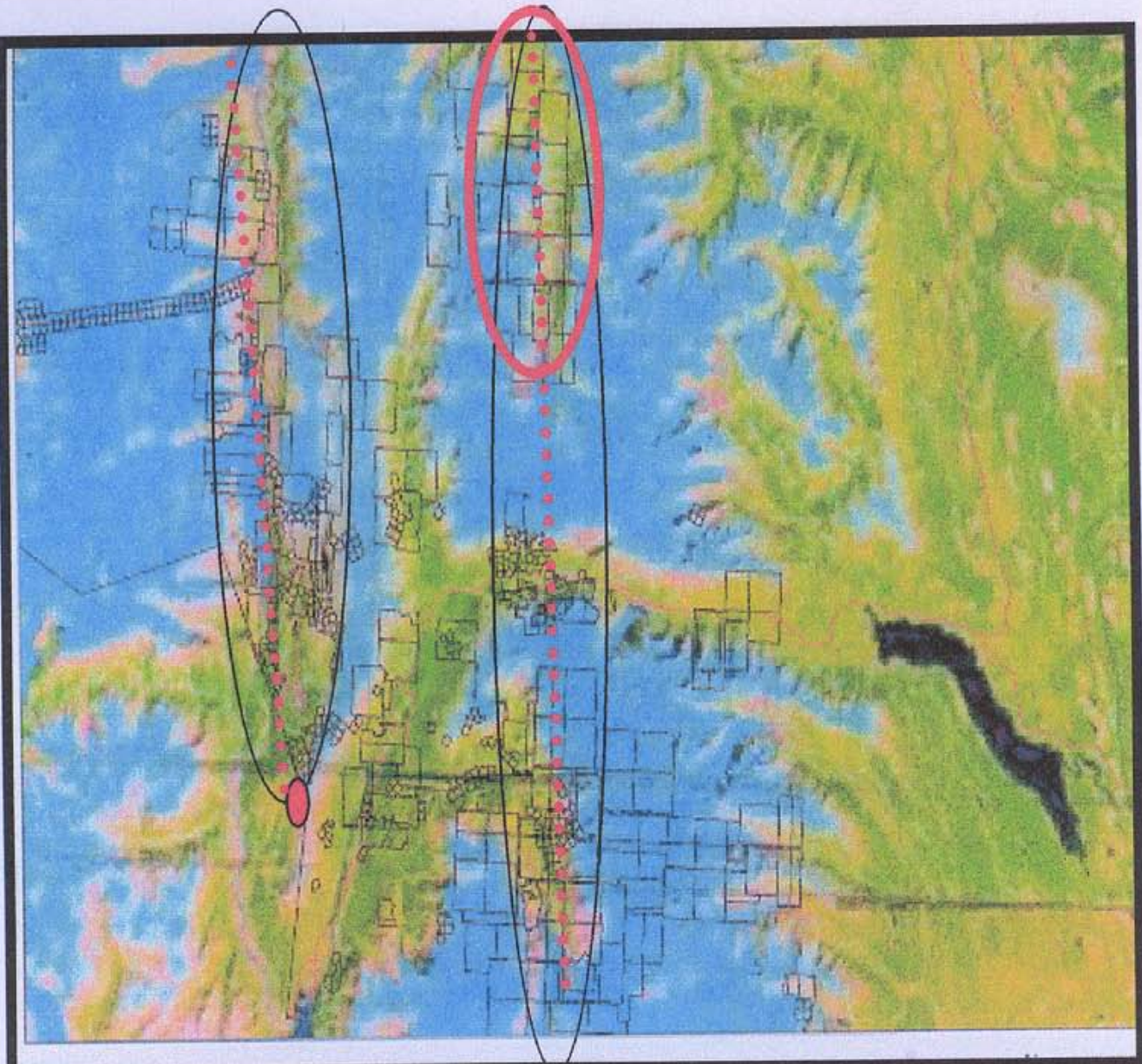


FIGURE 8A





EPITHERMAL MINERALIZATION TYPES,  
TODD CREEK PROPERTY





**FIGURE 8B**

**LANDSAT IMAGE, STEWART AREA**

-  **MINERAL TITLES**
-  **TODD CREEK PROPERTY**
-  **STEWART**
-  **MINERALIZATION TREND**



SCALE ~1: 383,595

Porphyry molybdenum deposits are associated with Tertiary Alice Arm Intrusions, a belt of quartz-monzonite intrusions parallel to the eastern margin of the Coast Plutonic Complex. An example of this type of deposit is the BC Molybdenum Mine at Lime Creek.

Barrick Gold Corporation acquired its 100% interest in the Eskay Creek Mine via a merger with Homestake in December 2001. In 2003 the mine produced about 350,000 ounces of gold and about 17 million ounces of silver. Proven and probable reserves at the end of 2003 totalled 927,000 tons grading 1.02 ounces gold/ton and 46.78 ounces silver/ton. Production for 2004 is expected to be about 300,000 ounces of gold and 14 million ounces of silver (Barrick, 2003).

The deposit is hosted within Contact Unit carbonaceous mudstone and breccia, as well as the underlying rhyolite breccia. Two styles of mineralization are present. The first is a visually striking assemblage of disseminated to near massive stibnite and realgar within the Contact Unit. The second style occurs in the adjacent footwall rhyolite, and features a stock work style quartz-muscovite-chlorite breccia mineralized with sphalerite, tetrahedrite and pyrite. Highest gold and silver values are obtained where the Contact Unit is thickest and the immediately underlying rhyolite breccia is highly fractured and altered (Blackwell, 1990; Barrett et al, 1996). Drilling continues to expand the original, approximately 280 m by 100 m zone that has an average thickness of 10 m.

The Eskay Creek 21B deposit is approximately 900 m long, from 60 to 200 m wide and locally in excess of 40 m thick. Contact Unit mineralization comprises a continuous stratiform sheet of banded high-grade gold and silver bearing base metal sulfide layers, from 2 to 12 m thick. Mineralization appears to be bedding parallel. Sulfide minerals present include sphalerite, tetrahedrite, boulangerite, bornite plus minor galena and pyrite. Gold and silver are associated with electrum, which occurs as abundant grains associated with sphalerite. Peripheral and footwall to the banded sulfide mineralization, are areas of microfracture, veinlet hosted, disseminated tetrahedrite, pyrite and minor boulangerite mineralization.

On December 31, 2001, Seabridge Gold Inc. acquired a 100% interest in the Red Mountain advanced stage gold project from North American Metals Corp. a subsidiary of Wheaton River Minerals Ltd. In January 2003 Steffen Robertson and Kirsten (Canada) Inc. ("SRK") completed an engineering and preliminary economic study of the project for Seabridge. The SRK mineral resource calculation is shown in the following table (Seabridge, 2004):

| <b>Resources Used in SRK Study - All Categories of Resources (000's)</b> |                |               |               |
|--------------------------------------------------------------------------|----------------|---------------|---------------|
|                                                                          | <b>Tonnes</b>  | <b>Au g/t</b> | <b>Ag g/t</b> |
| <b>Mineral Resources (All Categories &gt; 0 g/t Au)</b>                  | <b>1,941.2</b> | <b>7.74</b>   | <b>26.2</b>   |
| <b>Mineral Resources (All Categories &gt; 6 g/t Au)</b>                  | <b>1,216.6</b> | <b>9.14</b>   | <b>28.7</b>   |
| Mining Recovery                                                          | 89%            |               |               |
| Recovered Tonnes                                                         | 1,081.2        | 9.13          | 28.9          |
| Dilution Percent                                                         | 14%            |               |               |
| Dilution Tonnes                                                          | 180.7          | 0.55          | n/a           |
| <b>Tonnes</b>                                                            | <b>1,261.9</b> | <b>7.90</b>   | <b>24.7</b>   |

Under SRK's base case analysis and using a 5% discount rate, a break-even project is achieved at a gold price of US\$399/oz. The life of mine cash operating costs average US\$213 per ounce and total costs, inclusive of capital, average US\$358 per ounce. A 50% increase in mineable tonnage and reductions of 15% in capital and operating costs would reduce the break even gold price to \$338.

Seabridge did not carry out any work on the Red Mountain project in 2004. The deposit is comprised of the Marc Zone and its northerly extension, the AV Zone. The zones comprise sulfide lenses or cylinders associated with a structural junction and the brecciated contact of the Goldslide Intrusion. The mineralization consists of densely disseminated to massive pyrite and/or pyrite stringers and veinlets and variable amounts of arsenopyrite, tetrahedrite and various tellurides. Several phases of mineralization and deformation are indicated by the presence of different generations of pyrite and breccia fragments consisting of pyrite. High-grade gold values are usually associated with the semi massive, coarse-grained pyrite aggregates, but also with stock works of pyrite stringers and veinlets. Gold occurs as native gold, electrum and as tellurides.

As reported by the BC Ministry of Energy and Mines, the substantial increase in exploration activities in BC in 2003 (\$45-\$55 M) continued in 2004 with estimated expenditures between \$90 - \$120 M. Exploration expenditures in the Northwest Region in 2004 are expected to range between \$32 - \$42 M. In the Eskay-Bob Quinn-Stewart-Smithers-Terrace area, 47 projects were expected to be carried out, including 19 drill programs.

One of the largest drill programs in the Stewart area in 2004 comprised about 4800 m in 36 holes and was completed on the Del Norte Property by Teuton Resources Corporation and Lateegra Resource Corp. (LEG). The Del Norte property is located approximately 32 km east of Stewart in the upper drainage area of the White River system. The target is silver-gold mineralization in quartz-sulfide breccia veins (the Kosciuszko Zone, the LG Vein, the LG Vein Extension and the Horatio Zone) that have been found over a vertical distance of over 300 m and along a 9.7 km long trend (Teuton Resources Corp., 2004)

LEG also funded work carried by Geofine on the Poly Property (Geofine, 2004). The Poly Property is located on the Stewart Hwy 37A, about 10 km northwest of the Del Norte Property. Spectral IP and magnetic surveys carried out in 2004 have outlined 3 moderate to very strong chargeability zones interpreted to be associated with coarse sulfides in epithermal-mesothermal quartz veins and stockworks. The veins often contain significant precious and base metal mineralization. The zones have strike lengths up to over 800 m and will be tested by a drill program funded by LEG in 2005.

## **8. TODD CREEK PROPERTY GEOLOGY, MINERALIZATION:**

The Lower Jurassic Unuk River Formation of the Hazelton Group dominates southern and central areas of the property geology (Grove, 1982; Figure 9; Maps 2-4). The formation hosts most of the significant base and polymetallic mineralization in the Stewart Camp. Unaltered rocks mainly comprise monotonous green-grey, red, purple tuff-breccia, breccia and agglomerate, with interbeds of crystal and lithic tuff. Green and grey-black andesite and dacite to rhyolite flows are commonly found in various areas of the property; however, their distribution is rather limited relative to that of the ubiquitous pyroclastic rocks.

Middle Jurassic Hazelton Group sediments (siltstone, greywacke, sandstone and conglomerate) of the Salmon Arm Formation overlie Unuk River Rocks on the northern part of the property. Rhyolite and rhyolite breccia of the Mt. Dilworth Formation (Figure 7) are found mainly on the northeast part of the property.

As indicated in Min File Report 104A 001, the rocks are reported to have been intruded by a number of feldspar porphyry bodies, the extent of which remain to be determined. As indicated by the regional total field magnetics (Figure 10), a number of circular magnetic lows in the southern area of the property may reflect such intrusions or zones of alteration. However, based on Geofine's experience on the property, much of the reported porphyry in the South Zone is crystal tuff. Feldspar porphyry +/-hornblende was observed at the north end of the NEXT Zone and quartz feldspar porphyry +/-hornblende is associated with sulfidized breccias at the north end of the Knob Zone. Based on the coarse breccia and associated porphyry, the Knob Zone is interpreted to be located proximal to a volcanic centre.

Varying degrees of pervasive alteration have been mapped ranging from calcite-epidote-pyrite, chlorite-quartz-pyrite, quartz-carbonate-pyrite to quartz-pyrite-sericite-jarosite-alunite. A spectacular gossan zone comprises much of the Orange Mountain Target Area (Map 2A) and is associated with altered (quartz-barite-hematite) pyroclastic rocks and andestitic flows. The Amarillo Zone is located on the east side of Orange Mountain (Maps 1, 2A; Figure 8A) and is thought to epitomize the top of a large epithermal system, characterized by ubiquitous barite, often mineralized with varying amounts of galena, sphalerite and chalcopyrite.

As mapped by Grove (Figure 9), the property is bordered on the west by a major northeast trending fault that follows American Creek, and partially on the east by a north trending structure. A major north trending fault system is postulated to be associated with the Todd Creek Valley. The fault system includes the South Zone Structure (Map 2A) that generally trends about 10° and dips 65° to the west. As noted in Section 7, the regional system is interpreted to extend from the south of the Red Mountain deposit north, across Bear Valley and the Todd Ice field, and down the Todd Creek Valley. As indicated in Figure 8B, a regional mineralization trend is related to the structure, which is thought to be associated with a second zone of volcanism, the Eastern Jurassic Volcanic Belt (Figures 6, 8B).

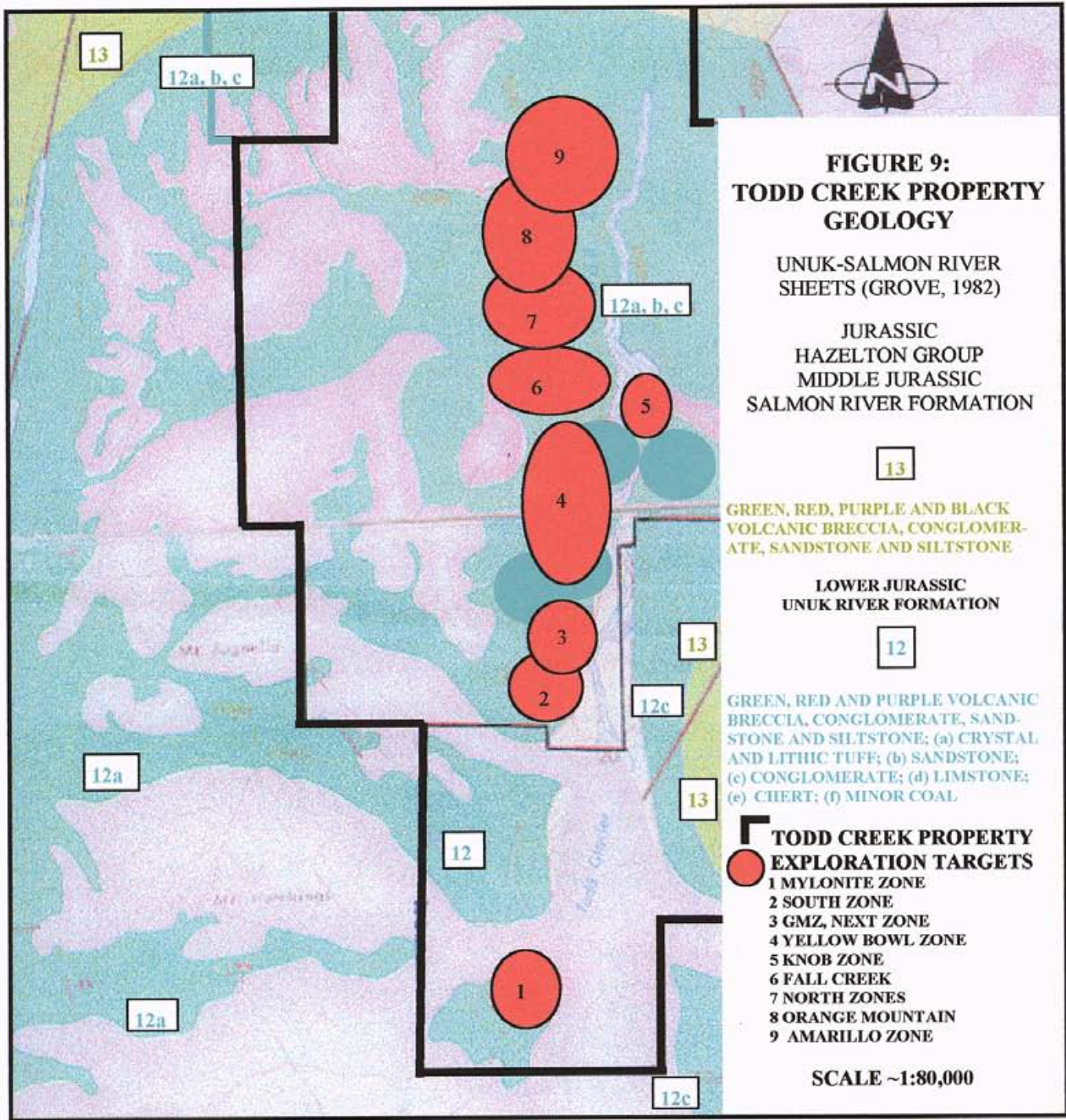
The structural components of the Todd Creek Property are dominated by an orthogonal to sub



orthogonal fabric that generally trends north-northeast and west-northwest. Dips are generally to the northwest and southwest. Most of the mineralization discovered to date on the property is associated with the fabric and is most often hosted by South Zone Structure, or structures orthogonal to it, particularly at or in the vicinity of structural junctions. Such junctions are conducive to the development of south plunging ore shoot morphologies, which are one of the current exploration targets.

Many of the historical showings on the property, including the South Zone Deposit (207,000 t grading 5.48 g gold/t, along with significant copper credits) comprise multiphase quartz-pyrite-chalcopyrite +/-hematite, galena and sphalerite breccia veins. Such banded veins generally have a massive to semi-massive pyrite +/- chalcopyrite core, surrounded by sulfide matrix breccia and/or blebby chalcopyrite breccia. Along strike metallic zoning apparently includes the replacement of chalcopyrite by auriferous specular hematite. The mineralization is hosted mainly by quartz-pyrite and quartz-pyrite-sericite altered volcanic breccia, agglomerate and crystal tuff-breccia and crystal tuff. Extensive gossan zones of limonite +/- hematite and jarosite/alunite are developed on the sulfidized host rocks.

*Altered dacite to rhyolite stratigraphy at Yellow Bowl, as well as the intensely sulfidized breccia at the Knob Zone, are deemed to have volcanogenic massive sulfide potential. Historic exploration efforts have not been focused on these targets in view of the much more readily apparent copper-gold mineralization exposed in the outcrops of well-mineralized breccia veins. However, exploration success on the property is dependent on the discovery of an ore body, and the apparent targets with size potential to host a large, economic deposit are associated with the Amarillo, Yellow Bowl and Knob Zones.*



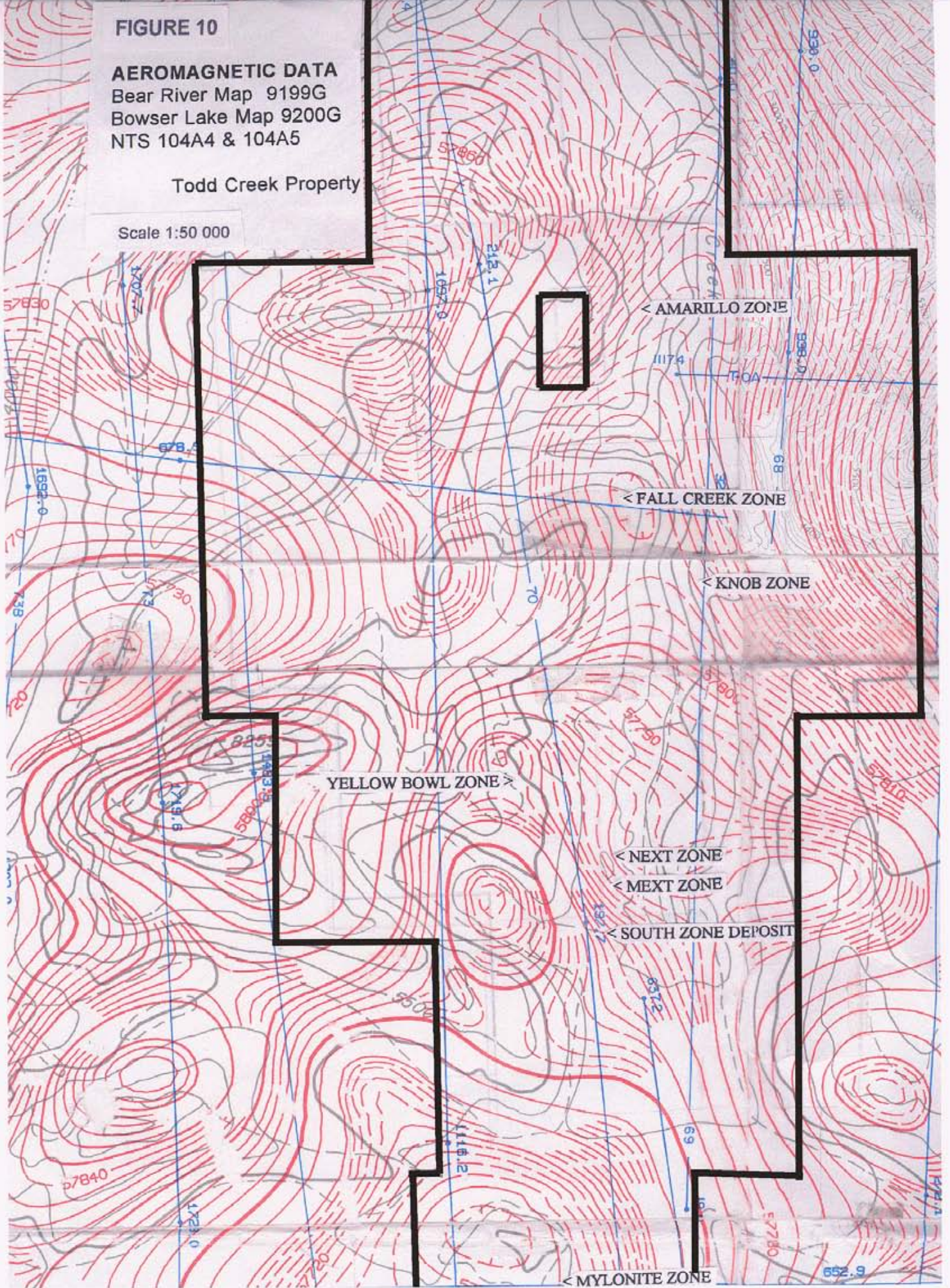


**FIGURE 10**

**AEROMAGNETIC DATA**  
Bear River Map 9199G  
Bowser Lake Map 9200G  
NTS 104A4 & 104A5

Todd Creek Property

Scale 1:50 000





## **9. 2004 DRILL PROGRAM, TODD CREEK PROPERTY:**

Geofine Exploration Consultants Ltd. carried out the 2004 drill program on the Todd Creek Property in June, July and August. The work was supervised by David Molloy, P. Geo. (APGO, BCAPEG) and David Kennedy, P. Geo. (BCAPEG). Exploration expenditures, including drill target selection and prioritization, permitting, camp, helicopter, fuel, supplies and equipment, communications, field work, pad building, reclamation, mob-demob, subsistence, analyses, security, data verification and quality assurance, reporting, filing fees, overhead and GST total about \$329,000 and are summarized in Table 2.

The 2004 Todd Creek program comprised a number of phases:

**1A: target selection and prioritization in May;**

**1B: grid refurbishing, topographic surveys, hole spotting, geological surveys, composite sampling, camp installation, diamond drilling, core logging and sampling, and reclamation in June, July and August;**

**1C: final reporting in November and December.**

### **9.1.A. PHASE 1A: Drill Target Selection:**

The historic database was reviewed in May to prioritize drill targets on the Todd Creek Property. Two priority drill target areas were identified:

- 1) the South Zone deposit and its apparent northern extensions i.e., the Gold Gully-MEXT and NEXT Zones;
- 2) the Fall Creek East F1 and North A Zones, located about 4 km north of the South Zone deposit.

The 2004 diamond drill program proposed by Geofine is shown in Table S1 and the exploration rationale is described below.

TABLE 2: 2004 EXPLORATION EXPENDITURES, TODD CREEK PROPERTY:

| EXPENDITURE TYPE:                                                                                                                                                                           | AMOUNT*<br>(\$CDN): | GST INCL.<br>(\$CDN): |
|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------|-----------------------|
| SALARIES, FEES:<br>RE. DRILL TARGET COMPILE, SELECTION,<br>BUDGETING, PERMITTING, FIELD WORK INCL.<br>DRILL PROGRAM, SECURITY, QUALITY<br>ASSURANCE, DATA VERIFY, RECLAMATION,<br>INSURANCE | 47731.75            | 3018.25               |
| SUPPLIES:                                                                                                                                                                                   | 3619.62             | 184.39                |
| COMMUNICATIONS                                                                                                                                                                              | 3013.70             | 186.97                |
| ACCOMODATION, SUBSISTANCE INCL COOK                                                                                                                                                         | 23547.90            | 850.05                |
| MOB-DEMOB:                                                                                                                                                                                  | 4547.83             | 297.01                |
| AIRCRAFT TRAVEL:                                                                                                                                                                            | 365.99              | 19.39                 |
| HELI CHARTER                                                                                                                                                                                | 58553.78            | 3830.63               |
| ANALYSES:                                                                                                                                                                                   | 9581.61             | 626.74                |
| VEHICLE, KMS, INSURANCE                                                                                                                                                                     | 2926.52             | 191.45                |
| COURIER, SHIP, EXPEDITE:                                                                                                                                                                    | 2225.45             | 145.61                |
| CAMP MOB, DEMOB, BUILD, MAINTENANCE<br>DISMANTLE; DRILL PADS: BUILD, DISMANTLE                                                                                                              | 50557.50            | 3307.50               |
| DIAMOND DRILLING, PROJECT FUEL,<br>EXPEDITING                                                                                                                                               | 82312.37            | 939.50                |
| COPIER                                                                                                                                                                                      | 1114.94             | 70.78                 |
| DATA ENTRY, VERIFY, COMPILE, COMPUTER<br>PLOTS, INTERPRET, QUALITY ASSURANCE,<br>DRAFTING; REPORTING, REPRODUCTION;<br>CLOSE PERMIT INCL PHOTO RECORDS,                                     | 15500.00            | 1013.70               |
| FILING FEES, CLOSE PERMIT,<br>PERMITTING REQUIREMENTS                                                                                                                                       | 13180.00            |                       |
|                                                                                                                                                                                             | _____               | _____                 |
| TOTAL:                                                                                                                                                                                      | 318778.96           | 14681.97              |
| OVERHEAD                                                                                                                                                                                    | <u>10208.37</u>     |                       |
| GRAND TOTAL:                                                                                                                                                                                | 328987.33           | <u>14681.97</u>       |



**TABLE S1: PROPOSED 2004 DRILL PROGRAM, TODD CREEK PROPERTY:**

**AREA 1, SOUTH ZONE TARGET AREA:**

| <b>TARGET:</b>                 | <b>HOLES:</b> | <b>METERS:</b> |
|--------------------------------|---------------|----------------|
| i. SOUTH ZONE DEPOSIT          | 4             | 755            |
| ii. GOLD GULLY-MEXT ZONES      | 4             | 330            |
| iii. NEXT ZONE                 | 1             | 175            |
| <b>AREA 1, PHASE 1 TOTALS:</b> | <b>9</b>      | <b>1260</b>    |

**AREA 2, FALL CREEK, ORANGE MOUNTAIN TARGET AREAS:**

| <b>TARGET:</b>                 | <b>HOLES:</b> | <b>METERS:</b> |
|--------------------------------|---------------|----------------|
| 7i. FALL CREEK EAST F1 ZONE    | 3             | 255            |
| ii NORTH A ZONE                | 2             | 280            |
| <b>AREA 2, PHASE 1 TOTALS:</b> | <b>5</b>      | <b>535</b>     |

**9.1.A.i. AREA 1. i) SOUTH ZONE DEPOSIT (MAPS 1, 2, 2A, 3, 4, 4A, 5):**

The South Zone deposit (“SZD”) is hosted by the South Zone Structure (“SZS”) and is reported to contain drill indicated reserves of 207,000 tonnes grading 5.48 g Au/t (Hemlo Gold Mines Inc., 1988 Annual Report), along with significant copper credits. The mineralization mainly comprises epithermal to mesothermal, multiphase hematite-quartz breccia veins containing coarse blebs of chalcopyrite (“M Type” mineralization; Frontspiece Photo 1). There is an apparent thickening of the SZD near the Camp Creek Fault and it is in this area that Noranda obtained some of its widest and highest grade drill intersections e.g., 6.12 g Au/t and 0.35% Cu over 6.1 m; 8.83 g Au/t and 0.45% Cu over 11.7 m; and, 3.61 g Au/t and 0.27% Cu over 29.75 m, including 6.91 g Au/t and 0.31% Cu over 8.15 m. These results, when plotted on Vertical Long Section 1 (“VLS 1”, Appendix D) are interpreted as evidence of possible plunging ore shoot morphologies in which the higher-grade mineralization is concentrated

Such shoots often have a major plunge direction and an orthogonal back plunge direction, with a regular periodicity of distribution of shoots along the principal controlling structure. For example on VLS 1, forward plunge axis line FP1 is a postulated major plunge direction and back plunge axis line BP1 is a postulated minor plunge direction. Closely spaced, initial follow-up drilling is often required to delineate the parameters of a plunging shoot. Once so defined, holes are drilled at or in proximity to the plunge axes, to obtain the highest grades and the widest intersections.

It should also be noted that holes drilled into such ore shoots often have a 1 in 3 success rate in hitting ore grade mineralization. This effect can usually be attributed to the physical characteristics of the ore, including the nugget effect. For example, the M Type mineralization in the SZD can apparently produce highly variable drill results, since it consists of coarse blebby disseminations of chalcopyrite +/- bornite and pyrite in multiphase breccia veins (Frontspiece Photo 1).

Additional rationale for follow-up drilling on the SZD includes evidence that the importance of auriferous hematite may not have been recognized and evaluated historically - both in the existing deposit and in its along strike extension i.e., the Gold Gully- MEXT Zone, where Spec Type is a main component.

Geofine proposed four 2004 confirmation and step out holes on the SZD to evaluate the postulated shoots:

**DDHSZD04-01 (Maps 4, 5; Cross Section 10115N; VLS 1; Proposed Length: 135 m):**

The hole was proposed to further define the morphology of the interpreted shoot i.e., to intersect the SZD about 27 m vertically below the intercept in Noranda Hole 88-27, which returned 3.08 g Au/t and 0.50% Cu over 8.25 m, including 6.34 g Au/t and 1.05% Cu over 2.95 m (VLS 1); and, about 15 m north of the intercept in Noranda Hole 88-35, which returned 8.6 g Au and 0.45% Cu over 11.7 m.

**DDHSZD04-02 (Maps 4, 5; Cross Section 10075N; VLS 1; Proposed Length 120 m):**

The hole was proposed to further define the morphology of the interpreted shoot i.e., to intersect the SZD about 25 m vertically below the intercept in Noranda Hole 88-19, which returned 3.61 g Au/t and 0.27% Cu over 29.75 m, including 6.91 g Au/t and 0.36% Cu over 8.15 m (VLS 1).

**DDHSZD04-03 (Maps 4, 5; Cross Section 10100N; VLS 1; Proposed Length 160 m):**

The hole was proposed to further define the shoot morphology, including the back plunge direction. It was originally designed to provide an intercept of the SZD about 15 m vertically below the intercept in Noranda Hole 88-37, which returned 6.12 g Au/t and 0.35% Cu over 6.10 m (VLS 1).

**DDHSZD04-04 (Maps 4, 5; Cross Section 10050N (See Noranda Section 10044N); VLS 1; Proposed Length 160 m):**

The hole was proposed to further define the shoot morphology, including the south plunge direction. It was designed to provide an intercept of the SZD about 38 m down the interpreted south plunge direction from DDHSZ04-02.

### **9.1.A.ii. AREA 1. ii) GOLD GULLY-MEXT ZONE (MAPS 4, 4A):**

The Gold Gully-MEXT Zone (“GMZ”) and NEXT Zone (Maps 4A, B) have never been evaluated with diamond drilling. They are postulated to represent the along strike, northern extension of the South Zone deposit and are located approximately 300 and 500 m north, respectively, of the northernmost Noranda historic hole on the SZD. Exploration conducted by Geofine in 1999 discovered the GMZ and work in 2000 suggested that the SZD mineralization continues along strike to the north, to and beyond the NEXT Zone.

The GMZ was discovered via Geofine’s follow-up of the Zinc Zone (Map 4A). In 2000, helicopter side looking air photos were used to trace the SZS from the SZD to the GMZ and the NEXT Zones and further to the north, along the cliff face on the west side of the Todd Creek Valley. The GMZ-NEXT Target Area extends at least 600 m beyond the SZD. At the MEXT Zone and to the north and south, mineralization often entails the introduction of significant amounts of Spec Type i.e., massive to semi-massive specular hematite to specular hematite (spec) matrix breccia +/- pyrite and chalcopyrite. Although Spec Type is usually deficient in copper and arsenic, it is usually strongly auriferous and has a tungsten association – where assayed, tungsten values range up to 900 ppm. The target area is deemed to be extremely interesting, since the auriferous hematite was apparently not recognized historically.

The exploration rationale of the target area was further advanced via the discovery of mineralized talus at the base of the cliff in which the SZS is exposed; and, the discovery of significant in situ mineralization and geochemical anomalies in soil samples. For example, the GMZ-NEXT Zone target area was evaluated in 2000 by installing a control line below the cliff and collecting 104 samples of mineralized angular talus and in situ mineralization from the northern area of the SZD to beyond the NEXT Zone. Of the 104 samples, 65% were collected north of the northernmost Noranda drill hole on the SZD, over a strike length of about 600 m; and, 52% of these were collected in the GMZ over a strike length of over 300 m. All strengths and varieties of mineralization were collected.

Samples were classified into types: massive to semi-massive sulfides (SM Type: pyrite +/- chalcopyrite); semi-massive sulfide matrix breccia (SMB Type: pyrite + chalcopyrite) and/or a sulfide breccia (M TYPE: blebby chalcopyrite, bornite +/- pyrite); sulfide stock works, and breccia veins and stringers (WRC Type: malachite, azurite, chalcopyrite +/- pyrite); and Spec Type.

The 104 samples had gold and copper contents ranging between <5 and 17740 ppb and 6 and 90900 ppm, and averaging 2728 ppb and 6941 ppm, respectively. SM Type comprised 11% of the samples collected and associated gold and copper values ranged between 560 and 8420 ppb and 137 to 90900 ppm, and averaged 4334 ppb and 23115 ppm, respectively. SMB Type comprised 13% of samples and associated gold and copper values ranged between 50 and 3860 ppb and 144 and 17400 ppm, and averaged 944 ppb and 8514 ppm, respectively. M Type comprised 32% of the samples and associated gold and copper values ranged between 35 and 12470 ppb and 472 and 28800 ppm, and averaged 2853 ppb and 8440 ppm, respectively. Spec Type comprised 29% of the samples and associated gold and copper values ranged between 60 and 17740 ppb and 6 and 7980 ppm, and

averaged 4134 ppb and 876 ppm, respectively. Tungsten values were associated with Spec Type and ranged up to 900 ppm where check assaying was carried out.

WRC Type, the primary wall rock indicator of proximity to the mineralized SZS, comprised 8% of the samples. Associated gold and copper values ranged between 30 and 1425 ppb and 481 and 18200 ppm, and average 391 ppb and 3810 ppm, respectively. GAL Type (disseminated galena in oxidized quartz veins) and HW/FW Types were minor components of the samples (3% and 4%, respectively). However, one of the GAL samples returned 480 ppb gold, 3810 ppm copper and 385 ppm silver.

The application of some basic grade parameters is indicative of the relative importance of the mineral types and their distribution along the SZS. For example:

a> If a 1 gram Au/t cut off is used, the resulting 60 samples have average gold and copper contents of 4.52 g/t and 0.94%, respectively. The mineralization type components of this group are: SPEC (40%), M (33%), SM (17%), SMB (8%), and WRC (2%), with 73% of the samples located north of the northernmost Noranda historic drill hole, and 57 % of the samples being located in the Gold Gully-MEXT Zone (GMZ) target area. The mineralization types located in the GMZ target area comprise 56% Spec Type; 15% SM Type; 15% M Type; 12% SMB Type; and, 2 % WRC Type.

b> If a 3 gram Au/t cut off is used, the resulting 37 samples have average gold and copper contents of 6.25 g/t and 1.19%, respectively. The mineralization type components of this group are: M (38%), Spec (35%), SM (24%), and SMB (3%), with 73% of the samples located north of the northernmost Noranda historic drill hole, and 49% of the samples being located in the Gold Gully-MEXT Zone (GMZ) target area. The mineralization types located in the GMZ target area comprise 61% Spec Type; 22% SM Type; 11% M Type; and, 6% SMB Type.

These results, when referenced with the apparent structural fabric and other geological and geochemical parameters, are considered definitive of high priority drill targets. For example, the structural junctions of the Camp Gully, Zinc Gully, Gold Gully, the MEXT Zone (Map 4A) and the NEXT Zone Faults with the SZS (Map 4B) are postulated to be conducive to the development of plunging ore shoot morphologies, similar to those at the Golden Patricia Mine in Northwestern Ontario.

Four Phase 1 drill holes have been proposed and spotted in the GMZ Target Area to evaluate the postulated iron oxide style target associated with the west dipping SZS near the structural junctions:

**DDHMEXT04-01 (Map 4A; VSL 1A; Proposed Length 100 m):**

The hole was proposed to test the SZS in the area of MEXT Fault and MEXT Waterfall where abundant Spec Type talus and some in situ Spec Type mineralization (up to 9.93 g Au/t) can be found at the base of the cliff. The hole is also located in a small valley on the west side of a ridge, which is strewn with mineralized boulders. Those sampled by Geofine averaged 2.37 g Au/t and 0.97% Cu. It is postulated that a glacier scoured the SZS at Gold Gully, about 130 m south of the proposed DDHMEXT04-01, and deposited the angular boulders on the ridge. When a 1 ppm cut off

is applied to the analytical results from the boulders, the resulting grade is 4.18 g Au/t and 1.67% Cu.

**DDHMEXT04-02 (Map 4A; VSL 1A; Proposed Length 80 m):**

The hole is proposed to test the SZS where a prominent area of jarosite/alunite is postulated to be associated with the SZS near the top of the cliff. Three soil samples taken over the gossan have average gold and copper contents of 172 ppb and 751 ppm, respectively. A sample of in situ Spec Type taken on the edge of the cliff returned 2.31 g Au/t and 166 ppm Cu. Four samples of Spec Type collected below the cliff returned up to 5.98 g Au/t.

**DDHMEXT04-03 (Map 4A; VSL 1A; Proposed Length 75 m):**

The hole is proposed to test the SZS near the south end of the aforementioned boulder train referenced with respect to DDHMEXT04-01, or at about 10 m south of the gossan referenced with respect to DDHMEXT04-02. Abundant mineralized (mainly Spec Type), angular talus is located below the cliff on which DDHMEXT04-03 is spotted. Samples contain up to 7.33 g Au/t and 0.23% Cu. A sample of GAL Type (disseminated galena in oxidized quartz veins) returned 480 ppb Au, 0.38% Cu and 385 ppm Ag.

**DDHMEXT04-04 (Map 4A; VSL 1A; Proposed Length 75 m):**

The hole is proposed to test the SZS about 50 m south of DDHMEXT04-03, near the north end of Gold Gully. The Gully is the postulated source of the boulder train referenced under DDHMEXT04-01. Abundant angular, mineralized boulders (mainly Spec, SMB and SM Types) are found at the base of the cliff below the proposed hole. Samples have returned up to 7.74 g Au/t and 3.74% Cu.

**9.1.A.iii. AREA 1. iii) NEXT ZONE (MAPS 4A, B):**

The NEXT Zone is postulated to be the dextrally offset, most northerly, 150 m long segment of the SZS; or, a parallel structure (equivalent to Zone B, South Zone deposit?) before it disappears under the glacial-fluvial deposits of the Todd Creek Valley (Molloy, 1999). The NEXT Zone is located about 170 m north of the MEXT Zone Fault.

The NEXT Zone (Map 4B) is located near the contact with hanging wall mafic pyroclastic rocks - thus apparently not in the same stratigraphic position as the SZD and the MEXT Zone i.e., near the contact of rocks similar to the footwall rocks of the SZD and the MEXT Zone. The hanging wall mafic breccias and agglomerates are moderately to weakly altered (pyrite-quartz-carbonate +/- chlorite, carbonate, epidote stringers, lenses and stockworks) and often include lenses and disseminations of chalcopyrite. The hanging wall rocks are distinctly different than the intensely altered (quartz-pyrite-sericite-carbonate-limonite +/- hematite) hanging wall rocks of the South Zone deposit. South of the NEXT Zone, the intensely altered hanging wall rocks are dextrally offset by the



northwest trending, NEXT Zone Fault (Map 4B). If the position of the SZS remains in the same relative position to the west boundary of the altered pyroclastic rocks at the NEXT Zone, the SZS may be located farther to the east, under the Todd Creek Valley.

The NEXT Zone (Map 4B) is often mineralized with disseminations of fine pyrite and blebby chalcopyrite, and has been traced on surface over about a 100 m strike length, with an apparent width between 3 to 6+ m, a strike of about 10°, and a dip between 50 and 70° to the west. The zone often comprises angular, green-white siliceous fragments up to over 0.5 m; and, varying sizes of quartz-carbonate and red hematite fragments, along with coarse chalcopyrite blebs and fine disseminations of pyrite and chalcopyrite set in an aphanitic, siliceous matrix. Occasional bifurcating quartz-carbonate, and massive sulfide veins and stringers also occur in the zone, some with banded textures indicative of multiphase activity.

No detailed historic work appears to have ever been carried out. The NEXT Zone is intensely silicified, and has flat surfaces that render detailed sampling very difficult (Noranda used a diamond saw on such surfaces on the South Zone deposit). Although considerable effort was made to obtain representative panel samples in 1999, samples could only be taken where irregular surfaces allowed, and may thus not reflect the true potential of the zone.

The mineralization is generally characterized by anomalous to high gold values ranging up to 1.3 g/t; weakly anomalous silver values; anomalous to high copper values ranging up to 1.31%; anomalous lead values; and, highly anomalous arsenic values (Molloy, 1999). Panel sample 160417RP, taken about 50 m west of Todd Creek at the hanging wall contact of the zone, returned interesting gold (600 ppb) and copper (0.79%) values over a 3 m width. A panel sample contiguous, and to the south of 160417RP, returned 1.3 g Au/t and 1.31% Cu over 1 x 5 m. Panel sample 160420RP, taken about 27 m south of 160419RP, contained 755 ppb Au and 0.94% Cu over a 2 m width. Panel sample 160424RP, starting at about 25 m south of 160420RP, and taken over 1.5 x 20 m, in an area where there are few surfaces amenable to sampling, returned 715 ppb Au and 1.39% Cu.

The NEXT Zone (Map 4B) is cut by a recessed mafic dyke just north of sample 160424RP, where 16 contiguous panel samples, each over a meter width, were collected on the east side of the hanging wall. As noted above, the hard rock and flat surfaces are prohibitive to sampling, and any anomalous values should not be overlooked. The first sample, 160401RP taken at the hanging wall, returned 495 ppb Au and 1.14% Cu over 1 m. The next six samples, taken over a total of 6 m all have anomalous Au contents (up to 125 ppb), elevated Cu contents (up to 1290 ppm), and strongly anomalous As contents (up to 556 ppm). The 11th sample, 160411RP returned 0.29% Cu.

One initial diamond drill hole is recommended to evaluate the northern extension of the SZD:

**DDHNEXT04-01 (Map 4B; Section 10700N; Proposed Length of up to 175 m):**

The hole should be spotted about 10 m out into the Todd Creek Valley, with a planned dip of about thirty degrees to intersect the apparent west dipping (50°-70°) NEXT Zone, south of the NEXT

Dyke. The hole would be to some extent chasing the zone down dip.

#### **9.1.A.iv. AREA 2. i) FALL CREEK EAST F1 ZONE (MAP 6; VLS 20500E):**

The Fall Creek Target Area ("FCTA") is located about 4 km north of the NEXT Zone on the south side of the Fall Creek Valley (Map 6). The area is of general interest because the Yellow Bowl Target Area is located south of the FCTA and the Orange Mountain Epithermal Target Area ("OMTA"), including the Amarillo Zone, is located immediately to the north (Maps 2, 2A).

The FCTA and southern part of the OMTA are characterized by numerous quartz-carbonate-chalcopyrite-pyrite +/- hematite, barite, fuchsite multi-phase breccia veins (e.g., Fall Creek East F1 and West Zones, Ice Creek Zone, North A Zone, B Zone). As historic work has indicated, the veins can have significant gold and copper contents.

The East F1 Zone (Map 6) was discovered in 1986 by Noranda as a follow-up of anomalous values returned in a soil survey on the south side of Fall Creek. As shown on Vertical Longitudinal Section 20500E ("VLS 20500E"), Noranda completed four holes totalling 368 m. Significant intersections include:

Hole 88-45: 0.43 g Au/t and 0.041% Cu over 48.7 m  
incl. 6.72 g Au/t and 0.68% Cu over 1.45 m

Hole 88-46: 0.52 g Au/t and 0.058% Cu over 52.25 m  
incl. 12.10 g Au/t and 0.58% Cu over 1.25 m

Hole 88-47: 1.24 g Au/t and 0.39% Cu over 31.5 m  
incl. 3.14 g Au/t and 0.97% Cu over 11 m  
incl. 5.96 g Au/t and 0.50% Cu over 7.9 m  
incl. 24.14 g Au/t and 3.79% Cu over 1 m

Hole 88-48: 1.27 g Au/t and 0.12% Cu over 27.85 m  
Incl. 3.94 g Au/t and 0.31% Cu over 7.90 m  
incl. 4.71 g Au/t and 0.50% Cu over 4.75 m  
incl. 15.22 g Au/t and 1.97% Cu over 1 m

IP and gold soil geochemical anomalies delineate the vein systems of the East and West Zones over a 900 by 450 m area. The East F1 Zone has an apparent strike length of over 800 m and a vertical extent of over 300 m. Noranda tested the zone with diamond drilling over a strike length of 100 m and to a depth of 50 m. Ggeofine proposed a Phase 1, three-hole 2004 diamond drill program comprising 255 m to follow-up the significant mineralization. It should be noted that the holes are located on the steep, south side of the Fall Creek Valley and that some time may be required to find the old collars and establish the new drill pads.

**DDHFCF104-01 (Map 6; Section 20218N; VLS 20500E; Proposed Length: 90 m):**

The hole is proposed as a confirmation hole of the interesting results referenced above for holes 88-47 and 88-48. It would be collared about 18 m behind the historic collars.

**DDHFCF104-02 (Map 6; Section 20303N; VLS 20500E; Proposed Length: 100 m):**

The hole is proposed as a confirmation hole of the interesting results referenced above for holes 88-45 and 88-46. It would be collared about 16 m behind the historic collars.

**DDHFCF104-03 (Map 6, VLS 20500E; Proposed Length: 80 m):**

The hole is proposed to evaluate the F1 Zone approximately midway between Holes 88-45, 46 and 88-47, 48, as the topography permits.

**9.1.A.v. AREA 2. ii) NORTH A ZONE (Maps 7, 7A; Cross Sections 9999E, 10097.5E; VLS 10000N, 10050N):**

The North A Zone is located in the OMTA on the north side of Fall Creek. It was a Newmont discovery and yielded significant results (Baerg, 1989). The zone is described as northwest trending and vertically to steeply west dipping, up to 30 m wide and comprised of 0.1-2 m wide quartz, chalcopyrite, pyrite, hematite and breccia veins. The veins are commonly banded and brecciated and have been traced for 320 m. Trenching results ranged up to 3.8 g Au/t across 14.3 m.

As shown on Vertical Longitudinal Sections 10000N and 10050N (“VLS 10000N” and “VLS 10050N”), Noranda tested the zone with 9 holes and the significant results include:

3.47 g Au/t, 0.75% Cu over 31.85 m  
incl. 14.47 g Au/t, 2.06% Cu over 5.95 m  
2.83 g Au/t, 0.58% Cu over 1.95 m  
3.95 g Au/t, 0.22% Cu over 2.00 m  
3.43 g Au/t, 0.73% Cu over 1.70 m  
6.21 g Au/t, 0.60% Cu over 1.75 m

In 1990, Noranda drilled Hole 90-49 on an IP anomaly located about 85 m south of Fall Creek that appears to represent the along strike extension of the North A Zone. The hole returned anomalous copper, gold and zinc values over a core length of 16.4 m including 3.37 g Au/t and 0.27% Cu over a 2.85 m core length. The intersection and an IP anomaly located 100 m further south suggest the North A Zone has a strike length of at least 500 m. The zone remains open to the southeast and also to the northwest, where Holes 88-43 and 88-44 returned a number of interesting assays including 2.74 g Au/t and 0.41% Cu over 3 m and 2.57 g Au/t over 3 m, respectively.

In 1997, Geofine located the southern extension of the North A Zone, south of Fall Creek. Contiguous chip samples over a 13.5 m width averaged 330 ppb Au and 0.40% Cu, including 3 m averaging 2.16 g Au/t, 8.7 g Ag/t, 1.28% Cu, and 0.15% Zn. A 1 m chip sample from the zone north of Fall Creek returned 44.81 g Au/t and 3.28% Cu. In 1999, the outcrop was re-sampled, with an expanded width and returned 44.18 g Au/t and 3.30% Cu over 2 m. The next outcrop, located about 2 m to the south was evaluated with three contiguous samples that returned 1.58 g Au/t and 1.20% Cu over 2 m; 20.14 g Au/t and 0.48% Cu over 2 m; and 0.63 g Au/t and 0.28% Cu over 2 m.

The Phase 1 2004 diamond drilling activities proposed by Geofine on the North A Zone contemplated the drilling of two holes totalling about 280 m:

**DDHAZ04-01 (Maps 7, 7A; Cross Section 10097.5E; VLS 10050N; Proposed Length 140m):**

The hole is proposed to follow-up the wide intersection (1.51 g Au/t and 0.34% Cu over 16.75 m) in DDH 88-41; the outcrop sample (160505RP) near Trench 5 which returned 44.18 g Au/t and 3.30% Cu over 2 m; and, the Au values in outcrop samples 86091 and 86092, which ranged up to 4.04 g /t. The hole is planned to intersect the A Zone at a vertical depth of about 70 m.

**DDHAZ04-02 (Maps 7, 7A; Cross Section 9999E; VLS 10050N; Proposed Length 140 m):**

The hole is proposed to provide additional information on the strong intersection in DDH88-22:

3.07 g Au/t, 0.64% copper over 36.35 m  
incl. 14.47 g Au/t, 2.06% Cu over 5.95 m

DDH88-23, which was drilled under the zone failed to intersect the strong mineralization, while DDH88-40, drilled from the opposite direction but about 8 m to the east, intersected some weaker mineralization in proximity to the strong zone in DDH88-22; and, stronger mineralization at depth (1.66 g Au/t and 0.06% Cu over 8.9 m). It is conceivable that DDH88-23 went through the veins and stockworks without returning higher values; or, as shown on Cross Section 9999E, that the mineralization is bifurcating; or, that the mineralization dips north and the zones in the lower part of DDH88-40 are new zones.

### **9.1.B. PHASE 1B: 2004 DRILL PROGRAM, TODD CREEK PROPERTY:**

The Phase 1B, 2004 Todd Creek drill program was initiated in the field in June when some grid refurbishing, hole spotting and topographic surveys were carried. This work continued in July and August along with the camp installation, geological mapping, diamond drilling, core logging and sampling, composite talus sampling and reclamation. The work was supervised by David Molloy, P. Geo. (APGO, BCAPEG) and by David Kennedy, P. Geo. (BCAPEG).

The 6 confirmation and step out drill holes are described in Table D1 and comprise about 761m. Five of the holes were initiated on the South Zone deposit (SZD) in the vicinity of the highest-grade Noranda historic holes and one of these (DDHSZD04-02) had to be abandoned in overburden. The NEXT Zone was tested with one hole (DDHNEXT04-01). The lithological units, core samples and selected assays are described in the drill logs (Appendix E). The holes and lithologies are also shown on the individual cross sections included in Appendix C. The penetration points and gram meter products of the 2004 holes and the historic holes are shown on Vertical Longitudinal Section 1 (VLS 1), included in Appendix D.

A total of 372 drill core, check and rock samples were submitted to Chemex Labs in Vancouver and are summarized in Table 3A by sample type and in Table 3B by descriptions of the 3 composite talus samples taken from the MEXT Zone. The Chemex Certificates of Analysis are included in Appendix A.

The program was hindered by on-going mechanical breakdowns experienced by the drill contractor. As a result, only about 60% of the South Zone Target Area drill program (Table S2) was carried out and it required about twice the time originally allocated for the complete program. As a result, the MEXT Zone was not tested, since the drill and camp had been contracted to another project commencing in August.

#### **9.1.B.1. 2004 SECURITY, SAFETY, ENVIRONMENTAL PROTECTION, QUALITY ASSURANCE OF ANALYTICAL DATA (TABLES 4, 5A, 5B, 6, 7), DATA VERIFICATION:**

##### **9.1.B.1.a. SECURITY:**

The 2004 drill program utilized a number of security/confidentiality measures and procedures. The requirement of confidentiality for third party contractors was documented in their service contracts. The exploration camp was located some distance from the main drill camp (Photos 2-5), to ensure privacy and security for the program orchestration, core logging and sampling, communications, and database generation. The core was sealed in core boxes at the drill sites and once delivered to the exploration camp, remained in the care of Geofine.

The core logging and splitting were carried out in the core shack by Geofine personnel and samples placed in labelled and tagged sample bags were immediately secured in rice bags for shipment. The



**TABLE 3A**

**2004 SAMPLE TYPES ANALYZED BY ALS CHEMEX**

| <b>TYPE</b>                  | <b>NO. OF SAMPLES</b> |
|------------------------------|-----------------------|
| <b>ROCK</b>                  | <b>3</b>              |
| <b>DRILL CORE</b>            | <b>303</b>            |
| <b>STANDARD CHECKS</b>       | <b>24</b>             |
| <b>METALLIC SIEVE CHECKS</b> | <b><u>42</u></b>      |
| <b>TOTAL SAMPLES</b>         | <b>372</b>            |

TABLE 3B  
MINERALIZED ROCK SAMPLE DESCRIPTIONS AND SELECTED ANALYTICAL RESULTS


| NUMBER<br>REP. NO.,<br>LOCATION, SIZE                    | NAME, TYPE<br>COMPOSITION                                                                                                                                                                                                                                                                                                                | COLOUR<br>(WEATHERED, FRESH)                                                                           | GRAIN SIZE,<br>TEXTURE                                                                                                    | MINERALIZATION TYPE,<br>ALTERATION, COMMENTS                                                                                                                                                         | SELECTED ANALYTICAL RESULTS |             |             |             |             |             |             |             |
|----------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
|                                                          |                                                                                                                                                                                                                                                                                                                                          |                                                                                                        |                                                                                                                           |                                                                                                                                                                                                      | AU<br>(ppm)                 | AG<br>(ppm) | CD<br>(ppm) | CU<br>(ppm) | PB<br>(ppm) | ZN<br>(ppm) | AS<br>(ppm) | SB<br>(ppm) |
| SAMPLE M<br>AREA AT BASE<br>OF MEXT WATERFALL<br>~ 75 KG | MIN TALUS<br>M TYPE: CO DISSEM OF BLEBBY<br>CPY IN MULTIPHASE QTZ-HEM BX VN<br>60% MATRIX OF QTZ, CHL & BA<br>40% ANG BX FRAGS OF<br>HEM (3%), QTZ (80%), CHL (10%),<br>BLEBBY CPY (8-10%, LOC TO 25%),<br>OXID MAT (2-3%)                                                                                                               | W: GRY BL-BRASSY MET -<br>GRN GRY, MOD LIM, SOME<br>MAL STAIN<br>F: GRY WH - GRN BL-RED<br>BRN-MET GRY | APHANITIC - CO<br>LOC VUGGY,<br>EARTHY<br>WELL BX, BLEBBY                                                                 | M TYPE; WK-MOD OXID OF LIM<br>LOCALLY WELL CHL, SHEARED<br>C/W SLICKS                                                                                                                                | 5.76                        | 1.1         | NA          | 23300       | NA          | NA          | NA          | NA          |
| SAMPLE S<br>AREA AT BASE<br>OF MEXT WATERFALL<br>~ 75 KG | MIN TALUS<br>MULTIPHASE BX VNS C/W FRAGS<br>TO 12 x 8 CM (BA, CHL, QTZ)<br>50-80% MATRIX OF WH<br>QTZ & BA WITH UP TO 5%<br>BLEBS, STRINGERS. STWK OF<br>CHL; 10-45% MASS SPEC<br>SPEC AS VNS, BLEBS, DISS.<br>5% OX MAT (LIM); < 1%<br>HEM AS VNS TO 5 MM;<br>BANDING: HEM TO 0.3 CM,<br>1 CM WH QTZ, SPEC TO 2 CM,<br>OXID MAT TO 2 CM | W:ORGE/BRN - GRY/BLK,<br>SOME MAL STAIN<br>F:GRY MET GRY - WH GRN<br>GRY - RED BRN                     | FI-CO, SUGARY MATRIX;<br>VUGGY, EARTH<br>C/W JAR/AL;<br>MOD STWK; BANDING<br>WELL BX<br>SOME NET TEXT OF<br>QTZ & CO SPEC | WHITE SPEC TYPE (WITH BA & QTZ)<br>10-45% MASS SPEC; WELL BREC.<br>CHL, BX, BA; MOD OXIDIZED (HEM)<br>MULTIPHASE BANDING (QTZ, SPEC,<br>HEM, BA)                                                     | 3.07                        | < 2         | NA          | 262         | NA          | NA          | NA          | NA          |
| 686851<br>AREA AT BASE<br>OF MEXT WATERFALL<br>~ 75 KG   | MIN TALUS<br>MULTIPHASE BX VN C/W VNS,<br>LENSES, MASS, GEN CO SPEC, LOC<br>TO 75% GEN 30-40%, IN GRN-GRY<br>SIL (25%), CHL (35%) MATRIX, OXID<br>MAT (5%, LIM, JAR/AL, MN); MINOR<br>DISSEM CPY AND HEM.                                                                                                                                | W: ORGE/BRN-YEL/BRN-GRN<br>GRY<br>F: GRN/GRY-MET GRY-<br>ORGE/BRN                                      | VUGGY, EARTHY<br>SOME NET TEXTURE<br>OF SPEC VNS IN SIL<br>MATRIX; LOC WELL BX                                            | SEMI MASSIVE SPEC TYPE C/W<br>75% MASSIVE TO SEMI-MASS<br>SPEC HEM; MIN DISSEM CPY,<br>HEM. WELL SIL, CHL MOD OXID,<br>MIN BA.<br>MET GRY TYPE OF SPEC<br>AS OPPOSED TO LOWER<br>GRADE, WH SPEC TYPE | 6.77                        | 0.9         | < 5         | 3090        | 8           | 52          | < 5         | < 5         |



**PHOTO 2:** 2004 TODD CREEK DRILL CAMP: LOOKING WEST AT UPPER AREA OF DRILL CAMP IN FOREGROUND AND LOWER AREA OF DRILL CAMP ACROSS CAMP CREEK BELOW BY GLACIER.



