



ASSESSMENT REPORT

of the

OK COPPER PROPERTY

VANCOUVER MINING DIVISION, BRITISH COLUMBIA

NTS: 92K/02E
(092K007)

Latitude 50 degrees, 02' N, Longitude 124 degrees, 38' W

Owner Operator

EASTFIELD RESOURCES LTD.
Suite 110 – 325 Howe St.
Vancouver, B.C.
V6C 1Z7

Joint Venture Partner

PROPHECY RESOURCE CORP.
Suite 1400 – 400 Burrard Street,
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By

J.W. Morton, P.Geo.

August 15, 2007
GEOLOGICAL SURVEY BRANCH
ASSESSMENT REPORT

20,200

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INTRODUCTION

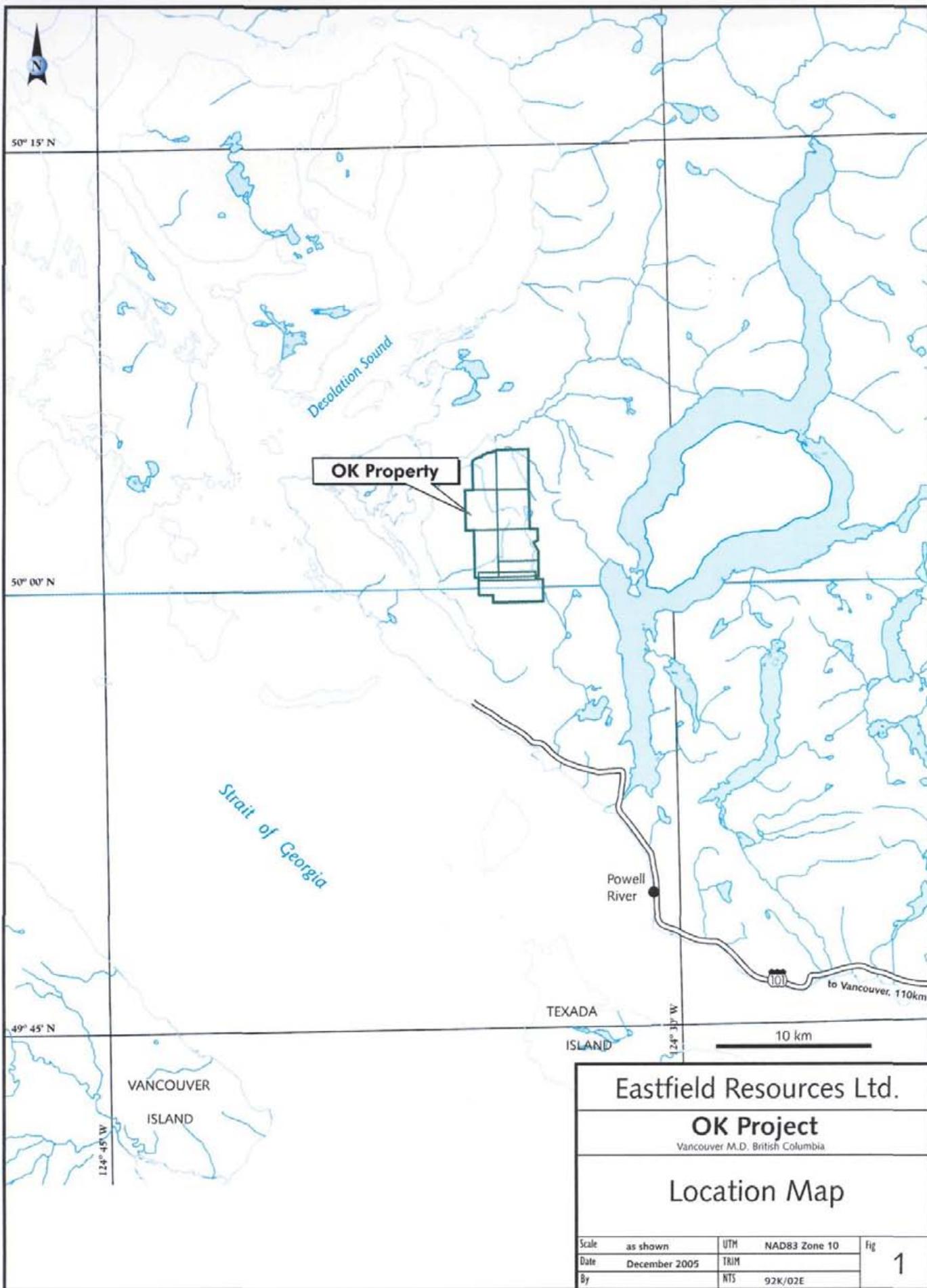
During the month of June, 2006 Surface work Prophecy Resource Corp. funded the collection and analyses of several hundred soil samples from two grid areas and road and drill road construction in the North Lake area using a large excavator. More precise locations of a number of old roads throughout the property area were determined by a global positioning system device. Total program costs for the 2006 work were \$102,000 (\$25,000 was claimed on the assessment filing document with \$1,161.89 of this for the required work).

GENERAL GEOGRAPHIC and PHYSIOGRAPHIC POSITION and ACCESS

The OK copper-molybdenum property consists of fourteen contiguous mineral claims located in the Vancouver Mining Division of southwestern British Columbia 25 kilometres north of Powell River and 145 kilometres northwest of Vancouver. Collectively, the claims cover an area of approximately 5233 hectares between latitudes $49^{\circ}59.5'$ and $50^{\circ}04.6'$ North and longitudes $124^{\circ}37.0'$ and $124^{\circ}41.2'$

The OK copper property is situated on the southwest coast of British Columbia and borders the south shore of Theodosia Inlet. Mineral claims comprising the property are about midway between Powell Lake on the east and Okeover Inlet on the west. The southern part of the property is accessible by vehicle via highway 101 and secondary logging roads from the community of Powell River. Road distance is about 35 kilometres; driving time is approximately one hour. The preferred access route from the BC ferry terminal in the southern part of Powell River (Westview) is northwest by way of highway 101 to Southview Road, a distance of 15 kilometres, then north on Southview Road for 10 kilometres to a stop sign which marks the junction with Branch 02 of the Theodosia 6423 Forest Service Road (FSR). Conventional vehicles are adequate to this point; steeper grades and loose gravel on the FSR roads are best negotiated by 4-wheel drive vehicles. Traveling west on the Branch 02 road for 6 kilometres leads to Branch 03 which extends north 3.3 kilometres to the southern part of the OK property.

Logging roads, which provide access to the northern claims area from Theodosia



Inlet, are currently accessible only by barge.

Powell River, a community of 18,000 offering most supplies and services, is 120 kilometres northwest of Vancouver and may be reached by highway and coastal ferry. Daily scheduled airline service from Vancouver is also available.

The OK property is situated in the Pacific Ranges of the southern Coast Mountains. Elevations within the property area range from sea level at Theodosia Inlet to a maximum of 1100 metres and average between 800 and 900 metres within an upland, plateau-like area which is prevalent throughout much of the central property area. The claims area is bordered on the east by the Bunster Hills which rise between 100 and 200 metres above the plateau surface. Relatively moderate slopes prevail between the upland surface and Okeover Inlet to the west while the northern claims area features steep slopes to Theodosia Inlet.

The climate is typical of the southwest coast of British Columbia with mild winters and an annual precipitation of about 110 centimetres. Temperatures between the months of June and September average between 18 and 24 degrees Celsius; mean January temperatures are slightly above freezing. Fieldwork is best carried out between early spring and late fall.

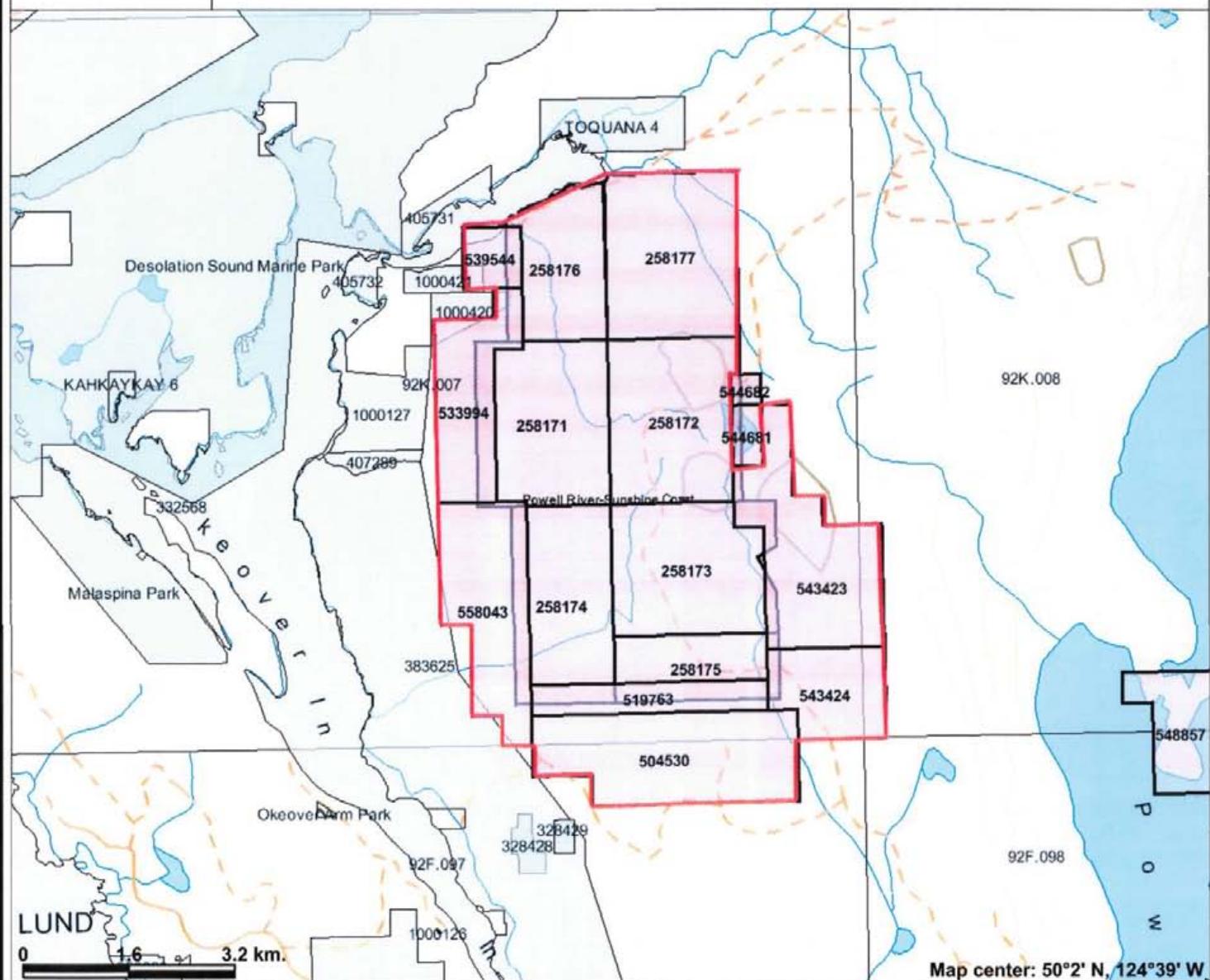
Much of the area of the claims has a relatively subdued topography and would offer a number of alternate options for the construction of mining facilities. The coastal climate would almost certainly ensure that water could be locally sourced and the relative proximity of the BC Hydro grid would be expected to provide accessible hydropower.

PROPERTY DEFINITION

OK Claim Status

Claim Name	Record #	Hectares	Expiry Date
Ok A	258171	500	Nov. 30, 08
Ok B	258172	500	Nov. 30, 08
Ok C	258173	500	Nov. 30, 08

OK CLAIMS



Legend

- Indian Reserves
- National Parks
- Parks
- Mineral Tenures (Mineral - MTO)
- Mineral Claim
- Mineral Lease
- Reserves (Mineral - MTO Sites)
- Placer Claim Designation
- Placer Lease Designation
- No Staking Reserve
- Conditional Reserve
- Release Required Reserve
- Surface Restriction
- Recreation Area
- Others
- Mining Division (MTO)
- BCGS Grid
- Contours (1:250K)
- Contour - Index
- Contour - Intermediate
- Areaof Exclusion
- Areaof Indefinite Contours
- Annotation (1:250K)
- Transportation - Points (1:250K)
- Airfield
- Anchorage - Seaplane
- Ferry Route
- Heliport
- Seaplane Base
- Air Field
- Airport
- Air Feature - Condition Unknown
- Airport.Abandoned

Scale: 1:90,989

This map is a user generated static output from an Internet mapping site and is for general reference only. Data layers that appear on this map may or may not be accurate, current, or otherwise reliable. THIS MAP IS NOT TO BE USED FOR NAVIGATION.

Ok D	258174	450	Nov. 30, 08
Ok E	258175	250	Nov. 30, 08
Ok F	258176	375	Nov. 30, 08
Ok G	258177	500	Nov. 30, 08
Ok H	504530	519.3	Jan. 21, 08
Ok Connector	519763	166	Sept. 7, 08
OK West	533994	291.4	May 12, 2008
Ok Northwest	539544	82.5	August 17, 2007
OKE	543423	477	Oct 17, 2007
OKE1	543424	228	Oct 17, 2007
SOUTHWEST	558043	<u>394</u>	May 3, 2008
Total		5233	

All claims are registered in the name of Eastfield Resources Ltd. and are subject to a March 4, 2003 option agreement with Robert Edward Mickle of Likely, B.C. whereby Eastfield has the right to earn a 100% interest in the property subject to a 2.5% net smelter royalty interest which may be purchased from the vendor for \$2 million on commencement of commercial production. Cash payments to the vendor totaling \$88,000 over a five years period are due at six month intervals in addition to the annual issuance of Eastfield securities amounting to 125,000 shares over the life of the agreement.

Prophecy Resource Corp. is Eastfield's option partner on the OK property and can earn a 60% interest in the OK property, by making cash payments and/or stock issuances amounting to \$105,000 to Eastfield over the next four years plus incurring exploration expenditures totaling \$1 million over the same time frame.

HISTORY

Copper and molybdenum mineralization was discovered in creek bottoms in the central part of on the OK property by the current registered owner in 1965. Between 1966 and 1977, seven companies carried out a number of geological, geochemical and geophysical surveys, mechanical trenching and more than 14000 metres of drilling. Companies included Noranda Exploration Company Ltd., Asarco Exploration Company of Canada Limited, Falconbridge Nickel Mines Ltd., Duval International Corporation, Granite Mountain Mines Ltd., Sierra Empire and Western Mines Ltd.

Drilling completed between 1966 and 1977 consisted of 13,832 metres of diamond drilling in 82 holes and 12 vertical percussion holes totaling 732 metres. Most of the diamond drill holes were inclined at -45° or less and five were vertical holes. Average hole length was 169 metres and the deepest hole drilled was 363 metres in length. Average vertical depth tested was between 120 and 140 metres below surface. Vertical percussion holes were drilled to 61 metres depths. Readily available reports pertaining to drilling include only those of Western Mines Ltd. in 1974 and 1977. Original drill logs and analytical results for core and cuttings samples from all holes drilled between 1966 and 1977 were digitized in the late 1980s and these data were acquired on behalf of Goldrush Resources Ltd. in late 2004.

Work on the property between 1979 and 1982, undertaken by Aquarius Resources Ltd., was mainly directed to a breccia zone with enhanced copper, molybdenum and silver values in the southern property area. Work included limited diamond drilling (3 holes totaling 205 metres), geological mapping, an Induced Polarization geophysical survey and soil geochemical surveys, road building and trenching).

CanQuest Resource Corporation acquired the rights to the property in the early 1990s and a reconnaissance geological mapping and sampling program was undertaken in the area of the southern breccia zone in 1994. A small grid (4.2 line kilometres) was established in 1995 to cover this area in the south-central part of the OK C mineral claim and an Induced Polarization survey was completed. An area of higher chargeability identified by this survey was tested by one short (154 metres) inclined diamond drill hole in 1996. Follow-up work in 1997 included mapping of bedrock exposed in newly constructed logging roads. An expanded program in 1998 consisted of geological

mapping and bedrock chip sampling in other areas of the property plus limited soil geochemical sampling and orientation magnetometer, VLF-EM and Self Potential geophysical surveys in selected areas.

A geological mapping, prospecting and bedrock sampling program on the OK property was undertaken by Mincord Exploration Consultants Ltd. on behalf of Lumina Copper Corp. in October of 2003. This work, which was mainly directed to bedrock exposures along logging roads in the central southern property area, included geological mapping at 1:5000 scale, petrographic studies and the collection and subsequent analyses of 81 rock samples.

An airborne geophysical survey over a large part of the property was completed between July 12 and 15, 2004 by Fugro Airborne Surveys Corp. on behalf of Goldrush Resources Ltd. This survey, conducted by helicopter, involved the collection of electromagnetic, resistivity and magnetic data. Goldrush also funded a six hole, 975 metres diamond drilling program in 2005.

SUMMARY OF WORK COMPLETED (2006)

Surface work on the OK property in May and June of 2006 was funded by Prophecy Resources Ltd. Work included the collection and analyses of several hundred soil samples from two grid areas and road and drill pad construction in the North Lake area using a large excavator. More precise locations of a number of old roads throughout the property area were determined by a global positioning system device. 598 soil samples were collected and analyzed. Total program costs for the 2006 work were \$102,000 (\$25,000 was claimed on the assessment filing document with \$1,161.89 of this to cover the required work).

GEOLOGICAL SETTING

Regional Setting

The OK property is situated in the western part of the Coast Plutonic Complex which is coincident with the Coast tectonic belt extending along the western margin of mainland British Columbia. The complex consists mainly of a series of granitic plutons which intrude volcanic and sedimentary rocks along its eastern margin. Numerous

pendants of metavolcanic and metasedimentary rocks plus orthogneisses are present within the granitic rocks which range in age from Jurassic to Tertiary.

The regional setting of the OK property is somewhat unique inasmuch as most of the known porphyry copper-molybdenum deposits in the Canadian Cordillera are situated in the Intermontane Superterrane east of the Coast Plutonic Complex and to a lesser degree in the Insular Superterrane to the west. Notable exceptions are some porphyry molybdenum deposits in British Columbia and the Alaskan panhandle which are related to younger granitic intrusions within the Coast Plutonic Complex. Examples include the large Quartz Hill molybdenum deposit east of Ketchikan in southeastern Alaska and the Salal Creek and Gem porphyry molybdenum prospects in southwestern British Columbia. The Don porphyry copper-molybdenum prospect, north of Jervis Inlet some 40 kilometres east of the OK property, is a relatively recent discovery (early 1980s) of porphyry mineralization within Coast granitic terrane.

Some previous investigators have remarked on the position of the OK intrusive complex between two apparent subcircular structures including East Redonda Island to the north and Powell Lake to the east. These features may represent collapsed caldera structures.

Granitic rocks of the Coast Plutonic Complex in the immediate area of the OK property include granodiorites, quartz diorites and more basic diorites and gabbros. Screens or pendants of intermediate to basic volcanic rocks have been reported. Radiometric ages of similar granitic rocks in southwestern British Columbia range from early to mid Cretaceous.

Property Geology

In the central part of the property, older Coast Plutonic Complex granitic rocks have been intruded by the OK intrusive complex which is elongate in a northerly direction and measures 3.6 x 2.3 kilometres. The age of this complex is not known but it is reasonable to assume a late Cretaceous to mid-Tertiary age (75 – 35 Ga), similar to other mineralized granitic intrusions on Vancouver Island (Catface, Mt. Washington) and elsewhere in the southwestern British Columbia mainland (Gem, Salal Creek).

Contacts between the intrusive complex and older Coast granitic rocks have been observed along the northern and eastern margins of the complex where some development of gneisses in the older rocks has been reported by Meyer et al in 1976. Williams in 1998 refers to the granitic rocks of the complex displacing older Coast diorites and gabbros.

The OK intrusive complex features multiple intrusive events, a characteristic of many porphyry deposits. At least six intrusive phases were noted by N.C. CARTER, Ph.D. P.Eng., during a brief examination of the southern property area in 1984. The two principal intrusive phases include an earlier, variably altered, fine- to medium-grained, equigranular granodiorite which is intruded by a large, northerly-trending, dyke-like body of quartz-feldspar porphyry featuring crowded feldspar phenocrysts and scattered 1 centimetre-size, rounded quartz "eyes".

The previously reported granodiorite composition for much of the OK intrusive complex may be incorrect. An adjunct of the 2003 geological mapping program involved diamond sawing of a number of rock samples for sodium cobaltinitrate staining to determine the potassium feldspar content. This work suggests that the dominant intrusive phase of the OK intrusive complex is of quartz diorite composition rather than granodiorite. A leucocratic quartz diorite phase is prevalent in the central claims area and the younger quartz-feldspar porphyry also appears to be of quartz diorite composition. These observations are supported by a petrographic study of seven thin sections by Vancouver Petrographics Ltd.

The foregoing conclusions regarding the composition of the principal intrusive phase was confirmed during the examination of drill cores recovered from the North Lake mineral zone in 2005. A leucocratic quartz diorite was the principal host rock for copper and molybdenum mineralization while relatively massive, weakly mineralized, crowded quartz feldspar porphyry represented a later intrusive phase.

Younger, definitely post-mineral intrusive phases include narrow, aphanitic and porphyritic mafic dykes and hornblende diorites, termed diabase by some workers. These occur as steeply-dipping, north-northeast and north-northwest-trending dykes of up to 3 metres or more in width. Previous drilling suggested that these dykes occurred as swarms within a 1 kilometre-wide, north-northeast-trending zone in the central property area.

Discontinuous, fine-grained "andesite" dykes of variable orientation, and locally referred to as lamprophyre, apparently represent the youngest intrusive phase.

Drilling in 2005 identified at least two distinct post-minerals dyke phases and confirmed the vertical to subvertical nature of most of these dykes. Precise strike orientations remain to be determined but in the central property area they may be trending both north-northwest and roughly east-west.

Of interest is an intermineral intrusive breccia first recognized in the southern grid area in 1979. The geometry of this breccia zone is not well defined although trenching and limited drilling has suggested a north-northwest trend for the zone with widths of between 10 and 30 metres and an indicated strike length of at least 100 metres. This zone, examined by the writer in 1984 and again in 2004, has characteristics of intrusive breccias typical of most porphyry deposits. Rounded to subangular, closely-spaced, several centimeter clasts of varying lithology are contained in a fine-grained chloritic matrix containing a good percentage of sulphide minerals. Geological investigations in 2003 showed the breccia zone as being central to a northwest-trending, 600 x 300 metres, structurally complex fracture zone.

Other breccia zones, previously identified elsewhere within the complex, have in part been identified as tectonic breccias and some apparent intrusive breccias were identified in 2005 drill cores.

North-northeast striking faults cut and offset both Coast granitic rocks and the intrusive complex. These are thought to post-date mineralization and possibly provided conduits for some of the post-mineral dyke swarms.

Propylitic alteration, present in all phases of the OK intrusive complex, is locally overprinted by potassic, phyllitic and argillic alteration facies.

Mapping of alteration, undertaken in the southern half of the property, completed in the early 1980's, indicated moderate to strong sericite and kaolinite (phyllitic-argillic) alteration centred on the breccia zone and in an area south of the Claim Lake zone.

Elsewhere within the property there is limited evidence of an inner potassic alteration zone developed in quartz diorite (previously referred to as granodiorite) which grades outward to through phyllitic, argillic and propylitic alteration zones typical of

porphyry systems. Meyer in 1976 describes strong quartz-sericite alteration of the central quartz-feldspar porphyry dyke which grades outward to predominantly chlorite-epidote alteration in the bordering quartz "granodiorite".

At least two stages of quartz veining and quartz stockwork development are evident within the OK intrusive complex. Attendant sulphide mineralization consists of pyrite, chalcopyrite and molybdenite with lesser bornite, sphalerite and magnetite occurring in narrow quartz-filled fractures and quartz veinlet stockworks which have a predominant east to northeast trend. Molybdenite occurs as selvages along the margins of quartz veinlets and also coats dry fractures.

Younger quartz veinlet stockworks are best developed in the central, later phase quartz-feldspar porphyry dyke but it is significant that these contain little or no sulphide mineralization. The older, leucocratic quartz diorite ("granodiorite") phase marginal to the quartz-feldspar porphyry hosts the best copper and lesser molybdenum mineralization suggesting that the later intrusive phase may have been the mineralizing unit. The most widespread copper (+molybdenum) mineralization is best developed along the eastern flank of the quartz-feldspar porphyry dyke. Some smaller mineralized zones also occur along the west flank of the dyke; this may be an expression of lesser drill-testing of this area.

Minor pyrite occurs with chalcopyrite and molybdenite but is most widespread in peripheral zones as a typical pyrite halo.

Eight copper-molybdenum zones have been explored by previous drilling over a northerly trend of 5 kilometres. Most of these mineralized zones contain apparent large volumes of low copper (0.10-0.20%) and molybdenum values.

The breccia zone in the southern grid area has demonstrably higher copper grades plus some silver values. Fine- to coarse-grained chalcopyrite, bornite, pyrite and lesser molybdenite occur interstitially between breccia fragments. A chip sample collected from a trench across a 12 metres width within this zone returned values of 2.4% copper and 0.52% MoS₂ (molybdenum disulphide = molybdenite) and a parallel chip sample 12 metres away in less altered material averaged 0.43% copper and 0.08% MoS₂ over a sample length of 6 metres.

DETAILED TECHNICAL DATA and INTERPRETATION

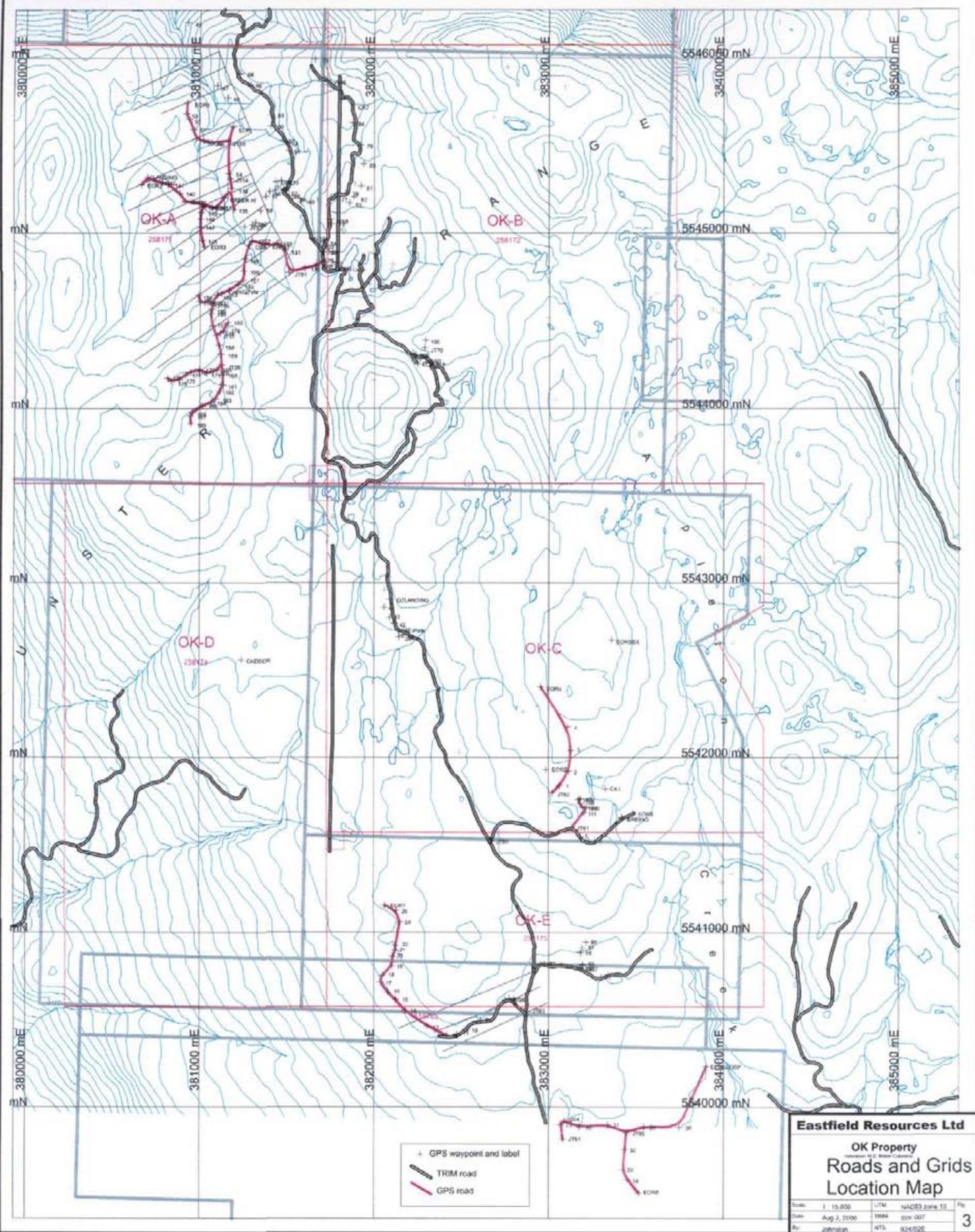
The northernmost grid area, which is immediately northwest of the North Lake Zone, was selected following a review of 2004 airborne geophysical data which had identified geophysical responses similar to those underlying the North Lake Zone. These included a relatively low magnetic response and generally coincident high resistivity readings. A flagged grid consisting of 15 lines at roughly 100 metres intervals was established off part of the original survey baseline. A total of 499 soil samples were collected at 25 metres intervals along the flagged lines and submitted to Acme Analytical Laboratories in Vancouver for 4-acid digestion and the subsequent determination of 35 major and trace elements (including copper and molybdenum) by ICP – emission spectrography procedures.

