ASSESSMENT REPORT

on

GEOLOGY
SOIL & ROCK GEOCHEMISTRY
VLF-EM SURVEYING



# EDDY PROPERTY

Weaver Creek area, SE B.C.

UTM 569000E 5473000N

TRIM 82F.040, 82F.050 & 82G.041

For

RUBY RED RESOURCES INC.
Suite 207, 239 12th Ave. SW
Calgary, Alberta
T2R 1H6



By
Peter Klewchuk, P. Geo.
February, 2005

TABLE OF CONTENTS



LIST OF ILLUSTRATIONS

# 1.00 INTRODUCTION

## 1.10 Location and Access

The Eddy property is located in southeastern British Columbia, approximately 25 kilometers southwest of Cranbrook, centered at UTM coords. 569000E, 5473000N on Weaver Creek, a major east-flowing tributary of the Moyie River (Figs. 1 & 2).

The eastern portion of the claims is accessed by road south of Cranbrook, using the Lumberton and Moyie Forest Service Roads and tributary roads in Noke, Weaver, North Moyie and Ryder Creeks. The Western portion of the claims is in Galway Creek and is accessed by the Perry Creek forest road system.

## 1.20 Property

The Eddy property includes 143 claim units in one 20 unit 4-post claim and 120 2-post claims (Fig. 2). Many of the claims have duplicate names:

| Claim name and No. | | Tenure numbers | | |
|---|---|---|---|---|
| Eddy | | 387078 | | |
| Eddy1-6 inclusive | | 387079-84 inclusive | | |
| Eddy 7, 8 | | 387776, 77 | | |
| Eddy 9-12 | " | 387833-36 | " | |
| Eddy 13, 14 | | 387778, 79 | | |
| Eddy 15 | | 393225 | | 20 units |
| Eddy 15-18 | " | 395123-26 inclusive | | |
| Eddy 20-26 | " | 395271-77 | " | |
| Eddy 16-43 | " | 395294-321 | " | |
| Eddy 27-31 | " | 395322-26 | " | |
| Eddy 44 | | 395344 | | |
| Eddy 32-41 | " | 395754-63 | " | |
| Eddy 42-63 | " | 396088-109 | " | |
| Nelly 1-4 | " | 387670-73 | " | |
| L3772A | | 210255 | | |
| L3773 | | 210256 | | |
| L3774 | | 210257 | | |
| EDD 1-22 | | 412493-512 | " | |

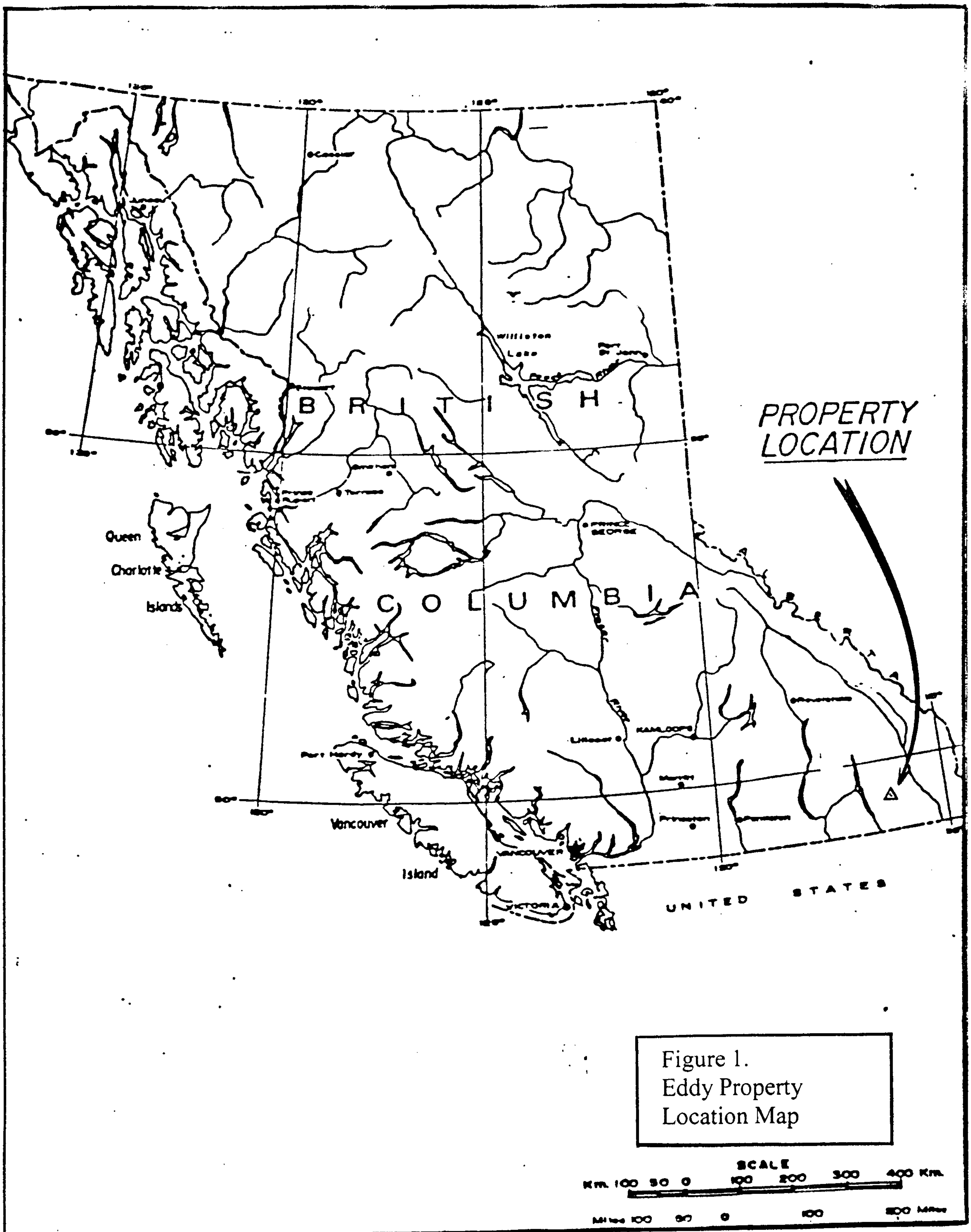
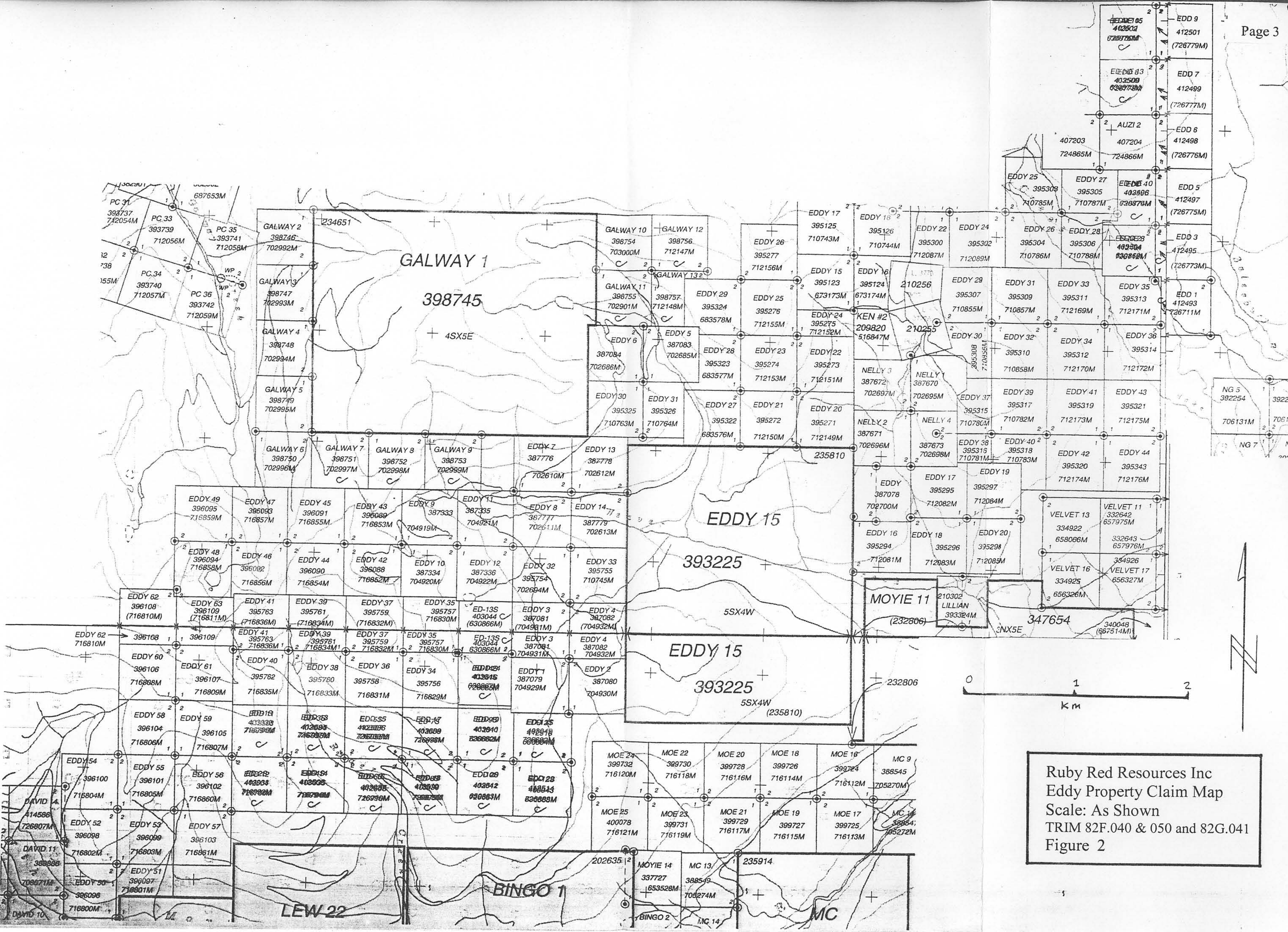



Figure 1.
Eddy Property
Location Map




Ruby Red Resources Inc
Eddy Property Claim Map
Scale: As Shown
TRIM 82F.040 & 050 and 82G.041
Figure 2

### 1.30 Physiography

The Eddy claim area is within the Moyie Range of the Purcell Mountains. Elevations on the property range from 1460 to 2210 meters and topography varies from gentle and moderate wooded slopes to steep rocky slopes. Forest cover includes mainly pine, fir and larch. Areas within the claim block have been clear-cut logged within the past 30 years and are in various stages of regeneration.

### 1.40 History

The Moyie River is one of three prominent placer gold drainages in the Cranbrook area and Weaver Creek, a tributary of the Moyie River, has had considerable placer gold produced from it. During the time of extensive placer gold production in the late 1800 and early to mid 1900's, prospecting for lode gold sources of the placers in the Cranbrook area was widespread. Numerous quartz veins were tested, some were found to be auriferous, and a few had minor production, although no significant lode gold production is known from the area of the present Eddy claims. Two workings in the Prospector's Dream area may date back to the 1890's.

Building of logging roads in the Weaver Creek drainage in 1981 exposed gold-bearing quartz veins and led to staking of mineral claims. Early exploration on the property consisted of road building and trenching with minor geologic and geochemical work.

In 1984 a program of prospecting, geological mapping and soil and rock geochemistry was conducted. Encouraging gold values were obtained by reconnaissance soil sampling in a few areas. In 1987 a program of more soil sampling, trenching and diamond drilling further tested these areas (Morris, 1987). Three holes were drilled at the Hill Vein, three at the MC2 Shear area (Old Baldy Fault) and nine at the Galena Vein.

In 1989 an exploration program of prospecting, heavy mineral sampling in selected tributary drainages, soil and rock geochemistry, VLF-EM and magnetic geophysical surveying, and geological mapping and trenching was conducted (Klewchuk and Kennedy, 1990). Emphasis continued to be on areas that were known to contain gold but the importance of the Old Baldy Fault as a control for gold mineralization was recognized. A small program in 1990 focused on a galena-bearing quartz vein hosted by gabbro south of the MC2 area.

In 2002, Ruby Red Resources Inc. staked a core claim group over the old showings and purchased the Prospector's Dream claims from Ed Frost of Cranbrook. Their initial work included prospecting and rock geochemistry with favorable results (Rodgers, 2002). In 2003 this work was expanded on with additional geologic mapping, soil and rock geochemistry and trenching (Klewchuk, 2004).

### 1.50 Scope of Present Program

In 2004 exploration work on the Eddy claims included geologic mapping, rock geochemistry (50 samples), contour and grid soil geochemistry (865 samples) and VLF-EM surveying (32.575m). Much of the work was carried out on and near the Old Baldy Fault structure.

## 2.00 GEOLOGY

### 2.10 Regional Geology

Mapping by Reesor (1981), Hoy and Diakow (1982) and Hoy (1984) has developed a good understanding of the geology and structure of the Cranbrook area of southeastern British Columbia. This area, which includes the Eddy claims, is part of the Purcell Anticlinorium, a geologic sub-province which lies between the Rocky Mountain Thrust and Fold Belt to the east and the Kootenay Arc to the west.

The mesoproterozoic Purcell Supergroup which occurs within the core of the anticlinorium includes up to 11 kilometers of dominantly fine-grained clastic and carbonate rocks.

The Eddy claims are underlain by parts of the two lowermost units of the Purcell Supergroup, namely the Aldridge and Creston Formations. Both formations are comprised of fine-grained clastic sedimentary rocks; the Aldridge is a thick succession of predominantly impure quartzites and siltstones of turbidite affinity while the Creston Formation is a shallower water sequence of cleaner quartzites but with considerable siltstone and argillite. The Aldridge Formation is intruded by a series of gabbro to diorite composition sills and dikes which are called the Moyie Intrusions; a few dikes extend into the Creston Formation.

In a broad regional manner, structure of the Cranbrook area is dominated by a series of NNE oriented faults, at least some of which are believed to have been active during sedimentation in the Precambrian and thus have locally modified the type, distribution and thickness of late Proterozoic and Paleozoic rocks (Leech, 1958; Lis and Price, 1976).

The Eddy claims sit within an area of increased structural complexity which is more or less centered on the three prominent placer gold streams in the Cranbrook area, namely Perry Creek and the Moyie and Wild Horse Rivers. A series of NNE to NE oriented shear zones and a series of east to NE oriented transverse faults create the structurally complex, block-faulted area within which the placer gold occurs.

Cretaceous intrusions of granodiorite to syenite composition are scattered through the general area of placer gold occurrence near Cranbrook. These young rocks are probably the eastern limit of the Bayonne Magmatic Belt. Some of the syenite and quartz monzonite stocks carry appreciable pyrite, pyrrhotite and chalcopyrite and tend to be associated with anomalous gold.

## 2.20 Property Geology

Regional mapping by federal and provincial government geologists provides only a very basic framework of the geology of the Eddy claims. The claim block is underlain by Aldridge and Creston Formation rocks which here are situated between the Cranbrook and Moyie transverse faults; structures that may have acted as controls of gold mineralization. No east-west oriented cross faults are known on the Eddy claims but the strong east-west linears of Weaver Creek and the North Moyie River suggest both of these drainages may reflect such structures. The only major intrusions in the claim block are Precambrian gabbro and diorite sills and dikes. Minor occurrences of younger, Cretaceous or early Tertiary felsic intrusion activity have been recognized by previous work and new occurrences were identified during the 2003 and 2004 work.

Bedding typically strikes northeasterly with moderate to steep west dips. The Old Baldy Fault (OBF), which also strikes northeasterly with moderate to steep northwest dip, is the dominant structure on the claim block, and is believed to be an important factor in the localization of gold mineralization on the property. Within a part of the claim area the OBF has a more easterly trend than its typical NNE strike and this may be a factor in the association of gold with this structure locally. In the area of the Eddy claims the OBF usually separates lower Creston Formation rocks on the northwest from middle Aldridge Formation rocks on the southeast, with an apparent vertical displacement of about 1100m. In the very southern portion of its exposure on the property, the OBF separates upper and middle Aldridge rocks with a lesser apparent vertical displacement, of about 800m.

Geologic mapping at the Eddy property in 2004 focused on the OBF with an emphasis on recognizing any structural complexity that could be a favorable factor in localizing gold. Exposures of the OBF are sparse and typically incomplete, and location of the structure has been inferred from subcropping float material in areas between bedrock exposures.

Stress associated with development of the OBF has also affected the hangingwall and footwall rocks. This stress has developed shear zones, quartz veins and quartz vein breccias in the adjacent host stratigraphy and these features are best developed in more brittle quartzitic rock units. Upper Aldridge and lower Creston Formation rocks are typically thin bedded and argillaceous and are not a good host for brittle fracturing. However the more quartzitic units (wackes to impure quartzites) of the middle Aldridge Formation to the southeast of the OBF do tend to host shear / quartz vein zones that are subordinate to the OBF. Thus very little brittle shearing is evident in the less favorable lower Creston Formation, hangingwall side of the OBF, and considerably more shearing and quartz veining is developed in the more favorable middle Aldridge Formation, footwall side of the fault. Middle Aldridge Formation rocks also host a number of gabbro to diorite composition Moyie Intrusions; these may have acted as favorable physical or chemical influences on the deposition of gold.

Gold mineralization on the Eddy property, at Prospector's Dream, Hill Vein and 'MC2' prospects, occurs near or between two large gabbro sills that are near the middle part of the middle Aldridge Formation. Their stratigraphic position is known from bar code -like laminated argillites that are time-stratigraphic units and which can be correlated over very large distances within the middle Aldridge Formation (and U.S.A. equivalent Pritchard Formation to the south). These large gabbro sills on the Eddy property are near the 'Sundown marker' and are commonly referred to as the Sundown sills or Sundown gabbros. Not all known gold occurrences in the Cranbrook Gold Belt occur near this Sundown stratigraphy but many of the Eddy occurrences do. The presence of the gabbros may have been a factor in gold deposition, either by focusing stress and allowing favorable fracturing / shearing to develop, or by acting as a favorable chemical factor for precipitation of gold.

At the David property, immediately south-southwest of the Eddy, significant gold is present within a shear zone hosted by middle Aldridge rocks on the footwall side of the OBF: the resource is about 100,000 tonnes of 10grams gold/tonne and within a single lens, exposed at surface, about 150 m long, which averages 2.2 meters in width (Murrell et al, 1991). Similar targets may exist on the Eddy ground. Detailed VLF-EM surveying in 2001 identified a WNW-oriented feature which crosses the zone of concentrated gold mineralization at the David (Klewchuk, 2002). It is not known what this VLF-EM feature is but it may reflect a structure that has influenced the deposition of gold. Such a model for gold deposition is present also on the Zinger property located east of the David in the headwaters of Perry Creek. Here high grade gold occurs within narrow, lensey, bedding and/or cleavage -parallel quartz veins immediately adjacent to WNW-trending fractures. This style of structurally-controlled gold mineralization is widespread on the Zinger property and it serves as a model for exploration in the area.

Contour soil geochemistry lines run in 2003 (Klewchuk, 2004) crossed the OBF in a few places to test for the presence of anomalous gold associated with this structure. Some of the soil lines that crossed the OBF returned little or no anomalous gold but, in a few places, anomalous gold was detected in soils, across the inferred trend of the OBF. Furthermore, trenching in 1989 encountered significant anomalous gold in the OBF in the 'MC2' area. This evidence of gold within the OBF is just cause for exploring the structure for an economic deposit. The OBF is a fairly wide structure, commonly more than 8 meters, and any zone of gold mineralization developed within the structure could be of considerable size.

For these reasons the OBF was targeted as an important feature to explore in 2004, with geologic mapping, soil and rock geochemistry and VLF-EM surveying. The objective was to locate and evaluate any areas of structural complexity such as an intersection with a WNW-trending structure.

Mapping and VLF-EM surveying in 2004 established or indicated four right lateral offsets of the OBF: in North Moyie Creek, in Claim Creek, in Ryder Creek and in Weaver Creek (Fig. 3). Widespread gold in soils east of the north fork of Weaver Creek, where the OBF is present but has not been identified on the ground, may represent another offset of the OBF.

The offset in Weaver Creek was surveyed with VLF-EM and the results sbstantiate the geologic interpretation. The inferred offsets in Claim Creek and Ryder Creek were established mostly by geologic mapping, then tested with contour soil geochemistry.

A large 'footwall shear / alteration' zone is developed a short distance east of the OBF on both sides of Weaver Creek. North of the creek the zone has been called the "MC2" zone (for a former "Weaver Mineral Claim 2"). This is a very wide zone with extensive silicification, shearing, disseminated pyrite, widespread low grade gold mineralization and at least some high grade gold in shear zones including grab samples of 34,662 and 28,322 ppb Au (Klewchuk and Kennedy, 1990; Rodgers, 2002). In this area south of Weaver Creek, the OBF is mostly overburden-covered between the creek and the ridge to the south. A few trenches tested the OBF in 1989 with one 40 cm width of quartz vein returning 29,000 ppb Au (0.845 oz/tonne). On the north side of the creek the area was called the 'Red Zone' and included wide zones of massive silicification and disseminated pyrite in two parallel-trending zones; one in the OBF and one in footwall middle Aldridge rocks a short distance to the east. It is not clear if the two zones were distinguished by previous work on the property.

This large shear / alteration zone in the immediate footwall of the OBF is a structural complexity that is not well understood at the present time. Strong gold mineralization exists within the northern-most exposures and trenches on the southern side of Weaver Creek, which are at least 400 m south of an inferred structure that offsets the two silicified zones about 500 meters in a right lateral manner (Fig. 3). A similar 400m of strike length of the two northeast structures is covered by overburden immediately north of Weaver Creek. Extensive bulldozer trenching further toward the northeast exposed the zones but only very weak gold values have been reported. The wide silicified zone within the OBF appears to pinch down to a narrower fault zone going northeast, although exposure is poor. The wide footwall silicified zone can be traced northeast to the Galena Vein area where local high grade gold has been previously located (Klewchuk and Kennedy, 1990).

The Weaver Creek / OBF intersection is an intriguing one because of the presence of gold in both of the parallel-trending structures and because of the offset in Weaver Creek. This is considered an excellent exploration target on the property.

Geologic mapping south of the Hill Vein area located an occurrence of quartz vein breccia, mostly as subcropping float and hosted by fairly flat-lying stratigraphy (Fig. 3). Rock samples returned up to 4g Au (see also section 3.10). Three E-W soil lines run across this area, roughly centered on the anomalous quartz vein breccia zone, failed to detect a significant anomaly.

This quartz vein breccia may be a bedding-parallel zone that emanates off a stronger shear zone that is in the footwall of the OBF or the OBF itself. Better concentrations of gold than those sampled in 2004 may exist where this quartz vein breccia zone encountered a local dilatent zone, for example in association with a fold or an intersecting structure.

North of Weaver Creek, new logging road construction exposed extensive weaker limonitic alteration in association with a felsite intrusion on a landing near 5473700N 569700E. A broad zone of limonitic quartz vein and quartz vein breccia float occurs a short distance northwest of the landing. Two soil lines and a VLF-EM grid were completed in the area (see also sections 3.00 and 4.00). As little gold was picked up in the soils, the area is not considered of high priority but the alteration and felsite exposure demonstrate there may be considerably more gold-related activity in the area of the Eddy claims than we presently know. This new exposure is in forest-covered moderate topography with no bedrock exposures and is typical of much of the Eddy property terrain.

## 3.00 ROCK AND SOIL GEOCHEMISTRY

### 3.10 Rock Geochemistry

Fifty rock samples were collected in 2004 during the course of geologic mapping in selected areas of the property. Rock samples were shipped to Acme Analytical Laboratories Ltd. at 852 East Hastings Street, Vancouver, B.C., and analyzed for a 30 element ICP package and geochemical gold by standard analytical techniques. Rock sample sites with gold values in ppb are shown in Figures 3 and 4 with sample descriptions in Appendix 1 and complete geochemical analyses in Appendix 2.

Most of the rock samples collected are on or near the Old Baldy Fault (OBF). Rock geochemistry results indicate that widespread gold mineralization is present within the OBF, with some gold present along the entire exposed strike length of just over 9 kilometers on the Eddy property. Rock and soil geochemistry data further support the possibility that gold mineralization is stronger where the OBF has been offset by east-west to northwest structures; these areas of structural intersection remain prime exploration targets on the Eddy claims.

The highest gold value obtained in rock samples in 2004 is from south of the Hill Vein area where a flat-lying, bedding-parallel quartz vein breccia returned 3944 ppb gold. This zone is thought to emanate from the OBF and could underlie the Hill Vein area.

### 3.20 Soil Geochemistry

Contour and grid soil samples were collected from a number of areas on the Eddy property in 2004, to evaluate areas of known bedrock gold mineralization, to follow up on favorable results obtained in 2003 and to test areas with inferred favorable geology. A total of 865 soil samples were collected; soils were taken from the B Horizon at an approximate depth of 15 cm, placed in Kraft paper bags, dried and shipped to Acme Analytical Laboratories Ltd. at 852 East Hastings Street, Vancouver, B.C., where they were analyzed for a 30 element ICP package and geochemical gold by standard analytical techniques. Soil sample lines are shown on Figure 4 with gold values in ppb. Complete geochemical analyses are provided in Appendix 3.

*Prospector's Dream Area*

Four east-west lines (5500N to 5800N; Fig. 4) were sampled north of the Prospector's Dream showings, to evaluate a possible mineralized north-trending structure. A few elevated gold values up to 75 ppb were obtained. A weak NNE linear trend of 15 to 29 ppb Au occurs near the eastern ends of the 3 southern lines.

Two east-west lines (4900N and 5000N) were sampled south of the Prospector's Dream showings, to also cross the trace of the inferred north-trending fault. Two elevated gold values, 152 and 2026 ppb, were detected. Both sample sites are near the area of one gold showing and may reflect that mineralization. The 2 gram analysis is, however, near the projected location of the fault structure and this area should be further evaluated.

*Weaver Area*

Recent logging road construction to a landing at ~569700E 5473650N exposed a wide zone of limonitic and argillic altered sedimentary rocks in association with a felsite intrusion. The limited exposure of the felsite doesn't provide a width or orientation to the felsite body. Favorable-looking quartz vein float occurs a short distance NW of the felsite and alteration on the landing. Two east-west soil lines (3650N and 3900N; Fig. 4) were run across the landing and to the west and north. Generally low gold values were obtained although one high of 275 ppb Au warrants confirmation and possible follow-up.

*Hill Vein Area*

Trenching in 2003 at the Hill Vein area identified north-striking faults that appear to control flat-lying gold-mineralized quartz veins, one of which is the 'Hill Vein'. A single contour soil line, done at ~1640m in 2003 to the north of the Hill Vein, has two higher gold values (33 and 111 ppb; Klewchuk, 2004) and supports the presence of anomalous gold extending northerly from the Hill Vein area.

A series of north-south and east-west grid lines were soil sampled between the Hill Vein and the 2003 contour line south of Weaver Creek (Fig. 4). Widespread elevated gold values occur on most of the lines although no obvious pattern exists. The area has no exposed bedrock and overburden is of unknown thickness. The gold-in-soil anomaly here may be reflecting bedrock gold and additional work is warranted. VLF-EM surveying completed here in 2004 (see section 4.00) supports the presence of structure in the area and a program of trenching should be undertaken to evaluate these structures and the gold-in-soil geochemical anomaly.

*South Hill Vein Area*

Four east-west lines (13N to 16N; Fig. 4) were sampled across a sub-cropping zone of quartz vein breccia which returned over 3900 ppb Au in rock samples. This zone appears to be bedding-parallel and it may extend under the area of the Hill Vein to the north. The four lines of soil sampling were intended to help identify the strike extension of the zone but failed to detect any appreciable gold, with only one sample above 10 ppb Au.

*Claim Creek Area*

Claim Creek is a south-flowing tributary of North Moyie Creek, located near 563500E (Fig. 4). Mapping of this area of the property in 2004 indicates a right lateral offset of the OBF of just over 200m; the offset may coincide with a tributary drainage that trends ~315$^0$. Three soil lines tested this area in 2004 and scattered elevated gold values exist on all three lines (Fig. 4). Very limited float and bedrock sampling of quartz vein / shear zone material which appears part of the OBF system returned generally low gold values with the only higher value, of 230 ppb, coming from the east side of claim creek. These limited rock and soil geochemistry results are compatible with elevated gold occurring near the fault offset and further evaluation of this exploration target is recommended.

*Ryder Creek Area*

Mapping of the OBF in the Ryder Creek area indicates a minor right lateral offset of the fault may exist in the upper part of Ryder Creek; the offset may coincide with a tributary drainage that trends 315$^0$ (Fig. 4). Heavy mineral sampling in 1989 returned one 14,500 ppb Au value just below the area of this inferred offset thus contour soil sampling was used in 2004 to further evaluate the area of inferred fault offset.

Four contour lines (L1820, L1840, L1860 and L1880; Fig.4) were sampled near where the OBF crosses Ryder Creek. The two soil lines east of Ryder Creek have only very low gold values; the highest value of 16 ppb occurs near Ryder Creek and near the inferred location of the OBF.

Three lines west of Ryder Creek show widespread low, moderate and local high gold values, up to 197 and 368 ppb. Rock geochemistry on the OBF mostly east of the lines also detected anomalous gold, with two samples having 417 and 590 ppb. Although the specific area of inferred fault offset may not be well tested by this rock and soil geochemistry, the data is consistent with higher gold values present in and near the OBF at or close to the inferred offset of the OBF, and further work, including trenching, should be done.

*North Weaver Area*

Two long contour lines were sampled in this area in 2003 and crossed the area of the Old Baldy Fault (Klewchuk, 2003 and Fig. 4). Both of these 2003 contours detected anomalous gold in soil on both sides of the north-trending ridge (which roughly parallels 569000E; Fig. 4) east of the north Fork of Weaver Creek. Location of the OBF across this ridge is unknown; bedrock exposure is limited and the current level of geological mapping has not defined the fault trace.

The contour soil coverage was expanded in 2004 with 7 short contour lines (Lines NW1, 2, 3 & 4 and Lines EW 1, 2 & 3; Fig. 4) sampled to provide additional detail. The uppermost contour line, at ~2000m elevation (soil line '20') has little gold and appears to represent a local uphill cutoff. Two clusters of gold mineralization indicated by the 2003 work are substantiated by the new contour soil sampling with gold values up to 184 ppb in the western cluster and up to 405 ppb in the eastern cluster.

The OBF has not been mapped through the areas of the anomalous gold-in soil geochemistry but it should project into the western anomaly and into the upper part of the eastern anomaly. A significant structural offset on the OBF may exist in the area of these soil anomalies and extensive further work including detailed geology, rock geochemistry, VLF-EM geophysics and trenching are warranted to evaluate the bedrock source of the soil geochemistry anomalies.

## 4.00 VLF-EM GEOPHYSICS

### 4.10 Introduction

Known gold mineralization on the Eddy property is structurally-controlled and VLF-EM geophysical surveying can detect structures which may not be evident using any other type of geophysics so a program of VLF-EM surveying was initiated on the claim block in 2004. In areas of interest, roads were typically surveyed first, in the hope of efficiently detecting anomalous responses which could then be surveyed in more detail. Subsequently, grid surveying was carried out on east-west and north-south lines using GPS as a control for starting points and for determining intermediate points on the survey lines. A total of 32,575 meters of line was surveyed (Figs. 5a and 5b).

## 4.20 VLF-EM Survey

### 4.21 Instrumentation and Survey Procedure

The VLF-EM (**V**ery **L**ow **F**requency **E**lectro**m**agnetics) method uses powerful radio transmitters set up in different parts of the world for military communication and navigation. In radio communication terminology, VLF means very low frequency, about 15 to 25 kHz. However, relative to frequencies generally used in geophysical exploration, the VLF technique actually uses very high frequencies.

A Crone Radem VLF-EM receiver, manufactured by Crone Geophysics Ltd. of Mississauga, Ontario, was used for the VLF-EM survey. Seattle, Washington, transmitting at 24.8 kHz and at an approximate azimuth of 249° from the survey area, was used as the transmitting station for most of the survey while Annapolis Maryland (21.4 kHz and at ~118$^0$) was used for part of one grid.

In all electromagnetic prospecting, a transmitter produces an alternating magnetic (primary) field by a strong alternating current usually through a coil of wire. If a conductive mass such as a sulfide body is within this magnetic field, a secondary alternating current is induced within it, which in turn induces a secondary magnetic field that distorts the primary magnetic field. The VLF-EM receiver measures the resultant field of the primary and secondary fields, and measures this as the tilt or 'dip angle'. The Crone Radem VLF-EM receiver measures both the total field strength and the dip angle.

The VLF-EM uses a frequency range from about 15 to 28 kHz, whereas most EM instruments use frequencies ranging from a few hundred to a few thousand Hz. Because of its relatively high frequency, the VLF-EM can detect zones of relatively lower conductivity. This results in it being a useful tool for geologic mapping in areas of overburden but it also often results in detection of weak anomalies that are difficult to explain. However the VLF-EM can also detect sulfide bodies that have too low a conductivity for other EM methods to pick up.

Survey lines on the grid were initially located by using a Garmin 76 hand-held GPS, then run by compass. All survey lines were measured with a hip-chain with VLF-EM readings (field strength and dip angle) taken at 25 meter spacings. Sufficient GPS readings were taken during VLF-EM surveying to provide confidence in plotting all survey lines on the base maps. A total of 32.575 kilometers of VLF-EM surveying was completed on the Eddy property in 2004, on various targets.

Results were reduced by applying the Fraser Filter and both dip angle and Fraser Filter values are shown on the survey lines in Figures 5a and 5b.

The Fraser Filter is essentially a 4-point difference operator which transforms zero crossings into peaks, and a low pass operator which induces the inherent high frequency noise in the data. Thus the noisy, often non-contourable data are transformed into less noisy, contourable data. Another advantage of this filter is that a conductor which does not show up as a zero crossover in the unfiltered data quite often shows up in the filtered data.

### 4.22 Discussion of Results

*Prospector's Dream Area*

Trenching at the Prospector's Dream in 2003 indicated that a north-striking fault controlled high-grade gold mineralization present in relatively flat-lying quartz veins and quartz vein breccia zones. VLF-EM surveying was done to try and detect the fault with the hope of tracing it northward to the OBF where a better exploration target could exist. Some of the available roads were surveyed as well as a series of east-west lines (Fig. 5a) to test the inferred north-south fault. Unfortunately, the north-south fault was not detected by the VLF-EM survey. An apparent NE structure was detected on the northern lines but has no evident continuity onto the southern 2 surveyed lines. This NE anomaly may be a fault or shear, parallel to the OBF and related to that structure. This NE orientation is similar to VLF trends detected on the former Zau claims, on trend to the north of Noke Creek (Klewchuk, 2000, AR 26,156). The Noke Creek road, which crosses a northern portion of the Eddy property, was also surveyed and a series of anomalies were detected (Fig. 5a), one of which may correspond to the NE anomaly at Prospector's Dream.

A small survey was also done near 5475400N 569800E across a 2003 trench where weak gold was identified in small fault/fracture zones within a broad argillic altered zone. A broad VLF-EM anomaly was detected just south of the old trench (Fig. 5a). This area is in the footwall of the OBF and warrants more work -both VLF-EM and soil geochemistry- to acquire more data.

Other, currently 'one line' anomalies were detected in the general Prospector's Dream area and should be detailed as time permits. One anomaly, at 5474800N 569500E is below and east of an area of strong gold in soil geochemistry and should be further evaluated as it may be a structure related to the gold mineralization detected by the soil geochemistry.

*Weaver Area*

New logging road construction north of Weaver Creek has exposed limonitic and argillic -altered middle Aldridge sediments in association with a felsite intrusion, on a landing near 5473725N 569730E (Fig. 3). Just NW of the landing is a broad area of quartz vein and quartz vein breccia float. A small program of VLF-EM surveying was conducted here in association with some soil geochemistry. A series of east-west lines were originally surveyed and the data indicated the presence of an east-west anomaly (Fig. 5a) which was subsequently surveyed with north-south lines. The eastern part of the N-S line grid, including Line 9500E, used Annapolis, Maryland as the transmitting station (21.4 kHz and at an approximate azimuth of $118^0$ from the survey area) while the remainder of the grid used Seattle (24.8 kHz).

A NE oriented anomaly is centered over the felsite intrusion that is partially exposed on the landing. The broad VLF-EM may reflect the structure controlling the intrusion and the alteration zone associated with it.

In the western half of the grid area an E-W anomaly with a locally strong response occurs on a moderate south-dipping forest-covered slope where no bedrock is exposed. Grid soils on east-west lines did not detect any significant gold associated with the anomaly; either overburden masks the response or the structure is not gold-bearing.

In the extreme NW corner of the grid an apparent NE trending anomaly was detected; the currently known strike length is short but this may be an OBF-parallel footwall shear or fault zone.

*Hill Vein Area*

Trenching in 2003 identified a north-striking fault which appears to control flat-lying gold-bearing quartz veins as well as local strong alteration of gabbros. Available roads and east-west lines were surveyed to try and detect this structure (Fig. 5b). As with the Prospector's Dream area, the north-south fault was not detected but other anomalies were identified. As a result of other anomalous responses on the roads, a series of north-south lines were surveyed and detected a broad but moderately strong anomaly from 566950E to 567400E; further east, in the vicinity of the inferred Hill Vein Fault, the anomaly appears to be cut off by a fault (?). The east-west trend and character of this VLF-EM response is similar to the main anomaly in the 'Weaver area' and is also parallel to Weaver Creek, which may be structurally controlled.

The area of trenching at the Hill Vein, where strong gold mineralization is known, appears to be a relatively 'neutral' area of VLF-EM response. This may be due to intersecting structures causing extensive brecciation such that no distinct structures remain in the immediate area. One such structure may trend northeast along the southeastern boundary of the longer east-west anomaly.

*Old Baldy Fault / Weaver Creek Intersection Area*

Weaver Creek is a strong east-west linear and it has long been considered that the drainage is structurally controlled. Weaver Creek loses its linear character above where the OBF crosses it. Given that gold mineralization is known in some parts of the OBF, any intersecting structure could create a favorable site for gold deposition. Another additional possible favorable feature is the strong silicified zone which occurs in the immediate footwall area of the OBF in this Weaver Creek area .

In 2004, some of the VLF-EM surveying was completed in this OBF-Weaver Creek intersection area. Initially the roads were surveyed and a few widespread weak to moderate anomalies were detected. Two lines were run across old skid roads across the inferred trace of the strong silicic altered zone in the middle Aldridge Formation, footwall to the OBF (the MC2 zone). A moderate VLF-EM anomaly was detected across the lower line and a stronger anomaly was seen on the upper line (Fig. 5b). The stronger response may be due to the presence of gabbro at the contact of the shear zone here. The Old Baldy Fault, which here is inferred from 1989 trench data, is apparently not detected at this locality by the VLF-EM surveying although there are three separate VLF-EM responses on the road lines just northwest of the OBF; their orientation and possible cause is unknown.

On the north side of Weaver Creek, the road and two east-west lines were surveyed south of the exposed OBF and footwall silicified zone. Two anomalies which closely coincide with the southern projection of these zones were detected. The anomalies narrow southward; the eastern one disappears and the western one diminishes in width and strength, compatible with an inferred ~500m offset of the OBF zone along a fault (?) structure which roughly coincides with the drainage of Weaver Creek. Subsequently the northern terminus of the alteration zone south of Weaver Creek was detailed enough to infer the approximate location of the offset. A few north-south lines were run (Fig. 5b) to try and define the inferred east-west structure in Weaver Creek but the structure was not obviously detected.

## 5.00 CONCLUSIONS

Geologic mapping on the Eddy claims in 2004 focused on the Old Baldy Fault as it is the largest structure known on the property and it hosts significant gold mineralization in places. Geologic mapping established a number of right lateral offsets on the OBF; the offset in Weaver Creek was confirmed with VLF-EM surveying, and two inferred offsets, in Claim Creek and Ryder Creek, have anomalous gold-in-soil anomalies associated with them.

Rock geochemistry results generally support the presence of gold mineralization within the Old Baldy Fault and also support the presence of gold at or near inferred structural intersections.

Soil sampling tested a number of targets on the property and results indicate that widespread gold mineralization exists, in some cases in association with the Old Baldy Fault.

Widespread VLF-EM surveying detected a number of inferred structures on the Eddy claims; these are generally E-W to NE and are considered a favorable orientation for hosting gold mineralization. The OBF itself was detected by VLF-EM on the north side of Weaver Creek and a zone of strong silicification and pyrite alteration in the footwall of the OBF was detected on both sides of Weaver Creek.

The 2004 Eddy program of geologic mapping, soil and rock geochemistry, and VLF-EM surveying has advanced understanding of the property and provided targets for trenching and diamond drilling. Further work is recommended; priority should be on potential target areas such as the inferred structural intersection of the OBF at Weaver Creek, Claim Creek, Ryder Creek and northeast of the north fork of Weaver Creek.

## 6.00 REFERENCES

Hoy, T., 1984. Geology of the Cranbrook sheet and Sullivan Mine area. NTS 82G/12, 82F/9. BC MEMPR Preliminary Map No. 54.

Hoy, T., and Diakow, L, 1982. Geology of the Moyie Lake area. BC MEMPR Preliminary Map No. 49.

Klewchuk, P. 2000, Geologic mapping, rock geochemistry and VLF-EM geophysics, Zau claims, Moyie River area, Fort Steele Mining Division, BCGSB AR 26,156.

Klewchuk, P., and Kennedy, C.R., 1990. Weaver claims, prospecting, geology, geochemistry and geophysics.

Leech, G.B., 1958. Fernie Map-Area, West-half, British Columbia. Geol. Surv. Can. Paper 58-10, 40pp.

Lis, M.G., and Price, R., 1976. Large scale block faulting during deposition of the Windermere Supergroup (Hadrynian) in southeastern British Columbia. Geol. Surv. Can. Paper 76-1A p. 135-136

Morris, R., 1987. Weaver Claims, southeastern British Columbia, NTS 82F/8E. Report on drilling performed in June and July, 1987.

Murrell, M.R., Klewchuk, P., and Bapty, M, 1991
Property development report, David (David, Lew, Harmony, Rob claims), Fort Steele Mining Division, Internal Report for Dragoon Resources Ltd.

Reesor, J.E., 1981. Geology of the Grassy Mountain Map Sheet. NTS 82F/8. Geol. Surv. Can. Open File 820.

Rodgers, G., 2002. Prospecting and Geochemical report, Eddy 1-63 mineral claims, Weaver Creek area, Fort Steele Mining Division, BCGSB AR 26972 .

## 7.00 STATEMENT OF COSTS

| | |
|---|---|
| Geologic mapping, VLF-EM surveying, program supervision (P. Klewchuk) | $13,771.95 |
| Soil (865 samples) and rock (50 samples) @ ~15.90/sample | 14,508.67 |
| Field Assistants (D. & R. Klewchuk) soil and rock sampling, VLF-EM surveying | 3,912.46 |
| Total | $32,193.08 |

## 8.00 AUTHOR'S QUALIFICATIONS

As author of this report I, Peter Klewchuk, certify that:

1. I am an independent consulting geologist with offices at 246 Moyie Street, Kimberley, B.C.
2. I am a graduate geologist with a B.Sc. degree (1969) from the University of British Columbia and an M.Sc. degree (1972) from the University of Calgary.
3. I am a Fellow of the Geological Association of Canada and a member of the Association of Professional Engineers and Geoscientists of British Columbia.
4. I have been actively involved in mining and exploration geology, primarily in the province of British Columbia, for the past 29 years.
5. I have been employed by major mining companies and provincial government geological departments.

Dated at Kimberley, British Columbia, this 16th day of February, 2005.

Peter Klewchuk
P. Geo.

APPENDIX 1 Description of Rock Samples

| Sample No. | UTM Coords | Description |
|---|---|---|
| E-15 | 568908E 5474713N | Float sample of very rusty quartzite, top of gabbro rubble. Abundant limonite spots (py?), vugs, irregular quartz pods and veins. |
| E-16 | 569091E 5474980N | Float. Shear zone type quartz with seds. Finer vugs, limonitic. Sulfides (py?) Leached out. |
| E-17 | 569091E 5474980N | Float. More massive quartz with some rodded quartz veining, brecciated quartz and irregular vugs. Probable py, oxidized. |
| E-18 | 569091E 5474980N | Float. Granular, vuggy quartz from same area. |
| E-19 | 569091E 5474980N | Largest piece of quartz float, vuggy and rodded, hematitic quartz. Probable ox py. |
| E-20 | 569091E 5474980N | Float - fragments of more limonitic quartz from larger boulder. |
| E-21 | 568932E 5475077N | Thin QV bx in altered quartzites. Lensey, thin light gray QV, dissem py. Orange and reddish hematitic limonite. |
| E-22 | 569942E 5477190N | Noke Creek adit. Possibly related to OBF. Quartz vein shear zone ~70 cm wide, cuts through seds Massive, very strong silicification with abundant dissem pyrite in QV and in adjacent phyllitic seds. |
| E-23 | 564707E 5470881N | Rubbly subcrop /outcrop of QV bx. QV are few mm to few cm wide, wavy, lensey, discontinuous. Some are cross-cutting. Within phyllitic, argillaceous seds. Relatively minor dissem py in QV and seds. Most QV looks granular, weakly limonitic, fairly white. Looks like a shear zone structure. |
| E-24 | 564531E 5471136N | Suite of angular chips of float. Various quartz veins; some thin QV breccia, limonitic, liesegange-altered. Some of sample is bedrock, some not. |
| E-25 | 564540E 5471250N | Quartz chips from area of stronger shearing with very strong limonite (some limonite breccia). Thin, irregular, indistinct veins and small patches. Mostly pinkish hematitic. |
| E-26 | 564540E 5471250N | Chips of more argillaceous seds. Brecciated, limonitic with abundant weathered out, dissem py. |

| | | |
|---|---|---|
| E-27 | 564587E 5471347N | Phyllitic float with thin QV, oxidized dissem py. Widespread float - may be a wide zone. |
| E-28 | | Similar to E-27. |
| E-29 | 564598E 5471284N | FW edge of OBF; dolomitic unit, silicified, with dissem py. |
| E-30 | 564801E 5471624N | Small lens of dolomite vein bx with very fine dissem py in foliated argillite band. Nearby bed-parallel QV and flattish, SW-dipping QV (cross-cutting structure?). |
| E-31 | 564770E 5471543 | Float of good looking, shear type quartz vein breccia with rusty, phyllitic argillite / siltstone. Abundant oxidized pyrite. |
| E-32 | 564733E 5471650N | Sheared siltstone / argillite in OBF. Weak silica as thin veins on cross-cutting fractures. Vuggy, rusty with oxidized pyrite. |
| E-33 | 564716E 5471687N | Very sheared part of fault zone; bleached, silicified, pastel-colored argillites -Hc? Sample of bedding or shear -parallel white, lensey quartz vein. |
| E-34 | 565280E 5471550N | Limonite breccia with hematite alteration and quartz veining. Specks of disseminated limonite - ox py? |
| E-35 | 568414E 5471642N | Float of bedding or cleavage -parallel quartz vein in quartzites. |
| E-36 | 568298E 5471564N | Float of granular QV with altered, bleached seds. Limonite bands, med to coarse ox py and cpy (malachite stain). |
| E-37 | 568258E 5471516N | QV bx. Bedding-sub-parallel wavy, anastomosing / braided veins (similar to E-35). Sub-crop. Weakly limonitic QV, possible ox py. |
| E-38 | 568303E 5471480N | Single 2 cm wide QV from bedrock. Rusty, granular quartz with different textures - fine, med and coarse-grained. Darker reddish-brown oxidation. |
| E-39 | 568306E 5471480N | QV bx. 1.5 to 2.5 cm QV with some cross-cutting fabric. Float but abundant local QV bx; subcropping. Minor dissem ox py. |
| E-40 | 568306E 5471480N | (Same loc as E-39) Float of thin braided QV (Zinger-type) Pink to reddish-brown limonite. |

| | | |
|---|---|---|
| E-41 | 564204E 5470682N | Limonitic QV bx float. More weak limonite bx around. Shear type bx; dark reddish limonite with thin cross-cutting QV. |
| E-42 | 564209E 5470720N | Float QV bx, similar to E-41; bleached, pastel-colored quartzite, dark reddish limonite, open space quartz crystals. |
| E-43 | 563991E 5470484N | QV bx float. Rusty, reddish limonitic QV. Bleached yellow-white-reddish siltstone, quartzite host. |
| E-44 | 563088E 5469933N | Sample of rusty part of flat QV (070/18SE). May be amalgamated with shear-parallel (050/76W) quartz. Host is sheared argillite. |
| E-45 | 563088E 5469933N | Narrow (2-3 cm wide) bed-parallel QV bx zone. Could be part of a shear zone in FW of OBF. |
| E-46 | 563088E 5469933N | Thicker bed-parallel QV, up to 20 cm wide, lensey. Coarse granular quartz. Sed contacts are bx with ox dissem py. Sample is of quartz, some vugs, some fresh py, minor PbS. |
| E-47 | 563088E 5466933N | Same rock as E-46, with more concentration on fresh py (most still leached out). Larger QV here are associated with pale greenish-gray massive silicification with dissem py ie similar to much of MC2 area. |
| E-48 | 563088E 5466933N | Sample of massive silicification, dissem py (mostly ox). Some bx, one wavy seam of limonite. |
| E-49 | 563130E 5470022N | Small pods of pyritic quartz and cross-cutting QV with py in both quartz and adjacent altered seds. |
| E-50 | 563431E 5470133N | Sample of QV bx float, fine dissem py. Brown-orange limonite. |
| E-51 | 565456E 5472297N | OBF or proximal FW zone; abundant siliceous altered siltstone. Sample of oxidized shear-type quartz. QV with phyllitic argillite margins, internal crustiform, limonitic quartz. |
| E-52 | 565456E 5472297N | Sample of more vuggy quartz with abundant dissem ox py, vague banding. |
| E-53 | 567407E 5474250N | Large boulder; quartz with open space vugs, some limonite. |

| | | |
|---|---|---|
| E-54 | 567407E 5474250N | Another probable boulder (very,large) bands of quartz veining qith crystalline quartz, purplish limonite, in phyllitic host. Sample mostly of crystalline quartz. |
| E-55 | 569030E 5474815N | QV bx float, dissem py. |
| E-56 | 569213E 5475026N | Float. Bx quartzite, thin QV, dissem ox py. |
| E-57 | 569213E 5475026N | QV bx, dissem py. More QV than sample E-56. |
| E-58 | 569213E 5475026N | Phyllitic seds and QV - possible contact of QV zone. Abundant ox dissem py. |
| E-59 | 569157E 5475019N | QV bx, fragments of chloritic seds, strong limonite in patches. Site of Line EW1, 175N soil. |
| E-60 | 565809E 5472746N | Bedding / cleavage -parallel QV is seds, ~1.5m west of gabbro contact. |
| E-61 | 567800E 5474575N | Grab of QV chips from massive silicified zone; vuggy, rusty, lensey QV with phyllitic argillite, silicified siltstone or quartzite. Dissem py in QV and in seds; some ox, some fresh. |
| E-62 | 567800E 5474575N | Same as E-61. |
| E-63 | 567693E 5474462N | Sample of cross-cutting QV (119/69W). Vein is quite bland - sampled vugs and possible ox py. |
| E-64 | 567693E 5474462N | Sample of lensey, vuggy, bedding-parallel QV at site of E-63. Small limonitic vugs, no py seen. |

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

## GEOCHEMICAL ANALYSIS CERTIFICATE

Ruby Red Resources Inc. PROJECT EDDY File # A403183
207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au* ppb |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| SI | 1 | <1 | <3 | 1 | <.3 | <1 | <1 | <2 | <.01 | <2 | <8 | <2 | <2 | 2 | <.5 | <3 | <3 | <1 | .10 | <.001 | <1 | <1 | <.01 | 2 | <.01 | <3 | <.01 | .57 | <.01 | <2 | .5 |
| E 15 | 3 | 11 | 18 | 48 | 1.4 | 12 | 71 | 165 | 14.83 | 25 | <8 | <2 | 2 | 4 | .5 | <3 | <3 | 85 | .01 | .088 | 9 | 14 | .04 | 26 | .02 | <3 | .72 | .05 | .08 | <2 | 1107.1 |
| E 16 | 1 | 5 | 10 | 3 | <.3 | 1 | 3 | 192 | 6.73 | 23 | <8 | <2 | 4 | 1 | <.5 | <3 | 4 | 11 | <.01 | .019 | 22 | 1 | .02 | 23 | <.01 | <3 | .29 | .01 | .19 | <2 | 30.4 |
| E 17 | 3 | 5 | 6 | 14 | <.3 | 5 | 5 | 97 | 6.92 | 11 | <8 | <2 | 2 | 1 | <.5 | <3 | <3 | 7 | .01 | .039 | 6 | 10 | .01 | 13 | <.01 | <3 | .20 | .01 | .10 | <2 | 10.2 |
| E 18 | 4 | 2 | 13 | 11 | .4 | 16 | 100 | 305 | 10.11 | 37 | <8 | <2 | 4 | 1 | <.5 | <3 | <3 | 10 | <.01 | .050 | 31 | <1 | .02 | 31 | <.01 | <3 | .36 | .01 | .18 | <2 | 17.5 |
| E 19 | 3 | 2 | 12 | 17 | .5 | 11 | 11 | 414 | 10.67 | 13 | <8 | <2 | 3 | 2 | <.5 | <3 | <3 | 5 | <.01 | .077 | 3 | 4 | .01 | 9 | <.01 | <3 | .16 | .01 | .01 | <2 | 4.3 |
| E 20 | 1 | 4 | 32 | 133 | <.3 | 1 | 3 | 43 | 4.40 | 5 | <8 | <2 | <2 | 1 | .6 | <3 | <3 | 2 | <.01 | .015 | 2 | <1 | <.01 | 4 | <.01 | <3 | .07 | .01 | .02 | 2 | 8.2 |
| E 21 | 3 | 16 | <3 | 22 | .3 | 14 | 7 | 527 | 2.69 | <2 | <8 | <2 | 6 | 2 | <.5 | <3 | <3 | 3 | <.01 | .031 | 16 | <1 | .02 | 26 | <.01 | <3 | .42 | .05 | .06 | <2 | 740.7 |
| STANDARD DS5/AU-R | 13 | 139 | 24 | 135 | .3 | 25 | 12 | 748 | 2.98 | 19 | <8 | <2 | 3 | 46 | 5.5 | 4 | 5 | 59 | .73 | .094 | 12 | 185 | .69 | 136 | .10 | <3 | 2.00 | .04 | .15 | 6 | 478.0 |

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

## GEOCHEMICAL ANALYSIS CERTIFICATE

Ruby Red Resources Inc. PROJECT EDDY File # A403683
207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au* ppb |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| SI | <1 | <1 | 7 | 4 | <.3 | <1 | <1 | 3 | .02 | <2 | <8 | <2 | <2 | 2 | <.5 | <3 | <3 | <1 | .10 | <.001 | <1 | <1 | <.01 | 2 | <.01 | 3 | .01 | .44 | <.01 | <2 | <.5 |
| E-22 | 2 | 2 | <3 | 8 | <.3 | 34 | 142 | 88 | 7.06 | 7 | <8 | <2 | 9 | 1 | <.5 | <3 | <3 | 17 | <.01 | .007 | 18 | 13 | 2.51 | 3 | <.01 | 14 | 1.96 | .01 | .01 | 2 | 1.3 |
| E-23 | 1 | 2 | 22 | 14 | <.3 | 25 | 54 | 900 | 2.74 | 11 | <8 | <2 | 6 | 7 | .5 | <3 | <3 | 4 | <.01 | .024 | 18 | 1 | .12 | 43 | <.01 | <3 | .25 | .01 | .09 | <2 | 1.4 |
| E-24 | 1 | 9 | 158 | 180 | <.3 | 10 | 20 | 167 | 4.12 | 11 | <8 | <2 | 5 | 1 | .7 | <3 | <3 | 3 | <.01 | .021 | 15 | <1 | .03 | 15 | <.01 | 10 | .20 | .01 | .10 | <2 | 416.6 |
| E-25 | <1 | 2 | 7 | 14 | <.3 | 41 | 22 | 53 | 7.42 | 3 | <8 | <2 | 2 | 1 | <.5 | <3 | <3 | 42 | .01 | .010 | 1 | 24 | 5.50 | 4 | <.01 | 13 | 4.39 | <.01 | .02 | <2 | 4.8 |
| E-26 | <1 | 2 | 4 | 14 | <.3 | 47 | 25 | 121 | 8.27 | <2 | <8 | <2 | 2 | <1 | <.5 | <3 | <3 | 44 | .01 | .009 | 1 | 21 | 5.59 | 4 | <.01 | 14 | 4.50 | <.01 | .02 | <2 | 3.9 |
| E-27 | 3 | 14 | 34 | 29 | <.3 | 75 | 105 | 137 | 19.68 | 4 | <8 | <2 | 4 | 2 | <.5 | <3 | <3 | 12 | <.01 | .024 | 4 | 5 | 1.09 | 58 | <.01 | 29 | 1.05 | <.01 | .06 | <2 | 14.8 |
| E-28 | 1 | 7 | 46 | 23 | .5 | 19 | 19 | 110 | 9.21 | 3 | <8 | <2 | 5 | 4 | <.5 | <3 | <3 | 18 | <.01 | .009 | 24 | 6 | .08 | 25 | <.01 | 16 | .33 | .01 | .13 | <2 | 88.4 |
| E-29 | <1 | 3 | 5 | 33 | <.3 | 71 | 58 | 602 | 8.08 | 5 | <8 | <2 | 11 | 2 | <.5 | 10 | <3 | 10 | .11 | .005 | 1 | 4 | 11.84 | 20 | <.01 | 13 | .27 | .01 | .13 | <2 | 5.1 |
| E-30 | <1 | 3 | 29 | 20 | <.3 | 24 | 9 | 631 | 3.97 | 2 | <8 | <2 | 12 | 52 | <.5 | <3 | <3 | <1 | 4.47 | .029 | 19 | 5 | 3.53 | 35 | <.01 | 3 | .25 | .01 | .18 | <2 | 2.6 |
| E-31 | 1 | 4 | 41 | 14 | <.3 | 14 | 17 | 27 | 4.93 | 6 | <8 | <2 | 2 | 3 | <.5 | <3 | <3 | 8 | .02 | .004 | 3 | 7 | .18 | 37 | <.01 | 12 | .26 | .01 | .13 | 2 | 3.4 |
| E-32 | 1 | 2 | 5 | 11 | <.3 | 3 | 3 | 15 | 6.35 | 6 | <8 | <2 | 5 | 2 | <.5 | <3 | <3 | 3 | .04 | .017 | 8 | 3 | .03 | 19 | <.01 | 12 | .19 | .01 | .13 | <2 | 2.5 |
| E-33 | 1 | 31 | 114 | 92 | .5 | 16 | 10 | 699 | 4.22 | 2 | <8 | <2 | 6 | 32 | <.5 | <3 | 3 | 3 | .31 | .057 | 12 | 2 | .32 | 564 | <.01 | 5 | .22 | .01 | .15 | 3 | 590.0 |
| E-34 | 1 | 1 | 6 | 5 | <.3 | 9 | 13 | 11 | 1.99 | <2 | <8 | <2 | 5 | 2 | <.5 | <3 | <3 | 5 | .01 | .017 | 42 | <1 | .01 | 22 | <.01 | 5 | .25 | .01 | .18 | <2 | 2.4 |
| E-35 | 1 | 14 | 31 | 14 | <.3 | 2 | <1 | 49 | 1.27 | 2 | <8 | <2 | 4 | 20 | <.5 | <3 | <3 | 5 | .01 | .019 | 22 | <1 | .02 | 44 | <.01 | 9 | .16 | .02 | .13 | <2 | 63.1 |
| E-36 | 3 | 582 | 1153 | 120 | 16.1 | 5 | 2 | 54 | 1.92 | 10 | <8 | 4 | 2 | 1 | 1.2 | 52 | 3 | 130 | .01 | .009 | 7 | 13 | .04 | 11 | <.01 | 5 | .09 | .01 | .05 | 2 | 3943.7 |
| RE E-36 | 4 | 591 | 1176 | 119 | 16.5 | 4 | 3 | 55 | 1.95 | 14 | <8 | 4 | 2 | 1 | 1.0 | 53 | <3 | 134 | .01 | .009 | 7 | 11 | .04 | 11 | <.01 | 5 | .09 | .01 | .05 | 2 | 3452.9 |
| E-37 | 2 | 9 | 36 | 12 | .5 | 1 | <1 | 19 | 1.58 | 2 | <8 | <2 | 6 | 30 | <.5 | <3 | <3 | 6 | .01 | .018 | 33 | 2 | .01 | 34 | <.01 | 5 | .12 | .02 | .13 | <2 | 451.6 |
| E-38 | 3 | 37 | 267 | 50 | 43.0 | 3 | <1 | 20 | 1.89 | 7 | <8 | 3 | 3 | 3 | <.5 | 30 | 6 | 23 | .01 | .018 | 14 | <1 | .03 | 20 | <.01 | 7 | .10 | .01 | .08 | 2 | 1841.7 |
| E-39 | 3 | 84 | 525 | 19 | 5.4 | 1 | <1 | 20 | 1.13 | 2 | <8 | <2 | 3 | 3 | <.5 | 3 | 7 | 6 | <.01 | .013 | 6 | <1 | .01 | 11 | <.01 | 6 | .07 | .01 | .08 | 2 | 540.7 |
| E-40 | 1 | 14 | 84 | 11 | .5 | 2 | <1 | 32 | 1.03 | <2 | <8 | <2 | 4 | 15 | <.5 | <3 | <3 | 6 | .01 | .015 | 20 | <1 | .04 | 51 | .01 | 3 | .20 | .03 | .14 | <2 | 80.0 |
| STANDARD DS5/AU-R | 12 | 143 | 25 | 129 | .4 | 26 | 11 | 763 | 3.03 | 17 | 10 | <2 | 3 | 49 | 5.3 | 5 | 7 | 62 | .72 | .097 | 12 | 191 | .68 | 141 | .11 | 15 | 2.00 | .04 | .15 | 6 | 465.0 |

