# SUMMARY REPORT OF THE 2006 FIELD PROGRAM

# (FILED FOR ASSESSEMENT WORK)

ON THE

**CROWSNEST PROPERTY** FORT STEELE MINING DIVISION, BC

NTS: 82G017, 82G018 Latitude 49 degrees 09' N, Longitude 114 degrees 33' W (centre)

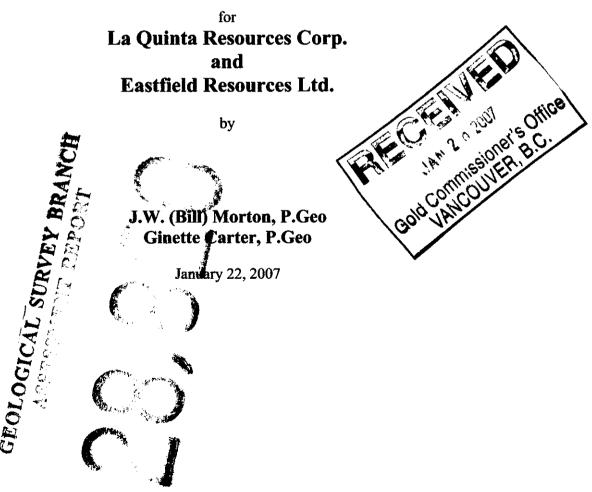


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- Appendix A High grade float table
- Appendix B Crowsnest Trench Au-Ag Intervals
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#### Summary

An exploration program consisting of road reconstruction and mechanical trenching was initiated on the Crowsnest property in June 2006. The Crowsnest property is underlain by a thick sequence of Pennsylvanian and Mississippian carbonate and clastic rocks, of which the Mississippian Rundle Group shows the greatest exposure. Mid-Cretaceous syenite and trachyte intrusions as sills, dykes, plugs and possible diatremes intrude these units.

The object of the 2006 program was to trench untested soil gold anomalies and to provide further insight in the area peripheral to the upper trench (exposed in 1993 and reexposed in 1999). The lower trenches were designed to become drill roads for a possible later drill program and to allow access to higher elevations along the slope where it is believed that high-grade mineralized float may be sourcing from. The existing exploration road was, at the same time, repaired as required.

Although the results of the trenching were largely disappointing a new model has been developed which interprets a structure higher up the slope providing a possible source for mineralized float which has been discovered over a 2 kilometres stretch of the property over the last eighteen years. A review of the database calculates an average grade for samples of this float exceeding 1/g/t to be 32.656 g/t gold (based on 36 determinations) with a corresponding copper value of 0.23% (based on 34 determinations). The majority of mineralized samples in this population are from limonitic, pyritic or magnetite rich syenite / monzonite with and without quartz veining. The highest-grade sample in this population (#21714), collected in 1989 by Placer Dome Inc., is described as an intrusive breccia with a gold value of 524.41 g/t (15.20 ounces per ton). Clearly more exploration for probable multiple sources of this mineralization is warranted.

Mincord Exploration Consultants Ltd. of Vancouver provided the geological management for the project with Astraf Construction Ltd. of Jaffray BC providing a track-mounted excavator.

# **1 INTRODUCTION AND TERMS OF REFERENCE**

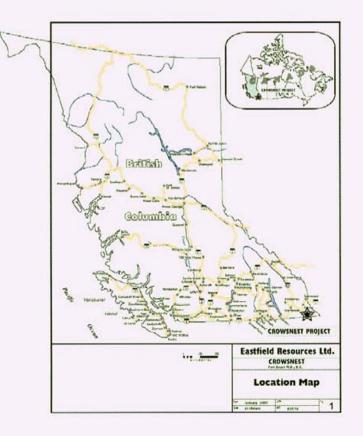
At the request of LaQuinta Resources Ltd., this report was prepared by Bill Morton and Ginette Carter, both P.Geo. to document and discuss the results of the 2006 trenching work conducted on the Crowsnest claim group located 50 kilometers southeast of Fernie, B.C. This report summarizes the fieldwork carried out on the claims and discusses the implication of this year's results on further exploration programs on the Crowsnest Property.

The purpose of the report is to qualify targets for future mineral exploration and development within the subject property.

The 2006 exploration report is based on fieldwork carried out by Ginette Carter, who was on site during the whole program from and supervised the project from July 4<sup>th</sup> to July 29<sup>th</sup>, 2006. This rest of the report is partly based on published and unpublished fieldwork reports carried out by various private sector mining company personnel and public sector government personnel. Current compilation of the geological and geochemical data undertaken by the author has led to recommendations for work on the Crowsnest mineral claims which include a 2 phase program involving further prospecting, geological mapping and trenching, and later drilling.

## 2 RELIANCE ON OTHER EXPERTS

No experts additional to Ginette Carter and Bill Morton were consulted for the 2006 program.



## **3 PROPERTY DESCRIPTION AND LOCATION**

The Crowsnest claim group is located 50 km southeast of Fernie, B.C. (Lat. 49° 10' N, Long. 114° 32' W) some 25 kilometres west of the Alberta boundary and 20 kilometres north of the Montana border within the Fort Steele Mineral Division. The Crowsnest property consists of 10 staked (unpatented) mineral claims totaling 2,388 hectares.

Eastfield Resources Ltd owns the Crowsnest property. In 2004 La Quinta Resources Corporation of Vancouver, BC, entered into an option agreement with Eastfield. By this agreement, La Quinta can earn up to 60 % of the Crowsnest Property by spending \$800,000 over four years, paying \$100,000 and issuing 150,000 shares.

A listing of claim tenures is as follows:

Claim Name	Record #	Area (hectares)	Expiry Date
Aubyrd 4	406552	375	Oct 31, 09
Aubyrd 5	406551	500	Oct 31, 09
Aubyrd 6	406550	500	Oct 31, 09
Aubyrd 7	406553	250	Oct 31, 09
Aubyrd 8	406554	150	Oct 31, 09
Crowsnest Lookout	504310	317	Jan 19, 10
Crowsnest Revenge	504297	85	Jan 19, 09
Connector	517530	127	Jul 12, 09
Lower Connector	520838	63	Oct 06, 09
Hilltop	549732	21	Jan 17, 08
Total area		2388	

TABLE I: Tenure Table

All claims are located in the Fort Steele Mining Division

## 4 ACCESSIBILITY, CLIMATE, LOCAL RESOURCES, INFRASTRUCTURE AND PHYSIOGRAPHY

Road access to the property is via a series of major logging roads that lead southerly from Highway 3 at Morrissey approximately 15 kilometres southwest of the town of Fernie (the Lodgepole, Harvey and Flathead forest access roads progressively lead into each other). At the 71-kilometre road marker, on the right side of the road, the Crowsnest property road initially follows a seismic line in a westerly direction and then turns northerly into the "B" grid area of the property. Elevations on the claim group range from 1320 metres at the Flathead River to 2100 metres at the highest point on the property.

Vegetation is dominated by pine with lesser larch and Douglas fir at the lower elevations and deciduous brush and alpine grasses at higher elevations. Extensive clearcut logging has occurred over the last twenty years in much of the mature timber in the

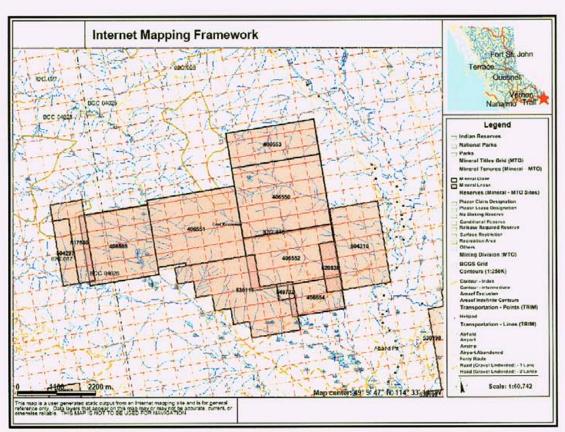


Figure 2: Crowsnest Claims Location

Flathead Valley and its tributary drainages with immature pine remaining in much of the remainder. Snow is typically gone by the third week of May and returns about the first week of November.

## **5 HISTORY**

Early exploration in the vicinity of the Crowsnest project was almost exclusively for hydrocarbons. In the early 1900's oil seeps on Sage Creek, located approximately ten kilometers southeast of the southeast corner of the Crowsnest claims (on the opposite side of the Flathead valley) attracted the attention of early oil exploration groups and a number of wooden derricks were constructed on site. None of these early wells however encountered commercial quantities of oil and the rigs were eventually abandoned. In the nineteen fifties Shell Canada completed a 3500 metre oil and gas wildcat seven kilometers to the northeast of the claims, Pacific Atlantic Oil completed a 2,700 metre test nine kilometers to the east of the claims and in 1971 Imperial Oil completed a 1400 metre wildcat fifteen kilometers to the northwest of the claims (on Harvey Creek at the Howell Creek road junction). In the late 1980's and early 1990's a consortium including Shell Canada Resources and Chevron Canada completed extensive seismic surveys and completed four drill tests for reservoir quantities of carbon dioxide that if found could be piped to Southern Alberta for well injection purposes. This exploration, although still largely confidential, is not believed to have been immediately successful.

Coal was explored for by several groups at different times in the general area of the claims beginning in the mid 1900's and continuing to the present. First approximately twelve kilometers northeast of the northeast claim boundary near the now abandoned village of Flathead and later eight kilometers south of the claims in the valley of Cabin Creek at its confluence with the Flathead River (Sage Creek Coal Consortium). In 1997 Fording Coal Limited drilled nine exploration holes in the upper Flathead Valley (the Lodgepole Leases located approximately 15 kilometres to the north).

Dome Exploration (Canada) Limited (later Placer Dome Inc.) staked the first mineral claims on the Crowsnest Property in 1984 following the discovery of several gold anomalies during a silt sampling program conducted that year in the vicinity of Trachyte Ridge. The Dome Mine's program was managed by Dr. Peter Fox PhD and was initially called the Flathead Project. Fox was at this time conducting a BC wide reconnaissance gold and copper program which had started in 1972 for Dome Exploration (Canada) Limited focusing on alkalic intrusive complexes. Doctor Fox had keyed this area as a result of the recent documentation of alkalic intrusives in the area in the 1965 Geological of Canada memoir for the area (Price et al 1965) and anecdotally because of reference to gold having been panned from a stream near the 71-kilometre road marker in the 1960's.

Further work completed in 1985 and 1986, focusing on the "A Grid" area of the property, outlined encouraging rock, float and soil results and discovered a small calc-silicate vein (<0.5 m) which returned an analysis of 1.5 g/t gold and 2.3% zinc. A soil gold anomaly measuring 1000 metres by 300 metres with peak soil values to 5,590 ppb was outlined and a raft of limestone cut by red and white chalcedonic veins within the syenite was noted. Additional minor grids were located at several other locations on the then claim block including the "E" grid where a greater than 200 ppm soil copper anomaly was located but never evaluated. Success on the "A grid", which included grab samples up to 36.80 grams per ton gold was sufficiently successful to justify a diamond drill program the following season.

The 1987 field program at Flathead (now Crowsnest) was initiated in mid May and completed in late August in the "A Grid" area of the property which is located in the extreme western side. The drill program totalled 1262 metres in ten holes and was completed using a helicopter. An unexpected collapse of the core rack occurred during the program with eight holes being spilled and 25% of the core lost. Several holes intersected syenite intrusive through their full lengths while one encountered only marble and the others intersected a mixture of marble, limestone and syenite. Gold mineralization was noted to be correlative with increased limonite. Despite the small scale of the program five holes obtained encouraging intercepts as follows:

Hole	From-To (m)	Intercept (m)	Gold (g/t)
FA-1	32-33	1.0	1.39
FA-2	80-81 and	1.0	5.49
	99-100	1.0	3.54
FA-4	76.8-78.3	1.5	1.16
FA-6	44.2-45.7 and	1.5	1.71
	48.6-50.1	1.5	7.58
FA-9	50.3-51.7	1.4	1.13

TABLE II: Significant Au g/t intervals drilled in the A grid

Also in 1987 exploration was initiated on the "B grid", located seven kilometres to the east, and resulted in the discovery of a "sulphide rich gossanous boulder" that returned an analysis of 122,000 g/t gold (3.56 ounces per ton) and can be considered the initial discovery of significant mineralization on the "B grid". This sample consisted of limonite, pyrite, chalcopyrite with minor quartz and altered rock fragments.

In 1988 Placer Dome Inc. (formerly Dome Exploration (Canada), Limited) continued to work on the "B" grid and extended the grid coverage to the north, completed induced polarization surveying and began road construction up the "B Grid" valley.

In 1989 Placer Dome Inc. continued to expand the grid in a northerly direction, completed ground based geophysics (VLF and magnetometer) and completed six short diamond drill holes totaling 886 metres. Four of the holes were designed to follow up VLF geophysical anomalies while one hole was designed to test a coincident induced polarization soil gold response and one was designed to test a magnetic lineament. The 1989 drill holes, which did not return significant results, predominantly intersected limestone with lesser shale and syenite. Prospecting completed while the program was being conducted located several pieces of impressively mineralized float including a sample of pyritic intrusive breccia that returned an analysis of 521,101 ppb gold (15.20 ounces per ton).

In 1991 Placer Dome Inc. conducted 215 metres of excavator trenching (three trenches) on the slope above the 1989 drill sites. The results were unremarkable excepting the most easterly sample in trench 91-2 which returned an analysis o 542 ppb gold in the last sample. Further pieces of mineralized float were found with values to 66,211 ppb gold (1.93 oz/ton).

In 1993 Phelps Dodge Corporation of Canada (Optionee from Placer Dome Inc.) discovered a limonitic quartz vein outcropping higher in the drainage of the "B Grid". A new grid "K grid" was established in this area and the exposure sampled returning analysis to 4.6 g/t gold. The existing road was then continued to this area and mechanical trenching initiated resulting in a number of high grade samples including two which exceeded 99,999 ppb gold which upon full assay returned values to 350.70 g/t gold.

In 1994 Phelps Dodge Corporation of Canada drilled four diamond drill holes totaling 364 metres without encountering any significant intersections (all holes were

angled southwesterly. If a vein structure was also dipping southwesterly it would be missed by all of these holes).

In 1998 Eastfield Resources Ltd. purchased the Crowsnest project claims and in 1999 optioned a 75% interest to International Curator Resources Ltd. The 1999 program which started the last week of May included 2.8 kilometres of road construction, 20 kilometres of induced polarization survey, 19 kilometres of magnetometer survey, 341 soil samples, 30 till bank samples, nine stream sediment samples, 101 rock and trench samples, six trenches totaling 106 metres and ten diamond drill holes totaling 1056 metres. Of the rock samples collected 15 were boulders or cobbles in till with seven samples exceeding 1 gram per tonne gold with the average value being 19.27 g/t. Trench TK-99-1(a) yielded a 16.5 metre channel sample grading 8.338 g/t gold including 3 metres grading 19.063 g/t. Other trenches were far less successful and a complex system of faults was interpreted to explain the apparent lack of continuity. Drilling did not encounter significant gold intercepts.

In 2002 Goldrea Resources Corp. optioned a 60% interest in the Crowsnest claims from Eastfield and subsequently completed a program of mechanical trenching, road construction and diamond drilling. A new spur road, 175 metres in length, was constructed from the Spur "2" road to the southwest of the trench area and minor trenching was competed to the northwest of this area. A total of 11 drill holes were completed with and aggregate meterage of 641 metres (8 holes were drilled of the new road and three were drilled in the vicinity of the discovery trench). Most holes were terminated short of their target depths due to drilling problems. One of the holes, 02-03, intersected 12 separate syenite dykes or sills over an interval of 91 metres and returned an intercept of 1.05 g/t gold over 12 metres (approximately 150 metres south of the discovery trench area).

In 2004 Goldrea Resources Corp. completed 4 diamond drill holes totaling 476 metres. Results included hole 03-03 with 3.1 metres grading 248-g/t silver and hole 03-04 which ended with 3.4 metres grading 240 g/t silver (7.0 oz/t). Hole 03-04 was drilled southwesterly into the hill above spur road 3 (constructed in 1999) and may have intersected an important structure integral to the new exploration model.

In 2005 La Quinta Resources Corp. completed minor sampling and mapping in the vicinity of the discovery trench area, which is described in more detail in further sections of this report.

### 6.0 GEOLOGICAL SETTING

The Crowsnest property is located within the Eastern Ranges of the Canadian Rocky Mountains on the ancestral North American Craton. Here the stratigraphic column is dominated with marine sediments that vary in age from the Pre-Cambrian Purcell (Belt Group) to younger Paleozoic carbonate and clastic sediments.

Major structural complexities developed during the Laramide Orogeny when thrusting juxtapositioned older Purcell (Belt Series) rocks over Paleozoic carbonate and clastic sequences. A 10,500 foot (2700 metre) oil exploration well drilled by Pacific Atlantic Oil in the 1950's, nine kilometres to the east of the Flathead River encountered 1200 metres of Purcell rocks before encountering younger Mesozoic carbonates for the

remainder of the hole. The Lewis Overthrust, intersected by this hole, is one of the more significant faults in this region of the Canadian Rocky Mountains and is exposed in several locations on and around the Crowsnest claims.

The Crowsnest Property is predominantly underlain by a thick sequence of Pennsylvanian and Mississippian carbonate and clastic units with carbonate units of the Mississippian Rundle group predominating.

Basin and Range tectonics were operative in this area in late Cretaceous and Tertiary time and represent the northernmost extension of this structural province that is more prevalent in the western United States. The Flathead Fault, one of the younger features in the area, is interpreted to be part of this regime and forms the edge of an extensional graben that developed during this event. Paleo-reconstruction of the Flathead Valley interprets 9.6 kilometres of extension over the present surface exposure of the valley of 27.2 kilometres. Several southwesterly dipping normal faults (one being named the Flathead Fault) are interpreted. This interpretation suggests that mineralizing structures may likewise trend north-northwest and dip steeply to the southwest in multiple repetitions.

The Flathead Valley contains the only significant volumes of intrusive rocks known in the Eastern Ranges of the Canadian Rockies. These intrusive rocks are dominantly alkalic in composition and occur as dykes, sills and stocks and possibly diatremes that include monzonite, syenite and trachyte varieties. Some appear to have been emplaced along faults and these can consequently be fractured and sheared. Many of the fault controlled syenites are extensively clay altered and are manifested as prominent surface lineations. Larger intrusives, interpreted to occur as stocks and dykes, are often fresh or propylitically altered in outcrop. Altered syenites exposed in trenches and encountered in drill core can be variably clay and sericite altered and sometimes silicified. Occasional areas of skarning in the hosting carbonates have been noted (particularly on the "A grid") and contact areas in the carbonates are often brecciated and silicified. Flathead intrusions are generally propylitically altered in surface exposure and drill core exhibiting silicification, sericitization, pyritization and clay alteration. At surface, alteration is generally limited to marbleization, re-crystallization, and bleaching, while in drill holes skarn and hornfels alteration has been noted.

It has been speculated that trachytic volcanics outcropping in the nearby Crowsnest Pass area of Alberta are the volcanic equivalents of these rocks.

Faulting in the predominantly carbonate stratigraphy can be divided into low angle types which are often associated with some brecciation and are quite possibly thrusts (part of the Lewis Thrusting event) and high angle normal faults related to graben development during extension. The later types predominantly strike north-south (or north northwest) often dipping to the west with the west (or west south-west) side down dropped. Dykes, and stocks have intruded the sedimentary sequence.

### 6.1 PROPERTY GEOLOGY

The Crowsnest property is underlain by a thick sequence of Pennsylvanian and Mississippian carbonate and clastic rocks, dominated by the Mississippian Rundle Group. Mid-Cretaceous syenite and trachyte intrusions as sills, dykes, and stocks have intruded the sedimentary sequence. Flathead intrusions are generally propylitically altered in

surface exposure. Drill core exhibit silicification, limited to marbleization, rerystallization, and bleaching, and to a lesser extent skarn and hornfels alteration. The Crowsnest property is within a basin and range structural domain, dominated by an abundance of listric faults. These structures have been displaced by high angle easterly, northwesterly and northeasterly trending normal faults associated with regional Tertiary extension. The low to moderate angle structures are mainly hosted in shaly parts of the carbonate and clastic section.

Both intrusive and carbonate hosted gold mineralization is present on the Crowsnest and nearby Howell properties. Data from several drill campaigns suggests that the Crowsnest has mostly intrusive hosted gold mineralization while the nearby Howell features dominantly carbonate hosted gold mineralization. The Crowsnest property also contains elevated gold values hosted in sediments, but a drill program completed in 2002 suggests that elevated gold values are closely associated with the margin phases of the Flathead Intrusive Complex, and to a large extent intrusive hosted or in close proximity to intrusive rock. Thus the deposit type for the Crowsnest property is best described as alkalic intrusion-associated Au, a sub-type of low-sulphidation epithermal Au deposits.

### 7.0 DEPOSIT TYPES

The integral component of the deposit model for the Crowsnest project is the association between gold and alkalic intrusive rocks-particularly in a setting where the intrusives in question have been emplaced in a regime of extensional tectonics. Many of the analogues that can be cited are "world class gold deposits" and include Lanolam (Lahir Island) with resources of 422 million tonnes grading 2.95 g/t gold (40 million ounces gold), Porgera (PNG) with current and previous production resources of 23 million ounces gold and Cripple Creek (Colorado) also with current and previous production resources of 23 million ounces gold. Cripple Creek, the closest analogue, is still in production with lowgrade resources currently being mined by AngloGold Ashanti. Located about 1500 kilometres to the south-south-east of Crowsnest, Cripple Creek shares many similarities with Crowsnest including a comparable setting on the ancestral North American craton and gold mineralization associated with a Tertiary age alkaline complex occurring in a horst and grabon structural setting. The bulk of the mineralization at Cripple Creek is within or spatially associated with heterolithic breccias interpreted to be diatremes. Lowgrade gold mineralization occurs with pyrite in micro-fractures and as disseminations while high-grade mineralization is fracture controlled and occurs with gold-silver tellurides. High-grade minerlization is often associated with larger areas of low-grade mineralization commonly in the contact areas of the Cripple Creek Breccia. Historically the greatest amount of gold produced at Cripple Creek has been the high-grade variety.

### 8 MINERALIZATION

The drusy, probably late stage, quartz veining and silicification that has been observed at Crowsnest may be the controlling feature for gold mineralization. Cu and Bi tend to be elevated in strong gold zones. Silver values generally increase with increasing gold and copper. Earlier hydrothermal events may be responsible for the various

alteration phases that have been noted, including pervasive silicification, sericitization and skarning. It may suggest that the gold enriched fluids were gold-silver rich and base metal deficient. The trace elements match the alkalic intrusive hosted model by including molybdenum, bismuth, by the low but anomalous levels of copper, zinc, lead, and elevated levels of barium. Elevated tellurium was reported by earlier workers. Fluorite has been noted as a common, but not prolific, gangue mineral.

### STRATIGRAPHIC AND GEOLOGICAL MODEL

(MODIFIED FROM L.M CLARK 1964)

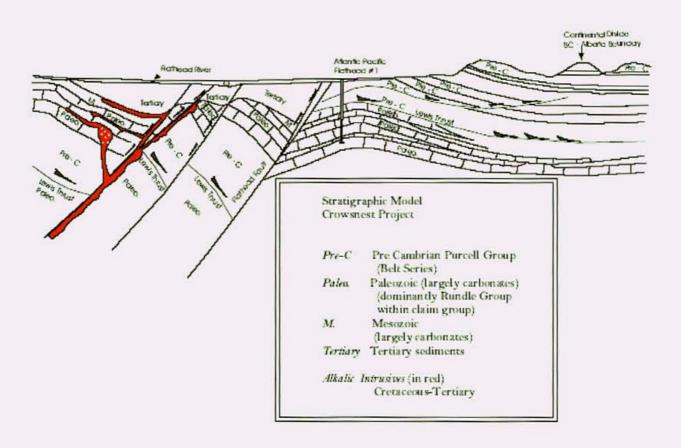


FIG. 3

Figure 3: Stratigraphy and Geology Model

### 9 EXPLORATION

The 2006 exploration program consisted of 10 trenches totaling 718meters and 332 samples over two areas, across the K grid (Discovery Grid) and on the B grid near the second switch back driving northerly on the access road.

Trenching results are described in section 10.2. In addition to trenching nine grab samples were collected during the field season with sample 29-08-R1 consisting of limonitic syenite occurring as float from the hairpin on the access road north of DDH FB-4 (Fig. 6) returning 3.49g/t gold.

SAMPLE_ID	Easting83Z11	Northings83Z Mo	,	Cu	Ag	Fe_perc	As	Au_ppbFA	Ca_perc	Labfile
29-08-R1	680222	5447027	11.21	827.13	325	4 14.51	182.9	3489.2	0.16	A605724
29-08-R2	679413	5447924	13.02	25.12	11	5 30.44	2.7	26.7	0.06	A605724
29-08-R3	679420	5447917	22.57	46.09	47	5 -40	) 12.3	140.3	0.16	A605724
29-08-R4	679420	5447928	2.64	2.84	11	7 1.59	19.5	50	25.25	A605724
29-08-R5	679315	5447886	0.86	4.27	2	9 3.09	4.6	2	2.28	A605724
29-08-R6	679364	5447854	6.29	53.64	10	4 3.03	7.2	14.1	0.5	A605724
29-08-R8	679413	5447838	43.55	81.49	62	9 -40	56.8	333.1	0.17	A605724
29-08-R9	679376	5447795	0.45	7.45	1	6 0.13	8 7.1	2.8	24.79	A605724
29-08-R10	679926	5447373	1.35	11.63	10	1 1.07	/ 11.5	9.8	33.35	A605724

TABLE III: Grab Samples collected on the Crowsnest property in 2006

### **10.1 DRILLING**

No drilling was undertaken at the Crowsnest Property during the 2006 program. Between 1987 and 2003 4,553 metres of drilling has been completed.

In 1987 Placer Dome Inc completed a drill program in the "A Grid" area with ten hols drilled totaling 1262 metres. Several holes intersected syenite intrusive through their full lengths while one encountered only marble and the others intersected a mixture of marble, limestone and syenite. Gold mineralization was noted to be correlative with increased limonite. Despite the small scale of the program five holes obtained encouraging intercepts.

In 1989 Placer Dome Inc completed six short diamond drill holes totaling 886 metres in the southern area of the "B" Grid. The 1989 drill holes, which did not return significant results, predominantly intersected limestone with lesser shale and syenite.

In 1994 Phelps Dodge Corporation of Canada drilled four diamond drill holes totaling 364 metres in the vicinity of the discovery trench without encountering significant results. All holes were angled southwesterly such that if a vein structure were also dipping southwesterly it would be missed by these holes.

In 1999 International Curator Resources Ltd completed ten diamond drill holes totaling 1056 metres in various areas of the "B" grid without obtaining significant results. Thick sections of limestone and calcareous siltstones with lesser volumes of carbonaceous siltstone to carbonaceous limestone, divided by several thin (1 meter or less) to thick (up to 85 m) feldspar porphyry intrusions were encountered. Local calc-silicate (skarn) alteration was encountered including garnet-epidote-magnetite.

In 2002 Goldrea Resources Corp. completed eleven diamond drill holes totaling 641 metres (8 holes were drilled of the new road constructed up the hill to the south of the discovery trench and three were drilled in the vicinity of the discovery trench). One of the holes, 02-03 drilled 150 metres to the south, intersected 12 separate syenite dykes or sills over an interval of 91 metres and returned an intercept of 1.05 g/t gold over 12 metres. In 2003 Goldrea Resources Corp. completed four diamond drill holes totaling 476 metres. Results included hole 03-03 with 3.1 metres grading 248-g/t silver and hole 03-04 which ended with 3.4 metres grading 240 g/t silver (7.0 oz/t). Hole 03-04 was drilled southwesterly into the hill above spur road 3 (constructed in 1999) and may have intersected an important structure. A summary of significant drill results is as follows:

#### TABLE IV: Significant Au g/t drill intercepts from the Crowsnest property

Hole	From-To (m)	Intercept (m)	Gold (g/t)	Silver (g/t)	Grid
FA-1	32-33	1	1.39	not assayed	"A"
FA-2	80-81 and	1	5.49	not assayed	"A"
	99-100	1	3.54	not assayed	"A"
FA-4	76.8-78.3	1.5	1.16	not assayed	"A"
FA-6	44.2-45.7 and	1.5	1.71	not assayed	"A"
	48.6-50.1	1.5	7.58	not assayed	"A"
FA-9	50.3-51.7	1.4	1.13	not assayed	"A"
CR-02-03	66.5-78.5	12	1.05	not assayed	"K"
CR-02-04	63.0-69.0 and	6	0.52	not assayed	"K"
	87.5-90.5	3	0.92	not assayed	"K"
CR-03-03	44.8-47.9	3.1	insignificant	248.0	"K"
CR-03-04	99.4-102.7	3.3	insignificant	240.0	"B"

### **10.2 TRENCHING**

Four previous trenching programs took place at the Crowsnest property.

In 1991 Dome Exploration cut three trenches in the B Grid area with limited success for a total of 215.m.

In 1993 Phelps Dodge Corporation of Canada (Optionee from Placer Dome Inc.) discovered a limonitic quartz vein outcropping higher in the drainage of the "B Grid". A new grid "K grid" was established in this area and the exposure sampled returning analysis to 4.6 g/t gold. The existing road was then continued to this area and mechanical

trenching initiated resulting in a number of high grade samples including two which exceeded 99,999 ppb gold which upon full assay returned values to 350.70 g/t gold.

International Curator Resources Ltd. trenched the K grid area (Discovery Grid) in 1999, and the discovery trench area. Trench TK99-1 encountered 16.5 metres grading 8.338 g/t gold including 3 metres grading 19.063 g/t. Other trenches were less successful and a complex system of faults was interpreted to explain the apparent lack of continuity.

In 2002 Goldrea Resources Corp. excavated a duplicate trench "Discovery" to confirm both location and grade of the discovery trench and encountered similar grades.