As illustrated on Figures 3, 4 and 5, enhanced copper and molybdenum values were found throughout the grid area with the highest values being 1244 ppm (parts per million) copper and 534 ppm molybdenum. Significantly, several of these are near the western limits of the sample grid. Molybdenum features a much broader distribution of “anomalous” values with some 90 samples collected throughout the grid area containing values in excess of 27 ppm molybdenum (Figure 5).

A smaller grid, consisting of three flagged lines at 100 metres spacings, was established to further assess the potential of the Southwest Zone situated southwest of the Breccia Zone (Figures 3, 6 and 7). Ninety-nine soil samples, collected at 25 metres intervals, returned only slightly enhanced copper and molybdenum values with the highest values being 115 ppm copper and 52 ppm molybdenum.

RECOMMENDATION

An initial diamond drill test of the new anomaly outlines in the Northwest grid is recommended. This testing should occur concurrent with continued drilling in the North Lake Zone and may require helicopter assistance owing to the deactivation which has occurred to the logging roads existing in this area. More work is also recommended to the area surrounding the South Breccia Zone

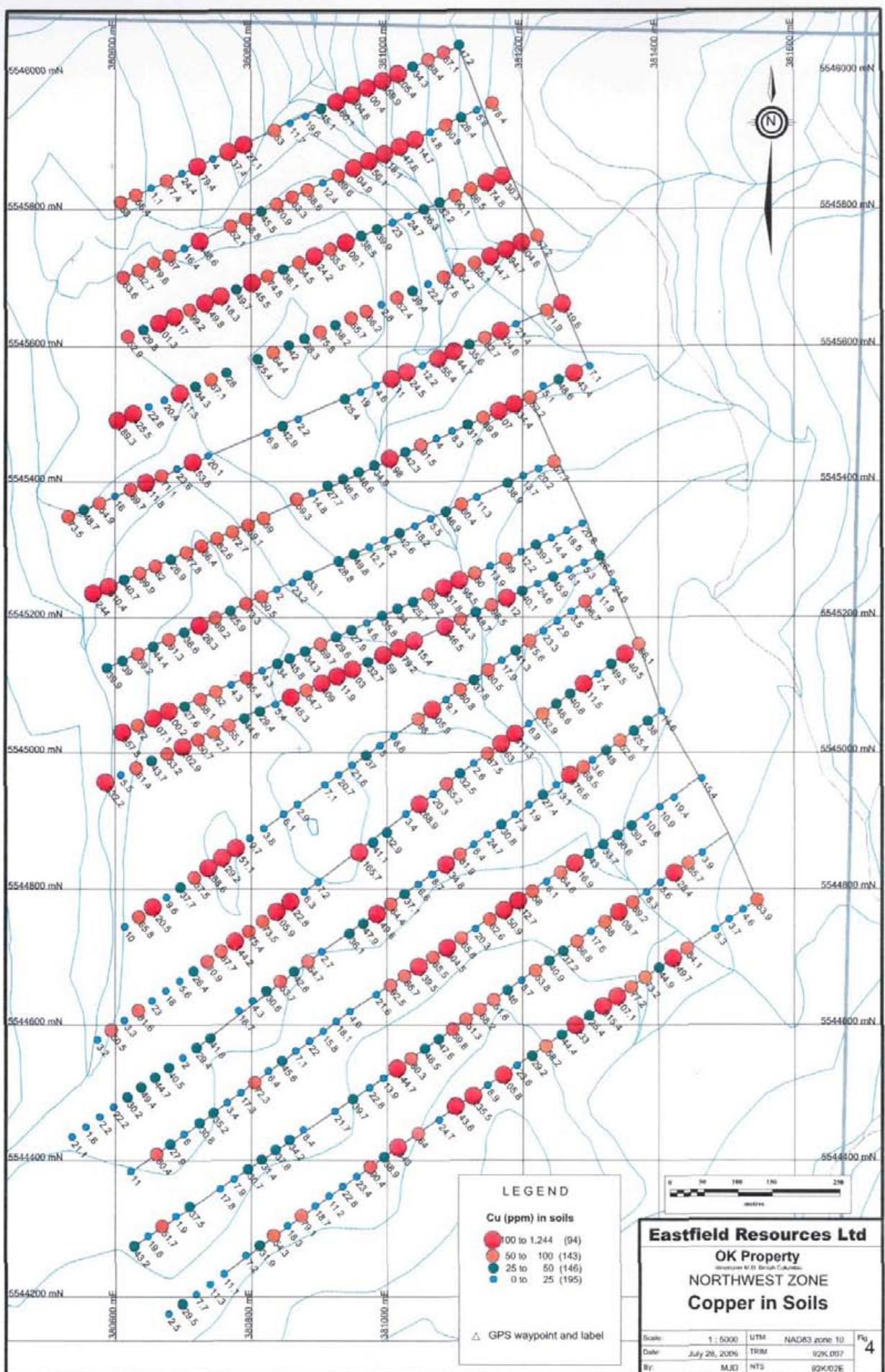


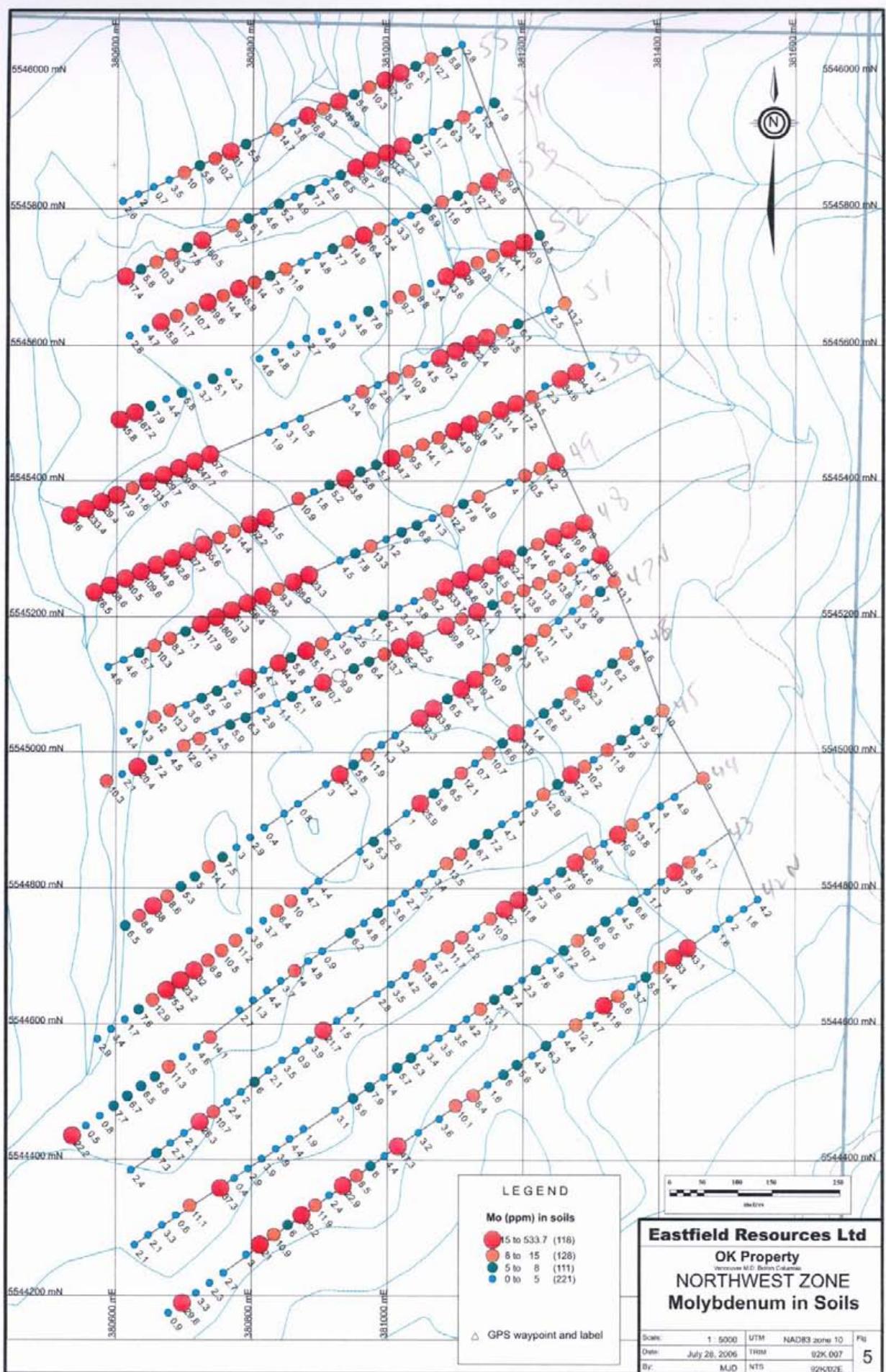
Eastfield Resources Ltd

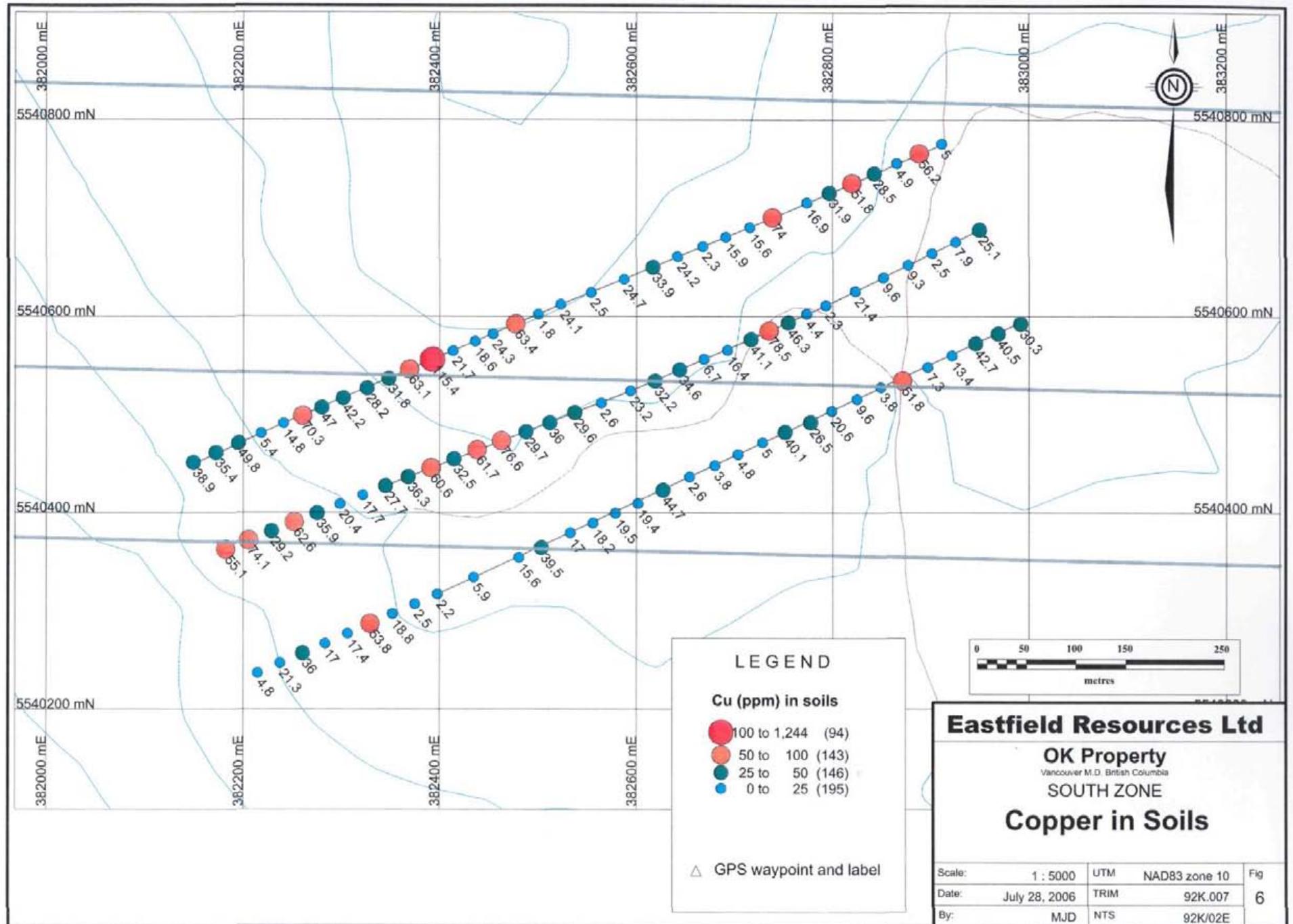
**OK Property
Roads and Grids
Location Map**

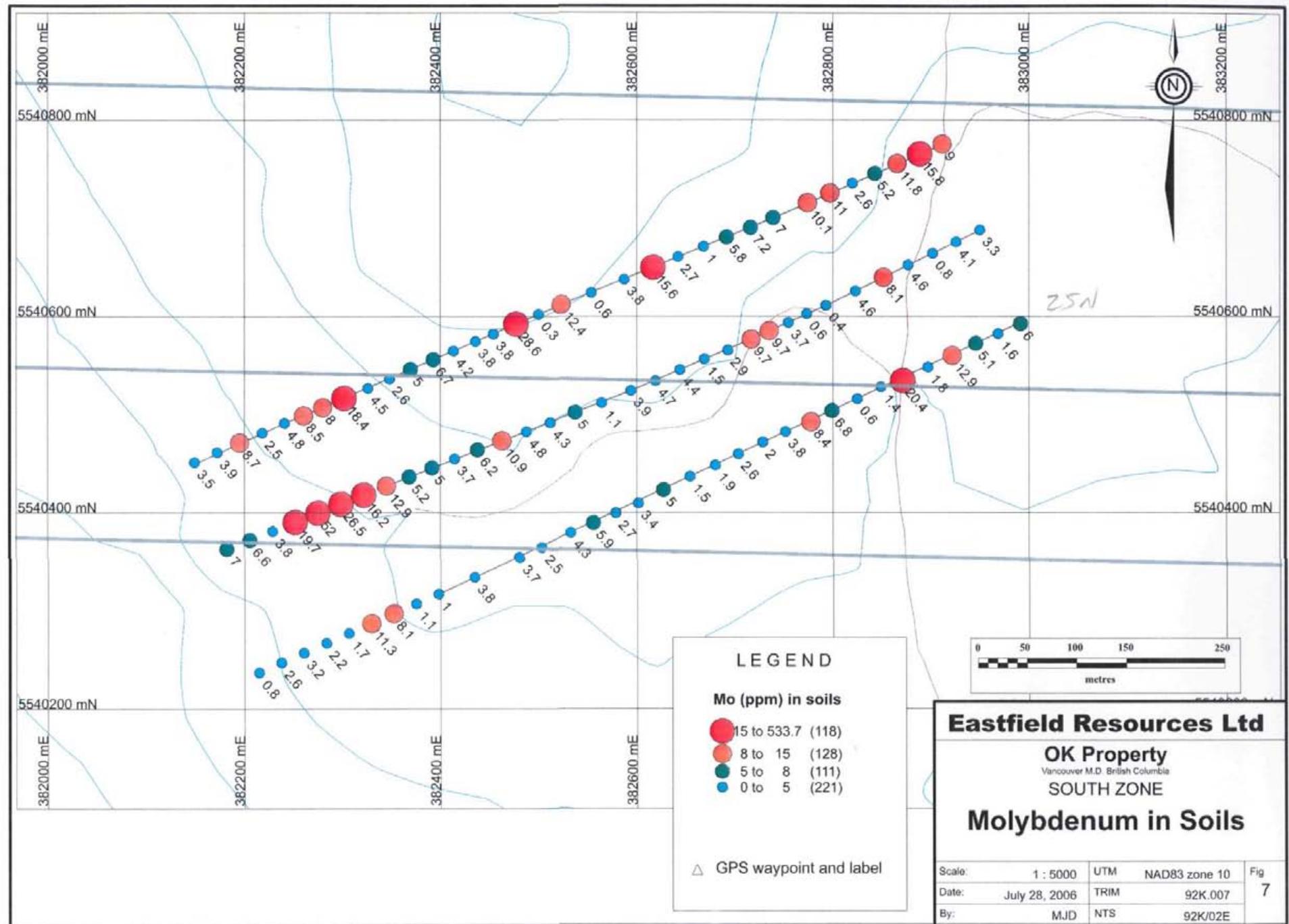
Date: 15.000 UTM HADES zone 13
 Date: Aug 2, 2000 T10R 00N 007
 By: 2000000 NTS 02402E

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ITEMIZED COST STATEMENT**May 23- 24 / 2006**

Number of Days	2	
Number persons on payroll	1	
Number persons requiring room and board	0	
Persons code	BL	
Persons costs		\$1,200

May 25-May 26 / 2006

Number of Days	2	
Number persons on payroll	2	
Number persons requiring room and board	2	
Persons code	BL, JC	
Persons costs		\$1,840
Room and board costs		\$400
Truck Rental, number units, cost	1.5	\$240
ATV Rental, number of units, cost	2	\$280

May 28-May 31 / 2006

Number of Days	4	
Number persons on payroll	3	
Number persons requiring room and board	2	
Persons code	BL, JC, DL	
Persons costs		\$4,960
Room and board costs		\$800
Truck Rental, number units, cost	1.5	\$480
ATV Rental, number of units, cost	2	\$560

June 1-June 15 / 2006

Number of Days	15	
Number persons on payroll	3	
Number persons requiring room and board	2	
Persons code	BL, JC, DL	
Persons costs		\$18,600
Room and board costs		\$3,000
Truck Rental, number units, cost	1.5	\$1,800
ATV Rental, number of units, cost	2	\$2,100

June 16-24 / 2006

Number of Days	9	
Number persons on payroll	3	
Number persons requiring room and board	2	
Persons code	BL, JC, DL	
Persons costs		\$11,160
Room and board costs		\$1,800
Truck Rental, number units, cost	1.5	\$1,080
ATV Rental, number of units, cost	2	\$1,260
Soil Samples	598	\$13,400
Total Costs (this statement)		\$63,760

Total claimed on filing	[\$25,000]
Item cost Schedule	Cost
Bruce Laird, BL	\$600
J.P.Charbonneau, JC	\$320
Dean Louie, DL	\$320
Third Field Assistant , TFA	\$320
Accommodation and Food, per man per day	\$100
Radios, each, per day	\$5
Chainsaw rental, per day	\$10
Pickup truck rental, per day	\$80
ATV Rental, each per Day	\$70
Bulldozer, per hour	\$110
Excavator, per hour	\$120
Analytical Costs, each, per rock sample	\$25
Analytical Costs, each, per soil sample	\$20

AUTHOR QUALIFICATION

JW. (Bill) Morton P.Geo

I, J.W. Morton am a graduate of Carleton University Ottawa with a B.Sc. (1972) in Geology and a graduate of the University of British Columbia with a M. Sc. (1976) in Graduate Studies.

I, J.W Morton have been a member of the Association of Professional Engineers and Geoscientists of the Province of BC (P.Geo.) since 1991.

I, J.W. Morton have practiced my profession since graduation throughout Western Canada, the Western USA and Mexico.

I, J.W Morton supervised the work outlined in this report.

Signed this 15 day of August, 2007

Station	Easting	Northing	Elev	Nad83 Zn10
1	383064	5541838	945	
2	383117	5541921	954	
3	383130	5542039	960	
4	383110	5542174	974	
5	383184	5541546	929	
6	383231	5541520	929	
7	383266	5541522	927	
8	383422	5541652	914	
9	382612	5540494	860	
10	382521	5540441	856	
11	382476	5540414	853	
12	382416	5540408	848	
13	382305	5540460	842	
14	382178	5540547	834	
15	382124	5540613	832	
16	382079	5540654	827	
17	382036	5540714	828	
18	382048	5540752	832	
19	382104	5540807	843	
20	382106	5540860	848	
21	382121	5540897	853	
22	382123	5540924	852	
24	382150	5541058	854	
25	382130	5541126	854	
26	382750	5540612	854	
27	382774	5540618	854	
28	382802	5540616	860	
29	383068	5539898	814	
30	383175	5539883	817	
31	383336	5539896	816	
32	383437	5539755	815	
33	383425	5539642	821	
34	383451	5539585	817	
35	383546	5539886	806	
36	383747	5539881	802	
37	383806	5540018	796	
38	382143	5542691	871	
39	382160	5542702	872	
40	382168	5542701	873	
42	382117	5542770	880	
43	382088	5542803	901	
44	382058	5542861	892	
45	382235	5544308	940	
46	381161	5545774	728	
47	381102	5545842	723	
48	380931	5546203	680	
49	381067	5545516	734	
50	380981	5545537	740	
51	380967	5545590	745	
52	380941	5545649	748	

53	380926	5545681	742
54	381168	5545339	758
55	381433	5545243	813
56	381401	5545235	808
57	381380	5545207	804
58	381350	5545128	795
59	381322	5545060	792
60	381302	5545049	792
61	382951	5540816	849
62	382976	5540815	853
63	383074	5540810	858
64	383181	5540791	858
65	383194	5540817	859
66	383183	5540882	866
67	383192	5540911	868
68	383213	5540943	871
70	383193	5540809	862
71	383300	5540742	852
72	383340	5540756	850
73	381756	5545054	895
74	381712	5544949	882
75	381704	5544891	879
76	381700	5544843	879
77	381773	5545195	890
78	381836	5545225	900
79	381921	5545498	880
80	381937	5545393	888
81	381925	5545268	896
82	381885	5545206	887
83	381859	5545170	889
84	381879	5545626	860
85	381661	5545992	822
86	381232	5545912	749
87	381231	5545909	752
88	381291	5545847	760
89	381409	5545671	789
90	381408	5545608	820
91	381480	5545530	811
92	381489	5545522	788
93	381489	5545522	787
94	381512	5545470	809
95	381467	5545298	814
96	381448	5545266	816
97	381498	5545238	817
98	381511	5545211	822
99	381533	5545196	824
100	381579	5545178	856
101	381646	5544970	848
102	381659	5544959	845
103	381686	5544925	852
104	381708	5544891	853

105	382291	5544388	944
106	383183	5541765	948
107	383171	5541759	948
108	383180	5541738	942
109	383196	5541715	939
110	383213	5541711	939
111	383203	5541685	938
128	381761	5544793	868
129	381669	5544814	854
130	381603	5544799	850
131	381490	5544902	831
132	381452	5544940	829
133	381422	5544926	822
134	381374	5544934	815
135	381197	5545135	792
136	381185	5545253	780
137	381100	5545144	768
138	381071	5545146	769
139	380952	5545178	773
140	380888	5545226	770
141	380820	5545277	776
142	380784	5545288	776
143	380743	5545296	784
144	381021	5545150	776
145	381011	5545117	781
146	381007	5545080	783
147	381006	5545038	784
148	381017	5544959	792
149	381260	5544856	807
150	381253	5544786	816
151	381248	5544734	820
152	381219	5544709	827
153	381123	5544656	840
154	381099	5544649	839
155	381070	5544569	841
156	381062	5544544	846
157	381071	5544475	853
158	381109	5544360	862
159	381120	5544311	868
160	381130	5544190	892
161	381132	5544136	895
162	381113	5544100	897
163	381089	5544055	898
164	381065	5544035	906
165	381016	5544015	914
166	380959	5543974	917
167	380945	5543959	916
168	380948	5543913	917
169	381098	5544221	879
170	381072	5544210	879
171	381038	5544203	880

172	380996	5544224	881
173	380947	5544210	875
174	380919	5544190	876
175	380881	5544166	870
176	380835	5544156	866
177	380815	5544172	865
178	381116	5544430	867
179	381137	5544444	870
180	381160	5544493	873
181	381056	5544617	842
182	381027	5544604	837
183	380996	5544612	833
184	380991	5544648	831
BL Park	382141	5542726	880
CK2	380915	5545181	767 creek crossings
CK4	383090	5539921	815
CK5	381051	5546402	610
CK6	381054	5545516	729
CK7	381883	5545732	850
CK1	383326	5541820	935
CREEK2	383419	5541656	916
CREEK rd	381141	5545202	763
CRK	381284	5544930	796
EOR10	381437	5545291	815 EOR is end of road
EOR3	381027	5544921	797
EOR4	382956	5542403	987
EOP5	382985	5541930	954
EOR6	383482	5541682	912
EOR7	382064	5541155	854
EOP8	383515	5539508	821
EOR9	380931	5545745	742
EOR NLk	382247	5544255	931
EOR	381193	5545605	734
EORSLGS	383902	5540230	802
EORSBX	383361	5542673	984
EOR2	380668	5545275	785
JT50	381712	5544837	863 JT is a road junction
JT51	381510	5544776	848
JT52	381301	5544958	803
JT53	381258	5545037	794
JT54	381177	5545310	776
JT55	381035	5545158	772
JT56	381070	5544601	836
JT57	381094	5544418	860
JT58	381125	5544250	876
JT59	382675	5541524	895
JT60	382954	5541576	931
JT61	383136	5541602	936
JT62	383023	5541798	943
JT63	382878	5540543	866
JT64	383081	5539812	807

JT65	383444	5539852	808
JT66	381164	5545525	731
JT67	383184	5540795	857
JT68	381747	5545077	898
JT69	381732	5545872	833
JT70	382286	5544346	956
LANDING	380702	5545319	788
LN Lake	381798	5544803	860
QZLANDIN	382091	5542908	897
RD	382221	5544315	942
ROAD	382262	5544283	944
WKQZVN	381166	5544673	835
OKDEOR	381240	5542558	854

Grid North	Grid East	UTM East	UTM North	Elevation
0+00	100+00	382913	5540774	854
42+00	106+00	381545	5544784	843
43+00	106+00	381500	5544880	829
44+00	106+00	381461	5544963	828
45+00	106+00	381405	5545062	827
46+05	106+00	381371	5545161	817
47+70	106+00	381333	5545252	779
48+00	106+00	381295	5545340	762
49+00	106+00	381252	5545432	771
50+00	106+00	381211	5545524	748
50+00	107+00	381296	5545575	740
0+00	98+25	382739	5540700	856
51+00	107+00	381259	5545662	736
52+00	107+00	381222	5545761	726
55+00	107+00	381107	5546039	720
55+00	105+75	380992	5546001	659
42+00	100+00	381016	5544420	846
43+00	100+00	380974	5544507	829
42+00	97+00	380759	5544233	819
43+00	96+00	380628	5544274	829
44+00	100+00	380946	5544620	824
44+00	97+10	380709	5544444	826
0+00	96+25	382523	5540612	881
45+00	100+00	380904	5544708	809
45+00	97+75	380719	5544566	816
46+00	100+00	380878	5544796	803
47+00	100+00	380819	5544889	809
44+00	96+00	380618	5544380	1304
47+50	106+00	381313	5545291	822
48+00	101+00	380839	5545132	797
48+00	99+25	380679	5545062	786
49+00	99+25	380632	5545148	815
49+00	98+75	380588	5545126	789
0+00	92+00	382146	5540448	825
50+00	99+25	380590	5545246	766
51+00	99+25	380531	5545349	737
53+00	107+00	381181	5545853	739
53+00	102+75	380779	5545683	725
54+00	107+00	381140	5545949	735
55+00	104+75	380899	5545948	669
55+00	102+00	380656	5545832	737
55+00	101+50	380608	5545811	753
54+00	101+00	380612	5545701	736
1+00S	100+00	382950	5540688	855
1+00S	98+50	382792	5540612	868
2+00S	100+00	382992	5540594	860
2+00S	98+75	382873	5540532	843
2+00	94+00	382398	5540317	835
55+00	105+75	380994	5545990	661
1+00S	96+25	382594	5540524	
42+00	106+00	381544	5544783	837

43+00	106+00	381501	5544885	825
45+00	104+50	381290	5544979	796
46+00	101+75	381028	5544910	795
47+00	102+25	381011	5545025	786
55+00	105+75	380993	5545986	685
0+00	100+00	382910	5540774	858
0+00	93+00	382241	5540491	840
1+00S	93+75	382345	5540427	845
1+00S	97+50	382717	5540577	854
1+00S	98+30	382791	5540609	851
2+00S	98+75	382876	5540544	850

GEOCHEMICAL ANALYSIS CERTIFICATE

Mincord Exploration Consultants Ltd.

