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VANCOUVER, B.C.

ASSESSMENT REPORT

on

SOIL GEOCHEMISTRY

SPIRIT DREAM PROPERTY

Wild Horse River area
Fort Steele Mining Division

TRIM 82G.063 & 073
602000 E 5516000 N

Owner and Operator
Ruby Red Resources
Suite 207 239 - 12th Ave SW
Calgary, Alberta, T2R 1H6

by
Peter Klewchuk, P. Geo.

October, 2006

GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT

28,643

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1.10 Location and Access

The Spirit Dream property is located in the Fort Steele Mining Division approximately 25 km northeast of Cranbrook, B.C., within the Wild Horse River drainage (Fig. 1). Access is via forestry roads on either side of the Wild Horse River and logging roads which cross parts of the claim block.

1.20 Property

The Spirit Dream property includes Tenures 515884, 515885, 515887, 515888, 530862, 535380, 535381, 535382, 535383 and 536399 (Fig. 2). The claims are owned by or under option to Ruby Red Resources Inc. of Calgary, Alberta.

1.30 Physiography

The Spirit Dream property is located east of the Rocky Mountain Trench and within the Wild Horse River drainage in the Hughes Range of the Rocky Mountains. Topography is moderate to steep with mainly wooded and locally rocky slopes. Elevation ranges from 1060 to 2060 meters. Forest cover includes mainly pine, fir and larch. Parts of the claim block have been logged and are in various stages of regeneration.

1.40 History

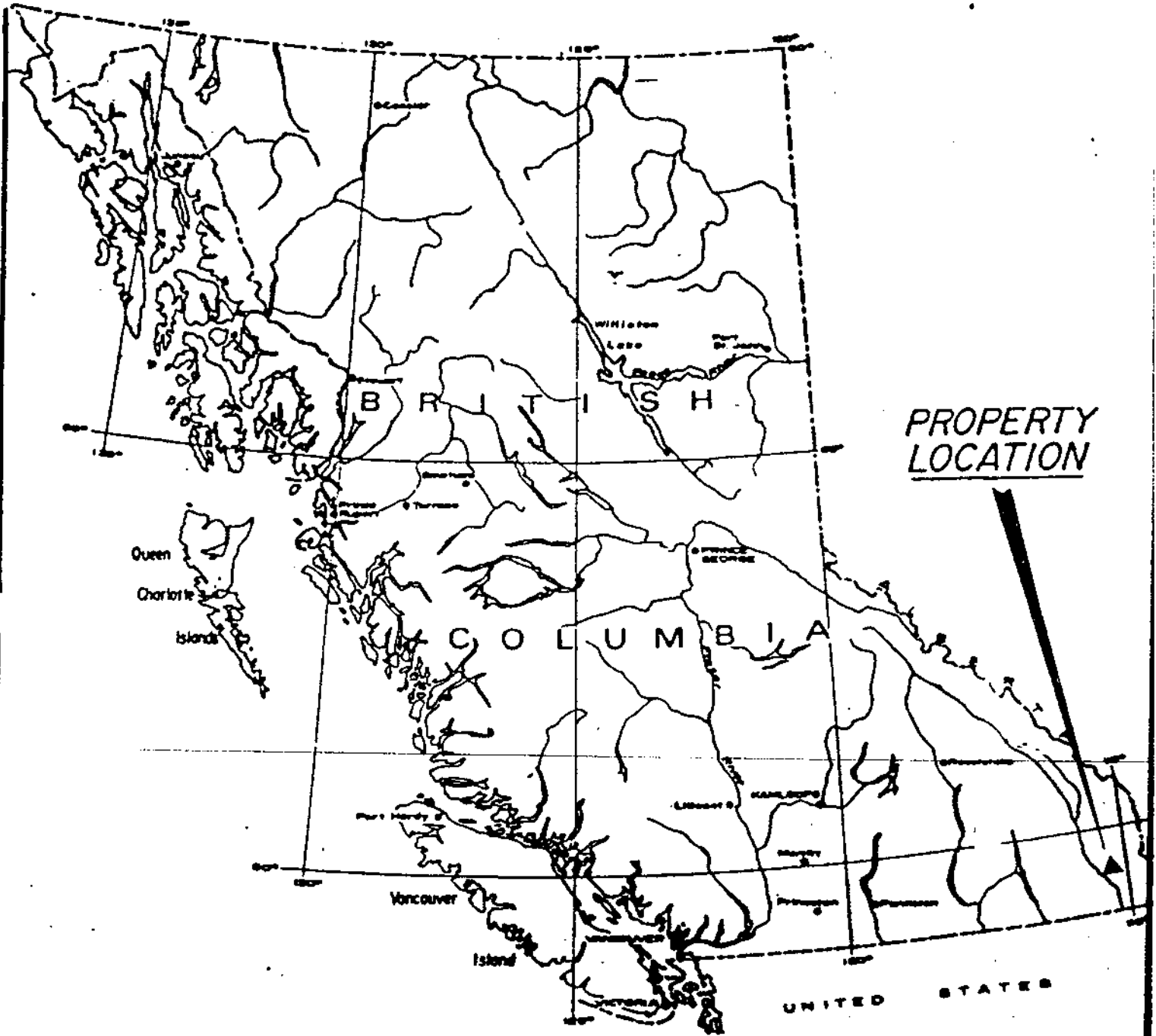
Old workings are present on the claim block north of the Wild Horse River. In 2002 a program of prospecting and rock geochemistry was conducted on the claims (Rodgers and Kennedy, 2002; AR 26976) with anomalous gold detected at a number of localities. In 2003 contour soil geochemistry in the northern part of the property outlined anomalous gold geochemistry (Klewchuk, 2003, AR 27254). In 2004, D.L. Pighin mapped the southern part of the property (Pighin, 2004, AR 27505) and in 2005 additional contour soil geochemistry was completed (Kennedy & Klewchuk, 2006, AR 28268).

1.50 Purpose of Survey

In 2006 additional contour soil geochemistry was completed in the south portion of the claim block to evaluate areas of favorable alteration and quartz veining previously located by prospecting. In addition 6 grid lines were surveyed in the Spirit Creek area in the northern part of the claim block as a follow-up on previous favourable soil geochem results.

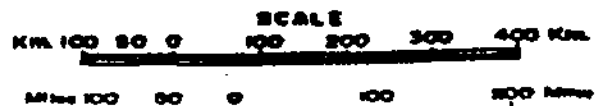
2.00 GEOLOGY

The area of the Spirit Dream property has been most recently mapped by Hoy (1979) and is entirely underlain by the Aldridge and Creston Formations, the lowermost units of the mesoproterozoic Purcell Supergroup. Both formations are of fine-grained clastic rocks including mudstone, siltstone and quartzite.



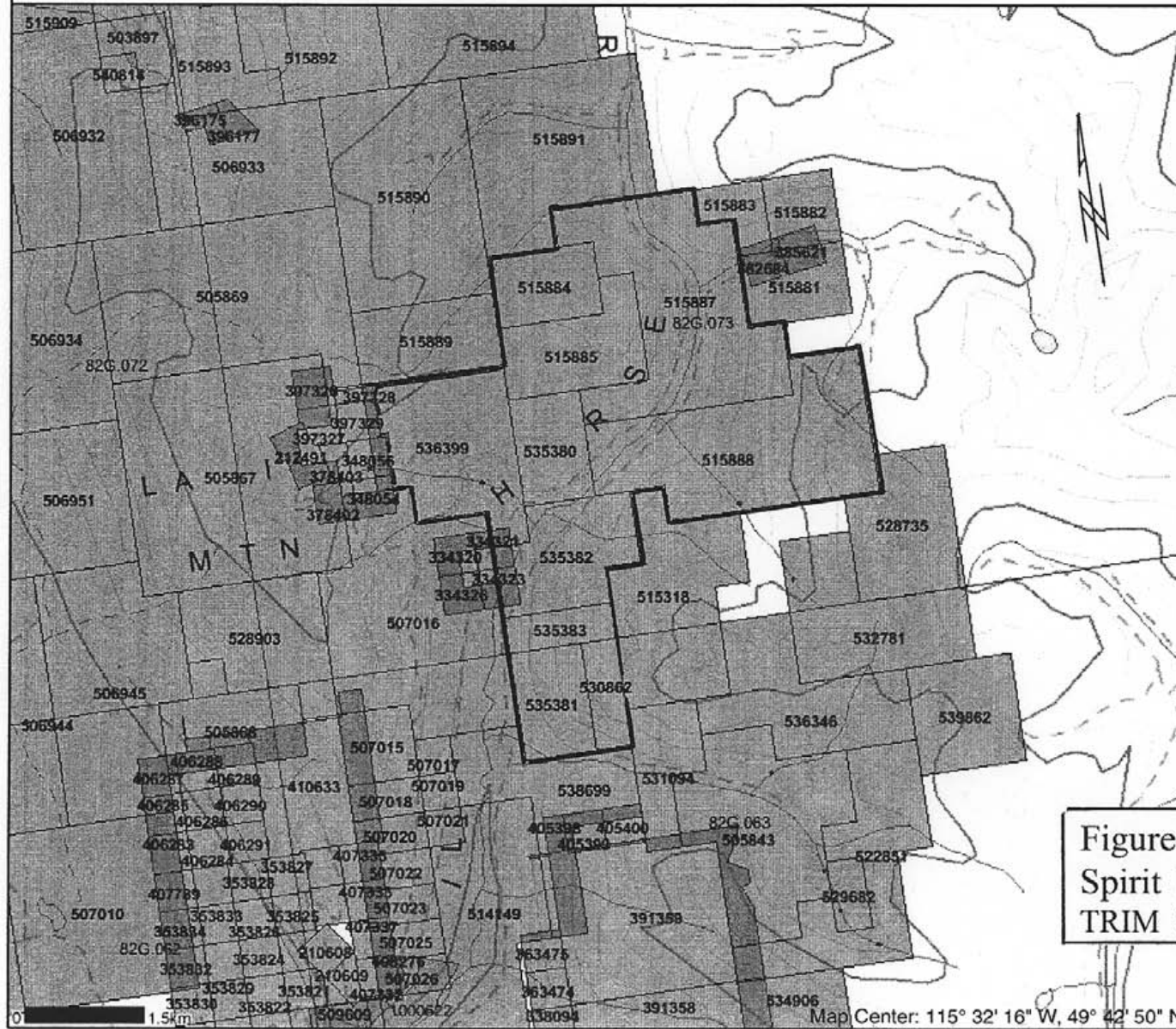
PROPERTY LOCATION

Figure 1
Spirit Dream Property Location



Map created Sun Oct 15 13:01:15 PDT 2006

Legend



- Indian Reserves
- National Parks
- Parks
- Mineral Tenures Reserves (Sitas)
- Placer Claim Designation
- Placer Lease Designation
- No Staking Reserve
- Conditional Reserve
- Release Required Reserve
- Surface Restriction
- Recreation Area
- Others
- BCGS Grid
- Contours (1:250K)
- ~ Contour - Index
- ~ Contour - Intermediate
- ~ Areaof Exclusion
- ~ Areaof Indefinite Contours
- Annotation (1:250K)
- Transportation - Points (1:250K)
- ✈ Airfield
- ✈ Anchorage - Seaplane
- ✈ Ferry Route
- ✈ Heliport
- ✈ Seaplane Base
- ✈ Air Field
- ✈ Airport
- ✈ Air Feature - Condition Unknown
- ✈ Airport, Abandoned
- Transportation - Lines (1:250K)
- ~ Ferry Route
- ~ Aerial Cableway
- ~ Road (Gravel Undivided) - 1 Lane
- ~ Road (Gravel Undivided) - 3 Lanes
- ~ Road - Paved, Lanes, 2 or More, Divided
- ~ Road (Paved Undivided) - Not Elevated - 1 Lane
- ~ Road (Paved Undivided) - Not Elevated - 2 Lanes
- ~ Road - Paved, Lanes, 3 or More, Undivided
- ~ Road (Unimproved)
- ~ Road - Loose access Dry Weather
- ~ Road (Winter Road)
- ~ Road - Paved, Lanes, 2, Undivided