**PHOTO 3:** LOOKING EAST FROM AREA OF LOWER DRILL CAMP (GEOLOGY & CORE PROCESSING) TOWARDS UPPER DRILL CAMP (KITCHEN, DRY, FIRST AID, DRILLERS' & PAD BUILDERS' TENTS).

 AREA OF 2004 DRILL HOLES ON SOUTH ZONE DEPOSIT.





**PHOTO 4: LOOKING SOUTHWEST ON AREA OF RECLAIMED UPPER DRILL CAMP IN FORE GROUND AND AREA OF LOWER DRILL CAMP WITH LUMBER AND HISTORIC NORANDA CORE STORAGE, IN UPPER RIGHT OF PICTURE.**



**PHOTO 5: LOOKING NORTH AT RECLAIMED AREA OF LOWER CAMP AND STORAGE OF 2004 DRILL CORE AND HISTORIC NORANDA DRILL CORE.**



bags were sealed and three colour-coded security tags were fastened to each bag. The bags were shipped to Stewart by Geofine personnel and were stored in a secure Geofine cargo trailer until shipment by Bandstra Transportation to ALS Chemex Labs in Vancouver. The lab was required to verify that the security tags were still in place for each shipping bag when the samples arrived at their facility.

#### **9.1.B.1.b. SAFETY, ENVIRONMENT PROTECTION:**

The program was carried out based on the requirements of the government project permit and the laws and regulations of BC. All project staff were required to have at least Level 1 BC First Aid Certificates. A cook with Level 3 was on site for the duration of the program and a first aid station was maintained in her tent. David Kennedy, P. Geo. and David Molloy, P. Geo. the project geologists, each had Level 1 Certificates with Transportation Endorsement. A helicopter contracted from Prism Helicopters in Stewart remained on-site for most of the program (Photos 6, 7) and three satellite telephones were available for communications. No injuries were sustained during the drill program.

The program was carried out with adherence to the appropriate environmental standards, safeguards and equipment requirements. The campsite was maintained in a clean and natural state with garbage burned in a proper fire pit on a daily basis and non-combustible materials flown to the staging area and shipped to Stewart. Fuel drums were shipped out from the property as emptied and absorbent materials were placed under drums used for tent heating and drill fuel. The drill sites were maintained in a clean and orderly state, with cuttings being contained in sump ponds (Photos 8, 9). The ponds were lined with tarps and sediments were allowed to settle out, with clear water drained off the top of the ponds. After the drill program the ponds were drained and the sludge material removed and buried (Photos 10, 11).

All the drill set-ups were dismantled and the lumber stored with the core at the exploration camp (Photos 3, 4, 5, 11, 12). All drill sites were left in a clean and natural state and no contaminants were discharged in drainage channels (Photos 10, 13-17). The upper and lower camps were dismantled and all garbage and materials removed (Photos 4, 5). The camp floors were moved with the helicopter and stored with the core (Photo 12). Before, during and after photos were taken of most activities and provided to the mining inspector.

#### **9.1.B.1.c. QUALITY ASSURANCE:**

Five CANMET Standards (Tables 4, 5, 5A, 5B) as described below were used to monitor the quality of the Chemex analytical results from the analyses of the drill core. It should be noted that not all CANMET values are certified values. Those provided by other laboratories are so named by CANMET (i.e., provisional and informational) to indicate a lower confidence level relative to certified values.

- a) CANMET Standard MA-1b was used as a "high" gold check and has a certified gold content of 17 g Au/t and an informational value of 4 g Ag/t (Table 4).





**PHOTO 6: LOOKING SOUTHEAST: HUGHES 500D DRILL MOVE TO DDHSZD04-01.**



**PHOTO 7: LOOKING SOUTHEAST: HUGHES 500D DRILL MOVE FROM DDHSZD04-03  
(BELOW HELICOPTER) TO DDHSZD04-04.**





**PHOTO 8:** DDHSZD04-04: LOOKING SOUTHEAST ON DRILL SET-UP AND FOUR SUMP PONDS USED FOR DDHSZD04-01, 02A, 03 AND 04. NOTE CLEAR WATER IN LOWEST POND. TODD CREEK VALLEY IS IN BACK GROUND.



**PHOTO 9:** AREA OF DDHSZD04-04: LOOKING SOUTHWEST AT UPPER SUMP PONDS WITH TARPS IN PLACE.





**PHOTO 10:** LOOKING NORTHWEST ON RECLAIMED DRILL SITE OF DDHSZD04-03 AND ON DRYING TARPS FROM SUMP PONDS SHOWN IN PHOTO 2.



**PHOTO 11:** LOOKING SOUTHWEST AT RECLAIMED SUMP PONDS IN THE VICINITY OF DDHSZD04-04.





**PHOTO 13: LOOKING EAST: DRILL PAD MATERIALS AND 2004 AND HISTORIC CORE STORAGE, LOWER DRILL CAMP.**



**PHOTO 12: LOOKING SOUTHEAST AT TENT FLOORS, LUMBER AND HISTORIC CORE STORAGE, LOWER DRILL CAMP.**





**PHOTO 14:** LOOKING SOUTHEAST: RECLAMATION, DDHSZD04-01.



**PHOTO 15:** LOOKING EAST: RECLAMATION, DDHSZD04-02.





**PHOTO 16: LOOKING SOUTHEAST: RECLAMATION, DDHSZD04-02A.**



**PHOTO 17: LOOKING WEST: RECLAMATION, DDHSZD04-04.**

**TABLE 4:**

**CANMET ANALYTICAL DATA**

**FOR CANMET STANDARDS**

**MA-1b, MA-3a,**

**MA-2c, CH-3, WMG-1**

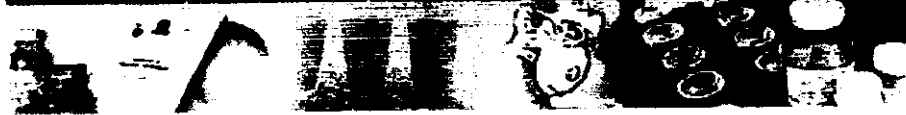


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## MA-1b Gold Ore

### Certified Reference Materials at CANMET-MMSL



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MA-1b was prepared from mill feed from Lac Minerals Limited, Macassa Division, Kirkland Lake, Ontario. MA-1b replaces MA-1a, a gold reference ore prepared from material from the same source, the stock of which is now depleted.

MA-1b is a relatively simple siliceous ore containing elemental gold. It complements MA-2b - a waste-rock grade siliceous material - and MA-3 - a blend of MA-1a and MA-2a. CH-1 and CH-3 are also available as certified gold-bearing reference materials for purposes where a sulphide mineral matrix is more appropriate. CCRMP has also certified PTC-1a and PTM-1a for gold; these are rich in one or more of copper, nickel, and iron, and contain platinum-group metals.

Thirty laboratories provided gold results by one or more of four methods in the certification program for MA-1b.

A certificate of analysis will be issued with each order of MA-1b. A copy of CANMET Report CCRMP 90-2E, "MA-1b: A certified gold reference ore", will be forwarded, free of charge, on request to the Coordinator, CCRMP.

#### Recommended Value and 95% Confidence Interval

| Constituent | oz/ton        | µg/g       |
|-------------|---------------|------------|
| Au          | 0.497 ± 0.008 | 17.0 ± 0.3 |

#### Approximate Chemical Composition

| Constituent | wt % |
|-------------|------|
| Si          | 24.5 |
| Al          | 6.11 |
| Fe          | 4.62 |
| K           | 4.45 |
| Na          | 1.49 |
| S           | 1.17 |

|                           |            |
|---------------------------|------------|
| C (total)                 | 2.44       |
| H <sub>2</sub> O- (100°C) | 0.1        |
| LOI (1000°C)              | 7.9        |
| Ag                        | 4 µg/g     |
| Au                        | 17.0 µg/g* |

\* Certified value

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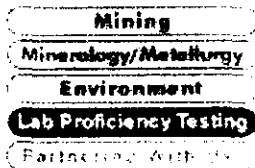
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## MA-3a Gold Ore Reference Material

### Certified Reference Materials at CANMET-MMSL



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CCRMP has replaced reference material MA-3 with a better sample, MA-3a. MA-3 was a blend of ore and "waste rock" material from Lac Minerals Limited, Macassa Division, Kirkland Lake, Ontario. MA-3a is a gold ore sample obtained from the Macassa Division of Barrick Gold Corporation (now Kinross Gold Corporation) from the mine at Kirkland Lake, Ontario.

The product is a compositional reference material having primarily a siliceous matrix and an intermediate gold concentration. It is inferred, from a mineralogical examination of material from the same mine previously used to produce MA-1 and MA-2, that quartz, feldspar, dolomite, muscovite, and chlorite are major mineral constituents in decreasing order of abundance. Pyrite, chalcopyrite, sphalerite, hematite, magnetite, altaite (PbTe), and melonite (NiTe<sub>2</sub>) are present in minor-to-trace levels. Calaverite (AuTe<sub>2</sub>) occurs as inclusions in some pyrite grains. The majority of gold occurs as an electrum (containing silver) dispersed in the gangue minerals.

The material, in the form of 10-cm chunks, was shipped in two 300-kg lots to CANMET for processing.

Each lot was dried and passed through primary and secondary crushers to reduce the size to 1 mm or less.

The resultant samples were milled, in 25-kg batches, in a vibration energy mill, and screened to -200 mesh. MA-3a was blended according to a split-blending protocol, and bottled in 200-g units.

The homogeneity of the stock with respect to its gold content was tested and confirmed at CANMET using bottles chosen according to a stratified random sampling scheme. A fire assay-atomic absorption method using a 20-g sample was employed for these tests.

Thirty-one industrial, commercial, and government laboratories participated in an interlaboratory certification program by providing gold analyses by methods of each laboratory's choice. Methods involving fire assay preconcentration predominated. Several laboratories also provided analyses for many other elements. A statistical analysis of the



data yielded a certified value for gold and information values for twenty-four other constituents. Data for other elements are either inadequate or inconclusive, but are disclosed in the final report.

A CANMET report describing this reference material is in preparation and will be available at no charge upon request to the Coordinator of CCRMP.

#### Certified Value and 95% Confidence Interval

| Constituent | oz/ton  | µg/g |
|-------------|---------|------|
| Au          | 0.250   | 8.56 |
|             | ± 0.003 | 0.09 |

#### Information Values

| Element | Wt % |
|---------|------|
| Al      | 6    |
| Ca      | 5.5  |
| C       | 2.5  |
| Fe      | 5    |
| K       | 4    |
| LOI     | 10   |
| Mg      | 3    |
| Mn      | 0.1  |
| Na      | 1.5  |
| P       | 0.2  |
| S       | 1    |
| Si      | 21   |
| Element | µg/g |
| Ag      | 2.4  |
| As      | 8    |
| Co      | 30   |
| Cu      | 100  |
| Mo      | 55   |
| Ni      | 70   |
| Pb      | 20   |
| Sb      | 3    |
| Sr      | 850  |
| Te      | 12   |
| V       | 80   |
| Zn      | 80   |

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## MA-2c Gold Ore

### Certified Reference Materials at CANMET-MMSL

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First issued: July 2000 Last revision: August 2000

**Table i - Certified and provisional values for gold and silver, respectively.**

| Element                                 | Ag (µg/g)   | Au (µg/g) |
|-----------------------------------------|-------------|-----------|
| Mean                                    | 0.51        | 3.02      |
| Within-laboratory standard deviation    | 0.07        | 0.14      |
| Between-laboratories standard deviation | 0.13        | 0.13      |
| 95% confidence interval                 | 0.10        | 0.06      |
| Status                                  | provisional | Certified |

Informational values are in Table ii on page 4

#### Source

The raw material for MA-2c was donated by Kinross Gold from its operation in Kirkland Lake, Ontario.

#### Description

MA-2c is the fourth generation in a series with predecessors, MA-2, MA-2a and MA-2b, which are no longer available. The deposits of the area are known to contain electrum in a relatively simple siliceous ore.

#### Intended Use

MA-2c is suitable for analysis of gold, silver, majors, minors, and trace elements in gold ores. Examples of intended use are: for quality control in the analysis of samples of a similar type, method development, arbitration and the calibration of equipment.

#### Instructions for Use

The assigned values pertain to the date when issued. CCRMP is not

responsible for changes occurring after receipt by the user. MA-2c should be used "as is". The contents of the bottle should be thoroughly mixed before taking samples.

#### **Method of Preparation**

Both gold ore and waste rock were dried, crushed, ground and sieved to produce a product with a mesh size of less than 75 µm. After blending, the material was bottled in 400-g units. This is the only size available.

#### **State of Homogeneity**

A homogeneity assessment for gold was performed by an independent laboratory on 30 g samples using instrumental neutron activation analysis. Thirty gram samples were analysed for silver using fire assay with lead collection and determination by atomic absorption spectroscopy. No evidence of inhomogeneity was found for gold or silver. A one-way analysis of variance technique (ANOVA) was used to assess the homogeneity of gold and silver (1). The ratio of the between-bottle to within-bottle mean squares was compared to the F statistic at the 95% level of probability. No evidence of inhomogeneity was observed. Use of a smaller sub-sample will invalidate the use of the certified value and associated parameters. Further details are available in the certification report.

#### **Method of Certification**

Twenty industrial, commercial, and government laboratories participated in the 1998 interlaboratory certification program. Gold and silver were analysed by a variety of methods. A statistical analysis of the data yielded Certified Values for gold, and a provisional value for silver. Informational values are derived from the mean of five results from up to six laboratories using one or more of instrumental neutron activation; acid digestion followed by atomic absorption spectroscopy, inductively coupled plasma – atomic emission spectroscopy, or inductively coupled plasma – mass spectrometry; fusion with lithium metaborate followed by x-ray fluorescence, and combustion methods. A one-way analysis of variance technique was used to estimate the consensus value and other statistical parameters (1). Full details of all phases of the work, including statistical analysis, the methods and the names of the participants are contained in CCRMP Report 00-2E.

#### **Legal Notice**

The Canadian Certified Reference Materials Project has prepared this reference material and statistically evaluated the analytical data of the interlaboratory certification program to the best of its ability. The purchaser, by receipt hereof, releases and indemnifies the CANMET from and against all liability and costs arising out of the use of this material and information.

#### **Period of Validity**

These certified values are valid until 2007. The stability of the material will be monitored every seven years. Purchasers will be notified of any significant changes.

#### **Certifying Officers**

Joseph Salley  
Maureen E. Leaver

#### For Further Information

The preparation and certification procedures used for MA-2c, including methods and values obtained by individual laboratories, are given in CCRMP Report 00-2E. This report is available free of charge on application to:

Sales Manager, CCRMP  
CANMET-MMSL (NRCan)  
555 Booth Street  
Ottawa, Ontario, Canada K1A 0G1

Telephone: (613) 995-4738

Facsimile: (613) 943-0573

E-mail

#### Reference

Brownlee, K.A., *Statistical Theory and Methodology in Science and Engineering*; John-Wiley and Sons, Inc.; New York; 1960

**Table ii – Informational values for the mean of up to six sets using a variety of methods.**

| Element | Unit | Mean  | SD   |
|---------|------|-------|------|
| Al      | %    | 6.70  | 0.29 |
| As      | µg/g | 9.10  | 2.32 |
| Ba      | %    | 0.22  | 0.01 |
| Be      | µg/g | 3.74  | 0.48 |
| Bi      | µg/g | 0.66  | 0.05 |
| C       | %    | 1.78  | 0.07 |
| Ca      | %    | 4.76  | 0.05 |
| Cd      | µg/g | 0.7   | 0.1  |
| Ce      | µg/g | 141   | 2    |
| Co      | µg/g | 25    | 2    |
| Cr      | µg/g | 216   | 45   |
| Cs      | µg/g | 9.09  | 0.73 |
| Cu      | µg/g | 95    | 5    |
| Dy      | µg/g | 5.16  | 0.05 |
| Er      | µg/g | 2.26  | 0.02 |
| Eu      | µg/g | 3.15  | 0.15 |
| Fe      | %    | 5.39  | 0.51 |
| Ga      | µg/g | 17.62 | 0.48 |
| Gd      | µg/g | 9.58  | 0.19 |
| Hf      | µg/g | 5.40  | 0.14 |
| Ho      | µg/g | 0.92  | 0.03 |
| K       | %    | 3.20  | 0.06 |
| La      | µg/g | 61.49 | 8.48 |

|     |      |       |      |
|-----|------|-------|------|
| Li  | µg/g | 27.71 | 1.94 |
| Lu  | µg/g | 0.30  | 0.01 |
| Mg  | %    | 2.91  | 0.32 |
| Mn  | %    | 0.10  | 0.01 |
| Mo  | µg/g | 14.3  | 1.4  |
| Na  | %    | 2.23  | 0.08 |
| Nb  | µg/g | 6.52  | 0.13 |
| Nd  | µg/g | 61.9  | 1.2  |
| Ni  | µg/g | 64    | 8    |
| P   | %    | 0.24  | 0.02 |
| Pb  | µg/g | 25    | 4    |
| Pr  | µg/g | 16.26 | 0.20 |
| Rb  | µg/g | 147   | 5    |
| S   | %    | 0.23  | 0.03 |
| Sb  | µg/g | 3.31  | 0.20 |
| Sc  | µg/g | 17.47 | 1.13 |
| Si  | %    | 24.40 | 0.20 |
| Sm  | µg/g | 12.0  | 0.4  |
| Sr  | µg/g | 1471  | 16   |
| Ta  | µg/g | 0.56  | 0.17 |
| Tb  | µg/g | 1.10  | 0.13 |
| Th  | µg/g | 9.2   | 2.6  |
| Ti  | %    | 0.40  | 0.02 |
| Tl  | µg/g | 0.92  | 0.04 |
| Tm  | µg/g | 0.30  | 0.02 |
| U   | µg/g | 2.69  | 0.11 |
| V   | µg/g | 155   | 29   |
| W   | µg/g | 6.02  | 0.63 |
| Y   | µg/g | 24.5  | 1.4  |
| Yb  | µg/g | 2.00  | 0.09 |
| Zn  | µg/g | 93    | 9    |
| Zr  | µg/g | 211   | 38   |
| LOI | %    | 7.55  | 0.04 |

Last Modified: 2004-01-05

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# Certificate of Analysis

## CH-3

Sulphide Matrix Gold-Bearing Reference Material

### RECOMMENDED VALUES

| Constituent           | Ag<br>µg/g | As<br>µg/g | Au<br>µg/g | CaO<br>wt % | Cu<br>wt % | Fe<br>wt % | S<br>wt % | SiO <sub>2</sub><br>wt % | Zn<br>µg/g |
|-----------------------|------------|------------|------------|-------------|------------|------------|-----------|--------------------------|------------|
| Mean                  | 2.63       | 143.       | 1.40       | 6.35        | 0.83       | 12.65      | 2.82      | 40.3                     | 164.       |
| 95% confidence limits | ± 0.20     | ± 14.      | ± 0.03     | ± 0.13      | ± 0.02     | ± 0.25     | ± 0.03    | ± 1.1                    | ± 15.      |

### DESCRIPTION

The source for CH-3 is a gold-bearing material obtained from Westminer Canada Limited from its mine in Chibougamau, Quebec, the same source as CH-2. CH-3 was made by blending raw mill feed and waste-rock material.

The ore-grade sample was found to contain pyrite, pyrrhotite, magnetite, siderite, chloritoid, and chalcopryrite with traces of sphalerite, arsenopyrite, chlorite, quartz, and gold. The main gold-bearing mineral was found to be electrum, which occurred as inclusions in the pyrite and chalcopryrite. The waste-rock sample contained mainly silicate minerals.

The raw mill feed sample, weighing 600 kg, was received in the form of wet 3-cm chips. It was dried, crushed and milled to pass a 74 µm (200 mesh) screen. Approximately 1000 kg of waste rock was received in the form of 30-cm chunks. These chunks were broken, crushed and milled to obtain 450 kg of -74µm product; the oversize was discarded.

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**PROVISIONAL VALUES for CH-3**

| Constituent           | Al <sub>2</sub> O <sub>3</sub><br>wt % | Ba<br>μg/g | C<br>wt % | Co<br>μg/g | Cr<br>μg/g | K <sub>2</sub> O<br>wt % | LOI<br>wt % | MgO<br>wt % | Mn<br>wt % |
|-----------------------|----------------------------------------|------------|-----------|------------|------------|--------------------------|-------------|-------------|------------|
| Mean                  | 16.1                                   | 31.        | 1.74      | 245.       | 35.        | 0.64                     | 6.7         | 4.47        | 0.203      |
| 95% confidence limits | ± 0.5                                  | ± 14.      | ± 0.03    | ± 21.      | ± 16.      | ± 0.04                   | ± 0.6       | ± 0.12      | ± 0.014    |

| Constituent           | Mo<br>μg/g | Na <sub>2</sub> O<br>wt % | Ni<br>μg/g | Sb<br>μg/g | Sr<br>μg/g | Ti<br>wt % |
|-----------------------|------------|---------------------------|------------|------------|------------|------------|
| Mean                  | 2.5        | 1.47                      | 86.        | 0.7        | 49.        | 0.29       |
| 95% confidence limits | ± 2.5      | ± 0.10                    | ± 28.      | ± 1.0      | ± 11.      | ± 0.07     |

**INFORMATIONAL VALUES**

| Constituent           | Bi<br>μg/g | Cd<br>μg/g | Hg<br>μg/g | La<br>μg/g | P <sub>2</sub> O <sub>5</sub><br>wt % | Pb<br>μg/g | Se<br>μg/g | Te<br>μg/g | Zr<br>μg/g |
|-----------------------|------------|------------|------------|------------|---------------------------------------|------------|------------|------------|------------|
| Mean                  | 1.6        | 0.8        | 0.01       | 19.        | 0.06                                  | 2.         | 1.3        | 2.7        | 18.        |
| 95% confidence limits | ± 2.6      | ± 1.0      | ± 0.07     | ± 6.       | ± 0.12                                | ± 3.       | ± 0.9      | ± 0.9      | ± 9.       |
| No. of sets           | 3          | 4          | 2          | 2          | 3                                     | 3          | 3          | 3          | 3          |
| No. of results        | 15         | 20         | 10         | 11         | 15                                    | 15         | 15         | 15         | 13         |

Based on gold assays of test samples, a blend of 227 kg of ore-grade and 295 kg of waste rock was prepared according to a split-blending scheme. The resulting material (CH-3) was bottled in 200-gram units. Each bottle was sealed under nitrogen in a laminated aluminum foil-mylar pouch to prevent oxidation.

The homogeneity of the stock with respect to its gold content was confirmed at CANMET and at a commercial laboratory using bottles chosen according to a stratified random sampling scheme.

### CERTIFICATION

Twenty-five industrial, commercial, and government laboratories participated in an interlaboratory certification program. Up to 56 elements were analyzed by methods of each laboratory's choice. A statistical analysis of the data yielded recommended values for nine constituents and a further fifteen elements had provisional values assigned. The means for nine more elements are given for information. Data for the remaining elements was either inadequate or inconclusive, but will be disclosed in the final report.

### LEGAL NOTICE

The Canadian Certified Reference Materials Project has prepared this reference material and statistically evaluated the analytical data of the inter-laboratory certification program to the best of its ability. The purchaser, by receipt hereof, releases and indemnifies the Canadian Certified Reference Materials Project from and against all liability and costs arising out of the use of this material and information.

### REFERENCE

The preparation and certification procedures used for CH-3 will be given in CANMET report *CCRMP 93-2E* which is in preparation. This report will be made available free of charge on application to:

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CANMET (EMR)  
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Ottawa, Ontario, Canada  
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Phone: (613) 995-4738  
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Telex: 053-3395

(1)

### Raw Data, Means and Standard Deviations for Gold in CH-3

| Gold, #g/g    |       |       |       |       |       |       | Mean | S.D. |
|---------------|-------|-------|-------|-------|-------|-------|------|------|
|               |       |       |       |       |       |       | ---- | ---  |
| CANMET FA-AAS | 1.57  | 1.49  | 1.21  | 1.46  | 1.30  |       | 1.41 | 0.15 |
| LAB- 5 FA-AAS | 1.26  | 1.32  | 1.60  | 1.14  | 1.18  |       | 1.30 | 0.18 |
| LAB- 6 FA-AAS | 1.38  | 1.3   | 1.3   | 1.35  | 1.38  |       | 1.34 | 0.04 |
| LAB- 7 FA-G   | 1.37  | 1.44  | 1.58  | 1.37  | 1.44  |       | 1.44 | 0.09 |
| LAB- 8 FA-AAS | 1.41  | 1.41  | 1.39  | 1.35  | 1.33  |       | 1.38 | 0.04 |
| LAB-10 FA-G   | 1.37  | 1.44  | 1.34  | 1.58  | 1.30  |       | 1.41 | 0.11 |
| LAB-11 AAS    | 1.48  | 1.46  | 1.47  | 1.45  | 1.39  |       | 1.45 | 0.04 |
| LAB-12 INAA   | 1.30  | 1.23  | 1.42  | 1.10  | 1.08  | 1.14  | 1.21 | 0.13 |
| LAB-13 FA-G   | 1.215 | 1.463 | 1.428 | 1.320 | 1.462 | 1.215 | 1.35 | 0.12 |
| LAB-14 FA-G   | 1.44  | 1.58  | 1.51  | 1.44  | 1.51  |       | 1.50 | 0.06 |
| LAB-15 ICP-MS | 0.982 | 1.30  | 1.10  | 0.960 | 1.64  |       | 1.19 | 0.29 |
| LAB-17 FA-G   | 1.37  | 1.41  | 1.44  | 1.37  | 1.44  |       | 1.41 | 0.04 |
| LAB-18 FA-G   | 1.5   | 1.4   | 1.3   | 1.3   | 1.2   |       | 1.34 | 0.11 |
| LAB-19 FA-G   | 1.37  | 1.51  | 1.65  | 1.44  | 1.34  |       | 1.46 | 0.12 |
| LAB-19 FA-AAS | 1.37  | 1.51  | 1.51  | 1.44  | 1.51  |       | 1.47 | 0.06 |
| LAB-20 FA-AAS | 1.43  | 1.35  | 1.46  | 1.36  | 1.30  |       | 1.38 | 0.06 |
| LAB-20 FA-AAS | 1.31  | 1.43  | 1.39  | 1.48  | 1.30  |       | 1.38 | 0.08 |
| LAB-22 FA-G   | 1.43  | 1.47  | 1.47  | 1.43  | 1.57  |       | 1.47 | 0.06 |
| LAB-24 FA-AAS | 1.55  | 1.49  | 1.47  | 1.43  | 1.49  |       | 1.49 | 0.04 |
| LAB-26 FA-ICP | 1.30  | 1.51  | 1.27  | 1.47  | 1.27  |       | 1.36 | 0.12 |
| LAB-28 FA-G   | 1.44  | 1.37  | 1.37  | 1.58  | 1.51  |       | 1.45 | 0.09 |
| LAB-28 FA-G   | 1.37  | 1.47  | 1.41  | 1.37  | 1.47  |       | 1.42 | 0.05 |
| LAB-29 FA-AAS | 1.44  | 1.34  | 1.70  | 1.66  | 1.58  |       | 1.54 | 0.15 |
| LAB-29 FA-AAS | 1.38  | 1.35  | 1.27  | 1.30  | 1.48  | 1.30  | 1.35 | 0.08 |
| LAB-32 FA-G   | 1.58  | 1.47  | 1.47  | 1.51  | 1.47  |       | 1.50 | 0.05 |
| LAB-34 FA-ICP | 1.36  | 1.49  | 1.45  | 1.44  | 1.42  |       | 1.43 | 0.05 |
| LAB-35 FA-AAS | 1.38  | 1.32  | 1.41  | 1.12  | 1.12  |       | 1.27 | 0.14 |
| LAB-39 FA-G   | 1.30  | 1.35  | 1.45  | 1.80  | 1.45  |       | 1.47 | 0.20 |
| LAB-39 FA-AAS | 1.49  | 1.46  | 1.63  | 1.51  | 1.29  |       | 1.48 | 0.12 |

### Raw Data, Means and Standard Deviations for Hafnium in CH-3

| Hafnium, #g/g |    |    |    |    |    |    | Mean | S.D. |
|---------------|----|----|----|----|----|----|------|------|
|               |    |    |    |    |    |    | ---- | ---  |
| LAB-12 INAA   | 1. | 1. | 1. | 1. | 1. | 1. | 1.   | 0.   |

### Raw Data, Means and Standard Deviations for Iridium in CH-3

| Iridium, ng/g |     |     |     |     |     |     | Mean | S.D. |
|---------------|-----|-----|-----|-----|-----|-----|------|------|
|               |     |     |     |     |     |     | ---- | ---  |
| LAB-12 INAA   | <20 | <20 | <20 | <20 | <20 | <20 | ---- | ---- |

STATISTICAL PARAMETERS FOR CH-3

1. RECOMMENDED VALUES

| Constituent              | Ag<br>μg/g | As<br>μg/g | Au<br>μg/g | CaO<br>wt % | Cu<br>wt % | Fe<br>wt % | S<br>wt % | SiO <sub>2</sub><br>wt % | Zn<br>μg/g |
|--------------------------|------------|------------|------------|-------------|------------|------------|-----------|--------------------------|------------|
| Mean                     | 2.63       | 143.       | 1.40       | 6.35        | 0.83       | 12.65      | 2.82      | 40.3                     | 164.       |
| 95% confidence<br>limits | ± 0.20     | ± 14.      | ± 0.03     | ± 0.13      | ± 0.02     | ± 0.25     | ± 0.03    | ± 1.1                    | ± 15.      |
| Av. SD                   | 0.24       | 8.4        | 0.10       | 0.09        | 0.009      | 0.17       | 0.031     | 0.67                     | 9.6        |
| Certif. Crit.            | 2.5        | 2.4        | 0.9        | 2.2         | 2.7        | 2.6        | 1.6       | 2.6                      | 2.6        |
| % rejection              | 0.0        | 9.1        | 0.0        | 8.3         | 6.7        | 10.5       | 0.0       | 0.0                      | 7.7        |
| Within-lab SD            | 0.32       | 8.9        | 0.11       | 0.11        | 0.011      | 0.24       | 0.036     | 1.1                      | 11.0       |
| Between-lab SD           | 0.32       | 19.8       | 0.07       | 0.19        | 0.031      | 0.49       | 0.047     | 1.7                      | 23.        |
| No. of sets              | 14         | 10         | 29         | 11          | 13         | 18         | 11        | 12                       | 12         |
| No. of results           | 71         | 51         | 148        | 53          | 68         | 90         | 57        | 60                       | 57         |





## CCRMP

Canadian Certified Reference Materials Project

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# Certificate of Analysis

First issued: January 1994

Date of this Certificate: September 2004

## WMG-1

Certified Reference Material for a Mineralized Gabbro with Gold and Platinum Group Elements

Table 1 – Certified Values

| Constituent                    | Unit | Mean  | Within-Lab Standard Deviation | Between-Labs Standard Deviation | 95% Confidence Limit |
|--------------------------------|------|-------|-------------------------------|---------------------------------|----------------------|
| Al <sub>2</sub> O <sub>3</sub> | %    | 8.32  | 0.17                          | 0.35                            | ± 0.24               |
| As                             | ug/g | 7     | 1                             | 2                               | ± 1                  |
| Au                             | ng/g | 110   | 23                            | 25                              | ± 11                 |
| Fe <sub>2</sub> O <sub>3</sub> | %    | 17.52 | 0.52                          | 0.43                            | ± 0.29               |
| Ir                             | ng/g | 46.4  | 5.0                           | 7.0                             | ± 4.1                |
| K <sub>2</sub> O               | %    | 0.09  | 0.02                          | 0.03                            | ± 0.02               |
| La                             | ug/g | 8.2   | 0.9                           | 0.9                             | ± 0.7                |
| MnO                            | %    | 0.151 | 0.004                         | 0.008                           | ± 0.005              |
| Na <sub>2</sub> O              | %    | 0.174 | 0.029                         | 0.012                           | ± 0.013              |
| Pd                             | ng/g | 382   | 29                            | 28                              | ± 13                 |
| Pt                             | ng/g | 731   | 45                            | 81                              | ± 35                 |
| Rh                             | ng/g | 26.3  | 3.2                           | 3.5                             | ± 2.0                |
| Ru                             | ng/g | 34.7  | 2.8                           | 7.3                             | ± 5.1                |
| Sb                             | ug/g | 1.8   | 0.2                           | 0.4                             | ± 0.3                |
| Zn                             | ug/g | 110   | 9                             | 17                              | ± 10                 |

## **DESCRIPTION**

The raw material for WMG-1 was obtained from the Wellgreen Complex, Yukon Territory, Canada. WMG-1 was prepared and certified in cooperation with Geological Survey of Canada (GSC). WMG-1 is a mineralized gabbro, which consists largely of pyroxene with prehnite, amphibole, chlorite and accessory magnetite, ilmenite and titanite. Mineralization consists chiefly of chalcopyrite, pyrrhotite, pendlandite, violarite and altaite.

The raw material was dried, crushed, ground, sieved and blended to obtain a minus 74 micron (200 mesh) product. The yield was 76%. The material comes in glass bottles containing 400 g each. This is the only size available. Each bottle was sealed under nitrogen in a laminated aluminum foil-mylar pouch to prevent oxidation.

## **INTENDED USE**

WMG-1 is suitable for the analysis of gold, elements from the platinum group and other elements at major, minor and trace levels. Examples of intended use are for quality control in the analysis of samples of a similar type, method development, arbitration and the calibration of equipment.

## **INSTRUCTIONS FOR THE CORRECT USE OF THE REFERENCE MATERIAL**

The assigned values pertain to the date when issued. WMG-1 should be used "as is", without drying. The contents of the bottle should be thoroughly mixed before taking samples. The contents of the bottle should be exposed to the atmosphere for the shortest possible time. After opening the sealed pouch, the bottle should be kept in a dessicator, or preferably, resealed under nitrogen in a new heat-sealed laminated foil pouch to prevent oxidation.

## **HAZARDOUS SITUATION**

Normal safety precautions such as the use of safety glasses, breathing protection for fine particulate matter, gloves and a laboratory coat are suggested.

## **LEVEL OF HOMOGENEITY**

The homogeneity of the stock with respect to its gold, platinum and palladium was investigated using twenty-two bottles chosen according to the bottling sequence and a stratified random sampling scheme. Two splits were analysed from each bottle. Fire assay preconcentration was performed on a 10g-sample followed by inductively coupled plasma mass spectrometry. The analyses for gold, platinum and palladium were performed at GSC.

A one-way analysis of variance technique (ANOVA) was used to assess the homogeneity of these elements (1). The ratio of the between-bottles to within-bottle mean squares is compared to the F statistic at the 95% level of probability. No

evidence of inhomogeneity was observed for all three elements. Use of a smaller than indicated mass will invalidate the use of the certified value and associated parameters.

## CERTIFIED VALUES AND THEIR UNCERTAINTIES

The first interlaboratory measurement program was held in 1992 for the certification of gold and the platinum group elements. Twelve university, government, industrial and commercial laboratories submitted results. In 1994, thirty-three individual laboratories participated in the interlaboratory measurement program in an attempt to certify other elements. Up to 80 elements were analyzed by methods of each laboratory's choice. For gold and the platinum group elements, fire assay, multi-acid digestion followed by solvent extraction, gravimetric, inductively coupled plasma –optical emission spectroscopy, inductively coupled plasma – mass spectroscopy, graphite furnace atomic absorption spectroscopy, direct current plasma spectroscopy, and neutron activation analysis were used. For the other elements, various acid digestions, fusions, gravimetric, combustion, x-ray fluorescence, hydride generation, inductively coupled plasma – optical emission spectroscopy, inductively coupled plasma – mass spectroscopy, graphite furnace atomic absorption spectroscopy, direct current plasma spectroscopy, and neutron activation analysis were used.

A one-way analysis of variance technique (ANOVA) was used to estimate the consensus value and other statistical parameters (1). The two criteria for certification involve the agreement of within- and between-laboratories standard deviations and the number of sets with acceptable agreement. Table 1 contains the means and associated statistical parameters for the fifteen certified elements. Full details of all phases of the work, including statistical analysis, the methods and the names of the participants are contained in the certification report.

## UNCERTIFIED VALUES

Table 2 contains the provisional elements which did not meet either one or both of the two criteria for certification. Table 3 contains the informational values calculated from the mean of two or more sets of results which were considered to be in good agreement.

**Table 2 - Provisional Values**

| Constituent | Unit | Mean | Within-Lab Standard Deviation | Between-Labs Standard Deviation | 95% Confidence Limit |
|-------------|------|------|-------------------------------|---------------------------------|----------------------|
| Ag          | ug/g | 2.7  | 0.2                           | 0.4                             | ± 0.3                |
| Ba          | ug/g | 114  | 8                             | 12                              | ± 8                  |
| Be          | ug/g | 0.6  | 0.2                           | 0.4                             | ± 0.5                |
| CaO         | %    | 15.0 | 0.4                           | 1.2                             | ± 0.8                |

WMG-1 Provisional Values (Cont.)

| Constituent                   | Unit | Mean  | Within-Lab Standard Deviation | Between-Labs Standard Deviation | 95% confidence limit |
|-------------------------------|------|-------|-------------------------------|---------------------------------|----------------------|
| Cd                            | ug/g | 1.1   | 0.1                           | 0.5                             | ± 0.5                |
| Ce                            | ug/g | 16    | 3                             | 4                               | ± 3                  |
| Co                            | ug/g | 200   | 7                             | 21                              | ± 12                 |
| Cr                            | %    | 0.077 | 0.002                         | 0.008                           | ± 0.005              |
| Cs                            | ug/g | 0.48  | 0.08                          | 0.05                            | ± 0.08               |
| Cu                            | %    | 0.59  | 0.01                          | 0.05                            | ± 0.03               |
| Dy                            | ug/g | 2.8   | 0.2                           | 0.6                             | ± 0.8                |
| Eu                            | ug/g | 0.8   | 0.1                           | 0.1                             | ± 0.1                |
| Ga                            | ug/g | 10.3  | 0.9                           | 1.6                             | ± 1.5                |
| Hf                            | ug/g | 1.3   | 0.1                           | 0.3                             | ± 0.2                |
| Ho                            | ug/g | 0.5   | 0.05                          | 0.1                             | ± 0.1                |
| Li                            | ug/g | 35    | 3                             | 6                               | ± 5                  |
| Lu                            | ug/g | 0.21  | 0.03                          | 0.06                            | ± 0.06               |
| MgO                           | %    | 11.86 | 0.19                          | 0.39                            | ± 0.28               |
| LOI                           | %    | 4.0   | 0.1                           | 0.7                             | ± 0.9                |
| Mo                            | ug/g | 1.4   | 0.2                           | 0.4                             | ± 0.4                |
| Nb                            | ug/g | 6     | 1                             | 1                               | ± 1                  |
| Nd                            | ug/g | 9.0   | 0.6                           | 0.5                             | ± 0.7                |
| Ni                            | %    | 0.27  | 0.006                         | 0.03                            | ± 0.02               |
| Os                            | ng/g | 24.1  | 1.7                           | 3.2                             | ± 3.5                |
| P <sub>2</sub> O <sub>5</sub> | %    | 0.13  | 0.01                          | 0.03                            | ± 0.03               |
| Pb                            | ug/g | 15    | 2                             | 10                              | ± 10                 |
| Rb                            | ug/g | 4     | 0.6                           | 3                               | ± 3                  |
| S                             | %    | 3.7   | 0.2                           | 0.2                             | ± 0.2                |
| Sc                            | ug/g | 26    | 1                             | 4                               | ± 2                  |
| Se                            | ug/g | 15    | 2                             | 3                               | ± 3                  |
| SiO <sub>2</sub>              | %    | 40.3  | 0.4                           | 0.6                             | ± 0.6                |



**WMG-1 Provisional Values (Cont.)**

| Constituent      | Unit | Mean | Within-Lab Standard Deviation | Between-Labs Standard Deviation | 95% confidence limit |
|------------------|------|------|-------------------------------|---------------------------------|----------------------|
| Sm               | ug/g | 2.3  | 0.1                           | 0.1                             | ± 0.1                |
| Sn               | ug/g | 2.2  | 0.3                           | 0.3                             | ± 0.5                |
| Sr               | ug/g | 41   | 1.7                           | 4.6                             | ± 4                  |
| Ta               | ug/g | 0.5  | 0.1                           | 0.3                             | ± 0.3                |
| Tb               | ug/g | 0.4  | 0.06                          | 0.1                             | ± 0.1                |
| Te               | ug/g | 1.3  | 0.3                           | 0.6                             | ± 0.8                |
| Th               | ug/g | 1.1  | 0.09                          | 0.10                            | ± 0.1                |
| TiO <sub>2</sub> | %    | 0.68 | 0.02                          | 0.07                            | ± 0.05               |
| Tm               | ug/g | 0.2  | 0.03                          | 0.07                            | ± 0.1                |
| U                | ug/g | 0.65 | 0.10                          | 0.18                            | ± 0.17               |
| V                | ug/g | 149  | 4                             | 66                              | ± 43                 |
| W                | ug/g | 1.3  | 0.8                           | 0.2                             | ± 0.6                |
| Y                | ug/g | 12   | 1                             | 5                               | ± 4                  |
| Yb               | ug/g | 1.3  | 0.1                           | 0.2                             | ± 0.2                |
| Zr               | ug/g | 43   | 3                             | 9                               | ± 8                  |

**Table 3 - Informational Values**

| Constituent     | Unit | Range     |
|-----------------|------|-----------|
| B               | ug/g | 20-650    |
| Bi              | ug/g | 0.2-30    |
| Cl              | ug/g | 100-200   |
| Er              | ug/g | 1.0-1.7   |
| Gd              | ug/g | 1.8-3.1   |
| Ge              | ug/g | 0.1-4     |
| In              | ug/g | 0.1-0.2   |
| Pr              | ug/g | 2.1-2.4   |
| SO <sub>3</sub> | %    | 0.24-0.45 |
| Tl              | ug/g | 0.08-0.24 |

## **TRACEABILITY**

The certified values quoted herein are based on the consensus value derived from the statistical analysis of the data from the interlaboratory measurement program.

## **DATE OF CERTIFICATION**

WMG-1 was released in 1994. This 2004 version of this certificate was written in order to release new or upgraded values. This version of the certificate includes nine new certified values, forty-six new provisional values and ten new informational values.

## **PERIOD OF VALIDITY**

These certified values are valid until 2009. The stability of the material will be monitored every two years. Purchasers will be notified of any significant changes.

## **LEGAL NOTICE**

CANMET - Mining and Mineral Sciences Laboratories (MMSL) has prepared this reference material and statistically evaluated the analytical data of the interlaboratory certification program to the best of its ability. The purchaser, by receipt hereof, releases and indemnifies CANMET - MMSL from and against all liability and costs arising out of the use of this material and information.

## **CERTIFYING OFFICER**



Maureen E. Leaver

## **FOR FURTHER INFORMATION**

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## **REFERENCE**

1. Brownlee, K.A., Statistical Theory and Methodology in Science and Engineering; John-Wiley and Sons, Inc.; New York; 1960



TABLE 5

**ANALYTICAL QUALITY ASSURANCE FOR CANMET STANDARDS  
DDH CHECK SAMPLES SORTED BY TYPE & DATE**

| 2004 CERT.<br>DATE | DRILL HOLE                                       | SAMPLE NO. | TYPE  | Au ppm       | Ag ppm | As ppm | Cd ppm | Cu ppm | Pb ppm | Sb ppm | Zn ppm |
|--------------------|--------------------------------------------------|------------|-------|--------------|--------|--------|--------|--------|--------|--------|--------|
| 12-Aug             | DDHSZD04-01                                      | 599584     | MA-2c | 2.75         |        |        |        |        |        |        |        |
| 19-Aug             | DDHSZD04-03                                      | 599654     | MA-2c | 3.09         | 0.7    |        | 11     | <.5    | 98     | 37     | <5     |
| 30-Aug             | DDHSZD04-02A                                     | 609761     | MA-2c | 3.28         | <.5    |        | 7      | <.5    | 102    | 28     | 9      |
|                    | <b>CANMET CERTIFIED VALUE:</b>                   |            |       | <b>3.02</b>  |        |        |        |        |        |        |        |
|                    | <b>CANMET PROVISIONAL VALUE:</b>                 |            |       |              | 0.51   |        |        |        |        |        |        |
|                    | <b>CANMET INFORMATIONAL VALUE:</b>               |            |       |              |        |        | 9.1    | 0.7    | 95     | 25     | 3.31   |
|                    | CHEMEX AVERAGE VALUE:                            |            |       | 3.04         |        |        |        |        |        |        | 93     |
|                    | CHEMEX AVERAGE VALUE<br>AS % OF CERTIFIED VALUE: |            |       | 100.66%      |        |        |        |        |        |        |        |
| 2004 CERT.<br>DATE | DRILL HOLE                                       | SAMPLE NO. | TYPE  | Au ppm       | Ag ppm | As ppm | Cd ppm | Cu ppm | Pb ppm | Sb ppm | Zn ppm |
| 12-Aug             | DDHNEXT04-01                                     | 609130     | CH3   | 1.17         |        |        |        |        |        |        |        |
| 12-Aug             | DDHNEXT04-01                                     | 609175     | CH3   | 1.31         | 2.4    |        | 164    | <.5    | 9060   | 5      | <5     |
| 19-Aug             | DDHSZD04-03                                      | 599671     | CH3   | 1.26         | 2.7    |        | 159    | 1.2    | 8530   | 15     | <5     |
| 25-Aug             | DDHSZD04-03                                      | 599653A    | CH3   | 1.32         | 5.1    |        | 156    | <.5    | 8480   | 2      | <5     |
| 27-Aug             | DDHNEXT04-01                                     | 609200     | CH3   | 1.66         | 2.8    |        | 142    | <.5    | 8950   | 6      | 5      |
| 27-Aug             | DDHNEXT04-01                                     | 599567A    | CH3   | 1.79         | 2.3    |        | 150    | <.5    | 8570   | 12     | <5     |
| 30-Aug             | DDHSZD04-04                                      | 609201     | CH3   | 1.19         | 3.6    |        | 150    | <.5    | 8240   | 6      | <5     |
| 30-Aug             | DDHSZD04-02A                                     | 609245     | CH3   | 1.48         | 3.2    |        | 106    | <.5    | 8820   | 6      | <5     |
| 30-Aug             | DDHSZD04-04                                      | 609228A    | CH3   | 1.46         | 2.7    |        | 114    | <.5    | 8580   | 10     | 10     |
|                    | <b>CANMET CERTIFIED VALUE:</b>                   |            |       | <b>1.40</b>  |        |        |        |        |        |        |        |
|                    | <b>CANMET PROVISIONAL VALUE:</b>                 |            |       |              | 2.63   |        |        |        |        |        |        |
|                    | <b>CANMET INFORMATIONAL VALUE:</b>               |            |       |              |        |        | 143    | 8300   |        |        | 164    |
|                    | CHEMEX AVERAGE VALUE:                            |            |       | 1.40         |        |        |        |        |        |        |        |
|                    | CHEMEX AVERAGE VALUE<br>AS % OF CERTIFIED VALUE: |            |       | 100%         |        |        |        |        |        |        |        |
| 2004 CERT.<br>DATE | DRILL HOLE                                       | SAMPLE NO. | TYPE  | Au ppm       | Ag ppm | As ppm | Cd ppm | Cu ppm | Pb ppm | Sb ppm | Zn ppm |
| 12-Aug             | DDHSZD04-01                                      | 599600     | MA-1b | 15.80        |        |        |        |        |        |        |        |
| 12-Aug             | DDHSZD04-01                                      | 599615     | MA-1b | 16.25        |        |        |        |        |        |        |        |
| 12-Aug             | DDHNEXT04-01                                     | 609101     | MA-1b | 21.40        | 2.7    |        | <5     | <.5    | 96     | 226    | <5     |
|                    | <b>CANMET CERTIFIED VALUE:</b>                   |            | MA-1b | <b>17.00</b> |        |        |        |        |        |        |        |
|                    | <b>CANMET PROVISIONAL VALUE:</b>                 |            | MA-1b |              |        |        |        |        |        |        |        |
|                    | <b>CANMET INFORMATIONAL VALUE:</b>               |            | MA-1b |              |        | 4      |        |        |        |        |        |
|                    | CHEMEX AVERAGE VALUE:                            |            |       | 17.82        |        |        |        |        |        |        |        |
|                    | CHEMEX AVERAGE VALUE<br>AS % OF CERTIFIED VALUE: |            |       | 104.82%      |        |        |        |        |        |        |        |



- b) CANMET Standard MA-3a was used as a "moderate" gold check and has a certified content of 8.56 g Au/t (Table 4). Other analytical values for MA-3a referenced are informational (Table 4).
- c) CANMET Standard MA-2c was used as a "moderate-low" gold check and has a CANMET certified gold content of 3.02 g/t and a provisional silver value of 0.51 g/t. Other analytical values for MA-2c referenced in Tables 4 and 5 are informational.
- d) CANMET Standard CH-3 was used as a "low" gold check and has a CANMET certified content of 1400 ppb gold (Table 4). Other analytical values for CH-3 shown in Tables 4 and 5 are informational.
- e) CANMET Standard, WGM-1, that is used as a "anomalous" gold check and that has a CANMET certified content of 110 ppb gold (Table 4); other values for WGM-1 are now available as certified, provisional and informational values (Table 4).

Selected Chemex analytical results for each of the CANMET standards submitted during the Todd drill program are shown in Table 5 relative to the analytical values referenced above and reported by CANMET. The Chemex Certificates and their issue dates are also referenced in Table 5 in order to ascertain any apparent trends over time in deviations from the certified values. The complete analytical results for each standard sample are shown on the Chemex Certificates included in Appendix A, along with the samples they were submitted with. In addition to the utilization of the standards, a number of the pulps were re-run at Chemex and some additional pulps were prepared for metallic sieving, which was carried out on the samples from highest grade core.

Based on the results referenced above, and on the use of some of the same standards in the 1999 and 2000 Todd Creek programs and issues that were then resolved (Molloy, 1999, 2000), it is concluded that:

- i> Most Chemex gold analytical results for the standards relative to the CANMET values fall within the range of acceptable statistical variance (Table 5). The variability in some of the gold results probably relates to the difficulty in maintaining the homogeneous concentration of it in the standards. There is one large discrepancy with regard to one of the silver values: 5.1 ppm in sample 599653A relative to the CH-3 standard silver value of 2.63 PPM (Table 5). This may again relate to a homogeneity issue.
- ii> There is some evidence of the Chemex downward biases experienced by Geofine in 1999 and 2000 (Molloy 1999, 2000) regarding some of the Chemex 2004 zinc values i.e., with respect to standard CH-3 (Table 5). Historically, this was interpreted as probably reflective of the Chemex ICP digestion method. There is also evidence of an upward bias with respect to most of the Chemex 2004 copper values relative to the CANMET values (Table 5).

Chemex was asked to review these matters and the results of their investigation are included below (Chemex 2004):

*The answer is not easy as to why. It is not easy as to why the Chemex copper values are slightly higher than the standard value. The copper values you are receiving are generally within our method specification but are slightly higher within that specification. It is not easy to come up with one answer, as it can be a series of factors contributing to it:*

*1. The standard value for Cu is an informational value. When they make the standard they produce it in batches or lots. They certify certain elements to be within a certain range between these lots and other elements like your Cu are just informational values. This means that between lots and between the bottle of standards you are using the mean value of the Cu may not be the same. For example MA-3a has a informational value of 100 ppm copper but over the production of this standard the value of each lot may vary. For "lot A" it may have a mean of 90 ppm and "lot B" a mean of 110 ppm. So one bottle of standard may have a mean value of 110 ppm Cu even though the informational value says 100 ppm.*

*2. Have the standards that you are using been rolled? We have found that if the standards sit for too long of a time, either at our facility or maybe the company we bought them from had them sitting for too long the material will settle. You will get low values as you start using the standard and as you use the bottom of the standard bottle the values will increase. Certain elements will settle faster than other elements as well. As well the material that is taken from the standard bottle should be taken from the middle not just scooped off the top. All of this can contribute to the slight bias.*

*3. The method of the procedure may also contribute to this. The method ME-ICP61 is a Geochem method and is not as precise as say an AA method when you are only running one element at a time. It consist of running 40 elements all at the same time and trying to keep all elements in specification throughout the 1ppm to 10000 ppm range, It is a tight balancing act. So for Cu we maybe running slightly high at the 100-ppm range but also slightly low at the 200-ppm range and right on at the 500-ppm range, again all are within our method specifications. We have to try keeping all 40 elements within this specifications and adjusting for one element to be increased may affect another element to be suppressed. There are a lot of factors within the method that may account for this from calibration solutions to digestion procedures. Maybe another element of this particular standard causes a slight interference with another element on the ICP instrument.*

*It is not easy to come up with one single answer for you as I say it maybe a little bit of everything.*

When asked why are most of the Chemex copper values higher than the standard values, relative to them having a range of values both above and below the standard value, Chemex indicated:

*Yes we contribute the slight bias to the method specifications. In general we have made some improvements to our ME-ICP61 method this year and this is probably why you have seen a shift in your standards from slightly below the mean to slightly above.*

- iii> In spite of the apparent reliability of the Chemex gold results relative to the standards, a number of concerns arose with regard to some of the Chemex gold results relative to mineralization intersected in the holes i.e., some analytical results were expected to be higher based on the amount of auriferous chalcopyrite (Tables 5B, 5C). As a result of the re-assaying, the Chemex Assay Certificates were revised as described below:
  - a) As shown in Table 5A, an investigation of the original Chemex results for samples 609756 and 609757 from hole SZD04-02A determined that they had been reversed.
  - b) The results for samples 609769 and 609770 from DDHSZD04-02A had also been reversed (Table 5A).
  - c) The re-analysis of sample 599606 in DDHSZD04-01 indicated the original value (0.005 ppm) was incorrect and should have been 2.58 g Au/t (see Section iv, below).
- iv> In view of the apparent nugget affect observed in previous years with regard to the blebby, auriferous chalcopyrite mineralization, 41 samples from the mineralized zones intersected in the drill holes were re-run with metallic sieving. The total gold values obtained via the metallic sieving process are compared in Table 5B with the original (unscreened) values from the Chemex Certificates attached to this report in Appendix A. There is generally very good correspondence between the two sets of values and it is concluded that at least for these samples, the overall nugget affect is minor. As shown on Chemex Certificate VA04062620 (part of Table 5B), the plus size fraction of the sieved material can have a significant gold content. However, the weight of the plus fraction relative to the weight of the overall sample is generally so small in the samples analyzed that the grade of the plus fraction has little affect on the overall grade.
- v> Based on the aforementioned quality assurance work, most of the Chemex final analytical results, including the corrections referenced above fall within the range of acceptable statistical variance. It is concluded that the results as reported herein are considered very reliable and that such quality assurance work is a very essential part of any exploration program.

