

Eddy Claims

Fort Steele Mining Division B.C.G.S. 082 F040 and 050, G041 Latitude 50° 07' 30", Longitude 115° 52' 00"

> for Ruby Red Resources Inc. Suite 207, 239 - 12th Ave. SW Calgary, Alberta T2P 1H6

> > Submitted by:

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Submitted: March, 2005



SUMMARY

The Eddy property is located approximately 27 km southwest of Cranbrook, BC on the west side of the Moyie River, one of the prolific gold placers in the area. A summary total of total gold production from the BC provincial MINFILE database documents 285,895 grams of gold recovered from 53,901 tonnes mined for a average value of 5.30 g/t from the Moyie placer workings. To date, no significant lode source has been located for the placer gold although a number of gold-bearing mineralized occurrences identified within the Moyie River drainage.

The Eddy property was acquired by Ruby Red Resources Inc. in 2002 and subsequently expanded by the acquisition of the Prospector's Dream claims and now consists of 2,800 ha (6,919 acres), comprised of 92 2-post and 1 4-post (MGS) claim. The property extends from the North Fork of the Moyie River, northeast to Noke Creek on TRIM mapsheets 082F040, 050 and 082G041.

Exploration on the property was first documented in the 1890's with work in the Prospector's Dream area and evidence of previous work remains in the form of old workings, including adits, shafts and trenches. Many of the old workings have slumped or are caved, while many of the old trenches have been back-filled.

Recent programs over the past 20 years are reasonably well documented in the Assessment files and comprise the basis for this report. Analytical data for a total of 19 heavy mineral samples, 322 rocks and 1779 soils were compiled for this report, many of which have had UTM coordinates determined to facilitate plotting of the data. All data available were included in the geochemical database for the purposes of determining a correlation matrix to assess inter-element dependencies and associations. In addition, the data for a total of 1333 VLF stations were compiled, comprised of Dip Angle and Fraser Filter values. Finally, the data from a 1995 gravity survey was compiled, comprised of readings from 540 stations. These data are considered to be a variable usefulness, in the following order, Heavy Mineral samples, rock samples, soils samples, VLF-EM data and gravity. Gravity, based on the 1995 survey and subsequent drill results is interpreted to indicate the presence of mafic gabbro sills and possibly base metals veins. It is not believed to have much application in exploration for auriferous quartz veins and shears.

Gold is hosted in quartz veins associated with shears and faults on the property. Five main areas have been identified on the basis of previous work, including the Prospector's Dream, Red Zone, Weaver No. 2 M.C. (MC Shear), Galena Vein and Hill Zone. Visible gold has been noted in association with pyrite and limonite within or immediately adjacent to quartz veins / shear zones. The shear zones are generally oriented sub-parallel to the Old Baldy Fault System (OBFS), a northeast trending shear zones with a number of splays and en echelon faults. There is also at least one set of cross-cutting faults that have been identified on the basis of regional mapping.

The stratigraphy underlying the property belongs the middle Aldridge and Creston Formations, with the OBFS cross-cutting stratigraphically upward at the southern extent of the property and subsequently localized at the stratigraphic level of the contact between Ryder and Noke Creek. A number of felsic intrusions have been identified within the property, comprised of "syenitic" dykes and sills. They are most probably correlated to the Bayonne Magmatic Suite of Cretaceous age, analogous to the Kiakho Stock and Reade Lake Pluton to the north.

Limited analysis of the geochemical data compiled suggests there may be a magmatic component to the samples, interpreted to arise from the presence and influence of the Cretaceous intrusions within and adjacent to the property. Moderate to strong correlations were identified in the data in both soils and, in particular, rock sample analyses for Ag-As-Au-Bi-Sb-W, which is an association proposed as characteristic of the intrusion-related gold model. On the basis of this elemental association and the local presence of Cretaceous felsic intrusions, as well as the documented presence of gold in both lode and placer occurrences within, and immediately adjacent to, the property, infiltration of magmatic fluids into pre-existing regional faults, such as the Moyie and St. Mary Faults, is proposed as a source of gold. Further work will need to evaluate the validity of this proposed model.

Table of Contents

.

-,

.....

.

F

1.0 Introduction 1 2.0 Property Description and Location 5 3.0 Physiography and Climate 9 4.0 History 9 5.0 Geological Setting 14 5.1 Regional Geology 14 5.1.1 Stratigraphy 14 5.1.2 Proterozoic 14 5.1.2 Proterozoic 14 5.1.2.1 Aldridge Formation 14 5.1.2.1.1 Laminated Siltstone Markers 14 5.1.2.1.1 Laminated Siltstone Markers 14 5.1.2.1 Laminated Siltstone Markers 14 5.1.2.1 Intrusives 16 5.1.2.1 Proterozoic 16 5.1.2.1 Proterozoic 16 5.1.2.2.1 Boyie Sills 16 5.1.2.2.1 Boyie Sills 16 5.1.2.2.1 Granitic Intrusions 17 5.1.2 Local Geology 19 5.3 Property Geology 20 5.3.1.1 Shear - Controlled Gold Deposits 21		Summ	arv			i
	1.0		-			
4.0 History 9 5.0 Geological Setting 14 5.1 Regional Geology 14 5.1.1 Stratigraphy 14 5.1.2 Proterozoic 14 5.1.2 Proterozoic 14 5.1.2 Proterozoic 14 5.1.2 Intrustrigge 14 5.1.2.1 Middle Aldridge 14 5.1.2.1 Luminated Siltstone Markers 14 5.1.2.1 Duper Aldridge 15 5.1.2.1 Duper Aldridge 15 5.1.2.1 Intrustrives 16 5.1.2.1 Proterozoic 16 5.1.2.1 Proterozoic 16 5.1.2.1 Moyie Sills 16 5.1.2.2 Mesozoic 17 5.1.3 Structure 17 5.2 Local Geology 19 5.3 Property Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1.1 Shaer-Controlled Gold Deposits 21 5.3.1.2 David 21						
14 14 5.0 Geological Setting 14 5.1 Regional Geology 14 5.1.1 Stratigraphy 14 5.1.2 Proterozoic 14 5.1.2 Proterozoic 14 5.1.2 Stratigraphy 14 5.1.2 Proterozoic 14 5.1.2.1 Middle Aldridge 14 5.1.2.1.1 Middle Aldridge 14 5.1.2.1.1 Middle Aldridge 14 5.1.2.1.1 Proterozoic 16 5.1.2.1 Intrusives 16 5.1.2.1 Intrusives 16 5.1.2.1 Proterozoic 16 5.1.2.1 Moyie Sills 16 5.1.2.1 Moyie Sills 16 5.1.2.2 Messozoic 17 5.1.3 Structure 17 5.1.4 Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1 Identified Areas of Mineralization 20 5.3.1.1 Shacovery / Shadow Vein 22						-
5.1 Regional Geology 14 5.1.1 Stratigraphy 14 5.1.2 Proterozoic 14 5.1.2 Proterozoic 14 5.1.2.1 Aldridge Formation 14 5.1.2.1 Aldridge Formation 14 5.1.2.1.1 Laminated Siltstone Markers 14 5.1.2.1.2 Upper Aldridge 15 5.1.2.1 Intrusives 16 5.1.2.1 Intrusives 16 5.1.2.1 Proterozoic 16 5.1.2.1 Proterozoic 16 5.1.2.1 Intrusives 16 5.1.2.1 Proterozoic 17 5.1.2.2 Mayie Sills 16 5.1.2.2.1 Granitic Intrusions 17 5.1.2.2 Local Geology 19 5.3 Property Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vei						
5.1.1 Stratigraphy 14 5.1.2 Proterozoic 14 5.1.2.1 Aldridge Formation 14 5.1.2.1.1 Middle Aldridge 14 5.1.2.1.1 Laminated Siltstone Markers 14 5.1.2.1.2 Upper Aldridge 15 5.1.2.1 Intrusives 16 5.1.2.1 Proterozoic 16 5.1.2.1 Granitic Intrusions 17 5.1.2.2.1 Granitic Intrusions 17 5.1.3 Structure 17 5.1.2 Local Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 23 5.3.1.6 Galena Vein 23 5.3.1.7 Prospector	5.0					
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		J.1	+		+	
5.1.2.1 Aldridge Formation 14 5.1.2.1.1 Middle Aldridge 14 5.1.2.1.2 Upper Aldridge 15 5.1.2.1.2 Upper Aldridge 15 5.1.2.1.2 Upper Aldridge 16 5.1.2.1 Proterozoic 16 5.1.2.1 Proterozoic 16 5.1.2.1 Proterozoic 16 5.1.2.1 Proterozoic 17 5.1.2.1 Granitic Intrusions 17 5.1.2 Local Geology 19 5.3 Property Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 23 5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.1 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26			5.1.1	517	Droterozoic	
5.1.2.1.1 Middle Aldridge 14 5.1.2.1.1 Laminated Siltstone Markers 14 5.1.2.1.2 Upper Aldridge 15 5.1.2.1 2 Upper Aldridge 15 5.1.2.1 2 Upper Aldridge 16 5.1.2.1 Proterozoic 16 5.1.2.1 Moyie Sills 16 5.1.2.1 Moyie Sills 16 5.1.2.1 Moyie Sills 16 5.1.2.1 Moyie Sills 16 5.1.2.2 Mesozoic 17 5.1.2.1 Granitic Intrusions 17 5.1.3 Structure 17 5.2 Local Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1.1 Shear-Controlled Gold Deposits 21 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26				J.1.2		
5.1.2.1.1.1 Laminated Siltstone Markers 14 5.1.2.1 2 Upper Aldridge 15 5.1.2.1 Creston Formation 15 5.1.2.1 Intrusives 16 5.1.2.1 Proterozoic 17 5.1.2.2 Mesozoic 17 5.1.2.2.1 Granitic Intrusions 17 5.1.3 Structure 17 5.2 Local Geology 20 5.3 Property Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 23 5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1 Heavy Minerals 26 6.1.1 Ryder Creek 26						
5.1.2.1.2 Upper Aldridge 15 5.1.2.2 Creston Formation 15 5.1.2 Intrusives 16 5.1.2.1 Proterozoic 16 5.1.2.1 Moyie Sills 16 5.1.2.2 Mesozoic 17 5.1.3 Structure 17 5.1.4 Granitic Intrusions 17 5.1.3 Structure 17 5.1 Local Geology 19 5.3 Property Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1.1 Shear-Controlled Gold Deposits 21 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1.1 Ryder Creek 26 6.1.2 W						
5.1.2.2 Creston Formation 15 5.1.2 Intrusives 16 5.1.2.1 Proterozoic 16 5.1.2.1 Proterozoic 16 5.1.2.1 Proterozoic 16 5.1.2.1 Moyie Sills 16 5.1.2.2 Mesozoic 17 5.1.2.2 Mesozoic 17 5.1.3 Structure 17 5.2 Local Geology 19 5.3 Property Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1 Identified Areas of Mineralization 20 5.3.1.2 David 21 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26						
5.1.2 Intrusives 16 5.1.2.1 Proterozoic 16 5.1.2.1 Moyie Sills 16 5.1.2.2 Mesozoic 17 5.1.2.1 Granitic Intrusions 17 5.1.2.2.1 Granitic Intrusions 17 5.1.3 Structure 17 5.1.4 Geology 19 5.3 Property Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1.1 Shear-Controlled Gold Deposits 21 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Gelana Vein 23 5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 26 6.1.1 Heavy Minerals 26 26						
5.1.2.1 Proterozoic 16 5.1.2.1.1 Moyie Sills 16 5.1.2.2 Mesozoic 17 5.1.2.2.1 Granitic Intrusions 17 5.1.3 Structure 17 5.2 Local Geology 19 5.3 Property Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1.1 Shear-Controlled Gold Deposits 21 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 22 5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26			C 1 O	T (1		
5.1.2.1.1 Moyie Sills 16 5.1.2.2 Mesozoic 17 5.1.2.2.1 Granitic Intrusions 17 5.1.3 Structure 17 5.2 Local Geology 19 5.3 Property Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1 Identified Areas of Mineralization 20 5.3.1.1 Shear-Controlled Gold Deposits 21 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 22 5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 26 6.1.1 Ryder Creek 26 26 6.1.2 Weaver Creek 26			5.1.2			
5.1.2.2 Mesozoic 17 5.1.2.2.1 Granitic Intrusions 17 5.1.3 Structure 17 5.2 Local Geology 19 5.3 Property Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1.1 Shear-Controlled Gold Deposits 21 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 22 5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26				5.1.2.1		
5.1.2.2.1 Granitic Intrusions 17 5.1.3 Structure 17 5.2 Local Geology 19 5.3 Property Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1.1 Shear-Controlled Gold Deposits 21 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 22 5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26					•	
5.1.3 Structure 17 5.2 Local Geology 19 5.3 Property Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1.1 Shear-Controlled Gold Deposits 21 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 22 5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26 26 26				5.1.2.2		
5.2 Local Geology 19 5.3 Property Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1.1 Shear-Controlled Gold Deposits 21 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 22 5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.9 Shadow Vein 25 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC 6.0 Geochemical Database 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26						
5.3 Property Geology 20 5.3.1 Identified Areas of Mineralization 20 5.3.1 Identified Areas of Mineralization 20 5.3.1 Shear-Controlled Gold Deposits 21 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 22 5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26						
5.3.1 Identified Areas of Mineralization 20 5.3.1.1 Shear-Controlled Gold Deposits 21 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 22 5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC 6.0 Geochemical Database 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26		5.2		-	r	
5.3.1.1 Shear-Controlled Gold Deposits 21 5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 22 5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26		5.3				
5.3.1.2 David 21 5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 22 5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26			5.3.1			
5.3.1.3 Discovery / Shadow Vein 22 5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 22 5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1 Heavy Minerals 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26				5.3.1.	Shear-Controlled Gold Deposits	
5.3.1.4 Fast Eddy 22 5.3.1.5 Galena Vein 22 5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1 Heavy Minerals 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26				5.3.1.2	2 David	
5.3.1.5 Galena Vein 22 5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1 Heavy Minerals 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26				5.3.1.2	B Discovery / Shadow Vein	
5.3.1.6 Hill Vein 23 5.3.1.7 Prospector's Dream 23 5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1 Heavy Minerals 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26				5.3.1.4	Fast Eddy	22
5.3.1.7 Prospector's Dream 23 5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1 Heavy Minerals 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26				5.3.1.3	5 Galena Vein	22
5.3.1.8 Red Zone 24 5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1 Heavy Minerals 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26				5.3.1.0	5 Hill Vein	23
5.3.1.9 Shadow Vein 25 5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1 Heavy Minerals 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26				5.3.1.	7 Prospector's Dream	23
5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1 Heavy Minerals 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26				5.3.1.	Red Zone	24
5.3.1.10 Weaver No. 2 MC Shear 25 6.0 Geochemical Database 26 6.1 Heavy Minerals 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26				5.3.1.	9 Shadow Vein	25
6.0Geochemical Database266.1Heavy Minerals266.1.1Ryder Creek266.1.2Weaver Creek26				5.3.1.	10 Weaver No. 2 MC Shear	25
6.1 Heavy Minerals 26 6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26	6.0	Geoch	nemical	Databas	;e	26
6.1.1 Ryder Creek 26 6.1.2 Weaver Creek 26						26
6.1.2 Weaver Creek			-			26
				-		26
0.1.3 NOTTH FORK Weaver Ureek			6.1.3		Fork Weaver Creek	27
6.1.4 Weaver Creek						
6.2 Soil Samples		62				

.

		6.2.1	Ag	28
		6.2.2	AĪ	28
		6.2.3	Bi	28
		6.2.4	Со	31
		6.2.5	Cr	31
		6.2.6	Sb	31
	6.3	Rock	Samples	31
		6.3.1	Ag	31
		6.3.2	As	32
		6.3.3	Au	32
		6.3.4	Bi	32
		6.3.5	Со	32
		6.3.6	Zn	32
7.0	Geopl	hysics		35
	7.1	Gravit	y	35
	7.2			35
8.0	Discu	ssion		36
	8.1	Depos	sit Types	36
		-	Veins	36
	8.2	Explo	ration Model	39
		8.2.1	Factors Contributing to Mineralization	39
	8.3	Gold I	Index	40
		8.3.1	Prospector's Dream	40
		8.3.2	Northwest of Prospector's Dream	40
		8.3.3	Galena Vein	41
		8.3.4	Weaver No. 2 M.C.	41
		8.3.5	South Baldy Shear	41
9.0	Concl			42
10.0			tions	44
11.0				46

.

,

iv

List of Figures

	Page
Figure 1 - Regional Location Map	2
Figure 2 - Property Location Map	3
Figure 3 - Local Geology Map	4
Figure 4 - Claim Map (1:20,000 scale)	6
Figure 5 - Eddy Compilation Map	In Back Pocket
Figure 6 - VLF-EM Map	In Back Pocket
Figure 7 - Gold Index Map	In Back Pocket

Tables *

Table 1: Placer Gold Production from Fort Steele Mining Division	10
Table 2: MINFILE Record of Production for Moyie Placer	.11
Table 3: Mean and Standard Deviation for Soil database	29
Table 4: Correlation matrix for Soil database	30
Table 5: Mean and Standard Deviation for Rock database	- 33
Table 6: Correlation matrix for Rock database	34

List of Appendices

Appendix A - Statement of Qualifications Appendix B - Excerpts from the Minister of Mines and MINFILE Reports

Appendix C - Compilation of Analytical Results

- Soil Analytical Results

- Rock Analytical Results

- VLF-EM Results

- Gravity Data

Appendix D - Statement of Expenditures Appendix E - Program - Related Documents

1.0 INTRODUCTION

The Eddy property is located approximately 27 km southwest of Cranbrook, BC (Fig. 1 and 2) on the west side of the Moyie River (Fig. 3), one of the prolific gold placers in the area. A summary of total gold production from the BC provincial MINFILE database documents 285,895 grams of gold recovered from 53,901 tonnes mined for a average value of 5.30 g/t from the Moyie placer workings. To date, no significant lode source has been located for the placer gold although a number of gold-bearing mineralized occurrences identified within the Moyie River drainage.

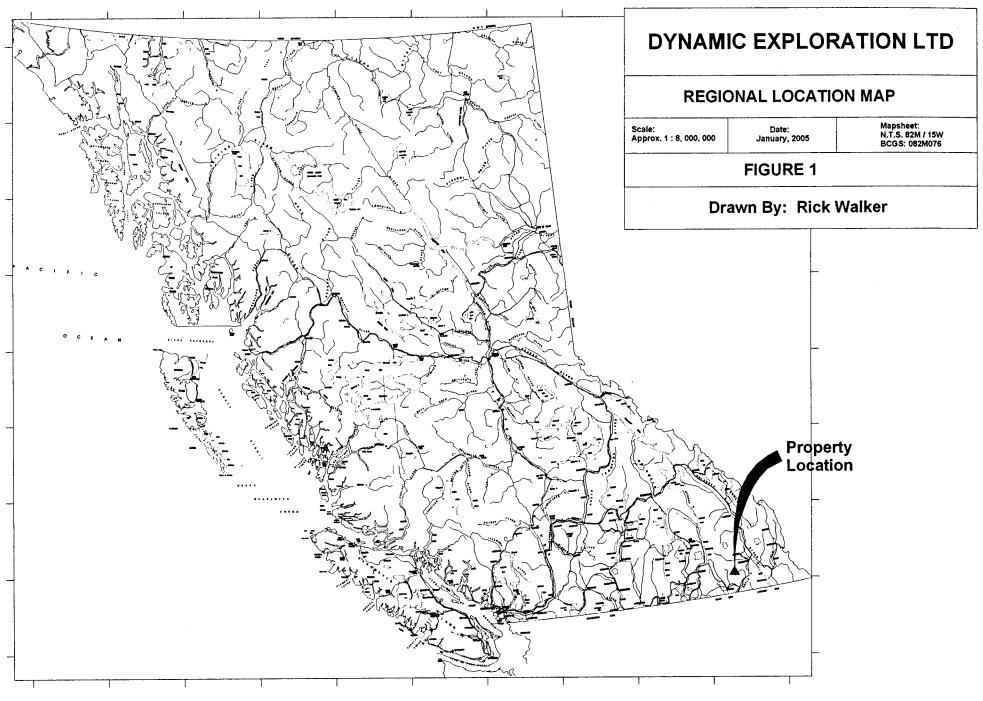
The Eddy property was acquired by Ruby Red Resources Inc. in 2002 and subsequently expanded by the acquisition of the Prospector's Dream claims and now consists of 2,800 ha (6,919 acres), comprised of 92 2-post and 1 4-post (MGS) claim (Fig. 4). The property extends from the North Fork of the Moyie River, northeast to Noke Creek on TRIM mapsheets 082F040, 050 and 082G041.

Exploration on the property was first documented in the 1890's with work in the Prospector's Dream area and evidence of previous work remains in the form of old workings, including adits, shafts and trenches. Many of the old workings have slumped or are caved, while many of the old trenches have been back-filled.

Recent programs over the past 20 years are reasonably well documented in the Assessment files and comprise the basis for this report. Analytical data for a total of 19 heavy mineral samples, 322 rocks and 1779 soils were compiled for this report, many of which have had UTM coordinates determined to facilitate plotting of the data. All data available were included in the geochemical database for the purposes of determining a correlation matrix to assess inter-element dependencies and associations. In addition, the data for a total of 1333 VLF stations were compiled, comprised of Dip Angle and Fraser Filter values. Finally, the data from a 1995 gravity survey was compiled, comprised of readings from 540 stations. These data (Fig. 5) are considered to be a variable usefulness, in the following order, Heavy Mineral samples, rock samples, soils samples, VLF-EM data and gravity. Gravity, based on the 1995 survey and subsequent drill results is interpreted to indicate the presence of mafic gabbro sills and possibly base metals veins. It is not believed to have much application in exploration for auriferous quartz veins and shears.

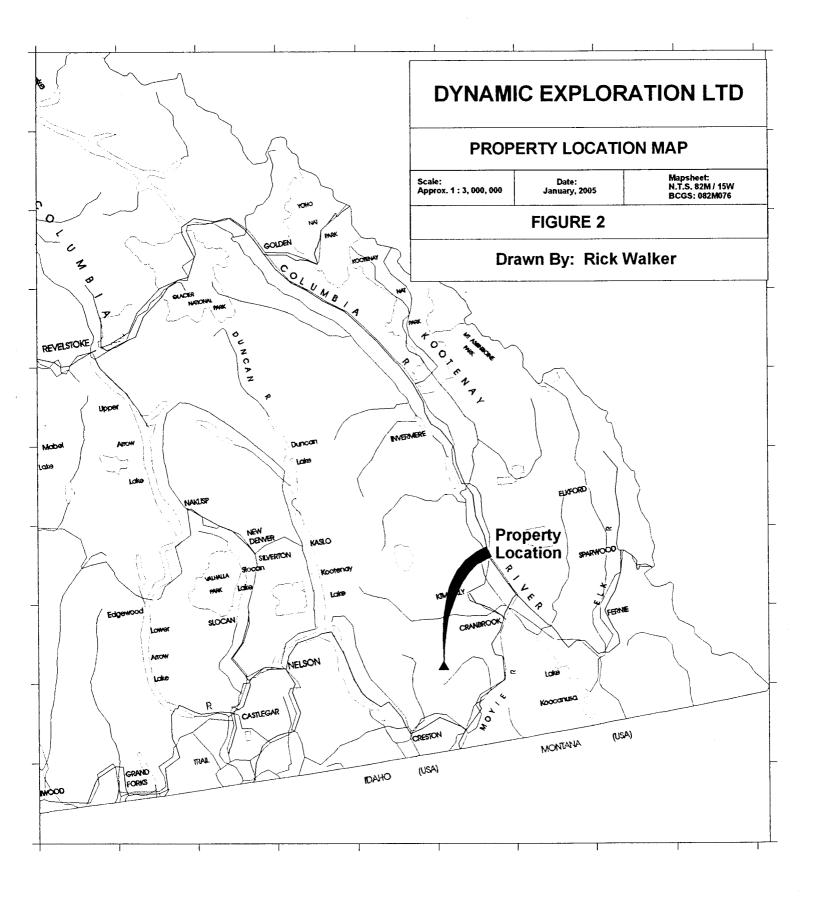
Gold is hosted in quartz veins associated with shears and faults on the property (Fig. 5). Five main areas have been identified on the basis of previous work, including the Prospector's Dream, Red Zone, Weaver No. 2 M.C. (MC Shear), Galena Vein and Hill Zone. Visible gold has been noted in association with pyrite and limonite within or immediately adjacent to quartz veins/shear zones. The shear zones are generally oriented sub-parallel to the Old Baldy Fault System (OBFS), a northeast trending shear zones with a number of splays and en echelon faults. There is also at least one set of cross-cutting faults that have been identified on the basis of regional mapping.

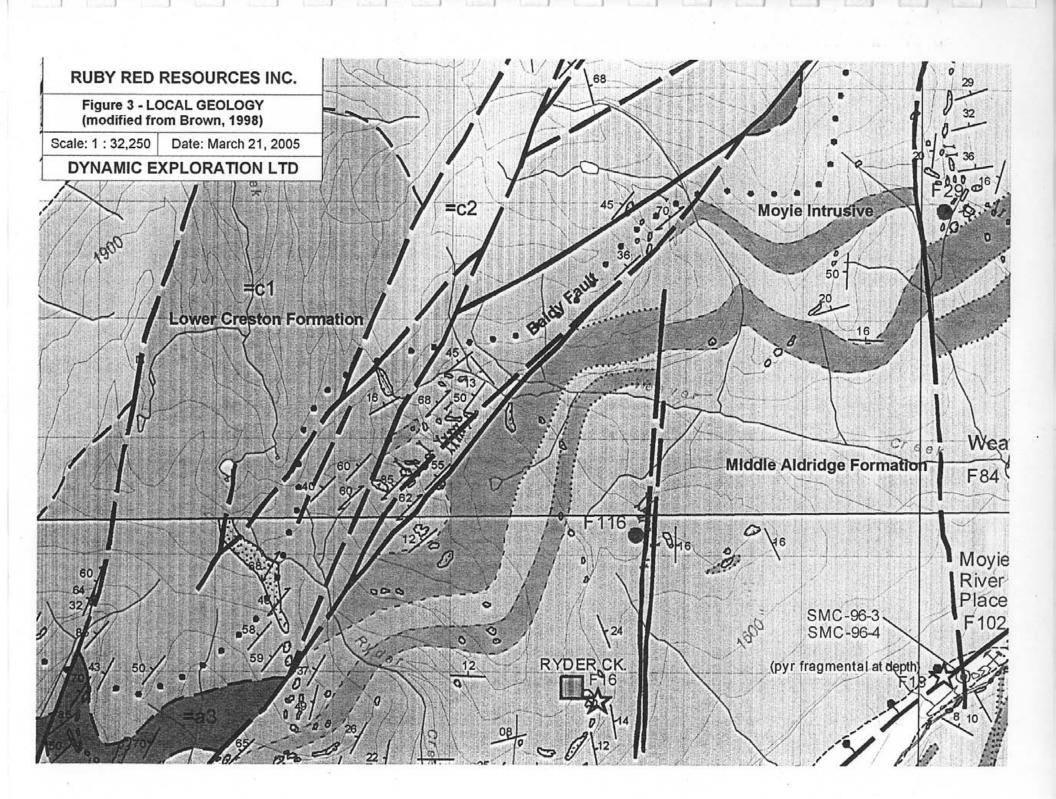
The stratigraphy underlying the property belongs the middle Aldridge and Creston Formations, with the OBFS cross-cutting stratigraphically upward at the southern extent of the property and subsequently localized at the stratigraphic level of the contact between Ryder and Noke Creek. A



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number of felsic intrusions have been identified within the property, comprised of "syenitic" dykes and sills. They are most probably correlated to the Bayonne Magmatic Suite of Cretaceous age, analogous to the Kiakho Stock and Reade Lake Pluton to the north.

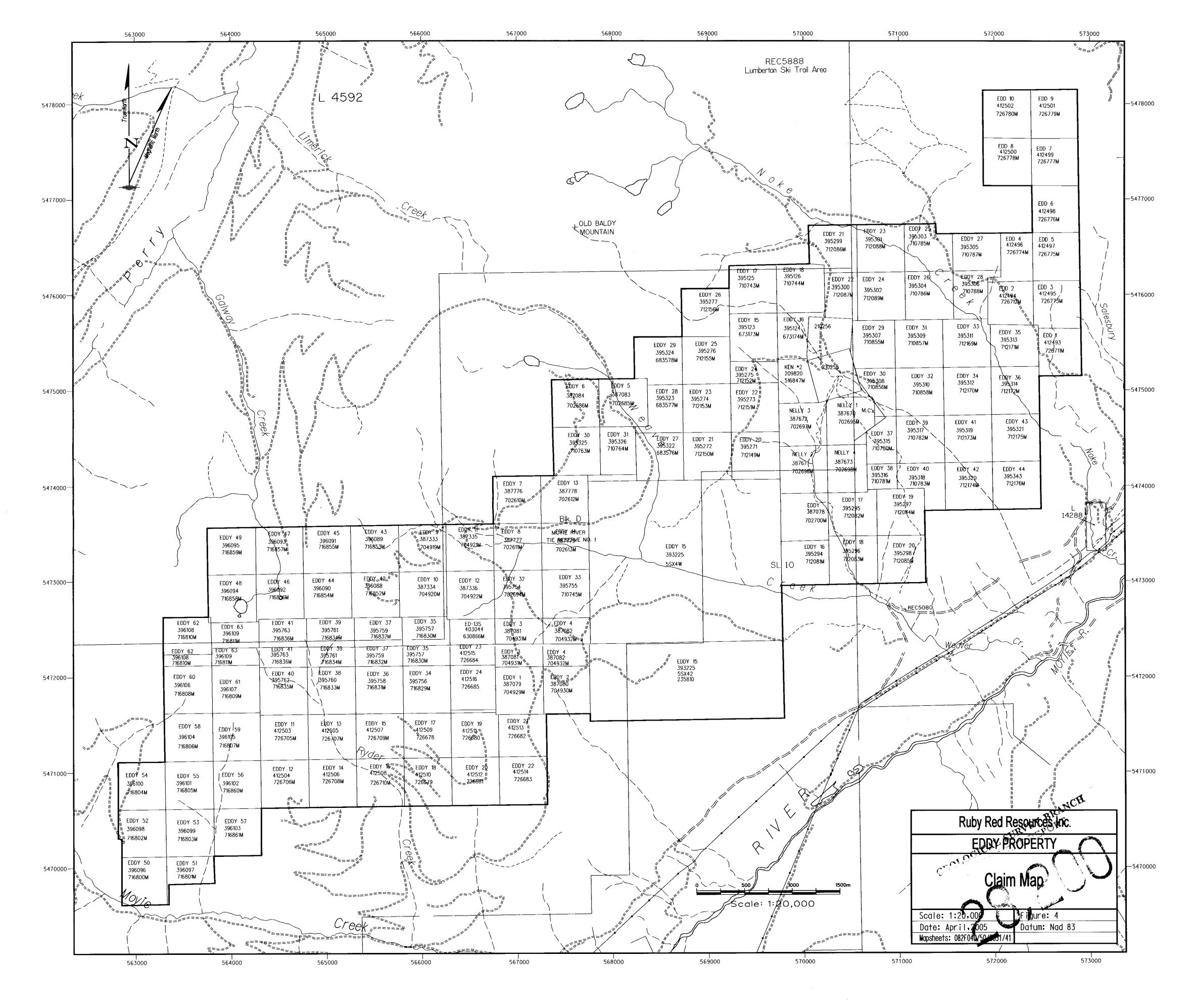
Limited analysis of the geochemical data compiled suggests there may be a magmatic component to the samples, interpreted to arise from the presence and influence of the Cretaceous intrusions within and adjacent to the property. Moderate to strong correlations were identified in the data in both soils and, in particular, rock sample analyses for Ag-As-Au-Bi-Sb-W, which is an association proposed as characteristic of the intrusion-related gold model. On the basis of this elemental association and the local presence of Cretaceous felsic intrusions, as well as the documented presence of gold in both lode and placer occurrences within, and immediately adjacent to, the property, infiltration of magmatic fluids into pre-existing regional faults, such as the Moyie and St. Mary Faults, is proposed as a source of gold. A proprietary "Gold Index" was developed from the correlation matrix and applied to the geochemical data, both rock and soil, resulting in a strong spatial association between anomalous values and identified faults. Further work will need to evaluate the validity of this proposed model.

2.0 PROPERTY DESCRIPTION AND LOCATION

The property (Fig. 4) consists 2,800 ha (6,919 acres), located on TRIM mapsheets 082F040, 050 and 082G041, and is comprised of 92 2-post and 1 4-post (MGS) claim (see Figure 4), staked in accordance with existing government claim location regulations. Significant claim data has been taken from the Ministry of Energy and Mines Mineral Titles web-page and is summarized below:

The following 16 claims are held by Greg Ewonus on behalf of Ruby Red Resources Inc and consist entirely of 2-post claims.

Tenure	Claim	Map	Good To	Area
Number	Name	Number	Date	
387079	EDDY 1	082F040	2006/JUL/15	25
387080	EDDY 2	082F040	2006/JUL/15	25
395303	EDDY 25	082F050	2005/JUL/17	25
395304	EDDY 26	082F050	2005/JUL/17	25
395305	EDDY 27	082F050	2005/JUL/17	25
395306	EDDY 28	082F050	2005/JUL/17	25
387081	EDDY 3	082F040	2006/JUL/15	25
395311	EDDY 33	082F050	2005/JUL/17	25
395312	EDDY 34	082F050	2005/JUL/17	25
395313	EDDY 35	082F050	2005/JUL/17	25
395314	EDDY 36	082F050	2005/JUL/17	25
387082	EDDY 4	082F040	2006/JUL/15	25
395319	EDDY 41	082F050	2005/JUL/17	25



395320	EDDY 42	082F050	2005/JUL/17	25
395321	EDDY 43	082F050	2005/JUL/17	25
395343	EDDY 44	082F050	2005/JUL/17	25

The following 77 claims are held by Ruby Red Resources Inc and consist of 76 2-post claims and 1 4-post claim.

Tenure	Claim Name	Мар	Good To	Area
Number		Number	Date	
387078	EDDY	082F050	2005/JUL/15	25
387334	EDDY 10	082F050 ~	2006/JUL/15	25
387335	EDDY 11	082F050	2005/OCT/30	25
387336	EDDY 12	082F050	2005/JUL/15	25
387778	EDDY 13	082F050	2005/OCT/30	25
387779	EDDY 14	082F050	2005/OCT/30	25
393225	EDDY 15	082F050	2006/JUL/15	500
395123	EDDY 15	082F050	2007/JUL/05	25
395124	EDDY 16	082F050	2007/JUL/05	25
395294	EDDY 16	082F050	2005/JUL/16	25
395125	EDDY 17	082F050	2007/JUL/05	25
395295	EDDY 17	082F050	2005/JUL/16	25
395126	EDDY 18	082F050	2007/JUL/05	25
395296	EDDY 18	082F050	2005/JUL/16	25
395297	EDDY 19	082F050	2005/JUL/16	25
395271	EDDY 20	082F050	2005/JUL/10	25
395298	EDDY 20	082F050	2005/JUL/16	25
395272	EDDY 21	082F050	2005/JUL/10	25
395299	EDDY 21	082F050	2005/JUL/16	25
395273	EDDY 22	082F050	2005/JUL/10	25
395300	EDDY 22	082F050	2005/JUL/16	25
395274	EDDY 23	082F050	2005/JUL/10	25
395301	EDDY 23	082F050	2005/JUL/16	25
395275	EDDY 24	082F050	2005/JUL/10	25
395302	EDDY 24	082F050	2005/JUL/16	25
395276	EDDY 25	082F050	2005/JUL/10	25
395277	EDDY 26	082F050	2005/JUL/10	25
395322	EDDY 27	082F050	2005/JUL/29	25
395323	EDDY 28	082F050	2005/JUL/29	25
395307	EDDY 29	082F050	2005/JUL/16	25
395324	EDDY 29	082F050	2005/JUL/29	25
395308	EDDY 30	082F050	2005/JUL/16	25
395325	EDDY 30	082F050	2007/OCT/30	25
395309	EDDY 31	082F050	2005/JUL/16	25

395326	EDDY 31	l082F050	2005/JUL/29	25
395310	EDDY 32		2005/JUL/16	25
395754	EDDY 32		2005/JUL/30	25
395755	EDDY 33		2005/JUL/30	25
395756	EDDY 34	082F040	2005/AUG/01	
395757	EDDY 35	082F040	2005/AUG/01	
395758	EDDY 36	082F040	2005/AUG/01	
395315	EDDY 37	082F050	2005/JUL/17	25
395759	EDDY 37	082F040	2005/AUG/01	25
395316	EDDY 38	082F050	2005/JUL/17	25
395760	EDDY 38	082F040	2007/AUG/01	25
395317	EDDY 39	082F050	2005/JUL/17	25
395761	EDDY 39	082F040	2007/AUG/01	
395318	EDDY 40	082F050	2005/JUL/17	25
395762	EDDY 40	082F040	2007/AUG/01	
395763	EDDY 41	082F040	2007/AUG/01	
396088	EDDY 42	082F050	2005/AUG/10	
396089	EDDY 43	082F050	2005/OCT/29	25
396090	EDDY 44	082F050	2005/AUG/12	25
396091	EDDY 45	082F050	2005/OCT/29	25
396092	EDDY 46	082F050	2006/AUG/12	25
396093	EDDY 47	082F050	2007/OCT/29	25
396094	EDDY 48	082F050	2006/AUG/12	25
396095	EDDY 49	082F050	2006/OCT/29	25
387083	EDDY 5	082F050	2006/JUL/15	25
396096	EDDY 50	082F040	2006/AUG/15	25
396097	EDDY 51	082F040	2006/AUG/15	25
396098	EDDY 52	082F040	2006/AUG/15	25
396099	EDDY 53	082F040	2006/AUG/15	25
396100	EDDY 54	082F040	2006/AUG/15	25
396101	EDDY 55	082F040	2006/AUG/15	25
396102	EDDY 56	082F040	2006/AUG/15	25
396103	EDDY 57	082F040	2006/AUG/15	25
396104	EDDY 58	082F040	2006/AUG/17	25
396105	EDDY 59	082F040	2006/AUG/17	25
387084	EDDY 6	082F050	2006/OCT/30	25
396106	EDDY 60	082F040	2006/AUG/17	25
396107	EDDY 61	082F040	2006/AUG/17	25
396108	EDDY 62	082F040	2006/AUG/17	25
396109	EDDY 63	082F040	2006/AUG/17	25
387776	EDDY 7	082F050	2006/OCT/30	25
387777	EDDY 8	082F050	2006/OCT/30	25
387333	EDDY 9	082F050	2006/OCT/30	25

3.0 PHYSIOGRAPHY AND CLIMATE

The project area is located in the Purcell Mountains (Fig 1 and 2), approximately 25 kilometres southwest of Cranbrook, British Columbia, centred at UTM coordinates 567000 E, 5472000N. The claims comprising the Eddy property extend north from North Moyie Creek to Noke Creek on the west side of the Moyie River Drainage (Fig. 4).

Access to the property is available from the main Lumberton and Moyie Forest Service Roads and along a relatively well developed system of tributary roads along the North Moyie, Ryder, Weaver and Noke creek drainages. A number of skid roads and short exploration trails, some constructed during previous exploration programs, provide access to specific areas of exploration interest.

The coniferous forest consists predominantly of pine, fir and larch which has been actively logged over the past 30 years. A number of clear-cuts are present throughout the property in various stages of regeneration.

Relief on the property is generally moderate at lower to middle elevation areas, with high relief areas at upper elevations (Fig. 5). Elevation ranges from approximately 1400 m along Weaver Creek, near its confluence with the Moyie River, to 2300 m at the height of the drainage divide between Ryder and Galway creeks. Due to the location of the property within the core of the Purcell Mountains east of Kootenay Lake, the area is generally subject to moderately heavy accumulations of snow during the winter months. As a result, the property is available for exploration from mid-May to late October. However, 4WD vehicle supported diamond drilling can take place later into the year despite snow due the relatively extensive network of logging roads.

4.0 HISTORY

The area underlying the property have had a long history of exploration, dating back to the 1890's on the Prospector's Dream. The following history of the areas of interest on the property have been summarized from the literature.

There are three predominant drainages in the Cranbrook area from which significant placer gold has been recovered, specifically, Wild Horse Creek in the Rocky Mountains east of the Rocky Mountain Trench and Moyie River and Perry Creek on the west side of the Rocky Mountain Trench in the Purcell Mountains. A summary of reported placer gold production has been modified from Holland (1950) in Table 1.

Prospecting for lode gold sources for the placer gold in these drainages was extensive in the late 1800's and into the 1900's. The exploration focus was on quartz-hosted gold and many quartz veins were identified and tested, with some identified as gold-bearing. Limited production from a small number of these auriferous gold veins is documented in MINFILE. No significant lode gold production is known from the Eddy property, although a number of adits, shafts and declines, predominantly in the Prospector's Dream area, document previous work on these veins.

Year	Kiakho (Fis Creek	sh Lake)		Monville, oyea) River ¹	Perr	ry Creek ²	Weaver Creek		
	Ounces	Value \$	Ounces	Value \$	Ounces	Value \$	Ounces	Value \$	
1874-75			-3		7533	14050	-3	••••••	
1876-80			70	1300	576	10750	65	1200	
1881-85			1652	30832	670	12500	146	2700	
1886-90		·····	1008	18800	618	11515	493	9200	
1891-95			255	4750	386	7200	32	600	
1896-1900									
1901-05					14	260			
1906-10									
1911-15									
1916-20									
1921-25							22	400	
1926-30			6	112	16	298	1	19	
1931-35	81	1941	202	6177	142	3733			
1936-40	81	2682	1461	46479	152	4829			
1941-45	18	625	132	4581	11	382			
Totals	180	5248	4786	113031	3338	65517	759	14119	

Table 1: Placer Gold Production from Fort Steele Mining Division

1 - Includes production from Palmer Bar Creek.

2 - Includes production from Paris Creek.

3 - Production for 1874 from Perry and Weaver Creeks and Moyie River is combined with production from Wild Horse River.

Table 2: The MINFILE record for occurrence 082FSE102 (Moyie River) documents a total of 285,895 grams of gold recovered from 53,901 tonnes mined for a average value of 5.30 g/t. The documented recovery was as follows:

Production Year	Tonnes Mined	Tonnes Milled	Grams Recovered
1989	11468	11468	30509
1988	42433	42433	106542
1945			4105
1940			45437
1935			6282
1930			187
1895			7930
1890			31349
1885			51377
1880			2177

Many of the current areas of exploration interest were identified as a direct result of road building on behalf of forestry operations, particularly in 1982. A number of gold-bearing quartz veins were subsequently identified and formed the basis for successive exploration programs on the current Eddy property. Many of the auriferous quartz veins have been trenched, with at least 50 trenches documented in the literature (most with poor location data).

A brief summary of exploration for the Eddy claims, as documented in the BC Ministry of Energy and Mines Assessment Report Index System (ARIS) follows.

- 1979 access road put into the Prospector's Dream property
- 1981 Weaver claims staked by J. Kennelly after excavation for logging roads exposed extensive quartz veins and zones of alteration
- 1983 Prospector's Dream (Ken Group) and Weaver properties optioned to Fenway Resources Ltd - objective to create access for exploration program

- discovered four main zones of mineralization: Weaver No. 2 M.C. Shear, Galena Vein, Hill Vein and Baldy Shear

- program included: limited geological mapping, 18,562 m of road construction, 271 m. of trenching, 114 soil and 29 rock samples (assayed for Pb, Zn, Ag, Au) and 4100 m of magnetometer survey (Morris 1987)

1984 - Fenway Resources Ltd

- objective to further evaluation of mineralized zones discovered in 1983 program
- program included prospecting, 415 soil and 10 rock samples (ICP analysis, Au by AA)
- six mineralized areas geologically mapped
- Weaver No. 2 M.C. Shear returned 66% of the anomalous samples in program
- 1987 Fenway Resources Ltd Retained Weaver property
 - objective to further test mineralized areas from 1983 and 1984
 - program included diamond drilling, logging and sampling

- 456 m. of BQ core in fifteen holes on the Hill Vein (holes 1-3), Weaver N0. 2 M.C. Shear Area (holes 4-6) and the Galena Vein (holes 7-15), depth 54.3 m depth or less

"When the drill holes were plotted on the updated geological map derived from the 1990 program, it was found that a majority of the holes did not test the perceived structure, due to erroneous location of the drill collar and orientation. Some holes were recognized as redundant, duplicating the results from previous holes, while others were drilled vertically adjacent to the vertically dipping structure. The majority of the holes were drilled short depth ranging from 14.6 meters to 54.3 meters. It can be speculated that insufficient geologic control was employed in the layout of the drill holes" (Banting 1992).

- 1988 Prospector's Dream property returned to Ed Frost
- 1989 1:1,500 scale geological mapping of Prospector's Dream area with 7 grab samples analyzed for gold

- objective to test mineralization associated with the Prospector's Dream claims

1989 - Fenway Resources Ltd

- objective to continue evaluation of the mineralized zones at Galena vein, Hill vein and MC2 shear, as well as the Galway Creek area on the west side of the claims Program included prospecting; Geological Mapping; ground geophysics (6.7 km

Magnetometer, 3.4 km VLF-EM); 207 soil, 177 rock and 19 heavy mineral samples (31 element ICP + Au) and trenching (22 trenches) on the Weaver claims

- 1990 geological mapping, geophysics, soil and rock geochemistry and trenching on the Weaver Claims on three grids designated A-C - A - MC2 shear
 - B A/C fault
 - C A/C MC2 merger

- objective to extend the strike length of known mineralization associated with the MC2 and A/C faults

"The presence of gold mineralization from rock samples combined with the distinct NE - oriented quartz shear zones on trend with the high gold values obtained from Ryder Creek drainage are significant indicators of a favourable economic environment" (Banting 1992).

1991 - 12 trenches excavated in the Prospector's Dream area

- 32 samples - analysis of gold by fire assay, 2-for ICP

- 1992 26.7 km Magnetometer survey (15.4 km of reconnaissance survey plus 11.3 km of detailed survey at station spacing of 4 or 8 metres) undertaken on the Weaver Claims
 objective to test magnetic response along roads through mineralized areas
- 1995 Excel Geophysics Inc undertakes limited ground geophysical survey for J.E. Kennelly
 program includes 0.1 km of VLF-EM, 1.5 km of gravity, 0.8 km Mise-a-la-masse
 objective to use a variety of geophysical methods to test the possible sub-surface extent of lead zinc mineralization associated with outcrop at UTM 565910 E, 5472350 N into which a short adit had previously been driven
 - shadow maps from TRIM DEM to identify fault patterns

1996 - Excel Geophysics Inc. undertakes ground geophysical program for Kennelly

- program includes 14.2 km VLF-EM, 21.3 km gravity, 4 BQ drill holes totalling 269.4 m - objective to continue detailed testing of lead zinc vein at 565910 E, 5472350 N "... to determine the extent and location of the subsurface continuation of the galena outcrop, and to determine if similar bodies existed in the immediate area" (Jones 1996).

1998 - Glen Rodgers for Ed Frost (Prospector's Dream)

- eight 70 kg rock samples taken 2.0 m apart from Main Workings area, derived from bedrock over 1.5-2.0 m within auriferous shear zone which underlies gabbro sill.

- processed for recovery of gold bead to independently determine grade

- average 9.68 g/t gold

- also sampled 1.5 tonnes of material hand selected from ore grade stockpile, pieces chosen contained massive hematite with or without visible gold - recovered over 30 grams of gold - "Gold is visible within a quartz-hematite filled shear zone up to 1.5m wide which underlies the gabbro sill. Previous sampling gave values of up to 3 oz/t Au by fire assay with the mean being approximately 0.5 oz/t Au" (Rodgers 1998)

1999 - James Ryley and Michael Thompson - Shadow Claims (replaced Weaver 3, 4 and 8 claims)
 - reconnaissance prospecting
 objective to "... define the structural trend, determine stratigraphic position through the

collection of markers, and prospect for indicators of sedimentary exhalative and hydrothermal activity" (Ryley 1999).

2002 - Ruby Red Resources Inc acquired the Eddy property by staking, purchased Prospector's Dream claims from Ed Frost Prospecting and sampling 51 rock samples (32 element ICP + gold) on the Eddy Claims

2003 - geologic mapping, rock geochemistry (49 samples), contour soil geochemistry (250 samples) and trenching (17 trenches)
9 trenches - Prospector's Dream area - very high grade gold in trenches at 'Shaft prospect' 7 trenches - Hill Vein area - anomalous gold to 13565 ppb

2004 - geologic mapping, rock geochemistry (49 samples), contour and grid soil geochemistry (250 samples) and 7.6 km VLF-EM surveying

5.0 GEOLOGICAL SETTING

5.1 **REGIONAL GEOLOGY**

The publication by Höy (1993) represents a comprehensive review of the geology pertaining to the Femie West-Half mapsheet. The following has been taken from Höy (1993):

5.1.1 Stratigraphy

5.1.2 Proterozoic

5.1.2.1 Aldridge Formation

"Within the Purcell Mountains, it has been subdivided into three main divisions: the lower Aldridge comprises rusty weathering siltstone, quartz wacke and argillite; the middle Aldridge, grey weathering quartz wacke and siltstone interbedded with silty argillite; and the upper Aldridge, rusty to dark weathering laminated argillite and silty argillite ...

5.1.2.1.1 Middle Aldridge

The middle Aldridge comprises more than 2000 metres of dominantly well-bedded, medium to locally coarse-grained quartz arenite, wacke and siltstone. ...

A continuous section ... is not exposed in the Purcell Mountains; the most complete section, between the Moyie and Cranbrook faults, is broken by a number of faults. In general, the basal part comprises interbedded quartz wacke and arenite with only minor sections of silty argillite. Exposures of the basal part are typically grey weathering; however, in recent manmade exposures ... These units are typically rusty weathering. Within the upper part of the middle Aldridge, quartz arenite and quartz wacke beds become thinner and less pure, and the proportion of bedded siltstone and argillite increases. The upper part of the middle Aldridge comprises a number of distinct cycles of massive, grey quartz arenite beds that grade upward into an interlayered sequence of quartz wacke, siltstone and argillite, and are capped by siltstone and argillite. The contact with the upper Aldridge is placed above the last bed of massive grey quartz arenite. ...

5.1.2.1.1.1 Laminated Siltstone markers

The marker units are sequences of laminated dark, and siltstone, up to several metres thick, in which each laminae can be matched in precise detail for distances up to several hundred kilometres. The pattern of each laminae is each sequence in unique and hence recognition of a specific sequence of laminae allows accurate positioning of isolated outcrops or drill intersections within the thick middle Aldridge succession. At least fourteen of these marker sequences are recognized. Locally, the markers are interrupted by turbidity deposits, or partly or totally removed due to erosion by turbidity currents. ...

5.1.2.1.2 Upper Aldridge

The upper Aldridge Formation comprises about 500 ... metres of dominantly medium to dark grey siltstone, argillaceous siltstone and argillite. It is generally rusty weathering, thin bedded and thinly laminated. Thin graded ailtite-argillite couplets and lenticular bedding with tan siltstone lenses in argillite are common bed-forms; syneresis cracks are commonly observed near the top of the upper Aldridge. ...

The contact of the upper Aldridge with the Creston Formation is relatively abrupt, and is placed where green tinged siltite layers first appear. Elsewhere, a massive, thick-bedded siltstone or wacke marks the base of the Creston Formation...

5.1.2.2 Creston Formation

The following has been paraphrased from Höy (1993).

"The basal Creston Formation comprises several hundred metres of interlayered argillites, argillaceous siltstone and minor quartz wacke. It is generally grey to dark grey and rusty weathering near the base, but becomes green tinged upsection with increasing siltite component. Thinly laminated argillite or siltite, graded siltite-argillite couplets and lenticular-bedded siltstone are the most abundant bedforms; more massive medium-bedded quartz wacke is less common and brown-weathering silty dolomite layers are occasionally recognized. Syneresis cracks are common in the thin-bedded argillite and argillaceous siltite units.

The thick, middle part of the Creston Formation comprises mauve or green argillite and siltstone with variable amounts of more massive quartz wacke or arenite. Siltstone-argillite couplets, up to several centimetres thick, dominate the basal section of the middle Creston and differ from units in the basal section as they are commonly purple in colour, thicker bedded and contain abundant mud cracks. Lenses of massive to graded, green, purple, or white quartzite that may contain large tangential crossbeds or wavy, irregular laminations are inter-bedded with the purple siltstone. The quartzites commonly scour the underlying siltstone and may contain numerous rip-up clasts. Coarsening-upward cycles, with massive to laminated purple and green siltstone at the base and interlayered purple siltstone and white quartzite with crossbeds, rip-up clasts, scour-and-fill structures and graded beds at the top have been described at Premier Lake.

A prominent, thick, white orthoquartzite unit occurs near the middle of the middle Creston. It is medium to thick bedded and contains broad trough and tangential crossbeds and numerous rip-up clasts. The upper part of the quartzite unit comprises a number of coarsening-upward cycles, 3 to 10 metres thick, with purple and green siltstones at the base grading up through ripple cross-laminated siltstones and quartzites to massive thick-bedded quartzite at the top. Smaller fining-upward sequences are also common in the middle quartzite interval and overlying siltstone units.

Interbedded mauve siltstone and argillaceous siltstone, white quartz arenite and minor green siltstone overlie the white quartzite unit. Small fining-upward cycles are common, with massive to cross-bedded quartzites at the base and thin-bedded, mud-cracked and rippled argillite or siltstone at the top. Rip-up clasts, mud-chip breccias and some load casts occur throughout these units.

Higher in the succession, laminated green siltstone and graded siltstone-argillite couplets become prominent. Surfaces may be mud-cracked or rippled, but these structures are less prominent than in underlying units. Small fining-upward cycles are common, with thick-bedded, white or green quartzite or more massive siltstone at the base grading up into thinbedded siltite".

5.1.2 Intrusives

The following has been paraphrased from Höy (1993):

5.1.2.1 Proterozoic

5.1.2.1.1 Moyie Sills

The Moyie Sills (or Intrusives) comprise laterally extensive gabbro (to dioritic) sills which are restricted to the lower Aldridge and the lower part of the middle in the Purcell Mountains. The sills comprise up to 30 percent of the lower to middle Aldridge stratigraphic succession, having an aggregate thickness in excess of 2000 metres, with the abundance decreasing upwards relative to the abundance of thick-bedded A-E turbidites. In the Lamb Creek area west of Moyie Lake, (east of the Eddy property) an aggregate thickness of approximately 1300 metres of sills is interlayered with 2800 metres of lower and middle Aldridge sedimentary rock.

Moyie sills form an extensive suite of basaltic rocks that intruded lower and middle Aldridge turbidites and siltstones. ... Although it has been proposed that Moyie sills are coeval with deposition of upper Aldridge or Creston rocks, or perhaps with the Nicol Creek lavas, contact relationships between sills and Aldridge rocks indicate that some sills were extruded at very shallow depths in unconsolidated, water-saturated sediments. Others with fine-grained chilled margins have contact metamorphosed the country rocks. As these sills are interpreted to be part of a continuous magmatic event, they record an igneous/thermal event of regional extent during deposition of lower and middle Aldridge rocks. Hence, a Middle Proterozoic uranium-lead date of 1445 Ma from zircons in the Lumberton sill west of Cranbrook defines the minimum age of deposition of lower and basal middle Aldridge ...

5.1.2.2 Mesozoic

5.1.2.2.1 Granitic Intrusions

Cretaceous intrusives of broadly "granitic" composition are present in a belt extending from the westernmost Rocky Mountains to Kootenay Lake, northward to the Baldy Batholith. Intrusions range from small dykes and sills to larger intrusive complexes such as the Mt. Skelly Batholith and are collectively referred to as the Bayonne Magmatic Belt (or Suite).

"Intrusive rocks ... include a number of small post kinematic mesozonal quartz monzonite, monzonite and syenitic plutons, numerous small quartz monzonite to syenite dikes and sills probably related to these stocks, and late mafic dikes. The Kiakho and Reade Lake stocks, two of the larger of the mesozonal plutons, cut across and apparently seal two prominent east-trending faults that transect the eastern flank of the Purcell anticlinorium, and hence place constraints on the timing of latest movement on these faults.

The Kiakho stock is exposed on the heavily wooded slopes of Kiakho Creek approximately 10 kilometres (west-southwest) ... of Cranbrook ... Exposures consist mainly of large, fresh angular boulders of boulder fields. Although contacts with country rock were not observed, regional mapping indicates that it intrudes clastic rocks of the Aldridge and Creston formations. The distribution of outcrops and a pronounced aeromagnetic anomaly indicate that it cuts the east-trending Cranbrook normal fault with no apparent offset. ...

The Kiakho stock is similar to the Reade Lake stock with the dominant phase being a light grey, medium-grained quartz monzonite. It is generally equigranular but grades into a hypidiomorphic granular porphyritic phase with prominent plagioclase and light grey to flesh-coloured potassic feldspar phenocrysts; both are up to several centimetres in diameter in a granular groundmass of white subhedral plagioclase, light grey potassic feldspar, quartz and black hornblende" (Höy 1993).

5.1.3 Structure

The following has been summarized from Höy (1993):

Rocks of the Purcell Supergroup have been affected by several separate phases of deformation, ranging from Middle Proterozoic through to Paleocene. The North American craton underwent two phases of extension, a compressional orogeny and subsequent continental rifting, followed by development of a miogeocline. Thrusting and folding associated with development of the Foreland Fold and Thrust belt took place from Cretaceous to Paleocene time and was followed by Eocene extension.

The earliest deformation was associated with extension in the Middle Proterozoic which resulted in block faulting along the margin of the Purcell Basin, coincident with deposition of the Fort Steele and

Aldridge formations. Movement along growth faults is interpreted to have ceased by upper middle to upper Aldridge time. ...

A late Middle to early Upper Proterozoic (1300 to 1350 Ma) compressional event, the East Kootenay orogeny, has been interpreted based upon evidence for deformation and metamorphism prior to deposition of lower Paleozoic miogeoclinal strata. This event was associated with folding, development of a regional cleavage and granitic intrusions (i.e. 1305 ± 52 Ma Hellroaring Creek stock). Localized high grade metamorphic areas (i.e. Mathew Creek) are related to this tectonic event which is interpreted to have terminated Belt Purcell sedimentation.

The extensional Goat River orogeny occurred during deposition of the Windermere Supergroup (800 to 900 Ma) and is characterized by large-scale block faulting during and perhaps immediately prior to deposition of strata. The Windermere Supergroup is comprised of a basal conglomerate (Toby Formation) overlain by immature clastic and carbonate sediments of the Horsethief Creek Group. The Toby Formation consists of "... predominantly conglomerates and breccias, interpreted to have been deposited in fan sequences adjacent to active fault scarps in large structural basins. Locally, up to 2000 metres of underlying Belt-Purcell rocks have been eroded from uplifted blocks, providing a sediment source ... in adjacent basins" (Höy 1993).

The earlier tectonic events may record incipient rifting, with development of block-faulted, intracratonic structural basins, whereas by early Paleozoic time continental separation had occurred as platformal and miogeoclinal sediments were deposited on a western continental margin. The Laramide orogeny (Late Jurassic to Paleocene) resulted in the horizontal, northeast directed compression of Proterozoic strata and the overlying Paleozoic miogeoclinal prism onto the North American craton. Easterly verging thrust faults and folds developed with normal faults and westerly verging back thrusts and normal faults, resulting in a complex structural pattern. Two major faults, St. Mary and Moyie faults, have had a significant role in the structural history and fabric of the region, controlling facies and thickness changes in Proterozoic and Paleozoic strata.

A final episode of north-trending, west-dipping normal faulting took place in the Late Tertiary. The Rocky Mountain Trench is the most prominent and is a listric normal fault having dip-slip separation of at least 5 to 10 kilometres. However, strike slip separation is interpreted to be minimal based on stratigraphic correlations across the trench.

5.2 LOCAL GEOLOGY

The structure of the area is dominated by the Purcell Anticlinorium, a broad anticlinal structure which exposes strata of the Purcell Supergroup. The western limb of the anticlinorium is host to several regionally significant faults, having considerable east side down dip-slip displacement and resulting in duplication of the Purcell Supergroup strata. The property is bounded by two major northeast trending faults, the St. Mary fault to the north and the Cranbrook Fault to the south.

"The St. Mary fault is a right-lateral reverse fault with an estimated displacement of 11 kilometres. The age of this displacement is constrained by a date of 94 Ma on the Reade Lake stock which truncates the fault south of Kimberley. However, minor shearing in the stock along the projection of the fault indicates some post-intrusive movement. ...

West of Cranbrook, tight overturned, variable plunging folds with well-developed axial planar foliation are outlined by units in the upper Aldridge and lower Creston formations" (Hoy 1993).

The Moyie Fault, at Moyie Lake, juxtaposes the upper Kitchener Formation against the lower Aldridge Formation, representing in excess of 4.6 km of vertical displacement (Brown 1998). The Aldridge Formation in the hangingwall is comprised predominantly of the middle Aldridge Formation, with subordinate exposures of the lower Aldridge Formation immediately west of the Moyie Fault. The contact between the upper Aldridge Formation and the overlying Creston Formation is the locus of the Old Baldy Fault (or its interpreted en echelon equivalents). Vertical displacement is in excess of 250 metres where the fault juxtaposes lower Creston Formation against the upper middle Aldridge Formation. The Moyie River Fault follows the Moyie River valley and has an unknown, west side down component of displacement. These represent the main northeast- trending faults.

A number of north-trending faults have been mapped, including the Kid Fault and the west side down McNeil Fault, as well as northeast trending faults such as the Little Lamb Creek fault, the Fors Fault. Finally, there are a limited number of west to northwest trending faults such as the Cranbrook and Ice Faults, respectively.

... The Cranbrook fault is an east-trending normal fault that is younger than folding associated with initial reverse displacement on the Palmer Bar fault, but is later than normal movement. The Cranbrook fault juxtaposes Creston Formation in its hangingwall against middle Aldridge turbidites. It is cut by the Kiakho stock which has been dated by potassium-argon at 122 Ma. Due to possible excess argon in the hornblendes, this date is interpreted to be a maximum age of emplacement of the stock. ..." (Höy 1993).

Of particular interest are several faults along the east boundary, and immediately east, of the Eddy property, including the Palmer Bar Fault, which undergo a dramatic change in trend (as mapped) from north-trending to northeast trending. Also of note are the number of faults and fault segments comprising the Old Baldy Fault and its interpreted en echelon equivalents, such as the AC Fault.

5.3 PROPERTY GEOLOGY

The property is predominantly underlain by middle Aldridge Formation strata, with upper Aldridge to lower Creston Formation strata along the west-northwest boundary. Regional mapping, as compiled by Brown (1998), documents the juxtaposition of strata of the lower Creston Formation against middle and highly subordinate upper Aldridge Formation strata by the Old Baldy Fault system (OBFS). From southwest to northeast, the OBFS cuts upsection from approximately the stratigraphic levels of the Sundown marker at the headwaters of South Moyie Creek to the lower Creston Formation at the height of land between Perry Creek and Moyie River underlying the Eddy Property. At the headwaters of Ryder Creek, the Sundown gabbros are juxtaposed against the lower Creston Formation by the OBFS. A number of north-northeast to north-trending splays have been mapped extending from the OBFS along the east side of the Perry Creek drainage through lower and middle Creston Formation strata.

The Sundown gabbros provide local stratigraphic control throughout the Eddy property, extending from North Moyie Creek to Noke Creek and projected through the Hill Vein to, and through, Prospector's Dream. In addition, marker laminae have been identified on the property, which allow for precise determination of stratigraphic position within the middle Aldridge Formation.

Bedding measurements at lower elevations southeast of the OBFS document gentle dips to the east on north to north-northeast striking strata. At higher elevations (i.e. closer to the OBFS), the strike of bedding changes to northeast and dips steepen up to between 60° and 70°, to an orientation subparallel to the foliation.

The geology, as mapped by Klewchuk (2005), differs slightly in that there are a number of offsets of the OBFS across northwest trending faults, having horizontal displacements of approximately 200 metres. These offsets are evident at the southwest corner of the mapsheet and at the headwaters of Weaver Creek. In addition, the OBFS appears to consist of a pair of closely spaced faults, namely, the Old Baldy Fault to the east and the AC (Aldridge 7 Creston) Fault to the west.

Another difference between the maps is that Klewchuk (2005) has not projected the Sundown sills, which have a markedly different map pattern at the Hill Vein and at Prospector's Dream. The Sundown sills at Prospector's Dream on Klewchuk (2005) are perpendicular to those as projected by Brown (1998).

5.3.1 Identified Areas of Mineralization (Fig. 5)

"Although many of the copper veins and some of the lead-zinc veins contain minor gold, a number of veins in the Perry Creek area contain gold as their primary commodity. They are gold-quartz veins controlled by northeast-trending faults that cut Creston Formation quartzite and siltstone. Shearing and fracturing are extensive, commonly occurring in a zone several hundred metres wide on either side of the faults. Many of the veins are also associated with mafic dikes. They vary in thickness from a few centimetres to greater than 10 metres. They comprise massive, white to occasionally pink quartz, minor calcite, disseminated pyrite, and occasionally trace chalcopyrite and galena. They are commonly severely fractured or sheared and locally cut and offset by crossfaults. Others cut the prominent schistosity, which suggested ... they formed during and immediately following deformation. ...

5.3.1.1 SHEAR-CONTROLLED GOLD DEPOSITS

Significant gold mineralization has been discovered recently in northeast-trending shears in the middle Aldridge Formation on tributaries of the Moyie River 30 kilometres southwest of Cranbrook. The prospect, referred to as the **David** Property, ... is underlain by northeast-trending, west-dipping middle Aldridge siltstones and quartz wackes that are intruded by a number of Moyie sills. These sills locally contain anomalous magnetite concentrations near the mineralized zones. North-northeast-trending shears and faults, including the Baldy Mountain fault which juxtaposes Creston Formation on the west against the Aldridge Formation are prominent in the area.

Gold mineralization, associated with galena and chalcopyrite, occurs in zones of intense silicification within a number of these shear zones. Small crosscutting quartz tension veins and stockwork breccia zones occur within the shears. Although pyritic, these generally have low gold values. Chlorite, pyrite and associated bleaching occur within and marginal to the shears.

One of the zones is 1 to 2 metres thick and has been traced on surface for 950 metres. Drillhole intersections include 1.5 metres assaying 26.76 grams per tonne gold and 1.8 metres assaying 8.02 grams per tonne gold ..." (Höy 1993).

The following brief descriptions of the documented mineralized areas within and, in the case of the David, immediate adjacent ground have been summarized from the available literature. Additional information is available from the references cited.

5.3.1.2 David

The David occurrence occurs off the property to the southwest but has a structural setting similar to many of the mineralized occurrences within the Eddy property. The David occurrence (MINFILE #082FSE108) was discovered in 1990 and evaluated by Dragoon Resources Ltd in a program that included prospecting, geologic mapping, soil geochemistry, trenching and diamond drilling. Follow-up work in 1991 resulted in determination of a "drill-indicated" resource of approximately "... 96,000 tonnes grading 13.08 grams per tonne gold (uncut) or 7.11 grams per tonne (cut)" (see MINFILE Report in Appendix B).

The David occurrence consists of a 0.2 to 1.5 m wide shear zone within strata of the middle Aldridge Formation in the footwall of the OBFS. There are several auriferous shear zones identified on the David property, including the West and David shears, of which the David has the best gold values. "Numerous small northeast-oriented quartz veins are present and many carry anomalous gold mineralization. The main zone of gold mineralization ... is a NNE-striking shear zone composed of wavy, lensey quartz veins and intensely sheared middle Aldridge Formation sediments. The gold

mineralized zone and its immediate host rocks are characterized by strong silicification, related bleaching and elevated lead and copper values. Chlorite and pyrite occur within and marginal to the mineralized zone (Klewchuk 2005b).

"Gabbro sills ... are common in the David map area. As it is unusual to see more than 3 sills developed in close proximity to each other, the unusually high number of sills (at least seven) ... is likely due to repetition caused by a series of bedding sub-parallel reverse faults" (Klewchuk 1996).

The sills are oriented north-east and are apparently discontinuous, interpreted to represent "... structural attenuation during lateral movement along zones of northeast shearing" (Klewchuk 2001).

5.3.1.3 Discovery / Shadow Vein

The Discovery Vein is a poorly documented mineralized occurrence having a speculative location (Banting 1992; Ryley 1990). Unfortunately no map is known to the author indicating the location of the vein.

The vein is described as a 0.80 metre thick quartz vein having a trend of 130° over an exposed strike length of 20 metres (Ryley 1990). Old workings identified in the immediate vicinity attempted to intersect the down dip extension of a lenticular zone of massive galena (2.5 x 0.6 m) with up to 4% chalcopyrite, with associated minor malachite and azurite staining. Gabbro is present at both the hangingwall and footwall contacts suggesting the vein is hosted entirely within a gabbro. "The projection of the Discovery vein occurs at the intersection of the A/C fault and the Shadow vein" where visible gold in metasediments was tested in Trench 90-A (Ryley 1990).

5.3.1.4 Fast Eddy

The Fast Eddy occurrence is a fragmental discovered as a result of prospecting in 2002. "Sericite altered Middle Aldridge boulders were discovered on an old exploration road. Further prospecting found a tourmalinized PreCambrian vent system on the property 50m wide and at least 100m long. It is striking 340° and dipping 70° to the SW. Outcrop consists of massive black tourmaline within chloritic, sericitic and actinolitic altered sediments that exhibit soft sediment deformation and fragmental characteristics. ..." (Rodgers et al. 2002)

5.3.1.5 Galena Vein

The Galena Vein is located approximately 400 m north of the Red Zone immediately east of the OBFS and south of the headwaters of Weaver Creek. The vein is exposed in a trench adjacent to the road and is hosted by upper Aldridge Formation strata and reportedly "... occurs adjacent to a block of gabbro or perhaps a diabase dike ..." (Mason 1984) or has a footwall contact with gabbro (Ryley 1990). Ryley (1990) reports the Galena Vein "... yielded gold values up to 4200 ppb Au from a 0.50 m. quartz vein while Klewchuk and Kennedy (1990) report an average value of 0.108 oz Au/tonne over 1.2 metres zone of silicification. Mason (1984) reported that the vein had a strike of 50° (230°) with a vertical dip.

5.3.1.6 Hill Vein

The Hill Vein is another mineralized quartz vein that was discovered in the early 1980's during road construction. The 0.5 to 1.0 metre thick vein reportedly has a strike length in excess of 500 metres on a bearing of 035° with a gentle dip of 15° west and is located along a shear zone striking 180° and having a vertical dip. The Hill Vein has been the locus of a significant amount of trenching in various programs and "... is one of the largest gold-bearing quartz veins known in the placer gold drainages of Perry Creek and the Moyie River. The vein carries irregularly-developed coarse visible gold in association with euhedral pyrite along its entire known length ..." (Klewchuk and Kennedy 1990).

The vein has been described as a "... clean milky quartz vein with iron staining, rare sulfide and limonite present ..." while an adjacent shear "... crystalline quartz veins with limonite and a purplish oxide" (Rodgers et al. 2002). A number of other shears hosting visible gold were reported in the immediate area, striking 130° and dipping steeply southwest comprised of limonite and/or pyrite-rich crystalline quartz veins hosted by silicified sediments (Rodgers et al. 2002). The precise location of these gold-bearing shears was, unfortunately, not documented.

The stratigraphic position of the Hill Vein is constrained by its location between two thick gabbro sills hosted in middle Aldridge Formation strata. A marker sequence ("Laminated Siltstone Marker") is documented in a logging landing to the west, above the lower sill and was identified as the "Sundown" marker. The Sundown sills are the same as those exposed at Prospector's Dream and, therefore, these two mineralized occurrences are located at a similar stratigraphic position.

5.3.1.7 Prospector's Dream

The Prospector's Dream occurrence represents the earliest known (documented) mineralized occurrence on the Eddy property and was first reported in the 1890's (see Appendix B). The Minister if Mines Report for 1898 states "To the west of Weaver Creek and at the base of the hills forming the divide between it and Perry Creek, quite a number of mineral locations have been made and a considerable amount of work done". Therefore, the area had obviously been worked, but not reported(?), prior to 1898. There are several short adits and winzes that have been driven into the gabbro. With regard to previous workings in the Prospector's Dream area, O'Grady (1990) reported

"A quartz vein .3 meters wide with an accompanying additional .7 meter shear zone lies conformably within the sediments. Two shafts 1.5 meters by 1.5 meters have been sunk on the vein. The shafts are badly sloughed in and filled with water to within 2 meters of the top.

The quartz vein material from the trenches is from milky white to range colour. Material in the quartz consists of pyrite, in cubes and on shears, minor chalcopyrite, sericite and hematite.

... Two grab samples were taken from piles of quartz vein material near the shaft collars. The grab sample from the northern shaft assayed .85 oz/ton gold. The grab sample from the southern shaft assayed 1.34 oz/ton gold. ... The southern portion of the showing is underlain by diorite of the Moyie sills.

A quartz vein and accompanying shear approximately 1.5 meters wide is exposed within the diorite. The vein strikes at 100 degrees east of north and dips 15 degrees to the north. The vein contains minor pyrite and 10-15% black hematite. A grab sample from a 10 ton stockpile in front of this decline assayed 2.13 oz/ton gold.

A second decline is poorly exposed approximately 50 meters to the south and at a slightly lower elevation. A grab sample of quartz vein material from the front of the decline assayed 0.3 oz/ton gold. The quartz vein material at this location is milky white to orange where gossan is present.

A sample of diorite material from the footwall of the vein in this area assayed .021 oz/ton gold"

The Prospector's Dream was described as a quartz fissure vein hosted by gabbro (on of the "Sundown" sills) and middle Aldridge Formation strata (Mason 1984). The north-trending "Frost Fault" cross-cuts the area on either side of which are developed "Two historic relatively flat-lying gold-bearing quartz vein prospects ... (which) may be related to it. Trenching crossed the Frost Fault in the saddle and established that anomalous gold mineralization (best value of 436 ppb over 25 cm.) occurs with brecciation, quartz veining and limonitic alteration within the structure" (Rodgers et al. 2002). Free gold has been reportedly observed in a limonitic gossan on the quartz veins. "... Widespread limonitic and manganese alteration with brecciation ..." was described for the area.

5.3.1.8 Red Zone

The Red Zone is a pervasive gossan, having a width of up to 150 metres and exposed over a reported strike length of 1100 metres along the road between the Galena Vein, to the north, and MC2 Shear, to the south (Mason 1983, Ryley 1990). The occurrence consists of a quartz stockwork system, comprised of quartz stringers and veinlets in altered (bleached and strongly silicified) middle Aldridge Formation quartzites and argillites.

The Red Zone is believed to be equivalent to the Baldy Shear (Klewchuk, pers. comm. 2005) which has an orientation of 225°, dipping 65° NW and is slightly oblique to the Baldy Shear (Mason 1984). "There are large blocks of sheared quartz + 2% pyrite with brecciated fragments of sheared sediments enclosed. There are masses of quartz breccia 25' (7.62 m) thick and 200 (61 m) to 300' (91 m) strike length. In addition there is a zone extending 500' (152 m) across the strike which have numerous lenses of quartz under a foot thick. This appears to be a crush breccia associated with Old Baldy Fault" (Mason 1984).

5.3.1.9 Shadow Vein

The Shadow vein is located proximal to the Discovery Vein as Trench 90-A apparently exposed both the Discovery and Shadow veins (Ryley 1990). The Shadow vein is located at the projection of the Discovery Vein and the A/C Fault where "visible gold in strongly altered metasediments/diorite was located near the footwall contact" (Ryley 1990).

Trench 90-B subsequently exposed the interpreted strike extension of the Shadow Vein, having pervasive silicic alteration at both the hangingwall and footwall contacts. "This silicic zone extends north to the base of Weaver Ridge (where) .. Visible gold in altered quartzites in contact with a 3.6 m. quartz vein was discovered ..." (Ryley 1990)

5.3.1.10 Weaver No. 2 MC Shear

The Weaver No. 2 M.C. Shear (MC2 Shear) was initially located as a result of road building in 1989 and is localized within strata of the upper Aldridge Formation. The mineralized occurrence is located immediately east of the Old Baldy Fault and is probably within the OBFS. Stratigraphically, it is hosted by upper Aldridge Formation strata within 170 metres of the Aldridge / Creston contact (Mason 1984). The shear extends for approximately 240 metres along strike and varies in thickness up to 20 metres wide. "The MC shear is defined by phyllitic sediments with late quartz veins which cross-cut and parallel the shearing. Brecciation along the shear is common with fresh pyrite, silicification, chlorite, hematite, limonite, manganese and albite. Gabbros intrusions were noted in the MC shear in a number of areas. Quartz veins with abundant carbonate and calcite were present in both the sheared gabbro and sediments. Visible gold was noted in a number of locations in the MC shear" (Rodgers et al. 2002).

