Geophysical and Geochemical Report

-- on the --

KENTUCKY LAKE PROPERTY
Nicola Mining Division, British Columbia

-- for --

Max Investments Inc.

-- on behalf of --

Bold Ventures Inc.
#430 – 580 Hornby Street
Vancouver, B.C. V6C 3B6

Located: 120 degrees, 30 minutes W; 50 degrees 50 minutes N
NTS map sheet 92H/15
25 kilometers southwest of Merritt, B.C.

Prepared By:

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208 – 515 West Pender Street
Vancouver, B.C. V6B 6H4

January 15, 2007

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SUMMARY

Bold Ventures Inc. (Bold) has entered into an agreement with Richard Billingsley and Gayle Richards, whereby Bold can earn up to a 100% interest in the ***Kentucky Lake Project****, an early stage exploration project with no known resource. This report summarizes all data available on the property. The property consists of 5 mineral claims (2414 hectares), located in the Nicola Mining Division, 25 km south of Merritt, British Columbia. Well-maintained gravel roads leaving Highway #5A north of Princeton and south of Merritt provide good access to all areas of the property.*

Copper mineralization in the area was recognized early in the twentieth century. Early explorers completed some trenching, pitting, shaft sinking and diamond drilling in the 1920s and 1930s. Modern day exploration was undertaken in the late 1960s, early 1970s, and 1980s. It is believed that 15 - 16 drill holes were completed on the property with very little documented data. At least two shafts were sunk and several old trenches have been located. There is evidence of old grids, with various geochemical and geophysical surveys documented in assessment reports.

The property is located in the Intermontane belt of Triassic volcanic rocks in central British Columbia. In the southern areas of the province, the dominant rock types are volcanic rocks of the Nicola group. The Nicola group is the principal rock group of the property and is the host rocks of most mineralization of value. Intruding the Nicola group are late Triassic felsic intrusive bodies, believed to be the mineralizing source. The structural setting of the property is a very complex set of faults, the main structure being the Summers Creek/Kentucky Lake fault.

Nine mineral showings are reported on the property, six having been located and are discussed in detail in this report. The known mineralized showings are associated with faults, small shears and main intrusive contacts and occur in highly altered, sheared and brecciated rocks of both the volcanics and intrusives. Strong alteration patterns of typical porphyry deposits have been identified, mainly being propyllitic in nature, however phyllic and argillic alteration is also present. Sulphide minerals identified are pyrite, chalcopyrite, chalcocite with lesser contents of pyrrhotite, marcasite, and bornite. Secondary oxide minerals include malachite and azurite.

Max Investments Inc., on behalf of Bold Ventures Inc., carried out the initial phase of an exploration program on the property during the summer months of 2006. The program consisted of a 28 kilometer grid over the area of the property containing all nine mineral showings. SJ Geophysics Ltd. was retained to complete a 3D Induced Polarization survey, the survey collecting reliable depth readings to 300 meters. Cost of the program was $110,718.

Results established viable chargeability IP drill targets in areas associated with mineral showings. In addition, soil samples were collected along all grid lines and analyzed for 36 elements by MS-ICP methods. Resulting plots of copper values indicate an association of mineral showings to copper soil anomalies. There were no other elements of potential economic worth identified in these results.

*Ongoing work programs are warranted on the property and a **Phase I** program has been designed to detail various soil anomalies, continue property exploration and initiate diamond drilling. A total of five diamond drill holes (1350 meters) are being recommended as the **PHASE I** exploration program.*

BOLD VENTURES INC.

KENTUCKY LAKE PROPERTY

BRITISH COLUMBIA

LOCATION MAP

DRAWN BY: JOHN R. KERR	DATE: SEPTEMBER, 2006
SCALE: AS SHOWN	FIGURE NO. 1

INTRODUCTION

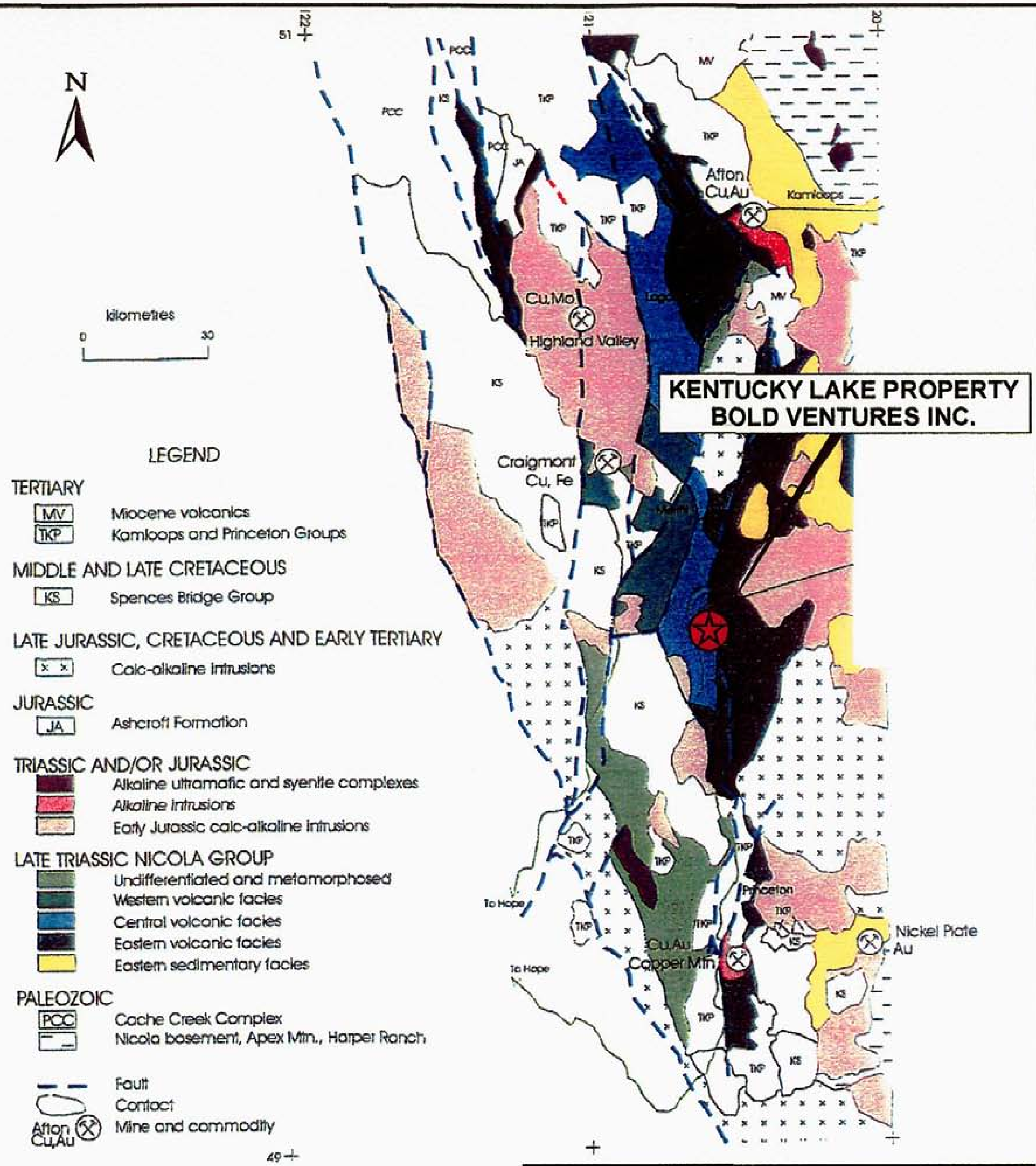
General Statement and Terms of Reference:

The porphyry copper (gold, molybdenum) deposits of central British Columbia have been the main base/precious metal mining operations of the province for the past five decades. Exploration for these type of deposits were at a peak in the late 1960s and early 1970s, however by 1980 and mainly due to weak copper prices, much of the interest in porphyry deposits had ended, as emphasis was placed on exploration for precious metal deposits. Therefore, much of the exploration glamour of central British Columbia had shifted other areas of North America and the rest of the world. Improvement in base and precious metal prices and recent advances in exploration tools, such as airborne geophysical systems, induced polarization techniques, geochemistry, and drilling techniques, it is now time to revisit the porphyry deposits of British Columbia. Major changes to mining and recovery methods have vastly improved the efficiency of large-scale, open-pit mining operations. Coupled with a better geological understanding of the nature of porphyry deposits, the opportunity now exists to focus on this style of mineralization, applying new and advanced techniques of exploration, mining and recovery of the metals.

South-central British Columbia is considered the copper mining center of Canada. In total, some 3 billion tonnes have been identified in ore of the Highland Valley grading an average of 0.45% copper and up to 0.8 grams per tonne gold. Current annual production from the Highland Valley mine operated by Cominco is 160,000 tonnes of copper. The Alwin Mine property adjoins Cominco's large Highland Valley land holding and is located 5 km to the west of the Valley Copper open pit.

Richard Billingsley and Gaye Richards, currently the beneficial owners of the Kentucky Lake property, have entered into an option/joint venture agreement with Bold Ventures Inc. (Bold), dated June 21, 2006, to sell 100% interest in the Kentucky Lake property. Mr. Chris Dyakowski, President of Max Investments Inc., requested on behalf of Bold, that I examine the property, compile all available data and prepare this report.

I visited the site and observed the line-cutting and soil sampling programs in progress on July 24, 2006. I was a **Qualified Person**, as defined in NI 43-101, at the time of this property examination.



BOLD VENTURES INC.

KENTUCKY LAKE PROPERTY

SIMILKAMEEN MINING DIVISION,
BRITISH COLUMBIA

REGIONAL GEOLOGICAL MAP

DRAWN BY: JOHN R. KERR	DATE: OCTOBER, 2006
SCALE: AS SHOWN	FIGURE NO. 2

To accompany a report by John R. Kerr, P. Eng.

Location and Access:

The property is located in south-central British Columbia, 25 kilometers south of Merritt. The geographic coordinates of the property are 120 30' west; and 50 50' north (NTS map sheet 92H/15). The property is accessed along well-maintained roads from Merritt or Princeton along Highway #5A to the west end of the Kentucky Lake Provincial campsite turn-off, approximately 22 km south of Merritt. A well maintained logging road leads 1.8km to the east a road junction, and then south approximately 0.5km to the northern property line. This road traverses the entire 4 km north/south length of the property and is the main access route. Several other logging roads provide good access to most areas of the property.

Topography and Vegetation:

Semi-arid weather conditions prevail in the Merritt/Princeton area of British Columbia, the property being located at the transition of the eastern margin of the Coast Mountains with the interior plateau. The property is very flat, with local knolls exposing outcrop. Valleys are generally flat and filled with overburden ranging 2 – 30 meters deep. Overall relief is 200 meters, elevations ranging 1,000 – 1,350 meters (asl).

Vegetation is typical interior light forest cover of fir, hemlock, balsam and pine. Portions of the claims have been selectively logged.

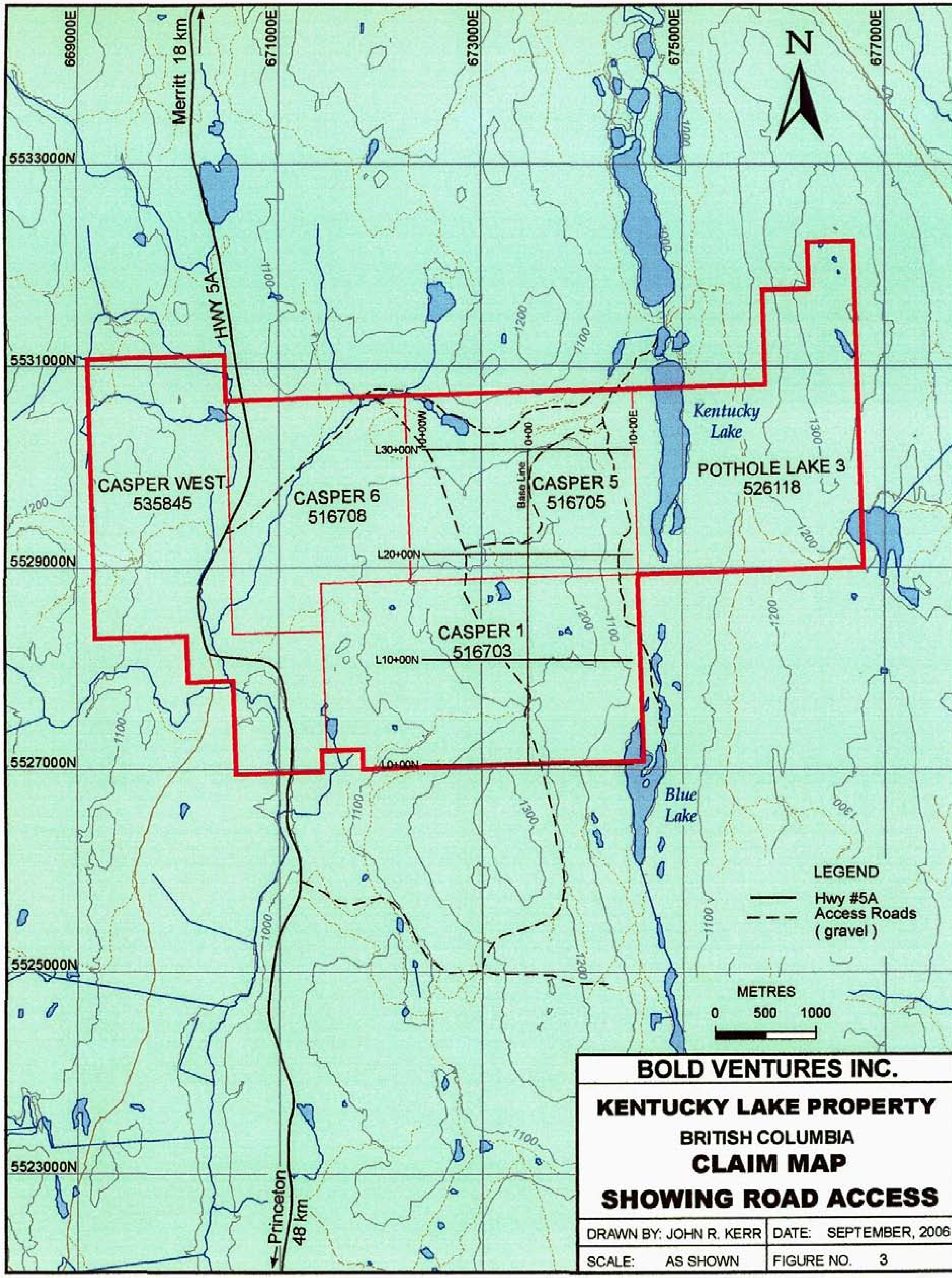
Claims:

The Kentucky Lake property consists of five contiguous claims, comprising approximately 2414 hectares.

Claim Name	Type of Claim	Size of Claim	Tenure Number	Expiry Date
Casper 1	CGS	583h/a	516703	Jan. 31, 2010
Casper 5	CGS	416h/a	516705	Jan. 31, 2010
Casper 6	CGS	375h/a	516708	Jan. 31, 2010
Pothole Lake 3	CGS	520h/a	526118	Jan. 31, 2010
Casper West	CGS	520h/a	535845	Jan. 31, 2010

- Expiry dates are as documented at Mining Recorder's records on January 8, 2007
- CGS – Claims located on-line by Cell Grid System

All claims are located in the Merritt Mining Division and recorded in the name of Richard John Billingsley (RJB). RJB and his partner Gaye Richards entered into an agreement dated June 21, 2006 with Bold Ventures Inc., whereby Bold can earn a 100% interest in the property by paying $115,000 and issuing 200,000 shares to the vendors over a three year period. The claims are subject to a 2%NSR interest, which can be purchased during the initial 5 years of commercial production by Bold for $2.0 million.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CASPER 5
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CASPER 1
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L20+00N
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10+00W
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Base Line
LEGEND
Hwy #5A
Access Roads (gravel)
METRES
0 500 1000
BOLD VENTURES INC.
KENTUCKY LAKE PROPERTY
BRITISH COLUMBIA
CLAIM MAP
SHOWING ROAD ACCESS
DRAWN BY: JOHN R. KERR
DATE: SEPTEMBER, 2006
SCALE: AS SHOWN
FIGURE NO. 3

Adjacent Properties:

The claims are surrounded by existing mineral tenure on the north, east and south sides. To the north the adjoining claims are owned by Christopher James Mines Ltd., an aggressive junior mining company, who have completed extensive surface surveys and diamond drilling over the past five years in search of a porphyry copper/gold resource. To the east and south, the bordering claims are owned by Gary Robert Brown, with no knowledge apparent of major exploration work. The ground is open to the west.

HISTORY of DEVELOPMENT

Historical Exploration:

Copper mineralization was discovered in the area in the late nineteenth century. The Bunker Hill and Tom Cat showings are documented to be two of the earlier showing discovered. Early exploration in the1910 – 1930 period included prospecting, geological mapping, limited diamond drilling (Boomerang showing) and a number of pits, trenches, shafts and short adits being excavated on the more promising showings. There is no record of early commercial production

The property remained dormant until the early the 1960s, when the several operators located mining claims covering various mineral showing in the area. The following summarizes the work since 1964:

1964 - 1974: The principle operators in the area during this period were Scope Development Ltd., Alscope Consolidated Ltd. and Pyramid Mining Company Ltd. Scope and Alscope conducted geological mapping, geophysics, limited geochemistry and trenching over most of the showing areas. They also completed an unknown, however believed very limited, diamond drill program on the Boomerang showing in 1967. Results are not reported.

Pyramid Mining completed 13 diamond drill holes (1042 meters) on the Tom Cat showing in 1965, the best intersection reported is an average grade of 0.32%Cu over a 45.7 meter length of the hole.

Vananda Explorations Ltd. and Merritt Copper Co. completed geophysical surveys and diamond drilling on the showings immediately north of the property in 1967. It is believed this property is currently owned by Christopher James Mining Co.

1975 – 1981?: Most of the area of the current property was owned by Fred Gingell of Merritt, who completed geochemical and geophysical surveys in various areas of the property for assessment credits. Mr. Gingell allowed the claims to expire.

1983 - 1985: I.M. Watson and J. Randa staked the ground in 1983/84, and immediately optioned the property to Vanco Explorations Ltd. Vanco completed limited grid and geological mapping over selected grid areas.

1986 – 1989: The property was optioned to Laramide Resources Ltd. who completed further geochemical and geophysical surveys on the selected grid areas. There is no record of diamond drilling during this tenure.

The claims were permitted to lapse in the 1990s. No work is documented on the property since 1987.

Recent Exploration:

2005 - 2006: Richard Billingsley commenced locating claims in the area in July, 2005, and by June, 2006 had completed establishing the current claim package. An option agreement was completed to permit Bold Ventures Inc. to earn a 100% interest in the property. They have completed a Three Dimensional Induced Polarisation program over 28 kilometers of grid covering the entire the property. Soil samples were collected at 50 meter intervals along all grid lines and analyzed for 32 elements by ICP methods.

This report integrates the results of 2006 work programs into historical data and provides the material to recommend ongoing work programs. There are no historical resource estimates documented for this property.

GEOLOGY

Regional Setting

The project area lies within the Intermontane belt of Mesozoic rocks between Princeton and Merritt. This belt of rocks carries south into the United States and north into the Yukon Territory. The distinguishing and oldest rock group in this belt is the volcanic and sedimentary rocks of the Triassic Nicola group. Preto (Bulletin 69) has subdivided this group into the western, central, and eastern facies. The eastern facies is dominantly intermediate purple/gray/green flows, breccias, tuffs, lahar breccias, with minor sandstones and siltstones. The central facies is intermediate to basic flows, breccias and tuffs, with more dominant limestone, siltstone, argillite, and conglomerate. The western facies is acidic to intermediate flows, breccias and tuffs, with minor limestone.

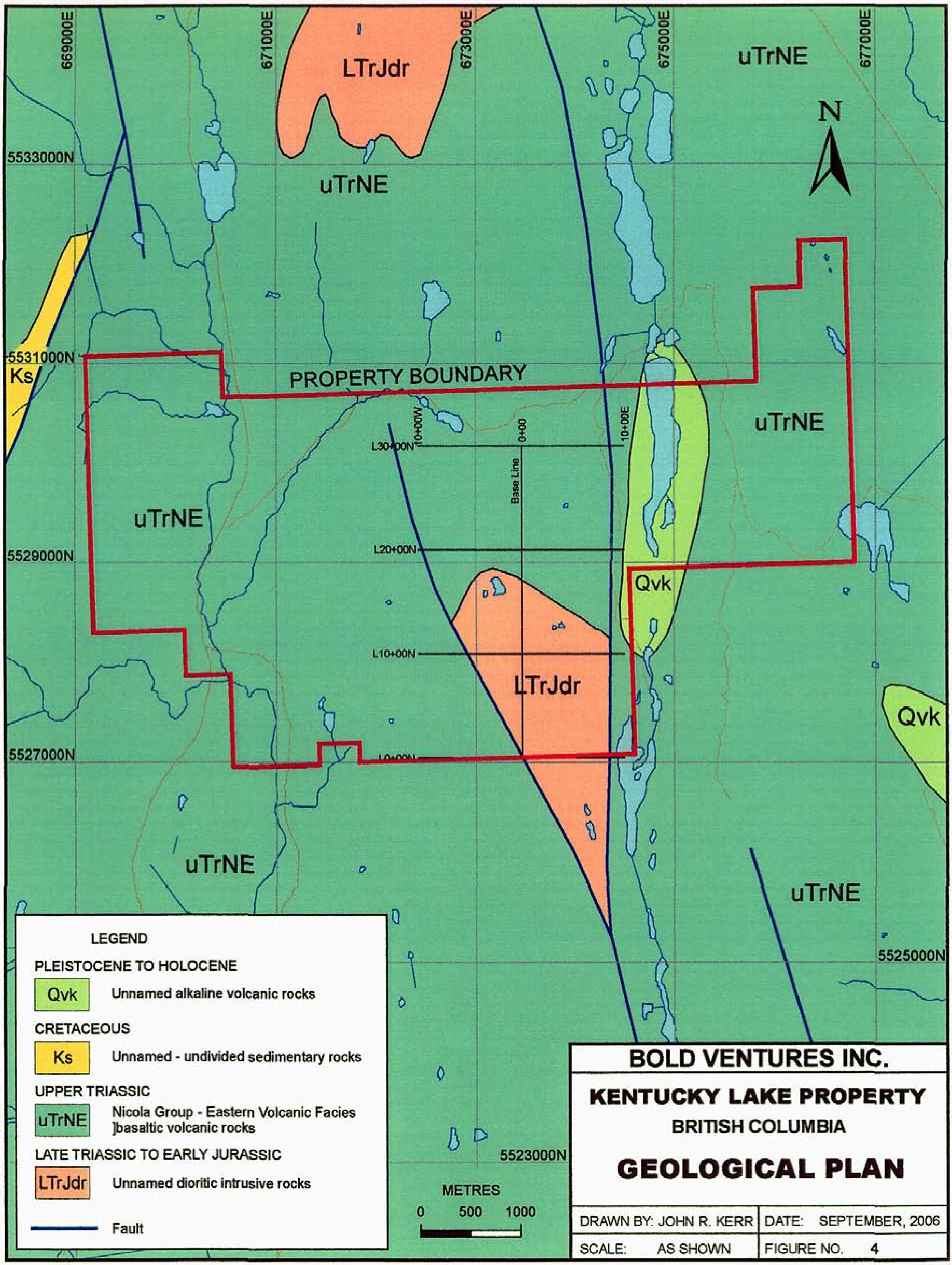
Intruding the Nicola volcanics are numerous stocks, sills, small plutons, batholiths and dikes of various ages and of a varied composition. The more sizeable intrusions are the Jurassic Pennask batholith, the lower Jurassic Allison Lake pluton, and the Cretaceous Summers Creek stocks. The intrusive rocks are acidic to basic in composition, however most are alkalic in nature. The most dominant rock descriptions are diorite, monzonite and granodiorite.

The lower Cretaceous Kingsvale group of dominantly volcanic rocks unconformably overly the Nicola group and earlier intrusions. These rocks are intermediate to felsic flows, tuffs, ash flows and lahar breccias. The Summers Creek stocks intrude rocks of the Kingsvale group, Overlying all rocks are Tertiary basalts and andesites of the Princeton group and sedimentary rocks of the Coldwater beds.

Property Geology

The dominant rock types of the property are volcanic and sedimentary rocks of the central facies of the Triassic Nicola group, and stocks and small batholiths of Triassic diorites and monzonites. The eastern facies is present along the eastern property boundary.

The central facies of the Nicola group has been subdivided into three basic units; flows, pyroclastics and sediments. The flows are most abundant and are described as purple/green amygdaloidal augite andesite with interbedded trachyandesite feldspar porphyry. The pyroclastic units are massive to finely bedded crystallithic andesite tuffs with interbedded siltstone and light gray/green dacite tuff. Graded bedding is locally identified, with occasional diagnostic lapilli sized fragments, common to explosive breccias and lahars.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Fault
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BOLD VENTURES INC.
KENTUCKY LAKE PROPERTY
BRITISH COLUMBIA
GEOLOGICAL PLAN
DRAWN BY: JOHN R. KERR
DATE: SEPTEMBER, 2006
SCALE: AS SHOWN
FIGURE NO. 4

The sediments are dominantly interbedded greywacke, siltstone and minor conglomerate and massive beds of gray to light brown limestone. All Triassic rocks are hornfelsic in nature near the contact of intrusions. Some of the sedimentary horizons have developed slaty and/or schistose cleavages.

The intrusive rocks on the property have been classified as alkalic late Triassic granodiorite and quartz diorite, and are located in one small batholith covering the southeastern area of the property. Late felsic and porphyritic dike swarms are found in all areas of the property, dominantly in the contact area of the batholith.. The ages are unknown, however are probably related to late phase intrusive activity. Very late basic dikes are related to Tertiary vulcanism. These dikes are post-mineralization. A simplified interpretation of the geology is presented on figure 4.

Structural Geology

Bluey and Kentucky Lakes form a strong lineal feature that probably is related to the northern projection of the Summers Creek fault. This lineament passes through the eastern boundary area of the claims. A splay fault trending northwest forms the western boundary of the granodiorite intrusion. Small local shears and fault zones were noted during the time of the property examination.

Alteration and Mineralization

Alteration and mineralization noted on the property are mainly related to the main structures and to the main intrusive body. In total, nine old mineral prospects are reported on the property, seven having been found and examined and sampled. The following is a brief description of each of the prospects:

1) Tom Cat Showing: Located in a large area of outcrop, approximately 100x100meters in the west-central portion of the property. Rock types examined included med grained granodiorite in contact with andesites of the Nicola Group. Mineralization observed is chalcopyrite, chalcocite, pyrite, magnetite and malachite disseminated in altered granodiorite. Alteration included epidote, chlorite, sericite, quartz and calcite. A chip sample (K-02) across a 2 meter face of the trench assayed 3.68% copper. 20 meters west of the trench, a well-mineralized pod (sample K-03) assayed 1.77% copper across 1.5 meters. Two old drill pads were located from drilling in the 1960s. One of these holes reports 0.32% copper over 45.7 meters of core length.

   The Tom Cat Showing is located on the southeastern flank of a moderate soil anomaly ranging to 145ppmCu and to the south of a strong chargeability IP anomaly. For these associations as well as the assays reported in trenches and old drill holes, this area becomes the prime target of further exploration on the property.

2) <u>Bluey Showing:</u> Located in the southern portion of the property. Chalcopyrite, chalcocite, pyrite, malachite and azurite are associated with small quartz veinlets hosted by altered andesite of the Nicola Group. Alteration includes epidote, chlorite, quartz and sericite, with considerable rusting from oxidized sulphide minerals. One chip sample (K-04) across a 4 meter length indicates 9189ppm copper, 1551ppm lead, 7973ppm zinc and 10.9ppm silver. Zinc and lead minerals were not identified in hand specimens.

   The Bluey showing is located on the eastern flank of a moderate soil anomaly (ranging to 147ppmCu) and a strong chargeability anomaly.

3) <u>Bunker Hill Showing:</u> Located in the south/central portion of the property, in volcanic rocks, very near an intrusive contact. Brown carbonate alteration and quartz veining were observed in several pits and short trenches. Chalcopyrite, chalcocite, pyrite and malachite are found in altered zones. One chip sample K-05 across a 2 meter width yielded 3.73% copper.

   The Bunker Hill showing is located within a 200x400 meter weak soil anomaly ranging to 58ppmCu, and is on the eastern flank of the same strong chargeability IP anomaly as the Bluey showing.

4) <u>Portland Showing:</u> Located in the western portion of the property and in the western fringe area of the grid. A shaft, reported to be 35 meters deep, and an old building exists at the site. Outcrops at the shaft are red and dark green laharic breccia and basaltic flows of the Nicola Group of volcanic rocks. The shaft appears to have been sunk on an altered shear zone. Mineralization was not observed in bedrock. A black mineral (chalcocite or magnetite?) was evidenced in samples from the dumps leading from the shaft. A sample (K-06) of this material yielded 1702ppmCu.

   The showing is located near a moderate soil anomaly to 148ppmCu and to the west of the strong chargeability IP anomaly near the Bluey showing.

5) <u>AR Showing:</u> Located in the northern area of the property and grid area. Two old trenches expose altered volcanic breccia and andesite/basalt flows of the Nicola Group. Chalcopyrite, pyrite and malachite are located as replacement pods and smears along fracture faces of altered volcanic rocks. Alteration includes epidote, carbonate, chlorite, minor quartz and sericite. A chip sample (K-01) over 1.5 meters length yielded 6962ppmCu.

   The area of the showing is associated wit a very weak copper soil anomaly and in the middle of a significant donut shaped chargeability IP anomaly.

6) AR 2 Showing: Located in the northern area of the property and grid area. One old pit (shaft?) is exposed in a minor shear zone of altered volcanic rocks of the Nicola Group. Pyrite, chalcocite?, and malachite are found in shears. A chip sample (K-07) across 0.5 meters yielded 5347ppmCu.

   The showing area is associated with only weak soil geochemistry and no chargeability IP anomalies.

7) Bloo Showing: Reported to be in the central portion of the claim area, however could not be located by crews. Reports indicate chalcopyrite and malachite in altered diorite, with assays reporting up to .483% copper.

   The reported location of the showing is 100 – 200 meters south of a moderate copper soil anomaly, with values up to 285ppmCu. There are no chargeability IP responses in the area.

8) Boomerang Showing: Located in the southeastern area of the property and grid area. The reported showings, shafts and old trenches have not been located to date, however signs of drill pads and old buildings do exist in the area. Chalcopyrite, bornite and malachite are reported along fractures of altered diorite. Main alteration is chlorite. Mineralized samples are reported to range 0.18 – 14.7% copper with up to 4 g/tAu and 74g/tAg. The reported location of the showing is associated with a moderate chargeability IP anomaly.

9) AM Showing: Located in the northeastern area of the property and could not be located due to very steep terraine. An old shaft is reported into a shear zone of altered andesite. Reported assays range up to 2% copper over 1.5 meters.

Several other alteration and shear zones were observed on the property, mainly in the southern and western portion of the grid, near the contact of the volcanic Nicola Group and diorite/granodiorite intrusion.

Deposit Types Searched For

The geological environment is suited to host a number of deposit types. The principle targets are alkalic porphyry copper (gold/molybdenum) deposits similar in nature to the deposits of the Axe property, 20 km to the south and to the inferred deposits of the Christopher James holdings to the north. The Tom Cat, Boomerang and Bloo showings are probably the most representative of porphyry styles of mineralization. There are many examples of replacement and skarn type of showings on the property, including the Bluey, Bunker Hill, Portland and AR showings. This could be related to the contact area of the intrusion and possibly be similar to the Craigmont deposit, northwest of Merrit along the contact of the Guichon Batholith. Of lesser importance on the property are vein gold/copper type of occurrences and epithermal gold deposits.

EXPLORATION

Pre – 2006 Exploration Programs:

Exploration Programs were conducted on the property during the period 1964 – 1989 by seven various operators, and are detailed in the History of Exploration section of this report. In summary, 15 -16 diamond drill holes were completed. Limited geophysics, geochemistry and geological mapping programs were also completed. Results of these programs are not well documented.

2006 Field Program:

In July, 2006, Max Investments Inc., on behalf of Bold Ventures Inc., commissioned a 28 kilometer 3D Induced Polarization Program (IP) to SJ Geophysics of Vancouver, B.C. The methodology is discussed in a report entitled 3D Induced Polarization Survey Geophysical Report, Kentucky Lake Project by Ron Sheldrake, Geophysicist, of SJ Geophysics (attached as Appendix C). A 3 km baseline and 28 km of cross lines were established by GPS, chain and compass methods of control. All cross lines were cleared by power saw suitable to complete induced polarization surveys. The gridded area covered the four main zones at 200 meter line intervals, with readings taken at 50 meters along all lines. The readings were computer processed producing a 3D model of the resource areas. A summary of these results are shown in Figure 6, with the showing areas superimposed.

At the time of establishing the grid, soil samples were collected at 50 meter stations along all cross lines. Every second sample collected was analyzed by multi-spectrographic ICP methods for 36 elements at the laboratories of Acme Analytical Laboratories Ltd. of Vancouver. The principle metal being copper was plotted on a representation of the grid, shown in Figure 5, with interpreted anomalies. The second set of samples are being saved for future analysis. Analytical sheets are presented in Appendix D.

On conclusion of grid establishment, the author visited the property examining all available showing areas. Seven rock-chip samples were collected and also submitted to Acme analytical for MS ICP analysis. Copper values over the limit (three samples) were assayed for copper. Results and sample descriptions are shown in Appendix D.

Costs of the 2006 are documented in Appendix A and total $110,718.

