

**TITLE:** TURNAGAIN NICKEL PROPERTY  
DIAMOND DRILL REPORT

**CLAIMS WORKED:** 511348, 511330

**RECORD NUMBERS:** 511348, 511330

**MINING DIVISION:** LIARD

**NTS MAP SHEET:** 104I/07W

**MINERAL TITLES  
REFERENCE MAP:** M104I 046

**LATITUDE:** 58°27' - 58°30'

**LONGITUDE:** 128°48' - 128°56'

**CLAIM OWNER:** HARD CREEK NICKEL CORP.

**OPERATOR:** HARD CREEK NICKEL CORP.

**DATE SUBMITTED:** 24 January 2006

**AUTHORS:** C. Baldys, A. Hitchins and B. Northcote

GEOLOGICAL SURVEY BRANCH  
MINING DIVISION  
DIAMOND DRILL REPORT

23,101

## TABLE OF CONTENTS

	Page
INTRODUCTION	1
PROPERTY DESCRIPTION AND ACCESS	1
PREVIOUS WORK	2
GEOLOGICAL SETTING	3
REGIONAL GEOLOGY	3
PROPERTY GEOLOGY	3
MINERALIZATION	4
2005 DIAMOND DRILL PROGRAM	5
ANALYTICAL TECHNIQUES	5
DRILL HOLE RESULTS	6
CONCLUSIONS	8
RECOMMENDATIONS	8
REFERENCES	9

### List of Figures

	Following Page
Figure 1    General Location – Turnagain Property	1
Figure 2    Claim Map – Turnagain Property	1
Figure 3    Claim Map – 1:50,000	1
Figure 4    Property Geology and Occurrences	3
Figure 5    Drill Hole Location Map	6

### Appendices

Appendix A	Claim List
Appendix B	Drill Logs
Appendix C	Assay Results and Assay Methods
Appendix D	Cost Statement
Appendix E	Statement of Qualifications

## INTRODUCTION

The Turnagain Property of Hard Creek Nickel Corp. (previously named Canadian Metals Exploration Limited) has been sporadically explored for nickel-copper-platinum-palladium mineralization since the mid-1960s. Disseminated intercumulus sulphide grains and blebs are the most widespread type of mineralization within the ultramafic suite of rocks present on the property. Occasionally, the coalescing sulphide blebs produce net-textured to locally massive sulphide intervals in dunite, wehrlite and olivine pyroxenite. Where disseminated sulphides occur in dunite or wehrlite, nickel sulphide (principally pentlandite) is commonly present in sufficient concentrations to be of economic interest, given the potential for a relatively large quantity of this disseminated mineralization.

For the past several years, Hard Creek Nickel has been conducting diamond drilling programs, focused mainly on the Horsetrail Zone, a known zone of low grade nickel mineralization north of the Turnagain River in the south eastern portion of the intrusion. This report describes the first nine holes of Hard Creek Nickel Corporation's 2005 diamond drilling program, comprising 1785.5 m of drilling.

## PROPERTY DESCRIPTION AND ACCESS

The Turnagain Property is located in the Liard Mining Division, 65 kilometres east of the community of Dease Lake and 1350 kilometres north-northwest of Vancouver (Figure 1). The property covers approximately 24,000 hectares, spread across mineral titles maps 1041 03, 1041 046, 1041 047, 1041 055 and 1041 056, and comprises 50 four-post claims and four electronically acquired claims. Claim details are summarized in Appendix A and their relative locations illustrated in Figures 2 and 3.

The property can be accessed by helicopter and fixed-wing aircraft from Dease Lake to a 700m long gravel strip, located beside the exploration camp and core storage. During the drier summer months, access via the Turnagain River-Kutcho Creek mining road from Dease Lake to the property is possible. Several drill roads provide access to portions of the property on both sides of the Turnagain River.

An exploration camp was constructed on the property in April, 2003. Prior to this date, exploration was based in the placer mining camp located at Wheaton Creek (Boulder City) some 15 km east of the property. All core drilled before late April, 2003, by previous operators and Canadian Metals, is stored at the placer camp. The majority of the core from 2003 program and all that from the 2004 and 2005 drill programs is stored in core racks beside the airstrip on the Turnagain property.

The Turnagain property covers a south-facing slope, which begins just above 1780 metres elevation and extends down to the Turnagain River at 1000 metres above sea level.

Outcrop exposure is abundant between tree line and the ridge crest but, except for approximately one percent exposure in the Horsetrail area, is poor over most of the claim block located west of the Turnagain River. Exposure is abundant on the low ridge extending east from the Turnagain River on the Pup 4 claim.

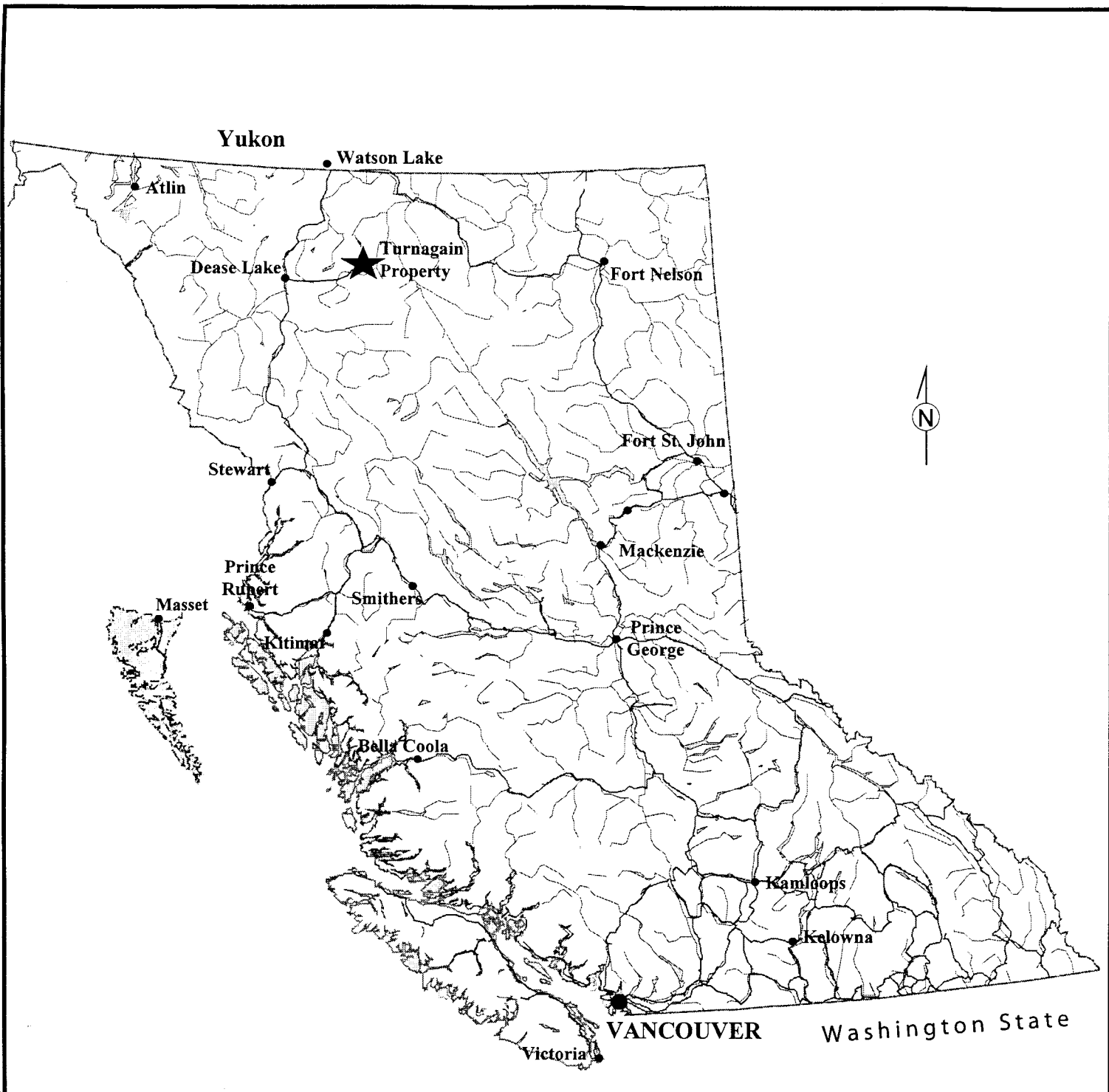
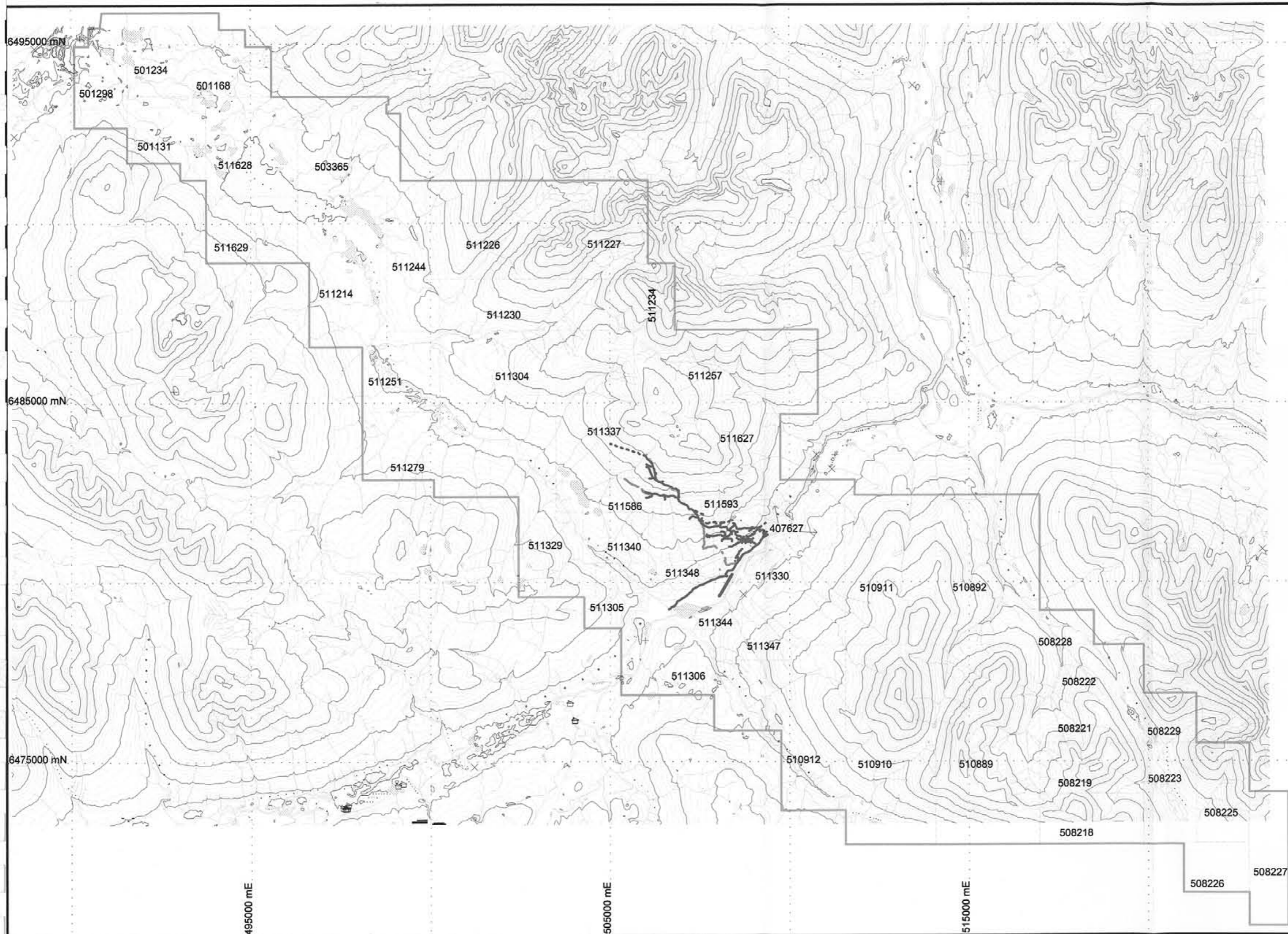


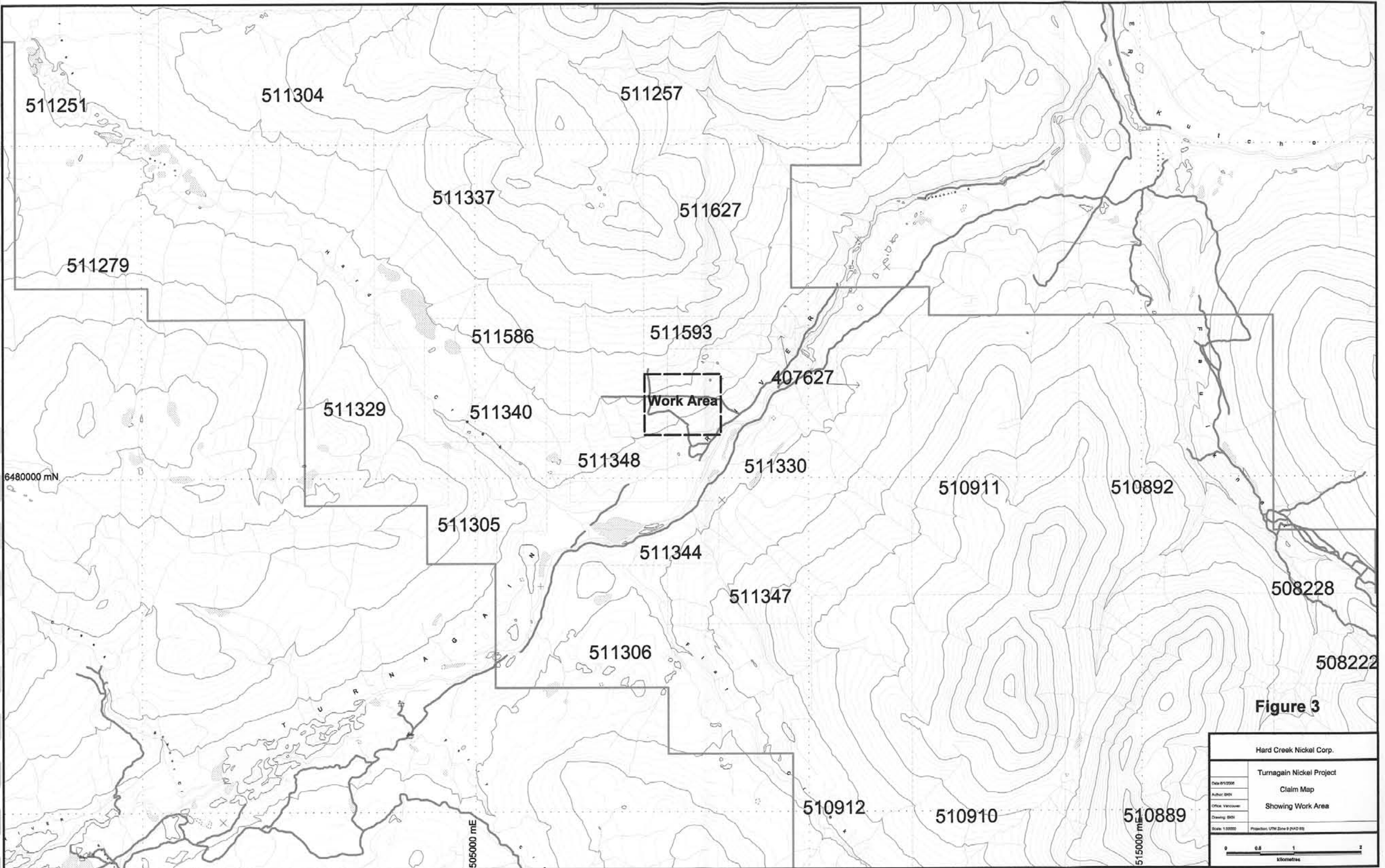
Fig. 1

<b>Hard Creek Nickel Corp.</b>	
Turnagain Nickel Project	
Liard M.D., British Columbia	
Date: 2/12/2005	<b>Location Map</b>
Author:	
Office: Vancouver	
Drawing:	
Scale: As shown	



Hard Creek Nickel Corp.	
Turnagain Nickel Project	
Claim Map, Entire Property	
Date: 02/2008	
Author: BDI	
Office: Vancouver	
Drawing: BDI	
Scale: 1:10000	Projection: UTM Zone 9 (NAD 83)





**Figure 3**

Hard Creek Nickel Corp.	
Turnagain Nickel Project	
Claim Map	
Showing Work Area	
Date: 01/2008	
Author: BWN	
Office: Vancouver	
Drawing: B01	
Scale: 1:5000	Projection: UTM Zone 9 (NAD 83)

## PREVIOUS WORK

Nickel and copper sulphides were first recognized in rusty weathering exposures of the Discovery showing on the bank of the Turnagain River in about 1956. Falconbridge Nickel Mines acquired the property in 1966 and during the next seven years completed an airborne geophysical survey, ground geophysical surveys, geological mapping, geochemical surveys, and 2895 metres of core drilling in approximately 28 widely spaced holes (McDougall and Clark, 1972, 1973). During the early 1970s, adjacent claims were investigated with a geochemical survey by Union Minière Exploration and Mining Corporation Ltd. (Burgoyne, 1971). Once the Falconbridge and UMEX claims expired, a number of the showings were restaked and tested with short, small diameter core holes. Three EX-sized core holes, totaling 55.5 m, were drilled on the west bank of the Turnagain in 1977 (Brown, 1978). No significant intersections were reported and the collars have not been located. In 1979, a single drill hole for 17 metres was located near the east bank of the Turnagain River and intersected unmineralized quartz diorite (Cukor, 1980).

By the mid-1980s, exploration interest shifted to platinum group elements. The Falconbridge core was re-sampled and a geochemical survey for platinum group elements was conducted for Equinox Resources Ltd. (Cukor, 1987; Page, 1986).

In 1996, Bren-Mar Resources Limited (predecessor to Canadian Metals Exploration Limited) optioned the Cub claim from J. Schussler and E. Hatzl. Between 1996 and 1998, Bren-Mar completed an airborne magnetic survey over 45 square kilometres, 19 core holes for 3889 metres, down-hole pulse electromagnetic survey in four of the 1997-1998 drill holes and preliminary metallurgical test work on drill core composite samples (Livgard, 1996; Downing, 1998).

Canadian Metals Exploration Limited resumed exploration in 2002 with an induced polarization and ground magnetic survey followed by 1687 metres of diamond drilling in seven holes (Downing, 2003; Woods, 2003). The 2003 exploration program emphasized diamond drilling and resulted in 23 holes, including deepening one of the 2002 holes, for a total of 8769 metres. Results from three drill holes were documented by Canadian Metals in 2004 (Baldys, Hitchins, 2004).

Hard Creek Nickel Corp. conducted a comprehensive exploration program over the claim block in 2004 (Baldys and Hitchins, 2005), including;

- 1700 line-km helicopter borne magnetic and electromagnetic survey,
- 14 line-km of detailed ground magnetometer, transient EM, and VLF surveys over the Horsetrail Zone,
- transient EM surveys in nine boreholes,
- collection of approximately 3000 soil samples,
- several lines of biogeochemical sample collection
- geological mapping of the exposed ultramafic lithology,
- 1:20,000 scale air photography and preparation of base maps,
- 7,387 metres of core drilling in 49 holes, and
- +4000 core samples analysed for 30 elements including Ni, Cu, Co, S, Pt, and Pd.

The 2005 exploration program was similarly extensive and included;

- follow-up prospecting and interpretation of geophysical targets,
- further borehole transient EM surveys in 13 holes for a total of 7400 m,
- more than 1900 fill-in soil geochemistry samples,
- continued geological mapping,
- 7144 m of diamond drilling in 37 holes
- more than 3700 core samples analysed for 30 elements including Ni, Cu, Co, S, Pt, and Pd.

## **GEOLOGICAL SETTING**

### **Regional Setting**

The Turnagain nickel property is hosted by an ultramafic complex, of mid to late Jurassic age, within Paleozoic metasedimentary and metavolcanic rocks assigned to the Road River Formation (Gabrielse, 1998) along the faulted terrane boundary between the cratonic margin and accreted terrane. Hornfelsed metasediments found within the ultramafic complex are possibly Triassic, however further work is in progress (E. Scheel, personal communication). There has been some uncertainty as to the age and origin of the Paleozoic rocks adjacent to the Turnagain ultramafic complex and Nixon (1998) has presented two interpretations. One interpretation suggests that the Paleozoic rocks are autochthonous and range in age from Cambrian to Upper Paleozoic – Triassic. An alternative interpretation, and the one favoured by Nixon, places the Turnagain ultramafic complex within an imbricated sequence of Late Paleozoic to Triassic sedimentary and volcanic rocks which were thrust eastward onto the margin of the North American craton. Support for this latter interpretation comes in part from the belief that the Turnagain ultramafic body is a zoned, Alaskan-type complex and other known examples in the northwestern Cordillera occur in accretionary terrane. Despite the differing interpretations, both place the Turnagain ultramafic body along a major terrane boundary, a geological environment similar to many of the major nickel-bearing ultramafic intrusions of the Canadian Shield.

A number of non-zoned, apparently alpine-type ultramafic bodies are exposed in rocks of the Cache Creek terrane, south and west of the Turnagain ultramafic body. Most of these are strongly serpentized and host a number of asbestos and jade occurrences.

### **Property Geology**

The property covers the known extent of a zoned, Alaskan-type ultramafic intrusion, which measures 8 kilometres by 3 kilometres and is elongate in northwest direction, conformable to the regional structural grain. The ultramafic body is in fault contact with Paleozoic, graphitic sedimentary rocks along its northern and eastern margins. The southern contact is poorly exposed, but several drill holes have penetrated the contact and intersected deformed, graphitic, phyllitic rocks in fault contact with the ultramafic sequence. Locally, the phyllitic rocks displayed a weak brownish cast, suggestive of minor thermal alteration. Within the area of the intrusion, hornfelsed metasediments of uncertain affinity show a range of stronger thermal effects.



The ultramafic complex consists of a central, well exposed dunite core and an outer zone of less exposed dunite, wehrlite, olivine pyroxenite, pyroxenite and hornblendite. Poorly exposed hornblendite and pyroxenite dominate the south western portion of the complex (Figure 4). All of these rock types and gradations between them have been interpreted as crystal cumulates (Clark, 1980; Nixon, 1998). Narrow bands and schlieren of millimetre-sized chromite crystals have been noted in dunite exposures and drill core. Phlogopite is a minor accessory mineral, but is locally conspicuous in dunite and wehrlite.

Alteration varies from weak to intense serpentinization, with several ages and colours of serpentine present. Generally serpentinization is not intense. Most of the prominent magnetic anomaly coinciding with the ultramafic body is thought to result from magnetite produced during serpentinization rather than from cumulus magnetite. Talc replacement of narrow felsic dykes, some faults and adjacent wall rock is often intense and is later than most of the serpentine alteration.

Fine-grained tremolite often occurs with serpentine alteration but does comprise the majority of some core intervals, particularly where pyroxene appears to have been present originally.

The Turnagain ultramafic body is considered an Alaskan-type intrusion for the following features (Nixon, 1998):

- orthopyroxene is lacking
- clinopyroxene compositions are diopsidic and comparable to other Alaskan-type intrusions
- ultramafic cumulates are restricted to mixtures of olivine and clinopyroxene with minor chromite, rare amphibole and trace phlogopite
- localized chromitite layers in the dunite have been remobilized to form schlieren and syndepositional folds, features that are characteristic of all Alaskan-type intrusions in British Columbia.

The Turnagain Complex is broadly zoned, but with a few local exceptions, generally lacks fine original structures such as magmatic layering.

## **MINERALIZATION**

The Turnagain ultramafic complex differs from most other Alaskan types in at least one important aspect: it hosts half a dozen known occurrences of magmatic pyrrhotite-pentlandite-chalcopyrite mineralization (Figure 4). In drill core, these sulphides generally occur as disseminated zones of intercumulus to blebby sulphides that locally coalesce to form net-textured zones of sulphides enclosing silicate grains. Sections of semi-massive to massive sulphides are occasionally in contact with overlying (?) net-textured sulphides and rarely in sharp contact with only weakly disseminated sulphides. The latter occurrences are interpreted as resulting from a squirt of liquid sulphide from a nearby, originally molten, semi-massive to massive, cumulus sulphide body. Host rock for most of the disseminated intercumulus mineralization is dark grey coloured wehrlite to dunite, usually proximal to a gradational contact between wehrlite and dunite. The higher-grade, more sulphide-rich intercepts are often adjacent to more pyroxene-rich lithologies.

Short intervals of vein or massive pyrrhotite, usually with varying amounts of veinlet-stringer chalcopyrite, massive graphite and blebby to massive magnetite, are spatially related to faults and zones of intense serpentine-tremolite alteration. These sulphide occurrences usually have a lower pentlandite/pyrrhotite ratio than primary sulphide intervals and might represent partial remobilization from nearby primary sulphides during a post-magmatic event.

## **2005 DIAMOND DRILL PROGRAM**

This report covers the first nine holes of the 2005 diamond drill program, from May 15 to August 1. DJ Drilling of Surrey, BC supplied the crews and equipment. The drill rig was a skid mounted Longyear 38 drilling NQ size core. Recoveries were generally better than 95% and down hole surveys (where conducted) and acid dip tests indicate holes generally deviate only a few metres from collar to end of hole. The 2005 targets consisted of AeroTEM conductors and potential extensions to known mineralization.

### **Analytical Techniques**

All core was split into two metre or shorter sample intervals and the bagged samples transported by helicopter and truck to Acme Laboratory in Vancouver for analyses on as many as 25 elements. Most elements were determined by ICP-emission spectrometry following four acid digestion ( $\text{HF-HClO}_4\text{-HNO}_3\text{-HCl}$ ). Sulphur was determined by the Leco furnace method. Platinum, palladium and gold were measured by ICP-ES following lead collection fire assay fusion of a 30 gm sample.

Since ICP-ES analysis for nickel and cobalt following four acid digestion, includes nickel and cobalt from both silicate minerals (mainly olivine) and also sulphide minerals, a second sample pulp was subjected to a sulphide specific digestion of ammonium citrate-hydrogen peroxide.

Nickel analyses were considered to be of exploration significance when nickel results from the four acid digestion were  $\geq 0.25$  percent and were supported by sulphur values  $\geq 0.3$  percent. Generally, when these two conditions were satisfied more than 70 percent of the total nickel occurs in sulphide minerals.

Certificates of analyses for all elements and descriptions of Acme's analytical methods are included in Appendix C.

Ten percent of the sample pulps were check analyzed at either SGS-Lakefield in Ontario or ALS Chemex in North Vancouver. Comparison of analytical results for reference standards between the three laboratories were within ten percent of accepted values.

6485000 mN

RR

### Legend

Du - Dunite  
 Wh - Wehrlite  
 Op - Olivine Pyroxenite  
 Mp/Px - Magnetite Pyroxenite/Pyroxenite  
 Hb - Hornblendite  
 Gd/Di - Granodiorite to Diorite  
 Hf - Metasediment of Uncertain Affinity  
 RR - Road River Graphitic Slate/Phyllite

★ Mineral Occurrence  
 Lithologic Contact  
 Lineament  
 Inferred Fault  
 Fault

6483000 mN

6481000 mN

505000 mE

507000 mE

509000 mE

# Kutcho Fault

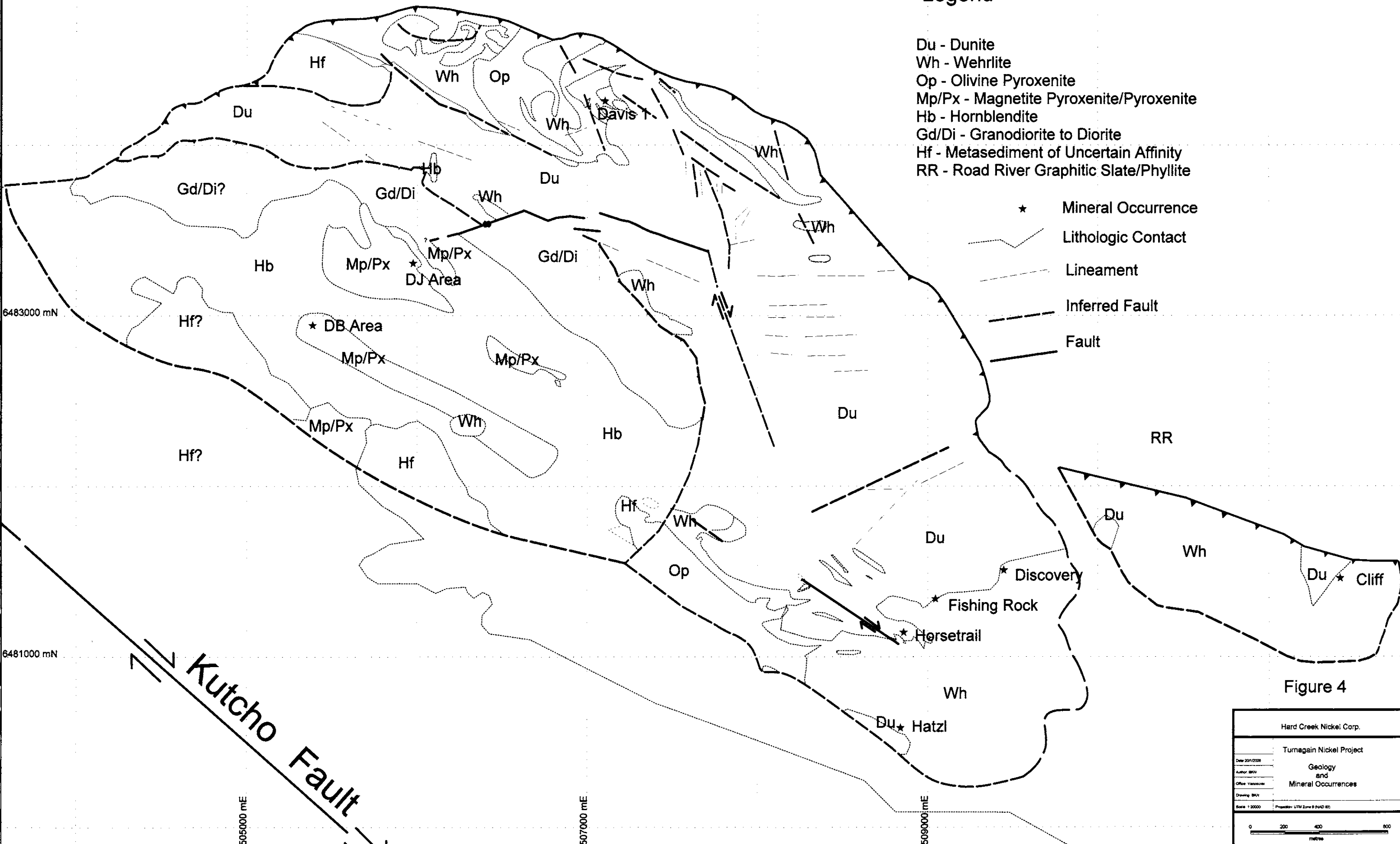


Figure 4

Hard Creek Nickel Corp.	
Turnagain Nickel Project	
Geology and Mineral Occurrences	
Date: 20/1/2008	Author: BKH
Office: Vancouver	Drawing: BKH
Scale: 1:20000	Projection: UTM Zone 9 (NAD 83)
0 200 400 800 metres	

## Drill Hole Results

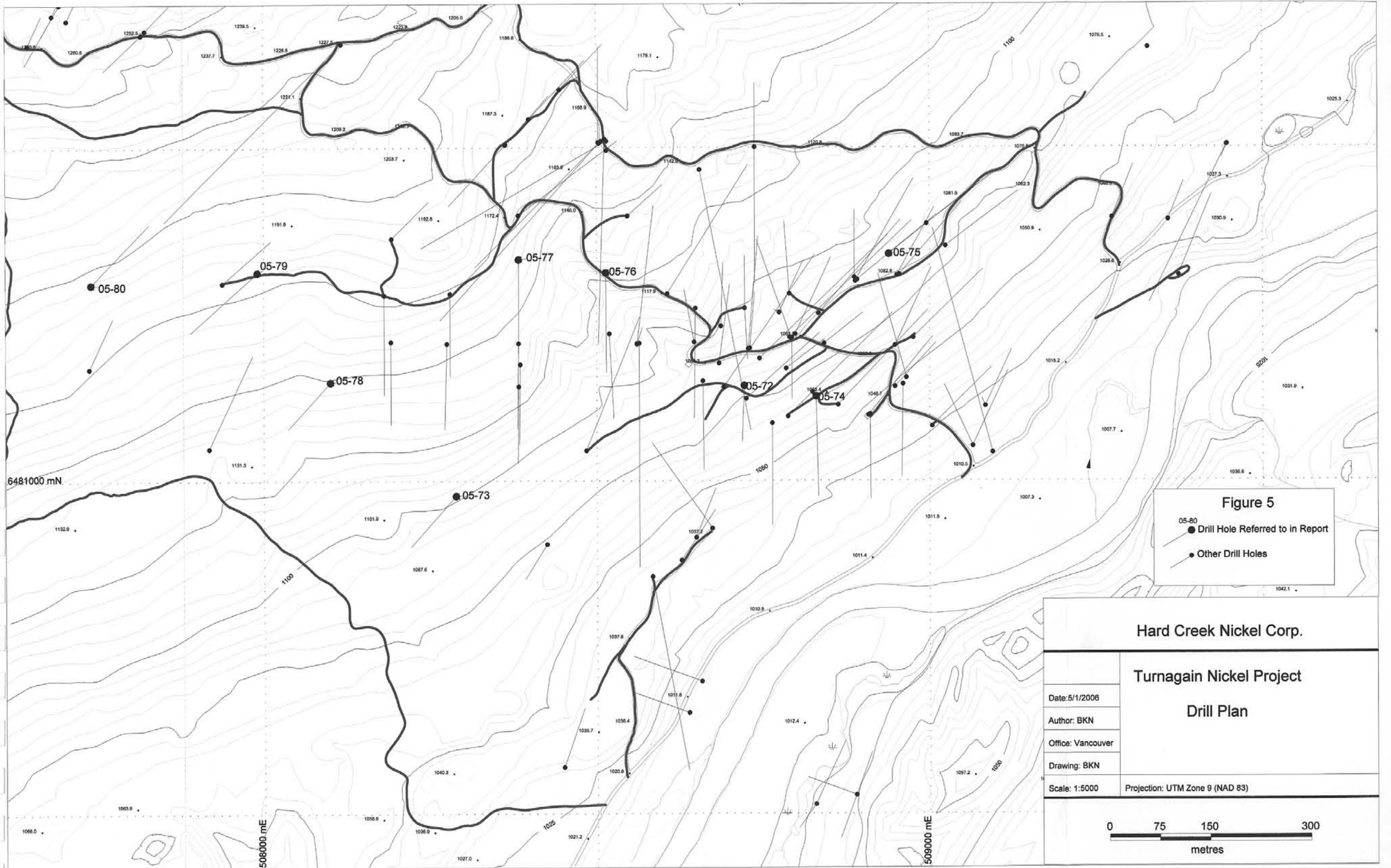
Locations are given below in UTM coordinates (Zone 9, NAD 83 datum) and also in Figure 5. Drill logs are included in Appendix B.

Hole	Northing	Easting	Elevation	Azimuth	Inclination	Depth
05-72	6481143	508722	1077	182	-63	186.4 m
05-73	6480977	508288	1101	222	-48	152.4 m
05-74	6481127	508829	1067	179	-50	223.8 m
05-75	6481340	508939	1088	51.55	-50	217.6 m
05-76	6481312	508514	1125	180	-48	223.7 m
05-77	6481332	508383	1163	180	-51	223.7 m
05-78	6481148	508100	1148	222	-50	147.5 m
05-79	6481313	507990	1180	228	-52	211.3 m
05-80	6481296	507741	1196	44	-51	199.4 m

Hole 05-72 was designed to test the Horsetrail zone south of hole 04-71, which encountered mineralization and a downhole EM conductor. 05-72 intersected dunite and wehrlite to approximately 140 m and from 140 the lithology is dominated by olivine clinopyroxenite and pyroxenite. Much of the dunite and wehrlite are serpentinized. A serpentinized, locally graphitic zone was encountered from 68.5 to 74.7 m. Low grade sulfide is present near surface to 36.4 m with stronger sulfide mineralization from 88 to 179.5 m. Analyses return ammonium citrate nickel values above 0.1% from 7 m to 145 m, below which they decline in the pyroxene-rich rocks.

Hole 05-73 was designed to intersect an EM conductor identified by the 2004 airborne survey. The lithology encountered was primarily olivine pyroxenite with intervals of wehrlite. Graphitic zones between 19 and 26 m are presumed to be the conductors. Much of the core is strongly mineralized with sulfide, however it is dominated by pyrrhotite with only sparse pentlandite. Both total and ammonium citrate nickel analyses are erratic, confirming discontinuous nickel sulfide mineralization.

Hole 05-74 was designed to test the southern extent of the Horsetrail zone and intersect EM conductors detected by both downhole and airborne surveys. Lithology is dominated by wehrlite and borderline dunite-wehrlite, with shorter intervals of clinopyroxenite and olivine clinopyroxenite until approximately 183 m, below which the pyroxenites predominate. The majority of the core from near surface to 197 m is mineralized with disseminated sulfide. Ammonium citrate nickel is generally over 0.1% above 197m downhole depth with higher intervals, notably 141-166 m which returned values above 0.25%. Graphitic zones from 29.3 to 46m and from 197.4 to 223.7 m are presumed to be the conductors detected by the EM surveys.



**Figure 5**  
 ● Drill Hole Referred to in Report  
 ● Other Drill Holes

<b>Hard Creek Nickel Corp.</b>	
<b>Turnagain Nickel Project</b>	
<b>Drill Plan</b>	
Date: 5/1/2006	
Author: BKN	
Office: Vancouver	
Drawing: BKN	
Scale: 1:5000	Projection: UTM Zone 9 (NAD 83)



Hole 05-75 was designed as a step in hole to test for a near surface extension of mineralization encountered in hole 03-18, northeast of the Horsetrail zone. This hole intersected a number of dykes and shear zones near the surface, with dunite, wehrlite, olivine clinopyroxenite lithologies. Below 74 m the core is mainly dunite, cut by diorite dykes. Sulfides are finely disseminated in the dunite. Ammonium citrate analyses reveal weak nickel sulfide mineralization in the ultramafics (generally between 0.1 and 0.2%)

Hole 05-76 was a step-in from 02-06, testing near surface inferred resource in the western part of the Horsetrail zone. Lithology encountered was primarily dunite, with the hole ending in 34 m of wehrlite. Low grade disseminated sulfide zones containing pentlandite were identified from 39 to 56.1 m and from 112-145.7 m. Nearly all samples returned ammonium citrate nickel values above 0.1% with the exception of a dyke. Several intervals average above 0.25% ammonium citrate nickel, notably 126-161 m.

05-77 was intended to test the near-surface resource west of 02-06 in the western Horsetrail zone or eastern Silesia zone. Lithology was mostly dunite with 70 m of wehrlite from 82.7 m to 153 m, ending in wehrlite and clinopyroxenite. Dunite was unmineralized or very weakly mineralized near surface, but ammonium citrate nickel is generally above 0.1% below 100 m, with several short intervals above 0.25%, including the last 6 m.

Hole 05-78 was designed to intersect an AeroTEM conductor, part of a series of conductors also intersected by 05-73 farther southeast, along strike. Lithology was dominated by olivine clinopyroxenite and clinopyroxenite. No significant nickel mineralization was encountered, although there were pyrrhotite-rich intervals, some with minor graphite. Those at 56.4 to 60 m and at 68 m were probably responsible for the airborne-detected conductor. Platinum and palladium were elevated in these sulfide rich intervals, approximately 1:1, but not reaching levels of economic interest.

Hole 05-79 was designed to test the same series of AeroTEM conductors as 05-73 and 05-78, farther northwest along strike. In this case the conductor coincided with a strong nickel soil geochemical anomaly. Apart from a short interval of wehrlite near the top of the hole, the rock was mainly clinopyroxenite and olivine clinopyroxenite. Nickel sulfide mineralization was only marginally better than 05-78, with a short interval from 16.0 to 18.0 m returning ammonium citrate nickel results averaging over 0.2%. Pyrrhotite was locally strong, with and without graphite. Again, intervals of elevated Pt+Pd were intersected, but these did not reach economic concentrations.

Hole 05-80 tested three AeroTEM conductors northwest of those tested by 05-73, 78 and 79. There is a gap in the line of conductors between 05-79 and 05-80. The lithologies intersected were primarily dunite and wehrlite, with intervals of olivine pyroxenite. A sulfide rich interval from 15 to 53 m contains some net textured sulfide and probably accounts for the southern conductor. Graphite + pyrrhotite in olivine pyroxenite are presumed to account for the northern conductors. Nearly all of the core returned ammonium citrate nickel values of 0.1% or better, with short intervals above 0.25%.

## CONCLUSIONS

Holes 72, 74, 75, 76, 77 and 80 all intersected nickel sulfide zones of economic interest. With additional subsequent drilling 72 and 74 may help extend the Horsetrail resource to the south, whereas 76 and 77 better define the western Horsetrail extension. Hole 05-75 intersected a number of dykes and failed to intersect the high grade mineralization hoped for, but low grade nickel sulfide is present in the ultramafic portions of the hole.

Results in holes 73, 78 and 79 were disappointing, but they appear to define a southwestern limit to the style of finely disseminated nickel mineralization found in dunite and wehrlite of the Horsetrail and Silesia areas. This limit is coincident with what appears to be a northwest-southeast oriented pyroxenite-dominated zone, as defined by drilling and sparse outcrop. While sulfide is often abundant in these rocks, it is typically nearly all pyrrhotite and nickel values are erratic and generally very low overall, unless near a contact with a more olivine-rich rock type.

Strong AeroTEM-identified conductors in pyroxene rich rocks have in most cases so far turned out to be zones of massive or semimassive graphite and/or pyrrhotite. However, there may be some spatial association with more economically interesting disseminated mineralization where these zones occur near nickeliferous olivine rich rock bodies.

## RECOMMENDATIONS

The first part of the 2005 program has succeeded in extending the mineralization of the Horsetrail zone to the south. Further drilling has already continued to test the boundaries of mineralization to the south and west, and ultimately the entire perimeter of known mineralization should be tested for local extensions. A program of grid drilling on 200 m centres is planned for 2006. Ideally, this and infill drilling on 100m spacings will broadly define the limits of mineralization and aid in better defining the nature of geologic controls on mineralization.

## REFERENCES

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**Appendix A  
Claims List**

<b>Tenure No.</b>	<b>Claim Name</b>	<b>Area (ha.)</b>	<b>Issue Date</b>	<b>New Good To Date</b>
501234	Drift 3	421.73	2005/Jan/12	2008/Jan/12
501131	Drift 1	421.97	2005/Jan/12	2008/Jan/12
501298	Drift 4	421.79	2005/Jan/12	2008/Jan/12
501168	Drift 2	421.76	2005/Jan/12	2008/Jan/12
508218	Dinah 1	407.2	2005/Mar/03	2009/Mar/03
508219	Dinah 2	407.05	2005/Mar/03	2009/Mar/03
508221	Dinah 3	406.86	2005/Mar/03	2009/Mar/03
508222	Dinah 4	406.7	2005/Mar/03	2009/Mar/03
508223	Dinah 5	407.1	2005/Mar/03	2009/Mar/03
508225	Dinah 6	407.1	2005/Mar/03	2009/Mar/03
508226	Dinah 7	254.58	2005/Mar/03	2009/Mar/03
508227	Dinah 8	407.3	2005/Mar/03	2009/Mar/03
508228	Dinah 9	135.53	2005/Mar/03	2009/Mar/03
508229	Dinah 10	203.4	2005/Mar/03	2009/Mar/03
511214		979.88	2005/Apr/20	2009/Feb/18
511244		489.92	2005/Apr/20	2009/Feb/18
511251		473.41	2005/Apr/20	2009/Feb/17
511279		896.69	2005/Apr/20	2009/Feb/17
511629		472.92	2005/Apr/25	2009/Feb/18
511628		708.95	2005/Apr/25	2009/Feb/18
503365		793.35	2005/Jan/14	2009/Feb/18
511226		1216.08	2005/Apr/20	2009/Feb/18
511230		760.47	2005/Apr/20	2009/Feb/17
511227		506.71	2005/Apr/20	2009/Feb/17
511234		185.89	2005/Apr/20	2009/Feb/16
511257		1014.44	2005/Apr/20	2009/Feb/17
510912		779.89	2005/Apr/18	2010/Apr/07
510910		1424.28	2005/Apr/18	2010/Apr/07
510911		1066.87	2005/Apr/18	2010/Apr/07
510889		1627.86	2005/Apr/18	2010/Apr/07
510892		1219.26	2005/Apr/18	2010/Apr/07
511304		1149.68	2005/Apr/21	2010/Feb/17
511329		1015.36	2005/Apr/21	2010/Sep/27
511305		270.96	2005/Apr/21	2010/Sep/27
511340		253.92	2005/Apr/21	2015/Dec/01
511337		1065.75	2005/Apr/21	2015/Dec/01
511627		592.12	2005/Apr/25	2015/Dec/01
511348		389.39	2005/Apr/21	2015/Dec/01
511330		592.59	2005/Apr/21	2015/Dec/01
511344		271	2005/Apr/21	2013/Feb/19
511306		881.17	2005/Apr/21	2013/Feb/19
511347		474.34	2005/Apr/21	2013/Apr/07
511586		236.94	2005/Apr/25	2016/Jan/01
511593		101.55	2005/Apr/25	2016/Jan/01
407627	Pup 4	500	2004/Jan/01	2016/Jan/01

New expiry dates are conditional upon acceptance of this assessment report.

**APPENDIX B**

**DRILL LOGS**





**DDH 05-72**



SAMPLE DATA				SULPHIDES						SIL	MINERALOGY (W/M/I)							DESCRIPTION			
From	To	Sample No.	QC (S, D or B)	% magmatic sulphide	% non-magm sulphide	% TOTAL sulphide	pentlandite	chalcopyrite	other (mack, hz, gd, mi, mo)	dominant (ol, cpx, hb, ...)	black serpentine	other serpentine	talc	magnetite vn-nnlet	chromite	graphite	CaCO2	colour code	Rock type	Dominant Alteration (sp, tl, cs, hbbx....alt? )	Structure: c,b,f,sh,ft / Angle to C/A
49.70	53.40			0.1	15	15.1	0	0	0	sp	W	I	I	I	N	I		shSP			
49.70	51.70	267027																			
51.70	53.40	267028																			
53.40	56.70			0	0.1	0.1	0	0	0	sp	W	I	I	M	N	N		SP	sp-tl	f/15	
53.40	55.40	267029																			
55.40	56.70	267030	D																		
56.70	61.80			0.7	0	0.7	0.05	0	0	ol	W	N	N	W	N	N		Wh		C/-1	
56.70	58.70	267031																			
58.70	60.70	267032																			
60.70	61.80	267033																			
61.80	68.50			1.5	1.0	2.5	0	0	0	sp	W	M	W	W	N	N		spWh	sp		
61.80	63.80	267034																			
63.80	65.80	267035																			
65.80	67.00	267036																			
67.00	68.50	267037																			
68.50	74.70			0	5.0	5.0	0	0.1	0	sp	N	I	M	W	N	M		SP	sp=mgs	f/20	
68.50	70.50	267038																			
70.50	72.50	267039																			
blank		267040	B																		
72.50	73.50	267041																			
73.50	74.70	267042																			
74.70	82.40			3.0	2.0	5.0	0	0.1	0	sp	N	I	M	W	N	N		spDu	sp	C/-1	
74.70	76.70	267043																			
76.70	78.70	267044																			
78.70	80.70	267045																			
80.70	82.40	267046																			
82.40	85.60			0.5	6	6.5	0	0.1	0	sp	N	I	M	W	N	N		SP	sp	f/20	
82.40	84.40	267047																			
84.40	85.60	267048																			
85.60	86.00			0	0	0	0	0	0	sp	N	I	I	N	N	N		C		C/-1	
85.60	86.00	267049																			
UM-2		267050	S																		
86.00	88.00			0	0	0	0	0	0	sp	N	I	I	N	N	N		FLT		flt	
86.00	88.00	267051																			
88.00	106.70			5	0	5	0.3	0	0	ol	M	W	W	M	N	N		spWh		f/35	









**DDH 05-73**



SAMPLE DATA				SULPHIDE SUMMARY					MINERALOGY & DESCRIPTION										DESCRIPTION				
From	To	Sample No.	QC (S, D or B)	% Magmatic Sulphide	% Magmatic pentlandite	% Magmatic chalcopyrite	% Remobilized Sulphide	% TOTAL Sulphide	pyroxene black serpentine	late serpentine	talc	tremolite	biotite	hornblende	chromite	magnetite habit	graphite	colour code	Rock type	Alteration	Structure Angle to C/A	Description	
38.00	40.00	267132																					
40.00	42.00	267133																					
42.00	44.00	267134																					
44.00	46.00	267135																					
45.60	47.80						7	7	50	W/M	W	W	M	W		DV	M/S		oPxWh	talc chlor	crushed		
46.00	48.00	267136																					
47.80	48.40						tr	tr													FLT		
48.00	50.00	267137																					
48.40	56.00			tr	tr			tr	20	M	W	M	W	tr		V		WhoPx			strg frx		
50.00	52.00	267138																					
52.00	54.00	267139																					
54.00	56.00	267140																					
56.00	58.00	267141																					
56.00	65.00			1	tr	tr	tr	1-2	20?	M			W/M			V/D		WhoPx			competent		
58.00	60.00	267142																					
60.00	62.00	267143																					
62.00	64.00	267144																					
64.00	66.00	267145																					
65.00	72.30			1-2		tr	1	3	25	S	tr		M	tr		V		Wh	blk srp trem		strg frx		
66.00	68.00	267146																					
68.00	70.00	267147																					
70.00	72.00	267148																					
72.00	74.00	267149																					
72.30	86.20			1	tr		tr	1-2	20	S			M					Wh	blk srp trem		mod strong frx		
UM-4		267150	S																				
74.00	76.00	267151																					
76.00	78.00	267152																					
78.00	80.00	267153																					
80.00	82.00	267154																					
82.00	84.00	267155																					
84.00	86.00	267156																					
86.00	88.00	267157																					
86.20	92.70			tr			1	1-2	50	W	tr	tr	M	M			tr		oPx	trem biot	mod frx		





**DDH 05-74**





SAMPLE DATA				SULPHIDES						SIL	MINERALOGY (W/M/I)							DESCRIPTION					
From	To	Sample No.	QC (S, D or B)	% magmatic sulphide	% non-magm sulphide	% TOTAL sulphide	pentlandite	chalcopyrite	other (mack, hz, gd, m, i, mo)	dominant (ol, cpx, hb, ...)	black serpentine	other serpentine	talc	secondary magnetit	chromite	graphite	tremolite	calcite	colour code	Rock type	Dominant Alteration (sp, tl, cs, hbbx...alt ?)	Structure: c,b,f,sh,ft / Angle to C/A	
44.00	45.00	267216																					
45.00	46.00			0.0	5.0	5.0	0.00	0	0.0	sp	N	I	W	N	N	M				SP	sp	C/-1	
45.00	46.00	267217																					
46.00	47.90			1.0	0.0	1.0	0.00	0	0.0	cpx	N	N	N	N	N	N				cPx?	cs?	C/-1	
46.00	47.90	267218																					
47.90	49.50			15.0	0.0	15.0	0.00	0	0.0	cpx	N	N	N	N	N	N				cPx?	cs?	C/-1	
47.90	49.50	267219																					
49.50	51.40			4.0	0.0	4.0	0.30	0	?	cpx	N	N	N	W	N	N				cPx		C/-1	
49.50	51.40	267220	D																				
51.40	56.00			15.0	0.0	15.0	1.50	0	?	cpx	N	N	N	W	N	N				cPx		C/-1	
51.40	53.00	267221																					
53.00	55.00	267222																					
55.00	56.00	267223																					
56.00	64.40			3.0	1.0	4.0	0.10	0	0.0	cPx	W	W	W	W	N	N		loc I		cPx	loc CS	loc sh C/-1	
56.00	58.00	267224																					
UM-2		267225	S																				
58.00	60.00	267226																					
60.00	62.00	267227																					
62.00	63.00	267228																					
63.00	64.40	267229																					
64.40	66.80			0.0	5.0	5.0	0.00	0	0.0	dp	N	N	N	N	N	N				CS	cs	C/-1	
64.40	65.50	267230																					
65.50	66.80	267231																					
66.80	72.20			0.5	0.1	0.6	0.00	0	0.0	cpx	N	W	W	N	N	N				cPx	sp-tr? Cs	loc sh	
66.80	68.80	267232																					
68.80	70.80	267233																					
70.80	71.50	267234																					
71.50	72.20	267235																					
72.20	76.90			0.8	0.0	0.8	0.05	0	0.0	ol	M	N	N	M	N	N				Du	sp	C/-1	
72.20	74.00	267236																					
74.00	75.00	267237																					
75.00	76.90	267238																					
76.90	83.00			4.5	1.0	5.5	0.30	0	0.0	ol	I	N	W	I	N	N				spDu	sp	f/10-15	









**DDH 05-75**











**DDH 05-76**











**DDH 05-77**











**DDH 05-78**

SAMPLE DATA			SULPHIDES						SIL	MINERALOGY (W/M/I)						DESCRIPTION				
From	To	Sample No.	QC (S, D or B)	% magmatic sulphide	% non-magm sulphide	% TOTAL sulphide	pentlandite	chalcopyrite	other (mack, hz, g d, mi, mo)	dominant (ol, cpx, hb, ....)	black serpentine	other serpentine	talc	magnetite	chromite	graphite	colour code	Rock type	Dominant Alteration (sp, tl, cs, hbbx....alt?)	Structure: c,b,f,sh,ft / Angle to C/A
0.00	7.00																	Ob		
7.00	15.50																	Ob		
15.50	17.50	267679																		
17.50	19.50	267680																		
19.50	21.50	267681																		
21.50	23.00	267682																		
23.00	25.00	267683																		
25.00	27.00	267684																		
15.50	27.10			1		1		tr		px	W	W	W-M	D		tr		ocPx	trem/serp	
27.00	28.40	267685																		
27.10	28.40					tr?				px	W	W	W					FLT		
28.40	30.50	267686																		
30.50	32.50	267687																		
32.50	34.20	267688																		
34.20	36.20	267689																		
		267690	B																	
36.20	38.00	267691																		
38.00	40.00	267692																		
28.40	34.20			1		1		tr		px	W	tr	W	D				ocPx	blk/serp	mod frdx
40.00	42.00	267693																		
42.00	44.00	267694																		
44.00	46.00	267695																	Dk	Dk 85
46.00		267696																		
34.20	40.80			2	tr+	2		tr		px	W	tr	W	D				ocPx		frx 40-70
48.00	50.00	267697																		
50.00	52.00	267698																		
52.00	54.00	267699																		
		267700	S																	
54.00	56.00	267701																		
56.00	58.00	267702																		
40.80	56.40			1-2	tr+	2		tr		px	W	tr	W					cPx		loc f
58.00	60.00	267702A																		
56.40	60.10			5	2	7		0.1			W-M		tr	D	tr			Wh	blk sep	C
60.00	62.00	267703																		
60.10	66.60			0.05	tr	0.05		tr		cPx	W	tr	W	D	W			cPx		