"Gold in the MC2 Shear is concentrated within late quartz veins which parallel and cross-cut the shearing, with values up to 0.933 oz/ton across 40cm, and within a central quartz-sericite schist zone where gold values exceed 60 PPB across a width of 4 meters. Altered wallrock adjacent to quartz veins and within shear zones is locally anomalous in gold ... (Klewchuk and Kennedy 1990).

The MC2 Shear area was the site of a relatively large number of trenches in 1989 to expose bedrock and develop a better understanding of the controls of gold mineralization.

6.0 GEOCHEMICAL DATABASE

Three separate geochemical databases have been compiled from the assessments reports available for the property, 19 heavy mineral samples, 322 rocks and 1779 soils. The majority of the samples were submitted for multi-element ICP analysis with analysis predominantly completed by Acme Analytical Laboratories and the remainder by Rossbacher labs. Most of the data were then tied to UTM coordinates determined from maps accompanying the reports, of highly variable quality. The data of Morris (1987) has been included in the database and utilized in the correlation matrix but does not have associated UTM coordinates as the maps are considered to be unsuitable for determination of coordinates.

6.1 Heavy Minerals

A total of 19 heavy mineral samples were compiled from Klewchuk and Kennedy (1990) and are considered to demonstrate the utility of the method. Of the 19 samples compiled, 18 plot within the map area comprising the Eddy property (Fig. 5). Two samples in Galway Creek, draining tot he northwest from the OBFS, returned values of 2060 and 560 ppb gold. Given the spatial association of anomalous gold in heavy mineral samples on the Eddy property, these should be further evaluated for possible follow-up work.

The remaining 16 samples were recovered from creeks draining to the southeast from the height of land, which is broadly coincident with the trend of the OBFS. Five of the samples, three in the headwaters of Weaver Creek and 1 from the headwaters of Weaver Creek, returned values of 5 ppb and were recovered upstream and west of the OBFS. These are not worthy of further consideration.

6.1.1 Ryder Creek

Three samples were taken from Ryder Creek at the southwest end of the property and returned values ranging from 340 to 10400 ppb. The samples were taken immediately east and downstream of the OBFS and document highly anomalous gold values. The area has subsequently been the site of limited follow-up work including recovery of soil and rock samples, however, the return of anomalous gold from a variety of different sample types has not been adequately pursued. Additional work is proposed for this area.

6.1.2 Weaver Creek

A total of 6 samples were recovered from Weaver Creek, upstream of the confluence with the North Fork of Weaver Creek. Two samples were recovered upstream and west of the OBFS, one of which returned an anomalous value of 70 ppb. Three additional samples were recovered along, and within, the trend of the OBFS and returned highly anomalous values to 266 ppb. This location is immediately southwest of the "Red Zone" and northeast of the "MC2 Shear", both sites of subsequent exploration activity including trenching soil and rock sampling, gravity and VLF-EM. The results of this work (as documented in the assessment reports and briefly summarized previously) resulted in identification of anomalous mineralization. The final sample along Weaver Creek, taken immediately above the confluence with the North Fork, returned a value of 100 ppb and may reflect mineralization identified at higher elevations adjacent to the creek or it may represent gold associated with an, as yet, unidentified source.

6.1.3 North Fork Weaver Creek ~

Five samples were taken along the North Fork of Weaver Creek, three of which returned a value of 5 ppb. A single sample taken approximately 600 metres east and downstream of the OBFS returned a value of 9650 ppb. In addition, it lies below the "Red Zone" and downstream of the "Galena Vein". A traditional approach of prospecting upstream of this highly anomalous value probably contributed to identification of these mineralized occurrences.

A single value immediately above the confluence with Weaver Creek returned a value of 70 ppb, which is very similar to the value of 100 ppb on the main branch of Weaver Creek described previously. Again, this may reflect the presence of the mineralized occurrences farther upstream along the North Fork or it may represent proximity to an, as yet, undiscovered source.

6.1.4 Weaver Creek

A single sample was recovered downstream of the confluence between the North Fork and the main branch of Weaver Creek, but upstream of the confluence with the tributary draining the Prospector's dream area. The sample returned a value of 310 ppb and may reflect the mineralization documented upstream or, possibly, unidentified proximal mineralization.

6.2 Soil Samples

A total of 1779 soils were compiled for the purposes of this report (Fig. 5), predominantly from work completed on behalf of Ruby Red Resources during the 2003 and 2004 field programs (Klewchuk 2005a, 2004). Additional data were recovered from Banting (1992), Klewchuk and Kennedy (1990 - analyses not included in assessment report but internal report for R.T. Banting Engineering) and Morris (1987). As mentioned previously, the sample location maps accompanying the report by Morris (1987) were not considered to be of sufficient quality to allow determination of UTM coordinates but were utilized for the purposes of identifying correlations.

The majority of the data (see Appendix C) consist of multi-element ICP analyses, predominantly through Acme Analytical Laboratories and a subordinate amount from Rossbacher Labs. Similar suites of elements were analyzed through each lab allowing a relatively large geochemical database to be compiled and analyzed.

The data were taken along grids (Banting 1992, Klewchuk and Kennedy 1990, Morris 1987) and along contours (Klewchuk 2005a, 2004). Sample spacing generally varied between 20 and 25 metres along lines spaced between 20 and 50 metres. Contour soils were along contours between 20 and 60 metres apart. The samples were all taken within or immediately adjacent to the known mineralized areas and/or along the projected trend of the presumed controlling shears. There are very few of the samples which can be considered to be reconnaissance in nature. Therefore, the correlations are interpreted to be potentially biased, with one or more inherent controls.

The calculated mean and standard deviation for the data is presented in Table 3, while the correlation matrix arising from analysis of the compiled soil data is presented in Table 4. Initial analysis suggested some of the elements could be eliminated from analysis due to low correlation coefficients. The software package utilized for determination of the correlation matrix identified all correlation coefficients having an absolute value in excess of 0.204 to be significant at the 95% level, while some greater than 0.48 were identified as significant at the 90% level. No rigorous statistical analysis has been performed on the data, but these low levels of significance are suspect given that a correlation of "0" indicates an absence of any correlation and an absolute value of "1" indicates 100% correlation. Therefore, for the purposes of the following discussion, only those elements having a qualitatively determined correlation coefficient greater than 0.40 will be discussed.

6.2.1 Ag

Silver has surprisingly strong coefficients with antimory (0.973) and zinc (0.877) while lead returned a coefficient of (0.328). This is surprising in that silver would most likely be hosted by galena as an impurity or perhaps tetrahedrite in association with copper. The implied relationship between antimony (perhaps as a sulphosalt) and zinc (as sphalerite) suggests silver may be preferentially associated with base metal mineralization rather than structurally controlled (i.e. iron and/or magnesium as chlorite and/or potassium as white mica (i.e. sericite))

6.2.2 Al

Again, there only two elements that are strongly correlated with aluminum, namely, sodium (0.447) and Ti (0.598). Given that the next element having a relatively strong correlation is nickel (0.232), this is interpreted to indicate proximity of gabbro as a source of weathered material in the soils (although this is not supported by the value for Cr (0.025) and only weakly by cobalt (0.138)). Sodium may be present in pyroxene comprising gabbroic (but not dioritic) sills. Alternatively, sodium may indicate an albitic plagioclase component to the soils which has been reported as a mineral phase in some of the veins.

6.2.3 Bi

Bismuth presents some very interesting correlation coefficients for interpretation and subsequent evaluation. There are three elements which correlate strongly with bismuth, specifically, molybdenum (0.525), uranium (0.752) and tungsten (0.812). The data for uranium must be interpreted with caution as there were three distinct detection limits documented, 5, 8 and 0.1. The majority of the data returned values of <8 or 5, while the more recent data returned values between 0.1 and 1 ppm. Therefore, beyond noting a possible correlation, no further interpretation will be made,.

Tungsten and molybdenum returned average values of 1.15 and 1.23 ppm, respectively, and so the analysis is comprised of analysis of these elements at very low levels and, therefore, must also be interpreted with caution. However, the interesting feature with regard to interpreting these data is the association of bismuth, molybdenum and tungsten, particularly if one also includes arsenic (0.260) and antimony (0.324). This suite of elements may indicate the influence of magmatic fluids arising

	Mean	Std. Deviation	N
Ag	0.31	3.491	1,396
AI	2.25	0.875	1,715
As	5.55	4.912	1,676
Au	24.27	104.564	1,727
Bi	1.26	1.340	1,404
Co	10.90	8.569	1,715
Cr	14.02	10.424	1,680
Cu	35.15	262.021	1,715
Fe	2.62	0.918	1,715
к	0.06	0.037	1,530
Mg	0.35	0.195	1,715
Mn	383.47	497.553	1,715
Мо	1.23	0.766	1,581
Na	0.01	0.004	1,695
Ni	15.07	7.432	1,714
Pb	28.07	62.858	1,775
Sb	1.51	7.926	1,378
Sr	7.80	5.046	1,715
Th	4.73	2.469	1,520
Ti	0.08	0.038	1,715
U	2.63	2.146	1,374
w	1.15	1.536	1,395
Zn	71.29	89.750	1,778

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										Con	elations													
		Ag	Al	As	Au	Bi	Co	Cr	Cu	Fe	ĸ	Mg	Mn	Мо	Na	Ni	Pb	Sb	Sr	Th	Ti	U	W	Zn
Ag	Pearson Correlation	1	-0.062	•0.008	0.011	0.170	-0.020	0.276	0.255	0.135	-0.050	-0.049 0.069	-0.014	-0.001 0.984	0.008 0.758	-0.020 0.456	0.328 0.000	0.973	-0.017 0.537	-0.109 0.000	-0.042 0.120	0.036 0.197	0.024 0.396	0.877
	Sig. (2-tailed) N	1, 39 6	0.020		0.675 1,355	0.000 1,309	0.465 1,396	0.000 1,392	1,396	0.000	0.080	1,396	0.607 1,396	1,359	1,395	1,395	1,395	1,296	1,396	1,208	1,396	1,295	1,284	1,396
AI	Pearson Correlation	-0.062	1	0.007	-0.111	-0.145	0.138	0.025	-0.053	0.169	0.039	-0.081	0.041	0.025	0.447	0.232	-0.094	-0.078	0.080	0.130	0.598	-0.091	-0.121	0.002
1	Sig. (2-tailed)	0.020		0,777	0.000	0.000	0.000	0.304	0.028	0.000	0.131	0.001	0.091	0.314	0.000	0.000	0.000	0.004	0.001	0.000	0.000	0.001	0.000	0.919
	N Retmon Correlation	1,396	1,715	1,676	1,664 0.083	1,404	1,715 0.187	1,680	1,715	1,715 0.378	1,530 0.025	1,715 0.142	1,715 0.044	1,581 0.348	1,695 0.006	1,714 0.187	<u>1,712</u> 0.109	1,378 0.062	1,715 0.023	1,520 0.399	-0.026	1,374 0.278	1,395 0.304	1,715
As	Pearson Correlation Sig. (2-tailed)	-0.008 0.757	0.007 0.777		0.083	0.200	0.187	0.044	0.003	0.000	0.025	0.142	0.044	0.040		0.000	0.000	0.0021	0.352	0.000	0.296	0.000	0.000	0.003
	N	1,384	1,676	1,876	1,628	1,400	1,676	1,653	1,676	1,676	1,491	1,676	1,676	1,553	1,657	1,675	1,674	1,377	1,676	1,482	1,676	1,373	1,392	1,676
Au	Pearson Correlation	0.011	-0.111	0.083	1	0.076	0.059	0.003	0.002	0.083	0.014	0.056	0.038	0.052	-0.042	0.016	0.108	0.019	0.001	0.024	-0.070	0.078	0.073	0.030
	Sig. (2-tailed) N	0.675	0.000	0.001	1 727	0.005	0.017 1,664	0.893 1,632	0.919 1,664	0.001	0.586 1,479	0.021 1,664	0.124 1,664	0.043 1,538	0.092	0.517 1,663	0.000 1,724	0.488 1,337	0.963 1,664	0.348 1,470	0.004 1,664	0.004 1,334	0.007 1,353	0.215 1,727
Bi	Pearson Correlation	1,355 0.170	1,664 -0.145	1,628 0.260	1,727 0.076	1,304	0,097	0.128	0.198	0.205	-0.091	0.113	-0.059	0.525	0.134	0.148	0.243	0.324	-0.076	0.193	-0.027	0.752	0.812	0.193
	Sig. (2-tailed)	0.000	0.000	1 1	0.005	.]	0.000	0.000	0.000	0.000	0.001	0.000	0.027	0.000		0.000	0.000	0.000	0.004	0.000	0.312	0.000	0.000	0.000
	N	1,309	1,404	1,400	1,364	1,404	1,404	1,403	1,404	1,404	1,219	1,404	1,404	1,387	1,400	1,403	1,403	1,370	1,404	1,218	1,404	1,371	1,341	1,404
Co	Pearson Correlation	-0.020	0.138	0.187	0.059	0.097	1	0.170	0.051	0.287	0,153	0.252	0.351	0.277	0.019 0.431	0.568	0.126	0.007 0.793	0.239 0.000	0.243 0.000	-0.009 0.722	0.098 0.000	0.089	0.054 0.026
	Sig. (2-tailed) N	0.465	0.000	0.000 1,676	0.017	0.000 1,404	1,715	0.000 1,680	0.036 1,715	0.000 1,715	0.000 1,530	0.000 1,715	0.000 1,715	0.000	1,695	1,714	1,712	1,378	1,715	1,520	1,715	1,374	1,395	1,715
Cr	Pearson Correlation	0.276	0.025	0.044	0.003	0.128	0.170	1,000	0,367	0.199	0.123	0.332	0.026	-0.014	-0.005	0.475	0.115	0.277	0.191	-0.064	0.046	0.005	0.017	0.232
	Sig. (2-tailed)	0.000	0.304	0.074	0.893	0.000	0.000	. 1	0.000	0.000	0.000	0.000	0.285	0.577	0,833	0.000	0.000	0.000	0.000	0.014	0.057	0.849	0.533	0.000
<u> </u>	N	1,392	1,680	1,653	1,632	1,403	1,680	1,680	1,680	1,680	1,495	1,680	1,680	1,559	1,660	1,879	1,678	1,378	1,680	1,485	1,680	1,374	1,394	1,680 0.207
Cu	Pearson Correlation	0.255	-0.053	0.003	0.002	0.198 0.000	0.051 0.036	0.367	1	0.085	0.094	0.010 0.665	0.007	0.026	0.023 0.339	0.064 0.008	0.402	0.242	0.007 0.785	-0.066 0.010	-0.016 0.518	0.063	0.013 0.633	0.207
	Sig. (2-tailed) N	0.000 1,396	0.028	0.887 1,676	0.919 1,664	1,404	1,715	1,680	1,715	1,715	1,530	1,715	1,715	1,581	1,695	1,714	1,712	1,378	1,715	1,520	1,715	1,374	1,395	1,715
Fe	Pearson Correlation	0.135	0.169	0.378	0.083	0.205	0.287	0.199	0.085	1	0.139	0.374	0.055	0.304	-0.015	0.338	0.085	0.165	0.192	0.470	0.115	0.244	0,133	0.171
	Sig. (2-tailed)	0.000	0.000	0.000	0.001	0.000	0.000	0.000	0.000		0.000	0.000	0.022	0.000		0.000	0.000		0.000	0.000	0.000	0.000	0.000	0.000
	N	1,396	1,715	1,676	1,664	1,404	1,715	1,680	1,715	1,715	1,530	1,715	1,715	1,581	1,695	1,714	1,712	1,378	1,715	1,520	1,715	1,374	1,395 -0.131	1,715 0.229
к	Pearson Correlation Sig. (2-tailed)	-0.050 0.080	0.039	0.025	0.014 0.586	-0.091 0.001	0.153 0.000	0.123	0.094 0.000	0,139 0.000	1	0.147 0.000	0.193 0.000	-0.068 0.011	-0.064 0.013	0.277	0.013 0.604	-0.114 0.000	0.172 0.000	0.144 0.000	0.162 0.000	0.001	0.000	0.229
	N	1,212	1,530	1,491	1,479	1,219	1,530	1,495	1,530	1,530	1,530	1,530	1,530	1,396	1,510	1,529	1,528	1,193	1,530	1,520	1,530	1,189	1,210	1,530
Mg	Pearson Correlation	-0.049	-0.081	0.142	0,056	0.113	0.252	0.332	0.010	0.374	0.147	1	0.053	0.071	-0.180	0.496	0.040	-0.031	0,100	0.121	-0.146	0.178	0.066	0.023
	Sig. (2-tailed)	0.069	0.001	0.000	0.021	0.000	0.000	0.000	0.665	0.000	0.000		0.028	0.005	0.000	0.000	0,101	0.247	0.000	0.000	0.000	0.000	0.014	0.346
	N	1,396	1,715	1,676	1,664	1,404	1,715	1,680	1,715	1,715	1,530	1,715	1,715	1,581	1,695	1,714	1,712	1,378	1,715	1,520	1,715 0.056	1,374	1,395	1,715 0,118
Mn	Pearson Correlation Sig. (2-tailed)	-0.014 0.607	0.041	0.044	0.038 0.124	-0.059 0.027	0.351	0.026 0.285	0.007 0.781	0.055 0.022	0.193	0.053 0.028	1	0.088 0.000	0.042 0.081	0.154	0.079 0.001	-0.022 0.421	0.368 0.000	-0.155 0.000	0.050	0.004	0.080	0,000
	N	1,396	1,715	1,676	1,664	1,404	1,715	1,680	1,715	1,715	1,530	1,715	1,715	1,581	1,695	1,714	1,712	1,378	1,715	1,520	1,715	1,374	1,395	1,715
Mo	Pearson Correlation	-0.001	0.025	0.348	0.052	0.525	0.277	-0.014	0.026	0.304	-0.068	0.071	0.088	1	0.057	0.202	0.177	0.120	0.019	0.327	-0.012	0.458	0.542	0.064
	Sig. (2-tailed)	0.984	0.314	0.000	0,043	0.000	0.000	0.577	0.306	0.000	0.011	0.005	0.000		0.024	0.000	0.000	0.000	0.456	0.000	0.640	0.000	0.000	0.011
	N	1,359	1,581	1,553	1,538	1,387	1,581 0,019	1,559	1,581	1,581	1,396	1,581 -0.180	1,581 0.042	1,581 0.057	1,568	1,580 0.127	1,579	1,377	1,581 0.218	1,389 -0.188	1,581	1,373 0.226	1,374 0.147	1,581 0.035
Na	Pearson Correlation Sig. (2-tailed)	0.008 0.758	0.447	0.006	-0.042 0.092	0.134	0.019	0.833	0.023	0.549	0.013	0.000	0.042	0.024	. 1	0.000	0.173	0.434	0.000	0.000	0.000	0.000	0.000	0.154
	N	1,395	1,695	1,657	1,644	1,400	1,695	1,680	1,695	1,695	1,510	1,695	1,695	1,568	1,695	1,694	1,693	1,378	1,695	1,500	1,695	1,374	1,392	1,695
Ni	Pearson Correlation	-0.020	0.232	0,187	0.016	0.148	0.568	0,475	0.064	0.338	0.277	0.498	0.154	0.202	0.127	1	0.089	-0.007	0.289	0.282	0.091	0.180	0.088	0.165
1	Sig. (2-tailed)	0.456	0.000		0.517	0.000	0.000	0.000	0.008	0.000	0.000	0,000	0.000	0.000			0.000	0.788	0.000	0.000 1,519	0.000	0.000 1,373	0.001 1,395	0.000 1,714
Рb	N Pearson Correlation	1,395	1,714 -0.094	1,675 0.109	1,663 0.108	1,403 0.243	1,714 0.126	1,679 0.115	1,714	1,714	1,529 0.013	1,714 0.040	1,714 0.079	1,580 0.177	1,694 -0.033	1,714	1,711	1,377 0.143	1,714	0.050	1,714 -0.117	0.191	0.174	0.396
L. P.	Sig. (2-tailed)	0.000	0.000		0.000	0.000	0.000	0.000	0.000	0.000	0.604	0.101	0.001	0.000	0.173	0.000		0.000	0.096	0.052	0.000	0.000	0.000	0.000
	<u>N</u>	1,395	1,712	1,674	1,724	1,403	1,712	1,678	1,712	1,712	1,528	1,712	1,712	1,579	1,693	1,711	1,775	1,377	1,712	1,518	1,712	1,373	1,394	1,775
Sb	Pearson Correlation	0.973	-0.078	0.062	0.019	0.324	0.007	0.277	0.242	0.165	-0.114	-0.031	-0.022	0.120	0.021	-0.007	0.143	1	-0.041	0.158 0.000	-0.037	0.186 0.000	0.213 0.000	0.684 0.000
	Sig. (2-tailed)	0.000	0.004 1,378	0.021 1,377	0.488 1,337	0.000 1,370	0.793 1,378	0.000 1,378	0.000 1,378	0.000 1,378	0.000	0.247 1,378	0.421 1,378	0.000 1,377	0.434 1,378	0.788 1,377	0.000 1,377	1,378	0.129 1,378	1,192	0.174 1,378	1,371	1,338	1,378
Sr	Pearson Correlation	-0.017	0.080	0.023	0.001	-0.076	0.239	0.191	0.007	0.192	0.172	0.100	0.368	0.019	0.218	0.289	0.040	-0.041	1	-0.063	0.101	0.002	-0.088	0.029
l"	Sig. (2-tailed)	0.537	0.001	0.352	0.963	0.004	0.000	0.000	0.785	0.000	0.000	0.000	0.000	0.456	0.000	0.000	0.096	0.129		0.014	0.000	0.947	0.001	0.227
	N	1,396	1,715	1,676	1,664	1,404	1,715	1,680	1,715	1,715	1,530	1,715	1,715	1,581	1,695	1,714	1,712	1,378	1,715	1,520	1,715	1,374	1,395	1,715
Th	Pearson Correlation	-0.109	0.130	0.399	0.024	0.193	0.243	-0.064	-0.066	0.470	0.144	0.121	-0.155 0.000	0.327	-0.188 0.000	0.282 0.000	0.050 0.052	0.158	-0.063 0.014	. 1	-0.128 0.000	0.236	0.144 0.000	0.074 0.004
	Sig. (2-tailed) N	0.000	0.000 1,520		0.348 1,470	0.000 1,218	0.000 1,520	0.014 1,485	0.010	0.000 1,520	1,520	1,520	1,520	1,389		1,519	1,518		1,520	1,520	1,520	1,188	1,209	1,520
Ti	Pearson Correlation	-0.042	0.598		-0.070	-0.027	-0.009	0.046	-0.016	0.115	0.162	-0.146	0.056	-0.012		0.091	-0.117	-0.037	0.101	-0.128	1	0.059	0.029	0.020
	Sig. (2-tailed)	0.120	0.000	0.296	0.004	0.312	0.722	0.057	0.518	0.000		0.000	0.020	0.640		0.000	0.000		0.000	0.000	·	0.030	0.278	0.398
L	N	1,396	1,715		1,664	1,404	1,715	1,680	1,715	1,715	1,530	1,715	1,715	1,581	1,695	1,714	1,712	1,378	1,715	1,520	1,715	1,374	1,395	1,715
U	Pearson Correlation	0.036	-0.091	0.278	0.078	0.752 0.000	0.098 0.000	0.005 0.849	0.063	0.244 0.000	-0.094 0.001	0.178 0.000	-0.064 0.017	0,458		0.180 0.000	0.191 0.000	0.186	0.002 0.947	0.236	0.059 0.030	. 1	0.000	0.086 0.001
	Sig. (2-tailed) N	0.197 1,295	0.001 1,374	0.000 1,373	0.004 1,334	1,371	1,374	0.849 1,374	1,374	1,374	1,189	1,374	1,374	1,373	1,374	1,373	1,373	1,371	1,374	1,188	1,374	1,374	1,336	1,374
ŵ	Pearson Correlation	0.024	-0.121	0.304	0.073	0,812	0.089	0.017	0.013	0.133	-0.131	0.066	-0.060	0.542		0.088	0.174	0.213	-0.088	0.144	0.029	0,703	1	0.064
	Sig. (2-tailed)	0.396	0.000	0.000	0.007	0.000	0.001	0.533	0.633	0.000	0.000	0.014	0.025	0.000		0.001	0.000		0.001	0.000	0.278	0.000	·	0.017
ļ	N	1,284	1,395		1,353	1,341	1,395	1,394	1,395	1,395	1,210	1,395	1,395	1,374	1,392	1,395	1,394	1,338	1,395	1,209	1,395	1,336	1,395	1,395
Zn	Pearson Correlation	0.877	0.002 0.919		0.030 0.215	0.193 0.000	0.054 0.026	0.232	0.207 0.000	0.171 0.000	0.229	0.023 0.346	0.118	0.064 0.011	0.035 0.154	0.165 0.000	0.396	0.884	0.029 0.227	0.074 0.004	0.020 0.398	0.086 0.001	0.064	. 1
	Sig. (2-tailed) N	1,396	0.919		0.215	1,404	1,715	1,680	1,715	1,715		1,715	1,715	1,581	1,695	1,714	1,775		1,715	1,520	1,715	1,374	1,395	1,778
	lation is significant at the 0.0													المقت المعدية										

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*. Correlation is significant at the 0.05 level (2-tailed). **. Correlation is significant at the 0.01 level (2-tailed).

from proximity to the Cretaceous Bayonne Magmatic Suite and the "Intrusion-related Gold" model (Logan, 2001, 2000; Lang et al. 2000; Lefebure et al. 1999).

6.2.4 Co

Nickel (0.568) is strongly correlated to cobalt and together with iron (0.287) and magnesium (0.252) is interpreted to indicate the mafic gabbro (to dioritic) sills as the probable source for these elements.

6.2.5 Cr

Chromium also has a strong correlation with nickel (0.475), with weaker correlations with cobalt (0.170), iron (0.199) and magnesium (0.332), which again suggests a mafic source such as the gabbro sills. In addition, a weak correlation with copper (0.367) is interpreted to indicate that the gabbros may be a local source of copper or acted as a preferential geochemical barrier to copper.

6.2.6 Sb

Antimony correlates very strongly with silver (0.973) and zinc (0.884) which is interpreted to indicate sphalerite occurs predominantly with tetrahedrite (or some other sulphosalt), rather than galena. The moderate correlation between copper and lead (0.402) relative to lead and zinc (0.396), together with a weak correlation between copper and zinc (0.232) suggests base metal mineralization may be separated into a copper-lead phase and a silver-antimony-zinc phase.

The remainder of the elements have either been discussed relative to those above or are interpreted to be minor geochemical associations not pertinent to this discussion.

6.3 Rock Samples

A total of 322 rocks were compiled for the purposes of this report (Fig. 5), again, some of which do not have corresponding UTM coordinates. The samples were taken predominantly from areas of known mineralization and/or alteration and, therefore, have corresponding dependencies evident within the correlation matrix.

Table 5 is a tabulation of the mean and standard deviations for the data within the rock sample database while Table 6 represents the correlation matrix determined from the data. Again, a qualitative lower limit of 0.500 has been utilized as a cut-off for the correlation coefficients for the purposes of discussing the analytical data from the rock samples.

6.3.1 Ag

Silver documents a strong correlation with bismuth (0.830), lead (0.725) and antimony (0.638). In addition, a moderate correlation with gold (0.442) is evident, which was not apparent in the soil data. These data are interpreted to suggest the presence of argentiferous galena in association with sulphosalts (i.e. tetrahedrite (note: the correlation with copper at (0.153)). The correlation with

bismuth and antimony, when considered with arsenic (0.171) and tungsten (0.229) may indicate magmatic fluids as a possible source of mineralization.

6.3.2 As

Arsenic has a strong correlation with gold (0.557) which may indicate that the presence of arsenicbearing phases (arsenopyrite) or secondary alteration products (scorodite) may be indicative of the presence of gold. In previous reports, visible gold has been noted in the presence of pyrite and limonite but no mention has been made of arsenopyrite. This possible association of arsenic with gold may be of value in subsequent exploration.

6.3.3 Au

In contrast with the soil data, gold has a strong correlation with arsenic (described above) and lead (0.562). In addition, silver (0.442) has a relatively strong correlation with gold. Of potential interest is the weak to moderate association of bismuth (0.241), molybdenum (0.258), and tungsten (0.153) which may be interpreted, once agin, to indicate the contribution of magmatic fluids.

6.3.4 Bi

The data for bismuth documents a strong correlation with silver (0.830), lead (0.510) and antimony (0.567), in addition to weaker correlations with gold (0.241), copper (0.390), and tungsten (0.266). The data could be interpreted to indicate a magmatic contribution utilizing an intrusion-related gold model and the As-Au-Bi-Sb-W metal association.

6.3.5 Co

Cobalt again appears to record a mafic signature, most likely associated with the Aldridge sills of gabbroic (to dioritic) composition as documented by the correlation with iron (0.516) an nickel (0.744).

6.3.6 Zn

Again, in contrast to the soils, zinc documents a strong correlation with lead (0.510) which is interpreted to indicate that the common base metal association of galena (possibly argentiferous galena) and sphalerite are present on the property.

	Descriptive Sta	tistics	
		Std.	
	Mean	Deviation	Ν
Ag	3.52	12.207	234
AI	0.59	0.724	322
As	41.41	243.819	287
Au*	1,895.20	7,208.317	316
Bi	6.87	21.877	215
Co	19.10	32.955	308
Cr	59.00	54.138	313
Cu	118.85	709.000	322
Fe	3.69	3.201	322
к	0.06	0.057	320
Mg	0.46	1.099	308
Mn	386.83	927.403	321
Мо	5.58	19.341	303
Na	0.02	0.023	291
Ni	15.95	19.812	322
Pb	868.25	3,987.541	306
Sb	4.48	7.682	194
Sr	5.72	13.289	321
Th	5.95	3.755	129
Ti	0.02	0.028	196
U	5.49	2.659	182
w	2.89	3.507	219
Zn	76.46	170.987	322

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		<u> </u>			A.1			<u> </u>			relation		1/-	··· D= ··	<u>k'-</u> -	- N - N	- DE			- YL				7
	Passan Completion	Ag	AI	As	Au*	Bi 0,830	Co	Cr 0.045	Cu 0.157	Fe	X 0.053	Mg	Mn	Mö	Na 0.001	NI 0.000	Pb A 724	Sb	Sr	Th -0.116	11	-0.020	W 0.229	Zn 0.131
-	Pearson Correlation Sig. (2-1ailed)	1	-0.168 0.010	0.171	0.442	0.830	-0.080 0.238	0.045 0.501	0.153	-0.025	-0.053 0.419	-0.115 0.085	-0.081 0.216	0.134	0.001	-0.099 0.132	0.725	0,638 0,000	-0.028 0.670	0.116	-0.042 0.571	-0.020	0.229	0.131
	N	234	234	226	233	199	222	229	234	234	232	225	233	229	221	234	230	187	234	49	185	174	196	234
	Paarson Correlation	-0,168	1	-0.045	-0,144	-0.140	0.102	-0.153	-0.029	0.232	0.054	0.583	0.153	-0.056	-0.013	0.306	-0.115	-0.020	0.164	0.002	0,297	0.137	-0,098	0.018
1	Sig. (2-tailed)	0.010		0.448	0.011	0.041	0.073	0.007	0.602	0.000	0.332	0.000	0,006	0.328	0.821	0.000	0.044	0,765	0.003	0.985	0.000	0.065	0.150	0.751
	N	234	322	287	316	215	308	313	322	322	320	308	321	303	291	322	306	194	321	129	196	182	219	322
	Pearson Correlation	0.171	-0.045	1	0.657	0.080	-0.018	-0.114	0.039	0.364	0,055	-0.042	+0.027	0.483	-0.011	0.025	0.141	0.144	-0.016	-0.063	-0.013	0.058	0,354	0.307
	Sig. (2-teiled)	0.010	0.448		0.000	0.252	0.767	0.057	0,508	0.000	0.355	0.486	0.650	0.000	0.855	0.674	0.019	0.046	0.790	0.537	0.853	0.442	0.000	0.000
	N	226	287	287	285	209	275	281	287	287	285	275	286	274	263	287	277	192	287	99	192	178	207	287
	Pearson Correlation Sig. (2-tailed)	0.442	0.144	0.557	1	0.241	-0.084 0.146	0.142	0.152 0.007	0.099	-0.039 0.493	-0.090 0.119	-0.065 0.246	0.258	-0.046	-0.066 0.243	0,562	0.087 0.228	-0.021 0.707	-0.077	-0.049 0.491	-0.042 0.575	0.153 0.024	0.259 0.000
	N (2-14110-0)	233	316	285	316	214	302	307	316	316	314	303	315	297	286	316	300	0.220	315	123	195	182	217	316
	Pearson Correlation	0.630	-0.140	0.080	0.241	1	-0.056	+0.030	0.390	-0.033	-0.064	-0.115	-0.054	0.056	-0.055	-0.072	0.510	0.567	-0.024	0.015	-0.013	0.013	0.266	-D.057
	Sig. (2-tailed)	0.000	0.041	0.252	0.000		0.423	0.663	0.000	0.631	0,349	860.0	0.433	0.413	0.430	0.293	0.000	0.000	0.729	0.926	0.868	0.654	0.000	0,403
	N	. 199	215	209	214	215	205	213	215	215	214	207	215	213	207	215	212	185	215	40	177	175	190	215
Co	Pearson Correlation	-0.080	0.102	-0.018	0.084	-0.056	1	+0.030	0.006	0.516	-0.006	0.113	0.231	0.038	-0.023	0.744	-0.059	-0.034	-0.014	-0.067	0.018	0,111	0.040	-0,013
	Sig. (2-tailed)	0.238	0.073	0.767	0.146	0.423	•	0.608	0.865	0.000	0.918	0.049	0.000	0.517	0.699	0.000	0.313	0.638	0.811	0.467	0.804	0.134	0.559	0.821
	N	222	308	275	302	205	308	303	306	308	307	301	307	289	277	308	292	190	307	120	195	182	211	306
	Pearson Correlation Sig. (2-tailed)	0.045	-0,153 0,007	-0,114 0.057	0.142 0.013	-0.030 0.663	-0.030 0.608	1	0.017 0.771	-0.112 0.048	-0.513 0.000	-0.114 0.048	-0.054 0,342	-0.112 0.055	-0.018 0.766	0.075 0.186	0.132 0.023	-0,178 0,013	-0.045 0.432	0.087	0.071 0.323	-0.273	-0.282	0.042 0.457
	Sig. (z-uineu) N	229	313	281	307	213	303	313	313	313	311	300	0.342	294	282	313	298	192	312	121	195	182	216	313
	Pearson Correlation	0.153	-0.029	0.039	0.152	0,390	0,008	0.017	1	0.006	-0.107	-0.009	-0.019	0.021	-0.031	0.023	0,171	0.087	-0.012	0.01B	-0.015	-0.016	0.027	0.076
	Sig. (2-tailed)	0.019	0.002		0.007	0.000	0.885	0.771	. 1	0.912	0.058	0.672	0.734	0.716	0.602	0.676	0.003	D.230	0.835	0.844	D.833	0.826	0.695	0.172
	N	234	322	287	316	215	308	313	322	322	320	308	321	303	291	322	308	194	321	129	196	182	219	322
0	Pearson Correlation	-0.025	D,232	0.364	0.099	-0.033	0.516	-0.112	0.006	1	0.130	0.221	0.404	0.215	-0.115	0,500	-0.016	0.014	0.062	-0.093	0.032	0.273	0.087	0.164
	Sig. (2-tailed)	0.702	0.000	0.000	0.080	0.631	0.000	0.048	0.912	·	0.020	0.000	0.000	0.000	0.049	0.000	0.774	0.649	0.271	0.296		0.000	0.199	0.001
	N	234	322	287	316	215	306	313	322	322	320	-0.005	321	303	291	322	306	194	321	129	196	182	219	322
	Pearson Correlation Sig. (2-tailed)	-0.053	0.054	0.055 0.355	-0.039 0.493	-0.064 0.349	-0.006 0.916	-0.513	-0.107 0.056	0.130	4	-0.005	0.029	0.008	-0.085	-0.056 0.320	-0.062 0.280	0.080 0.273	0.059	0.237	-0.038 0.598	0.653	0.274	0.030
	Ng. (z-talled) N	0.419 232	320	0.335	0.483	0.349	307	311	320	320	320	307	319	301	289	0.320 320	304	192	319	129	0.598 195	182	217	320
	Pearson Correlation	-0.115	0.583	-0.042	-0.090	-0.115	0.113	-0.114	-0.009	0.221	-0.005	1	0.147	-0.032	-0.019	0.329	-0.067	0.110	0.204	0.051	0.164	-0.001	0.040	-0.025
+	Sig. (2-tailed)	0.085	0.000	0.486	0.119	0.098	0,049	0.048	0.872	0.000	0.924	. '	0.010	0.588	0.757	0.000	0.256	0,130	0.000	0.573	0.022	0.986	0.563	0.661
	N	225	308	275	303	207	301	300	308	308	307	308	307	290	279	308	292	191	307	122	198	182	208	308
In ,	Pearson Correlation	-0.081	D.153	-0.027	-0.065	-0.054	0.231	-0.054	-0.019	0.404	0.029	0,147	1	-0.002	-0.0\$5	D.197	-0.035	-0.035	0.128	-0.005	0.013	0.214	0.218	0.095
	Sig. (2-tailed)	0.216	0.006	0.650	0.248	0.433	0.000	0.342	0.734	0.000	0.604	0.010		0.970	0.353	0,000	0,547	0.625	0.022	D.954	0,859	0.004	0.001	0.088
	N	233	321	286	315	215	307	312	321	321	319	307	321	302	291	321	305	194	320	126	195	182	219	321
	Pearson Correlation	0.134	-0.056 0,328	0,483 0,000	0.256	0.056 0.413	0.038	-0.112 0.055	0.021 0.716	0.215	0.008 0.687	-0.032 0.588	-0.002 0.970	1	0.292	0.005	0.137 0.020	0.104 0.152	0.029	0.015	-0.033	0.003	0.098	0.252 0.000
	Sig. (2-tailed) N	0.043 229	0,328 303	274	297	213	289	294	303	303	301	0.388	302	303	279	303	290	192	303	116	0.654 192	182	218	303
	Pearson Correlation	0.001	-0.013	-0.011	0.046	-0.055	-0.023	0.018	-0.031	-0.115	-0.085	-0.018	-0.055	0.292	1	0.069	0.049	-0.026	-0.031	0.333	-0.052	-0.041	-0.017	0,128
	Sig. (2-tailed)	0.990	0.821	0.855	0.442	0.430	0.699	0.766	0.602	0.049	0.149	0.757	0.353	0.000		0.242	0.416	0.717	0.599	0.000	0.476	0.587	0.805	0.029
	N	221	281	263	288	207	277	282	291	291	289	279	291	279	291	291	277	190	291	108	187	. 177	214	291
11 1	Pearson Correlation	-0.099	0.306	0.025	-0.066	-0.072	9.744	0.075	0.023	0.500	-0.056	0.329	0.197	0.005	-0.069	1	-0.067	-0.052	0.100	0.021	0.115	0.074	-0.071	0.051
	Sig. (2-tailed)	0.132	0.000	0.674	0.243	0.293	0.000	0.186	0.676	0.000	0.320	0.000	0.000	0,928	0.242		0.245	0.475	0.074	0.814	0,109	0.320	0.292	0.364
_	N	234	322	287	316	215	308	313	322	322	320	308	321	303	201	322	306	194	321	129	196	182	219	322
	Pearson Correlation	0,725	-0.115 0.044	0.141	0.562	0.510	-0.059 0.313	0.132	0.171	-0.016 0.774	-0.062 0.280	-0.067 0.256	-0.035 0.547	0.137	0.049	-0.067 0.245	1	0.414 0.000	0.017 0.771	0.009 0.927	-0.039 0.583	-0.034 0.651	0,179	0,510 0.000
	Sig. (2-tailed) N	230	0.044	0.019	300	212	292	298	306	306	304	0.200 292	0.547 305	290	277	308	306	194	305	0.927 114	0.963	180	216	300
	Pearson Correlation	0.636	-0.020	0.144	0.087	0,567	0.034	-0.178	0.087	0.014	0.080	0.110	-0.035	0.104	0.026	-0.052	0.414		0.060	-0.442	-0.035	0,041	0.157	0.158
	Sig. (2-tailed)	0,000	0.785	0.046	0.228	0.000	0.638	0.013	0.230	0.849	0.273	0.130	0.625	0.152	0.717	0,475	0.000	. 1	0.403	0.039	0.640	0.591	0.032	0.019
	N	187	194	192	193	185	190	192	194	194	192	191	194	192	190	194	194	194	194	22	178	172	185	194
	Pearson Correlation	-0.028	0.164	-0.016	-0.021	-0.024	-0.014	-0.045	-0.012	0.062	0.059	0.204	0.126	0.029	-0.031	0.100	0.017	0.060	1	0.139	0.085	0.003	0.242	0.050
	Sig. (2-tailed)	0.670	0.003	0.790	0.707	0.729	0,811	0 432	0.835	0.271	0.291	0.000	0.022	0.614	0.599	0.074	0.771	0.403	·	0.118	0.238	0.967	0.000	0.374
		234	321	287	315	215	307	312	321	321	319	307	320	303	291	321	305	194	321	128	196	182	219	321
	Peerson Correlation	-0.116	0.002	-0.063 0.537	-0.077 0.397	0.015 0.926	-0.067 0.467	0.087	0.018	-0.093 0.296	0.237	0.051 0.573	-0.005	0.015	0.333	0.021	0.009 0.927	-0,442 0.039	0.139	1	0.270 0.213	-0.249 0.413	0.125	0.005
	Sig. (2-tailed) N	0.429	0.965	0.03/	0.397	0.925	0.46/	0.344	0.044	0.296	129	0.573	0.954	0.670	0.000	0.014	0.927	22	128	129	0.213 23	12	0.400	129
	Pearson Correlation	-0.042	0.297	-0.013	-0.049	-0.013	0.018	0.071	-0.015	0.032	-0.038	0.164	0.013	-0.033	-0.052	0.115	-0.039	-0.035	0.085	0.270	1	-0.017	-0.016	-0.023
	Big. (2-teiled)	0.571	0.000		0.491	0.868	0.804	0.323	0.833	0.657	0.598	0.022	0.859	0.654	0.476		0.583	0.640	0.238	0.213	L I	0.829	0.838	المسما
	N N	185	196	192	196	177	195	195	196	198	196	196	195	192	187	196	196	178	196	23	196	173	173	196
ı I	Pearson Correlation	+0.020	0.137	0.058	-0.042	0.013	0.111	-0,273	-0.016	0.273	0.653	-0.001	0.214	0.003	-0.041	0.074	-0.034	0.041	0.003	-0.249		۱	0.050	
5	Sig. (2-tailed)	0.794	0.065	0.442	0.575	0.864	0.134	0.000	0.826	0.000	0.000	0.986	0.004		0.587		0.651	0.591	0.967	0,413	0.829	.	0,517	í (
	4	174	182	178	182	175	182	182	182	182	182	182	182	182	177	182	180	172	182	13	173	182	173	182
	Pearson Correlation	0.229	-0.098	0.354	0.153	0.266	0.040	-0,282	0.027	0.087	0.274	0.040	0.218	660.0	-0.017		0.179	0.157	0.242	0.125	-0.016	0.050	1	0.111
		0.001	0.150	0.000	0.024	0.000	0.559	0.000	0.695	0,199	0.000	0.563	0.001	0.149	0.805		0.008	0.032	0.000	0.455	0.838	0.517	· .	0.102
	Sig. (2-tailed)					44-1		المريح	المعخ			844												
	4	196	219	207	217	190	211	216	219	219	217	208	219	218	214	219	218	185	219	38	173	173	219	219
in J	V Pearson Correlation	196 0.131	219 0.018	207 0.307	217 0.259	-0.057	-0.013	0.042	0.076	0.184	0.030	-0.025	D,095	0.252	0.128	0.051	0.610	0,168	0.050	38 0.005 0.959	-0.023	-0.026	0.111	1
in J	4	196	219	207	217					_										38 0.005 0.959 129	-0.023		0.111	. 1

Correlations

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Correlation is significant at the 0.05 level (2-tailed).
 Correlation is significant at the 0.01 level (2-tailed).

7.0 GEOPHYSICS

7.1 GRAVITY

In the exploration program of 1996, gravity data was collected from along the network of logging roads between Ryder Creek and Noke Creek, throughout the upper elevations of the Eddy property. Subsequent drill testing of some of the anomalous gravity data documented the presence of gabbro sills. These laterally extensive mafic sills have a higher density than the host strata of the Aldridge Formation and so should be expected to result in gravity anomalies. At this time, based on the available data and limited drill testing, the gravity data is considered to document the presence of gabbro sills in the sub-surface and the possible presence of base metal veins of limited extent. At this time, neither is considered to be an emphasis of the exploration program. As shear zones are associated with brecciation, then gravity lows may represent exploration targets of more interest, however, gold appears to be generally associated with quartz veins, which have densities very similar to the host sediments. Therefore, gravity surveys are not expected to contribute significantly to a exploration program for gold.

7.2 VLF-EM

The data from a total of 1333 VLF stations were compiled (see Appendix C). From these data, Fraser Filter values were calculated and plotted (Fig. 6), together with the Dip Angle data. The resulting data were then contoured so as to indicate areas having a Fraser Filter value greater than 5 (Fig. 6). The anomalies were contoured with an north-east-southwest bias on the assumption that they are related to the shear and fault structures interpreted to control gold-mineralization.

Due to the lack of geological control, it is difficult to interpret the anomalies beyond the immediate vicinity of their location. It is tempting to correlate the anomalies between known mineralized areas, such as between the Hill Vein and the Prospector's Dream areas, however, the features that the VLF-EM is responding to are unknown at this time.

Again, the data have been collected in, and surrounding, areas of known mineralization and so the resulting anomalies must be interpreted with caution. In general terms, however, the VLF-EM anomalies spatially occur in proximity to areas of known quartz veining, shearing and mineralization. In areas of dense data, the northeast trend is generally the best orientation in which to contour the data, arguably providing possible evidence for a VLF-EM response to northeast trending features. A subordinate amount of data was collected outside of areas of known mineralization (i.e. along the road between the Hill Vein and the OBFS and resulted in a low proportion of anomalies (low proportion of data though). An area of dense VLF-EM data in an area north of Weaver Creek and between the North Fork of Weaver Creek and the tributary draining the Prospectors Dream area, resulted in a proportionally high number of anomalies. The area consists predominantly of Fraser Filter values greater than 5, however, two soils lines through the area returned very weak anomalies for gold (1 samples greater than 275 ppb) and the remainder less than 16 ppb with most less than 3 ppb) and no value for the Gold Index (given a number of elements returning values below the detection limit).

The VLF-EM method requires rigorous evaluation of the anomalies delineated on the Eddy property prior to further utilization.

8.0 DISCUSSION

8.1 Deposit Types

Although potential exists for base metal mineralization, both as veins (i.e. Discovery/Shadow vein), vent ("fragmental") associated and/or (arguably) possible stratabound sedimentary exhalative (SEDEX)-type mineralization, the emphasis in recent years has been on further evaluation of gold mineralization. In simple terms, the mineralization is localized by or immediately adjacent to shear zones and, in many cases, in proximity to one or more gabbro sills (i.e. David, MC2, Prospector's Dream, Shadow Vein) which suggests structural control. The fine-grained sediments of the middle Aldridge generallyundergo plastic deformation in which a foliation develops through recrystallization of the silts into sheet silicates. In contrast, more competent units such as the quartz-rich wackes to quartzites deform by brittle means through the development of fractures. The gabbros may express the effects of deformation in a plastic manner if they have undergone hydration reactions resulting in the development of chlorite. Alternatively, they may behave in a brittle manner if they have not undergone a significant degree of chloritic alteration or if deformation occurred prior to significant alteration.

As such, the presence of competent units within a less competent package, such as gabbro sills within the middle Aldridge Formation strata or quartz-rich intervals within the middle and upper Aldridge Formation and the overlying Creston Formation were likely sites of a pressure gradient during deformation. Finally, on a larger scale, the Creston Formation is generally more quartz-rich, and therefore competent, than the underlying Aldridge Formation, which may explain the localization of the OBFS along the Aldridge / Creston contact through the Eddy property.

The models considered to apply include the generic polymetallic gold, Au-quartz veins and shear-hosted gold.

8.1.2 VEINS

The model currently being pursued to evaluate the gold potential on the Eddy property is that of veinhosted gold, in close association with gabbro sills and/or northeast-trending shear zones. The following quotes demonstrate a consistent emphasis over the past twenty years.

"The Galena Vein is 2.5 km NE of the MC2 Shear and on the same structure. A silicified zone at this locality averages .108 oz gold/ton across a 1.2 meter width at one of only two sample sites on the structure. The MC2 - Galena Vein shear zone has a strike length of 6 km across the Weaver claims; it has been sampled for gold only at surface and only at very few localities" (Klewchuk and Kennedy 1990).

"The attitude of the vein St. 35° Dip N.W. or S.W. 15° is almost sill like in form and is similar to Prospector's Dream structure some 12,000 feet to the northeast. It is possible the Hill & Prospector's Dream are structurally related and have been offset by Weaver #2 Shear" (Mason 1984).

"A few exposures of the Old Baldy Fault occur along a steep sidehill northwest of the Prospector's Dream area, notably near 547600N 569150E. The fault is a fairly wide zone of sheared middle Aldridge Formation quartzites, siltstones and argillites. The zone is variably silicified with fine disseminated pyrite as well as thin lensey quartz veins. Rock geochemistry done in 2002 apparently did not detect any significant gold mineralization. The Old Baldy Fault can be traced in float and sparse outcrop easterly to about 570000E where sample E4 returned only 0.2 ppb Au. To the west the position of the fault is uncertain across the ridge at ~ 568900E although there is considerable limonitic-altered float and some quartz vein breccia float near 1980-2000 m elevation on the ridge. Further west there is abundant quartz vein and altered float just east of the north fork of Weaver Creek near 568250E, 5475550N, suggesting the fault comes through here. Further to the southwest the fault zone is partially exposed by previous roadbuilding and trenching in the Galena Vein area. Rock sampling of sheared, silicified and pyritic fault zone material in 2002 from the Galena Vein area returned up to 3878 ppm Au from grab samples (Rodgers 2002).

This limited rock sampling along the Baldy Fault NW of the Prospector's Dream area indicates gold mineralization is present within the fault structure but is not consistently developed.

West of the north fork of Weaver Creek, a parallel-trending but narrower fault zone separates middle Aldridge Formation rocks to the southwest from Creston Formation rocks to the northwest. The AC (<u>Aldridge/Creston</u>) Fault parallels the Old Baldy Fault from the MC2 area (~565500E 5472900N) to the north fork of Weaver Creek and possibly further east toward Noke Creek. Anomalous gold was identified within the AC Fault in 1989 (Klewchuk and Kennedy 1990) and it remains a potential structural control of gold across much of the Eddy property" (Klewchuk 2004).

Data and observations to date have consistently noted the association of gold with quartz veins and shears. Many of these gold-bearing occurrences are spatially associated with gabbro and some suggest a structural control. For instance, the Galena Vein has a footwall contact with a gabbro (Ryley 1990) and the Discovery / Shadow Vein may be hosted within a gabbro. The David occurrence is closely associated with probable fault repeats of gabbro sills. These observations are interpreted to suggest the gabbros represent a potential structural control for mineralization. At the David property, the fault(s) repeat a number of gabbro sills, gabbro occurs at one (or more) contacts of a number of the shear-hosted or shear-associated quartz veins described and gabbro has been incorporated as fragments within a number of shears. These observations suggest that one or more of the faults identified within the Eddy property have been localized along and/or within gabbro for at least a portion of their trajectory. Furthermore, the described occurrence of magnetite, hematite

and/or specular hematite (specularite) suggests alteration of the gabbro by oxidized iron-bearing fluids, most likely in proximity to faults and/or shears.

Intrusions correlated to the Cretaceous Bayonne Magmatic Suite are a probable source of some of the fluids which have influenced the Eddy property, either through alteration and/or mineralization. There no fluid inclusion data known to the author for the local Cretaceous intrusions with which to document a magmatic contribution. However, as described briefly in the discussion on rock and soil geochemistry, there are, arguably, subtle indications of a magmatic contribution.

On a regional magnetic map for southeastern British Columbia, the Cretaceous intrusions have a characteristically strong magnetic signature, either within the intrusions themselves (i.e. Fry Creek Batholith, Mount Skelly Pluton, Reade Lake Stock) or as an oxidized aureole surrounding, or comprising the outer fringe of, the intrusion (i.e. White Creek Batholith). In addition, molybdenum is typically hosted within (i.e. Jaim / Elmo MINFILE occurrence) or immediately adjacent to many of these intrusions (i.e. Jodi MINFILE occurrence). Finally, as a result of development and refinement of the intrusion-related gold model, a characteristic geochemical signature has been proposed for these types of gold-bearing mineral occurrences, comprised of arsenic-antimony-bismuth-tungsten in a tungsten-bearing mineral province. A number of tungsten-bearing mineral occurrences are known within the Bayonne Magmatic Suite, of which the best known are those west of the Battle Range Batholith near Albert Canyon. Finally, analysis of the province's Regional Geochemical Survey (RGS) database suggests the Cretaceous intrusions in southeast BC can be regionally defined by anomalous uranium values.

The presence of magnetite, hematite and specular hematite suggests either a source of reduced iron that was subsequently oxidized subsequent to precipitation or, more probably, precipitation of these mineral phases from a fluid phase bearing oxidized iron. A number of oxidized iron occurrences have been documented throughout the Purcell Mountains, including the Iron Range and Gray Creek Pass. A number of much smaller occurrences have been documented within the Eddy property. Given the regional presence of strongly oxidized Cretaceous intrusions, the most probable source of oxidized iron would be these intrusions. The Kiakho stock occurs within the Cranbrook Fault and the Reade Lake Stock was intruded into the St. Mary Fault. Shearing within the St. Mary Fault suggests there was limited movement along the fault subsequent to intrusion. If this interpretation is correct, then magmatic fluids derived from the Reade Lake stock probably infiltrated the St. Mary Fault and utilized it as a conduit for fluid movement. If these fluids contained oxidized iron, then this provides a reasonable means of associating deposits of oxidized iron with at least one Cretaceous intrusion. The Kiakho stock might similarly have contributed iron-bearing fluids into the Cranbrook Fault and the Palmer Bar Fault, which occurs within the Eddy property. Similarly, molybdenum, uranium and the IRG suite of indicator elements might have been derived from Cretaceous intrusions and subsequently transported to, and precipitated within, the Eddy property along the mapped network of regional faults.

8.2 EXPLORATION MODEL

The following has been paraphrased from Walker (2002):

From a review of Höy (1993), it is interpreted that the St. Mary and Cranbrook faults were sealed by the emplacement of the Reade Lake and Kiakho intrusions, respectively, thus constraining the age of their latest movement. The emplacement of these intrusive bodies, as well as other Cretaceous age intrusive bodies of the Bayonne Magmatic Suite, is interpreted to have resulted in the infiltration of magmatic fluids into, and along, faults, including the Old Baldy Fault System, and utilized them as conduits for fluid movement.

Furthermore, the Cretaceous age monzonitic to syenitic intrusions of the Cretaceous Bayonne Magmatic Suite (including the Reade Lake, Kiakho and Mt. Skelly stocks), would also have provided local heat sources for formation (if any) and meteoric fluids within adjacent host rocks, which may have subsequently leached metals from host strata of the Purcell Supergroup. Finally, as these magmas crystallized, incompatible elements would have partitioned into the fluid (or vapour) phase and been liberated from the intrusions and incorporated into the adjacent convection cells.

The many faults mapped in the area are interpreted to have acted as fluid conduits, if present during intrusion, crystallization and subsequent cooling of the magma. As the Kiakho stock seals the Cranbrook fault and the Reade Lake stock similarly seals the St. Mary fault, they pre-date the intrusions. Furthermore, there is evidence for limited late stage movement on the St. Mary fault subsequent to intrusion in that deformation is evident in the Reade Lake stock along the projection of the St. Mary fault. Furthermore, the Moyie fault, like the St. Mary fault, has been interpreted to have been periodically re-mobilized. Therefore, it is interpreted that if the major faults in the area are documented or reasonably interpreted to have been active in the Cretaceous, a logical interpretation is that splays and conjugate faults may also have been similarly active. Movement on these faults, both magmatic and meteoric, and subsequent precipitation of metals. Specifically, veins having "... a metal assemblage which variably combines gold with Bi, W, As, Mo, Te, and/or Sb, and typically has a low base metal concentration ..." may represent a contribution from magmatic fluids analogous to intrusion-related gold systems (Lang et al. 2000).

8.2.1 Factors Contributing to Mineralization

In a simple convection model, the theory holds that fluids begin precipitating metals as they cool. However, other factors may provide barriers to fluid movement or otherwise initiate or enhance metal enrichment. Rising mineralized fluids, upon encountering these proposed barriers, are expected to have "pooled" along the stratigraphic and/or structural base of one or more of these proposed barriers and therefore to be prospective for potential mineralization.

Physical barriers are those which could be considered to impose impermeable limits to upward fluid movement such as gabbroic and/or dioritic sills. Possible examples include Moyie Sills in the upper Purcell Supergroup such as the paired gabbro intrusives mapped at Sundown time. Metal enrichments have been described associated with the Moyie Sills within the Aldridge Formation with the most significant being the mineralized David occurrence (MINFILE 082FSE108).

Other possible physical barriers which are possible within the Eddy claims would be the more competent lithologies, such as quartz wackes and quartzitic units within the more recessive siltstones and sub-wackes which characterize the Aldridge Formation.

In 2001, the author submitted a proposal under the British Columbia Prospector's Assistance Program to undertake evaluation of the area underlain, in part, by the current Eddy claims. It was proposed that intrusion-related gold (IRG) potential may exist in the area due to the proximity of a number of intrusive bodies of the Cretaceous Bayonne Magmatic Suite (including the Reade Lake, Kiakho and Mt. Skelly stocks) to, and within, major local and regional scale faults (i.e. Cranbrook and St. Mary faults, respectively). Anomalous and unusual metal assemblages have been reported in the Moyie and Perry Creek drainages, including bismuth, iron (as magnetite, hematite, siderite, etc), tungsten (both geochemically and as scheelite) and molybdenum. In addition, many gold (\pm base metals) mineralized vein occurrences are reported in these drainages, the largest of which has a reported resource of 96,000 tonnes of gold grading 13 grams / tonne (uncut) associated with anomalous magnetite-bearing Moyie sills (David - Minfile 082FSE108).

8.3 GOLD INDEX

The author has been working on development of a proprietary "Gold Index" with which to identify potentially gold-bearing areas in the Kootenay region. Work to date has been based predominantly on the provincial government's Regional Geochemical Survey (RGS) database and a number of property-specific databases. Based on the compiled analytical results for the Eddy property, the "Gold Index" was utilized in an attempt to delineate areas on the property for subsequent follow-up (Fig. 7). The Index is obviously constrained by areas for which rock and or soil geochemical results are available. Furthermore, as it has been developed on the basis of all the available data, taken predominantly in areas of known mineralization, it agrees well with the data. It has not been field tested and must, therefore, be interpreted with caution.

With the above qualifiers, however, some interpretation can be made, as follows:

8.3.1 Prospector's Dream

The soil lines oriented at a high angle to the "Frost Fault" at the southern end of the Prospector's Dream area confirm high grade values for the index straddling the fault. Moderate values extend to either side of the fault to the end of the lines, suggesting the possibility of an alteration halo associated with the fault in the host sediments.

8.3.2 Northwest of Prospector's Dream

A series of soil lines are located northwest of Prospector's Dream and northeast of the Galena Vein. The samples returned several areas of anomalous values in the immediate footwall (i.e. east of the OBFS) and along the ridge crest extending to the east-southeast from the OBFS. A feature of note and possible exploration interest is the fact that only low to weakly anomalous values occur within the mapped OBFS. If valid (and not an artifact of the Gold Index), this is consistent with observations made for Orogenic gold mineralized occurrences in which gold occurs adjacent to and/or within secondary structures, which may be the case for the Frost Fault.

Alternatively, there may be an as yet unidentified splay fault immediately north of the North Fork of Weaver Creek and extending northeast to the ridge crest where it is truncated. This interpretation, although possible, is not favoured as it requires two unmapped and unrecognized faults (or other impediment) to the mineralization.

8.3.3 Galena Vein

Weak values for the Gold Index are generally associated with the Galena Vein, together with some scattered highly anomalous values. The anomalous values appear to extend northeast to the southwestern portion of area described above, which, again, is located in the immediate footwall of the OBFS.

8.3.4 Weaver No. 2 M.C.

A very strong anomaly comprised of multiple, adjacent Gold Index values is evident at the MC2 shear area on the basis of soils taken in 1989 (Klewchuk and Kennedy 1990). On the basis of the map data available, the soils, once again, document anomalous values in the immediate footwall (i.e. east of) the OBFS. The anomaly is very strong and comprised of a large proportion of the data.

8.3.5 South Baldy Shear

Anomalous data are evident along the OBFS to the southwest of the MC 2 Shear area, in the probable location of South Baldy Shear, as defined in earlier exploration programs. Two long and a short contour soil lines extend around the headwaters of Ryder Creek in the footwall of the OBFS. The data document anomalous values on the southwest side of the creek but, apparently, do not extent to the northeast side. Given the apparent relationship between anomalous values in the immediate footwall of the OBFS, these data may document a northwest trending fault, with a dip to the northeast, placing the anomalous values in the footwall of the interpreted structure.

9.0 CONCLUSIONS

The presence of gold in association with quartz veins spatially associated with shears within and adjacent to the Eddy property has been documented in a number of independent exploration programs since 1984. Old workings, such as those in the Prospector's Dream area, document recognition of the gold potential and attempts to assess that potential as early as the 1890's.

This compilation report represents the first attempt at synthesizing the available information into a single exploration database. Much of the available data has been incorporated into the database and additional work can increase the exploration value of the database through determination of UTM coordinates for those samples lacking this data. In particular, a large number of analyses are available in the report of Morris (1987) and could be recovered by someone having better knowledge and more familiarity with the project. Some of these data were recovered in areas that have not been evaluated since 1987 (i.e. the road to Prospector's Dream).

The gold, on the basis of work to date, is hosted predominantly by quartz veins within, and/or adjacent to, shears and faults correlated to the Old Baldy Fault System, which transects the property from southwest to northeast. The quartz veins were precipitated subsequent to development of the associated shears, where hosted by such shears, which in turn have been interpreted in the case of the St. Mary Fault to have latest movement subsequent to intrusion of the Reade Lake stock in the Cretaceous. Therefore, many of the faults between the Moyie and St. Mary Fault and mapped on the Eddy property are probable Cretaceous and younger in age.

On the basis of a cursory evaluation of both the soil and rock analytical data compiled within this report, magmatic fluids derived from local intrusions correlated to the Cretaceous Bayonne Magmatic Suite are interpreted to have contributed to mineralized occurrences documented on the Eddy property. The presence of subtly anomalous arsenic, antimony, bismuth, molybdenum, tungsten and uranium, particularly given that strong correlations appear to be developed between many of these elements and gold is interpreted as possible evidence for the influence of an intrusion-related gold-type model for the property.

The presence of local intrusions of monzonites, syenites and other broadly "granitic" intrusions of the Cretaceous Bayonne Magmatic Suite, the presence of numerous faults (including the Old Baldy Fault System) and competent lithologies within the Aldridge and Creston Formations are all considered to have had a significant role in the localization of gold within and throughout the Eddy property.

On the basis of the rock and soil samples compiled for this report, a proprietary "Gold Index" was utilized in an attempt to identify areas of anomalous geochemistry based on a number of indicator elements specific to the Eddy property. As the "Gold Index" for the Eddy property is based on geochemical data within and surrounding areas of known mineralization, the apparent success of the Index in identifying anomalous areas may be due to a bias inherent in the samples. Acquisition of additional samples (i.e. along the possible Hill Vein - Prospector's Dream trend), together with the inevitable recovery of more samples having low to negligible values will allow the Index to be evaluated in a more rigorous manner. At this time it remains largely theoretical until the resulting anomalies are field tested.

43

The Eddy property has had a number of exploration programs over the past twenty years, largely focused on specific areas with only limited emphasis on the areas between known mineralized areas, most of which were identified as a result of road construction. An obvious question is that if the construction of logging roads, placed with no consideration of the underlying geology (but dictated by the geography arising as a result of underlying geology) has resulted in identification of significant gold-bearing mineralization, then how much more mineralization might be identified as a result of a logical exploration program.

To this end, further geological mapping is strongly recommended, directed toward establishing the location of the gabbro sills and faults, both a probable controls to gold-bearing quartz veins, throughout the property. Siltstone markers have been utilized with great success throughout the Aldridge Formation for precise determination of stratigraphic position. Markers have been documented on the Eddy property (i.e. Meadowbrook and Sundown) and further effort should be made to locate and identify these markers so as: 1) to further constrain stratigraphic position, 2) allow stratigraphic projections to be made, and constrained, between outcrops, 3) to identify areas of stratigraphic inconsistencies which would probably indicate the presence of faults and 4) to allow determination of offsets in faults. North to northwest-trending faults have been proposed along the Weaver Creek drainage on the basis of the orientation of the drainage and its linear nature, however, there is no other information with which to evaluate this hypothesis.

Geochemistry, through soil and rock samples, have been useful in identifying anomalous areas, however, previous surveys have been largely localized in specific areas within and surrounding areas of known mineralization. Soil surveys should be undertaken across the trend of the possible Hill Vein - Prospector's Dream trend, perhaps as an initial series of contours on either side of Weaver Creek. Heavy mineral concentrates were particularly effective as a part of the 1989 program and consideration should be given to utilizing such samples again. Regularly spaced samples along Weaver Creek might assist in evaluating the possibility of the Hill Vein - Prospector's Dream trend.

Given the apparent preferential mineralization in the footwall of the OBFS, consideration should be given to acquisition of additional soils along its trend between areas of known mineralization. Soil lines should extend across the OBFS into the hangingwall side to a limited degree in the event the data to date is biased. Four short to moderate length soils lines were completed in the headwaters of Ryder Creek in the immediate footwall of the OBFS. As this is an area where a number if splays have been mapped, extending northwest into the Perry Creek drainage, further soils should be taken to assess the area along the OBFS from Ryder Creek to Weaver Creek and the Weaver No. 2 M.C. (MC2 Shear) area.

10.0 RECOMMENDATIONS

- 1. To the extent possible, complete compilation of the geochemical database pertaining to the Eddy property by determining UTM coordinates for all remaining sample sites,
- 2. Maintain the geochemical and geophysical databases by appending new data each year for all subsequent programs to facilitate future analysis and plotting of the data,
- 3. The value of heavy mineral concentrates was demonstrated in 1989 through the work of Klewchuk and Kennedy (1990). Further sampling should be considered for the watercourses transecting the property. Anomalous samples along the lower elevations of Weaver Creek for instance may represent gold transported from the known occurrences at higher elevations, but may, alternatively, represent gold from as yet unidentified occurrences. For instance, the Sundown sills, and associated shears, probably extend from the Hill Vein to Prospector's Dream, both of which have auriferous gold. It is possible that auriferous quartz veins / shears extend into, and through, Weaver Creek at approximate UTM coordinates 569200 E, 54723000 N. A series of heavy mineral concentrates at regular intervals along the drainages is expected to assist in the identification of unidentified occurrences, if present,
- 4. Two different sets of stratigraphic markers are available for the property, the Aldridge "Markers" (laminated siltstone markers) and the Sundown sills. Although the property has been described as having 95% cover, an effort should be made to map the stratigraphy throughout the property so as to identify, and quantify, fault offsets. It has been proposed that some, or all, of the east-west trending drainages represent cross-cutting faults highly oblique to the Old Baldy Fault System (Klewehuk, pers. comm. 2005). Obviously, if such faults are present, then identification of offsets should be possible and the intersections of orthogonal faults would be a valid exploration target for subsequent evaluation,
- 5. Soil samples have been utilized to date with positive results. Continued sampling should be considered to extend geochemical coverage to those areas between known mineralization. In particular, soil coverage should be considered so as to cover the entire Old Baldy Fault System and the areas along the trend of the possible Hill Vein Prospector's Dream system,
- 6. Obviously, continued recovery of rock samples is recommended to evaluate areas of potential gold mineralization. Further work is recommended to assess areas of obvious alteration (bleaching, silicification, chloritization, etc) as well as areas of mineralization (magnetite, hematite, specular hematite). Rodgers (1998) sampled 1.5 tonnes of material hand selected from ore grade stockpile, in which the **pieces chosen contained massive hematite with or without visible gold** and from which they recovered over 30 grams of gold,
- 7. Ground geophysics (VLF-EM) is recommended as it appears to be contributing useful information to the program. However, an effort should be made to critically evaluate the anomalies arising from the VLF-EM surveys.

- 8. In the event subsequent evaluation of VLF-EM anomalies confirms they are providing valid indications of mineralization, proximity to mineralization and /or alteration associated with mineralization, infill surveys should be considered along the trend of the OBFS and the possible Hill Vein Prospector's Dream trend.
- 9. An effort should be made to accurately ascertain the location of all previous trenches, together with the results of any associated sampling. These data should be plotted on the property base map at a scale suitable to show the results.
- 10. Given the model of mineralization associated with shearing and, in particular, an orogenic model in which mineralization is expected to be better developed in secondary structures, then the area in the northwest portion of the property underlying the Eddy 58-63, 34-47 and 7-14 claims should be given early emphasis to evaluate the area of the north-northwest trending splays off the OBFS into the Creston Formation. If warranted on the basis of this early evaluation, consideration should be given to acquiring additional claims to the west and north of the Eddy property and west of the Galway claims.
- 11. Additional trenching should be considered to test those mineralized areas identified on the basis of soil sampling, VLF-EM surveys (if determined to accurately detect areas with anomalous mineralization) and/or along the trend of known mineralized veins and/or faults.
- 12. To date, the property can be reasonably considered to be untested by diamond drilling. The drill program supervised by Morris (1987) was apparently poorly planned and completed with regard to testing the features of interest. The 1996 program by Jones (1996) drill-tested an anomaly which was subsequently identified as a gabbro. It is the author's understanding that the gold-bearing areas, auriferous veins / shears and/or potential host structures remain untested. Therefore, diamond drilling should be considered in areas of good surface control (i.e. soil / rock geochemistry, geological mapping, trenching and/or VLF-EM anomalies).

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Appendix A

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Statement of Qualifications

STATEMENT OF QUALIFICATIONS

I, Richard T. Walker, of 656 Brookview Crescent, Cranbrook, BC, hereby certify that:

- 1) I am a graduate of the University of Calgary of Calgary, Alberta, having obtained a Bachelors of Science in 1986.
- 2) I obtained a Masters of Geology at the University of Calgary of Calgary, Alberta in 1989.
- 3) I am a member of good standing with the Association of Professional Engineers and Geoscientists of the Province of British Columbia.
- 4) I am a consulting geologist, residing at 656 Brookview Crescent, Cranbrook, British Columbia.
- 5) I am the author of this report which is based on a compilation of data available in the public domain, largely from Assessment Reports on file with the BC Ministry of Energy and Mines, some of which remain on confidential hold and were provided by Ruby Red Resources Inc..

Dated at Cranbrook, British Columbia this 30th day of March, 2004.

ESSIO R. T. WALKER BRITISH COLUMBIA Richard T. Walker, P.Geo. OSCIEN'

Appendix B

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Excerpts - Minister of Mines Reports

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MINFILE Reports

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Excerpts from the Minister of Mines Reports

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To the west of Weaver Creek and at the base of the hills forming the divide between it and Perry Creek, quite a number of mineral locations have been made and a considerable amount of work done. The claim best known and most developed is the *Prospector's Dream*, around which are grouped the Old Abe, Last Chance, Annie, Ben d'Or, Parker, Lennis, and the *Pauper's Dream Fraction*. How these claims lay I could not exactly determine, so much restaking had been done, as many as twelve posts being found within a radius of as many feet, and nothing short of an actual survey would untangle the claims. The same general conditions, however, apply to each, and I was able to identify certain works as belonging to certain of the claims.

Owned by J. C. Green *et al*, Fort Steele. The country rock, seemingly, Prospector's is entirely of igneous origin, probably a symite or diorite. A quarte voin bas been exposed, outcropping nearly horizontally along the hillside, and Mineral Claim. dipping into the hill N. 30' E. at an angle of 15'. This has been developed by a 20-foot open cut leading to a 40-foot inclined tunnel, both on the voin.

In the open cut the quarts was very much broken, but nearer the mouth of the tunnel the vein was more solid and showed a width of 5 feet of solid quarts. Following the tunnel down, the width of quarts seems to gradually diminish, until at 40 feet in, the vein has only a width of some 6 inches. About 15 tons of quarts, of a rusty nature, was piled on the dump, which is said to run \$10.00 in gold to the ton. The vein-matter will show free gold in the pau almost anywhere, but not indicating high values. The apparent pinching out of the vein in this one tunnel has discouraged for a while, deeper prospecting and the continuity of the vein to the dip remains to be proven.

Whether the gold obtained is the result of the weathering of iron sulphides carrying gold, or whether it will continue to a depth as free gold, has not yet been determined.

I am informed that one or more shafts have been sunk on this property on another vein, but these shafts I was unable to find, being filled, doubtless, with water. In these the vein showing is said to be nearly vertical and to carry a width of some 5 feet of quarts with gold values.

Old Abe, owned by Steve Young et al, of Fort Steele, is practically an extension of the claim just mentioned.

Located by Nitzel and Johnson, is supposed to lie between Old Abs Pauper's Dream and the Prospector's Dream, some 100 feet east of the workings on the Fraction. Istter. The area of this fraction is uncertain, until the prior claims have been surveyed. There has been some work done on the property, consisting

of an open cut and two tunnels, 10 and 8 feet respectively. The fraction was evidently located to eatch that portion of the *Prospector's Dream* lead which may not be covered by the main claims.

The Last Chance, owned by Wm. Haupt et al; War Kagle, Hy. Kershaw et al; Annie, Wm. Thompson et al; Ben d'Or, J. C. Green et al; Parker, Gue Theise, and Lennie, J. S. Parker, all of Fort Steele, are all locations in the same vicinity, but with only slight development work done on them that I could find. The limits of these claims I was unable to distinguish without a survey, in the absence of the owners to point out the true lines.

