



## **GEOCHEMICAL ASSESSMENT REPORT**

on the

### **MAGNOLIA PROPERTY**

Nanaimo Mining Division  
British Columbia

N.T.S. 092F/09, 10  
Latitude 49° 42' 30" N  
Longitude 124° 29' 30" W

for

Owner:  
LORRIE ANN ARCHIBALD  
1745 Larkhall Crescent  
North Vancouver, BC.  
V7H 2Z3

Operator:  
GREENLITE VENTURES INC.  
810 Peace Portal Drive  
Blaine, WA.  
98230

by

P. REYNOLDS, B.Sc., P.Geo.  
2006 January 17

GEOLOGICAL SURVEY BRANCH  
ASSESSMENT REPORT  
28,050

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## **INTRODUCTION**

This report was prepared at the request of the directors of Greenlite Ventures Inc. in order to satisfy assessment requirements. It discusses the 2005 exploration program completed during 2005 April 8 – 12 and July 4 – September 15 and recommends further exploration.

The information for the accompanying report was obtained from sources cited under references, from a personal examination of the property on 2003 April 18 - 19 and from the supervision of the 2005 exploration program.

Pertinent information such as extent and character of ownership was submitted by the Company and the Company's representatives and is believed to be true. No attempt was made to verify this information as this is beyond the scope of this report.

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## **LOCATION, ACCESS & PHYSIOGRAPHY**

The Magnolia property is located on Texada Island, B.C., one kilometre north of the Town of Gillies Bay. This largest island in the Strait of Georgia lies 110 km west-northwest of Vancouver and is accessible from Vancouver by car and ferry combinations either directly via Powell River on the mainland or circuitously through the Town of Comox on Vancouver Island. Alternatively, charter air service is available.

The property is centered at 49° 42' 30" north latitude (UTM 5507050 N) and 124° 29' 30" west longitude (UTM 392500 E) on N.T.S. mapsheets 092F 09W. Road access to and within the property is good. The gravel Central Road and the paved Gillies Bay - Vananda highway provide access to the northeastern and southwestern boundaries respectively. Interior travel is aided by old logging roads traversable by 4-wheel drive vehicles and other trails suitable for foot access only.

The topographic relief on the property ranges from 75 metres above sea level on the southwest to approximately 200 metres on the east boundary, which is on the southwest flank of Mount Pocahontas.

The island is within the "Sunshine Coast" area of British Columbia and features mild winters and moderate, dry summers. Consequently, all aspects of surface exploration may be carried out year round. Drinking water for the two towns on the island is provided by two dammed lakes. One of them, Cranby Lake, is located one kilometre southwest of the property. Water for diamond drilling is available from the many creeks and swamps on the property.

## CLAIM STATUS

The Magnolia property is comprised of one four-post legacy claim containing 18 units. The claim is approximately 1.5 kilometres east-west by three kilometres north-south with an area of 450 hectares. Complete claim information is as follows.

<u>Claim Name</u>	<u>Tenure Number</u>	<u>No. of Units</u>	<u>Expiry Date *</u>
Magnolia 1	392905	18	29 April 2008

\* Includes assessment being applied.

The property overstakes one reverted crown grant, the X-Ray reverted Crown grant (229535). Lorrie Ann Archibald is the registered owner of the claim.

## REGIONAL GEOLOGY

The geology of Texada Island has been reported on by several people since magnetite was first discovered in 1873. G.M. Dawson, of the Geological Survey of Canada, examined the shoreline geology in 1887. A comprehensive report on Texada Island Geology was made in 1914 by R.G. McConnell of the Geological Survey of Canada. That report mainly concentrated on the iron occurrences adjacent to the northwestern shore of the Island. Swanson studied the iron skarns in 1925. More recent work was done on the skarn mineralization by Bacon (1952), Muller and Carson (1968), Sangster (1969), Ettliger and Ray (1988) and Webster and Ray (1990). The only map of the whole Island is by Muller (1968) who mapped on a reconnaissance basis. Webster and Ray (1990) produced a geological map of the northern third of the Island based on reconnaissance mapping during July and August 1989 and information provided by local prospectors, geologists and quarry managers.

Texada Island is located along the eastern margin of both the Insular tectono-stratigraphic belt and the Wrangellia Terrane of the Canadian Cordillera. The oldest rocks mapped on the Island are calc-alkaline volcanics of the Paleozoic Sicker Group exposed on the southeastern tip of the Island. These are unconformably overlain to the north by pillowed to massive basaltic flows and volcanics of the Middle to Upper Triassic Karmutsen Formation. Near the top of the formation the flows contain thin interbeds of fossiliferous limestone.

The Karmutsen is conformably overlain by limestones of the Upper Triassic Quatsino Formation whose exposures vary in thickness from marginal east and south of the exhausted iron mines to more than 500 metres at the northern tip of the Island. Cretaceous sediments of the Nanaimo Group crop out around Gillies Bay and may extend northward under alluvium for one to two kilometers.

Various stocks and minor intrusions, ranging in composition from gabbro through the more common diorite to quartz monzonite intrude the volcanics and limestones. These have been radiometrically dated as Middle to Upper Jurassic, and may correlate with the Coast Plutonic Complex on the mainland or the Island Intrusions on Vancouver Island. The more mafic stocks, which tend to be concentrated along the northwest trending Marble Bay Fault, are associated with copper-gold skarn mineralization around Vananda and the northeastern tip of the Island. The Gillies Bay felsic stock is associated with several magnetite-rich skarn

deposits. Other stocks and minor intrusives reportedly have skarn development but apparently have not been examined in great detail.

According to Webster and Ray the limestone and volcanics have been deformed into a series of broad, northwest trending open folds that plunge gently to moderately northwards.

Three sub-parallel, northwesterly lineaments are the most striking structural features of the north end of the Island. The most persistent and visually striking one, the Marble Bay fault, appears to traverse the entire length of the Island, albeit with some offsets. The other two, the Holly and Ideal faults are substantially shorter. All of them, according to Webster and Ray (1990) appear to have controlled the emplacement of the Jurassic intrusives and their associated skarn mineralization. The area between these faults has undergone substantial brittle deformation expressed by numerous low-angle splay faults and right-angle faults and shear zones either mapped or inferred from airborne geophysical surveys and photographs.

## **REGIONAL ECONOMIC SETTING**

Texada Island has a long history of mining and exploration for gold, copper and iron ore that began with the discovery of magnetite in 1873.

Gold, copper and silver were produced during intermittent production mainly from three mines during the period 1896 to 1952. The Marble Bay, Little Billie and Cornell mines, located at Vananda 5 kilometres northwest of the Magnolia property, produced a total of 303,608 tonnes of ore with an average grade of 7.83 grams/tonne gold, 52.74 grams/tonne silver and 2.9% copper (Ettlinger & Ray, 1988). These three deposits were in skarn mineralization at contacts between the Quatsino limestone and diorite intrusions. Other deposits which produced small amounts of ore during the same period were either in similar skarn environments or in quartz-flooded breccia zones along faults cutting the interbedded volcanics and limestones of the Karmutsen formation. It is believed that northwesterly trending faults, as well as low-angle splays from these faults, are associated with the emplacement of the diorite intrusions and locally, skarn mineralization (Webster and Ray 1990).

Iron ore was mined from a discontinuous line of magnetite-copper lenses, approximately two kilometres in length, situated immediately northwest of the town of Gillies Bay. Magnetite-copper skarn mineralization is developed along either the Quatsino-Karmutsen contact near the margin of the Gillies stock or along the intrusive-Quatsino contact. Alternatively, skarn mineralization may form in the limestone and volcanic rocks some distance from the stock where the skarn forming fluids were controlled by near vertical brittle fractures (Webster and Ray, 1990). Between 1885 and 1976 Texada Iron Mines Ltd., produced from four open pits and subsequent underground workings 20,880,900 tonnes of ore which yielded 10,000,000 tonnes of iron concentrate, 887,560 grams of gold, 23,644,310 grams of silver and 26,740,300 kilograms of copper.

Numerous small magnetite lenses associated with limestone beds within the Karmutsen Formation occur near the east coast of the Island from the northern tip to Mount Pocahontas. Most of them contain considerable amounts of copper (McConnell 1914) and at least one of them, the Yew showing which was discovered in 1985, contains free gold in unevenly distributed amounts (J. Bissett, personal communication). None of them has produced on a commercial basis. The Capsheaf and Southcap showings, within the central part of the existing claims, falls under this category. Similarly, a number of small quartz veins and

silicified shear zones containing free gold have been discovered on the northern part of the Island. The Holly showing, approximately four kilometres northwest of the Magnolia property, exhibited spectacular near-surface free gold in silicified, brecciated Karmutsen volcanics within the Holly Fault.

The iron and copper-gold skarns are believed to be coeval, are structurally and stratigraphically controlled and are related to a varied suite of continental margin intrusions that formed part of the early to middle Jurassic Bonanza magmatic arc. Limestone of the Quatsino Formation is being mined from open pits on the northern and northeastern end of the Island. The limestone is crushed, screened and barged to Vancouver and Portland, Oregon for use in a variety of pharmaceutical and industrial uses.

## **HISTORY**

Numerous pits, trenches, adits and at least one shaft on the Magnolia property attest to previous, mostly unrecorded exploration of the property. The Capsheaf showing, in the centre of the property, occurs within a skarn lens within a gently west-southwest dipping limestone interlayer of the Karmutsen Formation at a diorite intrusive contact. A shaft was sunk, before 1914, to a depth of 27 metres (90 feet) and some drifting done (McConnell 1914). In 1975 Longbar Minerals Ltd., conducted a magnetometer and electromagnetic (VLF) survey in conjunction with geological mapping on and around the Cap Sheaf. Three short diamond drill holes were completed to the south of the Capsheaf shaft. Assay results from drill core included one 1.5 metre (5 foot) section containing 6.17 grams/tonne (0.18 oz/ton) gold, 54.17 grams/tonne (1.58 oz/ton) silver, 5.52% copper and 26.80% iron. Several sections returned 0.5 to 1.0% copper with negligible gold.

Reconnaissance-scale geologic mapping, prospecting, and soil/rock geochemical surveys were conducted in the area during 1984 and 1985 by Packard Resources Ltd. A magnetic and E.M. survey was run over a the south end of the present claim in 1988. Also in 1988, BP Minerals Canada Limited conducted a large-scale soil sampling and geological mapping program on a large block of claims immediately to the north and east of the Magnolia property.

An airborne geophysical survey was conducted for CanQuest Resource Corp., in August 1988. Aerodat Ltd. flew 175 line kilometres over an area partially covered by the property. In November 1990, reconnaissance scale programs of geologic mapping, prospecting and soil sampling were conducted by CanQuest over a portion of the existing claim. In April 1991, reconnaissance scale ground magnetic and electromagnetic surveys were carried out by CanQuest. In February 1992, further soil sampling and geophysical surveys together with limited geological mapping were conducted by CanQuest. In January 1994, a 1,500 metre long baseline was established for survey control for geological mapping in the Capsheaf area. During the same period, portions of the property were mapped at a scale of 1:10,000. Rock sampling at the Capsheaf and Southcap showings in 1994 returned gold values ranging from 66 ppb to 8,620 ppb. Copper values ranged from 3,244 ppm to 73,320 ppm. During 1995, Canquest conducted further geological mapping and prospecting.

The property lay dormant until Greenlite began exploration during 2003 at which time four grab samples of rock were collected from the area of the Capsheaf showing. At this showing, magnetite-garnet-epidote skarn is exposed in a trench and one outcrop. The skarn zone trends north-northwest and most likely dips southwest. Within the trench, a one metre wide zone of massive magnetite-pyrrhotite-pyrite-chalcopyrite-

bornite-malachite occurs on the footwall of the magnetite-garnet-epidote skarn. Details of the samples are as follows.

Sample No.	Type	Au (g/t)	Cu (%)	Description
3844	Grab	3.85	2.457	Dump material. Magnetite-chalcopyrite skarn. Highly oxidized with malachite after chalcopyrite.
3845	Grab	4.61	3.376	Dump material. Magnetite-chalcopyrite skarn. Less oxidized than 3844.
3846	Grab	2.33	4.463	Grab of magnetite- pyrrhotite -chalcopyrite skarn. Malachite after chalcopyrite.
3847	Grab	5.19	1.915	Grab of magnetite-garnet-chalcopyrite-pyrrhotite skarn (approx 70% magnetite).

## **PROPERTY GEOLOGY AND MINERALIZATION**

The property is underlain, for the most part, by basaltic flows and volcanoclastics of the Middle to Upper Triassic Karmutsen Formation. The basalt consists of undifferentiated, dark green to black, variably magnetic basalt. The basalt grades from massive to feldsparphyric with individual laths of feldspar to three millimetres in size. The basalt almost always contains disseminated, fine grained magnetite.

At the Capsheaf and Southcap showings dark grey, massive limestone (unit 1c) hosts magnetite-garnet-sulphide skarn zones. The limestone strikes approximately 350° and dips 20° to the southwest. This limestone unit occurs as interbeds within the top of the Karmutsen Formation and, as such, suggests that the basalt flows have a gentle attitude.

There are two styles of mineralization present on the property; (a) pyritized, carbonate-silica altered sheared basalts and (b) magnetite-garnet-sulphide skarn zones within limestone interlayers of the Karmutsen. The carbonate-silica altered basalts tend to have low grade copper mineralization and anomalous gold values. Lead, zinc and silver mineralization may also be present.

Two zones of magnetite-garnet-sulphide skarn are present on the property - Capsheaf and Southcap. Both skarn zones have developed within an interlayer of limestone surrounded by basalt at or near the contact of a diorite intrusive. These skarn zones appear to form proximal to the intersection of northwest trending and northeast trending faults which most likely served as a conduit for the mineralizing solutions.

At the Capsheaf showing, magnetite-garnet-epidote skarn is exposed in a trench and one outcrop. It is assumed that this same unit is exposed in the shaft but, at present, the shaft is full of water so this can not be confirmed. The skarn zone trends north-northwest and most likely dips southwest. Within the trench, a one metre wide zone of massive magnetite-pyrrhotite-pyrite-chalcopyrite-bornite-malachite occurs on the footwall of the magnetite-garnet-epidote skarn. Previous sampling of this showing returned gold values ranging from 66 to 5,260 ppb and copper values ranging from 0.3% to 4.463%.

