Geochemical Assessment Report

On the

Rossland Claims

(Rossland Property)

Trail Creek Mining Division – British Columbia

Latitude 49° 03' North, Longitude 117° 48' West

NTS 82F4W

For

Yellowstone Resources Ltd.

By

Stan A. Endersby, P. Eng. (B.C.)
Gary M. Allen, P. Eng (Manitoba, Ontario)

January 18, 2007

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Summary and Conclusions

Yellowstone Resources Ltd. holds title to six mineral claims consisting of a total of 1545.55 hectares located south of the town of Rossland in south-eastern British Columbia. The claims lie approximately 4 km south of the historic Rossland gold mining camp. The camp has the second largest production of gold in British Columbia.

The claims were originally staked in 1982 and 1983 to cover an area of favourable geology and a weak electromagnetic anomaly from an airborne survey. Previous preliminary geological fieldwork and geophysical and geochemical surveys on the claims indicate anomalous gold in the soil samples and geophysical anomalies trending northeast – southwest.

The 2006 field work continued the earlier work on the south portion of the claims, and consisted of 120 geochemical soil samples on 25m spacing on a grid spaced 100 and 50m apart. The samples were analysed by Acme Analytical Laboratories Ltd. for the full suite of metals. Results confirmed earlier findings of scattered and clumped anomalous gold values in the soils. Of the 120 samples taken, 31 were considered anomalous, i.e. greater than 10 ppb.

Each of the anomalies warrant following up exploration to pinpoint the source of gold. The future work recommended includes further geophysical surveying, geochemical sampling as well as surface trenching and if warranted diamond drilling.

Recommendations

A two phase exploration program is recommended to determine the economic potential of the Rossland claims. The initial phase would comprise of detailed geophysical and geochemical surveying of the anomalous gold areas to better define the source of gold. Concurrent and following the surveys is backhoe trenching.

Contingent upon the results of Phase 1, the proposed Phase II program would consist of diamond drilling of defined targets. The estimated costs for Phases I and II are $72,000 and $156,600, respectively, for a total of $228,600. The costs are in line with the costs recommended to be spent on the claims in 1987.

Estimated Cost of Recommendations

Phase I Additional mapping, geophysical surveying, geochemical sampling and backhoe trenching .

Salaries	Geologist for 15 days @ $400/day	$6,000
	2 – Assistants for 15 days @ $400/day	6,000
Accommodations & meals 45 mandays @ $150/manday		6,750
Transportation	15 days @ $200	3,000
Trenching	10 days @ $150/hr	12,000
Analytical	800 @ $20/sample	16,000
Report Preparation		5,000
Management fees		5,000
Total		59,750
Contingencies	20% of above	12,000
Total Phase I		**$72,000**

Phase II Diamond drilling and trenching of Phase I targets and for extending the geophysics and geochemical surveys onto the remaining Rossland claims.

Salaries	Geologist for 10 days @ $400/day	$4,000
	Assistants 10 days @ $400/day	$4,000
Accommodations & meals 10 mandays @ $100/manday		1,000

Drilling 550m @ $150/m (all included)		82,500
Transportation	10 days @ $200	2,000
Trenching	5 days @ $150/hr	6,000
Analytical	1,000 @ $20/sample	20,000
Report Preparation		6,000
Management fees		5,000
Total		130,500
Contingencies	20% of above	26,100
Total Phase II		**$156,600**
Total Phase I & II		**$228,600**

Introduction

Yellowstone Resources holds title to 6 claims numbered 520619 and 520621-520625. The claims lie south of the town of Rossland in the Rossland gold mining camp in south-eastern British Columbia. This report documents the work done on claims numbered 520619, 520625 and 520623.

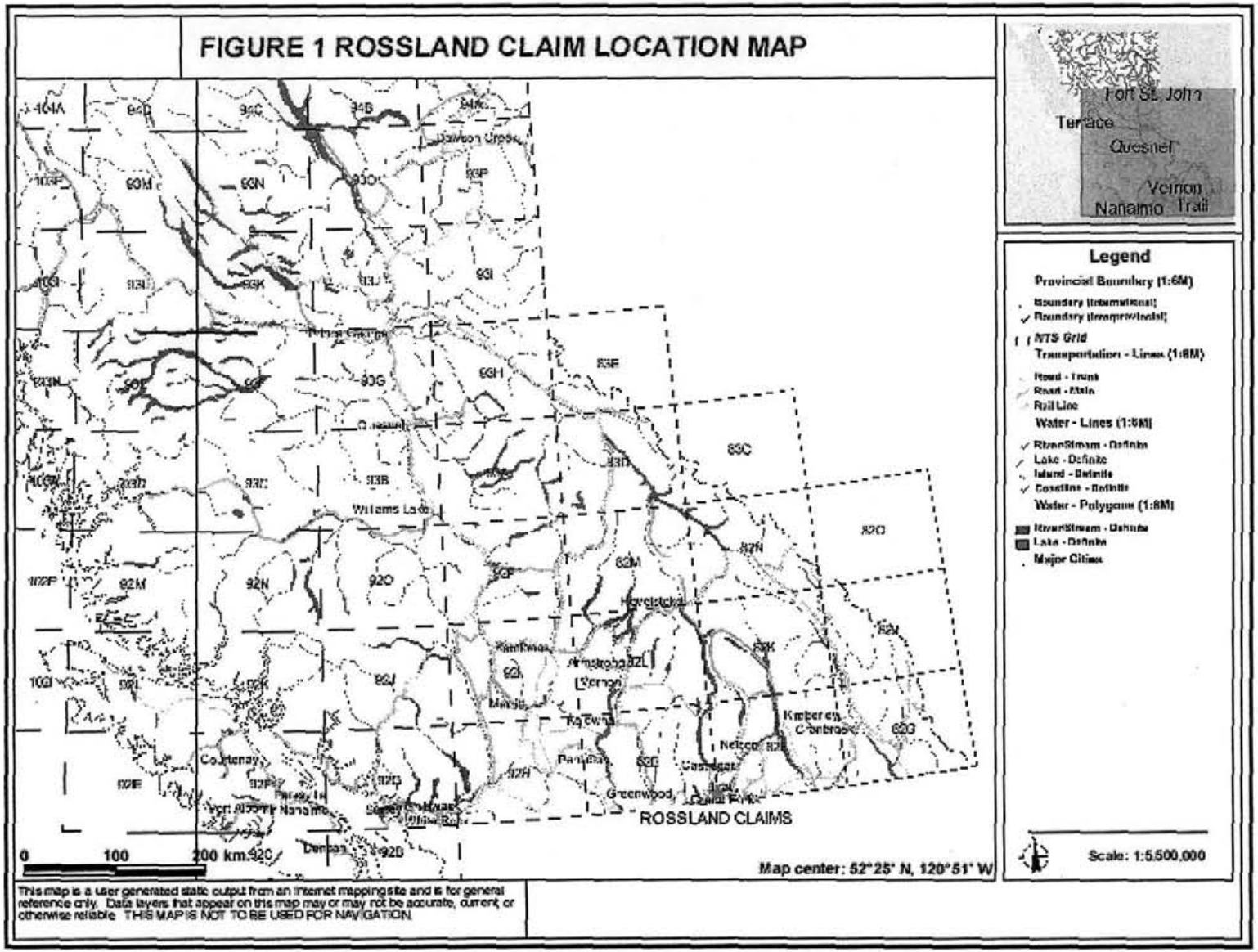
There is no known mineral occurrence on the above mentioned claims. The claims were staked to cover electromagnetic conductors outlined by an airborne geophysical survey that coincided with favourable geology similar to the Rossland gold mining camp. Previous ground surveys conducted on 520619 in 1983 and 1987 outlined coincident anomalous gold and base metals in the soils with electromagnetic inferred conductors and magnetic highs.

The 2006 exploration program comprised of 120 geochemical soil samples on 25m spacing on lines spaced 50 and 100m apart. The work was performed by J. Denny with an assistant on October 17, 18 and 19, 2006.