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Appendix C

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Compilation of Analytical Results

Soil Analytical Results

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Line Samp	e Easting	Northing	Mo C	u Pb	Zn	Ag Ni	Co	Ma Fe	As	U Au	Th	Sr Cd	Sb	9 Bi	V Ca	Р	La Cr M	Ag Ba	TI B AI	Na	κw	/ Ho	Sc T	s	Ga Se S	Sample Au	r"Au s	Si Be
1 1	•							ppm %						n pprn p	om %	* ;	opm ppm 9	6 ppm	% ppm %	%	% pp	•	ррпт рр		nqq mqq	ppm pp	•	× pom
EW1 000S		5474884			2 78	0.2 11.4	9.6	219 2.72				7 0		2 0.3			7 8.8 0.			5 0.015	0.08 0	3.1 0.0		0.1 < 05	10 <.5	ີ 15	18.9	
EW1 025S		5474884	0.9 1			0.1 5.8		184 3.01				9 0			35 0.14		11 10.4 0.					0.0	3 2.1	0.2 < .05	10 <.5	15	10.2	
EW1 050S		5474904		7.4 12.				367 3.58		0.9 1.		12 0			77 0.19		13 9.7 0.					0.0		0.3 <.05	11 <.5	15	1.7	
EW1 0755 EW1 1005	569120	5474928 5474950	0.7 1			0.2 10.0		282 2.76		0.5 15		7 0			35 0.09		12 10.6 1		30.076 12.04 30.044 < 11.54			0.2 0.0 0.1 0.0		0.1 <.05	9<.5 5<5	15 15	15	
EWT 1005	569136.7	5474969		1.2 10. 0.4 23.		0.1 10.4		462 2.28		0.6 56.7		8 0			30 0.05		14 11.5 0		0.044 1 1.54			2.1 0.0 2.1 0.0		0.1 <.05	3<.5	15	37 56.7	
EW1 1505	569145.9		0.5 1			0.1 9.4		98 1.75		0.5 13.2		4 0			21 0.03		13 10.5 0.		2 0.048 <1 1.7		4.4.	21 0.0		0.1 < 0.0	5<5	15	13.2	
EW1 175S	569158.3	5475018	0.8 1			0.4 1		282 2.23		0.6 405		5 0			23 0.04		17 10 0.		0.059 <1 1.9			0.2 0.0		0.1 <.05	6<.5	15	404.7	
EW1 200S	569163.6	5475040	0.6	11 1	0 51	0.2 10.1	f 9,4	201 2.03	4.3	0.7 11.8	5.9	4 0.	2 0	2 0.3	24 0.03	0.051	16 10.6 0.	25 80	0.052 1 2.11	0.012	0.04 0	0.1 0.0	4 1.6	0.1 <.05	6 < .5	15	11.8	
EW1 225S	569171.8		0.6 1			0.1 10.4		88 2. 6		0.7 11.2		4 0.			21 0.03		23 9.8 (0.027 <1 1.23).1 0.0		0.1 <.05	5 < 5	15	11.2	
EW1 250S	569180			3.7 7.		0.1 14.3		149 2.5		0.7 21.4		6 D.			24 0.03		22 11.5 0		3 0.032 <1 1.5			3.1 0.0			5 <.5	15	21.4	
EW1 275S	589187	5475113	**** *	t.5 5.		<.1 12.5		164 2.17		0.7 9.8		30.			20 0.02		23 9.9 0.		3 0.024 <1 1.3			0.1 0.0		<.05	4<.5	15	9.8	
EW1 300S EW2 350N	569194.1 569034.8	5475138 5474845		5.8 9. 7.8 18.		0.2 14.0		149 2.48 281 2.57		0.7 8		5 0. 6 0.			32 0.04 28 0.05		13 11.6 0. 14 14 0.		3 0.071 <1 2.49 0 0.087 1 2.75			0.1 0.0 0.2 0.0		0.1 <.05 0.1 <.05	7<.5 7<.5	15 15	8 5.8	
EW2 325N	569044.3			B.1 13.		0.1 10.5		186 2.55		0.7 1.1		5 0.			30 0.07		10 12.1 0.		0.095 1 2.37			0.2 0.0		0.1 <.05	8<.5	7.5	1.1	
RE EW2 325N	569044.3			8.5 12.		0.1 10.4		187 2.61		0.7 < 5	5.5	5 0.			29 0.08		10 12.1 0.		0.084 1 2.38			0.1 0.0		0.1 <.05	9<.5	7.5	<.5	
EW2 300N	569055.6		0.8 1	1.4 13.				199 3.04		0.7 3.7	3.8				34 0.1		9 12.5 0.		3 0.112 2 2.5			0.2 0.0		0.1 <.05	12 < 5	15	3.7	
EW2 275N	569067.8	5474911	D.8 1	0,4 17.	3 43	0.1 8	3 4,4	74 2.54	3.9	1.3 6.2	4.8	90.	t D	3 0.3	24 0.11	0.052	23 10.2 0.	.19 37	0.044 <1 1.52	0.005	0.05 0	0.1 0.0	5 1.3	0.1 <.05	7 < 5	15	6.2	
EW2 250N	569079.4		0.8 1					498 2.27		0.6 22.5					23 0.05		20 10.8 0.		0.053 1 1.96			0.2 0.0		D.1 <.05	6 < 5	15	22.5	
EW2 225N	569088.7	5474951		7.2 18.				246 2.4		0.7 79.7		4 0.			22 0.02		19 10.4 0.		0.055 <1 1.86			0.1 0.0		0.1 <.05	6 < 5	15	79.7	
EW2 200N	569100.3		0.8 1					410 2.34	3.5	0.8 17.2		6 0.			28 0.04		17 13.6 0.		0.058 1 2.0			0.1 0.0		0.1 < 05	7 < 5	15	17.2	
EW2 175N EW2 150N	569109.9 569117.7			3.7 12. 12 14				783 2.27 598 2.43		0.7 9.4		50. 50.			29 0.04 31 0.04		14 11.9 0.		0.076 2 2.32 0.069 <1 2.1			0.1 0.0 0.2 0.0		0.1 <.05	7<.5 8<.5	15 15	9.4 52.6	
EW2 150N	569126.2	5475020		12 14.				462 2.09		1.1 3.7		7 0.			24 0.05		6 8.7 0.		0.12 1 3.84			0.1 0.0		0.1 < 05	9<.5	15	3.7	
EW2 100N	589136.7	5475063	1 2					238 2.22		1.1 8.6		6 D.			28 0.04		5 9,1 0.		0.129 1 3.99			0.2 0.0		0.1 <.05	9<.5	15	8.6	
EW2 075N	569147.4		0.9 1	7,8 8.				224 2.54		0.8 18.7		5 0.			30 0.03		24 12.4 0.		0.042 <1 1.83			0.1 0.0	3 1.4	0.1 <.05	6<.5	15	16.7	
EW2 050N	569159	5475110	0.9 14	3.3 10.	7 42	0.2 15.3	11.3	258 2.59	5.1	0.8 8.4	6.3	8 0.	1 0	2 0.4	32 0.05	0.044	13 12.3 0.	26 83	0.089 1 2.57	0.01	0.05 0	0.2 0.0	(1.9)	0.1 <.05	8<.5	15	6.4	
EW2 025N	569167.4		1.2 1					110 2.69		0.7 4.8		8 C.			29 0.03		16 11.4 0.		0.067 1 2.08			0.0		3.1 < 05	8 < 5	15	4.8	
EW2 000N	589174.6		1 1/					421 2.46		0.8 6.5		4 0,			26 0.03		16 11.7 0.		0.058 1 2.11			2 0.0		0.1 <.05	7 < 5	15	6.5	
EW3 000S	568999.2							279 2.27		0.8 1		9 Ó.			28 0.06		10 10.7 0.		0.103 1 2.33			0.2 0.0		0.1 < 05	9<.5	15	1	
EW3 025S EW3 050S	569010.8 569019.8		0.7	13 15. Lá 14.		0.1 11.4		184 2.33		0.8 46.3		\$0. 50.			21 0.09		21 10 0. 9 9.3 0.		0.042 <1 1.08).1 0.0).1 0.0		0.1 <.05 0.1 <.05	6<.5 7<.5	15 15	46.3 3.1	
EW3 0303 EW3 075S	569030.6			1.4 14. 1.7 19.				156 2.28		1.5 5		7 0.			27 0.05		13 14,1 0.					0.1 0.0		0.1 <.05	\$<5	15	5	
EW3 100S	569037.5			16 14				413 2.29		0.8 19.9					28 0.04		11 10.9 0		0.096 1 2.67			0.2 0.0		0.1 < 05	8<5	15	19.9	
EW3 125S	569048.6	5475010	1	1.5 14.		0.1 8.8		243 2.03				5 0.			29 0.04		12 8.5 0.		0.065 2 1.56			0.1 0.0		1 <.05	7 < 5	15	18.0	
EW3 150S	569057.1	5475034	0.9 2			0.2 16	5 10	175 2.25	5.4	0.9 19.4	8	4 0.		3 0.4			22 12.4 0.	36 78	0.04 2 1.78	D.004	0.05 0).1 0.0).1 <.05	5 < 5	15	19.4	
EW3 175S	569067.6			2.1 11.				261 2.01		0.9 5.1		7 0.		2 0.3			8 10.3 0.		0.109 1 3.12			0.2 0.0		1 <.05	7 0.5	15	5.1	
EW3 200S		5475080		5 13				237 2.33		1 11.3		5 0.		.2 0.4			9 12.2 0.					0.2 0.0		0.1 <.05	8<5	15 15	11.3	
EW3 225S EW3 250S	569090.2	5475102 5475125						150 2.27 296 2.04		0.8 19,3		6 0. 5 0.			30 0.03 29 0.04		15 ±1.3 0. 7 9.8 0.		0.082 1 2.54 0.132 3 3.85).2 0,0).2 0,0).1 < 05).1 < 05	8<.5 9 0.5	15	2 19.3 5.2	
EW3 275S		5475149		15 11				179 2.13		1.2 1.2					30 0.04		12 11.5 0.		0.102 3 3.65			0.2 0.0		1 < 05	¥ 9.5 8<.5	15	J.2 9	
EW3 300S	569115.5	5475189	1 1					177 2.29		0.8 7					28 0.03		20 14.2 0		0.047 1 2.17			0.1 0.0		1 < 05	6<.5	15	Ť	
NW1 000S	\$68075.7		0.4	5.2 8.				114 1.3		0.5 2.3		4<.1			11 0.03		21 7.5 0		0.014 1 0.9			0.0 1.0		<.05	3<5	15	2.3	
NW1 025S	568099.4	5475180		2.7 20.				127 2.33		1.1 <.5	7	11 0.			23 0.07		21 13.4 0.		0.047 1 2.65			.2 0.0).1 <.05	7 < 5	15	<.\$	
NW1 050S				7.2 1		0.1 6.8		111 2.32		0.8 5.4		7 <.1			28 0.07		17 10 0.		0.078 1 1.96			0.0).1 <.05	\$<.5	15	5.4	
NW1 075S	568125.6			5.9 10.		<.t 7.8		92 1.8		0.6 0.8		5<.1			19 0.04		15 8.9 0.		0.038 <1 1.63			0.1 0.0			5<5	15	0.8	
NW1 100S NW1 125S	568141.1 566159	5475124 5475108		13 18. 11 13.		0.1 11.8		73 2.23		1.4 1.3 0.8 <.5		9 0. 4,1 1			29 0.07 33 0.16		9 10.2 0 6 10.7 0.1		0.111 1 4			0.1 0.0 0.2 0.).1 <.05).1 <.05	10<.5 9 0.5	15 15	1.3 <.5	
NW1 1255 NW1 1505	568178.4	5475088		9 10.				304 2.37		0.9 1.6					34 0.07		5 11 0.		0.105 1 4.14			.2 0.0			10 <.5	15	1.6	
NW1 175S	558194.8	5475073		9 9				94 2.58		0.6 13.5					36 0.07		8 10.8 0.		0.084 1 2.90			.1 0.0		1 < 05	8<5	15	13.5	
NW1 200S	568211	5475058	1.1 1		8 40	0.1 19.3	25.9	230 3.14	3.8	0.9 6.2	4.7	9 C.	1 0.	2 0.5	64 0.08	0.062	9 16 0.	61 112	0.097 1 3.34	0.012	0.05 0	2 0.0	540	1 <.05	9<.5	15	6.2	
NW1 225S	568228.5	5475039		11 9.:				290 2.71		0.6 1.9		7 Q.			58 0.05		5 11.8 0.					2 0.0		1.1 < 05	11 <.5	15	1.9	
NW1 250S	568244.1	5475021	1.2 2					294 3.4		0.8 3.3					58 0.11		7 16.4 0					2 0.0		11 < 05	12 < 5	7.5	3.3	
RE NW1 2505 NW1 275S	568244.1 568260.7	5475021 5475002	1.1 23 0.8 21					303 3.22 316 2.87	4.4 3.7	0.8 4,1		10 0. 13 0.			80 0.11 33 0.2		8 16.2 0. 11 12.2 0.					0.2 0.0 0.1 0.0),1 ≺.05 }.1 ≺.05	12 0.5 8<.5	7.5 15	4.1 184.3	
NW1 2755 NW1 300S	566276.5	5474982	0.9 2					340 2.07		0.7 57.2		8 0.			40 0.12		14 13.6 0.					1 0.0		1 < 05	8<.5	15	57.2	
NW1 325S	568291.9	5474963		4 33.				534 2.9		0.8 42		14 D.		2 0.5			11 14.1 0.					2 0.0		1 < 05	8 0.5	15	42	
NW1 350S	568307	5474942			2 62	0.4 21.1	17.3	418 3.4	- 4	0.5 44.8		70.			61 0.09		13 15.5 0.					.3 0.0		1.1 < 05	9 <.5	15	44.8	
NW1 375S	568323.4	5474923	0.9 9:					5057 3.07		1.2 9.9		19 0.			60 0.38		14 13.8 0.							1.1 < 05	9<.5	15	9.9	
NW1 4005		5474905	1.3 3					590 3.46	5.3	1 32.0		5 0.			48 0.05		20 15.5 0.					2 0.0		1 < 05	8<.5	15 15	32.8	
NW1 425S NW1 450S	568357.8 568379.2	5474892 5474878	1.4	58 30. 18 15		0.3 27.8		540 3.62 435 2.48	8.1 ≰9	2 55.9		6 0. S 0			43 0.04 38 0.08		21 14.8 0	32 124				1.2 0.0 1.2 0.0		1 < .05	9<.5 9<5	15	55.9 15-4	
NW1 475S	568399.9	5474863	1 2					435 2.46		0.5 1.6	5.0	15 0.			36 0.06		8 10 0.			0.012		12 0.0		1 < 05	10 < 5	7.5	15.4	
NW1 500S	568418.4	5474847	0.5 1					226 1.9		0.6 2.7	3	11 0.			34 0.14		8 8.9 0.		0.093 1 1.83					1 < 05	9<.5	15	2.7	
NW1 5255	568438.1	5474827	0.7 30	5 13.	2 81	0.1 13.5	14.3	280 2.59		0.5 5.1	4.1	8 0.			54 0.11		12 10.4 0.		0.078 1 2.01	0.011	0.08 0	1 0.0		1 < 05	8<5	15	5.1	
NW1 550S	568450.4	5474807	0.5 28					134 2.45	3.6	0.7 15.6	5.2	5 < 1			40 0.06		14 10.2 0.3		0.055 <1 1.87	0.007		.1 0.0		1 < 05	8 < 5	15	15.6	
NW1 575S	555487.4	5474790	0.6 52					481 2.33		2.1 5.1	5.1	19 0.			40 0.2		25 15.7 0		0.027 1 2.14		0.05 0			1.1 <.05	7 <.5	15	5.1	
NW1 600S		5474770	0.6 1					125 2.42	2.8	0.5 8.1	4.9	7 < 1	-		35 0.07		15 12 0.		0.061 1 1.96	0.008				1.1 < 05	7<.5	15	5.1	
NW1 825S NW1 850S	568497.1 568512.5	5474753 5474733	0.7 21					195 2.54 177 2.29	4	0.7 6.8	3.5 3.8	16 C. 7 O.		2 0.3 2 0.3	44 0.25		8 9.5 0.1 7 8.7 0.1		0.128 2 3.34	0.022				1 < 05	11 <.5 10 <.5	15 15	6.8 0.5	
NW1 6505		5474733						506 2.44						2 0.3			5 9.6 0.1		0.12 1 4.18	0.016				1 < 05	9 < 5	15	1.1	
NW1 700S		5474693												1 0.3			14 12.3 0.3					1 0.03		1 < 05	8 < 5	15	2	
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NW2 600N NW2 575N	588584.5 568570	5474759	0.7 0.8	10.9		23 0.1		7.1 175 1.79		2.2 <.5 1.1 4.5	6.6	6 0.1			21 0.08 0.076		0.1 0.37		1 3.04	0.01 0.1		0.04	2	0.1 < 05	7 < 5	15	4.5	
NW2 550N		5474793	1.5	9.8		35 < 1		14.2 300 2.83		1.6 1.6	7.4	4 < 1			23 0.03 0.06		3.2 0.72		1 2.53	0.005 D.		0.04	1.7	0.1 <.05	8 <.5	15	1.6	
NW2 525N		5474811	1.6					21.5 291 2.77		1 1.7	5.4	6 0.1			34 0.06 0.074		1.6 0.31	99 0.1	1 2.85	0.012 0.0	06 0.2	0.04	2.2	0.1 <.05	10 <.5	15	1.7	
NW2 500N		5474827	1.4			37 0.1		23.3 271 2.81		1.2 12.3	8.4	7 0.1	0.2	0.4	32 0.06 0.071	13 1	1.8 0.47	103 0.083	1 3.2	0.013 0.	06 0.2	0.05	2.9	0.1 <.05	8 <.5	15	12.3	
NW2 475N		5474845	2.1		11.3	43 0.1	30.9	51.2 218 4.87	6	1.6 9.7	7.4	5 <.1	0.3		69 0.04 0.07		9.5 1.13			0.007 0.1		0.04	7	0.1 < 05	9 <.5	15	9.7	
NW2 450N	568468.3	5474882	1.4	21.2				37.2 257 4.35		1 9.8	5.3	7 0.1			82 0.07 0.049		9.6 1.26		1 3.39	0.008 D.I		0.03	8.1	0.1 <.05	10 <.5	15	9.6	
NW2 425N	568470.2		1.1					28.9 268 3.5		0.9 15.1	5.7	8 0.1			54 0.08 0.078			125 0.098	2 3.57	0.011 0.1		0.04	3.7	0.1 0.06	9 <.5 10 <.5	15 15	15.1	
NW2 400N	568450.4							15.5 514 2.85		1 95.4	5.2	15 0.1 9 0.2			37 0.21 0.041		2.6 0.36	152 0.102 195 0.108	2 2.86 2 3.19	0.016 0.1		0.04	2.4 2.4	0.1 <.05 0.1 <.05	10 < 5	15	95.4 91	
NW2 375N		5474903	1.5			75 0.6		18.1 485 3.19		0.8 91 1 17.8	6.4 6.5	P 0.2 10 0.4		0.6 0.7	42 0.12 0.038			214 0.083	2 2.59	0.014 0.		0.05	2.9	0.1 <.05	9 0.5	7.5	17.8	
NW2 350N RE NW2 350N		5474911 5474911	1.6 1.6					22.7 2700 3.47 22.2 2707 3.27		1 26.6	6.1	9 0.4	0.3		40 0.09 0.04			215 0.077	3 2.44	0.007 0.		0.05	3	0.1 < 05	9<.5	7.5	26.6	
NW2 325N		5474923						16.6 361 3.39		1.1 33.2	6.1	7 0.2	0.3	0.4	56 0.07 0.116		14 0.53		3 4.7	0.011 0.		0.06	- 4	0.1 <.05	11 0.7	15	33.2	
NW2 300N	568371.2		1.1			52 0.2				0.7 14	5.1	7 0.1	0.2	D.5	49 0.09 0.035		4.7 0.78		1 2.11	0.006 0.	06 0.2	0.03	3.6	0.1 <.05	B <.5	15	14	
NW2 275N		5474955	1.2				24.6	24 324 3.77		1.9 62.6	11.8	5 0.1	0.3	0.7	40 0.04 0.046		4.7 0.88		1 2.91	0.004 0.0		0.03	- 4	0.1 <.05	7 <.5	15	52.8	
NW2 250N		5474971	1.9	64.3	73.6	121 0.3		38.9 1364 4.2		2.2 30.5	8.2	9 0.2			45 0.1 0.054		7.7 0.79		1 3.25	0.006 0.1		0.04	3.7	0.1 < 05	9 0.5	15	30.5	
NW2 225N		5474991		17.2		84 0.1		12.8 428 2.87		0.7 11.7	5.8	6 0.1			40 0.1 0.035		2.5 0.35		1 2.41	0.011 0.0		0.03	1.9	0.1 < 05 0.1 0.07	10 <.5 11 <.5	15 15	11.7 5.2	
NW2 200N		5475011				64 0.3		8.6 971 2.6		0.7 5.2	4.7	12 0.2			36 0.1 0.085		0.3 0.19		1 4.01 1 2.62	0.02 0.0		0.04	2.3	0.1 <.05	8 < 5	15	11.4	
NW2 175N		5475024				56 0.1		8.1 209 2.52		0.7 11.4	5.1				33 0.09 0.086 29 0.06 0.066		2.8 0.3 2.5 0.41		1 2.31	0.009 0.		0.04	2.3	0.1 <.05	7 < 5	15	14.3	
NW2 150N		5475044				57 0.1		12.5 188 2.53		0.8 143	5.9 4.7	-8 <.I 14 0,1			35 0.18 0.026		13 0.46		1 1.88	0.03 0.		0.01	2.1	0.1 < 05	6 < 5	15	29.4	
NW2 125N		5475060				50 0.1 55 0.1		9.7 1071 2.17 6.6 147 2.75		1.2 29.4 0.4 3.6	4.3	14 0.1 7 0.1		0.4	40 0.08 0.093		10 0.24		1 1.53	0.008 0.		0.02	1.6	0.1 <.05	8 <.5	15	3.6	
NW2 100N NW2 075N		5475077 5475093				55 0.1 72 0.1		8.4 374 2.32		0.5 3.1	4.4	8 0,1			38 0.08 0.091		0.8 0.25		2 2.49	0.011 0.		0.03	2.1	0.1 <.05	8 <.5	15	3.1	
NW2 050N		5475112		24.9		42 0.1		8 240 1.98		0.7 12.5	5.9	4 0.1			25 0.05 0.049		8.4 0.39			0.005 0.		0.01	1.7	0.1 <.05	4 <.5	15	12.8	
NW2 025N		5475131	1.1			58 0.1		9.2 258 2.19		1 0.7	4.5	5 0.1			36 0.05 0.211		9.2 0.11		2 5.06	0.015 0.0	0.2	0.06	2.7	0.1 0.07	11 <.5	15	0.7	
NW2 000N		5475150				51 0.2		7.6 253 1.98		0.9 1.5	4.1	9 D,1			31 0.09 0.149	3 5	7.8 0.15	70 0.143	2 3.85	0.016 0.	05 0.2	0.05	2.2	0.1 <.05	9 < 5	15	1.6	
NW3 000S		5475259				61 0.1		12.2 290 2.43		1.2 2	5.3	9 0.1			33 0.08 0.085	5 10 1	1.1 0.26	107 0.121	2 3.7	0.013 0.	06 0.2	0.06	2.5	0.1 <.05	9 <.5	15	2	
NW3 0255		5475239	1.3			34 0.1	12.6	10.9 87 2.54	3.9	1.2 2.1	5.2	7 0.1	0.2	0.3	38 0.06 0.073	3 6 1	1.6 0.2		1 4.37	0.017 0.		0.1	2.2	0.1 <.05	11 <.5	15	2.1	
NW3 0505	568313.5	5475216	8.0	7.6	12.6	35 < 1	16.7	17.8 418 2.29	3	1.9 11.7	5.1	17 <.1	0.3	0.3	27 0.15 0.055		1.2 0.35		2 1.79	0.011 0.0		0.02	2	0.1 0.11	7 <.5	7.5	11.7	
NW3 075S	588322.2	5475193	1.3	10.3	15.8	32 0.1	15.3	19.7 203 2.22	2.6	2.2 0.5	7.3	12 0.1			25 0.11 0.027		2.2 0.49		1 1.95	0.007 0.0		0.03	2.2	0.1 <.05	7 <.5	15	0.5	
NW3 100S	568329.8	5475184	1.5	10.9	12.7	53 0.1	15.4			0.8 5.2	5.8	0 0.1		0.3	10 32 0.07		2.2 0.23		2 3.05	0.011 0.0		0.06	2.1	0.1 < 05	9 < 5	15	5.2	
NW3 125S	568347.2	5475144				52 0.1		15.8 238 2.22		1 20.4	7.4	6 0.1					1.8 0.39			0.009 0.0		0.05	1.6	0.1 < .05	7 < 5	7.5	20.4	
NW3 150S		5475130					12.2			0.6 6.1		5 0.1		0.4	10 33 0.04		0.7 0.19		1 2.8	0.011 0.0		0.04	1.6 1.6	0.1 <.05	9<.5 5<.5	15 15	8.1 10.8	
NW3 175S		5475115		10.8		50 0.1		8.3 219 2.01		0.6 10.8	4.8	5 0.1		0.4	12 27 0.04		9.7 0.23			0.009 0.		0.05	1.5	0.1 < 05	8 < 5	15	11.3	
NW3 200S		5475093	0.9	13		74 0.2		9.7 488 2.28		0.7 11.3	5.5	5 0.2		0.4	15 28 0.04		2.1 0.29 9.1 0.17		1 2.20	0.009 0.0		0.04	1.4	0.1 < 05	10 < 5	15	31.3	
NW3 225S		5475074	1.2			56 0.3		7.4 230 1.97 8 8 382 2.17		0.6 31.3 0.8 13.2	3.3 5.6	11 0.2		0.3	13 25 0.07		9.3 0.22		1 2 87	0.012 0.		0.04	17	0.1 < 05	8 <.5	15	13.2	
NW3 250S		5475053				49 D.1 87 D.2		8.0 382 2.17 12.5 193 2.71		0.9 23.2	5.5	7 0.1		0.5	16 30 0.06		2.1 0.28		1 2.57	0.009 0.		0.06	1.7	0.1 < 05	9 <.5	7.5	23.2	
NW3 275S NW3 300S	588452.5 588473.1	5475036				69 0.2		10.9 164 2.34		0.6 7.8	5	8 0.1		0.4	19 25 0.1		0.3 0.28		1 1.8	0.01 0.		0.03	1.3	0.1 < 05	8 <.5	15	7.6	
NW3 325S		5475010	0.9			73 0.1		10 659 1.95		0.6 8.9	4.8	5 0.1		0.4	18 21 0.03		0.4 0.25		1 1.71	0.006 0.	05 0.1	0.03	1.2	0.1 <.05	6 <.5	15	8.9	
NW3 3505		5474998	0.8	9.3		29 < 1		6.5 105 1.82		0.7 12.5	6.2	3 < 1			24 14 0.02		8.2 0.29		1 0.85	0.002 0.0	032 0.1	0.01	0.8 <	1 <.05	3 <.5	15	11.5	
NW3 375S		5474983				55 0.1		9.7 148 2.21		0.7 10.8	5.6	7 0.1	0.2	0.3	16 26 0.07	7 0.06 1	2.2 0.31	96 0.066	1 2.47	0.008 0.0		0.04	1.7	0.1 <.05	7 <.5	15	10.8	
NW3 400S		5474970	1.2	8.9	12.8	51 0.1	12.9	8.4 305 2.06	3	0.5 1.2	4.9	7 <.1		0.4	13 26 0.07		11 0.21		1 2.43	0.000 0.		0.04	1.4	0.1 <.05	5 <.5	7.5	1.2	
RE NW3 400S	568556.7	5474970	1.1	0.2		56 0.1		5.6 326 2.15		0.5 3.1	4.5	7 0.1		0.4	13 27 0.07		2.2 0.22		1 2.34	0.01 0.		0.04	1.5	0.1 <.05	8<.5 9<5	7.5	3.1 6 1	
NW3 425S		5474958				48 0.1		7.3 179 1.99		0.6 6.1	4.2	B 0.1			11 29 0.05 13 28 0.07		9.9 0.19	• • • • • • • • • • • • • • • • • • • •	1 2.23	0.011 0.0		0.04	1.4	0.1 < .05	\$<.5	15	11.9	
NW3 450S		5474944	0.6	0.9		63 0.1		6.4 272 1.99		0.4 11.9	3.6 5.3	8 0.1 7 0.1	0.2	0.4	13 20 0.07 15 27 0.07		2.6 0.24		1 2.21	0.009 0.		0.04	1.8	0.1 < 05	7 < 5	15	8	
NW3 475S		5474928				76 0.2		11.7 254 2.3		0.6 9	5.3 6.4	5 0.1	0.2	0.3			1.4 0.28		1 2.45	0.008 0.		0.04	1.9	0.1 < 05	7 < 5	15	9	
NW3 500S NW3 525S		5474918 5474901				66 0.1 68 0.2		8.5 119 2.54		0.6 2.4	4.2	6 0.2		0.4	9 36 0.11		0.7 0.17		1 3.27	0.015 0	08 0.2	0.06	1.7	0.1 <.05	12 0.5	15	2.4	
NW3 550S	568676	5474687		16.3		73 < 1	14.7	13.5 402 2.37		1.2 15.8	8.4	5 0.1	0.2	0.5	19 26 0.05		2.2 0.27		1 1.4	0.004 0.0	05 0.1	0.02	1.4	0.1 <.05	6 <.5	15	15.6	
NW3 575S	588697.1	5474872				84 0.1				1 18.1	7.1	5 0.2	0.3	0.5	16 31 0.04	0.05 1	2.4 0.31	87 0.083	1 2.74	0.007 0.	07 0.1	0.05	1.8	0.1 <.05	8 <.5	15	18.1	
NW3 BOOS		5474858	1.6	17.3	40.1	125 0.2		16.5 3129 2.46	3.6	0.9 40	3.2	12 0.3	0.3	0.5	13 35 0.14		2.8 0.25		2 2.44		.1 0.2	0.05	1.6	0.2 <.05	9 0.5	15	40	
NW4 400N	588021.1	5475058	0.6	7.7	20.3	39 D.1		13.9 579 1.59		0.6 <.5	2.2	10 0.1	0.1	0.3	23 14 0.05		7.4 0.25		ct 1.13	0.006 0.		0.02	0.0	0.1 < 05	6 <.5	7.5	<.5	
NW4 375N		5475050	8.0		21.9	37 0.1				1,4 0.8	6.3	7 0.1	0.1	0.5	19 20 0.08		0.8 0.28		1 2.2	0.007 0		0.03	1.5 1.4	0.1 <-05	7 <.5 6 <.5	15 15	0.8	
NW4 350N		5475043	0.5		14.6	49 0.1		6.6 D5 1.87		0.9 1.4	3.6	8 0.1	0.1	0.3	18 17 0.07 17 23 0.05		9.2 0.28	95 0.031 79 0.018	1 2.29	0.008 0.0		0.05	1.4	0.1 < 05	7 < 5	15	<.5	
NW4 325N		5475034	0.5			33 0.1		3.5 118 1.78		0.4 < 5	4.2	5 0.1 4 < 1	0.1	0.3 0.2	21 18 0.04		8.8 0.23	68 0.018	1 1.21	0.006 0.		0.04	1.5	0.1 < 05	5 < 5	15	11	
NW4 300N		5475020 5475008	0.4 1.4	9		27 0.1		3.9 108 1.39		0.4 1.1 2.6 1.3	7.5	13 0.1	0.1	85	8 38 0.15		0.0 0.24		1 3.88	0.018 0.		0.06	2.2	0.1 < 05	13 <.5	15	1.3	
NW4 275N NW4 250N		5474995				55 0.2				1.2 1.7	3.6	8 0.2	0.2	0.3		D.18	9 0.15		1 3,99	0.015 0.	04 0.2	0.07	2.6 <	.1 <.05	12 <.5	15	1.7	
NW4 225N		5474983				23 0.2		6.1 61 2.01		0.6 2	2.5	6 0.1	0.1	0.3	6 35 0.05	5 0.14	8.4 0.08	77 0.107	1 3.04	0.014 0.4	03 0.1	0.07	1.9	0.1 <.05	11 < 5	15	2	
NW4 200N		5474967	0.7				13.7			0.6 8.5	4.9	7 0.1	0.3	0.4	15 48 0.09	9 0.09 1	4.8 0.55	91 0.07	1 2.05	0.011 0.	07 0.2	0.03	2.1	0.1 <.05	9 <.5	15	8.5	
NW4 175N		5474947	0.9	22.5	10.7	49 0.3		17.5 171 2.9		1 24.9	5.7	5 0.2	0.2	0.4	12 43 0.05	5 0.11 1	6.1 0.53	95 0.087	1 3.79	0.011 0.		0.08	3.5	0.1 <.05	9 <.5	15	24.9	
NW4 150N		5474929			12.2	40 0.1	18.4	8.8 301 2.02	43	2.9 9.1	5.2	9 0.1	0.1	0.3			1.5 0.46		1 1.52	0.005 0.4		0.02	1.9	0.1 < 05	5 <.5	15	9.1	
NW4 125N		5474911	1.2	22.7	11.7	55 0.2	2 12.4			0.6 14.1	- 4	6 0.2	0.1	0.3	13 48 0.11		2.4 0.35		1 2.3	0.011 0.4		0.03	2.4	0.1 <.05	9 <.5	15	14.1 9.1	
NW4 100N		5474890		19.9		44 0.1		8.8 510 2.09		0.4 9.1	2.7	4 0.1	0.2	0.3	40 0.06 0.11		9.4 0.25		1 2.21	0.012 0.		0 03	1.8	0.1 0.09	8 <.5 12 <.5	15 15	9.1	
NVV4 075N		5474872				36 0.3		8.9 132 2.81		0.8 2.2	4.1	5 0.1	0.3	0.3	43 0.06 0.155		1.1 0.17		2 4.4	0.011 0.		0.06	1.8 < 1.9	0.1 <.05	12 <.5	15	17.4	
NW4 050N		5474853	1.3			40 0.2		9.1 135 2.72		0.5 17.4	4	9 0.1 7 0.1	0.2	0.3 0.3	43 0.15 0.037		13,1 0.43 10.6 0.24		1 2.2	0.011 0.		0.03	1.7	0.1 < 05	9<5	15	3.3	
NW4 025N		5474836	0.0			45 0.2		9.4 186 2.66		0.5 3.3 3.5 1.6	3 8.7	7 0.1	0.2	0.7	48 0.11 0.055		17.1 0.39		1 5.06	0.009 0.		0.04	3	0.1 < 05	12 0.6	7.5	16	
NW4 000N		5474820	1.9 2			58 0.4		18.7 567 3.83		3.5 1.6	5.1	34 U.2 13 D.3	0.3	0.8	37 0.11 0.208		5.9 0.18		1 3.38		0.1 0.1	0.05	2.1	0.2 < 05	12 <.5	15	2.3	
L14 700W		5471384				149 0.4 115 0.3	24.7 3 13.6	12.9 1091 2.53		0.6 <.5	2.6	17 0.4	0.2	0.3	33 0.18 0.126		9.2 0.13		2 3.02	0.014 0.		0.06	1.3	0.1 0.11	11 <.5	15	<.5	
L14 675W		5471384 5471384			-	115 0.3		7.9 2131 1.95		0.7 < 5	2.9	10 0.4	0.2	0.3	34 0.11 0.37		9.0 0.1		1 4.3	0.016 0.		0.07	1.7	0.1 <.05	10 <.5	15	<.5	
L14 625W		5471384				165 0.2				0.7 1.5	3.5	12 0.5		0.4	33 0.05 0.347				2 3.32	0.014 D.	05 0.2	0.04	1.6	0.1 < 05	12 <.5	15	1.5	
L14 600W	568115.3							8.5 235 2.11		1 1	3.8	11 0.3			29 0.12 0.242			92 0.154	1 4.1	0.018 0	06 0.2	0.05	2.3	0.1 <.05	10 0.5	15	1	
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L14 575W L14 550W	568140.3 5 568185.4 5		0.7 13.6 0.6 13.3		92 0.2 1 76 0.2 1	7.8 10.8 426 4.8 8.1 342			4.2	8 0.3 17 0.3	0.3 0.3 0.4		0.07 0.224 0.14 0.129	8 10.9 0.14 5 9.2 0.11	108 0.139 1 3.5 109 0.17 1 3.5				0.1 < 05	10 <.5	15	0.9
L14 550W			0.0 13.3			1.5 10.4 302			¶.∠ 6.7	11 0.3	0.2 0.4		0.1 0.156		131 0.13 1 3.1				0.1 < 05 0.2 < 05	11 0 <u>5</u> 9<.5	15 15	0.7 1.5
L14 500W			1.1 18.6			9.7 11.4 1067			5.2	5 0.1	0.4 0.5		0.04 0.11	9 11.8 0.2	95 0.113 1 3.0				0.2 <.05	10 <.5	15	1.7
L14 475W			0,7 10		101 0.2 1		1.78 4.4		2.8	8 0.3	0.3 0.3		0.07 0.081		126 0.106 2 2.3			3 1.4	0.2 < .05	9 <.5	15	0.5
L14 450W		471384	1 17.6				2.41 28		4	5 0.1	0.2 0.4		0.05 0.073		118 0.123 1 3.3				0.2 < 05	9 <.5	15	1.3
L14 425W RE L14 425W			0.8 11.4 0.8 12.4		79 0.2 84 0.1 1		2.28		3.4 3.4	6 0.2 6 0,1	0.2 0.3		0.06 0.069	9 10.4 0.15 8 12.4 0.14	80 0.102 2 3 77 0.099 2 3				0.2 < 05	10 <.5 9 < 5	7.5 7.5	0.9 1.1
L14 400W			1.5 27.4		••••••		2.88 4.8		6.6	7 0.3	0.5 0.7		0.05 0.115		107 0.105 1 1				0.2 < 05	9 < 5	15	0.5
L14 375W			0.8 19.2	32.4 1		4.7 18.8 863	3.6 5.4	1.2 0.5	9.9	5 0.2	0.5 0.7	34	0.04 0.148	28 15.1 0.27	82 0.115 1 2.2			4 1.9	0.3 <.05	10 <.5	15	0.5
L14 350W			0.8 17.1			6.4 11.1 201			3.8	5 0.2	0.2 0.3		0.05 0.074	8 12.2 0.18	80 0.129 1 3.4				0.2 < 05	10 <.5	15	0.6
L14 325W L14 300W			07 204			9.8 11.8 587 6.3 12 658	2.12 3.6		4	7 0.2	0.2 0.2		0.08 0.066		108 0.093 1 2		••••		0.2 < 05	7<.5 7<5	15 15	8.4
L14 300W			0.1 20.7		79 0.1 2		2.11 3.0		5.8	5 01	0.1 0.2		0.07 0.083		111 0.08 2 2.1			-	0.2 < 05	/ ≤.5 8 <.5	15	1.8
L14 250W		5471384	1 17.5	15.8 1			2.28 8	0.7 4	4.8	7 0.1	0.3 0.3	31	0.06 0.047		110 0.102 1 2				0.2 < 05	7 <.5	15	4
L14 225W			0.4 26.1				2.09 6.2		5.1	5 0.1	0.2 0.2		0.07 0.015	13 20.8 0.38	87 0.069 <1 1.5				0.2 <.05	4 <.5	15	3.1
L14 200W			0.6 30.6			2.5 21.5 1206			3.5	7 0.2	0.2 0.3		0.09 0.068		118 0.099 <1 2				0.2 < 05	8 <.5	15	1.5
L14 175W L14 150W			0.7 16.5 0.6 20.2			8.2 11.1 1190 3.5 8.8 820			3.4 3.9	8 0.2 11 0.2	0.1 0.2		0.09 0.083		115 0.112 <1 2.4 119 0.139 1 3.7			-	0.2 < 05	8 < 5 9 < 5	15 15	1.3 3.1
L14 125W			0.7 21.4			0.4 11.4 541			4.1	7 0.2	0.2 0.2		0.09 0.042		117 0.107 1 2.0				0.2 < 05	8<.5	15	1.2
L14 100W			0.8 19.7			7.3 12.2 667			3.6	11 0.1	0.2 0.2		0,16 0.063		103 0.107 1 2.6				0.2 <.05	8 <.5	15	1.2
L14 075W			0.6 18.4			1.3 11.6 1008			2.8	8 0.1	0.1 0.2		0.08 0.122		100 0.123 1				0.1 <.05	10 <.5	15	0.9
L14 050W			1.1 50				3.69 5.9		10.9 6	11 0.1	0.3 0.7		0.08 0.048		183 0.132 <1 4.0 93 0.091 <1 2.0				0.3 0.06	13 0.6	15	2.8
L14 025W L14 000W			0.4 29.7 0.5 25.4				2.48 4		5	8<1	0.2 0.3		0.1 0.025 0.1 0.039	19 24.7 0.41 15 24.4 0.31	93 0.091 <1 2.0				0.3 0.07 0.2 <.05	6<.5 9<.5	15 15	1.8
L15 000E			.4 18.8				2.17 2.7		5.3	5 0.1	0.2 0.3		0.07 0.043	17 19.8 0.37	92 0.079 1 1.8				0.3 <.05	8 <.5	15	2.8
L15 025E	568018.5 5		0.6 19.8			•	1.83 2.6		4.2	5 0.1	0.2 0.2		0.05 0.095	9 12.7 0.28	87 0.116 2 3.1				0.2 <.05	8 0.5	15	2
L15 050E			0.4 20.4			6.6 8.5 288 9.8 7.4 1828		••••	6 3.3	5 0 <u>1</u> 6 0.3	0.2 0.3		0.08 0.033	19 23.8 0.42 5 7.3 0.09	69 0.082 <1 1.7 84 0.126 1 3.6				0.3 < 05	8≺.5 9<5	15 15	24
L15 100E	568069.7 5)7 12.1 15 15.8			9.0 7.4 1820 5.6 7.6 1427			3.3	11 0.2	0.3 0.4		0.08 0.287		139 0.126 1 2.3				0.1 < 05	9 <.5 10 <.5	15	2.2
L15 125E	568114 5		0.4 18		81 0.1 1				5.7	8 <.I	0.2 0.4		0.07 0.033	23 22.3 0.4	93 0.109 <1 1.6				0.3 < 05	8 <.5	15	1.1
L15 150E			5 24.9		131 0.1 2		2.58 4.5		6.1	12 0.3	0.2 0.3		0.17 0.15		159 0.13 <1 3.2				0.2 < 05	9 <.5	15	4
L15 175E	588164.6 5		0.4 18.3		96 0.2 2				8.1	9 0.2	0.2 0.4		0.1 0.091		138 0.108 1 2.3				0.5 < 0.5	8 <.5	15	0.8
L15 200E L15 225E	568189.7 5 568214.7 5),4 11.6),5 12.8		62 0.1 1 73 0.2 2		1.99 2.7		5, 8 5,1	5<.l 50.1	0.2 0.3		0.05 0.028		111 0.08 1 132 0.075 <1 2.0				03<05 03<05	6<.5 6<.5	15 15	0.9 0.7
L15 250E	568239.8 5		3.6 28.2		49 0.5 1				4.9	14 0.3	0.6 0.8		0.08 0.119		143 0.108 2 2.0				0.4 < 05	10 0.5	7.5	2.7
L15 275E	568264.8 5		2.1 80.5		54 0.3 3				8.1	13 0.2	0.4 0.5	35	0.06 0.19		125 0.13 2 3				0.4 < 05	11 0.8	7.5	2.1
L15 300E	568289.8 5		.5 23.7		82 D.1 1				7	7 0.1	0.3 0.2		0.05 0.096		94 0.137 1 3.3				0.5 <.05	10 0.5	15	1.2
L15 325E L15 350E	568314.7 5 568339.4 5		1 29.1		98 0.1 2 15 0.1 2				6.5 7.6	11 0.1 12 0.1	0.4 0.3		0.13 0.092		80 0.134 1 3.8 115 0.151 1 2.7				0.3 <.05	10 0.5 12 0.5	15 15	1.5
L15 375E	568364.6 5		1 29.1 0.8 20.5			23 16.6 130			6.4	9 01	0.2 0.3		0.1 0.1 27		76 0.137 1 4.5				0.2 < 05	11 0.5	10 13	3
L15 400E			0.7 17.8			4.8 13.2 223			6.2	7 0.2	0.7 0.3	30	0.07 0.09		107 0.069 1 1.8			2 1.8	0.2 < 05	8 <.5	5	3.7
L15 425E			0.6 25.5			8.8 10.2 631			5.6	6 0.3	0.2 0.3		0.08 0.073		83 0.112 1 2.4				0.3 <.05	8 <.5	15	1.9
L15 450E RE L15 450E		1471518 1471516 1	1 28.3			21 12.7 430 1.4 12.4 419			5.7 5.5	7 0.4	0.4 0.5		0.05 0.053		131 0.118 1 2. 125 0.111 1 2.5			• ••	0.5 < 05	9<5 805	15 15	1.4 t
L15 475E		471514	1 25.6			1.7 11.8 709			5.1	8 0.8	0.2 0.4		0,08 0.098		114 0.121 1 3		••••		0.3 < 05	8<5	15	2.4
L15 500E	568489.6 5	471515 1	1.1 17.2		95 0.1	15 13.8 1154		0.5 2.1	3.4	7 0.3	0.2 0.3		0.08 0.037	12 16 0.2	123 0.08 1 1.8	0.009 0.1;			0.2 < 05	8 < 5	15	2.1
L15 525E			0.7 26.4			7.7 \$1.3 309			6.2	5 0.1	0.2 0.3		0.06 0.062	18 17.5 0.3	86 0.098 1 2.7				0.3 < 05	7 0.6	15	2.1
L15 550E L15 575E			0.8 25.8 18 18.6			8.3 10.6 284 3.6 15.5 1462			6.6 3.7	6 0.1 7 0.2	0.2 0.3		0.05 0.053		135 0.095 1 2.9 135 0.116 1 2.8				0.3 < 05	8 0.5 10 < 5	15 15	3.2 1.8
L15 600E			6 16.3			9.8 10.7 1193			2.4	8 0.2	0.2 0.2		0.09 0.093		146 0.094 1 2.3				01<05	9 <.5	15	1.1
L16 400W			5 17.3			2.7 7.9 348	1.9 3.1		3.8	6 0.1	0.2 0.2		0.06 0.186	7 13.4 0.22	84 0.138 1 3.8				0.1 < 05	10 <.5	15	1.7
L16 375W			.6 16.8		52 0.1		2.06 4	0.9 1.5	3.8	7 0.2	0.2 0.2 0.3		9.08 0.141		77 0.158 1 4.9				0.1 < 05 0.1 < 05	11 <.5 11 <.5	7.5 15	1.5 1.9
L16 350W L16 325W			0.8 17.7 0.3 51.3				2.24 3.2 2.51 2.8		3.6 4.7	7 0.1	0.2 0.3		0.12 0.038	5 11.6 0.11 10 28.3 0.58	8/ 0.12 1 2.0 114 0.108 <1 2.1				0.1 < 05	7 <.5	15	1.8
L18 300W	568198.9 5		.4 15.8			0.3 8 1295			3.4	19 0.4	0.1 0.3		0.27 0.08		185 0.08 2 1.4				0.2 <.05	9 < 5	15	2.8
L18 275W	568224.5 5	471594 0	0.2 12.2				2.54 1.7		8.4	8 0.1	0.1 0.1		0.08 0.038		140 0.148 1 2.3				0.3 < 05	9 < 5	15	0.7
L18 250W			0.2 27.5 13 42			28 15.1 189 8 3 11.8 288	2.49 2		2 3.4	7<1 80.1	0.1 0.1 0.1 0.2 0.1		0.29 0.021	5 47.1 0.7 6 38.7 0.5	83 0.112 1 2.3 76 0.075 <1 1.8				0.1 <.05 0.1 <.05	6<.5 5<.5	15 · 15	<.5 15
L16 225W			0.3 42 05 25 6		37 0.1 2	6.3 11.5 288 16 10.7 319		UA 15	3.4	8 U.1 7 D.1	0.2 0.1	32	0.1 0.023	15 21.1 0.34	70 0.104 <1 2.4				0.1 <.05	5 < 5 7 < 5	15	3.8
L16 175W			0.6 13.9				2.04 3.7	0.7 2.4	3.5	8 0.2	0.2 0.4		0.09 0.087		75 0.098 2 2.2				0.2 < 05	9 < 5	15	2.4
L16 150W			5 17.1			1.2 8.7 2191			2.9	6 0.2	0.2 9.2		0.07 0.143	• • • • • • • • • •	109 0.093 1 2.9				0.2 <.05	7 < 5	15	1.8
L16 125W			1.9 26 19 14				2.22 3		4.9 2.8	8 0.2 7 0.1	0.2 0.4	34 33	0.1 0.061		115 0.109 <1 2.4 79 0.122 <1 3.				0.3 <.05	7 < 5 8 < 5	15 15	2.8
L18 100W			1.9 14 1.8 17.4		63 0.1	9.3 8.3 357 14 8.7 839			2.8 8.7	7 0.1 8 0.2	0.3 0.3		0.07 0.119		79 0.122 <1 3. 106 0.116 1 2.2				0.1 < 05	8<5 7<5	15	3.4 2.1
L16 050W).5 13.5			4.5 8.5 587	2.2 2.9		5.1	7 0.1	0.2 0.4		0.08 0.069		104 0.106 1 2.2				0.3 <.05	7 < 5	15	1
L16 025W	568474 5		7 27.4		74 0.1 1	8.9 9.3 354	2.25 4.4		6.2	7 0.1	0.3 0.3	32	0.07 0.082	18 19.1 0.33	86 0.099 <1 3.2	0.008 0.18	0.2 0.0	3 2.8	0.2 < 05	7 <.5	7.5	3.1
RE L16 025W			9 26.8				2.49 4.5		8.3	6 0.1	0.2 0.3		0.07 0.082	17 21.4 0.33	86 0.1 <1 2.9				0.2 <.05	7 < 5	7.5	0.9
L16 000W) 5 20 1 22		58 0.1 1 143 0.4		2.23 3.8 2.53 8	0.7 1.8 <8 <2	6 7	8 Q.1 8<5 -	0.2 0.3 <3 <3		0.05 0.037	21 18.6 0.38 16 13 0.32	97 0.066 <1 1.8			2 1.9	0.3 <.05	6 < 5	15 1.5	1.8 1.5
1700 1200W		470080	1 22 2 32		22 0.4			<8 <2 <8 <2	9		⊂s <s <š <š</s 		0.03 0.041	23 13 0.34	92 0.05 <3 2.0						1.3	2.2
1700 1150W		470044	2 44		85 < 3			<8 <2	7		⊲ ⊲	27	0.1 0.032		128 0.04 <3 3.0						17.3	17.3
1700 1125W	583004.6 5		2 24	33 2	63 <.3	24 12 125	2.9 11	<8 <2	8	5 < 5	⊲ ⊲	18	0.04 0.035	27 14 0.28	83 0.03 3 2.1	0.01 0.05	<2				2.2	2.2
1700 1100W	563025.8 5	470009	1 18	23 2	215 <.3	21 11 139	2.51 5	<8 <2	7	5 <.5	<3 <3	20	0.03 0.035	21 11 0.27	76 0.06 <3 2.4	0.01 0.06	3				1.5	1.6

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1700 1075W	563048.3	5469997 1	18	12 67 <.3	13	8 145 2.1	6 <8	<2	9	2 < 5 <3	<3	10 0.01 0.022	35	10 0.33	61 0.02 <3	1.22 <.01	ŧ.	0.04 <2	
1700 1050W	563073.7	5489984 2	16	25 209 <.3	17	13 448 2.48	9 < 8	<2	7	5 < 5 < 3	<3	19 0.04 0.028	21	11 0.25	81 0.05 <3	2.01	0.01	0.05 2	2
1700 1025W	563094.6	5469974 1	21	19 191 0.5	15	11 249 2.38	8 <8	<2	5	6<.5<3	<3	24 0.05 0.034	22	11 0.21	133 0.08 <3	2.12	0.01	0.05 2	2
1700 1000W	563120	5469966 1	26	32 222 0.3	26	21 871 2.4	6 <8	<2	ŝ	13 < 5 <3	<3	23 0.07 0.04	20		155 0.05 <3	2.74	0.01	0.07 <2	-
1700 975W	563146.9	5469959 1	14	20 144 0.3	17	11 363 2.41	8 <8	<2	5	4 < 5 <3	<3	21 0.02 0.027	24		106 0.03 <3	2.12	0.01	0.06 <2	
																			-
1700 950W	583174.8	5489958 1	17	23 127 <.3	17	12 582 2.29	6 <8	<2		4 <.5 <3	<3	15 0.03 0.023	30	9 0.27	98 0.02 <3	1.85	0.01	0.05 2	-
1700 925W	583198.7	5469957 1	28	32 174 0.3	34	21 326 2.9	8 <8	<2	9	9⊧<.5 <3	<3	23 0.06 0.048	18		142 0.04 <3	3.22	0.01		2
1700 900W	583222.1	5469956 1	- 14	45 178 <.3	21	12 171 2,19	4 <8	<2	8	6 <.5 <3	<3	16 0.06 0.037	22	10 0.31	99 0.04 <3	2.27	0.01	0.05 3	3
1700 875W	583249.2	5469953 1	13	61 199 0.4	13	10 352 2.3	7 <8	<2	5	5<.5<3	<3	23 0.04 0.032	20	13 0.25	108 0.05 <3	2.08	0.01	0.05	2
RE 1700 825W	563249.2	5469953 1	18	93 315 <.3	21	8 143 2.59	10 <8	<2	8	4 < 5 < 3	<3	19 0.02 0.047	24	15 0.4	84 0.04 <3	2.34	0.01	0.05 <2	
1700 850W	563279.9	5489960 2	9	38 399 0.5	19	12 704 2.33	4 <8	<2	- Ā	10 0.5 <3	<3	28 0.12 0.07	13		107 0.09 <3	2.9	0.01	0.08 <2	
1700 825W	583302.5	5469973 1	16	100 320 0.5	21	8 143 2.58	10 <8	<2	Å	4 < 5 < 3	3	19 0.03 0.046	23	12 0.41	82 0.04 <3	2.34	0.01	0.05 <2	
			22	77 341 <.3	31	12 374 2.98	13 <8	<2	a v	7 < 5 < 3	<3		28						
1700 800W	563318.3													15 0.41	••••••	2.03	0.01	0.07 <2	
1700 775W	563335 .5	5470009 1	24	57 224 <.3	19	12 283 2.82	11 <8	<2	8	5 <.5 <3	<3	18 0.03 0.038	29		74 0.04 <3	1.89	0.01	0.05 <2	
1700 750W	563351.7	5470026 2	15	62 326 <.3	21	14 743 2.72	10 <8	<2	7	8 < 5	3 < 3	20 0.06 0.031	30		139 0.04 <3	1.61	0.01	0.06 <2	
1700 725W	583371.8	5470044 2	23	85 264 0.5	22	36 1358 2.7	10 <8	<2	8	5 < 5 < 3	<3	19 0.04 0.033	30	13 0.33	112 0.03 <3	1.98	0.01	0.05 <2	
1700 700W	563382.8	5470080 2	15	47 491 0.8	22	15 1513 2.54	7 <8	<2	6	10 0.8 <3	<3	26 0.08 0.058	20	16 0.22	180 0.06 1	5 3.27	0.01	0.07 <2	
1700 675W	563394	5470078 2	12	57 338 0.6	21	15 1888 2.8	7 <8	<2	5	24 0.7 <3	<3	23 0.23 0.025	21	16 0.25	149 0.03 6	3 1.99	0.01	0.09 <2	
1700 650W	563406	5470097 2	15	41 272 0.6	18	14 313 2.67	7 <8	<2	6	8 < 5 < 3	<3	26 0.06 0.037	20		14 0.05 <3	2.16	0.01	0.06 <2	
1700 625W	563417.5	5470120 2	12	50 116 0.7	12	7 155 2.84	8 <8	<2	Ā	4 < 5 < 3	<3	25 0.03 0.028	25		61 0.04		0.01	0.04 <2	
1700 600W	563430.7		26	86 200 0.5	21	18 699 2.91	7 <8	<2	ž	8 < 5 < 3	- 3	23 0.05 0.038	21	14 0.2	75 0.03 <3	1.84	0.01		
																		0.08 <2	
1700 575W	563442.5	5470166 4	19	50 212 0.4	23	17 293 3.04	10 <8	<2	B	7 <.5 <3	<3	20 0.07 0.033	23	13 0.28	89 0.04 <3	2.37	0.01	0.07 <2	
1700 550W	563459.5	5470185 2	26	303 399 0.9	33	24 418 3.42	11 <8	<2	8	8<.5<3	6	23 0.05 0.043	26	18 0.33	87 0.05 <3	2.43	0.01	0.08 <2	
1700 525W	563475	5470203 1	22	77 266 0.8	28	14 328 2.85	8 <8	<2	9	10 0.5 <3	- 4	21 0.07 0.039	19	16 0.31	86 0.05 1	3 2.63	0.01	0.05 <2	
1700 500W	563489.8	5470220 2	22	44 210 0.8	22	18 322 3.01	11 <8	<2	8	4 <.5 <3	<3	22 0.03 0.035	23	16 0.31	91 0.04 <3	2.16	0.01	0.08 <2	
1700 475W	563503.6	5470238 2	23	56 179 0.3	19	17 1141 3.05	15 <8	<2	7	4 < 5 < 3	<3	21 0.02 0.045	23	12 0.32	90 0.04 <3	1,96	0.01	0.06 2	2
1700 450W	563519,2		22	83 204 0.7	19	13 438 3.48	13 <8	<2	a	5 < 5 < 3	<3	25 0.03 0.041	23		108 0.05 <3	2.27	0.01	0.05 3	-
1700 425W	563534.7	5470278 2	27	66 313 0.4	37	28 684 3.66	12 <8	<2	ň	20 < 5 <3	<3	22 0.18 0.037	25		100 0.03 <3	2.03	0.01		3
1700 400W	563553.3	5470296 2	29	55 217 0.9	22	12 189 2.78	9 <8	<2	7	9 0.5 <3	3	24 0.07 0.043	18	13 0.29	88 0.1 <3	3.37	0.01	0.05 <2	
1700 375W	563570.7	5470313 1	22	68 217 <.3	24	16 416 3.1	10 <8	<2	9	6 <.5 <3	<3	22 0.04 0.036	22	15 0.33	90 0.04 1	_	0.01	0.07 <2	
1700 350W	563586.4	5470325 2	15	41 169 0.3	16	15 264 2.92	8 <8	<2	7	8 < 5 < 3	<3	26 0.05 0.029	23	13 0.24	\$1 0.05 T	2.12	0.01	0.07 3	3
1700 325W	563603.2	5470342 1	11	32 140 < 3	12	11 492 2.77	9 <8	<2	8	5 <.5	3 < 3	26 0.04 0.027	27	13 0.24	97 0.02 8	5 1.8	0.01	0.05 2	2
1700 300W	563619.2		24	53 197 < 3	18	13 794 2.89	10 <8	<2	8	7 < 5 <3	<3	26 0.06 0.037	22	15 0.28	08 0.07 7	2.47	0.01	0.07 <2	-
1700 275W	563632.2		19	42 175 0.5	18	13 681 2.6	\$<8	<2	Ā	8 < 5 <3	<3	27 0.08 0.051	15			2.87	0.82	0.07 2	,
1700 250W	563643.8	5470409 <1	10	17 91 <.3	8	8 240 1.22	4 <8	<2	3	4 < 5 < 3	<3	13 0.03 0.03	10		53 0.05		0.01	0.03 <2	£.
									-										
1700 225W	563650.5	5470430 3	21	28 134 0.6	16	10 190 2.47	6 <8	<2	?		<3	23 0.06 0.046	14	12 0.21	97 0.09 7		0.02		_
1700 200W	563660.7	5470458 <1	23	39 182 0.5	18	12 381 2.28	4 <8	<2	\$	7 0.5 <3	<3	25 0.05 0.054	13	11 0.22	95 0.11 6		0.02	0.06 2	2
1700 175W	563671.2	5470478 2	17	29 144 <.3	19	10 201 2.29	3 <8	<2	5	7<.5<3	<3	24 0.06 0.07	10	9 0.17	96 0.11 5	i 3.9	0.02	0.04 <2	
1700 150W	563669.5	5470500 1	18	31 259 0.4	28	18 440 3.09	8 <8	<2	5	9 0.5 <3	<3	23 0.05 0.068	14	13 0.25	19 0.06 6	3.12	0,01	0.07 <2	
1700 125W	583705.5	5470517 2	18	42 105 <.3	16	10 392 3.35	12 <8	<2	7	8<.5<3	<3	29 0.04 0.035	24	17 0.24	03 0.04 8	1.97	0.01	0.07 <2	
1700 100W	563713.8	5470536 2	21	34 146 0.3	15	13 333 3,22	10 18	<2	7	4 < 5 <3	<3	25 0.02 0.033	23	13 0.24	74 0.03 8	1.82	0.61	0.08 2	2
1700 075W	563710.4	5470562 1	18	25 114 0.3	18	17 405 2.72	6 8	<2	6	5 < 5 < 3	<3	20 0.03 0.041	22		85 0.04 8		0.01	0.05 2	-
1700 050W	563725.0	5470585 1	14	17 85 <.3	18	12 461 2.39	7 <8	<2	ĕ	8 < 5 <3	<3	16 0.05 0.036	27			5 1.85	0.01	0.05 <2	L
1700 025W	563744.4	5470605 1	18	15 89 <.3	- 54	11 455 2.57	7 <8	<2	6	6 < 5 <3	<3	24 0.04 0.056	15			2.71	0.01	0.04 <2	
1700 000W	563761.3	5470622 1	10	17 57 <.3	11	5 159 2.46	7 <8	<2	4	8 < 5 <3	<3	21 0.04 0.027	26			1.15	0.01	0.05 <2	
1770 000E	563867.4	5471028 2	24	22 49 <.3	34	22 225 2.4	3 < 8	<2	8	15 <.5	3 < 3	18 0.14 0.027	34		88 0.12 €	5.32	0.02	0.04 <2	
1770 025E	583890.1	5471022 1	8	7 35 <.3	8	4 107 3.06	5 <8	<2	8	3 < 5 < 3	<3	21 0.01 0.024	34	15 0.28	45 0.02 4	i 1.21 <.01		0.05 <2	
RE 1770 125E	563954.6	5470942 1	8 <3	24 < 3	5	2 50 1.29	5 <5	<2	4	1<.5 <3	<3	7 0.01 0.014	21	3 0.17	20 0.01 3	0.68 <.01		0.02 <2	
1770 050E	563906.6	5471002 <1	15	15 58 < 3	14	7 121 2.85	\$<8	<2	8	3 < 5 < 3	<3	18 0.01 0.045	27	16 0.32	47 0.03 6	2.24	0.01	0.04 <2	
1770 075E	563921.7	5470982 <1	18	13 46 <.3	11	8 116 1.94	5 <8	<2	7	8 < 5 < 3	<3	21 0.08 0.077	17	12 0.17	54 0.07 5	3,18	0.01	0.04 <2	
1770 100E	563935.8	5470961 2	15	18 40 <.3	13	5 103 2 42	3 <8	<2	5	10 < 5 < 3	<3	22 0.09 0.059	18			3,35	0.01	0.05 <2	
1770 125E	563954.6	5470942 1	8	10 25 <,3	6	2 54 1.37	5 < 8	<2		2 < 5 < 3	<3	7 0.01 0.015	22		21 0.01 4		Q .Q1	0.03 <2	
									- 2										
1770 150E	563972.9	5470922 <1	10	15 48 <.3	10	6 118 2.36	6<8	<2	5	8 < 5 <3	<3	22 0.04 0.028	24			1.87	0.01	0.04 <2	
1770 175E	583990.5	5470904 <1	12	13 37 <.3	8	5 106 2.19	2 <8	<2	5	8 < 5 < 3	<3	19 0.05 0.033	23			1.63		0.09 <2	
1770 200E		5470885 <1	8	20 40 <.3	12	5 101 2.32	5 <8	<2	6	5<5<3	<3	18 0.03 0.028	25			1.7		0.04 <2	
1770 225E	564024	5470871 1	8	16 40 < 3	12	5 109 2,13	4 <8	<2	- 4	7<5<3	<3	19 0.05 0.021	28	†1 0.38	75 0.02 4	1.47	0.01	0.05 <2	
1770 250E	564038.3	5470854 1	5	10 22 <.3	8		2 <8	<2	8	4 < 5 <3	<3	20 0.02 0.019	30	9 0.28		1.01 <.01		0.03 <2	
1770 275E	564053.8	5470835 2	4	8 24 <.3	8	3 48 1.89	6 <8	<2	5	3 <.5 <3	<3	17 0.01 0.018	30			1.07		0.03 <2	
1770 300E	564064.6	5470818 1	¢.	13 34 < 3	10	6 87 2 64	5 <8	<2	5	5 < 5 < 3	3	22 0.04 0.026	26			1.23 <.01		0.04 <2	
1770 325E	564076.3	5470795 1	11	12 34 < 3	11		2 <8	<2	š	8 < 5 < 3	<3	24 0.04 0.059	, a		67 0.1 7			0.03 <2	
1770 350E		5470770 2	15	17 42 < 3	14	7 118 2.46	2 ~0 8<8	<2	7	2 < 5 < 3	<3	12 0.01 0.024	30		28 0.01 7			0.03 <2	
					• •				•										
1770 375E		5470745 1	13	12 41 <.3	- 14	8 79 2.19	3 < 8	<2	8	5 < 5 < 3	<3	21 0.02 0.025	21		73 0.04 4			0.04 <2	
1770 400E	564105.9	5470723 <1	12	12 34 <.3	10	7 163 2.33	2 <8	<2	5	5 <.5 <3	<3	32 0.03 0.033	14		03 0.09 5			0.04 <2	
1770 425E	554114.4	5470701 1	18	17 51 <.3	12	8 188 2.41	3 <8	<2	4	6 <-5 <3	<3	34 0.04 0.051	11		83 0.11 <3	3.13		0.05 3	
1770 450E	564120.9	5470677 1	13	16 54 < 3	17	12 230 2.22	2 <8	<2	6	9<.5<3	<3	27 0.06 0.041	17	11 0.3 1	16 0.06 3	2.52	0.01	0.06 2	2
1770 475E		5470647 <1	10	10 40 < 3	13	9 118 2.29	4 <8	<2	8	4 < 5 < 3	<3	21 0.02 0.034	27		67 0.04 <3	1.85		0.04 2	2
1770 500E	564133.7	5470816 <1	15	14 49 < 3	17	9 136 2.34	3 <8	<2	8	5 < 5 < 3	<3	28 0.03 0.027	28		79 0.03 <3	1.87		0.05 2	
1770 525E		5470591 <1	21	9 31 < 3	14	9 102 2.1	5 <8	<2	š	6<5<3	<3	29 0.04 0.055	15		79 0.14 <3	3.77		0.04 2	
								-	7		-								
1770 550E		5470568 <1	11	6 37 < 3	13		5 <8	<2			<3	20 0.02 0.038	28		58 0.04 <3	1.58	0.01		-
1770 575E	564151	5470539 <1	15	15 42 < 3	17	9 271 2.15	7 <8	<2	6	7 < 5 <3	<3	28 0.05 0.052	11		75 0.11 4		0.02		-
1770 600E	564156	5470510 1	17	11 45 0.3	18	10 505 2.21	4 <8	<2	5	8 < 5	3 < 3	31 0.05 0.05	10	11 0.18	79 0.18 <3	4.17	0.02		2
1770 625E		5470489 1	16	30 85 <.3	20	15 477 2.44	5 <8	<2	8	7<.5<3	<3	32 0.05 0.06	12	13 0.27 1	01 0.12 <3	3.04	0.02	0.05 2	2
1770 650E		5470463 1	11	12 86 0.6	11	10 332 2.47	6 <8	<2	4	8 < 5 < 3	<3	35 0.08 0.17	8	12 0.11	70 0.18 <3	3.92	0.02	0.04 4	1
1770 675E	564184.3		28	29 107 0.5	17	12 595 2.17	7 <8	<2	5	10 < 5 < 3	<3	31 0.07 0.099	18		32 0.16 <3	3.66	0.02		
									-										-

 $\begin{array}{c} 1.1\\ 1.29\\ 0.79\\ 3.18\\ 1.2\\ 2.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.24\\ 4.25\\ 3.26\\ 3.25\\ 3.26\\ 3.25\\ 3.26\\ 3$

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1770 700E	564192.6	5470419	1 13	5 23	99 <.3	14	15 799 2.31	7 <8	<2	5	9 < 5	<3	<3	31 0.08 0	14 10	12 0.12	99	0.16 <3	4.25	0.02 0.04	3				1,2	1.2	
1770 725E	564201.1	5470398	1 2	3 38	188 0.4	25	15 531 2.82		<2	7	11 <,5	<3	<3	31 0.09 0.0	79 20	15 0.38	100	0.09 <3	2.29	0.01 0.00	3 4				2.5	2.6	
1770 750E	564207.7	5470374	1 1			19	11 334 2.35		<2	5	9 <.5	<3	3	31 0.07 0.0				0.12 <3	3.04	0.02 0.05					2.3	2.3	
1770 775E	564219.7 564234.4	5470351			74 <.3 83 0.3	15	9 295 2.16		<2 <2	5 6	8<.5 5<5	<3 <3	<3	26 0.04 0.0				0.07 <3	2.19	0.01 0.04					4.7	4.7	
1770 800E 1770 825E	564254.8	5470330 5470315	1 1: c1 1:		83 0.3 85 <.3	20 19	12 513 2.24		<2	6	≏<.≎ 5<.5	<3	<3	26 0.04 0.0				0.07 <3	2.39 1.91	0.01 0.05					10.2 13.8	10.2 13.8	
1770 850E		5470304	1 t.		78 < 3	13	12 1027 2.20		<2	š	4<.5	<3	<3	25 0.04 0.0				0.04 <3	1.78 < 0		3 <2				33.2	33.2	
1770 875E		5470294			75 <.3	19	12 369 2.45		<2	7	4 < 5	<3	<3	22 0.03 0.4				0.04 <3	2.08 < 0						10.2	10.2	
1770 900E	564318.3	5470286	ct 13	8 18	69 <.3	20	15 426 2.31	7 <8	<2	7	5 <.5	<3	<3	26 0.03 0.4	31 21	12 0.3	100	0.09 <3	2.73	0.01 0.06	3 2				12.1	12.1	
1770 \$25E		5470279	12		74 0.3	19	15 390 2.52		<2	7	\$<.5	<3	3	29 0.04 0.0				0.07 <3	2.47	9.01 0.00					9.2	\$.2	
RE 1770 825E		5470315	្រា			20	12 299 2.31		<2 <2	6	5<.5 5<5	<3	<3	24 0.04 0.1				0.05 <3	2.01	0.01 0.00					20.2	20.2	
1770 950E 1770 975E	564367.5	5470272 · 5470260 ·			67 C.3 83 C.3	19	17 678 2.50		<2 <2		5<.5 5<.5	<3	<3 5	33 0.04 0.1					2.39	0.01 0.0					4.8	4.8	
1770 1000E		5470260				19	25 1144 2.84		~	5	8<.5	<3	4	47 0.1 0.0				0.08 <3	2.59	0.01 0.0					12.2	12.2	
1870 1000W		5471245				12	7 151 2.22		<2	5	4 < 5	<3	8	20 0.02 0.0				0.03 <3	1.47 < 0		5 < 2				11.2	11.2	
1870 975W	563904.2	5471240	c1 1	5 10	53 <.3	13	6 115 2.25	7 <8	<2	6	5 <.5	<3	<3	14 0.03 0.0	23 35	5 12 0.35	58	0.02 <3	1.27 <.0	1 0.04	2				13	13	
1870 950W		5471234	1		40 <.3	8	4 102 2.24		<2	5	3 < 5	<3	- 4	21 0.02 0.0				0.02 <3	1.55 <.0		i <2				21.1	21.1	
1870 925W	563950.6		1 1			12	6 121 2.06		<2	5	9 <.5	<3	3	14 0.06 0				0.02 <3	1.33 < 0		5 <2				2	2	
1870 900W	563972.7				52 < 3	11	5 123 2.44		<2	7	\$<.5 4<5	<3 <3	<3	16 0.03 0.0				0.01 <3	1.4 <.0		5 <2				3.7	3.7	
1870 875W 1870 850W		5471215 · 5471206 ·		, ,,	40 <.3 45 <.3	10 12	4 94 2.72 5 125 2.47		<2 <2	7	4 < 5	<3	3	23 0.02 0.0				0.05 <3 0.02 <3	2.67 1.37 <.0	0.01 0.04	s <2 s <2				25.7 1.5	25.7 1.5	
1870 825W	584045.7		2 1		57 <.3	15	9 176 2.77		<2	i.	8<5	<3	4	24 0.07 0.0				0.03 <3	1.87	0.01 0.03					8.8	8.8	
1870 800W	564065.4		1 1		47 < 3	14	7 100 2.44		<2	8	4 <.5	<3	<3	14 0.02 0				0.02 <3	1.48 <.0						28.5	26.5	
1870 775W		5471160	4		6! <.3	13	7 103 2.43	5 <8	<2	6	5 <.5	<3	<3	22 0.03 0.0				0.05 <3	2.58	0.01 0.05					9.4	9.4	
1670 750W		5471145			50 <.3	10	6 86 2.33		<2	8	4 <.5	<3	<3	19 0.02 0.6					2.35	0.01 0.05					4.6	4.8	
1870 725W		5471129			52 < 3	16	19 773 2.38		<2	2	19 <.5	<3	3	20 0.16 0.0				0.02 <3	1.95	0.01 0.06					6.5	6.5	
1870 700W		5471111			73 <.3	19	10 241 2.77		<2	3	€<.5	<3	<3	25 0.07 0.0				0.03 <3	2.15	0.01 0.07					4.4	4.4	
1870 675W 1870 650W		5471092 · 5471070 ·			65 0.3 48 0.3	15 12	7 146 2.33		<2 <2	÷	6<.5 4<.5	<3 <3	<3 <3	19 0.03 0.0				0.02 3	1.67	0.01 0.06	<2				12.7	12.7	
1870 625W		5471048			53 < 3	14	7 97 2.46		<2	2	3<.5	<3	٠ <i>،</i>	21 0.02 0.0					2.95	0.01 0.04	_				30.3	30.3	
1870 600W				B 11	45 < 3	13	8 92 2.01		<2	6	4 < 5	<3	<3	18 0.02 0.0					1,16	0.01 0.04					22.2	22.2	
1870 575W	564215.3			8 12	43 <.3	8	5 74 2.17	7 <8	<2	5	4 <.5	<3	3	21 0.03 0.0	42 22	8 0.24	53	0.03 <3	1.96	0.01 0.04	<2				8.4	8.4	
1870 550W		5470987		4 15	34 <.3	11	8 72 1.48		<2	- 4	6 < 5	<3	<3	13 0.04 0.0					0.19	0.01 0.04					35.9	35.9	
1870 525W	564243				39 <.3	14	11 224 1.89		<2	5	4 <.5	<3	<3	15 0.02 0.0				0.02 <3		0.01 0.05					6.7	8.7	
1870 500W	584257				31 <.3	13	7 76 2.22		<2	6 6	3 <.5	<3 <3	<3	11 0.02 0.0				0.01 <3	0.08 <.0		<2				35.6	35.6	
1870 475W 1870 450W		5470916 5470891 ·	1	3 14 6 14	48 0.6 32 0.3	9 8	5 113 3.86 4 59 2.37		<2 <2	Č Č	4 <,5 3 <,5	<3 <3	<3 5	32 0.03 0.0				0.04 3 0.03 <3	0.54	0.01 0.05					13.5 8.5	13.5 8.5	
1870 425W		5470866			39 < 3	13	7 99 3.04		<2	6	5<.5	<3	<1	24 0.03 0.0					1.84	0.01 0.05					8.7	8.7	
1870 400W		5470842			40 < 3	12	8 111 2.23		<2	5	4 <.5	<3	3	23 0.02 0.0					3.13	0.01 0.04					39.6	39.6	
RE 1870 300W		5470742		3 15	52 0.3	12	7 112 2.36	5 <8	<2	7	3 <.5	<3	<3	20 0.01 0.0	28 24	13 0.34	59	0.03 <3	1.88	0.01 0.04	<2				4.7	4.7	
1870 375W		5470821 (57 <.3	11	8 116 2.91		<2	8	3 <.5	<3	<3	24 1 02 0.0				0.03 <3	2.89	0.01 0.05				L	6.8	6.8	
1870 350W		5470794			51 <.3	11	6 98 2.26		<2	8	6 <.5	<3	<3	25 0.04 0.0				0.08 <3	2.84	0.01 0.05					24.1	24.1	
1870 325W 1870 300W	564319.7 564330.9	5470770 · 5470742 ·			59 0.6 51 <.3	9 13	5 268 2.81		<2 0 <2	8	4 <.5 3 < 5	<3 <3	<3 <3	28 0.04 0.0 0.19 0.01 0.0				0.02 <3 0.03 <3	1.84 1.88	0.01 0.05					12.3 8.1	12.3 8.1	
1870 275W	564340 1	5470722			54 0.3	15	11 202 2.13		<2	6	8<.5	<3	<3	21 0.05 0.0					1.37	0.01 0.05					22.2	22.2	
1870 250W	564349.1	5470698			59 0.4	10	8 94 1.94		<2	5	8 < 5	<3	<3	27 0.04 0.1				0.11 <3	3.58	0.02 0.04					7.5	7.5	
1870 225W	564380	5470675	:1 1:	3 11	74 0.3	12	7 169 2.21		<2	5	7 <.5	<3	<3	26 0.05 0.0	37 12			6.09 <3	3.28	0.02 0.04	<2				2.9	2.9	
1870 200W	564371.3	5470651	1 10		95 0.4	12	7 295 2.30		<2	6	5 <.5	<3	3	23 0.04 0				0.05 <3	2.24	0.01 0.05	-				10	10	
1870 175U 1870 150W	584377.9 564388	5470629 · 5470603			123 1 106 0.3	11 14	8 257 2.48		<2 <2	8 7	5<.5 5<.5	<3 <3	<3	31 0.04 0.0				0.13 4 0.07 <3	4.19	0.02 0.04	-				3.1 2.5	3.1	
1870 150W	564396.2		1 1		91 0.6	14	10 405 3.08		<2	' ź	১<.১ 8<5	<3	<3	30 0.04 0.0				0.07 <3	∠.¥ 3.18	0.01 0.04					2.3	2.5 2.2	
1870 125W	564409.6	5470559 -			70 0.3	14	11 254 2.68		<2	ż	4 < 5	<3	<3	28 0.03 0.0				0.07 <3	2.31	0.01 0.05					2.8	2.8	
1870 075W	584427.8	5470541			99 0.3	15	20 809 2.84	6 <8	<2	7	5 < 5	<3	<3	33 0.05 0.1		13 0.16	84	0.13 <3	4.65	0.01 0.05	<2				2	2	
1870 050W	584447.5	5470527 -		3 26	120 <.3	12	8 582 2.55		<2	3	7 <.5	<3	<3	37 0.07 0		• • • • •		0.13 <3	2.89	0.02 0.05					3.2	3.2	
1870 025W	564465.2	5470513 <			104 <.3	20	13 254 2.16		<2	5	5 < 5	<3	<3	26 0.03 0.0				0.08 <3	3.26	0.01 0.05					1.9	5.9	
1870 000W	564480.9	5470494 <		3 27	70 <.3 79 04	9	8 527 2.28		<2 5 4 9	47	4 <.5	<3 ເ ດາ	<3 0.5	32 0.02 0.0				0.04 <3	1.93 3.38	0.01 0.05	_	0.07	8 01<0	10 0.8	7.5	11,1 4.9	
2750N 425E 2750N 450E	567451.7		0.9 55.0		79 0.4 38 0.1		11.5 347 3.71 3.9 102 1.94			29	8 01	• • •	0.0	86 0.17 0.0 37 0.06 0.0		24.7 0.48		0.095 2	J.JØ 15	0.009 0.08			8 0.1<.05 3.4<.1 <.05		15	4.9	
2750N 475E	567476.9		0.5 21.		51 0.2	12.5	6.1 142 2.62			2.4	7 0,1			58 0,1 0.0		14.9 0.44			1.48	0.005 0.04			2.5 0.1 <.0		7.5	17.2	
2750N 500E	567501.8	5472753	0.6 39.1	24.9		15.1	7.4 160 2.75		1 2.8	2.5	9 0.4	0.2		61 0.11 0.		18.7 0.47		0.066 1	2.39	0.009 0.05			4.9 0.1 <.05		7.5	2.8	
2750N 525E			0.4 29.		36 0.2	6.8	2.9 138 1.25			1.1	11 0.3		0.4	34 0.14 0.0					1.13	0.007 0.04			2.6 0.1 <.05		15	7.8	
2750N 550E	587551.7	5472753	0.9 41.				18.4 1644 3.17			1.2	19 0.5			72 0.25 0.0		19.2 0.52		0.056 <1	2.52	0.01 0.08			4.3 0.1 <.05		15	10.9	
2750N 575E	567576.9 567801.6		0.5 3				14.1 773 2.48 8.3 593 2.52			1.9 1.3	19 0.7			55 0.26 0.0		21.9 0.65		••••	1.79	0.007 0.07		+	3.6 0.1<.05 2.5 0.1<05		15	6.4	
2750N 600E 2750N 625E		5472753 5472752	0.6 24.0		79 0.3 63 0.2	15.5 10.9	8.3 593 2.52 5.8 170 3.5			1.3	25 0.9			51 0.29 0.0 54 0.16 0.0		21.4 0.5 15.4 0.31			1.92	0.007 0.06			2.5 0.1<0		7.5 7.5	4.1 3.5	
2750N 650E			0.8 28.1				15.2 599 3.31			2.3	17 0.2			71 0.18 0.		28.2 0.54				0.009 0.08			3,5 0,1 <.05		7.5	4.5	
2650N 425E	587649.4		0.6 32				19.2 1374 2.6				21 0.7			53 0.29 0.0		22.1 0.53			1.62	0.008 0.08			3.4 0.1 <.05		7.5	8.9	
2650N 450E			0.9 35.5	5 42.3	133 0.3	24.3	25.2 598 2.28	5.2 2.1	1 38.8	1.2	14 0.8			73 0.15 0.0	9 40	21.4 0.45	109	0.051 1	2.09	0.009 0.07	0.1	0.05	3.2 0.2 <.05	\$ 0.6	15	38.6	
2650N 475E		5472655	0.6 21				8.4 293 2.28			2.8	6 0.3			53 0.07 0.0	23 14	14 0.44	47	0.062 <1		0.007 0.05			2.2 0.1 <.05		7.5	14	
RE 2650 475E			0.7 22.6		73 0.2		8.5 296 2.39			2.8	7 0.3			56 0.08 0.0		15.3 0.48			1.34	0.007 0.05			2.2 0.1 <.05		7.5	24.9	
2650N 500E			0.8 32				29.9 1591 2.88 5.7 153 2.12			2.5 2.4	9 0.5 7 0.3			55 0.06 0.0 42 0.05 0.0		18.5 0.46			1.78	0.008 0.08			2.5 0.1<.05 1.6<.1 <.05		15 15	35.2 5.5	
2650N 525E 2650N 550E	587549.7 587523.9		0.7 22.4		40 0.3 51 0.2		5.7 153 2.12 6.7 378 1.64		5 5.5 7 14,9		11 0.1			42 0.05 0.0		11.2 0.28		0.13 1		0.014 0.04 0.05			1.6<1 <.03 1.6 0.1<03		15	5.5 14.9	
2650N 575E			0.9 21.5				6 162 1.8				13 0.2			48 0.11 0.0		13.7 0.28		0.095 <1	1.37	0.012 0.05			16 01<0		15	2	
				-																							