EXPLORATION RESULTS

Geochemistry:

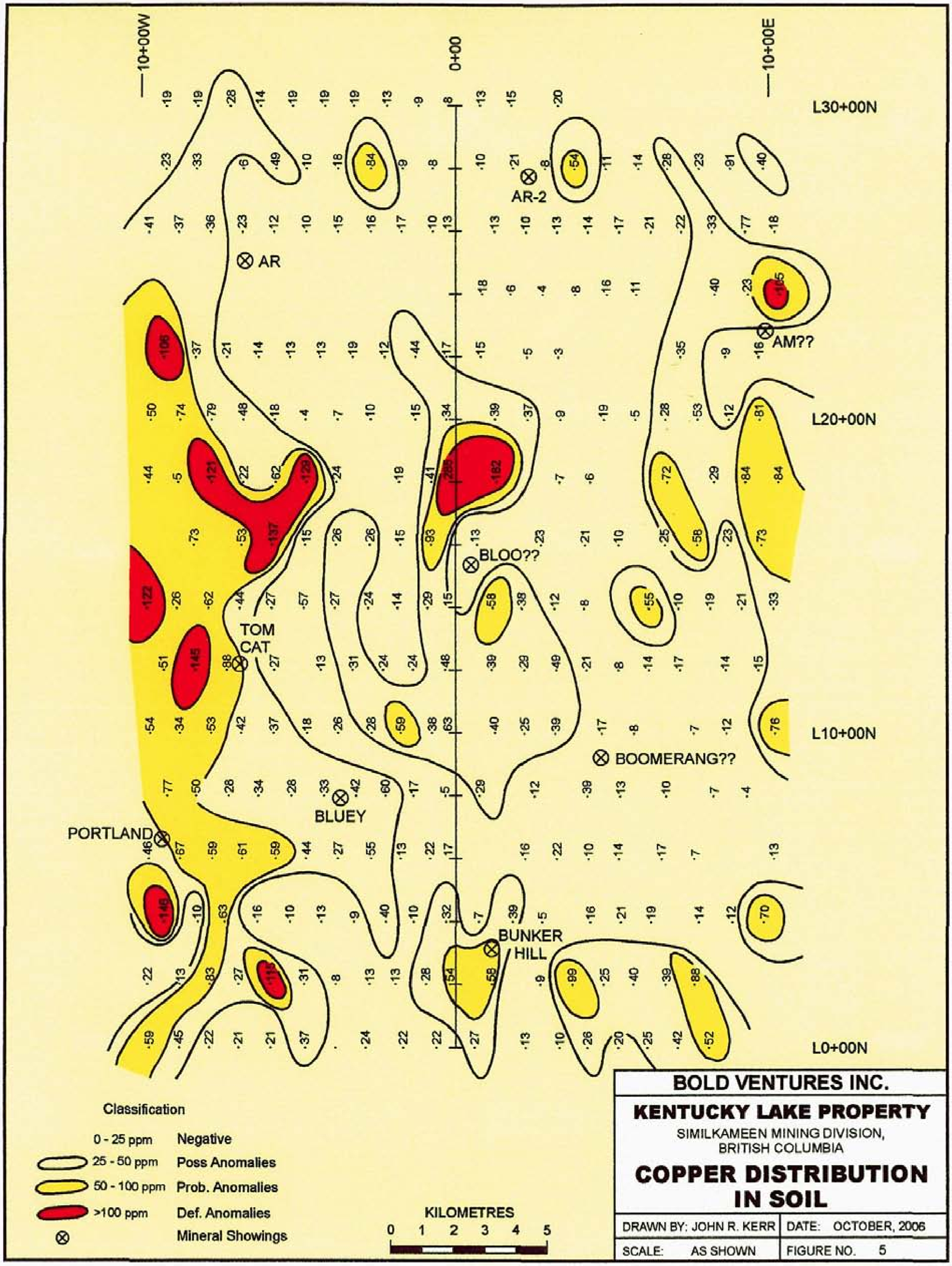
Soil sampling and rock-chip sampling has been completed as part of the grass-roots phase of several exploration programs. These surveys have generally been completed on small detailed grids covering the mineral showing areas. There is no evidence of a comprehensive regional soil sampling program over the entire showing area. It was not possible to integrate these historical surveys to the 2006 program due to inconsistencies of laboratories and inability to tie in base control of the older surveys.

Rock chip sampling of almost all outcrop areas has been done throughout the exploration history of the property. There has been no attempt to compile this data over history and the results of early surveys were not documented. Recent rock-geochemistry collected in the main mineralized resource areas confirms the presence of the mineral bearing zones. Future programs should incorporate thirty-element geochemistry and whole-rock analysis of surface samples and drill core to gain a better understanding of mineralized geochemistry and alteration.

The copper distribution plan as shown on Figure 5, indicates only a moderate response to copper content in soil. This probably is not a reflection of copper content in rock, and is probably more related to the chemical nature of the soil environment. In summary, the dominant soil results indicate a substantially large anomaly in the western portion of the grid, with several areas of bull's eye targets, and one substantial anomaly in the central portion of the grid. Most of the showing areas are in the periphery areas of the geochemical anomalies, leading to the speculation that the main mineralized bodies have yet to be discovered. The Tom Cat, Bluey, Bloo, Bunker Hill, and Portland showing areas are examples of showings being located near the centers of interpreted anomalies.

Geophysics:

Historical geophysical surveys in the area are similar in nature to historical geochemical surveys, the surveys completed over small local grids over showing areas. This work is documented as mainly magnetometer and electromagnetic surveys, however, some induced polarization surveys are reported, mainly centered on showing areas to the north of the property. Although reviewed, the historical surveys could not be used for detailed assessment of the property.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AR
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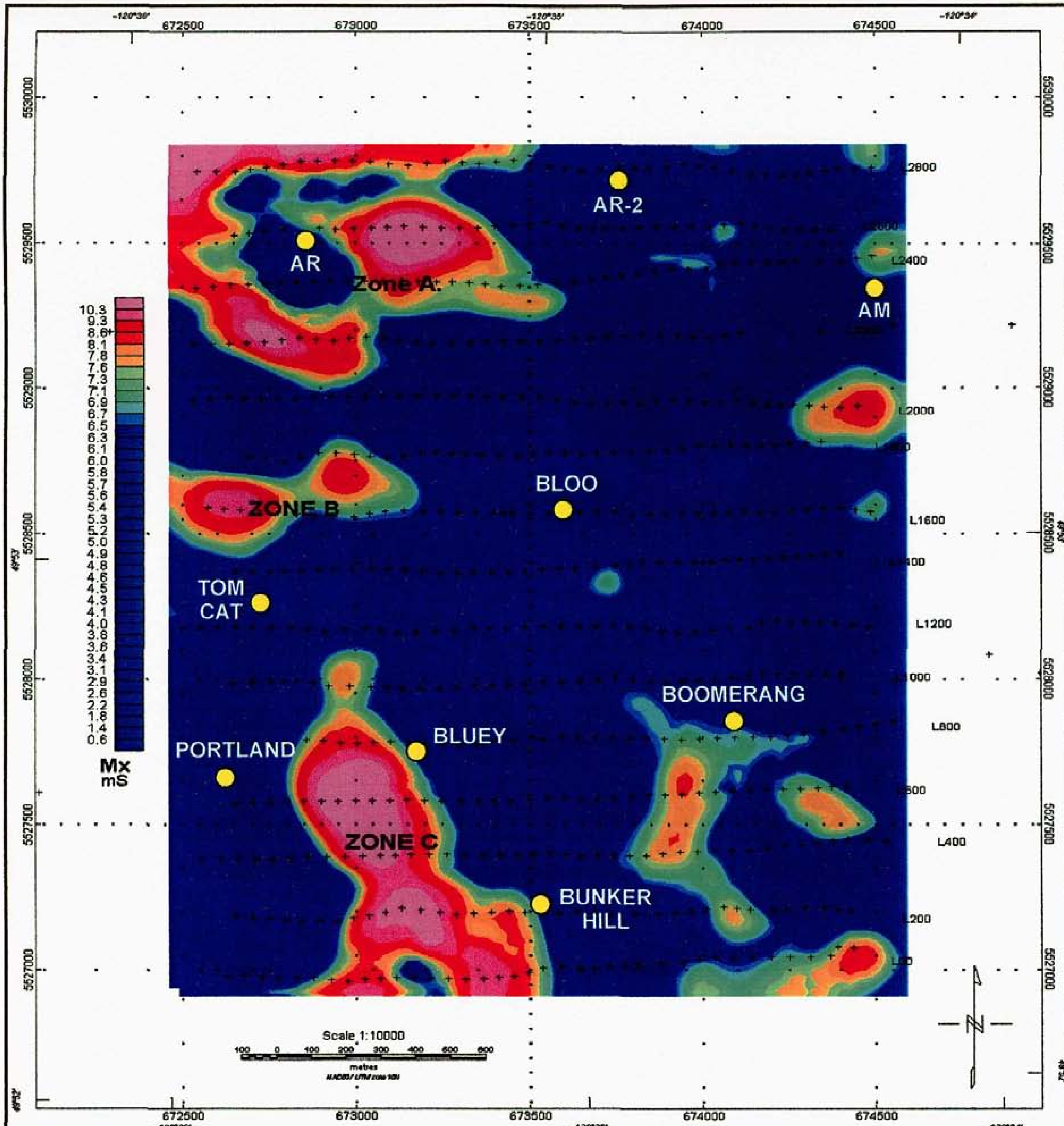
AM??
TOM CAT
BLOO??
BLUEY
BOOMERANG??
PORTLAND
BUNKER HILL
Classification
0 - 25 ppm Negative
25 - 50 ppm Poss Anomalies
50 - 100 ppm Prob. Anomalies
>100 ppm Def. Anomalies
Mineral Showings
KILOMETRES
0 1 2 3 4 5
BOLD VENTURES INC.
KENTUCKY LAKE PROPERTY
SIMILKAMEEN MINING DIVISION, BRITISH COLUMBIA
COPPER DISTRIBUTION IN SOIL
DRAWN BY: JOHN R. KERR
DATE: OCTOBER, 2006
SCALE: AS SHOWN
FIGURE NO. 5

In 2006, SJ Geophysics completed 28 km of 3D IP survey over the mineral showing areas covering the Casper 1 and 5 mineral claims.. The sensitivity of the 2005 survey gives depth credibility of readings to 300 meters. This is 1.5 – 2 times deeper than any previous survey completed in the area, and provides drill chargeability targets associated with each zone to these depths. The survey allows for topographic corrections, which provides a much more realistic plot of chargeability values on topography. In addition, "pantleg" effects at depth on these "corrected" sections have been eliminated.

Interpretation of the results of the recent IP data has provided some very good correlation of mineral showing areas to chargeability highs. In summary, the mineral showings appear to correlate well to the periphery portion of the stronger chargeability anomalies. The 2006 survey indicates the following:

1) Three strong chargeability anomalies are all located along the western portion of the grid area, aligned in north/south direction. The anomalies are shallow to deep, the middle anomaly is shallow (50 – 150 meters), the northern anomaly is deep (300 meters) and the southern anomaly is 150 – 200 meters deep.
2) One moderate strength chargeability anomaly is located in the southeastern area of the grid.
3) The Tom Cat, Bluey, Bunker Hill, Portland, AR and Boomerang showing areas are all located on the periphery area of moderate to strong chargeability anomalies.
4) The largest and strongest chargeability anomaly is a 1 kilometer diameter donut shaped anomaly located in the northwest corner of the grid area. This anomaly is quite deep and is strongest at the 300 meter depth. The AR showing is situated within the low chargeability center of this anomaly.
5) The strongest chargeability is characteristically areas of highest sulphide content, however does not necessarily relate to copper mineralized showing areas or soil geochemistry. The stronger chargeability may be due to high sulphide content in the form of pyrite. The copper bearing portions of these anomalies may be along the edges or borders of these anomalies. It is in this periphery area of the stronger chargeability anomalies that most exploratory diamond drilling should be completed.
6) A moderate chargeability anomaly is appearing in the eastern boundary of the grid and encompasses the reported location of the AM showing. This may be of significance or it may be due to a topographic effect.
7) There is a relationship of the chargeability anomalies to the contact of the Nicola Group and intrusive rocks.
8) Resistivity plots delineate the main Kentucky Lake/Summers Creek fault zone.
9) Other structures appear to be weakly defined by chargeability and resistivity interpretation.
10) Other targets were identified from the surveys that are not been discussed in this report.



LEGEND

● Mineral Showings

NOTE: Geophysical Survey by S.J. Geophysical Ltd. 2006

BOLD VENTURES INC.	
KENTUCKY LAKE PROPERTY SIMILKAMEEN MINING DIVISION, BRITISH COLUMBIA **CHARGEABILITY ANOMALIES**	
DRAWN BY: JOHN R. KERR	DATE: OCTOBER, 2006
SCALE: AS SHOWN	FIGURE NO. 6

DRILLING

There is recorded reference of historical diamond drilling having been completed on the Tom Cat and Boomerang mineral showings, however results and data from these programs are not well documented. Results of these programs are summarized where reported from early literature, however cannot be substantiated. It is believed that 15 - 16 drill holes have been drilled on the property. The nature and size of cores obtained from these programs are not available.

Several reports of the 1970s and 1980s refer to diamond drill programs on projects to the north and south of the property, and it is believed that some of these drill holes may have been located on the existing claims.

SAMPLE QUALITY

Sampling Method and Approach: As there are no records of previous sampling programs and historical sampling, the results are not being used in this evaluation. Details of the sampling methods and approach of historical programs are not discussed.

The 2006 program consisted of soil sampling and limited rock-chip sampling. Soil samples were collected at 50 meter stations along all grid lines and packed in brown kraft envelopes for shipment to the laboratory. Samples were taken from the "B" horizon of soil where possible and identified. Swampy and high organic areas were avoided.

The rock chip samples were collected in plastic sample bags. Appendix B defines the location, nature and results of these samples

Sample Preparation, Analysis and Security:

Sample handling methods, preparation and analysis are briefly discussed as follows:

The soil samples were shipped to Acme Analytical Laboratories Ltd. in Vancouver, British Columbia. All soils were sieved to -80 mesh and then were analyzed for 36 elements by MS ICP methods. Results were reported to the company and the author and are documented on original laboratory sheets in Appendix D.

The rock chip samples were carried by the author directly to Acme Analytical Laboratories in Vancouver. All samples were pulverized and then were analyzed for 36 elements by MS ICP methods. Copper values reported in excess of 10,000ppm were assayed for copper. Results were reported directly to the author.

Data Verification:

Except for in-house standard laboratory testing, there has been no attempt to verify any of the geochemical results presented in this report. The author believes there is no necessity to have this completed at this time.

METALLURGICAL TESTING

There is no documented history of metallurgical testing on the property.

MINERAL RESOURCE ESTIMATES

There are no documented reports of mineral resource estimates ever being completed on this property. A mineral resource has not been confirmed by sampling or drill testing.

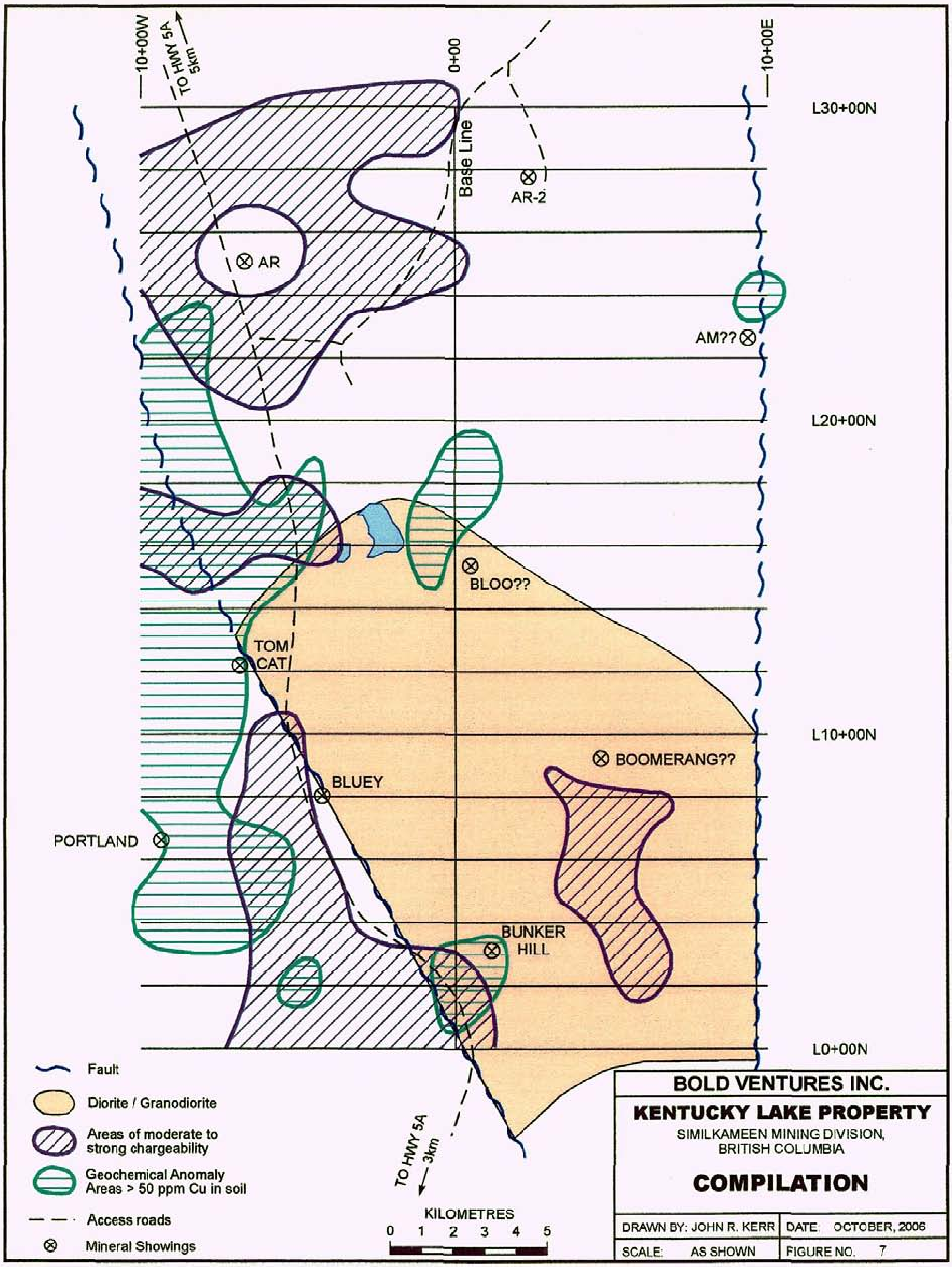
INTERPRETATION and CONCLUSIONS

A mineral resource has not been discovered on the property at this time. For this reason, the property is considered an early stage exploration project, with excellent potential of discovering resource.

Since most grass-roots exploration completed on the property was done in the 1960s, 1970s and 1980s, there is sufficient justification to incorporate updated and sophisticated methods into ongoing work programs to assist in locating new targets for potential resource. The 2006 3D Induced Polarization survey has provided excellent targets for exploration, and additional drilling is being recommended to explore the potential of these target areas. Analysis of all samples is to include copper and gold, as well as periodic testing by ICP methods for other metals.

Discussions and conclusions regarding the reliability and quality of all work programs have been thoroughly discussed in previous sections of this report and need not be discussed again.

In summary, the Kentucky Lake property is considered a property of merit, and is worthy of a significant initial phase of exploration drilling.



10+00W
TO HWY 5A 5km
0+00
10+00E
L30+00N
Base Line
AR-2
AR
AM??
L20+00N
BLOO??
TOM CAT
L10+00N
BOOMERANG??
BLUEY
PORTLAND
BUNKER HILL
L0+00N
TO HWY 5A 3km
Fault
Diorite / Granodiorite
Areas of moderate to strong chargeability
Geochemical Anomaly Areas > 50 ppm Cu in soil
Access roads
Mineral Showings
KILOMETRES
0 1 2 3 4 5
BOLD VENTURES INC.
KENTUCKY LAKE PROPERTY
SIMILKAMEEN MINING DIVISION, BRITISH COLUMBIA
COMPILATION
DRAWN BY: JOHN R. KERR
DATE: OCTOBER, 2006
SCALE: AS SHOWN
FIGURE NO. 7

RECOMMENDATIONS

It is recommended that initial exploration work be oriented at diamond drilling the geochemical and chargeability targets from the recently completed IP survey as they relate to mineral showings. A two-phase exploration program is therefore recommended. **Phase I** incorporates a total of five diamond drill (NQ – 5.2cm diameter) holes on the property, two holes to test the strong IP anomaly and geochemical anomaly as it relates to the Tom Cat showing (250 meters each), two holes to test the large and strong chargeability anomaly in the southwest portion of the grid as it relates to the Bunker Hill and Bluey showings (275 meters each) and one hole to test the northern chargeability anomaly as it relates to the AR showing (300 meters). In total, 1250 meters of drilling is allowed for in **Phase I.**

Sufficient access roads exist into all areas contemplated for drilling, therefore building of roads to drill sites would be minimal. A small allowance is being made in **Phase I** for site preparation to suit permit requirements.

Prior to drilling, further detailed grid work is being recommended in **Phase I** to refine the location of drill holes. In the area of mineral showings, detailed grid line spacing at 100 meter intervals are to be established, with soil samples collected at 50 meter intervals. All samples are to be analyzed by MS-ICP methods for 36 elements. In addition to soil sampling, the grid areas should be geologically mapped. From this work, the collar, bearing and angle of each hole will be identified.

The Bloo and Boomerang showings were not identified or located in the early phase grid work. **Phase I** should include a program to establish detailed grids over the approximate areas of these showings completing geochemistry and geological mapping to identify future targets for drilling. Other areas of the claims are to be prospected and geologically mapped.

Phase II incorporates continued exploration drilling by reverse circulation drilling and/or diamond drilling methods, to test priority targets delineated drilling and continued grid work of the Phase I program. Additional expanded IP surveys would also be recommended in other areas of the property.

Submitted by:

John R. Kerr, P. Eng.
January 15, 2007

Appendix A – Cost Statement, 2006 Field Program

APPENDIX A

Costs and Details of Work Performed on the Kentucky Lake property during the 2006 Exploration Program

Wages:		
C. Dyakowski, P. Geo, Project Manager	6 days @ 500/day	$3000.00
J.J. McDougall & Associates 2 days @ 500/day		1000.00
Mike Schmidt, Field Coordinator	27 days @ $325/day	8775.00
K. Forsberg, Linecutter	22 days@ 250/day	5500.00
B. Squinas, Linecutter, soil sampler	12.5 days@ 225/day	2856.64
N. Retasket, Linecutter, soil sampler	9 days@ 225/day	2025.00
T. Dyakowski, Soil sampler	22 days @ $150/day	3300.00
M. Cormack, Soil Sampler22 days @ $150/day		3300.00
Transportation:		
Truck Rental 24 days @ $65		1560.00
Fuel		1952.00
Tolls		90.00
Meals and Accommodation:		
122 days @ 75/man day		9150.00
Contractors:		
SJV Consultants Ltd		
IP survey		
34 km @ 1600/km		48,800.00
Mob and demob		3000.00
2 trim positional maps		880.00
Rentals:		
ATV rental 23 days @ 50/day		1150.00
Assays:		
Acme Analytical Labs		$3930.24
WCB		872.75
Report Preparation and Property Visits:		
John Kerr, P. Eng		8243.45
Drafting		1332.50
TOTAL		**$110,717.58**

Appendix B - References

REFERENCES

2006, R. Sheldrake, Geophysicist – 3D Induced Polarization Survey, Kentucky Lake Property, Merritt Area, B.C., October, 2006

1988, Ivor M. Watson, P. Eng. – Geochemical Report on the Bloo, Climax and Thor Claims Nicola and Similkameen Mining Divisions, Aspen Grove Area British Columbia

1979, V. A. Preto, P. Eng. - Bulletin 69, Geology of the Nicola Group between Merritt and Princeton, British Columbia Ministry of Energy, Mines and Petroleum Resources

1947, H.M.A. Rice, PhD - Memoir 243, Geological Survey of Canada Geology of the Princeton Area

1969 – 1988, Various Assessment Reports from Ministry of Energy, Mines and Petroleum Resources files (too numerous to list)

1965 - 1984, Annual Reports and Mineral Inventory Files, Ministry of Energy, Mines and Petroleum Resources.

Appendix C – 3D Induced Polarisation Survey, Geophysical Report
Ronald F. Sheldrake, SJ Geophysics Ltd.

3D INDUCED POLARIZATION SURVEY

Geophysical Report

for

MAX INVESTMENTS

on behalf of

BOLD VENTURES INC.

Suite 430-580 Hornby Street

Vancouver, B.C., V6C 3B6

on the

KENTUCKY LAKE PROJECT

Merritt Area, B.C.

Similkameen Mining Division

Latitude *49⁰ 53′ N*, Longitude *120⁰ 35′ W*

(673,500E, 5,528,500N, Nad 83 Zone 10)

N.T.S 092H15E

Claims: Casper 1, 5, 6, 7 & 8

Survey Conducted by

SJ Geophysics Ltd.

August 2006

Report by

Ronald F. Sheldrake,

S.J.V. Consultants Ltd., Delta B.C.

September 25, 2006

Table of Contents

Illustrations

List of Plates (Page size versions of the maps are located in Appendix 4 (Chargeability) and Appendix 5 (Resistivity). Digital PDF versions of the maps are included on a CD that comes with this report. Also include on the CD is MeshTools3d.exe (the 3D viewing program) and the chargeability and resistivity model files that were created from the survey data.)

PLATE	Depth Slice Maps	Scale at 100%
Plate R-8	Interpreted Resistivity – 300m below topography	1:5,000
Plate C-8	Interpreted Chargeability – 300m below topography	1:5,000

List of Files on the CD

FILE NAME	FILE DESCRIPTION
MeshTools3d.exe	3D viewing program for IP Resistivity and Chargeability models

FILE NAME	FILE DESCRIPTION
Kentucky_Lake_Model.chg	Chargeability Model called for in MeshTools3d.exe
Kentucky_Lake_Model.res	Resistivity Model called for in MeshTools3d.exe
Kentucky_Lake_Model.con	Conductivity Model called for in MeshTools3d.exe
KL_UTM_Meshfile.txt	Meshfile called for in MeshTools3d.exe

1. Summary

Between August 10 and August 27, 2006 a 3D Induced Polarization survey of 28 km was undertaken by SJV Geophysics Ltd. over the Kentucky Lake Property at the direction of Max Investments. The property is located in the Similkameen Mining Division near Merrit, B.C.

B.C. Min-file data indicate the property has at least 7 showings of copper mineralization in breccias within Upper Triassic Nicola Group rocks. The purpose of the 3D IP survey was to test for disseminated copper (sulphide) mineralization.

The results of the survey indicated three areas of increased IP chargeability responses that could arise from sulphide copper mineralization. Drill holes have been selected to test these targets.

A more comprehensive report will be prepared by John Kerr, P.Eng., who will be providing recommendations for ongoing work programs, therefore this report does not detail previous exploration work, regional and local geology, history, and costs associated with the exploration of the property.

2. Disclaimer

The author has prepared this report based upon information believed to be accurate, but is not guaranteed. This report may contain sanguine statements. For example, a statement such as, "*the IP responses suggest the presence of sulphide mineralization*," is accepted as incomplete. It is taken for granted that the reader accepts this class of statement as an inherent element in an interpretation report, and therefore does not require a cautionary statement at every instance.

3. Survey Grid

The claims are situated approximately about 30 km southeast of Merrit, B.C. The survey area is easily accessible from roads in the area and is only moderately hilly. Elevations range from about 1035 meters to 1265 meters. There are cliffs on the eastern side of the grid. Evidence of previous exploration activity was noted here and there by the field crew.

The IP grid measured about 2800 x 2000 m and consisted of 15 east-west oriented lines.

The survey grid-lines had been previously prepared and were satisfactory except for a few labeling errors, which were corrected by the geophysical crew.

The illustration below shows the station locations and mineral showings on topography.

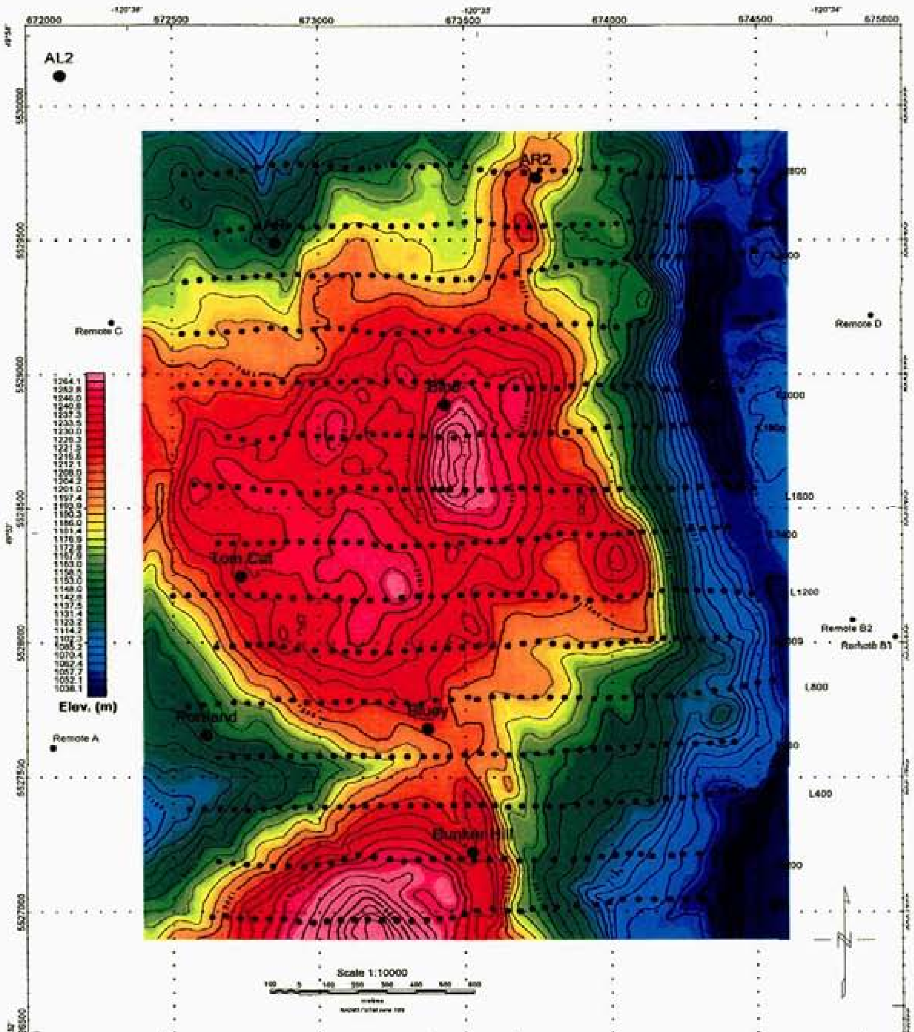


Illustration 1: Survey Stations plotted on topographic image

Note that all data collected on this survey was NAD 83,UTM Zone 10.

4. Field Work and Procedure

The SJ Geophysics Ltd. crew consisted of nine SJ Geophysics employees: Graham Fulton, Ryan Tapp, Sol Meyer, Masresha Akalu, Matthew Harrison, Michael Pettersson, Alex Visser, Michael Seguin, and Franzi Unterberger. Alex Visser was project leader for the crew and Michael Pettersson was geophysical technician. The majority of the crew mobilized from Vancouver via vehicle on August 10. The crew demobilized to Vancouver via vehicle on August 27, arriving very late at night.

The collection of survey measurements began on August 11. Production rates were impeded somewhat due to the proximity of holiday campers as well as broken survey wires caused by animals. Warning signs were erected to advise campers to stay clear of the survey area, and extra care was taken not to expose wires or electrodes where they might endanger citizens.

4.1 Survey Parameters and Instrumentation

A 3D-IP configuration array was used with 12 dipoles of 100 m, 200m and 300 m separations. The IP data was collected using SJ Geophysics' Full Waveform receiver which provides for acquisition of the full IP signal/waveform.

The current was injected with a 2 seconds on, 2 seconds off duty cycle into the ground via stainless steel electrodes. A GDD 3.6kW voltage-regulated transmitter was used for the entire program. For equipment specifications see Appendix 2.

In a 3D IP configuration, the current lines were located on either side of the receiver line, and subsequent lines were surveyed with a single current line overlap. For this survey four IP "remotes" were used (see Illustration1) Remotes "A" and "C" were located on the western extremity of the grid. Remotes "B1" and "B2" were located off the eastern side. To achieve better signals the eastern remotes were used, whenever practicable,when surveying the western side of the lines. Because of the flexibility of the 3D IP system gradient IP measurements can be (and were) taken using the appropriate western and eastern remotes as the current injection locations. This provides for even greater depth penetration and enhanced measurement accuracy.

Remote B1 was used for a short while but it was too close to a campground and was moved for safety reasons to location B2. A remote "D" was laid out but was removed after complaints from campers and was not used.

5. Geophysical Techniques

5.1 IP Method

The induced polarization (IP) technique is one of the principal tools used in the exploration for metallic minerals and resistive and conductive zones that copper sulphide mineralization is associated with. IP surveys are comprised of two different measurements; chargeability and resistivity. The purpose of IP chargeability measurements is to map the distribution of disseminated metallic mineralization in the subsurface rocks. Also, from the IP measurements, the apparent resistivity of the underlying rock below and around the electrodes is calculated from the input current (I) and the measured primary voltage (Vp). The resistivity data (units of ohm-meters) are used to distinguish conductive and resistive rocks. With regard to precision, IP/Resistivity measurements are generally considered to be repeatable within five percent depending on the range of readings. However, variation will exceed that if field conditions change due to changes in water content of the ground or variable electrode contact.

The time domain IP technique energizes the ground with an alternating square wave series of pulses via a pair of current electrodes that make electrical contact with the ground. After the transmitter (Tx) pulse has been transmitted into the ground via the current electrodes, the IP effect is measured at the receiver electrodes as a time diminishing voltage. The IP effect is a measure of the amount of electrically polarizable material in the subsurface rock in the area around, and below, the measuring electrodes. Under ideal circumstances, IP responses (units of chargeability = milliseconds) are proportional to the amount of disseminated metallic sulfides in the subsurface rocks. Unfortunately, there are other rock materials that give rise to IP effects, including some graphitic rocks, clays and metamorphic rocks (serpentinite, for example) so, that from a geological point of view, IP responses are almost never uniquely interpretable. Because of the non-uniqueness of geophysical measurements it is always prudent to incorporate other data sets to assist in interpretation.

5.2 3DIP Method

Traditionally Induced Polarization (IP) measurements have been made with the current electrodes (input electrodes) and the measuring electrodes positioned on the same line (called 2D IP). This technique suffers from two deficiencies; 1) All IP measurements "look" sideways so the interpreter must speculate whether the IP response came from below the survey line or off to either side of it, and 2) there were no IP measures made with current flow ***between*** the lines, and can serve to misrepresent the distribution of IP and chargeability responses in the ground.

Three dimensional (3D IP) surveys are designed to also take advantage of the 3D "inversion" techniques, which are mathematical calculations on the IP data in a 3 dimensional matrix.

Unlike conventional 2D IP surveys, in 3D IP surveys the electrode arrays are no longer restricted to in-line geometry allowing a more flexible and more definitive control of current flow. Typically in 3D IP surveys, the current electrodes and receiver electrodes are located on *adjacent* lines so that there is always current flow between the lines, and along the lines, both in a forward and reverse direction. Under these conditions, multiple current sources are applied to a single receiver potential dipole and data interpretation and noise cancellation improves accordingly. However, there is some trade off. An interpretive decision has to be made as to the viability of the readings as the primary voltage (Vp) diminishes when the current electrodes are adjacent, or nearly adjacent, to the potential dipoles. Very low amplitude Vp values are evaluated by inspection and, if necessary, they are deleted from the dataset. However, there is sufficient redundancy of data that this has little effect.