Figure 2
Spirit Dream Claim Map
TRIM 82G.063 & 073

Scale: 1:80,001
DO NOT USE FOR NAVIGATION

3.00 SOIL GEOCHEMISTRY

Three hundred fifty-eight soil samples were collected from the Spirit Dream property in 2006; these included two contour lines immediately north of Boulder Creek, two lines paralleling Sheperd Gulch and 6 grid lines at Spirit Creek in the northern part of the claim group, which followed up on a local gold anomaly detected in 2005 (Figure 2).

Line locations were established using a Garmin XL-12 hand-held GPS unit and soil lines were run using a hip chain with samples taken at 25 meter intervals. The grid lines were run by compass. Sufficient GPS readings (typically every 200m) were taken to allow accurate plotting of the soil sample locations. Soils were collected from the 'B' horizon at an approximate depth of 15 cm, placed in Kraft paper bags, dried, sieved to -80 mesh, and then shipped to ACME Analytical Laboratories Ltd. at 852 East Hastings Street, Vancouver, B.C., V6A 1R6. Soils were analyzed for a 35 element ICP package by standard analytical techniques and for geochemical gold. Sample sites and individual values for gold are shown in Figures 3 & 5; gold values for previous contour soil geochemistry in the area of the grid soils (Fig. 5), taken between 2003 and 2005, are included for reference. Figures 4 and 6 show sample locations and values for copper, lead, zinc and silver; complete geochemical analyses are provided in Appendix 1.

Results

Sheperd Gulch / Boulder Creek Area

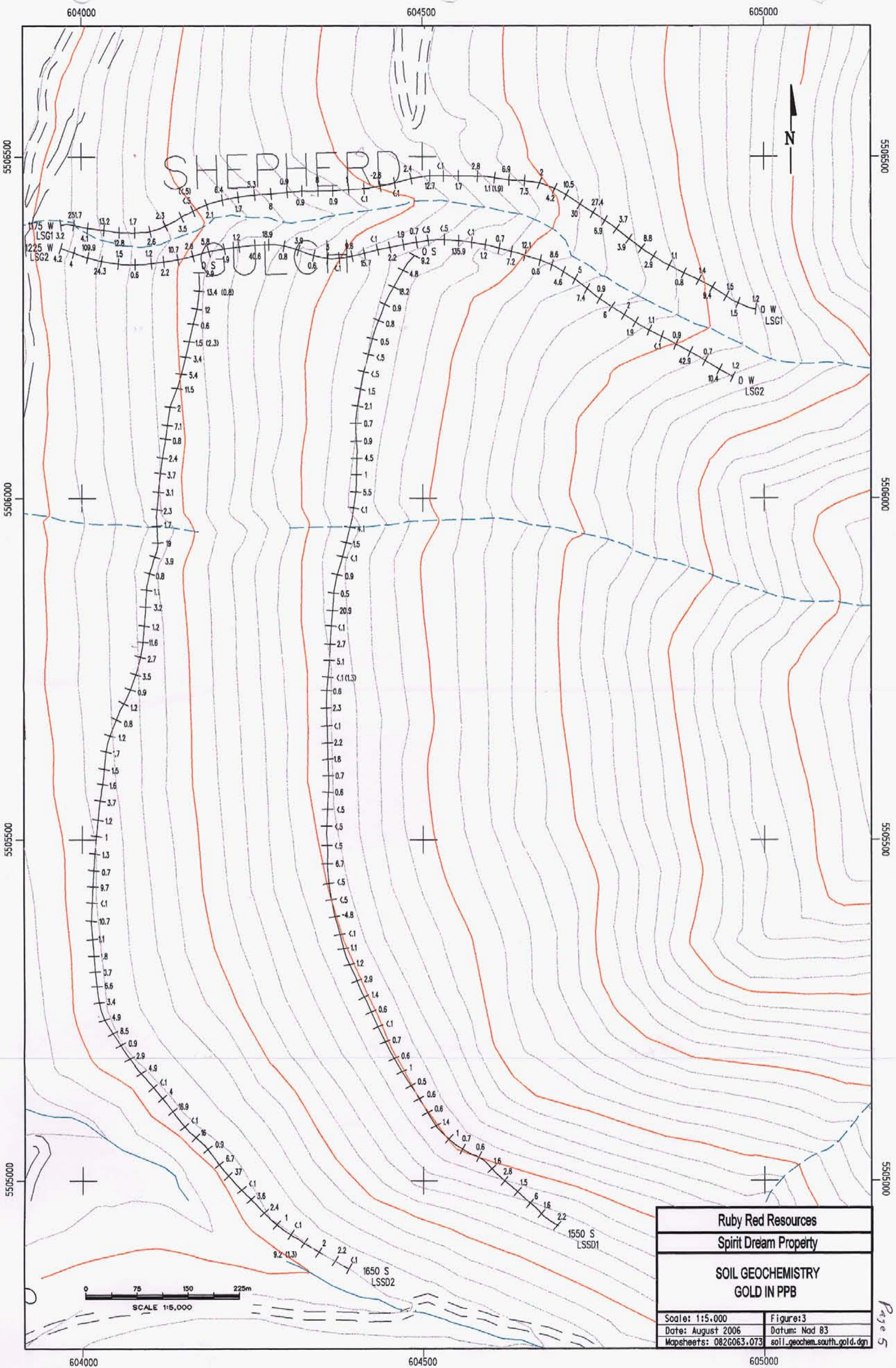
On the contour lines between Sheperd Gulch and Boulder Creek and the lines paralleling Sheperd Gulch, gold values are low (Fig.3). Only 10 of 130 samples have gold values above 10 ppb with the two highest values at 37 and 21 ppb.

Copper is locally elevated at the south end of the upper contour line (L SSD1; Fig. 4) with values ranging from 43 to 154 ppm. Weaker elevated copper values also occur near the south end of the lower contour line, L SSD2.

Higher lead values occur with elevated copper at the south end of Line SSD1 with values up to 187 ppm.

Only 5 samples have values above 150 ppm zinc on the contour lines; 4 of these are coincident with elevated lead and copper. Only one soil sample on the lower line is above 150 ppm zinc (249 / 262 ppm Zn); it is near the south end of the line and coincident with weakly elevated Pb and Cu.

Silver values on the 2 contour lines are low with only a few samples having 0.2 ppm; 3 of these are with elevated base metals at the south end of Line SSD1.



Ruby Red Resources	
Spirit Dream Property	
SOIL GEOCHEMISTRY	
GOLD IN PPB	
Scale: 1:5,000	Figure:3
Date: August 2006	Datum: Nad 83
Mapsheet: 0826063,073	soil_geochem_south_gold.dgn

604000

604500

605000

5506500

5506500

5506000

5506000

5505500

5505500

5505000

5505000



604000

604500

605000

Ruby Red Resources	
Spirit Dream Property	
SOIL GEOCHEMISTRY	
Cu, Pb, Zn, Ag IN PPM	
Scale: 1:5,000	Figure: 4
Date: August 2006	Datum: Nad 83
Mapsheet: 082G063.073	soil_geochem_south.dgn

Page 6

On the Sheperd Gulch lines, gold values are generally low but there are isolated higher values; 16 of 98 samples are >10 ppb Au; 5 of these are >40 ppb Au and 3 are >100 ppb Au.

Only weakly anomalous copper was detected on the Sheperd Gulch lines with a maximum value of 50 ppm Cu.

Lead is also low with a high value of 49 ppm.

For zinc, no values are above 150 ppm on the Sheperd Gulch lines; the highest value of 111 ppm Zn coincides with weak elevated copper (47 ppm) and lead (45 ppm).

Silver is at a maximum of 0.3 ppm at two sample sites.

Spirit Creek Grid Area

A contour soil geochem line run in 2005 in the Spirit Creek area detected an isolated gold anomaly consisting of eight 25 meter spaced samples ranging from 14 to 78 ppb Au. A single sample at the west end of the contour line, 100 meters from the clustered anomaly, returned 59 ppb Au (Fig. 5). Previous work by Pighin (2004) had detected visible gold in two apparently northeast trending shear zones near this location, thus a series of six east-west grid lines were soil sampled in 2006 to follow up on these results.

Of the 130 soil samples collected, 34 (26%) are >20 ppb Au with 6 of the samples (4.6%) being above 100 ppb Au. The maximum gold value detected is 207.8 ppb. The anomalous gold values are scattered across all lines of the grid area with no obvious pattern. The eastern edge of some lines end in anomalous gold and the grid should be expanded to the east and up hill to the north.

Anomalous copper, lead, zinc and silver are present on the Spirit Creek soil grid (Fig. 6).