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2650N 600E	587473 0	5472653	0.6 12.2	12 A	56 0.3	A2 4	164 2.85	43	0.7 1.5	3	10 0.2	02 03	10	0.14 0.248	9 11.2 0.21	59 0 103 1	1.94	0.009 0.03 0.	f 0.08	1.7 < 1 <.05	13 0.5	15	1.5
2650N 825E	567449.3		0.4 51	11.6			312 2.72	7.7	0.8 1.6		12 0.2	0.2 0.2		0.21 0.029	10 28.6 0.5		1.77	0.012 0.04 0.		4.9 0.1 < 05	7 < 5	15	1.6
2650N 650E		5472852	1.1 109.1	28			1729 3.71		2.6 18.3		20 0.4	0.3 0.3			30 50.1 0.52		2.79	0.01 0.07 0		11.9 0.1 < 05	10 0.9	7.5	18.3
50N DE	569997	5474999	0.8 16.2				282 2.03	3.9	0.6 2.1	3.7	8 0.3	0.2 0.3	28	0.09 0.073	11 18 2 0.44		2.03	0.009 0.08 0.	5 0.03	1.8 0.1 <.05	8 < 5	15	2.1
50N 25E	570020.8	5474999	0.9 8	12.2	78 O.1	14.8 9.1	198 2.06	3.6	0.5 <.5	3	8 0.2	0.1 0.3	32	0.09 0,131	8 13.9 0.28	67 0.085 1	2.27	0.012 0.06 0.	1 0.05	1.8 0.1 <.05	8 < 5	15	<.5
50N 50E	570046	5474999	0.7 15.2	14	59 0.1	22 12.1	187 2	4.7	0.6 1.5	4.5	7 0.1	0.2 0.2	31	0.1 0.135	7 17 0.38	63 0.084 1	2.4	0.01 0.06 0.	1 0.04	2 0.1 < 05	6 < 5	15	1.8
50N 75E	570071.6	5475000	0.6 11.9	10.8	87 < 1	17 10.8		3.3	0.4 0.6	3.3	8 0.t	0.2 0.2	28	0.07 0.08	8 13.6 0.32	68 0.075 1	1.98	0.01 0.05 0.	t 0.05	1.8 0.1 <.05	8 <.5	15	0.8
50N 100E	570097.3	5475000	0.7 17.2	12.9		21.2 11.7		3.8	0.8 1	- 4	7 0.1	0.2 0.2			8 17.2 0.37	67 0.091 <1	2.38	0.011 0.06 0,		2.3 0.1 < 05	7 < 5	15	1
50N 125E	570122.4	5475000	0.8 14.4	13.5		19.5 10		3.4	0.9 1.4	4.5	7 0.1	0.2 0.2		0.07 0.077	8 13.8 0.27	83 0.109 1	2.8	0.011 0.07 0.		2.4 0.1 < 05	8 < 5	15	1.4
50N 150E	570148.2	5475000	0.5 15	14.8		17.3 9.8		4.1	0.4 4.1	3.9	5 <.1	0.2 0.2		0.09 0.033	9 18.7 0.4		1.58	0.007 0.06 0.		2 0.1 <.05	6 <.5	15	4.1
50N 175E 50N 200E	570173.9 570199	5475000 5475000	0.4 15.8	19.4 22.3		12.3 6.5 22.7 11.7		3.9	0.4 18.3	4.3 3.5	4 0.1 8 0.3	0.2 0.2			11 18.8 0.42 9 22.2 0.58		1.19 1.07	0.008 0.06 0.		1.8 0.1 < 05	5<.5 6<5	15 15	18.3
50N 225E	570224.4	5475000	0.5 25.6	15.7		23.2 11.3		3.5	0.6 1.8	3.5	8 0.2	0.1 0.2		0.11 0.052	7 20.6 0.37	90 0.09 <1	2.02	0.013 0.08 0.		2.5 0.1 < .05	0 < 3 7 < 5	15	15.2 1.8
50N 250E	570250.3	5475000	0.5 19.3	18.8		18.5 8.8	285 2.3	4.3	0.8 < 5		12 0.2	0.4 0.3	36	0.21 0.031	27 29.2 1.37	43 0.087 <1	2.32	0.005 0.1 0		2.5 0.1 < 0.5	8<.5	15	<.5
50N 275E	570275.8	5475000	0.3 21.8	15.4		21.4 8.6	145 2.17	4.5	0.8 3.8	43	7 0.1	0.2 0.2		0.11 0.022	11 33.4 0.73		1 47	0.005 0.08 < 1	0.02	2.5 0.1 < 05	5<5	15	38
50N 300E	570301	5475000	0.5 22.2	20		27.2 13.1		5.5	1.2 3.6	8.3	15 0.3	0.2 0.3	30	0.14 0.08	32 18.5 0.6		3.01	0.014 0.13 0.		2.5 0.1 < 05	9 < 5	15	3.6
50N 325E		5475001	1.5 25.2	54.3		29.4 10.9		5.8	0.9 3.3		11 0.4	0.3 0.3	45	0.1 0.048	14 31.2 1.21	94 0.171 1	2.92	0.01 0.22 0	3 0.04	4 0.3 <.05	12 < 5	15	3.3
50N 350E	570352.2	5475001	1.3 13.1	30.3	177 0.1	28.7 10.8	495 2.27	3.7	0.7 1.3	4.2	16 0.8	0.2 0.3	37	0.2 0.082	11 17.9 0.51	69 0.151 2	2.71	0.016 0.09 0.	2 0.06	2.7 0.1 < 05	10 <.5	15	1.3
50N 375E	570377.3	5475001	0.5 143.7			25.9 22.9		4.8	0.6 1.2		12 0.3	0.2 0.2		0.15 0.047	10 19.8 1		2.57	0.011 0.11 <0.1	0.03	6.5 0.1 < 05	9 0.5	15	1.2
50N 400E	570402.9	5475001	0.8 176.2			18.3 15.1		5.8	0.4 2.2	2.7	9 0.5	0.3 0.2		0.18 0.059	6 14,5 0.38		2.23	0.016 0.07 0.		2.9 0.1 <.05	10 < 5	15	2.2
50N 425E	570427.8	5475001	0.8 44.8	11.5		14.9 12.8		7	0.6 <.5	3	7 0.4	0.2 0.2		0.1 0.11	4 12.4 0.2		3.72	0.018 0.05 0.		2.8 0.1 < 05	9 <.5	15	<.5
50N 450E	570453.9	5475001	0.5 76.6	17.6		19.9 20.8		8.9	0.3 0.8	2.3	8 0.3	0.2 0.2	77	0.19 0.063	5 12.4 0.37	63 D.115 1	2.5	0.016 0.08 0.		3.2 0.1 <.05	9 <.5	15	0.8
50N 475E	570479.5	5475001	0.6 28.6	21.9		20.5 17.4		10.7	0.3 3	2.4	7 0.3	0.3 0.2	75	0.14 0.069	5 14.8 0.38	52 0.135 <1	2.74	0.016 0.06 0.		3.2 0.1 <.05	10 <.5	15	3
50N 500E	570504.4	5475001	0.5 23.2	18.4		12.1 11.5		4	0.4 2.5	2.8	5 0.3	0.2 0.2	- 54	0.11 0.072	7 21.2 0.35		2.02	0.012 0.05 0.		2.4 0.1 < 05	9<.5	15	2.5
300E 3000N 300E 2975N	567298.5 567298.5		0.4 10.4	8.3 14.1	21 0.1 32 0.1	4.2 2.5 5.4 3.3	89 1.47 126 1.82	1.6 2.7	0.3 13.1	2.4 2.7	4 0.1 6 0.1	0.2 0.2		0.04 0.023	14 6.7 0.14 13 9.5 0.2	59 0.06 1 64 0.057 <1	0.82	0.008 0.02 <0.1		1.1 0.1 <.05 1.4 0.1 <.05	7<.5 8<5	15 15	13.1 12.5
300E 2950N	567298.5		0.7 20.2	18.9	52 0.1 61 0.1	9.4 7.3		3.4	0.4 12.5	3.9	8 0.2	0.1 0.3	45	0.06 0.027	13 12.1 0.25		1.3	0.008 0.03 0.		2.5 0.1 < 05	10 0.5	15	32.5
300E 2925N		5472926	0.5 42.2	12.4		21.8 12		4.9	0.8 13.2	5.3	3 0.1	0.2 0.2	70	0.05 0.039	15 28.4 0.73		2.32	0.003 0.04 <0.1	0.03	4.2 01<.05	6 < 5	15	13.2
300E 2900N	567298.5		0.4 14.8				2326 1.91	3	0.3 3.2		10 0.2	0.3 0.3	52	0.12 0.039	12 12 0.16		1 07	0.009 0.05 0.		1.6 0.1 <.05	8 < 5	15	3.2
300E 2875N	567298.5		0.6 30	13.3			207 2.73	3.3	0.8 22	3.1	5 0,1	02 02		0.06 0.029	15 17.7 0.54	53 0.095 <1	1.89	0.008 0.04 0		3.8 0.1 <.05	8<5	15	22
300E 2850N	567298.3		0.7 25.2	15		8.8 5.6		4.5	0.6 3.3	3.3	8 0.1	0.3 0.3		0.08 0.042	8 13.2 0.2	80 0.089 1	2.53	0.009 0.04 0.		2.3 0.1 < 0.5	10 0.5	15	3.3
300E 2825N	587298.5		0.4 61.4	13.8			201 4.08	4.7	0.7 17.3	5.7	8 0,1	0.3 0.2		0.1 0.037	14 23.4 0.86	66 0.08 <1	2.35	0.004 0.05 <0.1	0.03	5.7 0.1 <.05	7 < 5	7.5	17.3
RE 300E 2825N	567298.5	5472828	0.5 63.3	13.8			201 4.07	4.8	0.7 12.8	5.7	8 0.1	0.2 0.2	97	0.1 0.034	14 23.2 0.87	65 0.078 <1	2.51	0.004 0.04 <0.1	0.03	5.3 <0.1 <.05	7 < 5	7.5	12.8
300E 2800N	567298.5		0.5 30.2	18.2			488 3.24	3.3	0.6 4.1	4.5	7 0.1	0.2 0.3			16 21.1 0.58		2.28	0.008 0.05 0.		3.4 0.1 < 05	10 <.5	15	4.1
300E 2775N	567298.5		0.9 93.6	25.3			462 5.26	5.3	2.6 3.1		14 0.3	0.3 0.5			47 31.2 0.47		4.54	0.013 0.07 <0.1	0.07	15 0.1 <.05	16 0.7	15	3.1
300E 2750N	567298.3		1 65.8				306 5.05	5.1	1.1 3.1		13 0.3	0.3 0.6		0.14 0.037	20 28.1 0.42		3.73	0.015 0.07 0.		6.1 0.1 <.05	18 0.5	7.5	3.1
300E 2725N	567298.3		0.8 54.3	28.3	85 0.5		349 3.26	5.3	1.3 1.7		15 0.4	0.2 0.5	66	0.18 0.051	20 24.1 0.42		3.81	0.013 0.07 0.		5.1 0.1 < 05	12 0.5	7.5	1.7
300E 2700N	567298.3		0.5 61.7	38.2		21.2 9.9		3.2	1.8 10.9		14 0.4	0.2 0.5	56	0.16 0.054	39 23.7 0.49	126 0.082 1	3.6	0.011 0.05 0.		6.7 0.1 < .05	12 0.5	15	10.9
300E 2675N 300E 2650N	567298.3 567298.3		0.9 41.9 0.7 67.4	55.7 35			389 2.37 444 2.74	3.1 3.7	1.3 32.3 2 2.7		26 0.6 16 0.8	0.5 0.5 0.2 0.4		0.32 0.017 0.22 0.057	36 13.1 0.31 29 22 0.37		2.02 2.65	0.013 0.08 0.		4.7 0.1 <.05 3.4 0.1 <.05	11 0.5 10 < 5	15 75	32.3 2.7
300E 2625N	567298.3		0.6 23.3		67 0.2		275 2:14	4.6	1 4.1		14 0.3	0.3 0.4		0.17 0.033	12 29 0.49		2.05	0.007 0.05 0		3.2 0.1 < 0.5	7 0.8	7.5	4.1
300E 2600N	567298.3		0.5 12.2			7.7 5.1		2.3	0.4 10.1		11 <.i	0.1 0.4		0.18 0.015	14 12.5 0.28		1.15	0.008 0.04 0.		1.6 0.1 <.05	7<5	75	10.1
300E 2575N	567298.3		0.5 33.3	26			663 2.46	3.9	0.9 32.7		14 0.3	0.3 0.3		0.24 0.033	17 21.2 0.61		1.74	0.008 0.07 0		3.3 01<05	5 < 5	15	32.7
300E 2550N	567298.3		0.4 28.6				925 2.22	4	0.8 5.2		21 0.5	0.2 0.3		0.31 0.045	15 17.4 0.48	128 0.045 2	1.84	0.006 0.06 0.	0.08	2.4 0.1 < .05	6 0.6	1	5.2
300E 2525N	587298	5472528	0.3 87.3		58 0.4	14.1 2.7	33 D.57	1.8	2.8 4.1	0.2	16 1.2	0.3 0.3	13	0.1 0.059	81 16.4 0.09	92 0.042 1	1.84	0.011 0.04 <0.1	D.18	2.4 0.1 0.17	7 1.2	7.5	4.1
300E 2500N		5472501	0.5 22	18.5	52 0.3		319 2.55	5.4	0.6 22	4.1	6 0.3	0.3 0.3		0.09 0.029	17 14.7 0.4		1.08	0.005 0.05 0.		2.1 0.1 < 05	5 <.5	15	22
400E 3300N		5473300	0.9 27.5	21.8			1137 1.92	2.3	0.8 1.4		13 0.2	0.1 0.3	36	0.16 0.038	18 13.6 0.39		1.45	0.009 0.08 0.		2.1 0.1 < .05	7 <.5	\$	1.4
400E 3275N	567398.4	5473275	2.5 45.8	31.1	52 0.3		4891 4.82	6.6	1.6 3.9		20 0.5	0.1 0.5	76	0.28 0.052	32 18.5 0.37		2.18	0.011 0.07 0.		3.9 0.1 < .05	9 0.5	15	3.9
400E 3250N	567398.4	5473250	1 58	25.6	., .,	11.3 9.4		2.9	1.3 1.7	1.8	16 0.5	0.1 0.4	42	0.18 0.043	19 15.4 0.31		1.85	0.012 0.06 0.		3.1 0.1 0.08	10 < 5 9 < 5	76	1.7
400E 3225N 400E 3200N	567398.4 567398.7	5473225 5473200	0.8 15.1	20.8 31		4.3 2.2 7.1 6.2	70 1	1.5 1.9	0.4 0.6	0.7 1.3	8 0.3 12 0.3	0.1 0.4	28 30	0.06 0.02	13 9.5 0.17		1.21	0.022 0.03 0.		0.7 <0.1 <0.05	9 < 5 10 < 5	7.5 15	0.6 1.4
400E 3175N	567398.7	5473175	0.6 15.8	15.5		6.4 4.4	\$9 2.39	3.9	0.7 2.4	3.6	5 0.1	0.1 0.2	37	0.05 0.109	5 12.3 0.12		4.76	0.015 0.03 0.		2.4 <0.1 0.07	9<.5	15	2.4
400E 3150N	567395.7	5473150	0.7 26.2	23.1			171 2.81	4.8	0.6 21.3	4.7	7 0.1	0.1 0.4	50	0.09 0.04	15 15.8 0.53		1.99	0.01 0.05 D.		2.2 0.1 < 0.05	10 < 5	15	21.3
400E 3125N	567398.7	5473125	0.5 24.8	15.4	73 0.1		320 2.85	4.4	0.5 9.7	4.2	4 0.t	0.1 0.3	49	0.06 0.049	13 19.5 0.48	65 0.04 1	1.6	0.004 0.05 0.	0.02	2.1 0.1 <0.05	7 <.5	15	9.7
400E 3100N	567398.7	5473100	0.7 12.4	12.7	57 0.1	8.5 4.7	145 2.99	4.2	0.5 2.8	3.7	7 0.1	0.2 0.2	43	0.09 0.07	7 14.7 0.25		2.21	0.01 0.03 0.	2 0.06	2 <0.1 <0.05	10 <.5	15	2.8
400E 3075N	567398.7	5473075	0.6 22.3	17.4		3.1 8.2		4.1	0.5 13.8	5.9	3 0.1	0.1 0.3	55	0.05 0.064	11 20.5 0.48		2.22	0.005 0.04 0.		2.8 0.1 < 0.05	8 <.5	15	13.8
400E 3050N	567398.9	5473050	0.6 34	13.4		13.6 9.2	190 3.22	3.9	0.8 11	4.6	5 0.1	0.2 0.2		0.05 0.084	10 14.5 0.59	66 0.063 1	2.6	0.008 0.03 0.		3.8 0.1 <0.05	8 < 5	15	11
400E 3025N	567398.9	5473025	1 21.1	14.1		8.3 5.9	88 2.85	4.8	1 13.4	4.2	6 0.2	0.2 0.2		0.07 0.078	9 13 0.29		3,36	0.011 0.03 0.		3.5 0.1 <0.05	10 0.8	15	13.4
400E 3000N		5473000	81 8:0	21		8.5 4.8	104 3.28	3.2	0.6 2		11 0.2	0.2 0.4		0.12 0.038	10 10.3 0.16		1.35	0.023 0.03 0.		2.1 0.1 <0.05	16 < 5	7.5	2
400E 2975N	567398.9	5472975	0.4 16.6	17.4		6.9 3	96 1.65 148 3.25	2.2	0.4 <.5	1.6	14 0.2	0.2 0.3	35 53	0.13 0.025	9 9.3 0.16 7 18,7 0.33		1.04	0.015 0.04 0.		1.3 < 0.1 < 0.05	9<5 9<5	15 15	<.5 26.8
400E 2950N 400E 2925N	587398.9 567398.9	5472950 5472925	0.6 34.1	16,3 7,5		5.1 5	146 3.25	4.3 3.1	0.7 20.8	3.1	8 01	0.2 0.3	- 33 26	0.08 0.072	4 6.9 0.08		5.55	0.012 0.04 0.		2.8 < 0.1 < 0.05	9.05	15	25.5
400E 2920N	567399.1	5472900	0.7 15.7	12.2	46 0.3		348 28	3	08 12	3.5	5 01	0.1 0.2	39	0.04 0.081	4 12.3 0.1		5.18	0.02 0.02 0.		2.5 0.1 <0.05	12 <.5	15	1.2
400E 2875N	567399.1	5472875	0.5 25.9	23.3		0 0.0	173 2.61	22	0.5 1.5	3.5 79	8 0.1	0.1 0.2	52	0.08 0.022	9 12.8 0.23		1.94	0.016 0.05 0.		2.5 0.1 < 0.05	12 <.5	15	1.5
RE 400E 2850N		5472850	0.7 15.2	23.3		8,3 5,5		2.8	0.7 1.8	3.4	5 0.1	0.2 0.3	88	0.06 0.022	7 15.7 0.18		2.85	0.012 0.04 0.		2.9 0.1 < 0.05	13 < 5	15	1.8
400E 2850N	567399.1	5472850	0.9 15.3	14.3	50 0.2	7 5	128 3.72	2.8	0.6 2.7	3.3	5 0.1	0.2 0.3	64	0.06 0.035	7 15.1 0.18		2.50	0.013 0.04 0.	0.13	2.8 0.1 <0.05	13 < 5	15	2.7
400E 2825N	567399.1	5472825	0.8 32.7	17.4		0.1 3.9	94 2.57	2.8	1.1 2.5		10 0.3	0.1 0.3	39	0.09 0.03	25 11.5 0.15		2.03	0.02 0.03 0.		4.5 0.1 <0.05	13 < 5	7.5	2.5
400E 2800N	567399.1	5472800	0.5 48.4	17.6		4.3 7	138 1.85	1.8	2.2 4.8		11 0.2	0.1 0.2	48	0.12 0.063	31 19.2 0.45	58 0.032 <1	2.38	0.009 0.05 0.	0.11	4.9 0.1 <0.05	8 0.8	15	4.8
400E 2775N		5472775	0.6 22.7	23.4		9.7 6.6	169 2.26	1.6	0.6 1.6		11 0.2	0.1 0.3	50	0.1 0.019	12 14 0.28	90 0.114 <1	1.83	0.014 0.04 0.	0.05	3.1 0.1 <0.05	11 <.5	7.5	1.6
400E 2750N	567399.3	5472750	0.8 34.1	35.6	74 0.3 1	4.4 15,3	294 2.54	3.5	1.2 1.6	2	16 0.3	0.2 0.4	64	0.21 0.046	28 18.5 0.43	113 0.055 1	2.87	0.008 0.05 0.1	0.05	5 0.1 <0.05	10 0.5	7.5	1.6
400E 2725N		5472725	0.7 49.8	38.1	120 0.4 2	25.1 17.8	570 4.23	8	1.2 46.1	6,7	15 0.4	0.2 0.8	93	0.15 0.035	26 27 0.54		4.27	0.011 0.07 <.1	0.06	8.6 0.1 <0.05	13 <.5	15	48.1
400E 2700N		5472700	1.3 74.1	42.5		2.6 20	758 2.73	3.8	1.9 1.9		13 0.6	0.1 0.4	56	0.18 0.05	32 18.6 0.45		2.27	0.01 0.07 <.1	0.07	3.6 0.1 0.06	9 0.5	1	1.9
400E 2675N		5472675	0.6 28.1	30	55 0.2 1		718 2.11	3.1	0.9 1.8		18 0.4	0.2 0.4		0.25 0.044			2.06	0.009 0.05 <.1	0.06	2.9 0.1 <0.05	8 <.5	7.5	1.8
400E 2850N	567399.3	5472650	0.5 24.2	24.7	67 0.1 1	3.8 9.5	289 2.39	3.3	1 1.3	2.5	15 0.2	0.2 0.3	48	0.17 0.03	15 21.4 0.42	74 0.057 1	2	0.008 0.06 0.1	0.05	2.9 0.1 < 0.05	7 <.5	1	1.3

400E 2625N	567399.3		0.6 29.8				8.7 175 1.97		1.1 1.2		10 0.3				26 15.8 0.4		0.011 0			2.5 0.1 <0.0		15	1.2	
400E 2600N	567399.5		0.6 15				3.3 148 2.1		0.5 1.7		8 0.3	0.1 0.3			12 10.3 0.18		0.012 0	.03 0.1	0.03	1.5 0.1 <0.0	5 10 <.5	7.5	1.7	
400E 2575N	567399.5		0.5 31.1				0.2 313 2,53		0.7 3.1		7 0.2	0.2 0.2		0.12 0.029	18 16.4 0.66	44 0.05 <1 1.48	0.008 0		0.02	3.5 0.1 <0.0		15	3.1	
400E 2550N	567399.5		0.8 17.8		43 0.2		5 123 2.28		0.8 1.2		5 0.1	0.2 0.2			11 14.4 0.28			.04 0.1	0.07	3.1 0.1 <0.0		15	1.2	
400E 2525N	567399.5			14.2			1.6 214 2.64		0.7 17.5		3 0.1			0.06 0.028	19 15.8 0.63			.05 0.1	0.02	3.3 0.1 <0.0		15	17.5	
400E 2500N	587399.5		0.5 27.3				0.6 187 2.7		0.9 21.7		4 0.1	0.2 0.3				52 0.084 <1 1.62	0.003 0		0.02	3.3 0.1 < 0.0		15	21.7	
400E 2475N	567399.5		0.6 20.6				8.4 145 2.17		0.9 73.8	+	3 0.1			0.03 0.039	12 18.5 0.33			.08 0.1		2.8 0.1 <0.0		15	73.8	
400E 2450N			0.8 9.3				2.2 115 1.96		1 2.7		4 0.1				5 9.3 0.08			.02 0.2		2.8 <.! <.05		15	2.7	
400E 2425N							2.1 99 2.4		0.5 6.4		4 0.1					38 0.138 1 1.94		.03 0.1	0.05	1.4 0.1 <.05		15	8.4	
400E 2400N	567399.7		0.8 12.6				1.8 162 1.9		1 2.8		5 0.1				3 8.5 0.05			.02 0.2	0.1	2.2 < 1 < .05		15	2.8	
49 0E 49 25E	570018.5	5474895					9.7 168 2.12 9.6 411 1.88		0.5 2.6		8 0.1 8 0.1				10 17.7 0.54 8 15.2 0.39		0.011 0	.07 0.2	0.03	2.2 0.1 <.05		15 15	2.8	
49 50E	570016.5						1.1 201 1.9		0.4 1.9		6 0.1				10 17.1 0.32		0.009 0		0.04	1.7 0.1 < 05		15	1.1	
49 50E	570044.5						9.8 186 1.97				9 0,1				8 14.1 0.3			.07 0.1	0.03	1.9 0.1 <.05		15		
49 100E	570095.1						0.7 190 2.14		0.5 <.5		9 0.2				11 16 0.32			.09 0.1	0.03	1.7 0.1 <.05		7.5	1.5 <.5	
49 125E	570120.4						0.9 191 1.76		0.5 7.4		5 0.1				12 19.8 0.42		0.005 0			1.8 0.1 <.05		15	7.4	
49 150E		5474898					8.9 143 1.77		0.4 7.8		5 0.1				14 20 0.52		0.004 0			1.9 0.1 <.05		15	7.8	
49 175E	570171.8						3.5 289 1.99		0.5 3.5		8 0.1					66 0.083 <1 2.33	0.011 0			2.6 0.1 < 05		15	3.5	
49 200E		5474897					0.8 235 2.25		0.5 7.4		8 0.1				10 27.7 0.63			.07 0.1		2.8 0.1 < 05		15	7.4	
49 225E	570222.3						1.7 965 2.86		1.1 19.8		14 0.8				20 25.5 0.61		0.011 0			2.8 0.1 < 05		15	19.8	
49 250E	570248.6						3.3 312 2.7		1 1.5		13 0.5				20 24.1 0.71			09 02		3.1 0.1 <.05		15	15	
RE 49 175E	570171.8						4.2 299 2.05		0.6 3.3		8 0.1					70 0.089 2 2.45	0.011 0	.07 0.1		2.6 0.1 <.05	7 < 5	15	33	
49 275E	570273.5						0.8 2408 2.66				14 0.8			0.21 0.098	8 23 8 0.5		0.012			2.6 0.1 <.05	9<.5	7.5	2025.8	
49 300E	570298.6						9.1 380 3.43							0.17 0.045		79 0.116 1 2.41	0.01 0	07 D.1	0.03	4 0.1 <.05	10 <.5	15	3.3	
49 325E	570324.3						2.1 199 2.82				8 0.1			0.15 0.021	9 55.4 0.73	48 0.097 <1 1.91	0.009 0	05 0.1	0.02	4.7 0.1 <.05	6 <.5	15	2.1	
49 350E	570349.9						3.6 147 2.34		0.6 2.1		7 0.3			0.09 0.07	5 23.6 0.39	63 0.123 1 3.43	0.015 0	.06 D.1		3.2 0.1 <.05		15	2.1	
49 375E	570375.2	5474898	0.5 44.1	19.2	78 0.6	24.1 1	3.2 271 2.14	5.9	0.5 4.4	3.4	8 0.1			0.1 0.068	6 28.1 0.37	62 0.1 1 2.73	0.012 0	.06 0.1	0.04	3 0.1 <.05	8 <.5	15	4.4	
49 400E	570401.2	5474899	0.6 19.9	13.8	87 0.3	12.8 1/	0.2 598 2.12	3.5	0.4 4.5	1.9	6 0.2	0.2 0.2	54	0.1 0.121	-7 14.6 0.25	59 0.081 1 2.22	0.014 C	.05 0.1	0.03	2.3 0.1 <.05	8 <.5	15	4.5	
49 425E	570426.8						9.4 811 1.75		0.5 1.9		6 0.2			0.08 0.131	5 13 0.18	47 0.108 1 2.98	0.014 0			2.1 0.1 <.05	8 <.5	15	1.9	
49 450E	570451.5						9.5 207 2.01				6 0.1			0.11 0.091		51 0.073 1 1.88	0.011 0			2.1 0.1 <.05		15	4.3	
49 475E	570476.7						3.8 384 2.53									60 0.098 <1 2.82	0.013 0			3.4 0.1 <.05	• .•	15	152	
49 500E	570502.3		0.5 247.2				7.9 179 2.68		0.7 3.2		8 0.1				12 21.9 0.57		0.012 0			4.6 0.1 <.05		15	3.2	
1820 500W	564990.7		0.7 9.1				4.2 81 2.08		0.7 6.8		4 0.1				10 12.2 0.23		0.007 0		0.1	5.8 < 1 < 05		15	8.6	
1820 475W	564980.8						3.9 82 1.58		0.5 20.8		4 0.1					34 0.023 <1 1.08	0.005 0.			0.9 0.1 <.05		15	20.6	
1820 450W	564968.9		0.9 9.7				6 400 2.51		0.8 7.6		2 0.1				11 13.2 0.17		0.008 0			2.1 0.1 < 05		15	7.6	
1820 425W	564962.4						8.5 257 2.74 8.9 118 3.25				3 <.1				16 13.5 0.37 20 15.2 0.3		0,006 0.		+	1.7 0.1 <.05	7 <.5 8 <.5	15 15	8,4 44,2	
1820 400W 1820 375W	564954.3 564945.1						8.1 148 2.34		1.2 44.2		5 0.1 4 0.2					55 0.051 1 2.83	0.007 0.		0.04	1.7 0.1 <.05	8<.5 7<5	15	44.Z 14.6	
1820 350W	564937.5						5.4 109 2.08		0.7 43.3		3 0.1				16 8.4 0.2		0.008 0.		0.07	1.4 0.1 < 05	• •=	15	43.3	
1820 325W	564931.5		1.2 11.4				4.2 419 2.07		1.4 7,8		4 0.2				25 12.9 0.35	49 0.019 1 1.18	0.006 0.			1.2 < 1 < .05		1	7.8	
1820 300W	564925.7		1.6 14	17			9.8 205 4.1		1 17		8 0.2				23 18.7 0.47		0.005 0			1.3 0.1 0.		7.5	17	
1820 275W	584919.2		1.5 18				7 7 262 2.68		1.7 147		6 0.1	0.3 0.3			29 10.7 0.5	50 0.008 <1 1.17	0.003 0			1.2 <0.1 <0.0		15	147.2	
1820 250W			1.3 13.7				5.5 232 3.1		1.1 12.9	3.9	8 0.2	0.3 0.6			21 11.1 0.28	62 0.032 1 1.67	0.007 0	05 0.2	0.05	1.4 0.1 <0.0		7.5	12.9	
1820 225W	564910.2	5471291	1.4 10.5	19.5	56 0.2	11.6 F	6,1 147 3.35	5.4	0.9 16.9	6.1	5 0.1	03 0.5	33	0.05 0.094	17 14.9 0.25	69 0.049 <1 3.17	0.008 0.	05 0.2	0.07	1.9 0.1 <0.0	5 8 < 5	15	16.9	
1820 200W	564907.2	5471313	1.3 13.6	22.3			9.9 144 3.04		1.7 22.4		0 0.2	0.3 0.7			31 11,5 0.28	70 0.017 <1* 1.47	0.006 0.		0.02	1.5 0.1 <0.0		7.5	22.4	
1820 175W	584908.3		2.6 17.8				7.4 2478 2.88		1.6 15.4		2 0.4	0.2 0.8			26 11.7 0.33	91 0.022 1 1.55		06 0.t	0.04	1.6 0.1 <0.0		7.5	15,4	
1820 150W		5471384	1 14.8				9.9 284 2.78		0.7 23.1		9 0.2	0.3 0.6			22 11 0.27	88 0.023 <1 1.88	0.006 0.		0.02	1.0 0.1 <0.0		15	23.1	
1820 125W		5471385	1.2 10.4		42 0.2		4.7 167 3.58		0.8 5.4		4 0.1	0.2 0.4			8 13.8 0.11	44 0.085 1 4.51		03 0.2	0.12	1.8 0.1 <0.0		15	5.4	
1840 0S 1840 025S		5471504	1.3 9.3	15.9	48 0.1		5.4 99 3.03 5.4 99 2.72		0.7 26.9	*	4 0.1	0.2 0.5			16 11.1 0.25 28 9.3 0.22	92 0.043 <1 2.52 44 0.035 1 0.88	0.007 0.		0.06 0.02	1.5 0.1 <0.0		15 15	28.9 21.9	
1840 0505		5471482 5471456	1.3 8.3		39 <.1 48 0.1		5.4 99 2.72 6.6 140 3.42		0.4 21.9		4 0.1				18 12.6 0.23	43 0.041 1 2.12	0.005 0		0.02	14 01 <0.0		15	49.3	
1840 0755	564809.8	5471432	1.4 10.2		48 0.1		7.3 127 3.43		0.7 49.3		• 0.1 3 0.1	0.3 0.5			24 12.3 0.33	50 0.022 1 1.63	0.005 0.	•••	0.06	1.3 0.1 <0.0		15	46.6	
1840 100S		5471408	1.8 19.6				4.9 3359 3.52		t.7 17.6		5 0.3	0.2 0.8				133 0.021 1 1.8	0.007 0		0.01	1.7 0.1 <0.0		7.5	17.8	
1840 125S			1.5 22.7				9.3 711 3.75		1.7 7		0 0.2					181 0.04 1 2.88	0.007 0		0.04	2 0.1 <0.0	5 9 < 5	15	7	
1840 150S			2.1 28.5				8.5 239 4.3		1.4 13.9	6.8	5 0.2	0.3 0.5			11 16.2 0.23	70 0.093 1 3.18	0.009 0.	05 0.2	0.09	2.2 0.1 <0.0	5 11 <.5	15	13.9	
1840 175S			1.7 17.3		98 0.2		8.1 523 2.91		1.1 6.6		6 0.1	0.3 0.5			14 12.9 0.29	86 0.079 2 3.25		05 0.2	0.07	2.3 0.1 <0.0		15	8.8	
1840 200S			1.9 19.6				9.7 1663 3.53		2.4 388		6 Q.3	0.3 0.8				97 0.022 1 2.07		09 0.1	0.02	1.6 0.1 <0.0		7.5	367.7	
1840 2255			2.9 22.7				6.9 360 2.56		33 8		3 0.8	0.3 0.7			30 10.6 0.26	65 0.02 <1 1.34	0.005 0.		0.03	1.5 0.1 <0.0		15	8	
1840 2505			1.5 22.3				4.2 1238 2.97		1.8 26.7		1 0.4	0.2 0.8				97 0.025 <1 1.58	0.008 0.			1.4 0.1 <0.0		15	26.7	
1860 50N			0.9 11.5		63 0.1		4 217 2.18		0.5 1		4 0.1 5 0.1	0.3 0.4			14 10.9 0.18	53 0.045 2 1.57 60 0.041 1 1.74	0.009 0.		0.05	1.3 0.1 <0.0		7.5	1	
1860 25N RE 1860 25N			1.5 15.9	23.8 26	79 0.1		8 570 2.97 7,7 597 2.97		0.7 1.5		5 0.1 5 0.1	0.2 0.6			15 14.9 0.28 15 14.1 0.27	60 0.041 1 1.74 64 0.042 2 1.75	0.008 0.			1.5 0.1 < 0.0		3	1.5	
1860 05	584777.5 584775.1		1.5 18		73 0.1		7,7 597 2.97 8,4 199 3.54		0.7 10.2	***	3 0.1	0.2 0.6				53 0.041 2 1,9	0.008 0.			1.8 0.1 < 0.0		75	41	
1860 255			1.5 17				8.3 192 3.63		0.9 2.6		3 0,1	0.3 0.7			21 14.8 0.36	54 0.037 <1 2.03	0.006 0.			1.7 0.1 <0.0		7.5	2.6	
1880 505		5471749	1.4 26				1.4 428 3.35		1.2 3.2		3 0.1	0.3 0.6				47 0.035 1 2.38	0.005 0.		0.07	1.6 0.1 <0.0		7.5	3.2	
1860 755	584751.3		1.4 9		55 0.1		5 548 2.33		0.3 60		8 0.1	0.4 0.5				135 0.043 1 0.68	0.006 0.		0.01	1 0.1 <0.0	5 7 < 5	1	60	
1860 100\$			1.8 10		58 0.1		5 120 3.18		0.7 68.5		4 0.2	0.2 0.6			18 10.8 0.18	82 0.054 1 1.4	0.008 0.	05 D.1	0.02	1.3 0.1 <0.0	5 9 < 5	7.5	68.5	
1860 1255	564741,7	5471880	1.4 9.9	10.5	48 0.1		5.3 119 2.94		0.5 39.4	8.9	3 0.2	0.2 0.5	19 (0.01 0.022	27 10 0.23	49 0.014 1 0.92	0.003 0.	04 0.1	0.01	1.1 0.1 <0.0	5 5 < 5	7.5	39.4	
1560 150S	584739.1	5471853	1.2 13.3	27	94 0.1	18.5 1	1.8 318 3.38	6	0.9 15.3		2 0.1	0.2 0.6			25 11.9 0.39	95 0.026 1 1.26	0.008 0.		****	1.4 0.1 <0.0		7.5	15.3	
1860 1758	564738.9		1.3 10.2	24			8.7 351 2.82	6.2			4 0.1	02 0.7			27 10.9 0.35	60 0.015 <1 1.01	0.004 0.			1.3 <0.1 <0.0		1	48.8	
1860 200S			1.2 11.3				8.5 178 2.64		0.7 20.2		3 < 1					61 0.014 1 0.94	0,004 0.			1.2 0.1 <0.0		1	20.2	
1860 2255			1.2 8.6				8.3 154 2.82									80 0.019 <1 1.1	0.005 0.			1.1 <0.1 <0.0		1	13.7	
1660 250S							0.2 253 3									81 0.027 1 1.81	0.006 0.			1.4 0.1 <0.0		7.5	14.6	
1860 2755	584735	5471532	1.3 13.5	72	91 0.1	13.7 17	7.6 1405 1.87	3.5	0.6 9.6	4.1 1	2 0.6	0.1 0.5	15 (0.12 0.03/	J1 11.3 U.45	211 0.01 <1 1.43	0.006 0.	05 0.5	0.03	1.4 0.1 <.05	4 < 5	7.5	9.6	

1880 3005							3.3 0.9 28					25 8.8 0.33			1 0.02	0.6 <0.1 <.05	3<5	7.5	28.8	
1860 3255		171451 1.8 18								0.3 0.8			97 0.015 <1 1.07	0.005 0.05 0		0,7 0.1 <.05	4 <.5	1	9.2	
1860 350\$		71454 1.7 15								0.3 0.7			51 0.03 <1 1.08	0.004 0.05 0		1.1 <0.1 <.05	6 <.5	1	8.4	
1880 3755	564752.4 54					7 175 1.54					29 0.08 0.033	21 10.5 0.18		0.006 0.05 0		1.1 0.1 <.05	7 <.5	7.5	7.7	
1860 400S		171404 1.3 11									29 0.04 0.026		49 0.024 <1 1.21		2 0.03	1.1 0.1 <.05	7 < 5	15	5	
1860 4255		171380 1.9 22									28 0.17 0.051		182 0.017 <1 2.58	0.006 0.13 0		1.8 0.1 <.05	8 < 5	7.5	2.3	
1860 4505		171356 1.5 29									26 0.15 0.105		184 0.016 1 1.79		1 0.08	1.3 0.1 <.05	7 0.5	7.5	5.7	
1860 4755		71328 1.3 33									26 0.11 0.137	13 14.7 0.29		0.008 0.1 0		0,7 0.1 0.18	5 0.7	7.5	1.1	
1860 500S 1860 525S		171304 1.1 21 171280 2.3 18									15 0.45 0.083 27 0.16 0.038	13 7.9 0.45 24 14.1 0.45			1 0.08	0.6 < 0.1 0.12	3<5	1 75	0.5	
1860 5235		171259 2.8 10									28 0.04 0.027	20 11.4 0.31			1 0.02	1.0 0.1 <.05	/ <.5 R < 5	7.5	1.7 24.3	
RE 1860 600S		71206 1.2 13									28 0.04 0.095	20 13.4 0.29			2 0.07	1.6 0.1 <.05	8<5	7.5	7.4	
1860 5755		71229 1.3 10									30 0.11 0.043	20 13.3 0.44			1 0.03	1.4 0.1 <.05	8 < 5	7.5	84.5	
1860 8005		171206 1.2 13									28 0.04 0.091				2 0.06		8 < 5	7.5	4.4	
1860 6255		71180 1.3 14									34 0.03 0.064		78 0 102 2 3.78	0.013 0.05 0		2 0.1 <.05	10 0.5	15	14.1	
1860 6505	564805.9 54						3.7 0.8 9						36 0.043 2 1.12			1.1 0.1 <.05	8 < 5	15	9.8	
1860 6755	564603.8 54	71129 1 11	3 18.4	62 0.1	8.6 4	2 139 2.98	5.7 0.8 6.	2 5.3	6 0.3	0.2 0.5	31 0.05 0.074	23 11.7 0.28	70 0.04 1 1.15	0.007 0.05 D	2 0.03	1 0.1 <.05	8 <.5	15	8.2	
1860 7005	564808.2 54	71106 1 18	9 18,7	75 0.2	14.2 9	8 385 3.24	5.5 0.9 58.						58 0.035 2 1.58	0.005 0.05 0	1 0.05	1,3 0.1 <.05	7 < 5	15	56.9	
5800N 425E	570424.2 54	75806 <1 10	02 17	102 0.5	25 2	21 384 5.3	10 <8 <2				190 0.18 0.042		65 0 11 8 2 42	0.01 0.05 <2				5.1	5.1	
5800N 450E						18 298 4.35			22 < 5 < 3	5	140 0.28 0.026		97 0.1 10 2.52	0.01 0.06 <2				2.8	2.8	
5800N 475E	570472.4 54						4<8<2		17 <.5 <3		72 0.22 0.02		65 0.16 <3 2.17	0.03 0.04 <2				0.3	0.3	
5800N 500E				59 < 3			5<8<2		6 < 5 < 3		97 0.14 0.02	5 38 0.57		0.01 0.04 <2				1.4	1.4	
5800N 525E	570523.1 54					20 911 2.42			7 <.5 <3		63 0.19 0.015		49 0.06 <3 2.3	0.01 0.03 <2				0.3	0.3	
5800N 550E	570548,5 54					23 204 2.84			10 < 5 <3		62 0.21 0.017	3 70 0.65		0.01 0.03 <2				0.1	0.1	
5800N 575E	570574 54			38 0.3		11 143 2.91			13 <.5 <3			10 39 0.46		0.01 0.09 <2				0.1	0.1	
5800N 600E	570599.2 54			63 0.4		13 169 3.11 <			12 <.5 <3			29 27 0.31		0.01 0.08 <2				0.6	0.6	
5800N 625E	570524.6 54		9 9			7 117 2.17			5 < 5 < 3		50 0.07 0.019	8 7 0.28		0.01 0.06 <2				0.8 0.9	0.6	
5800N 650E 5800N 675E	570650.1 54			48 <.3 22 <.3		18 113 2.89 22 322 2.6 <	3<8<2		8 < 5 < 3		49 0.09 0.06 41 0.13 0.088		55 0.11 <3 4.28 127 0.14 <3 5.31	0.02 0.03 <2				0.9 2.6	0.9 2.6	
5800N 875E	570675.7 54		13 12 17 10			22 322 2.6 < 15 661 2.23			7 < 5 <3				75 0.04 <3 1.69	0.01 0.04 <2				<i>2.</i> 0 0.5	0.5	
5700N 200E	570698.7 54			4⊃ <,3 91 <,3			3 < 8 < 2		6 < 5 < 3			11 3 0.37		0.01 0.07 <2				0.5	0.3	
5700N 200E 5700N 225E	570224.8 54			91 <.3 69 <.3			2 <8 <2		5<-5<3		37 0.07 0.048		58 0.05 <3 1.83	0.01 0.07 <2				03	03	
5700N 223E			¥ 15 23 15			6 236 2.22 11 228 2.34	4 <8 <2		5<5<3		42 0.07 0.039	13 7 0.64		0.01 0.05 12	2			3	3	
5700N 230E	570250.2 54			58 < 3		10 153 2.95	2 <8 <2		4 < 5 < 3		58 0.05 0.038	11 3 0.53		0.01 0.05 <2	2			3.4	3.4	
5700N 275E	570300.9 54			65 <.3		15 169 3,1	3 < 8 < 2		6<.5<3		6P 0.09 0.051		58 0.06 <3 2.87	D.02 0.05 <2				22.2	22.2	
5700N 325E	570325.8 54			33 <.3		5 130 2.27	5<8<2		4 < 5 <3		75 0.09 0.03	9<1 0.28		0.01 0.04 <2				24	2.4	
5700N 350E	570352.4 54			74 0.3			7 <8 <2		6<5<3		115 0.14 0.073		46 0.08 <3 2.3	0.01 0.08 <2				41	41	
RE \$700N 350E	570352.4 54					5 402 3.68	8<8 <2		6<5<3		118 0.15 0.075	8 5 0.33		0.01 0.06 <2				1.6	1.8	
5700N 375E		75702 2 14					5 < 8 < 2		10 < 5 <3		122 0.22 0.057	8 7 0.35		0.02 0.1 <2				5	5	
5700N 400E	570403.1 54			66 < 3		3 244 3.94	8 < 8 < 2		12 <.5 <3		141 0.24 0.032	8 7 0.42	50 0.08 4 1.64	0.01 0.04 <2				1.4	1.4	
5700N 425E	570428.1 54		80 24	85 0,6	30 2	24 527 4.57	7 <8 <2	5	17 0.5 <3	<3	137 0.15 0.03	14 21 0.48	150 0.13 + 3 3.51	0.02 0.06 <2				7,3	7.3	4.
5700N 450E	570454.1 54	75702 1 4	17 15	83 <.3	18 1	lu 225 4.19	8<8<2	3	8 < 5 < 3	<3	128 0.19 0.034	11 21 0.66	60 0.08 3 1.89	0.01 0.08 <2				11.7	11.7	
5700N 475E	570479.8 54					10 173 2.89	4 < 8 < 2		10 <.5 <3		77 0.19 0.014	8 7 0.49		0.01 0.04 <2				0.3	0.3	
5700N 500E	570505 54					12 120 2.81	3<8<2	3	8 < 5 < 3			7 17 0.34	54 0.09 <3 2.22	0.02 0.04 <2				3.6	3.6	
5700N 525E	570529.9 54					21 417 3.57	6<8<2	<2	11 <.5 <3		94 0.27 0.019	5 114 0.82		0.01 0.04 <2				0.4	0.4	
\$700N 550E		75703 1		50 < 3		20 895 2.92	3 < 8 < 2	2	13 < 5 < 3		77 0.26 0.017	7 47 0.48 8 19 0.3		0.01 0.04 <2				0.4 1.3	0.4	
5700N 575E 5700N 800E	570580.9 54 570606.7 54	175703 1	15 11 12 19			0 305 2.37 6 99 1.95	4 <8 <2 3 <8 <2	<2 Z	7 <-5 <3		55 0.12 0.019 61 0.22 0.011	6 18 0.28		0.01 0.07 <2				2.7	1.3 2.7	
5700N 625E			14 20	48 < 3		8 172 2.02	3 < 8 < 2	-	5 <-5 <3	3		10 2 0.3		0.01 0.04 <2				52	5.2	
5700N 650E	570857.4 54		26 18			10 125 2.87	6 <8 <2		5 <-5 <3		54 0.09 0.043	11 10 0.48	48 0.05 <3 1.69	0.01 0.04 <2				7.1	7.1	
5700N 675E	570682.9 54		27 16			4 314 2.53	2 <8 <2		5 < 5 < 3		54 0.09 0.03	10 6 0.5	70 0.06 <3 1.7	0.01 0.06 <2				7.9	7.9	
5700N 700E	570709.1 54		17 29	19 0.7		4 89 0.79	3 11 <2		70 0.9 <3		27 1.33 0.049	55 34 0.32	78 0.03 <3 1.72	0.02 0.04 <2				2.8	2.8	
5800N 200E	570195.8 54		1 22	38 < 3	11	7 175 2.01	3 < 8 < 2		7 <.5 <3	<3	34 0,13 0.019	17 <1 0.5	53 0.04 3 1.35	0.01 0.04 <2				1.5	1.5	
5600N 225E	570219.3 54		20 19	48 < 3		10 154 2.79	4 <8 <2		6<.5<3	<3	46 0.09 0.036		62 0.06 <3 2.59	0.01 0.07 <2				14,4	14.4	
5600N 250E	570244.8 54			38 <.3		8 113 2.75	5 < 8 < 2		7 <.5 <3	<3	53 0.09 0.05	12 1 0.36		0.01 0.04 <2				29.3	29.3	
5600N 275E	570270 54			58 <.3		6 144 2,9	5<8<2		5 < 5 < 3	- 4		10 <1 0.34		0.01 0.05 <2				14.6	14.6	
5600N 300E	570295.3 54			109 0.4		5 162 3.06	2 <8 <2		12 0.8 <3	<3	54 0.14 0.109	9 3 0.34		0.02 0.06 <2	-			1.3	1.3	
5600N 325E	570320.9 54		70 31			2 334 3.31	4 <8 <2		9 < 5 <3	<3	97 0.15 0.025	11 7 0.55		0.01 0.05	2			1.2	1.2	
5600N 350E	570346.9 54			90 <.3 79 < 3		6 440 4.33	14 <8 <2 4 <8 <2		23 < 5 < 3	<3 <3	117 0.28 0.056 178 0.2 0.034	8 19 0.67 13 15 0.32		0.01 0.07 <2				5.6 3.3	5.5 3.3	
5600N 375E 5600N 400E	570372.2 54 570398 54		51 20 56 14	/⊌<.3 125 0.4		26 692 5.26 20 584 4.4	4 <8 <2 3 <8 <2		10 < .5 < 3	<3 <3	178 0.2 0.034	5 8 0.22		0.01 0.04 <2	2			3.3 <.5 <.		
5800N 400E	570423.8 54		27 11			8 387 3.05	8 < 8 < 2		8 05 <3	<3	87 0.12 0.034	10 9 0.31	69 0.07 <3 2.03	0.01 0.06 <2	4			2.8	2.8	
5600N 425E	570423.0 54			85 0.3		1 309 2.59	6 <8 <2		9<5<3	<3	67 0.17 0.025	8 17 0.32	85 0.08 <3 1.59	0.01 0.06 <2				1.8	1.8	
5600N 450E	570474.1 54			100 <.3		5 282 4.45	19 <8 <2	<2	14 < 5 < 3	<3	110 0.23 0.032	3 151 0.93		0.01 0.04 <2				1.3	1.3	
5000N 500E	570499.5 54			158 0.3		0 531 3.83	8<8 <2	<u></u> 2		<3	90 0.18 0.027	4 83 0.94	78 0.09 <3 2.69	0.01 0.06	2			<.5 <		
5600N 525E	570524.8 54			24 0.4		0 114 2.99	5<8<2	<2 -	19 < 5 <3	<3	64 0.25 0.035	5 41 0.18		0.02 0.03 <2				2	2	
RE 5600N 525E	570524.8 54		20 9	24 0.5	18 1	0 113 3.01	8 <8 <2	2	19 <.5 <3	<3	64 0.25 0.038	6 38 0.15	56 0.15 <3 3.64	0.03 0.03 <2				1.8	1.6	
5600N 550E	570550.4 54		27 21			8 554 3.75	10 <8 <2		23 <.5 <3	<3	101 0.34 0.022		100 0.09 <3 3.08	0.02 0.05 <2				2.7	2.7	
5600N 575E			23 19	54 <.3		0 101 3.68	5 <8 <2	4	5 < 5 < 3	<3	74 0.07 0.057	6 25 0.38	56 0.08 <3 3.5	0.01 0.04 <2				1.4	1.4	
5600N 600E			4 6	27 <.3	13	7 82 2.6	5 <8 <2	6	5 < 5 <3	<3	38 0.07 0.028	6 8 0.25	57 0.05 <3 2.53	0.01 0.03 <2				1.4	1.4	
5600N 625E			1 8	41 <.3		2 150 2.89 <		3	8 <.5 <3	<3	56 0.1 0.022		127 0.11 <3 3.31	0.02 0.05 <2				1	1	
\$600N 850E	570852.2 54			14 0.3			6<8<2		33 <.5 <3	<3		15 19 0.51		0.01 0.05 <2				<,5 <,		
5600N 875E	570677.2 54			50 <.3		4 181 2.8	8<8 <2		7 <.5 <3		72 0.18 0.019	6 29 0.63		0.01 0.04 <2				0.6	0.8	
5600N 700E	570702.8 54	75602 <1	18	52 <.3	28 1	0 168 3.38	8<8 <2	4	5<.5<3	<3	89 0.13 0.021	10 41 0.81	50 0.09 <3 1.83	0.01 0.06 <2				1.2	1.2	

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| 5500N 200E | 570194.1 | 5475502 1 | 22
 | 18
 | 73 <.3 | 17
 | 10 404 2.48 4 <8
 | <2 | 6
 | 5 <.5 3<3 | 39 0.06 0.043
 | 16 5 0.82 8 | 6 0.06 <3
 | 2.15
 | 0.01 0.08 <2 |
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| 5500N 225E | 570219.5 | 5475502 1 | 19
 | 15
 | 64 <.3 | 13
 | 8 329 2.68 3 <8
 | <2 | - 4
 | 5<,5<3<3 | 56 0.07 0.028
 | 18 1 0.73 4 | 4 0.04 <3
 | 1.5
 | 0.01 0.05 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 250E | 570244.2 | 5475502 <1 | 22
 | 20
 | 62 <.3 | 13
 | 8 181 2.65 7 <8
 | <2 | 5
 | 5 < 5 < 3 < 3 | 50 0.07 0.038
 | 13 2 0.54 5 | 2 0.08 < 3
 | 2.03
 | 0.01 0.05 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 275E | 570270.4 | 5475502 2 | 12
 | 37
 | | 9
 | 7 176 2.17 2 <8
 | <2 | 3
 | 5 0.5 <3 <3 | 36 0.06 0.092
 | 8 <1 0.22 8 |
 | 2.07
 | 0.02 0.05 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 300E | 570295.3 | | 21
 | 18
 | | 8
 | 10 425 2.3 <2 <8
 | <2 | 2
 | 5 0.9 <3 <3 | 41 0.05 0.178
 | 5 <1 0.15 5 |
 | 3.36
 | 0.02 0.03 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 325E | 570321.3 | | 17
 | 18
 | | â
 | 7 114 2.48 3 <8
 | <2 | <2 -
 | 8 0.5 <3 <3 | 73 0.12 0.028
 | 6 1 0.2 4 |
 | 1.21
 | 0.01 0.04 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 350E | 570346.5 | | 27
 | 15
 | | 14
 | 13 388 3.44 8 <8
 | <2 | 4
 | 8<.5<3<3 | 88 0.11 0.048
 | 10 8 0.43 4 |
 | 2.3
 | 0.01 0.06 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 375E | | 5475502 1 | 10
 | 10
 | | 10
 | 7 136 2.98 2 <8
 | <2 | 3
 | 8 0.5 <3 <3 | 56 0.09 0.035
 | 8 2 0 21 5 |
 | 2.15
 | 0.01 0.05 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 400E | | 5475502 <1 | 24
 | 7
 | 91 0.4 | 24
 | 11 324 3.88 2 <8
 | ~2 | 2
 | 15 < 5 < 3 < 3 | 107 0.15 0.055
 | 4 13 0.3 8 |
 | 3.64
 | 0.02 0.09 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 425E | 570423 | | 14
 | 11
 | | 15
 | 9 198 2.95 5 <8
 | <2 | 23
 | 9<5<3<3 | 83 0.12 0.029
 | 9 11 0.35 5 |
 | 1.65
 | 0.02 0.09 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 450E | | | 34
 | 11
 | | 15
 | 12 535 2.73 7 <8
 | <2 | 3
 | 14 < 5 < 3 < 3 | 85 0.24 0.023
 | 9 19 0.55 5 |
 | 1.58
 | 0.01 0.04 <2 |
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| | | 5475502 1 |
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| 5500N 475E | 570473.9 | | 21
 | 9
 | 71 < 3 | 25
 | 14 678 2.96 6 <8
 | <2 | 2
 | 18 < 5 < 3 < 3 | 80 0.27 0.022
 | 8 33 0.58 8 |
 | 2
 | 0.01 0.05 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 500E | 570499.3 | | 16
 | 20
 | | 19
 | 15 211 2.01 7 <8
 | <2 | 2
 | 10 <.5 <3 <3 | 56 0.14 0.043
 | 4 28 0.28 5 |
 | 3.04
 | 0.02 0.05 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 525E | 570524.8 | | 23
 | 17
 | | 25
 | 14 282 3.03 12 <8
 | <2 | 2
 | 25 <.5 <3 <3 | 89 0.44 0.022
 | 7 45 0.48 9 |
 | 2.44
 | 0.02 0.05 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 550E | 570549.8 | | 21
 | 10
 | | 26
 | 11 139 2.63 5 <8
 | <2 | 2
 | 7 <.5 <3 <3 | 61 0.15 0.031
 | 6 38 0.5 5 |
 | 2.34
 | 0.01 0.04 2 |
 | | | | | | | | | | | | | | | |
| 5500N 575E | 570575.8 | | 41
 | 18
 | | 42
 | 17 215 2.9 7 <8
 | <2 | <2
 | 8<.5<3<3 | 73 0.16 0.021
 | 4 81 0.83 5 |
 | 2.5
 | 0.01 0.03 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 800E | | 5475503 <1 | 21
 | 12
 | | 21
 | 9 110 2.63 4 <8
 | <2 | 2
 | 7 <.5 <3 <3 | 57 D.18 0.02
 | 6 29 0.37 5 |
 | 2.31
 | 0.01 0.04 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 625E | | 5475503 <1 | 14
 | 12
 | | 17
 | 8 157 2.67 5 <8
 | <2 | 2
 | 5<,5<3<3 | 52 0.1 0.023
 | 7 17 0.27 8 |
 | 2.32
 | 0.01 0.05 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 650E | 570654 | 5475503 2 | 29
 | 16
 | 44 <.3 | 18
 | 8 138 2.47 6 <8
 | <2 | - 4
 | 6<.5<3<3 | 46 0.11 0.015
 | 13 15 0.53 3 | 9 0.07 <3
 | 1.73
 | 0.01 0.07 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 675E | 570877.8 | 5475503 1 | 18
 | 8
 | 32 < 3 | 12
 | 6 103 2.82 7 <8
 | <2 | 3
 | 8<.5<3<3 | 56 0.12 0.024
 | 8 16 0.29 5 | 0 0.09 <3
 | 1.85
 | 0.02 0.04 <2 |
 | | | | | | | | | | | | | | | |
| 5500N 700E | 570702.8 | 5475503 <1 | 18
 | 7
 | 28 < 3 | 13
 | 8 100 2.45 10 <8
 | <2 | 2
 | 13 <.5 <3 <3 | 66 0.31 0.015
 | 10 17 0.8 5 | 5 0.05 <3
 | 1.49
 | 0.01 0.04 <2 |
 | | | | | | | | | | | | | | | |
| 850N 8900E | 568892.6 | 5473891 1 | 16
 | 11
 | 110 <.3 | 15
 | 14 886 2.35 5 <8
 | <2 | 2
 | 7 <.5 <3 <3 | 52 0.15 0.069
 | 5 1 0.22 6 | 1 0.1t<3
 | 2.2
 | 0.02 0.06 <2 |
 | | | | | | | | | | | | | | | |
| 850N 8925E | 588917.8 | 5473891 2 | 67
 | 18
 | 89 0.3 | 39
 | 16 440 3.34 2 <8
 | <2 | 5
 | 14 <.5 <3 <3 | 77 0.18 0.072
 | 10 10 0.35 9 | 9 0.16 <3
 | 4.26
 | 0.02 0.09 <2 |
 | | | | | | | | | | | | | | | |
| 850N 8950E | 566942.7 | 5473891 1 | 72
 | 10
 | 64 < 3 | 17
 | 11 929 2.24 2 <8
 | <2 | 3
 | 10 < 5 < 3 < 3 | 60 0.23 0.03
 | 11 3 0.41 5 | 1 0.08 <3
 | 1.51
 | 0.01 0.06 <2 |
 | | | | | | | | | | | | | | | |
| 650N 8975E | 568967.7 | 5473891 <1 | 21
 | 12
 | | 12
 | 13 1078 2.44 3 <8
 | -2 | 3
 | 13 < 5 < 3 < 3 | 56 0.21 0.076
 | 9 5 0.22 6 |
 | 1,68
 | 0.01 0.08 <2 |
 | | | | | | | | | | | | | | | |
| 650N 9000E | 568993.6 | 5473891 1 | 30
 | 11
 | | 21
 | 11 167 2.82 <2 <8
 | < |
 | 10 < 5 < 3 < 3 | 57 0.15 0.081
 | 11 8 0.25 8 |
 | 2.77
 | 0.02 0.07 <2 |
 | | | | | | | | | | | | | | | |
| 850N 9025E | 569019 | 5473891 1 | 23
 | 11
 | | 15
 | 9 151 2.43 2 <8
 | ~2 |
 | 11 < 5 < 3 < 3 | 44 0.22 0.117
 | 11 4 0.25 6 |
 | 2.28
 | 0.02 0.07 <2 |
 | | | | | | | | | | | | | | | |
| 850N 9050E | 569044.7 | 5473891 1 | 12
 | 12
 | | 10
 | 8 140 2.17 4 <8
 | ~ | 5
 | 6<5<3<3 | 30 0.06 0.127
 | 5 2 0.12 6 |
 | 3.67
 | 0.02 0.06 <2 |
 | | | | | | | | | | | | | | | |
| 850N 9075E | 569070 | 5473891 1 |
 | 12
 | | 14
 | 10 340 2.13 3 <8
 | <2 | 8
 | 7 < 5 < 3 < 3 | 34 0,1 0.077
 | 12 3 0.24 8 |
 | 2.83
 | 0.02 0.09 <2 |
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| RE 850N 9075E | 569070 | 5473891 1 | 26
 | 11
 | | 15
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 | <2 | 6
 | |
 | 13 5 0.25 9 |
 | 2.98
 | 0.02 0.09 <2 |
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| 850N 9100E | 589095.6 | 5473890 <1 | 15
 | 12
 | | 12
 | 7 117 1.99 <2 <8
 | ~2 | 3
 | 8 <.5 <3 <3 | 31 0.06 0.158
 | 5 <1 0.1 7 |
 | 3.48
 | 0.02 0.05 <2 |
 | | | | | | | | | | | | | | | |
| 850N 9125E | 569120.1 | 5473891 2 | 8
 | 15
 | 89 <.3 | 10
 | 4 90 2.28 3 <8
 | <2 | 5
 | 8 < 5 < 3 < 3 | 36 0.12 0.137
 | 13 2 0.16 6 |
 | 1.75
 | 0.01 0.08 <z< td=""><td></td></z<> |
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| 850N 9150E | 569146.5 | 5473890 <1 | 8
 | 12
 | | 10
 | 5 176 1.61 2 <8
 | <2 | 4
 | 5<.5<3<3 | 0.25 0.07 0.064
 | 15 <1 0.24 81 |
 | 1.35
 | 0.01 0.09 <2 |
 | | | | | | | | | | | | | | | |
| 850N 9175E | 569171.4 | | 14
 | 8
 | 92 < 3 | 14
 | 8 199 1.76 2 <8
 | <2 | - 4
 | 8<.5<3<3 | 27 0.05 0.11
 | 6 <1 0.11 7 |
 | 3.09
 | 0.02 0.05 <2 |
 | | | | | | | | | | | | | | | |
| 850N 9200E | 569197 | 5473890 <1 | 8
 | 12
 | | 10
 | 5 308 1.82 2 <8
 | <2 | - 4
 | 6 <.5 <3 <3 | 28 0.09 0.064
 | 10 <1 0.22 8 |
 | 1,54
 | 0.01 0.1 <2 |
 | | | | | | | | | | | | | | | |
| 850N 9225E | 589222.5 | 5473890 <1 | 7
 | 10
 | 52 <.3 | 10
 | 8 137 1.8 <2 <8
 | <2 | - 4
 | 7<.5<3<3 | 28 0.09 0.049
 | 11 <1 0.31 54 |
 | 1.47
 | 0.01 0.07 <2 |
 | | | | | | | | | | | | | | | |
| 850N 9250E | 569247.9 | 5473890 1 | 10
 | 11
 | 77 <.3 | 13
 | 11 511 1.74 3 <8
 | <2 | 2
 | \$<.5 <3 <3 | 29 0.08 0.053
 | 8 <1 0.37 7 |
 | 1.81
 | 0.02 0.08 <2 |
 | | | | | | | | | | | | | | | |
| 850N 9275E | 569273.4 | 5473890 1 | 10
 | 8
 | 59 <.3 | 12
 | 9 914 1.84 <2 <8
 | <2 | 3
 | 7 < 5 <3 <3 | 31 0.07 0.074
 | 11 <1 0.21 9K | 8 0.07 <3
 | 1.79
 | 0.01 0.08 <2 |
 | | | | | | | | | | | | | | | |
| 850N 9300E | 569297.7 | 5473890 1 | 11
 | 26
 | 130 <.3 | 16
 | 11 1129 1.98 <2 <8
 | <2 | 5
 | 15 <.5 <3 <3 | 31 0.15 0.058
 | 13 1 0.22 18 |
 | 1.74
 | 0.01 0.11 <2 |
 | | | | | | | | | | | | | | | |
| 850N 9325E | 569323.9 | 5473890 2 | 21
 | 19
 | 103 <.3 | 22
 | 18 1531 2.78 <2 <8
 | <2 | 6
 | 12 <,5 <3 <3 | 44 0,16 0.045
 | 17 6 0.41 14 | 4 0.09 <3
 | 2.52
 | 0.01 0.12 <2 |
 | | | | | | | | | | | | | | | |
| 850N 9350E | 139349.2 | 5473890 2 | 21
 | 21
 | 158 <.3 | 19
 | 18 1119 2.74 4 <8
 | <2 | 7
 | 22 <.5 13 <3 | 42 0.2 0.094
 | 18 7 0.35 286 | 5 0.08 <3
 | 2.45
 | 0.01 0.11 2 | 4
 | | | | | | | | | | | | | | | |
| 850N 9375E | .89374.6 | 5473890 1 | 23
 | 18
 | 81 < 3 | 19
 | 14 1470 2.88 <2 <8
 | <2 | 5
 | 9<5 3 <3 | 51 0,11 0.037
 | 16 7 0.43 134 | 5 0.07 <3
 | 2.48
 | 0.01 0.1 <2 |
 | | | | | | | | | | | | | | | |
| 850N 9400E | 569399.7 | 5473890 2 | 35
 | 16
 | 69 <.3 | 18
 | 14 251 2.94 <2 <8
 | <2 | 8
 | 5 < 5 < 3 < 3 | 53 0.08 0.061
 | 15 6 0.51 86 | B 0,1 <3
 | 3,16
 | 0.01 0.11 .0 |
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| 850N 9425E | 569425.9 | 5473890 1 |
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 | 0.01 0.11 <2 |
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| 650N 9450E | | | 21
 | 22
 | 47 < 3 | 13
 |
 | <2 | 8
 | 5<5<3<3 |
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| | 559451 | | 21
37
 | 22
19
 | | 13
20
 | 12 412 2.65 3 <8
 | <2
<2 | 8
 | | 49 0.06 0.029
 | 18 1 0.45 5 | 9 0.05 <3
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650N 9600E	569602.5					87 <.3	24		725 2.25	2 <8	<2	4	11 <.5	<3	<3		0.14 0.063				0.06 <3	2.51		0.14 <2		1.8	
650N 9625E		5473849 <1				87 < 3	30		467 2.97	2 <8	<2	4	12 <.5	<3	<3 <3		0.16 0.077				0.08 <3	2.87		0.09 <2		0.5	
650N 9650E 650N 9675E		5473649 <1		15 16		45 <.3 44 <.3	17 19		210 1.47 < 203 1.51 <		<2 <2	3 2	10 <.5 B < 5	<3 <3	<3 <3		0.19 0.009 0.18 0.01		6 0.46 13 0.49).05 <3	1.32 1.29		0.05 <2		0.0 0.5	
650N 9700E		5473849 <1 5473849 <1		23		45 < 3	26		203 1.51 ~	2 <8	<2	2	16 <.5	<3	<3		0.17 0.02				0.07 <3	2.21		0.05 <2		0.5	
650N 9725E	589729.3	5473849 <1		36		85 <.3	31		484 3.1	5 < 8	~2	ŝ	7 <.5	<3	<3		0.1 0.077				0.1 <3	3.45		0.16 <2		5.4	
650N 9750E	569754.1	5473849			•																						
650N 9775E	569778.8	5473649 <1		22	12	51 <.3	22	11	366 2.32	3 <8	<2	5	13 <.5	<3	<3		0.15 0.018	14	15 0.5	97 0	0.07 <3	2.32	0.02	0.07 <2		0.8	
650N 9800E	569804.6					41 <.3	28		225 3.21	3 < 8	<2	9	10 <.5	<3	<3		0.07 0.057).14 <3	4.05	0.02	0.1 <2		1.6	
20 800W	568566.1		1			41 <.3	8	4	71 1.99	3<8 4<8	<2	6	4 < 5	<3	<3		0.02 0.041	12 <1			0.05 <3	2.13		0.04 <2		1.2	
RE 20 600W 20 575W	568566.1 568581.7	5475251 5475222 <1	1	*		40 < 3 24 < 3	8	3 2	70 1.94 50 1.47	4 <8	<2 <2	6	4 <.5 2 <.5	<3 <3	<3 <3		0.02 0.041	12 <1).04 <3).04 <3	2.08 0.6		0.05 <2			
20 575W	568591.9		1	6		31 < 3	6	2	66 1.95	3<8	<2	3	2 < 5	<3	<3		0.02 0.02	17 <1).04 <3	1.07		0.04 <2		6.6	
20 525W	568600.1		ż			21 < 3	Ă	1	50 1.76	3 <8	<2	3	3 < 5	<3	<3		0.02 0.02		1 0 07		.03 <3	1.06		0.04 <2		2.5	
20 500W	568615.1	5475162 <1				40 <.3	11	5	84 2	4 <8	<2	6	4 < 5	<3	<3		0.03 0.045	12 <1			07 <3	2.37		0.04 <2		4.2	
20 475W	568834.1	5475142	2	9	12	52 <.3	10		155 2.08	3 <8	<2	4	5 <.5	<3	<3	34 (0.03 0.043	10	1 0.16	72	0.1 <3	2.02	0.01	0.06 <2		1.1	
20 450W	568654.8					63 <.3	14		385 2.75 <		<2	3	7 <.5	<3	<3		0.08 0.099				12 <3	3.26		0.06 <2		2	
20 425W	568876.3					63 < 3	15		162 2.7	5 <8	<2	5	6 < 5	<3	<3		0.04 0.08		1 0.3		.09 <3	3.22		0.06 <2		11.9	1
20 400W 20 375W	588704.7 568725.7					47 < 3 38 < 3	11 13		176 2.12 < 132 2.16	2 <8 2 <8	<2 <2	1	8 <.5 7 <.5	<3 <3	<3 <3		0.06 0.13	6 6 < 1	10.17		1.13 <3 1 14 <3	4.01 3.9		0.05 <2		2.1	
20 375W	568748.9					50 <.3 64 0.4	15		170 2.56 <		<2	5	8<5	<3	<3		0.05 0.088	7 <1			0.15 < 3	3.9		0.05 <2		1.8 4.6	
20 325W	568769.8					41 < 3	19		425 2.13 <		<2	5	11 < 5	<3	<3	••••	0.1 0.08				13 <3	3.66		0.05 <2		9.4	
20 300W	568791.1				14	48 <.3	18	11	305 2.4	4 <8	<2	6	7 < 5	<3	<3	29 (0.05 0.067	8	1 0.19	107 0	.12 <3	3.76		0.05 <2		18.4	t
20 275W	566820	5475048	2	24	18	58 <.3	20	13	379 2.93	4 <8	<2	8	B <.5	<3	<3	30 0	0.04 0.083	18	4 0.35	96 Q	D8 <3	2.87	0.01	0.06 <2		29.2	2
20 250W	566656					48 <.3	13		287 2.73	4 <8	<2	6	4 <.5	<3	<3		0.03 0.044		1 0.21		08 <3	2.44		0.05 <2		20.9	2
20 225W	568869.1					68 < 3	12		366 2.97	4 <8	<2	6	6 < 5	<3	<3		0.04 0.081	12	6 0.19		0.1 <3	2.32		0.06 <2		33.1	3
20 200W	568884.9 568897.1			· -		63 0.4	12 17		238 3.38 440 2.97	4 <8 5 <8	<2 <2	4	5 <.5 4 <.5	<3 <3	<3 <3		0.04 0.057		10 0.24		0.1 <3	2.21 3.52		0.06 <2		17.2 18.6	1
20 175W 20 150W	568907.6					67 <.3 57 0.3	15		225 2.62	2 <8	<2	é	8 < 5	<3	<3		0.04 0.094		5 0.25		0.1 <3	4.1		0.05 <2		5.9	'
20 125W	568913.8					54 0.8	9		251 1.78 <		<2	4		5 < 3	<3		0.05 0.14	š	1 0.11		16 <3	4,6		0.04 <2		2	
20 100W	568926.3				11	53 <.3	18		174 2.28	2 <8	<2	2	6 <.5	<3	<3		0.04 0,11	5	1 0.12	4: 0	14 <3	2.98		0.04 <2		2.1	
20 75W	568938.2					50 <.3	11		146 2.01	2 <8	<2	5	7 <.5	<3	<3		0.04 0.14	6 <1			.14 <3	4.12		0.05 <2		3.3	
20 50W	508942.2					38 <.3	10		245 1.89 <		<2	3	10 <.5	<3	<3		0.08 0.05	6 <1			0.1 <3	2.95		0.03 <2		3.2	
20 25W 20 00W	588943.9 588943.9					38 <.3 39 <.3	12 11		106 2.7 126 2.24	4 <8 4 <8	<2 <2	6	4 < 5 5 < 5	<3 <3	<3 <3		0.02 0.052 0.03 0.038		2 0.3 1 0.25		05 <3	1.74 1.69		0.05 <2 0.05 <2		7.2 2.4	
1970 OOE	568494.1		2 3	13 B		30 < 3	13		235 1.51	3 <8	<2	4	12 <.5	<3	<3		0.09 0.030	17 <1			.03 <3	1.29		0.03 <2		0.8	
1970 25E	568508.3					45 < 3	12		76 2.09 <		<2	6	4 < 5	<3	<3		0.03 0.08	10 <1			05 3			0.04 <2		1.7	
1970 50E	568522.5		2	8		28 <.3	9	5	55 1.82 <		<2	5	4 <.5	<3	<3	19 (0.03 0.033	13 <1	0.18	51 0	.05 <3	2.1	0.01	0.03 <2		6.9	
1970 75E		5475139 <1		10 <3		35 <.3	10		98 1.88 <		<2	6	4 <.5	<3	<3		0.03 0.08	8 <1			07 <3	2.73		0.03 <2		1.9	
1970 100E	568554.2					46 <.3	11		161 2.02 <		<2	5	5 <.5	<3	<3		0.04 0.074	8 <1			08 <3	2.88		0.04 <2		3.9	
1970 125E	566572.9		3	7		40 <.3 54 < 3	10 12	4	98 2.09 131 2.38	3<8 4<8	<2 <2	5 15	4 <.5 6 <.5	<3 <3	<3 <3		0.02 0.027 · 0.04 0.079	17 <1 9	0.26		.04 <3 .09 <3	1.18 2.89		0.04 <2		7.2 3.5	
1970 150E 1970 175E	568593 568612.9					54 < 3 53 < 3	12		131 2.30 241 1.91 <		~2	4	6 <.5 7 < 5	<3	<3		0.04 0.079		0.12		14 <3	2.89 3.37		0.04 <2		3.5	
1970 200E	566632.7					42 < 3	26		239 2.83	8 <8	<2	6	12 < 5	<3	<3		0.12 0.039				.05 <3	2.26		0.04 <2		33.4	3
1970 225E	566658.2	5475046			12	64 < 3	12	7	298 2.35	2 <8	<2	4	6 < 5	<3	<3	33 (0.06 0.062	7			13 <3	2.85		0.05 <2		2.8	,
1970 250E	588676.3					64 <.3	13		090 3.17	3 <8	<2	5	5 < 5	<3	<3		0.04 0.046				.09 <3	1.74		0.06 <2		15.1	1
1970 275E	566701.3					45 < 3	14		163 2.45	4 <8	<2	6	5 < 5	<3	<3		0.04 0.044		2 0.28		.07 <3	1.83		0.05 <2		12	
1970 300E RE 1970 300E	568722.3 568722.3					40 < 3 38 < 3	16 16		108 2.74 104 2.67	6<8 5<8	<2 <2	8 8	4 <.5 4 <.5	<3 <3	<3 <3		0.02 0.034		2 0.34		03 <3	1.65 <.01		0.04 <2 0.03 <2		65.2 68	6
1970 325E	568722.3			20 13		36 < 3	20		104 2.67	5<8 3<8	<2	7	4 <.5	<3 <3	<3		0.02 0.033				09 <3	3.02	0.01	0.03 <2		54.9	5
1970 350E	568763.6					63 < 3	13		435 3.18	2 <8	<2	i i	8 < 5	<3	<3		0.03 0.076		3 0.21		11 <3	2.58		0.05 <2		4.9	•
1970 375E	568760.9					58 < 3	16		185 2.58	2 8	<2	6	8 <.5	<3	<3		0.05 0.047				.09 <3	2.6		0.05 <2		17.1	1
1970 400E	568808.1	5474953	2	12	16	84 < 3	16	10	570 2.63	2 <8	<2	3	8 <.5	<3	<3	36 0	0.04 0.05	9	2 0.23	126 D	.11 <3	2.52	0.01	0.05 2		3.3	
1970 425E						68 < 3	21		646 4.06	7 <8	<2	6	5 <.5	<3	<3		0.04 0.069				.08 <3	1.91		0.04 <2		149	14
1970 450E	568848.1					68 < 3	13		488 2.34 <		<2		10 <.5	<3	<3		0.1 0.076				.14 <3	3.94		0.05 <2		5.9	-
1970 475E	568897.7					82 0.5	14		657 2.84 <	2 <8 6 <8	<2	6	6 <.5	<3 <3	<3 <3		0.05 0.096				.11 <3 .08 <3	3.57 3.41		0.06 <2		29.5 19.8	2
1970 500E 1970 525E	568914.1 568933.1					92 0.4 55 <.3	16 15		568 3.32 397 2.49	6<8 3<8	<2 <2	7	4 <.5	<3 <3	<3		0.02 0.095				.08 <3	3.41		0.05 <2 0.04 <2		19.8	10
1970 523E	568947.9					53 < 3	15		235 2.61	4 <8	<2	,	5 <.5	<3	<3		0.04 0.093	9 <1			.09 <3	3.63		0.04 <2		13.8	1
1970 575E	568964					53 < 3 52 < 3	19		135 2.55	3 <8	<2	7	5<.5	3	<3		0.04 0.055	11 <1			0.1 < 3	3.44		0.04 <2		63.4	6
1970 600E	568974.2					74 < 3	18		235 2.69	4 <8	<2	7	5 <.5	<3	<3		0.04 0.072				08 < 3	2.66		0.05 <2		22	2
1970 625E	568966.1		1	16		49 <.3	15		206 2.74	4 <8	<2	6	6 <.5	<3	<3		0.05 0.049				.06 <3	2.36		0.05 2		40.9	- 4
1970 650E	568994.9					45 <.3	16		227 2.7	2 <8	<2	5	6 <.5	<3	<3		0.05 0.051				07 <3	2.65		0.04 <2		34.6	3
1970 675E	569003.7	5475127	3	20	9	47 <.3	17	11 :	237 2.81	2 <8	<2	6	8 <.5	<3	<3	30 0	0.06 0.096	8	3 0.21	96	0.1 <3	3.7	0.01	0.05 2		5.8	