At the Southcap showing, garnet skarn with or without sulphides occurs along the contact of carbonate altered basalt and recrystallized limestone within an approximately 20 metre long open cut. Massive magnetite-pyrrhotite-pyrite-chalcopyrite occurs within a highly sheared area on the north end of the trench. Previous sampling of this zone returned gold values ranging from 980 to 8,620 ppb and copper values ranging from 4,715 to 73,320 ppm.

## **2005 EXPLORATION PROGRAM**

During the period 2005 April 8 – 12, a survey grid, comprised of 10 east-west oriented lines each 900 metres long, spaced at 100 metre intervals was established across a portion of the Magnolia property. A total of nine kilometres of grid was surveyed and stations established at 50 metre intervals by a two man crew. The lines were laid out utilizing a Trimble Pathfinder ProXR used in conjunction with a Canadian Coast Guard real-time differential receiver. Figures 4 - 6 are projected in UTM zone 10 N and utilize the North American Datum 1983.

### **Grid Lines**

Line Number	Start Station	End Station	Length
6400 N	2300 E	3200 E	900 m
6500 N	2300 E	3200 E	900 m
6600 N	2300 E	3200 E	900 m
6700 N	2300 E	3200 E	900 m
6800 N	2300 E	3200 E	900 m
6900 N	2300 E	3200 E	900 m
7000 N	2300 E	3200 E	900 m
7100 N	2300 E	3200 E	900 m
7200 N	2300 E	3200 E	900 m
7300 N	2300 E	3200 E	900 m
		<b>Total Length</b>	<b>9,000 m</b>

During the period 2005 July 4 to September 15, a soil geochemical survey was conducted on the Magnolia property. A two man crew collected soil samples at 50 metre intervals along the east-west oriented grid lines established during April 2005. Soils were collected from the B-horizon at a depth of approximately 30 centimetres utilizing a shovel and grubhoe. If no soil was present at a proposed sample site then the site was moved east or west until a suitable sample could be collected. Samples were placed in kraft wet-strength paper bags and marked with the grid location. Soil samples were shipped to Acme Analytical Laboratories Ltd. in Vancouver, BC for analysis. Bubble plots of gold, copper and iron in soil are shown in Figures 4, 5 and 6 respectively.

Gold values (Figure 4) show two distinct anomalies; the first on line 6500N from 2650E to 2900E and the second on line 6700N extending from 2700E to 2900E. The central portion of the anomaly on line 6500N is due to the adit at the Southcap showing however the other anomalous sites on this line are all uphill of the showing so are worthy of follow up. Several other single station anomalies are present and need to be followed up with additional soil sampling.

Copper and Iron values (Figures 5 & 6) tend to be much more widely distributed than gold. There is a very prominent north-south trending semi-coincident Cu-Fe anomaly at the east end of the grid. This anomaly extends from 6400N, 3000E to 7300N, 3100E and is 50 to 100 metres in width. A second Fe anomaly is centred at 6900N, 2650E and has dimensions of approximately 175 metres east-west by 300 metres north-south. A coincident Fe-Cu anomaly is present at the Southcap showing. Several other scattered Fe and Cu anomalies are present on the grid, many of which should be followed up by additional soil sampling.

## **CONCLUSION AND RECOMMENDATIONS**

There are two known gold and copper bearing skarn zones on the Magnolia property, Capsheaf and Southcap. These zones are located at the north and south end of the grid respectively. Several coincident copper – iron – (gold) soil anomalies occur between the Capsheaf and Southcap showings (Figures 4 – 6). Additional soil sampling is needed in order to better define the anomalies.

Weak skarn development occurs in the suspected area of the Milner Trench. This area needs to be prospected and mapped in more detail.

Due to the strong association of Iron and copper (gold) within the skarn zones a ground based magnetic survey should be helpful in locating areas of possible copper (gold) mineralization. It is recommended that Greenlite Ventures conduct further exploration on the Magnolia property. The next phase of exploration should consist of a magnetic survey over the flagged grid established during this program. In conjunction with the magnetic survey, geological mapping and prospecting as well as infill soil sampling should be conducted over the flagged grid.

## **REFERENCES**

Benvenuto, G: Assessment Report - Magnolia Property, Texada Island, B.C. for Canquest Resource Corp. March 30, 1992.

Economic Geology and the Bulletin of the Society of Economic Geologists. Volume 77, number 4, June-July 1982.

Ettlinger, A.D. and Ray, G.E: Gold-enriched Skarn Deposits in British Columbia; B.C. Ministry of Energy, Mines and Petroleum Resources, Geological Fieldwork 1987, Paper 1988-1, pages 263-279.

Findlay, A.R. and Hoffman, S.J: Assessment Report - 1988 Exploration Program, Pocahontas Bay Project for BP Resources Canada Ltd. October, 1988.

Ray, G.E., Ettlinger, A.D. and Meinert, L.D: Gold Skarns: Their Distribution, Characteristics and Problems in Classification; B.C. Ministry of Energy, Mines and Petroleum Resources, Geological Fieldwork 1989, Paper 1990-1, pages 237-246.

Reynolds, Paul: Geological Report with Recommendations on the Magnolia Property for Canquest Resource Corp. February 15, 1994.

Reynolds, Paul: Geological Assessment Report on the Magnolia Property for Canquest Resource Corp. February 15, 1996.

Reynolds, Paul: Summary Report on the Magnolia Property for Greenlite Ventures Inc. May 4, 2002

Webster, I.C.L. and Ray, G.E: Geology and Mineral Deposits of Northern Texada Island; B.C. Ministry of Energy, Mines and Petroleum Resources, Geological Fieldwork 1989, Paper 1990-1, pages 257-265.

Webster, I.C.L. and Ray, G.E: Geology and Mineral Deposits of Northern Texada Island; B.C. Ministry of Energy, Mines and Petroleum Resources, Open File 1990-3.

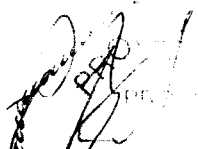
Whittles, A.B.L: Geophysical Report on the Capsheaf Claim Group. December 1975.

## **CERTIFICATE**

I, Paul Reynolds, of Vancouver, British Columbia hereby certify that:

- I am a Professional Geoscientist registered in good standing with the Association of Professional Engineers and Geoscientists of British Columbia (Registration No. 19603)
- I am a graduate of the University of British Columbia, with a B.Sc. in Geology (1987).
- I have been engaged in geological work continuously since 1987, in North and South America.
- I am the author of this report. The information in this report is based upon a review of unpublished and published reports and maps and on field work conducted under my supervision during the period 2005 April 4 to September 15.
- I have no interest, directly or indirectly, in the Magnolia property, or any property within 10 kilometres of the Magnolia property. I have no interest, directly or indirectly, in Greenlite Ventures Inc. or its securities nor do I expect to receive any interest in Greenlite Ventures Inc.
- Permission is hereby granted to Greenlite Ventures Inc. to use this report in support of any filing to be submitted to the Ministry of Energy, Mines and Petroleum Resources of the Province of British Columbia for the purpose of filing assessment on the Magnolia property.

Signed this 17th day of January, 2006.



\_\_\_\_\_  
Paul Reynolds, B. Sc., P. Geo.

**APPENDIX 1**  
**STATEMENT OF COSTS**

**Magnolia Property  
2005 assessment**

Name	No.	Days	Rate	Total
<b>April 8 - 12, 2005</b>				
Neil Swift	1	3	\$ 350.00	\$ 1,050.00
Chris Stoyles	1	2	\$ 300.00	\$ 600.00
Field Supplies				\$ 100.00
Radios	2	3	\$ 5.00	\$ 30.00
Trimble Pro XR with Coast Guard beacon real time antenna	1	3	\$ 100.00	\$ 300.00
Accommodation				\$ 244.13
Groceries				\$ 132.34
Travel - BC Ferries				\$ 116.85
Truck rental	1	4	\$ 50.00	\$ 200.00
Subtotal				\$ 2,773.32
Project Management Fee				\$ 416.00
Subtotal				\$ 3,189.32
GST				\$ 223.25
<b>Total (Event No. 4028933)</b>				<b>\$ 3,412.57</b>

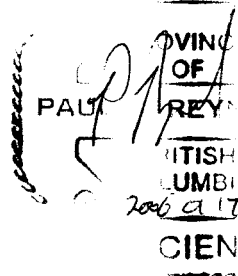
**July 4 - November 1, 2005**

Neil Swift	1	3	\$ 350.00	\$ 1,050.00
Chris Stoyles	1	4	\$ 300.00	\$ 1,200.00
Field Supplies				\$ 196.99
Radios	2	3	\$ 5.00	\$ 30.00
Accommodation				\$ 221.89
Groceries				\$ 115.70
Travel - BC Ferries				\$ 131.60
Truck rental	1	3	\$ 75.00	\$ 225.00
ATV Rental	1	3	\$ 50.00	\$ 150.00
Paul Reynolds (Report Prep)	1	2	\$ 500.00	\$ 1,000.00
Meridian Mapping (Map prep & GIS work)				\$ 416.67
Acme Analytical (Analysis)		188	\$ 15.90	\$ 2,989.20
Shipping				\$ 35.98
Project Management Fee				\$ 498.18
Subtotal				\$ 8,261.21
GST				\$ 578.28
<b>Total (Event No. 4055870)</b>				<b>\$ 8,839.49</b>