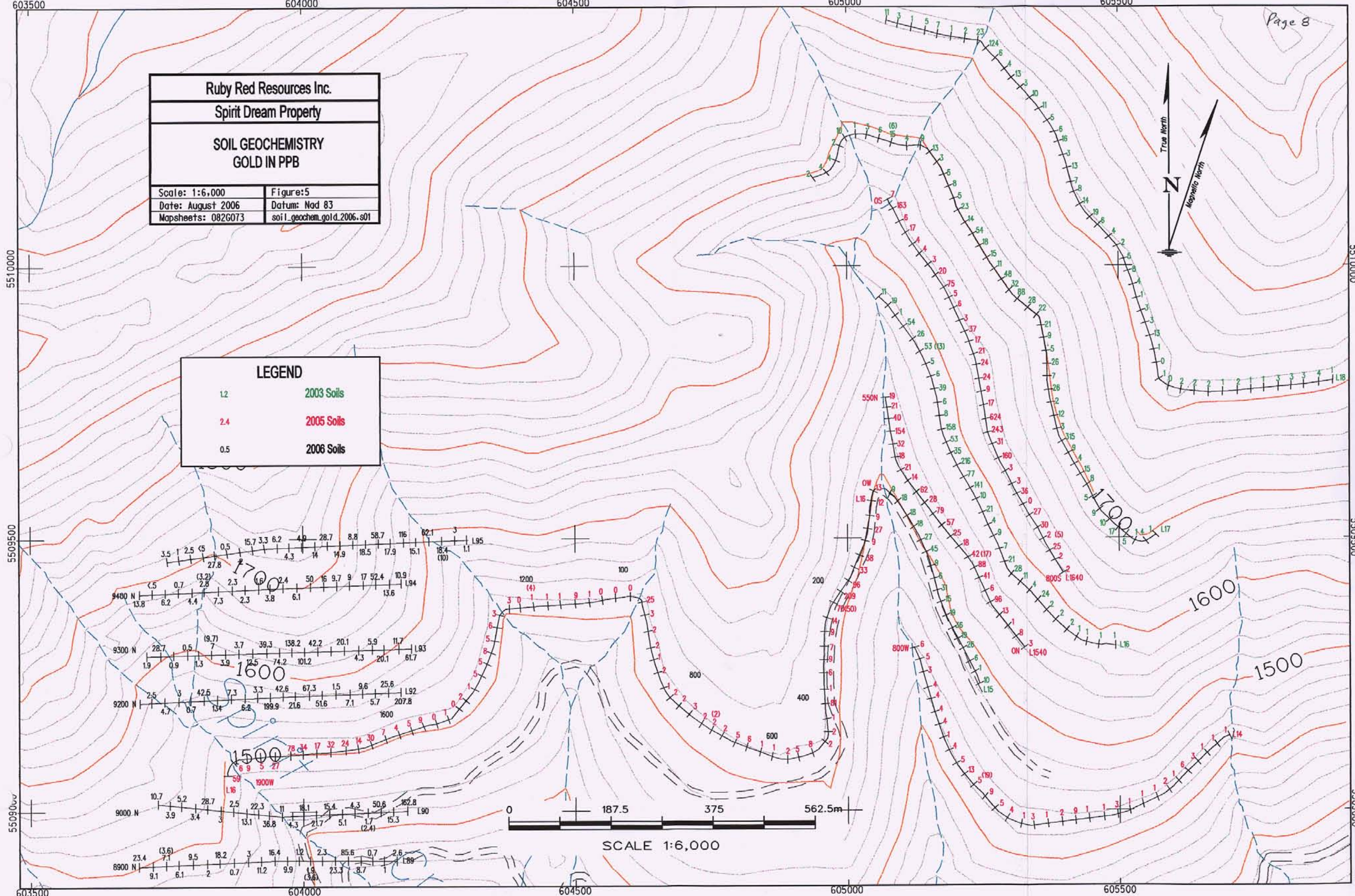
For copper, 18 of the 130 samples (13.5%) are above 50 ppm; of these, 5 are above 70 ppm and 2 are >100 ppm Cu. The anomalous copper values are spread across the grid area and suggest a broad mineralizing process, similar to the gold results.

For lead, 36 of the 130 samples (27.6%) are >50 ppm; of these, 6 are >100 ppm with a maximum value of 835 ppm Pb. This highest lead value occurs with elevated copper, zinc, silver, arsenic, antimony and bismuth but only 15 ppb Au, although higher lead values generally do tend to be with higher gold values.

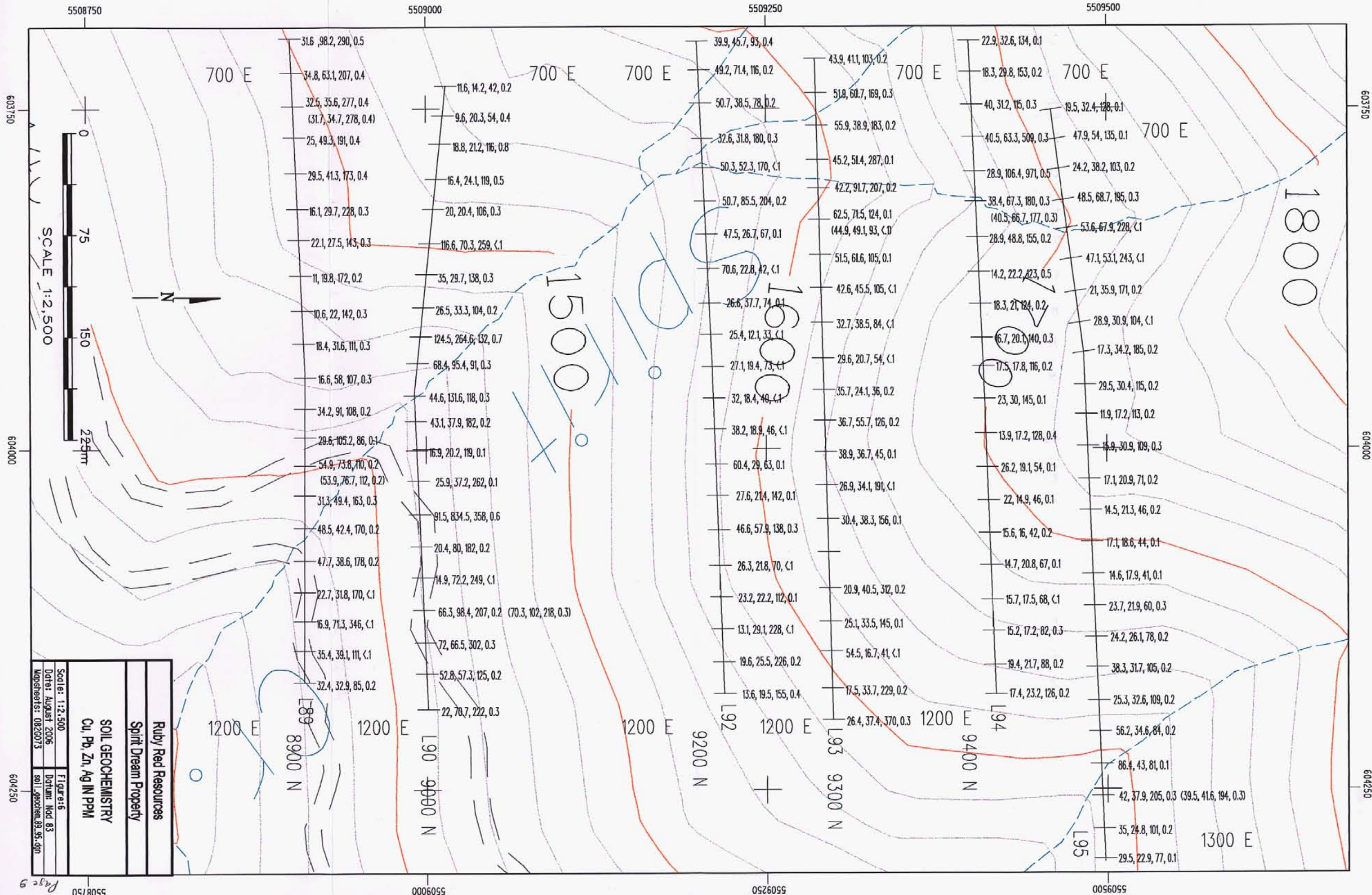
For zinc, 21 of the 130 samples (16%) are >200 ppm; of these, 11 (8.5%) are > 250 ppm and 5 (3.8%) are >300 ppm; maximum value for zinc in the Spirit Creek area is 370 ppm.

Ruby Red Resources Inc.	
Spirit Dream Property	
SOIL GEOCHEMISTRY GOLD IN PPB	
Scale: 1:6,000	Figure:5
Date: August 2006	Datum: Nad 83
Mapsheets: 082G073	soil_geochem_gold_2006.s01

LEGEND	
1.2	2003 Soils
2.4	2005 Soils
0.5	2006 Soils



SCALE 1:6,000



Ruby Red Resources Spirit Dream Property	
SOIL GEOCHEMISTRY Cu, Pb, Zn, Ag IN PPM	
Scale: 1:2,500 Date: August 2006 Mapsheet: 0826073	Figure: 6 Datum: NAD 83 Mapsheet: soil_geochem_08_26_06.dwg

For silver, 24 of the 130 samples are >0.3 ppm with 4 samples between 0.5 to 0.7 ppm and one sample at 0.8 ppm. The high silver is not associated with higher gold, copper, lead or zinc. Silver is generally but not consistently associated with elevated Au, Cu, Pb and Zn.

4.00 CONCLUSIONS

Relatively low base metal and precious metal values were detected on the contour lines between Boulder Creek and Sheperd Gulch and on the two lines paralleling Sheperd Gulch. Somewhat anomalous copper and lead near Boulder Creek may be worthy of prospecting and geologic follow-up.

Elevated precious metal and base metal values on the Spirit Creek grid in the northern part of the claim block warrant more work. This zone should be delineated with additional soil sampling, detailed prospecting and rock geochemistry, geological mapping and trenching.

