BC Geological Survey
Assessment Report
29765h

Schaft Creek Project -

ML-ARD Assessment of Surficial Samples from the Proposed Access Road

prepared for:

Rescan Environmental Services Ltd.
Attn: Mr. Soren Jensen
Sixth Floor,
1111 West Hastings Street.
Vancouver, British Columbia V6E 2J3

prepared by:

Kevin A. Morin, Ph.D., P.Geo., L.Hydrogeo.
Nora M. Hutt, A.Sc.T, c.C.T.
Minesite Drainage Assessment Group
A Division of Morwijk Enterprises Ltd.
8035 Redtail Court,
Surrey, British Columbia V3W 0N4

February 20, 2008

P.Geo. and A.Sc.T. Notice

This study is based on detailed technical information interpreted through standard and advanced chemical and geoscientific techniques available at this time. As with all geoscientific investigations, the findings are based on data collected at discrete points in time and location. In portions of this report, it has been necessary to infer information between and beyond the measured data points using established techniques and scientific judgement. In our opinion, this report contains the appropriate level of geoscientific information to reach the conclusions stated herein.

This study has been conducted in accordance with British Columbia provincial legislation as stated in the Engineers and Geoscientists Act and in the Applied Science Technologists and Technicians Act.

Kevin A. Morin, Ph.D., P.Geo.
Registration No. 18,721
Association of Professional
Engineers and Geoscientists

Nora M. Hutt, A.Sc.T., c.C.T.
Registration No. 10700
Association of Applied Science
Technologists and Technicians

TABLE OF CONTENTS

List of Tables

List of Figures

Executive Summary

For the Schaft Creek Project, a proposed access road reaches from km 0 in the south, at the Galore Creek access road, to km 39.5 at the proposed plantsite and minesite. Most of the surficial geological material along the proposed road alignment is sediment and alluvium, but rock is exposed in places.

Based on direct and indirect information, the potential for metal leaching (ML) and acid rock drainage (ARD) was ranked for the surficial geological materials along the alignment. These rankings were as follows.

1. Negligible to Minor (green)
2. Moderate, or Unknown, or Beyond Current Analytical Capability suggesting caution (yellow)
3. High to Severe (red)

The results are compiled in Table ES-1.

Recommendations were offered in Chapter 6 for more detailed ML-ARD characterization of sediment and rock, including deeper material that may be disturbed during construction and quarrying. These recommendations should be carried out before, during, and after road construction.

Table ES-1. ML-ARD Rankings for Surficial Sediments and Surficial Rock along the Proposed Alignment of the Schaft Creek Access Road

Road Section (km)	Surficial Sediment Ranking [1]		Surficial Rock Ranking [1,3]	
	ARD[2]	ML	ARD	ML
0-2	1	3	1	1
2-3	1	3	2	2
3-5	1	3	1	3
5-10	1	3	1	1
10-15	1	3	3	3
15-25	1	3	2	2
25-28	1	3	2	3
28-34	1	1	1	3
34-36	1	3	1	1
36-39.5	1	3	2	2

[1] Ranking 1 = Negligible to Minor (green); Ranking 2 = Moderate, or Unknown, or Beyond Current Analytical Capability suggesting caution (yellow); Ranking 3 = High to Severe (red); elevated solid-phase levels are used as surrogates for the ML rankings, although aqueous metal leaching is not necessarily dependent on solid-phase levels.

[2] ARD potential for surficial sediments is based on only four samples, and is thus not reliable over the entire alignment; ML potential was based on many more samples, from other studies.

[3] The number of surficial rock samples (8) does not provide thorough coverage of surficial rock along the road alignment. However, much of the alignment lies on sediments and alluvium, not rock. Mineral potential and iron staining are used for rankings at km 5-24 and at km 34-39.5.

Report Summary

Metal leaching (ML) and acid rock drainage (ARD) are often water-chemistry issues for many minesites. As a result, the accurate prediction and control of ML-ARD at minesites in British Columbia are high priorities of the provincial government. This is explained in British Columbia's formal Policy, Guidelines, and draft Prediction Manual.

In addition to minesites, ML-ARD issues have also arisen at roads and highways, because they can also disturb rock and unconsolidated sediments during construction. Thus, British Columbia's ML-ARD documents can also be generally applied to them. Recent ML-ARD precedents established in Canada for roads and highways include the following.

1) Successful criminal prosecution under the *Fisheries Act* for ML-ARD from a road cut a few meters high and a few hundred meters long.
2) Visual examination of every horizontal meter of rock cut along dozens of kilometers of road alignment, with sampling and analysis as appropriate.
3) Major re-alignment of a highway to avoid disturbance of potentially acid-generating rock.
4) Special environmental controls and remediation for reactive rock removed from rock cuts and quarries and for broken rock used in the road bed.
5) Failure of geologic maps, preconstruction environmental and geologic surveys, and surficial sampling of exposures to identify all geochemically reactive rock reliably.

As part of the Schaft Creek Project, an access road has been proposed. It extends from km 0, at the Galore Creek Access Road, generally northward to km 39.5 near the proposed plantsite and minesite. Some rock quarries and sand-gravel pits may be needed.

This report assessed the ML-ARD potential of the surficial geological materials along the proposed alignment. This assessment was based on pre-existing "indirect" information from various sources, like the provincial Minfile website and air photos, and on "direct" information, like ML-ARD sampling by the authors.

Indirect ML-ARD Information

Indirect ML-ARD information started at the Ministry of Energy, Mines and Petroleum Resources' Minfile and MapPlace website, which provided details of watersheds, surficial geology, bedrock geology, Regional Geochemical Studies (RGS), and nearby mineral deposits and showings. Another source of indirect ML-ARD for this study was air photographs of the road alignment and nearby areas.

The proposed access road passes through two primary watersheds. Most of the road alignment is in the Mess Creek watershed, which drains to the north. A small section, approximately 1.5 km long at the southern end, lies in the More Creek watershed that drains east and south to the Iskut River.