For this survey, a full wave form receiver designed by SJ Geophysics Ltd. was used. The current electrodes were located on the two adjacent lines (called "current lines") on either side of the measured "potential" line. The IP receiver is located at a station on the "potential" line and the current electrodes are moved station by station down the "current lines". The ground material (rock and overburden) is energized, first from one current line, and then from the other, in a back and forth routine, allowing for more efficient data collection.

6. DATA PRESENTATION

6.1 3D Representation of IP Data

The principal presentation in 3D IP is a ***volume*** or "matrix-model" of IP responses that represent the properly located distribution of interpreted IP chargeability and resistivity values. For example, see below Illustration 2.

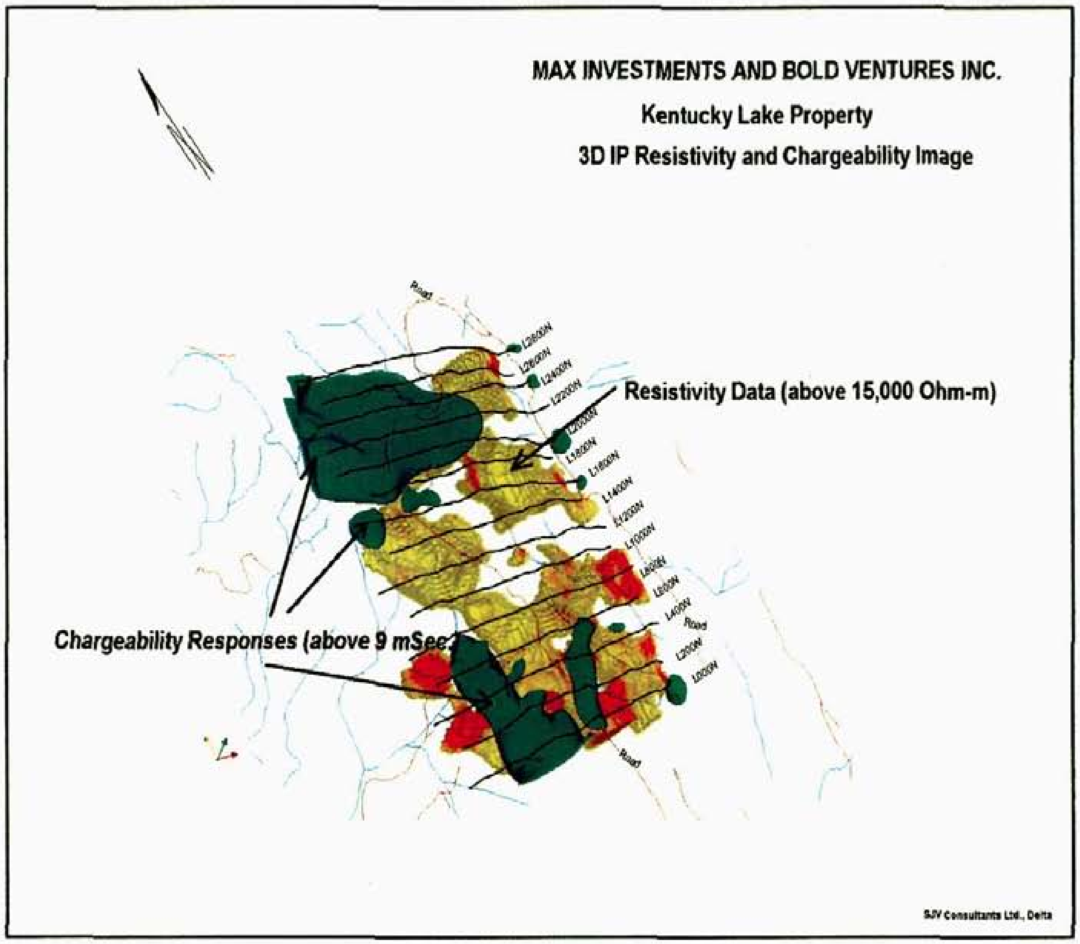


Illustration 2: 3D IP Chargeability and Resistivity Image (Paraview)

The image shows the roads, drainage, lakes, IP survey traverses as well as the IP resistivity and chargeability "threshold" responses.

(Note: "Threshold Response" means that what is displayed is a limited range of data values. The full data range of the IP chargeability responses may be from 1 to 19 milliseconds. The "threshold" may be set to display limited chargeability values, say, between 10 to 19 milliseconds.)

The 3D IP model–matrix data is delivered with MeshTools3D.exe a program that allows the user to "slice-dice and rotate" the volume for detailed inspection. Other free-ware programs are also available. Paraview, downloadable from the Internet, is more comprehensive but less easy to use. The MeshTools3d.exe program that is used for the inversion and display of the IP data originates from the University of BC GIF facility (www.eos.ubc.ca/research/ubcgif). See Appendix 3 for details on the use of MeshTools3D.exe.

REMARK: It should be stressed that the inversion of 3D IP data is subject to distortion with depth. The 3D images represent the responses in the their proper location, however, it should be recognized that even though the images display a constant cell size per unit depth(which may be considered as resolution) this is not the case. Both the measuring process and the inversion of IP data inherently reflect diminishing sensitivity with depth. In fact, the very deep responses in the images (typically basin like "bottoms") often have no geological reality and are an imaging artifact. Unfortunately, no convenient way has yet been developed to trim from below those data that are invalid.

6.2 2D Representation of IP Data

For 2D interpretation purposes images of the 3D matrix-model are produced as "levels" or "depth slices" so that the IP data can be related to other 2D data sets.

(Note: "3D levels" and "3D depth slices" mean different things. "Levels" are flat surfaces of the model at a fixed elevation and is what is displayed in the 3D modelling program, MeshTools3d.exe. A "depth-slice," on the other hand, refers to a curved surface of the model that is equidistant from the ground surface. The 2D maps produced in the appendices of this report are referred to as "depth slices" and the metric units are defined as "depths below surface.")

Adobe PDF files of all the resistivity and chargeability depth slices at 25 m, 50 m, 75 m, 100 m, 200 m, 250 m and 300 m are included in Appendix 4 and Appendix 5 and on the CD-ROM that is included with this report.

7. DISCUSSION OF THE KENTUCKY LAKE 3D IP SURVEY DATA

7.1 Chargeability Data

As noted earlier, the Kentucky Lake Property has a number of copper (Cu) mineral showings (BC Minfile data), however none of them are coincident with the areas of increased chargeability that were mapped by the present survey. The image below shows the Cu showings on the "stretched" version of the chargeability data.

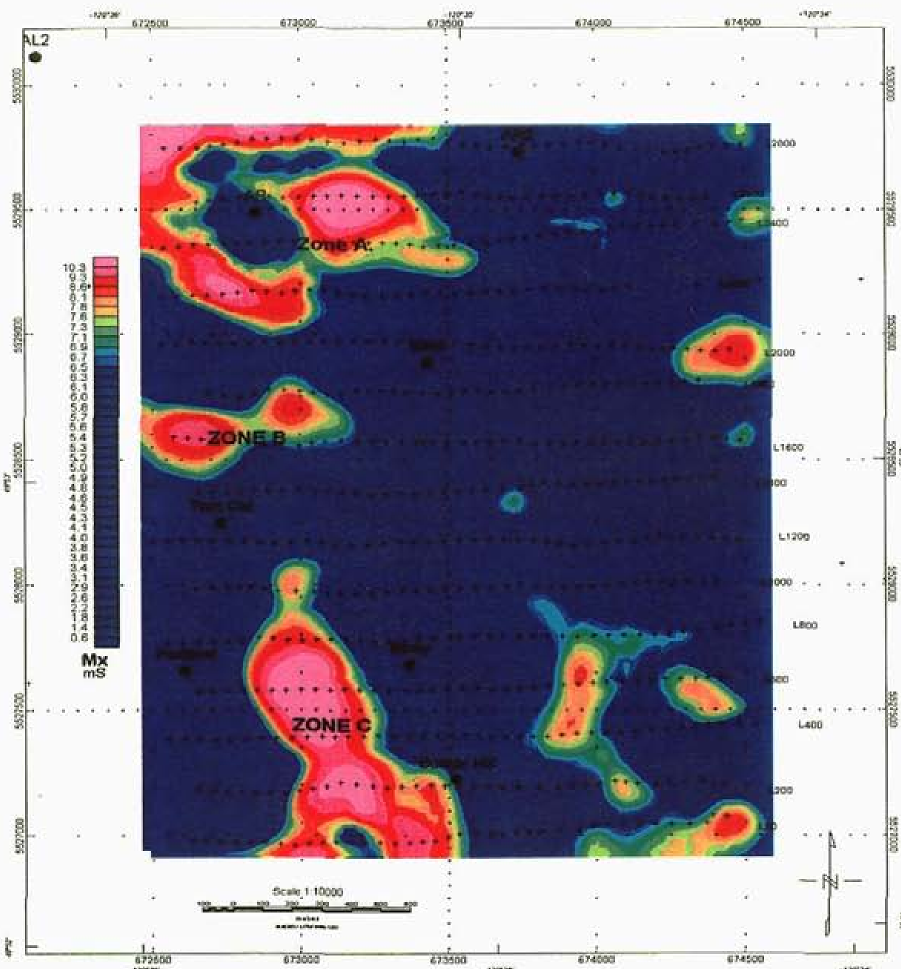


Illustration 3: Chargeability Depth Slice 100m Image showing mineralized zones

("Stretched" means that the colour range has been altered to enhance a certain range of values, in this case, of course, the higher chargeablity values.)

The three lettered zones, A, B, and C show areas of significantly elevated chargeability values. It can be speculated that the extant mineralization may be secondary to more substantial mineralization at depth as implied by the 3D IP data.

Zone A - This zone is centered on the AR showing that is described in the BC Minfile as "Two closely spaced trenches with exposed chalcopyrite and bornite in green volcanic breccia and laharic deposits." The IP response appears to encompass the AR showing.

Zone B – Is the smallest of the three geophysical responses, however because its proximity to the Tom Cat showing (0.32% Cu over 45.7m), it is included.

Zone C - Is the largest of the geophysical responses and is proximal to the Portland, Bluey, Bunker Hill and AR-1 showings, although none of them are coincident with the 3D IP response.

7.2 Resistivity Data

The resistivity data were not helpful in evaluating the chargeability IP targets mentioned above. However, the data do indicate some structural information, however their significance is indeterminate. Illustration 4 below displays a "stretched" resistivity image showing the interpreted lineaments.

The lineaments indicated on the map may reflect fault structures, the distribution of brecciation or, in some cases, laharic (flow) distribution. None of the features interpreted from the resistivity data seem related to the mapped mineral occurrences.

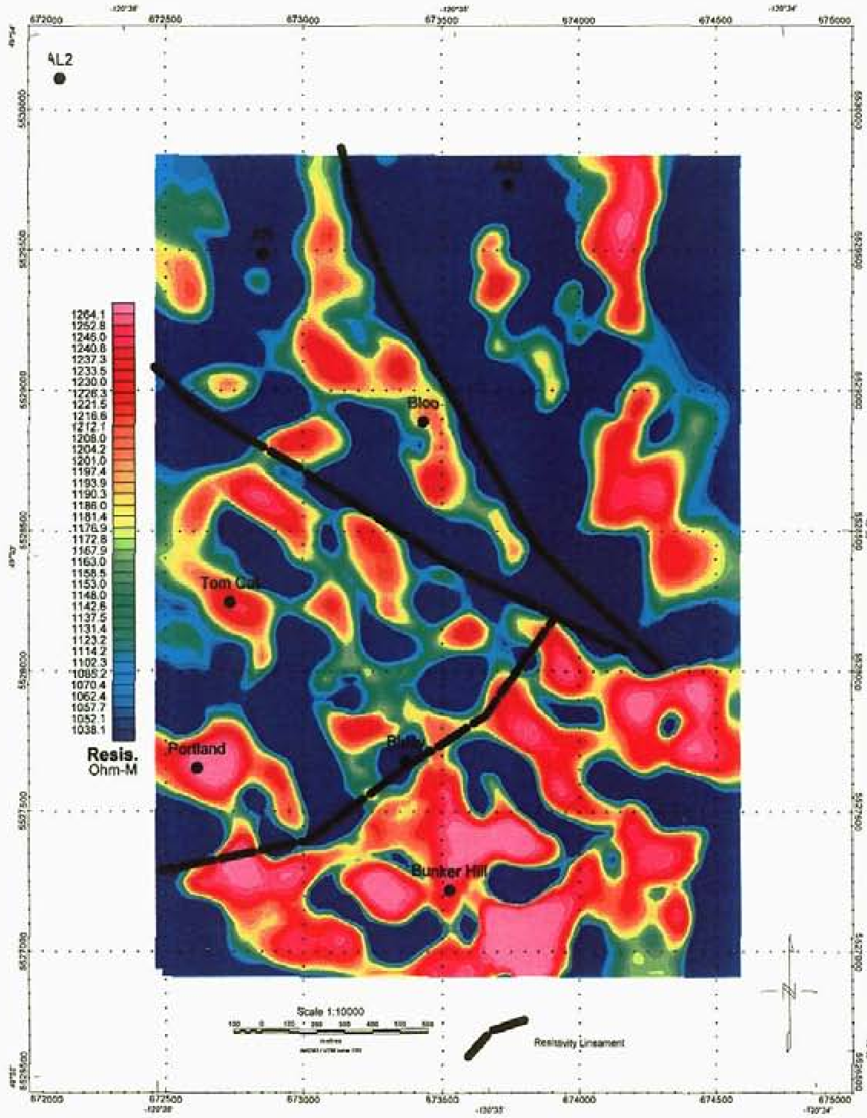


Illustration 4: Resistivity Depth Slice 50 m Image with Interpretation

7.3 Combined 3D Chargeability and Resistivity Images

3D IP data are best evaluated by dynamically viewing the images on a computer screen, since various parameters and thresholds can be adjusted to bring out more comprehensive detail and relationships. Only a limited number of static representation can be realistically included in any report. Two images are presented below using different observation views. They provide starting points for evaluation by the exploration geologist. Paraview, the program used to display this class of data, is a free program available on the Internet. Contact S.J.V. Consultants Ltd. if training is required on Paraview.

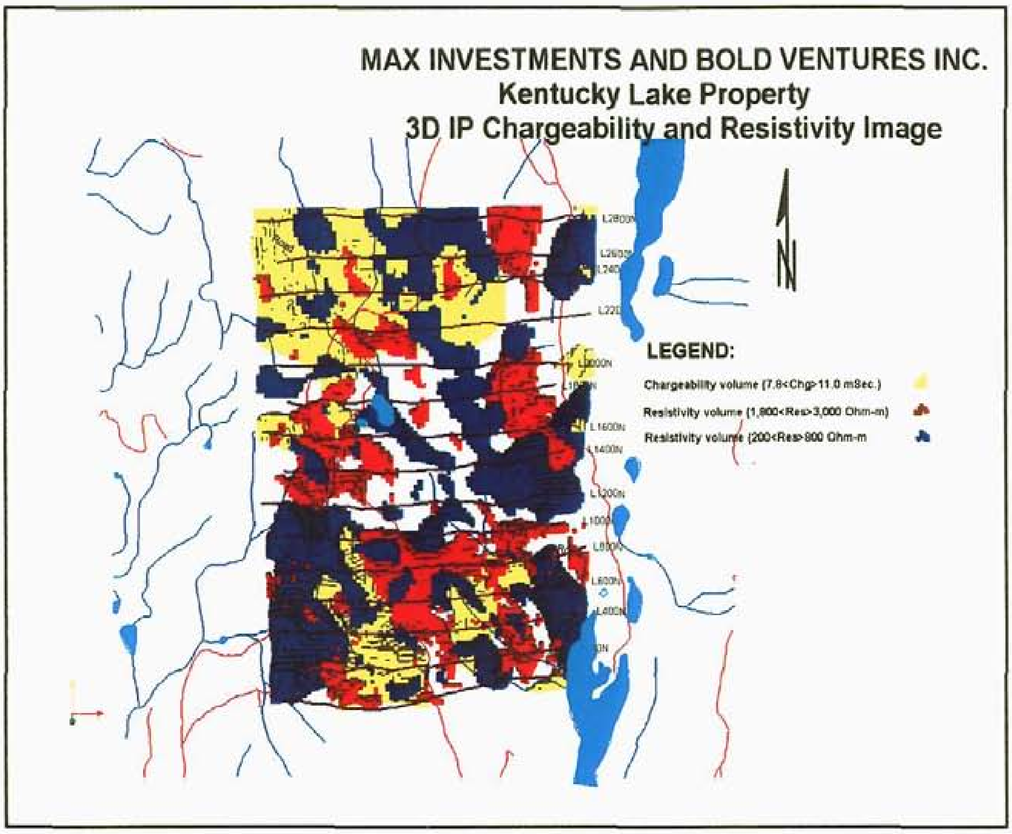


Illustration 5: 3D IP Chargeability and Resistivity Image with threshold values

Illustration 5 shows the complexity in the data that arises from this class of IP survey. However, note that there are several inferred lineaments that may be important in a structural evaluation.

Illustration 6 below was created using the same parameter and thresholds but it is upside down and rotated.

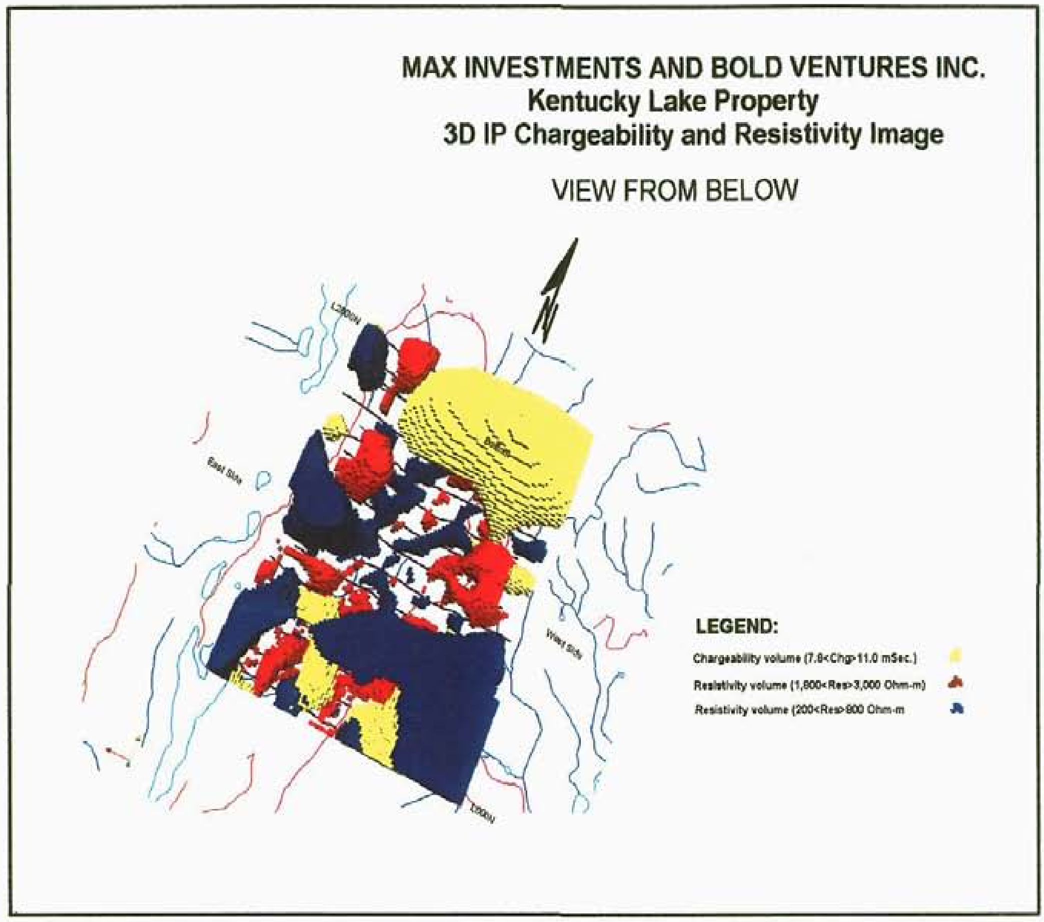


Illustration 6: 3D IP Chargeability and Resistivity Image (viewed from bottom)

It is important to note that the expansive blue (low resistivity) and yellow (high chargeability) areas that extend to the bottom of the model-matrix are not geological, but as previously mentioned, they are both processing and data collection artifacts.

8. Conclusions and Recommendations

In general, an interpreter is obliged to determine as much useful exploration information from the data sets as is possible, and yet avoid excessive extrapolations. It is recognized that interpretations are simplifications of the data into conceptual models, and are inherently subjective.. Note that the present geophysical interpretations are undertaken with very sparse geological control, so that they must be considered of a preliminary nature.

The 3D IP survey outlined 3 areas of increased IP chargeability, that may be related to metallic sulphide mineralization. The geophysical data, of course, provide only a bulk image of the characteristics of the underlying rocks, and the local geological picture may be very much more complex than the geophysical data suggest. Comparison of the geophysical results with the geology is always warranted before drilling targets are finally selected.

Respectfully submitted,

As per S.J.V. Consultants Ltd.

Ronald E. Sheldrake, B.Sc. (Geophysics)

Bibliography

Sol Meyer, ***"Logistical Report for Bold Ventures Inc., 3D Induced Polarization Survey on the Kentucky Lake Property",*** August 2006" (draft version)

"Ministry of of Energy, Mines and Petroleum Resources", MinfileInventory Reports: 092HNE089, 092HNE167, 092HNE258, 092HNE257, 092HNE117, 092HNE259, 092HNE088, and 092HNE086.

Appendix 1 – Statement of Qualifications, R. Sheldrake

I, **Ronald F. Sheldrake**, do certify that:

1) I received my B.Sc. in Geophysics from the University of British Columbia in 1974.

2) I have practised the profession of exploration geophysics for in excess of 30 years.

3) This report is written solely by Ronald F. Sheldrake, except where other credit is given.

4) I have no interest, either direct, indirect or contingent in either of Max Investments or Bold Ventures Inc.

I hereby authorize Max Investments and/or Bold Ventures Inc. to use this report for their corporate use.

September 25, 2006

Ronald F. Sheldrake
S. J. V. Consultants Ltd.

Appendix 2 – IP Receiver and Transmitter Equipment

SJ-24 Full Waveform Digital IP Receiver

Technical:	
Input impedance:	10 Mohm
Input overvoltage protection:	up to 1000V
External memory:	Unlimited readings
Number of dipoles:	4 to 16 +, expandable.
Synchronization:	Software signal post-processing user selectable
Common mode rejection:	More than 100 dB (for Rs =0)
Self potential (Sp):	Range:-5V to + 5V Resolution: 0.1 mV Proprietary intelligent stacking process rejecting strong non-linear SP drifts
Primary voltage:	Range: 1μV – 10V (24bit) Resolution: 1μV Accuracy: typ. <1.0%
Chargeability:	Resolution: 1μV/V Accuracy: typ. <1.0%
General (4 dipole unit):	
Dimensions:	18x16x9 cm
Weight:	1.1 Kg
Battery:	12V External
Operating temperature range:	-20°C to 40°C

GDD Tx II IP Transmitter

Input voltage:	120V / 60 Hz or 240V / 50Hz (optional)
Output power:	3.6 kW maximum.
Output voltage:	150 to 2200 Volts
Output current:	5 ma to 10Amperes
Time domain:	1,2,4,8 second on/off cycle.
Operating temp. range:	-40° to +65° C
Display:	Digital LCD read to 0.001A
Dimensions (h w d):	34 x 21 x 39 cm
Weight:	20kg.

APPENDIX 3 – MESHTOOLS3D.EXE VIEWING PROGRAM

This program is used to view 3D models originate from the University of BC Gif facility (www.eos.ubc.ca/research/ubcgif). The program is owned by the GIF Facility, and use of the program is restricted to non-commercial use to view data sets produced by UBC inversion programs. All other rights reserved.

Instructions:

1) It is easiest to have the all the four files that you need in the same directory, namely, **MeshTools3d.exe, 3dmesh.txt, dcinv3ds.con, ipinv3d.chg** (or equivalent names)

MeshTools3d.exe is the viewing program.

3dmesh.txt is the mesh file that the program will ask for (comes with the model).

dcinv3ds.con and **ipinv3ds.chg** (or similar names) are the conductivity and chargeability model-matrices that are to be viewed.

2) Start by double clicking on MeshTools3d.exe. Go to File>Open and on the first line browse to the file "3dmesh.txt", then on the 2nd line input the conductivity model you want (dcinv3ds.con). For conductivity and resistivity models (only) a more effective array of colours is needed. Click on the little "log" box (means logarithmic). Leave the 2nd model line blank. Click on "OK."

3) There will appear a question "that some cells are set to 1e-008, do you want to ignore these" click "Yes"

4) The model will load and you should see the first image. This shows conductivity. If you wish to view resistivity toggle the "sigma/rho" button in the middle of the toolbar, then go to "view" menu pull down to "flip colours". You should now see low resistivities in blue and highs in red (the scale bar goes from, say, 1-1e+05). Now go to "view" again and select "labels" and this will put the coordinates on the axes. These are the trimmed models which are already cut down to the extent of the data (there are no padding cells).

If you hold the right mouse button down (it is not a click) while the cursor is on the model and you move the mouse the whole thing spins and rotates in 3D; with a little practice you can be looking at any orientation you like.

Go back to :options" to experiment. Change the colour bar: Max/Min set Max=5000, Min=50, this makes the highs look redder and the lows look bluer and enhances the difference. Also try Max=2000, Min=20.

5) Use the WESNTB buttons to select a direction and then slice in and out with the arrow buttons just to the right.

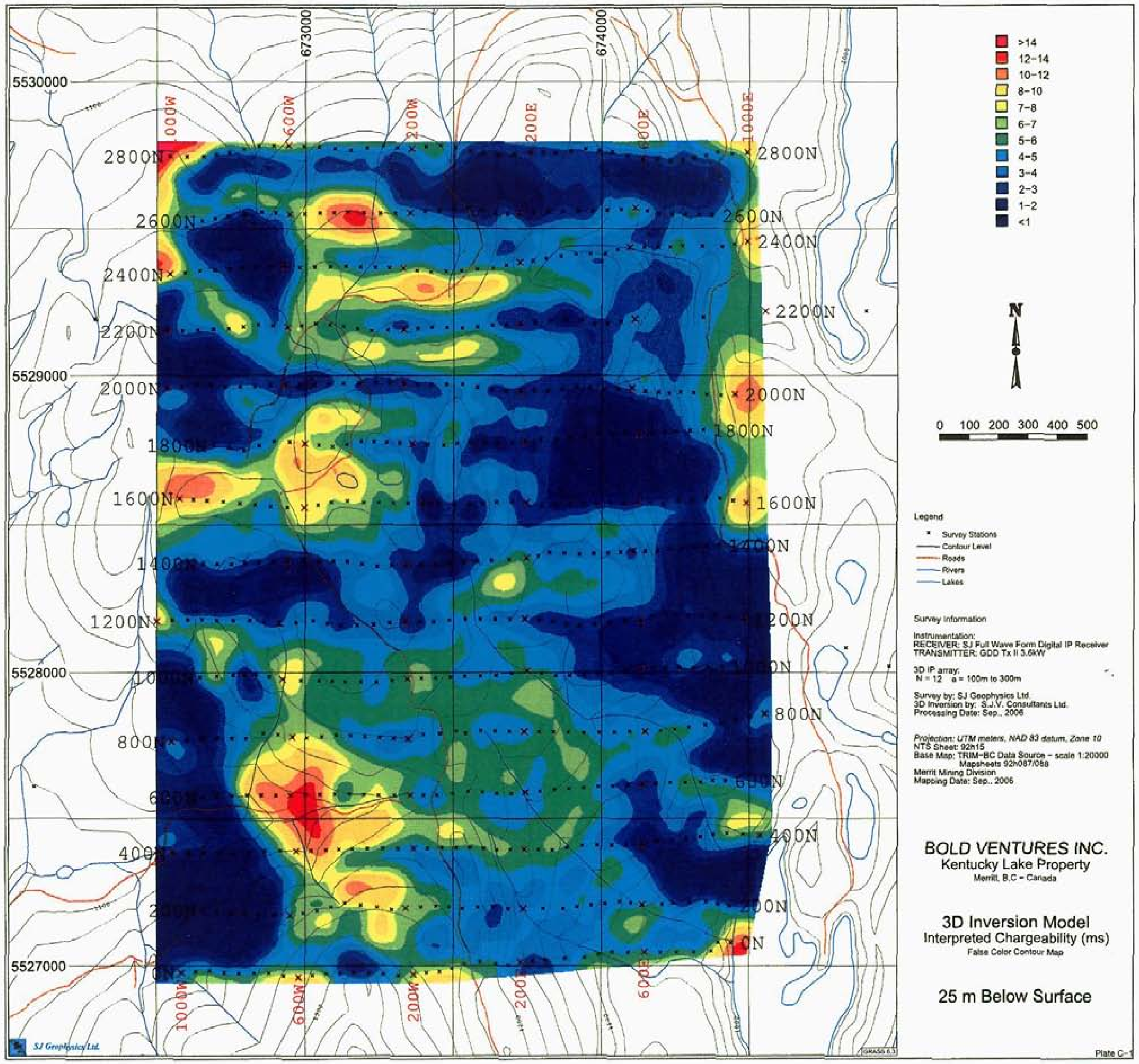
One very useful viewing technique is the "cut off" which displays a selected range of values and for resistivity it can show all the values above a certain limit and all values below a limit at the same time. "options"> "cut off"> min=2000 (you can leave max= alone) this will show all the values above 2000 and you can see the high resistivity bodies as volumes. To orient yourself in the block you can step in with the cut-planes (WESNTB) buttons from several sides to bracket (or center) the feature in the mesh coordinates.

6) Now minimize the model and start the program again. Load the mesh, and now load the chargeability model "ipinv3ds.chg", but do not click the "log" box, as the colour display won't be correct. There will appear a question "that some cells are set to 1e-008, do you want to ignore these" click "Yes"

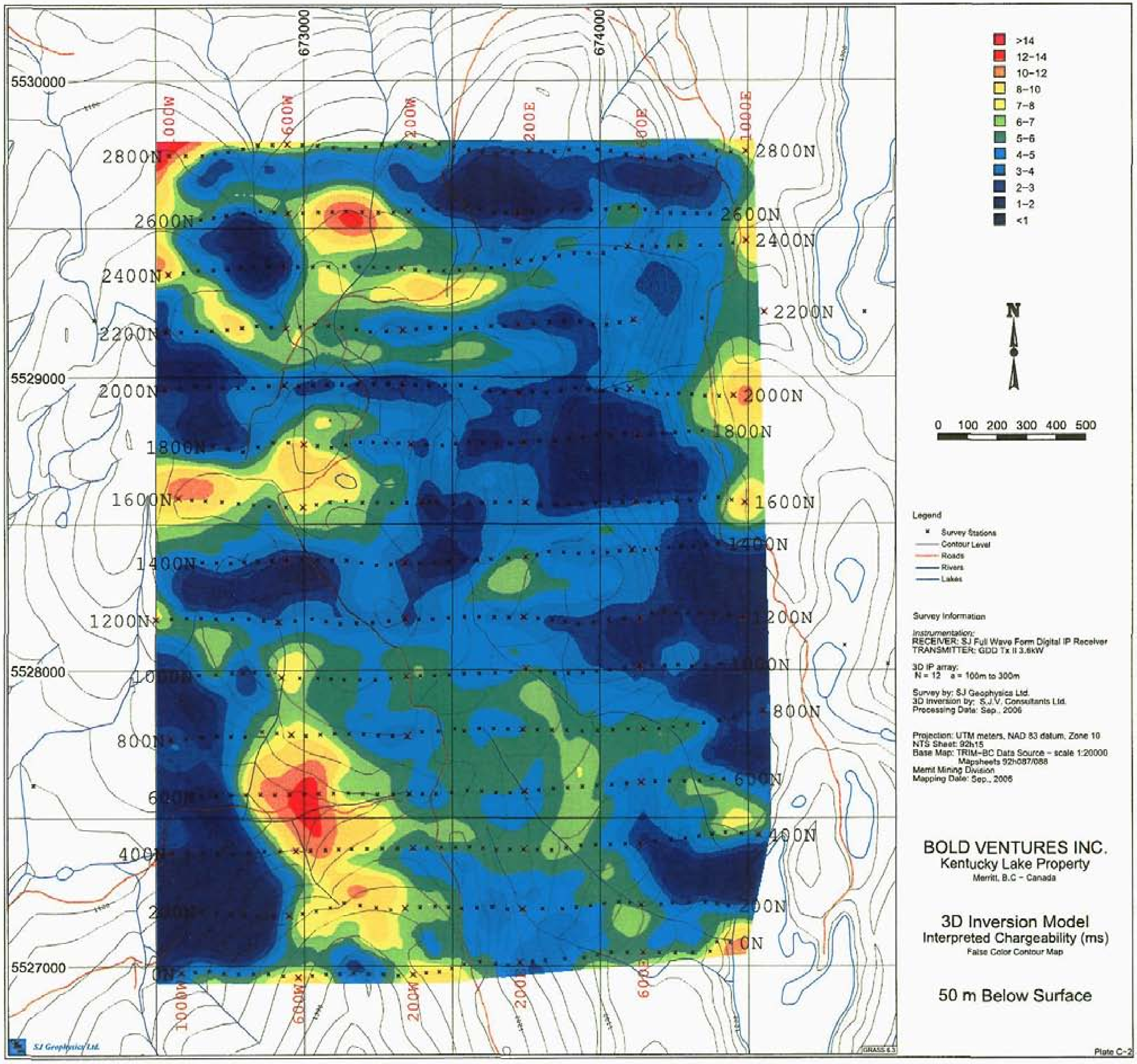
7) For the chargeability model-matrix you do not need to change sigma/rho or flip colours you can proceed directly with putting the labels and to set to color bar (0-30).

8) Compare with the resistivity (you can have both models side by side).