**TOTAL 2005 PROGRAM**

**SSI**

**\$ 12,252.06**



***APPENDIX 2***  
***ANALYTICAL RESULTS***



GEOCHEMICAL ANALYSIS CERTIFICATE



Reynolds, Paul PROJECT MAGNOLIA File # A503730 Page 1

4035 W. 31st Ave, Vancouver BC V6S 1Y7 Submitted by: Paul Reynolds

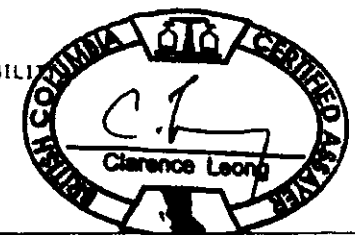
SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga	Se	Sample gm
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppb	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	%	ppm	ppm	ppm	ppm	%	ppm	ppm	
G-1	.7	2.1	2.1	38	<1	6.0	3.5	472	1.49	<5	2.1	.9	4.0	43	<1	<1	.1	33	.40	.081	7	68.6	.48	158	.105	3	.78	.050	.39	<1	.01	1.7	.3	<.05	4	<.5	15
7300N 2300E	1.0	144.3	8.2	122	.3	38.3	21.7	1227	4.26	15.9	.4	2.5	1.4	25	.4	.3	.2	112	.45	.085	9	62.2	.37	140	.215	4	3.78	.014	.03	.1	.09	5.6	.1	<.05	9	.7	15
7300N 2350E	6	74.9	5.7	48	.1	22.5	10.2	779	2.31	3.2	.2	2.2	.9	16	.1	.2	.1	65	.22	.060	5	25.3	.32	66	.118	3	2.24	.010	.03	.1	.10	2.3	.1	<.05	6	<.5	15
7300N 2400E	3.5	102.4	6.0	47	.1	22.9	13.1	370	2.87	4.6	.5	1.8	1.2	26	.1	.3	.1	91	.41	.053	7	35.8	.46	93	.152	2	3.35	.011	.03	.1	.06	2.7	.1	<.05	8	.6	15
7300N 2450E	1.1	97.3	6.4	59	.1	27.0	16.8	399	3.71	3.8	.2	3.5	.8	18	.1	.2	.1	113	.28	.080	3	37.6	.69	66	.253	3	3.74	.014	.03	<.1	.08	2.4	<.1	<.05	11	<.5	15
7300N 2500E	.7	61.8	12.2	79	.1	37.8	26.5	1456	6.67	4.3	.2	1.8	.5	20	.1	.5	.3	202	.33	.058	3	86.2	1.68	69	.461	1	2.68	.007	.02	<.1	.07	3.8	<.1	<.05	16	<.5	15
7300N 2550E	2.5	98.0	5.1	24	.2	20.2	20.9	298	3.91	2.9	.6	2.1	1.1	11	.1	.2	.1	118	.19	.045	9	32.5	.24	13	.167	2	2.52	.008	.02	<.1	.08	3.0	<.1	<.05	9	.9	15
7300N 2600E	1.0	58.9	8.5	73	.1	35.0	18.8	654	7.00	1.4	.2	3.6	.7	13	.1	.3	.3	234	.21	.064	4	76.1	.65	43	.225	<1	2.25	.009	.03	<.1	.10	3.1	.1	<.05	20	<.5	15
7300N 2650E	.7	138.2	11.1	69	.2	28.3	25.2	2217	6.99	3.3	.4	2.6	.2	8	.3	.2	.2	146	.13	.315	5	73.6	.39	85	.118	<1	2.26	.006	.03	<.1	.11	2.6	.1	<.05	17	.6	15
7300N 2720E	.9	105.4	6.2	40	<.1	20.2	9.7	521	2.66	3.8	.4	3.6	1.5	15	<.1	.2	.1	86	.23	.039	5	28.8	.53	56	.165	3	2.86	.011	.04	<.1	.07	3.0	.1	<.05	8	.5	15
7300N 2750E	1.8	138.8	5.9	51	.1	23.7	10.4	333	5.06	6.4	.5	3.4	1.8	9	.1	.3	.2	164	.16	.146	4	69.7	.47	37	.226	3	5.06	.008	.04	<.1	.17	4.4	.1	<.05	14	.8	15
7300N 2800E	.8	48.1	7.1	41	.1	18.9	11.2	258	3.27	4.0	.3	1.6	1.1	9	.1	.2	.1	92	.13	.070	4	29.4	.25	46	.172	<1	2.71	.010	.02	<.1	.11	2.2	.1	<.05	9	.5	15
7300N 2850E	1.0	94.3	8.7	74	.1	19.1	13.0	1230	5.00	4.2	.4	3.6	1.2	19	.1	.5	.2	148	.25	.167	4	43.2	.29	71	.257	2	3.19	.012	.03	<.1	.14	3.3	.1	<.05	13	.6	15
7300N 2900E	1.0	53.8	5.8	74	.3	17.4	22.9	444	3.10	5.7	.1	14.3	.8	25	.1	.5	.2	81	.30	.062	4	28.1	.38	51	.230	1	1.41	.011	.04	<.1	.06	2.3	<.1	<.05	7	.5	15
7300N 2950E	.6	122.2	10.1	141	.2	25.3	29.3	1075	3.99	14.4	.2	11.9	1.1	15	.3	1.1	.2	110	.23	.072	5	27.1	.28	55	.163	1	1.94	.012	.02	<.1	.05	4.2	.1	<.05	11	<.5	15
7300N 3000E	.3	24.0	11.1	76	.1	12.0	7.6	1177	1.71	6.0	.2	.7	.7	12	.1	.1	.1	50	.15	.061	4	16.8	.29	72	.073	2	1.44	.010	.02	<.1	.03	1.6	.1	<.05	5	<.5	15
7300N 3050E	1.3	209.6	10.7	86	.5	40.9	21.7	696	5.22	7.3	.3	4.3	1.4	10	.3	.5	.1	160	.13	.098	6	53.0	1.12	28	.165	1	4.24	.011	.02	.1	.08	6.5	.1	<.05	13	.5	15
7300N 3100E	1.7	263.8	7.0	100	.2	50.6	29.1	1907	8.46	15.2	.3	3.9	.7	20	.3	1.8	.1	168	.24	.145	6	49.8	1.55	50	.028	2	4.02	.006	.05	.2	.10	7.4	.1	<.05	12	.5	15
7300N 3150E	.6	52.4	16.5	184	.3	22.0	24.9	4216	4.98	9.4	.1	10.9	.7	36	.3	.3	.2	112	.47	.348	4	39.4	.41	134	.202	2	2.19	.011	.03	<.1	.17	3.4	.1	<.05	11	.8	15
7300N 3200E	1.0	94.1	29.0	171	.4	35.1	33.5	3513	5.07	30.7	.3	13.7	1.4	24	.4	.7	.3	125	.45	.251	6	46.4	1.02	87	.145	2	3.62	.021	.04	.1	.22	5.8	.1	.08	14	.7	15
7200N 2320E	.9	98.7	11.1	121	.3	86.3	37.1	1479	6.07	13.4	.3	35.0	.8	66	.3	.3	.2	146	.41	.202	5	91.0	1.79	58	.325	3	3.68	.011	.03	<.1	.14	5.0	.1	<.05	15	.7	15
7200N 2350E	.7	16.8	5.3	18	<.1	8.1	4.6	223	1.46	2.2	.2	7.7	.7	14	<.1	.1	.1	51	.22	.007	3	14.8	.20	36	.073	1	.97	.011	.02	.1	.03	1.4	<.1	<.05	4	<.5	15
7200N 2400E	.5	93.1	2.8	32	.1	17.7	10.3	374	2.32	5.2	.3	3.0	1.3	18	.1	.2	.1	76	.21	.026	5	30.0	.41	41	.139	2	2.08	.011	.06	.1	.04	3.0	<.1	<.05	6	<.5	15
7200N 2450E	.8	149.3	4.8	39	.1	24.3	12.4	354	2.61	5.6	.4	3.1	1.6	19	<.1	.2	.1	85	.21	.052	5	35.7	.64	52	.170	3	3.43	.009	.04	.1	.06	3.4	.1	<.05	8	.5	15
7200N 2500E	1.0	94.2	20.1	199	.4	25.1	32.6	3647	6.23	13.7	.2	8.8	.8	44	.5	.6	.6	155	.78	.132	6	68.1	.42	134	.257	2	2.01	.008	.03	.1	.11	5.2	.1	<.05	14	.7	15
7200N 2550E	.7	120.4	10.7	99	.2	67.6	38.4	1439	7.62	5.1	.1	14.1	.4	10	.1	.7	.1	267	.25	.054	3	142.2	2.09	35	.475	1	2.74	.006	.06	<.1	.10	9.8	.1	<.05	16	.5	15
7200N 2585E	2.9	161.4	11.3	54	.1	38.2	18.9	636	4.77	6.2	.4	1.7	1.5	14	.1	.6	.2	142	.20	.044	7	49.5	.87	51	.213	1	3.59	.010	.04	.1	.05	3.7	.1	<.05	11	<.5	15
RE 7200N 2585E	2.8	163.1	11.8	57	.1	38.4	19.9	643	4.92	6.2	.4	2.3	1.6	13	.1	.6	.2	144	.19	.044	7	49.6	.90	51	.211	2	3.72	.011	.04	.1	.07	3.7	.1	<.05	11	<.5	15
7200N 2680E	.7	91.5	16.5	68	.1	24.5	45.9	1582	5.11	2.4	.2	10.3	.6	10	.2	.4	.2	137	.22	.078	5	53.7	.44	46	.364	1	1.88	.009	.03	<.1	.13	2.3	.1	<.05	12	.6	15
7200N 2750E	1.2	115.3	3.9	38	.1	19.1	12.1	285	2.68	3.8	.6	5.8	2.3	14	.1	.3	.1	85	.20	.049	15	30.4	.50	38	.182	3	3.57	.015	.07	.1	.07	5.6	.1	<.05	8	.7	15
7200N 2800E	.7	89.1	14.1	74	.1	18.3	10.2	2389	2.92	9.1	.4	3.5	1.2	22	.2	.3	.2	83	.32	.265	5	34.3	.35	134	.143	2	3.17	.011	.04	.1	.13	3.6	.1	<.05	9	.8	15
7200N 2830E	.9	50.2	7.8	54	.1	17.2	10.2	1555	2.77	4.5	.5	15.8	1.1	18	.1	.2	.1	83	.37	.084	8	25.5	.46	78	.143	2	2.64	.013	.04	.1	.05	2.5	.1	<.05	8	.5	15
7200N 2900E	1.3	70.5	5.4	182	.3	5.5	5.0	3573	2.00	13.1	1.0	3.1	<.1	61	8.0	1.0	<.1	25	2.72	.071	3	7.3	.06	62	.006	4	.34	.012	.02	.2	.23	.9	.1	.14	1.4	.4	1
7200N 2950E	1.0	59.7	7.3	69	.2	18.4	12.4	890	2.54	8.5	.2	15.0	.8	19	.2	.2	.1	74	.30	.046	4	23.4	.37	76	.110	2	2.09	.012	.04	.1	.08	2.3	<.1	<.05	7	.5	15
7200N 3000E	1.4	219.8	6.3	89	.3	30.9	21.3	681	4.21	18.8	.2	27.8	.6	88	.4	1.1	.1	126	.54	.076	5	48.9	.85	55	.278	2	3.07	.012	.06	.1	.11	5.4	<.1	<.05	12	1.2	15
STANDARD DS6	11.9	127.0	29.7	143	.3	25.0	11.2	740	2.79	22.1	6.9	48.9	3.0	37	6.2	3.3	5.2	60	.84	.084	14	185.5	.59	166	.085	17	1.91	.072	.16	3.4	.24	3.3	1.8	<.05	6	4.4	15

GROUP 1DX - 15.00 GM SAMPLE LEACHED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 300 ML, ANALYSED BY ICP-MS.

(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.

- SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Returns and 'RRE' are Reject Returns.