Maps and air photos showed that much of the proposed road alignment lies on the unconsolidated alluvium in the Mess Creek valley. Most of the alignment was covered by trees and other vegetation, and was thus not readily visible. If unconsolidated sediments were composed of locally weathered bedrock, their geochemistry may reflect weathered aspects of the bedrock. If the sediments were transported large distances by water and/or glaciers, then their geochemistry may bear little resemblance to the underlying bedrock. Thus, unconsolidated alluvium was not automatically assumed to have a similar ML-ARD potential as the underlying or nearby bedrock. However, if local rock had a high potential and the potential of local sediment could not be determined, then the sediments were assumed in this report to have the same potential as rock.

Bedrock geology, mostly hidden below the unconsolidated sediments in the Mess Creek valley, is complex. Zones of volcanic, intrusive, sedimentary, and metamorphic rock are mixed, sometimes on a relatively small scale. If ML-ARD potential is related to rock types, then the potential can be highly variable over short distances along the proposed road.

The potential for enriched metals and other minerals can sometimes serve as a proxy for ML-ARD potential. Metallic-mineral potential along the proposed access-road alignment, from the provincial MapPlace website, showed that areas near the road ranged from the lowest mineral potential to the highest. The highest-potential zone coincided with a band of sedimentary rock from ~km 10 to ~km 15. Also, two zones of second-highest potential were at ~km 15-26 and ~km 36-39.5.

Another general indicator of ML-ARD potential can be mineral claims, prospects, and showings. The provincial Minfile site showed two developed mineral prospects and four mineral showings near the proposed road or in tributaries of Mess Creek. All six contained potentially acid-generating sulphide-borne metals like iron, copper, cadmium, arsenic, and/or molybdenum. All six also contained some carbonate minerals, but it was not clear if the carbonate was sufficient to prevent ARD. RGS (Regional Geochemical Survey) water pH values (see below) showed that, just to the north and east of one mineral showing, values as low as 4.5 were measured. Even without ARD, near-neutral metal leaching would remain a concern in these areas. Therefore, along the nearby proposed road alignment, ~km 4-17 and ~km 21-26 were given high, indirect ML-ARD potentials.

The RGS data from the provincial government provided aqueous pH measurements and solid-phase analyses of sediment near the proposed road alignment. Based on aqueous measurements, most pH values upstream of and near the road alignment were around 6.9 to 8.1. The lowest value of 4.5 was found in a tributary to the north and east of one mineral showing, suggesting ARD was actively produced in that tributary.

Solid-phase levels of metals and other elements do not necessarily produce accelerated leaching rates into water. In fact, some solid-phase levels might be high due to slow leaching, but laboratory kinetic tests and detailed RGS water analyses were not available to resolve this. In any case, the RGS surveys provided selected solid-phase elements in alluvium sediments near the proposed road alignment and in tributaries to Mess Creek. Based on solid-phase antimony, arsenic, copper, mercury, nickel, and zinc, the portions of the road alignment with relatively elevated levels included the aforementioned ~km 4-17 and ~km 21-26. Some elements like copper were less variable along the length of the alignment. Also, one sample, only with elevated copper and zinc, was found at the north end of the alignment, around km 34.

The final indirect source of ML-ARD potential came from air photographs, which provided targets for “direct” ML-ARD sampling and analyses (see below). Surficial rusty-coloured iron staining can sometimes signal accelerated metal leaching and/or sulphide oxidation. Such staining appeared to be present in the air photos around km 10.0-14.8 and km 22.0-23.0, which coincided with the aforementioned sections of high, indirect ML-ARD potential. Iron staining was also apparent around: km 0.0, which may be from natural organic processes in the local wetlands; km 18.5-19.5, in a zone of second-highest mineral potential; and km 28-32, anomalously in a zone of lowest mineral potential. These areas of apparent iron staining could not be reached during the field visit, but could be signs of ML-ARD.

Direct ML-ARD Information

The authors of this report flew by helicopter along the proposed road alignment, collecting photographs, notes, and surficial solid-phase samples. This field study confirmed most of the alignment was covered by trees and other vegetation, and thus was not readily accessible for sampling of geological materials.

Rusty-coloured iron staining, sometimes a sign of surficial ML-ARD, was seen along some portions of the alignment. These areas could not be safely reached without additional equipment, so their ML-ARD status is unknown. However, the colouring and staining appeared consistent with locally significant ML-ARD.

Eight samples of surficial rock and four samples of surficial sediments were collected near the proposed access-road alignment. Acid base accounting (U.S. EPA 600 compliant Sobek ABA) of these samples showed that all had near-neutral paste pH at the time of analysis. Total sulphur ranged from <0.01%S in one rock sample to 0.39%S in another rock sample. Most of that total sulphur was potentially acid-generating sulphide, so the more easily measured total sulphur can be used for convenience. However, sulphur values below 0.05%S were relatively inaccurate. Three of the four highest sulphide values were found in the sediment samples, which are typically thought of as weathered and oxidized. Thus, the ARD potential of the sediments cannot be ignored.

Neutralization Potential (NP) ranged from 9 to 387 kg $CaCO_3$ equivalent/tonne, with four of the five highest NP values in sediments. Thus, the sediments contained sufficient NP to offset any internal acid generation by sulphur. In many samples, the Sobek NP was apparently mostly comprised of calcite ($CaCO_3$), which could be measured by the simpler analytical techniques for total carbon or inorganic carbonate.

Net balances of acid-generating and acid-neutralizing capacities were based on the Total-Sulphur-Based Net Potential Ratio (TNPR), with and without adjustments for unavailable NP. This showed eleven samples were net neutralizing indefinitely, plus one sample of rock that was “uncertain” without additional testing. When various amounts of unavailable NP were considered, a second sample of rock showed large changes in TNPR, suggesting the ARD status of this sample was also uncertain without additional testing.

Total-element contents of the 12 access-road samples of surficial rock and sediments were measured by ICP-MS analysis after strong four-acid digestion, and by x-ray-fluorescence (XRF) whole-rock analysis. This showed that most of the 12 access-road samples consisted predominantly of silica and alumina, with substantial and sometimes dominant amounts of iron, calcium, magnesium, sodium, potassium, and Loss on Ignition (LOI). LOI often reflects the weight loss from the samples of some or all sulphur, carbon, and tightly bound or crystalline water. Also, the 12 samples often contained elevated levels of bismuth and selenium, with fewer to rare elevated levels of silver, cadmium, chromium, phosphorus, lead, antimony, and zinc.