5.00 REFERENCES

- Hoy, T., 1979, *Geology of the Estella-Kootenay King area, Hughes Range, southeastern British Columbia: BCMEMPR, Preliminary Map 36, and notes to accompany Preliminary Map 36.*
- Klewchuk, P., 2003, *Assessment report on soil geochemistry on the Spirit Dream property, Fort Steele Mining Division, for Ruby Red Resources, BCMEMPR Assessment Report 27254.*
- Kennedy, S. & Klewchuk, P., 2006, *Assessment report on prospecting, soil geochemistry and VLF-EM geophysics, Rockies Block property, Fort Steele Mining Division, for Ruby Red Resources, BCMEMPR Assessment Report 28268.*
- Pighin, D.L., 2004, *Geological mapping covering the Spirit Dream, HD and SD mineral claims, Fort Steele Mining division, for Ruby red resources, BCMEMPR Assessment Report 27505.*
- Rodgers, G.M., and Kennedy, C., 2002, *Geochemical report, Spirit Dream, HD & SD mineral claims, Wild Horse Creek area, Fort Steele Mining Division, BC Assessment Report #26976.*

6.00 STATEMENT OF EXPENDITURES

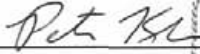
Collection and analysis of 348 soil samples @ \$21/sample	\$7308.00
Supervision and report (P.Klewchuk) 2.5 days @ \$400/day	1000.00
4X4 truck 4 days @ 110/day	440.00
Drafting (Kevin Franck and Associates)	362.00
Total Expenditure	\$9110.00

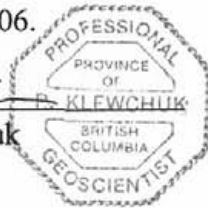
7.00 AUTHOR'S QUALIFICATIONS

As author of this report I, Peter Klewchuk, certify that:

1. I am an independent consulting geologist with offices at 246 Moyie Street, Kimberley, B.C.
2. I am a graduate geologist with a B.Sc. degree (1969) from the University of British Columbia and an M.Sc. degree (1972) from the University of Calgary.
3. I am a Fellow of the Geological Association of Canada and a member of the Association of Professional Engineers and Geoscientists of British Columbia.
4. I have been actively involved in mining and exploration geology, primarily in the province of British Columbia, for the past 30 years.
5. I have been employed by major mining companies and provincial government geological departments.

Dated at Kimberley, British Columbia, this 27th day of October, 2006.


Peter Klewchuk
P. Geo.





SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B %	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample g/n		
SSD1 825S	.2	11.6	13.1	101	<.1	27.2	6.0	321	1.32	4.8	.5	<.5	2.4	36	.2	.1	.2	13	.28	.138	7	7	.19	232	.075	3	2	.12	.034	.11	.1	.03	1.8	<.05	5	<.5	15.0		
SSD1 850S	.8	18.7	18.8	80	.1	31.4	12.3	926	2.31	6.0	.7	<.5	5.3	35	.2	.3	.3	17	.28	.055	15	19	.40	222	.047	4	1	.93	.009	.18	.1	.02	2.4	<.05	5	<.5	5		
SSD1 875S	.4	14.7	17.9	103	<.1	30.6	9.9	909	2.03	5.5	.5	<.5	4.0	53	.3	.2	.3	17	.42	.090	10	15	.35	280	.072	5	2	.47	.017	.22	.1	.03	2.1	<.05	6	<.5	5		
SSD1 900S	.5	15.2	17.3	117	<.1	31.9	10.0	723	2.16	4.4	.4	12.7	3.4	47	.2	.2	.3	20	.34	.082	11	23	.42	267	.057	4	2	.37	.017	.22	.1	.03	2.5	<.05	6	<.5	5		
SSD1 925S	1.1	23.3	28.1	112	<.1	41.3	11.4	905	2.47	6.1	.7	<.5	4.6	39	.2	.2	.4	15	.26	.087	12	12	.29	298	.070	3	2	.64	.017	.19	.1	.03	2.4	<.05	6	<.5	5		
SSD1 950S	.6	17.8	23.0	96	<.1	33.5	12.3	1236	2.33	6.7	.8	<.5	4.8	52	.3	.3	.4	17	.42	.063	11	11	.26	374	.087	6	2	.89	.017	.27	.1	.04	2.7	<.05	7	<.5	5		
SSD1 975S	.5	26.2	19.7	116	.1	34.9	11.3	785	2.15	7.2	1.0	1.2	4.5	45	.3	.3	.4	17	.35	.102	11	11	.27	222	.096	5	2	.92	.032	.15	.2	.04	2.9	<.05	7	<.5	5		
SSD1 1000S	.8	22.2	18.4	96	<.1	31.0	11.8	794	2.48	7.1	.8	<.5	4.8	45	.1	.3	.4	16	.39	.110	14	11	.32	188	.074	7	2	.59	.015	.29	.1	.02	2.7	<.05	6	<.5	5		
SSD1 1025S	.7	28.3	21.8	95	<.1	34.3	14.0	498	2.72	8.8	.8	1.1	4.8	45	.2	.4	.5	16	.42	.038	14	13	.32	141	.072	5	2	.59	.015	.26	.1	.03	2.6	<.05	6	<.5	5		
SSD1 1050S	1.1	28.2	24.3	99	<.1	37.2	16.4	762	3.01	8.4	.7	1.2	6.3	29	.2	.6	.6	18	.29	.035	19	18	.48	157	.043	3	2	.05	.009	.21	.1	.03	2.5	<.05	5	<.5	7.5		
SSD1 1075S	.9	29.8	24.1	108	<.1	36.3	15.4	504	2.94	9.0	.7	2.9	6.4	19	.2	.5	.6	15	.16	.028	22	14	.44	125	.040	3	2	.02	.009	.17	.1	.01	2.1	<.05	5	<.5	7.5		
SSD1 1100S	1.6	44.4	23.7	94	.2	39.2	18.8	276	3.06	14.8	1.0	1.4	6.3	13	.2	.7	.6	11	.18	.034	18	12	.50	41	.008	2	1	.25	.004	.16	.1	.02	1.5	<.05	3	<.5	5		
SSD1 1125S	.9	22.2	24.3	132	<.1	28.1	13.4	1453	2.89	9.4	.5	.6	4.6	48	.2	.4	.6	17	.35	.064	14	14	.44	249	.033	6	1	.91	.009	.29	.1	.02	2.6	<.05	5	<.5	7.5		
SSD1 1150S	1.0	34.7	27.3	119	.1	34.1	16.7	736	3.22	10.2	.7	<.5	4.8	30	.2	.5	.7	21	.30	.048	16	14	.51	126	.028	6	1	.93	.006	.21	.1	.02	2.5	<.05	5	<.5	5		
SSD1 1175S	1.0	25.1	24.8	121	<.1	37.6	16.9	1022	2.93	8.2	.7	.7	5.4	35	.2	.5	.7	16	.25	.051	16	14	.39	197	.045	4	2	.22	.010	.21	.1	.03	2.1	<.05	5	<.5	5		
SSD1 1200S	.5	20.3	21.5	143	.2	44.6	10.5	390	2.30	7.5	.6	.6	4.2	39	.2	.4	.5	19	.26	.110	11	12	.34	170	.086	5	2	.76	.028	.21	.2	.02	2.2	<.05	7	<.5	7.5		
SSD1 1225S	.7	24.3	36.0	177	<.1	29.3	12.0	1443	3.16	9.8	.7	1.0	6.4	99	.3	.7	.9	16	.72	.167	15	14	.45	283	.042	9	2	.12	.013	.21	1	.05	2.1	<.05	5	<.5	7.5		
SSD1 1250S	.7	31.7	29.4	130	.1	32.1	13.6	618	3.16	9.1	.8	.5	6.4	44	.1	.7	.9	17	.35	.087	17	15	.47	138	.044	6	2	.22	.012	.21	1	.03	2.0	<.05	6	<.5	5		
SSD1 1275S	1.6	42.7	35.1	105	.1	42.3	16.5	702	3.52	9.2	.9	.6	7.6	44	.2	.7	1.0	17	.41	.057	19	23	.55	119	.023	2	2	.21	.008	.20	1	.04	2.0	<.05	5	<.5	5		
SSD1 1300S	1.1	53.6	29.0	127	<.1	122.5	20.1	976	4.14	11.5	.6	.6	6.5	46	.2	1.3	.8	36	.51	.050	17	84	.77	131	.039	7	2	.56	.008	.26	1	.03	4.0	<.05	7	<.5	5		
SSD1 1325S	1.5	47.9	33.8	105	<.1	46.8	20.3	848	3.65	11.0	.7	1.4	8.3	31	.1	1.2	1.0	17	.30	.048	23	22	.58	87	.017	3	1	.89	.005	.23	1	.02	1.8	<.05	5	<.5	15.0		
SSD1 1350S	2.1	53.6	47.8	122	.1	56.1	23.5	1600	4.17	13.3	.6	1.0	8.5	45	.2	1.6	1.3	18	.88	.042	24	28	.64	98	.014	5	1	.80	.005	.20	1	.02	1.9	<.05	5	<.5	7.5		
SSD1 1375S	1.9	62.6	43.2	121	.1	43.5	22.6	781	3.91	12.3	.9	.7	10.0	18	.1	1.0	1.3	13	.14	.038	28	14	.53	80	.005	1	1	.75	.005	.13	1	.03	1.7	<.05	4	<.5	7.5		
SSD1 1400S	2.6	62.5	56.2	128	<.1	47.2	27.4	1420	4.46	13.1	.9	.6	10.0	32	.2	1.4	1.7	13	.23	.039	27	14	.56	77	.009	2	1	.65	.006	.17	<.1	.02	1.6	<.05	4	<.5	7.5		
SSD1 1425S	1.9	62.1	80.2	139	.1	47.3	33.7	2363	4.14	18.2	1.0	1.6	7.7	51	.6	1.3	1.8	12	.40	.053	19	16	.59	90	.009	3	1	.57	.006	.13	1	.06	1.5	<.06	4	<.5	5		
SSD1 1450S	5.8	96.1	77.7	134	.2	50.1	26.3	919	4.89	24.2	.7	2.8	7.8	23	.2	1.8	2.3	13	.06	.060	21	14	.58	54	.005	1	1	.82	.007	.09	1	.06	1.5	<.09	4	<.5	15.0		
SSD1 1475S	2.8	81.4	106.1	274	<.1	51.7	38.7	1927	4.48	19.8	1.3	1.5	8.8	30	.6	1.4	1.8	13	.25	.050	22	14	.58	84	.007	2	1	.59	.006	.10	1	.07	1.7	<.05	4	<.5	5		
SSD1 1500S	4.6	154.9	187.1	435	.2	49.1	24.8	338	14.33	216.8	1.6	6.0	6.7	11	.2	3.6	10.2	11	.03	.110	13	9	.32	26	.004	1	1	.49	.004	.06	1	.11	1.4	<.16	3	1	8	7.5	
SSD1 1525S	2.6	89.8	92.6	170	.2	51.0	30.9	1876	4.81	23.9	.9	1.6	9.7	36	.3	1.4	2.2	13	.28	.051	22	15	.61	87	.004	3	1	.64	.006	.09	1	.07	1.9	<.1	10	4	5	7.5	
SSD1 1550S	2.6	84.1	84.2	150	.1	37.9	25.2	1197	4.75	19.9	1.2	2.2	9.2	39	.2	1.5	1.9	14	.16	.061	24	15	.66	75	.007	3	1	.71	.009	.13	1	.04	1.7	<.1	08	4	5	7.5	
SSD2 0S	.7	14.4	14.8	48	<.1	21.8	10.4	197	2.12	5.2	.4	2.9	3.7	18	.1	.2	.4	19	.23	.020	12	13	.54	92	.045	4	1	.70	.007	.11	1	.02	1.5	<.05	5	<.5	5		
SSD2 25S	.4	11.4	14.0	50	<.1	22.8	8.6	772	1.87	4.8	.5	13.4	3.0	48	.2	.1	.3	20	.35	.047	8	11	.35	438	.089	5	2	.91	.024	.15	1	.03	2.0	<.05	7	<.5	5		
RE SSD2 25S	.4	11.0	14.8	50	<.1	21.9	8.5	766	1.87	4.8	.5	.8	3.2	47	.1	.1	.3	21	.36	.047	8	11	.35	454	.090	3	2	.89	.026	.15	1	.03	2.0	<.05	7	<.5	5		
SSD2 50S	.7	10.6	12.9	42	<.1	18.8	8.9	2445	1.72	4.9	.4	12.0	2.6	35	.3	.2	.3	18	.41	.049	10	10	.29	375	.053	5	1	.98	.014	.16	1	.05	1.7	<.05	5	<.5	15.0		
STANDARD DS7	21.1	111.8	72.9	409	.9	56.2	9.7	632	2.42	47.9	5.0	71.5	4.4	67	6.4	6.0	4.5	87	.93	.079	12	167	1.06	375	.124	40	96	.072	.44	3	9	20	2.5	4.2	.21	4	3	6	15.0