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

## GEOCHEMICAL ANALYSIS CERTIFICATE

Ruby Red Resources Inc. PROJECT EDDY File # A404155
207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au* ppb |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| SI | 1 | 1 | <3 | 3 | <.3 | <1 | <1 | <2 | .10 | 2 | <8 | <2 | <2 | 5 | <.5 | <3 | <3 | <1 | .25 | <.001 | <1 | <1 | <.01 | 6 | <.01 | <3 | .02 | .90 | .01 | <2 | <.5 |
| E 41 | 3 | 4 | <3 | 8 | .3 | 12 | 6 | 37 | 1.89 | 2 | <8 | <2 | 7 | 2 | <.5 | <3 | 3 | 3 | <.01 | .017 | 24 | 14 | .03 | 19 | <.01 | 6 | .27 | .06 | .09 | 6 | 9.8 |
| E 42 | 1 | 4 | 3 | 12 | <.3 | 8 | 2 | 109 | 2.03 | <2 | <8 | <2 | 6 | 7 | <.5 | <3 | 5 | 3 | .01 | .016 | 18 | 9 | .01 | 27 | <.01 | 8 | .25 | .08 | .03 | <2 | 8.7 |
| E 43 | 13 | 60 | 29 | 76 | 1.5 | 26 | 9 | 223 | 2.66 | 38 | <8 | <2 | 4 | 12 | .7 | 4 | 3 | 31 | .23 | .042 | 6 | 25 | .24 | 76 | .01 | 10 | .65 | .03 | .20 | 4 | 230.2 |
| E 44 | 4 | 6 | 26 | 9 | .3 | 2 | <1 | 20 | 1.17 | 4 | <8 | <2 | 6 | 2 | <.5 | <3 | 4 | 3 | .01 | .008 | 11 | 5 | .01 | 10 | <.01 | 3 | .17 | .07 | .02 | <2 | 1.2 |
| E 45 | 7 | 49 | 93 | 66 | .9 | 12 | 6 | 47 | 5.94 | 15 | <8 | <2 | 19 | 9 | <.5 | <3 | 7 | 12 | .02 | .029 | 29 | 14 | .02 | 87 | <.01 | 13 | .49 | .07 | .20 | <2 | 37.9 |
| E 46 | 21 | 36 | 1982 | 78 | 23.3 | 3 | <1 | 24 | 1.61 | 4 | <8 | <2 | <2 | 4 | 1.1 | <3 | 57 | 1 | <.01 | .003 | 2 | 14 | <.01 | 4 | <.01 | 4 | .02 | .02 | .01 | 4 | 31.5 |
| E 47 | 19 | 42 | 2258 | 80 | 31.0 | 8 | <1 | 21 | 1.39 | 2 | <8 | <2 | <2 | 11 | 1.3 | <3 | 76 | 1 | <.01 | .002 | 2 | 26 | <.01 | 3 | <.01 | 3 | .02 | .02 | .01 | 7 | 60.6 |
| E 48 | 171 | 22 | 1240 | 26 | 9.1 | 2 | <1 | 16 | 1.76 | 16 | <8 | <2 | 6 | 4 | <.5 | <3 | 20 | 2 | <.01 | .008 | 25 | 14 | <.01 | 6 | <.01 | <3 | .12 | .10 | .02 | <2 | 18.3 |
| RE E 48 | 173 | 22 | 1246 | 25 | 9.5 | 2 | <1 | 17 | 1.80 | 16 | <8 | <2 | 6 | 4 | <.5 | <3 | 20 | 2 | <.01 | .008 | 25 | 17 | <.01 | 6 | <.01 | <3 | .13 | .11 | .02 | 2 | 17.5 |
| E 49 | 3 | 10 | 38 | 11 | <.3 | 13 | 8 | 483 | 1.68 | 11 | <8 | <2 | 9 | 4 | <.5 | <3 | <3 | 3 | .05 | .022 | 31 | 18 | .03 | 41 | <.01 | 3 | .31 | .06 | .15 | 4 | 1.9 |
| E 50 | 3 | 248 | 66 | 75 | .5 | 13 | 8 | 27 | 1.74 | 18 | <8 | <2 | 27 | 3 | <.5 | <3 | 4 | 2 | <.01 | .008 | 82 | 15 | <.01 | 4 | <.01 | <3 | .15 | .08 | .01 | 2 | 8.6 |
| E 51 | 2 | 9 | 66 | 156 | .6 | 14 | 11 | 39 | 9.59 | 14 | <8 | <2 | 8 | 1 | <.5 | <3 | 15 | 11 | <.01 | .064 | 2 | 18 | .01 | 8 | <.01 | 22 | .34 | .01 | .08 | 6 | 11.1 |
| E 52 | 3 | 4 | 20 | 17 | .4 | 2 | <1 | 29 | 4.78 | 11 | <8 | <2 | <2 | 1 | <.5 | <3 | 6 | 6 | <.01 | .013 | 1 | 11 | .01 | 10 | <.01 | 17 | .17 | .01 | .10 | <2 | 9.1 |
| E 53 | 2 | 3 | 3 | 3 | <.3 | 6 | <1 | 20 | 1.12 | 2 | <8 | <2 | <2 | 1 | <.5 | <3 | <3 | 1 | <.01 | .005 | 1 | 21 | <.01 | 13 | <.01 | <3 | .12 | .01 | .09 | 6 | .7 |
| E 54 | 2 | 5 | 3 | 7 | <.3 | 5 | 4 | 95 | 1.87 | <2 | <8 | <2 | 2 | 1 | <.5 | <3 | <3 | 3 | <.01 | .013 | 2 | 12 | <.01 | 12 | <.01 | 4 | .13 | .01 | .07 | 2 | <.5 |
| STANDARD DS5/AU-R | 12 | 141 | 24 | 134 | .3 | 24 | 12 | 739 | 2.95 | 16 | <8 | <2 | 3 | 44 | 5.5 | 4 | 6 | 58 | .72 | .094 | 12 | 190 | .69 | 135 | .09 | 16 | 1.97 | .04 | .14 | 7 | 467.0 |

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

## GEOCHEMICAL ANALYSIS CERTIFICATE

Ruby Red Resources Inc. PROJECT EDDY File # A405350
207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au* ppb |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| SI | <1 | 1 | <3 | 1 | <.3 | <1 | <1 | 9 | .10 | <2 | <8 | <2 | <2 | 2 | <.5 | <3 | <3 | <1 | .09 | <.001 | <1 | 2 | <.01 | 3 | <.01 | 3 | .01 | .33 | <.01 | <2 | <.5 |
| E-55 | <1 | 16 | 5 | 8 | .9 | 2 | 2 | 63 | 2.66 | 2 | <8 | <2 | <2 | 11 | <.5 | <3 | <3 | 21 | .01 | .019 | 2 | 2 | <.01 | 28 | <.01 | 6 | .10 | .02 | .07 | <2 | 1004.9 |
| E-56 | 1 | 3 | 3 | 8 | <.3 | 2 | 11 | 62 | 3.03 | 11 | <8 | <2 | 3 | 1 | <.5 | <3 | <3 | 8 | .01 | .015 | 15 | 5 | .02 | 24 | <.01 | 5 | .31 | .01 | .19 | <2 | 18.0 |
| E-57 | <1 | 2 | 3 | 8 | <.3 | 3 | 25 | 71 | 3.13 | 11 | <8 | <2 | 2 | 1 | <.5 | <3 | <3 | 5 | <.01 | .010 | 13 | 3 | .01 | 11 | <.01 | <3 | .18 | .01 | .08 | <2 | 26.4 |
| E-58 | 1 | 5 | <3 | 19 | <.3 | 6 | 36 | 98 | 6.79 | 33 | <8 | <2 | 7 | 1 | <.5 | <3 | 5 | 9 | .01 | .035 | 71 | 6 | .02 | 13 | <.01 | <3 | .28 | .01 | .09 | <2 | 45.4 |
| E-59 | 2 | 13 | 7 | 44 | <.3 | 41 | 22 | 458 | 5.73 | 2 | <8 | <2 | 5 | 3 | <.5 | <3 | 3 | 4 | .01 | .027 | 15 | 3 | .02 | 26 | <.01 | <3 | .42 | .03 | .12 | <2 | 6.9 |
| E-60 | 2 | 17 | 244 | 14 | .6 | 3 | 1 | 67 | 2.16 | 6 | <8 | 2 | 4 | 2 | <.5 | <3 | <3 | 4 | <.01 | .011 | 12 | 4 | .02 | 23 | <.01 | 3 | .18 | .01 | .10 | <2 | 1412.8 |
| RE E-60 | 3 | 16 | 242 | 14 | .8 | 3 | 1 | 70 | 2.15 | 5 | <8 | <2 | 4 | 2 | <.5 | <3 | <3 | 4 | <.01 | .011 | 12 | 4 | .02 | 22 | <.01 | 3 | .17 | .01 | .10 | <2 | 1214.6 |
| E-61 | 1 | 7 | 8 | 7 | <.3 | 11 | 32 | 92 | 3.96 | 8 | <8 | <2 | 3 | 3 | <.5 | <3 | <3 | 15 | .04 | .092 | 8 | 5 | .03 | 33 | <.01 | <3 | .38 | .01 | .19 | <2 | 74.2 |
| E-62 | 1 | 9 | <3 | 4 | <.3 | 13 | 40 | 39 | 2.72 | 8 | <8 | <2 | 2 | 3 | <.5 | <3 | 3 | 3 | .01 | .026 | 12 | 4 | .01 | 29 | <.01 | <3 | .18 | .01 | .11 | <2 | 30.5 |
| E-63 | 1 | 2 | <3 | 6 | <.3 | 8 | 9 | 53 | 1.57 | <2 | <8 | <2 | 4 | 2 | <.5 | <3 | <3 | 3 | <.01 | .012 | 6 | 5 | .01 | 34 | <.01 | 3 | .24 | .01 | .14 | <2 | 12.4 |
| E-64 | <1 | 3 | <3 | 9 | <.3 | 11 | 19 | 58 | 2.30 | <2 | <8 | <2 | 14 | 2 | <.5 | <3 | <3 | 3 | <.01 | .025 | 27 | 6 | .01 | 32 | <.01 | <3 | .21 | <.01 | .12 | <2 | 9.6 |
| STANDARD DS5/AU-R | 13 | 146 | 24 | 138 | .3 | 24 | 12 | 750 | 3.03 | 19 | 8 | <2 | 2 | 45 | 5.5 | 5 | 7 | 58 | .72 | .092 | 11 | 183 | .68 | 136 | .10 | 16 | 1.97 | .04 | .14 | 5 | 484.6 |

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

# GEOCHEMICAL ANALYSIS CERTIFICATE

**Ruby Red Resources Inc. PROJECT EDDY File # A405351 Page 1**
207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| G-1 | 1.4 | 2.7 | 2.6 | 52 | <.1 | 5.4 | 4.6 | 655 | 2.24 | <.5 | 1.8 | 1.4 | 4.8 | 89 | <.1 | <.1 | .1 | 48 | .63 | .093 | 8 | 50.4 | .63 | 289 | .143 | 1 | 1.02 | .104 | .58 | .4 | .01 | 3.2 | .4 | <.05 | 6 | <.5 | 15.0 |
| EW1 000S | .5 | 22.9 | 14.2 | 78 | .2 | 11.4 | 9.6 | 219 | 2.72 | 3.1 | .3 | 18.9 | 2.3 | 7 | .1 | .2 | .3 | 63 | .14 | .072 | 7 | 8.8 | .28 | 66 | .094 | 2 | 1.65 | .015 | .08 | .1 | .04 | 2.5 | .1 | <.05 | 10 | <.5 | 15.0 |
| EW1 025S | .9 | 10.5 | 13.8 | 69 | .1 | 6.6 | 6.1 | 184 | 3.01 | 2.9 | .4 | 10.2 | 4.0 | 9 | .1 | .2 | .4 | 35 | .14 | .066 | 11 | 10.4 | .19 | 100 | .080 | 1 | 1.77 | .009 | .13 | .2 | .03 | 2.1 | .2 | <.05 | 10 | <.5 | 15.0 |
| EW1 050S | .6 | 57.4 | 12.1 | 89 | .1 | 18.0 | 16.9 | 367 | 3.58 | 3.0 | .9 | 1.7 | 3.2 | 12 | .1 | .1 | .3 | 77 | .19 | .083 | 13 | 9.7 | .38 | 111 | .153 | 1 | 2.67 | .018 | .19 | .2 | .03 | 2.4 | .3 | <.05 | 11 | <.5 | 15.0 |
| EW1 075S | .7 | 11.8 | 15.8 | 73 | .2 | 10.6 | 9.3 | 282 | 2.76 | 3.9 | .5 | 15.0 | 4.6 | 7 | .1 | .2 | .4 | 35 | .09 | .106 | 12 | 10.6 | .20 | 86 | .076 | 1 | 2.04 | .009 | .06 | .2 | .04 | 1.4 | .1 | <.05 | 9 | <.5 | 15.0 |
| EW1 100S | .7 | 11.2 | 10.9 | 86 | .1 | 12.1 | 8.7 | 196 | 2.15 | 3.3 | .6 | 37.0 | 5.3 | 4 | .1 | .2 | .3 | 20 | .04 | .037 | 15 | 11.7 | .39 | 79 | .044 | <1 | 1.58 | .004 | .05 | .1 | .03 | 1.1 | .1 | <.05 | 5 | <.5 | 15.0 |
| EW1 125S | .9 | 10.4 | 23.6 | 67 | .1 | 10.4 | 8.2 | 462 | 2.28 | 3.1 | .6 | 56.7 | 5.0 | 6 | .1 | .3 | .3 | 30 | .05 | .044 | 14 | 11.5 | .20 | 86 | .083 | 1 | 1.99 | .009 | .07 | .1 | .04 | 1.4 | .1 | <.05 | 8 | <.5 | 15.0 |
| EW1 150S | .5 | 10.5 | 9.1 | 42 | .1 | 9.4 | 6.9 | 98 | 1.75 | 2.8 | .5 | 13.2 | 4.7 | 4 | .1 | .1 | .2 | 21 | .03 | .030 | 13 | 10.5 | .25 | 52 | .046 | <1 | 1.71 | .006 | .05 | .1 | .03 | 1.5 | .1 | <.05 | 5 | <.5 | 15.0 |
| EW1 175S | .8 | 16.8 | 17.3 | 49 | .4 | 13.0 | 8.3 | 282 | 2.23 | 4.7 | .6 | 404.7 | 5.3 | 5 | .2 | .2 | .4 | 23 | .04 | .050 | 17 | 10.0 | .26 | 78 | .059 | <1 | 1.97 | .008 | .05 | .2 | .03 | 1.5 | .1 | <.05 | 6 | <.5 | 15.0 |
| EW1 200S | .6 | 11.0 | 10.0 | 51 | .2 | 10.1 | 9.4 | 201 | 2.03 | 4.3 | .7 | 11.8 | 5.9 | 4 | .2 | .2 | .3 | 24 | .03 | .051 | 16 | 10.6 | .25 | 80 | .052 | 1 | 2.19 | .012 | .04 | .1 | .04 | 1.6 | .1 | <.05 | 6 | <.5 | 15.0 |
| EW1 225S | .6 | 11.6 | 10.6 | 45 | .1 | 10.8 | 6.8 | 88 | 2.60 | 5.3 | .7 | 11.2 | 5.7 | 4 | .1 | .2 | .4 | 21 | .03 | .038 | 23 | 9.8 | .30 | 39 | .027 | <1 | 1.22 | .003 | .04 | .1 | .02 | 1.1 | .1 | <.05 | 5 | <.5 | 15.0 |
| EW1 250S | .7 | 13.7 | 7.2 | 51 | .1 | 14.3 | 8.8 | 149 | 2.50 | 4.0 | .7 | 21.4 | 6.3 | 6 | .1 | .2 | .3 | 24 | .03 | .041 | 22 | 11.5 | .40 | 53 | .032 | <1 | 1.50 | .004 | .04 | .1 | .02 | 1.2 | <.1 | <.05 | 5 | <.5 | 15.0 |
| EW1 275S | .7 | 11.5 | 5.4 | 31 | <.1 | 12.5 | 8.4 | 164 | 2.17 | 5.1 | .7 | 9.8 | 6.4 | 3 | .1 | .2 | .3 | 20 | .02 | .025 | 23 | 9.9 | .37 | 56 | .024 | <1 | 1.33 | .003 | .03 | .1 | .02 | 1.2 | <.1 | <.05 | 4 | <.5 | 15.0 |
| EW1 300S | .9 | 16.8 | 9.1 | 40 | .2 | 14.8 | 11.8 | 149 | 2.48 | 5.0 | .7 | 8.0 | 5.8 | 5 | .1 | .2 | .3 | 32 | .04 | .039 | 13 | 11.6 | .26 | 83 | .071 | <1 | 2.49 | .013 | .05 | .1 | .05 | 1.9 | .1 | <.05 | 7 | <.5 | 15.0 |
| EW2 350N | 1.0 | 17.8 | 18.1 | 92 | .2 | 17.0 | 9.9 | 281 | 2.57 | 4.2 | .9 | 5.6 | 5.8 | 6 | .2 | .2 | .3 | 26 | .05 | .078 | 14 | 14.0 | .33 | 70 | .087 | 1 | 2.75 | .008 | .07 | .2 | .05 | 1.6 | .1 | <.05 | 7 | <.5 | 15.0 |
| EW2 325N | .8 | 8.1 | 13.3 | 80 | .1 | 10.5 | 6.9 | 186 | 2.55 | 2.5 | .7 | 1.1 | 5.6 | 5 | .2 | .2 | .3 | 30 | .07 | .081 | 10 | 12.1 | .23 | 67 | .095 | 1 | 2.37 | .008 | .05 | .2 | .07 | 1.4 | .1 | <.05 | 9 | <.5 | 7.5 |
| RE EW2 325N | .8 | 8.5 | 12.9 | 83 | .1 | 10.4 | 7.7 | 187 | 2.61 | 2.8 | .7 | <.5 | 5.5 | 5 | .1 | .2 | .4 | 29 | .06 | .087 | 10 | 12.1 | .24 | 67 | .094 | 1 | 2.38 | .008 | .06 | .1 | .05 | 1.4 | .1 | <.05 | 9 | <.5 | 7.5 |
| EW2 300N | .8 | 11.4 | 13.4 | 97 | .1 | 10.6 | 7.5 | 199 | 3.04 | 2.7 | .7 | 3.7 | 3.6 | 10 | .2 | .1 | .3 | 34 | .10 | .116 | 9 | 12.5 | .23 | 73 | .112 | 2 | 2.69 | .011 | .06 | .2 | .05 | 1.3 | .1 | <.05 | 12 | <.5 | 15.0 |
| EW2 275N | .8 | 10.4 | 17.3 | 43 | .1 | 8.0 | 4.4 | 74 | 2.54 | 3.9 | 1.3 | 6.2 | 4.6 | 9 | .1 | .3 | .3 | 24 | .11 | .052 | 23 | 10.2 | .19 | 37 | .044 | <1 | 1.52 | .005 | .05 | .1 | .05 | 1.3 | .1 | <.05 | 7 | <.5 | 15.0 |
| EW2 250N | .8 | 13.1 | 12.8 | 70 | .2 | 14.5 | 9.2 | 498 | 2.27 | 3.5 | .6 | 22.5 | 6.5 | 5 | .1 | .2 | .3 | 23 | .05 | .042 | 20 | 10.8 | .27 | 94 | .053 | 1 | 1.96 | .008 | .06 | .2 | .03 | 1.6 | .1 | <.05 | 6 | <.5 | 15.0 |
| EW2 225N | .9 | 17.2 | 16.7 | 62 | .3 | 13.0 | 10.5 | 246 | 2.40 | 4.5 | .7 | 79.7 | 6.8 | 4 | .1 | .2 | .4 | 22 | .02 | .041 | 19 | 10.4 | .26 | 59 | .055 | <1 | 1.86 | .006 | .05 | .1 | .04 | 1.6 | .1 | <.05 | 6 | <.5 | 15.0 |
| EW2 200N | .8 | 13.6 | 16.0 | 73 | .3 | 13.2 | 10.1 | 410 | 2.34 | 3.5 | .6 | 17.2 | 5.3 | 6 | .1 | .2 | .4 | 26 | .04 | .047 | 17 | 13.6 | .27 | 98 | .058 | 1 | 2.07 | .006 | .07 | .1 | .03 | 1.6 | .1 | <.05 | 7 | <.5 | 15.0 |
| EW2 175N | .9 | 13.7 | 12.4 | 75 | .3 | 12.9 | 10.8 | 763 | 2.27 | 3.8 | .7 | 9.4 | 5.7 | 5 | .1 | .2 | .3 | 29 | .04 | .082 | 14 | 11.9 | .25 | 70 | .076 | 2 | 2.32 | .008 | .05 | .1 | .04 | 1.8 | .1 | <.05 | 7 | <.5 | 15.0 |
| EW2 150N | .9 | 12.0 | 14.1 | 60 | .3 | 9.1 | 9.1 | 596 | 2.43 | 3.4 | .7 | 52.6 | 5.6 | 5 | .1 | .2 | .4 | 31 | .04 | .063 | 12 | 11.4 | .15 | 71 | .069 | <1 | 2.10 | .009 | .06 | .2 | .04 | 1.7 | .1 | <.05 | 8 | <.5 | 15.0 |
| EW2 125N | 1.1 | 18.5 | 10.9 | 42 | .2 | 13.2 | 12.7 | 462 | 2.09 | 7.4 | 1.1 | 3.7 | 5.4 | 7 | .2 | .2 | .3 | 24 | .05 | .092 | 6 | 8.7 | .16 | 91 | .120 | 1 | 3.84 | .015 | .04 | .1 | .07 | 1.9 | .1 | <.05 | 9 | <.5 | 15.0 |
| EW2 100N | 1.0 | 23.5 | 11.0 | 33 | .1 | 15.1 | 12.5 | 236 | 2.22 | 5.4 | 1.1 | 8.6 | 6.4 | 6 | .1 | .2 | .3 | 28 | .04 | .061 | 5 | 9.1 | .15 | 82 | .129 | 1 | 3.99 | .015 | .03 | .2 | .05 | 2.2 | .1 | <.05 | 9 | <.5 | 15.0 |
| EW2 075N | .9 | 17.8 | 8.4 | 43 | .1 | 14.6 | 8.6 | 224 | 2.54 | 5.4 | .8 | 16.7 | 7.0 | 5 | .1 | .2 | .4 | 30 | .03 | .038 | 24 | 12.4 | .32 | 68 | .042 | <1 | 1.83 | .004 | .04 | .1 | .03 | 1.4 | .1 | <.05 | 6 | <.5 | 15.0 |
| EW2 050N | .9 | 18.3 | 10.7 | 42 | .2 | 15.3 | 11.3 | 258 | 2.59 | 5.1 | .8 | 6.4 | 6.3 | 6 | .1 | .2 | .4 | 32 | .05 | .044 | 13 | 12.3 | .26 | 83 | .089 | 1 | 2.57 | .010 | .05 | .2 | .04 | 1.9 | .1 | <.05 | 8 | <.5 | 15.0 |
| EW2 025N | 1.2 | 14.2 | 9.2 | 36 | .1 | 14.1 | 8.6 | 110 | 2.69 | 4.3 | .7 | 4.8 | 6.2 | 6 | .1 | .2 | .3 | 29 | .03 | .039 | 16 | 11.4 | .32 | 84 | .067 | 1 | 2.08 | .008 | .06 | .2 | .05 | 1.6 | .1 | <.05 | 8 | <.5 | 15.0 |
| EW2 000N | 1.0 | 14.7 | 9.9 | 44 | .1 | 12.7 | 9.6 | 421 | 2.46 | 5.3 | .8 | 6.5 | 6.5 | 4 | .1 | .2 | .4 | 26 | .03 | .039 | 16 | 11.7 | .26 | 71 | .058 | 1 | 2.11 | .006 | .05 | .2 | .06 | 1.8 | .1 | <.05 | 7 | <.5 | 15.0 |
| EW3 000S | 1.0 | 12.1 | 16.3 | 148 | .1 | 10.4 | 9.2 | 279 | 2.27 | 3.7 | .8 | 1.0 | 4.3 | 9 | .2 | .2 | .3 | 28 | .06 | .138 | 10 | 10.7 | .16 | 73 | .103 | 1 | 2.33 | .011 | .07 | .2 | .06 | 1.7 | .1 | <.05 | 9 | <.5 | 15.0 |
| EW3 025S | .7 | 13.0 | 15.8 | 67 | .1 | 11.4 | 7.3 | 184 | 2.33 | 3.4 | .8 | 46.3 | 3.7 | 9 | .2 | .3 | .4 | 21 | .09 | .045 | 21 | 10.0 | .22 | 56 | .042 | <1 | 1.08 | .006 | .05 | .1 | .02 | 1.2 | .1 | <.05 | 6 | <.5 | 15.0 |
| EW3 050S | .8 | 14.4 | 14.7 | 90 | .3 | 13.6 | 8.0 | 130 | 1.85 | 3.6 | 1.2 | 3.1 | 4.7 | 6 | .2 | .1 | .3 | 20 | .05 | .094 | 9 | 9.3 | .18 | 50 | .094 | <1 | 2.95 | .012 | .04 | .1 | .06 | 1.5 | .1 | <.05 | 7 | <.5 | 15.0 |
| EW3 075S | .9 | 23.7 | 19.1 | 87 | .5 | 20.0 | 14.9 | 156 | 2.28 | 4.7 | 1.5 | 5.0 | 6.5 | 7 | .1 | .2 | .3 | 27 | .05 | .067 | 13 | 14.1 | .25 | 100 | .105 | 2 | 3.75 | .013 | .05 | .1 | .08 | 2.4 | .1 | <.05 | 9 | <.5 | 15.0 |
| EW3 100S | 1.0 | 13.6 | 14.8 | 82 | .2 | 15.6 | 11.0 | 413 | 2.29 | 4.0 | .8 | 19.9 | 5.2 | 5 | .1 | .2 | .3 | 26 | .04 | .050 | 11 | 10.9 | .21 | 97 | .096 | 1 | 2.67 | .010 | .05 | .2 | .05 | 1.9 | .1 | <.05 | 8 | <.5 | 15.0 |
| STANDARD DS5 | 12.3 | 145.1 | 26.0 | 134 | .3 | 24.4 | 11.8 | 747 | 3.03 | 18.3 | 5.9 | 42.0 | 2.7 | 46 | 5.4 | 3.9 | 5.9 | 58 | .74 | .103 | 12 | 189.8 | .70 | 137 | .094 | 18 | 2.00 | .033 | .14 | 4.9 | .18 | 3.5 | 1.0 | <.05 | 7 | 4.8 | 15.0 |

GROUP 1DX - 15.00 GM SAMPLE LEACHED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 300 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA DATE RECEIVED: SEP 9 2004 DATE REPORT MAILED: Sept. 27/04

BRITISH COLUMBIA CERTIFIED ASSAYER
Clarence Leong

ACME ANALYTICAL

## Ruby Red Resources Inc. PROJECT EDDY FILE # A405351



ACME ANALYTICAL

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| G-1 | 1.3 | 1.9 | 2.1 | 43 | <.1 | 4.5 | 4.2 | 566 | 1.73 | <.5 | 1.8 | <.5 | 4.3 | 73 | <.1 | <.1 | .1 | 41 | .51 | .082 | 7 | 43.2 | .57 | 254 | .140 | 2 | .92 | .096 | .50 | .4 | <.01 | 2.4 | .3 | <.05 | 5 | <.5 | 15.0 |
| EW3 125S | 1.0 | 7.5 | 14.3 | 43 | .1 | 8.8 | 8.0 | 243 | 2.03 | 3.4 | .4 | 18.6 | 3.8 | 5 | .1 | .2 | .4 | 29 | .04 | .034 | 12 | 8.5 | .14 | 65 | .065 | 2 | 1.56 | .009 | .04 | .1 | .03 | 1.1 | .1 | <.05 | 7 | <.5 | 15.0 |
| EW3 150S | .9 | 21.6 | 9.8 | 42 | .2 | 16.0 | 10.0 | 175 | 2.25 | 5.4 | .9 | 19.4 | 8.0 | 4 | .1 | .3 | .4 | 21 | .03 | .044 | 22 | 12.4 | .36 | 78 | .040 | 2 | 1.78 | .004 | .05 | .1 | .04 | 1.5 | .1 | <.05 | 5 | <.5 | 15.0 |
| EW3 175S | 1.1 | 22.1 | 11.8 | 38 | .1 | 15.6 | 13.5 | 261 | 2.01 | 4.8 | .9 | 5.1 | 5.7 | 7 | .1 | .2 | .3 | 28 | .05 | .041 | 8 | 10.3 | .18 | 90 | .109 | 1 | 3.12 | .013 | .04 | .2 | .07 | 1.9 | .1 | <.05 | 7 | .5 | 15.0 |
| EW3 200S | 1.0 | 23.5 | 13.6 | 52 | .2 | 15.8 | 10.9 | 237 | 2.33 | 6.3 | 1.0 | 11.3 | 7.2 | 5 | .1 | .2 | .4 | 29 | .03 | .052 | 9 | 12.2 | .21 | 103 | .112 | 2 | 3.39 | .011 | .05 | .2 | .08 | 2.0 | .1 | <.05 | 8 | <.5 | 15.0 |
| EW3 225S | 1.0 | 15.2 | 11.1 | 38 | .1 | 14.0 | 11.9 | 150 | 2.27 | 4.9 | .8 | 19.3 | 6.4 | 6 | .1 | .2 | .4 | 30 | .03 | .033 | 15 | 11.3 | .24 | 81 | .082 | 1 | 2.54 | .008 | .05 | .2 | .04 | 2.0 | .1 | <.05 | 6 | <.5 | 15.0 |
| EW3 250S | 1.1 | 22.1 | 10.5 | 42 | .1 | 10.3 | 7.1 | 296 | 2.04 | 5.4 | 1.2 | 5.2 | 5.4 | 5 | .1 | .2 | .3 | 29 | .04 | .095 | 7 | 9.8 | .17 | 60 | .132 | 3 | 3.85 | .013 | .04 | .2 | .09 | 2.4 | .1 | <.05 | 9 | .5 | 15.0 |
| EW3 275S | 1.0 | 24.5 | 11.5 | 41 | .1 | 15.1 | 9.7 | 179 | 2.13 | 4.4 | 1.2 | 9.0 | 5.8 | 6 | .1 | .2 | .3 | 30 | .04 | .062 | 12 | 11.5 | .25 | 76 | .105 | 1 | 3.51 | .012 | .05 | .2 | .07 | 2.7 | .1 | <.05 | 8 | <.5 | 15.0 |
| EW3 300S | 1.0 | 15.8 | 10.6 | 48 | .1 | 14.5 | 9.3 | 177 | 2.29 | 4.8 | .8 | 7.0 | 7.2 | 4 | .1 | .2 | .3 | 28 | .03 | .041 | 20 | 14.2 | .37 | 89 | .047 | 1 | 2.17 | .006 | .05 | .1 | .04 | 1.8 | .1 | <.05 | 6 | <.5 | 15.0 |
| NW1 000S | .4 | 5.2 | 8.8 | 33 | <.1 | 7.1 | 5.2 | 114 | 1.30 | 1.4 | .5 | 2.3 | 4.5 | 4 | <.1 | .1 | .2 | 11 | .03 | .018 | 21 | 7.5 | .30 | 38 | .014 | 1 | .90 | .003 | .03 | .1 | .01 | .7 | <.1 | <.05 | 3 | <.5 | 15.0 |
| NW1 025S | .9 | 12.7 | 20.5 | 41 | .1 | 21.8 | 12.8 | 127 | 2.33 | 3.2 | 1.1 | <.5 | 7.0 | 11 | .1 | .1 | .5 | 23 | .07 | .036 | 21 | 13.4 | .34 | 175 | .047 | 1 | 2.65 | .009 | .06 | .2 | .06 | 1.5 | .1 | <.05 | 7 | <.5 | 15.0 |
| NW1 050S | .6 | 7.2 | 13.0 | 34 | .1 | 6.8 | 5.7 | 111 | 2.32 | 3.4 | .8 | 5.4 | 4.9 | 7 | <.1 | .1 | .3 | 28 | .07 | .135 | 17 | 10.0 | .16 | 62 | .078 | 1 | 1.96 | .010 | .04 | .2 | .03 | 1.6 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW1 075S | .6 | 6.9 | 10.4 | 26 | <.1 | 7.6 | 5.2 | 92 | 1.80 | 2.9 | .6 | .8 | 4.8 | 5 | <.1 | .1 | .3 | 19 | .04 | .039 | 15 | 8.9 | .24 | 67 | .038 | <1 | 1.63 | .008 | .04 | .1 | .03 | 1.2 | <.1 | <.05 | 5 | <.5 | 15.0 |
| NW1 100S | .7 | 11.3 | 18.1 | 23 | .1 | 11.8 | 10.7 | 73 | 2.23 | 2.7 | 1.4 | 1.3 | 5.7 | 9 | .1 | .1 | .3 | 29 | .07 | .071 | 9 | 10.2 | .10 | 101 | .111 | 1 | 4.00 | .016 | .03 | .1 | .07 | 2.1 | .1 | <.05 | 10 | <.5 | 15.0 |
| NW1 125S | .9 | 9.1 | 13.6 | 24 | .1 | 7.4 | 6.0 | 106 | 2.31 | 4.2 | .8 | <.5 | 4.1 | 11 | .1 | .3 | .3 | 33 | .16 | .149 | 6 | 10.7 | .09 | 55 | .105 | 1 | 4.14 | .015 | .03 | .2 | .10 | 1.9 | .1 | <.05 | 9 | .5 | 15.0 |
| NW1 150S | .7 | 9.0 | 10.4 | 25 | .1 | 12.3 | 17.8 | 304 | 2.37 | 4.3 | .9 | 1.6 | 4.3 | 9 | .1 | .2 | .3 | 34 | .07 | .190 | 5 | 11.0 | .18 | 74 | .136 | 1 | 4.80 | .018 | .04 | .2 | .06 | 2.2 | <.1 | <.05 | 10 | <.5 | 15.0 |
| NW1 175S | .8 | 8.9 | 9.5 | 25 | .1 | 15.3 | 16.9 | 94 | 2.58 | 3.5 | .6 | 13.5 | 4.8 | 7 | .1 | .1 | .3 | 36 | .07 | .079 | 8 | 10.8 | .29 | 78 | .084 | 1 | 2.96 | .010 | .04 | .1 | .04 | 2.0 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW1 200S | 1.1 | 17.1 | 9.6 | 40 | .1 | 19.3 | 25.9 | 230 | 3.14 | 3.8 | .9 | 6.2 | 4.7 | 9 | .1 | .2 | .5 | 64 | .08 | .062 | 9 | 16.0 | .81 | 112 | .097 | 1 | 3.34 | .012 | .05 | .2 | .05 | 4.0 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW1 225S | .9 | 11.0 | 9.5 | 35 | .2 | 13.6 | 20.6 | 290 | 2.71 | 3.1 | .6 | 1.9 | 3.1 | 7 | .1 | .2 | .4 | 56 | .05 | .097 | 5 | 11.8 | .48 | 112 | .141 | 1 | 3.56 | .014 | .03 | .2 | .05 | 3.2 | .1 | <.05 | 11 | <.5 | 15.0 |
| NW1 250S | 1.2 | 27.9 | 13.8 | 58 | .3 | 20.0 | 27.1 | 294 | 3.40 | 4.4 | .8 | 3.3 | 4.5 | 10 | .1 | .2 | .5 | 58 | .11 | .133 | 7 | 16.4 | .70 | 91 | .128 | 3 | 3.94 | .014 | .05 | .2 | .05 | 3.9 | .1 | <.05 | 12 | <.5 | 7.5 |
| RE NW1 250S | 1.1 | 27.2 | 13.3 | 57 | .3 | 20.3 | 26.1 | 303 | 3.22 | 4.4 | .8 | 4.1 | 4.5 | 10 | .2 | .2 | .5 | 60 | .11 | .125 | 8 | 16.2 | .69 | 86 | .131 | 2 | 3.98 | .013 | .06 | .2 | .05 | 4.0 | .1 | <.05 | 12 | .5 | 7.5 |
| NW1 275S | .8 | 29.3 | 11.3 | 60 | .3 | 25.7 | 19.9 | 316 | 2.87 | 3.7 | 1.0 | 184.3 | 5.6 | 13 | .1 | .2 | .5 | 33 | .20 | .071 | 11 | 12.2 | .43 | 122 | .088 | 2 | 2.95 | .012 | .06 | .1 | .05 | 3.3 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW1 300S | .9 | 21.3 | 12.3 | 60 | .3 | 20.7 | 16.7 | 340 | 2.70 | 3.4 | .7 | 57.2 | 4.8 | 8 | .2 | .2 | .4 | 40 | .12 | .062 | 14 | 13.6 | .68 | 178 | .073 | 1 | 2.42 | .010 | .06 | .1 | .03 | 2.6 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW1 325S | 1.2 | 24.4 | 33.1 | 84 | .3 | 20.1 | 16.9 | 534 | 2.90 | 4.4 | .8 | 42.0 | 5.7 | 14 | .4 | .2 | .5 | 37 | .22 | .065 | 11 | 14.1 | .48 | 198 | .092 | 3 | 2.89 | .012 | .07 | .2 | .05 | 2.3 | .1 | <.05 | 8 | .5 | 15.0 |
| NW1 350S | 1.1 | 40.0 | 13.2 | 62 | .4 | 21.1 | 17.3 | 418 | 3.40 | 4.0 | .5 | 44.8 | 4.7 | 7 | .2 | .2 | .4 | 61 | .09 | .061 | 13 | 15.5 | .62 | 125 | .075 | 1 | 2.45 | .008 | .07 | .3 | .04 | 3.1 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW1 375S | .9 | 93.2 | 23.6 | 88 | .3 | 19.5 | 20.8 | 5057 | 3.07 | 4.3 | 1.2 | 9.9 | 4.8 | 19 | .5 | .2 | .5 | 60 | .36 | .091 | 14 | 13.8 | .58 | 206 | .081 | 1 | 2.36 | .011 | .09 | .1 | .03 | 3.5 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW1 400S | 1.3 | 32.3 | 22.0 | 59 | .1 | 20.4 | 22.3 | 590 | 3.46 | 5.3 | 1.0 | 32.8 | 8.6 | 5 | .1 | .2 | .7 | 48 | .05 | .039 | 20 | 15.5 | .82 | 103 | .048 | 1 | 2.54 | .004 | .06 | .2 | .05 | 2.8 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW1 425S | 1.4 | 58.0 | 30.4 | 82 | .3 | 27.8 | 23.6 | 540 | 3.62 | 8.1 | 2.0 | 55.9 | 11.3 | 6 | .1 | .3 | .7 | 43 | .04 | .047 | 21 | 14.8 | .70 | 105 | .070 | 1 | 3.08 | .006 | .06 | .2 | .06 | 3.6 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW1 450S | 1.0 | 21.8 | 15.5 | 63 | .2 | 18.9 | 14.0 | 435 | 2.48 | 4.9 | .7 | 15.4 | 5.6 | 9 | .2 | .2 | .4 | 36 | .06 | .070 | 9 | 12.0 | .32 | 124 | .105 | 2 | 2.95 | .012 | .06 | .2 | .03 | 2.1 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW1 475S | 1.0 | 11.4 | 22.5 | 81 | .1 | 11.6 | 10.4 | 541 | 2.30 | 3.5 | .5 | 1.6 | 4.0 | 15 | .2 | .2 | .5 | 37 | .20 | .080 | 8 | 10.0 | .15 | 123 | .125 | 2 | 2.10 | .015 | .06 | .2 | .02 | 1.8 | .1 | <.05 | 10 | <.5 | 7.5 |
| NW1 500S | .5 | 15.7 | 14.7 | 65 | .5 | 9.2 | 7.5 | 226 | 1.90 | 2.4 | .6 | 2.7 | 3.0 | 11 | .1 | .2 | .4 | 34 | .14 | .112 | 8 | 8.9 | .12 | 97 | .093 | 1 | 1.83 | .019 | .05 | .1 | .05 | 1.5 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW1 525S | .7 | 30.5 | 13.2 | 81 | .1 | 13.5 | 14.3 | 280 | 2.59 | 3.2 | .5 | 5.1 | 4.1 | 8 | .1 | .2 | .3 | 54 | .11 | .073 | 12 | 10.4 | .32 | 98 | .078 | 1 | 2.01 | .011 | .08 | .1 | .02 | 2.0 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW1 550S | .5 | 28.1 | 9.0 | 52 | .1 | 13.0 | 10.4 | 134 | 2.45 | 3.6 | .7 | 15.6 | 5.2 | 5 | <.1 | .2 | .3 | 40 | .06 | .070 | 14 | 10.2 | .36 | 60 | .055 | <1 | 1.87 | .007 | .04 | .1 | .02 | 2.1 | .1 | .06 | 6 | <.5 | 15.0 |
| NW1 575S | .6 | 52.8 | 16.5 | 53 | .1 | 18.6 | 12.2 | 481 | 2.33 | 2.6 | 2.1 | 5.1 | 5.1 | 19 | .1 | .2 | .3 | 40 | .20 | .038 | 25 | 15.7 | .60 | 94 | .027 | 1 | 2.14 | .010 | .05 | .1 | .03 | 2.7 | .1 | <.05 | 7 | <.5 | 15.0 |
| NW1 600S | .6 | 17.8 | 13.0 | 76 | .1 | 13.4 | 10.8 | 125 | 2.42 | 2.8 | .5 | 6.1 | 4.9 | 7 | <.1 | .2 | .3 | 35 | .07 | .062 | 15 | 12.0 | .31 | 103 | .061 | 1 | 1.96 | .008 | .05 | .1 | .02 | 1.9 | .1 | <.05 | 7 | <.5 | 15.0 |
| STANDARD DS5 | 13.4 | 145.1 | 25.9 | 140 | .3 | 26.3 | 12.7 | 832 | 3.04 | 18.9 | 6.3 | 43.8 | 2.9 | 47 | 5.7 | 3.9 | 6.1 | 62 | .72 | .090 | 12 | 196.2 | .68 | 140 | .099 | 18 | 1.95 | .032 | .13 | 4.8 | .19 | 3.4 | 1.1 | .06 | 7 | 4.9 | 15.0 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data FA

# Ruby Red Resources Inc. PROJECT EDDY FILE # A405351



ACME ANALYTICAL

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| G-1 | 1.4 | 2.5 | 2.1 | 49 | <.1 | 5.1 | 4.3 | 620 | 2.05 | <.5 | 1.8 | <.5 | 4.1 | 79 | <.1 | <.1 | .1 | 46 | .60 | .085 | 8 | 47.1 | .62 | 269 | .141 | <1 | 1.03 | .085 | .56 | .3 | <.01 | 2.8 | .3 | <.05 | 5 | <.5 | 15.0 |
| NW1 625S | .7 | 21.9 | 15.0 | 54 | .3 | 14.4 | 8.4 | 195 | 2.54 | 4.0 | .7 | 6.8 | 3.6 | 16 | .1 | .2 | .3 | 44 | .25 | .150 | 8 | 9.5 | .21 | 85 | .128 | 2 | 3.34 | .022 | .06 | .2 | .04 | 1.9 | .1 | <.05 | 11 | <.5 | 15.0 |
| NW1 650S | 1.1 | 19.6 | 15.3 | 70 | .3 | 14.5 | 10.7 | 177 | 2.29 | 3.3 | .8 | .5 | 3.8 | 7 | .1 | .2 | .3 | 33 | .07 | .148 | 7 | 8.7 | .17 | 88 | .131 | 1 | 4.14 | .016 | .05 | .2 | .05 | 2.3 | .1 | <.05 | 10 | <.5 | 15.0 |
| NW1 675S | .8 | 17.9 | 16.4 | 68 | .2 | 13.0 | 10.5 | 506 | 2.44 | 5.2 | .7 | 1.1 | 4.9 | 8 | .1 | .2 | .3 | 32 | .09 | .152 | 5 | 9.6 | .17 | 69 | .120 | 1 | 4.16 | .016 | .05 | .2 | .06 | 1.9 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW1 700S | .6 | 18.8 | 12.1 | 95 | .1 | 13.6 | 9.8 | 199 | 2.47 | 3.0 | .6 | 2.0 | 4.9 | 5 | .1 | .1 | .3 | 37 | .06 | .094 | 14 | 12.3 | .32 | 95 | .064 | 1 | 2.52 | .010 | .07 | .1 | .03 | 2.3 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW2 600N | .7 | 10.9 | 13.7 | 23 | .1 | 12.2 | 7.1 | 175 | 1.79 | 2.0 | 2.2 | <.5 | 4.8 | 16 | .1 | .1 | .4 | 24 | .16 | .017 | 34 | 10.5 | .24 | 104 | .036 | <1 | 1.86 | .010 | .05 | .1 | .03 | 1.9 | .1 | <.05 | 7 | <.5 | 15.0 |
| NW2 575N | .8 | 10.7 | 9.3 | 37 | <.1 | 15.2 | 12.6 | 134 | 2.36 | 3.9 | 1.1 | 4.5 | 6.6 | 6 | .1 | .2 | .3 | 21 | .06 | .076 | 14 | 10.1 | .37 | 82 | .079 | 1 | 3.04 | .010 | .05 | .1 | .04 | 2.0 | .1 | <.05 | 7 | <.5 | 15.0 |
| NW2 550N | 1.5 | 9.8 | 9.8 | 35 | <.1 | 18.1 | 14.2 | 300 | 2.83 | 5.0 | 1.6 | 1.6 | 7.4 | 4 | <.1 | .3 | .4 | 23 | .03 | .060 | 19 | 13.2 | .72 | 80 | .039 | 1 | 2.53 | .005 | .04 | .1 | .04 | 1.7 | .1 | <.05 | 6 | <.5 | 15.0 |
| NW2 525N | 1.6 | 9.0 | 11.2 | 37 | .1 | 16.6 | 21.5 | 291 | 2.77 | 4.4 | 1.0 | 1.7 | 5.4 | 6 | .1 | .2 | .4 | 34 | .06 | .074 | 10 | 11.6 | .31 | 99 | .100 | 1 | 2.85 | .012 | .06 | .2 | .04 | 2.2 | .1 | <.05 | 10 | <.5 | 15.0 |
| NW2 500N | 1.4 | 14.4 | 11.6 | 37 | .1 | 21.0 | 23.3 | 271 | 2.81 | 5.5 | 1.2 | 12.3 | 6.4 | 7 | .1 | .2 | .4 | 32 | .06 | .071 | 13 | 11.6 | .47 | 103 | .083 | 1 | 3.20 | .013 | .06 | .2 | .05 | 2.9 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW2 475N | 2.1 | 16.5 | 11.3 | 43 | .1 | 30.9 | 51.2 | 218 | 4.67 | 6.0 | 1.6 | 9.7 | 7.4 | 5 | <.1 | .3 | .7 | 69 | .04 | .070 | 11 | 19.5 | 1.13 | 93 | .070 | <1 | 3.77 | .007 | .06 | .1 | .04 | 7.0 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW2 450N | 1.4 | 21.2 | 10.2 | 42 | .1 | 24.6 | 37.2 | 257 | 4.35 | 4.0 | 1.0 | 9.8 | 5.3 | 7 | .1 | .3 | .6 | 82 | .07 | .049 | 13 | 19.8 | 1.26 | 97 | .075 | 1 | 3.39 | .008 | .06 | .2 | .03 | 6.1 | .1 | <.05 | 10 | <.5 | 15.0 |
| NW2 425N | 1.1 | 13.7 | 11.0 | 42 | .2 | 23.0 | 26.9 | 268 | 3.50 | 4.3 | .9 | 15.1 | 5.7 | 8 | .1 | .3 | .5 | 54 | .08 | .078 | 10 | 14.0 | .69 | 125 | .096 | 2 | 3.57 | .011 | .06 | .2 | .04 | 3.7 | .1 | .06 | 9 | <.5 | 15.0 |
| NW2 400N | 1.0 | 11.4 | 12.4 | 41 | .2 | 19.9 | 15.5 | 514 | 2.85 | 2.8 | 1.0 | 95.4 | 5.2 | 15 | .1 | .2 | .5 | 37 | .21 | .041 | 13 | 10.8 | .36 | 152 | .102 | 2 | 2.86 | .016 | .07 | .1 | .04 | 2.4 | .1 | <.05 | 10 | <.5 | 15.0 |
| NW2 375N | 1.6 | 17.6 | 16.7 | 75 | .6 | 22.0 | 18.1 | 485 | 3.19 | 4.2 | .8 | 91.0 | 6.4 | 9 | .2 | .2 | .6 | 42 | .12 | .038 | 14 | 12.6 | .36 | 195 | .106 | 2 | 3.19 | .014 | .08 | .1 | .05 | 2.4 | .1 | <.05 | 10 | <.5 | 15.0 |
| NW2 350N | 1.6 | 25.5 | 28.2 | 86 | .2 | 20.4 | 22.7 | 2700 | 3.47 | 4.2 | 1.0 | 17.8 | 6.5 | 10 | .4 | .2 | .7 | 44 | .08 | .038 | 19 | 15.6 | .56 | 214 | .083 | 2 | 2.59 | .008 | .08 | .1 | .05 | 2.9 | .1 | <.05 | 9 | .5 | 7.5 |
| RE NW2 350N | 1.6 | 24.1 | 26.5 | 80 | .2 | 20.0 | 22.2 | 2707 | 3.27 | 3.8 | 1.0 | 26.6 | 6.1 | 9 | .4 | .3 | .7 | 40 | .09 | .040 | 17 | 13.9 | .58 | 215 | .077 | 3 | 2.44 | .007 | .08 | .1 | .05 | 3.0 | .2 | <.05 | 9 | <.5 | 7.5 |
| NW2 325N | 1.0 | 166.6 | 17.2 | 73 | .4 | 21.2 | 16.6 | 361 | 3.39 | 6.9 | 1.1 | 33.2 | 6.1 | 7 | .2 | .3 | .4 | 56 | .07 | .118 | 9 | 14.0 | .53 | 127 | .123 | 3 | 4.70 | .011 | .07 | .3 | .06 | 4.0 | .1 | <.05 | 11 | .7 | 15.0 |
| NW2 300N | 1.1 | 26.8 | 12.5 | 52 | .2 | 17.2 | 15.5 | 389 | 3.27 | 3.7 | .7 | 14.0 | 5.1 | 7 | .1 | .2 | .5 | 49 | .09 | .035 | 20 | 14.7 | .78 | 89 | .042 | 1 | 2.11 | .006 | .06 | .2 | .03 | 3.8 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW2 275N | 1.2 | 59.5 | 22.5 | 66 | .2 | 24.6 | 24.0 | 324 | 3.77 | 7.6 | 1.9 | 62.8 | 11.8 | 5 | .1 | .3 | .7 | 40 | .04 | .046 | 26 | 14.7 | .88 | 90 | .049 | 1 | 2.91 | .004 | .07 | .2 | .03 | 4.0 | .1 | <.05 | 7 | <.5 | 15.0 |
| NW2 250N | 1.9 | 64.3 | 73.8 | 121 | .3 | 42.7 | 36.9 | 1364 | 4.20 | 11.7 | 2.2 | 30.5 | 8.2 | 9 | .2 | .4 | .9 | 45 | .10 | .054 | 34 | 17.7 | .79 | 106 | .045 | 1 | 3.25 | .006 | .09 | .2 | .04 | 3.7 | .1 | <.05 | 9 | .5 | 15.0 |
| NW2 225N | 1.3 | 17.2 | 22.0 | 84 | .1 | 15.9 | 12.6 | 428 | 2.87 | 4.8 | .7 | 11.7 | 5.8 | 8 | .1 | .3 | .5 | 40 | .10 | .035 | 14 | 12.5 | .35 | 129 | .087 | 1 | 2.41 | .011 | .07 | .2 | .03 | 1.9 | .1 | <.05 | 10 | <.5 | 15.0 |
| NW2 200N | .9 | 17.7 | 19.5 | 64 | .3 | 12.4 | 8.6 | 971 | 2.60 | 3.7 | .7 | 5.2 | 4.7 | 12 | .2 | .2 | .4 | 36 | .10 | .085 | 9 | 10.3 | .19 | 170 | .142 | 1 | 4.01 | .020 | .06 | .2 | .04 | 2.0 | .1 | .07 | 11 | <.5 | 15.0 |
| NW2 175N | .6 | 14.3 | 13.7 | 56 | .1 | 11.7 | 8.1 | 209 | 2.52 | 3.1 | .7 | 11.4 | 5.1 | 7 | .1 | .2 | .3 | 33 | .09 | .086 | 12 | 12.8 | .30 | 101 | .077 | 1 | 2.62 | .013 | .07 | .1 | .04 | 2.3 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW2 150N | .6 | 24.8 | 13.4 | 57 | .1 | 16.9 | 12.5 | 186 | 2.53 | 3.3 | .6 | 14.3 | 5.9 | 6 | <.1 | .2 | .3 | 29 | .06 | .068 | 16 | 12.5 | .41 | 98 | .052 | 1 | 2.31 | .009 | .06 | .1 | .04 | 2.0 | .1 | <.05 | 7 | <.5 | 15.0 |
| NW2 125N | .7 | 23.2 | 12.7 | 50 | .1 | 15.3 | 9.7 | 1071 | 2.17 | 2.5 | 1.2 | 29.4 | 4.7 | 14 | .1 | .2 | .3 | 35 | .18 | .026 | 19 | 13.0 | .46 | 79 | .034 | 1 | 1.88 | .010 | .06 | .1 | .01 | 2.1 | .1 | <.05 | 6 | <.5 | 15.0 |
| NW2 100N | .8 | 18.2 | 16.5 | 55 | .1 | 10.2 | 6.6 | 147 | 2.75 | 4.3 | .4 | 3.6 | 4.3 | 7 | .1 | .3 | .4 | 40 | .08 | .093 | 13 | 10.0 | .24 | 51 | .064 | 1 | 1.53 | .008 | .05 | .2 | .02 | 1.6 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW2 075N | .8 | 18.4 | 11.8 | 72 | .1 | 13.9 | 9.4 | 374 | 2.32 | 3.8 | .5 | 3.1 | 4.4 | 8 | .1 | .2 | .3 | 38 | .08 | .091 | 12 | 10.8 | .25 | 98 | .084 | 2 | 2.49 | .011 | .07 | .2 | .03 | 2.1 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW2 050N | .5 | 24.9 | 9.4 | 42 | .1 | 11.5 | 8.0 | 240 | 1.98 | 3.1 | .7 | 12.6 | 5.9 | 4 | .1 | .1 | .3 | 25 | .05 | .049 | 20 | 8.4 | .39 | 54 | .034 | <1 | 1.44 | .005 | .05 | .1 | .01 | 1.7 | .1 | <.05 | 4 | <.5 | 15.0 |
| NW2 025N | 1.1 | 17.0 | 12.4 | 58 | .1 | 8.6 | 9.2 | 256 | 2.19 | 3.5 | 1.0 | .7 | 4.5 | 5 | .1 | .2 | .2 | 36 | .05 | .211 | 5 | 9.2 | .11 | 49 | .149 | 2 | 5.06 | .018 | .04 | .2 | .06 | 2.7 | .1 | .07 | 11 | <.5 | 15.0 |
| NW2 000N | .9 | 26.9 | 14.5 | 51 | .2 | 11.7 | 7.6 | 253 | 1.98 | 4.3 | .9 | 1.6 | 4.1 | 9 | .1 | .2 | .2 | 31 | .09 | .149 | 5 | 7.8 | .15 | 70 | .143 | 2 | 3.85 | .018 | .05 | .2 | .05 | 2.2 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW3 000S | .9 | 10.3 | 14.7 | 61 | .1 | 14.0 | 12.2 | 290 | 2.43 | 4.5 | 1.2 | 2.0 | 5.3 | 9 | .1 | .3 | .3 | 33 | .08 | .085 | 10 | 11.1 | .26 | 107 | .121 | 2 | 3.70 | .013 | .06 | .2 | .06 | 2.5 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW3 025S | 1.3 | 9.9 | 11.8 | 34 | .1 | 12.6 | 10.9 | 87 | 2.54 | 3.9 | 1.2 | 2.1 | 5.2 | 7 | .1 | .2 | .3 | 38 | .06 | .073 | 6 | 11.6 | .20 | 66 | .142 | 1 | 4.37 | .017 | .04 | .2 | .10 | 2.2 | .1 | <.05 | 11 | <.5 | 15.0 |
| NW3 050S | .8 | 7.6 | 12.6 | 36 | <.1 | 16.7 | 17.8 | 416 | 2.29 | 3.0 | 1.9 | 11.7 | 5.1 | 17 | <.1 | .3 | .3 | 27 | .15 | .055 | 16 | 11.2 | .35 | 66 | .051 | 2 | 1.79 | .011 | .08 | .1 | .02 | 2.0 | .1 | .11 | 7 | <.5 | 7.5 |
| NW3 075S | 1.3 | 10.3 | 15.8 | 32 | .1 | 18.3 | 19.7 | 203 | 2.22 | 2.6 | 2.2 | .5 | 7.3 | 12 | .1 | .2 | .4 | 25 | .11 | .027 | 29 | 12.2 | .49 | 80 | .028 | 1 | 1.95 | .007 | .07 | .1 | .03 | 2.2 | .1 | <.05 | 7 | <.5 | 15.0 |
| STANDARD DS5 | 12.6 | 142.1 | 25.4 | 138 | .3 | 25.6 | 12.0 | 800 | 3.00 | 18.1 | 6.2 | 43.0 | 2.8 | 46 | 5.3 | 3.8 | 6.0 | 66 | .72 | .093 | 12 | 190.7 | .68 | 135 | .097 | 17 | 2.09 | .032 | .15 | 4.7 | .18 | 3.4 | 1.0 | <.05 | 7 | 5.0 | 15.0 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data FA