**DDH 05-79**



SAMPLE DATA				SULPHIDES						SIL	MINERALOGY (W/M/I)						DESCRIPTION			
From	To	Sample No.	QC (S, D or B)	% magmatic sulphide	% non-magm sulphide	% TOTAL sulphide	pentlandite	chalcopyrite	other (mack, h z, gd, ml, mo)	dominant (ol, cpx, hb, ...)	black serpentine	other serpentine	talc	magnetite	chromite	graphite	colour code	Rock type	Dominant Alteration (sp, tl, cs, hbbx....alt?)	Structure: c,b,f,sh,ft / Angle to C/A
96.00	103.20			5	5	10	<0.5	tr		p	W/M	tr	tr	P		M				
55.00	57.00	267776																		
57.00	58.70	267777																		
58.70	60.80	267778																		
60.80	63.00	267779																		
blank		267780	B																	
63.00	65.00	267781																		
65.00	67.00	267782																		
67.00	69.10	267783																		
69.10	71.20	267784																		
71.20	73.15	267785																		
73.15	75.00	267786																		
75.00	77.00	267787																		
77.00	79.00	267788																		
79.00	81.15	267789																		
81.15	83.00	267790																		
83.00	84.90	267791																		
84.90	87.00	267792																		
87.00	89.00	267793																		
89.00	91.00	267794																		
91.00	92.60	267795																		
92.60	94.60	267796																		
94.60	96.60	267797																		
96.60	98.60	267798																		
98.60	100.60	267799																		
UM-2		267800	S																	
100.60	102.60	267801																		
102.60	104.60	267802																		
103.20	110.20			<1	tr	<1		tr		Px	W	tr	tr				ocPx		wk fr	
104.60	106.60	267803																		
105.70	113.90			2	0.5	2	tr	0	0	90%	W	N	W	M	N	N	gy	cPx		f/45
106.60	108.50	267804																		
108.50	110.50	267805																		
110.50	112.50	267806																		
112.50	114.50	267807																		
113.90	125.30			3	0	3	tr	tr	0	90%	2	N	W	M	N	W	dk	cPx	bk sp	C/-1





**DDH 05-80**







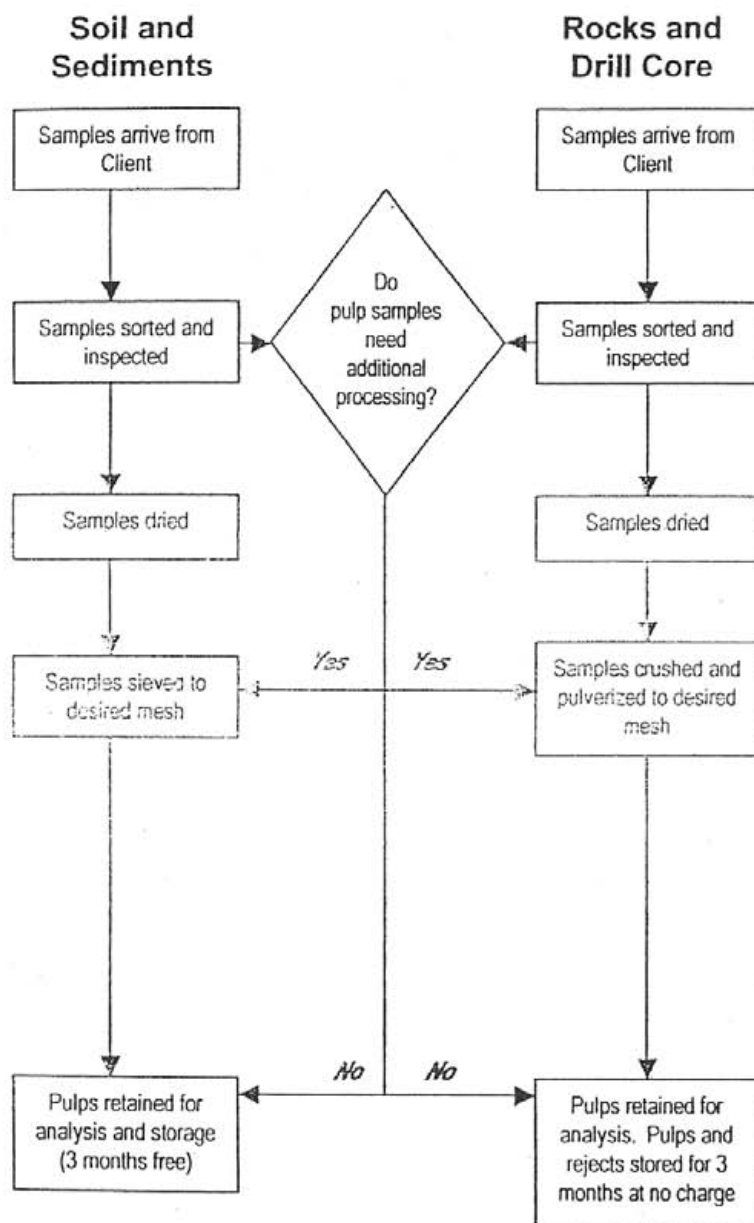
SAMPLE DATA				SULPHIDES						SIL	MINERALOGY (W/M/I)								DESCRIPTION			
From	To	Sample No.	QC (S, D or B)	% magmatic sulphide	% non-magm sulphide	% TOTAL sulphide	pentlandite	chalcopyrite	other (mack, hz, gd, mi, mo)	dominant (ol, cpx, hb, ...)	black serpentine	other serpentine	talca	magnetite	chromite	graphite	trem	biotite	colour code	Rock type	Dominant Alteration (sp, tl, cs, hbbx...alt ?)	Structure: c,b,f,sh,ft / Angle to C/A
107.00	109.00	267916																				
109.00	111.00	267917																				
111.00	113.00	267918																				
112.20	122.00			.05						ol/sp	S	W	W	D/V						Wh		C
113.00	115.00	267919																				
115.00	117.00	267920																				
117.00	119.00	267921																				
119.00	121.00	267922																				
119.00	119.60																			Dk		
121.00	123.00	267923																				
122.00	133.10			tr		tr				ol/(sp)	M	W	tr	V/D						WhocPx		
123.00	124.50	267924																				
124.50	126.50	267926																				
124.50	125.30																			Dk		
126.50	129.00	267927																				
129.00	131.00	267928																				
131.00	133.00	267929																				
131.15	133.10																			Dk		
133.00	135.00	267931																				
133.10	141.30																			WhDu		
134.30	134.50			tr+																Dk		
135.00	137.00	267932																				
137.00	139.00	267933																				
139.00	141.00	267934																				
141.00	143.00	267935																				
141.30	145.00			.05						ol/(sp)	M	W	tr	D						WhocPx	blk serp wk trem	
143.00	145.00	267936																				
145.00	147.00	267937																				
145.00	149.00			2		2	tr			Px	W	tr	tr	D			W			ocPx	blk serp wk frx	
147.00	149.00	267938																				
149.00	151.00	267939																				
149.00	161.00			.05	2	3	tr	tr		Px/ol	W	W	M	V		loc S	S	W		ocPx	frx loc b	



**APPENDIX C**  
**ANALYTICAL METHODS AND RESULTS**



## General Sample Preparation Methods



### Comments

**Receiving:** Samples arrive via courier, post or by client drop-off; shipment inspected for completeness.

**Sorting and Inspection:** Samples sorted and inspected for quality of use (quantity and condition). Rock and Drill Core samples inspected for mineralisation (colour and % sulphides, metal oxides or carbonates). Pulp samples inspected for homogeneity and fineness. Coarse pulps are screened or pulverized after getting client's approval.

**Drying:** Wet or damp samples are dried at 60°C (40°C if specified by the client).

**Sieving:** Soil and sediment sieved to -80 mesh ASTM (-177 microns) unless client specifies otherwise. Sieve cleaned by brush and compressed air between samples. Reference material G-1 (pulp made of granite blank) is carried as first sample in sequence (sieve>weigh>digest>analyse) to monitor background noise.

**Crushing and Pulverizing:** Rock and Drill Core crushed to 70% passing 10 mesh (2 mm), homogenized, riffle split (250 g subsample) and pulverized to 95% passing 150 mesh (100 microns). Crusher and pulverizer cleaned by brush and compressed air between routine samples. Silica wash scours equipment after high-grade samples, between changes in rock colour and at end of each file. Silica is crushed and pulverized as first sample in sequence and carried through to analysis to monitor background noise.

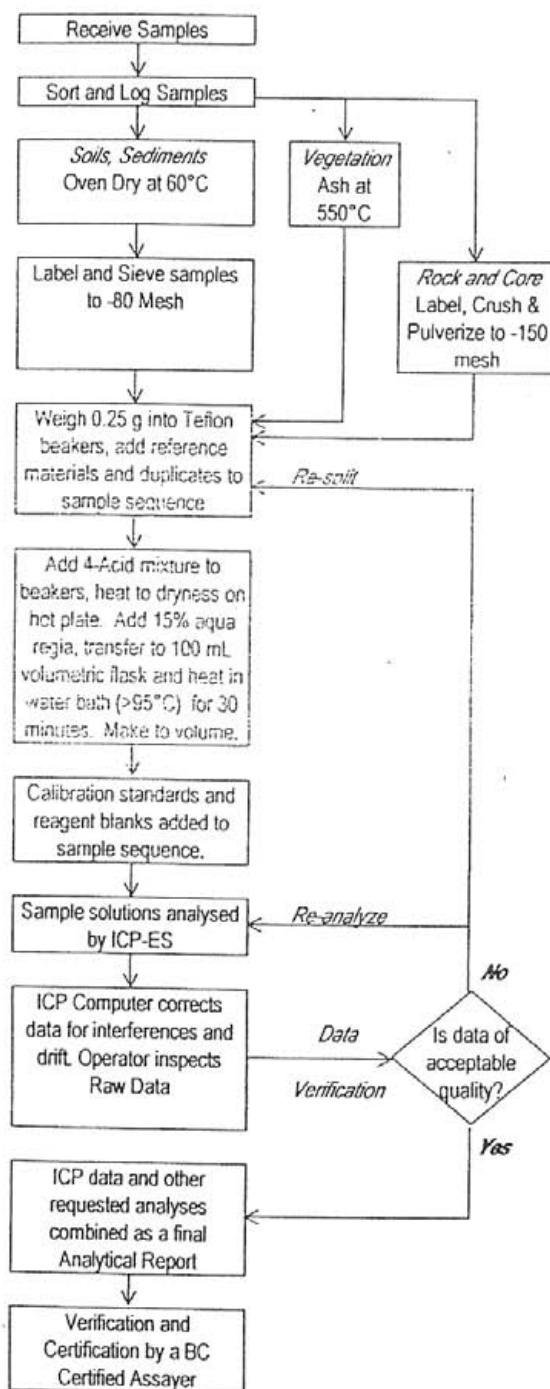
**Compositing:** Equal weights of crushed, pulverized or sieved material from 2 or more samples are combined and pulverized for 60+ seconds to produce a homogeneous mixture.

**Storage:** Pulp samples (up to 100g for soils or sediments and up to 250 g for rock and drill core) are archived for 3 months at no cost. Soil and sediment rejects are discarded immediately. Rock and drill core rejects are stored for 3 months at no charge. Client may request additional storage, return or disposal of pulps and rejects after initial free-storage period.



## METHODS AND SPECIFICATIONS FOR ANALYTICAL PACKAGE GROUP 7TD – MULTI-ELEMENT ASSAY BY ICP-ES • TOTAL DIGESTION

### Analytical Process



### Comments

#### Sample Preparation

Assaying is warranted for representative well-mineralized samples (eg. Cu > 1%). Samples are dried at 60°C. Soil, sediment and moss mats (after pounding) are sieved to -80 mesh (-177 µm). Vegetation is dried (60°C) and pulverized or ashed (475°C). Rock and drill core is jaw crushed to 70% passing 10 mesh (2 mm), a 250 g aliquot is riffle split and pulverized to 95% passing 150 mesh (100 µm) in a mild-steel ring-and-puck mill. Aliquots of 0.250 ± 0.002 g are weighed into Teflon beakers. Acme's QA/QC protocol requires two pulp duplicates to monitor analytical precision and an aliquot of in-house reference material STD R-1 to monitor accuracy in each batch of 34 samples. Trench and drill core programs will also include a pulp made from a 2<sup>nd</sup> crushed fraction split (rejects duplicate) to measure method precision.

#### Sample Digestion

A 18:10:3:6 mixture of H<sub>2</sub>O-HF-HClO<sub>4</sub>-HNO<sub>3</sub> (ACS grade) is added, the sample is heated to fuming on a hot plate and taken to dryness. The residue is taken up in dilute (15%) aqua regia (HCl:HNO<sub>3</sub>:H<sub>2</sub>O), transferred to a 100 mL volumetric flask and heated for 30 minutes in a boiling water (>95°C) bath. After cooling for 3 hrs, solutions are made up to volume (100 mL) with dilute (5%) HCl. Very high-grade samples may require a 1 g to 250 mL or 0.25 g to 250 mL sample/solution ratio for accurate determination. Acme's QA/QC protocol requires simultaneous digestion of two reagent blanks inserted in each batch.

#### Sample Analysis

Sample solutions are aspirated into a Jarrel Ash Atomcomp model 800 or 975 ICP emission spectrograph to determine 21 elements: Ag, Al, Bi, Ca, Cd, Co, Cr, Cu, Fe, K, Mg, Mn, Mo, Na, Ni, P, Pb, Sb, Sr, W, Zn.

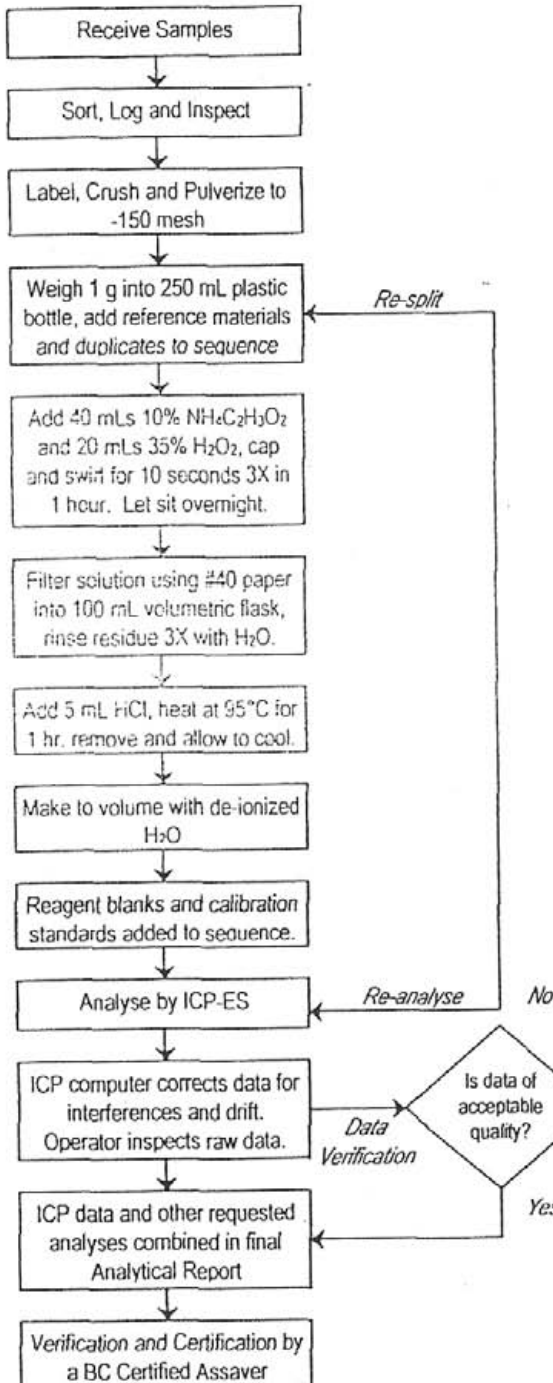
#### Data Evaluation

Raw and final data from the ICP-ES undergoes a final verification by a British Columbia Certified Assayer who then signs the Analytical Report before it is released to the client. Chief Assayer is Clarence Leong, other certified assayers are Dean Toye and Jacky Wang.



## METHODS AND SPECIFICATIONS FOR ANALYTICAL PACKAGE GROUP 8 – NI-SULPHIDE ASSAY BY ICP-ES

### Analytical Process



### Comments

#### Sample Preparation

Assaying is warranted for representative well-mineralized samples (eg. Ni > 0.5%). Rock and drill core is jaw crushed to 70% passing 10 mesh (2 mm), a 250 g aliquot is riffle split and pulverized to 95% passing 150 mesh (100 µm) in a mild-steel ring-and-puck mill. Aliquots of 1.000 ± 0.002 g are weighed into 250 mL plastic bottles. Acme's QA/QC protocol requires two pulp duplicates to monitor analytical precision and aliquots of certified reference material UM-2 or UM-4 and/or in-house reference material NC-1 to monitor accuracy in each batch of 34 samples. Drill core programs will include a pulp from a 2<sup>nd</sup> crushed fraction split (rejects duplicate) to measure method precision.

#### Sample Digestion

Samples are cold leached with a mixture of 40 mLs of 10% ammonium acetate and 20 mLs of 35% hydrogen peroxide that is agitated for 10 seconds three times within the first hour then let to stand overnight. Solutions are filtered into a 100 mL volumetric flask and the residue is rinsed 3X with de-ionized water. Solutions are heated in hot water bath (95°C) for 1 hour then allowed to cool. Solutions are made up to volume (100 mL) with de-ionized water. Acme's QA/QC protocol requires simultaneous digestion of two reagent blanks inserted in each batch.

#### Sample Analysis

Sample solutions are aspirated into a Jarrel Ash Atomcomp model 800 or 975 ICP emission spectrograph to determine Ni.

#### Calculation

This leach extracts both Ni sulphide and Ni oxide (Ni<sub>s-o</sub>). A Ni-Oxide (Ni<sub>o</sub>) leach must be conducted then used to back calculate for Ni sulphide (Ni<sub>s</sub>) content using the following equation:

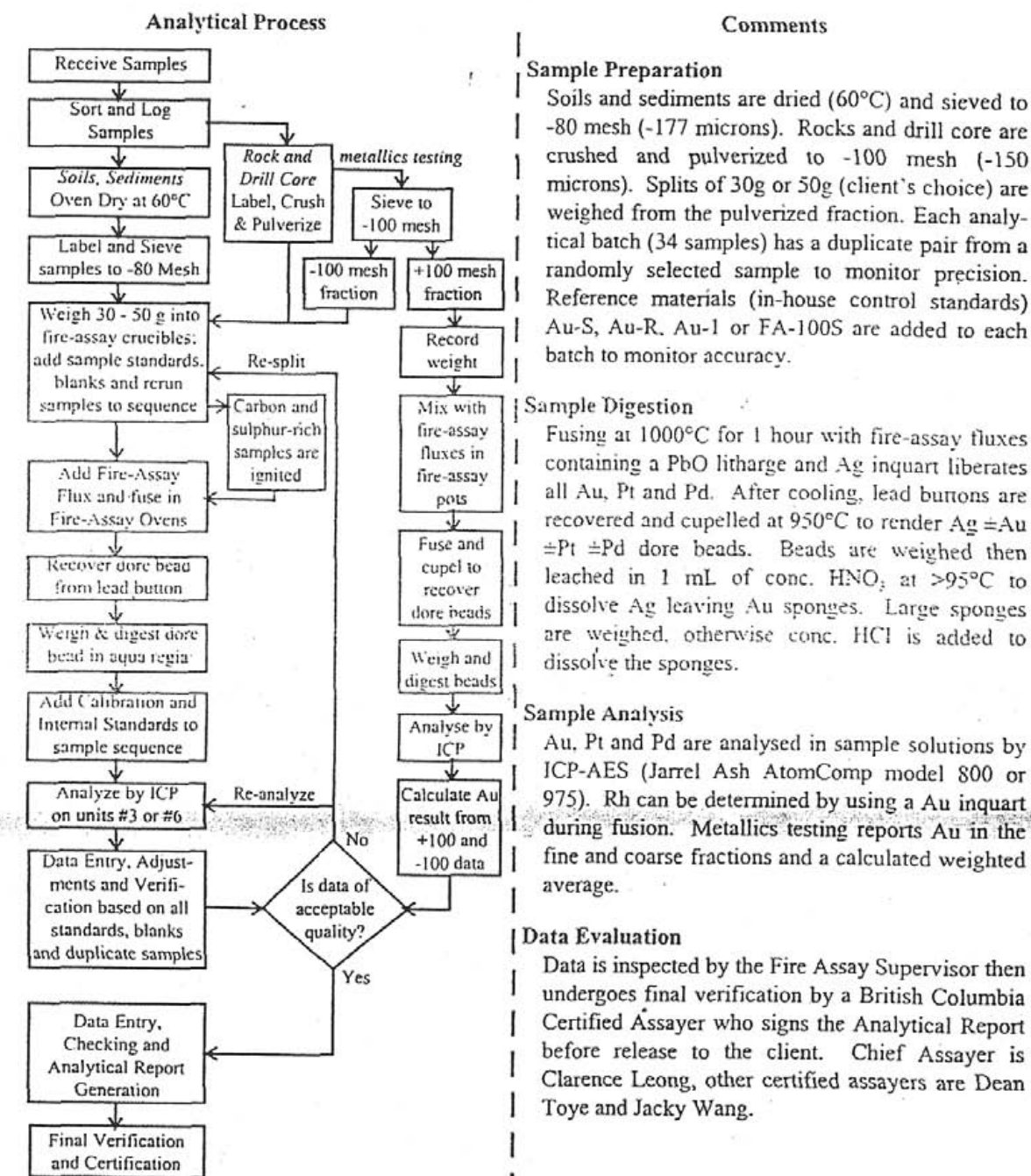
$$Ni_s = Ni_{s-o} - Ni_o$$

#### Data Evaluation

Raw and final data from the ICP-ES undergoes a final verification by a British Columbia Certified Assayer who then signs the Analytical Report before it is released to the client. Chief Assayer is Clarence Leong, other certified assayers are Dean Toye and Jacky Wang.

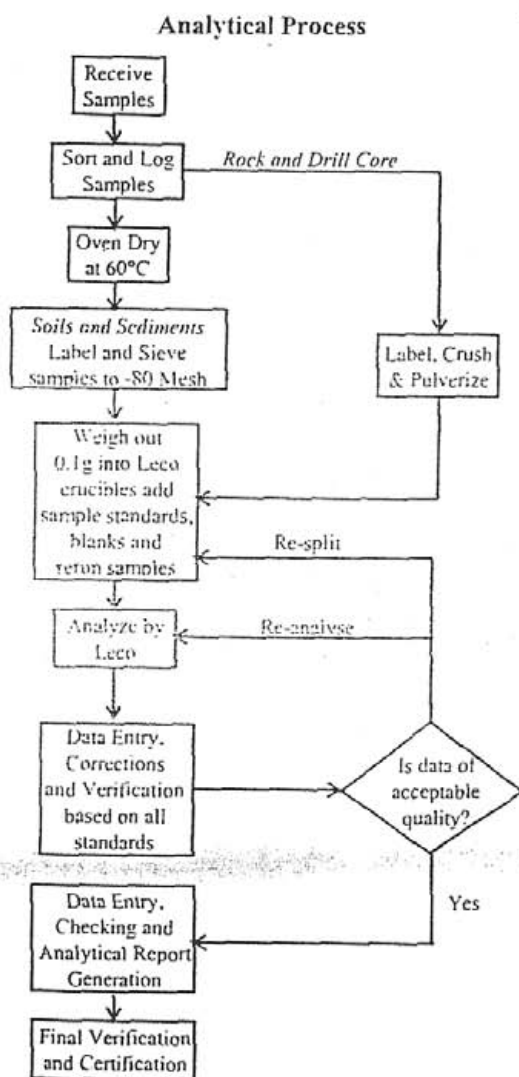


**METHODS AND SPECIFICATIONS FOR ANALYTICAL PACKAGE  
GROUP 3B - PRECIOUS METALS BY FIRE GEOCHEM**



## METHODS AND SPECIFICATIONS FOR ANALYTICAL PACKAGE

### GROUP 2A: TOTAL SULPHUR



#### Comments

##### Sample Preparation

Soils and sediments are dried (60°C) and sieved to -80 mesh ASTM (-177 microns), rocks and drill core are crushed and pulverized to -100 mesh ASTM (-150 microns). Moss-mat samples are dried (60°C), macerated then sieved to recover -80 mesh sediment or ashed at 550°C (upon a client's request). Sample splits (0.1 g) are placed in Leco crucibles. Duplicate splits of crushed (rejects duplicate) and pulverized (pulp duplicate) fractions are included with every 34 drill core or trench samples to define sample homogeneity (reject duplicate) and analytical precision (pulp duplicate). Duplicate pulp splits (only) are included in every batch of soil, sediment and routine rock samples. A blank and in-house standard material STD CSA are carried through weighing, ignition and analytical stages to monitor accuracy.

##### Sample Analysis

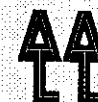
Samples are analyzed in a Leco C244 Carbon-Sulphur analyser. The sulphur determined is total and attributed to the presence of sulphur in all forms.

##### Data Evaluation

Raw and final data from the Leco Carbon-Sulphur analyser undergoes a final verification by a British Columbia Certified Assayer who must sign the analytical report before release to the client. Chief assayer is Clarence Leong, other certified assayers are Dean Toye and Jacky Wang.

ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-72A File # A503749 Page 1  
1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Chris Baldys

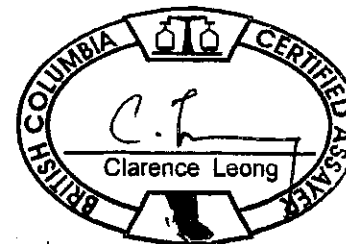


SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg	
267001	<.001	.009	<.02	.01	<2	.195	.017	.21	9.99	<.01	<.01	<.001	<.01	<.01	<.01	.73	.02	.207	28.86	.03	.23	.12	.04	<.01	.60	<2	4	2	1.19
267002	<.001	.028	<.02	<.01	<2	.242	.013	.11	6.68	<.01	<.01	<.001	<.01	<.01	<.01	.29	.01	.195	28.02	.01	.09	<.01	<.01	<.01	.22	3	30	24	2.50
267003	<.001	.007	<.02	<.01	<2	.228	.014	.11	6.54	<.01	<.01	<.001	<.01	<.01	<.01	.48	.01	.201	29.39	.01	.06	.07	<.01	<.01	.12	<2	24	28	2.73
267004	<.001	.037	<.02	<.01	<2	.380	.015	.12	6.85	<.01	<.01	<.001	<.01	<.01	<.01	.25	.01	.237	30.14	.01	.05	<.01	<.01	<.01	.26	<2	128	151	4.80
267005	<.001	.055	<.02	<.01	<2	.558	.018	.11	6.73	<.01	<.01	<.001	<.01	<.01	<.01	.21	.01	.174	29.30	<.01	.05	<.01	.02	<.01	.48	5	48	62	2.87
267006	<.001	.016	<.02	<.01	<2	.251	.012	.11	6.41	<.01	<.01	<.001	<.01	<.01	<.01	.40	.01	.230	28.39	.02	.63	.02	.04	<.01	.16	3	21	33	3.13
267007	<.001	.039	<.02	<.01	<2	.347	.015	.10	6.55	<.01	<.01	<.001	<.01	<.01	<.01	.36	.01	.204	29.11	.01	.17	.02	<.01	<.01	.30	6	42	53	4.76
267008	<.001	.052	<.02	<.01	<2	.321	.014	.10	6.46	<.01	<.01	<.001	<.01	<.01	<.01	.30	.01	.151	28.10	.01	.10	.08	<.01	<.01	.37	9	51	62	3.92
267009	<.001	.020	<.02	<.01	<2	.244	.016	.10	7.56	<.01	<.01	<.001	<.01	<.01	<.01	.65	.01	.207	25.98	.01	.17	.08	.03	<.01	.82	7	3	8	4.24
267010A	<.001	.028	<.02	.01	<2	.167	.011	.14	6.86	<.01	.02	<.001	<.01	<.01	.01	3.14	.03	.173	22.21	.06	.68	.14	.04	<.01	1.26	2	5	3	3.70
267010B	<.001	.027	<.02	.01	<2	.172	.012	.13	6.86	<.01	.02	<.001	<.01	<.01	.01	2.95	.02	.166	21.97	.05	.60	.09	.06	<.01	1.31	2	3	9	-
267011	<.001	.047	<.02	.01	<2	.320	.019	.13	9.10	<.01	<.01	<.001	<.01	<.01	<.01	.31	.01	.136	29.89	.01	.05	.31	.01	<.01	.56	9	27	22	5.92
267012	<.001	.045	<.02	.01	<2	.243	.019	.14	9.95	<.01	<.01	<.001	<.01	<.01	<.01	.41	.01	.172	30.20	.01	.04	.12	.04	<.01	.58	32	27	17	5.72
267013	<.001	.046	<.02	<.01	<2	.300	.021	.13	9.49	<.01	<.01	<.001	<.01	<.01	<.01	1.55	.01	.159	27.45	.02	.25	.04	.06	<.01	.88	37	22	20	6.35
267014	<.001	.046	<.02	.01	<2	.297	.023	.14	11.21	<.01	<.01	<.001	<.01	<.01	<.01	.14	.01	.192	30.23	<.01	.02	.04	.03	<.01	1.13	<2	16	18	5.74
267015	<.001	.023	<.02	.01	<2	.238	.018	.14	10.44	<.01	<.01	<.001	<.01	<.01	<.01	.77	.01	.159	28.78	.01	.01	<.01	<.01	<.01	.79	2	12	8	3.78
.STD RTS-2	<.001	.076	<.02	.01	<2	.274	.008	.04	38.68	<.01	<.01	<.001	<.01	<.01	.01	.64	.01	.013	.42	.18	.84	.27	.15	<.01	19.56	<2	<2	<2	-
267016	<.001	.022	<.02	.01	<2	.217	.015	.11	9.35	<.01	<.01	<.001	<.01	<.01	<.01	.85	.01	.254	25.79	.02	.27	<.01	<.01	<.01	1.08	<2	17	20	3.66
267017	<.001	.038	<.02	.01	<2	.306	.021	.13	11.19	<.01	<.01	<.001	<.01	<.01	<.01	.25	.01	.194	28.61	<.01	.04	<.01	<.01	<.01	1.49	6	23	23	5.65
267018	<.001	.040	<.02	.01	<2	.316	.023	.11	10.92	<.01	<.01	<.001	<.01	<.01	.01	.48	.01	.265	25.83	.01	.37	.19	.03	<.01	1.97	5	33	39	3.66
267019	<.001	.038	<.02	.01	<2	.050	.006	.18	8.81	<.01	.08	<.001	<.01	<.01	.04	5.87	.17	.013	6.07	.50	8.10	2.24	2.80	<.01	.34	<2	48	45	2.45
267020	.001	.033	<.02	.01	<2	.213	.013	.17	9.24	<.01	<.01	<.001	<.01	<.01	.02	1.73	.01	.097	21.48	.04	.40	.12	.04	<.01	1.83	4	6	16	4.90
267021	<.001	.007	<.02	.01	<2	.227	.008	.12	6.52	<.01	<.01	<.001	<.01	<.01	.01	.60	<.01	.070	23.96	.05	.51	.12	.12	<.01	.70	2	6	8	4.74
267022	<.001	.015	<.02	.01	<2	.189	.011	.11	7.83	<.01	<.01	<.001	<.01	<.01	.01	.85	.01	.082	22.90	.06	.66	.07	.36	<.01	1.18	<2	10	9	4.55
267023	<.001	.024	<.02	.01	<2	.200	.013	.14	8.68	<.01	<.01	<.001	<.01	<.01	.02	2.05	.04	.104	20.34	.10	1.10	.19	.72	<.01	1.65	<2	3	13	5.44
267024	<.001	.041	<.02	.01	<2	.214	.018	.15	10.66	<.01	<.01	<.001	<.01	<.01	.01	.66	.01	.215	26.83	.01	.07	.19	.02	<.01	1.98	<2	21	18	4.74
267025 (pulp)	<.001	.100	<.02	.01	<2	.353	.017	.06	9.41	<.01	<.01	<.001	<.01	<.01	.01	3.49	.01	.376	16.27	.15	2.67	.57	.09	<.01	1.13	14	98	390	-
267026	.001	.040	<.02	.01	<2	.204	.021	.12	10.57	<.01	<.01	<.001	<.01	.01	.01	1.82	.01	.151	22.33	.04	.34	.31	.04	<.01	2.97	22	8	19	3.89
267027	.003	.065	<.02	.01	<2	.361	.023	.14	14.55	<.01	<.01	<.001	<.01	<.01	.02	1.67	<.01	.205	19.37	.03	.19	.47	<.01	<.01	5.40	3	35	38	3.63
RE 267027	.004	.068	<.02	.01	<2	.367	.022	.14	14.69	<.01	<.01	<.001	<.01	<.01	.02	1.67	.01	.206	19.49	.03	.20	.20	.05	<.01	5.82	5	44	37	-
RRE 267027	.003	.068	<.02	.01	<2	.361	.023	.14	14.60	<.01	<.01	<.001	<.01	.01	.02	1.68	<.01	.202	19.02	.03	.18	.20	.07	<.01	5.76	2	41	35	-
267028	.002	.014	<.02	.01	<2	.204	.012	.13	10.02	<.01	<.01	<.001	<.01	<.01	.02	1.17	<.01	.134	22.07	.04	.23	.15	<.01	<.01	3.04	<2	3	16	2.96
267029	<.001	.006	<.02	.01	<2	.212	.009	.11	5.82	<.01	<.01	<.001	<.01	<.01	.01	1.77	<.01	.088	23.48	.04	.27	.15	.01	<.01	.25	<2	13	12	3.77
267030A	<.001	.007	<.02	<.01	<2	.253	.011	.09	5.93	<.01	<.01	<.001	<.01	<.01	.01	.55	.01	.041	26.21	.03	.20	.26	.06	<.01	.30	<2	4	14	2.12
STANDARD R-2a	.051	.575	1.67	4.20	166	.382	.048	.25	25.26	.21	.15	.030	.13	<.01	.02	3.85	.09	.066	2.65	.19	2.77	.52	.66	.08	5.28	476	485	480	-

Standard is STANDARD R-2a/CSB/FA-10R.

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCL) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.  
TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B BY FIRE ASSAY & ANALYSIS BY ICP. (30 gm)  
- SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data h FA \_\_\_\_\_ DATE RECEIVED: JUL 22 2005 DATE REPORT MAILED: Aug 10/05



All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267030B	<.001	.006	<.02	.01	<2	.251	.011	.09	5.88	<.01	<.01	<.001	<.01	<.01	.01	.51	.01	.045	27.28	.03	.25	<.01	.08	<.01	.29	4	16	15	-
267031	<.001	.011	<.02	.01	<2	.311	.015	.13	7.65	<.01	<.01	<.001	<.01	<.01	.01	.08	.01	.129	31.88	.01	.08	<.01	<.01	<.01	.42	10	23	25	6.00
267032	<.001	.021	<.02	.01	<2	.361	.013	.12	7.12	<.01	<.01	<.001	<.01	<.01	.01	.29	.01	.179	29.44	.02	.12	<.01	<.01	<.01	.53	20	57	78	5.22
267033	<.001	.022	<.02	.01	<2	.398	.015	.12	7.08	<.01	<.01	<.001	<.01	<.01	.01	.17	<.01	.231	30.32	.01	.12	.12	.02	<.01	.61	26	83	108	2.64
267034	<.001	.010	<.02	.01	<2	.387	.016	.14	7.69	<.01	<.01	<.001	<.01	<.01	.01	1.27	.01	.213	26.31	.03	.22	<.01	.02	<.01	.96	5	31	45	4.86
267035	<.001	.034	<.02	.01	<2	.410	.017	.13	8.05	<.01	<.01	<.001	<.01	<.01	.01	.60	.02	.437	27.92	.02	.21	<.01	<.01	<.01	1.15	14	68	101	4.96
267036	<.001	.022	<.02	.01	<2	.300	.014	.13	7.22	<.01	<.01	<.001	<.01	<.01	.01	1.01	.01	.271	25.71	.04	.26	<.01	.04	<.01	.80	9	46	61	2.63
267037	<.001	.014	<.02	.01	<2	.262	.013	.13	7.59	<.01	<.01	<.001	<.01	<.01	.01	2.00	.01	.177	24.62	.04	.24	.13	.01	<.01	.84	6	25	29	3.33
267038	<.001	.016	<.02	.01	<2	.132	.010	.16	8.61	<.01	<.01	<.001	<.01	<.01	.02	1.83	.01	.174	22.57	.04	.25	.08	.04	<.01	1.51	3	9	9	3.24
267039	.004	.056	<.02	.01	<2	.200	.020	.17	17.28	<.01	<.01	<.001	<.01	<.01	.05	2.06	<.01	.147	16.47	.05	.34	<.01	.11	<.01	7.22	4	26	26	5.18
267040	<.001	.016	<.02	.01	<2	.068	.008	.20	7.84	<.01	<.01	<.001	<.01	<.01	.05	5.74	.01	.162	17.74	.09	.43	.14	.08	<.01	1.23	2	2	<2	1.35
267041	<.001	.011	<.02	.01	<2	.178	.011	.14	7.82	<.01	<.01	<.001	<.01	<.01	.01	1.32	.01	.134	24.62	.03	.18	<.01	.10	<.01	.76	3	6	4	.78
267042	<.001	.011	<.02	.01	<2	.214	.013	.15	7.96	<.01	<.01	<.001	<.01	<.01	.02	2.63	<.01	.154	23.08	.05	.26	<.01	.07	<.01	1.08	5	15	15	2.99
.STD RTS-2	<.001	.076	<.02	.01	<2	.276	.007	.04	38.72	<.01	<.01	<.001	<.01	<.01	.01	.64	.01	.012	.40	.18	.80	.25	.19	<.01	19.45	<2	<2	<2	-
267043	<.001	.012	<.02	.01	<2	.178	.012	.15	8.60	<.01	<.01	<.001	<.01	.01	.02	1.98	.01	.126	23.39	.05	.25	.14	.03	<.01	1.28	6	15	11	4.59
267044	.001	.017	<.02	.01	<2	.160	.011	.16	8.85	<.01	<.01	<.001	<.01	<.01	.03	2.94	.01	.149	20.44	.07	.40	.04	.03	<.01	2.03	31	3	5	4.98
267045	<.001	.020	<.02	.01	<2	.190	.015	.16	9.57	<.01	<.01	<.001	<.01	<.01	.02	1.97	.01	.130	25.07	.04	.23	<.01	<.01	<.01	1.57	4	8	10	5.48
267046	<.001	.016	<.02	.01	<2	.168	.011	.15	9.01	<.01	<.01	<.001	<.01	<.01	.02	3.33	.01	.191	23.25	.04	.22	<.01	.04	<.01	1.37	4	8	8	4.58
267047	<.001	.014	<.02	.01	<2	.080	.008	.15	7.15	<.01	<.01	<.001	<.01	<.01	.03	7.30	.01	.159	17.94	.08	.38	.20	.02	<.01	1.10	8	3	5	4.89
267048	.001	.058	<.02	.01	<2	.168	.021	.16	16.67	<.01	<.01	<.001	<.01	<.01	.05	5.67	.01	.097	13.42	.10	1.10	.36	.67	<.01	6.99	9	17	19	3.22
267049	<.001	.009	<.02	.02	<2	.007	.003	.36	11.73	<.01	.15	<.001	<.01	<.01	.03	9.30	.25	.005	6.84	.70	7.10	.15	2.04	<.01	1.34	6	<2	<2	.55
267050 (pulp)	<.001	.101	<.02	<.01	<2	.355	.017	.05	9.45	<.01	<.01	<.001	<.01	<.01	.01	3.57	.01	.370	17.05	.16	2.63	.26	.02	<.01	1.11	23	97	371	-
267051	.001	.033	<.02	.01	<2	.174	.016	.17	10.14	<.01	.01	<.001	<.01	<.01	.03	4.18	.02	.178	18.66	.12	1.05	.05	.34	<.01	1.85	7	6	7	2.10
267052	.001	.050	<.02	<.01	<2	.201	.018	.13	10.64	<.01	<.01	<.001	<.01	<.01	.02	5.06	.02	.161	21.87	.04	.23	<.01	.03	<.01	2.84	6	8	7	6.00
267053	<.001	.011	<.02	.01	<2	.191	.013	.17	9.46	<.01	<.01	<.001	<.01	<.01	.01	1.75	.02	.234	28.71	.02	.11	<.01	<.01	<.01	.93	3	5	6	5.53
267054	<.001	.017	<.02	.01	<2	.172	.014	.17	9.60	<.01	<.01	<.001	<.01	<.01	.01	2.35	.01	.212	27.33	.03	.17	<.01	.04	<.01	1.01	5	7	6	5.28
267055	<.001	.040	<.02	.01	<2	.471	.024	.16	11.34	<.01	<.01	<.001	<.01	.01	<.01	1.29	.01	.164	29.60	.02	.15	<.01	.04	<.01	2.06	6	28	28	5.25
267056	<.001	.025	<.02	.01	<2	.242	.021	.15	10.26	<.01	<.01	<.001	<.01	<.01	<.01	.59	.01	.115	30.16	.02	.15	<.01	<.01	<.01	1.30	4	8	4	5.12
RE 267056	<.001	.025	<.02	.01	<2	.234	.020	.14	10.03	<.01	<.01	<.001	<.01	<.01	<.01	.56	.01	.112	29.45	.02	.14	<.01	.03	<.01	1.36	5	11	12	-
RRE 267056	<.001	.025	<.02	<.01	<2	.240	.020	.14	10.08	<.01	<.01	<.001	<.01	.01	<.01	.51	.01	.113	29.51	.02	.14	<.01	.02	<.01	1.30	3	14	12	-
267057	<.001	.033	<.02	<.01	<2	.287	.020	.15	10.22	<.01	<.01	<.001	<.01	.01	<.01	.34	.01	.115	30.16	.01	.03	<.01	.04	<.01	1.49	5	11	12	5.03
267058	<.001	.026	<.02	<.01	<2	.323	.016	.15	9.72	<.01	<.01	<.001	<.01	<.01	<.01	.26	.01	.139	29.95	.02	.12	<.01	.03	<.01	1.33	5	11	6	5.62
267059	<.001	.019	<.02	.01	<2	.270	.013	.15	8.59	<.01	<.01	<.001	<.01	<.01	<.01	.84	.02	.154	27.80	.06	.79	.18	.08	<.01	.82	6	22	15	4.91
267060 (rock)	<.001	.005	<.02	.01	<2	.003	.001	.11	4.36	<.01	.05	<.001	<.01	<.01	.01	4.77	.06	.003	1.94	.34	8.63	2.50	1.26	<.01	.02	6	4	5	2.65
STANDARD R-2a	.051	.573	1.71	4.26	169	.383	.047	.25	25.18	.22	.16	.030	.14	<.01	.02	3.89	.09	.062	2.67	.20	2.60	.56	.68	.08	5.31	499	482	473	-

Standard is STANDARD R-2a/CSB/FA-10R. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267061	<.001	.037	<.02	<.01	<2	.365	.018	.12	9.07	<.02	<.01	<.001	<.01	<.01	<.01	.25	<.01	.308	24.25	.02	.22	.01	.01	<.01	1.46	9	41	44	2.81
STANDARD	.049	.572	1.65	4.24	164	.383	.048	.22	25.17	.22	.14	.029	.13	<.01	.01	3.81	.08	.061	2.68	.18	2.66	.48	.61	.11	5.28	484	487	490	-

Standard is STANDARD R-2a/CSB/FA-10R.



ASSAY CERTIFICATE

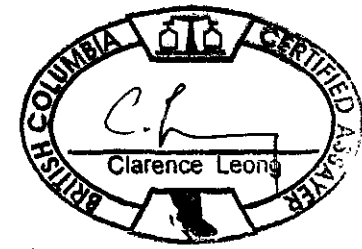
Hard Creek Nickel Corporation PROJECT Tur C05-72A File # A503749 Page 1  
1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Chris Baldys



SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267001	.007	.136	.011	.98
267002	.021	.154	.009	.70
267003	.005	.137	.008	.73
267004	.036	.248	.009	1.07
267005	.052	.468	.014	1.33
267006	.014	.167	.008	.71
267007	.037	.274	.011	.91
267008	.049	.286	.012	.90
267009	.018	.234	.015	.74
267010A	.026	.158	.010	1.15
267010B	.025	.162	.010	1.17
267011	.046	.216	.011	1.15
267012	.043	.161	.010	1.09
267013	.045	.249	.014	1.04
267014	.044	.228	.014	1.29
267015	.022	.186	.011	1.27
.STD RTS-2	.058	.231	.007	3.47
267016	.020	.206	.013	.96
267017	.037	.257	.015	1.36
267018	.038	.300	.021	1.50
267019	.036	.031	.002	.33
267020	.031	.186	.011	1.25
267021	.007	.187	.006	.58
267022	.014	.165	.009	.65
267023	.023	.176	.011	.74
267024	.039	.214	.016	1.25
267025 (pulp)	.098	.273	.012	1.29
267026	.038	.197	.020	1.41
267027	.065	.346	.023	3.21
RE 267027	.065	.358	.023	3.35
RRE 267027	.069	.358	.023	3.31
267028	.014	.180	.011	1.21
267029	.006	.187	.007	.41
267030A	.005	.229	.009	.43
STANDARD R-2a	.542	.334	.044	7.79

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
- SAMPLE TYPE: DRILL CORE R150  
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data h FA \_\_\_\_\_ DATE RECEIVED: JUL 22 2005 DATE REPORT MAILED: Aug 10/05





SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267030B	.008	.242	.010	.45
267031	.011	.227	.008	1.07
267032	.022	.310	.009	.97
267033	.021	.324	.010	1.06
267034	.010	.344	.013	.80
267035	.033	.362	.012	1.11
267036	.022	.269	.011	.71
267037	.013	.238	.010	.65
267038	.015	.111	.008	.71
267039	.056	.201	.020	4.33
267040	.014	.057	.006	.76
267041	.008	.160	.008	.58
267042	.010	.192	.010	.80
.STD RTS-2	.060	.240	.007	4.22
267043	.012	.144	.008	.94
267044	.016	.144	.009	1.07
267045	.018	.163	.010	1.07
267046	.015	.148	.009	1.01
267047	.013	.071	.006	.63
267048	.056	.164	.020	4.24
267049	.009	.004	.001	2.49
267050 (pulp)	.096	.266	.012	1.24
267051	.029	.160	.014	1.35
267052	.047	.188	.016	1.39
267053	.010	.143	.008	1.19
267054	.013	.137	.008	1.16
267055	.036	.416	.019	1.73
267056	.023	.207	.015	1.47
RE 267056	.023	.206	.015	1.49
RRE 267056	.022	.201	.015	1.54
267057	.031	.252	.014	1.52
267058	.024	.271	.012	1.60
267059	.018	.209	.009	1.14
267060 (rock)	.004	.002	<.001	.18
STANDARD R-2a	.536	.333	.043	7.44

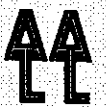
Sample type: DRILL CORE R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Cu*	Ni*	Co*	Fe*
	%	%	%	%
267061 STANDARD R-2a	.035 .529	.332 .322	.014 .041	1.34 6.24

Sample type: DRILL CORE R150.



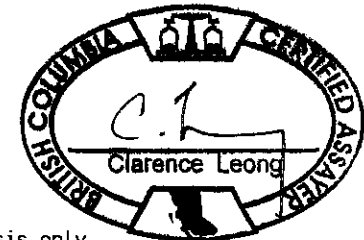


SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	Ca %	P %	Cr %	Mg %	Al %	Na %	K %	W %	V %	Ti %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267062	<.001	.022	<.02	.01	<2	.299	.014	.13	8.28	<.02	.03	<.001	<.01	<.01	1.45	.01	.219	22.31	.67	.01	.02	<.01	<.01	.04	.81	3	42	45	4.20
267063	<.001	.023	<.02	.01	<2	.297	.014	.13	9.01	<.02	<.01	<.001	<.01	<.01	.49	<.01	.197	24.40	.28	<.01	<.01	<.01	<.01	.06	.77	<2	29	23	5.22
267064	<.001	.024	<.02	<.01	<2	.260	.015	.13	9.40	<.02	<.01	<.001	<.01	<.01	.45	<.01	.231	23.91	.28	<.01	.01	<.01	<.01	.03	1.04	5	11	12	5.14
267065	<.001	.032	<.02	.01	<2	.221	.014	.14	9.04	<.02	<.01	<.001	<.01	<.01	.44	<.01	.326	24.65	.09	<.01	<.01	<.01	<.01	.01	.81	17	4	5	6.01
267066	<.001	.021	<.02	.01	2	.233	.016	.14	9.48	<.02	<.01	<.001	<.01	<.01	.62	<.01	.238	24.71	.08	<.01	<.01	<.01	<.01	.01	.99	5	24	22	5.09
267067	<.001	.019	<.02	<.01	<2	.215	.016	.13	9.00	<.02	<.01	<.001	<.01	<.01	.74	<.01	.144	24.18	.08	<.01	<.01	<.01	<.01	.01	1.00	5	9	20	5.54
267068	<.001	.023	<.02	.01	<2	.238	.016	.12	9.61	<.02	<.01	<.001	<.01	<.01	1.28	.01	.261	22.41	.56	<.01	<.01	<.01	<.01	.04	1.22	5	7	9	3.26
267069	<.001	.023	<.02	.01	<2	.297	.017	.14	10.15	<.02	<.01	<.001	<.01	<.01	.24	<.01	.278	24.17	.16	<.01	<.01	<.01	<.01	.01	1.30	4	20	26	3.01
267070A	<.001	.035	<.02	.01	<2	.197	.013	.12	9.28	<.02	<.01	<.001	<.01	<.01	.56	<.01	.218	22.81	.34	<.01	.01	<.01	<.01	.03	1.15	12	18	11	5.61
267070B	<.001	.035	<.02	.01	<2	.200	.013	.12	9.41	<.02	<.01	<.001	<.01	<.01	.59	<.01	.235	22.81	.36	<.01	.01	<.01	<.01	.03	1.13	8	16	19	-
267071	<.001	.018	<.02	.01	<2	.202	.016	.12	9.15	<.02	<.01	<.001	<.01	<.01	1.52	<.01	.148	22.98	.16	<.01	<.01	<.01	<.01	.01	1.14	7	<2	4	5.60
267072	<.001	.019	<.02	.01	<2	.212	.017	.14	10.25	<.02	<.01	<.001	<.01	<.01	.04	<.01	.237	25.17	.08	<.01	<.01	<.01	<.01	.01	1.30	7	6	4	5.12
267073	<.001	.031	<.02	.01	<2	.284	.019	.13	10.75	<.02	<.01	<.001	<.01	<.01	.13	<.01	.162	24.51	.08	<.01	<.01	<.01	<.01	.01	1.92	4	21	8	2.72
267074	<.001	.033	<.02	.01	<2	.418	.037	.14	15.34	<.02	<.01	<.001	<.01	<.01	.03	<.01	.253	23.06	.07	<.01	<.01	<.01	<.01	.01	3.97	2	29	19	4.68
267075 (pulp)	<.001	.058	<.02	.01	<2	.241	.012	.11	9.25	<.02	<.01	<.001	<.01	<.01	4.24	<.01	.806	13.28	3.86	.33	.11	<.01	.02	.18	.53	22	92	271	-
267076	<.001	.020	<.02	.01	<2	.229	.022	.13	10.78	<.02	<.01	<.001	<.01	<.01	1.66	<.01	.208	22.34	.12	.02	<.01	<.01	<.01	.02	1.89	32	7	2	5.10
267077	<.001	.030	<.02	.01	2	.237	.017	.14	10.38	<.02	<.01	<.001	<.01	<.01	.27	<.01	.281	24.08	.11	<.01	<.01	<.01	<.01	.01	1.35	7	15	13	5.97
.STD RTS-2	<.001	.073	<.02	.02	3	.275	.007	.04	37.97	<.02	<.01	<.001	<.01	<.01	.56	<.01	.012	.37	.84	.21	.13	<.01	<.01	.16	18.27	-	-	-	-
267078	<.001	.013	<.02	.01	<2	.207	.018	.16	10.22	<.02	<.01	<.001	<.01	<.01	.77	<.01	.232	24.45	.10	.01	<.01	<.01	<.01	.01	1.26	3	12	6	6.13
267079	<.001	.046	<.02	.01	<2	.180	.014	.12	9.82	<.02	<.01	<.001	<.01	<.01	.07	<.01	.196	22.51	.32	<.01	<.01	<.01	<.01	.03	1.41	17	12	16	5.34
267080	<.001	.029	<.02	.01	<2	.227	.020	.09	9.93	<.02	<.01	<.001	<.01	<.01	2.23	<.01	.171	20.37	.64	.01	<.01	<.01	<.01	.05	2.10	13	24	20	4.97
267081	<.001	.020	<.02	.02	2	.345	.026	.14	11.38	<.02	<.01	<.001	<.01	<.01	1.99	<.01	.153	22.04	.15	.02	<.01	<.01	<.01	.02	2.39	18	27	48	4.43
RE 267081	<.001	.019	<.02	.01	<2	.347	.027	.14	11.25	<.02	<.01	<.001	<.01	<.01	1.96	<.01	.144	22.25	.14	.01	<.01	<.01	<.01	.02	2.44	16	19	33	-
RRE 267081	<.001	.019	<.02	.01	<2	.343	.026	.15	11.32	<.02	<.01	<.001	<.01	<.01	2.01	<.01	.140	22.07	.14	.02	<.01	<.01	<.01	.02	2.39	13	22	43	-
267082	<.001	.011	<.02	.01	<2	.146	.010	.14	7.96	<.02	<.01	<.001	<.01	<.01	3.50	<.01	.184	20.81	.14	.03	<.01	<.01	.01	.02	.89	7	<2	5	5.69
267083	<.001	.017	<.02	.01	<2	.118	.014	.14	9.29	<.02	<.01	<.001	<.01	<.01	5.25	<.01	.168	18.65	.17	.04	<.01	<.01	.01	.03	1.55	7	6	<2	5.54
267084	.002	.042	<.02	<.01	<2	.122	.019	.10	10.96	<.02	<.01	<.001	<.01	<.01	7.06	<.01	.173	15.47	.21	.05	<.01	<.01	.01	.04	3.45	6	7	16	5.53
267085	<.001	.027	<.02	.01	<2	.101	.012	.10	8.64	<.02	<.01	<.001	<.01	<.01	6.78	<.01	.185	16.54	.22	.05	<.01	<.01	.01	.03	1.87	11	8	10	5.56
267086	<.001	.031	<.02	<.01	<2	.107	.019	.09	11.97	<.02	<.01	<.001	<.01	<.01	7.21	<.01	.148	13.96	.22	.05	<.01	<.01	.02	.03	4.03	3	12	6	2.34
267087	.001	.007	<.02	<.01	<2	.026	.004	.03	2.86	<.02	<.01	<.001	<.01	<.01	2.26	<.01	.035	3.56	.06	.02	<.01	<.01	.01	.01	3.38	18	5	2	5.98
267088	.001	.012	<.02	<.01	<2	.062	.008	.11	8.95	<.02	<.01	<.001	<.01	<.01	8.19	<.01	.176	14.57	.23	.07	<.01	<.01	.03	.04	1.65	4	17	9	4.84
267089	.001	.018	<.02	.01	<2	.084	.013	.13	10.45	<.02	<.01	<.001	<.01	<.01	10.56	<.01	.187	11.91	.32	.09	<.01	<.01	.05	.06	2.66	5	23	10	5.77
267090 (rock)	.001	.005	<.02	.01	<2	.002	.002	.09	4.36	<.02	.04	<.001	<.01	<.01	4.17	.05	.003	1.84	8.68	2.37	1.22	<.01	.01	.29	.04	4	3	<2	2.13
267091	<.001	.014	<.02	<.01	<2	.086	.012	.12	8.35	<.02	<.01	<.001	<.01	<.01	9.34	<.01	.217	14.43	.34	.09	<.01	<.01	.02	.05	1.39	<2	8	12	4.76
STANDARD R-2a	.048	.581	1.61	4.17	166	.390	.049	.24	25.09	.23	.16	.030	.14	<.01	3.46	.08	.064	2.62	2.85	.52	.65	.11	.01	.18	5.28	504	489	486	-

Standard is STANDARD R-2a/CSB/FA-10R.