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1.7 1.8 2.3 1.5 1.4 0.7 0.5 0.9 1.8 0.5 0.5 0.5 1.4

0.8 1.8 1.2

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1970 700E	569011.6		1 11	8 50 <.	• • •	9 462 2.24	3<8<2	5	6 < 5 <		28 0.04 0.089		58 0.11 <3 3.77	0.01 0.05 <2				1	1.8 1.8	
1970 725E	569019.3			12 49 <	• ••	6 148 3.02 6 183 2.29	4 < 5 < 2 3 < 8 < 2	8 6	5 < 5 •	• •	36 0.03 0.049	17 5 0.32		0.01 0.05 <2				30	0.5 30.5	
1970 750E 1970 775E	569028.6 569036	5475204 5475227	• ••	13:45 <. 10:42 <.		6 183 2.29 7 204 2.28	3<8<2	5	6 <.5 ×		32 0.03 0.124 27 0.03 0.078	6 <1 0.14	59 0.14 <3 5.12 60 0.08 <3 2.86	0.02 0.04 <2 0.01 0.04 <2					1 1	
1970 800E	569047.0			8 40 <		4 130 2.54	8<8<2	4	4<5		33 0.02 0.036	19 1 0.3		0.01 0.04 <2						
25 500E	567502		0.4 20.2 9	8 60 <	1 t0	5.2 150 2.42	4.2 1.8 4.9	4.5	2 <.1	0.1 0.2	28 0.02 0.038	8 17.2 0.3	67 0.08 <1 1.47	0.003 0.21 0.1	0.01 2.2	0.3 <.05	5 <.5	15	4.9	
25 525E	567526.3		0.7 26.7 42			8.5 592 2.64	4.5 1 8.4	4.2	3 0.2	0.4 0.2	26 0.05 0.169		56 D.102 <1 2.93	0.013 0.08 0.2	0.08 2.2			7.5	6.4	
25 550E	587551.5		•	13 48 6		4.4 145 2.1	3.8 1.2 2.4	3.4	5 0.1	0.1 0.2	32 0.06 0.167		44 0.118 <1 5.89	0.018 0.04 0.2	0.1 4			15	2.4	
25 575E 25 600E	567576.4 567601.4		0.8 52.5 15			6.3 164 2.57 16.2 255 3.81	5.9 0.7 1.4 15.6 1.1 18.5	3 2.2	4 0.1 6 0.1	0.2 0.2	47 0.06 0.113		48 0.108 <1 4.37 61 0.104 <1 2.44	0.011 0.03 0.2	0.09 3.5		11: 0.5 10 < 5	15 15	1.4 18.5	
25 625E	567626.5		0.6 60.1 10				7.2 0.6 8.5		8 0.2	0.2 0.1	69 0.14 0.047		67 0.082 <1 1.9	0.011 0.07 0.1	0.03 3.7	0.1 < 05	8 < 5	15	8.5	
25 850E	587851.5		0.4 142.4 11	3 73 0	0.2 17.1	19.8 241 5.23	18.7 1,1 8.2	2.8	10 0.2	0.3 0.1	135 0.17 0.067	7 15.7 0.78	133 0.089 <1 2.47	0.006 0.04 0.1	0.02 9.2	0.1 <.05	9 < 5	15	8.2	
25 675E	567676.4						4.3 0.8 4.5		7 0.3	0.1 0.2	90 0.1 0.043		116 0.097 <1 2.69	0.011 0.05 < 1	0.08 6.4			15	4.5	
25 700E	567701.4						2.3 0.5 33.5		4 0.1	0.1 0.1	59 0.08 0.028		54 0.07 <1 1.52	0.004 0.05 <.1	0.01 4.8			15	33.5	
25 725E 25 750E	567728.5 567751.4		0.3 25.4 17				2.6 0.5 4	2.7 3.7	9 0.1 18 0.5	0.2 0.3 0.2 0.5	45 0.12 0.028 74 0.25 0.048		93 0.055 <1 1.28	0.009 0.05 0.1 0.013 0.07 0.1	0.03 2.9			15 15	4 3.1	
25 775E	567776.4						1.6 0.2 4.6		5 0.1	0.1 0.2	75 0.13 0.02		39 0.071 <1 0.79	0.006 0.03 < 1	0.01 2.5	••••		15	4.6	
25 800E	567801.3						3.2 0.6 15.6		8 0.1	0.1 0.2	52 0.1 0.055		80 0.081 1 2.77	0.009 0.04 0.1	0.05 3.2		8 <.5	15	15.6	
25 825E	567826.5						2.9 0.7 1.5		7 0.1	0.2 0.2	36 0.07 0.031		62 0.078 <1 1.34	0.006 0.07 0.1	0.03 2.1		7 <.5	15	1.5	
25 850E	567851.4						4.1 0.7 1.9		9 0.1	0.2 0.3	45 0.09 0.041		86 0.104 <1 1.38	0.015 0.06 0.1	0.05 2.5			7.5	1.9	
25 875E	567876.4						2.5 0.7 2.3 26 0.5 1.7	4.3	3 0.1 4 0.1	0.1 0.1	34 0.04 0.053 39 0.07 0.02		65 0.073 <1 1.08 86 0.072 <1 1.38	0.004 0.1 <.1 0.004 0.13 <.1	0.01 2		5<.5 4<5	15	2.3	
25 900E 25 925E	567901.5 1 567926.5			19 53 <.		9 185 2.1 6.7 177 2.28	2.6 0.5 1.7 2 1.1 1.7		4 0.1 7 0.1				89 0.082 <1 1.74	0.01 0.07 < 1	0.02 2.2		7 < 5	15 15	1.7	
25 950E	567951.4					11.2 332 2.89	4 0.7 1.8	3.7	9 0.1				70 0.138 <1 2.6	0.017 0.05 0.1	0.05 4.8			15	1.8	
25 975E	567976.4						3.1 1 1.1				87 0.19 0.039		134 0.125 <1 2.93	0.012 0.07 < 1	0.03 10.4			7.5	1.1	
RE 25 975E	567976.4						2.8 1.1 0.7				105 0.18 0.038		132 0.114 <1 2.81	0.013 0.06 < 1	0.03 11.6			7.5	0.7	
25 1000E	568001.5						5.4 1 0.5				73 0.2 0.034		65 0.112 1 2.12	0.015 0.05 0.1	0.05 4.8			15	0.5	
26 500E 26 525E	587499.7					8.8 163 2.63 22.5 2118 3.3	4.7 0.8 18						39 0.059 <1 1.2 113 0.103 1 1.9	0.004 0.06 0.1 0.013 0.1 0.1	0.03 2.6			15 7.5	16 26.1	
26 525E	567524.6 567549.8						8.4 1.4 1.5						58 D.178 <1 1.84	0.016 0.04 0.2	0.04 2.8			15	1.5	
26 575E	587574.7		1.1 32.9 22			8.1 343 4.14	6 0.5 0.8				75 0.17 0.049		107 0.152 1 1.57	0.012 0.06 0.2	0.08 2	•	5 17 <.5	7.5	0.8	
26 600E	587599.7					7 477 1.14			21 0.6				93 0.04 2 0.94	0.009 0.07 0.1	0.04 0.9		6 < 5	7.5	1.7	
26 625E	567624.6					14.8 859 2.86	5.8 1 19.8						106 0.091 1 1.81	0.011 0.08 0.1	0.02 2.4		11 <.5	15	19.8	
26 650E	567649.8		0.4 12.3				5.2 0.4 5.2						53 0.075 <1 0.98	0.007 0.05 0.1	0.02 1.4			15	5.2	
26 675E 26 700E	587874.7						8.5 2.7 5.2		12 0.2 13 0.3	0.2 0.4	91 0.11 0.053	45 35.8 0.34	70 0.122 1 4.02 88 0.108 <1 2.13	0.015 0.08 0.1	0.09 12.7			15 15	5.2 2.9	
26 725E	567699.7 567724.8 5						1,4 0.5 5		5 0.3 5 0.2				55 0.089 <1 0.92	0.007 0.03 < 1	0.03 3	•		15	5	
26 750E	567749.8						3.4 0.5 4.9		4 0.1		51 0.06 0.023		51 0.053 2 1.84	0.008 0.04 0.1	0.05 2.9			15	4.9	
26 775E	587774.7	5472602	0.7 24.1 16				4.7 0.9 3.6		5 0.2		47 0.05 0.099	8 17.5 0.28		0.011 0.04 0.1	0.09 2.8			15	3.8	
26 800E	567799.6						3.7 0.8 3				50 0.04 0.081	4 13.3 0.07		0.014 0.02 0.1	0.13 2.4			15	3	
26 8∡5E 26 8∪0E	567824.8 587849.7					21.9 2153 2.89 4.4 623 1.58					52 0.15 0.041 37 0.06 0.073	34 23.4 0.38 8 9.2 0.13		0.011 0.06 0.1 0.011 0.04 0.1	0.04 ± 3.2		5 10 <.5 5 9 <.5	7.5 15	2.2	
26 875E	567874.7					7.1 313 2.15		3.1			36 0.06 0.018			0.008 0.04 0.1	0.04 1.5			15	<.5	
28 9006	567899.8					20.8 238 5.48						19 32.7 0.72		0.016 0.07 0.1	0.05 5.3		20 <.5	7.5	10.7	
26 925E	567924.8					6.7 113 3.23					83 0.07 C.027	7 18.8 0.17		0,012 0.03 0.1	0.08 4.4		5 13 < 5	15	3.1	
28 950E	567949.7						2.4 2 2.8				80 0.24 0.043			0.014 0.08 <.1	0.06 10.1		5 14 0.5	15	2.8	
26 975E 26 1000E	587974.7 5 587999.8 5					8.8 138 3.11 17.8 963 3.32	2.6 0.5 2				87 0.13 0.021 90 0.21 0.031	8 48 0.34 12 57.7 0.58		0.013 0.03 0.1 0.012 0.06 <.1	0.08 4,7		5 10 <.5 5 9 <.5	15 15	2 2.8	
27 500E	567499.9					11.1 289 2.01					45 0.09 0.024	19 21.8 0.89		0.008 0.05 0.1	0.02 2.4			7.5	121.1	
27 525E	587524.9					10.2 251 3.72			9 Q.3	0.2 0.8	69 0.08 0.032	16 23.4 0.46		0.01 0.08 0.1	0.08 3.9		5 12 < 5	7.5	2.1	
27 550E	567549.8						2 0.9 19.6		7 0.3		40 0.07 0.025	16 14 0.37		0.008 0.04 0.1	0.04 1.9			15	19.6	
27 575E 27 600E	587574.9 5 587599.9 5		0.8 44.5 39			9.9 136 1.79 5.6 107 2.51			11 0.5 11 0.1		56 0.1 0.054 45 0.16 0.044	37 24.1 0.44		0.01 0.09 0.1 0.004 0.03 0.1	0.03 1.5	0.1 0.0		15 7.5	15 1317.3	
RE 27 600E	567599.9		0.5 37.1 10				5.8 0.5 48.1		31 0.1 31 0.1		49 0.14 0.04	14 11.9 0.29		0.004 0.03 0.3		<0.1 <0.0		7.5	48.1	
27 625E			0.4 18.4 10				3.6 0.5 34.7	1.4	8 0,1		31 0.08 0.015	23 12.1 0.39		0.005 0.04 < 1	0.01 1.5			15	34.7	
27 850E	567649.8	5472700	0.3 10.4	20 21 0			1.2 0.4 0.6	0.4	10 0.2	0.1 0.4	19 0.12 0.018	9 4.7 0.05		0.014 0.02 <.1	0.03 0.8			15	0.6	
27 87\$E			0.5 98 20				6.9 1.7 4	4.8	15 0.2		76 0.18 0.039	18 38.1 0.39		0.013 0.08 0.1	0.08 7.5			7.5	4	
27 700E 27 725E	567699.9 5 567724.8 5		0.5 20.7 12 0.3 19.1 12		11 10 5		3.2 0.5 14.1 2.1 0.8 5	3.7 1.5	6 0.1 12 0.1	0.1 0.2	41 0.11 0.021 36 0.19 0.037	15 15.7 0.37		0.005 0.04 0.1	0.01 2.2			15 15	14.1	
27 750E	567749.8		1 18.3 18				3.9 0.8 2.4	1.8	13 0.2		51 0.19 0.044	8 9.9 0.11		0.021 0.03 0.1	0.11 1.9			15	2.4	
27 775E	567774.9		0.9 19 16				3.9 1.1 2.1	3.5	7 0.2	0.1 0.2	31 0.1 0.048	7 9.5 0.07		0.019 0.02 0.2	0.12 2.4	<0.1 <0.0		15	2.1	
27 800E				48 0			6.4 1.8 2.2		23 0.3		71 0.26 0.058	41 32.7 0.38		0.009 0.07 0.1	0.06 3.3	0.1 <0.0		15	2.2	
27 825E			0.5 28.9 18				2.8 1.1 2.7		11 0.1		40 0.11 0.031	20 13.9 0.21		0.016 0.04 0.1	0.08 2.7	0.1 0.0		15	2.7	
27 850E 27 875E	567849.9 5		0.8 23.8 18			110 100 0101	5.4 1 2.5	4.2	7 0.1		43 0.1 0.087 81 0.11 0.029	14 21.1 0.3 11 36.2 0.56		0.009 0.04 0.1	0.12 3.1	0.1 <0.0		15 15	2.5 4.4	
27 875E	567874.9 5 567899.8 5		0.5 38.9 12				4.5 0.9 2.8		8 0.2		40 0.1 0.026	7 14.8 0.16		0.013 0.03 0.1	0.03 3.7	0.1 < 0.0		15	2.8	
27 925E	567924.8 5		0.5 56.3 30				2.4 0.9 2.4		19 0.2		72 0.2 0.028		103 0.096 2 1.95	0.013 0.05 0.1	0.04 4.2			15	2.4	
27 950E	567949.0		0.4 16.1 11	8 63 0	1 8.2	8 148 2.65	4.3 0.8 2	3	9 0.1		42 0.14 0.064		87 0.108 <1 4.41	0.013 0.02 0.1		<0.1 <0.0		15	2	
27 975E	587974.9 5		0.7 29.6 12				2.4 1 2.8	3.2	9 0.2		37 0.11 0.033		47 0.145 1 2.95	0.017 0.03 0.1	0.13 4.8			15	2.6	
27 1000E			0.3 25.1 10				2.8 0.4 1.9		11 0.1		68 0.21 0.016		72 0.076 <1 1.65 122 0.044 <1 3.35	0.008 0.04 < 1 0.009 0.08 0.1	0.01 2.9	0.1 < 0.0		15 15	1.9 6.2	
28 500E 28 525E	567499.9 5 587525,1 5		0.9 61 33			12.8 703 3.57 11.4 303 2.98	4.9 1,7 6.2 3.7 1.4 11.7		14 0.6 15 0.4		73 0.2 0.094 54 0.18 0.048		122 0.044 <1 3.35	0.009 0.06 0.1		0.1 0.1		15 15	5.2 11.7	
28 550E	567550 5					12.7 404 3.18							123 0.06 2 2.56	0.007 0.08 < 1	0.05 4.1			15	4	
28 575E	567574.9 5					4.6 141 3.01					36 0.17 0.049			0.014 0.04 0.1				15	18	

1 3 9 9

28 600E	567599.9	5472802	t 26.	1 26.1	74 0.2	16	8.7 217 3.68	5.1	0.7 2.3	3.1	10 0.4	0.3 0.6	82	2 0.11 0.035	13 21.3 0.41	105 0.131 <1	2.18	0.011 0.06	0.1	0.05	2.4 0.1	0.05	15 0.5	7.5	2.3
28 625E	567625	5472802	1.1 38.				8.9 210 3.71		1.5 4.8	3.6	9 0.3	0.2 0.5			17 20.5 0.3		3.19 2.07	0.008 0.05	0.2	0.15			12 0.7	15	4.8
28 850E 28 675E	587650 567674.9	5472802 5472802	0.7 28.				10.2 170 2.82 4.4 131 2.04	3.3 2.4	0.9 7	4.6	5 0.2 10 0.3	0.1 0.3		B 0.08 0.028 0 0.11 0.025	19 18.7 0.52		2.07	0.005 0.05	0.1 0.†	0.03 0.03			7 <.5 12 <.5	15 7.5	7 3.3
28 700E	587700.t	5472802	0.8 21.	4 15.5	29 0.1	5.3	3.1 70 1.95	4.1	1.4 2.3	3.3	8 0.3	0.1 0.2	28	5 0.09 0.052	11 10.2 0.1	31 0.116 1	3.93	0.018 0.02	0.2	0.12	2.7 0.1	0.06	10 0.8	15	2.3
28 725E 28 750E	567725 567750	5472802 5472802	0.8 31.				26.6 2088 2.95 19.7 1031 3.5	5.5 4.8	1.5 2.9	1.3 2.4	29 0.9 15 0.2	0.2 0.5		8 0.39 0.071 3 0.16 0.037		137 0.039 <1 112 0.072 <1	2.11	0.009 0.05	0.1 0.1	0.09		0.09	7 0.6	7.5 15	2.9
26 750E	567774.9	5472802	0.5 33.				19.7 1031 3.5		0.9 12.3	1.4	13 0.2	0.1 0.5		3 0.16 0.037 3 0.17 0.047	15 20.2 0.43		2.55	0.011 0.07	0.1	0.03		0.05	10 05	15	4.9 12.3
28 800E	567800.1	5472802	0.8 38						1 5	0.5	16 0.4	0.1 0.4		4 0.23 0.065	12 16.3 0.32	87 0.063 <1	1.42	0.015 0.04	0.1	0.04	1.5 0.1	0.05	8 < 5	15	5
28 825E 26 850E	567825 567849.9	5472802 5472802	0.9 38. 0.7 32.				1.5 320 2.27 12.5 689 2.1		1.4 1.8	0.9 1.4	18 0.3 15 0.4	0.1 0.4		2 0.23 0.08	10 19.3 0.2 33 28.2 0.26		2.09	0.023 0.04 0.012 0.05	0.1 0,1	0.08 0.06		0.05 0.05	12 0.6	15 7.5	1.8
28 875E	567874.9	5472802	0.7 48				8.3 183 2.75		2.1 3.3	1.8	17 0.4	0,1 0.6		9 0.18 0.042		125 0.082 <1	2.77	0.012 0.08	0.1	0.05			12 0.5	1.5	5.9 3.3
28 900E	567900	5472802	0.6 33.				5.6 104 2.28		0.9 4.2	1.4	12 0.3	0.2 0.4		5 0.14 0.027	15 16.9 0.27		1.45	0.01 0.03	0.1	0.06			8 <.5	7.5	4.2
28 925E 28 950E	567925 567949 9	5472802 5472802	0.4 68.				4.6 331 3.77 6.2 128 2.45	3.8 3	0.8 2.8	2.4	13 0.1 10 0.2	0.1 0.3		1 0.16 0.035 9 0.12 0.025	17 42.2 0.59		2.71	0.009 0.06	0.1	0.03			10 < 5	15 15	2.8 5.8
28 975E	567975.1	5472802	0.5 33				4.3 133 1.74		0.8 1.3	1.1	13 0.1	0,1 0.3		2 0.12 0.027	9 13.3 0.15		1.18	0.02 0.03	0.1	0.04	2 <0.1		10 <.5	15	1.3
28 1000E	568000	5472802	0.6 5			21.2 1			0.8 1.9	2.9	18 0.1	0.2 0.4				118 0.201 <1	2.85 2.88	0.019 0.05	0.1	0.03	4.3 0.1		14 <.5	7.5	\$.9
RE 28 1000E 1820 100W	568000 564909.3	5472802 5471409	0.5 59.				14.4 379 3.93 7.8 115 3.47	3.7 6.2	D.8 1 0.9 82.7	3.2 8.8	18 0.1 4 0.1	0.1 0.4		1 0.15 0.042 8 0.04 0.091	12 33.8 0.36	116 0.197 <1 54 0.061 <1	2.88	0.02 0.05	0.1 0.2	0.03		0.05	14 <.5 8 <.5	7.5 15	82.7
1820 075W	564906.8	5471432	0.9 14.				3.9 81 2.04	4.5	5.1 14.4	4.8	3 0.1	0.2 0.3			10 10.6 0.21	46 0.067 <1	3.29	0.01 0.04	0.2	0.11	2.9 0.1		8 0.5	7.5	14.4
1820 050W	564902.8	5471458	0.9 1		40 0.1		3.8 99 3.32		0.6 38	6.1	4 <1	0.3 0.5			22 12.9 0.16	34 0.029 <1	1.8 4.9	0.005 0.03	0.1	0.04			10 <.5	7.5	38
1820 025W 1820 000E	564898.8 564886.7	5471483 5471511	0.9 12.		56 0.2 35 0.1		5.9 118 2.52 3.1 73 3	4.8 5.3	1.2 5.7	5.6 8.4	4 0,1 3 <.!	0.2 0.3			10 13.4 0.19 28 12 0.18	47 0.054 <1 36 0.014 1		0.007 0.04 0.04 0.04	0.2 0.1	0.1 0.06	2.8 0.1	*.**	7 0.5 7<.5	7.5 15	5.7 23.9
1820 25E	564877.6	5471532	1.4 8.				4.8 89 3.15		0.7 7.8	4.7	7 0.2	0.2 0.6			19 11.8 0.23	88 0.032 <1	1.63	0.006 0.08	0.2	0.06	1.4 0.1		8 < 5	7.5	7.8
1820 50E	564873	5471552	1.7 20.				23.3 1757 2.89	5.4	2.7 197	2.7	14 0.3	0.2 0.7			23 14.1 0.57	150 0.021 <1	1.98	0.008 0.09	0.1	0.03	1.7 0.1		6 <.5	7.5	197.3
1820 75E 1820 100E	564879.1 564891.4		1.2 17.				7.5 224 2.65 7.1 158 3.13	5.6 7.9	0.9 78.9	8.8 6.8	4 0.1 5 0.1	0.2 0.6			21 12.7 0.33 18 14 0.24	66 0.047 <1 57 0.05 <1	1.85	0.009 0.05	0.2	0.05	1.9 0.1		6<.5 7 06	15 7.5	76.9 14.1
1820 125E		5471618	0.5 10.		36 0.1		4.9 88 1.9		0.5 3.3	5.7	5 0,1	0.2 0.5			25 9.3 0.2		1.09	0.004 0.04	0.1	0.03	1.1 0.1	0.05	5 < 5	15	3.3
1820 150E	564928.3		0.8 10.				4.5 77 2.67	5	0.5 28.1	3.8	4 0.1	0.2 0.4			19 9 0.2	33 0.028 1	1.05	0.005 0.03	0.1	0.03	0.9 0.1		8 <.5	15	28.1
1820 175E 1820 200E		5471860 5471879	1.3 36.				8.1 217 2.92 3.5 70 2.45		4.8 3.3	4.9 3,4	11 0.2	0.2 0.8			31 15.3 0.3	127 0.037 <1 52 0.053 <1	2.31	0.01 0.09	0.1 0.2	0.05	2.8 0.1	0.05 <.05	9 0.7 9<5	7.5 15	3.3 3.8
1820 225E		5471690	0.6 15				7.1 289 2.02		1.5 1.1	2.3	7 0.2	0.1 0.4		3 0.05 0.053	31 9.2 0.35	53 0.01 <1	1.01	0.004 D.05	0.1	0.03	0.8 <.1	<.05	3 < 5	7.5	1.1
1820 250E	564978.1		0.5 17.				9.2 223 2.12	. 4	0.9 2	8	3 0.1	0.1 0.4		0.02 0.039	28 10.3 0.49	35 0.008 <1	1.19	0.003 0.06	0.1	0.03	0.9 <.1	<.05	3 <.5	15	2
1820 275E 1820 300E	565002.8 565023.8	5471668 5471644	1.3 17.				8.1 415 2.24 7.3 186 2.35		1.3 1	3.5 5.7	B 0.2 5 0.2	0.1 0.4			28 12.5 0.42 25 10.5 0.35	78 0.026 <1 65 0.03 <1	1.87 1.63	0.008 0.07	0.2	0.04 0.05		0.07	8 <0.5 7 <0.5	15 15	1.5
1820 325E	585039.5		0.9 24				4.5 853 2.18		2.9 1.8	2	16 0.3	0.1 0.5		9 0.15 0.05	31 13.8 0.48	78 0.01 <1	1.75	0.007 0.08	0.1	0.02		<0.05	6 < 0.5	15	1.6
1820 350E	585053.4		0.6 11.				5.5 168 2.43		0.8 5.9	4.3	6 0.1	0.2 0.4	_		24 12.8 0.32	75 0.018 <1	1.48	0.007 0.08	0.2	0.03		<0.05	7 < 0.5	15	5.9
1820 375E 1820 400E		5471582 5471558	0.6 21.			14.8 1 10	12.6 853 2.31 8.2 352 2	3.4 2.6	2 2.7	4 3.4	14 0.2	0.1 0.5			32 14 0.45 28 11 0.32	85 0.015 <1 60 0.016 <1	1.81 1.53	0.008 0.08	0.1	0.02		<0.05	7 <0.5 6 <0.5	15 7.5	2.7
1820 425E	565102.3	5471532	0.4 5.	7 7	31 0.1	5.7	3.3 109 1.67	2.2	0.5 0.8	2.7	8 0.1	0.1 0.3	21	0.08 0 023	23 8.6 0,18	75 0.018 <1	1.02	0.008 0.04	0,1	0.02	1 0.1	<0.05	6 <0.5	15	0.8
1820 450E		5471513	0.8 10				5.9 297 2.01	1.8	0.8 <.5	3.3	5 0.1	0.1 0.4			16 11 0.14	78 0.046 <1	1.74 3.18	0.01 0.04	0.1 0.2	0.05		<0.05	\$<0.5 8<0.5	.↓ 15 45	<,5
1820 475E 1820 500E	565138.9 565158.2	5471498 5471478	0.6 13. 0.5 11.				7.3 211 2.28 8.8 127 1.84	3.7 2.2	1.1 2.3	7.1 5.3	4 0.1	0.1 0.3			12 11.5 0.22 28 10.8 0.21	76 0.073 <1 70 0.021 <1	3.18	0.01 0.04	0.2	0.08		<0.05 <0.05	o≪0.5 5≪0.5	15 15	2.3 <.5
1820 525E	565178.1	5471455	0.4 12.3		45 0.1	17.1	8.7 171 2.04	2.7	1.2 1.9	5.4	6 0,1	0.1 0.3			28 11.8 0.45	57 0.013 <1	1.23	0.003 0.05	6.1	0.01	1.8 <0.1	<0.05	4 <0.5	15	1.9
1820 550E 1820 575E	565195.3 565215.4	5471438 5471422	0.6 10.		49 0.1		10.7 162 2.13 22.1 237 2.64	2.8 5.1	0.9 1.2	6.1 9.1	4 0,1 10 0,1	0.1 0.3			21 11.9 0.3	91 0.036 11	2.24	0.006 0.07 0.007 0.08	0.1 0.1	0.04		<0.05 <0.05	\$<0.5 \$<0.5	15 15	1.2 1.5
1820 600E	565235.3	5471404	0.6 25.		44 0,1		5.9 214 2.51	8.1	2.7 5.8	6.4	10 0.1	0.1 0.5			31 22.2 0.55	118 0.023 <1	2.2	0.006 0.05	0.1	0.03		<0.05	7 <0.5	7.5	5.8
1820 625E	565262 1	5471387	0.6 9.		39 <.1		8.3 124 1.92	3.4	0.7 4	6.2	3 0.1	0.2 0.3			24 9.3 0.34	59 0.016 1		0.004 0.04	0.1	0.02		<0.05	5<0.5 6<0.5	7.5	4
1820 650E RE 1820 650E	565283.1 565283.1	5471373 5471373	0.7 29.				26.2 367 2.76 26.1 361 2.81	5.9 5.8	2 2.1	9.7 9.5	8 0.1 6 <.í	0.1 0.4			27 20.2 0.58 29 17.4 0.68	131 0.011 <1	2.55	0.005 0.11	0.1 0.1	0.03		<0.05 <0.05	6 < 0,5 7 < 0.5	7.5 7.5	2.1 1.4
1820 675E	565301.4	5471382	0.3 12.	6.2	42 < 1	13.3	7.6 174 1.74	2.5	0.9 1.1	6.4	5 <.1	0.1 0.2	12	2 0.04 0.02	28 12.9 0.46	43 0.006 <1	1.2	0.003 0.05	0.1	D.01	1.2 <0.1	<0.05	3 <0.5	15	1.1
1620 700E 1820 725E	565325.9 565346.5	5471347 5471338	0.5 28.				18.4 273 2.29 17.1 231 2.05	3.7 3.6	1.1 0.9	5.3 5	10 0.1 7 0.1	0.1 0.4			23 21.8 0.43 24 18.8 0.43	103 0.019 1 79 0.018 <1	1.96	0.01 0.09	0.1 0.1	0.03 0.01		<0.05 <0.05	8 < 0.5 5 < 0.5	7.5 15	0.9 0.8
1820 750E	565369.2	5471330	0.8 23		57 0.1			5.2	1.3 1.1	8.4	8 <.1	0.1 0.4			24 18.7 0.54	144 0.03 <1	2.77	0.007 0.1	0.1	0.02		<0.05	\$ <0.5	15	1.1
1880 000E	564889.7	5471751	0.7	8 14.3	35 0,1	7,8	3.7 101 2.49	3	0.8 22.1	4.1	5 0.2	0.1 0.4			23 10.8 0.24	80 0.025 <1	1.28	0.005 0.08	0.1	0.03			7 <0.5	7.5	22.1
1880 025E 1880 050E	564900.2 564912.9	5471772 5471791	0.9 1				4.1 143 2.87 8.3 187 2.04	3.9 2.5	0.5 0.8	4.2 4.2	5 0.2 8 0.1	0.2 0.5			21 11 0.22 29 12.3 0.37	61 0.034 1 81 0.026 1	1.24	0.007 0.05	0.1	0.04			8 <0.5 7 <0.5	7.5	0.8
1880 075E	564929.6	5471794	0.6 5.		32 0.1		3.7 109 2.01	2.4	0.6 0.6	3.9	3 0.1	0.1 0.4			20 10.2 0.23		1.15	0.004 0.05	0.1	0.03		<0.05	8 <0.5	7.5	0.6
1880 100E	564954	5471787	0.5 11.		48 0.1		6.5 164 1.97	2.8	1.3 1.1	6.8	5 0.1	0.1 0.3			24 11.3 0.36	53 0.025 <1	1.45	0.004 0.08	0,1	0.03		+·	5 <0.5 4 <0.5	15	1.1
1880 125E 1880 150E	564978.1 565001.1	5471777 5471782	0.5 8.1		34 <.1 38 <.1		7.5 176 1.24 4.9 127 2.07	1.4	1.1 1.9	1.8 8.5	13 0.1 4 < 1	0.1 0.3			31 9.6 0.25 26 9.5 0.33	88 0.011 <1 28 0.011 1		0.004 0.08	0.1	0.02 0.03		<0.05 <0.05	< <0.5 2 <0.5	7.5 7.5	1.9 16.3
1880 175E	565022.3	5471747	1.2 14.	• • •			9.2 248 2.58	4.5	1.8 7.2	6.3	6 0.3	0.2 0.4		0.04 0.049	27 12 0.34	61 0.028 <1	2.09	0.004 0.05	0.2	50.0	1.8 0.1	<0.05	8 < 0.5	15	7.2
1880 200E	565042.9	5471733	0.7 11.				8.4 525 2	2.9	0.8 0.8	8.5	3 0.1	0.1 0.4			25 10.5 0.32	84 0.015 <1 72 0.019 <1	1.57	0.003 0.05	0.1	0.05		<0.05 <0.05	5 <0.5 6 <0.5	7.5 15	0.6 1.2
1880 225E 1880 250E	585060.7 585075	5471718 5471697	0.5 9.		55 0.1 68 0.2		7.4 192 2.13 8.4 178 2.35	3.2 4.2	0.7 1.2	7.5 7.3	3 0.1 4 0.1	0.1 0.3			22 9.4 0.35 22 12.5 0.32	61 0.023 <1	2.08	0.004 0.05	0.1	0.04			6 <0.5 6 <0.5	15 7.5	0.7
1880 275E	565088	5471879	0.8 11.	7 12.2	53 0.1	12.6	6.1 145 2.35	4	0.9 1.2	8	5 0.1	0.1 0.4			24 10.5 0.4	55 0.022 1		0.005 0.06	0.1	0.04	1.5 0.1	<0.05	6 <0.5	15	1.2
1880 300E 1880 325E	565102.3 565115	5471657 5471839	0.6 10.3		42 0.1		5.6 114 2.43 7.6 221 2.41	3.8	0.8 6.2	7.2 4.4	3 0.1 9 0 2	0.1 0.4			20 12.4 0.31	51 0.02 <1 62 0.02 1	1.86	0.004 0.05	0.1	0.05		<0.05 <0.05	6 <0.5 7 <0.5	15 7.5	6.2 2.1
1880 325E	565128.8	5471639	0.5 17.	· ·•	49 0.1		2,8 444 2.33	3	1.2 1.7	4.4 3.4	11 0.1	0.1 0.4			24 12.2 0.41	70 0.017 <1	1.86	0.005 0.06	0.1	0.02		<0.05	6 < 0.5	7.5	1.7
1880 375E	565144.1	5471593	0.7 11	14.8	51 0.2	10.5	8.2 154 2.84	3.7	0.7 0.7	4.8	4 0.1	0.1 0.4	_		20 12.9 0.33	62 0.026 <1	1.78	0.008 0.04	0.1	0.05		<0.05	7 <0.5	15	0.7
1880 400E 1880 425E	585158.5 585187.1	5471577 5471537	0.7 18.		48 0.1		3.2 841 2.75 7.7 174 2.31	3.8 4.1	1.3 0.7	4.6 7.5	9 0.1 3 < 1	0.1 0.4			24 14.3 0,48 20 10.9 0.35	86 0.01 1 78 0.015 <1	1,8 1,9	0.005 0.07 0.004 0.05	0.1 0.1	0.02 0.06		<0.05 <0.05	8 <0.5 5 <0.5	7.5 15	0.7
1880 450E	565198.6	5471522	0.4 5.				3.5 137 1.58	1.4	0.5 9.9	4.4	3 < 1	0.1 0.3		0.02 0 022	20 8.5 0.2	85 0.021 <1	1.15	0.005 0.04	0.1	0.03			5 < 0.5	15	9.9
1880 475E	565218.8	5471508	0.8 9.	5 9.1	40 0.1	9.8	7.5 176 2.05	2.5	0.7 t.8	4.3	4 0.1	0.1 0.3	26	0.03 0.055	18 9.6 0.2	83 0.049 <1	2.03	0.009 0.04	0.1	0.08	2 0.1	<0.05	7 <0.5	7.5	1.6

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RE 1880 475E	565218.8	5471506	0.6 8.9	9.7	••		164 1.98		0.7 2.3	4.4	4 0,1	0,1 0.3	25	0.03 0.054	17 10 0.21	80 0.048 <1 2.			0.1 0.08			7 < 0.5	7.5	2.3
1880 500E	585239.4	5471492	0.5 10.1	11.3		14.2 12.2	145 2.49		0.9 0.8	4.8	9 0.1	0.2 0.4	34	0.12 0.024	21 12.3 0.22	85 0.036 <1 1.			0.1 0.02		****	8 < 0.5	15	6.0
1880 525E	565263	5471478	0.4 15.1	12.8		19.9 18.1	139 2.42		0.9 3.1	4.2	7 0.1	0.1 0.4	32	0.08 0.025	18 12.9 0.32	90 0.025 <1 1.			0.1 0.02			6 < 0.5	7.5	3.1
1880 550E 1880 575E	565287.3 585310.7	5471468 5471462	0.7 10.2	10.1 9.5		11.5 18.4 14.8 20.5	125 2.45 164 2.08		0.9 2.1 1.3 2.2	6.9 6.7	3 < 1	0.1 0.3	28 27	0.02 0.08	13 12 0.23 11 10.6 0.21	77 0.042 <1 2. 71 0.056 1 3.			0.1 0.04	2 0.1		6 <0.5 7 <0.5	15 15	2.1
1580 600E	565335	5471460	1 11.6			15.3 22.6	867 2.56		0.8 2.5	5.5	4 D.1	0.2 0.4	33	0.03 0.064	11 14.6 0.24	76 0.077 1 3.			0.2 0.05			8 < 0.5	15	2.2
L1890 0SE	567443.8	5473385	0.5 16.4	19	31 0.2	8.1 3.5	191 1.32		0.5 1.4		10 0.1	0.1 0.5	25	0.1 0.022	10 7.9 0.25	79 0.138 2 1.			0.1 0.03	1.4 0.1		1 0.5	1.2	1.4
11890 25SE	567466.8	5473373	0.2 15.2		17 0.1	4.3 2.7	172 0.7		0.7 14.9	0.5	8 0.2	0.1 0.2	10	0.06 0.021	21 5.3 0.2	50 0.017 1 0.			1 D.03			3<5		14.9
L1690 75SE	567508.6	5473345	0.4 11	11.8	27 0.1	6.5 5.6	670 1.49	2.5	0.5 6.4	1.3	6 0.2	0.2 0.4	24	0.05 0.038	13 8.4 0.21	61 0.036 1 0.			0.1 0.05			5 < 5		6.4
1.1690 100SE	567529.2	5473330	0.7 16.8	10.4	33 0.1	8.5 7	235 1.35	1.8	0.6 4.3	0.8	11 0.2	0.1 0.3	22	0.15 0.027	20 10.1 0.39	57 0.029 <1 1.	26 0.0	8 0.03	0.1 0.03	1.4 0.1	<.05	6 < 5		4.3
L1690 125SE	567550.1	5473315	1.1 49.5	55			413 1.58		2.8 4.7		30 1.4	0.4 0.4	24	0.33 0,134	36 37.2 0.23	122 0.019 1 2			0.1 0.14	2.1 0.1	0.14	5 1.5		4.7
11890 150SE	567575.3	5473301	0.3 7.4	11.1		3.9 2.2	97 1.13		0.3 10.7	1.3	8 0.1	0.1 0.3	28	0.07 0.018	15 8.4 0.16	48 0.067 <1 0.1			0.1 0.03	1.1 <.1		7 <.5		10.7
L1690 175SE	567596.6	5473288	0.2 6.7	8.5	15 0.1		291 0.45		0.4 10.3	0.9		.1 0.3	9	0.05 0.015	22 5.4 0.14	45 0.022 <1 0.				0.7 <.1		4 <.5		10.3
L1690 200SE L1690 225SE	587816.2 587635.3	5473273 5473256	0.9 45	29.2 21.9	25 0.2 21 0.1		312 1.78 270 1.33	3 2.3	1 1.8 0.9 <.5		12 0.3 13 0.2	0.1 0.5	34 22	0.09 0.032	16 10.0 0.24	70 0.118 <1 1. 61 0.081 <1 1.			0.2 D.05			:0<.5 0<.5		1.8 < 5
L1690 2255E	567650.3	5473238	0.5 23.4	14.4			215 1.68		0.8 1.5	1.6	8 0.2	0.1 0.3	30	0.07 0.023	24 12.9 0.5	57 0.044 <1 1/			0.1 0.04			u <.5 6 <.5		10.4
L1690 275SE	587684.2		0.7 31.9	19.8	25 0.2	7.3 4	99 1.53		0.7 1.2	3	6 0.2	0.1 0.3	25	0.05 0.027	20 9.9 0.29	57 0.05 <1 1.			0.1 0.03			7<.5		1.2
L1690 300SE	567679.2	5473197	0.8 19.7	12.9		8.7 5.6	133 3		0.9 111	- Ă	5 0.2	0.2 0.3		0.07 0.06	13 14.3 0.32	50 0.058 <1 3.1			0.1 0.12	25 01		0 < 5		110.7
L1690 325SE	567697.1	5473179	1 67.6	31.4	55 0.2		1295 3.11		1.8 3.4	2.7	15 0.3	0.3 0.5	58	0.15 0.081	26 20.8 0.55	185 0.045 1 3.			0.1 0.05	3.8 0.1	<.05	9 < 5		3.4
L1690 350SE	567718.4	5473163	0.3 12.2	16.4	22 0.1	5 2.9	101 1.14	1.7	0.4 32.7	1.8	15 0,1	0.1 6.3	28	0.18 0.017	17 6.6 0.2	82 0.083 <1 0.1	71 0.0	3 0.03	0.1 0.01	1.1 0.1	<.05	7 <.5		32.7
L1690 375SE	567734.6	5473147	0.6 11.3	11.8		7.6 4.1	95 2.94	· · · ·	0.4 2.6	3.4	6 0.1	0.2 0.3	78	0.1 0.042	20 11.8 0.31	47 0.052 <1 1.			0.1 0.03			8 <.5		2.8
L1690 400SE	567750.6	5473128	0.6 10.3	18		5.3 2.8	97 1.87	-	0.6 2.3		10 0.1	0.2 0.3		0.13 0.045	16 89 0.21	\$0 0.094 <1 1.1			0.1 0.04			1 < 5		2.3
RE 11690 400SE L1690 425SE	567750.6 567763.2	5473128 5473106	0.6 10.9	14.9 5	30 0.2 15 5.1	5 2.8	100 1.83 52 0.72		0.5 3.8 0.3 2.3	2.7 1.2	9 0.1 10 0.1	0.1 0.3		0.12 0.042	13 8.1 0.18	57 0.087 <1 1.4 40 0.025 <1 0.4		1 0.04	0.1 0.05	1.6 0.1 0.9 < 1		2 < 5 3 < 5		3.8 2.3
L1690 450SE	567776.7	5473087	0.4 14.7	9.2			174 1.81		0.3 2.3	2.6	8 0.1	0.1 0.2		0.11 0.027	23 9.6 0.34	52 0.03 1 1.0			0.1 0.01	•··• ···		5<.5		18.4
L1690 475SE	567790.2	5473067	0.8 59.5			15.5 35.3			1.3 1.5		25 0.4	0.2 0.5	55	0.3 0.079	26 17.8 0.38	119 0.079 4 2.1			0.1 0.09			2 0.6		1.5
L1890 500SE	567804.4	5473048	0.6 12.3	25	23 0.1	4 3.5	87 0.92		0.5 1.5		11 0.1	0.1 0.4	23	0.12 0.018	11 5.5 0.12	68 0.107 <1 0.			0.1 0.02	1.1 0.1		9 <.S		1.5
L1890 525SE	567817.6	5473024	0.4 16.7	8.5	40 < 1		226 2.33		0.5 4.7	4.7	3 0.1	0,1 0,3	45	0.07 0.025	20 13.8 0.54	38 0.033 1 1	.1 0.00	5 0.04	0.1 0.02	1.9 < 1	<.05	5 <.5		4.7
L1690 550SE	567832	5473004	0.2 4	8			128 0.19		0.1 <.5	0.3	6 0.1	0.1 0.3	8	0.06 0.012	9 2.5 0.03	44 0.053 <1 0.				0.5 < 1		4 <.5		<.5
1690 575SE	567848 567865.2	5472984 5472966	0.7 105	36.5 31.5	28 0.4 40 0.4		189 1.75 853 1.33	3.1 3.3	2.7 3.4		11 0.4 28 0.5	0.1 0.3		0.12 0.058	30 11 0.2 33 11 4 0 33	60 0.064 3 2.5 122 0.05 <1 1.5			0.1 0.12	3.1 0.1		0 0 6		3.4
L1690 600SE	567884.3	5472950	12 243	31.5	40 U.4 85 01		653 1,33 3455 2,67		1 1.5		26 0.5 12 0.6	0.2 0.3		0.17 0.058	25 10.0 0.32	122 0.05 <1 1.1			0.1 0.08	1.7 0.1		7<.5 505		1.5
11690 650SE	587902.7	5472933	0.7 39.1	27.7	50 0.2		871 2.28		1.2 17.8		20 0.8	0.3 0.5		0.15 0.048	48 15.4 0.38	183 0.066 <1 1.1			0.1 0.12	4 0.1	0.07 1			17.8
L1860 0S	589646.8	5478138	1.1 9.3	10.6	22 < 1	6.2 2.5	54 4.2		0.6 1.6	6	3 0,1	0.3 0.4		0.03 0.052	13 15.7 D.24	18 0.073 1 1.1			0.2 0.04	1.3 0.1				1.8
L1880 255	569671.2	5476130	0.9 5.7	6	14 0.1	5.4 2.5	44 1.74	3.4	0.5 <.5	4.2	4 0.1	0.1 0.3	19	0.04 0.027	22 7.7 0.24	28 0.024 <1 1.1	0.00	4 0.02	0.1 0.04	0.8 0.1	<.05	6 <.5		<.5
11860 50S	589898.5	5476126	0.9 3.7	3.6	13 <.1	4.9 2.1	54 1,18		0.5 2.3	4.7	3 <1	0.2 0.3		0.04 0.025	28 5.3 0.28	24 0.013 <1 0.0			0.1 0.01			4 <.5		2.3
L1880 75S	588721.2	5476119	1.2 8.3	6.2		10.5 3.8	57 3.38		0.6 1.6	7.4	2 0.1	0.2 0.3		0.02 0.054	26 18.3 0.57	27 0.018 2 1.1			0.1 0.04			6 <.5		1.8
L1860 100S	589747 589770	5476110 5476105	0.7 6.1	5.8 9.6	23 0.1 39 0.2	7.1 2.4	54 2.17 253 2.47		0.5 1.7	5	1 0.1	0.1 0.2		0.01 0.028	20 11 2 0.43	17 0.022 <1 1			0.1 0.03			5 0.5 7 0.5		1.7
L1860 125S L1860 150S	569798.1	5476105	1 7.2	9.0	39 U.2	9.5 6.8 4.3 1.9	47 1.77		0.8 1.6 0.4 1	8.1 5.1	4 0.2 3 0.1	0.2 0.3		0.05 0.058	17 16.1 0.44 27 8.6 0.22	48 0.043 1 2.4 21 0.034 <1 0.8			0.1 0.09			7 0,5 8<.5		1.8
L1860 175S	569822.8	5476099	1.3 3.6	6.6	21 < 1	5.8 2.9	79 2.83		0.4 1.9	5.1	3 0.1	0.2 0.4		0.02 0.035	25 12.1 0.33	24 0.048 6 1.0			0.2 0.02	••••		0<5		1.9
L1860 200S	569848.4	5+76100	0.8 8.1	8.2	24 <.1	7.2 4.6	49 2.43		0.5 3.2	4.5	3 0.1	0.2 0.3	37	0.02 0.049	19 14.4 0.41	38 0.04 <1 2.1			0.1 0.1	1.7 0.1		7 <.5		3.2
L1860 225S	569872.5	5478104	0.6 2.3	3.9	8 <.1	4.1 1.8	29 1.5		0.3 1.3	3.9	2 <.1	0.1 0.2	25	0.01 0.024	25 8.3 0.29	17 0.017 <1 0.9			0.1 0.04	1 <.1		8 <.5		1.3
L1860 250S	569893.8	5478109	1.2 5.3	10.3	20 < 1	8.5 3.8	47 2.83		0.6 3.5	56	3 0.1	0.3 0.4	42	0.02 0.044	20 12.8 0.47	30 0.085 <1 1.1			0.2 0.04	1,4 0.1		" <.5		3.5
L1860 275S	569916.5	5476104	0.8 8.2	8.5	18 0.1	4.6 2.7	50 1.73		0.9 1.7	3.6	4 0.1	0.2 0.3	33	0.03 0.065	7 7.7 0.16	32 0.1 2 2.1			0.1 0.07	1.6 < 1		9 <.5 7		1.7
L1860 300S L1860 325S	589930.7 589954.9	5476088 5476075	1.2 10	8.3 11.4	24 D.1 25 0.2	9.5 5.5 7.9 7	64 1.9 60 2	5 4.9	1 3 1.2 2.8	4.9 4.4	4 0.1 5 0.1	0.1 0.2	26 33	0.04 0.085	13 10 0.42 8 8.9 0.23	39 0.059 1 3.0 52 0.098 2 3.5			0.1 0.08	2 <.1 2.8 0.1		7<.5 90.6		3 2.6
L1860 350S	569977.6	5478087	0.8 11.3	10.3	28 < 1	7.9 5.2	129 2.17	6	1 2.7	4.1	5 0.1	0.2 0.3		0.04 0.141	4 9.8 0.11	37 0.124 <1 5.1			0.2 0.09	2.4 < 1	0.06 1			2.7
L1880 375S	569991.5	5476049	1.4 7.1	12.9	30 0.1		251 2.26	5.6	0.7 15.4	4.5	8 0.1	0.3 0.3	38	0.05 0.089	8 10.7 0.18	58 0.067 1 3.0	0.00		0.2 0.08	1.5 D.1		9 <.5		15.4
L1860 400S	559998.9	5476020	1.3 6.7	12.8			187 2.28	6.7	0.8 2.3	5.2	6 0.1	0.2 0.4		0.03 0.057	14 11.5 0.37	83 0.054 <1 2.4			0.1 0.04	1.8 0.1		B <.5		2.3
L1860 425S	569997.5	5475993	1.5 7.3	19.1			185 2.48	6.9	1 2.1	7.4	5 <.)	0.2 0.4		0.03 0.044	19 12.2 0.65	67 0.048 <1 2.4			0.1 0.04	2 0.1		7 <.5		2.1
11860 450S 11860 475S	569992.9 569988,1	5475960 5475945	0.9 8.3	13.5 15.8	•••••	10.4 9.6	108 2.28 520 2.68		0.6 2.5 1.2 2.4	4.5	7 0.1 5 0.1	0.2 0.3		0.06 0.057	10 10.2 0.28 20 13.2 0.83	74 0.067 1 2.3 64 0.046 1 1.8			0.1 0.07	1.3 0.1 1.5 0.1		9<5 8<5		2.5 2.4
L1860 500S	589973.9	5475918	1.6 84	15.0			210 3.31	-	0.9 2.3	7.8	5 0.1	0.3 0.4		0.05 0.037	19 17.5 0.68	95 0.061 <1 2.6			0.2 0.03	1.5 0.1		0 < 5 0 < 5		2.4
RE 11880 500S	569973.9	5475918	1.6 6.4	15.4			197 3.2		0.9 1.7	7.7	6 0.1	0.2 0.4		0.05 0.041	18 16 2 0.68	97 0.061 3 2.1			0.1 0.05	1.7 0.1		0 < .5		1.7
L1860 525S	569962.5	5475898	1.5 6.8	17.8	40 0.1		217 2.87	9.6	0.8 2.2	6.3	6 0.1	0.3 0.4		0.06 0.04	17 14 0.58	67 0.062 <1 2.3			0.1 0.04	1.7 0.1	<.05	9 < .5		2.2
L1860 550S	559947.2	5475873	1.4 8.1	\$50.4			214 2.95		1.6 75.5	8.9	5 0.1	0.2 0.4		0.03 0.038	19 15.4 0.66	50 0.057 <1 2.1			0.1 0.04	1.7 0.1		7 <.5		75.5
L1860 575S	589933.6	5475850	2.1 5.7	16.8			147 3.42		0.7 2.6	7.7	4 0.1	0.3 0.5		0.03 0.033	20 19.6 0.7	62 0.05 <1 2.6			0.1 0.04	2.1 0.1		1 < 5		2.8
L1860 600S L1860 625S	569916.5 569896.4	5475827 5475803	1.7 4.8	28.5 148.1			278 2.95		0.5 8 1.7 13.2	5.8	7 0.1	0.3 0.5		0.05 0.03	21 16.9 0.85 26 18.4 0.88	76 0.037 <1 1.8 58 0.02 <1 2.1			0.1 0.04	1.8 0.1 2.3 0.1		9 0.5 6 0.5		8 13.2
L1860 650S	569881.3	5475789	2.1 45.7				386 2.85		2.2 12.7	95	4 03	0.2 0.6		0.03 0.035	22 18.8 0.74	54 0.048 <1 2.4			0.1 0.04	2.3 0.1		6 U.D 8 <.5		12.7
£1860 675S	569659.7	5475774	1.5 12.5			2,4 8.8	166 2.56		0.8 61.3	6.1	4 0.4	1.5 0.4		0.03 0.047	14 13.2 0.47	68 0.06 4 3.2			0.8 0.07	1.9 0.1		7<.5		61.3
L1860 700S	569839	5475759	1 7.5	49.8	110 0.5		260 2.09		0.4 6.3	4	5 0.8	0.2 0.4	30	0.05 0.048	14 11 0.3	72 0.058 3 2.2			0.3 0.04	1.3 0.1	< 05	8 < 5		8.3
L1860 725S	569516.6	5475740	1.3 8.8	32.4	66 0.1		127 2.24	4.2	0.9 7	5.7	5 0.2	0.3 0.3		0.04 0.058	12 11.5 0.32	54 0.072 <1 2.8			0.5 0.07	2 0.1		8 <.5		7
L1860 750S	569795	5475722	1.1 22.5	12.3		12.7 10	181 2.35		0.5 20.7	5.2	8 0.3	0.3 0.3		0.07 0.041	17 10.9 0.55	48 0.047 <1 1.7			0.1 0.03	2 0.1		7 0.5		20.7
L1860 775S	569777.4	5475709	1.4 9.6	21.1			260 2.48	4.7	1 8,3	6.8	7 0.3	0.4 0.4		0.07 0.04	18 12.7 0.52	81 0.053 3 2			0.2 0.06	1.5 0.1		7 < 5		8.3
L1860 800S	569750.7 569727.1	5475890 5475874	1 7				144 2.22		0.7 8.6 0.7 0.9	5.5 4.2	7 0.3	0.5 0.3		0.06 0.048	16 11.7 0.42 7 10.1 0.25	82 0.053 <1 2.5 44 0.103 <1 3.8			0.2 0.05	1.4 0.1		7 < 5 9 < 5		8.6 0.9
11860 825S 11860 850S	569727.1	5475681	1.1 55	10.7 9.7			444 2.39		07 0.9 0.6 1.7	4.2	8 0.2	0.2 0.3		0.08 0.087	7 10.1 0.25	44 0.103 <1 3.0 74 3.047 <1 1.8			0.2 0.05	2 D.1 1.3 0.1		9<5 7 0,6		0.9
L1860 875S	569685.4	5475844	0.9 11.4	9.2	40 4.1		539 2.15	4.4	0.5 1.7	47	5 0.1	0.2 0.4		0.06 0.031	18 11.5 0.38	57 0.044 1 1.5			0.1 0.03	1.4 0.1		7 0.7		1
1.1860 900S	569659.6	5475623	1.3 5.2	29.2			111 2.48		0.5 1.8	5.1	4 0.1	0.6 0.5		0.04 0.024	20 11.1 0.32	54 0.034 <1 1.6			0.1 0.01	1.3 0.1		7 < 5		1.8
L1860 925S	569634.9	5475606	0.7 7.4	58.2	41 D.1	10 9.5	178 1.59	4.8	1 1	5.7	4 0.1	0.5 0.3		0.02 0.022	25 8.4 0.39	32 0.014 <1 1.0	6 0.00	2 0.03	0.1 0.02			4 < 5		1
L1860 950S	569613.3	5475592	1.4 8.1	17.2	40 0.3		141 1.9		0.7 2.9	5.9	6 0.1	0.2 0.3		0.04 0.027	18 10.4 0.29	74 0.041 <1 2.0			0.1 0.05	1.3 0.1		8 < 5		2.9
L1860 975S	569588.3	5475579	1.2 7.2	92	29 <.1	0.9 8.4	161 1.84	3.6	0.6 1.4	5.3	6 0.1	0.2 0.3	22	0.05 0.027	16 8.9 0.25	81 0.041 <1 2.2	1 0.00	6 0.05	0.1 0.03	1.3 0.1	<.05 (6 0.5		1.4

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L1860 1000S	569562.5	5475567	0.9 12.9	12.7	30 < 1 1	14.9 17.1 1					5 0.1	0.2 0.3			15 11.2 0.32	89 0.071 <1 2.87	80.0 800.0		0,04 1.8	0.1 0.11	8<5 8<5		1 3.3
L1860 1025S	569535.5	5475555	0.7 12.5	9.9				3.3 0.4		-	8 0.1	0.2 0.3			13 10.3 0.25 19 10.4 0.37	100 0.09 <1 3 67 0.04 <1 2.24	0.011 0.07		0.03 1.8 0.03 1.3	0.1 0.08	o <.5 7 < 5		2.4
L1550 1050S		5475544	9 0.1	10.1				3.9 0.8 3.4 0.4			6<.1 4 0.1	0.2 0.3 0.2 0.4		04 0.031 03 0.019	19 10.3 0.28	75 0.032 <1 1.54	0.004 0.05		0.03 1	0.1 <.05	7 < 5		55
L1860 1075S L1860 1100S	569482.1 569451.7	5475533 5475523	0.9 6.2	11.8				3.2 0.7		-	0 0.1	0.2 0.3		.1 0.075	P 9.3 0.18	91 0.075 3 2.89	0.01 0.08	0.2	0.04 1.4	0.1 0.07	8 <.5		0.6
L1660 1125S		5475517	8 84	10.4				2.5 0.6			6 0.1	0.2 0.3		03 0.04	14 9.4 0.25	66 0.046 1 1.7	0.007 0.04	÷	0.04 1.2		7 < 5		0.7
L1660 1150S		5475513	1.2 9.6	16.7				6.6 0.6			6 0.1	0.3 0.4		04 0.08	10 12.8 0.23	71 0.076 <1 2.97	0.01 0.06		0.06 1.5 0.07 1.4	0.1 <.05 0.1 <.05	10 <.5 11 <.5		<.5 < 5
L1660 1175S	589383.0	5475508	1.3 8.8	14.5					3<.5 30.6		6 0.1 5 0.1	0.3 0.4		05 D.069 04 D.08	8 10.2 0.13 7 10.6 0.18	64 0.091 <1 3.11 48 0.095 <1 2.78	0.011 0.05		0.07 1.4 0.04 1.3	0.1 <.05	10 < 5		0.6
L1860 1200S L1860 1225S	589359.4 589338 7	5475500 5475492	1.3 7.8	14.5 20.1				5.4 0.0 4.8 0.0			B 0.1	0.4 0.4		05 0.069	12 12.2 0.27	98 0.088 <1 3.15	0.01 0.05		0.04 1.9	0.1 <.05	9 < 5		0.8
L1860 12255	569318.3	5475484	1 8.6	12.5					I <.5		8 0.1	0.2 0.4		06 0.026	14 8.8 0.15	51 0.045 <1 1.08	0.008 0.06		0.02 1	0.1 <.05	7 <.5		<.5
L1880 1275S	569298.1	5475475	0.4 5	9.3				2.4 0.5	5 1.9		5 0.1	0.1 0.4			20 7 0.13	48 0.027 1 0.96	0.004 0.05		0.02 1.1	0.1 <.05	6 <.5		1.9
11860 1300S	559273.7	5475458	1 10.9	24.4				••••	2 <.5		29 0.1	0.2 0.7			28 12 0.38	72 0.041 <1 1.79	0.007 0.06		0.02 1.3 0.04 1.2	0.1 <.05 0.1 <.05	8<.5 12<5		<.5
L1860 1325S	569254.9	5475438	1.4 9	18.5 17.7				3.7 0.5 5.3	5<.5 0.7		8 0.1	0.3 0.6			13 12 0.18 21 14.1 0.47	76 0 055 3 2.05	0.005 0.07		0.04 1.2	0.1 < 05	8<5		0.7
L1860 1350S L1860 1425S	569244.1 569243.9	5475418 5475358	1.2 12.4 0.8 15	25.5				5.5 4.4 1.5			26 0.2	0.3 0.5			25 15.2 0.42	72 0.026 <1 2.11	0.007 0.08	0.1	0.03 1.5	0.1 <.05	7 <.5		1.7
L1860 14255	569249.3	5475338	0.8 15.6	15.7				5.3 1.4			8 0.1	0.2 0.4			20 15.1 0.44	88 0.041 1 2.72	0.005 0.07		0.03 1.7	0.1 <.05	7 <.5		0.9
L1860 1475S	569257.8	5475313	0.6 9.5	11.1	39 0.1			2.8 0.1			9 0.1	0.1 0.4		08 0.097	16 9.1 0.18	89 0.038 <1 1.42	0.006 0.05		0.03 0.9	0.1 <.05	6 <.5		1.1 3.5
L1860 1500S	569266	5475295	1 11	12.2				6.4 0.4			6 0.1 7 0.1	0.2 0.4		04 0.077 04 0.075	16 12.3 0.32 17 12.9 0.32	70 0.082 <1 2.31 71 0.086 1 2.32	0.006 0.08		0.05 1.4 0.04 1.4	0.1 <.05	8<.5 8<.5		2.1
RE L1860 1500S	589266	5475295	D.9 11.3 0.7 11.6	12.7 8.5				6.3 0.1 67	€ 2.1 I 4.19	5.3 69	4 0.1	0.2 0.3		04 0.075	19 10.4 0.33	56 0.055 2 2.21	0.006 0.04		0.04 1.5	÷	7 <.5		4.9
L1860 1525S L1860 1550S	569264.3 569259.2	5475277 5475259	1.3 13.8	12.9				8.6 0.1		8.9	5 0.1	0.2 0.4		03 0.035	15 12.3 0.34	86 0.044 <1 2.48	0.005 0.05	0.1	0.08 1.4	0.1 < 05	8 <.5		2.6
L1860 1575S	569252.7	5475240	1 7.9					6.4 0.	4.1	5.4	7 <.1	0.2 0.4		08 0.031	18 10.3 0.32	63 0.04 <1 1.92	0.005 0.05		0.02 1	0.1 <.05	7 <.5		4.1
L1860 1600S	589247	5475222	0.8 6.9	10	35 D.1			6.2 0.3		4.6	5 0.1	0.2 0.4		04 0.031	15 8.7 0.2	66 0,059 5 1.6	0.009 0.05		0.03 1.3 0.01 0.8		7 < 5		3.6 13
L1860 1825S	569242.4	5475204	0.6 5.9	6.8				5.8 0.		4.6 5.7	3 <.⊧ 6 0.1	0.2 0.4		03 0.02 04 0.041	22 7.7 0.2 12 9.8 0.23	38 0.021 2 1.2 110 0.089 3 2.67	0.004 0.04 0.05		0.01 0.8		8 <.5 7 <.5		4
L1860 1850S	569239	5475188	0.9 12	11.3 11.2	41 0.1 30 < 1			5.4 1.1 48 01	•	ə.r 4.5	5 <.I	0.2 0.3		05 0.033	15 8.9 0.22	65 0.051 2 1.57	0.007 0.05		0.02 1	0.1 <.05	6 < 5		4
L1860 1675S L1860 1700S	569234.8 569230.5	5475187 5475150	0.8 10.3	12.8			91 2.13	5.8 1.			13 0.1	0.2 0.4		14 0.033	19 11.8 0.29	51 0.053 3 2.03	0.01 0.06		0.02 1.4		B 0.5		4.3
L1960 1725S	589223.4	5475127	0.5 6.2	14.5				4.2 0.	4 0.9	3.6	4 0.1	0.2 0.4		04 0.026	15 9.7 0.21	49 0,038 2 1.51	0.008 0.05		0.02 1	0.1 < 05	7 <.5		0.9
L1660 1750S	589219.7	5475102	0.5 8.6	16.7			58 2.04	3.3 0.			7 0.2	0.2 0.3		07 0.065	7 10.5 0.2	66 0.069 4 2.81	0.009 0.06		0.04 1.6		8<.5 6<.5		1.2 15.9
L1860 1775S	569216.3	5475077	0.5 12.7	18.3				3.2	1 18.9		15 0.1	0.2 0.4			21 16.2 0.74 15 9.9 0.23	61 0.028 <1 1.6 70 0.076 5 2.52	0.007 0.05		0.01 1.7 0.03 1.5		0 < 5 7 < 5		96
L1860 1800S	569210.6	5475055	0.9 10.1	11.2				6.1 0. 5.6 0.		6.2 5.6	5 0.1 4 0.1	0.2 0.3		04 0.056 04 0.036	20 10.7 0.26	82 0.054 2 1.64	0.007 0.05		0.03 1.2		7 <.5		51.3
L1860 1825S L1860 1850S	589203 589194.7	5475032 5475008	0.9 8.8	15.4 12.3				3.4 0.		3.5	5 1	0.2 0.3		05 0.024	15 8.2 0.2	88 0.049 2 1.38	0.006 0.06		0.02 0.9		6 <.5		10.4
L1880 1875S	569184.2	5474983	0.7 14	19.5			326 2.49	3.6 0.		4	5 0.1	0.3 0.3	49 D.I	07 0.078	10 10.4 0.29	85 0.104 <1 2.67	0.012 0.08		0.05 1.8		9 O.6		5.6
L1860 1900S	569173.4	5474961	0.5 15.2	14	69 0.1	12.3 B.6 4	182 2.43	3.4 0.	7 6.1	5.4	6 0.1	0.2 0.2		06 0.067	9 9.6 0.23	61 0.113 1 2.99	0.014 0.07		0.03 1.7		8 0.7		5.1 14.8
L1880 1925S	569162.4	5474938	0.6 14.3	12.3		••••	276 2.84	2.6 0.		3.3	5 0.1	0.2 0.3		11 0.051	13 8.6 0.27 20 11.4 8.48	93 8,099 <1 1.66 98 0,084 1 2.21	0.012 0.14		0.02 2 0.04 2.4		\$<.5 7<.5		19.9
L1880 1950S	569147 569137.7	5474907 5474885	0.8 36.8	14.2 10.3			246 3.31	5.1 0. 2.9 0.		6.6 3.8	6 0.1 5 0.1	0.2 0.3		08 0.045 11 0.048	16 9.4 0.32	85 0.093 3 1.81	0.011 0.14		0.03 2.3		9 0.7		39.4
L1860 1975S L1860 2000S	569137.7	5474863 5474863	0.7 21	12.6				2.9 0.		2.8	6 0.1	0.2 0.3		14 0.034	12 9 0.29	85 0.077 3 1.91	0.013 0.08		0.02 2.3	0.1 <.05	8 < 5		2.8
L1860 2025S	589114.9	5474842	0.7 24.3	12.8				3.7 0.		4.6	5 0.1	0.2 0.3		09 0.04	15 9.9 0.34	73 0.0634 2 2.14	0.01 0.09		0.02 2.4		8<5		5.2 8.9
L1860 2050S	559102.5	5474819	0.6 20.5	10.5				3.1 0.		4.7	6 0.1	0.1 0.3		07 0.057	17 8.7 0.31 9 9.7 0.25	69 0.05 3 2.18 75 0.103 3 3.14	0.008 0.07 0.017 0.09		0.03 1.7	0.1 <.05	6<.5 80.6		2.9
£1860 2075S	559090.5		0.6 33.7	11.7		12.2 17 5		3.3 0. ²		3.8 3.3	6 0.1 6 0.1	0.1 0.3		09 0.088	10 7.4 0.45	87 0.102 3 1.95	0.015 0.1		0.03 3.9		7 0.5		
L1560 2100S L1560 2125S	589078.9 589064.4	5474778 5474749	0.4 70.2					3.6 0.		2.1	9 0.2	0.2 0.2		21 0.077	6 7.3 0.36	65 0.132 2 2.55	0.021 0.1		0.06 3.6		9 0.6		2.7
L1560 2150S	589054.5	5474729	0,7 110.1	12.6				5.2 0.	5 107	3.3	8 0.1	0.2 0.2		13 D.133	5 9.7 0.28	59 0.138 4 4.13	0.015 0.08		0.08 3.5		10 0.5		106.6
L1860 21755	589042.8	5474703	0.8 71.8	11.6				3.9 0.		2.5	6 0.3 9 0.3	0.2 0.2		13 0.098 13 0.108	6 8.5 0.21 8 8 0.15	62 0.104 2 2.8 65 0.116 4 2.42	0.015 0.07 0.017 0.05		0.05 2.1		8 <.5 8 <.5		2.1
L1880 2200S	589029.5	5474877 5474658	0.4 21.3	13.1 12.8			330 1.85 499 1.9	3 0. 43 1		2.2 3.3	9 0.3	0.2 0.3		08 0.142	8 8.3 0.16	66 0,149 4 4.13	0.021 0.04		0.05 3.9		11 0.7		1.7
L1860 2225S L1880 2250S	569012.4 568995.1	54746541	0.8 23.3	9.9				2.6 0.		2.6	9 0.2	0.1 0.2		19 0.08	6 9.8 0.35	69 0.11 <1 2.8	0.024 0.09	0.1	0.03 3.6		8 < 5		2.7
L1860 2275S	565974.1	5474628	0.6 12.8	14.4				3.1 0	3 1.2		10 0.1	0.3 0.3		16 0.09	5 10.4 0.24	67 0.121 1 2.8	0.018 0.05		0.06 1.5		9 0.5 10 0.5		1.2 2.1
L1880 2300S	565974.1	5474628	1 38.3	12.5			908 2.39	4.1 0.		3.3	6 0.1	0.2 0.3		0.1 0.115 0.1 0.125	7 11 0.24	58 0.133 <1 3.84 68 0.137 2 4.17	0.013 0.07 0.015 0.08		0.06 3.3		10 0.5		2.1
RE L1860 2300S	568939.2	5474617 5474616	1 41.1	13.2 11.3			900 2.41 117 2.23	4.4 3.2 D.	1 2.1 5 1.4	3.5 2.7	7 0.1	0.2 0.3		13 0.084	8 9.8 0.22	B7 0.14 <1 3.18	0.02 0.06		0.03 2.3		10 <.5		1.4
L1880 2320M		5474610	0.5 20	14.4		20.7 18.4 18		4.5 0.			11 0.2	0.3 0.2	71 0.	17 0.084	7 12.2 0.43	87 0.129 <1 3	0.016 0.08	0.1	0.04 2.6		10 < 5		1.9
L1860 2375N		5474632	0.8 42.7	13.3		16.5 19.3 10	009 2.94	3.4 0.	5 5.2	2.7	7 0.2	0.2 0.3		12 0.087	7 12.2 0.26	90 0.134 <1 3.05	0.013 0.09		0.05 2.6		11 <.5		5.2 17.9
L1880 2400N		5474645	0 6 63.4	13.1		14.7 13.5 3		3.7 0.		4	7 0.1	0.2 0.3		13 0.053	11 9.1 0.32 12 9.9 0.35	79 0.105 <1 2.45	0.014 0.07 0.016 0.07		0.04 2.7		8<.5 8<.5		15.5
L1880 2425N		5474601 5474674	0.7 92	12.3 26.7			325 2.78 038 2.19	4.4 0.		4.9 2.8	8 0.1 13 0.3	0.2 0.2		.12 0.081 0.2 0.095	12 0.0 0.33	111 0.096 2 1.76	0.016 0.09		0.02 2.1		7 <.5		4.4
L1880 2475NA		5474691	0.4 46.6	11.3	• • • •			3.5 0.		3.9	9 0.1	8.2 0.Z	51 0.	14 0.08	11 9.9 0.31	100 0.111 <1 2.57	0.015 0.11		0.02 2.8		7 0.5		5.3
L1860 2500N		5474708	0.8 96	12.1		17.2 14.3 8	561 2.82	3.9 0.		3.5	9 0,2	0.2 0.3		09 0.063	14 11.1 0.29	100 0.1 <1 2.39	0.011 0.06		0.03 2		10 <.5		9.6 19.2
L1860 2525N		5474722	0.8 42.8	12.9	65 0.1		451 2.53	4.8 0.		3,9	7 0,1	0.3 0.3		09 0.061 0.1 0.12	15 10.2 0.34 5 9 0.13	78 0.087 <1 2.33 53 0.138 <1 4.47	0.012 0.08		0.02 2.2		8<.5 10 0.5		3.5
11860 2550N		5474738	0.8 25.5	17.5 14.8			260 2.26	4.4 0. 4.1 0.	-	4.6 3.9	9 0.2 12 0.2	0.2 0.3		.12 0.12	5 0 0.13 8 10.1 0.17	81 0.121 <1 3.51	0.015 0.06		0.04 1.7		10 <.5		4
L1860 2575NN L1860 2600NN		5474752 5474772	0.8 13.4	14.8	76 0.2		295 1.98	- 1 U. 3 D.	•	3.5	7 0.1	8.2 0.3		07 0.112	8 9.6 0.14	89 0.109 <1 2.83	0.013 0.05		0.03 1.4	0.1 <.05	9 <.5		2.1
1860 2825N		5474793	0.9 11.5	14.9				3.4 0.	• •••	2.9	5 0.1	0.2 0.4		06 0.082	8 9.2 0.14	56 0.122 2 2.12	0.015 0.05		0.02 1.4		10 0.5	46	1.5 3.3
DUP L1860 2650N	W 566533.1	5474810	1 13.3	15.2			147 2.22	4.1 0.	• • • •	4.6	9 0.1	0.1 0.3		.08 0.141	6 9.2 0.17	77 0.125 1 3.0	0.016 0.05		0.06 1.8		10 <.5 7 < 5	15	3.3 5.2
L1860 2650N		5474810	0.7 13.0	11.5	56 0 1		358 1.93	2.6 0.		3.4 3.6	7 0.1	0.1 0.3		.09 0.079 .05 0.138	17 9.3 0.25	71 0.063 <1 1.51 60 0.129 <1 3.51	0.009 0.05		0.03 1.3		9<5	15	18.5
OUP L1880 2875N		5474843	1 13	12	••••••		113 1.8 283 2	4.3 0,		3.0	6 0.1	0.2 0.2		.05 0.138	9 8.7 0.18	56 0.082 <1 2.37	0.013 0.05		0.04 1.2		7 < 5	-	8.1
L1860 2675NN L1860 2700NN		5474843 5474888	0.8 13.8	14.2 11.8				3.8 0		4.3	6 0.1	0.2 0.4		08 0,109	18 7.5 0.28	74 0.06 3 1.97	8.009 0.06		0.02 1.6	0.1 0.09	6 <.5		17.7
L1860 2825N		5474915	0.9 9.6	12.6	•••		310 2.39	4 0.	5 17.9	4.6	B 0.1	0.2 0.4	35 0.	09 0.044	20 10.4 0.3	105 0.058 6 2.3	0.008 0.08		0.03 1.6		7 < 5		17.9
L1860 2850N		5474927	0.9 11.6		50 0.1	15.2 9.2 4	435 2.67	4.2 0.		4.9	7 0.1	0.3 0.5		12 0.032	28 12.9 0.4	92 0.043 5 1.83	0.008 0.08		0.02 1.8		8<.5 8<.5		9.5 15 6
L1880 2075M	W 568469.5	5474936	1.9 37.2	42.8	84 0.2	30.9 19.2 26	642 3.14	B 3.	3 15.6	8 .1	28 0.6	0.4 0.8	29 (0.4 0.074	55 13.4 0.51	126 0.031 1 2.35	0.01 0.1	U .1	0.00 0.0	• v.i v.ta			