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Submitted by: B. Laird

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P ppm	La ppm	Cr ppm	Mg ppm	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.2	2.1	2.8	41	<.1	3.8	3.7	505	1.84	<.5	2.5	<.5	4.1	64	<.1	.1	35	.56	.079	8	14	.54	183	.123	1	.94	.091	.46	<.1	<.01	2.1	.3	.08	4	<.5	
L47N 97+50E	6.5	10.0	4.6	9	<.1	2.2	1.5	54	2.38	.8	.1	5.8	.6	7	.1	.3	.2	114	.07	.009	2	12	.04	12	.160	1	.82	.004	.01	<.1	.05	.7	<.1	.06	12	<.5
L47N 97+75E	8.8	65.8	5.2	24	<.2	3.2	3.0	91	3.45	1.3	.4	2.6	1.9	9	.2	.2	.1	102	.08	.033	2	19	.17	20	.136	<1	3.63	.008	.01	.1	.11	2.2	<.1	.07	13	.6
L47N 98+00E	38.0	120.5	6.2	35	<.4	3.6	3.4	110	3.25	2.3	.4	2.3	1.7	11	.1	.2	.1	92	.10	.035	3	16	.21	22	.156	<1	3.45	.010	.02	.1	.14	2.3	<.1	.07	11	.5
L47N 98+25E	8.6	9.6	3.7	9	<.1	1.5	1.7	54	2.38	1.2	.1	1.1	.5	6	<.1	.2	.1	90	.06	.016	2	9	.05	10	.087	1	1.12	.006	.02	.1	.05	.8	<.1	<.05	13	<.5
L47N 98+50E	5.3	37.7	5.4	20	.2	2.5	2.4	69	2.98	1.7	.5	1.7	2.4	11	.1	.2	.1	80	.08	.046	3	15	.13	22	.109	1	4.46	.010	.02	.1	.16	2.8	<.1	.09	10	.9
L47N 98+75E	5.0	57.5	4.2	25	<.4	3.2	2.6	86	2.70	1.1	.3	1.4	1.1	13	.1	.1	.1	72	.11	.022	3	15	.18	20	.119	<1	2.29	.012	.01	.1	.12	1.4	<.1	.06	10	<.5
L47N 99+00E	14.1	288.6	6.9	40	<.5	4.6	4.4	123	3.58	1.6	1.0	2.3	2.0	12	.2	.2	.1	84	.09	.059	5	16	.30	27	.158	1	6.50	.009	.02	.1	.14	3.7	<.1	.09	12	1.3
L47N 99+25E	7.5	129.2	5.9	23	<.4	2.2	2.0	76	3.78	2.9	.7	1.6	2.2	18	.1	.1	.1	72	.07	.118	4	16	.10	25	.118	<1	>10	.008	.01	.1	.24	4.3	<.1	.15	13	1.8
L47N 99+50E	3.0	151.1	9.8	23	<.2	2.1	1.3	41	2.72	1.3	1.7	1.8	2.3	5	<.1	.1	.1	54	.05	.245	5	15	.08	29	.089	1	>10	.007	.01	<.1	.08	6.2	<.1	.18	14	1.4
L47N 99+75E	2.9	9.7	1.5	5	<.1	.9	1.0	37	.87	<.5	.2	<.5	.4	12	<.1	.2	.1	27	.06	.008	2	5	.02	8	.054	<1	.27	.008	.01	<.1	.01	.4	<.1	<.05	3	<.5
L47N 100+00E	.4	3.8	5.8	3	<.1	.4	.3	45	.26	<.5	.1	<.5	.2	11	.1	.2	.1	23	.12	.013	2	2	.01	8	.041	<1	.32	.003	.01	<.1	.03	.7	<.1	<.05	3	<.5
L47N 100+25E	1.0	6.1	2.7	5	<.1	.9	.5	42	.73	<.5	.1	.7	.6	31	<.1	.2	.1	33	.11	.006	2	4	.01	25	.075	<1	.54	.007	.01	<.1	.02	.3	<.1	<.05	6	<.5
L47N 100+50E	.8	2.9	1.2	12	<.1	1.1	1.3	49	.54	<.5	.1	.5	.4	30	<.1	<.1	<.1	19	.03	.006	1	5	.09	30	.005	<1	.89	.006	.02	<.1	.01	.5	<.1	<.05	6	<.5
L47N 101+00E	3.0	7.1	1.1	5	<.1	1.6	1.7	38	1.08	.7	.1	1.5	.5	11	<.1	.3	<.1	56	.08	.006	3	8	.02	10	.058	1	.25	.006	.02	<.1	.02	.4	<.1	<.05	4	<.5
L47N 101+25E	21.2	20.7	9.6	14	.2	1.6	1.3	47	3.18	1.7	.3	2.2	1.1	10	<.1	.2	.2	90	.07	.036	3	10	.07	16	.139	<1	3.17	.006	.01	<.1	.07	2.2	<.1	<.05	14	<.5
L47N 101+50E	5.8	21.6	6.3	10	<.3	1.9	1.4	49	3.06	1.8	.2	1.6	.9	14	.1	.2	.2	87	.07	.026	3	13	.06	13	.143	<1	1.94	.006	.01	.1	.08	1.3	<.1	<.05	13	<.5
L47N 101+75E	11.9	37.0	4.4	14	<.3	.8	1.3	77	2.28	1.6	.2	1.4	.5	12	<.1	.1	.1	69	.05	.031	3	4	.10	13	.243	1	.60	.006	.01	.1	.03	.5	<.1	<.05	12	<.5
L47N 102+00E	1.3	5.0	2.4	3	<.2	.8	.6	43	.97	.7	.1	1.1	.3	10	<.1	.2	.1	65	.10	.008	2	5	.02	6	.125	<1	.35	.005	<.01	<.1	.02	.7	<.1	<.05	6	<.5
L47N 102+25E	3.2	8.8	1.4	5	<.1	1.4	1.5	50	1.76	<.5	.1	4.4	.4	10	.1	.1	.1	67	.05	.008	2	9	.01	8	.062	1	.24	.005	.01	<.1	.01	.4	<.1	<.05	4	<.5
L47N 102+50E	32.3	98.0	12.0	39	.2	3.2	8.4	833	3.72	1.5	.2	1.4	.5	20	.2	.1	.1	127	.18	.037	2	15	.13	31	.189	<1	1.03	.006	.02	.1	.04	.8	<.1	.09	13	<.5
L47N 102+75E	33.6	305.9	23.4	79	<.3	4.4	36.4	593	1.98	.7	.4	1.1	.2	22	.2	.1	.1	48	.21	.034	3	10	.36	50	.107	1	1.39	.009	.02	.1	.06	1.2	<.1	.06	8	.5
L47N 103+00E	6.5	9.1	2.8	4	<.2	1.5	1.1	30	.68	1.7	.1	29.5	.1	25	.1	.2	.1	31	.06	.012	2	5	.01	30	.019	<1	.79	.004	.01	<.1	.02	.3	<.1	<.05	10	<.5
L47N 103+25E	22.4	80.8	5.0	10	<.2	1.7	1.6	56	2.90	1.5	.2	1.1	.7	12	.1	.2	.2	120	.09	.039	2	10	.08	18	.171	1	1.28	.005	.01	.1	.06	1.0	<.1	<.05	18	<.5
L47N 103+50E	19.7	37.8	5.3	18	<.5	1.6	1.1	72	3.83	2.7	.2	1.6	.3	18	.1	.3	.2	44	.12	.033	2	6	.06	15	.159	<1	1.69	.007	.01	.1	.09	.5	<.1	<.05	14	<.5
L47N 103+75E	10.9	80.5	4.1	17	<.4	1.9	1.7	69	2.37	1.2	.4	3.0	1.3	12	.1	.1	.1	67	.08	.025	3	11	.10	20	.097	1	3.19	.014	.01	<.1	.16	1.9	<.1	<.05	9	.7
L47N 104+00E	8.0	17.9	4.7	9	<.3	1.9	1.1	40	2.74	1.3	.2	2.8	.7	11	.1	.2	.1	88	.08	.030	2	11	.05	8	.126	1	1.34	.006	.01	<.1	.08	1.2	<.1	<.05	14	.5
L47N 104+25E	7.3	41.3	4.9	17	<.3	1.8	1.6	71	2.14	1.5	.4	2.3	1.0	16	.1	.2	.1	65	.09	.038	3	8	.11	22	.104	1	2.35	.008	.02	<.1	.11	1.7	<.1	<.05	10	.6
L47N 104+50E	14.2	75.6	6.5	27	<.1	2.3	1.9	79	3.27	2.3	.7	1.8	2.5	12	.1	.2	.1	55	.08	.091	5	14	.15	29	.105	2	>10	.007	.01	.1	.28	3.9	<.1	.15	11	2.0
RE L47N 104+50E	14.1	72.8	6.5	25	<.1	2.2	1.9	79	3.21	2.3	.7	2.5	2.4	12	.1	.2	.1	54	.08	.096	5	14	.15	28	.101	2	9.90	.007	.01	.1	.28	3.8	<.1	.15	11	1.9
L47N 104+75E	11.0	23.3	7.6	18	<.1	1.4	1.4	55	2.79	1.2	.3	2.3	1.0	10	<.1	.2	.1	77	.08	.024	3	8	.06	16	.099	1	2.10	.006	.01	.1	.07	1.4	<.1	<.05	12	<.5
L47N 105+00E	2.3	2.9	1.0	3	<.1	1.1	1.0	36	1.11	.5	.1	.6	.4	6	<.1	.2	.1	45	.05	.006	2	5	.01	5	.049	2	.16	.005	.01	<.1	.02	.3	<.1	<.05	3	<.5
L47N 105+25E	3.5	3.5	1.5	3	<.1	.6	.5	38	.76	.7	.1	1.2	.6	9	<.1	.2	.1	42	.06	.006	3	3	.01	5	.063	1	.31	.006	.01	<.1	.02	.3	<.1	<.05	5	<.5
L47N 105+50E	13.8	96.7	3.9	30	<.3	4.6	4.0	163	3.36	2.2	.6	2.6	1.8	22	.2	.1	.1	72	.14	.033	4	15	.36	40	.153	<1	3.25	.015	.02	.2	.16	2.2	<.1	.08	10	1.2
L47N 105+75E	7.0	11.9	4.1	7	<.1	2.0	1.5	46	1.38	.7	.2	1.0	.3	20	<.1	.1	.1	50	.10	.016	2	9	.05	18	.070	1	.65	.006	.01	<.1	.05	.6	<.1	<.05	6	<.5
STANDARD DS6	11.6	122.8	29.0	141	.3	25.0	10.9	701</																												



Mincord Exploration Consultants Ltd.

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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.2	2.2	3.2	41	<.1	3.6	4.0	520	1.84	<.5	2.7	.8	4.4	71	<.1	<.1	.1	37	.60	.079	10	15	.55	193	.136	1	1.01	.095	.46	.1	<.01	2.3	.3	<.05	5	<.5
L47N 106+00E	13.1	24.6	5.6	11	<.1	2.3	1.3	66	2.69	.9	.4	2.3	.7	14	.1	.1	.1	74	.10	.022	3	10	.09	18	.142	1	1.62	.007	.02	.1	.06	1.3	<.1	<.05	11	.5
L46N 96+25E	2.9	3.2	1.1	4	<.1	1.3	2.2	31	.85	<.5	.1	2.3	.3	7	.1	.2	<.1	30	.09	.007	2	6	.02	18	.019	2	.43	.007	.03	<.1	.01	.3	<.1	<.05	5	<.5
L46N 96+50E	3.4	50.5	3.5	5	.2	7.4	.7	48	.36	<.5	.7	1.0	<.1	29	.3	.1	.1	6	.36	.130	14	13	.02	55	.004	1	1.80	.010	.01	.1	.20	.3	<.1	.20	1	1.6
L46N 96+75E	1.7	3.3	2.1	5	<.1	1.2	1.7	61	1.43	<.5	.1	1.6	.4	15	<.1	.2	.1	56	.08	.005	2	8	.02	10	.061	<1	.35	.007	.01	<.1	<.01	.3	<.1	<.05	6	<.5
L46N 97+00E	7.6	81.6	8.8	25	.3	3.7	2.8	72	3.67	2.6	.8	3.0	2.3	9	.2	.2	.2	84	.08	.066	9	20	.13	25	.140	2	7.23	.009	.02	.1	.21	5.5	<.1	.09	14	1.4
L46N 97+25E	12.9	23.0	4.2	9	.2	1.5	1.3	60	2.38	1.1	.3	2.4	1.0	8	<.1	.2	.1	85	.08	.015	3	10	.07	11	.132	1	1.68	.007	.01	.1	.08	1.3	<.1	<.05	11	<.5
L46N 97+50E	75.2	18.0	6.1	22	.2	2.2	2.4	90	2.31	.7	.2	4.3	.5	12	<.1	.1	.1	72	.09	.015	3	7	.14	15	.108	1	.92	.006	.01	.1	.03	.8	<.1	<.05	12	<.5
L46N 97+75E	23.2	5.6	5.4	13	<.1	1.0	.9	66	.26	<.5	.2	1.6	.2	22	.1	.1	.1	15	.13	.008	3	3	.06	24	.064	<1	.49	.007	.02	<.1	.02	.6	<.1	<.05	6	<.5
L46N 98+00E	32.0	26.4	6.9	19	<.1	2.5	1.4	89	1.23	1.6	.2	.7	.8	14	<.1	.2	.1	45	.14	.014	3	8	.13	16	.141	1	1.32	.007	.02	.2	.06	1.0	<.1	<.05	12	<.5
L46N 98+25E	8.9	70.9	5.7	16	.3	1.6	1.3	39	2.55	2.6	.6	3.4	1.5	7	.1	.2	.1	54	.06	.078	5	13	.06	17	.066	1	6.03	.007	.02	.1	.13	3.2	<.1	<.05	9	1.6
L46N 98+50E	10.5	87.7	8.7	40	.3	3.0	2.6	110	3.50	2.3	.4	5.8	1.5	13	<.1	.2	.4	98	.11	.039	3	17	.15	24	.097	1	3.47	.008	.02	.1	.05	2.2	<.1	<.05	14	<.5
L46N 98+75E	11.2	144.2	5.0	26	1.0	3.1	2.6	99	2.91	1.8	.4	1.8	1.4	22	.1	.2	.1	73	.11	.036	2	15	.17	34	.127	1	3.77	.011	.02	<.1	.11	2.4	<.1	<.05	11	.5
L46N 99+00E	3.8	75.4	6.2	29	.4	4.6	3.6	105	4.18	2.2	.3	1.6	1.6	10	.1	.2	.1	112	.11	.048	3	23	.22	24	.176	1	4.88	.010	.02	.1	.13	2.4	<.1	<.05	16	.5
L46N 99+25E	3.7	73.5	7.1	17	.2	2.6	2.3	90	3.84	2.0	.5	3.1	1.9	9	.1	.2	.1	96	.09	.034	3	20	.17	18	.151	<1	5.22	.010	.01	<.1	.26	4.1	<.1	<.05	16	1.0
L46N 99+50E	8.4	105.9	6.8	20	.4	2.0	1.4	53	3.18	2.1	.5	1.7	1.7	14	.1	.3	.2	82	.06	.063	4	17	.08	23	.094	<1	5.06	.007	.01	.1	.42	3.4	<.1	<.05	13	1.3
L46N 99+75E	10.0	122.8	7.8	48	.2	4.8	4.3	132	3.89	2.1	.6	2.9	1.8	17	.1	.2	.1	103	.13	.064	3	21	.28	34	.162	1	5.17	.012	.02	.1	.03	3.0	<.1	<.05	15	<.5
L46N 100+00E	4.7	6.3	2.2	9	.2	.9	1.2	43	.78	<.5	.1	<.5	.2	12	<.1	.1	.1	36	.08	.004	2	6	.05	11	.049	1	.89	.010	.02	<.1	.01	.5	<.1	<.05	10	<.5
L46N 100+25E	4.4	7.2	3.4	7	<.1	7.7	1.5	58	1.86	.9	.1	1.0	.5	8	.1	.2	.1	76	.08	.006	3	69	.12	10	.114	<1	.58	.009	.01	<.1	.04	.6	<.1	<.05	10	<.5
RE L46N 100+25E	4.2	7.3	3.0	7	<.1	8.4	1.5	61	1.91	.9	.1	2.6	.5	8	.1	.2	.1	77	.07	.006	3	70	.12	10	.115	1	.58	.008	.01	<.1	.03	.5	<.1	<.05	10	<.5
L46N 101+00E	4.3	1165.7	5.2	46	.3	5.3	4.9	98	.17	<.5	4.2	.6	.1	26	2.3	.1	.1	3	.40	.104	42	6	.02	69	.008	1	1.97	.028	.01	<.1	.22	1.6	<.1	.32	1	4.7
L46N 101+25E	5.3	41.1	7.5	24	.3	2.8	2.2	77	4.28	2.7	.4	.6	1.7	11	.1	.2	.2	94	.09	.043	3	18	.13	26	.143	1	5.69	.012	.01	.1	.30	3.3	<.1	<.05	16	1.3
L46N 101+50E	2.6	32.9	8.1	17	.2	2.4	1.9	54	4.37	3.1	.5	2.5	2.1	7	.1	.2	.1	95	.07	.052	3	21	.10	16	.158	1	8.09	.008	.02	.1	.62	4.6	<.1	.07	16	1.8
L46N 101+75E	1.0	3.4	3.9	5	.2	1.1	1.1	96	1.59	.8	.1	1.3	.3	7	<.1	.2	.1	58	.13	.010	3	9	.02	5	.112	3	.17	.009	.01	<.1	.04	.5	<.1	<.05	3	<.5
L46N 102+00E	26.9	268.9	5.1	101	.2	5.5	8.6	318	2.03	.7	.6	1.7	.3	24	.2	.1	.1	57	.25	.045	5	12	.35	62	.117	2	1.86	.011	.03	.2	.11	1.5	<.1	<.05	13	.6
L46N 102+25E	5.8	20.3	5.2	10	.3	1.9	1.5	57	3.32	1.4	.2	2.9	.6	11	.1	.3	.2	121	.10	.024	3	10	.05	12	.196	1	1.39	.008	.01	<.1	.07	1.1	<.1	<.05	18	<.5
L46N 102+50E	6.5	65.2	5.0	28	.1	3.9	3.7	202	4.01	2.2	.4	1.3	1.9	12	.1	.2	.2	101	.11	.227	3	18	.23	21	.159	1	4.56	.013	.02	.1	.07	2.9	<.1	<.05	15	.6
L46N 102+75E	12.1	32.5	6.3	12	.3	2.6	2.0	72	3.28	2.5	.2	1.6	.6	15	<.1	.3	.2	137	.12	.048	3	12	.09	18	.200	<1	1.02	.009	.02	<.1	.06	.7	<.1	<.05	19	<.5
L46N 103+00E	.7	2.6	.7	4	<.1	.8	6	70	.97	.5	.1	2.0	.4	7	<.1	.1	<.1	32	.08	.005	3	5	.01	4	.046	1	.16	.007	.01	<.1	.01	.3	<.1	<.05	2	<.5
L46N 103+25E	10.7	87.5	6.8	13	.1	2.4	1.4	55	3.63	1.9	.5	2.5	1.7	9	.1	.2	.1	77	.10	.043	2	17	.09	14	.124	1	5.17	.014	.01	.1	.21	2.9	<.1	<.05	12	1.0
L46N 103+50E	6.6	363.0	2.3	15	.1	2.1	1.8	90	.54	1.0	.8	3.4	.4	20	<.1	.1	.1	17	.21	.117	6	6	.17	36	.047	<1	2.89	.015	.02	.1	.05	1.1	<.1	<.05	5	.8
L46N 103+75E	73.9	511.3	7.9	24	1.0	1.3	2.7	119	4.69	2.1	1.0	7.2	1.5	96	.3	.2	.2	45	.12	.054	5	8	.10	87	.128	1	9.05	.039	.03	.1	.27	3.0	<.1	.13	13	2.3
L46N 104+00E	1.4	6.9	.9	5	.1	1.2	1.3	74	1.72	<.5	.1	2.9	.6	9	<.1	.2	.1	83	.06	.006	3	7	.01	5	.075	1	.26	.005	.01	<.1	.01	.4	<.1	<.05	5	<.5
L46N 104+25E	6.6	52.9	7.9	17	<.1	2.2	1.6	54	4.42	3.0	.6	3.0	3.5	8	.1	.2	.2	101	.06	.053	3	19	.10	17	.164	1	6.95	.012	.01	.1	.27	4.9	<.1	<.05	18	1.4
L46N 104+50E	5.3	46.6	7.5	14	.2	2.2	2.0	77	4.56	3.0	.6	1.6	2.7	9	.1	.2	.1	110	.08	.054	4	19	.12	15	.183	1	6.16	.025	.01	.1	.25	3.3	<.1	.07	21	1.4
STANDARD DS6	11.7	124.5	29.3	143	.3	25.3	11.0	702	2.85	21.1	6.6	48.2	3.1	40	6.2	3.5	5.0	56	.86	.082	13	188	.59	165	.080	16	1.95	.078	.16	3.4	23	3.3	1.8	<		



Mincord Exploration Consultants Ltd.