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| G-1 | 1.2 | 2.1 | 2.0 | 44 | <.1 | 4.7 | 4.0 | 542 | 1.80 | <.5 | 1.8 | <.5 | 4.0 | 76 | <.1 | <.1 | .1 | 41 | .53 | .078 | 7 | 44.5 | .55 | 257 | .126 | 1 | .92 | .082 | .54 | .3 | <.01 | 2.3 | .4 | <.05 | 5 | <.5 | 15.0 |
| NW3 100S | 1.5 | 10.9 | 12.7 | 53 | .1 | 15.4 | 13.2 | 195 | 2.56 | 3.8 | .8 | 5.2 | 5.8 | 8 | .1 | .2 | .3 | 32 | .07 | .082 | 10 | 12.2 | .23 | 98 | .090 | 2 | 3.05 | .011 | .06 | .2 | .06 | 2.1 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW3 125S | .8 | 16.8 | 13.6 | 52 | .1 | 15.3 | 15.8 | 238 | 2.22 | 4.0 | 1.0 | 20.4 | 7.4 | 6 | .1 | .2 | .4 | 23 | .05 | .050 | 17 | 11.8 | .39 | 96 | .058 | <1 | 2.49 | .009 | .05 | .2 | .05 | 1.6 | .1 | <.05 | 7 | <.5 | 7.5 |
| NW3 150S | 1.1 | 12.9 | 14.1 | 56 | .2 | 12.2 | 8.2 | 287 | 2.17 | 3.1 | .6 | 6.1 | 4.0 | 5 | .1 | .1 | .4 | 33 | .04 | .049 | 10 | 10.7 | .19 | 96 | .095 | 1 | 2.80 | .011 | .05 | .2 | .04 | 1.6 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW3 175S | 1.2 | 10.8 | 14.0 | 50 | .1 | 11.7 | 8.3 | 219 | 2.01 | 3.5 | .6 | 10.8 | 4.8 | 5 | .1 | .2 | .4 | 27 | .04 | .042 | 12 | 9.7 | .23 | 101 | .068 | <1 | 2.39 | .009 | .05 | .2 | .05 | 1.6 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW3 200S | .9 | 13.0 | 15.0 | 74 | .2 | 14.6 | 9.7 | 488 | 2.28 | 3.8 | .7 | 11.3 | 5.5 | 5 | .2 | .2 | .4 | 28 | .04 | .058 | 15 | 12.1 | .29 | 92 | .074 | <1 | 2.26 | .009 | .07 | .1 | .04 | 1.5 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW3 225S | 1.2 | 9.2 | 17.8 | 66 | .3 | 10.0 | 7.4 | 230 | 1.97 | 2.9 | .6 | 31.3 | 3.3 | 11 | .2 | .2 | .3 | 29 | .17 | .104 | 10 | 9.1 | .17 | 91 | .099 | 1 | 2.67 | .015 | .06 | .2 | .07 | 1.4 | .1 | <.05 | 10 | <.5 | 15.0 |
| NW3 250S | 1.2 | 13.7 | 13.3 | 49 | .1 | 12.2 | 8.9 | 382 | 2.17 | 3.9 | .8 | 13.2 | 5.6 | 7 | .1 | .2 | .3 | 25 | .07 | .068 | 13 | 9.3 | .22 | 121 | .082 | 1 | 2.67 | .012 | .05 | .2 | .04 | 1.7 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW3 275S | 1.5 | 19.9 | 17.5 | 87 | .2 | 17.0 | 12.6 | 193 | 2.71 | 5.2 | .9 | 23.2 | 5.5 | 7 | .1 | .3 | .5 | 30 | .06 | .081 | 16 | 12.1 | .28 | 93 | .079 | 1 | 2.57 | .009 | .07 | .2 | .06 | 1.7 | .1 | <.05 | 9 | <.5 | 7.5 |
| NW3 300S | 1.0 | 11.1 | 16.2 | 69 | .2 | 12.5 | 10.9 | 184 | 2.34 | 3.9 | .6 | 7.6 | 5.0 | 8 | .1 | .2 | .4 | 25 | .10 | .057 | 19 | 10.3 | .28 | 71 | .055 | 1 | 1.60 | .010 | .06 | .1 | .03 | 1.3 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW3 325S | .9 | 9.3 | 13.4 | 73 | .1 | 13.3 | 10.0 | 659 | 1.95 | 2.8 | .6 | 8.9 | 4.8 | 5 | .1 | .2 | .4 | 21 | .03 | .040 | 18 | 10.4 | .25 | 84 | .042 | <1 | 1.71 | .006 | .05 | .1 | .03 | 1.2 | .1 | <.05 | 6 | <.5 | 15.0 |
| NW3 350S | .6 | 9.3 | 6.5 | 29 | <.1 | 10.7 | 6.5 | 105 | 1.82 | 3.2 | .7 | 11.5 | 6.2 | 3 | <.1 | .1 | .3 | 14 | .02 | .027 | 24 | 8.2 | .29 | 37 | .018 | <1 | .85 | .002 | .03 | .1 | .01 | .8 | <.1 | <.05 | 3 | <.5 | 15.0 |
| NW3 375S | 1.2 | 13.8 | 13.9 | 55 | .1 | 17.5 | 9.7 | 146 | 2.21 | 3.5 | .7 | 10.8 | 5.6 | 7 | .1 | .2 | .3 | 26 | .07 | .057 | 16 | 12.2 | .31 | 96 | .066 | 1 | 2.47 | .008 | .06 | .1 | .04 | 1.7 | .1 | <.05 | 7 | <.5 | 15.0 |
| NW3 400S | 1.2 | 8.9 | 12.8 | 51 | .1 | 12.9 | 8.4 | 305 | 2.06 | 3.0 | .5 | 1.2 | 4.9 | 7 | <.1 | .2 | .4 | 26 | .07 | .056 | 13 | 11.0 | .21 | 105 | .072 | 1 | 2.43 | .009 | .06 | .2 | .04 | 1.4 | .1 | <.05 | 8 | <.5 | 7.5 |
| RE NW3 400S | 1.1 | 9.2 | 12.0 | 56 | .1 | 15.0 | 8.6 | 326 | 2.15 | 3.1 | .5 | 3.1 | 4.5 | 7 | .1 | .2 | .4 | 27 | .07 | .061 | 13 | 12.2 | .22 | 104 | .074 | 1 | 2.34 | .010 | .07 | .2 | .04 | 1.5 | .1 | <.05 | 8 | <.5 | 7.5 |
| NW3 425S | 1.0 | 10.9 | 14.1 | 48 | .1 | 11.7 | 7.3 | 179 | 1.99 | 2.6 | .6 | 6.1 | 4.2 | 6 | .1 | .2 | .3 | 29 | .06 | .071 | 11 | 9.9 | .19 | 97 | .093 | 1 | 2.23 | .011 | .06 | .2 | .04 | 1.4 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW3 450S | .8 | 8.9 | 16.0 | 63 | .1 | 10.6 | 8.4 | 272 | 1.99 | 2.4 | .4 | 11.9 | 3.8 | 8 | .1 | .2 | .4 | 28 | .07 | .049 | 13 | 9.6 | .17 | 141 | .078 | 1 | 1.92 | .010 | .06 | .2 | .04 | 1.5 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW3 475S | 1.0 | 11.4 | 16.4 | 78 | .2 | 13.0 | 11.7 | 254 | 2.30 | 3.5 | .7 | 8.0 | 5.3 | 7 | .1 | .2 | .3 | 27 | .07 | .069 | 15 | 12.6 | .24 | 93 | .067 | 1 | 2.21 | .009 | .06 | .1 | .04 | 1.8 | .1 | <.05 | 7 | <.5 | 15.0 |
| NW3 500S | .9 | 14.6 | 13.6 | 66 | .1 | 16.9 | 10.5 | 126 | 2.12 | 3.9 | .8 | 9.0 | 6.4 | 5 | .1 | .2 | .3 | 24 | .05 | .053 | 15 | 11.4 | .28 | 77 | .075 | 1 | 2.45 | .008 | .07 | .2 | .04 | 1.9 | .1 | <.05 | 7 | <.5 | 15.0 |
| NW3 525S | 1.4 | 13.8 | 20.3 | 68 | .2 | 12.3 | 8.6 | 119 | 2.54 | 4.5 | .8 | 2.4 | 4.2 | 8 | .2 | .3 | .4 | 36 | .11 | .133 | 9 | 10.7 | .17 | 73 | .142 | 1 | 3.27 | .015 | .06 | .2 | .06 | 1.7 | .1 | <.05 | 12 | .5 | 15.0 |
| NW3 550S | 1.0 | 16.3 | 24.0 | 73 | <.1 | 14.7 | 13.5 | 402 | 2.37 | 4.4 | 1.2 | 15.6 | 6.4 | 5 | .1 | .2 | .5 | 26 | .05 | .032 | 19 | 12.2 | .27 | 66 | .047 | <1 | 1.40 | .004 | .05 | .1 | .02 | 1.4 | .1 | <.05 | 6 | <.5 | 15.0 |
| NW3 575S | 1.0 | 19.9 | 21.9 | 84 | .1 | 21.5 | 13.9 | 674 | 2.73 | 5.0 | 1.0 | 18.1 | 7.1 | 5 | .2 | .3 | .5 | 31 | .04 | .053 | 16 | 12.4 | .31 | 87 | .083 | 1 | 2.74 | .007 | .07 | .1 | .05 | 1.8 | .1 | <.05 | 8 | <.5 | 15.0 |
| NW3 600S | 1.6 | 17.3 | 40.1 | 125 | .2 | 16.7 | 16.5 | 3129 | 2.46 | 3.6 | .9 | 40.0 | 3.2 | 12 | .3 | .3 | .5 | 35 | .14 | .079 | 13 | 12.8 | .25 | 172 | .086 | 2 | 2.44 | .008 | .10 | .2 | .05 | 1.6 | .2 | <.05 | 9 | .5 | 15.0 |
| NW4 400N | .6 | 7.7 | 20.3 | 39 | .1 | 8.0 | 13.9 | 579 | 1.59 | 2.1 | .6 | <.5 | 2.2 | 10 | .1 | .1 | .3 | 14 | .09 | .027 | 23 | 7.4 | .25 | 82 | .033 | <1 | 1.13 | .006 | .06 | .1 | .02 | .9 | .1 | <.05 | 6 | <.5 | 7.5 |
| NW4 375N | .8 | 10.1 | 21.9 | 37 | .1 | 15.0 | 12.3 | 225 | 1.96 | 2.3 | 1.4 | .8 | 6.3 | 7 | .1 | .1 | .5 | 20 | .08 | .025 | 19 | 10.8 | .28 | 149 | .033 | 1 | 2.20 | .007 | .06 | .1 | .03 | 1.5 | .1 | <.05 | 7 | <.5 | 15.0 |
| NW4 350N | .5 | 7.6 | 14.6 | 49 | .1 | 10.7 | 8.6 | 96 | 1.87 | 2.3 | .9 | 1.4 | 3.6 | 8 | .1 | .1 | .3 | 17 | .07 | .056 | 18 | 9.2 | .28 | 96 | .031 | 1 | 2.29 | .008 | .05 | .1 | .05 | 1.4 | .1 | <.05 | 6 | <.5 | 15.0 |
| NW4 325N | .5 | 6.2 | 11.6 | 33 | .1 | 5.8 | 3.5 | 118 | 1.78 | 2.1 | .4 | <.5 | 4.2 | 5 | .1 | .1 | .3 | 23 | .05 | .062 | 17 | 8.4 | .23 | 79 | .018 | 1 | 1.48 | .006 | .05 | .1 | .03 | 1.3 | .1 | <.05 | 7 | <.5 | 15.0 |
| NW4 300N | .4 | 9.0 | 7.2 | 27 | .1 | 6.6 | 3.9 | 108 | 1.39 | 1.5 | .4 | 1.1 | 4.0 | 4 | <.1 | .1 | .2 | 18 | .04 | .044 | 21 | 6.8 | .24 | 68 | .018 | 1 | 1.21 | .006 | .04 | .1 | .04 | 1.0 | .1 | <.05 | 5 | <.5 | 15.0 |
| NW4 275N | 1.4 | 37.4 | 22.1 | 37 | .1 | 17.9 | 17.9 | 182 | 3.18 | 8.7 | 2.6 | 1.3 | 7.5 | 13 | .1 | .3 | .5 | 36 | .15 | .108 | 8 | 10.4 | .15 | 72 | .153 | 1 | 3.86 | .018 | .05 | .3 | .06 | 2.2 | .1 | <.05 | 13 | <.5 | 15.0 |
| NW4 250N | .8 | 24.9 | 11.8 | 55 | .2 | 10.7 | 25.3 | 351 | 2.54 | 4.1 | 1.2 | 1.7 | 3.6 | 8 | .2 | .2 | .3 | 48 | .11 | .182 | 7 | 9.0 | .15 | 59 | .137 | 1 | 3.99 | .015 | .04 | .2 | .07 | 2.8 | <.1 | <.05 | 12 | <.5 | 15.0 |
| NW4 225N | .6 | 12.8 | 13.9 | 23 | .2 | 5.6 | 6.1 | 61 | 2.01 | 2.2 | .6 | 2.0 | 2.5 | 6 | .1 | .1 | .3 | 35 | .05 | .140 | 6 | 8.4 | .08 | 77 | .107 | 1 | 3.04 | .014 | .03 | .1 | .07 | 1.9 | .1 | <.05 | 11 | <.5 | 15.0 |
| NW4 200N | .7 | 15.0 | 13.5 | 59 | .2 | 13.7 | 14.5 | 239 | 2.84 | 4.0 | .6 | 8.5 | 4.9 | 7 | .1 | .3 | .4 | 46 | .09 | .087 | 15 | 14.8 | .55 | 91 | .070 | 1 | 2.05 | .011 | .07 | .2 | .03 | 2.1 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW4 175N | .9 | 22.5 | 10.7 | 49 | .3 | 18.5 | 17.5 | 171 | 2.90 | 3.6 | 1.0 | 24.9 | 5.7 | 5 | .2 | .2 | .4 | 43 | .05 | .108 | 12 | 16.1 | .53 | 96 | .087 | 1 | 3.79 | .011 | .04 | .4 | .08 | 3.5 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW4 150N | .8 | 58.5 | 12.2 | 40 | .1 | 18.4 | 8.8 | 301 | 2.02 | 4.3 | 2.9 | 9.1 | 5.2 | 9 | .1 | .1 | .3 | 29 | .18 | .022 | 23 | 11.8 | .46 | 218 | .021 | 1 | 1.82 | .005 | .06 | .2 | .02 | 1.9 | .1 | <.05 | 5 | <.5 | 15.0 |
| NW4 125N | 1.2 | 22.7 | 11.7 | 55 | .2 | 12.4 | 11.8 | 178 | 2.69 | 3.1 | .6 | 14.1 | 4.0 | 6 | .2 | .1 | .3 | 46 | .11 | .071 | 13 | 12.4 | .35 | 100 | .071 | 1 | 2.30 | .011 | .04 | .2 | .03 | 2.4 | .1 | <.05 | 9 | <.5 | 15.0 |
| STANDARD DS5 | 13.2 | 147.2 | 25.6 | 139 | .3 | 26.0 | 12.7 | 827 | 3.09 | 18.9 | 6.2 | 42.0 | 2.8 | 49 | 5.4 | 3.9 | 6.1 | 65 | .76 | .106 | 12 | 196.2 | .71 | 142 | .105 | 17 | 2.01 | .035 | .16 | 5.2 | .18 | 3.5 | 1.1 | <.05 | 7 | 5.1 | 15.0 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data FA

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| G-1 | 1.2 | 1.9 | 2.1 | 47 | <.1 | 4.7 | 4.0 | 577 | 1.89 | <.5 | 1.7 | <.5 | 4.0 | 77 | <.1 | <.1 | .1 | 43 | .53 | .082 | 7 | 45.5 | .53 | 265 | .136 | 1 | .94 | .125 | .60 | .4 | <.01 | 3.2 | .4 | <.05 | 5 | <.5 | 15.0 |
| NW4 100N | .6 | 19.9 | 9.9 | 44 | .1 | 8.6 | 6.6 | 510 | 2.09 | 3.0 | .4 | 9.1 | 2.7 | 4 | .1 | .2 | .3 | 40 | .06 | .110 | 9 | 9.4 | .25 | 91 | .058 | 1 | 2.21 | .012 | .04 | .1 | .03 | 1.6 | .1 | .09 | 8 | <.5 | 15.0 |
| NW4 075N | 1.0 | 29.8 | 10.9 | 36 | .3 | 9.6 | 8.9 | 132 | 2.81 | 5.2 | .8 | 2.2 | 4.1 | 5 | .1 | .3 | .3 | 43 | .06 | .155 | 5 | 11.1 | .17 | 67 | .114 | 2 | 4.40 | .011 | .03 | .2 | .06 | 1.8 | <.1 | <.05 | 12 | <.5 | 15.0 |
| NW4 050N | 1.3 | 21.5 | 14.8 | 40 | .2 | 12.4 | 9.1 | 135 | 2.72 | 3.1 | .5 | 17.4 | 4.0 | 9 | .1 | .2 | .3 | 43 | .15 | .037 | 14 | 13.1 | .43 | 105 | .055 | 1 | 2.20 | .011 | .05 | .2 | .03 | 1.9 | .1 | <.05 | 7 | <.5 | 15.0 |
| NW4 025N | .9 | 28.7 | 12.3 | 45 | .2 | 10.0 | 9.4 | 186 | 2.66 | 3.1 | .5 | 3.3 | 3.0 | 7 | .1 | .2 | .3 | 46 | .11 | .055 | 9 | 10.6 | .24 | 85 | .076 | 1 | 2.44 | .009 | .05 | .3 | .03 | 1.7 | .1 | <.05 | 9 | <.5 | 15.0 |
| NW4 000N | 1.9 | 226.9 | 30.2 | 58 | .4 | 40.6 | 16.7 | 567 | 3.63 | 11.1 | 3.5 | 1.6 | 8.7 | 34 | .2 | .3 | .7 | 82 | .32 | .057 | 20 | 17.1 | .39 | 517 | .084 | <1 | 5.06 | .019 | .11 | .1 | .04 | 3.0 | .1 | <.05 | 12 | .6 | 7.5 |
| L14 700W | .6 | 27.9 | 25.9 | 149 | .4 | 24.7 | 12.9 | 1091 | 2.53 | 7.2 | 1.1 | 2.3 | 5.1 | 13 | .3 | .2 | .6 | 37 | .11 | .208 | 19 | 15.9 | .18 | 139 | .134 | 1 | 3.38 | .015 | .10 | .1 | .05 | 2.1 | .2 | <.05 | 12 | <.5 | 15.0 |
| L14 675W | .7 | 10.3 | 20.8 | 115 | .3 | 13.6 | 10.9 | 301 | 2.01 | 3.6 | .6 | <.5 | 2.6 | 17 | .4 | .1 | .3 | 33 | .18 | .126 | 6 | 9.2 | .13 | 99 | .135 | 2 | 3.02 | .014 | .07 | .2 | .06 | 1.3 | .1 | .11 | 11 | <.5 | 15.0 |
| L14 650W | .7 | 11.4 | 13.2 | 117 | .2 | 11.1 | 7.9 | 2131 | 1.98 | 4.3 | .7 | <.5 | 2.9 | 10 | .4 | .2 | .3 | 34 | .11 | .370 | 6 | 9.8 | .10 | 97 | .140 | 1 | 4.30 | .016 | .06 | .2 | .07 | 1.7 | .1 | <.05 | 10 | <.5 | 15.0 |
| L14 625W | .5 | 9.1 | 29.5 | 165 | .2 | 11.6 | 7.5 | 1108 | 2.05 | 3.9 | .7 | 1.5 | 3.5 | 12 | .5 | .2 | .4 | 33 | .08 | .347 | 5 | 10.1 | .12 | 164 | .144 | 2 | 3.32 | .014 | .05 | .2 | .04 | 1.6 | .1 | <.05 | 12 | <.5 | 15.0 |
| L14 600W | .5 | 14.9 | 11.5 | 112 | .2 | 18.2 | 8.5 | 235 | 2.11 | 6.2 | 1.0 | 1.0 | 3.8 | 11 | .3 | .2 | .2 | 29 | .12 | .242 | 6 | 10.3 | .15 | 92 | .154 | 1 | 4.10 | .018 | .06 | .2 | .05 | 2.3 | .1 | <.05 | 10 | .5 | 15.0 |
| L14 575W | .7 | 13.6 | 14.6 | 92 | .2 | 17.8 | 10.8 | 426 | 2.13 | 4.4 | .8 | .9 | 4.0 | 8 | .3 | .3 | .3 | 29 | .07 | .224 | 6 | 10.9 | .14 | 108 | .139 | 1 | 3.58 | .015 | .09 | .2 | .06 | 1.9 | .1 | <.05 | 10 | <.5 | 15.0 |
| L14 550W | .6 | 13.3 | 15.6 | 76 | .2 | 14.8 | 8.1 | 342 | 2.08 | 5.2 | .8 | .7 | 4.2 | 17 | .3 | .2 | .4 | 32 | .14 | .129 | 5 | 9.2 | .11 | 109 | .170 | 1 | 3.88 | .020 | .06 | .2 | .05 | 1.6 | .1 | <.05 | 11 | .5 | 15.0 |
| L14 525W | .6 | 13.8 | 15.6 | 139 | .2 | 21.5 | 10.4 | 302 | 2.27 | 5.5 | .8 | 1.5 | 6.7 | 11 | .3 | .3 | .4 | 27 | .10 | .156 | 11 | 12.1 | .24 | 131 | .130 | 1 | 3.18 | .013 | .18 | .2 | .05 | 1.7 | .2 | <.05 | 9 | <.5 | 15.0 |
| L14 500W | 1.1 | 18.6 | 17.7 | 137 | .1 | 19.7 | 11.4 | 1067 | 3.11 | 18.6 | 1.0 | 1.7 | 5.2 | 5 | .1 | .4 | .5 | 34 | .04 | .110 | 9 | 11.8 | .20 | 95 | .113 | 1 | 3.02 | .010 | .10 | .2 | .06 | 2.0 | .2 | <.05 | 10 | <.5 | 15.0 |
| L14 475W | .7 | 10.0 | 14.0 | 101 | .2 | 12.1 | 8.4 | 702 | 1.78 | 4.4 | .4 | .5 | 2.8 | 8 | .3 | .3 | .3 | 29 | .07 | .081 | 9 | 9.7 | .12 | 126 | .106 | 2 | 2.34 | .013 | .10 | .1 | .03 | 1.4 | .2 | <.05 | 9 | <.5 | 15.0 |
| L14 450W | 1.0 | 17.6 | 16.5 | 87 | .4 | 12.9 | 10.2 | 688 | 2.41 | 28.0 | .8 | 1.3 | 4.0 | 5 | .1 | .2 | .4 | 34 | .05 | .073 | 8 | 12.6 | .18 | 116 | .123 | 1 | 3.36 | .013 | .11 | .2 | .06 | 1.8 | .2 | <.05 | 9 | <.5 | 15.0 |
| L14 425W | .8 | 11.4 | 14.2 | 79 | .2 | 11.0 | 6.1 | 360 | 2.28 | 5.0 | .6 | .9 | 3.4 | 6 | .2 | .2 | .3 | 32 | .06 | .069 | 9 | 10.4 | .15 | 80 | .102 | 2 | 3.20 | .012 | .09 | .2 | .06 | 1.5 | .2 | <.05 | 10 | <.5 | 7.5 |
| RE L14 425W | .8 | 12.4 | 13.8 | 84 | .1 | 11.1 | 6.2 | 396 | 2.41 | 5.0 | .6 | 1.1 | 3.4 | 6 | .1 | .2 | .3 | 34 | .06 | .075 | 8 | 12.4 | .14 | 77 | .099 | 2 | 3.20 | .010 | .10 | .1 | .05 | 1.4 | .2 | <.05 | 9 | <.5 | 7.5 |
| L14 400W | 1.5 | 27.4 | 28.0 | 135 | .4 | 19.8 | 12.6 | 485 | 2.88 | 4.8 | 1.0 | .5 | 6.6 | 7 | .3 | .5 | .7 | 29 | .05 | .115 | 29 | 12.3 | .22 | 107 | .105 | 1 | 1.80 | .008 | .16 | .1 | .03 | 1.6 | .3 | <.05 | 9 | <.5 | 15.0 |
| L14 375W | .8 | 19.2 | 32.4 | 127 | .1 | 14.7 | 16.8 | 863 | 3.60 | 5.4 | 1.2 | .5 | 9.9 | 5 | .2 | .5 | .7 | 34 | .04 | .148 | 28 | 15.1 | .27 | 82 | .115 | 1 | 2.28 | .009 | .23 | .2 | .04 | 1.9 | .3 | <.05 | 10 | <.5 | 15.0 |
| L14 350W | .8 | 17.1 | 15.7 | 79 | .2 | 16.4 | 11.1 | 201 | 2.15 | 4.4 | .7 | .6 | 3.8 | 5 | .2 | .2 | .3 | 31 | .05 | .074 | 8 | 12.2 | .18 | 80 | .129 | 1 | 3.45 | .012 | .12 | .1 | .04 | 2.3 | .2 | <.05 | 10 | <.5 | 15.0 |
| L14 325W | .7 | 20.4 | 12.6 | 82 | .1 | 19.8 | 11.8 | 587 | 2.12 | 3.9 | .7 | 8.4 | 4.0 | 7 | .2 | .2 | .2 | 34 | .08 | .066 | 12 | 17.5 | .27 | 108 | .093 | 1 | 2.60 | .010 | .15 | .1 | .02 | 2.4 | .2 | <.05 | 7 | <.5 | 15.0 |
| L14 300W | .7 | 20.7 | 13.0 | 94 | .1 | 26.3 | 12.0 | 658 | 2.11 | 3.6 | .5 | 1.8 | 4.0 | 7 | .2 | .1 | .2 | 31 | .07 | .083 | 12 | 15.4 | .26 | 122 | .107 | 1 | 2.86 | .012 | .14 | .1 | .04 | 2.0 | .2 | <.05 | 7 | <.5 | 15.0 |
| L14 275W | .7 | 24.4 | 13.6 | 79 | .1 | 20.3 | 10.7 | 487 | 2.19 | 4.5 | .8 | 1.0 | 5.8 | 6 | .1 | .2 | .3 | 31 | .07 | .040 | 14 | 17.8 | .31 | 111 | .080 | 2 | 2.18 | .006 | .20 | .1 | .02 | 2.2 | .2 | <.05 | 6 | <.5 | 15.0 |
| L14 250W | 1.0 | 17.5 | 15.8 | 106 | .2 | 24.0 | 11.0 | 555 | 2.28 | 8.0 | .7 | 4.0 | 4.8 | 7 | .1 | .3 | .3 | 31 | .06 | .047 | 12 | 14.2 | .24 | 110 | .102 | 1 | 2.30 | .008 | .15 | .1 | .03 | 1.9 | .2 | <.05 | 7 | <.5 | 15.0 |
| L14 225W | .4 | 26.1 | 11.0 | 51 | <.1 | 15.9 | 8.7 | 169 | 2.09 | 6.2 | .6 | 3.1 | 5.1 | 5 | .1 | .2 | .2 | 28 | .07 | .015 | 13 | 20.8 | .38 | 87 | .069 | <1 | 1.52 | .010 | .20 | .1 | .01 | 1.8 | .2 | <.05 | 4 | <.5 | 15.0 |
| L14 200W | .6 | 30.6 | 16.1 | 90 | .1 | 22.5 | 21.5 | 1206 | 2.14 | 5.1 | .6 | 1.5 | 3.5 | 7 | .2 | .2 | .3 | 35 | .09 | .068 | 10 | 17.8 | .23 | 118 | .099 | <1 | 2.70 | .009 | .13 | .1 | .06 | 1.7 | .2 | <.05 | 8 | <.5 | 15.0 |
| L14 175W | .7 | 16.5 | 13.7 | 107 | .2 | 16.2 | 11.1 | 1190 | 2.06 | 3.0 | .5 | 1.3 | 3.4 | 8 | .2 | .1 | .2 | 29 | .09 | .083 | 9 | 15.7 | .22 | 115 | .112 | <1 | 2.42 | .013 | .15 | .1 | .04 | 2.0 | .2 | <.05 | 8 | <.5 | 15.0 |
| L14 150W | .6 | 20.2 | 14.0 | 73 | .2 | 13.5 | 8.8 | 820 | 1.74 | 4.2 | .8 | 1.1 | 3.9 | 11 | .2 | .1 | .2 | 26 | .11 | .155 | 10 | 9.9 | .12 | 119 | .139 | 1 | 3.75 | .017 | .06 | .2 | .04 | 2.2 | .1 | <.05 | 9 | <.5 | 15.0 |
| L14 125W | .7 | 21.4 | 13.5 | 79 | .2 | 20.4 | 11.4 | 541 | 2.31 | 3.3 | .5 | 1.2 | 4.1 | 7 | .2 | .2 | .2 | 37 | .09 | .042 | 9 | 17.4 | .31 | 117 | .107 | 1 | 2.62 | .011 | .20 | .1 | .02 | 2.3 | .2 | <.05 | 8 | <.5 | 15.0 |
| L14 100W | .6 | 19.7 | 13.8 | 86 | .2 | 17.3 | 12.2 | 667 | 1.86 | 4.0 | .7 | 1.2 | 3.6 | 11 | .1 | .2 | .2 | 27 | .16 | .063 | 8 | 12.6 | .23 | 103 | .107 | 1 | 2.67 | .012 | .15 | .2 | .05 | 2.0 | .2 | <.05 | 8 | <.5 | 15.0 |
| L14 075W | .6 | 18.4 | 13.3 | 64 | .1 | 11.3 | 11.6 | 1008 | 1.94 | 3.9 | .6 | .9 | 2.8 | 8 | .1 | .1 | .2 | 31 | .08 | .122 | 8 | 10.7 | .11 | 100 | .123 | 1 | 4.00 | .014 | .06 | .2 | .04 | 1.6 | .1 | <.05 | 10 | <.5 | 15.0 |
| L14 050W | 1.1 | 50.0 | 37.9 | 86 | .2 | 26.7 | 27.1 | 850 | 3.69 | 5.9 | 1.8 | 2.6 | 10.9 | 11 | .1 | .3 | .7 | 53 | .08 | .048 | 27 | 31.7 | .36 | 183 | .132 | <1 | 4.02 | .013 | .21 | .1 | .06 | 4.5 | .3 | .06 | 13 | .6 | 15.0 |
| L14 025W | .4 | 29.7 | 18.5 | 63 | .1 | 17.8 | 13.5 | 528 | 2.48 | 4.0 | .9 | 1.8 | 6.0 | 10 | <.1 | .2 | .3 | 32 | .10 | .025 | 19 | 24.7 | .41 | 93 | .091 | <1 | 2.05 | .007 | .24 | .1 | .03 | 2.5 | .3 | .07 | 6 | <.5 | 15.0 |
| STANDARD DS5 | 13.1 | 141.2 | 25.5 | 136 | .3 | 24.6 | 11.9 | 791 | 3.03 | 18.6 | 6.1 | 39.9 | 2.7 | 45 | 5.3 | 4.0 | 6.3 | 62 | .76 | .099 | 12 | 187.0 | .66 | 137 | .099 | 18 | 2.05 | .033 | .17 | 5.1 | .18 | 3.4 | 1.1 | <.05 | 7 | 5.5 | 15.0 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data FA

ACME ANALYTICAL

# Ruby Red Resources Inc. PROJECT EDDY FILE # A405351



ACME ANALYTICAL

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| G-1 | 1.3 | 2.1 | 2.1 | 45 | <.1 | 5.0 | 4.1 | 578 | 1.82 | <.5 | 1.8 | .5 | 3.9 | 72 | <.1 | <.1 | .1 | 38 | .50 | .072 | 7 | 40.3 | .52 | 243 | .130 | 1 | .87 | .087 | .50 | .4 | <.01 | 2.8 | .3 | <.05 | 5 | <.5 | 15.0 |
| L14 000W | .5 | 25.4 | 21.2 | 80 | .2 | 23.1 | 16.1 | 534 | 2.48 | 4.0 | .7 | 1.3 | 5.0 | 8 | <.1 | .2 | .4 | 38 | .10 | .039 | 15 | 24.4 | .31 | 108 | .094 | 1 | 2.86 | .008 | .17 | .1 | .03 | 2.4 | .2 | <.05 | 9 | <.5 | 15.0 |
| L15 000E | .4 | 18.8 | 14.0 | 77 | .1 | 17.1 | 8.1 | 414 | 2.17 | 2.7 | .7 | 2.6 | 5.3 | 5 | .1 | .2 | .3 | 30 | .07 | .043 | 17 | 19.8 | .37 | 92 | .079 | 1 | 1.88 | .005 | .21 | .1 | .02 | 2.0 | .3 | <.05 | 6 | <.5 | 15.0 |
| L15 025E | .6 | 19.8 | 11.4 | 62 | .2 | 15.7 | 8.1 | 174 | 1.83 | 2.6 | 1.1 | 2.0 | 4.2 | 5 | .1 | .2 | .2 | 27 | .05 | .095 | 9 | 12.7 | .26 | 87 | .116 | 2 | 3.15 | .011 | .16 | .2 | .05 | 2.9 | .2 | <.05 | 8 | .5 | 15.0 |
| L15 050E | .4 | 20.4 | 13.4 | 66 | .1 | 16.6 | 8.6 | 288 | 2.52 | 2.7 | .7 | 2.4 | 6.0 | 5 | .1 | .2 | .3 | 31 | .08 | .033 | 19 | 23.8 | .42 | 69 | .082 | <1 | 1.78 | .005 | .28 | .1 | .02 | 2.4 | .3 | <.05 | 6 | <.5 | 15.0 |
| L15 075E | .7 | 12.1 | 12.2 | 96 | .1 | 9.8 | 7.4 | 1828 | 1.68 | 2.6 | 1.0 | 2.0 | 3.3 | 6 | .3 | .1 | .3 | 25 | .06 | .287 | 5 | 7.3 | .09 | 84 | .126 | 1 | 3.64 | .014 | .05 | .1 | .05 | 2.1 | .1 | <.05 | 9 | <.5 | 15.0 |
| L15 100E | .5 | 15.8 | 18.0 | 89 | .1 | 15.6 | 7.6 | 1427 | 2.23 | 2.7 | .6 | 2.2 | 4.0 | 11 | .2 | .3 | .4 | 32 | .08 | .086 | 15 | 12.7 | .20 | 139 | .126 | 1 | 2.32 | .010 | .13 | .1 | .04 | 1.9 | .2 | <.05 | 10 | <.5 | 15.0 |
| L15 125E | .4 | 18.0 | 14.7 | 81 | .1 | 17.8 | 9.2 | 260 | 2.47 | 2.4 | .6 | 1.1 | 5.7 | 6 | <.1 | .2 | .4 | 33 | .07 | .033 | 23 | 22.3 | .40 | 93 | .109 | <1 | 1.95 | .006 | .28 | .1 | .01 | 2.2 | .3 | <.05 | 8 | <.5 | 15.0 |
| L15 150E | .5 | 24.9 | 16.0 | 131 | .1 | 24.6 | 11.0 | 936 | 2.58 | 4.5 | .8 | 4.0 | 6.1 | 12 | .3 | .2 | .3 | 35 | .17 | .150 | 15 | 18.5 | .33 | 159 | .130 | <1 | 3.22 | .012 | .25 | .1 | .05 | 2.4 | .2 | <.05 | 9 | <.5 | 15.0 |
| L15 175E | .4 | 16.3 | 13.4 | 96 | .2 | 21.3 | 10.0 | 273 | 2.40 | 3.0 | 1.6 | .8 | 8.1 | 9 | .2 | .2 | .4 | 27 | .10 | .091 | 55 | 17.5 | .39 | 136 | .106 | 1 | 2.33 | .008 | .43 | .1 | .02 | 2.6 | .5 | <.05 | 8 | <.5 | 15.0 |
| L15 200E | .4 | 11.6 | 18.7 | 62 | .1 | 16.4 | 9.6 | 184 | 1.99 | 2.7 | .5 | .9 | 5.6 | 5 | <.1 | .2 | .3 | 23 | .05 | .028 | 23 | 12.4 | .30 | 111 | .080 | 1 | 2.00 | .005 | .34 | .1 | .02 | 1.5 | .3 | <.05 | 6 | <.5 | 15.0 |
| L15 225E | .5 | 12.6 | 18.3 | 73 | .2 | 22.2 | 9.7 | 193 | 1.97 | 2.5 | .5 | .7 | 5.1 | 5 | .1 | .1 | .3 | 20 | .04 | .021 | 18 | 13.3 | .28 | 132 | .075 | <1 | 2.01 | .008 | .29 | .1 | .01 | 1.7 | .3 | <.05 | 6 | <.5 | 15.0 |
| L15 250E | 3.6 | 28.2 | 45.8 | 149 | .5 | 14.3 | 10.4 | 1051 | 4.62 | 7.7 | 1.3 | 2.7 | 4.9 | 14 | .3 | .6 | .8 | 47 | .08 | .119 | 21 | 16.1 | .28 | 143 | .106 | 2 | 2.01 | .009 | .15 | .2 | .07 | 1.9 | .4 | <.05 | 10 | .5 | 7.5 |
| L15 275E | 2.1 | 80.5 | 23.4 | 154 | .3 | 30.4 | 14.0 | 928 | 5.39 | 5.8 | 2.5 | 2.1 | 8.1 | 13 | .2 | .4 | .5 | 35 | .06 | .190 | 27 | 15.6 | .25 | 125 | .130 | 2 | 3.60 | .011 | .15 | .2 | .11 | 2.3 | .4 | <.05 | 11 | .8 | 7.5 |
| L15 300E | 1.5 | 23.7 | 12.6 | 82 | .1 | 16.9 | 6.7 | 205 | 2.91 | 5.9 | 1.6 | 1.2 | 7.0 | 7 | .1 | .3 | .2 | 31 | .05 | .096 | 14 | 14.3 | .37 | 94 | .137 | 1 | 3.36 | .008 | .19 | .2 | .05 | 2.5 | .5 | <.05 | 10 | .6 | 15.0 |
| L15 325E | 1.2 | 26.4 | 13.1 | 98 | .1 | 20.1 | 10.0 | 291 | 2.91 | 6.4 | 1.7 | 1.5 | 6.5 | 11 | .1 | .4 | .3 | 36 | .13 | .092 | 12 | 14.6 | .31 | 80 | .134 | 1 | 3.86 | .010 | .15 | .2 | .07 | 2.7 | .3 | <.05 | 10 | .5 | 15.0 |
| L15 350E | 1.0 | 29.1 | 18.8 | 115 | .1 | 26.7 | 12.0 | 355 | 3.86 | 6.1 | 1.1 | 2.0 | 7.6 | 12 | .1 | .3 | .5 | 48 | .09 | .052 | 21 | 25.4 | .44 | 115 | .151 | 1 | 2.72 | .009 | .27 | .2 | .03 | 2.6 | .5 | <.05 | 12 | .5 | 15.0 |
| L15 375E | .8 | 25.5 | 13.4 | 88 | .2 | 23.0 | 16.6 | 130 | 2.10 | 4.6 | 2.1 | 3.0 | 6.4 | 9 | .1 | .2 | .3 | 31 | .10 | .117 | 16 | 12.2 | .17 | 76 | .137 | 1 | 4.57 | .016 | .07 | .2 | .08 | 3.8 | .2 | <.05 | 11 | .5 | 15.0 |
| L15 400E | .7 | 17.8 | 23.6 | 137 | .1 | 14.8 | 13.2 | 223 | 2.79 | 6.6 | 1.1 | 3.7 | 6.2 | 7 | .2 | .7 | .3 | 30 | .07 | .090 | 16 | 11.5 | .18 | 107 | .069 | 1 | 1.89 | .011 | .10 | .2 | .02 | 1.8 | .2 | <.05 | 8 | <.5 | 15.0 |
| L15 425E | .6 | 25.5 | 14.3 | 103 | <.1 | 16.8 | 10.2 | 631 | 2.55 | 4.8 | .9 | 1.9 | 5.6 | 6 | .3 | .2 | .3 | 40 | .08 | .073 | 15 | 19.4 | .32 | 83 | .112 | 1 | 2.46 | .009 | .18 | .1 | .03 | 2.6 | .3 | <.05 | 8 | <.5 | 15.0 |
| L15 450E | 1.0 | 26.3 | 22.0 | 142 | .3 | 21.0 | 12.7 | 430 | 2.89 | 5.1 | 1.1 | 1.4 | 5.7 | 7 | .4 | .4 | .5 | 37 | .05 | .053 | 22 | 17.9 | .33 | 131 | .118 | 1 | 2.50 | .009 | .24 | .1 | .03 | 2.6 | .5 | <.05 | 9 | <.5 | 15.0 |
| RE L15 450E | 1.1 | 25.4 | 21.1 | 143 | .2 | 21.4 | 12.4 | 419 | 2.78 | 4.9 | 1.0 | 1.0 | 5.5 | 7 | .4 | .4 | .5 | 35 | .04 | .053 | 21 | 17.7 | .34 | 125 | .111 | 1 | 2.55 | .009 | .27 | .1 | .03 | 2.5 | .5 | <.05 | 8 | .5 | 15.0 |
| L15 475E | 1.0 | 26.6 | 27.9 | 164 | .4 | 21.7 | 11.8 | 709 | 2.18 | 5.3 | 1.1 | 2.4 | 5.1 | 8 | .6 | .2 | .4 | 31 | .08 | .098 | 13 | 14.0 | .28 | 114 | .121 | 1 | 3.40 | .011 | .15 | .1 | .04 | 2.4 | .3 | <.05 | 9 | <.5 | 15.0 |
| L15 500E | 1.1 | 17.2 | 16.2 | 95 | .1 | 15.0 | 13.6 | 1154 | 2.18 | 2.5 | .5 | 2.1 | 3.4 | 7 | .3 | .2 | .3 | 36 | .08 | .037 | 12 | 16.0 | .20 | 123 | .080 | 1 | 1.86 | .009 | .12 | .1 | .03 | 2.2 | .2 | <.05 | 8 | <.5 | 15.0 |
| L15 525E | .7 | 26.4 | 16.5 | 84 | <.1 | 17.7 | 11.3 | 309 | 2.40 | 4.5 | 1.2 | 2.1 | 6.2 | 5 | .1 | .2 | .3 | 31 | .06 | .062 | 18 | 17.5 | .30 | 86 | .098 | 1 | 2.79 | .007 | .18 | .2 | .04 | 2.5 | .3 | <.05 | 7 | .6 | 15.0 |
| L15 550E | .8 | 25.8 | 17.6 | 70 | .1 | 18.3 | 10.6 | 284 | 2.46 | 5.0 | .9 | 3.2 | 6.6 | 6 | .1 | .2 | .3 | 30 | .06 | .053 | 15 | 19.6 | .31 | 135 | .095 | 1 | 2.98 | .007 | .19 | .1 | .03 | 2.3 | .3 | <.05 | 8 | .5 | 15.0 |
| L15 575E | .8 | 16.6 | 18.4 | 101 | .2 | 13.6 | 15.5 | 1462 | 2.25 | 3.1 | .6 | 1.8 | 3.7 | 7 | .2 | .3 | .4 | 34 | .06 | .087 | 8 | 13.2 | .19 | 135 | .116 | 1 | 2.88 | .012 | .12 | .2 | .06 | 2.1 | .2 | <.05 | 10 | <.5 | 15.0 |
| L15 600E | .6 | 16.3 | 12.4 | 93 | .3 | 9.8 | 10.7 | 1193 | 1.74 | 2.1 | .5 | 1.1 | 2.4 | 8 | .2 | .2 | .2 | 30 | .09 | .093 | 8 | 11.8 | .13 | 146 | .094 | 1 | 2.33 | .012 | .07 | .1 | .05 | 1.9 | .1 | <.05 | 9 | <.5 | 15.0 |
| L16 400W | .5 | 17.3 | 10.7 | 84 | .1 | 12.7 | 7.9 | 346 | 1.90 | 3.1 | .9 | 1.7 | 3.8 | 6 | .1 | .2 | .2 | 27 | .06 | .166 | 7 | 13.4 | .22 | 84 | .136 | 1 | 3.89 | .013 | .08 | .2 | .04 | 2.8 | .1 | <.05 | 10 | <.5 | 15.0 |
| L16 375W | .6 | 16.8 | 13.8 | 52 | .1 | 14.0 | 8.4 | 148 | 2.06 | 4.0 | .9 | 1.5 | 3.8 | 7 | .2 | .2 | .2 | 30 | .08 | .141 | 4 | 13.5 | .18 | 77 | .156 | 1 | 4.96 | .015 | .07 | .2 | .06 | 2.7 | .1 | <.05 | 11 | <.5 | 7.5 |
| L16 350W | .8 | 17.7 | 20.7 | 72 | .2 | 8.2 | 7.9 | 383 | 2.24 | 3.2 | .4 | 1.9 | 3.6 | 8 | .1 | .2 | .3 | 39 | .08 | .105 | 5 | 11.6 | .11 | 87 | .120 | 1 | 2.64 | .013 | .05 | .1 | .06 | 1.7 | .1 | <.05 | 11 | <.5 | 15.0 |
| L16 325W | .3 | 51.3 | 12.2 | 64 | .1 | 19.8 | 12.0 | 226 | 2.51 | 2.8 | .7 | 1.8 | 4.7 | 7 | .1 | .2 | .2 | 39 | .12 | .036 | 10 | 28.3 | .56 | 114 | .108 | <1 | 2.18 | .008 | .23 | .1 | .02 | 2.7 | .2 | <.05 | 7 | <.5 | 15.0 |
| L16 300W | .4 | 15.8 | 16.6 | 82 | .2 | 10.3 | 8.0 | 1295 | 1.82 | 1.7 | .5 | 2.8 | 3.4 | 19 | .4 | .1 | .3 | 30 | .27 | .080 | 15 | 17.5 | .25 | 185 | .080 | 2 | 1.45 | .010 | .17 | .1 | .03 | 2.0 | .2 | <.05 | 9 | <.5 | 15.0 |
| L16 275W | .2 | 12.2 | 8.2 | 56 | <.1 | 17.1 | 10.8 | 156 | 2.54 | 1.7 | .6 | .7 | 6.4 | 6 | .1 | .1 | .1 | 35 | .08 | .038 | 28 | 24.7 | .48 | 140 | .146 | 1 | 2.37 | .008 | .45 | .1 | .03 | 3.5 | .3 | <.05 | 9 | <.5 | 15.0 |
| L16 250W | .2 | 27.5 | 9.0 | 39 | <.1 | 28.0 | 15.1 | 189 | 2.49 | 2.0 | .3 | <.5 | 2.0 | 7 | <.1 | .1 | .1 | 54 | .29 | .021 | 5 | 47.1 | .70 | 83 | .112 | 1 | 2.38 | .016 | .13 | .1 | .01 | 3.0 | .1 | <.05 | 6 | <.5 | 15.0 |
| STANDARD DS5 | 12.6 | 144.7 | 24.9 | 141 | .3 | 24.1 | 11.7 | 759 | 2.99 | 17.8 | 6.1 | 41.0 | 2.7 | 46 | 5.4 | 3.9 | 5.9 | 61 | .74 | .086 | 12 | 184.8 | .66 | 136 | .093 | 18 | 2.06 | .031 | .14 | 4.9 | .19 | 3.6 | 1.1 | <.05 | 7 | 5.0 | 15.0 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data FA

ACME ANALYTICAL

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| G-1 | 1.3 | 2.2 | 7.6 | 45 | <.1 | 4.4 | 4.1 | 538 | 1.88 | <.5 | 1.8 | 1.1 | 4.1 | 82 | <.1 | <.1 | .1 | 42 | .58 | .080 | 7 | 44.3 | .60 | 258 | .132 | <1 | .87 | .070 | .59 | .3 | <.01 | 2.2 | .4 | .15 | 5 | <.5 | 15.0 |
| L16 225W | .3 | 42.0 | 14.7 | 37 | .1 | 26.3 | 11.8 | 286 | 2.00 | 1.8 | .4 | 15.0 | 3.4 | 6 | .1 | .2 | .1 | 42 | .17 | .023 | 6 | 36.7 | .50 | 76 | .075 | <1 | 1.85 | .011 | .08 | <.1 | .01 | 2.8 | .1 | <.05 | 5 | <.5 | 15.0 |
| L16 200W | .5 | 25.6 | 22.3 | 88 | .2 | 16.0 | 10.7 | 319 | 2.17 | 3.3 | 1.0 | 3.8 | 5.3 | 7 | .1 | .2 | .3 | 32 | .10 | .098 | 15 | 21.1 | .34 | 70 | .104 | <1 | 2.48 | .010 | .22 | .1 | .05 | 3.0 | .2 | .06 | 7 | <.5 | 15.0 |
| L16 175W | .8 | 13.9 | 23.4 | 74 | .2 | 8.8 | 6.0 | 422 | 2.04 | 3.7 | .7 | 2.4 | 3.5 | 8 | .2 | .2 | .4 | 33 | .09 | .087 | 9 | 12.8 | .15 | 75 | .098 | 2 | 2.24 | .010 | .11 | .2 | .04 | 1.6 | .2 | <.05 | 9 | <.5 | 15.0 |
| L16 150W | .5 | 17.1 | 21.5 | 94 | .2 | 11.2 | 8.7 | 2191 | 1.61 | 2.1 | .6 | 1.8 | 2.9 | 6 | .2 | .2 | .2 | 27 | .07 | .143 | 9 | 11.8 | .16 | 109 | .093 | 1 | 2.96 | .015 | .10 | .2 | .04 | 2.1 | .2 | <.05 | 7 | <.5 | 15.0 |
| L16 125W | .9 | 26.0 | 18.7 | 108 | .2 | 19.3 | 10.9 | 620 | 2.22 | 3.0 | .9 | 2.8 | 4.9 | 8 | .2 | .2 | .4 | 34 | .10 | .061 | 13 | 18.3 | .32 | 115 | .109 | <1 | 2.42 | .008 | .24 | .2 | .04 | 2.3 | .3 | <.05 | 7 | <.5 | 15.0 |
| L16 100W | .9 | 14.0 | 14.5 | 63 | .1 | 9.3 | 6.3 | 357 | 2.08 | 3.1 | .6 | 1.4 | 2.8 | 7 | .1 | .3 | .3 | 33 | .07 | .119 | 8 | 11.1 | .16 | 79 | .122 | <1 | 3.20 | .014 | .10 | .2 | .04 | 1.8 | .1 | <.05 | 8 | <.5 | 15.0 |
| L16 075W | .8 | 17.4 | 22.4 | 91 | .1 | 14.0 | 8.7 | 839 | 2.36 | 5.3 | .9 | 2.1 | 6.7 | 6 | .2 | .3 | .5 | 30 | .05 | .077 | 22 | 15.0 | .34 | 106 | .116 | 1 | 2.29 | .009 | .31 | .2 | .06 | 2.3 | .4 | <.05 | 7 | <.5 | 15.0 |
| L16 050W | .5 | 13.5 | 17.8 | 86 | .1 | 14.5 | 8.5 | 567 | 2.20 | 2.9 | .6 | 1.0 | 5.1 | 7 | .1 | .2 | .4 | 34 | .08 | .069 | 16 | 16.7 | .32 | 104 | .106 | 1 | 2.28 | .009 | .24 | .2 | .03 | 2.3 | .3 | <.05 | 7 | <.5 | 15.0 |
| L16 025W | .7 | 27.4 | 27.6 | 74 | .1 | 18.9 | 9.3 | 354 | 2.25 | 4.4 | .9 | 3.1 | 6.2 | 7 | .1 | .3 | .3 | 32 | .07 | .082 | 18 | 19.1 | .33 | 86 | .099 | <1 | 3.26 | .008 | .18 | .2 | .03 | 2.6 | .2 | <.05 | 7 | .6 | 7.5 |
| RE L16 025W | .9 | 26.8 | 17.6 | 75 | .1 | 17.7 | 10.0 | 400 | 2.49 | 4.5 | 1.0 | .9 | 6.3 | 6 | .1 | .2 | .3 | 38 | .07 | .082 | 17 | 21.4 | .33 | 86 | .100 | <1 | 2.97 | .008 | .18 | .2 | .03 | 2.7 | .2 | <.05 | 7 | <.5 | 7.5 |
| L16 000W | .5 | 20.0 | 17.7 | 56 | .1 | 14.8 | 10.2 | 322 | 2.23 | 3.6 | .7 | 1.8 | 6.0 | 6 | .1 | .2 | .3 | 33 | .06 | .037 | 21 | 18.6 | .36 | 97 | .066 | <1 | 1.87 | .005 | .22 | .1 | .02 | 1.9 | .3 | <.05 | 6 | <.5 | 15.0 |
| L1860 2675NW | 1.0 | 13.0 | 12.0 | 34 | .1 | 9.2 | 6.3 | 113 | 1.80 | 4.3 | .7 | 18.5 | 3.6 | 7 | .1 | .2 | .2 | 31 | .05 | .138 | 4 | 7.9 | .11 | 60 | .129 | <1 | 3.51 | .017 | .04 | .2 | .03 | 1.7 | .1 | <.05 | 9 | <.5 | 15.0 |
| L1860 2650NW | 1.0 | 13.3 | 15.2 | 46 | .3 | 10.9 | 8.8 | 147 | 2.22 | 4.1 | .8 | 3.3 | 4.6 | 9 | .1 | .1 | .3 | 32 | .08 | .141 | 6 | 9.2 | .17 | 77 | .125 | 1 | 3.60 | .016 | .05 | .2 | .06 | 1.8 | .1 | <.05 | 10 | .7 | 15.0 |
| STANDARD DS5 | 12.1 | 141.0 | 25.3 | 132 | .3 | 24.8 | 12.0 | 792 | 3.10 | 17.9 | 6.0 | 42.0 | 2.9 | 48 | 5.4 | 3.9 | 5.8 | 66 | .74 | .096 | 12 | 189.4 | .67 | 138 | .106 | 16 | 2.00 | .035 | .16 | 5.2 | .19 | 3.6 | 1.1 | .06 | 7 | 4.8 | 15.0 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data ___ FA ___

ACME ANA YTICAL LABORATORIES LTD. 852 E. HASTINGS ST. COUVER BC V6A 1R6 PHONE(604)253-3158 FAX(60 53-1716
(IS 002 Accredited Co.)