Data & FA \_\_\_\_\_ DATE RECEIVED: JUL 25 2005 DATE REPORT MAILED: Aug 5/05



All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Tl	B	Al	Na	K	W	Hg	Sc	Ti	S	Ga	Se	Sample
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppb	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	ppm	ppm	ppm	ppm	%	ppm	ppm	gm	
7200N 3050E	2.2	34.2	8.5	74	.1	20.5	11.2	1492	2.95	30.6	9	1.1	.8	14	.3	.4	.1	49	.40	.133	5	22.2	.48	95	.053	2	1.69	.009	.03	.2	.07	2.4	.1	.08	5	<.5	15.0
7200N 3100E	.7	107.8	5.5	120	.2	27.5	15.5	2202	3.93	10.5	.3	6.5	1.1	26	.3	.2	.1	102	.29	.181	6	38.0	.56	77	100	3	2.61	.011	.09	.1	.08	3.7	.1	<.05	9	<.5	15.0
7200N 3150E	1.7	120.7	7.8	103	.1	35.7	18.8	917	7.32	10.9	.2	3.5	1.1	15	.3	1.2	.1	127	.22	.058	10	36.0	.39	59	100	1	2.32	.010	.02	.1	.08	4.9	.1	<.05	9	<.5	15.0
7200N 3200E	.4	240.2	4.5	425	.4	23.5	11.1	298	2.65	174.4	.3	10.7	1.9	37	.5	1.1	<.1	68	.27	.018	8	27.8	.66	46	109	1	2.16	.018	.04	.1	.16	6.1	<.1	<.05	6	6	15.0
7100N 2300E	1.0	234.0	5.9	85	.1	53.2	20.8	1977	4.20	6.4	.2	4.9	.9	42	.2	.2	.1	120	.71	.066	4	67.4	.85	148	331	3	2.65	.015	.05	<.1	.09	4.3	.1	<.05	11	5	15.0
7100N 2350E	4.2	86.9	16.9	88	.2	51.1	40.4	6844	4.01	12.9	.9	1.4	1.4	26	.8	.4	.2	107	.90	.097	17	67.9	.35	96	140	3	3.98	.016	.03	.1	.14	7.1	.2	<.05	8	1.6	15.0
RE 7100N 2500E	.6	98.8	4.8	31	.1	18.3	7.1	491	1.92	6.3	.6	1.2	.7	23	.2	.2	.1	59	.52	.026	9	30.3	.30	48	093	2	1.97	.012	.02	.1	.07	3.2	.1	<.05	4	.8	15.0
7100N 2400E	2.0	133.5	21.7	33	.1	13.2	7.4	625	3.29	125.0	.6	2.1	1.3	27	.4	1.0	.2	21	2.53	.026	15	14.3	.12	75	.003	2	1.33	.008	.05	.1	.07	5.5	.1	<.05	3	6	15.0
7100N 2450E	2.8	45.0	3.7	37	.1	14.2	9.2	170	2.65	4.5	.2	.9	1.2	15	<.1	.2	.1	71	.16	.013	6	26.0	.33	47	.064	1	1.91	.009	.03	.1	.02	2.0	<.1	<.05	7	<.5	15.0
7100N 2500E	.7	99.0	4.7	28	.1	19.3	7.0	484	1.95	5.9	.6	6.2	.6	22	.2	.2	<.1	58	.48	.025	9	28.5	.29	45	090	2	1.92	.012	.02	<.1	.06	3.3	<.1	<.05	5	.7	15.0
7100N 2550E	.9	66.6	10.3	84	.1	24.9	13.2	812	4.15	5.9	.2	1.5	.9	23	.2	.2	.2	124	.48	.103	4	42.9	.42	63	.324	2	1.97	.009	.06	<.1	.07	2.4	.1	<.05	11	<.5	15.0
7100N 2600E	1.7	317.8	17.0	90	.2	45.0	26.9	750	6.53	6.5	.3	14.0	.9	24	.3	.7	.2	234	.40	.082	6	90.2	.82	40	.380	1	3.33	.008	.03	.1	.13	7.4	.1	<.05	14	.8	15.0
7100N 2650E	.8	77.7	8.4	38	.1	18.4	9.9	218	3.43	3.1	.2	5.8	1.0	14	.1	.3	.1	108	.23	.033	3	31.9	.28	44	.203	2	2.41	.009	.02	<.1	.05	2.2	<.1	<.05	10	<.5	15.0
7100N 2725E	1.6	106.5	8.4	46	.1	28.9	13.5	223	4.30	6.9	.3	9.5	1.4	13	.1	.5	.2	136	.17	.061	5	50.2	.44	67	.263	1	4.52	.010	.02	<.1	.06	2.9	.1	<.05	13	<.5	15.0
7100N 2750E	1.0	52.8	9.4	70	.1	19.3	17.0	1123	4.33	9.5	.2	5.5	.9	26	.1	.4	.2	134	.32	.107	6	50.9	.41	87	.291	2	1.97	.012	.03	<.1	.10	2.8	.1	<.05	13	<.5	15.0
7100N 2800E	1.0	153.4	11.9	87	.1	28.0	19.7	1021	5.90	11.5	.2	18.4	.7	28	.2	.7	.1	203	.39	.128	5	64.0	.82	74	.282	2	2.65	.010	.07	<.1	.09	6.5	.1	<.05	13	.6	15.0
7100N 2840E	.6	57.6	5.6	20	.1	11.1	7.1	196	1.73	4.4	.3	1.6	.8	19	.1	.2	.1	51	.51	.015	7	19.7	.21	39	.095	<.1	1.66	.011	.02	.1	.05	2.0	.1	.06	5	<.5	15.0
7100N 2900E	.8	121.2	26.8	193	.6	18.9	25.1	1110	4.72	6324.4	.3	95.1	1.0	29	1.0	11.1	1.1	68	.32	.088	6	31.6	.36	96	.059	1	2.11	.011	.03	.1	.13	3.4	.1	<.05	7	.8	15.0
7100N 2950E	.8	56.1	24.0	126	.1	17.9	12.2	1676	2.64	32.4	.3	3.5	1.0	31	.4	.3	.1	81	.36	.090	4	24.1	.41	134	.108	2	2.62	.012	.04	.1	.09	2.5	.1	<.05	7	<.5	15.0
7100N 3000E	1.4	113.1	7.6	76	.2	25.4	15.1	216	4.18	34.0	.4	3.4	1.3	16	.2	.6	.1	123	.21	.065	7	40.0	.52	26	.188	1	4.15	.013	.04	.1	.09	3.9	<.1	<.05	12	.6	15.0
7100N 3050E	.7	74.6	9.8	103	.3	38.5	23.4	1798	6.78	9.8	.1	8.4	.4	21	.2	.4	.1	226	.33	.208	3	76.2	1.62	42	.136	1	2.93	.008	.06	<.1	.20	6.9	<.1	<.05	16	.5	7.5
7100N 3100E	1.3	137.1	9.3	147	.2	44.4	27.8	964	8.13	10.6	.2	6.1	.7	9	.2	2.1	.1	306	.18	.109	5	62.8	1.43	28	.402	1	2.91	.005	.04	<.1	.07	9.4	.1	<.05	19	.5	7.5
7100N 3150E	1.0	198.5	17.9	133	.2	46.0	34.5	5350	7.20	8.8	.2	9.0	.5	31	.4	.7	.1	252	.93	.081	7	60.4	1.47	75	.459	2	2.63	.007	.02	.1	.16	10.5	.1	<.05	16	.5	1.0
7100N 3200E	1.1	91.7	6.7	150	.2	48.9	35.5	3189	6.43	14.2	.1	9.1	.5	16	.3	.9	.1	193	.24	.120	6	75.6	1.57	68	.093	1	3.29	.006	.06	<.1	.08	11.1	.1	<.05	13	<.5	1.0
7000N 2300E	.4	28.5	8.1	65	.1	29.5	11.3	750	3.69	1.1	.1	2.8	.6	15	.1	.2	.2	120	.45	.054	3	72.4	.56	40	.205	1	1.64	.009	.02	<.1	.08	5.6	<.1	<.05	10	<.5	15.0
7000N 2350E	1.3	51.9	21.9	79	.1	44.4	20.4	1191	4.06	9.2	.2	13.4	.5	32	.6	.4	.2	140	.79	.021	6	56.7	.97	60	.269	<.1	1.95	.012	.03	<.1	.17	4.6	<.1	<.05	9	<.5	7.5
7000N 2400E	1.2	290.4	5.6	41	.2	55.9	22.2	272	3.88	6.5	.8	3.3	2.6	17	.2	.3	.1	127	.27	.017	11	95.8	.85	79	.235	2	4.63	.016	.03	.1	.05	11.4	.1	<.05	12	.6	15.0
7000N 2450E	1.1	78.4	4.4	44	.1	41.2	15.6	398	3.43	10.2	.2	4.9	.9	23	.1	.1	.1	109	.33	.024	5	45.7	.82	49	.174	2	2.62	.011	.03	.1	.04	3.2	<.1	<.05	8	<.5	15.0
7000N 2500E	.7	55.7	21.3	195	.1	52.1	25.2	5139	4.35	17.0	.2	5.3	.8	40	.6	.3	.2	93	.71	.296	5	59.1	.76	187	.269	2	2.35	.014	.05	.1	.22	4.8	.2	.16	12	.8	7.5
7000N 2525E	.5	51.8	12.1	102	.1	15.6	18.7	1189	4.87	1.3	.2	13.6	.8	24	.2	.3	.2	113	.36	.052	4	58.8	.26	32	.488	1	.99	.006	.02	<.1	.09	2.9	<.1	<.05	12	<.5	15.0
7000N 2600E	1.1	122.8	12.2	78	.1	17.0	9.5	205	5.04	7.6	.7	17.5	1.8	7	.1	.2	.3	158	.13	.256	6	92.4	.24	41	.397	1	3.33	.008	.04	<.1	.12	4.2	.1	<.05	24	.5	15.0
7000N 2650E	.6	30.8	6.8	42	.1	14.4	10.1	856	2.34	2.7	.2	4.2	.7	15	.1	.2	.1	91	.35	.042	3	27.4	.38	45	.275	1	1.34	.013	.03	<.1	.04	2.3	.1	<.05	7	<.5	15.0
7000N 2700E	.6	57.0	4.9	83	.1	19.1	11.3	445	3.31	7.5	.2	2.9	1.0	12	.1	.1	.1	92	.22	.166	4	31.2	.27	71	.172	1	1.93	.016	.03	<.1	.04	2.2	.1	<.05	9	<.5	15.0
7000N 2750E	.8	54.2	11.2	78	.2	22.8	16.5	1196	6.09	683.1	.2	6.4	.7	17	.2	1.1	.3	182	.25	.052	4	62.8	.50	62	.382	1	1.87	.013	.02	<.1	.09	3.9	.1	<.05	14	<.5	15.0
STANDARD DSG	11.6	124.9	29.6	147	.3	24.7	10.8	714	2.80	21.9	6.4	49.6	2.9	37	6.1	3.5	4.8	58	.87	.083	15	198.0	.59	163	.085	17	1.88	.070	.16	3.6	.23	3.5	1.7	<.05	6	4.6	15.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B %	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
7000N 2800E	.7	39.1	3.5	22	.1	12.4	6.5	151	1.77	4.1	.2	1.8	.8	12	.1	.1	.1	54	.22	.008	5	20.1	.26	27	.102	3	1.64	.009	.02	.1	.03	1.7	<.05	<.05	5	<.5	15.0
7000N 2850E	.8	31.6	3.8	36	.1	15.6	9.1	265	2.29	4.5	.2	7.8	.7	23	.1	.1	.1	67	.24	.021	4	24.1	.34	74	.109	2	1.82	.011	.07	.1	.04	1.6	<.05	<.05	6	<.5	15.0
7000N 2900E	.6	80.0	4.8	37	.1	15.2	9.9	554	2.37	14.4	.3	4.9	1.1	26	.1	.2	.1	74	.34	.033	6	27.8	.50	55	.116	1	1.99	.015	.03	.1	.04	3.3	<.05	<.05	5	<.5	15.0
7000N 2950E	1.2	73.8	16.7	64	.2	20.2	15.3	601	4.01	12.8	.4	5.2	1.6	20	.1	.4	.1	112	.21	.094	8	28.0	.44	85	.171	2	3.04	.011	.07	.1	.07	3.5	<.05	10	.6	15.0	
7000N 3000E	1.0	110.6	29.0	292	.4	24.1	26.2	4917	7.40	2846.2	.2	10.6	.7	36	1.9	3.7	.3	117	.52	.306	5	51.0	.60	139	.158	2	2.53	.012	.05	<.1	.17	4.4	<.05	15	.7	15.0	
7000N 3050E	2.1	2061.6	17.7	262	5.7	65.8	40.1	1816	12.54	69.3	.1	19.5	.5	24	1.5	310.2	.1	339	.31	.095	11	67.8	.96	41	.031	2	2.55	.006	.06	<.1	.11	15.5	<.05	15	1.1	7.5	
7000N 3100E	.9	123.3	8.8	95	.2	57.3	33.7	2494	8.66	7.7	.2	19.8	.5	17	.1	3.1	.1	315	.80	.079	7	69.9	1.53	51	.617	3	2.44	.007	.04	<.1	.12	14.0	<.05	18	.6	7.5	
7000N 3150E	.5	19.6	17.7	54	.1	15.0	10.5	1794	5.33	3.6	.1	6.7	.5	24	.1	.6	.2	159	.45	.055	3	27.8	.29	107	.446	2	.78	.010	.03	<.1	.12	2.7	<.05	8	<.5	15.0	
7000N 3200E	1.0	238.3	6.3	56	.1	26.2	14.5	466	3.77	7.4	.4	8.0	1.7	17	.1	.6	.1	115	.29	.046	8	35.1	.65	29	.162	2	3.15	.011	.03	.1	.06	6.9	<.05	9	.8	15.0	
6900N 2300E	1.0	65.9	21.6	95	.2	55.6	28.7	890	6.22	3.3	.3	4.0	.9	13	.2	.5	.3	184	.39	.077	4	93.6	.76	63	.325	1	3.07	.008	.04	<.1	.17	5.9	<.05	15	.6	15.0	
6900N 2350E	1.4	80.3	5.3	65	.1	33.7	14.6	269	3.41	3.8	.3	4.0	1.4	16	.1	.2	.1	96	.26	.030	4	37.7	.57	42	.189	3	2.84	.010	.07	.1	.06	3.0	<.05	9	<.5	15.0	
6900N 2400E	.9	125.6	10.2	72	.2	66.7	26.5	882	5.14	4.1	.2	59.5	.9	38	.1	.4	.1	143	.47	.047	5	76.0	1.40	55	.210	3	3.36	.011	.05	.1	.10	5.5	<.05	11	.6	15.0	
6900N 2450E	.6	27.0	13.1	71	.2	22.5	10.0	1995	3.54	5.8	.2	3.4	.5	17	.2	.3	.2	103	.28	.100	3	41.1	.44	75	.150	2	1.98	.010	.03	<.1	.17	2.0	<.05	10	.6	15.0	
6900N 2500E	.4	45.8	15.5	40	.2	21.1	10.4	851	2.14	2.8	.1	4.2	.3	40	.2	.3	.1	64	.69	.040	3	33.4	.47	76	.139	1	1.13	.011	.03	.1	.12	2.3	<.05	5	<.5	15.0	
6900N 2550E	1.0	36.7	8.9	118	.2	34.0	20.8	786	7.42	6.1	.2	5.4	.7	17	.2	.3	.2	193	.36	.099	3	102.9	1.41	39	.374	3	2.25	.007	.04	<.1	.09	3.3	<.05	18	.5	15.0	
6900N 2600E	1.0	71.2	13.2	168	.1	29.9	21.6	1902	7.27	27.8	.6	1.1	1.3	27	.2	.3	.3	157	.44	.149	6	64.1	.49	75	.298	2	2.69	.009	.04	<.1	.07	3.9	<.05	22	<.5	15.0	
6900N 2650E	3.6	50.6	30.8	80	.2	17.1	31.4	1165	7.78	41.6	.6	.9	.9	28	.2	.5	.5	231	.53	.146	5	55.0	.34	67	.274	2	2.00	.008	.04	.1	.13	3.2	<.05	21	.6	15.0	
6900N 2700E	1.1	244.2	8.3	69	.2	27.5	20.5	1423	6.25	20.0	.6	4.4	.9	12	.2	.3	.2	150	.32	.208	5	102.7	.62	38	.217	1	3.15	.011	.03	<.1	.27	6.0	<.05	14	1.4	15.0	
6900N 2750E	.7	110.3	3.2	45	.1	19.7	11.3	302	2.69	23.4	.3	2.2	1.4	17	.1	.3	.1	76	.19	.019	5	32.5	.60	74	.135	1	2.39	.010	.05	.1	.03	2.5	<.05	6	<.5	15.0	
6900N 2800E	.5	108.6	7.0	43	.1	21.3	12.0	731	2.84	13.3	.2	3.2	1.1	25	.1	.3	.1	83	.39	.035	4	34.7	.61	84	.151	3	2.13	.013	.04	.1	.06	2.7	<.05	6	<.5	15.0	
6900N 2850E	1.4	141.3	5.7	45	.2	25.0	20.4	194	3.29	220.1	.5	9.2	2.1	14	.2	.5	.1	92	.24	.038	7	45.4	.28	35	.151	1	3.88	.015	.04	.1	.06	4.2	<.05	9	.9	15.0	
6900N 2900E	.7	91.1	10.3	51	.1	25.1	18.4	494	3.27	13.2	.1	4.1	.6	26	.1	.3	.1	94	.39	.030	3	38.5	.58	66	.135	2	2.20	.014	.03	.1	.08	2.5	<.05	7	.5	15.0	
6900N 2950E	1.1	152.3	4.0	31	.2	23.0	15.9	221	2.82	10.2	.3	30.5	1.2	40	.1	.5	.1	83	.31	.045	6	34.1	.40	35	.130	3	3.26	.008	.03	.1	.06	3.9	<.05	7	.7	15.0	
6900N 3000E	.9	159.5	16.3	70	.2	30.8	22.7	2210	4.35	9.8	.4	5.7	.7	42	.3	1.0	.3	120	1.61	.063	9	61.5	1.00	52	.204	5	2.56	.014	.04	.1	.13	6.3	<.05	8	1.0	15.0	
6900N 3050E	1.9	907.3	15.0	99	.2	53.1	28.4	2254	7.83	17.5	.4	7.4	1.3	22	.4	1.2	.2	303	.54	.094	10	74.7	1.17	46	.310	3	4.15	.009	.05	.1	.12	12.6	<.05	17	.8	15.0	
6900N 3100E	2.1	331.1	12.4	126	.8	42.5	30.8	9649	5.98	13.2	1.0	6.6	1.3	35	2.4	1.5	.2	175	1.27	.127	31	48.0	.72	102	.364	5	3.13	.010	.05	<.1	.23	16.6	<.05	13	2.0	15.0	
6900N 3150E	1.2	123.3	17.5	88	.3	25.4	16.0	1595	3.72	16.0	.3	1.7	1.1	31	.3	1.5	.1	107	.50	.064	9	34.4	.46	57	.149	1	2.70	.010	.04	.1	.16	4.9	<.05	8	.8	15.0	
6900N 3200E	1.1	47.7	21.0	108	.2	16.1	21.3	1781	4.97	26.6	.2	7.5	1.2	18	.2	1.1	.3	139	.29	.051	6	32.0	.29	66	.194	1	1.76	.008	.03	<.1	.12	3.2	<.05	12	<.5	15.0	
6800N 2300E	1.5	131.9	5.3	64	.1	27.2	11.1	283	3.87	10.4	.8	5.9	2.5	8	.1	.3	.1	126	.11	.295	6	64.9	.58	24	.208	2	5.97	.008	.03	.1	.12	8.9	<.05	10	1.5	15.0	
6800N 2350E EMPTY	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
6800N 2400E	.7	15.1	8.6	51	.1	1.9	7.6	670	2.31	2.6	.7	2.8	1.6	66	.1	.4	.1	63	.30	.025	7	3.3	.20	105	.029	1	1.61	.006	.03	.1	.07	2.1	<.05	7	<.5	15.0	
6800N 2450E	1.3	79.6	9.0	67	.1	55.4	19.1	654	4.12	3.9	.2	1.1	.6	43	.2	.3	.1	134	.56	.039	3	65.6	1.13	62	.322	2	2.55	.012	.02	<.1	.11	2.6	<.05	10	<.5	15.0	
RE 6900N 2850E	1.4	136.3	5.8	42	.2	24.1	19.6	186	3.23	215.3	.5	67.3	2.1	13	.2	.4	.1	88	.22	.037	6	44.6	.28	35	.137	2	4.08	.015	.04	.1	.06	3.9	<.05	8	.8	15.0	
6800N 2500E	1.3	147.9	6.8	41	.3	26.9	13.8	550	3.24	6.7	.3	2.1	.7	20	.1	.3	.1	100	.87	.055	5	47.3	.69	23	.209	3	2.62	.019	.02	.1	.15	3.6	<.05	8	.6	15.0	
STANDARD DS6	11.9	124.9	30.3	149	.3	24.4	10.5	708	2.86	21.2	6.6	48.2	3.1	37	6.2	3.6	5.0	56	.86	.074	15	186.3	.59	163	.085	14	1.82	.073	.18	3.6	.22	3.5	1.7	<.05	6	4.4	15.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