**TABLE 5A**  
**CORRECTED SAMPLE ANALYSES FROM ALS CHEMEX**

| ISSUE NO. | SAMPLE DESCRIP | Au-AA23          | Au-GRA2 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | CERT. NUMBER | CERT. DATE |
|-----------|----------------|------------------|---------|----------|----------|----------|----------|----------|----------|--------------|------------|
|           |                | Au ppm           | Ag ppm  | As ppm   | Cd ppm   | Cu ppm   | Pb ppm   | Sb ppm   | Zn ppm   |              |            |
| 1         |                | ORIGINAL VALUES  |         |          |          |          |          |          |          |              |            |
|           | 609756         | 0.18             | <0.5    | 13       | <0.5     | 378      | 4        | 6        | 10       | VA04054017   | 30-Aug-04  |
|           | 609757         | 1.685            | <0.5    | 21       | <0.5     | 2260     | 3        | 6        | 15       | VA04054017   | 30-Aug-04  |
|           |                | CORRECTED VALUES |         |          |          |          |          |          |          |              |            |
|           | 609756         | 1.685            | <0.5    | 21       | <0.5     | 2260     | 3        | 6        | 15       | VA04054017   | 30-Aug-04  |
|           | 609757         | 0.18             | <0.5    | 13       | <0.5     | 378      | 4        | 6        | 10       | VA04054017   | 30-Aug-04  |
| 2         |                | ORIGINAL VALUES  |         |          |          |          |          |          |          |              |            |
|           | 609769         | 0.09             | <0.5    | <5       | <0.5     | 486      | 5        | 7        | 28       | VA04054017   | 30-Aug-04  |
|           | 609770         | 0.418            | <0.5    | <5       | <0.5     | 2180     | 3        | <5       | 19       | VA04054017   | 30-Aug-04  |
|           |                | CORRECTED VALUES |         |          |          |          |          |          |          |              |            |
|           | 609769         | 0.418            | <0.5    | <5       | <0.5     | 2180     | 3        | <5       | 19       | VA04054017   | 30-Aug-04  |
|           | 609770         | 0.09             | <0.5    | <5       | <0.5     | 486      | 5        | 7        | 28       | VA04054017   | 30-Aug-04  |
| 3         | 599606         | ORIGINAL VALUES  |         |          |          |          |          |          |          |              |            |
|           |                | 0.005            | 0.6     | 19       | 0.6      | 1770     | 7        | <5       | 18       | VA04049586   | 12-Aug-04  |
|           |                | CORRECTED VALUES |         |          |          |          |          |          |          |              |            |
|           | 599606         | 2.58             | 0.6     | 19       | 0.6      | 1770     | 7        | <5       | 18       | VA04049586   | 12-Aug-04  |



| TABLE 5B                                                              |  |                                 |            |             |        |           |
|-----------------------------------------------------------------------|--|---------------------------------|------------|-------------|--------|-----------|
| COMPARISON OF SCREENED & UNSCREENED<br>FA-AA ANALYTICAL RESULTS       |  |                                 |            |             |        |           |
| * Certificate reissued by ALS Chemex with revised analyses (Table 5B) |  |                                 |            |             |        |           |
|                                                                       |  | SCREENED                        | UNSCREENED | CERTIFICATE | HOLE   |           |
|                                                                       |  | CERT. VA04062620                |            | NUMBER      | NUMBER |           |
| SAMPLE<br>NUMBER                                                      |  | Au Total (+)(-) Combined<br>ppm | Au ppm     |             |        |           |
| 599601                                                                |  | 2.16                            | 3.51       | *VA04049586 |        | SZD04-01  |
| 599602                                                                |  | 0.05                            | 0.061      | *VA04049586 |        | SZD04-01  |
| 599603                                                                |  | <0.05                           | 0.035      | *VA04049586 |        | SZD04-01  |
| 599604                                                                |  | 0.13                            | 0.152      | *VA04049586 |        | SZD04-01  |
| 599605                                                                |  | 1.28                            | 1.295      | *VA04049586 |        | SZD04-01  |
| 599606                                                                |  | 2.72                            | 2.58       | *VA04049586 |        | SZD04-01  |
| 599635                                                                |  | 0.25                            | 0.305      | VA04054018  |        | SZD04-03  |
| 599636                                                                |  | 0.17                            | 0.175      | VA04054018  |        | SZD04-03  |
| 599656                                                                |  | 0.08                            | 0.068      | VA04052342  |        | SZD04-03  |
| 599661                                                                |  | <0.05                           | 0.033      | VA04052342  |        | SZD04-03  |
| 599662                                                                |  | 8.32                            | 8.55       | VA04052342  |        | SZD04-03  |
| 599670                                                                |  | 0.49                            | 0.541      | VA04052342  |        | SZD04-03  |
| 609144                                                                |  | <0.05                           | 0.063      | VA04049585  |        | NEXT04-01 |
| 609146                                                                |  | 0.29                            | 0.337      | VA04049585  |        | NEXT04-01 |
| 609147                                                                |  | 0.45                            | 0.477      | VA04049585  |        | NEXT04-01 |
| 609148                                                                |  | 4.55                            | 4.44       | VA04049585  |        | NEXT04-01 |
| 609149                                                                |  | 3.57                            | 3.8        | VA04049585  |        | NEXT04-01 |
| 609151                                                                |  | 1.43                            | 1.55       | VA04049585  |        | NEXT04-01 |
| 609226                                                                |  | 10.2                            | 9.83       | VA04053799  |        | SZD04-04  |
| 609227                                                                |  | 10.8                            | 11.1       | VA04053799  |        | SZD04-04  |
| 609228                                                                |  | 0.17                            | 0.172      | VA04053799  |        | SZD04-04  |
| 609230                                                                |  | 0.27                            | 0.285      | VA04053799  |        | SZD04-04  |
| 609231                                                                |  | 1.07                            | 1.045      | VA04053799  |        | SZD04-04  |
| 609232                                                                |  | 0.11                            | 0.08       | VA04053799  |        | SZD04-04  |
| 609233                                                                |  | 4.2                             | 4.15       | VA04053799  |        | SZD04-04  |
| 609234                                                                |  | 0.28                            | 0.258      | VA04053799  |        | SZD04-04  |
| 609235                                                                |  | 1.85                            | 1.985      | VA04053799  |        | SZD04-04  |
| 609237                                                                |  | 0.05                            | 0.052      | VA04053799  |        | SZD04-04  |
| 609238                                                                |  | 0.13                            | 0.113      | VA04053799  |        | SZD04-04  |
| 609751                                                                |  | 1.71                            | 1.74       | *VA04054017 |        | SZD04-02A |
| 609752                                                                |  | 0.38                            | 0.358      | *VA04054017 |        | SZD04-02A |
| 609753                                                                |  | 0.09                            | 0.091      | *VA04054017 |        | SZD04-02A |
| 609754                                                                |  | 10.05                           | 10.2       | *VA04054017 |        | SZD04-02A |
| 609755                                                                |  | 2.62                            | 2.92       | *VA04054017 |        | SZD04-02A |
| 609756                                                                |  | 1.23                            | 1.685      | *VA04054017 |        | SZD04-02A |
| 609757                                                                |  | 0.17                            | 0.18       | *VA04054017 |        | SZD04-02A |
| 609765                                                                |  | 3.51                            | 3.5        | *VA04054017 |        | SZD04-02A |
| 609767                                                                |  | 0.43                            | 0.487      | *VA04054017 |        | SZD04-02A |
| 609768                                                                |  | 0.16                            | 0.249      | *VA04054017 |        | SZD04-02A |
| 609769                                                                |  | 0.45                            | 0.418      | *VA04054017 |        | SZD04-02A |
| 609770                                                                |  | 0.09                            | 0.09       | *VA04054017 |        | SZD04-02A |



**ALS Chemex**  
**EXCELLENCE IN ANALYTICAL CHEMISTRY**  
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North Vancouver BC V7J 2C1 Canada  
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To: GEOFINE EXPLORATION CONSULTANTS LTD.  
49 NORMANDALE RD  
UNIONVILLE ON L3R 4J8

Page  
Finalized Date: 26-SEP-2004  
Account:

**CERTIFICATE VA04062620**

Project: Stewart  
P.O. No.:  
This report is for 42 Other samples submitted to our lab in Vancouver, BC, Canada on 15-SEP-2004.  
The following have access to data associated with this certificate:  
DAVID MOLLOY

**SAMPLE PREPARATION**

| ALS CODE | DESCRIPTION                    |
|----------|--------------------------------|
| FND-03   | Find Reject for Addn Analysis  |
| SCR-21   | Screen to -100 um              |
| SPL-21   | Split sample - riffle splitter |
| PUL-32   | Pulverize 1000g to 85% < 75 um |
| BAG-01   | Bulk Master for Storage        |

**ANALYTICAL PROCEDURES**

| ALS CODE | DESCRIPTION                   | INSTRUMENT |
|----------|-------------------------------|------------|
| Au-SCRa  | Au Screen FA - Over Wt. A     | WST-SIM    |
| Au-SCR21 | Au Screen Fire Assay - 100 um | WST-SIM    |
| Au-AA25  | Ore Grade Au 30g FA AA finish | AAS        |
| Au-AA25D | Ore Grade Au 30g FA AA Dup    | AAS        |

To: GEOFINE EXPLORATION CONSULTANTS LTD.  
ATTN: DAVID MOLLOY  
49 NORMANDALE RD  
UNIONVILLE ON L3R 4J8

This is the Final Report and supersedes any preliminary report with this certificate number. Results apply to samples as submitted. All pages of this report have been checked and approved for release.

Signature: 



#### **9.1.B.1.d. DATA VERIFICATION:**

On-going data verification was carried out related to both technical and financial information. David Kennedy P. Geo., and David Molloy, P. Geo were responsible for the data verification. Procedures related to the technical data included ensuring the correct drill set up location and elevation and verifying the drill head inclination and checking the setting a number of times during the drilling of each hole.

At least one acid test was taken in each hole and once the inclination of the hole at that point was determined via the correction of the angle etched on the test tube, the inclination was so corrected on the cross-section. Core boxes were labelled on the inside with permanent marker and with metal tags on the outside. Each drill run of each hole was measured as a verification of core lengths and recoveries reported by the driller. The runs, core recoveries and acid tests are shown in each drill log. The drillers' footage measurements of the core were converted to meters and the blocks were so relabelled in the core boxes.

Sample intervals were marked in the core boxes via the affixing of sample tags at the beginning of each sample interval. Duplicate tags were included in each labelled sample bag for use by of Chemex. Hole information including runs, sample numbers, recoveries and lithologies were entered as generated by the P. Geo. and checked by him on a daily basis. Cross-sections and vertical long sections were updated as each hole progressed and so verified by the P. Geo. Selected assay data from the final and corrected Chemex Certificates of Analysis were entered on the logs and so verified. The components of the report have been signed and stamped by the relevant P. Geo.

Data verification with regard to financial issues included the careful scrutiny of specific contractor services, performance, and consumption of supplies relative to invoices, records, work sheets and contract terms. Such approved or revised and approved back-up information was used for the checking of the interim and final invoices of each contractor. Approved expenditures were also used on a daily basis to verify budget projections and to determine the overall size and duration of the drill program.

### **9.1.B.2. LITHOLOGIES, ALTERATION AND MINERALIZATION INTERSECTED BY 2004 DIAMOND DRILL PROGRAM:**

The 6 confirmation and step out drill holes are described in Table D1 and other attributes, including the vertical depth of the mineralizations and the coordinates of penetration points on the Vertical Longitudinal Section 1 (VLS 1) are in shown Tables D2 and D3. The lithologies, alteration and mineralizations intersected in the holes and described in the drill logs (Appendix E) and shown on the cross sections (Appendix C) are summarized below.

Crystal tuff is the main host lithology and the South Zone Deposit Stratigraphy (SZDS) is the strongly altered host for the target gold-copper mineralization. The down hole approach to the mineralization through the hanging wall rocks can be recognized by the increase in alteration (silicification, hematization, sulfidization) and by the intensity of brecciation. The SZDS and its northern extension equivalent the NEXT Zone Stratigraphy (NZS), as herein referenced, represent the most intense sections of alteration and brecciation in the drill holes. They include the well sulfidized crackle breccias and quartz-hematite veins that host the auriferous, blebby chalcopyrite, the main target of the drill program.

#### **9.1.B.2.i. CRYSTAL TUFF (CT):**

**COLOUR:** Light to dark grey to green, green to grey, mottled grey and green, purple, brown and red brown; also bleached sections which are tan to light brown to pink brown.

**GRAIN SIZE:** Fine to aphanitic ash groundmass with rounded to sub angular fragments of quartz and feldspar up to 4 mm more typically 2mm.

**COMPOSITION:**

- silica 50-70%
- feldspar 0-30%
- chlorite 5-15%
- epidote 0-10%
- fuchsite 0-10%
- ankerite 0-20%
- hematite 0-5%

**ATTRIBUTES:** May have rusty orange brown colour where acid leached, most prevalent near faults and fractures or the near surface portion of the holes; may have banding - red hematite rich bands alternating with grey, green, brown or purple sections; varying degrees of fracturing with some fairly massive sections.



|              |                                           |                    | TABLE D1                                       |        |                      |                     | Nov 30/04         |           |  |
|--------------|-------------------------------------------|--------------------|------------------------------------------------|--------|----------------------|---------------------|-------------------|-----------|--|
|              |                                           |                    |                                                |        |                      |                     | a:/tabled1        |           |  |
|              |                                           |                    | ANALYTICAL RESULTS, 2004 DIAMOND DRILL PROGRAM |        |                      |                     |                   |           |  |
|              |                                           |                    | TODD CREEK PROPERTY                            |        |                      |                     |                   |           |  |
|              |                                           |                    | <u>NEXT ZONE</u>                               |        |                      |                     |                   |           |  |
|              |                                           |                    |                                                |        |                      |                     |                   | Estimated |  |
| HOLE NUMBER  | SECTION (N), STATION (E)<br>ELEVATION (m) | Hole<br>Length (m) | Au (g/t)                                       | Cu (%) | Core Interval<br>(m) | Core Length:<br>(m) | True Width<br>(m) |           |  |
| DDHNEXT04-01 | 10700N, 10190E<br>1033 m                  | 154.53             | 7.28                                           | 0.76   | 94.70-94.91          | 0.21                | 0.1               |           |  |
|              |                                           |                    | 2.6                                            | 0.26   | 107.00-108.00        | 1.00                | 0.46              |           |  |
|              |                                           |                    | 1.68                                           | 0.49   | 114.98-122.00        | 7.02                | 3.25              |           |  |
|              |                                           |                    | incl. 2.48                                     | 0.6    | 118.70-122.00        | 3.30                |                   |           |  |
|              |                                           |                    | incl. 4.18                                     | 0.92   | 118.70-120.20        | 1.50                |                   |           |  |
|              |                                           |                    | <u>SOUTH ZONE DEPOSIT</u>                      |        |                      |                     |                   |           |  |
| DDHSZD04-01  | 10115N, 9934E<br>1135 m                   | 125.00             | 3.51                                           | 0.09   | 102.27-102.77        | 0.50                | 0.45              |           |  |
|              |                                           |                    | 2.02                                           | 0.23   | 105.97-107.42        | 1.45                | 1.38              |           |  |
| DDHSZD04-02  | 10075N, 9950E<br>1132 m                   | 6.09               | Abandoned in overburden                        |        |                      |                     |                   |           |  |
| DDHSZD04-02A | 10075N, 9930E<br>1132 m                   | 121.64             | 1.08                                           | 0.18   | 101.66-120.00        | 18.34               | 13.75             |           |  |
|              |                                           |                    | incl. 1.35                                     | 0.2    | 101.66-115.42        | 13.76               |                   |           |  |
|              |                                           |                    | incl. 2.65                                     | 0.44   | 101.66-107.28        | 5.62                |                   |           |  |
|              |                                           |                    | incl. 5.39                                     | 0.88   | 104.98-107.28        | 2.30                |                   |           |  |
|              |                                           |                    | incl. 7.02                                     | 1.16   | 104.98-106.58        | 1.60                |                   |           |  |
| DDHSZD04-03  | 10100N, 9900E<br>1131 m                   | 154.27             | 8.55                                           | 0.67   | 142.43-143.75        | 1.32                | 1.25              |           |  |
| DDHSZD04-04  | 10050N, 9925E<br>1132 m                   | 199.39             | 3.09                                           | 0.29   | 180.90-190.90        | 10.00               | 5.25              |           |  |
|              |                                           |                    | incl. 4.04                                     | 0.35   | 180.90-187.13        | 6.23                |                   |           |  |
|              |                                           |                    | incl. 10.51                                    | 0.88   | 180.90-183.12        | 2.22                |                   |           |  |
|              |                                           |                    | <b>TOTAL METERS DRILLED</b>                    |        |                      |                     |                   |           |  |
|              |                                           | <b>760.92</b>      |                                                |        |                      |                     |                   |           |  |

|                                                                |                          | TABLE D2    |             |             |        |       | 20-Dec-04 |
|----------------------------------------------------------------|--------------------------|-------------|-------------|-------------|--------|-------|-----------|
| <b>SOUTH ZONE DEPOSIT &amp; NEXT ZONE: TODD CREEK PROPERTY</b> |                          |             |             |             |        |       |           |
| <b>AU &amp; CU ANALYTICAL RESULTS FROM HISTORIC &amp;</b>      |                          |             |             |             |        |       |           |
| <b>2004 DIAMOND DRILL HOLES</b>                                |                          |             |             |             |        |       |           |
| SECTION                                                        | HOLE NO.                 | Au g/t      | %Cu         | CORE LENGTH | GMP    | GMP   |           |
| (N)                                                            |                          |             |             | (m)         | Au     | Cu    |           |
| 9832                                                           | 87-1                     | 0.420       | 0.12        | 2.13        | 0.895  | 0.26  |           |
| 9868                                                           | 87-2                     | 4.10        | 0.25        | 2.00        | 8.20   | 0.50  |           |
| 9868                                                           | 87-3                     | 5.86        | 0.40        | 0.72        | 4.22   | 0.29  |           |
| 9868                                                           | 88-16                    | 1.91        | 0.17        | 2.05        | 3.91   | 0.35  |           |
| 9927                                                           | 87-4                     | 1.41        | 0.06        | 0.53        | 0.75   | 0.03  |           |
| 9927                                                           | 87-5                     | 11.93       | 1.50        | 1.73        | 20.64  | 2.60  |           |
| 9927                                                           | 88-15                    | 1.53        | 0.11        | 2.60        | 3.98   | 0.29  |           |
| 9959                                                           | 87-6                     | 3.53        | 0.34        | 0.50        | 1.77   | 0.17  |           |
| 9959                                                           | 87-7                     | 4.00        | 0.23        | 1.50        | 6.00   | 0.35  |           |
| 9959                                                           | 88-14                    | 7.65        | 0.97        | 0.15        | 1.15   | 0.15  |           |
| 9996                                                           | 87-8                     | 6.85        | 0.23        | 6.15        | 42.10  | 1.41  |           |
| 9996                                                           | 87-9                     | 2.24        | 0.27        | 9.93        | 22.21  | 2.68  |           |
| 9996                                                           | 88-13                    | 4.17        | 0.62        | 4.25        | 17.72  | 2.64  |           |
| 10021                                                          | 88-10A                   | 4.25        | 0.38        | 5.64        | 23.97  | 2.14  |           |
| 10021                                                          | 88-11                    | 4.35        | 0.56        | 0.40        | 1.74   | 0.22  |           |
| 10021                                                          | 88-12                    | 2.59        | 0.46        | 3.95        | 10.24  | 1.82  |           |
| 10044                                                          | 88-39                    | 5.62        | 0.67        | 1.35        | 7.59   | 0.90  |           |
| 10050                                                          | 04-04                    | 3.09        | 0.29        | 10.00       | 30.90  | 2.90  |           |
| 10075                                                          | 88-17                    | 1.95        | 0.19        | 6.20        | 12.06  | 1.18  |           |
| 10075                                                          | 88-18                    | 2.26        | 0.13        | 4.25        | 9.61   | 0.55  |           |
| 10075                                                          | 88-19                    | 3.61        | 0.27        | 29.75       | 107.40 | 8.03  |           |
| 10075                                                          | 04-02A                   | 1.08        | 0.18        | 18.34       | 19.81  | 3.30  |           |
| 10075                                                          | 88-38                    | 2.02        | 0.20        | 1.40        | 2.83   | 0.28  |           |
| 10100                                                          | 88-33                    | 4.59        | 0.88        | 0.90        | 4.13   | 0.79  |           |
| 10100                                                          | 88-34                    | 3.66        | 0.66        | 3.35        | 12.26  | 2.21  |           |
| 10100                                                          | 88-35                    | 8.61        | 0.45        | 11.70       | 100.74 | 5.27  |           |
| 10100                                                          | 88-37                    | 6.12        | 0.35        | 6.10        | 37.33  | 2.14  |           |
| 10100                                                          | 04-03                    | 8.55        | 0.67        | 1.32        | 11.29  | 0.88  |           |
| 10116                                                          | 88-26                    | 4.65        | 0.74        | 6.15        | 28.60  | 4.55  |           |
| 10116                                                          | 88-27                    | 3.09        | 0.50        | 8.25        | 25.50  | 4.13  |           |
| 10116                                                          | 04-01                    | 2.02        | 0.23        | 1.45        | 2.93   | 0.33  |           |
| 10116                                                          | 88-28                    | 5.97        | 1.30        | 0.25        | 1.49   | 0.33  |           |
| 10154                                                          | 88-29                    | 1.98        | 0.16        | 3.00        | 5.93   | 0.48  |           |
| 10154                                                          | 88-30                    | 5.04        | 0.54        | 0.85        | 4.28   | 0.46  |           |
| 10200                                                          | 88-31                    | 2.19        | 0.34        | 1.75        | 3.83   | 0.60  |           |
| 10200                                                          | 88-32                    | 0.03        | 0.06        | 3.00        | 0.10   | 0.18  |           |
| 10700                                                          | N04-01                   | 1.68        | 0.49        | 7.02        | 11.79  | 3.44  |           |
| Total                                                          | 37                       | 144.59      | 15.97       | 170.61      | 609.90 | 58.80 |           |
|                                                                | <b>Ave Au g/t</b>        | <b>3.57</b> |             |             |        |       |           |
|                                                                | <b>Ave %Cu</b>           |             | <b>0.34</b> |             |        |       |           |
|                                                                | <b>Ave Core Length m</b> |             |             | <b>4.61</b> |        |       |           |
| a:\tabled2                                                     |                          |             |             |             |        |       |           |

**TABLE D3**

20-Dec-04

**AU & CU VALUES OBTAINED WHEN CUT-OFF CRITERIA  
OF 3 G AU/T & 8.2 GMP ARE APPLIED TO, OR HIGHER GRADE  
INTERSECTIONS ARE USED FOR, RESULTS SHOWN IN TABLE D2.  
\* higher grade portion of intercept on VLS 1**

| SECTION<br>(N) | HOLE NO.          | Au g/t | %Cu  | CORE<br>LENGTH<br>(m) | GMP<br>Au | GMP<br>Cu |      |
|----------------|-------------------|--------|------|-----------------------|-----------|-----------|------|
| 9868           | 87-2              | 4.10   | 0.25 | 2.00                  | 8.20      | 0.50      |      |
| 9927           | 87-5              | 11.93  | 1.50 | 1.73                  | 20.64     | 2.60      |      |
| 9996           | 87-8              | 6.85   | 0.23 | 6.15                  | 42.10     | 1.41      |      |
| 9996           | 88-13             | 4.17   | 0.62 | 4.25                  | 17.72     | 2.64      |      |
| *              | 9996              | 87-9   | 3.25 | 0.48                  | 3.69      | 11.99     | 1.77 |
| 10021          | 88-10A            | 4.25   | 0.38 | 5.64                  | 23.97     | 2.14      |      |
| *              | 10021             | 88-12  | 4.22 | 0.78                  | 2.00      | 8.44      | 1.56 |
| 10050          | 04-04             | 3.09   | 0.29 | 10.00                 | 30.90     | 2.90      |      |
| *              | 10075             | 04-02A | 5.39 | 0.88                  | 2.30      | 12.40     | 2.02 |
| 10075          | 88-19             | 3.61   | 0.27 | 29.75                 | 107.40    | 8.03      |      |
| 10100          | 88-35             | 8.61   | 0.45 | 11.70                 | 100.74    | 5.27      |      |
| 10100          | 04-03             | 8.55   | 0.67 | 1.32                  | 11.29     | 0.88      |      |
| 10100          | 88-37             | 6.12   | 0.35 | 6.10                  | 37.33     | 2.14      |      |
| 10100          | 88-34             | 3.66   | 0.66 | 3.35                  | 12.26     | 2.21      |      |
| 10116          | 88-26             | 4.65   | 0.74 | 6.15                  | 28.60     | 4.55      |      |
| 10116          | 88-27             | 3.09   | 0.50 | 8.25                  | 25.50     | 4.13      |      |
| Total          | 16                | 81.44  | 8.80 | 102.38                | 491.28    | 44.25     |      |
|                | Ave Au g/t        | 4.80   |      |                       |           |           |      |
|                | Ave %Cu           |        | 0.43 |                       |           |           |      |
|                | Ave Core Length m |        |      | 6.40                  |           |           |      |

a:\tabled3.xls

## **MINERALIZATION/ALTERATION:**

Sulfidization occurs both as disseminations and as massive patches and stringers in quartz and quartz carbonate veins and stringers, and as rims around fragments. Sulfides are generally pyrite occurring as disseminated grains to euhedral crystals to sooty coatings, generally in or on the margins of quartz and quartz carbonate veins and stringers and chlorite patches. Chalcopyrite is often found with pyrite or as blebs up to several mm. Chalcopyrite is also often occurs as coarse blebs in quartz-hematite veins typically up to 10% and generally with lesser amounts of pyrite. Pyrrhotite was noted but is a less important constituent. Arsenopyrite, bornite and native copper were present as very minor constituents.

Brecciation and crackling appear to be the main ground preparation events and are often accompanied by sulfidization. Quartz and quartz-carbonate veining and stringers are often sulfidized. Silicification is ubiquitous through all holes (locally to 80%) with strongest intensities associated with sulfide mineralization. Intense silicification often results in the crystals within the tuff becoming ghost like or obscure. The core is often lighter in color in highly silicified sections.

Chlorite is prevalent throughout in varying amounts, up to 15% locally and occurs as patches and interstitial patches to 1cm x 3cm, as at 63.55 m in DDHSZD04-01. Sericite is generally minor but was noted on numerous fractures, slips and in faults in all holes; more sericite was noted in DDHSZD04-04, up to 10% locally, e.g. at 105.54-109.0 m.

Epidote is present in all holes in varying amounts up to 10% locally and occurs as crystals and patches. Limonite is generally associated with fractures, slips, faults and more common in the upper more broken portions of the holes. Manganese staining was noted along fracture planes and slips.

Hematite is present as crystals ranging up to 2mm, typically finer, in varying amounts up to 5% locally and up to 10% locally in quartz veins, often with specular hematite or specularite. Although generally minor (up to 1%) in hole DDHNEXT04-01, specularite occurs in the SZD holes locally to 70%, generally in quartz and quartz-carbonate veins and stringers often associated with red hematite. Specularite (to 5% locally) also occurs as fine crystals (1-2mm) in the CT matrix e.g., DDHSZD04-03 at 79.5 m.

Ankerite was most commonly observed in crackle or brecciated areas associated with quartz, apparently replacing carbonate. There is some pseudomorphing after feldspar. More ankerite was noted as the South Zone mineralization was approached. No ankerite was noted in hole DDHNEXT04-01. Fuchsite is prevalent in all holes in varying amounts up to 10% locally and occurs as crystals to 4mm and patches to 1 cm.

**9.1.B.2.ii. MINERALIZED/UNMINERALIZED QUARTZ VEINS, QUARTZ-CARBONATE/QUARTZ-ANKERITE VEINS AND BRECCIA VEINS, STRINGERS, LENSES:**

**COLOUR:** white to grey to blue-grey, cream to yellow and red stained

**GRAIN SIZE:** aphanitic to fine to sugary.

**COMPOSITION:**

- silica 40-100%
- carbonate 0-40%
- chlorite 0-40%
- ankerite 0-20%
- hematite 0-5%
- specularite 0-40%
- sulfides 0-30%

**ATTRIBUTES:** Mostly contained within the altered CT unit; massive to crackled or brecciated, usually without carbonate but present in some cases.

**MINERALIZATION/ALTERATION:**

Veins may be mineralized or unmineralized as in DDHSZD04-01 at 74.33 m. Sulfidization, both disseminated and as massive stringers, occurs in quartz and quartz carbonate veins and stringers, and as rims around silica fragments. Sulfides are generally pyrite, disseminated to euhedral to sooty, generally occurring in or on the margins of quartz and quartz carbonate veins and stringers or chlorite patches. Chalcopyrite is often found with pyrite or as blebs up to several mm. Chalcopyrite often occurs as coarse, disseminated blebs in quartz-hematite veins typically up to 10% and generally with lesser amounts of pyrite.

Chlorite tends to occur as patches and stringers within the veins. Sericite is generally weak but was noted on numerous fractures. Hematite occurs mainly as staining locally in quartz veins often with specularite, up to 5% locally. Specularite occurs generally in quartz and quartz-carbonate veins and stringers and is often associated with red hematite, with or without sulfides. Ankerite is most commonly observed in crackled or brecciated areas associated with quartz.

**9.1.B.2.iii SOUTH ZONE DEPOSIT STRATIGRAPHY ("SZDS"), NEXT ZONE STRATIGRAPHY ("NZS"):**

The stratigraphies are the visual components of the drill core with the strongest alteration and apparent auriferous mineralization. For example, the NZS comprises five multiphase quartz breccia veins usually mineralized with pyrite and blebby chalcopyrite and hosted by silicified and sulfidized, crackled CT. The stratigraphy generally includes elevated Au, As and Cu values as well as the highest-grade Au and Cu mineralization (Drill Log NEXT04-01).



The components directly associated with the SZDS and NZS mineralization include:

moderately to intensely silicified and crackled CT  
moderately to intensely chloritized and sulfidized CT  
multiphase hydrothermal quartz breccia veins  
multiphase sulfide matrix quartz breccia veins  
quartz-hematite sulfide breccia veins  
quartz-carbonate breccia veins  
quartz-hematite breccia veins  
quartz-ankerite matrix breccia veins

**COLOR:** light grey to green, purple, brown and red brown; also bleached sections in the CT sections; light grey to blue grey to yellow or cream in the quartz, quartz-carbonate, and quartz ankerite sections; pink to red in the sections with quartz hematite, brassy where sulfides are abundant.

**GRAIN SIZE:** fragments of CT up to 4 cm in matrix of aphanitic to fine grained quartz, quartz-carbonate, or quartz-ankerite veins, crackled zones; aphanitic quartz fragments up to 5 cm in sulfide matrix breccia

**COMPOSITION:**

- silica 50-90%
- carbonate 0-20%
- feldspar 0-30%
- chlorite 0-15%
- epidote 0-10%
- ankerite 0-20%
- hematite 0-10%
- sulfides 5-30%

**ATTRIBUTES:** Crackling of CT becomes increasingly more intense as the sulfide breccia vein components of the SZD is approached; crackle fragments are surrounded by quartz, hematite, quartz-carbonate, and/or quartz ankerite usually with sulfides (pyrite and chalcopyrite) often rimming the fragments; silicification is generally intense, probably providing the brittle environment permissive of crackling; there is a crustiform nature to some of the quartz-carbonate often rimming other components e.g., DDHSZD04-04 at 189.28 m.

#### **MINERALIZATION/ALTERATION:**

Sulfides, as referenced in 2. above, and locally up to 30% occur mostly in the quartz-hematite/quartz-carbonate/quartz-ankerite surrounding crackle fragments and in the breccia veins, sometimes forming a net texture. Stringers and blebs of massive sulfide (chalcopyrite, pyrite) are also present e.g., DDHSZD04-01 at 102.85 m and DDHSZD04-02A, Frontspiece Photo 1.

Chlorite is prevalent throughout in varying degrees up to 25-35% and occurs as patches and fragments to 6 cm x 10 cm as in Hole SZD04-04 at 175.38 m and as intensely chloritized CT. Sericite is generally weak but noted on fractures, slips and in faults e.g., DDHSZD04-04 at 194.60 m. Epidote occurs up to 5% e.g., DDHSZD04-01 at 102.26 m. Manganese staining was noted on fractures. Hematite occurs as red stain in quartz and quartz-breccia veins and as rims on breccia fragments, often with specularite, up to 10% locally. Specularite occurs generally in quartz-hematite and quartz-carbonate veins and stringers often associated with red hematite. The specularite is generally fine to coarsely disseminated to massive in veins and stringers e.g., DDHSZD04-04 at 191.15 m. Ankerite is most commonly observed in crackled or brecciated areas associated with quartz, apparently replacing carbonate. Fuchsite is found in all holes in varying amounts up to 10% locally, and occurs as crystals to 4mm and patches to 1 cm.

**9.1.B.2.iv. COARSE CHLORITE MATRIX BRECCIA (noted only in DDHNEXT04-01 at 130.9-138.35 m):**

**COLOUR:** light to dark grey to green, red hematite rimming quartz crystals

**GRAIN SIZE:** fine to aphanitic ash groundmass with rounded to sub angular fragments of quartz and feldspar, brecciated, fragments to 5 cm, fine chlorite patches to 5 cm with disseminated and rimming sulfides

**COMPOSITION:**

- silica 50-70%
- feldspar 10-30%
- chlorite 15%
- sulfides 4-12%
- hematite 0-5%
- fuchsite 0-1%

**ATTRIBUTES:** Chlorite matrix breccia, coarse fragments with pyrite up to 12% locally.

**MINERALIZATION/ALTERATION:**

Chlorite is prevalent throughout section as matrix to brecciated crystal tuff, also as chlorite-sulfide patches. Sulfides are mainly pyrite, locally to 12%, 4-5% overall, with traces of chalcopyrite. Quartz occurs as veining and as rims on breccia fragments and net texture. Hematite rims quartz crystals and occurs as veins and stringers. Fuchsite occurs as patches and disseminations, locally up to 1%.

**9.1.B.2.v. SERICITE CHLORITE SCHIST (DDHSZD04-03 at 97.5 m and DHSZD04-01 at 44.85 m):**

**COLOUR:** rusty orange brown to blue grey

**GRAIN SIZE:** fine grained, soft in part, mud in fault or slip

**COMPOSITION:** silica 50-60%  
sericite 10-15%  
chlorite 7-15%  
feldspar 0-30%  
epidote 0-3%  
limonite 5-7%

**ATTRIBUTES:** Occurs in fault zones, poorly cored, in part fault gouge.

**MINERALIZATION/ALTERATION:**

Sericite occurs in shattered core section with fault gouge or area of slickensides. Chlorite occurs with sericite. Epidote occurs as remnant crystals and is minor component. Limonite is associated with fractures, slips, and faults, giving rusty orange color.

**9.1.B.2.vi. COARSE PYROCLASTIC (DDHSZD04-04 at 96.25 m):**

**COLOUR:** purple-brown

**GRAIN SIZE:** fine to coarse; rounded fragments to 5 cm.

**COMPOSITION:** silica 30-40%%  
feldspar 0-30%  
chlorite 5-15%  
carbonate 0-20%  
hematite 0-10%  
specularite 0-10%

**ATTRIBUTES:** volcanic ejecta, rounded, up to 5 cm, chloritic selvages

**MINERALIZATION/ALTERATION:**

Silicification is weak with silica also in quartz and quartz-carbonate veins. Chlorite occurs in fragment selvages and as veins. Quartz-carbonate occurs as veins up to 2 cm wide and as patches. Hematite occurs locally up to 10% in chlorite veins. Specularite occurs locally up to 10% in chlorite veins.

### **9.1.B.3. 2004 DIAMOND DRILL HOLES:**

The results of the 2004 diamond drill holes are discussed below in numerical order. DDHSZD04-04 was drilled before DDHSZD04-02A since DDHSZD04-02 was abandoned in overburden.

#### **9.1.B.3.i. DDHNEXT04-01 (Photos 18-24; Maps 4, 4A, 4B; Tables D1-3; Drill Log NEXT4-01, Cross Section 10700N, Vertical Longitudinal Section 1):**

DDHNEXT04-01 (Photos 18, 19, 21) constitutes a 500 m step out from the most northerly Noranda historic hole. As referenced in Section 9.1.A.iii., the NEXT Zone is postulated to be the dextrally and vertically (down faulted) offset, northern extension of the South Zone Structure (SZS). Or, the zone may be a parallel structure, e.g., equivalent to the Zone B, South Zone deposit (SZD; VLS 2, Appendix D), such that the SZS is located farther to the east under the glacial-fluvial deposits of the Todd Creek Valley. The NEXT Zone is located about 170 m north of the MEXT Zone (Maps 4, 4A) and if it does represent the northern extension of the SZS, the vertical offset measured relative to the SZS at the MEXT Zone is estimated to be at least 30 m and the horizontal offset, about 70 m to the east.

As shown on Section 10700N, at surface the NEXT Zone dips at about 50° to the west. Because of the local topographic conditions (Photo 20), the hole was drilled at an inclination of -30° to the west to chase the zone somewhat down dip and to intersect it at a vertical depth of about 55 m below the collar of the hole. The hole hit the target precisely as planned and returned 1.68 Au/t and 0.49% Cu over a core length of 7.02 m, including 4.18 g Au/t and 0.92% Cu over 1.5 m.

As discussed in Section 9.1.A.i., there is evidence of possible plunging ore shoot morphologies in the SZD. Based on that evidence, an orthogonal grid of forward and back plunge axes has been plotted on VLS 1 (Appendix D). For targeting purposes, DDHNEXT04-01 was designed to intersect the Next Zone Stratigraphy (NZS) in the vicinity of a forward plunge axis (VLS 1).

In spite of the low gold values, the hole is considered to have returned some very positive information. The South Zone Deposit Stratigraphy (SZDS) appears to extend beyond the offset, suggesting the SZDS/NZS is rather strong and continues for another 500 m north of the most northerly Noranda drill hole on the SZD. The hole did intersect about a 36 m core length (94.7 to 130.90 m) of favourable NZS that is rather similar to the SZDS (Photo 22). The stratigraphies are the visual components of the core with the strongest alteration and apparent auriferous mineralization. The NZS comprises five multiphase quartz breccia veins (Photos 22-24) usually mineralized with hematite and blebby chalcopyrite and hosted by silicified and sulfidized, crackled CT. The stratigraphy generally includes elevated Au, As and Cu values as well as the highest-grade Au and Cu mineralization (Drill Log NEXT4-01). The NZS geochemical signature also includes some elevated amounts of Bi, Fe, Mn, Mo, Pb, S, Sb and some Na and Ca depletion (Appendix C).

The altered crystal tuff that comprises the often-silicified footwall and hanging wall rocks of the NZS



**PHOTO 18:** LOOKING 280 ° AT DDHNEXT04-01 DRILL SITE ○ .



**PHOTO 19:** LOOKING SOUTHWEST: DDHNEXT04-01.





**PHOTO 20:** LOOKING NORTHWEST AT SOUTH END OF NEXT ZONE.  
— SOUTH ZONE STRUCTURE ○ AREA OF DDHNEXT04-01.



**PHOTO 21:** LOOKING SOUTHWEST: DDHNEXT04-01 WITH SUMP POND.



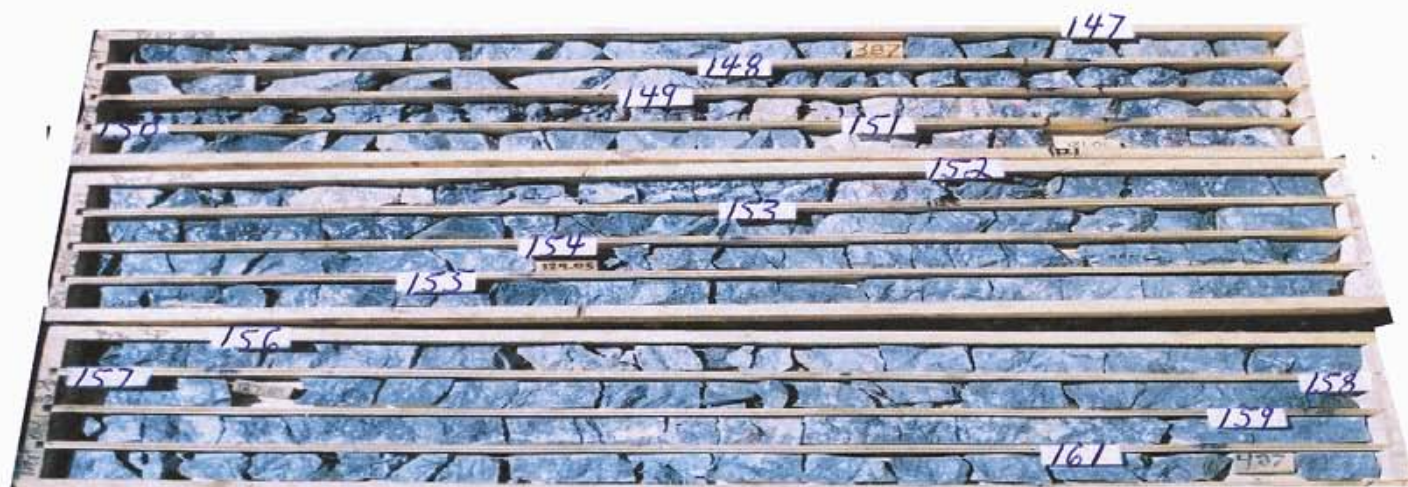
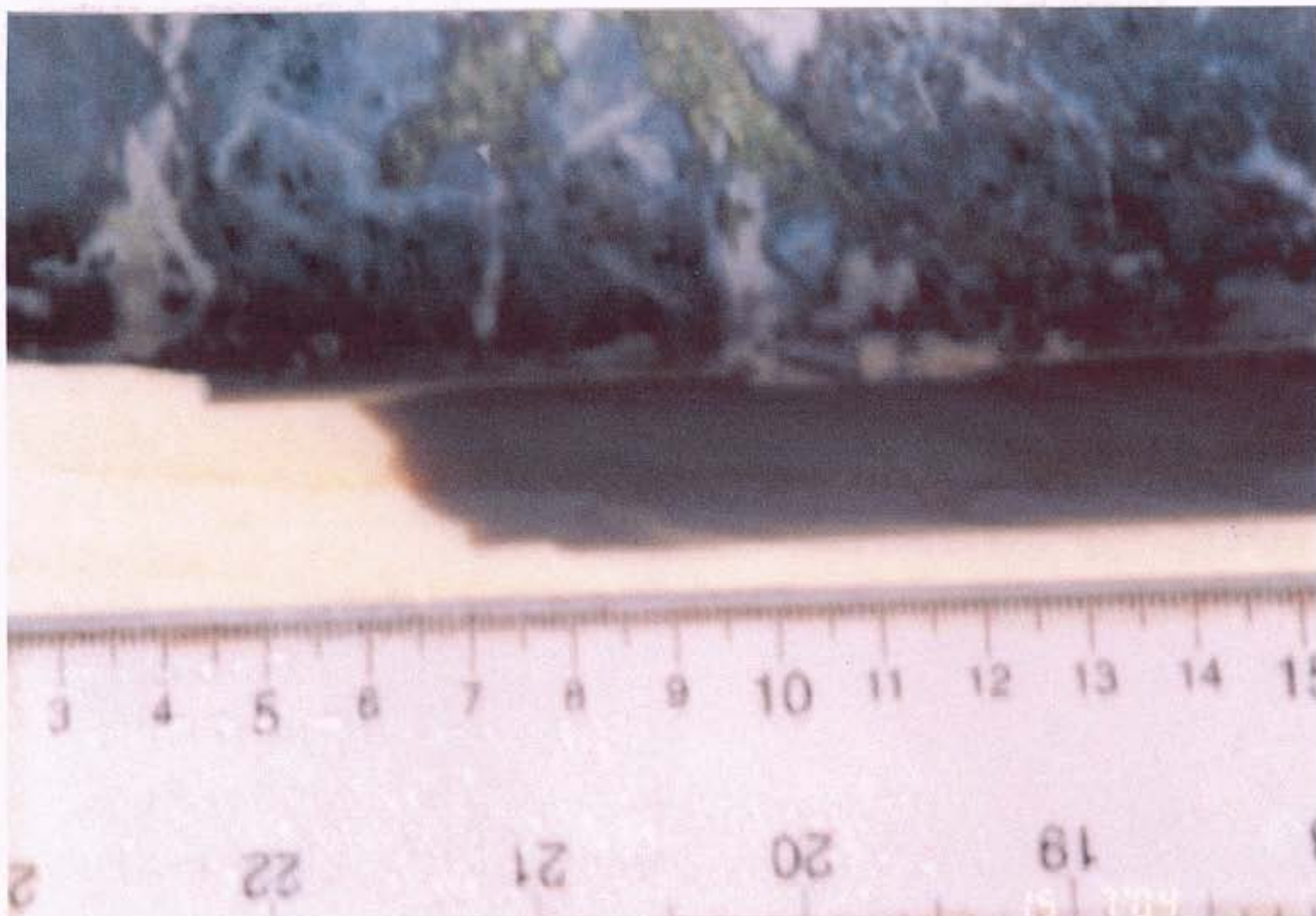


PHOTO 22: NEXT ZONE STRATIGRAPHY: 94.7 TO 130.9 m. SAMPLE NO. PREFIX IS 609.





**PHOTO 23: NEXT04-01 @ 128 m, BOX 30: HEMATITE-BLEBBY CHALCOPYRITE  
QUARTZ BRECCIA VEIN. SAMPLE 609158: 0.187 g Au/t, 0.23% Cu, 774 ppm As.**



**PHOTO 24: NEXT04-01 @ 121.01 m, BOX 28: HEMATITE-BLEBBY CHALCOPYRITE  
QUARTZ BRECCIA VEIN. SAMPLE 609151: 1.55 g Au/t, 0.49% Cu, 631 ppm As.**

Zone has the strongest overall sulfidization of the 2004 drill holes. The sulfides are mainly pyrite but often include disseminations and stringers of chalcopyrite, which are reflected in the anomalous Cu analytical results for many of core samples from DDHNEXT04-01. Many of these values occur in the footwall rocks e.g., 79 m to 94.7 m, which have elevated Cu values with weekly anomalous Au and As values. The hanging wall rocks adjacent to the NZS are characterized by stronger As values than the footwall rocks but with fewer anomalous Au and Cu values.

The NEXT Zone appears to have a fairly constant dip of 50° to where it was intersected by DDHNEXT04-01. There is evidence from the historic Noranda drill holes (VLS 1) and some of the 2004 holes of an inflection in the dip of the SZDS in the South Zone deposit. The inflection mainly occurs around the 1050 m elevation and some of the Noranda highest-grade intersections were obtained in the vicinity of the inflection (VLS 1). In view of the wide NZS with multiple quartz breccia veins (Photos 22-24), the anomalous copper mineralization in DDHNEXT04-04 and the possibility of gold values being concentrated in an inflection and/or plunging shoot morphologies, follow-up hole PNZ05-01 is proposed to intersect the NZS about 75 m vertically below the intersection in DDHNEXT04-01 (VSL 1). The hole would have to be drilled from the cliff about the NEXT Zone (Photo 20) and would total about 300 m.

**9.1.B.3.ii. DDHSZD04-01 (Photos 6, 14; 25 - 29) Maps 4; Tables D1- D3; Drill Log SZD4-01; Cross Section 10115N; Vertical Longitudinal Sections 1, 2):**

As noted above in Section 9.1.A.i., DDHSZD04-01 (Photos 6, 14) was proposed to further define the morphology of the interpreted shoot i.e., to intercept the SZD mineralization about 27 m vertically below the intercept in Noranda hole 88-27, which returned 3.09 g Au/t and 0.50% Cu over 8.25 m, including 6.34 g Au/t and 1.05% Cu over 2.95 m (VLS 1); and, about 15 m north of the intercept in Noranda hole 88-35, which returned 8.6 g Au and 0.45% Cu over 11.7 m.

As shown on Section 10115N and VLS 1, the hole intersected SZD mineralization about 29 m below the intersection in Noranda DDH 88-27 referenced above and returned 3.51 g Au/t and 0.10% Cu over a 0.5 m core length. The hole also returned 2.02 g Au/t and 0.23% Cu over 1.45 m about 5 m vertically below the first intersection. The values occur in an approximate 24 m core length (91.90 – 115.45 m) of favourable SZDS that is comprised of pyritized and crackled CT and multiphase sulfide matrix (3-8% pyrite, hematite and 0.5-2% chalcopyrite) quartz breccia veins (Photos 25- 29). The stratigraphy is generally signatred by anomalous Au and Cu values along with some elevated Cr, Fe, Mn, S and W and some depleted Ca, Na and K.

As shown on VLS 1, a number of higher grade Noranda holes are located in the vicinity of the forward and back plunge axes above and to the south of DDHSZD04-01. There is the possibility that the higher grade and better widths of the mineralization are located in close proximity to such axes. Or, as demonstrated by Noranda DDH88-28 and DDHSZD04-03, which are located relatively close





PHOTO 25: DDHSZD04-01: UPPER AREA (91.9- ~ 100 m) OF SOUTH ZONE DEPOSIT STRATIGRAPHY.





**PHOTO 27: CRACKLED CRYSTAL TUFF WITH SILICA AND CARBONATE FLOODING.**



**PHOTO 26: DDHSZD04-01: SULFIDE MATRIX QUARTZ BRECCIA VEIN.  
SAMPLE 599601: 3.41 g/Au/t, 991 ppm Au, 346 ppm As over 0.5 m (102.27 - 102.77 m).**



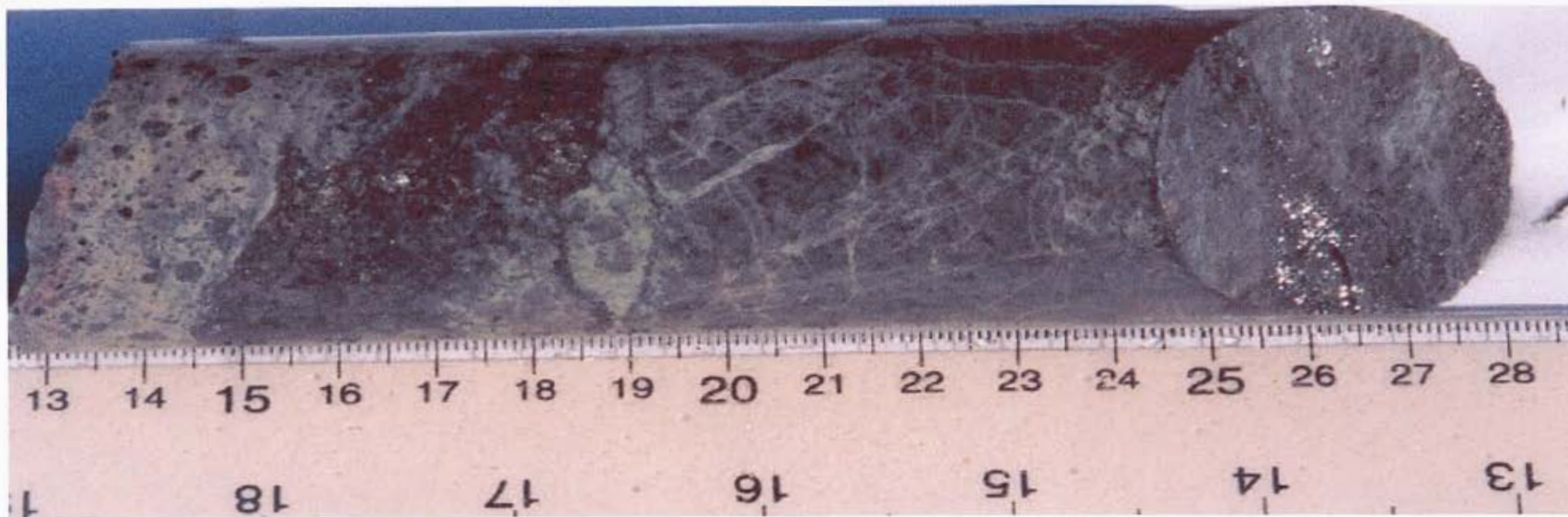


PHOTO 29: DDHSZD04-01: SULFIDE MATRIX BRECCIA WITH PY, CPY.  
SAMPLE 599604: 0.15 g Au/t, 0.34% Cu over 1.1 m (104.87-105.97 m).



PHOTO 28: DDHSZD04-01: SULFIDE-HEMATITE BRECCIA VEIN.  
SAMPLE 599605: 1.23 g Au/t, 0.29% Cu over 0.71 m (105.97—106.68 m).

to Noranda DDH88-28, is it possible for holes to drill through the coarse blebby chalcopyrite mineralization without returning elevated gold and copper values? Based on the author's experience, this phenomenon often occurs in ore grade shoots with disseminated mineralization and is referred to as "the one in three effect" i.e., one good hole out of three in an ore grade shoot.

The last four samples (599621-599624) from the hole were taken starting at 5 m down the core from the bottom of the SZDS. The analytical results are rather interesting, since they average 11.1 ppm Ag and 80.5 Sb ppm over 4.15 m. The last sample returned 18.2 ppm Ag, 35 ppm As, 3 ppm Cd, 154 ppm Sb, 251 ppm Cu, 315 ppm Pb and 142 Zn. Although the values referenced above are not on their own startling and although the four samples only contain some weakly anomalous gold values (up to 15 ppb), the results are considered important since the Ag, Pb and Sb values are some of the highest returned by the 2004 drill holes. The values are increasing down hole and such a specific type of polygeochemical signature often halos gold and gold-copper mineralization in the Stewart Camp. The altered CT from which the samples came contains vugs with quartz-carbonate crystals and trace sulfides – not a conspicuous target. However, if future programs on the Todd Property are successful, the deepening of DDHSDZ04-01 should be considered to evaluate the possibility of another Au-Cu zone in the SZD.

**9.1.B.3.iii. DDHSZD04-02, DDHSZD04-2A (Photos Frontpiece Photo 1, 15, 16, 30-32; Map 4; Tables D1-D3; Drill Logs SZD4-02, 2A: Cross Section 10075N; Vertical Longitudinal Section 1):**

DDHSZD04-02 (Photos 15; Section 10075N) was proposed to further define the morphology of the interpreted shoot i.e., to intercept the South Zone about 25 m vertically below the intercept in Noranda hole 88-19, which returned 3.61 g Au/t and 0.27% Cu over 29.75 m, including 6.91 g Au/t and 0.36% Cu over 8.15 m (VLS 1).

DDHSZ04-02 never reached bedrock and had to be abandoned in overburden at about 6 m. The new hole, DDHSZD04-02A (Photo 16), was collared about 20 m to the west of DDHSZ04-02 and shallowed to intersect the SZD mineralization about 20 m vertically below the Noranda intersection referenced above (Map 4, Cross Section 10075N). The hole returned 1.8 g Au/t and 0.18% Cu over 18.34 m, including 5.39 g Au/t and 0.88% Cu over 2.3 m.

DDHSZD04-02A intersected a core length of the SZDS totalling about 20 m (Photo 30). The favourable stratigraphy includes cracked and sulfidized CT, multiphase quartz-hematite-sulfide breccia veins and quartz-hematite-chlorite breccia veins (Photos 31, 32). The geochemical signature is generally characterized by high to strongly anomalous Au and Cu values. It also includes some elevated Ca, Cr, Bi, Fe, Mn, Mo, Sb and W, along with some K, Na and P depletion.

There appears to be a number of inflections in the dip of the SZD on Section 10075N as indicated by DDHSZ04-02A and the historic Noranda holes. The axis of the largest inflection appears to be in





**PHOTO 30:** DDHSZD04-02A: SOUTH ZONE DEPOSIT STRATIGRAPHY FROM 101.20 TO 120 m (SEE DRILL LOG). SAMPLE PREFIX IS 609.





**PHOTO 31: DDHSZD04-02A: QUARTZ-HEMATITE-ANKERITE MULTIPHASE BRECCIA VEINS, SZDS.  
SAMPLE 609753: 0.09 g Au/t, 0.11% Cu over 1.12 m.**



**PHOTO 32: DDHSZD04-02A: QUARTZ-HEMATITE-SULFIDE VEIN (M TYPE MINERALIZATION) BRECCIA VEIN,  
SZDS. SAMPLE 609754: 10.29 g Au/t, 1.34% Cu over 0.9 m.**

the vicinity of DDHSZD04-2A (~1025 m elevation) where the interpreted dip changes from near 70° to about 80°. This interpretation assumes Noranda DDH88-38 missed most of the SZD target because of the change of dip. The results from the hole are considered transitional from the impressive results in, for example, Noranda DDH88-19 and the low values and widths in, for example, DDSZD04-01. It is postulated that given the nature of the target i.e., coarse blebby chalcopyrite disseminated in quartz breccia veins, that a hole could drill through a well-mineralized zone with a variety of results. Sufficient, closely spaced holes are recommended to adequately evaluate the target, particularly in the case of a strong SZDS such as that intersected in DDHSZD-04-2A.

**9.1.B.3.iv. DDHSZD04-03 (Photos 7, 10, 33-36); Map 4; Tables D1-D3; Drill Log SZD4-03; Cross Section 10100N; Vertical Longitudinal Section 1):**

The hole (Photo 33) was proposed to further define the morphology of the shoot, including its back plunge direction. It was originally designed to provide an intercept of the South Zone about 15 m vertically below the intercept in Noranda hole 88-37, which returned 6.12 g Au/t and 0.35% Cu over 6.10 m (VLS 1).

DDHSZD-04-03 intersected the SZD mineralization (8.6 g Au/t, 12.5 g Ag/t and 0.67% Cu over a core length of 1.32 m) at about 13 m below the Noranda intersection referenced above. The intersection was also signatored by 12.3 ppm Cd, 74 ppm Pb, 453 ppm Zn, 451 ppm As and 1105 ppm Sb.

The SZDS was intersected over a core length of about 25 m (126.23 – 151.25 m; Photos 34, 35) and is mainly comprised of well sulfidized (mainly pyrite) crackled CT often with some hematite. The assay results reported above were returned from a prominent quartz-sulfide breccia vein that contained 2% chalcopyrite and possibly 5% tetrahedrite (Photo 36). As in the other 2004 holes drilled on the SZD, without chalcopyrite, the pyritized crackled CT does generally not contain significant gold values.

The SZDS is generally signatored by weakly to moderately anomalous Au values, and some weakly to strongly anomalous Cu values. Arsenic values, except for the one (451 ppm) associated with the intersection reported above are generally low. Other components of the signature include some elevated Bi, Cr, Fe, Mn, S, Sb and W values, along with some P, Na and K depletion. The signature of the SZDS is generally weak and somewhat similar to that of DDHSZD04-01.