# GEOCHEMICAL ANALYSIS CERTIFICATE

**Ruby Red Resources Inc.** PROJECT EDDY File # A404156 Page 1

207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au* ppb |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| G-1 | 2 | 2 | 5 | 43 | <.3 | 5 | 4 | 581 | 2.07 | <2 | <8 | <2 | 4 | 89 | <.5 | <3 | <3 | 41 | .62 | .076 | 11 | 18 | .59 | 272 | .16 | <3 | 1.14 | .15 | .58 | 4 | <.5 |
| 1700 1200W | 1 | 22 | 56 | 243 | .4 | 27 | 11 | 335 | 2.53 | 6 | <8 | <2 | 7 | 8 | <.5 | <3 | <3 | 26 | .08 | .050 | 16 | 13 | .32 | 94 | .06 | <3 | 2.68 | .01 | .08 | <2 | 1.5 |
| 1700 1175W | 2 | 32 | 47 | 222 | .4 | 31 | 14 | 161 | 2.71 | 11 | <8 | <2 | 9 | 4 | .5 | <3 | <3 | 22 | .03 | .041 | 23 | 13 | .34 | 92 | .05 | <3 | 2.60 | .01 | .06 | <2 | 2.2 |
| 1700 1150W | 2 | 44 | 46 | 485 | <.3 | 50 | 18 | 205 | 3.66 | 9 | <8 | <2 | 7 | 12 | <.5 | <3 | <3 | 27 | .10 | .032 | 18 | 15 | .30 | 128 | .04 | <3 | 3.09 | .01 | .07 | <2 | 17.3 |
| 1700 1125W | 2 | 24 | 33 | 263 | <.3 | 24 | 12 | 128 | 2.90 | 11 | <8 | <2 | 8 | 5 | <.5 | <3 | <3 | 18 | .04 | .035 | 27 | 14 | .28 | 83 | .03 | 3 | 2.14 | .01 | .05 | <2 | 2.2 |
| 1700 1100W | 1 | 18 | 23 | 215 | <.3 | 21 | 11 | 139 | 2.51 | 5 | <8 | <2 | 7 | 5 | <.5 | <3 | <3 | 20 | .03 | .035 | 21 | 11 | .27 | 76 | .06 | <3 | 2.47 | .01 | .06 | 3 | 1.6 |
| 1700 1075W | 1 | 16 | 12 | 67 | <.3 | 13 | 6 | 145 | 2.10 | 6 | <8 | <2 | 6 | 2 | <.5 | <3 | <3 | 10 | .01 | .022 | 35 | 10 | .33 | 61 | .02 | <3 | 1.22 | <.01 | .04 | <2 | 1.1 |
| 1700 1050W | 2 | 16 | 25 | 209 | <.3 | 17 | 13 | 448 | 2.46 | 9 | <8 | <2 | 7 | 5 | <.5 | <3 | <3 | 19 | .04 | .028 | 21 | 11 | .25 | 81 | .05 | <3 | 2.01 | .01 | .05 | 2 | 1.3 |
| 1700 1025W | 1 | 21 | 19 | 191 | .5 | 15 | 11 | 249 | 2.36 | 6 | <8 | <2 | 5 | 6 | <.5 | <3 | <3 | 24 | .05 | .034 | 22 | 11 | .21 | 133 | .06 | <3 | 2.12 | .01 | .05 | 2 | 2.9 |
| 1700 1000W | 1 | 26 | 32 | 222 | .3 | 26 | 21 | 871 | 2.40 | 6 | <8 | <2 | 6 | 13 | <.5 | <3 | <3 | 23 | .07 | .040 | 20 | 13 | .25 | 155 | .05 | <3 | 2.74 | .01 | .07 | <2 | .7 |
| 1700 975W | 1 | 14 | 20 | 144 | .3 | 17 | 11 | 363 | 2.41 | 6 | <8 | <2 | 5 | 4 | <.5 | <3 | <3 | 21 | .02 | .027 | 24 | 13 | .26 | 106 | .03 | <3 | 2.12 | .01 | .06 | <2 | .9 |
| 1700 950W | 1 | 17 | 23 | 127 | <.3 | 17 | 12 | 582 | 2.29 | 6 | <8 | <2 | 7 | 4 | <.5 | <3 | <3 | 15 | .03 | .023 | 30 | 9 | .27 | 98 | .02 | <3 | 1.65 | .01 | .05 | 2 | 3.1 |
| 1700 925W | 1 | 28 | 32 | 174 | .3 | 34 | 21 | 326 | 2.90 | 6 | <8 | <2 | 9 | 9 | <.5 | <3 | <3 | 23 | .06 | .048 | 18 | 15 | .32 | 142 | .04 | <3 | 3.22 | .01 | .08 | 2 | 1.8 |
| 1700 900W | 1 | 14 | 45 | 178 | <.3 | 21 | 12 | 171 | 2.19 | 4 | <8 | <2 | 6 | 6 | <.5 | <3 | <3 | 16 | .06 | .037 | 22 | 10 | .31 | 99 | .04 | <3 | 2.27 | .01 | .05 | 3 | 1.7 |
| 1700 875W | 1 | 13 | 61 | 199 | .4 | 13 | 10 | 352 | 2.30 | 7 | <8 | <2 | 5 | 5 | <.5 | <3 | <3 | 23 | .04 | .032 | 20 | 13 | .25 | 106 | .05 | <3 | 2.06 | .01 | .05 | 2 | 1.6 |
| RE 1700 825W | 1 | 16 | 93 | 315 | <.3 | 21 | 8 | 143 | 2.59 | 10 | <8 | <2 | 8 | 4 | <.5 | <3 | <3 | 19 | .02 | .047 | 24 | 15 | .40 | 84 | .04 | <3 | 2.34 | .01 | .05 | <2 | 2.8 |
| 1700 850W | 2 | 9 | 38 | 399 | .5 | 19 | 12 | 704 | 2.33 | 4 | <8 | <2 | 4 | 10 | .5 | <3 | <3 | 26 | .12 | .070 | 13 | 13 | .23 | 107 | .09 | <3 | 2.90 | .01 | .06 | <2 | 1.2 |
| 1700 825W | 1 | 16 | 100 | 320 | .5 | 21 | 8 | 143 | 2.58 | 10 | <8 | <2 | 8 | 4 | <.5 | <3 | 3 | 19 | .03 | .046 | 23 | 12 | .41 | 82 | .04 | <3 | 2.34 | .01 | .05 | <2 | 8.5 |
| 1700 800W | 1 | 22 | 77 | 341 | <.3 | 31 | 12 | 374 | 2.98 | 13 | <8 | <2 | 9 | 7 | <.5 | <3 | <3 | 22 | .05 | .037 | 28 | 15 | .41 | 91 | .07 | <3 | 2.03 | .01 | .07 | <2 | 3.8 |
| 1700 775W | 1 | 24 | 57 | 224 | <.3 | 19 | 12 | 283 | 2.62 | 11 | <8 | <2 | 8 | 5 | <.5 | <3 | <3 | 18 | .03 | .038 | 29 | 10 | .37 | 74 | .04 | <3 | 1.89 | .01 | .05 | <2 | 33.2 |
| 1700 750W | 2 | 15 | 62 | 326 | <.3 | 21 | 14 | 743 | 2.72 | 10 | <8 | <2 | 7 | 8 | <.5 | 3 | <3 | 20 | .06 | .031 | 30 | 12 | .33 | 139 | .04 | <3 | 1.61 | .01 | .06 | <2 | 6.4 |
| 1700 725W | 2 | 23 | 85 | 264 | .5 | 22 | 36 | 1358 | 2.70 | 10 | <8 | <2 | 8 | 5 | <.5 | <3 | <3 | 19 | .04 | .033 | 30 | 13 | .33 | 112 | .03 | <3 | 1.98 | .01 | .05 | <2 | 97.4 |
| 1700 700W | 2 | 15 | 47 | 491 | .6 | 22 | 15 | 1513 | 2.54 | 7 | <8 | <2 | 6 | 10 | .8 | <3 | <3 | 26 | .08 | .058 | 20 | 16 | .22 | 180 | .06 | 5 | 3.27 | .01 | .07 | <2 | 4.7 |
| 1700 675W | 2 | 12 | 57 | 338 | .6 | 21 | 15 | 1888 | 2.80 | 7 | <8 | <2 | 5 | 24 | .7 | <3 | <3 | 23 | .23 | .025 | 21 | 16 | .25 | 149 | .03 | 6 | 1.99 | .01 | .09 | <2 | 1.4 |
| 1700 650W | 2 | 15 | 41 | 272 | .6 | 18 | 14 | 313 | 2.67 | 7 | <8 | <2 | 6 | 8 | <.5 | <3 | <3 | 26 | .06 | .037 | 20 | 10 | .22 | 114 | .05 | <3 | 2.16 | .01 | .06 | <2 | 2.4 |
| 1700 625W | 2 | 12 | 50 | 116 | .7 | 12 | 7 | 155 | 2.84 | 8 | <8 | <2 | 6 | 4 | <.5 | <3 | <3 | 25 | .03 | .026 | 25 | 10 | .20 | 61 | .04 | 7 | 1.39 | .01 | .04 | <2 | 4.7 |
| 1700 600W | 2 | 26 | 88 | 200 | .5 | 21 | 18 | 699 | 2.91 | 7 | <8 | <2 | 4 | 8 | <.5 | <3 | 3 | 23 | .05 | .038 | 21 | 14 | .20 | 75 | .03 | <3 | 1.84 | .01 | .06 | <2 | 2.5 |
| 1700 575W | 4 | 19 | 50 | 212 | .4 | 23 | 17 | 293 | 3.04 | 10 | <8 | <2 | 8 | 7 | <.5 | <3 | <3 | 20 | .07 | .033 | 23 | 13 | .28 | 89 | .04 | <3 | 2.37 | .01 | .07 | <2 | 2.1 |
| 1700 550W | 2 | 26 | 303 | 399 | .9 | 33 | 24 | 418 | 3.42 | 11 | <8 | <2 | 8 | 6 | <.5 | <3 | 6 | 23 | .05 | .043 | 26 | 18 | .33 | 87 | .05 | <3 | 2.43 | .01 | .08 | <2 | 6.8 |
| 1700 525W | 1 | 22 | 77 | 266 | .8 | 28 | 14 | 326 | 2.85 | 8 | <8 | <2 | 9 | 10 | .5 | <3 | 4 | 21 | .07 | .039 | 19 | 16 | .31 | 86 | .05 | 3 | 2.63 | .01 | .05 | <2 | 4.2 |
| 1700 500W | 2 | 22 | 44 | 210 | .6 | 22 | 16 | 322 | 3.01 | 11 | <8 | <2 | 8 | 4 | <.5 | <3 | <3 | 22 | .03 | .035 | 23 | 16 | .31 | 91 | .04 | <3 | 2.16 | .01 | .06 | <2 | 2.8 |
| 1700 475W | 2 | 23 | 56 | 179 | .3 | 19 | 17 | 1141 | 3.05 | 15 | <8 | <2 | 7 | 4 | <.5 | <3 | <3 | 21 | .02 | .045 | 23 | 12 | .32 | 90 | .04 | <3 | 1.96 | .01 | .06 | 2 | 5.4 |
| 1700 450W | 2 | 22 | 83 | 204 | .7 | 19 | 13 | 438 | 3.48 | 13 | <8 | <2 | 8 | 5 | <.5 | <3 | <3 | 26 | .03 | .041 | 23 | 15 | .34 | 108 | .05 | <3 | 2.27 | .01 | .05 | 3 | 3.8 |
| 1700 425W | 2 | 27 | 66 | 313 | .4 | 37 | 28 | 684 | 3.66 | 12 | <8 | <2 | 6 | 20 | <.5 | <3 | <3 | 22 | .18 | .037 | 25 | 21 | .40 | 100 | .03 | <3 | 2.03 | .01 | .07 | <2 | 1.7 |
| 1700 400W | 2 | 29 | 55 | 217 | .9 | 22 | 12 | 189 | 2.76 | 9 | <8 | <2 | 7 | 9 | .5 | <3 | 3 | 24 | .07 | .043 | 18 | 13 | .29 | 86 | .10 | <3 | 3.37 | .01 | .05 | <2 | 2.5 |
| STANDARD DS5 | 13 | 147 | 28 | 134 | .3 | 25 | 12 | 752 | 2.99 | 19 | <8 | <2 | 2 | 47 | 5.6 | 5 | 6 | 61 | .73 | .093 | 13 | 194 | .69 | 142 | .10 | 15 | 1.99 | .04 | .14 | 6 | 43.8 |

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: SOIL SS80 60C AU* BY ACID LEACHED, ANALYZED BY ICP-MS. (15 gm)
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA ____ DATE RECEIVED: AUG 3 2004 DATE REPORT MAILED: Aug 21/04

BRITISH COLUMBIA CERTIFIED ASSAYER
Clarence Leong

ACME ANALYTICAL

# Ruby Red Resources Inc. PROJECT EDDY FILE # A404156



ACME ANALYTICAL

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au* ppb |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| G-1 | 4 | 3 | 6 | 47 | <.3 | 5 | 4 | 628 | 2.18 | <2 | 9 | <2 | 5 | 91 | <.5 | <3 | <3 | 43 | .66 | .078 | 12 | 21 | .63 | 279 | .16 | 5 | 1.18 | .15 | .60 | 5 | <.5 |
| 1700 375W | 1 | 22 | 68 | 217 | <.3 | 24 | 16 | 416 | 3.10 | 10 | <8 | <2 | 9 | 6 | <.5 | <3 | <3 | 22 | .04 | .036 | 22 | 15 | .33 | 90 | .04 | 9 | 2.59 | .01 | .07 | <2 | 8.2 |
| 1700 350W | 2 | 15 | 41 | 169 | .3 | 16 | 15 | 264 | 2.92 | 8 | <8 | <2 | 7 | 8 | <.5 | <3 | <3 | 26 | .05 | .029 | 23 | 13 | .24 | 91 | .05 | 7 | 2.12 | .01 | .07 | 3 | 1.8 |
| 1700 325W | 1 | 11 | 32 | 140 | <.3 | 12 | 11 | 492 | 2.77 | 9 | <8 | <2 | 6 | 5 | <.5 | 3 | <3 | 26 | .04 | .027 | 27 | 13 | .24 | 97 | .02 | 8 | 1.80 | .01 | .05 | 2 | 4.0 |
| 1700 300W | 2 | 24 | 53 | 197 | <.3 | 18 | 13 | 794 | 2.89 | 10 | <8 | <2 | 8 | 7 | <.5 | <3 | <3 | 26 | .06 | .037 | 22 | 15 | .28 | 108 | .07 | 7 | 2.47 | .01 | .07 | <2 | 21.3 |
| 1700 275W | 1 | 19 | 42 | 175 | .5 | 18 | 13 | 681 | 2.60 | 9 | <8 | <2 | 6 | 9 | <.5 | <3 | <3 | 27 | .06 | .051 | 15 | 10 | .22 | 114 | .10 | 8 | 2.67 | .02 | .07 | 2 | 2.9 |
| 1700 250W | <1 | 10 | 17 | 91 | <.3 | 8 | 6 | 240 | 1.22 | 4 | <8 | <2 | 3 | 4 | <.5 | <3 | <3 | 13 | .03 | .030 | 10 | 5 | .10 | 53 | .05 | 4 | 1.46 | .01 | .03 | <2 | 1.2 |
| 1700 225W | 3 | 21 | 28 | 134 | .6 | 16 | 10 | 190 | 2.47 | 6 | <8 | <2 | 7 | 8 | <.5 | <3 | <3 | 23 | .06 | .046 | 14 | 12 | .21 | 97 | .09 | 7 | 2.74 | .02 | .05 | <2 | 2.6 |
| 1700 200W | <1 | 23 | 39 | 182 | .5 | 18 | 12 | 381 | 2.28 | 4 | <8 | <2 | 6 | 7 | .5 | <3 | <3 | 25 | .05 | .054 | 13 | 11 | .22 | 95 | .11 | 6 | 3.22 | .02 | .06 | 2 | 2.5 |
| 1700 175W | 2 | 17 | 29 | 144 | <.3 | 19 | 10 | 201 | 2.29 | 3 | <8 | <2 | 5 | 7 | <.5 | <3 | <3 | 24 | .06 | .070 | 10 | 9 | .17 | 96 | .11 | 5 | 3.90 | .02 | .04 | <2 | 1.3 |
| 1700 150W | 1 | 18 | 31 | 259 | .4 | 29 | 18 | 440 | 3.09 | 9 | <8 | <2 | 5 | 9 | .5 | <3 | <3 | 23 | .05 | .066 | 14 | 13 | .25 | 119 | .06 | 6 | 3.12 | .01 | .07 | <2 | 1.8 |
| 1700 125W | 2 | 18 | 42 | 105 | <.3 | 16 | 10 | 392 | 3.35 | 12 | <8 | <2 | 7 | 6 | <.5 | <3 | <3 | 29 | .04 | .035 | 24 | 17 | .24 | 103 | .04 | 8 | 1.97 | .01 | .07 | <2 | 5.7 |
| 1700 100W | 2 | 21 | 34 | 146 | .3 | 15 | 13 | 333 | 3.22 | 10 | <8 | <2 | 7 | 4 | <.5 | <3 | <3 | 25 | .02 | .033 | 23 | 13 | .24 | 74 | .03 | 8 | 1.82 | .01 | .06 | 2 | 1.9 |
| 1700 075W | 1 | 18 | 25 | 114 | .3 | 18 | 17 | 405 | 2.72 | 6 | <8 | <2 | 6 | 5 | <.5 | <3 | <3 | 20 | .03 | .041 | 22 | 14 | .25 | 85 | .04 | 8 | 2.51 | .01 | .05 | 2 | 1.6 |
| 1700 050W | 1 | 14 | 17 | 85 | <.3 | 16 | 12 | 461 | 2.39 | 7 | <8 | <2 | 6 | 6 | <.5 | <3 | <3 | 16 | .05 | .036 | 27 | 11 | .27 | 83 | .03 | 5 | 1.85 | .01 | .05 | <2 | .8 |
| 1700 025W | 1 | 16 | 16 | 89 | <.3 | 14 | 11 | 455 | 2.57 | 7 | <8 | <2 | 6 | 6 | <.5 | <3 | <3 | 24 | .04 | .056 | 15 | 12 | .23 | 90 | .07 | 8 | 2.71 | .01 | .04 | <2 | .9 |
| 1700 000W | 1 | 10 | 17 | 57 | <.3 | 11 | 5 | 159 | 2.46 | 7 | <8 | <2 | 4 | 8 | <.5 | <3 | <3 | 21 | .04 | .027 | 26 | 10 | .22 | 72 | .02 | 7 | 1.15 | .01 | .05 | <2 | .7 |
| 1770 000E | 2 | 24 | 22 | 49 | <.3 | 34 | 22 | 226 | 2.40 | 3 | <8 | <2 | 8 | 16 | <.5 | 3 | <3 | 18 | .14 | .027 | 34 | 15 | .15 | 68 | .12 | 6 | 5.32 | .02 | .04 | <2 | 1.6 |
| 1770 025E | 1 | 9 | 7 | 35 | <.3 | 9 | 4 | 107 | 3.06 | 5 | <8 | <2 | 6 | 3 | <.5 | <3 | <3 | 21 | .01 | .024 | 34 | 15 | .28 | 45 | .02 | 4 | 1.21 | <.01 | .05 | <2 | 4.5 |
| RE 1770 125E | 1 | 8 | <3 | 24 | <.3 | 5 | 2 | 50 | 1.29 | 6 | <8 | <2 | 4 | 1 | <.5 | <3 | <3 | 7 | .01 | .014 | 21 | 3 | .17 | 20 | .01 | 3 | .66 | <.01 | .02 | <2 | 4.2 |
| 1770 050E | <1 | 15 | 15 | 58 | <.3 | 14 | 7 | 121 | 2.86 | 9 | <8 | <2 | 8 | 3 | <.5 | <3 | <3 | 18 | .01 | .045 | 27 | 16 | .32 | 47 | .03 | 6 | 2.24 | .01 | .04 | <2 | 3.5 |
| 1770 075E | <1 | 18 | 13 | 48 | <.3 | 11 | 6 | 116 | 1.94 | 5 | <8 | <2 | 7 | 8 | <.5 | <3 | <3 | 21 | .08 | .077 | 17 | 12 | .17 | 54 | .07 | 5 | 3.18 | .01 | .04 | <2 | 2.4 |
| 1770 100E | 2 | 15 | 16 | 40 | <.3 | 13 | 5 | 103 | 2.42 | 3 | <8 | <2 | 5 | 10 | <.5 | <3 | <3 | 22 | .09 | .059 | 16 | 14 | .20 | 63 | .06 | 6 | 3.35 | .01 | .05 | <2 | 1.5 |
| 1770 125E | 1 | 8 | 10 | 25 | <.3 | 6 | 2 | 54 | 1.37 | 5 | <8 | <2 | 4 | 2 | <.5 | <3 | <3 | 7 | .01 | .015 | 22 | 4 | .18 | 21 | .01 | 4 | .70 | <.01 | .02 | <2 | 2.8 |
| 1770 150E | <1 | 10 | 15 | 49 | <.3 | 10 | 6 | 118 | 2.36 | 6 | <8 | <2 | 5 | 6 | <.5 | <3 | <3 | 22 | .04 | .028 | 24 | 12 | .23 | 83 | .02 | 3 | 1.87 | .01 | .04 | <2 | 2.7 |
| 1770 175E | <1 | 12 | 13 | 37 | <.3 | 9 | 5 | 106 | 2.19 | 2 | <8 | <2 | 5 | 6 | <.5 | <3 | <3 | 19 | .05 | .033 | 23 | 11 | .20 | 69 | .02 | 4 | 1.63 | .01 | .09 | <2 | 3.1 |
| 1770 200E | <1 | 9 | 20 | 40 | <.3 | 12 | 5 | 101 | 2.32 | 5 | <8 | <2 | 6 | 5 | <.5 | <3 | <3 | 18 | .03 | .028 | 25 | 11 | .28 | 70 | .03 | 4 | 1.70 | .01 | .04 | <2 | 44.2 |
| 1770 225E | 1 | 9 | 16 | 40 | <.3 | 12 | 5 | 109 | 2.13 | 4 | <8 | <2 | 4 | 7 | <.5 | <3 | <3 | 19 | .05 | .021 | 28 | 11 | .36 | 75 | .02 | 4 | 1.47 | .01 | .05 | <2 | .9 |
| 1770 250E | 1 | 5 | 10 | 22 | <.3 | 8 | 3 | 50 | 1.97 | <2 | <8 | <2 | 6 | 4 | <.5 | <3 | <3 | 20 | .02 | .019 | 30 | 9 | .28 | 42 | .02 | 5 | 1.01 | <.01 | .03 | <2 | 7.3 |
| 1770 275E | 2 | 4 | 6 | 24 | <.3 | 8 | 3 | 48 | 1.89 | 4 | <8 | <2 | 5 | 3 | <.5 | <3 | <3 | 17 | .01 | .018 | 30 | 10 | .27 | 39 | .02 | 4 | 1.07 | .01 | .03 | <2 | 6.9 |
| 1770 300E | 1 | 9 | 13 | 34 | <.3 | 10 | 6 | 87 | 2.64 | 5 | <8 | <2 | 5 | 5 | <.5 | <3 | <3 | 22 | .04 | .026 | 26 | 12 | .32 | 45 | .03 | 6 | 1.23 | <.01 | .04 | <2 | 4.5 |
| 1770 325E | 1 | 11 | 12 | 34 | <.3 | 11 | 7 | 77 | 2.06 | <2 | <8 | <2 | 5 | 6 | <.5 | <3 | <3 | 24 | .04 | .059 | 9 | 12 | .15 | 67 | .10 | 7 | 4.07 | .02 | .03 | <2 | 2.9 |
| 1770 350E | 2 | 15 | 17 | 42 | <.3 | 14 | 7 | 118 | 2.46 | 6 | <8 | <2 | 7 | 2 | <.5 | <3 | <3 | 12 | .01 | .024 | 30 | 13 | .47 | 28 | .01 | 7 | 1.25 | <.01 | .03 | <2 | 11.6 |
| 1770 375E | 1 | 13 | 12 | 41 | <.3 | 14 | 8 | 79 | 2.19 | 3 | <8 | <2 | 6 | 5 | <.5 | <3 | <3 | 21 | .02 | .025 | 21 | 11 | .31 | 73 | .04 | 4 | 2.03 | .01 | .04 | <2 | 3.6 |
| 1770 400E | <1 | 12 | 12 | 34 | <.3 | 10 | 7 | 163 | 2.33 | 2 | <8 | <2 | 5 | 5 | <.5 | <3 | <3 | 32 | .03 | .033 | 14 | 12 | .17 | 103 | .09 | 5 | 2.44 | .02 | .04 | <2 | 86.0 |
| STANDARD DS5 | 12 | 143 | 24 | 135 | <.3 | 25 | 12 | 772 | 3.03 | 18 | 8 | <2 | 3 | 46 | 5.6 | 5 | 7 | 62 | .74 | .092 | 13 | 189 | .69 | 135 | .10 | 16 | 2.00 | .04 | .14 | 6 | 42.0 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data FA

**Ruby Red Resources Inc.** PROJECT EDDY FILE # A404156



ACME ANALYTICAL

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au* ppb |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| G-1 | 1 | 3 | 4 | 44 | <.3 | 6 | 5 | 612 | 2.14 | <2 | <8 | <2 | 4 | 89 | <.5 | <3 | <3 | 44 | .67 | .078 | 11 | 23 | .62 | 268 | .17 | <3 | 1.15 | .15 | .59 | 6 | .8 |
| 1770 425E | 1 | 18 | 17 | 51 | <.3 | 12 | 8 | 188 | 2.41 | 3 | <8 | <2 | 4 | 6 | <.5 | <3 | <3 | 34 | .04 | .051 | 11 | 14 | .16 | 83 | .11 | <3 | 3.13 | .02 | .05 | 3 | 3.1 |
| 1770 450E | 1 | 13 | 16 | 54 | <.3 | 17 | 12 | 230 | 2.22 | 2 | <8 | <2 | 6 | 9 | <.5 | <3 | <3 | 27 | .06 | .041 | 17 | 11 | .30 | 116 | .08 | 3 | 2.52 | .01 | .06 | 2 | 2.9 |
| 1770 475E | <1 | 10 | 10 | 40 | <.3 | 13 | 9 | 118 | 2.29 | 4 | <8 | <2 | 6 | 4 | <.5 | <3 | <3 | 21 | .02 | .034 | 27 | 11 | .36 | 67 | .04 | <3 | 1.85 | .01 | .04 | 2 | 12.8 |
| 1770 500E | <1 | 15 | 14 | 49 | <.3 | 17 | 9 | 136 | 2.34 | 3 | <8 | <2 | 6 | 5 | <.5 | <3 | <3 | 28 | .03 | .027 | 28 | 13 | .52 | 79 | .03 | <3 | 1.87 | .01 | .05 | 2 | 6.4 |
| 1770 525E | <1 | 21 | 9 | 31 | <.3 | 14 | 9 | 102 | 2.10 | 5 | <8 | <2 | 5 | 6 | <.5 | <3 | <3 | 29 | .04 | .055 | 15 | 10 | .21 | 79 | .14 | <3 | 3.77 | .02 | .04 | 2 | 78.7 |
| 1770 550E | <1 | 11 | 6 | 37 | <.3 | 13 | 7 | 121 | 2.24 | 5 | <8 | <2 | 7 | 3 | <.5 | <3 | <3 | 20 | .02 | .038 | 28 | 12 | .41 | 56 | .04 | <3 | 1.58 | .01 | .03 | 2 | 10.0 |
| 1770 575E | <1 | 15 | 15 | 42 | <.3 | 17 | 9 | 271 | 2.15 | 7 | <8 | <2 | 6 | 7 | <.5 | <3 | <3 | 28 | .05 | .052 | 11 | 10 | .23 | 75 | .11 | 4 | 3.01 | .02 | .04 | 2 | 3.4 |
| 1770 600E | 1 | 17 | 11 | 45 | .3 | 16 | 10 | 505 | 2.21 | 4 | <8 | <2 | 5 | 8 | <.5 | 3 | <3 | 31 | .05 | .050 | 10 | 11 | .18 | 79 | .16 | <3 | 4.17 | .02 | .04 | 2 | 2.3 |
| 1770 625E | 1 | 16 | 30 | 85 | <.3 | 20 | 15 | 477 | 2.44 | 5 | <8 | <2 | 6 | 7 | <.5 | <3 | <3 | 32 | .05 | .060 | 12 | 13 | .27 | 101 | .12 | <3 | 3.04 | .02 | .05 | 2 | 4.4 |
| 1770 650E | 1 | 11 | 12 | 86 | .6 | 11 | 10 | 332 | 2.47 | 6 | <8 | <2 | 4 | 8 | <.5 | <3 | <3 | 35 | .08 | .170 | 6 | 12 | .11 | 70 | .16 | <3 | 3.92 | .02 | .04 | 4 | 1.4 |
| 1770 675E | 1 | 28 | 29 | 107 | .5 | 17 | 12 | 595 | 2.17 | 7 | <8 | <2 | 5 | 10 | <.5 | <3 | <3 | 31 | .07 | .099 | 18 | 13 | .20 | 132 | .16 | <3 | 3.66 | .02 | .06 | 4 | 2.1 |
| 1770 700E | 1 | 15 | 23 | 99 | <.3 | 14 | 15 | 799 | 2.31 | 7 | <8 | <2 | 5 | 9 | <.5 | <3 | <3 | 31 | .08 | .140 | 10 | 12 | .12 | 99 | .16 | <3 | 4.25 | .02 | .04 | 3 | 1.2 |
| 1770 725E | 1 | 23 | 38 | 188 | .4 | 25 | 15 | 531 | 2.82 | 9 | <8 | <2 | 7 | 11 | <.5 | <3 | <3 | 31 | .09 | .079 | 20 | 15 | .38 | 100 | .09 | <3 | 2.29 | .01 | .06 | 4 | 2.6 |
| 1770 750E | 1 | 19 | 16 | 100 | .4 | 19 | 11 | 334 | 2.35 | 7 | <8 | <2 | 5 | 9 | <.5 | <3 | 3 | 31 | .07 | .077 | 11 | 14 | .19 | 88 | .12 | <3 | 3.04 | .02 | .05 | 3 | 2.3 |
| 1770 775E | <1 | 11 | 17 | 74 | <.3 | 15 | 9 | 295 | 2.16 | 7 | <8 | <2 | 5 | 6 | <.5 | <3 | <3 | 26 | .04 | .049 | 17 | 10 | .21 | 86 | .07 | <3 | 2.19 | .01 | .04 | 2 | 4.7 |
| 1770 800E | 1 | 13 | 16 | 83 | .3 | 20 | 12 | 513 | 2.22 | 3 | <8 | <2 | 6 | 5 | <.5 | <3 | 3 | 26 | .04 | .038 | 18 | 12 | .25 | 121 | .07 | <3 | 2.39 | .01 | .05 | 2 | 10.2 |
| 1770 825E | <1 | 12 | 22 | 86 | <.3 | 19 | 11 | 289 | 2.21 | 5 | <8 | <2 | 6 | 5 | <.5 | <3 | <3 | 22 | .04 | .027 | 24 | 11 | .37 | 110 | .04 | <3 | 1.91 | .01 | .06 | 2 | 13.8 |
| 1770 850E | 1 | 12 | 19 | 76 | <.3 | 13 | 12 | 1027 | 2.26 | 5 | <8 | <2 | 6 | 4 | <.5 | <3 | <3 | 25 | .04 | .028 | 26 | 14 | .28 | 96 | .04 | <3 | 1.78 | <.01 | .06 | 2 | 33.2 |
| 1770 875E | <1 | 17 | 17 | 75 | <.3 | 19 | 12 | 369 | 2.45 | 5 | <8 | <2 | 7 | 4 | <.5 | <3 | <3 | 22 | .03 | .025 | 29 | 13 | .40 | 109 | .04 | <3 | 2.08 | <.01 | .05 | 2 | 10.2 |
| 1770 900E | <1 | 18 | 18 | 69 | <.3 | 20 | 15 | 426 | 2.31 | 7 | <8 | <2 | 7 | 5 | <.5 | <3 | <3 | 26 | .03 | .031 | 21 | 12 | .30 | 100 | .09 | <3 | 2.73 | .01 | .06 | 2 | 12.1 |
| 1770 925E | 1 | 25 | 14 | 74 | .3 | 19 | 15 | 390 | 2.52 | 6 | <8 | <2 | 7 | 5 | <.5 | <3 | 3 | 29 | .04 | .031 | 22 | 13 | .39 | 119 | .07 | <3 | 2.47 | .01 | .06 | 2 | 9.2 |
| RE 1770 825E | 1 | 13 | 20 | 91 | <.3 | 20 | 12 | 299 | 2.31 | 7 | <8 | <2 | 6 | 5 | <.5 | <3 | <3 | 24 | .04 | .028 | 26 | 11 | .39 | 116 | .05 | <3 | 2.01 | .01 | .06 | <2 | 20.2 |
| 1770 950E | <1 | 28 | 23 | 67 | .3 | 19 | 17 | 678 | 2.58 | 7 | <8 | <2 | 7 | 5 | <.5 | 3 | <3 | 33 | .04 | .029 | 21 | 16 | .37 | 111 | .06 | 3 | 2.39 | .01 | .07 | <2 | 4.8 |
| 1770 975E | <1 | 46 | 19 | 83 | .3 | 22 | 17 | 305 | 2.73 | 9 | <8 | <2 | 7 | 5 | <.5 | <3 | 5 | 39 | .04 | .039 | 20 | 11 | .44 | 94 | .07 | 4 | 2.59 | .01 | .07 | <2 | 12.2 |
| 1770 1000E | <1 | 81 | 22 | 86 | .4 | 19 | 25 | 1144 | 2.84 | 11 | <8 | <2 | 5 | 8 | <.5 | <3 | 4 | 47 | .10 | .099 | 17 | 16 | .31 | 88 | .08 | <3 | 2.55 | .01 | .07 | 2 | 1.5 |
| 1870 1000W | <1 | 11 | 20 | 63 | <.3 | 12 | 7 | 151 | 2.22 | 6 | <8 | <2 | 5 | 4 | <.5 | <3 | 6 | 20 | .02 | .031 | 28 | 12 | .27 | 57 | .03 | <3 | 1.47 | <.01 | .05 | <2 | 11.2 |
| 1870 975W | <1 | 16 | 10 | 53 | <.3 | 13 | 6 | 115 | 2.25 | 7 | <8 | <2 | 6 | 5 | <.5 | <3 | <3 | 14 | .03 | .023 | 35 | 12 | .35 | 58 | .02 | <3 | 1.27 | <.01 | .04 | 2 | 13.0 |
| 1870 950W | 1 | 8 | 11 | 40 | <.3 | 8 | 4 | 102 | 2.24 | 5 | <8 | <2 | 5 | 3 | <.5 | <3 | 4 | 21 | .02 | .028 | 26 | 13 | .18 | 52 | .02 | <3 | 1.55 | <.01 | .04 | <2 | 21.1 |
| 1870 925W | 1 | 11 | 12 | 46 | <.3 | 12 | 6 | 121 | 2.06 | 6 | <8 | <2 | 5 | 9 | <.5 | <3 | 3 | 14 | .06 | .020 | 32 | 12 | .36 | 91 | .02 | <3 | 1.33 | <.01 | .05 | <2 | 2.0 |
| 1870 900W | <1 | 13 | 17 | 52 | <.3 | 11 | 5 | 123 | 2.44 | 4 | <8 | <2 | 7 | 5 | <.5 | <3 | <3 | 16 | .03 | .032 | 35 | 12 | .35 | 83 | .01 | <3 | 1.40 | <.01 | .05 | <2 | 3.7 |
| 1870 875W | <1 | 7 | 13 | 48 | <.3 | 10 | 4 | 94 | 2.72 | 6 | <8 | <2 | 4 | 4 | <.5 | <3 | 3 | 23 | .02 | .046 | 16 | 14 | .25 | 48 | .05 | <3 | 2.67 | .01 | .04 | <2 | 25.7 |
| 1870 850W | <1 | 14 | 9 | 45 | <.3 | 12 | 5 | 125 | 2.47 | 6 | <8 | <2 | 7 | 4 | <.5 | <3 | 4 | 15 | .03 | .024 | 32 | 19 | .39 | 44 | .02 | <3 | 1.37 | <.01 | .05 | <2 | 1.5 |
| 1870 825W | 2 | 14 | 21 | 57 | <.3 | 15 | 9 | 176 | 2.77 | 7 | <8 | <2 | 4 | 9 | <.5 | <3 | 4 | 24 | .07 | .042 | 23 | 13 | .33 | 81 | .03 | <3 | 1.87 | .01 | .07 | <2 | 8.8 |
| 1870 800W | 1 | 13 | 12 | 47 | <.3 | 14 | 7 | 100 | 2.44 | 8 | <8 | <2 | 8 | 4 | <.5 | <3 | <3 | 14 | .02 | .030 | 32 | 12 | .37 | 56 | .02 | <3 | 1.48 | <.01 | .03 | 2 | 26.5 |
| STANDARD DS5 | 13 | 146 | 25 | 140 | .3 | 25 | 12 | 779 | 3.04 | 18 | <8 | <2 | 3 | 47 | 5.7 | 5 | 6 | 62 | .76 | .095 | 13 | 188 | .71 | 140 | .11 | 17 | 2.04 | .04 | .15 | 8 | 45.2 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data FA

ACME ANALYTICAL

# Ruby Red Resources Inc. PROJECT EDDY FILE # A404156



ACME ANALYTICAL

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au* ppb |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| G-1 | 1 | <1 | 4 | 45 | <.3 | 5 | 5 | 578 | 2.08 | <2 | <8 | <2 | 4 | 106 | <.5 | <3 | 4 | 41 | .66 | .074 | 11 | 14 | .58 | 296 | .15 | 7 | 1.34 | .22 | .64 | 4 | <.5 |
| 1870 775W | <1 | 7 | 11 | 61 | <.3 | 13 | 7 | 103 | 2.43 | 5 | <8 | <2 | 6 | 5 | <.5 | <3 | <3 | 22 | .03 | .066 | 17 | 11 | .27 | 73 | .05 | <3 | 2.58 | .01 | .05 | <2 | 9.4 |
| 1870 750W | <1 | 6 | 16 | 50 | <.3 | 10 | 6 | 86 | 2.33 | 6 | <8 | <2 | 6 | 4 | <.5 | <3 | <3 | 19 | .02 | .048 | 22 | 9 | .27 | 61 | .02 | 4 | 2.35 | .01 | .05 | <2 | 4.6 |
| 1870 725W | <1 | 12 | 29 | 52 | <.3 | 16 | 19 | 773 | 2.38 | 9 | <8 | <2 | 2 | 19 | <.5 | <3 | 3 | 20 | .16 | .048 | 24 | 12 | .42 | 106 | .02 | <3 | 1.95 | .01 | .06 | <2 | 6.5 |
| 1870 700W | <1 | 13 | 20 | 73 | <.3 | 19 | 10 | 241 | 2.77 | 9 | <8 | <2 | 3 | 9 | <.5 | <3 | <3 | 25 | .07 | .043 | 21 | 16 | .37 | 114 | .03 | <3 | 2.15 | .01 | .07 | <2 | 4.4 |
| 1870 675W | <1 | 10 | 20 | 65 | .3 | 15 | 7 | 146 | 2.33 | 10 | <8 | <2 | 7 | 6 | <.5 | <3 | <3 | 19 | .03 | .031 | 29 | 17 | .41 | 77 | .02 | 3 | 1.67 | .01 | .06 | <2 | 12.7 |
| 1870 650W | <1 | 8 | 10 | 48 | .3 | 12 | 7 | 113 | 2.87 | 7 | <8 | <2 | 7 | 4 | <.5 | <3 | <3 | 16 | .02 | .036 | 33 | 9 | .37 | 52 | .01 | <3 | 1.27 | <.01 | .04 | <2 | 6.0 |
| 1870 625W | <1 | 12 | 16 | 53 | <.3 | 14 | 7 | 97 | 2.46 | 4 | <8 | <2 | 7 | 3 | <.5 | <3 | 4 | 21 | .02 | .059 | 21 | 11 | .28 | 76 | .04 | 5 | 2.95 | .01 | .04 | <2 | 30.3 |
| 1870 600W | <1 | 8 | 11 | 45 | <.3 | 13 | 6 | 92 | 2.01 | 5 | <8 | <2 | 6 | 4 | <.5 | <3 | <3 | 18 | .02 | .018 | 31 | 11 | .39 | 74 | .03 | <3 | 1.16 | .01 | .04 | <2 | 22.2 |
| 1870 575W | <1 | 8 | 12 | 43 | <.3 | 9 | 5 | 74 | 2.17 | 7 | <8 | <2 | 5 | 4 | <.5 | <3 | 3 | 21 | .03 | .042 | 22 | 8 | .24 | 53 | .03 | <3 | 1.96 | .01 | .04 | <2 | 8.4 |
| 1870 550W | <1 | 4 | 11 | 34 | <.3 | 11 | 6 | 72 | 1.48 | 3 | <8 | <2 | 4 | 6 | <.5 | <3 | <3 | 13 | .04 | .016 | 35 | 10 | .45 | 93 | .01 | 3 | 1.19 | .01 | .04 | <2 | 35.9 |
| 1870 525W | <1 | 7 | 18 | 39 | <.3 | 14 | 11 | 224 | 1.89 | 2 | <8 | <2 | 5 | 4 | <.5 | <3 | <3 | 15 | .02 | .017 | 33 | 10 | .45 | 93 | .02 | <3 | 1.25 | .01 | .05 | <2 | 6.7 |
| 1870 500W | <1 | 4 | 7 | 31 | <.3 | 13 | 7 | 76 | 2.22 | 4 | <8 | <2 | 6 | 3 | <.5 | <3 | <3 | 11 | .02 | .018 | 39 | 9 | .50 | 41 | .01 | <3 | 1.08 | <.01 | .04 | <2 | 35.6 |
| 1870 475W | 1 | 3 | 14 | 46 | .6 | 9 | 5 | 113 | 3.86 | 10 | <8 | <2 | 6 | 4 | <.5 | <3 | <3 | 32 | .03 | .035 | 24 | 17 | .22 | 46 | .04 | 3 | 1.54 | .01 | .06 | <2 | 13.5 |
| 1870 450W | <1 | 4 | 14 | 32 | .3 | 6 | 4 | 59 | 2.37 | 5 | <8 | <2 | 5 | 3 | <.5 | <3 | 5 | 32 | .02 | .023 | 23 | 14 | .15 | 52 | .03 | <3 | 1.58 | .01 | .04 | <2 | 6.5 |
| 1870 425W | <1 | 7 | 13 | 39 | <.3 | 13 | 7 | 99 | 3.04 | 7 | <8 | <2 | 6 | 5 | <.5 | <3 | <3 | 24 | .03 | .025 | 26 | 18 | .27 | 94 | .03 | 3 | 1.84 | .01 | .05 | <2 | 8.7 |
| 1870 400W | <1 | 9 | 14 | 40 | <.3 | 12 | 8 | 111 | 2.23 | 3 | <8 | <2 | 5 | 4 | <.5 | <3 | 3 | 23 | .02 | .058 | 13 | 9 | .19 | 72 | .06 | <3 | 3.13 | .01 | .04 | <2 | 39.6 |
| RE 1870 300W | <1 | 13 | 15 | 52 | .3 | 12 | 7 | 112 | 2.36 | 5 | <8 | <2 | 7 | 3 | <.5 | <3 | <3 | 20 | .01 | .028 | 24 | 13 | .34 | 59 | .03 | <3 | 1.88 | .01 | .04 | <2 | 4.7 |
| 1870 375W | <1 | 9 | 21 | 57 | <.3 | 11 | 8 | 116 | 2.91 | 6 | <8 | <2 | 8 | 3 | <.5 | <3 | <3 | 24 | .02 | .061 | 21 | 21 | .24 | 64 | .03 | <3 | 2.89 | .01 | .05 | <2 | 6.8 |
| 1870 350W | <1 | 9 | 14 | 51 | <.3 | 11 | 6 | 98 | 2.26 | 2 | <8 | <2 | 6 | 6 | <.5 | <3 | <3 | 25 | .04 | .059 | 14 | 10 | .22 | 72 | .06 | <3 | 2.84 | .01 | .05 | <2 | 24.1 |
| 1870 325W | <1 | 3 | 15 | 59 | .6 | 9 | 5 | 268 | 2.81 | 7 | <8 | <2 | 6 | 4 | <.5 | <3 | <3 | 28 | .04 | .042 | 24 | 12 | .25 | 54 | .02 | <3 | 1.84 | .01 | .06 | <2 | 12.3 |
| 1870 300W | <1 | 13 | 16 | 51 | <.3 | 13 | 7 | 112 | 2.34 | 6 | 10 | <2 | 7 | 3 | <.5 | <3 | <3 | 19 | .01 | .028 | 24 | 10 | .35 | 59 | .03 | <3 | 1.86 | .01 | .04 | <2 | 8.1 |
| 1870 275W | <1 | 12 | 20 | 54 | .3 | 15 | 11 | 202 | 2.13 | 5 | <8 | <2 | 6 | 8 | <.5 | <3 | <3 | 21 | .06 | .023 | 30 | 12 | .44 | 41 | .02 | 3 | 1.37 | .01 | .05 | <2 | 22.2 |
| 1870 250W | <1 | 15 | 11 | 59 | .4 | 10 | 6 | 94 | 1.94 | <2 | <8 | <2 | 5 | 6 | <.5 | <3 | <3 | 27 | .04 | .102 | 10 | 7 | .13 | 55 | .11 | <3 | 3.58 | .02 | .04 | <2 | 7.5 |
| 1870 225W | <1 | 13 | 11 | 74 | .3 | 12 | 7 | 169 | 2.21 | 4 | <8 | <2 | 5 | 7 | <.5 | <3 | <3 | 26 | .05 | .067 | 12 | 7 | .24 | 64 | .09 | <3 | 3.28 | .02 | .04 | <2 | 2.9 |
| 1870 200W | 1 | 10 | 41 | 98 | .4 | 12 | 7 | 295 | 2.36 | 7 | <8 | <2 | 6 | 5 | <.5 | <3 | 3 | 23 | .04 | .050 | 19 | 12 | .29 | 69 | .05 | <3 | 2.24 | .01 | .05 | 2 | 10.0 |
| 1870 175W | <1 | 13 | 65 | 123 | 1.0 | 11 | 8 | 257 | 2.48 | <2 | <8 | <2 | 6 | 5 | <.5 | <3 | 5 | 31 | .04 | .083 | 8 | 12 | .15 | 68 | .13 | 4 | 4.19 | .02 | .04 | <2 | 3.1 |
| 1870 150W | 1 | 14 | 62 | 106 | .3 | 14 | 8 | 138 | 2.46 | 4 | <8 | <2 | 7 | 5 | <.5 | <3 | <3 | 25 | .04 | .059 | 13 | 10 | .28 | 64 | .07 | <3 | 2.90 | .01 | .04 | <2 | 2.5 |
| 1870 125W | <1 | 12 | 55 | 91 | .6 | 18 | 10 | 405 | 3.06 | 7 | <8 | <2 | 7 | 6 | <.5 | <3 | <3 | 30 | .04 | .066 | 14 | 12 | .24 | 76 | .08 | <3 | 3.16 | .01 | .05 | <2 | 2.2 |
| 1870 100W | <1 | 14 | 30 | 70 | .3 | 14 | 11 | 254 | 2.68 | 4 | <8 | <2 | 7 | 4 | <.5 | <3 | <3 | 28 | .03 | .062 | 19 | 11 | .33 | 50 | .07 | <3 | 2.31 | .01 | .05 | <2 | 2.6 |
| 1870 075W | <1 | 19 | 58 | 99 | .3 | 15 | 20 | 809 | 2.84 | 6 | <8 | <2 | 7 | 5 | <.5 | <3 | <3 | 33 | .05 | .104 | 9 | 13 | .16 | 64 | .13 | <3 | 4.65 | .01 | .05 | <2 | 2.0 |
| 1870 050W | <1 | 8 | 26 | 120 | <.3 | 12 | 8 | 582 | 2.55 | 3 | <8 | <2 | 3 | 7 | <.5 | <3 | <3 | 37 | .07 | .060 | 7 | 5 | .14 | 92 | .13 | <3 | 2.89 | .02 | .05 | 2 | 3.2 |
| 1870 025W | <1 | 20 | 27 | 104 | <.3 | 20 | 13 | 254 | 2.16 | 2 | <8 | <2 | 5 | 5 | <.5 | <3 | <3 | 26 | .03 | .043 | 13 | 14 | .29 | 98 | .08 | <3 | 3.26 | .01 | .05 | <2 | 1.9 |
| 1870 000W | <1 | 6 | 27 | 70 | <.3 | 9 | 8 | 527 | 2.28 | 4 | <8 | <2 | 3 | 4 | <.5 | <3 | <3 | 32 | .02 | .029 | 18 | 11 | .19 | 70 | .04 | <3 | 1.93 | .01 | .05 | <2 | 11.1 |
| STANDARD DS5 | 12 | 140 | 26 | 138 | .3 | 25 | 12 | 750 | 2.99 | 19 | <8 | <2 | 3 | 45 | 5.5 | 5 | 7 | 59 | .72 | .091 | 13 | 185 | .68 | 137 | .10 | 16 | 2.00 | .04 | .14 | 5 | 41.4 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data FA

ACME AN[ALY]TICAL LABORATORIES LTD. 852 E. HASTINGS ST. [VAN]COUVER BC V6A 1R6 PHONE(604)253-3158 FAX(60[4]2[5]3-1716
(IS[O 9]002 Accredited Co.)

# GEOCHEMICAL ANALYSIS CERTIFICATE

**Ruby Red Resources Inc.** File # A406457 Page 1

207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 2750N 425E | .9 | 55.9 | 32.4 | 79 | .4 | 21.6 | 11.5 | 347 | 3.71 | 6.6 | 1.5 | 4.9 | 4.7 | 15 | .5 | .3 | .5 | 86 | .17 | .047 | 30 | 24.7 | .48 | 128 | .095 | 2 | 3.38 | .009 | .06 | .2 | .07 | 8.0 | .1 | <.05 | 10 | .8 | 7.5 |
| 2750N 450E | .7 | 26.9 | 22.2 | 38 | .1 | 8.6 | 3.9 | 102 | 1.94 | 3.3 | 1.1 | 4.1 | 2.9 | 8 | .1 | .1 | .3 | 37 | .08 | .033 | 18 | 10.4 | .26 | 41 | .110 | <1 | 1.50 | .014 | .03 | .1 | .07 | 3.4 | <.1 | <.05 | 10 | <.5 | 15.0 |
| 2750N 475E | .5 | 21.7 | 16.6 | 51 | .2 | 12.5 | 6.1 | 142 | 2.62 | 3.1 | .5 | 17.2 | 2.4 | 7 | .1 | .1 | .4 | 58 | .10 | .027 | 17 | 14.9 | .44 | 78 | .053 | 1 | 1.48 | .005 | .04 | .1 | .02 | 2.5 | .1 | <.05 | 9 | <.5 | 7.5 |
| 2750N 500E | .6 | 39.7 | 24.9 | 60 | .3 | 15.1 | 7.4 | 160 | 2.75 | 3.7 | 1.1 | 2.8 | 2.5 | 9 | .4 | .2 | .5 | 61 | .11 | .030 | 44 | 18.7 | .47 | 92 | .066 | 1 | 2.39 | .009 | .05 | .1 | .05 | 4.9 | .1 | <.05 | 9 | .5 | 7.5 |
| 2750N 525E | .4 | 29.1 | 19.1 | 36 | .2 | 6.8 | 2.9 | 138 | 1.25 | 1.7 | .8 | 7.6 | 1.1 | 11 | .3 | .1 | .4 | 34 | .14 | .022 | 24 | 9.8 | .21 | 71 | .037 | 1 | 1.13 | .007 | .04 | .1 | .03 | 2.6 | .1 | <.05 | 6 | <.5 | 15.0 |
| 2750N 550E | .9 | 41.5 | 32.8 | 71 | .3 | 17.5 | 16.4 | 1644 | 3.17 | 4.1 | 1.3 | 10.9 | 1.2 | 19 | .5 | .2 | .5 | 72 | .25 | .073 | 22 | 19.2 | .52 | 126 | .056 | <1 | 2.52 | .010 | .06 | .1 | .09 | 4.3 | .1 | <.05 | 10 | .5 | 15.0 |
| 2750N 575E | .5 | 35.0 | 28.0 | 95 | .2 | 17.2 | 14.1 | 773 | 2.48 | 3.8 | 1.2 | 6.4 | 1.9 | 19 | .7 | .2 | .3 | 55 | .26 | .053 | 23 | 21.9 | .65 | 94 | .043 | 1 | 1.79 | .007 | .07 | .1 | .06 | 3.6 | .1 | <.05 | 6 | <.5 | 15.0 |
| 2750N 600E | .6 | 24.6 | 29.2 | 79 | .3 | 15.5 | 8.3 | 593 | 2.52 | 4.7 | 1.0 | 4.1 | 1.3 | 25 | .9 | .2 | .4 | 51 | .29 | .041 | 21 | 21.4 | .50 | 122 | .044 | 1 | 1.92 | .007 | .06 | .1 | .06 | 2.6 | .1 | <.05 | 7 | <.5 | 7.5 |
| 2750N 625E | 1.0 | 25.7 | 21.6 | 63 | .2 | 10.9 | 5.8 | 170 | 3.50 | 6.5 | 1.4 | 3.5 | 2.2 | 15 | .4 | .2 | .4 | 54 | .16 | .036 | 15 | 15.4 | .31 | 119 | .080 | 1 | 1.92 | .008 | .05 | .1 | .07 | 2.2 | .1 | <.05 | 11 | <.5 | 7.5 |
| 2750N 650E | .8 | 28.1 | 34.4 | 88 | .3 | 18.7 | 15.2 | 599 | 3.31 | 5.7 | 1.4 | 4.6 | 2.3 | 17 | .2 | .1 | .5 | 71 | .18 | .050 | 18 | 28.2 | .54 | 98 | .055 | 1 | 2.60 | .009 | .06 | .1 | .07 | 3.5 | .1 | <.05 | 9 | <.5 | 7.5 |
| 2650N 425E | .6 | 32.5 | 31.0 | 99 | .2 | 19.2 | 19.2 | 1374 | 2.60 | 3.9 | 1.3 | 8.9 | 1.6 | 21 | .7 | .2 | .4 | 53 | .29 | .049 | 23 | 22.1 | .53 | 103 | .049 | 1 | 1.82 | .009 | .06 | .1 | .05 | 3.4 | .1 | <.05 | 6 | .5 | 7.5 |
| 2650N 450E | .9 | 35.5 | 42.3 | 133 | .3 | 24.3 | 25.2 | 598 | 2.28 | 5.2 | 2.1 | 38.8 | 1.2 | 14 | .8 | .2 | .5 | 73 | .15 | .049 | 40 | 21.4 | .45 | 109 | .051 | 1 | 2.09 | .009 | .07 | .1 | .05 | 3.2 | .2 | <.05 | 9 | .6 | 15.0 |
| 2650N 475E | .6 | 21.0 | 15.4 | 70 | .1 | 13.8 | 8.4 | 293 | 2.28 | 3.2 | .7 | 14.0 | 2.8 | 6 | .3 | .2 | .3 | 53 | .07 | .023 | 14 | 14.0 | .44 | 47 | .062 | <1 | 1.23 | .007 | .05 | .1 | .03 | 2.2 | .1 | <.05 | 6 | <.5 | 7.5 |
| RE 2650N 475E | .7 | 22.8 | 15.7 | 73 | .2 | 14.0 | 8.5 | 296 | 2.39 | 3.4 | .7 | 24.9 | 2.8 | 7 | .3 | .2 | .3 | 56 | .08 | .025 | 15 | 15.3 | .48 | 50 | .067 | 1 | 1.34 | .007 | .05 | <.1 | .03 | 2.2 | .1 | <.05 | 7 | <.5 | 7.5 |
| 2650N 500E | .8 | 32.0 | 33.5 | 88 | .3 | 22.2 | 29.9 | 1591 | 2.88 | 4.7 | 1.4 | 35.2 | 2.5 | 9 | .5 | .3 | .5 | 55 | .06 | .031 | 22 | 18.5 | .46 | 83 | .069 | 1 | 1.76 | .008 | .08 | .1 | .06 | 2.5 | .1 | <.05 | 8 | <.5 | 15.0 |
| 2650N 525E | .7 | 22.4 | 23.2 | 40 | .3 | 9.6 | 5.7 | 153 | 2.12 | 2.6 | .8 | 5.5 | 2.4 | 7 | .3 | .1 | .4 | 42 | .05 | .025 | 10 | 11.2 | .28 | 46 | .130 | 1 | 1.05 | .014 | .04 | .1 | .04 | 1.6 | <.1 | <.05 | 8 | <.5 | 15.0 |
| 2650N 550E | .6 | 16.9 | 18.6 | 51 | .2 | 9.5 | 6.7 | 378 | 1.64 | 2.0 | .7 | 14.9 | 1.8 | 11 | .1 | .1 | .3 | 41 | .10 | .021 | 15 | 11.3 | .34 | 52 | .065 | <1 | .92 | .007 | .05 | .1 | .02 | 1.6 | .1 | <.05 | 6 | <.5 | 15.0 |
| 2650N 575E | .9 | 21.5 | 28.0 | 40 | .2 | 10.3 | 6.0 | 162 | 1.80 | 9.5 | 1.3 | 2.0 | 1.4 | 13 | .2 | .1 | .4 | 48 | .11 | .026 | 14 | 13.7 | .28 | 55 | .095 | <1 | 1.37 | .012 | .05 | .1 | .03 | 1.6 | .1 | <.05 | 10 | <.5 | 15.0 |
| 2650N 600E | .6 | 12.2 | 12.6 | 56 | .3 | 6.2 | 4.0 | 164 | 2.85 | 4.3 | .7 | 1.5 | 3.0 | 10 | .2 | .2 | .3 | 39 | .14 | .248 | 9 | 11.2 | .21 | 59 | .103 | 1 | 1.94 | .009 | .03 | .1 | .08 | 1.7 | <.1 | <.05 | 13 | .5 | 15.0 |
| 2650N 625E | .4 | 51.0 | 11.6 | 51 | .5 | 15.5 | 8.8 | 312 | 2.72 | 7.7 | .8 | 1.6 | 1.3 | 12 | .2 | .2 | .2 | 78 | .21 | .029 | 10 | 28.6 | .50 | 61 | .070 | 1 | 1.77 | .012 | .04 | .1 | .04 | 4.9 | .1 | <.05 | 7 | <.5 | 15.0 |
| 2650N 650E | 1.1 | 109.1 | 26.0 | 64 | .4 | 20.5 | 23.5 | 1729 | 3.71 | 14.8 | 2.6 | 18.3 | 2.3 | 20 | .4 | .3 | .3 | 120 | .21 | .076 | 30 | 50.1 | .52 | 111 | .086 | <1 | 2.79 | .010 | .07 | .1 | .06 | 11.9 | .1 | <.05 | 10 | .9 | 7.5 |
| 50N 0E | .8 | 16.2 | 12.8 | 146 | .1 | 28.8 | 9.8 | 282 | 2.03 | 3.9 | .6 | 2.1 | 3.7 | 8 | .3 | .2 | .3 | 28 | .09 | .073 | 11 | 16.2 | .44 | 100 | .065 | 1 | 2.03 | .009 | .08 | .1 | .03 | 1.8 | .1 | <.05 | 6 | <.5 | 15.0 |
| 50N 25E | .9 | 8.0 | 12.2 | 78 | .1 | 14.8 | 9.1 | 196 | 2.06 | 3.6 | .5 | <.5 | 3.0 | 8 | .2 | .1 | .3 | 32 | .09 | .131 | 8 | 13.9 | .26 | 67 | .085 | 1 | 2.27 | .012 | .06 | .1 | .05 | 1.6 | .1 | <.05 | 8 | <.5 | 15.0 |
| 50N 50E | .7 | 15.2 | 14.0 | 59 | .1 | 22.0 | 12.1 | 187 | 2.00 | 4.7 | .6 | 1.8 | 4.5 | 7 | .1 | .2 | .2 | 31 | .10 | .135 | 7 | 17.0 | .38 | 63 | .084 | 1 | 2.40 | .010 | .06 | .1 | .04 | 2.0 | .1 | <.05 | 6 | <.5 | 15.0 |
| 50N 75E | .6 | 11.9 | 10.8 | 67 | <.1 | 17.0 | 10.8 | 194 | 1.79 | 3.3 | .4 | .6 | 3.3 | 6 | .1 | .2 | .2 | 28 | .07 | .080 | 8 | 13.6 | .32 | 68 | .075 | 1 | 1.98 | .010 | .05 | .1 | .05 | 1.6 | .1 | <.05 | 6 | <.5 | 15.0 |
| 50N 100E | .7 | 17.2 | 12.9 | 61 | <.1 | 21.2 | 11.7 | 293 | 1.89 | 3.8 | .6 | 1.0 | 4.0 | 7 | .1 | .2 | .2 | 32 | .09 | .062 | 8 | 17.2 | .37 | 67 | .091 | <1 | 2.38 | .011 | .06 | .1 | .04 | 2.3 | .1 | <.05 | 7 | <.5 | 15.0 |
| 50N 125E | .8 | 14.4 | 13.6 | 67 | .1 | 19.5 | 10.0 | 271 | 1.82 | 3.4 | .9 | 1.4 | 4.5 | 7 | .1 | .2 | .2 | 30 | .07 | .077 | 8 | 13.8 | .27 | 83 | .109 | 1 | 2.80 | .011 | .07 | .1 | .04 | 2.4 | .1 | <.05 | 8 | <.5 | 15.0 |
| 50N 150E | .5 | 15.0 | 14.6 | 48 | <.1 | 17.3 | 9.8 | 141 | 1.97 | 4.1 | .4 | 4.1 | 3.9 | 5 | <.1 | .2 | .2 | 37 | .09 | .033 | 9 | 18.7 | .40 | 48 | .062 | 1 | 1.58 | .007 | .06 | .1 | .02 | 2.0 | .1 | <.05 | 6 | <.5 | 15.0 |
| 50N 175E | .4 | 15.8 | 19.4 | 57 | <.1 | 12.3 | 6.5 | 129 | 1.87 | 3.9 | .4 | 16.3 | 4.3 | 4 | .1 | .2 | .2 | 36 | .09 | .055 | 11 | 18.8 | .42 | 41 | .046 | <1 | 1.19 | .006 | .06 | .1 | .01 | 1.8 | .1 | <.05 | 5 | <.5 | 15.0 |
| 50N 200E | .5 | 25.6 | 22.3 | 111 | .1 | 22.7 | 11.7 | 422 | 1.96 | 4.1 | .4 | 15.2 | 3.5 | 8 | .3 | .2 | .2 | 35 | .11 | .052 | 9 | 22.2 | .56 | 67 | .072 | 1 | 1.87 | .008 | .08 | .1 | .02 | 2.5 | .1 | <.05 | 6 | <.5 | 15.0 |
| 50N 225E | .4 | 18.3 | 15.7 | 78 | .1 | 23.2 | 11.3 | 329 | 1.86 | 3.5 | .6 | 1.8 | 3.1 | 8 | .2 | .1 | .2 | 36 | .11 | .090 | 7 | 20.6 | .37 | 90 | .090 | <1 | 2.02 | .013 | .08 | .1 | .03 | 2.5 | .1 | <.05 | 7 | <.5 | 15.0 |
| 50N 250E | .5 | 19.3 | 16.6 | 86 | .1 | 16.5 | 6.8 | 265 | 2.30 | 4.3 | .6 | <.5 | 5.3 | 12 | .2 | .4 | .3 | 36 | .21 | .031 | 27 | 29.2 | 1.37 | 43 | .087 | <1 | 2.32 | .005 | .10 | .1 | .01 | 2.5 | .1 | <.05 | 8 | <.5 | 15.0 |
| 50N 275E | .3 | 21.8 | 15.4 | 54 | <.1 | 21.4 | 8.6 | 145 | 2.17 | 4.5 | .6 | 3.8 | 4.3 | 7 | .1 | .2 | .2 | 44 | .11 | .022 | 11 | 33.4 | .73 | 52 | .053 | 1 | 1.47 | .005 | .08 | <.1 | .02 | 2.5 | .1 | <.05 | 5 | <.5 | 15.0 |
| STANDARD DS5 | 13.2 | 145.8 | 25.9 | 140 | .3 | 25.8 | 11.8 | 806 | 3.04 | 17.9 | 6.9 | 45.0 | 2.9 | 46 | 5.9 | 4.6 | 6.3 | 63 | .74 | .093 | 12 | 196.3 | .72 | 131 | .099 | 17 | 1.92 | .033 | .14 | 5.0 | .20 | 3.5 | 1.0 | <.05 | 6 | 5.0 | 15.0 |