ACME ANALYTICAL



ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B %	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
6800N 2550E	.8	25.2	23.0	101	.1	17.5	23.8	9752	3.13	8.9	.1	3.0	.3	50	.4	.3	.2	64	1.18	.214	3	28.4	26	191	.107	3	1.23	.008	.06	<.1	.23	2.6	.1	<.05	7	.8	15
6800N 2600E	.5	64.1	11.0	147	.3	46.0	30.8	6691	5.71	9.7	.3	.9	.3	16	.5	.2	.2	104	.39	.330	4	85.3	35	80	.139	1	2.29	.008	.03	<.1	.26	3.2	.1	<.05	15	1.0	15
6800N 2650E	1.1	42.1	11.4	60	.1	35.1	14.8	828	5.90	4.3	.2	12.4	.8	10	.1	.3	.3	185	.20	.086	3	78.2	52	40	.212	<1	2.31	.007	.02	<.1	.08	2.0	.1	<.05	15	<.5	15
6800N 2715E	1.5	13.2	29.2	64	.1	15.7	6.3	130	2.16	54.5	.8	17.9	.7	9	.1	.4	.2	26	19	.040	8	20.3	64	50	.005	<1	2.22	.006	.04	.1	.01	3.0	.2	<.05	4	.5	15
6800N 2750E	.7	61.7	11.3	208	.1	33.5	34.5	3257	5.65	40.5	.2	7.9	1.0	49	.3	.5	.4	124	.45	.435	4	64.6	88	166	.192	1	3.16	.010	.04	<.1	.11	4.8	.1	<.05	14	.8	15
6800N 2800E	.5	37.6	9.3	71	.1	16.0	9.1	1703	2.31	72.7	.2	6.5	.7	28	.3	.2	.1	66	41	.063	4	22.9	31	118	.101	1	1.89	.011	.03	<.1	.06	1.7	.1	<.05	6	<.5	15
6800N 2850E	.8	146.7	7.3	71	.1	25.8	17.6	506	4.25	9.5	.3	15.9	1.3	24	.1	.3	.1	119	27	.084	5	41.9	49	69	.227	2	2.98	.011	.03	<.1	.06	2.9	.1	<.05	12	<.5	15
6800N 2900E	1.0	102.4	5.8	49	.1	19.1	10.6	356	3.20	8.3	.3	4.3	1.3	15	.1	.2	.1	96	25	.043	4	37.2	43	37	.173	2	2.81	.010	.05	.1	.07	3.1	.1	<.05	8	<.5	15
6800N 2950E	.5	77.2	6.3	25	.1	13.2	7.5	293	1.95	3.0	.2	.7	.8	11	.1	.3	<.1	60	18	.016	4	22.8	33	32	.102	<1	1.78	.009	.02	.1	.04	1.9	<.1	<.05	5	<.5	15
6800N 3000E	1.0	154.0	6.9	43	.1	19.4	10.6	659	2.96	6.4	.3	2.4	1.3	18	.1	.3	.1	85	22	.067	5	30.0	59	50	.128	1	2.84	.011	.04	.1	.04	2.9	<.1	<.05	8	<.5	15
6800N 3050E	.9	59.9	17.7	81	.2	13.9	13.9	3529	6.03	7.1	.2	1.8	.5	22	.3	.4	.3	189	28	.146	4	37.3	18	63	.365	2	1.24	.008	.03	<.1	.24	2.6	.1	<.05	13	.7	15
6800N 3100E	2.1	158.4	23.1	153	.2	56.2	39.6	2392	8.70	36.3	.1	27.5	.7	13	.7	1.3	.5	255	21	.132	6	69.4	1.53	58	.155	<1	3.53	.006	.03	<.1	.06	8.8	.1	<.05	17	.6	15
6800N 3150E	.7	68.9	19.1	76	.1	21.0	13.7	2412	3.79	8.7	.2	2.3	1.3	12	.1	.5	.2	117	21	.063	5	29.7	32	71	.201	1	2.68	.010	.04	<.1	.10	2.7	.1	<.05	11	<.5	15
6800N 3200E	.9	116.5	8.2	59	.1	22.7	13.7	628	3.56	5.7	.3	2.7	1.3	13	.1	.4	.1	110	19	.077	6	30.6	52	62	.179	1	3.03	.010	.03	<.1	.08	3.2	.1	<.05	9	<.5	15
6700N 2300E	2.2	52.7	22.8	97	.2	27.9	23.8	3285	4.41	25.2	.7	108.0	1.8	40	.2	.7	.2	68	51	.058	15	25.7	1.00	153	.014	1	3.51	.008	.12	.1	.14	3.1	.2	<.05	8	.6	15
6700N 2350E	1.2	33.0	11.8	60	.1	41.9	17.9	651	5.98	4.9	.2	3.8	.7	15	.1	.3	.3	198	25	.122	3	73.9	1.04	51	.352	2	2.42	.009	.04	<.1	.12	1.9	.1	<.05	20	.5	15
6700N 2400E	.2	17.2	6.9	39	.1	20.2	5.8	258	1.81	1.7	.1	.6	.3	17	.1	.1	.1	79	30	.041	2	42.7	51	30	.266	1	.92	.012	.02	<.1	.06	2.2	<.1	<.05	6	<.5	15
6700N 2450E	.8	53.4	14.5	64	.2	41.1	23.1	2541	5.54	2.4	.2	1.1	.7	15	.2	.3	.3	163	46	.077	4	75.2	76	65	.332	1	2.07	.009	.03	<.1	.11	3.6	<.1	<.05	16	.5	15
6700N 2500E	.9	153.4	4.2	87	.1	23.1	16.0	522	2.65	28.7	.4	11.4	1.0	10	.2	.3	.1	67	27	.108	4	31.9	55	20	.103	<1	2.14	.009	.02	.1	.07	2.8	<.1	<.05	6	.5	15
6700N 2560E	.8	50.7	15.0	73	.1	30.3	11.2	634	6.16	3.9	.2	8.7	.9	8	.1	.6	.2	199	25	.143	3	104.6	.32	40	.301	1	2.48	.007	.02	<.1	.16	3.5	.1	<.05	16	.5	15
6700N 2600E	.8	40.9	13.4	66	.1	30.9	11.2	645	5.92	5.5	.3	10.9	1.0	8	.1	.2	.3	124	16	.298	3	87.4	.32	46	.297	<1	2.36	.007	.03	<.1	.12	3.0	.1	<.05	16	.5	15
6700N 2650E	.6	54.0	15.2	76	.2	59.7	27.1	3434	4.01	4.8	.1	20.2	.5	56	.3	.3	.2	109	77	.130	3	54.5	92	144	.214	2	2.77	.012	.05	<.1	.19	2.9	.1	<.05	12	.6	15
6700N 2700E	2.0	111.3	11.9	76	.2	50.2	28.4	1714	5.92	9.8	.4	18.6	1.3	18	.2	.5	.4	158	30	.131	5	72.7	59	83	.230	1	3.67	.014	.04	<.1	.11	3.3	.1	<.05	15	.7	15
RE 6700N 2800E	5.2	476.7	3.2	50	.5	21.5	18.1	293	4.70	210.1	.8	55.6	1.7	17	.2	.8	.4	69	36	.057	5	30.1	53	45	.106	2	1.96	.018	.03	<.1	.05	3.6	.1	<.05	6	2.5	15
6700N 2750E	4.1	189.3	4.8	22	.1	14.9	17.1	872	12.15	23.2	.7	186.0	.6	8	.1	.4	.2	43	3.95	.096	5	26.2	23	27	.084	1	1.25	.005	.01	.3	.05	3.7	<.1	<.05	9	.7	15
6700N 2800E	5.7	472.6	3.2	48	.5	21.8	18.4	295	4.71	215.4	.8	54.0	1.6	18	.2	.9	.4	67	37	.054	5	30.4	49	46	.108	1	1.78	.017	.03	.1	.04	3.7	.1	<.05	6	2.4	15
6700N 2850E	.5	26.8	4.4	35	<.1	12.7	6.2	192	2.23	2.1	.1	1.7	.7	13	.1	.1	.1	71	20	.014	4	21.4	19	36	.125	1	1.38	.008	.02	<.1	.02	1.3	<.1	<.05	6	<.5	15
6700N 2900E	.8	115.7	8.5	41	.1	23.2	13.2	625	2.82	5.4	.2	51.0	.9	20	.2	.3	.1	87	48	.034	5	37.3	63	40	.165	3	2.19	.016	.03	.1	.04	3.5	<.1	<.05	6	.7	15
6700N 2950E	1.2	142.2	9.9	37	.1	21.6	14.2	320	3.29	6.0	.3	4.9	1.2	23	.1	.3	.1	92	24	.055	5	32.4	58	24	.142	1	2.48	.010	.03	.1	.05	3.7	<.1	<.05	7	.6	15
6700N 3000E	1.0	115.1	11.5	100	.2	21.0	35.8	4401	5.23	8.6	.2	1.5	.7	108	.3	.5	.2	127	.80	.173	6	24.0	1.17	169	.113	2	3.37	.009	.07	.1	.12	4.1	.1	<.05	11	.7	15
6700N 3050E	1.1	156.8	4.8	107	.4	52.3	27.5	1328	6.41	6.4	.7	4.2	.3	45	.2	.4	.1	167	24	.103	4	99.7	2.77	54	.161	1	4.80	.010	.04	<.1	.22	5.6	.1	.06	13	1.4	15
6700N 3100E	.7	66.9	22.3	85	.1	33.8	22.7	3004	5.12	4.1	.2	5.0	.5	44	.2	.4	.2	134	51	.096	4	48.4	1.07	85	.339	2	2.32	.015	.05	<.1	.12	2.8	.1	<.05	13	.6	15
6700N 3150E	.7	34.0	21.1	72	.1	18.1	15.3	3489	4.79	5.3	.2	1.3	.7	29	.3	.5	.3	135	38	.091	3	38.2	46	109	.342	1	1.55	.009	.04	<.1	.17	2.1	.1	<.05	13	.5	15
6700N 3200E	.5	39.4	9.3	75	.1	16.5	11.9	3126	3.34	5.9	.2	.9	1.1	17	.1	.2	.1	77	25	.343	4	30.1	22	123	.200	2	2.52	.010	.03	<.1	.14	2.7	.1	<.05	9	.6	15
STANDARD DS6	12.2	125.0	31.2	148	.3	25.6	11.0	731	2.87	21.9	6.7	48.9	3.1	37	6.1	3.6	5.2	59	89	.087	15	200.6	60	166	.088	16	2.04	.074	.17	3.5	.23	3.4	1.8	<.05	6	4.6	15