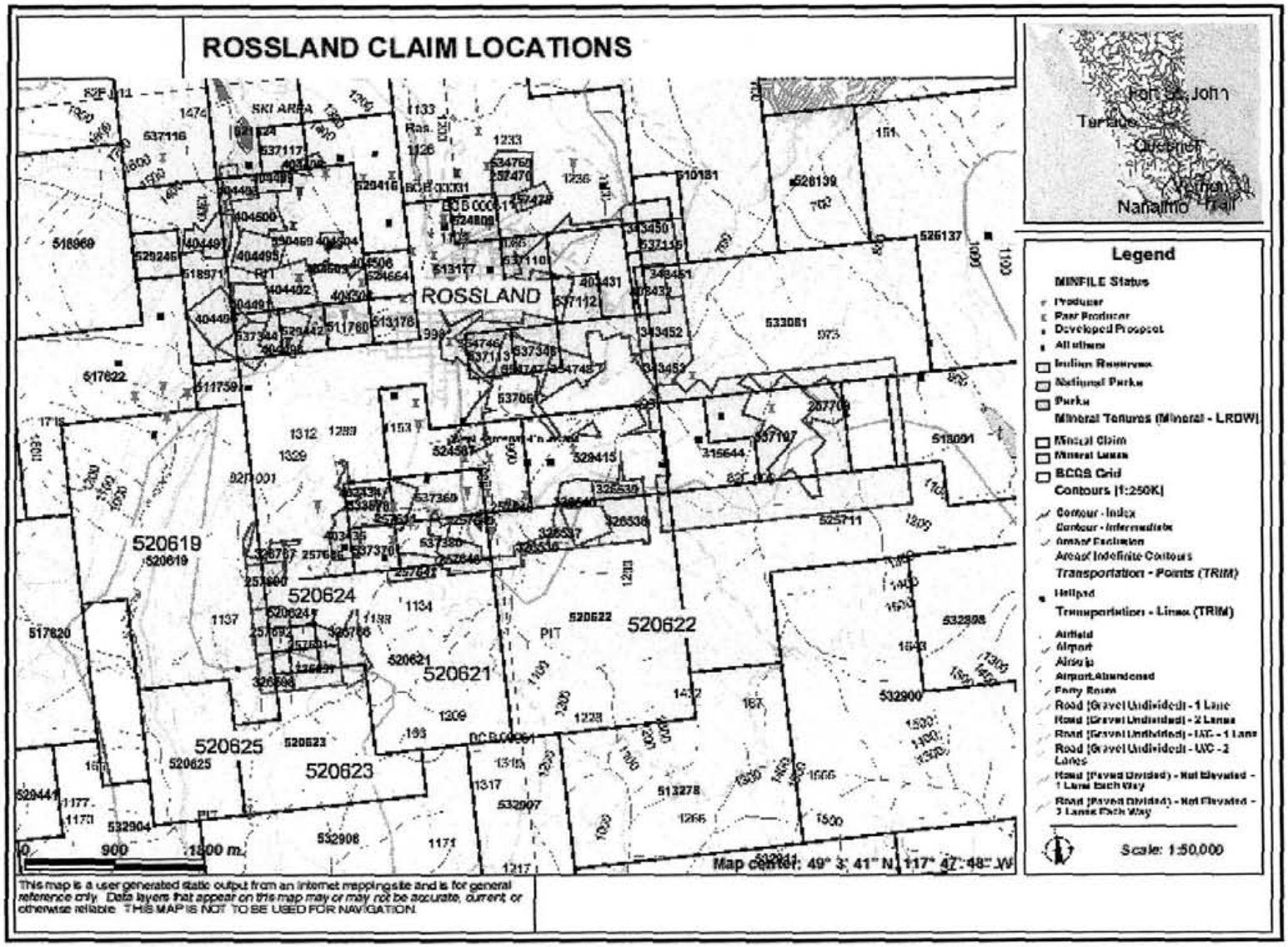
Location, Access and Physiography

The Yellowstone Resources Rossland claims, covering 1545.55 hectares, lie approximately 2 km south of the town of Rossland in south-eastern British Columbia. The property elevations vary from 600m along Little Sheep Creek to 1300m on the southern flank of Deer Park Hill. Slope gradient varies from gentle to moderate. Vegetation is a secondary growth of balsam, fir, cedar, jack pine, spruce, birch and alder. Primary cedar stands can be found along some water courses. The area is predominantly overburden covered and there are 4x4 accesses to most areas of the claims.

FIGURE 1 ROSSLAND CLAIM LOCATION MAP



ROSSLAND CLAIM LOCATIONS



This map is a user generated static output from an internet mapping site and is for general reference only. Data layers that appear on this map may or may not be accurate, current, or otherwise reliable. THIS MAP IS NOT TO BE USED FOR NAVIGATION

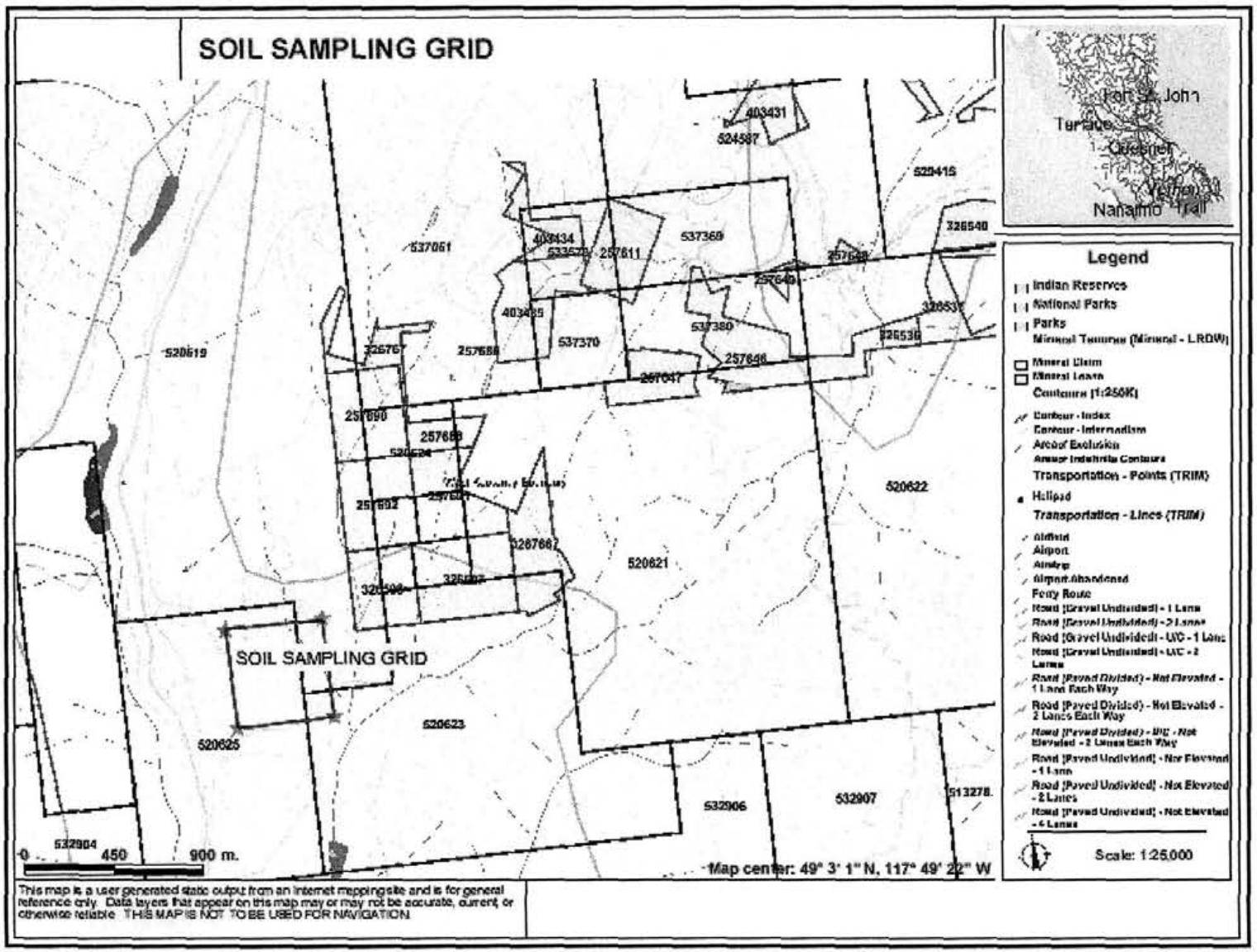
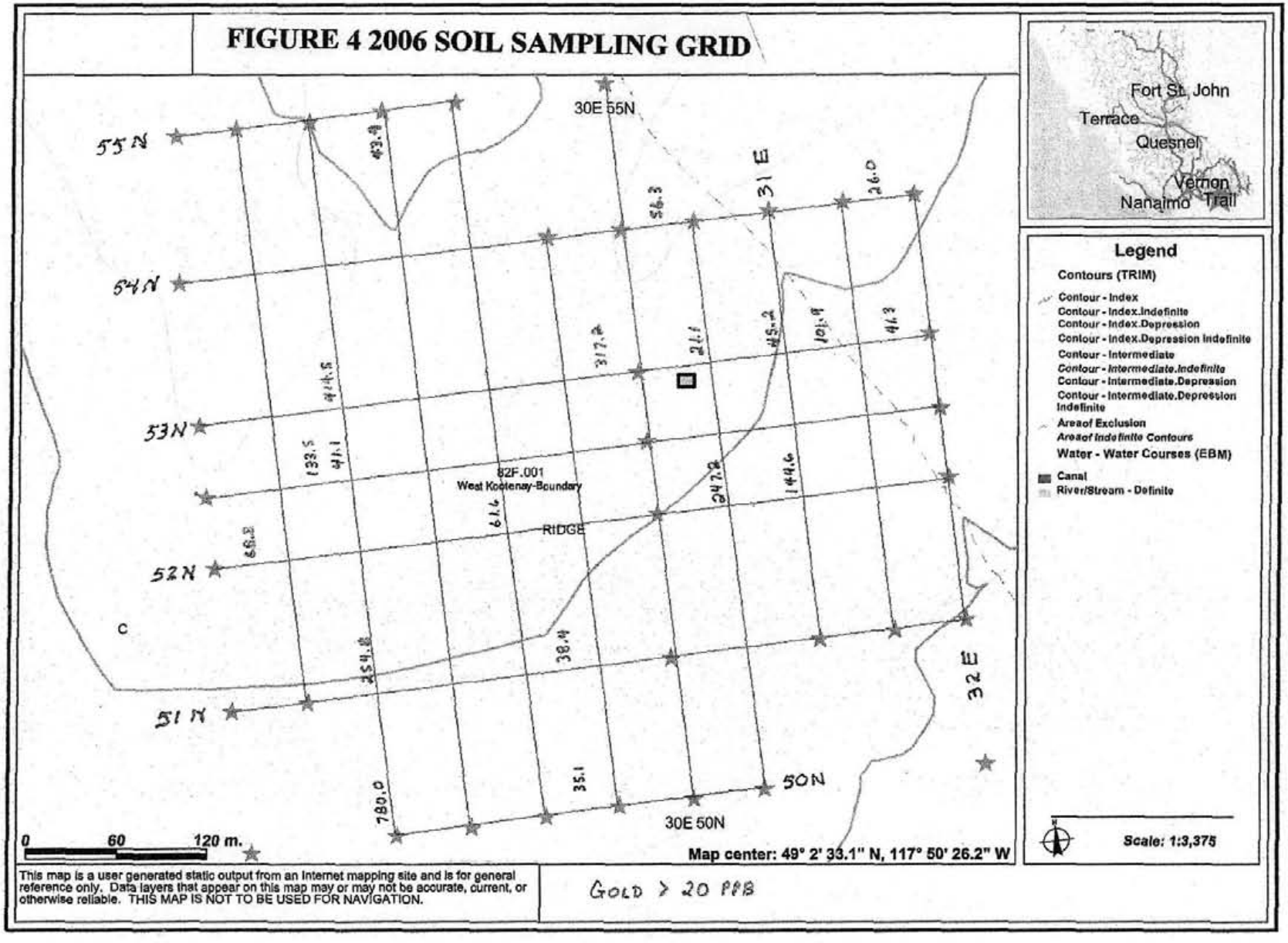