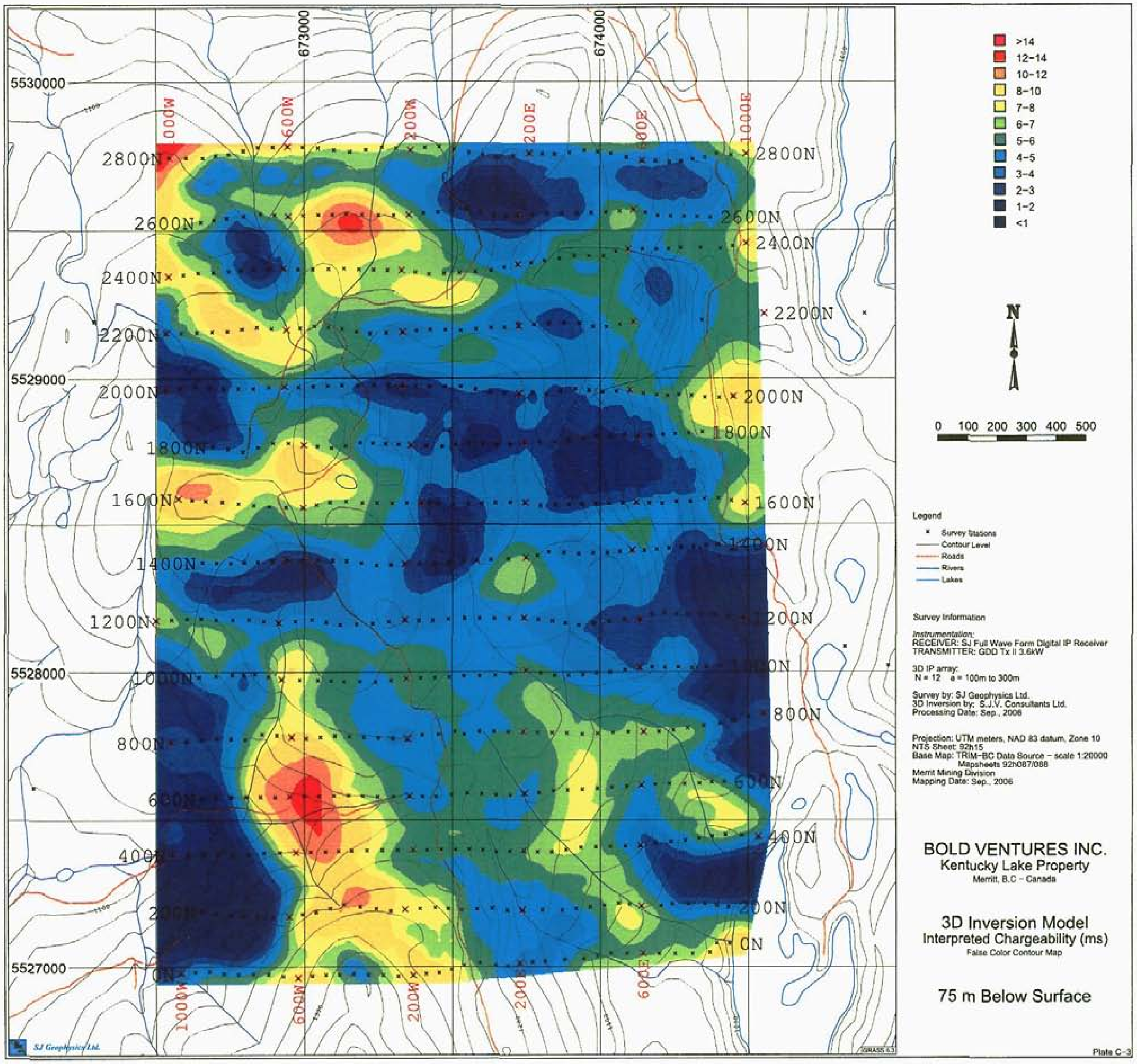
Appendix 4 – Inverted Depth Slice Maps- Chargeability



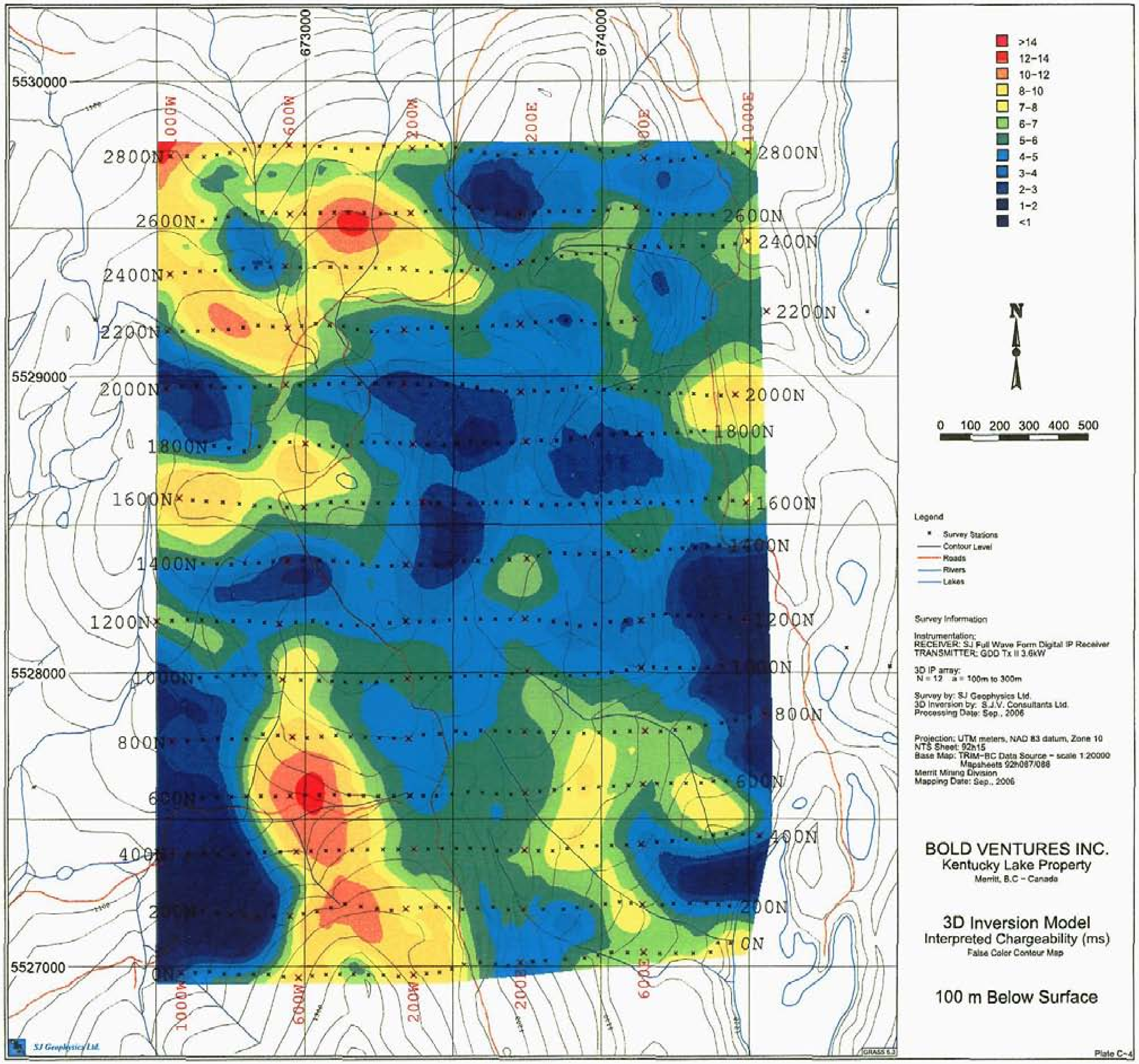
>14
12-14
10-12
8-10
7-8
6-7
5-6
4-5
3-4
2-3
1-2
<1
N
0 100 200 300 400 500
Legend
Survey Stations
Contour Level
Roads
Rivers
Lakes
Survey Information
Instrumentation:
RECEIVER: SJ Full Wave Form Digital IP Receiver
TRANSMITTER: GDD Tx II 3.6kW
3D IP array:
N = 12 a = 100m to 300m
Survey by: SJ Geophysics Ltd.
3D Inversion by: S.J.V. Consultants Ltd.
Processing Date: Sep., 2006
Projection: UTM meters, NAD 83 datum, Zone 10
NTS Sheet: 92h15
Base Map: TRIM-BC Data Source - scale 1:20000
Mapsheets 92h087/088
Merritt Mining Division
Mapping Date: Sep., 2006
BOLD VENTURES INC.
Kentucky Lake Property
Merritt, B.C - Canada
3D Inversion Model
Interpreted Chargeability (ms)
False Color Contour Map
25 m Below Surface
Plate C-1
SJ Geophysics Ltd.
5530000
5529000
5528000
5527000
673000
674000
2800N
2600N
2400N
2200N
2000N
1800N
1600N
1400N
1200N
800N
400N
200N
0N
1000W
600W
200W
200E
600E
1000E

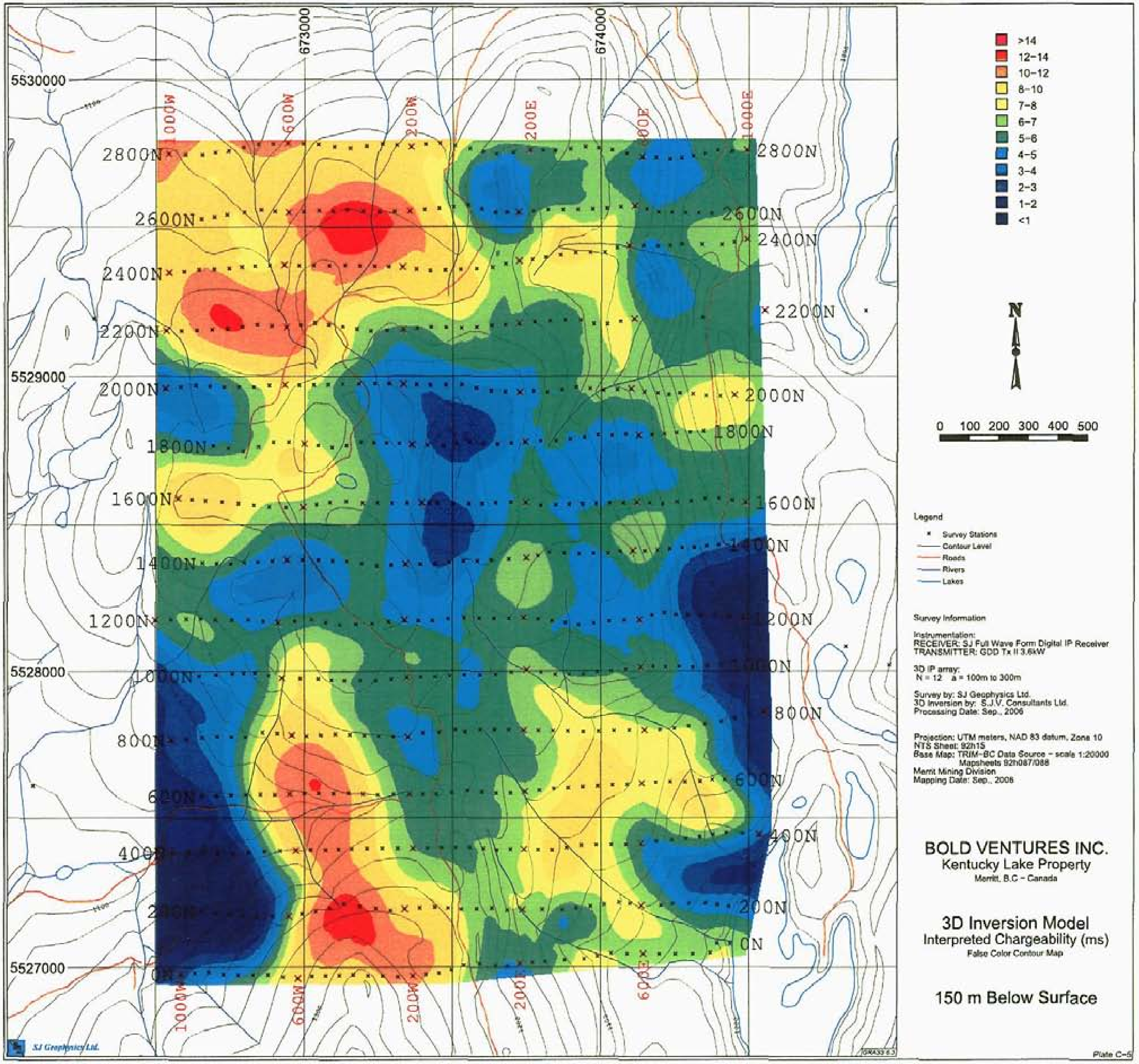


5530000
5529000
5528000
5527000
673000
674000
1000W
600W
200W
200E
600E
1000E
2800N
2600N
2400N
2200N
2000N
1800N
1600N
1400N
1200N
1000N
800N
600N
400N
200N
0N
>14
12-14
10-12
8-10
7-8
6-7
5-6
4-5
3-4
2-3
1-2
<1
N
0 100 200 300 400 500
Legend
Survey Stations
Contour Level
Roads
Rivers
Lakes
Survey Information
Instrumentation:
RECEIVER: SJ Full Wave Form Digital IP Receiver
TRANSMITTER: GDD Tx II 3.6kW
3D IP array:
N = 12 a = 100m to 300m
Survey by: SJ Geophysics Ltd.
3D Inversion by: S.J.V. Consultants Ltd.
Processing Date: Sep., 2006
Projection: UTM meters, NAD 83 datum, Zone 10
NTS Sheet: 92h15
Base Map: TRIM-BC Data Source - scale 1:20000
Mapsheets 92h087/088
Merrit Mining Division
Mapping Date: Sep., 2006
BOLD VENTURES INC.
Kentucky Lake Property
Merritt, B.C - Canada
3D Inversion Model
Interpreted Chargeability (ms)
False Color Contour Map
50 m Below Surface
SJ Geophysics Ltd.
Plate C-2

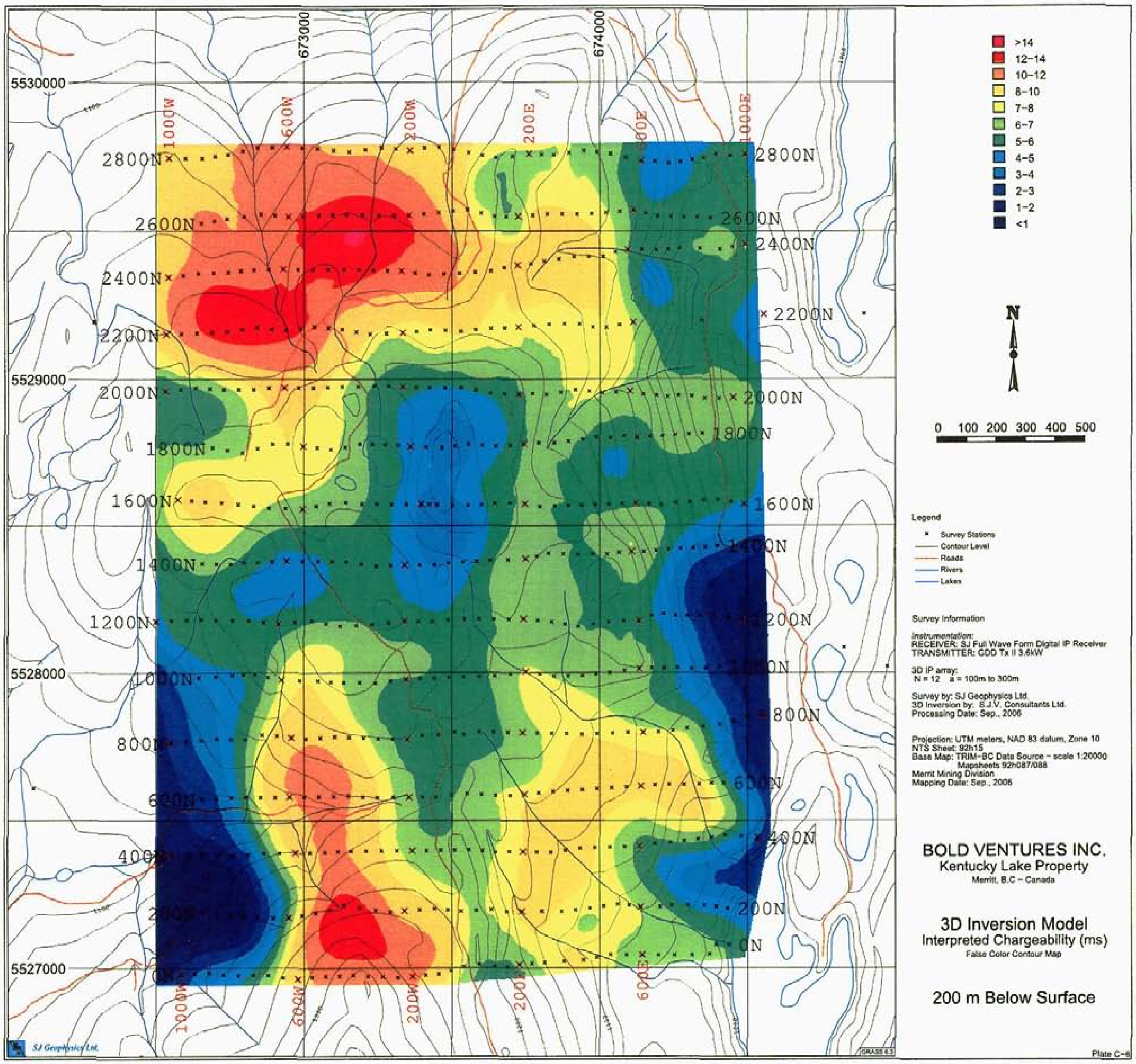


>14
12-14
10-12
8-10
7-8
6-7
5-6
4-5
3-4
2-3
1-2
<1
N
0 100 200 300 400 500
Legend
Survey Stations
Contour Level
Roads
Rivers
Lakes
Survey Information
Instrumentation:
RECEIVER: SJ Full Wave Form Digital IP Receiver
TRANSMITTER: GDD Tx II 3.6kW
3D IP array:
N = 12 a = 100m to 300m
Survey by: SJ Geophysics Ltd.
3D Inversion by: S.J.V. Consultants Ltd.
Processing Date: Sep., 2006
Projection: UTM meters, NAD 83 datum, Zone 10
NTS Sheet: 92h15
Base Map: TRIM-BC Data Source - scale 1:20000
Mapsheets 92h087/088
Merrit Mining Division
Mapping Date: Sep., 2006
BOLD VENTURES INC.
Kentucky Lake Property
Merritt, B.C - Canada
3D Inversion Model
Interpreted Chargeability (ms)
False Color Contour Map
75 m Below Surface
Plate C-3
SJ Geophysics Ltd.
5530000
5529000
5528000
5527000
673000
674000
2800N
2600N
2400N
2200N
2000N
1800N
1600N
1400N
1200N
1000N
800N
600N
400N
200N
0N
1000W
600W
200W
200E
600E
1000E


>14
12-14
10-12
8-10
7-8
6-7
5-6
4-5
3-4
2-3
1-2
<1
N
0 100 200 300 400 500
Legend
Survey Stations
Contour Level
Roads
Rivers
Lakes
Survey Information
Instrumentation;
RECEIVER: SJ Full Wave Form Digital IP Receiver
TRANSMITTER: GDD Tx II 3.6kW
3D IP array:
N = 12 a = 100m to 300m
Survey by: SJ Geophysics Ltd.
3D Inversion by: S.J.V. Consultants Ltd.
Processing Date: Sep., 2006
Projection: UTM meters, NAD 83 datum, Zone 10
NTS Sheet: 92h15
Base Map: TRIM-BC Data Source - scale 1:20000
Mapsheets 92h087/088
Merrit Mining Division
Mapping Date: Sep., 2006
BOLD VENTURES INC.
Kentucky Lake Property
Merritt, B.C - Canada
3D Inversion Model
Interpreted Chargeability (ms)
False Color Contour Map
100 m Below Surface
Plate C-4
SJ Geophysics Ltd.
673000
674000
5530000
5529000
5528000
5527000
2800N
2600N
2400N
2200N
2000N
1800N
1600N
1400N
1200N
1000N
800N
600N
400N
200N
0N
1000W
600W
200W
200E
600E
1000E



5530000
5529000
5528000
5527000
673000
674000
2800N
2600N
2400N
2200N
2000N
1800N
1600N
1400N
1200N
1000N
800N
600N
400N
200N
0N
1000W
600W
200W
200E
600E
1000E
>14
12–14
10–12
8–10
7–8
6–7
5–6
4–5
3–4
2–3
1–2
<1
N
0 100 200 300 400 500
Legend
Survey Stations
Contour Level
Roads
Rivers
Lakes
Survey Information
Instrumentation:
RECEIVER: SJ Full Wave Form Digital IP Receiver
TRANSMITTER: GDD Tx II 3.6kW
3D IP array:
N = 12 a = 100m to 300m
Survey by: SJ Geophysics Ltd.
3D Inversion by: S.J.V. Consultants Ltd.
Processing Date: Sep., 2006
Projection: UTM meters, NAD 83 datum, Zone 10
NTS Sheet: 92h15
Base Map: TRIM–BC Data Source – scale 1:20000
Mapsheets 92h087/088
Merrit Mining Division
Mapping Date: Sep., 2006
BOLD VENTURES INC.
Kentucky Lake Property
Merritt, B.C – Canada
3D Inversion Model
Interpreted Chargeability (ms)
False Color Contour Map
150 m Below Surface
SJ Geophysics Ltd.
Plate C-5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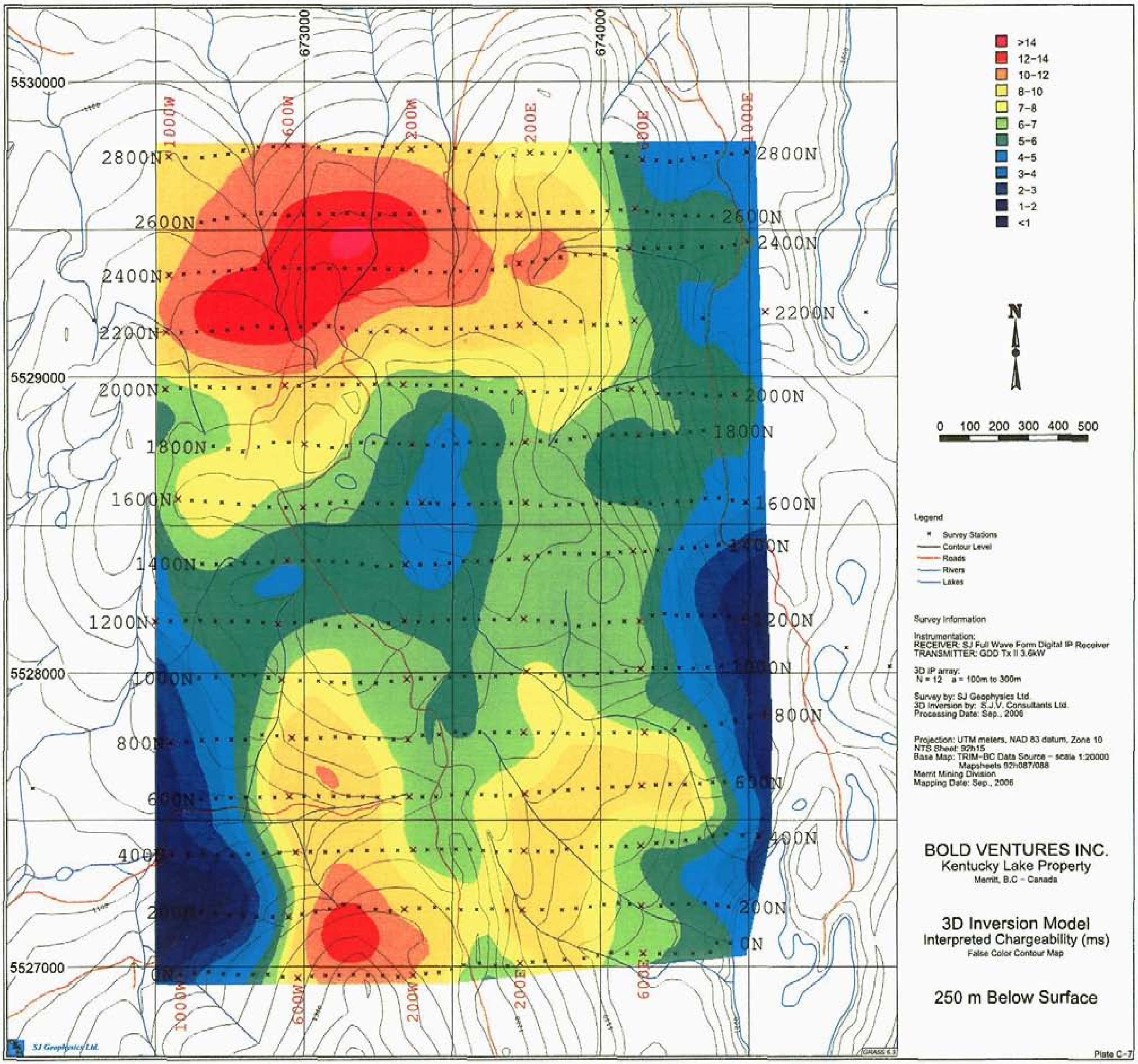
6–7
5–6
4–5
3–4
2–3
1–2
<1
N
0 100 200 300 400 500
Legend
Survey Stations
Contour Level
Roads
Rivers
Lakes
Survey Information
Instrumentation:
RECEIVER: SJ Full Wave Form Digital IP Receiver
TRANSMITTER: GDD Tx II 3.6kW
3D IP array:
N = 12 a = 100m to 300m
Survey by: SJ Geophysics Ltd.
3D Inversion by: S.J.V. Consultants Ltd.
Processing Date: Sep., 2006
Projection: UTM meters, NAD 83 datum, Zone 10
NTS Sheet: 92h15
Base Map: TRIM–BC Data Source – scale 1:20000
Mapsheets 92h087/088
Merrit Mining Division
Mapping Date: Sep., 2006
BOLD VENTURES INC.
Kentucky Lake Property
Merritt, B.C – Canada
3D Inversion Model
Interpreted Chargeability (ms)
False Color Contour Map
200 m Below Surface
Plate C-6
5530000
5529000
5528000
5527000
673000
674000
2800N
2600N
2400N
2200N
2000N
1800N
1600N
1400N
1200N
1000N
800N
600N
400N
200N
0N
1000W
600W
200W
200E
600E
1000E
SJ Geophysics Ltd.



673000
674000
5530000
5529000
5528000
5527000
1000W
600W
200W
200E
600E
1000E
2800N
2600N
2400N
2200N
2000N
1800N
1600N
1400N
1200N
1000N
800N
600N
400N
200N
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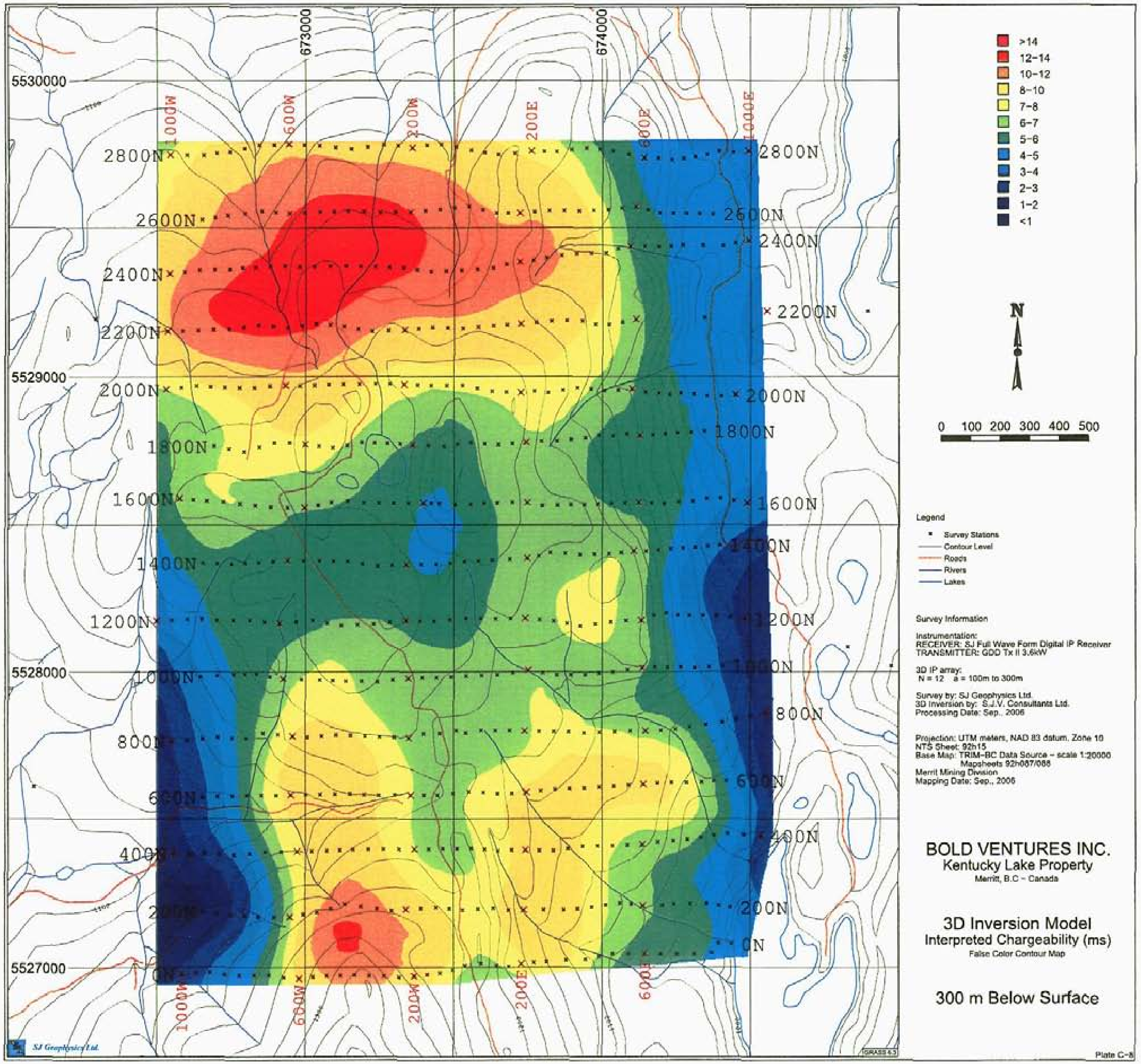
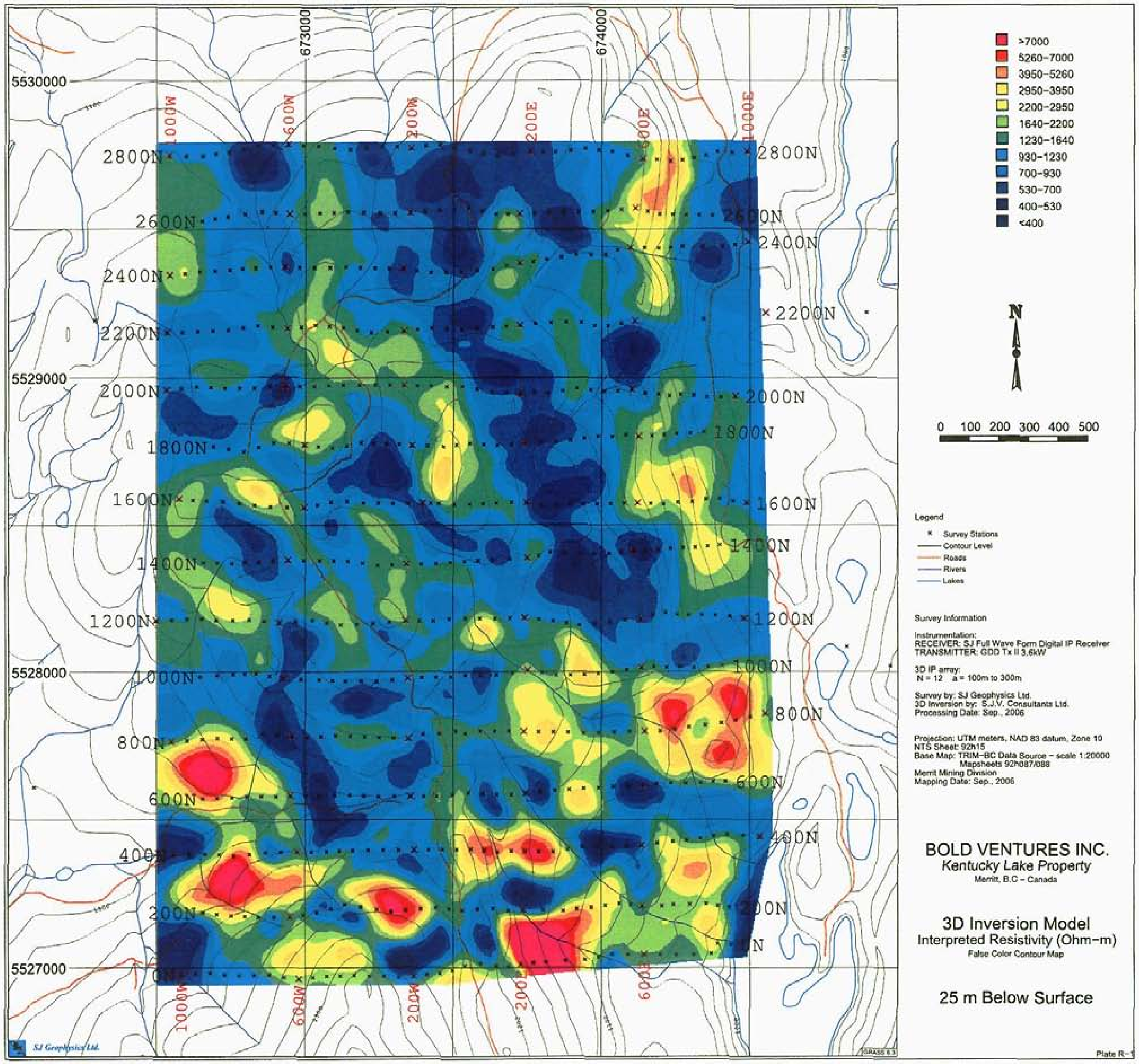
10–12
8–10
7–8
6–7
5–6
4–5
3–4
2–3
1–2
<1
N
0 100 200 300 400 500
Legend
Survey Stations
Contour Level
Roads
Rivers
Lakes
Survey Information
Instrumentation:
RECEIVER: SJ Full Wave Form Digital IP Receiver
TRANSMITTER: GDD Tx II 3.6kW
3D IP array:
N = 12 a = 100m to 300m
Survey by: SJ Geophysics Ltd.
3D Inversion by: S.J.V. Consultants Ltd.
Processing Date: Sep., 2006
Projection: UTM meters, NAD 83 datum, Zone 10
NTS Sheet: 92h15
Base Map: TRIM-BC Data Source – scale 1:20000
Mapsheets 92h087/088
Merrit Mining Division
Mapping Date: Sep., 2006
BOLD VENTURES INC.
Kentucky Lake Property
Merritt, B.C - Canada
3D Inversion Model
Interpreted Chargeability (ms)
False Color Contour Map
250 m Below Surface
SJ Geophysics Ltd.
Plate C-7