GROUP 1DX - 15.0 GM SAMPLE LEACHED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 300 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: SOIL SS80 60C <u>Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.</u>

Data ✓ FA ____ DATE RECEIVED: OCT 19 2004 DATE REPORT MAILED: Nov. 9/04

BRITISH COLUMBIA CERTIFIED ASSAYER
C. L.
Clarence Leong

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 50N 300E | .5 | 22.2 | 20.0 | 99 | .1 | 27.2 | 13.1 | 270 | 2.43 | 5.5 | 1.2 | 3.6 | 8.3 | 15 | .3 | .2 | .3 | 30 |
| 50N 325E | 1.5 | 25.2 | 54.3 | 181 | .1 | 29.4 | 10.9 | 366 | 3.49 | 5.8 | .9 | 3.3 | 7.4 | 11 | .4 | .3 | .3 | 45 |
| 50N 350E | 1.3 | 13.1 | 30.3 | 177 | .1 | 28.7 | 10.8 | 495 | 2.27 | 3.7 | .7 | 1.3 | 4.2 | 16 | .8 | .2 | .3 | 37 |
| 50N 375E | .5 | 143.7 | 12.9 | 110 | .2 | 25.9 | 22.9 | 390 | 3.70 | 4.8 | .6 | 1.2 | 3.6 | 12 | .3 | .2 | .2 | 118 |
| 50N 400E | .6 | 176.2 | 20.3 | 110 | .5 | 18,3 | 15.1 | 488 | 2.77 | 5.8 | .4 | 2.2 | 2.7 | 9 | .5 | .3 | .2 | 72 |
| 50N 425E | .8 | 44.6 | 11.5 | 96 | .5 | 14.9 | 12.6 | 484 | 2.10 | 7.0 | .6 | <.5 | 3.0 | 7 | .4 | .2 | .2 | 48 |
| 50N 450E | .5 | 76.6 | 17.6 | 104 | .1 | 19.9 | 20.8 | 579 | 2.84 | 9.9 | .3 | .8 | 2.3 | 8 | .3 | .2 | .2 | 77 |
| 50N 475E | .6 | 28.6 | 21.9 | 81 | .1 | 20.5 | 17.4 | 387 | 2.64 | 10.7 | .3 | 3.0 | 2.4 | 7 | .3 | .3 | .2 | 75 |
| 50N 500E | .5 | 23.2 | 18.4 | 89 | .2 | 12.1 | 11.5 | 596 | 2.32 | 4.0 | .4 | 2.5 | 2.8 | 5 | .3 | .2 | .2 | 54 |
| 300E 3000N | .4 | 10.4 | 8.3 | 21 | .1 | 4.2 | 2.5 | 89 | 1.47 | 1.6 | .3 | 13.1 | 2.4 | 4 | .1 | .2 | .2 | 41 |
| 300E 2975N | .4 | 7.7 | 14.1 | 32 | .1 | 5.4 | 3.3 | 126 | 1.82 | 2.7 | .4 | 12.5 | 2.7 | 6 | .1 | .2 | .3 | 46 |
| 300E 2950N | .7 | 20.2 | 16.9 | 61 | .1 | 9.4 | 7.3 | 206 | 2.57 | 3.4 | .7 | 8.4 | 3.9 | 6 | .2 | .1 | .3 | 45 |
| 300E 2925N | .5 | 42.2 | 12.4 | 64 | <.1 | 21.8 | 12.0 | 188 | 3.13 | 4.9 | .8 | 13.2 | 5.3 | 3 | .1 | .2 | .2 | 70 |
| 300E 2900N | .4 | 14.8 | 20.7 | 67 | .1 | 6.3 | 4.3 | 2326 | 1.91 | 3.0 | .3 | 3.2 | 2.2 | 10 | .2 | .3 | .3 | 52 |
| 300E 2875N | .6 | 30.0 | 13.3 | 50 | .1 | 14.3 | 9.5 | 207 | 2.73 | 3.3 | .8 | 22.0 | 3.1 | 5 | .1 | .2 | .2 | 57 |
| 300E 2850N | .7 | 25.2 | 15.0 | 54 | .2 | 8.8 | 5.6 | 157 | 3.09 | 4.5 | .6 | 3.3 | 3.3 | 6 | .1 | .3 | .3 | 53 |
| 300E 2825N | .4 | 61.4 | 13.8 | 76 | .1 | 21.7 | 13.3 | 201 | 4.08 | 4.7 | .7 | 17.3 | 5.7 | 8 | .1 | .3 | .2 | 97 |
| RE 300E 2825N | .5 | 63.3 | 13.8 | 71 | .1 | 22.4 | 13.4 | 201 | 4.07 | 4.6 | .7 | 12.8 | 5.7 | 8 | .1 | .2 | .2 | 97 |
| 300E 2800N | .5 | 30.2 | 16.2 | 93 | .1 | 18.2 | 13.2 | 488 | 3.24 | 3.3 | .6 | 4.1 | 4.5 | 7 | .1 | .2 | .3 | 68 |
| 300E 2775N | .9 | 93.6 | 25.3 | 59 | .2 | 29.7 | 13.3 | 462 | 5.26 | 5.3 | 2.6 | 3.1 | 8.8 | 14 | .3 | .3 | .5 | 116 |
| 300E 2750N | 1.0 | 65.8 | 36.9 | 74 | .5 | 23.3 | 12.2 | 306 | 5.05 | 5.1 | 1.1 | 3.1 | 5.6 | 13 | .3 | .3 | .6 | 104 |
| 300E 2725N | .6 | 54.3 | 28.3 | 85 | .5 | 21.7 | 7.6 | 349 | 3.26 | 5.3 | 1.3 | 1.7 | 2.6 | 15 | .4 | .2 | .5 | 66 |
| 300E 2700N | .5 | 61.7 | 38.2 | 85 | .4 | 21.2 | 9.9 | 229 | 2.05 | 3.2 | 1.8 | 10.9 | 1.5 | 14 | .4 | .2 | .5 | 56 |
| 300E 2675N | .9 | 41.9 | 55.7 | 50 | .2 | 12.8 | 21.6 | 389 | 2.37 | 3.1 | 1.3 | 32.3 | 4.4 | 26 | .6 | .5 | .5 | 51 |
| 300E 2650N | .7 | 67.4 | 35.0 | 59 | .5 | 14.4 | 12.7 | 444 | 2.74 | 3.7 | 2.0 | 2.7 | .8 | 16 | .8 | .2 | .4 | 49 |
| 300E 2625N | .6 | 23.3 | 28.2 | 67 | .2 | 14.8 | 8.9 | 275 | 2.74 | 4.6 | 1.0 | 4.1 | 3.1 | 14 | .3 | .3 | .4 | 61 |
| 300E 2600N | .5 | 12.2 | 18.1 | 55 | .1 | 7.7 | 5.1 | 235 | 1.62 | 2.3 | .4 | 10.1 | 1.7 | 11 | <.1 | .1 | .4 | 47 |
| 300E 2575N | .5 | 33.3 | 26.0 | 84 | .1 | 15.6 | 14.6 | 663 | 2.46 | 3.9 | .9 | 32.7 | 2.5 | 14 | .3 | .3 | .3 | 51 |
| 300E 2550N | .4 | 28.6 | 26.1 | 92 | .2 | 15.1 | 12.8 | 925 | 2.22 | 4.0 | .8 | 5.2 | 2.0 | 21 | .5 | .2 | .3 | 41 |
| 300E 2525N | .3 | 67.3 | 36.1 | 56 | .4 | 14.1 | 2.7 | 33 | .57 | 1.8 | 2.8 | 4.1 | .2 | 16 | 1.2 | .3 | .3 | 13 |
| 300E 2500N | .5 | 22.0 | 18.5 | 52 | .3 | 12.4 | 7.1 | 319 | 2.55 | 5.4 | .6 | 22.0 | 4.1 | 6 | .3 | .3 | .3 | 58 |
| 400E 3300N | .9 | 27.5 | 21.6 | 38 | .2 | 11.6 | 14.5 | 1137 | 1.92 | 2.3 | .8 | 1.4 | 1.2 | 13 | .2 | .1 | .3 | 36 |
| 400E 3275N | 2.5 | 45.8 | 31.1 | 52 | .3 | 14.0 | 42.5 | 4891 | 4.82 | 6.6 | 1.6 | 3.9 | 1.4 | 20 | .5 | .1 | .5 | 76 |
| STANDARD DS5 | 12.7 | 143.2 | 25.7 | 136 | .3 | 23.9 | 11.8 | 781 | 2.99 | 17.5 | 6.0 | 44.1 | 2.8 | 45 | 5.4 | 3.9 | 6.0 | 59 |

| SAMPLE# | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 50N 300E | .14 | .080 | 32 | 18.5 | .60 | 142 | .122 | 1 | 3.01 | .014 | .13 | .1 | .03 | 2.5 | .1 | <.05 | 9 | <.5 | 15.0 |
| 50N 325E | .10 | .046 | 14 | 31.2 | 1.21 | 94 | .171 | 1 | 2.92 | .010 | .22 | .3 | .04 | 4.0 | .3 | <.05 | 12 | <.5 | 15.0 |
| 50N 350E | .20 | .082 | 11 | 17.9 | .51 | 69 | .151 | 2 | 2.71 | .016 | .09 | .2 | .06 | 2.7 | .1 | <.05 | 10 | <.5 | 15.0 |
| 50N 375E | .15 | .047 | 10 | 19.8 | 1.00 | 110 | .128 | 1 | 2.57 | .011 | .11 | <.1 | .03 | 6.5 | .1 | <.05 | 9 | .5 | 15.0 |
| 50N 400E | .16 | .059 | 6 | 14.5 | .36 | 74 | .143 | 1 | 2.23 | .016 | .07 | .2 | .04 | 2.9 | .1 | <.05 | 10 | <.5 | 15.0 |
| 50N 425E | .10 | .110 | 4 | 12.4 | .20 | 57 | .157 | 2 | 3.72 | .018 | .05 | .2 | .07 | 2.8 | .1 | <.05 | 9 | <.5 | 15.0 |
| 50N 450E | .19 | .063 | 5 | 12.4 | .37 | 63 | .115 | 1 | 2.50 | .016 | .08 | .2 | .03 | 3.2 | .1 | <.05 | 9 | <.5 | 15.0 |
| 50N 475E | .14 | .069 | 5 | 14.6 | .36 | 52 | .135 | <1 | 2.74 | .016 | .06 | .2 | .04 | 3.2 | .1 | <.05 | 10 | <.5 | 15.0 |
| 50N 500E | .11 | .072 | 7 | 21.2 | .35 | 50 | .104 | 2 | 2.02 | .012 | .05 | .1 | .04 | 2.4 | .1 | <.05 | 9 | <.5 | 15.0 |
| 300E 3000N | .04 | .023 | 14 | 6.7 | .14 | 59 | .060 | 1 | .82 | .008 | .02 | <.1 | .02 | 1.1 | .1 | <.05 | 7 | <.5 | 15.0 |
| 300E 2975N | .08 | .027 | 13 | 9.5 | .20 | 64 | .057 | <1 | 1.30 | .008 | .03 | .1 | .04 | 1.4 | .1 | <.05 | 8 | <.5 | 15.0 |
| 300E 2950N | .06 | .038 | 13 | 12.1 | .25 | 68 | .086 | 1 | 1.98 | .012 | .04 | .1 | .06 | 2.5 | .1 | <.05 | 10 | .5 | 15.0 |
| 300E 2925N | .05 | .039 | 15 | 28.4 | .73 | 64 | .073 | 1 | 2.32 | .003 | .04 | <.1 | .03 | 4.2 | .1 | <.05 | 6 | <.5 | 15.0 |
| 300E 2900N | .12 | .039 | 12 | 12.0 | .16 | 143 | .061 | 1 | 1.07 | .009 | .05 | .1 | .04 | 1.6 | .1 | <.05 | 8 | <.5 | 15.0 |
| 300E 2875N | .06 | .029 | 15 | 17.7 | .54 | 53 | .095 | <1 | 1.89 | .008 | .04 | .1 | .03 | 3.8 | .1 | <.05 | 8 | <.5 | 15.0 |
| 300E 2850N | .08 | .042 | 8 | 13.2 | .20 | 60 | .089 | 1 | 2.53 | .009 | .04 | .1 | .14 | 2.3 | .1 | <.05 | 10 | .5 | 15.0 |
| 300E 2825N | .10 | .037 | 14 | 23.4 | .86 | 66 | .080 | <1 | 2.35 | .004 | .05 | <.1 | .03 | 5.7 | .1 | <.05 | 7 | <.5 | 7.5 |
| RE 300E 2825N | .10 | .034 | 14 | 23.2 | .87 | 65 | .078 | <1 | 2.51 | .004 | .04 | <.1 | .03 | 5.3 | <.1 | <.05 | 7 | <.5 | 7.5 |
| 300E 2800N | .08 | .032 | 16 | 21.1 | .58 | 89 | .083 | 2 | 2.28 | .008 | .05 | .1 | .04 | 3.4 | .1 | <.05 | 10 | <.5 | 15.0 |
| 300E 2775N | .13 | .054 | 47 | 31.2 | .47 | 146 | .091 | <1 | 4.54 | .013 | .07 | <.1 | .07 | 15.0 | .1 | <.05 | 16 | .7 | 15.0 |
| 300E 2750N | .14 | .037 | 20 | 26.1 | .42 | 131 | .156 | 1 | 3.73 | .015 | .07 | .1 | .13 | 6.1 | .1 | <.05 | 18 | .5 | 7.5 |
| 300E 2725N | .18 | .051 | 20 | 24.1 | .42 | 126 | .103 | 1 | 3.81 | .013 | .07 | .1 | .09 | 5.1 | .1 | <.05 | 12 | .5 | 7.5 |
| 300E 2700N | .16 | .054 | 39 | 23.7 | .49 | 126 | .082 | 1 | 3.60 | .011 | .08 | .1 | .09 | 6.7 | .1 | <.05 | 12 | .5 | 15.0 |
| 300E 2675N | .32 | .017 | 36 | 13.1 | .31 | 143 | .121 | 2 | 2.02 | .013 | .08 | .1 | .07 | 4.7 | .1 | <.05 | 11 | .5 | 15.0 |
| 300E 2650N | .22 | .057 | 29 | 22.0 | .37 | 97 | .060 | 1 | 2.65 | .010 | .06 | .1 | .11 | 3.4 | .1 | <.05 | 10 | <.5 | 7.5 |
| 300E 2625N | .17 | .033 | 12 | 29.0 | .49 | 71 | .080 | <1 | 2.16 | .007 | .05 | .1 | .08 | 3.2 | .1 | <.05 | 7 | .6 | 7.5 |
| 300E 2600N | .16 | .016 | 14 | 12.5 | .26 | 72 | .067 | 1 | 1.15 | .008 | .04 | .1 | .02 | 1.6 | .1 | <.05 | 7 | <.5 | 7.5 |
| 300E 2575N | .24 | .033 | 17 | 21.2 | .61 | 64 | .062 | 2 | 1.74 | .009 | .07 | .1 | .05 | 3.3 | .1 | <.05 | 6 | <.5 | 15.0 |
| 300E 2550N | .31 | .045 | 15 | 17.4 | .46 | 128 | .045 | 2 | 1.64 | .006 | .06 | .1 | .08 | 2.4 | .1 | <.05 | 6 | .6 | 1.0 |
| 300E 2525N | .10 | .059 | 81 | 16.4 | .09 | 92 | .042 | 1 | 1.84 | .011 | .04 | <.1 | .18 | 2.4 | .1 | .17 | 7 | 1.2 | 7.5 |
| 300E 2500N | .09 | .029 | 17 | 14.7 | .40 | 47 | .058 | 1 | 1.08 | .005 | .05 | .1 | .04 | 2.1 | .1 | <.05 | 5 | <.5 | 15.0 |
| 400E 3300N | .16 | .038 | 18 | 13.6 | .39 | 81 | .032 | 1 | 1.41 | .009 | .06 | .1 | .06 | 2.1 | .1 | <.05 | 7 | <.5 | 1.0 |
| 400E 3275N | .28 | .052 | 32 | 18.5 | .37 | 109 | .039 | 2 | 2.16 | .011 | .07 | .1 | .07 | 3.9 | .1 | <.05 | 9 | .5 | 15.0 |
| STANDARD DS5 | .74 | .087 | 12 | 187.5 | .67 | 132 | .104 | 17 | 1.94 | .034 | .14 | 5.1 | .17 | 3.4 | 1.1 | <.05 | 7 | 4.9 | 15.0 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data ___ FA ___

ACME ANALYTICAL

# Ruby Red Resources Inc.    FILE # A406457



ACME ANALYTICAL

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 400E 3250N | 1.0 | 58.0 | 25.6 | 47 | .4 | 11.3 | 9.4 | 329 | 2.28 | 2.9 | 1.3 | 1.7 | 1.6 | 16 | .5 | .1 | .4 | 42 | .18 | .043 | 19 | 15.4 | .31 | 75 | .059 | 1 | 1.85 | .012 | .06 | .1 | .04 | 3.1 | .1 | .08 | 10 | <.5 | 1.0 |
| 400E 3225N | .8 | 15.1 | 20.6 | 25 | .3 | 4.3 | 2.2 | 70 | 1.00 | 1.5 | .4 | .6 | .7 | 8 | .3 | .1 | .4 | 28 | .06 | .020 | 7 | 7.0 | .07 | 50 | .100 | 1 | .62 | .014 | .03 | .1 | .04 | .7 | <.1 | <.05 | 9 | <.5 | 7.5 |
| 400E 3200N | .8 | 27.7 | 31.0 | 34 | .3 | 7.1 | 6.2 | 166 | 1.17 | 1.9 | .9 | 1.4 | 1.3 | 12 | .3 | .1 | .4 | 30 | .13 | .032 | 13 | 9.5 | .17 | 60 | .102 | 1 | 1.21 | .022 | .03 | .1 | .04 | 1.9 | .1 | .07 | 10 | <.5 | 15.0 |
| 400E 3175N | .6 | 15.8 | 15.5 | 54 | .3 | 6.4 | 4.4 | 99 | 2.39 | 3.9 | .7 | 2.4 | 3.6 | 5 | .1 | .1 | .2 | 37 | .05 | .109 | 5 | 12.3 | .12 | 55 | .114 | 1 | 4.76 | .015 | .03 | .2 | .07 | 2.4 | <.1 | .07 | 9 | <.5 | 15.0 |
| 400E 3150N | .7 | 26.2 | 23.1 | 79 | .2 | 14.2 | 8.0 | 171 | 2.81 | 4.6 | .6 | 21.3 | 4.7 | 7 | .1 | .1 | .4 | 50 | .09 | .040 | 15 | 15.8 | .53 | 86 | .073 | <1 | 1.99 | .010 | .05 | .1 | .04 | 2.2 | .1 | <.05 | 10 | <.5 | 15.0 |
| 400E 3125N | .5 | 24.8 | 15.4 | 73 | .1 | 11.5 | 8.9 | 320 | 2.65 | 4.4 | .5 | 9.7 | 4.2 | 4 | .1 | .1 | .3 | 49 | .06 | .049 | 13 | 19.5 | .48 | 65 | .040 | 1 | 1.60 | .004 | .05 | .1 | .02 | 2.1 | .1 | <.05 | 7 | <.5 | 15.0 |
| 400E 3100N | .7 | 12.4 | 12.7 | 57 | .1 | 8.5 | 4.7 | 145 | 2.99 | 4.2 | .5 | 2.8 | 3.7 | 7 | .1 | .2 | .2 | 43 | .09 | .070 | 7 | 14.7 | .25 | 67 | .098 | 1 | 2.21 | .010 | .03 | .2 | .06 | 2.0 | <.1 | <.05 | 10 | <.5 | 15.0 |
| 400E 3075N | .6 | 22.3 | 17.4 | 66 | .2 | 13.1 | 8.2 | 156 | 2.96 | 4.1 | .5 | 13.8 | 5.9 | 3 | .1 | .1 | .3 | 55 | .05 | .064 | 11 | 20.6 | .46 | 64 | .042 | 1 | 2.22 | .005 | .04 | .1 | .08 | 2.8 | .1 | <.05 | 6 | <.5 | 15.0 |
| 400E 3050N | .6 | 34.0 | 13.4 | 49 | .1 | 13.6 | 9.2 | 190 | 3.22 | 3.9 | .8 | 11.0 | 4.6 | 5 | .1 | .2 | .2 | 74 | .05 | .064 | 10 | 14.5 | .59 | 66 | .063 | 1 | 2.60 | .008 | .03 | .1 | .05 | 3.8 | .1 | <.05 | 8 | <.5 | 15.0 |
| 400E 3025N | 1.0 | 21.1 | 14.1 | 45 | .2 | 8.3 | 5.9 | 88 | 2.85 | 4.6 | 1.0 | 13.4 | 4.2 | 6 | .2 | .2 | .2 | 51 | .07 | .076 | 9 | 13.0 | .29 | 52 | .106 | 1 | 3.36 | .011 | .03 | .2 | .12 | 3.5 | .1 | <.05 | 10 | .8 | 15.0 |
| 400E 3000N | .6 | 18.0 | 21.0 | 54 | .2 | 8.5 | 4.8 | 104 | 3.28 | 3.2 | .6 | 2.0 | 2.5 | 11 | .2 | .2 | .4 | 43 | .12 | .038 | 10 | 10.3 | .16 | 63 | .206 | 1 | 1.35 | .023 | .03 | .1 | .03 | 2.1 | .1 | <.05 | 16 | <.5 | 7.5 |
| 400E 2975N | .4 | 16.6 | 17.4 | 28 | .2 | 6.9 | 3.0 | 96 | 1.65 | 2.2 | .4 | <.5 | 1.6 | 14 | .2 | .2 | .3 | 35 | .13 | .025 | 9 | 9.3 | .16 | 54 | .091 | <1 | 1.04 | .015 | .04 | .1 | .03 | 1.3 | <.1 | <.05 | 9 | <.5 | 15.0 |
| 400E 2950N | .6 | 34.1 | 16.3 | 62 | .2 | 11.4 | 7.4 | 148 | 3.25 | 4.3 | .7 | 26.8 | 4.7 | 7 | .1 | .2 | .3 | 53 | .09 | .040 | 7 | 18.7 | .33 | 65 | .090 | 1 | 2.87 | .012 | .04 | .1 | .04 | 3.2 | .1 | <.05 | 9 | <.5 | 15.0 |
| 400E 2925N | .6 | 17.1 | 7.5 | 21 | .2 | 5.1 | 5.0 | 113 | 1.77 | 3.1 | .9 | 2.6 | 3.1 | 8 | .1 | .1 | .1 | 26 | .08 | .072 | 4 | 6.9 | .08 | 39 | .139 | <1 | 5.55 | .023 | .02 | .2 | .09 | 2.8 | <.1 | <.05 | 9 | .5 | 15.0 |
| 400E 2900N | .7 | 15.7 | 12.2 | 46 | .3 | 6.0 | 6.6 | 348 | 2.80 | 3.0 | .8 | 1.2 | 3.5 | 5 | .1 | .1 | .2 | 39 | .04 | .081 | 4 | 12.3 | .10 | 77 | .136 | 1 | 5.18 | .020 | .02 | .1 | .10 | 2.5 | .1 | <.05 | 12 | <.5 | 15.0 |
| 400E 2875N | .5 | 25.9 | 23.3 | 51 | .3 | 11.5 | 9.3 | 173 | 2.61 | 2.2 | .5 | 1.5 | 2.9 | 8 | .1 | .2 | .4 | 52 | .08 | .022 | 9 | 12.8 | .23 | 89 | .134 | 1 | 1.94 | .016 | .05 | .1 | .05 | 2.5 | .1 | <.05 | 12 | <.5 | 15.0 |
| RE 400E 2850N | .7 | 15.2 | 14.9 | 50 | .2 | 8.3 | 5.5 | 132 | 3.77 | 2.8 | .7 | 1.8 | 3.4 | 5 | .1 | .2 | .3 | 68 | .06 | .037 | 7 | 15.7 | .18 | 65 | .105 | 1 | 2.65 | .012 | .04 | .1 | .15 | 2.9 | .1 | <.05 | 13 | <.5 | 15.0 |
| 400E 2850N | .9 | 15.3 | 14.3 | 50 | .2 | 7.0 | 5.0 | 128 | 3.72 | 2.9 | .6 | 2.7 | 3.3 | 5 | .1 | .2 | .3 | 64 | .06 | .035 | 7 | 15.1 | .18 | 64 | .107 | 1 | 2.58 | .013 | .04 | .1 | .13 | 2.8 | .1 | <.05 | 13 | <.5 | 15.0 |
| 400E 2825N | .8 | 32.7 | 17.4 | 32 | .2 | 10.1 | 3.9 | 94 | 2.57 | 2.8 | 1.1 | 2.5 | 2.9 | 10 | .3 | .1 | .3 | 39 | .09 | .030 | 25 | 11.5 | .15 | 68 | .172 | 1 | 2.03 | .020 | .03 | .1 | .07 | 4.5 | .1 | <.05 | 13 | <.5 | 7.5 |
| 400E 2800N | .5 | 48.4 | 17.6 | 51 | .1 | 14.3 | 7.0 | 138 | 1.85 | 1.6 | 2.2 | 4.6 | .6 | 11 | .2 | .1 | .2 | 48 | .12 | .063 | 31 | 19.2 | .45 | 58 | .032 | <1 | 2.38 | .009 | .05 | .1 | .11 | 4.9 | .1 | <.05 | 8 | .8 | 15.0 |
| 400E 2775N | .6 | 22.7 | 23.4 | 49 | .2 | 9.7 | 6.6 | 169 | 2.26 | 1.8 | .6 | 1.6 | 3.6 | 11 | .2 | .1 | .3 | 50 | .10 | .019 | 12 | 14.0 | .26 | 90 | .114 | <1 | 1.83 | .014 | .04 | .1 | .05 | 3.1 | .1 | <.05 | 11 | <.5 | 7.5 |
| 400E 2750N | .8 | 34.1 | 35.6 | 74 | .3 | 14.4 | 15.3 | 294 | 2.54 | 3.6 | 1.2 | 1.6 | 2.0 | 16 | .3 | .2 | .4 | 64 | .21 | .046 | 26 | 18.5 | .43 | 113 | .055 | 1 | 2.67 | .008 | .05 | .1 | .05 | 5.0 | .1 | <.05 | 10 | .5 | 7.5 |
| 400E 2725N | .7 | 49.8 | 38.1 | 120 | .4 | 25.1 | 17.6 | 570 | 4.23 | 6.0 | 1.2 | 46.1 | 6.7 | 15 | .4 | .2 | .6 | 93 | .15 | .035 | 26 | 27.0 | .54 | 182 | .085 | 2 | 4.27 | .011 | .07 | <.1 | .06 | 6.6 | .1 | <.05 | 13 | <.5 | 15.0 |
| 400E 2700N | 1.3 | 74.1 | 42.5 | 73 | .3 | 12.6 | 20.0 | 758 | 2.73 | 3.8 | 1.9 | 1.9 | 1.5 | 13 | .6 | .1 | .4 | 56 | .16 | .050 | 32 | 18.6 | .45 | 80 | .041 | 1 | 2.27 | .010 | .07 | <.1 | .07 | 3.6 | .1 | .06 | 9 | .5 | 1.0 |
| 400E 2675N | .6 | 28.1 | 30.0 | 55 | .2 | 11.8 | 9.9 | 718 | 2.11 | 3.1 | .9 | 1.8 | 1.1 | 18 | .4 | .2 | .4 | 45 | .25 | .044 | 26 | 18.7 | .40 | 110 | .041 | 1 | 2.06 | .009 | .05 | <.1 | .06 | 2.9 | .1 | <.05 | 8 | <.5 | 7.5 |
| 400E 2650N | .5 | 24.2 | 24.7 | 67 | .1 | 13.8 | 9.5 | 289 | 2.39 | 3.3 | 1.0 | 1.3 | 2.5 | 15 | .2 | .2 | .3 | 46 | .17 | .030 | 15 | 21.4 | .42 | 74 | .057 | 1 | 2.00 | .008 | .06 | .1 | .05 | 2.9 | .1 | <.05 | 7 | <.5 | 1.0 |
| 400E 2625N | .6 | 29.6 | 30.0 | 89 | .3 | 14.2 | 8.7 | 175 | 1.97 | 3.3 | 1.1 | 1.2 | 1.9 | 10 | .3 | .1 | .4 | 45 | .10 | .024 | 26 | 15.8 | .40 | 81 | .059 | 1 | 1.89 | .011 | .06 | .1 | .03 | 2.5 | .1 | <.05 | 8 | <.5 | 15.0 |
| 400E 2600N | .6 | 15.0 | 22.1 | 50 | .3 | 6.8 | 3.3 | 148 | 2.10 | 2.5 | .5 | 1.7 | 2.9 | 8 | .3 | .1 | .3 | 45 | .08 | .018 | 12 | 10.3 | .18 | 59 | .107 | 1 | 1.16 | .012 | .03 | .1 | .03 | 1.5 | .1 | <.05 | 10 | <.5 | 7.5 |
| 400E 2575N | .5 | 31.1 | 15.3 | 67 | .1 | 15.4 | 10.2 | 313 | 2.53 | 3.9 | .7 | 3.1 | 4.1 | 7 | .2 | .2 | .2 | 50 | .12 | .029 | 18 | 16.4 | .66 | 44 | .050 | <1 | 1.48 | .008 | .06 | <.1 | .02 | 3.5 | .1 | <.05 | 5 | <.5 | 15.0 |
| 400E 2550N | .6 | 17.8 | 12.0 | 43 | .2 | 7.7 | 5.0 | 123 | 2.28 | 2.9 | .6 | 1.2 | 4.0 | 5 | .1 | .2 | .2 | 44 | .10 | .037 | 11 | 14.4 | .28 | 45 | .053 | 2 | 2.69 | .010 | .04 | .1 | .07 | 3.1 | .1 | <.05 | 7 | <.5 | 15.0 |
| 400E 2525N | .4 | 35.0 | 14.2 | 60 | <.1 | 15.9 | 11.6 | 214 | 2.64 | 4.4 | .7 | 17.5 | 6.3 | 3 | .1 | .2 | .3 | 48 | .06 | .028 | 19 | 15.8 | .63 | 50 | .047 | 1 | 1.80 | .005 | .05 | .1 | .02 | 3.3 | .1 | <.05 | 5 | <.5 | 15.0 |
| 400E 2500N | .5 | 27.3 | 17.3 | 81 | .1 | 21.8 | 10.8 | 187 | 2.70 | 5.4 | .9 | 21.7 | 6.4 | 4 | .1 | .2 | .3 | 44 | .05 | .027 | 18 | 30.2 | .56 | 52 | .064 | <1 | 1.62 | .003 | .11 | <.1 | .02 | 3.3 | .2 | <.05 | 4 | <.5 | 15.0 |
| 400E 2475N | .6 | 20.6 | 17.2 | 51 | .2 | 11.7 | 8.4 | 145 | 2.17 | 5.9 | .9 | 73.8 | 5.7 | 3 | .1 | .2 | .3 | 31 | .03 | .039 | 12 | 18.6 | .33 | 43 | .043 | 1 | 2.15 | .005 | .06 | .1 | .08 | 2.6 | .1 | <.05 | 5 | <.5 | 15.0 |
| STANDARD DS5 | 13.1 | 144.4 | 25.6 | 138 | .3 | 23.1 | 11.8 | 797 | 2.97 | 17.9 | 6.1 | 44.9 | 2.7 | 45 | 5.7 | 3.8 | 6.1 | 61 | .76 | .096 | 12 | 190.2 | .68 | 137 | .098 | 19 | 2.09 | .034 | .15 | 4.9 | .20 | 3.5 | 1.0 | <.05 | 6 | 4.9 | 15.0 |

Sample type: SOIL SS80 60C.  Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data ___ FA ___

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 400E 2450N | .8 | 9.3 | 10.0 | 25 | .2 | 3.5 | 2.2 | 115 | 1.96 | 3.4 | 1.0 | 2.7 | 3.2 | 4 | .1 | .2 | .2 | 27 | .03 | .080 | 5 | 9.3 | .06 | 25 | .110 | 2 | 5.63 | .011 | .02 | .2 | .12 | 2.6 | <.1 | <.05 | 10 | .6 | 15.0 |
| 400E 2425N | .7 | 7.7 | 14.9 | 35 | .1 | 4.4 | 2.1 | 99 | 2.40 | 2.8 | .5 | 6.4 | 2.8 | 4 | .1 | .2 | .4 | 51 | .03 | .063 | 8 | 9.2 | .09 | 38 | .136 | 1 | 1.94 | .009 | .03 | .1 | .05 | 1.4 | .1 | <.05 | 15 | <.5 | 15.0 |
| 400E 2400N | .8 | 12.6 | 11.3 | 19 | .3 | 3.7 | 1.8 | 162 | 1.90 | 4.4 | 1.0 | 2.8 | 3.8 | 5 | .1 | .3 | .2 | 33 | .05 | .124 | 3 | 8.5 | .05 | 22 | .134 | 3 | 5.49 | .014 | .02 | .2 | .10 | 2.2 | <.1 | <.05 | 11 | <.5 | 15.0 |
| 49 0E | 1.1 | 15.3 | 15.9 | 85 | .1 | 19.8 | 9.7 | 166 | 2.12 | 4.4 | .5 | 2.6 | 4.2 | 6 | .1 | .2 | .3 | 32 | .07 | .058 | 10 | 17.7 | .54 | 68 | .095 | 2 | 2.46 | .010 | .07 | .2 | .03 | 2.2 | .1 | <.05 | 8 | <.5 | 15.0 |
| 49 25E | .8 | 11.0 | 15.8 | 99 | .2 | 19.9 | 9.6 | 411 | 1.88 | 2.9 | .4 | 1.1 | 3.0 | 8 | .1 | .2 | .3 | 28 | .08 | .070 | 8 | 15.2 | .39 | 86 | .103 | 2 | 2.36 | .011 | .07 | .1 | .04 | 1.7 | .1 | <.05 | 8 | <.5 | 15.0 |
| 49 50E | .7 | 9.6 | 12.8 | 65 | .1 | 16.4 | 11.1 | 201 | 1.90 | 3.5 | .4 | 1.9 | 3.6 | 6 | .1 | .2 | .3 | 32 | .08 | .045 | 10 | 17.1 | .32 | 67 | .069 | 2 | 2.14 | .009 | .07 | .1 | .04 | 1.7 | .1 | <.05 | 7 | <.5 | 15.0 |
| 49 75E | 1.2 | 12.0 | 14.5 | 76 | .1 | 21.4 | 9.8 | 186 | 1.97 | 3.2 | .5 | 1.5 | 3.8 | 9 | .1 | .2 | .3 | 30 | .09 | .077 | 8 | 14.1 | .30 | 92 | .121 | 1 | 2.54 | .014 | .07 | .2 | .03 | 1.9 | .1 | <.05 | 10 | <.5 | 15.0 |
| 49 100E | .6 | 12.4 | 15.1 | 91 | .2 | 20.0 | 10.7 | 190 | 2.14 | 2.9 | .6 | <.5 | 3.9 | 9 | .2 | .2 | .3 | 30 | .11 | .197 | 11 | 16.0 | .32 | 102 | .086 | 2 | 2.04 | .013 | .09 | .1 | .04 | 1.7 | .1 | <.05 | 9 | <.5 | 7.5 |
| 49 125E | .5 | 15.1 | 13.2 | 69 | .1 | 20.0 | 10.9 | 191 | 1.76 | 3.8 | .5 | 7.4 | 4.0 | 5 | .1 | .2 | .2 | 30 | .08 | .029 | 12 | 19.8 | .42 | 64 | .054 | 1 | 1.65 | .006 | .06 | .1 | .02 | 1.8 | .1 | <.05 | 5 | <.5 | 15.0 |
| 49 150E | .5 | 19.1 | 13.8 | 76 | .1 | 18.9 | 8.9 | 143 | 1.77 | 3.6 | .4 | 7.8 | 4.2 | 5 | .1 | .2 | .2 | 29 | .07 | .024 | 14 | 20.0 | .52 | 53 | .044 | 1 | 1.39 | .004 | .08 | .1 | .02 | 1.9 | .1 | <.05 | 4 | <.5 | 15.0 |
| 49 175E | .5 | 23.7 | 17.9 | 89 | .1 | 24.8 | 13.5 | 289 | 1.99 | 5.2 | .5 | 3.5 | 3.9 | 6 | .1 | .2 | .2 | 38 | .10 | .066 | 7 | 24.5 | .43 | 66 | .083 | <1 | 2.33 | .011 | .06 | .1 | .02 | 2.6 | .1 | <.05 | 7 | <.5 | 15.0 |
| 49 200E | .6 | 26.1 | 21.8 | 94 | .1 | 22.3 | 10.8 | 235 | 2.25 | 4.5 | .5 | 7.4 | 4.0 | 6 | .1 | .2 | .2 | 48 | .10 | .044 | 10 | 27.7 | .63 | 69 | .079 | 1 | 1.95 | .007 | .07 | .1 | .02 | 2.8 | .1 | <.05 | 7 | <.5 | 15.0 |
| 49 225E | .9 | 36.4 | 34.3 | 190 | .1 | 42.6 | 21.7 | 965 | 2.86 | 8.5 | 1.1 | 19.8 | 5.9 | 14 | .8 | .3 | .4 | 40 | .15 | .096 | 20 | 25.5 | .61 | 113 | .091 | 1 | 2.87 | .011 | .11 | .1 | .04 | 2.9 | .1 | <.05 | 9 | <.5 | 15.0 |
| 49 250E | .7 | 22.6 | 31.4 | 181 | .4 | 26.1 | 13.3 | 312 | 2.70 | 5.0 | 1.0 | 1.5 | 5.2 | 13 | .5 | .3 | .3 | 38 | .19 | .193 | 20 | 24.1 | .71 | 75 | .128 | 1 | 3.57 | .014 | .09 | .2 | .04 | 3.1 | .1 | <.05 | 10 | <.5 | 15.0 |
| RE 49 175E | .5 | 25.4 | 18.3 | 87 | .1 | 25.2 | 14.2 | 299 | 2.06 | 5.1 | .6 | 3.3 | 4.0 | 6 | .1 | .2 | .2 | 41 | .11 | .069 | 7 | 26.1 | .46 | 70 | .089 | 2 | 2.45 | .011 | .07 | .1 | .02 | 2.6 | .1 | <.05 | 7 | <.5 | 15.0 |
| 49 275E | .6 | 80.4 | 51.6 | 140 | .4 | 20.0 | 20.8 | 2408 | 2.66 | 6.3 | .4 | 2025.8 | 2.8 | 14 | .6 | .2 | .3 | 59 | .21 | .096 | 8 | 23.6 | .50 | 165 | .086 | 2 | 1.96 | .012 | .10 | .1 | .05 | 2.6 | .1 | <.05 | 9 | <.5 | 7.5 |
| 49 300E | .6 | 196.3 | 37.3 | 118 | .2 | 28.5 | 29.1 | 380 | 3.43 | 10.2 | .5 | 3.3 | 3.1 | 9 | .3 | .2 | .3 | 95 | .17 | .045 | 7 | 29.0 | .64 | 79 | .116 | 1 | 2.41 | .010 | .07 | .1 | .03 | 4.0 | .1 | <.05 | 10 | <.5 | 15.0 |
| 49 325E | .5 | 73.0 | 27.6 | 67 | .1 | 30.3 | 22.1 | 199 | 2.82 | 7.2 | .6 | 2.1 | 3.5 | 6 | .1 | .2 | .1 | 79 | .15 | .021 | 9 | 55.4 | .73 | 48 | .097 | <1 | 1.91 | .009 | .05 | .1 | .02 | 4.7 | .1 | <.05 | 6 | <.5 | 15.0 |
| 49 350E | .6 | 61.6 | 15.9 | 73 | .6 | 24.9 | 13.6 | 147 | 2.34 | 6.4 | .6 | 2.1 | 3.6 | 7 | .3 | .2 | .2 | 58 | .09 | .070 | 5 | 23.6 | .39 | 63 | .123 | 1 | 3.43 | .015 | .06 | .1 | .04 | 3.2 | .1 | <.05 | 9 | <.5 | 15.0 |
| 49 375E | .5 | 44.1 | 19.2 | 78 | .6 | 24.1 | 13.2 | 271 | 2.14 | 5.9 | .5 | 4.4 | 3.4 | 6 | .1 | .2 | .2 | 50 | .10 | .068 | 6 | 26.1 | .37 | 62 | .100 | 1 | 2.73 | .012 | .06 | .1 | .04 | 3.0 | .1 | <.05 | 8 | <.5 | 15.0 |
| 49 400E | .6 | 19.9 | 13.6 | 87 | .3 | 12.6 | 10.2 | 596 | 2.12 | 3.5 | .4 | 4.5 | 1.9 | 6 | .2 | .2 | .2 | 54 | .10 | .121 | 7 | 14.6 | .25 | 59 | .081 | 1 | 2.22 | .014 | .05 | .1 | .03 | 2.3 | .1 | <.05 | 8 | <.5 | 15.0 |
| 49 425E | .8 | 13.6 | 13.1 | 72 | .1 | 13.3 | 9.4 | 611 | 1.75 | 4.3 | .5 | 1.9 | 2.7 | 6 | .2 | .2 | .2 | 38 | .08 | .131 | 5 | 13.0 | .18 | 47 | .106 | 1 | 2.98 | .014 | .05 | .1 | .05 | 2.1 | .1 | <.05 | 8 | <.5 | 15.0 |
| 49 450E | .5 | 17.2 | 11.8 | 90 | .3 | 15.0 | 9.5 | 207 | 2.01 | 3.5 | .4 | 4.3 | 2.7 | 6 | .1 | .1 | .2 | 40 | .11 | .091 | 8 | 17.7 | .33 | 51 | .073 | 1 | 1.88 | .011 | .05 | .1 | .03 | 2.1 | .1 | <.05 | 7 | <.5 | 15.0 |
| 49 475E | .5 | 49.9 | 16.9 | 89 | .3 | 20.9 | 13.8 | 384 | 2.53 | 6.5 | .6 | 152.0 | 3.1 | 6 | .2 | .2 | .2 | 68 | .11 | .074 | 6 | 20.4 | .44 | 60 | .098 | <1 | 2.82 | .013 | .06 | .1 | .04 | 3.4 | .1 | <.05 | 8 | <.5 | 15.0 |
| 49 500E | .5 | 247.2 | 16.0 | 72 | .2 | 21.9 | 17.9 | 179 | 2.68 | 9.8 | .7 | 3.2 | 4.2 | 6 | .1 | .3 | .2 | 73 | .13 | .045 | 12 | 21.9 | .57 | 85 | .092 | 1 | 2.54 | .012 | .05 | .1 | .04 | 4.6 | .1 | <.05 | 7 | <.5 | 15.0 |
| 1820 500W | .7 | 9.1 | 7.8 | 47 | .2 | 9.1 | 4.2 | 81 | 2.08 | 3.0 | .7 | 6.6 | 5.0 | 4 | .1 | .2 | .3 | 24 | .03 | .078 | 10 | 12.2 | .23 | 44 | .053 | 1 | 3.54 | .007 | .04 | .1 | .10 | 1.8 | <.1 | <.05 | 6 | <.5 | 15.0 |
| 1820 475W | .6 | 8.7 | 10.3 | 42 | .1 | 10.9 | 3.9 | 82 | 1.58 | 7.7 | .5 | 20.6 | 3.2 | 4 | .1 | .1 | .3 | 19 | .03 | .023 | 22 | 10.1 | .30 | 34 | .023 | <1 | 1.08 | .005 | .04 | .1 | .02 | .9 | .1 | <.05 | 6 | <.5 | 15.0 |
| 1820 450W | .9 | 9.7 | 11.8 | 52 | .3 | 7.5 | 6.0 | 400 | 2.51 | 4.0 | .8 | 7.6 | 4.9 | 2 | .1 | .2 | .4 | 34 | .02 | .103 | 11 | 13.2 | .17 | 40 | .053 | 1 | 2.76 | .008 | .03 | .2 | .09 | 2.1 | .1 | <.05 | 9 | .5 | 15.0 |
| 1820 425W | 1.2 | 11.0 | 13.5 | 75 | .1 | 12.7 | 6.5 | 257 | 2.74 | 5.8 | .9 | 8.4 | 7.1 | 3 | <.1 | .3 | .4 | 21 | .02 | .111 | 16 | 13.5 | .37 | 56 | .047 | 1 | 3.02 | .006 | .05 | .2 | .08 | 1.7 | .1 | <.05 | 7 | <.5 | 15.0 |
| 1820 400W | 1.3 | 13.0 | 19.3 | 68 | .3 | 13.4 | 6.9 | 118 | 3.25 | 6.7 | 1.2 | 44.2 | 6.9 | 5 | .1 | .2 | .5 | 27 | .04 | .071 | 20 | 15.2 | .30 | 47 | .040 | 1 | 2.19 | .007 | .05 | .1 | .04 | 1.7 | .1 | <.05 | 8 | <.5 | 15.0 |
| 1820 375W | 1.0 | 12.4 | 15.4 | 68 | .3 | 13.3 | 8.1 | 148 | 2.34 | 4.5 | 1.0 | 14.6 | 6.0 | 4 | .2 | .2 | .4 | 25 | .03 | .090 | 16 | 11.2 | .26 | 55 | .051 | 1 | 2.63 | .008 | .05 | .2 | .09 | 1.8 | .1 | <.05 | 7 | <.5 | 15.0 |
| 1820 350W | 1.0 | 10.4 | 15.4 | 60 | .4 | 7.8 | 5.4 | 109 | 2.08 | 3.1 | .7 | 43.3 | 4.4 | 3 | .1 | .1 | .4 | 29 | .03 | .057 | 16 | 8.4 | .20 | 40 | .042 | 1 | 1.76 | .008 | .05 | .2 | .07 | 1.4 | .1 | <.05 | 8 | <.5 | 15.0 |
| 1820 325W | 1.2 | 11.4 | 18.7 | 63 | .1 | 18.0 | 14.2 | 419 | 2.07 | 4.9 | 1.4 | 7.8 | 4.2 | 14 | .2 | .2 | .5 | 19 | .15 | .031 | 25 | 12.9 | .35 | 49 | .019 | 1 | 1.18 | .006 | .05 | .2 | .02 | 1.2 | <.1 | <.05 | 5 | <.5 | 1.0 |
| STANDARD DS5 | 13.9 | 143.7 | 25.3 | 140 | .3 | 25.7 | 11.4 | 763 | 2.93 | 18.8 | 6.5 | 43.1 | 2.6 | 47 | 5.8 | 3.7 | 6.2 | 58 | .75 | .095 | 12 | 197.2 | .68 | 131 | .100 | 18 | 2.06 | .034 | .16 | 4.9 | .19 | 3.6 | 1.0 | <.05 | 7 | 5.0 | 15.0 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data ( FA ____

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1820 300W | 1.6 | 14.0 | 17.0 | 89 | .1 | 18.3 | 9.8 | 205 | 4.10 | 7.6 | 1.0 | 17.0 | 5.3 | 8 | .2 | .3 | .6 | 29 | .08 | .102 | 23 | 16.7 | .47 | 62 | .025 | 1 | 1.48 | .005 | .07 | .2 | .02 | 1.3 | .1 | .10 | 8 | <.5 | 7.5 |
| 1820 275W | 1.5 | 16.0 | 16.0 | 42 | .1 | 17.9 | 17.7 | 262 | 2.68 | 7.9 | 1.7 | 147.2 | 5.0 | 6 | .1 | .3 | .6 | 14 | .06 | .044 | 29 | 10.7 | .50 | 50 | .008 | <1 | 1.17 | .003 | .06 | .1 | <.01 | 1.2 | <.1 | <.05 | 4 | <.5 | 15.0 |
| 1820 250W | 1.3 | 13.7 | 23.4 | 48 | .2 | 11.2 | 15.5 | 232 | 3.10 | 4.5 | 1.1 | 12.9 | 3.9 | 8 | .2 | .3 | .6 | 28 | .07 | .060 | 21 | 11.1 | .28 | 62 | .032 | 1 | 1.67 | .007 | .05 | .2 | .05 | 1.4 | .1 | <.05 | 8 | <.5 | 7.5 |
| 1820 225W | 1.4 | 10.5 | 19.5 | 56 | .2 | 11.6 | 6.1 | 147 | 3.35 | 5.4 | .9 | 16.9 | 6.1 | 5 | .1 | .3 | .5 | 33 | .05 | .094 | 17 | 14.9 | .25 | 69 | .049 | <1 | 3.17 | .008 | .05 | .2 | .07 | 1.9 | .1 | <.05 | 8 | <.5 | 15.0 |
| 1820 200W | 1.3 | 13.6 | 22.3 | 51 | .1 | 15.5 | 9.9 | 144 | 3.04 | 6.6 | 1.7 | 22.4 | 5.1 | 10 | .2 | .3 | .7 | 26 | .11 | .038 | 31 | 11.5 | .28 | 70 | .017 | <1 | 1.47 | .006 | .07 | .2 | .02 | 1.5 | .1 | <.05 | 7 | <.5 | 7.5 |
| 1820 175W | 2.6 | 17.8 | 52.2 | 66 | .1 | 17.8 | 37.4 | 2478 | 2.68 | 5.3 | 1.6 | 15.4 | 3.7 | 12 | .4 | .2 | .6 | 21 | .11 | .045 | 26 | 11.7 | .33 | 91 | .022 | 1 | 1.55 | .008 | .06 | .1 | .04 | 1.6 | .1 | <.05 | 7 | <.5 | 7.5 |
| 1820 150W | 1.0 | 14.8 | 21.1 | 59 | .1 | 14.2 | 9.9 | 284 | 2.78 | 7.1 | .7 | 23.1 | 5.8 | 9 | .2 | .3 | .6 | 21 | .12 | .070 | 22 | 11.0 | .27 | 88 | .023 | <1 | 1.86 | .006 | .06 | .1 | .02 | 1.6 | .1 | <.05 | 6 | <.5 | 15.0 |
| 1820 125W | 1.2 | 10.4 | 16.3 | 42 | .2 | 6.6 | 4.7 | 167 | 3.58 | 5.4 | .8 | 5.4 | 5.1 | 4 | .1 | .2 | .4 | 43 | .02 | .102 | 8 | 13.8 | .11 | 44 | .085 | 1 | 4.51 | .010 | .03 | .2 | .12 | 1.8 | .1 | <.05 | 10 | .5 | 15.0 |
| 1840 0S | 1.3 | 9.3 | 15.9 | 48 | .1 | 10.6 | 5.4 | 99 | 3.03 | 5.2 | .7 | 26.9 | 5.7 | 4 | .1 | .2 | .5 | 28 | .03 | .066 | 16 | 11.1 | .25 | 92 | .043 | <1 | 2.52 | .007 | .04 | .2 | .06 | 1.5 | .1 | <.05 | 8 | <.5 | 15.0 |
| 1840 025S | 1.3 | 8.3 | 10.2 | 39 | <.1 | 9.2 | 5.4 | 99 | 2.72 | 5.7 | .4 | 21.9 | 5.6 | 3 | .1 | .3 | .6 | 29 | .01 | .046 | 28 | 9.3 | .22 | 44 | .035 | 1 | .88 | .005 | .04 | .2 | .02 | .9 | .1 | <.05 | 7 | <.5 | 15.0 |
| 1840 050S | 1.4 | 10.2 | 16.8 | 48 | .1 | 9.8 | 6.6 | 140 | 3.42 | 6.4 | .7 | 49.3 | 6.3 | 4 | .1 | .3 | .5 | 29 | .03 | .086 | 18 | 12.6 | .23 | 43 | .041 | 1 | 2.12 | .006 | .04 | .2 | .06 | 1.4 | .1 | <.05 | 7 | <.5 | 15.0 |
| 1840 075S | 1.4 | 12.6 | 16.4 | 58 | .1 | 12.0 | 7.3 | 127 | 3.43 | 7.4 | .6 | 46.6 | 5.9 | 3 | .1 | .3 | .6 | 29 | .02 | .055 | 24 | 12.3 | .33 | 50 | .022 | 1 | 1.63 | .005 | .04 | .2 | .04 | 1.3 | .1 | <.05 | 7 | <.5 | 15.0 |
| 1840 100S | 1.8 | 19.6 | 48.2 | 110 | .1 | 19.2 | 24.9 | 3369 | 3.52 | 6.4 | 1.7 | 17.6 | 1.7 | 16 | .3 | .2 | .8 | 31 | .13 | .081 | 19 | 16.0 | .51 | 133 | .021 | 1 | 1.80 | .007 | .06 | .2 | .01 | 1.7 | .1 | <.05 | 8 | <.5 | 7.5 |
| 1840 125S | 1.5 | 22.7 | 38.5 | 129 | .1 | 31.9 | 19.3 | 711 | 3.75 | 8.5 | 1.7 | 7.0 | 4.7 | 10 | .2 | .3 | .8 | 32 | .07 | .113 | 15 | 15.3 | .42 | 181 | .040 | 1 | 2.88 | .007 | .09 | .2 | .04 | 2.0 | .1 | <.05 | 9 | <.5 | 15.0 |
| 1840 150S | 2.1 | 26.5 | 23.5 | 117 | .3 | 15.8 | 8.5 | 239 | 4.30 | 6.8 | 1.4 | 13.9 | 6.8 | 5 | .2 | .3 | .5 | 37 | .03 | .111 | 11 | 16.2 | .23 | 70 | .093 | 1 | 3.18 | .009 | .05 | .2 | .09 | 2.2 | .1 | <.05 | 11 | <.5 | 15.0 |
| 1840 175S | 1.7 | 17.3 | 19.9 | 98 | .2 | 18.0 | 18.1 | 523 | 2.91 | 5.7 | 1.1 | 6.6 | 5.8 | 6 | .1 | .3 | .5 | 30 | .04 | .074 | 14 | 12.9 | .29 | 86 | .079 | 2 | 3.25 | .010 | .05 | .2 | .07 | 2.3 | .1 | <.05 | 9 | .6 | 15.0 |
| 1840 200S | 1.9 | 19.6 | 31.7 | 99 | .2 | 21.9 | 19.7 | 1663 | 3.53 | 8.0 | 2.4 | 367.7 | 2.3 | 16 | .3 | .3 | .8 | 25 | .15 | .068 | 22 | 15.3 | .52 | 97 | .022 | 1 | 2.07 | .008 | .09 | .1 | .02 | 1.6 | .1 | <.05 | 8 | .5 | 7.5 |
| 1840 225S | 2.9 | 22.7 | 24.8 | 67 | .1 | 18.5 | 16.9 | 380 | 2.56 | 6.0 | 3.3 | 8.0 | 1.5 | 13 | .8 | .3 | .7 | 22 | .06 | .045 | 30 | 10.6 | .26 | 65 | .020 | <1 | 1.34 | .005 | .06 | .1 | .03 | 1.5 | .1 | <.05 | 6 | 1.1 | 15.0 |
| 1840 250S | 1.5 | 22.3 | 36.7 | 114 | .2 | 14.6 | 24.2 | 1238 | 2.97 | 6.3 | 1.8 | 26.7 | 1.6 | 21 | .4 | .2 | .8 | 34 | .24 | .069 | 19 | 14.5 | .33 | 97 | .025 | <1 | 1.58 | .008 | .06 | .2 | .04 | 1.4 | .1 | <.05 | 8 | <.5 | 15.0 |
| 1860 50N | .9 | 11.5 | 15.7 | 63 | .1 | 7.5 | 4.0 | 217 | 2.18 | 5.6 | .5 | 1.0 | 3.4 | 4 | .1 | .3 | .4 | 33 | .03 | .034 | 14 | 10.9 | .18 | 53 | .045 | 2 | 1.57 | .009 | .04 | .1 | .05 | 1.3 | .1 | <.05 | 8 | <.5 | 7.5 |
| 1860 25N | 1.5 | 15.9 | 23.8 | 79 | .1 | 9.5 | 8.0 | 570 | 2.97 | 7.0 | .7 | 1.5 | 4.5 | 5 | .1 | .2 | .6 | 32 | .04 | .076 | 15 | 14.9 | .26 | 60 | .041 | 1 | 1.74 | .008 | .06 | .2 | .04 | 1.5 | .1 | <.05 | 8 | <.5 | 1.0 |
| RE 1860 25N | 1.4 | 16.3 | 26.0 | 84 | .1 | 10.3 | 7.7 | 597 | 2.97 | 7.3 | .7 | 16.2 | 4.7 | 5 | .1 | .2 | .6 | 30 | .04 | .077 | 15 | 14.1 | .27 | 64 | .042 | 2 | 1.75 | .008 | .06 | .2 | .05 | 1.3 | .1 | <.05 | 8 | <.5 | 1.0 |
| 1860 0S | 1.5 | 18.0 | 23.8 | 73 | .1 | 12.2 | 6.4 | 199 | 3.54 | 10.2 | .9 | 4.1 | 8.1 | 3 | .1 | .2 | .6 | 29 | .02 | .041 | 20 | 15.7 | .32 | 53 | .041 | 2 | 1.90 | .007 | .05 | .2 | .08 | 1.8 | .1 | <.05 | 7 | .5 | 7.5 |
| 1860 25S | 1.5 | 17.0 | 20.0 | 74 | .1 | 13.8 | 8.3 | 192 | 3.63 | 10.8 | .9 | 2.6 | 7.5 | 3 | .1 | .3 | .7 | 29 | .03 | .043 | 21 | 14.8 | .36 | 54 | .037 | <1 | 2.03 | .006 | .06 | .2 | .04 | 1.7 | .1 | <.05 | 8 | <.5 | 7.5 |
| 1860 50S | 1.4 | 26.0 | 26.3 | 78 | .1 | 14.2 | 11.4 | 426 | 3.35 | 11.4 | 1.2 | 3.2 | 7.7 | 3 | .1 | .3 | .6 | 25 | .03 | .060 | 18 | 15.2 | .33 | 47 | .035 | 1 | 2.38 | .005 | .05 | .1 | .07 | 1.6 | .1 | <.05 | 7 | .5 | 7.5 |
| 1860 75S | 1.4 | 9.0 | 14.5 | 55 | .1 | 9.4 | 5.0 | 548 | 2.33 | 5.5 | .3 | 60.0 | 3.8 | 8 | .1 | .4 | .5 | 34 | .10 | .028 | 24 | 10.5 | .16 | 135 | .043 | 1 | .68 | .006 | .06 | .1 | .01 | 1.0 | .1 | <.05 | 7 | <.5 | 1.0 |
| 1860 100S | 1.6 | 10.0 | 19.5 | 58 | .1 | 9.0 | 5.0 | 120 | 3.18 | 6.5 | .7 | 68.5 | 5.2 | 4 | .2 | .2 | .6 | 35 | .03 | .023 | 18 | 10.8 | .18 | 82 | .054 | 1 | 1.40 | .008 | .05 | .1 | .02 | 1.3 | .1 | <.05 | 9 | <.5 | 7.5 |
| 1860 125S | 1.4 | 9.9 | 10.5 | 48 | .1 | 9.5 | 5.3 | 119 | 2.94 | 6.1 | .5 | 39.4 | 6.9 | 3 | .2 | .2 | .5 | 19 | .01 | .022 | 27 | 10.0 | .23 | 49 | .014 | 1 | .92 | .003 | .04 | .1 | .01 | 1.1 | .1 | <.05 | 5 | <.5 | 7.5 |
| 1860 150S | 1.2 | 13.3 | 27.0 | 94 | .1 | 16.5 | 11.6 | 318 | 3.36 | 6.0 | .9 | 15.3 | 4.2 | 12 | .1 | .2 | .6 | 23 | .16 | .049 | 25 | 11.9 | .39 | 95 | .026 | 1 | 1.26 | .006 | .07 | .1 | .02 | 1.4 | .1 | <.05 | 7 | <.5 | 7.5 |
| 1860 175S | 1.3 | 10.2 | 24.0 | 56 | <.1 | 12.7 | 8.7 | 351 | 2.82 | 6.2 | .9 | 48.8 | 3.5 | 4 | .1 | .2 | .7 | 20 | .03 | .053 | 27 | 10.9 | .35 | 60 | .015 | <1 | 1.01 | .004 | .05 | .1 | .01 | 1.3 | <.1 | <.05 | 5 | <.5 | 1.0 |
| 1860 200S | 1.2 | 11.3 | 32.9 | 46 | .1 | 13.4 | 8.5 | 178 | 2.64 | 5.9 | .7 | 20.2 | 5.2 | 3 | <.1 | .2 | .7 | 19 | .02 | .034 | 25 | 9.2 | .28 | 61 | .014 | 1 | .94 | .004 | .05 | .1 | .01 | 1.2 | .1 | <.05 | 5 | <.5 | 1.0 |
| 1860 225S | 1.2 | 8.6 | 15.4 | 46 | .1 | 10.5 | 6.3 | 154 | 2.82 | 5.5 | .4 | 13.7 | 4.3 | 5 | .1 | .2 | .5 | 22 | .04 | .045 | 23 | 11.2 | .31 | 80 | .019 | <1 | 1.10 | .005 | .05 | .2 | .03 | 1.1 | <.1 | <.05 | 6 | <.5 | 1.0 |
| 1860 250S | 1.1 | 12.2 | 31.3 | 73 | .1 | 14.7 | 10.2 | 253 | 3.00 | 7.0 | .9 | 14.6 | 5.5 | 5 | .1 | .3 | .5 | 21 | .04 | .049 | 22 | 12.1 | .32 | 81 | .027 | 1 | 1.81 | .006 | .05 | .1 | .03 | 1.4 | .1 | <.05 | 5 | <.5 | 7.5 |
| STANDARD DS5 | 12.9 | 143.2 | 26.1 | 136 | .3 | 24.3 | 11.2 | 785 | 2.98 | 18.3 | 6.3 | 40.9 | 2.6 | 46 | 5.4 | 3.8 | 6.6 | 60 | .71 | .090 | 13 | 185.7 | .67 | 137 | .094 | 19 | 1.91 | .034 | .13 | 4.7 | .19 | 3.3 | 1.2 | <.05 | 6 | 4.8 | 15.0 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data ___ FA ___