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ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P ppm	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
S-1	.2	2.2	2.9	40	<.1	3.9	3.6	511	1.84	.5	2.5	.8	4.3	68	<.1	<.1	.1	38	.57	.081	10	15	.54	191	.123	1	.96	.089	.43	.1 <.01	2.1	.3 <.05	5	<.5		
L46N 104+75E	8.2	40.8	6.4	23	.4	4.0	2.4	85	4.27	2.6	.4	2.7	1.8	13	.1	.2	.2	101	.09	.038	3	19	.18	27	.191	1	4.87	.012	.02	.1	.41	2.5	<.1 <.05	16	1.2	
L46N 105+00E	52.3	111.5	7.7	36	.8	2.0	2.2	118	5.51	3.7	.3	3.5	.9	88	.2	.2	.2	109	.12	.037	3	10	.17	85	.229	<1	3.65	.023	.01	.1	.14	1.6	<.1 <.05	20	1.0	
L46N 105+25E	3.1	7.4	2.3	5	<.1	1.5	1.6	45	1.68	.5	.1	2.0	.4	8	.1	.3	.1	92	.07	.008	2	10	.03	11	.096	1	.41	.008	.01	<.1	.02	.5	<.1 <.05	6	<.5	
L46N 105+50E	6.2	49.5	3.4	20	.2	2.5	2.3	86	2.34	1.2	.4	2.0	1.2	16	.1	.2	.1	83	.14	.018	5	11	.11	22	.091	1	1.99	.009	.01	.1	.12	1.9	<.1 <.05	9	.8	
L46N 105+75E	8.8	140.5	4.2	24	.2	4.2	3.9	162	2.70	2.0	.8	2.7	2.3	14	.1	.1	.1	71	.11	.038	5	15	.24	30	.111	2	5.07	.012	.01	.2	.21	3.0	<.1 <.05	7	1.6	
L46N 106+00E	4.6	66.1	1.6	3	.1	.9	.6	11	1.26	2.7	.9	4.9	2.1	3	.1	.1	<.1	19	.04	.091	8	12	.02	9	.040	2	>10	.006	<.01	.1	.21	4.4	<.1 <.05	3	2.5	
L45N 95+50E	22.2	21.1	7.5	33	<.1	4.4	3.5	123	3.35	3.1	1.2	2.2	.6	19	<.1	.3	.2	134	.16	.033	5	12	.23	34	.201	1	1.69	.006	.02	.1	.02	1.2	<.1 <.05	24	<.5	
L45N 95+75E	.5	1.6	1.6	4	<.1	.8	.7	39	.97	.5	.2	1.7	.7	6	<.1	.1	<.1	35	.07	.008	2	6	.02	7	.036	2	.32	.007	.02	<.1	.01	.4	<.1 <.05	5	<.5	
L45N 96+00E	.8	2.2	2.7	4	<.1	1.5	1.1	65	1.48	.6	.1	3.5	.7	8	<.1	.3	.1	63	.08	.005	4	10	.03	8	.078	<1	.47	.004	.01	<.1	.02	.5	<.1 <.05	6	<.5	
L45N 96+25E	7.7	22.2	4.0	11	<.1	2.6	2.1	59	3.50	1.3	.2	3.3	.8	12	.1	.3	.1	128	.11	.013	2	15	.07	14	.183	<1	1.64	.007	.01	.1	.05	.9	<.1 <.05	18	<.5	
L45N 96+50E	6.7	30.2	6.1	17	.1	3.2	2.8	80	3.63	2.1	.3	2.5	.9	12	.1	.3	.2	139	.11	.020	3	15	.13	15	.218	<1	2.00	.006	.01	.1	.11	1.3	<.1 <.05	20	.7	
RE L45N 96+50E	6.4	28.3	6.1	16	.2	2.9	2.6	72	3.47	1.9	.2	3.0	.9	10	.1	.3	.2	130	.10	.019	3	15	.13	14	.205	<1	1.86	.006	.01	.1	.12	1.2	<.1 <.05	18	.6	
L45N 96+75E	6.5	49.4	7.6	37	.3	4.6	3.3	107	3.70	2.2	.4	2.1	1.6	13	.1	.2	.2	102	.11	.032	3	19	.21	26	.156	1	3.53	.007	.02	.1	.24	2.0	<.1 <.05	14	.8	
L45N 97+00E	5.8	44.7	7.5	24	.2	3.7	2.9	87	3.91	2.3	.4	8.9	1.6	10	.1	.2	.1	102	.08	.050	3	20	.17	20	.141	<1	5.43	.007	.01	.1	.32	2.9	<.1 <.05	14	1.2	
L45N 97+25E	11.3	40.5	7.4	20	<.1	3.0	2.2	85	3.32	1.8	.4	3.1	1.4	10	<.1	.2	.2	95	.09	.045	3	14	.18	20	.137	<1	3.54	.007	.02	.1	.08	2.8	<.1 <.05	16	.6	
L45N 97+50E	1.5	2.0	6.6	4	<.1	.6	.2	55	.16	<.5	.1	1.2	.4	11	<.1	.2	.2	21	.10	.013	3	3	.02	8	.075	<1	.58	.005	.01	<.1	.03	.6	<.1 <.05	11	<.5	
L45N 97+75E	4.6	29.4	8.0	21	<.1	2.8	2.2	74	4.04	2.3	.4	1.7	1.7	11	<.1	.3	.2	106	.09	.053	3	19	.13	19	.154	<1	4.59	.006	.02	.1	.11	2.6	<.1 <.05	17	.6	
L45N 98+00E	14.1	41.8	5.0	19	<.1	3.4	2.5	89	3.57	2.0	.2	5.0	.7	11	<.1	.3	.2	116	.09	.030	3	16	.14	19	.168	1	1.97	.005	.02	.1	.07	1.0	<.1 <.05	19	<.5	
L45N 98+50E	2.7	18.7	4.4	9	.1	2.0	.7	45	.18	<.5	.3	1.1	<.1	16	.1	.1	10	.10	.023	4	5	.06	41	.014	<1	.63	.007	.02	<.1	.07	.4	<.1 <.05	5	<.5		
L45N 98+75E	1.3	4.3	1.3	5	.1	1.4	1.1	43	1.05	.6	.1	1.8	.4	10	<.1	.2	.1	56	.09	.005	2	4	.04	7	.047	<1	.43	.007	.01	<.1	.01	.5	<.1 <.05	7	<.5	
L45N 99+00E	4.4	30.6	5.4	16	.1	2.3	2.3	74	3.10	1.7	.2	2.6	1.1	10	<.1	.2	.1	106	.09	.030	3	15	.10	16	.115	1	3.34	.007	.01	<.1	.09	2.0	<.1 <.05	18	.6	
L45N 99+25E	3.7	53.7	5.1	21	<.1	3.4	2.8	103	3.20	2.0	.4	2.4	1.4	12	.1	.3	.2	113	.11	.044	2	17	.19	16	.115	1	3.83	.007	.02	.1	.02	1.7	<.1 <.05	15	<.5	
L45N 99+50E	14.0	42.8	5.7	18	.2	1.9	1.5	94	1.97	.6	.2	3.9	.7	12	<.1	.1	.1	61	.11	.014	3	7	.12	17	.079	<1	1.37	.005	.02	<.1	.08	.9	<.1 <.05	9	<.5	
L45N 99+75E	4.8	54.7	4.5	32	<.1	4.6	2.7	169	2.24	1.5	.2	8	.6	20	<.1	.3	.2	73	.23	.025	2	15	.25	22	.089	<1	1.74	.004	.02	.2	.03	1.1	<.1 <.05	14	<.5	
L45N 100+00E	.9	2.7	4.9	5	<.1	1.0	.8	61	.87	.5	.1	.5	.2	13	<.1	.2	.1	49	.12	.008	2	5	.02	6	.053	2	.30	.004	.01	<.1	.03	.7	<.1 <.05	5	<.5	
L45N 100+25E	6.2	36.1	4.5	23	.3	2.4	2.4	86	3.53	1.9	.4	2.2	.8	13	.3	.2	.1	109	.13	.030	3	11	.12	21	.142	1	3.00	.007	.02	.1	.18	2.0	<.1 <.05	14	.9	
L45N 100+50E	4.8	47.9	5.0	20	.3	2.5	2.3	81	2.70	1.3	.4	2.7	1.2	24	.1	.1	.1	71	.10	.029	3	12	.13	35	.103	1	3.36	.008	.01	.1	.16	1.9	<.1 <.05	10	1.1	
L45N 100+75E	6.1	149.6	4.8	97	.4	5.5	16.4	675	2.33	.9	.3	.8	.4	23	.4	.1	.1	61	.21	.022	4	14	.34	38	.085	1	1.25	.009	.02	.1	.05	1.4	<.1 <.05	6	<.5	
L45N 101+00E	3.6	64.4	6.5	25	.4	2.2	2.3	82	2.85	1.2	.5	2.0	1.7	13	.2	.1	.1	82	.11	.026	3	14	.12	23	.093	1	3.54	.009	.01	.1	.27	2.5	<.1 <.05	10	1.2	
L45N 101+25E	2.7	37.1	6.3	18	.2	1.9	1.6	55	3.63	2.0	.4	1.7	1.7	7	.1	.2	.1	84	.07	.042	3	17	.10	18	.103	1	5.76	.007	.01	.1	.21	4.5	<.1 <.05	12	1.2	
L45N 101+50E	2.1	6.6	2.6	7	<.1	1.1	1.1	60	1.83	<.5	.1	2.1	.3	9	.1	.1	.2	82	.08	.010	2	6	.03	10	.087	1	.47	.005	.01	<.1	.04	.6	<.1 <.05	9	<.5	
L45N 101+75E	3.4	8.7	3.2	6	.1	.9	.3	47	.26	<.5	.1	1.2	.2	13	.1	.1	.1	26	.08	.011	2	3	.04	19	.065	<1	.50	.006	.01	<.1	.02	.4	<.1 <.05	8	<.5	
L45N 102+00E	13.5	134.8	3.4	12	.3	1.5	1.5	104	3.04	1.3	.2	5.5	2.3	4.5	.6	.1	.1	67	.07	.043	5	6	.12	17	.174	1	4.41	.012	.02	<.1	.28	2.5	<.1 <.05	12	.8	
L45N 102+25E	11.0	81.9	4.9	11	.3	1.6	1.4	82	3.40	1.3	1.4	2.6	2.8	9	<.1	.2	.1	81	.08	.035	4	10	.10	14	.141	<1	3.28	.009	.01	<.1	.16	2.0	<.1 <.05	13	.7	
STANDARD DS6	11.7	124.8	29.5	143	.3	25.0	10.9	702	2.85	21.2	6.7	48.4	3.1	39	6.2	3.5	5.0	55	.85	.080	14	187	.59	165	.064	16	1.94	.078	.14	3.4	.23	3.2	1.8	<.05	7	4.6

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



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ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P % ppm	La ppm	Cr ppm	Mg % ppm	Ba % ppm	Ti % ppm	B % ppm	Al % ppm	Na % ppm	K % ppm	W ppm	Hg ppm	Sc ppm	Tl ppm	S % ppm	Ga ppm	Se ppm
G-1	.2	2.3	2.9	40 <.1	3.8	3.8	478	1.81	<.5	2.4	.7	4.0	58	<.1	<.1	.1	36	.54	.080	8	14	.54	176	.123	2	.94	.089	.45	<.1<.01	1.9	.3	.08	4	<.5		
L45N 102+50E	6.7	8.4	3.4	6 .1	1.9	.9	47	1.05	.7	.2	.9	.2	5	.1	.1	33	.06	.017	2	5	.06	10	.042	1	.62	.006	.01	<.1	.06	.4	<.1	.08	4	<.5		
L45N 102+75E	7.2	24.7	6.1	9 .2	1.8	1.3	46	3.33	1.4	.3	2.6	1.2	8	<.1	.2	.2	94	.06	.029	2	13	.06	9	.112	1	2.15	.005	.01	<.1	.05	1.6	<.1	.07	12	<.5	
L45N 103+00E	4.7	30.8	6.5	18 .3	3.9	2.5	77	3.86	3.3	.3	2.1	2.2	7	.1	.3	.1	114	.10	.044	2	23	.15	13	.154	2	3.69	.007	.02	.1	.32	2.1	<.1	.10	16	.9	
L45N 103+25E	4.0	7.3	3.4	5 <.1	1.8	1.2	51	1.39	.8	.1	4.8	.6	8	<.1	.2	.1	65	.05	.008	3	10	.05	7	.107	1	.38	.005	.01	<.1	.02	.4	<.1<.05	6	<.5		
L45N 103+50E	3.0	1.9	1.0	3 <.1	.9	1.0	74	1.12	<.5	.1	1.7	.5	4	<.1	.2	.1	53	.04	.002	2	7	.01	4	.056	1	.16	.004	.01	<.1<.01	.2	<.1<.05	3	<.5			
L45N 103+75E	12.9	27.4	3.1	5 <.1	1.6	.5	42	.29	.5	.2	2.1	.3	8	.1	.2	.1	24	.06	.010	2	6	.05	12	.059	1	.82	.005	.01	<.1	.05	.8	<.1<.05	8	<.5		
L45N 104+00E	6.3	13.1	1.6	4 <.1	1.3	1.1	44	1.90	1.1	.1	1.5	.3	10	<.1	.3	.1	110	.07	.007	2	8	.02	9	.105	1	.50	.005	<.01	<.1	.01	.5	<.1<.05	11	<.5		
L45N 104+25E	47.2	876.6	4.5	73 .3	4.5	14.0	264	4.71	3.6	1.3	2.5	1.8	41	.1	.2	.2	69	.17	.070	5	14	.30	100	.113	1	7.50	.009	.03	.4	.20	4.1	<.1	.13	10	1.9	
RE L45N 104+50E	10.5	68.2	6.8	29 <.1	3.3	3.9	163	3.15	2.3	.6	2.9	1.2	22	.1	.2	.1	91	.16	.048	4	14	.29	33	.192	1	4.23	.010	.02	.1	.11	3.9	<.1	.06	13	1.3	
L45N 104+50E	10.2	68.5	6.8	30 <.1	3.0	3.9	168	3.15	2.3	.6	3.0	1.2	23	.1	.2	.1	94	.18	.050	4	15	.31	34	.194	1	4.22	.011	.02	.1	.10	3.9	<.1<.05	14	1.3		
L45N 104+75E	2.0	3.6	1.7	4 <.1	1.0	.9	54	1.17	.5	.1	4.0	.5	8	<.1	.2	.1	61	.07	.005	2	6	.01	8	.075	1	.24	.005	.01	<.1	.01	.4	<.1<.05	3	<.5		
L45N 105+00E	11.8	48.0	6.4	22 .1	2.5	1.8	60	3.63	3.0	.3	2.0	.7	17	.1	.3	.2	107	.11	.025	3	11	.10	26	.118	<1	2.11	.006	.02	.1	.13	1.1	<.1<.05	20	.9		
L45N 105+25E	7.6	52.8	5.9	19 .1	2.3	2.1	71	3.74	2.8	.5	2.3	2.8	9	.1	.2	.1	77	.07	.034	3	17	.12	19	.129	<1	5.49	.008	.01	.1	.32	2.5	<.1	.07	11	1.6	
L45N 105+50E	7.5	25.4	6.3	14 <.1	2.1	1.5	57	5.36	2.3	.3	.9	1.2	9	.1	.3	.2	136	.08	.027	2	13	.09	14	.205	1	2.94	.006	.01	.1	.17	1.9	<.1	.06	23	.7	
L45N 105+75E	6.4	38.0	5.3	10 <.1	2.5	1.7	67	2.72	1.6	.3	1.7	.9	11	.1	.2	.2	103	.09	.021	4	14	.10	17	.145	1	2.20	.006	.01	.1	.14	1.9	<.1<.05	15	.7		
L45N 106+00E	10.0	14.6	4.9	9 <.1	1.3	.9	65	.27	.6	.2	1.3	.3	16	<.1	.2	.1	25	.11	.013	2	5	.10	16	.114	1	.60	.007	.02	.1	.04	.7	<.1<.05	10	<.5		
L44N 96+00E	2.4	11.0	2.9	10 <.1	2.9	1.6	57	2.03	1.1	.1	1.6	.5	9	<.1	.2	.1	81	.07	.024	2	13	.07	12	.105	1	.97	.007	.01	<.1	.03	.6	<.1<.05	9	<.5		
L44N 96+50E	7.3	60.4	5.2	24 .2	3.0	2.7	102	4.58	2.8	.3	1.6	.9	19	.2	.2	.2	146	.13	.030	2	15	.17	23	.233	<1	2.23	.008	.02	.1	.08	1.1	<.1<.05	20	.5		
L44N 96+75E	2.7	27.9	5.4	17 <.1	2.9	2.0	63	3.73	3.9	.2	1.6	1.0	9	.1	.4	.1	102	.07	.029	2	20	.12	13	.151	1	2.84	.007	.02	<.1	.21	1.9	<.1<.05	13	.7		
L44N 97+00E	2.1	6.0	2.0	5 <.1	1.8	1.3	52	1.74	.5	.1	4.2	.6	6	<.1	.2	.1	82	.09	.005	2	11	.03	8	.092	<1	.46	.003	.01	<.1	.03	.4	<.1<.05	7	<.5		
L44N 97+25E	26.3	30.6	5.4	14 .1	2.0	1.4	53	2.51	1.3	.3	10.4	.6	9	.1	.2	.2	95	.08	.023	3	11	.08	16	.121	<1	1.75	.006	.01	.1	.12	.8	<.1<.05	13	.8		
L44N 97+50E	10.7	35.2	3.8	15 <.1	3.1	2.3	70	2.83	1.3	.3	2.7	1.0	9	<.1	.2	.1	99	.07	.030	2	17	.11	11	.144	1	2.24	.005	.01	.1	.05	.9	<.1<.05	12	<.5		
L44N 97+75E	2.4	3.4	1.1	3 <.1	.9	.7	46	1.06	<.5	.1	4.6	.3	6	<.1	.1	.1	50	.04	.006	2	6	.01	4	.056	1	.28	.005	.01	<.1	.01	.3	<.1<.05	5	<.5		
L44N 98+00E	2.0	17.3	5.0	13 <.1	1.7	1.0	55	2.09	.7	.3	1.5	1.1	7	<.1	.1	.1	56	.08	.019	3	11	.05	12	.048	<1	1.90	.007	.01	<.1	.03	1.6	<.1<.05	9	<.5		
L44N 98+25E	6.0	72.3	4.2	19 .3	2.8	2.4	88	2.75	1.3	.5	2.7	2.0	10	.1	.2	.1	68	.07	.034	2	14	.18	24	.097	<1	3.71	.010	.01	.1	.43	2.6	<.1	.08	9	1.2	
L44N 98+50E	2.1	6.4	3.5	7 <.1	1.5	.7	38	1.87	.6	.1	2.6	.8	5	<.1	.1	.1	60	.04	.017	2	10	.03	13	.066	<1	1.48	.004	.01	<.1	.03	.9	<.1<.05	8	<.5		
L44N 98+75E	3.5	45.6	6.5	21 .4	3.5	2.5	68	3.75	2.4	.5	1.1	2.1	6	.1	.2	.1	79	.06	.055	2	20	.14	19	.124	1	8.20	.008	.01	.1	.40	3.6	<.1	.12	11	1.7	
L44N 99+00E	.9	7.1	5.2	10 <.1	2.2	1.3	83	.83	.6	.1	<.5	.2	41	<.1	.2	.1	47	.21	.014	2	5	.09	24	.084	<1	.63	.008	.02	<.1	.02	1.0	<.1<.05	5	<.5		
L44N 99+25E	3.9	22.0	4.2	19 .1	1.5	1.1	65	1.59	.8	.2	1.0	.8	14	.1	.2	.1	55	.11	.011	3	7	.06	16	.050	1	1.34	.007	.01	<.1	.06	.8	<.1<.05	8	<.5		
L44N 99+50E	21.7	15.8	4.7	16 .1	2.4	1.4	62	1.61	.7	.2	3.9	.5	11	.1	.2	.2	73	.08	.007	2	8	.08	18	.126	<1	.93	.005	.01	<.1	.03	.6	<.1<.05	15	<.5		
L44N 99+75E	1.5	18.1	2.3	7 .1	1.4	1.2	45	1.59	<.5	.2	3.2	.5	7	.1	.1	.1	56	.06	.008	2	9	.02	8	.056	<1	.82	.004	.01	<.1	.04	.5	<.1<.05	5	<.5		
L44N 100+00E	1.1	4.6	1.8	4 <.1	1.6	1.3	52	1.35	<.5	.1	3.3	.4	8	<.1	.2	.1	60	.07	.005	2	8	.01	8	.072	<1	.32	.005	.01	<.1	.01	.4	<.1<.05	5	<.5		
L44N 100+25E	2.8	21.6	3.6	12 .2	2.6	1.6	60	2.66	1.7	.2	4.8	1.1	9	<.1	.2	.1	85	.08	.037	2	14	.09	11	.111	1	2.15	.007	.01	<.1	.10	1.3	<.1	.06	12	<.5	
L44N 100+50E	3.5	92.5	4.0	15 .5	2.2	1.3	63	1.67	3.2	1.0	5.0	2.3	6	.1	.1	.1	40	.06	.095	5	16	.08	13	.061	2	9.90	.006	.01	.1	.43	5.0	<.1	.13	6	2.6	
STANDARD DS6	11.6	124.7	29.8	142 .3	25.3	10.9	706	2.85	20.9	6.6	48.4	3.0	40	6.0	3.5	5.0	56	.85	.079	13	188	.58	163	.080	18	1.87	.075	.16	3.5	.23	3.3	1.8<.05	6	4.3		

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data *hfa*



Mincord Exploration Consultants Ltd.

FILE # A602790

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ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca ppm	P % ppm	La ppm	Cr ppm	Mg ppm	Ba ppm	Ti % ppm	B % ppm	Al % ppm	Na % ppm	K % ppm	W ppm	Hg ppm	Sc ppm	Tl ppm	S % ppm	Ga ppm	Se ppm
G-1	.2	2.0	3.0	40	<.1	3.5	3.7	507	1.76	<.5	2.7	.6	4.3	.68	<.1	<.1	.1	36	.58	.079	9	14	.52	190	.132	2	.97	.101	.45	.1<.01	2.1	.3<.05	5	<.5		
L44N 100+7SE	4.2	86.7	4.9	22	.4	2.8	2.6	86	3.46	2.0	.6	1.2	2.8	10	.2	.2	.1	68	.07	.059	4	19	.17	24	.108	1	7.80	.011	.01	.1	.36	4.2	<.1	.08	9	1.8
L44N 101+00E	13.8	139.5	5.2	61	.2	4.0	3.6	146	3.30	2.0	.4	1.6	1.4	19	.3	.2	.1	81	.16	.039	3	16	.27	38	.129	1	3.39	.010	.02	.1	.08	1.9	<.1	.06	12	.6
L44N 101+25E	2.7	65.5	3.9	42	.3	2.1	2.4	105	2.00	.9	.3	.8	.7	23	.1	.2	.1	57	.18	.016	3	7	.15	29	.050	<1	2.45	.007	.01	.1	.10	1.7	<.1<.05	10	<.5	
L44N 101+50E	11.7	304.5	5.6	49	<.1	2.8	2.2	124	.60	1.0	.6	1.3	.2	29	.2	.1	.1	30	.33	.049	4	9	.18	73	.068	1	1.85	.011	.02	.1	.10	1.3	<.1	.06	10	.6
L44N 101+7SE	12.2	65.8	6.8	27	.2	2.4	2.3	105	.42	<.5	.2	.6	.1	21	.1	.2	.1	27	.17	.026	2	6	.22	58	.011	1	1.33	.007	.02	.1	.04	1.2	<.1<.05	11	<.5	
L44N 102+00E	3.0	20.3	2.9	7	.2	1.8	.8	40	.70	.9	.2	1.0	.2	22	<.1	.4	.1	33	.12	.017	2	6	.04	19	.042	1	.98	.009	.01	.1	.02	.5	<.1<.05	11	<.5	
RE L44N 102+25E	11.4	63.4	5.3	13	.3	2.7	2.0	68	2.84	2.3	.4	1.6	1.3	13	.1	.2	.1	77	.10	.032	3	13	.12	20	.085	1	2.85	.009	.02	<.1	.13	2.2	<.1<.05	12	.7	
L44N 102+25E	10.9	62.6	5.1	13	.3	2.5	2.0	69	2.93	2.2	.4	2.6	1.2	13	.1	.2	.1	81	.10	.030	3	13	.12	20	.085	1	2.82	.009	.02	.1	.12	2.2	<.1<.05	12	.8	
L44N 102+50E	22.0	150.9	5.0	14	.5	3.2	2.1	88	2.10	1.5	.5	1.6	.9	14	.5	.1	.1	54	.12	.048	4	13	.13	28	.102	1	3.00	.010	.02	.1	.15	1.8	<.1<.05	9	1.2	
L44N 102+7SE	31.8	212.7	4.9	33	.2	4.0	4.3	196	1.93	1.5	.5	1.2	.9	21	.3	.1	.1	44	.16	.030	4	11	.36	46	.145	1	2.74	.012	.02	.2	.08	1.7	<.1<.05	11	.6	
L44N 103+00E	7.3	58.0	6.3	22	.3	2.6	2.3	89	4.24	3.0	.5	1.4	2.0	12	.1	.2	.1	95	.10	.039	3	18	.15	20	.179	<1	6.10	.009	.01	.1	.08	2.5	<.1	.08	16	.5
L44N 103+25E	2.9	6.1	1.6	5	.4	1.0	.8	51	1.20	<.5	.1	4.9	.3	16	<.1	.2	.1	46	.07	.007	2	5	.01	11	.073	2	.21	.007	.01	<.1	.02	.3	<.1<.05	3	<.5	
L44N 103+50E	7.8	64.8	4.3	21	.5	1.1	1.7	57	1.74	1.5	.2	<.5	.3	29	.2	.3	.1	41	.12	.017	2	4	.10	30	.018	1	2.18	.007	.02	.1	.06	1.0	<.1<.05	9	<.5	
L44N 103+7SE	84.6	116.9	9.4	29	.2	2.2	2.0	100	8.10	4.4	.2	1.1	.6	16	<.1	.5	.2	258	.13	.042	2	11	.12	18	.185	1	1.26	.007	.02	.1	.07	.7	<.1<.05	20	.5	
L44N 104+00E	8.8	43.0	6.4	19	<.1	3.0	2.5	103	4.07	1.9	.4	1.4	2.1	17	.1	.2	.2	123	.11	.027	3	17	.14	33	.220	<1	3.14	.009	.02	.1	.05	2.0	<.1<.05	15	.5	
L44N 104+25E	4.0	33.7	3.3	9	.2	2.0	2.1	91	2.10	1.5	.3	1.5	1.6	13	.1	.2	.1	61	.15	.011	2	12	.19	9	.136	<1	1.88	.007	.01	.1	.13	2.0	<.1<.05	7	<.5	
L44N 104+50E	15.9	30.6	2.7	24	.3	2.2	1.3	107	2.08	1.1	.2	1.1	.4	21	<.1	.1	.1	64	.09	.012	2	9	.17	33	.062	1	1.31	.005	.01	.1	.05	.7	<.1<.05	10	<.5	
L44N 104+7SE	13.8	30.5	4.9	17	.2	3.1	1.2	64	2.15	1.5	.2	1.7	.7	29	.1	.2	.1	61	.08	.016	3	11	.07	43	.088	<1	2.02	.008	.02	<.1	.18	1.1	<.1<.05	12	.5	
L44N 105+00E	4.1	10.8	2.8	6	.1	2.3	1.2	52	1.77	.7	.2	.9	.4	7	<.1	.2	.1	74	.06	.010	2	11	.02	6	.085	1	.90	.005	.01	<.1	.08	.8	<.1<.05	8	<.5	
L44N 105+25E	4.0	10.9	2.7	5	.1	2.2	1.2	52	1.75	.7	.2	4.1	.4	6	<.1	.2	.1	71	.06	.010	2	11	.02	6	.083	1	.86	.005	.01	<.1	.08	.7	<.1<.05	8	<.5	
L44N 105+50E	4.9	19.4	5.5	11	.3	2.1	1.4	66	3.00	1.3	.3	1.5	1.1	9	.1	.3	.2	109	.10	.014	3	13	.05	10	.187	<1	1.95	.006	.01	<.1	.19	1.3	<.1<.05	15	.5	
L44N 106+00E	9.0	15.4	7.9	10	.1	2.2	1.4	66	2.12	.7	.2	1.1	.6	10	<.1	.3	.2	115	.08	.008	3	11	.04	11	.191	<1	.63	.005	.01	<.1	.02	.6	<.1<.05	13	<.5	
L43N 96+00E	2.1	43.2	6.4	21	.1	3.2	2.4	84	3.48	2.4	.6	1.4	2.6	10	.1	.2	.1	79	.10	.047	4	20	.15	18	.136	1	5.80	.010	.02	.1	.19	4.0	<.1	.07	11	1.1
L43N 96+25E	2.1	19.6	4.9	16	.2	2.2	1.9	66	2.29	1.7	.4	1.4	1.6	19	.1	.2	.1	61	.08	.041	3	10	.07	41	.068	<1	3.11	.007	.02	<.1	.11	1.4	<.1<.05	11	<.5	
L43N 96+50E	3.3	51.7	6.3	29	.2	4.3	3.4	129	2.99	2.3	.6	3.3	2.1	15	<.1	.2	.1	75	.14	.034	3	18	.27	23	.142	<1	4.00	.010	.02	.1	.16	2.4	<.1<.05	10	.5	
L43N 96+7SE	.6	1.9	4.5	6	<.1	1.5	.5	77	.61	.7	.1	<.5	.5	37	<.1	.5	.1	49	.45	.006	2	7	.03	8	.085	<1	.77	.006	.01	<.1	.02	1.7	<.1<.05	7	<.5	
L43N 97+00E	11.1	37.5	6.3	54	.3	3.8	24.1	883	1.95	3.5	1.5	.5	.1	17	.3	.1	.1	39	.20	.073	10	9	.11	38	.032	1	4.60	.012	.02	.1	.15	1.2	.1	.10	5	1.8
L43N 97+50E	37.3	17.8	5.7	16	.2	4.5	2.3	74	3.91	1.9	.2	1.6	.7	15	<.1	.2	.2	127	.14	.019	3	19	.11	16	.210	<1	1.39	.007	.02	<.1	.08	1.5	<.1<.05	21	<.5	
L43N 97+7SE	.4	7.9	3.0	8	.1	1.6	2.1	104	2.18	.7	.2	<.5	.5	12	<.1	.1	.1	69	.14	.009	2	4	.09	7	.117	1	.32	.020	.02	<.1	.02	.4	<.1<.05	4	<.5	
L43N 98+00E	2.9	30.7	5.3	14	.2	2.4	1.8	68	2.63	1.7	.3	1.9	.6	17	.1	.1	.1	79	.16	.034	4	10	.08	16	.107	<1	1.78	.006	.01	<.1	.11	1.4	<.1<.05	12	.7	
L43N 98+25E	3.9	31.4	5.5	33	.2	3.5	3.1	105	3.33	1.6	.3	1.1	1.5	13	.1	.2	.1	91	.13	.034	3	16	.17	23	.119	<1	3.96	.009	.01	.1	.06	2.0	<.1<.05	11	<.5	
L43N 98+50E	3.9	37.8	7.9	33	.1	3.6	3.0	88	3.74	1.9	.5	1.7	1.9	10	<.1	.2	.2	74	.09	.073	3	17	.15	29	.104	<1	7.20	.009	.04	.1	.08	2.7	<.1	.06	14	.7
L43N 98+7SE	4.4	34.2	5.4	17	.1	2.6	2.3	81	3.39	1.7	.3	1.2	.9	11	.1	.2	.2	95	.10	.037	3	14	.14	21	.139	<1	2.56	.007	.02	<.1	.20	1.8	<.1<.05	17	.6	
L43N 99+00E	1.9	8.4	3.1	18	.1	4.7	2.4	83	1.22	.6	.2	.8	.4	50	.1	.2	.1	47	.23	.009	3	13	.14	40	.060	<1	1.28	.008	.04	<.1	.01	.9	<.1<.05	10	<.5	
STANDARD DS6	11.7	125.1	29.7	144	.3	25.7	11.1	699	2.85	21.1	6.6	48.6	3.1	40	6.2	3.5	5.0	56	.85	.080	13	186	.58	166	.079	17	1.94	.074	.16	3.5	.23	3.3	1.8<.05	7	4.5	