Solid-phase correlations of total elements can sometimes reveal mineralogical associations. For example, elements correlating with sulphide may occur predominantly within the sulphide minerals. The elements showing at least some minor correlation with sulphide included arsenic, copper, mercury, and nickel. The elements showing at least some minor correlation with Neutralization Potential, which can dissolve and release metals even without sulphide oxidation, included calcium and manganese.

The preceding information on total elements was combined with “indirect” RGS data and Rescan data along the proposed road alignment. This allowed a spatial interpretation of the data, to highlight sections of the proposed roads with higher ML potential. However, these other sources did not include ABA, so ARD potential was available only for our 12 MDAG samples. For total sulphur, the highest and lowest values were in surficial rock, between km 26 and 31. Nevertheless, some surficial sediments carried significant levels of total sulphur, which were well distributed along the road alignment. For ARD potential, the lowest, “uncertain” values were found near km 26 around Nahta Creek also near the southern end around km 2. The latter sample had low, relatively inaccurate sulphur analyses, so its ARD status was considered “uncertain”.

In areas where both surficial rock and sediment analyses were available, sediments sometimes had notably higher levels of some elements. This suggested sediments were not necessarily genetically related to local rock.

Based on selected solid-phase criteria that do not necessarily characterize ML-ARD potential accurately, the seven elements of greatest ML-ARD potential in surficial sediments were antimony, arsenic, barium, cadmium, chromium, copper, and nickel. However, these elements were only elevated along specific sections of the proposed road, and not all seven were elevated at the same location.

Similarly for surficial rock, there were 12 elements of greatest potential ML concern, plus at least an “uncertain” potential for ARD along specific sections of the proposed road. Notably, at km 32-34, eight of the 12 elements of greatest concern were elevated. The lack of rock samples from roughly km 5 to km 24, and from km 34 to km 39.5, precluded assessments there. This incorrectly implied no ML-ARD concern, because zero elements were elevated in these sections. However, indirect information from Chapter 3 was used to supplement the less abundant direct information for rock.

ML-ARD Rankings

The preceding indirect and direct ML-ARD information showed that some surficial rock had an uncertain capacity to release ARD, and more extensive areas of surficial rock and sediments might leach metals at elevated levels even at neutral pH. This was expressed spatially as ML-ARD rankings along sections of the proposed road. Separate rankings were developed for ARD and for ML, because ML can arise even without ARD. Not included here were water-quality parameters potentially created by construction activities, like suspended solids, nitrogen species from any blasting, organic compounds like fuel, and any mined rock from the proposed minesite.

The Rankings used here were based on three levels.

1. Negligible to Minor (green)
2. Moderate, or Unknown, or Beyond Current Analytical Capability suggesting caution (yellow)
3. High to Severe (red)

It is important to note that Rankings should reflect the local receiving environment, but such environmental assessments are beyond the scope of this study. For example, pre-existing high background aqueous concentrations of dissolved copper might show no additional environmental effects in the future after road construction, despite a Ranking of 2 or 3 for a road section or quarry. Thus, the Rankings here assume a pristine environment. This is not consistently the case as shown by some elevated pre-existing metal levels and sulphide in sediments and rock.

The results produced Rankings for ARD and ML that spanned the range from 1 to 3 (Table RS-1). There was no consistent spatial trend of increasing or decreasing Ranking with distance along the road. Overall, the ML Ranking along nearly the entire proposed alignment was high for surficial sediment, and was mostly moderate to high for surficial rock.

As a result, some accelerated metal leaching should be expected from the road during and after disturbance of surficial sediments and rock. However, the ML-ARD potentials of deeper sediments and rock remain unknown at this time. To clarify and improve the ML-ARD assessment of the proposed road alignment, both surficial and deeper, recommendations were offered in Chapter 6 before, during, and after road construction.

Table RS-1. ML-ARD Rankings for Surficial Sediments and Surficial Rock along the Proposed Alignment of the Schaft Creek Access Road

Road Section	Surficial Sediment Ranking [1]		Surficial Rock Ranking [1,3]	
(km)	ARD[2]	ML	ARD	ML
0-2	1	3	1	1
2-3	1	3	2	2
3-5	1	3	1	3
5-10	1	3	1	1
10-15	1	3	3	3
15-25	1	3	2	2
25-28	1	3	2	3
28-34	1	1	1	3
34-36	1	3	1	1
36-39.5	1	3	2	2

[1] Ranking 1 = Negligible to Minor (green); Ranking 2 = Moderate, or Unknown, or Beyond Current Analytical Capability suggesting caution (yellow); Ranking 3 = High to Severe (red); elevated solid-phase levels are used as surrogates for the ML rankings, although aqueous metal leaching is not necessarily dependent on solid-phase levels.

[2] ARD potential for surficial sediments is based on only four samples, and is thus not reliable over the entire alignment; ML potential was based on many more samples, from other studies.

[3] The number of surficial rock samples (8) does not provide thorough coverage of surficial rock along the road alignment. However, much of the alignment lies on sediments and alluvium, not rock. Mineral potential and iron staining are used for rankings at km 5-24 and at km 34-39.5.

1. INTRODUCTION

Metal leaching (ML) and acid rock drainage (ARD) are often water-chemistry issues for many minesites (e.g., Morin and Hutt, 1997 and 2001). As a result, the accurate prediction and control of ML-ARD at minesites in British Columbia are high priorities of the provincial government. This is explained in British Columbia's formal Policy, Guidelines, and draft Prediction Manual (Price and Errington, 1998; Price, 1998; Price et al., 1997).

In addition to minesites, ML-ARD issues have also arisen at roads and highways, because they can also disturb rock and unconsolidated sediments during construction (Morin et al., 2003; Morin and Hutt, 2005 and 2007a). Thus, British Columbia's ML-ARD documents can also be generally applied to them. Recent ML-ARD precedents established in Canada for roads and highways include the following.

1) Successful criminal prosecution under the *Fisheries Act* for ML-ARD from a road cut a few meters high and a few hundred meters long.
2) Visual examination of every horizontal meter of rock cut along dozens of kilometers of road alignment, with sampling and analysis as appropriate.
3) Major re-alignment of a highway to avoid disturbance of potentially acid-generating rock.
4) Special environmental controls and remediation for reactive rock removed from rock cuts and quarries and for broken rock used in the road bed.
5) Failure of geologic maps, preconstruction environmental and geologic surveys, and surficial sampling of exposures to identify all geochemically reactive rock reliably.