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1860 275S | 1.3 | 13.5 | 72.0 | 91 | .1 | 13.7 | 17.6 | 1405 | 1.87 | 3.6 | 6.8 | 9.6 | 4.1 | 12 | .6 | .1 | .5 | 15 | .12 | .037 | 31 | 11.3 | .45 | 211 | .010 | <1 | 1.43 | .006 | .05 | .5 | .03 | 1.4 | .1 | <.05 | 4 | <.5 | 7.5 |
| 1860 300S | 1.3 | 8.0 | 11.1 | 41 | .1 | 8.6 | 6.6 | 152 | 1.56 | 3.3 | .9 | 28.6 | 2.6 | 7 | .2 | .1 | .4 | 15 | .07 | .028 | 25 | 8.8 | .33 | 85 | .009 | <1 | .66 | .005 | .05 | .1 | .02 | .6 | <.1 | <.05 | 3 | <.5 | 7.5 |
| 1860 325S | 1.8 | 18.8 | 22.3 | 76 | .1 | 14.1 | 17.8 | 1386 | 2.37 | 5.8 | 1.7 | 9.2 | 1.4 | 8 | .4 | .3 | .8 | 18 | .07 | .061 | 14 | 13.2 | .41 | 97 | .015 | <1 | 1.07 | .005 | .05 | .1 | .04 | .7 | .1 | <.05 | 4 | <.5 | 1.0 |
| 1860 350S | 1.7 | 15.7 | 20.8 | 59 | .1 | 13.1 | 10.7 | 250 | 2.76 | 6.3 | .9 | 8.4 | 4.9 | 5 | .2 | .3 | .7 | 22 | .04 | .043 | 14 | 11.9 | .34 | 51 | .030 | <1 | 1.08 | .004 | .05 | .2 | .04 | 1.1 | <.1 | <.05 | 6 | <.5 | 1.0 |
| 1860 375S | 1.0 | 7.9 | 13.2 | 43 | .1 | 7.1 | 3.7 | 175 | 1.54 | 2.9 | .8 | 7.7 | 3.3 | 9 | .1 | .3 | .6 | 29 | .08 | .033 | 21 | 10.5 | .18 | 32 | .042 | <1 | .86 | .006 | .05 | .1 | .02 | 1.1 | .1 | <.05 | 7 | <.5 | 7.5 |
| 1860 400S | 1.3 | 11.9 | 17.5 | 41 | .1 | 10.8 | 5.2 | 98 | 2.67 | 5.5 | .8 | 5.0 | 5.9 | 7 | .1 | .3 | .6 | 29 | .04 | .026 | 23 | 11.4 | .29 | 49 | .024 | <1 | 1.21 | .006 | .06 | .2 | .03 | 1.1 | .1 | <.05 | 7 | <.5 | 15.0 |
| 1860 425S | 1.9 | 22.2 | 49.5 | 107 | .1 | 31.5 | 17.4 | 416 | 3.77 | 8.4 | 1.3 | 2.3 | 6.2 | 15 | .2 | .3 | .9 | 28 | .17 | .051 | 15 | 17.2 | .48 | 182 | .017 | <1 | 2.58 | .006 | .13 | .2 | .03 | 1.8 | .1 | <.05 | 8 | <.5 | 7.5 |
| 1860 450S | 1.5 | 29.5 | 43.6 | 142 | .2 | 17.8 | 28.1 | 4843 | 2.98 | 6.9 | 3.2 | 5.7 | 1.2 | 16 | .7 | .4 | .7 | 26 | .15 | .105 | 16 | 14.6 | .40 | 184 | .016 | 1 | 1.79 | .006 | .08 | .1 | .06 | 1.3 | .1 | <.05 | 7 | .5 | 7.5 |
| 1860 475S | 1.3 | 33.6 | 74.6 | 116 | .3 | 15.6 | 25.4 | 5165 | 2.44 | 13.8 | 2.5 | 1.1 | .3 | 14 | 1.5 | .9 | .8 | 26 | .11 | .137 | 13 | 14.7 | .29 | 134 | .014 | 3 | 1.42 | .008 | .10 | .1 | .11 | .7 | .1 | .16 | 5 | .7 | 7.5 |
| 1860 500S | 1.1 | 21.8 | 83.1 | 110 | .1 | 21.5 | 22.9 | 3183 | 1.67 | 4.2 | 2.3 | .5 | .4 | 40 | 1.1 | .6 | .7 | 15 | .45 | .083 | 13 | 7.9 | .45 | 126 | .011 | 1 | .97 | .010 | .06 | .1 | .08 | .6 | <.1 | .12 | 3 | <.5 | 1.0 |
| 1860 525S | 2.3 | 16.3 | 22.4 | 107 | .2 | 18.7 | 16.4 | 954 | 2.57 | 6.6 | 1.6 | 1.7 | 3.0 | 18 | .4 | .2 | .5 | 27 | .16 | .038 | 24 | 14.1 | .45 | 72 | .034 | 1 | 1.76 | .010 | .07 | .1 | .02 | 1.6 | .1 | <.05 | 7 | <.5 | 7.5 |
| 1860 550S | 2.8 | 10.7 | 21.3 | 75 | .2 | 14.1 | 5.7 | 132 | 2.69 | 5.1 | .8 | 24.3 | 4.1 | 8 | .3 | .2 | .6 | 28 | .04 | .027 | 20 | 11.4 | .31 | 59 | .037 | 1 | 1.56 | .008 | .06 | .1 | .03 | 1.1 | .1 | <.05 | 8 | <.5 | 7.5 |
| RE 1860 600S | 1.2 | 13.7 | 13.9 | 56 | .1 | 10.6 | 5.6 | 303 | 2.44 | 5.1 | 1.6 | 7.4 | 5.0 | 4 | .1 | .2 | .4 | 28 | .04 | .095 | 20 | 13.4 | .29 | 78 | .029 | 1 | 1.94 | .006 | .07 | .2 | .07 | 1.6 | .1 | <.05 | 8 | <.5 | 7.5 |
| 1860 575S | 1.3 | 10.4 | 28.5 | 98 | .1 | 19.6 | 10.9 | 338 | 2.78 | 4.1 | 1.1 | 84.5 | 3.9 | 12 | .3 | .2 | .7 | 30 | .11 | .043 | 20 | 13.3 | .44 | 90 | .046 | 2 | 1.79 | .008 | .07 | .1 | .03 | 1.4 | .1 | <.05 | 8 | <.5 | 7.5 |
| 1860 600S | 1.2 | 13.6 | 14.5 | 57 | .1 | 10.6 | 5.6 | 306 | 2.44 | 4.6 | 1.6 | 4.4 | 5.0 | 4 | .1 | .2 | .4 | 28 | .04 | .091 | 21 | 14.0 | .29 | 79 | .033 | 1 | 1.97 | .006 | .08 | .2 | .06 | 1.6 | .1 | <.05 | 8 | <.5 | 7.5 |
| 1860 625S | 1.3 | 14.5 | 15.8 | 83 | .2 | 10.0 | 5.9 | 117 | 2.69 | 5.1 | 1.1 | 14.1 | 6.1 | 5 | .2 | .2 | .4 | 34 | .03 | .064 | 9 | 12.9 | .21 | 76 | .102 | 2 | 3.76 | .013 | .05 | .1 | .13 | 2.0 | .1 | <.05 | 10 | .5 | 15.0 |
| 1860 650S | 1.0 | 11.9 | 12.6 | 49 | .1 | 9.2 | 4.6 | 193 | 1.93 | 3.7 | .6 | 9.8 | 6.3 | 3 | .1 | .2 | .5 | 30 | .01 | .027 | 25 | 10.7 | .27 | 36 | .043 | 2 | 1.12 | .007 | .05 | .1 | .03 | 1.1 | .1 | <.05 | 8 | <.5 | 15.0 |
| 1860 675S | 1.0 | 11.3 | 16.4 | 62 | .1 | 8.6 | 4.2 | 139 | 2.98 | 5.7 | .6 | 6.2 | 5.3 | 6 | .3 | .2 | .5 | 31 | .05 | .074 | 23 | 11.7 | .28 | 70 | .040 | 1 | 1.15 | .007 | .05 | .2 | .03 | 1.0 | .1 | <.05 | 8 | <.5 | 15.0 |
| 1860 700S | 1.0 | 16.9 | 18.7 | 75 | .2 | 14.2 | 9.6 | 385 | 3.24 | 5.5 | .9 | 56.9 | 7.0 | 3 | .2 | .2 | .5 | 27 | .02 | .087 | 29 | 13.9 | .46 | 58 | .035 | 2 | 1.56 | .005 | .05 | .1 | .05 | 1.3 | .1 | <.05 | 7 | <.5 | 15.0 |
| STANDARD DS5 | 12.7 | 144.2 | 26.1 | 141 | .3 | 25.2 | 11.2 | 769 | 2.98 | 18.0 | 6.7 | 44.5 | 3.1 | 48 | 5.7 | 3.7 | 6.1 | 61 | .73 | .091 | 13 | 190.2 | .71 | 136 | .097 | 16 | 1.99 | .034 | .14 | 4.7 | .18 | 3.3 | 1.1 | <.05 | 6 | 5.0 | 15.0 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data ___ FA ___

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

# GEOCHEMICAL ANALYSIS CERTIFICATE

Ruby Red Resources Inc. PROJECT EDDY File # A403182 Page 1
207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au* ppb |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| G-1 | 2 | 2 | 4 | 36 | <.3 | 4 | 3 | 480 | 1.75 | <2 | <8 | <2 | 4 | 78 | <.5 | <3 | <3 | 37 | .53 | .084 | 7 | 33 | .49 | 207 | .12 | <3 | .83 | .09 | .46 | <2 | .5 |
| 5800N 425E | <1 | 102 | 17 | 102 | .5 | 25 | 21 | 384 | 5.30 | 10 | <8 | <2 | 3 | 11 | <.5 | <3 | <3 | 190 | .18 | .042 | 6 | 16 | .55 | 65 | .11 | 6 | 2.42 | .01 | .05 | <2 | 5.1 |
| 5800N 450E | 1 | 58 | 13 | 95 | .7 | 28 | 18 | 296 | 4.35 | 7 | <8 | <2 | 3 | 22 | <.5 | <3 | 5 | 140 | .26 | .026 | 7 | 16 | .50 | 97 | .10 | 10 | 2.52 | .01 | .06 | <2 | 2.8 |
| 5800N 475E | <1 | 23 | 18 | 49 | .9 | 16 | 9 | 178 | 3.13 | 4 | <8 | <2 | 2 | 17 | <.5 | <3 | <3 | 72 | .22 | .020 | 7 | 9 | .24 | 65 | .16 | <3 | 2.17 | .03 | .04 | <2 | .3 |
| 5800N 500E | 1 | 31 | 12 | 59 | <.3 | 27 | 10 | 159 | 3.17 | 5 | <8 | <2 | <2 | 6 | <.5 | <3 | <3 | 97 | .14 | .020 | 5 | 38 | .57 | 33 | .07 | <3 | 1.52 | .01 | .04 | <2 | 1.4 |
| 5800N 525E | <1 | 42 | 13 | 47 | .4 | 36 | 20 | 911 | 2.42 | 3 | <8 | <2 | 2 | 7 | <.5 | <3 | <3 | 63 | .19 | .015 | 4 | 61 | .53 | 49 | .06 | <3 | 2.30 | .01 | .03 | <2 | .3 |
| 5800N 550E | <1 | 27 | 14 | 73 | .3 | 49 | 23 | 204 | 2.84 | 2 | <8 | <2 | <2 | 10 | <.5 | <3 | <3 | 62 | .21 | .017 | 3 | 70 | .65 | 46 | .08 | <3 | 2.16 | .01 | .03 | <2 | .1 |
| 5800N 575E | <1 | 23 | 14 | 38 | .3 | 25 | 11 | 143 | 2.91 | 5 | <8 | <2 | 2 | 13 | <.5 | <3 | <3 | 67 | .23 | .019 | 10 | 39 | .46 | 48 | .08 | <3 | 1.79 | .01 | .09 | <2 | .1 |
| 5800N 600E | <1 | 23 | 19 | 63 | .4 | 27 | 13 | 169 | 3.11 | <2 | <8 | <2 | 5 | 12 | <.5 | <3 | 4 | 61 | .15 | .026 | 29 | 27 | .31 | 108 | .10 | <3 | 2.74 | .01 | .08 | <2 | .6 |
| 5800N 625E | <1 | 9 | 9 | 47 | .4 | 13 | 7 | 117 | 2.17 | 3 | <8 | <2 | 3 | 5 | <.5 | <3 | 3 | 50 | .07 | .019 | 8 | 7 | .28 | 70 | .05 | <3 | 1.39 | .01 | .06 | <2 | .6 |
| 5800N 650E | <1 | 15 | 15 | 48 | <.3 | 16 | 16 | 113 | 2.89 | 3 | <8 | <2 | 3 | 6 | <.5 | <3 | <3 | 49 | .09 | .060 | 4 | 16 | .24 | 55 | .11 | <3 | 4.28 | .02 | .03 | <2 | .9 |
| 5800N 675E | <1 | 13 | 12 | 22 | <.3 | 15 | 22 | 322 | 2.60 | <2 | <8 | <2 | 4 | 11 | <.5 | <3 | 4 | 41 | .13 | .088 | 5 | 10 | .15 | 127 | .14 | <3 | 5.31 | .02 | .02 | <2 | 2.6 |
| 5800N 700E | <1 | 17 | 10 | 45 | <.3 | 18 | 15 | 661 | 2.23 | 3 | <8 | <2 | 4 | 7 | <.5 | <3 | 5 | 49 | .10 | .019 | 13 | 14 | .57 | 75 | .04 | <3 | 1.69 | .01 | .04 | <2 | .5 |
| 5700N 200E | 1 | 10 | 21 | 91 | <.3 | 14 | 10 | 446 | 1.97 | 3 | <8 | <2 | 5 | 6 | <.5 | <3 | <3 | 27 | .07 | .048 | 11 | 3 | .37 | 73 | .05 | 3 | 2.12 | .01 | .07 | <2 | 4.0 |
| 5700N 225E | <1 | 9 | 15 | 69 | <.3 | 12 | 8 | 239 | 2.22 | 2 | <8 | <2 | 4 | 5 | <.5 | <3 | <3 | 37 | .07 | .037 | 12 | <1 | .40 | 58 | .05 | <3 | 1.83 | .01 | .05 | <2 | .3 |
| 5700N 250E | 1 | 23 | 15 | 64 | <.3 | 16 | 11 | 228 | 2.34 | 4 | <8 | <2 | 5 | 5 | <.5 | <3 | <3 | 42 | .07 | .039 | 13 | 7 | .64 | 55 | .06 | <3 | 2.10 | .01 | .06 | 2 | 3.0 |
| 5700N 275E | <1 | 28 | 23 | 58 | <.3 | 16 | 10 | 153 | 2.95 | 2 | <8 | <2 | 5 | 4 | <.5 | <3 | <3 | 58 | .05 | .036 | 11 | 3 | .53 | 54 | .06 | <3 | 2.61 | .01 | .05 | <2 | 3.4 |
| 5700N 300E | <1 | 31 | 23 | 65 | <.3 | 15 | 15 | 189 | 3.10 | 3 | <8 | <2 | 4 | 6 | <.5 | <3 | <3 | 69 | .09 | .051 | 8 | 3 | .40 | 58 | .06 | <3 | 2.87 | .02 | .05 | <2 | 22.2 |
| 5700N 325E | <1 | 16 | 13 | 33 | <.3 | 8 | 5 | 130 | 2.27 | 5 | <8 | <2 | 2 | 4 | <.5 | <3 | <3 | 75 | .09 | .030 | 9 | <1 | .26 | 29 | .06 | <3 | 1.09 | .01 | .04 | <2 | 2.4 |
| 5700N 350E | <1 | 59 | 12 | 74 | .3 | 14 | 15 | 387 | 3.61 | 7 | <8 | <2 | 2 | 6 | <.5 | <3 | <3 | 115 | .14 | .073 | 6 | 5 | .32 | 46 | .08 | <3 | 2.30 | .01 | .06 | <2 | 4.1 |
| RE 5700N 350E | <1 | 60 | 19 | 74 | .3 | 14 | 15 | 402 | 3.68 | 6 | <8 | <2 | 2 | 6 | <.5 | <3 | <3 | 118 | .15 | .075 | 6 | 5 | .33 | 48 | .09 | <3 | 2.37 | .01 | .06 | <2 | 1.6 |
| 5700N 375E | 2 | 141 | 20 | 82 | .3 | 20 | 24 | 392 | 3.80 | 5 | <8 | <2 | 4 | 10 | <.5 | <3 | <3 | 122 | .22 | .057 | 8 | 7 | .35 | 54 | .08 | <3 | 3.08 | .02 | .10 | <2 | 5.0 |
| 5700N 400E | 1 | 53 | 15 | 66 | <.3 | 15 | 13 | 244 | 3.94 | 6 | <8 | <2 | 2 | 12 | <.5 | <3 | <3 | 141 | .24 | .032 | 8 | 7 | .42 | 50 | .08 | 4 | 1.64 | .01 | .04 | <2 | 1.4 |
| 5700N 425E | 1 | 80 | 24 | 85 | .6 | 30 | 24 | 527 | 4.57 | 7 | <8 | <2 | 5 | 17 | .5 | <3 | <3 | 137 | .16 | .030 | 14 | 21 | .48 | 150 | .13 | <3 | 3.51 | .02 | .06 | <2 | 7.3 |
| 5700N 450E | 1 | 47 | 15 | 83 | <.3 | 18 | 15 | 225 | 4.19 | 6 | <8 | <2 | 3 | 8 | <.5 | <3 | <3 | 128 | .19 | .034 | 11 | 21 | .66 | 60 | .08 | <3 | 1.89 | .01 | .06 | <2 | 11.7 |
| 5700N 475E | 1 | 26 | 14 | 42 | <.3 | 13 | 10 | 173 | 2.69 | 4 | <8 | <2 | 2 | 10 | <.5 | <3 | <3 | 77 | .19 | .014 | 8 | 7 | .49 | 50 | .08 | <3 | 1.53 | .01 | .04 | <2 | .3 |
| 5700N 500E | 1 | 28 | 18 | 43 | <.3 | 15 | 12 | 120 | 2.81 | 3 | <8 | <2 | 3 | 6 | <.5 | <3 | 3 | 74 | .10 | .018 | 7 | 17 | .34 | 54 | .09 | <3 | 2.22 | .02 | .04 | <2 | 3.6 |
| 5700N 525E | <1 | 11 | 20 | 66 | <.3 | 45 | 21 | 417 | 3.57 | 6 | <8 | <2 | <2 | 11 | <.5 | <3 | <3 | 94 | .27 | .019 | 5 | 114 | .82 | 51 | .08 | <3 | 2.32 | .01 | .04 | <2 | .4 |
| 5700N 550E | 1 | 18 | 20 | 50 | <.3 | 26 | 20 | 898 | 2.92 | 3 | <8 | <2 | 2 | 13 | <.5 | <3 | <3 | 77 | .26 | .017 | 7 | 47 | .48 | 53 | .08 | <3 | 1.87 | .01 | .04 | <2 | .4 |
| 5700N 575E | 1 | 15 | 11 | 67 | .3 | 17 | 10 | 308 | 2.37 | 4 | <8 | <2 | 2 | 7 | <.5 | <3 | <3 | 55 | .12 | .019 | 6 | 19 | .30 | 64 | .07 | <3 | 1.73 | .01 | .07 | <2 | 1.3 |
| 5700N 600E | <1 | 12 | 9 | 25 | <.3 | 15 | 6 | 99 | 1.95 | 3 | <8 | <2 | <2 | 13 | <.5 | <3 | <3 | 61 | .22 | .011 | 6 | 18 | .28 | 41 | .07 | <3 | 1.36 | .01 | .03 | <2 | 2.7 |
| 5700N 625E | 2 | 14 | 20 | 46 | <.3 | 11 | 8 | 172 | 2.02 | 3 | <8 | <2 | 3 | 5 | <.5 | <3 | 3 | 49 | .08 | .027 | 10 | 2 | .30 | 70 | .05 | <3 | 1.45 | .01 | .04 | <2 | 5.2 |
| 5700N 650E | 2 | 26 | 18 | 43 | <.3 | 15 | 10 | 125 | 2.67 | 6 | <8 | <2 | 4 | 5 | <.5 | <3 | <3 | 54 | .09 | .043 | 11 | 10 | .48 | 48 | .05 | <3 | 1.69 | .01 | .04 | <2 | 7.1 |
| 5700N 675E | <1 | 27 | 16 | 68 | <.3 | 18 | 14 | 314 | 2.53 | 2 | <8 | <2 | 3 | 5 | <.5 | <3 | <3 | 54 | .09 | .030 | 10 | 6 | .50 | 70 | .06 | <3 | 1.70 | .01 | .06 | <2 | 7.9 |
| 5700N 700E | 1 | 47 | 29 | 19 | .7 | 27 | 4 | 89 | .79 | 3 | 11 | <2 | 2 | 70 | .9 | <3 | <3 | 27 | 1.33 | .049 | 55 | 34 | .32 | 78 | .03 | <3 | 1.72 | .02 | .04 | <2 | 2.8 |
| STANDARD DS5 | 13 | 147 | 26 | 137 | .4 | 26 | 12 | 791 | 3.06 | 18 | <8 | <2 | 3 | 46 | 5.8 | 4 | 6 | 61 | .77 | .098 | 11 | 196 | .71 | 143 | .10 | 16 | 2.02 | .04 | .15 | 5 | 44.0 |

GROUP 1D - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: SOIL SS80 60C AU* BY ACID LEACHED, ANALYZED BY ICP-MS. (15.00 gm)
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data d FA ____ DATE RECEIVED: JUN 29 2004 DATE REPORT MAILED: July 14/04

BRITISH COLUMBIA CERTIFIED ASSAYER
Clarence Leong

ACME ANALYTICAL

# Ruby Red Resources Inc. PROJECT EDDY FILE # A403182



ACME ANALYTICAL

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au* ppb |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 5600N 200E | 1 | 11 | 22 | 36 | <.3 | 11 | 7 | 175 | 2.01 | 3 | <8 | <2 | 4 | 7 | <.5 | <3 | <3 | 34 | .13 | .019 | 17 | <1 | .50 | 53 | .04 | 3 | 1.35 | .01 | .04 | <2 | 1.5 |
| 5600N 225E | 1 | 20 | 19 | 48 | <.3 | 16 | 10 | 154 | 2.79 | 4 | <8 | <2 | 4 | 6 | <.5 | <3 | <3 | 48 | .09 | .036 | 10 | 1 | .51 | 62 | .06 | <3 | 2.59 | .01 | .07 | <2 | 14.4 |
| 5600N 250E | <1 | 14 | 24 | 38 | <.3 | 10 | 6 | 113 | 2.75 | 5 | <8 | <2 | 3 | 7 | <.5 | <3 | <3 | 53 | .09 | .050 | 12 | 1 | .36 | 47 | .05 | <3 | 1.64 | .01 | .04 | <2 | 29.3 |
| 5600N 275E | <1 | 17 | 32 | 58 | <.3 | 10 | 6 | 144 | 2.90 | 5 | <8 | <2 | 3 | 5 | <.5 | <3 | 4 | 57 | .08 | .055 | 10 | <1 | .34 | 43 | .05 | <3 | 1.89 | .01 | .05 | <2 | 14.6 |
| 5600N 300E | <1 | 48 | 49 | 109 | .4 | 19 | 15 | 162 | 3.06 | 2 | <8 | <2 | 5 | 12 | .6 | <3 | <3 | 54 | .14 | .109 | 9 | 3 | .34 | 88 | .10 | <3 | 3.82 | .02 | .06 | <2 | 1.3 |
| 5600N 325E | <1 | 70 | 31 | 86 | <.3 | 17 | 22 | 334 | 3.31 | 4 | <8 | <2 | 3 | 9 | <.5 | <3 | <3 | 97 | .15 | .025 | 11 | 7 | .55 | 63 | .08 | <3 | 1.99 | .01 | .05 | 2 | 1.2 |
| 5600N 350E | <1 | 46 | 26 | 90 | <.3 | 33 | 16 | 440 | 4.33 | 14 | <8 | <2 | 2 | 23 | <.5 | <3 | <3 | 117 | .28 | .056 | 8 | 19 | .67 | 128 | .09 | <3 | 2.24 | .01 | .07 | <2 | 5.6 |
| 5600N 375E | <1 | 51 | 20 | 79 | <.3 | 20 | 26 | 692 | 5.26 | 4 | <8 | <2 | 2 | 16 | <.5 | <3 | <3 | 178 | .20 | .034 | 13 | 15 | .32 | 49 | .09 | <3 | 2.58 | .01 | .04 | <2 | 3.3 |
| 5600N 400E | <1 | 56 | 14 | 125 | .4 | 21 | 20 | 564 | 4.40 | 3 | <8 | <2 | 2 | 11 | <.5 | <3 | <3 | 150 | .17 | .051 | 5 | 8 | .22 | 63 | .11 | <3 | 2.64 | .01 | .08 | 2 | <.5 |
| 5600N 425E | 1 | 27 | 11 | 83 | <.3 | 20 | 18 | 387 | 3.05 | 6 | <8 | <2 | 5 | 8 | .5 | <3 | <3 | 87 | .12 | .034 | 10 | 9 | .31 | 69 | .07 | <3 | 2.03 | .01 | .06 | <2 | 2.8 |
| 5600N 450E | <1 | 16 | 18 | 65 | .3 | 16 | 11 | 309 | 2.59 | 6 | <8 | <2 | 3 | 9 | <.5 | <3 | <3 | 67 | .17 | .025 | 8 | 17 | .32 | 65 | .06 | <3 | 1.59 | .01 | .06 | <2 | 1.8 |
| 5600N 475E | 2 | 39 | 27 | 100 | <.3 | 53 | 25 | 262 | 4.45 | 19 | <8 | <2 | <2 | 14 | <.5 | <3 | <3 | 110 | .23 | .032 | 3 | 151 | .93 | 72 | .10 | <3 | 3.67 | .01 | .04 | <2 | 1.3 |
| 5600N 500E | <1 | 21 | 12 | 156 | .3 | 41 | 20 | 531 | 3.83 | 8 | <8 | <2 | 2 | 10 | <.5 | <3 | <3 | 90 | .18 | .027 | 4 | 83 | .94 | 78 | .09 | <3 | 2.69 | .01 | .06 | 2 | <.5 |
| 5600N 525E | 1 | 19 | 12 | 24 | .4 | 19 | 10 | 114 | 2.99 | 5 | <8 | <2 | <2 | 19 | <.5 | <3 | <3 | 64 | .25 | .035 | 5 | 41 | .16 | 56 | .15 | <3 | 3.59 | .02 | .03 | <2 | 2.0 |
| RE 5600N 525E | <1 | 20 | 9 | 24 | .5 | 18 | 10 | 113 | 3.01 | 6 | <8 | <2 | 2 | 19 | <.5 | <3 | <3 | 64 | .25 | .036 | 6 | 38 | .16 | 56 | .15 | <3 | 3.64 | .03 | .03 | <2 | 1.6 |
| 5600N 550E | <1 | 27 | 21 | 55 | .3 | 30 | 18 | 554 | 3.75 | 10 | <8 | <2 | 4 | 23 | <.5 | <3 | <3 | 101 | .34 | .022 | 10 | 48 | .50 | 100 | .09 | <3 | 3.06 | .02 | .05 | <2 | 2.7 |
| 5600N 575E | <1 | 23 | 19 | 54 | <.3 | 20 | 10 | 101 | 3.68 | 5 | <8 | <2 | 4 | 5 | <.5 | <3 | <3 | 74 | .07 | .057 | 6 | 25 | .38 | 56 | .08 | <3 | 3.50 | .01 | .04 | <2 | 1.4 |
| 5600N 600E | <1 | 14 | 6 | 27 | <.3 | 13 | 7 | 82 | 2.60 | 5 | <8 | <2 | 6 | 5 | <.5 | <3 | <3 | 38 | .07 | .028 | 6 | 8 | .25 | 57 | .05 | <3 | 2.53 | .01 | .03 | <2 | 1.4 |
| 5600N 625E | 1 | 11 | 8 | 41 | <.3 | 21 | 12 | 150 | 2.89 | <2 | <8 | <2 | 3 | 8 | <.5 | <3 | <3 | 56 | .10 | .022 | 5 | 11 | .29 | 127 | .11 | <3 | 3.31 | .02 | .05 | <2 | 1.0 |
| 5600N 650E | <1 | 13 | 14 | 14 | .3 | 15 | 4 | 51 | 1.42 | 6 | <8 | <2 | 6 | 33 | <.5 | <3 | <3 | 26 | .67 | .017 | 15 | 19 | .51 | 49 | .02 | <3 | 1.67 | .01 | .05 | <2 | <.5 |
| 5600N 675E | <1 | 31 | 10 | 50 | <.3 | 22 | 14 | 181 | 2.80 | 8 | <8 | <2 | 3 | 7 | <.5 | <3 | <3 | 72 | .16 | .019 | 6 | 29 | .63 | 56 | .07 | <3 | 1.44 | .01 | .04 | <2 | .6 |
| 5600N 700E | <1 | 42 | 16 | 52 | <.3 | 28 | 10 | 168 | 3.38 | 8 | <8 | <2 | 4 | 5 | <.5 | <3 | <3 | 89 | .13 | .021 | 10 | 41 | .81 | 50 | .09 | <3 | 1.83 | .01 | .06 | <2 | 1.2 |
| 5500N 200E | 1 | 22 | 18 | 73 | <.3 | 17 | 10 | 404 | 2.48 | 4 | <8 | <2 | 6 | 6 | <.5 | 3 | <3 | 39 | .06 | .043 | 16 | 5 | .82 | 66 | .06 | <3 | 2.15 | .01 | .08 | <2 | 3.5 |
| 5500N 225E | 1 | 19 | 15 | 64 | <.3 | 13 | 8 | 329 | 2.66 | 3 | <8 | <2 | 4 | 5 | <.5 | <3 | <3 | 56 | .07 | .028 | 18 | 1 | .73 | 44 | .04 | <3 | 1.50 | .01 | .05 | <2 | 15.3 |
| 5500N 250E | <1 | 22 | 20 | 62 | <.3 | 13 | 8 | 161 | 2.65 | 7 | <8 | <2 | 5 | 5 | <.5 | <3 | <3 | 50 | .07 | .036 | 13 | 2 | .54 | 52 | .06 | <3 | 2.03 | .01 | .05 | <2 | 12.1 |
| 5500N 275E | 2 | 12 | 37 | 94 | .5 | 9 | 7 | 176 | 2.17 | 2 | <8 | <2 | 3 | 5 | .5 | <3 | <3 | 36 | .06 | .092 | 8 | <1 | .22 | 67 | .07 | <3 | 2.07 | .02 | .05 | <2 | 4.1 |
| 5500N 300E | <1 | 21 | 16 | 91 | .3 | 8 | 10 | 425 | 2.30 | <2 | <8 | <2 | 2 | 5 | .9 | <3 | <3 | 41 | .05 | .176 | 5 | <1 | .15 | 57 | .11 | <3 | 3.36 | .02 | .03 | <2 | <.5 |
| 5500N 325E | 1 | 17 | 19 | 89 | <.3 | 9 | 7 | 114 | 2.48 | 3 | <8 | <2 | <2 | 8 | .5 | <3 | <3 | 73 | .12 | .028 | 6 | 1 | .20 | 42 | .07 | <3 | 1.21 | .01 | .04 | <2 | 3.3 |
| 5500N 350E | 1 | 27 | 15 | 83 | .3 | 14 | 13 | 386 | 3.44 | 8 | <8 | <2 | 4 | 6 | <.5 | <3 | <3 | 88 | .11 | .048 | 10 | 8 | .43 | 49 | .06 | <3 | 2.30 | .01 | .06 | <2 | 2.0 |
| 5500N 375E | 1 | 10 | 9 | 77 | .4 | 10 | 7 | 136 | 2.98 | 2 | <8 | <2 | 3 | 8 | .5 | <3 | <3 | 56 | .09 | .035 | 8 | 2 | .21 | 54 | .08 | <3 | 2.15 | .01 | .05 | <2 | 1.5 |
| 5500N 400E | <1 | 24 | 7 | 91 | .4 | 24 | 11 | 324 | 3.86 | 2 | <8 | <2 | 2 | 15 | <.5 | <3 | <3 | 107 | .15 | .055 | 4 | 13 | .30 | 64 | .11 | <3 | 3.64 | .02 | .09 | <2 | <.5 |
| 5500N 425E | <1 | 14 | 11 | 80 | .3 | 15 | 9 | 198 | 2.95 | 5 | <8 | <2 | 3 | 9 | <.5 | <3 | <3 | 83 | .12 | .029 | 9 | 11 | .35 | 53 | .10 | <3 | 1.65 | .01 | .06 | <2 | 74.6 |
| 5500N 450E | 1 | 34 | 12 | 39 | <.3 | 18 | 12 | 535 | 2.73 | 7 | <8 | <2 | 3 | 14 | <.5 | <3 | <3 | 85 | .24 | .023 | 9 | 19 | .55 | 54 | .07 | <3 | 1.58 | .01 | .04 | <2 | 9.5 |
| 5500N 475E | 1 | 21 | 9 | 71 | <.3 | 25 | 14 | 678 | 2.96 | 6 | <8 | <2 | 2 | 18 | <.5 | <3 | <3 | 80 | .27 | .022 | 8 | 33 | .58 | 65 | .07 | <3 | 2.00 | .01 | .05 | <2 | 1.0 |
| STANDARD DS5 | 12 | 143 | 23 | 129 | .3 | 25 | 12 | 753 | 3.03 | 18 | <8 | <2 | 3 | 47 | 5.6 | 4 | 6 | 58 | .72 | .093 | 11 | 188 | .67 | 138 | .09 | 15 | 1.96 | .04 | .14 | 6 | 45.3 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data FA

ACME ANALYTICAL

# Ruby Red Resources Inc. PROJECT EDDY FILE # A403182



ACME ANALYTICAL

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au* ppb |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 5500N 500E | 2 | 16 | 20 | 82 | .6 | 19 | 15 | 211 | 2.91 | 7 | <8 | <2 | 2 | 10 | <.5 | <3 | <3 | 56 | .14 | .043 | 4 | 26 | .26 | 54 | .11 | <3 | 3.04 | .02 | .05 | <2 | 1.0 |
| 5500N 525E | 2 | 23 | 17 | 47 | .3 | 25 | 14 | 282 | 3.03 | 12 | <8 | <2 | 2 | 25 | <.5 | <3 | <3 | 89 | .44 | .022 | 7 | 45 | .48 | 90 | .07 | <3 | 2.44 | .02 | .05 | <2 | <.5 |
| 5500N 550E | 1 | 21 | 10 | 69 | <.3 | 26 | 11 | 139 | 2.63 | 5 | <8 | <2 | 2 | 7 | <.5 | <3 | <3 | 61 | .15 | .031 | 6 | 38 | .50 | 55 | .07 | <3 | 2.34 | .01 | .04 | 2 | 19.4 |
| 5500N 575E | 1 | 41 | 18 | 64 | <.3 | 42 | 17 | 215 | 2.90 | 7 | <8 | <2 | <2 | 6 | <.5 | <3 | <3 | 73 | .16 | .021 | 4 | 81 | .83 | 51 | .08 | <3 | 2.50 | .01 | .03 | <2 | 1.8 |
| 5500N 600E | <1 | 21 | 12 | 46 | <.3 | 21 | 9 | 110 | 2.63 | 4 | <8 | <2 | 2 | 7 | <.5 | <3 | <3 | 57 | .16 | .020 | 6 | 29 | .37 | 50 | .08 | <3 | 2.31 | .01 | .04 | <2 | 1.5 |
| 5500N 625E | <1 | 14 | 12 | 48 | <.3 | 17 | 8 | 157 | 2.67 | 5 | <8 | <2 | 2 | 5 | <.5 | <3 | <3 | 52 | .10 | .023 | 7 | 17 | .27 | 69 | .05 | <3 | 2.32 | .01 | .05 | <2 | 1.6 |
| 5500N 650E | 2 | 29 | 16 | 44 | <.3 | 18 | 8 | 138 | 2.47 | 6 | <8 | <2 | 4 | 6 | <.5 | <3 | <3 | 46 | .11 | .015 | 13 | 15 | .53 | 39 | .07 | <3 | 1.73 | .01 | .07 | <2 | 4.8 |
| 5500N 675E | 1 | 18 | 9 | 32 | <.3 | 12 | 6 | 103 | 2.82 | 7 | <8 | <2 | 3 | 8 | <.5 | <3 | <3 | 56 | .12 | .024 | 8 | 16 | .29 | 50 | .09 | <3 | 1.85 | .02 | .04 | <2 | 1.7 |
| 5500N 700E | <1 | 16 | 7 | 28 | <.3 | 13 | 6 | 100 | 2.45 | 10 | <8 | <2 | 2 | 13 | <.5 | <3 | <3 | 66 | .31 | .015 | 10 | 17 | .60 | 55 | .05 | <3 | 1.49 | .01 | .04 | <2 | 10.3 |
| 850N 8900E | 1 | 16 | 11 | 110 | <.3 | 15 | 14 | 686 | 2.35 | 5 | <8 | <2 | 2 | 7 | <.5 | <3 | <3 | 52 | .15 | .069 | 5 | 1 | .22 | 61 | .11 | <3 | 2.20 | .02 | .06 | <2 | .9 |
| 850N 8925E | 2 | 87 | 18 | 89 | .3 | 39 | 16 | 440 | 3.34 | 2 | <8 | <2 | 5 | 14 | <.5 | <3 | <3 | 77 | .16 | .072 | 10 | 10 | .35 | 99 | .16 | <3 | 4.26 | .02 | .09 | <2 | 1.5 |
| 850N 8950E | 1 | 72 | 10 | 64 | <.3 | 17 | 11 | 929 | 2.24 | 2 | <8 | <2 | 3 | 10 | <.5 | <3 | <3 | 60 | .23 | .030 | 11 | 3 | .41 | 51 | .06 | <3 | 1.51 | .01 | .06 | <2 | 1.3 |
| 850N 8975E | <1 | 21 | 12 | 91 | <.3 | 12 | 13 | 1078 | 2.44 | 3 | <8 | <2 | 3 | 13 | <.5 | <3 | <3 | 56 | .21 | .076 | 9 | 5 | .22 | 69 | .07 | <3 | 1.66 | .01 | .06 | <2 | <.5 |
| 850N 9000E | 1 | 30 | 11 | 73 | .5 | 21 | 11 | 167 | 2.82 | <2 | <8 | <2 | 4 | 10 | <.5 | <3 | <3 | 57 | .15 | .081 | 11 | 6 | .25 | 81 | .09 | <3 | 2.77 | .02 | .07 | <2 | .8 |
| 850N 9025E | 1 | 23 | 11 | 79 | .4 | 15 | 9 | 151 | 2.43 | 2 | <8 | <2 | 4 | 11 | <.5 | <3 | <3 | 44 | .22 | .117 | 11 | 4 | .25 | 65 | .07 | <3 | 2.28 | .02 | .07 | <2 | 1.4 |
| 850N 9050E | 1 | 12 | 12 | 68 | <.3 | 10 | 6 | 140 | 2.17 | 4 | <8 | <2 | 5 | 6 | <.5 | <3 | <3 | 30 | .06 | .127 | 6 | 2 | .12 | 61 | .11 | <3 | 3.07 | .02 | .06 | <2 | 1.3 |
| 850N 9075E | 1 | 24 | 12 | 60 | .4 | 14 | 10 | 340 | 2.13 | 3 | <8 | <2 | 6 | 7 | <.5 | <3 | <3 | 34 | .10 | .077 | 12 | 3 | .24 | 88 | .08 | <3 | 2.83 | .02 | .09 | <2 | 1.2 |
| RE 850N 9075E | 1 | 26 | 11 | 62 | .3 | 15 | 11 | 357 | 2.21 | <2 | <8 | <2 | 6 | 7 | <.5 | <3 | <3 | 35 | .10 | .081 | 13 | 5 | .25 | 92 | .08 | <3 | 2.96 | .02 | .09 | <2 | 1.1 |
| 850N 9100E | <1 | 15 | 12 | 74 | .5 | 12 | 7 | 117 | 1.99 | <2 | <8 | <2 | 3 | 6 | <.5 | <3 | <3 | 31 | .06 | .158 | 5 | <1 | .10 | 70 | .13 | <3 | 3.48 | .02 | .05 | <2 | 1.2 |
| 850N 9125E | 2 | 8 | 15 | 89 | <.3 | 10 | 4 | 90 | 2.26 | 3 | <8 | <2 | 5 | 8 | <.5 | <3 | <3 | 36 | .12 | .137 | 13 | 2 | .16 | 67 | .09 | <3 | 1.75 | .01 | .09 | <2 | .8 |
| 850N 9150E | <1 | 8 | 12 | 61 | <.3 | 10 | 5 | 176 | 1.61 | 2 | <8 | <2 | 4 | 5 | <.5 | <3 | <3 | 25 | .07 | .064 | 15 | <1 | .24 | 69 | .04 | <3 | 1.35 | .01 | .09 | <2 | 1.5 |
| 850N 9175E | <1 | 14 | 6 | 92 | <.3 | 14 | 8 | 199 | 1.76 | 2 | <8 | <2 | 4 | 6 | <.5 | <3 | <3 | 27 | .05 | .110 | 6 | <1 | .11 | 75 | .15 | <3 | 3.09 | .02 | .05 | <2 | 1.1 |
| 850N 9200E | <1 | 8 | 12 | 78 | <.3 | 10 | 5 | 308 | 1.82 | 2 | <8 | <2 | 4 | 6 | <.5 | <3 | <3 | 28 | .09 | .064 | 10 | <1 | .22 | 65 | .07 | <3 | 1.54 | .01 | .10 | <2 | .5 |
| 850N 9225E | <1 | 7 | 10 | 52 | <.3 | 10 | 6 | 137 | 1.80 | <2 | <8 | <2 | 4 | 7 | <.5 | <3 | <3 | 28 | .09 | .049 | 11 | <1 | .31 | 54 | .06 | <3 | 1.47 | .01 | .07 | <2 | <.5 |
| 850N 9250E | 1 | 10 | 11 | 77 | <.3 | 13 | 11 | 511 | 1.74 | 3 | <8 | <2 | 2 | 9 | <.5 | <3 | <3 | 29 | .08 | .053 | 8 | <1 | .37 | 75 | .09 | <3 | 1.81 | .02 | .08 | <2 | .9 |
| 850N 9275E | 1 | 10 | 8 | 69 | <.3 | 12 | 9 | 914 | 1.84 | <2 | <8 | <2 | 3 | 7 | <.5 | <3 | <3 | 31 | .07 | .074 | 11 | <1 | .21 | 96 | .07 | <3 | 1.79 | .01 | .06 | <2 | 1.7 |
| 850N 9300E | 1 | 11 | 26 | 130 | <.3 | 16 | 11 | 1129 | 1.98 | <2 | <8 | <2 | 5 | 15 | <.5 | <3 | <3 | 31 | .15 | .058 | 13 | 1 | .22 | 183 | .11 | <3 | 1.74 | .01 | .11 | <2 | .9 |
| 850N 9325E | 2 | 21 | 19 | 103 | <.3 | 22 | 18 | 1531 | 2.76 | <2 | <8 | <2 | 6 | 12 | <.5 | <3 | <3 | 44 | .16 | .045 | 17 | 6 | .41 | 144 | .09 | <3 | 2.52 | .01 | .12 | <2 | 2.4 |
| 850N 9350E | 2 | 21 | 21 | 156 | <.3 | 19 | 16 | 1119 | 2.74 | 4 | <8 | <2 | 7 | 22 | <.5 | <3 | <3 | 42 | .20 | .094 | 18 | 7 | .35 | 286 | .08 | <3 | 2.45 | .01 | .11 | 2 | .8 |
| 850N 9375E | 1 | 23 | 18 | 81 | <.3 | 19 | 14 | 1470 | 2.88 | <2 | <8 | <2 | 6 | 9 | <.5 | <3 | <3 | 51 | .11 | .037 | 16 | 7 | .43 | 136 | .07 | <3 | 2.48 | .01 | .10 | <2 | 6.5 |
| 850N 9400E | 2 | 35 | 16 | 69 | <.3 | 18 | 14 | 251 | 2.94 | <2 | <8 | <2 | 9 | 5 | <.5 | <3 | <3 | 53 | .06 | .061 | 15 | 6 | .51 | 86 | .10 | <3 | 3.16 | .01 | .11 | <2 | 5.7 |
| 850N 9425E | 1 | 21 | 22 | 47 | <.3 | 13 | 12 | 412 | 2.65 | 3 | <8 | <2 | 6 | 5 | <.5 | <3 | <3 | 49 | .06 | .029 | 16 | 1 | .45 | 59 | .05 | <3 | 1.65 | .01 | .07 | <2 | 11.6 |
| 850N 9450E | 2 | 37 | 19 | 69 | <.3 | 20 | 15 | 245 | 3.12 | 5 | <8 | <2 | 9 | 5 | <.5 | <3 | <3 | 57 | .07 | .042 | 18 | 8 | .56 | 79 | .08 | <3 | 2.56 | .01 | .11 | <2 | 8.2 |
| 850N 9475E | 1 | 13 | 17 | 77 | <.3 | 19 | 14 | 730 | 2.69 | 4 | <8 | <2 | 4 | 7 | <.5 | <3 | <3 | 49 | .08 | .038 | 12 | 5 | .34 | 102 | .08 | <3 | 2.44 | .01 | .09 | <2 | 4.6 |
| STANDARD DS5 | 14 | 145 | 23 | 138 | .3 | 26 | 12 | 786 | 3.08 | 18 | <8 | <2 | 3 | 46 | 5.7 | 4 | 5 | 62 | .77 | .097 | 12 | 195 | .70 | 146 | .10 | 16 | 2.12 | .04 | .15 | 6 | 45.1 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data FA