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCl) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.  
 TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* & PD\*\* GROUP 3B BY FIRE ASSAY & ANALYSIS BY ICP-ES. (30 gm)  
 - SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA DATE RECEIVED: JUL 22 2005 DATE REPORT MAILED: Aug 5/05



All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	Ca %	P %	Cr %	Mg %	Al %	Na %	K %	W %	V %	Ti %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267092	<.001	.005	<.02	.01	<2	.136	.012	.17	9.24	<.02	<.01	<.001	<.01	<.01	1.70	<.01	.140	24.79	.11	.02	<.01	<.01	<.01	.02	.72	6	65	63	5.85
267093	<.001	.004	<.02	.01	<2	.191	.013	.21	9.96	<.02	<.01	<.001	<.01	<.01	1.42	<.01	.311	27.79	.15	.02	<.01	<.01	<.01	.02	.54	9	15	17	4.25
267094	<.001	.012	<.02	.01	<2	.266	.020	.15	10.12	<.02	<.01	<.001	<.01	<.01	3.19	<.01	.136	22.04	.14	.04	<.01	<.01	<.01	.02	2.03	3	12	16	5.65
267095	<.001	.037	<.02	<.01	<2	.093	.015	.14	9.69	<.02	<.01	<.001	<.01	<.01	6.09	<.01	.173	20.46	.26	.05	<.01	<.01	.01	.04	2.33	8	2	6	2.32
267096	<.001	.044	<.02	.01	<2	.126	.029	.15	13.98	<.02	<.01	<.001	<.01	<.01	6.12	<.01	.144	17.29	.21	.06	<.01	<.01	.01	.03	4.94	9	<2	5	3.75
RE 267096	<.001	.044	<.02	<.01	<2	.127	.029	.14	13.68	<.02	<.01	<.001	<.01	<.01	6.65	<.01	.143	18.99	.21	.06	<.01	<.01	.01	.03	4.88	10	4	11	-
RRE 267096	<.001	.044	<.02	<.01	<2	.126	.029	.15	14.04	<.02	<.01	<.001	<.01	<.01	6.34	<.01	.150	18.32	.21	.06	<.01	<.01	.01	.03	4.86	7	10	6	-
267097	<.001	.022	<.02	.01	<2	.077	.014	.15	9.94	<.02	<.01	<.001	<.01	<.01	6.47	<.01	.150	19.07	.30	.06	<.01	<.01	.01	.05	2.72	21	2	5	6.20
267098	<.001	.015	<.02	<.01	<2	.079	.012	.13	9.01	<.02	<.01	<.001	<.01	<.01	5.49	<.01	.128	16.27	.21	.04	<.01	<.01	.01	.04	2.59	27	6	3	3.10
267099	<.001	.016	<.02	<.01	<2	.113	.015	.15	10.71	<.02	<.01	<.001	<.01	<.01	6.59	<.01	.139	15.91	.44	.06	.01	<.01	.02	.08	3.08	9	4	8	3.14
267100 (pulp)	<.001	.101	<.02	<.01	4	.361	.016	.05	8.83	<.02	<.01	<.001	<.01	<.01	3.14	<.01	.356	15.75	2.74	.22	.05	<.01	.01	.14	1.14	29	90	384	-
.STD RTS-2	<.001	.068	<.02	.01	3	.268	.007	.04	32.55	<.02	<.01	<.001	<.01	.01	.52	<.01	.012	.36	.78	.19	.12	<.01	<.01	.16	18.90	-	-	-	-
267101	<.001	.019	<.02	.01	<2	.055	.008	.14	9.43	<.02	<.01	<.001	<.01	<.01	6.78	<.01	.136	14.98	.26	.06	<.01	<.01	.03	.05	2.11	2	3	6	4.30
267102	<.001	.016	<.02	<.01	<2	.072	.009	.13	11.01	<.02	<.01	<.001	<.01	<.01	5.66	<.01	.107	14.52	.56	.04	<.01	<.01	.03	.05	2.79	10	3	4	4.34
267103	.002	.020	<.02	<.01	<2	.072	.013	.12	14.43	<.02	<.01	<.001	<.01	<.01	7.38	<.01	.102	11.96	.27	.05	<.01	<.01	.04	.06	6.54	111	<2	3	4.07
267104	<.001	.017	<.02	<.01	<2	.049	.008	.18	10.01	<.02	<.01	<.001	<.01	<.01	6.46	<.01	.109	14.59	.44	.07	.01	<.01	.03	.10	2.97	5	<2	4	5.17
267105	<.001	.011	<.02	<.01	<2	.015	.005	.18	7.64	<.02	<.01	<.001	<.01	<.01	7.63	<.01	.080	12.58	.56	.22	.05	<.01	.05	.14	2.08	35	<2	3	5.28
267106	<.001	.014	<.02	<.01	<2	.030	.006	.17	8.06	<.02	<.01	<.001	<.01	<.01	7.94	<.01	.075	11.89	.53	.18	.03	<.01	.05	.14	2.52	5	2	<2	5.17
267107	<.001	.057	<.02	.01	<2	.106	.015	.11	11.56	<.02	<.01	<.001	<.01	<.01	8.91	<.01	.064	11.24	.57	.06	<.01	<.01	.05	.19	2.87	19	3	5	4.82
267108	<.001	.015	<.02	<.01	<2	.105	.008	.13	7.87	<.02	<.01	<.001	<.01	<.01	5.95	<.01	.097	16.31	.48	.05	.01	<.01	.04	.14	2.02	9	4	<2	5.12
267109	<.001	.018	<.02	.01	<2	.133	.013	.17	11.50	<.02	<.01	<.001	<.01	<.01	2.99	<.01	.138	15.51	.50	.13	.09	<.01	.02	.11	3.68	2	3	5	5.13
267110	<.001	.046	<.02	.01	<2	.087	.013	.16	12.10	<.02	<.01	<.001	<.01	<.01	2.04	<.01	.129	15.68	.56	.16	.22	<.01	.02	.11	4.08	3	11	6	3.79
STANDARD R-2a	.049	.583	1.65	4.24	164	.383	.049	.22	22.46	.22	.14	.029	.13	<.01	3.47	.08	.061	2.68	2.66	.48	.61	.11	.01	.18	5.30	483	481	474	-

Standard is STANDARD R-2a/CSB/FA-10R. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-72B File # A503750 Page 1

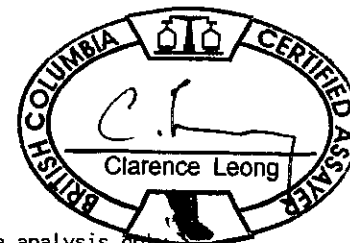
1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Chris Baldys



SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267062	.023	.268	.011	1.08
267063	.024	.238	.009	1.12
267064	.024	.228	.011	1.22
267065	.030	.168	.008	1.21
267066	.021	.197	.010	1.21
267067	.019	.190	.011	1.12
267068	.023	.226	.013	1.01
267069	.023	.277	.014	1.28
267070A	.033	.190	.011	1.13
267070B	.034	.193	.011	1.09
267071	.017	.195	.013	.97
267072	.020	.205	.015	1.23
267073	.031	.275	.017	1.66
267074	.032	.432	.037	2.30
267075 (pulp)	.060	.205	.008	.63
267076	.020	.228	.019	1.28
267077	.029	.227	.014	1.23
.STD RTS-2	.062	.238	.007	4.21
267078	.013	.194	.014	1.10
267079	.045	.179	.012	1.31
267080	.027	.229	.018	1.28
267081	.019	.334	.025	1.78
RE 267081	.019	.337	.025	1.78
RRE 267081	.019	.329	.024	1.69
267082	.011	.139	.008	.82
267083	.017	.115	.012	1.06
267084	.041	.130	.019	1.97
267085	.025	.099	.011	1.13
267086	.031	.111	.019	2.27
267087	.029	.105	.015	2.14
267088	.012	.060	.007	.89
267089	.018	.081	.012	1.51
267090 (rock)	.004	.002	<.001	.19
267091	.014	.078	.010	.87
STANDARD R-2a	.531	.328	.042	8.57

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
- SAMPLE TYPE: DRILL CORE R150  
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data 1 FA \_\_\_\_\_ DATE RECEIVED: JUL 22 2005 DATE REPORT MAILED: Aug 5/05





SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267092	.010	.084	.007	1.01
267093	.010	.091	.005	1.15
267094	.025	.235	.016	1.49
267095	.048	.083	.014	1.23
267096	.050	.113	.026	2.35
RE 267096	.043	.110	.026	2.38
RRE 267096	.041	.108	.025	2.11
267097	.022	.061	.011	1.25
267098	.015	.075	.011	1.04
267099	.018	.107	.014	1.62
267100 (pulp)	.095	.269	.012	1.44
.STD RTS-2	-	-	-	-
267101	.018	.052	.008	1.18
267102	.017	.067	.009	1.41
267103	.021	.067	.014	3.92
267104	.017	.044	.007	2.19
267105	.012	.014	.004	1.54
267106	.015	.027	.005	1.72
267107	.058	.104	.015	3.96
267108	.015	.098	.007	1.43
267109	.017	.121	.012	3.18
267110	.043	.078	.012	3.87
STANDARD R-2a	.528	.327	.044	9.03

Sample type: DRILL CORE R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



**Hard Creek Nickel Corporation PROJECT Tur C05-73A File # A503751 Page 1**  
 1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchins

SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	Ca %	P %	Cr %	Mg %	Al %	Na %	K %	W %	V %	Ti %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267111	.002	.025	<.02	.01	<2	.087	.014	.19	11.22	<.01	<.01	<.001	<.01	<.01	5.78	<.01	.146	15.82	.56	.16	.03	<.01	.04	.11	3.07	3	11	2	5.52
267112	.002	.037	<.02	.01	<2	.132	.014	.16	10.37	<.01	<.01	<.001	<.01	<.01	5.25	.01	.141	18.32	.45	.16	<.01	<.01	.04	.09	2.69	4	6	5	4.76
267113	.003	.056	<.02	.01	<2	.174	.022	.18	14.96	<.01	<.01	<.001	<.01	<.01	3.85	<.01	.138	15.38	.51	.15	<.01	<.01	.04	.10	5.09	6	5	15	6.18
267114	.001	.035	<.02	.01	<2	.147	.022	.17	14.84	<.01	<.01	<.001	<.01	<.01	1.71	.01	.114	21.19	.28	.34	<.01	<.01	.02	.05	4.31	13	27	13	4.44
267115	.001	.047	<.02	.01	<2	.170	.021	.19	14.06	<.01	<.01	<.001	<.01	<.01	1.73	<.01	.158	21.34	.52	<.01	.07	<.01	.02	.07	3.98	7	32	18	5.64
267116	<.001	.019	<.02	.01	<2	.123	.012	.18	9.72	<.01	.01	<.001	<.01	<.01	2.25	.04	.183	21.35	1.50	.45	.23	<.01	.02	.17	1.12	8	15	11	2.63
267117	.001	.049	<.02	.01	<2	.413	.023	.16	12.15	<.01	<.01	<.001	<.01	<.01	1.31	.01	.254	24.90	.26	.13	<.01	<.01	.01	.04	2.51	9	58	63	3.58
267118	.001	.037	<.02	.01	<2	.303	.023	.17	13.09	<.01	<.01	<.001	<.01	<.01	1.00	.01	.225	25.75	.19	.12	<.01	<.01	.01	.03	2.51	10	35	42	4.12
267119	.001	.028	<.02	.01	<2	.157	.020	.17	13.19	<.01	<.01	<.001	<.01	<.01	1.26	<.01	.181	26.09	.15	.05	<.01	<.01	.01	.03	2.18	8	4	10	4.40
267120 (rock)	<.001	.005	<.02	<.01	<2	.003	.002	.11	4.72	<.01	.05	<.001	<.01	<.01	4.72	.06	.003	2.01	8.80	2.77	1.28	<.01	.01	.35	.02	2	2	5	3.20
267121	.002	.023	<.02	.01	<2	.112	.016	.23	12.99	<.01	<.01	<.001	<.01	<.01	3.10	.01	.144	18.69	.43	.05	.01	<.01	.02	.08	2.81	3	2	2	5.46
267122	.002	.018	<.02	.01	<2	.129	.016	.19	12.73	<.01	<.01	<.001	<.01	.01	3.37	.01	.128	18.44	.43	.28	<.01	<.01	.03	.08	2.92	5	10	5	5.61
267123	<.001	.013	<.02	.01	<2	.041	.009	.16	7.22	<.01	<.01	<.001	<.01	<.01	12.36	.01	.181	14.03	.47	.15	<.01	<.01	.04	.11	1.40	3	2	2	3.20
267124	.006	.106	<.02	.01	<2	.223	.044	.15	24.41	<.01	<.01	<.001	<.01	<.01	5.03	<.01	.091	13.30	.26	.34	<.01	<.01	.03	.06	10.39	14	8	9	5.48
267125 (pulp)	<.001	.058	<.02	.01	<2	.247	.012	.12	9.41	<.01	<.01	<.001	<.01	<.01	4.67	<.01	.860	15.31	3.57	.27	.07	<.01	.02	.19	.52	32	116	300	-
267126	.001	.021	<.02	.01	<2	.031	.009	.17	9.59	<.01	.02	<.001	<.01	<.01	10.00	.03	.146	13.82	1.14	.32	.16	<.01	.03	.16	1.71	6	3	<2	4.67
.STD RTS-2	<.001	.076	<.02	.01	<2	.275	.007	.04	40.72	<.01	<.01	<.001	<.01	<.01	.65	.01	.013	.40	.82	.19	.11	<.01	.01	.18	19.07	-	-	-	-
267127	<.001	.019	<.02	.01	<2	.034	.011	.17	9.32	<.01	.02	<.001	<.01	<.01	9.45	.02	.147	13.64	1.26	.34	.40	<.01	.03	.13	1.80	2	<2	<2	5.45
267128	<.001	.024	<.02	.01	<2	.100	.011	.18	9.42	<.01	.04	<.001	<.01	<.01	8.27	.05	.171	13.40	2.47	.06	.96	<.01	.03	.24	1.44	3	18	9	5.80
267129	<.001	.059	<.02	.01	<2	.419	.018	.15	10.53	<.01	.01	<.001	<.01	<.01	3.50	.03	.195	18.99	1.88	.23	.69	<.01	.01	.10	1.69	4	53	58	4.08
267130A	<.001	.096	<.02	<.01	<2	.569	.021	.16	10.04	<.01	<.01	<.001	<.01	<.01	6.99	.01	.195	17.91	.91	<.01	.01	<.01	.01	.09	2.49	10	66	71	5.30
267130B	<.001	.097	<.02	.01	<2	.575	.020	.16	9.99	<.01	<.01	<.001	<.01	<.01	7.05	.02	.184	17.80	.95	.29	.01	<.01	.01	.09	2.54	10	67	64	-
267131	<.001	.043	<.02	<.01	<2	.133	.011	.14	6.68	<.01	.02	<.001	<.01	<.01	11.94	.01	.239	14.44	.96	<.01	.12	<.01	.02	.11	1.10	<2	<2	<2	5.91
267132	<.001	.014	<.02	.01	<2	.061	.009	.17	8.99	<.01	.10	<.001	<.01	<.01	9.47	.07	.141	13.74	3.22	.11	.84	<.01	.03	.28	.62	9	8	9	5.68
267133	<.001	.019	<.02	.01	<2	.063	.011	.18	9.36	<.01	.01	<.001	<.01	<.01	7.88	.02	.158	16.03	.98	.13	.10	<.01	.02	.13	1.35	36	9	6	4.75
267134	<.001	.015	<.02	.01	<2	.062	.009	.19	8.44	<.01	<.01	<.001	<.01	<.01	8.48	.01	.211	15.73	.46	.06	.02	<.01	.03	.11	1.18	2	10	3	5.20
RE 267134	<.001	.014	<.02	.01	<2	.059	.009	.19	8.46	<.01	<.01	<.001	<.01	<.01	8.58	<.01	.210	15.75	.46	<.01	.01	<.01	.03	.11	1.19	<2	7	4	-
RRE 267134	<.001	.014	<.02	.01	2	.063	.009	.19	8.47	<.01	<.01	<.001	<.01	<.01	8.47	.01	.208	15.61	.48	<.01	.08	<.01	.03	.11	1.25	2	3	5	-
267135	.002	.037	<.02	.01	<2	.071	.014	.17	11.11	<.01	<.01	<.001	<.01	<.01	9.22	<.01	.187	14.14	.46	<.01	.05	<.01	.04	.11	3.33	10	5	<2	6.06
267136	.004	.059	<.02	.01	<2	.132	.024	.16	18.46	<.01	<.01	<.001	<.01	<.01	5.22	<.01	.096	14.35	.35	<.01	<.01	<.01	.04	.09	7.52	7	2	11	5.97
267137	<.001	.012	<.02	.01	<2	.120	.008	.19	8.76	<.01	<.01	<.001	<.01	<.01	5.75	<.01	.141	18.25	.55	<.01	.04	<.01	.02	.09	1.05	2	16	11	4.90
267138	<.001	.008	<.02	.01	<2	.172	.009	.20	9.70	<.01	<.01	<.001	<.01	<.01	4.26	.04	.127	19.35	1.41	<.01	.02	<.01	.01	.15	.52	<2	9	24	5.20
267139	<.001	.003	<.02	.01	<2	.191	.010	.17	9.61	<.01	<.01	<.001	<.01	<.01	2.07	.02	.170	23.45	.61	<.01	<.01	<.01	.01	.08	.37	5	11	7	5.06
267140	<.001	.007	<.02	.01	<2	.184	.011	.16	11.51	<.01	<.01	<.001	<.01	<.01	.19	.01	.163	24.67	.19	<.01	<.01	<.01	.01	.04	.61	23	13	10	3.22
STANDARD R-2a	.052	.576	1.72	4.34	170	.386	.049	.25	26.80	.20	.17	.031	.13	<.01	3.88	.09	.066	2.69	2.68	.50	.70	.08	.02	.20	5.28	487	482	491	-

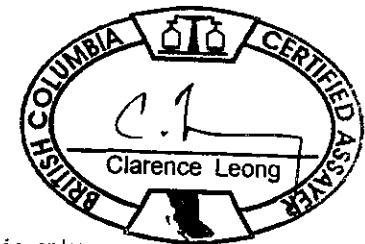
Standard is STANDARD R-2a/CSB/FA-10R.

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCL) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.  
 TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* & PD\*\* GROUP 3B BY FIRE ASSAY & ANALYSIS BY ICP-ES. (30 gm)  
 - SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

DATE RECEIVED: JUL 22 2005

DATE REPORT MAILED: Aug 5/05



All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	Ca %	P %	Cr %	Mg %	Al %	Na %	K %	W %	V %	Ti %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267141	<.001	.010	<.02	<.01	<2	.194	.011	.14	9.15	<.02	<.01	<.001	<.01	<.01	1.52	<.01	.135	20.24	.26	.01	<.01	<.01	.01	.05	.80	5	10	19	6.45
267142	<.001	.003	<.02	.01	<2	.207	.010	.17	8.70	<.02	<.01	<.001	<.01	<.01	.36	<.01	.193	24.71	.18	<.01	<.01	<.01	.01	.04	.24	<2	7	8	5.35
267143	<.001	.007	<.02	.01	<2	.255	.011	.17	9.03	<.02	<.01	<.001	<.01	<.01	1.69	<.01	.156	21.55	.26	.01	<.01	<.01	.01	.05	.41	<2	43	53	5.34
.STD RTS-2	<.001	.072	<.02	.01	5	.276	.007	.04	38.26	<.02	<.01	<.001	<.01	.02	.66	.01	.013	.41	.90	.23	.13	<.01	<.01	.18	18.90	-	-	-	-
267144	<.001	.004	<.02	.01	<2	.228	.009	.15	8.51	<.02	<.01	<.001	<.01	<.01	1.81	<.01	.154	22.07	.26	.01	<.01	<.01	.01	.06	.28	<2	55	41	5.87
267145	<.001	.006	<.02	.01	3	.217	.010	.16	8.96	<.02	<.01	<.001	<.01	<.01	2.07	.01	.172	21.15	.72	.01	.01	<.01	.01	.08	.36	15	18	54	4.01
267146	<.001	.054	<.02	.01	<2	.426	.018	.16	10.86	<.02	<.01	<.001	<.01	<.01	1.05	<.01	.230	19.67	.28	.01	<.01	<.01	.01	.06	2.60	20	154	159	4.85
STANDARD R-2a/CSB/FA-10R	.051	.565	1.69	4.28	164	.389	.046	.23	22.84	.23	.16	.030	.14	<.01	3.85	.08	.063	2.69	2.72	.48	.62	.14	.01	.19	5.32	475	478	477	-

Sample type: DRILL CORE R150.

ASSAY CERTIFICATE



Hard Creek Nickel Corporation PROJECT Tur C05-73A File # A503751 Page 1

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens



SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267111	.026	.084	.012	3.34
267112	.038	.132	.012	2.83
267113	.058	.186	.022	5.58
267114	.036	.138	.019	2.85
267115	.047	.155	.018	2.58
267116	.019	.107	.009	1.02
267117	.050	.381	.019	1.81
267118	.038	.290	.020	1.99
267119	.027	.138	.016	1.73
267120 (rock)	.005	.002	<.001	.23
267121	.022	.106	.014	3.11
267122	.019	.113	.014	3.62
267123	.015	.041	.008	1.63
267124	.106	.226	.044	8.57
267125 (pulp)	.058	.199	.007	.63
267126	.022	.031	.007	1.52
.STD RTS-2	.061	.232	.007	4.61
267127	.019	.030	.007	1.72
267128	.023	.094	.008	1.24
267129	.058	.399	.016	1.60
267130A	.094	.590	.019	2.01
267130B	.092	.580	.019	2.02
267131	.044	.138	.008	1.04
267132	.016	.059	.006	.56
267133	.019	.058	.008	1.31
267134	.016	.057	.007	1.27
RE 267134	.016	.058	.007	1.20
RRE 267134	.016	.057	.007	1.25
267135	.039	.070	.012	3.36
267136	.057	.126	.024	7.90
267137	.013	.106	.006	1.28
267138	.008	.146	.007	.66
267139	.004	.185	.009	.44
267140	.007	.180	.009	.50
STANDARD R-2a	.551	.330	.044	8.73

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
 - SAMPLE TYPE: DRILL CORE R150  
 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data h FA \_\_\_\_\_ DATE RECEIVED: JUL 22 2005 DATE REPORT MAILED: Aug 5/05





SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267141	.011	.204	.011	.60
267142	.003	.188	.009	.49
267143	.008	.235	.009	.51
.STD RTS-2	-	-	-	-
267144	.005	.221	.009	.34
267145	.007	.196	.008	.68
267146	.054	.396	.018	2.52
STANDARD R-2a	.530	.327	.044	9.03

Sample type: DRILL CORE R150.



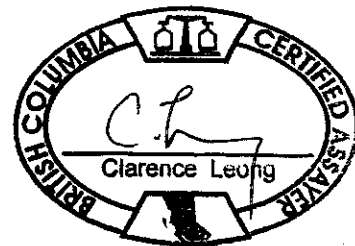


**Hard Creek Nickel Corporation PROJECT Tur C05-73B File # A504243 Page 1**  
 1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens

SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267147	<.001	.010	<.02	<.01	<2	.152	.009	.15	9.31	<.02	<.01	<.001	<.01	<.01	.02	4.05	<.01	.103	17.80	.08	.31	.02	.01	<.01	.70	2	6	2	5.80
267148	.001	.022	<.02	<.01	<2	.231	.012	.16	8.47	<.02	<.01	<.001	<.01	<.01	.02	4.19	<.01	.098	16.92	.09	.50	.03	.01	<.01	1.73	9	23	23	5.83
267149	<.001	.007	<.02	.01	<2	.207	.008	.16	6.37	<.02	<.01	<.001	<.01	<.01	.01	3.60	<.01	.065	18.05	.09	.75	.03	.01	<.01	.29	<2	7	5	5.17
267150 (pulp)	<.001	.058	<.02	.01	<2	.239	.010	.11	9.07	<.02	<.01	<.001	<.01	<.01	.02	4.55	<.01	.706	13.20	.19	3.84	.33	.11	<.01	.56	22	98	324	-
267151	<.001	.004	<.02	.01	<2	.199	.009	.12	8.22	<.02	<.01	<.001	<.01	<.01	.01	1.57	<.01	.122	20.55	.05	.26	<.01	<.01	<.01	.22	<2	7	5	4.56
267152	<.001	.014	<.02	.01	<2	.244	.011	.14	7.42	<.02	<.01	<.001	<.01	<.01	.01	1.78	<.01	.115	19.61	.07	.42	.01	.01	<.01	.55	4	12	19	4.83
267153	<.001	.003	<.02	.01	<2	.232	.010	.10	7.04	<.02	<.01	<.001	<.01	<.01	.01	1.48	<.01	.103	20.92	.05	.40	<.01	<.01	<.01	.26	5	6	3	5.69
267154	<.001	.004	<.02	.01	<2	.208	.009	.14	7.07	<.02	<.01	<.001	<.01	<.01	.01	1.54	<.01	.101	20.40	.06	.44	<.01	<.01	<.01	.24	2	7	8	4.31
267155	<.001	.002	<.02	.01	<2	.213	.009	.14	7.95	<.02	<.01	<.001	<.01	<.01	.01	.90	<.01	.100	20.26	.05	.33	<.01	<.01	<.01	.19	<2	7	8	5.54
267156	<.001	.005	<.02	.01	<2	.175	.008	.19	8.92	<.02	<.01	<.001	<.01	<.01	.01	2.08	<.01	.088	18.70	.08	.44	.01	.01	<.01	.41	2	7	5	4.90
267157	.001	.047	<.02	.01	<2	.132	.012	.19	12.26	<.02	<.01	<.001	<.01	<.01	.04	5.64	<.01	.076	12.71	.15	.55	.19	.05	<.01	3.96	5	11	15	5.46
267158	<.001	.020	<.02	.01	<2	.036	.007	.19	10.01	<.02	<.01	<.001	<.01	<.01	.04	8.11	<.01	.092	11.49	.25	1.10	.25	.15	<.01	3.03	2	4	6	4.76
267159	.001	.021	<.02	.01	<2	.043	.008	.16	9.10	<.02	<.01	<.001	<.01	<.01	.04	7.73	<.01	.149	12.43	.28	1.28	.30	.14	<.01	2.62	4	2	3	5.50
267160A	<.001	.026	<.02	<.01	<2	.042	.008	.16	8.79	<.02	<.01	<.001	<.01	<.01	.04	7.69	<.01	.144	12.25	.14	.68	.24	.05	<.01	2.80	2	3	3	5.62
267160B	<.001	.026	<.02	.01	<2	.044	.008	.17	9.00	<.02	<.01	<.001	<.01	<.01	.04	7.86	<.01	.152	12.51	.14	.70	.24	.05	<.01	2.84	3	<2	3	-
267161	<.001	.012	<.02	.01	<2	.075	.008	.16	8.81	<.02	.02	<.001	<.01	<.01	.03	5.48	.03	.105	12.31	.21	2.48	.48	.95	<.01	1.19	3	7	10	4.06
267162	<.001	.018	<.02	<.01	<2	.065	.007	.15	7.86	<.02	<.01	<.001	<.01	<.01	.03	6.90	<.01	.168	13.84	.17	.96	.21	.12	<.01	1.73	<2	5	<2	5.58
.STD RTS-2	.001	.073	<.02	.01	<2	.267	.007	.04	38.81	<.02	<.01	<.002	<.01	<.01	.01	.57	.01	.012	.35	.17	.82	.21	.12	<.01	18.68	-	-	-	-
267163	<.001	.012	<.02	.01	<2	.120	.009	.15	8.52	<.02	<.01	<.001	<.01	<.01	.02	3.12	<.01	.106	16.75	.15	.87	.13	.14	<.01	1.07	<2	4	11	4.53
267164	<.001	.017	<.02	.01	<2	.121	.010	.14	8.72	<.02	<.01	<.001	<.01	<.01	.02	3.31	<.01	.110	17.02	.13	.78	.09	.13	<.01	1.29	<2	4	5	5.41
267165	<.001	.018	<.02	.01	<2	.090	.009	.15	8.65	<.02	<.01	<.001	<.01	<.01	.02	4.47	<.01	.110	15.62	.11	.67	.11	.06	<.01	1.46	3	2	<2	4.13
267166	<.001	.016	<.02	<.01	<2	.090	.010	.15	9.23	<.02	<.01	<.001	<.01	<.01	.02	6.42	<.01	.130	15.54	.12	.59	.07	.02	<.01	1.58	<2	6	9	4.90
267167	<.001	.010	<.02	.02	<2	.137	.010	.14	8.97	<.02	<.01	<.001	<.01	<.01	.01	2.02	<.01	.129	19.02	.10	.71	.01	.07	<.01	.74	5	2	2	5.49
267168	<.001	.009	<.02	.01	<2	.156	.011	.11	8.05	<.02	<.01	<.001	<.01	<.01	.01	.48	<.01	.134	19.44	.14	1.07	.01	.18	<.01	.71	<2	<2	<2	4.10
267169	<.001	.016	<.02	.01	<2	.114	.009	.14	7.42	<.02	<.01	<.001	<.01	<.01	.02	5.08	<.01	.143	16.31	.12	.95	.04	.06	<.01	1.25	<2	7	11	2.10
RE 267169	<.001	.017	<.02	.01	<2	.116	.010	.14	7.45	<.02	<.01	<.001	<.01	<.01	.02	4.92	<.01	.132	16.48	.12	.95	.04	.06	<.01	1.23	2	6	5	-
RRE 267169	<.001	.019	<.02	.01	<2	.118	.010	.14	7.49	<.02	<.01	<.001	<.01	<.01	.02	5.01	.01	.132	16.66	.12	.98	.04	.06	<.01	1.28	<2	3	6	-
267170	<.001	.020	<.02	.01	<2	.126	.009	.15	8.38	<.02	<.01	<.001	<.01	<.01	.02	4.15	<.01	.124	16.19	.11	.98	.06	.05	<.01	1.58	2	6	7	3.62
267171	<.001	.006	<.02	.01	<2	.164	.009	.12	7.80	<.02	<.01	<.001	<.01	<.01	.01	2.32	<.01	.120	19.37	.09	.73	.02	.10	<.01	.65	2	3	2	4.34
267172	<.001	.004	<.02	.01	<2	.170	.009	.12	7.32	<.02	<.01	<.001	<.01	<.01	.01	1.93	<.01	.113	19.02	.11	.88	.02	.17	<.01	.47	12	4	5	4.24
267173	<.001	.004	<.02	.01	<2	.131	.008	.13	7.22	<.02	<.01	<.001	<.01	<.01	.01	2.34	<.01	.103	18.30	.11	.90	.04	.07	<.01	.41	9	<2	8	3.40
267174	<.001	.005	<.02	.02	<2	.147	.008	.14	7.73	<.02	<.01	<.001	<.01	<.01	.01	2.06	<.01	.117	18.22	.08	.74	.08	.03	<.01	.51	<2	<2	6	4.20
267175 (pulp)	<.001	.058	<.02	.02	<2	.238	.011	.11	9.35	<.02	<.01	<.001	<.01	<.01	.02	4.20	<.01	.823	13.55	.20	4.00	.34	.11	<.01	.53	15	94	321	-
267176	<.001	.005	<.02	.01	<2	.136	.008	.15	7.88	<.02	<.01	<.001	<.01	<.01	.02	2.22	<.01	.130	17.49	.09	.72	.12	.03	<.01	.55	<2	<2	<2	5.90
STANDARD R-2a	.049	.577	1.56	4.14	160	.385	.043	.24	25.54	.23	.13	.029	.13	<.01	.02	3.59	.08	.058	2.59	.19	2.83	.50	.64	.07	5.41	487	488	471	-

Standard is STANDARD R-2a/CSB/FA-10R.

GROUP 7D - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCl) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.  
 TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B BY FIRE ASSAY & ANALYSIS BY ICP. (30 gm)  
 - SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data by FA \_\_\_\_\_ DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Aug 25/05



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267177	<.001	.005	<.02	.02	<2	.124	.010	.15	8.05	<.02	.02	<.001	<.01	<.01	.02	2.83	.02	.122	15.97	.11	1.30	.23	.27	<.01	.74	4	1	4	4.32
267178	.001	.012	<.02	.01	<2	.021	.004	.15	7.42	<.02	.08	<.001	<.01	<.01	.03	5.52	.11	.052	6.51	.34	6.36	1.97	1.93	<.01	.40	3	5	5	4.82
267179	.001	.012	<.02	.01	3	.077	.008	.16	7.38	<.02	.01	<.001	<.01	<.01	.03	5.79	.02	.130	13.07	.16	1.47	.23	.50	<.01	1.25	2	3	3	5.03
267180 (rock)	.001	.004	<.02	.01	<2	.001	.001	.09	4.29	<.02	.05	<.001	<.01	<.01	.01	4.07	.06	.001	1.68	.28	8.52	2.31	1.23	<.01	.01	<1	1	3	2.69
267181	.001	.023	<.02	.01	<2	.097	.010	.17	10.27	<.02	<.01	<.001	<.01	<.01	.03	4.24	.02	.096	12.85	.15	1.32	.42	.24	<.01	2.83	10	3	6	4.06
267182	.001	.007	<.02	.01	<2	.109	.007	.16	8.23	<.02	<.01	<.001	<.01	<.01	.02	2.91	<.01	.095	15.46	.13	.94	.22	.08	<.01	.98	<1	2	2	5.01
267183	.001	.010	<.02	.01	<2	.094	.007	.16	8.10	<.02	<.01	<.001	<.01	<.01	.02	3.22	<.01	.120	14.70	.10	.92	.21	.17	<.01	1.19	1	<1	1	5.71
267184	<.001	.010	<.02	.01	<2	.078	.007	.16	7.81	<.02	<.01	<.001	<.01	<.01	.02	3.72	<.01	.125	15.11	.10	.83	.18	.07	<.01	1.04	1	3	7	3.25
267185	.001	.015	<.02	.01	<2	.106	.009	.15	8.70	<.02	<.01	<.001	<.01	<.01	.02	3.97	.01	.135	14.66	.11	.95	.20	.06	<.01	1.88	3	9	15	4.83
.STD RTS-2	.001	.072	<.02	.01	<2	.279	.006	.04	37.92	<.02	<.01	.002	<.01	<.01	.01	.55	.01	.011	.36	.16	.83	.22	.13	<.01	18.53	-	-	-	-
267186	<.001	.005	<.02	.01	<2	.096	.006	.16	7.43	<.02	<.01	<.001	<.01	<.01	.02	3.38	<.01	.115	15.36	.13	1.00	.21	.07	<.01	.60	<1	4	6	3.05
267187	<.001	.009	<.02	.01	<2	.088	.007	.16	7.62	<.02	<.01	<.001	<.01	<.01	.03	4.53	<.01	.106	14.46	.12	.93	.19	.12	<.01	1.11	2	5	4	4.11
RE 267187	<.001	.008	<.02	<.01	<2	.087	.007	.16	7.62	<.02	<.01	<.001	<.01	<.01	.03	4.64	<.01	.109	14.48	.12	.93	.19	.12	<.01	1.16	<1	<1	<1	-
RRE 267187	<.001	.008	<.02	<.01	<2	.089	.006	.16	7.66	<.02	<.01	<.001	<.01	<.01	.02	4.46	<.01	.111	14.66	.12	.91	.19	.11	<.01	1.07	1	3	8	-
267188	.001	.029	<.02	.01	<2	.063	.009	.17	10.76	<.02	<.01	<.001	<.01	<.01	.03	4.71	<.01	.117	13.24	.11	.68	.15	.05	<.01	3.35	9	3	8	5.49
267189	<.001	.013	<.02	.01	<2	.088	.008	.15	8.89	<.02	<.01	<.001	<.01	<.01	.02	1.68	.01	.156	17.33	.08	.85	.10	.05	<.01	1.19	1	<1	3	5.04
267190A	<.001	.010	<.02	.02	<2	.075	.012	.15	9.11	<.02	<.01	<.001	<.01	<.01	.02	1.66	.02	.198	17.36	.08	.95	.10	.06	<.01	.96	<1	1	1	4.76
267190B	<.001	.009	<.02	.01	<2	.075	.010	.15	9.09	<.02	<.01	<.001	<.01	<.01	.02	1.62	.02	.182	17.17	.08	.94	.10	.06	<.01	1.00	1	<1	<1	-
267191	<.001	.010	<.02	.01	<2	.113	.009	.14	8.22	<.02	<.01	<.001	<.01	<.01	.01	2.26	.01	.130	16.59	.11	1.35	.17	.07	<.01	1.05	1	2	1	4.89
STANDARD R-2a	.048	.575	1.58	4.34	161	.388	.047	.23	24.49	.22	.14	.030	.14	<.01	.01	3.24	.08	.053	2.51	.18	2.76	.51	.65	.07	5.32	479	489	482	-

Standard is STANDARD R-2a/CSB/FA-10R. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE

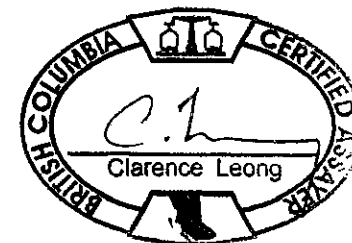


Hard Creek Nickel Corporation PROJECT Tur C05-73B File # A504243 Page 1  
 1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchins

SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267147	.016	.144	.009	.54
267148	.025	.208	.012	1.53
267149	.009	.178	.007	.56
267150 (pulp)	.060	.198	.008	.79
267151	.006	.193	.009	.29
267152	.015	.223	.010	.73
267153	.005	.222	.010	.33
267154	.006	.185	.008	.30
267155	.003	.188	.008	.28
267156	.006	.142	.006	.46
267157	.048	.127	.013	3.51
267158	.021	.032	.007	2.25
267159	.020	.036	.008	2.19
267160A	.027	.039	.008	2.81
267160B	.025	.038	.008	2.60
267161	.013	.064	.006	.78
267162	.017	.054	.007	1.33
.STD RTS-2	.057	.217	.007	3.56
267163	.012	.102	.007	.90
267164	.017	.108	.009	1.01
267165	.018	.084	.008	1.35
267166	.016	.086	.010	1.22
267167	.010	.131	.010	.89
267168	.009	.141	.010	.80
267169	.016	.111	.009	1.22
RE 267169	.017	.113	.010	1.16
RRE 267169	.018	.120	.010	1.54
267170	.020	.123	.009	1.51
267171	.007	.150	.008	.62
267172	.004	.152	.007	.57
267173	.004	.109	.006	.60
267174	.005	.127	.006	.70
267175 (pulp)	.060	.206	.008	.69
267176	.005	.106	.006	.56
STANDARD R-2a	.514	.331	.041	8.54

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
 - SAMPLE TYPE: DRILL CORE R150  
 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data 6 FA \_\_\_\_\_ DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Sept. 3/05





SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267177	.009	.106	.008	.75
267178	.016	.015	.002	.53
267179	.013	.067	.007	.84
267180 (rock)	.006	.001<	.001	.10
267181	.023	.083	.010	2.09
267182	.008	.090	.006	.78
267183	.011	.078	.006	.85
267184	.012	.063	.005	.89
267185	.016	.086	.008	1.33
.STD RTS-2	.056	.217	.007	3.74
267186	.007	.069	.005	.62
267187	.009	.067	.005	.88
RE 267187	.009	.066	.005	.86
RRE 267187	.009	.067	.005	.87
267188	.029	.056	.009	3.23
267189	.013	.073	.007	1.11
267190A	.011	.064	.009	.88
267190B	.010	.062	.008	.77
267191	.011	.096	.007	.97
STANDARD R-2a	.515	.330	.041	8.46

Sample type: DRILL CORE R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-74A File # A504242 Page 1

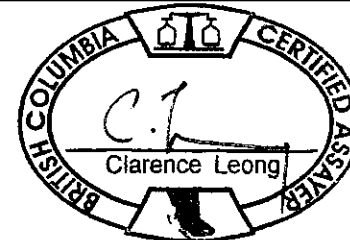
1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267192	<.001	.058	<.02	<.01	<2	.354	.023	.16	9.73	<.02	<.01	<.001	<.01	<.01	.01	.16	<.01	.223	23.43	.01	.13	.02	.02	<.01	1.46	11	46	59	2.73
267193	<.001	.001	<.02	<.01	<2	.006	.003	.16	7.52	<.02	.20	<.001	<.01	<.01	.03	13.39	.16	.005	3.99	.47	10.50	.05	.15	<.01	<.02	6	6	5	.45
267194	.001	.064	<.02	<.01	<2	.252	.026	.11	11.99	<.02	<.01	<.001	<.01	<.01	.01	.53	<.01	.220	20.72	.04	.57	.02	.01	<.01	1.76	18	40	51	4.11
267195	<.001	.029	<.02	<.01	<2	.179	.015	.13	9.04	<.02	<.01	<.001	<.01	<.01	.01	1.20	<.01	.151	21.25	.02	.20	.01	<.01	<.01	1.12	12	23	20	3.72
267196	<.001	.018	<.02	<.01	<2	.135	.012	.14	8.08	<.02	<.01	<.001	<.01	<.01	.01	1.07	<.01	.185	22.67	.02	.15	.01	<.01	<.01	.45	14	2	7	4.93
267197	<.001	.014	<.02	<.01	<2	.111	.013	.15	7.97	<.02	<.01	<.001	<.01	<.01	.01	2.24	<.01	.176	22.10	.05	.43	.02	<.01	<.01	.52	10	16	12	5.27
267198	<.001	.011	<.02	<.01	<2	.108	.010	.11	7.79	<.02	<.01	<.001	<.01	<.01	.01	3.47	<.01	.165	19.63	.05	.53	.03	<.01	<.01	.49	6	12	12	4.15
267199	<.001	.016	<.02	<.01	<2	.128	.011	.08	6.42	<.02	<.01	<.001	<.01	<.01	.01	3.21	<.01	.148	20.26	.04	.28	.03	<.01	<.01	.72	7	18	17	1.88
267200 (pulp)	<.001	.059	<.02	.01	<2	.223	.012	.10	8.36	<.02	<.01	<.001	<.01	<.01	.02	4.48	<.01	.898	13.93	.18	3.90	.32	.12	<.01	.53	20	73	302	-
267201	<.001	.012	<.02	<.01	2	.120	.009	.07	8.03	<.02	<.01	<.001	<.01	<.01	.01	1.76	<.01	.187	20.72	.03	.25	.02	<.01	<.01	.57	6	13	10	1.98
267202	<.001	.018	<.02	<.01	<2	.114	.011	.07	8.25	<.02	<.01	<.001	<.01	<.01	.01	2.26	<.01	.175	20.58	.03	.22	.02	<.01	<.01	.68	9	3	17	3.63
267203	<.001	.013	<.02	<.01	<2	.120	.011	.08	8.21	<.02	<.01	<.001	<.01	<.01	.01	3.33	<.01	.175	19.77	.03	.25	.03	<.01	<.01	.74	9	14	16	1.78
267204	.001	.017	<.02	.01	<2	.161	.009	.10	6.34	<.02	<.01	<.001	<.01	<.01	.01	5.57	<.01	.112	18.14	.05	.39	.02	.01	<.01	.95	7	24	21	4.89
267205	.001	.026	<.02	<.01	<2	.205	.009	.07	7.50	<.02	<.01	<.001	<.01	<.01	.01	.92	<.01	.124	21.37	.03	.41	.01	<.01	<.01	1.40	7	6	19	3.02
267206	<.001	.013	<.02	<.01	<2	.198	.006	.09	5.29	<.02	<.01	<.001	<.01	<.01	.01	2.73	<.01	.086	20.62	.05	.57	.01	<.01	<.01	.59	2	5	4	3.17
RE 267206	<.001	.013	<.02	<.01	<2	.200	.006	.09	5.37	<.02	<.01	<.001	<.01	<.01	.01	2.71	<.01	.083	20.88	.05	.57	.01	<.01	<.01	.60	6	7	4	-
RRE 267206	<.001	.014	<.02	<.01	<2	.202	.006	.09	5.33	<.02	<.01	<.001	<.01	<.01	.01	2.81	<.01	.086	20.81	.05	.57	.01	<.01	<.01	.61	4	<2	4	-
267207	.001	.034	<.02	.01	<2	.263	.012	.13	9.45	<.02	<.01	<.001	<.01	<.01	.02	2.70	.02	.095	17.53	.10	1.25	.04	.04	<.01	2.66	6	20	21	4.01
.STD RTS-2	<.001	.072	<.02	.01	2	.272	.007	.04	38.09	<.02	<.01	<.001	<.01	<.01	.01	.58	<.01	.012	.38	.18	.88	.22	.13	<.01	19.03	-	-	-	-
267208	.001	.016	<.02	.01	<2	.211	.009	.12	7.23	<.02	<.01	<.001	<.01	<.01	.01	.91	<.01	.087	19.75	.06	.72	.03	.09	<.01	1.51	5	9	8	4.51
267209	<.001	.013	<.02	<.01	<2	.182	.009	.14	7.21	<.02	<.01	<.001	<.01	<.01	.01	2.10	<.01	.078	18.72	.08	.75	.06	.05	<.01	1.35	<2	15	11	4.03
267210 (rock)	<.001	.006	<.02	<.01	<2	.008	.002	.10	4.40	<.02	.05	<.001	<.01	<.01	.01	4.30	.06	.003	2.12	.31	9.13	2.41	1.23	<.01	.07	<2	<2	<2	2.82
267211	.001	.008	<.02	.01	<2	.173	.009	.14	6.99	<.02	<.01	<.001	<.01	<.01	.02	1.57	<.01	.072	19.23	.09	.79	.06	.04	<.01	1.16	2	<2	5	3.34
267212	.002	.026	<.02	.01	<2	.153	.010	.14	9.78	<.02	<.01	<.001	<.01	<.01	.02	1.88	<.01	.086	17.96	.08	.74	.07	.12	<.01	2.77	9	8	15	5.63
267213	.005	.033	<.02	.01	<2	.125	.012	.13	12.37	<.02	<.01	<.001	<.01	<.01	.04	6.39	<.01	.171	13.17	.07	.44	.12	.04	<.01	5.48	4	10	12	5.21
267214	<.001	.002	<.02	<.01	<2	.179	.008	.12	5.51	<.02	<.01	<.001	<.01	<.01	.01	1.40	<.01	.068	19.41	.10	.80	.06	.15	<.01	.42	4	11	3	3.11
267215	.002	.019	<.02	.01	<2	.104	.011	.12	11.43	<.02	<.01	<.001	<.01	<.01	.02	3.63	.01	.116	16.26	.09	.91	.06	.62	<.01	3.83	3	8	9	3.49
267216	<.001	.008	<.02	.01	<2	.152	.009	.10	6.90	<.02	<.01	<.001	<.01	<.01	.01	.87	<.01	.093	19.42	.08	.92	.04	.29	<.01	1.23	2	3	6	2.32
267217	.002	.025	<.02	.01	<2	.162	.012	.13	10.38	<.02	<.01	<.001	<.01	<.01	.03	2.01	<.01	.095	17.53	.08	.73	.06	.15	<.01	3.35	3	10	10	2.47
267218	.002	.013	<.02	.01	<2	.029	.007	.12	6.93	<.02	<.01	<.001	<.01	<.01	.04	11.59	<.01	.214	11.48	.11	.57	.15	.03	<.01	2.32	4	3	4	5.01
267219	.003	.020	<.02	<.01	<2	.056	.010	.12	9.01	<.02	.02	<.001	<.01	<.01	.03	10.97	.02	.207	10.87	.12	1.35	.36	.23	<.01	3.28	4	7	9	4.12
267220A	<.001	.010	<.02	.01	<2	.088	.013	.10	7.95	<.02	<.01	<.001	<.01	<.01	.01	3.59	<.01	.182	20.43	.03	.23	.03	.01	<.01	1.43	3	7	9	4.77
267220B	<.001	.010	<.02	.01	<2	.086	.013	.11	8.10	<.02	<.01	<.001	<.01	<.01	.01	3.77	<.01	.188	20.59	.04	.24	.03	<.01	<.01	1.44	<2	3	4	-
267221	<.001	.034	<.02	.01	<2	.159	.029	.14	13.81	<.02	<.01	<.001	<.01	<.01	.01	1.48	<.01	.147	22.59	.02	.11	.02	<.01	<.01	3.85	<2	2	<2	4.53
STANDARD R-2a	.048	.587	1.58	4.32	166	.384	.045	.25	24.88	.23	.15	.030	.13	<.01	.02	3.62	.08	.062	2.71	.19	2.96	.53	.65	.09	5.00	486	477	481	-

Standard is STANDARD R-2a/CSB/FA-10R.

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCl) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.  
 TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B BY FIRE ASSAY & ANALYSIS BY ICP. (30 gm)  
 - SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data FA DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Aug 15/05



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267222	.001	.026	<.02	.01	<2	.156	.026	.13	12.79	<.02	<.01	<.001	<.01	<.01	.01	2.29	<.01	.151	21.49	.03	.16	.03	.01	<.01	3.51	5	3	5	5.24
267223	.001	.034	<.02	.01	<2	.159	.029	.13	12.87	<.02	<.01	<.001	<.01	<.01	.01	2.00	<.01	.156	21.87	.02	.12	.02	<.01	<.01	4.54	6	2	9	2.56
267224	.001	.010	<.02	.01	<2	.092	.011	.13	7.96	<.02	.02	<.001	<.01	<.01	.01	2.71	.03	.083	15.96	.11	2.74	1.00	.44	<.01	1.04	2	11	2	5.13
267225 (pulp)	.001	.099	<.02	.01	<2	.351	.016	.05	9.25	<.02	<.01	<.001	<.01	<.01	.01	3.27	<.01	.346	14.90	.15	2.90	.24	.05	<.01	1.09	30	96	368	-
267226	.001	.020	<.02	.01	<2	.131	.016	.13	9.41	<.02	.02	<.001	<.01	<.01	.01	3.07	.02	.080	16.73	.08	2.05	.90	.28	<.01	1.91	52	<2	<2	4.54
267227	.001	.011	<.02	.01	<2	.199	.012	.11	7.88	<.02	<.01	<.001	<.01	<.01	.01	.73	<.01	.092	22.81	.02	.10	.01	<.01	<.01	1.52	52	2	5	5.08
267228	.001	.014	<.02	.01	<2	.147	.015	.09	9.62	<.02	<.01	<.001	<.01	<.01	.01	2.71	<.01	.150	19.77	.03	.17	.01	<.01	<.01	1.73	7	<2	3	2.43
.STD RTS-2	.001	.073	<.02	.02	<2	.273	.007	.04	37.98	<.02	<.01	<.001	<.01	<.01	.01	.58	.01	.012	.38	.17	.87	.22	.14	<.01	18.76	-	-	-	-
267229	.001	.016	<.02	<.01	<2	.141	.016	.09	9.64	<.02	<.01	<.001	<.01	<.01	.01	3.74	<.01	.211	19.27	.03	.21	.04	<.01	<.01	2.41	10	63	12	3.37
267230	.001	.017	<.02	.01	<2	.068	.014	.12	7.83	<.02	<.01	<.001	<.01	<.01	.03	11.99	<.01	.286	12.22	.08	.46	.13	.01	<.01	2.57	8	8	14	3.56
267231	.003	.021	<.02	.01	<2	.059	.011	.15	9.20	<.02	.02	<.001	<.01	<.01	.02	8.50	.04	.143	11.11	.15	2.06	1.00	.96	<.01	2.30	8	2	10	3.04
267232	.001	.015	<.02	.01	<2	.161	.011	.14	7.59	<.02	.03	<.001	<.01	<.01	.01	5.15	<.01	.163	16.46	.03	.92	.18	.71	<.01	1.71	44	18	13	4.37
RE 267232	.001	.016	<.02	.01	<2	.163	.011	.14	7.59	<.02	.03	<.001	<.01	<.01	.01	5.18	.01	.167	16.77	.03	.92	.18	.72	<.01	1.72	41	13	14	-
RRE 267232	.001	.016	<.02	.01	<2	.166	.012	.14	7.47	<.02	.03	<.001	<.01	<.01	.01	5.30	.01	.164	16.48	.04	.94	.19	.73	<.01	1.73	55	18	14	-
267233	.001	.014	<.02	<.01	<2	.192	.013	.10	8.92	<.02	<.01	<.001	<.01	<.01	.01	1.38	<.01	.162	21.26	.02	.11	.01	<.01	<.01	.96	44	4	4	4.38
STANDARD R-2a	.048	.571	1.57	4.32	162	.382	.046	.24	24.61	.22	.15	.030	.14	<.01	.02	3.59	.08	.062	2.68	.19	2.93	.52	.65	.11	5.08	491	480	475	-

Standard is STANDARD R-2a/CSB/FA-10R. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

## ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-74A File # A504242 Page 1

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchins

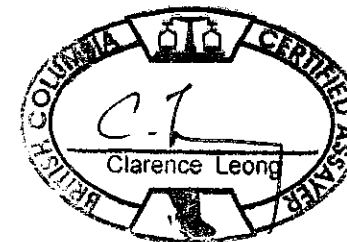


SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267192	.053	.314	.021	1.32
267193	.002	.001	<.001	.35
267194	.056	.247	.025	1.07
267195	.023	.176	.014	.63
267196	.014	.116	.010	.45
267197	.011	.096	.010	.64
267198	.009	.099	.009	.38
267199	.013	.119	.010	.43
267200 (pulp)	.056	.187	.007	.53
267201	.009	.115	.008	.38
267202	.013	.104	.010	.35
267203	.009	.111	.010	.31
267204	.015	.156	.008	.67
267205	.022	.189	.009	.70
267206	.011	.184	.006	.45
RE 267206	.012	.185	.006	.43
RRE 267206	.013	.191	.006	.50
267207	.033	.250	.011	2.16
.STD RTS-2	.060	.233	.007	4.40
267208	.014	.194	.008	1.51
267209	.012	.171	.008	1.16
267210 (rock)	.004	.007	.001	.23
267211	.007	.152	.007	1.17
267212	.024	.133	.009	2.63
267213	.031	.112	.012	4.05
267214	.002	.135	.006	.44
267215	.018	.081	.009	1.97
267216	.006	.110	.007	.76
267217	.023	.126	.010	2.37
267218	.011	.025	.006	1.73
267219	.020	.049	.009	2.15
267220A	.008	.065	.010	.77
267220B	.008	.062	.010	.78
267221	.031	.143	.026	2.11
STANDARD R-2a	.530	.324	.043	7.80

CU\* NI\* CO\* &amp; FE\* - LEACHED WITH H2O2 + NH4 CITRATE.