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns



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ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca ppm	P %	La ppm	Cr ppm	Mg ppm	Ba ppm	Ti ppm	B %	Al %	Na %	K %	W %	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.2	2.4	3.0	41	<.1	3.8	3.8	534	1.85	<.5	2.6	1.3	4.4	69	<.1	<.1	.1	38	.57	.079	9	15	.57	187	.127	2	1.03	.097	.47	.1<.01	2.3	.3	.06	5	<.5	
L43N 99+50E	3.1	21.7	3.6	15	.2	1.6	1.6	88	2.19	.7	.2	2.0	.9	11	.1	.1	.1	78	.12	.011	3	9	.08	16	.096	1	1.54	.008	.01	<.1	.08	1.3	<.1	.07	10	<.5
RE L43N 99+50E	3.0	21.9	3.6	16	.2	1.8	1.5	86	2.12	.7	.3	2.0	.9	11	.1	.1	.1	78	.12	.011	3	10	.08	15	.095	<1	1.53	.007	.01	<.1	.07	1.3	<.1	<.05	10	<.5
L43N 99+75E	5.6	39.7	4.7	19	.3	2.3	1.7	84	2.66	1.6	.3	2.3	1.2	11	<.1	.2	.1	78	.11	.019	3	14	.11	22	.065	1	2.85	.009	.01	<.1	.14	1.5	<.1	.07	9	.6
L43N 100+00E	7.9	22.8	4.2	13	.3	1.7	1.7	84	2.67	.8	.2	2.6	1.1	8	.1	.2	.1	88	.07	.015	3	10	.10	10	.116	<1	1.59	.006	.01	<.1	.12	.9	<.1	<.05	11	.6
L43N 100+25E	4.4	13.9	2.8	12	<.1	1.6	2.5	87	2.13	.8	.1	1.7	.5	12	<.1	.2	.1	94	.14	.012	2	9	.06	9	.099	3	.34	.007	.02	<.1	.02	.7	<.1	<.05	6	<.5
L43N 100+50E	5.7	144.7	4.5	30	.4	3.0	3.0	133	2.82	2.0	.8	6.4	1.6	18	.2	.2	.1	69	.14	.034	4	13	.24	28	.113	1	4.30	.012	.02	.1	.25	2.8	<.1	.09	9	1.5
L43N 100+75E	5.3	80.3	8.4	34	.3	3.5	3.2	99	6.14	3.9	.7	2.0	1.6	15	.3	.3	.2	147	.10	.082	5	19	.13	35	.195	2	5.77	.008	.02	.1	.18	2.7	<.1	.11	24	1.2
L43N 101+00E	3.4	46.5	5.7	30	.2	2.9	2.7	155	3.47	2.2	.5	2.5	2.0	6	.2	.2	.1	71	.09	.059	3	21	.11	15	.120	1	8.25	.008	.01	.1	.30	3.2	<.1	.13	10	1.6
L43N 101+25E	3.5	47.6	5.8	15	.2	2.4	2.0	86	3.69	2.5	.6	1.4	2.6	9	.1	.2	.1	93	.09	.065	3	18	.12	18	.125	1	6.32	.010	.01	<.1	.16	2.9	<.1	.09	14	1.3
L43N 101+50E	3.5	59.8	8.6	23	.4	2.9	2.5	109	4.73	3.0	.6	1.6	2.7	9	.1	.2	.2	82	.09	.069	3	20	.18	21	.138	1	8.00	.008	.02	.2	.27	3.6	<.1	.11	15	1.2
L43N 101+75E	4.2	51.3	9.9	20	.2	2.2	2.0	71	3.56	2.0	.5	2.1	2.4	8	.1	.1	.2	83	.08	.070	3	18	.10	19	.123	<1	6.52	.009	.01	.1	.27	2.8	<.1	.07	15	1.4
L43N 102+00E	13.1	68.2	4.7	24	.1	2.9	2.9	117	3.62	2.1	.5	1.6	.7	15	.2	.2	.1	97	.12	.062	3	13	.20	24	.148	2	3.01	.009	.02	.1	.14	1.3	<.1	.06	14	1.0
L43N 102+25E	7.1	51.8	6.1	13	.2	2.3	1.7	66	3.23	2.4	.4	2.2	1.2	10	<.1	.2	.2	80	.09	.038	3	13	.10	16	.128	1	3.60	.008	.01	.1	.14	2.1	<.1	.06	13	.9
L43N 102+50E	7.4	46.0	6.6	13	.3	2.0	1.8	75	4.16	3.8	.4	2.4	1.8	11	.1	.3	.2	91	.10	.029	3	15	.12	15	.143	1	4.30	.008	.01	.1	.15	2.0	<.1	.09	13	.9
L43N 102+75E	2.3	8.7	5.8	10	<.1	1.1	1.4	123	2.16	.6	.1	.8	.4	28	<.1	.2	.1	67	.24	.011	2	4	.10	11	.205	1	.80	.006	.01	<.1	.03	1.8	<.1	<.05	10	<.5
L43N 103+00E	7.6	53.8	4.9	15	.2	2.3	2.0	69	3.17	2.0	.4	2.3	1.4	13	.1	.2	.1	84	.09	.028	3	14	.10	23	.120	1	3.47	.009	.01	.1	.17	2.1	<.1	.06	11	1.0
L43N 103+25E	4.9	40.9	5.2	15	.1	2.0	1.4	59	3.45	1.7	.4	1.5	1.8	8	.1	.2	.1	93	.08	.043	3	17	.08	15	.117	1	5.01	.008	.01	.3	.28	2.7	<.1	.08	11	.9
L43N 103+50E	7.2	37.2	8.8	12	<.1	2.5	1.8	64	4.99	3.6	.4	3.0	1.5	9	.1	.3	.2	110	.09	.040	2	17	.11	15	.176	1	3.53	.007	.02	.1	.29	2.0	<.1	.07	21	1.2
L43N 103+75E	10.7	66.8	7.9	14	<.1	2.7	1.2	78	.56	.5	.3	1.2	.3	15	.1	.2	.2	36	.14	.019	3	6	.12	26	.093	1	.96	.007	.02	<.1	.09	.8	<.1	<.05	12	<.5
L43N 104+00E	6.8	17.6	9.8	5	.1	.6	.2	51	.20	<.5	.2	<.5	.1	12	<.1	.2	.1	16	.10	.017	2	3	.03	16	.082	1	.70	.009	.04	<.1	.08	.5	<.1	<.05	13	<.5
L43N 104+25E	6.5	88.0	6.6	23	<.1	1.6	1.3	80	3.35	2.5	.4	1.3	1.1	19	<.1	.1	.2	129	.06	.039	4	11	.12	38	.261	<1	4.49	.008	.02	<.1	.12	1.9	<.1	<.05	24	.6
L43N 104+50E	4.5	108.7	4.1	20	.1	3.6	3.2	114	2.73	2.0	.8	2.1	3.8	12	.1	.1	.1	68	.11	.018	3	19	.26	21	.118	1	6.00	.013	.01	.1	.17	5.1	<.1	.10	7	.8
L43N 104+75E	6.6	89.2	5.6	21	<.1	3.5	3.0	113	3.95	2.2	.5	1.9	2.0	13	.1	.2	.2	127	.13	.019	3	21	.18	25	.175	<1	4.34	.009	.02	<.1	.13	3.1	<.1	.08	16	.7
L43N 105+00E	1.7	8.3	5.3	5	.1	.9	.2	48	.16	<.5	.2	1.6	.1	6	<.1	.1	.1	17	.04	.016	3	3	.02	10	.066	<1	.81	.006	.01	<.1	.06	.4	<.1	<.05	9	<.5
L43N 105+25E	3.0	5.6	2.7	5	<.1	1.7	1.6	63	1.72	.5	.1	1.9	.4	10	.1	.2	.1	89	.09	.008	2	11	.02	6	.077	1	.46	.005	.01	<.1	.02	.5	<.1	<.05	7	<.5
L43N 105+50E	17.8	128.4	5.0	21	.2	3.0	2.4	108	2.89	1.8	.8	3.2	1.6	12	.1	.2	.1	72	.11	.047	4	13	.19	21	.124	1	4.46	.008	.02	.2	.17	2.5	<.1	.06	13	1.6
L43N 105+75E	8.8	85.7	6.2	26	.1	3.2	2.6	109	3.21	1.5	.7	1.3	2.1	10	.1	.2	.1	83	.10	.040	4	15	.20	22	.138	1	5.60	.010	.02	.1	.14	3.2	<.1	.07	12	1.2
L43N 106+00E	1.7	3.9	1.6	4	<.1	1.2	1.4	76	1.72	<.5	.1	1.9	.5	4	<.1	.2	.1	69	.04	.005	2	9	.01	5	.041	<1	.25	.004	<.01	<.1	.02	.3	<.1	<.05	3	<.5
L42N 96+00E	.9	2.5	2.6	5	.1	1.3	.6	50	.45	<.5	.2	<.5	1.7	30	<.1	.3	<.1	28	.28	.009	3	8	.03	6	.070	1	.58	.009	.02	<.1	.02	.6	<.1	<.05	5	<.5
L42N 96+25E	29.6	29.5	7.0	51	.1	3.4	3.7	113	2.77	1.1	.5	.5	.5	17	.1	.2	.1	82	.20	.028	3	11	.15	30	.102	1	2.42	.008	.02	.1	.03	1.1	<.1	<.05	13	<.5
L42N 96+50E	3.3	7.7	6.2	18	.1	1.7	2.6	110	2.33	2.5	.2	<.5	.8	72	.1	.6	.1	108	.23	.015	3	8	.17	73	.192	1	1.19	.007	.02	<.1	.02	1.8	<.1	<.05	14	<.5
L42N 96+75E	2.3	11.3	5.4	18	.2	1.9	1.6	72	1.90	.9	.2	.5	.7	19	.1	.2	.1	57	.16	.018	3	7	.09	13	.082	1	1.50	.006	.02	<.1	.06	.9	<.1	<.05	11	<.5
L42N 97+00E	2.7	11.1	6.3	19	.2	2.0	1.7	73	2.15	1.2	.3	.5	.9	29	.1	.3	.1	61	.19	.020	3	8	.09	15	.076	1	1.89	.006	.01	<.1	.08	1.0	<.1	<.05	13	<.5
L42N 97+25E	3.0	7.2	3.9	10	.1	1.4	1.2	50	1.98	1.6	.3	.7	.6	18	.1	.2	.1	50	.12	.016	3	8	.06	19	.089	1	1.87	.007	.01	<.1	.08	.9	<.1	<.05	10	<.5
STANDARD DS6	11.5	122.8	29.4	142	.3	25.4	11.0	693	2.82	21.1	6.6	57.9	3.1	4																						



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ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P ppm	La ppm	Cr ppm	Mg ppm	Ba %	Ti ppm	B %	Al ppm	Na %	K ppm	W ppm	Hg ppm	Sc ppm	Tl ppm	S ppm	Ga ppm	Se ppm
G-1	.2	2.2	2.8	41 <.1	3.5	3.9	482	1.76	<.5	2.4	.8	4.1	62	<.1	<.1	.1	35	.55	.076	8	13	.53	187	.105	1	.96	.083	.47	<.1	0.1	2.0	.3	.06	5 <.5		
L42N 97+50E	21.0	31.9	4.6	34 .1	3.9	8.5	280	3.11	1.7	.2	2.5	.5	17	.1	.2	.1	93	.14	.026	2	12	.17	31	.069	1	2.06	.008	.02	.1	.09	.9 <.1	.11	10	.5		
L42N 97+75E	10.9	54.3	5.5	44 .1	4.6	3.6	104	2.66	2.0	.5	1.4	1.1	25	.1	.2	.1	54	.14	.039	3	12	.22	37	.085	1	4.27	.009	.02	.1	.10	1.8 <.1	.06	11	.7		
L42N 98+00E	6.0	18.3	4.7	25 .1	2.9	2.8	99	2.57	1.0	.2	1.3	.5	14	.1	.1	.1	81	.12	.016	2	11	.15	20	.080	<1	1.37	.006	.01	.1	.04	.7 <.1	.07	12	<.5		
L42N 98+25E	29.2	79.1	5.7	34 .3	4.4	4.8	105	3.37	1.5	.8	2.1	1.5	12	.2	.1	.1	68	.10	.037	5	15	.21	28	.101	<1	4.57	.008	.02	.1	.12	3.0 <.1	.06	12	.8		
L42N 98+50E	11.9	18.7	5.4	29 .3	2.0	1.9	77	2.27	1.3	.2	2.0	.7	16	<.1	.2	.1	74	.12	.028	2	11	.10	27	.084	1	2.08	.007	.03	.1	.33	1.2 <.1	<.05	11	.6		
L42N 98+75E	2.4	11.2	2.7	10 .1	1.3	1.5	47	1.25	.5	.1	.7	.5	14	<.1	.1	.1	40	.07	.011	2	5	.05	30	.041	1	1.17	.006	.02	<.1	.03	.6 <.1	<.05	8	<.5		
L42N 99+00E	22.9	22.8	4.7	20 .1	1.2	5.2	192	.80	.8	.2	7.3	.2	12	<.1	.1	.1	23	.13	.021	2	3	.07	39	.005	<1	1.48	.007	.03	<.1	.05	.5 <.1	<.05	7	<.5		
L42N 99+25E	8.5	23.4	7.5	22 .2	2.6	2.3	92	3.97	1.6	.2	40.8	.8	13	.1	.3	.2	131	.11	.021	3	12	.13	20	.158	<1	1.74	.005	.02	<.1	.06	1.2 <.1	<.05	24	<.5		
L42N 99+50E	6.0	90.4	6.1	37 .1	3.5	3.1	108	3.93	2.0	.4	21.7	1.8	13	.2	.2	.1	91	.10	.034	3	18	.20	37	.117	<1	5.43	.010	.02	.2	.08	2.1 <.1	<.05	13	.7		
L42N 99+75E	4.4	38.9	5.6	26 .2	2.0	1.9	68	3.02	1.2	.2	2.4	.8	11	.1	.2	.1	85	.09	.022	2	9	.09	19	.095	<1	2.40	.007	.02	.1	.06	1.5 <.1	<.05	11	<.5		
L42N 100+00E	47.3	343.0	4.2	69 .3	3.8	29.8	506	3.61	1.5	.5	3.0	.9	27	.3	.1	.1	89	.14	.026	3	12	.27	45	.116	1	2.66	.009	.02	.1	.10	1.4 <.1	<.05	10	.8		
RE L42N 100+00E	48.1	343.4	4.1	71 .3	3.8	30.0	517	3.58	1.6	.4	1.3	.9	27	.3	.2	.1	95	.14	.027	3	13	.28	46	.124	<1	2.72	.010	.02	.2	.09	1.4 <.1	<.05	10	.7		
L42N 100+25E	3.2	64.0	3.4	17 <.1	2.8	2.2	93	1.67	1.5	.6	1.2	1.6	14	.1	.1	.1	42	.13	.045	4	13	.17	22	.070	1	4.11	.011	.01	.1	.12	2.0 <.1	<.05	6	1.3		
L42N 100+50E	3.6	24.7	7.1	16 .1	2.0	1.7	91	3.89	1.7	.4	2.4	1.5	9	.1	.2	.2	110	.11	.041	3	13	.08	15	.143	<1	3.00	.005	.01	.1	.15	1.5 <.1	<.05	15	.5		
L42N 100+75E	10.1	143.8	5.6	34 .2	3.1	3.4	145	1.88	1.5	.6	2.3	1.0	15	.1	.1	.1	50	.13	.043	4	9	.24	32	.072	1	2.83	.009	.02	.1	.17	1.9 <.1	<.05	8	.9		
L42N 101+00E	8.4	235.5	6.2	26 .4	2.4	2.9	128	2.85	2.5	2.0	5.2	3.0	12	.1	.1	.1	50	.09	.074	4	15	.20	28	.095	1	9.70	.010	.02	.2	.20	8.6 <.1	.11	9	1.9		
L42N 101+25E	1.6	8.9	2.6	8 .2	1.3	1.3	66	1.70	.9	.1	.9	.4	13	.1	.2	.1	73	.13	.013	2	8	.02	10	.068	2	.42	.005	.01	<.1	.04	.5 <.1	<.05	7	<.5		
L42N 101+50E	6.0	105.8	4.0	28 .2	2.4	2.2	107	2.28	1.9	.4	1.7	1.2	23	.1	.1	.1	54	.13	.030	3	9	.13	30	.049	1	3.05	.008	.02	.1	.10	1.4 <.1	<.05	9	.6		
L42N 101+75E	5.6	23.6	7.6	18 .1	2.4	1.6	81	3.58	2.2	.3	1.4	1.5	9	.1	.3	.2	105	.08	.044	2	15	.10	16	.137	<1	3.42	.007	.01	.1	.10	2.0 <.1	<.05	14	.6		
L42N 102+00E	4.3	29.2	5.1	15 .2	1.8	1.7	63	2.34	1.5	.3	171	.9	.8	14	.1	.2	.1	69	.12	.019	3	11	.08	18	.103	1	2.87	.007	.01	.1	.12	2.1 <.1	<.05	10	.7	
L42N 102+25E	6.3	58.2	6.5	17 .2	2.9	2.5	99	3.08	2.4	.4	2.6	2.0	12	.1	.2	.1	91	.11	.037	3	16	.18	20	.148	<1	3.66	.008	.02	.1	.23	2.0 <.1	<.05	12	.8		
L42N 102+50E	4.4	44.4	4.2	18 .1	2.4	2.1	84	2.73	2.0	.3	2.8	1.2	12	.1	.2	.1	83	.11	.048	3	15	.11	23	.119	<1	2.73	.009	.01	.1	.13	2.0 <.1	<.05	9	.8		
L42N 102+75E	12.1	233.0	5.9	19 .1.6	3.4	2.3	27	1.33	1.6	1.5	3.3	.7	6	.1	.1	.1	37	.05	.225	8	12	.05	21	.051	1	>10	.008	.01	.1	.24	2.9 <.1	.07	7	3.7		
L42N 103+00E	4.7	25.4	4.9	10 <.1	1.3	1.1	44	2.32	1.2	.3	1.9	1.5	8	<.1	.2	.1	81	.07	.023	3	13	.04	10	.086	<1	3.24	.006	.01	<.1	.05	2.2 <.1	<.05	9	.5		
L42N 103+25E	41.6	815.4	6.3	38 .7	5.9	7.3	164	1.77	1.3	.9	3.1	1.4	17	.1	.1	.2	46	.16	.075	9	13	.39	40	.104	1	3.60	.012	.03	.1	.10	2.7 <.1	<.05	11	1.1		
L42N 103+50E	8.6	107.1	8.0	15 .3	2.4	2.0	96	3.24	3.3	.4	2.7	2.2	12	.1	.2	.1	73	.09	.026	2	16	.18	18	.138	<1	5.30	.008	.02	.1	.24	2.4 <.1	.09	13	1.3		
L42N 103+75E	3.7	77.2	5.7	12 <.1	2.2	1.7	58	2.58	1.5	.7	1.0	2.4	8	.1	.1	.1	71	.08	.046	3	20	.11	16	.112	<1	6.12	.012	.01	.1	.19	4.6 <.1	.11	10	1.6		
L42N 104+00E	5.6	73.2	5.8	12 .2	2.5	1.8	56	3.11	2.5	.6	1.5	2.6	7	.1	.2	.1	77	.06	.042	3	24	.11	14	.109	1	6.20	.011	.01	.1	.20	4.0 <.1	.07	10	1.3		
L42N 104+25E	14.4	44.9	6.3	10 <.1	2.3	1.1	41	2.67	.8	.2	.7	.7	9	.1	.2	.2	111	.07	.022	2	15	.06	13	.087	<1	1.78	.009	.01	<.1	.12	1.1 <.1	<.05	17	<.5		
L42N 104+50E	63.0	249.7	7.0	25 .2	3.3	2.9	121	1.83	1.2	.3	1.5	.8	16	<.1	.1	.1	78	.13	.026	3	11	.26	32	.129	<1	2.21	.009	.02	.1	.07	1.5 <.1	.06	12	.5		
L42N 104+75E	43.1	84.1	5.0	23 .2	4.1	3.3	124	.76	.5	.4	2.2	.3	10	.1	.2	.1	35	.14	.020	3	8	.54	21	.103	1	2.01	.007	.04	.1	.07	2.1 <.1	.11	8	.7		
L42N 105+25E	1.6	5.3	1.2	3 <.1	1.0	1.3	62	1.60	<.5	.1	4.7	.4	4	<.1	1	<.1	67	.04	.003	2	6	.02	5	.060	<1	.22	.005	.01	<.1	.01	.2 <.1	<.05	3	<.5		
L42N 105+50E	2.0	3.7	1.3	4 <.1	.8	.8	36	1.37	<.5	.1	<.5	.3	8	<.1	.1	<.1	50	.06	.005	2	4	.02	6	.038	<1	.22	.006	.01	<.1	.02	.3 <.1	<.05	2	<.5		
L42N 105+75E	1.6	4.6	1.5	4 <.1	1.1	1.2	52	1.44	.5	.1	.5	.5	7	<.1	.2	.1	64	.05	.005	2	6	.02	7	.060	<1	.32	.007	.01	<.1	.02	.3 <.1	<.05	4	<.5		
STANDARD DS6	11.6	122.9	29.6	142 .3	25.1	10.9	701	2.86	21.0	6.7	48.6	3.0	40	6.1	3.6	5.0	55	.86	.081	13	186	.58	164	.069	20	1.93	.074	.15	3.4	.23	3.3	1.8 <.05	6	4.4		

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data *[Signature]*



Mincord Exploration Consultants Ltd.

FILE # A602790

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ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca ppm	P %	La ppm	Cr ppm	Mg ppm	Ba ppm	Ti ppm	B %	Al %	K %	W %	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.2	2.3	3.3	40 <.1	3.6	3.7	490	1.77	<.5	2.5	1.5	4.2	65	<.1	<.1	.1	36	.54	.076	8	14	.54	186	.119	3	1.01	.100	.44	.1<.01	2.5	.3<.05	5 <.5			
L42N 106+00E	4.2	53.9	7.4	13 <.1	3.2	2.2	73	4.22	3.1	.5	2.4	2.6	8	.1	.3	.2	121	.09	.031	3	20	.12	17	.185	2	4.36	.009	.02	.1	.16	3.3	<.1	.08	16	1.0
L25N 92+00E	.8	4.8	2.7	5 <.1	1.1	.8	55	1.41	.6	.1	2.1	.7	8	<.1	.2	.1	57	.07	.007	3	5	.02	9	.073	1	.60	.006	.01	<.1	.05	.5	<.1<.05	6 <.5		
L25N 92+25E	2.6	21.3	6.0	23 <.1	2.7	1.8	103	2.35	2.4	.2	2.5	1.2	12	.1	.3	.1	71	.12	.021	3	10	.13	20	.084	1	2.14	.007	.01	.1	.07	1.2	<.1<.05	9 <.5		
L25N 92+50E	3.2	36.0	5.0	19 <.1	2.8	2.1	118	2.53	2.2	.3	3.0	1.4	10	.1	.3	.1	71	.11	.023	3	11	.17	15	.120	1	3.16	.008	.02	.1	.08	1.5	<.1<.05	10 <.5		
L25N 92+75E	2.2	17.0	5.8	18 <.1	3.4	2.3	117	3.08	1.8	.2	.7	.9	10	<.1	.3	.2	104	.09	.018	3	17	.13	20	.125	1	1.82	.006	.02	<.1	.08	1.3	<.1<.05	16	.5	
L25N 93+00E	1.7	17.4	4.9	19 <.1	2.9	2.2	111	2.78	1.9	.3	2.0	1.0	11	.1	.2	.1	74	.11	.023	3	13	.15	19	.077	1	2.85	.008	.01	<.1	.06	1.5	<.1<.05	10 <.5		
L25N 93+25E	11.3	53.8	6.0	32 <.1	4.8	4.1	172	2.75	2.5	.7	2.9	1.3	16	.1	.2	.1	70	.13	.053	6	13	.34	37	.124	1	4.48	.010	.02	.2	.12	2.7	<.1<.05	11	1.6	
L25N 93+50E	8.1	18.8	8.7	31 <.1	4.1	2.7	118	5.17	3.1	.4	6.6	1.9	11	.1	.3	.2	128	.10	.061	3	19	.20	19	.169	<1	3.87	.006	.02	.1	.03	1.9	<.1<.05	22 <.5		
L25N 93+75E	1.1	2.5	6.2	9 <.1	1.2	.5	63	.34	1.1	.2	.9	.4	18	<.1	.3	.2	21	.19	.012	3	4	.04	10	.038	<1	.65	.008	.01	<.1	.03	.8	<.1<.05	5 <.5		
L25N 94+00E	1.0	2.2	5.3	7 <.1	1.3	.9	75	1.12	.9	.1	5.8	.7	17	<.1	.2	.2	56	.17	.007	3	6	.04	6	.062	<1	.50	.005	.01	<.1	.01	.8	<.1<.05	6 <.5		
L25N 94+25E	3.8	5.9	5.6	12 <.1	4.2	1.3	26	.23	.9	.2	<.5	.1	29	.5	.1	.1	9	.28	.023	4	13	.05	66	.014	1	.41	.011	.03	<.1	.04	.5	<.1<.05	3 <.5		
L25N 94+75E	3.7	15.6	6.6	25 <.1	2.8	2.1	93	3.73	2.6	.4	5.2	1.8	15	.1	.3	.2	101	.11	.058	3	13	.13	26	.115	12	3.00	.006	.02	.1	.07	1.6	<.1<.05	17	.5	
L25N 95+00E	2.5	39.5	6.9	32 <.1	5.1	4.4	173	1.65	.7	.7	6.4	1.4	14	<.1	.1	.1	50	.12	.039	5	12	.38	28	.137	<1	2.90	.008	.03	.1	.05	2.2	<.1<.05	12	1.0	
L25N 95+25E	4.3	17.0	8.2	47 <.1	4.0	4.4	142	3.26	2.7	.2	1.6	1.1	15	.1	.3	.2	92	.14	.028	4	12	.23	26	.135	1	1.80	.006	.02	.1	.05	1.3	<.1<.05	16 <.5		
RE L25N 95+25E	4.1	17.7	8.4	48 <.1	4.1	4.6	142	3.33	2.8	.2	1.6	1.1	15	.1	.3	.3	89	.15	.028	4	12	.22	25	.128	1	1.75	.006	.02	.1	.05	1.3	<.1<.05	16 <.5		
L25N 95+50E	5.9	18.2	8.6	30 <.1	3.1	2.3	110	4.42	4.5	.3	3.8	1.0	12	.1	.4	.3	116	.11	.028	3	11	.16	17	.131	<1	1.69	.005	.02	.1	.06	1.0	<.1<.05	17 <.5		
L25N 95+75E	2.7	19.5	16.8	46 <.1	4.0	4.0	107	1.02	1.7	.4	5.6	.2	18	.2	.2	.2	23	.17	.038	4	9	.14	37	.049	1	1.44	.009	.03	<.1	.11	.9	<.1<.05	11 <.5		
L25N 96+00E	3.4	19.4	7.7	19 <.1	3.3	1.6	106	.50	.5	.4	1.6	.2	15	.1	.1	.1	21	.12	.019	4	7	.18	27	.026	1	1.17	.009	.02	<.1	.06	.8	<.1<.05	9 <.5		
L25N 96+25E	5.0	44.7	8.2	52 <.1	6.4	6.2	211	2.09	1.6	.7	2.0	1.3	19	.1	.2	.2	61	.15	.027	5	14	.44	35	.134	<1	2.59	.008	.02	.1	.06	2.1	<.1<.05	15	1.0	
L25N 96+50E	1.5	2.6	4.4	7 <.1	1.9	.7	62	1.11	.6	.2	3.0	.7	14	<.1	.2	.1	55	.12	.008	3	6	.04	10	.108	1	.51	.005	.02	<.1	.01	.5	<.1<.05	9 <.5		
L25N 96+75E	1.9	3.8	8.4	9 <.1	1.4	.6	55	.80	2.1	.2	2.2	.9	10	<.1	.3	.3	64	.09	.017	4	7	.04	10	.116	<1	.55	.005	.02	<.1	.02	.7	<.1<.05	9 <.5		
L25N 97+00E	2.6	4.8	11.7	12 <.1	2.1	.8	65	1.13	1.7	.2	247	4	1.1	13	<.1	.3	.3	66	.11	.023	4	7	.06	12	.143	<1	.79	.005	.02	<.1	.03	.8	<.1<.05	15 <.5	
L25N 97+25E	2.0	5.0	4.5	6 <.1	1.2	.7	54	.83	1.1	.1	.8	.5	15	.1	.2	.2	40	.09	.012	2	5	.02	12	.076	1	.27	.008	.01	<.1	.02	.4	<.1<.05	4 <.5		
L25N 97+50E	3.8	40.1	7.2	31 <.1	3.0	1.8	102	.96	.7	.7	1.2	.7	13	.1	.1	.2	33	.11	.023	6	9	.16	21	.062	1	1.57	.006	.02	.1	.09	1.3	<.1<.05	10	.8	
L25N 97+75E	8.4	26.5	6.0	50 <.1	4.3	5.6	280	2.02	1.4	.4	2.1	.7	20	.1	.1	.1	65	.16	.022	3	8	.46	28	.130	<1	1.62	.013	.04	.1	.07	1.6	<.1<.05	12	.6	
L25N 98+00E	6.8	20.6	7.0	30 <.1	3.3	2.4	129	.90	1.2	.4	2.4	.9	17	.1	.2	.2	32	.13	.016	4	9	.21	23	.091	<1	1.48	.009	.02	.1	.11	1.4	<.1<.05	12	.5	
L25N 98+25E	.6	9.6	8.5	8 <.1	1.5	.7	70	1.01	1.7	.1	.8	.4	13	<.1	.3	.2	46	.10	.013	3	6	.04	11	.061	1	.64	.010	.02	<.1	.02	.4	<.1<.05	9 <.5		
L25N 98+50E	1.4	3.8	2.0	5 <.1	1.4	.9	51	.94	.6	.1	9.0	.6	8	.1	.2	.1	45	.05	.008	3	7	.01	9	.042	1	.24	.004	.01	<.1	.01	.4	<.1<.05	4 <.5		
L25N 98+75E	20.4	51.8	4.4	43 <.1	3.8	4.1	194	1.70	1.7	.9	2.8	2.2	18	.1	.1	.1	56	.12	.027	5	12	.38	25	.115	1	3.74	.010	.02	.2	.08	3.2	<.1<.05	8	1.2	
L25N 99+00E	1.8	7.3	7.2	7 <.1	1.9	.4	30	.21	1.2	.1	55.1	.2	9	.3	.2	.1	15	.07	.013	2	5	.02	11	.053	<1	.43	.011	.02	<.1	.03	.2	<.1<.05	6 <.5		
L25N 99+25E	12.9	13.4	13.6	22 <.1	1.6	.7	78	.57	.9	.2	8.8	.8	25	.1	.3	.3	43	.19	.011	4	6	.08	20	.138	<1	.99	.006	.02	<.1	.04	.8	<.1<.05	16 <.5		
L25N 99+50E	5.1	42.7	7.1	37 <.1	3.8	3.4	154	3.72	3.1	.5	2.6	2.5	12	.1	.2	.2	108	.12	.067	3	16	.22	18	.147	1	3.67	.008	.03	.1	.07	2.6	.1<.05	14	.6	
L25N 99+75E	1.6	40.5	4.4	28 <.1	3.6	4.3	224	1.12	1.4	.7	3.1	1.9	23	.1	.1	.1	42	.15	.056	6	11	.43	35	.093	1	3.68	.014	.03	.1	.05	2.7	<.1<.05	7	.8	
L25N 100+00E	6.0	30.3	7.1	35 <.1	4.6	4.2	173	4.66	2.4	.4	3.6	2.4	14	.1	.3	.2	112	.10	.022	3	19	.29	36	.203	<1	3.38	.006	.02	.1	.24	2.4	<.1<.05	19	1.0	
STANDARD DS6	11.7	123.8	29.2	142	.3	24.8	10.8	693	2.81	20.9	6.6	56.7	3.0	39	6.1	3.6	4.9	.56	.84	.080	13	186	.56	163	.078	18	1.85	.070	.14	3.6	.23	3.2	1.8<.05	6	4.2