Sample type: SOIL PULP. Samples beginning 'RE' are Reruns and 'ARE' are Reject Reruns.



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga	Se	Sample
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppb	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	%	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm
SSD2 755	.5	8.6	9.8	39	<.1	17.3	5.8	626	1.38	4.5	.3	.6	2.0	26	.1	.1	.2	16	.30	.044	6	8	.27	170	.078	2	2	.12	.030	.11	.1	.03	1.4	<.05	5	<.5	15.0
SSD2 1005	.5	10.0	14.0	50	<.1	22.2	8.8	583	1.96	5.2	.5	1.5	3.2	33	.1	.2	.3	16	.32	.036	10	12	.38	302	.084	4	2	.84	.021	.20	.1	.03	2.0	<.05	7	<.5	5
RE SSD2 1005	.5	10.6	14.6	51	<.1	23.0	9.3	593	2.02	5.6	.5	2.3	3.2	35	.1	.2	.3	17	.34	.037	10	12	.39	305	.086	3	2	.87	.023	.21	.1	.03	2.1	<.05	7	<.5	5
SSD2 1255	.8	12.1	16.6	47	<.1	19.2	8.5	808	1.82	5.1	.3	3.4	3.4	27	.2	.2	.3	14	.29	.027	12	10	.33	212	.055	3	2	.00	.018	.15	.1	.03	1.5	<.05	5	<.5	7.5
SSD2 1505	.7	13.3	17.0	57	<.1	22.9	9.6	655	2.06	5.8	.4	5.4	3.6	23	.1	.3	.3	17	.27	.032	13	13	.40	239	.057	4	2	.23	.015	.18	.1	.03	1.9	<.05	5	<.5	7.5
SSD2 1755	.6	12.8	15.1	60	<.1	20.8	9.8	439	1.92	6.9	.4	11.5	4.1	23	.1	.3	.3	15	.29	.053	13	13	.40	177	.044	3	1	.80	.013	.19	.1	.02	1.7	<.05	5	<.5	15.0
SSD2 2005	1.1	24.8	20.0	76	<.1	22.2	11.3	358	2.50	9.6	.5	2.0	7.4	14	.1	.4	.5	11	21	.021	22	12	.49	91	.024	2	1	.18	.004	.18	.1	.01	1.5	<.05	3	<.5	7.5
SSD2 2255	.6	23.0	15.6	69	<.1	27.1	11.0	447	1.96	8.5	.5	7.1	4.2	33	.1	.3	.3	16	.40	.061	10	12	.40	195	.070	3	2	.39	.027	.19	.1	.02	2.1	<.05	6	<.5	15.0
SSD2 2505	.5	25.0	40.1	57	<.1	47.5	13.8	357	2.63	7.8	.5	.8	3.8	31	.2	.2	.3	22	.40	.043	12	30	.59	176	.077	3	2	.56	.024	.21	.1	.03	3.8	<.05	6	<.5	5
SSD2 2755	.8	17.0	18.4	64	<.1	25.5	10.3	631	2.16	7.4	.4	2.4	4.7	22	.1	.3	.3	15	.27	.040	16	16	.47	163	.042	3	1	.72	.010	.19	.1	.02	1.7	<.05	4	<.5	7.5
SSD2 3005	.6	14.9	15.3	78	.2	22.2	9.3	605	1.89	5.8	.4	3.7	3.4	29	.2	.2	.2	16	.35	.048	11	13	.41	194	.063	4	2	.19	.019	.18	.1	.02	1.9	<.05	5	<.5	7.5
SSD2 3255	.8	21.0	15.6	80	<.1	71.7	12.9	347	2.53	8.4	.5	3.1	4.0	19	.1	.3	.3	30	.21	.030	13	52	.58	182	.057	3	2	.26	.015	.15	.1	.02	3.0	<.05	6	<.5	15.0
SSD2 3505	1.2	24.2	29.0	60	<.1	26.1	12.6	325	2.51	10.7	.4	2.3	6.6	12	.1	.5	.5	14	.17	.018	23	18	.46	96	.013	1	1	.30	.004	.11	.1	.03	1.5	<.05	3	<.5	7.5
SSD2 3755	.8	23.2	31.8	93	<.1	27.5	14.6	1860	2.61	9.8	.7	1.7	5.2	38	.4	.3	.5	16	.41	.075	16	14	.36	395	.051	3	2	.12	.011	.20	.1	.04	2.5	<.05	5	<.5	5
SSD2 4005	1.0	27.1	32.6	98	<.1	37.2	15.9	619	2.56	10.3	.4	19.0	5.2	16	.3	.3	.4	19	.24	.031	18	33	.71	128	.022	2	1	.53	.004	.11	.1	.02	2.0	<.05	4	<.5	5
SSD2 4255	.4	14.6	19.0	83	<.1	29.9	9.7	530	1.95	5.0	.5	3.9	3.3	29	.2	.1	.2	20	.29	.072	10	22	.41	227	.087	3	2	.64	.027	.16	.1	.02	2.5	<.05	6	<.5	15.0
SSD2 4505	.5	15.3	27.1	77	<.1	36.1	10.4	643	1.98	5.8	.4	.8	2.5	35	.2	.2	.2	20	.39	.040	9	24	.46	316	.083	4	2	.67	.019	.19	.1	.04	2.1	<.05	7	<.5	5
SSD2 4755	.4	13.9	14.1	97	<.1	37.5	8.9	320	1.75	6.4	.5	1.1	2.6	31	.2	.2	.2	20	.33	.068	9	19	.35	190	.087	3	2	.58	.031	.14	.1	.03	2.2	<.05	7	<.5	15.0
SSD2 5005	.7	16.0	17.9	61	<.1	32.3	11.4	660	2.09	6.9	.5	3.2	3.7	30	.1	.3	.3	20	.36	.036	11	20	.43	202	.077	5	2	.56	.023	.23	.1	.03	2.5	<.05	6	<.5	15.0
SSD2 5255	.5	11.2	13.4	65	<.1	27.8	8.0	512	1.65	7.0	.5	1.2	2.6	43	.1	.2	.2	18	.43	.082	8	11	.26	249	.099	4	2	.99	.032	.21	.1	.03	2.0	<.05	7	<.5	15.0
SSD2 5505	1.3	30.0	18.1	56	<.1	24.8	11.6	178	2.56	11.2	.4	11.6	7.2	17	.1	.4	.5	12	.20	.026	25	14	.47	86	.019	2	1	.19	.005	.12	.1	.02	1.3	<.05	3	<.5	7.5
SSD2 5755	.5	19.7	13.2	42	<.1	20.6	7.9	267	1.79	6.6	.6	2.7	3.8	35	.1	.2	.3	14	.24	.038	11	9	.28	167	.075	2	2	.37	.030	.12	.1	.02	1.9	<.05	6	<.5	15.0
SSD2 6005	1.3	26.1	22.3	61	<.1	24.9	12.4	739	2.47	10.4	.4	3.5	5.9	24	.1	.4	.5	13	.28	.026	20	11	.35	164	.029	3	1	.46	.007	.15	.1	.02	1.5	<.05	4	<.5	7.5
SSD2 6255	.3	9.8	13.5	101	<.1	22.3	6.2	428	1.63	5.4	.5	.9	2.9	35	.1	.1	.3	17	.35	.174	7	8	.23	229	.093	2	2	.68	.028	.14	.1	.03	1.9	<.05	6	<.5	15.0
SSD2 6505	.3	9.0	10.6	79	<.1	20.7	6.3	285	1.43	4.3	.4	1.2	2.2	27	.1	.2	.2	15	.23	.076	7	8	.22	202	.071	2	2	.26	.027	.12	.1	.02	1.4	<.05	6	<.5	15.0
SSD2 6755	.7	12.9	20.2	101	<.1	22.8	9.4	863	1.92	5.6	.4	.8	2.9	37	.2	.3	.4	13	.38	.065	12	11	.28	288	.037	4	1	.71	.014	.14	.1	.04	1.4	<.05	4	<.5	5
SSD2 7005	.4	12.0	12.8	67	<.1	21.1	6.9	562	1.62	7.6	.4	1.2	2.6	32	.1	.2	.2	16	.31	.077	7	9	.24	247	.092	3	2	.77	.031	.13	.1	.02	1.6	<.05	7	<.5	15.0
SSD2 7255	.8	24.3	20.2	65	<.1	26.2	14.0	786	2.48	9.3	.5	1.7	4.8	19	.1	.3	.4	16	.27	.031	18	14	.49	188	.030	6	1	.86	.005	.15	.1	.03	1.9	<.05	5	<.5	5
SSD2 7505	.4	11.3	14.2	67	<.1	20.7	7.8	465	1.73	6.7	.4	1.5	3.0	34	.1	.2	.3	17	.32	.098	7	9	.27	205	.080	3	2	.52	.028	.15	.2	.03	1.5	<.05	6	<.5	15.0
SSD2 7755	.9	16.8	18.5	71	<.1	21.3	10.3	787	2.09	5.7	.4	1.6	4.3	29	.1	.3	.4	15	.27	.030	15	13	.37	208	.038	3	1	.60	.009	.14	.1	.02	1.5	<.05	4	<.5	7.5
SSD2 8005	1.1	16.4	15.9	58	<.1	19.9	8.5	287	2.24	5.9	.4	3.7	5.1	22	.1	.3	.4	15	.21	.030	17	11	.33	134	.042	2	1	.66	.010	.13	.1	.01	1.3	<.05	4	<.5	7.5
SSD2 8255	.8	15.0	19.4	136	<.1	25.4	10.5	1374	2.12	5.8	.5	1.2	3.7	54	.3	.3	.4	17	.58	.134	12	12	.30	351	.050	6	2	.27	.015	.25	.1	.03	2.0	<.05	6	<.5	7.5
SSD2 8505	.9	12.4	21.4	78	<.1	22.5	9.5	785	2.08	3.9	.4	1.0	3.5	21	.1	.2	.4	19	.21	.025	13	13	.33	221	.052	3	1	.91	.009	.14	.1	.03	1.6	<.05	5	<.5	5
SSD2 8755	.5	14.5	18.3	71	<.1	25.2	8.5	378	2.11	5.2	.3	1.3	4.0	30	.2	.3	.3	21	.30	.037	12	14	.36	208	.072	5	2	.39	.019	.21	.1	.02	1.7	<.05	6	<.5	7.5
STANDARD DS7	21.0	110.7	70.7	410	.9	56.1	9.7	624	2.40	47.8	5.0	69.3	4.5	69	6.3	6.0	4.5	87	.92	.079	13	166	1.06	373	.125	39	.96	.073	.44	3.9	.20	7.5	4.2	.21	4.3	5	15.0