L1860 2900NW					61 0.1		386 2.43		1.7 20.3		11 0.1	0.2 0.6	25 0.18 0.1		10.7 0.45		1.61	0.005 0.07		0.01 f.				20.3
L1860 2925NW			1.6 33.1						1.6 27.6		11 0.1	0.3 0.7	37 0.15 0.		15.8 0.51		2.47	0.008 0.09		0.01 2.				27.6
L1860 2950NW		5474983	1.9 33				2319 3.24	9.7	1.2 24.9		11 0.8	0.5 0.9	35 0.15 0.				1.83	0.007 0.09		0.06 1.		=		24.9
1,1860 2975MW			1.7 27				1039 3.37	8.5	1.1 9.3		11 0.2	0.3 0.6	39 0.14 0.1				2.76	0.011 0.1		0.05 2.				9.3
L1860 3000NW			1.2 18.6		66 0.1		877 2.83	6.7	08 18.4	5.8	12 0.1	0.3 0.8	35 0.14 0.				2.12	0.009 0.08		0.05 1.				16.4
L1860 3025NW			1.2 18				1259 2.94	5	0.9 84.5	5.4	12 0.3	0.3 0.6	39 0.19 0				2.73	0.013 0.13		0.05 2.				84.5
L1860 3050NW			1.3 \$1,3				365 2.7	4.1	0.6 25.9	4	18 0.2	0.2 0.4	46 0.27 0.				2.84	0.022 0.07		0.05 1.				25.9
L1860 3075NW			1.1 10.3				1621 2.8	4.2	0.8 112	5.1	10 0.2	0.2 0.6	38 0.18 0				1.25	0.007 0.1	*	0.02 1.				112.1
L1860 3100NW			1.2 14.6				503 3.13	4,7	1 93.5	5.9	8 <0.1	0.3 0.5	43 0.07 0.			106 0.093 <1		0.011 0.07		0.06 2.				93.5
L1860 3125NW			1.5 7.1				1457 2.98	3.8	0.7 7.8	4.8	8 0.1	0.2 0.5	43 0.12 0.1				1.82	0.008 0.09		0.02 2.				7.8
11860 3150NW			1.9 9.9		39 0.1		248 3.61	5.2	0.8 10.7	5.1	6 0.1	0.3 0.6	54 0.05 0.0		12.3 0.77	72 0.048 <1	2.27	0.006 0.07	*	0.03 3.				10.7
L1860 3175HW			1.5 9				330 2.95	3.5	0.6 18.4	4.2	9 0.1	0.2 0.5	48 0.08 0.		13 0.39		2.12	0.011 0.08		0.84 2.				16.4
L1860 3200NW			1.5 11.1				249 2.46	5.7	1.2 2.6	5.2	11 0.1	0.3 0.3	34 0.1 0.1		9.7 0.2		4.28	0.021 0.05		0.09 2				2.6
RE 11860 3200NW			1.5 10.5				233 2.28		1.2 2.9	5.5	10 0.1	0.3 0.3	32 0.09 0.3		8.8 0.19		4.12	0.019 0.05		0.09 2.				2.9
11860 3225NW			1,4 10.5				674 2.69		1.2 3.9	6.4	8 0.1	0.3 0.4	32 0.07 0.				2.58	0.01 0.08		0.05 1.				3.9
L1860 3250NW			1.4 10.7				182 2.45		1.3 3.2	5 ∡	13 0.2	0.4 0.3	33 0.14 0.1		9.9 0.16		2.93	0.018 0.04 0.018 0.05	0.2 0.2	0.1 2.			.5	3.2
11860 3275NW			1,3 6.5				172 2.47	4.7	0.6 1.4		9 0.1 21 0.1	0.2 0.4	38 0.08 0.1		9.8 0.18		2.93	0.015 0.05		0.03 1.				1.4
L1860 3300NW			1 11.3				453 2.37					0.2 0.5	22 0.17 0.0				1.61	0.009 0.06	•••				.5	1.5
L1860 3325NM			0.8 5.8		26 .1		115 2.1	4.8 24	0.6 < 5	4.5	6 0.1 5≺01	0.2 0.3	28 0.05 0.1		10.2 0.28		5 1.02	0.005 0.04		0.05 1.				<.5 < 5
L1860 3350NW			0.4 5.3		22 0.1	6.1 3.1		2.4	04 19	•.•	5 ×0,1 16 02	• •			5.6 0.17		1.01	0.007 0.08		0.02 1.				-10
L1860 3375NW		5475293	0,4 6.6		25 0.1		525 1.19	2.2	0.4 1.9	1.7	16 U.Z 5 D1	0.1 0.4	18 0.14 0.1 17 0.04 0.1			43 0.027 <1	1.01	0.004 0.08	0.1 <0		¥ 0,1<.0; 7<0,1 <.0;			1.9 3.4
L1880 3400NW			0,4 8.8	9.3	34 <.1		154 1.65		0,5 3.4 DR<5	4,9 5.3	5 ₽.1 3 <01	0.7 0.3	17 0.04 0.0		8.5 0.36		1.07	0.003 0.03						3.4 < 5
L1940 0S		5476067	0.7 10.1	12	28 0.1					•.•	3 < 0.1		24 0.02 0.0			19 0.045 <1	0.96	0.006 0.03		0.04 1.				
L1940 25S	000100.1		0.6 4.5		12 0.1		00 2.00	3	0.4 < 5	3.1					8.4 0.08								5	<.5
L1940 50S	569423.6	5476039 5476026	0.8 9.7		21 0.1	3.9 2		3.7	0.9 <.5	4.7	5 0.1	0.2 0.2	32 0.05 0.0		10.2 0.1 8.3 0.13	27 0.078 <1 27 0.032 2	3.9 1.11	0.013 0.03		0.06 1.				<.5 <.5
L1940 755			0.5 5.3	9.8	22 0.1			3.6	0.5 < 5	3.1	3 0.1													
L1940 100S		5478015	0.4 6.1	\$	42 0.1		120 1.68	3.4	0.7 <.5	5.7	3 0.1	0.1 0.2	19 0.02 0.0		9.8 0.28		1.55	0.002 0.04			1 0.1 <.0			<.5
L1940 125S		5476001	0.8 8		26 0.1		112 1.85	3.3	0.7 <.5	4.1	4 <0.1	0.2 0.3	23 0.03 0.1		7.2 0.17		5 1.99	0.009 0.04			1 0.1 <.0			<.5
L1940 150S		5475984	1 6,1	8.2		5.3 3		3.6	0.7 <.5	4.7	3 <0.1	0.2 0.4	25 0.02 0.0		8 0.17	31 0.031 <1	1.44	0.005 0.03		0.03 1.				<.5
L1940 175S		5475981	0.6 7	8.1	24 <.1	6.7 2.9		4.8	0.8 <.5	5.5	2 < 0.1	0.2 0.3	19 0.02 0.1		9.5 0.26		1.24	0.003 0.03		0.03 1.				<.5
L1940 2005	589534.1		0.8 12.8		30 0.1	6.4 3.6		3.7	0.8 2.7	5.3	5 0.1	0.2 0.3	35 D.04 0.1		10.8 0,13	35 0.064 <1	2.75	0.01 0.05		0.05 1.			-	2.7
L1940 225S	569538.5		1.1 11.6		35 0.1	6.7 4.5		4.9	0.9 1.8	8.2	4 0,1	0.3 0.4	40 0.03 0.0		11.9 0.18		2.88	0.009 0.04		0.05 1.			-	1.8
L1940 250S	569540.5		28			7.1 4.5		8.8	0.7 2.8	5.9	4 0.1	0.5 0.6	57 0.03 0.0		17.7 D.18		2.41	0.007 0.05		0.07 1.			8	2.6
L1940 275S	569536.4		2.1 11.3			7.6 3.6		5.7	0.7 4.1	7.2	3 <.1	0.4 0.5	32 D.02 0.1		15.1 0.31		2.02	0.004 0.03		0.04 1.				4.5
L1940 300S	569527.5		3 19.8		36 0.1		131 2.89	4.8	0.8 1.5	5.4	8 0.1	0.4 0.4	39 0.04 0.0		14.3 0.31		2.21	0.006 0.03		0.03 1.		•		1.5
L1940 325S	569513.5		1.3 12.9				150 2.85		0.8 1.2	8.2	6 0.1	0.3 0.4	35 0.04 0.0		15.8 0.53		2.2	0.004 0.04		0.03 1.	• • •		•	1.2
L1940 350S	569502.1		1.6 10.7		33 < 1		226 2.9	5.6	1 0.5	6	7 0.1	0.3 0.4	38 0.06 0.1		12.3 0.2	64 0.093 <1	3.67	0.01 0.04		0.08 2.			•	0.5
L1940 375S	569487.6		1.2 10.3				482 3.18	4.5	0.5 < 5		12 0.1	0.3 0.5	48 0.1 0.1		21.2 0.29		2.14	0.008 0.06			2 0.1 0.0		-	<.5
L1940 400S	569469.3		1.5 16.1						1.1 1.5	5.8	6 0.2	0.3 0.5	35 0.04 0.0		13.7 0.33		2.95	0.009 0.05		0.06 2.				1.5
L1940 425S		5475746	1.3 13.4					5.8	0.8 1.1	5.3	8 0.1	0.3 0.4	41 0.06 0.1		12.9 0.21	80 0.098 <1	3.18	0.01 0.06		0.05 1.				1.1
£1940 450S			1,2 16.9					5.5	1 1.3	5.3	7 0,1	0.3 0.3	37 0.06 0.1		12.6 0.28	62 0.104 1	3.53	0.011 0.05		0.08 2.			6	1.3
L1940 475S		5475731	1.2 12.7				349 2.91		0.5 1.9	4.4	7 0.1	0.4 0.4	37 0.05 0.1		13.1 0.29	65 0.077 -1	2.48	0.009 0.05		0.05 1.			_	1.9
L1940 5005			2.3 19.9					····	0.9 <.5		12 0.1	0.4 0.6	44 0.09 0.1		18.3 0.29		2.18	0.009 0.09		0.04 2.				<.5
L1940 525S		5475710	1.4 11.7				674 2.3	4.9	0.5 < 5	4.1	7 0.1	0.3 0.4	32 0.06 0.4		12.4 0.24		1.61	0.008 0.06		0.03 1.				<.5
L1940 550S	589337.2		1.4 10.5				582 2.18	6.8	0.6 <.5	4.4	7 0.1	0.3 0.4	30 0.06 0.4		11.3 0.21		1.66	0.007 0.06		0.03 1.				<.5
L1940 575S		5475668	1.1 9.7		48 0.1	8.5 0		4.8	0.5 1.3	3.1	14 0.2	0.3 04	23 0.14 0.1		7.9 0.14		1.55	0.01 0.07		0.03 1.				1.3
L1940 600S		5475674	0.9 9.4		40 0.1	8.7 5		3.9	0.5 1.3	3.7	12 0.1	0.2 0.4	30 0.05 0.0		10.5 0.17		1.54	0.008 0.05		0.03 1.			-	1,3
L1940 825S	569270.9	5475660	1.4 12		48 0.1 57 01	8.7 7.2		4.7	1 1.1 0.7 1.9	5.7	7 0.1	0.3 0.3	29 0.05 0.0		11.3 0.19	76 0.064 1 96 0.087 2	2.9	0.01 0.05		0.05 1.			1	1,1 1,9
L1940 650S L1940 675S	569252.1 569234	5475848 5475835	1.3 11.6	17.9 18.7		8.8 8.7 10.5 7.5	773 1.93	4.4 5.1	0.7 1.9	3.8 4 2	12 0.2	0.3 0.3	29 0.1 0		9.5 0.14 8.9 0.12		3.77	0.012 0.05		0.04 1.			,	1.4
L1940 700S		5475622	2 11.0				392 2.49	5.1 81	0.6 1.5	4.4	8 0.1	0.3 0.3	33 0.08 0.0	-	11.0 0.17		2,44	0.012 0.07		0.07 2.			,	1.5
RE L1940 700S		5475622	1.8 10.9			10.6 7.6		7.9	0.8 1.1	4.2	9 0.2	0.3 0.4	34 0.1 0.0		11.7 0.17	72 0.105 <1		0.012 0.07	****	0.07 1.			۶.	1.1
L1940 725S		5475606	1.6 17.7	20.3			181 2.37	5.3	0.9 1.8	5.5	8 01	0.3 0.4	35 0.05 0.0				2.54	0.01 0.07		0.05 1.			-	1.8
L1940 7205		5475587	0.8 74.6			15.5 13.5		5.3 5.7	0.9 1.0	5.5	10 0.1	0.3 0.4	52 0.1 0		11.8 0.5	94 0.059 <1		0.005 0.08		0.02 3.				<.5
L1940 775S		5475568	2.1 17.1				315 3.3	7.2	0.7 2.2	43	12 0.2	0.3 07	41 0.08 0.0		14 0.35		2.31	0.008 0.08		0.04 1.			-	2.2
L1940 800S		5475549	1.1 14.1			11.7 14.5		4.9	1.6 0.8		35 0.4	0.2 0.5	28 0.3 0.4				1.84	0.009 0.08		0.05 1.				0.8
L1940 825S		5475531	09 132				912 2.13	3.8	1.6 2.4		20 0.4	0.2 0.5	27 0.18 0.0				2.24	0 007 0.09		0.04 1			7	2.4
L1940 850S		5475505	0.9 12.3		56 0.1		311 2.97	4	1 2.3	8.7	5 0.1	0.2 0.5	39 0.03 0.0		15.3 0.32	67 0.06 2	1.99	0.005 0.06	0.1	0.04 1.	9 0.1 0.0	7 9 0.	6	2.3
L1940 875S	569112.1		1 11.8		53 0.1	9.6 6.7		5.5	0.9 2	5.2	4 0.1	0.3 0.4	28 0.04 0.4		12.3 0.3	60 0.038 <1	1.71	0.004 0.05		0.04 1				2
L1940 900S		5475457	14 16.4			18.3 14		5.6	1.4 2.5	7.7	7 0.2	0.2 0.8	39 0.06 0.0		17.3 0.38	92 0.08 <1	3.5	0.009 0.08		0.07 2.			5	2.5
L1940 925S	569105.3		18 24.4			17.5 14.3		5.7	2 3.5	8.9	5 0.2	0.4 0.5	32 0.04 0.0		15.1 0.42		2.64	0.005 0.06		0.08 2			8	3.5
L1940 950S	569103.4		0.9 156	15	81 0.2	13 9.4		4.9	1 4.6	7.1	6 0.1	0.3 0.4	32 0.05 0.0		14.8 0.32	77 0.072 <1	2.66	0.007 0.07	0.1	0.06 2.			8	4.6
L1940 975S	569100.6		0.8 5.7	9.7	25 0,1	6.1 3.6		2.7	0.5 4.1	3.6	4 0.1	0.1 0.3	26 0.03 0		9 0.18	42 0.031 1	1.05	0.006 0.05	0.1	0.01	1 0.1 <.0	8<5		4.1
L1940 1000S		5475386	1.1 9.5		31 0.1	7.3 3.6		4.4	0.7 4.8	4.4	8 0.1	0.2 0.4	31 0.06 0.0		10.6 0.14	60 0.064 <1	2.45	0.01 0.05	0.1	0.04 1.	7 0.1 0.0	7 8 <.5		4.8
L1940 1025S		5475343	1.3 11.5		42 0.1	9.4 6.5		4.3	0.9 2.6	5	7 0.1	0.3 0.3	36 0.05 0.0		8.9 0.17	69 0.087 <1	2.93	0.011 0.05	0.2	0.04 1.	8 0.1 0.0	6 10 <.5		2.6
L1940 1050S		5475323	1.4 12.8		49 0.1	9.9 7		5.1	0.7 2.6	4.4	8 0.1	0.2 0.4	41 0.05 0.4		8.2 0.21	73 0.099 <1	2.58	0.012 0.05		0.06 1.	6 0.1 0.1	1 10 <.5		2.6
L1940 1075S		5475298	1.4 15.2		60 0.2		214 2.33	5.5	0.9 2.6	4.2	14 0.2	0.3 0.4	43 0.16 0.0		10.1 0.18	76 0 119 2	2.93	0.014 0.06	0.3	0.08 1.	5 0.1 0.1	2 10 <.5		2.6
L1940 1100S		5475276	0.8 12.6		49 0.1	9.5 5.2		4.6	0.7 2.5	5.8	5 0.1	0.2 0.3	38 0.04 0.0		11.2 0.25	66 0.06 <1	2.61	0.01 0.04	0.1	0.05 1.	9 0.1 <.0	8 <.5		2.5
L1940 1125S		5475253	0.9 17.8	9.8	45 <,1	12.9 8.9		5.7	0.8 2.9	5.9	4 0.1	0.3 0.3	31 0.03 0.1		13.3 0.38	57 0.024 1	2.23	0.004 0.03	0.1	0.03 5.	7 0.1 <.05	5<.5		2.9
L1940 1150S		5475235	1 9.1	10.8	32 < 1	7.3 4		4.4	0.4 2.2	4.6	5 0.1	0.2 0.4			10 0.21	58 0.044 1	1.71	0.006 0.05	0.2	0.04 1.	4 0.1 <.0	8<.5		2.2
L1940 1175S		5475207	1.1 15.9		52 0.1		253 2.38	4.4	0.6 3.4	4.8	6 0.1	0.2 0.4	39 0.05 0.0	11 B	11.8 0.23	91 0.098 1	2.83	0.01 0.06	0.2	0.03 2.				3.4
L1940 1200S		5475184	0.9 13.5				364 1.93	3.9	0.6 2.4	3.8	5 0,1	0.2 0.4	36 0.04 0.0	59 10	8.8 0.17	66 0.067 <t< td=""><td>2.36</td><td>0.011 0.04</td><td>0.1</td><td>0.06 L</td><td>4 0.1 0.0</td><td>6 9<.5</td><td></td><td>2.4</td></t<>	2.36	0.011 0.04	0.1	0.06 L	4 0.1 0.0	6 9<.5		2.4
L1940 1225S	569060.8				53 0.1			5.1	0.7 3.5	5	5 0.1	0.2 0.5	42 0.04 0.0	76 11	11.3 0.19	75 0.098 <1	2.69	0.011 0.06	0.1	0.05 1.7	9 0.1 0.0	6 9 0.	5	3.5
L1940 1250S	589055.6	5475138					272 2.98	8.8	1 28.5	7.1	5 0.1	0.5 0.6	35 0.04 0.0	49 20	10.8 0.35	71 0.046 <1	2.07	0.004 0.04	0.2	0.04 1,	8 0.5 <.09	8 < 5		28.5

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CP-24 1 58 26 76 0.2 24 11 229 2.58 8 5 ND 5 9 1 2 2 58 0.12 0.06 4 20 0.4 62 0.12 6 7.79 0.02 0.05 2 5 5 CP-25 1 51 15 95 0.1 20 6 11 0.05 7 24 0.58 45 0.06 2 0.05 2 5 5 CP-26 1 39 11 70 2 2 48 0.11 0.05 7 24 0.58 45 0.06 2 0.05 2 5 5 CP-26 1 39 11 70 2 2 48 0.11 0.09 7 24 0.58 45 0.06 2 5 5 CP-26 1 39 11 70 2 2 48 0.13 0.09 2 20 39 55 0.09 2 162

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1 2	22 23	15 13	95 (69 (3.1 11 0.3 21		8 1032 2.0 7 297	2 6	5 ND	8 5	ź	1	2	2	37	0.07	0.13	- 2	13 0.26	68 48	0.12	2 2		0.02		2 2	
1	47	28		3.2 2	-	9 242 2.5		5 ND	5	é	÷	2	2	57	0.11	0.05	2	30 0.48	42	0.09	4		0.02		2	
ť	95	24	83 (2 230 2.7		5 ND	5	6	f	2	2	85	0.1	0.05	3	17 0.41	81	0.12	2 :		0.01		2	
1	85 71	24		0.4 2. 0.4 2.		1 352 2.5		5 ND	5	2	ł	2	2	59	0.1	0.05	4	20 0.4	5ê	0.12	3		0.01		2	
2	148	44		0.1 2		3 210 3.4		5 ND	7	ź	÷	2	2		0.08	0.08	5	22 0.75	77	0.12	3 :		0.01		2	
1	224	77		1.2 2		2 424 3.0		5 ND	é	é	ť	2	2		0.00	0.08	4	24 0.52	68	0.12	2		0.01		ź	
+	84			3.2 2 ³		1 511 3		6 ND	8	ê	, t	2	2		0.00	0.08	5	23 0.58	59	0.12	3		0.01		ź	
2	101	53		2.1 2		0 303 3.0		5 NO	6	6	ł	3	2		0.11	0.04	12	27 0.79	87	0.13	4		0.01		2	
2	118	44		0.2 2		0 479 2.5		5 ND	Ă	12	1	ž	3		0.13	0.07	11	16 0.49	85	0.13	5 :		0.01		2	
3	47	53		0.1 2		3 1132 2.9		5 ND	5	14	ť	3	2		0.12	0.05	15	23 0.83	95	0.16	5 3		0.01	D.1	2	
3	50			12 4		9 388 3.5		5 ND	11		ł	2	2		0.07	0.04	16	29 1.02	73	0.12	6		0.01	01	2	
2	68			0.3 1		0 417 2.5		5 ND	4	8	1	2	2		0.08	0.1	11	9 0.39	61	0.1	5 3		0.01		2	
2	66			0.4 18		9 392 2.4		5 ND	5	5	i	2	2		0.87	0.09	10	11 0.38	57	0.1	4		0.01		2	
1	58			0.3 1		8 399 2.1		5 ND		5	i	2	2		0.08	0.09	9	10 0.34	54	0.09	5		0.01	0.05	2	
3	128			0.1 1		0 350 3.4		5 ND	6	6	1	2	2		0.51	0.07	14	11 0.65	85	0.11	4		0.01	0.07	2	
ĩ	181			0.1 2		0 270 3.4		5 ND	, g	5	1	2	2		0.11	0.07	13	12 0.81	72	0,11	4		0.01	0.08	2	
1	29			5.4		8 596 2.2		5 ND	Å	4	1	2	2	47	0.05	0.1	9	10 0.22	42	0.08	- i -		0.01	0.04	2	
3	71			0.6 1		9 401 2.6		5 ND	6	7	2	2	2	49	0.08	0.09	11	14 0.5	84	0.1	4 :				2	
ž	41			1.2 1		7 450 2.4		5 ND	6	6	1	2	2	42	0.07	0.09	51	18 0.64	71	0.11		1.9		0.11	2	
1	42			0.3 14		5 344 2.2		5 ND	5	5	i	2	2		0.09	0.08	10	14 0.57	85	0.09	4		0.01		2	
1	45			0.1 1		7 218 2		5 ND	5	8	1	2	2		0.05	0.1	7	9 0.31	70	0.13	3 3		0.01		2	
ł	101			2.1 2		1 247 3.0		5 ND	7	7	1	2	2	77	0.1	0.07	14	14 0.7	89	0.1	7		0.01	0.08	ž	
1	26	23		2.4 1		7 308 2.0		5 ND	3	4	1	2	2		0.04	0.12	7	9 0.17	39	0.1	4 1			0.04	2	
1	80			0.1 1		8 332 2.7		5 ND	7	5	1	2	2		0.07	0.06	14	16 0.77	69	80.0	4 :			0.09	2	
1	86			0.1 20		9 189 2.8		5 ND	6	8	1	2	2		0.08	0.06	15	17 0.76	66	0.09	4 :			0.08	2	
1	50	33).2 tž		5 339 2.2		5 ND	5	4	1	2	2		0.06	0.06	11	14 0.59	27	0.07	3			80.0	2	
2	80	516		0.4 10		4 228 2		5 ND	5	5	1	2	3		0.08	0.09	11	12 0.32	38	0.07	3 1			0.06	2	
1	48			0.4 1		2 108 2.7		5 ND	8	13	1	2	2		0.12	0.09	10	12 0.25	69	0.15	4 2		0.02	0.06	2	
1	35	43	97 ().† 1)	2	6 208 2.5	3 9	5 ND	8	6	1	2	2	42	80.0	0.11	12	\$4 0.47	43	0.07	5 1	1.81	0.01	0.05	2	
1	26	31	76 (0.4 53	2	4 227 2.0	8 3	5 ND	4	4	1	3	3	44	0.85	0.09	9	11 0.31	40	0.07	4 1	.31	0.01	0.05	2	
1	61	19	101 0	0.1 1:	3	5 119 2.4	3 7	5 ND	5	4	t	2	2	55	0.05	0.04	11	13 0.53	43	0.05	4 1	1.54	0.01	0.04	2	
1	18	28	59 0).Z (в	2 121 1.7	17	5 ND	5	- 4	1	2	Ż	43	0.06	0.05	10	8 0.27	23	0.06	2 (.83	0.01	0.05	2	
1	37	42	114 0).3 11	1	6 302 2.0	7 5	5 ND	- 4	6	1	2	2	40	0.07	0.12	8	9 0.29	44	0.08	2 1	1.85	0.01	0.05	2	
1	42	30	150 0	0.3 1	7	5 182 2.6	7 5	5 ND	7	- 4	1	2	2	51	0.08	0.04	8	23 0.64	53	0.12	5 1	1.75	0.01	80.0	2	
1	58	56	137 0	2.5 14	•	9 195 2.1	8 8	5 ND	5	6	1	2	2	43	0.06	0.1	8	11 0.36	55	0.09	- 4	1.9	0.01	0.05	2	
1	40	25	207 ().2 13	3	6 221 2.5	1 6	6 ND	6	5	1	2	2	48	0.08	0.12	7	15 0.38	55	0.09	3 1	1.99	0.01	0.06	2	
1	26	20		3.2		1 82 2.8		5 ND	- 4	- 4	1	2	2		0,03	0.1	- 4	9 0.1	31	0.13	3 2			0.02	2	
1	113).2 2		9 243 3.1		5 ND	8	8	1	2	2		0.11	0.05	10	15 0.88	72	0.11	2 1			0.12	2	
2	49			0.3 14		7 185 2.8		5 ND	8	- 4	1	2	2		0.05	0.1	7	12 0.37	52	0.11	- 4- 2		0.01		2	
1	81	19).t 1		7 876 2.8		i ND	3	3	1	2	Ż		0.85	0.1	6	9 0.15	42	0,09	3 2		0.01		2	
1	31	29		0.6 1		7 302 2.3		d ND	8	5	1	2	2		0.05	0.11	8	13 0.39	47	0.08	8 1		0.01		2	
2	51	54		0.2 1		0 189 2.8		5 ND	5	5	1	2	z		0.05	0.12	5 3	11 0.22	53	0.12	8 3		0.01		3	
1	41	17	52 0			3 86 1.6		8 ND	4	7	1	2	2		0.04	0.09	7	7 0.08	18 30	0.13	3 3		0.02		2	
1	14 54	87 34	81 C			2 179 1.5		5 ND 5 ND	5	5 4	1	2 2	ź		0.07	0.04	8	9 0.18 14 0.27	40	0.07	·2 (4 2		0.01 0.01		2 2	
- 1	80	19		51 1		6 221 3.1		5 ND	4			2	2		0.09	0.08	ě	12 0.29	44	0.1	8 1		0.01		2	
÷.	19	39		0.3		2 145 2.0		5 ND	3	-	1	2	2		0.05	0.09	ě	8 0.14	38	0.09	3 1		0.01		2	
i	34	16		2 8		7 339 1.9		6 ND		8	i	2	2		0.05	0.14	4	8 0.1	40	0.13	3 2		0.01		2	
Í.	48	16	88 0	1.1 1	i	5 245 3.3		6 ND	4	5	1	2	ž	75	80.0	0.09	4	10 0.3	35	0,11	4 2	44	0.01		2	
1	23	27	155 0	2 1		3 205 2		5 ND	4	4	1	2	2	52	0.05	0.09	6	8 0.24	37	0.09	3 1		0.01		2	
1	31		124 0	0.1 1	•	5 288 2.4	2 3	5 ND	5	8	\$	2	2	37	0.05	D.13	5	10 0.18	45	0.13	4 3	.96	0.01		2	
2	66	73	292 (0.3 17	r	8 215 3.	8 8	5 ND	6	8	1	2	2	77	0.07	0.07	8	13 0.4	59	0.12	2 2	2.89	0.01	0.05	2	
2	55	20	140 0	0.1 14	6	5 151 3.0	69	5 ND	4	5	1	2	2	72	0.11	0.07	9	11 0.47	33	0.07	4 1	.55	0.01	0.04	2	
t	29).2 1	-	4 345 2.		5 ND	3	5	1	2	2		0.09	0.05	7	12 0.19	39	0.1	5 1			0.05	z	
1	78			0.2 17		0 210 4.3		5 ND	5	5	1	2			0.11	0.08	5	12 0.45	82	0.12	3 2			0.08	2	
1	52			0.3 15		9 416 3.1		5 ND	6	8	1	2	2		80.0	0.18	8	15 0.37	63	0.13	4 3		0.02		2	
2	94			7.2 10		0 376 3.5		5 ND	5	8	1	2	2		0.12	0.09	10	15 0.61	81	0.1	5 2		0.01		2	
1	36	21		0.2 1		8 497 3.2	-	5 ND	3	5	1	2	3		0.07	0.08	5	10 0.2	49	0.13	3 3			0.04	2	
1	50			0.2 14		9 714 2.8		5 ND	4	8	1	2	2		0.08	0.14	8 7	11 0.41	57	0.11	3 3		0.01		2	
1	58	21		0.2 14		9 331 3.1		5 ND	4	5	1	2	2		80.0	0.07	ź	12 0.32	44	0.1	8 2		0.01		2	
1	46	18		0.2 10		8 508 2.4 8 361 2		5 ND 5 ND	3	5	1	2	2		0.07	0.05	÷	8 0.17 10 0.3	63 39	0.1 0.1	4 1		0.01 0.01		2	
1	33		144 0						4	5	1	2			0.14	0.07	10	15 0.72	38 88	0.12	2 2		0.01		22	
1	113 89		116 0 106 0			2 221 4.7 8 356 3.0		5 ND 8 ND	6	8 8	1	2	3		0.14	0.07	:0	12 0.47	80 57	0.12	3 2		0.01		2	
;					·				•	-	? 1	_	-		0.08	0.14	7				4 2					
2	28		110 0			7 421 2.4		5 ND	3	8	1	2	2		0.05	0.14	10	6 0.2 12 0.68	43 84	0.11				0.04	2	
3	134	24	•	0.1 2		3 281 4.4 5 215 3.3		5 ND	6 5	8 4	1	2	2		0.07	0.08	10	12 0.00	32	0.13	32			0.06	2 2	
;	68	20).2 1°				5 ND		;	1	2	2		0.14	0.07	÷	42 0.97	52 64	0.12	2 1		0.01		2	
3	81 85	29 22).1 25).2 25		9 223 3.0 1 262 2.4		5 ND 5 ND	° 5	8	1	2	2		0.09	0.03	5	15 0.33	65	0.12	8 2			0.08	2	
3	90	13).2 Z.).1 2:		2 476 2.6		5 ND		7	1	2	2		0.14	0.07	4	26 0.53	44	0.09	3 1			0.05	2	
4	WU 86	13).1 2.).2 2:		1 163 2.4		5 ND			ł	2	2		0.08	0.00	2	8 0.24	82	0.05	3 3			0.05	2	
2	20	21).z 23).1 20		5 368 2.1		5 ND	5	8	í	2	ź		0.09		8	21 0.72	60	0.12	3 2		0.01		2	
1	139		106 0			0 232 3.1		5 ND	5	8	1	2	2		0.12		5	19 0.92	45	0.12	2 1		0.01		2	
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1	77		87 0			682 2.3			5 ND	- 4	10	1	2	2		0,11		- 4	14 0.32		0.14		2.73		0.06	2	
2	67		107 0			511 2.4			5 ND	- 4	10	1	2	2		0.15		6	17 0.49	66	0.12		2.32		0.07	2	
2	54	17	92 0.						5 ND	5	8	1	2	2		0.09	0.08	- 4	13 0.3	58	0.14		2.85		0.06	2	
1	353	29	94 0						5 ND	7	8	1	2	2	86	0.2		7	40 1.13	72	0.13		2.07		0.1	2	
3	90		104 0						5 ND	3	7	1	2	2	56	0.14	0.04	7	33 0.85	63	0.12		2.07		0.06	2	
2	134	22	92 0						5 ND	3	8	1	2	2	61	0.15	0.06	6	15 0.44	55	0.11		2.03		0.06	2	
1	78	16	94 0	2 18	8				5 ND	3	7	1	2	2	62	0.14	0.06	-6	11 0.33	50	0,13	- 4	1.82	0.02	0.06	2	
1	68	20	88 0		-				5 ND	2	8	1	2	2	41	0.13	Q.1	6	12 0.29	50	0.13		2.35		0.05	2	
1	39	13	83 0						5 ND	2	8	1	2	2	42	0.09	80.0	- 4	12 0.17	59	0.13		2.22		0.05	2	
1	108	17	90 0						5 ND	Э	8	1	2	2	48	0.11	0.1	- 4	10 0.2	- 71	0.14		2.81		0.05	2	
1	191		104 0			510 3.			5 ND	2	7	1	2	2	98	0.25	0.07	4	13 0.54	80	0.11		2.13		0.06	2	
1	100	17	94 0						5 ND	3	6	1	2	2		0.15	0.05	5	21 0.53	46	0.11		1.58		0.06	2	
1	228	16	82 0			313 3			5 ND	3	7	1	2	2		0.18		3	18 0.54	67	0.13		2.21	0.02		2	
2	125	18	89 0			341 2			5 ND	2	8	1	2	2		0.12	0.1	3	11 0.28	72	0.14		3.29		0.05	2	
2	72	14	6t C.						5 ND	2	6	1	2	2		0.13		5	12 0.21	61	0.13		1.9		0.04	2	
1	135	14	86 0			249 3.			5 ND	3	7	1	2	3		0.14	0.1	5	16 0.41		0.13		2.85		0.08	2	
1	123	19	97 0			848 2.1			5 ND	2	7	1	2	2		0.15		5	12 0.27		0.13		2.3	0.02		2	
1	155	13	71 0.			301 2.4			5 ND	•	8	1	2	23		0.09	0.14	6	12 0.26		0.16		3.45		0.05	2	
1	80		140 0			244 3.			S ND	4	8 9	1	2	2		0.13		9	23 0.89		D.14		2.21		0.11	2	
1	95 26	21 18	97 C. 86 C.			867 2.1			5 ND 5 ND	3	8	1	2	2	33	0.19	0.07	\$ 6	24 0.54		0.13		2.45 2.62		0.07 0.07	2	
1	27	15	94 0						S ND	3	7	1	2	3	35 35	0.1	0.05	7	19 0.30		0.13		2.11		0.07	2	
1	41	17	78 0			236 2.			5 ND	2	8	÷	2	2		0.12	0.00	8	24 0.56	68	0.00		2.17		0.07	2	
;	39	18	77 0			215 2.			5 ND	3	6	ł	2	2		0.12		8			0.09		2.23		0.05	2	
1	85	17	70 0			194 3.			5 ND	4	7	i	2	Â		0.13		7	17 0.71	98	0.09		2.17		0.07	2	
ż	78	22	83 0			236 2.1			5 ND	3	7	i	2	2		0.12		á			0.11		2.63		0.05	2	
1	55	21	72 0			295 2.0			5 ND	3	8	i	2	4	50	0.1	0.08	9	20 0.43		0.11		2.32		0.06	2	
i	52	22	95 0			501 2.9			5 ND	2	6	1	2	3		0.12		š	20 0.4		0.09		2.34	0.01		2	
÷	76	35	67 0			173 2.0			5 ND	ŝ	ž	1	2	3		0.15		11			0.09		1.78	0.01		2	
i	81	18	59 0			279 2.1			5 ND	Å	ż	1	2	2		0.17		8	28 0.61		0.09		1.82	0.01		2	
1	71	28	59 0			276 2.0			5 ND	Å	7	1	2	2		0.14		8			0.09		1.68		0.06	2	
Í.	80	22	54 0			185 2.0			5 ND	8	ŝ	1	2	2		0.13		š		54	0.09		1.59	0.01		2	
2	71	29	58 0		-				5 ND	4	5	1	2	2		0.11		7	17 0.58	45	0.07	2	2	0.01	0.04	2	
1	75	12	48 0		ิต	283 2.3			5 ND	5	6	1	2	2	43	0.12	0.08	8	16 0.4	45	0.08	2	1.95	0.02	0.05	2	
i	58	15	48 0.			218 2.			5 ND	5	ā	i	2	2		0.11	0.07	ē	14 0.38	70	0.09		2.34		0.05	2	
2	42	11	44 0						5 ND	3	6	1	2	2		0.09		5	15 0.34	69	0.08		1.98	0.01		2	
1	41	12	49 0		8	361 2.0			5 ND	3	6	1	2	2			0.08		18 0,38	49	0.07		1.61	0.01		2	
1	65	12	61 0	2 18					5 ND	4	6	1	2	2		0.11		7	20 0.45	57	0.07	2	1.64	0.01	0.05	2	
1	51	10	61 D.	3 16	10	320 1.9			5 ND	3	8	1	2	2		80.0		5	11 0.2	77	0,13	2	2.68	0.02	0.04	2	
1	143	17	80 0	2 19	: 13	252 2.0	53 8	L :	5 ND	3	9	1	2	2	52	0.14	0.09	6	14 0.4	80	0.11	3	2.55	0.02	0.04	2	
42	59	18	81 D.	4 13	8	249 2.3	23 8	1	5 ND	4	7	1	2	2	15	0.04	0.2	4	11 0.16	67	0.17	14	3.76	0.02	0.04	2	
1	30	18	63 0.	2 15	8	282 1.1	98 5	ι.	5 ND	1	8	1	2	2	31	0,15	0.11	6	26 0.33	61	0.09	3	2.1	0.01	0.05	2	
1	29	23	53 C.	3 28	10	168 2.2	26 9		5 ND	2	11	1	2	2	46	0.17	0.05	4	54 0.39	63	0.08	2	2.42	0.01	0.04	2	
1	45	24	58 D.	3 54	13	219 2.7	78 7		5 ND	2	17	1	2	3	58	0.21	0.03	3	50 0.88	65	0.07	2	2.63	0.01	0.03	2	
1	21	16	75 0.	1 45	13	314 2.1	98 7		5 ND	2	9	1	2	3	60	0.22	0.03	3	62 0.58	56	0.1	2	2.39	0.02	0.05	2	
1	21	18	74 0.						5 ND	2	10	1	2	2		0.24	0.02	2	80 0.58	52	0.09		2.24		0.05	2	
1	15	8	44 0.						5 ND	5	4	1	2	2		0.04	0.02	13	98 0.22	82	0.03		1.38	0.01		2	
1	19	15	58 0.			320 1.			5 ND	4	8	1	2	2		0.07	0.04	12	11 0.28	79	0.08		1,55	0.01		2	
1	18	18	83 0.			597 1.3			5 ND	5	8	1	2	2		0.06	0.07	16	9 0.2		0.11		2.21		0.1	2	
1	29		116 0.			399 1.6			5 ND	5 7	10	1	2	2		0.08	0.05	6	9 0.23	110	0.12		2.4	0.01		2	
2	25 33	18 23	60 Q. 94 Q.			462 1 450 2.2			5 ND 5 ND		6 10	1	2	2		0.05	0.03	¥ 5	13 0.32 15 0.42	90	0.07		1.86	0.01 0.02		2	
2	.33 18	19	60 D.			239 2.0			5 ND	2	8	1	ź	2		0.07	0.11	3	10 0.18	41	0.14		1.54	0.02		ź	
f	86	15	71 0						5 ND	5	7	1	2	2		0.07	0.13	2	9 0.18	50	0.14		3.13	0.02		2	
2	86	15	65 0.						5 ND	3	8	1	2	2		0.07	0.13	2	7 0.15	55	0.14		2.84	0.02		2	
2	173	16	77 0.			445 3,2			5 ND	3	7	•	2	2	87	0.22			13 0.52	72	0.12		2.32	0.03		2	
2	103	18	93 0			758 2.5			S ND	ž	7	ŕ	ž	2	55	0.1	0.12	2	12 0.28	81	0.14		2.72	0.02		2	
2	270	20				461 3 (5 ND	ž	8	t	5	2	75	0,14	0.11	- - -	16 0.5	59	0.12	10	2.3	0.02		2	
5	80		105 0.						5 ND	3	7	1	2	2	49	0.1	0.08	3	9 0.23	70	0.14		1.93	0.02		2	
1	60	17	77 0.						5 ND	3	8	ł	2	2	40	0.11	0.11	3	11 0.28	46	0.13		2.29	0.02		2	
, i	96	18	85 0.						5 ND	2	9	1	ž	2	40	0.11	0.11	2	11 0.24	57	0.14		2.91		0.04	2	
2	30		133 0	2 22	9				5 ND	5	11	1	2	2		0.13	0.09	7	24 0.87	90	0.16		2.7		0.1	2	
2	32	34	84 D.		- 4	188 2.6	54 6		5 ND	z	6	1	2	2	50	0.07	0.08	7	15 0.3	46	0.15	5	1.89	0.01	0.05	2	
2	19	25	108 0.	1 17	8				5 ND	2	6	f	2	2		0.07	0.08	7	15 0.3	57	0.13		1.98	0.01		2	
1	37		127 0						5 ND	4	6	t	2	3		0.07	0.09	8	14 0.47	75	0.13		2.61	0.01		2	
2	20	58	144 0.	1 21	7	689 2.4	12 5		5 ND	3	9	1	2	2	32	0.09	0.15	5	9 0.2	74	0.15	7	3.42	0.02	0.04	2	
2	13	34	157 0.	3 14	6	737 1.6	81 3		5 ND	3	6	t	2	Ż	26	0.06	0.09	5	11 0.39	64	0.1	- 4	2.23	0.01	0.04	2	
1	16	21	132 0.	1 17	5	702 2.3	38 5		5 ND	3	6	1	2	2		0.08	0.11	8	21 0.61	77	0.18	-	2.65	0.01		2	
1	22		100 0.	1 16	6				5 ND	5	5	1	2	2	42	0.07	0.09	8	20 0.46	54	0.13		2.6	0.01		2	
1	23		123 0.		6				5 ND	4	7	1	2	2	34	0.1	0.09	8	22 0.52	77	0.12		2.15	0.01		2	
1	15	26	90 0.						5 ND	3	6	5	2	2	34	0.08	0.06	8	18 0.62	61	0.11		1.66	0.01		2	
2	19	15	94 0.						5 ND	- 4	6	1	Ż	2	29	0.05	0.11	7	9 0.32	82	0.14	5	3	0.02		3	
2	107	18	86 0.			527 2			5 ND	2	8	1	2	2		0.12	0.1	6	12 0.29		0.14		2.47	0.02		2	
1	22	12	50 0.	2 10	4	786 1	.7 3		5 ND	2	7	1	2	2	43	0.07	0.1	4	7 0.18	57	0.11	2	1.69	0.62	0.03	2	

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2	17	12		0.2	15		374 2.			ND	8	8	-	2	2		0.07		-	18 0.59	75	0.12		2.01		0.06	2
3	24			0.2	18	8	509 2.			5 ND	- 4	7	1	2	2	34	0.08	0.14	7	22 0.43	55	0.1		2.38	0.01	0.04	2
1	11	20	35	0.2	5	2	183 1.	82 :	2 3	ND	3	- 4	1	2	2	35	0.03	0.08	- 4	7 0.07	43	0.11	2	2.05	0.01	Q.01	2
2	44	18	61	0.1	13	8	511 2.	53 :	B :	S ND	3	6	1	2	2	42	0.05	0.11	5	9 0,14	54	0.14	6	3.45	0.02	0.02	2
2	58	17	93	0.2	17	12	1088 2.	82	8 :	ND	3	8	1	2	2	66	0.16	0.11	5	10 0.32	60	0.13	3	2.15	0.02	0.04	2
1	32	18	64	0.4	12	8	772 2			ND	3	9	1	2	2	40	0.12	0.12	5	8 0.15	48	0.13			0.02		2
3	85	17		0.3	18		1095 2.			ND	3	å	i	2	2	63	0.12	0.1	ě	15 0.37	50	0.11	3	1.9	0.02	0.04	2
ĭ	35	11		0.4	8	8	135 1.			ND	ž	6	i	2	2	25	0.04	0.12	5	4 0.11	50	0.14	3	3.47	0.02	0.02	
					-						-	-		_	-												2
1	47	16		0.3	11	8	143 2			ND	5	6	1	2	2	27	0.05	0.12	9	9 0.28	53	0.1		3.24	0.02	0.04	2
1	61	17		0.4	11	12	228 2.			S ND	3	6	1	2	2	- 44	0.08	0.13	7	12 0.24	73	0.12		2.77	0.02	0.04	2
1	50	19		0.4	8	6	318 3.			ND	- 4	5	1	3	2	53	0.05	0.21	5	10 0.22	58	0.15	5	2.7	0.01	0.04	2
1	43	15		0.4	11	15	414 2) (ND .	- 4	6	1	2	2	38	0.05	0.16	8	9 0.25	58	0.11	6	3.23	0.02	0.04	2
1	31	13	45	0.2	14	18	302 2	62 🛛	5 5	ND .	5	6	ş	2	2	28	0.05	0.13	8	10 0.24	61	0.11	8	3.91	0.02	0.03	2
1	44	18	46	0.2	18	12	216 2	94 1		ND	7	3	\$	2	2	32	0.03	0.06	16	12 0.87	76	0.04	3	2.09	0.01	0.04	2
1	21	19	35	0.1	11	8	147 2.	37 i	8 8	i ND	8	5	1	2	2	26	0.03	0.11	16	8 D.4	66	0.09	4	2.8	0.01	0.04	2
t	22	15		0.2	13	15	120 2			ND	8	7	ŧ	2	2	24	0.04	0.13	5	6 0.15	47	0.13		3.77	0.02	0.03	2
1	18	15		0.3	13		281 2.			ND	6	8	ŕ	2	2	26	0.05	0.2	5	8 0,18	71	0.15		3.12	0.02	0.04	2
ŝ	17	14		0.4	14		135 2			ND	8	8	ŕ	2	2		0.04	0.27	ž	11 0.28	84	0.13		3.32	0.02	0.04	2
3	22	18		0.2	21	-	193 4.			ND	10	10	÷	2	ź		0.05	0.19	8	14 0.8	106	0.05		1.95	0.02		
													;													0.05	2
3	22	12	33		18	11	110 3.			ND	11	5	1	2	2		0.02	0.09	11	13 0.87	84	0.04		1.98	0.01	0.04	2
2	22	21		0.1	21	11	381 4.			ND	10	12	1	2	2		0.05	0.27	11	17 0.93	101	0.07		2.51	0.01	0.06	2
3	22	21	44	0.2	21	11	340 4.		3	ND	10	12	1	2	2	29	0.05	0.29	10	17 0.9	96	0.07	- 5	2,68	0.01	0.06	2
1	21	15	30	0.1	17	9	90 2.	63 1	3 5	ND	7	9	1	2	2	26	0.06	0.23	4	9 0,24	59	0.15	5	4.49	0.02	0.03	2
1	26	22	63	0.1	28	17	243 4	92 13	7 5	ND	12	11	1	3	Ż	31	0.04	0.32	17	18 0.73	87	0.08	8	2.83	0.01	0.06	2
1	24	20	54	0.1	24	18	264 3.:	58 13	3 5	ND	10	9	f	2	2	26	0.04	0.11	17	14 0.73	96	0.06		2.9	0.01	0.06	2
1	28	15	46	0.1	17	10	138 2.	59 1		ND	9	5	1	2	2		0.03	0.03	15	14 0.4	84	0.09		2.69		0.05	2
1	21	15	44	0.1	14		112 3			ND	10	5	1	2	2	23	0.02	0.03	22	16 0.45	48	0.04		1.94		0.05	2
÷	19	15		0.2	12		146 3.			ND	17	ă.	÷	2	2	27	0.02	0.04	18	14 0.35	48	0.05		1.99		0.04	2
÷	21	18	42		15	-					9	2	1	2	2	23	0.02	0.04	22	13 0.43	52				0.01		
•						-	148 3.			ND			•									0.04		1.99		0.04	2
1	16	19		0.1	14		143 2.			ND	7	4	1	3	2	27	0.03	0.05	15	12 0.3	56	0.07		2.48	0.01	0.05	2
1	19	14		0.2	16		296 2.			ND	6	7	1	2	2		0.05	0.06	10	11 0.23	74	0.12		3.64		0.05	2
1	18	18	48	0.2	16	11	157 2.	83 🔅	1 5	ND .	7	8	1	2	2	28	0.04	0.07	10	14 0.25	76	0.11	7	3.84	0.01	0.05	2
1	26	19	56	0,1	17	11	120 2.	51 1) 5	ND	10	8	1	2	2	27	0.05	0.03	16	13 0.37	98	0.1	7	2.93	0.02	0.07	2
1	19	14	50	0.1	14	12	200 2.0	83 !		ND	6	7	t	2	2	29	0.05	0.05	14	13 0.3	79	0.09	5	2.65	0.01	0.05	2
ŕ	18	14	39	0.1	15		170 2.			ND	11	5	i	2	2		0.04	0.03	14	10 0.31	60	0.1		2.19	0.01	0.04	2
ł	20	14		0.2	16		215 21			ND	9	å	i	2	2	25	0.03	0.05	15	13 0.35	82	0.06		2.27	0.01	0.05	2
-	24	19		0.1	19		144 2.			ND	10	5	-	2	2	27	0.03	0.04	10	13 0.30	93	0.08		2.5	0.01	0.05	-
t												+	1														2
1	15	11		0.2	11	8	101 2.			ND	8	4	1	2	2	17	0.02	0.02	16	8 0.25	71	0.06		1.45	0.01	0.02	2
1	15	6		0.1	11	5	85 1.1			ND	9	3	1	2	2	15	0.01	0.02	19	8 0.28	43	0.03		0.98	9.01	0.02	2
1	17	12		0.2	14		177 2.0			ND	8	4	1	2	2	25	0.02	0.04	14	10 0.25	58	0.07		1.9	0.01	0.04	2
1	20	18	48	0.1	21	20	181 2	.54 1	5 5	ND	10	5	t	2	2	27	0.02	0.03	16	11 0.32	71	0.07	3	2.18 4	0.01	0.64	2
1	24	16	44	0.1	18	18	134 2.1	98 8	1 5	ND	12	5	1	2	2	26	0.02	0.05	18	11 0.35	69	0.06	4	1.94	0.01	0.04	2
1	30	15	35	0.1	15	10	221 2.1	91 S	} 5	ND	7	9	1	2	2	32	0.05	0.06	11	8 0.2	78	0.14	5	3.1	0.02	0.04	2
1	45	13		0.3	21	18	281 2.1			ND	7	6	1	2	2	42	0.04	0.05	10	10 0.42	91	0.09	6	2.68	0.01	0.05	2
•	29	14		0.2	31		728 3.			ND	5	6	1	2	2		0.03	0.04	17	14 0.55	117	0.06		2.22	0.01	0.06	2
2	26	17		0.1	15	11	145 2.0			ND	8	8	1	2	2	27	0.05	0.05	13	10 0.33	78	0.1		2.85	0.02	0.04	2
2	31	16		0.1	18		228 3.			ND	8	7	1	2	2		0.04	0.07	16	10 0.44	97	0.07		2.46	0.01	0.05	2
	62	19		0.1			590 4.3			ND	8	÷		2	2		0.05	0.07			85	0.05		2.13			-
3					18						-	-	1	_	-				14	11 0.56			_		0.01	0.05	2
2	20	19		0.2	14		825 3.			ND	3	9	1	2	2		0.09	0.1	8	9 0.24	72	0.15		3.06	0.02	0.08	2
3	17	18		0.1	22		538 2.1			ND	5	9	t	2	2		0.09	0.1	8	31 0.24	125	0.13		3.59	0.02	0.08	2
3	22	20		0.1	25		455 3.2		-	ND	10	8	1	2	2		0.03	0.07	17	10 0.35	72	0.07		2.8	0.01	0.06	2
3	25	27	64	0.1	40	83	371 3.3	33 6	6 6	NÐ	12	7	1	2	2	27	0.05	0.11	14	14 0.34	76	0.11		3.73	0,01	0.06	2
2	21	24	49	0.1	37	89	480 3.4	33 e	; e	ND	13	10	1	2	3	26	0.09	0.09	10	13 0.35	112	0.1	- 4	3.28	0.01	0.08	2
4	27	29	50	0.1	73	115	375 3.1	96 4	1 5	ND	17	7	1	2	3	22	0.04	0.08	11	12 0.33	66	0.08	2	3.3	0.01	0.08	2
4	26	28	48	0.1	71	118	451 3	9 9	, 7	ND	17	7	1	2	3	22	0.03	0.08	11	12 0.33	84	0.07	5	3.23	0.01	0.07	2
2	17	21	39	0.1	33	58	151 3.4	81 7		ND	8	9	i	2	2		0.06	0.07	14	11 0.29	122	0.08		2.55	0.01	0.07	2
ã.	43	32		0.1	80		178 8.			ND	24	9	i i	2	3		0.03	0.15	24	14 0.37	97	0.07		2.74	0.01	0.08	2
3	29	27		0.1	37		143 7.3			ND	13	11	ł	2	3		0.06	0.15	15	12 0.25	134	0.08		2.65	0.01	0.08	2
-			53									13		2	4		0.06	0.44	, S 8		123	0.13		3.03		0.08	
2	30	29			29		232 7.			ND	10		1							11 0.18					0.01		2
3	21	24	37		13		265 4			ND	17	10	1	2	2		0.03	0.25	15	9 0,18	91	0.1		2.59	0.01	0.07	2
2	18	13	27		20		155 3.2			ND	11	3	1	2	4		0.02	0.06	23	10 0.68	55	0.03		1.54	0.01	0.03	2
2	13	17	30		17		100 3.4			ND	8	7	1	2	3		0.08	0.08	17	12 0.47	83	0.08		2.27	0.01	0.06	2
2	32	18	53	6.2	9		306 5.			ND	2	5	1	2	2		0.04	0.07	7	11 0.81	34	0.15		2.7	0.01	0.04	2
2	28	17	59	0.1	15	7	367 5.3	73 5	i 5	ND	3	4	٢	2	2	117	0.03	0.09	9	11 1.38	33	0.11	3	2.48	0.01	0.04	2
2	21	13		D.1	9		232 4.2			ND	4	4	۲	2	2	72	0.03	0.05	8	13 0.51	37	0.11		2.41		0.03	2
2	28	15		0.1	8		531 4.4			ND	2	7	Ť	2	2	78	0.07	0.07	9	10 0.43	50	0.1		1.73		0.06	2
2	39	10	56		10	-	271 5.			ND	4	ś	ł	2	-		0.03	0.06	ž	7 0.58	39	0.1		2.37		0.04	2
1	3¥ 5	5			2	1					2	5	1	2	2		0.03	0.00		3 0.06	18			0.49			2
•	-	-		0.1	-		41 0.3			ND	_	+		-	-				12			0.05	_		0.02		
1	22	13		0.1	9		128 2.2			ND	3	4	1	2	2		0.04	0.04	12	9 0.48	29	0.02	_	1.04	0.01		2
2	8	8	17		5	4	73 1.			ND	4	5	1	2	2		0.05	0.03	13	6 0.22	30	0.05	_	0.49	0.01	0.04	2
2	5	5		0.1	4	3	38 1.1			ND	- 4	3	1	2	2		0.03	0.02	13	3 0.21	12	0.02		0.37	0.01	0.02	2
2	13	11	27	0.1	19	11	299 2.			ND	3	6	1	2	2		0.07	0.04	13	21 0.53	46	0.04	Ż	0.97	Q.01	0.06	2
2	61	18	59	0.2	17	9	269 4.	74 6	i 5	ND	- 4	4	1	2	2	117	0.02	0.06	8	9 1.34	44	0.09	2	2.88	0.01	0.03	2
2	203	13	68	0.t	17	20	482 8.4	43 2		ND	2	3	1	2	2	307	0.02	0.06	2	7 1.87	29	0.03	2	3.2	0.01	0.02	2
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CW-13		1 38	12 43 0		5 215 5.48	2	5 NO	24	1	22		5	11 0.75		0.11	2 1.92	0.01 0.04	2
CW-14		1 17	9 32 0	.1 9	3 108 2.43	- 4	5 ND	35	1	2 2	42 0.02 0.03	12	10 0.37	40	0.07	4 2.64	0.01 0.02	2
CW-15		1 21	12 29 0	1 11	4 114 2.51	2	5 ND	4 4	1	2 2	53 0.02 0.04	10	8 0.47	34	0.08	2 3.11	0.01 0.04	2
CW-18		1 18	10 29 0		4 102 3,06	5	5 ND	3 4	è	2 2		12	8 0.59		0.05	4 1.8	0.01 0.03	2
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CW-17		1 29	10 52 0	.1 19	10 250 4.42	5	5 ND	34	1	2 2	115 0.02 0.03	12	13 1.15		0.04	2 2.92	0.01 0.03	2
CW-18		1 17	9 31 0	1 10	4 100 3.78	8	5 ND	83	1	2 2	34 0.02 0.03	20	10 0.47	22	0.03	3 1.23	0.01 0.04	2
CW-19		1 16	12 30 0	1 8	4 102 2.78	2	5 ND	4 3	1	2 2		15	9 0.57	33	0.04	2 1.62	0.01 0.04	2
								5 4	1									
CW-20				•••••	• • • • • • •	2	5 ND		1	22		11	9 0.28		0.09	6 3.38	0.01 0.03	2
CW-21		2 12	14 28 0	.28	3 113 2.33	9	5 ND	64	1	2 2	21 0.03 0.04	10	8 0.27	35	0.07	4 1.87	0.01 0.03	2
CW-22		1 13	11 24 0	1 9	4 91 2.51	8	5 ND	7 3	1	2 2	11 0.02 0.03	15	9 0.35	16	0.02	2 0.82	0.01 0.03	2
CW-23		2 15	16 24 0	• •	3 114 4.31	12	5 ND	5 3				10	8 0.18		0.06	3 0.98		
									1	22							0.01 0.05	2
CW-24		3 31	29 37 0	.3 14	11 224 4.34	13	5 ND	4 8	1	2 2	23 0.1 0.06	18	12 0.38	36 1	0.05	4 2.52	0.01 0.05	2
CW-25		2 23	15 46 0	2 8	4 294 3.78	8	5 ND	65	1	2 2	28 0.03 0.14	10	13 0.28	46	0.1	4 3.88	0.01 0.05	2
CW-26		1 15	13 40 0		3 216 2.91	5	5 ND	3 3	÷	2 2		20	11 0.34		0.06	4 1.8	0.01 0.04	2
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CW-27		2 21	16 48 0	2 9	3 231 3.52	6	5 ND	54	1	22	23 0.03 0.12	21	12 0.37	35	0.06	4 2.15	0.01 0.08	2
CW-28		1 15	13 35 0	.1 6	4 477 2.21	5	5 ND	2 3	1	2 2	22 0.03 0.05	16	8 0.23	39 1	0.03	3 1.05	0.01 0.06	2
CW-29		2 19	23 40 0	1 9	11 594 2.87	7	5 ND	3 7	4	3 2	22 0.08 0.06	15	10 0.28		0.06	4 1.45	0.01 0.06	2
						,		• •										
CW-30		1 11	15 31 0		2 285 2.19	8	5 ND	* *	1	32		18	7 0.18		0.08	4 0.8	0.01 0.06	2
CW-31		2 18	25 45 0	2 12	6 383 3.1	5	5 ND	55	1	2 2	26 0.07 0.07	16	12 0.48	45 1	0.05	4 1.43	0.01 0.08	2
CW-32		2 21	29 51 0	2 12	4 171 5.54	14	5 NO	6 5	1	2 2	58 0.05 0.08	12	18 0.47	59 (0 13	3 1.88	0.01 0.07	2
CW-33		2 21	124 82 0	1 13	9 472 268	1	5 ND	4 6		2 2	15 0 14 0 05	18	8 0 44		0.02	4 1 25	0.01 0.06	2
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CW-34		1 14	19 26 0	37	2 38 2.45	5	5 ND	66	1	32	22 0.05 0.05	7	8 0.13	22	0.1	4 3.57	0.02 0.04	2
CW-35		1 20	26 33 0	1 13	7 156 2.98	6	5 ND	57	t	2 2	28 0.09 0.03	18	9 0.38	3B I	0.03	3 2.05	0.01 0.05	2
CW-38		2 31	98 41 0		33 717 2.75	5	5 ND	2 8	1	2 2		17	10 0.31		0.06	3 1.94	0.01 0.05	2
CW-37		1 34	573 184 0		7 201 2.69	8	5 ND	54	1	23	11 0.07 0.04	18	8 0.42		0.02	3 1.13	0.01 0.05	2
CW-38		1 37	778 247 0	4 18	9 148 3.58	7	5 ND	4 5	1	2 3	19 0.07 0.04	17	8 0.4	49 4	0.02	3 1.35	0.01 0.05	2
CW-39		1 25	278 359 0		7 153 2.27	3	5 ND	6 5		2 2	14 0.07 0.03	18	10 0.47		0.01	4 1.43	0.01 0.07	2
						-												
CW-40		1 21	107 168 0		8 349 2.62	2	5 ND	4 7	3	22	16 0,1 0.04	17	8 0.43		0.03	3 1.44	0.01 0.06	4
CW-41		1 14	50 130 0	1 16	6 264 2.28	- 4	5 ND	6 6	1	2 2	13 0.09 0.03	18	10 0.54	49 4	0.01	3 1.22	0.01 0.06	2
CW-42		1 20	73 80 0	2 10	4 97 2.72	6	5 ND	3 10	4	2 2	19 0.15 0.03	13	7 0.18	59 (0.04	3 1.51	0.01 0.03	2
						•	* • • • •									*		
CW-43		1 38	487 195 D		12 930 2.84	6	5 ND	5 9	1	22	19 0.14 0.05	13	9 0.38		0.03	3 1.62	0.01 0.06	2
CW-44		1 17	97 84 0	2 14	8 221 2.55	4	5 ND	4 9	1	2 2	18 0.12 0.03	18	8 0.45	57 (0.02	3 1.35	0.01 0.08	2
CW-45		1 21	126 81 0	5 15	14 378 3.21	5	5 ND	5 10	4	2 2	19 0.17 0.08	15	7 0.29	65 (0.02	2 1.42	0.01 0.07	2
						-												
CW-46		2 17	114 64 0		6 246 2.98	5	5 ND	48	1	22		12	9 0.37		80.0	3 1.85	0.01 0.08	2
CW-47		1 15	80 51 0	1 19	8 283 2.77	10	5 ND	11 5	1	2 2	10 0.09 0.04	28	6 0.45	53 1	D.01	3 1.23	0.01 0.05	2
CW-48		2 22	56 54 0	3 21	13 480 3.71	9	5 ND	58	1	2 2	20 0.11 0.05	15	10 0.48	86 (0.02	2 1.74	0.01 0.09	2
					5 165 2 22	2	5 ND	4 8	:	2 2	17 0.07 0.02	18	10 0.46		0.03	9 1.47		
CW-49						-			1								0.01 0.08	2
CW-50		1 15	15 48 0	1 12	6 188 2.52	4	5 ND	6 6	1	22	15 0.1 0.03	21	9 0.47	73 1	0.02	3 1.43	0.01 0.05	2
CW-51		2 13	34 29 0	1 7	2 92 2.45	4	5 ND	55	1	2 2	29 0.04 0.07	12	9 0.24	42 (80.0	4 1.81	0.01 0.04	2
CW-52		3 27	29 53 0		9 207 4.41		5 ND	8 5		2 2	29 0.05 0.1	18	13 0.63		0.04	3 1.96	0.01 0.05	2
						11			3									
CW-53	4	1 18	31 32 0	.3 9	4 295 2.29	6	5 ND	4 6	1	22	≰23 0.09 0.08	15	8 0.31	49 (0.05	4 1.12	0.01 0.05	2
CW-54		1 13	22 29 0	4 5	2 68 2.52	3	5 ND	4 5	1	2 2	21 0.05 0.07	11	6 0.14	27 (0.05	4 1.2	0.01 0.03	2
CW-55		2 19	212 58 0	9 9	3 120 2.89	2	5 ND	5 6	1	2 2	24 0.08 0.05	15	9 0.26		0.05	3 1.27	0.01 0.05	2
									•									
CW-56		1 29	522 65 0		5 178 1.96	2	5 ND	2 9	1	22		14	6 0.17		0.03	4 1.18	0.01 0.03	2
CW-57		1 21	138 92 0	5 11	5 175 3.08	3	5 NO	58	1	22	23 0.13 0.03	12	9 0.26	43 (0.07	3 1.95	0.01 0.04	2
CW-58		2 27	553 99 0	3 12	81 1659 2.28	6	5 ND	3 10	2	2 2	20 0.14 0.07	17	8 0.24	58 (0.03	4 1.5	0.01 0.05	2
CW-59		1 19	46 74 0		12 135 0.94	2	12 ND	4 13	2	2 2	11 0.27 0.14	26	9 0 33		0.01	2 1.75	0.01 0.08	2
																		-
CW-60		3 16	26 52 0		31 542 2.78	8	5 ND	28	•	22		13	9 0.29		0.05	2 1.81	0.01 0.07	2
CW-61		1 14	12 39 0	2 10	4 124 2.78	7	5 ND	7 4	1	2 2	15 0.05 0.04	18	7 0.32	- 34 (0.01	2 0.94	0.01 0.05	2
CW-62		2 24	19 42 0	3 24	8 421 2.93	9	5 ND	4 19	1	2 2	26 0.32 0.1	14	13 0 42	108 (108	2 3.49	0.02 0.1	2
		1 29			5 482 2.42	8	5 ND	5 10	1	2 2		14	10 0.34		0.04	2 1.63	0.01 0.07	2
CW-63									+									-
CW-84		2 32	185 122 0	5 16	18 579 2.84	6	5 ND	4 8	T	2 2				68 (0.03	2 1.35	0.01 0.05	2
CW-65											17 0.1 0.04	17	9 0.35					
CW-66		1 22	95 75 Û	4 14	22 585 2.23	4	5 ND	2 10	1	2 2	22 0.12 0.04	16	10 0.35	59 (3.05	3 1.38	0.01 0.08	2
						4 6				2 2	22 0.12 0.04				0.05 0.03			
		1 15	20 37 0	1 10	5 119 3.06	-	5 ND	8 4	1	2 2 2 3	22 0.12 0.04 19 0.03 0.04	16 22	10 0.35 7 0.22	40 0	0.03	4 1.19	0.01 0.05	2
CW-67		1 15 1 15	20 37 0. 30 33 0.	1 10 3 9	5 119 3.06 6 154 2.12	4	5 ND 5 ND	84 36	1	2 2 2 3 2 2	22 0.12 0.04 19 0.03 0.04 23 0.06 0.03	16 22 12	10 0.35 7 0.22 10 0.2	40 (43 (2.03 2.08	4 1.19 2 1.45	0.01 0.05 0.01 0.06	2 2
CW-67 CW-68		1 15 1 15 1 15	20 37 0. 30 33 0. 11 48 0.	1 10 3 9 1 12	5 119 3,06 6 154 2,12 8 143 2,31	-	5 ND 5 ND 5 ND	8 4 3 6 5 4	1	2 2 2 3 2 2 2 2 2 2	22 0.12 0.04 19 0.03 0.04 23 0.06 0.03 17 0.04 0.04	16 22 12 17	10 0.35 7 0.22 10 0.2 11 0.4	40 (43 (44 (0.03 0.08 0.03	4 1.19 2 1.46 2 1.77	0.01 0.05 0.01 0.06 0.01 0.05	2 2 2
CW-67		1 15 1 15	20 37 0. 30 33 0.	1 10 3 9 1 12	5 119 3,06 6 154 2,12 8 143 2,31	4	5 ND 5 ND	84 36	1	2 2 2 3 2 2	22 0.12 0.04 19 0.03 0.04 23 0.06 0.03	16 22 12	10 0.35 7 0.22 10 0.2	40 (43 (44 (2.03 2.08	4 1.19 2 1.45	0.01 0.05 0.01 0.06	2 2
CW-67 CW-68 CW-69		1 15 1 15 1 15 2 18	20 37 0. 30 33 0. 11 48 0. 102 99 0.	1 10 3 9 1 12 1 14	5 119 3.08 6 154 2.12 6 143 2.31 15 824 2.62	4	5 ND 5 ND 5 ND 5 ND	8 4 3 6 5 4 2 10	1 1 1	2 2 2 3 2 2 2 2 2 2 2 3	22 0.12 0.04 19 0.03 0.04 23 0.06 0.03 17 0.04 0.04 21 0.14 0.05	16 22 12 17 13	10 0.35 7 0.22 10 0.2 11 0.4 10 0.39	40 0 43 0 44 0 76 0	0.03 0.08 0.03 0.04	4 1.19 2 1.46 2 1.77 4 1.43	0.01 0.05 0.01 0.06 0.01 0.05 0.01 0.08	2 2 2 2
CW-67 CW-68 CW-69 CW-70		1 15 1 15 1 15 2 18 1 19	20 37 0. 30 33 0. 11 48 0. 102 99 0. 85 83 0.	1 10 3 9 1 12 1 14 2 14	5 119 3.06 6 154 2.12 8 143 2.31 15 824 2.62 7 339 3.03	4 5 4 4	5 ND 5 ND 5 ND 5 ND 5 ND 5 NO	8 4 3 6 5 4 2 10 3 11	1 1 1 1	2 2 2 3 2 2 2 2 2 2 2 3 2 2 2 3 2 2	22 0.12 0.04 19 0.03 0.04 23 0.06 0.03 17 0.04 0.04 21 0.14 0.05 31 0.16 0.05	16 22 12 17 13 14	10 0.35 7 0.22 10 0.2 11 0.4 10 0.39 12 0.34	40 (43 (44 (76 (78 (0.03 0.08 0.03 0.04 0.07	4 1.19 2 1.46 2 1.77 4 1.43 3 1.78	0.01 0.05 0.01 0.06 0.01 0.05 0.01 0.08 0.01 0.08	2 2 2 2 2
CW-67 CW-68 CW-69 CW-70 CW-71		1 15 1 15 1 15 2 18 1 19 1 18	20 37 0. 30 33 0. 11 48 0. 102 99 0. 85 83 0. 91 142 0.	1 10 3 9 1 12 1 14 2 14 1 18	5 119 3.06 6 154 2.12 8 143 2.31 15 824 2.62 7 339 3.03 7 418 2.8	4 5 4 4	5 ND 5 ND 5 ND 5 ND 5 NO 5 NO 5 ND	8 4 3 6 5 4 2 1D 3 11 4 10	1 1 1 1 1 1	2 2 2 3 2 2 2 2 2 2 2 3 2 2 2 3 2 2 2 2	22 0.12 0.04 19 0.03 0.04 23 0.06 0.03 17 0.04 0.04 21 0.14 0.05 31 0.16 0.05 27 0.15 0.04	16 22 12 17 13 14 17	10 0.35 7 0.22 10 0.2 11 0.4 10 0.39 12 0.34 12 0.46	40 (43 (44 (76 (78 (86 (0.03 0.08 0.03 0.04 0.07 0.06	4 1.19 2 1.46 2 1.77 4 1.43 3 1.78 3 1.75	0.01 0.05 0.01 0.06 0.01 0.05 0.01 0.08 0.01 0.08 0.01 0.08 0.03 0.08	2 2 2 2 2 2 2 2
CW-67 CW-68 CW-69 CW-70		1 15 1 15 1 15 2 18 1 19 1 18	20 37 0. 30 33 0. 11 48 0. 102 99 0. 85 83 0.	1 10 3 9 1 12 1 14 2 14 1 18	5 119 3.06 6 154 2.12 8 143 2.31 15 824 2.62 7 339 3.03	4 5 4 4	5 ND 5 ND 5 ND 5 ND 5 ND 5 NO	8 4 3 6 5 4 2 10 3 11	1 1 1 1 1 1	2 2 2 3 2 2 2 2 2 2 2 3 2 2 2 3 2 2	22 0.12 0.04 19 0.03 0.04 23 0.06 0.03 17 0.04 0.04 21 0.14 0.05 31 0.16 0.05	16 22 12 17 13 14	10 0.35 7 0.22 10 0.2 11 0.4 10 0.39 12 0.34	40 0 43 0 44 0 76 0 78 0 86 0	0.03 0.08 0.03 0.04 0.07	4 1.19 2 1.46 2 1.77 4 1.43 3 1.78	0.01 0.05 0.01 0.06 0.01 0.05 0.01 0.08 0.01 0.08	2 2 2 2 2
CW-67 CW-68 CW-69 CW-70 CW-71 CW-72		1 15 1 15 1 15 2 18 1 19 1 18 1 17	20 37 0. 30 33 0. 11 48 0. 102 99 0. 85 83 0. 91 142 0.	1 10 3 9 1 12 1 14 2 14 1 18 1 18	5 119 3.06 6 154 2.12 8 143 2.31 15 824 2.62 7 339 3.03 7 418 2.8	4 5 4 4	5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND	8 4 3 6 5 4 2 1D 3 11 4 10	1 1 1 1 1 1	2 2 2 3 2 2 2 2 2 2 2 3 2 2 2 3 2 2 2 2	22 0.12 0.04 19 0.03 0.04 23 0.06 0.03 17 0.04 0.04 21 0.14 0.05 31 0.16 0.05 27 0.15 0.04 31 0.04 0.04	16 22 12 17 13 14 17 28	10 0.35 7 0.22 10 0.2 11 0.4 10 0.39 12 0.34 12 0.46 11 0.97	40 0 43 0 44 0 76 0 86 0 48 0	0.03 0.08 0.03 0.03 0.04 0.07 0.06 0.01	4 1.19 2 1.46 2 1.77 4 1.43 3 1.78 3 1.75	0.01 0.05 0.01 0.06 0.01 0.05 0.01 0.08 0.01 0.08 0.01 0.08 0.03 0.08	2 2 2 2 2 2 2 2
CW-67 CW-68 CW-69 CW-70 CW-71 CW-72 CW-73		1 15 1 15 2 18 1 19 1 18 1 17 1 29	20 37 0. 30 33 0. 11 48 0. 102 99 0. 85 83 0. 91 142 0. 13 43 0. 24 48 0.	1 10 3 9 1 12 1 14 2 14 1 18 1 18 1 21	5 119 3.06 6 154 2.12 8 143 2.31 15 824 2.62 7 339 3.03 7 418 2.8 7 180 2.97 17 360 3.7	4 5 4 4 7 8	5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND	8 4 3 6 5 4 2 10 3 11 4 10 6 4 3 7	1 1 1 1 1 1 1	2 2 2 2 2 2 2 2 2 2 2 2 2 4 6	22 0.12 0.04 19 0.03 0.04 23 0.06 0.03 17 0.04 0.04 21 0.14 0.05 31 0.16 0.05 27 0.15 0.04 31 0.16 0.05 37 0.16 0.05 36 0.08 0.05	16 22 12 17 13 14 17 28 19	10 0.35 7 0.22 10 0.2 11 0.4 10 0.39 12 0.34 12 0.46 11 0.97 15 0.85	40 0 43 0 44 0 76 0 78 0 88 0 48 0 102 0	0.03 0.08 0.03 0.04 0.07 0.06 0.01 0.04	4 1.19 2 1.46 2 1.77 4 1.43 3 1.78 3 1.75 2 1.61 4 2.21	0.01 0.05 0.01 0.06 0.01 0.05 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.05 0.01 0.1	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
CW-67 CW-68 CW-69 CW-70 CW-71 CW-72 CW-73 CW-74		1 15 1 15 1 15 2 18 1 19 1 18 1 17 1 29 1 35	20 37 0. 30 33 0. 11 48 0. 102 99 0. 85 83 0. 91 142 0. 13 43 0. 24 48 0. 18 54 0.	1 10 3 9 1 12 1 14 2 14 1 18 1 21 1 24	5 119 3.06 6 154 2.12 6 143 2.31 15 824 2.62 7 339 3.03 7 418 2.8 7 180 2.97 17 360 3.7 11 350 3.9	4 5 4 4 4 2 8 5	5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND	8 4 3 6 5 4 2 10 3 11 4 10 8 4 3 7 8 10	1 1 1 1 1 1 1 1 1	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	22 0.12 0.04 19 0.03 0.04 23 0.06 0.03 17 0.04 0.04 21 0.14 0.05 31 0.16 0.05 27 0.15 0.04 31 0.04 0.04 36 0.08 0.05 27 0.13 0.07	16 22 12 17 13 14 17 28 19 23	10 0.35 7 0.22 10 0.2 11 0.4 10 0.39 12 0.34 12 0.46 11 0.97 15 0.88 14 0.9	40 0 43 0 44 0 76 0 88 0 48 0 102 0 138 0	0.03 0.08 0.03 0.04 0.07 0.06 0.01 0.04 0.03	4 1.19 2 1.46 2 1.77 4 1.43 3 1.78 3 1.75 2 1.61 4 2.21 3 2.86	0.01 0.05 0.01 0.06 0.01 0.05 0.01 0.08 0.01 0.08 0.03 0.08 0.03 0.08 0.01 0.05 0.01 0.14	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
CW-67 CW-68 CW-69 CW-70 CW-71 CW-72 CW-73		1 15 1 15 1 15 2 18 1 19 1 18 1 17 1 29 1 35	20 37 0. 30 33 0. 11 48 0. 102 99 0. 85 83 0. 91 142 0. 13 43 0. 24 48 0.	1 10 3 9 1 12 1 14 2 14 1 18 1 21 1 24	5 119 3.06 6 154 2.12 8 143 2.31 15 824 2.62 7 339 3.03 7 418 2.8 7 180 2.97 17 360 3.7	4 5 4 4 7 8	5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND	8 4 3 6 5 4 2 10 3 11 4 10 6 4 3 7	1 1 1 1 1 1 1 1 1	2 2 2 2 2 2 2 2 2 2 2 2 2 4 6	22 0.12 0.04 19 0.03 0.04 23 0.06 0.03 17 0.04 0.04 21 0.14 0.05 31 0.16 0.05 27 0.15 0.04 31 0.16 0.05 37 0.16 0.05 36 0.08 0.05	16 22 12 17 13 14 17 28 19	10 0.35 7 0.22 10 0.2 11 0.4 10 0.39 12 0.34 12 0.46 11 0.97 15 0.85	40 0 43 0 44 0 76 0 88 0 48 0 102 0 138 0	0.03 0.08 0.03 0.04 0.07 0.06 0.01 0.04	4 1.19 2 1.46 2 1.77 4 1.43 3 1.78 3 1.75 2 1.61 4 2.21	0.01 0.05 0.01 0.06 0.01 0.05 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.05 0.01 0.1	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
CW-67 CW-68 CW-69 CW-70 CW-71 CW-72 CW-73 CW-74 CB-75		1 15 1 15 1 15 2 18 1 18 1 17 1 29 1 35 1 19	20 37 D. 30 33 0. 11 48 D. 102 99 D. 88 83 0. 91 142 0. 13 43 0. 24 48 0. 18 54 0. 15 40 0.	1 10 3 9 1 12 1 14 2 14 1 18 1 21 1 24 1 15	5 119 3.08 6 154 2.12 8 143 2.31 15 824 2.62 7 339 3.03 7 418 2.8 7 180 2.97 17 360 3.9 16 2.97 17 350 3.9 9 109 2.7	4 5 4 4 4 2 8 5	5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND	8 4 3 6 5 4 2 10 3 11 4 10 8 4 3 7 8 10	1 1 1 1 1 1 1 1 1	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	22 0.12 0.04 19 0.03 0.04 23 0.06 0.03 17 0.04 9.04 21 0.14 0.05 31 0.16 0.05 27 0.15 0.04 31 0.04 0.04 36 0.08 0.05 29 0.13 0.07 24 0.02 0.03	16 22 17 13 14 17 28 19 23 18	10 0.35 7 0.22 10 0.2 11 0.4 10 0.39 12 0.34 12 0.46 11 0.97 15 0.86 14 0.9	40 0 43 0 44 0 76 0 78 0 88 0 48 0 102 0 138 0 85 0	0.03 0.08 0.03 0.04 0.07 0.06 0.01 0.04 0.03 0.03	4 1.19 2 1.45 2 1.77 4 1.43 3 1.78 3 1.75 2 1.61 4 2.21 3 2.86 2 2.06	0.01 0.05 0.01 0.06 0.01 0.05 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.05	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
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CW-67 CW-68 CW-69 CW-70 CW-71 CW-72 CW-73 CW-74 CB-75 CB-76 CB-76 CB-77 CB-78 CB-79 CB-80 CB-81 CB-81 CB-82		1 15 1 15 1 15 2 18 1 18 1 18 1 17 1 35 1 19 1 17 1 17 1 18 1 17 1 18 1 17 1 18 1 17 1 17 1 17 1 17 1 18 1 17 1 17 1 17 1 17 1 18 1 17 1 17 1 18 1 17 1 18 2 18	20 37 0. 30 33 0. 11 48 0. 102 99 0. 88 83 0. 91 142 0. 13 43 0. 15 40 0. 12 41 0. 13 47 0. 14 43 0. 10 43 0. 11 42 0. 12 41 0. 13 47 0. 14 43 0. 10 43 0. 94 42 0.	1 10 3 9 1 12 1 14 1 14 1 18 1 21 1 24 1 24 1 24 3 13 2 16 2 14 3 15 1 18 3 12 1 18 3 12 1 21	5 119 3.06 6 154 2.12 8 143 2.31 15 824 2.62 7 339 3.03 7 418 2.8 7 180 2.97 17 360 3.7 11 350 3.9 9 109 2.7 8 228 2.51 7 181 2.85 8 237 2.59 8 160 2.67 12 161 3.09 7 225 2.4 11 117 3.14	4 5 4 4 4 2 8 5 9 6 8 4 10 7 9	5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 6 ND 6 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5	8 4 3 6 2 10 3 11 6 4 10 6 4 10 6 4 10 8 4 5 7 7 5 7 5 7 5 7 5 10 4 8 6 11 4	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2 3 2 2 3 2 2 4 6 5 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	16 22 17 13 14 17 20 19 23 11 19 10 20 8 7	10 0.35 7 0.22 10 0.2 11 0.4 12 0.38 12 0.44 12 0.46 14 0.97 15 0.48 14 0.2 15 0.42 12 0.26 13 0.29 14 0.63 12 0.24 12 0.25 13 0.29 14 0.63 12 0.24	40 (43 (43 (44 (76 (78 (88 (138 (65 (65 (65 (67 (2.03 2.08 2.03 2.04 2.04 2.07 2.06 2.01 2.04 2.03 2.05 2.11 2.15 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.	4 1.19 2 1.46 2 1.77 4 1.43 3 1.76 2 1.81 4 2.21 4 2.86 2 2.06 2 2.38 2 2.07 6 3 3 3.12 2 2.4 2 2.9 2 2.47	0.01 0.05 0.01 0.06 0.01 0.05 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
CW-67 CW-68 CW-76 CW-71 CW-72 CW-73 CW-74 CB-75 CB-76 CB-76 CB-77 CB-78 CB-79 CB-80 CB-81 CB-82 CB-83 CB-83 CB-84		1 15 1 15 1 15 2 18 1 19 1 18 1 17 1 29 1 35 1 17 1 35 1 17 1 18 1 17 1 18 1 18 1 18 2 16 2 16 2 16	20 37 0 30 33 0 11 48 0 102 99 0 88 83 0 91 142 0 13 43 0 24 48 0 15 40 0 12 41 0 14 43 0 11 43 0 11 43 0 11 43 0 11 42 0 33 34 0	1 10 3 9 1 12 1 14 2 14 1 14 1 14 1 14 1 14 1 14 1 14 1 14 1 21 1 21 1 21 1 21 1 21 1 21 1 21 1 21 1 21 1 21 1 21 1 15 3 15 1 18 3 12 2 14 2 19 1 20	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4 5 4 4 4 2 8 5 9 8 8 4 10 7 9 27	5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND	8 4 3 6 2 10 3 11 4 10 6 4 5 7 6 4 5 7 6 4 8 10 9 6 11 3	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2 2 2 2 2 2 2 2 4 6 5 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	22 0.12 0.04 19 0.03 0.04 23 0.06 0.03 17 0.04 0.04 21 0.06 0.03 17 0.04 0.05 21 0.16 0.05 21 0.16 0.05 21 0.16 0.05 21 0.16 0.04 36 0.06 0.05 29 0.13 0.07 24 0.02 0.03 31 0.04 0.06 28 0.03 0.04 29 0.04 0.06 28 0.03 0.04 29 0.04 0.06 28 0.03 0.08 20 0.03 0.08 20 0.04 0.05	16 22 17 13 14 17 29 23 18 19 10 20 8 7 18	10 0.35 7 0.22 10 0.2 11 0.4 12 0.46 12 0.46 12 0.46 14 0.97 15 0.48 14 0.2 15 0.42 12 0.46 13 0.29 14 0.63 12 0.24 16 0.63 15 0.89	40 (43 (43 (76 (76 (76 (76 (76 (138 (65 (65 (70 (67 (0.03 0.08 0.08 0.03 0.04 0.07 0.06 0.01 0.04 0.03 0.05 0.1 0.09 0.05 0.11 0.09 0.05 0.11 0.05 0.11 0.05 0.01	4 1.19 2 1.46 2 1.77 4 1.43 3 1.76 3 1.75 2 1.61 4 2.21 3 2.66 2 2.38 2 2.07 6 3 3 3.12 2 2.4 2 2.4 2 2.4 2 2.49 2 2.48	0.01 0.05 0.01 0.06 0.01 0.05 0.01 0.06 0.01 0.08 0.01 0.08 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.04	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
CW-67 CW-68 CW-69 CW-70 CW-72 CW-72 CW-73 CW-74 CB-75 CB-76 CB-76 CB-76 CB-76 CB-76 CB-78 CB-81 CB-81 CB-81 CB-82 CB-83 CB-84 CB-85		1 15 1 15 1 15 2 18 1 15 1 18 1 17 1 35 1 19 1 18 1 17 1 18 1 17 1 18 1 17 1 18 2 16 2 16 3 19 2 16 3 19 1 17 1 21 1 3 2 16 3 19 2 17	20 37 0 30 33 0 31 48 0 85 83 0 98 0 99 91 142 0 13 43 0 15 40 0 12 41 0 13 47 0 14 43 0 10 43 0 11 42 0 13 34 0 13 34 0 13 34 0 10 34 0 10 34 0 10 34 0 12 38 0	1 10 3 9 1 12 1 14 2 14 1 14 1 14 1 14 1 14 1 14 1 14 1 14 1 21 1 24 1 18 3 15 3 15 1 18 3 15 1 18 3 15 1 18 3 15 1 18 3 12 1 18 1 21 1 20 2 20	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	4 5 4 4 2 8 5 9 8 8 4 10 7 9 27 12 10	5 ND 5 ND	8 4 3 6 2 10 3 11 6 4 3 10 8 4 5 7 6 4 5 7 7 6 8 4 10 4 11 3 12 3 10 5	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2 3 2 2 3 2 2 4 8 5 4 4 2 2 7 2 2 7 2 2 7 2 2 7 2 2 7 2 2 7 2 2 7 2 2 7 2 2 7 2	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	16 22 17 13 14 17 28 19 23 18 11 19 10 20 8 17 18 20 15	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	40 (43 (43 (44 (76 (76 (76 (136 (65 (65 (70 (67 (67 (67 (67 (70 (67 (70 (70))))))))))))))))))))))))))))))))))))	0.03 0.08 0.03 0.03 0.04 0.07 0.06 0.01 0.05 0.11 0.05 0.11 0.05 0.11 0.05 0.11 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.05 0.05 0.01 0.05 0.05 0.05 0.05 0.01 0.05 0.05 0.01 0.05	4 1.19 2 1.46 2 1.77 4 1.43 3 1.78 3 1.75 2 1.61 4 2.21 3 2.56 2 2.06 2 2.06 2 2.06 2 2.06 2 2.06 2 2.07 6 3 3 3.12 2 2.4 2 2.4 2 2.47 2 2.48 2 2.24 2 2.25	0.01 0.05 0.01 0.06 0.01 0.05 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
CW-67 CW-68 CW-76 CW-71 CW-72 CW-73 CW-74 CB-75 CB-76 CB-76 CB-77 CB-78 CB-79 CB-80 CB-81 CB-82 CB-83 CB-83 CB-84		1 15 1 15 1 15 2 18 1 15 1 15 1 18 1 17 1 29 1 35 1 19 1 18 1 197 1 18 1 19 1 18 1 18 2 16 4 26 3 19	20 37 C 30 33 O 11 48 C 102 99 O 85 83 O 91 142 O 13 43 O 14 60 C 15 40 C 12 41 O 13 47 O 14 43 C 10 43 C 14 43 C 14 43 C 15 47 C 14 43 C 10 43 O 11 42 O 9 42 O 13 34 O 10 34 O	1 10 3 9 1 12 1 14 2 14 1 14 1 14 1 14 1 14 1 14 1 14 1 14 1 21 1 24 1 18 3 15 3 15 1 18 3 15 1 18 3 15 1 18 3 15 1 18 3 12 1 18 1 21 1 20 2 20	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4 5 4 4 4 2 8 5 9 8 8 4 10 0 7 9 27 12	5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND 5 ND	8 4 3 6 2 10 3 11 4 10 6 4 7 5 7 5 10 4 8 10 9 4 5 5 7 5 10 4 11 3 312 3	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2 2 2 2 2 2 2 2 4 8 5 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	16 22 17 13 14 17 28 11 19 20 8 11 10 20 8 7 18 20	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	40 (43 (43 (44 (76 (76 (76 (136 (65 (65 (70 (67 (67 (67 (67 (67 (70 (70))))))))))))))))))))))))))))))))))))	0.03 0.08 0.08 0.03 0.04 0.07 0.06 0.01 0.03 0.05 0.1 0.09 0.05 0.11 0.09 0.05 0.11 0.09 0.05 0.11 0.09 0.05 0.11 0.09 0.05 0.11 0.09 0.05 0.11 0.09 0.05 0.11 0.09 0.05 0.11 0.09 0.05 0.11 0.09 0.05 0.11 0.09 0.05 0.11 0.09 0.05 0.11 0.09 0.05 0.11 0.09 0.05 0.11 0.09 0.05 0.11 0.09 0.05 0.11 0.05 0.11 0.05 0.11 0.09 0.05 0.11 0.05 0.02 0.04 0.05 0.11 0.05 0.02 0.04 0.05 0.05 0.11 0.05 0.02 0.04 0.05 0.05 0.05 0.02 0.04 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.02 0.04 0.05 0.05 0.05 0.05 0.02 0.04 0.05 0.02 0.04 0.05 0.02 0.04 0.05 0.02 0.04 0.05 0.02 0.04 0.05 0.02 0.04 0.05 0.02 0.04 0.05 0.02 0.04 0.04 0.05 0.02 0.04 0.04 0.04 0.05 0.04 0.04 0.04 0.05 0.04 0.04 0.05 0.04 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0	4 1.19 2 1.46 2 1.77 4 1.43 3 1.78 3 1.78 3 1.78 3 1.78 3 1.78 3 1.78 3 1.78 2 1.81 4 2.21 2 2.08 2 2.08 2 2.08 3 3 3.12 2 2.4 2 2.9 2 2.47 2 2.47 2 2.9 2 2.47 2 2.9	0.01 0.05 0.01 0.06 0.01 0.06 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.08 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