The question remains with respect to both DDHSZD04-01 and -04: how can holes located so close to wide widths of favourable mineralization intersected by the historic Noranda holes (VLS 1) return such narrow widths of similar mineralization? As referenced above with regard to DDHSZD04-01 and -02A, it is postulated that given the physical attributes of the target, it is possible to obtain a variety of wide ranging results from holes drilled into the SZDS. Based on the author's experience, the situation is rather analogous to that with respect to the mineralization at the Golden Patricia Mine





**PHOTO 33: LOOKING NORTHWEST: DDHSZD04-03.**





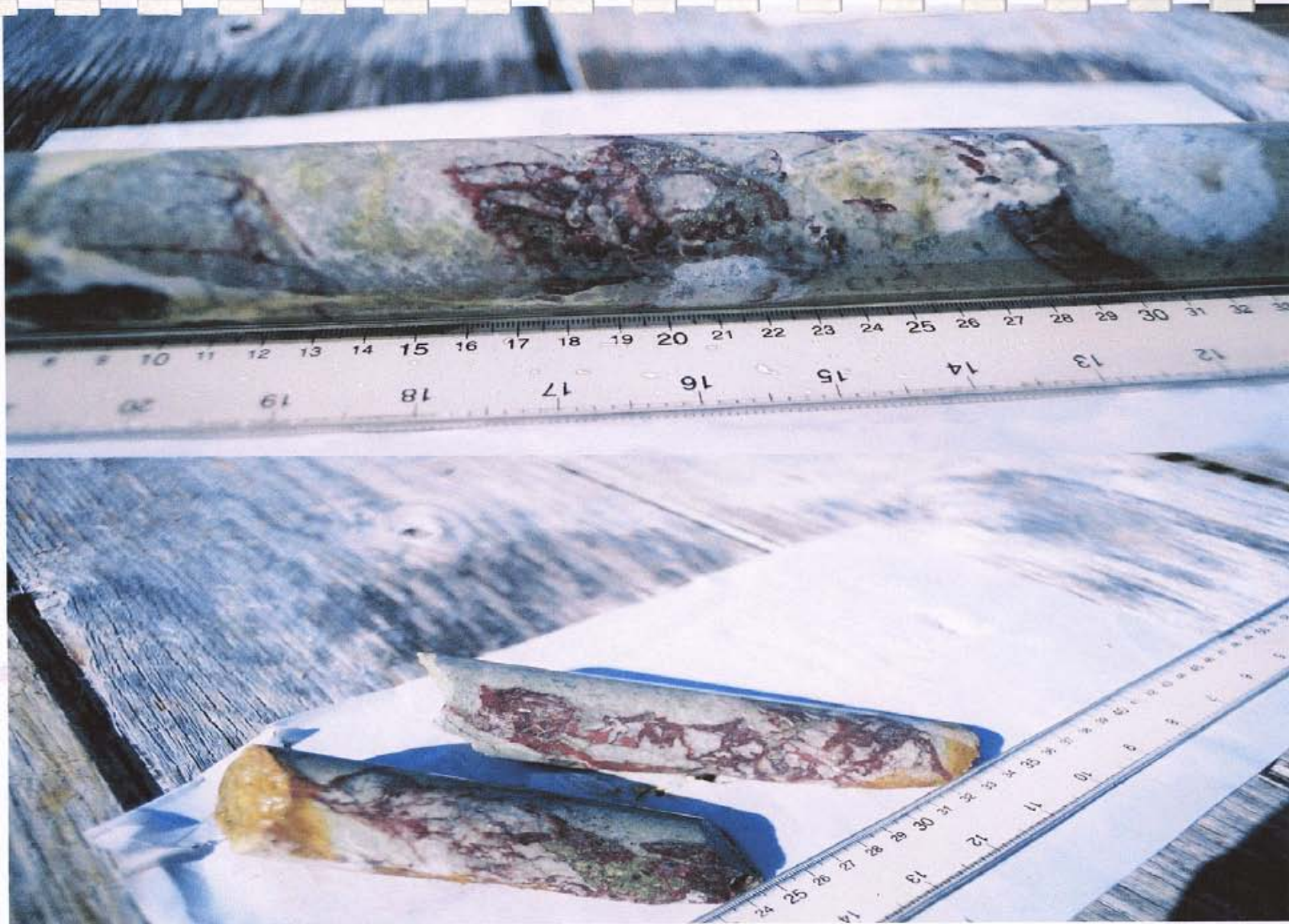
**PHOTO 34: DDHSZD04-03: SOUTH ZONE DEPOSIT STRATIGRAPHY: 126.23~142 m.  
SAMPLE PREFIX IS 599.**





**PHOTO 35: DDHSZD04-03: SOUTH ZONE DEPOSIT STRATIGRAPHY: ~142 -151.25 m.  
SAMPLE PREFIX IS 599.**





**PHOTO 36: DDHSZD04-03: QUARTZ-HEMATITE-SULFIDE VEINS IN ALTERED CT.  
SAMPLE 599660: 0.051 g Au/t, 13 ppm Cu over 1.01 m.**

in the Pickle Lake area of Northwestern Ontario. There, fine to coarse disseminations of gold in a cherty exhalite entailed that only one in three exploration holes in an oreshoot actually returned ore grades and widths.

**9.1.B.3.v. DDHSZD04-04 (Photos 8-11, 17, 37-40); Map 4; Tables D1-D3; Drill Log SZD4-04; Cross Section 10050N; Vertical Longitudinal Sections 1, 1.1, 2):**

DDHSZD04-04 (Photos 8, 9, 11, 17) is the deepest hole ever drilled on the SZD and intersected the target mineralization (Photos 39, 40) at a vertical depth of 182 m (Map 4, Section 10050N, VLS 1). The SZD was intersected over a core length of about 22 m (174.38 - 196.25 m; Photos 37, 38; Drill Log SZD4-04) and returned 3.09 g Au/t and 0.29% Cu over a core length of 10 m, including 10.51 g Au/t and 0.88% Cu over a core length of 2.22 m. In addition to the Au and Cu and values, the geochemical signature includes some weak Ag and Bi; some elevated Ca; generally elevated Cr, Fe, Mn, S, Sb and W; and, generally depleted Na, K, and P (Chemex Certificates of Analysis, Appendix A).

The hole also intersected an 12 m interval (35.85 m to 47.85 m) of altered (silicified, carbonated, chloritized) hanging wall tuff with some fine disseminated pyrite and hematite mineralization. The interval is generally characterized by weakly to strongly anomalous gold values and strongly anomalous copper values i.e., 0.04 g Au/t, 250 ppm Cu over 12 m. The geochemical signature also includes some elevated Ag, Cd, Mo, Mn, Pb, Sb, W and Zn values, along with some Na and Ca depletion. The intersection is of interest with some indication of the Cd-Zn mineralization that often halos gold-copper mineralization in the Stewart Camp. The intersection appears to be too far west to be associated with the B Zone shown on Vertical Longitudinal Section 2 (VLS 2), which is parallel to the SZS and which is located in the SZD hanging wall rocks. The B Zone was intersected in most of the historic Noranda holes drilled to the south of Section 10050N (VLS 2).

There is little information of the dip of the SZS above the 1050 m elevation, other than the projection to near surface shown on Section 10050N. Based on that projection and the intersections shown on the section, the SZS has a dip between about 68° and 72°, which accounts for the deeper intersection than that which was planned and referenced in Section 9.1.A.i. The presence of an inflection in the SZS around the 1050 m elevation has yet to be ascertained by diamond drilling.

DDHSZD04-04 is considered important evidence of continuity of the mineralization at depth, where it remains strong and completely open (VLS 1, 1.1). As shown on VLS 1 and 1.1, a number of follow-up holes (PSZD05-01 to 04) are proposed to test the down dip/plunge potential of the SZD at depth. The four follow-up holes would total about 1200 m and are all planned to intersect the SZD at the 925 m elevation on the postulated forward plunge axes shown on VLS 1. For example, PSZD05-02 is designed to follow-up the down plunge direction of Noranda DDH88-13 (VLS 1), which returned 4.17 g Au/t and 0.62% Cu over a core length of 4.25 m. PSZD05-04 is designed to follow-up the down plunge direction of the MEXT Zone, on which an initial 2005 drill evaluation is proposed in this report.





PHOTO 37: DDHSZD04-04: UPPER AND MIDDLE AREA OF SZDS (~ 175 -190 m)  
SAMPLE PREFIX: 609



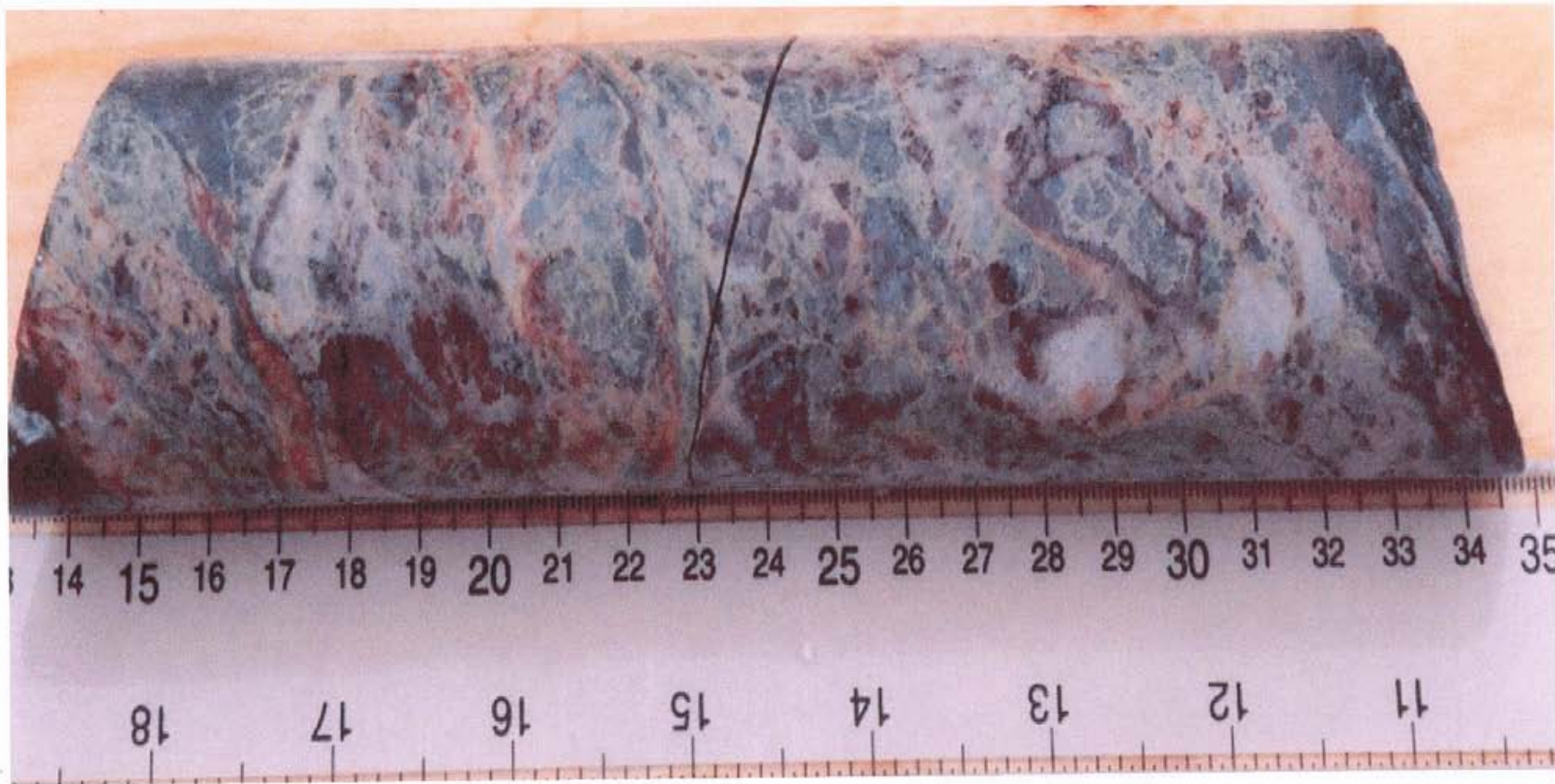


PHOTO 38: DDHSZD04-04: MIDDLE AND LOWER AREA OF SZDS (~183 - 196 m)  
SAMPLE PREFIX: 609



**PHOTO 39: DDHSZD04-04: @ 192.38 m, GREY QUARTZ SULFIDE BRECCIA VEINS IN ALTERED CRYSTAL TUFF.  
SAMPLE 609238: 0.113 g Au/t, 0.24% Cu over 1 m (191.90 – 192.90 m).**





**PHOTO 40: DDHSZD04-04: @ 182 .5 m, QUARTZ SULFIDE HEMATITE BRECCIA VEINS;  
PART OF SAMPLE 609227: 11.1 g Au/t, 0.78% Cu over 1.19 m (181.93 –183.12 m)**

## **9.2. CONCLUSIONS, RECOMMENDATIONS:**

### **9.2.A. CONCLUSIONS:**

As illustrated on VLS 1, the 32 historic and the five 2004 drill holes have all intersected various strengths of the SZS mineralization. As shown in Table D2, the overall average grade of all these holes is 3.57 g Au/t and 0.34% Cu over an average core length of 4.61 m or over an estimated true width of 3.23 m. Using a cutoff of 3 g Au/t and an 8.2 gram meter product, the resulting average grade from the remaining 16 holes is 4.8 g Au/t and 0.43% Cu over an average core length of 6.4 m or an estimated true width of 4.5 m (Table D3). Approximately 43% of the holes meet these cut-off criteria. Although the parameters of its calculation for the South Zone Deposit (207,000 t grading 5.48 g gold/t) are not known, the grade referenced by Noranda can be obtained by increasing the cutoff parameters.

The SZDS and NZS, as intersected by the 2004 drill holes, are mainly signified by elevated gold and copper values; and, often by elevated values of Bi, Cr, Fe, Mn, S, Sb and W, along with Na and K depletion and variable Ca contents. Arsenic values are generally low, except the elevated values associated with the NZS.

As shown on VLS 1 and VLS 1.1, there is some indication that plunging shoot morphologies control the distribution of the higher-grade mineralization. For example, most of the higher-grade mineralization is located in proximity to a number of postulated orthogonal plunge axes (i.e., south plunging axes at about 10050N and 10150N and the north plunging axis at 10000N). As contemplated on VLS 1 and VLS 1.1, such axes often have a regular periodicity of distribution (e.g., as at the Golden Patricia Mine in Northwestern Ontario) and the resulting structural fabric can provide strong rationale for the orchestration of an ore discovery drill program.

The physical characteristics of the sulfide mineralization in the SZD are another important consideration in the interpretation of the drill results. The disseminated, generally coarse, blebby chalcopyrite associated with the M Type mineralization can constitute a “nugget effect”, such that a drill hole could pass through a well-mineralized zone and return low-grade gold and copper values over the width of the zone. This “one in three effect” was experienced at the Golden Patricia Mine, where the distribution of coarse grains of visible gold in a cherty exhalite required close space drilling to partially outline the ore shoots. Only one in three holes in such ore shoots commonly returned ore grade values.

In view of the factors referenced above, it is concluded that the SZDS continues to offer significant exploration potential. As indicated by VLS 1 and the historical database, the SZS target is large. To date it has been delineated over a 1 km strike length and it may extend another 3 km to the south to the Mylonite Zone. It may also extend another 4 km to the north to the Knob Zone, located at the junction of Fall Creek and Todd Creek. As shown on VLS 1, 1.1 and 1.2., about 60% of the known strike length of the SZS has yet to be drill tested and the area that has been tested remains open at



depth (VLS 1, 1.1, 1.2).

One of the most apparently prospective areas of the SZS, the GMZ, is located where the four proposed intercepts (PM05-01, -02, -03, -04) of the recommended 2005 holes are shown on VLS 1. Composite samples taken in 2004 of the rather abundant mineralized talus at the base of cliff in which the GMZ outcrops continue to confirm the importance of the target. A composite sample of Spec Type mineralization returned 6.77 g Au/t and 0.31% Cu and a composite of M Type material returned 5.76 g/Au t and 2.33% Cu. The composites were prepared from two larger samples each weighing approximately 75 kg.

### **9.2.B. RECOMMENDATIONS:**

It is recommended that a 2005 diamond drill program of sufficient scope and size be carried out to attempt to determine if the SZS has potential for hosting a significant orebody. Four initial holes totalling about 1200 m are thus proposed to evaluate the SZD at depth and 4 holes totalling about 350 m are recommended to initially test the GMZ.

The projection points of the proposed intersections of the holes on the SZD (PSZD05-01 to -04) and of those proposed on the GMZ (PM05-01 to -04) are shown on VLS 1. The four proposed holes on the SZD are planned to intersect SZS at the 925 m elevation, approximately 200 m below the collars of the holes (VLS 1.1). The first hole would be drilled 25 m under DDHSZD04-04 to intersect the SZS along the postulated south plunge axis shown on VLS 1. The three other holes are also proposed to intersect the SZD in the vicinity of the south plunging axes shown on VSL 1. For example, the projection point of the PSZD05-02 intersection shown on VLS 1 is located 70 m down plunge of that of Noranda hole DDH88-13 and the projection point of the PSZD05-04 intersection is about 270 m down plunge of the GMZ. The rationale of the SZD drill program is to test the deposit down dip/plunge where it remains open and in the vicinity of where the higher-grade mineralization is postulated to occur.

JVX Ltd. of Toronto has proposed that borehole Spectral IP be utilized, if warranted, in 3 or 4 deep holes drilled on the SZD. Such geophysical methods could map the sulfide mineralization associated with the SZS at depth in order to maximize the on-going drill targeting process. The deeper holes would have to be drilled 60 m beyond the zone of interest.

The four holes proposed on the GMZ would evaluate the apparent higher-grade gold-copper mineralization located in proximity to the structural junction of the MEXT Zone Fault and the SZS. The potential of the auriferous oxide or Spec Type mineralization apparently was not recognized until 1999, when discovered by Geofine in the GMZ target area. As noted by Geofine in 2000, the GMZ is currently deemed to offer one of the highest priority drill targets on the property. An initial target grade of greater than 6 g gold/t and 1% copper is considered reasonable, with the expectation that tonnage and grade components can be enhanced by substantial, plunging ore shoot morphologies.

A follow-up drill program is also recommended on the F1 Zone in the Fall Creek Target Area that

would entail three holes totalling about 255 m. The prospective target is similar to the M Type mineralization in the SZD. It is located in steeper topography but has been delineated by an IP anomaly over an 800 m strike length.

IP surveying could prove very useful elsewhere on the Todd Creek Property. For example, the large Amarillo Zone covers a high-level epithermal system with a very strong polymetallic geochemical signature. Although a number of drill targets have been spotted historically, IP surveying could provide the definition required to prioritize specific targets. The Spectral IP survey technique could also be invaluable at the south end of the South Zone deposit to evaluate its southern strike extension under the glacial fluvial deposits of the Todd Creek Valley.

The proposed 2005 Phase 1 drill program is summarized in Table S2 and would entail 12 holes comprising about 2100 m of diamond drilling. The on site helicopter and camp supported drill program is estimated to total about \$716,000 or about \$649,000 net of GST and refundable reclamation bond (Table S3). The estimated cost is subject to contractor bids and permitting requirements. The program would take about 40 days to complete. If the helicopter was allowed to undertake additional work when not required on the property, it is estimated the program cost would drop to about \$646,000 or about \$581,000 net of GST and refundable reclamation bond.

The program could also be carried out in a number of phases. For example, a Phase 1A program could contemplate testing the Gold Gully – MEXT Zone, the NEXT Zone, the Fall Creek East FI Zone and one deep hole on the South Zone deposit. This program would total about 1200 m. A Phase 1B program could continue with the three remaining holes proposed on the South Zone deposit or as specifically warranted by the results of the Phase 1A program.

**TABLE S2:**

**PROPOSED 2005 DRILL PROGRAM, TODD CREEK PROPERTY**

**AREA 1, SOUTH TARGET AREA:**

| <b>TARGET:</b>                 | <b>HOLES:</b> | <b>METERS:</b> |
|--------------------------------|---------------|----------------|
| i. SOUTH ZONE DEPOSIT          | 4             | 1200           |
| ii. GOLD GULLY-MEXT ZONES      | 4             | 350            |
| iii. NEXT Zone                 | <u>1</u>      | <u>300</u>     |
| <b>AREA 1, PHASE 1 TOTALS:</b> | <b>9</b>      | <b>1850</b>    |

**AREA 2, FALL CREEK TARGET AREA:**

| <b>TARGET:</b>                 | <b>HOLES:</b>   | <b>METERS:</b>    |
|--------------------------------|-----------------|-------------------|
| i. FALL CREEK EAST F1 ZONE     | <u>3</u>        | <u>255</u>        |
| <b>AREA 2, PHASE 1 TOTALS:</b> | <b><u>3</u></b> | <b><u>255</u></b> |

**2005 PROPOSED DRILL PROGRAM                    12                    2105**

TABLE S3: PROPOSED PHASE 1 BUDGET, 2005 FINAL WORK  
PROGRAM: 2100 M DIAMOND DRILLING PROGRAM\*:

| <u>ITEM</u>                                                                                  | <u>ESTIMATED COST</u> |
|----------------------------------------------------------------------------------------------|-----------------------|
|                                                                                              | (\$)                  |
| i) Property, assessment work research                                                        |                       |
| ii) Project permitting, planning, gov't bond                                                 | 28000                 |
| iii) Geochemical signature analyses                                                          |                       |
| iv) Property Compensation                                                                    |                       |
| v) Structural fabric studies, airphotos,<br>mag maps                                         |                       |
| vi) Field equipment, supp incl standards, coresplit                                          | 5500                  |
| vii) Mob-demob                                                                               | 10000                 |
| viii) Ground transport, shipping, GF helicopter                                              | 25000                 |
| ix) Analyses, assays 250 @ \$40                                                              | 10000                 |
| xii) Linecutting                                                                             |                       |
| xiii) Geophys surveys: 12 days, travel mob, report                                           |                       |
| xii) Land surveys                                                                            |                       |
| xiii) Food, sustenance, accommodation                                                        | 4500                  |
| xiv) Communications - in field (sat phone, fax)                                              | 2500                  |
| xv) Compilations, drafting, reporting, assess. rpts,<br>quality assurance, data verification | 12500                 |
| Government filing fees                                                                       | 15000                 |
| xvi) Land acquisition payments, option payments                                              |                       |
| xvii) Legal fees                                                                             |                       |
| xviii) Licences                                                                              |                       |
| xix) Salaries: local labour, geological crew                                                 | 60000                 |
| Workers Comp Ins.<br>\$1200/day @ 50 days;                                                   |                       |
| xx) Diamond drilling: 2100m @210/m                                                           | 441000                |
| incl mob/demob, camp & maint, drill pads,<br>cook, on site heli support                      |                       |
| xxi) Contingency:                                                                            | 44000                 |
| Subtotal                                                                                     | 658000                |
| xxii) Geofine Overhead @3%                                                                   | 19000                 |
| xxiii) GST                                                                                   | 39000                 |
| ESTIMATED TODD 2005 PROPOSED BUDGET*                                                         | \$716000              |
| NET OF RECLAM BOND AND GST:                                                                  | 649000                |
| ESTIMATED TODD 2005 PROPOSED BUDGET**                                                        | \$646000              |
| NET OF RECLAM BOND AND GST:                                                                  | 581000                |

\*Subject to contractor bids and permit requirements. Assumes an on site helicopter.

\*\*If helicopter is allowed to do other work as in 2004, cost of helicopter support may be about 40% less than budgeted.



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**11. STATEMENT OF QUALIFICATIONS:**

I, David E. Molloy P.Geo. of the Town of Unionville, of the Regional Municipality of York, Ontario, hereby certify that:

- i. I am President of Geofine Exploration Consultants Ltd. with a business address at 49 Normandale Road, Unionville, Ontario, L3R 4J8.
- ii. I am a graduate of McMaster University, in the City of Hamilton, Ontario, with a B.A. in Philosophy (1968); I am a graduate of the University of Waterloo, in the City of Waterloo, Ontario, with a B.Sc. in Earth Science (1972);
- iii. I have practiced my profession in mineral exploration continuously for the past 32 years, including 14 years as a consultant; 10 years with St. Joe Canada Inc./Bond Gold Canada Inc./LAC Minerals Ltd. as Regional Geologist, Exploration Manager, Vice President and as Senior Vice President, Canadian Exploration; and, 8 years with Beth-Canada Mining Company as a Regional Geologist;
- iii. I am a Fellow of The Geological Association of Canada;
- iv. I am a Member of the Canadian Institute of Mining and Metallurgy; of the Association of Exploration Geochemists; and, of the BC Yukon Chamber of Mines;
- v. I am a member of the Association of Professional Geoscientists of Ontario and the Association of Professional Engineers and Geoscientists of BC;
- vi. I have supervised the fieldwork and the preparation of this report entitled "Report On the 2004 Diamond Drill Program Carried Out On The Todd Creek Property, Skeena Mining Division, Stewart Gold Camp, Northwestern British Columbia", for Lateegra Resources Corp., by Geofine Exploration Consultants Ltd.;
- vii. The recommendations herein are solely the responsibility of Geofine Exploration Consultants Ltd.

*David E. Molloy, P. Geo.*  
David E. Molloy, P. Geo.,  
President

Dated at Unionville, Ontario, this 13th day of January, 2005.

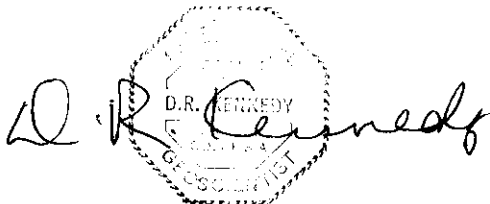




**11. STATEMENT OF QUALIFICATIONS:**

I, David R. Kennedy P.Geo., of the District of North Vancouver, British Columbia, hereby certify that:

- i. I am President of Ailsa Exploration Consultants Ltd. with a business address at 5596 Nuthatch Place, North Vancouver, British Columbia V7R 4R8.
- ii. I am a graduate of Acadia University, Wolfville, Nova Scotia, with a B.Sc. in Geology (1970);
- iii. I have practiced my profession in mineral exploration continuously for the past 34 years, including 14 years as a consultant; 10 years with St. Joe Canada Inc./Bond Gold Canada Inc./LAC Minerals Ltd. as Regional Geologist, Exploration Manager, Western Canada; 2 years with Campbell Resources as a Regional Geologist; and 8 years with consulting group Flanagan McAdam & Co. as a Regional Geologist;
- iv. I am a member of the Association of Professional Engineers and Geoscientists of British Columbia
- v. I am a Member of the BC Yukon Chamber of Mines;
- vi. I have logged the drill core and participated in the fieldwork documented in this report entitled "Report On the 2004 Diamond Drill Program Carried Out On The Todd Creek Property, Skeena Mining Division, Stewart Gold Camp, Northwestern British Columbia", for Lategra Resources Corp., by Geofine Exploration Consultants Ltd.;



The image shows a handwritten signature of David R. Kennedy in black ink. To the right of the signature is a circular professional seal. The seal contains the text "D.R. KENNEDY" at the top and "GEOLOGIST" at the bottom, with a decorative border.

David R. Kennedy, P. Geo.,

Dated at North Vancouver, British Columbia, this 13th day of January, 2005.



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 49 NORMANDALE RD  
 UNIONVILLE ON L3R 4J8

Page: 2 - A  
 Total # Pages: 2 (A - B)  
 Date: 12-JUL-2004  
 Account: KIV

Project: Stewart

**CERTIFICATE OF ANALYSIS VA04040232**

| Sample Description | Method Analyte Units LOR | WEI-21    | Au-AA23 | Au-GRA21 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |       |
|--------------------|--------------------------|-----------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-------|
|                    |                          | Recvd Wt. | Au      | Au       | Aq       | Al       | As       | Ba       | Be       | Bi       | Ca       | Cd       | Co       | Cr       | Cu       | Fe    |
|                    |                          | kg        | ppm     | ppm      | ppm      | %        | ppm      | ppm      | ppm      | ppm      | ppm      | %        | ppm      | ppm      | ppm      | ppm   |
|                    |                          | 0.02      | 0.005   | 0.05     | 0.5      | 0.01     | 5        | 10       | 0.5      | 2        | 0.01     | 0.5      | 1        | 1        | 1        | 0.01  |
| N686851 Text.      |                          | 4.28      | 6.77    |          | 0.9      | 2.69     | <5       | 690      | <0.5     | <2       | 0.50     | <0.5     | 4        | 2        | 3090     | 17.95 |
| N686852 Pow        |                          | 1.54      | 3.64    |          | 45.5     | 2.49     | 1715     | 260      | 1.1      | <2       | 1.30     | 7.9      | 4        | 10       | 478      | 7.09  |
| N686853 Fin.       |                          | 0.06      | >10.0   | 16.65    | 3.2      | 6.23     | 7        | 1620     | 3.1      | <2       | 4.19     | <0.5     | 23       | 146      | 143      | 4.85  |



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Project: Stewart

## CERTIFICATE OF ANALYSIS VA04040232

| Sample Description | Method<br>Analyte<br>Units<br>LOR | ME-ICP61 | ME-ICP61 | ME-ICP61  | ME-ICP61  | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61  | ME-ICP61  | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61  |
|--------------------|-----------------------------------|----------|----------|-----------|-----------|----------|-----------|----------|-----------|----------|-----------|-----------|----------|----------|----------|-----------|
|                    |                                   | K<br>%   | Mg<br>%  | Mn<br>ppm | Mo<br>ppm | Na<br>%  | Ni<br>ppm | P<br>ppm | Pb<br>ppm | S<br>%   | Sb<br>ppm | Sr<br>ppm | Ti<br>%  | V<br>ppm | W<br>ppm | Zn<br>ppm |
|                    |                                   | 0.01     | 0.01     | 5         | 1         | 0.01     | 1         | 10       | 2         | 0.01     | 5         | 1         | 0.01     | 1        | 10       | 2         |
| N686851            |                                   | 0.76     | 0.69     | 589       | 5         | 0.02     | <1        | 90       | 8         | 0.35     | <5        | 24        | 0.03     | 39       | 680      | 52        |
| N686852            |                                   | 1.20     | 0.34     | 3240      | 1         | 0.03     | 9         | 70       | 419       | 5.36     | 19        | 87        | 0.05     | 52       | 10       | 403       |
| N686853            |                                   | 4.34     | 2.57     | 922       | 76        | 1.49     | 69        | 1660     | 239       | 1.39     | <5        | 1100      | 0.27     | 175      | 20       | 69        |



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Page: 2 - A

Total # Pages: 4 (A - C)

Finalized Date: 12-AUG-2004

Account: KIV

Project: Stewart

NEXT04-01

## CERTIFICATE OF ANALYSIS VA04049585

| Sample Description | Method Analyte Units LOR | WEI-21       | Au-AA23 | Au-GRA21 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|--------------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | Recvd Wt. kg | Au ppm  | Au ppm   | Ag ppm   | Al %     | As ppm   | Ba ppm   | Be ppm   | Bi ppm   | Ca %     | Cd ppm   | Co ppm   | Cr ppm   | Cu ppm   | Fe %     |
|                    |                          | 0.02         | 0.005   | 0.05     | 0.5      | 0.01     | 5        | 10       | 0.5      | 2        | 0.01     | 0.5      | 1        | 1        | 1        | 0.01     |
| 609101             |                          | 0.08         | >10.0   | 21.4     | 2.7      | 5.95     | <5       | 1440     | 2.9      | <2       | 4.09     | <0.5     | 22       | 143      | 96       | 4.39     |
| 609102             |                          | 1.68         | 0.016   |          | <0.5     | 7.54     | 5        | 1200     | 0.6      | <2       | 1.02     | <0.5     | 4        | 77       | 150      | 3.34     |
| 609103             |                          | 1.96         | 0.033   |          | <0.5     | 7.07     | 25       | 450      | 0.7      | 3        | 1.19     | <0.5     | 7        | 38       | 1640     | 4.19     |
| 609104             |                          | 1.80         | 0.008   |          | <0.5     | 7.07     | 21       | 640      | 0.7      | <2       | 0.74     | <0.5     | 6        | 85       | 209      | 3.96     |
| 609105             |                          | 1.70         | 0.011   |          | <0.5     | 7.33     | 23       | 480      | 0.7      | <2       | 1.06     | <0.5     | 5        | 59       | 410      | 3.85     |
| 609106             |                          | 1.98         | 0.006   |          | <0.5     | 7.36     | 6        | 2510     | 0.6      | <2       | 1.34     | <0.5     | 3        | 92       | 31       | 2.79     |
| 609107             |                          | 1.62         | 0.009   |          | <0.5     | 7.44     | 30       | 1370     | 0.7      | <2       | 0.89     | <0.5     | 5        | 61       | 1780     | 3.17     |
| 609108             |                          | 1.58         | 0.005   |          | <0.5     | 7.58     | 17       | 2500     | 0.7      | <2       | 1.02     | <0.5     | 4        | 91       | 575      | 2.79     |
| 609109             |                          | 1.64         | 0.007   |          | <0.5     | 7.25     | 7        | 770      | 0.6      | <2       | 1.25     | <0.5     | 3        | 63       | 434      | 3.19     |
| 609110             |                          | 1.68         | 0.017   |          | <0.5     | 7.38     | 20       | 280      | 0.6      | 2        | 0.87     | <0.5     | 5        | 94       | 1515     | 4.02     |
| 609111             |                          | 1.90         | 0.008   |          | <0.5     | 7.15     | 10       | 540      | 0.5      | 3        | 1.51     | <0.5     | 5        | 77       | 167      | 3.74     |
| 609112             |                          | 1.62         | 0.014   |          | <0.5     | 7.05     | 20       | 350      | 0.6      | 3        | 1.35     | <0.5     | 6        | 81       | 1105     | 4.56     |
| 609113             |                          | 1.72         | 0.008   |          | <0.5     | 7.03     | 7        | 500      | 0.5      | 2        | 1.38     | <0.5     | 5        | 56       | 240      | 3.76     |
| 609114             |                          | 1.72         | 0.015   |          | <0.5     | 6.94     | 10       | 630      | 0.5      | <2       | 1.12     | <0.5     | 4        | 71       | 1395     | 3.71     |
| 609115             |                          | 0.10         | 8.35    |          |          |          |          |          |          |          |          |          |          |          |          |          |
| 609116             |                          | 1.68         | 0.007   |          | <0.5     | 7.99     | 12       | 470      | 0.6      | <2       | 0.61     | <0.5     | 5        | 59       | 41       | 3.54     |
| 609117             |                          | 1.72         | 0.007   |          | <0.5     | 7.60     | 16       | 500      | 0.6      | <2       | 0.70     | <0.5     | 4        | 79       | 56       | 3.32     |
| 609118             |                          | 1.20         | 0.023   |          | <0.5     | 6.90     | 24       | 520      | 0.6      | 3        | 1.06     | <0.5     | 5        | 57       | 226      | 3.36     |
| 609119             |                          | 0.32         | 7.28    |          | 3.9      | 4.06     | 529      | 70       | <0.5     | 16       | 0.60     | 4.5      | 8        | 95       | 7640     | 6.77     |
| 609120             |                          | 2.00         | 0.080   |          | <0.5     | 7.29     | 7        | 380      | 0.6      | <2       | 0.85     | <0.5     | 4        | 48       | 376      | 3.62     |
| 609121             |                          | 1.88         | 0.020   |          | <0.5     | 7.40     | 12       | 530      | 0.6      | <2       | 0.75     | <0.5     | 4        | 73       | 136      | 3.45     |
| 609122             |                          | 1.90         | 0.007   |          | <0.5     | 7.60     | 22       | 420      | 0.5      | <2       | 0.74     | <0.5     | 5        | 54       | 49       | 3.40     |
| 609123             |                          | 1.76         | <0.005  |          | <0.5     | 7.76     | 7        | 440      | 0.6      | <2       | 1.01     | <0.5     | 5        | 80       | 25       | 2.99     |
| 609124             |                          | 1.88         | 0.009   |          | <0.5     | 7.27     | 58       | 370      | 0.6      | <2       | 0.35     | <0.5     | 6        | 62       | 69       | 3.10     |
| 609125             |                          | 1.68         | 0.011   |          | <0.5     | 6.91     | 35       | 420      | 0.6      | 3        | 0.23     | <0.5     | 7        | 98       | 229      | 3.33     |
| 609126             |                          | 1.88         | 0.016   |          | <0.5     | 6.94     | 68       | 280      | 0.6      | <2       | 0.22     | <0.5     | 8        | 58       | 53       | 3.40     |
| 609127             |                          | 2.08         | 0.029   |          | 0.5      | 5.84     | 49       | 540      | 0.6      | 3        | 0.16     | <0.5     | 8        | 99       | 336      | 2.97     |
| 609128             |                          | 1.80         | 0.027   |          | <0.5     | 6.57     | 54       | 170      | 0.7      | <2       | 0.14     | <0.5     | 8        | 64       | 176      | 3.28     |
| 609129             |                          | 1.62         | 0.025   |          | <0.5     | 6.33     | 36       | 560      | 0.7      | <2       | 0.12     | <0.5     | 6        | 104      | 184      | 2.91     |
| 609130             |                          | 0.06         | 1.170   |          |          |          |          |          |          |          |          |          |          |          |          |          |
| 609131             |                          | 1.58         | 0.010   |          | <0.5     | 3.99     | 26       | 1440     | <0.5     | <2       | 0.08     | <0.5     | 2        | 150      | 49       | 1.36     |
| 609132             |                          | 1.60         | 0.032   |          | 0.5      | 7.20     | 36       | 230      | 0.7      | 2        | 0.38     | <0.5     | 7        | 94       | 315      | 3.06     |
| 609133             |                          | 1.24         | 0.319   |          | 1.0      | 7.57     | 58       | 250      | 0.7      | 2        | 0.32     | <0.5     | 7        | 61       | 568      | 3.58     |
| 609134             |                          | 0.54         | 8.04    |          | 3.5      | 4.48     | 501      | 90       | 0.5      | 12       | 3.70     | <0.5     | 10       | 77       | 7280     | 5.86     |
| 609135             |                          | 1.60         | 0.029   |          | <0.5     | 7.58     | 30       | 480      | 0.7      | 2        | 0.72     | <0.5     | 4        | 64       | 423      | 2.85     |
| 609136             |                          | 2.10         | 0.038   |          | <0.5     | 7.18     | 93       | 200      | 0.6      | 2        | 0.95     | <0.5     | 6        | 76       | 782      | 3.90     |
| 609137             |                          | 1.74         | 0.022   |          | <0.5     | 7.67     | 34       | 300      | 0.6      | 3        | 0.40     | <0.5     | 5        | 54       | 417      | 3.01     |
| 609138             |                          | 1.76         | 0.022   |          | <0.5     | 6.46     | 92       | 320      | 0.5      | <2       | 0.96     | <0.5     | 4        | 91       | 1230     | 2.80     |
| 609139             |                          | 1.86         | 0.017   |          | <0.5     | 6.85     | 112      | 310      | 0.6      | 3        | 0.90     | <0.5     | 4        | 59       | 1765     | 2.88     |
| 609140             |                          | 1.92         | 0.012   |          | <0.5     | 7.45     | 29       | 450      | 0.6      | 2        | 0.71     | <0.5     | 5        | 73       | 336      | 2.97     |

Comments: ALL SECURITY CODES ARE IN PLACE





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 49 NORMANDALE RD  
 UNIONVILLE ON L3R 4J8

Page: 2 - B  
 Total # Pages: 4 (A - C)  
 Finalized Date: 12-AUG-2004  
 Account: KIV

Project: Stewart

**CERTIFICATE OF ANALYSIS VA04049585**

| Sample Description | Method<br>Analyte<br>Units<br>LOR | ME-ICP61  | ME-ICP61  | ME-ICP61 | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61  | ME-ICP61 |
|--------------------|-----------------------------------|-----------|-----------|----------|----------|-----------|----------|-----------|----------|-----------|----------|----------|-----------|----------|-----------|----------|
|                    |                                   | K         | Mg        | Mn       | Mo       | Na        | Ni       | P         | Pb       | S         | Sb       | Sr       | Ti        | V        | W         | Zn       |
|                    |                                   | %<br>0.01 | %<br>0.01 | ppm<br>5 | ppm<br>1 | %<br>0.01 | ppm<br>1 | ppm<br>10 | ppm<br>2 | %<br>0.01 | ppm<br>5 | ppm<br>1 | %<br>0.01 | ppm<br>1 | ppm<br>10 | ppm<br>2 |
| 609101             |                                   | 4.18      | 2.57      | 855      | 74       | 1.45      | 63       | 1650      | 226      | 1.24      | <5       | 1105     | 0.25      | 168      | 10        | 63       |
| 609102             |                                   | 6.45      | 0.53      | 752      | 5        | 0.18      | <1       | 480       | 8        | 1.55      | <5       | 84       | 0.19      | 48       | <10       | 31       |
| 609103             |                                   | 5.82      | 0.58      | 820      | 6        | 0.14      | <1       | 460       | 7        | 2.45      | <5       | 110      | 0.17      | 50       | 10        | 31       |
| 609104             |                                   | 5.52      | 0.57      | 460      | 6        | 0.15      | <1       | 460       | 20       | 1.97      | <5       | 115      | 0.17      | 54       | <10       | 40       |
| 609105             |                                   | 6.04      | 0.57      | 746      | 7        | 0.16      | <1       | 450       | 12       | 2.07      | <5       | 81       | 0.18      | 53       | <10       | 35       |
| 609106             |                                   | 6.60      | 0.51      | 792      | 4        | 0.14      | <1       | 470       | 9        | 0.77      | <5       | 114      | 0.18      | 48       | <10       | 36       |
| 609107             |                                   | 6.14      | 0.45      | 541      | 3        | 0.10      | <1       | 490       | 15       | 1.32      | <5       | 76       | 0.18      | 49       | <10       | 36       |
| 609108             |                                   | 6.45      | 0.42      | 556      | 5        | 0.11      | 2        | 510       | 9        | 0.97      | <5       | 98       | 0.18      | 47       | <10       | 34       |
| 609109             |                                   | 6.50      | 0.40      | 655      | 4        | 0.10      | <1       | 470       | 5        | 1.76      | <5       | 143      | 0.17      | 45       | <10       | 27       |
| 609110             |                                   | 6.34      | 0.45      | 605      | 8        | 0.09      | 1        | 470       | 9        | 2.69      | <5       | 69       | 0.18      | 49       | <10       | 23       |
| 609111             |                                   | 6.34      | 0.56      | 853      | 5        | 0.09      | <1       | 450       | 3        | 2.22      | <5       | 140      | 0.17      | 47       | <10       | 27       |
| 609112             |                                   | 5.97      | 0.62      | 952      | 7        | 0.09      | 1        | 440       | 8        | 2.65      | <5       | 72       | 0.17      | 50       | <10       | 31       |
| 609113             |                                   | 6.14      | 0.59      | 880      | 6        | 0.09      | <1       | 460       | 8        | 2.12      | <5       | 85       | 0.16      | 45       | <10       | 28       |
| 609114             |                                   | 6.11      | 0.52      | 796      | 5        | 0.09      | <1       | 430       | 9        | 1.94      | 5        | 85       | 0.16      | 44       | <10       | 29       |
| 609115             |                                   |           |           |          |          |           |          |           |          |           |          |          |           |          |           |          |
| 609116             |                                   | 6.94      | 0.40      | 394      | 5        | 0.11      | <1       | 520       | 8        | 2.38      | <5       | 68       | 0.19      | 54       | 10        | 23       |
| 609117             |                                   | 6.17      | 0.40      | 472      | 6        | 0.14      | <1       | 480       | 8        | 2.10      | 5        | 78       | 0.18      | 48       | <10       | 21       |
| 609118             |                                   | 6.19      | 0.51      | 771      | 10       | 0.12      | <1       | 430       | 6        | 2.06      | <5       | 77       | 0.16      | 45       | <10       | 31       |
| 609119             |                                   | 2.56      | 0.54      | 510      | 65       | 0.04      | <1       | 220       | 68       | 4.07      | 15       | 120      | 0.09      | 39       | <10       | 254      |
| 609120             |                                   | 6.38      | 0.48      | 677      | 6        | 0.10      | 1        | 460       | 10       | 2.21      | 5        | 70       | 0.17      | 48       | <10       | 30       |
| 609121             |                                   | 6.84      | 0.40      | 545      | 5        | 0.11      | 2        | 460       | 10       | 2.14      | <5       | 73       | 0.18      | 45       | <10       | 22       |
| 609122             |                                   | 6.60      | 0.41      | 499      | 5        | 0.11      | 1        | 470       | 13       | 2.29      | 7        | 73       | 0.18      | 50       | <10       | 18       |
| 609123             |                                   | 7.15      | 0.49      | 711      | 5        | 0.13      | <1       | 480       | 14       | 2.18      | <5       | 89       | 0.18      | 49       | 10        | 12       |
| 609124             |                                   | 6.03      | 0.31      | 192      | 5        | 0.10      | <1       | 470       | 11       | 2.21      | 5        | 75       | 0.18      | 47       | <10       | 16       |
| 609125             |                                   | 6.49      | 0.27      | 102      | 7        | 0.10      | <1       | 460       | 23       | 2.28      | 5        | 69       | 0.17      | 48       | <10       | 19       |
| 609126             |                                   | 5.49      | 0.30      | 102      | 5        | 0.10      | 1        | 460       | 8        | 2.17      | <5       | 114      | 0.17      | 48       | 10        | 20       |
| 609127             |                                   | 5.22      | 0.25      | 78       | 6        | 0.07      | 1        | 370       | 9        | 1.88      | <5       | 73       | 0.14      | 41       | <10       | 17       |
| 609128             |                                   | 5.87      | 0.27      | 71       | 7        | 0.08      | <1       | 440       | 11       | 2.11      | 5        | 277      | 0.16      | 47       | <10       | 20       |
| 609129             |                                   | 5.63      | 0.24      | 65       | 10       | 0.08      | <1       | 400       | 10       | 1.76      | <5       | 70       | 0.16      | 50       | <10       | 17       |
| 609130             |                                   |           |           |          |          |           |          |           |          |           |          |          |           |          |           |          |
| 609131             |                                   | 3.23      | 0.13      | 33       | 5        | 0.05      | 1        | 240       | 6        | 0.79      | <5       | 36       | 0.10      | 30       | <10       | 7        |
| 609132             |                                   | 5.69      | 0.28      | 140      | 10       | 0.07      | 2        | 450       | 16       | 2.16      | 5        | 64       | 0.17      | 52       | <10       | 16       |
| 609133             |                                   | 6.12      | 0.31      | 192      | 9        | 0.12      | <1       | 480       | 12       | 2.73      | <5       | 56       | 0.18      | 54       | <10       | 15       |
| 609134             |                                   | 3.07      | 1.30      | 2090     | 12       | 0.04      | 1        | 280       | 23       | 3.79      | 8        | 103      | 0.10      | 42       | <10       | 36       |
| 609135             |                                   | 5.85      | 0.42      | 553      | 5        | 0.10      | <1       | 490       | 10       | 2.03      | 7        | 76       | 0.18      | 50       | <10       | 9        |
| 609136             |                                   | 6.48      | 0.46      | 706      | 8        | 0.10      | 1        | 470       | 16       | 2.78      | 6        | 98       | 0.17      | 51       | <10       | 14       |
| 609137             |                                   | 6.22      | 0.26      | 257      | 5        | 0.10      | <1       | 490       | 8        | 2.47      | <5       | 74       | 0.19      | 50       | <10       | 7        |
| 609138             |                                   | 5.78      | 0.39      | 632      | 11       | 0.09      | 1        | 420       | 9        | 2.27      | <5       | 102      | 0.16      | 41       | 10        | 6        |
| 609139             |                                   | 5.88      | 0.44      | 614      | 15       | 0.09      | <1       | 450       | 13       | 2.27      | 5        | 78       | 0.16      | 43       | 10        | 7        |
| 609140             |                                   | 6.42      | 0.40      | 491      | 8        | 0.09      | 1        | 480       | 6        | 2.08      | <5       | 73       | 0.18      | 54       | <10       | 11       |

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49 NORMANDALE RD

UNIONVILLE ON L3R 4J8

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Total # Pages: 4 (A - C)

Finalized Date: 12-AUG-2004

Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04049585

| Sample Description                             | Method<br>Analyte<br>Units<br>LOR | Cu-AA62<br>Cu<br>%<br>0.01 |
|------------------------------------------------|-----------------------------------|----------------------------|
| 609101<br>609102<br>609103<br>609104<br>609105 |                                   |                            |
| 609106<br>609107<br>609108<br>609109<br>609110 |                                   |                            |
| 609111<br>609112<br>609113<br>609114<br>609115 |                                   |                            |
| 609116<br>609117<br>609118<br>609119<br>609120 |                                   |                            |
| 609121<br>609122<br>609123<br>609124<br>609125 |                                   |                            |
| 609126<br>609127<br>609128<br>609129<br>609130 |                                   |                            |
| 609131<br>609132<br>609133<br>609134<br>609135 |                                   |                            |
| 609136<br>609137<br>609138<br>609139<br>609140 |                                   |                            |

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Page: 3 - A  
 Total # Pages: 4 (A - C)  
 Finalized Date: 12-AUG-2004  
 Account: KIV

Project: Stewart

**CERTIFICATE OF ANALYSIS VA04049585**

| Sample Description | Method Analyte Units LOR | WEI-21    | Au-AA23 | Au-GRA21 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|-----------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | Recvd Wt. | Au      | Au       | Ag       | Al       | As       | Ba       | Be       | Bi       | Ca       | Cd       | Co       | Cr       | Cu       | Fe       |
|                    |                          | kg        | ppm     | ppm      | ppm      | %        | ppm      | ppm      | ppm      | ppm      | %        | ppm      | ppm      | ppm      | ppm      | %        |
|                    | 0.02                     | 0.005     | 0.05    | 0.5      | 0.01     | 5        | 10       | 0.5      | 2        | 0.01     | 0.5      | 1        | 1        | 1        | 0.01     |          |
| 609141             |                          | 1.56      | 0.024   |          | <0.5     | 7.44     | 36       | 380      | 0.6      | 2        | 0.61     | <0.5     | 3        | 62       | 636      | 3.17     |
| 609142             |                          | 0.36      | >10.0   | 21.6     | 5.3      | 3.52     | 757      | 70       | 0.5      | 5        | 1.06     | <0.5     | 17       | 121      | >10000   | 7.42     |
| 609143             |                          | 1.80      | 0.060   |          | <0.5     | 7.92     | 23       | 400      | 0.8      | 3        | 0.51     | <0.5     | 5        | 49       | 552      | 2.98     |
| 609144             | X                        | 1.96      | 0.063   |          | 0.6      | 6.91     | 64       | 240      | 0.6      | 3        | 0.68     | <0.5     | 6        | 84       | 2440     | 3.18     |
| 609145             |                          | 0.06      | 0.176   |          | 2.8      | 5.03     | <5       | 110      | <0.5     | <2       | 10.95    | <0.5     | 197      | 530      | 6810     | 12.20    |
| 609146             | X                        | 1.80      | 0.337   |          | 1.8      | 6.84     | 170      | 300      | 0.7      | <2       | 0.24     | <0.5     | 6        | 68       | 7490     | 3.40     |
| 609147             | X                        | 1.14      | 0.477   |          | 0.7      | 7.34     | 56       | 1420     | 0.9      | <2       | 0.37     | <0.5     | 4        | 84       | 1355     | 3.07     |
| 609148             | X                        | 1.22      | 4.44    |          | 5.1      | 3.08     | 679      | 70       | 0.9      | 8        | 0.88     | <0.5     | 20       | 95       | 7860     | 5.82     |
| 609149             | X                        | 1.20      | 3.80    |          | 3.9      | 2.35     | 146      | 60       | 0.8      | 2        | 0.37     | <0.5     | 7        | 164      | >10000   | 5.92     |
| 609150             |                          | 1.20      | 0.054   |          | <0.5     | 5.94     | 190      | 140      | 0.5      | 5        | 0.17     | <0.5     | 7        | 69       | 132      | 3.51     |
| 609151             | X                        | 2.36      | 1.550   |          | 3.2      | 2.84     | 631      | 50       | 0.6      | 27       | 0.40     | <0.5     | 8        | 146      | 4890     | 8.28     |
| 609152             |                          | 1.60      | 0.041   |          | 0.6      | 7.57     | 114      | 200      | 0.9      | 3        | 0.28     | <0.5     | 7        | 41       | 80       | 5.13     |
| 609153             |                          | 1.68      | 0.033   |          | 0.5      | 6.52     | 45       | 340      | 0.6      | <2       | 1.26     | <0.5     | 5        | 95       | 1050     | 3.96     |
| 609154             |                          | 1.96      | 0.069   |          | <0.5     | 6.46     | 63       | 290      | 0.7      | <2       | 2.61     | <0.5     | 6        | 39       | 853      | 5.54     |
| 609155             |                          | 1.94      | 0.071   |          | <0.5     | 5.83     | 127      | 130      | 0.7      | <2       | 0.26     | <0.5     | 8        | 91       | 102      | 4.52     |
| 609156             |                          | 1.56      | 0.041   |          | 0.8      | 6.70     | 121      | 160      | 0.7      | 4        | 0.67     | <0.5     | 6        | 55       | 33       | 5.14     |
| 609157             |                          | 2.02      | 0.031   |          | 1.1      | 6.55     | 146      | 200      | 0.8      | 8        | 0.72     | <0.5     | 6        | 76       | 714      | 6.55     |
| 609158             |                          | 2.08      | 0.187   |          | 2.0      | 4.13     | 774      | 60       | 0.6      | 6        | 3.00     | <0.5     | 10       | 57       | 2340     | 9.05     |
| 609159             |                          | 2.10      | 0.019   |          | 1.9      | 6.23     | 120      | 270      | 0.6      | 18       | 1.96     | <0.5     | 7        | 78       | 178      | 4.82     |
| 609160             |                          | 0.10      | 9.58    |          | 1.9      | 6.66     | 14       | 1460     | 3.3      | <2       | 5.32     | <0.5     | 28       | 176      | 130      | 5.46     |
| 609161             |                          | 1.68      | 0.019   |          | 0.8      | 6.41     | 100      | 110      | 0.7      | 7        | 2.68     | <0.5     | 6        | 46       | 77       | 5.35     |
| 609162             |                          | 2.26      | 0.014   |          | 0.6      | 6.84     | 118      | 170      | 0.8      | <2       | 1.48     | <0.5     | 6        | 72       | 20       | 5.22     |
| 609163             |                          | 1.70      | 0.008   |          | <0.5     | 6.35     | 121      | 140      | 0.7      | 3        | 1.18     | <0.5     | 4        | 56       | 19       | 4.57     |
| 609164             |                          | 1.78      | 0.009   |          | <0.5     | 6.46     | 104      | 200      | 0.7      | 4        | 1.78     | <0.5     | 5        | 72       | 88       | 4.57     |
| 609165             |                          | 1.80      | 0.008   |          | <0.5     | 6.25     | 117      | 220      | 0.6      | 2        | 0.92     | <0.5     | 4        | 56       | 15       | 4.13     |
| 609166             |                          | 1.98      | 0.011   |          | <0.5     | 6.16     | 132      | 200      | 0.6      | <2       | 0.83     | <0.5     | 6        | 84       | 18       | 4.14     |
| 609167             |                          | 1.88      | 0.007   |          | <0.5     | 6.26     | 98       | 180      | 0.7      | <2       | 0.83     | <0.5     | 5        | 57       | 31       | 4.43     |
| 609168             |                          | 2.16      | 0.005   |          | <0.5     | 5.63     | 64       | 220      | 0.6      | <2       | 1.64     | <0.5     | 5        | 97       | 102      | 3.41     |
| 609169             |                          | 1.72      | 0.007   |          | <0.5     | 6.23     | 128      | 190      | 0.5      | <2       | 1.29     | <0.5     | 5        | 65       | 36       | 3.55     |
| 609170             |                          | 1.74      | 0.016   |          | <0.5     | 6.16     | 234      | 110      | 0.5      | <2       | 1.30     | <0.5     | 5        | 104      | 70       | 4.31     |
| 609171             |                          | 1.74      | 0.014   |          | <0.5     | 6.19     | 125      | 160      | 0.5      | <2       | 1.52     | <0.5     | 4        | 76       | 88       | 3.52     |
| 609172             |                          | 2.00      | 0.013   |          | <0.5     | 6.34     | 124      | 220      | 0.5      | 3        | 1.91     | <0.5     | 6        | 86       | 621      | 3.90     |
| 609173             |                          | 2.04      | 0.005   |          | <0.5     | 6.74     | 60       | 210      | 0.5      | <2       | 1.76     | <0.5     | 4        | 60       | 168      | 3.28     |
| 609174             |                          | 2.20      | <0.005  |          | <0.5     | 6.87     | 43       | 230      | 0.5      | <2       | 1.58     | <0.5     | 3        | 89       | 52       | 3.17     |
| 609175             |                          | 0.06      | 1.310   |          | 2.4      | 8.78     | 164      | 40       | <0.5     | <2       | 4.42     | <0.5     | 224      | 29       | 9060     | 12.35    |
| 609176             |                          | 1.80      | 0.007   |          | <0.5     | 6.88     | 47       | 250      | 0.6      | <2       | 1.21     | <0.5     | 6        | 67       | 27       | 3.02     |
| 609177             |                          | 1.62      | <0.005  |          | <0.5     | 6.97     | 46       | 300      | 0.6      | <2       | 1.04     | <0.5     | 6        | 89       | 22       | 3.34     |
| 609178             |                          | 1.78      | <0.005  |          | <0.5     | 7.36     | 39       | 250      | 0.6      | <2       | 1.00     | <0.5     | 5        | 56       | 46       | 3.26     |
| 609179             |                          | 1.74      | 0.005   |          | <0.5     | 6.95     | 81       | 170      | 0.6      | 2        | 1.24     | <0.5     | 6        | 88       | 310      | 4.28     |
| 609180             |                          | 1.94      | <0.005  |          | <0.5     | 6.85     | 40       | 240      | 0.5      | <2       | 1.42     | <0.5     | 4        | 58       | 14       | 3.10     |