Sample type: SOIL PULP. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B %	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gr
SG2 500W	.7	11.9	17.0	73	<.1	22.4	9.9	769	1.87	6.8	.3	<.5	2.4	17	.1	.3	.3	24	.20	.054	12	12	.34	163	.047	4	1.84	.012	.07	.1	.03	1.2	<.05	6	<.5	7.5	
SG2 525W	.8	13.1	20.0	77	<.1	21.7	10.0	1264	1.96	7.0	.5	141.9	2.5	23	.1	.3	.4	25	.25	.059	11	12	.34	224	.062	3	2.22	.017	.08	.1	.04	1.4	<.05	6	<.5	7.5	
SG2 550W	.6	12.1	16.7	80	.1	27.4	10.5	473	1.95	6.7	.4	<.5	2.5	25	.1	.2	.4	26	.22	.059	11	12	.31	218	.060	4	2.26	.017	.08	.1	.03	1.4	<.05	6	<.5	7.5	
SG2 575W	.8	15.4	18.7	67	.1	26.0	11.4	652	1.98	6.4	.4	<.5	3.3	22	.1	.3	.4	22	.31	.038	12	14	.38	212	.040	5	2.02	.014	.09	.1	.02	1.4	<.05	6	<.5	7.5	
SG2 600W	1.0	19.6	17.2	53	<.1	23.1	10.2	361	2.12	9.4	.4	.7	4.4	17	.1	.4	.4	21	.21	.059	17	13	.40	108	.046	4	1.73	.017	.11	.1	.02	1.3	<.05	5	<.5	7.5	
SG2 625W	1.1	24.4	19.6	43	<.1	20.2	11.1	230	2.29	10.3	.6	1.9	5.2	13	.1	.4	.4	27	.26	.034	18	16	1.38	127	.059	4	2.07	.012	.14	.3	.02	2.5	2<.05	6	<.5	7.5	
SG2 650W	.7	17.1	14.8	33	<.1	17.3	9.7	225	2.25	7.4	.5	2.2	5.5	12	.1	.3	.3	23	.18	.039	21	12	.95	120	.050	4	1.83	.011	.15	.2	.01	2.3	<.05	5	<.5	7.5	
SG2 675W	.8	18.0	16.8	34	<.1	18.1	9.8	389	2.30	8.0	.4	<.5	4.8	15	.1	.3	.3	20	.25	.042	19	12	.83	145	.039	6	1.68	.009	.15	.2	.01	2.4	<.05	4	<.5	7.5	
SG2 700W	.6	18.3	17.5	49	<.1	21.2	12.9	676	2.21	8.2	.7	15.7	4.8	30	.1	.2	.4	23	.36	.072	17	12	.64	125	.052	4	1.99	.015	.16	.1	.02	2.2	<.05	5	<.5	15.0	
SG2 725W	.7	21.3	47.6	47	<.1	24.3	12.6	362	2.21	8.4	.7	9.6	4.3	26	.1	.3	.4	22	.25	.041	16	12	.45	125	.050	3	2.18	.017	.10	.1	.02	2.0	<.05	5	<.5	15.0	
SG2 750W	.7	13.4	18.6	50	<.1	21.5	11.0	723	2.07	7.7	.3	<.5	4.6	15	<.1	.3	.4	22	.17	.029	17	17	.49	162	.032	3	1.77	.010	.12	.1	.02	1.5	<.05	5	<.5	7.5	
SG2 775W	1.0	18.1	20.1	48	<.1	23.5	11.0	368	2.15	11.4	.3	3.0	4.5	17	.1	.4	.4	20	.19	.050	18	14	.45	139	.041	4	1.85	.013	.10	.1	.02	1.5	<.05	5	<.5	7.5	
SG2 800W	1.2	16.6	27.7	36	<.1	14.4	8.5	174	2.12	9.7	.3	.6	6.4	5	.1	.4	.4	13	.06	.019	30	8	.45	42	.018	3	.85	.003	.17	.1	.01	1.7	<.05	3	<.5	7.5	
SG2 825W	1.1	19.8	29.6	43	<.1	19.5	10.1	271	2.23	9.5	.6	3.9	6.0	15	.1	.4	.4	17	.18	.032	24	12	.50	98	.038	3	1.46	.009	.13	.2	.01	2.0	<.05	4	<.5	7.5	
SG2 850W	.7	17.0	16.1	36	<.1	20.8	9.4	186	1.98	5.9	.4	.8	4.0	20	<.1	.2	.3	21	.18	.041	13	10	.45	185	.072	3	2.54	.021	.11	.1	.02	1.7	<.05	6	<.5	15.0	
SG2 875W	.9	23.3	15.6	37	<.1	20.4	10.9	163	2.36	9.1	.6	18.9	6.4	9	.1	.5	.4	16	.13	.017	23	14	.73	58	.027	2	1.32	.007	.09	.1	.02	2.2	<.05	4	<.5	7.5	
SG2 900W	.6	10.7	13.0	39	<.1	22.3	8.5	223	1.90	6.3	.3	40.6	2.8	22	.1	.2	.3	20	.23	.029	11	11	.41	170	.075	3	2.54	.022	.13	.1	.02	1.4	<.05	7	<.5	15.0	
SG2 925W	.8	15.6	13.6	36	<.1	18.6	10.4	294	2.23	7.1	.3	1.2	5.3	8	.1	.3	.3	15	.14	.016	21	13	.68	75	.033	3	1.40	.005	.14	.1	.01	1.5	<.05	4	<.5	7.5	
SG2 950W	.9	16.1	14.1	36	<.1	18.6	10.1	341	2.32	6.1	.4	1.9	5.4	12	.1	.3	.3	18	.27	.016	19	13	.95	94	.047	3	1.68	.008	.18	.1	.01	2.4	<.05	5	<.5	7.5	
SG2 975W	1.0	17.8	17.1	44	<.1	21.6	10.4	558	2.28	6.1	.5	5.8	5.1	19	.1	.3	.3	18	.19	.022	16	11	.55	195	.058	2	2.18	.013	.13	.1	.01	2.1	<.05	6	<.5	7.5	
SG2 1000W	1.1	19.3	19.2	41	<.1	18.6	10.2	445	2.34	6.7	.5	2.6	5.1	17	.1	.4	.4	17	.30	.022	18	12	.76	122	.045	3	1.71	.010	.16	.1	.02	2.4	<.05	5	<.5	7.5	
SG2 1025W	1.0	34.8	24.6	42	<.1	21.2	12.3	382	2.72	8.2	.6	10.7	7.1	16	.1	.5	.4	21	.36	.024	21	14	.96	116	.049	3	1.83	.014	.21	.2	.02	3.1	<.05	5	<.5	7.5	
SG2 1050W	.8	13.1	17.9	39	<.1	16.5	9.5	781	2.25	5.1	.3	2.2	4.7	17	.1	.3	.3	19	.23	.021	17	12	.65	180	.047	4	1.69	.008	.17	.1	.03	2.2	<.05	4	<.5	7.5	
SG2 1075W	.6	12.7	16.0	37	<.1	19.0	9.2	574	2.02	3.8	.6	1.2	4.0	29	.1	.2	.3	19	.42	.020	14	11	.52	155	.084	5	2.61	.023	.15	.1	.03	2.5	<.05	6	<.5	7.5	
SG2 1100W	.7	20.6	13.1	34	<.1	21.8	12.2	212	2.17	7.2	.4	.6	3.9	14	.1	.3	.3	18	.30	.017	14	15	1.00	74	.043	2	1.70	.005	.09	.1	.02	2.2	<.05	4	<.5	5	
SG2 1125W	.7	15.8	14.0	33	<.1	18.3	11.0	293	2.14	6.0	.4	1.5	4.8	11	.1	.3	.3	20	.19	.016	20	13	.86	81	.035	2	1.59	.005	.10	.1	.01	1.9	<.05	4	<.5	7.5	
SG2 1150W	.8	13.9	16.7	34	<.1	16.7	11.0	856	2.13	5.2	.4	24.3	4.6	18	.1	.2	.4	16	.33	.018	15	11	.68	164	.041	4	1.65	.007	.14	.1	.03	2.2	<.05	4	<.5	7.5	
SG2 1175W	.6	16.6	17.8	45	<.1	21.6	11.3	463	2.18	6.1	.4	109.9	3.4	20	.1	.2	.3	21	.33	.022	11	12	.91	222	.081	4	2.94	.018	.13	.2	.02	2.1	<.05	7	<.5	7.5	
SG2 1200W	1.1	31.0	17.6	34	<.1	23.0	15.3	257	2.72	11.7	.5	4.0	9.1	20	.1	.5	.6	11	2.19	.035	25	11	.76	63	.011	3	.92	.007	.12	.1	.03	1.9	<.05	3	<.5	7.5	
SG2 1225W	.9	29.1	18.7	47	<.1	24.7	13.5	462	2.50	9.4	.6	4.2	6.4	17	.1	.4	.4	20	.27	.033	20	14	.85	152	.050	4	1.83	.016	.19	.1	.02	2.9	<.05	5	<.5	7.5	
L89 700E	.9	31.6	98.2	290	.5	37.3	14.3	512	2.78	14.0	.8	23.4	5.0	17	.4	.8	.4	31	.16	.082	11	13	.30	154	.089	2	3.01	.012	.09	.2	.07	2.6	2<.05	7	<.5	15.0	
L89 725E	1.1	34.8	63.1	207	.3	37.0	16.7	512	2.78	11.6	.8	9.1	5.0	17	.4	.9	.5	27	.16	.066	19	15	.34	148	.053	3	1.91	.009	.12	.2	.02	2.3	2<.05	5	<.5	7.5	
L89 750E	1.0	32.5	35.6	277	.4	35.6	13.1	398	2.57	10.8	.7	7.1	5.4	15	.4	.6	.4	29	.12	.064	17	13	.35	237	.066	3	2.25	.010	.11	.2	.02	2.4	2<.05	5	<.5	7.5	
RE L89 750E	.9	31.7	34.7	278	.4	35.0	13.4	399	2.56	10.7	.7	3.6	5.3	15	.4	.6	.4	30	.12	.064	17	14	.34	233	.067	3	2.20	.010	.11	.2	.03	2.5	2<.05	6	<.5	7.5	
STANDARD DS7	21.2	112.5	72.3	416	.9	57.2	9.9	626	2.41	47.1	5.0	71.2	4.4	68	6.2	5.8	4.4	90	.91	.078	12	169	1.05	366	.125	39	.96	.071	.43	3.8	.20	2.5	4.2	.22	5	3.5	15.0