- SAMPLE TYPE: DRILL CORE R150

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data h FA \_\_\_\_\_DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Aug 23/05



SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267222	.026	.133	.024	1.58
267223	.034	.148	.029	1.89
267224	.010	.088	.010	.48
267225 (pulp)	.097	.264	.012	1.20
267226	.018	.127	.017	1.06
267227	.009	.188	.011	.73
267228	.012	.145	.015	.80
.STD RTS-2	.056	.223	.007	3.40
267229	.014	.141	.016	1.06
267230	.016	.064	.013	1.48
267231	.019	.051	.010	.82
267232	.013	.152	.010	.94
RE 267232	.013	.155	.010	.97
RRE 267232	.014	.153	.010	.91
267233	.013	.175	.011	.63
STANDARD R-2a	.521	.325	.043	7.40

Sample type: DRILL CORE R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



ASSAY CERTIFICATE



Hard Creek Nickel Corporation PROJECT Tur C05-74B File # A504241 Page 1

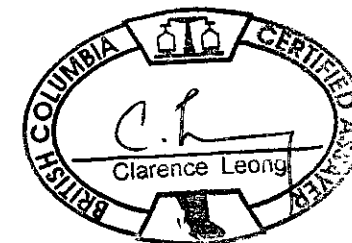
1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Chris Baldys

SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267234	.014	.138	.009	.47
267235	.009	.058	.004	.28
267236	.008	.109	.007	.86
267237	.007	.115	.008	.85
267238	.005	.077	.006	.79
267239	.038	.220	.021	1.52
267240 (rock)	.004	.001<	.001	.17
267241	.030	.249	.024	1.35
267242	.031	.203	.019	1.20
267243	.025	.103	.010	.83
267244	.019	.106	.009	.98
267245	.005	.098	.007	.41
267246	.007	.114	.007	.46
267247	.004	.163	.008	.33
267248	.007	.208	.011	.38
267249	.006	.179	.010	.36
.STD RTS-2	.060	.229	.007	3.70
267250 (pulp)	.098	.268	.012	1.12
267251	.012	.174	.010	.44
267252	.012	.198	.010	.48
267253	.006	.171	.008	.53
267254	.003	.181	.008	.44
267256	.005	.220	.010	.56
267257	.005	.194	.009	.65
267258	.009	.141	.008	.41
267259	.019	.171	.011	.60
267260	.030	.266	.018	.95
RE 267260	.029	.261	.017	.79
RRE 267260	.030	.264	.018	.78
267261	.013	.145	.008	.44
267262	.006	.217	.009	.55
267263	.006	.155	.007	.46
267264	.003	.020	.001	.23
267265	.012	.179	.011	.49
STANDARD R-2a	.538	.315	.041	6.94

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
- SAMPLE TYPE: DRILL CORE R150  
Samples beginning 'RE' are Reruns and 'RRE' are Rerun Reruns.

Data h FA \_\_\_\_\_

DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Aug 24/05





SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267266	.051	.418	.026	1.47
267267	.015	.309	.017	1.14
267268	.018	.205	.011	.85
267269	.004	.076	.005	1.25
RE 267269	.003	.076	.005	1.22
RRE 267269	.003	.074	.005	1.21
267270 (rock)	.002	.002	<.001	.17
267271	.002	.062	.004	1.11
267272	.009	.091	.006	1.25
267273	.017	.173	.008	1.47
267274	.003	.142	.008	1.59
267275 (pulp)	.056	.187	.007	.58
267276	.036	.224	.009	1.51
267277	.054	.301	.010	1.84
267278	.065	.313	.011	1.79
267279	.089	.610	.026	2.83
267280A	.047	.274	.014	1.81
267280B	.012	.282	.014	1.84
267281	.069	.316	.018	1.87
267282	.083	.396	.022	2.00
.STD RTS-2	.059	.224	.007	4.32
267283	.088	.348	.018	1.84
267284	.036	.252	.010	1.32
267285	.066	.296	.013	1.45
267286	.060	.272	.014	1.32
267287	.085	.410	.020	1.75
267288	.085	.394	.016	1.77
267289	.155	.504	.018	2.04
267290	.022	.412	.019	1.83
267291	.046	.400	.018	1.84
267292	.037	.172	.020	1.50
267293	.038	.157	.023	1.74
267294	.055	.199	.025	1.70
267295	.040	.321	.017	1.58
STANDARD R-2a	.534	.321	.044	8.81

Sample type: DRILL CORE R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267296	.046	.406	.021	1.74
267297	.009	.173	.008	1.22
267298	.012	.167	.007	1.10
267299	.009	.159	.008	1.04
267300 (pulp)	.057	.190	.007	.59
267301	.025	.155	.013	1.23
267302	.023	.114	.009	.95
267303	.011	.091	.007	.59
267304	.011	.103	.007	.63
267305	.010	.109	.007	.79
267306	.014	.290	.016	1.32
267307	.009	.167	.008	.80
267308	.003	.120	.006	.76
.STD RTS-2	.059	.218	.006	3.68
267309	.012	.153	.011	.62
267310A	.009	.048	.006	.37
267310B	.009	.048	.006	.59
267311	.008	.036	.006	.40
267312	.006	.060	.009	.80
267313	.012	.096	.008	.72
267314	.005	.136	.007	.46
267315	.029	.069	.009	1.21
267316	.022	.041	.009	2.48
267317	.013	.018	.007	1.83
267318	.012	.041	.007	1.31
267319	.009	.015	.005	1.10
267320	.012	.021	.005	2.28
RE 267320	.012	.020	.005	2.41
RRE 267320	.013	.019	.005	2.32
267321	.016	.021	.006	3.24
267322	.012	.006	.004	1.74
267323	.022	.019	.006	2.78
STANDARD R-2a	.535	.334	.042	8.15

Sample type: DRILL CORE R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE



Hard Creek Nickel Corporation PROJECT Tur C05-74B File # A504241 Page 1

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Chris Baldys

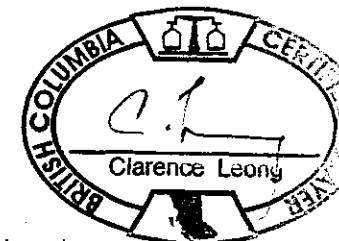
SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267234	<.001	.015	<.02	.01	<2	.141	.010	.13	8.86	<.02	<.01	<.001	<.01	<.01	.01	1.60	.02	.114	19.58	.06	1.32	.04	.17	<.01	.75	<2	5	2	2.33
267235	<.001	.010	<.02	<.01	<2	.061	.005	.14	6.92	<.02	.05	<.001	<.01	<.01	.01	4.24	.08	.044	8.77	.24	6.76	2.55	.67	<.01	.34	<2	2	3	1.38
267236	<.001	.011	<.02	.01	<2	.145	.012	.15	10.14	<.02	<.01	<.001	<.01	<.01	<.01	.45	<.01	.170	25.50	.01	.08	.01	<.01	<.01	.70	3	7	2	5.05
267237	<.001	.009	<.02	<.01	2	.144	.013	.15	10.20	<.02	<.01	<.001	<.01	<.01	<.01	.15	<.01	.139	24.66	.01	.07	.01	<.01	<.01	.75	2	12	6	2.56
267238	<.001	.007	<.02	.01	<2	.124	.012	.14	9.68	<.02	<.01	<.001	<.01	<.01	<.01	.45	<.01	.117	25.27	.01	.05	.01	<.01	<.01	.45	4	5	6	5.28
267239	<.001	.041	<.02	<.01	2	.232	.023	.12	12.76	<.02	<.01	<.001	<.01	<.01	<.01	.44	<.01	.095	22.40	.01	.06	<.01	.01	<.01	2.52	9	11	3	5.22
267240 (rock)	<.001	.006	<.02	.01	<2	.002	.001	.10	4.55	<.02	.04	<.001	<.01	<.01	.01	4.32	.06	.001	1.91	.30	8.93	2.36	1.18	<.01	<.02	2	<2	2	2.61
267241	<.001	.032	<.02	.01	<2	.241	.026	.13	12.24	<.02	<.01	<.001	<.01	.01	.01	.43	<.01	.073	23.63	.01	.06	.01	.01	<.01	2.79	6	<2	6	5.03
267242	<.001	.033	<.02	<.01	<2	.194	.018	.12	10.36	<.02	<.01	<.001	<.01	<.01	<.01	.39	<.01	.113	22.60	.01	.14	.01	.01	<.01	1.77	38	5	3	5.14
267243	.001	.026	<.02	<.01	<2	.110	.011	.16	9.94	<.02	<.01	<.001	<.01	<.01	.03	6.36	.05	.143	12.89	.19	2.58	.20	.86	<.01	2.32	<2	9	<2	5.24
267244	.001	.019	<.02	.01	<2	.110	.010	.15	9.21	<.02	<.01	<.001	<.01	<.01	.03	3.98	.01	.138	15.47	.09	.95	.19	.43	<.01	1.89	<2	10	<2	8.28
267245	<.001	.005	<.02	<.01	<2	.102	.008	.14	7.77	<.02	<.01	<.001	<.01	<.01	.02	4.55	<.01	.132	17.81	.07	.41	.06	.03	<.01	.71	4	<2	<2	4.41
267246	<.001	.008	<.02	.01	<2	.121	.008	.15	6.98	<.02	<.01	<.001	<.01	<.01	.02	5.00	<.01	.111	17.03	.06	.30	.06	.02	<.01	.88	<2	<2	<2	4.56
267247	<.001	.005	<.02	.01	<2	.163	.009	.15	7.75	<.02	<.01	<.001	<.01	<.01	.01	2.79	<.01	.105	19.72	.03	.20	.01	<.01	<.01	.52	2	7	9	4.95
267248	<.001	.008	<.02	<.01	<2	.207	.011	.08	8.01	<.02	<.01	<.001	<.01	<.01	.01	.84	<.01	.144	21.18	.02	.14	.01	<.01	<.01	.81	<2	9	5	2.33
267249	<.001	.008	<.02	.01	<2	.176	.011	.09	9.70	<.02	<.01	<.001	<.01	<.01	.01	1.33	<.01	.258	20.48	.03	.18	.01	<.01	<.01	.82	<2	7	5	3.40
.STD RTS-2	<.001	.073	<.02	.01	3	.263	.007	.04	38.92	<.02	<.01	.002	<.01	.03	<.01	.56	<.01	.011	.36	.16	.84	.21	.13	<.01	19.79	-	-	-	-
267250 (pulp)	<.001	.098	<.02	<.01	<2	.342	.015	.05	9.52	<.02	<.01	<.001	<.01	<.01	.01	3.18	<.01	.288	14.57	.14	2.77	.23	.05	<.01	1.07	4	73	357	-
267251	<.001	.015	<.02	<.01	<2	.172	.010	.08	10.36	<.02	<.01	<.001	<.01	<.01	.01	.48	<.01	.168	20.75	.03	.20	<.01	<.01	<.01	.99	3	159	6	3.77
267252	<.001	.015	<.02	<.01	<2	.196	.010	.08	9.22	<.02	<.01	<.001	<.01	<.01	.01	1.11	<.01	.143	20.80	.03	.19	.01	<.01	<.01	1.19	<2	<2	<2	4.70
267253	<.001	.008	<.02	.01	<2	.183	.009	.15	8.05	<.02	<.01	<.001	<.01	<.01	.01	1.21	<.01	.211	21.97	.02	.13	.01	<.01	<.01	.65	<2	5	4	3.67
267254	<.001	.004	<.02	.01	<2	.188	.009	.17	7.23	<.02	<.01	<.001	<.01	<.01	.01	1.65	<.01	.142	22.77	.02	.12	.01	<.01	<.01	.35	<2	<2	<2	6.12
267256	<.001	.006	<.02	<.01	<2	.220	.011	.12	8.08	<.02	<.01	<.001	<.01	<.01	.01	1.00	<.01	.102	21.74	.02	.12	.01	<.01	<.01	.55	<2	3	<2	5.50
267257	<.001	.006	<.02	<.01	<2	.198	.009	.14	8.12	<.02	<.01	<.001	<.01	<.01	.01	.90	<.01	.096	22.53	.02	.11	.01	<.01	<.01	.61	<2	<2	<2	4.32
267258	<.001	.013	<.02	.01	<2	.146	.009	.08	7.82	<.02	<.01	<.001	<.01	<.01	.01	2.89	<.01	.174	20.24	.03	.19	.02	<.01	<.01	.96	<2	<2	<2	3.80
267259	<.001	.024	<.02	<.01	<2	.184	.013	.12	10.15	<.02	<.01	<.001	<.01	<.01	.01	2.72	<.01	.125	20.62	.03	.14	.03	<.01	<.01	1.36	<2	<2	<2	4.89
267260	.001	.033	<.02	<.01	<2	.260	.018	.09	10.63	<.02	<.01	<.001	<.01	<.01	.01	2.15	<.01	.152	20.38	.02	.15	.02	<.01	<.01	1.99	<2	6	14	3.83
RE 267260	.001	.033	<.02	.01	<2	.261	.018	.09	10.64	<.02	<.01	<.001	<.01	<.01	.01	2.12	<.01	.154	20.31	.02	.15	.02	<.01	<.01	2.00	<2	<2	10	-
RRE 267260	.001	.034	<.02	.01	<2	.266	.018	.09	10.85	<.02	<.01	<.001	<.01	<.01	.01	2.21	<.01	.158	20.46	.03	.16	.02	<.01	<.01	1.98	<2	9	15	-
267261	<.001	.017	<.02	<.01	<2	.153	.009	.06	7.61	<.02	<.01	<.001	<.01	<.01	.01	2.05	.03	.109	20.77	.08	.91	.01	<.01	<.01	.70	<2	6	7	3.39
267262	<.001	.007	<.02	<.01	2	.229	.010	.12	7.13	<.02	<.01	<.001	<.01	<.01	.01	2.61	<.01	.167	21.72	.03	.19	.02	<.01	<.01	.47	<2	4	7	4.42
267263	<.001	.007	<.02	<.01	<2	.184	.010	.11	7.31	<.02	<.01	<.001	<.01	<.01	.01	3.75	<.01	.185	20.70	.03	.27	.02	<.01	<.01	.43	<2	3	6	4.12
267264	.001	.003	<.02	.01	2	.035	.003	.25	7.64	<.02	<.01	<.001	<.01	<.01	.02	14.17	.14	.031	6.69	.37	8.63	.02	.17	<.01	.06	<2	<2	<2	1.66
267265	<.001	.015	<.02	<.01	<2	.184	.011	.10	8.38	<.02	<.01	<.001	<.01	<.01	<.01	3.81	<.01	.146	19.78	.02	.53	<.01	<.01	<.01	.73	5	3	8	4.10
STANDARD R-2a/CSB/FA-10R	.050	.582	1.61	4.03	170	.377	.045	.24	25.68	.23	.14	.031	.14	<.01	.01	3.56	.08	.060	2.65	.18	2.92	.52	.65	.07	5.32	497	462	472	-

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCl) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.  
 AU\*\* PT\*\* & PD\*\* GROUP 3B - 30.00 GM SAMPLE ANALYSIS BY FA/ICP. TOTAL S GROUP 2A BY LECO.  
 - SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data K FA

DATE RECEIVED: AUG 8 2005

DATE REPORT MAILED: Aug. 12/05





SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267266	<.001	.055	<.02	.01	<2	.422	.024	.13	9.91	<.02	<.01	.001	<.01	<.01	<.01	1.58	<.01	.199	22.10	.01	.15	.01	.01	<.01	2.15	13	34	51	4.74
267267	<.001	.060	<.02	.01	<2	.314	.017	.08	8.67	<.02	<.01	.001	<.01	<.01	<.01	.97	<.01	.194	22.61	.02	.36	.01	.01	<.01	1.22	6	31	47	5.03
267268	<.001	.018	<.02	.01	<2	.219	.012	.09	7.41	<.02	<.01	.001	<.01	<.01	<.01	1.21	<.01	.160	21.54	.05	1.04	.01	.01	<.01	.73	5	14	25	4.60
267269	<.001	.004	<.02	.01	<2	.162	.011	.13	7.93	<.02	<.01	.001	<.01	<.01	<.01	1.23	<.01	.168	24.97	.01	.10	.02	<.01	<.01	.19	6	6	6	4.72
RE 267269	<.001	.004	<.02	.01	<2	.159	.012	.13	7.86	<.02	<.01	.001	<.01	<.01	<.01	1.22	<.01	.164	25.02	.01	.10	.01	<.01	<.01	.19	<2	5	12	-
RRE 267269	<.001	.004	<.02	.01	<2	.159	.012	.13	7.79	<.02	<.01	.001	<.01	<.01	<.01	1.12	<.01	.162	24.83	.01	.09	.01	<.01	<.01	.18	8	3	7	-
267270 (rock)	<.001	.005	<.02	.01	<2	.003	.001	.10	4.48	<.02	.05	<.001	<.01	<.01	.01	4.29	.06	.003	2.03	.30	8.97	2.37	1.20	<.01	<.02	2	<2	<2	2.49
267271	<.001	.004	<.02	.01	<2	.147	.012	.13	7.80	<.02	<.01	.001	<.01	<.01	<.01	2.07	<.01	.158	24.43	.02	.14	.03	.01	<.01	.19	3	9	6	5.50
267272	<.001	.012	<.02	.01	<2	.171	.013	.13	8.11	<.02	<.01	.001	<.01	<.01	<.01	.70	<.01	.178	25.00	.02	.15	.01	.01	<.01	.27	5	9	14	5.16
267273	<.001	.020	<.02	.01	<2	.257	.014	.13	8.20	<.02	<.01	.001	<.01	<.01	<.01	.56	<.01	.155	25.75	.02	.12	.01	<.01	<.01	.48	6	24	24	5.11
267274	<.001	.018	<.02	.01	<2	.208	.014	.13	8.45	<.02	<.01	.001	<.01	<.01	<.01	1.01	<.01	.153	24.99	.03	.16	.01	<.01	<.01	.49	3	8	13	4.65
267275 (pulp)	<.001	.057	<.02	.01	2	.231	.010	.11	8.77	<.02	<.01	.001	<.01	<.01	.01	4.22	<.01	.658	13.22	.18	3.84	.33	.11	<.01	.55	16	119	299	-
267276	<.001	.039	<.02	.01	<2	.316	.015	.13	8.60	<.02	<.01	.001	<.01	<.01	<.01	.27	<.01	.248	25.58	.01	.10	<.01	<.01	<.01	.63	9	120	126	5.61
267277	<.001	.057	<.02	.01	<2	.420	.016	.13	8.80	<.02	<.01	.001	<.01	<.01	<.01	.37	<.01	.200	25.64	.01	.08	.01	<.01	<.01	.79	10	82	94	5.79
267278	<.001	.071	<.02	.01	<2	.433	.018	.13	9.30	<.02	<.01	.001	<.01	<.01	<.01	.66	<.01	.146	25.62	.03	.18	.01	<.01	<.01	1.12	10	93	112	5.21
267279	<.001	.095	<.02	.01	<2	.684	.029	.13	11.78	<.02	<.01	.001	<.01	<.01	<.01	.15	<.01	.574	24.18	.01	.12	<.01	<.01	<.01	2.86	18	152	177	5.79
267280A	<.001	.051	<.02	.02	<2	.355	.020	.13	9.26	<.02	<.01	.001	<.01	<.01	<.01	.31	<.01	.231	25.38	.01	.09	<.01	<.01	<.01	1.26	6	26	30	5.29
267280B	<.001	.053	<.02	.01	<2	.363	.020	.12	9.40	<.02	<.01	.001	<.01	<.01	<.01	.29	<.01	.237	25.92	.01	.08	<.01	<.01	<.01	1.30	5	25	28	-
267281	<.001	.076	<.02	.01	<2	.368	.023	.13	10.60	<.02	<.01	.001	<.01	<.01	<.01	.41	<.01	.229	25.94	.01	.11	.01	<.01	<.01	1.85	<2	34	41	4.80
267282	<.001	.089	<.02	.01	<2	.447	.025	.12	10.74	<.02	<.01	.001	<.01	<.01	<.01	.33	<.01	.218	25.55	.01	.09	<.01	<.01	<.01	2.19	6	44	49	6.01
.STD RTS-2	<.001	.074	<.02	.01	<2	.268	.007	.04	38.97	<.02	<.01	.002	<.01	<.01	<.01	.57	.01	.013	.37	.17	.86	.22	.13	<.01	17.20	-	-	-	-
267283	<.001	.098	<.02	.01	<2	.418	.023	.12	9.67	<.02	<.01	.001	<.01	<.01	<.01	.16	<.01	.189	24.35	.01	.09	<.01	<.01	<.01	1.74	7	19	33	5.29
267284	<.001	.039	<.02	.01	<2	.317	.015	.12	8.25	<.02	<.01	.001	<.01	<.01	<.01	.66	<.01	.223	24.55	.03	.28	<.01	<.01	<.01	.77	6	80	94	4.20
267285	<.001	.071	<.02	.01	<2	.370	.019	.13	8.92	<.02	<.01	.001	<.01	<.01	<.01	.51	<.01	.205	25.02	.03	.26	<.01	<.01	<.01	1.05	4	31	39	1.56
267286	<.001	.065	<.02	.01	<2	.340	.019	.13	8.65	<.02	<.01	.001	<.01	<.01	<.01	.81	<.01	.194	24.40	.01	.14	.01	<.01	<.01	1.05	8	2	8	3.28
267287	<.001	.093	<.02	.01	<2	.471	.023	.13	10.12	<.02	<.01	.001	<.01	<.01	<.01	.22	<.01	.251	24.53	.01	.13	<.01	.01	<.01	1.98	9	37	41	5.56
267288	<.001	.094	<.02	.01	<2	.475	.021	.13	9.97	<.02	<.01	.001	<.01	<.01	<.01	.40	<.01	.216	25.33	.01	.11	<.01	<.01	<.01	1.72	5	74	79	6.23
267289	<.001	.171	<.02	.01	<2	.593	.022	.13	10.12	<.02	<.01	.001	<.01	<.01	<.01	.24	<.01	.199	25.09	.01	.13	<.01	<.01	<.01	2.20	8	80	71	5.68
267290	<.001	.086	<.02	.01	<2	.470	.024	.12	10.20	<.02	<.01	.001	<.01	<.01	<.01	.40	<.01	.152	25.28	.02	.25	<.01	.01	<.01	2.13	3	6	18	6.00
267291	<.001	.051	<.02	.01	<2	.462	.021	.12	9.24	<.02	<.01	.001	<.01	<.01	<.01	.48	<.01	.150	24.31	.03	.27	<.01	<.01	<.01	2.15	4	19	15	2.75
267292	<.001	.039	<.02	.01	<2	.183	.025	.13	10.17	<.02	<.01	.001	<.01	<.01	<.01	.11	<.01	.236	25.70	.01	.08	<.01	<.01	<.01	1.95	18	4	5	5.51
267293	<.001	.040	<.02	.01	<2	.162	.027	.13	11.57	<.02	<.01	.001	<.01	<.01	<.01	.13	<.01	.231	25.18	.01	.07	<.01	<.01	<.01	2.57	2	11	14	5.32
267294	<.001	.060	<.02	.01	<2	.213	.028	.13	12.41	<.02	<.01	.001	<.01	<.01	<.01	.47	<.01	.200	24.90	.01	.09	<.01	.01	<.01	2.94	2	14	12	5.59
267295	<.001	.045	<.02	.01	<2	.374	.022	.13	10.20	<.02	<.01	.001	<.01	<.01	<.01	.23	<.01	.205	25.58	.01	.08	<.01	<.01	<.01	2.12	16	20	21	5.31
STANDARD R-2a	.048	.585	1.57	4.12	160	.377	.045	.24	25.37	.19	.14	.030	.13	<.01	.01	3.53	.08	.058	2.63	.18	2.90	.52	.63	.07	5.23	498	481	478	-

Standard is STANDARD R-2a/CSB/FA-10R. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267296	<.001	.045	<.02	.01	<2	.419	.024	.12	10.31	<.02	<.01	<.001	<.01	<.01	<.01	.11	<.01	.188	24.50	.02	.14	.01	.01	<.01	2.68	5	15	22	5.43
267297	<.001	.010	<.02	.01	<2	.199	.013	.16	9.23	<.02	<.01	<.001	<.01	<.01	<.01	.10	<.01	.206	25.59	.01	.07	.01	.01	<.01	1.07	<2	<2	2	5.32
267298	<.001	.015	<.02	.01	<2	.208	.012	.15	8.98	<.02	<.01	<.001	<.01	<.01	<.01	1.08	<.01	.164	24.31	.01	.10	.01	<.01	<.01	1.06	6	7	9	5.42
267299	<.001	.010	<.02	.01	<2	.189	.011	.17	8.88	<.02	<.01	<.001	<.01	<.01	<.01	2.34	<.01	.187	23.23	.02	.11	.02	<.01	<.01	1.09	<2	9	7	5.67
267300 (pulp)	<.001	.056	<.02	.01	<2	.228	.010	.11	8.72	<.02	<.01	<.001	<.01	<.01	.01	4.21	<.01	.696	12.94	.18	3.83	.32	.11	<.01	.53	8	77	268	-
267301	<.001	.028	<.02	<.01	<2	.170	.016	.16	12.99	<.02	<.01	.001	<.01	<.01	<.01	2.25	<.01	.250	20.59	.02	.12	.02	<.01	<.01	2.46	7	12	12	3.82
267302	<.001	.026	<.02	.01	<2	.132	.012	.16	9.97	<.02	<.01	<.001	<.01	<.01	.01	5.88	<.01	.215	18.18	.03	.18	.05	<.01	<.01	1.79	9	4	13	5.03
267303	<.001	.012	<.02	.01	<2	.104	.009	.14	8.70	<.02	<.01	<.001	<.01	<.01	.01	5.91	<.01	.228	17.31	.03	.18	.06	<.01	<.01	1.15	3	9	<2	5.43
267304	<.001	.012	<.02	<.01	<2	.114	.009	.15	8.77	<.02	<.01	<.001	<.01	<.01	.01	4.51	<.01	.158	18.76	.04	.26	.03	.01	<.01	1.02	<2	9	12	3.23
267305	<.001	.012	<.02	<.01	<2	.144	.011	.18	9.75	<.02	<.01	<.001	<.01	<.01	.01	3.65	<.01	.161	20.71	.02	.14	.04	<.01	<.01	.99	3	6	8	5.14
267306	<.001	.016	<.02	.01	<2	.333	.019	.18	12.04	<.02	<.01	<.001	<.01	<.01	.01	2.64	<.01	.165	20.40	.04	.24	.03	.01	<.01	2.05	<2	11	18	5.54
267307	<.001	.010	<.02	.01	<2	.197	.012	.19	9.91	<.02	<.01	<.001	<.01	<.01	.01	2.95	<.01	.171	21.22	.02	.16	.03	.01	<.01	1.03	<2	11	11	4.62
267308	<.001	.005	<.02	.01	<2	.168	.010	.20	9.40	<.02	<.01	<.001	<.01	<.01	.01	1.97	<.01	.163	22.06	.02	.13	.02	<.01	<.01	.51	3	5	<2	4.65
.STD RTS-2	<.001	.074	<.02	.01	<2	.273	.007	.04	39.13	<.02	<.01	.002	<.01	<.01	<.01	.58	.01	.013	.37	.17	.86	.22	.13	<.01	19.50	-	-	-	-
267309	<.001	.014	<.02	<.01	<2	.165	.012	.13	10.28	<.02	<.01	<.001	<.01	<.01	.01	.78	<.01	.166	20.65	.02	.20	.01	<.01	<.01	1.12	4	10	17	3.26
267310A	<.001	.010	<.02	<.01	<2	.054	.008	.13	6.36	<.02	<.01	<.001	<.01	<.01	.01	11.46	.02	.137	12.44	.13	1.17	.06	.01	<.01	.62	40	<2	6	4.66
267310B	<.001	.010	<.02	<.01	<2	.054	.008	.13	6.37	<.02	<.01	<.001	<.01	<.01	.01	11.31	.02	.139	12.40	.13	1.17	.06	<.01	<.01	.66	<2	<2	<2	-
267311	<.001	.009	<.02	<.01	<2	.039	.007	.11	5.85	<.02	<.01	<.001	<.01	<.01	.01	11.11	<.01	.165	13.04	.06	.56	.08	<.01	<.01	.66	2	3	3	3.93
267312	<.001	.007	<.02	<.01	<2	.064	.010	.13	7.74	<.02	<.01	<.001	<.01	<.01	.01	11.14	<.01	.127	12.44	.07	.75	.08	.01	<.01	1.42	<2	14	2	2.93
267313	<.001	.014	<.02	<.01	<2	.110	.010	.16	9.44	<.02	<.01	<.001	<.01	<.01	.01	5.19	<.01	.121	17.31	.04	.31	.04	<.01	<.01	1.02	<2	<2	-5	4.95
267314	<.001	.006	<.02	<.01	<2	.156	.009	.14	9.43	<.02	<.01	<.001	<.01	<.01	.01	3.01	<.01	.081	18.66	.04	.45	.02	.01	<.01	.36	<2	9	2	3.15
267315	<.001	.030	<.02	<.01	<2	.077	.011	.15	8.80	<.02	<.01	<.001	<.01	<.01	.02	11.26	<.01	.115	11.85	.11	.87	.08	.01	<.01	1.92	<2	27	23	5.41
267316	<.001	.022	<.02	<.01	<2	.045	.010	.16	10.77	<.02	<.01	<.001	<.01	<.01	.04	7.76	<.01	.108	12.24	.10	.70	.21	.11	<.01	3.26	2	6	5	3.05
267317	.001	.014	<.02	<.01	<2	.024	.008	.19	9.72	<.02	<.01	<.001	<.01	<.01	.05	8.16	<.01	.130	11.86	.11	.49	.23	.09	<.01	2.94	<2	6	4	3.09
267318	<.001	.013	<.02	<.01	<2	.051	.008	.19	10.01	<.02	<.01	<.001	<.01	<.01	.04	5.79	<.01	.162	13.40	.10	.50	.18	.14	<.01	2.29	5	16	9	4.82
267319	.001	.010	<.02	<.01	<2	.020	.007	.20	9.26	<.02	.01	<.001	<.01	<.01	.05	8.86	.02	.110	11.27	.16	1.02	.26	.26	<.01	1.96	<2	7	<2	4.96
267320	.002	.014	<.02	<.01	2	.027	.006	.24	10.84	<.02	<.01	.001	<.01	<.01	.06	7.27	<.01	.088	11.99	.12	.52	.24	.09	<.01	3.14	2	<2	3	4.61
RE 267320	.001	.014	<.02	.01	<2	.027	.006	.24	10.86	<.02	<.01	<.001	<.01	<.01	.06	7.19	<.01	.091	12.00	.12	.52	.24	.09	<.01	3.21	<2	11	6	-
RRE 267320	.002	.015	<.02	<.01	<2	.028	.006	.24	10.80	<.02	<.01	<.001	<.01	<.01	.06	7.39	<.01	.089	12.23	.12	.52	.25	.08	<.01	3.09	2	6	3	-
267321	.002	.017	<.02	.01	<2	.027	.007	.24	11.96	<.02	<.01	<.001	<.01	<.01	.06	7.29	<.01	.064	12.13	.11	.45	.24	.08	<.01	4.11	2	<2	9	5.56
267322	<.001	.013	<.02	<.01	<2	.010	.005	.21	9.28	<.02	<.01	<.001	<.01	.01	.06	8.96	<.01	.083	11.35	.13	.64	.26	.20	<.01	2.52	<2	3	<2	6.88
267323	.001	.023	<.02	<.01	<2	.027	.007	.20	11.80	<.02	<.01	.001	<.01	<.01	.05	7.51	<.01	.084	11.42	.16	.97	.29	.30	<.01	4.01	6	7	<2	1.91
STANDARD R-2a	.049	.579	1.57	4.07	156	.380	.045	.24	25.30	.21	.13	.029	.13	<.01	.01	3.54	.08	.062	2.60	.18	2.88	.50	.62	.08	5.14	511	498	489	-

Standard is STANDARD R-2a/CSB/FA-10R. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

## ASSAY CERTIFICATE



Hard Creek Nickel Corporation PROJECT Tur C05-75A File # A504244 Page 1

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchins

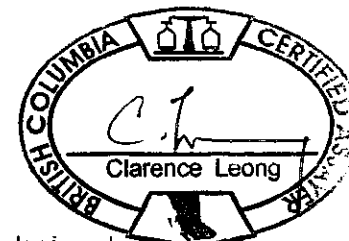


SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267324	.014	.137	.006	.79
267325 (pulp)	.102	.265	.014	1.30
267326	.001	.061	.002	.14
267327	.009	.002	<.001	.22
267328	.009	.012	.001	.13
267329	.057	.177	.009	.82
267330 (rock)	.005	.001	<.001	.16
267331	.058	.136	.006	.55
267332	.026	.201	.010	.71
267333	.012	.063	.004	.37
267334	.008	.001	.001	.14
267335	.011	.116	.007	.42
267336	.016	.092	.006	.30
.STD RTS-2	.060	.222	.008	3.67
267338	.011	.003	.001	.17
267340	.003	<.001	<.001	.10
267342A	.037	.134	.014	.67
267342B	.035	.131	.014	.66
267343	.039	.197	.016	1.22
267344	.025	.140	.011	.91
267345	.015	.147	.011	.91
267346	.011	.118	.009	.89
267347	.025	.126	.014	.94
267348	.049	.025	.015	1.07
267349	.030	.022	.009	.77
267350 (pulp)	.099	.263	.013	1.27
267351	.040	.049	.011	1.06
267352	.015	.091	.007	.87
267353	.008	.120	.006	.73
RE 267353	.007	.121	.006	.72
RRE 267353	.007	.117	.006	.69
267354	.008	.149	.008	.96
267355	.007	.128	.006	.81
267356	.009	.142	.010	.88
STANDARD R-2a	.531	.320	.044	7.80

CU\* NI\* CO\* &amp; FE\* - LEACHED WITH H2O2 + NH4 CITRATE.

- SAMPLE TYPE: DRILL CORE R150

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data K FA \_\_\_\_\_DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Aug 29/05.....



SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267357	.018	.151	.011	1.18
267358	.028	.053	.009	1.27
267359	.023	.078	.011	1.14
267360 (rock)	.004	.001	<.001	.15
.STD RTS-2	.057	.225	.007	4.11
267361	.007	.103	.007	.78
267362	.007	.128	.009	.72
267363	.014	.153	.009	1.24
STANDARD R-2a	.520	.327	.044	8.94

Sample type: DRILL CORE R150.



ASSAY CERTIFICATE

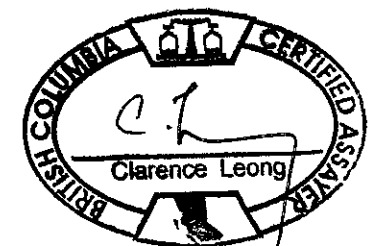
Hard Creek Nickel Corporation PROJECT Tur C05-75A File # A504244 Page 1  
1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267324	<.001	.013	<.02	.01	<2	.150	.007	.10	4.52	<.02	<.01	<.001	<.01	<.01	<.01	5.80	<.01	.108	15.63	.01	1.22	.16	.30	<.01	.65	<2	6	8	4.32
267325 (pulp)	<.001	.099	<.02	.01	<2	.349	.015	.05	9.26	<.02	<.01	<.001	<.01	<.01	.01	3.32	<.01	.342	14.86	.14	2.84	.24	.05	<.01	1.12	24	128	417	-
267326	<.001	.001	<.02	.01	<2	.114	.005	.12	3.83	<.02	<.01	<.001	<.01	<.01	<.01	7.29	<.01	.075	13.66	.01	1.69	.19	1.18	<.01	.07	5	<2	6	3.61
267327	<.001	.009	<.02	.01	<2	.006	.003	.16	7.99	<.02	.14	<.001	<.01	<.01	.03	7.48	.14	.009	4.13	.52	9.11	2.05	2.42	<.01	.02	<2	8	10	4.17
267328	<.001	.009	<.02	.01	<2	.024	.003	.14	6.28	<.02	.11	<.001	<.01	<.01	.02	6.21	.11	.023	4.39	.37	8.63	2.78	2.12	<.01	.04	<2	16	12	3.73
267329	<.001	.056	<.02	.01	<2	.195	.009	.09	4.88	<.02	<.01	<.001	<.01	<.01	<.01	5.43	<.01	.130	15.04	.02	1.21	.14	.91	<.01	.93	<2	34	29	2.72
267330 (rock)	<.001	.006	<.02	.01	<2	.001	.001	.10	4.27	<.02	.05	<.001	<.01	<.01	.01	4.49	.06	.001	1.82	.31	9.19	2.45	1.26	<.01	<.02	<2	2	<2	2.22
267331	<.001	.056	<.02	.01	<2	.179	.008	.10	5.09	<.02	<.01	<.001	<.01	<.01	<.01	5.80	.02	.097	12.90	.05	2.53	.21	2.21	<.01	.78	2	20	22	3.88
267332	<.001	.027	<.02	.01	<2	.237	.010	.10	5.73	<.02	<.01	<.001	<.01	<.01	<.01	3.92	<.01	.087	14.88	.02	2.63	.08	2.48	<.01	.92	4	43	28	2.24
267333	<.001	.013	<.02	.01	<2	.078	.006	.13	5.55	<.02	.07	<.001	<.01	<.01	.01	4.67	.08	.036	9.21	.19	6.54	1.84	2.10	<.01	.44	<2	3	13	4.15
267334	<.001	.010	<.02	.02	<2	.004	.001	.11	4.30	<.02	.11	<.001	<.01	<.01	.01	3.99	.10	.004	1.91	.31	10.14	4.91	1.32	<.01	.09	<2	<2	4	2.08
267335	<.001	.011	<.02	.01	<2	.133	.008	.11	5.24	<.02	.01	<.001	<.01	<.01	.01	4.99	.02	.116	15.38	.09	2.16	.29	.85	<.01	.64	8	62	61	3.97
267336	<.001	.017	<.02	<.01	2	.102	.007	.12	6.22	<.02	.08	<.001	<.01	<.01	.02	7.49	.07	.066	9.46	.23	5.19	1.06	1.31	<.01	.46	2	18	17	5.59
.STD RTS-2	<.001	.073	<.02	.02	2	.271	.007	.04	37.87	<.02	<.01	<.001	<.01	<.01	.01	.59	.01	.012	.38	.17	.86	.23	.14	<.01	18.88	-	-	-	-
267338	<.001	.011	<.02	.01	<2	.005	.002	.14	6.62	<.02	.10	<.001	<.01	<.01	.03	7.02	.13	.006	3.17	.40	9.30	3.38	1.18	<.01	.05	4	9	7	6.56
267340	<.001	.004	<.02	.01	<2	.002	.002	.16	5.96	<.02	.16	<.001	<.01	<.01	.02	7.92	.14	.004	2.79	.40	10.00	2.89	1.36	<.01	<.02	2	<2	5	3.53
267342A	<.001	.041	<.02	.01	<2	.151	.014	.08	8.61	<.02	<.01	<.001	<.01	<.01	.01	1.89	<.01	.121	21.13	.04	.44	.13	.03	<.01	1.03	10	28	19	5.25
267342B	.001	.040	<.02	.01	<2	.150	.014	.08	8.58	<.02	<.01	<.001	<.01	<.01	.01	1.84	<.01	.119	21.05	.04	.43	.12	.03	<.01	1.06	9	18	19	-
267343	<.001	.041	<.02	.01	<2	.233	.019	.17	10.36	<.02	<.01	<.001	<.01	<.01	.01	1.94	<.01	.196	23.92	.03	.14	.02	<.01	<.01	.91	3	12	15	5.22
267344	<.001	.028	<.02	.01	<2	.181	.015	.17	9.86	<.02	<.01	<.001	<.01	<.01	.01	2.00	<.01	.203	23.79	.03	.15	.02	<.01	<.01	.62	4	9	9	5.23
267345	<.001	.017	<.02	.01	<2	.199	.015	.16	9.15	<.02	<.01	<.001	<.01	<.01	<.01	1.69	<.01	.161	25.08	.03	.18	.02	.01	<.01	.54	5	15	13	5.23
267346	<.001	.012	<.02	.01	<2	.181	.013	.15	8.80	<.02	<.01	<.001	<.01	<.01	.01	2.61	<.01	.185	24.12	.05	.24	.02	<.01	<.01	.50	3	12	16	5.24
267347	<.001	.028	<.02	.01	<2	.169	.018	.15	9.82	<.02	<.01	<.001	<.01	<.01	.01	2.75	<.01	.148	22.59	.04	.18	.03	<.01	<.01	1.14	5	20	22	7.48
267348	<.001	.051	<.02	.01	<2	.029	.016	.13	8.94	<.02	<.01	<.001	<.01	<.01	.01	10.39	<.01	.126	14.45	.12	.46	.08	<.01	<.01	2.02	4	18	15	4.56
267349	<.001	.032	<.02	.01	3	.028	.010	.13	7.45	<.02	<.01	<.001	<.01	<.01	.02	11.93	<.01	.102	12.74	.15	.60	.08	<.01	<.01	1.49	3	19	20	5.03
267350 (pulp)	<.001	.099	<.02	.01	<2	.346	.016	.05	9.32	<.02	<.01	<.001	<.01	<.01	.01	3.27	<.01	.342	14.90	.15	2.82	.24	.05	<.01	1.10	26	85	346	-
267351	<.001	.042	<.02	.01	<2	.058	.012	.14	8.60	<.02	<.01	<.001	<.01	<.01	.02	11.96	<.01	.088	12.54	.17	.64	.08	<.01	<.01	2.23	2	8	13	3.74
267352	.001	.016	<.02	.02	<2	.178	.011	.17	8.76	<.02	<.01	<.001	<.01	<.01	.01	4.30	<.01	.251	22.24	.11	.48	.03	.14	<.01	.71	4	13	16	4.53
267353	<.001	.009	<.02	.01	<2	.249	.011	.15	7.49	<.02	<.01	<.001	<.01	<.01	.01	1.93	<.01	.178	24.95	.06	.33	.01	.10	<.01	.30	7	3	4	4.55
RE 267353	<.001	.009	<.02	.01	<2	.246	.011	.15	7.43	<.02	<.01	<.001	<.01	<.01	.01	1.93	<.01	.172	25.36	.06	.33	.01	.10	<.01	.29	10	5	10	-
RRE 267353	<.001	.009	<.02	.02	<2	.245	.011	.15	7.39	<.02	<.01	<.001	<.01	<.01	.01	1.85	<.01	.181	25.20	.06	.33	.01	.10	<.01	.28	8	12	13	-
267354	<.001	.009	<.02	.01	<2	.242	.012	.17	9.57	<.02	<.01	<.001	<.01	<.01	.01	2.24	<.01	.246	23.47	.07	.33	.02	.07	<.01	.63	5	21	34	5.34
267355	.001	.009	<.02	.02	<2	.235	.011	.16	8.20	<.02	<.01	<.001	<.01	<.01	.01	3.35	<.01	.152	22.92	.07	.33	.03	.03	<.01	.51	7	14	25	5.75
267356	<.001	.010	<.02	.01	<2	.252	.015	.14	8.94	<.02	<.01	<.001	<.01	<.01	.01	2.52	<.01	.133	24.53	.06	.26	.02	.02	<.01	.70	11	42	12	5.79
STANDARD R-2a	.047	.579	1.58	4.28	162	.384	.045	.24	24.87	.23	.15	.030	.13	<.01	.02	3.68	.08	.065	2.71	.19	2.93	.53	.66	.10	5.23	496	477	481	-

Standard is STANDARD R-2a/CSB/FA-10R.

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCL) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.  
TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B BY FIRE ASSAY & ANALYSIS BY ICP. (30 gm)  
- SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data by FA \_\_\_\_\_ DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Aug 25/05



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267357	<.001	.019	<.02	.01	<2	.205	.013	.13	8.85	<.02	<.01	<.001	<.01	<.01	.01	2.74	<.01	.141	22.21	.11	.52	.02	.15	<.01	1.38	4	15	23	4.57
267358	<.001	.029	<.02	<.01	<2	.063	.010	.14	7.86	<.02	<.01	<.001	<.01	<.01	.03	10.59	<.01	.089	14.60	.16	.61	.08	.01	<.01	1.66	<2	2	6	5.44
267359	<.001	.024	<.02	<.01	<2	.090	.011	.14	9.21	<.02	<.01	<.001	<.01	<.01	.02	7.69	<.01	.123	17.15	.12	.53	.06	<.01	<.01	1.47	<2	3	5	8.04
267360 (rock)	<.001	.005	<.02	<.01	<2	.001	.001	.10	4.37	<.02	.05	<.001	<.01	<.01	.01	4.32	.06	.001	1.84	.31	8.97	2.40	1.26	<.01	.02	2	<2	<2	2.73
.STD RTS-2	<.001	.073	<.02	.01	4	.266	.007	.04	37.96	<.02	<.01	<.001	<.01	<.01	.01	.59	.01	.012	.37	.17	.86	.23	.14	<.01	18.75	-	-	-	-
267361	<.001	.010	<.02	.01	<2	.138	.009	.13	8.20	<.02	<.01	<.001	<.01	<.01	.01	5.03	<.01	.158	20.79	.09	.43	.04	<.01	<.01	.70	2	4	<2	5.25
267362	<.001	.009	<.02	<.01	<2	.136	.010	.09	8.18	<.02	<.01	<.001	<.01	<.01	.01	3.99	<.01	.156	20.46	.08	.53	.03	.01	<.01	.67	3	7	3	4.84
267363	<.001	.016	<.02	.01	<2	.185	.012	.15	9.89	<.02	<.01	<.001	<.01	<.01	.01	2.31	<.01	.173	24.08	.05	.21	.02	.01	<.01	1.04	3	<2	9	6.67
STANDARD R-2a	.047	.565	1.54	4.33	164	.375	.044	.24	24.88	.24	.15	.030	.13	<.01	.02	3.55	.08	.060	2.69	.18	2.87	.53	.65	.11	5.29	490	482	485	-

Standard is STANDARD R-2a/CSB/FA-10R.

## ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-75B File # A504245 Page 1

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267364	<.001	.018	<.02	.01	<2	.227	.016	.17	10.62	<.01	<.01	.001	<.01	<.01	.01	1.68	.01	.225	27.98	.04	.26	<.01	.05	<.01	1.37	<2	2	<2	6.67
267365	<.001	.015	<.02	.01	<2	.213	.013	.16	9.58	<.01	<.01	.001	<.01	<.01	.01	2.36	.01	.176	28.16	.05	.27	.06	.03	<.01	1.00	<2	7	5	6.38
267366	<.001	.016	<.02	<.01	<2	.239	.013	.13	8.82	<.01	<.01	.001	<.01	<.01	.01	1.76	.01	.195	27.47	.03	.23	.25	<.01	<.01	1.10	4	<2	5	4.94
267367	<.001	.018	<.02	<.01	<2	.218	.015	.13	8.88	<.01	<.01	.001	<.01	<.01	.01	1.94	.01	.133	24.74	.06	.37	<.01	<.01	<.01	1.19	<2	4	12	4.68
267368	<.001	.012	<.02	.01	<2	.199	.012	.17	9.05	<.01	<.01	.001	<.01	<.01	.01	2.83	.01	.138	27.16	.04	.20	.12	<.01	<.01	.82	<2	8	11	4.49
267369	<.001	.010	<.02	<.01	<2	.216	.012	.18	9.52	<.01	<.01	.001	<.01	<.01	.01	2.89	.01	.140	27.95	.04	.16	<.01	.03	<.01	.51	4	9	7	5.36
267371A	<.001	.021	<.02	<.01	<2	.244	.014	.17	9.22	<.01	<.01	.001	<.01	<.01	<.01	1.69	.01	.150	29.52	.02	.12	.12	.02	<.01	.62	<2	22	21	5.63
267371B	<.001	.020	<.02	<.01	<2	.238	.013	.17	8.90	<.01	<.01	.001	<.01	<.01	<.01	1.60	.01	.126	28.69	.02	.12	.18	<.01	<.01	.63	7	16	18	-
267372	<.001	.023	<.02	<.01	2	.255	.014	.16	9.50	<.01	<.01	.001	<.01	<.01	.01	1.42	.01	.347	28.47	.02	.15	.11	.02	<.01	.76	<2	33	38	5.54
267373	<.001	.025	<.02	<.01	2	.294	.017	.17	10.02	<.01	<.01	.001	<.01	<.01	.01	1.47	.01	.200	28.33	.02	.13	.05	<.01	<.01	1.23	<2	31	39	5.37
267374	<.001	.023	<.02	<.01	<2	.300	.018	.16	9.84	<.01	<.01	.001	<.01	<.01	.01	1.29	.01	.187	28.17	.02	.12	.24	.04	<.01	1.13	<2	20	20	5.35
267375 (pulp)	<.001	.057	<.02	.01	<2	.249	.012	.12	9.57	<.01	<.01	.001	<.01	<.01	.02	4.92	.01	1.071	15.97	.20	4.20	.44	.12	<.01	.55	10	74	260	-
267376	<.001	.045	<.02	<.01	<2	.308	.023	.16	11.65	<.01	<.01	.001	<.01	<.01	.01	1.23	.01	.232	28.39	.02	.13	.24	.04	<.01	1.64	<2	24	36	5.38
267377	<.001	.021	<.02	<.01	<2	.208	.017	.17	10.21	<.01	<.01	.001	<.01	<.01	.01	1.13	.01	.234	31.24	.02	.13	.17	<.01	<.01	.69	5	6	6	5.94
267378	<.001	.021	<.02	<.01	<2	.275	.019	.17	10.14	<.01	<.01	.001	<.01	<.01	.01	1.04	.01	.234	30.75	.02	.09	<.01	.05	<.01	.92	<2	16	11	6.39
.STD RTS-2	<.001	.074	<.02	.01	<2	.284	.007	.04	38.10	<.01	<.01	.001	<.01	<.01	.01	.63	.02	.013	.48	.18	.91	.31	.19	<.01	18.72	-	-	-	-
267379	<.001	.009	<.02	<.01	<2	.220	.014	.16	9.11	<.01	<.01	.001	<.01	<.01	.01	1.10	<.01	.224	30.46	.01	.10	.10	.01	<.01	.36	<2	7	7	4.97
267380	<.001	.013	<.02	<.01	<2	.269	.014	.16	9.42	<.01	<.01	.001	<.01	<.01	.01	1.12	<.01	.226	30.67	.02	.11	.10	<.01	<.01	.44	<2	5	6	5.85
267381	<.001	.015	<.02	<.01	<2	.267	.015	.16	9.61	<.01	<.01	.001	<.01	<.01	.01	1.29	.01	.232	30.57	.02	.10	.10	.05	<.01	.58	<2	18	14	6.12
267382	<.001	.021	<.02	<.01	<2	.223	.016	.16	10.20	<.01	<.01	.001	<.01	<.01	.01	1.04	.01	.183	29.55	.01	.09	<.01	<.01	<.01	.86	5	14	13	5.71
267383	<.001	.030	<.02	<.01	<2	.210	.017	.16	10.62	<.01	<.01	.001	<.01	<.01	.01	1.12	.01	.170	29.64	.01	.07	.17	.04	<.01	1.06	5	20	13	5.93
267384	<.001	.026	<.02	<.01	<2	.200	.019	.16	11.04	<.01	<.01	.001	<.01	<.01	.01	1.29	.01	.200	28.55	.02	.10	.23	.01	<.01	1.16	6	18	9	5.70
267385	<.001	.034	<.02	<.01	<2	.303	.020	.16	11.40	<.01	<.01	.001	<.01	<.01	.01	1.20	.01	.233	28.60	.02	.08	.16	<.01	<.01	1.42	<2	25	25	5.86
267386	<.001	.023	<.02	<.01	<2	.290	.016	.17	10.89	<.01	<.01	.001	<.01	<.01	.01	1.44	.01	.249	29.06	.02	.13	.09	.01	<.01	1.20	<2	19	21	5.49
267387	<.001	.012	<.02	<.01	<2	.223	.014	.17	10.11	<.01	<.01	.001	<.01	<.01	.01	1.55	.01	.218	29.31	.02	.10	.30	<.01	<.01	.63	<2	9	5	5.60
267388	<.001	.007	<.02	<.01	<2	.218	.011	.16	9.01	<.01	<.01	.001	<.01	<.01	.01	3.14	.01	.180	26.91	.03	.15	.09	<.01	<.01	.46	<2	13	7	5.27
267389	<.001	.022	<.02	<.01	<2	.179	.014	.17	10.49	<.01	<.01	.001	<.01	<.01	.01	2.90	.02	.212	26.47	.03	.15	.02	.06	<.01	.90	6	21	12	5.40
267390 (rock)	<.001	.003	<.02	<.01	<2	.004	.001	.10	4.23	<.01	.05	.001	<.01	<.01	.01	4.66	.05	.002	2.09	.34	9.52	2.93	1.36	<.01	<.01	<2	<2	<2	.28
267391	<.001	.027	<.02	<.01	<2	.200	.016	.16	11.10	<.01	<.01	.001	<.01	<.01	.02	4.30	.01	.223	24.44	.04	.22	.20	.01	<.01	1.31	2	14	13	5.89
RE 267391	<.001	.028	<.02	<.01	<2	.207	.017	.17	11.19	<.01	<.01	.001	<.01	<.01	.02	4.27	.01	.225	24.72	.04	.21	.22	.03	<.01	1.29	16	14	19	-
RRE 267391	<.001	.028	<.02	<.01	<2	.207	.017	.17	11.16	<.01	<.01	.001	<.01	<.01	.02	4.34	.01	.229	24.92	.04	.20	.08	<.01	<.01	1.26	8	11	21	-
267392	<.001	.020	<.02	<.01	<2	.187	.017	.17	11.45	<.01	<.01	.001	<.01	<.01	.01	1.99	.01	.223	28.23	.04	.15	.01	.02	<.01	.97	<2	3	2	5.75
267393	<.001	.017	<.02	<.01	<2	.186	.017	.18	10.85	<.01	<.01	.001	<.01	<.01	.01	1.48	.01	.289	28.58	.02	.10	.01	.02	<.01	.90	<2	13	3	5.60
267394	<.001	.017	<.02	<.01	<2	.195	.015	.17	10.62	<.01	<.01	.001	<.01	<.01	.01	1.57	.01	.223	28.23	.01	.11	.01	<.01	<.01	.84	<2	11	2	6.02
STANDARD R-2a	.051	.584	1.74	4.45	173	.394	.049	.26	25.69	.23	.15	.032	.14	<.01	.02	3.95	.10	.066	2.90	.19	3.02	.50	.72	.08	5.35	489	487	489	-

Standard is STANDARD R-2a/CSB/FA-10R.