The 2006 trenching component of the exploration program was designed to test mineralization extension in the K (Discovery) grid area and to test soil and float anomalies in the B grid. Ten trenches totalling 718m were excavated (Fig.4), mapped, sampled and photographed. The trenches were immediately refilled and seeded. The following table provides the NAD 83 Zone 11 UTM grid location for the start of all the 2006 trenches.

TABLE II. 2006	Trenching P	rogram – I	rench I	leaders
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\_\_\_\_

TR_ID	Easting	Northing	EL	Azimuth	Dip	Length
CTR601N	679,386	5,447,917	1716	57	-10	56
CTR601S	679,383	5,447,915	1716	255	5	38
CTR602	679,429	5,447,950	1700	164	-3	27
CTR603N	679,409	5,447910	1715	37	-7	25
CTR603S	679,381	5,447,880	1720	41	-10	43
CTR604E	679,358	5,447,889	1725	124	-3	80
CTR604W	679,259	5,447,926	1730	114	-5	105
CTR612C	680,653	5,446,662	1605	356	5	60
CTR612N	680,627	5,446,718	1612	360	11	94
CTR612S	680,653	5,446,662	1605	174	5	190

In the trench sample interval table provided in Appendix (TABLE III) the uphill side and if samples were available from the downhill side both sides of the trenches were sampled. The table includes sampled intervals, sample ID and Au ppb values. One column specifies the trench side sampled. ACME's Fire Assay certificates and the ICP certificates were formatted for page size PDF and can be found in Appendix B (2006 Assay certificates).

Of the 332 chip samples collected from either or both sides of the average 3m deep and 1.5m wide trenches, 307 samples represented unique intervals, while the balance indicated overlapping lithologies within the same intervals. Composites of the 25 overlapping intervals were weighted by their length to produce the composited Au ppb values used with the Discover program to produce the Trenching 2006 Assay plans included in Appendix. (See Table I "Crowsnest Trench FA Intervals"). Twenty-six (26) intervals from the K grid trenches CTR603N, CTR601N, CTR601S, CTR602, and an isolated sample on 603S (TableII). returned gold over 100ppb.

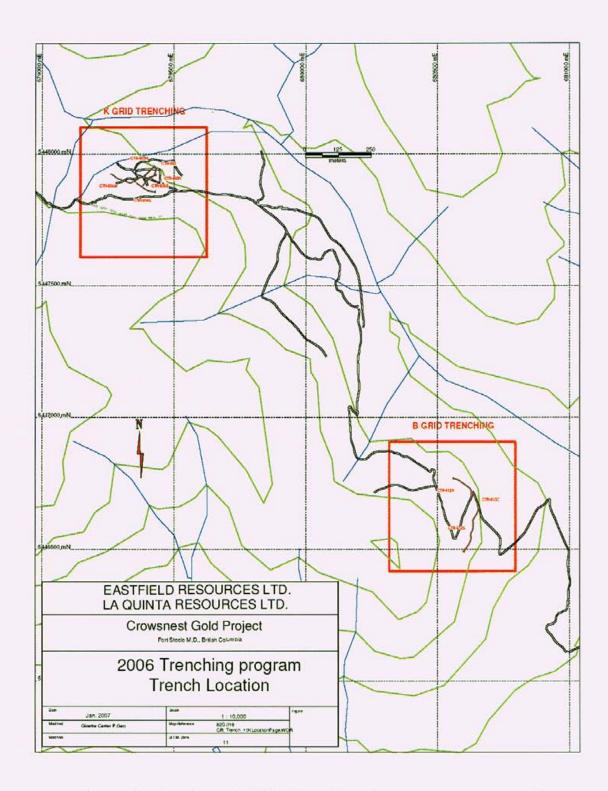


Figure 4: Location of 2006 Trenching Program - Crowsnest Property

Except for sample 173456 all came from representative chip samples. The only interval with over 500ppb Au was sample 173402 on CTR603N, near the start of the trench carrying 976ppb Au on the west side and 425 ppb Au on the East side of the trench.

Trench_No	Fromm_ Tom	_ Sa	ample_No AuPPB	Side	profile part
CTR-601NE	8	10	201371	140East	all
CTR-601NE	27	31	201379	135East	down
CTR-601NE	31	32	201380	141 East	top
CTR-601NE	37	40	201384	163East	all
CTR-601NW	17	18.55	201357	200 West	top
CTR-601NW	37	40	201366	133West	down
CTR-601SE	11	12	173129	208 East	all
CTR-601SE	12	14	173131	285 East	up
CTR-601SE	25	27	173142	176East	down
CTR-601SW	11	13	173106	102West	all
CTR-601SW	14	16	173109	349West	top
CTR-601SW	16	18	173111	155West	up
CTR-601SW	18	20	173112	140West	down
CTR-601SW	20	22	173114	154West	down
CTR-602N	9	12	173465	107 North	all
CTR-602N	12	15	173466	172North	all
CTR-602S	15	17	173475	133 South	all
CTR-603NE	5	9	173419	132East	ир
CTR-603NE	6	9	173413	425 East	all
CTR-603NE	9	10	173414	161 East	top
CTR-603NE	9	10	173415	186East	down
CTR-603NE	10	16	173416	162 East	all
CTR-603NW	2	4	173402	973West	all
CTR-603NW	4	5.5	173403	287 West	up
CTR-603NW	5.5	6.5	173404	110West	down
CTR-603S	25	30	173456	286 DF	Deep float

Significant Intersections - 2006 Trenching program

The 2006 trenching program provided us with further insights on the stratigraphic and structural setting of K and B grid area. On the K grid area, a layered undulating package of fractured and bleached limestone and oxidized syenite (partly sills?) was mapped. Within CTR603N and CTR601N and between them minor subhorizontal mesofolds were recognized as trending roughly WNW (roughly 290 degrees trend).

While intense fracturing and jointing obscured much of the bedding attitude, several greyish decalcified clayey strata remnants confirmed the attitude of the wrinkled lithological sequence as gently dipping to the North. Jointing and minor axial planes

encountered in the 2006 trenches dipped moderately to steeply (45 to 60 deg) to the North. Strong oxidation haloes were present at most contacts between fractured decalcified limestone sequences and totally oxidized clayey interlayered syenite sill or bodies. Except for trenches CTR604E, CTR604W where the sample population was derived form deep regolith, colluvium and till, most trenches provided with continuous and reliable weathered rock cuts. Although a significant section of CTR604 W did cut through a slightly pyritic and oxidized porphyritic green syenite, there were no significant results from either CTR 604E or CTR604W. A single limonitic clayey deep float accounts for the one anomalous interval found in the northern part of CTR603S.

Anomalous gold was intersected to the north in trenches CTR601N, CTR602, and CTR603N. Oxidation appeared to follow the trend of minor mesofold sets recognized between CTR601N and CTR603N. These meso hinges were slightly undulating to subhorizontal. In trench CTR603N, an oxidized syenite flattish small body within a mesofold set returned our highest gold interval (973 ppb Au -sample 173402). Sample 173413, on the opposite (East) side of the trench returned 425ppb Au, which was the second highest sample of the program. Both samples came from the same mesofold axis - ripple trend. That trend appears to aim directly at the high grade intervals that were trenched in 1999 by International Curator (TK99-1). Small structural mesofolds also coincide with an increase in alteration and oxidation. The following sketch illustrate the structural style observed in the trenches.

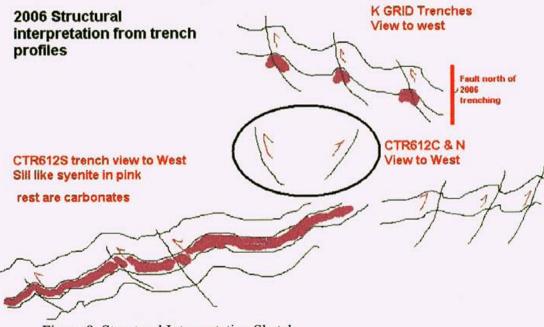


Figure 9. Structural Interpretation Sketch

Phelps Dodge's drilling of the K grid in 1994 also led them to the conclusion that strata and syenite sills generally dipped gently to the north.

The B grid 2006 trenching CTR612N, CTR612C and CTR612S outlined a generally southwesterly shallow dipping carbonate sequence intruded by a 25 meter thick

green porphyritic syenite in the first half of CTR612S, with a few very thin sills further south in in CTR612S. These minor sills are highly argillized, usually very thin and often associated with minor thrust faulting and minor mesofolding. There was no significant new mineralization intersected in the CTR 612 trenches.

### 11 SAMPLING METHOD AND APPROACH

Trenches were surveyed and mapped by the project geologist who defined and spray painted each interval to be sampled. Each meter was marked at the top of the trench. At 5m intervals, red sprayed pickets were marked with the meterage and were placed along the upper part of the trenches. Both trench sides were photographed with continuous photo coverage, with pictures covering every 3-5m intervals or so. Height and width of the trenches were measured and recorded over the length of the trenches. The project geologist used the survey data to construct several sets of geological trench profiles at a scale of 1:50. These field profiles were later scanned and pasted together and can be used to assist structural and lithological interpretation in the future. All intervals were sampled, usually as representative chip samples across distinct lithologies, or panel sampled within uniform lithologies. One tag from a dual tag sample book was inserted into each polypropylene plastic sample bag. The second tag stayed in the sample book with the recorded trench name, and sampled interval, notes and date. Sample location was marked by a metallic tag nailed by a green pin galvanized nail placed at the top of the trench or attached to adjacent branches. Representative samples from each trench were also collected by the geologist. These were taken to the camp and briefly described for future reference. Several grab samples were collected and the results are described below in this report.

### 12 SAMPLE PREPARATION, ANALYSIS AND SECURITY

After collection all samples were locked with a sample tag in 6 millimetre polypropylene plastic bags with a zip tie. The bags were registered in a ledger and placed 4-5 at a time in a numbered rice bag for a total weight of roughly 40-60lbs. The rice bags were in turn zip tied and recorded, the last rice bag holding the sample list and analytical instructions for the laboratory. The shipment of rice bags was brought directly to Fernie under the supervision of the project geologist. A total of four shipments were delivered to Greyhound in Fernie. Each shipment left the same day with the bus to Acme Analytical Laboratories in Vancouver (ACME). At ACME, the 4-6kg samples were crushed to 10 mesh then pulverized to 150 mesh. For the ICP-ES (Inductively Coupled Plasma – Atomic Emission Spectrometer –Acme Group 1D) analysis, samples were reduced to 0.5gm then dissolved by Aqua Regia (leached with 3ml 2-2-2 HCL-HNO3-H2O at 95 deg C for one hour, diluted to 10ml) and analyzed by ICP-ES for 30 elements. All samples were analyzed for gold by fire assay (FA - ACME's group 3B). ACME's Fire geochemistry Au analysis uses 30gm sample fusion and the doré is dissolved in Aqua

Regia. In general, Fire Assay is recommended to detect with precision Au content of less than 10ppm.

To provide control on the assaying quality and accuracy, ACME inserted 11 DS7 standards for the ICP analysis, and repeated 11 ICP analysis. ACME inserted 11 OxF41 standard, and repeated twice 11 Fire Assays. All Fire Assay certificates and ICP certificates are included in APPENDIX DATA. Both ICP and FA results were sent to us within 3 to 5 weeks of shipping. Acme Analytical Laboratories Ltd. is an accredited (ISO 9001:2000) laboratory.

### **13 ADJACENT PROPERTIES**

As quoted from Andris Kikauka's (2003) Report on the Flat 1-7, Crow1-9 Claims: "The Elk River valley and the Flathead River valley are the sight of several coal mines (Eagle Mountain, Line Creek, Fording Bridge, Green Hills, Edwin Creek, Bingay Creek, and others) which have generated high quality, high-volatile bituminous coal. These two river valleys have also been explored for oil and gas by Shell and Chevron. The prospective reservoirs include the Flathead Gas Field (estimated resource of 600 bcf).

There are numerous lead-zinc-silver bearing sulphide mineral zones in the area east of the Crowsnest property. Most of these occurrences consist of carbonate-hosted galena and sphalerite mineralization with variable silver and gold values. The Howell claim group is located northwest of the Crowsnest property. La Quinta Resources Corp. has entered into an agreement with Eastfield whereby La Quinta can earn 60% of the Howell Property claims by completing a schedule of fieldwork on the property and by completing certain cash and stock payments to Eastfield. The Howell property has a history of gold exploration by numerous mining companies."

## **14 MINERAL PROCESSING AND METALLURGICAL TESTING**

The Crowsnest property has no reported metallurgical testwork that would define gold size and distribution, amenability to gravity concentration and cyanide leach tests, and grindability.

### 15 MINERAL RESOURCE AND MINERAL RESERVE ESTIMATES

The Crowsnest property has no measured, indicated, or probable mineral resource. The Crowsnest property has not been evaluated for mineral reserve estimates.

## **16 OTHER RELEVANT DATA AND INFORMATION**

All assay certificates are included in Appendix Data. Compiled 2006 Trench interval data with brief field notes are provided in Appendix (Data) "Crowsnest06TrenchAu\_AgIntervals"). A complete set of scanned field trench profiles now merged and set up to be printed at 1:100 scale is readily available on request.

### **17 INTERPRETATIONS AND CONCLUSIONS**

The 2006 trenching work outlined WNW trending mesofolds with moderately NNE dipping axial planes in the K Grid area, suggesting a NE to SW structural compression of a northwest trending moderately NE dipping sequence of Mississippian carbonate and Flathead syenite sills. Exposures of the lower trenches (CTR612) outlined a generally SW gently dipping sequence of carbonates and with a few thin Flathead syenite sills. Trench profile mapping outlined enough mesostructures to document two opposite stress directions, with moderately SW dipping minor axial planes and thrust planes in the northern part (CTR612N) and moderately NE dipping minor axial planes and fault planes in the southern part. This combination suggests the structural bloc slightly lifted by compression from both the NE and the SW.

While CTR612 trenching did not return any significant samples, high grade floats and anomalous soils in the area still need to be followed to their source. While the 2006 K Grid trenches demonstrated that alteration and anomalous gold values increase near the WNW trending mesofolds hosting clay altered porphyritic syenite, the 2006 trenching program failed to return any samples over 1g/t Au. These results essentially closed the eastern potential extension of the mineralization intersected by the TK99-1 trench. It is currently postulated that the mineralization intersected in TK99-1, TGR93-1, TK93-2, and TK99-2 is the surface expression of the same WNW mineralized trend. However, we now feel that the conjunction of cross cutting structures might be the key to higher grade and thicker mineralization associated with Flathead intrusions. Such structures need to be defined and sampled throughout the property.

The source of much of the high grade float samples found on the property is still unknown. A set of parallel structures connecting the southeast to the northwest end of the property could be the source of the property wide high-grade float distribution.

Structural mapping of trenches and outcrops could help locate other mineralized intersecting structures, in particular where associated with syenite intrusive bodies.

### **18 RECOMMENDATIONS**

A detailed mapping and prospecting program combined with trenching of prospective areas up hill from mineralized floats and generally away from previous drilling and trenching, is recommended. The general area surrounding Fortress Peak (at elevations of 1,720-1,780 m) should be investigated in an effort to locate the source of high-grade gold floats found on the lower access road. Further evidence for the existence of a gold bearing structure up the hill (to the southwest) is afforded by the results of the 1999 silt sampling conducted by International Curator Resources Ltd. in which the highest silt sample (# 10917) returned 1150 ppb gold from a small eastward flowing tributary which crosses the Spur 3 road approximately 125 metres north west of drill hole CR-03-04.

A two phase program consisting of detailed geological and structural mapping, trenching and lithogeochemical sampling followed by a series of diamond drill holes is proposed to test the depth extension of any resulting new surface mineralization. Previous

geophysical surveys and available ASTER, LANDSAT images need to be investigated prior to setting up field work with the purpose of outlining significant crosscutting structures that may intersect known or expected syenite limestone contacts. Alteration haloes picked up from these images will need to be field checked to assess the reliability of the image analysis and to refine its selective criteria.

A suggested budget of this two-phase exploration program is described as follows:

#### **PHASE 1: PROPOSED BUDGET FOR TARGET DEFINITION:**

FIELD CREW- 2 Geologists, 2 Geotechnicians, 15 days	\$40,000
ANALYTICAL COSTS 400 determinations	\$9,000
PIMA or other alteration survey	\$10,000
ASTER IMAGE ANALSIS to flush out structures	\$10,000
EXCAVATOR	\$25,000
EQIPMENT AND SUPPLIES	\$5,000
COMUNICATIONS	\$1,000
FOOD and CONSUMABLES	\$5,000
CAMP RENTAL	\$5,000
TRUCKS AND TRANSPORTATION	\$4,500
REPORTING	\$3,500
TOTAL PHASE 1	\$118,000

### PHASE 2: PROPOSED BUDGET FOR TARGET EVALUATION:

FIELD CREW- Geologist, 3 geotechnicians, 1 cook 60 days	\$120,000
DRILLING COSTS- diamond 2000 metres (all in at \$120 metre)	\$240,000
ANALYTICAL COSTS 1500 assays	\$37,500
EQUIPMENT AND SUPPLIES	\$9,000
EXCAVATOR AND CRAWLER	\$35,000
COMUNICATION	\$2,000
FOOD and CONSUMABLES	\$10,000
CAMP RENTAL	\$10,000
TRUCKS AND TRANSPORTATION	\$8,000
REPORTING	\$3,500
TOTAL PHASE 2	\$475,000

# **19 2006 FIELDWORK COST STATEMENT**

A new four men camp was built on the old base camp location, off the seismic line at elevation 1340m. It consisted of two sleeping platform tents, a platform kitchen tent and a shower hut. Astaraf Contracting of Jaffray was retained for the road building, trench digging and part of the reclamation work.

Date	Item	Details	Cost
June 14-22/06	Professional Fees	Ginette Carter P.Geo, 2 days @ \$550	\$3,575.00
July 2,3/06	Professional Fees	Ginette Carter P.Geo, 6.5 days @ \$550	\$825.00
July 4-25/06	Professional Fees	Ginette Carter P.Geo, 22 days @ \$600	\$13,200.00
Aug 7-9/06	Professional Fees	Ginette Carter P.Geo, 3 days @ \$550	\$1,650.00
Aug 26/06	Professional Fees	Ginette Carter P.Geo, 1 days @ \$600	\$600.00
Nov 28-30/06	Professional Fees	Ginette Carter P.Geo, 3 days @ \$550	\$1,650.00
June 22/06	Professional Fees	J.W. Morton P.Geo, 1 day @ \$600	\$600.00
July 13, 14/06	Professional Fees	J.W. Morton P.Geo, 2 day @ \$600	\$1,200.00
Sept 6/06	Professional Fees	J.W. Morton P.Geo, 0.5 day @ \$600	\$300.00
June 29, 30/06	Professional Fees	J.P. Charbonneau, 2 days @ \$320	\$640.00
July 1-27/06	Professional Fees	J.P. Charbonneau, 26.5 days @ \$320	\$8,480.00
June 28-July 15	Professional Fees	Eric Mackenzie, 18 days @ \$340	\$6,120.00
July 12-19/06	Professional Fees	B Patterson, 8 days @ \$300	\$2,400.00
July 21-27/0	Professional Fees	M Berkvens, 7.5 days @ \$300	\$2,250.00
June 28-30/06	Camp & Generator Rental	3 days @ \$325	\$975.00
July 1-28/06	Camp & Generator Rental	28 days @ \$325	\$9,100.00
	Analytical costs	332 samples @ \$27.90	\$9,508.21
	Filed Equipment Purchased		\$4,126.98
	Truck Rental (2 units)		\$5,012.88
	Vehicle repairs		\$1,108.52
	ATV rental	2 units at \$70 +PST for 26.5 days	\$3,969.70
	Travel Expenses		\$2,478.82
	Freight		\$3,507.37
	Camp Lumber and materials		\$13,264.91
	Communications		\$1,786.82
	Food and Groceries		\$3,380.49
	Transportation (scheduled)		\$178.68
	Accommodation		\$2,217.19
	Fuel		\$264.19
	Expeditor charges		\$1,058.75
	Excavator charges	215 hours @ approximately \$90 hr	\$19,355.00
	Sat phone rental	1 @ \$5 day for 33 days	\$165.00
	4 radios rental	4 at \$5 day for 33 days	\$660.00
	GPS rental	1 At \$15 day for 33 days	\$495.00
	Lap top computer rental	1 at 15 days for 31 days	\$465.00
	GST Charged		<u>\$3,275.50</u>
	Total		\$129,844.01

## **20 AUTHOR QUALIFICATIONS**

#### Author Qualifications JW. (Bill) Morton P.Geo

I, J.W. Morton am a graduate of Carleton University Ottawa with a B.Sc. (1972) in Geology and a graduate of the University of British Columbia with a M. Sc. (1976) in Graduate Studies.

I, J.W Morton have been a member of the Association of Professional Engineers and Geoscientists of the Province of BC (P.Geo.) since 1991.

I, J.W. Morton have practiced my profession since graduation throughout Western Canada, the Western USA and Mexico.

I, J.W Morton supervised the work outlined in this report.

Signed this 22 day of January, 2007

#### Author Qualifications Ginette Carter P.Geo

I, G. (Ginette) Carter, P.Geo. do hereby certify that: 1. I am currently employed as a Consulting Geologist by: Mincord Exploration Consultants Ltd. 110-325 Howe Street Vancouver, BC, V6C 1Z7

2. I graduated with a B.Sc. in Geology from the University of Quebec at Montreal in 1981 and a M.Sc. from the University of Calgary, in 1984.

3. I am a member of the Association of Professional Engineers and Geoscientists of British Columbia since 1991, and a Member of the Northwest Territories Association of Professional Geologists since 1985.

4. I have worked as a geologist for at least 20 years since graduation from university.

5. I am a co-author of the technical report titled Summary Report on the 2006 Field Program Filed for Assessment Work on the Crowsnest Property, dated January 22, 2007.

6. I have spend 25 days during July 2006 on the Crowsnest property as the project geologist and supervised the work from the laying out of the trenches, the mapping, sampling of the trenches and shipping of the samples.

Appendix Table of H	igh-Grad	e Float			
Sample	Grid	gold	Copper	Sample	Year
Number	Ullu	ppb	ррт	Туре	Sampled
TAURDEL		hhn	hhm	турс	Sampicu
13585	В	122000	9404	Float	1988
21714	В	524410	5989	Float	1990
21715	В	1743	1605	Float	1990
21716	В	101705	6727	Float	1990
24464	В	45675	4565	Float	1992
24466	В	4505	533	Float	1992
24467	В	1449	168	Float	1992
24472	B	11760	702	Float	1992
24473	В	32025	1470	Float	1992
34025	В	3003	848	Float	1992
34362	В	3190	3396	Float	1992
34366	В	2740	1893	Float	1992
34367	В	6500	1644	Float	1992
34368	В	1462	201	Float	1992
34378	В	1309	83	Float	1992
34383	В	5207	1145	Float	1992
34384	В	66211	205	Float	1992
34385	В	1210	56	Float	1992
34387	В	6591	73	Float	1992
34462	В	1490	102	Float	1992
34463	В	2630	657	Float	1992
34575	B	17380	2274	Float	1992
34576	В	48500	2293	Float	1992
34577	В	17800	11556	Float	1992
33688	В	1160	104	Float	1992
121683	K	6580	4748	Float	1999
121684	Κ	4830	6515	Float	1999
121685	Κ	60750	2890	Float	1999
121686	Κ	5680	206	Float	1999
121693	Κ	46000	2810	Float	1999
10876	K	1700	353	Float	1999
10899	K	9360	803	Float	1999
104407	Κ	1280	22	Float	1999
CR03AR3	Κ	1700		Float	2003
CR03AR4	K	2580		Float	2003
29-08-R1	K	3489	827	Float	2006
Average go	ld value 3	2.655 g/t (	from a po	pulation of	f 36)

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Average gold value 32.655 g/t (from a population of 36) Average copper value 2,261 ppm (from a population of 34)