In addition to ML-ARD, road construction can also affect local water quality and downstream environments through effects like suspended solids, any blasting residues (nitrate, ammonia, etc.), and organic compounds (fuel, lubricating oil, etc.). These potential additional effects are not addressed here in this ML-ARD study.

As part of the Schaft Creek Project, ML-ARD has been characterized and predicted in detail for the ore zones (Morin and Hutt, 2007b and 2008). This information is of limited value to the proposed access road, which lies mostly at substantial distances from the ore zones.

Chapter 2 of this report discusses the layout and alignment of the proposed access road for the Schaft Creek Project. "Indirect" ML-ARD information, obtained from various existing sources, is discussed in Chapter 3. Chapter 4 presents "direct" information, based on the field study by the authors of this report. All information is combined into ML-ARD predictions for surficial materials along the road alignment in Chapter 5. Finally, recommendations are made for environmental protection against ML-ARD before, during, and after road construction in Chapter 6. All relevant data are compiled in the appendices.

2. ALIGNMENT OF THE PROPOSED ACCESS ROAD FOR THE SCHAFT CREEK PROJECT

Rescan provided UTM coordinates in NAD 83 datum and a general map of the proposed road alignment (Figure 2-1 and Appendix A). The proposed road reaches from km 0.0 km at the Galore Creek access road to km 39.5 near the proposed millsite. It follows Mess Creek, which flows northward, along most of its length. Quarries and granular-fill areas will be needed for road construction, but their locations were not provided in the time for this study.

For simplicity in this report, the linear km distance (0.0 to 39.5) is used to discuss and depict information, rather than two-dimensional UTM coordinates. However, Appendix A can be used to convert from km distance to UTM if needed.

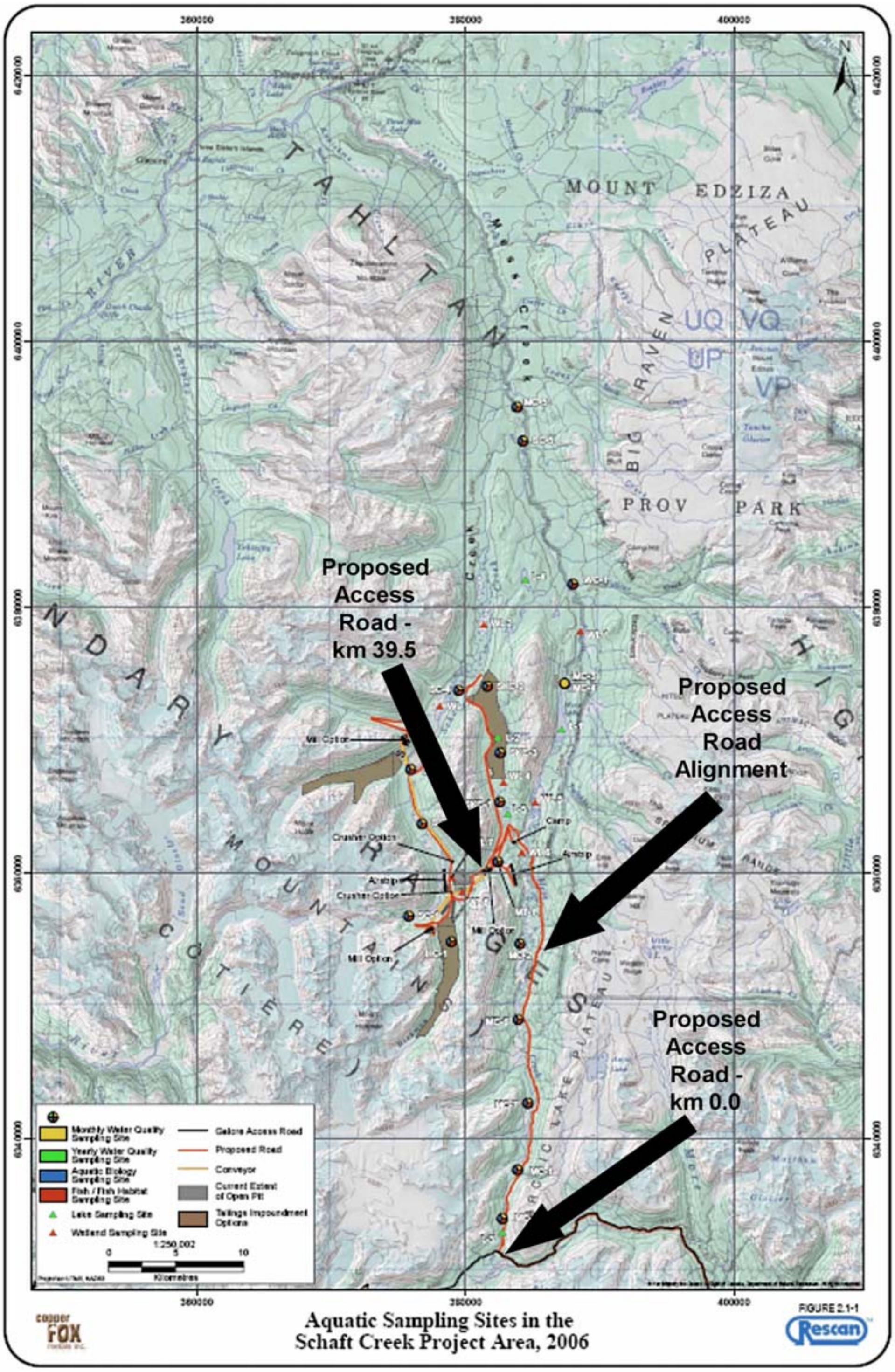


Figure 2-1. Map of the Schaft Creek Site and Proposed Access Road (adapted from Rescan, 2007).