Comments: ALL SECURITY CODES ARE IN PLACE

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To: GEOFINE EXPLORATION CONSULTANTS LTD.  
49 NORMANDALE RD  
UNIONVILLE ON L3R 4J8

Page: 3 - B  
Total # Pages: 4 (A - C)  
Finalized Date: 12-AUG-2004  
Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04049585

| Sample Description | Method Analyte Units LOR | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | K        | Mg       | Mn       | Mo       | Na       | Ni       | P        | Pb       | S        | Sb       | Sr       | Ti       | V        | W        | Zn       |
|                    |                          | %        | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      |
| 609141             |                          | 6.17     | 0.39     | 466      | 7        | 0.08     | 1        | 480      | 11       | 2.18     | <5       | 65       | 0.18     | 51       | <10      | 14       |
| 609142             |                          | 1.94     | 0.51     | 786      | 152      | 0.02     | <1       | 230      | 70       | 6.42     | 15       | 89       | 0.07     | 40       | <10      | 44       |
| 609143             |                          | 6.17     | 0.33     | 314      | 11       | 0.08     | 2        | 500      | 7        | 2.25     | <5       | 62       | 0.19     | 56       | <10      | 11       |
| 609144             |                          | 6.02     | 0.37     | 515      | 18       | 0.09     | <1       | 480      | 14       | 2.63     | <5       | 56       | 0.17     | 44       | <10      | 6        |
| 609145             |                          | 0.11     | 7.32     | 1115     | 2        | 0.13     | 2760     | 590      | 10       | 3.40     | <5       | 44       | 0.41     | 176      | <10      | 91       |
| 609146             |                          | 5.49     | 0.24     | 125      | 28       | 0.07     | 4        | 460      | 26       | 2.56     | 5        | 57       | 0.17     | 45       | <10      | 15       |
| 609147             |                          | 5.39     | 0.35     | 245      | 9        | 0.06     | <1       | 470      | 9        | 1.34     | <5       | 48       | 0.18     | 52       | <10      | 27       |
| 609148             |                          | 1.70     | 0.45     | 655      | 97       | 0.02     | 3        | 180      | 70       | 5.17     | 15       | 67       | 0.06     | 52       | <10      | 24       |
| 609149             |                          | 0.97     | 0.37     | 447      | 22       | 0.02     | 3        | 90       | 28       | 3.60     | 13       | 329      | 0.04     | 51       | <10      | 33       |
| 609150             |                          | 6.17     | 0.21     | 122      | 16       | 0.09     | 2        | 400      | 10       | 2.53     | 6        | 61       | 0.14     | 32       | 10       | 13       |
| 609151             |                          | 1.68     | 0.46     | 419      | 8        | 0.03     | <1       | 140      | 67       | 6.16     | 14       | 93       | 0.05     | 33       | 10       | 42       |
| 609152             |                          | 6.61     | 0.50     | 241      | 7        | 0.09     | 9        | 480      | 19       | 2.89     | 10       | 112      | 0.19     | 56       | <10      | 38       |
| 609153             |                          | 6.13     | 0.62     | 1055     | 8        | 0.10     | 12       | 410      | 16       | 2.34     | 9        | 100      | 0.15     | 44       | <10      | 34       |
| 609154             |                          | 5.04     | 1.30     | 2260     | 2        | 0.07     | 3        | 400      | 22       | 2.63     | 7        | 118      | 0.15     | 50       | 10       | 35       |
| 609155             |                          | 4.93     | 0.37     | 225      | 3        | 0.07     | 2        | 360      | 26       | 3.20     | <5       | 129      | 0.14     | 44       | <10      | 22       |
| 609156             |                          | 6.01     | 0.47     | 558      | 3        | 0.08     | <1       | 430      | 62       | 4.18     | 7        | 93       | 0.16     | 44       | <10      | 29       |
| 609157             |                          | 5.50     | 0.50     | 588      | 3        | 0.07     | <1       | 410      | 66       | 5.68     | 7        | 67       | 0.16     | 47       | 10       | 19       |
| 609158             |                          | 3.13     | 1.32     | 1895     | 1        | 0.04     | <1       | 220      | 59       | 8.12     | 9        | 108      | 0.09     | 50       | 10       | 30       |
| 609159             |                          | 5.85     | 0.84     | 1410     | 3        | 0.09     | 4        | 400      | 75       | 3.82     | 8        | 139      | 0.15     | 40       | <10      | 22       |
| 609160             |                          | 4.46     | 3.31     | 1135     | 54       | 1.56     | 71       | 2220     | 33       | 1.15     | <5       | 1255     | 0.32     | 193      | 10       | 86       |
| 609161             |                          | 5.55     | 1.14     | 1830     | 3        | 0.07     | <1       | 420      | 46       | 3.88     | <5       | 164      | 0.15     | 47       | 10       | 25       |
| 609162             |                          | 5.82     | 0.70     | 1085     | 3        | 0.07     | <1       | 430      | 42       | 4.27     | 6        | 96       | 0.16     | 47       | <10      | 18       |
| 609163             |                          | 5.62     | 0.55     | 924      | 3        | 0.07     | <1       | 400      | 34       | 3.74     | 7        | 87       | 0.15     | 41       | <10      | 14       |
| 609164             |                          | 5.59     | 0.79     | 1360     | 3        | 0.07     | 1        | 400      | 36       | 3.14     | <5       | 115      | 0.15     | 45       | <10      | 20       |
| 609165             |                          | 5.64     | 0.45     | 710      | 3        | 0.07     | <1       | 380      | 29       | 3.44     | <5       | 93       | 0.15     | 40       | <10      | 11       |
| 609166             |                          | 5.60     | 0.41     | 640      | 3        | 0.07     | 1        | 390      | 23       | 3.50     | <5       | 82       | 0.15     | 36       | <10      | 10       |
| 609167             |                          | 5.39     | 0.50     | 625      | 2        | 0.07     | <1       | 390      | 25       | 3.10     | <5       | 87       | 0.14     | 40       | <10      | 19       |
| 609168             |                          | 5.16     | 0.68     | 1100     | 4        | 0.07     | <1       | 380      | 16       | 2.29     | <5       | 144      | 0.13     | 40       | <10      | 12       |
| 609169             |                          | 5.93     | 0.53     | 664      | 5        | 0.08     | <1       | 400      | 14       | 3.14     | 5        | 93       | 0.14     | 43       | 10       | 7        |
| 609170             |                          | 5.61     | 0.53     | 629      | 6        | 0.08     | <1       | 400      | 18       | 4.01     | <5       | 98       | 0.14     | 42       | <10      | 8        |
| 609171             |                          | 5.63     | 0.61     | 733      | 3        | 0.08     | <1       | 390      | 13       | 3.06     | <5       | 95       | 0.14     | 39       | <10      | 10       |
| 609172             |                          | 5.59     | 0.77     | 973      | 4        | 0.07     | <1       | 400      | 14       | 3.15     | <5       | 108      | 0.15     | 41       | <10      | 11       |
| 609173             |                          | 6.09     | 0.67     | 1005     | 4        | 0.08     | 1        | 450      | 12       | 2.62     | 5        | 178      | 0.16     | 43       | <10      | 8        |
| 609174             |                          | 6.84     | 0.62     | 1035     | 5        | 0.09     | <1       | 450      | 9        | 2.52     | <5       | 160      | 0.16     | 44       | <10      | 7        |
| 609175             |                          | 0.55     | 2.68     | 1895     | 3        | 1.10     | 88       | 190      | 5        | 2.90     | <5       | 63       | 0.17     | 106      | <10      | 145      |
| 609176             |                          | 6.36     | 0.55     | 830      | 4        | 0.08     | <1       | 430      | 28       | 2.43     | 5        | 138      | 0.16     | 41       | <10      | 15       |
| 609177             |                          | 6.06     | 0.48     | 664      | 5        | 0.07     | 2        | 470      | 22       | 2.59     | <5       | 108      | 0.17     | 46       | 10       | 18       |
| 609178             |                          | 5.56     | 0.48     | 616      | 4        | 0.08     | <1       | 460      | 11       | 2.61     | <5       | 99       | 0.18     | 47       | 10       | 8        |
| 609179             |                          | 6.40     | 0.53     | 779      | 6        | 0.08     | <1       | 430      | 23       | 3.48     | <5       | 96       | 0.16     | 49       | <10      | 12       |
| 609180             |                          | 6.39     | 0.54     | 800      | 6        | 0.09     | <1       | 450      | 14       | 2.28     | <5       | 97       | 0.16     | 44       | <10      | 10       |

Comments: ALL SECURITY CODES ARE IN PLACE





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To: GEOFINE EXPLORATION CONSULTANTS LTD.

49 NORMANDALE RD

UNIONVILLE ON L3R 4J8

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Finalized Date: 12-AUG-2004

Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04049585

| Sample Description                             | Method<br>Analyte<br>Units<br>LOR | Cu-AA62<br>Cu<br>%<br>0.01 |
|------------------------------------------------|-----------------------------------|----------------------------|
| 609141<br>609142<br>609143<br>609144<br>609145 |                                   | 2.34                       |
| 609146<br>609147<br>609148<br>609149<br>609150 |                                   | 1.12                       |
| 609151<br>609152<br>609153<br>609154<br>609155 |                                   |                            |
| 609156<br>609157<br>609158<br>609159<br>609160 |                                   |                            |
| 609161<br>609162<br>609163<br>609164<br>609165 |                                   |                            |
| 609166<br>609167<br>609168<br>609169<br>609170 |                                   |                            |
| 609171<br>609172<br>609173<br>609174<br>609175 |                                   |                            |
| 609176<br>609177<br>609178<br>609179<br>609180 |                                   |                            |

Comments: ALL SECURITY CODES ARE IN PLACE



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Project: Stewart

**CERTIFICATE OF ANALYSIS VA04049585**

| Sample Description | Method Analyte Units LOR | WEI-21       | Au-AA23 | Au-GRA21 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |      |
|--------------------|--------------------------|--------------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|------|
|                    |                          | Recvd Wt. kg | Au ppm  | Au ppm   | Ag ppm   | Al %     | As ppm   | Ba ppm   | Be ppm   | Bi ppm   | Ca %     | Cd ppm   | Co ppm   | Cr ppm   | Cu ppm   | Fe % |
|                    |                          | 0.02         | 0.005   | 0.05     | 0.5      | 0.01     | 5        | 10       | 0.5      | 2        | 0.01     | 0.5      | 1        | 1        | 1        | 0.01 |
| 609181             |                          | 1.34         | <0.005  |          | <0.5     | 7.14     | 43       | 290      | 0.6      | <2       | 1.14     | <0.5     | 4        | 80       | 12       | 3.42 |
| 609182             |                          | 1.62         | <0.005  |          | <0.5     | 8.49     | 50       | 250      | 0.7      | 3        | 1.80     | <0.5     | 5        | 47       | 14       | 4.74 |
| 609183             |                          | 1.82         | <0.005  |          | <0.5     | 7.49     | 37       | 370      | 0.6      | <2       | 1.72     | <0.5     | 3        | 65       | 11       | 3.33 |
| 609184             |                          | 1.88         | <0.005  |          | <0.5     | 6.71     | 37       | 560      | 0.5      | <2       | 0.79     | 0.5      | 3        | 46       | 7        | 2.59 |
| 609185             |                          | 2.00         | <0.005  |          | <0.5     | 7.76     | 34       | 580      | 0.7      | 3        | 0.99     | 0.6      | 4        | 59       | 8        | 3.32 |

Comments: ALL SECURITY CODES ARE IN PLACE



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Account: KIV

Project: Stewart

**CERTIFICATE OF ANALYSIS VA04049585**

| Sample Description | Method Analyte Units LOR | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |     |
|--------------------|--------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----|
|                    |                          | K        | Mg       | Mn       | Mo       | Na       | Ni       | P        | Pb       | S        | Sb       | Sr       | Ti       | V        | W        | Zn  |
|                    |                          | %        | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm |
|                    |                          | 0.01     | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2   |
| 609181             |                          | 6.72     | 0.48     | 674      | 5        | 0.09     | <1       | 480      | 14       | 2.60     | 5        | 100      | 0.17     | 42       | <10      | 10  |
| 609182             |                          | 6.99     | 0.77     | 1145     | 5        | 0.08     | <1       | 550      | 17       | 3.34     | 6        | 123      | 0.20     | 58       | <10      | 19  |
| 609183             |                          | 6.70     | 0.64     | 1055     | 6        | 0.09     | <1       | 540      | 13       | 2.26     | <5       | 107      | 0.18     | 47       | <10      | 11  |
| 609184             |                          | 6.44     | 0.32     | 473      | 3        | 0.09     | 3        | 460      | 10       | 2.02     | 6        | 98       | 0.17     | 37       | <10      | 9   |
| 609185             |                          | 6.17     | 0.46     | 630      | 3        | 0.09     | 3        | 590      | 30       | 2.37     | <5       | 88       | 0.19     | 50       | <10      | 13  |

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Account: KIV

Project: Stewart

**CERTIFICATE OF ANALYSIS VA04049585**

| Sample Description                             | Method<br>Analyte<br>Units<br>LOR | Cu-AA62<br>Cu<br>%<br>0.01 |
|------------------------------------------------|-----------------------------------|----------------------------|
| 609181<br>609182<br>609183<br>609184<br>609185 |                                   |                            |
|                                                |                                   |                            |

Comments: ALL SECURITY CODES ARE IN PLACE





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 Finalized Date: 12-AUG-2004  
 Account: KIV

Project: Stewart *Original 599606*

*SZ004-01*

**CERTIFICATE OF ANALYSIS VA04049586**

| Sample Description | Method Analyte Units LOR | WEI-21       | Au-AA23 | Au-GRA21 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |      |
|--------------------|--------------------------|--------------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|------|
|                    |                          | Recvd Wt. kg | Au ppm  | Au ppm   | Ag ppm   | Al %     | As ppm   | Ba ppm   | Be ppm   | Bi ppm   | Ca %     | Cd ppm   | Co ppm   | Cr ppm   | Cu ppm   | Fe % |
|                    |                          | 0.02         | 0.005   | 0.05     | 0.5      | 0.01     | 5        | 10       | 0.5      | 2        | 0.01     | 0.5      | 1        | 1        | 1        | 0.01 |
| 599568             |                          | 0.08         | 0.121   |          |          |          |          |          |          |          |          |          |          |          |          |      |
| 599569             |                          | 2.20         | <0.005  |          | <0.5     | 7.81     | 6        | 1810     | 0.7      | <2       | 2.24     | <0.5     | 5        | 16       | 118      | 3.56 |
| 599570             |                          | 1.02         | <0.005  |          | <0.5     | 5.71     | <5       | 2160     | 0.5      | <2       | 7.59     | <0.5     | 2        | 28       | 4        | 4.97 |
| 599571             |                          | 2.00         | <0.005  |          | <0.5     | 7.67     | <5       | 2050     | 0.6      | <2       | 2.06     | <0.5     | 1        | 6        | 20       | 3.24 |
| 599572             |                          | 1.44         | <0.005  |          | <0.5     | 7.49     | <5       | 2440     | 0.5      | <2       | 3.04     | <0.5     | <1       | 35       | 3        | 3.58 |
| 599573             |                          | 1.76         | <0.005  |          | <0.5     | 7.97     | <5       | 1680     | 0.7      | <2       | 2.82     | <0.5     | 2        | 4        | 7        | 3.39 |
| 599574             |                          | 2.08         | <0.005  |          | <0.5     | 7.67     | 8        | 940      | 0.9      | <2       | 2.49     | <0.5     | 2        | 26       | 2        | 2.82 |
| 599575             |                          | 1.74         | <0.005  |          | <0.5     | 7.78     | <5       | 900      | 0.9      | <2       | 2.56     | <0.5     | 2        | 3        | 13       | 2.66 |
| 599576             |                          | 1.72         | <0.005  |          | <0.5     | 7.43     | <5       | 1810     | 0.6      | <2       | 2.28     | <0.5     | 1        | 32       | 11       | 2.86 |
| 599577             |                          | 1.94         | <0.005  |          | <0.5     | 7.50     | 7        | 2180     | 0.7      | <2       | 2.36     | <0.5     | 2        | 3        | 5        | 3.08 |
| 599578             |                          | 2.10         | 0.014   |          | <0.5     | 8.04     | 12       | 1760     | 0.8      | <2       | 2.83     | <0.5     | 1        | 28       | 4        | 3.06 |
| 599579             |                          | 1.68         | <0.005  |          | <0.5     | 7.62     | <5       | 1150     | 0.6      | <2       | 3.01     | <0.5     | <1       | 4        | 3        | 3.23 |
| 599580             |                          | 1.66         | <0.005  |          | <0.5     | 8.11     | <5       | 1340     | 0.6      | <2       | 2.48     | <0.5     | 2        | 28       | 5        | 3.23 |
| 599581             |                          | 1.92         | <0.005  |          | <0.5     | 7.63     | <5       | 1690     | 0.5      | <2       | 2.55     | <0.5     | <1       | 4        | 3        | 3.34 |
| 599582             |                          | 1.74         | 0.006   |          | <0.5     | 7.09     | 42       | 1960     | <0.5     | <2       | 4.08     | <0.5     | 2        | 30       | 10       | 4.02 |
| 599583             |                          | 2.32         | <0.005  |          | <0.5     | 7.34     | 7        | 1260     | 0.5      | <2       | 2.47     | <0.5     | 1        | 5        | 4        | 3.20 |
| 599584             |                          | 0.08         | 2.75    |          |          |          |          |          |          |          |          |          |          |          |          |      |
| 599585             |                          | 1.84         | <0.005  |          | <0.5     | 7.33     | <5       | 1250     | <0.5     | <2       | 3.01     | 0.5      | 1        | 30       | 3        | 3.49 |
| 599586             |                          | 2.04         | <0.005  |          | <0.5     | 6.51     | <5       | 1540     | 0.5      | <2       | 3.88     | <0.5     | <1       | 4        | 12       | 3.61 |
| 599587             |                          | 1.84         | 0.038   |          | <0.5     | 7.12     | <5       | 1440     | 0.5      | <2       | 2.69     | <0.5     | 2        | 30       | 58       | 3.31 |
| 599588             |                          | 1.68         | 0.007   |          | <0.5     | 6.88     | 24       | 2170     | 0.5      | <2       | 1.84     | <0.5     | 4        | 4        | 94       | 3.78 |
| 599589             |                          | 1.70         | <0.005  |          | <0.5     | 5.83     | 12       | 3840     | <0.5     | <2       | 5.82     | <0.5     | 6        | 27       | 10       | 4.69 |
| 599590             |                          | 1.88         | 0.006   |          | <0.5     | 6.64     | 15       | 2650     | 0.5      | <2       | 3.47     | <0.5     | 3        | 5        | 11       | 4.74 |
| 599591             |                          | 1.70         | <0.005  |          | <0.5     | 5.92     | 18       | 2980     | <0.5     | <2       | 5.01     | <0.5     | 5        | 31       | 7        | 4.86 |
| 599592             |                          | 1.92         | 0.009   |          | <0.5     | 5.07     | 12       | 1320     | <0.5     | <2       | 9.14     | <0.5     | 4        | 3        | 14       | 5.89 |
| 599593             |                          | 1.82         | 0.005   |          | <0.5     | 6.03     | 26       | 1940     | <0.5     | <2       | 4.46     | <0.5     | 5        | 69       | 14       | 3.22 |
| 599594             |                          | 1.82         | 0.011   |          | <0.5     | 6.82     | 32       | 2420     | <0.5     | <2       | 1.34     | <0.5     | 3        | 78       | 64       | 1.72 |
| 599595             |                          | 1.76         | 0.016   |          | <0.5     | 6.73     | 46       | 2250     | <0.5     | <2       | 1.98     | 0.5      | 3        | 89       | 41       | 1.96 |
| 599596             |                          | 0.58         | 0.006   |          | <0.5     | 6.93     | 28       | 2370     | <0.5     | <2       | 1.10     | <0.5     | 3        | 57       | 24       | 1.56 |
| 599597             |                          | 2.02         | 0.038   |          | <0.5     | 6.39     | 127      | 570      | <0.5     | <2       | 1.60     | <0.5     | 9        | 56       | 283      | 2.66 |
| 599598             |                          | 1.80         | 0.017   |          | <0.5     | 7.43     | 73       | 2500     | 0.5      | <2       | 1.49     | <0.5     | 4        | 47       | 16       | 3.15 |
| 599599             |                          | 1.46         | 0.060   |          | <0.5     | 6.71     | 117      | 1210     | 0.5      | <2       | 1.68     | <0.5     | 8        | 51       | 285      | 3.21 |
| 599600             |                          | 0.08         | >10.0   | 15.80    |          |          |          |          |          |          |          |          |          |          |          |      |
| 599601             |                          | 0.94         | 3.51    |          | 0.8      | 6.53     | 346      | 190      | 0.5      | 3        | 1.02     | 0.5      | 11       | 48       | 991      | 3.71 |
| 599602             |                          | 2.04         | 0.061   |          | <0.5     | 7.82     | 132      | 1460     | 0.7      | <2       | 0.85     | <0.5     | 9        | 41       | 357      | 6.65 |
| 599603             |                          | 2.16         | 0.035   |          | <0.5     | 7.14     | 89       | 1140     | 0.6      | <2       | 0.90     | <0.5     | 9        | 36       | 125      | 6.38 |
| 599604             |                          | 1.94         | 0.152   |          | <0.5     | 6.57     | 166      | 140      | 0.6      | <2       | 0.79     | <0.5     | 11       | 33       | 3420     | 8.01 |
| 599605             |                          | 1.44         | 1.295   |          | <0.5     | 3.91     | 37       | 380      | 0.6      | <2       | 0.69     | <0.5     | 5        | 42       | 2890     | 5.84 |
| 599606             | X                        | 1.54         | 0.005   |          | 0.6      | 4.54     | 19       | 580      | 0.7      | <2       | 2.46     | 0.6      | 6        | 48       | 1770     | 4.60 |
| 599607             |                          | 1.96         | 0.064   |          | <0.5     | 6.64     | 5        | 6870     | 0.7      | <2       | 1.93     | <0.5     | 3        | 26       | 149      | 3.32 |

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To: GEOFINE EXPLORATION CONSULTANTS LTD.  
 49 NORMANDALE RD  
 UNIONVILLE ON L3R 4J8

Page: 2 - B  
 Total # Pages: 3 (A - B)  
 Finalized Date: 12-AUG-2004  
 Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04049586

| Sample Description | Method Analyte Units LOR | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |     |
|--------------------|--------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----|
|                    |                          | K        | Mg       | Mn       | Mo       | Na       | Ni       | P        | Pb       | S        | Sb       | Sr       | Ti       | V        | W        | Zn  |
|                    |                          | %        | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm |
|                    |                          | 0.01     | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2   |
| 599568             |                          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |     |
| 599569             |                          | 5.87     | 0.81     | 819      | 1        | 0.16     | 50       | 500      | 7        | 0.08     | 5        | 94       | 0.20     | 54       | <10      | 21  |
| 599570             |                          | 4.33     | 2.70     | 2390     | <1       | 0.09     | <1       | 360      | 2        | 0.04     | 8        | 183      | 0.13     | 63       | <10      | 41  |
| 599571             |                          | 5.84     | 0.70     | 735      | <1       | 0.10     | 9        | 510      | 2        | 0.02     | 5        | 99       | 0.19     | 52       | <10      | 27  |
| 599572             |                          | 6.45     | 0.96     | 1110     | <1       | 0.11     | 1        | 470      | <2       | 0.02     | <5       | 136      | 0.18     | 53       | 10       | 25  |
| 599573             |                          | 5.56     | 0.90     | 997      | <1       | 0.09     | 3        | 540      | 4        | 0.01     | <5       | 118      | 0.20     | 57       | <10      | 18  |
| 599574             |                          | 4.20     | 0.72     | 756      | 1        | 0.05     | 1        | 560      | <2       | 0.02     | <5       | 116      | 0.21     | 55       | <10      | 15  |
| 599575             |                          | 4.33     | 0.65     | 804      | 1        | 0.30     | 3        | 550      | 9        | 0.01     | 6        | 140      | 0.20     | 52       | <10      | 14  |
| 599576             |                          | 5.39     | 0.66     | 822      | 10       | 0.58     | 7        | 460      | 6        | 0.03     | 6        | 131      | 0.18     | 60       | <10      | 18  |
| 599577             |                          | 5.18     | 0.80     | 796      | 2        | 0.12     | 3        | 510      | <2       | 0.03     | 7        | 109      | 0.19     | 63       | <10      | 15  |
| 599578             |                          | 4.80     | 0.98     | 953      | 1        | 0.08     | 2        | 540      | 3        | 0.03     | <5       | 101      | 0.20     | 79       | <10      | 13  |
| 599579             |                          | 5.10     | 1.05     | 1095     | <1       | 0.09     | 1        | 500      | <2       | <0.01    | <5       | 99       | 0.19     | 60       | <10      | 12  |
| 599580             |                          | 5.42     | 0.92     | 941      | <1       | 0.09     | 3        | 550      | 4        | 0.01     | 5        | 95       | 0.20     | 58       | <10      | 14  |
| 599581             |                          | 5.64     | 0.89     | 858      | 1        | 0.11     | 1        | 520      | 3        | 0.01     | 5        | 105      | 0.19     | 57       | <10      | 17  |
| 599582             |                          | 5.28     | 1.43     | 1415     | 5        | 0.11     | 2        | 460      | 3        | 0.41     | <5       | 126      | 0.17     | 67       | 10       | 20  |
| 599583             |                          | 5.30     | 0.97     | 958      | 1        | 0.09     | 4        | 510      | <2       | <0.01    | <5       | 82       | 0.18     | 55       | <10      | 18  |
| 599584             |                          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |     |
| 599585             |                          | 5.14     | 1.12     | 1045     | <1       | 0.11     | 4        | 480      | 3        | <0.01    | 5        | 80       | 0.18     | 57       | <10      | 17  |
| 599586             |                          | 3.79     | 1.36     | 1370     | <1       | 0.07     | 5        | 410      | 8        | 0.04     | <5       | 95       | 0.17     | 58       | <10      | 31  |
| 599587             |                          | 4.44     | 0.91     | 960      | <1       | 0.06     | 2        | 450      | 6        | 0.03     | <5       | 81       | 0.17     | 57       | <10      | 16  |
| 599588             |                          | 5.40     | 0.64     | 738      | <1       | 0.08     | <1       | 420      | 3        | 0.23     | <5       | 92       | 0.17     | 52       | 10       | 24  |
| 599589             |                          | 4.67     | 1.21     | 2410     | 2        | 0.09     | 2        | 360      | 10       | 0.12     | 9        | 237      | 0.14     | 73       | <10      | 62  |
| 599590             |                          | 5.62     | 0.55     | 1830     | 1        | 0.09     | <1       | 410      | 7        | 0.24     | 7        | 114      | 0.17     | 60       | <10      | 42  |
| 599591             |                          | 5.07     | 1.33     | 2070     | <1       | 0.10     | 2        | 350      | 9        | 0.21     | <5       | 218      | 0.14     | 63       | <10      | 38  |
| 599592             |                          | 4.01     | 2.03     | 2650     | <1       | 0.08     | <1       | 300      | 3        | 0.21     | <5       | 253      | 0.11     | 83       | <10      | 47  |
| 599593             |                          | 5.59     | 1.01     | 1525     | <1       | 0.10     | 1        | 370      | 5        | 0.19     | <5       | 197      | 0.15     | 48       | <10      | 20  |
| 599594             |                          | 6.10     | 0.38     | 444      | 1        | 0.10     | 3        | 440      | 6        | 0.25     | <5       | 116      | 0.17     | 45       | <10      | 5   |
| 599595             |                          | 6.10     | 0.46     | 667      | <1       | 0.10     | 2        | 430      | 5        | 0.43     | <5       | 146      | 0.17     | 39       | <10      | 5   |
| 599596             |                          | 5.80     | 0.27     | 477      | <1       | 0.10     | 4        | 450      | 5        | 0.28     | <5       | 93       | 0.18     | 34       | <10      | 4   |
| 599597             |                          | 5.33     | 0.40     | 484      | 1        | 0.09     | <1       | 430      | 10       | 2.01     | <5       | 132      | 0.16     | 27       | 10       | 4   |
| 599598             |                          | 5.81     | 0.38     | 811      | 1        | 0.11     | 1        | 480      | 8        | 0.66     | 5        | 131      | 0.19     | 47       | 10       | 9   |
| 599599             |                          | 5.87     | 0.48     | 757      | <1       | 0.09     | 1        | 430      | 7        | 1.67     | <5       | 100      | 0.16     | 40       | <10      | 9   |
| 599600             |                          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |     |
| 599601             |                          | 5.58     | 0.22     | 416      | 2        | 0.10     | 2        | 450      | 17       | 2.86     | <5       | 97       | 0.16     | 35       | <10      | 7   |
| 599602             |                          | 5.76     | 0.53     | 1840     | <1       | 0.08     | 2        | 470      | 7        | 1.85     | 5        | 75       | 0.20     | 52       | 10       | 18  |
| 599603             |                          | 5.31     | 0.44     | 1735     | <1       | 0.08     | 3        | 480      | 5        | 2.01     | <5       | 71       | 0.19     | 53       | 10       | 18  |
| 599604             |                          | 4.76     | 0.46     | 1785     | 6        | 0.05     | 2        | 460      | 11       | 3.86     | <5       | 53       | 0.19     | 64       | 10       | 18  |
| 599605             |                          | 1.88     | 0.23     | 1920     | 1        | 0.03     | 2        | 230      | <2       | 0.78     | <5       | 40       | 0.09     | 34       | 40       | 10  |
| 599606             |                          | 2.22     | 0.45     | 2210     | <1       | 0.03     | <1       | 280      | 7        | 0.30     | <5       | 106      | 0.11     | 41       | <10      | 18  |
| 599607             |                          | 5.79     | 0.35     | 1050     | <1       | 0.13     | 2        | 430      | 6        | 0.25     | <5       | 379      | 0.17     | 46       | <10      | 12  |

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To: GEOFINE EXPLORATION CONSULTANTS LTD.  
 49 NORMANDALE RD  
 UNIONVILLE ON L3R 4J8

Page: 3 - A  
 Total # Pages: 3 (A - B)  
 Finalized Date: 12-AUG-2004  
 Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04049586

| Sample Description | Method Analyte Units LOR | WEI-21    | Au-AA23 | Au-GRA21 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |      |
|--------------------|--------------------------|-----------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|------|
|                    |                          | Recvd Wt. | Au      | Au       | Ag       | Al       | As       | Ba       | Be       | Bi       | Ca       | Cd       | Co       | Cr       | Cu       | Fe   |
|                    |                          | kg        | ppm     | ppm      | ppm      | %        | ppm      | ppm      | ppm      | ppm      | %        | ppm      | ppm      | ppm      | ppm      | %    |
|                    |                          | 0.02      | 0.005   | 0.05     | 0.5      | 0.01     | 5        | 10       | 0.5      | 2        | 0.01     | 0.5      | 1        | 1        | 1        | 0.01 |
| 599608             |                          | 1.98      | 0.019   |          | <0.5     | 6.91     | 11       | 3900     | 0.7      | <2       | 1.25     | <0.5     | 2        | 29       | 130      | 3.14 |
| 599609             |                          | 1.64      | 0.009   |          | <0.5     | 6.60     | <5       | 3640     | 0.6      | <2       | 1.80     | <0.5     | 1        | 31       | 23       | 2.03 |
| 599610             |                          | 2.16      | 0.022   |          | <0.5     | 6.68     | 8        | 2570     | 0.7      | <2       | 1.98     | <0.5     | 2        | 29       | 25       | 2.47 |
| 599611             |                          | 2.10      | 0.009   |          | <0.5     | 6.74     | <5       | 6530     | 0.6      | <2       | 1.72     | <0.5     | 3        | 40       | 309      | 2.98 |
| 599612             |                          | 1.72      | <0.005  |          | <0.5     | 6.39     | 12       | 4550     | 0.6      | <2       | 2.38     | <0.5     | 2        | 30       | 50       | 2.79 |
| 599613             |                          | 1.98      | <0.005  |          | <0.5     | 6.20     | 17       | 2520     | 0.7      | <2       | 1.71     | 0.5      | 2        | 42       | 229      | 1.81 |
| 599614             |                          | 2.00      | 0.081   |          | <0.5     | 5.86     | <5       | 2270     | 0.6      | <2       | 1.49     | <0.5     | 4        | 36       | 1400     | 2.27 |
| 599615             |                          | 0.10      | >10.0   | 16.25    |          |          |          |          |          |          |          |          |          |          |          |      |
| 599616             |                          | 1.70      | 0.013   |          | <0.5     | 6.01     | <5       | 2540     | 0.7      | <2       | 1.86     | <0.5     | 3        | 32       | 53       | 2.80 |
| 599617             |                          | 1.90      | <0.005  |          | <0.5     | 5.91     | 10       | 2930     | 0.6      | <2       | 1.95     | 0.7      | 2        | 25       | 168      | 2.36 |
| 599618             |                          | 2.10      | 0.029   |          | <0.5     | 6.74     | <5       | 2600     | 0.6      | <2       | 1.98     | <0.5     | 2        | 32       | 11       | 3.18 |
| 599619             |                          | 1.78      | 0.005   |          | <0.5     | 6.58     | <5       | 2360     | 0.7      | <2       | 1.76     | <0.5     | 3        | 27       | 84       | 2.95 |
| 599620             |                          | 1.62      | <0.005  |          | <0.5     | 6.81     | 6        | 2150     | 0.6      | <2       | 1.36     | <0.5     | 3        | 43       | 13       | 3.56 |
| 599621             |                          | 1.90      | 0.015   |          | 5.0      | 6.09     | 9        | 2080     | 0.6      | <2       | 3.33     | 1.5      | 2        | 26       | 106      | 3.05 |
| 599622             |                          | 1.66      | 0.012   |          | 14.4     | 7.45     | 43       | 1360     | 0.9      | <2       | 1.26     | 1.2      | 3        | 17       | 132      | 2.97 |
| 599623             |                          | 1.22      | 0.009   |          | 3.8      | 6.53     | 25       | 4340     | 0.7      | <2       | 2.84     | 1.0      | 2        | 24       | 53       | 2.52 |
| 599624             |                          | 1.98      | 0.009   |          | 18.2     | 7.47     | 35       | 2640     | 0.9      | <2       | 1.60     | 3.0      | 3        | 31       | 251      | 2.03 |

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|--------------------|-----------------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----|
|                    |                                   | K        | Mg       | Mn       | Mo       | Na       | Ni       | P        | Pb       | S        | Sb       | Sr       | Ti       | V        | W        | Zn  |
|                    |                                   | %        | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm |
|                    |                                   | 0.01     | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2   |
| 599608             |                                   | 5.87     | 0.27     | 935      | <1       | 0.11     | 1        | 450      | 3        | 0.17     | <5       | 172      | 0.17     | 44       | <10      | 10  |
| 599609             |                                   | 6.45     | 0.21     | 644      | 1        | 0.12     | <1       | 410      | <2       | 0.05     | <5       | 200      | 0.18     | 45       | <10      | 6   |
| 599610             |                                   | 6.18     | 0.32     | 997      | 4        | 0.10     | 7        | 440      | 3        | 0.02     | 7        | 142      | 0.18     | 45       | <10      | 14  |
| 599611             |                                   | 6.06     | 0.32     | 1100     | 2        | 0.13     | 3        | 420      | 3        | 0.21     | <5       | 315      | 0.17     | 44       | <10      | 10  |
| 599612             |                                   | 6.55     | 0.31     | 1180     | 1        | 0.13     | 3        | 410      | 5        | 0.08     | <5       | 198      | 0.17     | 47       | <10      | 9   |
| 599613             |                                   | 6.28     | 0.13     | 637      | 1        | 0.11     | 1        | 470      | 5        | 0.08     | <5       | 168      | 0.19     | 47       | 10       | 6   |
| 599614             |                                   | 5.27     | 0.15     | 950      | 1        | 0.11     | <1       | 380      | 4        | 0.27     | 8        | 165      | 0.16     | 40       | <10      | 7   |
| 599615             |                                   |          |          |          |          |          |          |          |          |          |          |          |          |          |          |     |
| 599616             |                                   | 6.46     | 0.14     | 1040     | 1        | 0.14     | 4        | 400      | 4        | 0.02     | 5        | 164      | 0.18     | 49       | <10      | 11  |
| 599617             |                                   | 6.33     | 0.13     | 899      | 1        | 0.17     | 2        | 400      | 3        | 0.08     | <5       | 223      | 0.17     | 45       | <10      | 9   |
| 599618             |                                   | 6.67     | 0.23     | 1090     | <1       | 0.24     | 3        | 460      | 6        | 0.01     | <5       | 196      | 0.18     | 52       | <10      | 10  |
| 599619             |                                   | 6.32     | 0.20     | 1105     | 1        | 0.13     | 2        | 440      | 2        | 0.07     | <5       | 170      | 0.18     | 47       | <10      | 12  |
| 599620             |                                   | 5.97     | 0.28     | 1515     | <1       | 0.11     | 2        | 410      | 2        | 0.01     | <5       | 106      | 0.16     | 43       | <10      | 15  |
| 599621             |                                   | 4.70     | 0.50     | 1325     | 1        | 0.08     | 1        | 380      | 14       | 0.04     | 59       | 124      | 0.15     | 46       | <10      | 61  |
| 599622             |                                   | 3.92     | 0.23     | 918      | 1        | 0.04     | 3        | 460      | 24       | 0.24     | 73       | 161      | 0.19     | 49       | <10      | 87  |
| 599623             |                                   | 4.76     | 0.21     | 1080     | <1       | 0.12     | 1        | 450      | 8        | 0.16     | 36       | 394      | 0.17     | 44       | 10       | 48  |
| 599624             |                                   | 4.80     | 0.16     | 680      | <1       | 0.17     | 3        | 500      | 315      | 0.14     | 154      | 231      | 0.19     | 50       | <10      | 142 |

Comments: ALL SECURITY CODES ARE IN PLACE.





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To: GEOFINE EXPLORATION CONSULTANTS LTD.  
 49 NORMANDALE RD  
 UNIONVILLE ON L3R 4J8

Page: 2 - A  
 Total # Pages: 3 (A - B)  
 Finalized Date: 12-AUG-2004  
 Account: KIV

Project: Stewart Corrected 599606 S21004-01

**CERTIFICATE OF ANALYSIS VA04049586**

| Sample Description | Method Analyte Units LOR | WEI-21       | Au-AA23 | Au-GRA21 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|--------------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | Recvd Wt. kg | Au ppm  | Au ppm   | Ag ppm   | Al %     | As ppm   | Ba ppm   | Be ppm   | Bi ppm   | Ca %     | Cd ppm   | Ce ppm   | Cr ppm   | Cu ppm   | Fe %     |
| 599568             |                          | 0.08         | 0.121   |          |          |          |          |          |          |          |          |          |          |          |          |          |
| 599569             |                          | 2.20         | <0.005  |          | <0.5     | 7.81     | 6        | 1810     | 0.7      | <2       | 2.24     | <0.5     | 5        | 16       | 118      | 3.56     |
| 599570             |                          | 1.02         | <0.005  |          | <0.5     | 5.71     | <5       | 2160     | 0.5      | <2       | 7.59     | <0.5     | 2        | 28       | 4        | 4.97     |
| 599571             |                          | 2.00         | <0.005  |          | <0.5     | 7.67     | <5       | 2050     | 0.6      | <2       | 2.06     | <0.5     | 1        | 6        | 20       | 3.24     |
| 599572             |                          | 1.44         | <0.005  |          | <0.5     | 7.49     | <5       | 2440     | 0.5      | <2       | 3.04     | <0.5     | <1       | 35       | 3        | 3.58     |
| 599573             |                          | 1.76         | <0.005  |          | <0.5     | 7.97     | <5       | 1680     | 0.7      | <2       | 2.82     | <0.5     | 2        | 4        | 7        | 3.39     |
| 599574             |                          | 2.08         | <0.005  |          | <0.5     | 7.67     | 8        | 940      | 0.9      | <2       | 2.49     | <0.5     | 2        | 26       | 2        | 2.82     |
| 599575             |                          | 1.74         | <0.005  |          | <0.5     | 7.78     | <5       | 900      | 0.9      | <2       | 2.56     | <0.5     | 2        | 3        | 13       | 2.66     |
| 599576             |                          | 1.72         | <0.005  |          | <0.5     | 7.43     | <5       | 1810     | 0.6      | <2       | 2.28     | <0.5     | 1        | 32       | 11       | 2.86     |
| 599577             |                          | 1.94         | <0.005  |          | <0.5     | 7.50     | 7        | 2180     | 0.7      | <2       | 2.36     | <0.5     | 2        | 3        | 5        | 3.08     |
| 599578             |                          | 2.10         | 0.014   |          | <0.5     | 8.04     | 12       | 1760     | 0.8      | <2       | 2.83     | <0.5     | 1        | 28       | 4        | 3.06     |
| 599579             |                          | 1.68         | <0.005  |          | <0.5     | 7.62     | <5       | 1150     | 0.6      | <2       | 3.01     | <0.5     | <1       | 4        | 3        | 3.23     |
| 599580             |                          | 1.66         | <0.005  |          | <0.5     | 8.11     | <5       | 1340     | 0.6      | <2       | 2.48     | <0.5     | 2        | 28       | 5        | 3.23     |
| 599581             |                          | 1.92         | <0.005  |          | <0.5     | 7.63     | <5       | 1690     | 0.5      | <2       | 2.55     | <0.5     | <1       | 4        | 3        | 3.34     |
| 599582             |                          | 1.74         | 0.006   |          | <0.5     | 7.09     | 42       | 1960     | <0.5     | <2       | 4.08     | <0.5     | 2        | 30       | 10       | 4.02     |
| 599583             |                          | 2.32         | <0.005  |          | <0.5     | 7.34     | 7        | 1260     | 0.5      | <2       | 2.47     | <0.5     | 1        | 5        | 4        | 3.20     |
| 599584             |                          | 0.08         | 2.75    |          |          |          |          |          |          |          |          |          |          |          |          |          |
| 599585             |                          | 1.84         | <0.005  |          | <0.5     | 7.33     | <5       | 1250     | <0.5     | <2       | 3.01     | 0.5      | 1        | 30       | 3        | 3.49     |
| 599586             |                          | 2.04         | <0.005  |          | <0.5     | 6.51     | <5       | 1540     | 0.5      | <2       | 3.88     | <0.5     | <1       | 4        | 12       | 3.61     |
| 599587             |                          | 1.84         | 0.038   |          | <0.5     | 7.12     | <5       | 1440     | 0.5      | <2       | 2.69     | <0.5     | 2        | 30       | 58       | 3.31     |
| 599588             |                          | 1.68         | 0.007   |          | <0.5     | 6.88     | 24       | 2170     | 0.5      | <2       | 1.84     | <0.5     | 4        | 4        | 94       | 3.78     |
| 599589             |                          | 1.70         | <0.005  |          | <0.5     | 5.83     | 12       | 3840     | <0.5     | <2       | 5.82     | <0.5     | 6        | 27       | 10       | 4.69     |
| 599590             |                          | 1.88         | 0.006   |          | <0.5     | 6.64     | 15       | 2650     | 0.5      | <2       | 3.47     | <0.5     | 3        | 5        | 11       | 4.74     |
| 599591             |                          | 1.70         | <0.005  |          | <0.5     | 5.92     | 18       | 2980     | <0.5     | <2       | 5.01     | <0.5     | 5        | 31       | 7        | 4.86     |
| 599592             |                          | 1.92         | 0.009   |          | <0.5     | 5.07     | 12       | 1320     | <0.5     | <2       | 9.14     | <0.5     | 4        | 3        | 14       | 5.89     |
| 599593             |                          | 1.82         | 0.005   |          | <0.5     | 6.03     | 26       | 1940     | <0.5     | <2       | 4.46     | <0.5     | 5        | 69       | 14       | 3.22     |
| 599594             |                          | 1.82         | 0.011   |          | <0.5     | 6.82     | 32       | 2420     | <0.5     | <2       | 1.34     | <0.5     | 3        | 78       | 64       | 1.72     |
| 599595             |                          | 1.76         | 0.016   |          | <0.5     | 6.73     | 46       | 2250     | <0.5     | <2       | 1.98     | 0.5      | 3        | 89       | 41       | 1.96     |
| 599596             |                          | 0.58         | 0.006   |          | <0.5     | 6.93     | 28       | 2370     | <0.5     | <2       | 1.10     | <0.5     | 3        | 57       | 24       | 1.56     |
| 599597             |                          | 2.02         | 0.038   |          | <0.5     | 6.39     | 127      | 570      | <0.5     | <2       | 1.60     | <0.5     | 9        | 56       | 283      | 2.66     |
| 599598             |                          | 1.80         | 0.017   |          | <0.5     | 7.43     | 73       | 2500     | 0.5      | <2       | 1.49     | <0.5     | 4        | 47       | 16       | 3.15     |
| 599599             |                          | 1.46         | 0.060   |          | <0.5     | 6.71     | 117      | 1210     | 0.5      | <2       | 1.68     | <0.5     | 8        | 51       | 285      | 3.21     |
| 599600             |                          | 0.08         | >10.0   | 15.80    |          |          |          |          |          |          |          |          |          |          |          |          |
| 599601             |                          | 0.94         | 3.51    |          | 0.8      | 6.53     | 346      | 190      | 0.5      | 3        | 1.02     | 0.5      | 11       | 48       | 991      | 3.71     |
| 599602             |                          | 2.04         | 0.061   |          | <0.5     | 7.82     | 132      | 1460     | 0.7      | <2       | 0.85     | <0.5     | 9        | 41       | 357      | 6.65     |
| 599603             |                          | 2.16         | 0.035   |          | <0.5     | 7.14     | 89       | 1140     | 0.6      | <2       | 0.90     | <0.5     | 9        | 36       | 125      | 6.38     |
| 599604             |                          | 1.94         | 0.152   |          | <0.5     | 6.57     | 166      | 140      | 0.6      | <2       | 0.79     | <0.5     | 11       | 33       | 3420     | 8.01     |
| 599605             |                          | 1.44         | 1.295   |          | <0.5     | 3.91     | 37       | 380      | 0.6      | <2       | 0.69     | <0.5     | 5        | 42       | 2890     | 5.84     |
| 599606             |                          | 1.54         | 2.58    |          | 0.6      | 4.54     | 19       | 580      | 0.7      | <2       | 2.46     | 0.6      | 6        | 48       | 1770     | 4.60     |
| 599607             |                          | 1.96         | 0.064   |          | <0.5     | 6.64     | 5        | 6870     | 0.7      | <2       | 1.93     | <0.5     | 3        | 26       | 149      | 3.32     |

Comments: ALL SECURITY CODES ARE IN PLACE.  
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 49 NORMANDALE RD  
 UNIONVILLE ON L3R 4J8

Page: 2 - B  
 Total # Pages: 3 (A - B)  
 Finalized Date: 12-AUG-2004  
 Account: KIV

Project: Stewart

**CERTIFICATE OF ANALYSIS VA04049586**

| Sample Description | Method Analyte Unks LOR | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |        |
|--------------------|-------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|--------|
|                    |                         | K %      | Mg %     | Mn ppm   | Mo ppm   | Na %     | Ni ppm   | P ppm    | Pb ppm   | S %      | Sb ppm   | Sr ppm   | Ti %     | V ppm    | W ppm    | Zn ppm |
|                    |                         | 0.01     | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2      |
| 599568             |                         |          |          |          |          |          |          |          |          |          |          |          |          |          |          |        |
| 599569             |                         | 5.87     | 0.81     | 819      | 1        | 0.16     | 50       | 500      | 7        | 0.08     | 5        | 94       | 0.20     | 54       | <10      | 21     |
| 599570             |                         | 4.33     | 2.70     | 2390     | <1       | 0.09     | <1       | 360      | 2        | 0.04     | 8        | 183      | 0.13     | 63       | <10      | 41     |
| 599571             |                         | 5.84     | 0.70     | 735      | <1       | 0.10     | 9        | 510      | 2        | 0.02     | 5        | 99       | 0.19     | 52       | <10      | 27     |
| 599572             |                         | 6.45     | 0.96     | 1110     | <1       | 0.11     | 1        | 470      | <2       | 0.02     | <5       | 136      | 0.18     | 53       | 10       | 25     |
| 599573             |                         | 5.56     | 0.90     | 997      | <1       | 0.09     | 3        | 540      | 4        | 0.01     | <5       | 118      | 0.20     | 57       | <10      | 18     |
| 599574             |                         | 4.20     | 0.72     | 756      | 1        | 0.05     | 1        | 560      | <2       | 0.02     | <5       | 116      | 0.21     | 55       | <10      | 15     |
| 599575             |                         | 4.33     | 0.65     | 804      | 1        | 0.30     | 3        | 550      | 9        | 0.01     | 6        | 140      | 0.20     | 52       | <10      | 14     |
| 599576             |                         | 5.39     | 0.66     | 822      | 10       | 0.58     | 7        | 460      | 6        | 0.03     | 6        | 131      | 0.18     | 60       | <10      | 18     |
| 599577             |                         | 5.18     | 0.80     | 796      | 2        | 0.12     | 3        | 510      | <2       | 0.03     | 7        | 109      | 0.19     | 63       | <10      | 15     |
| 599578             |                         | 4.80     | 0.98     | 953      | 1        | 0.08     | 2        | 540      | 3        | 0.03     | <5       | 101      | 0.20     | 79       | <10      | 13     |
| 599579             |                         | 5.10     | 1.05     | 1095     | <1       | 0.09     | 1        | 500      | <2       | <0.01    | <5       | 99       | 0.19     | 60       | <10      | 12     |
| 599580             |                         | 5.42     | 0.92     | 941      | <1       | 0.09     | 3        | 550      | 4        | 0.01     | 5        | 95       | 0.20     | 58       | <10      | 14     |
| 599581             |                         | 5.64     | 0.89     | 858      | 1        | 0.11     | 1        | 520      | 3        | 0.01     | 5        | 105      | 0.19     | 57       | <10      | 17     |
| 599582             |                         | 5.28     | 1.43     | 1415     | 5        | 0.11     | 2        | 460      | 3        | 0.41     | <5       | 126      | 0.17     | 67       | 10       | 20     |
| 599583             |                         | 5.30     | 0.97     | 958      | 1        | 0.09     | 4        | 510      | <2       | <0.01    | <5       | 82       | 0.18     | 55       | <10      | 18     |
| 599584             |                         |          |          |          |          |          |          |          |          |          |          |          |          |          |          |        |
| 599585             |                         | 5.14     | 1.12     | 1045     | <1       | 0.11     | 4        | 480      | 3        | <0.01    | 5        | 80       | 0.18     | 57       | <10      | 17     |
| 599586             |                         | 3.79     | 1.36     | 1370     | <1       | 0.07     | 5        | 410      | 8        | 0.04     | <5       | 95       | 0.17     | 58       | <10      | 31     |
| 599587             |                         | 4.44     | 0.91     | 960      | <1       | 0.06     | 2        | 450      | 6        | 0.03     | <5       | 81       | 0.17     | 57       | <10      | 16     |
| 599588             |                         | 5.40     | 0.64     | 738      | <1       | 0.08     | <1       | 420      | 3        | 0.23     | <5       | 92       | 0.17     | 52       | 10       | 24     |
| 599589             |                         | 4.67     | 1.21     | 2410     | 2        | 0.09     | 2        | 360      | 10       | 0.12     | 9        | 237      | 0.14     | 73       | <10      | 62     |
| 599590             |                         | 5.62     | 0.55     | 1830     | 1        | 0.09     | <1       | 410      | 7        | 0.24     | 7        | 114      | 0.17     | 60       | <10      | 42     |
| 599591             |                         | 5.07     | 1.33     | 2070     | <1       | 0.10     | 2        | 350      | 9        | 0.21     | <5       | 218      | 0.14     | 63       | <10      | 38     |
| 599592             |                         | 4.01     | 2.03     | 2650     | <1       | 0.08     | <1       | 300      | 3        | 0.21     | <5       | 253      | 0.11     | 83       | <10      | 47     |
| 599593             |                         | 5.59     | 1.01     | 1525     | <1       | 0.10     | 1        | 370      | 5        | 0.19     | <5       | 197      | 0.15     | 48       | <10      | 20     |
| 599594             |                         | 6.10     | 0.38     | 444      | 1        | 0.10     | 3        | 440      | 6        | 0.25     | <5       | 116      | 0.17     | 45       | <10      | 5      |
| 599595             |                         | 6.10     | 0.46     | 667      | <1       | 0.10     | 2        | 430      | 5        | 0.43     | <5       | 146      | 0.17     | 39       | <10      | 5      |
| 599596             |                         | 5.80     | 0.27     | 477      | <1       | 0.10     | 4        | 450      | 5        | 0.28     | <5       | 93       | 0.18     | 34       | <10      | 4      |
| 599597             |                         | 5.33     | 0.40     | 484      | 1        | 0.09     | <1       | 430      | 10       | 2.01     | <5       | 132      | 0.16     | 27       | 10       | 4      |
| 599598             |                         | 5.81     | 0.38     | 811      | 1        | 0.11     | 1        | 480      | 8        | 0.66     | 5        | 131      | 0.19     | 47       | 10       | 9      |
| 599599             |                         | 5.87     | 0.48     | 757      | <1       | 0.09     | 1        | 430      | 7        | 1.67     | <5       | 100      | 0.16     | 40       | <10      | 9      |
| 599600             |                         |          |          |          |          |          |          |          |          |          |          |          |          |          |          |        |
| 599601             |                         | 5.58     | 0.22     | 416      | 2        | 0.10     | 2        | 450      | 17       | 2.86     | <5       | 97       | 0.16     | 35       | <10      | 7      |
| 599602             |                         | 5.76     | 0.53     | 1840     | <1       | 0.08     | 2        | 470      | 7        | 1.85     | 5        | 75       | 0.20     | 52       | 10       | 18     |
| 599603             |                         | 5.31     | 0.44     | 1735     | <1       | 0.08     | 3        | 480      | 5        | 2.01     | <5       | 71       | 0.19     | 53       | 10       | 18     |
| 599604             |                         | 4.76     | 0.46     | 1785     | 6        | 0.05     | 2        | 460      | 11       | 3.86     | <5       | 53       | 0.19     | 64       | 10       | 18     |
| 599605             |                         | 1.88     | 0.23     | 1920     | 1        | 0.03     | 2        | 230      | <2       | 0.78     | <5       | 40       | 0.09     | 34       | 40       | 10     |
| 599606             |                         | 2.22     | 0.45     | 2210     | <1       | 0.03     | <1       | 280      | 7        | 0.30     | <5       | 106      | 0.11     | 41       | <10      | 18     |
| 599607             |                         | 5.79     | 0.35     | 1050     | <1       | 0.13     | 2        | 430      | 6        | 0.25     | <5       | 379      | 0.17     | 46       | <10      | 12     |

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 UNIONVILLE ON L3R 4J8

Page: 3 - A  
 Total # Pages: 3 (A - B)  
 Finalized Date: 12-AUG-2004  
 Account: KIV

Project: Stewart

**CERTIFICATE OF ANALYSIS VA04049586**

| Sample Description | Method Analyte Units LOR | WEI-21 Recvd Wt. kg | Au-AA23 Au ppm | Au-GRA21 Au ppm | ME-ICP61 Ag ppm | ME-ICP61 Al % | ME-ICP61 As ppm | ME-ICP61 Ba ppm | ME-ICP61 Be ppm | ME-ICP61 Bi ppm | ME-ICP61 Ca % | ME-ICP61 Cd ppm | ME-ICP61 Co ppm | ME-ICP61 Cr ppm | ME-ICP61 Cu ppm | ME-ICP61 Fe % |
|--------------------|--------------------------|---------------------|----------------|-----------------|-----------------|---------------|-----------------|-----------------|-----------------|-----------------|---------------|-----------------|-----------------|-----------------|-----------------|---------------|
|                    |                          | 0.02                | 0.005          | 0.05            | 0.5             | 0.01          | 5               | 10              | 0.5             | 2               | 0.01          | 0.5             | 1               | 1               | 1               | 0.01          |
| 599608             |                          | 1.98                | 0.019          |                 | <0.5            | 6.91          | 11              | 3900            | 0.7             | <2              | 1.25          | <0.5            | 2               | 29              | 130             | 3.14          |
| 599609             |                          | 1.64                | 0.009          |                 | <0.5            | 6.60          | <5              | 3640            | 0.6             | <2              | 1.80          | <0.5            | 1               | 31              | 23              | 2.03          |
| 599610             |                          | 2.16                | 0.022          |                 | <0.5            | 6.68          | 8               | 2570            | 0.7             | <2              | 1.98          | <0.5            | 2               | 29              | 25              | 2.47          |
| 599611             |                          | 2.10                | 0.009          |                 | <0.5            | 6.74          | <5              | 6530            | 0.6             | <2              | 1.72          | <0.5            | 3               | 40              | 309             | 2.98          |
| 599612             |                          | 1.72                | <0.005         |                 | <0.5            | 6.39          | 12              | 4550            | 0.6             | <2              | 2.38          | <0.5            | 2               | 30              | 50              | 2.79          |
| 599613             |                          | 1.98                | <0.005         |                 | <0.5            | 6.20          | 17              | 2520            | 0.7             | <2              | 1.71          | 0.5             | 2               | 42              | 229             | 1.81          |
| 599614             |                          | 2.00                | 0.081          |                 | <0.5            | 5.86          | <5              | 2270            | 0.6             | <2              | 1.49          | <0.5            | 4               | 36              | 1400            | 2.27          |
| 599615             |                          | 0.10                | >10.0          | 16.25           |                 |               |                 |                 |                 |                 |               |                 |                 |                 |                 |               |
| 599616             |                          | 1.70                | 0.013          |                 | <0.5            | 6.01          | <5              | 2540            | 0.7             | <2              | 1.86          | <0.5            | 3               | 32              | 53              | 2.80          |
| 599617             |                          | 1.90                | <0.005         |                 | <0.5            | 5.91          | 10              | 2930            | 0.6             | <2              | 1.95          | 0.7             | 2               | 25              | 168             | 2.36          |
| 599618             |                          | 2.10                | 0.029          |                 | <0.5            | 6.74          | <5              | 2600            | 0.6             | <2              | 1.98          | <0.5            | 2               | 32              | 11              | 3.18          |
| 599619             |                          | 1.78                | 0.005          |                 | <0.5            | 6.58          | <5              | 2360            | 0.7             | <2              | 1.76          | <0.5            | 3               | 27              | 84              | 2.95          |
| 599620             |                          | 1.62                | <0.005         |                 | <0.5            | 6.81          | 6               | 2150            | 0.6             | <2              | 1.36          | <0.5            | 3               | 43              | 13              | 3.56          |
| 599621             |                          | 1.90                | 0.015          |                 | 5.0             | 6.09          | 9               | 2080            | 0.6             | <2              | 3.33          | 1.5             | 2               | 26              | 106             | 3.05          |
| 599622             |                          | 1.66                | 0.012          |                 | 14.4            | 7.45          | 43              | 1360            | 0.9             | <2              | 1.26          | 1.2             | 3               | 17              | 132             | 2.97          |
| 599623             |                          | 1.22                | 0.009          |                 | 3.8             | 6.53          | 25              | 4340            | 0.7             | <2              | 2.84          | 1.0             | 2               | 24              | 53              | 2.52          |
| 599624             |                          | 1.98                | 0.009          |                 | 18.2            | 7.47          | 35              | 2640            | 0.9             | <2              | 1.60          | 3.0             | 3               | 31              | 251             | 2.03          |

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To: GEOFINE EXPLORATION CONSULTANTS LTD.  
 49 NORMANDALE RD  
 UNIONVILLE ON L3R 4J8

Page: 3 - B  
 Total # Pages: 3 (A - B)  
 Finalized Date: 12-AUG-2004  
 Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04049586

| Sample Description | Method<br>Analyte<br>Units<br>LOR | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |     |
|--------------------|-----------------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----|
|                    |                                   | K        | Mg       | Mn       | Mo       | Na       | Ni       | P        | Pb       | S        | Sb       | Sr       | Tl       | V        | W        | Zn  |
|                    |                                   | %        | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm |
|                    |                                   | 0.01     | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2   |
| 599608             |                                   | 5.87     | 0.27     | 935      | <1       | 0.11     | 1        | 450      | 3        | 0.17     | <5       | 172      | 0.17     | 44       | <10      | 10  |
| 599609             |                                   | 6.45     | 0.21     | 644      | 1        | 0.12     | <1       | 410      | <2       | 0.05     | <5       | 200      | 0.18     | 45       | <10      | 6   |
| 599610             |                                   | 6.18     | 0.32     | 997      | 4        | 0.10     | 7        | 440      | 3        | 0.02     | 7        | 142      | 0.18     | 45       | <10      | 14  |
| 599611             |                                   | 6.06     | 0.32     | 1100     | 2        | 0.13     | 3        | 420      | 3        | 0.21     | <5       | 315      | 0.17     | 44       | <10      | 10  |
| 599612             |                                   | 6.55     | 0.31     | 1180     | 1        | 0.13     | 3        | 410      | 5        | 0.08     | <5       | 198      | 0.17     | 47       | <10      | 9   |
| 599613             |                                   | 6.28     | 0.13     | 637      | 1        | 0.11     | 1        | 470      | 5        | 0.08     | <5       | 168      | 0.19     | 47       | 10       | 6   |
| 599614             |                                   | 5.27     | 0.15     | 950      | 1        | 0.11     | <1       | 380      | 4        | 0.27     | 8        | 165      | 0.16     | 40       | <10      | 7   |
| 599615             |                                   |          |          |          |          |          |          |          |          |          |          |          |          |          |          |     |
| 599616             |                                   | 6.46     | 0.14     | 1040     | 1        | 0.14     | 4        | 400      | 4        | 0.02     | 5        | 164      | 0.18     | 49       | <10      | 11  |
| 599617             |                                   | 6.33     | 0.13     | 899      | 1        | 0.17     | 2        | 400      | 3        | 0.08     | <5       | 223      | 0.17     | 45       | <10      | 9   |
| 599618             |                                   | 6.67     | 0.23     | 1090     | <1       | 0.24     | 3        | 460      | 6        | 0.01     | <5       | 196      | 0.18     | 52       | <10      | 10  |
| 599619             |                                   | 6.32     | 0.20     | 1105     | 1        | 0.13     | 2        | 440      | 2        | 0.07     | <5       | 170      | 0.18     | 47       | <10      | 12  |
| 599620             |                                   | 5.97     | 0.28     | 1515     | <1       | 0.11     | 2        | 410      | 2        | 0.01     | <5       | 106      | 0.16     | 43       | <10      | 15  |
| 599621             |                                   | 4.70     | 0.50     | 1325     | 1        | 0.08     | 1        | 380      | 14       | 0.04     | 59       | 124      | 0.15     | 46       | <10      | 61  |
| 599622             |                                   | 3.92     | 0.23     | 918      | 1        | 0.04     | 3        | 460      | 24       | 0.24     | 73       | 161      | 0.19     | 49       | <10      | 87  |
| 599623             |                                   | 4.76     | 0.21     | 1080     | <1       | 0.12     | 1        | 450      | 8        | 0.16     | 36       | 394      | 0.17     | 44       | 10       | 48  |
| 599624             |                                   | 4.80     | 0.16     | 680      | <1       | 0.17     | 3        | 500      | 315      | 0.14     | 154      | 231      | 0.19     | 50       | <10      | 142 |

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To: GEOFINE EXPLORATION CONSULTANTS LTD.