Trench_No	Fromm_ To	_m_	interval_n A	uPP8_F/ Ag_PPN	Sample_N	o LabFile	Side	Part	Notes	LabDate
CTR-601NE	5.00	7.00	2.00	27 -	.3 2013	69 A603953	East	ali	beneath dirt line only	16-Jul-06
CTR-601NE	7.00	8.00	1.00	61 -	.3 2013	70 A603953	East	top	lower contact within syenite I yellow brownish sand/clay	16-Jul-06
CTR-601NE	8.00	10.00	2.00	140 -	.3 2013	71 A603953	East	all	(7-10m) all I grey dshattered hrnf Ist +/- sil - all beneath soil	16-Jul-06
CTR-601NE	10.00	12.00	2.00	52 -	.3 2013	72 A603953	East	all	Brown sand regolith - follow band - transition to syenite from decalc I grey lst?	16-Jul-06
CTR-601NE	12.00	16.00	4.00	60 -1	.3 2013	73 A603953	East	down?	Blocky syn gossan v limonitic shattered - between lines drawn in trench	16-Jul-06
CTR-601NE	14.00	16.00	2.00	94 -	.3 2013	74 A603953	East	top	Transition - less altered more brownish still shattered	16-Jul-06
CTR-601NE	16.00	19.00	3.00	34 -4	.3 2013	75 A603953	East	all	Massive jointed I grey decalc/hnfl Ist - hump area on trench floor - sample 1/2 each side	16-Jul-06
CTR-601NE	19.00	22.00	3.00	8 -1	.3 2013	76 A603953	East	ali	dolomitic fract hnflds & E 1/2 floor	16-Jul-06
CTR-601NE	22.00	25.00	3.00	13 -	.3 2013	77 A603953	East	all	Hump - +/- fractured shattered rel massive I grey decal/hrnfil ist	16-Jul-06
CTR-601NE	25.00	27.00	2.00			78 A603953	East	all	hmfl to contact with more transitional (grey brown dirt)	16-Jul-06
CTR-601NE	27.00	31.00	4.00	135 -	.3 2013	79 A603953	East	down	limonitic rusty - syenite remnant?	16-Jul-06
CTR-601NE	31.00	32.00	1.00	141 (	.3 2013	80 A603953	East	top	(29-32 m up). Only I grey jointed hnfi Ist	· 16-Jul-06
CTR-601NE	32.00	35.00	3.00	62 -	.3 2013	81 A603953	East	all	I grey shattered rubbly decaic hrnf ist	16-Jul-06
CTR-601NE	35.00	37.00	2.00	45 (	.3 2013	83 A603953	East	ałi	I grey shattered rubbly decalc hrnf ist	16-Jul-06
CTR-601NE	37.00	40.00	3.00	163 (	.6 2013	84 A603953	East	ali	rusty main zone - likely remnant of syenite - trench to be extended	16-Jul-06
CTR-601NE	40.00	42.00	2.00	27 -	.3 2013	91 A604109	East	ail	I grey jointed shattered hnfl Ist	16-Jul-06
CTR-601NE	42.00	44.00	2.00	14 -1	.3 2013	92 A604109	East	ali	I grey jointed shattered hnfi lst	16-Jul-06
CTR-601NE	44.00	46.00	2.00	5 -(	.3 2013	93 A604109	East	ali	I grey jointed shattered hnfi list	16-Jul-06
CTR-601NE	46.00	48.00	2.00	4 -	.3 2013	94 A604109	East	ali	I grey jointed shattered hnfi list _bleached zone as well	16-Jul-06
CTR-601NE	48.00	51.00	3.00	2 -	.3 2013	95 A604109	East	ali	I grey jointed shattered hnfl ist - intersection with 602 trench start	16-Jul-06
CTR-601NE	51.00	53.00	2.00	3-0	.3 2013	96 A604109	East	all	Also flor same unit as 94 95 sample	16-Jul-06
CTR-601NE	53.00	56.00	3.00	5 -0	.3 2013	97 A604109	East	all	Recessive +/- dol +/- coaley veneer (carbonaceous sooty wisps).	16-Jul-06
CTR-601NE	0.00	5.00	5.00	22 -0	.3 2013	68 A603953	East	all	I grey shattered rubbly decalc hrnf Ist	16-Jul-06
CTR-601NW	5.00	7.00	2.00	26 -0	.3 2013	52 A603953	West	all	not brown	16-Jul-06
CTR-601NW	7.00	10.00	3.00	35 -0	.3 2013	53 A603953	West	top	Brown only	16-Jul-06
CTR-601NW	7.00	10.00	3.00	18 -0	.3 2013	54 A603953	West	down	grey Decaic (hrnfis?)	16-Jul-06
CTR-601NW	10.00	13.00	3.00	40 -	.3 2013	55 A603953	West	top	lim dirt - likely syenite remains, its very base has grey shattered decalc (hrnfis?)	16-Jul-06
CTR-601NW	13.00	17.00	4.00	83 -	.3 2013	56 A603953	West	ail	Buff alt lim dirt syenite +/- gossan	16-Ju <del>l</del> -06
CTR-601NW	17.00	18.55	1.55	200 -	.3 2013	57 A603953	West	top	Brown top only w shattered blocky syenite limonitic/buff alt	16-Ju <del>l</del> -06
CTR-601NW	18.55	22.00	3.45	41 -	.3 2013	58 A603953	West	ali	grey decalc (hrnfis?) ist	16-Jul-06
CTR-601NW	22.00	25.00	3.00	15 -	.3 2013	59 A603953	West	all	grey decalc +/- sil (hrnfts?) lst	16-Jul-06
CTR-601NW	25.00	27.00	2.00	26 -4	.3 2013	60 A603953	West	all	dirt buff to brown transition zone (both alt syenite and grey decalc (hrnfis?) lst)	16-Jul-06
CTR-601NW	27.00	29.00	2.00	30 -	.3 2013	61 A603953	West	all	w dol/sil grey beige decalc (hrnfis?) ist - gossan not taken in this sample	16-Jul-06
CTR-601NW	29.00	31.00	2.00	58 -	.3 2013	62 A603953	West	ctr	Irreg shaped limonitic rusty zone exclusively	16-Jul-06
CTR-601NW	31.00	32.00	1.00	19 -1	.3 2013	63 A603953	West	down	down zone mostly it grey shattered decalc hnfi list	16-Jul-06
CTR-601NW	32.00	35.00	3.00	29 -1	.3 2013	64 A603953	West	ali		16-Jul-06
CTR-601NW	35.00	37.00	2.00	94 -4	.3 2013	65 A603953	West	ചി	transition (into intense lim syenite) buff gravel	16-Jul-06
CTR-601NW	37.00	40.00	3.00	133	.6 2013	66 A603953	West	down	Intense lim syenite /up to it grey hrnfl decal contact	16-Jul-06
CTR-601NW	40.00	42.00		15 -	.3 2013	85 A604109	West	all	Jointed subvertical I grey shattered rubbly decalc hrnf Ist	16-Jul-06
CTR-601NW	42.00	44.00	2.00	9 -	.3 2013	86 A604109	West	all	L grey (+/- doi) massive ist micrite	16-Jul-06
CTR-601NW	44.00	46.00	2.00	2 -	.3 2013	87 A604109	West	all	Massive ited and shattered L grey (+/- dol) ist micrite	16-Jul-06
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CTR-601NW	46.00	48.00	2.00	5	-0.3	201388 A604109	West			16-Jul-06
CTR-601NW	46.00	48.00 51.00	2.00	5	-0.3	201388 A604109 201389 A604109	West		dull dk grey streaked L grey (+/- dol) massive ist micrite Beige shattered ist/dol + coaley veneer	16-Jul-06
CTR-601NW	40.00	56.00	5.00	29	-0.3	201389 A604109 201390 A604109	West		Coaley layer + yellow brown sand (syenite veneer?) +/- dol ist end of extension	16-Jul-06
CTR-601NW	0.00	5.00	5.00	29	-0.3	201350 A603953	West	<b>a</b> 11	Decaic (hmits?) Shattered ist - only grey	16-Jul-06
				16				all		19-Jui-06
CTR-601SE	2.00	4.00	2.00		0.3	173125 A604234	East	all	Shattered I m grey hnfl Ist/cc - same unit	
CTR-601SE	4.00	7.00	3.00	21	-0.3	173126 A604234	East	all	Massive I m grey ist motiled	19-Jul-06
CTR-601SE	7.00	9.00	2.00	42	-0.3	173127 A604234	East	all	Shattered I m grey hnfl Ist/cc - same unit - f gr micrite	19-Jul-06
CTR-601SE	9.00	11.00	2.00	28	0.3	173128 A604234	East	ali	Shattered I m grey hnfl Ist/cc - same unit - f gr micrite	19-Jui-06
CTR-601SE	11.00	12.00	1.00	208	0.5	173129 A604234	East	ail	Rusty yellow zone brief syenite sills :contact minz trend ? 176 deg az -60? Could intersect sills?	19-Jul-06
CTR-601SE	12.00	14.00	2.00	20	-0.3	173130 A604234	East	down	grey & orange shattered loose face - decal lst?	19-Jul-06
CTR-601SE	12.00	14.00	2.00	285	-0.3	173131 A604234	East	up	SC?/rusty brown likely a thin syenite sill or OB root stains - check ICP	19-Jul-06
CTR-601SE	14.00	16.00	2.00	24	0.4	173132 A604234	East	down	Massive I grey Ist +/- sooty bands at base	19-Jul-06
CTR-601SE	14.00	16.00	2.00	58	0.4	173133 A604234	East	up	Same interval as 131 - brown clay, dirt and sootey spots above - SC?	19-Jul-06
CTR-601SE	16.00	18.00	2.00	78	-0.3	173134 A604234	East	down	Dol blocky ist	19-Jul-06
CTR-601SE	16.00	18.00	2.00	30	-0.3	173135 A604234	East	up	Same interval as 134 - brown clay, mush alt -	19-Jui-06
CTR-601SE	18.00	20.00	2.00	25	-0.3	173136 A604234	East	down	Blocky massive dol ist	19-Jul-06
CTR-601SE	18.00	20.00	2.00	18	-0.3	173137 A604234	East	up	Same interval as 136 - brown clay, dirt and sootey spots above	19-Jui-06
CTR-601SE	20.00	22.00	2.00	52	-0.3	173138 A604234	East	down	orangish & grey dirt rubble	19-Jul-06
CTR-601SE	20.00	22.00	2.00	23	-0.3	173139 A604234	East	υр	Same interval as 138 - sootey brown clay, dirt	19-Jul-06
CTR-601SE	22.00	25.00	3.00	40	-0.3	173140 A604234	East	down	foliow rocks	19-Jul-06
CTR-601SE	22.00	25.00	3.00	25	0.3	173141 A604234	East	up	ali clayey mush above 140 sample - regolith or till?	19-Jul-06
CTR-601SE	25.00	27.00	2.00	176	-0.3	173142 A604234	East	down	rocky- ml grey 4 cm thick lst beds, v f grained xline ist following +/- slope	19-Jul-06
CTR-601SE	25.00	27.00	2.00	15	-0.3	173143 A604234	East	up	all clayey mush above 142 sample - regolith or till?	19-Jul-06
CTR-601SE	27.00	31.00	4.00	37	-0.3	173144 A604234	East	down	Loose rocks - regolith dk m grey lst 30-50cm thick beds	19-Jul-06
CTR-601SE	27.00	31.00	4.00	22	-0.3	173145 A604234	East	up	Brown thick clay same interval as 144	19-Jul-06
CTR-601SE	31.00	32.00	1.00	59	0.3	173146 A604234	East	ctr	Large deep float - rusty - sample it only.	19-Jul-06
CTR-601SE	0.00	2.00	2.00	9	0.3	173124 A604234	East	all	I m grey hnfl lst/cc	19-Jul-06
CTR-601SW	2.00	4.00	2.00	10	-0.3	173102 A604234	West	all	Grey/butf sl dol tract ist -	19-Jul-06
CTR-601SW	4.00	7.00	3.00	22	-0.3	173103 A604234	West	ali	Grey/buff sl dol fract lst - oranger near top roots	19-Jul-06
CTR-601SW	7.00	9.00	2.00	15	0.4	173104 A604234	West	afi	Grey/buff si dol fract ist -	19-Jul-06
CTR-601SW	9.00	11.00	2.00	7	-0.3	173105 A604234	West	ali	I grey unit only - leave rusty zone for next sample	19-Jul-06
CTR-601SW	11.00	13.00	2.00	102	-0.3	173106 A604234	West	ali	take only rusty zone - most of interval - likely alt syenite narrow sill	19-Jul-06
CTR-601SW	13.00	14.00	1.00	19	0.3	173107 A604234	West	ali	I grey shattered rubbly decalc hml ist	19-Jul-06
CTR-601SW	14.00	16.00	2.00	14	-0.3	173108 A604234	West	down	I grey hrnfl with +/- dk streaked ist	19-Jul-06
CTR-601SW	14.00	16.00	2.00	349	0.4	173109 A604234	West	top	Brown buff - same interval as 108	19-Jul-06
CTR-601SW	16.00	18.00	2.00	73	-0.3	173110 A604234	West	•	I grey unit only - leave rusty zone for next sample	19-Jul-06
CTR-601SW	16.00	18.00	2.00	155	0.4	173111 A604234	West		Brown buff dirt - same interval as 110	19-Jul-06
CTR-601SW	18.00	20.00	2.00	140	0.5	173112 A604234	West		I grey loose rock hni shattered decal ist	19-Jul-06
CTR-601SW	18.00	20.00	2.00	17	0.3	173113 A604234	West		Brown buff dirt - same interval as 112	19-Jul-06
CTR-601SW	20.00	22.00	2.00	154	0.5	173114 A604234	West	down	I prev loose rock hni shattered decal ist	19-Jul-06
CTR-601SW	20.00	22.00	2.00	14	-0.3	173115 A604234	West	up	Brown buff dirt - same interval as 114	19-Jul-06
CTR-601SW	22.00	24.00	2.00	45	0.3	173116 A604234	West	down	loose I grey rock decalc hnil ist - getting rustier - near syenite contact?	19-Jul-06
011-001014	22.00	24.00	2.00		0.0				inere states reactioner time at Some logare uner about country:	10 001-00

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CTR-601SW	22.00	24.00	2.00	85	0.4	173117 A604234	West	up	Brown buff dirt - same interval as 116	19-Jul-06
CTR-601SW	24.00	26.00	2.00	41	-0.3	173118 A604234	West	all	SI dol ist +/- rusty rock and dirt	19-Jul-06
CTR-601SW	26.00	28.00	2.00	34	-0.3	173119 A604234	West	down	grey and dk grey sooty ist	19-Jul-06
CTR-601SW	26.00	28.00	2.00	55	-0.3	173120 A604234	West	up	Brown buff dirt - same interval as 119	19-Ju <del>l</del> -06
CTR-601SW	28.00	29.00	1.00	12	-0.3	173121 A604234	West	ail	upper brownish dirt and sootey carbonaceous lst	19-Jul-06
CTR-601SW	29.00	31.00	2.00	11	-0.3	173122 A604234	West	all	Brown buff dirt	19-Jul-06
CTR-601SW	31.00	32.00	1.00	32	0.6	173123 A604234	West	all	Brown buff dirt	19-Jul-06
CTR-601SW	0.00	2.00	2.00	7	-0.3	173101 A604234	West	ali	Grey/buff st dol fract list - sample below line. Bedding 292/40; blue grey thin list	19-Jul-06
CTR-602N	4.00	6.00	2.00	18	-0.3	173463 A604109	North	all		17-Jul-06
CTR-602N	6.00	9.00	3.00	19	-0.3	173464 A604109	North	ail	Massive grey tst +/- dol jpinted	17-Jul-06
CTR-602N	9.00	12.00	3.00	107	-0.3	173465 A604109	North	ail	Recessive - transitional?- brown dirt +/- dol	17-Jul-06
CTR-602N	12.00	15.00	3.00	172	-0.3	173466 A604109	North	all	part doVist part recessive brown dirt	17-Jul-06
CTR-602N	15.00	20.00	5.00	83	-0.3	173467 A604109	North	all	ends near end of 603N	17-Jul-06
CTR-602N	2.00	4.00	2.00	22	-0.3	173462 A604109	North	all	Massive grey lst +/- dol jpinted	17-Jบ -06
CTR-602N	0.00	2.00	2.00	7	-0.3	173461 A604109	North	all	Massive +/- hornf /decal lst jointed. Cleavage 55/60. 164 deg azimuth, -3 slope to 16.5m. 679428E, 5447950N;	17-Jul-06
CTR-602S	2.00	4.00	2.00	15	-0.3	173469 A604109	South	all	Massive less ited Ist/dol	18-Jul-06
CTR-602S	4.00	6.00	2.00	12	-0.3	173470 A604109	South	all	Massive less ited lst/dol	18-Jul-06
CTR-602S	6.00	8.00	2.00	16	-0.3	173471 A604109	South	ali	More shattered Massive less ited ist/dol	18-Jul-06
CTR-602S	8.00	10.00	2.00	77	-0.3	173472 A604109	South	ali	below line	18-Jui-06
CTR-602S	10.00	12.00	2.00	47	-0.3	173473 A604109	South	all	buff dolomitic	18-Jul-06
CTR-602S	12.00	15.00	3.00	86	-0.3	173474 A604109	South	괢	Increasingly beige dol - a hake? Syenite nearby?	18-Jul-06
CTR-602S	15.00	17.00	2.00	133	-0.3	173475 A604109	South	all	buff dirty brown dol/lst shattered - thin syenite remnant within?	18-Jul-06
CTR-602S	17.00	20.00	3.00	62	-0.3	173476 A604109	South	all	includes hump floor dol lst	18-Jul-06
CTR-602S	0.00	2.00	2.00	13	-0.3	173468 A604109	South	ail	Massive multi ited Ist/dot	18-Jul-06
CTR-603NE	2.00	6.00	4.00	6	-0.3	173412 A604109A	East	all	Jts shattered white/beige carbonates +/- dol lst	17-Jul-06
CTR-603NE	6.00	9.00	3.00	425	-0.3	173413 A604109A	East	ail	rusty yellowish brown mush - likely syenite sill remnant	17-Jul-06
CTR-603NE	5.00	9.00	4.00	132	-0.3	173419 A604109A	East	up	rusty yellowish brown mush - likely syenite sill remnant	17-Jul-06
CTR-603NE	9.00	10.00	1.00	161	-0.3	173414 A604109A	East	up	rusty yellowish brown dirt - likely syenite sill remnant	17-Jul-06
CTR-603NE	9.00	10.00	1.00	186	-0.3	173415 A604109A	East	down	grey white dol/ist	17-Jul-06
CTR-603NE	10.00	16.00	6.00	162	-0.3	173416 A604109A	East	ali	poor outerop	17-Jul-06
CTR-603NE	16.00	21.00	5.00	88	-0.3	173417 A604109A	East	all	poor outcrop dol ist	17-Jul-06
CTR-603NE	21.00	25.00	4.00	46	-0.3	173418 A604109A	East	all	grey m grey micrite (+/- dol fractured)	17-Jul-06
CTR-603NE	0.00	2.00	2.00	62	-0.3	173411 A604109A	East	ali	white & dk grey lst - possibly cc massive m kine vein or hornfelsed white lst	17-Jul-06
CTR-603NW	2.00	4.00	2.00	973	-0.3	173402 A604109A	West	ał	beige to sl rusty dirt base - transitional zone to alt syenite sill?	17-Jul-06
CTR-603NW	4.00	5.50	1.50	287	-0.3	173403 A604109A	West	up	(4-6m intv) Transitional - less altered syenite - mostly dirt -	17-Jul-06
CTR-603NW	5.50	6.50	1.00	110	-0.3	173404 A604109A	West	down	(5-7m intv) rusty gossan clay alt around horst	17-Jul-06
CTR-603NW	6.50	8.00	1.50	77	-0.3	173405 A604109A	West	top	(6-8m intv) grevish dirt - trans or weathered lst	17-Jul-06
CTR-603NW	8.00	9.00	1.00	91	-0.3	173406 A604109A	West	top	rusty lim dirt alt in narrow contact zone	17-Jul-06
CTR-603NW	9.00	11.00	2.00	14	-0.3	173407 A604109A	West	all	m dik grey dol/lst - rocks only	17-Jul-06
CTR-603NW	11.00	15.00	4.00	64	-0.3	173408 A604109A	West	all	end of hump - witin bedded dol ist +/- localy rusty	17-Jul-06
CTR-603NW	15.00	20.00	5.00	98	-0.3	173409 A604109A	West		within bedded I gr m grey dol ist +/- localy rusty _ honey comb textures	17-Jul-06
CTR-603NW	20.00	25.00	5.00	48	-0.3	173410 A604109A	West	ail	v shallow trench doi fract lst and narrow beige buff doi lst	17-Jul-06
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CTR-603S     5.00     10.00     5.00     7     0.3     173454     A604169A     DF     deep float       CTR-603S     15.00     20.00     5.00     7     0.3     173454     A604169A     DF     deep float       CTR-603S     25.00     30.00     5.00     7     0.3     173454     A604169A     DF     deep float       CTR-603S     30.00     5.00     2.00     173457     A604169A     DF     deep float       CTR-603S     30.00     5.00     2.03     173457     A604169A     DF     deep float       CTR-603S     4.00     5.00     7     -0.3     17357     A604169A     DF     deep float       CTR-604S     10.00     5.00     5     -0.3     17357     A604169A     DF     deep float       CTR-604E     10.00     5.00     5     -0.3     17357     A604169A     DF       CTR-604E     2.00     5.00     4     -0.3     17357     A604169     DF <t< th=""><th>CTR-603NW</th><th>0.00</th><th>2.00</th><th>2.00</th><th>44</th><th>-0.3</th><th>173401 A604109A</th><th>West</th><th>all</th><th>white grey ist micrite - I crystalline - beneath</th></t<>	CTR-603NW	0.00	2.00	2.00	44	-0.3	173401 A604109A	West	all	white grey ist micrite - I crystalline - beneath
CTR-8035     15.00     20.00     5.00     7     4.0.3     174454 A6A1106A     DF     deep feat       CTR-8035     25.00     30.00     5.00     8.0.3     17456 A6A1106A     DF     deep feat       CTR-8035     30.00     5.00     4.0.3     17456 A6A1106A     DF     deep feat       CTR-8035     40.00     5.00     7.0.3     17456 A6A1106A     DF     deep feat       CTR-8035     40.00     5.00     7.7     -0.3     17357 A6A1109     DF     deep feat       CTR-8046     10.00     15.00     5.00     7.7     -0.3     17357 A6A1109     DF       CTR-8046     10.00     15.00     5.00     3.03     17357 A6A1109     DF       CTR-8046     25.00     5.00     3.03     17357 A6A140190     DF       CTR-8046     30.00     5.00     5.00     3.03     173578 A6A140190     DF       CTR-8046     5.00     5.00     5.00     3.03     173588 A6A1190     DF       CTR-8046     5.00 <td< td=""><td>CTR-603S</td><td>5.00</td><td>10.00</td><td>5.00</td><td>7</td><td>-0.3</td><td>173452 A604109A</td><td>DF</td><td></td><td>deep float</td></td<>	CTR-603S	5.00	10.00	5.00	7	-0.3	173452 A604109A	DF		deep float
CTR-8285     25.00     5.00     5.00     7.84     5.604/104     DF     deep feat       CTR-8285     25.00     35.00     5.00     4.4     0.3     17.4457.464/1040     DF     deep feat       CTR-8285     5.00     4.00     5.00     7.4     7.4647.464/1040     DF     deep feat       CTR-8285     4.00     4.00     5.00     7.4     7.4547.464/1040     DF     deep feat       CTR-8285     4.00     4.00     5.00     7.4     3.3     17.3457.464/1040     DF     deep feat       CTR-8246     10.00     5.00     5.0     3.3     17.357.464/109     DF       CTR-8246     10.00     5.00     5.0     3.3     17.357.464/109     DF       CTR-8246     5.00     5.00     5.0     3.3     17.357.464/109     DF       CTR-8246     5.00     5.00     5.0     3.3     17.355.464/109     DF       CTR-8246     5.00     5.00     5.0     4     -3.3     17.355.464/109     DF  <										
CTR-R005     S0.00										
CTR-9305     55.00     64.00     60.00										
CTR-R005     Sto0     40.00     50.00     -2     0.3     173458< A04100A     DF     deep float       CTR-R005     0.00     5.00     5.00     7     -0.3     173451< A041109A										
CTR-R02S     0.00     40.00     3.00     7.34     173459     ADM (100)     DF     deep float       CTR-R04E     5.00     10.00     5.00     5     -0.3     17357     ASM 109     DF       CTR-R04E     10.00     15.00     5.00     3     17357     ASM 109     DF       CTR-R04E     10.00     25.00     5.00     3     17357     ASM 109     DF       CTR-R04E     20.00     25.00     5.00     3     17357     ASM 109     DF       CTR-R04E     20.00     25.00     5.00     1     -0.3     173587     ASM 109     DF       CTR-R04E     30.00     50.00     5.0     5.03     1     -0.3     173588     ASM 109     DF       CTR-R04E     50.00     50.00     5.00     5.00     5.03     1388     ASM 109     DF       CTR-R04E     50.00     5.00     5.00     5.00     5.00     5.00     5.03     173589     ASM 109     DF       CTR-R04E<										
CTR-903     0.00     5.00     7     -0.3     172451 A604100 PF       CTR-904E     10.00     15.00     5.00     5     -0.3     17357 A604100 PF       CTR-904E     10.00     5.00     5     -0.3     17357 A604100 PF       CTR-904E     20.00     25.00     5.00     4     -0.3     17357 A604109 PF       CTR-904E     20.00     25.00     5.00     4     -0.3     17357 A604109 PF       CTR-904E     30.00     5.00     3     -0.3     17350 A604109 PF       CTR-904E     40.00     5.00     5     -0.3     17350 A604109 PF       CTR-904E     40.00     5.00     5     -0.3     17350 A604109 PF       CTR-904E     5.00     5.00     5     -0.3     17350 A604109 PF       CTR-904E     50.00     5.00     5     -0.3     17350 A604109 PF       CTR-904E     60.00     5.00     5     -0.3     17350 A604109 PF       CTR-904E     7.00     5.00     5.0     3     17350 A604109 PF										•
CTR-904E   5.00   15.00   5.00   5   -0.3   173575   A604109   DF     CTR-904E   15.00   25.00   5.00   3   -0.3   173577   A604109   DF     CTR-904E   25.00   5.00   3   -0.3   173577   A604109   DF     CTR-904E   25.00   35.00   5.00   3   -0.3   173578   A604109   DF     CTR-904E   35.00   5.00   5   -0.3   173588   A604109   DF     CTR-904E   45.00   5.00   5   -0.3   173588   A604109   DF     CTR-904E   45.00   5.00   5   -0.3   173588   A604109   DF     CTR-904E   45.00   5.00   5   -0.3   173588   A604109   DF     CTR-904E   50.00   5.00   5   -0.3   173588   A604109   DF     CTR-904E   75.00   5.00   5   -0.3   173588   A604109   DF     CTR-904W   3.00   5.00   5   -0.3   173588										
CTR-604E   10.00   5.00   5.00   5   0.30   17357 A6X01409   DF     CTR-604E   20.00   25.00   5.00   4   0.3   17357 A6X0149   DF     CTR-604E   25.00   30.00   5.00   3   0.33   17357 A6X0149   DF     CTR-604E   30.00   5.00   5.00   10   0.3   17357 A6X0149   DF     CTR-604E   30.00   5.00   5.00   10   0.3   17358 A6X0149   DF     CTR-604E   40.00   5.00   5.00   5   0.3   17358 A6X0149   DF     CTR-604E   55.00   5.00   5   0.3   17358 A6X0149   DF     CTR-604E   55.00   5.00   5   0.3   17358 A6X0149   DF     CTR-604E   70.00   5.00   4   0.3   17358 A6X0149   DF     CTR-604E   70.00   5.00   5   0.3   17358 A6X0149   DF     CTR-604E   70.00   5.00   5   0.3   17358 A6X0149   DF     CTR-604W   3.00   6.00 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>going north from 604 west intersect - deep float</td>										going north from 604 west intersect - deep float
CTR-604E     15.00     25.00     5.00     3     0.33     173577     A604109     DF       CTR-604E     25.00     35.00     5.00     3     0.3     173579     A604109     DF       CTR-604E     35.00     35.00     5.00     1     0.3     173589     A604109     DF       CTR-604E     35.00     5.00     5     0.3     173589     A604109     DF       CTR-604E     40.00     45.00     5.00     5     0.3     173589     A604109     DF       CTR-604E     50.00     5.00     5.0     3     173589     A604109     DF       CTR-604E     50.00     5.00     4     0.3     173589     A604109     DF       CTR-604E     70.00     5.00     4     0.3     173589     A604109     DF       CTR-604E     70.00     5.00     4     -0.3     173589     A604109     DF       CTR-604W     5.00     5.00     5     -0.3     173558     A60										
CTR-604E     20.00     5.00     6.00     3     0.31     173579     A604109     DF       CTR-604E     30.00     35.00     1.00     -0.3     173597     A604109     DF       CTR-604E     30.00     4.00     5.00     1.0     -0.3     173581     A604109     DF       CTR-604E     40.00     5.00     5.00     5     -0.3     173581     A604109     DF       CTR-604E     40.00     5.00     5.00     5     -0.3     173581     A604109     DF       CTR-604E     60.00     5.00     5.00     4     -0.3     173581     A604109     DF       CTR-604E     65.00     6.00     5.00     4     -0.3     173581     A604109     DF       CTR-604E     70.00     75.00     5.00     6     -0.3     173581     A604109     DF       CTR-604E     70.00     5.00     6     -0.3     173581     A604109     DF       CTR-604W     6.00     1.00										
CTR-604E     25.00     30.00     5.00     10     -0.3     17359 A604109     DF       CTR-604E     35.00     40.00     5.00     5.00     10     -0.3     173581 A604109     DF       CTR-604E     40.00     45.00     5.00     5     -0.3     173581 A604109     DF       CTR-604E     45.00     5.00     5.00     3     -0.3     173583 A604109     DF       CTR-604E     60.00     5.00     5.00     3     -0.3     173583 A604109     DF       CTR-604E     60.00     65.00     5.00     4     -0.3     173583 A604109     DF       CTR-604E     75.00     8.00     5.00     4     -0.3     173584 A604109     DF       CTR-604E     75.00     8.00     5.00     4     -0.3     173584 A604109     DF       CTR-604W     5.00     5.00     4     -0.3     173584 A604109     DF       CTR-604W     5.00     5.00     4     -0.3     173585 A604109     DF										
CTR-604E   30.00   35.00   5.00   10   -0.3   173580 A60109   DF     CTR-604E   40.00   5.00   5.00   5   -0.3   173582 A60109   DF     CTR-604E   40.00   5.00   5.00   5   -0.3   173582 A60109   DF     CTR-604E   60.00   55.00   5.00   4   -0.3   173582 A60109   DF     CTR-604E   60.00   65.00   5.00   4   -0.3   173582 A60109   DF     CTR-604E   60.00   65.00   5.00   4   -0.3   173583 A60109   DF     CTR-604E   70.00   75.00   5.00   4   -0.3   173583 A60109   DF     CTR-604E   70.00   75.00   5.00   4   -0.3   173583 A60109   DF     CTR-604W   3.00   6.00   3.00   4   -0.3   173583 A60109   DF     CTR-604W   3.00   10.00   13.00   3.00   7   -3.3   173583 A60109   DF     CTR-604W   13.00   13.00   2.00   7   -3.3<					-					
CTR-604E     55.00     40.00     500     4     -0.3     173651 A604109     DF       CTR-604E     45.00     5.00     5.0     5     -0.3     173558 A604109     DF       CTR-604E     50.00     5.00     5.0     3     -0.3     173558 A604109     DF       CTR-604E     50.00     5.00     5.00     3     -0.3     173558 A604109     DF       CTR-604E     60.00     5.00     5.0     -0.3     173558 A604109     DF       CTR-604E     60.00     5.00     5.0     4     -0.3     173558 A604109     DF       CTR-604E     75.00     75.00     5.00     4     -0.3     173558 A604109     DF       CTR-604E     75.00     5.00     5     -0.3     173558 A604109     DF       CTR-604W     3.00     6.00     3.00     7     -0.3     173558 A604109     DF       CTR-604W     13.00     15.00     2.00     3     173558 A604109     DF       CTR-604W     13.00										
CTR-BOME     40.00     46.00     5.00     5.00     5     -0.3     173582     AB01109     DF       CTR-BOME     45.00     5.00     5.00     5     -0.3     173583     AB01109     DF       CTR-BOME     50.00     5.00     5.00     4     -0.3     173584     AB01109     DF       CTR-BOME     60.00     5.00     4     -0.3     173587     AB01109     DF       CTR-BOME     65.00     70.00     5.00     4     -0.3     173587     AB01109     DF       CTR-BOME     70.00     5.00     4     -0.3     173587     AB01109     DF       CTR-BOME     70.00     5.00     6     -0.3     173587     AB01109     DF       CTR-BOMW     3.00     5.00     6     -0.3     173583     AB01109     DF       CTR-BOMW     10.00     13.00     3.00     7     -0.3     173585     AB01109     DF       CTR-BOMW     15.00     2.00     5.00		30.00			10					
CTR-604E     45.00     50.00     50.00     5     -0.3     173583 A604109     DF       CTR-604E     50.00     55.00     5.00     3     -0.3     173584 A604109     DF       CTR-604E     60.00     65.00     5.00     5     -0.3     173584 A604109     DF       CTR-604E     60.00     75.00     5.00     4     -0.3     173586 A604109     DF       CTR-604E     75.00     5.00     4     -0.3     173586 A604109     DF       CTR-604E     75.00     5.00     6     -0.3     173587 A604109     DF       CTR-604E     75.00     5.00     6     -0.3     173557 A604109     DF       CTR-604W     6.00     10.00     4.00     173557 A604109     DF     Deep angular floats - no outcrops or subcrops taken from bottom of both sides       CTR-604W     13.00     15.00     2.00     4     -0.3     173557 A604109     DF       CTR-604W     13.00     15.00     2.00     4     -0.3     173557 A604109     DF		35.00	40.00	5.00						
CTR-604E     50.00     S5.00     S0.00					-					
CTR-604E     55.00     60.00     5.00     4     -0.3     173585     A604109     DF       CTR-604E     60.00     65.00     5     -0.3     173587     A604109     DF       CTR-604E     75.00     75.00     5.00     4     -0.3     173587     A604109     DF       CTR-604E     75.00     75.00     5.00     4     -0.3     173587     A604109     DF       CTR-604E     75.00     80.00     5.00     5     -0.3     173587     A604109     DF       CTR-604W     3.00     6.00     3.00     4     -0.3     173554     A604109     DF       CTR-604W     3.00     6.00     3.00     4     -0.3     173554     A604109     DF       CTR-604W     13.00     13.00     7     -0.3     173554     A604109     DF       CTR-604W     13.00     13.00     2     -0.3     173556     A604109     DF       CTR-604W     15.00     2.00     5		45.00	50.00							
CTR-604E     60.00     65.00     5.00     5     -0.3     173586     A604109     DF       CTR-604E     65.00     70.00     5.00     4     -0.3     173586     A604109     DF       CTR-604E     70.00     75.00     60.00     5.00     4     -0.3     173586     A604109     DF       CTR-604E     70.00     5.00     5     -0.3     173576     A604109     DF       CTR-604W     3.00     6.00     3.00     4     -0.3     173553     A604109     DF       CTR-604W     10.00     13.00     3.00     7     -0.3     173553     A604109     DF       CTR-604W     15.00     2.00     4     -0.3     173554     A604109     DF       CTR-604W     13.00     3.00     7     -0.3     173554     A604109     DF       CTR-604W     25.00     5.00     2     -0.3     173555     A604109     DF       CTR-604W     25.00     5.00     0     <		50.00	55.00		3					
CTR-604E     65.00     70.00     5.00     4     -0.3     173587     A604109     DF       CTR-604E     70.00     75.00     5.00     4     -0.3     173589     A604109     DF       CTR-604E     75.00     80.00     5     6     -0.3     173589     A604109     DF       CTR-604E     0.00     5.00     5     -0.3     173574     A604109     DF     Deep angular floats - no outcrops or subcrops taken from bottom of both sides       CTR-604W     3.00     6.00     3.00     4     -0.3     173554     A604109     DF       CTR-604W     6.00     10.00     4.00     4     -0.3     173555     A604109     DF       CTR-604W     13.00     15.00     2.00     4     -0.3     173557     A604109     DF       CTR-604W     15.00     2.00     4     -0.3     173558     A604109     DF       CTR-604W     25.00     3.00     5     0.3     173558     A604109     DF <t< td=""><td>CTR-604E</td><td>55.00</td><td>60.00</td><td>5.00</td><td>4</td><td>-0.3</td><td>173585 A604109</td><td></td><td></td><td></td></t<>	CTR-604E	55.00	60.00	5.00	4	-0.3	173585 A604109			
CTR-604E     70.00     75.00     5.00     4     -0.3     173588     A604109     DF       CTR-604E     75.00     80.00     5.00     6     -0.3     173578     A604109     DF       CTR-604W     3.00     5.00     5     -0.3     173574     A604109     DF       CTR-604W     6.00     10.00     4.00     4     -0.3     173554     A604109     DF       CTR-604W     10.00     10.00     4.00     4     -0.3     173554     A604109     DF       CTR-604W     13.00     15.00     2.00     4     -0.3     173554     A604109     DF       CTR-604W     13.00     15.00     2.00     4     -0.3     173554     A604109     DF       CTR-604W     13.00     25.00     5.00     0     0     173558     A604109     DF       CTR-604W     25.00     30.00     5.00     0     0     173558     A604109     DF       CTR-604W     30.00 <t< td=""><td>CTR-604E</td><td>60.00</td><td>65.00</td><td></td><td>5</td><td></td><td></td><td></td><td></td><td></td></t<>	CTR-604E	60.00	65.00		5					
CTR-604E     75.00     80.00     5.00     6     -0.3     173589 A604109     DF       CTR-604E     0.00     5.00     5     -0.3     173574 A604109     DF       CTR-604W     3.00     6.00     3.00     4     -0.3     173552 A604109     DF       CTR-604W     6.00     13.00     3.00     7     -0.3     173553 A604109     DF       CTR-604W     10.00     13.00     3.00     7     -0.3     173555 A604109     DF       CTR-604W     15.00     20.00     4     -0.3     173555 A604109     DF       CTR-604W     15.00     20.00     5.00     0     0     173555 A604109     DF       CTR-604W     25.00     30.00     5.00     0     0     173557 A604109     DF       CTR-604W     35.00     30.00     5.00     0     0     173557 A604109     DF       CTR-604W     30.00     5.00     5     -0.3     173560 A604109     DF       CTR-604W     40.00	CTR-604E	65.00	70.00	5.00	4	-0.3	173587 A604109			
CTR-604E   0.00   5.00   5   -0.3   173574   A604109   DF   Deep angular floats - no outcrops or subcrops taken from bottom of both sides     CTR-604W   3.00   6.00   3.00   4   -0.3   173552   A604109   DF     CTR-604W   6.00   10.00   4.00   4   -0.3   173553   A604109   DF     CTR-604W   10.00   13.00   3.00   7   -0.3   173554   A604109   DF     CTR-604W   15.00   20.00   5.00   2   -0.3   173555   A604109   DF     CTR-604W   15.00   20.00   5.00   0   0   173557   A604109   DF     CTR-604W   25.00   30.00   5.00   0   0   173557   A604109   DF     CTR-604W   25.00   30.00   5.00   0   0   173557   A604109   DF     CTR-604W   35.00   5.00   5   -0.3   173560   A604109   DF     CTR-604W   40.00   45.00   5.00   2   -0.3   173561 <td>CTR-604E</td> <td>70.00</td> <td>75.00</td> <td>5.00</td> <td>4</td> <td>-0.3</td> <td>173588 A604109</td> <td></td> <td></td> <td></td>	CTR-604E	70.00	75.00	5.00	4	-0.3	173588 A604109			
CTR-604W   3.00   6.00   3.00   4   -0.3   173552 A604109   DF     CTR-604W   6.00   10.00   4.00   4   -0.3   173553 A604109   DF     CTR-604W   10.00   13.00   3.00   7   -0.3   173554 A604109   DF     CTR-604W   13.00   15.00   2.00   4   -0.3   173555 A604109   DF     CTR-604W   15.00   2.00   5.00   0   0   173557 A604109   DF     CTR-604W   25.00   5.00   0   0   173557 A604109   DF     CTR-604W   25.00   30.00   5.00   0   0   173557 A604109   DF     CTR-604W   25.00   30.00   5.00   0   0   173557 A604109   DF     CTR-604W   35.00   5.00   0   0   173558 A604109   DF     CTR-604W   35.00   5.00   5.00   2   -0.3   173563 A604109   DF     CTR-604W   45.00   5.00   5.00   2   -0.3   173563 A604109   DF <tr< td=""><td>CTR-604E</td><td>75.00</td><td>80.00</td><td>5.00</td><td>6</td><td>-0.3</td><td>173589 A604109</td><td></td><td></td><td></td></tr<>	CTR-604E	75.00	80.00	5.00	6	-0.3	173589 A604109			
CTR-604W   6.00   10.00   4.00   4   -0.3   173553   A604109   DF     CTR-604W   10.00   13.00   3.00   7   -0.3   173554   A604109   DF     CTR-604W   13.00   15.00   2.00   4   -0.3   173555   A604109   DF     CTR-604W   15.00   20.00   5.00   2   -0.3   173556   A604109   DF     CTR-604W   25.00   5.00   0   0   173557   A604109   DF     CTR-604W   25.00   30.00   5.00   0   0   173557   A604109   DF     CTR-604W   25.00   30.00   5.00   0   0   173557   A604109   DF     CTR-604W   35.00   5.00   0   0   173559   A604109   DF     CTR-604W   35.00   5.00   5   -0.3   173561   A604109   DF     CTR-604W   45.00   5.00   5.00   -2   -0.3   173563   A604109   DF     CTR-604W   45.00	CTR-604E	0.00	5.00	5.00	5	-0.3	173574 A604109			Deep angular floats - no outcrops or subcrops taken from bottom of both sides
CTR-604W   10.00   13.00   3.00   7   -0.3   173554 A604109   DF     CTR-604W   13.00   15.00   2.00   4   -0.3   173555 A604109   DF     CTR-604W   15.00   20.00   5.00   2   -0.3   173557 A604109   DF     CTR-604W   20.00   25.00   5.00   0   0   173557 A604109   DF     CTR-604W   25.00   30.00   5.00   0   0   173557 A604109   DF     CTR-604W   25.00   30.00   5.00   0   0   173557 A604109   DF     CTR-604W   30.00   35.00   5.00   0   0   173557 A604109   DF     CTR-604W   30.00   35.00   5.00   0   0   173558 A604109   DF     CTR-604W   35.00   40.00   45.00   5.00   2   -0.3   173561 A604109   DF     CTR-604W   45.00   55.00   2   -0.3   173563 A604109   DF     CTR-604W   55.00   5.00   2   -0.3   173564 A604109   <	CTR-604W	3.00	6.00	3.00	4	~0.3	173552 A604109			
CTR-604W   13.00   15.00   2.00   4   -0.3   173555   A604109   DF     CTR-604W   15.00   20.00   5.00   2   -0.3   173556   A604109   DF     CTR-604W   20.00   25.00   5.00   0   0   173557   A604109   DF     CTR-604W   25.00   30.00   5.00   0   0   173557   A604109   DF     CTR-604W   30.00   35.00   5.00   0   0   173557   A604109   DF     CTR-604W   30.00   35.00   5.00   0   0   173558   A604109   DF     CTR-604W   30.00   44.00   45.00   5.00   5   -0.3   173561   A604109   DF     CTR-604W   45.00   5.00   2   -0.3   173562   A604109   DF     CTR-604W   45.00   5.00   2   -0.3   173563   A604109   DF     CTR-604W   50.00   5.00   2   -0.3   173563   A604109   DF     CTR-604W	CTR-604W	6.00	10.00	4.00	4	-0.3	173553 A604109			
CTR-604W   15.00   20.00   5.00   2   -0.3   173556   A604109   DF     CTR-604W   20.00   25.00   5.00   0   0   173557   A604109   DF     CTR-604W   25.00   30.00   5.00   0   0   173558   A604109   DF     CTR-604W   30.00   35.00   5.00   0   0   173559   A604109   DF     CTR-604W   35.00   40.00   5.00   5   -0.3   173550   A604109   DF     CTR-604W   35.00   40.00   5.00   5   -0.3   173561   A604109   DF     CTR-604W   40.00   45.00   5.00   -2   -0.3   173561   A604109   DF     CTR-604W   45.00   50.00   -2   -0.3   173562   A604109   DF     CTR-604W   50.00   5.00   -2   -0.3   173563   A604109   DF     CTR-604W   50.00   5.00   -2   -0.3   173564   A604109   DF     CTR-604W   60.00 <td>CTR-604W</td> <td>10.00</td> <td>13.00</td> <td>3.00</td> <td>7</td> <td>-0.3</td> <td>173554 A604109</td> <td>DF</td> <td></td> <td></td>	CTR-604W	10.00	13.00	3.00	7	-0.3	173554 A604109	DF		
CTR-604W   20.00   25.00   5.00   0   0   173557   A604109   DF     CTR-604W   25.00   30.00   5.00   0   0   173558   A604109   DF     CTR-604W   30.00   35.00   5.00   0   0   173559   A604109   DF     CTR-604W   35.00   40.00   5.00   5   -0.3   173560   A604109   DF     CTR-604W   40.00   45.00   5.00   -2   -0.3   173561   A604109   DF     CTR-604W   40.00   45.00   5.00   -2   -0.3   173561   A604109   DF     CTR-604W   50.00   5.00   -2   -0.3   173562   A604109   DF     CTR-604W   50.00   5.00   -2   -0.3   173562   A604109   DF     CTR-604W   50.00   5.00   -2   -0.3   173564   A604109   DF     CTR-604W   60.00   65.00   5.00   -2   -0.3   173565   A604109   DF     CTR-604W   60.00 </td <td>CTR-604W</td> <td>13.00</td> <td>15.00</td> <td>2.00</td> <td>4</td> <td>-0.3</td> <td>173555 A604109</td> <td></td> <td></td> <td></td>	CTR-604W	13.00	15.00	2.00	4	-0.3	173555 A604109			
CTR-604W   25.00   30.00   5.00   0   0   173558   A604109   DF     CTR-604W   30.00   35.00   5.00   0   0   173559   A604109   DF     CTR-604W   35.00   40.00   5.00   5   -0.3   173560   A604109   DF     CTR-604W   40.00   45.00   5.00   -2   -0.3   173561   A604109   DF     CTR-604W   40.00   45.00   5.00   -2   -0.3   173561   A604109   DF     CTR-604W   45.00   50.00   -2   -0.3   173562   A604109   DF     CTR-604W   50.00   50.00   -2   -0.3   173562   A604109   DF     CTR-604W   50.00   50.00   2   -0.3   173563   A604109   DF     CTR-604W   50.00   50.00   -2   -0.3   173564   A604109   DF     CTR-604W   60.00   65.00   5.00   -2   -0.3   173565   A604109   DF     CTR-604W   65.00	CTR-604W	15.00	20.00	5.00	2	-0.3	173556 A604109	DF		
CTR-604W   30.00   35.00   5.00   0   0   173559   A604109   DF     CTR-604W   35.00   40.00   5.00   5   -0.3   173560   A604109   DF     CTR-604W   40.00   45.00   5.00   -2   -0.3   173561   A604109   DF     CTR-604W   45.00   50.00   -2   -0.3   173562   A604109   DF     CTR-604W   45.00   50.00   -2   -0.3   173562   A604109   DF     CTR-604W   50.00   50.00   2   -0.3   173562   A604109   DF     CTR-604W   50.00   50.00   2   -0.3   173562   A604109   DF     CTR-604W   55.00   5.00   -2   -0.3   173563   A604109   DF     CTR-604W   60.00   65.00   5.00   -2   -0.3   173565   A604109   DF     CTR-604W   65.00   70.00   5.00   -2   -0.3   173565   A604109   DF     CTR-604W   65.00   70.00   <	CTR-604W	20.00	25.00	5.00	0	0	173557 A604109			
CTR-604W   35.00   40.00   5.00   5   -0.3   173560   A604109   DF     CTR-604W   40.00   45.00   5.00   -2   -0.3   173561   A604109   DF     CTR-604W   45.00   50.00   5.00   -2   -0.3   173561   A604109   DF     CTR-604W   45.00   55.00   5.00   -2   -0.3   173562   A604109   DF     CTR-604W   50.00   55.00   2   -0.3   173563   A604109   DF     CTR-604W   55.00   60.00   5.00   -2   -0.3   173563   A604109   DF     CTR-604W   55.00   65.00   5.00   -2   -0.3   173563   A604109   DF     CTR-604W   65.00   5.00   -2   -0.3   173565   A604109   DF     CTR-604W   65.00   70.00   5.00   -2   -0.3   173566   A604109   DF     CTR-604W   65.00   70.00   5.00   -2   -0.3   173566   A604109   DF <t< td=""><td>CTR-604W</td><td>25.00</td><td>30.00</td><td>5.00</td><td>0</td><td>0</td><td></td><td></td><td></td><td></td></t<>	CTR-604W	25.00	30.00	5.00	0	0				
CTR-604W   40.00   45.00   5.00   -2   -0.3   173561   A604109   DF     CTR-604W   45.00   50.00   5.00   -2   -0.3   173562   A604109   DF     CTR-604W   50.00   55.00   5.00   -2   -0.3   173563   A604109   DF     CTR-604W   50.00   55.00   5.00   -2   -0.3   173564   A604109   DF     CTR-604W   55.00   60.00   5.00   -2   -0.3   173564   A604109   DF     CTR-604W   60.00   65.00   5.00   -2   -0.3   173565   A604109   DF     CTR-604W   65.00   70.00   5.00   -2   -0.3   173565   A604109   DF     CTR-604W   65.00   70.00   5.00   -2   -0.3   173566   A604109   DF	CTR-604W	30.00	35.00	5.00	0	0	173559 A604109			
CTR-604W   45.00   50.00   5.00   -2   -0.3   173562 A604109   DF     CTR-604W   50.00   55.00   5.00   2   -0.3   173563 A604109   DF     CTR-604W   55.00   60.00   5.00   -2   -0.3   173564 A604109   DF     CTR-604W   55.00   60.00   5.00   -2   -0.3   173564 A604109   DF     CTR-604W   60.00   65.00   5.00   -2   -0.3   173565 A604109   DF     CTR-604W   65.00   70.00   5.00   -2   -0.3   173566 A604109   DF	CTR-604W	35.00	40.00	5.00	5	-0.3	173560 A604109			
CTR-804W   50.00   55.00   5.00   2   -0.3   173563   A604109   DF     CTR-604W   55.00   60.00   5.00   -2   -0.3   173564   A604109   DF     CTR-604W   60.00   65.00   5.00   -2   -0.3   173565   A604109   DF     CTR-604W   60.00   65.00   5.00   -2   -0.3   173565   A604109   DF     CTR-604W   65.00   70.00   5.00   -2   -0.3   173566   A604109   DF	CTR-604W	40.00	45.00	5.00	-2	-0.3	173561 A604109			
CTR-604W 55.00 60.00 5.00 -2 -0.3 173564 A604109 DF CTR-604W 60.00 65.00 5.00 -2 -0.3 173565 A604109 DF CTR-604W 65.00 70.00 5.00 -2 -0.3 173566 A604109 DF	CTR-604W	45.00	50.00	5.00		-0.3				
CTR-604W 60.00 65.00 5.00 -2 -0.3 173565 A604109 DF CTR-604W 65.00 70.00 5.00 -2 -0.3 173566 A604109 DF	CTR-604W	50.00	55.00	5.00	2	-0.3	173563 A604109			
CTR-604W 65.00 70.00 5.00 -2 -0.3 173566 A604109 DF	CTR-604W	55.00	60.00	5.00	-2	-0.3				
	CTR-604W	60.00	65.00	5.00	-2	-0.3	173565 A604109			
CTR-604W 70.00 75.00 5.00 -2 -0.3 173567 A604109 DF	CTR-604W	65.00	70.00	5.00	-2	-0.3	173566 A604109			
	CTR-604W	70.00	75.00	5.00	-2	-0.3	173567 A604109	DF		