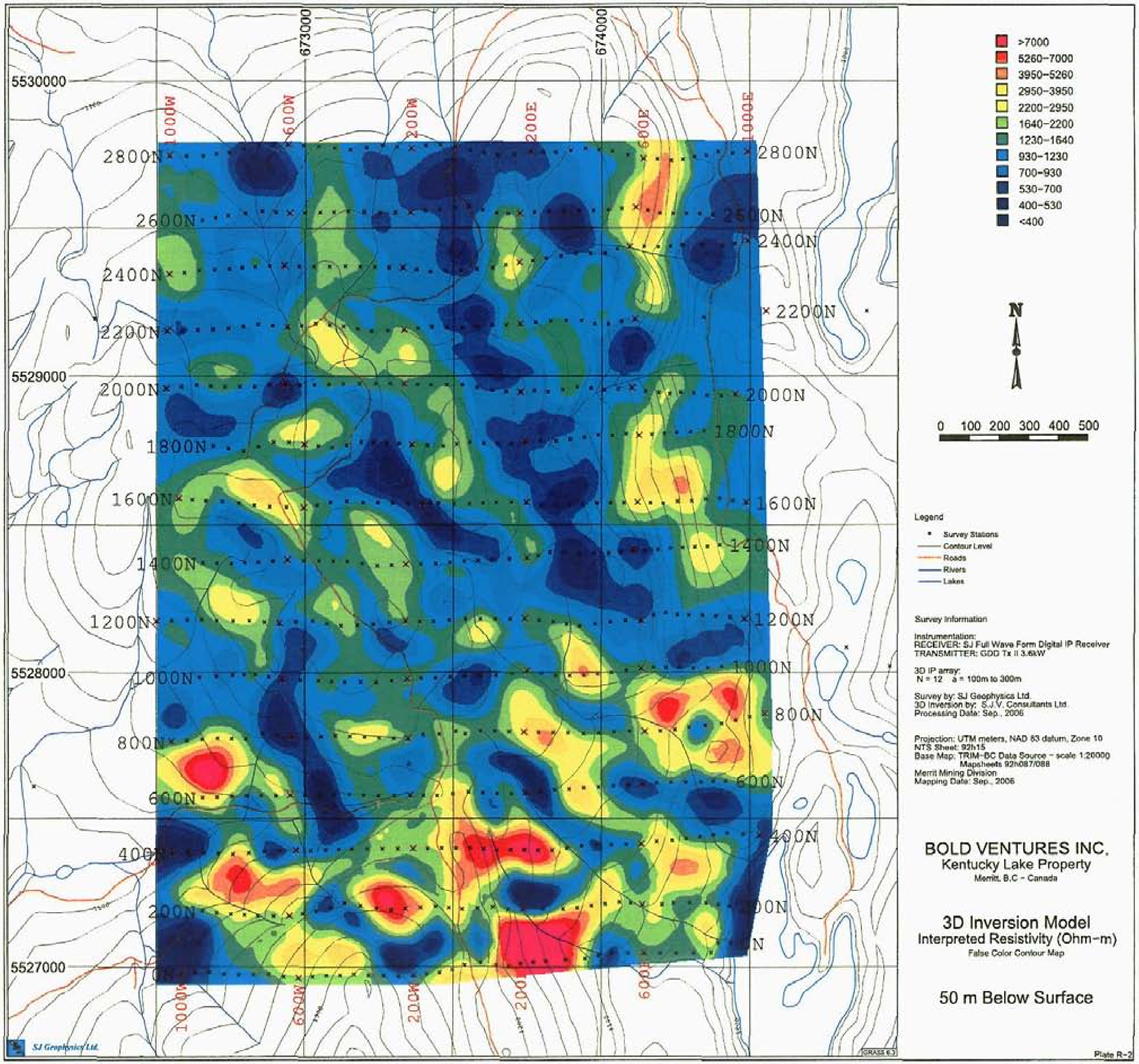


>14
12-14
10-12
8-10
7-8
6-7
5-6
4-5
3-4
2-3
1-2
<1
N
0 100 200 300 400 500
Legend
Survey Stations
Contour Level
Roads
Rivers
Lakes
Survey Information
Instrumentation:
RECEIVER: SJ Full Wave Form Digital IP Receiver
TRANSMITTER: GDD Tx II 3.6kW
3D IP array:
N = 12 a = 100m to 300m
Survey by: SJ Geophysics Ltd.
3D Inversion by: S.J.V. Consultants Ltd.
Processing Date: Sep., 2006
Projection: UTM meters, NAD 83 datum, Zone 10
NTS Sheet: 92h15
Base Map: TRIM-BC Data Source - scale 1:20000
Mapsheets 92h087/088
Merrit Mining Division
Mapping Date: Sep., 2006
BOLD VENTURES INC.
Kentucky Lake Property
Merritt, B.C - Canada
3D Inversion Model
Interpreted Chargeability (ms)
False Color Contour Map
300 m Below Surface
Plate C-8
5530000
5529000
5528000
5527000
673000
674000
2800N
2600N
2400N
2200N
2000N
1800N
1600N
1400N
1200N
1000N
800N
600N
400N
200N
0N
1000W
600W
200W
200E
600E
1000E
SJ Geophysics Ltd.

APPENDIX 5 – INVERTED DEPTH SLICE MAPS- RESISTIVITY



673000
674000
5530000
5529000
5528000
5527000
1000W
600W
200W
200E
600E
1000E
2800N
2600N
2400N
2200N
2000N
1800N
1600N
1400N
1200N
1000N
800N
600N
400N
200N
0N
>7000
5260-7000
3950-5260
2950-3950
2200-2950
1640-2200
1230-1640
930-1230
700-930
530-700
400-530
<400
N
0 100 200 300 400 500
Legend
Survey Stations
Contour Level
Roads
Rivers
Lakes
Survey Information
Instrumentation:
RECEIVER: SJ Full Wave Form Digital IP Receiver
TRANSMITTER: GDD Tx II 3.6kW
3D IP array:
N = 12 a = 100m to 300m
Survey by: SJ Geophysics Ltd.
3D Inversion by: S.J.V. Consultants Ltd.
Processing Date: Sep., 2006
Projection: UTM meters, NAD 83 datum, Zone 10
NTS Sheet: 92h15
Base Map: TRIM-BC Data Source - scale 1:20000
Mapsheets 92h087/088
Merrit Mining Division
Mapping Date: Sep., 2006
BOLD VENTURES INC.
Kentucky Lake Property
Merritt, B.C - Canada
3D Inversion Model
Interpreted Resistivity (Ohm-m)
False Color Contour Map
25 m Below Surface
SJ Geophysics Ltd.
Plate R-1



>7000
5260-7000
3950-5260
2950-3950
2200-2950
1640-2200
1230-1640
930-1230
700-930
530-700
400-530
<400
N
0 100 200 300 400 500
Legend
Survey Stations
Contour Level
Roads
Rivers
Lakes
Survey Information
Instrumentation:
RECEIVER: SJ Full Wave Form Digital IP Receiver
TRANSMITTER: GDD Tx II 3.6kW
3D IP array:
N = 12 a = 100m to 300m
Survey by: SJ Geophysics Ltd.
3D Inversion by: S.J.V. Consultants Ltd
Processing Date: Sep., 2006
Projection: UTM meters, NAD 83 datum, Zone 10
NTS Sheet: 92h15
Base Map: TRIM-BC Data Source - scale 1:20000
Mapsheets 92h087/088
Merrit Mining Division
Mapping Date: Sep., 2006
BOLD VENTURES INC.
Kentucky Lake Property
Merritt, B.C - Canada
3D Inversion Model
Interpreted Resistivity (Ohm-m)
False Color Contour Map
50 m Below Surface
Plate R-2
SJ Geophysics Ltd.
5530000
5529000
5528000
5527000
673000
674000
2800N
2600N
2400N
2200N
2000N
1800N
1600N
1400N
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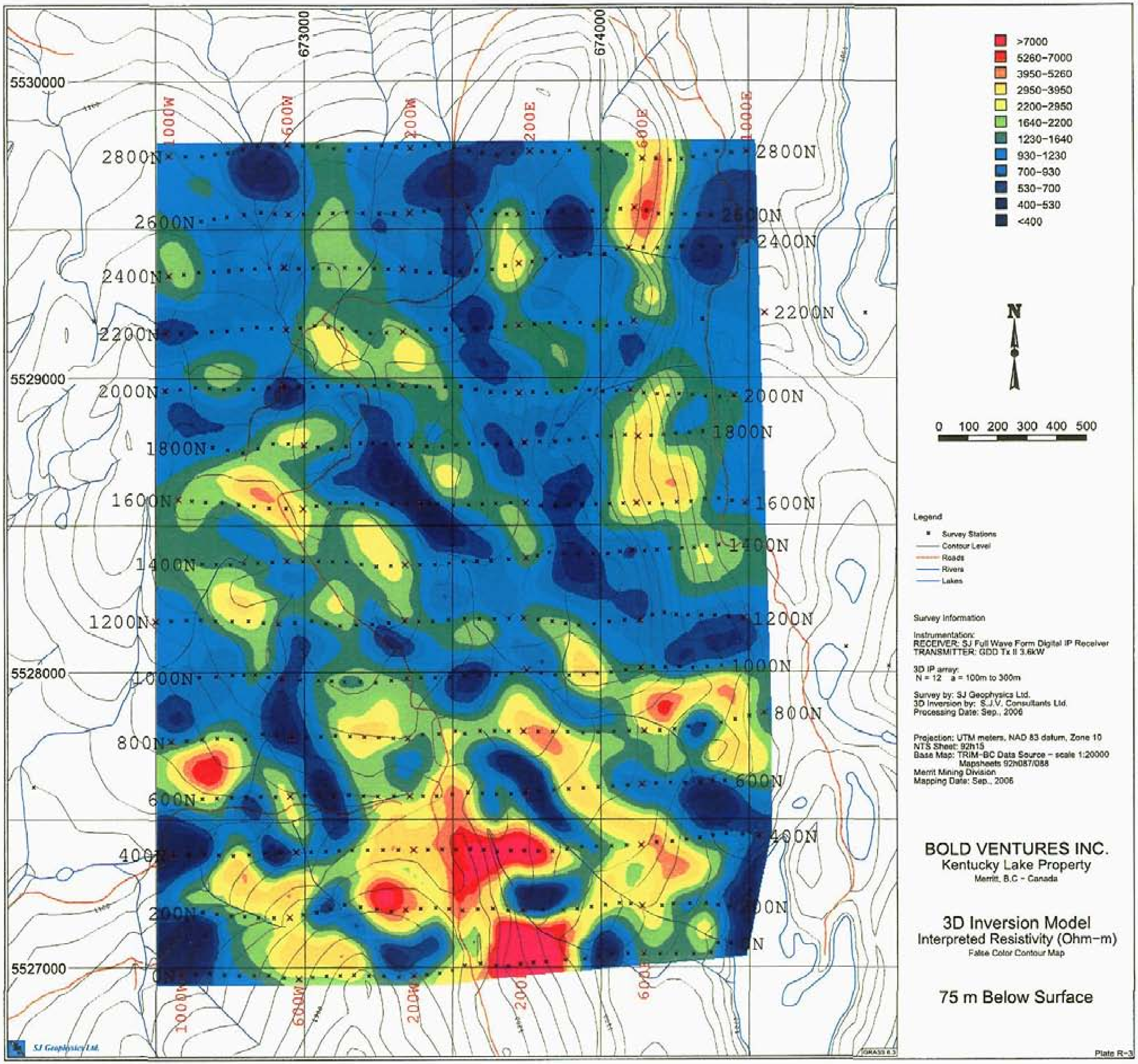
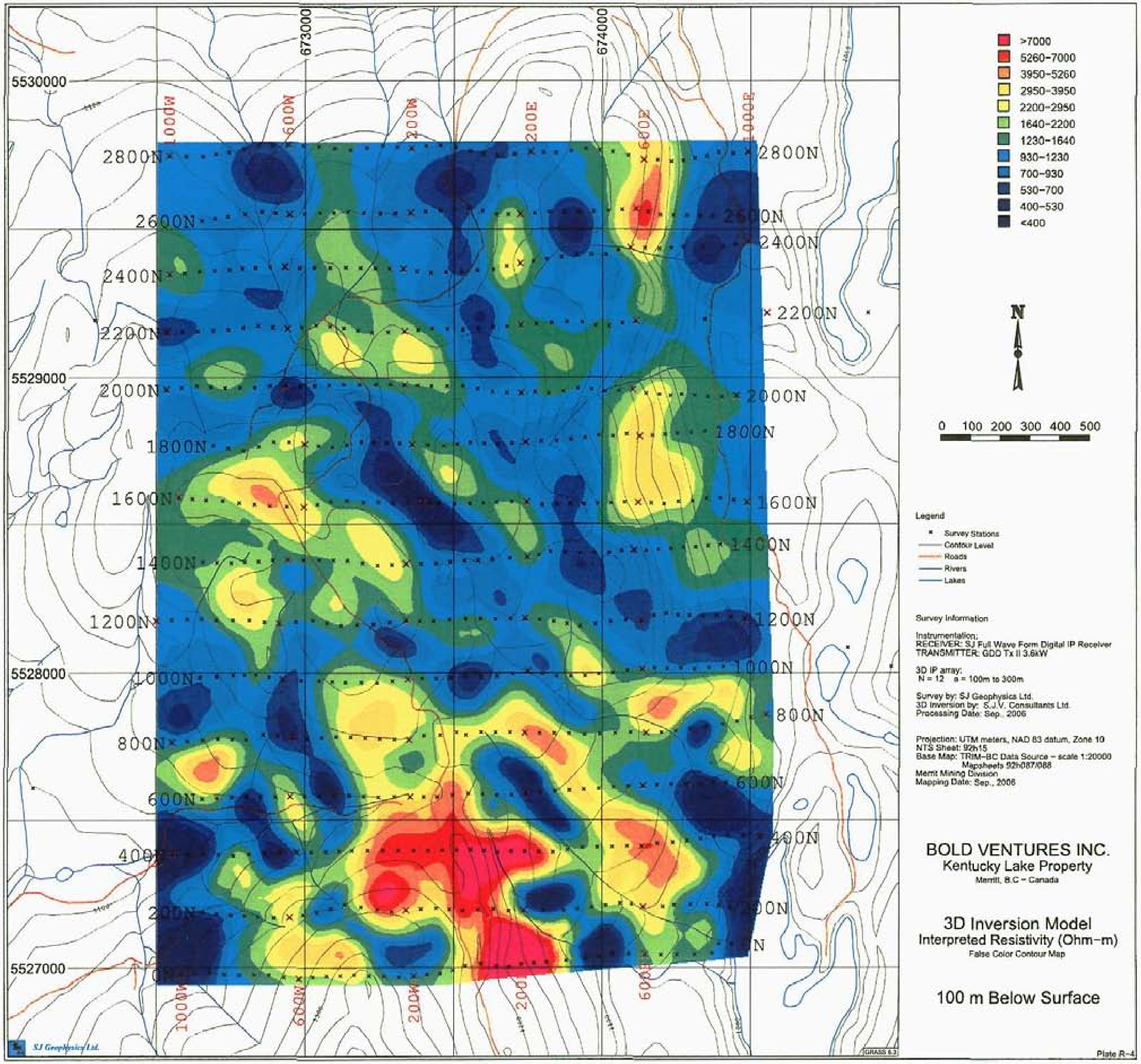
200W
200E
600E
1000E



>7000
5260-7000
3950-5260
2950-3950
2200-2950
1640-2200
1230-1640
930-1230
700-930
530-700
400-530
<400
N
0 100 200 300 400 500
Legend
Survey Stations
Contour Level
Roads
Rivers
Lakes
Survey Information
Instrumentation:
RECEIVER: SJ Full Wave Form Digital IP Receiver
TRANSMITTER: GDD Tx II 3.6kW
3D IP array:
N = 12 a = 100m to 300m
Survey by: SJ Geophysics Ltd.
3D Inversion by: S.J.V. Consultants Ltd.
Processing Date: Sep., 2006
Projection: UTM meters, NAD 83 datum, Zone 10
NTS Sheet: 92h15
Base Map: TRIM-BC Data Source - scale 1:20000
Mapsheets 92h087/088
Merrit Mining Division
Mapping Date: Sep., 2006
BOLD VENTURES INC.
Kentucky Lake Property
Merritt, B.C - Canada
3D Inversion Model
Interpreted Resistivity (Ohm-m)
False Color Contour Map
75 m Below Surface
Plate R-3
SJ Geophysics Ltd.
5530000
5529000
5528000
5527000
673000
674000
2800N
2600N
2400N
2200N
2000N
1800N
1600N
1400N
1200N
1000N
800N
600N
400N
200N
1000W
600W
200W
200E
600E
1000E



>7000
5260-7000
3950-5260
2950-3950
2200-2950
1640-2200
1230-1640
930-1230
700-930
530-700
400-530
<400
N
0 100 200 300 400 500
Legend
Survey Stations
Contour Level
Roads
Rivers
Lakes
Survey Information
Instrumentation;
RECEIVER: SJ Full Wave Form Digital IP Receiver
TRANSMITTER: GDD Tx II 3.6kW
3D IP array:
N = 12 a = 100m to 300m
Survey by: SJ Geophysics Ltd.
3D Inversion by: S.J.V. Consultants Ltd.
Processing Date: Sep., 2006
Projection: UTM meters, NAD 83 datum, Zone 10
NTS Sheet: 92h15
Base Map: TRIM-BC Data Source - scale 1:20000
Mapsheets 92h087/088
Merrit Mining Division
Mapping Date: Sep., 2006
BOLD VENTURES INC.
Kentucky Lake Property
Merritt, B.C - Canada
3D Inversion Model
Interpreted Resistivity (Ohm-m)
False Color Contour Map
100 m Below Surface
Plate R-4
SJ Geophysics Ltd.
GRASS 6.3
5530000
5529000
5528000
5527000
673000
674000
2800N
2600N
2400N
2200N
2000N
1800N
1600N
1400N
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800N
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200N
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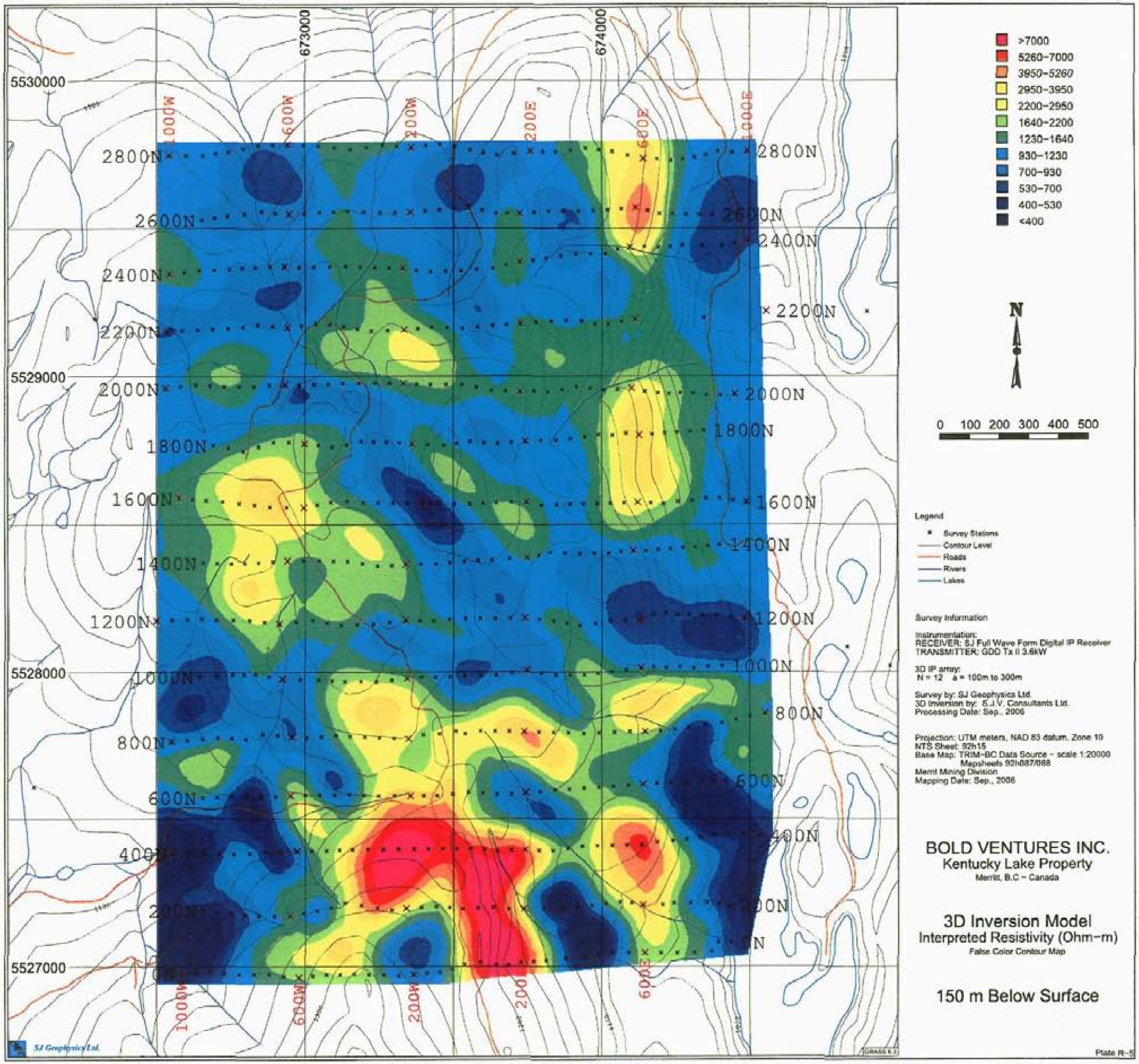
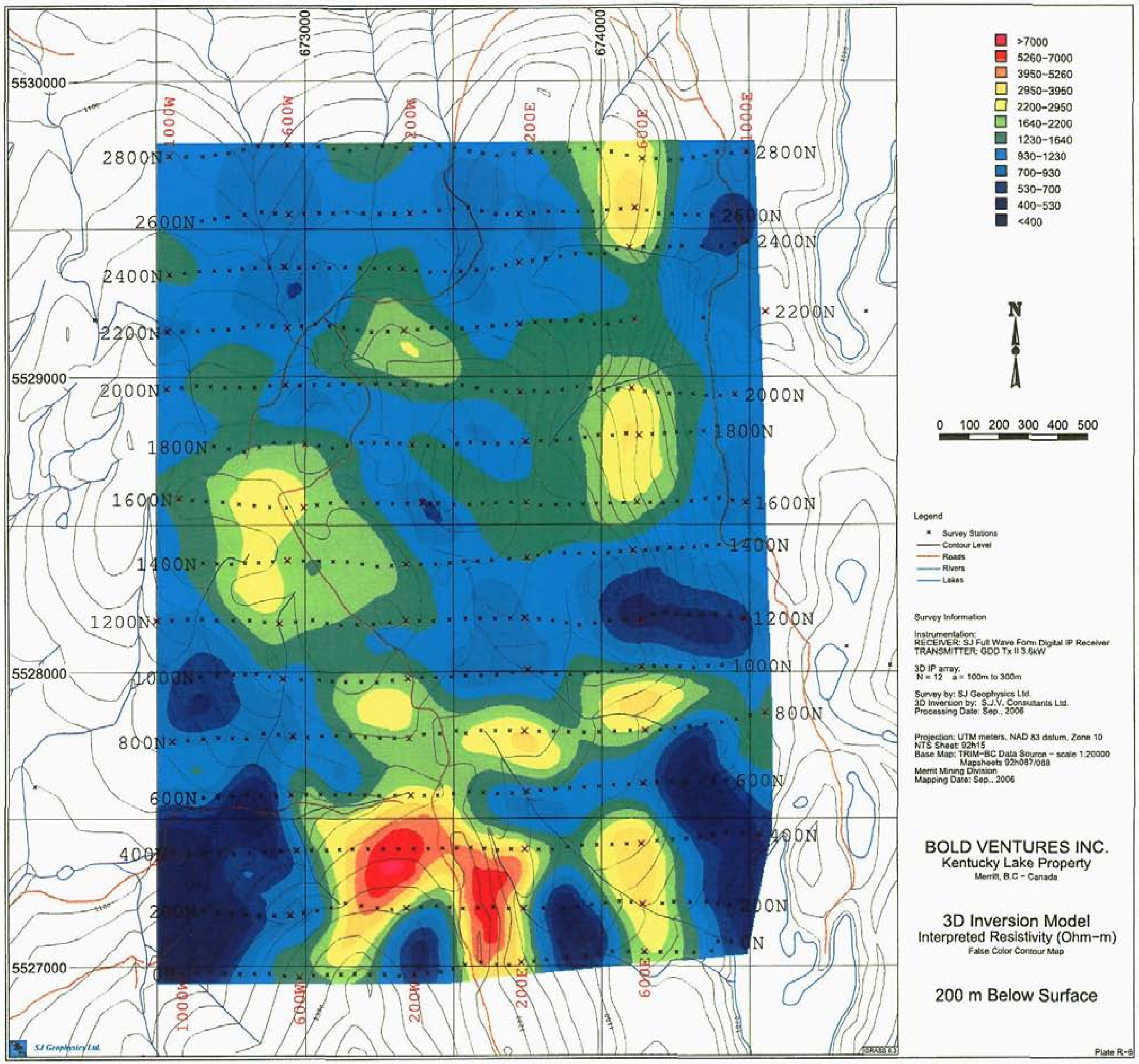
200W
200E
600E
1000E



5530000
5529000
5528000
5527000
673000
674000
1000W
600W
200W
200E
600E
1000E
2800N
2600N
2400N
2200N
2000N
1800N
1600N
1400N
1200N
1000N
800N
600N
400N
200N
>7000
5260-7000
3950-5260
2950-3950
2200-2950
1640-2200
1230-1640
930-1230
700-930
530-700
400-530
<400
N
0 100 200 300 400 500
Legend
Survey Stations
Contour Level
Roads
Rivers
Lakes
Survey Information
Instrumentation:
RECEIVER: SJ Full Wave Form Digital IP Receiver
TRANSMITTER: GDD Tx II 3.6kW
3D IP array:
N = 12 a = 100m to 300m
Survey by: SJ Geophysics Ltd.
3D Inversion by: S.J.V. Consultants Ltd.
Processing Date: Sep., 2006
Projection: UTM meters, NAD 83 datum, Zone 10
NTS Sheet: 92h15
Base Map: TRIM-BC Data Source - scale 1:20000
Mapsheets 92h087/088
Merrit Mining Division
Mapping Date: Sep., 2006
BOLD VENTURES INC.
Kentucky Lake Property
Merritt, B.C - Canada
3D Inversion Model
Interpreted Resistivity (Ohm-m)
False Color Contour Map
150 m Below Surface
SJ Geophysics Ltd.
Plate R-5



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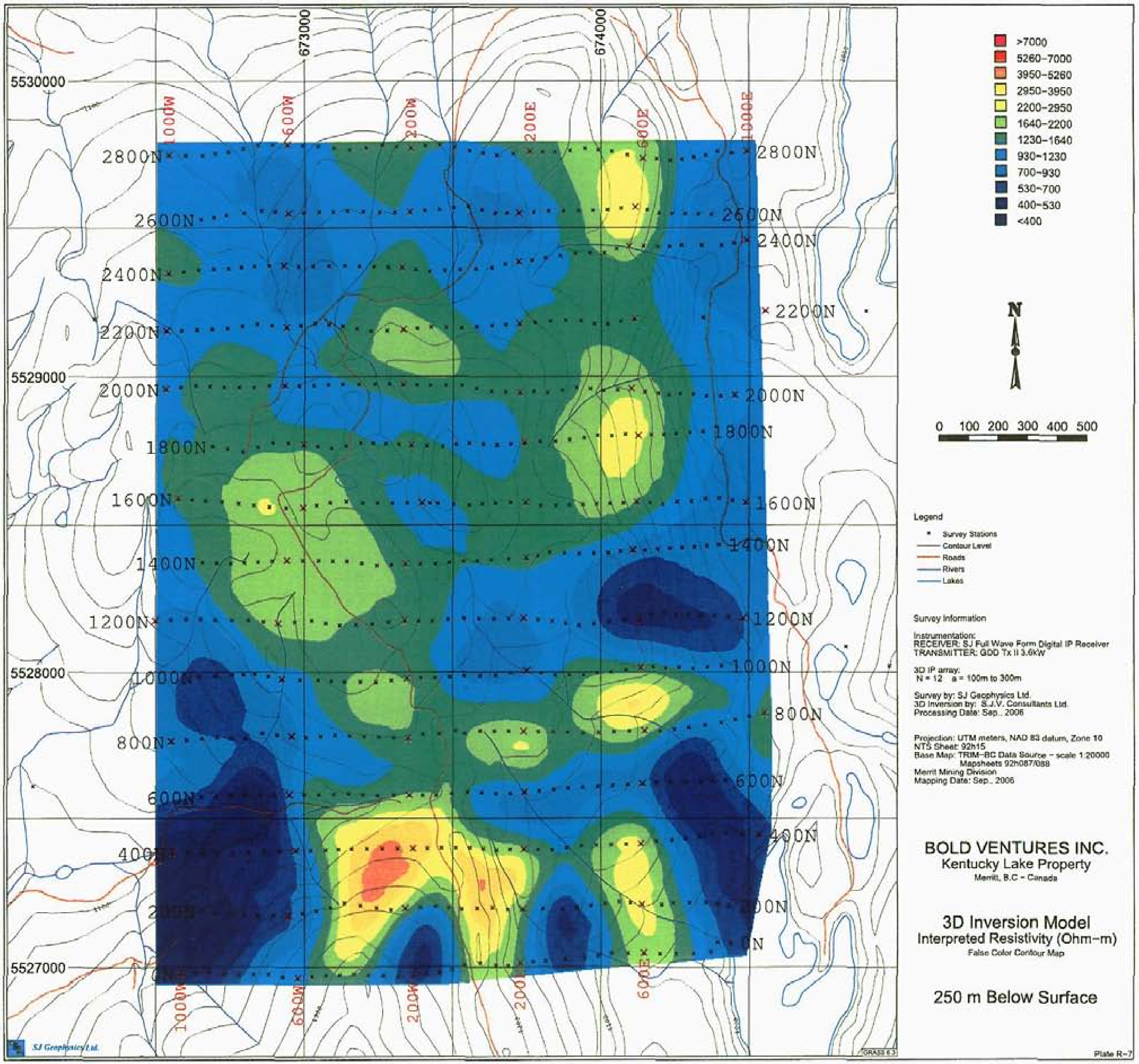
2200-2950
1640-2200
1230-1640
930-1230
700-930
530-700
400-530
<400
N
0 100 200 300 400 500
Legend
Survey Stations
Contour Level
Roads
Rivers
Lakes
Survey Information
Instrumentation:
RECEIVER: SJ Full Wave Form Digital IP Receiver
TRANSMITTER: GDD Tx II 3.6kW
3D IP array:
N = 12 a = 100m to 300m
Survey by: SJ Geophysics Ltd.
3D Inversion by: S.J.V. Consultants Ltd.
Processing Date: Sep., 2006
Projection: UTM meters, NAD 83 datum, Zone 10
NTS Sheet: 92h15
Base Map: TRIM-BC Data Source - scale 1:20000
Mapsheets 92h087/088
Merrit Mining Division
Mapping Date: Sep., 2006
BOLD VENTURES INC.
Kentucky Lake Property
Merritt, B.C - Canada
3D Inversion Model
Interpreted Resistivity (Ohm-m)
False Color Contour Map
200 m Below Surface
Plate R-6
SJ Geophysics Ltd.
5530000
5529000
5528000
5527000
673000
674000
2800N
2600N
2400N
2200N
2000N
1800N
1600N
1400N
1200N
1000N
800N
600N
400N
200N
1000W
600W
200W
200E
600E
1000E



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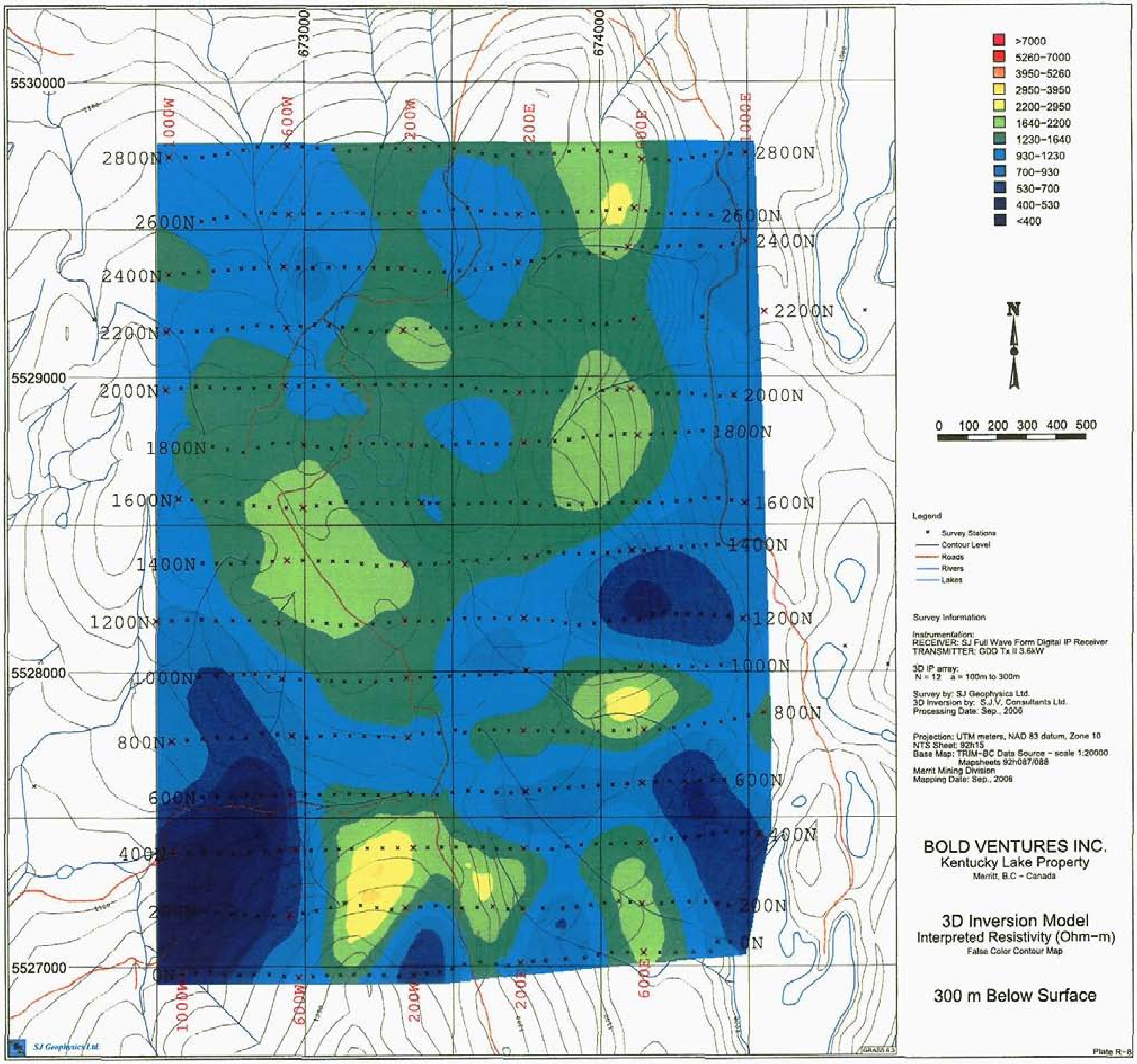
700-930
530-700
400-530
<400
N
0 100 200 300 400 500
Legend
Survey Stations
Contour Level
Roads
Rivers
Lakes
Survey Information
Instrumentation:
RECEIVER: SJ Full Wave Form Digital IP Receiver
TRANSMITTER: GDD Tx II 3.6KW
3D IP array:
N = 12 a = 100m to 300m
Survey by: SJ Geophysics Ltd.
3D Inversion by: S.J.V. Consultants Ltd.
Processing Date: Sep., 2006
Projection: UTM meters, NAD 83 datum, Zone 10
NTS Sheet: 92h15
Base Map: TRIM-BC Data Source - scale 1:20000
Mapsheets 92h087/088
Merrit Mining Division
Mapping Date: Sep., 2006
BOLD VENTURES INC.
Kentucky Lake Property
Merritt, B.C - Canada
3D Inversion Model
Interpreted Resistivity (Ohm-m)
False Color Contour Map
250 m Below Surface
SJ Geophysics Ltd.
Plate R-7