Ruby Red Resources Inc. PROJECT EDDY FILE # A403182 

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au* ppb |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 850N 9500E | 1 | 26 | 27 | 85 | <.3 | 20 | 14 | 282 | 2.77 | 3 | <8 | <2 | 6 | 6 | <.5 | <3 | <3 | 47 | .07 | .067 | 12 | 4 | .45 | 100 | .10 | <3 | 3.55 | .01 | .09 | 2 | 7.9 |
| 850N 9525E | 1 | 19 | 25 | 72 | <.3 | 17 | 13 | 741 | 2.56 | <2 | <8 | <2 | 5 | 12 | <.5 | <3 | <3 | 46 | .13 | .046 | 15 | 3 | .39 | 129 | .08 | <3 | 2.55 | .01 | .09 | 4 | 7.4 |
| 850N 9550E | 1 | 17 | 19 | 88 | <.3 | 16 | 14 | 1751 | 2.21 | <2 | <8 | <2 | 3 | 12 | <.5 | <3 | <3 | 39 | .18 | .072 | 10 | 1 | .30 | 115 | .08 | <3 | 2.64 | .01 | .08 | <2 | 2.6 |
| 850N 9575E | 1 | 19 | 24 | 96 | <.3 | 19 | 14 | 581 | 2.22 | 3 | <8 | <2 | 3 | 8 | <.5 | <3 | <3 | 40 | .11 | .072 | 9 | <1 | .34 | 92 | .08 | <3 | 2.27 | .01 | .08 | 2 | 1.4 |
| 850N 9600E | <1 | 34 | 14 | 94 | <.3 | 14 | 11 | 632 | 2.10 | 5 | <8 | <2 | 4 | 7 | <.5 | <3 | <3 | 35 | .11 | .084 | 11 | 2 | .46 | 68 | .07 | <3 | 1.59 | .01 | .09 | 2 | 2.0 |
| 850N 9625E | <1 | 18 | 18 | 96 | <.3 | 13 | 12 | 530 | 1.99 | 4 | <8 | <2 | 4 | 7 | <.5 | <3 | <3 | 34 | .11 | .084 | 10 | <1 | .35 | 66 | .07 | <3 | 1.95 | .01 | .08 | <2 | 4.4 |
| 850N 9650E | 1 | 26 | 7 | 106 | <.3 | 19 | 14 | 599 | 2.08 | 2 | <8 | <2 | 3 | 8 | <.5 | <3 | <3 | 36 | .12 | .086 | 8 | 1 | .35 | 95 | .09 | <3 | 2.35 | .02 | .08 | <2 | 275.3 |
| 850N 9675E | <1 | 15 | 13 | 108 | <.3 | 19 | 20 | 512 | 2.36 | 2 | <8 | <2 | 3 | 10 | <.5 | <3 | <3 | 37 | .11 | .117 | 6 | 3 | .23 | 78 | .12 | <3 | 3.24 | .02 | .05 | 2 | 1.2 |
| 850N 9700E | 1 | 47 | 16 | 78 | .3 | 20 | 13 | 370 | 2.37 | 3 | <8 | <2 | 3 | 7 | <.5 | <3 | <3 | 48 | .10 | .021 | 8 | 2 | .53 | 110 | .09 | <3 | 2.36 | .01 | .08 | <2 | .5 |
| 650N 8900E | 2 | 38 | 7 | 72 | <.3 | 23 | 15 | 481 | 2.29 | 5 | <8 | <2 | 3 | 7 | <.5 | <3 | <3 | 46 | .13 | .112 | 6 | 3 | .29 | 86 | .09 | <3 | 2.76 | .02 | .06 | 4 | 3.9 |
| 650N 8925E | 1 | 15 | 6 | 50 | <.3 | 21 | 13 | 165 | 1.96 | 2 | <8 | <2 | 3 | 10 | <.5 | <3 | <3 | 38 | .15 | .032 | 8 | 3 | .35 | 76 | .09 | <3 | 1.96 | .01 | .10 | <2 | 1.8 |
| 650N 8950E | <1 | 14 | 9 | 80 | <.3 | 29 | 18 | 317 | 2.37 | 7 | <8 | <2 | 2 | 10 | <.5 | <3 | <3 | 48 | .17 | .079 | 6 | 5 | .31 | 102 | .10 | <3 | 2.28 | .02 | .08 | <2 | 2.5 |
| 650N 8975E | 2 | 15 | 13 | 58 | .3 | 22 | 15 | 207 | 2.34 | 5 | <8 | <2 | 3 | 10 | <.5 | <3 | <3 | 39 | .16 | .105 | 10 | 4 | .35 | 71 | .07 | <3 | 2.10 | .01 | .07 | <2 | 4.9 |
| 650N 9000E | <1 | 14 | 11 | 37 | <.3 | 24 | 11 | 464 | 2.42 | 4 | <8 | <2 | 2 | 20 | <.5 | <3 | <3 | 67 | .40 | .023 | 8 | 23 | .44 | 108 | .05 | <3 | 1.50 | .01 | .08 | <2 | 12.5 |
| 650N 9025E | <1 | 15 | 16 | 85 | <.3 | 22 | 15 | 315 | 2.55 | 2 | <8 | <2 | 3 | 10 | <.5 | <3 | <3 | 39 | .17 | .116 | 6 | 10 | .28 | 106 | .10 | <3 | 3.13 | .02 | .07 | <2 | 1.7 |
| 650N 9050E | <1 | 10 | 13 | 46 | <.3 | 12 | 8 | 134 | 2.05 | 4 | <8 | <2 | 2 | 9 | <.5 | <3 | <3 | 41 | .13 | .127 | 6 | 4 | .16 | 60 | .08 | <3 | 2.11 | .02 | .04 | 2 | 4.6 |
| 650N 9075E | 1 | 21 | 12 | 59 | <.3 | 17 | 13 | 214 | 2.67 | 4 | <8 | <2 | 3 | 13 | <.5 | <3 | <3 | 64 | .27 | .031 | 11 | 4 | .54 | 64 | .07 | <3 | 1.60 | .01 | .08 | <2 | 1.5 |
| 650N 9100E | <1 | 22 | 11 | 49 | <.3 | 14 | 10 | 170 | 2.28 | 5 | <8 | <2 | 3 | 9 | <.5 | <3 | <3 | 52 | .21 | .019 | 12 | 5 | .50 | 69 | .06 | <3 | 1.49 | .01 | .06 | <2 | 15.7 |
| 650N 9125E | <1 | 42 | 18 | 72 | .8 | 27 | 14 | 342 | 2.94 | 6 | <8 | <2 | 2 | 39 | .5 | <3 | <3 | 94 | .82 | .040 | 18 | 21 | .54 | 97 | .06 | <3 | 2.63 | .02 | .08 | 2 | <.5 |
| RE 650N 9125E | 2 | 44 | 19 | 75 | .7 | 29 | 15 | 363 | 3.11 | 6 | <8 | <2 | 2 | 41 | .6 | 3 | <3 | 99 | .85 | .042 | 18 | 24 | .57 | 102 | .06 | <3 | 2.76 | .02 | .08 | <2 | - |
| 650N 9150E | <1 | 13 | 11 | 82 | <.3 | 11 | 7 | 241 | 1.89 | <2 | <8 | <2 | 3 | 6 | <.5 | <3 | <3 | 38 | .09 | .144 | 10 | 2 | .14 | 93 | .04 | <3 | 1.61 | .01 | .06 | <2 | 2.7 |
| 650N 9175E | <1 | 25 | 8 | 53 | <.3 | 46 | 11 | 171 | 2.70 | 3 | <8 | <2 | 3 | 19 | <.5 | <3 | <3 | 59 | .30 | .033 | 9 | 22 | .45 | 131 | .08 | <3 | 2.69 | .02 | .07 | <2 | 1.8 |
| 650N 9200E | 1 | 28 | 17 | 44 | .3 | 28 | 7 | 144 | 1.84 | <2 | <8 | <2 | <2 | 38 | <.5 | <3 | <3 | 39 | .69 | .043 | 19 | 13 | .34 | 73 | .03 | <3 | 1.37 | .01 | .10 | <2 | .5 |
| 650N 9225E | 1 | 40 | 15 | 65 | <.3 | 31 | 16 | 462 | 3.21 | 5 | <8 | <2 | 5 | 19 | <.5 | <3 | <3 | 73 | .28 | .022 | 18 | 24 | .57 | 109 | .08 | <3 | 2.59 | .01 | .12 | <2 | 1.2 |
| 650N 9250E | 1 | 20 | 13 | 67 | <.3 | 35 | 16 | 459 | 3.65 | 4 | <8 | <2 | 2 | 28 | <.5 | <3 | 3 | 104 | .54 | .033 | 11 | 46 | .90 | 67 | .08 | <3 | 2.55 | .01 | .10 | 2 | 1.1 |
| 650N 9275E | <1 | 31 | 7 | 57 | <.3 | 20 | 11 | 168 | 1.92 | 5 | <8 | <2 | 4 | 7 | <.5 | <3 | <3 | 37 | .15 | .041 | 14 | 7 | .53 | 84 | .06 | <3 | 1.59 | .01 | .07 | <2 | 7.9 |
| 650N 9300E | 1 | 24 | 11 | 85 | <.3 | 29 | 13 | 301 | 2.17 | 3 | <8 | <2 | 3 | 8 | <.5 | <3 | <3 | 37 | .12 | .091 | 9 | 19 | .44 | 98 | .07 | <3 | 2.24 | .01 | .07 | <2 | 9.3 |
| 650N 9325E | <1 | 15 | 10 | 82 | <.3 | 41 | 13 | 368 | 1.79 | 4 | <8 | <2 | 2 | 8 | <.5 | <3 | <3 | 35 | .15 | .059 | 8 | 24 | .49 | 72 | .05 | <3 | 2.09 | .01 | .07 | <2 | 1.0 |
| 650N 9350E | 1 | 23 | 11 | 33 | <.3 | 19 | 7 | 117 | 1.92 | 2 | <8 | <2 | 2 | 19 | <.5 | <3 | <3 | 55 | .29 | .027 | 12 | 18 | .40 | 48 | .06 | <3 | 1.84 | .02 | .07 | <2 | 1.7 |
| 650N 9375E | <1 | 20 | 12 | 58 | <.3 | 23 | 11 | 211 | 2.29 | 2 | <8 | <2 | 3 | 6 | <.5 | <3 | <3 | 47 | .11 | .063 | 9 | 8 | .39 | 68 | .07 | <3 | 1.95 | .01 | .09 | <2 | 1.6 |
| 650N 9400E | <1 | 21 | 8 | 49 | <.3 | 17 | 9 | 247 | 2.39 | 3 | <8 | <2 | 4 | 5 | <.5 | <3 | <3 | 48 | .11 | .041 | 11 | 10 | .45 | 71 | .07 | <3 | 1.71 | .01 | .06 | <2 | 2.3 |
| 650N 9425E | <1 | 18 | 11 | 74 | <.3 | 28 | 12 | 373 | 2.11 | 2 | <8 | <2 | 3 | 8 | <.5 | <3 | 4 | 36 | .11 | .113 | 6 | 15 | .37 | 79 | .08 | <3 | 2.57 | .02 | .06 | <2 | 2.1 |
| 650N 9450E | <1 | 14 | 10 | 57 | <.3 | 23 | 11 | 530 | 1.86 | 3 | <8 | <2 | 3 | 7 | <.5 | <3 | <3 | 35 | .12 | .071 | 7 | 14 | .42 | 73 | .08 | <3 | 1.95 | .01 | .06 | <2 | 1.5 |
| 650N 9475E | <1 | 14 | 7 | 64 | <.3 | 36 | 12 | 840 | 1.91 | 4 | <8 | <2 | 2 | 8 | <.5 | <3 | <3 | 37 | .14 | .089 | 5 | 18 | .36 | 73 | .10 | <3 | 2.52 | .02 | .06 | 2 | 2.0 |
| STANDARD DS5 | 13 | 148 | 26 | 137 | .4 | 26 | 12 | 786 | 3.13 | 19 | 12 | <2 | 3 | 47 | 5.9 | 4 | 6 | 62 | .76 | .099 | 12 | 198 | .71 | 145 | .11 | 16 | 2.11 | .04 | .16 | 6 | 44.0 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data FA

ACME ANALYTICAL

# Ruby Red Resources Inc. PROJECT EDDY FILE # A403182



ACME ANALYTICAL

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au* ppb |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 650N 9500E | <1 | 14 | 12 | 78 | <.3 | 28 | 13 | 643 | 1.81 | 2 | <8 | <2 | 3 | 8 | <.5 | <3 | <3 | 29 | .11 | .070 | 6 | 3 | .21 | 79 | .09 | <3 | 2.41 | .02 | .07 | <2 | 1.4 |
| 650N 9525E | <1 | 25 | 13 | 83 | <.3 | 12 | 10 | 875 | 1.98 | 2 | <8 | <2 | 3 | 7 | <.5 | <3 | <3 | 34 | .08 | .187 | 3 | 1 | .08 | 78 | .13 | <3 | 4.04 | .02 | .04 | <2 | .7 |
| 650N 9550E | 1 | 16 | 10 | 60 | <.3 | 21 | 13 | 376 | 1.84 | 2 | <8 | <2 | 3 | 6 | <.5 | <3 | <3 | 32 | .12 | .043 | 8 | 5 | .36 | 59 | .06 | <3 | 1.85 | .01 | .09 | <2 | .5 |
| 650N 9575E | <1 | 13 | 11 | 84 | <.3 | 25 | 11 | 655 | 1.72 | 2 | <8 | <2 | 3 | 7 | <.5 | <3 | <3 | 27 | .11 | .056 | 9 | 5 | .29 | 82 | .07 | <3 | 1.80 | .01 | .10 | <2 | .9 |
| 650N 9600E | <1 | 29 | 12 | 67 | <.3 | 24 | 14 | 725 | 2.25 | 2 | <8 | <2 | 4 | 11 | <.5 | <3 | <3 | 44 | .14 | .063 | 12 | 15 | .37 | 116 | .06 | <3 | 2.51 | .02 | .14 | <2 | 1.8 |
| 650N 9625E | <1 | 32 | 12 | 87 | <.3 | 30 | 15 | 467 | 2.97 | 2 | <8 | <2 | 4 | 12 | <.5 | <3 | <3 | 59 | .18 | .077 | 10 | 28 | .60 | 115 | .08 | <3 | 2.87 | .02 | .09 | <2 | .5 |
| 650N 9650E | <1 | 15 | 6 | 45 | <.3 | 17 | 6 | 210 | 1.47 | <2 | <8 | <2 | 3 | 10 | <.5 | <3 | <3 | 34 | .19 | .009 | 8 | 6 | .46 | 51 | .05 | <3 | 1.32 | .01 | .05 | <2 | .6 |
| 650N 9675E | <1 | 16 | 6 | 44 | <.3 | 19 | 8 | 203 | 1.51 | <2 | <8 | <2 | 2 | 8 | <.5 | <3 | <3 | 32 | .18 | .010 | 8 | 13 | .49 | 46 | .05 | <3 | 1.29 | .01 | .05 | <2 | .5 |
| 650N 9700E | <1 | 23 | 7 | 45 | <.3 | 26 | 9 | 283 | 1.92 | 2 | <8 | <2 | 2 | 16 | <.5 | <3 | <3 | 44 | .17 | .020 | 6 | 13 | .47 | 158 | .07 | <3 | 2.21 | .03 | .05 | <2 | .5 |
| 650N 9725E | <1 | 36 | 8 | 85 | <.3 | 31 | 15 | 484 | 3.10 | 5 | <8 | <2 | 5 | 7 | <.5 | <3 | <3 | 66 | .10 | .077 | 18 | 23 | .50 | 115 | .10 | <3 | 3.45 | .03 | .16 | <2 | 1.4 |
| 650N 9775E | <1 | 22 | 12 | 51 | <.3 | 22 | 11 | 366 | 2.32 | 3 | <8 | <2 | 5 | 13 | <.5 | <3 | <3 | 49 | .15 | .018 | 14 | 15 | .50 | 97 | .07 | <3 | 2.32 | .02 | .07 | <2 | .8 |
| 650N 9800E | 2 | 27 | 15 | 41 | <.3 | 28 | 13 | 225 | 3.21 | 3 | <8 | <2 | 9 | 10 | <.5 | <3 | <3 | 54 | .07 | .057 | 18 | 21 | .21 | 122 | .14 | <3 | 4.05 | .02 | .10 | <2 | 1.6 |
| 20 600W | 1 | 9 | 12 | 41 | <.3 | 8 | 4 | 71 | 1.99 | 3 | <8 | <2 | 6 | 4 | <.5 | <3 | <3 | 22 | .02 | .041 | 12 | <1 | .15 | 51 | .05 | <3 | 2.13 | .01 | .04 | <2 | 1.2 |
| RE 20 600W | 1 | 8 | 11 | 40 | <.3 | 8 | 3 | 70 | 1.94 | 4 | <8 | <2 | 6 | 4 | <.5 | <3 | <3 | 22 | .02 | .041 | 12 | <1 | .15 | 50 | .04 | <3 | 2.08 | .01 | .05 | <2 | - |
| 20 575W | <1 | 4 | 10 | 24 | <.3 | 6 | 2 | 50 | 1.47 | 3 | <8 | <2 | 3 | 2 | <.5 | <3 | <3 | 22 | .02 | .020 | 19 | <1 | .16 | 48 | .04 | <3 | .80 | .01 | .03 | <2 | .5 |
| 20 550W | 1 | 6 | 8 | 31 | <.3 | 6 | 2 | 66 | 1.95 | 3 | <8 | <2 | 3 | 2 | <.5 | <3 | <3 | 29 | .01 | .023 | 17 | <1 | .16 | 32 | .04 | <3 | 1.07 | .01 | .04 | <2 | 6.6 |
| 20 525W | 2 | 4 | 11 | 21 | <.3 | 4 | 1 | 50 | 1.76 | 3 | <8 | <2 | 3 | 3 | <.5 | <3 | <3 | 29 | .02 | .020 | 15 | 1 | .07 | 38 | .03 | <3 | 1.06 | .01 | .04 | <2 | 2.5 |
| 20 500W | <1 | 13 | 11 | 40 | <.3 | 11 | 5 | 84 | 2.00 | 4 | <8 | <2 | 6 | 4 | <.5 | <3 | <3 | 23 | .03 | .045 | 12 | <1 | .22 | 90 | .07 | <3 | 2.37 | .01 | .04 | <2 | 4.2 |
| 20 475W | 2 | 9 | 12 | 52 | <.3 | 10 | 4 | 155 | 2.08 | 3 | <8 | <2 | 4 | 5 | <.5 | <3 | <3 | 34 | .03 | .043 | 10 | 1 | .16 | 72 | .10 | <3 | 2.02 | .01 | .06 | <2 | 1.1 |
| 20 450W | 1 | 23 | 15 | 83 | <.3 | 14 | 10 | 385 | 2.75 | <2 | <8 | <2 | 3 | 7 | <.5 | <3 | <3 | 52 | .08 | .099 | 9 | 2 | .31 | 125 | .12 | <3 | 3.26 | .02 | .06 | <2 | 2.0 |
| 20 425W | 2 | 19 | 13 | 63 | <.3 | 15 | 7 | 162 | 2.70 | 5 | <8 | <2 | 5 | 6 | <.5 | <3 | <3 | 33 | .04 | .080 | 10 | 1 | .30 | 81 | .09 | <3 | 3.22 | .01 | .06 | <2 | 11.9 |
| 20 400W | 3 | 20 | 11 | 47 | <.3 | 11 | 6 | 176 | 2.12 | <2 | <8 | <2 | 4 | 8 | <.5 | <3 | <3 | 29 | .06 | .130 | 6 | 1 | .17 | 75 | .13 | <3 | 4.01 | .02 | .05 | <2 | 2.1 |
| 20 375W | 1 | 14 | 11 | 36 | <.3 | 13 | 6 | 132 | 2.16 | 2 | <8 | <2 | 4 | 7 | <.5 | <3 | <3 | 32 | .05 | .088 | 6 | <1 | .18 | 93 | .14 | <3 | 3.90 | .02 | .05 | <2 | 1.8 |
| 20 350W | 3 | 14 | 18 | 64 | .4 | 16 | 7 | 170 | 2.56 | <2 | <8 | <2 | 5 | 6 | <.5 | <3 | <3 | 34 | .05 | .112 | 7 | <1 | .19 | 98 | .15 | <3 | 3.50 | .02 | .06 | <2 | 4.8 |
| 20 325W | 2 | 14 | 14 | 41 | <.3 | 19 | 9 | 425 | 2.13 | <2 | <8 | <2 | 5 | 11 | <.5 | <3 | <3 | 29 | .10 | .080 | 6 | 1 | .18 | 106 | .13 | <3 | 3.66 | .02 | .05 | <2 | 9.4 |
| 20 300W | 1 | 16 | 14 | 48 | <.3 | 18 | 11 | 305 | 2.40 | 4 | <8 | <2 | 6 | 7 | <.5 | <3 | <3 | 29 | .05 | .067 | 8 | 1 | .19 | 107 | .12 | <3 | 3.76 | .02 | .05 | <2 | 16.4 |
| 20 275W | 2 | 24 | 18 | 58 | <.3 | 20 | 13 | 379 | 2.93 | 4 | <8 | <2 | 8 | 6 | <.5 | <3 | <3 | 30 | .04 | .083 | 16 | 4 | .35 | 96 | .08 | <3 | 2.87 | .01 | .06 | <2 | 29.2 |
| 20 250W | 3 | 17 | 22 | 48 | <.3 | 13 | 10 | 287 | 2.73 | 4 | <8 | <2 | 6 | 4 | <.5 | <3 | <3 | 34 | .03 | .044 | 16 | 1 | .21 | 98 | .06 | <3 | 2.44 | .01 | .05 | <2 | 20.9 |
| 20 225W | 2 | 15 | 14 | 68 | <.3 | 12 | 9 | 1366 | 2.97 | 4 | <8 | <2 | 6 | 6 | <.5 | <3 | <3 | 40 | .04 | .081 | 12 | 6 | .19 | 99 | .10 | <3 | 2.32 | .01 | .06 | <2 | 33.1 |
| 20 200W | 3 | 19 | 20 | 63 | .4 | 12 | 8 | 1238 | 3.38 | 4 | <8 | <2 | 4 | 5 | <.5 | <3 | <3 | 46 | .04 | .057 | 14 | 10 | .24 | 103 | .09 | <3 | 2.21 | .01 | .06 | <2 | 17.2 |
| 20 175W | 1 | 24 | 18 | 67 | <.3 | 17 | 10 | 440 | 2.97 | 5 | <8 | <2 | 7 | 4 | <.5 | <3 | <3 | 33 | .03 | .092 | 13 | 4 | .30 | 96 | .10 | <3 | 3.52 | .01 | .06 | <2 | 18.6 |
| 20 150W | 2 | 23 | 13 | 57 | .3 | 15 | 9 | 225 | 2.62 | 2 | <8 | <2 | 6 | 6 | <.5 | <3 | <3 | 37 | .04 | .094 | 8 | 5 | .25 | 91 | .14 | <3 | 4.10 | .01 | .05 | <2 | 5.9 |
| 20 125W | 1 | 16 | 10 | 54 | .6 | 9 | 5 | 251 | 1.78 | <2 | <8 | <2 | 4 | 7 | .5 | <3 | <3 | 28 | .05 | .140 | 5 | 1 | .11 | 61 | .16 | <3 | 4.60 | .02 | .04 | <2 | 2.0 |
| 20 100W | 2 | 18 | 11 | 53 | <.3 | 8 | 4 | 174 | 2.28 | 2 | <8 | <2 | 2 | 6 | <.5 | <3 | <3 | 36 | .04 | .110 | 5 | 1 | .12 | 44 | .14 | <3 | 2.98 | .02 | .04 | <2 | 2.1 |
| STANDARD DS5 | 12 | 141 | 25 | 129 | .3 | 25 | 12 | 746 | 3.04 | 20 | <8 | <2 | 3 | 46 | 5.6 | 3 | 6 | 58 | .74 | .092 | 11 | 190 | .68 | 139 | .10 | 16 | 2.00 | .04 | .15 | 6 | 45.0 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data ✓ FA ____

ACME ANALYTICAL

**Ruby Red Resources Inc.** PROJECT EDDY FILE # A403182



ACME ANALYTICAL

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au* ppb |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 20 75W | 2 | 24 | 6 | 50 | <.3 | 11 | 6 | 146 | 2.01 | 2 | <8 | <2 | 5 | 7 | <.5 | <3 | <3 | 28 | .04 | .140 | 6 | <1 | .15 | 60 | .14 | <3 | 4.12 | .02 | .05 | <2 | 3.3 |
| 20 50W | 1 | 18 | 8 | 38 | <.3 | 10 | 6 | 245 | 1.89 | <2 | <8 | <2 | 3 | 10 | <.5 | <3 | <3 | 27 | .08 | .080 | 6 | <1 | .16 | 52 | .10 | <3 | 2.95 | .02 | .03 | <2 | 3.2 |
| 20 25W | 1 | 20 | 13 | 38 | <.3 | 12 | 5 | 106 | 2.70 | 4 | <8 | <2 | 6 | 4 | <.5 | <3 | <3 | 28 | .02 | .052 | 16 | 2 | .30 | 45 | .05 | <3 | 1.74 | .01 | .05 | <2 | 7.2 |
| 20 00W | 2 | 13 | 9 | 39 | <.3 | 11 | 5 | 126 | 2.24 | 4 | <8 | <2 | 5 | 5 | <.5 | <3 | <3 | 24 | .03 | .038 | 15 | 1 | .25 | 49 | .04 | <3 | 1.69 | .01 | .05 | <2 | 2.4 |
| 1970 00E | 3 | 8 | 13 | 30 | <.3 | 13 | 11 | 235 | 1.51 | 3 | <8 | <2 | 4 | 12 | <.5 | <3 | <3 | 16 | .09 | .011 | 17 | <1 | .33 | 51 | .03 | <3 | 1.29 | .01 | .03 | <2 | .8 |
| 1970 25E | 1 | 10 | 8 | 45 | <.3 | 12 | 5 | 76 | 2.09 | <2 | <8 | <2 | 6 | 4 | <.5 | <3 | <3 | 23 | .03 | .080 | 10 | <1 | .13 | 68 | .05 | 3 | 2.54 | .01 | .04 | <2 | 1.7 |
| 1970 50E | 2 | 8 | 5 | 28 | <.3 | 9 | 5 | 55 | 1.82 | <2 | <8 | <2 | 5 | 4 | <.5 | <3 | <3 | 19 | .03 | .033 | 13 | <1 | .18 | 51 | .05 | <3 | 2.10 | .01 | .03 | <2 | 6.9 |
| 1970 75E | <1 | 10 | <3 | 35 | <.3 | 10 | 5 | 98 | 1.88 | <2 | <8 | <2 | 6 | 4 | <.5 | <3 | <3 | 21 | .03 | .080 | 8 | <1 | .17 | 60 | .07 | <3 | 2.73 | .01 | .03 | <2 | 1.9 |
| 1970 100E | 1 | 10 | 10 | 46 | <.3 | 11 | 6 | 161 | 2.02 | <2 | <8 | <2 | 5 | 5 | <.5 | <3 | <3 | 25 | .04 | .074 | 8 | <1 | .17 | 94 | .08 | <3 | 2.88 | .01 | .04 | <2 | 3.9 |
| 1970 125E | 3 | 7 | 6 | 40 | <.3 | 10 | 4 | 98 | 2.09 | 3 | <8 | <2 | 5 | 4 | <.5 | <3 | <3 | 23 | .02 | .027 | 17 | <1 | .26 | 61 | .04 | <3 | 1.18 | .01 | .04 | <2 | 7.2 |
| 1970 150E | 1 | 13 | 9 | 54 | <.3 | 12 | 6 | 131 | 2.38 | 4 | <8 | <2 | 6 | 6 | <.5 | <3 | <3 | 29 | .04 | .079 | 9 | 3 | .22 | 86 | .09 | <3 | 2.89 | .01 | .05 | <2 | 3.5 |
| 1970 175E | 2 | 13 | 11 | 53 | <.3 | 9 | 5 | 241 | 1.91 | <2 | <8 | <2 | 4 | 7 | <.5 | <3 | <3 | 27 | .06 | .095 | 5 | <1 | .12 | 92 | .14 | <3 | 3.37 | .02 | .04 | <2 | 1.4 |
| 1970 200E | 2 | 50 | 11 | 42 | <.3 | 26 | 10 | 239 | 2.83 | 8 | <8 | <2 | 6 | 12 | <.5 | <3 | <3 | 34 | .12 | .039 | 20 | 4 | .43 | 109 | .05 | <3 | 2.26 | .01 | .04 | <2 | 33.4 |
| 1970 225E | 2 | 12 | 12 | 64 | <.3 | 12 | 7 | 298 | 2.35 | 2 | <8 | <2 | 4 | 6 | <.5 | <3 | <3 | 33 | .06 | .062 | 7 | 1 | .18 | 105 | .13 | <3 | 2.85 | .01 | .05 | <2 | 2.6 |
| 1970 250E | 2 | 14 | 23 | 64 | <.3 | 13 | 8 | 1090 | 3.17 | 3 | <8 | <2 | 5 | 5 | <.5 | <3 | <3 | 42 | .04 | .046 | 14 | 6 | .23 | 129 | .09 | <3 | 1.74 | .01 | .06 | <2 | 15.1 |
| 1970 275E | 2 | 13 | 13 | 45 | <.3 | 14 | 8 | 163 | 2.45 | 4 | <8 | <2 | 6 | 5 | <.5 | <3 | <3 | 27 | .04 | .044 | 16 | 2 | .28 | 91 | .07 | <3 | 1.83 | .01 | .05 | <2 | 12.0 |
| 1970 300E | 2 | 21 | 11 | 40 | <.3 | 16 | 9 | 108 | 2.74 | 6 | <8 | <2 | 8 | 4 | <.5 | <3 | <3 | 19 | .02 | .034 | 23 | 2 | .34 | 92 | .03 | <3 | 1.65 | <.01 | .04 | <2 | 65.2 |
| RE 1970 300E | 2 | 20 | 12 | 38 | <.3 | 16 | 8 | 104 | 2.67 | 5 | <8 | <2 | 8 | 4 | <.5 | <3 | <3 | 19 | .02 | .033 | 20 | 2 | .33 | 89 | .03 | <3 | 1.58 | <.01 | .03 | <2 | 88.0 |
| 1970 325E | 2 | 13 | 9 | 60 | <.3 | 20 | 10 | 153 | 2.82 | 3 | <8 | <2 | 7 | 5 | <.5 | <3 | <3 | 28 | .04 | .082 | 10 | 3 | .26 | 109 | .09 | <3 | 3.02 | .01 | .06 | <2 | 54.9 |
| 1970 350E | 1 | 13 | 9 | 63 | <.3 | 13 | 7 | 435 | 3.18 | 2 | <8 | <2 | 4 | 6 | <.5 | <3 | <3 | 42 | .03 | .076 | 9 | 3 | .21 | 94 | .11 | <3 | 2.58 | .01 | .05 | <2 | 4.9 |
| 1970 375E | 2 | 14 | 12 | 58 | <.3 | 16 | 9 | 165 | 2.56 | 2 | <8 | <2 | 6 | 6 | <.5 | <3 | <3 | 31 | .05 | .047 | 12 | 1 | .25 | 104 | .09 | <3 | 2.60 | .01 | .05 | <2 | 17.1 |
| 1970 400E | 2 | 12 | 16 | 84 | <.3 | 16 | 10 | 570 | 2.63 | 2 | <8 | <2 | 3 | 6 | <.5 | <3 | <3 | 36 | .04 | .050 | 9 | 2 | .23 | 128 | .11 | <3 | 2.52 | .01 | .05 | 2 | 3.3 |
| 1970 425E | 2 | 31 | 122 | 66 | <.3 | 21 | 16 | 646 | 4.06 | 7 | <8 | <2 | 6 | 5 | <.5 | <3 | <3 | 27 | .04 | .069 | 16 | 5 | .25 | 77 | .06 | <3 | 1.91 | .01 | .04 | <2 | 149.1 |
| 1970 450E | 2 | 12 | 27 | 66 | <.3 | 13 | 8 | 468 | 2.34 | <2 | <8 | <2 | 5 | 10 | <.5 | <3 | <3 | 31 | .10 | .076 | 5 | <1 | .16 | 119 | .14 | <3 | 3.94 | .02 | .05 | <2 | 5.9 |
| 1970 475E | 3 | 17 | 15 | 82 | .5 | 14 | 8 | 657 | 2.84 | <2 | <8 | <2 | 6 | 6 | <.5 | <3 | <3 | 35 | .05 | .096 | 8 | 2 | .19 | 83 | .11 | <3 | 3.57 | .01 | .06 | <2 | 29.5 |
| 1970 500E | 2 | 24 | 68 | 92 | .4 | 16 | 11 | 568 | 3.32 | 6 | <8 | <2 | 8 | 4 | <.5 | <3 | <3 | 31 | .02 | .095 | 11 | 6 | .25 | 86 | .08 | <3 | 3.41 | .01 | .05 | <2 | 19.8 |
| 1970 525E | 1 | 23 | 16 | 55 | <.3 | 15 | 10 | 397 | 2.49 | 3 | <8 | <2 | 7 | 4 | <.5 | <3 | <3 | 24 | .03 | .090 | 10 | 1 | .21 | 71 | .08 | <3 | 3.40 | .01 | .04 | <2 | 108.4 |
| 1970 550E | 3 | 26 | 16 | 53 | <.3 | 15 | 8 | 235 | 2.61 | 4 | <8 | <2 | 7 | 5 | <.5 | <3 | <3 | 25 | .04 | .093 | 9 | <1 | .21 | 71 | .09 | <3 | 3.63 | .01 | .04 | <2 | 13.8 |
| 1970 575E | 1 | 23 | 6 | 52 | <.3 | 19 | 12 | 135 | 2.55 | 3 | <8 | <2 | 7 | 5 | <.5 | <3 | <3 | 27 | .04 | .055 | 11 | <1 | .22 | 107 | .10 | <3 | 3.44 | .01 | .04 | <2 | 63.4 |
| 1970 600E | 1 | 23 | 13 | 74 | <.3 | 18 | 11 | 235 | 2.69 | 4 | <8 | <2 | 7 | 5 | <.5 | <3 | <3 | 26 | .04 | .072 | 15 | 3 | .30 | 102 | .06 | <3 | 2.66 | .01 | .05 | <2 | 22.0 |
| 1970 625E | 1 | 16 | 10 | 49 | <.3 | 15 | 11 | 206 | 2.74 | 4 | <8 | <2 | 6 | 6 | <.5 | <3 | <3 | 26 | .05 | .049 | 16 | 3 | .23 | 75 | .06 | <3 | 2.36 | .01 | .05 | 2 | 40.9 |
| 1970 650E | 1 | 26 | 6 | 45 | <.3 | 16 | 12 | 227 | 2.70 | 2 | <8 | <2 | 5 | 6 | <.5 | <3 | <3 | 25 | .05 | .051 | 11 | 2 | .23 | 70 | .07 | <3 | 2.65 | .01 | .04 | <2 | 34.6 |
| 1970 675E | 3 | 20 | 9 | 47 | <.3 | 17 | 11 | 237 | 2.81 | 2 | <8 | <2 | 6 | 8 | <.5 | <3 | <3 | 30 | .06 | .096 | 8 | 3 | .21 | 96 | .10 | <3 | 3.70 | .01 | .05 | 2 | 5.6 |
| 1970 700E | 1 | 17 | 6 | 50 | <.3 | 14 | 9 | 462 | 2.24 | 3 | <8 | <2 | 5 | 6 | <.5 | <3 | <3 | 28 | .04 | .089 | 8 | 2 | .20 | 58 | .11 | <3 | 3.77 | .01 | .05 | <2 | 1.8 |
| STANDARD DS5 | 13 | 144 | 23 | 133 | <.3 | 25 | 12 | 758 | 3.02 | 18 | <8 | <2 | 3 | 47 | 5.6 | 4 | 6 | 58 | .73 | .092 | 11 | 189 | .68 | 141 | .09 | 16 | 2.00 | .03 | .14 | 6 | 45.2 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data FA

ACME ANALYTICAL



ACME ANALYTICAL

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au* ppb |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1970 725E | 2 | 16 | 12 | 49 | <.3 | 13 | 6 | 148 | 3.02 | 4 | <8 | <2 | 6 | 5 | <.5 | <3 | <3 | 36 | .03 | .049 | 17 | 5 | .32 | 54 | .05 | 3 | 2.07 | .01 | .05 | <2 | 30.5 |
| 1970 750E | 3 | 25 | 13 | 45 | <.3 | 11 | 6 | 183 | 2.29 | 3 | <8 | <2 | 6 | 6 | <.5 | <3 | <3 | 32 | .03 | .124 | 6 | <1 | .14 | 59 | .14 | <3 | 5.12 | .02 | .04 | <2 | 1.0 |
| 1970 775E | 1 | 18 | 10 | 42 | <.3 | 14 | 7 | 204 | 2.26 | 5 | <8 | <2 | 7 | 4 | <.5 | <3 | <3 | 27 | .03 | .078 | 11 | 1 | .31 | 60 | .08 | 3 | 2.86 | .01 | .04 | <2 | 2.5 |
| 1970 800E | 1 | 9 | 8 | 40 | <.3 | 10 | 4 | 130 | 2.54 | 6 | <8 | <2 | 4 | 4 | <.5 | <3 | <3 | 33 | .02 | .036 | 19 | 1 | .30 | 40 | .05 | <3 | 1.46 | .01 | .04 | <2 | .8 |
| STANDARD DS5 | 13 | 143 | 25 | 132 | <.3 | 25 | 12 | 751 | 2.99 | 18 | 9 | <2 | 3 | 46 | 5.4 | 3 | 6 | 60 | .74 | .092 | 12 | 189 | .69 | 138 | .10 | 17 | 1.98 | .04 | .15 | 6 | 45.5 |

Sample type: SOIL SS80 60C.



Data FA

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

# GEOCHEMICAL ANALYSIS CERTIFICATE

Ruby Red Resources Inc. PROJECT EDDY File # A403684 Page 1

207 - 239 - 12th Ave S.W., Calgary AB T2R 1H6

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| G-1 | 2.3 | 4.0 | 3.5 | 48 | <.1 | 4.6 | 4.1 | 612 | 2.17 | .6 | 2.7 | .9 | 4.9 | 95 | <.1 | <.1 | .2 | 39 | .76 | .088 | 12 | 22.5 | .59 | 254 | .147 | <1 | 1.00 | .148 | .55 | 4.7 | <.01 | 2.9 | .3 | <.05 | 6 | <.5 | 15.0 |
| 25 500E | .4 | 20.2 | 9.8 | 60 | <.1 | 10.0 | 5.2 | 150 | 2.42 | 4.2 | 1.8 | 4.9 | 4.5 | 2 | <.1 | .1 | .2 | 28 | .02 | .038 | 8 | 17.2 | .30 | 67 | .080 | <1 | 1.47 | .003 | .21 | .1 | .01 | 2.2 | .3 | <.05 | 5 | <.5 | 15.0 |
| 25 525E | .7 | 26.7 | 42.4 | 80 | .2 | 8.3 | 8.5 | 592 | 2.64 | 4.5 | 1.0 | 6.4 | 4.2 | 3 | .2 | .4 | .2 | 26 | .05 | .169 | 7 | 13.5 | .22 | 56 | .102 | <1 | 2.93 | .013 | .08 | .2 | .08 | 2.2 | .1 | .06 | 10 | .5 | 7.5 |
| 25 550E | .8 | 22.9 | 8.3 | 48 | .3 | 6.9 | 4.4 | 145 | 2.10 | 3.8 | 1.2 | 2.4 | 3.4 | 5 | .1 | .1 | .2 | 32 | .06 | .167 | 4 | 10.8 | .13 | 44 | .116 | <1 | 5.89 | .018 | .04 | .2 | .10 | 4.0 | .1 | <.05 | 10 | .5 | 15.0 |
| 25 575E | .8 | 52.5 | 15.1 | 60 | .3 | 8.2 | 6.3 | 164 | 2.57 | 5.9 | .7 | 1.4 | 3.0 | 4 | .1 | .2 | .2 | 47 | .06 | .113 | 4 | 27.4 | .19 | 48 | .108 | <1 | 4.37 | .011 | .03 | .2 | .09 | 3.5 | .1 | <.05 | 11 | .5 | 15.0 |
| 25 600E | .4 | 112.6 | 11.9 | 72 | .6 | 16.4 | 16.2 | 255 | 3.81 | 15.6 | 1.1 | 16.5 | 2.2 | 6 | .1 | .2 | .1 | 103 | .15 | .051 | 7 | 21.0 | .62 | 61 | .104 | <1 | 2.44 | .012 | .09 | .1 | .04 | 6.6 | .2 | <.05 | 10 | <.5 | 15.0 |
| 25 625E | .6 | 60.1 | 10.5 | 73 | .5 | 10.6 | 11.8 | 173 | 2.89 | 7.2 | .6 | 6.5 | 2.0 | 8 | .2 | .2 | .2 | 69 | .14 | .047 | 9 | 13.6 | .31 | 67 | .082 | <1 | 1.90 | .011 | .07 | .1 | .03 | 3.7 | .1 | <.05 | 8 | <.5 | 15.0 |
| 25 650E | .4 | 142.4 | 11.3 | 73 | .2 | 17.1 | 19.8 | 241 | 5.23 | 16.7 | 1.1 | 8.2 | 2.8 | 10 | .2 | .3 | .1 | 135 | .17 | .067 | 7 | 15.7 | .76 | 133 | .089 | <1 | 2.47 | .006 | .04 | .1 | .02 | 9.2 | .1 | <.05 | 9 | <.5 | 15.0 |
| 25 675E | .5 | 58.7 | 9.0 | 78 | .3 | 13.4 | 15.3 | 620 | 3.85 | 4.3 | .8 | 4.5 | 3.0 | 7 | .3 | .1 | .2 | 90 | .10 | .043 | 11 | 21.4 | .48 | 116 | .097 | <1 | 2.69 | .011 | .05 | <.1 | .08 | 6.4 | .1 | <.05 | 10 | <.5 | 15.0 |
| 25 700E | .3 | 30.3 | 7.5 | 55 | .1 | 17.7 | 13.2 | 166 | 2.96 | 2.3 | .5 | 33.5 | 3.8 | 4 | .1 | .1 | .1 | 59 | .08 | .028 | 11 | 66.1 | .64 | 54 | .070 | <1 | 1.52 | .004 | .05 | <.1 | .01 | 4.8 | .1 | <.05 | 5 | <.5 | 15.0 |
| 25 725E | .3 | 25.4 | 17.5 | 53 | .1 | 9.7 | 10.2 | 737 | 2.06 | 2.6 | .5 | 4.0 | 2.7 | 9 | .1 | .2 | .3 | 45 | .12 | .026 | 16 | 28.4 | .35 | 93 | .055 | <1 | 1.28 | .009 | .05 | .1 | .03 | 2.9 | .1 | <.05 | 8 | <.5 | 15.0 |
| 25 750E | 1.0 | 92.5 | 32.0 | 67 | .5 | 17.9 | 21.9 | 3139 | 3.26 | 3.1 | 1.6 | 3.1 | 3.7 | 18 | .5 | .2 | .5 | 74 | .25 | .046 | 34 | 40.9 | .37 | 129 | .097 | <1 | 2.86 | .013 | .07 | .1 | .05 | 7.2 | .3 | <.05 | 13 | .6 | 15.0 |
| 25 775E | .2 | 33.3 | 7.3 | 35 | .1 | 6.1 | 3.6 | 83 | 1.68 | 1.6 | .2 | 4.6 | 1.7 | 5 | .1 | .1 | .2 | 75 | .13 | .020 | 7 | 23.1 | .17 | 39 | .071 | <1 | .79 | .006 | .03 | <.1 | .01 | 2.5 | .1 | <.05 | 7 | <.5 | 15.0 |
| 25 800E | .4 | 32.9 | 14.0 | 85 | .2 | 13.6 | 13.1 | 193 | 2.66 | 3.2 | .6 | 15.6 | 3.9 | 6 | .1 | .1 | .2 | 52 | .10 | .055 | 10 | 31.4 | .33 | 80 | .061 | 1 | 2.77 | .009 | .04 | .1 | .05 | 3.2 | .1 | <.05 | 8 | <.5 | 15.0 |
| 25 825E | .4 | 21.9 | 10.7 | 72 | .2 | 9.9 | 5.9 | 156 | 2.65 | 2.9 | .7 | 1.5 | 4.5 | 7 | .1 | .2 | .2 | 36 | .07 | .031 | 17 | 16.6 | .32 | 62 | .078 | <1 | 1.34 | .006 | .07 | .1 | .03 | 2.1 | .1 | <.05 | 7 | <.5 | 15.0 |
| 25 850E | .6 | 20.7 | 17.3 | 51 | .3 | 9.7 | 9.5 | 201 | 2.78 | 4.1 | .7 | 1.9 | 4.6 | 9 | .1 | .2 | .3 | 45 | .09 | .041 | 15 | 17.4 | .28 | 86 | .104 | <1 | 1.38 | .015 | .06 | .1 | .05 | 2.5 | .1 | <.05 | 10 | <.5 | 7.5 |
| 25 875E | .3 | 17.8 | 9.0 | 46 | .1 | 7.9 | 4.7 | 123 | 1.75 | 2.5 | .7 | 2.3 | 4.3 | 3 | .1 | .1 | .1 | 34 | .04 | .053 | 15 | 15.4 | .23 | 65 | .073 | <1 | 1.08 | .004 | .10 | <.1 | .01 | 2.0 | .2 | <.05 | 5 | <.5 | 15.0 |
| 25 900E | .3 | 21.1 | 6.9 | 53 | <.1 | 11.3 | 9.0 | 185 | 2.10 | 2.6 | .5 | 1.7 | 4.1 | 4 | .1 | .1 | .1 | 39 | .07 | .020 | 14 | 17.8 | .34 | 86 | .072 | <1 | 1.38 | .004 | .13 | <.1 | .02 | 2.2 | .1 | <.05 | 4 | <.5 | 15.0 |
| 25 925E | .4 | 27.8 | 13.3 | 37 | .2 | 9.2 | 6.7 | 177 | 2.28 | 2.0 | 1.1 | 1.7 | 5.8 | 7 | .1 | .1 | .2 | 45 | .09 | .025 | 23 | 21.0 | .32 | 69 | .082 | <1 | 1.74 | .010 | .07 | <.1 | .02 | 3.7 | .1 | <.05 | 7 | <.5 | 15.0 |
| 25 950E | .6 | 32.8 | 13.8 | 58 | .2 | 11.9 | 11.2 | 332 | 2.89 | 4.0 | .7 | 1.8 | 3.7 | 9 | .1 | .2 | .3 | 55 | .10 | .049 | 14 | 18.6 | .25 | 70 | .136 | <1 | 2.60 | .017 | .05 | .1 | .05 | 4.6 | .1 | <.05 | 11 | <.5 | 15.0 |
| 25 975E | .5 | 78.7 | 17.3 | 69 | .4 | 27.1 | 14.1 | 449 | 4.05 | 3.1 | 1.0 | 1.1 | 4.6 | 20 | .2 | .2 | .3 | 97 | .19 | .039 | 19 | 66.5 | .61 | 134 | .125 | <1 | 2.93 | .012 | .07 | <.1 | .03 | 10.4 | .1 | .07 | 12 | .6 | 7.5 |
| RE 25 975E | .4 | 79.2 | 15.7 | 71 | .4 | 25.1 | 13.6 | 489 | 3.95 | 2.6 | 1.1 | .7 | 4.4 | 18 | .2 | .2 | .3 | 105 | .18 | .038 | 16 | 67.6 | .69 | 132 | .114 | <1 | 2.81 | .013 | .06 | <.1 | .03 | 11.6 | .1 | .06 | 12 | .5 | 7.5 |
| 25 1000E | .8 | 60.4 | 27.4 | 53 | .7 | 13.7 | 38.8 | 724 | 2.66 | 5.4 | 1.0 | .5 | 2.1 | 18 | .3 | .2 | .3 | 73 | .20 | .034 | 15 | 46.6 | .40 | 65 | .112 | 1 | 2.12 | .015 | .05 | .1 | .05 | 4.8 | .1 | <.05 | 10 | .6 | 15.0 |
| 26 500E | .6 | 21.6 | 16.0 | 54 | .1 | 13.7 | 8.8 | 163 | 2.63 | 4.7 | .8 | 16.0 | 4.7 | 6 | .1 | .2 | .3 | 47 | .07 | .030 | 19 | 18.0 | .47 | 39 | .059 | <1 | 1.20 | .004 | .06 | .1 | .03 | 2.6 | .1 | <.05 | 5 | <.5 | 15.0 |
| 26 525E | 1.0 | 36.5 | 36.8 | 91 | .4 | 23.7 | 22.5 | 2118 | 3.30 | 4.7 | 1.6 | 26.1 | 2.8 | 19 | .6 | .2 | .6 | 62 | .14 | .059 | 21 | 23.8 | .48 | 113 | .103 | 1 | 1.90 | .013 | .10 | .1 | .04 | 2.9 | .2 | <.05 | 11 | <.5 | 7.5 |
| 26 550E | .9 | 55.5 | 16.5 | 43 | .5 | 9.6 | 6.6 | 150 | 3.10 | 8.4 | 1.4 | 1.5 | 3.0 | 12 | .3 | .1 | .3 | 60 | .13 | .033 | 14 | 20.9 | .28 | 56 | .176 | <1 | 1.84 | .016 | .04 | .2 | .11 | 3.9 | .1 | .07 | 15 | .7 | 15.0 |
| 26 575E | 1.1 | 32.9 | 22.1 | 86 | .6 | 7.8 | 6.1 | 343 | 4.14 | 6.0 | .5 | .8 | 2.8 | 13 | .3 | .3 | .4 | 75 | .17 | .049 | 8 | 20.3 | .20 | 107 | .152 | 1 | 1.57 | .012 | .06 | .2 | .08 | 2.0 | .1 | <.05 | 17 | <.5 | 7.5 |
| 26 600E | .4 | 30.3 | 28.7 | 43 | .4 | 10.7 | 7.0 | 477 | 1.14 | 2.6 | 2.0 | 1.7 | .2 | 21 | .6 | .1 | .4 | 21 | .15 | .056 | 30 | 11.0 | .20 | 93 | .040 | 2 | .94 | .009 | .07 | .1 | .04 | .9 | .1 | .14 | 6 | <.5 | 7.5 |
| 26 625E | .6 | 26.6 | 31.8 | 72 | .2 | 14.5 | 14.8 | 659 | 2.86 | 5.8 | 1.0 | 19.8 | 3.4 | 16 | .2 | .2 | .5 | 56 | .14 | .057 | 17 | 21.6 | .46 | 106 | .091 | 1 | 1.81 | .011 | .08 | .1 | .02 | 2.4 | .1 | .11 | 11 | <.5 | 15.0 |
| 26 650E | .4 | 12.3 | 11.0 | 60 | .2 | 7.7 | 7.1 | 573 | 1.96 | 5.2 | .4 | 5.2 | 3.3 | 4 | .2 | .2 | .3 | 49 | .05 | .085 | 16 | 12.9 | .33 | 53 | .075 | <1 | .98 | .007 | .05 | .1 | .02 | 1.4 | .1 | <.05 | 8 | <.5 | 15.0 |
| 26 675E | .6 | 136.0 | 28.3 | 56 | .8 | 18.3 | 15.1 | 388 | 3.34 | 8.5 | 2.7 | 5.2 | 5.0 | 12 | .2 | .2 | .4 | 91 | .11 | .053 | 45 | 35.8 | .34 | 70 | .122 | 1 | 4.02 | .015 | .06 | .1 | .09 | 12.7 | .2 | .07 | 13 | 1.2 | 15.0 |
| 26 700E | .7 | 68.7 | 27.5 | 51 | .6 | 13.5 | 24.6 | 1185 | 2.61 | 4.8 | 1.6 | 2.9 | 3.3 | 13 | .3 | .1 | .4 | 73 | .16 | .036 | 25 | 42.2 | .27 | 86 | .108 | <1 | 2.13 | .016 | .05 | .1 | .05 | 7.0 | .1 | <.05 | 12 | .8 | 15.0 |
| 26 725E | .2 | 24.5 | 11.2 | 21 | .2 | 4.8 | 1.8 | 57 | 1.03 | 1.4 | .5 | 5.0 | 1.3 | 8 | .2 | .1 | .2 | 28 | .08 | .017 | 13 | 14.7 | .10 | 55 | .089 | <1 | .92 | .007 | .03 | <.1 | .03 | 3.0 | .1 | <.05 | 7 | <.5 | 15.0 |
| 26 750E | .4 | 20.3 | 15.0 | 45 | .3 | 10.4 | 5.9 | 119 | 2.18 | 3.4 | .5 | 4.9 | 4.3 | 4 | .1 | .1 | .2 | 51 | .06 | .023 | 12 | 24.7 | .38 | 51 | .053 | 2 | 1.84 | .008 | .04 | .1 | .05 | 2.9 | .1 | <.05 | 6 | <.5 | 15.0 |
| 26 775E | .7 | 24.1 | 16.6 | 80 | .3 | 10.8 | 7.0 | 375 | 2.35 | 4.7 | .9 | 3.6 | 5.1 | 5 | .2 | .2 | .2 | 47 | .05 | .099 | 8 | 17.6 | .28 | 77 | .078 | 1 | 3.85 | .011 | .04 | .1 | .09 | 2.8 | .1 | .09 | 9 | <.5 | 15.0 |
| STANDARD DS5 | 12.1 | 141.4 | 24.7 | 136 | .3 | 23.6 | 11.4 | 791 | 2.95 | 18.2 | 6.3 | 42.6 | 2.7 | 46 | 5.9 | 3.7 | 6.4 | 62 | .73 | .094 | 12 | 187.8 | .68 | 143 | .096 | 18 | 2.00 | .034 | .15 | 4.8 | .18 | 3.5 | 1.2 | <.05 | [illegible] | [illegible] | 15.0 |

GROUP 1DX - 15.00 GM SAMPLE LEACHED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 300 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA ____ DATE RECEIVED: JUL 20 2004 DATE REPORT MAILED: Aug 3/2004

BRITISH COLUMBIA CERTIFIED ASSAYER — Jacky Wang

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| G-1 | 2.2 | 3.5 | 3.5 | 50 | <.1 | 4.8 | 3.9 | 553 | 1.91 | .8 | 2.1 | .6 | 4.9 | 89 | <.1 | <.1 | .1 | 38 | .71 | .088 | 11 | 20.0 | .53 | 234 | .125 | 2 | 1.03 | .127 | .48 | 3.8 | <.01 | 2.1 | .3 | <.05 | 6 | <.5 | 15.0 |
| 26 800E | .6 | 16.0 | 12.7 | 34 | .4 | 5.3 | 3.7 | 269 | 3.08 | 3.7 | .8 | 3.0 | 3.5 | 4 | .1 | .2 | .2 | 50 | .04 | .081 | 4 | 13.3 | .07 | 44 | .107 | 3 | 4.53 | .014 | .02 | .1 | .13 | 2.4 | .1 | <.05 | 11 | <.5 | 15.0 |
| 26 825E | .7 | 38.1 | 22.6 | 87 | .4 | 17.3 | 21.9 | 2153 | 2.69 | 2.9 | 1.2 | 2.2 | 3.1 | 16 | .3 | .2 | .4 | 52 | .15 | .041 | 34 | 23.4 | .38 | 121 | .077 | 3 | 1.86 | .011 | .06 | .1 | .04 | 3.2 | .1 | <.05 | 10 | <.5 | 7.5 |
| 26 850E | .5 | 15.2 | 13.0 | 51 | .2 | 5.7 | 4.4 | 623 | 1.58 | 2.2 | .3 | 2.0 | 2.2 | 6 | .1 | .2 | .3 | 37 | .06 | .073 | 8 | 9.2 | .13 | 70 | .088 | 1 | 1.12 | .011 | .04 | .1 | .04 | 1.3 | .1 | <.05 | 9 | <.5 | 15.0 |
| 26 875E | .3 | 23.8 | 21.1 | 55 | .3 | 12.3 | 7.1 | 313 | 2.15 | 2.2 | .9 | <.5 | 3.1 | 9 | .1 | .1 | .4 | 36 | .06 | .018 | 15 | 14.6 | .11 | 69 | .086 | 2 | 1.23 | .008 | .04 | .1 | .02 | 2.5 | .1 | <.05 | 8 | <.5 | 15.0 |
| 26 900E | .9 | 62.5 | 30.6 | 107 | .3 | 28.0 | 20.8 | 236 | 5.48 | 4.4 | 1.1 | 10.7 | 6.1 | 18 | .2 | .1 | .5 | 112 | .16 | .038 | 19 | 32.7 | .72 | 184 | .143 | 2 | 4.09 | .016 | .07 | .1 | .05 | 5.3 | .1 | .09 | 20 | <.5 | 7.5 |
| 26 925E | .7 | 27.4 | 16.6 | 47 | .2 | 9.6 | 6.7 | 113 | 3.23 | 3.3 | .8 | 3.1 | 3.8 | 6 | .1 | .1 | .3 | 63 | .07 | .027 | 7 | 18.8 | .17 | 53 | .124 | 1 | 2.59 | .012 | .03 | .1 | .08 | 4.4 | .1 | <.05 | 13 | <.5 | 15.0 |
| 26 950E | .4 | 125.1 | 17.2 | 78 | .3 | 21.7 | 14.8 | 695 | 4.16 | 2.4 | 2.0 | 2.8 | 2.7 | 23 | .2 | .2 | .4 | 80 | .24 | .043 | 46 | 46.2 | .48 | 115 | .097 | 1 | 3.27 | .014 | .08 | <.1 | .06 | 10.1 | .1 | <.05 | 14 | .5 | 15.0 |
| 26 975E | .4 | 29.8 | 11.5 | 70 | .3 | 17.6 | 8.8 | 138 | 3.11 | 2.6 | .5 | 2.0 | 2.6 | 8 | .1 | .1 | .2 | 67 | .13 | .021 | 6 | 48.0 | .34 | 89 | .089 | 2 | 2.72 | .013 | .03 | .1 | .06 | 4.7 | .1 | <.05 | 10 | <.5 | 15.0 |
| 26 1000E | .5 | 77.7 | 14.5 | 50 | .2 | 21.1 | 17.8 | 963 | 3.32 | 2.9 | .8 | 2.8 | 1.6 | 17 | .2 | .2 | .3 | 90 | .21 | .031 | 12 | 57.7 | .58 | 92 | .093 | 2 | 2.47 | .012 | .06 | <.1 | .05 | 5.4 | .1 | <.05 | 9 | <.5 | 15.0 |
| 27 500E | .5 | 22.9 | 20.4 | 81 | .1 | 21.6 | 11.1 | 289 | 2.01 | 1.3 | 1.1 | 121.1 | 1.4 | 9 | .3 | .1 | .4 | 45 | .09 | .024 | 19 | 21.6 | .69 | 67 | .060 | 1 | 1.82 | .006 | .05 | .1 | .02 | 2.4 | .1 | <.05 | 9 | <.5 | 7.5 |
| 27 525E | 1.3 | 41.9 | 38.8 | 106 | .3 | 29.5 | 10.2 | 251 | 3.72 | 6.5 | 1.7 | 2.1 | 7.3 | 9 | .3 | .2 | .6 | 69 | .08 | .032 | 16 | 23.4 | .46 | 102 | .075 | 1 | 3.73 | .010 | .08 | .1 | .08 | 3.9 | .1 | <.05 | 12 | <.5 | 7.5 |
| 27 550E | .5 | 26.7 | 20.9 | 59 | .1 | 14.6 | 4.9 | 102 | 1.52 | 2.0 | .9 | 19.6 | 1.6 | 7 | .3 | .2 | .3 | 40 | .07 | .025 | 16 | 14.0 | .37 | 46 | .058 | 2 | 1.42 | .008 | .04 | .1 | .04 | 1.9 | .1 | <.05 | 6 | <.5 | 15.0 |
| 27 575E | .8 | 44.5 | 39.4 | 59 | .4 | 18.7 | 9.9 | 136 | 1.79 | 15.3 | 3.2 | 15.0 | .4 | 11 | .5 | .1 | .5 | 56 | .10 | .054 | 37 | 24.1 | .44 | 94 | .055 | 1 | 2.61 | .010 | .09 | .1 | .03 | 1.5 | .2 | .08 | 9 | <.5 | 15.0 |
| 27 600E | .5 | 17.1 | 10.5 | 48 | .2 | 8.0 | 5.6 | 107 | 2.51 | 5.4 | .5 | 1317.3 | 2.7 | 11 | .1 | .1 | .3 | 45 | .16 | .044 | 14 | 11.9 | .29 | 60 | .035 | 1 | 1.18 | .004 | .03 | .1 | .02 | 1.9 | <.1 | <.05 | 5 | <.5 | 7.5 |
| RE 27 600E | .5 | 16.0 | 9.9 | 49 | .1 | 8.9 | 6.0 | 112 | 2.92 | 5.6 | .5 | 48.1 | 2.6 | 11 | .1 | .1 | .2 | 49 | .14 | .040 | 14 | 11.9 | .33 | 64 | .032 | 1 | 1.18 | .004 | .02 | .1 | .03 | 1.6 | <.1 | <.05 | 5 | <.5 | 7.5 |
| 27 625E | .4 | 16.4 | 10.4 | 38 | .1 | 9.0 | 4.9 | 128 | 1.46 | 3.6 | .5 | 34.7 | 1.4 | 6 | .1 | .1 | .2 | 31 | .08 | .016 | 23 | 12.1 | .39 | 54 | .034 | <1 | 1.09 | .005 | .04 | <.1 | .01 | 1.5 | .1 | <.05 | 5 | <.5 | 15.0 |
| 27 650E | .3 | 10.4 | 20.0 | 21 | .1 | 2.6 | 2.4 | 105 | .58 | 1.2 | .4 | .6 | .4 | 10 | .2 | .1 | .4 | 19 | .12 | .016 | 9 | 4.7 | .05 | 54 | .105 | 1 | .72 | .014 | .02 | <.1 | .03 | .8 | .1 | <.05 | 10 | <.5 | 15.0 |
| 27 675E | .5 | 98.0 | 20.9 | 50 | .3 | 23.9 | 9.9 | 221 | 4.08 | 8.9 | 1.7 | 4.0 | 4.8 | 15 | .2 | .2 | .3 | 76 | .16 | .039 | 16 | 38.1 | .39 | 113 | .131 | <1 | 4.10 | .013 | .08 | .1 | .08 | 7.5 | .1 | <.05 | 14 | .5 | 7.5 |
| 27 700E | .5 | 20.7 | 12.7 | 48 | .1 | 10.8 | 7.0 | 154 | 2.01 | 3.2 | .5 | 14.1 | 3.7 | 6 | .1 | .1 | .2 | 41 | .11 | .021 | 15 | 15.7 | .37 | 52 | .059 | 1 | 1.31 | .006 | .04 | .1 | .01 | 2.2 | .1 | .07 | 6 | <.5 | 15.0 |
| 27 725E | .3 | 19.1 | 12.6 | 51 | .2 | 10.2 | 6.2 | 184 | 2.09 | 2.1 | .8 | 5.0 | 1.5 | 12 | .1 | .1 | .3 | 36 | .19 | .037 | 19 | 17.4 | .39 | 86 | .047 | 2 | 1.43 | .008 | .04 | .1 | .04 | 2.6 | .1 | .07 | 9 | <.5 | 15.0 |
| 27 750E | 1.0 | 18.3 | 18.4 | 53 | .2 | 5.5 | 4.3 | 250 | 3.13 | 3.9 | .8 | 2.4 | 1.8 | 13 | .2 | .1 | .4 | 51 | .19 | .044 | 8 | 9.9 | .11 | 52 | .246 | 1 | 2.08 | .021 | .03 | .1 | .11 | 1.9 | .1 | .09 | 24 | .5 | 15.0 |
| 27 775E | .9 | 19.0 | 16.7 | 30 | .2 | 4.3 | 2.0 | 41 | 2.19 | 3.9 | 1.1 | 2.1 | 3.5 | 7 | .2 | .1 | .2 | 31 | .10 | .048 | 7 | 9.5 | .07 | 39 | .146 | 2 | 3.69 | .019 | .02 | .2 | .12 | 2.4 | <.1 | <.05 | 13 | .6 | 15.0 |
| 27 800E | .5 | 52.4 | 29.0 | 48 | .2 | 18.0 | 12.4 | 313 | 3.11 | 6.4 | 1.8 | 2.2 | 1.5 | 23 | .3 | .2 | .5 | 71 | .26 | .058 | 41 | 32.7 | .36 | 139 | .066 | <1 | 2.63 | .009 | .07 | .1 | .06 | 3.3 | .1 | <.05 | 12 | .5 | 15.0 |
| 27 825E | .5 | 26.9 | 18.1 | 43 | .2 | 10.1 | 8.2 | 156 | 2.92 | 2.8 | 1.1 | 2.7 | 3.4 | 11 | .1 | .1 | .3 | 40 | .11 | .031 | 20 | 13.9 | .21 | 85 | .112 | 1 | 1.97 | .016 | .04 | .1 | .08 | 2.7 | .1 | .09 | 12 | <.5 | 15.0 |
| 27 850E | .8 | 23.6 | 16.4 | 59 | .3 | 11.2 | 7.3 | 296 | 3.12 | 5.4 | 1.0 | 2.5 | 4.2 | 7 | .1 | .1 | .3 | 43 | .10 | .087 | 14 | 21.1 | .30 | 73 | .073 | 2 | 4.22 | .009 | .04 | .1 | .12 | 3.1 | .1 | <.05 | 8 | .6 | 15.0 |
| 27 875E | .5 | 38.9 | 12.7 | 69 | .2 | 17.8 | 9.6 | 176 | 3.88 | 4.3 | .6 | 4.4 | 3.2 | 6 | .2 | .2 | .2 | 81 | .11 | .029 | 11 | 36.2 | .56 | 68 | .080 | <1 | 1.78 | .005 | .05 | <.1 | .03 | 3.7 | .1 | <.05 | 6 | <.5 | 15.0 |
| 27 900E | .8 | 19.8 | 13.7 | 38 | .2 | 7.2 | 4.8 | 131 | 2.82 | 4.5 | .9 | 2.8 | 4.2 | 8 | .2 | .2 | .2 | 40 | .10 | .037 | 7 | 14.6 | .16 | 52 | .114 | <1 | 4.13 | .013 | .03 | .1 | .12 | 2.8 | .1 | <.05 | 11 | .5 | 15.0 |
| 27 925E | .5 | 56.3 | 30.7 | 51 | .4 | 13.9 | 29.2 | 1550 | 2.94 | 2.4 | .9 | 2.4 | 1.4 | 19 | .2 | .2 | .4 | 72 | .20 | .028 | 21 | 26.2 | .38 | 103 | .096 | 2 | 1.96 | .013 | .05 | .1 | .04 | 4.2 | .1 | .08 | 11 | <.5 | 15.0 |
| 27 950E | .4 | 16.1 | 11.8 | 63 | .1 | 8.2 | 6.0 | 148 | 2.65 | 4.3 | .8 | 2.0 | 3.0 | 9 | .1 | .2 | .2 | 42 | .14 | .064 | 5 | 23.6 | .16 | 67 | .108 | <1 | 4.41 | .013 | .02 | .1 | .09 | 2.9 | <.1 | <.05 | 9 | <.5 | 15.0 |
| 27 975E | .7 | 29.6 | 12.4 | 30 | .4 | 7.7 | 3.8 | 102 | 2.32 | 2.4 | 1.0 | 2.6 | 3.2 | 9 | .2 | .1 | .3 | 37 | .11 | .033 | 16 | 20.0 | .12 | 47 | .145 | 1 | 2.95 | .017 | .03 | .1 | .13 | 4.8 | .1 | <.05 | 12 | .6 | 15.0 |
| 27 1000E | .3 | 25.1 | 10.1 | 53 | .1 | 20.2 | 9.6 | 194 | 2.79 | 2.8 | .4 | 1.9 | 1.9 | 11 | .1 | .1 | .2 | 68 | .21 | .016 | 11 | 45.1 | .65 | 72 | .076 | <1 | 1.65 | .008 | .04 | <.1 | .01 | 2.9 | .1 | <.05 | 8 | <.5 | 15.0 |
| 28 500E | .9 | 61.0 | 33.5 | 66 | .3 | 19.1 | 12.8 | 703 | 3.57 | 4.9 | 1.7 | 6.2 | .9 | 14 | .6 | .1 | .6 | 73 | .20 | .094 | 36 | 22.9 | .51 | 122 | .044 | <1 | 3.35 | .009 | .06 | .1 | .08 | 4.4 | .1 | .12 | 10 | <.5 | 15.0 |
| 28 525E | .6 | 55.5 | 29.1 | 55 | .3 | 15.5 | 11.4 | 303 | 2.98 | 3.7 | 1.4 | 11.7 | 1.4 | 15 | .4 | .1 | .5 | 54 | .18 | .048 | 34 | 16.8 | .37 | 100 | .055 | 1 | 2.54 | .009 | .05 | .1 | .07 | 4.0 | .1 | .09 | 10 | <.5 | 15.0 |
| 28 550E | .6 | 43.7 | 24.8 | 73 | .3 | 18.0 | 12.7 | 404 | 3.18 | 4.3 | 1.2 | 4.0 | 1.6 | 16 | .4 | .2 | .5 | 53 | .25 | .045 | 28 | 21.7 | .52 | 123 | .060 | 2 | 2.56 | .007 | .06 | <.1 | .05 | 4.1 | .1 | <.05 | 10 | <.5 | 15.0 |
| STANDARD DS5 | 12.3 | 138.0 | 24.6 | 138 | .3 | 24.3 | 11.9 | 793 | 3.04 | 18.1 | 6.4 | 43.3 | 2.7 | 45 | 5.7 | 3.7 | 6.3 | 61 | .73 | .087 | 11 | 177.9 | .68 | 135 | .093 | 18 | 2.03 | .034 | .13 | 4.8 | .17 | 3.4 | 1.1 | <.05 | 7 | 5.0 | 15.0 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data FA