49 NORMANDALE RD

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Page: 2 - A

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Finalized Date: 12-AUG-2004

Account: KIV

Project: Stewart

NEXT 04-01

## CERTIFICATE OF ANALYSIS VA04049585

| Sample Description | Method Analyte Units LOR | WEI-21       | Au-AA23 | Au-GRA21 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|--------------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | Recvd Wt. kg | Au ppm  | Au ppm   | Ag ppm   | Al %     | As ppm   | Ba ppm   | Be ppm   | Bi ppm   | Ca %     | Cd ppm   | Co ppm   | Cr ppm   | Cu ppm   | Fe %     |
|                    |                          | 0.02         | 0.005   | 0.05     | 0.5      | 0.01     | 5        | 10       | 0.5      | 2        | 0.01     | 0.5      | 1        | 1        | 1        | 0.01     |
| 609101             |                          | 0.08         | >10.0   | 21.4     | 2.7      | 5.95     | <5       | 1440     | 2.9      | <2       | 4.09     | <0.5     | 22       | 143      | 96       | 4.39     |
| 609102             |                          | 1.68         | 0.016   |          | <0.5     | 7.54     | 5        | 1200     | 0.6      | <2       | 1.02     | <0.5     | 4        | 77       | 150      | 3.34     |
| 609103             |                          | 1.96         | 0.033   |          | <0.5     | 7.07     | 25       | 450      | 0.7      | 3        | 1.19     | <0.5     | 7        | 38       | 1640     | 4.19     |
| 609104             |                          | 1.80         | 0.008   |          | <0.5     | 7.07     | 21       | 640      | 0.7      | <2       | 0.74     | <0.5     | 6        | 85       | 209      | 3.96     |
| 609105             |                          | 1.70         | 0.011   |          | <0.5     | 7.33     | 23       | 480      | 0.7      | <2       | 1.06     | <0.5     | 5        | 59       | 410      | 3.85     |
| 609106             |                          | 1.98         | 0.006   |          | <0.5     | 7.36     | 6        | 2510     | 0.6      | <2       | 1.34     | <0.5     | 3        | 92       | 31       | 2.79     |
| 609107             |                          | 1.62         | 0.009   |          | <0.5     | 7.44     | 30       | 1370     | 0.7      | <2       | 0.89     | <0.5     | 5        | 61       | 1780     | 3.17     |
| 609108             |                          | 1.58         | 0.005   |          | <0.5     | 7.58     | 17       | 2500     | 0.7      | <2       | 1.02     | <0.5     | 4        | 91       | 575      | 2.79     |
| 609109             |                          | 1.64         | 0.007   |          | <0.5     | 7.25     | 7        | 770      | 0.6      | <2       | 1.25     | <0.5     | 3        | 63       | 434      | 3.19     |
| 609110             |                          | 1.68         | 0.017   |          | <0.5     | 7.38     | 20       | 280      | 0.6      | 2        | 0.87     | <0.5     | 5        | 94       | 1515     | 4.02     |
| 609111             |                          | 1.90         | 0.008   |          | <0.5     | 7.15     | 10       | 540      | 0.5      | 3        | 1.51     | <0.5     | 5        | 77       | 167      | 3.74     |
| 609112             |                          | 1.62         | 0.014   |          | <0.5     | 7.05     | 20       | 350      | 0.6      | 3        | 1.35     | <0.5     | 6        | 81       | 1105     | 4.56     |
| 609113             |                          | 1.72         | 0.008   |          | <0.5     | 7.03     | 7        | 500      | 0.5      | 2        | 1.38     | <0.5     | 5        | 56       | 240      | 3.76     |
| 609114             |                          | 1.72         | 0.015   |          | <0.5     | 6.94     | 10       | 630      | 0.5      | <2       | 1.12     | <0.5     | 4        | 71       | 1395     | 3.71     |
| 609115             |                          | 0.10         | 8.35    |          |          |          |          |          |          |          |          |          |          |          |          |          |
| 609116             |                          | 1.68         | 0.007   |          | <0.5     | 7.99     | 12       | 470      | 0.6      | <2       | 0.61     | <0.5     | 5        | 59       | 41       | 3.54     |
| 609117             |                          | 1.72         | 0.007   |          | <0.5     | 7.60     | 16       | 500      | 0.6      | <2       | 0.70     | <0.5     | 4        | 79       | 56       | 3.32     |
| 609118             |                          | 1.20         | 0.023   |          | <0.5     | 6.90     | 24       | 520      | 0.6      | 3        | 1.06     | <0.5     | 5        | 57       | 226      | 3.36     |
| 609119             |                          | 0.32         | 7.28    |          | <0.5     | 4.06     | 529      | 70       | <0.5     | 16       | 0.60     | 4.5      | 8        | 95       | 7640     | 6.77     |
| 609120             |                          | 2.00         | 0.080   |          | <0.5     | 7.29     | 7        | 380      | 0.6      | <2       | 0.85     | <0.5     | 4        | 48       | 376      | 3.62     |
| 609121             |                          | 1.88         | 0.020   |          | <0.5     | 7.40     | 12       | 530      | 0.6      | <2       | 0.75     | <0.5     | 4        | 73       | 136      | 3.45     |
| 609122             |                          | 1.90         | 0.007   |          | <0.5     | 7.60     | 22       | 420      | 0.5      | <2       | 0.74     | <0.5     | 5        | 54       | 49       | 3.40     |
| 609123             |                          | 1.76         | <0.005  |          | <0.5     | 7.76     | 7        | 440      | 0.6      | <2       | 1.01     | <0.5     | 5        | 80       | 25       | 2.99     |
| 609124             |                          | 1.88         | 0.009   |          | <0.5     | 7.27     | 58       | 370      | 0.6      | <2       | 0.35     | <0.5     | 6        | 62       | 69       | 3.10     |
| 609125             |                          | 1.68         | 0.011   |          | <0.5     | 6.91     | 35       | 420      | 0.6      | 3        | 0.23     | <0.5     | 7        | 98       | 229      | 3.33     |
| 609126             |                          | 1.88         | 0.016   |          | <0.5     | 6.94     | 68       | 280      | 0.6      | <2       | 0.22     | <0.5     | 8        | 58       | 53       | 3.40     |
| 609127             |                          | 2.08         | 0.029   |          | 0.5      | 5.84     | 49       | 540      | 0.6      | 3        | 0.16     | <0.5     | 8        | 99       | 336      | 2.97     |
| 609128             |                          | 1.80         | 0.027   |          | <0.5     | 6.57     | 54       | 170      | 0.7      | <2       | 0.14     | <0.5     | 8        | 64       | 176      | 3.28     |
| 609129             |                          | 1.62         | 0.025   |          | <0.5     | 6.33     | 36       | 560      | 0.7      | <2       | 0.12     | <0.5     | 6        | 104      | 184      | 2.91     |
| 609130             |                          | 0.06         | 1.170   |          |          |          |          |          |          |          |          |          |          |          |          |          |
| 609131             |                          | 1.58         | 0.010   |          | <0.5     | 3.99     | 26       | 1440     | <0.5     | <2       | 0.08     | <0.5     | 2        | 150      | 49       | 1.36     |
| 609132             |                          | 1.60         | 0.032   |          | 0.5      | 7.20     | 36       | 230      | 0.7      | 2        | 0.38     | <0.5     | 7        | 94       | 315      | 3.06     |
| 609133             |                          | 1.24         | 0.319   |          | 1.0      | 7.57     | 58       | 250      | 0.7      | 2        | 0.32     | <0.5     | 7        | 61       | 568      | 3.58     |
| 609134             |                          | 0.54         | 8.04    |          | 3.5      | 4.48     | 501      | 90       | 0.5      | 12       | 3.70     | <0.5     | 10       | 77       | 7280     | 5.86     |
| 609135             |                          | 1.60         | 0.029   |          | <0.5     | 7.58     | 30       | 480      | 0.7      | 2        | 0.72     | <0.5     | 4        | 64       | 423      | 2.85     |
| 609136             |                          | 2.10         | 0.038   |          | <0.5     | 7.18     | 93       | 200      | 0.6      | 2        | 0.95     | <0.5     | 6        | 76       | 782      | 3.90     |
| 609137             |                          | 1.74         | 0.022   |          | <0.5     | 7.67     | 34       | 300      | 0.6      | 3        | 0.40     | <0.5     | 5        | 54       | 417      | 3.01     |
| 609138             |                          | 1.76         | 0.022   |          | <0.5     | 6.46     | 92       | 320      | 0.5      | <2       | 0.96     | <0.5     | 4        | 91       | 1230     | 2.80     |
| 609139             |                          | 1.86         | 0.017   |          | <0.5     | 6.85     | 112      | 310      | 0.6      | 3        | 0.90     | <0.5     | 4        | 59       | 1765     | 2.88     |
| 609140             |                          | 1.92         | 0.012   |          | <0.5     | 7.45     | 29       | 450      | 0.6      | 2        | 0.71     | <0.5     | 5        | 73       | 336      | 2.97     |

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Page: 2 - B  
 Total # Pages: 4 (A - C)  
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Project: Stewart

## CERTIFICATE OF ANALYSIS VA04049585

| Sample Description | Method Analyte Units LOR | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61 |          |
|--------------------|--------------------------|----------|-----------|----------|----------|-----------|----------|----------|----------|----------|----------|----------|-----------|----------|----------|----------|
|                    |                          | K % 0.01 | Mg % 0.01 | Mn ppm 5 | Mo ppm 1 | Na % 0.01 | Ni ppm 1 | P ppm 10 | Pb ppm 2 | S % 0.01 | Sb ppm 5 | Sr ppm 1 | Ti % 0.01 | V ppm 1  | W ppm 10 | Zn ppm 2 |
| 609101             |                          | 4.18     | 2.57      | 855      | 74       | 1.45      | 63       | 1650     | 226      | 1.24     | <5       | 1105     | 0.25      | 168      | 10       | 63       |
| 609102             |                          | 6.45     | 0.53      | 752      | 5        | 0.18      | <1       | 480      | 8        | 1.55     | <5       | 84       | 0.19      | 48       | <10      | 31       |
| 609103             |                          | 5.82     | 0.58      | 820      | 6        | 0.14      | <1       | 460      | 7        | 2.45     | <5       | 110      | 0.17      | 50       | 10       | 31       |
| 609104             |                          | 5.52     | 0.57      | 460      | 6        | 0.15      | <1       | 460      | 20       | 1.97     | <5       | 115      | 0.17      | 54       | <10      | 40       |
| 609105             |                          | 6.04     | 0.57      | 746      | 7        | 0.16      | <1       | 450      | 12       | 2.07     | <5       | 81       | 0.18      | 53       | <10      | 35       |
| 609106             |                          | 6.60     | 0.51      | 792      | 4        | 0.14      | <1       | 470      | 9        | 0.77     | <5       | 114      | 0.18      | 48       | <10      | 36       |
| 609107             |                          | 6.14     | 0.45      | 541      | 3        | 0.10      | <1       | 490      | 15       | 1.32     | <5       | 76       | 0.18      | 49       | <10      | 36       |
| 609108             |                          | 6.45     | 0.42      | 556      | 5        | 0.11      | 2        | 510      | 9        | 0.97     | <5       | 98       | 0.18      | 47       | <10      | 34       |
| 609109             |                          | 6.50     | 0.40      | 655      | 4        | 0.10      | <1       | 470      | 5        | 1.76     | <5       | 143      | 0.17      | 45       | <10      | 27       |
| 609110             |                          | 6.34     | 0.45      | 605      | 8        | 0.09      | 1        | 470      | 9        | 2.69     | <5       | 69       | 0.18      | 49       | <10      | 23       |
| 609111             |                          | 6.34     | 0.56      | 853      | 5        | 0.09      | <1       | 450      | 3        | 2.22     | <5       | 140      | 0.17      | 47       | <10      | 27       |
| 609112             |                          | 5.97     | 0.62      | 952      | 7        | 0.09      | 1        | 440      | 8        | 2.65     | <5       | 72       | 0.17      | 50       | <10      | 31       |
| 609113             |                          | 6.14     | 0.59      | 880      | 6        | 0.09      | <1       | 460      | 8        | 2.12     | <5       | 85       | 0.16      | 45       | <10      | 28       |
| 609114             |                          | 6.11     | 0.52      | 796      | 5        | 0.09      | <1       | 430      | 9        | 1.94     | 5        | 85       | 0.16      | 44       | <10      | 29       |
| 609115             |                          |          |           |          |          |           |          |          |          |          |          |          |           |          |          |          |
| 609116             |                          | 6.94     | 0.40      | 394      | 5        | 0.11      | <1       | 520      | 8        | 2.38     | <5       | 68       | 0.19      | 54       | 10       | 23       |
| 609117             |                          | 6.17     | 0.40      | 472      | 6        | 0.14      | <1       | 480      | 8        | 2.10     | 5        | 78       | 0.18      | 48       | <10      | 21       |
| 609118             |                          | 6.19     | 0.51      | 771      | 10       | 0.12      | <1       | 430      | 6        | 2.06     | <5       | 77       | 0.16      | 45       | <10      | 31       |
| 609119             |                          | 2.56     | 0.54      | 510      | 65       | 0.04      | <1       | 220      | 68       | 4.07     | 15       | 120      | 0.09      | 39       | <10      | 254      |
| 609120             |                          | 6.38     | 0.48      | 677      | 6        | 0.10      | 1        | 460      | 10       | 2.21     | 5        | 70       | 0.17      | 48       | <10      | 30       |
| 609121             |                          | 6.84     | 0.40      | 545      | 5        | 0.11      | 2        | 460      | 10       | 2.14     | <5       | 73       | 0.18      | 45       | <10      | 22       |
| 609122             |                          | 6.60     | 0.41      | 499      | 5        | 0.11      | 1        | 470      | 13       | 2.29     | 7        | 73       | 0.18      | 50       | <10      | 18       |
| 609123             |                          | 7.15     | 0.49      | 711      | 5        | 0.13      | <1       | 480      | 14       | 2.18     | <5       | 89       | 0.18      | 49       | 10       | 12       |
| 609124             |                          | 6.03     | 0.31      | 192      | 5        | 0.10      | <1       | 470      | 11       | 2.21     | 5        | 75       | 0.18      | 47       | <10      | 16       |
| 609125             |                          | 6.49     | 0.27      | 102      | 7        | 0.10      | <1       | 460      | 23       | 2.28     | 5        | 69       | 0.17      | 48       | <10      | 19       |
| 609126             |                          | 5.49     | 0.30      | 102      | 5        | 0.10      | 1        | 460      | 8        | 2.17     | <5       | 114      | 0.17      | 48       | 10       | 20       |
| 609127             |                          | 5.22     | 0.25      | 78       | 6        | 0.07      | 1        | 370      | 9        | 1.88     | <5       | 73       | 0.14      | 41       | <10      | 17       |
| 609128             |                          | 5.87     | 0.27      | 71       | 7        | 0.08      | <1       | 440      | 11       | 2.11     | 5        | 277      | 0.16      | 47       | <10      | 20       |
| 609129             |                          | 5.63     | 0.24      | 65       | 10       | 0.08      | <1       | 400      | 10       | 1.76     | <5       | 70       | 0.16      | 50       | <10      | 17       |
| 609130             |                          |          |           |          |          |           |          |          |          |          |          |          |           |          |          |          |
| 609131             |                          | 3.23     | 0.13      | 33       | 5        | 0.05      | 1        | 240      | 6        | 0.79     | <5       | 36       | 0.10      | 30       | <10      | 7        |
| 609132             |                          | 5.69     | 0.28      | 140      | 10       | 0.07      | 2        | 450      | 16       | 2.16     | 5        | 64       | 0.17      | 52       | <10      | 16       |
| 609133             |                          | 6.12     | 0.31      | 192      | 9        | 0.12      | <1       | 480      | 12       | 2.73     | <5       | 56       | 0.18      | 54       | <10      | 15       |
| 609134             |                          | 3.07     | 1.30      | 2090     | 12       | 0.04      | 1        | 280      | 23       | 3.79     | 8        | 103      | 0.10      | 42       | <10      | 36       |
| 609135             |                          | 5.85     | 0.42      | 553      | 5        | 0.10      | <1       | 490      | 10       | 2.03     | 7        | 76       | 0.18      | 50       | <10      | 9        |
| 609136             |                          | 6.48     | 0.46      | 706      | 8        | 0.10      | 1        | 470      | 16       | 2.78     | 6        | 98       | 0.17      | 51       | <10      | 14       |
| 609137             |                          | 6.22     | 0.26      | 257      | 5        | 0.10      | <1       | 490      | 8        | 2.47     | <5       | 74       | 0.19      | 50       | <10      | 7        |
| 609138             |                          | 5.78     | 0.39      | 632      | 11       | 0.09      | 1        | 420      | 9        | 2.27     | <5       | 102      | 0.16      | 41       | 10       | 6        |
| 609139             |                          | 5.88     | 0.44      | 614      | 15       | 0.09      | <1       | 450      | 13       | 2.27     | 5        | 78       | 0.16      | 43       | 10       | 7        |
| 609140             |                          | 6.42     | 0.40      | 491      | 8        | 0.09      | 1        | 480      | 6        | 2.08     | <5       | 73       | 0.18      | 54       | <10      | 11       |

Comments: ALL SECURITY CODES ARE IN PLACE



# ALS Chemex

**EXCELLENCE IN ANALYTICAL CHEMISTRY**

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212 Brooksbank Avenue  
North Vancouver BC V7J 2C1 Canada  
Phone: 604 984 0221 Fax: 604 984 0218

To: GEOFINE EXPLORATION CONSULTANTS LTD.  
49 NORMANDALE RD  
UNIONVILLE ON L3R 4J8

Page: 2 - C  
Total # Pages: 4 (A - C)  
Finalized Date: 12-AUG-2004  
Account: KIV

Project: Stewart

**CERTIFICATE OF ANALYSIS VA04049585**

| Sample Description                             | Method<br>Analyte<br>Units<br>LOR | Cu-AA62<br>Cu<br>%<br>0.01 |
|------------------------------------------------|-----------------------------------|----------------------------|
| 609101<br>609102<br>609103<br>609104<br>609105 |                                   |                            |
| 609106<br>609107<br>609108<br>609109<br>609110 |                                   |                            |
| 609111<br>609112<br>609113<br>609114<br>609115 |                                   |                            |
| 609116<br>609117<br>609118<br>609119<br>609120 |                                   |                            |
| 609121<br>609122<br>609123<br>609124<br>609125 |                                   |                            |
| 609126<br>609127<br>609128<br>609129<br>609130 |                                   |                            |
| 609131<br>609132<br>609133<br>609134<br>609135 |                                   |                            |
| 609136<br>609137<br>609138<br>609139<br>609140 |                                   |                            |

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 49 NORMANDALE RD  
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Page: 3 - A  
 Total # Pages: 4 (A - C)  
 Finalized Date: 12-AUG-2004  
 Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04049585

| Sample Description | Method Analyte Units LOR | WEI-21    | Au-AA23 | Au-GRA21 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|-----------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | Recvd Wt. | Au      | Au       | Ag       | Al       | As       | Ba       | Be       | Bi       | Ca       | Cd       | Co       | Cr       | Cu       | Fe       |
|                    |                          | kg        | ppm     | ppm      | ppm      | %        | ppm      | ppm      | ppm      | ppm      | %        | ppm      | ppm      | ppm      | ppm      | %        |
| 609141             |                          | 1.56      | 0.024   |          | <0.5     | 7.44     | 36       | 380      | 0.6      | 2        | 0.61     | <0.5     | 3        | 62       | 636      | 3.17     |
| 609142             |                          | 0.36      | >10.0   | 21.6     | 5.3      | 3.52     | 757      | 70       | 0.5      | 5        | 1.06     | <0.5     | 17       | 121      | >10000   | 7.42     |
| 609143             |                          | 1.80      | 0.060   |          | <0.5     | 7.92     | 23       | 400      | 0.8      | 3        | 0.51     | <0.5     | 5        | 49       | 552      | 2.98     |
| 609144             |                          | 1.96      | 0.063   |          | 0.6      | 6.91     | 64       | 240      | 0.6      | 3        | 0.68     | <0.5     | 6        | 84       | 2440     | 3.18     |
| 609145             |                          | 0.06      | 0.176   |          | 2.8      | 5.03     | <5       | 110      | <0.5     | <2       | 10.95    | <0.5     | 197      | 530      | 6810     | 12.20    |
| 609146             |                          | 1.80      | 0.337   |          | 1.8      | 6.84     | 170      | 300      | 0.7      | <2       | 0.24     | <0.5     | 6        | 68       | 7490     | 3.40     |
| 609147             |                          | 1.14      | 0.477   |          | 0.7      | 7.34     | 56       | 1420     | 0.9      | <2       | 0.37     | <0.5     | 4        | 84       | 1355     | 3.07     |
| 609148             |                          | 1.22      | 4.44    |          | 5.1      | 3.08     | 679      | 70       | 0.9      | 8        | 0.88     | <0.5     | 20       | 95       | 7860     | 5.82     |
| 609149             |                          | 1.20      | 3.80    |          | 3.9      | 2.35     | 146      | 60       | 0.8      | 2        | 0.37     | <0.5     | 7        | 164      | >10000   | 5.92     |
| 609150             |                          | 1.20      | 0.054   |          | <0.5     | 5.94     | 190      | 140      | 0.5      | 5        | 0.17     | <0.5     | 7        | 69       | 132      | 3.51     |
| 609151             |                          | 2.36      | 1.550   |          | 3.2      | 2.84     | 631      | 50       | 0.6      | 27       | 0.40     | <0.5     | 8        | 146      | 4890     | 8.28     |
| 609152             |                          | 1.60      | 0.041   |          | 0.6      | 7.57     | 114      | 200      | 0.9      | 3        | 0.28     | <0.5     | 7        | 41       | 80       | 5.13     |
| 609153             |                          | 1.68      | 0.033   |          | 0.5      | 6.52     | 45       | 340      | 0.6      | <2       | 1.26     | <0.5     | 5        | 95       | 1050     | 3.96     |
| 609154             |                          | 1.96      | 0.069   |          | <0.5     | 6.46     | 63       | 290      | 0.7      | <2       | 2.61     | <0.5     | 6        | 39       | 853      | 5.54     |
| 609155             |                          | 1.94      | 0.071   |          | <0.5     | 5.83     | 127      | 130      | 0.7      | <2       | 0.26     | <0.5     | 8        | 91       | 102      | 4.52     |
| 609156             |                          | 1.56      | 0.041   |          | 0.8      | 6.70     | 121      | 160      | 0.7      | 4        | 0.67     | <0.5     | 6        | 55       | 33       | 5.14     |
| 609157             |                          | 2.02      | 0.031   |          | 1.1      | 6.55     | 146      | 200      | 0.8      | 8        | 0.72     | <0.5     | 6        | 76       | 714      | 6.55     |
| 609158             |                          | 2.08      | 0.187   |          | 2.0      | 4.13     | 774      | 60       | 0.6      | 6        | 3.00     | <0.5     | 10       | 57       | 2340     | 9.05     |
| 609159             |                          | 2.10      | 0.019   |          | 1.9      | 6.23     | 120      | 270      | 0.6      | 18       | 1.96     | <0.5     | 7        | 78       | 178      | 4.82     |
| 609160             |                          | 0.10      | 9.58    |          | 1.9      | 6.66     | 14       | 1460     | 3.3      | <2       | 5.32     | <0.5     | 28       | 176      | 130      | 5.46     |
| 609161             |                          | 1.68      | 0.019   |          | 0.8      | 6.41     | 100      | 110      | 0.7      | 7        | 2.68     | <0.5     | 6        | 46       | 77       | 5.35     |
| 609162             |                          | 2.26      | 0.014   |          | 0.6      | 6.84     | 118      | 170      | 0.8      | <2       | 1.48     | <0.5     | 6        | 72       | 20       | 5.22     |
| 609163             |                          | 1.70      | 0.008   |          | <0.5     | 6.35     | 121      | 140      | 0.7      | 3        | 1.18     | <0.5     | 4        | 56       | 19       | 4.57     |
| 609164             |                          | 1.78      | 0.009   |          | <0.5     | 6.46     | 104      | 200      | 0.7      | 4        | 1.78     | <0.5     | 5        | 72       | 88       | 4.57     |
| 609165             |                          | 1.80      | 0.008   |          | <0.5     | 6.25     | 117      | 220      | 0.6      | 2        | 0.92     | <0.5     | 4        | 56       | 15       | 4.13     |
| 609166             |                          | 1.98      | 0.011   |          | <0.5     | 6.16     | 132      | 200      | 0.6      | <2       | 0.83     | <0.5     | 6        | 84       | 18       | 4.14     |
| 609167             |                          | 1.88      | 0.007   |          | <0.5     | 6.26     | 98       | 180      | 0.7      | <2       | 0.83     | <0.5     | 5        | 57       | 31       | 4.43     |
| 609168             |                          | 2.16      | 0.005   |          | <0.5     | 5.63     | 64       | 220      | 0.6      | <2       | 1.64     | <0.5     | 5        | 97       | 102      | 3.41     |
| 609169             |                          | 1.72      | 0.007   |          | <0.5     | 6.23     | 128      | 190      | 0.5      | <2       | 1.29     | <0.5     | 5        | 65       | 36       | 3.55     |
| 609170             |                          | 1.74      | 0.016   |          | <0.5     | 6.16     | 234      | 110      | 0.5      | <2       | 1.30     | <0.5     | 5        | 104      | 70       | 4.31     |
| 609171             |                          | 1.74      | 0.014   |          | <0.5     | 6.19     | 125      | 160      | 0.5      | <2       | 1.52     | <0.5     | 4        | 76       | 88       | 3.52     |
| 609172             |                          | 2.00      | 0.013   |          | <0.5     | 6.34     | 124      | 220      | 0.5      | 3        | 1.91     | <0.5     | 6        | 86       | 621      | 3.90     |
| 609173             |                          | 2.04      | 0.005   |          | <0.5     | 6.74     | 60       | 210      | 0.5      | <2       | 1.76     | <0.5     | 4        | 60       | 168      | 3.28     |
| 609174             |                          | 2.20      | <0.005  |          | <0.5     | 6.87     | 43       | 230      | 0.5      | <2       | 1.58     | <0.5     | 3        | 89       | 52       | 3.17     |
| 609175             |                          | 0.06      | 1.310   |          | 2.4      | 8.78     | 164      | 40       | <0.5     | <2       | 4.42     | <0.5     | 224      | 29       | 9060     | 12.35    |
| 609176             |                          | 1.80      | 0.007   |          | <0.5     | 6.88     | 47       | 250      | 0.6      | <2       | 1.21     | <0.5     | 6        | 67       | 27       | 3.02     |
| 609177             |                          | 1.62      | <0.005  |          | <0.5     | 6.97     | 46       | 300      | 0.6      | <2       | 1.04     | <0.5     | 6        | 89       | 22       | 3.34     |
| 609178             |                          | 1.78      | <0.005  |          | <0.5     | 7.36     | 39       | 250      | 0.6      | <2       | 1.00     | <0.5     | 5        | 56       | 46       | 3.26     |
| 609179             |                          | 1.74      | 0.005   |          | <0.5     | 6.95     | 81       | 170      | 0.6      | 2        | 1.24     | <0.5     | 6        | 88       | 310      | 4.28     |
| 609180             |                          | 1.94      | <0.005  |          | <0.5     | 6.85     | 40       | 240      | 0.5      | <2       | 1.42     | <0.5     | 4        | 58       | 14       | 3.10     |

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Page: 3 - B  
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Project: Stewart

**CERTIFICATE OF ANALYSIS VA04049585**

| Sample Description | Method Analyte Units LOR | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | K        | Mg       | Mn       | Mo       | Na       | Ni       | P        | Pb       | S        | Sb       | Sr       | Ti       | V        | W        | Zn       |
|                    |                          | %        | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      |
|                    |                          | 0.01     | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        |
| 609141             |                          | 6.17     | 0.39     | 466      | 7        | 0.08     | 1        | 480      | 11       | 2.18     | <5       | 65       | 0.18     | 51       | <10      | 14       |
| 609142             |                          | 1.94     | 0.51     | 786      | 152      | 0.02     | <1       | 230      | 70       | 6.42     | 15       | 89       | 0.07     | 40       | <10      | 44       |
| 609143             |                          | 6.17     | 0.33     | 314      | 11       | 0.08     | 2        | 500      | 7        | 2.25     | <5       | 62       | 0.19     | 56       | <10      | 11       |
| 609144             |                          | 6.02     | 0.37     | 515      | 18       | 0.09     | <1       | 480      | 14       | 2.63     | <5       | 56       | 0.17     | 44       | <10      | 6        |
| 609145             |                          | 0.11     | 7.32     | 1115     | 2        | 0.13     | 2760     | 590      | 10       | 3.40     | <5       | 44       | 0.41     | 176      | <10      | 91       |
| 609146             |                          | 5.49     | 0.24     | 125      | 28       | 0.07     | 4        | 460      | 26       | 2.56     | 5        | 57       | 0.17     | 45       | <10      | 15       |
| 609147             |                          | 5.39     | 0.35     | 245      | 9        | 0.06     | <1       | 470      | 9        | 1.34     | <5       | 48       | 0.18     | 52       | <10      | 27       |
| 609148             |                          | 1.70     | 0.45     | 655      | 97       | 0.02     | 3        | 180      | 70       | 5.17     | 15       | 67       | 0.06     | 52       | <10      | 24       |
| 609149             |                          | 0.97     | 0.37     | 447      | 22       | 0.02     | 3        | 90       | 28       | 3.60     | 13       | 329      | 0.04     | 51       | <10      | 33       |
| 609150             |                          | 6.17     | 0.21     | 122      | 16       | 0.09     | 2        | 400      | 10       | 2.53     | 6        | 61       | 0.14     | 32       | 10       | 13       |
| 609151             |                          | 1.68     | 0.46     | 419      | 8        | 0.03     | <1       | 140      | 67       | 6.16     | 14       | 93       | 0.05     | 33       | 10       | 42       |
| 609152             |                          | 6.61     | 0.50     | 241      | 7        | 0.09     | 9        | 480      | 19       | 2.89     | 10       | 112      | 0.19     | 56       | <10      | 38       |
| 609153             |                          | 6.13     | 0.62     | 1055     | 8        | 0.10     | 12       | 410      | 16       | 2.34     | 9        | 100      | 0.15     | 44       | <10      | 34       |
| 609154             |                          | 5.04     | 1.30     | 2260     | 2        | 0.07     | 3        | 400      | 22       | 2.63     | 7        | 118      | 0.15     | 50       | 10       | 35       |
| 609155             |                          | 4.93     | 0.37     | 225      | 3        | 0.07     | 2        | 360      | 26       | 3.20     | <5       | 129      | 0.14     | 44       | <10      | 22       |
| 609156             |                          | 6.01     | 0.47     | 558      | 3        | 0.08     | <1       | 430      | 62       | 4.18     | 7        | 93       | 0.16     | 44       | <10      | 29       |
| 609157             |                          | 5.50     | 0.50     | 588      | 3        | 0.07     | <1       | 410      | 66       | 5.68     | 7        | 67       | 0.16     | 47       | 10       | 19       |
| 609158             |                          | 3.13     | 1.32     | 1895     | 1        | 0.04     | <1       | 220      | 59       | 8.12     | 9        | 108      | 0.09     | 50       | 10       | 30       |
| 609159             |                          | 5.85     | 0.84     | 1410     | 3        | 0.09     | 4        | 400      | 75       | 3.82     | 8        | 139      | 0.15     | 40       | <10      | 22       |
| 609160             |                          | 4.46     | 3.31     | 1135     | 54       | 1.56     | 71       | 2220     | 33       | 1.15     | <5       | 1255     | 0.32     | 193      | 10       | 86       |
| 609161             |                          | 5.55     | 1.14     | 1830     | 3        | 0.07     | <1       | 420      | 46       | 3.88     | <5       | 164      | 0.15     | 47       | 10       | 25       |
| 609162             |                          | 5.82     | 0.70     | 1085     | 3        | 0.07     | <1       | 430      | 42       | 4.27     | 6        | 96       | 0.16     | 47       | <10      | 18       |
| 609163             |                          | 5.62     | 0.55     | 924      | 3        | 0.07     | <1       | 400      | 34       | 3.74     | 7        | 87       | 0.15     | 41       | <10      | 14       |
| 609164             |                          | 5.59     | 0.79     | 1360     | 3        | 0.07     | 1        | 400      | 36       | 3.14     | <5       | 115      | 0.15     | 45       | <10      | 20       |
| 609165             |                          | 5.64     | 0.45     | 710      | 3        | 0.07     | <1       | 380      | 29       | 3.44     | <5       | 93       | 0.15     | 40       | <10      | 11       |
| 609166             |                          | 5.60     | 0.41     | 640      | 3        | 0.07     | 1        | 390      | 23       | 3.50     | <5       | 82       | 0.15     | 36       | <10      | 10       |
| 609167             |                          | 5.39     | 0.50     | 625      | 2        | 0.07     | <1       | 390      | 25       | 3.10     | <5       | 87       | 0.14     | 40       | <10      | 19       |
| 609168             |                          | 5.16     | 0.68     | 1100     | 4        | 0.07     | <1       | 380      | 16       | 2.29     | <5       | 144      | 0.13     | 40       | <10      | 12       |
| 609169             |                          | 5.93     | 0.53     | 664      | 5        | 0.08     | <1       | 400      | 14       | 3.14     | 5        | 93       | 0.14     | 43       | 10       | 7        |
| 609170             |                          | 5.61     | 0.53     | 629      | 6        | 0.08     | <1       | 400      | 18       | 4.01     | <5       | 98       | 0.14     | 42       | <10      | 8        |
| 609171             |                          | 5.63     | 0.61     | 733      | 3        | 0.08     | <1       | 390      | 13       | 3.06     | <5       | 95       | 0.14     | 39       | <10      | 10       |
| 609172             |                          | 5.59     | 0.77     | 973      | 4        | 0.07     | <1       | 400      | 14       | 3.15     | <5       | 108      | 0.15     | 41       | <10      | 11       |
| 609173             |                          | 6.09     | 0.67     | 1005     | 4        | 0.08     | 1        | 450      | 12       | 2.62     | 5        | 178      | 0.16     | 43       | <10      | 8        |
| 609174             |                          | 6.84     | 0.62     | 1035     | 5        | 0.09     | <1       | 450      | 9        | 2.52     | <5       | 160      | 0.16     | 44       | <10      | 7        |
| 609175             |                          | 0.55     | 2.68     | 1895     | 3        | 1.10     | 88       | 190      | 5        | 2.90     | <5       | 63       | 0.17     | 106      | <10      | 145      |
| 609176             |                          | 6.36     | 0.55     | 830      | 4        | 0.08     | <1       | 430      | 28       | 2.43     | 5        | 138      | 0.16     | 41       | <10      | 15       |
| 609177             |                          | 6.06     | 0.48     | 864      | 5        | 0.07     | 2        | 470      | 22       | 2.59     | <5       | 108      | 0.17     | 46       | 10       | 18       |
| 609178             |                          | 5.56     | 0.48     | 616      | 4        | 0.08     | <1       | 460      | 11       | 2.61     | <5       | 99       | 0.18     | 47       | 10       | 8        |
| 609179             |                          | 6.40     | 0.53     | 779      | 6        | 0.08     | <1       | 430      | 23       | 3.48     | <5       | 96       | 0.16     | 49       | <10      | 12       |
| 609180             |                          | 6.39     | 0.54     | 800      | 6        | 0.09     | <1       | 450      | 14       | 2.28     | <5       | 97       | 0.16     | 44       | <10      | 10       |

Comments: ALL SECURITY CODES ARE IN PLACE



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212 Brooksbank Avenue

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49 NORMANDALE RD

UNIONVILLE ON L3R 4J8

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Finalized Date: 12-AUG-2004

Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04049585

| Sample Description                             | Method<br>Analyte<br>Units<br>LOR | Cu-AA62<br>Cu<br>%<br>0.01 |
|------------------------------------------------|-----------------------------------|----------------------------|
| 609141<br>609142<br>609143<br>609144<br>609145 |                                   | 2.34                       |
| 609146<br>609147<br>609148<br>609149<br>609150 |                                   | 1.12                       |
| 609151<br>609152<br>609153<br>609154<br>609155 |                                   |                            |
| 609156<br>609157<br>609158<br>609159<br>609160 |                                   |                            |
| 609161<br>609162<br>609163<br>609164<br>609165 |                                   |                            |
| 609166<br>609167<br>609168<br>609169<br>609170 |                                   |                            |
| 609171<br>609172<br>609173<br>609174<br>609175 |                                   |                            |
| 609176<br>609177<br>609178<br>609179<br>609180 |                                   |                            |

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Project: Stewart

**CERTIFICATE OF ANALYSIS VA04049585**

| Sample Description | Method Analyte Units LOR | WEI-21       | Au-AA23 | Au-GRA21 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|--------------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | Recvd Wt. kg | Au ppm  | Au ppm   | Ag ppm   | Al %     | As ppm   | Ba ppm   | Be ppm   | Bi ppm   | Ca %     | Cd ppm   | Co ppm   | Cr ppm   | Cu ppm   | Fe %     |
|                    |                          | 0.02         | 0.005   | 0.05     | 0.5      | 0.01     | 5        | 10       | 0.5      | 2        | 0.01     | 0.5      | 1        | 1        | 1        | 0.01     |
| 609181             |                          | 1.34         | <0.005  |          | <0.5     | 7.14     | 43       | 290      | 0.6      | <2       | 1.14     | <0.5     | 4        | 80       | 12       | 3.42     |
| 609182             |                          | 1.62         | <0.005  |          | <0.5     | 8.49     | 50       | 250      | 0.7      | 3        | 1.80     | <0.5     | 5        | 47       | 14       | 4.74     |
| 609183             |                          | 1.82         | <0.005  |          | <0.5     | 7.49     | 37       | 370      | 0.6      | <2       | 1.72     | <0.5     | 3        | 65       | 11       | 3.33     |
| 609184             |                          | 1.88         | <0.005  |          | <0.5     | 6.71     | 37       | 560      | 0.5      | <2       | 0.79     | 0.5      | 3        | 46       | 7        | 2.59     |
| 609185             |                          | 2.00         | <0.005  |          | <0.5     | 7.76     | 34       | 580      | 0.7      | 3        | 0.99     | 0.6      | 4        | 59       | 8        | 3.32     |

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Project: Stewart

**CERTIFICATE OF ANALYSIS VA04049585**

| Sample Description | Method<br>Analyte<br>Units<br>LOR | ME-ICP61 | ME-ICP61 | ME-ICP61  | ME-ICP61  | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61  | ME-ICP61  | ME-ICP61 | ME-ICP61 | ME-ICP61 |           |
|--------------------|-----------------------------------|----------|----------|-----------|-----------|----------|-----------|----------|-----------|----------|-----------|-----------|----------|----------|----------|-----------|
|                    |                                   | K<br>%   | Mg<br>%  | Mn<br>ppm | Mo<br>ppm | Na<br>%  | Ni<br>ppm | P<br>ppm | Pb<br>ppm | S<br>%   | Sb<br>ppm | Sr<br>ppm | Ti<br>%  | V<br>ppm | W<br>ppm | Zn<br>ppm |
|                    |                                   | 0.01     | 0.01     | 5         | 1         | 0.01     | 1         | 10       | 2         | 0.01     | 5         | 1         | 0.01     | 1        | 10       |           |
| 609181             |                                   | 6.72     | 0.48     | 674       | 5         | 0.09     | <1        | 480      | 14        | 2.60     | 5         | 100       | 0.17     | 42       | <10      | 10        |
| 609182             |                                   | 6.99     | 0.77     | 1145      | 5         | 0.08     | <1        | 550      | 17        | 3.34     | 6         | 123       | 0.20     | 58       | <10      | 19        |
| 609183             |                                   | 6.70     | 0.64     | 1055      | 6         | 0.09     | <1        | 540      | 13        | 2.26     | <5        | 107       | 0.18     | 47       | <10      | 11        |
| 609184             |                                   | 6.44     | 0.32     | 473       | 3         | 0.09     | 3         | 460      | 10        | 2.02     | 6         | 98        | 0.17     | 37       | <10      | 9         |
| 609185             |                                   | 6.17     | 0.46     | 630       | 3         | 0.09     | 3         | 590      | 30        | 2.37     | <5        | 88        | 0.19     | 50       | <10      | 13        |

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**CERTIFICATE OF ANALYSIS VA04049585**

| Sample Description                             | Method<br>Analyte<br>Units<br>LOR | Cu-AA62<br>Cu<br>%<br>0.01 |
|------------------------------------------------|-----------------------------------|----------------------------|
| 609181<br>609182<br>609183<br>609184<br>609185 |                                   |                            |
|                                                |                                   |                            |

Comments: ALL SECURITY CODES ARE IN PLACE





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Account: KIV

Project: Stewart

SZD04-03

## CERTIFICATE OF ANALYSIS VA04052342

| Sample Description | Method<br>Analyte<br>Units<br>LOR | WEI-21          | Au-AA23   | ME-ICP61  | ME-ICP61 | ME-ICP61  | ME-ICP61  | ME-ICP61  | ME-ICP61  | ME-ICP61 | ME-ICP61  | ME-ICP61  | ME-ICP61  | ME-ICP61  | ME-ICP61 | ME-ICP61 |
|--------------------|-----------------------------------|-----------------|-----------|-----------|----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|-----------|-----------|----------|----------|
|                    |                                   | Recvd Wt.<br>kg | Au<br>ppm | Ag<br>ppm | Al<br>%  | As<br>ppm | Ba<br>ppm | Be<br>ppm | Bi<br>ppm | Ca<br>%  | Cd<br>ppm | Co<br>ppm | Cr<br>ppm | Cu<br>ppm | Fe<br>%  | K<br>%   |
|                    |                                   | 0.02            | 0.005     | 0.5       | 0.01     | 5         | 10        | 0.5       | 2         | 0.01     | 0.5       | 1         | 1         | 1         | 0.01     | 0.01     |
| N599654            |                                   | 0.08            | 3.09      | 0.7       | 6.63     | 11        | 1960      | 3.1       | <2        | 4.70     | <0.5      | 28        | 144       | 98        | 4.88     | 3.31     |
| N599655            |                                   | 1.94            | <0.005    | <0.5      | 8.00     | 23        | 2500      | 0.7       | 3         | 1.52     | <0.5      | 4         | 79        | 7         | 3.69     | 6.71     |
| N599656            | X                                 | 2.30            | 0.068     | <0.5      | 7.00     | 17        | 1890      | 0.6       | <2        | 1.48     | <0.5      | 6         | 68        | 100       | 2.14     | 5.71     |
| N599657            |                                   | 2.32            | 0.015     | <0.5      | 7.20     | 29        | 1710      | 0.6       | <2        | 2.22     | <0.5      | 5         | 66        | 11        | 2.31     | 5.74     |
| N599658            |                                   | 1.86            | 0.036     | <0.5      | 7.08     | 27        | 1540      | 0.5       | <2        | 1.52     | <0.5      | 7         | 46        | 10        | 2.22     | 5.56     |
| N599659            |                                   | 1.32            | 0.016     | <0.5      | 7.43     | 22        | 1680      | 0.6       | <2        | 1.08     | <0.5      | 4         | 58        | 10        | 2.16     | 5.81     |
| N599660            |                                   | 1.96            | 0.051     | <0.5      | 5.38     | 61        | 910       | 0.5       | <2        | 4.12     | <0.5      | 6         | 38        | 13        | 3.83     | 3.65     |
| N599661            | X                                 | 1.82            | 0.033     | <0.5      | 6.56     | 28        | 1260      | 0.6       | 2         | 1.43     | <0.5      | 6         | 48        | 25        | 3.80     | 4.33     |
| N599662            | X                                 | 2.46            | 8.55      | 12.5      | 2.39     | 451       | 1370      | <0.5      | 3         | 1.46     | 12.3      | 5         | 74        | 6650      | 3.83     | 1.14     |
| N599663            |                                   | 2.00            | 0.020     | <0.5      | 7.74     | 7         | 1950      | 0.5       | <2        | 1.42     | <0.5      | 2         | 39        | 56        | 2.63     | 5.67     |
| N599664            |                                   | 1.94            | 0.011     | <0.5      | 7.16     | 5         | 2150      | <0.5      | <2        | 1.60     | <0.5      | 5         | 50        | 20        | 3.25     | 5.98     |
| N599665            |                                   | 2.08            | 0.007     | <0.5      | 7.23     | 16        | 2260      | 0.5       | 4         | 1.57     | <0.5      | 3         | 47        | 6         | 2.66     | 6.15     |
| N599666            |                                   | 1.56            | 0.005     | <0.5      | 7.24     | 10        | 5370      | <0.5      | <2        | 1.48     | <0.5      | 4         | 39        | 7         | 3.19     | 6.15     |
| N599667            |                                   | 1.92            | 0.064     | <0.5      | 6.95     | 16        | 2730      | <0.5      | 3         | 1.98     | <0.5      | 6         | 52        | 73        | 4.14     | 6.25     |
| N599668            |                                   | 1.94            | 0.019     | <0.5      | 7.54     | 13        | 4090      | 0.5       | <2        | 0.74     | <0.5      | 3         | 49        | 104       | 3.47     | 6.60     |
| N599669            |                                   | 1.20            | <0.005    | <0.5      | 7.50     | 9         | 2160      | 0.5       | <2        | 1.44     | <0.5      | 5         | 46        | 54        | 3.65     | 6.22     |
| N599670            | X                                 | 1.32            | 0.541     | <0.5      | 6.20     | 7         | 2220      | <0.5      | 3         | 2.24     | <0.5      | 2         | 54        | 1715      | 2.78     | 5.14     |
| N599671            |                                   | 0.08            | 1.260     | 2.7       | 8.34     | 159       | 40        | <0.5      | 4         | 4.35     | 1.2       | 217       | 29        | 8530      | 11.50    | 0.53     |
| N599672            |                                   | 1.78            | <0.005    | <0.5      | 7.73     | 11        | 2560      | 0.5       | <2        | 1.65     | <0.5      | 4         | 47        | 114       | 2.77     | 6.62     |
| N599673            |                                   | 1.96            | <0.005    | <0.5      | 7.88     | 6         | 2690      | 0.6       | <2        | 1.40     | <0.5      | 3         | 37        | 25        | 3.12     | 6.75     |
| N599674            |                                   | 1.70            | 0.108     | <0.5      | 7.27     | 7         | 2410      | 0.6       | <2        | 2.15     | <0.5      | 3         | 38        | 16        | 3.66     | 6.22     |

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## CERTIFICATE OF ANALYSIS VA04052342

| Sample Description | Method       | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    | Analyte      | Mg       | Mn       | Mo       | Na       | Ni       | P        | Pb       | S        | Sb       | Sr       | Ti       | V        | W        | Zn       |
|                    | Units<br>LOR | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      |
|                    |              | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        |
| N599654            |              | 2.83     | 1025     | 12       | 2.36     | 74       | 2190     | 37       | 0.31     | <5       | 1560     | 0.39     | 166      | <10      | 100      |
| N599655            |              | 0.70     | 816      | 2        | 0.08     | 2        | 510      | 9        | 0.04     | 8        | 138      | 0.19     | 56       | 10       | 29       |
| N599656            |              | 0.59     | 800      | <1       | 0.07     | 2        | 470      | 7        | 0.29     | 9        | 122      | 0.17     | 48       | <10      | 16       |
| N599657            |              | 0.84     | 1110     | <1       | 0.07     | 2        | 510      | 17       | 0.37     | <5       | 130      | 0.17     | 45       | <10      | 18       |
| N599658            |              | 0.65     | 699      | <1       | 0.07     | <1       | 560      | 10       | 0.90     | <5       | 91       | 0.20     | 43       | 10       | 15       |
| N599659            |              | 0.53     | 522      | <1       | 0.07     | 2        | 540      | 5        | 0.41     | <5       | 95       | 0.19     | 44       | 10       | 18       |
| N599660            |              | 1.47     | 1960     | <1       | 0.04     | 2        | 370      | 16       | 1.24     | <5       | 151      | 0.13     | 39       | 10       | 23       |
| N599661            |              | 0.68     | 1185     | 2        | 0.04     | 3        | 430      | 8        | 0.47     | 12       | 99       | 0.16     | 36       | <10      | 32       |
| N599662            |              | 0.51     | 1355     | 1        | 0.01     | 5        | 130      | 74       | 1.28     | 1105     | 121      | 0.04     | 26       | <10      | 453      |
| N599663            |              | 0.60     | 933      | 1        | 0.06     | 1        | 470      | 8        | 0.06     | 27       | 84       | 0.18     | 45       | <10      | 52       |
| N599664            |              | 0.66     | 1525     | <1       | 0.07     | 2        | 440      | 7        | 0.04     | <5       | 93       | 0.16     | 42       | <10      | 39       |
| N599665            |              | 0.57     | 1220     | 1        | 0.08     | <1       | 470      | 7        | 0.01     | 7        | 111      | 0.17     | 45       | <10      | 41       |
| N599666            |              | 0.55     | 1530     | 1        | 0.07     | <1       | 430      | 7        | 0.14     | 6        | 220      | 0.17     | 47       | <10      | 41       |
| N599667            |              | 0.68     | 2000     | <1       | 0.10     | 1        | 430      | 14       | 0.06     | 15       | 132      | 0.17     | 46       | <10      | 42       |
| N599668            |              | 0.37     | 1170     | 1        | 0.09     | 1        | 470      | 8        | 0.18     | <5       | 154      | 0.19     | 47       | <10      | 36       |
| N599669            |              | 0.56     | 1340     | 2        | 0.08     | 1        | 450      | 9        | 0.07     | <5       | 110      | 0.17     | 49       | <10      | 36       |
| N599670            |              | 0.72     | 1120     | <1       | 0.11     | <1       | 390      | 9        | 0.22     | <5       | 122      | 0.15     | 43       | <10      | 30       |
| N599671            |              | 2.51     | 1860     | 1        | 1.14     | 91       | 180      | 15       | 2.94     | <5       | 60       | 0.18     | 101      | <10      | 127      |
| N599672            |              | 0.58     | 887      | 1        | 0.11     | 4        | 480      | 10       | 0.05     | <5       | 117      | 0.18     | 49       | <10      | 49       |
| N599673            |              | 0.55     | 980      | <1       | 0.10     | 2        | 470      | 6        | 0.03     | <5       | 130      | 0.18     | 50       | <10      | 47       |
| N599674            |              | 0.80     | 1475     | <1       | 0.08     | <1       | 480      | 12       | 0.01     | <5       | 143      | 0.18     | 46       | <10      | 44       |



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Project: Stewart

SZ1504-03

**CERTIFICATE OF ANALYSIS VA04054018**

| Sample Description | Method Analyte Units LOR | WEI-21       | Au-AA23 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|--------------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | Recvd Wt. kg | Au ppm  | Ag ppm   | Al %     | As ppm   | Ba ppm   | Be ppm   | Bi ppm   | Ca %     | Cd ppm   | Co ppm   | Cr ppm   | Cu ppm   | Fe %     | K %      |
|                    |                          | 0.02         | 0.005   | 0.5      | 0.01     | 5        | 10       | 0.5      | 2        | 0.01     | 0.5      | 1        | 1        | 1        | 0.01     | 0.01     |
| N599625            |                          | 2.42         | <0.005  | <0.5     | 6.03     | 9        | 420      | 0.5      | <2       | 5.29     | <0.5     | 4        | 26       | 3        | 3.24     | 2.95     |
| N599626            |                          | 1.52         | <0.005  | <0.5     | 7.33     | 18       | 2050     | 0.5      | <2       | 1.06     | <0.5     | 4        | 56       | 5        | 2.50     | 5.45     |
| N599627            |                          | 1.42         | <0.005  | <0.5     | 7.94     | 14       | 820      | 0.5      | <2       | 0.75     | <0.5     | 8        | 52       | 8        | 3.48     | 6.77     |
| N599628            |                          | 1.92         | <0.005  | <0.5     | 7.14     | 6        | 1180     | <0.5     | <2       | 1.19     | <0.5     | 9        | 63       | 7        | 2.82     | 6.64     |
| N599629            |                          | 1.64         | <0.005  | <0.5     | 7.21     | 10       | 1140     | 0.5      | <2       | 1.82     | <0.5     | 7        | 46       | 9        | 3.20     | 6.73     |
| N599630            |                          | 1.20         | <0.005  | <0.5     | 6.91     | 14       | 2480     | 0.5      | <2       | 2.74     | <0.5     | 6        | 55       | 7        | 3.02     | 5.88     |
| N599631            |                          | 1.96         | <0.005  | <0.5     | 6.74     | 7        | 2460     | 0.5      | <2       | 2.30     | <0.5     | 3        | 48       | 4        | 2.91     | 5.95     |
| N599632            |                          | 1.84         | <0.005  | <0.5     | 7.23     | 7        | 2150     | 0.7      | <2       | 2.26     | <0.5     | 4        | 46       | 4        | 3.23     | 5.85     |
| N599633            |                          | 1.72         | <0.005  | <0.5     | 7.07     | 8        | 2740     | 0.7      | <2       | 1.14     | <0.5     | 3        | 47       | 23       | 4.45     | 6.55     |
| N599634            |                          | 2.04         | <0.005  | <0.5     | 7.45     | 7        | 3080     | 0.8      | <2       | 0.99     | <0.5     | 4        | 57       | 14       | 3.73     | 7.10     |
| N599635 X          |                          | 1.78         | 0.305   | <0.5     | 7.30     | <5       | 3030     | 0.7      | <2       | 0.78     | <0.5     | 3        | 53       | 10       | 3.43     | 6.75     |
| N599636 X          |                          | 1.64         | 0.175   | <0.5     | 7.31     | 9        | 3070     | 0.8      | <2       | 1.33     | <0.5     | 2        | 67       | 5        | 3.62     | 6.92     |
| N599637            |                          | 1.82         | <0.005  | <0.5     | 7.13     | 8        | 3090     | 0.7      | <2       | 0.88     | <0.5     | 3        | 49       | 15       | 3.22     | 6.76     |
| N599638            |                          | 1.70         | <0.005  | <0.5     | 7.57     | <5       | 3090     | 0.7      | <2       | 0.66     | <0.5     | 3        | 65       | 13       | 3.34     | 7.07     |
| N599639            |                          | 1.90         | <0.005  | <0.5     | 6.99     | <5       | 2650     | 0.7      | <2       | 1.78     | <0.5     | 2        | 49       | 14       | 3.31     | 6.61     |
| N599640            |                          | 1.42         | <0.005  | <0.5     | 7.53     | <5       | 3020     | 0.8      | <2       | 1.52     | <0.5     | 3        | 64       | 3        | 3.39     | 6.92     |
| N599641            |                          | 0.08         | 8.12    | 1.8      | 5.98     | 5        | 1600     | 3.1      | <2       | 4.69     | <0.5     | 25       | 151      | 120      | 4.83     | 3.97     |
| N599642            |                          | 1.68         | 0.007   | <0.5     | 6.75     | 13       | 2450     | 0.5      | <2       | 1.20     | <0.5     | 4        | 50       | 6        | 2.90     | 5.11     |
| N599643            |                          | 1.62         | <0.005  | <0.5     | 7.26     | 6        | 2840     | 0.6      | <2       | 0.99     | <0.5     | 3        | 56       | 32       | 3.00     | 6.79     |
| N599644            |                          | 1.76         | <0.005  | <0.5     | 7.05     | 11       | 2940     | 0.6      | <2       | 1.20     | <0.5     | 3        | 53       | 13       | 3.09     | 6.60     |
| N599645            |                          | 2.04         | <0.005  | <0.5     | 7.54     | 10       | 3230     | 0.6      | <2       | 0.87     | <0.5     | 5        | 73       | 10       | 3.02     | 7.03     |
| N599646            |                          | 1.82         | 0.062   | <0.5     | 7.01     | 5        | 2290     | 0.7      | <2       | 1.48     | <0.5     | 2        | 40       | 4        | 2.68     | 5.91     |
| N599647            |                          | 1.82         | 0.031   | <0.5     | 5.53     | <5       | 1540     | 0.5      | <2       | 5.09     | <0.5     | 2        | 33       | 12       | 3.75     | 4.32     |
| N599648            |                          | 1.72         | 0.213   | <0.5     | 6.84     | 6        | 2570     | 0.6      | <2       | 1.26     | <0.5     | 4        | 55       | 12       | 3.90     | 6.24     |
| N599649            |                          | 1.76         | <0.005  | <0.5     | 6.85     | 12       | 2310     | 0.6      | <2       | 2.38     | <0.5     | 4        | 58       | 19       | 3.47     | 5.55     |
| N599650            |                          | 1.68         | 0.005   | <0.5     | 6.92     | 13       | 2750     | 0.7      | <2       | 3.09     | <0.5     | 2        | 48       | 6        | 3.72     | 3.98     |
| N599651            |                          | 1.72         | 0.010   | <0.5     | 6.38     | <5       | 1830     | 0.7      | <2       | 3.04     | <0.5     | 4        | 55       | 12       | 3.36     | 4.70     |
| N599652            |                          | 1.80         | <0.005  | <0.5     | 6.91     | <5       | 2070     | 0.6      | <2       | 3.08     | <0.5     | 2        | 35       | 8        | 3.29     | 5.21     |
| N599653            |                          | 3.20         | <0.005  | <0.5     | 6.34     | 7        | 4290     | 0.5      | <2       | 4.86     | <0.5     | 3        | 30       | 3        | 3.84     | 5.50     |
| N599653A           |                          | 0.08         | 1.315   | 5.1      | 8.34     | 156      | 40       | <0.5     | <2       | 4.13     | <0.5     | 205      | 28       | 8480     | 11.45    | 0.53     |
| N599675            |                          | 3.94         | <0.005  | <0.5     | 6.32     | 16       | 2220     | 0.5      | <2       | 3.71     | <0.5     | 4        | 40       | 54       | 3.39     | 5.74     |

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# ALS Chemex

EXCELLENCE IN ANALYTICAL CHEMISTRY

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To: GEOFINE EXPLORATION CONSULTANTS LTD.