Sample type: SOIL PULP. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B %	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gr.
L89 775E	.8	25.0	49.3	191	.4	36.2	12.7	593	2.58	9.2	.7	6.1	5.0	13	.4	.6	.4	27	.14	.060	10	12	.30	175	.092	3	3.03	.012	.10	2	.03	2.6	2<.05	7	<.5	7.5	
L89 800E	.9	29.5	41.3	173	.4	35.4	14.0	313	2.65	9.4	.6	9.5	5.1	12	.3	.6	.4	28	.10	.045	13	13	.36	175	.073	2	2.48	.010	.09	2	.02	2.2	1<.05	6	<.5	15.0	
L89 825E	.5	16.1	29.7	228	.3	37.1	9.9	423	1.83	6.5	.5	2.0	3.5	13	.3	.2	.3	23	.10	.065	9	10	.26	218	.085	3	2.29	.019	.16	1	.03	2.0	1<.05	5	<.5	7.5	
L89 850E	.7	22.1	27.5	143	.3	33.8	10.5	532	2.19	9.0	.7	18.2	3.1	15	2	.4	.3	22	.13	.134	12	11	.29	228	.070	2	2.50	.012	.08	2	.03	2.0	1<.05	7	<.5	7.5	
L89 875E	.5	11.0	19.8	172	.2	19.8	8.4	1443	1.57	4.2	.4	7	2.2	15	2	.2	.3	19	.12	.078	9	9	.17	216	.051	3	1.74	.013	.06	1	.03	1.4	1<.05	5	<.5	7.5	
L89 900E	.7	10.6	22.0	142	.3	23.3	8.3	1412	1.71	5.6	.4	3.0	2.5	28	.3	.3	.3	18	.25	.111	10	10	.22	261	.051	2	1.79	.013	.08	1	.03	1.5	1<.05	5	<.5	15.0	
L89 925E	.6	18.4	31.6	111	.3	49.6	9.1	458	1.93	7.5	.4	11.2	4.1	20	.3	.4	.3	18	.15	.079	12	9	.23	192	.061	2	2.09	.015	.09	1	.02	1.6	1<.05	5	<.5	7.5	
L89 950E	.8	16.6	58.0	107	.3	31.6	9.8	521	2.20	10.7	.3	16.4	4.5	20	2	.7	.4	17	.16	.052	15	10	.19	143	.036	2	1.48	.009	.09	1	.03	1.2	1<.05	4	<.5	7.5	
L89 975E	1.3	34.2	91.0	108	.2	27.5	13.5	337	2.98	14.8	.5	9.9	6.2	14	1	1.3	.6	17	.14	.052	22	11	.33	96	.026	2	1.37	.005	.13	1	.02	1.5	1<.05	4	<.5	7.5	
L89 1000E	1.4	29.6	105.2	86	.1	27.9	15.6	637	2.48	14.0	.5	1.2	5.6	27	2	1.0	.6	12	.25	.043	22	13	.20	113	.009	4	1.00	.005	.11	1	.02	1.9	1<.05	2	<.5	5	
L89 1025E	1.3	54.9	73.8	110	2	27.5	21.0	606	2.60	27.2	.7	1.9	9.7	13	2	1.2	.8	6	.16	.041	30	7	.17	52	.006	6	.76	.004	.11	1	.02	1.6	1<.05	2	<.5	5	
RE L89 1025E	1.2	53.9	76.7	112	2	27.7	21.8	615	2.61	28.3	.7	3.6	9.6	13	2	1.2	.8	6	.16	.041	30	7	.17	51	.006	5	.77	.004	.11	<.1	.02	1.6	1<.05	2	<.5	5	
L89 1050E	.9	31.3	49.4	163	.3	25.5	13.6	2238	2.07	14.7	.7	2.3	1.8	30	.7	.8	.6	12	.28	.193	15	8	.17	240	.035	5	1.57	.011	.10	1	.04	1.3	1<.05	4	<.5	5	
L89 1075E	1.0	48.5	42.4	170	.2	26.5	15.8	1389	2.83	22.3	.8	23.3	3.4	42	6	1.2	.8	12	.37	.227	17	9	.22	155	.038	6	1.60	.012	.12	1	.04	2.0	1<.05	4	<.5	5	
L89 1100E	1.0	47.7	38.6	178	.2	27.8	17.3	1201	3.15	24.3	.9	85.6	4.5	43	5	1.2	.8	13	.38	.263	18	10	.24	141	.043	4	1.80	.013	.13	1	.03	2.5	1<.05	4	<.5	5	
L89 1125E	.8	22.7	31.8	170	<.1	20.1	9.5	745	1.99	13.0	.4	8.7	4.7	49	.4	.5	.5	14	.31	.105	16	6	.12	217	.031	4	1.22	.010	.11	1	.02	1.3	1<.05	3	<.5	5	
L89 1150E	.6	16.9	71.3	346	<.1	26.3	9.2	1986	1.70	13.3	.4	.7	2.6	60	6	.4	.4	14	.33	.149	12	13	.17	346	.051	4	1.70	.016	.13	<.1	.03	1.6	1<.05	4	<.5	5	
L89 1175E	.8	35.4	39.1	111	<.1	27.0	13.1	158	2.69	12.3	.5	1.0	8.8	17	2	1.0	.7	12	.17	.020	29	9	.33	72	.032	2	1.60	.008	.09	1	.01	1.7	1<.05	4	<.5	5	
L89 1200E	.8	32.4	32.9	85	2	30.0	11.7	132	2.51	10.6	.8	2.6	7.0	33	2	.7	.5	19	.16	.038	17	10	.29	125	.084	2	2.83	.021	.09	1	.03	2.4	1<.05	6	<.5	15.0	
L90 700E	.9	11.6	14.2	42	2	36.8	11.7	479	2.00	7.3	8	10.7	4.1	18	1	.3	.3	23	.14	.062	9	9	.20	146	.120	2	3.58	.019	.07	2	.03	2.2	1<.05	8	<.5	15.0	
L90 725E	.8	9.6	20.3	54	.3	48.3	9.2	823	1.80	10.3	.3	3.9	2.2	16	3	.3	.4	20	.18	.063	7	8	.15	153	.078	2	2.34	.013	.07	2	.05	1.4	1<.05	7	<.5	15.0	
L90 750E	.9	18.8	21.2	116	8	64.0	9.6	916	1.90	7.3	.7	5.2	3.6	15	.4	.4	.3	20	.12	.108	11	9	.19	161	.090	2	2.66	.019	.07	2	.04	2.6	2<.05	6	<.5	15.0	
L90 775E	.8	16.4	24.1	119	.5	34.1	9.5	1139	1.89	6.6	.4	3.4	2.6	24	5	.3	.3	18	.20	.097	12	9	.21	197	.049	2	1.88	.010	.07	1	.04	1.5	1<.05	5	<.5	7.5	
L90 800E	.9	20.0	20.4	106	.3	28.7	10.6	864	2.28	7.9	.5	28.7	3.9	18	2	.6	.4	16	.14	.069	18	11	.24	215	.030	2	1.61	.008	.09	1	.03	1.4	1<.05	4	<.5	7.5	
L90 825E	2.8	116.6	70.3	259	<.1	32.9	33.2	549	4.16	79.4	.5	3.0	6.5	12	3	2.4	1.4	7	.09	.071	23	9	.33	87	.005	4	.96	.003	.06	<.1	.02	1.2	1<.05	2	<.5	5	
L90 850E	1.8	35.0	29.7	138	.3	60.2	12.7	483	2.66	52.5	.3	2.5	5.4	10	3	1.0	.6	13	.06	.035	19	8	.22	105	.026	2	1.42	.007	.07	1	.02	1.3	1<.05	4	<.5	5	
L90 875E	1.3	26.5	33.3	104	2	45.7	13.2	384	2.80	14.8	.4	13.1	5.3	16	3	1.0	.7	14	.13	.035	19	9	.20	114	.023	1	1.63	.006	.12	1	.03	1.3	2<.05	4	<.5	5	
L90 900E	3.1	124.5	264.6	132	.7	44.1	18.4	518	4.82	42.6	.6	22.3	8.5	23	3	2.8	2.5	6	.18	.047	29	5	.07	73	.005	7	.54	.002	.09	1	.03	1.9	2<.05	1	<.5	5	
L90 925E	3.1	68.4	95.4	91	.3	31.6	12.4	140	3.23	30.6	.5	36.8	7.4	8	2	2.3	1.3	5	.07	.038	39	5	.06	26	.003	1	.43	.002	.08	1	.01	1.3	2<.05	1	<.5	5	
L90 950E	2.1	44.6	131.6	118	.3	32.2	16.7	927	2.81	23.9	.5	11.0	4.6	26	4	1.5	1.0	8	.26	.067	29	5	.08	124	.011	4	.76	.004	.09	1	.03	1.2	2<.05	2	<.5	5	
L90 975E	1.0	43.1	37.9	182	.2	34.6	19.6	1540	3.26	16.8	1.2	4.3	2.8	59	5	1.0	.9	18	.50	.414	16	11	.26	281	.046	6	2.36	.010	.13	1	.04	2.4	2	.07	5	<.5	5
L90 1000E	.4	16.9	20.2	119	.1	26.2	10.1	1031	2.02	16.6	.5	18.1	2.9	48	.3	.3	.4	18	.44	.279	9	10	.16	231	.076	6	2.16	.022	.11	1	.04	2.0	1<.05	5	<.5	5	
L90 1025E	.8	25.9	37.2	262	.1	29.5	15.9	2304	2.45	17.4	.5	21.7	4.3	42	.6	.4	.5	20	.32	.129	18	12	.19	359	.036	3	1.65	.010	.13	1	.04	2.0	2<.05	4	<.5	5	
L90 1050E	2.0	91.5	834.5	358	.6	46.7	19.1	425	5.21	50.8	.6	15.4	12.2	16	4	6.1	2.2	13	.13	.034	29	12	.47	49	.012	2	1.37	.003	.09	1	.02	1.6	1<.05	4	<.5	7.5	
STANDARD DS7	21.3	111.3	71.3	416	.9	57.0	9.8	630	2.42	48.4	5.0	71.4	4.4	68	6.4	6.0	4.5	88	.93	.080	12	166	1.06	375	.126	39	.97	.073	.44	3.9	.20	2.5	4.2	.22	5	3.7	15.0