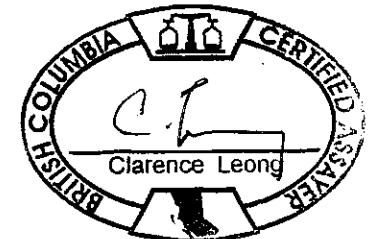
GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCl) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.

TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B BY FIRE ASSAY &amp; ANALYSIS BY ICP. (30 gm)

- SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data n FA \_\_\_\_\_

DATE RECEIVED: AUG 8 2005

DATE REPORT MAILED: Aug 25/05

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.



ACME ANALYTICAL



ACME ANALYTICAL

SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267395	<.001	.012	<.02	.01	<2	.194	.014	.17	9.65	<.01	<.01	<.001	<.01	<.01	.01	2.05	.01	.213	28.85	.02	.19	.27	.02	<.01	.49	2	7	9	5.65
267396	<.001	.009	<.02	.01	<2	.228	.014	.16	9.49	<.01	<.01	<.001	<.01	<.01	.01	1.42	.01	.136	29.60	.02	.10	.13	.02	<.01	.39	<2	9	9	5.45
267397	<.001	.008	<.02	.01	<2	.234	.013	.17	9.21	<.01	<.01	<.001	<.01	<.01	.01	1.55	.01	.130	30.52	.02	.10	.34	.01	<.01	.32	6	4	10	5.44
.STD RTS-2	<.001	.076	<.02	.01	<2	.275	.008	.04	38.99	<.01	<.01	<.001	<.01	<.01	.01	.64	.01	.013	.49	.18	.83	.26	.20	<.01	18.59	-	-	-	-
267398	<.001	.010	<.02	.01	<2	.232	.013	.16	9.93	<.01	<.01	<.001	<.01	<.01	.01	1.22	.01	.148	30.34	.03	.17	.33	.05	<.01	.32	<2	3	3	6.03
267399	<.001	.012	<.02	.01	<2	.228	.014	.17	10.01	<.01	<.01	<.001	<.01	<.01	.01	1.54	.01	.179	29.96	.02	.14	.12	<.01	<.01	.50	<2	2	2	6.07
267400 (pulp)	<.001	.059	<.02	.02	<2	.246	.012	.12	9.47	<.01	<.01	<.001	<.01	<.01	.02	4.86	.01	1.036	15.99	.21	4.26	.57	.13	<.01	.53	18	53	261	-
STANDARD R-2a	.051	.576	1.67	4.37	168	.388	.048	.26	26.03	.23	.16	.031	.14	<.01	.02	3.96	.08	.058	2.73	.20	2.98	.60	.71	.08	5.37	490	476	473	-

Standard is STANDARD R-2a/CSB/FA-10R.

ASSAY CERTIFICATE



Hard Creek Nickel Corporation PROJECT Tur C05-75B File # A504245 Page 1

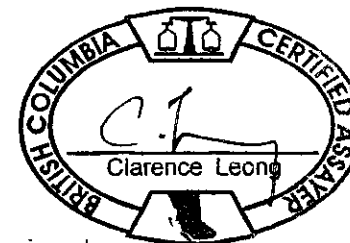
1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens

SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267364	.016	.200	.012	1.27
267365	.013	.162	.009	1.08
267366	.015	.184	.010	1.08
267367	.015	.212	.014	1.47
267368	.011	.131	.007	1.16
267369	.009	.125	.006	1.02
267371A	.019	.139	.007	1.23
267371B	.020	.139	.006	1.09
267372	.021	.166	.009	1.15
267373	.023	.230	.012	1.26
267374	.022	.244	.013	1.53
267375 (pulp)	.057	.197	.008	.55
267376	.042	.275	.019	1.52
267377	.020	.138	.009	1.34
267378	.021	.198	.011	1.42
. STD RTS-2	.059	.235	.008	4.46
267379	.009	.120	.007	1.09
267380	.012	.145	.006	1.23
267381	.015	.161	.007	1.33
267382	.020	.155	.009	1.28
267383	.028	.153	.011	1.46
267384	.026	.169	.014	1.30
267385	.033	.248	.014	1.64
267386	.023	.219	.010	1.43
267387	.013	.140	.007	1.31
267388	.007	.126	.005	1.14
267389	.022	.139	.009	1.41
267390 (rock)	.004	.001	<.001	.16
267391	.026	.178	.013	1.24
RE 267391	.026	.182	.013	1.24
RRE 267391	.026	.177	.013	1.18
267392	.019	.151	.012	1.24
267393	.017	.137	.010	1.14
267394	.017	.149	.010	1.21
STANDARD R-2a	.525	.331	.043	7.99

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
- SAMPLE TYPE: DRILL CORE R150  
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Sept 3/05





SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267395	.010	.116	.007	1.16
267396	.008	.133	.007	1.02
267397	.007	.120	.006	1.15
.STD RTS-2	.061	.232	.008	3.53
267398	.008	.121	.006	1.02
267399	.011	.141	.007	1.22
267400 (pulp)	.059	.202	.008	.55
STANDARD R-2a	.530	.325	.042	8.33

Sample type: DRILL CORE R150.

ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-75C File # A504246 Page 1

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267401	<.001	.017	<.02	<.01	<2	.227	.017	.16	10.66	<.01	<.01	<.001	<.01	<.01	<.01	1.21	.01	.097	28.94	.03	.25	.19	.11	<.01	.85	4	12	2	5.60
267402	<.001	.024	<.02	<.01	<2	.225	.016	.17	11.05	<.01	<.01	<.001	<.01	<.01	.01	1.75	.01	.096	29.05	.02	.15	.13	.05	<.01	1.04	<2	5	8	6.57
267403	<.001	.024	<.02	<.01	<2	.212	.017	.17	10.86	<.01	<.01	<.001	<.01	<.01	.01	1.21	.01	.136	30.07	.02	.09	.12	.05	<.01	.93	3	18	4	6.18
267404	<.001	.038	<.02	<.01	<2	.197	.015	.16	11.36	<.01	<.01	<.001	<.01	<.01	.02	2.15	.01	.119	26.80	.03	.16	.06	.03	<.01	1.72	3	11	27	6.07
267405	<.001	.036	<.02	<.01	<2	.188	.019	.16	11.64	<.01	<.01	<.001	<.01	<.01	.01	.84	.01	.086	29.57	.01	.10	<.01	.07	<.01	1.48	5	11	17	5.80
267406	<.001	.035	<.02	<.01	<2	.261	.016	.16	10.74	<.01	<.01	<.001	<.01	<.01	<.01	1.46	.01	.090	29.86	.02	.13	<.01	<.01	<.01	.87	7	11	16	5.55
267407	<.001	.016	<.02	<.01	<2	.280	.017	.16	9.40	<.01	<.01	<.001	<.01	<.01	<.01	.17	.02	.085	31.76	.01	.07	.06	<.01	<.01	.51	4	11	12	6.23
267408	<.001	.013	<.02	<.01	3	.221	.013	.14	7.72	<.01	<.01	<.001	<.01	<.01	<.01	2.17	.01	.157	29.72	.03	.20	<.01	<.01	<.01	.15	4	18	15	5.47
267409	<.001	.030	<.02	<.01	<2	.231	.016	.14	8.48	<.01	<.01	<.001	<.01	<.01	<.01	.67	.01	.197	29.41	.02	.15	<.01	.04	<.01	.34	2	10	8	6.09
267410	<.001	.011	<.02	<.01	<2	.059	.008	.19	8.06	<.01	.11	<.001	<.01	<.01	.02	8.44	.15	.058	13.08	.34	4.61	.19	1.02	<.01	.20	5	<2	5	2.23
RE 267410	<.001	.011	<.02	<.01	2	.058	.008	.19	8.05	<.01	.11	<.001	<.01	<.01	.02	8.49	.14	.055	12.91	.34	4.68	.35	1.06	<.01	.20	5	15	7	-
RRE 267410	<.001	.011	<.02	<.01	<2	.058	.008	.19	7.97	<.01	.11	<.001	<.01	<.01	.02	8.44	.14	.053	12.40	.34	4.70	.45	1.09	<.01	.20	9	9	8	-
267411	<.001	.007	<.02	<.01	<2	.012	.002	.15	5.80	<.01	.08	<.001	<.01	<.01	.02	6.09	.11	.008	3.78	.34	9.08	3.41	2.22	<.01	.02	<2	<2	3	7.23
267413	<.001	.008	<.02	<.01	<2	.008	.002	.14	5.63	<.01	.08	<.001	<.01	<.01	.02	5.82	.11	.006	3.31	.33	9.08	3.94	2.00	<.01	<.02	<2	12	9	5.11
267415	<.001	.006	<.02	<.01	2	.010	.003	.17	6.85	<.01	.16	<.001	<.01	<.01	.03	7.04	.14	.006	3.84	.43	10.32	2.25	2.93	<.01	<.02	<2	6	4	4.94
267416	<.001	.011	<.02	<.01	<2	.229	.011	.10	7.71	<.01	<.01	<.001	<.01	<.01	<.01	1.50	.02	.131	25.60	.04	.70	.13	.06	<.01	.40	4	40	30	6.05
267417	<.001	.009	<.02	<.01	<2	.177	.009	.09	7.01	<.01	.03	<.001	<.01	<.01	.01	4.33	.04	.105	21.13	.09	2.09	<.01	.08	<.01	.37	6	35	28	6.03
.STD RTS-2	<.001	.075	<.02	<.01	<2	.266	.007	.04	38.27	<.01	<.01	<.001	<.01	<.01	.01	.66	.02	.011	.51	.18	.92	.36	.20	<.01	18.56	-	-	-	-
267418	<.001	.010	<.02	<.01	<2	.006	.002	.17	7.51	<.01	.12	<.001	<.01	<.01	.03	9.64	.13	.004	3.42	.48	9.42	1.68	2.38	<.01	<.02	5	7	2	4.89
267419	<.001	.044	<.02	<.01	<2	.184	.011	.08	6.20	<.01	<.01	<.001	<.01	<.01	<.01	2.60	.02	.072	23.12	.03	.69	.28	.08	<.01	.54	3	17	20	4.07
267420 (rock)	<.001	.005	<.02	<.01	2	.002	<.001	.10	4.41	<.01	.05	<.001	<.01	<.01	.01	4.49	.05	.001	1.86	.34	9.16	2.44	1.34	<.01	<.02	<2	2	2	2.71
267421	<.001	.034	<.02	<.01	<2	.253	.013	.14	8.64	<.01	<.01	<.001	<.01	<.01	<.01	.24	.01	.117	29.56	.02	.15	<.01	<.01	<.01	.20	7	38	45	6.88
267422	<.001	.025	<.02	<.01	<2	.379	.018	.15	8.94	<.01	<.01	<.001	<.01	<.01	<.01	.64	.01	.048	29.08	.02	.12	<.01	.07	<.01	.73	9	52	47	4.52
267423	<.001	.026	<.02	<.01	<2	.222	.019	.14	9.63	<.01	<.01	<.001	<.01	<.01	<.01	.30	.01	.057	29.03	.01	.06	<.01	.09	<.01	.96	3	23	29	5.56
267424	<.001	.017	<.02	<.01	<2	.216	.014	.12	8.42	<.01	<.01	<.001	<.01	<.01	<.01	.50	.01	.091	28.46	.03	.25	.20	.12	<.01	.38	<2	17	16	4.23
267425 (pulp)	<.001	.099	<.02	<.01	<2	.334	.016	.05	9.40	<.01	<.01	<.001	<.01	<.01	.01	3.31	.01	.320	15.64	.15	2.70	.21	.12	<.01	1.16	24	142	409	-
267426	<.001	.007	<.02	<.01	<2	.224	.015	.15	8.87	<.01	<.01	<.001	<.01	<.01	<.01	.35	.01	.139	29.79	.01	.08	.13	.06	<.01	.25	4	23	16	5.67
267427	<.001	.011	<.02	<.01	<2	.323	.017	.14	9.12	<.01	<.01	<.001	<.01	<.01	<.01	.14	<.01	.116	29.92	.01	.06	<.01	.04	<.01	.50	3	23	26	5.42
267428	<.001	.013	<.02	<.01	<2	.244	.014	.14	8.51	<.01	<.01	<.001	<.01	<.01	<.01	.94	.01	.158	29.07	.05	.22	<.01	.02	<.01	.28	4	6	18	4.33
267429	<.001	.003	<.02	<.01	<2	.239	.014	.14	8.64	<.01	<.01	<.001	<.01	<.01	<.01	.31	.01	.143	30.38	.01	.09	<.01	.02	<.01	.11	4	21	31	3.78
267431A	<.001	.003	<.02	<.01	<2	.111	.007	.07	4.41	<.01	<.01	<.001	<.01	<.01	<.01	.21	<.01	.077	15.04	.01	.02	.22	<.01	<.01	.12	7	18	10	5.34
267431B	<.001	.010	<.02	<.01	<2	.227	.014	.14	8.63	<.01	<.01	<.001	<.01	<.01	<.01	.30	.01	.145	29.65	.01	.07	<.01	.01	<.01	.12	9	12	13	-
267432	<.001	.014	<.02	.01	<2	.245	.015	.15	9.04	<.01	<.01	<.001	<.01	<.01	<.01	.67	<.01	.174	30.14	.01	.09	<.01	.06	<.01	.14	3	19	12	7.08
267433	<.001	.021	<.02	.01	<2	.218	.015	.14	9.05	<.01	<.01	<.001	<.01	<.01	<.01	.48	.01	.241	30.32	.01	.08	.05	.04	<.01	.11	3	5	15	5.52
STANDARD R-2a	.051	.587	1.77	4.42	175	.390	.049	.26	26.63	.23	.16	.032	.14	<.01	.02	3.97	.10	.042	3.01	.20	2.96	.52	.70	.10	5.40	491	492	490	-

Standard is STANDARD R-2a/CSB/FA-10R.

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCL) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.

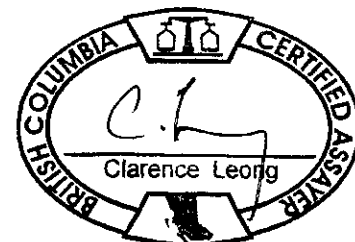
TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B BY FIRE ASSAY & ANALYSIS BY ICP. (30 gm)

- SAMPLE TYPE: DRILL CORE R150

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Aug 25/05





SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267434	<.001	.007	<.02	.01	<2	.237	.015	.15	8.66	<.01	<.01	<.001	<.01	<.01	<.01	.24	.01	.306	31.93	.01	.11	<.01	.02	<.01	.07	<2	25	27	5.58
267435	<.001	.016	<.02	.01	<2	.236	.015	.15	8.44	<.01	<.01	<.001	<.01	<.01	<.01	.20	.01	.187	32.18	.01	.07	.11	<.01	<.01	.14	3	10	10	6.27
267436	<.001	.026	<.02	.01	<2	.268	.017	.16	8.93	<.01	<.01	<.001	<.01	<.01	<.01	.24	.02	.220	32.45	.01	.06	<.01	.07	<.01	.13	<2	15	11	5.54
.STD RTS-2	<.001	.075	<.02	.01	2	.270	.008	.04	38.89	<.01	<.01	<.001	<.01	<.01	.01	.61	.01	.014	.48	.18	.87	.17	.19	<.01	18.45	-	-	-	-
267437	<.001	.013	<.02	.01	<2	.227	.015	.14	8.74	<.01	<.01	<.001	<.01	<.01	<.01	.26	.01	.203	30.70	.02	.09	.10	.04	<.01	.08	2	2	2	4.66
267438	<.001	.018	<.02	<.01	<2	.228	.017	.14	9.00	<.01	<.01	<.001	<.01	<.01	<.01	.16	.01	.191	30.97	.01	.08	.17	<.01	<.01	.33	<2	5	5	5.58
267439	<.001	.020	<.02	.01	<2	.213	.016	.14	8.80	<.01	<.01	<.001	<.01	<.01	<.01	.48	.01	.217	30.83	.01	.08	.02	.03	<.01	.28	2	6	5	4.53
STANDARD R	.051	.576	1.67	4.37	168	.384	.048	.26	26.31	.23	.16	.031	.14	<.01	.02	3.96	.08	.058	2.73	.20	2.98	.60	.71	.08	5.44	490	482	482	-

Standard is STANDARD R-2a/CSB/FA-10R.



ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-75C File # A504246 Page 1

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchins

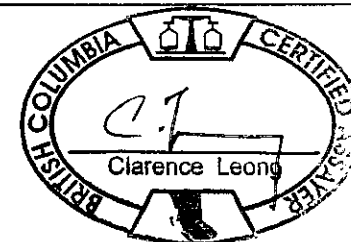


SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267401	.018	.174	.010	1.40
267402	.024	.178	.009	1.40
267403	.025	.156	.009	1.31
267404	.036	.167	.011	1.18
267405	.036	.164	.012	1.17
267406	.033	.179	.010	1.09
267407	.013	.155	.007	.95
267408	.013	.081	.004	.82
267409	.029	.151	.009	1.13
267410	.011	.053	.006	.53
RE 267410	.011	.054	.005	.55
RRE 267410	.010	.051	.006	.64
267411	.008	.002	<.001	.13
267413	.009	.003	<.001	.14
267415	.005	.004	<.001	.15
267416	.011	.182	.008	.72
267417	.008	.135	.006	.54
.STD RTS-2	.057	.225	.006	3.81
267418	.010	.004	<.001	.12
267419	.040	.150	.008	.59
267420 (rock)	.004	<.001	<.001	.12
267421	.031	.125	.006	.83
267422	.023	.248	.009	1.04
267423	.025	.173	.013	.95
267424	.016	.121	.007	.96
267425 (pulp)	.093	.267	.012	1.41
267426	.005	.084	.004	1.03
267427	.011	.150	.006	1.12
267428	.012	.098	.004	.87
267429	.004	.084	.004	.83
267431A	.009	.086	.005	.87
267431B	.009	.081	.004	.81
267432	.011	.094	.005	.93
267433	.019	.078	.005	.93
STANDARD R-2a	.522	.327	.038	8.00

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
- SAMPLE TYPE: DRILL CORE R150  
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data h FA \_\_\_\_\_

DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Sept 3/05.....





SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267434	.005	.080	.005	1.03
267435	.014	.077	.005	1.18
267436	.025	.092	.005	1.24
267437	.011	.103	.006	1.07
267438	.017	.103	.006	1.20
267439	.018	.104	.007	1.06
STANDARD R-2a	.531	.330	.041	8.46

Sample type: DRILL CORE R150.

ASSAY CERTIFICATE



Hard Creek Nickel Corporation PROJECT Tur C05-76A File # A504247

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens

SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267440	<.001	.016	<.02	.01	<2	.245	.011	.09	5.41	<.01	<.001	<.01	<.01	<.01	<.01	.61	.03	.201	25.43	.05	.75	.19	.02	<.01	.31	<2	19	17	4.62
267441	<.001	.026	<.02	<.01	<2	.263	.016	.11	6.20	<.01	<.01	<.001	<.01	<.01	<.01	.42	.01	.182	28.41	.01	.32	<.01	<.01	<.01	.34	6	10	12	2.65
267442	<.001	.040	<.02	<.01	<2	.259	.017	.11	6.46	<.01	<.01	<.001	<.01	<.01	<.01	.59	.01	.181	28.24	<.01	.13	.04	.04	<.01	.52	7	49	57	4.46
267443	<.001	.040	<.02	<.01	<2	.273	.017	.11	7.22	<.01	<.01	<.001	<.01	<.01	<.01	.31	.01	.144	31.13	<.01	.11	<.01	.01	<.01	.40	13	22	26	5.10
267444	<.001	.045	<.02	<.01	<2	.262	.017	.11	7.14	<.01	<.01	<.001	<.01	<.01	<.01	.52	.01	.342	29.99	.01	.08	.10	<.01	<.01	.55	10	19	24	5.22
267445	<.001	.038	<.02	<.01	<2	.259	.015	.10	6.24	<.01	<.01	<.001	<.01	<.01	<.01	.20	.01	.232	28.01	.01	.37	.17	.02	<.01	.62	8	44	46	4.86
267446	<.001	.039	<.02	<.01	<2	.268	.015	.10	5.33	<.01	<.01	<.001	<.01	<.01	<.01	2.51	.01	.137	22.22	.01	1.46	.23	.49	<.01	.60	4	21	22	4.28
267447	<.001	.037	<.02	<.01	<2	.260	.021	.11	7.95	<.01	<.01	<.001	<.01	<.01	<.01	.51	.01	.131	28.29	.01	.07	.15	<.01	<.01	.67	7	15	16	4.02
267448	<.001	.017	<.02	.01	<2	.035	.004	.17	7.20	<.01	.08	<.001	<.01	<.01	.03	6.27	.14	.036	7.11	.47	7.36	2.79	1.67	<.01	.22	<2	9	12	4.35
267449	<.001	.034	<.02	<.01	<2	.269	.015	.11	7.56	<.01	<.01	<.001	<.01	<.01	<.01	.15	.01	.236	30.37	.01	.07	.35	<.01	<.01	.46	3	29	35	4.70
RE 267449	<.001	.034	<.02	<.01	<2	.273	.016	.11	7.47	<.01	<.01	<.001	<.01	<.01	<.01	.14	.01	.239	30.11	.01	.04	.14	.04	<.01	.48	2	25	27	-
RRE 267449	<.001	.037	<.02	.01	<2	.277	.016	.11	7.66	<.01	<.01	<.001	<.01	<.01	<.01	.13	.01	.244	30.84	.01	.06	.14	<.01	<.01	.46	2	19	28	-
267450 (pulp)	<.001	.099	<.02	<.01	2	.353	.017	.05	9.27	<.01	<.01	<.001	<.01	.01	.01	3.58	.01	.375	16.97	.15	2.77	.21	.06	<.01	1.11	26	111	401	-
.STD RTS-2	<.001	.074	<.02	.01	<2	.271	.007	.04	38.05	<.01	<.01	<.001	<.01	<.01	.01	.61	.01	.013	.40	.18	.78	.20	.20	<.01	17.75	-	-	-	-
267451	<.001	.038	<.02	<.01	<2	.238	.014	.15	7.04	<.01	.02	<.001	<.01	<.01	<.01	1.44	.03	.156	24.37	.07	1.96	.74	.34	<.01	.55	4	27	35	4.79
267452	<.001	.081	<.02	<.01	<2	.293	.019	.13	8.27	<.01	<.01	<.001	<.01	<.01	<.01	.19	.01	.149	31.79	<.01	.03	<.01	.02	<.01	.59	26	45	39	5.88
267453	<.001	.101	<.02	<.01	<2	.370	.021	.13	8.76	<.01	<.01	<.001	<.01	<.01	<.01	.16	.02	.128	31.95	.01	.03	<.01	<.01	<.01	.81	8	40	40	6.26
267454	<.001	.081	<.02	<.01	<2	.305	.021	.13	8.77	<.01	<.01	<.001	<.01	<.01	<.01	.20	.01	.199	31.10	.01	.01	.18	<.01	<.01	.92	8	17	17	5.34
267455	<.001	.055	<.02	<.01	<2	.223	.025	.14	9.92	<.01	<.01	<.001	<.01	<.01	<.01	.23	.01	.152	31.02	.01	.02	.03	<.01	<.01	1.35	5	23	27	5.50
267456	<.001	.045	<.02	<.01	<2	.231	.023	.14	10.04	<.01	<.01	<.001	<.01	<.01	<.01	.08	.01	.141	31.28	<.01	.03	<.01	<.01	<.01	1.32	<2	17	18	5.55
267457	<.001	.021	<.02	<.01	<2	.254	.018	.12	7.98	<.01	<.01	<.001	<.01	.01	<.01	.27	.01	.151	31.58	.01	.03	<.01	<.01	<.01	.71	3	22	18	5.37
267458	<.001	.030	<.02	<.01	<2	.131	.024	.14	10.83	<.01	<.01	<.001	<.01	<.01	<.01	.11	.02	.111	30.76	<.01	.02	<.01	<.01	<.01	1.75	2	9	12	5.50
267459	<.001	.035	<.02	<.01	<2	.164	.021	.14	10.39	<.01	<.01	<.001	<.01	<.01	<.01	.23	.01	.073	30.82	.01	.02	<.01	<.01	<.01	1.41	6	38	33	5.26
267460A	<.001	.023	<.02	<.01	<2	.176	.017	.14	8.64	<.01	.01	<.001	<.01	<.01	<.01	1.15	.02	.169	26.89	.05	.95	.08	.32	<.01	.86	2	7	11	4.58
267460B	<.001	.022	<.02	<.01	<2	.178	.018	.14	8.68	<.01	.01	<.001	<.01	<.01	<.01	1.16	.02	.159	27.26	.05	.92	<.01	.28	<.01	.85	2	9	14	-
STANDARD R-2a	.051	.577	1.73	4.33	170	.386	.048	.26	25.10	.23	.15	.030	.13	<.01	.02	3.95	.09	.066	2.76	.20	2.82	.78	.71	.09	5.31	490	476	473	-

Standard is STANDARD R-2a/CSB/FA-10R.

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCL) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.

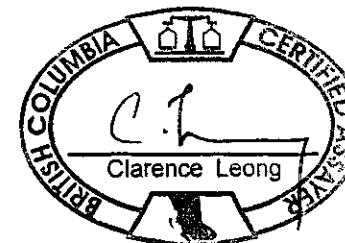
TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B BY FIRE ASSAY & ANALYSIS BY ICP. (30 gm)

- SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data    FA   

DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED:   

*Aug 23/05*



ASSAY CERTIFICATE



Hard Creek Nickel Corporation PROJECT Tur C05-76A File # A504247

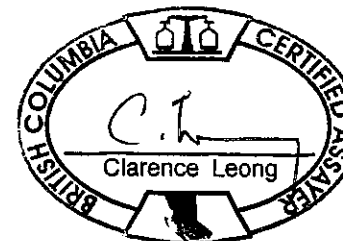
1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens

SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267440	.015	.159	.008	.47
267441	.025	.164	.009	.54
267442	.038	.196	.012	.72
267443	.039	.189	.011	.69
267444	.045	.200	.011	.79
267445	.038	.231	.013	.59
267446	.040	.231	.013	.68
267447	.036	.227	.017	1.33
267448	.016	.023	.002	.30
267449	.033	.182	.010	1.03
RE 267449	.033	.189	.010	1.06
RRE 267449	.035	.186	.010	1.10
267450 (pulp)	.097	.265	.013	1.27
.STD RTS-2	.059	.221	.007	3.79
267451	.038	.183	.010	1.26
267452	.081	.183	.009	1.47
267453	.103	.253	.010	1.50
267454	.080	.229	.014	1.62
267455	.055	.180	.017	1.55
267456	.042	.185	.015	1.43
267457	.021	.140	.011	1.44
267458	.030	.111	.017	1.51
267459	.034	.130	.014	1.37
267460A	.022	.124	.013	1.28
267460B	.022	.122	.013	1.23
STANDARD R-2a	.536	.332	.044	8.25

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
- SAMPLE TYPE: DRILL CORE R150  
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data K FA \_\_\_\_\_

DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Aug 30/05 .....



(IS 001 Accredited Co.)

ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-76B File # A504130 Page 1

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens

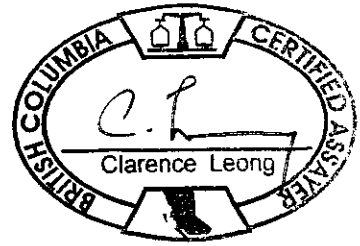


SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267461	<.001	.026	<.02	<.01	<2	.158	.023	.12	8.41	<.01	<.01	<.001	<.01	<.01	<.01	.13	.01	.146	29.11	.01	.23	.09	.05	<.01	.72	2	4	8	6.03
267462	<.001	.040	<.02	<.01	<2	.347	.026	.12	8.14	<.01	<.01	<.001	<.01	<.01	<.01	.47	.01	.177	30.75	.01	.05	<.01	<.01	<.01	.75	20	19	21	5.05
267463	<.001	.039	<.02	<.01	<2	.421	.025	.11	7.35	<.01	<.01	<.001	<.01	<.01	<.01	.51	.01	.116	31.18	.01	.05	.04	.04	<.01	.66	9	29	23	4.95
267464	<.001	.023	<.02	<.01	<2	.322	.015	.12	7.43	<.01	<.01	<.001	<.01	<.01	<.01	.57	.02	.158	31.18	.01	.11	<.01	<.01	<.01	.36	6	38	38	5.10
267465	<.001	.007	<.02	<.01	<2	.291	.015	.13	7.46	<.01	<.01	<.001	<.01	<.01	<.01	.52	.02	.114	33.21	<.01	.04	<.01	<.01	<.01	.12	<2	25	18	5.71
267466	<.001	.007	<.02	<.01	<2	.315	.014	.14	7.81	<.01	<.01	<.001	<.01	<.01	<.01	.81	.01	.107	32.10	.01	.05	.04	<.01	<.01	.22	<2	44	48	5.83
267467	<.001	.006	<.02	<.01	<2	.313	.013	.13	6.93	<.01	<.01	<.001	<.01	<.01	<.01	.73	.01	.064	32.27	.01	.03	<.01	.03	<.01	.22	4	36	40	5.56
267468	<.001	.006	<.02	<.01	<2	.297	.014	.12	6.80	<.01	<.01	<.001	<.01	<.01	<.01	.34	.01	.121	31.88	.01	.04	<.01	<.01	<.01	.23	<2	24	16	4.99
267469	<.001	.006	<.02	<.01	<2	.288	.013	.12	6.75	<.01	<.01	<.001	<.01	<.01	<.01	.50	.01	.155	30.38	.01	.04	.04	.02	<.01	.18	3	24	18	5.26
267470	<.001	.006	<.02	<.01	<2	.281	.013	.12	7.02	<.01	<.01	<.001	<.01	<.01	<.01	.45	.01	.237	30.15	.01	.05	.03	.03	<.01	.17	4	13	9	5.13
267471	<.001	.006	<.02	<.01	<2	.281	.013	.12	6.89	<.01	<.01	<.001	<.01	<.01	<.01	.39	.01	.181	30.57	.01	.05	<.01	.01	<.01	.15	7	7	6	5.30
267472	<.001	.005	<.02	<.01	<2	.278	.013	.11	6.26	<.01	<.01	<.001	<.01	<.01	<.01	.53	.01	.208	30.90	.01	.10	.09	.05	<.01	.15	2	3	2	4.99
267473	<.001	.002	<.02	<.01	<2	.271	.013	.12	6.53	<.01	<.01	<.001	<.01	<.01	<.01	.69	.01	.179	30.98	.03	.27	.09	<.01	<.01	.12	2	<2	6	5.40
267474	<.001	.002	<.02	<.01	<2	.269	.014	.12	6.48	<.01	<.01	<.001	<.01	<.01	<.01	.52	.02	.202	31.79	.02	.14	<.01	.03	<.01	.09	3	<2	4	5.93
267475 (pulp)	<.001	.056	<.02	.01	<2	.234	.013	.12	8.97	<.01	<.01	<.001	<.01	<.01	.02	4.65	.01	1.064	14.89	.20	3.95	.36	.12	<.01	.52	13	92	275	-
.STD RTS-2	<.001	.072	<.02	<.01	<2	.268	.010	.04	38.42	<.01	<.01	<.001	<.01	.01	.01	.63	.02	.011	.35	.18	.84	.08	.16	<.01	18.28	-	-	-	-
267476	<.001	.004	<.02	<.01	<2	.275	.012	.11	6.14	<.01	<.01	<.001	<.01	<.01	<.01	.14	.01	.210	30.06	.01	.13	.03	.02	<.01	.16	2	20	8	4.70
267477	<.001	.018	<.02	<.01	<2	.249	.021	.12	8.04	<.01	<.01	<.001	<.01	<.01	<.01	.63	.01	.147	28.62	.02	.33	<.01	.03	<.01	.77	<2	22	15	5.34
267478	<.001	.012	<.02	<.01	<2	.261	.016	.15	8.52	<.01	<.01	<.001	<.01	<.01	<.01	.11	.02	.153	28.30	.01	.09	.02	<.01	<.01	.38	6	68	51	4.33
267479	<.001	.012	<.02	<.01	<2	.265	.016	.15	8.53	<.01	<.01	<.001	<.01	<.01	<.01	.14	.02	.148	28.50	.01	.10	<.01	.01	<.01	.22	<2	53	47	4.76
267480 (rock)	<.001	.005	<.02	<.01	<2	.003	.001	.11	4.17	<.01	.05	<.001	<.01	<.01	.01	4.62	.06	.002	1.87	.33	8.68	2.54	1.26	<.01	<.02	<2	<2	2	2.52
267481	.001	.033	<.02	<.01	<2	.232	.018	.16	10.46	<.01	<.01	<.001	<.01	<.01	.01	.72	.01	.116	28.65	.01	.03	.07	.03	<.01	1.46	5	33	24	6.02
267482	.001	.025	<.02	<.01	<2	.255	.014	.16	9.18	<.01	<.01	<.001	<.01	<.01	.01	1.38	.02	.154	27.16	.01	.11	<.01	<.01	<.01	1.28	<2	15	10	5.28
RE 267482	.001	.025	<.02	<.01	<2	.251	.014	.16	9.14	<.01	<.01	<.001	<.01	<.01	.01	1.35	.02	.146	27.04	.01	.09	<.01	<.01	<.01	1.25	2	14	8	-
RRE 267482	<.001	.026	<.02	<.01	<2	.259	.015	.16	9.32	<.01	<.01	<.001	<.01	<.01	.01	1.47	.02	.149	27.79	.01	.11	.02	.01	<.01	1.26	<2	19	11	-
267483	<.001	.023	<.02	<.01	<2	.324	.017	.13	8.51	<.01	<.01	<.001	<.01	<.01	<.01	.36	.02	.167	29.83	.01	.03	<.01	.02	<.01	1.02	6	35	30	5.34
267484	<.001	.020	<.02	<.01	<2	.295	.016	.12	7.30	<.01	<.01	<.001	<.01	<.01	<.01	.26	.02	.249	30.07	.01	.05	.02	.07	<.01	.46	11	29	29	5.44
267485	<.001	.012	<.02	<.01	<2	.291	.016	.12	7.13	<.01	<.01	<.001	<.01	<.01	<.01	.21	.02	.173	31.63	.01	.04	.01	.05	<.01	.43	<2	20	21	4.50
267486	<.001	.028	<.02	<.01	<2	.355	.016	.11	6.84	<.01	<.01	<.001	<.01	<.01	<.01	.54	.02	.173	31.93	.01	.05	<.01	.04	<.01	.48	4	12	12	5.18
267487	<.001	.012	<.02	<.01	<2	.287	.014	.11	7.02	<.01	<.01	<.001	<.01	<.01	<.01	.31	.02	.157	31.98	.01	.04	<.01	.05	<.01	.40	6	49	21	5.37
267488	<.001	.006	<.02	<.01	<2	.280	.014	.11	6.82	<.01	<.01	<.001	<.01	<.01	<.01	.34	.01	.112	31.15	.01	.03	<.01	.05	<.01	.29	4	6	7	5.30
267489	<.001	.019	<.02	<.01	<2	.313	.014	.11	6.46	<.01	<.01	<.001	<.01	<.01	<.01	.64	.02	.143	30.69	.01	.21	<.01	.03	<.01	.35	3	12	14	5.74
267490A	<.001	.006	<.02	<.01	<2	.275	.014	.12	6.86	<.01	<.01	<.001	<.01	<.01	<.01	.15	.02	.244	31.36	.01	.06	<.01	.04	<.01	.19	6	19	15	5.45
267490B	<.001	.007	<.02	<.01	<2	.278	.014	.12	6.93	<.01	<.01	<.001	<.01	<.01	<.01	.17	.02	.262	31.54	.01	.04	.06	.03	<.01	.20	<2	20	16	-
STANDARD R-2a	.052	.568	1.68	4.27	169	.383	.050	.26	25.31	.23	.15	.031	.14	<.01	.02	3.92	.09	.064	2.59	.20	2.84	.53	.68	.08	5.32	486	475	483	-

Standard is STANDARD R-2a/CSB/FA-10R.

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCl) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.  
 TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B BY FIRE ASSAY & ANALYSIS BY ICP. (30 gm)  
 - SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data h FA \_\_\_\_\_ DATE RECEIVED: AUG 3 2005 DATE REPORT MAILED: Aug 17/05



All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267491	<.001	.015	<.02	<.01	<2	.378	.015	.11	6.74	<.01	<.01	<.001	<.01	<.01	<.01	.51	.01	.126	33.54	.01	.05	.26	<.01	<.01	.26	8	55	45	5.37
267492	<.001	.022	<.02	<.01	<2	.414	.016	.11	6.57	<.01	<.01	<.001	<.01	<.01	<.01	.23	.01	.407	32.67	.01	.09	.04	<.01	<.01	.40	4	65	62	5.24
267493	<.001	.010	<.02	<.01	<2	.313	.015	.11	6.86	<.01	<.01	<.001	<.01	.01	.01	.33	.01	.439	32.56	.01	.15	.21	<.01	<.01	.28	3	48	47	2.68
267494	<.001	.017	<.02	<.01	<2	.298	.015	.10	7.52	<.01	<.01	<.001	<.01	<.01	.01	.29	.01	.240	30.11	.02	.11	.21	<.01	<.01	.81	9	42	41	5.12
267495	<.001	.029	<.02	<.01	<2	.223	.018	.11	8.76	<.01	<.01	<.001	<.01	<.01	<.01	.20	.01	.190	30.74	.01	.09	.09	<.01	<.01	1.23	8	13	14	5.66
267496	<.001	.022	<.02	<.01	<2	.299	.021	.13	9.15	<.01	<.01	<.001	<.01	<.01	<.01	.16	.01	.130	31.70	.01	.06	.31	<.01	<.01	1.07	8	23	28	5.85
267497	<.001	.022	<.02	<.01	<2	.341	.021	.14	9.30	<.01	<.01	<.001	<.01	<.01	<.01	.13	.01	.103	32.10	<.01	.02	<.01	<.01	<.01	.94	19	31	25	5.43
267498	<.001	.017	<.02	<.01	<2	.297	.018	.13	8.22	<.01	<.01	<.001	<.01	<.01	<.01	.07	.01	.159	32.75	<.01	.03	.09	<.01	<.01	.63	4	11	11	5.34
267499	<.001	.016	<.02	<.01	<2	.309	.015	.13	7.36	<.01	<.01	<.001	<.01	<.01	<.01	.16	.01	.185	32.91	<.01	.03	<.01	<.01	<.01	.31	8	21	21	5.32
.STD RTS-2	<.001	.073	<.02	.01	<2	.282	.008	.04	38.21	<.01	<.01	<.001	<.01	<.01	.01	.63	.01	.012	.36	.18	.82	.25	.08	<.01	18.28	-	-	-	-
267500 (pulp)	<.001	.098	<.02	<.01	<2	.354	.016	.05	9.38	<.01	<.01	<.001	<.01	<.01	.01	3.52	.01	.372	16.73	.15	2.62	.30	.04	<.01	1.14	39	111	395	-
267501	<.001	.017	<.02	<.01	<2	.319	.015	.12	7.18	<.01	<.01	<.001	<.01	<.01	<.01	.18	<.01	.134	32.29	.01	.02	.09	<.01	<.01	.42	8	12	13	5.43
267502	<.001	.018	<.02	<.01	<2	.345	.016	.13	7.65	<.01	<.01	<.001	<.01	<.01	<.01	.22	.01	.177	32.61	.01	.04	.19	<.01	<.01	.41	6	25	33	5.36
267503	<.001	.029	<.02	<.01	<2	.431	.019	.12	7.93	<.01	<.01	<.001	<.01	<.01	<.01	.10	.01	.139	32.32	<.01	.03	<.01	<.01	<.01	.79	11	56	82	5.81
267504	<.001	.027	<.02	<.01	<2	.297	.018	.12	8.11	<.01	<.01	<.001	<.01	<.01	<.01	.13	.01	.216	31.84	.01	.08	.19	<.01	<.01	.56	7	18	20	5.91
267505	<.001	.018	<.02	<.01	<2	.399	.017	.12	6.90	<.01	<.01	<.001	<.01	<.01	<.01	.80	.01	.173	31.48	.01	.09	<.01	<.01	<.01	.65	5	33	47	5.54
267506	<.001	.016	<.02	<.01	<2	.289	.017	.11	7.92	<.01	.05	<.001	<.01	<.01	<.01	1.89	.02	.123	26.83	.06	1.24	<.01	.02	<.01	.82	7	25	27	5.26
267507	<.001	.019	<.02	<.01	<2	.370	.022	.13	8.61	<.01	<.01	<.001	<.01	<.01	<.01	.06	.01	.092	31.66	<.01	.17	.02	<.01	<.01	1.05	7	23	33	5.51
267508	<.001	.015	<.02	<.01	<2	.342	.021	.13	8.49	<.01	<.01	<.001	<.01	<.01	<.01	.10	.01	.056	32.22	<.01	<.01	.07	<.01	<.01	.90	6	28	25	6.19
RE 267508	<.001	.015	<.02	<.01	<2	.343	.022	.13	8.57	<.01	<.01	<.001	<.01	<.01	<.01	.12	.01	.060	32.49	<.01	.03	.13	.01	<.01	.90	6	43	26	-
RRE 267508	<.001	.015	<.02	<.01	<2	.346	.021	.13	8.57	<.01	<.01	<.001	<.01	<.01	<.01	.12	.01	.068	32.63	<.01	.02	.29	<.01	<.01	.92	8	19	22	-
267509	<.001	.018	<.02	<.01	<2	.339	.019	.13	8.35	<.01	<.01	<.001	<.01	<.01	<.01	.18	<.01	.072	32.66	<.01	.04	<.01	<.01	<.01	.86	7	8	16	4.25
267510 (rock)	<.001	.003	<.02	.01	<2	.006	.002	.11	4.35	<.01	.05	<.001	<.01	<.01	.01	4.71	.05	.002	2.02	.35	8.92	2.38	1.34	<.01	.01	<2	<2	<2	2.52
267511	<.001	.019	<.02	<.01	<2	.339	.018	.11	7.75	<.01	<.01	<.001	<.01	<.01	<.01	.31	.01	.066	30.06	.03	.29	.06	<.01	<.01	.81	7	39	44	3.96
STANDARD R-2a	.051	.571	1.72	4.31	172	.386	.050	.25	25.00	.24	.16	.031	.14	<.01	.02	3.80	.08	.065	2.67	.20	2.77	.39	.64	.08	5.39	485	474	483	-

Standard is STANDARD R-2a/CSB/FA-10R. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-76B File # A504130 Page 1

Submitted by: Tony Hitchens

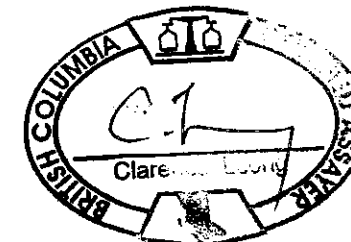


SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267461	.031	.118	.016	1.36
267462	.043	.261	.015	1.39
267463	.040	.310	.014	1.47
267464	.022	.192	.007	.99
267465	.006	.084	.003	.80
267466	.006	.132	.004	1.07
267467	.005	.146	.004	1.02
267468	.005	.143	.006	1.01
267469	.005	.154	.006	.92
267470	.005	.138	.006	.91
267471	.005	.123	.005	.97
267472	.004	.127	.005	.81
267473	.001	.119	.005	.74
267474	.001	.092	.005	.83
267475 (pulp)	.056	.192	.007	.52
.STD RTS-2	.057	.220	.007	3.38
267476	.003	.155	.006	.74
267477	.017	.197	.013	1.06
267478	.010	.179	.008	1.04
267479	.010	.172	.008	.87
267480 (rock)	.004	.002	.001	.21
267481	.031	.200	.012	1.58
267482	.024	.203	.010	1.31
RE 267482	.024	.206	.009	1.32
RRE 267482	.024	.202	.009	1.24
267483	.021	.257	.010	1.50
267484	.019	.216	.009	1.13
267485	.011	.202	.009	1.26
267486	.027	.262	.008	1.21
267487	.012	.180	.006	1.16
267488	.005	.162	.006	.90
267489	.018	.195	.007	.95
267490A	.005	.136	.005	.85
267490B	.006	.140	.005	.87
STANDARD R-2a	.531	.320	.042	7.50

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
- SAMPLE TYPE: DRILL CORE R150  
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data h FA \_\_\_\_\_

DATE RECEIVED: AUG 3 2005 DATE REPORT MAILED: Sept 5/05





SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267491	.012	.217	.006	1.09
267492	.022	.297	.008	1.19
267493	.009	.203	.007	.89
267494	.016	.246	.011	.99
267495	.028	.183	.013	1.19
267496	.022	.235	.013	1.28
267497	.020	.246	.012	1.38
267498	.016	.198	.009	1.18
267499	.015	.175	.007	.99
.STD RTS-2	.057	.224	.007	3.00
267500 (pulp)	.095	.259	.010	1.13
267501	.017	.203	.008	1.14
267502	.018	.220	.007	1.17
267503	.027	.305	.011	1.35
267504	.025	.216	.011	1.50
267505	.018	.283	.010	1.11
267506	.014	.232	.012	.83
267507	.017	.281	.014	1.23
267508	.015	.260	.013	1.26
RE 267508	.015	.260	.013	1.25
RRE 267508	.015	.265	.013	1.29
267509	.016	.260	.012	1.24
267510 (rock)	.003	.003	<.001	.17
267511	.016	.278	.014	1.07
STANDARD R-2a	.520	.332	.044	7.94

Sample type: DRILL CORE R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



ASSAY CERTIFICATE



Hard Creek Nickel Corporation PROJECT Tur C05-76C File # A504131 Page 1

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens

SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267512	.021	.259	.013	.83
267513	.018	.265	.015	.91
267514	.012	.317	.015	.81
267515	.017	.241	.015	.91
267516	.008	.144	.011	.81
267517	.013	.154	.012	.72
RE 267517	.013	.155	.012	.73
RRE 267517	.014	.156	.012	.73
267518	.010	.232	.013	.85
267519	.005	.353	.017	.89
267520A	.014	.277	.011	.84
267520B	.016	.280	.011	.86
267521	.009	.224	.010	.79
267522	.023	.214	.012	1.06
267523	.021	.199	.009	1.02
267524	.024	.206	.008	.89
267525 (pulp)	.098	.269	.013	1.20
267526	.022	.219	.013	.72
267527	.031	.235	.012	1.00
.STD RTS-2	.058	.223	.007	3.31
267528	.043	.256	.011	1.00
267529	.043	.341	.011	1.01
267530	.022	.233	.008	.84
267531	.007	.128	.005	.73
267532	.002	.063	.004	.75
267533	.006	.090	.004	.84
267534	.010	.145	.006	.92
267535	.011	.245	.006	1.01
267536	.010	.191	.006	.92
267537	.014	.206	.006	1.04
267538	.022	.226	.012	.76
267539	.075	.311	.025	2.03
267540 (rock)	.004	.001	<.001	.15
267541	.033	.207	.017	1.41
STANDARD R-2a	.529	.326	.043	7.83

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
- SAMPLE TYPE: DRILL CORE R150  
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data h FA \_\_\_\_\_

DATE RECEIVED: AUG 3 2005 DATE REPORT MAILED: Aug 29/05 .....





SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267542	.006	.182	.008	.52
267543	.009	.213	.010	.91
267544	.005	.189	.010	.44
267545	.016	.137	.010	.70
267546	.031	.227	.016	1.23
267547	.036	.212	.024	1.02
RE 267547	.035	.212	.024	.99
RRE 267547	.036	.211	.023	1.14
267548	.025	.180	.017	1.08
267549	.016	.116	.010	.45
.STD RTS-2	.057	.235	.008	4.24
267550 (pulp)	.058	.195	.008	.01
267551	.017	.183	.013	.75
267552	.006	.152	.009	.44
267553	.008	.161	.009	.57
267554	.007	.231	.011	.50
267555	.008	.259	.011	.61
STANDARD R-2a	.521	.329	.043	8.67

Sample type: DRILL CORE R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-76C File # A504131 Page 1

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267512	<.001	.023	<.02	<.01	3	.283	.016	.10	7.14	<.02	<.01	<.001	<.01	<.01	<.01	.26	<.01	.071	25.28	.01	.12	.01	.01	<.01	.59	12	50	41	5.13
267513	<.001	.021	<.02	<.01	<2	.278	.017	.10	8.36	<.02	<.01	<.001	<.01	<.01	<.01	.12	<.01	.089	25.12	.01	.13	.01	.01	<.01	.89	6	33	44	1.68
267514	<.001	.015	<.02	<.01	<2	.324	.016	.11	6.51	<.02	<.01	<.001	<.01	<.01	<.01	.43	<.01	.065	25.11	.01	.18	<.01	<.01	<.01	.58	12	20	23	3.21
267515	<.001	.019	<.02	<.01	<2	.244	.017	.10	7.03	<.02	<.01	<.001	<.01	<.01	<.01	.27	.01	.041	24.08	.04	.43	<.01	.01	<.01	.92	10	10	9	4.10
267516	<.001	.010	<.02	.01	<2	.156	.014	.15	8.13	<.02	<.01	<.001	<.01	<.01	<.01	.09	<.01	.039	27.09	<.01	.07	<.01	<.01	<.01	.64	4	7	11	5.49
267517	<.001	.015	<.02	<.01	<2	.149	.013	.13	8.19	<.02	<.01	<.001	<.01	<.01	<.01	.22	<.01	.040	25.89	<.01	.05	<.01	<.01	<.01	.95	14	10	8	5.95
RE 267517	<.001	.015	<.02	<.01	<2	.150	.013	.13	8.24	<.02	<.01	<.001	<.01	<.01	<.01	.22	<.01	.039	26.30	<.01	.05	<.01	<.01	<.01	.99	8	8	12	-
RRE 267517	<.001	.016	<.02	<.01	<2	.154	.013	.13	8.57	<.02	<.01	<.001	<.01	<.01	<.01	.23	<.01	.041	25.71	<.01	.05	<.01	<.01	<.01	.92	9	6	11	-
267518	<.001	.011	<.02	<.01	<2	.233	.014	.12	8.11	<.02	<.01	<.001	<.01	<.01	<.01	.90	<.01	.084	24.23	.04	.39	<.01	<.01	<.01	.71	17	15	18	5.28
267519	<.001	.007	<.02	.01	2	.337	.016	.14	6.36	<.02	<.01	<.001	<.01	<.01	<.01	.08	<.01	.062	24.77	.01	.07	<.01	<.01	<.01	.56	17	35	33	4.14
267520A	<.001	.015	<.02	.01	<2	.300	.013	.11	6.05	<.02	<.01	<.001	<.01	<.01	<.01	.20	<.01	.105	25.74	.01	.07	<.01	<.01	<.01	.48	14	7	13	5.18
267520B	<.001	.017	<.02	<.01	<2	.295	.013	.11	6.11	<.02	<.01	<.001	<.01	<.01	<.01	.24	<.01	.108	24.99	.01	.07	<.01	.01	<.01	.49	8	20	18	-
267521	<.001	.010	<.02	<.01	<2	.259	.013	.11	6.42	<.02	<.01	<.001	<.01	<.01	<.01	.86	<.01	.100	24.42	.03	.34	.01	.01	<.01	.44	6	22	14	4.34
267522	<.001	.025	<.02	.01	<2	.255	.014	.10	6.14	<.02	<.01	<.001	<.01	<.01	<.01	.21	<.01	.179	24.78	.01	.22	<.01	<.01	<.01	.61	6	22	15	4.02
267523	<.001	.022	<.02	<.01	<2	.266	.015	.10	6.50	<.02	<.01	<.001	<.01	<.01	<.01	.59	<.01	.289	25.75	.01	.10	<.01	<.01	<.01	.44	4	6	7	5.35
267524	<.001	.027	<.02	<.01	<2	.269	.015	.10	6.78	<.02	<.01	<.001	<.01	<.01	<.01	.71	<.01	.199	25.78	.01	.07	<.01	<.01	<.01	.37	6	<2	3	5.62
267525 (pulp)	<.001	.100	<.02	<.01	2	.346	.017	.05	9.30	<.02	<.01	<.001	<.01	<.01	.01	3.42	<.01	.346	14.71	.14	2.65	.23	.05	<.01	1.20	27	77	376	-
267526	<.001	.023	<.02	<.01	<2	.235	.016	.09	6.84	<.02	<.01	<.001	<.01	<.01	<.01	1.71	<.01	.072	23.26	.05	.68	.01	<.01	<.01	.58	2	10	6	4.44
267527	<.001	.034	<.02	<.01	<2	.287	.018	.11	7.28	<.02	<.01	<.001	<.01	<.01	<.01	.20	<.01	.127	26.17	.01	.04	<.01	<.01	<.01	.64	5	40	45	4.95
.STD RTS-2	<.001	.071	<.02	.01	3	.264	.007	.04	37.57	<.02	<.01	.001	<.01	.02	<.01	.60	.01	.012	.37	.16	.79	.21	.13	<.01	19.19	-	-	-	-
267528	<.001	.045	<.02	<.01	<2	.311	.017	.10	7.01	<.02	<.01	<.001	<.01	<.01	<.01	.44	<.01	.182	26.54	.01	.07	<.01	<.01	<.01	.46	<2	13	13	4.93
267529	<.001	.046	<.02	.01	<2	.380	.014	.10	6.82	<.02	<.01	<.001	<.01	<.01	<.01	.65	<.01	.089	26.03	.01	.27	<.01	<.01	<.01	.60	5	53	30	4.58
267530	<.001	.022	<.02	.01	<2	.298	.014	.10	6.48	<.02	<.01	<.001	<.01	<.01	<.01	.23	<.01	.083	26.69	<.01	.06	<.01	<.01	<.01	.32	5	50	49	5.25
267531	<.001	.008	<.02	.01	<2	.243	.013	.11	6.65	<.02	.02	<.001	<.01	<.01	<.01	1.02	.01	.105	26.46	.03	.39	.01	.04	<.01	.17	5	18	10	5.95
267532	<.001	.003	<.02	<.01	2	.183	.014	.11	6.92	<.02	<.01	<.001	<.01	<.01	<.01	.22	<.01	.514	27.39	.01	.07	<.01	<.01	<.01	.06	12	30	13	5.40
267533	<.001	.007	<.02	.01	<2	.214	.014	.11	6.74	<.02	<.01	<.001	<.01	<.01	<.01	.15	<.01	.180	27.48	<.01	.03	<.01	<.01	<.01	.10	11	32	17	5.68
267534	<.001	.011	<.02	.01	<2	.233	.014	.10	6.65	<.02	<.01	<.001	<.01	<.01	<.01	.42	<.01	.373	26.35	.01	.07	<.01	<.01	<.01	.24	2	18	21	5.72
267535	<.001	.012	<.02	.01	<2	.353	.015	.10	7.01	<.02	<.01	.001	<.01	<.01	<.01	.21	<.01	.175	27.34	.01	.05	.01	<.01	<.01	.33	4	85	85	5.74
267536	<.001	.010	<.02	<.01	<2	.306	.014	.11	6.99	<.02	<.01	<.001	<.01	<.01	<.01	.20	<.01	.144	27.82	.01	.03	<.01	<.01	<.01	.27	11	6	9	5.78
267537	<.001	.014	<.02	<.01	<2	.307	.014	.11	7.44	<.02	<.01	<.001	<.01	<.01	<.01	.13	<.01	.218	27.70	.01	.04	.01	<.01	<.01	.30	25	13	5	5.68
267538	<.001	.023	<.02	.01	<2	.250	.015	.09	8.01	<.02	<.01	<.001	<.01	<.01	<.01	.59	<.01	.135	23.69	.01	.37	<.01	<.01	<.01	1.29	15	15	10	5.39
267539	.001	.079	<.02	.01	<2	.307	.026	.12	13.70	<.02	<.01	.001	<.01	<.01	<.01	.55	<.01	.095	23.39	.01	.22	.01	.06	<.01	4.05	6	2	17	5.95
267540 (rock)	<.001	.005	<.02	<.01	<2	.003	.001	.09	4.42	<.02	.04	<.001	<.01	<.01	.01	4.57	.06	.001	1.88	.30	8.36	2.30	1.22	<.01	.02	3	8	4	3.04
267541	<.001	.035	<.02	.01	<2	.209	.021	.12	10.05	<.02	<.01	.001	<.01	<.01	<.01	.44	.01	.071	24.87	.04	.46	.04	.09	<.01	1.82	2	24	13	6.53
STANDARD R-2a	.049	.579	1.57	4.28	164	.381	.049	.24	24.93	.23	.14	.030	.13	<.01	.01	3.82	.08	.065	2.69	.18	2.70	.51	.64	.07	5.33	482	465	455	-

Standard is STANDARD R-2a/CSB/FA-10R.