49 NORMANDALE RD

UNIONVILLE ON L3R 4J8

Page: 2 - B

Total # Pages: 2 (A - B)

Finalized Date: 25-AUG-2004

Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04054018

| Sample Description | Method Analyte Units LOR | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |     |
|--------------------|--------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----|
|                    |                          | Mg       | Mn       | Mo       | Na       | Ni       | P        | Pb       | S        | Sb       | Sr       | Ti       | V        | W        | Zn  |
|                    |                          | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm |
|                    |                          |          |          |          |          |          |          |          |          |          |          |          |          |          |     |
| N599625            |                          | 1.89     | 1950     | 2        | 0.04     | 4        | 390      | 4        | 0.17     | <5       | 102      | 0.14     | 59       | <10      | 18  |
| N599626            |                          | 0.41     | 798      | 3        | 0.08     | 3        | 490      | <2       | 0.98     | <5       | 65       | 0.17     | 45       | <10      | 9   |
| N599627            |                          | 0.29     | 764      | 6        | 0.09     | 3        | 540      | 4        | 1.76     | 5        | 78       | 0.19     | 53       | <10      | 8   |
| N599628            |                          | 0.36     | 631      | 3        | 0.10     | 5        | 470      | 4        | 1.70     | <5       | 87       | 0.17     | 48       | <10      | 7   |
| N599629            |                          | 0.53     | 762      | 3        | 0.10     | 5        | 480      | 4        | 1.82     | <5       | 88       | 0.19     | 53       | <10      | 11  |
| N599630            |                          | 0.79     | 1070     | 3        | 0.13     | 2        | 440      | <2       | 1.02     | 5        | 110      | 0.16     | 52       | <10      | 13  |
| N599631            |                          | 0.69     | 1090     | 3        | 0.15     | 3        | 450      | 2        | 0.32     | <5       | 128      | 0.16     | 44       | <10      | 13  |
| N599632            |                          | 0.77     | 1080     | 1        | 0.11     | 2        | 490      | 2        | 0.25     | <5       | 99       | 0.17     | 50       | <10      | 19  |
| N599633            |                          | 0.59     | 1255     | 5        | 0.11     | 3        | 460      | 4        | 0.13     | <5       | 112      | 0.16     | 46       | 30       | 31  |
| N599634            |                          | 0.48     | 1130     | 3        | 0.13     | 4        | 480      | 2        | 0.07     | <5       | 119      | 0.18     | 49       | <10      | 28  |
| N599635            |                          | 0.41     | 921      | 3        | 0.12     | 3        | 490      | 5        | 0.07     | <5       | 106      | 0.17     | 44       | 10       | 23  |
| N599636            |                          | 0.57     | 976      | 2        | 0.30     | 5        | 480      | <2       | 0.01     | <5       | 173      | 0.17     | 48       | 20       | 26  |
| N599637            |                          | 0.43     | 926      | 4        | 0.12     | 4        | 470      | 7        | 0.17     | <5       | 104      | 0.17     | 43       | <10      | 25  |
| N599638            |                          | 0.41     | 951      | 3        | 0.45     | 3        | 490      | 3        | 0.02     | <5       | 130      | 0.18     | 48       | <10      | 25  |
| N599639            |                          | 0.65     | 1035     | 4        | 0.13     | 3        | 460      | 4        | 0.03     | <5       | 152      | 0.17     | 47       | 10       | 23  |
| N599640            |                          | 0.59     | 957      | 2        | 0.14     | 3        | 510      | <2       | 0.03     | <5       | 153      | 0.18     | 50       | <10      | 23  |
| N599641            |                          | 3.00     | 1015     | 47       | 1.41     | 68       | 1950     | 29       | 1.03     | <5       | 1125     | 0.28     | 169      | <10      | 77  |
| N599642            |                          | 0.42     | 676      | 7        | 0.10     | 4        | 450      | 7        | 1.03     | <5       | 97       | 0.16     | 42       | <10      | 13  |
| N599643            |                          | 0.40     | 854      | 2        | 0.12     | 2        | 470      | <2       | 0.06     | <5       | 118      | 0.17     | 43       | <10      | 16  |
| N599644            |                          | 0.42     | 888      | 6        | 0.11     | 4        | 470      | 5        | 0.26     | <5       | 108      | 0.17     | 44       | <10      | 17  |
| N599645            |                          | 0.35     | 805      | 6        | 0.12     | 3        | 490      | 2        | 0.22     | 7        | 98       | 0.18     | 47       | <10      | 19  |
| N599646            |                          | 0.46     | 670      | 2        | 0.08     | 4        | 470      | 3        | 0.02     | 5        | 114      | 0.17     | 45       | 10       | 20  |
| N599647            |                          | 1.46     | 1415     | 6        | 0.06     | 6        | 360      | 3        | 0.02     | 8        | 171      | 0.12     | 41       | <10      | 40  |
| N599648            |                          | 0.56     | 976      | 2        | 0.09     | 3        | 450      | 4        | 0.04     | 7        | 99       | 0.16     | 46       | 10       | 24  |
| N599649            |                          | 0.76     | 869      | 5        | 0.08     | 3        | 440      | 4        | 0.08     | 7        | 119      | 0.16     | 50       | <10      | 21  |
| N599650            |                          | 0.91     | 1105     | 3        | 0.05     | 4        | 470      | 3        | 0.14     | 8        | 132      | 0.16     | 47       | <10      | 63  |
| N599651            |                          | 0.52     | 1080     | 3        | 0.06     | 3        | 510      | 5        | 0.06     | 5        | 86       | 0.17     | 64       | <10      | 32  |
| N599652            |                          | 1.03     | 1125     | 2        | 0.08     | 4        | 470      | 2        | 0.04     | <5       | 110      | 0.16     | 61       | <10      | 20  |
| N599653            |                          | 1.83     | 1915     | 2        | 0.10     | 4        | 410      | <2       | 0.08     | <5       | 233      | 0.14     | 63       | <10      | 28  |
| N599653A           |                          | 2.56     | 1790     | 2        | 1.05     | 82       | 180      | 2        | 2.77     | <5       | 57       | 0.16     | 99       | <10      | 132 |
| N599675            |                          | 1.25     | 1460     | 4        | 0.10     | 4        | 400      | 6        | 0.39     | <5       | 166      | 0.14     | 48       | <10      | 16  |



# ALS Chemex

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49 NORMANDALE RD

UNIONVILLE ON L3R 4J8

Page: 2 - A

Total # Pages: 2 (A - B)

Finalized Date: 26-AUG-2004

Account: KIV

Project: Stewart

SZ004-04

## CERTIFICATE OF ANALYSIS VA04054015

| Sample Description | Method Analyte Units LOR | WEI-21       | Au-AA23 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|--------------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | Recvd Wt. kg | Au ppm  | Ag ppm   | Al %     | As ppm   | Ba ppm   | Be ppm   | Bi ppm   | Ca %     | Cd ppm   | Co ppm   | Cr ppm   | Cu ppm   | Fe %     | K %      |
|                    |                          | 0.02         | 0.005   | 0.5      | 0.01     | 5        | 10       | 0.5      | 2        | 0.01     | 0.5      | 1        | 1        | 1        | 0.01     | 0.01     |
| N599676            |                          | 1.90         | 0.698   | <0.5     | 6.13     | <5       | 2020     | 0.6      | <2       | 1.45     | <0.5     | 4        | 101      | 5        | 4.51     | 4.41     |
| N599677            |                          | 1.98         | 0.007   | <0.5     | 6.07     | 8        | 1520     | <0.5     | <2       | 3.58     | <0.5     | 7        | 90       | 5        | 3.80     | 4.33     |
| N599678            |                          | 1.72         | 0.064   | <0.5     | 6.76     | <5       | 2410     | 0.6      | <2       | 2.84     | <0.5     | 3        | 73       | 27       | 3.47     | 5.36     |
| N599679            |                          | 1.82         | 0.082   | 0.6      | 6.33     | 11       | 1100     | 0.8      | <2       | 2.60     | 0.5      | 4        | 96       | 56       | 3.34     | 4.02     |
| N599680            |                          | 1.78         | 0.109   | <0.5     | 6.26     | 11       | 1550     | 0.7      | <2       | 1.90     | <0.5     | 4        | 84       | 48       | 4.24     | 4.84     |
| N599681            |                          | 1.70         | 0.035   | <0.5     | 6.46     | 11       | 1840     | 0.8      | <2       | 1.49     | <0.5     | 3        | 100      | 168      | 3.86     | 5.30     |
| N599682            |                          | 1.88         | 0.013   | <0.5     | 6.39     | 5        | 1750     | 0.7      | <2       | 1.97     | <0.5     | 3        | 75       | 350      | 4.38     | 5.07     |
| N599683            |                          | 1.78         | 0.100   | <0.5     | 6.48     | 8        | 1720     | 0.6      | <2       | 1.10     | <0.5     | 4        | 112      | 781      | 3.91     | 5.11     |
| N599684            |                          | 2.16         | 0.032   | <0.5     | 6.32     | 14       | 1900     | 0.6      | <2       | 1.40     | <0.5     | 4        | 87       | 555      | 3.64     | 5.25     |
| N599685            |                          | 1.52         | 0.008   | <0.5     | 6.08     | 26       | 1520     | 0.7      | <2       | 1.82     | 1.1      | 4        | 87       | 432      | 4.05     | 4.83     |
| N599686            |                          | 0.06         | 0.108   | 2.8      | 4.73     | <5       | 100      | <0.5     | 2        | 10.05    | 0.7      | 183      | 505      | 6310     | 11.20    | 0.09     |
| N599687            |                          | 1.70         | 0.010   | 0.8      | 6.83     | 29       | 1840     | 0.7      | <2       | 1.70     | 1.4      | 6        | 76       | 132      | 3.82     | 5.41     |
| N599688            |                          | 1.56         | 0.008   | 0.9      | 6.86     | 22       | 1460     | 0.7      | <2       | 1.51     | 1.9      | 6        | 82       | 274      | 4.01     | 5.10     |
| N599689            |                          | 1.60         | 0.007   | <0.5     | 6.49     | 12       | 2160     | 0.5      | <2       | 1.86     | <0.5     | 5        | 103      | 117      | 3.36     | 5.70     |
| N599690            |                          | 1.76         | 0.008   | <0.5     | 6.62     | 11       | 2150     | 0.5      | <2       | 3.92     | <0.5     | 5        | 78       | 63       | 2.75     | 6.13     |
| N599691            |                          | 0.98         | <0.005  | <0.5     | 6.58     | <5       | 2130     | 0.6      | <2       | 1.34     | <0.5     | 4        | 94       | 47       | 4.04     | 5.96     |
| N609205            |                          | 2.28         | <0.005  | <0.5     | 7.02     | 6        | 2850     | 0.5      | <2       | 1.52     | <0.5     | 5        | 94       | 33       | 2.83     | 6.86     |
| N609206            |                          | 2.32         | <0.005  | <0.5     | 6.43     | <5       | 2880     | 0.5      | <2       | 1.82     | <0.5     | 2        | 128      | 7        | 2.64     | 6.88     |
| N609207            |                          | 1.86         | 0.147   | <0.5     | 7.46     | 21       | 2400     | 0.6      | <2       | 1.84     | <0.5     | 1        | 110      | 90       | 3.67     | 6.98     |
| N609208            |                          | 1.66         | 0.011   | <0.5     | 6.90     | 9        | 2620     | 0.6      | <2       | 2.35     | <0.5     | 1        | 147      | 4        | 2.82     | 6.99     |
| N609209            |                          | 1.48         | 0.660   | <0.5     | 7.10     | 19       | 2190     | 0.6      | <2       | 1.80     | <0.5     | 2        | 110      | 8        | 4.20     | 6.60     |
| N609210            |                          | 2.04         | 0.030   | <0.5     | 7.37     | 5        | 2400     | 0.6      | <2       | 1.17     | <0.5     | 2        | 158      | 8        | 3.62     | 7.03     |
| N609211            |                          | 1.78         | <0.005  | <0.5     | 6.93     | 6        | 2460     | 0.5      | <2       | 1.48     | <0.5     | 1        | 102      | 8        | 3.23     | 7.32     |
| N609212            |                          | 2.14         | 0.087   | <0.5     | 7.04     | <5       | 2110     | 0.6      | 3        | 1.26     | <0.5     | 2        | 114      | 10       | 4.05     | 6.94     |
| N609213            |                          | 1.76         | <0.005  | <0.5     | 6.01     | <5       | 2170     | 0.5      | <2       | 5.03     | <0.5     | 3        | 90       | 7        | 4.19     | 5.89     |
| N609214            |                          | 1.86         | 0.027   | <0.5     | 6.65     | <5       | 2200     | 0.6      | 2        | 3.58     | <0.5     | 3        | 105      | 6        | 3.86     | 6.81     |
| N609215            |                          | 0.98         | <0.005  | <0.5     | 7.22     | 5        | 2430     | 0.7      | 3        | 1.32     | <0.5     | 4        | 91       | 22       | 3.69     | 7.02     |





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Page: 2 - B  
Total # Pages: 2 (A - B)  
Finalized Date: 26-AUG-2004  
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Project: Stewart

## CERTIFICATE OF ANALYSIS VA04054015

| Sample Description | Method Analyte Units LOR | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | Mg %     | Mn ppm   | Mo ppm   | Na %     | Ni ppm   | P ppm    | Pb ppm   | S %      | Sb ppm   | Sr ppm   | Ti %     | V ppm    | W ppm    | Zn ppm   |
|                    |                          | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        |
| N599676            |                          | 0.80     | 716      | 4        | 0.06     | 3        | 350      | 3        | 0.03     | <5       | 79       | 0.14     | 41       | 40       | 31       |
| N599677            |                          | 1.35     | 1545     | 2        | 0.07     | 2        | 390      | 11       | 0.25     | 9        | 118      | 0.14     | 51       | <10      | 28       |
| N599678            |                          | 0.79     | 1020     | 5        | 0.07     | 3        | 430      | 14       | 0.05     | 6        | 95       | 0.17     | 50       | <10      | 27       |
| N599679            |                          | 0.71     | 1275     | 2        | 0.04     | 2        | 400      | 37       | 0.07     | 20       | 80       | 0.16     | 43       | 10       | 100      |
| N599680            |                          | 0.77     | 1335     | 4        | 0.07     | 2        | 390      | 4        | 0.05     | 14       | 65       | 0.15     | 45       | 10       | 33       |
| N599681            |                          | 0.69     | 1545     | 3        | 0.08     | 2        | 410      | 6        | 0.08     | 7        | 62       | 0.16     | 45       | <10      | 29       |
| N599682            |                          | 0.88     | 1830     | 4        | 0.08     | 1        | 400      | 5        | 0.13     | 7        | 77       | 0.16     | 45       | <10      | 32       |
| N599683            |                          | 0.58     | 1370     | 2        | 0.08     | 1        | 410      | 7        | 0.14     | 11       | 60       | 0.16     | 42       | 10       | 29       |
| N599684            |                          | 0.63     | 1410     | 6        | 0.08     | 3        | 400      | 7        | 0.20     | 9        | 75       | 0.16     | 42       | 10       | 26       |
| N599685            |                          | 0.67     | 1575     | 14       | 0.06     | 2        | 410      | 37       | 0.20     | 89       | 87       | 0.15     | 41       | 10       | 82       |
| N599686            |                          | 6.97     | 1050     | <1       | 0.13     | 2540     | 580      | 12       | 2.98     | 12       | 41       | 0.39     | 164      | <10      | 100      |
| N599687            |                          | 0.63     | 1425     | 5        | 0.07     | 3        | 460      | 41       | 0.31     | 58       | 88       | 0.17     | 44       | <10      | 101      |
| N599688            |                          | 0.59     | 1480     | 8        | 0.06     | 1        | 450      | 80       | 0.29     | 66       | 61       | 0.18     | 49       | <10      | 112      |
| N599689            |                          | 0.72     | 1230     | 3        | 0.09     | <1       | 410      | 3        | 0.21     | 8        | 86       | 0.16     | 42       | <10      | 21       |
| N599690            |                          | 1.39     | 1395     | 3        | 0.10     | 1        | 400      | 7        | 0.24     | 9        | 124      | 0.16     | 53       | <10      | 19       |
| N599691            |                          | 0.58     | 1190     | 1        | 0.09     | <1       | 410      | 7        | 0.06     | 6        | 83       | 0.16     | 43       | 20       | 26       |
| N609205            |                          | 0.42     | 833      | 5        | 0.13     | 3        | 460      | 9        | 0.10     | 7        | 118      | 0.18     | 49       | 10       | 15       |
| N609206            |                          | 0.46     | 818      | 2        | 0.14     | 3        | 450      | 8        | 0.05     | 5        | 121      | 0.17     | 49       | 10       | 14       |
| N609207            |                          | 0.58     | 1020     | 7        | 0.14     | 1        | 450      | 7        | 0.12     | 9        | 141      | 0.18     | 48       | 10       | 20       |
| N609208            |                          | 0.61     | 824      | 2        | 0.17     | 1        | 420      | 6        | 0.06     | 7        | 156      | 0.17     | 48       | 10       | 18       |
| N609209            |                          | 0.52     | 1050     | 5        | 0.16     | 3        | 430      | 6        | 0.12     | <5       | 126      | 0.17     | 52       | 40       | 17       |
| N609210            |                          | 0.37     | 837      | 3        | 0.14     | 4        | 460      | 3        | 0.03     | <5       | 117      | 0.18     | 49       | 20       | 17       |
| N609211            |                          | 0.39     | 797      | 5        | 0.17     | <1       | 450      | 2        | 0.07     | <5       | 124      | 0.17     | 46       | <10      | 15       |
| N609212            |                          | 0.43     | 1080     | 3        | 0.14     | 3        | 450      | 2        | 0.12     | 6        | 117      | 0.17     | 47       | 20       | 19       |
| N609213            |                          | 1.42     | 1655     | 5        | 0.15     | <1       | 370      | 6        | 0.07     | <5       | 237      | 0.14     | 75       | 10       | 30       |
| N609214            |                          | 0.96     | 1235     | 3        | 0.15     | 1        | 420      | 4        | 0.06     | <5       | 188      | 0.16     | 57       | 10       | 20       |
| N609215            |                          | 0.36     | 1015     | 4        | 0.17     | 2        | 440      | 9        | 0.08     | <5       | 136      | 0.18     | 46       | <10      | 21       |



# ALS Chemex

**EXCELLENCE IN ANALYTICAL CHEMISTRY**

ALS Canada Ltd.

212 Brooksbank Avenue

North Vancouver BC V7J 2C1 Canada

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To: GEOFINE EXPLORATION CONSULTANTS LTD.  
49 NORMANDALE RD  
UNIONVILLE ON L3R 4J8

Page: 2 - A  
Total # Pages: 2 (A - B)  
Finalized Date: 27-AUG-2004  
Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04054019

| Sample Description | Method Analyte Units LOR | WEI-21       | Au-AA23 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|--------------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | Recvd Wt. kg | Au ppm  | Ag ppm   | Al %     | As ppm   | Ba ppm   | Be ppm   | Bi ppm   | Ca %     | Cd ppm   | Co ppm   | Cr ppm   | Cu ppm   | Fe %     | K %      |
|                    |                          | 0.02         | 0.005   | 0.5      | 0.01     | 5        | 10       | 0.5      | 2        | 0.01     | 0.5      | 1        | 1        | 1        | 0.01     | 0.01     |
| N599551            |                          | 1.96         | 0.010   | <0.5     | 7.48     | 7        | 2120     | 0.7      | 4        | 0.44     | 0.6      | 6        | 85       | 206      | 3.67     | 5.85     |
| N599552            |                          | 1.88         | 0.005   | <0.5     | 6.88     | 30       | 940      | 0.6      | 4        | 1.10     | <0.5     | 5        | 99       | 14       | 2.99     | 6.18     |
| N599553            |                          | 1.68         | 0.007   | <0.5     | 7.83     | 28       | 820      | 1.0      | 4        | 0.79     | <0.5     | 7        | 76       | 177      | 3.64     | 5.37     |
| N599554            |                          | 1.78         | <0.005  | <0.5     | 7.61     | <5       | 3880     | 0.8      | <2       | 1.57     | <0.5     | 2        | 63       | 29       | 2.71     | 5.98     |
| N599555            |                          | 1.32         | 0.007   | <0.5     | 7.52     | <5       | 2370     | 0.8      | 2        | 0.47     | <0.5     | 5        | 64       | 252      | 3.56     | 5.30     |
| N599556            |                          | 1.44         | <0.005  | <0.5     | 7.33     | 7        | 2450     | 0.8      | <2       | 0.63     | <0.5     | 3        | 43       | 40       | 3.13     | 5.62     |
| N599557            |                          | 1.72         | 0.005   | <0.5     | 7.19     | <5       | 2240     | 0.7      | 4        | 1.62     | <0.5     | 2        | 42       | 335      | 3.73     | 5.39     |
| N599558            |                          | 2.24         | 0.008   | <0.5     | 7.38     | 12       | 500      | 0.7      | 5        | 1.62     | <0.5     | 8        | 71       | 665      | 4.13     | 5.76     |
| N599559            |                          | 1.94         | 0.005   | <0.5     | 7.80     | 33       | 800      | 0.7      | 2        | 1.43     | <0.5     | 6        | 54       | 93       | 3.95     | 5.34     |
| N599560            |                          | 1.80         | 0.005   | <0.5     | 7.94     | 21       | 870      | 0.7      | 4        | 0.88     | <0.5     | 8        | 49       | 59       | 3.82     | 5.71     |
| N599561            |                          | 2.22         | <0.005  | <0.5     | 7.08     | 6        | 2180     | 0.6      | 2        | 1.17     | <0.5     | 5        | 104      | 21       | 3.46     | 5.15     |
| N599562            |                          | 1.90         | <0.005  | <0.5     | 7.82     | 7        | 2150     | 0.7      | 3        | 0.80     | <0.5     | 2        | 58       | 10       | 3.14     | 5.93     |
| N599563            |                          | 1.44         | <0.005  | <0.5     | 7.96     | 22       | 2300     | 0.7      | <2       | 0.56     | <0.5     | 3        | 86       | 38       | 3.14     | 6.27     |
| N599564            |                          | 1.74         | <0.005  | <0.5     | 7.74     | 8        | 2370     | 0.6      | 3        | 0.65     | <0.5     | 4        | 53       | 5        | 3.14     | 6.39     |
| N599565            |                          | 1.86         | <0.005  | <0.5     | 8.07     | 18       | 2040     | 0.7      | <2       | 0.61     | <0.5     | 2        | 75       | 132      | 3.76     | 6.07     |
| N599566            |                          | 1.92         | <0.005  | <0.5     | 7.75     | 15       | 2140     | 0.7      | 2        | 0.38     | <0.5     | 3        | 49       | 48       | 3.32     | 5.98     |
| N599567            |                          | 2.08         | <0.005  | <0.5     | 7.40     | 11       | 2240     | 0.6      | 3        | 0.66     | <0.5     | 4        | 87       | 16       | 3.54     | 5.32     |
| N599567A           |                          | 0.06         | 1.790   | 2.3      | 8.45     | 150      | 40       | <0.5     | <2       | 4.14     | <0.5     | 210      | 28       | 8570     | 11.55    | 0.52     |
| N609186            |                          | 2.10         | 0.116   | <0.5     | 7.15     | 9        | 2240     | 0.6      | <2       | 1.30     | <0.5     | 1        | 34       | 257      | 3.90     | 5.56     |
| N609187            |                          | 1.70         | <0.005  | <0.5     | 7.48     | 11       | 2520     | 0.7      | 3        | 1.40     | <0.5     | 3        | 59       | 31       | 3.32     | 5.51     |
| N609188            |                          | 1.34         | <0.005  | <0.5     | 7.34     | <5       | 2250     | 0.6      | 2        | 1.48     | <0.5     | 4        | 33       | 9        | 3.36     | 6.06     |
| N609189            |                          | 1.64         | 0.018   | <0.5     | 7.19     | 37       | 760      | 0.6      | 5        | 0.92     | <0.5     | 4        | 67       | 919      | 4.21     | 4.96     |
| N609190            |                          | 1.84         | 0.013   | <0.5     | 6.97     | 30       | 320      | 0.6      | 3        | 1.56     | <0.5     | 5        | 47       | 441      | 4.04     | 5.85     |
| N609191            |                          | 1.92         | 0.017   | <0.5     | 6.84     | 46       | 230      | 0.6      | 3        | 0.88     | <0.5     | 6        | 89       | 1555     | 4.44     | 5.19     |
| N609192            |                          | 1.86         | <0.005  | <0.5     | 7.07     | 30       | 480      | 0.6      | 3        | 1.31     | <0.5     | 5        | 51       | 70       | 3.83     | 5.41     |
| N609193            |                          | 1.86         | 0.008   | <0.5     | 7.63     | 18       | 520      | 0.6      | 3        | 0.48     | <0.5     | 5        | 96       | 50       | 4.01     | 5.61     |
| N609194            |                          | 1.92         | 0.013   | <0.5     | 7.00     | 16       | 1000     | 0.6      | 6        | 0.77     | <0.5     | 5        | 97       | 225      | 3.70     | 4.77     |
| N609195            |                          | 1.84         | 0.010   | <0.5     | 6.55     | 23       | 520      | 0.6      | 6        | 1.16     | <0.5     | 6        | 93       | 253      | 4.39     | 5.05     |
| N609196            |                          | 1.86         | 0.008   | 0.5      | 6.84     | 32       | 640      | 0.6      | 6        | 1.20     | <0.5     | 8        | 98       | 1610     | 4.69     | 5.28     |
| N609197            |                          | 1.56         | <0.005  | <0.5     | 7.80     | 26       | 2280     | 0.7      | 3        | 0.38     | <0.5     | 5        | 81       | 31       | 3.42     | 6.32     |
| N609198            |                          | 1.88         | <0.005  | <0.5     | 7.14     | 16       | 2370     | 0.5      | 4        | 0.58     | <0.5     | 5        | 83       | 669      | 3.45     | 6.03     |
| N609199            |                          | 1.96         | <0.005  | <0.5     | 7.56     | 20       | 2560     | 0.6      | 5        | 0.99     | <0.5     | 7        | 66       | 68       | 3.58     | 6.56     |
| N609200            |                          | 0.06         | 1.660   | 2.8      | 8.54     | 142      | 40       | <0.5     | 4        | 4.14     | <0.5     | 218      | 28       | 8950     | 11.70    | 0.56     |



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 49 NORMANDE RD  
 UNIONVILLE ON L3R 4J8

Page: 2 - B  
 Total # Pages: 2 (A - B)  
 Finalized Date: 27-AUG-2004  
 Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04054019

| Sample Description | Method Analyte Units LOR | ME-ICP61     | ME-ICP61    | ME-ICP61    | ME-ICP61     | ME-ICP61    | ME-ICP61    | ME-ICP61    | ME-ICP61    | ME-ICP61    | ME-ICP61    | ME-ICP61     | ME-ICP61   | ME-ICP61    | ME-ICP61    |
|--------------------|--------------------------|--------------|-------------|-------------|--------------|-------------|-------------|-------------|-------------|-------------|-------------|--------------|------------|-------------|-------------|
|                    |                          | Mg %<br>0.01 | Mn ppm<br>5 | Mo ppm<br>1 | Na %<br>0.01 | Ni ppm<br>1 | P ppm<br>10 | Pb ppm<br>2 | S %<br>0.01 | Sb ppm<br>5 | Sr ppm<br>1 | Ti %<br>0.01 | V ppm<br>1 | W ppm<br>10 | Zn ppm<br>2 |
| N599551            |                          | 0.46         | 407         | 4           | 0.10         | <1          | 470         | 8           | 1.18        | <5          | 75          | 0.18         | 53         | 10          | 34          |
| N599552            |                          | 0.48         | 914         | 14          | 0.10         | 2           | 460         | 7           | 1.34        | <5          | 149         | 0.17         | 56         | <10         | 22          |
| N599553            |                          | 0.43         | 349         | 5           | 0.18         | 2           | 510         | 13          | 1.66        | <5          | 133         | 0.19         | 55         | 10          | 34          |
| N599554            |                          | 0.68         | 1170        | 2           | 1.14         | 1           | 510         | 2           | 0.12        | <5          | 216         | 0.19         | 50         | <10         | 30          |
| N599555            |                          | 0.68         | 265         | 4           | 0.60         | <1          | 560         | 7           | 0.85        | 5           | 89          | 0.18         | 62         | <10         | 34          |
| N599556            |                          | 0.77         | 418         | 1           | 0.62         | 2           | 470         | 4           | 0.06        | <5          | 100         | 0.19         | 52         | <10         | 57          |
| N599557            |                          | 0.71         | 1085        | 3           | 0.08         | <1          | 460         | 8           | 1.25        | <5          | 192         | 0.17         | 52         | <10         | 40          |
| N599558            |                          | 0.56         | 953         | 5           | 0.09         | <1          | 450         | 10          | 2.37        | <5          | 197         | 0.18         | 57         | 10          | 31          |
| N599559            |                          | 0.69         | 1165        | 5           | 0.13         | 1           | 480         | 6           | 1.96        | <5          | 162         | 0.19         | 60         | <10         | 34          |
| N599560            |                          | 0.60         | 722         | 4           | 0.49         | <1          | 500         | <2          | 1.94        | <5          | 94          | 0.20         | 60         | <10         | 33          |
| N599561            |                          | 0.58         | 921         | 4           | 0.09         | 4           | 490         | 5           | 1.01        | <5          | 90          | 0.17         | 50         | 10          | 29          |
| N599562            |                          | 0.55         | 663         | 2           | 0.09         | 2           | 510         | 2           | 0.39        | <5          | 67          | 0.18         | 56         | <10         | 29          |
| N599563            |                          | 0.45         | 451         | 2           | 0.09         | 2           | 520         | <2          | 0.42        | <5          | 71          | 0.20         | 51         | 10          | 29          |
| N599564            |                          | 0.46         | 587         | 2           | 0.09         | 2           | 500         | 4           | 0.47        | <5          | 71          | 0.18         | 46         | <10         | 28          |
| N599565            |                          | 0.56         | 596         | 2           | 0.09         | <1          | 500         | <2          | 0.44        | <5          | 56          | 0.19         | 57         | 10          | 37          |
| N599566            |                          | 0.42         | 351         | 2           | 0.09         | 1           | 490         | 2           | 0.54        | <5          | 55          | 0.18         | 48         | <10         | 34          |
| N599567            |                          | 0.46         | 602         | 6           | 0.09         | 4           | 460         | 6           | 0.97        | 8           | 66          | 0.18         | 51         | 10          | 37          |
| N599567A           |                          | 2.47         | 1760        | 1           | 1.06         | 85          | 170         | 12          | 2.79        | <5          | 60          | 0.15         | 103        | 10          | 135         |
| N609186            |                          | 0.73         | 1030        | 2           | 0.16         | 1           | 450         | 2           | 0.70        | 7           | 89          | 0.17         | 51         | 10          | 35          |
| N609187            |                          | 0.65         | 1045        | <1          | 0.11         | 1           | 470         | 2           | 0.78        | <5          | 109         | 0.18         | 49         | 10          | 26          |
| N609188            |                          | 0.64         | 1005        | 1           | 0.12         | <1          | 480         | <2          | 0.46        | <5          | 104         | 0.17         | 48         | 10          | 30          |
| N609189            |                          | 0.53         | 752         | 5           | 0.10         | 1           | 450         | 5           | 2.04        | <5          | 76          | 0.18         | 59         | 10          | 29          |
| N609190            |                          | 0.61         | 1110        | 7           | 0.11         | <1          | 460         | 8           | 2.42        | <5          | 83          | 0.16         | 52         | 10          | 21          |
| N609191            |                          | 0.49         | 665         | 9           | 0.08         | <1          | 430         | 10          | 2.76        | 7           | 60          | 0.17         | 53         | <10         | 25          |
| N609192            |                          | 0.61         | 1020        | 4           | 0.10         | 1           | 440         | 3           | 2.34        | 7           | 69          | 0.17         | 50         | 10          | 19          |
| N609193            |                          | 0.42         | 362         | 4           | 0.13         | 1           | 470         | 8           | 2.37        | <5          | 58          | 0.19         | 53         | <10         | 24          |
| N609194            |                          | 0.48         | 597         | 3           | 0.13         | 2           | 460         | 3           | 1.63        | <5          | 70          | 0.16         | 45         | <10         | 27          |
| N609195            |                          | 0.59         | 1105        | 7           | 0.07         | 2           | 410         | 11          | 2.24        | <5          | 57          | 0.15         | 47         | <10         | 32          |
| N609196            |                          | 0.63         | 1230        | 10          | 0.07         | 2           | 430         | 20          | 2.12        | 8           | 74          | 0.16         | 55         | <10         | 35          |
| N609197            |                          | 0.44         | 400         | 4           | 0.09         | 3           | 480         | 7           | 0.81        | <5          | 52          | 0.19         | 53         | <10         | 35          |
| N609198            |                          | 0.47         | 621         | 4           | 0.09         | 2           | 440         | 3           | 0.53        | <5          | 67          | 0.17         | 52         | <10         | 40          |
| N609199            |                          | 0.56         | 910         | 4           | 0.10         | <1          | 500         | 7           | 1.01        | 5           | 110         | 0.18         | 58         | <10         | 33          |
| N609200            |                          | 2.56         | 1795        | 4           | 1.10         | 88          | 170         | 6           | 2.76        | 5           | 62          | 0.15         | 104        | 10          | 126         |



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 49 NORMANDALE RD  
 UNIONVILLE ON L3R 4J8

Page: 2 - A  
 Total # Pages: 3 (A - C)  
 Finalized Date: 30-AUG-2004  
 Account: KIV

Project: Stewart

SZD04-04

## CERTIFICATE OF ANALYSIS VA04053799

| Sample Description | Method Analyte Units LOR | WEI-21    | Au-AA23 | Au-GRA21 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|-----------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | Recvd Wt. | Au      | Au       | Ag       | Al       | As       | Ba       | Be       | Bi       | Ca       | Cd       | Co       | Cr       | Cu       | Fe       |
|                    |                          | kg        | ppm     | ppm      | ppm      | %        | ppm      | ppm      | ppm      | ppm      | %        | ppm      | ppm      | ppm      | ppm      | ppm      |
|                    | 0.02                     | 0.005     | 0.05    | 0.5      | 0.01     | 5        | 10       | 0.5      | 2        | 0.01     | 0.5      | 1        | 1        | 1        | 0.01     |          |
| N599692            |                          | 1.34      | 0.138   |          | <0.5     | 7.80     | 31       | 2720     | 0.7      | <2       | 1.83     | <0.5     | 11       | 21       | 72       | 5.04     |
| N599693            |                          | 1.94      | <0.005  |          | <0.5     | 7.71     | <5       | 2610     | 0.7      | 3        | 1.14     | <0.5     | 3        | 5        | 22       | 3.24     |
| N599694            |                          | 2.24      | 0.020   |          | <0.5     | 7.60     | 6        | 2480     | 0.7      | <2       | 1.24     | <0.5     | 6        | 19       | 33       | 3.23     |
| N599695            |                          | 1.10      | 0.070   |          | <0.5     | 6.85     | 19       | 1980     | 0.6      | 2        | 1.78     | <0.5     | 5        | 3        | 9        | 3.27     |
| N599696            |                          | 1.54      | 0.154   |          | <0.5     | 6.78     | 16       | 2310     | 0.6      | <2       | 3.03     | <0.5     | 7        | 23       | 229      | 3.29     |
| N599697            |                          | 1.36      | <0.005  |          | <0.5     | 7.14     | <5       | 2430     | 0.6      | <2       | 1.48     | <0.5     | 4        | 5        | 46       | 3.81     |
| N599698            |                          | 1.58      | 0.012   |          | <0.5     | 7.39     | 5        | 2210     | 0.7      | 2        | 1.39     | <0.5     | 3        | 18       | 34       | 3.33     |
| N599699            |                          | 1.26      | 0.007   |          | <0.5     | 7.57     | <5       | 4420     | 0.8      | <2       | 2.11     | <0.5     | 4        | 6        | 10       | 4.12     |
| N599700            |                          | 1.80      | 0.011   |          | <0.5     | 7.55     | 5        | 2230     | 0.8      | <2       | 1.34     | <0.5     | 5        | 5        | 61       | 3.40     |
| N609201            |                          | 0.06      | 1.190   |          | 3.6      | 8.63     | 150      | 40       | <0.5     | 4        | 4.21     | <0.5     | 205      | 27       | 8240     | 11.70    |
| N609202            |                          | 1.72      | 0.007   |          | <0.5     | 7.42     | <5       | 1780     | 0.9      | <2       | 1.88     | <0.5     | 4        | 3        | 13       | 3.42     |
| N609203            |                          | 2.38      | <0.005  |          | <0.5     | 7.20     | 12       | 2550     | 0.6      | <2       | 1.54     | <0.5     | 7        | 4        | 136      | 3.55     |
| N609204            |                          | 2.48      | 0.036   |          | <0.5     | 7.38     | 6        | 2710     | 0.6      | <2       | 1.24     | <0.5     | 6        | 6        | 12       | 3.66     |
| N609216            |                          | 1.44      | 0.006   |          | <0.5     | 7.66     | <5       | 1780     | 0.9      | 2        | 1.88     | <0.5     | 4        | 2        | 11       | 2.96     |
| N609217            |                          | 1.30      | <0.005  |          | <0.5     | 7.40     | <5       | 2790     | 0.7      | <2       | 1.46     | <0.5     | 3        | 4        | 15       | 3.00     |
| N609218            |                          | 2.36      | <0.005  |          | <0.5     | 7.72     | <5       | 2640     | 0.7      | 3        | 1.36     | <0.5     | 3        | 3        | 18       | 3.43     |
| N609219            |                          | 0.06      | 0.092   |          | 2.7      | 4.57     | <5       | 100      | <0.5     | 5        | 10.05    | <0.5     | 176      | 473      | 6100     | 11.15    |
| N609220            |                          | 2.56      | 0.013   |          | <0.5     | 7.10     | 6        | 2250     | 0.7      | <2       | 2.29     | <0.5     | 5        | 5        | 105      | 3.82     |
| N609221            |                          | 1.80      | 0.071   |          | <0.5     | 6.52     | 11       | 2000     | 0.6      | 2        | 3.38     | <0.5     | 7        | 3        | 13       | 3.26     |
| N609222            |                          | 1.76      | 0.022   |          | <0.5     | 6.91     | 14       | 1700     | 0.6      | <2       | 1.44     | <0.5     | 7        | 3        | 14       | 4.16     |
| N609223            |                          | 2.00      | <0.005  |          | <0.5     | 7.07     | <5       | 2300     | 0.6      | <2       | 1.34     | <0.5     | 4        | 17       | 75       | 3.54     |
| N609224            |                          | 2.02      | 0.006   |          | <0.5     | 6.60     | 5        | 2310     | 0.6      | <2       | 1.52     | <0.5     | 3        | 3        | 469      | 3.54     |
| N609225            |                          | 1.98      | 0.062   |          | <0.5     | 7.36     | 12       | 2520     | 0.7      | 2        | 1.30     | <0.5     | 4        | 9        | 41       | 3.61     |
| N609226            |                          | 1.98      | 9.83    |          | 1.6      | 2.75     | 11       | 560      | 0.7      | 2        | 3.57     | <0.5     | 5        | <1       | >10000   | 5.37     |
| N609227            |                          | 2.14      | >10.0   | 11.10    | 1.4      | 1.82     | 10       | 420      | 0.5      | 2        | 5.86     | <0.5     | 7        | 28       | 7770     | 5.22     |
| N609228            |                          | 1.88      | 0.172   |          | <0.5     | 5.37     | 8        | 1000     | 0.9      | <2       | 1.00     | <0.5     | 6        | 5        | 358      | 5.96     |
| N609228A           |                          | 0.08      | 1.460   |          | 2.7      | 8.56     | 114      | 50       | <0.5     | 4        | 4.40     | <0.5     | 220      | 31       | 8580     | 11.90    |
| N609229            |                          | 2.00      | 0.247   |          | <0.5     | 4.15     | 13       | 790      | 0.7      | <2       | 1.59     | <0.5     | 5        | 43       | 774      | 5.97     |
| N609230            |                          | 1.64      | 0.285   |          | <0.5     | 5.62     | 20       | 1170     | 0.8      | <2       | 1.64     | <0.5     | 4        | 4        | 236      | 4.89     |
| N609231            |                          | 2.12      | 1.045   |          | <0.5     | 3.97     | 43       | 1440     | 0.7      | <2       | 2.20     | <0.5     | 8        | 34       | 643      | 6.65     |
| N609232            |                          | 2.22      | 0.080   |          | <0.5     | 5.71     | 25       | 2810     | 0.7      | <2       | 1.50     | <0.5     | 7        | 3        | 492      | 5.62     |
| N609233            |                          | 1.78      | 4.15    |          | 1.0      | 3.95     | 11       | 630      | 0.7      | <2       | 2.68     | <0.5     | 8        | 3        | 4460     | 5.48     |
| N609234            |                          | 1.98      | 0.258   |          | <0.5     | 7.42     | 21       | 330      | 1.0      | <2       | 2.25     | <0.5     | 14       | 7        | 1440     | 9.57     |
| N609235            |                          | 1.18      | 1.985   |          | 0.5      | 7.55     | 13       | 6180     | 1.0      | <2       | 2.53     | <0.5     | 10       | 3        | 1500     | 9.33     |
| N609236            |                          | 0.08      | 8.66    |          | 2.1      | 6.22     | 12       | 1630     | 3.4      | <2       | 4.86     | <0.5     | 27       | 161      | 119      | 4.89     |
| N609237            |                          | 2.10      | 0.052   |          | <0.5     | 7.97     | 13       | 2960     | 1.2      | <2       | 2.01     | <0.5     | 16       | 9        | 319      | 9.73     |
| N609238            |                          | 1.46      | 0.113   |          | <0.5     | 7.64     | 11       | 2680     | 1.2      | <2       | 2.04     | <0.5     | 21       | 3        | 2410     | 8.71     |
| N609239            |                          | 2.26      | 0.016   |          | <0.5     | 8.63     | 16       | 2950     | 1.0      | <2       | 1.90     | <0.5     | 12       | 5        | 377      | 8.84     |
| N609240            |                          | 1.68      | 0.031   |          | <0.5     | 7.55     | 11       | 1640     | 0.9      | <2       | 4.51     | <0.5     | 18       | 2        | 50       | 8.68     |
| N609241            |                          | 1.32      | 0.008   |          | <0.5     | 8.55     | 6        | 4690     | 1.2      | <2       | 4.04     | <0.5     | 10       | 2        | 18       | 5.64     |



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Total # Pages: 3 (A - C)

Finalized Date: 30-AUG-2004

Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04053799

| Sample Description | Method Analyte Units LOR | ME-ICP61  | ME-ICP61  | ME-ICP61 | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61  | ME-ICP61 |
|--------------------|--------------------------|-----------|-----------|----------|----------|-----------|----------|-----------|----------|-----------|----------|----------|-----------|----------|-----------|----------|
|                    |                          | K         | Mg        | Mn       | Mo       | Na        | Ni       | P         | Pb       | S         | Sb       | Sr       | Ti        | V        | W         | Zn       |
|                    |                          | %<br>0.01 | %<br>0.01 | ppm<br>5 | ppm<br>1 | %<br>0.01 | ppm<br>1 | ppm<br>10 | ppm<br>2 | %<br>0.01 | ppm<br>5 | ppm<br>1 | %<br>0.01 | ppm<br>1 | ppm<br>10 | ppm<br>2 |
| N599692            |                          | 6.08      | 0.65      | 1340     | 1        | 0.17      | 3        | 670       | 9        | 0.53      | <5       | 186      | 0.24      | 74       | 10        | 33       |
| N599693            |                          | 6.94      | 0.36      | 684      | 1        | 0.16      | 2        | 480       | 5        | 0.02      | <5       | 142      | 0.17      | 46       | <10       | 20       |
| N599694            |                          | 5.57      | 0.33      | 817      | 1        | 0.17      | 2        | 480       | 4        | 0.12      | <5       | 161      | 0.18      | 49       | 10        | 19       |
| N599695            |                          | 5.88      | 0.39      | 1055     | 1        | 0.13      | 3        | 440       | 6        | 0.24      | <5       | 176      | 0.16      | 44       | 10        | 20       |
| N599696            |                          | 6.15      | 0.54      | 1120     | 1        | 0.15      | 3        | 510       | 10       | 0.37      | <5       | 305      | 0.17      | 56       | 10        | 20       |
| N599697            |                          | 4.81      | 0.43      | 1080     | 1        | 0.13      | <1       | 470       | 5        | 0.05      | 6        | 133      | 0.16      | 46       | <10       | 23       |
| N599698            |                          | 6.44      | 0.40      | 828      | 5        | 0.12      | 4        | 490       | 4        | 0.01      | <5       | 124      | 0.18      | 47       | <10       | 22       |
| N599699            |                          | 6.26      | 0.61      | 1245     | 1        | 0.12      | 2        | 560       | 6        | 0.07      | <5       | 266      | 0.20      | 59       | <10       | 29       |
| N599700            |                          | 6.17      | 0.42      | 798      | 1        | 0.30      | 1        | 500       | 5        | 0.07      | <5       | 125      | 0.18      | 48       | <10       | 19       |
| N609201            |                          | 0.53      | 2.58      | 1870     | 2        | 1.08      | 87       | 180       | 6        | 2.75      | <5       | 60       | 0.16      | 99       | <10       | 138      |
| N609202            |                          | 5.55      | 0.59      | 1080     | 1        | 0.25      | 2        | 540       | 4        | 0.01      | <5       | 134      | 0.19      | 50       | <10       | 21       |
| N609203            |                          | 6.54      | 0.45      | 877      | 1        | 0.13      | 1        | 480       | 13       | 0.15      | 5        | 132      | 0.17      | 45       | <10       | 22       |
| N609204            |                          | 5.46      | 0.41      | 917      | 1        | 0.13      | <1       | 490       | 7        | 0.12      | 5        | 135      | 0.17      | 46       | 10        | 64       |
| N609216            |                          | 5.68      | 0.59      | 909      | <1       | 0.41      | 3        | 510       | 6        | 0.01      | <5       | 130      | 0.18      | 50       | <10       | 18       |
| N609217            |                          | 5.25      | 0.41      | 802      | 1        | 0.29      | 1        | 490       | 3        | 0.02      | <5       | 158      | 0.18      | 46       | <10       | 17       |
| N609218            |                          | 6.79      | 0.37      | 859      | 1        | 0.14      | 3        | 520       | 5        | 0.03      | <5       | 153      | 0.19      | 52       | <10       | 17       |
| N609219            |                          | 0.08      | 6.90      | 1065     | 1        | 0.13      | 2490     | 580       | 15       | 3.05      | 6        | 39       | 0.38      | 158      | <10       | 95       |
| N609220            |                          | 6.04      | 0.51      | 1075     | 1        | 0.12      | 4        | 560       | 3        | 0.16      | <5       | 194      | 0.21      | 62       | <10       | 18       |
| N609221            |                          | 4.73      | 0.74      | 1125     | 1        | 0.09      | 5        | 420       | 6        | 0.34      | <5       | 206      | 0.15      | 49       | 10        | 24       |
| N609222            |                          | 5.28      | 0.38      | 1165     | <1       | 0.11      | 3        | 460       | <2       | 0.25      | <5       | 118      | 0.16      | 40       | 10        | 21       |
| N609223            |                          | 6.35      | 0.25      | 735      | 1        | 0.16      | 1        | 490       | 7        | 0.04      | <5       | 180      | 0.18      | 50       | <10       | 16       |
| N609224            |                          | 6.09      | 0.26      | 841      | 1        | 0.16      | <1       | 440       | 7        | 0.09      | <5       | 167      | 0.17      | 47       | 10        | 15       |
| N609225            |                          | 5.89      | 0.32      | 884      | 1        | 0.13      | 3        | 470       | 5        | 0.15      | <5       | 137      | 0.17      | 43       | 10        | 18       |
| N609226            |                          | 1.47      | 0.52      | 2100     | 1        | 0.02      | 3        | 150       | 6        | 1.20      | <5       | 130      | 0.06      | 25       | 10        | 19       |
| N609227            |                          | 0.90      | 0.59      | 2510     | 2        | 0.02      | 1        | 90        | 4        | 1.02      | 8        | 190      | 0.03      | 21       | <10       | 33       |
| N609228            |                          | 3.23      | 0.68      | 1590     | 2        | 0.04      | <1       | 340       | 9        | 0.27      | 5        | 87       | 0.13      | 37       | 10        | 62       |
| N609228A           |                          | 0.55      | 2.63      | 1875     | 1        | 1.07      | 86       | 190       | 10       | 2.74      | 10       | 59       | 0.17      | 105      | 10        | 152      |
| N609229            |                          | 2.48      | 0.64      | 1710     | 2        | 0.03      | <1       | 260       | 10       | 0.44      | 7        | 148      | 0.10      | 31       | 10        | 36       |
| N609230            |                          | 3.47      | 0.63      | 1370     | 4        | 0.05      | <1       | 350       | 9        | 0.36      | 10       | 158      | 0.13      | 36       | 10        | 33       |
| N609231            |                          | 2.32      | 0.91      | 1925     | 3        | 0.03      | <1       | 240       | 7        | 0.77      | 9        | 223      | 0.09      | 32       | 10        | 38       |
| N609232            |                          | 3.81      | 0.78      | 1415     | 4        | 0.10      | <1       | 360       | 11       | 0.73      | 8        | 218      | 0.14      | 37       | 10        | 38       |
| N609233            |                          | 1.98      | 0.65      | 1775     | 4        | 0.19      | <1       | 420       | 2        | 0.86      | 7        | 1080     | 0.14      | 61       | 10        | 32       |
| N609234            |                          | 3.46      | 1.04      | 1840     | 1        | 1.22      | <1       | 1450      | 15       | 1.06      | 14       | 1715     | 0.43      | 215      | 10        | 77       |
| N609235            |                          | 5.72      | 1.03      | 1515     | <1       | 0.25      | <1       | 1590      | 9        | 0.43      | 13       | 801      | 0.44      | 215      | 20        | 65       |
| N609236            |                          | 4.29      | 3.05      | 1040     | 51       | 1.46      | 69       | 1980      | 31       | 1.06      | 14       | 1170     | 0.32      | 181      | 30        | 84       |
| N609237            |                          | 5.98      | 1.20      | 1560     | <1       | 0.58      | 1        | 1740      | 7        | 0.76      | 11       | 248      | 0.43      | 219      | 10        | 65       |
| N609238            |                          | 5.74      | 0.99      | 1500     | <1       | 0.52      | 3        | 1650      | 7        | 0.78      | 11       | 203      | 0.41      | 186      | 10        | 65       |
| N609239            |                          | 6.82      | 1.05      | 1660     | <1       | 0.31      | <1       | 1920      | 3        | 0.13      | 11       | 196      | 0.47      | 215      | 10        | 62       |
| N609240            |                          | 4.00      | 1.68      | 1915     | 3        | 0.04      | 1        | 1640      | 8        | 0.65      | 11       | 180      | 0.40      | 168      | 10        | 84       |
| N609241            |                          | 4.57      | 1.18      | 1325     | <1       | 0.05      | <1       | 1840      | 4        | 0.15      | 8        | 305      | 0.46      | 177      | 10        | 75       |