SOIL SAMPLING GRID
SOIL SAMPLING GRID
Fort St. John
Terrace
Quesnel
Nanaimo
Legend
Indian Reserves
National Parks
Parks
Mineral Claim
Mineral Leases
Contours (1:250K)
Transportation - Points (TRIM)
Heliport
Transportation - Lines (TRIM)
Ferry Route
0 450 900 m.
Scale: 1:25,000
Map center: 49° 3' 1" N, 117° 49' 22" W
This map is a user generated static output from an Internet mapping site and is for general reference only. Data layers that appear on this map may or may not be accurate, current, or otherwise reliable. THIS MAP IS NOT TO BE USED FOR NAVIGATION.

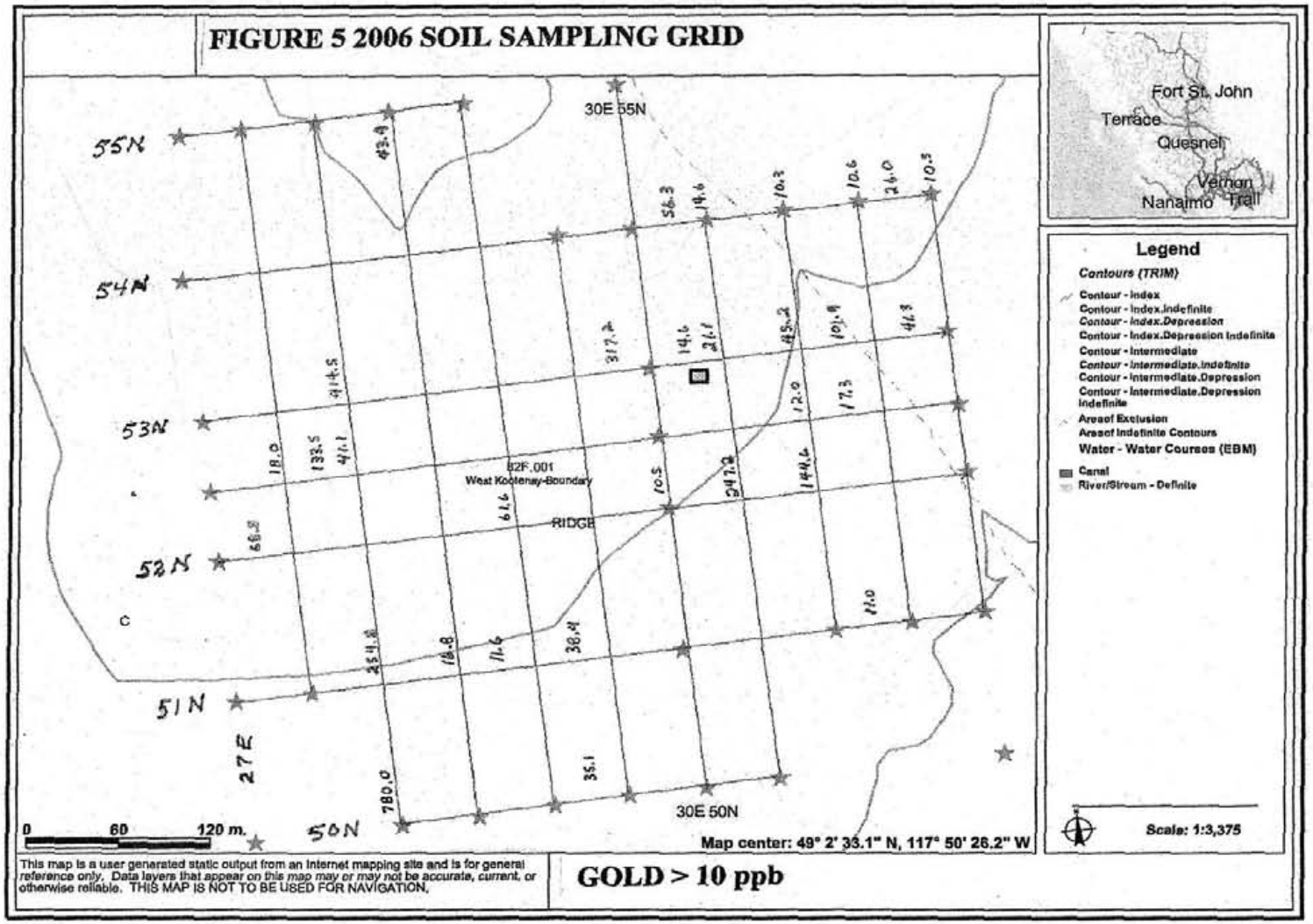
FIGURE 4 2006 SOIL SAMPLING GRID



This map is a user generated static output from an Internet mapping site and is for general reference only. Data layers that appear on this map may or may not be accurate, current, or otherwise reliable. THIS MAP IS NOT TO BE USED FOR NAVIGATION.

GOLD > 20 PPB

FIGURE 5 2006 SOIL SAMPLING GRID



This map is a user generated static output from an Internet mapping site and is for general reference only. Data layers that appear on this map may or may not be accurate, current, or otherwise reliable. THIS MAP IS NOT TO BE USED FOR NAVIGATION.

GOLD > 10 ppb

Claim Data

The Rossland claims were registered in the name of Nugget Mines Ltd. and are beneficially owned by Yellowstone Resources Ltd..

Tenure No.	Area (Hectares)
520619	486.85
520621	296.43
520622	423.46
520623	190.59
520624	21.17
520625	127.05
Total	**1545.55**

History

The Rossland mining camp was the second largest gold mining camp in British Columbia in terms of recorded gold production. The total camp production, mainly between 1895 and 1937, was 2.7 million ounces of gold and 3.3 million ounces of silver from 5.9 million tons of ore. The average grade of the ore was 0.47 ounces of gold per ton, 0.60 ounces of silver per ton and about 1% copper. Most of the production came from the Le Roi, Centre Star, War Eagle, and Josie mines. Molybdenum was also produced in the immediate area, from Red Mountain, during the period 1966 to 1971.

Examination of old information indicates that the Rossland claims have been staked and re-staked many times but with apparently very little systematic exploration work. In 1981 an airborne electromagnetic survey was conducted by Rubicon Resources Ltd. and reported by R. A. Sheldrake. The airborne survey outlined a number of electromagnetic anomalies which were later confirmed by ground VLF-EM surveys. In the same year a geochemical survey outlined a number of gold anomalies on 520619. Since 1982 preliminary ground geophysical, geological and geochemical surveys have been conducted over parts of the claims.

Geology

Regional Geology

The Rossland area lies in the Nelson Map area, 82F (West Half), the geology of which has been described by Little in 1960. The geology of the Rossland gold mining camp has also been documented by Drysdale (1915), Bruce (1917), Gilbert (1948), Fyles (1970), Fyles et al (1973) Thorpe (1973) and Little (1982). The gold deposits of the Rossland camp occur in a complex environment in which major volcanic, sedimentary and intrusive rocks occur.

Rossland Mine Geology

The gold-copper deposits of the Rossland camp are predominantly pyrrhotite-rich quartz veins containing up to 70% sulphides. The veins are localized by east and north trending faults where they intersect or lie along contacts with highly competent porphyry rocks. The Red Mountain molybdenum deposits occur in brecciated granodiorite and sedimentary rocks.

The Yellowstone Claim Geology

The Yellowstone claims lie to the south of the Rossland gold camp and are largely overburden covered. According to Fyles the claims are underlain by sedimentary and volcanic rocks.

Geochemical Survey

A total of 120 soil samples and one rock sample were taken on the claims over the period October 15 to 21, 2006. The survey grid covered the north east corner of claim No. 520625, the south end of claim No. 520619 and the north west corner of claim No. 520623 as shown in Figure 3 on page 10. Seven east-west lines were sampled on a 25m spacing. The lines were spaced 100m and 50m apart.

The overburden is predominantly comprised of a podzolic glacial till. Soil samples of 0.5 to 1 kg weight were collected from the B horizon at a depth

of 10 to 40 cm and placed in Kraft paper bags. The samples were shipped to Acme Analytical Laboratories Ltd. in Vancouver, B.C. for atomic absorption analyses. The results of the analyses are reported in Appendix 1.