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CTR-604W	75.00	80.00	5.00	-2	-0.3	173568 A604109	DF		
CTR-604W	80.00	85.00	5.00	-2	-0.3	173569 A604109	DF		
CTR-604W	85.00	90.00	5.00	2	-0.3	173570 A604109	DF		
CTR-604W	90.00	95.00	5.00	3	-0.3	173571 A604109	DF		
CTR-604W	95.00	100.00	5.00	2	-0.3	173572 A604109	DF		
CTR-604W	100.00	107.00	7.00	-2	-0.3	173573 A604109	DF		
CTR-604W	0.00	3.00	3.00	4	-0.3	173551 A604109	DF		Trench from
CTR-612-CE	50.00	53.00	3.00	8	-0.3	173523 A604467	East		
CTR-612-CE	38.00	41.00	3.00	11	0.3	173524 A604467	East		
CTR-612-CE	35.00	38.00	3.00	7	0.3	173525 A604467	East		
CTR-612-CE	32.00	35.00	3.00	3	0.3	173526 A604467	East		
CTR-612-CE	29.00	32.00	3.00	3	0.3	173527 A604467	East		
CTR-612-CE	27.00	29.00	2.00	3	0.4	173528 A604467	East		
CTR-612-CE	24.00	27.00	3.00	2	-0.3	173529 A604467	East	down	
CTR-612-CE	24.00	26.00	2.00	3	-0.3	173530 A604467	East	top	
CTR-612-CE	18.00	21.00	3.00	4	-0.3	173531 A604467	East		
CTR-612-CE	14.00	16.00	2.00	-2	-0.3	173532 A604467	East		
CTR-612-CE	11.00	14.00	3.00	5	-0.3	173533 A604467	East		
CTR-612-CE	8.00	11.00	3.00	4	0.5	173534 A604467	East		
CTR-612-CE	5.00	6.50	1.50	5	0.3	173535 A604467	East	down	
CTR-612-CE	2.00	6.00	4.00	4	-0.3	173536 A604467	East	ctr	
CTR-612-CE	1.00	2.00	1.00	-2	-0.3	173537 A604467	East	top	(1-3m intv)
CTR-612-CE	-1.00	2.00	3.00	-2	-0.3	173538 A604467	East		
CTR-612-CE	57.00	58.00	1.00	3	0.7	173522 A604467	East	down	
CTR-612-CW	2.00	5.00	3.00	2	0.3	173502 A604467	West		
CTR-612-CW	5.00	11.00	6.00	-2	-0.3	173503 A604467	West	down	
CTR-612-CW	5.00	11.00	6.00	3	-0.3	173504 A604467	West	top	
CTR-612-CW	11.00	15.00	4.00	-2	0.3	173505 A604467	West	•	
CTR-612-CW	15.00	19.00	4.00	2	-0.3	173506 A604467	West		
CTR-612-CW	19.00	24.00	5.00	-2	-0.3	173507 A604467	West		
CTR-612-CW	24.00	28.00	4.00	-2	-0.3	173508 A604467	West		
CTR-612-CW	28.00	31.00	3.00	2	-0.3	173509 A604467	West		
CTR-612-CW	31.00	34.00	3.00	-2	-0.3	173510 A604467	West		
CTR-612-CW	34.00	37.00	3.00	2	-0.3	173511 A604467	West		
CTR-612-CW	37.00	40.00	3.00	3	-0.3	173512 A604467	West		
CTR-612-CW	40.00	43.00	3.00	·2	-0.3	173513 A604467	West		
CTR-612-CW	43.00	46.00	3.00	-2	0.4	173514 A604467	West		
CTR-612-CW	46.00	49.00	3.00	2	-0.3	173515 A604467	West		
CTR-612-CW	49.00	52.00	3.00	2	-0.3	173516 A604467	West		
CTR-612-CW	52.00	55.00	3.00	-2	-0.3	173517 A604467	West	down	
CTR-612-CW	55.00	57.00	2.00	2	0.3	173518 A604467	West	top	
CTR-612-CW	56.00	58.00	2.00	8	0.5	173519 A604467	West	ctr	
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Trench from west to east - mostly deep float from heap side of trench - see notes

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CTR-612-CW	57.00	59.00	2.00	4	0.6	173520 A604467	West	down	n	24-Jul-06
CTR-612-CW	-1.00	2.00	3.00	2	-0.3	173501 A604467	West		Heading north	24-Jul-06
CTR-612NE	20.00	23.00	3.00	7	-0.3	201459 A603953	East		see trench map	14-Jul-06
CTR-612NE	23.00	26.00	3.00	·2	-0.3	201461 A603953	East		see trench map	14-Jul-06
CTR-612NE	26.00	29.00	3.00	4	-0.3	201463 A603953	East		see trench map	14-Jul-06
CTR-612NE	44.00	47.00	3.00	4	0.3	201470 A603953	East		see trench map	14-Jul-06
CTR-612NE	47.00	50.00	3.00	2	-0.3	201472 A603953	East		see trench map	14-ปมโ-06
CTR-612NE	50.00	53.00	3.00	-2	0.3	201474 A603953	East		see trench map	14-Jul-06
CTR-612NE	60.00	63.00	3.00	3	-0.3	201478 A603953	East		Mostly dirt	14-Jui-06
CTR-612NE	63.00	66.00	3.00	7	-0.3	201480 A603953	East		Mostly dirt	14-Jui-06
CTR-612NE	17.00	20.00	3.00	7	-0.3	201457 A603953	East		see trench map	14-Jul-06
CTR-612NW	4.00	8.00	4.00	-2	-0.3	201452 A603953	West	NW-	&Flor Mosaic fine breccia vnlet +/- sil+/- dol nodules	14-Ju <del>l</del> -06
CTR-612NW	8.00	11.00	3.00	-2	-0.3	201453 A603953	West		two third mosaic fine bx 1/3 fracture bx	· 14-Jul-06
CTR-612NW	11.00	14.00	3.00	7	0.3	201454 A603953	West		representative lst micrite	14-Jul-06
CTR-612NW	14.00	17.00	3.00	3	-0.3	201455 A603953	West		see trench map	14-Jul-06
CTR-612NW	17.00	20.00	3.00	2	0.4	201456 A603953	West		see trench map	14-Jul-06
CTR-612NW	20.00	23.00	3.00	-2	-0.3	201458 A603953	West		see trench map	14-Jul-06
CTR-612NW	23.00	26.00	3.00	-2	0.3	201460 A603953	West		see trench map; +floor	14-Jul-06
CTR-612NW	26.00	29.00	3.00	-2	-0.3	201462 A603953	West		see trench map; end of trench below rd level	14-Jul-06
CTR-612NW	29.00	32.00	3.00	2	-0.3	201464 A603953	West		see trench map	14-Jul-06
CTR-612NW	32.00	35.00	3.00	2	-0.3	201465 A603953	West		into broken ground BZ Micrite and sil nodules +/- dol fract	14-Jui-06
CTR-612NW	35.00	38.00	3.00	2	-0.3	201466 A603953	West		see trench map	14-Jui-06
CTR-612NW	38.00	41.00	3.00	2	-0.3	201467 A603953	West		see trench map	1 <b>4</b> -Jul-06
CTR-612NW	41.00	44.00	3.00	-2	0.3	201468 A603953	West	W&	llooré see trench map	14-Jul-06
CTR-612NW	44.00	47.00	3.00	-2	0.5	201469 A603953	West		see trench map	14-Jul-06
CTR-612NW	47.00	50.00	3.00	-2	-0.3	201471 A603953	West		see trench map	14-Jul-06
CTR-612NW	50.00	53.00	3.00	-2	-0.3	201473 A603953	West		see trench map	14-Jul-06
CTR-612NW	53.00	56.00	3.00	2	-0.3	201475 A603953	West		see trench map	14-Ju⊢06
CTR-612NW	56.00	60.00	4.00	2	-0.3	201476 A603953	West		see trench map	14-Jul-06
CTR-612NW	60.00	63.00	3.00	-2	-0.3	201477 A603953	West		see trench map	14-Jul-06
CTR-612NW	63.00	66.00	3.00	2	-0.3	201479 A603953	West			14-Jul-06
CTR-612NW	66.00	69.00	3.00	3	-0.3	201481 A603953	West		trench stops at 67m rest is on W rd bank exposure	14-Jul-06
CTR-612NW	69.00	72.00	3.00	3	0.3	201482 A603953	West			14-Jul-06
CTR-612NW	72.00	75.00	3.00	4	0.3	201483 A603953	West			14-Jul-06
CTR-612NW	75.00	78.00	3.00	2	-0.3	201484 A603953	West			1 <b>4-Jui-0</b> 6
CTR-612NW	78.00	81.00	3.00	6	-0.3	201485 A603953	West			14-Jul-06
CTR-612NW	81.00	86.00	5.00	-2	0.3	201486 A603953	West	υр	nodular sil/dol lst	1 <b>4</b> -Jul-06
CTR-612NW	81.00	86.00	5.00	-2	-0.3	201487 A603953	West			14-Jul-06
CTR-612NW	86.00	90.00	4.00	2	0.3	201488 A603953	West		bent structure?	14-Jul-06
CTR-612NW	90.00	94.00	4.00	2	-0.3	201489 A603953	West		end of rd cut	14-Jul-06
CTR-612NW	0.00	4.00	4.00	-2	0.5	201451 A603953	West		Starts at road elbow going north. Lst + dol cracled lst micrite	14-Jul-06
CTR-612SE	107.00	110.00	3.00	7	-0.3	201402 A604467	East			22-Jul-06

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CTR-612SE	110.00	112.00	2.00	7	-0.3	201403 A604467	East		Limey clayey dirt	22-Jul-06
CTR-612SE	112.00	114.00	2.00	15	-0.3	201404 A604467	East		velicw clay	22-Jul-06
CTR-612SE	114.00	117.50	3.50	4	-0.3	201405 A604467	East	down	base rusty clay only	22-Jul-06
CTR-612SE	114.00	177.50	63.50	3	-0.3	201406 A604467	East	ctr	grey clay layer only	22-Jul-06
CTR-612SE	114.00	117.50	3.50	5	-0.3	201407 A604467	East	top	brown clay/dirt above grey	22-Jul-06
CTR-612SE	117.50	120.00	2.50	7	-0.3	201408 A604467	East		brown & yellow clay	22-Jul-06
CTR-612SE	120.00	123.00	3.00	7	-0.3	201409 A604467	East		beige dirt & angular rubble	22-Jul-06
CTR-612SE	133.00	137.00	4.00	2	-0.3	201410 A604467	East		beige grey doi ist /argiilaceous	22-Jul-06
CTR-612SE	136.00	139.00	3.00	-2	-0.3	201411 A604467	East		limonitic dol claeyey rusty	22-Jui-06
CTR-612SE	139.00	141.00	2.00	-2	-0.3	201412 A604467	East	down	beige grey dol ist /argillaceous - gap in eastern sampling after that	22-Jul-06
CTR-612SE	150.00	154.00	4.00	3	-0.3	201413 A604467	East		dol +/- argillaceous	22-Jul-06
CTR-612SE	103.00	107.00	4.00	5	-0.3	201401 A604467	East		rocks only - dol ist beige to buff	22-Jul-06
CTR-612SW	3.00	6.00	3.00	4	-0.3	173002 A603953	West		Limonitic altered Syenite (green porph) - +/- rubbly. Shallow dipping sill	. 13-Jui-06
CTR-612SW	6.00	9.00	3.00	3	-0.3	173003 A603953	West		Limonitic attered Syenite (green porph) - +/- rubbly	13-Ju <del>l 0</del> 6
CTR-612SW	9.00	11.00	2.00	-2	-0.3	173004 A603953	West		Limonitic attered Syenite (green porph) - +/- rubbly	13-Jul-06
CTR-612SW	11.00	14.00	3.00	3	-0.3	173005 A603953	West		si Limonitic altered Syenite (green porph) - solid porphyry green syenite	13-Jul-06
CTR-612SW	14.00	17.00	3.00	5	-0.3	173006 A603953	West		st Limoniëc altered Syenite (green porph) - solid porphyry green syenite	13-Jul-06
CTR-612SW	17.00	19.00	2.00	-2	-0.3	173007 A603953	West		sl Limonitic altered Syenite (green porph) - solid porphyry green syenite	13-Jul-06
CTR-612SW	19.00	22.00	3.00	2	-0.3	173008 A603953	West		sl Limonitic altered Syenite (green porph) - solid porphyry green syenite	13-Jul-06
CTR-612SW	22.00	25.00	3.00	-2	-0.3	173009 A603953	West		sl Limonitic altered Syenite (green porph) - blocky porphyry green syenite. Much vert jointing	13-Jul-06
CTR-612SW	25.00	28.00	3.00	-2	-0.3	173010 A603953	West		sl Limonitic altered Syenite (green porph) - blocky porphyry green syenite	13-Jul-06
CTR-612SW	28.00	31.00	3.00	-2	-0.3	173011 A603953	West		sl Limonitic altered Syenite (green porph) - blocky porphyry green syenite	13-Jul-06
CTR-612SW	31.00	34.00	3.00	-2	-0.3	173012 A603953	West		sl Limonitic altered Syenite (green porph) - blocky porphyry green syenite	13-Jul-06
CTR-612SW	34.00	37.00	3.00	-2	-0.3	173013 A603953	West		sl Limonitic altered Syenite (green porph) - blocky porphyry green syenite	13-Jul-06
CTR-612SW	37.00	40.00	3.00	-2	-0.3	173014 A603953	West		sl Limonitic altered Syenite (green porph) - blocky porphyry green syenite	13-Jul-06
CTR-612SW	40.00	43.00	3.00	2	-0.3	173015 A603953	West		sl Limonitic altered Syeriite (green porph) - blocky porphyry green syenite	13-Jul-06
CTR-612SW	43.00	46.00	3.00	-2	-0.3	173016 A603953	West		sl Limonitic altered Syenite (green porph) - blocky porphyry green syenite	13-Jul-06
CTR-612SW	46.00	49.00	3.00	-2	-0.3	173017 A603953	West		st Limonitic altered Syenite (green porph) - blocky porphyry green syenite	13-Jul-06
CTR-612SW	49.00	52.00	3.00	-2	-0.3	173018 A603953	West		sl Limonitic altered Syenite (green porph) - blocky porphyry green syenite	13-Jul-06
CTR-612SW	52.00	55.00	3.00	2	-0.3	173019 A603953	West		sl Limonitic altered Syenite (green porph) - blocky porphyry green syenite	13-Jul-06
CTR-612SW	55.00	60.00	5.00	2	-0.3	173020 A603953	West	down	very Limonitic altered Syenite (green porph) - blocky porphyry green syenite	13-Jul-06
CTR-612SW	55.00	60.00	5.00	-2	-0.3	173021 A603953	West	top	grey ist just above rusty contact	13-Jul-06
CTR-612SW	60.00	63.00	3.00	-2	-0.3	173022 A603953	West		grey ist	13-Jul-06
CTR-612SW	63.00	66.00	3.00	4	0.3	173023 A603953	West		grey ist	13-Jul-06
CTR-612SW	66.00	70.00	4.00	3	-0.3	173024 A603953	West		grey ist	13-Jul-06
CTR-612SW	70.00	75.00	5.00	-2	-0.3	173201 A604467	West			22-Jul-06
CTR-612SW	75.00	80.00	5.00	-2	-0.3	173202 A604467	West			22-Jul-06
CTR-612SW	80.00	85.00	5.00	-2	-0.3	173203 A604467	West			22-Jul-06
CTR-612SW	85.00	88.00	3.00	-2	-0.3	173204 A604467	West			22-Jul-06
CTR-612SW	88.00	90.00	2.00	3	-0.3	173205 A604467	West			22-Jul-06
CTR-612SW	90.00	95.00	5.00	-2	-0.3	173206 A604467	West			22-Jul-06
CTR-612SW	95.00	100.00	5.00	-2	-0.3	173207 A604467	West			22-Jul-06