>7000
5260–7000
3950–5260
2950–3950
2200–2950
1640–2200
1230–1640
930–1230
700–930
530–700
400–530
<400
N
0 100 200 300 400 500
Legend
Survey Stations
Contour Level
Roads
Rivers
Lakes
Survey Information
Instrumentation:
RECEIVER: SJ Full Wave Form Digital IP Receiver
TRANSMITTER: GDD Tx II 3.6kW
3D IP array:
N = 12 a = 100m to 300m
Survey by: SJ Geophysics Ltd.
3D Inversion by: S.J.V. Consultants Ltd.
Processing Date: Sep., 2006
Projection: UTM meters, NAD 83 datum, Zone 10
NTS Sheet: 92h15
Base Map: TRIM-BC Data Source – scale 1:20000
Mapsheets 92h087/088
Merrit Mining Division
Mapping Date: Sep., 2006
BOLD VENTURES INC.
Kentucky Lake Property
Merritt, B.C – Canada
3D Inversion Model
Interpreted Resistivity (Ohm–m)
False Color Contour Map
300 m Below Surface
Plate R-8
SJ Geophysics Ltd.
5530000
5529000
5528000
5527000
673000
674000
1000W
600W
200W
200E
600E
1000E
2800N
2600N
2400N
2200N
2000N
1800N
1600N
1400N
1200N
1000N
800N
600N
400N
200N
0N

Appendix D – Sample Descriptions and Assay/Geochem Sheets

Sample Descriptions:

Sample No.	Showing	GPS Coords	Grid Coords	Elev.	Sample Description	Cu Content
K-01	AR	5529473N 672836E	L24+90N @7+00W	3840'	Chip sample from o/c and rubble/3m. Altd and with cpy, pyr, bor? and mal.	6962ppm
K-02	Tom Cat	5528165N 672793E	L12+00N @7+00W	4080'	Chip/2m of old trench. Altd and/intr, with cpy, chalk, mag, pyr, and mal	3.68%
K-03	Tom Cat	Same as above			Chip/0.5m. Well minerd and altd volc as K-02	1.76%
K-04	Bluey	5527639N 673474E	not located	3987'	Chip/4m. Rusty, altd volc with cpy, chal, pyr, mal.	9190ppm
K-05	Bunker Hill	5527320N 673587E	3+00N@ 1+00E	4026'	Chip/2m. Well mineralized andesite, cpy, chal, pyr, mal	3.73%
K-06	Portland	5527656N 672670E	L6+00N @9+00W	3775'	Dump sample. Diss black min chal? in altd andesite	1702ppm
K-07	AR-2	5529706N 676724E	L28+00N @1+75E	3948'	Chip/0.5m. Shear zone, weak altd volcs in pit (shaft?). pyr and malachite in shear	5347ppm

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604,[illegible]3-31[illegible] FAX[illegible])25[illegible]716
(ISO 9001 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Kerr, John PROJECT Kentucky Lake File # A603986

208 - 515 W Pender St., Vancouver BC V6B 6H5 Submitted by: John Kerr

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm
G-1	.1	2.8	2.1	44	<.1	3.2	4.2	492	1.58	<.5	2.3	<.5	3.2	38	<.1	<.1	.1	31
K-01	.3	6962.4	1.4	43	2.3	2.3	13.1	874	3.20	3.2	.5	4.5	1.0	39	.1	.2	<.1	75
K-02	.7	>10000	5.2	53	9.8	3.4	21.2	929	5.12	2.7	.7	7.1	.9	84	10.4	.2	.1	222
K-03	4.2	>10000	19.6	118	9.2	4.9	31.9	1389	6.41	1.4	.6	5.8	.8	37	289.1	.1	.1	254
K-04	12.5	9189.8	1551.1	7973	10.9	7.9	22.3	1308	4.51	16.3	.2	3.8	.9	83	110.0	3.2	.1	157
K-05	.5	>10000	7.4	42	33.4	2.8	11.9	934	1.91	5.9	.4	6.0	1.9	69	3.7	.3	2.2	67
K-06	2.7	1702.3	9.8	86	2.0	12.7	21.5	1326	3.70	5.2	.9	<.5	1.4	311	.8	.3	.1	151
K-07	.9	5347.0	3.3	50	4.0	4.2	21.5	1359	4.59	6.3	.5	7.4	.9	64	1.1	.1	.2	210
STANDARD DS7	20.9	107.8	70.4	410	1.0	55.1	9.4	630	2.41	48.0	4.9	86.0	4.5	71	6.3	5.9	4.5	86

SAMPLE#	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.48	.084	5	6	.57	176	.107	2	.80	.049	.48	<.1	<.01	1.8	.3	<.05	4	<.5
K-01	1.29	.155	6	3	.80	75	.141	2	.84	.044	.04	.2	.01	5.1	<.1	.08	5	.5
K-02	3.32	.199	7	4	.93	21	.156	9	1.96	.033	.03	.1	.04	7.6	<.1	.52	11	<.5
K-03	2.50	.187	7	4	1.91	36	.160	9	2.48	.033	.05	.1	.09	7.4	.1	.24	17	<.5
K-04	3.48	.118	7	10	1.43	121	.006	4	1.24	.040	.11	.1	9.19	4.2	.1	.39	10	2.8
K-05	1.52	.248	10	2	.36	67	.004	8	.45	.036	.28	.1	1.37	6.9	<.1	.39	2	<.5
K-06	2.40	.183	9	15	1.73	21	.169	10	1.79	.039	.08	.1	.08	4.6	<.1	.14	12	<.5
K-07	3.15	.190	6	2	1.69	114	.206	15	3.45	.028	.08	.1	.08	12.3	.1	.07	14	1.6
STANDARD DS7	.94	.079	13	172	1.05	379	.122	41	.98	.103	.46	4.0	.21	2.5	4.3	.21	5	3.5

GROUP 1DX - 15 GM SAMPLE LEACHED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 300 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: ROCK R150

2006-08-10 A08:52

Data ___ FA ___ DATE RECEIVED: JUL 26 2006 DATE REPORT MAILED:.................

BRITISH COLUMBIA CERTIFIED ASSAYER
Raymond Chan

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE (604) 2[illegible]-31[illegible] FAX (6[illegible]) 25[illegible]-[illegible]716
(ISO 9001 Accredited Co.)

ASSAY CERTIFICATE

Kerr, John PROJECT Kentucky Lake File # A603986R

208 - 515 W Pender St., Vancouver BC V6B 6H5 Submitted by: John Kerr

SAMPLE#	Cu %
K-02	3.683
K-03	1.765
K-05	3.727
STANDARD R-2a	.565

GROUP 7AR - 1.000 GM SAMPLE, AQUA - REGIA (HCL-HNO3-H2O) DIGESTION TO 100 ML, ANALYSED BY ICP-ES.
- SAMPLE TYPE: Rock Pulp

2006-08-16 P01:52

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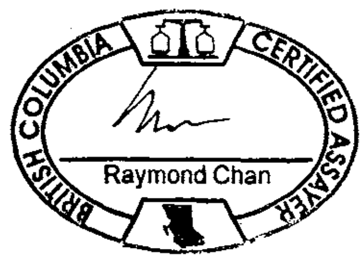

ACME ANALYTICAL LABORATORIES LTD. 8[illegible] H[illegible]INGS [illegible] V[illegible]UVE[illegible] 1R6 PH [illegible]604 [illegible]-31 FAX [illegible])25 [illegible]16
(ISO 9001 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Max Investment Inc. PROJECT Kentucky Lake File # A604334 Page 1

3750 West 49th Ave, Vancouver BC V6B 3T8

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
G-1	.3	2.3	3.0	40	<.1	3.8	4.0	506	1.99	<.5	2.3	1.6	3.9	81	<.1	<.1	.1	40	.61	.080	8	7	.55	216	.134	3	1.13	.141	.52	.1	<.01	3.2	.3	<.05	5	<.5	15.0
L30+00N 9+50W	.3	18.8	3.2	88	<.1	5.7	5.9	1041	1.75	2.0	.2	.7	.6	18	.1	.1	.1	48	.25	.098	2	8	.30	142	.070	2	1.24	.014	.07	.1	.03	1.9	.1	<.05	5	<.5	15.0
L30+00N 8+50W	.4	19.4	3.0	27	<.1	5.8	6.0	551	1.83	1.6	.2	2.6	.4	21	.1	.1	.1	53	.21	.048	2	10	.28	73	.073	3	1.03	.010	.07	.1	.01	2.2	<.1	<.05	4	<.5	15.0
L30+00N 7+50W	.4	27.8	4.3	52	<.1	13.3	7.3	1153	1.66	2.4	.2	1.0	.6	32	.2	.2	.1	48	.42	.056	3	26	.47	136	.069	2	.98	.012	.06	.1	.03	3.3	<.1	<.05	4	<.5	15.0
L30+00N 6+50W	.2	13.6	2.4	16	<.1	5.8	4.8	133	1.56	1.3	.1	1.0	.3	30	<.1	.1	.1	43	.27	.030	1	12	.24	68	.090	3	1.15	.015	.05	<.1	.01	1.7	<.1	<.05	4	<.5	15.0
L30+00N 5+50W	.3	18.7	3.7	55	<.1	5.6	7.5	579	2.12	.8	.3	1.1	.8	23	.1	.1	.1	70	.35	.033	3	10	.44	105	.126	3	1.05	.011	.11	<.1	.02	2.8	<.1	<.05	3	<.5	7.5
L30+00N 4+50W	.3	18.7	3.8	51	<.1	9.5	6.0	446	1.89	1.7	.2	1.8	.8	26	<.1	.1	.1	54	.30	.032	3	17	.32	126	.107	2	1.37	.015	.07	.1	.01	2.5	<.1	<.05	4	<.5	15.0
L30+00N 3+50W	.3	19.0	3.6	87	<.1	9.6	5.5	945	1.63	1.8	.2	1.3	.7	22	.1	.1	.1	42	.26	.110	3	12	.26	192	.080	2	1.55	.019	.09	.1	.01	2.2	<.1	<.05	5	<.5	15.0
L30+00N 2+50W	.4	13.0	4.1	53	<.1	8.6	5.4	930	1.41	1.6	.1	1.4	.4	21	.2	.1	.1	35	.35	.057	2	11	.26	105	.072	3	1.06	.014	.13	.1	.02	1.6	<.1	<.05	4	<.5	7.5
L30+00N 1+50W	.4	9.0	3.2	63	<.1	6.5	3.6	720	1.15	1.5	.2	2.0	.7	20	<.1	<.1	.1	28	.24	.185	2	8	.15	195	.068	1	1.11	.015	.05	.1	.02	1.6	<.1	<.05	4	<.5	15.0
L30+00N 0+50W	.5	8.2	3.7	46	<.1	6.8	3.3	494	1.04	1.3	.2	<.5	.6	20	.1	.1	.1	25	.28	.125	2	6	.12	113	.063	1	1.02	.018	.06	.1	.02	1.3	<.1	<.05	4	<.5	15.0
L30+00N 0+50E	.2	13.1	2.9	43	<.1	5.6	3.4	342	1.33	.9	.1	.9	.6	23	.1	.1	.1	35	.31	.023	2	10	.17	80	.087	2	1.16	.020	.07	.1	.01	1.6	<.1	<.05	4	<.5	15.0
L30+00N 1+50E	.3	14.8	3.1	34	<.1	6.7	3.8	326	1.43	.8	.2	1.8	.6	23	<.1	.1	.1	39	.28	.034	2	13	.19	77	.086	2	.96	.017	.08	.1	.01	1.6	<.1	<.05	3	<.5	15.0
L30+00N 3+00E	.5	20.4	3.7	65	<.1	6.0	4.4	951	1.36	1.3	.2	1.5	.7	33	.1	.1	.1	35	.40	.038	3	9	.19	123	.078	3	1.27	.017	.10	.1	.03	2.2	.1	<.05	4	<.5	7.5
L28+00N 9+50W	.5	22.7	3.8	40	<.1	7.5	6.3	655	1.60	4.1	.3	.8	.7	31	.2	.1	.1	44	.51	.127	3	9	.24	89	.072	3	1.63	.015	.06	.1	.04	2.0	.1	<.05	5	<.5	15.0
L28+00N 8+50W	.4	33.3	4.5	67	<.1	6.9	6.6	851	1.93	2.0	.3	1.3	.8	43	.4	.1	.1	56	.37	.072	3	9	.41	130	.084	6	1.63	.015	.23	<.1	.02	2.8	<.1	<.05	5	<.5	15.0
L28+00N 7+00W	.4	6.3	2.6	22	<.1	4.5	3.0	897	.88	1.2	.1	.8	.3	14	.1	<.1	<.1	25	.15	.034	1	12	.15	114	.054	1	.59	.013	.04	<.1	.04	1.2	<.1	<.05	3	<.5	15.0
L28+00N 6+00W	.3	48.6	2.0	12	.1	13.0	7.0	372	1.15	1.6	.2	1.2	.2	203	.1	.1	<.1	38	5.61	.068	3	26	.71	70	.041	15	.68	.020	.06	<.1	.03	1.3	<.1	.07	2	.6	15.0
L28+00N 5+00W	.3	10.4	3.4	46	<.1	8.3	3.5	301	1.14	2.8	.2	.9	.9	13	<.1	<.1	.1	26	.14	.317	2	7	.11	175	.069	1	1.29	.014	.05	.1	.02	1.7	<.1	<.05	4	<.5	15.0
L28+00N 4+00W	.3	18.0	3.2	46	.1	7.7	5.3	500	1.59	2.3	.2	<.5	.6	27	.1	.1	.1	44	.38	.072	2	12	.29	99	.093	3	1.33	.014	.09	.1	.02	2.0	<.1	<.05	4	<.5	15.0
L28+00N 3+00W	.2	83.8	4.8	46	<.1	8.6	5.9	441	1.82	1.5	.2	4.4	.8	31	.1	.1	.1	46	.46	.020	5	12	.35	88	.089	6	1.51	.025	.08	.1	.01	3.0	<.1	<.05	4	<.5	15.0
L28+00N 2+00W	.4	9.4	2.8	27	<.1	5.6	3.6	514	1.18	.8	.2	.9	.6	22	<.1	.1	.1	32	.25	.029	2	10	.17	105	.078	1	.93	.013	.10	.1	.01	1.6	<.1	<.05	3	<.5	15.0
RE L28+00N 2+00W	.5	9.3	2.7	27	<.1	5.2	3.6	515	1.15	.8	.2	.6	.6	21	.1	.1	.1	31	.23	.029	2	9	.16	103	.074	1	.89	.012	.10	.1	.01	1.5	<.1	<.05	3	<.5	15.0
L28+00N 1+00W	.2	8.2	3.1	49	<.1	5.7	3.0	446	1.12	1.2	.1	<.5	.6	19	.1	<.1	.1	27	.26	.130	2	7	.11	111	.067	1	1.15	.018	.04	.1	.02	1.2	<.1	<.05	4	<.5	15.0
L28+00N 0+50E	.3	10.4	3.3	41	<.1	5.7	3.6	812	1.27	1.0	.2	10.2	.6	25	.1	.1	.1	34	.33	.029	2	11	.16	123	.081	2	1.22	.016	.08	.1	.02	1.6	<.1	<.05	4	<.5	15.0
L28+00N 1+50E	.4	21.2	5.3	49	<.1	11.6	7.1	820	2.04	2.0	.3	3.8	1.0	35	.1	.1	.1	55	.43	.067	4	16	.32	149	.108	2	2.27	.014	.10	.1	.02	2.7	.1	<.05	7	<.5	15.0
L28+00N 2+50E	.2	7.5	2.4	51	<.1	5.9	2.8	380	1.10	.6	.1	.8	.5	20	.1	<.1	.1	26	.22	.062	2	7	.13	125	.065	1	1.08	.016	.06	.1	.01	1.2	<.1	<.05	4	<.5	15.0
L28+00N 3+50E	.3	53.8	2.8	41	<.1	12.2	9.0	590	2.34	1.5	.4	4.9	1.2	53	.1	.1	.1	76	.74	.043	6	20	.42	104	.132	4	1.52	.015	.20	.1	.01	5.0	<.1	<.05	5	<.5	15.0
L28+00N 4+50E	.4	11.3	3.3	43	<.1	6.2	3.6	560	1.25	.7	.1	1.5	.5	27	<.1	.1	.1	36	.31	.023	2	12	.20	88	.087	2	.98	.016	.08	.1	.01	1.8	<.1	<.05	3	<.5	15.0
L28+00N 5+50E	.4	14.4	3.0	82	<.1	6.6	3.6	836	1.27	.8	.2	<.5	.7	29	.1	.1	.1	34	.33	.028	2	12	.17	113	.083	2	1.20	.015	.07	.1	.01	1.9	<.1	<.05	4	<.5	15.0
L28+00N 6+50E	.5	28.2	3.2	80	<.1	10.1	8.0	998	2.08	1.3	.3	2.3	1.0	38	.1	.1	.1	65	.52	.032	4	17	.32	127	.131	3	1.40	.015	.11	.1	.02	3.7	<.1	<.05	4	<.5	15.0
L28+00N 8+50E	.8	23.2	3.8	111	<.1	10.2	5.9	766	1.46	4.8	.3	1.1	.7	17	.2	.1	.3	31	.20	.207	3	9	.19	172	.070	1	1.60	.021	.04	.2	.03	1.7	<.1	<.05	5	<.5	7.5
L28+00N 9+50E	1.6	90.5	4.2	44	<.1	22.5	12.3	501	2.73	6.5	.5	5.2	1.8	47	.1	.4	.3	82	.66	.090	8	28	.69	124	.088	2	1.35	.014	.12	.2	.04	5.0	.1	<.05	4	<.5	7.5
L26+00N 10+00W	1.8	40.5	5.0	77	<.1	8.1	8.4	729	2.45	6.3	.4	9.3	1.0	27	.3	.5	.1	55	.43	.058	6	11	.31	95	.056	4	1.32	.014	.16	.1	.02	3.6	.1	<.05	4	<.5	15.0
L26+00N 9+00W	.6	36.7	3.9	55	<.1	11.2	9.3	618	2.59	3.6	.3	.9	1.0	31	.1	.1	.1	73	.39	.061	4	16	.47	94	.100	3	2.03	.018	.10	.1	.01	4.2	<.1	<.05	7	<.5	15.0
STANDARD DS7	20.6	108.7	70.1	408	.9	55.9	9.5	623	2.38	47.6	4.9	67.3	4.4	68	6.3	5.9	4.4	85	.91	.079	12	174	1.05	370	.121	38	.96	.076	.43	3.9	.20	2.4	4.2	.20	4	3.4	15.0

GROUP 1DX - 15.0 GM SAMPLE LEACHED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 300 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data [illegible] FA ____ DATE RECEIVED: JUL 27 2006 DATE REPORT MAILED:................

BRITISH COLUMBIA CERTIFIED ASSAYER
Raymond Chan

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
G-1	.1	1.9	2.7	39	<.1	3.1	3.7	465	1.85	<.5	2.1	.7	3.6	63	<.1	<.1	.1	35	.52	.074	7	7	.49	186	.107	1	.89	.103	.43	.1	<.01	2.3	.3	<.05	4	<.5	15.0
L26+00N 8+00W	.5	36.4	4.2	68	<.1	9.6	9.4	843	2.93	1.8	.4	.8	.8	42	.1	.1	.1	98	.49	.039	3	20	.59	92	.129	4	1.60	.013	.12	.1	.02	3.4	.1	<.05	6	<.5	15.0
L26+00N 7+00W	.2	22.9	3.6	22	<.1	7.6	7.6	272	2.00	1.0	.2	.5	.6	41	<.1	.1	.1	49	.64	.017	2	24	.44	85	.080	5	1.28	.024	.08	<.1	.01	3.2	<.1	<.05	4	<.5	15.0
L26+00N 6+00W	.2	11.6	4.3	48	<.1	11.8	6.1	564	1.65	1.0	.2	.8	.5	24	.1	.1	.1	45	.29	.035	2	39	.41	91	.077	2	.95	.013	.06	.1	.02	1.5	<.1	<.05	4	<.5	15.0
L26+00N 5+00W	.5	9.6	3.5	62	<.1	5.4	4.5	835	1.15	1.1	.1	.7	.4	17	.1	<.1	.1	29	.25	.072	1	9	.22	134	.046	2	.87	.012	.09	.1	.02	1.1	<.1	<.05	3	<.5	7.5
L26+00N 4+00W	1.1	15.2	5.2	126	<.1	6.3	5.3	2866	1.26	2.1	.1	<.5	.5	35	.3	.1	.1	35	.66	.087	2	11	.24	305	.063	4	.99	.017	.10	.1	.05	2.1	<.1	<.05	4	<.5	7.5
L26+00N 3+00W	.5	16.0	4.0	66	<.1	8.1	5.6	850	1.60	1.7	.2	1.1	.7	21	.2	.1	.1	42	.27	.080	2	15	.29	119	.077	2	1.15	.014	.08	.1	.01	2.2	<.1	<.05	4	<.5	7.5
L26+00N 2+00W	.3	16.7	3.7	44	<.1	8.2	5.4	465	1.65	1.3	.2	1.0	.8	22	.1	.1	.1	42	.25	.047	3	16	.27	95	.080	2	1.17	.015	.08	.1	.01	2.2	<.1	<.05	4	<.5	7.5
L26+00N 1+00W	.3	9.8	3.3	38	<.1	7.4	4.5	386	1.51	.9	.2	.6	.7	23	<.1	.1	.1	39	.27	.027	2	18	.24	71	.092	1	.99	.017	.12	.1	.01	1.7	<.1	<.05	4	<.5	15.0
L26+00N 0+00	.3	12.8	3.2	30	<.1	6.4	3.5	375	1.25	1.1	.2	.5	.6	22	<.1	.1	.1	30	.26	.036	2	13	.16	92	.075	2	1.08	.018	.07	.1	.01	1.5	<.1	<.05	4	<.5	15.0
L26+00N 1+00E	.3	13.4	2.9	48	<.1	5.8	3.4	553	1.30	.6	.1	7.1	.5	24	.1	.1	.1	34	.31	.024	2	14	.14	84	.079	2	.87	.016	.09	.1	.01	1.8	<.1	<.05	3	<.5	15.0
L26+00N 3+00E	.2	10.3	2.6	106	<.1	4.4	3.4	540	1.11	1.0	.1	.7	.5	29	.2	.1	.1	33	.44	.053	2	8	.18	99	.069	6	.88	.018	.10	<.1	.02	1.8	<.1	<.05	3	<.5	7.5
L26+00N 4+00E	.3	13.1	2.9	17	<.1	6.0	5.7	316	1.44	.7	.2	.6	.4	28	.1	.1	.1	46	.39	.012	2	17	.24	55	.088	2	.79	.017	.07	.1	.01	2.0	<.1	<.05	3	<.5	15.0
L26+00N 5+00E	.3	14.3	3.0	47	<.1	7.6	4.4	405	1.52	1.0	.2	.7	.7	25	.1	.1	.1	41	.29	.034	2	17	.21	97	.082	2	1.09	.014	.09	.1	.01	1.9	<.1	<.05	4	<.5	15.0
L26+00N 6+00E	.3	16.6	3.0	73	<.1	7.9	4.3	578	1.64	1.1	.2	1.3	.8	28	.1	.1	.1	43	.34	.025	3	18	.20	131	.090	3	1.16	.017	.11	.1	.01	2.5	<.1	<.05	4	<.5	15.0
L26+00N 7+00E	.3	21.0	2.9	50	<.1	10.4	6.5	389	1.93	.8	.2	.6	1.0	32	.1	.1	.1	59	.46	.020	4	25	.31	85	.122	3	1.06	.020	.19	<.1	.01	3.2	<.1	<.05	4	<.5	15.0
L26+00N 8+00E	.3	22.0	3.3	76	<.1	9.6	5.7	832	1.82	1.5	.2	.9	.9	28	.1	.1	.1	50	.39	.025	4	21	.25	143	.100	3	1.10	.016	.19	.1	.01	3.0	<.1	<.05	4	<.5	7.5
L26+00N 9+00E	.9	32.8	4.6	73	<.1	12.0	8.5	1141	1.92	2.1	.3	23.9	1.3	32	.2	.1	.4	44	.42	.030	6	18	.32	219	.075	2	1.37	.015	.15	.2	.02	3.0	.1	<.05	5	<.5	15.0
RE L24+00 1+50E	.4	6.3	2.8	37	<.1	4.1	3.1	349	1.09	.7	.1	<.5	.4	19	<.1	.1	.1	31	.25	.027	1	11	.14	66	.066	2	.71	.012	.08	.1	.02	1.1	<.1	<.05	3	<.5	15.0
L26+00N 10+00E	.5	17.6	3.3	56	<.1	8.4	4.7	501	1.46	1.9	.2	4.8	.7	19	.1	.1	.2	35	.24	.028	3	15	.19	144	.074	1	1.11	.016	.12	.1	.01	1.6	<.1	<.05	4	<.5	7.5
L24+00 0+50E	.2	17.9	2.9	62	<.1	7.4	3.9	436	1.47	1.1	.2	<.5	.7	23	.1	.1	.1	44	.36	.044	2	12	.19	105	.088	3	1.19	.015	.07	.1	.01	2.0	<.1	<.05	4	<.5	15.0
L24+00 1+50E	.4	6.2	2.9	38	<.1	4.2	3.2	348	1.10	.7	.1	1.9	.4	19	<.1	.1	.1	31	.25	.027	1	11	.14	66	.069	2	.71	.011	.08	.1	.01	1.2	<.1	<.05	3	<.5	15.0
L24+00 2+50E	.2	3.6	2.6	46	<.1	3.7	2.2	489	.77	.7	.1	<.5	.4	9	<.1	<.1	.1	19	.11	.115	1	4	.05	75	.048	<1	.62	.015	.04	.1	.01	.6	<.1	<.05	3	<.5	15.0
L24+00 3+50E	.2	8.1	2.7	30	<.1	6.6	3.8	166	1.40	1.1	.1	.5	.6	16	<.1	.1	.1	35	.19	.090	2	14	.15	102	.072	1	1.07	.015	.05	<.1	.01	1.4	<.1	<.05	4	<.5	15.0
L24+00 4+50E	.4	16.0	3.1	67	<.1	5.9	4.0	1023	1.24	1.3	.1	.7	.6	19	.1	.1	.1	34	.25	.066	2	12	.16	118	.069	2	.99	.014	.06	<.1	.02	1.5	<.1	<.05	4	<.5	15.0
L24+00 5+50E	.2	10.8	2.9	38	<.1	6.2	4.2	609	1.48	.7	.2	2.4	.5	28	.1	.1	.2	45	.34	.025	2	17	.18	82	.087	2	.90	.015	.06	.1	.01	1.6	<.1	<.05	4	<.5	15.0
L24+00 8+00E	.3	39.5	3.6	54	<.1	11.9	7.3	512	2.08	1.7	.3	1.7	1.4	30	.1	.1	.2	55	.39	.026	6	26	.33	125	.099	3	1.16	.013	.21	.1	.01	3.5	.1	<.05	4	<.5	15.0
L24+00 9+00E	.8	23.1	5.7	63	<.1	8.4	6.3	590	1.62	2.4	.2	2.5	.8	20	.1	.1	.3	42	.28	.036	3	17	.21	130	.070	2	1.05	.012	.11	.2	.02	1.9	.1	<.05	4	<.5	15.0
L24+00 10+00E	4.8	105.4	5.8	59	<.1	21.2	13.4	569	2.96	5.8	.5	3.3	1.8	32	.1	.2	.6	83	.52	.103	6	36	.71	143	.091	1	1.51	.011	.18	.8	.02	4.7	.1	<.05	5	<.5	15.0
L22+00N 9+50W	1.5	159.9	5.7	135	.1	7.3	5.7	1010	1.34	2.9	.5	1.1	.3	122	4.1	.4	.1	32	4.84	.089	6	8	.34	64	.038	44	.91	.018	.08	<.1	.06	1.9	.2	.08	3	1.9	7.5
L22+00N 8+50W	.6	36.6	4.8	95	<.1	9.6	8.9	1005	2.49	4.2	.4	<.5	1.0	38	.2	.2	.1	67	.55	.039	5	18	.41	89	.106	5	1.89	.013	.14	.1	.02	3.8	.1	<.05	7	<.5	7.5
L22+00N 7+50W	.5	20.6	4.0	57	<.1	10.2	6.9	536	1.82	3.0	.3	<.5	.7	34	.1	.1	.1	51	.43	.042	3	21	.34	74	.089	3	1.37	.015	.07	.1	.02	2.4	<.1	<.05	5	<.5	7.5
L22+00N 6+50W	.4	14.2	3.6	72	<.1	5.9	4.4	552	1.38	1.9	.2	<.5	.8	17	.1	<.1	.1	34	.22	.172	2	13	.20	165	.066	1	1.34	.013	.04	.1	.02	1.7	<.1	<.05	6	<.5	15.0
L22+00N 5+50W	.6	13.1	3.7	47	<.1	8.5	6.4	783	1.64	1.3	.2	<.5	.4	29	.1	.1	.1	52	.37	.030	2	28	.37	102	.106	3	1.02	.013	.07	.1	.02	2.5	<.1	<.05	4	<.5	7.5
L22+00N 4+50W	.4	12.5	3.5	38	<.1	8.8	5.0	214	1.48	1.1	.2	<.5	.7	17	.1	.1	.1	37	.18	.109	2	17	.24	109	.071	2	1.16	.016	.06	.1	.01	1.8	<.1	<.05	4	<.5	15.0
STANDARD DS7	21.4	111.8	71.2	418	.9	58.1	9.9	628	2.44	48.6	5.0	83.4	4.5	71	6.5	6.1	4.5	88	.94	.080	13	220	1.06	375	.127	39	.98	.079	.45	3.9	.20	2.5	4.3	.21	5	3.7	15.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
G-1	.2	2.2	3.4	41	<.1	3.6	3.8	490	1.92	<.5	2.3	1.2	3.8	81	<.1	<.1	.1	39	.61	.080	7	7	.54	208	.127	1	1.10	.154	.54	.1	<.01	3.7	.3	<.05	5	<.5	15.0
L22+00N 3+50W	.3	19.0	3.4	82	<.1	6.6	5.5	989	1.75	1.9	.2	.7	.7	40	.2	.1	.1	54	.65	.063	2	9	.34	177	.095	6	1.33	.017	.14	.1	.03	2.5	<.1	<.05	4	<.5	15.0
L22+00N 2+50W	.3	12.2	3.6	66	<.1	7.6	4.6	462	1.54	1.6	.2	1.5	.7	21	.1	.1	.1	41	.25	.044	2	12	.24	108	.084	3	1.26	.018	.08	.1	.01	1.7	<.1	<.05	4	<.5	15.0
L22+00N 1+50W	.3	44.0	3.2	49	<.1	9.4	7.3	395	2.21	1.9	.3	<.5	1.1	33	.1	.1	.1	62	.37	.043	4	14	.44	81	.108	3	1.39	.016	.10	.1	.02	3.5	.1	<.05	4	<.5	7.5
L22+00N 0+50W	.4	16.7	4.5	38	<.1	7.2	5.0	387	1.53	2.1	.2	.9	.8	27	.1	.1	.1	50	.34	.036	2	10	.29	109	.100	4	1.31	.017	.05	.1	.01	2.3	<.1	<.05	4	<.5	15.0
L22+00N 0+50E	1.6	15.2	16.7	109	<.1	4.0	2.5	2230	.47	2.4	.1	1.3	.2	69	.5	.3	.1	14	2.08	.063	1	4	.15	192	.026	16	.41	.007	.14	.1	.24	1.1	<.1	.11	1	.5	15.0
L22+00N 2+00E	.2	4.8	2.6	48	<.1	4.6	2.3	206	.93	.7	.1	<.5	.4	16	<.1	.1	.1	26	.20	.050	1	6	.09	69	.060	2	.76	.016	.08	<.1	.02	1.0	<.1	<.05	3	<.5	15.0
L22+00N 3+00E	.2	2.9	2.9	34	<.1	1.9	1.9	207	.84	.6	.1	<.5	.4	13	<.1	<.1	.1	21	.18	.214	1	3	.05	159	.050	1	.61	.017	.03	<.1	.02	.8	<.1	<.05	3	<.5	15.0
L22+00N 7+00E	.5	35.0	6.0	61	<.1	7.4	6.3	1949	1.58	1.7	.2	.9	1.0	65	.2	.1	.1	37	1.29	.197	5	9	.31	187	.067	6	1.64	.012	.12	.1	.05	2.9	.1	<.05	5	<.5	7.5
L22+00N 8+50E	.4	9.4	3.0	66	<.1	6.2	3.4	307	1.35	1.1	.1	.7	.5	14	<.1	<.1	.2	31	.19	.021	2	8	.14	115	.068	2	1.14	.019	.11	.1	.01	1.1	<.1	<.05	4	<.5	15.0
L22+00N 9+50E	.7	15.7	4.2	135	<.1	10.4	5.9	1209	1.62	2.1	.2	<.5	1.3	16	.2	.1	.3	38	.19	.048	3	11	.21	214	.081	2	1.59	.018	.08	.2	.02	1.7	.1	<.05	5	<.5	15.0
L20+00N 10+00W	.9	49.8	6.6	108	<.1	9.5	9.4	1543	2.54	3.6	.6	<.5	1.3	31	.3	.2	.1	78	.38	.061	6	10	.48	160	.108	2	2.59	.015	.10	.1	.01	3.5	.4	<.05	8	<.5	15.0
L20+00N 9+00W	.7	73.6	5.5	57	<.1	9.9	11.1	556	2.87	3.0	.6	<.5	1.2	36	.2	.2	.1	98	.73	.079	5	12	.79	58	.123	5	2.29	.024	.19	.1	.02	4.4	.1	<.05	8	<.5	7.5
L20+00N 8+00W	.8	79.1	7.4	49	.2	8.2	8.6	529	2.01	4.7	.5	.9	.5	375	1.6	.3	.1	70	5.69	.038	5	10	1.22	101	.072	27	1.17	.071	.10	.1	.03	3.0	.1	.06	4	1.1	15.0
L20+00N 7+00W	.6	47.6	3.0	36	.1	4.1	3.8	332	1.14	1.0	.5	.9	.3	200	.9	.1	.1	31	12.33	.123	3	7	.30	57	.051	35	.94	.018	.04	<.1	.02	1.5	<.1	.11	3	1.6	15.0
L20+00N 6+00W	.3	17.7	3.4	64	<.1	7.7	5.8	715	1.93	1.5	.2	<.5	.6	34	.1	.1	.1	54	.45	.053	2	16	.35	93	.099	6	1.26	.012	.16	.1	.01	2.6	<.1	<.05	5	<.5	15.0
L20+00N 5+00W	.4	4.0	2.9	49	<.1	3.6	2.8	400	1.03	1.4	.1	<.5	.6	11	.1	<.1	.1	27	.13	.225	1	5	.10	116	.062	2	.81	.014	.04	.1	.02	1.0	<.1	<.05	4	<.5	15.0
L20+00N 4+00W	.3	7.1	3.1	82	<.1	5.7	3.8	612	1.34	1.4	.1	<.5	.4	17	.1	.1	.1	38	.28	.050	1	8	.19	108	.070	2	.95	.011	.09	.1	.02	1.3	<.1	<.05	4	<.5	15.0
L20+00N 3+00W	.4	9.5	2.8	87	<.1	6.6	5.4	906	1.55	1.5	.1	4.4	.4	25	.1	.1	<.1	46	.40	.104	1	10	.35	142	.072	5	.95	.014	.13	<.1	.02	1.8	<.1	<.05	4	<.5	15.0
L20+00N 1+50W	.4	14.7	2.5	28	<.1	4.7	4.1	205	1.46	.9	.1	<.5	.3	18	<.1	.1	<.1	50	.32	.042	1	7	.20	50	.090	3	.94	.013	.05	.1	.02	1.8	<.1	<.05	4	<.5	15.0
L20+00N 0+50W	.5	33.9	5.0	49	<.1	9.3	8.2	627	2.10	2.2	.3	1.0	1.0	32	.1	.1	.1	76	.46	.063	3	10	.50	144	.112	3	2.02	.013	.07	.1	.02	3.1	.1	<.05	6	<.5	15.0
L20+00N 1+00E	.4	39.2	5.6	53	<.1	10.9	8.4	822	2.28	1.3	.3	1.8	1.0	33	.1	.1	.1	68	.50	.038	4	14	.40	120	.133	2	2.53	.012	.09	.1	.03	3.1	.1	<.05	8	<.5	15.0
L20+00N 2+00E	.6	36.8	5.7	55	<.1	12.5	7.3	583	2.02	1.8	.5	1.4	1.5	25	.1	.1	.1	54	.25	.087	4	15	.35	145	.109	1	2.45	.017	.05	.1	.02	2.6	.1	<.05	7	<.5	15.0
RE L20+00N 2+00E	.6	36.5	5.7	55	<.1	13.5	7.5	612	2.13	1.8	.5	1.7	1.5	25	.1	.2	.1	57	.24	.087	4	15	.35	142	.111	1	2.48	.015	.06	.1	.02	2.8	.1	<.05	8	<.5	15.0
L20+00N 3+00E	.4	9.1	2.7	65	<.1	4.8	3.1	900	1.12	.9	.1	<.5	.5	28	.1	.1	.1	29	.39	.026	2	8	.16	123	.069	4	.94	.011	.13	.1	.02	1.7	<.1	<.05	3	<.5	15.0
L20+00N 4+50E	.2	19.3	3.9	58	<.1	8.2	5.5	486	1.66	1.2	.2	3.8	.7	26	.1	.1	.1	50	.37	.026	2	12	.25	96	.102	3	1.30	.012	.10	.1	.01	2.2	.1	<.05	4	<.5	15.0
L20+00N 5+50E	.2	5.1	2.2	38	<.1	3.2	2.3	352	.89	.5	.1	.9	.3	20	.1	<.1	<.1	24	.27	.053	1	5	.09	85	.056	2	.69	.015	.07	<.1	.01	1.0	<.1	<.05	3	<.5	15.0
L20+00N 6+50E	.2	27.9	2.9	37	<.1	5.9	6.2	490	1.67	1.8	.1	1.7	.7	56	.2	.1	.1	41	.70	.056	3	9	.22	72	.090	7	1.07	.014	.23	.1	.02	2.6	<.1	<.05	4	<.5	15.0
L20+00N 7+50E	.2	52.7	3.0	17	<.1	4.5	2.6	318	.61	2.0	.2	1.1	.1	237	.1	.1	<.1	21	17.33	.151	2	5	.53	85	.016	14	.41	.016	.04	<.1	.03	.4	<.1	.08	1	1.0	15.0
L20+00N 8+50E	.4	11.6	3.2	108	<.1	8.7	4.7	504	1.41	1.2	.2	.5	.7	16	.1	.1	.1	32	.23	.113	2	10	.18	166	.072	2	1.17	.016	.11	.1	.01	1.8	<.1	<.05	4	<.5	15.0
L20+00N 9+50E	.9	80.9	7.0	81	<.1	19.7	15.1	1434	2.77	3.7	.5	2.3	1.5	48	.3	.2	.4	63	.86	.072	9	20	.55	346	.085	3	1.78	.014	.29	.4	.04	4.7	.1	<.05	6	<.5	7.5
L18+00N 10+00W	.4	44.3	9.2	116	<.1	8.2	8.1	2029	2.04	2.3	.4	.6	1.2	37	.4	.1	.1	60	.56	.156	5	8	.44	179	.065	4	2.08	.016	.12	.1	.04	2.3	.1	<.05	7	<.5	7.5
L18+00N 9+00W	.6	5.2	4.4	44	<.1	3.0	2.9	389	.91	1.1	.1	<.5	.3	12	<.1	<.1	.1	25	.21	.097	1	4	.12	54	.056	3	.66	.011	.06	<.1	.03	.8	<.1	<.05	4	<.5	15.0
L18+00N 8+00W	.4	121.0	8.7	185	<.1	7.9	5.7	786	1.77	3.7	.2	.7	.9	31	.3	.2	.1	46	.33	.099	3	10	.28	117	.072	4	1.68	.012	.15	<.1	.01	2.2	.1	<.05	6	<.5	15.0
L18+00N 7+00W	1.1	21.9	4.8	90	<.1	7.6	4.9	489	1.77	4.1	.2	.6	.7	21	.2	.2	.1	46	.27	.059	3	10	.28	76	.071	3	1.43	.015	.12	.1	.01	2.1	.1	<.05	6	<.5	15.0
STANDARD DS7	20.7	110.0	70.2	411	.9	56.4	9.6	621	2.39	47.3	4.9	73.4	4.4	70	6.3	5.9	4.5	86	.92	.079	12	175	1.04	369	.123	38	.96	.077	.43	3.9	.20	2.5	4.1	.20	5	3.3	15.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