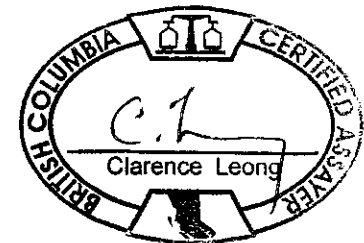
GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCl) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.

TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B BY FIRE ASSAY & ANALYSIS BY ICP. (30 gm)

- SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

DATE RECEIVED: AUG 3 2005 DATE REPORT MAILED: Aug 17/05





SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267542	<.001	.005	<.02	.01	<2	.206	.010	.10	6.24	<.02	<.01	<.001	<.01	<.01	.01	1.88	<.01	.088	20.93	.04	.29	.05	.03	<.01	.38	4	<2	7	3.53
267543	<.001	.009	<.02	.01	<2	.260	.014	.11	7.78	<.02	<.01	<.001	<.01	<.01	.01	.49	<.01	.152	24.96	.01	.12	.01	.01	<.01	.49	4	14	8	7.10
267544	<.001	.005	<.02	.02	<2	.195	.011	.08	5.72	<.02	<.01	<.001	<.01	<.01	.01	.13	<.01	.161	22.51	.03	.37	.01	.01	<.01	.30	6	45	24	2.69
267545	<.001	.015	<.02	.01	<2	.137	.010	.10	6.95	<.02	<.01	<.001	<.01	<.01	.01	.175	<.01	.108	20.13	.04	.35	.03	.02	<.01	1.43	2	31	17	3.55
267546	<.001	.034	<.02	.01	<2	.220	.016	.11	8.09	<.02	<.01	<.001	<.01	<.01	.01	.36	<.01	.243	22.48	.01	.07	<.01	<.01	<.01	1.32	9	29	22	2.35
267547	<.001	.038	<.02	.01	<2	.198	.022	.07	10.78	<.02	<.01	.001	<.01	<.01	.01	.81	<.01	.152	20.46	<.01	.10	.01	<.01	<.01	2.09	7	21	17	.69
RE 267547	<.001	.037	<.02	.01	<2	.199	.022	.07	10.74	<.02	<.01	.001	<.01	<.01	.01	.81	<.01	.161	20.66	<.01	.09	.01	<.01	<.01	2.16	2	17	17	-
RRE 267547	<.001	.039	<.02	.01	<2	.196	.022	.08	11.51	<.02	<.01	.001	<.01	<.01	.01	.97	<.01	.162	20.46	<.01	.09	<.01	<.01	<.01	2.09	2	12	16	-
267548	<.001	.029	<.02	.01	<2	.176	.017	.11	9.38	<.02	<.01	<.001	<.01	<.01	.01	1.65	<.01	.107	20.85	.03	.73	.01	.12	<.01	1.48	3	4	11	2.45
267549	<.001	.020	<.02	.01	<2	.124	.012	.11	7.04	<.02	.05	<.001	<.01	<.01	.01	2.09	.03	.149	17.13	.08	2.72	1.15	.39	<.01	.54	3	9	4	4.08
.STD RTS-2	<.001	.073	<.02	.01	<2	.276	.008	.04	37.06	<.02	<.01	.002	<.01	.02	<.01	.54	.01	.013	.36	.16	.82	.21	.13	<.01	18.42	-	-	-	-
267550 (pulp)	<.001	.058	<.02	.02	6	.246	.013	.12	9.42	<.02	<.01	<.001	<.01	<.01	.01	4.43	<.01	.949	14.03	.19	4.22	.35	.12	<.01	.52	10	107	283	-
267551	<.001	.018	<.02	.01	<2	.185	.014	.14	9.12	<.02	<.01	<.001	<.01	<.01	.01	1.83	.03	.164	20.40	.11	.85	.02	.09	<.01	.92	7	16	13	8.33
267552	<.001	.006	<.02	.01	<2	.151	.009	.13	7.12	<.02	<.01	<.001	<.01	<.01	.01	2.07	<.01	.217	20.19	.03	.19	.01	<.01	<.01	.58	6	2	4	4.12
267553	<.001	.009	<.02	.01	<2	.164	.009	.12	7.50	<.02	<.01	<.001	<.01	<.01	.01	.98	<.01	.193	21.61	.03	.18	.01	<.01	<.01	.82	7	3	10	4.84
267554	<.001	.008	<.02	.01	<2	.231	.011	.12	7.30	<.02	<.01	<.001	<.01	<.01	.01	1.50	<.01	.183	20.27	.03	.20	.01	<.01	<.01	.63	7	67	57	4.58
267555	<.001	.011	<.02	.01	<2	.277	.011	.14	8.29	<.02	<.01	<.001	<.01	<.01	.01	.25	<.01	.170	22.20	.02	.17	<.01	<.01	<.01	.60	4	23	19	4.08
STANDARD R-2a/CSB/FA-10R	.048	.579	1.55	4.27	166	.384	.049	.24	25.16	.24	.14	.030	.14	<.01	.01	3.53	.09	.061	2.66	.18	2.89	.52	.63	.07	5.30	477	473	486	-

Sample type: DRILL CORE R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE



Hard Creek Nickel Corporation PROJECT Tur C05-77A File # A504132

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchins

SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267556	<.001	.003	<.02	.01	<2	.229	.015	.10	6.65	<.02	<.01	<.001	<.01	<.01	<.01	.12	<.01	.215	26.09	.01	.07	.01	.01	<.01	.03	<2	<2	3	2.39
RE 267556	<.001	.002	<.02	.01	<2	.230	.015	.10	6.72	<.02	<.01	<.001	<.01	<.01	<.01	.12	<.01	.208	26.25	<.01	.06	.01	.01	<.01	.04	2	<2	2	-
RRE 267556	<.001	.001	<.02	<.01	<2	.229	.015	.10	6.69	<.02	<.01	<.001	<.01	<.01	<.01	.12	<.01	.223	25.92	.01	.09	.02	.01	<.01	.02	<2	<2	2	-
267557	<.001	.003	<.02	<.01	<2	.217	.017	.11	7.11	<.02	<.01	<.001	<.01	<.01	<.01	.26	<.01	.184	25.31	.02	.24	.07	.01	<.01	.04	<2	4	4	4.00
267558	<.001	.003	<.02	<.01	<2	.245	.017	.11	7.02	<.02	<.01	<.001	<.01	<.01	<.01	.12	<.01	.280	26.15	<.01	.05	<.01	<.01	<.01	.03	<2	6	10	5.72
267559	<.001	.004	<.02	.01	2	.253	.016	.11	7.07	<.02	<.01	<.001	<.01	<.01	<.01	.13	<.01	.159	26.30	<.01	.04	<.01	<.01	<.01	.02	4	4	6	5.51
267560	<.001	.011	<.02	<.01	<2	.237	.017	.11	7.12	<.02	<.01	<.001	<.01	<.01	<.01	.13	<.01	.241	26.45	<.01	.04	<.01	<.01	<.01	.05	4	<2	10	6.12
267561	<.001	.067	<.02	<.01	<2	.268	.017	.10	7.28	<.02	<.01	<.001	<.01	<.01	<.01	.13	<.01	.287	25.71	.01	.07	<.01	<.01	<.01	.20	4	18	28	4.79
.STD RTS-2	.001	.073	<.02	.01	4	.269	.007	.04	38.66	<.02	<.01	<.001	<.01	.01	.01	.59	.01	.012	.36	.16	.84	.22	.13	<.01	18.84	-	-	-	-
267562	<.001	.016	<.02	<.01	<2	.213	.017	.11	7.59	<.02	<.01	<.001	<.01	<.01	<.01	.11	<.01	.087	25.22	<.01	.03	<.01	<.01	<.01	.10	<2	3	6	5.30
267563	<.001	.058	<.02	<.01	<2	.234	.016	.10	7.47	<.02	<.01	<.001	<.01	<.01	<.01	.09	<.01	.227	24.70	<.01	.04	<.01	<.01	<.01	.25	2	<2	3	4.94
267564	<.001	.043	<.02	<.01	2	.303	.017	.11	7.68	<.02	<.01	<.001	<.01	<.01	<.01	.14	<.01	.171	24.83	<.01	.04	<.01	<.01	<.01	.38	2	18	24	5.51
267565	<.001	.034	<.02	.01	<2	.259	.019	.09	7.02	<.02	<.01	<.001	<.01	<.01	<.01	.14	<.01	.166	24.91	<.01	.05	<.01	<.01	<.01	.42	<2	18	24	4.91
267566	<.001	.014	<.02	<.01	3	.124	.018	.12	8.25	<.02	.02	<.001	<.01	<.01	<.01	.96	.02	.124	24.86	.05	.79	.01	.22	<.01	.35	3	14	9	5.30
267567	<.001	.016	<.02	<.01	<2	.148	.015	.11	7.66	<.02	.02	<.001	<.01	<.01	<.01	1.01	.02	.139	23.26	.04	1.45	.46	.23	<.01	.34	6	<2	8	5.26
267568	<.001	.009	<.02	<.01	<2	.122	.016	.11	8.05	<.02	<.01	<.001	<.01	<.01	<.01	.29	<.01	.112	25.89	<.01	.05	<.01	<.01	<.01	.32	3	5	5	4.98
267569	<.001	.011	<.02	<.01	2	.136	.016	.11	8.41	<.02	<.01	<.001	<.01	<.01	<.01	.10	<.01	.088	26.00	<.01	.03	<.01	<.01	<.01	.41	<2	<2	2	5.86
267570 (rock)	.001	.005	<.02	<.01	<2	.002	.001	.10	4.43	<.02	.05	<.001	<.01	<.01	.01	4.39	.06	.002	1.88	.29	8.76	2.40	1.22	<.01	<.02	<2	<2	<2	3.09
STANDARD R-2a	.048	.572	1.55	4.28	167	.378	.048	.24	25.12	.23	.15	.030	.14	<.01	.01	3.64	.08	.059	2.59	.18	2.83	.51	.64	.09	5.30	491	481	475	-

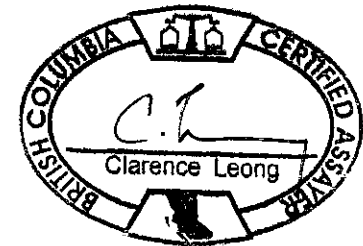
Standard is STANDARD R-2a/CSB/FA-10R.

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCl) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.  
TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B - 30 GM SAMPLE BY FIRE ASSAY & ANALYSIS BY ICP-ES.  
- SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data 1 FA \_\_\_\_\_

DATE RECEIVED: AUG 3 2005

DATE REPORT MAILED: Aug 17/05



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Hard Creek Nickel Corporation PROJECT Tur C05-77A File # A504132

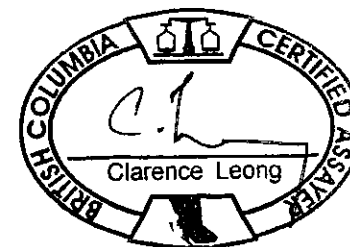
1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens

SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267556	.001	.045	.004	1.13
RE 267556	.001	.046	.004	1.17
RRE 267556	<.001	.045	.004	1.14
267557	.002	.052	.005	1.18
267558	.002	.054	.005	1.25
267559	.002	.052	.004	1.25
267560	.010	.063	.005	1.05
267561	.064	.128	.007	1.39
.STD RTS-2	.058	.230	.006	3.44
267562	.016	.101	.008	1.37
267563	.055	.173	.012	1.36
267564	.042	.229	.012	1.40
267565	.033	.205	.012	1.50
267566	.013	.083	.009	1.26
267567	.014	.077	.007	.97
267568	.008	.076	.008	.96
267569	.010	.093	.008	1.14
267570 (rock)	.002	<.001	<.001	.14
STANDARD R-2a	.527	.333	.043	7.40

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
- SAMPLE TYPE: DRILL CORE R150  
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data h FA \_\_\_\_\_

DATE RECEIVED: AUG 3 2005 DATE REPORT MAILED: Sept 3/05



ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-77B File # A504133 Page 1

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens



SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267571	.018	.123	.008	1.04
267572	.013	.071	.008	1.05
267573	.013	.055	.008	.96
267574	.012	.051	.008	.99
267575 (pulp)	.056	.182	.008	.51
267576	.019	.126	.010	.93
267577	.034	.120	.010	.92
267578	.011	.160	.008	1.08
267579	.008	.089	.007	1.03
267580A	.011	.064	.006	.83
267580B	.012	.067	.006	.91
267581	.009	.050	.004	.85
267582	.008	.054	.006	1.08
267583	.009	.058	.006	1.03
RE 267583	.008	.059	.006	1.04
RRE 267583	.009	.060	.006	1.00
267584	.008	.071	.005	.88
267585	.010	.069	.005	1.08
267586	.008	.082	.005	1.05
.STD RTS-2	.061	.225	.007	4.42
267587	.011	.104	.006	1.17
267588	.010	.092	.006	.81
267589	.017	.109	.006	.99
267590	.010	.086	.004	.80
267591	.010	.082	.005	.82
267592	.004	.079	.005	.88
267593	.008	.079	.004	.89
267594	.014	.091	.005	.98
267595	.017	.085	.005	1.07
267596	.011	.092	.007	1.04
267597	.009	.074	.011	.86
267598	.009	.084	.010	.44
267599	.006	.060	.009	.44
267600 (pulp)	.097	.244	.012	1.09
STANDARD R-2a	.521	.322	.042	8.08

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
- SAMPLE TYPE: DRILL CORE R150  
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data h FA \_\_\_\_\_

DATE RECEIVED: AUG 3 2005

DATE REPORT MAILED: Aug 29/05 .....





SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267601	.019	.111	.012	.58
267602	.014	.089	.009	.67
267603	.015	.085	.009	.58
267604	.019	.087	.010	.63
267605	.021	.110	.013	.89
267606	.014	.085	.008	.95
267607	.008	.078	.007	.85
267608	.009	.120	.007	.85
267609	.009	.123	.007	.83
267610A	.007	.102	.006	.81
267610B	.006	.104	.006	.84
267611	.008	.113	.006	.83
267612	.010	.106	.008	.90
267613	.016	.133	.010	1.01
267614	.019	.118	.009	1.04
267615	.012	.134	.008	1.03
267616	.014	.106	.011	1.00
267617	.013	.154	.010	1.03
.STD RTS-2	.061	.221	.007	3.32
267618	.014	.184	.010	1.25
267619	.011	.104	.010	1.00
267620	.012	.097	.009	1.07
267621	.018	.088	.008	.97
267622	.008	.093	.009	.73
267623	.008	.078	.009	.73
267624	.011	.090	.010	.75
267625 (pulp)	.058	.192	.008	.51
267626	.011	.133	.012	.78
267627	.006	.156	.012	.86
RE 267627	.006	.159	.013	.84
RRE 267627	.007	.154	.013	.86
267628	.008	.145	.010	1.05
267629	.009	.102	.008	1.03
267630 (rock)	.022	.002<	.001	.26
STANDARD R-2a	.540	.322	.042	7.50

Sample type: DRILL CORE R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.





SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267631	.011	.133	.009	1.19
267632	.009	.140	.010	1.29
267633	.015	.143	.010	1.21
STANDARD R-2a	.521	.329	.043	8.67

Sample type: DRILL CORE R150.

ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-77B File # A504133 Page 1

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens

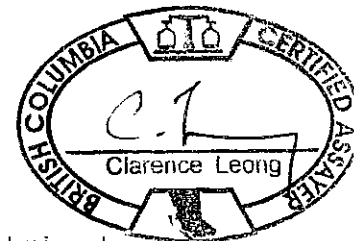
SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267571	<.001	.015	<.02	<.01	<2	.197	.016	.11	7.79	<.02	<.01	<.001	<.01	<.01	<.01	.13	<.01	.115	25.65	.01	.07	.01	.01	<.01	.51	4	19	8	5.22
267572	<.001	.009	<.02	<.01	<2	.120	.016	.11	7.75	<.02	<.01	<.001	<.01	<.01	<.01	.12	<.01	.105	26.27	.01	.05	.01	<.01	<.01	.37	<2	7	<2	5.83
267573	<.001	.012	<.02	.01	<2	.097	.016	.10	7.54	<.02	<.01	<.001	<.01	<.01	<.01	.15	<.01	.125	25.55	<.01	.05	.01	.01	<.01	.31	5	6	5	5.84
267574	<.001	.011	<.02	<.01	<2	.078	.015	.10	7.88	<.02	<.01	<.001	<.01	<.01	<.01	.14	<.01	.172	25.37	.01	.05	<.01	<.01	<.01	.28	4	3	2	5.83
267575 (pulp)	<.001	.058	<.02	.02	<2	.235	.012	.11	8.98	<.02	<.01	<.001	<.01	<.01	.02	4.54	<.01	.992	12.96	.18	4.01	.33	.11	<.01	.52	7	119	296	-
267576	<.001	.020	<.02	.01	<2	.173	.017	.10	7.42	<.02	<.01	<.001	<.01	<.01	<.01	.16	<.01	.183	26.08	.01	.05	<.01	<.01	<.01	.45	4	15	4	5.77
267577	<.001	.035	<.02	.01	<2	.166	.016	.10	6.94	<.02	<.01	<.001	<.01	<.01	<.01	.08	<.01	.205	25.88	<.01	.05	<.01	<.01	<.01	.37	<2	2	<2	5.34
267578	<.001	.012	<.02	<.01	<2	.255	.014	.09	6.25	<.02	<.01	<.001	<.01	<.01	<.01	.11	<.01	.153	25.68	<.01	.04	<.01	<.01	<.01	.47	4	31	14	5.98
267579	<.001	.008	<.02	<.01	<2	.155	.014	.11	7.72	<.02	<.01	<.001	<.01	<.01	<.01	.12	<.01	.190	26.31	<.01	.04	<.01	<.01	<.01	.35	<2	13	12	5.58
267580A	<.001	.012	<.02	<.01	<2	.120	.012	.12	7.58	<.02	<.01	<.001	<.01	<.01	<.01	.55	<.01	.174	25.15	.04	.39	.03	.03	<.01	.28	<2	8	<2	5.56
267580B	<.001	.013	<.02	.01	<2	.121	.012	.12	7.63	<.02	<.01	<.001	<.01	<.01	<.01	.56	<.01	.168	25.05	.04	.37	.03	.03	<.01	.29	<2	6	4	-
267581	<.001	.010	<.02	.01	<2	.099	.011	.13	8.46	<.02	.02	<.001	<.01	<.01	.01	1.95	.02	.135	22.53	.16	1.48	.23	.40	<.01	.24	4	12	4	5.97
267582	<.001	.009	<.02	.01	<2	.103	.014	.11	7.96	<.02	<.01	<.001	<.01	<.01	<.01	.17	<.01	.148	26.08	<.01	.05	<.01	.01	<.01	.29	2	2	2	5.70
267583	<.001	.009	<.02	.01	<2	.138	.014	.11	7.92	<.02	<.01	<.001	<.01	<.01	<.01	.13	<.01	.201	26.83	<.01	.05	<.01	<.01	<.01	.31	<2	8	2	6.06
RE 267583	<.001	.009	<.02	.01	<2	.140	.015	.11	7.92	<.02	<.01	<.001	<.01	<.01	<.01	.13	<.01	.203	26.38	<.01	.05	<.01	<.01	<.01	.31	<2	6	<2	-
RRE 267583	<.001	.009	<.02	<.01	<2	.140	.014	.11	7.99	<.02	<.01	<.001	<.01	<.01	<.01	.14	<.01	.196	26.61	<.01	.05	<.01	<.01	<.01	.31	4	3	2	-
267584	<.001	.009	<.02	<.01	<2	.148	.013	.12	8.03	<.02	<.01	<.001	<.01	<.01	<.01	.10	<.01	.148	26.60	<.01	.03	<.01	<.01	<.01	.36	3	13	8	5.74
267585	<.001	.010	<.02	.01	<2	.180	.014	.12	8.02	<.02	<.01	<.001	<.01	<.01	<.01	.15	<.01	.289	26.63	.01	.05	.01	<.01	<.01	.25	3	18	22	6.22
267586	<.001	.009	<.02	<.01	<2	.185	.014	.12	8.03	<.02	<.01	<.001	<.01	<.01	<.01	.14	<.01	.284	26.82	.01	.06	<.01	<.01	<.01	.28	<2	9	2	4.98
.STD RTS-2	<.001	.073	<.02	.01	<2	.275	.007	.04	37.98	<.02	<.01	.001	<.01	.02	<.01	.61	.01	.012	.36	.16	.83	.21	.13	<.01	19.40	-	-	-	-
267587	<.001	.011	<.02	.01	<2	.207	.015	.12	7.99	<.02	<.01	<.001	<.01	<.01	<.01	.25	<.01	.191	26.35	.01	.13	<.01	.02	<.01	.24	19	26	24	6.40
267588	<.001	.011	<.02	.01	<2	.190	.015	.13	8.08	<.02	<.01	<.001	<.01	<.01	<.01	.80	.01	.146	24.74	.05	.75	.01	.23	<.01	.23	<2	16	15	2.34
267589	<.001	.017	<.02	.01	<2	.227	.015	.11	7.71	<.02	<.01	<.001	<.01	<.01	<.01	.09	<.01	.172	26.07	<.01	.06	.01	<.01	<.01	.28	5	21	10	3.72
267590	<.001	.011	<.02	<.01	<2	.264	.015	.10	6.72	<.02	<.01	<.001	<.01	<.01	<.01	.13	<.01	.185	26.96	.01	.05	<.01	<.01	<.01	.16	2	9	<2	4.80
267591	<.001	.010	<.02	<.01	<2	.214	.015	.11	7.50	<.02	<.01	<.001	<.01	<.01	<.01	.61	.01	.219	25.19	.06	.67	.04	.24	<.01	.18	2	7	5	5.62
267592	<.001	.005	<.02	<.01	<2	.244	.015	.12	7.77	<.02	<.01	<.001	<.01	<.01	<.01	.12	<.01	.202	26.26	.01	.05	<.01	<.01	<.01	.16	2	6	10	5.98
267593	<.001	.009	<.02	<.01	<2	.247	.015	.12	7.69	<.02	<.01	<.001	<.01	<.01	<.01	.12	<.01	.178	27.07	<.01	.04	<.01	<.01	<.01	.17	5	6	4	6.09
267594	<.001	.015	<.02	.01	2	.184	.014	.12	8.34	<.02	<.01	<.001	<.01	<.01	<.01	.19	<.01	.170	26.70	<.01	.04	<.01	<.01	<.01	.33	<2	19	18	6.17
267595	<.001	.017	<.02	.01	<2	.170	.013	.13	8.50	<.02	<.01	<.001	<.01	<.01	<.01	.33	<.01	.175	26.69	.02	.19	<.01	.01	<.01	.34	3	25	25	5.57
267596	<.001	.012	<.02	.01	<2	.167	.015	.13	8.52	<.02	<.01	<.001	<.01	<.01	<.01	.17	<.01	.126	26.78	.01	.04	<.01	<.01	<.01	.40	3	19	23	6.28
267597	<.001	.010	<.02	<.01	<2	.099	.015	.13	8.34	<.02	<.01	<.001	<.01	<.01	<.01	.55	<.01	.067	24.85	<.01	.03	<.01	<.01	<.01	.38	8	5	7	3.41
267598	<.001	.011	<.02	<.01	<2	.096	.012	.11	7.59	<.02	<.01	<.001	<.01	<.01	.01	3.19	.02	.070	21.12	.09	1.05	.01	<.01	<.01	.28	<2	17	11	3.98
267599	<.001	.007	<.02	.01	<2	.066	.010	.10	7.83	<.02	<.01	<.001	<.01	<.01	<.01	.66	<.01	.040	23.29	.01	.27	<.01	<.01	<.01	.24	4	10	6	3.52
267600 (pulp)	<.001	.100	<.02	<.01	2	.355	.017	.05	9.38	<.02	<.01	<.001	<.01	<.01	.01	3.44	<.01	.371	14.54	.14	2.85	.23	.05	<.01	1.10	22	85	400	-
STANDARD R-2a/CSB/FA-10R	.048	.572	1.54	4.28	160	.379	.048	.23	25.06	.22	.14	.029	.13	<.01	.01	3.71	.08	.058	2.70	.18	2.76	.50	.62	.08	5.32	480	469	490	-

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCL) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.  
 TOTAL S BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B - 30 GM SAMPLE BY FIRE ASSAY & ANALYSIS BY ICP-ES.  
 - SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data h FA

DATE RECEIVED: AUG 3 2005

DATE REPORT MAILED: Aug 17/05





SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267601	<.001	.018	<.02	<.01	<2	.107	.012	.13	6.77	<.02	<.01	<.001	<.01	<.01	<.01	1.14	<.01	.114	23.65	.01	.11	.01	<.01	<.01	.46	2	7	7	5.27
267602	<.001	.013	<.02	<.01	<2	.092	.009	.07	7.33	<.02	<.01	<.001	<.01	<.01	<.01	.57	<.01	.085	23.27	.01	.13	.01	<.01	<.01	.47	4	4	8	5.29
267603	<.001	.014	<.02	<.01	<2	.090	.010	.13	7.87	<.02	<.01	<.001	<.01	<.01	<.01	.94	<.01	.095	24.40	<.01	.05	.01	<.01	<.01	.57	6	4	6	5.30
267604	<.001	.019	<.02	<.01	<2	.094	.011	.12	8.30	<.02	<.01	<.001	<.01	<.01	<.01	1.06	<.01	.079	24.64	.01	.05	<.01	<.01	<.01	.87	<2	11	10	5.18
267605	<.001	.021	<.02	<.01	<2	.114	.014	.11	8.65	<.02	<.01	<.001	<.01	<.01	<.01	.43	<.01	.085	23.65	.01	.04	<.01	<.01	<.01	1.21	3	3	5	5.26
267606	<.001	.014	<.02	.01	<2	.114	.012	.13	8.27	<.02	<.01	<.001	<.01	<.01	<.01	.24	<.01	.067	25.79	<.01	.05	<.01	<.01	<.01	.65	<2	5	14	5.36
267607	<.001	.008	<.02	<.01	<2	.119	.012	.12	8.00	<.02	<.01	<.001	<.01	<.01	<.01	.22	<.01	.160	25.57	.02	.23	<.01	<.01	<.01	.50	4	13	13	6.04
267608	<.001	.009	<.02	.01	<2	.204	.014	.13	8.19	<.02	<.01	<.001	<.01	<.01	<.01	.26	<.01	.196	26.04	.01	.06	<.01	<.01	<.01	.51	<2	16	20	5.99
267609	<.001	.009	<.02	.01	<2	.176	.011	.14	8.27	<.02	<.01	<.001	<.01	<.01	<.01	.19	<.01	.234	25.77	<.01	.02	<.01	<.01	<.01	.54	2	2	8	5.67
267610A	<.001	.006	<.02	.01	<2	.168	.011	.14	8.29	<.02	<.01	<.001	<.01	<.01	<.01	.22	<.01	.177	25.47	<.01	.03	<.01	<.01	<.01	.40	5	12	11	5.56
267610B	<.001	.006	<.02	.01	<2	.169	.012	.14	8.33	<.02	<.01	<.001	<.01	<.01	<.01	.23	<.01	.173	25.50	<.01	.02	<.01	<.01	<.01	.40	6	5	6	-
267611	<.001	.008	<.02	<.01	<2	.170	.011	.12	8.00	<.02	<.01	<.001	<.01	<.01	<.01	.36	<.01	.183	25.30	.02	.17	<.01	<.01	<.01	.51	7	6	9	5.43
267612	<.001	.011	<.02	<.01	<2	.139	.012	.11	8.20	<.02	<.01	<.001	<.01	<.01	<.01	.27	<.01	.174	25.33	.01	.24	<.01	<.01	<.01	.68	4	10	18	5.28
267613	<.001	.018	<.02	<.01	<2	.156	.013	.11	8.37	<.02	<.01	<.001	<.01	<.01	<.01	.16	<.01	.077	25.30	<.01	.05	<.01	<.01	<.01	.93	6	10	14	5.58
267614	<.001	.021	<.02	.01	<2	.141	.013	.11	8.43	<.02	<.01	<.001	<.01	<.01	<.01	.98	.02	.131	24.04	.08	.80	.02	.09	<.01	.87	<2	5	15	5.57
267615	<.001	.013	<.02	<.01	<2	.170	.013	.12	8.19	<.02	<.01	<.001	<.01	<.01	<.01	.11	<.01	.053	25.91	<.01	.02	<.01	<.01	<.01	.84	6	5	12	5.89
267616	<.001	.014	<.02	<.01	<2	.118	.015	.11	8.09	<.02	<.01	<.001	<.01	<.01	<.01	.18	<.01	.169	25.65	<.01	.03	<.01	<.01	<.01	.78	<2	4	5	6.07
267617	<.001	.013	<.02	<.01	<2	.203	.016	.10	6.67	<.02	<.01	<.001	<.01	<.01	<.01	.09	<.01	.154	25.61	<.01	.03	<.01	<.01	<.01	.60	4	31	35	5.88
.STD RTS-2	<.001	.071	<.02	.01	3	.265	.007	.04	38.00	<.02	<.01	<.001	<.01	.02	<.01	.61	.01	.011	.36	.16	.83	.21	.12	<.01	18.75	-	-	-	-
267618	<.001	.014	<.02	<.01	<2	.231	.015	.10	6.31	<.02	<.01	<.001	<.01	<.01	<.01	.14	<.01	.194	25.91	<.01	.03	<.01	<.01	<.01	.67	2	24	28	5.62
267619	<.001	.012	<.02	.02	<2	.132	.014	.11	7.52	<.02	<.01	<.001	<.01	<.01	<.01	.16	<.01	.217	26.07	.01	.06	<.01	<.01	<.01	.63	5	8	17	5.37
267620	<.001	.012	<.02	.01	<2	.132	.014	.12	8.46	<.02	<.01	<.001	<.01	<.01	<.01	.09	<.01	.232	26.13	<.01	.04	<.01	<.01	<.01	.80	3	8	5	5.48
267621	<.001	.018	<.02	.01	<2	.108	.012	.13	8.69	<.02	<.01	<.001	<.01	<.01	<.01	.09	<.01	.215	25.22	.01	.08	<.01	<.01	<.01	.71	2	7	7	5.72
267622	<.001	.009	<.02	.01	<2	.100	.010	.11	8.20	<.02	<.01	<.001	<.01	<.01	<.01	.08	<.01	.195	24.23	.01	.07	<.01	<.01	<.01	.58	3	5	2	5.18
267623	<.001	.009	<.02	.01	<2	.085	.012	.12	8.17	<.02	<.01	<.001	<.01	<.01	<.01	.25	<.01	.289	24.58	.01	.09	<.01	<.01	<.01	.49	75	<2	<2	5.21
267624	<.001	.012	<.02	.01	<2	.096	.011	.15	7.94	<.02	<.01	<.001	<.01	<.01	<.01	.15	<.01	.203	24.62	<.01	.05	<.01	<.01	<.01	.55	6	<2	3	4.99
267625 (pulp)	<.001	.058	<.02	.02	<2	.237	.012	.11	8.89	<.02	<.01	<.001	<.01	<.01	.02	4.62	<.01	.894	13.25	.18	3.94	.33	.11	<.01	.56	10	78	259	-
267626	<.001	.011	<.02	.01	<2	.137	.014	.12	8.25	<.02	<.01	<.001	<.01	<.01	<.01	.29	<.01	.145	24.59	<.01	.04	<.01	<.01	<.01	.76	2	6	7	5.30
267627	<.001	.007	<.02	.01	<2	.160	.013	.12	8.05	<.02	<.01	<.001	<.01	<.01	<.01	.07	<.01	.237	24.66	.01	.10	<.01	<.01	<.01	.69	2	9	11	5.23
RE 267627	<.001	.007	<.02	.01	<2	.154	.013	.12	7.80	<.02	<.01	<.001	<.01	<.01	<.01	.07	<.01	.229	23.72	.01	.09	<.01	<.01	<.01	.68	4	12	8	-
RRE 267627	<.001	.007	<.02	.01	<2	.156	.013	.12	8.01	<.02	<.01	<.001	<.01	<.01	<.01	.07	<.01	.231	24.10	.01	.10	<.01	<.01	<.01	.69	3	5	13	-
267628	<.001	.008	<.02	.01	<2	.181	.013	.11	7.47	<.02	<.01	<.001	<.01	<.01	<.01	.31	<.01	.238	24.05	.01	.10	<.01	<.01	<.01	.67	5	9	7	5.18
267629	<.001	.009	<.02	.01	<2	.147	.014	.12	8.49	<.02	<.01	<.001	<.01	<.01	<.01	.66	<.01	.108	24.26	.02	.25	.01	.04	<.01	.63	5	9	8	6.17
267630 (rock)	<.001	.024	<.02	.01	<2	.003	.001	.10	4.38	<.02	.04	<.001	<.01	<.01	.01	4.52	.06	.003	1.96	.29	8.58	2.27	1.21	<.01	.02	<2	<2	<2	2.34
STANDARD R-2a/CSB/FA-10R	.048	.582	1.55	4.38	167	.381	.047	.24	24.79	.22	.13	.030	.13	<.01	.01	3.80	.08	.059	2.60	.18	2.85	.51	.64	.08	5.33	489	477	478	-

Sample type: DRILL CORE R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267631	<.001	.013	<.02	.01	<2	.172	.014	.13	8.72	<.02	<.01	<.001	<.01	<.01	<.01	.09	<.01	.197	25.41	.01	.06	.01	<.01	<.01	.71	8	10	11	2.66
267632	<.001	.011	<.02	.01	<2	.169	.015	.12	8.61	<.02	<.01	.001	<.01	<.01	<.01	.22	<.01	.144	25.41	.01	.04	<.01	<.01	<.01	.82	3	15	9	5.75
267633	<.001	.017	<.02	.01	<2	.180	.016	.12	8.85	<.02	<.01	<.001	<.01	<.01	<.01	.43	<.01	.173	26.05	<.01	.05	.01	.01	<.01	.97	9	8	10	5.20
STANDARD	.048	.579	1.55	4.27	166	.384	.049	.24	25.16	.24	.14	.030	.14	<.01	.01	3.53	.09	.061	2.66	.18	2.89	.52	.63	.07	5.32	506	499	466	-

Standard is STANDARD R-2a/CSB/FA-10R.

ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-77C File # A504248 Page 1

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267634	.001	.025	<.02	<.01	<2	.280	.023	.13	11.95	<.01	<.01	<.001	<.01	<.01	<.01	.24	<.01	.094	28.97	.01	.04	<.01	.01	<.01	3.07	4	20	25	5.87
267635	<.001	.011	<.02	<.01	<2	.200	.011	.10	7.34	<.01	<.01	<.001	<.01	<.01	.01	.97	.01	.130	26.29	.01	.52	<.01	.03	<.01	.75	<2	<2	4	3.96
267636	<.001	.018	<.02	<.01	<2	.225	.017	.11	8.12	<.01	<.01	<.001	<.01	<.01	<.01	.75	.01	.137	27.30	.01	.72	.21	.05	<.01	1.05	<2	10	15	4.54
267637	<.001	.008	<.02	<.01	<2	.158	.011	.08	6.00	<.01	.02	<.001	<.01	<.01	<.01	1.32	.01	.275	24.26	.03	1.25	.15	.54	<.01	.29	3	7	10	4.33
267638	<.001	.002	<.02	<.01	<2	.011	.002	.16	4.44	<.01	.26	<.001	<.01	<.01	.01	7.54	.13	.006	3.80	.26	10.23	2.41	1.66	<.01	.03	21	<2	3	4.67
267639	<.001	.016	<.02	<.01	<2	.264	.015	.10	7.04	<.01	<.01	<.001	<.01	<.01	<.01	.21	<.01	.321	29.28	.01	.16	.09	.05	<.01	.59	9	20	21	4.44
267640A	<.001	.012	<.02	<.01	<2	.239	.015	.10	7.73	<.01	<.01	<.001	<.01	<.01	<.01	.95	<.01	.163	29.23	.01	.06	.15	<.01	<.01	.58	2	19	18	4.94
267640B	<.001	.012	<.02	<.01	<2	.233	.014	.10	7.94	<.01	<.01	<.001	<.01	<.01	<.01	.98	.01	.167	29.47	.01	.05	.10	.10	<.01	.60	<2	17	15	-
267641	<.001	.012	<.02	<.01	<2	.144	.016	.13	8.85	<.01	<.01	<.001	<.01	<.01	<.01	.28	.01	.237	30.63	<.01	.04	.16	.02	<.01	.56	<2	5	7	6.24
267642	<.001	.011	<.02	<.01	<2	.217	.014	.13	8.43	<.01	<.01	<.001	<.01	<.01	<.01	.33	.01	.168	31.38	<.01	.01	.10	<.01	<.01	.61	4	9	9	5.67
267643	<.001	.011	<.02	<.01	<2	.206	.012	.14	8.87	<.01	<.01	<.001	<.01	<.01	<.01	.23	<.01	.123	31.36	<.01	.02	<.01	.02	<.01	.82	2	5	5	5.62
267644	<.001	.014	<.02	<.01	<2	.192	.015	.14	8.81	<.01	<.01	<.001	<.01	<.01	<.01	.21	.01	.209	31.54	<.01	.03	.05	.03	<.01	.70	4	7	6	5.89
267645	<.001	.016	<.02	<.01	<2	.188	.013	.14	8.35	<.01	<.01	<.001	<.01	<.01	<.01	.28	<.01	.188	31.77	<.01	.02	<.01	<.01	<.01	.64	4	9	13	5.87
267646	<.001	.020	<.02	<.01	<2	.166	.020	.13	10.39	<.01	<.01	<.001	<.01	<.01	<.01	.42	.01	.206	29.47	<.01	.01	.12	.07	<.01	2.06	2	8	12	5.81
267647	<.001	.025	<.02	<.01	<2	.200	.023	.12	10.75	<.01	<.01	<.001	<.01	<.01	<.01	.27	<.01	.109	28.71	<.01	.02	.17	.07	<.01	2.50	2	6	8	5.77
RE 267647	<.001	.025	<.02	<.01	<2	.204	.024	.12	10.79	<.01	<.01	<.001	<.01	<.01	<.01	.27	<.01	.109	28.67	<.01	.02	.12	.03	<.01	2.57	<2	9	10	-
RRE 267647	<.001	.025	<.02	<.01	<2	.212	.025	.12	10.95	<.01	<.01	<.001	<.01	<.01	<.01	.30	.01	.112	29.26	<.01	.03	<.01	.10	<.01	2.60	3	7	9	-
267648	<.001	.050	<.02	<.01	<2	.286	.027	.12	12.89	<.01	<.01	<.001	<.01	<.01	<.01	.09	.01	.273	26.94	.01	.03	.12	.03	<.01	3.19	5	14	21	5.36
.STD RTS-2	<.001	.073	<.02	.01	<2	.279	.007	.04	38.65	<.01	<.01	<.001	<.01	<.01	.01	.61	.01	.012	.40	.17	.85	.36	.18	<.01	18.72	-	-	-	-
267649	<.001	.024	<.02	<.01	<2	.272	.025	.13	11.46	<.01	<.01	<.001	<.01	<.01	<.01	.22	.01	.049	29.50	<.01	.03	.19	.02	<.01	2.43	4	15	15	2.97
267650 (pulp)	<.001	.057	<.02	.01	<2	.250	.011	.12	8.95	<.01	<.01	<.001	<.01	<.01	.02	4.78	<.01	.683	15.37	.19	3.93	.63	.16	<.01	2.30	11	64	299	-
267651	<.001	.011	<.02	<.01	<2	.227	.018	.13	8.93	<.01	<.01	<.001	<.01	<.01	<.01	.27	.01	.074	30.24	<.01	.02	.07	.09	<.01	1.00	<2	29	27	4.95
267652	<.001	.008	<.02	<.01	<2	.253	.017	.13	8.23	<.01	<.01	<.001	<.01	<.01	<.01	.10	<.01	.153	31.79	<.01	.02	.07	.04	<.01	.78	<2	4	9	5.98
267653	<.001	.009	<.02	<.01	<2	.192	.014	.12	7.64	<.01	<.01	<.001	<.01	<.01	<.01	.64	.01	.182	28.51	.02	.51	.26	.14	<.01	.76	<2	7	7	4.84
267654	<.001	.032	<.02	<.01	<2	.227	.024	.14	10.37	<.01	<.01	<.001	<.01	<.01	<.01	.40	.01	.223	28.21	.01	.35	.14	.05	<.01	1.82	2	5	5	5.14
267655	<.001	.022	<.02	<.01	<2	.236	.022	.14	9.12	<.01	<.01	<.001	<.01	<.01	<.01	.19	.01	.109	30.19	<.01	.02	.20	.02	<.01	1.27	6	5	13	5.85
267656	<.001	.013	<.02	<.01	<2	.277	.015	.14	7.89	<.01	<.01	<.001	<.01	<.01	<.01	.14	.01	.123	30.87	<.01	<.01	.26	.03	<.01	.60	7	25	30	5.95
267657	<.001	.019	<.02	<.01	<2	.270	.013	.13	7.80	<.01	<.01	<.001	<.01	<.01	<.01	.18	.01	.152	28.99	<.01	.11	.09	<.01	<.01	.54	11	36	39	5.54
267658	<.001	.014	<.02	<.01	<2	.220	.012	.10	8.49	<.01	<.01	<.001	<.01	<.01	<.01	.07	.01	.162	28.10	.01	.19	.09	.07	<.01	.61	6	14	18	2.72
267659	<.001	.014	<.02	<.01	<2	.248	.014	.13	8.26	<.01	<.01	<.001	<.01	<.01	<.01	.05	.01	.195	27.94	.01	.15	.10	.05	<.01	.73	5	12	21	3.47
267660 (rock)	<.001	.004	<.02	<.01	<2	.003	.001	.12	4.40	<.01	.05	<.001	<.01	<.01	.01	4.64	.05	.003	2.00	.33	9.44	2.69	1.36	<.01	<.02	<2	<2	2	2.63
267661	<.001	.014	<.02	<.01	<2	.286	.014	.13	8.21	<.01	<.01	<.001	<.01	<.01	<.01	.36	.01	.185	30.55	<.01	.06	<.01	.04	<.01	.60	5	29	28	5.14
267662	<.001	.010	<.02	<.01	<2	.255	.014	.13	8.23	<.01	<.01	<.001	<.01	<.01	<.01	.18	.01	.248	30.10	<.01	.05	.23	.09	<.01	.68	4	9	12	5.34
267663	<.001	.013	<.02	<.01	<2	.268	.016	.12	8.23	<.01	<.01	<.001	<.01	<.01	<.01	.13	.01	.244	30.79	<.01	.06	<.01	.02	<.01	.65	2	6	14	4.99
STANDARD R-2a	.051	.577	1.68	4.29	171	.391	.047	.25	25.68	.22	.14	.031	.14	<.01	.02	3.85	.08	.064	2.71	.19	2.92	.59	.73	.08	5.30	485	464	466	-

Standard is STANDARD R-2a/CSB/FA-10R.

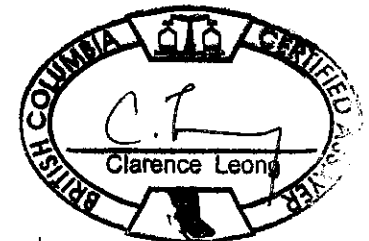
GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCL) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.

TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B BY FIRE ASSAY & ANALYSIS BY ICP. (30 gm)

- SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

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DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Aug. 25/05





SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267664	<.001	.011	<.02	<.01	<2	.243	.013	.11	6.90	<.01	<.01	<.001	<.01	<.01	<.01	.54	<.01	.253	29.52	.01	.12	<.01	.09	<.01	.39	6	18	15	4.97
267665	<.001	.007	<.02	<.01	<2	.252	.015	.13	7.67	<.01	<.01	<.001	<.01	<.01	<.01	.39	<.01	.316	30.85	.01	.08	<.01	.01	<.01	.35	3	18	15	4.81
RE 267665	<.001	.008	<.02	<.01	<2	.243	.014	.13	7.49	<.01	<.01	<.001	<.01	<.01	<.01	.31	<.01	.314	30.45	.01	.07	<.01	.03	<.01	.35	7	9	13	-
RRE 267665	<.001	.007	<.02	<.01	<2	.254	.016	.13	7.84	<.01	<.01	<.001	<.01	<.01	<.01	.31	.01	.325	31.14	.01	.07	<.01	.07	<.01	.35	2	4	13	-
267666	<.001	.024	<.02	<.01	<2	.221	.019	.12	7.96	<.01	<.01	<.001	<.01	<.01	<.01	.20	.01	.198	30.40	<.01	.05	<.01	.05	<.01	.86	2	20	20	5.23
267667	<.001	.029	<.02	<.01	<2	.232	.020	.13	8.64	<.01	<.01	<.001	<.01	<.01	<.01	.35	.01	.190	29.77	.01	.06	<.01	<.01	<.01	1.11	<2	18	16	5.64
267668	<.001	.032	<.02	<.01	<2	.233	.020	.12	9.42	<.01	<.01	<.001	<.01	.01	<.01	1.24	.01	.119	26.56	.03	.56	<.01	.03	<.01	1.70	2	7	13	5.54
267669	<.001	.043	<.02	<.01	<2	.224	.020	.14	10.01	<.01	<.01	<.001	<.01	<.01	.01	1.43	.02	.141	25.79	.07	.71	<.01	.21	<.01	2.06	<2	10	16	5.83
267670A	<.001	.028	<.02	<.01	<2	.234	.016	.14	9.10	<.01	<.01	<.001	<.01	<.01	<.01	.27	<.01	.255	29.23	.01	.07	<.01	.06	<.01	1.39	10	11	16	5.01
267670B	<.001	.028	<.02	<.01	<2	.237	.017	.14	9.29	<.01	<.01	<.001	<.01	<.01	<.01	.23	.01	.252	29.67	.01	.07	<.01	.02	<.01	1.42	7	5	12	-
.STD RTS-2	<.001	.073	<.02	.01	<2	.268	.007	.04	37.16	<.01	<.01	<.001	<.01	<.01	.01	.65	<.01	.012	.40	.18	.88	.20	.14	<.01	18.33	-	-	-	-
267671	<.001	.024	<.02	<.01	<2	.306	.017	.14	10.04	<.01	<.01	<.001	<.01	<.01	<.01	.31	.01	.144	29.87	.01	.05	<.01	.05	<.01	1.61	32	19	23	4.44
267672	<.001	.029	<.02	<.01	<2	.312	.018	.15	10.54	<.01	<.01	<.001	<.01	<.01	<.01	.19	<.01	.119	30.18	<.01	.02	<.01	<.01	<.01	1.89	14	17	14	3.35
267673	<.001	.014	<.02	.01	<2	.211	.014	.12	8.67	<.01	.01	<.001	<.01	<.01	.01	.67	.01	.182	26.94	.03	.55	<.01	.11	<.01	.97	4	3	7	2.13
267674	<.001	.023	<.02	<.01	3	.270	.018	.12	9.10	<.01	<.01	<.001	<.01	<.01	.01	2.41	.01	.156	25.30	.01	.09	<.01	.02	<.01	1.81	<2	21	16	3.55
267675 (pulp)	<.001	.962	<.02	.02	3	1.230	.042	.11	20.43	<.01	.02	<.001	<.01	<.01	.01	3.69	.05	.027	2.87	.34	5.78	1.26	.88	<.01	9.63	193	381	330	-
267676	<.001	.016	<.02	.01	<2	.247	.016	.14	9.07	<.01	<.01	<.001	<.01	<.01	.01	2.51	.01	.193	26.69	.02	.08	<.01	<.01	<.01	1.36	2	8	13	3.34
267677	<.001	.019	<.02	.01	<2	.293	.014	.14	8.13	<.01	<.01	<.001	<.01	<.01	.01	2.57	.01	.158	22.44	.03	.16	<.01	.04	<.01	1.50	3	24	28	5.05
267678	<.001	.029	<.02	<.01	<2	.283	.017	.10	8.91	<.01	<.01	<.001	<.01	<.01	.01	.90	.01	.251	25.59	.02	.08	<.01	<.01	<.01	2.27	2	27	29	2.17
STANDARD R-2a	.051	.583	1.59	4.39	170	.385	.048	.26	25.30	.25	.16	.031	.13	<.01	.02	3.96	.09	.068	2.74	.20	2.99	.44	.65	.09	5.31	484	489	487	-

Standard is STANDARD R-2a/CSB/FA-10R. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-77C File # A504248 Page 1

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens

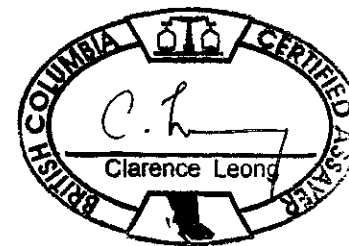


SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267634	.026	.264	.021	1.91
267635	.015	.174	.009	.90
267636	.020	.192	.013	.99
267637	.013	.133	.008	.45
267638	.008	.006	.001	.09
267639	.020	.189	.010	.84
267640A	.017	.184	.010	1.16
267640B	.019	.182	.010	1.17
267641	.016	.094	.008	1.14
267642	.013	.138	.007	1.10
267643	.014	.147	.007	1.33
267644	.019	.143	.008	1.24
267645	.018	.127	.007	1.33
267646	.023	.147	.015	1.39
267647	.029	.189	.020	1.82
RE 267647	.030	.190	.020	1.69
RRE 267647	.029	.186	.020	1.57
267648	.053	.264	.024	2.08
.STD RTS-2	.063	.225	.006	3.31
267649	.027	.231	.019	1.59
267650 (pulp)	.060	.187	.007	.51
267651	.015	.174	.012	2.41
267652	.012	.175	.009	1.27
267653	.012	.142	.010	1.15
267654	.032	.198	.020	1.10
267655	.024	.194	.016	1.25
267656	.016	.207	.009	1.13
267657	.019	.235	.011	.93
267658	.013	.191	.011	.81
267659	.015	.214	.012	1.46
267660 (rock)	.007	.001	<.001	.13
267661	.016	.212	.008	1.25
267662	.012	.195	.009	1.27
267663	.015	.196	.010	1.23
STANDARD R-2a	.532	.326	.042	7.63

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
- SAMPLE TYPE: DRILL CORE R150  
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

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DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Aug 29/05 .....





SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267664	.012	.170	.008	1.24
267665	.008	.151	.008	1.28
RE 267665	.009	.149	.008	1.22
RRE 267665	.008	.151	.008	1.36
267666	.024	.167	.013	1.43
267667	.030	.190	.014	1.74
267668	.031	.219	.018	1.54
267669	.043	.205	.018	1.66
267670A	.027	.204	.013	1.41
267670B	.027	.208	.013	1.59
.STD RTS-2	.057	.226	.008	4.12
267671	.024	.253	.013	1.65
267672	.028	.261	.014	1.83
267673	.013	.184	.012	.98
267674	.022	.248	.017	1.28
267675 (pulp)	.933	1.157	.041	5.68
267676	.016	.206	.014	1.00
267677	.020	.276	.014	1.10
267678	.030	.273	.018	1.19
STANDARD R-2a	.520	.327	.044	8.94

Sample type: DRILL CORE R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



ASSAY CERTIFICATE

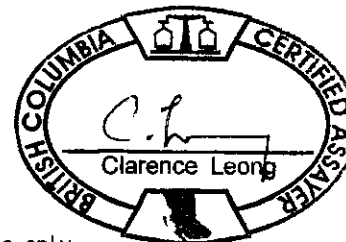
Hard Creek Nickel Corporation PROJECT Tur C05-78A File # A504249 Page 1  
 1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens

SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267679	<.001	.014	<.02	<.01	<2	.035	.008	.15	6.70	<.01	<.01	<.001	<.01	<.01	.02	13.66	.01	.210	12.55	.12	.63	.17	<.01	<.01	1.13	<2	<2	<2	5.33
267680	<.001	.033	<.02	<.01	<2	.022	.006	.22	7.32	<.01	.03	<.001	<.01	<.01	.02	12.94	.03	.168	11.54	.20	1.79	.17	.09	<.01	.62	2	<2	<2	2.53
267681	<.001	.009	<.02	<.01	<2	.026	.006	.16	6.58	<.01	.01	<.001	<.01	<.01	.02	13.47	.01	.200	12.89	.12	.60	.11	<.01	<.01	.81	2	3	<2	5.88
267682	<.001	.021	<.02	<.01	<2	.051	.011	.18	9.73	<.01	.01	<.001	<.01	<.01	.01	10.05	.01	.120	15.65	.10	.66	.26	.05	<.01	1.67	13	3	3	3.74
267683	<.001	.014	<.02	.01	<2	.064	.014	.18	11.91	<.01	<.01	<.001	<.01	<.01	.01	7.13	.02	.099	17.47	.07	.34	.17	<.01	<.01	2.38	4	<2	7	5.17
267684	<.001	.015	<.02	<.01	<2	.034	.009	.17	8.77	<.01	.01	<.001	<.01	<.01	.01	10.06	.01	.142	14.85	.08	.44	<.01	<.01	<.01	1.40	<2	2	4	3.25
267685	<.001	.004	<.02	<.01	<2	.019	.006	.19	8.90	<.01	.03	<.001	<.01	<.01	.03	10.14	.08	.092	10.16	.39	3.09	.29	2.16	<.01	.51	<2	10	10	1.34
267686	<.001	.007	<.02	<.01	<2	.013	.006	.16	7.06	<.01	.01	<.001	<.01	<.01	.02	11.62	.02	.119	12.77	.13	.97	.35	.09	<.01	.94	3	<2	<2	6.34
267687	<.001	.006	<.02	<.01	<2	.014	.006	.16	6.73	<.01	.01	<.001	<.01	<.01	.02	12.48	.01	.145	12.87	.11	.57	.06	<.01	<.01	.98	2	<2	2	5.93
267688	<.001	.013	<.02	<.01	<2	.023	.008	.16	7.69	<.01	.01	<.001	<.01	<.01	.02	11.59	.01	.133	12.72	.10	.70	.17	<.01	<.01	1.49	<2	<2	2	5.02
267689	<.001	.023	<.02	<.01	<2	.067	.014	.16	10.86	<.01	.01	<.001	<.01	<.01	.01	7.68	.02	.083	14.67	.10	.71	.08	<.01	<.01	3.19	<2	2	<2	5.12
267690 (rock)	<.001	.003	<.02	<.01	<2	.001	.001	.12	4.46	<.01	.05	<.001	<.01	<.01	.01	4.79	.05	.003	1.98	.34	8.78	2.64	1.27	<.01	.04	<2	<2	<2	2.44
267691	<.001	.012	<.02	<.01	<2	.018	.006	.16	7.57	<.01	.01	<.001	<.01	<.01	.02	11.38	.04	.134	11.79	.23	1.76	.23	1.16	<.01	.73	3	3	5	4.59
267692	<.001	.009	<.02	<.01	<2	.016	.006	.15	6.01	<.01	.01	<.001	<.01	<.01	.02	13.19	.01	.139	12.48	.11	.81	.12	.01	<.01	.75	15	4	4	5.17
267693	<.001	.032	<.02	<.01	<2	.048	.008	.15	7.02	<.01	.02	<.001	<.01	<.01	.02	11.87	.03	.140	11.41	.15	1.49	.18	.72	<.01	1.02	<2	12	12	3.95
RE 267693	<.001	.033	<.02	<.01	<2	.049	.009	.15	7.15	<.01	.02	<.001	<.01	<.01	.02	12.11	.02	.144	11.58	.15	1.47	.30	.69	<.01	1.04	2	10	6	-
RRE 267693	<.001	.033	<.02	<.01	<2	.047	.008	.15	7.04	<.01	.02	<.001	<.01	<.01	.02	11.78	.02	.148	11.38	.15	1.44	.17	.71	<.01	1.01	<2	11	10	-
.STD RTS-2	<.001	.072	<.02	.01	<2	.274	.008	.04	40.49	<.01	<.01	<.001	<.01	<.01	.01	.64	.01	.012	.36	.18	.81	.30	.11	<.01	18.10	-	-	-	-
267694	<.001	.015	<.02	<.01	<2	.025	.005	.16	6.74	<.01	.02	<.001	<.01	<.01	.02	11.88	.05	.138	11.19	.26	2.30	.62	.96	<.01	.30	2	14	13	5.02
267695	<.001	.019	<.02	<.01	<2	.048	.008	.15	6.92	<.01	.01	<.001	<.01	<.01	.01	11.56	.01	.148	13.46	.12	.75	.12	<.01	<.01	.85	2	24	26	5.39
267696	<.001	.016	<.02	<.01	<2	.053	.008	.15	7.08	<.01	.01	<.001	<.01	<.01	.01	10.60	.01	.113	13.51	.14	1.16	.24	.09	<.01	.84	3	6	4	5.11
267697	<.001	.014	<.02	<.01	<2	.025	.007	.15	6.63	<.01	.01	<.001	<.01	<.01	.02	11.90	.02	.109	12.02	.18	1.66	.77	.24	<.01	.53	<2	6	9	5.89
267698	<.001	.007	<.02	<.01	<2	.024	.006	.17	7.95	<.01	.03	<.001	<.01	<.01	.02	12.12	.06	.093	10.09	.32	2.68	.18	1.21	<.01	.42	2	7	15	4.43
267699	<.001	.018	<.02	<.01	<2	.032	.007	.14	6.01	<.01	.01	<.001	<.01	<.01	.01	13.60	<.01	.146	12.63	.13	.60	.12	<.01	<.01	.68	<2	5	2	5.66
267700 (pulp)	.001	.009	<.02	<.01	<2	.097	.003	.09	5.33	.01	.02	<.001	<.01	<.01	.01	4.07	.05	.088	1.80	.34	8.47	2.49	1.17	<.01	.33	660	467	1571	-
267701	<.001	.023	<.02	<.01	<2	.055	.007	.14	6.94	<.01	.01	<.001	<.01	<.01	.02	13.46	.01	.157	12.00	.17	.90	.11	.08	<.01	1.25	3	8	27	4.65
267702	<.001	.050	<.02	<.01	<2	.117	.016	.16	10.99	<.01	.01	<.001	<.01	<.01	.01	9.44	.02	.110	14.56	.13	.91	.12	.17	<.01	2.74	3	63	75	5.17
267702A	<.001	.049	<.02	<.01	<2	.120	.018	.15	12.14	<.01	.01	<.001	<.01	<.01	.01	6.14	.01	.068	18.26	.07	.35	<.01	.02	<.01	2.82	<2	103	50	4.47
267703	<.001	.016	<.02	<.01	<2	.040	.007	.15	6.68	<.01	.01	<.001	<.01	<.01	.01	12.29	<.01	.143	13.72	.11	.80	.24	<.01	<.01	.73	<2	21	25	4.81
267704	<.001	.019	<.02	<.01	<2	.015	.006	.14	6.17	<.01	.01	<.001	<.01	<.01	.02	13.93	<.01	.126	13.10	.13	.79	.06	<.01	<.01	.58	<2	2	2	6.00
267705	<.001	.015	<.02	<.01	<2	.017	.006	.16	6.11	<.01	.05	<.001	<.01	<.01	.02	16.67	.02	.145	9.96	.17	1.44	.18	.51	<.01	.52	<2	6	2	4.91
267706	<.001	.079	<.02	<.01	<2	.055	.012	.13	8.03	<.01	.01	<.001	<.01	<.01	.02	13.63	<.01	.163	11.54	.12	.61	.18	.03	<.01	2.37	<2	7	6	6.30
267707	<.001	.046	<.02	<.01	<2	.094	.015	.14	9.55	<.01	.01	<.001	<.01	<.01	.01	10.67	<.01	.133	14.05	.11	.58	.36	.08	<.01	2.61	3	24	27	5.56
267708	<.001	.015	<.02	<.01	<2	.070	.010	.15	8.21	<.01	.01	<.001	<.01	<.01	.01	9.06	<.01	.162	16.62	.10	.62	.12	.03	<.01	.99	7	38	45	5.33
STANDARD R-2a	.051	.572	1.69	4.23	172	.378	.047	.25	26.55	.21	.15	.031	.14	<.01	.02	3.93	.09	.066	2.70	.19	2.76	.60	.74	.08	5.36	488	479	480	-

Standard is STANDARD R-2a/CSB/FA-10R.

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCL) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.  
 TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B - 30.00 GM SAMPLE ANALYSIS BY FA/ICP.  
 - SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data SS FA \_\_\_\_\_ DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Aug 25/05



All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267709	.001	.028	<.02	<.01	<2	.056	.012	.17	9.38	<.01	.01	<.001	<.01	<.01	.01	9.42	.02	.094	15.14	.13	1.01	.04	.19	<.01	1.43	<2	<2	<2	5.37
STANDARD	.050	.571	1.73	4.28	173	.394	.049	.25	26.46	.23	.16	.031	.14	<.01	.02	3.81	.09	.063	2.67	.20	2.76	.71	.76	.09	5.33	488	478	484	-

Standard is STANDARD R-2a/CSB/FA-10R.

ASSAY CERTIFICATE



Hard Creek Nickel Corporation PROJECT Tur C05-78B File # A504250 Page 1

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens

SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267710	<.001	.014	<.02	.01	<2	.060	.008	.17	7.89	<.01	.01	<.001	<.01	<.01	.01	8.12	.02	.118	15.48	.14	1.30	.31	.19	<.01	.45	3	8	17	4.70
267711	<.001	.027	<.02	.01	<2	.092	.011	.16	9.05	<.01	.01	<.001	<.01	<.01	.01	7.95	<.01	.148	17.60	.09	.46	<.01	.05	<.01	1.00	11	12	32	4.42
267712	<.001	.006	<.02	.01	<2	.152	.009	.16	8.33	<.01	.01	<.001	<.01	<.01	.01	5.81	.01	.114	20.00	.09	.82	<.01	<.01	<.01	.25	2	<2	3	5.05
267713	<.001	.007	<.02	.01	<2	.192	.011	.17	9.29	<.01	.01	<.001	<.01	<.01	.01	2.37	<.01	.108	23.78	.05	.25	<.01	.04	<.01	.20	4	<2	<2	4.70
267714	<.001	.003	<.02	.01	<2	.185	.011	.14	9.18	<.01	.01	<.001	<.01	<.01	.01	2.69	.01	.103	23.77	.05	.25	.05	<.01	<.01	.16	6	2	6	4.76
267715	<.001	.005	<.02	.01	<2	.190	.010	.19	9.31	<.01	.01	<.001	<.01	<.01	.01	2.46	.01	.123	24.82	.05	.35	<.01	.03	<.01	.16	3	<2	9	5.24
267716	<.001	.007	<.02	.01	<2	.172	.011	.17	9.99	<.01	.01	<.001	<.01	<.01	.01	2.71	.01	.142	23.85	.04	.23	<.01	.04	<.01	.32	3	<2	6	5.65
267717	<.001	.028	<.02	<.01	<2	.053	.009	.14	7.05	<.01	.01	<.001	<.01	<.01	.01	10.62	.01	.172	14.60	.11	.54	<.01	.01	<.01	1.18	3	5	15	4.83
267718	<.001	.023	<.02	<.01	<2	.046	.009	.14	6.63	<.01	.01	<.001	<.01	<.01	.01	12.40	.01	.191	13.35	.15	.91	.02	.06	<.01	.93	<2	10	14	5.32
267719	<.001	.025	<.02	<.01	3	.032	.007	.14	6.74	<.01	.04	<.001	<.01	<.01	.02	12.32	.03	.157	11.04	.20	2.40	.09	.58	<.01	.62	<2	17	15	5.26
267720 (rock)	<.001	.008	<.02	<.01	<2	.002	.001	.12	4.49	<.01	.05	<.001	<.01	<.01	.02	4.61	.06	.005	2.04	.35	8.90	2.37	1.24	<.01	<.02	<2	<2	<2	2.28
267721	<.001	.022	<.02	<.01	2	.034	.008	.12	5.67	<.01	.01	<.001	<.01	<.01	.01	13.16	.01	.187	11.77	.12	.63	.10	.07	<.01	.97	5	9	11	5.06
267722	<.001	.034	<.02	<.01	<2	.044	.011	.13	6.83	<.01	.01	<.001	<.01	<.01	.02	13.67	<.01	.205	11.76	.12	.52	<.01	.06	<.01	1.79	2	4	7	6.11
RE 267722	<.001	.035	<.02	<.01	<2	.047	.011	.13	7.02	<.01	.01	<.001	<.01	<.01	.02	14.09	.01	.207	12.09	.12	.52	.18	.07	<.01	1.78	4	<2	4	-
RRE 267722	<.001	.036	<.02	<.01	<2	.046	.012	.13	6.88	<.01	.01	<.001	<.01	<.01	.02	13.71	.01	.203	11.72	.12	.51	.19	.06	<.01	1.84	5	<2	<2	-
267723	<.001	.024	<.02	<.01	<2	.036	.008	.12	6.07	<.01	.01	<.001	<.01	<.01	.01	13.15	<.01	.181	12.55	.11	.50	.01	<.01	<.01	1.19	2	<2	<2	5.91
267724	<.001	.031	<.02	<.01	<2	.068	.011	.12	7.52	<.01	.01	<.001	<.01	<.01	.01	9.39	.01	.168	16.24	.09	.50	.20	.09	<.01	1.36	<2	11	4	5.55
267725 (pulp)	.001	.011	<.02	<.01	<2	.097	.003	.09	5.28	<.01	.02	<.001	<.01	<.01	.01	3.95	.05	.091	1.94	.35	8.35	2.25	1.12	<.01	.32	770	454	1567	-
.STD RTS-2	<.001	.071	<.02	.01	3	.273	.008	.04	37.40	<.01	.01	<.001	<.01	<.01	.01	.62	.01	.012	.39	.18	.88	.41	.20	<.01	18.96	-	-	-	-
267726	<.001	.040	<.02	<.01	<2	.040	.012	.13	7.38	<.01	.01	<.001	<.01	<.01	.02	14.09	.01	.195	12.13	.12	.54	.02	.11	<.01	2.02	4	5	7	5.85
267727	<.001	.029	<.02	<.01	<2	.045	.010	.13	6.73	<.01	.01	<.001	<.01	<.01	.01	13.26	.01	.187	13.11	.13	.69	.09	.13	<.01	1.38	3	9	12	5.50
267728	<.001	.024	<.02	<.01	<2	.048	.008	.14	6.75	<.01	.02	<.001	<.01	<.01	.01	12.18	.01	.167	13.29	.17	1.47	.30	.45	<.01	.85	<2	4	14	6.40
267729	<.001	.018	<.02	<.01	<2	.049	.007	.13	6.07	<.01	.01	<.001	<.01	<.01	.01	12.45	.01	.161	13.13	.11	.88	.23	.04	<.01	1.04	4	6	11	5.40
267730A	<.001	.012	<.02	<.01	<2	.040	.006	.13	5.56	<.01	.02	<.001	<.01	<.01	.01	12.74	.02	.164	12.59	.14	1.08	.32	.21	<.01	.69	<2	6	8	5.59
267730B	<.001	.012	<.02	<.01	<2	.042	.006	.13	5.51	<.01	.02	<.001	<.01	<.01	.01	12.50	.01	.166	12.34	.14	1.07	.39	.25	<.01	.70	2	6	10	-
267731	<.001	.033	<.02	<.01	<2	.060	.008	.12	5.93	<.01	.01	<.001	<.01	<.01	.01	13.64	<.01	.206	11.80	.12	.62	.39	.08	<.01	1.44	3	9	10	6.13
267732	<.001	.016	<.02	<.01	<2	.038	.006	.13	5.32	<.01	.01	<.001	<.01	<.01	.01	13.46	.01	.180	12.74	.12	.71	.06	.07	<.01	.73	2	4	9	4.97
267733	<.001	.031	<.02	<.01	<2	.064	.008	.14	6.61	<.01	.02	<.001	<.01	<.01	.02	12.67	.03	.174	11.78	.17	1.52	.26	.22	<.01	1.12	<2	12	11	5.05
267734	<.001	.033	<.02	<.01	<2	.064	.010	.13	6.95	<.01	.01	<.001	<.01	<.01	.01	11.66	.01	.179	13.71	.11	.63	.07	.07	<.01	1.59	2	4	6	6.29
267735	<.001	.020	<.02	<.01	<2	.038	.006	.13	6.09	<.01	.01	<.001	<.01	<.01	.02	12.66	.02	.154	12.38	.16	1.03	.15	.22	<.01	.97	2	5	4	5.26
267736	<.001	.026	<.02	<.01	<2	.043	.008	.13	6.28	<.01	.01	<.001	<.01	<.01	.01	13.34	.02	.177	11.67	.16	.85	.22	.10	<.01	1.46	4	7	3	4.72
267737	<.001	.018	<.02	<.01	2	.022	.004	.14	5.94	<.01	.06	<.001	<.01	<.01	.02	11.02	.07	.120	8.55	.25	3.61	1.38	.72	<.01	.47	3	7	5	5.14
267738	<.001	.015	<.02	<.01	3	.132	.009	.11	6.75	<.01	.01	<.001	<.01	<.01	.01	7.03	.01	.178	18.74	.08	.50	.16	.17	<.01	.78	3	<2	<2	5.87
267739	<.001	.044	<.02	<.01	2	.132	.012	.13	8.43	<.01	.01	<.001	<.01	<.01	.01	6.86	.01	.151	16.71	.12	.86	.17	.16	<.01	1.62	4	<2	15	5.55
STANDARD R-2a	.052	.570	1.74	4.28	175	.386	.049	.26	25.38	.22	.15	.032	.14	<.01	.02	3.98	.09	.075	2.86	.20	2.87	.50	.68	.09	5.28	483	477	486	-

Standard is STANDARD R-2a/CSB/FA-10R.

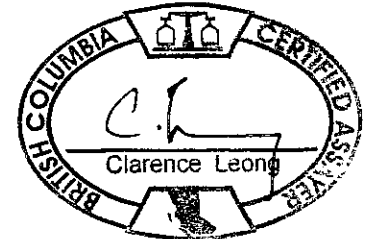
GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCl) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.

TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B BY FIRE ASSAY & ANALYSIS BY ICP. (30 gm)

- SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Aug 23/05





SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267740	<.001	.022	<.02	<.01	<2	.103	.010	.14	7.57	<.01	.01	<.001	<.01	<.01	.01	8.36	.01	.201	17.34	.10	.74	.15	.11	<.01	.70	3	6	11	5.57
267741	<.001	.037	<.02	<.01	<2	.066	.009	.14	7.78	<.01	.01	<.001	<.01	<.01	.01	11.64	.01	.180	14.61	.11	.54	.14	<.01	<.01	1.35	4	17	22	6.16
267742	<.001	.041	<.02	<.01	<2	.110	.015	.15	8.94	<.01	.01	<.001	<.01	<.01	.01	12.21	.01	.200	13.03	.12	.69	.13	<.01	<.01	2.49	2	25	25	5.61
267743	<.001	.036	<.02	<.01	<2	.057	.010	.15	7.95	<.01	.02	<.001	<.01	<.01	.02	11.38	.03	.147	12.25	.19	1.49	.43	.27	<.01	1.46	<2	11	14	5.35
.STD RTS-2	<.001	.072	<.02	.01	<2	.273	.008	.04	39.81	<.01	<.01	<.001	<.01	<.01	.01	.68	.01	.013	.43	.18	.83	.24	.11	<.01	18.87	-	-	-	-
267744	<.001	.033	<.02	<.01	<2	.056	.010	.14	7.48	<.01	.02	<.001	<.01	<.01	.02	10.11	.02	.135	13.26	.16	1.44	.42	.23	<.01	1.33	2	11	11	5.57
267745	<.001	.028	<.02	.01	<2	.046	.014	.17	10.56	<.01	.02	<.001	<.01	<.01	.02	8.29	.03	.105	15.21	.16	1.30	.30	.17	<.01	1.60	3	<2	<2	5.15
267746	<.001	.010	<.02	<.01	<2	.124	.012	.17	10.06	<.01	<.01	<.001	<.01	<.01	.01	5.76	.02	.104	18.83	.08	.67	.29	<.01	<.01	1.22	2	4	7	5.33
267747	<.001	.006	<.02	<.01	<2	.167	.011	.17	11.02	<.01	<.01	<.001	<.01	<.01	.01	3.65	.01	.089	22.30	.06	.29	.09	<.01	<.01	.61	5	3	4	5.32
267748	<.001	.009	<.02	<.01	<2	.178	.011	.18	11.36	<.01	<.01	<.001	<.01	<.01	.02	4.21	.01	.104	21.19	.08	.30	.08	<.01	<.01	.90	2	11	10	3.24
STANDARD R	.051	.570	1.74	4.39	174	.384	.049	.26	26.70	.21	.15	.031	.13	<.01	.02	3.94	.09	.071	2.72	.20	2.87	.52	.68	.08	5.31	497	485	477	-

Standard is STANDARD R-2a/CSB/FA-10R.

ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-79A File # A504251 Page 1  
1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens



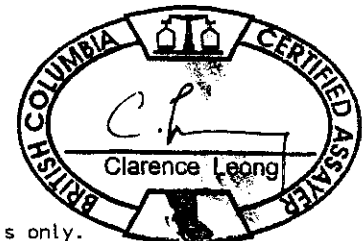
SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267749	<.001	.010	<.02	.01	<2	.120	.012	.18	9.21	<.01	<.01	<.001	<.01	<.01	.02	2.75	.01	.150	20.87	.05	.39	.07	<.01	<.01	.74	6	12	16	3.31
267750 (pulp)	<.001	.058	<.02	.01	<2	.248	.012	.12	9.16	<.01	<.01	<.001	<.01	<.01	.02	4.70	.02	.912	15.51	.20	4.17	.41	.14	<.01	.53	18	101	302	-
267751	<.001	.009	<.02	.01	<2	.110	.014	.17	9.63	<.01	<.01	<.001	<.01	<.01	.02	2.12	.01	.141	21.45	.05	.33	<.01	.06	<.01	.92	3	12	13	5.56
267752	<.001	.006	<.02	.01	<2	.106	.011	.19	8.48	<.01	<.01	<.001	<.01	<.01	.02	4.27	.01	.138	19.95	.06	.37	.06	.02	<.01	.68	3	8	8	5.09
267753	<.001	.023	<.02	<.01	<2	.094	.012	.21	8.40	<.01	<.01	<.001	<.01	<.01	.02	5.94	.01	.111	17.87	.09	.81	.12	.12	<.01	.93	2	15	12	4.24
267754	<.001	.017	<.02	<.01	<2	.101	.011	.18	8.01	<.01	<.01	<.001	<.01	<.01	.03	7.31	.01	.118	19.15	.06	.36	<.01	<.01	<.01	.84	5	7	13	5.30
267755	<.001	.005	<.02	<.01	<2	.229	.013	.17	8.67	<.01	<.01	<.001	<.01	<.01	.01	1.35	.02	.154	26.51	.03	.36	<.01	<.01	<.01	.55	5	35	31	4.30
267756	<.001	.001	<.02	<.01	<2	.238	.011	.15	6.88	<.01	<.01	<.001	<.01	<.01	.01	1.56	.01	.522	26.66	.02	.18	<.01	.01	<.01	.52	9	19	17	4.48
267757	<.001	.001	<.02	<.01	<2	.236	.012	.12	6.89	<.01	<.01	<.001	<.01	<.01	.01	.65	.01	.172	27.14	.02	.17	<.01	.01	<.01	.48	10	30	29	4.30
267758	<.001	.001	<.02	<.01	<2	.172	.009	.16	7.57	<.01	<.01	<.001	<.01	<.01	.02	3.27	.01	.311	22.24	.08	.65	.06	<.01	<.01	.38	4	10	17	4.09
267759	<.001	.004	<.02	<.01	<2	.157	.008	.17	8.42	<.01	.01	<.001	<.01	<.01	.02	3.95	.03	.110	18.35	.16	1.70	.29	.50	<.01	.67	6	6	9	4.11
267760A	.001	.013	<.02	<.01	<2	.108	.010	.19	9.68	<.01	<.01	<.001	<.01	<.01	.04	6.33	.01	.117	15.65	.17	1.04	.53	.19	<.01	2.16	7	17	9	4.40
267760B	.001	.014	<.02	<.01	<2	.101	.010	.20	9.58	<.01	<.01	<.001	<.01	<.01	.04	6.58	<.01	.113	15.73	.18	1.05	.35	.22	<.01	2.01	5	10	9	-
267761	<.001	.006	<.02	.01	<2	.057	.006	.23	9.13	<.01	<.01	<.001	<.01	<.01	.05	6.85	.01	.117	14.95	.21	1.02	.47	.04	<.01	.87	3	10	12	4.48
267762	<.001	<.001	<.02	<.01	<2	.075	.005	.19	7.83	<.01	.01	<.001	<.01	<.01	.03	6.48	.02	.087	14.69	.32	2.17	.59	.31	<.01	.49	2	10	11	4.12
.STD RTS-2	<.001	.071	<.02	<.01	<2	.269	.008	.04	38.17	<.01	<.01	<.001	<.01	<.01	.01	.66	.01	.013	.44	.17	.90	.23	.13	<.01	18.14	-	-	-	-
267763	<.001	.015	<.02	<.01	<2	.118	.011	.17	8.87	<.01	<.01	<.001	<.01	<.01	.03	6.47	.01	.098	17.70	.23	1.14	.24	.11	<.01	1.33	10	70	75	6.06
267764	<.001	.006	<.02	<.01	<2	.108	.009	.24	10.21	<.01	<.01	<.001	<.01	<.01	.03	4.04	.02	.094	18.01	.22	1.06	.06	.25	<.01	.77	5	2	4	4.05
267765	<.001	.004	<.02	<.01	<2	.036	.005	.18	7.85	<.01	.03	<.001	<.01	<.01	.03	7.47	.07	.075	10.37	.41	4.52	1.73	.64	<.01	.45	4	5	7	4.48
267766	<.001	.003	<.02	<.01	<2	.067	.007	.17	7.33	<.01	.01	<.001	<.01	<.01	.03	8.13	<.01	.096	15.01	.29	1.81	.41	.17	<.01	.69	6	4	2	5.73
RE 267766	<.001	.003	<.02	<.01	<2	.067	.007	.17	7.43	<.01	.01	<.001	<.01	<.01	.03	8.25	.01	.099	15.19	.30	1.89	.42	.16	<.01	.69	3	<2	<2	-
RRE 267766	<.001	.004	<.02	<.01	<2	.068	.007	.17	7.43	<.01	.01	<.001	<.01	<.01	.03	8.33	.01	.100	15.24	.30	1.89	.48	.17	<.01	.67	5	7	8	-
267767	<.001	.009	<.02	<.01	<2	.068	.008	.21	9.02	<.01	.01	<.001	<.01	<.01	.04	6.92	.01	.095	15.29	.30	1.79	.18	.15	<.01	1.51	6	<2	6	5.69
267768	<.001	.004	<.02	<.01	<2	.051	.006	.20	8.69	<.01	.04	<.001	<.01	<.01	.03	6.66	.08	.078	11.11	.38	4.59	1.62	.93	<.01	.57	2	<2	5	4.38
267769	.001	.009	<.02	.01	<2	.063	.009	.23	10.89	<.01	.01	<.001	<.01	<.01	.04	5.38	.05	.097	14.08	.28	2.07	.60	.37	<.01	2.13	5	14	9	4.83
267770	.001	.008	<.02	.01	<2	.073	.010	.18	11.12	<.01	.01	<.001	<.01	<.01	.04	5.96	.05	.109	14.41	.41	2.48	.54	.29	<.01	3.01	12	6	10	5.46
267771	<.001	.001	<.02	<.01	<2	.136	.009	.15	7.46	<.01	.01	<.001	<.01	<.01	.02	5.14	.03	.107	20.19	.27	1.98	.30	.26	<.01	.60	2	3	4	5.66
267772	<.001	.002	<.02	<.01	<2	.121	.008	.17	8.49	<.01	.01	<.001	<.01	<.01	.02	4.22	.03	.125	18.60	.36	2.37	.60	.36	<.01	.70	3	<2	<2	5.57
267773	<.001	.004	<.02	<.01	<2	.041	.007	.22	9.79	<.01	.01	<.001	<.01	<.01	.04	7.33	.01	.155	14.47	.40	1.99	.36	.17	<.01	1.44	3	2	9	5.67
267774	<.001	.004	<.02	<.01	<2	.048	.007	.18	9.90	<.01	.01	<.001	<.01	<.01	.03	6.27	.08	.119	13.93	.62	3.68	.72	.43	<.01	1.35	5	68	28	5.96
267775 (pulp)	<.001	.054	<.02	.01	<2	.242	.011	.11	9.25	<.01	<.01	<.001	<.01	<.01	.02	4.65	<.01	.952	14.99	.20	4.09	.24	.12	<.01	.54	12	88	307	-
267776	<.001	.001	<.02	<.01	<2	.086	.009	.15	8.22	<.01	.01	<.001	<.01	<.01	.02	3.32	.04	.155	18.23	.25	2.64	.24	.64	<.01	.76	3	45	20	5.07
267777	<.001	.002	<.02	<.01	<2	.110	.009	.14	7.53	<.01	.02	<.001	<.01	<.01	.01	3.77	.04	.125	18.36	.25	2.80	.41	.45	<.01	.76	2	57	24	4.31
267778	<.001	.002	<.02	<.01	<2	.103	.007	.16	8.24	<.01	.02	<.001	<.01	<.01	.02	6.10	.06	.126	15.05	.36	3.19	.42	.78	<.01	.43	6	8	12	5.27
STANDARD R-2a	.051	.580	1.72	4.34	171	.391	.048	.26	25.99	.03	.14	.031	.13	<.01	.02	3.93	.09	.067	2.78	.20	2.94	.50	.63	.08	5.43	484	482	481	-

Standard is STANDARD R-2a/CSB/FA-10R.

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCL) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.  
TOTAL S GROUP 2A BY LECD. AU\*\* PT\*\* PD\*\* GROUP 3B BY FIRE ASSAY & ANALYSIS BY ICP. (30 gm)  
- SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data d FA \_\_\_\_\_

DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Aug 26/05





SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267779	<.001	.023	<.02	.01	<2	.117	.008	.15	7.64	<.01	.01	<.001	<.01	<.01	.02	3.43	.04	.150	19.46	.22	1.89	.14	.18	<.01	.85	13	2	4	3.80
267780 (rock)	<.001	.010	<.02	.01	<2	.002	.001	.12	4.50	<.01	.05	<.001	<.01	<.01	.01	4.72	.06	.002	1.90	.35	9.58	2.64	1.31	<.01	<.02	<2	<2	<2	2.67
267781	<.001	.005	<.02	.01	<2	.137	.010	.15	7.79	<.01	<.01	<.001	<.01	<.01	.01	1.85	.01	.157	23.91	.18	1.61	<.01	.52	<.01	.41	2	3	<2	4.37
267782	<.001	.006	<.02	.01	<2	.142	.010	.16	7.45	<.01	.01	<.001	<.01	<.01	.01	2.56	.02	.139	21.69	.24	2.05	.12	.69	<.01	.48	4	7	4	4.66
267783	<.001	.009	<.02	.01	<2	.123	.010	.17	8.15	<.01	<.01	<.001	<.01	<.01	.02	2.13	.06	.143	22.72	.20	1.34	<.01	.33	<.01	.83	<2	4	<2	5.43
RE 267783	<.001	.009	<.02	.01	<2	.119	.009	.17	8.08	<.01	<.01	<.001	<.01	<.01	.02	2.10	.05	.143	22.30	.20	1.38	<.01	.27	<.01	.85	<2	4	4	-
RRE 267783	<.001	.008	<.02	.01	<2	.123	.010	.17	8.08	<.01	<.01	<.001	<.01	<.01	.02	2.17	.06	.144	22.26	.21	1.41	<.01	.35	<.01	.88	<2	7	8	-
.STD RTS-2	<.001	.076	<.02	.01	<2	.276	.007	.04	38.26	<.01	<.01	<.001	<.01	<.01	.01	.66	.01	.012	.43	.18	.86	.18	.16	<.01	18.53	-	-	-	-
267784	<.001	.027	<.02	.01	<2	.088	.013	.17	11.04	<.01	.02	<.001	<.01	<.01	.04	6.37	.08	.088	15.48	.65	3.30	.48	.65	<.01	2.06	2	12	4	5.66
267785	.002	.026	<.02	.01	<2	.049	.007	.17	8.16	<.01	.01	<.001	<.01	<.01	.03	12.14	.05	.093	12.75	.45	1.82	.35	.25	<.01	1.34	2	32	24	5.70
267786	<.001	.029	<.02	.01	<2	.058	.007	.17	9.29	<.01	.01	<.001	<.01	<.01	.04	10.88	.11	.097	13.33	.65	2.26	.43	.20	<.01	1.88	2	20	21	5.06
267787	<.001	.038	<.02	.01	<2	.119	.013	.18	10.72	<.01	.01	<.001	<.01	<.01	.03	6.20	.02	.099	18.88	.43	1.72	.37	.15	<.01	1.60	4	120	72	5.70
267788	<.001	.027	<.02	.01	<2	.159	.012	.17	10.45	<.01	.01	<.001	<.01	<.01	.02	4.85	.11	.163	19.46	.48	1.99	.32	.26	<.01	1.71	4	35	20	5.71
267789	<.001	.015	<.02	.01	<2	.182	.012	.15	8.86	<.01	.01	<.001	<.01	<.01	.02	2.98	.02	.152	20.97	.25	2.01	.26	.53	<.01	1.42	3	16	17	4.65
267790A	<.001	.021	<.02	.01	<2	.128	.010	.18	10.67	<.01	.01	<.001	<.01	<.01	.04	5.08	.11	.119	15.60	.60	2.59	.41	.47	<.01	2.13	3	7	15	4.42
267790B	<.001	.023	<.02	.01	<2	.126	.010	.18	10.72	<.01	.01	<.001	<.01	<.01	.04	5.16	.11	.116	15.65	.60	2.59	.50	.49	<.01	2.08	3	4	15	-
STANDARD R-2a	.050	.580	1.72	4.37	169	.379	.048	.26	25.75	.23	.14	.031	.14	<.01	.02	3.90	.09	.067	2.71	.20	2.97	.47	.67	.08	5.37	485	483	483	-

Standard is STANDARD R-2a/CSB/FA-10R. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE



Hard Creek Nickel Corporation PROJECT Tur C05-79A File # A504251 Page 1

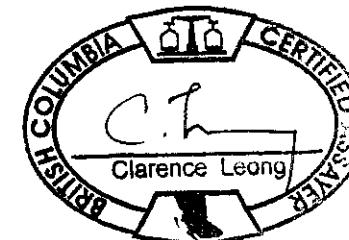
1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchins

SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267749	.011	.094	.009	.70
267750 (pulp)	.055	.191	.008	.60
267751	.010	.094	.011	.87
267752	.009	.084	.008	.67
267753	.024	.080	.010	1.01
267754	.018	.090	.010	.91
267755	.007	.189	.011	.78
267756	.004	.215	.010	.79
267757	.004	.202	.010	.68
267758	.005	.148	.007	.49
267759	.008	.128	.006	.69
267760A	.015	.087	.009	1.76
267760B	.015	.083	.009	1.73
267761	.010	.043	.005	1.01
267762	.004	.053	.004	.48
. STD RTS-2	.057	.221	.006	5.45
267763	.017	.083	.008	1.00
267764	.010	.064	.006	.74
267765	.007	.024	.003	.34
267766	.007	.044	.005	.59
RE 267766	.007	.045	.005	.67
RRE 267766	.007	.044	.005	.52
267767	.012	.056	.007	1.03
267768	.007	.038	.004	.48
267769	.012	.053	.007	1.12
267770	.011	.054	.008	1.42
267771	.006	.075	.005	.67
267772	.005	.075	.005	.59
267773	.007	.028	.005	.82
267774	.007	.034	.005	.76
267775 (pulp)	.057	.201	.008	.64
267776	.006	.060	.006	.52
267777	.006	.080	.006	.58
267778	.006	.069	.004	.38
STANDARD R-2a	.494	.327	.041	9.93

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
- SAMPLE TYPE: DRILL CORE R150  
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Sept 3/05





SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267779	.025	.096	.007	.65
267780 (rock)	.010	<.001	<.001	.13
267781	.006	.103	.007	.50
267782	.007	.098	.007	.38
267783	.010	.084	.007	.47
RE 267783	.010	.084	.007	.47
RRE 267783	.010	.084	.007	.47
.STD RTS-2	.059	.230	.007	3.46
267784	.026	.069	.010	.91
267785	.027	.038	.006	.59
267786	.028	.046	.006	.85
267787	.036	.092	.010	.72
267788	.026	.127	.009	.73
267789	.015	.142	.009	.60
267790A	.023	.107	.008	.83
267790B	.022	.105	.008	1.03
STANDARD R-2a	.503	.325	.042	8.33

Sample type: DRILL CORE R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



ASSAY CERTIFICATE



Hard Creek Nickel Corporation PROJECT Tur C05-79B File # A504252 Page 1

Submitted by: Tony Hitchins

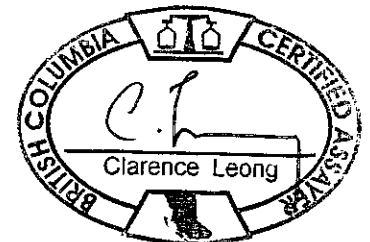
SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267791	.002	.020	<.02	.02	<2	.061	.009	.18	9.52	<.02	.04	<.001	<.01	<.01	.04	6.36	.06	.097	10.55	.34	3.94	1.15	.93	<.01	2.35	<2	16	22	4.95
267792	.002	.026	<.02	.01	<2	.133	.013	.18	10.69	<.02	<.01	<.001	<.01	<.01	.03	5.05	<.01	.122	15.14	.29	1.59	.28	.25	<.01	3.06	<2	14	14	5.47
267793	.001	.008	<.02	.02	<2	.158	.009	.17	7.63	<.02	<.01	<.001	<.01	<.01	.02	2.59	.02	.104	17.99	.29	1.49	.17	.50	<.01	1.07	2	9	10	4.97
267794	<.001	.003	<.02	.02	<2	.148	.008	.24	10.99	<.02	<.01	<.001	<.01	<.01	.03	3.45	<.01	.130	18.75	.12	.46	.07	.02	<.01	.29	<2	5	10	4.63
267795	.001	.005	<.02	.02	<2	.091	.006	.24	10.15	<.02	<.01	<.001	<.01	<.01	.05	6.18	<.01	.146	15.78	.16	.58	.09	.01	<.01	.79	<2	<2	2	4.14
267796	.001	.009	<.02	.02	<2	.109	.009	.24	13.33	<.02	<.01	<.001	<.01	<.01	.04	5.91	.01	.121	17.27	.13	.48	.09	.02	<.01	1.33	5	<2	8	5.34
267797	.001	.013	<.02	.01	<2	.089	.008	.23	12.51	<.02	<.01	<.001	<.01	<.01	.04	7.21	.02	.097	14.70	.15	.92	.21	.13	<.01	1.89	<2	5	6	5.90
267798	.001	.017	<.02	.01	<2	.029	.014	.18	14.46	<.02	<.01	<.001	<.01	<.01	.05	9.99	.01	.086	11.05	.16	.88	.13	.23	<.01	4.50	<2	12	6	4.92
267799	<.001	.035	<.02	.01	<2	.029	.019	.17	11.91	<.02	<.01	<.001	<.01	<.01	.02	11.29	<.01	.131	12.27	.12	.38	.11	<.01	<.01	3.64	2	5	10	6.46
267800 (pulp)	<.001	.101	<.02	.02	<2	.357	.016	.05	9.34	<.02	<.01	<.001	<.01	<.01	.01	3.56	<.01	.353	15.11	.15	2.72	.25	.05	<.01	1.05	9	75	397	-
267801	<.001	.038	<.02	.01	<2	.036	.014	.16	9.21	<.02	<.01	<.001	<.01	<.01	.02	12.30	<.01	.135	12.23	.12	.42	.12	<.01	<.01	2.25	<2	8	8	5.46
267802	<.001	.032	<.02	.01	<2	.032	.012	.16	8.66	<.02	<.01	<.001	<.01	<.01	.02	12.48	<.01	.148	12.14	.13	.55	.14	.01	<.01	1.84	<2	2	3	6.47
267803	<.001	.033	<.02	<.01	<2	.015	.008	.16	7.52	<.02	.02	<.001	<.01	<.01	.02	12.78	.02	.128	10.60	.19	1.36	.35	.25	<.01	1.22	<2	7	3	8.59
267804	<.001	.017	<.02	<.01	<2	.022	.011	.17	8.40	<.02	<.01	<.001	<.01	<.01	.02	12.95	<.01	.133	11.53	.13	.71	.14	.02	<.01	1.69	<2	<2	<2	2.61
267805	<.001	.032	<.02	.01	<2	.030	.015	.16	10.95	<.02	<.01	<.001	<.01	<.01	.03	11.33	<.01	.115	11.39	.13	.63	.11	.01	<.01	3.30	<2	8	14	5.43
267806	<.001	.011	<.02	<.01	<2	.051	.011	.16	10.12	<.02	<.01	<.001	<.01	<.01	.03	10.80	<.01	.116	13.79	.10	.34	.09	<.01	<.01	2.21	<2	<2	7	6.20
.STD RTS-2	<.001	.074	<.02	.02	<2	.276	.007	.04	38.22	<.02	<.01	<.001	<.01	<.01	.01	.64	<.01	.012	.40	.17	.81	.23	.13	<.01	18.92	-	-	-	-
267807	.001	.005	<.02	.01	<2	.035	.008	.18	8.80	<.02	<.01	<.001	<.01	<.01	.03	11.01	<.01	.124	13.99	.11	.51	.11	.03	<.01	1.13	<2	4	<2	5.67
RE 267807	.001	.005	<.02	.01	<2	.034	.008	.18	8.65	<.02	<.01	<.001	<.01	<.01	.03	11.21	<.01	.119	14.22	.11	.51	.11	.03	<.01	1.14	<2	7	2	-
RRE 267807	<.001	.006	<.02	.01	<2	.034	.008	.18	8.78	<.02	<.01	<.001	<.01	<.01	.03	10.87	<.01	.121	14.15	.11	.51	.11	.02	<.01	1.17	<2	3	7	-
267808	.001	.010	<.02	.01	<2	.101	.009	.19	10.58	<.02	<.01	<.001	<.01	<.01	.03	7.85	.02	.090	15.15	.14	1.12	.36	.22	<.01	1.14	<2	7	5	5.60
267809	<.001	.017	<.02	.01	<2	.251	.010	.19	11.44	<.02	<.01	<.001	<.01	<.01	.03	6.45	<.01	.099	17.80	.07	.25	.06	<.01	<.01	1.30	8	30	27	4.56
267810 (rock)	<.001	.007	<.02	.01	<2	.002	.001	.11	4.39	<.02	.05	<.001	<.01	<.01	.01	4.69	.06	.001	1.93	.32	8.71	2.42	1.29	<.01	<.02	<2	<2	3	2.15
267811	<.001	.009	<.02	.01	<2	.152	.009	.19	10.83	<.02	.01	<.001	<.01	<.01	.02	5.49	.02	.076	17.87	.09	.95	.30	.17	<.01	.66	2	13	13	5.58
267812	<.001	.011	<.02	.01	<2	.215	.010	.22	11.68	<.02	<.01	<.001	<.01	<.01	.02	3.42	<.01	.094	20.86	.06	.26	.05	.01	<.01	.66	<2	13	17	4.95
267813	<.001	.006	<.02	.01	<2	.119	.006	.19	9.32	<.02	.03	<.001	<.01	<.01	.03	4.27	.06	.059	13.68	.20	3.18	1.23	.66	<.01	.42	<2	6	11	5.31
267814	.005	.040	<.02	.01	<2	.222	.015	.19	14.82	<.02	<.01	<.001	<.01	<.01	.04	5.62	.01	.078	13.28	.13	.86	.10	.15	<.01	4.53	10	16	36	3.55
267815	.007	.054	<.02	.01	<2	.173	.019	.16	18.70	<.02	<.01	<.001	<.01	<.01	.04	6.72	.01	.068	12.11	.11	.78	.11	.13	<.01	7.73	11	21	30	4.78
267816	.001	.012	<.02	.01	<2	.014	.008	.18	10.72	<.02	<.01	<.001	<.01	<.01	.06	11.14	<.01	.084	12.65	.12	.53	.10	.04	<.01	2.38	<2	<2	<2	4.87
267817	.005	.027	<.02	.01	<2	.056	.012	.19	15.82	<.02	<.01	<.001	<.01	<.01	.07	7.99	<.01	.075	12.39	.10	.32	.07	.01	<.01	5.41	11	15	7	6.39
267818	.003	.012	<.02	.01	<2	.011	.008	.19	12.01	<.02	.02	<.001	<.01	<.01	.08	10.05	.03	.048	11.24	.22	1.80	.40	.44	<.01	2.63	<2	<2	<2	5.70
267819	.003	.018	<.02	.01	<2	.028	.010	.19	13.89	<.02	<.01	<.001	<.01	<.01	.08	8.61	.01	.079	11.85	.15	.80	.08	.09	<.01	3.99	6	8	6	2.01
267820A	.003	.021	<.02	<.01	<2	.027	.011	.20	13.64	<.02	<.01	<.001	<.01	<.01	.09	8.70	<.01	.074	11.94	.13	.46	.10	.04	<.01	4.57	4	6	<2	3.12
267820B	.004	.021	<.02	<.01	<2	.026	.011	.20	13.49	<.02	<.01	<.001	<.01	<.01	.09	8.81	<.01	.073	12.24	.13	.45	.10	.04	<.01	4.25	4	6	3	-
STANDARD R-2a	.049	.578	1.60	4.39	169	.385	.047	.25	25.11	.23	.16	.031	.13	<.01	.02	3.85	.08	.061	2.76	.19	2.79	.55	.67	.10	5.29	473	481	475	-

Standard is STANDARD R-2a/CSB/FA-10R.