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| G-1 | 2.2 | 4.1 | 2.9 | 45 | <.1 | 5.3 | 4.3 | 536 | 1.91 | .7 | 2.4 | .5 | 4.4 | 83 | <.1 | <.1 | .1 | 37 | .72 | .080 | 10 | 18.6 | .49 | 236 | .133 | 1 | 1.00 | .103 | .43 | 4.1 | <.01 | 2.2 | .3 | <.05 | 5 | <.5 | 15.0 |
| 28 575E | .6 | 43.7 | 20.6 | 34 | .3 | 10.9 | 4.6 | 141 | 3.01 | 3.5 | 1.5 | 1.8 | 1.0 | 14 | .5 | .2 | .4 | 36 | .17 | .049 | 30 | 12.8 | .21 | 62 | .108 | 1 | 1.51 | .014 | .04 | .1 | .07 | 3.4 | .1 | .06 | 11 | .7 | 15.0 |
| 28 600E | 1.0 | 26.1 | 26.1 | 74 | .2 | 16.0 | 8.7 | 217 | 3.68 | 5.1 | .7 | 2.3 | 3.1 | 10 | .4 | .3 | .6 | 82 | .11 | .035 | 13 | 21.3 | .41 | 105 | .131 | <1 | 2.16 | .011 | .06 | .1 | .05 | 2.4 | .1 | <.05 | 15 | .5 | 7.5 |
| 28 625E | 1.1 | 38.8 | 27.9 | 59 | .4 | 14.9 | 8.9 | 210 | 3.71 | 4.7 | 1.5 | 4.8 | 3.6 | 9 | .3 | .2 | .5 | 73 | .09 | .048 | 17 | 20.5 | .30 | 77 | .090 | 1 | 3.19 | .008 | .05 | .2 | .18 | 3.3 | .1 | <.05 | 12 | .7 | 15.0 |
| 28 650E | .7 | 28.8 | 15.0 | 73 | .2 | 17.3 | 10.2 | 170 | 2.82 | 3.3 | .9 | 7.0 | 4.6 | 5 | .2 | .1 | .3 | 46 | .08 | .028 | 19 | 18.7 | .52 | 63 | .046 | <1 | 2.07 | .005 | .05 | .1 | .03 | 2.7 | .1 | .08 | 7 | <.5 | 15.0 |
| 28 675E | .8 | 16.3 | 26.4 | 51 | .2 | 9.9 | 4.4 | 131 | 2.04 | 2.4 | .5 | 3.3 | 2.0 | 10 | .3 | .1 | .5 | 50 | .11 | .025 | 10 | 12.5 | .26 | 104 | .115 | <1 | 1.40 | .014 | .05 | .1 | .03 | 1.6 | .1 | <.05 | 12 | <.5 | 7.5 |
| 28 700E | .8 | 21.4 | 15.5 | 29 | .1 | 5.3 | 3.1 | 70 | 1.96 | 4.1 | 1.4 | 2.3 | 3.3 | 8 | .3 | .1 | .2 | 28 | .09 | .052 | 11 | 10.2 | .10 | 31 | .116 | 1 | 3.93 | .018 | .02 | .2 | .12 | 2.7 | .1 | .06 | 10 | .6 | 15.0 |
| 28 725E | .8 | 31.4 | 34.2 | 90 | .2 | 19.2 | 26.6 | 2086 | 2.95 | 5.5 | 1.5 | 2.9 | 1.3 | 29 | .9 | .2 | .5 | 56 | .39 | .071 | 27 | 23.6 | .46 | 137 | .039 | <1 | 2.11 | .009 | .06 | <.1 | .09 | 3.4 | .2 | .09 | 7 | .6 | 7.5 |
| 28 750E | .9 | 45.4 | 29.7 | 91 | .3 | 20.2 | 19.7 | 1031 | 3.50 | 4.8 | 1.4 | 4.9 | 2.4 | 15 | .2 | .1 | .5 | 73 | .16 | .037 | 20 | 31.2 | .48 | 112 | .072 | <1 | 2.55 | .011 | .07 | .1 | .03 | 3.9 | .2 | <.05 | 10 | .5 | 15.0 |
| 28 775E | .5 | 33.8 | 15.0 | 69 | .2 | 15.1 | 13.3 | 401 | 2.92 | 3.7 | .9 | 12.3 | 1.4 | 13 | .2 | .1 | .3 | 40 | .17 | .047 | 15 | 20.2 | .43 | 90 | .054 | <1 | 2.00 | .010 | .04 | .1 | .05 | 2.3 | .1 | <.05 | 8 | <.5 | 15.0 |
| 28 800E | .6 | 38.9 | 20.1 | 54 | .2 | 12.0 | 9.7 | 568 | 1.91 | 1.9 | 1.0 | 5.0 | .5 | 16 | .4 | .1 | .4 | 34 | .23 | .065 | 12 | 16.3 | .32 | 87 | .063 | <1 | 1.42 | .015 | .04 | .1 | .04 | 1.5 | .1 | <.05 | 8 | <.5 | 15.0 |
| 28 825E | .9 | 38.7 | 26.6 | 56 | .2 | 14.1 | 11.5 | 320 | 2.27 | 6.6 | 1.4 | 1.8 | .9 | 18 | .3 | .1 | .4 | 52 | .23 | .060 | 10 | 19.3 | .20 | 89 | .109 | 2 | 2.09 | .023 | .04 | .1 | .08 | 1.8 | .1 | <.05 | 12 | .6 | 15.0 |
| 28 850E | .7 | 32.3 | 22.2 | 49 | .3 | 14.2 | 12.5 | 689 | 2.10 | 12.2 | 1.8 | 5.9 | 1.4 | 15 | .4 | .2 | .3 | 60 | .21 | .046 | 33 | 28.2 | .26 | 89 | .071 | <1 | 2.12 | .012 | .05 | .1 | .06 | 2.7 | .1 | <.05 | 9 | .8 | 7.5 |
| 28 875E | .7 | 48.1 | 31.2 | 58 | .3 | 21.0 | 8.3 | 163 | 2.75 | 3.1 | 2.1 | 3.3 | 1.8 | 17 | .4 | .1 | .6 | 59 | .16 | .042 | 29 | 28.9 | .40 | 125 | .082 | <1 | 2.77 | .012 | .08 | .1 | .05 | 4.5 | .1 | <.05 | 12 | .5 | 15.0 |
| 28 900E | .6 | 33.8 | 22.6 | 39 | .2 | 9.5 | 5.6 | 104 | 2.28 | 2.4 | .9 | 4.2 | 1.4 | 12 | .3 | .2 | .4 | 35 | .14 | .027 | 15 | 16.9 | .27 | 76 | .058 | <1 | 1.45 | .010 | .03 | .1 | .06 | 2.4 | .1 | <.05 | 8 | <.5 | 7.5 |
| 28 925E | .4 | 66.7 | 21.1 | 78 | .2 | 23.9 | 14.6 | 331 | 3.77 | 3.8 | .8 | 2.8 | 2.4 | 13 | .1 | .1 | .3 | 71 | .16 | .035 | 17 | 42.2 | .59 | 102 | .085 | <1 | 2.71 | .012 | .06 | .1 | .03 | 4.5 | .1 | <.05 | 10 | <.5 | 15.0 |
| 28 950E | .7 | 17.3 | 16.7 | 42 | .2 | 7.8 | 6.2 | 128 | 2.45 | 3.0 | .6 | 5.6 | 1.7 | 10 | .2 | .1 | .4 | 49 | .12 | .025 | 13 | 17.7 | .24 | 68 | .081 | 1 | 1.30 | .009 | .04 | .1 | .03 | 1.9 | .1 | <.05 | 10 | <.5 | 15.0 |
| 28 975E | .5 | 33.2 | 21.6 | 36 | .3 | 6.9 | 4.3 | 133 | 1.74 | 1.7 | .8 | 1.3 | 1.1 | 13 | .1 | .1 | .3 | 32 | .12 | .027 | 9 | 13.3 | .15 | 56 | .137 | <1 | 1.18 | .020 | .03 | .1 | .04 | 2.0 | <.1 | <.05 | 10 | <.5 | 15.0 |
| 28 1000E | .6 | 58.0 | 26.3 | 48 | .4 | 21.2 | 15.3 | 354 | 3.72 | 3.8 | .8 | 1.9 | 2.9 | 18 | .1 | .2 | .4 | 66 | .17 | .038 | 12 | 33.8 | .35 | 118 | .201 | <1 | 2.85 | .019 | .05 | .1 | .03 | 4.3 | .1 | <.05 | 14 | <.5 | 7.5 |
| RE 28 1000E | .5 | 59.7 | 26.2 | 52 | .4 | 22.7 | 14.4 | 379 | 3.93 | 3.7 | .8 | 1.0 | 3.2 | 18 | .1 | .1 | .4 | 71 | .15 | .042 | 12 | 33.8 | .36 | 116 | .197 | <1 | 2.86 | .020 | .05 | .1 | .03 | 3.8 | .1 | <.05 | 14 | <.5 | 7.5 |
| 1820 100W | 1.0 | 12.6 | 13.1 | 66 | .2 | 11.8 | 7.8 | 115 | 3.47 | 6.2 | .9 | 82.7 | 6.8 | 4 | .1 | .2 | .4 | 36 | .04 | .091 | 16 | 16.1 | .32 | 54 | .061 | <1 | 3.53 | .008 | .05 | .2 | .05 | 2.2 | .1 | <.05 | 8 | <.5 | 15.0 |
| 1820 075W | .9 | 14.6 | 8.9 | 44 | .2 | 8.6 | 3.9 | 81 | 2.04 | 4.5 | 1.1 | 14.4 | 4.8 | 3 | .1 | .2 | .3 | 26 | .03 | .105 | 10 | 10.6 | .21 | 46 | .067 | <1 | 3.29 | .010 | .04 | .2 | .11 | 2.9 | .1 | <.05 | 8 | .6 | 7.5 |
| 1820 050W | .9 | 11.0 | 11.7 | 40 | .1 | 5.8 | 3.8 | 99 | 3.32 | 5.8 | .6 | 36.0 | 6.1 | 4 | <.1 | .3 | .5 | 39 | .04 | .063 | 22 | 12.9 | .16 | 34 | .029 | <1 | 1.60 | .005 | .03 | .1 | .04 | 1.3 | .1 | <.05 | 10 | <.5 | 7.5 |
| 1820 025W | .9 | 12.5 | 10.7 | 56 | .2 | 9.6 | 5.9 | 118 | 2.52 | 4.8 | 1.2 | 5.7 | 5.6 | 4 | .1 | .2 | .3 | 25 | .04 | .108 | 10 | 13.4 | .19 | 47 | .054 | <1 | 4.90 | .007 | .04 | .2 | .10 | 2.8 | .1 | <.05 | 7 | .5 | 7.5 |
| 1820 000E | .7 | 7.7 | 15.9 | 35 | .1 | 6.0 | 3.1 | 73 | 3.00 | 5.3 | .6 | 23.9 | 6.4 | 3 | <.1 | .2 | .5 | 26 | .04 | .062 | 28 | 12.0 | .18 | 36 | .014 | 1 | 1.83 | .004 | .04 | .1 | .06 | 1.5 | .1 | <.05 | 7 | <.5 | 15.0 |
| 1820 25E | 1.4 | 8.9 | 30.3 | 57 | .3 | 9.0 | 4.8 | 89 | 3.15 | 5.2 | .7 | 7.6 | 4.7 | 7 | .2 | .2 | .6 | 30 | .05 | .057 | 19 | 11.8 | .23 | 86 | .032 | <1 | 1.63 | .006 | .06 | .2 | .06 | 1.4 | .1 | <.05 | 8 | <.5 | 7.5 |
| 1820 50E | 1.7 | 20.4 | 72.8 | 83 | .1 | 15.9 | 23.3 | 1757 | 2.89 | 5.4 | 2.7 | 197.3 | 2.7 | 14 | .3 | .2 | .7 | 25 | .18 | .061 | 23 | 14.1 | .57 | 150 | .021 | <1 | 1.98 | .008 | .09 | .1 | .03 | 1.7 | .1 | .07 | 6 | <.5 | 7.5 |
| 1820 75E | 1.2 | 17.9 | 21.3 | 68 | .2 | 11.6 | 7.5 | 224 | 2.65 | 5.8 | .9 | 76.9 | 6.8 | 4 | .1 | .2 | .6 | 33 | .03 | .039 | 21 | 12.7 | .33 | 66 | .047 | <1 | 1.85 | .009 | .05 | .2 | .05 | 1.9 | .1 | <.05 | 8 | <.5 | 15.0 |
| 1820 100E | .9 | 13.1 | 17.8 | 65 | .2 | 10.6 | 7.1 | 158 | 3.13 | 7.9 | 1.0 | 14.1 | 6.6 | 5 | .1 | .2 | .4 | 26 | .05 | .074 | 16 | 14.0 | .24 | 57 | .050 | <1 | 2.92 | .008 | .05 | .1 | .10 | 2.0 | .1 | <.05 | 7 | .6 | 7.5 |
| 1820 125E | .6 | 10.2 | 11.4 | 36 | .1 | 7.1 | 4.9 | 86 | 1.90 | 5.8 | .5 | 3.3 | 5.7 | 5 | .1 | .2 | .5 | 21 | .06 | .044 | 25 | 9.3 | .20 | 42 | .013 | 1 | 1.09 | .004 | .04 | .1 | .03 | 1.1 | .1 | <.05 | 5 | <.5 | 15.0 |
| 1820 150E | .8 | 10.5 | 9.3 | 38 | .1 | 6.8 | 4.5 | 77 | 2.67 | 5.0 | .5 | 28.1 | 3.8 | 4 | .1 | .2 | .4 | 28 | .03 | .039 | 19 | 9.0 | .20 | 33 | .028 | 1 | 1.05 | .005 | .03 | .1 | .03 | .9 | .1 | <.05 | 6 | <.5 | 15.0 |
| 1820 175E | 1.3 | 36.3 | 16.4 | 48 | .2 | 13.9 | 8.1 | 217 | 2.92 | 13.7 | 4.8 | 3.3 | 4.9 | 11 | .2 | .2 | .6 | 25 | .09 | .049 | 31 | 15.3 | .30 | 127 | .037 | <1 | 2.31 | .010 | .09 | .1 | .05 | 2.8 | .1 | <.05 | 9 | .7 | 7.5 |
| 1820 200E | .8 | 10.5 | 12.8 | 34 | .2 | 5.7 | 3.5 | 70 | 2.45 | 4.2 | .7 | 3.8 | 3.4 | 3 | .2 | .2 | .4 | 26 | .03 | .062 | 11 | 9.6 | .13 | 52 | .053 | <1 | 2.72 | .010 | .03 | .2 | .10 | 1.7 | <.1 | <.05 | 9 | <.5 | 15.0 |
| 1820 225E | .6 | 15.5 | 11.6 | 33 | .1 | 10.0 | 7.1 | 289 | 2.02 | 3.4 | 1.5 | 1.1 | 2.3 | 7 | .2 | .1 | .4 | 13 | .05 | .053 | 31 | 9.2 | .35 | 53 | .010 | <1 | 1.01 | .004 | .05 | .1 | .03 | .8 | <.1 | <.05 | 3 | <.5 | 7.5 |
| 1820 250E | .5 | 17.1 | 10.1 | 42 | <.1 | 13.9 | 9.2 | 223 | 2.12 | 4.0 | .9 | 2.0 | 8.0 | 3 | .1 | .1 | .4 | 10 | .02 | .039 | 28 | 10.3 | .49 | 35 | .008 | <1 | 1.19 | .003 | .06 | .1 | .03 | .9 | <.1 | <.05 | 3 | <.5 | 15.0 |
| STANDARD DS5 | 12.2 | 141.5 | 24.7 | 131 | .3 | 24.7 | 12.8 | 749 | 3.01 | 18.2 | 6.3 | 42.3 | 2.8 | 45 | 5.7 | 3.5 | 6.3 | 62 | .78 | .099 | 14 | 175.0 | .70 | 145 | .097 | 18 | 1.99 | .035 | .14 | 4.7 | .16 | 3.6 | 1.1 | .06 | 7 | 4.9 | 15.0 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data FA

ACME ANALYTICAL

# Ruby Red Resources Inc. PROJECT EDDY FILE # A403684



ACME ANALYTICAL

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| G-1 | 2.3 | 4.0 | 2.8 | 50 | <.1 | 4.9 | 4.0 | 568 | 1.99 | <.5 | 2.4 | <.5 | 5.0 | 93 | <.1 | <.1 | .2 | 42 | .74 | .083 | 12 | 23.0 | .57 | 223 | .136 | <1 | 1.01 | .146 | .66 | 4.4 | <.01 | 2.7 | .4 | <.05 | 5 | <.5 | 15.0 |
| 1820 275E | 1.3 | 17.7 | 15.5 | 54 | .2 | 13.7 | 8.1 | 415 | 2.24 | 4.7 | 1.3 | 1.0 | 3.5 | 8 | .2 | .1 | .4 | 22 | .08 | .039 | 28 | 12.6 | .42 | 78 | .026 | <1 | 1.67 | .008 | .07 | .2 | .04 | 1.5 | .1 | .07 | 8 | <.5 | 15.0 |
| 1820 300E | .7 | 10.1 | 12.1 | 57 | .2 | 11.0 | 7.3 | 186 | 2.35 | 3.7 | 1.0 | 1.5 | 5.7 | 5 | .2 | .1 | .3 | 20 | .04 | .077 | 25 | 10.5 | .35 | 65 | .030 | <1 | 1.63 | .009 | .06 | .1 | .05 | 1.4 | .1 | <.05 | 7 | <.5 | 15.0 |
| 1820 325E | .9 | 24.5 | 18.4 | 58 | .2 | 22.4 | 14.5 | 853 | 2.18 | 3.4 | 2.9 | 1.6 | 2.0 | 16 | .3 | .1 | .5 | 19 | .15 | .050 | 31 | 13.8 | .46 | 78 | .010 | <1 | 1.75 | .007 | .08 | .1 | .02 | 1.5 | .1 | <.05 | 6 | <.5 | 15.0 |
| 1820 350E | .6 | 11.2 | 11.7 | 51 | .1 | 10.4 | 5.5 | 166 | 2.43 | 4.7 | .8 | 5.9 | 4.3 | 6 | .1 | .2 | .4 | 25 | .06 | .058 | 24 | 12.8 | .32 | 75 | .018 | <1 | 1.46 | .007 | .06 | .2 | .03 | 1.3 | .1 | <.05 | 7 | <.5 | 15.0 |
| 1820 375E | .6 | 21.9 | 22.3 | 47 | .2 | 14.8 | 12.6 | 853 | 2.31 | 3.4 | 2.0 | 2.7 | 4.0 | 14 | .2 | .1 | .5 | 23 | .19 | .042 | 32 | 14.0 | .45 | 85 | .015 | <1 | 1.81 | .008 | .06 | .1 | .02 | 1.8 | .1 | <.05 | 7 | <.5 | 15.0 |
| 1820 400E | .9 | 16.9 | 12.0 | 45 | .2 | 10.0 | 8.2 | 352 | 2.00 | 2.6 | 1.3 | .6 | 3.4 | 6 | .1 | .1 | .4 | 20 | .07 | .033 | 28 | 11.0 | .32 | 60 | .016 | <1 | 1.53 | .006 | .05 | .1 | .03 | 1.3 | .1 | .08 | 6 | <.5 | 7.5 |
| 1820 425E | .4 | 5.7 | 7.0 | 31 | .1 | 5.7 | 3.3 | 109 | 1.67 | 2.2 | .5 | .8 | 2.7 | 6 | .1 | .1 | .3 | 21 | .08 | .023 | 23 | 8.6 | .18 | 75 | .018 | <1 | 1.02 | .006 | .04 | .1 | .02 | 1.0 | .1 | <.05 | 6 | <.5 | 15.0 |
| 1820 450E | .8 | 10.4 | 10.8 | 39 | .2 | 7.4 | 5.9 | 297 | 2.01 | 1.8 | .8 | <.5 | 3.3 | 5 | .1 | .1 | .4 | 35 | .05 | .034 | 16 | 11.0 | .14 | 76 | .046 | <1 | 1.74 | .010 | .04 | .1 | .05 | 1.6 | .1 | <.05 | 9 | <.5 | 15.0 |
| 1820 475E | .6 | 13.7 | 11.2 | 50 | .1 | 11.6 | 7.3 | 211 | 2.28 | 3.7 | 1.1 | 2.3 | 7.1 | 4 | .1 | .1 | .3 | 25 | .04 | .097 | 12 | 11.5 | .22 | 76 | .073 | <1 | 3.18 | .010 | .04 | .2 | .08 | 2.1 | .1 | <.05 | 8 | <.5 | 15.0 |
| 1820 500E | .5 | 11.7 | 9.5 | 33 | .1 | 8.7 | 8.6 | 127 | 1.84 | 2.2 | 1.4 | <.5 | 5.3 | 5 | .1 | .1 | .3 | 22 | .07 | .029 | 26 | 10.8 | .21 | 70 | .021 | <1 | 1.40 | .006 | .04 | .1 | .03 | 1.8 | .1 | <.05 | 5 | <.5 | 15.0 |
| 1820 525E | .4 | 12.3 | 6.9 | 45 | .1 | 17.1 | 8.7 | 171 | 2.04 | 2.7 | 1.2 | 1.9 | 5.4 | 6 | .1 | .1 | .3 | 15 | .06 | .029 | 28 | 11.8 | .45 | 57 | .013 | <1 | 1.23 | .003 | .05 | .1 | .01 | 1.6 | <.1 | <.05 | 4 | <.5 | 15.0 |
| 1820 550E | .6 | 10.4 | 10.3 | 49 | .1 | 13.2 | 10.7 | 162 | 2.13 | 2.8 | .9 | 1.2 | 6.1 | 4 | .1 | .1 | .3 | 20 | .04 | .049 | 21 | 11.9 | .30 | 91 | .036 | 1 | 2.24 | .006 | .07 | .1 | .04 | 1.7 | .1 | <.05 | 6 | <.5 | 15.0 |
| 1820 575E | .5 | 22.4 | 14.0 | 52 | .1 | 31.4 | 22.1 | 237 | 2.64 | 5.1 | 1.7 | 1.5 | 9.1 | 10 | .1 | .1 | .4 | 30 | .12 | .030 | 21 | 16.8 | .43 | 150 | .033 | <1 | 2.66 | .007 | .08 | .1 | .04 | 3.0 | .1 | <.05 | 8 | <.5 | 15.0 |
| 1820 600E | .6 | 25.4 | 21.0 | 44 | .1 | 31.2 | 25.9 | 214 | 2.51 | 6.1 | 2.7 | 5.8 | 6.4 | 10 | .1 | .1 | .5 | 34 | .12 | .031 | 31 | 22.2 | .55 | 116 | .023 | <1 | 2.20 | .006 | .08 | .1 | .03 | 3.8 | .1 | <.05 | 7 | <.5 | 7.5 |
| 1820 625E | .6 | 9.4 | 9.1 | 39 | <.1 | 10.8 | 8.3 | 124 | 1.92 | 3.4 | .7 | 4.0 | 6.2 | 3 | .1 | .2 | .3 | 20 | .03 | .025 | 24 | 9.3 | .34 | 59 | .016 | 1 | 1.38 | .004 | .04 | .1 | .02 | 1.3 | .1 | <.05 | 5 | <.5 | 7.5 |
| 1820 650E | .7 | 29.5 | 16.9 | 61 | .1 | 27.7 | 26.2 | 367 | 2.76 | 5.9 | 2.0 | 2.1 | 9.7 | 6 | .1 | .1 | .4 | 24 | .04 | .044 | 27 | 20.2 | .56 | 131 | .011 | <1 | 2.55 | .005 | .11 | .1 | .03 | 2.6 | .1 | <.05 | 6 | <.5 | 7.5 |
| RE 1820 650E | .7 | 28.3 | 16.5 | 69 | .1 | 28.4 | 26.1 | 361 | 2.61 | 5.8 | 1.9 | 1.4 | 9.5 | 6 | <.1 | .1 | .4 | 23 | .04 | .050 | 29 | 17.4 | .66 | 133 | .012 | <1 | 2.48 | .005 | .11 | .1 | .03 | 2.5 | .1 | <.05 | 7 | <.5 | 7.5 |
| 1820 675E | .3 | 12.9 | 6.2 | 42 | <.1 | 13.3 | 7.6 | 174 | 1.74 | 2.5 | .9 | 1.1 | 6.4 | 5 | <.1 | .1 | .2 | 12 | .04 | .020 | 28 | 12.9 | .46 | 43 | .006 | <1 | 1.20 | .003 | .05 | <.1 | .01 | 1.2 | <.1 | <.05 | 3 | <.5 | 15.0 |
| 1820 700E | .5 | 26.7 | 17.2 | 52 | .2 | 16.6 | 16.4 | 273 | 2.29 | 3.7 | 1.1 | .9 | 5.3 | 10 | .1 | .1 | .4 | 28 | .09 | .042 | 23 | 21.8 | .43 | 103 | .019 | 1 | 1.96 | .010 | .09 | .1 | .03 | 2.2 | .1 | <.05 | 8 | <.5 | 7.5 |
| 1820 725E | .4 | 24.4 | 12.5 | 45 | .1 | 15.2 | 17.1 | 231 | 2.05 | 3.6 | 1.0 | .8 | 5.0 | 7 | .1 | .1 | .3 | 22 | .06 | .027 | 24 | 18.8 | .43 | 79 | .018 | <1 | 1.57 | .006 | .06 | .1 | .01 | 1.7 | .1 | <.05 | 5 | <.5 | 15.0 |
| 1820 750E | .8 | 23.1 | 13.5 | 57 | .1 | 24.2 | 23.7 | 214 | 3.07 | 5.2 | 1.3 | 1.1 | 8.4 | 8 | <.1 | .1 | .4 | 29 | .07 | .048 | 24 | 18.7 | .54 | 144 | .030 | <1 | 2.77 | .007 | .10 | .1 | .02 | 2.5 | .1 | <.05 | 9 | <.5 | 15.0 |
| 1880 000E | .7 | 8.0 | 14.3 | 35 | .1 | 7.8 | 3.7 | 101 | 2.49 | 3.0 | .8 | 22.1 | 4.1 | 5 | .2 | .1 | .4 | 24 | .02 | .022 | 23 | 10.8 | .24 | 80 | .025 | <1 | 1.26 | .005 | .06 | .1 | .03 | 1.3 | .1 | <.05 | 7 | <.5 | 7.5 |
| 1880 025E | .9 | 10.0 | 13.8 | 46 | .2 | 7.5 | 4.1 | 143 | 2.87 | 3.9 | .5 | .8 | 4.2 | 5 | .2 | .2 | .5 | 26 | .03 | .050 | 21 | 11.0 | .22 | 61 | .034 | 1 | 1.24 | .007 | .05 | .1 | .04 | 1.1 | .1 | <.05 | 8 | <.5 | 7.5 |
| 1880 050E | .5 | 12.8 | 15.9 | 43 | .1 | 10.4 | 6.3 | 187 | 2.04 | 2.5 | 1.9 | 1.0 | 4.2 | 8 | .1 | .1 | .4 | 21 | .07 | .021 | 29 | 12.3 | .37 | 81 | .026 | 1 | 1.68 | .006 | .06 | .1 | .03 | 1.5 | .1 | <.05 | 7 | <.5 | 15.0 |
| 1880 075E | .6 | 5.9 | 10.4 | 32 | .1 | 7.0 | 3.7 | 109 | 2.01 | 2.4 | .6 | .6 | 3.9 | 3 | .1 | .1 | .4 | 22 | .03 | .027 | 20 | 10.2 | .23 | 47 | .022 | 1 | 1.15 | .004 | .05 | .1 | .03 | 1.1 | .1 | <.05 | 6 | <.5 | 7.5 |
| 1880 100E | .5 | 11.1 | 10.3 | 48 | .1 | 11.8 | 6.5 | 164 | 1.97 | 2.8 | 1.3 | 1.1 | 6.6 | 5 | .1 | .1 | .3 | 15 | .03 | .028 | 24 | 11.3 | .36 | 53 | .025 | <1 | 1.45 | .004 | .06 | .1 | .03 | 1.1 | .1 | .06 | 5 | <.5 | 15.0 |
| 1880 125E | .5 | 8.7 | 12.1 | 34 | <.1 | 6.5 | 7.5 | 176 | 1.24 | 1.4 | 1.1 | 1.9 | 1.6 | 13 | .1 | .1 | .3 | 15 | .10 | .022 | 31 | 9.6 | .25 | 88 | .011 | <1 | .92 | .004 | .06 | .1 | .02 | .9 | .1 | <.05 | 4 | <.5 | 7.5 |
| 1880 150E | .4 | 9.0 | 6.5 | 36 | <.1 | 9.1 | 4.9 | 127 | 2.07 | 3.1 | .8 | 16.3 | 6.5 | 4 | <.1 | .1 | .3 | 11 | .04 | .028 | 26 | 9.5 | .33 | 28 | .011 | 1 | .85 | .002 | .04 | .1 | .03 | .8 | <.1 | <.05 | 2 | <.5 | 7.5 |
| 1880 175E | 1.2 | 14.7 | 17.8 | 53 | .2 | 12.2 | 9.2 | 246 | 2.56 | 4.5 | 1.6 | 7.2 | 6.3 | 6 | .3 | .2 | .4 | 24 | .04 | .049 | 27 | 12.0 | .34 | 61 | .026 | <1 | 2.09 | .004 | .06 | .2 | .08 | 1.6 | .1 | <.05 | 8 | <.5 | 15.0 |
| 1880 200E | .7 | 11.5 | 11.6 | 64 | .2 | 10.4 | 8.4 | 525 | 2.00 | 2.9 | .8 | .6 | 6.5 | 3 | .1 | .1 | .4 | 19 | .02 | .023 | 25 | 10.5 | .32 | 64 | .015 | <1 | 1.57 | .003 | .05 | .1 | .05 | 1.4 | .1 | <.05 | 5 | <.5 | 7.5 |
| 1880 225E | .5 | 9.4 | 10.1 | 55 | .1 | 11.7 | 7.4 | 192 | 2.13 | 3.2 | .7 | 1.2 | 7.5 | 3 | .1 | .1 | .3 | 17 | .02 | .034 | 22 | 9.4 | .35 | 72 | .019 | <1 | 1.94 | .004 | .05 | .1 | .04 | 1.3 | .1 | <.05 | 6 | <.5 | 15.0 |
| 1880 250E | .9 | 14.9 | 12.7 | 68 | .2 | 14.0 | 6.4 | 178 | 2.35 | 4.2 | 1.2 | .7 | 7.3 | 4 | .1 | .1 | .4 | 20 | .03 | .047 | 22 | 12.5 | .32 | 61 | .023 | <1 | 2.08 | .004 | .06 | .1 | .06 | 1.6 | .1 | <.05 | 6 | <.5 | 7.5 |
| 1880 275E | .8 | 11.7 | 12.2 | 53 | .1 | 12.6 | 6.1 | 145 | 2.35 | 4.0 | .9 | 1.2 | 8.0 | 5 | .1 | .1 | .4 | 20 | .04 | .035 | 24 | 10.5 | .40 | 55 | .022 | 1 | 1.74 | .005 | .06 | .1 | .04 | 1.5 | .1 | <.05 | 6 | <.5 | 15.0 |
| 1880 300E | .6 | 10.3 | 14.8 | 42 | .1 | 9.9 | 5.6 | 114 | 2.43 | 3.8 | .8 | 6.2 | 7.2 | 3 | .1 | .1 | .4 | 20 | .03 | .042 | 20 | 12.4 | .31 | 51 | .020 | <1 | 1.86 | .004 | .05 | .1 | .05 | 1.3 | .1 | <.05 | 6 | <.5 | 15.0 |
| STANDARD DS5 | 12.2 | 141.5 | 24.3 | 130 | .3 | 22.7 | 11.8 | 750 | 2.91 | 18.0 | 6.3 | 42.8 | 2.7 | 45 | 5.4 | 3.6 | 6.3 | 59 | .71 | .099 | 12 | 187.8 | .68 | 138 | .096 | 18 | 1.97 | .037 | .13 | 4.8 | .16 | 3.6 | 1.1 | <.05 | 7 | 5.0 | 15.0 |

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



Data ✓ FA ____

ACME ANALYTICAL

## Ruby Red Resources Inc. PROJECT EDDY FILE # A403684



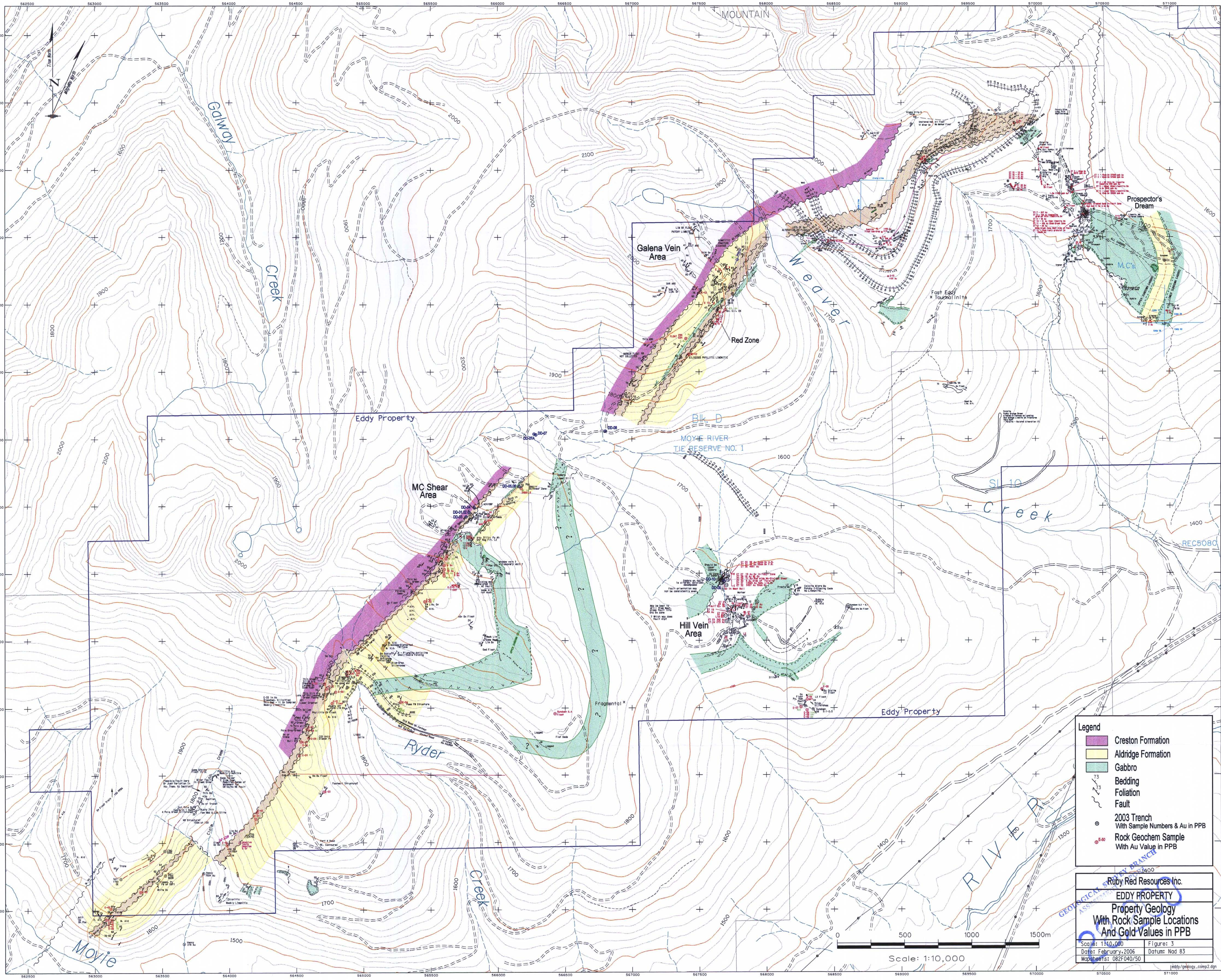
ACME ANALYTICAL

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppb | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Hg ppm | Sc ppm | Tl ppm | S % | Ga ppm | Se ppm | Sample gm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1880 325E | .6 | 11.0 | 13.0 | 49 | .1 | 10.6 | 7.6 | 221 | 2.41 | 3.0 | .8 | 2.1 | 4.4 | 9 | .2 | .1 | .4 | 24 | .11 | .040 | 25 | 13.5 | .41 | 62 | .020 | 1 | 1.25 | .006 | .06 | .1 | .02 | 1.5 | .1 | <.05 | 7 | <.5 | 7.5 |
| 1880 350E | .5 | 17.1 | 17.1 | 53 | .1 | 12.2 | 12.6 | 444 | 2.33 | 3.0 | 1.2 | 1.7 | 3.4 | 11 | .1 | .1 | .5 | 26 | .15 | .034 | 24 | 12.2 | .41 | 70 | .017 | <1 | 1.66 | .005 | .06 | .1 | .03 | 1.9 | .1 | <.05 | 6 | <.5 | 7.5 |
| 1880 375E | .7 | 11.1 | 14.6 | 51 | .2 | 10.5 | 6.2 | 154 | 2.64 | 3.7 | .7 | .7 | 4.6 | 4 | .1 | .1 | .4 | 26 | .05 | .033 | 20 | 12.9 | .33 | 62 | .028 | <1 | 1.78 | .006 | .04 | .1 | .05 | 1.5 | .1 | <.05 | 7 | <.5 | 15.0 |
| 1880 400E | .7 | 16.7 | 13.7 | 48 | .1 | 15.2 | 13.2 | 641 | 2.75 | 3.8 | 1.3 | .7 | 4.6 | 9 | .1 | .1 | .4 | 27 | .12 | .035 | 24 | 14.3 | .48 | 86 | .010 | 1 | 1.80 | .005 | .07 | .1 | .02 | 1.8 | .1 | <.05 | 6 | <.5 | 7.5 |
| 1880 425E | .6 | 11.4 | 10.4 | 41 | .1 | 11.3 | 7.7 | 174 | 2.31 | 4.1 | .8 | 1.0 | 7.5 | 3 | <.1 | .1 | .4 | 19 | .03 | .029 | 20 | 10.9 | .35 | 78 | .015 | <1 | 1.90 | .004 | .05 | .1 | .06 | 1.4 | .1 | <.05 | 5 | <.5 | 15.0 |
| 1880 450E | .4 | 5.7 | 6.6 | 26 | .1 | 5.8 | 3.5 | 137 | 1.56 | 1.4 | .5 | 9.9 | 4.4 | 3 | <.1 | .1 | .3 | 19 | .02 | .022 | 20 | 8.5 | .20 | 65 | .021 | <1 | 1.15 | .005 | .04 | .1 | .03 | 1.2 | .1 | <.05 | 5 | <.5 | 15.0 |
| 1880 475E | .8 | 9.5 | 9.1 | 40 | .1 | 9.8 | 7.5 | 176 | 2.05 | 2.5 | .7 | 1.6 | 4.3 | 4 | .1 | .1 | .3 | 26 | .03 | .055 | 18 | 9.6 | .20 | 83 | .049 | <1 | 2.03 | .009 | .04 | .1 | .08 | 2.0 | .1 | <.05 | 7 | <.5 | 7.5 |
| RE 1880 475E | .6 | 8.9 | 9.7 | 36 | .1 | 9.8 | 7.2 | 164 | 1.98 | 2.4 | .7 | 2.3 | 4.4 | 4 | .1 | .1 | .3 | 25 | .03 | .054 | 17 | 10.0 | .21 | 80 | .048 | <1 | 2.11 | .009 | .04 | .1 | .06 | 1.9 | .1 | <.05 | 7 | <.5 | 7.5 |
| 1880 500E | .5 | 10.1 | 11.3 | 34 | .1 | 14.2 | 12.2 | 145 | 2.49 | 3.4 | .9 | .8 | 4.8 | 9 | .1 | .2 | .4 | 34 | .12 | .024 | 21 | 12.3 | .22 | 85 | .036 | <1 | 1.84 | .008 | .05 | .1 | .02 | 2.1 | .1 | <.05 | 8 | <.5 | 15.0 |
| 1880 525E | .4 | 15.1 | 12.8 | 37 | .1 | 19.9 | 18.1 | 139 | 2.42 | 4.3 | .9 | 3.1 | 4.2 | 7 | .1 | .1 | .4 | 32 | .08 | .025 | 18 | 12.9 | .32 | 90 | .025 | <1 | 1.77 | .005 | .05 | .1 | .02 | 2.1 | .1 | <.05 | 6 | <.5 | 7.5 |
| 1880 550E | .7 | 10.2 | 10.1 | 43 | .1 | 11.5 | 16.4 | 125 | 2.45 | 3.3 | .9 | 2.1 | 6.9 | 3 | <.1 | .1 | .3 | 28 | .02 | .060 | 13 | 12.0 | .23 | 77 | .042 | <1 | 2.81 | .008 | .05 | .1 | .04 | 2.0 | .1 | <.05 | 6 | <.5 | 7.5 |
| 1880 575E | .8 | 10.6 | 9.5 | 38 | <.1 | 14.8 | 20.5 | 164 | 2.08 | 4.1 | 1.3 | 2.2 | 6.7 | 4 | .1 | .2 | .3 | 27 | .03 | .103 | 11 | 10.6 | .21 | 71 | .056 | 1 | 3.28 | .008 | .04 | .2 | .07 | 2.8 | .1 | <.05 | 7 | <.5 | 15.0 |
| 1880 600E | 1.0 | 11.6 | 13.8 | 51 | .1 | 15.3 | 22.6 | 867 | 2.56 | 3.9 | .9 | 2.5 | 5.5 | 4 | .1 | .2 | .4 | 33 | .03 | .064 | 11 | 14.6 | .24 | 76 | .077 | 1 | 3.79 | .009 | .04 | .2 | .06 | 2.4 | .1 | <.05 | 8 | <.5 | 15.0 |
| STANDARD DS5 | 12.3 | 136.9 | 25.1 | 131 | .3 | 24.4 | 11.5 | 734 | 3.03 | 17.7 | 6.4 | 45.4 | 2.7 | 44 | 5.6 | 3.8 | 6.4 | 61 | .75 | .103 | 13 | 175.5 | .70 | 133 | .089 | 18 | 1.95 | .031 | .12 | 4.8 | .18 | 3.4 | 1.1 | <.05 | 7 | 4.6 | 15.0 |

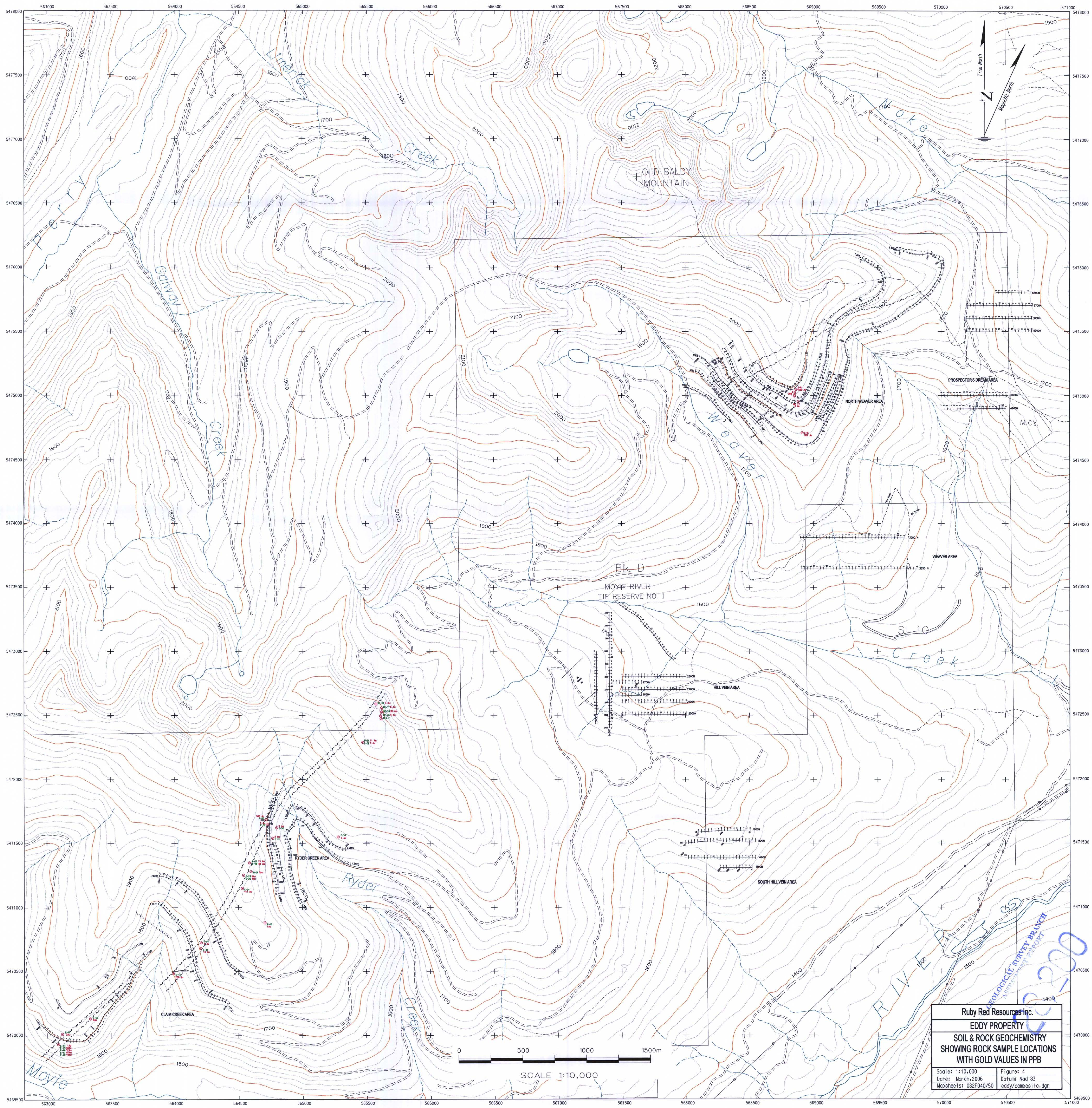
Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

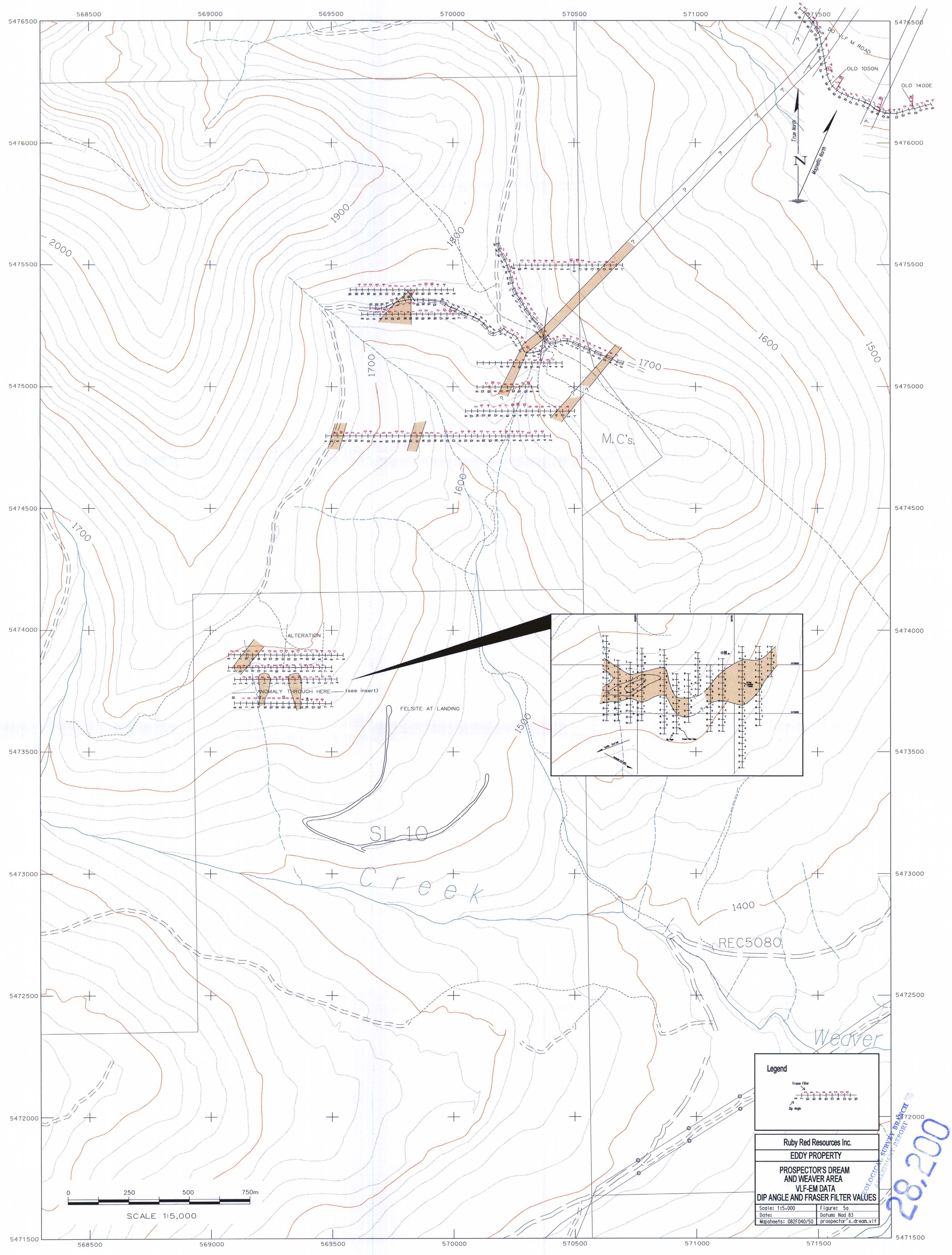


Data ___ FA ___



MOUNTAIN
Galway
Creek
Weaver
Galena Vein
Area
Red Zone
Prospector's
Dream
M.C's
Fast Eddy
x Tourmaline
Eddy Property
Blk. D
MOYIE RIVER
TIE RESERVE NO. 1
MC Shear
Area
Hill Vein
Area
SL 10
Creek
REC5080
Ryder
Creek
Moyie
RIVER
Fragmental
Legend
Creston Formation
Aldridge Formation
Gabbro
Bedding
Foliation
Fault
2003 Trench
With Sample Numbers & Au in PPB
Rock Geochem Sample
With Au Value in PPB
Ruby Red Resources Inc.
EDDY PROPERTY
Property Geology
With Rock Sample Locations
And Gold Values in PPB
Scale: 1:10,000
Figure: 3
Date: February,2006
Datum: Nad 83
Mapsheets: 082F040/50
eddy/geology_comp2.dgn
0
500
1000
1500m
Scale: 1:10,000
GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT


True North
Magnetic North
N
OLD BALDY MOUNTAIN
Limerick Creek
Perry
Galway Creek
Weaver
Creek
Ryder Creek
Moyie
RIVER
Blk. D
MOYIE RIVER
TIE RESERVE NO. 1
SL 10
NORTH WEAVER AREA
PROSPECTOR'S DREAM AREA
M.C's.
WEAVER AREA
HILL VEIN AREA
SOUTH HILL VEIN AREA
RYDER CREEK AREA
CLAIM CREEK AREA
0
500
1000
1500m
SCALE 1:10,000
GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT
Ruby Red Resources Inc.
EDDY PROPERTY
SOIL & ROCK GEOCHEMISTRY
SHOWING ROCK SAMPLE LOCATIONS
WITH GOLD VALUES IN PPB
Scale: 1:10,000
Figure: 4
Date: March,2006
Datum: Nad 83
Mapsheets: 082F040/50
eddy/composite.dgn



568500
569000
569500
570000
570500
571000
571500
5476500
5476000
5475500
5475000
5474500
5474000
5473500
5473000
5472500
5472000
5471500
OLD 1050N
OLD 1400E
VLF M ROAD
True North
Magnetic North
2000
1900
1800
1700
1600
1500
1400
M.C's.
ALTERATION
ANOMALY THROUGH HERE (see insert)
FELSITE AT LANDING
SL 10
Creek
REC5080
Weaver
Legend
Fraser Filter
Dip Angle
Ruby Red Resources Inc.
EDDY PROPERTY
PROSPECTOR'S DREAM
AND WEAVER AREA
VLF-EM DATA
DIP ANGLE AND FRASER FILTER VALUES
Scale: 1:5,000
Figure: 5a
Date:
Datum: Nad 83
Mapsheets: 082F040/50
prospector's_dream_vlf
0 250 500 750m
SCALE 1:5,000
GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT
28,200


Ruby Red Resources Inc.

EDDY PROPERTY

VLF-EM DATA
MC2 & HILL VEIN AREAS
DIP ANGLE AND FRASER FILTER VALUES

| | |
|---|---|
| Scale: 1:5,000 | Figure: 5b |
| Date: | Datum: Nad 83 |
| Mapsheets: 082F040/50 | hill_vein_vlf.dgn |