ACME ANALYTICAL

Max Investment Inc. PROJECT Kentucky Lake FILE # A604334

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
G-1	.3	3.3	3.7	41	<.1	3.6	4.0	515	2.03	<.5	2.5	2.5	4.2	91	<.1	<.1	.1	41	.66	.076	10	7	.54	217	.138	1	1.17	.179	.54	.1	<.01	4.2	.4	<.05	5	<.5	15.0
L18+00N 6+00W	.7	61.5	8.3	113	<.1	11.7	11.1	1345	2.87	5.3	.6	1.0	1.5	37	1.2	.3	.1	81	.56	.088	7	15	.49	160	.124	12	2.81	.021	.13	.1	.03	3.7	.2	<.05	9	<.5	15.0
L18+00N 5+00W	.6	129.4	5.2	82	.2	5.5	15.4	1932	2.40	7.2	.4	14.6	.5	52	.3	.1	.1	73	.59	.187	6	7	.56	130	.095	3	1.60	.015	.05	.1	.09	3.5	.1	<.05	7	<.5	7.5
L18+00N 4+00W	.5	24.0	1.9	3	<.1	5.1	2.2	274	.63	1.9	1.2	2.0	<.1	84	.1	.2	<.1	101	5.52	.076	<1	2	.21	89	.004	43	.09	.028	.02	.1	.10	.3	<.1	.23	<1	1.0	7.5
L18+00N 2+00W	.3	18.9	3.2	97	<.1	5.9	5.2	906	1.69	1.4	.2	.6	.6	34	.1	.1	.1	53	.47	.056	2	8	.26	115	.106	4	1.36	.020	.08	.1	.02	2.3	<.1	<.05	5	<.5	7.5
L18+00N 1+00W	.5	41.3	11.1	81	<.1	6.4	5.1	2648	1.41	3.3	.2	.9	.5	33	.4	.2	.2	40	.57	.118	3	6	.20	270	.072	3	1.13	.015	.06	.1	.16	1.4	.1	<.05	5	<.5	7.5
L18+00N 0+00	.3	285.3	5.1	49	<.1	5.7	5.0	1002	1.35	1.5	.3	1.3	.7	28	.2	.1	.1	38	.75	.188	4	7	.30	274	.068	4	1.32	.014	.07	.1	.05	2.7	<.1	<.05	4	<.5	.5
RE L18+00N 0+00	.3	281.6	5.1	49	<.1	5.6	5.1	991	1.34	1.5	.3	.6	.7	28	.2	.1	.1	38	.76	.183	4	7	.30	276	.068	4	1.32	.014	.07	.1	.05	2.7	<.1	<.05	4	<.5	.5
L18+00N 1+00E	.1	181.9	2.6	15	.1	8.2	4.0	308	1.12	2.3	.3	4.9	.5	201	.1	.2	.1	27	11.40	.105	5	9	.81	205	.042	4	1.42	.026	.04	.1	.07	2.5	<.1	<.05	4	.5	7.5
L18+00N 3+00E	.3	6.9	2.7	87	<.1	5.4	3.0	471	1.10	<.5	.1	<.5	.4	21	.1	<.1	<.1	31	.27	.060	1	8	.11	104	.070	2	.87	.022	.06	.1	.02	1.6	<.1	<.05	3	<.5	15.0
L18+00N 4+00E	.4	6.3	2.6	56	<.1	3.3	2.3	556	.84	1.0	.1	<.5	.5	21	.1	<.1	<.1	24	.27	.127	1	4	.08	138	.055	2	.60	.020	.06	<.1	.02	1.0	<.1	<.05	3	<.5	15.0
L18+00N 6+50E	.4	72.1	8.6	60	<.1	13.7	10.5	1134	2.80	3.7	.4	2.3	1.3	51	.2	.2	.1	82	.69	.045	6	25	.46	131	.152	4	2.11	.016	.14	.1	.03	5.2	.1	<.05	6	<.5	15.0
L18+00N 8+00E	.3	28.8	4.9	55	<.1	8.6	6.5	695	2.02	1.6	.2	<.5	.7	38	.1	.1	.1	59	.54	.043	3	13	.31	128	.110	4	1.27	.017	.13	.1	.02	2.5	<.1	<.05	4	<.5	15.0
L18+00N 9+00E	.6	84.1	4.2	67	<.1	18.1	11.1	523	2.50	3.4	.4	2.2	1.3	62	.1	.1	.2	71	.56	.124	6	20	.56	114	.103	3	1.71	.017	.14	.1	.02	4.2	.1	<.05	5	<.5	7.5
L18+00N 10+00E	1.2	84.2	6.3	74	<.1	18.4	14.4	1231	2.84	3.5	.5	4.6	1.7	57	.2	.2	.5	69	.73	.054	10	21	.49	308	.102	4	1.68	.017	.32	.4	.03	5.2	.1	<.05	5	<.5	15.0
L16+00N 8+50W	.6	72.8	6.1	65	<.1	12.2	10.7	843	3.22	3.3	.8	1.7	1.7	50	.2	.2	.1	107	.59	.032	8	18	.57	110	.174	3	2.76	.022	.13	.1	.02	5.9	.1	<.05	9	<.5	15.0
L16+00N 7+00W	.4	53.1	6.4	56	<.1	8.7	8.5	896	2.41	2.3	.5	.5	1.3	37	.1	.1	.1	74	.49	.032	5	12	.53	118	.116	4	2.95	.021	.08	.1	.01	3.9	.1	<.05	8	<.5	15.0
L16+00N 6+00W	2.9	137.1	96.6	236	.9	13.1	12.7	1107	1.70	16.4	1.1	1.9	.7	37	5.6	3.4	.1	37	1.86	.084	7	7	.23	129	.038	5	1.21	.013	.11	.1	.16	3.2	.6	<.05	3	<.5	7.5
L16+00N 5+00W	1.4	15.1	6.1	111	<.1	9.1	5.6	1999	1.37	1.6	.2	<.5	.4	31	.2	.1	.1	39	.41	.060	2	12	.24	123	.075	3	.99	.016	.06	.1	.04	1.5	<.1	<.05	4	<.5	15.0
L16+00N 4+00W	.7	26.4	8.0	57	<.1	4.5	4.5	1187	1.24	1.2	.1	<.5	.3	24	.1	.1	.1	36	.35	.032	1	5	.19	77	.063	6	.84	.017	.07	<.1	.03	1.3	<.1	<.05	4	<.5	7.5
L16+00N 3+00W	.2	25.5	3.4	21	<.1	6.0	4.3	198	1.36	1.2	.2	.5	.6	54	.1	.1	.1	35	.66	.022	2	7	.27	53	.074	21	1.20	.029	.07	<.1	.02	2.0	<.1	<.05	4	<.5	15.0
L16+00N 2+00W	.4	14.8	7.7	68	<.1	9.9	5.9	1175	1.82	1.5	.3	.7	.9	17	.2	.1	.1	53	.24	.093	4	11	.27	122	.116	2	1.48	.024	.05	.1	.02	1.8	.1	<.05	5	<.5	15.0
L16+00N 1+00W	.3	93.3	4.1	58	<.1	7.5	12.4	857	2.93	1.6	.5	4.9	1.2	41	.1	.1	.1	87	.58	.029	6	7	.61	116	.159	4	2.22	.016	.15	.1	.02	5.7	.1	<.05	7	<.5	15.0
L16+00N 0+50E	.4	13.3	3.2	45	<.1	5.7	4.1	700	1.28	.8	.1	.6	.5	21	.1	.1	.1	37	.33	.040	2	8	.18	137	.081	3	1.09	.014	.09	.1	.02	1.8	<.1	<.05	4	<.5	15.0
L16+00N 2+50E	.5	22.8	4.1	126	<.1	8.0	5.6	1685	1.75	.9	.1	2.2	.7	37	.1	.1	.1	54	.39	.066	3	10	.23	209	.103	3	1.40	.022	.12	.1	.02	2.7	<.1	<.05	5	<.5	15.0
L16+00N 4+00E	.4	20.7	5.3	99	<.1	10.9	5.8	1682	1.75	1.8	.2	.8	.7	33	.2	.1	.1	48	.40	.126	3	11	.24	255	.098	3	1.73	.016	.09	.1	.04	1.9	.1	<.05	6	<.5	15.0
L16+00N 5+00E	.1	9.9	2.0	64	<.1	2.7	2.4	540	.86	.5	<.1	<.5	.3	26	.2	<.1	<.1	23	.27	.042	1	4	.08	83	.052	2	.60	.018	.07	<.1	.01	1.3	<.1	<.05	3	<.5	15.0
L16+00N 6+50E	.3	25.0	3.2	78	<.1	5.0	3.9	442	1.42	.6	.1	2.0	.5	25	.1	.1	.1	46	.45	.037	1	7	.17	65	.091	4	.98	.015	.09	<.1	.01	1.6	<.1	<.05	4	<.5	15.0
L16+00N 7+50E	.3	57.5	3.2	58	<.1	9.4	6.4	824	2.03	1.5	.2	1.0	1.0	44	.1	.1	.1	56	.62	.035	4	15	.32	126	.109	6	1.32	.015	.20	.1	.02	3.6	<.1	<.05	4	<.5	15.0
L16+00N 8+50E	.3	22.7	2.9	95	.1	5.9	3.2	647	1.20	1.0	.1	347.1	.4	40	.1	.1	.1	33	.43	.059	2	8	.15	168	.062	3	.86	.019	.14	.1	.02	1.8	<.1	<.05	3	<.5	15.0
L16+00N 9+50E	1.1	72.5	4.9	71	<.1	14.9	10.7	1006	2.56	3.5	.3	5.0	1.4	31	.1	.2	.5	61	.55	.037	5	17	.45	262	.106	3	1.95	.017	.22	.3	.02	4.2	.1	<.05	6	<.5	15.0
L14+00N 10+00W	.4	182.0	6.5	106	.1	6.2	10.5	1044	2.66	3.7	.3	1.0	1.4	81	.2	.2	.1	70	.70	.081	8	7	.42	142	.094	5	2.55	.018	.25	.1	.02	5.2	.1	<.05	8	<.5	15.0
L14+00N 9+00W	.3	26.2	3.6	66	<.1	6.9	5.5	354	1.69	2.1	.3	1.2	.9	16	.1	.1	.1	45	.20	.180	3	7	.19	55	.085	2	1.73	.024	.05	.1	.02	1.8	.1	<.05	6	<.5	15.0
L14+00N 8+00W	.7	62.2	5.9	68	<.1	10.9	11.6	974	3.41	3.0	.5	1.8	1.1	57	.1	.2	.1	116	.53	.046	6	18	.66	131	.151	3	2.16	.011	.18	.1	.02	5.7	.1	<.05	8	<.5	15.0
L14+00N 7+00W	.4	44.3	6.2	67	<.1	10.4	9.3	798	2.59	2.7	.4	1.1	1.2	42	.1	.1	.1	75	.50	.044	4	15	.43	129	.112	4	2.38	.015	.12	.1	.02	3.0	.1	<.05	8	<.5	15.0
STANDARD DS7	20.8	111.2	70.7	419	.9	57.6	9.7	628	2.43	48.1	4.9	70.9	4.5	70	6.2	5.8	4.5	87	.93	.080	13	179	1.06	374	.125	39	.98	.078	.44	3.8	.20	2.5	4.2	.21	5	3.7	15.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
G-1	.3	2.5	3.2	41	<.1	3.5	3.7	493	1.92	<.5	2.3	2.1	3.9	85	<.1	<.1	.1	38	.60	.074	8	7	.53	234	.132	1	1.10	.184	.54	.1	<.01	4.4	.3	<.05	5	<.5	15.0
L14+00N 6+00W	.5	27.3	5.7	145	<.1	6.5	5.2	1439	1.63	1.5	.2	<.5	.7	26	.2	.1	.1	44	.27	.048	3	9	.21	180	.069	2	1.27	.016	.09	.1	.02	1.9	.1	<.05	4	<.5	15.0
L14+00N 5+00W	.9	56.8	13.9	155	<.1	9.1	10.2	1864	2.86	6.6	.5	.7	1.7	55	1.7	.5	.1	68	.90	.079	10	12	.35	206	.055	3	1.95	.011	.17	.1	.03	5.2	.4	<.05	6	<.5	7.5
L14+00N 4+00W	.6	26.9	5.3	184	<.1	5.8	6.5	2958	1.89	3.6	.2	<.5	.7	43	.5	.3	.1	50	.43	.149	5	6	.30	268	.047	4	1.42	.017	.09	.1	.03	3.7	.1	<.05	5	<.5	15.0
L14+00N 3+00W	.4	23.8	3.8	60	<.1	7.6	5.4	496	1.52	2.3	.2	.8	.8	21	.1	.1	.1	37	.27	.098	2	9	.28	117	.057	2	1.29	.013	.07	.1	.02	1.9	<.1	<.05	4	<.5	7.5
L14+00N 2+00W	.4	13.5	5.5	68	<.1	5.5	4.6	1508	1.28	2.6	.1	.6	.6	28	.2	.1	.1	29	.59	.173	2	6	.19	265	.044	3	1.10	.012	.08	.1	.06	1.4	<.1	<.05	4	<.5	7.5
L14+00N 1+00W	.6	29.1	4.4	88	<.1	5.5	6.8	691	2.10	1.7	.2	.6	.8	17	<.1	.1	.1	60	.27	.037	3	5	.38	230	.075	2	2.04	.018	.04	.1	.01	2.2	.1	<.05	7	<.5	15.0
L14+00N 0+00	.3	14.6	3.2	36	<.1	4.5	4.5	602	1.32	.8	.1	.8	.6	23	.1	.1	.1	36	.38	.027	2	8	.23	132	.068	1	.95	.012	.09	<.1	.02	2.0	<.1	<.05	3	<.5	7.5
L14+00N 1+00E	.3	58.1	5.2	82	<.1	9.1	6.5	1028	1.79	1.4	.3	1.4	1.0	25	.1	.1	.1	45	.35	.132	5	12	.27	251	.077	1	1.77	.014	.06	.1	.03	2.7	.1	<.05	5	<.5	15.0
L14+00N 2+00E	.3	37.6	3.4	50	<.1	9.3	7.1	755	1.99	1.4	.3	.8	.9	36	.1	.1	.1	54	.60	.089	5	14	.36	176	.075	5	1.29	.010	.20	.1	.02	3.1	<.1	<.05	4	<.5	15.0
RE L14+00N 2+00E	.3	38.2	3.2	51	<.1	9.6	7.5	767	2.06	1.6	.2	.9	1.0	35	.1	.1	.1	56	.62	.085	5	14	.36	176	.081	6	1.31	.011	.20	.1	.02	3.3	<.1	<.05	4	<.5	15.0
L14+00N 3+00E	.3	12.1	2.9	31	<.1	6.0	4.1	293	1.37	.9	.1	1.1	.5	19	<.1	.1	.1	39	.27	.022	2	13	.19	76	.087	1	.84	.013	.06	.1	.01	1.6	<.1	<.05	3	<.5	7.5
L14+00N 4+00E	.2	7.6	2.7	21	<.1	4.5	3.4	342	1.06	.7	.2	1.8	.5	19	<.1	.1	.1	31	.22	.024	2	10	.14	58	.070	1	.74	.013	.05	.1	.01	1.5	<.1	<.05	2	<.5	15.0
L14+00N 6+00E	.4	54.8	5.8	46	<.1	15.1	9.6	703	2.22	3.1	.4	1.6	1.1	47	.2	.2	.1	63	.61	.080	6	22	.45	135	.099	2	1.54	.010	.15	.1	.02	4.2	.1	<.05	5	<.5	15.0
L14+00N 7+00E	.3	9.6	3.0	89	.2	4.1	3.3	566	1.05	1.1	.1	.5	.4	22	.1	.1	.1	29	.32	.048	1	7	.13	74	.066	2	.79	.010	.10	.1	.02	1.3	<.1	<.05	3	<.5	15.0
L14+00N 8+00E	.2	19.1	2.3	51	<.1	3.7	2.7	164	1.03	1.6	.2	.5	.6	22	<.1	<.1	.1	25	.20	.255	2	5	.08	141	.058	1	.90	.017	.04	<.1	.02	1.1	<.1	<.05	3	<.5	15.0
L14+00N 9+00E	.2	21.2	2.7	46	<.1	6.3	4.5	348	1.62	.9	.2	1.5	.7	21	<.1	.1	.1	46	.34	.024	2	11	.22	74	.098	3	1.07	.014	.13	.1	.01	2.4	<.1	<.05	4	<.5	15.0
L14+00N 10+00E	.6	33.0	4.0	60	<.1	10.1	7.6	642	1.89	2.0	.2	1.4	1.2	24	.1	.1	.3	44	.36	.023	4	15	.31	184	.088	1	1.44	.014	.15	.2	.01	2.7	.1	<.05	5	<.5	15.0
L12+00N 9+50W	.8	51.3	4.5	33	<.1	5.2	8.3	513	2.23	1.8	.3	1.2	1.3	40	.1	.2	.1	56	.45	.036	6	8	.30	72	.090	4	1.45	.010	.15	.1	.01	4.1	<.1	<.05	5	<.5	15.0
L12+00N 8+50W	.5	145.3	7.9	138	<.1	9.0	8.6	2309	2.19	2.1	.4	.6	1.4	59	.4	.1	.1	56	.52	.124	7	12	.34	323	.091	3	2.26	.016	.21	.1	.04	4.0	.1	<.05	6	<.5	15.0
L12+00N 7+50W	.5	87.9	7.1	71	<.1	11.5	12.2	1316	2.85	3.9	.9	1.2	2.1	47	.3	.3	.1	82	.48	.046	12	17	.51	152	.127	2	2.68	.012	.19	.1	.02	6.5	.1	<.05	8	<.5	15.0
L12+00N 6+00W	.7	26.7	5.8	48	<.1	7.0	6.3	709	1.67	1.7	.3	2.7	.6	41	.1	.1	.1	49	.54	.041	3	13	.30	95	.080	2	1.19	.012	.11	.1	.03	2.2	<.1	<.05	4	<.5	7.5
L12+00N 4+50W	1.6	12.8	4.5	38	<.1	5.1	4.7	656	1.47	1.3	.2	.8	.6	20	.1	.1	.1	39	.30	.018	2	10	.22	72	.082	1	1.16	.013	.08	.1	.02	1.9	.1	<.05	4	<.5	15.0
L12+00N 3+50W	.5	31.0	5.1	63	<.1	13.1	8.1	550	2.23	2.7	.4	.5	1.1	29	.2	.2	.1	57	.38	.030	5	19	.42	144	.100	1	1.71	.014	.10	.1	.01	3.8	.1	<.05	5	<.5	15.0
L12+00N 2+50W	.5	23.8	6.3	70	<.1	5.8	6.6	1173	1.87	1.7	.2	<.5	.7	29	.3	.1	.1	47	.47	.035	4	9	.31	148	.066	2	1.35	.013	.12	.1	.02	2.7	.1	<.05	4	<.5	7.5
L12+00N 1+50W	.3	24.0	3.3	62	<.1	8.5	6.8	474	2.06	1.7	.2	<.5	.7	26	.1	.1	.1	61	.40	.027	3	12	.37	91	.108	2	1.36	.015	.10	.1	.01	2.8	.1	<.05	5	<.5	15.0
L12+00N 0+50W	.4	47.5	8.3	121	<.1	6.5	13.0	1859	2.68	2.2	.1	<.5	.7	75	.3	.2	.1	47	1.31	.096	6	5	.40	413	.055	7	1.46	.012	.30	<.1	.03	7.4	<.1	<.05	4	<.5	7.5
L12+00N 1+00E	.6	39.1	10.0	110	<.1	6.2	6.1	1709	1.75	1.9	.2	1.6	.9	44	.4	.1	.1	45	.45	.103	4	6	.33	298	.081	3	1.45	.018	.10	.1	.03	2.7	.1	<.05	5	<.5	15.0
L12+00N 2+00E	.2	23.5	3.0	56	<.1	5.8	3.3	348	1.34	.8	.2	3.2	.7	21	.1	.1	.1	38	.31	.022	2	10	.19	81	.096	4	1.03	.012	.11	.1	.01	1.7	<.1	<.05	3	<.5	15.0
L12+00N 3+00E	.3	49.0	3.5	47	<.1	12.2	7.7	283	2.17	1.6	.4	2.5	1.4	36	.1	.1	.1	64	.44	.058	4	17	.43	114	.124	2	1.82	.015	.07	.1	.01	3.5	.1	<.05	5	<.5	15.0
L12+00N 4+00E	.4	21.4	3.7	40	<.1	8.6	5.4	461	1.60	1.1	.2	.6	.8	27	.1	.1	.1	45	.35	.047	3	14	.25	95	.093	2	1.12	.015	.12	.1	.01	2.4	<.1	<.05	4	<.5	15.0
L12+00N 5+00E	.3	8.4	2.9	42	<.1	5.2	3.1	461	1.12	1.0	.1	.5	.5	20	.1	.1	.1	28	.31	.036	1	7	.14	88	.068	3	.93	.013	.13	.1	.01	1.4	<.1	<.05	3	<.5	7.5
L12+00N 6+00E	.2	14.0	2.7	61	<.1	5.3	3.6	457	1.41	.6	.1	3.0	.6	22	.1	.1	.1	41	.32	.016	2	11	.19	93	.096	2	.96	.014	.11	.1	.01	2.2	<.1	<.05	3	<.5	15.0
L12+00N 7+00E	.4	16.8	15.3	26	<.1	2.8	2.0	1193	.39	1.7	.1	1.3	.1	201	.2	.2	.1	11	3.54	.082	1	3	.30	294	.012	22	.40	.025	.17	<.1	.23	1.4	<.1	.12	1	.8	7.5
L12+00N 8+50E	.4	13.6	3.9	29	<.1	6.0	4.3	404	1.38	1.0	.2	2.6	.5	20	.1	.1	.1	41	.32	.026	2	13	.20	72	.076	2	.84	.013	.06	.1	.02	1.7	<.1	<.05	3	<.5	15.0
STANDARD DS7	20.9	108.6	69.1	410	.9	55.7	9.6	620	2.38	47.7	4.9	65.4	4.3	68	6.3	5.8	4.5	86	.91	.079	12	171	1.04	367	.120	38	.95	.076	.44	3.7	.20	2.4	4.2	.20	4	3.3	15.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
G-1	.2	2.2	2.5	43	<.1	3.4	4.2	529	2.02	<.5	2.3	.9	4.1	70	<.1	<.1	.1	39	.59	.088	7	7	.56	183	.130	1	1.01	.098	.45	.1	<.01	2.3	.3	<.05	5	<.5	15.0
L12+00N 9+50E	.5	14.5	4.0	61	<.1	6.2	4.4	1071	1.26	1.1	.2	<.5	.6	21	.1	.1	.1	32	.29	.057	2	10	.18	157	.066	3	1.08	.014	.09	.1	.03	1.8	<.1	<.05	3	<.5	15.0
L10+00N 10+00W	.9	54.1	4.9	48	<.1	9.0	9.1	841	2.10	3.3	.4	1.1	.8	59	.3	.2	.1	55	.74	.062	6	13	.43	100	.075	6	1.41	.012	.22	.1	.03	3.9	.1	<.05	5	<.5	15.0
L10+00N 9+00W	.8	33.9	11.2	109	<.1	5.5	5.9	1903	.97	3.1	.2	1.4	.3	104	.8	.2	.1	24	1.50	.117	3	6	.28	191	.039	17	.86	.009	.28	.1	.12	1.9	<.1	.07	2	<.5	.5
L10+00N 8+00W	.6	52.8	5.1	76	<.1	10.9	8.9	1085	2.36	2.8	.4	.6	1.2	39	.4	.1	.1	64	.58	.067	6	16	.42	100	.094	6	1.70	.013	.24	.1	.02	4.1	.1	<.05	5	<.5	15.0
L10+00N 7+00W	.3	42.3	7.7	96	<.1	10.1	9.9	1173	2.66	4.4	.7	1.8	2.0	46	.2	.2	.1	69	.57	.102	8	15	.42	180	.119	6	2.60	.016	.22	.1	.03	4.6	.1	<.05	8	<.5	15.0
L10+00N 6+00W	.8	37.3	7.6	88	<.1	8.5	6.9	1563	2.16	2.9	.3	3.8	1.2	55	.4	.2	.1	52	.64	.082	5	15	.34	148	.079	5	1.59	.014	.23	.1	.02	3.3	.1	<.05	5	<.5	15.0
L10+00N 5+00W	.4	18.0	3.8	50	<.1	7.7	5.2	338	1.58	1.8	.2	<.5	.7	22	.1	.1	.1	47	.29	.061	2	12	.24	73	.075	2	1.26	.015	.07	.1	.02	1.6	.1	<.05	4	<.5	15.0
L10+00N 4+00W	.3	25.6	4.8	84	<.1	8.2	8.2	684	2.60	1.8	.5	.9	1.6	34	.1	.1	.1	62	.40	.058	8	12	.40	107	.086	7	2.15	.016	.27	.1	.01	4.2	.1	<.05	7	<.5	15.0
L10+00N 3+00W	.3	27.9	4.0	47	<.1	9.4	6.5	305	2.08	1.9	.3	1.2	1.0	30	.1	.2	.1	59	.36	.026	4	16	.36	97	.110	2	1.59	.018	.09	.1	.02	3.1	.1	<.05	5	<.5	15.0
L10+00N 2+00W	.4	58.7	5.1	87	<.1	7.5	6.6	534	2.16	2.4	.3	.8	.8	29	.2	.3	.1	55	.35	.037	4	10	.31	108	.074	2	1.32	.015	.08	.1	.01	3.6	.1	<.05	4	<.5	15.0
L10+00N 1+00W	.6	37.8	12.1	76	<.1	7.7	8.6	812	2.31	2.1	.3	.5	.9	34	.4	.2	.1	64	.49	.029	4	12	.38	89	.093	3	1.30	.013	.16	.1	.02	3.7	.1	<.05	4	<.5	15.0
L10+00N 0+00	.3	63.2	5.4	110	<.1	5.0	11.9	1294	2.56	2.5	.3	1.2	1.5	30	.2	.1	.1	68	.90	.086	8	5	.71	467	.099	10	2.19	.015	.23	.1	.02	5.6	<.1	<.05	7	<.5	7.5
L10+00N 1+00E	.4	40.2	4.6	68	<.1	10.5	8.5	703	2.52	2.9	.3	1.0	1.1	34	.1	.2	.1	77	.51	.059	4	14	.47	202	.103	3	1.78	.012	.07	.1	.02	3.7	.1	<.05	6	<.5	15.0
L10+00N 2+00E	.4	24.8	3.6	97	<.1	6.1	4.9	1106	1.42	1.5	.2	2.6	.6	26	.1	.1	.1	38	.37	.063	2	9	.20	159	.078	5	1.05	.013	.13	.1	.02	1.8	<.1	<.05	4	<.5	15.0
L10+00N 3+00E	.3	38.7	3.8	128	<.1	6.7	5.9	1387	1.92	1.0	.2	4.3	1.0	30	.2	.1	.1	50	.37	.046	3	8	.30	253	.083	3	1.37	.013	.11	.1	.01	2.2	<.1	<.05	4	<.5	15.0
L10+00N 4+50E	.4	16.8	3.6	48	<.1	7.9	5.0	732	1.47	1.0	.2	2.3	.7	26	<.1	.1	.1	43	.36	.031	3	13	.21	106	.091	2	1.05	.015	.09	.1	.02	2.0	<.1	<.05	3	<.5	15.0
L10+00N 5+50E	.6	7.9	4.5	64	<.1	4.5	2.8	771	1.04	.9	.1	<.5	.4	23	.1	.1	.1	28	.37	.025	1	8	.15	96	.064	2	.80	.014	.10	<.1	.03	1.4	<.1	<.05	3	<.5	15.0
L10+00N 7+50E	.3	6.8	2.8	124	<.1	3.2	2.3	975	.84	.9	.1	<.5	.4	23	.1	<.1	<.1	22	.33	.038	1	5	.13	146	.049	3	.72	.012	.13	<.1	.02	1.3	<.1	<.05	3	<.5	15.0
L10+00N 8+50E	.2	11.9	2.4	56	<.1	6.6	4.0	415	1.29	1.0	.1	.5	.6	15	<.1	.1	.1	34	.16	.075	2	7	.14	122	.073	1	1.07	.020	.03	.1	.01	1.1	<.1	<.05	4	<.5	15.0
L10+00N 10+00E	.3	76.4	5.0	76	<.1	37.9	21.0	1783	2.65	5.1	.3	.7	.8	50	.2	.1	.1	75	.88	.219	3	31	1.30	243	.128	4	1.95	.008	.07	.1	.03	5.6	.1	<.05	6	<.5	15.0
L8+00 9+50W	1.0	77.1	5.8	61	<.1	16.0	13.2	983	2.82	4.5	.7	1.2	1.6	48	.2	.2	.1	81	.71	.088	8	20	.67	119	.098	5	2.05	.013	.26	.1	.02	4.8	.1	<.05	6	<.5	15.0
L8+00 8+50W	.8	49.6	4.4	56	<.1	9.6	8.8	982	1.93	2.7	.4	<.5	.5	40	.5	.1	.1	51	.60	.086	6	12	.42	129	.063	4	1.54	.012	.11	.1	.02	3.1	<.1	<.05	5	<.5	15.0
L8+00 7+50W	.5	28.1	3.5	53	<.1	4.7	7.4	871	1.78	1.4	.2	<.5	.9	44	.1	.1	.1	47	.58	.039	4	8	.44	92	.083	5	1.32	.012	.23	<.1	.02	3.2	.1	<.05	4	<.5	15.0
L8+00 6+50W	.6	33.9	5.9	66	<.1	8.1	8.5	1470	2.07	3.4	.3	<.5	1.0	49	.3	.1	.1	60	.84	.098	4	14	.40	141	.076	10	1.41	.016	.35	.1	.05	3.5	.1	<.05	5	<.5	.5
L8+00 5+50W	.7	27.6	5.7	72	<.1	9.1	7.7	1754	2.01	2.5	.5	1.3	1.1	24	.2	.1	.1	54	.30	.100	6	12	.33	184	.087	2	1.99	.015	.09	.1	.03	3.0	.1	<.05	6	<.5	15.0
L8+00 4+50W	.4	23.3	4.8	144	<.1	8.8	6.3	1255	1.68	4.3	.2	<.5	1.0	56	.4	.1	.1	39	.74	.256	5	9	.31	223	.066	7	1.63	.016	.14	.1	.04	2.8	.1	<.05	5	<.5	15.0
L8+00 3+50W	1.9	42.0	6.8	157	<.1	6.7	6.0	3114	1.41	2.1	.2	.9	.4	38	.9	.1	.1	43	.58	.070	3	8	.33	266	.048	3	1.07	.010	.12	.1	.05	2.2	.1	<.05	4	<.5	15.0
L8+00 2+50W	.3	58.0	5.4	68	<.1	27.4	9.7	824	2.38	2.1	.4	.5	1.1	30	.1	.1	.1	75	.45	.055	5	29	.63	115	.113	3	1.63	.018	.11	.1	.01	3.6	.1	<.05	6	<.5	7.5