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCl) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.  
 TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B BY FIRE ASSAY & ANALYSIS BY ICP. (30 gm)  
 - SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data 2 FA     

DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Aug 24/05





SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267821	.003	.015	<.02	.01	<2	.017	.010	.19	12.32	<.02	<.01	<.001	<.01	<.01	.08	9.72	<.01	.071	11.86	.12	.54	.11	.04	<.01	3.52	6	4	5	4.90
267822	<.001	.010	<.02	<.01	<2	.011	.008	.16	9.80	<.02	<.01	<.001	<.01	<.01	.06	11.42	<.01	.088	12.71	.10	.38	.11	.01	<.01	2.20	4	<2	2	6.45
267823	<.001	.006	<.02	.01	<2	.038	.008	.17	9.07	<.02	<.01	<.001	<.01	<.01	.03	9.82	<.01	.124	14.95	.08	.37	.09	.01	<.01	1.28	3	5	4	5.48
267824	<.001	.006	<.02	.01	<2	.028	.008	.16	8.10	<.02	<.01	<.001	<.01	<.01	.03	10.49	.02	.110	12.96	.14	1.09	.39	.17	<.01	1.10	<2	<2	<2	6.05
267825 (pulp)	<.001	.099	<.02	<.01	<2	.350	.017	.05	9.09	<.02	<.01	<.001	<.01	<.01	.01	3.57	.01	.296	14.61	.14	2.52	.24	.05	<.01	1.02	-	-	-	-
267826	<.001	.014	<.02	<.01	<2	.024	.011	.17	9.39	<.02	<.01	<.001	<.01	<.01	.03	11.10	<.01	.119	13.97	.10	.44	.12	.02	<.01	2.01	<2	<2	2	6.04
267827	<.001	.013	<.02	.01	<2	.070	.011	.18	10.02	<.02	<.01	<.001	<.01	<.01	.02	9.23	.02	.127	14.62	.13	.93	.31	.13	<.01	1.74	7	<2	<2	5.71
267828	<.001	.009	<.02	<.01	<2	.066	.011	.19	10.59	<.02	<.01	<.001	<.01	<.01	.02	6.38	.01	.142	17.34	.10	.77	.16	.13	<.01	1.09	<2	3	6	6.09
267829	<.001	.005	<.02	.01	<2	.153	.011	.20	10.64	<.02	<.01	<.001	<.01	<.01	.01	4.54	<.01	.145	20.06	.05	.25	.03	<.01	<.01	.59	2	2	4	5.98
267830	<.001	.006	<.02	.01	<2	.165	.010	.17	9.46	<.02	<.01	<.001	<.01	<.01	.01	4.11	<.01	.136	19.08	.06	.39	.03	.03	<.01	.58	<2	8	10	4.02
267831	<.001	.008	<.02	.01	<2	.155	.011	.17	9.10	<.02	<.01	<.001	<.01	<.01	.01	4.57	<.01	.203	20.16	.05	.27	.03	<.01	<.01	.64	4	3	5	5.34
267832	<.001	.009	<.02	.01	<2	.095	.010	.16	8.94	<.02	<.01	<.001	<.01	<.01	.01	7.27	<.01	.131	17.21	.07	.30	.04	<.01	<.01	.74	4	3	5	5.81
267833	<.001	.005	<.02	.01	<2	.125	.011	.18	9.40	<.02	<.01	<.001	<.01	<.01	.01	5.00	<.01	.111	20.45	.05	.21	.04	<.01	<.01	.46	2	<2	4	5.93
267834	<.001	.019	<.02	.01	<2	.075	.009	.16	7.92	<.02	.04	<.001	<.01	<.01	.02	8.23	.04	.106	13.12	.15	2.36	.13	.81	<.01	.90	<2	4	3	4.79
RE 267834	<.001	.020	<.02	.01	<2	.076	.009	.16	7.95	<.02	.04	<.001	<.01	<.01	.02	8.28	.04	.103	13.07	.15	2.36	.13	.81	<.01	.90	<2	4	5	-
RRE 267834	<.001	.020	<.02	.01	<2	.076	.009	.15	7.86	<.02	.05	<.001	<.01	<.01	.02	8.19	.04	.100	13.14	.15	2.38	.13	.83	<.01	.94	<2	9	8	-
267835	<.001	.007	<.02	.01	<2	.174	.010	.16	8.32	<.02	<.01	<.001	<.01	<.01	.01	3.80	<.01	.116	20.78	.05	.22	.03	<.01	<.01	.39	9	<2	2	4.56
267836	<.001	.005	<.02	.01	<2	.183	.011	.17	8.78	<.02	<.01	<.001	<.01	<.01	.01	3.39	<.01	.127	21.92	.04	.18	.03	<.01	<.01	.30	5	<2	2	5.57
267837	<.001	.005	<.02	.01	<2	.166	.010	.14	8.50	<.02	<.01	<.001	<.01	<.01	.01	3.03	<.01	.117	21.58	.04	.18	.02	.01	<.01	.27	3	2	<2	3.68
267838	<.001	.009	<.02	<.01	<2	.155	.011	.18	9.12	<.02	<.01	<.001	<.01	<.01	.01	4.67	.01	.113	20.89	.06	.62	.03	<.01	<.01	.43	<2	3	5	5.36
.STD RTS-2	<.001	.072	<.02	.01	2	.277	.008	.04	37.81	<.02	<.01	<.001	<.01	<.01	.01	.63	.01	.012	.40	.17	.80	.23	.13	<.01	17.84	-	-	-	-
267839	<.001	.013	<.02	.01	<2	.166	.012	.17	9.51	<.02	<.01	<.001	<.01	<.01	.01	4.35	<.01	.095	22.06	.04	.22	.04	<.01	<.01	.53	<2	3	<2	6.44
267840 (rock)	<.001	.007	<.02	.01	<2	.003	.002	.11	4.34	<.02	.05	<.001	<.01	<.01	.01	4.70	.06	.001	2.08	.32	8.55	2.41	1.28	<.01	<.02	7	2	5	2.31
267841	<.001	.013	<.02	<.01	<2	.075	.007	.14	6.82	<.02	<.01	<.001	<.01	<.01	.01	10.29	<.01	.166	15.92	.11	.56	.09	.02	<.01	.51	2	<2	3	5.72
267842	<.001	.030	<.02	.01	<2	.125	.013	.16	9.26	<.02	<.01	<.001	<.01	<.01	.01	6.88	<.01	.158	19.10	.08	.43	.06	.01	<.01	1.12	<2	58	71	6.27
267843	<.001	.050	<.02	<.01	<2	.138	.019	.16	9.95	<.02	<.01	<.001	<.01	<.01	.01	8.71	<.01	.174	16.42	.08	.40	.07	.01	<.01	2.35	2	57	80	6.04
267844	<.001	.044	<.02	.01	<2	.134	.016	.15	10.09	<.02	<.01	<.001	<.01	<.01	.01	6.08	<.01	.130	18.64	.07	.43	.04	.02	<.01	1.65	<2	78	99	5.39
267845	<.001	.042	<.02	<.01	<2	.145	.014	.16	9.35	<.02	<.01	<.001	<.01	<.01	.01	7.51	<.01	.145	18.73	.07	.41	.08	.03	<.01	1.44	3	68	87	6.47
267846	<.001	.047	<.02	.01	<2	.146	.017	.17	10.46	<.02	<.01	<.001	<.01	<.01	.01	6.66	<.01	.175	18.32	.06	.30	.05	<.01	<.01	1.98	2	56	70	5.60
267847	<.001	.032	<.02	.01	<2	.094	.013	.17	9.70	<.02	<.01	<.001	<.01	<.01	.01	7.32	.02	.145	16.89	.13	1.05	.28	.20	<.01	1.48	4	31	37	5.17
267848	<.001	.021	<.02	.01	<2	.071	.010	.16	8.24	<.02	<.01	<.001	<.01	<.01	.01	8.26	<.01	.235	17.11	.08	.43	.09	.02	<.01	.97	3	29	43	5.27
267849	<.001	.057	<.02	<.01	<2	.106	.023	.16	14.06	<.02	<.01	<.001	<.01	<.01	.02	7.77	.01	.130	14.12	.09	.65	.11	.09	<.01	5.40	5	43	47	5.28
267850 (pulp)	<.001	.101	<.02	.01	<2	.355	.017	.05	9.16	<.02	<.01	<.001	<.01	<.01	.01	3.55	<.01	.334	14.97	.15	2.69	.24	.05	<.01	1.07	-	-	-	-
267851	<.001	.056	<.02	.01	<2	.089	.022	.12	11.98	<.02	<.01	<.001	<.01	<.01	.03	13.09	<.01	.128	10.07	.10	.38	.13	.01	<.01	6.20	12	8	18	5.88
STANDARD R-2a	.048	.570	1.57	4.30	163	.385	.048	.24	24.09	.23	.15	.031	.14	<.01	.02	3.84	.08	.064	2.65	.19	2.68	.52	.65	.09	5.30	481	489	485	-

Standard is STANDARD R-2a/CSB/FA-10R. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267852	<.001	.034	<.02	.01	<2	.029	.010	.14	7.27	<.02	.02	<.001	<.01	<.01	.03	13.50	.03	.134	8.83	.21	1.79	.58	.22	<.01	2.04	<2	4	6	5.59
267853	<.001	.027	<.02	.01	<2	.037	.010	.14	7.22	<.02	<.01	<.001	<.01	<.01	.04	13.95	.01	.143	9.59	.18	.90	.28	.11	<.01	1.94	2	3	3	5.89
267854	<.001	.029	<.02	.02	<2	.046	.008	.14	6.97	<.02	.01	<.001	<.01	<.01	.04	13.60	.01	.130	9.99	.17	.94	.31	.14	<.01	1.89	5	<2	<2	5.95
267855	.001	.026	<.02	.01	<2	.039	.009	.14	6.67	<.02	.01	<.001	<.01	<.01	.03	13.53	.02	.125	9.27	.19	1.35	.52	.11	<.01	1.62	<2	<2	<2	5.46
267856	.001	.032	<.02	.01	<2	.035	.012	.14	9.16	<.02	.02	<.001	<.01	<.01	.04	11.92	.02	.107	9.63	.16	1.47	.52	.19	<.01	2.75	<2	3	2	6.26
267857	<.001	.022	<.02	.01	<2	.027	.009	.16	8.14	<.02	.03	<.001	<.01	<.01	.04	12.96	.03	.114	9.03	.22	2.09	.34	.38	<.01	1.74	<2	<2	3	5.10
.STD RTS-2	<.001	.073	<.02	.02	2	.279	.008	.04	37.28	<.02	<.01	<.001	<.01	<.01	.01	.64	.01	.011	.37	.17	.81	.22	.13	<.01	18.86	-	-	-	-
267858	<.001	.018	<.02	.01	<2	.028	.008	.14	6.60	<.02	<.01	<.001	<.01	<.01	.04	14.16	<.01	.137	10.40	.13	.63	.16	.03	<.01	1.53	2	4	4	5.60
267859	<.001	.023	<.02	.01	<2	.035	.010	.13	7.10	<.02	<.01	<.001	<.01	<.01	.05	14.34	<.01	.144	10.47	.12	.41	.14	.01	<.01	2.07	<2	3	<2	4.85
267860	.001	.026	<.02	.01	<2	.035	.012	.13	8.39	<.02	<.01	<.001	<.01	<.01	.05	14.23	<.01	.161	9.67	.11	.43	.13	.01	<.01	3.16	3	3	3	5.06
RE 267860	.001	.027	<.02	<.01	<2	.036	.012	.13	8.54	<.02	<.01	<.001	<.01	<.01	.05	14.38	<.01	.162	10.03	.11	.44	.14	.01	<.01	3.22	<2	<2	<2	-
RRE 267860	.001	.027	<.02	.01	<2	.036	.012	.13	8.53	<.02	<.01	<.001	<.01	<.01	.05	14.29	<.01	.162	10.02	.12	.44	.14	.01	<.01	3.12	2	<2	3	-
267861	.001	.023	<.02	.01	<2	.031	.010	.13	7.71	<.02	<.01	<.001	<.01	<.01	.05	13.56	<.01	.163	10.42	.11	.46	.14	.01	<.01	2.50	2	<2	<2	3.66
STANDARD R	.049	.570	1.55	4.25	162	.386	.048	.24	24.03	.25	.15	.030	.13	<.01	.02	3.91	.08	.059	2.67	.19	2.72	.52	.65	.11	5.30	480	474	481	-

Standard is STANDARD R-2a/CSB/FA-10R. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE



Hard Creek Nickel Corporation PROJECT Tur C05-79B File # A504252 Page 1

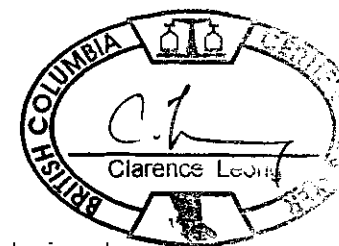
1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchins

SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267791	.021	.052	.007	1.74
267792	.027	.106	.010	1.19
267793	.012	.099	.005	.64
267794	.007	.070	.002	.80
267795	.009	.061	.003	.69
267796	.012	.076	.005	1.25
267797	.016	.066	.005	1.43
267798	.018	.019	.010	2.08
267799	.037	.024	.015	2.55
267800 (pulp)	.097	.270	.012	1.42
267801	.039	.032	.010	1.74
267802	.033	.026	.009	1.23
267803	.035	.012	.006	.77
267804	.018	.019	.009	1.13
267805	.033	.025	.012	1.86
267806	.013	.043	.009	1.17
.STD RTS-2	.061	.232	.007	4.73
267807	.009	.030	.005	.83
RE 267807	.007	.029	.005	.86
RRE 267807	.006	.028	.005	.74
267808	.011	.081	.006	1.01
267809	.018	.211	.007	1.20
267810 (rock)	.006	.001	<.001	.18
267811	.009	.112	.005	.72
267812	.011	.143	.005	.91
267813	.007	.089	.003	.47
267814	.039	.201	.014	3.15
267815	.054	.165	.018	4.06
267816	.014	.011	.006	1.02
267817	.026	.051	.011	4.10
267818	.013	.007	.005	1.28
267819	.016	.021	.008	2.29
267820A	.019	.019	.008	2.67
267820B	.019	.019	.008	2.40
STANDARD R-2a	.515	.326	.043	7.87

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
 - SAMPLE TYPE: DRILL CORE R150  
 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

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DATE RECEIVED: AUG 8 2005 DATE REPORT MAILED: Sept. 14/05





SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267821	.015	.013	.006	1.85
267822	.011	.008	.005	1.06
267823	.006	.031	.005	1.11
267824	.007	.024	.005	.81
267825 (pulp)	.095	.262	.011	1.24
267826	.015	.022	.008	1.35
267827	.014	.063	.008	1.04
267828	.010	.052	.006	.89
267829	.006	.116	.006	.84
267830	.007	.145	.007	.59
267831	.007	.132	.008	.73
267832	.010	.084	.007	.80
267833	.005	.093	.006	.83
267834	.019	.067	.006	.77
RE 267834	.020	.067	.006	.67
RRE 267834	.020	.069	.006	1.02
267835	.007	.143	.007	.64
267836	.006	.144	.006	.68
267837	.005	.136	.006	.52
267838	.009	.111	.006	.72
.STD RTS-2	.058	.226	.007	4.04
267839	.012	.112	.006	1.09
267840 (rock)	.005	.002	<.001	.16
267841	.013	.054	.004	.55
267842	.028	.104	.008	1.16
267843	.049	.130	.014	1.68
267844	.042	.124	.012	1.25
267845	.041	.126	.010	1.42
267846	.045	.134	.013	1.30
267847	.031	.085	.009	1.28
267848	.020	.060	.007	.91
267849	.055	.095	.020	2.90
267850 (pulp)	.095	.272	.012	1.31
267851	.056	.084	.020	4.91
STANDARD R-2a	.520	.328	.040	8.63

Sample type: DRILL CORE R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267852	.032	.024	.007	1.05
267853	.025	.033	.008	1.26
267854	.026	.041	.006	.93
267855	.024	.036	.007	.89
267856	.030	.030	.009	1.55
267857	.020	.021	.006	.82
267858	.016	.024	.007	.93
267859	.023	.032	.008	1.30
267860	.026	.033	.010	2.60
RE 267860	.026	.034	.010	2.79
RRE 267860	.025	.032	.010	2.29
267861	.022	.027	.008	1.97
STANDARD R-2a	.514	.342	.042	8.28

Sample type: DRILL CORE R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ASSAY CERTIFICATE



Hard Creek Nickel Corporation PROJECT Tur C05-80A File # A504486

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchins

SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267862	<.001	.007	<.02	.01	<2	.204	.012	.14	8.03	<.01	<.01	<.001	<.01	<.01	.01	1.10	.02	.072	27.62	.05	.56	<.01	.14	<.01	.34	<2	<2	<2	4.95
267863	<.001	.007	<.02	.01	<2	.176	.010	.15	7.73	<.01	<.01	<.001	<.01	<.01	.01	2.12	.03	.113	25.20	.10	1.11	<.01	.20	<.01	.28	<2	7	9	5.51
267864	<.001	.013	<.02	.01	3	.195	.011	.13	7.20	<.01	<.01	<.001	<.01	<.01	.01	1.55	.01	.102	27.36	.04	.41	<.01	.06	<.01	.39	2	2	9	4.56
267865	<.001	.049	<.02	.01	2	.238	.025	.14	9.46	<.01	<.01	<.001	<.01	<.01	.01	.88	.02	.141	29.23	.03	.35	<.01	.02	<.01	1.76	<2	17	14	5.88
267866	<.001	.042	<.02	.01	<2	.172	.027	.14	10.36	<.01	<.01	<.001	<.01	<.01	.01	.51	.02	.159	30.26	.02	.14	<.01	<.01	<.01	2.23	2	24	20	6.02
267867	<.001	.030	<.02	.01	<2	.127	.020	.14	10.14	<.01	<.01	<.001	<.01	<.01	.01	.77	.02	.227	29.68	.03	.34	<.01	<.01	<.01	1.52	5	11	10	4.45
267868	<.001	.035	<.02	.01	<2	.167	.023	.15	11.33	<.01	<.01	<.001	<.01	<.01	.01	.62	.02	.128	30.16	.02	.12	<.01	<.01	<.01	1.99	11	<2	7	5.98
267869	<.001	.034	<.02	.01	<2	.174	.024	.16	12.20	<.01	<.01	<.001	<.01	<.01	.01	.73	.02	.207	29.11	.03	.35	<.01	<.01	<.01	2.48	3	32	18	5.17
267870 (rock)	<.001	.007	<.02	<.01	<2	.001	.002	.12	4.45	<.01	.05	<.001	<.01	<.01	.01	4.66	.05	.001	1.89	.34	9.80	2.41	1.30	<.01	<.02	<2	<2	<2	2.66
267871	<.001	.047	<.02	<.01	<2	.255	.029	.15	13.30	<.01	<.01	<.001	<.01	<.01	.01	.90	.02	.202	27.39	.02	.18	<.01	.04	<.01	3.58	3	37	12	5.16
267872	<.001	.017	<.02	.01	<2	.139	.015	.17	9.77	<.01	<.01	<.001	<.01	<.01	.01	1.88	.03	.130	27.35	.07	.88	<.01	.16	<.01	1.11	3	10	16	5.75
267873	<.001	.017	<.02	.01	<2	.211	.018	.17	11.25	<.01	<.01	<.001	<.01	<.01	.01	.16	.01	.129	30.20	.02	.15	<.01	<.01	<.01	1.73	6	4	12	5.53
267874	<.001	.006	<.02	.01	2	.187	.014	.17	9.37	<.01	<.01	<.001	<.01	<.01	.01	.53	.01	.096	31.48	.02	.16	<.01	<.01	<.01	.46	<2	<2	4	6.11
.STD RTS-2	<.001	.075	<.02	.01	2	.274	.007	.04	38.82	<.01	<.01	<.001	<.01	.01	.01	.63	.01	.011	.40	.18	.85	<.01	.07	<.01	18.61	-	-	-	-
267875 (pulp)	<.001	.100	<.02	<.01	<2	.353	.016	.05	9.50	<.01	<.01	<.001	<.01	<.01	.01	3.59	.02	.204	17.14	.16	2.82	.11	<.01	<.01	1.02	-	-	-	-
267876	<.001	.007	<.02	.01	<2	.201	.013	.17	9.29	<.01	<.01	<.001	<.01	<.01	.01	.28	.01	.114	31.60	.02	.12	<.01	.01	<.01	.53	<2	<2	5	5.13
267877	<.001	.018	<.02	.01	<2	.236	.019	.17	10.38	<.01	<.01	<.001	<.01	<.01	.01	.90	.01	.087	31.55	.02	.13	<.01	<.01	<.01	1.08	<2	3	6	6.04
267878	<.001	.016	<.02	.01	<2	.224	.016	.16	9.86	<.01	<.01	<.001	<.01	<.01	.01	.52	.01	.114	31.38	.02	.12	<.01	<.01	<.01	.75	2	4	12	5.71
267879	<.001	.020	<.02	.01	<2	.273	.017	.16	9.75	<.01	<.01	<.001	<.01	<.01	.01	.45	.01	.107	30.70	.02	.12	<.01	<.01	<.01	.87	<2	12	20	5.41
267880A	<.001	.055	<.02	.01	<2	.269	.019	.16	10.64	<.01	<.01	<.001	<.01	<.01	.01	.79	.01	.129	30.24	.02	.10	<.01	.03	<.01	1.49	4	21	16	5.52
267880B	<.001	.055	<.02	.01	<2	.261	.019	.17	10.78	<.01	<.01	<.001	<.01	<.01	.01	.85	.01	.125	30.76	.02	.11	<.01	<.01	<.01	1.45	3	23	16	-
267881	<.001	.073	<.02	.01	<2	.380	.027	.17	13.63	<.01	<.01	<.001	<.01	<.01	.01	.55	.01	.196	30.29	.01	.08	<.01	<.01	<.01	2.97	6	30	24	6.04
267882	<.001	.027	<.02	.01	<2	.153	.015	.17	10.51	<.01	<.01	<.001	<.01	<.01	.01	1.01	.02	.206	27.72	.06	.88	.06	.13	<.01	1.16	4	35	45	5.11
267883	<.001	.093	<.02	.01	<2	.293	.027	.17	12.90	<.01	<.01	<.001	<.01	<.01	.01	.58	.02	.124	27.86	.04	.47	.11	.01	<.01	2.99	4	16	10	5.31
267884	<.001	.027	<.02	.01	<2	.242	.020	.17	11.07	<.01	<.01	<.001	<.01	<.01	.01	.60	.01	.178	31.60	.02	.16	.24	<.01	<.01	1.32	5	8	11	5.17
RE 267884	<.001	.027	<.02	.01	<2	.239	.019	.17	11.00	<.01	<.01	<.001	<.01	<.01	.01	.56	.01	.125	31.11	.02	.13	<.01	.06	<.01	1.29	4	13	16	-
RRE 267884	<.001	.022	<.02	.01	<2	.201	.015	.14	9.39	<.01	<.01	<.001	<.01	<.01	<.01	.53	.02	.122	26.63	.01	.10	<.01	<.01	<.01	1.20	7	3	13	-
267885	<.001	.026	<.02	.01	<2	.353	.017	.17	10.48	<.01	<.01	<.001	<.01	<.01	.01	.56	<.01	.166	30.76	.02	.16	<.01	.01	<.01	1.12	<2	4	10	5.10
267886	<.001	.025	<.02	.01	<2	.308	.017	.15	10.14	<.01	<.01	<.001	<.01	<.01	.01	.08	.01	.207	29.54	.02	.18	.07	<.01	<.01	2.03	<2	<2	6	5.60
267887	<.001	.013	<.02	.01	<2	.193	.011	.16	9.47	<.01	<.01	<.001	<.01	<.01	.01	1.12	.02	.132	27.51	.05	.82	<.01	.02	<.01	1.02	2	5	9	4.61
STANDARD R-2a	.050	.568	1.72	4.31	172	.381	.048	.26	25.50	.12	.17	.031	.14	<.01	.02	3.92	.09	.055	3.14	.20	3.00	.55	.67	.08	5.38	481	468	471	-

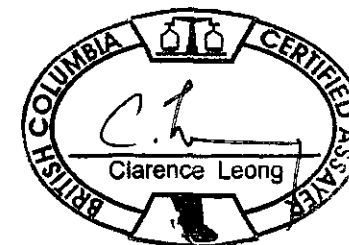
Standard is STANDARD R-2a/CSB/FA-10R.

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCl) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.  
TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B BY FIRE ASSAY & ANALYSIS BY ICP. (30 gm)

- SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data N FA

DATE RECEIVED: AUG 12 2005 DATE REPORT MAILED: Aug 30/05



ACME ANALYTICAL LABORATORIES LTD.  
(IS 001 Accredited Co.)

852 E. HASTINGS ST. VANCOUVER BC V6A 1R6  
PHONE (604) 253-5150 FAX (604) 253-1716

ASSAY CERTIFICATE

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchins



Hard Creek Nickel Corporation PROJECT Tur C05-80A File # A504486

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchins

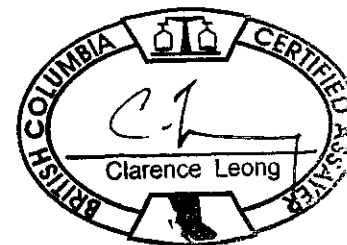
SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267862	.010	.161	.008	.97
267863	.010	.124	.006	1.25
267864	.013	.145	.007	1.32
267865	.047	.213	.020	1.58
267866	.041	.164	.022	1.69
267867	.029	.117	.016	1.39
267868	.034	.152	.018	1.69
267869	.032	.160	.018	1.89
267870 (rock)	.006	.001<	.001	.22
267871	.047	.239	.026	1.98
267872	.017	.118	.010	1.62
267873	.016	.195	.015	2.09
267874	.007	.144	.008	2.47
.STD RTS-2	.056	.236	.008	7.55
267875 (pulp)	.103	.309	.014	1.49
267876	.008	.159	.008	1.82
267877	.020	.204	.012	1.81
267878	.015	.163	.009	1.67
267879	.019	.230	.012	1.74
267880A	.047	.215	.013	1.46
267880B	.048	.209	.012	1.49
267881	.064	.322	.020	2.01
267882	.022	.121	.010	1.29
267883	.080	.242	.020	1.86
267884	.023	.168	.010	1.54
RE 267884	.025	.180	.011	1.65
RRE 267884	.024	.178	.011	1.66
267885	.024	.286	.011	1.65
267886	.023	.276	.013	1.74
267887	.012	.175	.009	1.42
STANDARD R-2a	.494	.327	.040	8.97

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
- SAMPLE TYPE: DRILL CORE R150  
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

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DATE RECEIVED: AUG 12 2005

DATE REPORT MAILED: Sept 3/05





ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-80B File # A504487 Page 1  
1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchins



SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267888	<.001	.013	<.02	.01	<2	.158	.011	.09	9.94	<.01	<.01	<.001	<.01	<.01	.01	.64	.01	.165	24.88	.02	.26	.06	.03	<.01	.98	4	7	5	5.51
267889	<.001	.022	<.02	.01	<2	.231	.017	.15	10.92	<.01	<.01	<.001	<.01	<.01	.01	1.72	.01	.179	25.40	.02	.18	.14	.02	<.01	1.26	5	8	8	4.88
267890	<.001	.007	<.02	.01	<2	.160	.010	.13	9.00	<.01	<.01	<.001	<.01	<.01	.01	1.55	.02	.156	26.04	.03	.16	.15	.01	<.01	.54	3	2	3	5.49
267891	<.001	.006	<.02	.01	<2	.167	.011	.16	8.80	<.01	<.01	<.001	<.01	<.01	.01	1.47	.01	.160	26.42	.03	.16	.29	.01	<.01	.58	2	9	7	5.56
267892	<.001	.005	<.02	.01	<2	.146	.009	.13	8.61	<.01	<.01	<.001	<.01	<.01	.01	1.48	.01	.149	25.84	.03	.16	<.01	.02	<.01	.41	5	3	<2	5.44
267893	<.001	.005	<.02	.01	<2	.157	.011	.16	8.53	<.01	<.01	<.001	<.01	<.01	.01	2.37	.02	.169	26.14	.03	.23	.07	<.01	<.01	.40	4	6	<2	5.57
267894	<.001	.007	<.02	.01	<2	.154	.010	.16	8.84	<.01	<.01	<.001	<.01	<.01	.01	2.82	.01	.168	25.45	.03	.18	<.01	.01	<.01	.50	3	2	4	5.58
267895	<.001	.007	<.02	.01	<2	.139	.010	.16	8.23	<.01	<.01	<.001	<.01	<.01	.01	4.12	.01	.155	23.66	.04	.23	.22	.08	<.01	.50	4	<2	<2	5.35
267896	<.001	.005	<.02	.01	<2	.161	.011	.16	9.03	<.01	<.01	<.001	<.01	<.01	.01	1.88	.01	.155	26.81	.03	.11	.14	<.01	<.01	.39	3	3	<2	5.96
RE 267896	<.001	.005	<.02	.01	<2	.157	.011	.16	8.96	<.01	<.01	<.001	<.01	<.01	.01	1.87	.01	.150	26.53	.03	.15	<.01	.02	<.01	.42	4	6	8	-
RRE 267896	<.001	.005	<.02	.01	<2	.160	.011	.17	9.15	<.01	<.01	<.001	<.01	<.01	.01	1.93	.02	.150	27.28	.02	.14	.14	<.01	<.01	.41	6	10	16	-
267897	<.001	.009	<.02	<.01	<2	.114	.009	.13	6.91	<.01	<.01	<.001	<.01	<.01	.02	6.88	.01	.157	19.62	.07	.43	.15	.05	<.01	.62	<2	6	6	5.52
267898	<.001	.008	<.02	.01	<2	.105	.008	.14	7.29	<.01	<.01	<.001	<.01	<.01	.02	6.34	.01	.164	19.96	.06	.31	<.01	.03	<.01	.47	2	<2	5	4.78
267899	<.001	.022	<.02	.01	<2	.155	.011	.14	7.92	<.01	<.01	<.001	<.01	<.01	.02	5.43	<.01	.136	18.86	.07	.32	<.01	.05	<.01	1.11	5	6	15	5.52
267900 (pulp)	<.001	.101	<.02	<.01	<2	.359	.016	.05	9.46	<.01	<.01	<.001	<.01	<.01	.01	3.38	.01	.350	16.08	.15	2.77	.15	.05	<.01	1.16	49	240	400	-
267901	<.001	.016	<.02	<.01	<2	.170	.011	.16	8.58	<.01	<.01	<.001	<.01	<.01	.02	3.51	.01	.119	21.52	.06	.25	<.01	.06	<.01	1.03	4	5	<2	5.65
267902	<.001	.007	<.02	.01	<2	.204	.011	.16	8.88	<.01	<.01	<.001	<.01	<.01	.01	1.17	.01	.124	26.59	.03	.15	.07	<.01	<.01	.42	2	8	7	5.18
267903	<.001	.005	<.02	.01	<2	.166	.010	.15	8.91	<.01	<.01	<.001	<.01	<.01	.01	.98	<.01	.210	25.66	.03	.16	.22	.03	<.01	.33	5	6	10	5.54
.STD RTS-2	<.001	.073	<.02	.01	<2	.271	.006	.04	38.93	<.01	<.01	<.001	<.01	<.01	.01	.56	.01	.011	.38	.17	.82	.21	.14	<.01	18.62	-	-	-	-
267904	<.001	.007	<.02	.01	<2	.170	.011	.16	8.47	<.01	<.01	<.001	<.01	<.01	.01	2.28	.02	.125	24.25	.07	.64	.03	.04	<.01	.35	2	6	9	5.56
267905	<.001	.008	<.02	.01	<2	.162	.011	.15	8.38	<.01	<.01	<.001	<.01	<.01	.01	1.93	.01	.190	24.59	.04	.18	<.01	<.01	<.01	.54	4	8	5	5.98
267906	<.001	.023	<.02	.01	<2	.174	.014	.14	10.00	<.01	<.01	<.001	<.01	<.01	.01	1.44	<.01	.210	22.64	.05	.30	<.01	.07	<.01	1.44	2	8	10	4.24
267907	<.001	.029	<.02	.01	<2	.111	.015	.18	10.53	<.01	.04	<.001	<.01	<.01	.02	5.21	.04	.113	13.82	.18	2.79	.66	.55	<.01	2.22	3	8	8	4.93
267908	<.001	.066	<.02	.01	<2	.043	.010	.20	10.99	<.01	<.01	<.001	<.01	<.01	.02	4.86	<.01	.129	14.98	.09	.75	.36	.26	<.01	3.65	4	3	10	3.72
267909	.001	.063	<.02	.01	<2	.079	.011	.20	12.57	<.01	.01	<.001	<.01	<.01	.04	6.67	.01	.113	13.90	.11	.87	.22	.25	<.01	4.58	4	6	9	5.53
267910A	.001	.075	<.02	.01	<2	.115	.016	.19	15.11	<.01	<.01	<.001	<.01	<.01	.04	6.44	<.01	.115	13.36	.11	.51	.29	.03	<.01	6.48	5	8	16	5.88
267910B	.001	.074	<.02	.01	<2	.121	.018	.19	15.64	<.01	<.01	<.001	<.01	<.01	.04	6.30	<.01	.118	13.45	.10	.47	<.01	.15	<.01	6.60	8	3	14	-
267911	<.001	.021	<.02	.01	3	.074	.010	.19	10.70	<.01	<.01	<.001	<.01	<.01	.03	4.36	.01	.165	17.56	.10	.44	.14	.06	<.01	2.78	6	<2	6	5.17
267912	<.001	.030	<.02	.01	<2	.055	.013	.19	11.36	<.01	<.01	<.001	<.01	<.01	.03	4.41	<.01	.164	17.78	.12	.57	.22	.05	<.01	2.98	7	3	2	6.24
267913	<.001	.026	<.02	.01	<2	.052	.010	.19	9.56	<.01	<.01	<.001	<.01	<.01	.03	5.02	<.01	.165	17.06	.13	.61	.22	.03	<.01	2.45	3	<2	2	5.52
267914	<.001	.037	<.02	.01	4	.083	.013	.17	9.17	<.01	<.01	<.001	<.01	<.01	.02	4.08	<.01	.170	17.43	.16	.88	.14	.27	<.01	2.72	8	4	<2	4.05
267915	<.001	.017	<.02	.01	<2	.106	.010	.14	8.07	<.01	<.01	<.001	<.01	<.01	.01	1.59	<.01	.133	22.07	.23	1.24	<.01	.71	<.01	1.35	3	<2	4	5.77
267916	<.001	.016	<.02	.01	<2	.113	.010	.15	8.58	<.01	.02	<.001	<.01	<.01	.01	5.45	.01	.157	19.36	.11	.72	.07	.03	<.01	1.33	<2	<2	4	3.18
267917	<.001	.053	<.02	.01	<2	.182	.016	.14	9.91	<.01	<.01	<.001	<.01	.01	.01	4.91	<.01	.165	19.09	.09	.54	.14	.07	<.01	2.46	<2	15	16	5.43
STANDARD R-2a	.048	.574	1.64	4.13	169	.382	.045	.24	25.10	.22	.16	.030	.14	<.01	.02	3.62	.09	.067	2.63	.19	2.90	.58	.71	.08	5.37	486	481	478	-

Standard is STANDARD R-2a/CSB/FA-10R.

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCL) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.

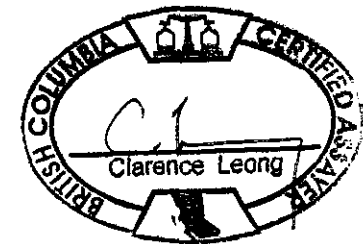
TOTAL S GROUP 2A BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B BY FIRE ASSAY & ANALYSIS BY ICP. (30 gm)

- SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

DATE RECEIVED: AUG 12 2005

DATE REPORT MAILED: Aug 29/05





SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267918	<.001	.006	<.02	.01	<2	.192	.012	.12	7.50	<.01	<.01	<.001	<.01	<.01	.01	1.22	.02	.158	25.27	.03	.31	<.01	<.01	<.01	.38	5	17	19	3.72
267919	<.001	.006	<.02	.01	<2	.217	.012	.13	7.39	<.01	<.01	<.001	<.01	.01	<.01	.50	<.01	.190	28.57	.02	.19	.24	<.01	<.01	.21	<2	16	23	4.03
267920	<.001	.006	<.02	.01	<2	.205	.012	.13	6.98	<.01	<.01	<.001	<.01	.01	<.01	.87	.01	.197	26.86	.03	.21	.16	.05	<.01	.15	4	11	13	4.82
267921	<.001	.004	<.02	.01	<2	.226	.012	.13	7.08	<.01	<.01	<.001	<.01	<.01	<.01	.73	.01	.197	27.26	.05	.51	.06	<.01	<.01	.21	3	5	11	4.73
267922	<.001	.007	<.02	.01	<2	.147	.008	.15	7.87	<.01	.04	<.001	<.01	<.01	.01	5.01	.06	.094	19.16	.21	2.64	.13	.61	<.01	.16	5	9	3	5.06
267923	<.001	.004	<.02	.01	<2	.241	.012	.14	7.34	<.01	<.01	<.001	<.01	<.01	.01	1.06	.01	.173	27.42	.03	.14	.13	.05	<.01	.15	<2	11	10	5.82
267924	<.001	.004	<.02	.01	<2	.229	.011	.12	7.29	<.01	<.01	<.001	<.01	.01	.01	1.14	.01	.151	26.37	.04	.34	.41	<.01	<.01	.19	<2	8	12	4.49
RE 267924	<.001	.004	<.02	<.01	<2	.236	.011	.13	7.50	<.01	<.01	<.001	<.01	.01	.01	1.15	.01	.155	27.22	.04	.37	.34	.01	<.01	.19	2	11	15	-
RRE 267924	<.001	.004	<.02	<.01	<2	.230	.011	.12	7.27	<.01	<.01	<.001	<.01	.01	.01	1.14	.01	.148	26.26	.04	.35	.41	.01	<.01	.19	<2	7	7	-
267925 (pulp)	<.001	.058	<.02	.01	<2	.233	.010	.11	8.87	<.01	<.01	<.001	<.01	<.01	.02	4.47	.01	.806	14.32	.19	3.82	.41	.11	<.01	.52	-	-	-	-
267926	<.001	.006	<.02	<.01	<2	.127	.007	.13	7.24	<.01	.03	<.001	<.01	<.01	.02	4.20	.08	.070	16.78	.30	3.22	1.19	.45	<.01	.11	2	3	5	5.24
267927	<.001	.005	<.02	.01	<2	.232	.011	.13	7.15	<.01	<.01	<.001	<.01	<.01	<.01	.83	.01	.147	27.19	.03	.33	.48	.04	<.01	.21	3	5	11	5.11
267928	<.001	.005	<.02	.01	<2	.256	.011	.10	6.42	<.01	<.01	<.001	<.01	<.01	<.01	1.27	.01	.148	25.69	.04	.52	.19	.04	<.01	.27	<2	34	44	5.13
267929	<.001	.020	<.02	.01	<2	.033	.005	.17	9.05	<.01	.07	<.001	<.01	<.01	.03	8.63	.13	.036	7.85	.55	7.16	1.11	1.66	<.01	.10	<2	3	6	5.09
267930 (rock)	<.001	.010	<.02	.01	<2	.003	.002	.12	4.52	<.01	.05	<.001	<.01	<.01	.01	4.54	.06	.002	2.06	.34	9.13	2.47	1.24	<.01	<.02	2	7	6	2.13
267931	<.001	.004	<.02	.01	<2	.214	.011	.13	6.98	<.01	.01	<.001	<.01	.01	.01	1.68	.03	.159	25.05	.09	1.11	.46	.25	<.01	.16	4	14	20	5.10
267932	<.001	.006	<.02	<.01	<2	.239	.011	.12	7.21	<.01	<.01	<.001	<.01	.01	<.01	.77	.01	.141	27.13	.02	.18	.33	<.01	<.01	.24	3	3	8	4.53
267933	<.001	.022	<.02	<.01	<2	.141	.007	.11	7.27	<.01	.03	.001	<.01	<.01	.01	6.26	.05	.112	17.41	.20	2.65	.47	.74	<.01	.23	7	54	71	5.54
.STD RTS-2	<.001	.076	<.02	.01	<2	.278	.007	.04	39.32	<.01	<.01	<.001	<.01	<.01	.01	.64	.01	.012	.42	.18	.82	.57	.14	<.01	18.40	-	-	-	-
267934	<.001	.006	<.02	<.01	<2	.232	.013	.14	7.84	<.01	<.01	<.001	<.01	<.01	<.01	1.01	<.01	.138	28.65	.03	.20	.10	<.01	<.01	.17	3	14	24	5.66
267935	<.001	.030	<.02	<.01	3	.288	.013	.13	7.40	<.01	<.01	<.001	<.01	.01	<.01	1.13	<.01	.122	28.44	.03	.15	.32	.02	<.01	.32	10	74	77	5.41
267936	<.001	.053	<.02	<.01	<2	.189	.011	.13	7.41	<.01	<.01	<.001	<.01	<.01	.01	4.64	.01	.097	22.71	.07	.38	.39	.04	<.01	.57	11	30	42	4.83
267937	<.001	.041	<.02	.01	<2	.198	.017	.15	9.39	<.01	<.01	<.001	<.01	.01	<.01	1.26	.01	.155	26.13	.03	.17	.17	.02	<.01	1.15	9	7	11	5.25
267938	<.001	.025	<.02	<.01	<2	.148	.012	.13	8.12	<.01	<.01	<.001	<.01	<.01	.01	6.13	.01	.127	20.63	.07	.37	.39	<.01	<.01	1.02	<2	8	16	5.49
267939	.003	.016	<.02	.01	3	.149	.011	.18	11.26	<.01	<.01	<.001	<.01	<.01	.04	3.75	.03	.128	17.39	.08	.42	.20	.05	<.01	2.85	6	4	19	4.34
267940A	<.001	.004	<.02	.01	<2	.196	.009	.14	8.15	<.01	<.01	<.001	<.01	<.01	.02	2.90	.01	.118	23.45	.06	.33	.39	.01	<.01	.50	2	7	9	5.97
267940B	<.001	.004	<.02	.01	<2	.194	.010	.15	8.18	<.01	<.01	<.001	<.01	<.01	.02	2.98	.01	.116	23.54	.06	.29	.31	.03	<.01	.47	3	<2	6	-
267941	<.001	.012	<.02	.01	<2	.151	.008	.17	7.82	<.01	.02	<.001	<.01	<.01	.02	3.50	.04	.098	16.55	.20	2.42	.60	.79	<.01	.79	<2	10	16	4.45
267942	.008	.056	<.02	.02	<2	.302	.022	.19	15.98	<.01	<.01	<.001	<.01	.01	.04	2.40	.06	.149	15.92	.09	.59	.17	.05	<.01	6.59	14	14	46	3.08
267943	<.001	.056	<.02	.01	<2	.421	.014	.13	7.81	<.01	<.01	<.001	<.01	<.01	.01	2.05	.01	.173	23.37	.10	.64	<.01	.21	<.01	1.29	11	65	79	5.82
267944	.002	.046	<.02	.01	<2	.308	.015	.16	9.53	<.01	.02	<.001	<.01	<.01	.02	4.14	.04	.167	16.38	.16	2.11	.71	.33	<.01	2.37	5	68	96	4.67
267945	<.001	.007	<.02	.01	<2	.180	.010	.13	7.24	<.01	<.01	<.001	<.01	<.01	.01	2.50	.01	.109	21.41	.14	1.07	.22	.22	<.01	.51	<2	9	10	3.78
267946	<.001	.029	<.02	.01	<2	.334	.013	.13	7.16	<.01	.01	<.001	<.01	<.01	.01	2.08	.02	.145	21.32	.12	1.58	.30	.59	<.01	.67	2	42	44	4.56
267947	<.001	.015	<.02	<.01	4	.234	.009	.14	7.20	<.01	.05	<.001	<.01	<.01	.02	3.43	.06	.123	17.89	.22	3.00	.37	1.25	<.01	.48	<2	22	23	3.73
STANDARD R-2a	.048	.570	1.64	4.16	168	.385	.044	.24	25.22	.21	.15	.030	.13	<.01	.02	3.68	.08	.063	2.66	.19	2.87	.68	.70	.08	5.30	489	486	480	-

Standard is STANDARD R-2a/CSB/FA-10R. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



ACME ANALYTICAL



ACME ANALYTICAL

SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267948	<.001	.011	<.02	.01	<2	.312	.013	.10	6.24	<.02	<.01	<.001	<.01	<.01	<.01	.53	<.01	.157	25.50	.05	.59	.03	.17	<.01	.32	4	23	33	4.78
267949	<.001	.031	<.02	.01	<2	.548	.017	.10	6.91	<.02	<.01	<.001	<.01	<.01	<.01	.57	<.01	.143	26.52	.05	.55	.02	.19	<.01	.75	7	93	107	5.79
267950 (pulp)	<.001	.058	<.02	.01	<2	.242	.012	.11	9.14	<.02	<.01	<.001	<.01	<.01	.02	4.52	<.01	.878	13.93	.20	4.18	.35	.12	<.01	.53	38	110	428	-
STANDARD R-2a/CSB	.051	.576	1.64	4.34	168	.389	.047	.25	25.42	.23	.15	.031	.14	<.01	.02	3.72	.09	.061	2.76	.20	3.00	.54	.67	.10	5.31	-	-	-	-

Sample type: DRILL CORE R150.

ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-80B File # A504487 Page 1  
1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens



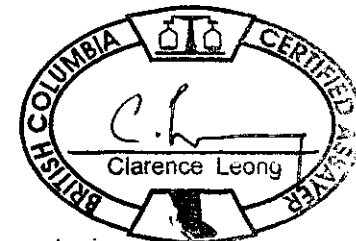
SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267888	.016	.145	.010	.88
267889	.023	.206	.016	1.22
267890	.008	.129	.007	.79
267891	.009	.131	.008	1.02
267892	.006	.114	.007	.88
267893	.006	.113	.006	1.04
267894	.008	.115	.007	1.26
267895	.008	.104	.007	1.14
267896	.007	.105	.006	1.36
RE 267896	.006	.104	.006	1.22
RRE 267896	.006	.104	.006	1.16
267897	.010	.095	.007	.85
267898	.009	.089	.006	.91
267899	.021	.140	.010	.99
267900 (pulp)	.094	.267	.012	1.31
267901	.016	.141	.008	1.09
267902	.008	.154	.008	1.20
267903	.006	.128	.007	.88
.STD RTS-2	.060	.224	.007	4.31
267904	.005	.124	.007	.88
267905	.008	.129	.008	.94
267906	.024	.157	.012	1.50
267907	.029	.102	.013	1.36
267908	.064	.037	.010	2.59
267909	.060	.068	.010	3.11
267910A	.075	.101	.017	4.40
267910B	.074	.106	.018	4.48
267911	.022	.064	.010	1.77
267912	.030	.047	.012	1.94
267913	.025	.045	.009	1.78
267914	.036	.074	.012	2.13
267915	.016	.091	.008	.85
267916	.016	.105	.009	1.07
267917	.052	.189	.017	2.02
STANDARD R-2a	.522	.331	.041	8.21

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
- SAMPLE TYPE: DRILL CORE R150  
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data h FA \_\_\_\_\_

DATE RECEIVED: AUG 12 2005

DATE REPORT MAILED: Sept 14/05





SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267918	.006	.141	.011	.97
267919	.005	.132	.009	.90
267920	.005	.126	.008	.80
267921	.003	.143	.009	.81
267922	.006	.118	.006	.44
267923	.003	.143	.007	.63
267924	.004	.153	.008	.65
RE 267924	.003	.151	.008	.63
RRE 267924	.003	.151	.008	.66
267925 (pulp)	.057	.195	.008	.55
267926	.006	.098	.005	.41
267927	.004	.163	.009	.66
267928	.005	.207	.010	.75
267929	.019	.029	.002	.34
267930 (rock)	.007	.002	<.001	.19
267931	.004	.134	.008	.84
267932	.005	.167	.009	.76
267933	.019	.124	.008	.48
.STD RTS-2	.058	.227	.007	3.96
267934	.006	.141	.008	.68
267935	.029	.181	.009	1.07
267936	.050	.141	.009	1.14
267937	.039	.177	.014	1.22
267938	.024	.127	.011	.80
267939	.016	.129	.011	1.52
267940A	.004	.143	.007	.71
267940B	.004	.142	.007	.73
267941	.011	.130	.006	.66
267942	.052	.278	.023	3.45
267943	.054	.380	.014	1.04
267944	.045	.286	.014	1.31
267945	.007	.143	.008	.51
267946	.028	.295	.012	.85
267947	.013	.185	.007	.57
STANDARD R-2a	.517	.324	.043	7.79

Sample type: DRILL CORE R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267948	.009	.230	.008	.86
267949	.029	.440	.011	1.32
267950 (pulp)	.056	.193	.008	.57
STANDARD R-2a	.520	.332	.044	8.25

Sample type: DRILL CORE R150.

ASSAY CERTIFICATE



Hard Creek Nickel Corporation PROJECT Tur C05-80C File # A504635

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens

SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag gm/mt	Ni %	Co %	Mn %	Fe %	As %	Sr %	Cd %	Sb %	Bi %	V %	Ca %	P %	Cr %	Mg %	Ti %	Al %	Na %	K %	W %	TOT/S %	Au** ppb	Pt** ppb	Pd** ppb	Sample kg
267951	<.001	.014	<.02	.01	<2	.244	.013	.10	6.89	<.02	<.01	<.001	<.01	<.01	<.01	.82	<.01	.150	23.57	.08	.68	.04	.27	<.01	.41	3	<2	8	4.59
267952	<.001	.035	<.02	.01	<2	.389	.014	.11	7.01	<.02	<.01	<.001	<.01	<.01	.01	1.31	<.01	.113	19.01	.09	.95	.13	.25	<.01	1.03	2	20	34	5.20
267953	.001	.021	<.02	.01	<2	.195	.010	.12	6.82	<.02	<.01	<.001	<.01	<.01	.01	1.41	.01	.104	17.45	.12	1.18	.20	.36	<.01	.88	<2	<2	9	4.53
267954	.001	.021	<.02	.02	<2	.154	.010	.18	7.87	<.02	<.01	<.001	<.01	<.01	.03	2.42	.02	.128	16.45	.11	.62	.10	.08	<.01	1.67	2	5	6	5.74
267955	.002	.023	<.02	.01	<2	.162	.010	.17	9.97	<.02	<.01	<.001	<.01	<.01	.03	1.99	.02	.119	16.35	.12	.74	.10	.09	<.01	2.26	6	3	19	5.23
267956	.002	.013	<.02	.02	<2	.111	.008	.20	9.06	<.02	.02	<.001	<.01	<.01	.03	3.15	.04	.130	13.72	.21	2.26	.33	.94	<.01	1.50	4	<2	10	4.65
267957	.001	.013	<.02	.02	<2	.140	.010	.18	8.45	<.02	<.01	<.001	<.01	<.01	.02	1.78	<.01	.134	16.56	.10	.64	.09	.09	<.01	1.92	6	<2	5	3.66
267958	<.001	.007	<.02	.01	<2	.196	.010	.12	6.37	<.02	<.01	<.001	<.01	.01	.01	1.27	<.01	.105	19.20	.09	.79	.06	.16	<.01	.54	4	<2	8	4.37
.STD RTS-2	<.001	.073	<.02	.01	<2	.272	.007	.04	39.21	<.02	<.01	.002	<.01	.01	.01	.57	.01	.011	.35	.17	.83	.21	.13	<.01	18.62	-	-	-	-
267959	.001	.014	<.02	.01	<2	.205	.012	.12	7.51	<.02	<.01	<.001	<.01	<.01	.01	1.01	<.01	.126	18.58	.08	.68	.06	.12	<.01	1.51	<2	14	15	4.34
RE 267959	.001	.014	<.02	.01	<2	.205	.012	.12	7.41	<.02	<.01	<.001	<.01	<.01	.01	1.01	.01	.127	18.48	.08	.68	.06	.11	<.01	1.50	2	4	18	-
267960 (rock)	.001	.008	<.02	<.01	<2	.004	.001	.10	4.51	<.02	.05	<.001	<.01	<.01	.01	4.30	.05	.003	1.91	.33	8.93	2.35	1.26	<.01	.02	<2	<2	<2	1.95
267961	<.001	.007	<.02	.01	<2	.182	.009	.11	6.79	<.02	<.01	<.001	<.01	<.01	.01	2.11	.03	.090	17.16	.22	1.99	.31	.72	<.01	.33	<2	14	10	5.38
267962	.002	.021	<.02	.01	<2	.173	.011	.16	8.34	<.02	<.01	<.001	<.01	<.01	.02	.69	.02	.145	16.76	.07	.55	.10	.12	<.01	2.22	5	3	17	5.17
267963	.003	.032	<.02	.01	<2	.199	.015	.16	10.83	<.02	<.01	<.001	<.01	<.01	.02	.67	<.01	.146	15.66	.07	.48	.13	.09	<.01	3.60	12	4	18	5.19
267964	<.001	.004	<.02	.02	<2	.200	.009	.11	5.63	<.02	<.01	<.001	<.01	<.01	.01	.67	<.01	.089	18.75	.10	.76	.04	.15	<.01	.30	3	2	<2	4.40
267965	<.001	.003	<.02	.01	<2	.193	.009	.09	5.16	<.02	<.01	<.001	<.01	<.01	.01	.72	<.01	.075	17.87	.09	.90	.05	.19	<.01	.24	2	<2	4	4.72
267966	<.001	.009	<.02	.01	<2	.235	.012	.11	6.05	<.02	<.01	<.001	<.01	<.01	.01	.92	<.01	.081	19.32	.07	.62	.06	.06	<.01	.52	<2	11	18	2.84
STANDARD R-2a	.046	.589	1.51	4.00	159	.386	.047	.24	25.74	.23	.14	.030	.12	<.01	.02	3.50	.08	.056	2.54	.19	2.80	.51	.64	.06	5.36	488	472	490	-

Standard is STANDARD R-2a/CSB/FA-10R.

GROUP 7TD - 0.500 GM SAMPLE, 4 ACID (HF-HClO4-HNO3-HCl) DIGESTION TO 100 ML, ANALYSIS BY ICP-ES.

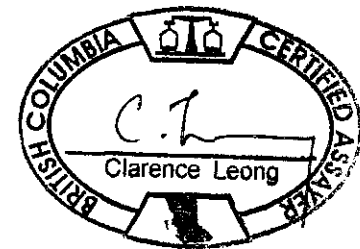
TOTAL S BY LECO. AU\*\* PT\*\* PD\*\* GROUP 3B - 30 GM SAMPLE BY FIRE ASSAY & ANALYSIS BY ICP-ES.

- SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data d FA \_\_\_\_\_

DATE RECEIVED: AUG 16 2005

DATE REPORT MAILED: Sept. 6/05



ASSAY CERTIFICATE

Hard Creek Nickel Corporation PROJECT Tur C05-80C File # A504635

1060 - 1090 W. Georgia St, Vancouver BC V6E 3V7 Submitted by: Tony Hitchens

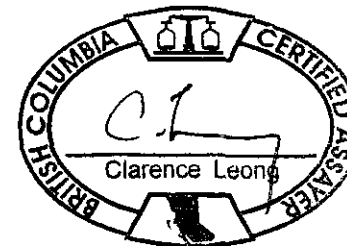


SAMPLE#	Cu* %	Ni* %	Co* %	Fe* %
267951	.014	.171	.007	.91
267952	.034	.336	.012	.88
267953	.021	.156	.008	.66
267954	.021	.119	.008	1.00
267955	.023	.129	.009	1.54
267956	.013	.088	.006	.88
267957	.013	.110	.008	1.56
267958	.007	.142	.006	.54
.STD RTS-2	.061	.226	.007	4.86
267959	.013	.166	.009	1.04
RE 267959	.013	.167	.009	1.04
267960 (rock)	.006	.003	<.001	.17
267961	.007	.140	.006	.41
267962	.019	.140	.009	1.32
267963	.031	.175	.013	2.69
267964	.003	.152	.007	.55
267965	.002	.151	.007	.39
267966	.008	.194	.009	.57
STANDARD R-2a	.520	.324	.040	8.66

CU\* NI\* CO\* & FE\* - LEACHED WITH H2O2 + NH4 CITRATE.  
- SAMPLE TYPE: DRILL CORE R150  
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data *h* FA \_\_\_\_\_

DATE RECEIVED: AUG 16 2005 DATE REPORT MAILED: *Sept 6/05*





**Appendix D**

**Statement of Costs**

HOLE	DEPTH	DJ DRILLING		ACME LABORATORY		BANDSTRA TRUCK		PACIFIC WESTERN		COMMENTS
		INVOICE	AMOUNT	INVOICE	AMOUNT	INVOICE	AMOUNT	INVOICE	AMOUNT	
		151	50,926.97							camp construction, road work, haul fuel, room and board, first aid attendant
O5-72	186.25m	157	21,151.50	A503749	3,619.30	S075767	759.9	31270	799.7	
				A503750	2,898.50			31352	342.4	
O5-73	152.4m	157	16,516.75	A503751	2,263.29			32359	799.7	
				A504243	2,716.86					
O5-74	223.75m	157, 161	25,135.50	A504242	2,454.71			32369	801.64	
				A504241	5,269.86			32371	801.64	
		157	22,017.36							room and board, core boxes, core splitter, first aid
O5-75	217.65m	161	26,398.00	A504244	2,195.32					
				A504245	2,160.61	S076469	2,145.39	32373	801.64	
				A504246	2,166.54					
O5-76	223.70m	161	24,835.25	A504247	1,274.44			32375	801.64	
				A504130	3,034.20			32380	801.64	
				A504131	2,604.60	S076285	968.96			
O5-77	223.70m	161	23,784.50	A504132	878.41			32383	801.64	
				A504133	3,791.73			32385	801.64	
				A504248	2,720.73					
O5-78	147.50m	161	16,020.75	A504249	1,387.42			32388	801.64	
				A504250	1,700.06			32392	801.64	
O5-79	211.20m	161	22,948.25	A504251	2,547.61			32393	801.64	
				A504252	4,204.13					
O5-80	199.35m	161	21,042.75	A504486	1,576.04					
				A504487	3,779.19	S076794	920.41	32400	801.64	
				A504635	931.30			32404	801.64	
	1785.5m	161	49,551.32							site and road pre., core splitter, room and board, first aid
	<b>Sub total</b>		<b>320,328.90</b>		<b>56,174.85</b>		<b>4,794.66</b>		<b>11,561.48</b>	
	Maxibor survey tool rental		#4764		8,004.30					
	Survey drill collars		25% of 05-0803		2,242.99					
	Salary of two geologists, supervision and logging				22,500.00					
	<b>Total expenditure; 15 May, 2005 to 1 Sept, 2005.</b>				<b>425,607.18</b>					

**APPENDIX E**  
**STATEMENT OF QUALIFICATIONS**  
**ANTHONY HITCHINS**

I, Anthony Hitchins, with address at 1648 Mayneview Terrace, North Saanich, B.C., certify the following :

1. I graduated with a B.A.Sc. degree in engineering geology from the University of Toronto in 1970 and a M.Sc. in geology, also from the University of Toronto, in 1973.
2. From 1970 until 1994 I worked in mineral exploration in Nova Scotia, Ontario, British Columbia, and Yukon for the Amax-Canamax group of companies in positions of increasing responsibility from field geologist to project manager. Exploration environments included Archean greenstone belts (gold and base metals), Paleozoic sedimentary belts (shale and carbonate hosted Pb-Zn-Ag), and Mesozoic intrusive and skarn environments (Au, Mo, W, Pb-Zn-Ag, and Cu-Fe).
3. Between 1994 and 1998, I was district exploration manager for Cyprus Gold in Western Australia and responsible for supervising both joint venture and Cyprus funded gold exploration projects.
4. From 1998 to the present I have worked as project manager for junior exploration companies in Nevada and British Columbia.
5. During 2003 - 2005, I was project manager for the exploration program on the Turnagain property and logged some of the drill core.

## **STATEMENT OF QUALIFICATIONS**

### **CHRIS BALDYS**

I, CHRISTOPHER BALDYS, P.Eng. do hereby certify that :

1. I am a Consulting Geologist with residence and business address at 23035 Cliff Avenue, Maple Ridge, British Columbia.
2. I graduated in 1980 with a degree in mining geology from the University of Mining and Metallurgy in Cracow, Poland
3. I have practiced my profession in Poland between 1980 and 1983 and in mineral exploration and mining in Canada since 1984.
4. I have been registered with the Association of Professional Engineers and Geoscientists of British Columbia since 1990.
5. I am responsible for the preparation of drill logs and geological interpretation for the purpose of this Assessment Report.

## Statement of Qualifications

I, Bruce Northcote of 21727 Ridgeway Crescent, Maple Ridge, BC, hereby certify that:

1. I am a consulting geologist, presently contracted by Hard Creek Nickel Corporation for geological services
2. I have worked in my profession as a geologist since 1996
3. I have been registered as a Geoscientist in Training with the Association of Professional Engineers and Geoscientists since 1997
4. I hold a B.Sc. (hons) in Geological Sciences from the University of British Columbia, awarded in 1991.
5. I hold a M.Sc. in Geology from Queen's University, awarded in 1997
6. This report is based on my examination of data collected in 2005 while employed as a consulting geologist for Hard Creek Nickel and observing and/or performing a portion of the work reported herein.

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Bruce Northcote

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Date