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CTR-612SW	100.00	104.00	4.00	-2	-0.3	173208 A604467	West			22-Jul-06
CTR-612SW	104.00	107.00	3.00	5	-0.3	173209 A604467	West			22-Jul-06
CTR-612SW	107.00	110.00	3.00	18	-0.3	173210 A604467	West		above diagonal line	22-Jul-06
CTR-612SW	110.00	112.00	2.00	2	-0.3	173211 A604467	West		below diagonal line	22-Jul-06
CTR-612SW	112.00	114.00	2.00	2	-0.3	173212 A604467	West			22-Jul-06
CTR-612SW	114.00	117.00	3.00	3	-0.3	173213 A604467	West	down		22-Jul-06
CTR-612SW	114.00	117.00	3.00	5	-0.3	173214 A604467	West	съ		22-Jul-06
CTR-612SW	114.00	117.00	3.00	13	-0.3	173215 A604467	West	top		22-Jul-06
CTR-612SW	117.00	120.00	3.00	3	-0.3	173216 A604467	West	down		22-Jul-06
CTR-612SW	117.00	120.00	3.00	3	-0.3	173217 A604467	West	top		22-Jul-06
CTR-612SW	120.00	123.00	3.00	-2	-0.3	173218 A604467	West	ail		22-JuH06
CTR-612SW	123.00	126.00	3.00	5	-0.3	173219 A604467	West			22-Jul-06
CTR-612SW	126.00	130.00	4.00	-2	-0.3	173220 A604467	West		rocks only	· 22-Ju#-06
CTR-612SW	130.00	133.00	3.00	6	-0.3	173221 A604467	West	all		22-Jul-06
CTR-612SW	133.00	135.00	2.00	2	-0.3	173222 A604467	West	down		22-Jul-06
CTR-612SW	133.00	135.00	2.00	10	-0.3	173223 A604467	West	top		22-Jul-06
CTR-612SW	135.00	138.00	3.00	4	-0.3	173224 A604467	West	down	beneath line rusty clay	22-Jul-06
CTR-612SW	135.00	138.00	3.00	4	-0.3	173225 A604467	West	top	grey clay mart	22-Jul-06
CTR-612SW	138.00	140.00	2.00	4	-0.3	173226 A604467	West	all	all grey beige	22-Jul-06
CTR-612SW	140.00	142.00	2.00	-2	-0.3	173227 A604467	West		rocks grey/beige	22-Jul-06
CTR-612SW	142.00	145.00	3.00	2	-0.3	173228 A604467	West	down	base grey ist/clay	22-Jul-06
CTR-612SW	142.00	145.00	3.00	9	-0.3	173229 A604467	West	top	yellow clay pocket above	22-Jul-06
CTR-612SW	145.00	147.00	2.00	3	-0.3	173230 A604467	West		angular beige rubble	22-Jul-06
CTR-612SW	147.00	151.00	4.00	5	-0.3	173231 A604467	West	down	beige rocks and clay	22-Jul-06
CTR-612SW	147.00	151.00	4.00	5	-0.3	173232 A604467	West	top	angular floats andd fine beige	22-Jul-06
CTR-612SW	151.00	153.00	2.00	5	-0.3	173233 A604467	West	down	lower clay - yellow only	22-Jul-06
CTR-612SW	153.00	156.00	3.00	2	-0.3	173234 A604467	West	down	below line yellow clay	22-Jui-06
CTR-612SW	153.00	156.00	3.00	2	-0.3	173235 A604467	West	top	above line angular float subcrop	22-Jul-06
CTR-612SW	156.00	160.00	4.00	2	-0.3	173236 A604467	West		rocks	22-Jul-06
CTR-612SW	160.00	165.00	5.00	-2	-0.3	173237 A604467	West		rocks	22-Jul-06
CTR-612SW	165.00	170.00	5.00	-2	-0.3	173238 A604467	West	down	rocks	22-Jul-06
CTR-612SW	165.00	170.00	5.00	5	-0.3	173239 A604467	West	top	rusty layer dirt	22-Jul-06
CTR-612SW	170.00	175.00	5.00	3	0.3	173240 A604467	West	down	beige clay - float dol	22-Jul-06
CTR-612SW	170.00	175.00	5.00	5	0.3	173241 A604467	West	top	upper bench grey and rusty	22-Jul-06
CTR-612SW	175.00	178.00	3.00	3	-0.3	173242 A604467	West			22-Jul-06
CTR-612SW	178.00	182.00	4.00	2	-0.3	173243 A604467	West			22-Jul-06
CTR-612SW	182.00	187.00	5.00	3	-0.3	173244 A604467	West			22-Jul-06
CTR-612SW	187.00	192.00	5.00	2	-0.3	173245 A604467	West		end of trench	22-Jul-06
CTR-612SW	0.00	3.00	3.00	2	-0.3	173001 A603953	West		grey ist	13-Jul-06
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لاستنبه الاستنبة الاستنبة الاستنبة الاستنبار المتنب الاستنبار المنابع

	From ACME	ANALYTICAL I	ABORATORI	ES LTD. 852	E. HASTIN	NGS ST. VANCOL	VER BC VE	6A 1R6 PHONE	E(604)	)253-3158 F	AX(604)253	-1716@C	OV TEXT FORM	IAT				<u> </u>
		lesources Ltd.			T	T	I			·	·····					-		
	Acme file # A	603953 Page 1	Received: J	UL 20 2006 *	101 sam	ples in this disk fil	Ð.		]									
	Anatysis: GRO					2-2-2 HCL-HNO3-												
ELEMENT	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	-	As	U	Au	Th	Sr	Cd		Sb
SAMPLES	ppm	ppm	ppm	ppm	ppm	ррт	ppm	ppm	%		ppm	ppm	ppm	ррт	ppm	ppn	<u> </u>	ppm
G-1	<1	2	3		<.3			3 49		1.81		<8	<2		3	53 <.5		<3
173001	4	¥ 1	4	13	<.3		3 <1	11	-	0.16		3 <8	<2	2	:	372 <.5		<3
173002	2	2 17	17	94	<.3	4		7 85		4.25		8 <8	<2		4	36	1.8	
173003	1	11	14		<.3		8	7 99		4.4		3 <8	<2		4	44	1.8	1
173004	1	13	15		<.3		J	7 100		4.45		5 <8	<2		5	43	1.8	
173005	<1	10	19		<.3	1		7 107	-	4.31		2 <8	<2		5	48		<3
173006	<1	12			<.3			6 107		4.37		3 <8	<2		6	59	2.1	
173007	<1	12			<.3	1		6 101	4	4.34		<8	<2		5	55	2.1	
173008	<1	11	22		<.3			6 100	)4	4.26		2 <8	<2		6	63	2.1	
173009	<1	11	17		<.3		2	6 105		4.46		3 <8	<2		5	61		<3
173010	<1	11	19	94	<.3	1	2	6 108	34	4.55		2 <8	<2		6	61		<3
173011	<1	12	19	103	<.3		2	6 109		4.51		2 <8	<2		5	63		<3
173012	1	i 12	15	95	<.3		2	7 113	35	4.48		2 <8	<2		6	61		<3
173013	1	14	20	97	′ <.3		2	7 106	<u>}5</u>	4.38		2 <8	<2		6	54		<3
RE 173013	<1	14	23	98	<.3		2	7 108	31	4.48	<2	<8	<2		6	55		<3
173014	<1	12	22	93	<.3		2	6 115	51	4.44	2	<8	<2		5	53	2.1	
173015	<1	9	23	98	<.3		?	7 137	79	4.57	~2	<8	<2		5	44	2.1	
173016	<1	8	8	91	<.3		2	7 108	31	4.39	<2	<8	<2		4	66		<3
173017	<1	8	14	90	<.3		2	7 80	)1	4.59	<2	<8	<2		4	59		<3
173018	<1	9	12	87	<.3		2	7 73	37	4.59		<8	<2		4	39		<3
173019	<1	6	16	73	<.3		2	7 59	97	4.3	<2	<8	<2		4	31	1.6	
173020	1	1 14	17	66	<.3		2	7 48	39	4		4 <8	<2		6	26	1.6	<3
173021		1	4	15	.3		3 <1	57	78	0.27	~2	<8	<2	<2		236 <.5		
173022	1	1 1	6	g	<.3		3 <1	43		0.27	<2	<8	<2	<2		329 <.5		<3
173023	1	1 <1	5	5		0.3	3 <1	37	78	0.19	<2	<8	<2	<2		261 <.5		<3
173024	1	1 <1	<3	4	<.3		2 <1	22	23	0.21		<8	<2	<2		153 <.5		<3
201451	:	3 4	7	33	5	0.5 1	1		74	0.94		3 <8	<2			204 <.5		<3
201452		1 3	9	27	<.3		5	-	64	0.39		3 <8	<2	2		286	0.5	<3
201453	<1	1	<3	15	<.3		2 <1	3	39	0.17	2	<8	<2	2		261 <.5		<3
201454	1	1 3	6	35	5	0.3	3	1 4	18	0.35		3	9 <2	2		259	0.6	<3
201455	1	1 2	<3	15	5 <.3		•	1 11	11	0.52		3 <8	<2	2		220 <.5		<3
201456	1 3	2 4	7	30		0.4 1	2	3 7	76	0.84		4 <8	<2	2		184 <.5		<3

Eastfield - A603953 (G1D)\_C01A

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							-				_			A.L.	N	w	Comple
	Bi	<u>v</u>	Ca	P		La	+	Mg %	Ba	Ti %	B	A %		Na %	K		Sample
	ppm	ppm	%	%		ppm –	ppm		ppm 197		ppm	3	° 0.96			ppm 3 <2	kg
	<3			).46	0.073	7	6			) <.01	2 <3	3	0.90			2 <2	3.94
173001		 		0.69	0.017	4	6 5				<3 1 <3		3.05			3 <2	9.51
173002				.68	0.115	32 38						i	2.4	0.01		1 <2	6.66
173003				).63	0.125		3				<u>4 &lt;3</u> 1 <3		2.25			<2	7.55
173004				).61	0.123	34	4		· · · · · · · · · · · · · · · · · · ·		1 <3 9 <3		2.25	0.02		1 <2	. 5.51
173005	3			).71	0.13	26		1.2			-	_		0.03		2 <2	6.02
173006				.02	0.132	26						4	1.41	0.06		2 <2 9 <2	5.85
173007	4			.25	0.133	25		0.9				-				# <2   <2	6.53
173008	4			.38	0.135	25						8	1.52				7.23
173009				.55	0.138	25						9	1.58			7 <2	1.23
173010				.49	0.141	28						12	1.59			1 <2	4.38
173011				.38	0.141	27						7	1.6			3 <2	
173012				.39	0.137	28						11	1.65			1 <2	4.81
173013	3			l.31	0.14	27						9	1.55			3 <2	4.58
RE 173013	<3			1.34	0.14	27	4	0.75				9	1.56			3 <2	
173014	<3			0.9	0.134	29			6			4	1.48			1 <2	5.2
173015	4			).64	0.135	27		1.63			6 <3		1.6			3 <2	3.92
173016				).63	0.127	27					4 <3		1.94			1 <2	4.23
173017				0.6	0.133	28		2.48			6 <3		2.3			1 <2	3.97
173018	<3			).57	0.132			2.56			1 <3		2.47			3 <2	3.96
173019	3		32	0.6	0.126			2.56			97 <3		2.7			3 <2	3.69
173020	3		83 0	).95	0.124	31	5				3 <3		<u>3.14</u>			4 <2	4.11
173021		T ·- · -		1.27	0.015		-			9 <.01	<3		0.18			1 <2	2.7
173022	<3		6 22	2.27	0.035	3	7	7.15		3 <.01	<3		0.24			1 <2	4.14
173023			5 23	3.67	0.025	3	10	8.85	5 3	7 <.01	<3		0.2	0.02		1 <2	2.69
173024			4 18	3.93	0.021	4	8	8.63	10	6 <.01	<3		0.14	0.02		1 <2	3.98
201451	<3	1	42 14	1.43	0.017	6	23	8.8	2	0<.01		16	0.89	0.03		2 <2	3.97
201452				25.1	0.016	7	17	2.78	23	ī <.01	1	7	0.29	0.02		6 <2	3.89
201453		1		6.39	0.012	5	12	0.39	) 7(	6 <.01	<3		0.08	0.01		4 <2	2.90
201454		1		).66	0.022	7	20	1.09		) <.01		4	0.2	0.01		1 <2	3.93
201455	3			7.92	0.022	5						5	0.26	0.01	0.1	3 <2	3.5
201456				5.17	0.02					3 <.01		9	0.63			9 <2	4.9

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ELEMENT	Mo	Cu		Pb	Zn	A	g	Ni	Co	Mn		Fe	As	U	Au	Th	Sr	•	Cd		Sb
SAMPLES	ppm	pp	n	ppm	ppm		pm	ppm	ppm	ppm		%	ррт	ppm	ppm	ppm	ppm		ppm		ppm
201457		1	3		\$ · · · · · · · · · · · · · · · · · · ·	32 <	.3	7	′ <b></b>	1	70	0.45		2 <8	<2	<2	2	04	<.5		<3
201458	<1		1	4	l I	22 <	.3	1	<1		28	0.12	<2	<8	<2	<2	3	43	<.5		<3
201459		1	5	S	)	24 <	:.3	5	;	1	101	0.46	<2	<8	<2	<2	3	31		0.6	<3
STANDARD DS7		21	101	75	5 4	\$19	1	52	2	8	644	2.43		51	8 <2		5	76		6.4	
G-1	<1		2	<u>ا</u>	3	44 <	3	3	1	3	506	1.71	<2	<8	<2		4	55	<.5		<3
201460	<1		3	10	)	35	0.3	2	<1		45	0.18	<2	<8	<2	<2	3	00		0.5	<3
201461	<1		3	i<3		38 <	.3	2	2	1	41	0.15	<2	<8	<2	<2	3	23		0.6	<3
201462	<1		ī	<3	-	26 <	.3	2	2 <1		28	0.14	<2	<8	<2	<2	2	66	<.5		<3
201463	1	1	1	<3		17 <	:.3	2	! <1		26	0.16	<2	<8	<2	2	2	82	<.5		<3
201464	1	1	1	3	3	20 <	:.3	2	2 <1		30	0.12	<2	<8	<2	2	3	61	<.5		<3
201465	<1		1	5	5	13 <	.3	3	<1		36	0.2	<2	<8	<2	2		86			<3
201466	<1		1	<3		15 <	.3	3	<1		35	0.2	<2	<8	<2	2		27			<3
201467	<1	-	1	4	۱)	11 <	3	3	<1		28	0.17	<2	<8	<2	2		03			<3
201468		<b>-</b>	1	3	3	17	0.3	4	<1		38	0.22	<2	<8	<2	<2		28			ŝ
201469	<1		1	5	5	23	0.5	4	<1		44	0.21	2	<8	<2	2	and the second s	21			3
201470			1	4	4	15	0.3	5	5]<1		38	0.22	<2	<8	<2	2		34			<3
201471	<1		1	3	3	19 <		4	<1		53	0.25	<2		9 <2	2		04			<3
201472	<1		1	3	3	14 <	:.3	4	ţ	1	44	0.23	2	<8	<2	<2		04			<3
201473		1	1	<3		17 <	.3	4	<1		38	0.23	<2	<8	<2	2	2	70	<.5		<3
201474	1	1	1	<3	1	16	0.3	4	<1		39	0.26		<8	<2	2		86	<.5		<3
201475		1 <1		<3		15 <	:.3	4	<1		35	0.19	2	<8	<2	2	_	04		0.5	<3
201476		1	1	3	3	14 <	3	4	li_<1		38	0.23		2 <8	<2	2			<.5		<3
201477		1	1	7	7	21 <	3	4	<1		44	0.22	<2		8 <2	<2		89	<.5		<3
201478		1	4	. 4	l	47 <	3	6	3	1	200	0.79		<8	<2	<2	·	80		0.5	
201479	<1	<1		<3	1	17 <	3	5	i <1		44	0.22		<8	<2	2		26	<.5		<3
201480		1	5	5 3	3	41 <	.3	11		2	156	0.89		2 <8	<2	<2		80		0.7	
201481		1 <1		<3	-	18.<	.3	E	š <1		46	0.25	-2	<8	<2	<2			<.5		<3
201482	<1		1	<3	1	25	0.3		8	1	42	0.33		<8	<2	2	_		<.5		<3
201483	<1	<1		<3	1	17	0.3	i  E	<b>i</b>	1	39	0.2		<8	<2	ୟ ସ		29	<.5		<3
201484	<1		1	<3		17 <	c.3	4	•	1	- 33	0.22		<8	<2	2		91		0.5	_
201485	<1		1	<3		19 <	:.3	1 7		2	34	0.32		2 <8	<2	<2		72			<3
201486	<1		1	<3		15	0.3		-	1	41	0.24			10 <2	<2		36			<3
201487	<1	<1		4	ł	20 <	c.3	5	5	1	37	0.24		3 <8	<2	<2			<.5		<3
201488		1 <1		<3		26	0.3	6	5 <1		49			4	8 <2	<2		1	<.5		<3
201489	1	1 <1		<3		28 <	c.3	5	5 <1		58	0.3		3 <8	<2	<2	4	22		0.6	<3

## Page 4 of 8

ELEMENT	Bi	i	V		Ca	P	La	Cr	Mg	Ba	Ti	В			Na	K	W	Sample
SAMPLES	PF	pm	ppm		%	%	ppm	ppm	%	ppm	%	ppm	q	%	%	%	ppm	kg
2014	57 <	3		16	21.39	0.024	6				<.01		5	0.26	0.0			3.4
2014	58 <	3		8	28.52	0.011	5				<.01		5	0.07	0.0			3.78
2014	59 <	3		15	26.73	0.018	7	16	2.03		<.01		7	0.31	0.0			4.33
STANDARD D	57	6		85	0.96	0.076	13	166			= -		37	1.01	0.0		the second second second	4 -
G-1		3		31	0.46	0.07	6	6	0.55		= -	11 <3		0.87	0.0			-
2014	60 <	3	[	9	24.7		-				<.01		13	0.1	0.0	-		3.94
2014	61 <	3		10	24.07	0.012	6	21	2.97				6	0.08	0.0			4.92
2014	62 <3	3		6	21.23	0.008	4	12	0.72		<.01		3	0.05	0.0			4.96
2014	63 <	3		9	24.65	0.012	5	13		the second second second	<.01		9	0.08	0.0			3.82
2014	64 <	3	[	6	30.63	0.015	5	12			<.01		4	0.06	0.0		3 <2	3.96
2014	<b>165</b> <3	3		11	24.79	0.012	4	15	0.22	23	<.01		3	0.07	0.0		1 <2	4.46
2014	<b>166</b> < 3	3		10	29.03	0.019	6	13	0.22		<.01		3	0.08	0.0			4.42
2014	67 <	3	1	7	26.19	0.021	4	10	0.21	8	<.01	<3		0.06	0.0			4.03
2014	I68 <	3		10	26.69	0.042	6	13	1.44	29	<.01		4	0.13	0.0	1 0.07	7 <2	3.55
2014	69	3		14	28.56	0.031	5	11	2.59	10	<.01		4	0.08	0.0		4 <2	5.37
2014	70 <	3	t	11	26.32	0.037	5	12	1.94	12	<.01		3	0.13	0.0		7 <2	5.32
2014	71 <	3		14	29.47	0.027	6	11	1.47	8	<.01	<3		0.11	0.0		5 <2	4.9
2014	72 <	3		11	29.92	0.021	6			14	<.01		3	0.11	0.0		5 <2	5.13
2014	173 <	3		14	25.46	0.033	6	12	0.36	10	<.01	\$3		0.13	0.0		5 <2	5.82
2014	174 <	3		13	26.19	0.023	5	12	0.21	8	<.01		3	0.1	0.0		4 <2	5.39
2014	¥75 <	3	1	13	28.3	0.036	6	13	0.22	7	<.01		3	0.13	0.0		/ <2	5.01
2014	176 <	3		10	23.51	0.023	5	13	0.22	9	<.01	<3		0.11	0.0		5 <2	4.21
2014	177	3		9	29.67	0.016	6	13	0.23	13	<.01		7	0.11	0.0		5 <2	4.35
2014	178 <	3	1	16	7.37	0.041	10	17	0.12	53	0.	02	3	0.86	0.0		5 <2	6.79
2014	179 <	3		10	32.78	0.032	6	12	0.24	8	<.01		11	0.14	0.0		7 <2	4.47
2014	180 <	3	f	20	20.07	0.043	14	19	0.29	46	0.	01	4	0.66	0.0		€<2	6.54
2014	181 <	3		11	31.74	0.036	6	13	0.32	28	<.01		3	0.16	0.0		) <2	4.09
2014	182 <	3		27	29.21	0.026	6	16	1.53	35	<.01		6	0.35	0.0		3 <2	4.46
2014	483 <	3	ļ	8	35.08	0.02	5	10	0.27	1470	<.01		8	0.13	0.0		7 <2	4.64
2014	184 <	3	1	8	29.66	0.023	6	13	0.24	305	<.01		3	0.1	0.0		5 <2	4.06
2014	<b>185</b> <	3	• • • • • • • • • • • • • • • • • • • •	10	26.86	0.043	6	10	0.35	3012	<.01		11	0.18	Ū.0		1 <2	6.82
	186 <			9	30.5	0.053	6			460	<.01		6	0.17	0.0		3 <2	6.33
201	187 <	3		11	34.35	0.027	5	15	0.36	297	<.01		5	0.22	0.0		1 <2	4.33
201-	188 <	ġ	1	11	36.34	0.012	2 4	9	0.24	13	<.01	<3		0.09	0.0		5 <2	5.8
	189 <		<u>+</u>	12	i		4	9	0.28	28	<.01	<3		0.09	0.0	1 0.0	5 <2	4.98

## Page 5 of 8

ELEMENT	Mo		Cu	Рb	Zn	Ag		Ni	Co	Mn		Fe	As	Į	J	Au	Th		Sr	Cd		Sb
SAMPLES	ppm	6	ppm	ppm	ppm	ppm		ppm	ppm	ррп	1	%	ppm	F	pm	ppm	ррт		ppm	ррт		ppm
201351		1	17	<3		11 <.3		2	<1		223	0.14	ł	5 <	<8	<2	<2		155	<.5		<3
RE 201351		1	17	5		11 <.3		2	<1		223	0.14	+	5 <	<8	<2	<2		160			<3
201352	1	2	23	5		28 <.3		3		1	262	0.4	2	9 <	<8	<2	2			<.5		<3
201353		3	46	12		62 <.3		8		6	408	2.4		12 <		<2		3	22		0.5	<3
STANDARD DS7		19	99	62		396	1.1	52		9	631	2.3		46 -		<2		5	76		6.2	1
G-1	<1		1	10		43 <.3		3		3	531	1.8	5 <2		<8	<2		5		<.5		<3
201354		2	4	12		19 <.3		1	<1		210	0.3	9	2 -	<8	<2	2			<.5		<3
201355		3	41	15		60 <.3		8		6	247	2.4	ł	8 <		<2		3		<.5		<3
201356		1	4	6		17 <.3		1		1	155	1.94		-5 <		<2		3		<.5		<3
201357	<1		6	14		33 <.3		2		3	312	2.2	1	7 <		<2		4	43		0.5	
201358		1	5	10		51 <.3		2	<1		331	0.2	i	2 <		<2	2			<.5		<3
201359		2	2	12		25 <.3		1	<1		258	0.13	3	4		<2	2			<.5		<3
RE 201359	1	2	2	3		25 <.3		1	<1		259	0.1		3		<2	<2			<.5		<3
201360	1	2	4	7		36 <.3		1	<1		669	0.3		10		<2	<2			<.5		<3
201361	T	1	6	10		22 <.3		2		1	527	0.5	3	11	<8	<2	<2			<.5		<3
201362		2	10	13		37 <.3		2		2	298	1.9	-1	28 -		<2		3		<.5		<3
201363		1	4	12	:]	35 <.3		1	<1		394	0.2	7	8 -	<8	<2	<2		137			<3
201364		2	11			70 <.3		1	<1		708	0.6		18 -		<2	2		99	L	0.5	
201365		1	22	15		29 <.3		3		3	472	2.3		55 -	_	<2	2		29		0.5	
201366	<1	T	16	17		75	0.6	2		3	228	2.3		58	<8	<2		2	14		0.5	
201368		1	10	3	1	13 <.3		2	<1		235	0.2		3		8 <2	2			<.5		<3
201369		4	21	10		29 <.3		2		1	329			5		<2	2			<.5		<3
201370		5	72			83 <.3		12		6	696		in the second second	22		<2		4	29		0.7	<3
201371		4	7	8		27 <.3		1		1	230			3		<2	<2		69		0.6	
201372		1	13	15		39 <.3		4		3	395			9 -		<2		3		<.5		
201373		1	4	8	i	17 <.3		1	]	1	115			43		<2		3		<.5		<3
201374	<1		7	12		34 <.3		2		2	291	2.2		6		<2		4		<.5		<3
201375	iT	1	12	8		22 <.3		1		1	212			2		<2	<2			<.5		<3
201376		1	5	4		14 <.3		1	<1		199		<2		<8	<2	<2			<.5		<3
201377		2	2	10		21 <.3		1	<1		237	0.0		4		<2	<2			<.5		<3
201378		1	1	4		28 <.3		<1	<1		421	0.1		8		<2	2			<.5		<3
201379		3	18	18		37 <.3		2		2	541	1.4		30		<2	2		75		0.7	
201380		2	20	217	1	279	0.3	2		1	586	0.7		20		<2	<2		99		2.3	
201381		2	11		)	100 <.3		1		1	583	0.5		22		<2	<2		94		0.7	
201383		2	13	19	)	34	0.3	2		1	661	0.7	7	24	<8	<2	<2		89	<.5	1	<3

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ELEMENT	Bi	V		Ca	Р	La	Cr	Mg	Ba	Ti	В		Na	K	W	Samp	ple
SAMPLES	ppm	ppr	TI	%	%	ppm	ppm	%	ррт	%	ppm	%	%	%	ррт	kg	
201351		1	11	21.32	0.003	3	1	11.93	9	<.01	<3	0.07	0.02	0.01	<2		13.62
RE 201351	<3		10	21.22	0.003	3	1	11.83	9	<.01	4	0.07	0.02			-	
201352	<3		9	18.3	0.009	5	3	11.3	13	<.01	<3	0.35	0.02	0.04	<2		7.32
201353	<3		40	0.94	0.059	17	11	1.83	53	0.06	3	2.3	0.02				8.15
STANDARD DS7		6	78	0.94	0.074	13	167	1.06	382	0.13	37	1.02	0.08			3 -	
G-1		3	34	0.59	0.068	9	7	0.57	207	0.13	<3	1.07	0.11	0.51	<2	-	
201354	<3		6	16.97	0.008	5	1	11.18	9	0.01	4		0.02				15.03
201355	<3	1.	39	0.37	0.068	18	11	0.87	63	0.06	4	2.25	0.04			2	8.48
201356	<3		28	0.74	0.042	26	2	2.21	78	0.05			0.06				12.67
201357	<3	1	31	0.46	0.049	23	3	0.97	102	0.06			0.07	0.19			6.56
201358	<3		5	24.73	0.005	3	1	8.14	12				0.01	0.01			9.32
201359	<3		4	20.61	0.003	2	1	11.62		<.01	7	= · · ·	0.02				11.54
RE 201359	<3		- 4	20.67	0.003	2	1	11.05		<.01	3		0.02			•	
201360	<3	1	5	19.03	0.005	3	1	11.27	the second se	<.01	<3	0.15	0.02				9.57
201361	<3		8		0.011	7	1	9.63		<.01	9		0.02		-	_	5.51
201362	<3		14	1.49	0.031	19	3			<.01	7	2.5	0.01	0.3		2	4.95
201363	<3		14		0.002	2	1	11.87	1	<.01	<3	0.04	0.02				12.42
201364	<3	1	9	18.85	0.005	4	1	10.98	14	<.01	<3	0.18	0.02				7.44
201365	<3		15	2.75	0.051	22	3			<.01	<3	1.75	0.02				5.71
201366	<3		11	0.51	0.058	22	2	0.77		<.01	<3	1.45	0.02				12.28
201368	<3	1	8	18.77	0.005	4	1	11.07	43		<3	0.17	0.01	0.03			16.02
201369	<3		10	18.08	0.01	6	2	10.84		<.01	<3	0.36	0.01	0.03			9.81
201370	<3		45	1.17	0.048		14	1.53			2 3		0.01	0.13			4.87
201371	<3		10		0.017	8	1	10.71			2 3		0.01				9.79
201372	<3		29		0.047	24	5		51	0.04	lj 5		0.01				10
201373		3	29	0.28	0.043			2.4	150	0.03						2	16.18
201374	<3	!	31	0.56	0.048	25	3	2.32	125	0.06	5 5	2.08	0.03		_		8.56
201375	<3		4	21.14	0.003	2	1	10.43	8	<.01	14		0.01				9.18
201376	<3		3		0.003	2	1	11.57	5	<.01	5	0.07	0.01	0.01			7.17
201377	<3		3	20.8	0.001	2	1	11.5	3	<.01	<3	0.04	0.02	<.01	<2		10.32
201378	<3		3	19.99	0.002	2		11.79		<.01	<3	0.04	0.02				8.82
201379	<3		11	11.64	0.02	11	2	7.32		<.01	<3	0.58	0.01				15.21
201380	<3	-	13	16.46	0.007	5		10.02	17	<.01	5	0.32	0.02				13.86
201381	<3		7	18.71	0.004	3	1	10.89		<.01	8						9.33
201383		-+	9	17.48	0.006	5	2			<.01	7	0.22	0.02	0.03	<2		10.33