RE L8+00 2+50W	.4	59.6	5.7	68	<.1	27.6	10.7	848	2.52	2.1	.5	1.5	1.1	31	.1	.1	.1	80	.47	.058	5	31	.66	122	.123	3	1.77	.020	.11	.1	.02	3.6	.1	<.05	6	<.5	7.5
L8+00 1+50W	.4	17.1	4.8	106	<.1	6.9	5.3	1153	1.67	1.2	.2	1.4	.9	23	.2	.1	.1	42	.30	.039	3	9	.24	191	.079	3	1.27	.014	.15	.1	.02	2.5	.1	<.05	4	<.5	15.0
L8+00 0+50W	.2	4.7	2.6	18	.2	.9	.3	51	.05	1.2	<.1	1.6	<.1	32	.1	.1	<.1	1	.37	.024	<1	2	.04	20	.002	3	.05	.007	.04	<.1	.05	.2	<.1	<.05	<1	<.5	.5
L8+00 0+50E	.5	29.2	8.7	80	<.1	5.4	6.4	282	1.85	1.2	.2	1.6	.5	26	.1	.1	.1	51	.30	.016	3	10	.30	58	.073	4	1.17	.014	.12	.1	.01	2.7	<.1	<.05	4	<.5	15.0
L8+00 2+50E	.5	12.0	3.1	118	<.1	5.1	3.5	1151	1.45	1.2	.1	1.4	.6	21	.2	.1	.1	32	.34	.037	3	7	.18	203	.059	3	1.15	.014	.13	.1	.02	2.1	<.1	<.05	4	<.5	15.0
L8+00 4+00E	.3	32.5	2.4	19	<.1	6.1	3.7	192	1.18	.9	.2	.6	.5	48	.1	<.1	.1	28	.65	.025	2	8	.18	164	.057	7	.88	.016	.04	<.1	.02	1.7	<.1	<.05	3	<.5	15.0
STANDARD DS7	20.5	107.3	70.3	412	.9	54.8	9.3	614	2.34	48.0	4.9	70.9	4.3	70	6.4	6.0	4.5	83	.92	.080	12	167	1.04	369	.122	38	.96	.076	.44	3.8	.20	2.4	4.2	.19	4	3.5	15.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga	Se	Sample
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppb	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	ppm	ppm	ppm	%	ppm	ppm	gm
G-1	.2	2.1	3.5	40	<.1	4.0	3.9	501	1.87	<.5	2.2	1.7	3.9	76	<.1	<.1	.1	36	.54	.074	6	7	.53	231	.113	1	1.06	.167	.53	.1	.01	3.9	.4	<.05	5	<.5	15.0
L8+00 5+00E	.6	12.6	5.0	79	<.1	5.7	3.8	1169	.98	1.0	.2	1.1	.5	26	.2	.1	.1	23	.35	.044	3	8	.18	187	.042	2	.84	.010	.10	.1	.02	1.3	<.1	<.05	3	<.5	15.0
L8+00 6+50E	.4	10.3	3.0	65	<.1	4.6	2.8	735	.87	.9	.1	<.5	.6	19	.1	<.1	.1	20	.23	.059	2	6	.12	131	.039	1	.80	.012	.07	.1	.01	1.5	<.1	<.05	3	<.5	15.0
L8+00 8+00E	.2	7.1	3.1	83	<.1	5.0	3.9	673	1.15	.9	.2	1.6	.8	22	.1	.1	.1	31	.26	.015	3	10	.20	133	.066	1	.95	.010	.08	<.1	.01	2.1	<.1	<.05	3	<.5	15.0
RE L8+00 8+00E	.2	7.5	3.2	82	<.1	5.2	3.9	681	1.16	.8	.2	1.1	.8	22	.1	.1	.1	31	.26	.015	3	10	.20	130	.066	2	.94	.011	.08	<.1	.01	2.1	<.1	<.05	3	<.5	15.0
L8+00 9+00E	.3	4.3	2.5	46	<.1	2.4	2.3	211	.80	2.7	.2	1.6	.6	14	<.1	<.1	.1	15	.11	.311	2	3	.05	179	.043	1	1.00	.014	.04	.1	.01	.8	<.1	<.05	3	<.5	15.0
L6+00N 10+00W	.4	45.7	5.2	41	<.1	9.4	8.5	531	2.00	1.8	.3	.9	1.4	49	.1	.1	.1	50	.64	.037	8	15	.46	104	.065	4	1.39	.015	.23	.1	.02	3.7	.1	<.05	4	<.5	7.5
L6+00N 9+00W	.6	66.5	6.6	62	<.1	14.0	12.0	1042	2.44	4.0	.4	1.3	1.1	46	.3	.2	.1	65	.88	.080	8	19	.58	129	.050	3	1.46	.014	.24	.1	.03	4.3	.1	<.05	5	<.5	15.0
L6+00N 8+00W	.7	58.5	6.5	57	<.1	10.8	10.4	1005	2.17	4.2	.4	1.5	1.0	48	.4	.2	.1	59	.74	.107	8	14	.50	141	.044	3	1.42	.008	.21	.1	.03	3.6	.1	<.05	4	<.5	15.0
L6+00N 7+00W	.7	61.4	8.1	84	<.1	12.5	12.4	1588	2.57	2.9	.3	2.1	1.4	79	.4	.2	.1	59	.89	.089	9	20	.60	231	.045	5	1.72	.011	.31	.1	.06	5.4	.1	<.05	5	<.5	7.5
L6+00N 6+00W	.6	58.7	5.1	70	<.1	12.2	11.5	1275	2.23	4.0	.4	.6	1.1	40	.3	.1	.1	55	.71	.110	8	15	.56	194	.044	4	1.61	.012	.27	<.1	.01	4.4	.1	<.05	5	<.5	7.5
L6+00N 5+00W	.4	43.7	5.7	79	<.1	4.3	12.0	1965	1.58	5.9	.5	1.9	1.5	82	.3	.1	.1	47	.90	.111	11	5	.61	250	.024	2	2.35	.321	.25	.1	.04	4.0	.1	<.05	5	<.5	15.0
L6+00N 4+00W	2.0	27.2	15.5	42	<.1	12.4	6.0	1452	1.20	2.5	.3	.5	.8	92	.3	.1	.1	29	.93	.054	6	17	.34	153	.029	6	1.08	.010	.11	.1	.06	2.3	<.1	<.05	3	<.5	7.5
L6+00N 3+00W	.3	55.2	5.1	47	<.1	8.1	7.4	1134	1.83	2.7	.3	3.0	1.0	61	.3	.2	.1	45	.81	.035	8	10	.46	108	.046	4	1.41	.018	.12	.1	.03	3.3	.1	<.05	4	<.5	15.0
L6+00N 2+00W	.2	12.5	4.1	20	<.1	5.0	5.0	309	1.30	.9	.2	<.5	.6	20	.1	.1	.1	34	.26	.034	2	10	.23	72	.057	1	.90	.016	.09	<.1	.01	2.0	<.1	<.05	3	<.5	15.0
L6+00N 1+00W	.5	22.0	5.9	76	<.1	7.5	5.5	801	1.57	1.4	.2	.5	1.0	25	.3	.1	.1	40	.37	.025	4	12	.33	123	.059	2	1.12	.017	.12	.1	.01	3.0	<.1	<.05	3	<.5	15.0
L6+00N 0+00E	.6	16.6	4.3	58	<.1	4.3	5.5	1159	1.26	1.8	.2	.6	.7	23	.1	.1	.1	32	.32	.081	3	4	.29	202	.035	2	1.34	.037	.12	<.1	.02	1.9	<.1	<.05	4	<.5	15.0
L6+00N 2+00E	.3	16.2	4.2	69	<.1	6.3	4.7	1021	1.27	1.4	.2	<.5	.8	28	.1	.1	.1	28	.30	.040	4	9	.22	182	.043	1	1.05	.015	.13	<.1	.02	2.7	.1	<.05	3	<.5	15.0
L6+00N 3+00E	.4	22.4	4.4	40	<.1	9.5	7.3	689	1.77	1.7	.3	2.9	1.1	25	.1	.1	.1	45	.31	.021	6	15	.32	127	.057	1	1.05	.011	.14	.1	.02	3.2	.1	<.05	3	<.5	15.0
L6+00N 4+00E	.7	9.9	3.5	51	<.1	6.5	4.7	817	1.26	1.0	.2	7.5	.4	24	.2	.1	.1	29	.25	.049	3	11	.19	127	.039	2	.82	.012	.11	<.1	.02	1.9	<.1	<.05	2	<.5	15.0
L6+00N 5+00E	.4	13.8	2.8	25	<.1	6.5	4.8	518	1.35	.9	.2	.6	.7	25	<.1	.1	.1	35	.30	.030	3	11	.21	120	.056	3	.86	.013	.12	.1	.01	2.4	<.1	<.05	3	<.5	15.0
L6+00N 6+50E	.3	17.2	3.0	32	<.1	7.3	4.7	232	1.50	1.1	.2	1.5	1.0	22	<.1	.1	.1	41	.25	.020	3	13	.27	92	.067	1	1.00	.015	.07	<.1	.01	2.4	<.1	<.05	3	<.5	15.0
L6+00N 7+50E	.3	6.5	2.6	29	<.1	3.7	2.4	411	.76	.8	.2	.5	.4	34	.1	<.1	.1	15	.27	.057	2	4	.11	113	.032	2	.81	.015	.10	<.1	.02	1.5	<.1	<.05	2	<.5	15.0
L6+00 10+00E	.5	13.2	4.8	59	<.1	7.5	4.9	680	1.18	1.2	.2	.7	.9	20	.1	.1	.2	26	.23	.028	3	10	.23	169	.054	1	1.09	.015	.12	.1	.02	1.8	.1	<.05	3	<.5	15.0
L4+00 9+50W	.2	146.1	3.4	31	.1	8.5	5.9	517	1.53	3.6	.2	1.9	.6	112	.4	.2	.1	38	1.97	.076	8	10	.40	186	.028	6	1.22	.038	.06	<.1	.02	2.4	.1	<.05	3	.5	15.0
L4+00 8+50W	1.6	10.3	8.3	107	.1	8.9	2.3	1786	.34	1.1	.1	.8	.1	106	.5	.1	.1	8	1.65	.059	1	13	.16	223	.010	6	.26	.005	.09	.1	.10	.9	<.1	.07	1	<.5	.5
L4+00 7+50W	.3	63.0	4.3	191	.2	4.9	6.3	2611	1.56	2.0	.2	<.5	.7	53	2.5	.1	.1	37	.71	.151	4	6	.25	417	.042	3	1.36	.031	.15	<.1	.02	2.6	<.1	<.05	4	<.5	15.0
L4+00 6+50W	.4	16.2	3.6	85	<.1	3.6	3.4	1062	1.15	1.8	.1	.6	.5	19	.1	.1	.1	26	.24	.093	2	5	.13	186	.037	1	.71	.013	.10	<.1	.02	1.4	<.1	<.05	3	<.5	15.0
L4+00 5+50W	1.7	10.2	6.7	41	<.1	13.1	3.6	583	1.14	2.3	.2	<.5	.5	24	.2	.1	.1	23	.47	.037	2	18	.18	102	.031	3	1.19	.017	.12	<.1	.03	1.5	<.1	<.05	3	<.5	15.0
L4+00 4+50W	.6	13.0	6.4	131	<.1	7.1	4.6	2110	1.54	1.3	.1	1.3	.7	37	.3	.1	.1	34	.56	.064	3	11	.25	377	.052	5	1.29	.012	.19	.1	.03	2.5	<.1	<.05	4	<.5	15.0
L4+00 3+50W	3.2	9.0	4.3	97	<.1	19.8	7.0	2282	1.55	2.6	.2	.5	.6	21	.2	.1	.1	36	.34	.067	3	28	.36	252	.064	2	1.20	.015	.11	.2	.02	2.4	.1	<.05	4	<.5	7.5
L4+00 2+50W	.4	39.5	5.9	66	<.1	7.5	5.2	1105	1.45	1.8	.2	.9	.7	24	.5	.1	.1	36	.47	.040	7	9	.27	114	.050	2	1.23	.014	.08	.1	.03	2.5	.1	<.05	4	<.5	15.0
L4+00 1+50W	2.0	10.2	5.9	123	<.1	16.4	6.8	1777	1.65	3.8	.2	<.5	.7	16	.3	.1	.1	35	.29	.221	3	21	.24	175	.049	1	1.52	.014	.09	.1	.02	1.9	.1	<.05	5	<.5	15.0
L4+00 0+50W	.3	31.5	6.1	62	<.1	9.1	6.8	486	1.82	2.1	.3	.7	1.1	25	.1	.1	.1	49	.30	.073	5	11	.33	161	.061	1	1.90	.017	.08	.1	.01	2.3	.1	<.05	5	<.5	15.0
L4+00 0+50E	.4	6.9	5.6	142	<.1	4.9	4.2	1061	1.23	1.9	.1	.9	.8	44	.1	.2	.1	25	.43	.102	4	6	.14	312	.030	4	.99	.014	.18	.1	.02	2.3	<.1	<.05	3	<.5	15.0
STANDARD DS7	21.0	111.0	70.8	413	.9	57.1	9.7	615	2.37	47.7	4.8	79.3	4.2	66	6.4	5.7	4.5	85	.90	.079	11	174	1.03	363	.106	38	.93	.072	.44	3.0	.20	2.4	4.2	.20	4	3.3	15.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
G-1	.2	2.0	3.5	44	<.1	4.0	4.0	507	1.99	<.5	2.3	.8	4.1	89	<.1	<.1	.1	39	.65	.083	8	7	.59	231	.132	1	1.22	.196	.63	.1	<.01	4.8	.4	<.05	6	<.5	15
L4+00 1+50E	.3	39.4	5.9	67	<.1	6.1	7.8	610	2.82	3.5	.3	1.4	1.4	35	.1	.4	.1	63	.46	.037	9	10	.31	133	.071	4	1.46	.014	.16	.1	.01	4.5	<.1	<.05	5	<.5	15
L4+00 2+50E	.3	4.7	3.1	50	<.1	2.5	1.8	537	.57	1.0	.1	<.5	.6	16	.1	<.1	.1	12	.18	.116	1	3	.08	164	.040	3	.81	.018	.09	<.1	.02	1.2	<.1	<.05	3	<.5	15
L4+00 4+00E	.5	15.5	3.8	62	<.1	8.2	5.1	661	1.57	1.6	.2	.7	.7	25	.1	.1	.1	41	.31	.035	3	14	.25	108	.085	3	1.14	.017	.10	.1	.01	2.6	<.1	<.05	4	<.5	15
L4+00 5+00E	.4	20.6	2.8	118	<.1	7.2	4.9	718	1.43	.7	.1	<.5	.7	49	.3	.1	.1	34	.41	.102	3	13	.25	173	.070	6	1.08	.022	.17	.1	.01	2.3	<.1	<.05	3	<.5	15
L4+00 6+00E	.3	19.0	2.9	22	<.1	7.8	5.2	340	1.65	.8	.2	<.5	.9	28	<.1	.1	.1	46	.31	.014	3	16	.25	78	.096	4	.93	.019	.13	.1	.01	2.5	<.1	<.05	3	<.5	15
L4+00 7+50E	.5	13.6	3.6	82	<.1	9.6	4.4	347	1.26	2.0	.2	.7	1.0	18	.1	.1	.1	23	.20	.135	2	10	.18	158	.066	3	1.50	.015	.16	.1	.01	1.7	<.1	<.05	5	<.5	15
L4+00 8+50E	.4	11.9	3.0	72	<.1	8.5	5.2	333	1.56	1.1	.2	.8	.8	25	.1	.1	.1	43	.34	.034	2	14	.27	102	.108	2	1.23	.028	.10	.1	<.01	2.5	<.1	<.05	4	<.5	15
L4+00 9+50E	1.1	70.4	4.4	62	<.1	19.4	10.0	390	2.54	2.5	.5	2.5	1.8	35	.1	.2	.3	63	.44	.033	7	30	.52	132	.130	3	1.89	.022	.29	.1	.01	4.4	.1	<.05	6	<.5	15
L2+00N 10+00W	.6	22.2	4.1	47	<.1	7.4	6.7	582	2.09	2.2	.4	.7	.9	32	.1	.1	.1	62	.35	.030	3	12	.34	117	.110	3	1.52	.019	.10	.1	.01	3.1	.1	<.05	5	<.5	15
L2+00N 9+00W	.3	12.5	3.3	52	<.1	5.2	4.2	398	1.30	1.6	.2	.7	.7	26	.2	.1	.1	35	.35	.049	2	9	.21	86	.073	4	1.21	.018	.14	.1	.01	2.0	.1	<.05	4	<.5	15
L2+00N 8+00W	.3	83.1	6.2	48	<.1	8.8	4.9	1222	1.45	2.0	.3	.6	.6	66	.4	.3	.1	47	1.22	.048	9	11	.26	178	.067	8	1.45	.018	.10	.1	.05	2.1	.1	<.05	4	<.5	15
L2+00N 7+00W	.5	27.3	5.2	78	<.1	10.2	7.6	704	2.25	3.9	.4	1.8	1.3	35	.1	.2	.1	59	.47	.059	4	16	.38	163	.111	4	2.27	.024	.11	.1	.01	3.4	.1	<.05	7	<.5	15
L2+00N 6+00W	.4	114.5	10.8	107	<.1	8.2	6.9	1367	2.22	5.3	.3	.6	.8	34	1.1	.3	.1	64	.42	.061	4	14	.37	221	.086	6	1.42	.013	.22	.1	.01	3.5	.1	<.05	5	<.5	15
L2+00N 5+00W	.9	30.6	6.0	63	<.1	17.2	10.9	1120	2.82	2.3	.5	1.7	1.4	47	.2	.3	.1	81	.50	.036	6	27	.59	186	.132	3	2.24	.016	.19	.1	.02	4.4	.1	<.05	6	<.5	15
L2+00N 4+00W	.2	8.1	3.6	64	<.1	4.8	4.8	288	1.38	1.6	.2	<.5	.5	20	.5	.1	.1	33	.24	.091	1	8	.19	91	.067	2	1.02	.019	.07	<.1	<.01	1.8	<.1	<.05	4	<.5	15
L2+00N 3+00W	1.6	12.5	4.9	94	<.1	16.0	6.1	1613	1.55	1.8	.2	.5	.9	24	.2	.1	.1	34	.30	.062	3	17	.26	171	.079	4	1.86	.023	.11	.1	.02	2.1	.1	<.05	5	<.5	15
L2+00N 2+00W	.4	12.9	3.3	89	<.1	7.7	4.7	946	1.33	2.8	.1	.6	.5	22	.2	.1	.1	36	.31	.135	1	11	.24	133	.068	2	1.20	.019	.05	.1	.01	1.6	.1	<.05	5	<.5	15
L2+00N 1+00W	1.1	27.7	5.2	66	<.1	14.1	6.7	605	1.79	3.5	.3	1.3	1.0	24	.4	.1	.1	41	.44	.102	3	18	.34	143	.075	3	1.69	.017	.16	.1	.01	2.7	<.1	<.05	5	<.5	15
L2+00E 0+00W	.3	53.8	5.4	135	<.1	8.4	10.9	706	2.24	6.3	.3	1.0	1.0	29	.2	.3	.1	54	.31	.128	4	8	.23	174	.066	3	1.95	.022	.07	.1	.02	3.1	.1	<.05	6	<.5	15
L2+00E 1+00W	1.1	58.2	23.0	291	<.1	9.9	7.1	1118	2.07	2.7	.3	<.5	.9	40	1.5	.4	.1	46	.57	.047	5	13	.23	245	.070	5	1.52	.017	.16	.1	.03	4.0	.1	<.05	5	<.5	15
L2+00E 2+50W	.2	9.4	3.6	100	<.1	5.8	4.0	573	1.59	1.5	.2	.5	.6	24	.1	.1	.1	43	.31	.040	2	9	.19	101	.089	4	1.22	.015	.14	.1	.01	2.0	<.1	<.05	4	<.5	15
RE L2+00E 2+50W	.3	9.6	3.7	101	<.1	6.0	4.0	588	1.59	1.6	.1	.6	.7	23	.1	.1	.1	41	.30	.039	2	9	.19	104	.085	4	1.21	.015	.14	<.1	.01	2.0	.1	<.05	4	<.5	15
L2+00E 3+50W	1.6	98.8	4.5	25	<.1	10.3	5.6	661	1.48	1.5	.4	1.2	.7	205	.3	.2	.1	30	3.12	.040	7	13	.42	299	.036	10	1.22	.025	.09	<.1	.03	2.2	.1	.06	4	.5	15
L2+00E 4+50W	.5	24.5	5.6	47	<.1	7.1	6.0	789	1.86	2.0	.3	<.5	.8	43	.2	.1	.1	43	.77	.034	4	11	.34	129	.089	11	1.27	.016	.30	.1	.04	3.0	.1	<.05	5	<.5	15
L2+00E 5+50W	.3	40.0	3.2	39	<.1	11.9	6.6	491	1.90	1.5	.2	1.6	1.1	61	.1	.1	.1	43	1.02	.049	5	18	.32	113	.103	9	1.28	.024	.21	.1	.01	3.3	<.1	<.05	4	<.5	15
L2+00E 6+50W	.2	39.1	1.8	27	<.1	7.5	4.0	578	1.05	1.6	.2	.5	.3	507	.2	.1	<.1	26	10.48	.097	4	8	.94	313	.039	15	.73	.026	.10	.1	.01	1.6	<.1	.07	2	.7	15
L2+00E 7+50W	.7	87.8	4.7	83	<.1	20.3	10.6	749	2.49	3.3	.5	1.7	1.7	36	.1	.1	.3	48	.51	.081	8	25	.46	210	.109	6	2.53	.020	.31	.2	.02	4.6	.1	<.05	7	<.5	15
L0+00 10+00W	.2	59.2	3.9	76	.1	7.2	6.4	591	1.91	4.3	.2	<.5	.8	51	.3	.2	.1	52	.77	.030	5	10	.30	86	.084	6	1.46	.025	.09	<.1	.03	2.7	.1	<.05	4	<.5	15
L0+00 9+00W	.5	44.6	4.5	38	<.1	11.0	9.3	508	2.50	2.7	.5	1.4	1.4	50	.1	.2	.1	81	.65	.028	6	19	.50	120	.143	6	1.59	.020	.23	.1	.01	5.0	.1	<.05	5	<.5	15
L0+00 8+00W	.8	21.5	5.8	67	<.1	7.5	7.1	1588	1.90	2.4	.3	5.2	.7	37	.2	.1	.1	58	.51	.035	3	12	.32	147	.098	5	1.35	.013	.11	.1	.03	2.8	.1	<.05	5	<.5	15
L0+00 7+00W	1.4	21.1	7.1	168	<.1	14.1	7.1	1767	1.86	4.5	.2	<.5	.9	41	.6	.2	.1	41	.71	.227	4	19	.29	435	.077	6	2.18	.019	.17	.1	.05	3.0	.1	<.05	6	<.5	15
L0+00 6+00W	.6	21.1	3.8	33	<.1	7.5	6.7	768	1.71	2.4	.2	<.5	.6	27	.2	.1	.1	45	.53	.058	3	12	.29	109	.081	4	1.36	.011	.11	<.1	.02	2.7	<.1	<.05	5	<.5	15
L0+00 5+00W	.6	36.5	7.9	172	<.1	18.0	10.0	2384	2.37	4.2	.5	.9	1.7	41	.7	.1	.1	55	.55	.223	7	19	.40	397	.101	5	3.11	.019	.17	.1	.03	5.1	.1	<.05	9	<.5	15
L0+00 3+00W	.6	24.2	5.9	94	<.1	12.5	9.1	1640	2.48	7.2	.3	<.5	1.2	43	.9	.3	.1	67	.54	.068	5	18	.41	231	.126	5	2.21	.018	.17	.1	.02	3.8	.1	<.05	7	<.5	15
STANDARD DS7	21.0	111.4	71.0	415	.9	56.9	9.7	638	2.41	48.6	4.9	70.3	4.4	70	6.4	5.9	4.5	88	.94	.080	13	177	1.06	373	.125	39	.98	.079	.45	3.9	.20	2.5	4.2	.21	5	3.5	15

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
G-1	.2	2.2	3.3	42	<.1	4.1	4.2	528	1.99	<.5	2.4	1.5	4.1	81	<.1	<.1	.1	39	.62	.076	8	7	.55	209	.134	1	1.08	.149	.52	.1	<.01	3.3	.4	<.05	5	<.5	15.0
L0+00 1+50W	1.1	21.6	5.8	121	<.1	8.1	5.4	2357	1.46	4.4	.2	3.6	.6	40	1.1	.2	.1	38	.76	.077	3	12	.25	248	.064	7	1.18	.012	.13	.1	.05	2.1	.1	<.05	4	<.5	7.5
L0+00 0+50W	.5	21.6	5.6	95	<.1	8.2	5.9	1993	1.74	3.0	.3	.6	1.0	33	.3	.1	.1	48	.53	.038	5	11	.25	253	.088	4	1.41	.014	.12	.1	.03	2.6	.1	<.05	4	<.5	7.5
RE L0+00 0+50W	.6	22.2	5.9	97	<.1	8.2	5.7	2033	1.77	3.1	.3	1.0	1.0	34	.3	.1	.1	48	.53	.038	4	12	.26	234	.089	4	1.41	.016	.12	.1	.04	2.7	.1	<.05	5	<.5	7.5
L0+00 0+50E	.6	27.5	8.6	179	<.1	9.4	15.8	1792	2.71	7.2	.4	.5	2.1	63	.5	.5	.1	45	.89	.096	9	11	.29	574	.049	9	2.10	.020	.23	.1	.04	9.9	.1	<.05	5	<.5	7.5
L0+00 2+00E	.9	12.8	4.5	54	<.1	2.6	1.1	174	.30	3.5	<.1	2.1	.1	53	.5	.1	<.1	7	1.16	.050	1	4	.12	99	.012	8	.23	.007	.08	<.1	.11	.6	<.1	.09	1	<.5	7.5
L0+00 3+00E	.5	9.7	3.6	52	<.1	4.8	4.5	1112	1.32	1.6	.1	1.1	.4	31	.1	.1	.1	33	.42	.083	2	8	.15	182	.058	7	.87	.021	.11	<.1	.03	1.5	<.1	<.05	3	<.5	15.0
L0+00 4+00E	.3	26.4	1.1	8	<.1	4.1	1.0	217	.20	1.3	.2	.7	<.1	215	.1	.1	<.1	5	20.28	.098	1	3	.21	333	.007	15	.27	.011	.04	<.1	.02	.2	<.1	<.05	1	.7	15.0
L0+00 5+00E	1.3	20.1	4.8	64	<.1	5.7	4.9	1035	1.50	2.0	.2	.5	.6	30	.1	.1	.1	38	.38	.031	3	9	.24	153	.069	3	1.20	.015	.08	<.1	.02	2.7	<.1	<.05	4	<.5	15.0
L0+00 6+00E	.5	25.3	4.0	92	<.1	11.8	7.3	457	1.81	3.1	.3	8.6	1.1	23	.1	.1	.2	37	.39	.081	4	13	.23	229	.075	3	1.99	.022	.10	.1	.01	2.5	.1	<.05	6	<.5	15.0
L0+00 7+00E	1.0	42.3	4.0	132	<.1	15.9	9.2	1112	2.26	3.3	.2	1.0	1.1	26	.2	.1	.3	57	.35	.046	5	15	.37	228	.097	3	1.92	.022	.09	.2	.01	3.0	.1	<.05	6	<.5	15.0
L0+00 8+00E	.6	51.6	5.4	139	<.1	13.2	7.4	837	2.03	3.1	.3	1.5	1.5	38	.2	.1	.3	37	.56	.066	6	14	.33	281	.092	4	2.32	.019	.16	.1	.01	3.4	.1	<.05	6	<.5	15.0
unknown MAX1	.2	59.2	4.8	20	.1	10.9	5.6	225	1.56	2.2	.5	2.1	1.0	65	.1	.2	.1	38	1.07	.034	6	14	.38	82	.074	3	1.71	.028	.04	.1	.04	3.1	<.1	<.05	5	<.5	15.0
unknown MAX2	1.7	32.3	4.7	54	<.1	15.7	6.7	1261	1.76	2.1	.3	.9	1.0	41	.2	.1	.1	42	.78	.085	5	21	.34	283	.075	6	1.49	.016	.12	.1	.04	3.0	<.1	<.05	4	<.5	7.5
STANDARD DS7	20.7	110.3	70.1	410	.9	56.4	9.6	627	2.41	47.9	4.9	71.5	4.4	70	6.3	5.8	4.5	87	.93	.080	13	177	1.05	377	.124	37	.98	.078	.44	3.8	.20	2.5	4.2	.20	5	3.3	15.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data FA

Appendix E - Writer's Certificate

APPENDIX C - Writer's Certificate

I, **John R. Kerr,** of the City of Vancouver, B.C. hereby certify that:

1) I graduated with a BASc degree in geological engineering from the University of British Columbia, Vancouver, B.C. in 1964.

2) I am a consulting, contract geologist, with my address of business 208 - 515 West Pender Street, Vancouver, B.C. V6B 6H5.

3) I am a member in good standing of the Association of Engineers and Geoscientists of the Province of British Columbia (#6858).

4) I have worked as a geologist continuously for 42 years since graduation.

5) I am responsible for the preparation of the entire report entitled **SUMMARY REPORT on the Kentucky Property, British Columbia,** and dated October 20, relating to the Casper mining claims. I visited the property on July 24, 2006. The purpose of this visit was for site examination, program coordination and work supervision on the property.

6) The costs of completing the 2006 field program totaling $110,718, are detailed in Appendix A, and to the best of the writer's knowledge are correct.

Certified Correct:

John R. Kerr, P. Eng.
Date: January 15, 2007