3. EXISTING “INDIRECT” ML-ARD INFORMATION

3.1 Sources of Indirect ML-ARD Information for the Proposed Access Road

The proposed access road for the Schaft Creek Project covers a length of approximately 39.5 km (Chapter 2 and Appendix A). This probably would include potential rock quarries and sand-gravel pits that would be located some lateral distances from the road. As a result, detailed ML-ARD sampling of the entire potential disturbed area would be intensive, and still not provide all information like kinetic testing (Chapter 4). Therefore, existing, external “indirect” sources of ML-ARD information are used in this report. These sources are critical. For example, certain factors like near-neutral metal leaching can sometimes be estimated from local water quality or solid-phase analyses.

The Government of British Columbia offers excellent sources of indirect ML-ARD information. This starts at the Ministry of Energy, Mines and Petroleum Resources’ Minfile website (www.em.gov.bc.ca/Mining/Geolsurv/minfile/). Minfile provides details of nearby mineral deposits and minesites. Minfile also provides valuable links to other provincial data sources. These include Regional Geochemical Studies (RGS), which contain solid-phase and aqueous analyses, and MapPlace, which displays maps of features such as local geology, roads, RGS results, and Minfile sites.

Minfile and its links were searched for geochemical and indirect ML-ARD information along the proposed access road. The Mess Creek valley and the Schaft Creek Minfile location provided geographic identification points in this search.

Another important source of indirect ML-ARD for this study was air photographs of the road alignment. This is also discussed later in this chapter (Section 3.6).

3.2 Watersheds Along the Road Alignment

Based on the provincial MapPlace (Section 3.1), the proposed access road passes through two watersheds. The first, short portion from km 0.0 to approximately km 1.5 lies in the Iskut River watershed, with water draining to the east and then south (Figures 3-1 and 3-2). The remaining, major portion of the proposed road, from approximately km 1.5 to km 39.5, lies in the Mess Creek watershed, which drains to the north.

3.3 General Geology Along the Road Alignment

Minfile maps showed that most of the proposed road lies on Quaternary unconsolidated alluvium (Figure 3-3), often sand and/or gravel on the Mess Creek floodplain. However, on this scale of mapping, rock outcrops may not be readily apparent or stored in MapPlace. Additional clarification on this was provided by other indirect information in the following subsections and by a site visit (Chapter 4).

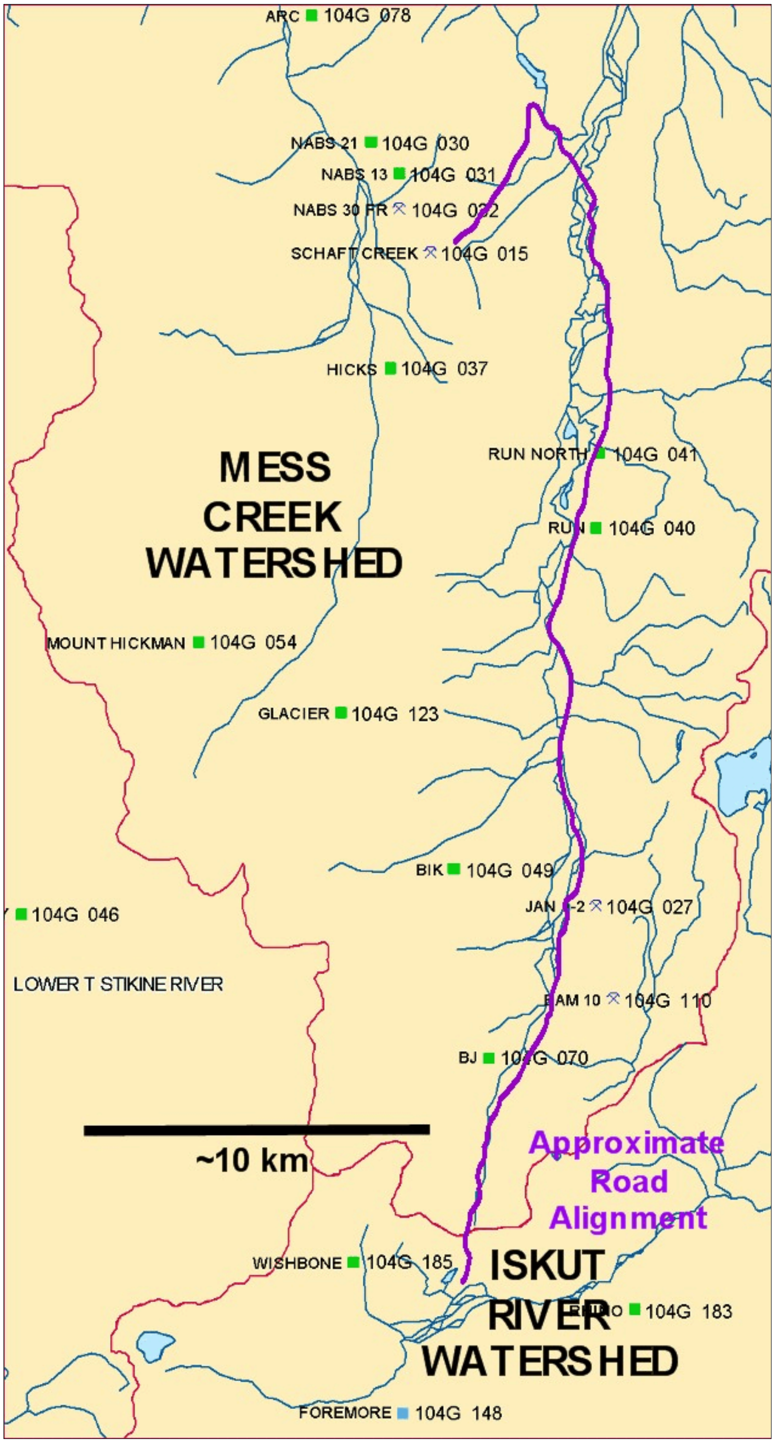


Figure 3-1. Major Watersheds along the Proposed Road Alignment (red lines mark watershed boundaries; taken from the British Columbia MapPlace website).