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga	Se	Sample gm
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppb	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	ppm	ppm	ppm	ppm	%	ppm	ppm		
6600N 2300E	1.3	83.1	7.6	80	.1	87.3	26.2	942	6.84	4.6	.4	2.4	8	23	.1	.5	.2	229	.38	.073	4	138.0	1.47	49	.576	2	3.05	.008	.03	<.1	.11	4.6	.1	<.05	15	<.5	15.0
6600N 2350E	6	33.9	13.5	76	.1	35.6	17.4	3184	3.39	2.9	.2	2.5	5	29	.2	.2	.2	102	.77	.111	3	73.8	.64	118	.253	3	1.54	.008	.03	<.1	.12	5.1	.1	<.05	8	<.5	15.0
6600N 2400E	1.2	39.1	8.5	53	.1	57.0	20.7	871	5.17	3.1	.2	1.7	5	24	.1	.1	.2	176	.48	.085	3	86.5	1.36	27	.372	2	2.50	.009	.02	<.1	.13	4.9	<.1	<.05	12	<.5	15.0
6600N 2450E	8	79.7	9.3	83	.1	102.0	34.7	1857	5.81	8.0	.2	5.6	5	35	.4	.2	.1	179	1.01	.091	5	132.3	2.56	82	.681	4	3.04	.017	.09	.14	9.4	.1	<.05	13	6	7.5	
6600N 2500E	1.7	151.9	5.4	65	.3	51.1	23.7	578	5.07	13.9	2.8	2.7	1.1	25	3	2.4	.1	142	1.68	.032	13	107.8	1.20	24	.323	3	3.55	.014	.03	<.1	.10	11.4	.1	<.05	15	1.6	15.0
6600N 2550E	1.0	43.1	18.4	60	.1	17.5	11.4	1122	2.74	8.4	.2	19.2	6	66	.2	.4	.2	78	.69	.091	6	20.6	.38	132	.131	3	1.90	.012	.05	.1	.14	3.1	.1	<.05	8	<.5	7.5
6600N 2600E	8	144.3	10.8	82	.2	32.5	18.5	1335	3.91	10.7	.6	3.6	5	8	2	.3	.2	91	.12	.389	6	71.4	.30	60	.117	1	4.03	.009	.03	<.1	.17	3.9	.1	<.05	13	1.8	15.0
6600N 2650E	9	183.0	5.7	31	.1	24.6	10.9	468	3.34	14.9	.6	7.0	2.7	22	.1	.3	.1	100	.27	.125	7	50.0	.58	22	.174	4	4.49	.012	.04	.2	.08	6.4	<.1	<.05	7	8	15.0
6600N 2700E	6	16.0	13.1	105	.1	7.4	14.6	3160	3.67	6.3	.3	3.1	8	34	.2	.2	.2	108	.33	.070	6	15.6	.32	166	.036	1	1.90	.010	.03	<.1	.10	2.8	.1	<.05	8	<.5	15.0
6600N 2750E	2.3	29.6	6.8	18	.1	15.2	8.6	188	2.11	6.2	.2	1.1	6	16	.1	.2	.1	68	.39	.009	4	23.8	.19	21	.122	1	1.27	.009	.02	<.1	.04	1.5	<.1	<.05	5	<.5	15.0
6600N 2800E	7	57.1	3.1	47	.2	15.0	10.0	192	2.19	498.6	.3	3.3	1.3	13	.2	.5	<.1	56	.19	.017	5	22.9	.30	30	.079	2	1.82	.008	.04	.1	.04	2.3	.1	<.05	5	<.5	15.0
6600N 2900E	1.4	137.4	21.7	145	.4	44.8	43.8	2792	7.59	14.7	.9	6.1	5.5	76	5	.4	.3	126	.64	.109	14	77.1	.78	91	.163	4	6.94	.013	.05	.1	.15	15.7	3	<.05	8	1.8	15.0
6600N 2950E	9	34.2	7.9	25	.1	16.2	7.9	293	2.47	2.3	.1	3.0	5	21	<.1	.3	.1	93	.30	.018	5	28.6	.56	30	.173	2	1.45	.011	.02	<.1	.07	2.8	<.1	<.05	6	<.5	15.0
6600N 3000E	1.1	133.4	4.3	48	.1	29.3	15.6	273	4.30	3.8	.2	32.6	9	21	.1	.3	.1	140	.26	.042	4	47.4	.69	36	.207	3	2.58	.010	.03	<.1	.04	4.5	<.1	<.05	10	5	15.0
6600N 3050E	1.6	88.1	13.5	102	.2	40.2	25.0	3275	6.14	6.5	.3	4.0	1.0	35	.2	.3	.2	164	.54	.123	6	58.2	.73	120	.228	2	3.41	.011	.04	<.1	.26	3.3	.1	<.05	14	9	15.0
6600N 3100E	1.0	39.4	18.8	79	.2	23.5	19.4	2033	4.45	5.2	.2	2.9	.6	28	.2	.4	.2	127	.51	.086	4	42.8	.51	95	.192	3	2.11	.009	.03	<.1	.16	2.0	.1	<.05	12	.6	15.0
6600N 3150E	.6	47.6	32.3	118	.1	31.4	29.0	10746	5.83	7.7	.2	1.8	6	39	.4	.5	.3	131	.60	.123	4	58.3	1.12	264	.206	1	2.34	.007	.03	<.1	.27	3.0	.1	<.05	13	8	15.0
6600N 3200E	.7	87.7	16.6	77	.1	39.8	24.2	4743	4.98	5.0	.5	2.7	2.0	45	.2	.2	.2	130	.46	.078	17	58.1	.83	248	.210	3	5.44	.009	.07	<.1	.16	7.2	.1	<.05	15	7	15.0
6500N 2300E	6	41.9	5.8	108	.3	73.1	28.5	1800	4.45	11.3	.2	3.8	6	50	.2	.2	.1	134	.79	.161	4	81.0	1.66	98	.260	3	2.97	.014	.06	<.1	.10	8.2	.1	<.05	11	6	7.5
6500N 2350E	.4	44.9	11.3	69	.1	26.5	13.0	1995	2.95	3.9	.3	3.1	1.1	16	.1	.2	.1	71	.27	.192	6	36.4	.31	73	.139	1	2.13	.010	.03	<.1	.09	3.0	.1	<.05	9	<.5	15.0
6500N 2400E	.8	124.2	8.4	133	.4	68.6	26.7	5642	6.22	10.5	.6	3.6	.1	15	.6	.2	.2	133	.29	.472	4	162.8	.80	67	.086	<.1	3.35	.009	.03	<.1	.22	3.0	<.1	<.05	16	1.7	15.0
6500N 2450E	.7	63.3	4.2	97	.1	72.3	28.6	1442	4.70	6.0	.3	4.5	.6	43	.2	.1	.1	120	.57	.139	4	84.3	1.53	47	.296	2	2.95	.011	.04	.1	.07	4.7	<.1	<.05	11	<.5	15.0
6500N 2500E	5	301.7	2.3	85	.1	65.2	38.8	688	6.91	3.2	.2	3.1	4	14	.1	.1	<.1	221	.91	.051	4	125.8	2.20	16	.489	2	2.91	.011	.05	<.1	.06	6.2	<.1	<.05	15	<.5	7.5
RE 6500N 2500E	4	300.6	2.5	86	.1	62.3	38.5	702	6.95	3.2	.2	3.2	4	15	.1	.1	.1	228	.94	.051	5	128.6	2.23	16	.512	3	2.93	.012	.05	<.1	.05	6.4	<.1	<.05	14	5	7.5
6500N 2550E	1.5	154.5	8.6	102	.2	50.0	28.6	1173	5.88	13.3	.3	4.9	7	29	.3	.7	.1	170	.43	.159	5	89.9	1.13	39	.286	2	2.82	.008	.05	.1	.09	8.2	.1	<.05	14	6	15.0
6500N 2615E	1.0	72.4	7.0	98	.1	77.6	30.7	1165	5.50	20.9	.3	47.7	8	56	3	.4	.1	143	.47	.103	7	82.7	2.06	53	.223	2	3.93	.010	.06	.1	.07	7.0	.1	<.05	12	5	7.5
6500N 2650E	1.1	60.2	5.8	50	.1	60.1	23.7	374	3.63	17.3	.1	44.0	4	18	.1	.4	.1	99	.28	.040	4	57.8	.54	59	.064	1	2.81	.013	.07	<.1	.06	4.3	.1	<.05	9	<.5	15.0
6500N 2700E	1.4	281.9	4.7	40	.6	54.0	31.6	429	4.44	25.2	.3	96.6	1.1	44	.1	.3	.1	85	.91	.024	10	30.8	.87	53	.029	<.1	3.16	.014	.05	.1	.06	5.5	.1	<.05	9	5	15.0
6500N 2715E	6.2	9381.7	30.3	164	7.6	67.0	328.5	2250	19.20	261.5	.8	2163.4	3	40	5.1	1.7	1.1	61	6.62	.044	5	25.7	.50	27	.024	2	1.19	.009	.04	2.3	.39	4.1	<.1	.26	11	4.9	15.0
6500N 2750E	1.2	213.0	15.6	119	.3	50.3	43.1	2695	7.29	20.8	.2	26.4	9	49	6	1.4	.2	176	.63	.042	8	65.5	.74	144	.066	2	3.81	.013	.07	<.1	.18	8.9	.2	<.05	12	6	15.0
6500N 2790E	3.1	178.4	8.1	57	.2	45.1	46.0	1021	8.39	71.0	.1	105.8	4	22	1	1.1	.2	195	.36	.046	5	55.4	1.30	99	.017	1	3.53	.009	.04	<.1	.07	6.6	.1	<.05	12	<.5	15.0
6500N 2850E	1.2	90.6	12.8	67	.2	23.4	24.5	1076	7.74	8.9	.4	13.8	6	21	.2	.4	.2	201	.29	.139	5	63.4	.65	54	.306	2	2.45	.008	.03	<.1	.25	2.8	<.1	<.05	19	1.1	15.0
6500N 2880E	1.6	72.5	17.1	56	.1	32.0	17.6	972	4.98	3.3	.2	42.3	8	23	1	.3	.2	147	.37	.051	4	50.4	.79	83	.322	1	3.07	.013	.03	<.1	.07	2.7	.1	<.05	13	<.5	15.0
6500N 2950E	1.1	205.9	4.1	37	.1	22.9	11.7	227	3.54	4.1	.5	6.8	1.7	13	1	.3	.1	110	.14	.036	10	42.5	.60	19	.192	3	3.04	.011	.03	.1	.05	7.7	<.1	<.05	8	7	15.0
STANDARD DS6	11.8	125.7	30.1	147	.4	25.4	10.5	701	2.89	21.2	6.8	51.5	3.1	38	6.1	3.5	5.0	58	.83	.075	15	184.7	.59	163	.080	21	1.83	.073	.16	3.3	.23	3.4	1.7	<.05	6	4.3	15.0

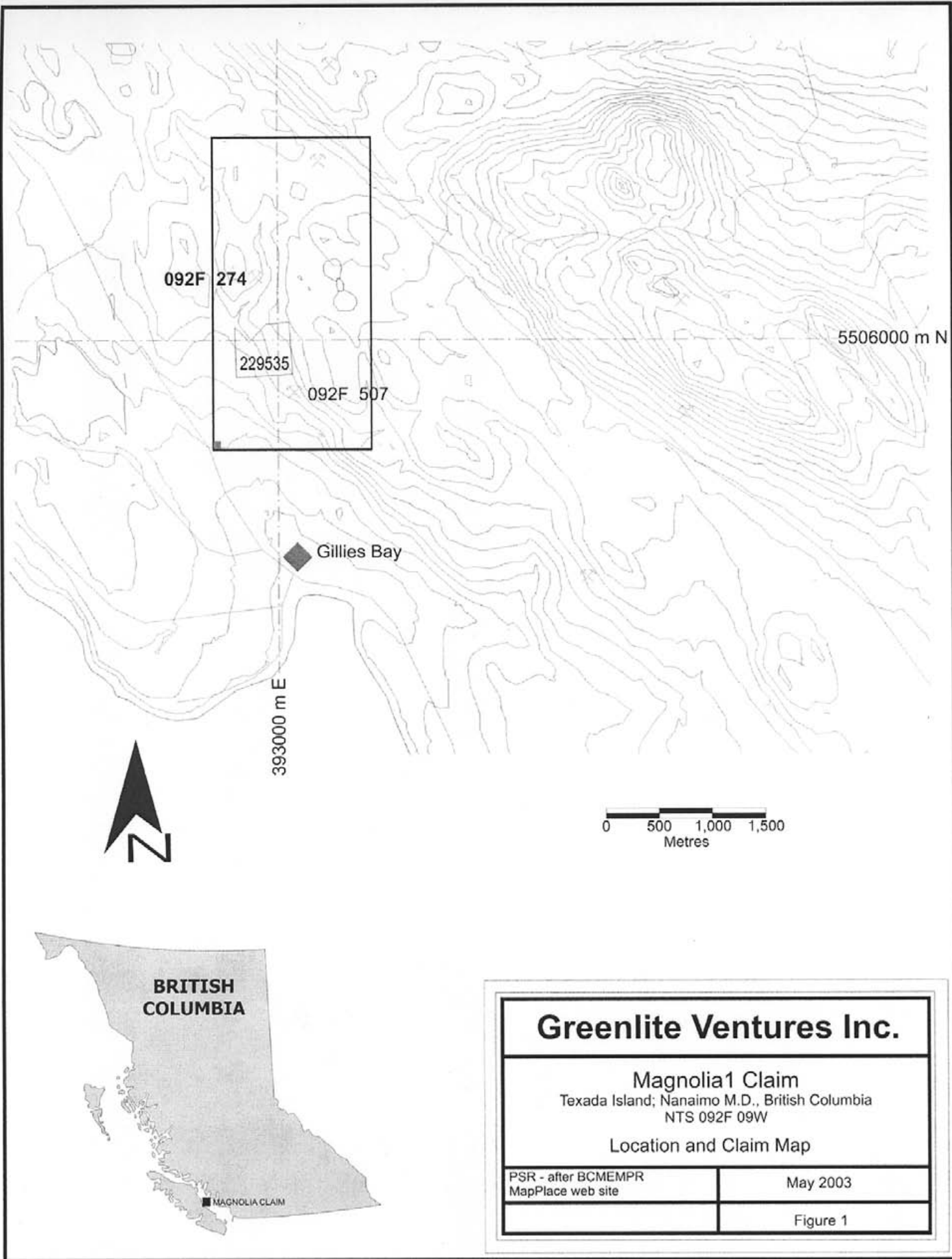
Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga	Se	Sample
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppb	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	%	ppm	ppm	ppm	ppm	%	ppm	ppm	gm
6500N 3000E	1.6	292.6	3.9	78	.1	53.5	31.5	1003	10.53	4.7	.1	7.5	.6	11	.1	.8	.1	286	.14	.089	10	93.5	1.40	60	.015	1	4.61	.006	.03	.1	.05	13.5	.1	<.05	17	.5	15.0
6500N 3050E	1.4	117.1	12.9	92	.1	39.3	23.3	517	8.62	3.3	.2	9.8	.9	12	.1	.7	.4	285	.28	.047	5	87.8	.89	37	.436	1	3.40	.007	.03	<.1	.09	5.9	.1	<.05	20	<.5	15.0
6500N 3100E	.6	22.0	8.6	46	<.1	18.5	9.1	1544	3.97	3.8	.2	2.4	.9	12	.1	.3	.2	118	.21	.089	3	37.2	.34	83	.190	1	2.25	.009	.03	<.1	.09	1.7	.1	<.05	11	<.5	15.0
6500N 3150E	.5	19.6	4.4	28	<.1	15.4	7.0	256	1.99	1.2	.1	.5	.7	10	<.1	.1	.1	59	.15	.016	4	18.6	.21	82	.094	2	1.89	.008	.02	<.1	.02	1.2	.1	<.05	6	<.5	15.0
6500N 3200E	1.3	69.8	5.3	25	<.1	24.1	10.7	151	3.54	3.3	.2	2.1	.9	11	<.1	.2	.1	104	.16	.018	4	34.6	.37	45	.162	1	3.11	.011	.01	<.1	.04	2.1	<.1	<.05	9	<.5	15.0
6400N 2300E	.5	23.6	11.8	73	.2	9.6	8.1	1639	2.52	6.8	.4	1.3	1.4	16	.1	.2	.1	53	.24	.375	4	18.4	.47	122	.077	1	1.88	.010	.04	.1	.10	2.4	.1	<.05	6	.7	7.5
6400N 2350E	.4	18.4	19.6	105	.1	15.7	8.9	1787	2.28	7.1	.4	2.4	.8	25	.2	.2	.1	56	.91	.150	4	21.1	.47	74	.085	2	1.64	.018	.03	.1	.16	2.0	.1	<.05	6	.7	7.5
6400N 2400E	2.3	114.5	7.0	63	.2	28.7	15.4	423	4.20	10.0	.6	2.4	2.0	17	.2	.8	.1	111	.29	.031	6	36.3	.87	31	.231	3	3.68	.015	.04	.1	.09	4.0	.1	<.05	11	.7	15.0
6400N 2450E	.8	131.6	16.3	87	.1	43.7	21.0	2720	4.85	6.3	.2	4.5	.6	41	.2	.3	.1	152	.66	.106	5	105.5	1.58	64	.248	2	2.73	.009	.05	.1	.12	8.0	.1	<.05	12	.7	7.5
6400N 2500E	.6	34.5	5.9	60	.1	34.7	17.6	529	4.63	1.1	.1	2.9	.3	21	<.1	.3	.1	154	.45	.028	3	75.9	.85	42	.330	2	1.78	.012	.04	<.1	.07	4.7	<.1	<.05	11	<.5	15.0
6400N 2550E	.9	69.9	4.8	31	.1	17.6	9.2	337	2.58	5.4	.2	4.1	1.1	19	.1	.3	.1	81	.30	.034	6	32.0	.37	32	.120	1	1.79	.011	.03	.1	.07	2.7	<.1	<.05	5	.5	15.0
6400N 2600E	6.8	14.8	21.5	104	.3	11.3	4.3	3419	2.48	53.2	.8	6.5	1.0	47	6	2.0	.2	10	2.85	230	18	9.7	.08	112	.004	6	.96	.007	.09	.1	.12	5.2	.2	<.05	2	1.0	15.0
6400N 2650E	.9	98.9	2.6	29	.2	16.0	9.3	182	2.38	22.4	.3	13.2	1.4	14	.1	1.5	<.1	74	.22	.014	6	31.6	.40	23	.122	2	2.06	.011	.02	<.1	.07	4.4	.1	<.05	6	.8	15.0
6400N 2700E	2.2	170.2	21.1	115	.3	32.3	44.2	1208	6.83	18.7	.3	30.5	1.1	22	.2	.8	.3	163	.34	.102	5	59.4	.55	73	.312	2	3.36	.011	.03	<.1	.09	3.6	.1	<.05	17	.6	7.5
6400N 2750E	1.2	69.2	12.5	74	.1	19.1	15.2	1066	5.01	9.1	.3	17.9	1.2	9	.1	.4	.3	108	.19	.201	4	52.3	.26	83	.201	2	3.15	.010	.03	<.1	.15	2.6	.1	<.05	14	1.0	15.0
6400N 2800E	.8	63.9	11.2	75	.1	24.8	24.2	1435	4.39	7.9	.2	10.3	1.0	12	.1	.4	.2	123	.21	.105	4	41.9	.45	76	.210	2	3.00	.010	.03	<.1	.07	2.4	.1	<.05	12	.5	15.0
6400N 2850E	.6	28.2	4.1	18	.1	9.8	6.0	118	2.22	1.6	.1	2.8	.5	14	.1	.2	.1	87	.25	.013	4	26.5	.23	17	.175	<.1	1.00	.012	.02	<.1	.05	2.1	<.1	<.05	5	<.5	15.0
6400N 2885E	.9	108.4	2.5	20	<.1	12.3	5.2	132	1.87	5.8	.7	9.1	2.1	9	<.1	.1	<.1	63	.11	.052	5	42.9	.35	9	.145	1	3.61	.009	.02	.1	.07	10.5	<.1	<.05	5	1.5	15.0
RE 6400N 2885E	.9	104.2	2.5	20	<.1	11.5	5.1	127	1.79	5.8	.7	10.1	2.2	9	.1	.2	<.1	60	.10	.051	5	41.9	.34	9	.140	1	3.54	.008	.02	.1	.08	10.3	<.1	<.05	5	1.5	15.0
6400N 2950E	1.2	470.2	5.9	79	.2	54.8	31.4	973	9.51	5.5	.3	6.4	1.4	11	.2	1.0	.1	232	.14	.081	12	103.1	1.43	48	.018	1	4.75	.007	.04	.1	.08	21.3	.1	<.05	14	.7	15.0
6400N 3000E	1.2	64.1	7.9	70	.1	27.7	20.7	876	5.05	3.2	.2	2.6	.7	26	.1	.3	.2	152	.39	.072	4	49.7	.68	59	.442	1	2.36	.009	.03	<.1	.10	2.8	.1	<.05	13	.5	15.0
6400N 3050E	.7	190.0	7.0	116	.2	51.6	33.5	3165	7.49	3.4	.2	4.2	.5	127	.2	.4	.1	186	.85	.120	4	69.0	1.57	236	.281	2	3.97	.015	.03	<.1	.13	6.0	<.1	<.05	16	.6	15.0
6400N 3100E	.9	62.7	6.2	47	<.1	28.9	15.6	449	4.97	2.3	.2	4.4	.8	21	.1	.4	.1	160	.25	.034	4	58.1	.88	68	.274	2	2.56	.011	.03	<.1	.03	3.0	.1	<.05	12	<.5	15.0
6400N 3150E	1.2	65.2	8.6	61	.1	25.3	12.6	786	4.01	3.7	.3	1.5	1.3	18	.1	.2	.2	114	.27	.079	4	41.3	.48	77	.223	3	3.99	.010	.04	.1	.10	2.8	.1	<.05	12	.5	15.0
6400N 3200E	.9	134.8	6.1	54	.1	24.0	14.3	234	3.91	3.6	.4	2.1	1.7	14	.1	.3	.1	98	.19	.044	7	38.7	.37	44	.174	1	3.49	.013	.04	.1	.05	4.8	.1	<.05	10	.6	15.0
STANDARD DS6	12.4	126.5	30.3	149	.3	25.8	10.9	731	2.94	22.2	6.8	52.0	3.2	38	6.2	3.3	5.2	58	.87	.081	15	196.4	.59	163	.079	18	1.90	.073	.16	3.5	.24	3.5	1.8	<.05	6	4.5	15.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