Sample type: SOIL PULP. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Il	S	Ga	Se	Sample		
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppb	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	%	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	
L94 1150E	1.0	15.2	17.2	82	.3	44.1	14.1	1461	2.34	13.5	.5	52.4	4.4	16	.2	.5	.4	22	15	.068	14	13	.20	195	.054	2	2	.01	.009	.09	.1	.03	1.8	1<.05	5	<.5	7.5		
L94 1175E	1.2	19.4	21.7	88	.2	39.7	14.0	705	2.56	14.5	.6	13.6	4.6	13	.2	.7	.5	21	.08	.051	14	13	.19	149	.051	2	2	.11	.008	.07	.2	.04	1.8	1<.05	6	<.5	15.0		
L94 1200E	.8	17.4	23.2	126	.2	50.0	15.6	2484	2.29	13.0	.4	10.9	4.1	31	.4	.5	.5	20	19	.047	16	12	.18	198	.051	2	1	.78	.010	.09	.1	.03	1.6	1<.05	5	<.5	15.0		
L95 700E	1.0	19.5	32.4	128	.1	46.4	18.0	3526	2.83	16.4	.7	3.5	4.7	42	.5	.8	.6	26	36	.084	14	12	.23	257	.076	4	2	.60	.013	.13	.2	.04	2.3	2<.05	7	<.5	7.5		
L95 725E	2.0	47.9	54.0	135	.1	47.1	31.5	2614	4.48	19.0	.8	1.0	4.4	46	.4	2.0	1.4	20	36	.104	21	15	.38	218	.044	2	2	.24	.007	.13	.1	.04	2.0	2<.05	6	<.5	5		
L95 750E	1.9	24.2	38.2	103	.2	48.4	18.9	1896	3.19	13.7	.6	2.5	5.3	25	.3	1.8	.9	19	18	.044	14	11	.27	205	.026	3	2	.05	.007	.13	.1	.03	1.8	2<.05	5	<.5	7.5		
L95 775E	1.6	48.5	68.7	195	.3	59.3	27.7	1427	4.34	36.0	.6	<.5	7.2	17	.4	2.9	1.3	16	12	.060	19	11	.31	146	.016	2	1	.84	.006	.13	<.1	.02	2.1	2<.05	5	<.5	5		
L95 800E	2.1	53.6	67.9	228	<.1	39.0	18.3	503	4.36	36.1	.7	27.8	8.0	15	.3	4.7	1.3	13	13	.050	29	13	.39	54	.011	2	1	.32	.004	.07	.1	.02	1.8	2<.05	4	<.5	7.5		
L95 825E	1.1	47.1	53.1	243	<.1	30.6	21.9	1368	3.41	24.6	.5	.5	7.8	36	.2	1.9	.8	12	31	.080	25	14	.54	123	.005	3	1	.83	.004	.11	.1	.03	1.8	3<.05	5	<.5	5		
L95 850E	.7	21.0	35.9	171	.2	33.9	11.4	681	2.36	12.2	.6	2.0	4.7	20	.2	.7	.5	24	13	.183	10	13	.28	172	.097	3	2	.89	.014	.09	.2	.04	2.0	2<.05	8	<.5	7.5		
L95 875E	1.5	28.9	30.9	104	<.1	25.6	13.6	972	2.87	18.4	.5	15.7	6.7	10	.2	1.5	.7	14	.04	.054	23	10	.32	103	.009	1	1	.27	.003	.05	.1	.02	1.3	1<.05	3	<.5	7.5		
L95 900E	.9	17.3	34.2	185	.2	32.8	13.7	1550	2.47	12.3	.4	3.3	4.3	12	.3	1.4	.7	18	.09	.112	15	11	.28	154	.039	1	1	.91	.007	.09	.2	.04	1.5	1<.05	6	<.5	7.5		
L95 925E	1.1	29.5	30.4	115	.2	23.8	13.6	826	2.86	20.4	.4	6.2	5.8	7	.2	1.7	.8	12	.06	.056	23	10	.33	84	.013	<.1	1	.26	.004	.06	.1	.02	1.4	1<.05	3	<.5	5		
L95 950E	.8	11.9	17.2	113	.2	24.8	9.6	2112	1.86	8.4	.6	4.3	2.4	20	.2	.3	.3	20	15	.135	10	9	.17	152	.073	2	2	.65	.012	.06	.1	.04	1.8	1<.05	7	<.5	15.0		
L95 975E	.8	15.9	30.9	109	.3	29.2	13.0	3354	1.91	7.2	.4	4.9	1.9	19	.3	.3	.3	20	11	.087	11	9	.14	154	.061	1	1	.65	.010	.07	.1	.05	1.4	1<.05	7	<.5	5		
L95 1000E	1.0	17.1	20.9	71	.2	36.1	13.5	1209	2.37	13.1	.4	14.0	4.7	17	.2	.7	.6	16	12	.097	19	8	.19	131	.035	2	2	.06	.008	.07	.1	.02	1.4	1<.05	6	<.5	7.5		
L95 1025E	1.1	14.5	21.3	46	.2	29.3	14.7	2312	2.46	14.7	.4	28.7	2.2	14	.2	.5	.6	20	.08	.063	16	10	.17	171	.028	2	1	.66	.007	.06	.2	.03	1.4	1<.05	6	<.5	7.5		
L95 1050E	.9	17.1	18.6	44	.1	28.2	15.7	1948	2.57	12.3	.4	14.9	3.5	20	.2	.5	.6	15	26	.047	19	9	.19	133	.014	2	1	.43	.006	.09	.1	.03	1.5	1<.05	4	<.5	5		
L95 1075E	.9	14.6	17.9	41	.1	27.3	13.0	741	2.50	12.2	.3	8.8	3.9	13	.1	.5	.6	17	16	.042	19	9	.19	105	.022	2	1	.57	.007	.09	.1	.03	1.4	1<.05	5	<.5	9		
L95 1100E	1.0	23.7	21.9	60	.3	28.6	16.7	1017	2.98	16.8	.6	18.5	4.0	18	.3	.7	.7	20	18	.039	17	11	.18	128	.027	1	1	.87	.007	.09	.1	.04	1.7	1<.05	6	<.5	7.5		
L95 1125E	1.5	24.2	26.1	78	.2	27.8	16.2	451	3.30	17.6	.7	58.7	7.1	15	.2	1.2	.7	20	11	.045	20	10	.18	81	.023	1	1	.63	.006	.10	.2	.03	2.0	1<.05	5	<.5	7.5		
L95 1150E	1.0	38.3	31.7	105	.2	26.9	16.7	1450	2.79	14.7	.5	17.9	5.0	25	.5	.8	.7	16	19	.051	23	12	.23	146	.014	1	1	.27	.004	.10	.1	.04	1.8	1<.05	4	<.5	5		
L95 1175E	1.0	25.3	32.6	109	.2	41.5	16.5	1497	2.81	15.1	.5	116.0	4.1	28	.4	.8	.7	19	16	.055	21	12	.28	113	.023	2	1	.78	.008	.11	.1	.03	1.7	1<.05	5	<.5	5		
L95 1200E	2.7	56.2	34.6	84	.2	33.0	24.7	604	4.25	27.7	.5	15.1	6.1	7	.1	2.2	1.5	10	.04	.054	15	7	.21	46	.006	1	.95	.003	.08	.1	.02	1.4	1<.05	3	<.5	5			
L95 1225E	2.3	86.4	43.0	81	.1	37.2	22.6	299	4.45	32.9	.6	62.1	7.0	9	.1	3.1	1.8	8	.08	.036	26	9	.32	20	.003	<.1	.90	.002	.07	<.1	.02	1.6	1<.05	2	5	5			
L95 1250E	1.8	42.0	37.9	205	.3	34.6	26.2	4211	3.39	17.6	.6	18.4	1.8	39	.9	.9	1.0	19	36	.131	16	11	.25	325	.028	3	1	.47	.007	.14	.1	.03	1.7	1<.05	5	<.5	5		
RE L95 1250E	1.7	39.5	41.6	194	.3	33.2	25.6	3995	3.22	17.2	.7	10.0	1.8	37	.8	.9	1.0	18	34	.129	16	10	.25	326	.027	3	1	.47	.007	.13	.1	.03	1.6	1<.05	4	<.5	5		
L95 1275E	1.1	35.0	24.8	101	.2	32.0	17.3	4657	2.67	15.9	.9	3.0	4.0	73	.5	.9	.7	21	58	.206	17	8	.20	347	.054	5	2	.14	.011	.12	.2	.06	2.4	2<.05	5	5	7.5		
L95 1300E	1.0	29.5	22.9	77	.1	39.9	19.8	1081	3.00	22.6	.6	1.1	8.4	33	.1	.8	1.0	21	18	.051	28	11	.25	186	.052	3	2	.12	.009	.12	.1	.03	1.7	2<.05	5	<.5	5		
STANDARD DS7	21.4	115.2	73.2	421	.9	57.8	10.0	637	2.47	48.4	5.1	70.8	4.4	69	6.5	6.0	4.5	89	94	.080	12	170	1.08	379	.126	40	.97	.074	.45	4.0	21	2	5	4	3	22	5	3.8	15.0

Sample type: SOIL PULP. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.