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UNIONVILLE ON L3R 4J8

Page: 2 - C  
Total # Pages: 3 (A - C)  
Finalized Date: 30-AUG-2004  
Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04053799

| Sample Description                                   | Method<br>Analyte<br>Units<br>LOR | Cu-AA62<br>Cu<br>%<br>0.01 |
|------------------------------------------------------|-----------------------------------|----------------------------|
| N599692<br>N599693<br>N599694<br>N599695<br>N599696  |                                   |                            |
| N599697<br>N599698<br>N599699<br>N599700<br>N609201  |                                   |                            |
| N609202<br>N609203<br>N609204<br>N609216<br>N609217  |                                   |                            |
| N609218<br>N609219<br>N609220<br>N609221<br>N609222  |                                   |                            |
| N609223<br>N609224<br>N609225<br>N609226<br>N609227  |                                   | 1.01                       |
| N609228<br>N609228A<br>N609229<br>N609230<br>N609231 |                                   |                            |
| N609232<br>N609233<br>N609234<br>N609235<br>N609236  |                                   |                            |
| N609237<br>N609238<br>N609239<br>N609240<br>N609241  |                                   |                            |



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Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04053799

| Sample Description | Method<br>Analyte<br>Units<br>LOR | WEI-21      | Au-AA23      | Au-GRA21    | ME-ICP61   | ME-ICP61    | ME-ICP61 | ME-ICP61  | ME-ICP61   | ME-ICP61 | ME-ICP61    | ME-ICP61   | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61    |
|--------------------|-----------------------------------|-------------|--------------|-------------|------------|-------------|----------|-----------|------------|----------|-------------|------------|----------|----------|----------|-------------|
|                    |                                   | Recvd Wt.   | Au           | Au          | Ag         | Al          | As       | Ba        | Be         | Bi       | Ca          | Cd         | Co       | Cr       | Cu       | Fe          |
|                    |                                   | kg          | ppm          | ppm         | ppm        | %           | ppm      | ppm       | ppm        | ppm      | %           | ppm        | ppm      | ppm      | ppm      | %           |
|                    |                                   | <b>0.02</b> | <b>0.005</b> | <b>0.05</b> | <b>0.5</b> | <b>0.01</b> | <b>5</b> | <b>10</b> | <b>0.5</b> | <b>2</b> | <b>0.01</b> | <b>0.5</b> | <b>1</b> | <b>1</b> | <b>1</b> | <b>0.01</b> |
| N609242            |                                   | 1.74        | <0.005       |             | <0.5       | 8.42        | <5       | .1400     | 1.3        | <2       | 4.98        | <0.5       | 17       | 5        | 3        | 6.38        |
| N609243            |                                   | 1.60        | <0.005       |             | <0.5       | 8.56        | 13       | 3310      | 1.1        | <2       | 5.72        | <0.5       | 21       | 5        | 1        | 6.18        |
| N609244            |                                   | 2.08        | <0.005       |             | <0.5       | 8.98        | 10       | 1980      | 1.1        | <2       | 4.65        | <0.5       | 21       | 5        | 4        | 6.62        |



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Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04053799

| Sample Description | Method<br>Analyte<br>Units<br>LOR | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|-----------------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                                   | K        | Mg       | Mn       | Mo       | Na       | Ni       | P        | Pb       | S        | Sb       | Sr       | Tl       | V        | W        | Zn       |
|                    |                                   | %        | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      |
|                    |                                   | 0.01     | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        |
| N609242            |                                   | 4.92     | 1.61     | 1635     | <1       | 0.66     | <1       | 1640     | 8        | 0.02     | 10       | 247      | 0.47     | 224      | <10      | 74       |
| N609243            |                                   | 5.36     | 1.98     | 1520     | <1       | 0.57     | 1        | 1500     | 10       | 0.06     | 9        | 383      | 0.47     | 235      | <10      | 58       |
| N609244            |                                   | 5.88     | 1.92     | 1420     | <1       | 0.87     | 3        | 1640     | 11       | 0.02     | 11       | 258      | 0.55     | 270      | 10       | 46       |



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Project: Stewart

## CERTIFICATE OF ANALYSIS VA04053799

| Sample Description            | Method<br>Analyte<br>Units<br>LOR | Cu-AA62<br>Cu<br>%<br>0.01 |
|-------------------------------|-----------------------------------|----------------------------|
| N609242<br>N609243<br>N609244 |                                   |                            |



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*S2004-0204*

**CERTIFICATE OF ANALYSIS VA04054017**

| Sample Description | Method<br>Analyte<br>Units<br>LOR | WEI-21          | Au-AA23   | Au-GRA21  | ME-ICP61  | ME-ICP61 | ME-ICP61  | ME-ICP61  | ME-ICP61  | ME-ICP61  | ME-ICP61 | ME-ICP61  | ME-ICP61  | ME-ICP61  | ME-ICP61  | ME-ICP61 |
|--------------------|-----------------------------------|-----------------|-----------|-----------|-----------|----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|-----------|-----------|----------|
|                    |                                   | Recvd Wt.<br>kg | Au<br>ppm | Au<br>ppm | Ag<br>ppm | Al<br>%  | As<br>ppm | Ba<br>ppm | Be<br>ppm | Bi<br>ppm | Ca<br>%  | Cd<br>ppm | Co<br>ppm | Cr<br>ppm | Cu<br>ppm | Fe<br>%  |
|                    |                                   | 0.02            | 0.005     | 0.05      | 0.5       | 0.01     | 5         | 10        | 0.5       | 2         | 0.01     | 0.5       | 1         | 1         | 1         | 0.01     |
| N609245            |                                   | 0.08            | 1.475     |           | 3.2       | 8.47     | 106       | 40        | <0.5      | 4         | 4.48     | <0.5      | 234       | 29        | 8820      | 12.20    |
| N609246            |                                   | 1.60            | 0.009     |           | <0.5      | 7.00     | 48        | 2160      | 0.6       | 3         | 2.52     | <0.5      | 5         | 98        | 9         | 3.07     |
| N609247            |                                   | 2.06            | <0.005    |           | <0.5      | 7.00     | 7         | 3040      | 0.6       | 2         | 2.19     | <0.5      | 2         | 82        | 6         | 2.90     |
| N609248            |                                   | 1.90            | 0.014     |           | <0.5      | 7.63     | 47        | 2760      | 0.7       | 3         | 1.38     | <0.5      | 2         | 96        | 33        | 2.95     |
| N609249            |                                   | 1.50            | 0.006     |           | <0.5      | 7.98     | 30        | 2670      | 0.6       | 4         | 1.70     | <0.5      | 4         | 82        | 43        | 3.23     |
| N609250            |                                   | 0.90            | 0.014     |           | <0.5      | 7.52     | 42        | 1710      | 0.7       | 3         | 0.98     | <0.5      | 4         | 88        | 89        | 3.67     |
| N609751            |                                   | 2.22            | 1.740     |           | <0.5      | 4.44     | 30        | 550       | 0.6       | 2         | 0.93     | <0.5      | 5         | 126       | 1765      | 4.46     |
| N609752            |                                   | 2.08            | 0.358     |           | <0.5      | 5.52     | <5        | 2520      | 0.7       | 3         | 2.40     | <0.5      | 3         | 123       | 1150      | 4.25     |
| N609753            |                                   | 1.94            | 0.091     |           | <0.5      | 4.62     | <5        | 720       | 0.7       | 2         | 0.83     | <0.5      | 3         | 78        | 1080      | 4.67     |
| N609754            |                                   | 1.88            | >10.0     | 10.20     | 1.0       | 1.25     | <5        | 190       | <0.5      | <2        | 5.49     | <0.5      | 2         | 198       | >10000    | 4.21     |
| N609755            |                                   | 1.32            | 2.92      |           | 0.7       | 3.95     | 8         | 440       | 0.6       | 2         | 2.77     | <0.5      | 4         | 65        | 9300      | 5.95     |
| N609756            |                                   | 1.48            | 1.685     |           | <0.5      | 4.66     | 21        | 540       | 0.6       | 4         | 2.14     | <0.5      | 4         | 95        | 2260      | 5.54     |
| N609757            |                                   | 1.84            | 0.180     |           | <0.5      | 6.25     | 13        | 700       | 0.8       | 3         | 2.68     | <0.5      | 3         | 93        | 378       | 3.46     |
| N609758            |                                   | 1.92            | 0.075     |           | <0.5      | 6.70     | 5         | 1210      | 0.7       | 5         | 2.34     | <0.5      | 3         | 113       | 110       | 4.13     |
| N609759            |                                   | 1.90            | 0.035     |           | <0.5      | 5.82     | <5        | 1100      | 0.6       | 3         | 2.00     | <0.5      | 3         | 116       | 38        | 3.59     |
| N609760            |                                   | 1.92            | 0.094     |           | <0.5      | 5.25     | 10        | 960       | 0.6       | 2         | 1.76     | <0.5      | 3         | 155       | 302       | 3.41     |
| N609761            |                                   | 0.08            | 3.28      |           | <0.5      | 6.82     | 7         | 2070      | 3.3       | 2         | 4.66     | <0.5      | 25        | 144       | 102       | 5.07     |
| N609762            |                                   | 1.80            | 0.460     |           | <0.5      | 6.37     | <5        | 1320      | 0.7       | 2         | 1.84     | <0.5      | 3         | 161       | 232       | 4.92     |
| N609763            |                                   | 2.34            | 0.153     |           | <0.5      | 5.52     | 5         | 780       | 0.8       | <2        | 1.22     | <0.5      | 4         | 110       | 342       | 6.06     |
| N609764            |                                   | 2.38            | 0.234     |           | <0.5      | 5.69     | 8         | 500       | 0.8       | 2         | 1.22     | <0.5      | 4         | 119       | 72        | 7.29     |
| N609765            |                                   | 1.32            | 3.50      |           | <0.5      | 2.77     | 6         | 1720      | 0.6       | 4         | 0.73     | <0.5      | 6         | 196       | 2220      | 7.95     |
| N609766            |                                   | 2.04            | 0.075     |           | <0.5      | 6.78     | 14        | 2290      | 0.9       | 2         | 0.81     | <0.5      | 4         | 77        | 478       | 4.10     |
| N609767            |                                   | 1.90            | 0.487     |           | <0.5      | 6.03     | <5        | 2830      | 0.7       | <2        | 2.46     | <0.5      | 4         | 118       | 758       | 3.48     |
| N609768            |                                   | 1.64            | 0.249     |           | <0.5      | 6.90     | <5        | 2150      | 0.7       | 3         | 0.81     | <0.5      | 3         | 96        | 1220      | 2.96     |
| N609769            |                                   | 1.38            | 0.418     |           | <0.5      | 5.49     | <5        | 3810      | 0.6       | 3         | 2.70     | <0.5      | 3         | 142       | 2180      | 3.30     |
| N609770            |                                   | 1.40            | 0.090     |           | <0.5      | 7.02     | <5        | 1850      | 1.0       | <2        | 0.70     | <0.5      | 4         | 123       | 486       | 4.24     |
| N609771            |                                   | 1.56            | 0.027     |           | <0.5      | 7.20     | 11        | 3600      | 0.8       | <2        | 1.36     | <0.5      | 1         | 111       | 95        | 3.32     |
| N609772            |                                   | 1.52            | 0.012     |           | <0.5      | 7.69     | <5        | 3410      | 0.7       | <2        | 1.46     | <0.5      | 2         | 90        | 83        | 3.49     |
| N609773            |                                   | 1.82            | <0.005    |           | <0.5      | 7.35     | <5        | 2030      | 0.7       | 2         | 3.39     | <0.5      | 1         | 83        | 4         | 3.00     |
| N609774            |                                   | 0.08            | 8.59      |           | 2.1       | 6.28     | <5        | 1640      | 3.3       | 2         | 4.99     | <0.5      | 25        | 166       | 133       | 5.14     |

Comments: \*\*CORRECTED COPY for Au and all ME-ICP61 elements - samples N609756 and N609757\*\*  
 \*\*CORRECTED COPY for Au - samples N609769 and N609770\*\*





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 49 NORMANDALE RD  
 UNIONVILLE ON L3R 4J8

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 Finalized Date: 30-AUG-2004  
 Account: KIV

Project: Stewart

**CERTIFICATE OF ANALYSIS VA04054017**

| Sample Description | Method Analyte Units LOR | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61  | ME-ICP61 | ME-ICP61 |          |
|--------------------|--------------------------|----------|-----------|----------|----------|-----------|----------|----------|----------|----------|----------|----------|-----------|----------|----------|----------|
|                    |                          | K % 0.01 | Mg % 0.01 | Mn ppm 5 | Mo ppm 1 | Na % 0.01 | Ni ppm 1 | P ppm 10 | Pb ppm 2 | S % 0.01 | Sb ppm 5 | Sr ppm 1 | Ti % 0.01 | V ppm 1  | W ppm 10 | Zn ppm 2 |
| N609245            |                          | 0.54     | 2.58      | 1875     | 4        | 1.05      | 94       | 180      | 6        | 2.77     | <5       | 60       | 0.17      | 104      | <10      | 150      |
| N609246            |                          | 6.27     | 0.87      | 1070     | 5        | 0.09      | 1        | 480      | 9        | 0.59     | <5       | 179      | 0.17      | 51       | <10      | 28       |
| N609247            |                          | 6.57     | 0.71      | 1035     | 4        | 0.10      | 3        | 450      | 3        | 0.19     | <5       | 160      | 0.18      | 49       | <10      | 29       |
| N609248            |                          | 6.56     | 0.54      | 705      | 3        | 0.09      | 3        | 490      | 5        | 0.38     | 6        | 134      | 0.18      | 51       | 10       | 29       |
| N609249            |                          | 6.60     | 0.60      | 941      | 5        | 0.10      | 1        | 560      | 4        | 0.37     | <5       | 113      | 0.21      | 57       | 10       | 20       |
| N609250            |                          | 5.20     | 0.50      | 1120     | 2        | 0.06      | 3        | 510      | 3        | 0.25     | <5       | 66       | 0.18      | 51       | 10       | 20       |
| N609751            |                          | 2.05     | 0.40      | 2370     | 7        | 0.03      | 3        | 290      | 2        | 0.46     | 7        | 34       | 0.10      | 34       | 20       | 11       |
| N609752            |                          | 2.65     | 0.85      | 2410     | 2        | 0.04      | 5        | 360      | <2       | 0.19     | <5       | 100      | 0.13      | 42       | 10       | 15       |
| N609753            |                          | 2.07     | 0.48      | 1885     | 4        | 0.02      | 2        | 300      | 4        | 0.20     | <5       | 35       | 0.11      | 31       | 10       | 13       |
| N609754            |                          | 0.55     | 0.22      | 2630     | 2        | 0.01      | 5        | <10      | <2       | 1.08     | 5        | 125      | <0.01     | 14       | <10      | 9        |
| N609755            |                          | 1.78     | 0.30      | 3060     | 4        | 0.02      | <1       | 220      | <2       | 1.04     | <5       | 76       | 0.08      | 30       | 10       | 6        |
| N609756            |                          | 2.11     | 0.48      | 1860     | 7        | 0.03      | 2        | 280      | 3        | 0.61     | 6        | 102      | 0.11      | 34       | 20       | 15       |
| N609757            |                          | 3.00     | 0.34      | 1570     | 6        | 0.03      | 4        | 420      | 4        | 0.27     | 6        | 102      | 0.15      | 38       | 10       | 10       |
| N609758            |                          | 3.81     | 0.55      | 1470     | 2        | 0.04      | 2        | 430      | 2        | 0.20     | 6        | 140      | 0.16      | 38       | 10       | 16       |
| N609759            |                          | 3.49     | 0.45      | 1230     | 6        | 0.05      | 2        | 380      | 3        | 0.22     | <5       | 143      | 0.14      | 35       | 10       | 11       |
| N609760            |                          | 3.09     | 0.33      | 1265     | 2        | 0.04      | 4        | 320      | <2       | 0.24     | 6        | 131      | 0.13      | 35       | 10       | 9        |
| N609761            |                          | 3.44     | 2.93      | 1035     | 12       | 2.35      | 67       | 2260     | 28       | 0.29     | 9        | 1595     | 0.35      | 168      | <10      | 96       |
| N609762            |                          | 3.68     | 0.50      | 1415     | 2        | 0.05      | 3        | 400      | <2       | 0.21     | 6        | 140      | 0.15      | 42       | 10       | 19       |
| N609763            |                          | 2.69     | 0.59      | 1570     | 4        | 0.03      | 4        | 350      | 3        | 0.14     | 5        | 78       | 0.13      | 39       | 10       | 29       |
| N609764            |                          | 2.36     | 0.70      | 1720     | 6        | 0.02      | 2        | 330      | 3        | 0.07     | 6        | 60       | 0.13      | 43       | 10       | 32       |
| N609765            |                          | 1.22     | 0.48      | 3750     | 7        | 0.03      | 1        | 170      | 6        | 0.36     | 5        | 75       | 0.06      | 30       | 10       | 14       |
| N609766            |                          | 3.90     | 0.47      | 1085     | 7        | 0.06      | 1        | 440      | 2        | 0.21     | <5       | 83       | 0.17      | 46       | 10       | 22       |
| N609767            |                          | 4.35     | 0.84      | 1495     | 2        | 0.07      | 3        | 370      | 5        | 0.21     | <5       | 213      | 0.14      | 41       | 10       | 27       |
| N609768            |                          | 5.27     | 0.45      | 678      | 5        | 0.08      | 3        | 430      | <2       | 0.22     | <5       | 79       | 0.17      | 38       | <10      | 27       |
| N609769            |                          | 3.76     | 0.89      | 1715     | 7        | 0.07      | 2        | 330      | 3        | 0.35     | <5       | 262      | 0.13      | 43       | 10       | 19       |
| N609770            |                          | 4.68     | 0.44      | 940      | 9        | 0.10      | 2        | 460      | 5        | 0.14     | 7        | 60       | 0.18      | 49       | 10       | 28       |
| N609771            |                          | 6.23     | 0.29      | 916      | 3        | 0.44      | 2        | 470      | <2       | 0.05     | 5        | 194      | 0.18      | 50       | 10       | 36       |
| N609772            |                          | 5.79     | 0.29      | 927      | 5        | 0.45      | 1        | 500      | 8        | 0.03     | <5       | 193      | 0.19      | 55       | 10       | 41       |
| N609773            |                          | 5.96     | 1.19      | 1380     | 2        | 0.07      | 1        | 500      | 5        | 0.12     | 6        | 201      | 0.18      | 54       | 10       | 46       |
| N609774            |                          | 4.37     | 3.09      | 1070     | 52       | 1.48      | 68       | 2050     | 33       | 1.08     | 5        | 1180     | 0.32      | 185      | 10       | 84       |

Comments: \*\*CORRECTED COPY for Au and all ME-ICP61 elements - samples N609756 and N609757\*\*  
 \*\*CORRECTED COPY for Au - samples N609769 and N609770\*\*



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49 NORMANDALE RD  
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Finalized Date: 30-AUG-2004  
Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04054017

| Sample Description                                  | Method<br>Analyte<br>Unks<br>LOR | Cu-AA62<br>Cu<br>%<br>0.01 |
|-----------------------------------------------------|----------------------------------|----------------------------|
| N609245<br>N609246<br>N609247<br>N609248<br>N609249 |                                  |                            |
| N609250<br>N609751<br>N609752<br>N609753<br>N609754 |                                  | 1.34                       |
| N609755<br>N609756<br>N609757<br>N609758<br>N609759 |                                  |                            |
| N609760<br>N609761<br>N609762<br>N609763<br>N609764 |                                  |                            |
| N609765<br>N609766<br>N609767<br>N609768<br>N609769 |                                  |                            |
| N609770<br>N609771<br>N609772<br>N609773<br>N609774 |                                  |                            |
|                                                     |                                  |                            |

Comments: \*\*CORRECTED COPY for Au and all ME-ICP61 elements - samples N609756 and N609757\*\*  
\*\*CORRECTED COPY for Au - samples N609769 and N609770\*\*



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Total # Pages: 2 (A - C)

Finalized Date: 30-AUG-2004

Account: KIV

Project: Stewart

*Original Copy*

## CERTIFICATE OF ANALYSIS VA04054017

| Sample Description | Method Analyte Units LOR | WEI-21       | Au-AA23 | Au-GRA21 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|--------------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | Recvd Wt. kg | Au ppm  | Au ppm   | Ag ppm   | Al %     | As ppm   | Ba ppm   | Be ppm   | Bj ppm   | Ca %     | Cd ppm   | Co ppm   | Cr ppm   | Cu ppm   | Fe %     |
|                    |                          | 0.02         | 0.005   | 0.05     | 0.5      | 0.01     | 5        | 10       | 0.5      | 2        | 0.01     | 0.5      | 1        | 1        | 1        | 0.01     |
| N609245            |                          | 0.08         | 1.475   |          | 3.2      | 8.47     | 106      | 40       | <0.5     | 4        | 4.48     | <0.5     | 234      | 29       | 8820     | 12.20    |
| N609246            |                          | 1.60         | 0.009   |          | <0.5     | 7.00     | 48       | 2160     | 0.6      | 3        | 2.52     | <0.5     | 5        | 98       | 9        | 3.07     |
| N609247            |                          | 2.06         | <0.005  |          | <0.5     | 7.00     | 7        | 3040     | 0.6      | 2        | 2.19     | <0.5     | 2        | 82       | 6        | 2.90     |
| N609248            |                          | 1.90         | 0.014   |          | <0.5     | 7.63     | 47       | 2760     | 0.7      | 3        | 1.38     | <0.5     | 2        | 96       | 33       | 2.95     |
| N609249            |                          | 1.50         | 0.006   |          | <0.5     | 7.98     | 30       | 2670     | 0.6      | 4        | 1.70     | <0.5     | 4        | 82       | 43       | 3.23     |
| N609250            |                          | 0.90         | 0.014   |          | <0.5     | 7.52     | 42       | 1710     | 0.7      | 3        | 0.98     | <0.5     | 4        | 88       | 89       | 3.67     |
| N609751            |                          | 2.22         | 1.740   |          | <0.5     | 4.44     | 30       | 550      | 0.6      | 2        | 0.93     | <0.5     | 5        | 126      | 1765     | 4.46     |
| N609752            |                          | 2.08         | 0.358   |          | <0.5     | 5.52     | <5       | 2520     | 0.7      | 3        | 2.40     | <0.5     | 3        | 123      | 1150     | 4.25     |
| N609753            |                          | 1.94         | 0.091   |          | <0.5     | 4.62     | <5       | 720      | 0.7      | 2        | 0.83     | <0.5     | 3        | 78       | 1080     | 4.67     |
| N609754            |                          | 1.88         | >10.0   | 10.20    | 1.0      | 1.25     | <5       | 190      | <0.5     | <2       | 5.49     | <0.5     | 2        | 198      | >10000   | 4.21     |
| N609755            |                          | 1.32         | 2.92    |          | 0.7      | 3.95     | 8        | 440      | 0.6      | 2        | 2.77     | <0.5     | 4        | 65       | 9300     | 5.95     |
| N609756            |                          | 1.48         | 0.180   |          | <0.5     | 6.25     | 13       | 700      | 0.8      | 3        | 2.68     | <0.5     | 3        | 93       | 378      | 3.46     |
| N609757            |                          | 1.84         | 1.685   |          | <0.5     | 4.66     | 21       | 540      | 0.6      | 4        | 2.14     | <0.5     | 4        | 95       | 2260     | 5.54     |
| N609758            |                          | 1.92         | 0.075   |          | <0.5     | 6.70     | 5        | 1210     | 0.7      | 5        | 2.34     | <0.5     | 3        | 113      | 110      | 4.13     |
| N609759            |                          | 1.90         | 0.035   |          | <0.5     | 5.82     | <5       | 1100     | 0.6      | 3        | 2.00     | <0.5     | 3        | 116      | 38       | 3.59     |
| N609760            |                          | 1.92         | 0.094   |          | <0.5     | 5.25     | 10       | 960      | 0.6      | 2        | 1.76     | <0.5     | 3        | 155      | 302      | 3.41     |
| N609761            |                          | 0.08         | 3.28    |          | <0.5     | 6.82     | 7        | 2070     | 3.3      | 2        | 4.66     | <0.5     | 25       | 144      | 102      | 5.07     |
| N609762            |                          | 1.80         | 0.460   |          | <0.5     | 6.37     | <5       | 1320     | 0.7      | 2        | 1.84     | <0.5     | 3        | 161      | 232      | 4.92     |
| N609763            |                          | 2.34         | 0.153   |          | <0.5     | 5.52     | 5        | 780      | 0.8      | <2       | 1.22     | <0.5     | 4        | 110      | 342      | 6.06     |
| N609764            |                          | 2.38         | 0.234   |          | <0.5     | 5.69     | 8        | 500      | 0.8      | 2        | 1.22     | <0.5     | 4        | 119      | 72       | 7.29     |
| N609765            |                          | 1.32         | 3.50    |          | <0.5     | 2.77     | 6        | 1720     | 0.6      | 4        | 0.73     | <0.5     | 6        | 196      | 2220     | 7.95     |
| N609766            |                          | 2.04         | 0.075   |          | <0.5     | 6.78     | 14       | 2290     | 0.9      | 2        | 0.81     | <0.5     | 4        | 77       | 478      | 4.10     |
| N609767            |                          | 1.90         | 0.487   |          | <0.5     | 6.03     | <5       | 2830     | 0.7      | <2       | 2.46     | <0.5     | 4        | 118      | 758      | 3.48     |
| N609768            |                          | 1.64         | 0.249   |          | <0.5     | 6.90     | <5       | 2150     | 0.7      | 3        | 0.81     | <0.5     | 3        | 96       | 1220     | 2.96     |
| N609769            |                          | 1.38         | 0.090   |          | <0.5     | 5.49     | <5       | 3810     | 0.6      | 3        | 2.70     | <0.5     | 3        | 142      | 2180     | 3.30     |
| N609770            |                          | 1.40         | 0.418   |          | <0.5     | 7.02     | <5       | 1850     | 1.0      | <2       | 0.70     | <0.5     | 4        | 123      | 486      | 4.24     |
| N609771            |                          | 1.56         | 0.027   |          | <0.5     | 7.20     | 11       | 3600     | 0.8      | <2       | 1.36     | <0.5     | 1        | 111      | 95       | 3.32     |
| N609772            |                          | 1.52         | 0.012   |          | <0.5     | 7.69     | <5       | 3410     | 0.7      | <2       | 1.46     | <0.5     | 2        | 90       | 83       | 3.49     |
| N609773            |                          | 1.82         | <0.005  |          | <0.5     | 7.35     | <5       | 2030     | 0.7      | 2        | 3.39     | <0.5     | 1        | 83       | 4        | 3.00     |
| N609774            |                          | 0.08         | 8.59    |          | 2.1      | 6.28     | <5       | 1640     | 3.3      | 2        | 4.99     | <0.5     | 25       | 166      | 133      | 5.14     |



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Project: Stewart

## CERTIFICATE OF ANALYSIS VA04054017

| Sample Description | Method Analyte Units LOR | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | K        | Mg       | Mn       | Mo       | Na       | Ni       | P        | Pb       | S        | Sb       | Sr       | Ti       | V        | W        | Zn       |
|                    |                          | %        | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      |
|                    |                          | 0.01     | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        |
| N609245            |                          | 0.54     | 2.58     | 1875     | 4        | 1.05     | 94       | 180      | 6        | 2.77     | <5       | 60       | 0.17     | 104      | <10      | 150      |
| N609246            |                          | 6.27     | 0.87     | 1070     | 5        | 0.09     | 1        | 480      | 9        | 0.59     | <5       | 179      | 0.17     | 51       | <10      | 28       |
| N609247            |                          | 6.57     | 0.71     | 1035     | 4        | 0.10     | 3        | 450      | 3        | 0.19     | <5       | 160      | 0.18     | 49       | <10      | 29       |
| N609248            |                          | 6.56     | 0.54     | 705      | 3        | 0.09     | 3        | 490      | 5        | 0.38     | 6        | 134      | 0.18     | 51       | 10       | 29       |
| N609249            |                          | 6.60     | 0.60     | 941      | 5        | 0.10     | 1        | 560      | 4        | 0.37     | <5       | 113      | 0.21     | 57       | 10       | 20       |
| N609250            |                          | 5.20     | 0.50     | 1120     | 2        | 0.06     | 3        | 510      | 3        | 0.25     | <5       | 66       | 0.18     | 51       | 10       | 20       |
| N609751            |                          | 2.05     | 0.40     | 2370     | 7        | 0.03     | 3        | 290      | 2        | 0.46     | 7        | 34       | 0.10     | 34       | 20       | 11       |
| N609752            |                          | 2.65     | 0.85     | 2410     | 2        | 0.04     | 5        | 360      | <2       | 0.19     | <5       | 100      | 0.13     | 42       | 10       | 15       |
| N609753            |                          | 2.07     | 0.48     | 1885     | 4        | 0.02     | 2        | 300      | 4        | 0.20     | <5       | 35       | 0.11     | 31       | 10       | 13       |
| N609754            |                          | 0.55     | 0.22     | 2630     | 2        | 0.01     | 5        | <10      | <2       | 1.08     | 5        | 125      | <0.01    | 14       | <10      | 9        |
| N609755            |                          | 1.78     | 0.30     | 3060     | 4        | 0.02     | <1       | 220      | <2       | 1.04     | <5       | 76       | 0.08     | 30       | 10       | 6        |
| N609756            |                          | 3.00     | 0.34     | 1570     | 6        | 0.03     | 4        | 420      | 4        | 0.27     | 6        | 102      | 0.15     | 38       | 10       | 10       |
| N609757            |                          | 2.11     | 0.48     | 1860     | 7        | 0.03     | 2        | 280      | 3        | 0.61     | 6        | 102      | 0.11     | 34       | 20       | 15       |
| N609758            |                          | 3.81     | 0.55     | 1470     | 2        | 0.04     | 2        | 430      | 2        | 0.20     | 6        | 140      | 0.16     | 38       | 10       | 16       |
| N609759            |                          | 3.49     | 0.45     | 1230     | 6        | 0.05     | 2        | 380      | 3        | 0.22     | <5       | 143      | 0.14     | 35       | 10       | 11       |
| N609760            |                          | 3.09     | 0.33     | 1265     | 2        | 0.04     | 4        | 320      | <2       | 0.24     | 6        | 131      | 0.13     | 35       | 10       | 9        |
| N609761            |                          | 3.44     | 2.93     | 1035     | 12       | 2.35     | 67       | 2260     | 28       | 0.29     | 9        | 1595     | 0.35     | 168      | <10      | 96       |
| N609762            |                          | 3.68     | 0.50     | 1415     | 2        | 0.05     | 3        | 400      | <2       | 0.21     | 6        | 140      | 0.15     | 42       | 10       | 19       |
| N609763            |                          | 2.69     | 0.59     | 1570     | 4        | 0.03     | 4        | 350      | 3        | 0.14     | 5        | 78       | 0.13     | 39       | 10       | 29       |
| N609764            |                          | 2.36     | 0.70     | 1720     | 6        | 0.02     | 2        | 330      | 3        | 0.07     | 6        | 60       | 0.13     | 43       | 10       | 32       |
| N609765            |                          | 1.22     | 0.48     | 3750     | 7        | 0.03     | 1        | 170      | 6        | 0.36     | 5        | 75       | 0.06     | 30       | 10       | 14       |
| N609766            |                          | 3.90     | 0.47     | 1085     | 7        | 0.06     | 1        | 440      | 2        | 0.21     | <5       | 83       | 0.17     | 46       | 10       | 22       |
| N609767            |                          | 4.35     | 0.84     | 1495     | 2        | 0.07     | 3        | 370      | 5        | 0.21     | <5       | 213      | 0.14     | 41       | 10       | 27       |
| N609768            |                          | 5.27     | 0.45     | 678      | 5        | 0.08     | 3        | 430      | <2       | 0.22     | <5       | 79       | 0.17     | 38       | <10      | 27       |
| N609769            |                          | 3.76     | 0.89     | 1715     | 7        | 0.07     | 2        | 330      | 3        | 0.35     | <5       | 262      | 0.13     | 43       | 10       | 19       |
| N609770            |                          | 4.68     | 0.44     | 940      | 9        | 0.10     | 2        | 460      | 5        | 0.14     | 7        | 60       | 0.18     | 49       | 10       | 28       |
| N609771            |                          | 6.23     | 0.29     | 916      | 3        | 0.44     | 2        | 470      | <2       | 0.05     | 5        | 194      | 0.18     | 50       | 10       | 36       |
| N609772            |                          | 5.79     | 0.29     | 927      | 5        | 0.45     | 1        | 500      | 8        | 0.03     | <5       | 193      | 0.19     | 55       | 10       | 41       |
| N609773            |                          | 5.96     | 1.19     | 1380     | 2        | 0.07     | 1        | 500      | 5        | 0.12     | 6        | 201      | 0.18     | 54       | 10       | 46       |
| N609774            |                          | 4.37     | 3.09     | 1070     | 52       | 1.48     | 68       | 2050     | 33       | 1.08     | 5        | 1180     | 0.32     | 185      | 10       | 84       |



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49 NORMANDALE RD  
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Page: 2 - C  
Total # Pages: 2 (A - C)  
Finalized Date: 30-AUG-2004  
Account: KIV

Project: Stewart

**CERTIFICATE OF ANALYSIS VA04054017**

| Sample Description                                  | Method<br>Analyte<br>Units<br>LOR | Cu-AA62<br>Cu<br>%<br>0.01 |
|-----------------------------------------------------|-----------------------------------|----------------------------|
| N609245<br>N609246<br>N609247<br>N609248<br>N609249 |                                   |                            |
| N609250<br>N609751<br>N609752<br>N609753<br>N609754 |                                   | 1.34                       |
| N609755<br>N609756<br>N609757<br>N609758<br>N609759 |                                   |                            |
| N609760<br>N609761<br>N609762<br>N609763<br>N609764 |                                   |                            |
| N609765<br>N609766<br>N609767<br>N609768<br>N609769 |                                   |                            |
| N609770<br>N609771<br>N609772<br>N609773<br>N609774 |                                   |                            |
|                                                     |                                   |                            |





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Page: 2 - A

Total # Pages: 3 (A - C)

Finalized Date: 30-AUG-2004

Account: KIV

Project: Stewart

SZDCY-04

## CERTIFICATE OF ANALYSIS VA04053799

| Sample Description | Method Analyte Units LOR | WEI-21    | Au-AA23 | Au-GRA21 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|-----------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | Recvd Wt. | Au      | Au       | Ag       | Al       | As       | Ba       | Be       | Bi       | Ca       | Cd       | Co       | Cr       | Cu       | Fe       |
|                    |                          | kg        | ppm     | ppm      | ppm      | %        | ppm      | ppm      | ppm      | ppm      | %        | ppm      | ppm      | ppm      | ppm      | %        |
|                    | 0.02                     | 0.005     | 0.05    | 0.5      | 0.01     | 5        | 10       | 0.5      | 2        | 0.01     | 0.5      | 1        | 1        | 1        | 0.01     |          |
| N599692            |                          | 1.34      | 0.138   |          | <0.5     | 7.80     | 31       | 2720     | 0.7      | <2       | 1.83     | <0.5     | 11       | 21       | 72       | 5.04     |
| N599693            |                          | 1.94      | <0.005  |          | <0.5     | 7.71     | <5       | 2610     | 0.7      | 3        | 1.14     | <0.5     | 3        | 5        | 22       | 3.24     |
| N599694            |                          | 2.24      | 0.020   |          | <0.5     | 7.60     | 6        | 2480     | 0.7      | <2       | 1.24     | <0.5     | 6        | 19       | 33       | 3.23     |
| N599695            |                          | 1.10      | 0.070   |          | <0.5     | 6.85     | 19       | 1980     | 0.6      | 2        | 1.78     | <0.5     | 5        | 3        | 9        | 3.27     |
| N599696            |                          | 1.54      | 0.154   |          | <0.5     | 6.78     | 16       | 2310     | 0.6      | <2       | 3.03     | <0.5     | 7        | 23       | 229      | 3.29     |
| N599697            |                          | 1.36      | <0.005  |          | <0.5     | 7.14     | <5       | 2430     | 0.6      | <2       | 1.48     | <0.5     | 4        | 5        | 46       | 3.81     |
| N599698            |                          | 1.58      | 0.012   |          | <0.5     | 7.39     | 5        | 2210     | 0.7      | 2        | 1.39     | <0.5     | 3        | 18       | 34       | 3.33     |
| N599699            |                          | 1.26      | 0.007   |          | <0.5     | 7.57     | <5       | 4420     | 0.8      | <2       | 2.11     | <0.5     | 4        | 6        | 10       | 4.12     |
| N599700            |                          | 1.80      | 0.011   |          | <0.5     | 7.55     | 5        | 2230     | 0.8      | <2       | 1.34     | <0.5     | 5        | 5        | 61       | 3.40     |
| N609201            |                          | 0.06      | 1.190   |          | 3.6      | 8.63     | 150      | 40       | <0.5     | 4        | 4.21     | <0.5     | 205      | 27       | 8240     | 11.70    |
| N609202            |                          | 1.72      | 0.007   |          | <0.5     | 7.42     | <5       | 1780     | 0.9      | <2       | 1.88     | <0.5     | 4        | 3        | 13       | 3.42     |
| N609203            |                          | 2.38      | <0.005  |          | <0.5     | 7.20     | 12       | 2550     | 0.6      | <2       | 1.54     | <0.5     | 7        | 4        | 136      | 3.55     |
| N609204            |                          | 2.48      | 0.036   |          | <0.5     | 7.38     | 6        | 2710     | 0.6      | <2       | 1.24     | <0.5     | 6        | 6        | 12       | 3.66     |
| N609216            |                          | 1.44      | 0.006   |          | <0.5     | 7.66     | <5       | 1780     | 0.9      | 2        | 1.88     | <0.5     | 4        | 2        | 11       | 2.96     |
| N609217            |                          | 1.30      | <0.005  |          | <0.5     | 7.40     | <5       | 2790     | 0.7      | <2       | 1.46     | <0.5     | 3        | 4        | 15       | 3.00     |
| N609218            |                          | 2.36      | <0.005  |          | <0.5     | 7.72     | <5       | 2640     | 0.7      | 3        | 1.36     | <0.5     | 3        | 3        | 18       | 3.43     |
| N609219            |                          | 0.06      | 0.092   |          | 2.7      | 4.57     | <5       | 100      | <0.5     | 5        | 10.05    | <0.5     | 176      | 473      | 6100     | 11.15    |
| N609220            |                          | 2.56      | 0.013   |          | <0.5     | 7.10     | 6        | 2250     | 0.7      | <2       | 2.29     | <0.5     | 5        | 5        | 105      | 3.82     |
| N609221            |                          | 1.80      | 0.071   |          | <0.5     | 6.52     | 11       | 2000     | 0.6      | 2        | 3.38     | <0.5     | 7        | 3        | 13       | 3.26     |
| N609222            |                          | 1.76      | 0.022   |          | <0.5     | 6.91     | 14       | 1700     | 0.6      | <2       | 1.44     | <0.5     | 7        | 3        | 14       | 4.16     |
| N609223            |                          | 2.00      | <0.005  |          | <0.5     | 7.07     | <5       | 2300     | 0.6      | <2       | 1.34     | <0.5     | 4        | 17       | 75       | 3.54     |
| N609224            |                          | 2.02      | 0.006   |          | <0.5     | 6.60     | 5        | 2310     | 0.6      | <2       | 1.52     | <0.5     | 3        | 3        | 469      | 3.54     |
| N609225            |                          | 1.98      | 0.062   |          | <0.5     | 7.36     | 12       | 2520     | 0.7      | 2        | 1.30     | <0.5     | 4        | 9        | 41       | 3.61     |
| N609226 x          |                          | 1.98      | 9.83    |          | 1.6      | 2.75     | 11       | 560      | 0.7      | 2        | 3.57     | <0.5     | 5        | <1       | >10000   | 5.37     |
| N609227 x          |                          | 2.14      | >10.0   | 11.10    | 1.4      | 1.82     | 10       | 420      | 0.5      | 2        | 5.86     | <0.5     | 7        | 28       | 7770     | 5.22     |
| N609228 x          |                          | 1.88      | 0.172   |          | <0.5     | 5.37     | 8        | 1000     | 0.9      | <2       | 1.00     | <0.5     | 6        | 5        | 358      | 5.96     |
| N609228A           |                          | 0.08      | 1.460   |          | 2.7      | 8.56     | 114      | 50       | <0.5     | 4        | 4.40     | <0.5     | 220      | 31       | 8580     | 11.90    |
| N609229            |                          | 2.00      | 0.247   |          | <0.5     | 4.15     | 13       | 790      | 0.7      | <2       | 1.59     | <0.5     | 5        | 43       | 774      | 5.97     |
| N609230 x          |                          | 1.64      | 0.285   |          | <0.5     | 5.62     | 20       | 1170     | 0.8      | <2       | 1.64     | <0.5     | 4        | 4        | 236      | 4.89     |
| N609231 x          |                          | 2.12      | 1.045   |          | <0.5     | 3.97     | 43       | 1440     | 0.7      | <2       | 2.20     | <0.5     | 8        | 34       | 643      | 6.65     |
| N609232 x          |                          | 2.22      | 0.080   |          | <0.5     | 5.71     | 25       | 2810     | 0.7      | <2       | 1.50     | <0.5     | 7        | 3        | 492      | 5.62     |
| N609233 x          |                          | 1.78      | 4.15    |          | 1.0      | 3.95     | 11       | 630      | 0.7      | <2       | 2.68     | <0.5     | 8        | 3        | 4460     | 5.48     |
| N609234 x          |                          | 1.98      | 0.258   |          | <0.5     | 7.42     | 21       | 330      | 1.0      | <2       | 2.25     | <0.5     | 14       | 7        | 1440     | 9.57     |
| N609235 x          |                          | 1.18      | 1.985   |          | 0.5      | 7.55     | 13       | 6180     | 1.0      | <2       | 2.53     | <0.5     | 10       | 3        | 1500     | 9.33     |
| N609236 x          |                          | 0.08      | 8.66    |          | 2.1      | 6.22     | 12       | 1630     | 3.4      | <2       | 4.86     | <0.5     | 27       | 161      | 119      | 4.89     |
| N609237 x          |                          | 2.10      | 0.052   |          | <0.5     | 7.97     | 13       | 2960     | 1.2      | <2       | 2.01     | <0.5     | 16       | 9        | 319      | 9.73     |
| N609238 x          |                          | 1.46      | 0.113   |          | <0.5     | 7.64     | 11       | 2680     | 1.2      | <2       | 2.04     | <0.5     | 21       | 3        | 2410     | 8.71     |
| N609239            |                          | 2.26      | 0.016   |          | <0.5     | 8.63     | 16       | 2950     | 1.0      | <2       | 1.90     | <0.5     | 12       | 5        | 377      | 8.84     |
| N609240            |                          | 1.68      | 0.031   |          | <0.5     | 7.55     | 11       | 1640     | 0.9      | <2       | 4.51     | <0.5     | 18       | 2        | 50       | 8.68     |
| N609241            |                          | 1.32      | 0.008   |          | <0.5     | 8.55     | 6        | 4690     | 1.2      | <2       | 4.04     | <0.5     | 10       | 2        | 18       | 5.64     |

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Finalized Date: 30-AUG-2004

Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04053799

| Sample Description | Method Analyte Units LOR | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | K        | Mg       | Mn       | Mo       | Na       | Ni       | P        | Pb       | S        | Sb       | Sr       | Ti       | V        | W        | Zn       |
|                    |                          | %        | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      |
|                    |                          | 0.01     | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        |
| N599692            |                          | 6.08     | 0.65     | 1340     | 1        | 0.17     | 3        | 670      | 9        | 0.53     | <5       | 186      | 0.24     | 74       | 10       | 33       |
| N599693            |                          | 6.94     | 0.36     | 684      | 1        | 0.16     | 2        | 480      | 5        | 0.02     | <5       | 142      | 0.17     | 46       | <10      | 20       |
| N599694            |                          | 5.57     | 0.33     | 817      | 1        | 0.17     | 2        | 480      | 4        | 0.12     | <5       | 161      | 0.18     | 49       | 10       | 19       |
| N599695            |                          | 5.88     | 0.39     | 1055     | 1        | 0.13     | 3        | 440      | 6        | 0.24     | <5       | 176      | 0.16     | 44       | 10       | 20       |
| N599696            |                          | 6.15     | 0.54     | 1120     | 1        | 0.15     | 3        | 510      | 10       | 0.37     | <5       | 305      | 0.17     | 56       | 10       | 20       |
| N599697            |                          | 4.81     | 0.43     | 1080     | 1        | 0.13     | <1       | 470      | 5        | 0.05     | 6        | 133      | 0.16     | 46       | <10      | 23       |
| N599698            |                          | 6.44     | 0.40     | 828      | 5        | 0.12     | 4        | 490      | 4        | 0.01     | <5       | 124      | 0.18     | 47       | <10      | 22       |
| N599699            |                          | 6.26     | 0.61     | 1245     | 1        | 0.12     | 2        | 560      | 6        | 0.07     | <5       | 266      | 0.20     | 59       | <10      | 29       |
| N599700            |                          | 6.17     | 0.42     | 798      | 1        | 0.30     | 1        | 500      | 5        | 0.07     | <5       | 125      | 0.18     | 48       | <10      | 19       |
| N609201            |                          | 0.53     | 2.58     | 1870     | 2        | 1.08     | 87       | 180      | 6        | 2.75     | <5       | 60       | 0.16     | 99       | <10      | 138      |
| N609202            |                          | 5.55     | 0.59     | 1080     | 1        | 0.25     | 2        | 540      | 4        | 0.01     | <5       | 134      | 0.19     | 50       | <10      | 21       |
| N609203            |                          | 6.54     | 0.45     | 877      | 1        | 0.13     | 1        | 480      | 13       | 0.15     | 5        | 132      | 0.17     | 45       | <10      | 22       |
| N609204            |                          | 5.46     | 0.41     | 917      | 1        | 0.13     | <1       | 490      | 7        | 0.12     | 5        | 135      | 0.17     | 46       | 10       | 64       |
| N609216            |                          | 5.68     | 0.59     | 909      | <1       | 0.41     | 3        | 510      | 6        | 0.01     | <5       | 130      | 0.18     | 50       | <10      | 18       |
| N609217            |                          | 5.25     | 0.41     | 802      | 1        | 0.29     | 1        | 490      | 3        | 0.02     | <5       | 158      | 0.18     | 46       | <10      | 17       |
| N609218            |                          | 6.79     | 0.37     | 859      | 1        | 0.14     | 3        | 520      | 5        | 0.03     | <5       | 153      | 0.19     | 52       | <10      | 17       |
| N609219            |                          | 0.08     | 6.90     | 1065     | 1        | 0.13     | 2490     | 580      | 15       | 3.05     | 6        | 39       | 0.38     | 158      | <10      | 95       |
| N609220            |                          | 6.04     | 0.51     | 1075     | 1        | 0.12     | 4        | 560      | 3        | 0.16     | <5       | 194      | 0.21     | 62       | <10      | 18       |
| N609221            |                          | 4.73     | 0.74     | 1125     | 1        | 0.09     | 5        | 420      | 6        | 0.34     | <5       | 206      | 0.15     | 49       | 10       | 24       |
| N609222            |                          | 5.28     | 0.38     | 1165     | <1       | 0.11     | 3        | 460      | <2       | 0.25     | <5       | 118      | 0.16     | 40       | 10       | 21       |
| N609223            |                          | 6.35     | 0.25     | 735      | 1        | 0.16     | 1        | 490      | 7        | 0.04     | <5       | 180      | 0.18     | 50       | <10      | 16       |
| N609224            |                          | 6.09     | 0.26     | 841      | 1        | 0.16     | <1       | 440      | 7        | 0.09     | <5       | 167      | 0.17     | 47       | 10       | 15       |
| N609225            |                          | 5.89     | 0.32     | 884      | 1        | 0.13     | 3        | 470      | 5        | 0.15     | <5       | 137      | 0.17     | 43       | 10       | 18       |
| N609226            |                          | 1.47     | 0.52     | 2100     | 1        | 0.02     | 3        | 150      | 6        | 1.20     | <5       | 130      | 0.06     | 25       | 10       | 19       |
| N609227            |                          | 0.90     | 0.59     | 2510     | 2        | 0.02     | 1        | 90       | 4        | 1.02     | 8        | 190      | 0.03     | 21       | <10      | 33       |
| N609228            |                          | 3.23     | 0.68     | 1590     | 2        | 0.04     | <1       | 340      | 9        | 0.27     | 5        | 87       | 0.13     | 37       | 10       | 62       |
| N609228A           |                          | 0.55     | 2.63     | 1875     | 1        | 1.07     | 86       | 190      | 10       | 2.74     | 10       | 59       | 0.17     | 105      | 10       | 152      |
| N609229            |                          | 2.48     | 0.64     | 1710     | 2        | 0.03     | <1       | 260      | 10       | 0.44     | 7        | 148      | 0.10     | 31       | 10       | 36       |
| N609230            |                          | 3.47     | 0.63     | 1370     | 4        | 0.05     | <1       | 350      | 9        | 0.36     | 10       | 158      | 0.13     | 36       | 10       | 33       |
| N609231            |                          | 2.32     | 0.91     | 1925     | 3        | 0.03     | <1       | 240      | 7        | 0.77     | 9        | 223      | 0.09     | 32       | 10       | 38       |
| N609232            |                          | 3.81     | 0.78     | 1415     | 4        | 0.10     | <1       | 360      | 11       | 0.73     | 8        | 218      | 0.14     | 37       | 10       | 38       |
| N609233            |                          | 1.98     | 0.65     | 1775     | 4        | 0.19     | <1       | 420      | 2        | 0.86     | 7        | 1080     | 0.14     | 61       | 10       | 32       |
| N609234            |                          | 3.46     | 1.04     | 1840     | 1        | 1.22     | <1       | 1450     | 15       | 1.06     | 14       | 1715     | 0.43     | 215      | 10       | 77       |
| N609235            |                          | 5.72     | 1.03     | 1515     | <1       | 0.25     | <1       | 1590     | 9        | 0.43     | 13       | 801      | 0.44     | 215      | 20       | 65       |
| N609236            |                          | 4.29     | 3.05     | 1040     | 51       | 1.46     | 69       | 1980     | 31       | 1.06     | 14       | 1170     | 0.32     | 181      | 30       | 84       |
| N609237            |                          | 5.98     | 1.20     | 1560     | <1       | 0.58     | 1        | 1740     | 7        | 0.76     | 11       | 248      | 0.43     | 219      | 10       | 65       |
| N609238            |                          | 5.74     | 0.99     | 1500     | <1       | 0.52     | 3        | 1650     | 7        | 0.78     | 11       | 203      | 0.41     | 186      | 10       | 65       |
| N609239            |                          | 6.82     | 1.05     | 1660     | <1       | 0.31     | <1       | 1920     | 3        | 0.13     | 11       | 196      | 0.47     | 215      | 10       | 62       |
| N609240            |                          | 4.00     | 1.68     | 1915     | 3        | 0.04     | 1        | 1640     | 8        | 0.65     | 11       | 180      | 0.40     | 168      | 10       | 84       |
| N609241            |                          | 4.57     | 1.18     | 1325     | <1       | 0.05     | <1       | 1840     | 4        | 0.15     | 8        | 305      | 0.46     | 177      | 10       | 75       |



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Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04053799

| Sample Description                                   | Method<br>Analyte<br>Units<br>LOR | Cu-AA62<br>Cu<br>%<br>0.01 |
|------------------------------------------------------|-----------------------------------|----------------------------|
| N599692<br>N599693<br>N599694<br>N599695<br>N599696  |                                   |                            |
| N599697<br>N599698<br>N599699<br>N599700<br>N609201  |                                   |                            |
| N609202<br>N609203<br>N609204<br>N609216<br>N609217  |                                   |                            |
| N609218<br>N609219<br>N609220<br>N609221<br>N609222  |                                   |                            |
| N609223<br>N609224<br>N609225<br>N609226<br>N609227  |                                   | 1.01                       |
| N609228<br>N609228A<br>N609229<br>N609230<br>N609231 |                                   |                            |
| N609232<br>N609233<br>N609234<br>N609235<br>N609236  |                                   |                            |
| N609237<br>N609238<br>N609239<br>N609240<br>N609241  |                                   |                            |



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**CERTIFICATE OF ANALYSIS VA04053799**

| Sample Description | Method Analyte Units LOR | WEI-21    | Au-AA23 | Au-GRA21 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|--------------------------|-----------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                          | Recvd Wt. | Au      | Au       | Ag       | Al       | As       | Ba       | Be       | Bi       | Ca       | Cd       | Co       | Cr       | Cu       | Fe       |
|                    |                          | kg        | ppm     | ppm      | ppm      | %        | ppm      | ppm      | ppm      | %        | ppm      | ppm      | ppm      | ppm      | ppm      | %        |
|                    |                          | 0.02      | 0.005   | 0.05     | 0.5      | 0.01     | 5        | 10       | 0.5      | 2        | 0.01     | 0.5      | 1        | 1        | 1        | 0.01     |
| N609242            |                          | 1.74      | <0.005  |          | <0.5     | 8.42     | <5       | 1400     | 1.3      | <2       | 4.98     | <0.5     | 17       | 5        | 3        | 6.38     |
| N609243            |                          | 1.60      | <0.005  |          | <0.5     | 8.56     | 13       | 3310     | 1.1      | <2       | 5.72     | <0.5     | 21       | 5        | 1        | 6.18     |
| N609244            |                          | 2.08      | <0.005  |          | <0.5     | 8.98     | 10       | 1980     | 1.1      | <2       | 4.65     | <0.5     | 21       | 5        | 4        | 6.62     |



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Project: Stewart

**CERTIFICATE OF ANALYSIS VA04053799**

| Sample Description | Method<br>Analyte<br>Units<br>LOR | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 | ME-ICP61 |
|--------------------|-----------------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                    |                                   | K        | Mg       | Mn       | Mo       | Na       | Ni       | P        | Pb       | S        | Sb       | Sr       | Ti       | V        | W        | Zn       |
|                    |                                   | %        | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      | %        | ppm      | ppm      | %        | ppm      | ppm      | ppm      |
|                    |                                   | 0.01     | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        | 0.01     | 5        | 1        | 0.01     | 1        | 10       | 2        |
| N609242            |                                   | 4.92     | 1.61     | 1635     | <1       | 0.66     | <1       | 1640     | 8        | 0.02     | 10       | 247      | 0.47     | 224      | <10      | 74       |
| N609243            |                                   | 5.36     | 1.98     | 1520     | <1       | 0.57     | 1        | 1500     | 10       | 0.06     | 9        | 383      | 0.47     | 235      | <10      | 58       |
| N609244            |                                   | 5.88     | 1.92     | 1420     | <1       | 0.87     | 3        | 1640     | 11       | 0.02     | 11       | 258      | 0.55     | 270      | 10       | 46       |





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Project: Stewart

## CERTIFICATE OF ANALYSIS VA04053799

| Sample Description            | Method<br>Analyte<br>Units<br>LOR | Cu-AA62<br>Cu<br>%<br>0.01 |
|-------------------------------|-----------------------------------|----------------------------|
| N609242<br>N609243<br>N609244 |                                   |                            |



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 Account: KIV

Project: TODD M

**CERTIFICATE OF ANALYSIS TO04063172**

| Sample Description | Method Analyte Units LOR | WEI-21          | Ag-AA45   | Cu-AA45   | Cu-AA46 | Au-SCR24        | Au-SCR24        | Au-SCR24        | Au-SCR24       | Au-SCR24      | Au-SCR24      | Au-AA26   | Au-AA26D  |
|--------------------|--------------------------|-----------------|-----------|-----------|---------|-----------------|-----------------|-----------------|----------------|---------------|---------------|-----------|-----------|
|                    |                          | Recvd Wt.<br>kg | Ag<br>ppm | Cu<br>ppm | Cu<br>% | Au Total<br>ppm | Au (+) F<br>ppm | Au (-) F<br>ppm | Au (+) m<br>mg | WT. + Fr<br>g | WT. - Fr<br>g | Au<br>ppm | Au<br>ppm |
|                    |                          | 0.02            | 0.2       | †         | 0.01    | 0.05            | 0.05            | 0.05            | 0.001          | 0.01          | 0.1           | 0.01      | 0.01      |
| SAMPLE M           |                          | 9.24            | 1.1       | >10000    | 2.33    | 5.76            | 4.28            | 5.84            | 0.222          | 51.85         | 982.0         | 5.88      | 5.80      |
| SAMPLE S           |                          | 15.71           | <0.2      | 262       |         | 3.07            | 1.77            | 3.12            | 0.063          | 35.68         | 1001.0        | 3.11      | 3.12      |





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Finalized Date: 26-SEP-2004

Account: KIV

Project: Stewart

## CERTIFICATE OF ANALYSIS VA04062620

| Sample Description | Method<br>Analyte<br>Units<br>LOR | Au-SCR21 | Au-SCR21 | Au-SCR21 | Au-SCR21 | Au-SCR21 | Au-SCR21 | Au-AA25 | Au-AA25D |
|--------------------|-----------------------------------|----------|----------|----------|----------|----------|----------|---------|----------|
|                    |                                   | Au Total | Au (+) F | Au (-) F | Au (+) m | WT. + Fr | WT. - Fr | Au      | Au       |
|                    |                                   | ppm      | ppm      | ppm      | mg       | g        | g        | ppm     | ppm      |
|                    |                                   | 0.05     | 0.05     | 0.05     | 0.001    | 0.01     | 0.1      | 0.01    | 0.01     |
| 609237             |                                   | 0.05     | <0.05    | 0.05     | <0.001   | 19.50    | 1013.0   | 0.05    | 0.05     |
| 609238             |                                   | 0.13     | <0.05    | 0.14     | <0.001   | 21.66    | 1035.0   | 0.15    | 0.12     |