***APPENDIX 3***  
***FIGURES 1 - 6***



## Greenlite Ventures Inc.

### Magnolia1 Claim

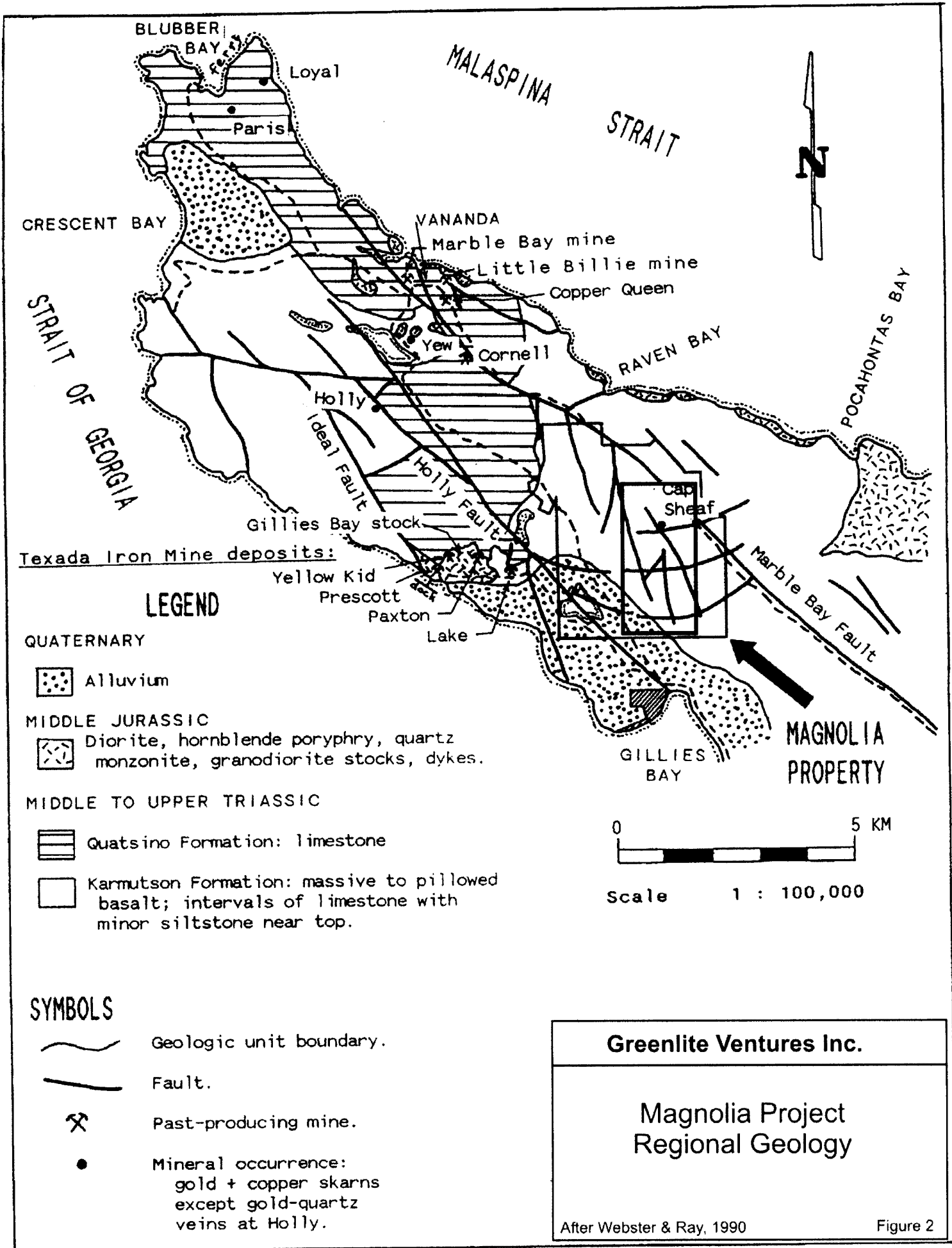
Texada Island; Nanaimo M.D., British Columbia  
NTS 092F 09W