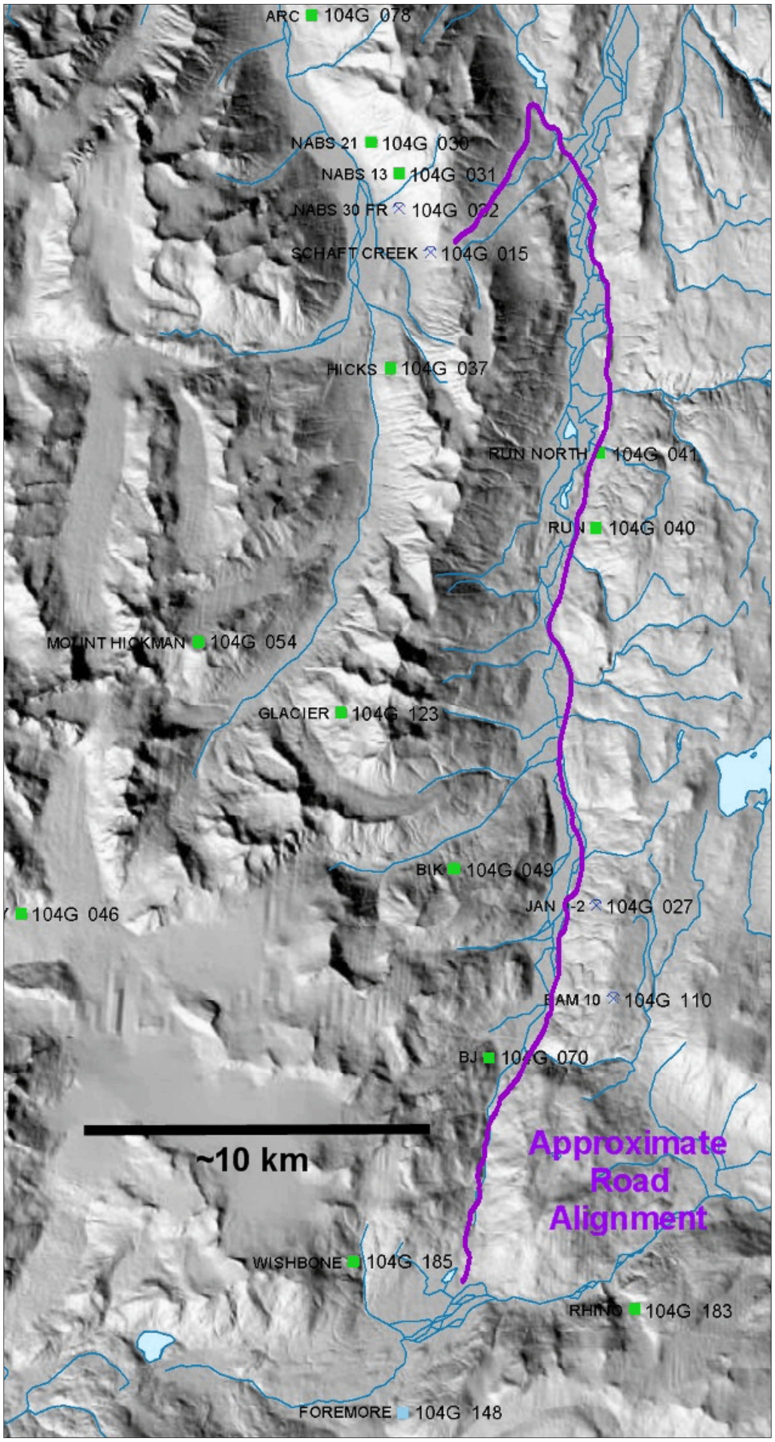


Figure 3-2. Shaded Relief Map of the Schaft Creek Area and the Proposed Access Road (taken from the British Columbia MapPlace website).