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Real Real Contraction Contract

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	Мо	Cu	P	0	Zn	Ag	Ni	Cc	)	Mn	F	e	As	U		Au	Th	Sr		d	Sb
SAMPLES	ppm	ppm	P		ppm	ppm	pp			ppm	%	1	ppm	ppm	וו	ppm	ppm	ppm	PF	m	ррт
201384		1	13	20	1	40	0.6	2	3	48	35	2.42	7:	3	10	<2		2	27	0.6	
STANDARD DS7	20	0	97	67		406	1.8	52	9	62		2.38	4	6 <8		<2		4	71	6.6	

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ELEMENT	Bi	V	Ċa	P	La	Cr	Mg	Ba	Ti	В	Al	Na	K	W	Sample
SAMPLES	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	kg
201384	<3	18	2.52	0.054	22	3	2.19	41	<.01	<3	1.45		0.12	<2	9.11
STANDARD DS7	5	78	0.92	0.076	13	157	1.05				0.99	0.08	0.44	5	•

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From ACME	ANALYTICAL LABO	RATORIES LTD. 85	2 E. HASTINGS	ST. VANCOL	JVER BC V6A	1R6 PHONE	604)253-3158 FAX	(604)253-1716 @	CSV TEXT F	ORMAT
To Eastfield F	Resources Ltd. PRO.	JECT Crowsnest	-							
Acme file # A	603953 Page 1 Re	ceived: JUL 20 2006	• 101 samples	s in this disk fil	e.					
Analysis: GR	OUP 3B - FIRE GEO	CHEM AU - 30 GM	SAMPLE FUSIC	N, DORE DIS	SOLVED IN A	QUA - REGIA,	ICP ANALYSIS. U	PPER LIMITS =	10 PPM.	
HIG	H GRADE GOLD AS	SSAY RECOMMEND	ED FOR 30 GM	ANALYSIS >	10ppm and 50	GM > 5ppm.				
ELEMENT	Au**									
SAMPLES	ppb									
G-1	2									
173001	2									
173002	1									
173003			1							
173004										
173005										
173006										
173007										
173008					1 					
173009			- +	L	i					
173010										
173011										
173012										
173013				ļ	ļ 					
RE 173013									~	
173014				 						
173015										
173016			 	i						
173017				·						
173018										
173019				·	··					
173020		I 		i						
173021				ļ						
173022				ļ	·		···· ····			
173023				 	└─────					
173024		· · · · · · · · · · · · · · · · · · ·	:							
201451			- <b>i</b>							
201452				 	ļi					
201453			_	<u> </u>	ļ į					
201454	7		<u> </u>							

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ELEMENT	Au**								 ·	
SAMPLES			÷							
201455	3									
201456	2								 	
201457	7								 	
201458									 	
201459										
STANDAR										
	<2									
201460										
201461									 	
201462	<2									
201463	4			· · · · · · · · · · · · · · · · · · ·						
201464	2									
201465	2									
201466	2		L	<u></u>						
201467	2		ļ 	l i						
201468			L							
201469									 	
201470			 						 	
201471			! +							
201472	2				•			i	 	į
201473	<2	·			· 					
201474										
201475							1	i		
201476			· · ··-	· 	•					
201477										
201478	3			 					 	ļ
201479	2		<u>.</u>	· · · · · · · · · · · · · · · · · · ·						Í
201480			·	·····	· · · · · · · · · · · · · · · · · · ·				 	
201481	3						<b></b>		 	
201482	3			ļ		i	L			
201483	4		L						 	ļ]
201484	2			: 					 · 	L
201485									 	
201486	<2		ļ					i	 ļ	ļ
201487	<2				•				 	L

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ELEMENT					 				
SAMPLES									
201488	2								i
201489	2								
201351	38				 				
RE 201351		·						 	
201352	26		i		 			i	
201353					 				
STANDAR					 				
G-1	<2				 				
201354									
201355					 			[ (	
201356									
201357	200				 		<u> </u>		
201358	41				 		,,,		
201359	15				 				
RE 201359							L		
201360	26								
201361	30								
201362	58			· · · · · · · · · · · · · · · · · · ·			1		
201363	19								
201364	29							 	
201365	94				 			: , •	
201366									
201368	22								
201369	27					l			
201370	61				 	•		•	
201371	140					<u>                                      </u>		•	
201372	52				 l		ļ	i	
201373	60								
201374					 	L		 	
201375					l L	· +	 	· +	
201376					 	• ···-	· •		
201377	13						L		
201378					 				
201379					 		l 	ļ	
201380	141					<u> </u>			

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ELEMENT		 [	1				
SAMPLES	ppb						
201381	62	 					
201383	45						
201384	163						
STANDAR	796						

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[]	From ACME	ANALYTIC	AL LABOR	ATORIES L	TD. 85	2 E. HASTINGS	ST. VAN	COUVER BC	V6A 1R6 P	HONE(604)	253-315	58 FAX(604)2	53-1716 @	CSV TEXT FO	ORMA	Т
	To Eastfield	Resources	Ltd. PROJE	CT Crowsn	est		-	]								
						* 69 samples i										
						WITH 3 ML 2-2-2				*		~ ~ ~ ~ ~				
ELEMENT	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	
SAMPLES	ppm		ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	1
G-1	1	_			<.3	7		4 531	1.93		<8	<2			<.5	
173461	1	16			<.3		<1	215			<8	<2	<2		<.5	
173462	1	20			<.3	<1	<1	233			<8	<2	<2		<.5	
173463	1	1	<3		<.3		<1	222			<8	<2			<.5	
173464	1	11	3	-	<.3		<1	238			<8	<2	<2	-	<.5	
173465	2		10			2		1 565	+		<8	<2	<2		<.5	
173466	2					<1	<1	719			<8	<2	<2		<.5	
173467	1	22	7	27	<.3	<1	<1	508			<8	<2	<2		<.5	
173468	1		<3	44		1	<1	305			<8		2 <2		<.5	
173469	1	13	8	33		1	<1	260				<2		2 130		0.6
173470	1	7	7	-	-	1	<1	231			<8	<2	<2		<.5	
173471	1	4	6	27		1	<1	218			<8	<2	<2		<.5	
173472	2	30	11			3		1 523				<2	<2		<.5	
173473	1	11	<3		<.3	1	<1	341			<8	<2	<2		2 <.5	
173474	1	9	<3	_	<.3	1	<1	485				9 <2	<2		<.5	
173475	2	9	9		<.3	1	<1	640			<8	<2	<2		i <.5	
173476	1	10	<3	22	<.3	<1	<1	518	0.33	11	<8	<2	<2		3 <.5	
173551	<1	1	4	20	<.3	4		1 109			<8	<2	<2		′ <.5	
173552	<1	1	<3	14	<.3	3		1 106	0.23	<2	<8	<2	<2		3 <.5	
173553	1	2	<3	15	<.3	4		1 109			<8	<2	<2		<.5	
173554	<1	2	8	17	′ <.3	3	<1	139			<8	<2	<2		) <.5	
173555	<1	1	3	13	<.3	4	i	1 117				9 <2	<2		\$ <.5	
173556	<1	1	<3	11	<.3	4	<1	113	0.27	<2	<8	<2	<2		2 <.5	
173560	1	6	17	60	<.3	3		6 612	- · · · · · · · · · · · · · · · · · · ·		<8	<2			l <.5	
RE 173560	1	6	19	58	<.3	3		6 602			<8	<2			2 <.5	
173561	1	6	21	63	<.3	3		6 652	3.02	2	<8	<2		and the second sec	) <.5	
173562	1	5	19	67	′ <.3	3		6 659	3.06	<2	<8	<2			5 <.5	
173563	1	6	18	61	<.3	4		6 612			<8	<2			′ <.5	
173564	1	5	18	61	<.3	3		5 616	2.97	′ <2	<8	<2		6 74	l <.5	
173565	1	5	16	58	8 <.3	4		6 614	3.02	<2	<8	<2			3 <.5	
173566	<1	5	19	63	8 <.3	4		6 599	3.13	3	<8	<2			2 <.5	
173567		5	22	62	? <.3	3		6 648	2.95	<2		14 <2		6 76	s <.5	

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					~		-	+	<u> </u>						<u> </u>
ELEMENT	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	В	AI	Na	K	W
SAMPLES	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm
G-1		<3		5 0.5		8						1.12	0.11	+	1 -
173461	<3	<3		8 18.5		1		11.1		<.01	<3	0.02	0.01		
173462		<3		2 18.0				10.97		<.01	<3	0.01	0.01		
173463		<3	1	1 18.6			<1	11.75	1	<.01	<3	0.02	0.01		
173464	<3	<3	1	0 18.10		2	-	11.4		<.01	<3	0.04			
173465		<3	2			4		3 7.29	1	<.01	<3	0.23			
173466		<3		3 19.7			<1	9.51			<3	0.04			
173467	<3	<3	1	1 20.9			<1	7.79		<.01	<3	0.03	-		
173468		<3		6 19.2			<1	11.23			<3	0.01	0.01		
173469	<3	<3	1	4 18.1			<1	10.73			<3	0.01	0.01		
173470	3	<3		2 18.2			<1 <sup>°</sup>	11.06		-	<3	0.02			
173471	4	<3		9 18.1			<1	11.12		<.01	<3	0.03			
173472	4			4 16.6		1		2 8.36	1	<.01	<3	0.34		1	
173473	3	<3	1	4 17.7			<1	7.92		<.01		6 0.04			
173474	3		3 1	1 18.19			<1	9.33		<.01	<3	0.04			
173475	<3	<3		7 17.			<1	10.67	}	<.01	<3	0.04			
173476	<3	<3	1	1 18.	9 0.002	2	<1	9.68		<.01	<3	0.03			
173551	<3	<3		5 25.	3 0.016			3 3.6		<.01	<3	0.13			
173552	<3	<3		5 23.8	6 0.013	3	3	3 3.84	5	<.01	<3	0.11	0.01		
173553	<3	<3		5 23.1	3 0.013			3 3.87		<.01	<3	0.1	0.01		
173554	3	<3	!	5 22.7	9 0.017	3	3 3	2 3.98	17	0.01	<3	0.12	-		
173555	<3	<3		5 25.0	2 0.014	3	3 ;	3 3.5	5 5	<.01		9 0.13			
173556	<3	<3		5 26.2	9 0.013	3	3 :	3 2.47	5	i <.01	<3	0.11	0.01		
173560	<3	<3	7	'8 1.3	7 0.109	27	· ·	9 0.58	58	0.15	5	5 1.47	0.05		
RE 173560		3 <3	7	6 1.3	7 0.105	27	7	3 0.56	58	0.14	1	0 1.42	0.05	1	
173561	3	1	3 8	1 1.2	6 0.107	27	7	8 0.59			<b>5</b> 10	0 1.53			
173562		i <3	8	2 1.1	5 0.114	27	7	8 0.57	85	i 0.16	5 !	9 1.5			
173563			3 8	3 1.1	2 0.114	28	3	9 0.58	60	0.15	5	5 1.5	0.04		
173564	_	<3	7	8 0.9	6 0.106	27	7	8 0.58	57	0.14		8 1.52	2 0.04		
173565		′ <3		6 0.8				8 0.62	2 50	0.14	l	4 1.65	0.04		
173566				4 0.8				0.61	66	6 0.15	5 .	4 1.6	6 0.04	1 0.07	7 <2
173567	4		· · · · · · · · · · · · · · · · ·	30 1.0	and the second s			B 0.54			-	5 1.45	5 0.04	1 0.07	7 <2

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<b>[</b>	
ELEMENT	Sample
SAMPLES	kg
G-1	-
173461	12
173462	9
173463	11
173464	8.5
173465	9.5
173466	8.5
173467	9.5
173468	6.5
173469	8
173470	9.5
173471	11
173472	6
173473	6
173474	5
173475	5.5
173476	5
173551	6.5
173552	8.5
173553	8.5
173554	9
173555	10
173556	· · · · · · · · · · · · · · · · · · ·
173560	7.5
RE 173560	
173561	6.5
173562	5.5
173563	6.5
173564	
173565	
173566	10.5

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ELEMENT	Мо	Cu	Pb	Zn	Ag	Ni	Со	Mn	Fe	As	U	Au	Th		Sr	Cd	
SAMPLES	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm		opm	ppm	
173568	1	5	1	63	<.3	3	6	622	3.01	2	<8	<2		5	77	<.5	
173569	1	6	1	3 62	<.3	4	6	666	3.07	2	<8	<2		6	79	<.5	
173570	1	6	2	2 58	<.3	3	6	618	2.95	<2	<8	<2		6	77	<.5	
STANDARE	21	94	6	3 375	1	50	8	600	2.27	47	<8	<2		4	67	_	6.2
G-1	<1	48	1	3 45	<.3	3	3	538	1.84	2	<8	<2		4	50	<.5	
173571	<1	16	2	3 68	<.3	4	6	570	3.13	4	<8	<2		5	69		0.8
173572	<1	12	2	) 64	<.3	4	6	568	3.19		<8	<2		5	64		0.7
173573	<1	12	2	4 72	<.3	4	6	586	3.28	3	<8	<2		6	66		0.8
173574	<1	7	1.	4 39	<.3	5	3	442	1.73	4	9	<2		3	115		0.5
173575	<1	5	1	2 13	<.3	4	1	250	0.56	<2	<8	<2	<2		176	<.5	
173576	<1	6	1	0 14	<.3	6	1	246	0.52	4	<8	<2	<2		181		
173577	<1	6	1	1 11	<.3	5	1	233	0.55	4	<8	<2	<2		189	<.5	
173578	<1	5	1	1 18	<.3	5	2		0.99	3	<8	<2	<2		192	<.5	
173579	<1	5		9 13	<.3	5	2	247	0.62	<2	<8	<2	<2		210		
173580	<1	5		9 35	<.3	4	1	321	0.39	4	<8	<2	<2		169	<.5	
173581	<1	6	1	1 20	<.3	2	1	273	0.65	2	<8	<2	<2		161	<.5	
RE 173581	<1	6		7 20	<.3	2	1	275	0.64	<2	<8	<2	<2		160	<.5	
173582	<1	6	1	6 52	<.3	4	5	564	2.76	4	<8	<2		4	68		0.6
173583	<1	8	1	9 58	<.3	4	6	619	2.98	3	<8	<2		5	61		0.6
173584	<1	4	1	6 29	<.3	2	2	443	1.49	3	<8	<2		2		<.5	
173585	<1	4		4 18	<.3	1	1	255	0.59	<2	<8	<2	<2		83	<.5	
173586	<1	3		3 13	<.3	1	<1	164	0.15	2	<8	<2	<2		94	<.5	
173587	<1	5		4 17	′ <.3	1	<1	191	0.2		<8	<2	<2			<.5	
173588	<1	5		4 16	.3	2	<1	174	0.19		<8	<2	<2		-	<.5	
173589	<1	4		6 15	i <.3	2	<1	173	0.15		<8	<2	<2				
201385	<1	7		3 9	<.3	1	<1	452	0.16		<8	<2	<2		117		
201386	<1	5	<3	18	3 <.3	1	<1	300	0.14			<2	<2			<.5	
201387	<1	2		9 15	.3	<1	<1	176	[		<8	<2	<2				
201388	<1	2			5 <.3	1	<1	204	0.1		<8	<2	<2			<.5	
201389	1	3	<3		′ <.3	1	<1	244	0.13		<8	<2	<2			<.5	
201390	3	12	1		3 <.3	1	1		0.53		<8	<2	<2			<.5	
201391	<1	3	<3		3 <.3	1	<1	472	0.17	_	<8	<2	<2				
201392	<1	3	-		) <.3		<1	335	0.12		<8	<2	<2				
201393	<1	2			5 <.3	1	<1	281	0.09		<8	<2	<2				
201394	2	7	1	7 37	′ <.3	<1	<1	339	0.14	4	<8	<2	<2		100	<.5	

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ELEMENT	Sb		Bi		V	Ca	P	La	Cr	Mg	Ba		В	Al	Na	K	W
SAMPLES	ppm		ppm	1	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm
173568		4		3	80	1.1	0.113	27	7	0.56		0.15	- 45				
173569	<3		<3		75	1.08	0.109	29	8	0.58	52	0.12	5	1.62	0.04		
173570		4	<3		76	1.78	0.104	26	8	0.58	71	0.14	6				
STANDAR		5		5	77	0.91	0.072	12	154		368	0.11	41	0.95			
G-1		3	<3		33	0.49	0.073	7	6		204	0.12	3				
173571	<3			5	86	1.04	0.116	28	8	0.58	81	0.16	8				
173572		4		3	86	0.96	0.12	28	7		71	0.15					
173573		4		3	89			29	9		89					1	
173574	<3			4	41	13.7	0.075	17	6		52		3		0.03		1
173575	<3			5	12	24.77	0.033	8		3.95	10		<3	0.32			
173576	<3			3	10	24.39	0.036	9		4.07	8		6				
173577		3	<3		9		0.028	8	<u> </u>	3.52	11	0.01		0.3			the second second second
173578	<3		<3		19		0.044	11					6				
173579	<3			4	14	26.13	1	9			12		6			-	<2
173580	<3			3	5	24.93		6				<.01	<3	0.18	1		
173581	<3			4	13	+		7			10		-	0.3			
RE 173581	<3		<3		13			7	£		10		<u> </u>	0.3	· ·		1
173582		3	<3		67		L	27				1		1.41			
173583	<3		<3		73	1.55	0.11	30									
173584	<3		<3		36	13.51	0.064	13			25	4	6				
173585	<3		<3		14	17.1	0.021	6						0.36			
173586	<3			3	3	20.59		3				<.01	<3	0.09			
173587	<3		<3		5	21.64	0.004	2				<.01					
173588	<3			4	3	23.81	0.008	2	<u></u>			<.01	<3	0.1	-		
173589	<3			5	2	21.19	0.008		1		1	<.01	Ś				
201385	<3		<3		6		0.002	2	1			<.01	<3	0.03			
201386	<3			4	3	19.75		2	11	11.67	1	<.01	<3	0.02			
201387	<3		<3		2	20.61	0.001	2		12.03		<.01	<3	0.04			
201388	<3		<3		2			2	1			<.01		5 0.04			
201389	<3		<3		3						· · · · · · · · · · · · · · · · · · ·	<.01	<3	0.07			
201390	<3		<3		7	17.7		5		10.31	· · · · · · · · · · · · · · · · · · ·	<.01	<3	0.34			
201391	<3		<3		9	19		2		12.44		<.01	<3	0.03			
201392	<3		<3		8	19.38	0.002	2	<1	12.19		<.01	<3	0.03			
201393	<3		<3		4	19.67	0.001	1	1			<.01	<3	0.02			
201394	<3			4	e	19.52	0.001	1	1	11.68	4	<.01	<3	0.03	0.01	0.01	<2

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ELEMENT     Sample       SAMPLES     kg       173568     7.5       173569     6.5       173570     5       STANDARI     -       G-1     -       173572     111       173573     8       173574     6.5       173575     7       173576     7       173576     7       173576     7       173576     7       173577     6.5       173578     4.5       173579     3       173580     6       173581     6       173582     6.5       173583     5       173584     3.5       173585     8.5       173586     9.5       173587     10.5       173588     7       173589     8       201385     12.6       201386     8.5       201389     8       201389     8       2013		Sample
173568     7.5       173569     6.5       173570     5       STANDARI -     -       G-1     -       173571     10       173572     11       173573     8       173574     6.5       173575     7       173576     7       173577     6.5       173578     4.5       173578     4.5       173578     4.5       173578     4.5       173578     6.5       173579     3       173580     6       173581     6       RE 173581     6       RE 173583     5       173583     5       173584     3.5       173585     8.5       173586     9.5       173587     10.5       173588     7       173589     8       201385     12.6       201386     11       201388     8.5       <	SAMPLES	ko
173569     6.5       173570     5       STANDARI     -       G-1     -       173571     10       173572     11       173573     8       173574     6.5       173575     7       173576     7       173577     6.5       173578     4.5       173579     3       173580     6       173581     6       173582     6.5       173583     5       173584     3.5       173585     8.5       173586     9.5       173587     10.5       173588     7       173589     8       201385     12.6       201386     11       201387     11       201388     8.5       201389     8       201390     8.6       201391     11       201392     12       201393     8.9		
173570   5     STANDARI   -     G-1   -     173571   10     173572   11     173573   8     173574   6.5     173575   7     173576   7     173577   6.5     173578   4.5     173578   4.5     173578   4.5     173579   3     173580   6     173581   6     173583   5     173584   3.5     173585   8.5     173586   9.5     173587   10.5     173588   7     173589   8     201385   12.6     201386   11     201387   11     201388   8.5     201389   8     201390   8.6     201391   11     201392   12     201393   8.9		
STANDAR   -     G-1   -     173571   10     173572   11     173573   8     173574   6.5     173575   7     173576   7     173577   6.5     173578   4.5     173579   3     173580   6     173581   6     173583   5     173584   3.5     173585   8.5     173586   9.5     173587   10.5     173588   7     173589   8     201385   12.6     201386   11     201387   11     201388   8.5     201390   8.6     201391   11     201392   12     201393   8.9		
G-1     -       173571     10       173572     11       173573     8       173574     6.5       173575     7       173576     7       173577     6.5       173578     4.5       173579     3       173580     6       173581     6       173583     5       173584     3.5       173585     8.5       173586     9.5       173587     10.5       173588     7       173589     8       201385     12.6       201386     11       201387     11       201388     8.5       201390     8.6       201391     11       201392     12       201393     8.9		
173571   10     173572   11     173573   8     173573   8     173574   6.5     173575   7     173576   7     173577   6.5     173578   4.5     173579   3     173580   6     173581   6     173583   5     173584   3.5     173585   8.5     173586   9.5     173587   10.5     173588   7     173589   8     201385   12.6     201386   11     201387   11     201388   8.5     201390   8.6     201391   11     201392   12     201393   8.9		· · ·
173572     11       173573     8       173574     6.5       173575     7       173576     7       173577     6.5       173578     4.5       173579     3       173580     6       173581     6       173582     6.5       173583     5       173584     3.5       173585     8.5       173586     9.5       173587     10.5       173588     7       173589     8       201385     12.6       201386     11       201388     8.5       201389     8       201390     8.6       201391     11       201392     12       201393     8.9		- 10
173573   8     173574   6.5     173575   7     173576   7     173577   6.5     173578   4.5     173579   3     173580   6     173581   6     173582   6.5     173583   5     173584   3.5     173585   8.5     173586   9.5     173587   10.5     173588   7     173589   8     201385   12.6     201386   11     201387   11     201388   8.5     201390   8.6     201391   11     201392   12     201393   8.9		
173574     6.5       173575     7       173576     7       173577     6.5       173578     4.5       173578     4.5       173578     4.5       173579     3       173580     6       173581     6       173582     6.5       173583     5       173583     5       173584     3.5       173585     8.5       173586     9.5       173587     10.5       173588     7       173589     8       201385     12.6       201386     11       201387     11       201388     8.5       201390     8.6       201391     11       201392     12       201393     8.9		
173575     7       173576     7       173576     7       173577     6.5       173578     4.5       173579     3       173580     6       173581     6       173582     6.5       173583     5       173584     3.5       173585     8.5       173586     9.5       173588     7       173589     8       201385     12.6       201386     11       201387     11       201388     8.5       201389     8       201390     8.6       201391     11       201392     12       201393     8.9		
173576     7       173577     6.5       173578     4.5       173579     3       173580     6       173581     6       173581     6       173582     6.5       173583     5       173584     3.5       173585     8.5       173586     9.5       173587     10.5       173588     7       173589     8       201385     12.6       201386     11       201387     11       201388     8.5       201390     8.6       201391     11       201392     12       201393     8.9		
173577     6.5       173578     4.5       173579     3       173580     6       173581     6       173581     6       173581     6       173581     6       173583     5       173583     5       173584     3.5       173585     8.5       173586     9.5       173587     10.5       173588     7       173589     8       201385     12.6       201386     11       201387     11       201388     8.5       201389     8       201390     8.6       201391     11       201392     12       201393     8.9		
173578     4.5       173579     3       173580     6       173581     6       173581     6       173581     6       173581     6       173581     6       173582     6.5       173583     5       173584     3.5       173585     8.5       173586     9.5       173587     10.5       173588     7       173589     8       201385     12.6       201386     11       201387     11       201388     8.5       201389     8       201390     8.6       201391     11       201392     12       201393     8.9		
173579   3     173580   6     173581   6     173581   6     RE 173581   -     173582   6.5     173583   5     173584   3.5     173585   8.5     173586   9.5     173587   10.5     173588   7     173589   8     201385   12.6     201386   11     201388   8.5     201389   8     201390   8.6     201391   11     201392   12     201393   8.9		
173580   6     173581   6     RE 173581   -     173582   6.5     173583   5     173584   3.5     173585   8.5     173586   9.5     173587   10.5     173588   7     173589   8     201385   12.6     201386   11     201388   8.5     201389   8     201390   8.6     201391   11     201392   12     201393   8.9		
173581   6     RE 173581   -     173582   6.5     173583   5     173584   3.5     173585   8.5     173586   9.5     173587   10.5     173588   7     173589   8     201385   12.6     201386   11     201388   8.5     201389   8     201390   8.6     201391   11     201392   12     201393   8.9		
RE 173581 -       173582     6.5       173583     5       173584     3.5       173585     8.5       173586     9.5       173587     10.5       173588     7       173589     8       201385     12.6       201386     11       201387     11       201388     8.5       201390     8.6       201391     11       201392     12       201393     8.9		
173582     6.5       173583     5       173584     3.5       173585     8.5       173586     9.5       173587     10.5       173588     7       173589     8       201385     12.6       201386     11       201387     11       201388     8.5       201390     8.6       201391     11       201392     12       201393     8.9		
173583   5     173584   3.5     173585   8.5     173586   9.5     173587   10.5     173588   7     173589   8     201385   12.6     201386   11     201387   11     201388   8.5     201390   8.6     201391   11     201392   12     201393   8.9		
173584   3.5     173585   8.5     173586   9.5     173587   10.5     173588   7     173589   8     201385   12.6     201385   12.6     201386   11     201387   11     201388   8.5     201389   8     201390   8.6     201391   11     201392   12     201393   8.9		
173585     8.5       173586     9.5       173587     10.5       173588     7       173589     8       201385     12.6       201385     12.6       201386     11       201387     11       201388     8.5       201389     8       201390     8.6       201391     11       201392     12       201393     8.9		
1735869.517358710.51735887173589820138512.620138611201387112013888.520138982013908.620139111201392122013938.9		
173587     10.5       173588     7       173589     8       201385     12.6       201386     11       201387     11       201388     8.5       201389     8       201390     8.6       201391     11       201392     12       201393     8.9		
173588     7       173589     8       201385     12.6       201386     11       201387     11       201388     8.5       201389     8       201390     8.6       201391     11       201392     12       201393     8.9		
173589     8       201385     12.6       201386     11       201387     11       201388     8.5       201389     8       201390     8.6       201391     11       201392     12       201393     8.9		10.5
201385     12.6       201386     11       201387     11       201388     8.5       201389     8       201390     8.6       201391     11       201392     12       201393     8.9		7
201386     11       201387     11       201388     8.5       201389     8       201390     8.6       201391     11       201392     12       201393     8.9	173589	8
201387     11       201388     8.5       201389     8       201390     8.6       201391     11       201392     12       201393     8.9	201385	12.6
201388     8.5       201389     8       201390     8.6       201391     11       201392     12       201393     8.9	201386	11
201389     8       201390     8.6       201391     11       201392     12       201393     8.9	201387	
201390     8.6       201391     11       201392     12       201393     8.9	201388	8.5
201391 11 201392 12 201393 8.9	201389	8
201392 12 201393 8.9	201390	8.6
201393 8.9	201391	11
201393 8.9	201392	12
201394 7	201393	8.9
	201394	7

Page	7	of	9	
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ELEMENT	Mo		Cu	Pt	<b>)</b>	Zn		Ag	Ni	Co	Mn		Fe	As	U	Au	Th	Sr	Cd	
SAMPLES	ppm		ppm	pp	m	ppm		ppm	ppm	ppm	ppn	1	%	ppm	ppm	ppm	ppm	ppm	pp	m
201395		2	2	1	6		30	<.3	1	<1		265	0.32	2	<8	<2	<2	9	3 <.5	5
201396	<1		2	<3	3		24	<.3	1	<1		218	0.07	<2	<8	<2	<2	8	9 <.5	5
201397		1	3	<3	3		20	<.3	1	<1		224	0.16	5	<8	<2	<2	8	4 <.5	5
STANDAR	1	19	98	1	69	4	01	0.9	48		8	615	2.35	48	<8	<2		3 7	1	6.