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

GEOCHEMICAL ANALYSIS CERTIFICATE

Mincord Exploration Consultants Ltd. PROJECT OK File # A603159 Page 1
 110 - 325 Howe St., Vancouver BC V6C 1Z7 Submitted by: JP Charbonneau

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppb	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V %	Ca ppm	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.4	3.0	3.1	41	<1	7.5	4.2	502	1.97	.5	2.9	<.5	4.5	90	<.1	<.1	.1	40	.62	.077	10	180	.58	225	.145	1	1.13	.165	.55	.1<.01	3.1	.4<.05	5	<.5		
L55N 101+50E	2.6	58.0	6.2	29	.1	4.9	3.7	124	3.33	1.9	.6	6.1	1.7	14	.1	.2	.1	83	.11	.053	2	21	.27	29	.137	1	5.62	.010	.02	.1	10	1.9<.1	.07	11	.7	
L55N 101+75E	2.0	56.4	6.1	28	.1	3.3	2.5	106	2.54	1.5	.5	6.8	1.4	16	.1	.2	.1	74	.12	.029	3	15	.20	25	.122	<1	2.88	.011	.02	.3	.06	1.4<.1	<.05	9	.7	
L55N 102+00E	.7	1.1	5.7	5	<.1	.4	.4	60	.52	.6	.1	2.3	.4	30	<.1	.1	.1	22	.23	.009	3	3	.03	8	.083	1	.45	.012	.02	<.1	.02	.6	<.1<.05	5	<.5	
L55N 102+25E	3.5	77.4	7.2	27	<.1	4.7	3.5	133	3.18	1.7	.7	4.0	1.8	12	.1	.2	.1	86	.10	.050	2	19	.30	26	.127	<1	5.55	.008	.02	.1	.06	1.5<.1	<.05	12	.6	
L55N 102+50E	10.0	24.4	6.7	24	.2	2.7	2.1	120	2.10	1.3	.2	2.4	.6	47	.1	.2	.1	69	.31	.022	3	11	.24	20	.146	1	1.55	.008	.01	<.1	.05	1.5<.1	<.05	9	<.5	
L55N 102+75E	5.8	179.4	5.9	32	.4	5.2	3.5	131	3.32	1.9	.8	7.4	2.7	15	.1	.2	.1	87	.11	.064	3	21	.30	26	.127	<1	5.06	.013	.02	.3	.16	3.4<.1	<.05	10	1.4	
L55N 103+00E	10.2	4.0	3.1	5	.2	.6	.8	59	.80	.5	.1	2.1	.6	28	<.1	.5	.1	40	.15	.004	4	5	.05	16	.085	1	.67	.008	.01	<.1	.03	.8	<.1<.05	6	<.5	
L55N 103+25E	31.0	137.4	6.5	35	.2	4.3	3.5	106	2.96	1.9	.5	3.0	1.8	13	.1	.2	.1	77	.10	.042	3	14	.23	27	.142	1	3.29	.014	.02	.1	.15	1.6<.1	<.05	11	1.0	
L55N 103+50E	5.5	127.1	5.4	41	.2	7.5	5.5	191	3.28	1.5	.5	5.0	2.0	20	.1	.2	.1	84	.14	.041	3	20	.48	48	.154	<1	4.55	.015	.03	.2	.08	2.2<.1	<.05	9	.7	
L55N 104+00E	14.7	53.0	7.9	18	.5	2.4	2.2	76	3.30	3.4	.4	4.0	.9	25	.3	.4	.2	78	.11	.038	3	12	.12	28	.111	1	2.89	.011	.02	.1	.19	1.5<.1	<.05	11	1.0	
L55N 104+25E	3.6	11.7	3.5	9	.1	1.8	2.0	62	1.52	.6	.1	2.3	.4	31	.1	.2	.1	65	.13	.015	2	10	.09	15	.155	1	.35	.008	.01	<.1	.02	.5	<.1<.05	6	.5	
L55N 104+50E	16.8	19.6	8.5	6	.1	2.2	2.4	64	1.65	1.2	.1	4.5	.3	19	.1	.4	.2	82	.12	.018	2	12	.03	13	.147	2	.32	.008	.01	<.1	.04	.5	<.1<.05	6	<.5	
L55N 104+75E	8.3	45.1	7.4	18	.4	2.4	2.0	72	4.58	2.3	.5	4.1	1.9	13	.1	.2	.2	108	.07	.083	3	17	.14	19	.177	1	4.51	.010	.01	.1	.22	2.3<.1	.07	18	1.2	
L55N 105+00E	149.9	460.1	5.5	86	.8	7.1	14.3	497	6.28	5.1	.7	7.5	1.2	206	.2	.2	.1	89	.47	.175	6	17	.89	124	.112	<1	3.29	.017	.07	.2	.09	3.0	<.1<.05	9	1.8	
L55N 105+25E	5.6	304.8	6.9	128	.2	13.1	14.9	550	3.05	1.7	.5	6.5	1.5	18	.1	.1	.1	46	.16	.059	5	20	1.01	62	.034	<1	2.77	.009	.05	.7	.03	2.7	<.1<.05	7	.6	
L55N 105+50E	10.3	100.4	6.9	21	.2	3.7	3.2	104	4.16	2.0	.8	3.3	2.5	15	.2	.2	.1	94	.08	.064	3	20	.25	23	.197	<1	5.02	.011	.02	.2	.18	2.7<.1	.07	15	1.1	
L55N 105+75E	62.1	359.9	5.9	32	.5	5.2	5.0	141	4.02	1.1	.6	2.6	1.9	15	.1	.1	.1	103	.11	.079	5	16	.22	27	.143	1	4.63	.014	.02	.2	.11	1.9	<.1<.05	13	1.4	
L55N 106+00E	15.0	205.4	4.3	34	.3	4.7	4.9	223	2.88	2.1	.5	4.8	1.7	44	.1	.2	.1	76	.21	.072	4	15	.44	45	.124	<1	2.93	.016	.02	.2	.07	2.3<.1	<.05	8	.7	
L55N 106+25E	5.1	34.3	5.3	21	.3	2.5	3.0	121	2.71	.8	.2	4.0	.7	17	.1	.1	.1	91	.12	.037	2	11	.19	25	.097	<1	1.30	.011	.01	<.1	.05	1.1	<.1<.05	9	.6	
L55N 106+50E	12.7	88.4	8.2	36	.3	5.0	4.4	207	3.24	2.3	.2	2.7	1.0	23	.1	.2	.2	87	.17	.069	3	12	.28	41	.127	<1	2.55	.011	.02	.1	.08	1.5<.1	<.05	10	.5	
L55N 106+75E	5.8	67.1	4.8	17	.4	2.4	2.6	178	2.17	1.1	.2	2.7	.8	22	.1	.2	.1	64	.13	.043	3	10	.18	23	.082	<1	1.45	.008	.01	<.1	.04	1.1	<.1<.05	7	<.5	
L55N 107+00E	2.8	47.2	5.5	29	.2	3.8	3.7	337	3.37	1.5	.3	2.5	1.3	12	.1	.2	.1	88	.10	.088	2	11	.29	18	.180	<1	3.65	.013	.02	.1	.16	2.3<.1	<.05	12	.8	
L54N 101+00E	17.4	63.6	9.4	26	.1	2.1	5.9	237	1.12	1.1	1.2	3.0	.3	22	.2	.2	.2	35	.15	.036	7	7	.14	38	.064	<1	1.72	.011	.02	.1	.20	1.1	<.1<.05	9	1.2	
L54N 101+25E	5.8	82.7	7.5	25	<.1	3.2	2.7	151	3.73	2.3	.7	3.8	3.9	9	.1	.2	.1	80	.07	.072	3	23	.21	23	.135	1	7.07	.010	.02	.2	.19	3.6<.1	.09	11	1.4	
L54N 101+50E	10.3	79.6	5.4	20	.1	3.2	2.4	116	2.37	1.1	.8	4.3	2.0	16	<.1	.2	.1	78	.11	.055	5	15	.29	29	.112	<1	4.61	.013	.02	.2	.11	3.0	<.1<.05	10	1.3	
L54N 101+75E	8.3	67.0	7.8	27	.1	3.1	2.8	108	4.14	1.6	.7	1.6	2.3	11	.1	.2	.1	88	.08	.084	5	21	.22	19	.133	<1	6.41	.010	.01	.1	.21	3.3	<.1	14	1.7	
L54N 102+00E	7.8	16.4	5.4	17	.2	2.1	2.3	115	1.33	.5	.1	<.5	.2	149	.1	.3	.1	54	.36	.020	2	13	.17	53	.123	<1	.72	.013	.01	.1	.04	1.6	<.1<.05	7	<.5	
L54N 102+25E	160.5	448.6	6.6	34	.4	2.7	167.5	3355	3.23	1.0	.8	2.7	.3	47	.3	.2	.1	67	.15	.058	5	12	.19	96	.034	<1	3.13	.015	.02	.2	.18	1.4	<.1<.05	9	1.8	
L54N 102+75E	9.7	52.1	5.6	31	.8	3.9	3.4	95	3.59	2.0	.5	2.9	1.9	18	.2	.2	.1	74	.10	.056	3	20	.17	34	.115	<1	5.88	.010	.01	.2	.30	2.6	<.1	10	1.5	
L54N 103+00E	6.1	58.8	6.0	26	.9	2.9	3.4	155	3.37	1.9	.5	1.3	1.7	20	.1	.2	.1	72	.11	.045	4	15	.20	31	.116	1	5.28	.013	.01	.2	.23	2.5	<.1	10	1.3	
L54N 103+25E	4.6	45.5	6.7	30	.2	2.9	3.0	114	3.57	1.5	.6	3.1	1.9	15	.1	.2	.1	78	.11	.068	3	18	.16	27	.124	<1	5.67	.012	.01	.2	.25	2.8	<.1	11	1.7	
RE L54N 103+25E	4.4	43.5	7.0	28	.2	2.7	2.9	111	3.46	1.4	.6	19.6	1.8	14	.2	.2	.1	76	.11	.066	3	16	.16	26	.121	<1	5.45	.011	.01	.2	.24	2.6	<.1	11	1.5	
L54N 103+50E	5.2	70.9	5.5	29	.2	3.3	4.6	136	3.06	1.4	.5	1.7	1.6	15	.1	.2	.1	89	.09	.052	4	15	.18	29	.104	1	3.96	.012	.01	.1	.24	2.2	<.1	10	1.2	
L54N 103+75E	4.9	63.3	5.8	33	.3	3.8	4.5	174	3.34	2.0	.4	14.7	2.2	22	.1	.2	.1	77	.14	.159	3	15	.25	38	.122	1	4.45	.011	.02	.2	.15	1.8	<.1	10	.9	
STANDARD DS7	19.3	105.8	77.7	395	.9	52.9	9.2	635	2.39	46.9	5.4	71.2	4.9	76</																						



Mincord Exploration Consultants Ltd. PROJECT OK FILE # A603159

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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P ppm	Ta ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K ppm	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.5	3.4	3.1	42	<.1	7.0	4.3	501	2.03	<.5	2.9	<.5	4.6	88	<.1	<.1	.1	41	.62	.082	10	170	.60	208	.147	2	1.12	.145	.54	.1	<.01	2.5	.4	<.05	5	<.5
L54N 104+00E	7.7	68.6	6.8	32	.2	3.4	3.2	136	3.35	2.2	.7	4.8	2.0	17	.1	.1	.1	75	.08	.180	4	16	.32	23	.130	2	7.46	.010	.01	.2	.25	3.2	<.1	.09	10	1.4
L54N 104+25E	2.9	12.4	7.2	12	.3	2.3	1.7	60	2.73	1.0	.2	2.2	.6	15	.1	.1	.2	93	.12	.056	2	11	.07	16	.208	2	1.20	.007	.01	.1	.06	.9	<.1	<.05	11	.5
L54N 104+50E	6.5	89.6	4.0	37	.6	4.6	3.7	114	3.11	1.5	.5	1.3	1.5	24	.1	.1	.1	77	.11	.095	3	15	.26	33	.133	4	4.51	.012	.01	.2	.17	2.2	<.1	<.05	9	1.1
L54N 104+75E	28.7	104.9	4.9	41	.5	3.8	3.5	111	3.44	1.6	.5	7.4	1.4	34	.1	.1	.1	89	.13	.103	3	14	.28	37	.165	1	3.97	.014	.01	.2	.20	2.0	<.1	<.05	10	1.6
L54N 105+00E	19.6	156.1	4.7	43	.3	9.3	8.4	250	2.41	3.6	.6	2.8	1.4	77	.2	.1	.1	56	1.15	.122	4	19	.55	53	.086	3	5.04	.026	.06	.4	.15	2.3	<.1	<.05	6	1.2
L54N 105+25E	33.2	118.1	4.6	35	.3	3.9	5.0	198	3.58	2.9	.5	1.4	.9	60	.1	.1	.1	76	.24	.086	4	15	.29	52	.133	4	4.29	.014	.02	.2	.16	2.0	<.1	<.05	9	1.4
L54N 105+50E	22.3	147.6	4.0	36	.1	4.6	6.9	304	2.82	1.3	.5	2.6	1.4	42	.1	.2	.1	66	.25	.067	4	13	.52	39	.082	3	3.26	.019	.05	.2	.05	1.9	<.1	<.05	5	1.1
L54N 105+75E	7.2	114.7	2.9	17	<.1	3.4	3.4	112	2.67	1.1	.7	2.3	2.0	15	.1	.1	<.1	67	.10	.046	4	13	.28	20	.099	3	5.09	.018	.01	.2	.14	2.5	<.1	<.05	6	1.3
L54N 106+00E	1.7	4.8	4.1	6	<.1	.8	1.0	53	1.13	.7	.1	.7	.3	20	<.1	.1	.1	60	.18	.019	2	5	.03	7	.110	3	.40	.008	.01	<.1	.02	.7	<.1	<.05	5	<.5
L54N 106+25E	6.3	80.9	3.6	21	.2	2.8	3.1	102	2.92	.8	.4	1.9	1.3	17	.1	.1	.1	81	.10	.041	3	11	.18	29	.113	1	2.76	.016	.01	.1	.10	1.6	<.1	<.05	9	.5
L54N 106+50E	13.4	26.4	5.6	9	.2	1.8	2.0	71	1.60	1.2	.2	1.4	.6	32	<.1	.2	.2	52	.12	.013	3	8	.11	16	.094	1	.62	.010	.02	.1	.03	.7	<.1	<.05	6	<.5
L54N 106+75E	1.5	5.8	3.7	7	.1	.8	1.1	56	.81	<.5	.1	.9	.3	14	.1	.1	.1	35	.13	.010	2	4	.08	10	.078	2	.41	.008	.01	<.1	.01	.6	<.1	<.05	4	<.5
L54N 107+00E	7.9	78.4	5.6	16	<.1	2.2	2.0	88	2.37	1.9	.3	2.7	1.1	14	<.1	.2	.1	69	.11	.045	2	10	.16	19	.100	3	3.26	.010	.01	.1	.04	1.0	<.1	<.05	8	.5
RE L54N 107+00E	8.0	77.9	5.4	14	<.1	2.0	2.0	90	2.32	1.9	.3	2.4	1.1	15	.1	.2	.1	67	.11	.047	2	10	.16	19	.097	4	2.12	.011	.01	.1	.05	1.1	<.1	<.05	7	<.5
L53N 101+00E	2.8	52.9	4.9	24	.2	3.0	2.9	120	2.50	1.3	.4	1.5	1.7	13	.1	.1	.1	75	.11	.025	3	12	.25	24	.132	<1	2.21	.013	.02	.3	.18	1.5	<.1	<.05	8	<.5
L53N 101+25E	4.7	29.8	6.2	26	.1	2.9	2.4	83	2.81	1.2	.4	3.7	1.5	10	.1	.1	.1	82	.09	.044	2	14	.14	18	.123	2	2.86	.010	.01	.1	.04	1.9	<.1	<.05	10	.5
L53N 101+50E	16.9	101.3	5.2	14	.3	1.5	1.4	58	2.40	1.2	.4	1.9	1.2	9	.1	.2	.1	59	.07	.046	2	11	.09	13	.092	2	3.00	.010	.01	.1	.18	1.8	<.1	<.05	9	.5
L53N 101+75E	11.7	117.0	6.7	18	.1	2.4	2.0	73	3.07	2.2	.6	6.5	1.9	10	.1	.2	.1	74	.08	.056	3	17	.14	19	.085	<1	4.77	.011	.01	.1	.08	2.3	<.1	<.05	10	.6
L53N 102+00E	10.7	99.2	4.2	33	.3	3.0	2.9	142	2.54	1.8	.4	2.4	1.1	37	<.1	.2	.1	62	.13	.037	3	11	.28	47	.085	1	2.78	.012	.02	.1	.07	1.7	<.1	<.05	8	.6
L53N 102+25E	19.6	149.8	6.7	30	.2	4.5	4.5	162	4.01	3.3	.4	2.2	1.8	30	.1	.3	.2	98	.14	.117	2	19	.40	29	.187	2	4.70	.014	.02	.2	.14	2.4	<.1	<.05	14	1.1
L53N 102+50E	14.4	118.3	7.4	33	.5	3.2	2.9	96	3.46	1.7	.5	22.1	1.6	17	.2	.2	.1	80	.10	.092	4	16	.18	25	.125	2	4.04	.012	.02	.1	.24	2.6	<.1	<.05	11	1.8
L53N 102+75E	45.9	49.7	6.0	38	<.1	2.6	2.7	95	3.48	1.2	.4	4.1	.9	14	.3	.1	.1	83	.11	.028	2	12	.15	31	.134	<1	1.60	.009	.01	.2	.10	.9	<.1	<.05	11	.5
L53N 103+00E	14.0	145.5	4.8	38	.8	3.9	4.0	135	2.78	1.9	.5	1.0	1.2	26	.1	.2	.1	68	.14	.043	3	11	.29	42	.111	1	3.28	.013	.02	.2	.11	2.1	<.1	<.05	8	.8
L53N 103+25E	7.5	74.8	4.5	24	.3	3.5	3.1	116	3.40	2.0	.5	2.8	2.0	18	.1	.1	.1	83	.11	.067	3	15	.26	27	.137	<1	4.91	.013	.02	.2	.16	2.4	<.1	<.05	11	1.3
L53N 103+50E	11.8	36.1	6.5	29	.4	3.1	3.2	100	4.48	2.1	.4	.9	1.5	16	.1	.2	.2	116	.10	.067	3	14	.19	25	.238	<1	3.97	.010	.02	.2	.12	2.1	<.1	<.05	17	.9
L53N 103+75E	4.0	54.5	5.7	23	.2	3.2	2.9	100	3.26	2.5	.4	3.0	1.8	16	.1	.2	.1	84	.10	.103	3	14	.24	26	.145	<1	3.76	.011	.02	.2	.12	2.2	<.1	<.05	11	1.5
L53N 104+00E	4.8	124.2	6.1	44	.8	6.3	5.2	224	3.21	1.9	.6	6.0	2.2	21	.1	.2	.1	75	.19	.081	4	16	.49	45	.146	1	3.93	.013	.05	.3	.17	3.4	<.1	<.05	11	1.0
L53N 104+25E	7.7	55.5	5.1	27	.2	3.0	2.6	104	2.57	1.4	.4	1.6	1.6	18	<.1	.2	.1	72	.12	.035	4	13	.20	21	.116	<1	2.44	.011	.02	.1	.17	1.9	<.1	<.05	9	.5
L53N 104+50E	14.9	109.1	4.7	37	.1	4.4	3.9	146	3.22	1.6	.7	2.0	2.1	22	.1	.2	.1	80	.12	.057	4	16	.34	30	.156	<1	4.23	.012	.02	.2	.10	3.1	<.1	<.05	9	<.5
L53N 104+75E	16.4	36.5	6.0	19	.2	1.8	1.8	75	2.87	1.2	.4	3.9	1.1	17	.1	.2	.1	89	.13	.028	3	10	.13	13	.154	<1	1.86	.010	.01	.1	.10	1.7	<.1	<.05	11	<.5
L53N 105+00E	13.4	39.9	3.9	23	.9	2.1	1.4	60	2.17	1.4	.3	23.8	1.0	15	<.1	.1	.1	59	.09	.055	3	10	.11	15	.102	1	2.27	.010	.01	.1	.20	1.6	<.1	<.05	7	.6
L53N 105+25E	3.3	23.0	4.2	10	.4	2.0	1.9	71	2.66	1.0	.2	23.8	.8	12	<.1	.1	.1	93	.09	.023	3	13	.11	10	.142	<1	1.22	.008	.01	<.1	.10	.9	<.1	<.05	8	<.5
L53N 105+50E	3.6	24.7	5.0	13	.1	1.1	1.3	55	2.82	1.2	.3	4.3	1.2	11	<.1	.2	.1	80	.08	.027	2	10	.09	13	.128	<1	2.76	.011	.01	.1	.10	1.9	<.1	<.05	11	.6
L53N 105+75E	5.9	26.3	4.9	11	.3	1.7	1.8	57	4.22	1.6	.2	2.3	.8	18	.1	.2	.2	164	.12	.027	2	10	.12	15	.277	1	2.69	.008	.01	<.1	.09	2.0	<.1	<.05	16	.6
STANDARD DS7	19.9	112.3	73.5	415	.9	52.2																														