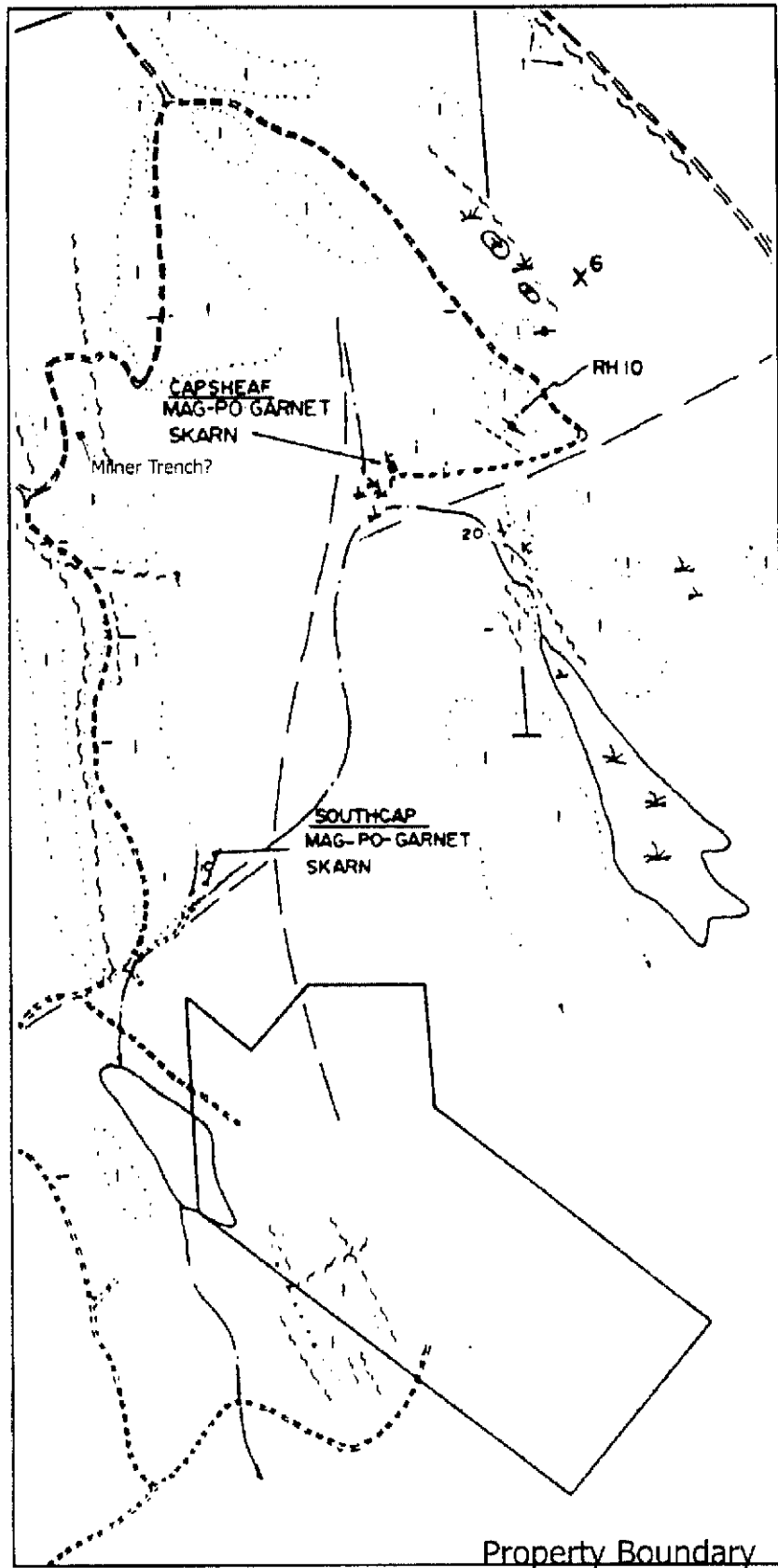
### Location and Claim Map

PSR - after BCMEMPR  
MapPlace web site

May 2003

Figure 1



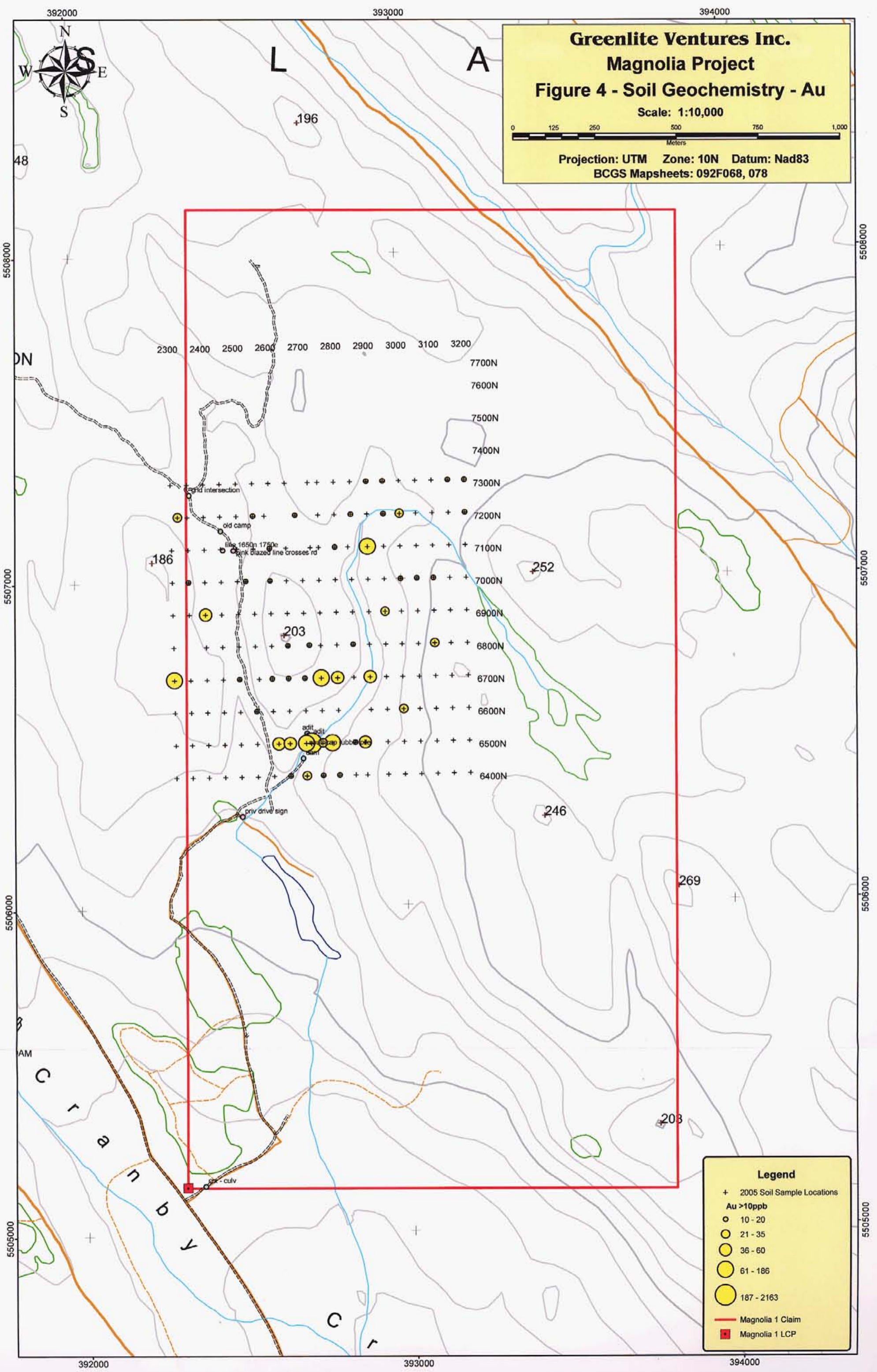


**LEGEND**

- ISLAND INTRUSIONS (JURASSIC)
- 3 DIONITE
- QUATERSD. FM. (TRIASSIC)
- 2 LIMESTONE
- KARMUTSEN FM. (TRIASSIC)
- 1a LIMESTONE INTERLAYER
- 1b MAFIC VOLCANICLASTICS
- 1c AMYGDALOIDAL BASALT
- 1 BASALT FLOWS
- ..... POWER LINE
- - - - ROAD
- ..... OUTCROP
- GEOLOGICAL CONTACT
- - - - FAULT
- LINEAMENT
- SHAFT
- x SULPHIDE SHOWING
- o- JOINT (VERTICAL)



Greenlite Ventures Inc.  
 Magnolia Claim  
 Property Geology  
 After Reynolds, 1996 Figure 3



**Greenlite Ventures Inc.**  
**Magnolia Project**  
**Figure 4 - Soil Geochemistry - Au**  
 Scale: 1:10,000  
 0 125 250 500 750 1,000  
 Meters  
 Projection: UTM Zone: 10N Datum: Nad83  
 BCGS Mapsheets: 092F068, 078

**Legend**

- + 2005 Soil Sample Locations
- Au >10ppb
- 10 - 20
- 21 - 35
- 36 - 60
- 61 - 186
- 187 - 2163
- Magnolia 1 Claim
- Magnolia 1 LCP



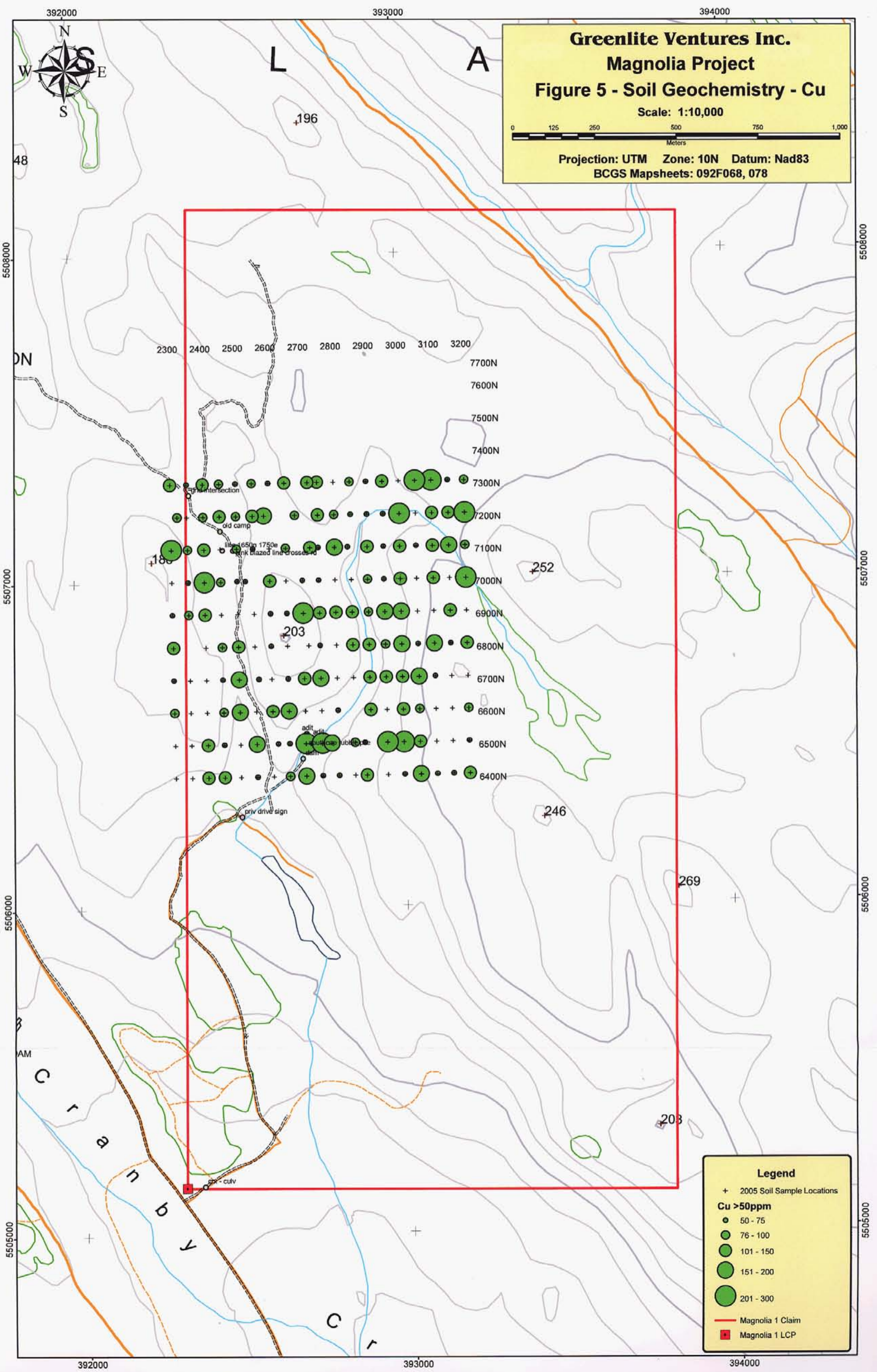
2300 2400 2500 2600 2700 2800 2900 3000 3100 3200

7700N  
7600N  
7500N  
7400N  
7300N  
7200N  
7100N  
7000N  
6900N  
6800N  
6700N  
6600N  
6500N  
6400N

old intersection  
old camp  
like 1650n 1750e  
pink blazed line crosses rd  
adit  
sub  
priv drive sign  
culv

392000 393000 394000

5505000 5506000 5507000 5508000



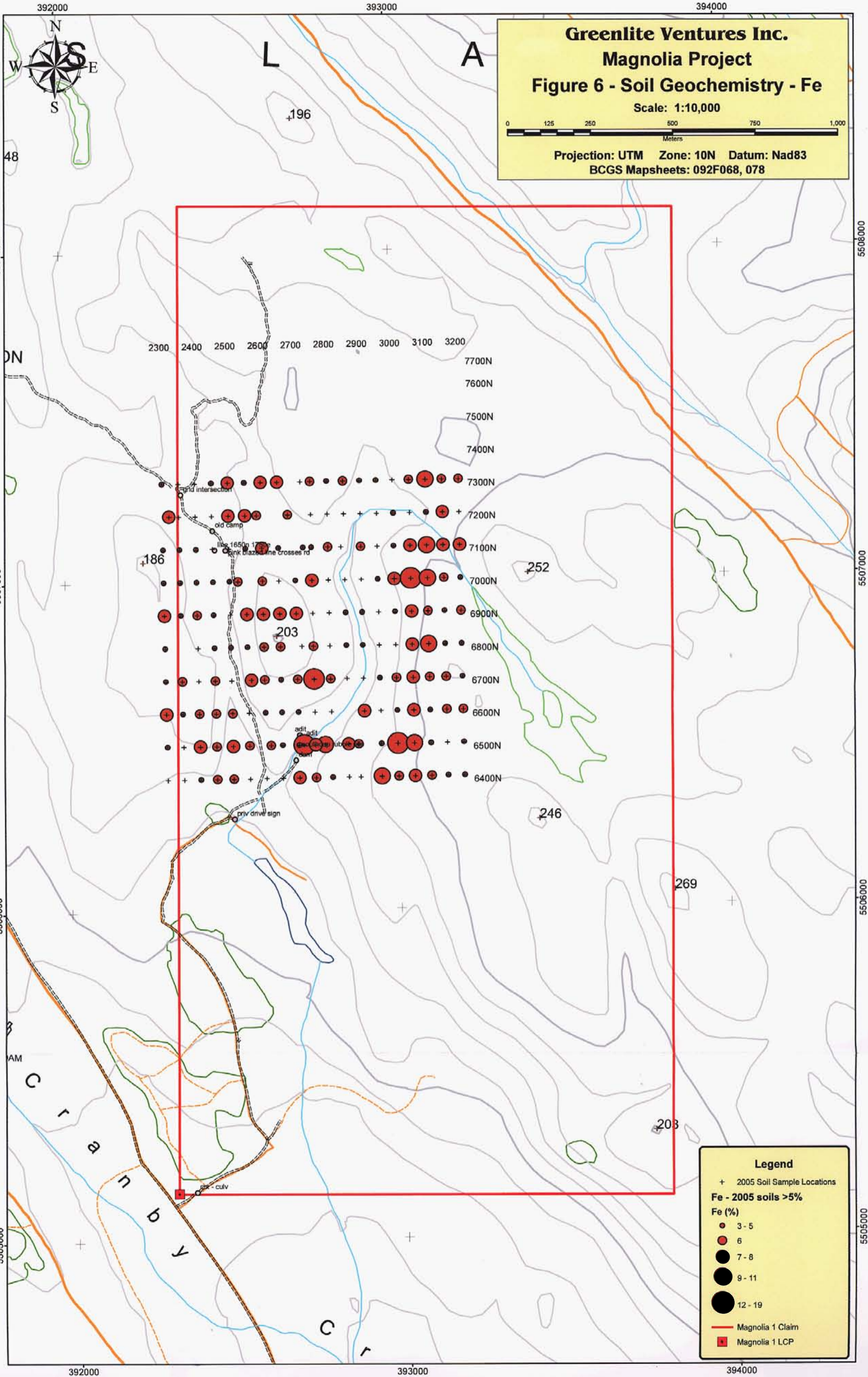
**Greenlite Ventures Inc.**  
**Magnolia Project**  
**Figure 5 - Soil Geochemistry - Cu**  
 Scale: 1:10,000

0 125 250 500 750 1,000  
 Meters

Projection: UTM Zone: 10N Datum: Nad83  
 BCGS Mapsheets: 092F068, 078

**Legend**

- + 2005 Soil Sample Locations
- Cu >50ppm**
- 50 - 75
- 76 - 100
- 101 - 150
- 151 - 200
- 201 - 300
- Magnolia 1 Claim
- Magnolia 1 LCP



**Greenlite Ventures Inc.**  
**Magnolia Project**  
**Figure 6 - Soil Geochemistry - Fe**  
 Scale: 1:10,000  
 0 125 250 500 750 1,000  
 Meters  
 Projection: UTM Zone: 10N Datum: Nad83  
 BCGS Mapsheets: 092F068, 078

**Legend**

- + 2005 Soil Sample Locations
- Fe - 2005 soils >5%
- Fe (%)
- 3 - 5
- 6
- 7 - 8
- 9 - 11
- 12 - 19
- Magnolia 1 Claim
- Magnolia 1 LCP