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ELEMENT	Sb	Bi	V	1	Ca	Ρ	La	Cr	Mg	Ba	Ti	В	AI	Na	K	W
SAMPLES	ppm	ppm	p	pm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm
201395	<3	<3		4	19.28	0.002	2	1	11.75	3	<.01	4	0.03	0.01	0.01	<2
201396	<3		3	2	20.05	0.001	1	1	11.54	3	<.01	3	0.03	0.01	0.01	<2
201397	<3	<3	-	2	21.16	0.003	2	1	11.36	4	<.01	<3	0.07	0.01	0.01	<2
STANDAR	İ	7	5	76	0.92	0.073	12	157	1.04	376	0.12	38	0.98	0.08	0.44	

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ELEMENT	Sample
SAMPLES	kg
201395	10.5
201396	9.5
201397	6.5
STANDAR	-

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From ACME	ANALYTICAL I	ABORATORI	ES LTD. 852	E. HASTINGS	ST. VANCOU	IVER BC V6A	1R6 PHONE	604)253-3158	FAX(604)253	1716 @ CSV	TEXT FORMA	T
To Eastfield F	Resources Ltd.	PROJECT Cro	owsnest									
Acme file # A	604109 Page 1	Received: J	IUL 21 2006 *	69 samples	in this disk file	).			-			
Analysis: GR	OUP 3B - FIRE	GEOCHEM A	U - 30 GM SA	MPLE FUSIO	N, DORE DIS	SOLVED IN A	QUA - REGIA,	ICP ANALYS	IS. UPPER LI	VITS = 10 PPI	vi.	
	H GRADE GOL	D ASSAY RE	COMMENDE	D FOR 30 GM	ANALYSIS >	10ppm and 50	) GM > 5ppm.					
ELEMENT												
SAMPLES	ppb											
G-1	<2				]							
173461	7											
173462	22											
173463	18											
173464												
173465	107											
173466	172											
173467	83											
173468		·······										
173469	15											
173470	12	-										
173471												
173472	77											
173473	47											
173474	86											
173475	133											
173476	62											
173551	4				·····							
173552	4					<b>.</b>						
173553	4											
173554	7											
173555	4					Ţ						
173556	2					ī						
173560	5					, I						
RE 173560								i				
173561		4										
173562		+				1			L			
173563			· · · · ·			1						
173564						†						
173565						<u> </u>						
173566						 				<u>}</u>		
L				L		<u> </u>						

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and the second terms to a second terms

ELEMENT	Au**	11	····							1	
SAMPLES	nob							· · · · · · · · · · · · · · · · · · ·			
173567	<2		-						-	·····	
173568											
173569											
173570		+								<u> </u>	
STANDAR		++									
	<2										· · ·
173571	3										
173572	2	-++					<u></u>				
173573		-++		· ·							
173574	5										
173575			!							· · ·	
173576											· · ·-
173577	3								1		·,
173578	4										
173579	•			· ·							
173580		- <b>+</b> <u>+</u>								<u> </u>	· · · · · ·
173581	4								· · · · · ·		
RE 173581								<b>_</b>	· -		
173582	5	-+								<u> </u>	
173583				•••••	····						
173584	3					L		r			
173585	4							<b>\</b>		ļ	
173586	· · ·							· ··	<b>--</b>		t
173587	4						<b>.</b>				
173588		+									
173589									<u> </u>		
201385							• ·				
201386											
201387	2										
201388								-	··· · ·	1	
201389					······	·	<b>⊢</b> .	+	+		
201390							L ····	•	t	<u> </u>	
201391	27						- • · · · · ·		<u>├</u>	 1	
201392		<u> </u>									
201393	5						·	<u>}</u>			
	· · · · · · · · · · · · · · · · · · ·							L	l	L	

Page	3	of	3	
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and the second 
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ELEMENT	Au**						
ELEMENT SAMPLES 201394	ppb						
201394	4						
201395	2					_	
201396	3						
201397 STANDAR	5						
STANDAR	794						

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	From ACME	ANALYTICAL	LABORATORI	ES LTD. 852	E. HASTING	S ST. VA	NCOUV	ER BC V6A	1R6 PHONE	604)253-3158	FAX(604)253-	1716 @ CSV TE	
			PROJECT Cro										
				2006 * 30 s									
												IL, ANALYSED E	
ELEMENT		Cu	Pb	Zn	Ag	Ni	. (	Co	Mn		As	U	Au
SAMPLES		ppm	ppm	ppm	ppm	ppm		ppm	ppm	%	ppm	ppm	ppm
G-1	<1	<1	5		<.3	<1		4	551	1.98		<8	<2
173401	2		6		<.3	<1		1	842	1.03		<8	<2
173402	1	59			<.3		7	6	642	2.41		<8	<2
173403	<1	65			<.3		3	6	485	2.42		<8	<2
173404	2	48	<3		<.3	<1		4	488	4.35		<8	<2
173405	1	+	<3		<.3	<1		5		2.77		<8	<2
173406	3	21	9		<.3	<1		6	961	3.7		<8	<2
173407	1	9	7	• •			1	<1	375	0.2	10	<8	<2
RE 173407	1	8			<.3			<1	374	0.2		<8	<2
173408	3	15	6			<1	•	<1	567	0.65		<8	<2
173409	3	24	8	35	<.3	<1		<1	774	0.75	22	<8	<2
173410	1	18	<3		<.3		2	<1	463	0.39		<8	<2
173411	1	8	6	22	<.3		3	2	421	0.61	12	<8	<2
173412	1	8	3	50	<.3		1	<1	549	0.68	8	<8	<2
173413	10	156	31	57	<.3		4	1	820	20.15	73	<8	2
173414	2	22	15	92	<.3		6	9	785	4.14	11	<8	<2
173415	10	52	25	23	<.3		5	<1	968	23.13	39	<8	<2
173416	6	28	9	21	<.3	<1		<1	726	1.64	28	<8	<2
173417	2	14	6	35	<.3	<1		<1	581	0.72	19	<8	<2
173418	2	4	6	7	<.3	<1		<1	576	0.38	11	<8	<2
173419	1	18	11	80	<.3		8	8	488	3.05	14	<8	<2
173451	<1	8	16	39	<.3		10	2	373	0.91	10	<8	<2
173452	1	7	15	35	<.3	i	2	<1	332	0.82	8	<8	<2
173453	1	7	10	26	<.3		7 -	<1	293	0.62	5	<8	<2
173454	1	7	4	30	<.3		8	2	309	0.69	11	<8	<2
173455	1	5	15	28	<.3		5	3	274	0.58	6	<8	<2
173456	1	6	3	24	<.3	<1		2	268	0.49	4	<8	<2
173457	<1	3	15	69	<.3	<1	+	6	584	2.86	3	<8	<2
173458	1	5	12	64	<.3		4	6	587	2.82	6	<8	<2
173459	1	6	17	71	<.3		4	6	652	3.06	<2	<8	<2
STANDAR	19	101	68	410	0	.8	54	9	627	2.38	50	<8	<2

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	<b>_</b>																	
ELEMENT		Sr		Cd		Sb		Bi		V	C		Р		La	Cr	Mg	Ba
SAMPLES	ppm	ppm		ppm		ppm		ppm		ppm	%		%		ppm	ppm	%	ppm
G-1		3	66		0.7	<3		<3			38	0.58	· · · · · · · · · · · · · · · · · · ·	076	7	-		
173401		2	114		0.7		7		4		0	20.99		019	8			
173402			47		0.9			<3			26	2.25		065	32			
173403				<.5		<3		<3			30	0.35		.067	25			
173404				<.5		<3		<3			5	1.29		.044	42	L .		
173405	<2		27		0.7			<3			21	0.39		.062	26			
173406		2	33		0.6	<3		<3		1	9	1.82		.048	24			
173407				<.5				<3			5	22.7	1	.004	2			
RE 173407		:		<.5			6	<3			5	22.43	1	.003	1			
173408				<.5		<3			3		0	21.07		.007	2			
173409	<2		254		0.5	<3		<3			17	24.29		.003		<1	10.81	
173410	<2		432	<.5	j			<3			<b>14</b>	26.17		.004		<1	7.3	
173411		2	221		0.5		6	<3		1	0	30.04		.014	6			
173412	<2		210		0.7	<3			11	1	5	29.54		.006	3			
173413		4	25		1.5		4		3		20	1.92		.033	19			
173414		3	33	<.5		<3		<3		Ę	55	0.57		.055	13	10		
173415		3	4	<.5			3	<3			10	0.12	0.	.025	7			
173416	<2		192		0.7	<3			4		17	24.87	0	.005	2	1	6.81	
173417	<2		183		1		4		10	1	11	26.33	0	.002	1	<1	8.74	
173418		- •	143		0.5	<3		<3			3	25.67	0	.002	<1	<1	11.2	1
173419		4	35	<.5		<3		<3			56	1.08	0	.068	15	10		
173451		2	137		0.6	<3		<3		1	6	23.73	0	.046				
173452		2	146	<.5		,	3	<3			4	24.88	0	.044	10	5	6.46	
173453	<2	-	176	<.5		<3			5		12	26.74	0.	.035	10	6	5.22	
173454		· + · · ·	181			<3			5		12	26.45	0	.038	11	5	5.49	
173455		2	166		0.5		4		3		10	27.69	i (	0.03		5	5.58	
173456	<2		187	<.5			3		7		9	28.89		0.03		5	5.39	
173457		4		<.5		<3		<3			75	7.94		.105			0.77	
173458		4		<.5				<3			76	7.76		.103			0.9	
173459	·····	5		<.5				<3			31	3.47		.115	and the second states of the second states and			
STANDAR	 	5	68		5.7			<3			31	0.93		.076				1

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											Į.
ELEMENT			В		Al		Na		к	W	Sample
SAMPLES	%		ppm		%		%		%	ppm	kg
G-1		0.13		5		0.98		0.08	0.48		-
173401	<.01		<3			0.42	<.01		0.07	<2	4
173402	<.01			4		1.44		0.03	0.11		10
173403	<.01			7		1.67		0.02	0.15	2	7.5
173404	<.01			7		1.57		0.02	0.11	<2	13
173405	<.01		<3			1.74	<.01		0.16	<2	8
173406	<.01		,	5		1.72	<.01		0.14	<2	5
173407	<.01		<3			0.06		0.01	0.04	<2	5.6
RE 173407	<.01		<3			0.06	<.01		0.03	<2	-
173408	<.01		<3			0.19	<.01		0.01	<2	6.2
173409	<.01		<3		• ·	0.06	<.01		0.03	<2	6
173410	<.01		<3			0.1		0.03	0.06	<2	6.7
173411		0.01	<3			0.3	<.01		0.09	<2	2.5
173412	<.01		<3			0.16		0.02	0.05		6.5
173413	<.01			16		1.04		0.02	0.08	<2	4.5
173414		0.01		5	•	2.59		0.05	0.05	<2	5
173415	<.01			9		0.35	<.01		0.05	<2	4.5
173416	<.01		<3			0.14	<.01		0.01	<2	7
173417	<.01		<3			0.04	<.01		0.01	<2	7
173418	<.01			5	†	0.02		0.06	0.01	<2	5.5
173419		0.01	+ · ·	5		2.56	<.01		0.06	3	5
173451		0.01	1	5		0.54	<.01		0.06	<2	13.5
173452		0.01		5 3		0.48		0.01	0.1	<2	14.5
173453		0.01	-		1	0.41		0.02	0.07	<2	12.5
173454		0.01		4	†	0.43		0.02	0.11	<2	12
173455		0.01		3		0.41		0.03	0.07	<2	11
173456	<.01			3		0.31	• 	0.01	0.09	<2	12
173457		0.13		8		1.3	<.01		0.1	2	5.5
173458		0.13		10		1.26		0.05	0.08		Ę
173459	+	0.14		7	+	1.49	ļ	0.04	+	•	4
STANDAR	J	0.12	<u> </u>	42		1	l	0.07			-

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				2 E. HASTING	S ST. VANCO	UVER BC V6/	1R6 PHONE	(604)253-3158	FAX(604)253	-1716 @ CSV	TEXT FORM	NT
		PROJECT Cr										
		ceived: JUL 21										
						SSOLVED IN A		ICP ANALYS	IS. UPPER LI	MITS = 10 PP	М.	
		DLD ASSAY RE	COMMEND	ED FOR 30 GI	M ANALYSIS :	> 10ppm and 5	0 GM > 5ppm.			L		
ELEMENT												
SAMPLES	ppb				:			i				
G-1	<2	1.								1		
173401	44									1		
173402	973											·
173403	287									-		
173404	110				1					-		
173405	77					- [				<u>+</u>		
173406	91	<u> </u>										
173407	14									+·	-·	
RE 173407				· · · · · · · · · · · · · · · · · · ·		+			<u> </u>			
173408	64					1						
173409	98					1	····					
173410	48											
173411	62								<u> </u>			
173412	6					-					ļ	<b>-</b>
173412	425			-+							:	
173413	425				ļ,					i		
							<u> </u>	· · · ·		·		
173415	186				·····		· · · ·					
173416	162				·					1		
173417	88						<b>!</b>			ŧ		
173418	46											
173419	132				! 	4						
173451	7							I 		 		
173452	7	: •								i		
173453	7	·		·			<b>.</b>					
173454	7											
173455	8											
173456	286						1					
173457	ā								 i			; i
173458	<2	<b>-</b>			1	1				ļ	!	
173459	3	<u></u> <u></u> ↓ - · - · - · - · - · - · - · - · - · -		-†	1		]			1		
STANDAR				+ · ·	:		ļ		·	<u> </u>	· ·	[
	001	<u> </u>		i	:			i			l	

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	From ACME	ANALYTICAL	LABORATORI	ES LTD. 852 F	E. HASTINGS	ST. VANCO	UVER	BC V6A	1R6 PHONE(6	04)253-3158	FAX(604)253-	1716 @ CSV "	EXT FORMAT
		Resources Ltd.				Ì.				· · · · · · · · · · · · · · · · · · ·			
	Acme file # A	604234 Page	1 Received: J	UL 24 2006 *	50 samples	in this disk	ile.						
		OUP 1D - 0.50										T	
	Mo	Cu	Pb	Zn	Ag	Ni	Co			Fe	As	U	Au
SAMPLES	ppm	ppm	ppm	ppm	ppm	ppm	ppn	n	1-1-	%	ppm	ppm	ppm
<u>3-1</u>	<1	2	4		<.3		5	4	580	1.98	and the second second	<8	<2
173101		1 21	<3	27	<.3		1 <1		206	0.12		<8	<2
173102		1 14	3		<.3		1 <1		195	0.17		<8	<2
173103			<3	32	<.3	<1	<1		276	0.24		<8	<2
173104		1 45	<3	14	0.4		1 <1		309	0.12		<8	<2
173105		2 31	<3	17	<.3		9	1	436	0.13		<8	<2
173106	<1	37	7	32	<.3	i	4	2	436	2.23		<8	<2
173107		1 13	<3	20	0.3		4	2	268	0.57		<8	<2
173108	<1	11	5	19	<.3		8	2	222	0.39		<8	<2
173109		2 58	22	86	0.4		23	7	656	2.71	11	<8	<2
173110		6 13	4	40	<.3		3 <1		250	0.61	8	<8	<2
173111		2 35	20	111	0.4		21	9	78 <del>9</del>	3.12	11	<8	<2
173112	· · · · · · · · · · · · · · · · · · ·	1 39	6	64	0.5		9	2	526	1.36	_	<8	<2
173113		1 11	14	89	0.3		11	8	681	3.03	8	<8	<2
173114		1 65	40	236	0.5		21	6	753	2.32	17	<8	<2
173115		1 12	14	108	<.3		15	6	731	3.15	6	<8	<2
173116	<b>**</b>	1 66	33	182	0.3	1	2 <1		410	1.09	6	<8	<2
173117		1 27	32	154	0.4		19	8	868	2.84	11	<8	<2
173118	<u> </u>	1 28	13	79	<.3	!	9	3	435	0.97	8	<8	<2
173119		15	<3	59	<.3	•	2 <1		345	0.4	6	<8	<2
173120		1 19	18	114	<.3		19	8	885	2.97	7	<8	<2
173121	++	1 14	16	91	<.3		12	7	767	2.69	10	<8	<2
173122	<b> </b>	1 13	19	95	<.3	1	11	7	752	3.13	5	<8	<2
173123	<u> </u>	1 41			0.6	5	11	10	765	2.85	6	<8	<2
173124		1 19	4	27	0.3		6 <1		219	0.15	3	<8	<2
RE 173124		18	3	22	0.4	<1		1	213	0.13	6	<8	<2
173125		2 46		· · · · · · · · · · · · · · · · · · ·	0.3	8	4 <1	· · ·	275	0.32	10	<8	<2
173126			<3	29	<.3	<1		2	243	0.46	16	<8	<2
173127	<b>++</b>		<3		<.3		4 <1		383	0.3	12	<8	<2
173128	↓↓	1 26		•		<1	<1		658	0.24	7	9	<2
173129		1 30		42			7	5	376	2.38	28	<8	<2
173130	1	13			.3	-	4	1	255	0.49		i <8	<2

Page 2 c	)† 6	
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ELEMENT		Sr	Cd	Sb	Bi	V		Ca	Р	La	Cr	Mg	Ba
SAMPLES	ppm	ppm	ppm	ppm	ppm	ррт		%	%	ppm	ppm	%	ppm
G-1	4		<.5	<3	<3		37	0.5		7			
173101		136		<3	<3		4	24		1	-		
173102	<2	108			5 <3		4	21.42			<1	12.81	·
173103	<2	162	0.5		3 <3		16	21.91	0.004		<1	11.82	
173104	2			7 <3		4	56	22.99			<1	12	
173105	<2	223	<.5	<3	<3		26	24.08	0.002		<1	11.9	
173106	<2	44	<.5	<3	<3		13	4.39	0.05	22		2.31	
173107	2	123	<.5	<3	<3		14	22.19	0.007	5			
173108	<2	93	<.5	<3	<3		11	19.97	0.005	3	-		
173109	4	32	0.8	3 <3	<3		54	1.45	0.072	41	22		
173110	<2	92	0.6	<b>პ &lt;</b> 3		7	10	20.72	0.007	3		12.73	
173111	6			5 (	5	4	59	0.56					
173112	<2	73	<.5	<3	<3		29	14.85	0.037	17	1		
173113	5	i 46	<.5	4	4 <3		67	2.49					
173114	3	62	1.5	5 <3		6	52	8.33	0.065				
173115	5	40	0.7	7 <3	<3	-	65	0.73	0.103	23	10	0.86	
173116	<2	121	0.9	9 <3	<3	-	17	18.6	0.019	5	3	11.26	
173117	4	59	1	<3	<3		55	4.02	0.097	28	10	2.61	
173118	<2	234	<.5	<3	<3		17	18.52	0.034	12			33
173119	<2	79	<.5	<3		6	8	20.29	0.013	3		12.88	
173120	3	27	1	<3	1	4	51	1.36	0.125	32	12	1.43	
173121	3	41	3.0	3 <3	<3	•	52	2.52	0.135			1.78	
173122	4	43	1.2	2 <3		6	61	1.05	0.109	32	10	1.08	3 58 3 72
173123	4	47	1.1	I <3	<3		61	3.65	0.114	29	13	4.36	5 72
173124	<2	181	<.5	<3	!	9	26	24.34	0.004	2	<1	11.78	3 7
RE 173124		176	1 ·····	<3		7	25	23.61	0.004	2	<1	11.4	
173125		171		<3		6	40	20.66				11.44	
173126		244		<3		6	20	24.24			<1	12.04	l e
173127			<.5	<3	<3	-	32	23.52			<1	12.14	4 8
173128			<.5	<3		7	16	22.24			<1	12.37	
173129	2			) <3	<3	·	14	1.68					
173130			<.5	<3		5	13	20.74					

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	<u>гі</u>		B		AI		Na		ĸ	w	Sample
SAMPLES 9			ppm		%		%		%	ppm	kg
G-1	/0	0.13	<3			0.96		0.07	0.47	<2	-
173101 -	<.01	••	~	6		0.06		0.03	0.03	<2	7.2
173102 <			<3			0.08		0.03		<2	7
173103 <			<3			0.05		0.05		<2	8.2
173104 <			<3		·	0.04		0.04		<2	6.5
173105 <	<.01			6	·	0.04		0.01	0.01	<2	5.5
173106 <				4		0.91		0.05	0.14	<2	7
173107		0.01		6		0.59		0.05	0.12	<2	7.5
173108		0.01		5		0.51		0.05	0.11	<2	7
173109		0.04		16		2.51	<.01		0.17	<2	6.5
173110		0.01	~3			0.44		0.05	0.09	<2	7.5
173111		0.04		8		2.28		0.07	0.14	<2	4.5
173112		0.03		10		1.06		0.1	0.1	<2	7
173113		0.08	<3			1.94		0.06	0.11	<2	10
173114		0.05		10		1.96		0.06	0.13	<2	6.5
173115		0.07	<3			2.25		0.07	0.14	2	7.5
173116		0.01		13		0.44		0.03	0.03	<2	5.5
173117		0.05		15		2.12		0.05	0.12	<2	10
173118		0.01		11		0.54		0.03	0.1	<2	7.5
173119		0.01		13		0.27		0.04	0.01		4
173120		0.03		3		2.06		0.06		<2	6.5
173121		0.05		4		1.67		0.05	0.09		6.5
173122		0.06		6		2.15		0.04	0.1	<2	7.5
173123		0.09		7		2.01		0.04	0.23	<2	3.5
173124 <			<3			0.09		0.02	0.03		3.5
RE 173124 <			<3			0.08		0.06	0.01	<2	-
173125 <			<3			0.17		0.02	0.01	<2	6
173126 <			<3			0.06		0.05	0.03		6
173127 <				4		0.09		0.06	0.02	<2	7
173128 <			<3			0.12		0.05	0.03		7 6 7
173129 <	<.01		<3			0.82		0.04	0.18		7
173130		0.02	<3			0.68		0.01	0.13	<2	9

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ELEMENT	Мо		Cu	Pb	Zn	Ag	Ni	Со	Mn	Fe	As	U	Au
SAMPLES	ppm		ppm		ppm	ppm	ppm						
173131		2	48	12	96	<.3	19	7	726	3.12	9	<8	<2
173132		2	14	19	174	0.4	31	8	992	2.81	18	<8	<2
173133	<1		20	<3	14	0.4		1	200	0.57	11	<8	<2
STANDARI	-	19	101	67	418	0.8	57	9	646	2.47	46	<8	<2
G-1	<1		<1	4	44	<.3	7	4	575	2.1		<8	<2
173134		1	28	<3	58	<.3	10	3	281	0.74	9	<8	<2
173135		2	11	14	96	<.3	13	9	848	3.33	9	9	<2
173136		1	28	7	45	<.3	8	3	340			<8	<2
173137		2	15	26	95	<.3	16	9	813	2.96	7	<8	<2
173138		1	20	21	80	<.3	8	1	423	0.84		<8	<2
173139		2	15	17	81	<.3	24	7	859	2.21	9	<8	<2
173140	<1		30	23	159	<.3	3	1	427	0.64		<8	<2
RE 173140	<1		31	22	161	<.3	1	<1	419	0.63		<8	<2
173141		2	18	28	118	0.3	22	9	857	3.02	14	<8	<2
173142		2	11		75	<.3		<1	477	0.83		<8	<2
173143		1	16	21	104	<.3	21	9		3.11		<8	<2
173144	<1		9	<3	+	<.3		<1	258			<8	<2
173145		1	17	18		<.3	17		857			<8	<2
173146		3	127	9	39	0.3			342			<8	<2
STANDAR		20	102	67	418	1	52	10	639	2.4	51	<8	<2

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ELEMENT	Th		Sr	Cd	Sb		Bi	V	Ca	Р	La	Cr	Mg	Ba
SAMPLES	ppm		ppm	ppm	ppm		ppm	ppm	%	%	ppm	ppm	%	ppm
173131		4	37	0.	8 <3		<3	58	0.59	0.099	35	15	1.44	69
173132		4	72	1.	5 <3		<3	52	5.79	0.172	38	12	0.96	58
173133	<2		100	<.5	<3		10	17	20.15	0.009	5	8	12.57	19
STANDAR		4	78	6.	1	6	5	81	0.98	0.074	13	164	1.07	406
G-1	~	4	90	<.5	<3		3	40	0.67	0.076	8	15	0.6	
173134		2	94	<.5	<3		<b>∽</b> 3	20	20.3	0.012		13		22
173135		5	44	1.	2 <3		5	69	0.84	0.114	37	13		
173136		2	99	0.	7 <3		5	16	21.24	0.009	10	9	13.1	27
173137		5	34	1.	4 <3		7	55	0.55	0.117	34	13		63
173138	<2		156	<.5	<3		<3	16	20.71	0.037	10	6	9.41	20
173139		4	47	1	1 <3		<3	34	7.69	0.111	37	11	4.11	. 56
173140		2	258		1 <3		<3	12	25.44	0.013	4	3	<u>9.77</u>	
RE 173140	<2	!	254	1.	2 <3		<3	11	25.08	0.015	3	5	9.65	
173141		5	39	1.	1	3	6	48	2.02	0.124	31	15	1.22	
173142	<2		95	1.	1 <3		<3	16	19.04	0.035	15	6	10.64	
173143		7	31	0.	8	4	4	51	0.67	0.128	33	14	0.91	59
173144	<2	1	101	<.5	<3		<3	6	23.79	0.011	3	1	12.76	
173145		3	50	0.	9 <3		3	47	5.51	0.111	45	13	2.01	
173146	 	5	60	0.	8	7	5	90	3.36	0.192	24	26	3.11	
STANDAR	, 	4	70	6.	1	6	5	87	0.94	0.077	11	156	1.07	392

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ELEMENT	Ti	В	Al	Na	К	W	Sample
SAMPLES	%	ppm	%	%	%	ppm	kg
173131	0.05	6	2.19	0.05	0.14	<2	4.5
173132	0.04	3	1.94	0.05	0.14	2	6.5
173133	0.02	9	0.81	0.06	0.18	<2	3
STANDARI	0.13	35	1.04	0.11	0.47	4	-
G-1	0.14	4	1.2	0.11	0.57	<2	-
173134	0.03	27	1.01	0.02	0.15	<2	6.5
173135	0.07	7	2.28	0.02	0.1	<2	5
173136	0.02	37	0.81	<.01	0.09	<2	4.5
173137	0.04	7	2.07	0.02	0.13	<2	3.5
173138	0.01	21	0.61	<.01	0.09	<2	6
173139	0.02	8	1.42	0.01	0.12	<2	2.5
173140	0.01	32	0.32	0.01	0.06	3	6
RE 173140	0.01	33	0.3	0.03	0.05	2	-
173141	0.03	10	1.99	<.01	0.14	<2	4.5
173142	0.01	8	0.53	<.01	0.08	<2	5.5
173143	0.04	6	2.21	0.03	0.16	<2	4.5
173144	<.01	6	0.19	<.01	0.02		5.5
173145	0.04	12	1.63	0.01	0.16		7.5
173146	0.14	12	1.98	0.02	0.18		5.5
STANDARI	0.12	40	0.98	0.08	0.48	5	-

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From ACME	ANALYTICAL L	ABORATOR	IES LTD. 852 I	. HASTINGS	ST. VANCOL	IVER BC V6A	1R6 PHONE	604)253-3158	FAX(604)253	-1716 @ CSV	TEXT FORM	λT
To Eastfield F	Resources Ltd.											
Acme file # Al	604234 Page 1	Received:	JUL 24 2006 *	50 samples	in this disk file	Э.						
	DUP 3B - FIRE							ICP ANALYS	IS. UPPER LI	MITS = 10 PP	M	
	H GRADE GOL	D ASSAY R	ECOMMENDE	FOR 30 GM	ANALYSIS >	10ppm and 50	) GM > 5ppm.					
ELEMENT												
SAMPLES												
	<2											
173101	7					i						
173102												
173103	22									·		
173104												
173105												
173106												
173107	19											
173108	14											
173109												
173110						1						
173111	155											
173112	140											
173113	17											
173114	154					1						
173115	14					i						í
173116	45											
173117	85											
173118	41					Ì						1
173119	34											
173120	55		1				. 1					
173121	12					· · · · · · · · · · · · · · · · · · ·						
173122	11										:	
173123	32											
173124			· · · ·									
RE 173124	16											
173125	16	<u></u>									1	
173126	21		• · · · · · · · · · · · • •		· · · · ·							
173127	42		· · · · · · · · · · · · · · · · · · ·			•			,			
173128						••••						
173129					· · · · · · · · · · · · · · · · · · ·	<u>∤</u>			···		<u>†</u>	
1/0129	200					<u> </u>		_		1		<u> </u>

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ELEMENT						
SAMPLES	ppb					
173130	20					
173131	285					
173132	24					
173133	58					
STANDAR	803				_	
G-1	<2					
173134	78					
173135	30					
173136	25					
173137	18					
173138	52					
173139	23					
173140				 í		
RE 173140						I
173141	25				 	
173142	176					
173143				 		
173144				 		L
173145			_			
173146				 ļ	 	
STANDAR	822					