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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P ppm	La ppm	Cr ppm	Mg ppm	Ba ppm	Ti ppm	B %	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.6	3.1	3.3	40	<.1	8.2	4.2	534	2.03	.5	3.2	<5	5.1	88	<.1	<.1	.1	40	.68	.077	12	187	.58	208	.151	<1	1.10	.137	.53	.1<.01	2.6	.4<.05	6<.5			
L53N 106+00E	11.6	32.2	5.0	12	.4	1.9	2.1	71	2.90	1.3	.3	3.2	1.0	15	.1	.2	.1	99	.13	.014	3	15	.09	12	.166	<1	1.64	.010	.01	<.1	.12	1.6	<.1<.05	10	.5	
L53N 106+25E	7.6	90.1	5.8	31	.5	5.0	3.9	117	3.91	1.8	.5	3.1	2.1	11	.1	.2	.1	99	.11	.062	5	18	.25	27	.169	<1	5.42	.013	.02	.1	.22	2.8	<.1<.10	14	1.3	
L53N 106+50E	12.7	66.5	6.4	26	.2	2.9	3.1	110	3.72	5.0	.2	12.8	1.1	26	<.1	.4	.2	108	.18	.062	3	12	.23	26	.166	1	2.54	.009	.02	.1	.08	1.7	<.1<.05	13	<.5	
L53N 106+75E	82.8	174.8	8.6	26	.4	3.3	3.0	121	4.04	4.5	.3	15.9	1.1	35	<.1	.5	.4	82	.20	.064	3	10	.22	45	.132	1	2.38	.011	.03	.3	.04	1.5	<.1<.05	14	<.5	
L53N 107+00E	9.6	130.3	6.9	29	.2	4.9	4.4	176	3.29	1.5	.3	11.2	1.2	20	<.1	.3	.1	103	.19	.033	4	15	.33	25	.161	1	1.95	.013	.02	.1	.05	1.5	<.1<.05	12	.5	
L52N 100+25E	45.8	189.3	3.0	12	.9	1.8	2.1	168	.54	<.5	2.4	1.8	<.1	25	.7	<.1	.1	9	.48	.184	11	8	.04	50	.005	<1	1.70	.016	.01	.1	.36	.3	<.1	.28	2	3.2
L52N 100+50E	187.2	425.5	11.8	152	.6	9.9	230.1	4149	3.61	1.4	3.8	<.5	1.4	26	1.1	.4	.2	49	.36	.079	20	15	.22	80	.111	1	5.69	.020	.05	.2	.11	2.3	<.1<.05	10	.8	
L52N 100+75E	7.9	22.6	5.9	16	.5	1.9	2.4	90	3.42	2.2	.4	1.9	1.9	10	.1	.3	.2	105	.11	.050	3	14	.12	10	.177	2	3.16	.012	.02	.1	.23	2.3	<.1<.05	13	.8	
L52N 101+00E	4.4	20.4	5.6	15	.5	2.0	1.7	91	2.59	1.7	.3	5.1	1.0	14	<.1	.3	.1	85	.13	.027	3	11	.13	11	.136	<1	1.74	.008	.01	.1	.12	1.3	<.1<.05	11	<.5	
L52N 101+25E	5.8	111.3	6.3	37	.2	6.3	5.2	198	3.70	1.9	.6	<.5	2.3	23	.1	.2	.1	93	.16	.050	3	20	.44	31	.176	<1	5.23	.016	.02	.2	.06	3.3	<.1<.05	13	.5	
L52N 101+50E	3.7	34.3	5.8	34	.2	2.8	2.6	135	2.88	1.6	.3	1.2	1.0	15	.1	.3	.1	86	.13	.058	3	13	.16	22	.119	<1	2.77	.011	.01	.1	.05	1.9	<.1<.05	12	<.5	
L52N 101+75E	5.1	57.1	7.0	26	.4	4.2	3.4	106	3.65	1.9	.4	4.8	1.6	11	.1	.2	.1	108	.10	.041	3	17	.23	23	.157	<1	4.62	.011	.02	.1	.17	3.2	<.1<.05	16	.7	
L52N 102+00E	4.3	28.0	7.7	17	1.0	2.4	1.8	77	3.53	2.3	.3	2.1	1.2	11	.1	.4	.2	111	.12	.029	3	16	.11	15	.172	1	2.43	.008	.02	<.1	.16	1.9	<.1<.05	16	.6	
L52N 102+50E	4.6	25.4	6.1	23	.6	3.1	2.1	75	3.51	1.9	.3	2.2	1.6	12	.1	.3	.1	102	.13	.057	3	26	.17	18	.142	1	3.66	.010	.02	.1	.25	2.8	<.1<.05	13	1.0	
L52N 102+75E	4.8	64.4	7.3	28	.3	4.7	4.1	151	3.67	3.0	.7	2.5	2.7	15	.1	.3	.1	91	.13	.086	4	20	.29	25	.158	<1	5.14	.013	.02	.2	.15	3.3	<.1<.05	11	1.2	
L52N 103+00E	3.0	42.0	5.5	19	<.1	2.5	2.2	105	2.64	1.5	.4	4.2	1.3	16	<.1	.2	.1	80	.15	.028	3	13	.17	14	.118	1	2.36	.012	.02	.1	.04	2.0	<.1<.05	9	<.5	
L52N 103+25E	2.7	28.3	4.7	16	<.1	2.4	2.0	103	2.32	.7	.2	11.6	.9	17	<.1	.2	.1	82	.15	.016	3	11	.16	13	.117	<1	1.44	.008	.01	<.1	.05	1.3	<.1<.05	9	<.5	
L52N 103+50E	4.9	75.8	4.4	29	.2	5.1	4.1	169	2.85	1.4	.4	2.8	1.6	20	.1	.2	.1	84	.17	.036	3	15	.38	26	.149	<1	3.37	.015	.02	.1	.10	2.1	<.1<.05	9	.6	
L52N 103+75E	3.0	38.2	3.2	20	<.1	2.2	2.3	107	2.26	1.0	.4	14.4	1.1	17	<.1	.2	.1	76	.16	.020	3	12	.14	17	.118	<1	1.86	.011	.01	<.1	.07	1.8	<.1<.05	7	<.5	
L52N 104+00E	4.6	55.7	6.3	25	<.1	3.7	3.0	107	4.11	3.0	.5	1.4	2.8	15	.1	.2	.1	111	.12	.086	3	17	.22	16	.183	2	5.21	.012	.02	.1	.09	2.7	<.1<.05	16	.9	
L52N 104+25E	7.8	66.2	5.9	26	.2	3.3	3.0	122	4.37	3.0	.5	1.7	2.4	18	.1	.3	.1	118	.13	.068	3	21	.27	20	.179	<1	4.43	.011	.02	.1	.16	2.5	<.1<.05	15	1.0	
L52N 104+50E	2.0	2.8	5.5	8	<.1	.6	.6	79	.92	1.0	.2	1.4	.5	31	<.1	.2	.1	40	.29	.014	3	4	.04	8	.186	<1	.57	.008	.01	<.1	.02	1.1	<.1<.05	6	<.5	
L52N 104+75E	9.7	52.4	4.6	16	.1	1.9	1.7	72	2.68	1.3	.2	2.8	.6	19	<.1	.1	.1	78	.13	.040	3	9	.13	13	.181	<1	1.38	.008	.01	<.1	.03	.9	<.1<.05	13	<.5	
L52N 105+00E	8.8	39.4	5.3	21	.1	3.3	3.3	105	4.05	2.6	.3	1.9	.9	23	<.1	.3	.2	131	.18	.031	3	13	.20	18	.221	<1	1.67	.010	.02	.1	.05	1.2	<.1<.05	19	.8	
L52N 105+25E	3.4	22.4	5.8	11	.2	1.7	1.7	61	4.24	2.9	.3	2.9	1.3	10	.1	.4	.2	149	.09	.027	2	13	.09	12	.183	<1	2.80	.008	.01	<.1	.10	2.1	<.1<.05	21	<.5	
L52N 105+50E	43.6	67.6	4.1	47	.3	4.1	4.6	214	5.14	2.2	.4	2.2	1.3	128	<.1	.4	.1	124	.12	.045	3	16	.53	72	.125	1	2.56	.011	.04	.1	.06	2.4	<.1<.05	17	.8	
L52N 105+75E	28.0	64.2	5.4	20	.2	1.4	1.9	96	3.19	2.0	.4	2.2	.8	35	<.1	.2	.2	89	.12	.023	3	7	.16	35	.158	<1	1.95	.011	.03	.1	.09	1.2	<.1<.05	16	<.5	
L52N 106+00E	9.8	65.1	8.4	14	.3	3.1	2.8	77	3.89	1.3	.4	4.3	.9	18	.2	.2	.2	125	.12	.023	3	15	.16	27	.224	<1	2.66	.014	.01	.1	.23	2.4	<.1<.05	19	.7	
L52N 106+25E	14.1	144.7	6.1	19	.6	4.0	3.3	105	5.27	2.6	.7	1.8	2.8	12	.1	.2	.2	104	.10	.040	5	23	.28	26	.219	1	7.44	.011	.02	.1	.34	4.4	<.1	12	19	2.0
L52N 106+50E	54.1	394.7	5.1	20	.1	2.6	5.9	130	4.91	1.8	.5	2.9	1.4	31	.1	.3	.1	112	.19	.038	3	15	.20	51	.125	<1	3.89	.014	.03	.2	.12	1.9	<.1<.05	14	1.4	
L52N 106+75E	50.9	804.6	4.8	35	.3	5.1	6.8	172	4.22	1.1	1.0	3.8	3.3	20	.1	.2	.1	92	.12	.039	4	16	.38	48	.135	1	6.07	.015	.02	.2	.07	3.3	<.1	10	9	1.1
L52N 107+00E	6.5	57.2	4.6	20	.1	2.9	2.7	116	2.71	.8	.4	4.5	1.2	15	<.1	.2	.1	87	.16	.014	3	10	.19	27	.149	1	2.22	.011	.02	<.1	.05	1.8	<.1<.05	10	.8	
RE L52N 107+00E	6.5	57.8	4.7	21	.1	3.1	2.8	113	2.75	.8	.4	2.8	1.3	15	.1	.2	.1	84	.15	.015	3	10	.19	26	.141	1	2.31	.011	.02	<.1	.04	1.6	<.1<.05	11	<.5	
L51N 99+25E	16.0	73.5	6.5	55	.1	5.5	26.3	4893	3.60	1.5	.5	1.4	1.5	26	1.2	.2	.1	96	.30	.037	4	14	.18	69	.121	<1	3.07	.015	.02	.1	.07	1.7	.1	.06	10	<.5
STANDARD DS7	20.4	104.4	73.6	394	1.0	53.5	9.4	628	2.39	46.0	5.4	76.4	5.0	78	6.2	6.4	4.6	84	.95	.074	14	160	1.00	363	.135	35	.96	.072	.45	3.8	20	2.				



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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppb	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca ppm	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti ppm	B %	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.5	3.1	2.9	41	<.1	8.6	4.1	521	1.98	<.5	3.0	<.5	4.4	83	<.1	<.1	.1	39	.58	.080	9	158	.54	212	.136	<1	.99	.128	.47	.1<.01	2.2	.4<.05	5	<.5		
L51N 99+50E	233.4	48.7	7.8	73	.1	5.0	46.3	900	5.50	1.2	.3	1.1	.3	49	.4	.2	.2	143	.34	.059	2	9	.57	54	.130	1	1.42	.009	.02	<1	.04	1.6	<.1	.13	13	.5
L51N 99+75E	29.4	54.9	7.9	34	.2	3.9	3.2	130	2.72	1.5	.4	3.6	1.0	29	.2	.2	.2	94	.19	.039	3	13	.32	30	.174	<1	3.04	.011	.02	.2	.11	2.1	<.1	.09	15	1.1
L51N 100+00E	17.9	16.0	6.8	10	<.1	1.3	1.2	73	.32	<.5	.2	3.7	.1	17	.1	.1	.1	19	.12	.017	3	4	.09	27	.095	<1	.81	.008	.01	<.1	.05	.6	<1<.05	9	<.5	
L51N 100+25E	11.6	89.7	4.8	27	.2	4.2	3.9	147	3.40	<.5	.6	2.9	1.7	16	.2	.1	.1	71	.10	.050	4	13	.32	33	.122	<1	3.22	.012	.02	.2	.20	2.3	<.1<.05	9	1.6	
L51N 100+50E	133.5	211.8	6.9	23	.5	2.1	5.8	106	1.01	<.5	3.2	3.0	.2	31	.2	.1	.1	26	.19	.051	8	6	.16	79	.070	1	1.88	.012	.02	.2	.14	1.2	<.1<.05	10	.8	
L51N 100+75E	29.7	71.1	6.2	30	.4	2.0	2.1	81	2.70	.8	.8	4.0	1.3	15	.1	.1	.1	66	.08	.056	4	11	.14	33	.078	<1	3.70	.010	.01	.1	.28	2.7	<.1<.05	10	.7	
L51N 101+00E	20.8	23.6	7.8	21	.2	2.1	1.8	84	3.03	1.5	.6	2.7	1.0	13	.1	.2	.1	75	.11	.030	3	11	.12	16	.084	1	2.23	.008	.01	.1	.06	1.4	<.1<.05	11	<.5	
L51N 101+25E	247.7	153.8	6.8	29	.5	4.5	4.0	203	3.34	1.9	4.9	1.1	3.1	13	.2	.2	.1	67	.09	.117	7	15	.28	25	.122	<1	8.65	.012	.02	.2	.28	4.9	<.1<.05	9	2.3	
L51N 101+50E	57.6	20.1	4.0	13	.2	1.8	1.6	66	2.77	<.5	.2	2.7	.6	14	.1	.2	.1	105	.08	.014	2	11	.10	19	.167	<1	1.43	.010	.01	.1	.05	.7	<.1<.05	12	<.5	
L51N 102+25E	1.9	6.9	1.1	4	.1	.5	.8	57	1.20	<.5	.1	1.3	.3	20	<.1	.1	<.1	36	.06	.006	2	5	.03	23	.051	1	.30	.013	.01	.1	.01	.2	<.1<.05	3	<.5	
L51N 102+50E	3.1	42.9	4.6	24	.4	3.2	2.3	94	2.58	1.6	.3	2.8	1.3	10	.1	.2	.1	76	.09	.061	2	13	.15	15	.099	<1	2.59	.010	.01	<.1	.09	1.9	<.1<.05	9	.5	
L51N 102+75E	.5	2.2	4.8	3	<.1	.2	.4	27	.35	.9	.1	<.5	.2	21	.1	.4	.1	46	.14	.005	1	1	.02	7	.084	1	.90	.004	.01	<.1<.01	.8	<.1<.05	10	<.5		
L51N 103+50E	3.4	25.4	6.7	36	.1	1.8	3.3	150	4.44	1.5	.2	5.1	1.1	12	.1	.4	.2	144	.09	.027	2	12	.30	14	.235	<1	2.93	.012	.02	.1	.15	2.0	<.1<.05	21	.6	
L51N 103+75E	8.6	19.0	4.7	15	.1	2.4	2.2	76	3.41	1.4	.2	1.7	.6	13	.1	.3	.2	121	.10	.017	2	11	.14	13	.168	1	1.25	.007	.02	<.1	.04	.7	<.1<.05	15	<.5	
L51N 104+00E	2.6	4.6	2.4	6	<.1	.8	1.3	49	1.82	.7	.1	3.5	.5	6	<.1	.2	.1	79	.04	.008	2	8	.02	6	.085	<1	.35	.004	.01	<.1	.02	.3	<.1<.05	7	.5	
L51N 104+25E	11.4	111.0	2.7	32	.3	4.2	4.4	170	2.33	1.2	.6	5.7	2.0	30	.2	.1	<.1	64	.21	.031	5	11	.37	43	.103	<1	2.83	.032	.02	.2	.08	2.4	<.1<.05	5	.5	
L51N 104+50E	10.9	124.5	4.4	24	.2	2.3	2.6	100	3.36	1.6	.5	1.7	2.6	15	.1	.2	.1	86	.11	.026	2	16	.20	18	.151	2	3.93	.014	.02	.1	.17	2.3	<.1	.10	11	<.5
L51N 104+75E	4.5	12.2	6.4	9	.4	1.1	1.3	46	2.58	1.6	.3	3.8	.8	27	<.1	.4	.2	79	.07	.012	3	6	.07	22	.251	<1	1.45	.009	.01	.1	.06	.8	<.1<.05	13	.7	
L51N 105+00E	70.2	255.4	5.2	93	.4	3.1	4.7	308	3.73	1.5	1.6	5.8	3.0	63	.2	.1	.2	59	.39	.065	7	13	.51	56	.148	<1	7.32	.011	.04	.6	.14	3.2	<.1	.08	11	2.8
L51N 105+25E	76.0	144.7	5.2	93	.6	9.8	4.1	322	5.26	2.0	.7	2.5	2.3	16	.2	.1	.1	117	.07	.042	3	55	.81	39	.302	<1	6.36	.009	.05	.1	.22	5.5	<.1	.10	15	2.2
L51N 105+50E	22.4	35.6	5.3	14	.2	2.4	1.6	56	2.26	1.9	.3	4.2	.3	15	.2	.2	.1	83	.10	.027	2	6	.09	21	.143	1	1.18	.008	.02	.2	.07	.5	<.1	.06	10	.7
L51N 105+75E	26.0	82.7	4.8	38	.4	4.1	4.8	173	4.27	1.9	.4	1.7	.6	20	.3	.2	.1	101	.11	.028	3	12	.39	29	.161	<1	1.96	.011	.03	.1	.10	.9	<.1	.08	13	1.1
L51N 106+00E	13.5	124.6	4.4	25	.3	3.2	3.1	128	3.54	1.9	1.0	1.0	2.4	16	.1	.1	.1	77	.10	.056	6	13	.27	26	.133	<1	5.54	.015	.02	.2	.16	4.0	<.1	.10	10	1.9
L51N 106+25E	6.1	21.4	5.1	11	.2	2.2	1.9	48	3.66	1.9	.3	2.8	.9	13	.1	.2	.1	90	.10	.022	3	9	.13	23	.162	<1	2.33	.009	.02	.1	.11	1.3	<.1	.11	16	.8
L51N 106+75E	2.5	71.9	3.7	16	.2	2.8	3.4	125	2.16	.6	.9	4.6	1.7	16	.1	.1	<.1	58	.13	.027	6	11	.26	23	.103	<1	3.58	.019	.01	.2	.08	3.3	<.1	.06	6	1.6
L51N 107+00E	13.2	119.6	4.8	23	.5	3.4	2.7	112	2.56	1.5	.6	3.4	1.8	16	.1	.1	.1	57	.11	.034	4	11	.25	31	.103	2	3.97	.014	.02	.2	.18	3.0	<.1	.06	8	1.7
L50N 99+00E	78.5	1244.0	9.5	96	.8	8.0	177.6	18285	2.10	1.4	3.1	3.0	.4	22	1.8	.2	.1	42	.22	.189	16	19	.26	89	.050	<1	5.62	.015	.03	.1	.25	1.9	.7	.09	9	3.5
L50N 99+25E	68.6	610.4	8.5	117	.4	8.4	133.0	1704	3.35	1.5	1.2	1.1	1.2	18	1.1	.2	.2	60	.18	.064	9	16	.31	43	.125	2	5.91	.013	.03	.2	.11	2.0	.1	.07	10	1.9
L50N 99+50E	40.5	40.7	4.3	18	.3	2.4	2.1	85	2.57	1.0	.5	3.3	1.4	14	.1	.1	.1	75	.09	.025	2	14	.16	20	.113	1	2.56	.011	.01	.1	.19	1.7	<.1<.05	7	1.0	
L50N 99+75E	109.6	99.9	5.8	42	.2	5.0	4.2	198	3.50	1.9	1.4	4.0	2.4	17	.2	.2	.1	84	.13	.059	6	18	.35	29	.151	<1	4.26	.014	.03	.3	.15	3.0	<.1	.09	10	1.8
L50N 100+00E	44.9	62.0	6.4	27	.1	4.2	3.2	549	3.06	2.3	.7	2.6	2.7	14	.1	.2	.1	74	.15	.102	2	15	.27	23	.141	1	4.81	.013	.03	.3	.17	1.8	<.1<.05	10	.5	
L50N 100+25E	42.8	26.9	5.8	11	.2	1.8	1.9	59	3.38	2.8	.5	4.7	2.3	9	.1	.2	.2	97	.06	.137	3	15	.10	20	.151	<1	4.58	.009	.02	.1	.21	2.3	<.1<.05	16	1.2	
RE L50N 100+25E	42.5	27.1	5.5	10	.2	1.9	1.9	60	3.35	2.6	.4	2.1	2.2	9	<.1	.2	.1	94	.06	.136	3	14	.10	20	.145	2	4.58	.009	.02	.1	.21	2.3	<.1<.05	15	.9	
L50N 100+50E	27.7	77.8	5.2	28	.1	5.2	4.2	154	3.51	1.5	.4	3.2	1.5	16	.1	.2	.1	87	.11	.042	2	17	.35	40	.118	1	2.97	.011	.02	.2	.11	1.7	<.1<.05	9	1.0	
STANDARD DS7	19.6	111.8	71.9	408	.9	53.7	9.0	627	2.37	49.2	5.0	70.1	4.6	74	6.4	6.4	4.8	83	.94	.078	12	153	1.03	391	.129	42	.92	.076	.45	4.2	.22	2.3	4.5	.24	5	4.5



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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K ppm	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.1	2.0	2.5	42	<.1	3.1	3.7	512	1.95	<.5	2.5	<.5	3.9	69	<.1	<.1	.1	36	.60	.077	7	7	.62	188	.128	2	.89	.076	.46	<.1	<.01	2.0	.4	<.05	5	<.5
L50N 100+75E	35.6	66.4	5.5	23	.2	4.5	4.2	145	3.36	.8	.4	1.5	1.4	22	.1	.2	.1	90	.11	.037	3	17	.37	38	.121	2	3.07	.013	.03	.2	.10	2.6	<.1	<.05	10	1.5
L50N 101+00E	14.0	62.6	6.0	30	.2	3.5	2.7	116	3.35	2.3	.6	3.0	2.1	16	.1	.2	.2	77	.10	.052	3	15	.21	30	.096	<1	3.60	.010	.02	.4	.11	2.3	<.1	<.05	10	1.4
L50N 101+25E	14.4	72.7	8.0	26	.6	2.4	2.5	141	3.05	1.0	.3	1.9	1.2	10	.1	.2	.2	78	.09	.026	2	12	.13	22	.102	1	2.37	.009	.01	.2	.11	1.5	<.1	<.05	10	.6
L50N 101+50E	52.2	59.1	7.7	17	.6	1.7	1.8	86	4.35	1.9	.3	4.7	.8	15	.1	.3	.2	136	.07	.051	3	12	.10	45	.173	<1	2.75	.008	.01	.1	.19	1.5	<.1	<.05	21	.9
L50N 101+75E	21.5	59.0	5.5	30	.5	2.7	2.2	90	2.90	1.3	.4	2.6	1.2	12	.1	.2	.1	67	.09	.041	3	11	.13	41	.055	1	2.95	.010	.01	.2	.19	1.5	<.1	<.05	9	1.0
L50N 102+25E	10.9	59.3	5.8	55	.3	4.2	3.0	108	3.41	1.1	.4	2.3	1.8	13	.2	.2	.1	82	.09	.043	4	16	.23	53	.102	1	4.23	.010	.02	.1	.08	2.4	<.1	<.05	12	.7
L50N 102+50E	1.8	14.8	4.9	27	.2	3.6	3.1	101	2.30	.9	.1	7.5	.4	24	<.1	.1	.1	66	.11	.019	2	20	.29	16	.101	2	1.78	.008	.01	<.1	.05	1.6	<.1	<.05	11	<.5
L50N 102+75E	5.2	27.7	5.1	28	.3	3.0	2.4	83	2.75	1.0	.3	1.9	1.1	11	.1	.2	.1	85	.09	.024	3	14	.17	16	.114	2	2.49	.010	.01	.1	.07	2.2	<.1	<.05	10	<.5
L50N 103+00E	23.8	46.5	5.2	18	<.1	3.6	1.6	86	.40	.5	.2	4.7	.2	33	.5	.2	.1	14	.32	.013	3	13	.17	45	.067	<1	.54	.009	.02	<.1	.04	1.1	<.1	<.05	6	.6
L50N 103+25E	5.8	48.6	6.3	36	<.1	3.3	2.4	88	3.59	1.7	.5	1.6	2.3	12	.2	.2	.1	88	.09	.034	2	21	.20	18	.149	<1	5.43	.011	.01	.1	.04	3.7	<.1	<.05	11	.7
L50N 103+50E	5.7	34.9	5.2	36	.1	2.8	2.6	92	2.94	1.0	.3	3.0	1.4	13	.3	.2	.1	77	.09	.012	2	12	.19	21	.145	1	3.64	.013	.01	.1	.08	2.5	<.1	<.05	11	1.2
L50N 103+75E	34.7	198.0	8.5	50	.1	3.0	8.0	190	1.32	<.5	1.1	3.2	.4	14	.2	.2	.2	40	.11	.059	9	10	.18	36	.089	<1	3.88	.010	.02	.1	.12	2.0	<.1	<.05	13	1.3
L50N 104+00E	9.5	42.3	4.6	12	<.1	1.8	1.7	51	3.31	2.1	.4	1.2	1.7	9	.2	.2	.1	81	.08	.043	3	12	.12	14	.145	<1	5.50	.010	.01	.2	.18	2.3	<.1	<.05	11	1.2
L50N 104+25E	14.1	91.5	7.5	58	<.1	2.5	2.4	138	3.91	2.3	.8	1.6	3.4	20	.2	.1	.1	71	.08	.028	7	14	.25	37	.153	<1	7.22	.008	.02	.1	.13	4.0	<.1	.07	17	1.6
L50N 104+50E	9.7	4.0	2.0	2	<.1	.7	.8	45	.74	<.5	.1	1.5	.5	4	<.1	.2	.1	26	.03	.005	2	4	.01	4	.042	5	.13	.005	.01	<.1	.02	.2	<.1	<.05	2	<.5
L50N 104+75E	24.9	8.3	2.6	11	<.1	.6	.8	88	1.12	<.5	.2	<.5	.5	13	.1	.1	.1	34	.19	.010	2	4	.09	16	.088	<1	.42	.008	.02	<.1	.02	.4	<.1	.07	5	<.5
L50N 105+00E	58.8	31.6	5.7	113	.1	1.1	4.0	126	.90	<.5	.6	<.5	.3	27	.2	.2	.1	26	.14	.018	6	3	.20	47	.050	<1	1.15	.008	.02	.1	.03	.9	.1	.08	11	<.5
L50N 105+25E	11.3	89.8	6.7	23	.2	2.1	1.8	59	4.29	2.4	1.1	2.6	4.5	6	.1	.2	.2	74	.07	.050	4	19	.14	13	.148	<1	9.30	.008	.01	.2	.23	6.0	<.1	.17	12	2.3
L50N 105+50E	31.4	107.0	4.6	42	.3	2.2	3.0	164	3.51	1.3	.9	5.4	2.0	23	.1	.1	.1	55	.10	.096	6	12	.32	38	.092	<1	6.72	.011	.02	.2	.17	3.1	<.1	.08	10	1.9
L50N 105+75E	117.2	334.4	8.9	65	.2	2.7	10.4	408	6.67	8.1	1.3	14.5	1.3	200	.2	.3	.2	35	.37	.140	5	6	.55	80	.073	<1	2.48	.019	.05	2	.05	2.1	<.1	.18	6	3.2
L50N 106+00E	9.5	52.2	7.9	16	.2	1.8	1.9	76	3.33	2.6	.8	1.3	1.8	15	.1	.2	.1	67	.08	.056	5	10	.15	25	.133	<1	5.95	.010	.02	2	.23	3.0	<.1	.10	14	1.4
L50N 106+25E	2.3	5.1	6.9	15	.2	6	2.1	103	1.74	1.3	.1	<.5	.2	30	.1	.3	.1	83	.28	.025	1	<1	.20	5	.188	<1	.71	.006	.01	.1	.06	.8	<.1	<.05	9	<.5
L50N 106+50E	34.6	48.6	6.6	37	.4	1.8	2.5	132	3.86	1.8	.5	.7	1.1	32	.4	.3	.2	68	.15	.030	4	5	.25	58	.110	<1	5.00	.012	.03	2	.23	2.1	<.1	.08	16	1.4
L50N 106+75E	94.3	143.4	8.1	41	.3	2.4	3.0	136	7.29	4.0	.3	2.2	.9	65	.2	.4	.2	82	.15	.037	2	9	.25	83	.130	1	2.90	.009	.03	2	.15	.8	<.1	.11	25	.9
L50N 107+00E	1.7	7.1	11.3	7	.4	.5	1.4	76	.90	.7	.1	1.0	.1	39	.1	.9	.1	89	.29	.009	1	<1	.11	5	.361	<1	.49	.004	<.01	<.1	.03	.6	<.1	.07	4	<.5
L49N 98+75E	4.6	39.9	6.8	20	.2	1.9	2.0	79	4.12	2.2	.3	1.3	1.1	18	.1	.4	.2	125	.09	.037	2	11	.14	21	.199	<1	2.31	.008	.01	.1	.07	1.1	<.1	.08	20	.8
L49N 99+00E	4.6	39.0	6.1	20	.4	2.4	1.9	118	2.83	1.6	.4	10.1	1.9	11	.1	.2	.1	75	.12	.039	3	14	.15	19	.115	<1	3.19	.010	.01	.1	.24	2.0	<.1	<.05	10	1.0
L49N 99+25E	5.7	59.2	6.8	21	.1	2.2	1.8	86	4.18	2.2	.5	3.5	2.8	7	.1	.3	.1	108	.07	.069	3	21	.14	16	.156	<1	6.07	.010	.01	.1	.07	3.0	<.1	.10	13	1.3
L49N 99+50E	10.3	44.4	6.5	20	.2	3.1	2.2	87	4.13	1.9	.3	.6	1.7	10	.2	.3	.2	115	.08	.046	2	15	.15	20	.174	<1	2.75	.008	.02	.1	.14	1.2	<.1	<.05	15	.6
L49N 99+75E	8.7	91.3	5.3	23	.2	3.9	2.9	130	2.32	2.0	.8	2.9	2.0	15	.1	.1	.1	54	.12	.052	4	13	.31	18	.102	<1	3.86	.014	.02	.2	.19	2.9	<.1	.08	7	1.3
L49N 100+00E	7.1	38.6	7.6	21	.2	3.4	2.2	82	4.23	2.1	.5	1.9	2.4	9	.1	.3	.2	101	.07	.046	3	20	.16	17	.161	1	5.47	.011	.01	.1	.12	2.9	<.1	.12	15	1.2
L49N 100+25E	117.9	126.3	7.6	42	.4	3.3	2.7	161	2.98	2.4	1.1	2.2	2.4	20	.2	.2	.1	54	.09	.076	4	12	.26	61	.063	<1	4.17	.011	.03	.1	.23	2.5	<.1	<.05	7	1.5
L49N 100+50E	180.6	89.2	7.5	19	.1	3.2	2.5	98	4.23	1.4	.4	7	3.0	2.3	.9	<.1	.2	82	.08	.041	3	16	.18	22	.122	<1	3.64	.011	.02	.2	.30	2.9	<.1	.06	10	.9
RE L49N 100+50E	181.5	88.6	7.7	20	.1	2.9	2.4	95	4.11	1.6	.4	6.3	3.3	2.2	.9	.1	.2	82	.08	.041	4	16	.18	22	.125	2	3.58	.011	.02	.2	.28	2.8	.1	.06	10	1.1
STANDARD DS7	19.5	112.9	73.2	408	.9	54.2	9.6	628	2.50	47.1	4.9	72.8	4.8	74	6.3	6.4	4.9	81	.96	.074	13	155	1.09	379	.125	39	.96</td									