Geochemical Results

The soil geochemical survey outlined anomalous gold, i.e. > 20 parts per billion (ppb), in 19 of the 120 samples taken or 32 samples > 10 ppb. The gold values vary from 1ppb to 780 ppb. There appears to be no correlation between gold and any other element. The anomalies seem to be clustered around the eastern central area of the grid although several single point anomalies occur throughout. The results appear to agree with past work over the claims.

References

E. Sykes Geophysical Assessment Report on the Cherry Group (Jero Claims) May 1990 No. 19,985

D. G. Allen Geochemical and Geophysical Report on the Jero 1 to 4 Claims August 25, 1983, No. 11,441

John Gravel, Donald G. Allen, D. R. MacQuarrie Geochemical and Geophysical Report on the Jero Claims February 2, 1987, No. 18759

Affidavit of Expenses

The following expenses were incurred on the Yellowstone Resources Ltd. Rossland claims:

Wages and labour		
Jack Denny	3 days @ $300/day	$900
Mark Best	3 days @ $200/day	600
Stan Endersby	1 days @ $500/day	500
Gary Allen	4 days @ $480/day	1,920
Travel		
Vehicle rental	3 days @ $50/day	150
Gas		60
Vancouver to Rossland	600km @ $0.50/km	300
Accommodation & meals	3 days @ 150/day	450
Miscellaneous		
Geochemistry analysis	120 @ $17.08/sample	2,048
Maps, flagging		40
Postage		35
Telephone		30
Stationary	6 Binders @ $4.54 each	27
Photocopying	210 pages @ $0.10each	21
Computer rental	4 days @ $10/day	40
Total		**$7,121**

CERTIFICATE

I, Stan A. Endersby, certify that;

1. I am a graduate of the University of British Columbia in Chemical Engineering (B. A. Sc. 1954). Also, I have an M.Sc. 1965.

2. I am a member in good standing of the Association of Professional Engineers of B.C.

3. This report is based on fieldwork performed by Jack Denny and Mark Best October 15 to 21, 2006. I have personally performed work on these claims in the past.

4. I am a director of Yellowstone Resources Ltd.

5. I have an interest in the claims.

January 19, 2007
White Rock, B.C.

Stan A. Endersby
P. Eng. (B.C.)

Certificate

I, Gary M. Allen, certify that:

1. I am a consulting mining engineer with offices at 5 Ursa Crt., Sudbury, Ontario.

2. I am a graduate of the South Dakota School of Mines & Technology with degrees in Mining Engineering B.Sc. and M.Sc.

3. I have practiced my profession since 1970 in Canada and the United States.

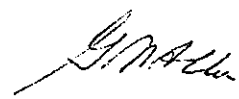
4. I am a member in good standing of the Association of Professional Engineers of Manitoba and Ontario.

5. This report is based upon a review of literature and field work completed by Jack Denny and Mark Best from October 15 to 21, 2006. I have personally performed work on these claims in the past.

6. I am a director of Yellowstone Resources Ltd.

7. I consent to the use of this report in a statement of Material Facts or in a Prospective in connection with the raising of funds for the project covered by this report.

Gary M. Allen,
P. Eng. Ontario, P. Eng. Manitoba



Sudbury, Ontario
January 18, 2007

Appendix

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9001 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Yellowstone Resources Ltd. PROJECT Bayoune & Rorsland File # A608562 Page 1

1124 Lee St., White Rock BC V4B 4P4 Submitted by: Stan Enderesby

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.5	2.1	2.2	44	<.1	5.8	4.3	505	1.76	<.5	1.8	1.3	3.5	42	<.1	<.1	.1	36	.47	.080	5	56	.58	196	.114	1	.80	.052	.42	.1	<.01	2.0	.3	<.05	5	<.5
L55N 27+00E	.5	53.8	41.6	142	.2	46.6	17.1	1753	2.95	17.7	.4	9.4	2.3	44	1.7	1.3	.5	68	.64	.194	8	59	.96	386	.121	4	2.65	.033	.21	.5	.05	3.8	.3	.08	7	<.5
L55N 27+25E	.4	64.8	14.8	136	.1	71.5	18.5	719	2.73	19.5	.3	4.2	2.9	40	.8	.7	.4	56	.57	.379	7	40	.73	416	.141	5	3.10	.029	.15	.4	.04	3.8	.2	<.05	9	<.5
L55N 27+50E	.6	57.7	14.8	105	<.1	62.7	19.3	955	3.87	18.7	.5	7.2	3.1	38	.6	1.3	.4	96	.49	.163	7	75	1.16	310	.168	3	3.80	.034	.22	.4	.04	5.8	.3	<.05	10	<.5
L55N 27+75E	.8	74.9	13.0	87	.1	62.0	17.6	611	3.75	14.1	1.3	3.8	4.5	37	.6	1.7	.3	98	.50	.068	16	65	1.02	163	.190	5	4.62	.038	.23	.6	.04	7.5	.3	.06	12	<.5
L55N 28+00E	.7	49.3	21.6	99	.1	30.4	15.6	1212	3.23	17.1	.7	6.6	3.5	43	.9	1.9	.4	85	.66	.088	11	39	.83	247	.162	5	3.24	.022	.17	.6	.04	5.0	.3	.06	9	.5
L55N 28+25E	.8	61.6	47.6	160	.3	24.0	16.4	2125	3.07	20.3	.6	7.9	1.5	55	2.1	1.9	.7	75	.87	.245	8	37	.84	371	.093	3	2.03	.014	.16	.5	.06	3.1	.3	.07	8	.5