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	From ACME		LABORATORI	ES LTD. 852	E. HASTINGS	ST. VANCOL	VER BC V6/	A 1R6 PHONE	604)253-3158	FAX(604)253-	1716 @ CSV "	TEXT FORMAT
	To Eastfield R	lesources Ltd.	PROJECT Cro	owsnest								
	Acme file # A6	604467 Page	1 Received:	JUL 27 2006 *	104 samples	in this disk fil	Ð.					
	Analysis: GRC		-		TH 3 ML 2-2-2	HCL-HNO3-I	120 AT 95 DE	G. C FOR ON	e hour, dill	JTED TO 10 N	IL, ANALYSE	BY ICP-ES.
ELEMENT	t	Cu	Pb	Zn	Ag	Ni	Со	Mn	Fe	As	U	Au
SAMPLES	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm
G-1	<1		<3	40	<.3	8		3 519			<8	<2
173201	<1	5	3		<.3	9	2				<8	<2
173202	<1	6	5	49	<.3		<1	128			<8	<2
173203	<1	4	<3	10	<.3	3		104			<8	<2
173204	<1	4	<3	26	<.3	2	2	2 138			<8	<2
173205	<1	3	<3	14	<.3	<1	<1	143		1	<8	<2
173206	<1	3		·	<.3		<1	109			<8	<2
173207	<1	6		10	<.3		<1	133	0.16		<8	<2
173208	<1	6	5	20	<.3	3	<1	166		_	<8	<2
173209	<1	7	10	50	<.3	9		3 344	0.53		<8	<2
173210	<1	11	6	41	<.3	10		1 285	0.64	9	<8	<2
173211	<1	16	10	29	<.3	11	6	5 206	1.1		<8	<2
173212	<1	13	10	26	<.3	19		6 130	1.67	8	<8	<2
173213	<1	10	12	38	<.3	23			2.01		<8	<2
RE 173213	<1	10	11	34	<.3	23	8	3 158	2	8	<8	<2
173214	<1	9	20	13	<.3	4	2	2 8	1.1	5	<8	<2
173215	<1	13	21	30	<.3	14		1 151	1.6	11	<8	<2
173216	<1	7	14	22	<.3	12		5 62	1.41	7	<8	<2
173217	<1	· 11	13	37	<.3	14	-	7 117	2.18	18	<8	<2
173218	<1	10	12	56	<.3	11	(	5 118	2.89	19	<8	<2
173219	<1	11	18	109	<.3	11	Į	5 299	2.71	26	<8	<2
173220	<1	5	24	117	<.3	8	1	2 237	0.47	10	<8	<2
173221	<1	3	8	45	<.3	2	<1	275	0.33	7	<8	<2
173222	<1	10	10	42	<.3	3		1 278			<8	<2
173223	1	7	11	32	<.3	4		2 270	1		<8	<2
173224	1	13	11	58	<.3	2	. (			13	8	
173225	1	3	<3	15	<.3	<1	<1	513	0.19	7	<8	<2
173226	1	3	4	13	<.3	<1	<1	331	0.23		<8	<2
173227	<1	1	<3	8	<.3	4	<1	212	0.17	8	<8	<2
173228	· · · · · · · · · · · · · · · · · · ·	9		47	<.3	13		5 180	0.98	11	<8	<2
173229		4	10	32	<.3	4	! .	1 152			<8 <	<2
173230		4	<3	34	<.3	3	· ·	1 89	0.36	5	<8	<2

Eastfield - A604467\_C04 (G1D)

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ELEMENT	Th	Sr		Cd		Sb		Bi	V		Ca	Р	La	Cr	Mg	Ba
SAMPLES	ppm	ppm		ppm		ppm		ppm	pp		%	%	ppm	ppm	%	ppm
G-1		3	62		1.3	<3		<3		33	0.48	1	7			
173201		3		<.5			8	5		17	15.57	0.041	10			439
173202		2	76		1.6		3	6		18	16.5		7			
173203		2	55		0.9		4	11		10	13.81	0.042				19
173204	<2	Ţ- ·	80		0.5	<3		10		8	18.54	0.055	1			31
173205	<2		94	<.5		<3		<3		6	22.14	1	3			12
173206		2	64	<.5			4	10	)	5	19.51	0.035				7
173207	<2		63	<.5			3	9		4	19.93	0.033				
173208	<2		60	<.5		<3		11		6	20.05	0.069	3	8		
173209		2	47		0.6		4	6	\$	11	14.73	0.055	4	10		20
173210		4	41	· · ·	1.1		4	5	5	16	12.71	0.052	5			
173211		4	32		0.8		6	<3		16	7.66	0.04	4	11	2.32	
173212		5	15		1		3	7	7	9	3.42	0.029	4	11	1.05	35
173213		4	14		1	<3		3	3	10	1.96	0.023	4	13	0.75	89
RE 173213		4	13		0.8		5	4	ŀ	11	1.93	0.021	4	13	0.74	
173214		3	13		0.6	<3		<3		9	0.17	0.01	4	12	0.13	58
173215		3	18		0.8			5	5	24	1.97	0.018	14	12	1.08	34
173216		3	10		0.8			<3	!	10	0.13	0.015	6	12	0.1	56
173217		3	7		0.9			6	3	18	0.25	0.014	13	14	0.13	32
173218		3	6		1.5		4	3	3	21	0.31	0.021	7	17	0.07	64
173219		3	35		1.4		3	7	7	22	12.62	0.061	5	15	5.62	43
173220		4	47		0.8	<3		5	5	16	13.33	0.134	7	14	4.33	
173221	<2			<.5		<3		8	_	11	21.11	0.061	3	8	8.89	13
173222		3	65		0.6	<3		15	5	11	18.45	0.082	10	9	6.16	88
173223		3	167		0.9			<3	+	21	17.4	0.045	9	7	4.71	43
173224		5	52	<b>-</b>	1.2		6	6	3	35	3.21	0.093	21	4	0.53	163
173225	<2		206	A		<3		4		4	28.44					
173226			175		0.9		3	<3		4	25.01					
173227			156	<.5	5.5	<3			3	4	23.9		4			
173228		2	106		0.6			10		33	15.41			1		
173229	<2			<.5	0.0	<3		4		15				· · · · · · · · · · · · · · · · · · ·		
173230	<u> </u>	2		<.5		<3		12		11	15.24					

Eastfield - A604467\_C04 (G1D)

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ELEMENT	Ti	B		Al		Na		к		w	Sample
SAMPLES		ppm		%		%		%		ppm	kg
G-1		12 <3			0.93		0.06	-	0.48		-
173201			4		0.35		0.01		0.14		5.31
173202			5		0.27				0.08		10.18
173203			4		0.19		0.03	<b>-</b>	0.05		9.9
173204			4		0.15	<.01			0.06	<2	5.74
173205		<3			0.11				0.02	<2	6.26
173206			3			<.01		ļ	0.04		11.08
173207			3		0.06		0.02	<b>†</b>	0.04	<2	7.78
173208		<3		(	0.12		0.02	· ·	0.07	<2	11.27
173209	<.01		3	····· (	0.22	<.01		+	0.07	<2	5.96
173210		<3			0.23	<.01			0.08	<2	5.15
173211	<.01		8	(	0.37	<.01		+ · · ·	0.17	<2	10.38
173212			7		0.4	<.01			0.22	<2	9.41
173213	<.01	·ŧ•	9		0.5		0.01		0.25	<2	11.48
RE 173213			7	t	0.5	<.01			0.26	<2	
173214	<.01		10		0.7	<.01			0.41	<2	5.57
173215	<.01		4		0.55	<.01		1	0.18	<2	4.96
173216	<.01		5		0.48		0.02		0.29	<2	5.72
173217			3	1	0.46	<.01			0.15	<2	7.69
173218	<.01		4	i (	0.28	<.01		1	0.12	<2	8.84
173219	<.01		3		0.2	<.01			0.1	<2	5.68
173220	<.01		4		0.11	<.01			0.06	<2	6.27
173221	<.01		3		0.07	<.01			0.02	<2	5.04
173222	<.01		3	+ · !	0.22		0.02		0.1	<2	9.09
173223	<.01	<3		i I	0.47		0.02		0.09	<2	3.85
173224	<.01	<3		<b>+</b> · - · · · · · · · · · · · · · · · · ·	1.16		0.04		0.13	<2	9.19
173225			3	1	0.06	1	0.03	1	0.02	<2	6.03
173226		<3			0.11	1	0.01	1	0.01	<2	6.39
173227	<.01	1	3	•···	0.08		0.03	,	0.02	<2	5.01
173228		1	9	1	0.82		0.02		0.3	<2	10.14
173229		<u> </u>	4	1	0.34	<.01		Ţ	0.09	<2	8.85
173230			5		0.25		0.01	1	0.06	<2	8.99

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ELEMENT	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au
SAMPLES	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm
173231	<1	5	5	40	<.3	7	/ <1	117	0.7	6	<8	<2
173232	<1	5	8	22	<.3	3	<1	171	0.52	3	<8	<2
173233	<1	7	6	31	<.3	6	)	2 129	0.9	9	<8	<2
STANDARI	19	100	69	391	0.8	54	•	9 607	2.3	50	<8	<2
G-1	<1	<1	<3	42	<.3	<1		3 502	1.66	<2	<8	<2
173234	<1	7	9	55	<.3	13		2 97	1	9	<8	<2
173235	<1	1	11	32	<.3	<1	<1	146	0.34	6	<8	<2
173236	<1	1	7	24	<.3	3	<1	115	0.23	8	<8	<2
173237	<1	<1	4	15	<.3	5	i <1	105	0.22		<8	<2
173238	<1	2	6		<.3	6	5<1	111	0.32	5	<8	<2
173239	<1	1	49	36	<.3	2	2 <1	184	0.64	6	<8	<2
173240	<1	3		37	0.3	14		3 162	0.74	9	<8	<2
173241	<1	3	5	60	0.3	4	ŀ	2 309	1.31	12	<8	<2
173242	<1	<1	4	35	<.3	8	}	1 125	0.51	4	<8	<2
173243	<1	<1	<3	13	<.3	1	<1	46	0.05	4	<8	<2
173244	<1	2	6		<.3	3	s <1	138	0.53		<8	<2
173245	<1	<1	4	20	<.3	<1	<1	111	0.18	3	<8	<2
173457	1	8	24	58	<.3	8	3 <1	503	0.82	9	<8	<2
173458	1	8	14	43	<.3	12	2	3 373	0.98	7	<8	<2
173459	1	12	18	78	0.4	13	3	7 661	2.22	10	<8	<2
173501	10	<1	5	28	<.3	8	3 <1	78	0.24	7	<8	<2
173502	7	6	19	88		19	)	3 120	0.92	11	<8	<2
173503	2	<1	4	60	<.3	6		2 83	0.41	7	<8	<2
173504	_6	8	17	70	<.3	18		4 122	_	12	12	<2
173505	· · · · · · · · · · · · · · · · · · ·	<1	<3	24	-	2	2 <1	61	-		<8	<2
173506	<1	<1	6	43	<.3	<1	<1	53		9		<2
173507	<1	<1	<3		<.3	2	2 <1	47			1 127	<2
RE 173507	<1	<1	3		<.3	2	2 <1	47				<2
173508	6	1	<3		<.3		<1	49		6	-	<2
173509	11	<1	<3		<.3	5	5 <b>&lt;1</b>	55		6	-	<2
173510	1	<1	<3		<.3	1	<1	52		4		<2
173511	1	<1	<3		<.3		3 <1	38	1			<2
173512	<1	<1	7		<.3	4	<b>∣ &lt;1</b>	21			<8	<2
173513	1	<1	<3	-	<.3	<1	<1	20				<2
173514	1	1	<3	15	0.4	9	) <1	20	0.06	4	<8	<2

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ELEMENT		Sr	Ī	Cd		Sb	E	Bi	V	C		P	La	Cr	Mg	Ba
SAMPLES	ppm	ppm		ppm		ppm	F	opm	ppm	%		%	ppm	ppm	%	ppm
173231			65		5	3	<	3	21		13.57	0.064	10		5.33	
173232	<2			<.5		<3	Γ	7	15		19.32	0.04	7	9		15
173233		3	57	<.5		<3	Γ	7	23	3	13.75	0.066	10	19	5.91	27
STANDAR		4	75	6.	1	5	Γ	4	76	3	0.94	0.073	12	186	1.02	384
G-1		3	53	<.5	-	<3	Γ	5	31		0.51	0.068	6	7	0.54	200
173234	<2		36	0.	9	<3		<3	26	5	8.56	0.06	10	21	1.96	
173235	<2		78		9	Ś		<3	17	7	19.35	0.038	5	7	7.76	
173236	<2			<.5		<3		<3	7	7	20.99	0.046	4	8	9.51	5
173237	<2		<b>60</b>	<.5		<3	<	<3	6	5	18.62	0.04		9	8.97	4
173238	<2		65	<.5		<3	<	<3	9	)	17.27	0.041	5	9	8.14	
173239	<2	1	28	0.		<3		11	14	1	21.1	0.042	7	4	3.94	
173240				<.5		<3		3	21		14.16		10		5.86	
173241	<2		B6			<3		<3	25	5	16.7	0.055	12		2.94	
173242	<2		59	0.		<3	<	<3	15	5	13.36	0.049	8	15	5.62	9
173243	<2			<.5		<3		3	1	1	<u>29.</u> 81	0.028	1	1	2.39	
173244			58	0.	8	3	<	<3	15	5	14.86		6		6.16	
173245	<2	1	01	<.5		4		5	3		25.78	0.048	2		0.97	7
173457	<2	1	23	1.	2	3	<	<3	13	3	20.76	i	12	5	6.92	-
173458	<2		37	0.	5	<3		4	17	7	19.61	0.054	14	í	5.03	
173459		3	96	1.	2	<3	1	3	44	1	11.01	0.076	29		2.49	
173501	<2	1	06	<.5	-	<3		3	14		16.4	0.025	3			
173502		2	85	1.	9	<3	<	<3	28		12.36	i .	10	19		17
173503	<2	1	51 j	2.	1	5		8	10		19.63	0.028	6		9.9	
173504		3	72	1.	6	3	i	5	32		9.84		1			
173505	<2	2	63	0.	7	4		<3	8		21.91	0.021	3	•	11.05	
173506	<2	2	91	2.		3	]	13	5		24.19		2		10.14	
173507	<2	1	72	2.	1	<3	Ì.	7	8	3	21.39		2		11.9	
RE 173507	<2	1	6 <del>9</del>	2.	3	<3	Τ	10	8	3	21.03		2		11.7	8
173508	<2	_1	89	1.	2	<3		ŝ	16		10.24					
173509	<2	1	19	<.5	1	3		<3	5		20.7	0.015	2		11.77	
173510	<2		97	<.5		5		8	8		21.96		2		12.08	
173511	<2	1	55	<.5		5		<3	10		23.32		2		1	
173512	<2	2	19	<.5	1	3		8	3	3	21.67		2	12		
173513	<2	2	13	0.	5	8		7	5		22.75					
173514	<2	1	76	0.	5	11	Ì	3	6	3	23.6	0.014	1	10	5.74	2

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ELEMENT	Ti		B	Al	Na	K	W	Sample
SAMPLES	%		ppm	%	%	%	ppm	kg
173231	<.01		4	0.55	0.0	2 0.21	<2	7.99
173232		0.01	8	0.28	0.0	2 0.09	<2	9.08
173233	<.01		11	0.58	0.0	0.29	<2	6.11
STANDAR		0.12	37	0.99	0.1	0.43	4	-
G-1		0.11	<3	0.86	0.0	3 0.43	<2	-
173234	<.01		11	0.76	<.01	0.38	<2	6.98
173235	<.01		11	0.2		0.06	<2	8.18
173236	<.01		3	0.12	0.0	3 0.08	<2	7.59
173237	<.01		4	0.13	<.01	0.06	<2	7.59
173238	<.01		8	0.19	0.0			10.45
173239	<.01		4	0.41	0.0	2 0.07	<2	10.03
173240	<.01	_	8	0.54	<.01	0.18		12.67
173241	<.01		<3	0.74	<.01	0.08		12.53
173242	<.01		6	0.38	0.0	2 0.12	2	11.49
173243	<.01		<3	0.04	0.0	<.01	<2	12.51
173244	<.01		9	0.33	0.0	0.16	<2	6.55
173245	<.01		<3	0.09	0.0	3 0.02	<2	8.83
173457		0.01	<3	0.57	<.01	0.07	<2	12.01
173458		0.01	<3	0.69	0.0	0.07		12.19
173459		0.04	<3	1.59	0.0	2 0.1	2	7.55
173501	<.01	··· ,	5	0.14	0.0	3 0.08	<2	4.89
173502	<.01		12	0.79	<.01	0.49	<2	5.21
173503	<.01		9	0.25	<.01	0.16		7.34
173504	<.01		16	1.2	0.04	0.74	<2	7.7
173505	<.01		6		0.0	1		5.51
173506	<.01		3	0.09	<.01	0.04	<2	4.83
173507	<.01		<3	0.08	<.01	0.06	<2	5.47
RE 173507	<.01		<3	0.09	<.01	0.05	<2	-
173508	<.01		8	0.58	<.01	0.36	<2	5.89
173509			4	0.18	0.0	2 0.08	<2	4.17
173510	<.01		4	0.1	0.0	1 0.04	<2	7.32
173511			<3	0.1	0.0	2 0.05	<2	8.28
173512	<.01		<3	0.04	<.01	0.02	<2	8.25
173513	<.01		<3	0.04	<.01	0.03	<2	9.28
173514	<.01		7	0.05	<.01	0.02	<2	6.51

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ELEMENT	Мо	C	u	Pb	Zn	Ag	Ni	(	Co	Mn	Fe	As	U	Au
SAMPLES	ppm	p	pm	ppm	ppm	ppm	ppm	F	opm	ppm	%	ppm	ppm	ppm
173515	• • • • • • • • •	1 <	1	3	1 7	<.3		1	<1	17	0.07	6	<8	<2
173516		1 <	1	<3	5	<.3		4	<1	17	0.06	8	<8	<2
173517		1 <	1	<3	6	<.3		5	<1	30	0.07	4	<8	<2
173518	~	1 <	1	<3	8	0	.3	3 -	<1	35	0.08	4	<8	<2
STANDAR	1	9	96	68	398		1 4	18	9	622	2.36	47	<8	<2
G-1	<1	<	1	9	67	<.3		6	4	556	1.94	4	<8	<2
173519		8	6	16	5 157	0	.5 6	55	7	71	2.74		<8	<2
173520		3 <	1	10	41	0		12	2	71	0.56	7	<8	<2
173522		5	1	12	2 87	Ō	.7 4	17	4	69	2.1	19	<8	<2
173523		1 <	1	<3	19	<.3		4 -	<1	41	0.21	4	<8	<2
173524		1<	1	<3	12	0	.3	4 -	<1	20	0.07	<2	8	<2
173525		1<	1	<3	25	0	.3	5	<1	60	0.2	2	<8	<2
173526		2	1	<3	20	Ō	.3	7.	<1	58	0.27	4	<8	<2
173527	1	5 <	1	8	3 100	0	.3	8	<1	73	0.43	6	<8	<2
173528	1	6	4	11	150	0	.4 2	22	3	79	1.14		<8	<2
173529		1<	1	<3	41	<.3		1	<1	49	0.23	2	<8	<2
173530		1 <	1	3	60	<.3		8	<1	49	0.33	<2	<8	<2
173531	<1	<	:1	<3	20	<.3		2	<1	41	0.09	<2	<8	<2
173532		1 <	:1	3	38	<.3		1	<1	63	0.24	4	<8	<2
173533		1<	:1	5	5 22	<.3		9	<1	78	0.37	2	<8	<2
173534	1	0	6	15	5 94	0		20	4	162	1.27	11	L	<2
173535	1	4	9	22	2 157	0	.3 2	25	6	131	1.48	16	9	<2
173536		7 <	:1	6	3 49	<.3		5	<1	114	0.32	4	<8	<2
173537		8 <	:1	7	7 43	<.3		7.	<1	159		3		<2
173538		7 <	:1	<3	36	<.3		6		106	0.26		·	<2
RE 173538	r	7 <	:1	<3	33	<.3		7	<1	105	0.25	7	<8	<2
201401	<1		2	4	37	<.3		7	2	292			<8	<2
201402	<1		10	5	5 38	<.3		7	6	187			<8	<2
201403	<1		7	3	3 26	<.3		16	4	187			<8	<2
201404		1	8	12	2 43	<.3		14	6	248			<8	<2
201405	<1		7	8	3 33	<.3		25	6	193			<8	<2
201406	;<1		1	15		<.3		6	1	7			L	<2
201407		1	10			<.3		28	11	124			<8	<2
201408		1	11			<.3		18	8	68			<8	<2
201409		1	14	22	2 247	<.3		33	13	147	6.17	23	<8	<2

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ELEMENT		S	sr	Cd		Śb	Bi	V	Ca	Р	La	Cr	Mg	Ba
SAMPLES	ppm	р	pm	ppm		ppm	ppm	ppm	%	%	ppm	ppm	%	ppm
173515	<2		163	<.5		3	<3	6	19.6		1	-		
173516	<2		164	<.5		5			19.15	0.016	<1	9		1
173517	<2		133	1	0.6	8			18.52	0.014	1			1 -
173518	<2		166		0.7	7	5	4	21.78	0.014	2		8.57	3
STANDARI	•	4	77		5.8	6	5	79	0.98	0.073	13	190	1.04	
G-1		4	67	<.5		<3	<3	34	0.71	0.071	7		0.65	206
173519		4	87		2	6	4	58	9.63		5		4.24	22
173520	<2	_ <b>[</b> -	176	<.5		<3	<3	31	19.98		4			11
173522		4	83		0.8		<3	72	9.77		5		4.77	30
173523	<2		148	<.5			<3	6	19.54	0.022	. 2			7
173524	<2		214	<.5			<3	4	23.81	0.011	1	16	13.6	
173525	<2		152	<.5		3	<3	10	23.23	0.018	3		11.62	11
173526	<2		107	<.5			<3	12	22.73	0.014	3		11.97	9
173527	<2	:	123		0.9	9	<3	8	20.94	0.02	4		12.06	
173528		3	107		1.5	<3	<3	27	10.17	0.041	7	1	6.35	
173529	<2		78		0.9	<3	4	5	14.85	0.046	4	9	8.67	
173530	<2		57	1	1.4	<3	<3	7	11.22	0.058	6	14	6.76	
173531	<2		269		0.6	<3	<3	3	23.68	0.014	1			
173532	<2		294		1.3	<3	4	6	24.4	0.017	2	5	11.36	
173533			226	<.5		<3	<3	8	21.21	0.025	4	7	11.5	
173534		3	62		1.7	<3	3	33	9.28	0.061	15		3.41	
173535		4	57		2	3	<3	54	7.03	0.078	15	34		31
173536	<2		133	1	1.2	<3	3	14	20.3	0.02	4	6	7.58	12
173537	<2		127		0.8	6	<3	20	20.16	0.028	5	10		
173538	- · · · · · · · · · · · · · · · · · · ·	2	116	<.5		5	<3	13	19.53	0.029	4	10		
RE 173538	<2	!	114	<.5		<3	<3	12	18.99	0.028				
201401	<2		65		0.9	<3	<3	9	19.51	0.045		9		
201402		2	88		0.9	3	4	20	12.87	0.043	4	14		
201403	<2	-	63	<.5		<3	Ę	5 13	8.01	0.036	5	14	1.69	
201404	<2	+	45	<.5		<3	+ <del>(</del>	23	6.2	0.031	11	14		25
201405				<.5		<3	<3	14	0.96	0.017	5	17		1
201406		4		<.5		<3	<3	6	0.16	0.014	4	9		77
201407		4	8			<3	<3	17	0.09	0.021	16	14	0.1	
201408		3	5	<.5		<3	3	3 21	0.09	0.014				
201409		3	6		0.6		<3	26	0.3	0.019	11	20	0.12	2 110

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ELEMENT	Ti		В	AI		Na		К	Ŵ	Sample
SAMPLES	%		ppm	%		%		%	ppm	kg
173515	<.01		<3		0.04	<.01		0.01		6.09
173516	<.01		5		0.03	<.01		0.01	<2	7.25
173517	<.01		3	1	0.04	<.01		0.02	<2	7.41
173518	<.01		<3		0.04		0.02	0.02	<2	6.23
STANDAR	) (	0.12	35		1.02		0.1	0.44	5	-
G-1		0.13	6		1		0.08	0.48		-
173519			9			<.01		0.49		4.87
173520			8		0.37		0.01	0.23		5.29
173522			14	•	1.22		0.01	0.77	2	
173523			<3		0.15		0.01	0.03		4.86
173524			<3			<.01		0.01		8.87
173525			4		0.15		0.01	0.04		5.7
173526			4	-	0.16		0.01	0.07	<2	4.34
173527			7		0.38		0.01	0.11	2	6.2
173528			18		1.14		0.01		2	4.71
173529			3		0.11		0.01	0.05		5.37
173530			7	'		<.01		0.05		4.47
173531			<3		0.03			0.02		6.3
173532			3		0.19		0.01			4.39
173533			5		0.29		0.01		<2	4.81
173534	<.01		20		1.11		0.06	0.54		4.68
173535			19		1.4		0.01	0.79	2	2.42
173536	<.01		5	, ' •		<.01		0.05		4.54
173537	<.01		6	<b>;</b>	0.32		0.01	0.11	<2	3.35
173538	<.01		6		0.17	<.01		0.1	<2	3.7
RE 173538			3		0.16		0.01	0.11		-
201401			5		0.16	<.01		0.09	<2	7.31
201402	<.01		5		0.33			0.18	<2	5.98
201403	<.01		8	\$	0.56	<.01		0.22	<2	6.02
201404	(	0.01	10		0.66		0.01	0.21		8.86
201405			8		0.64	<.01		0.3		4.21
201406	<.01		5	5		<.01		0.33	<2	8.8
201407	<.01		4		0.54	<.01		0.16	<2	9
201408	<.01		4		0.43			0.13		4.97
201409	<.01		7		0.38		0.01	0.13	<2	7.51

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Page	10	of	12
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ELEMENT	Mo		Cu	Pb	Zn	Ag	Ni	Со	Mn	Fe	As	U	Au
SAMPLES	ppm		ppm	%	ppm	ppm	ppm						
201410		1	1	27	108	<.3	9	1	222	1.04	15	18	<2
201411		1	11	21	114	<.3	11	7	148	4.47	23	<8	<2
201412		1	<1	3	10	<.3	2	1	353	0.18	<2	10	<2
201413	<1		1	8	28	<.3	8	1	154	0.63	6	<8	<2
STANDAR		21	100	64	417	1.1	55	10	645	2.46	52	<8	<2

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ELEMENT	Th	S	ir 🗌	Cd		Sb	Bi	V		Ca	P	La	Cr	Mg	Ba
SAMPLES p	ppm	p	pm	ppm	·	ppm	ppm	ppm		%	%	ppm	ppm	%	ppm
201410	<u> </u>	2	52		0.7	<3	<3		18	10.47	0.069	8	15	1.24	21
201411		5	25	<.5		<3	<3		31	1.98	0.065	18	8	0.54	37
201412		2	162		0.6	<3	<3		3	27.26	0.02	3	7	6.43	4
201413		2	71		0.6	<3	<3		17	19.42	0.051	8	14	7.18	17
STANDARI		4	78		6		7	5	83	1	0.077	13	201	1.08	398

Page	12	of	12

ELEMENT	Ti		В		Al	Na	K	W	Sample
SAMPLES	%		ppm		%	%	%	ppm	kg
201410	<.01			3	0.22	0.0	2 0.13	<2	6.11
201411	<.01		<3		0.82	0.0	0.09	<2	13.43
201412	<.01		<3		0.08	0.0	I <.01	<2	6.72
201413	<.01	ï		8	0.33	<.01	0.15	<2	9.76
STANDAR	ĺ	0.12		34	1.04	0.0	7 0.46	3	-

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From ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716 @ CSV TEXT FORMA       To Eastfield Resources Ltd. PROJECT Crowsnest	
Analysis: GROUP 3B - FIRE GEOCHEM AU - 30 GM SAMPLE FUSION, DORE DISSOLVED IN AQUA - REGIA, ICP ANALYSIS. UPPER LIMITS = 10 PPM.     HIGH GRADE GOLD ASSAY RECOMMENDED FOR 30 GM ANALYSIS > 10ppm and 50 GM > 5ppm.     ELEMENT Au**	
HIGH GRADE GOLD ASSAY RECOMMENDED FOR 30 GM ANALYSIS > 10ppm and 50 GM > 5ppm.   Image: Constraint of the system	
ELEMENT Au**	
SAMPLES   ppb   Image: second	
G-1   <2	
173201	
173202   2	
173203 <2	
173204 <2   3   6	
173205   3	
173206 <2   2   173207 <2   173207 <2   173208 <2   173209    173209    173209    173210    18   173210    18   173211    18   173212    18   173212    18   173212    18   19   19   10 <td< th=""><th></th></td<>	
173207   <2	
173208 <2   173209   5   173209   5   173210   18   173211   18   173211   18   173212   18   173212   10	·
173209   5	
173210   18	
173211     2	
173212 2 2	
173213 3	
RE 173213 6	
173214 5	
173215 13	
173216 3	
173217 3	
173218 <2	
173219 5	
173220 <2	
173221 6	
173222 2 2	
173223 10	
173224 4	
173225 4	
173226 4 .	
173227 <2	
173228 2	
173229 9 9	<del>_</del>

Page 2 of 4

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ELEMENT	Au**										<b>]</b>
SAMPLES	nnh										
173230	3										
173231	5										
173232	5										
173233	5										
STANDAR											
G-1	2										
173234	2			·							
173235	2				+						
173236											
173237		,									
173238											
173239	5										
173240	3	i									
173241	5										
173242	3				·						
173243	2;						<u> </u>				
173243	3								·		
173244	2										
173457	10			1			1				·
173458	11			·					······································		1
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RE 173507	<2				<u>.</u>	·					
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173509	<u> </u>	i				<u> </u>				<u> -</u>	
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173511					· · · · · · · · · · · · · · · · · · ·			<u>.</u>			
173512				ļ		•					
173513	<2			<u>i</u>		j					

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ELEMENT	Au**	· · · · · · · · · · · · · · · · · · ·				1			· · · · · · · · · · · · · · · · · · ·
SAMPLES	daa								- · · · · · · · · · · · · · · ·
173514	<2								
173515	2	·····			Í				
173516	2				-				
173517									
173518				Ī.					
STANDAR									
	<2								
173519									
173520	4								
173522	3								
173523					<b>_</b>				ļ
173524	11	, 							ļ
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173537		· · · · · · · · · · · · · · · · · · ·				· · ·			<u></u>
173538									· · · · · · · · · · · · · · · · · · ·
RE 173538		★ +				+			·
201401	5	·····							
201402	•	<u>↓</u>					·		+
201403				· · · · ·					<u>+</u>
201404			i						<u>+</u>
201405 201406		4							.+
201406				i					<u>+</u>
201407		· · · · · · · · · · · · · · · · · · ·			i			+	<u>+</u>
201408				I .		l	I		İ

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ELEMENT	Au**						
SAMPLES 201409	ppb						
201409	7						
201410	2						
201411	<2						
201412	<2						
201412 201413	3	]					
STANDAR	802						

Eastfield - A604467\_C04 (G3B)