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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P ppm	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.3	2.1	2.7	40	<.1	3.4	3.8	502	1.91	<.5	2.4	.8	3.9	67	<.1	<.1	.1	35	.54	.083	7	7	.57	188	.129	<1	.92	.075	.44	.1	<.01	1.8	.3	<.05	5	<.5
L49N 100+75E	51.3	25.9	11.8	16	.3	1.8	1.7	58	3.34	2.2	.5	1.1	1.7	15	.1	.2	.2	60	.06	.085	3	12	.12	57	.034	<1	4.61	.009	.02	.2	.09	2.0	<.1	<.05	10	.7
RE L49N 100+75E	50.3	26.9	11.4	17	.3	1.7	1.6	59	3.43	2.7	.4	2.4	1.7	15	<.1	.2	.1	60	.06	.084	3	13	.12	57	.033	<1	4.56	.009	.02	.2	.09	2.1	<.1	<.05	11	1.0
L49N 101+00E	56.4	73.3	6.3	26	.3	3.2	3.1	115	3.33	1.6	.5	3.3	1.8	13	.1	.2	.1	77	.09	.036	3	15	.27	33	.110	<1	3.77	.014	.02	.3	.16	2.3	<.1	<.05	10	1.1
L49N 101+25E	206.0	50.5	6.9	28	.3	4.1	3.1	132	4.06	4.3	.4	1.1	1.6	11	.1	.3	.1	88	.09	.059	2	18	.29	25	.131	1	3.85	.009	.03	.2	.14	2.2	<.1	.09	13	1.0
L49N 101+50E	9.3	2.0	2.6	6	.3	.3	.4	16	.53	<.5	.1	.8	.2	8	<.1	<.1	.1	9	.02	.017	2	4	.04	20	.004	<1	1.04	.010	.02	.1	.04	.4	<.1	<.05	5	<.5
L49N 101+75E	36.9	23.2	3.8	47	.3	3.1	3.4	174	2.91	1.2	2.0	1.3	1.5	29	.2	.1	.1	43	.19	.062	4	8	.47	48	.126	<1	4.47	.010	.02	.3	.15	2.1	<.1	.07	10	1.2
L49N 102+00E	23.3	33.1	5.0	23	.4	1.6	1.6	70	3.32	1.9	.4	4.0	1.1	20	.1	.3	.1	69	.16	.056	2	10	.13	20	.194	<1	2.70	.010	.01	.3	.09	1.3	<.1	.07	11	.7
L49N 102+50E	4.5	28.8	5.2	24	.3	2.4	2.3	68	3.24	1.3	.3	4.7	1.5	10	.2	.3	.1	89	.07	.024	2	14	.14	16	.140	<1	3.39	.010	.01	.1	.16	1.8	<.1	<.05	12	.8
L49N 102+75E	7.8	49.8	5.3	16	.2	2.6	2.5	98	3.42	2.5	.6	8.5	3.1	9	.1	.2	.1	82	.07	.050	2	19	.16	17	.140	1	5.87	.012	.01	.2	.26	3.6	<.1	.06	10	1.2
L49N 103+00E	13.3	12.1	7.7	7	.1	.7	.8	53	2.28	1.2	.2	1.0	.6	24	.1	.2	.2	69	.20	.030	2	3	.04	7	.204	<1	.90	.006	.01	<.1	.04	1.2	<.1	.06	10	<.5
L49N 103+25E	1.2	6.2	1.8	5	.1	.6	.8	31	.95	.6	.1	2.1	.6	4	<.1	<.1	<.1	23	.02	.009	5	3	.02	10	.033	<1	.91	.008	.01	.1	.02	.5	<.1	<.05	6	<.5
L49N 103+50E	6.0	42.6	6.0	17	<.1	2.3	2.4	102	4.12	2.1	.5	1.7	2.8	10	.1	.2	.1	83	.08	.065	2	16	.23	14	.170	<1	4.94	.011	.02	.2	.07	1.8	<.1	.07	13	1.0
L49N 103+75E	6.8	18.2	2.6	16	<.1	.6	.6	87	1.37	.9	.3	1.0	1.0	6	<.1	.1	.1	43	.03	.018	4	3	.14	9	.091	<1	.44	.008	.02	<.1	.02	.4	<.1	<.05	8	<.5
L49N 104+00E	1.3	5.5	1.7	5	<.1	1.2	1.7	47	2.16	.6	.1	2.0	.4	6	.1	.2	.1	77	.05	.010	2	6	.04	9	.057	1	.30	.009	.02	<.1	.02	.3	<.1	.06	4	<.5
L49N 104+25E	12.2	46.9	7.5	16	.3	1.5	1.2	59	3.36	1.2	.8	2.7	2.2	8	.2	.2	.1	65	.05	.026	3	12	.11	15	.122	<1	4.11	.008	.01	<.1	.17	2.5	<.1	.07	16	1.8
L49N 104+50E	7.8	60.4	5.8	26	.2	2.2	2.3	81	2.65	1.0	.4	4.5	1.8	12	.4	.1	.1	65	.07	.024	3	12	.16	36	.125	1	4.53	.012	.01	.1	.20	2.7	<.1	<.05	11	1.0
L49N 104+75E	14.9	11.3	3.4	14	.3	1.1	1.5	66	1.91	1.2	.3	.7	.8	13	<.1	.2	.1	81	.07	.018	2	5	.10	9	.156	2	.43	.007	.02	.1	.03	.4	<.1	<.05	10	<.5
L49N 105+25E	4.0	38.9	4.6	23	.2	2.1	1.9	66	2.85	1.5	.4	2.6	1.1	12	.2	.2	.1	71	.08	.031	4	11	.14	23	.127	1	3.79	.009	.01	.1	.16	2.2	<.1	.08	13	1.6
L49N 105+50E	10.5	13.7	5.9	10	.2	1.2	.8	39	3.46	2.0	.3	.8	.7	11	.1	.3	.2	92	.08	.021	3	7	.04	19	.162	1	1.87	.007	.01	.1	.15	.8	<.1	<.05	22	1.1
L49N 105+75E	14.2	20.2	5.5	15	.3	1.3	1.0	60	2.90	1.9	.4	<.5	1.0	13	.1	.2	.2	59	.05	.030	2	7	.10	29	.126	1	2.63	.009	.01	.1	.19	1.2	<.1	.06	13	1.1
L49N 106+00E	20.0	57.7	10.6	33	.1	1.5	.9	166	2.78	4.1	.9	2.4	1.2	11	.2	.2	.1	46	.10	.079	4	10	.27	26	.124	1	4.75	.010	.04	.1	.25	3.0	<.1	.09	12	2.1
L48N 98+50E	4.4	557.8	5.6	26	.8	3.3	2.1	65	1.76	.8	1.3	2.7	.4	12	.4	.2	.1	41	.09	.067	10	14	.16	25	.062	1	4.96	.011	.01	.1	.21	2.2	<.1	.12	6	2.5
L48N 98+75E	4.3	72.0	5.1	20	.3	3.6	2.9	107	3.14	1.9	.5	3.7	2.9	12	.1	.2	.1	71	.08	.032	2	20	.27	22	.131	1	5.62	.013	.02	.1	.15	3.0	<.1	.06	9	.7
L48N 99+00E	12.0	107.1	6.2	23	.1	2.9	2.7	121	3.51	2.0	.6	2.2	3.1	19	.2	.2	.1	70	.10	.033	2	17	.27	26	.139	1	5.76	.014	.02	.2	.10	2.6	<.1	.06	11	<.5
L48N 99+25E	13.3	100.2	8.0	29	.1	2.8	2.5	122	4.13	2.1	.7	2.4	2.1	14	.2	.3	.2	100	.08	.051	3	16	.23	29	.178	2	5.47	.009	.02	.1	.13	2.8	<.1	.06	18	.8
L48N 99+50E	3.6	27.6	4.1	15	.2	2.0	1.6	71	2.12	1.1	.2	4.1	.8	7	.1	.2	.1	70	.06	.022	2	9	.11	17	.076	<1	1.36	.008	.01	<.1	.08	.8	<.1	.06	9	<.5
L48N 99+75E	5.5	58.1	4.9	25	.4	3.8	3.3	102	3.19	1.5	.4	1.7	1.9	12	.1	.2	.1	76	.08	.040	2	16	.22	31	.124	1	4.74	.012	.02	.1	.11	2.2	<.1	<.05	10	.5
L48N 100+00E	7.9	52.0	6.6	19	.8	3.2	2.6	111	2.96	2.2	.4	2.5	1.9	12	.1	.2	.1	63	.08	.033	2	14	.24	23	.114	2	3.78	.011	.02	.2	.29	1.7	<.1	<.05	10	.8
L48N 100+25E	2.0	4.3	1.5	3	<.1	.5	.7	44	1.24	.6	.1	1.2	.5	9	<.1	.1	.1	48	.05	.006	2	5	.02	10	.069	<1	.40	.007	.01	<.1	.03	.4	<.1	<.05	6	<.5
L48N 100+50E	21.8	85.4	9.2	21	.3	2.4	2.2	100	4.55	3.5	1.2	1.8	4.6	8	<.1	.3	.2	97	.07	.075	5	17	.22	21	.139	2	7.37	.011	.01	.1	.16	4.4	<.1	.07	20	1.0
L48N 100+75E	4.7	4.3	3.3	10	.2	.6	.7	75	1.03	1.0	.3	.7	.6	5	<.1	.1	.1	22	.04	.008	2	4	.08	6	.094	1	.44	.009	.01	<.1	.03	.3	<.1	<.05	4	<.5
L48N 101+00E	44.4	34.0	4.3	12	.5	1.7	1.6	74	2.66	.9	.2	2.6	.7	9	.1	.2	.1	72	.08	.013	3	10	.12	19	.083	<1	1.72	.008	.01	.1	.24	1.0	<.1	<.05	8	<.5
L48N 101+25E	5.8	45.8	4.9	14	.2	2.8	2.8	112	3.06	1.4	.4	4.0	1.6	11	.1	.3	.1	82	.08	.027	2	15	.22	17	.103	2	3.30	.011	.01	<.1	.21	2.4	<.1	<.05	11	<.5
L48N 101+50E	15.1	34.3	4.8	20	.2	1.7	2.0	92	3.56	2.7	.2	9.9	.9	12	.1	.3	.2	94	.10	.095	2	11	.16	12	.165	1	2.50	.010	.01	.2	.04	.9	<.1	<.05	14	<.5
STANDARD DS7	19.2	99.1	70.9	391	.9	50.5	8.7	605	2.31	46.1	4.9	69.0	4.3	74	6.1	6.4	4.7	74	.86	.076	12	151	1.06	376	.116	44	.94	.072	.43	4.0	.20	2.1	4.4	.22	5	4.6



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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca ppm	P %	La ppm	Cr ppm	Mg ppm	Ba ppm	Ti ppm	B %	Al ppm	Na ppm	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.2	2.7	3.1	42	<.1	3.1	3.8	540	1.88	<.5	2.5	2.0	4.1	69	<.1	<.1	.1	35	.58	.085	7	7	.68	186	.123	<1	.96	.077	.46	.1	<.01	2.0	.3	.07	5	<.5
L48N 101+75E	8.7	69.7	4.1	33	.2	3.1	3.1	87	3.22	1.3	.3	2.5	1.0	12	.2	.1	87	.10	.030	2	16	.20	22	.163	<1	3.38	.013	.01	.3	.13	1.9	<.1	.13	11	.5	
L48N 102+00E	3.6	29.6	5.5	15	.2	1.5	1.6	48	3.68	1.7	.3	2.4	1.8	9	.1	.2	1	92	.08	.042	2	14	.08	15	.133	<1	4.58	.010	.01	.1	.21	2.3	<.1	.14	12	.6
L48N 102+25E	2.5	27.9	3.4	12	<.1	.8	1.0	71	2.11	<.5	.1	1.8	.4	5	<.1	.1	.1	70	.05	.033	2	5	.10	9	.217	<1	.51	.007	.01	<.1	.02	.4	<.1	.06	10	<.5
L48N 102+50E	1.1	4.6	1.5	4	<.1	1.1	1.5	54	1.45	<.5	.1	.9	.4	8	<.1	.1	.1	54	.06	.006	3	12	.01	4	.052	<1	.20	.007	.01	<.1	.01	.4	<.1	<.05	4	<.5
L48N 102+75E	5.7	35.8	6.3	17	.2	2.0	2.0	77	2.82	1.1	.4	2.3	1.6	11	.1	.2	.1	75	.09	.046	2	11	.14	15	.122	<1	3.02	.010	.01	.1	.10	1.4	<.1	.08	11	<.5
L48N 103+00E	3.4	34.0	8.0	19	.2	2.2	2.1	76	4.42	1.4	.4	1.9	2.4	10	.1	.3	.2	103	.07	.092	3	16	.14	19	.163	<1	5.16	.010	.01	.1	.33	2.4	<.1	.08	20	1.0
L48N 103+25E	3.8	25.7	7.9	13	<.1	1.5	1.4	54	3.56	1.9	.4	3.7	2.5	6	.1	.2	.2	80	.05	.034	3	14	.11	11	.124	3	4.93	.010	.01	.1	.15	2.7	<.1	.10	12	.7
L48N 103+50E	8.2	58.2	22.6	33	.2	2.1	2.0	87	4.78	3.3	.9	3.2	2.7	13	.2	.3	.2	79	.10	.047	4	11	.14	27	.190	<1	6.73	.010	.02	.2	.30	3.6	<.1	.10	13	1.6
L48N 103+75E	533.7	551.8	41.5	145	.3	3.7	214.3	3569	8.10	2.6	1.1	2.9	.4	39	.3	.2	.4	265	.23	.103	8	11	.33	125	.123	2	3.48	.014	.03	.2	.14	1.5	.2	.09	26	2.7
L48N 104+00E	28.8	195.5	10.2	34	.6	2.4	4.0	176	6.83	3.9	1.3	3.9	3.2	34	.3	.2	.2	91	.21	.043	6	12	.34	39	.258	<1	7.00	.012	.04	.2	.27	3.3	<.1	.12	28	1.2
L48N 104+25E	19.3	50.0	7.2	89	.2	4.4	4.3	345	4.53	1.4	.4	.6	1.2	12	.7	.2	.1	145	.13	.038	3	11	.70	36	.359	<1	1.70	.011	.10	<.1	.06	2.1	<.1	<.05	24	.5
L48N 104+50E	16.5	13.9	4.4	16	.1	1.2	1.5	93	1.73	1.0	.2	.6	.8	7	.1	.1	.1	62	.09	.017	2	4	.07	8	.135	<1	.60	.008	.01	<.1	.06	.5	<.1	<.05	10	<.5
L48N 104+75E	52.2	99.0	9.7	242	.2	3.8	5.8	296	3.81	3.7	1.4	1.4	1.9	21	.4	.3	.3	78	.13	.049	5	13	.45	28	.098	2	4.36	.011	.03	.3	.18	2.6	<.1	.09	13	1.2
L48N 105+00E	5.4	12.2	5.2	18	.2	1.0	.9	85	2.03	1.3	.4	1.1	1.6	13	.2	.1	.1	35	.08	.025	3	8	.07	23	.040	2	3.10	.010	.01	<.1	.18	2.0	<.1	.07	7	<.5
L48N 105+25E	14.6	39.7	6.8	27	.1	2.1	2.1	97	3.89	2.4	.7	15.1	1.7	17	.1	.2	.2	90	.11	.037	3	11	.17	28	.145	1	2.95	.011	.02	.1	.21	2.0	<.1	<.05	14	.5
L48N 105+50E	24.9	14.4	2.4	15	.1	.6	.6	52	1.34	1.1	.4	2.0	.3	55	.1	.1	<.1	40	.07	.026	2	4	.08	26	.075	2	.70	.011	.02	.1	.06	.6	<.1	<.05	7	<.5
L48N 105+75E	19.6	18.5	7.0	12	<.1	1.3	1.3	62	3.55	2.4	.3	2.6	.9	14	.1	.3	.2	106	.07	.032	2	6	.10	15	.222	<1	1.56	.007	.01	<.1	.08	.8	<.1	<.05	18	<.5
L48N 106+00E	19.0	20.8	5.8	12	.2	.7	.9	48	2.53	1.5	.4	.9	.9	13	.1	.1	.1	58	.04	.023	3	5	.06	22	.104	2	2.34	.009	.01	<.1	.20	1.3	<.1	<.05	12	.8
L47+50N 98+00E	10.3	332.2	4.5	30	.1	4.4	2.9	138	.85	.7	1.8	6.5	.3	19	.2	.1	.1	24	.14	.058	14	9	.35	53	.056	1	3.86	.013	.02	.2	.11	2.1	<.1	<.05	6	1.1
L47+50N 98+25E	2.1	5.5	4.9	4	<.1	.2	.3	22	.20	<.5	.2	3.1	.1	9	.2	.1	.1	8	.04	.013	3	1	.01	21	.025	2	.49	.007	.01	<.1	.03	.3	<.1	<.05	5	<.5
RE L47+50N 98+25E	2.2	6.7	4.9	3	<.1	.4	.3	21	.21	<.5	.2	2.1	.1	9	.2	.1	.1	9	.04	.015	3	1	.01	21	.025	1	.49	.008	.02	<.1	.04	.4	<.1	<.05	4	.5
L47+50N 98+50E	20.4	61.4	6.8	22	.4	2.7	2.0	72	4.35	2.1	.2	6.3	.9	10	<.1	.3	.3	161	.07	.056	2	15	.17	16	.228	2	1.91	.009	.02	.2	.07	.6	<.1	<.05	25	<.5
L47+50N 98+75E	7.2	43.7	7.8	18	.2	1.5	1.6	167	3.30	2.4	.6	<5	3.1	7	.1	.2	.1	77	.07	.044	3	17	.12	13	.097	3	5.95	.009	.02	.1	.21	3.7	<.1	.13	11	1.4
L47+50N 99+00E	4.5	53.2	9.9	14	<.1	1.9	1.5	64	4.07	1.9	.7	<5	2.5	8	.1	.2	.2	87	.07	.062	4	14	.10	15	.129	1	4.73	.011	.02	.1	.24	2.6	<.1	.10	16	1.1
L47+50N 99+25E	12.9	202.9	10.9	42	.2	3.6	3.4	108	3.69	2.1	1.3	2.4	2.7	11	.1	.1	.1	70	.07	.092	7	15	.26	22	.127	2	6.50	.012	.02	.2	.19	4.0	<.1	.13	10	2.1
L47+50N 99+50E	11.2	50.7	8.1	32	<.1	3.2	2.3	105	5.80	2.4	.4	6.0	1.8	10	.1	.4	.3	173	.07	.056	2	18	.22	18	.237	3	3.30	.009	.02	.1	.06	1.9	<.1	.08	24	.5
L47+50N 99+75E	4.5	72.7	8.5	18	.2	2.5	2.1	93	3.89	2.3	1.0	1.6	3.5	10	.1	.2	.2	98	.07	.081	4	16	.23	19	.168	2	5.78	.012	.02	.2	.20	4.3	<.1	.13	16	1.6
L47+50N 100+00E	5.9	55.1	9.1	21	.4	3.5	2.8	99	4.43	2.4	.6	3.8	1.9	11	.1	.3	.2	120	.08	.043	3	17	.20	25	.199	2	5.19	.008	.02	.1	.19	2.0	<.1	.06	22	1.1
L47+50N 100+25E	6.3	44.6	6.8	17	.1	2.5	2.3	83	3.10	1.3	.4	3.7	1.6	10	.1	.2	.2	87	.09	.029	3	13	.18	17	.141	2	2.78	.010	.01	.1	.07	1.9	<.1	<.05	12	.8
L47+50N 100+50E	2.9	29.4	6.7	13	<.1	2.1	2.1	77	3.81	2.5	.3	4.4	1.5	9	.1	.3	.2	116	.07	.054	2	14	.15	12	.169	3	3.11	.009	.02	<.1	.11	1.8	<.1	.08	20	.9
L47+50N 100+75E	1.1	5.4	4.2	6	<.1	.8	1.1	53	.58	.5	.1	1.9	.4	18	<.1	.1	.1	36	.18	.009	1	2	.10	7	.125	<1	.52	.005	.01	.1	.01	.8	<.1	<.05	4	<.5
L47+50N 101+00E	5.1	145.3	6.4	22	.2	2.8	2.6	102	2.79	1.1	.6	2.1	1.4	11	.1	.2	.1	77	.09	.031	3	10	.22	18	.130	3	3.07	.010	.01	.1	.18	2.0	<.1	.06	12	.6
L47+50N 101+25E	4.9	64.7	5.8	37	.2	2.9	2.9	77	2.85	.7	.3	3.7	1.2	10	.1	.2	.1	84	.09	.021	3	11	.16	25	.112	3	2.28	.010	.01	<.1	.11	1.6	<.1	<.05	11	.9
L47+50N 101+50E	70.7	409.0	10.7	198	.3	6.0	233.9	14445	4.75	1.9	2.1	<.5	.5	28	5.2	.2	.1	46	.33	.116	12	8	.09	100	.023	3	5.10	.013	.02	.1	.19	2.7	.6	.20	4	2.9
STANDARD DS7	19.4	118.7	79.3	400	.9	53.2	9.3	607	2.35	4																										



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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi %	V ppm	Ca ppm	P ppm	La ppm	Cr ppm	Mg ppm	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.2	1.8	2.9	40 <.1	3.2	4.0	505	1.83	<.5	2.6	<.5	4.0	73 <.1	<.1	.1	36	.57	.086	7	7	.59	209	.129	<1	.88	.078	.45	.1 <1	.01	1.9	.3 <.05	5 <.5				
L47+50N 101+75E	9.9	111.9	5.5	17 .8	2.5	2.2	104	3.29	1.5	.3	.8	1.5	12 .1	.2	.2	89	.08	.023	3	15	.15	15	.121	<1	2.52	.012	.02	.1	.21	1.7	<.1 <.05	10 <.5				
L47+50N 102+00E	6.0	103.0	5.4	17 .2	2.5	2.9	330	2.43	1.1	.5	3.6	1.6	16 .1	.1	.1	65	.13	.044	3	11	.22	18	.102	2	3.06	.016	.02	.2	.13	2.2	<.1 <.05	7 .9				
L47+50N 102+25E	6.4	32.7	6.5	13 .2	1.2	1.3	51	3.47	1.4	.3	2.5	1.1	8 <.1	.3	.2	108	.06	.028	2	11	.06	12	.102	<1	2.65	.009	.01	.1	.13	1.5	<.1 <.05	14 <.5				
L47+50N 102+50E	13.7	159.0	8.7	52 .6	2.6	2.7	95	3.90	2.2	.6	9.2	2.0	12 .1	.2	.1	83	.09	.058	4	15	.19	31	.118	1	5.44	.009	.02	.1	.40	3.4	<.1 <.05	15 1.8				
L47+50N 102+75E	25.2	179.2	7.2	44 .2	2.2	2.0	81	3.27	2.0	.4	3.0	2.1	11 .2	.2	.1	86	.07	.064	3	17	.18	20	.123	1	6.07	.009	.02	.2	.19	2.1	<.1 <.05	12 1.2				
L47+50N 103+00E	22.5	115.4	5.5	26 <.1	2.0	1.8	85	4.30	2.0	.3	1.9	1.6	13 .2	.2	.2	118	.10	.062	3	14	.13	17	.155	<1	3.38	.009	.02	.1	.09	1.4	<.1 <.05	18 .5				
L47+50N 103+50E	69.8	546.5	56.6	34 .6	2.8	22.1	316	2.65	1.0	1.1	2.1	.3	19 .2	.2	.2	58	.14	.056	5	10	.23	32	.108	1	3.61	.010	.02	.1	.20	1.3	<.1 .06	10 2.2				
L47+50N 103+75E	10.7	54.3	8.8	18 .2	2.0	1.8	72	3.22	1.6	.6	2.2	2.6	10 .1	.3	.2	110	.06	.032	4	16	.17	17	.220	1	6.73	.009	.01	.1	.18	2.8	<.1 <.05	21 .8				
L47+50N 104+00E	21.4	48.7	5.1	22 .2	2.0	2.6	94	3.92	1.8	.3	2.3	1.0	60 .1	.2	.2	99	.09	.028	2	11	.15	36	.194	1	2.28	.010	.02	.3	.08	1.3	<.1 <.05	15 1.0				
L47+50N 104+25E	6.0	98.5	4.3	29 .2	3.1	3.0	127	3.21	1.2	.7	4.1	2.4	14 .2	.1	.1	63	.10	.054	4	14	.26	22	.112	1	5.72	.015	.01	.2	.19	2.5	<.1 <.05	8 1.4				
L47+50N 104+50E	14.2	112.0	6.3	46 .4	2.0	2.7	119	4.97	3.7	.9	4.3	1.7	12 .2	.2	.2	83	.06	.070	7	11	.11	28	.164	4	8.18	.009	.01	.2	.41	3.3	<.1 .06	17 2.2				
L47+50N 104+75E	13.6	40.1	8.1	29 .5	1.7	1.6	76	4.87	2.1	.4	1.4	2.4	12 .1	.2	.2	89	.05	.095	3	14	.13	29	.138	2	6.06	.008	.01	.1	.20	2.0	<.1 <.05	17 .7				
L47+50N 105+00E	13.6	24.6	7.8	14 <.1	1.6	1.5	56	5.92	2.9	.3	2.2	2.3	9 <.1	.5	.3	147	.06	.063	2	14	.10	15	.240	1	3.54	.007	.01	.1	.11	1.1	<.1 <.05	28 <.5				
RE L47+50N 105+00E	13.5	25.1	7.9	14 <.1	1.7	1.5	57	6.08	3.2	.3	25.2	2.1	8 <.1	.4	.3	146	.06	.060	2	14	.10	14	.237	2	3.47	.007	.01	.1	.13	1.1	<.1 <.05	29 .5				
L47+50N 105+25E	13.8	45.9	6.2	21 <.1	2.4	2.0	95	2.98	2.3	.8	.8	2.2	14 .1	.2	.2	65	.08	.076	5	12	.24	27	.138	1	5.52	.010	.02	.6	.22	2.3	<.1 <.05	15 2.1				
L47+50N 105+50E	14.1	6.1	8.1	5 <.1	.8	.5	36	2.22	.5	.2	2.2	.6	9 .1	.4	.3	114	.06	.020	2	5	.04	8	.298	1	.59	.005	.01	<.1	.04	.2	<.1 <.05	19 <.5				
L47+50N 105+75E	3.6	5.3	2.4	4 <.1	.6	.5	32	1.18	<.5	.1	.6	.2	7 <.1	.1	.1	32	.06	.014	1	3	.02	6	.039	2	.53	.007	.01	<.1	.03	.2	<.1 <.05	5 <.5				
L47+50N 106+00E	39.8	26.6	5.4	24 .1	2.3	1.9	116	2.81	.9	.5	1.6	.1	28 <.1	.1	.1	62	.11	.042	2	6	.21	21	.061	2	.94	.010	.03	.1	.08	.5 <.1 <.05	9 .7					
STANDARD DS7	18.1	93.2	68.6	372 1.0	49.0	8.4	568	2.17	45.6	4.7	82.2	4.4	75	5.6	6.1	4.9	74	.88	.071	12	138	1.01	374	.114	37	.90	.071	.42	3.9	.20	2.1	4.0	.19	4 3.2		

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.