L55N 28+50E	1.1	61.5	16.2	105	.3	25.2	13.3	1246	2.72	22.6	.8	43.4	3.1	26	1.1	1.2	.5	73	.31	.156	11	31	.62	253	.115	2	2.21	.015	.13	1.2	.03	2.9	.3	<.05	7	<.5
L55N 28+75E	.8	58.6	11.6	113	.2	34.6	15.2	1017	2.92	26.6	.8	9.8	3.5	35	1.1	1.2	.5	77	.64	.119	12	35	.64	257	.124	3	2.36	.021	.16	1.4	.03	3.3	.4	<.05	8	<.5
L55N 29+00E	.7	79.6	29.4	161	.2	184.7	41.6	3074	5.17	19.4	.4	8.2	1.9	46	1.8	1.5	.3	106	.67	.269	7	160	1.73	567	.152	5	3.27	.019	.35	.4	.04	6.5	.3	.07	10	<.5
L54N 27+00E	.7	52.0	12.1	99	.2	36.3	14.1	525	2.97	34.0	1.0	7.4	4.6	36	.5	.5	.4	62	.40	.320	10	36	.70	221	.170	6	4.56	.023	.16	1.2	.02	3.4	.3	<.05	11	<.5
L54N 27+25E	.5	85.4	12.6	130	.3	55.8	27.6	978	4.77	17.3	.6	1.8	3.0	47	.7	.7	.3	112	.49	.284	7	112	1.99	324	.205	2	4.36	.022	.44	.3	.03	5.1	.3	.06	13	<.5
L54N 27+50E	.5	74.6	13.4	127	.2	44.6	22.9	1366	4.03	19.8	.6	5.3	2.7	44	.8	1.5	.3	95	.63	.223	7	59	1.36	399	.177	4	3.50	.025	.25	.5	.04	3.8	.2	<.05	11	<.5
L54N 27+75E	.6	56.6	12.4	142	<.1	43.2	21.2	1810	3.71	10.6	.4	1.7	2.9	31	1.2	.9	.3	80	.50	.280	8	42	1.03	425	.155	5	3.53	.026	.21	.3	.03	6.1	.2	.06	10	<.5
L54N 28+00E	1.0	88.9	12.7	125	.1	44.5	22.3	776	4.19	19.8	1.2	2.9	3.9	35	1.0	1.8	.3	109	.53	.108	15	55	1.40	228	.195	4	4.59	.029	.26	.6	.03	6.5	.5	.06	12	.5
L54N 28+25E	.9	81.8	42.0	190	.2	83.6	29.4	2047	4.87	14.8	.5	3.2	1.7	53	1.7	1.7	.3	136	.90	.145	7	131	1.97	411	.155	5	4.06	.021	.21	.2	.06	11.4	.4	.07	12	<.5
L54N 28+50E	2.5	77.8	17.5	185	.2	114.3	27.9	2067	4.94	28.9	.8	1.9	2.2	66	1.9	2.4	.2	132	.65	.159	9	162	1.98	281	.140	3	4.52	.030	.21	.3	.03	9.9	1.3	.08	13	.7
L54N 28+75E	10.7	70.5	23.5	218	.1	28.3	23.6	2507	4.18	95.6	.7	3.9	2.7	62	2.2	2.7	.4	92	.59	.216	11	36	1.22	275	.114	4	3.35	.014	.27	.4	.03	5.6	.4	<.05	10	<.5
L54N 29+00E	1.0	68.1	36.1	141	.2	33.6	19.5	1721	3.38	52.0	1.0	8.1	3.7	51	1.5	1.4	.5	84	.52	.222	15	52	.94	292	.136	3	3.06	.018	.26	.7	.04	4.4	.3	.07	9	<.5
L54N 29+25E	1.0	67.5	36.1	187	.1	36.8	20.7	3018	3.84	41.2	.6	3.3	3.3	52	1.9	2.0	.5	98	.54	.171	13	53	1.08	337	.151	3	3.10	.022	.29	.6	.04	4.9	.3	<.05	10	.5
L54N 29+50E	1.1	68.2	23.8	140	.2	35.7	21.6	1329	3.74	37.0	.9	6.9	3.9	43	1.0	1.8	.5	87	.47	.131	16	53	.96	250	.164	4	3.65	.023	.25	.6	.04	5.0	.4	.08	11	.5
L54N 29+75E	.7	42.5	11.6	113	<.1	35.5	16.5	693	3.17	28.2	.6	3.5	4.2	35	.5	1.1	.5	75	.42	.100	11	42	.75	169	.154	3	2.80	.029	.22	1.2	.02	3.7	.2	.06	8	<.5
L54N 30+00E	.8	46.2	12.7	165	.2	30.8	15.6	1249	2.94	28.2	.8	8.8	3.2	44	1.8	.9	.5	69	.46	.291	14	39	.66	309	.115	4	2.82	.022	.21	1.0	.02	3.6	.3	<.05	8	<.5
L54N 30+25E	.8	84.2	15.0	193	.3	32.7	19.4	1052	3.29	46.7	1.2	56.3	3.3	63	2.1	1.1	1.0	79	.63	.248	15	36	.74	230	.125	3	2.92	.023	.22	1.1	.03	3.7	.3	.07	9	.7
L54N 30+50E	.8	72.7	11.9	107	.3	33.8	15.9	414	3.09	43.0	.8	14.6	4.8	51	.5	.9	.6	75	.58	.095	17	42	.78	120	.162	2	2.96	.038	.23	1.0	.02	4.5	.3	<.05	9	.6
L54N 30+75E	1.9	49.0	30.3	417	.2	53.4	23.3	901	4.12	62.5	1.0	3.4	2.8	71	3.1	3.3	.5	78	.72	.381	10	34	.74	183	.121	5	3.69	.026	.21	.6	.04	4.3	.4	<.05	10	.8
L54N 31+00E	.7	55.4	33.7	239	<.1	53.8	17.4	1104	3.38	25.1	.5	10.3	3.3	60	2.5	1.8	.5	83	.78	.160	12	52	.90	158	.142	4	2.45	.031	.22	.8	.04	4.1	.4	<.05	7	<.5
L54N 31+25E	.8	68.9	27.9	151	.5	43.5	22.2	930	3.94	41.1	1.1	8.2	4.0	82	1.3	2.5	.5	102	.94	.182	15	54	1.14	188	.158	2	3.09	.036	.36	1.0	.04	5.5	.4	.07	10	.5
L54N 31+50E	1.0	55.8	19.6	148	<.1	45.5	21.1	1118	3.75	35.9	.9	10.6	4.7	53	.8	2.0	.6	90	.40	.185	16	54	.99	226	.166	2	3.92	.018	.35	1.0	.02	4.7	.4	.06	11	<.5
RE L54N 31+50E	.9	57.4	20.4	146	<.1	47.4	21.0	1147	3.79	37.1	1.0	4.5	4.9	53	.9	2.1	.6	89	.41	.184	16	57	1.03	226	.174	4	3.66	.017	.35	1.0	.02	4.6	.4	<.05	11	<.5
L54N 31+75E	.8	49.6	15.7	130	.2	33.5	16.5	1617	3.07	23.4	.7	26.0	3.5	63	.9	1.6	.5	68	.64	.282	12	36	.70	301	.139	6	3.09	.018	.26	.8	.05	3.5	.2	<.05	9	<.5
L54N 32+00E	.6	49.0	10.6	102	.2	92.0	20.5	698	3.39	14.5	.5	10.5	4.1	43	.5	.9	.8	76	.40	.169	11	103	1.22	379	.197	2	3.05	.018	.50	.9	.02	4.5	.3	<.05	10	<.5
L53N 27+00E	1.0	67.0	36.6	148	.1	24.0	24.2	2309	4.28	32.9	.6	3.1	2.7	70	1.4	1.6	.3	119	.68	.254	9	41	1.39	345	.184	3	3.68	.027	.31	.4	.04	7.2	.3	<.05	12	<.5
L53N 27+25E	1.4	89.7	31.1	150	.2	24.1	28.3	2590	5.38	28.6	.6	2.5	2.7	70	1.2	1.6	.2	157	.65	.123	11	43	1.79	317	.195	4	4.25	.029	.35	.2	.05	11.2	.3	.06	14	<.5
L53N 27+50E	.9	72.9	19.6	94	.1	22.4	19.0	1332	4.28	20.4	.9	2.6	3.5	66	.8	2.0	.2	122	.49	.183	13	45	1.40	281	.179	3	4.67	.035	.46	.3	.03	9.2	.3	<.05	12	<.5
STANDARD DS7	21.2	109.4	70.6	404	.9	57.4	10.0	667	2.49	50.0	4.9	76.4	4.6	74	6.3	6.2	4.5	88	.98	.081	14	263	1.07	394	.128	42	1.03	.101	.48	3.9	.20	6.5	7.4	.82	5	3.8