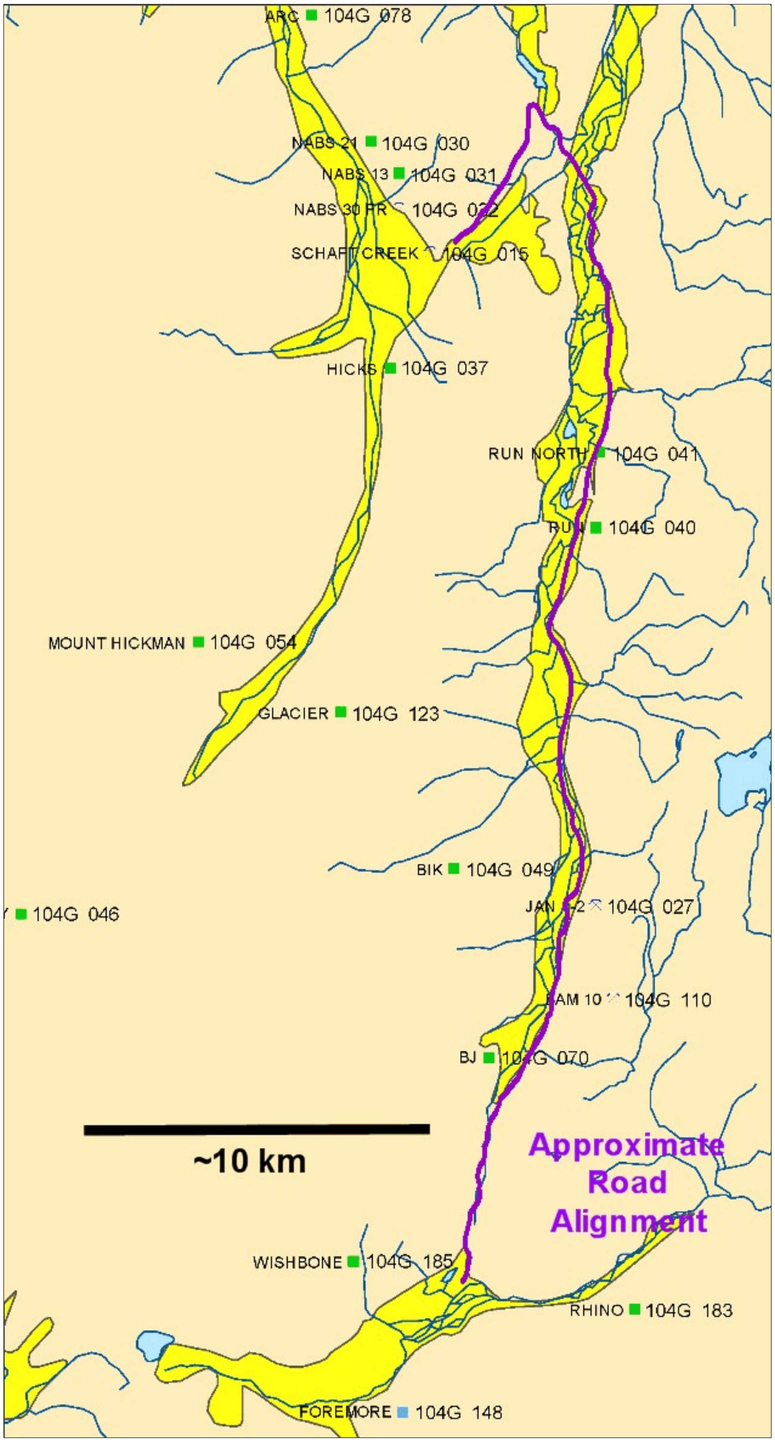


Figure 3-3. Alluvium Covering Most of the Proposed Road Alignment (alluvium shown in yellow) (taken from the British Columbia MapPlace website).

Bedrock geology, mostly hidden below the unconsolidated sediments, is complex (Figure 3-4). Rock of volcanic, intrusive, sedimentary, and metamorphic origins forms a “patchwork” around the road alignment and Mess Creek, sometimes on a relatively small scale. In some cases, ML-ARD potential can be related to rock types. If this applies to the Schaft Creek road, then the ML-ARD potential can be highly variable over short distances along the proposed road.

If unconsolidated sediments were composed of locally weathered bedrock, their geochemistry may reflect weathered aspects of the bedrock. If the sediments were transported large distances by water and/or glaciers, then their geochemistry may bear little resemblance to the underlying bedrock. Thus, unconsolidated sediments are not automatically assumed to have a similar ML-ARD potential as the underlying or nearby bedrock. However, if local rock has a high potential and the potential of local sediment cannot be determined, then the sediments are assumed in this report to have the same potential as rock. This is discussed further below, and in the direct ML-ARD analyses of Chapter 4.

3.4 Mineral Potential and Mineral Occurrences Near the Road Alignment

The local potential for metals and other minerals can serve as a proxy for ML-ARD potential. For example, occurrences of elevated levels of sulphide minerals can suggest a higher ARD potential than surrounding areas.

The provincial Minfile and MapPlace website provided a map of metallic-mineral potential along the existing access-road alignment (Figure 3-5 and Table 3-1). This showed that the southernmost, and part of the northernmost, sections lay in an area of lowest potential, while the remainder is at least second-highest potential.

The zone of highest mineral potential (Figure 3-5) coincides with a band of SSW-trending sedimentary rock (Figure 3-4). A smaller band of volcanic rock with lowest potential is embedded in this sedimentary rock, but for safety is still ranked as highest potential here (Table 3-1).

Another general indicator of ML-ARD potential can be mineral claims. The provincial Minfile website provides valuable details on certain claims, specifically mineral anomalies, showings, prospects, developed prospects, producers (operating minesites), and past producers (Figures 3-1 to 3-5). Each location is given a Minfile number and name, which leads to additional information such as geology, mineralogy, and mineral commodities. For the proposed road alignment, two developed mineral prospects (Jan 1-2 and Bam 10) and four lesser mineral showings (BJ, Bik, Run, and Run North) are relevant.

Jan 1-2 in sedimentary rock (Minfile 104G 027) and Bam 10 in intrusive rock (Minfile 104G 110) are the two developed prospects near the proposed road. The Schaft Creek deposit itself, while a developed prospect, is not included here. This is because it drains to a different valley and thus does not potentially affect ML-ARD of the road, unless mined rock is placed on the road.