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	CB-87			2	21	18	49	0.1	21	10 146 3.43	8	6 ND	11	6	•	2	2	27 0.0	0.07	14	16 0.82	50	0.07	3 2 8	0.05	0,06	2	
	CB-88			3	20	12		0.1	16	5 108 3.52	11	5 ND	, i 8	6	t	3	5	27 0.0		13	14 0.45	54	0.08	3 3.31		0.05	2	
	CB-89			2	21	17		0.1	26	13 146 3.09	9	5 ND	11	8	÷	2	2	21 0.0	0.07	20	18 0.72	84	0.06	2 2.44		0.04	2	
	CB-90			2	21	11		0.1	17	8 149 3.21	7	5 ND	9	6	1	2	3	27 0.0		14	16 0.59	51	0.08	2 3.12		0.06	2	
	CB-91			3	23	14	43	0.1	11	3 113 4.21	6	5 ND	6	5	1	5	2	38 0.0	03 0.13	9	20 0.3	44	0.13	4 4.83		0.05	2	
	CH-92			1	33	12	47	0.1	15	5 159 2.82	5	5 ND	8	3	1	2	2	30 0.0	05 0.04	14	17 0.44	58	0.09	3 1.55	0.01		ż	
	CH-93			1	55	16	60	0.1	16	7 294 2.95	6	5 ND	6	8	5	2	3	51 0	1 0.07	15	19 0.48	77	0.11	3 1.85	0.01	0.18	2	
	CH-94			1	34	11		0.2	16	7 235 2.38	5	5 ND	5	5	t	2	3	32 0.0		12	15 0.36	78	0.11	3 2.27		0,16	2	
	CH-95			1	40	20		0.2	15	6 278 2.4	6	5 ND	5	4	1	2	2	37 0.0		12	20 0.48	59	0.08	3 1.82	0.01		2	
	CH-96			3	29	11		0.1	7	3 293 2.02	5	5 ND	3	5	1	3	2	33 0.0		7	10 0.09	34	0.15	3 4.72		0.03	2	
	CH-87			3	17	10		0.1	6	1 172 2.23	6	5 ND	2	3	1	3	2	33 0.0		8	13 0.07	26	0.12	4 4.64		0.03	2	
	CH-98			2	19	13	27	0.1	6	1 91 1.97	3	5 ND	2	4	1	2	2	34 0.0		8	9 0.08	35	0.18	4 3.92		0.03	2	
	CH-99			1	39	30	40 70	0.3	8	4 153 2.14	5 5	5 ND	5	1	1	2	2	30 0.0		14 9	11 0.16	68	0.06	3 2.55		0.05	2	
	CH-100 CH-101			1	26 29	23 25		0.2 0.2	11 10	10 521 2.04 5 115 2.37	7	5 ND 5 ND	6	3	1	2 3	2 2	31 0.0		11	13 0.21 10 0.14	68 61	0.11	3 3.59 3 3.14		0.05	2 2	
	CH-101			1	20	11	27	0.2	5	2 228 1.86		5 ND	2	5	1	2	2	25 D.0		5	8 0.09	28	0.12	4 4.94	0.01		2	
	CH-103			1	29	22	50	D.1	11	6 141 2.32	ž	5 ND	5	Ĩ.	1	2	2	29 0.0		10	12 0.21	56	0.07	3 2.9	0.01		2	
	CH-104			ŕ	23	12	50	0.1		6 382 1.78		5 ND	3	5	i	3	2	24 0.0		8	10 0.15	62	D.12	3 4.24	0.02		2	
	CH-105			1	22	14	35	0.1	7	3 208 2.33	2	5 ND	- Ă	4	i	3	2	32 0.0		7	13 0.12	32	0.12	5 4,72	0.01		2	
	CH-106			1	23	16	48	0.1	8	3 241 2.39	2	5 ND	4	4	1	2	2	35 0.0	4 0.18	10	14 0.22	42	0.11	3 3.61	0.01		2	
	CH-107			1	27	17	41	0.1	8	5 143 2.2	4	5 ND	3	4	1	2	2	38 0.6	3 0.07	11	13 0.22	58	0.12	3 2.7	0.01	0.04	2	
	CH-108			1	26	33	40	0.2	6	2 129 1.99	- 4	5 ND	2	4	1	2	2	34 0.0	03 0.16	8	11 0.13	38	0.13	3 3.96	0.01	0.03	2	
	CH-109			1	22	14	43	0,1	9	4 121 2.03	2	5 ND	5	3	1	2	2	22 0.0	03 0.04	15	12 0.24	84	0.03	2 1.82	0.01	0.05	2	
	CH-110			1	65	48	49	0.1	14	8 282 2.82	8	5 ND	8	4	1	2	2	35 0.0		15	21 0.41	123	0.04	2 1.66	0.01		2	
	CH-111			1	19	12		0.1	5	2 190 1.67	4	5 ND	2	3	1	2	2	35 0.0		6	10 0.1	52	0.08	3 2.59	0.01		2	
	CH-112			2	24	- 51	23	0.2	5	4 225 1.51	5	5 ND	2	8	1	2	2	27 0.0		8	6 0.09	38	0.12	4 3.91		0.02	2	
	CH-113			1	35	15		0.1	11	5 268 2.13	2	5 ND	2	4	1	2	2	46 0.0		10	16 0.37	78	80.0	3 1.7	0.01		2	
	CH-114			1	39	12		0.2	12	6 274 2.15 9 377 2.82	3	5 ND	4	5	1	2	2	45 0.0		10	16 0.33	82	0.07	2 2.08	0.01		2	
	CH-115			2	73 15	35 14		0.1 0.1	18 12	9 377 2.82 6 178 2.09	8 3	5 ND 5 ND	3	6 5	1	2	2	74 0.1		9 18	12 0.48 10 0.44	86 73	0.11	3 2.54	0.01		2	
	CH-116 CH-117			1	12	55		0.2	12	5 363 2.35	5	5 ND	2	э 9	1	2	2	25 0.1		10	10 0.44	73	0.02	3 1.42 3 1.64	0.01		2 2	
	CH-118			3	20	50 16		0.2	11 15	7 148 2.72	7	5 ND	7	6	1	2	2	25 0.0		12	10 0.3	73 51	0.08	3 1.04 4 3.15	0.01		2	
	CH-119			1	78	40		0.1	18	7 393 3.39	12	5 ND	6	Ă	i	2	2	38 0.0		17	23 0.43	134	0.04	3 2.02	0.01		2	
	8P-1			2	46	15		0.2	15	10 266 2.65	4	5 ND	ě.	6	ł	2	2	70 0.0		10	8 0.61	58	0.08	4 2.38		0.05	2	
	BP-2			1	70	19		0.1	19	12 249 3.72	ė	5 ND	5	ž	1	2	2	98 0,1		11	7 1.19	43	0.08	2 2.2		0.03	2	
	BP-3			1	31	16		0.1	15	10 285 2.6	7	5 ND	3	2	1	2	2	58 0.1			10 0.53	45	0.08	4 2.47		0.04	2	
	BP-4			2	21	18	27	0.1	44	21 873 3.71	13	5 ND	16	14	1	2	3	50 0.2	2 0.05	32	34 1.22	43	0.01	3 2.11		0.05	2	
	BP-5			1	29	20	42	0.1	18	9 380 2.23	11	5 ND	4	14	1	2	2	39 0.2	7 0.04	13	15 0.65	41	0.05	2 1.26	0.01	0.07	2	
	BP-6			1	30	22		0.3	19	7 472 1.87	8	5 ND		17	1	2		36 0.3		15	22 06	59	0.05	2 1.48		0.07	2	
	8W-7			1	14	19		0.1	11	42 831 2.53	5	5 ND	2	7	1	2		25 0.0		12	10 0.68	58	0.04	4 1.16		0.06	2	
	BW-8			1	12	15		0.1	8	5 147 2.05	- 4	5 ND	2	7	1	2		32 0.0		11	10 0.47	37	0.04	4 0.89	0.01		2	
	BW-9			1	11	18		0.2	11	34 6,2 1.87	3	5 ND	2	9	1	2	2	16 0.1		12	8 0.51	55	0.01	3 1.13		0.05	2	
	BW-10			1	17	24 12		0.1 0.1	10 9	15 2645 2.94 6 170 3.37	25	5 ND 5 ND	2	8 ∡	1	2		187 0.0 30 0.0		8 26	7 1.61	119 32	0.08	4 1.83 4 1.1		0.07 0.03	2	
	BW-11 BW-12			1	14	23		0.1	э 9	3 592 3.36	5	5 ND	3	5	1	2	2	44 0.0		13	7 0.27	3∠ 46	0.09	4 1.1 14 1.88		0.03	2	
	BW-12			2	40	603			25	25 494 4.66	7	5 ND	5	5	•	2	3	19 0.0		12	9 0.57	59	0.02	6 1.97	0.01		2	
	BW-14			3	30	358		0.2	23	23 905 5.33	10	5 ND	7	6	ì	2	ž	18 0.0		13	10 0.53	59	0.02	4 1.41	0.01		2	
	BW-15			1	11	27		0.1	9	5 655 1.92	- 4	5 ND	2 .	10	1	ž	2	18 0.1		15	\$ 0.33	80	0.03	4 0.95		0.07	2	
	BB-16			3	14	56	19	0.3	21	16 120 5.4	24	5 ND	2	8	1	3	5	16 0.0	3 0.05	7	14 2.34	13	0.01	5 1.77	0.01	0.05	2	
	BB-17			4	52	38	31	0.2	15	11 192 20	35	13 ND	52	74	1	2	4	33 0.0	M 0.87	27	9 0.13	261	0.07	2 1.98	0.01	0,18	2	
	8H-18			t	307	13		0.1	18	20 789 9.16	2	5 ND		19	1	2		288 0.1		17	6 0.95	155	0.25	2 3,24	0.01		2	
	8P-19			t	292	42		0.1	41	47 1029 5.6	7	5 ND		9	1	2		82 0.0		9	8 0.16	26	0.01	5 0.77	0.01		2	
	BW-20			\$	8	7	34	0,1	9	2 195 2.33	2	5 ND	5	1	1	2	2	7 0.0	1 0.01	12	6 0.45	12	0.01	2 0.82	0.01	0.04	2	
190N	570E	566061	5473092	•	44	27	59		46	15 141 3.09	8	5 ND		12	1	13	2	25 0.1	5 0.1	24	13 0.24	89	0.04	5 1.41	0.01		16 ND	
190N	590E	566081	5473092	3	14	18		0.4 0.1	15 10	4 97 2.53	2	5 ND		4	1	13		25 0.1		13	15 0.24		0.04	5 2.23	0.01		5 ND	
190N	610E	566101	5473092	2	ē	18		01	8	3 86 2.79	2	5 ND		3	i	2		32 0.0		22	15 0.22		0.08	5 1.25	0.01		8 ND	
190N	630E	566121	5473092	2	13			0.4	10	4 91 2.15	2	5 ND		8	1	3		23 0.0		12	13 0.18		0.08	5 1.9	0.01		6 ND	
190N	650E	566141	5473092	1	51	100	151	0.7	10	4 117 4.5	8	5 ND		7	٢	2		5t 0.		11	13 0.28	68	0.14	5 1.17	0.01		3 ND	
190N	870E	566161	5473092	3	12	43		0.2	13	6 132 2.52	5	5 ND		8	1	5		31 0.0		22	16 0.31	64	0.07	5 1.47	0.01		6 ND	
190N	690E	566181	5473092	1	7	1		0.4	4	1 114 1.95	2	5 ND		5	1	2		27 0.0		2	9 0.07	38	0.09	5 2.01	0.01		1 ND	
190N	710E	566201	5473092	2	16	8		0.1	9	3 84 2.97	3	5 ND		5	1	2		52 0.0		19	13 0.35	40	0.12	5 1.15	0.01		1 ND	
190N	730E	566221	5473092	1	14	3		0.1	8	1 80 2.12	2	5 ND		5	1	10		30 0.0		2	12 0.11	23	0.14	5 4.09	0.01		1 ND	
190N	750E	566241	5473092	2	12	10	•••	0.1	8	1 116 3.53	3	5 ND		3	1	2		39 0.0		15	17 0.28	33	0.08	5 2.75	0.01		1 ND	
210N 210N	550E 570E	566041 568061	5473112 5473112	1 2	15 11	19 1		0.1	18 -4	16 764 2.37	5 3	5 ND 5 ND		10 5	1	4		23 0.2 27 0.0		25	14 0.38 9 0.08	114 3B	0.05	5 2.09 5 3.58	0.01		1 ND 1 ND	
210N	570E 590E	566081	5473112 5473112	2	10	27		0.3	8	1 54 2.2	5	5 ND		5	1	11		39 0.0		7	20 0.13	30 49	0.12	5 3,56	0.01		2 ND	
210N	610E	586101	5473112	2	8	14		0.1	6	2 52 2.48	2	5 ND		4	i	2		32 0.0		8	11 0.13		0.07	5 1.93	0.01		2 ND	
210N	630E	586121	5473112	ĩ	5	1		0.1	š	1 83 3.42	2	5 ND		á.	i	2		27 0.0		10	12 0.32		0.07	5 1.67	0.01		1 ND	
210N	850E	586141	5473112	1	24	273		0.5	8	3 133 2.63	2	5 ND		7	•	2		16 0.1		18	9 0.48	32	0.01	5 1.37	0.01		1 ND	
210N	670E	566161	5473112	1	9	62		0.1	6	3 85 1,52	2	5 ND		8	1	2		29 0.0		18	10 0.12	50	0.06	5 0.63	0.01		1 ND	
210N	690E	566181	5473112	1	8	8	50	0.1	4	1 103 1.8	2	5 ND		3	1	2		26 0.0		14	8 0.16		0.08	5 1.37	0.01		1 ND	
210N	710E	566201	5473112	1	12	18		0.1	6	3 158 3.57	4	5 ND		5	1	2		43 0.0		8	13 0.19	58	0.13	5 2.08	0.01		1 ND	
210N	730E	566221	5473112	2	13	24	37	0.1	7	3 74 2.96	5	5 ND		5	1	6	2	43 0.0	4 0.08	5	15 0.14	32	0.16	5 2,73	0.01		1 ND	

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210N	750E	566241 5473112	3 10 34 33	0.3 8 6 350 1.5	3 8 5 ND	3 1	7	37 0.02 0.05 13 13 0.09 43 0.1 5 1.19 0.01 7 ND 5	5 0.03 1
230N	550E	566041 5473132	4 29 47 102	0.4 21 14 1891 2.9	8 15 5 ND	18 2	13	38 0.81 0.11 30 20 0.43 180 0.07 5 2.93 0.01 9 ND 5	5 0.02 2
230N	570E	566061 5473132	2 13 21 51	0.4 10 6 101 2.1	8 9 5 ND	8 1	2	27 0.16 0.04 16 14 0.26 142 0.02 5 1.35 0.01 5 ND 5	5 0 02 1
230N	590E	566081 5473132	2 14 24 85	0.5 17 10 231 3.5	3 8 5 ND	9 1	2	40 0.12 0.06 16 18 0.42 98 0.07 5 1.78 0.01 4 ND 5	5 0.02 2
230N	610E	566101 5473132	2 13 36 93			8 2	2	30 0.12 0.04 19 18 0.42 101 0.05 5 1.79 0.01 3 ND 5	5 0.02 2
230N	630E	566121 5473132	3 16 34 49			6 3		28 0.05 0.04 8 14 0.12 48 0.11 5 3.44 0.01 8 ND 5	5 0.04 2
230N	650E	566141 5473132	2 40 608 340			11 3	2	25 0.18 0.06 27 16 0.37 67 0.04 5 1.81 0.01 5 ND 5	5 0.02 2
230N	670E	566181 5473132	3 22 211 143				-	32 0.08 0.04 20 15 0.19 73 0.05 5 1.28 0.01 8 ND 90	90 0.03 1
230N	690E	566161 5473132	4 37 110 58					37 0.04 0.06 30 15 0.18 49 0.05 5 1.15 0.01 8 ND 810	
230N	710E	566201 5473132					-	32 0,06 0,08 21 18 0,22 78 0,06 52,12 0,01 10 ND 40	
		566221 5473132				• •			40 0.05 2
230N	730E	586241 5473132	3 18 55 48			6 1 7 1			20 0.01 1
230N	750E		2 15 15 44						10 0.02 2
250N	570E	566061 5473152	1 7 1 34			5 1	-	18 0.07 0.03 21 10 0.21 80 0.02 5 1.14 0.01 2 ND 5	5 0.02 1
250N	590E	566081 5473152	1 7 10 51			4 1		24 0.04 0.06 19 11 0.26 63 0.03 5 1.03 0.01 1 ND 50	50 0.02 t
250N	610E	566101 5473152	2 8 11 48			6 1		24 0.08 0.03 17 13 0.32 87 0.04 5 1.28 0.01 1 ND 10	10 0.02 1
250N	630E	566121 5473152	2 11 9 71			5 1		16 0.06 0.07 22 12 0.38 76 0.02 5 1.45 0.01 1 ND 30	30 0.02 1
250N	650E	566141 5473152	2 28 577 279			11 1	2		10 0.02 1
250N	670E	566181 5473152	1 25 312 175			13 2	2		40 0.02 2
250N	690E	566181 5473152	3 38 561 225			7 2		29 0.11 0.07 16 13 0.36 87 0.03 5 1.57 0.01 1 ND 190	190 0.02 2
250N	710E	566201 5473152	2 15 63 70	0.5 9 5 183 3.3		4 1	2	38 0.04 0.09 21 11 0.18 44 0.08 5 0.97 0.01 1 ND 170	170 0.02 1
250N	730E	566221 5473152	2 10 13 42	0.2 10 8 151 2,1		6 1	2	23 0,06 0,04 23 12 0.31 42 0.04 5 0.82 0,01 1 ND 30	30 0.02 1
250N	750E	566241 5473152	3 12 32 53	0.1 12 7 188 3.8	8 10 5 ND	5 1	6	44 0.04 0.15 18 19 0.26 52 0.12 5 1.93 0.01 4 ND 10	10 0.02 2
270N	550E	566041 5473172	2 14 12 85	0.1 11 6 534 1.		13 1	2	22 0.24 0.05 19 12 0.32 118 0.04 5 1.65 0.01 1 ND 5	5 0.02 1
270N	570E	566081 5473172	1 14 8 54	0.1 17 11 528 2.	3 5 5 ND	8 1	2	19 0,17 0.08 27 14 0.48 113 0.02 5 1.95 0.01 1 ND 20	20 0.01 1
270N	590E	566081 5473172	3 46 113 89	0.3 57 26 902 3.		19 1	15	34 0.31 0.13 24 25 0.63 291 0.05 5 4.65 0.01 1 ND 5	5 0.01 3
270N	610E	566101 5473172	2 8 12 47			4 1		25 0.04 0.03 20 14 0.31 101 0.04 5 1.54 0.01 2 ND 5	5 0 02 1
270N	630E	566121 5473172	2 10 17 62			8 1		27 0.1 0.03 19 13 0.35 87 0.05 5 1.44 0.01 2 ND 5	5 0.01 1
270N	650F	586141 5473172	1 11 105 150			8 1		16 0,12 0,04 21 11 0,38 55 0,02 5 1,24 0,01 1 ND 20	20 0.01 1
270N	670E	566161 5473172	1 10 67 101			6 1		16 0.08 0.03 21 10 0.29 49 0.02 5 0.96 0.01 1 ND 30	30 0.01 1
270N	690E	566181 5473172	2 24 429 201			11 1	ž		30 0.04 t
270N	710E	586201 5473172	2 29 302 195			5 1	_		70 0.01 1
270N	730E	566221 5473172	1 27 148 48			S 1	_		5 0.03 2
270N	750E	566241 5473172	2 12 12 46			6 1	-		20 0.02 1
270N	570E	566081 5473192	2 12 12 40			12 t	•	29 0.07 0.09 21 12 0.28 92 0.09 5 1.07 0.01 9 MD 20	5 0.02 2
	570E	566081 5473192	4 24 68 82			12 I 51 1	•	31 0.19 0.07 26 20 0.48 139 0.05 5 2.43 0.01 9 NO 5	5 0.02 2
290N						7 1	-		
290N	610E	566101 5473192	3 16 23 69				•		5 0.02 1 5 0.01 2
290N	630E	566121 5473192	4 13 64 53			6 1			
290N	650E	566141 5473192	5 42 631 169			16 2		32 0.26 0.14 25 17 0.35 97 0.04 5 2.18 0.01 8 ND 5	5 0.01 3
290N	670E	566161 5473192	3 13 51 68			6 t		24 0.07 0.03 16 12 0.13 63 0.05 5 1.67 0.01 7 ND 20	20 0.03 1
300N	730E	566221 5473202	2 31 416 229			8 1		24 0.09 0.05 13 12 0.29 64 0.1 5 2.27 0.01 2 ND 10	10 0.04 1
300N	750E	58(4:41 5473202	f 8 33 27			6 1		22 0.07 0.03 10 6 0.05 42 0.1 5 0.67 0.01 3 ND 4 80	50 0.01 1
320N	550E	566,341 5473222	1 10 10 119			\$1 1	-	38 0.19 0.05 15 15 0.31 135 0.1 5 1.99 0.01 1 ND 5	5 0.01 1
320N	570E	566061 5473222	1 7 11 48			5 1	_	34 0.05 0.04 20 10 0.23 63 0.06 5 1.01 0.01 2 ND 5	5 0.02 1
320N	590E	566081 5473222	2 21 18 56			9 1		38 0.12 0.06 21 15 0.49 180 0.06 5 2.64 0.01 2 ND 10	10 0.01 2
320N	610E	566101 5473222	2 20 17 56			6 1		43 0.08 0.05 16 14 0.6 124 0.05 5 2.23 0.01 3 ND 5	5 0.01 2
320N	630E	566121 5473222	2 11 74 56			7 1		30 0.09 0.04 19 13 0.38 90 0.07 5 1.58 0.01 3 ND 5	5 0.01 1
320N	730E	566221 5473222	2 10 26 48			5 1	_	39 0.08 0.03 10 10 0.09 65 0.11 5 1.2 0.01 3 ND 5	5 0.03 1
320N	750E	568241 5473222	1 24 102 111			10 1		26 0.12 0.06 13 11 0.36 77 0.06 5 1.63 0.01 1 ND 20	20 0.02 1
340N	550E	566041 5473242	1 11 12 56		1 2 5 ND	12 1	3	28 0.22 0.04 12 9 0.2 108 0.11 5 1.9 0.01 1 ND 5	5 0.02 1
340N	570E	566061 5473242	1 7 1 57	0.1 8 4 145 2.1	3 2 5 ND	\$ 1	2	22 0.21 0.05 10 8 0.34 85 0.04 5 1.41 0.01 1 ND 5	5 0.02 1
340N	590E	588081 5473242	1 14 10 43	0.1 13 10 123 2.4	3 2 5 ND	4 1	2	24 0.03 0.03 22 13 0.46 88 0.03 5 1.96 0.01 1 ND 5	5 0.02 f
340N	610E	568101 5473242	3 38 42 68	0.4 30 18 276 5.1	3 10 5 ND	10 1	12	61 0.13 0.09 17 22 0.76 215 0.08 5 3.58 0.01 3 ND 5	5 0.02 3
340N	630E	566121 5473242	2 15 6 42	0.1 17 11 134 3.3	2 3 5 ND	4 1	2	44 0.04 0.06 34 11 0.94 50 0.01 5 1.63 0.01 1 ND 30	30 0.02 1
340N	710E	566201 5473242	3 23 110 141	0.3 19 12 145 3.1	3 5 5 ND	9 1	12	40 0.07 0.05 13 16 0.31 171 0.09 5 3.15 0.01 1 ND 5	5 0.03 2
340N	730E	568221 5473242	1 15 62 119	0.1 12 12 338 2.2	2 5 ND	9 1	2	23 0.12 0.04 12 11 0.45 89 0.04 5 1.72 0.01 1 ND 5	5 0.02 1
340N	750E	566241 5473242	2 11 44 109			5 1	3		5 0.02 1
360N	550E	566041 5473282	1 20 21 103			9 f	5	18 0.15 0.12 21 14 0.48 116 0.02 5 2.15 0.01 1 ND 5	5 0.01 t
360N	570E	566061 5473262	1 21 14 52		1 2 5 ND	15 1	2	22 0.35 0.1 20 10 0.31 112 0.07 5 1.86 0.01 2 ND 5	5 0.02 1
360N	590E	566081 5473262	1 16 1 55	0.1 15 6 168 2.8	2 5 ND	10 t	2	33 0.14 0.03 18 13 0.61 143 0.04 5 1.92 0.01 1 ND 5	5 0.02 1
360N	610E	566101 5473262	1 34 131 56	0.1 19 9 158 3.4	3 2 5 ND	7 1	2	43 0.09 0.04 23 14 0.77 141 0.04 5 2.4 0.01 1 ND 10	10 0.02 1
360N	650E	566141 5473262	2 17 32 63	0.1 13 10 292 2.2	2 5 ND	9 1	2	28 0.13 0.04 8 11 0.31 93 0.1 5 1.58 0.01 1 ND 5	5 0.01 1
360N	670E	566161 5473262	3 16 28 47	0.5 11 9 92 2.2	12 5 ND	4 2	8	34 0.04 0.05 15 18 0.19 59 0.06 5 1.28 0.01 9 ND 5	5 0.03 1
360N	690E	568181 5473262	4 15 59 48			4 2		37 0.02 0.02 23 17 0.26 65 0.05 5 1.35 0.01 9 ND 5	5 0.02 1
360N	710E	566201 5473262	2 15 22 38			9 1		21 0.15 0.03 17 17 0.14 51 0.02 5 0.76 0.01 4 ND 5	5 0.01 1
360N	730E	566221 5473262	3 17 69 73			10 2	_	38 0.15 0.03 15 16 0.23 76 0.1 5 1.75 0.01 9 ND 5	5 0.01 2
360N	750E	566241 5473262	3 21 95 96			8 1		37 0.12 0.03 16 17 0.19 88 0.09 5 1.14 0.01 9 ND 5	5 0.01 2
380N	550E	586041 5473282	3 22 45 98			10 1	-		5 0.01 2
380N	570E	566061 5473282		0.1 14 14 253 2.6		9 1		30 0.12 0.06 12 18 0.32 92 0.05 5 2.69 0.01 5 ND 5	5 0.02 2
380N	610E	588101 5473282	3 18 24 80			8 1		31 0.12 0.04 26 18 0.57 122 0.03 5 1.82 0.01 7 ND 5	5 0.01 1
380N	\$30E	566121 5473282		0.1 11 5 143 1.		8 1	2		5 0 02 1
380N	650E	586141 5473282	2 15 21 41			8 1	2		10 0.02 1
380N	670E	566161 5473282		0.4 15 10 271 2.		5 1	-		5 0.01 1
380N	890E	588181 5473282	2 12 24 53			5 1		34 0.04 0.03 15 15 0.34 63 0.06 5 1.33 0.01 3 ND 5	5 0.01 1
380N	710E	586201 5473282		0.2 11 7 186 2.		9 1		32 0.13 0.03 12 13 0.29 86 0.08 5 1.56 0.01 4 ND 5	5 0.01 1
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380N	730E	566221 5473282	1 4 3 31 0.1	5 2 65 1.05	2 5 ND	6	1 2	2 \$1 0.1 0.05	17 6 0.21 56 0.01 5 0.57	0.01 2 N	Ď	5	5 0.01	
380N	750E	566241 5473282	1 10 9 82 0.1	10 4 202 2.18	2 5 NĐ	5	1 2	2 20 0.1 0.03	13 11 0.43 77 0.02 5 1.11	0.01 1 N	D	5	5 0.02	1
400N 400N	590E 610E	566081 5473302 568101 5473302	1 17 13 66 0.1 1 10 1 47 0.1	12 9 410 2.68		11	12		13 12 0.43 145 0.07 5 2.22 19 13 0.57 62 0.02 5 1.32	0.01 1N 0.01 1N			5 0.01 5 0.01	1
400N	630E	566121 5473302	1 9 1 45 0.1	6 2 108 2.09		7	1 2	2 18 0.1 0.05	9 8 0.27 63 0.07 5 1.05	0.01 1 N	D		5 0.01	i
400N 400N	650E 670E	566141 5473302 566181 5473302	1 15 13 56 0.1 4 16 30 42 0.3			8	1 2		10 12 0.43 112 0.09 5 1.79 29 17 0.36 89 0.09 5 1.39	0.01 1 N 0.01 8 N			5 0.01 5 0.02	1
400N	690E	566181 5473302	3 20 26 69 0.1	17 11 177 2.95		12	1 6		15 15 0.35 128 0.08 5 2.15	0.01 5 N			0 0.02	2
400N 400N	710E 730E	566201 5473302 566221 5473302	3 33 28 57 0.1 3 14 38 51 0.7			8	1 9		20 16 0.48 106 0.05 5 1.97 25 18 0.42 83 0.03 5 1.27	0.01 7 N 0.01 7 N	-		5 0.04	2
400N	750E	586241 5473302	2 12 13 51 0.2			5	1 4		11 13 0.21 87 0.07 5 1.94	0.01 7 N			5 0.02 5 0.04	1
	MCPB		1 2691 >2% 3256 131			3	5 287		1 111 0.01 1 0.01 131 0.08	0.01 2 N			0 0.05	1
1330E	WEA-R22 920N	2 587798 5474393	2 10475 1089 24 1.8 1 21 5 47 0.3			6 5	12		1 142 0.19 1 0.01 481 0.19 15 10 0.35 42 0.07 5 1.49	0.01 1 N 0.01 3 N			0 0.03	1
1330E	960N	567799 5474429	1 38 11 48 0.2	15 15 154 2.95	2 5 ND	8	7	2 78 0.07 0.04	18 11 0.61 48 0.08 5 2.14	0.01 3 N	-	20 2	0 0.02	2
1330E 1330E	1000N 1040N	567799 5474473 567800 5474513	1 56 14 58 0.2 2 132 10 22 0.2			5 20	4		18 13 0.65 55 0.06 5 2.21 22 7 0.22 87 0.13 5 1.53	0.01 3 N 0.01 2 N			0 0.02	1
1330E	1080N	567799 5474553	1 7 6 21 0.2	4 6 48 1.13	2 5 ND	3 1	3	2 29 0.02 0.04	12 5 0.08 34 0.05 5 1.02	0.01 4 N	D	70 7	0 0.01	t
1330E 1330E	1120N 1160N	587799 5474592 567799 5474632	t 9 13 56 0.1 2 12 12 31 0.1	9 17 1870 1.98 16 20 208 2.94		6 8	16		14 11 0.27 147 0.1 5 1.94 21 9 0.59 86 0.06 5 1.51	0.01 3 N 0.01 3 N	-		0 0.02	1
1330E	1200N	567800 5474673	2 7 7 28 0.1	8 9 115 2.07	2 5 ND	4	i 3	2 38 0.02 0.08	15 8 0.25 38 0.08 5 0.96	0.01 3 N	D	130 13	0 0.01	1
1330E 1330E	1240N 1280N	587800 5474714 587799 5474753	3 7 1 31 0.1			4 1	2		12 3 0.38 66 0.04 5 1.44 7 6 0.42 60 0.02 5 0.88	0.01 1 N 0.01 1 N			0 0.01	1
1380E	920N	567849 5474393	1 11 12 32 0.1			5	10		6 10 0.09 43 0.1 5 3.25	0.01 IN			0 0.01	1
1380E 1380E	960N 1000N	567849 5474428 567849 5474473	1 27 16 49 0.1 1 14 15 39 0.1	12 13 143 2.26 9 11 88 2.73		5	1 7		10 11 0.37 57 0.1 5 3.19 14 9 0.34 41 0.07 5 1.51	0.01 4 N	-		0 0.04	1
1380E	1000N	567850 5474513	1 21 13 40 0.1	• • • • •		4	1 5		14 9 0.34 41 0.07 5 1.51 18 12 0.48 55 0.06 5 2.04	0.01 4 N 0.01 3 N		-	5 0.02 0 0.03	1
1380E	1080N	567848 5474553	1 23 23 34 0.1			7	6		16 9 0.34 65 0.06 5 1.08	0.01 3 N	-	60 E	0 0.01	1
1380E 1380E	1120N 1180N	567848 5474592 567849 5474632	1 9 4 29 0.1 1 15 1 43 0.1			5			11 6 0.18 86 0.08 5 1.1 16 8 0.37 58 0.06 5 1.13	0.01 1 N 0.01 1 N	-		0 0.01	1
1380E	1200N	567849 5474673	1 15 4 44 0.1	11 14 237 3.26	2 5 ND	5 1	1 2	2 79 0.04 0.1	11 7 0.58 80 0.1 5 2	0.01 1 N	D	80 8	0 0.02	1
1380E 1380E	1240N 1280N	567849 5474714 567849 5474753	1 5 1 22 0.1 3 10 17 52 0.1			4 1	-		5 4 0.08 58 0.1 5 1.3 13 8 0.45 168 0.05 5 1.55	0.01 1 N 0.01 4 N			0 0.02 0 0.01	1
1430E	920N	587899 5474393	1 14 34 40 0.1	8 13 1225 1.86	8 5 ND	9		2 50 0.09 0.08	4 9 0.13 116 0.15 5 2.81	0.01 5 N			0 0.03	i
1430E 1430E	960N 1000N	587898 5474428 587898 5474473	1 10 9 26 0.1 1 28 17 48 0.3			6	4		10 8 0.17 57 0.11 5 1.53 17 11 0.55 59 0.08 5 2.48	0.01 3 N 0.01 4 N			0 0.04 0 0.03	1
1430E	1040N	567899 5474513	1 26 17 40 0.3			5	• •		10 10 0.33 48 0.11 5 3.28	0.01 4 N	-		0 0.03	1
1430E	1000N	567898 5474553	2 37 9 39 0.3			6 2			21 7 0.71 38 0.06 5 1.58	0.01 5 N	-		0 0.01	2
1430E 1430E	1160N 1200N	567898 5474632 567899 5474873	1 10 15 34 0.1 2 117 27 48 0.1	7 9 134 2.32		9	_		19 9 0.32 66 0.06 5 1.2 24 11 0.62 77 0.06 5 1.84	0.01 3 N 0.01 4 N	-		0 0.02	1
1430E	1240N	567899 5474714	1 17 3 57 0.1	74 10 202 2.44	2 5 ND	5 1		2 31 0.04 0.14	9 9 0.27 78 4.07 5 3.44	0.01 1 N	-	50 5	i0 0.04 i	1
1430E 1430E	1280N 1320N	567899 5474753 567898 5474793	2 42 2 47 0.1 3 10 13 37 0.4	18 54 411 2.61 10 11 482 2.05		7 1			21 8 0.57 128 J.05 5 1.77 14 12 0.26 69 0.08 5 1.06	0.01 1 N 0.01 6 N	5		0 0.01	1 1
1480E	1080N	567948 5474553	2 23 7 32 0.3			4 2			25 12 0.45 38 0.06 5 1.59	0.01 4 N			0 0.01	1
1480E 1480E	1120N 1160N	567949 5474592 567949 5474632	3 12 16 22 0.6 1 27 7 35 0.3	9 10 59 5.02 13 13 127 2.3		4 3			12 8 0.12 54 0.2 5 1.35 18 11 0.43 84 0.06 5 1.57	0.01 7 N 0.01 5 N			0 0.01	2
1480E	1200N	587949 5474873	2 107 32 51 0.2			12 2			38 18 0.6 155 0.05 5 2.97	0.01 8 N			5 0.01	2
1480E 1480E	1240N 1280N	587950 5474714 587949 5474753	1 25 9 15 0.1	3 3 183 0.33		11 1 28 1	2		11 5 0.07 64 0.11 7 0.52 10 7 0.1 253 0.05 10 0.47	0.01 2 N 0.01 2 N		-	5 0.01 5 0.01	1
1480E	1360N	587948 5474833	4 10 24 24 0.1	8 17 384 1.1		8 1	5		18 9 0.15 78 0.11 5 0.73	0.01 5 N	D	20 2	0 0.01	1
1480E 1480E	1400N 1460N	567949 5474871 567949 5474952	1 10 13 17 0.1	9 1 61 2.64 11 3 71 2.91	2 5 ND 4 5 ND	3 1	2		15 15 0.25 47 0.08 5 2.34 19 18 0.33 50 0.03 5 1.61	0.01 1 N 0.01 1 N		-	5 0.01 5 0.01	1
	26687		7 6 16 200 0.1	20 58 23 2.59		1 1	7	6 4 0.01 0.01	5 85 0.01 22 0.01 487 0.14	0.01 4 N	Ď	5	5 0.01	1
	26668 26689		2 9 16 7 0.1 3 13 24 47 1.7	10 25 22 1.09 34 58 586 5.48	3 5 ND 7 5 ND	14 1	7		5 82 0.01 19 0.01 149 0.14 4 47 1.05 21 0.01 873 0.13	0.01 5 N 0.01 4 N		5 400 140	5 0.01 0 0.02	1
800N	280W		1 17 1 38 0.4	5 8 309 3.44	2 5 ND	5		2 50 0.02 0.03 1	17 3 0.19 56 0.12 5 1.29	0.01 £ N	D	5	S 0.01	t
600N 600N	300W 320W		2 22 25 63 0.2 1 10 21 32 0.2	14 19 334 3.92 8 12 112 2.7	24 5 ND 9 5 ND	5 1 5 1	-	2 29 0.02 0.1 3	31 7 0.31 54 0.05 5 1.42 21 7 0.15 44 0.05 5 1.57	0.01 2 N 0.01 2 N		-	5 0.01 5 0.01	1
600N	340W		1 11 27 20 0.3	3 15 48 1.86	7 5 ND	5 1	+	2 34 0.03 0.05	4 8 0.05 31 0.13 5 3.53	0.01 8 N	D	5	5 0.05	i
600N 600N	360W 380W		2 10 12 34 0.3 2 25 1 50 0.2	8 9 152 2.48 5 8 198 4 18	., .,	4 1	-	2 34 0.02 0.05 2 2 21 0.01 0.06 2	28 8 0.17 33 0.08 5 0.95 26 1 0.28 29 0.03 5 1.26	0.01 4 N 0.01 1 N	-	-	5 001 5 001	1
800N	400W		4 22 37 65 0.8	11 17 457 5.98	27 5 ND	5 2	_	2 50 0.02 0.12 1	15 9 0.19 60 0.17 5 2.57	0.01 6 N		5	5 0.02	Ť
600N 600N	420W		4 25 64 70 0.5 2 13 22 46 0.5	13 25 721 4.45	115 5 ND 21 5 ND	6 1 3 1	-		3 6 0.22 52 0.07 5 1.36 27 6 0.2 41 0.08 5 1.39	0.01 3 N 0.01 6 N		-	5 0.01 5 0.01	1
600N	440VV 460VV		2 13 22 46 0.5	8 14 140 3.03 11 17 280 3.88		4 1	•		18 7 0.2 50 0.07 5 1.39	0.01 BN		•	5 0.01	i
850N	240W		1 21 1 58 0.3	7 11 623 2.63		9 1 77 1	_		20 3 0.23 118 0.04 5 1.19 26 6 0.32 339 0.03 5 2.23	0.01 1 N		-	5 0.01	1
650N 650N	260W 280W		1 32 25 78 0.3	10 24 1347 2.27 1 3 189 1.65	10 5 ND 2 5 ND	27 1 8 1	-	- /* *.=* *.**	26 6 0.32 339 0.03 5 2.23 12 2 0.09 52 0.1 5 0.74	0.01 1 N 0.01 1 N	-	-	5 0.01 0 0.01	1
850N	300W		1 9 20 36 0.1	5 9 1091 1.16	5 5 ND	14 1	-	2 27 0.12 0.03 1	7 6 0.13 128 0.08 5 0.84	0.01 2 N		•	5 0.01	1
650N 650N	320W 340W		1 5 12 17 0.1 2 13 16 35 0.2	2 6 39 1.07 6 14 165 3.25	2 5 ND 15 5 ND	4 1		2 29 0.03 0.03 2 2 41 0.02 0.05 2		0.01 2 N 0.01 5 N		•	5 0.01 5 0.03	1
650N	360W		1 14 1 41 0.1	4 8 144 3.27	25 5 ND	3 1	2	2 21 0.02 0.05 3	7 1 0.26 23 0.02 5 1.04	0.01 1 N	0	5	5 0.01	1
650N 850N	380W 400W		1 11 18 40 0.1 2 14 33 54 0.6	6 12 146 3.38 6 17 153 4.11		5 1	-	2 51 0.02 0.04 2 2 38 0.02 0.08 1		0.01 1 N 0.01 6 N	-	-	5 0.01 5 0.04	1
00011			2 19 33 39 0.0	• 1) [04 4:1]	10 S ND	. .	v	L 00 0.02 0.00 1		on		-		,

650N	420W		1 12 1 33 0.7	1 11 189 2.53 2 5 ND	4 1 2 2 22 0.02 0.05 7 4 0.11 36 0.09 5 3.22 0.01 1 ND	5
650N	440W		1 15 1 31 0.6	1 10 78 2.84 2 5 ND	3 1 2 2 29 0.01 0.04 8 2 0.12 35 0.09 5 2.69 0.01 1 ND	5
850N	460W		1 14 1 29 0.9	1 11 87 1.98 2 5 ND	4 1 2 2 20 0.02 0.04 2 4 0.11 37 0.11 5 3.9 0.01 1 ND	5
700N 700N	240W 260W		8 54 84 92 0.5 1 16 6 79 0.1	14 43 5994 2.32 13 5 ND 6 13 1588 1.96 9 5 ND	35 1 9 2 30 0.27 0.1 29 9 0.24 239 0.09 12 2.07 0.01 6 ND 19 1 2 2 30 0.22 0.06 11 6 0.17 234 0.09 5 1.22 0.01 1 ND	5 5
700N	260W			11 31 1328 2.51 21 5 ND	11 1 6 2 25 0.07 0.05 33 7 0.25 135 0.04 5 1.45 0.01 4 ND	5
700N	300W		1 16 21 53 0.2	5 12 551 2.18 12 5 ND	11 1 2 2 24 0.09 0.07 13 6 0.2 92 0.07 \$ 1.87 0.01 1 ND	5
700N	320W		1 8 2 38 0.3	2 3 71 0.99 2 5 ND	7 1 2 2 31 0.07 0.03 9 4 0.07 39 0.08 5 0.63 0.01 1 ND	5
700N 700N	340W 360W		3 23 31 81 0.3 2 33 32 76 0.2	16 19 179 3.68 30 5 ND 19 17 208 2.95 40 5 ND	3 1 9 2 30 0.01 0.05 35 10 0.39 50 0.03 5 2.04 0.01 8 ND 3 1 5 2 14 0.01 0.05 40 8 0.44 32 0.01 5 1.22 0.01 3 ND	5
700N	380W		2 25 35 72 0.1	16 16 211 3.79 52 5 ND	3 1 5 2 14 0.01 0.05 40 8 0.44 32 0.01 5 1.22 0.01 3 ND 3 1 9 2 13 0.01 0.06 44 6 0.45 29 0.01 5 1.13 0.01 4 ND	45D 10
700N	400W			17 17 211 3.46 34 5 ND	4 1 8 2 12 0.05 0.05 41 8 0.45 31 0.01 5 1.32 0.01 5 ND	10 5
700N	420W		2 26 30 72	18 18 409 3.12 29 5 ND	4 1 8 2 12 0.03 0.04 43 7 0.41 59 0.01 5 1.29 0.01 5 ND	260
700N	440W			14 16 176 5.07 35 5 ND 10 22 3594 2.62 7 5 ND	7 1 8 2 34 0.05 0.05 28 9 0.24 78 0.05 5 1.8 0.01 6 ND 11 1 2 2 31 0.11 0.08 12 4 0.18 130 0.07 5 1.98 0.01 1 ND	5
700N 700N	480W 480W			10 22 3594 2.62 7 5 ND 10 15 348 4.38 20 5 ND	11 1 2 2 31 0.11 0.08 12 4 0.18 130 0.07 5 1.98 0.01 1 ND 4 1 2 2 42 0.01 0.04 15 5 0.26 84 0.1 5 2.76 0.01 1 ND	5 5
700N	500W			10 16 718 2.52 9 5 ND	8 1 6 2 57 0.02 0.04 12 11 0.17 101 0.15 5 1.19 0.01 4 ND	5
50N	430E	565921 5472952	12 10			50
SON	450E	565941 5472952	10 36			30
50N 50N	470E 490E	585981 5472952 565981 5472952	16 64 6 38			10 50
50N	5105	566001 5472952	260 94			160
50N	530E	566021 5472952	20 52			520
50 N	550E	566041 5472952	20 88			80
50N 50N	570E	586061 5472952 566081 5472952	12 34 8 28			20 10
70N	590E 450E	566081 5472952 565941 5472972	8 28 12 82			20
70N	470E	565961 5472972	20 312			50
70N	490E	585981 5472972	210 108			60
70N	510E	566001 5472972	14 30			10
70N 70N	530E 550E	586021 5472972 568041 5472972	14 46 12 14			380 100
70N	570E	566061 5472972	20 30			10
70N	590E	566081 5472972	12 40			20
70N	610E	566101 5472972	10 32			100
90N 90N	470E 490E	565961 5472992 565981 5472992	34 258 108 120			50 40
SON	510E	566001 5472992	8 16			50
90N	530E	566021 5472992	24 52			30
90N	550E	566041 5472992	12 22			30
90N 90N	570E4	566061 5472992	30 26		1	50
90N	590E 610E	586081 5472992 588101 5472992	22 36 10 54			90 80
90N	630E	568121 5472992	12 28			70
110N	490E	585981 5473012	218 148			50
110N 110N	510E 530E	566001 5473012 566021 5473012	8 32 8 26			130 60
110N	550E	556041 5473012	6 42			60
110N	570E	566061 5473012	10 30			290
110N	590E	566081 5473012	34 58			50
110N 110N	610E 830E	566101 5473012 566121 5473012	10 70 14 44			200 80
110N	650E	566141 5473012	10 30			70
130N	510E	566001 5473032	8 14			70
130N	530E	566021 5473032	4 18			50 30
130N 130N	550E 570E	566041 5473032 566061 5473032	12 30 16 22			100
130N	590E	566081 5473032	41 46			50
130N	610E	566101 5473032	8 30			100
130N	630E	565121 5473032	40 64			20
130N 130N	650E 670E	566141 5473032 566161 5473032	12 26 38 60			5
150N	530E	566021 5473052	18 36			20
150N	550E	566041 5473052	18 32			210
150N	570E	566061 5473052	12 20			40
150N 150N	590E 810E	566081 5473052 566101 5473052	10 26 34 38			40 1180
150N	630E	566121 5473052	34 38 30 58			30
150N	650E	566141 5473052	18 32			70
150N	670E	566161 5473052	t6 32			90
150N	890E	566181 5473052	8 16			30 5
170N 170N	550E 570E	566041 5473072 566061 5473072	14 34 16 48			40
170N	590E	566081 5473072	12 24			10

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610E 568101 5473072 42 34 830E 568121 5473072 66 148 650E 568141 5473072 20 42 670E 568181 5473072 25 56 690E 568181 5473072 12 20 710E 568210 5473072 10 20							
830E 566121 5473072 66 148 850E 568141 5473072 20 42 670E 568151 5473072 26 58 690E 568151 5473072 12 20			600404	6472072	13	24	
650E 560141 5473072 20 42 670E 560161 5473072 26 56 690E 568161 5473072 12 20	NN.						
670E 566181 5473072 26 56 690E 566181 5473072 12 20	70N						
890E 586181 5473072 12 20	ON						
	'ON						
710E 588201 5473072 10 20	ON						
	70N	710E	566201	5473072	10	20	

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Rock Analytical Results

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SAMPLE*			Мо	Cu	РЪ	Zn	Ag		Co	Mn	Fe	As	U	Au		Sr			Bi	v	Ca		La	Cr	Mg	Ba Ti	в	Al	Na	к	W Be		
	Easting	-	ppm	ppm		ppm	ppm			ppm		ppm p			-			•		• •	%		ppm J			• •	ppm	%	%		ppm ppm		
E-1 E-2	570268.3	5474874	2	11821 280	14 21	27	6.6	25	30 12	113 1555	3.86 8.05		<8 <8	<2	<2 8		0.7	4	<3 3		0.02		1 21).71	4 <.01 67 <.01	<3	0.59	0.02		2 <2	32	
			∠ <1	188	21 7	46 7	0.3 0.7	15 7	12		1.11		~o <8	<2 <2	<2	11 39	1 <.5	-9 <3	-3 -3		0.02	0.1 0	21 1).13).04	9 0.11	<3 <3	0.87 0.78	0.01 (<∠ <2	1.5	
E-3 E-4				100	7	10	<.3	9	3		1.89	20 4	~o <8	<2	8		<.5	<3	<3		0.03	0	24),49	13 < 01	<3	0.9	0.02		<2	2 0.2	
E-5			<1	13	<3	11	<.3	7	4	116	1.6		~0 <8	<2	8		<.5	<3	<3		0.03	-	2 4 26).45).04	16 < 01	<3	0.28	0.02		<2	267,8	
E-6			<1	58	-3	10	<.3	8	21		2.06	4	<8	<2	0 8		<.5	-3	-3		0.02	0	20 85).03	19 < 01	<3	0.28	0.02		~2 29	207.8	
E-0 E-7	569852.4	5475387	1		5	2	<.3	7	<u>2</u> 1 8		2.05	5	<0 <8	<2	2	-	<.5	<3	<3	3	<.01	õ	42	4		12 < 01	<3		<.01		25	19.9	
E-8	569846.9		2	3	15	14	<.3	7	10		4.31	12	<8	<2	7	-	<.5	<3	4	9	< 01	0,1	24		0.01	18 < 01	<3	0.22			<2	10.1	
E-9			3	10	42	19	<.3	14	16		8.01	26	<8	<2	4	-	< 5	3	5		0.04	0	31).66	14 < 01	<3	0.9	0.01		2	<.2	
E-10			1	2	6	21	<.3	15	.9	124			<8	<2	4	3	<.5	<3	<3		0.02	-	4	13		16 <.01	<3	1.4			<2	<.2	
E-11			<1	2	6	6	<.3	3	4	32	7.49	5	<8	<2	2	3	<.5	<3	3	19	0.01	0	5	11 1	28	36 <.01	<3	0.55	0.01	0.07	<2	2.3	
E-12			14	6	12	34	<.3	16	12	1527	6.86	<2	<8	<2	6	5	«.5	<3	<3	11	0,02	0.1	7	13 (9.93	58 <.01	<3	1.32	0.01	0.11	<2	<.2	
E-13			1	4	6	13	<.3	8	13	84	4.61	<2	<8	<2	8	4	<.5	<3	<3	7	0.01	C	5	11	0.4	36 <.01	<3	0.73	0.01	0.13	<2	<.2	
E-14			1	4	20	14	<.3	4	5	166	7.22	<2	<8	<2	7	2	<.5	<3	4	9	0.01	0	10	11 ().22	32 <.01	<3	0.67	0.01	0.12	<2	4.4	
E-15	568908	5474713	3	11	18	48	1.4	12	71	165	14.8	25	<8	<2	2	4	0.5	<3	<3	85	0.01	0.1	9	14 ().04	26 0.02	<3	0.72	0.05	0.08	<2	1107	
E-16	569091	5474980	1	5	10	3	<.3	1	3	192		23	<8	<2	4		<.5	<3	4	11	<.01	0	22		0.02	23 <.01	<3	0.29	0.01		<2	30.4	
E-17	569091	5474980	3	5	6	14	<-3	5	5		6,92	11	<8	<2	2		<.5	<3	<3		0.01	0	6		0.01	13 < 01	<3	0.2		0.1	<2	10.2	
E-18	569091	5474980	4	2	13	11	0.4	16	100		10.1	37	<8	<2	4		<.5	<3	<3	10	<.01	0.1	31		0.02	31 <.01	<3	0.36	0.01		<2	17.5	
E-19	569091	5474980	3	2	12	17	0.5	11	11		10.7	13	<8	<2	3		<.5	<3	<3		<-01	0.1	3		0.01	9 <.01	<3	0.16	0.01		<2	4.3	
E-20	569091	5474980	1	4	32	133	<.3	1	3	43	4.4		<8 ~0	<2	<2		0.6	<3	<3	_	<.01	0	2		:.01	4 <.01	<3	0.07			2	8.2	
E-21	568932	5475077	3	16 2	<3	22	0.3	14	7	527		<2 7	<8 ~9	<2	6 9		<.5	<3 ~2	<3	3	<.01	0	16		0.02	26 < 01	<3	0.42			<2 2	740.7	
E-22	569942	5477190	2	2	<3	8	<.3 <.3	34 25	142 54	88 900	7.06		<8 <8	<2 <2	9 6	•	<.5 0.5	<3 <3	<3 <3		<.01 <.01	ő	18 18		2.51	3 <.01 43 <.01	14 <3	1.96	0.01		<2	1.3 1.4	
E-23	564707	5470881	1		22	14		-	20	900 167					-			-	-			-).03		-	0.25			~2 <2	416.6	
E-24	564531	5471136	1	9	158	180	<.3	10					<8 /*	<2	5		0.7 ~ =	<3 <3	<3 <3	-	<.01	0	15			15 <.01	10		0.01	0.1	<2	4.8	
E-25 E-26	564540 564540	5471250 5471250	<1	2	7	14	<.3	41 47	22 25	121	7.42		<8 <8	<2 <2	2		<.5 <.5	<3	<3		0.01	0	1		5.5 5.59	4 <.01 4 <.01	13	4.39	<.01 (<2 <2	4.8 3.9	
E-20 E-27	564587	5471250	<1 3	14	34	14 29	<.3 <.3	75	105	137		-	<8 <8	<2	4		<.5	<3	<3		<-01	0	4		.09	58 < 01	14 29	1.05	<.01		<2	3.9 14.8	
E-27 E-28	564587 564587	5471347	3 1	7	46	2 9 23	<.5 0.5	/5 19	105	110			~o <8	<2	4 5	-	<.5	<3	<3		<-01	ő	24	-	0.08	25 < 01	29 16	0.33	0.01		<2	88.4	
E-20 E-29	564 598	5471347	ر 1>	3	40	33	<.3	71	58	602			~o <8	<24	11		<.5	10	<3		0.11	õ	24	4		20 < 01	13		2		<2	5.1	
E-29	564801	5471624	<1	3	29	20	<-3	24	9	631			~0 <8	<2	12		<.5	<3	<3		4.47	0	19		53	35 < 01	3		0.01		<2	2.6	
E-30 E-31	564770		1	4	∠⇒ 41	14	<.3	14	37 17		4,93		~o <8	<2	2		<.5	<3	<3		0.02	0	3		.55	34 < 01	-		0.01		2	3.4	
E-32	564733	5471650	1	2	5	11	<.3	3	3		6.35		<8	<2	5	-	<.5	<3	<3		0.04	õ	8		0.03	19 < 01	12	0.19	0.01		<2	2.5	
E-32	564716	5471687	1	31	114	92	0.5	16	10	699			<8	<2	6		<.5	<3	-3		0.31	-	12			564 <.01	5	0.22	0.01 (3	590	
E-34	565280	5471550	1	1	6	5	<.3	9	13		1.99		<8	<2	5		<.5	<3	<3		0.01	0	42		0.01	22 <.01	5		0.01 (<2	2.4	
E-35	568414	5471642	1	14	31	14	<.3	2	<1		1.27		<8	<2	4		<.5	<3	<3		0.01	0	22		0.02	44 <.01	9	0.16	0.02 (<2	63.1	
E-36	568298	5471564	3	582	1153	120	16.1	5	2		1.92		<8	4	2		1.2	52			0.01	õ	7		.04	11 < 01	5	0.09	0.01 (2	3944	
RE E-36	568298	5471564	4	591	1176	119	16.5	4	3		1.95	14	<8	4	2	1	1	53			0.01	ŏ	7		.04	11 < 01	5	0.09	0.01 (2	3453	
E-37	568258	5471516	2	9	36	12	0.5	1	<1		1.58		<8	<2	6	30	<.5	<3	<3		0.01	ŏ	33		.01	34 < 01	5		0.02 (<2	451.6	
E-38	568303	5471480	3	37	267	50	43	3	<1		1.89	_	<8	3	3		<,5	30	6	-	0.01	ŏ	14		1.03	20 <.01	7	0.1			2	1842	
E-39	568306	5471480	ž	84	525	19	5.4	1	<1		1.13		<8	<2	3	_	<-5	3	7		<.01	ő	6		.01	11 <.01	, 6		0.01 (2	540.7	
E-40	568306	5471480	1	14	84	11	0.5	2	<1		1.03		<8	<2	4		<.5	<3	-3		0.01	ō	20		.04	51 0.01	3		0.03		<2	80	
E-41	564204	5470682	3	4	<3	8	0.3	12	6	37		-	<8	<2	7		<.5	<3	3	-	<.01	ō	24		.03	19 <.01	-		0.06		6	9.8	
E-42	564209	5470720	Ť	4	3	12	<.3	8	2	109			<8	<2	6		<.5	<3	5		0.01	ŏ	18		1.01	27 <.01	ŝ	0.25	0.08 (<2	8.7	
E-43	563991	5470484	13	60	29	76	1.5	26	9	223			<8	<2	4		0.7	4	3	-	0.23	ŏ	6		.24	76 0.01	10			0.2	4	230.2	
E-44	563088	5469933	4	6	26	9	0.3	2	<1	20		-	<8	<2	6		<.5	<3	4		0.01	ŏ	11		.01	10 <.01			0.07 (<2	1.2	
E-45	563088	5469933	7	49	93	66	0.9	12	6		5.94	•	<8	<2	19		<.5	<3	7		0.02	ō	29		.02	87 <.01	13			0.2	<2	37.9	
E-46	563088	5469933	21	36	1982		23.3	3	<1	24			<8	<2	<2		1.1	<3	57		<.01	ŏ	2	14 <		4 <.01	4		0.02 (4	31.5	
E-47	563088	5466933	19	42	2258	80	31	a.	<1	-	1.39		<8	<2	<2		1.3	<3	76		<.01	ō	2		.01	3 <.01	3	0.02	0.02 (7	60.6	
E-48	563088	5466933	171	22	1240	26	9.1	2	<1		1,76		<8	<2	6	4		<3	20	-	<.01	ŏ	25		.01	6 < 01	<3	0.12	0.1 (<2	18.3	
RE E-48	563088	5466933	173	22	1240	20 25	9.1 9.5	2	<1	17	1.8		<8	<2	6		<.5	<3	20		<.01	ő	25		.01	6 < 01	<3		0.11 (2	17.5	
R⊆ E-49	563130	5470022	3	10	38	11	5.5 <.3	13	8		1.68		~0 <8	<2	9		<.5	<3	<3		0.05	ŏ	31		.03	41 < 01	3		0.06 0		4	1.9	
E-49 E-50	563431		3	248	- 30 66	75	0.5	13	8	403			~o <8	-	27	3		<3	4		<.01	ŏ	82	15 <		4 < 01			0.08 (2	8.6	
E-20	000401	04/0100	3	∠40	00	10	0.0	13	0	21	1.84	÷0	~0	~2	« 1	3	5	~ 3	4	2	~.01	v	υZ	10 ×		01	~	Q. 10	V.VO (7.QT	~	0.0	