GROUP 1DX - 15.0 GM SAMPLE LEACHED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 300 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILIT
- SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DEC 05 2006

Data FA DATE RECEIVED: NOV 15 2006 DATE REPORT MAILED:.....

BRITISH COLUMBIA CERTIFIED ASSAYER Raymond Chan

ACME ANALYTICAL

Yellowstone Resources Ltd. PROJECT Bayoune & Rorsland FILE # A608562 Page 2

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.5	1.9	2.3	44	<.1	5.5	4.2	510	1.71	<.5	1.8	<.5	3.5	44	<.1	<.1	.1	35	.47	.084	5	55	.61	196	.114	1	.85	.052	.47	.1	<.01	1.8	.4	<.05	5	<.5
L53N 27+75E	1.0	47.4	18.8	115	.2	25.7	14.7	1252	3.09	26.6	.8	5.5	3.2	49	1.1	1.5	.4	77	.48	.292	12	33	.79	275	.118	3	2.92	.016	.21	.9	.03	3.7	.3	<.05	9	<.5
L53N 28+00E	.9	66.2	47.5	141	.2	26.8	18.7	1906	3.42	33.0	.9	414.5	3.1	51	2.0	1.7	.6	88	.43	.191	14	37	.89	269	.117	2	2.96	.014	.23	.9	.03	4.7	.3	<.05	9	<.5
L53N 28+25E	1.3	78.2	44.2	148	.2	28.0	21.0	2026	3.64	32.2	1.0	9.0	3.2	53	1.9	1.8	.5	99	.45	.154	16	39	.95	245	.123	2	3.37	.013	.24	.8	.04	5.3	.3	<.05	10	<.5
L53N 28+50E	1.1	52.7	47.6	142	.1	30.3	17.0	2013	3.07	25.9	.9	5.0	2.8	54	1.5	2.0	.5	73	.47	.241	13	38	.81	294	.129	3	2.88	.016	.22	.6	.04	3.7	.3	<.05	9	<.5
L53N 28+75E	.8	65.2	12.9	129	.1	32.0	22.9	1275	3.81	22.1	.9	3.5	3.4	48	.6	1.4	.3	93	.48	.173	13	49	1.26	280	.183	3	3.61	.019	.37	.5	.02	6.0	.3	<.05	11	.5
L53N 29+00E	1.0	67.2	13.1	121	.1	27.5	19.0	1176	3.38	29.3	1.0	8.9	3.9	50	.6	1.5	.4	86	.50	.208	14	36	.88	261	.147	2	3.19	.019	.26	.7	.03	4.8	.3	<.05	10	<.5
L53N 29+25E	.8	44.3	12.7	132	<.1	32.9	16.2	958	3.13	31.7	.6	5.9	3.9	47	.8	.8	.9	75	.57	.272	12	39	.76	309	.128	3	2.58	.019	.26	1.0	.02	3.7	.3	<.05	8	<.5
L53N 29+50E	.5	51.5	12.4	140	.2	38.8	16.2	1233	2.91	19.9	.6	9.5	3.6	64	1.4	.8	.5	63	.54	.329	13	35	.60	313	.105	3	2.21	.021	.23	1.1	.02	3.4	.2	<.05	7	<.5
L53N 29+75E	.7	70.7	15.1	142	.1	65.3	26.3	722	3.90	28.0	.7	317.2	4.0	53	.9	1.1	.5	89	.45	.232	13	69	1.59	189	.176	2	3.24	.027	.38	1.0	.03	5.0	.4	<.05	9	<.5
L53N 30+00E	.8	84.5	27.7	141	.1	29.6	24.5	2424	4.00	27.6	1.1	5.4	3.9	73	1.3	1.3	.4	95	.54	.319	14	43	1.05	331	.168	4	3.95	.019	.35	.6	.04	6.1	.3	<.05	12	<.5
L53N 30+25E	1.0	79.7	31.2	126	.1	28.5	20.9	1404	4.08	27.7	1.2	14.6	4.6	52	.9	1.4	.5	106	.41	.216	17	38	1.10	209	.180	2	4.02	.014	.34	.9	.03	5.8	.4	<.05	12	<.5
L53N 30+50E	1.5	119.2	14.1	113	<.1	34.5	27.1	2724	4.18	23.2	1.1	21.1	3.7	56	.6	1.5	.3	96	.44	.217	14	35	1.05	172	.180	2	3.92	.017	.27	1.1	.05	5.2	.4	<.05	11	<.5
L53N 30+75E	.6	66.7	12.5	119	.1	30.4	20.2	1287	3.55	18.1	1.1	4.9	3.9	64	.7	1.3	.4	81	.57	.161	14	30	.82	201	.168	3	3.70	.023	.29	.7	.04	4.7	.3	<.05	10	<.5
L53N 31+00E	.6	66.8	20.5	173	.1	35.3	20.4	1390	3.45	35.2	.9	45.2	4.3	68	1.7	1.8	.6	80	.68	.354	14	42	.85	286	.159	4	3.58	.018	.24	.9	.04	4.5	.3	<.05	10	<.5
L53N 31+25E	.8	65.7	30.9	173	.2	38.6	24.6	2469	3.99	31.1	.7	101.9	3.2	66	1.6	1.4	.5	92	.58	.344	12	40	1.11	371	.160	4	3.52	.019	.31	.7	.05	5.3	.3	<.05	11	.5
L53N 31+50E	.8	72.1	18.0	138	<.1	55.7	21.8	1089	3.92	25.9	.9	5.9	4.1	49	.7	1.4	.5	95	.48	.225	13	71	1.23	223	.177	3	3.83	.021	.29	.9	.03	5.3	.3	<.05	11	<.5
L53N 31+75E	.6	61.6	24.9	216	.1	63.0	22.4	1591	3.79	14.8	.6	41.3	4.1	74	1.7	1.3	.4	80	.66	.243	14	82	1.32	437	.174	4	3.14	.020	.36	.5	.04	5.2	.4	<.05	9	<.5
L53N 32+00E	.8	69.3	27.9	97	.1	66.7	21.3	1202	4.06	16.8	.9	4.7	4.1	54	.7	1.2	.4	93	.46	.098	19	112	1.58	363	.207	2	3.73	.017	.72	.7	.02	8.5	.4	<.05	10	<.5
RE L53N 32+00E	.8	72.3	27.3	103	.1	69.5	23.3	1244	4.30	17.2	.8	2.4	4.1	55	.6	1.2	.4	94	.46	.097	19	116	1.58	371	.216	2	3.73	.018	.73	.6	.03	8.4	.4	<.05	11	<.5
L52+50N 27+00E	.9	50.0	57.4	155	.2	34.9	18.4	1997	3.49	28.9	.7	9.9	2.6	49	1.7	2.0	.5	88	.56	.305	10	54	1.10	349	.138	3	3.18	.015	.24	.6	.04	4.4	.3	<.05	10	<.5
L52+50N 27+25E	.9	27.9	39.8	183	.2	31.2	14.9	2421	2.65	18.1	.6	3.0	2.5	65	1.4	1.0	.4	46	.60	.565	12	25	.49	526	.112	5	2.98	.022	.16	.8	.04	3.4	.2	<.05	8	<.5
L52+50N 27+50E	1.1	64.3	20.4	174	.1	26.0	27.3	3409	4.40	19.5	.7	18.0	2.9	99	1.1	1.6	.4	99	.82	.413	14	50	1.07	496	.137	3	3.24	.020	.24	.4	.04	6.5	.3	.07	11	.6
L52+50N 27+75E	.9	58.3	70.6	161	.1	32.2	21.0	2003	3.74	26.6	.8	133.5	3.4	54	2.1	1.9	.6	98	.49	.219	15	54	1.05	310	.153	3	3.20	.015	.36	.7	.03	5.1	.3	.06	10	<.5
L52+50N 28+00E	.9	70.5	37.1	115	.1	30.1	22.0	1408	4.10	27.5	.9	41.1	4.0	54	1.1	1.6	.5	116	.47	.166	16	48	1.12	263	.159	3	3.29	.017	.53	1.1	.03	6.8	.3	<.05	10	<.5
L52+50N 28+25E	.8	71.3	59.4	145	.2	27.9	26.7	2342	4.88	21.2	.7	2.6	2.9	67	1.8	1.6	.4	135	.53	.217	14	64	1.76	329	.209	3	3.81	.018	.52	.4	.03	7.8	.3	<.05	12	<.5
L52+50N 28+50E	.7	81.6	56.7	149	.2	27.1	23.0	1944	3.97	22.8	1.0	4.1	3.5	59	1.8	1.6	.5	106	.55	.203	14	46	1.13	327	.158	2	3.28	.017	.42	.6	.03	5.7	.3	<.05	10	<.5
L52+50N 28+75E	.6	71.6	28.8	153	<.1	31.6	22.3	2590	4.16	18.4	.5	.8	3.5	77	1.4	1.5	.3	98	.79	.259	11	41	1.23	362	.163	5	3.50	.024	.36	.5	.04	5.8	.3	<.05	11	<.5
L52+50N 29+00E	.8	99.4	17.8	140	.2	32.4	27.4	2016	4.99	24.0	.9	6.7	3.7	49	.8	1.7	.4	131	.45	.157	13	45	1.47	251	.195	2	3.81	.020	.43	.9	.03	7.5	.4	.07	12	<.5
L52+50N 29+25E	.9	83.4	20.0	154	.1	32.4	29.3	2870	5.14	23.8	.7	2.3	3.2	72	1.0	2.2	.3	121	.70	.307	11	36	1.42	318	.175	4	4.04	.017	.43	.4	.05	7.8	.4	.06	13	<.5
L52+50N 29+50E	.6	103.0	36.1	222	.1	37.1	34.9	3057	4.76	15.9	.7	.8	3.1	75	1.4	1.7	.4	99	.59	.292	11	42	1.38	409	.174	3	3.84	.019	.41	.3	.04	6.2	.3	.06	11	<.5
L52+50N 29+75E	.7	65.1	17.4	131	.1	49.6	21.4	1706	3.63	28.1	.9	6.8	3.9	59	.7	1.1	.5	88	.63	.235	14	73	1.17	326	.162	3	3.22	.016	.38	1.0	.03	4.6	.3	<.05	9	<.5
L52+50N 30+00E	.9	71.6	39.4	238	.2	28.6	24.7	4292	3.74	21.6	.5	5.4	2.5	130	2.4	2.1	.4	75	1.25	.533	9	29	.98	822	.125	6	2.87	.025	.33	.3	.06	4.5	.3	<.05	9	.5
L52+50N 30+25E	.8	64.4	55.0	158	.1	27.8	18.2	1709	3.30	35.7	.8	6.4	3.7	51	2.2	1.8	.7	80	.40	.242	14	35	.79	268	.133	2	3.00	.016	.28	1.1	.04	4.1	.3	<.05	9	<.5
L52+50N 30+50E	.8	77.1	35.7	159	.1	28.0	21.8	2456	3.55	13.6	.8	2.9	3.5	61	1.5	1.5	.4	79	.44	.138	12	29	.90	361	.168	3	3.52	.022	.35	.4	.04	5.2	.3	<.05	10	<.5
STANDARD DS7	21.1	109.2	69.8	400	.9	55.4	9.8	654	2.49	50.6	4.9	69.4	4.5	75	6.6	6.3	4.5	88	.99	.080	14	264	1.05	385	.129	40	1.01	.104	.46	4.0	.20	2.6	4.3	.23	5	3.6

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.5	2.2	2.3	45	<.1	5.6	4.3	503	1.73	<.5	1.8	<.5	3.3	46	<.1	<.1	.1	36	.48	.086	6	58	.59	193	.115	1	.84	.048	.44	<.1	<.01	2.0	.3	<.05	5	<.5
L52+50N 30+75E	.7	90.5	29.9	241	.1	32.6	32.3	2918	3.94	13.9	.7	2.6	2.8	122	1.6	1.3	.5	75	.99	.394	10	33	1.19	424	.150	3	3.31	.014	.34	.4	.05	5.0	.3	.09	10	.5
L52+50N 31+00E	.7	72.9	28.0	118	.1	36.1	18.0	1427	3.29	20.6	1.1	12.0	4.1	49	.9	1.3	.6	76	.38	.198	15	38	.80	234	.168	2	3.63	.016	.23	1.1	.03	5.2	.3	<.05	10	<.5
L52+50N 31+25E	.8	53.9	19.9	127	<.1	27.3	17.3	1890	3.31	22.9	1.1	17.3	3.9	50	.8	1.4	.5	73	.46	.280	16	35	.79	240	.152	2	3.63	.017	.18	.7	.05	4.6	.3	<.05	10	.5
L52+50N 31+50E	.7	55.8	28.4	120	<.1	31.2	18.3	1923	3.53	18.7	1.0	3.8	3.7	51	.9	1.2	.4	84	.38	.217	14	36	.91	308	.163	3	3.82	.016	.30	.5	.04	5.5	.3	<.05	11	<.5
RE L52+50N 31+50E	.6	58.4	28.5	121	<.1	31.2	19.0	2033	3.69	18.3	1.1	3.6	3.7	53	.9	1.2	.4	87	.36	.247	15	36	.92	314	.166	2	4.20	.017	.30	.6	.04	5.6	.3	<.05	11	<.5
L52+50N 31+75E	.8	75.1	50.2	137	<.1	22.5	15.0	1715	2.89	19.7	.8	5.3	3.0	51	1.5	1.7	.5	61	.43	.195	13	23	.64	166	.148	2	3.22	.015	.20	.4	.05	4.4	.2	<.05	8	.6
L52+50N 32+00E	.5	70.5	19.5	111	.1	125.8	32.7	934	5.29	13.9	.7	7.3	4.5	48	.4	.9	.3	114	.47	.116	21	214	2.92	325	.265	1	3.81	.016	.58	.4	.02	9.7	.4	<.05	12	<.5
L52N 27+00E	.6	52.2	14.0	130	<.1	34.3	17.0	1519	3.16	22.9	.7	8.5	3.3	55	1.0	1.1	.5	78	.50	.276	13	43	.91	394	.139	2	2.57	.017	.26	.9	.02	4.8	.2	<.05	8	<.5
L52N 27+25E	.8	34.9	14.9	154	.1	26.9	14.2	1569	2.68	20.3	.5	68.8	2.7	58	1.0	.9	.4	59	.48	.366	12	28	.59	341	.108	3	2.37	.019	.19	.9	.02	3.5	.2	<.05	8	<.5
L52N 27+50E	.7	67.4	17.8	119	.1	32.0	19.9	1569	3.82	23.7	.8	2.6	3.4	74	.8	1.2	.4	96	.65	.264	15	50	.99	302	.145	3	2.89	.014	.38	.8	.01	6.1	.3	<.05	10	<.5
L52N 27+75E	.9	79.3	27.4	142	.2	52.7	32.3	2679	5.70	19.1	.8	1.4	3.6	63	.9	1.4	.3	137	.57	.169	23	186	2.26	363	.216	2	4.35	.016	.53	.3	.02	10.7	.4	.07	13	<.5
L52N 28+00E	1.1	86.0	30.7	136	.1	27.7	27.9	2266	5.45	18.0	.8	3.4	3.2	70	1.0	1.9	.4	144	.52	.188	16	49	1.67	334	.194	2	4.15	.019	.76	.6	.02	10.8	.4	.08	13	<.5
L52N 28+25E	.8	102.5	20.7	212	.1	59.2	40.5	2461	5.80	16.6	.4	2.2	3.0	90	1.1	1.5	.2	132	.87	.275	14	103	2.04	345	.208	5	4.34	.028	.41	.2	.03	11.0	.4	.07	14	.5
L52N 28+50E	.6	65.5	13.2	139	.2	35.5	22.2	872	3.92	14.6	.5	2.4	3.5	63	.5	1.3	.3	87	.57	.247	11	39	1.16	231	.168	5	3.18	.031	.36	.5	.02	6.2	.3	<.05	11	<.5
L52N 28+75E	.8	68.1	16.1	193	.2	28.1	26.8	2676	4.24	15.8	.5	1.1	2.6	68	.9	1.5	.3	88	.67	.188	11	29	1.09	320	.165	4	3.26	.021	.39	.3	.04	7.5	.3	.08	11	<.5
L52N 29+00E	.8	64.9	14.4	129	.1	29.6	20.6	885	4.06	27.6	.6	61.6	3.3	50	.6	1.3	.3	91	.55	.106	11	33	1.02	182	.189	4	3.56	.024	.31	.6	.02	5.1	.3	.11	11	<.5
L52N 29+25E	.6	44.4	13.3	111	.1	29.7	16.5	1190	3.08	33.7	.6	6.1	3.4	53	.7	.8	.5	67	.60	.205	11	30	.66	239	.144	4	2.52	.020	.26	.9	.03	4.0	.2	.09	8	<.5
L52N 29+50E	.7	55.7	18.2	146	.1	28.1	19.7	2083	3.52	16.3	.7	3.0	2.7	60	1.0	1.0	.4	79	.55	.270	11	32	.81	353	.147	3	2.98	.015	.21	.6	.04	3.7	.2	.08	9	<.5
L52N 29+75E	.6	51.1	31.3	152	.1	24.8	14.9	2875	3.29	21.6	.7	2.0	3.2	58	1.6	1.1	.4	62	.56	.357	10	25	.67	488	.155	5	3.58	.017	.22	.4	.05	4.5	.2	.08	10	<.5
L52N 30+00E	.6	56.3	29.2	123	.1	22.6	17.4	2245	2.95	18.7	.6	10.5	3.6	65	1.3	1.2	.5	61	.62	.389	11	25	.65	531	.129	4	2.74	.017	.25	.6	.05	4.0	.2	.08	8	<.5
L52N 30+25E	.5	58.0	12.8	166	.2	23.7	14.3	2567	2.78	17.5	.4	2.8	2.8	146	1.6	.9	.4	54	1.51	.583	11	28	.67	709	.113	9	2.46	.014	.30	.5	.05	3.8	.2	.10	7	<.5
L52N 30+50E	.4	42.2	15.7	186	.3	20.2	14.6	2271	2.87	13.5	.6	247.2	3.7	105	1.0	.8	.4	45	.81	.499	12	23	.65	695	.131	4	2.62	.021	.23	.3	.08	4.4	.2	.08	7	.5
L52N 30+75E	.7	60.7	22.0	103	.1	39.5	21.0	1070	3.59	21.4	.7	6.4	4.2	51	.8	1.1	.6	90	.39	.133	18	50	1.11	214	.165	2	2.88	.015	.34	.9	.01	5.3	.3	<.05	9	<.5
L52N 31+00E	.8	65.7	15.3	111	.2	30.1	18.7	1035	3.36	19.4	1.0	144.6	3.7	49	.7	.9	.5	79	.52	.123	18	40	.88	193	.161	2	3.30	.020	.35	.7	.02	4.8	.3	.06	9	<.5
L52N 31+25E	.4	50.7	14.8	119	.1	48.6	18.9	1167	3.35	13.0	.7	3.2	3.7	47	.7	.7	.4	70	.41	.161	15	65	1.19	291	.174	2	3.40	.019	.37	.4	.02	4.8	.3	<.05	9	<.5
L52N 31+50E	.6	70.9	27.5	119	.1	32.2	16.9	1138	3.62	34.5	1.0	3.9	3.9	72	1.2	2.7	.5	88	.65	.190	14	39	.99	222	.167	5	3.50	.017	.26	.5	.05	6.5	.2	.06	10	<.5
L52N 31+75E	.5	60.2	18.2	103	.2	42.0	19.0	1687	3.69	16.9	.9	3.3	3.6	49	.6	1.1	.4	87	.34	.146	14	56	1.09	254	.195	3	3.80	.018	.25	.4	.04	6.6	.2	<.05	11	<.5
L52N 32+00E	.6	56.6	23.9	140	.1	25.2	18.6	2842	3.35	14.0	.6	1.8	2.6	99	1.0	1.1	.3	66	.77	.199	10	32	.91	314	.158	3	2.86	.017	.26	.3	.05	4.4	.3	<.05	11	<.5
L51N 28+00E	.4	100.1	77.2	178	.2	44.1	21.2	2072	3.47	14.4	.5	254.4	1.9	100	2.8	1.3	.4	68	.95	.187	8	62	1.42	287	.145	5	2.85	.018	.27	.2	.08	2.9	.2	<.05	8	<.5
L51N 28+25E	.8	65.2	12.9	102	.2	24.2	15.0	1095	3.13	17.9	.8	8.5	2.7	48	.6	1.8	.4	68	.41	.232	9	35	.73	160	.152	2	3.76	.014	.17	.5	.05	3.5	.2	<.05	11	.5
L51N 28+50E	.3	43.7	24.2	160	.2	26.6	15.7	1260	2.78	8.3	.5	16.8	3.0	142	1.2	1.0	.3	45	1.02	.751	13	26	.66	813	.119	5	2.49	.024	.19	.3	.06	4.4	.2	<.05	7	<.5
L51N 28+75E	.5	61.7	17.0	126	.1	27.6	21.1	1037	3.72	9.4	.6	11.6	3.3	65	.6	.7	.3	70	.47	.205	12	44	1.06	192	.173	3	3.74	.031	.36	.3	.02	4.6	.3	<.05	11	<.5
L51N 29+00E	.6	62.3	44.3	122	.1	30.9	23.5	1513	4.40	11.3	.7	4.1	3.9	64	1.0	1.5	.4	97	.60	.090	18	73	1.37	265	.232	3	3.49	.019	.68	.5	.04	7.3	.4	<.05	12	<.5
L51N 29+25E	.4	63.7	18.8	100	.1	41.2	26.7	1284	5.06	5.9	.9	38.4	4.2	80	.6	.9	.2	108	.51	.094	21	128	1.92	290	.286	2	4.72	.018	.78	.3	.02	9.0	.4	<.05	14	<.5
STANDARD DS7	20.4	107.2	69.9	401	.8	55.0	9.6	637	2.43	49.1	5.0	67.4	4.5	73	6.6	6.1	4.5	84	.91	.080	13	241	1.03	374	.122	39	.97	.092	.45	3.9	.19	2.4	4.3	.22	5	3.7