E-50	563431	5470133	3	248	66	75	0.5	13	8	27	1.74	18	<8	<2	27	3	< 5	<3	4	2	<.01	0	82	15 <.01	4 <.01	<3	0.15 0.08 0.01	2	- 8	3.6
E-51	565456	5472297	2	9	66	156	0.6	14	11	39	9.59	14	<8	<2	8	1	<.5	<3	15	11	<.01	0.1	2	18 0.01	8 <.01	22	0.34 0.01 0.08	6	11	.1
E-52	565456	5472297	3	4	20	17	0.4	2	<1	29	4.78	11	<8	<2	<2	1	< 5	<3	6	6	<.01	0	1	11 0.01	10 <.01	17	0.17 0.01 0.1	<2	9	9.1
E-53	567407	5474250	2	3	3	3	<.3	6	<1	20	1.12	2	<8	<2	<2	1	<.5	<3	<3	1	<.01	0	1	21 <.01	13 <.01	<3	0.12 0.01 0.09	6	0).7
E-54	567407	5474250	2	5	3	7	<.3	5	4	95	1.87		<8	<2	2	1	<.5	<3	<3	3	<.01	0	2	12 <.01	12 <.01	4	0.13 0.01 0.07	2		5.5
E-55	569030	5474815	<1	16	5	8	0.9	2	2		2.66	2	<8	<2	<2	11	<.5	<3	<3	21	0.01	õ	2	2 <.01	28 <.01	6	0.1 0.02 0.07		100	
E-56	569213	5475026	1	3	3	8	<.3	2	11		3.03	11	<8	<2	3	1	<.5	<3	<3	8	0.01	ŏ	15	5 <.01	24 <.01	5	0.31 0.01 0.19			
					-	-							-		-	•			-	-		-						-		18
E-57	569213	5475026	<1	2	3	8	<-3	3	25		3.13	11	<8	<2	2	1	<.5	<3	<3	5	<.01	0	13	3 0.02	11 <.01	<3	0.18 0.01 0.08		26	
E-58	569213	5475026	1	5	<3	19	<.3	6	36		6.79	33	<8	<2	7	1	<.5	<3	5	9	0.01	0	71	6 0.01	13 <.01	<3	0.28 0.01 0.09	_		9.6
E-59	569157	5475019	2	13	7	44	<,3	41	22	458		2	<8	<2	5	3	<-5	<3	3	4	0.01	0	15	3 0.02	26 <.01	<3	0.42 0.03 0.12			5.9
E-60	565809	5472746	2	17	244	14	0.6	3	1	67	2.16	6	<8	2	4	2	<.5	<3	<3	- 4	<.01	0	12	4 0.02	23 <.01	3	0.18 0.01 0.1	<2	141	13
RE E-60	565809	5472746	3	16	242	14	0.8	3	1	70	2.15	5	<8	<2	4	2	<.5	<3	<3	- 4	<.01	0	12	4 0.02	22 <.01	3	0.17 0.01 0.1	<2	121	t5
E-61	567800	5474575	1	7	8	7	<.3	11	32	92	3.96	8	<8	<2	3	3	<-5	<3	<3	15	0.04	0.1	8	5 0.03	33 <.01	<3	0.38 0.01 0.19	<2	74	.2
E-62	567800	5474575	1	-9	<3	4	<.3	13	40	39	2.72	8	<8	<2	2	3	<.5	<3	3	3	0.01	0	12	4 0.01	29 <.01	<3	0.18 0.01 0.11	<2	30).5
E-63	567693	5474462	1	2	<3	6	<.3	8	9	53	1.57	<2	<8	<2	4	2	<.5	<3	<3	3	<.01	0	6	5 0.01	34 <.01	3	0.24 0.01 0.14	<2	12	4
E-64	567693	5474462	<1	3	<3	9	<.3	11	19	58	2.3	<2	<8	<2	14	-	<.5	<3	<3	3	<.01	Ō	27	6 0.01	32 <.01	<3	0.21 < 0.01 0.12	<2		9.6
2-04	00/000	0474402	- •	0	-0	v					2.0		-•		. 4	-				÷		•		0 0.01	62			-		
ET-1	570275,5	5475395	51	192	1837	296	11	23	16	21	14.9 1	asa	<8	30	<2	2	1.1	<3	<3	3	0.01	0	2	13 0.01	17 <.01	<3	0.09 <.01 0.04	<2	2700	00
•= · ·		5475395		219	5046	543	23.2	22	14	127	16 3		<8	77	3	3	9.3	<3	8			0.1	5	8 0.03	22 < 01	<3	0.21 <.01 0.06		5700	-
ET-3	570263.1	5475428	15	460	1082	402	1.9	15	20			698	<8	8	<2	ĩ	6.6	<3	<3	9	0.01	0	4	13 0.04	15 <.01	<3	0.23 <.01 0.05	_	657	
ET-4	570266.8	5475358	6	77	660	235	0.6	14	18	1003		86	<8	2	2	3	5.3	<3	<3	14	0.02	õ	9	8 0.09	30 0	<3	0.42 0.01 0.15	-	858	
ET-5	570266.8	5475358	11	141	4876	804	1.2	15	13	363		220	<8	4	5	6	4.7	<3	<3	11	0.05	0.1	21	8 0.15	21 0	<3	0.87 0.02 0.2		284	
	570266.8	5475358	206	225	6731	809	14.9	22	13		15.1 1		~o <8	30	6	5	4. 8.9	13	-5	9	0.03	0.1	14	10 0.11	23 0	<3	0.75 <.01 0.13	_	3200	
ET-6	570288.8	5475183											-		4	3	2.5	<3	3	7		0.1	14		23 0 39 0	<3	0.43 0.03 0.11		246	-
ET-7			11	174	381	230	0.3	16	12	856		32	<8	<2	•	-	2.5 10		<3	7	0.03	0		11 0.13 6 0.05		<3 <3				
ET-8	570380.3	5475183	10	83	659	621	<.3	15	10		4.48	18	<8	<2	4	3		<3	-			0	13						134	
ET-9	570380.3	5475183	1	12	128	404	<.3	21	11		4.36	2	<8	<2	8	19	3.6	<3 7	<3	17	0.24	-	21	17 1.38		3	2.4 0.02 0.25		48	
ET-10		5475183	2	19	105	91	<.3	40	30		7.54	2	<8	<2	9	19	< 5		3	26	0.16	0.1	67	17 0.91	29 0	<3	2.7 5 .01 0.1	-	40	
ET-11	570380.3	5475183	16	13	34	51	<.3	13	10		2.78	75	<8	<2	7	6	<.5	<3	<3	7	0.02	0	22	8 0.17	24 <.01	<3	0.99 <.01 0.1	-	435	
ET-12		5475183	1	11	15	28	<.3	9	5	144		5	<8	<2	9	13	<.5	<3	<3	6	0.11	0	30	6 0.42	19 <.01	<3	1.2 6<.01 0.08			25
ET-13	570380.3	5475183	4	32	233	327	<.3	15	7		4.51	13	<8	<2	5	6	<.5°	<3	<3	18	0.06	0	29	13 0.59	19 <.01	<3	1.1 5 .01 0.09	-	28	
ET-14		5475128	<1	90	12	21	<.3	13	13		1.99	<2	<8	<2	<2	9	<.5	<3	<3	55	0,16	0	3	24 1.27	9 0.1	<3	1.2 <.01< 0.01	-	11	• •
ET-15	569825	5475371	2	23	52	83	0.4	50	18	3075	9.4	31	17	<2	10	18	<.5	5		130	0.24	0	25	17 0.86	133 0	<3	2.3 5<.01 0.11		19	
ET-16	569825	5475371	<1	27	22	61	<.3	30	12		4.51	9	<8	<2	11	13	<.5	<3	<3	39	0.2	0	35	9 0.75	96 <.01	<3	1.74 <.01 0.16		47	
ET-17	569825	5475371	3	11	81	84	0.4	60	-		15.2	16	<8	<2	4	50	0.6	<3	-	121	0.61	0.1	25	15 2.51	331 0	<3	2.94 4<.01 0.05	_	41	
ET-18	569825	5475371	1	13	293	88	<.3	38	18			5	<8	<2	4	22	<.5	<3	<3	65	0.36	0	34	11 2.02	132 0	<3	2.6 0.01 0.07			9,9
RE ET-18	589825	5475371	1	13	286	86	<.3	36	17	3412		2	<8	<2	5	22	<.5	4	<3	63	0.35	0	32	12 1.98	130 0	<3	2.5 0.01 0.08			9
ET-19		5472228	1	16	227	15	<.3	4	3		0.91	4	<8	<2	6	3	<.5	<3	<3	9	0.01	0	21	9 0.07	23 <.01	<3	0.4 0.01 0.06		34	
ET-20		5472228	1	18	21	27	<.3	31	36	1.61	4		<8	<2	6	4	<.5	<3	<3	10	0.01	0	38	7 0.06	24 0	<3	0.5 0.03 0.14			37
ET-21	567738.8	5472228	1	61	14	44	<.3	13	11		7.52	11	<8	<2	14	5	<.5	4	<3	19	0.03	0.1	46	12 0.12	28 0	<3	1.7 0.02 0.1	<2	64	
ET-22		5472188	1	43	39	81	<.3	13	12		4.73	4	<8	<2	10	9	<.5	<3	<3	6	0.06	0	42	5 0.11	126 <.01	<3	1.13 <.01 0.21		13	
ET-23		5472161	4	157	17	108	0.9	38	49	2689		16	35	<2	3	6	0.6	<3	5	24	0.02	0.1	15	13 0.05	125 <.01	<3	0.84 <.01 0.23	-	342	
ET-24		5472161	<1	37	13	6	<.3	3	2	119		<2	<8	<2	<2	1	<.5	<3	<3	4	0.01	0	4	5 0.02	22 <.01	<3	0.26 <.01 0.03	_	272	
ET-25		5472274	1	15	117	85	<.3	15	7	173		13	<8	<2	7	7	<.5	<3	<3	16	0.05	0	24	17 0.5	45 0	<3	1.1 0.04 0.13		13	
ET-26		5472274	1	21	24	47	<.3	12	12		3.79	5	<8	<2	12	5	<.5	3	<3	57	0.02	0.1	69	20 0.52	42 0	<3	2.1 0.04 0.38		40	
ET-27	567673.5	5472455	1	102	8	11	<.3	10	13	492		3	<8	<2	3	6	<.5	<3	<3	34	0.03	0	8	11 0.28	21 0	<3	0.9 0.01 0.05	-	18	
ET-28		5472455	<1	118	9	7	0.4	24	76	-	2.63	12	<8	<2	<2	4	<.5	<3	<3	42	0.01	0	2	12 0.16	32 0	<3	0,6 0.01 0.01		18	
ET-29		5472455	1	82	8	16	<.3		192			16	15	<2	3	7	<.5	<3				0.1	24	30 0.52	97 0	<3	1.86 <.01 0.17	-	11	
ET-30		5472455	<1	4	4	5	<.3	5	4		1,72	<2	<8	<2	6	6	<.5	<3	<3	16	0.02	0	51	6 0.11	84 <.01	<3	1.16 0.03 0.04			9.2
ET-31	567677.7	5472437	3	44	11	4	0.9	2	1		1.44	<2	<8	10	<2	2	<.5	<3	<3	4	<.01	0	4	16 0.01	14 0	<3	0.19 <.01 0.03		1358	
ET-32	567677.7	5472437	1	42	18	7	1.4	2	1		0.84	2	<8	4	<2	1	<.5	<3	3		0.01	0	3	15 0.01	13 <.01	<3	0.13 <.01 0.02		54	
ET-33		5472477	1	50	86	9	<.3	2	2		0.58	<2	<8	<2	<2	1	<.5	<3	<3	4	<.01	0	7	14 0.01	21 <.01	<3	0.12 <.01 0.06		98	
ET-34	567675.1	5472477	<1	18	61	3	0.4	1	1		0.48	2	<8	<2	<2	1	<.5	<3	<3	2	0.01	0	1	11 0.01	18 <.01	<3	0.06 0.01 0.01			46
ET-35	567675.1	5472477	5	202	220	23	4.9	6	4	55	4.4	7	<8	6	9	5	<.5	<3	3	13	0.01	0	26	12 0.03	99 Û	<3	0.54 0.02 0.15	<2	465	51

MC 0001			1 32	1	24	0.7	8	14	278 1.26	11	5	ND	ND	4	1	4	2	66	1.45 0).1	3	47	0.44	37	0.2	5	1.53	0.01	0.01	5	1	5
2349			1 544	30336	37	53.4	1	1	26 0.57	2	5	73	ND	4	1	2	10	1	0.01	0	1	204	0.01	1	0	135	0.04	0.01	0.01	1	1	69300
2350			1 77	172	19	0.5	10	6	358 2.71	3	5	ND	ND	3	1	2	2	3	0.01	0	11	106	0.03	11	0	5	0.13	0.01	0.01	1	1	380
26659			2 24	99	10	0.3	16	13	63 5.38	18	5	ND	ND	5	1	2	2	89	0.08	0	4	148	0.02	8	0	135	0.09	0.01	0.01	3	1	190
26663			1 23	12	15	0.1	7	5	75 2.83	7	5	ND	ND	3	1	2	2	5	0.01	0	17		0.02	74	Ó	32	0.14		0.01	1	1	670
26664			2 8	16	74	0.1	19	22	683 2.83	3	5		ND	5	1	5	2	11	0.03	ō			0.45	84	0	5	1.31		0.01	2	1	10
26665			1 127	6	10	0.1	4	15	104 2.63	2	5		ND	2	1	2	2	58	0.01	õ			0.37	7	ō	5	0.56		0.01	2	1	5
26666			2 26	11	12	0.1	13	13	64 3.63	6	5		ND	2	1	5	2	12	0.01	õ	•		0.57	, 26	ŏ	213	0.67		0.01	2	1	5
WEA-R1	564138	5472392	1 24	15	64	0.1	15	1	903 4.2	5	5		ND	2	1	2	2	5	0.01	õ			0.03	20	õ	5	0.05		0.01	4	1	5
WEA-R2	564138	5472392	2 16	12	10	0.2	9	3	77 1.77	9	5		ND	3	-	2	Å	4	0.01	0			0.01	6	õ	5	0.14	0.01		1	1	20
WEA-R3	564600	5471464	3 12	46	1	2	15	19	90 1.68	19	5		ND	3	4	2	24	6	0.01	õ	9		0.01	4	Ő	5	0,1		0.01	4	1	5
				27	4	0.5	7	2	65 2.3				ND	4		2	2 4 6	3	0.02	0	3		0.01	4	0	89	0.18		0.01	1	1	-
WEA-R4	564126	5471841			4		-	2		15	5			•		2	-	-		-					0						1	270
WEA-R5	563910	5472111	2 3	2		0.1	8		49 1.17	4	5		ND	2	1		2	7	0.01	0			0.07	1	-	20	0.11		0.01	1		10
WEA-R6	563910	5472111	2 42	3	16	0.4	12	1	185 2.06	2	5		ND	2	1	2	2	5	0.01	0			0.01	1	0	5	0.06		0.01	2	1	5
WEA-R7	563637	5472359	1 2	3	1	0.5	10	8	48 1.52	10	5		ND	6	1	2	10	10	0.01	0	37		0.04	1	0	25	0.22		0.01	1	1	5
WEA-R8	564405	5471394	4 6	1	14	0.5	12	1	1025 5.42	2	5		ND	1	1	2	2	6),1			0.04	6	0	5	0.07	0.01		1	1	5
WEA-R9	568344	5471973	3 1258	205	14	4.2	38	5	96 5.76	2	5		ND	3	1	2	2	6	0.01	0			0.01	159	0	28	0.13		0.01	1	1	710
WEA-R10	568182	5472045	3 500	15	5	4.7	39	27	69 2.69	24	5		ND	1	1	2	22	17	0.01	Ó			0.16	1	Ó	7	0.22		0.01	5	1	40
WEA-R11	565263	5471188	1 44	1	83	0.1	88	17	1323 7.31	2	5	ND	ND	29	1	2	2	240	2.15 0	0.1	1	230 -	4.15	20	0.1	5	3.46	0.01	0.01	1	3	5
WEA-R12	566241	5471379	19	4	218	1.4	44	1	1822 14.6	33	5	ND	ND	3	1	2	12	68	0.01	0	1	202	0.06	50	0	5	0.18	0.01	0.01	1	2	5
WEA-R13	564321	5472622	1 116	3	45	0.8	9	3	184 4.12	15	5	ND	ND	8	1	2	2	2	0.01	0	37	104	0.03	17	0	5	0.33	0.01	0.01	1	1	20
WEA-R14	564321	5472622	16	4	49	0.1	9	9	243 3.5	20	5	ND	ND	3	1	2	2	1	0.01	0	9	111	0.02	19	0	7	0.19	0.01	0.01	1	1	830
WEA-R15	564321	5472622	1 4	1	44	0.3	5	3	177 3.01	17	5	ND	ND	2	1	2	2	1	0.01	0	8	85	0.02	20	0	5	0.24	0.01	0.01	1	1	250
WEA-R16	564527	5472797	1 17	21	33	0.1	2	1	66 2.74	79	5	ND	ND	4	1	2	2	1	0.02	0	6	70	0.01	23	0	19	0.14	0.01	0.01	1	1	1500
WEA-R17	564607	5472862	26	59	17	2.5	22	18	204 3.64	15	5	ND	ND	15	1	2	10	5	0,47	0	12	80	0.24	41	0	81	0.31	0.01	0.01	1	1	5
WEA-R18	564902	5473548	1 1	1	26	0.1		154	93 17.8	2	5	ND	ND	2	2	2	2	76	0.01	0	1	163	0.03	20	0.1	675	0.1	0.01	0.01	1	1	20
WEA-R19	565084	5473348	60 1785	60	96	3.4	17	33	479 3.98	10	5		ND	8	1	2	2	13	0.13	0			0.73	23	0	32	1.29		0.01	1	1	5
WEA-R20	564660	5472293	1 27	1	91	0.3	23	2	343 5.42	4	5		ND	2	1	2	2	5	0.01	ō			0.69	15	ō	5	1.18	0.01		1	1	160
WEA-R21	564720	5474288	2 6	18	23	0.9	16	23	329 4.01	18	5		ND	15	1	2	27	39	0.55	õ	8		0.13	22	õ	105	0.27	0.01		4	4	5
7236	004720	54/4200	5 133	278	59	2.4	10	5	34 2.34	17	5		ND	1	2	2	35	20	0.01	õ	-		0.01	16	õ	7	0.09		0.01	4	ť	4260
7237			3 72	319	31	50.3	9	6	41 1.65	16	5		ND	f	3	2	33	6	0.01	õ			C.01	27	õ	9	0.05	0.01		3	1	4100
7238			2 58	69	39	0.1	6	6	121 1.21	16	5		ND	3	2	2	6	5	0.01	ŏ			0.01	69	ŏ	7	0.24		0.01	Ť	ť	180
7239			2 355	37	46	0.6	15	6	46 2.08	17	5		ND	1	2	2	2	3	0.01	õ			0.01	21	ŏ	24	0.02		0.01	1	•	32000
			2 333			0.0	57	29	1007 5.33	18	5		ND	14	2	2	5	142		.1			2.08	126	0.3	24 5	2.67		0.01	1	4	10
7240				18	155		6	29 5			5		-	8	2	2	8	12	0.30 0	0	35		0.03	106	0.5	13	0.54	0.01		2	1	360
7241			3 56	39	43	0.9		9		16	5		ND	-	-	2	2			0					ő	65				1	f	5100
7242			2 413	185	36	0.4	18	-	108 5.95	35	-		ND	6	1	_	_	42 3	0.01	0			0.02	17 8	0	188	0.19		0.01			
7243			3 13	1895	16	26.5	9	1	79 2.66	18	5		ND	2	1	2	46	-	0.01	-			0.02	-	-		0.07		0.01	1	-	14500
7244			3 11	81	23	2.8	17	6	155 3.18	21	5		ND	3	1	3	14	8	0.03	0			0.05	23	0	69	0.3		0.01	3	1	6000
7245			1 14	125	23	0.1	12	6	46 2.16	14	5		ND	3	1	2	2	5	0.03	0		-	0.08	37	0	7	0.54		0.01	1	1	490
7246			35	291	28	5.7	11	7	99 3.12	4	5		ND	2	1	2	17	1	0.01	0			0.01	19	0	62	0.11		0.01	1	1	6600
7247			2 5	54	38	0.3	14	14	46 5.29	19	5		ND	4	2	2	2	9	0.01	0			0.24	37	0	100	0.34		0.01	1	1	5
7248			1 5	25	63	0.1	22	15	102 3.75	21	5		ND	4	3	2	2	16		0.1	6		2.09	69	0	109	1.94		0.01	1	1	5
WEA-R30			48 29	236	110	0.1		117	45 18.9	84	5		ND	5	1	2	2	25		.2	25		0.04	41	0	5	0.09	0.04		1	1	5
WEA-R31			7 275	317	36	0.5	25	16	14 7.69	3	5		ND	2	1	2	2	1		01			0.02	165	0	5	0.01		0.02	1	1	5
WEA-R32			5 57	67	27			359	12 9.56	11	5		ND	4	1	2	2	2	0.02	0	14		0.09	335	0	5	0.14		0.02	1	1	5
WEA-R33			1 3	9	1	0.1	5	1	41 1.41	3	5		ND	3	1	2	2	1	0.01	0	4		0.01	8	0	5	0.1		0.01	1	1	5
WEA-R34	566827	5475681	1 15	7	20	0.1	11	7	322 1.68	2	5	ND	ND	2	1	2	2	3	0,01	0	10	134	0.02	75	0	5	0.17	0.01	0.02	1	1	5
WEA-R35	567338	5475127	1 7	3	15	0.1	14	14	68 2.28	60	5	ND	ND	2	1	2	2	5	0.01	0	10	96	0.13	16	0	163	0.42	0.02	0.02	1	1	20
WEA-R37			2 334	9271	26	28.9	5	1	34 1.21	3	5	41	ND	1	1	2	35	3	0.01	0	1	168	0.01	5	0	59	0.06	0.01	0.01	1	1	47000
WEA-R38			1 73	753	20	0.3	13	10	401 1.44	2	5	ND	ND	6	1	2	6	5	0.07	0	12	125	0.18	330	0	18	0.3	0.02	0.02	1	1	230
WEA-R40			1 30	136	46	0.4	9	4	279 2.42	47	5	ND	ND	1	1	2	2	4	0.01	0	30	130	0.02	41	0	5	0.26	0.01	0.02	1	1	680
WEA-R41			1 4	3	9	0.1	11	60	69 2.57	2	5	ND	ND	f	t	5	2	4	0.01	0	14	122	80.0	11	0	52	0.23	0.01	0.02	1	1	5
WEA-R42			9 1751	29709		10	15	12	549 3,45	56	5	ND	6	23	11	11	2	7	0.31	0			0.17	7	0	841	0.1	0.01	0.02	1	1	12100
WEA-R43			1 81	1206	118	0.3	8	1	102 2.31	2	5		ND	6	1	2	2	3	0.02	õ			0.04	12	ō	19	0.24		0.02	1	1	430
WEA-R44			1 49	133	26	0.1	7	4	151 3.92	38	5		ND	7	í	2	2		0.01	õ		124		41	0.1	5	0.71	0.09		1	1	5
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WEA-R45		4	481	6322	246	7.5	7	1	13 1.78	20	5	9	ND	2	1	6	2		0.01 0	8	89	0.01	7	0	125	0.12		0.01	1		16000
26670		1	250	1072	139	0.2	36	41	1327 5.86	24	5	ND	ND	6	1	2	2	21 0	0.04 0.1	10	51	0.1	69	0	8	0.83	0.01	0.01	1	2	100
26671		1	53	34	51	0.1	21	16	757 3.84	14	5	ND	ND	5	1	3	2	26 0	03 0	2	148	0.1	45	0	5	0.36	0.01	0.02	1	1	10
26672		1	258	77	34	4.9	21	15	1175 3.29	33	5	ND	ND	4	1	2	2	34 0	.02 0	1	179	0.05	31	0	5	0.3	0.01	0.02	1	1	1300
26673		1	31	174	44	0.2	12	5	256 1.9	2	5	ND	ND	2	1	2	2	6 0	0 201	11	128	0.08	16	0	5	0.32	0.05	0.02	1	1	550
26674		4	227	1818	223	0.7	13	10	1399 3.82	13	5	ND	ND	1	1	4	2	50	0 10.	17	134	0.05	13	0	5	0.27		0.02	1	1	960
26675		3	580	6214	775	0.7	43	55	2658 7.73	14	5	ND	ND	Ś	6	Â	2		.15 0.2	22	34	0.3	19	õ	5	0.83		0.02	÷	2	40
26676		1	46	465	251	0.2	15	7	492 3.3	2	5	ND	ND	ž	4	ž	2		0.03 0		134	0,06	16	õ	5	0.21		0.02	4	1	5
				32	100	0.2	42	48	686 7	4	5	ND	ND	-	3	2	2			7				õ	5					2	
26677		1	64							2	•			7	3	5	_	-	0.14 0.2 0.07 0	•	40	2.64	17	-	-	2.92		0.02	4	-	5
26678		1	9	1	26	0.2	18	13	155 2.06		5	ND	ND	5	1	2	2			20	41	0.38	8	0	5	0.8		0.02	7	1	5
26679		1	38	51	41	0.1	15	27	377 3.04	2	5	ND	ND	4	1	3	2		0.12 0.1	7	20	0.69	7	0	5	0.85		0.01	1	1	340
26680		1	27	30	30	0.3	12	18	646 2.87	2	5	ND	ND	4	1	2	2		0.1 0	12	75	0.46	8	0	5	0.87		0.01	1	1	20
26681		1	14	241	71	0.1	16	13	548 2.83	2	5	ND	ND	8	1	2	2		0.17 0.1	21	65	0.24	24	0	7	0.87	0.01	0.02	1	1	120
26682		1	4	32	24	0,1	11	9	165 1.47	4	5	ND	ND	3	1	2	2	50	06 0	17	97	0.12	22	0	7	0.6	0.01	0.01	1	1	5
26683		1	35	60	87	0.1	15	14	375 2.55	8	5	ND	ND	3	1	2	2	10 0	05 0	13	92	0.08	20	0	5	0.41	0.09	0.02	1	1	220
26684		2	8	9	42	0.1	33	11	148 1.64	6	5	ND	ND	5	1	2	2	50	.13 0	13	130	0.16	14	0	122	0.43	0.05	0.02	1	1	20
26685		2	44	230	93	0.3	11	5	344 1.58	5	5	ND	ND	3	1	2	2	60	0 30.	12	108	0.13	12	0	30	0.52		0.02	1	1	240
26686		32		31134	1048	51.5	5	1	89 2.74	57	5	ND	9	11	7	27	2		0.02 0	3	134	0.04	7	0	472	0.21		0.02	1	1	2800
26687		4	24	3915	406	0.8	10	9	209 2	11	5	ND	NĎ	4	1	5	2		0.05 0	14	82	0.25	20	õ	48	0.75		0.02	÷	1	40
		3	27 8	280	186			16	247 2.41	14	5	ND	ND	~	4		2			• •			20	ő	-10				1	1	
26688		-	-			0.3	13				-			4	1	2				25	106	0.14		-	-	0.44		0.01	1	•	30
26689		1		55	56	0.1	9	3	273 1.77	2	5	ND	ND	2	1	2	2		02 0	20	40	0.04	15	0	5	0.2		0.01	1	1	110
900		4	153	1095		1	25	30	967 4.89	63	5	ND	ND	6	6	7	2		0.13 0.1	8	97	0.25	19	0	106	0.55		0.02	1	1	820
901		5	161	80	253	0.4	18	14	909 4.48	154	5	ND	ND	26	5	23	5	99 1	.29 0.1	6	91	3.19	14	0	57	2.64	0.01	0.05	7	2	10
902		3	35	403	297	0.1	20	15	175 2.81	6	5	ND	ND	4	1	2	2	90	0.11 0.1	17	48	0.97	20	0	30	1.1	0.01	0.02	1	t	50
903		2	10	98	156	0.1	16	13	94 2.25	3	5	ND	ND	2	1	2	2	70	0 80.0	14	33	0.64	22	0	14	0.77	0.03	0.02	1	1	60
904		2	13	187	146	0.1	20	16	98 2.76	2	5	ND	ND	3	1	2	2	60	0 80.	21	38	0.48	22	0	42	0.69	0.02	0.02	1	1	40
905		2	22	26	333	0.5	12	10	281 2.43	28	5	ND	ND	4	1	4	2	-	03 0	9	82	0.09	13	ō	45	0.23		0.02	1	Ť	5
906		3	6	1	17	0.2	12	14	109 2.29	15	5	ND	ND	3	1	2	2		01 0	6	71	0.03	12	õ	86	0.24	0.02		1	1	20
		2	9		107	0.1	51	63	407 6.03	5	5	ND	ND	ž	-	-	2		01 0	1	68	0.52	17	ő	168	0.64	0.01		1	1	460
26690		4	-	15						-	-			~		4				•				-					•	-	
26691	1	4	8	17	65	0.1	31	84	2117 8.67	9	5	ND	ND	Ś.	2	-	2		.02 0.1	10	27	0.14	42	0	48	0.42		0.02	1	2	30
26692		2	4	1	50	0.1	10	7	377 2.27	2	5	ND	ND		1	2	2		.01 0	1		0.15	25	0	28	0.24		0.02	1	1	20
26693		1	3	4	22	0.1	23	39	45 2.92	4	5	ND	ND	1	1	4	2		.01 0	1	66	2.19	14		519	1.97		0.03	2	1	10
26694		2	4	1	26	0.1	11	17	229 1.14	2	5	ND	ND	2	1	2	2	50	.02 0	2	147	0.11	19	0	5	0.28	0.01	0.02	1	1	5
26695		2	20	2	16	0.1	13	10	553 4.62	2	5	ND	ND	3	1	3	2	40	03 0	8	106	0.1	20	0	5	0.19	0.01	0.02	1	1	5
26696		1	4	1	22	0.1	6	- 4	251 2.27	2	5	ND	ND	4	1	2	2	4 0	06 0	46	41	0.13	28	0	- 5	0.46	0.09	0.02	1	1	5
26697		3	5	1	35	0.1	20	76	143 2.86	6	5	ND	ND	4	1	5	2	60	14 0	6	66	1.02	18	0	381	0.54	0.07	0.02	1	1	5
26698		2 3	2681	2601	14	7.4	8	1	41 1.16	2	5	28	ND	1	1	2	14	20	.01 0	4	159	0.02	9	0	158	0.09	0.02	0.02	2	1 :	29000
26699		1	28	17	14	0.1	9	28	79 0.98	5	5	ND	ND	7	1	2	2	4 0	17 0	13	95	0.25	26	0	148	0.28	0.07	0.02	1	1	340
26700		6	14	11	29	0.1	30	19	148 2.99	10	5	ND	ND	4	1	5	2	23 0	23 0.1	8	56	1.37	22	Ó	192	1,63	0.01	0.02	2	1	80
26751		2	11	1	16	0.1	9	9	194 0.8	2	5	ND	ND	3	ŕ	2	2		04 0	7		0.17	14	ō	18	0.24	0.08		1	1	20
26752		3	40	8	91	0.2	29	19	651 5.66	12	5	ND	ND	1		6			01 0	3		2.13	9	õ	5	2.73	0.01		1	3	10
26753		2	8	1	8	0.1	23	3	59 0.64	2	5	ND	ND	2	1	2	2		01 0	4		0.11	š	õ	5	0.19	0.04		1	1	30
		_	-	1	-		40	-		2	-	ND	ND	2		~	-			30	80		-	õ	5	1.22			1	1	10
26754		2	84	•	16	0.1	10	19	117 2.36		5			•	4	3	2					0.42	16	-	-		0.05		•	•	
26755		2	118	1	56	0.3	44	19	82 5.25	3	5	ND	ND	13	1	8			.02 0.1	9		1.23	36	0	7	2.94	0.01		1	3	110
26756		2	8	1	4	0.1	7	4	25 1.48	2	5	ND	ND	1	1	3	2		.01 0	18	100	0.54	17	0	8	0.65	0.04		1	1	10
26757		2	5	1	9	0.1	7	1	24 0.82	2	5	ND	ND	2	1	2	2	40	.01 0	1		0.15	5	0	5	0.22		0.03	1	1	5
26758		3	4	14	91	0.1	32	15	651 7.42	10	5	ND	ND	6	6	8	2	14 0	.17 0	6	20	7.97	24	-	313	1.73	0.05	0.03	1	1	50
26759		7	8	54	23	0.1	12	4	278 1.71	2	5	ND	ND	3	1	2	2	6 0	.03 0	22	157	0.42	16	0	115	0.43	0.05	0.02	1	1	380
26760		3	3	3	13	0.3	13	5	223 1.61	3	5	ND	ND	17	1	5	2	60	.49 0	16	38	1.33	31	0	93	0.59	0.01	0.02	2	1	140
26761		2	6	1	22	0.1	17	11	122 2.95	2	5	ND	ND	4	1	2	2		.03 0	11	74	0.08	13	0	561	0,19	0.01		1	1	3900
26762		3	89	37	35	0.1	13	47	122 8.88	16	5	ND	ND	7	1	5	2		.02 0.1	5	94	0.46	44	-	069	0.71		0.07	8	İ	5
26763		2	14	14	25	0.1	11	3	254 1.89	2	5	ND	ND		÷	2	ź		.02 0.1	40	89	0.09	32	ō,	5	0.57	0.02		1	t	140
		<u> </u>	14 8		_∠⊃ 5					2	5	ND		4	4	2	2		-				32 25	0	5	0.32		0.07	3	1	5
26764		1	-	46	-	0.1	7	4	161 1.33		-	-	ND	1	1				• •	18	48	0.03		-					-	4	-
26765		1	6	83	33	0.1	14	10	224 1.85	2	5	ND	ND	2	1	2	2		.01 0	23	56	0.19	29	0	5	0.53	0.02		1	1	30
26766		2	23	109	21	0.4	4	1	114 1.12	10	5	ND	ND	1	1	2	2	30	.01 0	4	83	0.02	6	0	5	0.15	0.02	0.07	5	1	1060

26767	16	46	96	44	0.6	19	9	773 3.3	33	5	ND	ND		2.5	7	2	13		0	11		2.22	15	0	539	0.65	0.01 0.0				
26768	1	36	8	11	0.4	8	1	561 1.46	18	5	ND	ND	3	1	2	2	3	0.03		2		0.03	12	0	130	0,11	0.01 0.0			210	00
26769	2	1	12	11	0.1	21	6	388 1.96	9	5	ND	ND	11	1	2	2	6			28		0.64	17	0	30	0.39	0.01 0.0	07 5	i 1	1	5
26770	3	1	15	7	0.1	23	13	264 2.35	10	5	ND	ND	12	1	2	2	8	0.58	0.1	5	24	0.87	15	0	94	0.57	0.01 0.0)6 t	; •	1 (60
26771	12	55	15	31	0.4	17	8	1870 3.29	35	5	ND	ND	8	1	2	2	6		0	3	84	0.07	10	0	333	0.23	0.05 0.0)7 4		1 281	80
26772	4	5	7	19	0.1	33	24	814 3.34	17	5	ND	ND	6	1	2	2	9			9	36	1.84	21	0	250	0.47	0.03 0.0)8 2	: :	1 4	40
26773	17	12	62	96	0.1	32	109	13530 19.5	47	5	ND	ND	11	1	2	5	18	0.09	0	4	28	1.93	40	0	129	0.05	0.02 0.0	02 17	' 1	1 13	40
26774	2	3	8	23	0.1	15	11	525 2.03	17	5	ND	ND	15	1	2	2	9	0.92	0,1	10	22	0.87	24	0	69	0,57	0.06 0.0)6 S	, · ·	1 (60
26775	2	3	17	34	0.1	47	45	430 5.05	15	5	NÐ	ND	1	1	2	2	162	0.06	0.1	1	18	3.67	15	0	120	3.64	0.02 0.0)5 1	1	3	5
26776	1	4	7	22	0.1	18	16	1440 4.1	6	5	ND	ND	6	1	2	2	13	0.1	0	10	32	0.33	52	0	16	0.54	0.05 0.0	07 1		1 .	10
26777	1	3	1	33	0.3	9	7	388 2,72	2	5	ND	ND	6	1	2	2	8	0.01	0	88	51	0.09	29	0	5	0.51	0.02 0.0	6 1	1	1 30	80
26778	2	6	83	72	0.8	23	8	622 3.7	20	5	ND	ND	30	1	2	2	15	0.99	0	25	73	0.71	24	0	134	0.51	0.02 0.0)6 <u>5</u>		1 15	80
26779	1	3	1	24	0.2	14	15	416 4.65	2	5	ND	ND	1	1	2	2	8	0.02	0	1	52	0.37	13	0	23	0.47	0.01 0.0)4 1			40
26780	1	3	1	15	0.3	10	3	203 1.58	2	5	ND	ND	1	1	2	2	5	0.01	0	2	90	0.03	12	0	41	0.18	0.03 0.0)6 1		1 23	30
26781	1	2	1	23	0.1	8	8	147 1.74	2	5	ND	ND	2	1	2	2	4	0.01	0	13	39	0.14	18	0	14	0.41	0.04 0.0	05 1		۱ ·	10
26782	4	3	9	20	0.1	12	6	50 1.79	8	5	ND	ND	2	1	2	7	9	0.01	0	17	46	0.22	22	0	5	0.56	0.02 0.0	3 2			30
26783	3	62	52	151	2.5	13	11	563 2.44	6	5	ND	ND	2	1	2	4	8	0.01	Ó	19		0.04	21	Ó	20	0.26	0.02 0.0	5 2		1 14	40
26784	2	13	6	40	0.3	7	8	212 1.85	ź	5	ND	ND	2	Í	2	2	4	0.01	Ō	9		0.02	15	ō	112	0.21	0.02 0.0				50
26785	4	16	9	67	0.2	11	10	539 2.42	4	5	ND	ND	1	1	2	5	7	0.01	õ	26		0.03	27	ō	66	0.29	0.01 0.0				00
26786	3	18	5	58	0.2	13	17	642 2.43	8	š	ND	ND	1	1	2	3	6		õ	22		0.03	24	ŏ	89	0.3	0.01 0.0				10
26787	2	5	9	52	0.1	14	14	631 2.27	8	5	ND	ND	4	i	2	2	6		ŏ	9		0.05	23	ŏ	18	0.37	0.01 0.0				5
26788	2	6	20	36	0.1	12	20	577 1.98	13	5	ND	ND	3	1	2	2	8		ŏ	44		0.07	26	ŏ	5	0.45	0.03 0.0			•	5
26789	2	10	14	42	0.1	17	20	882 2.83	.9	5	ND	ND	3	1	2	6	9		ŏ	30		0.11	22	ŏ	5	0.41	0.02 0.0			•	70
26790	2	4	1	20	0.1	10	11	355 2.73	3	5	ND	ND	3	1	2	2	8		0	1		0.27	14	õ	45	0.45	0.02 0.0				10
	_								9	5		ND	-		2		7			•				ŏ	40 5						5
26791	4	4	11	37	0.1	14	11		-	-	ND		4	1	-		-		0.1	12	41	0.2	21		-	0.4	0.02 0.0			•	_
26792	1	2	1	1	0.1	8	29	589 1.88	2	5	ND	ND	4	1	2	2	4	0.04	0	21		0.16	20	0	5	0.52	0.02 0.0				5
26793	1	101	9	11	0.1	6	17	212 1.14	2	5	ND	ND	16	1	2	2	22		0	3		0.28	96	0.1	5	2.84	0.01 0.0		1		5
26794	1	21	1	6	0.1	12	37	96 1.18	2	5	ND	ND	6	1	2	2	9		0	42		0.06	69	0	5	2.25	0.03 0.0				10
26795	1	144	3	3	0.1	11	7	480 0.92	2	5	ND	ND	5	1	2	2	4	0.01	0	30		0,04	38	0	5	0.41	0.03 0.0			· -	40
26796	1	197	27	1	0.7	4	1	49 0.93	2	5	ND	ND	1	1	2	2	3		0	5		0.01	8	0	85	0.1	0.06 0.0				
26797	2	80	14	2	0.2	-4	3	84 0.96	2	5	ND	ND	3	1	2	4	7		0	33		0.04	39	0	5	0.47	0.02 0.0				70
26798	1	9	1	23	0.2	3	12	13 2.12	5	5	ND	ND	1	1	2	2	4		0	10		0.18	20	0	5	0.42	0.09 0.0			•	5
26799	2	4	1	14	0.1	3	3	19 0.82	2	5	ND	ND	1	1	2	2	3		0	1		0.06	5	0	5	0,19	0.08 0.0				5
26800	1	3	1	18	0.1	15	24	13 2.99	3	5	ND	ND	1	1	3	2	10		0	1		1.43	18	0	340	1.61	0.08 0.0				5
26801	2	30	24	92	0.3	22	27	233 3.57	40	5	ND	ND	3	1	2	2	13		0	6		0.62	39	0	291	1.48	0.07 0.0				5
26802	12	188	7271	815	10.6	3	14	23 3.07	95	5	ND	ND	4	3	2	2	2		0	7		0.02	353	0	121	0.3	0.07 0.0				
26803	2	25	123	139	0.2	24	10	121 3.12	2	5	ND	ND	1	1	2	2	22			16		2.48	28	0	5	2.82	0.01 0.0				80
26804	2	110	619	211	1.4	14	29	746 3.4	18	5	ND	ND	4	1	2	2	8		0	1	120		11	0	123	0.25	0.01 0.0				
26805	3	47	357	573	0.2	17	31	686 3.93	2	5	ND	ND	6	3	2	2	9			16		0.24	21	0	70	0.53	0.02 0.0				00
26806	1	4	95	56	0.1	10	15	267 1.19	2	5	ND	ND	7	1	5	2	6		0	26		0.46	21	0	25	0.45	0.01 0.0				50
26807	2	3	16	14	0.1	8	6	18 0.67	2	5	ND	ND	1	1	7	2	4	0.01	0			0.12	3	0	5	0.13	0.01 0.0				5
26808	2	4	16	11	0.2	14	20	128 2.01	2	5	ND	ND	2	1	5	2	4	0.02	0	12	100	0.2	12	0	30	0.32	0.01 0.0				30
26809	1	198	124	1	1.1	6	5	1 1.59	2	5	ND	ND	1	1	2	2	3		0	6	151		8	0	27	0.13	0.01 0.0		,		60
26810	1	17	54	1	0.3	4	3	1 0.9	2	5	ND	ND	1	1	2	2	3		0		131		7	0	78	0.03	0.01 0.0				90
26811	2	16	198	21	0.9	9	16	63 1.91	2	5	ND	ND	1	1	7	2	3		0	13		0.08	14	0	18	0.43	0.03 0.0	_			
26812	1	59	132	11	0.7	9	12	14 1,89	2	5	ND	ND	2	1	2	2	3		0	10	108		10	0	240	0.17	0.01 0.0				
26813	4	16	110	18	0.3	12	21	153 2.67	2	5	ND	ND	2	1	2	2	5		0			0.04	16	0	57	0.34	0.01 0.0				
26814	2	116	17	58	0.3	12	16	181 2.1	9	5	ND	ND	10	1	5	2	4	0.18	0	12		0.25	28	0	250	0.26	0.01 0.0				
26815	2	11	22	107	0.3	17	18	249 2.28	11	5	ND	ND	20	1	10	3	4		0	4		1.04	15	0	148	0.2	0.08 0.0				70
26816	4	192	251	90	0.8	44	71	943 6.98	16	5	ND	ND	31	3	20	3	84		0.1	3			229	0	121	1.57	0.01 0.0				60
26817	7	138	919	97	8.4	30	58	674 5.94	5	5	ND	ND	7	1	3	2	29		0	1			121	0	494	0.43	0.01 0.0				
26818	4	105	2034	109	3.4	34	85	881 6,2	8	5	ND	ND	5	1	2	2	18		0.1	3		0.15	164	0	194	0.48	0.04 0.0				
26819	14	98	5418	79	20.7	23	57	609 6.12	2	5	ND	ND	12	1	2	19	18	0.03	0.1	11		0.09	270	0	249	0.43	0.1 0.0				
26820	1	6	72	18	0.4	12	22	174 1.79	3	5	ND	ND	3	1	10	2	8	0.03	0	4	93	0.57	22	0	66	0.7	0.11 0.0	02 3	1		40
26821	1	7	17	26	0.3	17	26	77 2.49	9	5	ND	ND	2	1	2	2	8	0.02	0	9	66	0.65	20	0	280	0.91	0.01 0.0	12 1	1	2	20

												-						-	-											
26822			1	9	1	29	0.2	16	30	101 2.87	4	5	ND	ND	3	1	2	2	5		0	12		0.17		0 214			1	1 100
26823			4	9	3	22	0.2	24	107	15 4.64	7	5	ND	ND	1	1	2	2	3	0.01	0	3		0.01		0 1081	0.21	0.03 0.01	1	1 240
26824			1	4	1	22	0.1	9	21	232 1.81	2	5	ND	ND	1	1	2	2	3	0.01	0	6		0.32		0 183	0.2		1	1 10
26825			3	4	11	7	0.7	19	39	346 3.19	3	5	ND	ND	2	1	5	5	14		0	1		1.43		0 273	0.24		7	1 1080
26826			4	11	23	40	1.1	25	49	519 3.94	2	5	ND	ND	8	1	8	2	21	0.19	0	2		0.64		0 430	0.35	0.01 0.02	8	1 1000
26827			3	3	9	1	0.2	14	21	214 1.8	2	5	ND	ND	13	1	10	5	4	0.28	0	10		0.18		0 118	0.18	0.01 0.02	9	1 100
WE-1	567788	5472196	5	67	70	15	0.8	4	1	97 1.31	<2	<8	4	7	2	<.2	3	з	6	0.01	0	20	20	0.02	41 <.0	1 <3	0.21	0.03 0.16	6	2869
WE-2	567788	5472196	2	59	34	48	1.8	- 14	13	272 3.74	2	<8	25	5	5	0.3	6	<3	6	< 01	0	15	54	0.01	41 <.0	1 <3	0.33	0.04 0.11	<2	7054
WE-3	567788	5472196	5	89	42	89	0.4	14	8	212 4.77	2	<8	3	6	3	0.4	8	<3	6	<.01	0	13	23	0.01	30 <.0	1 <3	0.24	0.02 0.1	9	3325
WE-4	567788	5472196	2	38	149	11	0.5	4	2	217 1.01	<2	<8	<2	2	12	<.2	<3	<3	4	<.01	0	6	66	0.01	1659 <.0	1 <3	0.09	0.02 0.07	2	776.7
WE-5	567788	5472196	3	71	500	9	4.8	5	<1	55 1.42	<2	<8	11	6	2	<.2	4	14	6	<-01	0	22	27 •	0.01	264 <.0	1 <3	0.15	0.02 0.2	8	10059
WE-6	565740	5472817	12	68	267	213	1.6	12	6	45 3.8	110	<8	4	8	1	< 5	<3	<3	1	0.01	0	19	18	0.01	26 <.0	14	0.34	0.01 0.17	8	3462
WE-7	565740	5472817	6	102	708	487	2.4	7	2	51 3.72	137	<8	5	7	1	1.6	<3	<3	4	0.01	0	15	69	0.01	28 <.0	1 3	0.33	0.01 0.18	4	3879
WE-8	565931	5472932	3	4	11	8	<.3	8	2	103 1.75	3	<8	<2	11	1	<.5	<3	<3	2	0.01	0	27	33	0.28	21 <.0	1 <3	0.51	0.02 0.09	10	39.6
WE-9	565908	5472884	1	6	6	35	<.3	7	7	60 1.69	2	<8	<2	5	1	<.S	<3	<3	1	0.01	0	11	67	0.02	8 <.0	1 <3	0.13	0.04 0.03	4	2047
WE-10	565903	5472876	3	4	4	6	<.3	9	8	112 3.73	6	<8	<2	6	3	<,5	<3	<3	<1	0.01	0	17	23	0.02	31 <-0	1 <3	0.16	0.03 0.06	10	667.9
WE-11	565805	5472823	1	7	4	24	<.3	12	9	552 2.81	<2	<8	4	8	3	< 5	<3	<3	3	0.02	0	12	56	0.07	39 <.0	1 3	0.32	0.04 0.11	2	1597
WE-12	565728	5472681	4	9	8	7	<.3	7	2	67 2.13	<2	<8	<2	<2	3	<.5	<3	<3	24	0.02	0	<1	32	0.15	5 <.0	1 4	0.2	0.01 0.01	10	4.4
WE-13	565805	5472823	2	15	3	7	<.3	8	3	43 1.41	<2	<8	4	11	2	<.5	<3	<3	7	<.01	ō	3		0.26	27 <.0		0.6	0.01 0.16	3	3124
WE-14	565765	5473006			27425	, 9	86.2	7	<1	41 3.6	-	<8	42	<2	2	<.5	26	218	<1	<.01	õ	<1		<.01	10 <.0		0.02		17	34662
WE-15	566188	5473175	1	21	173	36	0.6	49	209	43 13.2	4	<8	<2	6	1	<.5	<3	3	2	0.01	ō	<1		0.44	24 <.0	• •	0,61	0.01 0.15	3*	93.6
WE-16	566170	5473143			22096	939	10.1	6	1	40 1.7	49	<8	14	4	4	6.2	5	š	<1	<.01	õ	8		0.01	222 <.0		0.18	0.01 0.12	15	28322
WE-17	566150	5473109			25754	4	120	7	2	27 2.76	16	<8	<2	<2	4	10	63	210	<1	<.01	ŏ	<1		<.01	14 <.0		0.03	<.01 0.02	5	1022
			3	12	707	29	0.8	8	5	78 3,47	4	<8	<2	10	1	<.5	<3	<3	<1	0.01	õ	27		0.04	25 <.0		0.34	0.02 0.12	8	201.6
WE-18	566137	5473087					-		-						•		-	-	~~		•			••••						
WE-19	569725	5473637	<1	9	262	13	0.3	11	26	119 1.18	4	<8	<2	12	6	<.5	<3	<3	29	0.16	0	36		0.41	19 0.	• •	0.98	0.04 0.16	<2	10.8
WE-20	569749	5475933	1	8	7	3	<.3	11	6	27 2.06	13	<8	<2	4	2	<.5	<3	<3	5		0	3		0.94	25 <.0		0.9	0.01 0.11	2	0.6
WE-21	569777	5475909	2	5	5	6	<.3	16	6	20 2.24	31	<8	<2	3	2	<-5	<3	<3	5	0.01	0	3		1.02	23 <.0		0.99	0.01 0.1	<2	1.8
WE-22	569797	5475893	1	4	<3	10	0.3	12	2	49 4.07	17	11	<2	2	1	-	<3	<3	12		0	23	13	1.9	22 <.0		1.89	<.01 0.07	<2	0.7
WE-23	569812	5475878	2	4	5	12	0.3	13	10	146 4,97	13	<8	<2	3	2	<.5	<3	<3	13	0.01	0	1		1.16	14 <.0		1.71	0.01 0.06	<2	<.2
WE-24	569820	5475867	12	5	5	22	0.4	22	77	621 4.86	4	<8	<2	,<2	1	<.5	<3	<3	10	<.01	0	1		0.04	24 <.0		0.35	< 01 0.01	5	1.2
WE-25	5698: 4	5475853	10	3	<3	17	0.4	26	54	3431 6,51	2	<8	<2	`<2	2	<.5	<3	<3	7	0.01	0	3		0.03	88 <.0		0.38	0.01 0.07	<2	8.9
WE-26	568880	5474868	2	8	6	11	<.3	6	3	281 2.58	5	10	<2	3	1	<.5	<3	<3	4	0.01	0	11		0.01	13 <.0	14	0.27	0.01 0.11	4	84.3
WE-27	568868	5474943	3	5	5	5	<.3	6	8	71 0.91	3	<8	<2	<2	2	<.5	<3	<3	1	0.01	0	9	19	0.04	8 <.0	1 <3	0.12	0.01 0.01	<2	5.7
WE-28	568847	5474936	2	13	17	з	<.3	15	15	55 1.58	47	<8	<2	<2	2	< 5	<3	<3	1	0.02	0	1	16	0.02	5 <.0	1 <3	0.06	0.01 0.01	5	5
WE-29	568716	5475466	1	2	12	27	<.3	11	8	79 4.08	57	10	<2	5	3	<.5	<3	3	5	0.01	0	14	22	1,72	16 <.0	1 <3	1.69	<.01 0.08	<2	1.5
WE-30	569020	5475234	1	4	<3	3	<.3	4	3	46 1.09	4	10	<2	6	3	<.5	<3	<3	3	<.01	0	16	19	0.03	8 <.0	1 3	0.23	0.04 0.02	<2	1.5
WE-31	565622	5472634	4	3	<3	6	<.3	7	7	178 1.61	2	<8	<2	3	1	< 5	<3	<3	2	<.01	0	3	16	0.04	11 <.0	1 <3	0.21	0.01 0.05	<2	1.9
WE-32	565622	5472634	2	5	3	11	<.3	7	3	235 1.21	2	<8	<2	7	1	<.5	<3	<3	- 4	0.02	0	26	16	0.22	19 <.0	1 <3	0.48	0.02 0.07	<2	0.6
WE-33	565622	5472634	3	3	<3	15	<.3	11	10	231 3.01	<2	<8	<2	3	1	<.5	<3	<3	2	<.01	0	13	14	0.03	14 <.0	1 <3	0.25	0.02 0.05	<2	26.2
WE-34	565622	5472634	<1	2	<3	7	<.3	8	9	31 1.33	2	<8	<2	3	1	<.5	<3	<3	1	<.01	0	2	10	2.07	30 <.0	1 <3	1.58	0.01 0.06	<2	0.2
WE-35	565622	5472634	3	3	4	29	<.3	23	12	499 4.14	<2	8	<2	5	1	<.5	<3	<3	4	0.01	0	4	14	0.06	26 <.0	1 <3	0.34	0.02 0.07	<2	25.4
WE-36	565615	5472611	3	4	5	12	<.3	19	6	149 2.68	4	<8	<2	3	2	<.5	<3	<3	4	0.01	0	1	12	80.0	14 <.0	1 3	0.24	0.01 0.08	3	3.6
WE-37	565601	5472560	3	4	4	3	<.3	5	4	42 1.75	4	<8	<2	3	1	<.5	<3	<3	2	<.01	0	2	16	0.08	6 < 0	1 <3	0.23	0.01 0.05	<2	5.7
WE-38	565602	5472530	1	3	<3	4	<.3	6	2	41 1.4	<2	<8	<2	3	1	<.5	<3	<3	<1	<.01	0	4	11	0.01	5 <.0	1 <3	0.29	0.03 0.01	2	34.8
WE-39	565561	5472593	3	5	<3	5	<.3	6	3	27 2.06	14	<8	<2	2	1	<.5	<3	<3	3	<.01	0	1	20	0.13	8 <.0	1 <3	0.26	0.01 0.05	<2	2.9
WE-40	565598	5472503	1	3	5	6	<.3	13	14	141 2.38	<2	<8	<2	2	2	<.5	<3	<3	4	<.01	0	2	15	0.29	14 <.0	1 <3	0.4	0.01 0.07	2	3.4
WE-41	565622	5472634	2	6	8	6	<.3	14	19	32 2.34	3	<8	<2	2	1	<.5	<3	<3	1	<.01	0	1	15	0.16	6 <.0	1 <3	0.23	0.01 0.03	<2	21.8
WE-42	565622	5472634	3	10	5	7	<,3	11	6	52 1.31	<2	10	<2	5	1	<.5	<3	3	2	0.01	0	4	14	0.37	14 <.0	1 <3	0.43	0.01 0.07	3	8.3
WE-43	566298	5473861	2	13	20	3	<.3	5	3	17 2.09	35	<8	<2	5	5	< 5	<3	3	6	<.01	0	8		0.01	31 <.0		0.18	0.07 0.03	<2	2.9
WE-44	567743	5472152	10	40	78	14	0.6	2	Ĩ	22 1.58	<2	<8	<2	10	7	<.5	<3	<3	4	< 01	ō	26		0.01	58 <.0		0.31	0.01 0.13	<2	493
WE-45	567743	5472152	18	27	11	10	<.3	3	1	18 2.16	<2	10	<2	14	3	<.5	<3	<3	6	<.01	0	42	-	0.01	49 <.0		0.49	0.01 0.15	<2	370.7
WE-46	567829	5472163	3	19	29	44	<.3	16	10	52 3.48	<2		<2	6	8	<.5	<3	<3	9	<.01	õ	17		0.01	40 <.0		0.21	0.03 0.28	<2	99.5
WE-47	567829	5472163	4	42	100		0.4	3	1	16 1.65	<2	<8	<2	16	6	<.5	<3	3	15	<.01	õ	48	-	0.02	37 <.0		0.23	0.01 0.17	<2	37.3
WE-48	567829	5472163	2	42 14	40	6	<.3	2	1	59 0.9	<2	<8	<2	6	12	<.5	<3	4	7	<.01	õ	21		0.01	24 < 0		0.16	0.01 0.14	<2	166.2
4479-40	001029	0712103	2	14	40	0	~.5	2	,	JJ U.S	~2	~Q	~4	0	42		-0		'	01	v	∠ ↓	3	v.v i	24 4.0	, -3	Q. 10	5.61 0.14	-4	100.2

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VLF-EM Results

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	Easting	Northing		Cu	Pb ppm		Ag ppm		Co	Mn ppm		As ppm			Hg ppm	Sr	Cd ppm i	Sb	Bi pom i	V	Ca %	Р %	La ppm	Cr DDM	Mg %	Ba pom	⊺i %	B ppm	Al %	Na %		W ppm p		u (AA) ppb
WEA-1	566037	5473611	5	60	52	147	6.3	56	79	500	19.39	144	NA	ND	ND	10	1	27	2	94	0.1	0.03	60	319	0.31	88	0.1	16	0.79	0.01	0.03	2	3	70
WEA-2	566230	5473707	1	40	1	57	0.1	42	36	483	17.69	2	NA	ND	ND		1	2	2	73	0.06	0.02	44	213	0.3	76	0.1	5	0.72	0.01	0.03	1	2	5
WEA-3	566479	5473545	5	57	35	67	0.4	67	99	770	23.22	11	NA	ND	ND		1	2	8	91	0.11	0.05	55	229	0.34	118	0.1	5	0.79	0.01	0.03	1	4	100
WEA-4	566779	5473614	4	55	79	81	0.3	61	69	495	20.16	22	NA	ND	ND		1	2	2	93	0.07	0.04	109	230	0.35	70	0.1	10			0.03	2	4	2660
		5473653	-	58	44	79	0.1	66	80	485	20.39	25	NA	ND	ND		1	2	10	91	0.08	0.04	114	242	0.43	85	0.1	11		0.01		1	4	40
		5470448		29	11	40	0.1	19	17	366	2.21	2	NA	ND	ND		1	2	2	72	0.77	0.02	16	69	0.5		0.3	7			0.04	5	2	5
		5471562	12	171	242	286	2.6	162	265	719	22.5	114	NA	ND	ND		1	9	8	73	0.25	0.13	127	143	0.85	88	0.1	309	1.04		0.04	11	4	10400
		5471655	4	69	44	68	0.2	95	198	489	19.85	47	NA	ND	ND		1	2	2	88	0.12		65	167	0.36		0.1				0.03	1	3	340
		5471296		103	71	126	0.4	119	248		18.89	78	NA	ND	ND		1	6	1	78		80.0	64	126	0.47		0.1				0.03	1	3	920
		5475180	6	52	61	68	0.1	73	131	441	17.47	39	NA	ND	ND		1	2	2	92		0.02	254	299	0.46	91	D.1					1	4	5
		5475212	6	107	82	116	0.2	85	187	627	19.48	57	NA	ND	ND		1	2	-	118	0.25	0.06	328	287	0.55	136	0.2	19			0.03	1	5	5
		5475118	-	71	84	80	0.1	88	161	580	20.16	73	NA	ND	ND		1	2	_	117 148	0.25		280 216	308 243	0.44		0.2		0.85		0.03	1	4	0050
		5474438	6	93	81	96	0.7	95	219		20.08	58	NA	ND	ND		4	2	_	177		0.06			0.56		0.2				0.05	1	2	9650
WEA-17			4	72	4/	76	0.1	4/	74	601	7.8	28 28	NA NA	ND	ND		1	2	-		• • • =	0.00	45	100			0.4	-			0.05	1	4	70
· · · - · · · •		5473243		50	23	62	0.1	43	70 36		9.93	20		ND	ND		4	2	2	150	0.89 0.83		19	95 50	0.68 0.53		0.3 0.3	-			0.04	, ,	3	100
WEA-19		5472833	-	43	10	42	0.1	26			4.13	400	NA	ND	ND	13	40	9	22	97		• • • •	9	59		•-	0.5	-			0.03	4	4	310
		5473070		251	140	551	2.9	95 61		2014	18.97 10.08	400 79	ວ 5	ND	ND ND	12	12	11	33	36 35	0.12	0.31	27 31	40 30	0.32	35 22	0	-	0.76	0.01	0.02	2	3 1	2060 560
		5474228 5474228		59 116	208 78	100 143	1.8 1.5	72	81 101	367 750	11.56	99	5	ND ND	ND	14	3	2	5	36		0.17	33	30 37	0.47	37	Ő	18		0.01	0.01	3	1	310

Gravity Data

				Bouguer Anomaly 2.70
Survey year	Station Line #	Easting	Northing	density
1995	A	565915	5472351	61.13
1995	Â	565922	5472360	61.47
1995	A	565922	5472300	61.6
	A	565922	5472394	61.92
1995				
1995	A	565936	5472410	•
1995	A	565936	5472428	62.79
1995	A	565943	5472447	62.45
1995	A	565950	5472466	62.42
1995	A	565957	5472481	62.28
1995	A	565957	5472502	61.42
1995	A	565913	5472511	61.01
1995	A	565906	5472497	61.15
1995	A	565899	5472474	61.46
1995	A	565892	5472453	61.79
1995	A	565885	5472426	62.02
1995	A	565885	5472408	61.58
1995	A	565878	5472390	61.44
1995	A	565871	5472373	61.9
1995	Α	565857	5472355	. 61.84
1995	A	565849	5472425	61.74
1995	А	565849	5472443	61.77
1995	А	565848	5472458	60.8
1995	А	565855	5472477	60.71
1995	А	565855	5472498	60.72
1995	А	565862	5472514	61.14
1995	А	565869	5472533	60.79
1995	A	565869	5472550	
1995	А	565876	5472564	60.46
1995	A	565840	5472569	60.59
1995	А	565833	5472556	60.75
1995	А	565826	5472540	60.92
1995	А	565826	5472529	60.99
1995	A	565826	5472506	61.05
1995	А	565819	5472488	60.75
1995	А	565812	5472474	60.84
1995	В	565966	5472312	60.37
1995	В	565973	5472329	60.6
1995	В	565980	5472361	60.66
1995	В	565987	5472392	60.65
1995	В	566001	5472408	61.05
1995	B	566016	5472427	61.04
1995	В	566031	5472386	61.07
1995	В	566024	5472360	60.59
1995	В	566009	5472341	60.16
1995	В	566002	5472322	60.14
1995	В	565966	5472313	60.43
1995	В	565959	5472288	60.42
1995	В	565959	5472272	60.11
1995	B	565952	5472248	60.01
1995	В	565945	5472229	59.44
1995	В	565946	5472217	60
1995	В	565924	5472210	59.49
1995	В	565902	5472189	59.18
1995	В	565888	5472179	59.12

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1995	В	565866	5472164	58.44
1995	В	565867	5472109	58.4
1995	В	565874	5472114	58.98
1995	В	565896	5472113	59.61
1995	В	565940	5472106	61.59
1995	В	565961	5472148	60.49
1995	В	565954	5472159	60.12
1995	B	565946	5472179	60.04
1995	B	565939	5472192	59.86
1995	B	565924	5472208	59.91
1995	B	565924	5472222	59.47
1995	В	565916	5472252	59.98
1995	B	566025	5472286	60.06
1995	B	566018	5472268	60.59
1995	В	566018	5472250	60.43
1995	В	566011	5472236	60.56
1995	В	565996	5472222	60.57
1995	В	565989	5472206	60.84
1995	B	565975	5472202	60.5
1996	1 Å	565920	5472578	62.54
1996	2 A	565924	5472596	62.62
1996	2 A 3 A	565927	5472611	62.74
1996	4 A	565938	5472628	62.74
1996	5 A	565939	5472626	62.47
1996	6 A	565944	5472665	62.47
1990	7 A	565950	5472683	62.4
1996	8 A	565957	5472698	62.63
1996	9 A	565956	5472719	62.03
1996	10 A	565913	5472729	61.97
1996	11 A	565906	5472725	62.01
1996	12 A	565901	5472692	62.45
1996	12 A 13 A	565894	5472692	62.45
1996	14 A	565886	5472644	62.69
1996	15 A	565886	5472625	62.5
1996	16 A	565882	5472607	62.43
1996	10 A 17 A	565869	5472590	62.59
1996	18 A	565855	5472572	62.72
1996	19 A	565846	5472642	62.51
1996	20 A	565851	5472660	62.35
1996	20 A 21 A	565850	5472676	62.04
1996	21 A 22 A	565855	5472695	61.91
1996	23 A	565853	5472715	61.87
1996	24 A	565863	5472732 *	
1996	25 A	565869	5472750	62.01
1996	26 A	565873	5472767	61.89
1996	20 A 27 A	565878	5472782	61.77
1996	28 A	565838	5472787	61.53
1990	20 A 29 A	565832	5472773	61.66
1996 1996	29 A 30 A	565828	5472758	61.73
1996	30 A 31 A	565825	5472747	61.8
1996	32 A	565823	5472723	61.81
1996 1996	32 A 33 A	565818	5472725	61.59
1996 1996	33 A 34 A	565814	5472705 5472692	61.59 61.78
1996	34 A 1 B	565963	5472592	62.28
1996	2 B	565973	5472529	62.20
1996 1996	2 B 3 B	565981	5472546 5472579	62.43 62.35
1996	3 B 4 B	565989	5472579 5472610	62.35 62.24
1996	4 D 5 B	566001	5472610	62.24
1990	UD	500001	J472020	02.4

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1996	6 B	566015	5472645	62.29
1996	7 B	566032	5472603	62.52
1996	8 B	566023	5472578	62.42
1996	9 B	566007	5472559	62.33
1996	10 B	566000	5472540	62.25
1996	11 B	565970	5472530	62.46
1996	12 B	565960	5472506	62.57
1996	13 B	565958	5472490	62.33
1996	14 B	565953		62.39
1996	15 B	565949	5472447	61.98
1996	16 B	565943	5472435 🔍	62.47
1996	17 B	565923	5472428	61.99
1996	18 B	565899	5472407	61.81
1996	19 B	565886	5472397	61.88
1996	20 B	565869	5472382	61.54
1996	21 B	565865	5472327	61.42
1996	22 B	565877	5472332	61.66
1996	23 B	565893	5472331	61.83
1996	30 B	565955	5472354	62.27
1996	31 B	565959	5472366	62.34
1996	32 B	565954		62.25
1996	33 B	565948	5472397	62.27
1996	34 B	565938	5472410	62.24
1996	35 B	565927	5472427	62.1
1996	36 B	565923	5472440	62.06
1996	37 B	565916	5472454	61.97
1996	38 B	566024	5472503	62.29
1996	39 B	566018	5472486	62.41
1996	40 B	566019	5472468	62.38
1996	41 B	566009	5472453	62.45
1996	42 B	565999	5472440	62.47
1996	43 B	565987	5472424	62.63
1996	4 4 B	565978	5472419 ~	62.38
1996	100 C	565931	5472678	62.74
1996	101 C	565926	5472703	62.06
1996	102 C	565917	5472726	61.94
1996	103 C	565909	5472744	61.57
1996	104 C	565906	5472770	61.78
1996	105 C	565909	5472794	61.84
1996	106 C	565909	5472816	61.7
1996	107 C	565914	5472834	61.67
1996	108 C	565920	5472859	61.6
1996	109 C	565924	5472881	61.53
				61.32
1996	110 C	565923	5472901	
1996	111 C	565936	5472921	61.4
1996	112 C	565936	5472943	61.48
1996	114 C	565944	5472987	61.55
1996	115 C	565947	5473009	61,53
1996	116 C	565963	5473027	61.51
			5473054	
1996	117 C	565965		61.54
1996	118 C	565965	5473082	61.57
1996	119 C	566021	5473057	61.58
1996	120 C	566014	5473035	61.62
1996	121 C	566010	5473012	61.55
1996	122 C	566005	5472984	61.58
		565997	5472954	
1996	123 C			61.8
1996	124 C	565992	5472929	61.58
1996	125 C	565988	5472909	61.56

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1996	126 C	565992	5472883 🖕	61.69	
1996	127 C	565976	5472868	61.45	
1996	128 C	565977	5472849	61.65	
1996	129 C	565977	5472834	61.76	
1996	130 C	565977	5472816	61.98	
1996	130 C	565960	5472800	61.92	
1996	137 C	565959			•
				61.98	
1996	133 C	565955		62	
1996	135 C	565950	5472718	62.11	
1996	136 C	565951	5472694	62.27	
1996	137 C	565953	5472675	62.26	
1996	138 C	565947	5472655	62.49	
1996	139 C	565944	5472634	62.19	
1996	140 C	565941	5472618	62.28	
1996	141 C	565936	5472602	62.25	
1996	142 C	565996	5472613	62.18	
1996	143 C	565994	5472643	61.08	
1996	144 C	565995	5472644	62.62	
1996	146 C	566005	5472665	62.63	
1996	147 C	566009	5472683	62.35	
1996	148 C	566014		62.67	
1996	149 C	566022		62.32	
1996	150 C	566025		62.27	
1996	150 C	566022		62.29	
1996					
	200 D	566074		61.71	
1996	201 D	566056	5472956	61.52	
1996	202 D	566039	5472961	61.5	
- 1996	203 D	566019	5472965	61.75	
1996	204 D	566003	5472971	61.7	
1996	205 D	565978	5472976	61.72	
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1996	219 D 220 D		5472883		
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1996	222 D	565960	5472892	61.45	
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1996	224 D	565923	5472901	61.26	
1996	225 D	565905	5472901	61. 1 6	
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1996	235 D	565995	5472768	62.3	
1996	236 D	565976	5472774	61.99	
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1996	239 D		565909	5472794	61.71	
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1996	502 E		565929	5472636	62.55	**
1996	503 E		565922	5472640	62.36	
1996	504 E		565916	5472646	62.04	
1996	505 E		565907	5472654	62.15	
1996	506 E		565898	5472661	62.32	
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1996	1017	1	567023	5472903 -	61.83	
1996	1018	1	566970	5472953	62.09	
1996	1019	1	566917	5473004	62.36	

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1996	1007 A		567211	5471214	62.83
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1996	1008 A		567286		
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1996	1013 A		567327	5470876 ु	63.1
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1996	1013		567533	5473612	62.5
1996	1014		567614	5473600	62.47
1996	1015		567661	5473595	62.53
1996	1016	-	567716	5473596	62.76
1996	1017		567795	5473607	62.74
1996	1018		567853	5473633	62.8
1996	1019		567924	5473664	63.09
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1996	1025		568308	5473895	63.43
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1996	1031		568341	5474428	63.3
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1996	1032		568242	5474581	62.81
1996	1033		568212	5474640	62.62
1996	1034		568175	5474040	62.63
1996	1035		568109	5474739	62.03
1990	1030		568006	5474807	62.74
1996	1037		567980	5474885	62.16
1996	1038		567969		62.10
1990	1039	0	507 505	0-1-300	02.10

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1996	1040 C		567922	5474870	62.38	
1996	1041 C		567899	5474753	62.63	
1996	1042 C		567906	5474689	62.73	
1996	1043 C		567887	5474659	62.55	
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1996	1050 C		567575		61.44	
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	1053 C 1054 C					
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1996	1055 C		567604	5474893	61.39	
1996	1056 C		567668	5474805 [°]		
1996	1057 C		567696	5474724	61.51	
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1996	1000 D		567040	• • • • • • • •	61.91	
1996	1010 D		567025			
1996	1020 D		567008	5472912 🔍	61.98	
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1996	1040 D		566960	5472961	62.14	
1996	1050 D		566931	5472989	62.28	
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1996	1160 D		566612	5473254	62.32	
1996	1170 D		566572	5473285	62.41	
1996	1180 D		566521	5473314	62.46	
1996	1190 D		566462	5473358	62.38	
1996 W1		1090	566832		62.4	
1996 W2		1090	566807	5473087	62.33	
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	1996 W3	1090	566774	5473071	62.24
4	1996 W4	1090	566742	5473054	62.29
	1996 W5	1090	566714	5473039	62.38
	1996 E1	1090	566883	5473116	62.6
	1996 E2	1090	566899	5473124	62.52
	1996 E3	1090	566941	5473141	62.68
	1996 E4	1090	566997	5473185 *	62.66
	1996 E5	1090	566973	5473154	62.82
	1996 E6	1090	567008	5473208	62.72
	1996 E7	1090	567015	5473232	62.78
	1996 E8	1090	567024	5473256	62.8
	1996 W1	1145	566664	5473190	62.17
	1996 W2	1145	566657	5473174	62.29
	1996 W3	1145	566645	5473151	62.47
	1996 W4	1145	566637	5473135	62.29
	1996 W5	1145	566633	5473116	62.16
	1996 W6	1145	566633	5473095	62.23
	1996 E1	1145	566687	5473251	62.22
	1996 E2	1145	566697	5473281	62.19
	1996 E3	1145	566704	5473303	62.26
	1996 E4	1145	566711	5473325	62.23
	1996 E5	1145	566721	5473341	62.1

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Appendix D

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Statement of Expenditures

STATEMENT OF EXPENDITURES

The following expenses were incurred on behalf of Ruby Red Resources Inc. associated with a compilation of data associated with the Eddy claims for the period Feb. 14 - Mar. 30, 2004.

PERSONNEL

R.T. Walker, P.Geo.: 199 hours at \$50.00 / hour	\$ 9,950.00
DRAFTING / DIGITIZING	
Kevin Franck and Associates	\$ 3,000.00
REPRODUCTION	

Black and White

<u>\$ 140.00</u>

<u>\$13,398.09</u>

STATEMENT OF QUALIFICATIONS

I, Richard T. Walker, of 656 Brookview Crescent, Cranbrook, BC, hereby certify that:

- 1) I am a graduate of the University of Calgary of Calgary, Alberta, having obtained a Bachelors of Science in 1986.
- 2) I obtained a Masters of Geology at the University of Calgary of Calgary, Alberta in 1989.
- 3) I am a member of good standing with the Association of Professional Engineers and Geoscientists of the Province of British Columbia.
- 4) I am a consulting geologist, residing at 656 Brookview Crescent, Cranbrook, British Columbia.
- 5) I am the author of this report which is based on a compilation of data available in the public domain, largely from Assessment Reports on file with the BC Ministry of Energy and Mines, some of which remain on confidential hold and were provided by Ruby Red Resources Inc..

Dated at Cranbrook, British Columbia this 30th day of March, 2004.

FESSIO R. T. V.ALKER Richard T. Walker, P.Geo. PS CIEM