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	S pp
G-1	.5	2.1	2.4	43	<.1	5.2	4.1	479	1.66	<.5	1.8	<.5	3.4	45	<.1	<.1	.1	35	.45	.081	5	59	.57	195	.111	1	.80	.052	.49	.1	<.01	2.3	.4	<.05	5	<.
L51N 29+50E	.7	86.9	185.4	237	.2	18.6	24.5	5390	3.02	20.7	.4	5.1	2.0	107	6.3	4.7	.9	59	1.33	.144	13	36	.83	631	.118	3	2.24	.024	.25	.3	.13	4.3	.4	<.05	6	<.
L51N 29+75E	.3	52.8	14.0	135	.2	24.2	16.3	911	2.80	7.1	.3	7.7	2.7	165	1.1	.6	.3	49	2.43	.641	9	52	.94	613	.148	8	2.65	.012	.22	.4	.34	2.5	.2	<.05	7	<.
L51N 30+00E	.4	81.5	16.9	130	.2	34.4	19.3	1054	3.41	10.0	.6	2.7	2.3	59	.7	.7	.3	68	.67	.346	8	30	1.26	335	.140	3	3.13	.019	.28	.3	.03	3.2	.2	<.05	9	<.
L51N 30+25E	.5	64.0	38.0	136	.1	19.7	15.6	1835	3.27	12.0	.8	2.9	3.4	39	1.2	1.4	.4	70	.32	.367	11	24	.70	296	.159	4	3.88	.017	.20	.5	.02	3.5	.2	<.05	10	<.
L51N 30+50E	.6	42.9	67.7	255	.2	29.0	19.9	2317	2.52	27.9	.6	2.5	3.3	68	3.2	1.5	.5	39	.33	.607	8	22	.45	374	.122	3	3.15	.013	.13	4	.07	2.8	.3	<.05	8	<.
L51N 30+75E	.7	50.4	22.3	145	.2	34.9	16.8	1385	3.21	25.0	1.0	8.1	3.0	42	1.0	1.2	.5	71	.36	.367	12	41	.82	284	.140	2	3.47	.015	.21	.7	.04	3.5	.2	<.05	10	<.
L51N 31+00E	.6	48.4	15.4	120	.1	38.4	17.2	904	3.17	24.2	.8	4.0	3.5	34	.7	.5	.5	68	.29	.350	12	46	.91	231	.143	2	2.94	.017	.27	.8	.03	3.4	.3	<.05	8	<.
L51N 31+25E	.5	52.9	25.2	155	.1	37.3	16.6	1220	2.92	19.6	.7	11.0	3.5	63	2.1	.9	.6	65	.54	.354	14	38	.71	339	.124	2	2.55	.017	.22	1.0	.03	3.5	.3	<.05	7	<
L51N 31+50E	.9	56.1	75.9	232	.2	30.1	15.4	2572	2.72	27.1	.7	3.1	2.9	63	3.6	2.0	.8	62	.67	.359	13	34	.64	381	.111	6	2.48	.018	.25	.9	.06	3.2	.3	<.05	7	<.
L51N 31+75E	.8	51.8	43.0	161	.2	33.0	16.4	968	3.07	22.1	.8	5.9	2.8	55	1.2	1.1	.5	67	.50	.283	13	39	.68	261	.129	4	2.80	.019	.27	.5	.06	4.1	.3	<.05	8	<.
L50N 28+00E	.9	52.4	92.7	156	.2	33.0	15.8	1533	2.86	25.9	.7	788.0	2.9	51	2.5	1.4	.8	68	.37	.249	13	38	.66	354	.126	3	2.53	.017	.23	.9	.04	3.4	.3	<.05	7	<.
L50N 28+25E	.6	60.6	22.1	145	.1	36.0	18.4	1203	3.18	23.2	.7	6.3	3.6	73	1.7	.8	.6	75	.61	.300	14	43	.72	363	.124	4	2.44	.015	.27	1.0	.03	3.7	.2	<.05	7	<.
L50N 28+50E	.7	44.9	37.1	133	.2	32.3	17.3	1195	3.05	21.7	.6	5.3	3.6	56	1.4	1.4	.5	75	.59	.208	11	44	.80	301	.135	5	2.26	.021	.36	.9	.03	3.4	.3	<.05	7	<.
L50N 28+75E	.6	33.6	34.1	128	<.1	34.7	17.3	1610	3.24	11.5	.6	3.9	3.3	54	1.0	1.0	.5	71	.47	.198	11	49	.86	344	.150	3	2.89	.014	.35	.6	.03	3.7	.3	<.05	9	<.
L50N 29+00E	.8	38.2	18.3	141	.2	82.0	23.5	1930	3.78	9.8	.6	2.1	3.8	58	1.1	.9	.4	78	.71	.187	12	124	1.64	439	.213	4	3.86	.015	.46	.4	.04	5.2	.3	<.05	10	<.
L50N 29+25E	.5	32.9	17.8	151	.3	29.9	16.6	1978	3.27	10.5	.4	35.1	3.0	70	1.5	.8	.4	61	.73	.373	9	45	.80	471	.160	4	3.64	.018	.25	.3	.05	3.7	.2	<.05	10	<.
L50N 29+50E	.7	39.2	83.3	238	.2	36.4	13.1	838	2.58	18.3	.5	7.5	3.2	60	3.0	2.1	.6	52	.73	.316	9	37	.61	208	.145	4	2.78	.022	.21	.6	.06	3.7	.3	<.05	7	<.
L50N 29+75E	.7	29.7	45.1	291	.2	36.9	15.5	1485	2.77	23.1	.6	6.4	2.8	58	2.8	2.0	.6	54	.62	.390	9	39	.61	426	.131	4	2.41	.019	.20	.6	.06	3.1	.2	<.05	7	<.
L50N 30+00E	.5	49.6	19.6	133	.2	37.6	15.7	624	2.94	33.1	1.0	6.7	4.3	38	.8	.9	.5	66	.40	.303	15	39	.66	249	.157	3	3.35	.020	.20	1.2	.03	3.6	.2	< 05	9	<.
L50N 30+25E	.6	60.1	12.6	128	.1	31.7	14.8	560	2.74	21.9	1.3	6.2	4.4	33	.6	1.0	.4	59	.34	.192	17	40	.64	213	.161	3	2.92	.029	.20	.8	.03	4.0	.3	<.05	8	<.
L50N 30+50E	.9	57.3	33.6	130	.1	34.3	16.7	557	2.99	28.9	.8	3.6	4.2	44	.5	1.7	.6	78	.35	.202	13	42	.70	183	.156	3	2.33	.020	.27	1.1	.03	4.1	.2	< 05	7	<.
120	.1	2.3	11.3	38	.2	4.3	6.9	403	1.84	1.4	15.6	3.8	4.7	32	.2	.1	<.1	34	.41	.103	18	7	.64	69	.087	1	1.91	.019	.21	.1	.02	1.6	.2	<.05	4	<.
130	.2	4.7	42.8	75	.2	6.7	9.5	668	2.40	2.3	11.4	43.9	5.2	35	.3	.1	.2	44	.45	.087	17	9	.89	88	.128	1	2.19	.018	.36	.1	.02	1.7	.2	<.05	5	<.
140	.4	11.1	69.1	118	.6	7.3	7.1	815	2.17	4.2	34.5	13.1	1.7	27	.5	.2	.2	38	.29	.092	23	10	.42	77	.088	2	3.40	.016	.12	.1	.07	2.0	.2	.07	8	<.
150	.4	7.0	30.2	90	.2	6.6	6.4	458	2.29	4.3	3.9	29.7	1.7	19	.3	.1	.2	38	.21	.068	13	9	.54	81	.070	1	2.64	.012	.10	.1	.04	1.6	.1	<.05	7	<.
160	.2	5.0	8.9	32	<.1	4.5	5.5	290	1.61	3.1	4.6	10.1	3.7	20	.1	.1	.1	26	.24	.112	14	6	.44	42	.062	1	1.92	.018	.11	.1	.03	1.7	.1	<.05	4	<.
170	.3	4.5	9.9	40	.1	5.0	5.8	306	1.88	1.8	3.4	1.9	2.7	18	.1	.1	.1	30	.24	.104	13	7	.52	59	.055	1	2.31	.010	.10	.1	.03	1.6	.1	<.05	5	<.
180	.3	7.7	13.4	62	.1	8.5	7.4	532	2.19	2.5	20.3	1.4	2.0	28	.2	.1	.2	40	.35	.100	21	12	.54	93	.088	1	3.13	.012	.13	.1	.05	1.6	.2	.08	7	<.
190	.2	5.2	10.5	52	.1	6.9	7.4	394	2.07	2.0	13.2	.8	2.5	23	.2	.1	.1	38	.30	.096	20	9	.69	108	.083	1	2.99	.013	.18	1	.04	1.6	.2	.06	6	<.
200	.2	3.7	10.4	36	<.1	4.8	6.6	324	1.85	1.6	1.7	2.9	5.7	29	.1	.1	.1	32	.30	.108	17	6	.57	52	.069	1	2.65	.015	.14	.1	.04	1.8	.1	.06	4	<.
210	.3	5.8	11.0	48	<.1	6.3	5.9	377	1.99	2.1	3.5	1.2	2.7	24	.1	.1	.1	38	.27	.069	12	9	.43	66	.097	1	2.39	.013	.10	.2	.05	1.5	.1	.06	7	<.
220	.2	4.7	13.6	57	<.1	7.1	8.5	589	2.40	1.5	4.4	1.1	3.6	37	.1	.1	.1	43	.44	.094	15	10	.83	126	.109	1	2.52	.014	.29	.1	.03	1.6	.3	.07	7	<.
230	.4	6.7	18.4	61	.2	8.2	8.7	528	2.61	1.7	5.8	.8	3.5	58	.2	.1	.1	45	.57	.070	14	10	.78	125	.112	1	4.23	.013	.27	.1	.05	1.9	.2	<.05	9	<.
RE 230	.4	6.4	18.5	60	.1	7.8	8.5	504	2.48	1.7	5.6	<.5	3.5	54	.2	.1	.1	45	.53	.068	13	10	.78	118	.101	1	3.94	.013	.25	.1	.05	1.7	.2	.06	8	<.
STANDARD DS7	21.0	108.1	69.0	396	.9	55.7	9.7	632	2.41	49.5	4.9	62.3	4.4	75	6.5	6.0	4.4	87	.97	.080	13	243	1.07	385	.128	39	1.03	.097	.47	3.8	.19	2.6	4.2	.22	5	3

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.