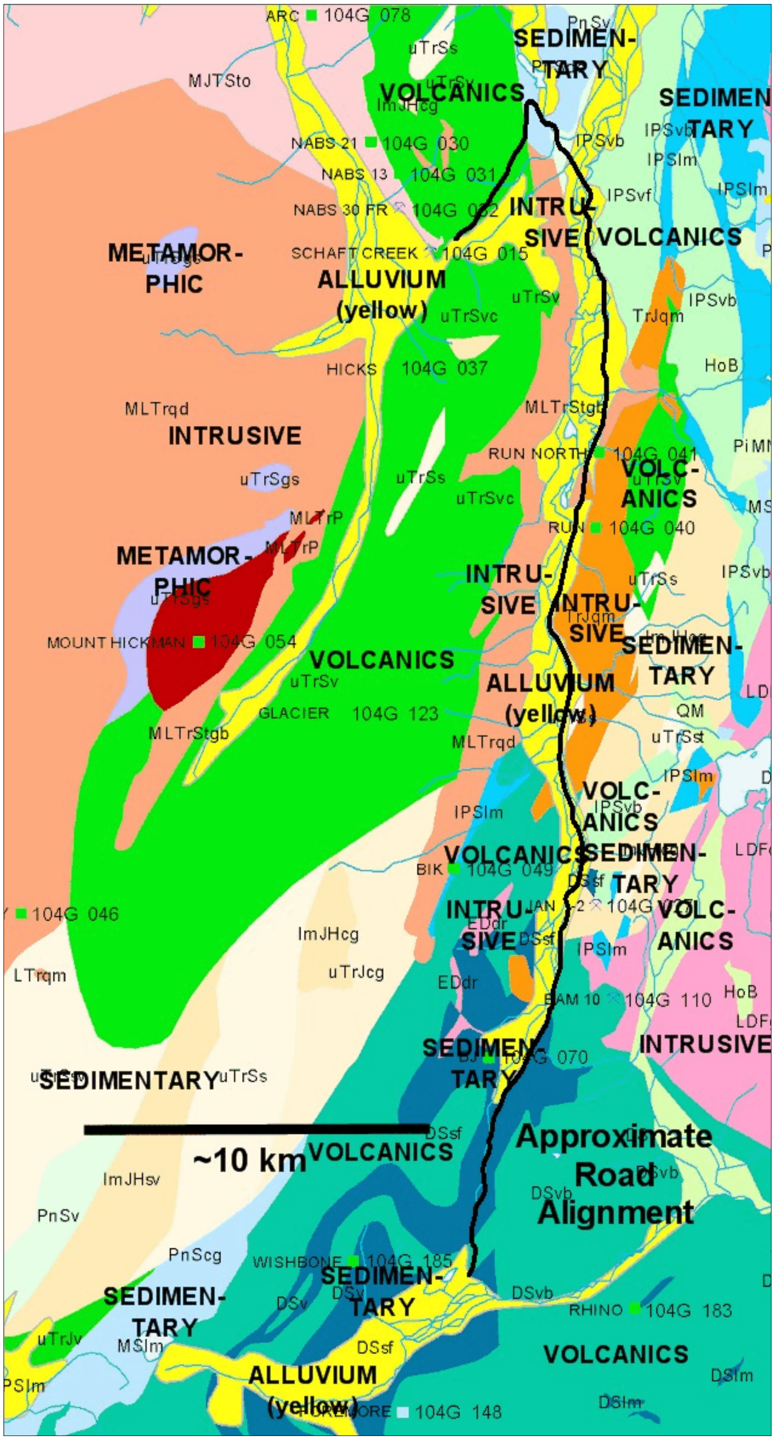


Figure 3-4. Bedrock Geology around the Proposed Road Alignment (taken from the British Columbia MapPlace website).

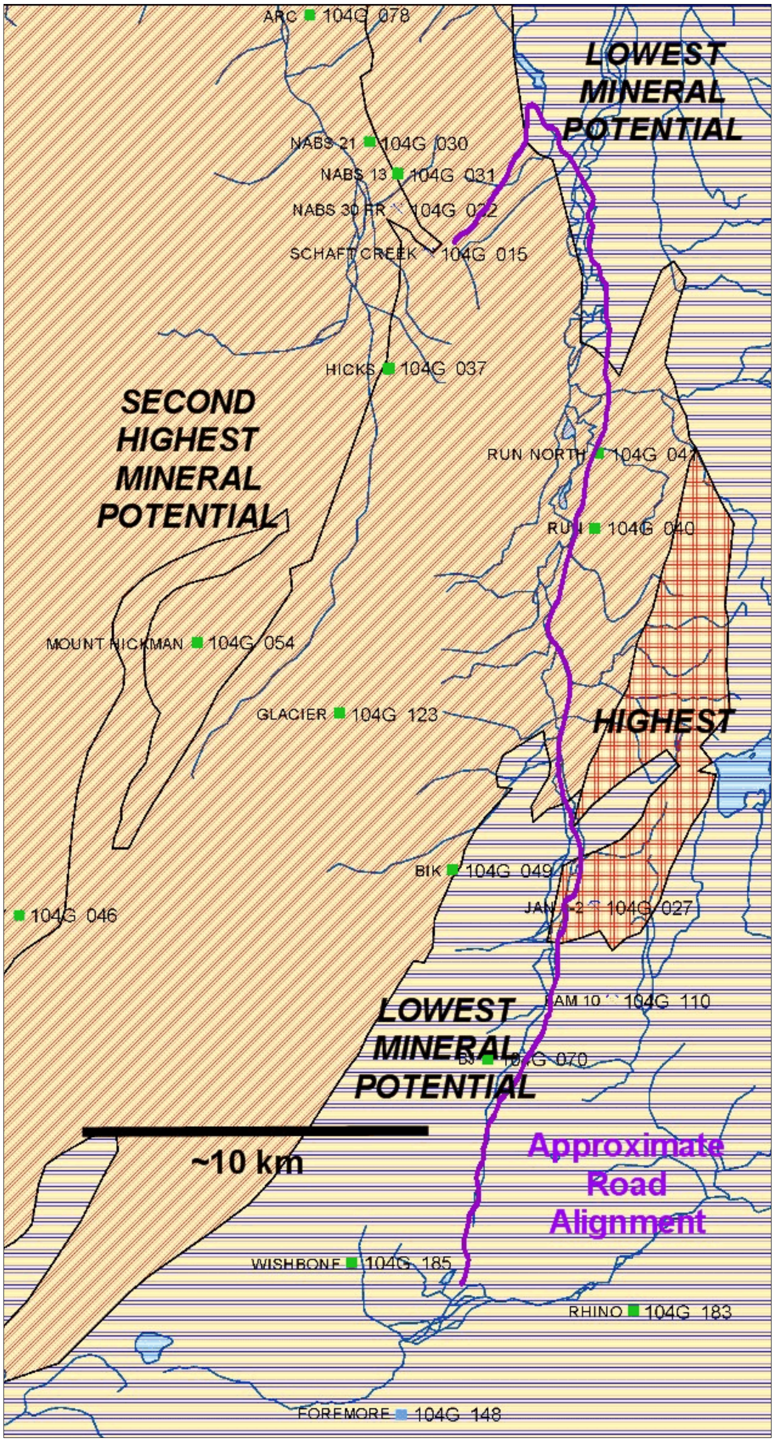


Figure 3-5. Metallic-Mineral Potential around the Proposed Road Alignment (taken from the British Columbia MapPlace website).

Table 3-1. Metallic-Mineral Potential by Distance Along the Proposed Access Road (data from British Columbia Minfile Website; see also Figure 3-4)

Distance	Metallic-Mineral Potential
0 to ~km 10	Lowest
~km 10 to ~km 15 [1]	Highest [1]
~km 15 to ~km 26	Second Highest
~km 26 to ~km 36	Lowest
~km 36 to ~km 39.5	Second Highest

[1] This Highest zone also contains some smaller segments of "Lowest" potential (Figure 3-4), but to be safe they are included here as "Highest".

Jan 1-2 and Bam 10 are pyritic sulphide deposits, with commodity elements of copper, silver, arsenic, cadmium, zinc, antimony, gold, bismuth, and barium. Thus, they mark areas of significant potential for ML-ARD from rock. The reported dark-orange limonite and iron staining at these sites suggest the sulphides have partially oxidized, but the reported limestone and dolomite may maintain near-neutral conditions. This is consistent with RGS near-neutral water-pH measurements in the area (Section 3.5). Nevertheless, near-neutral metal leaching from nearby rock, sediment, and/or drainages, including possibly some ARD, remains a potential concern for the section of the proposed road near these two sites (~km 7 to ~km 13).

The location of Jan 1-2 is within the zone of highest mineral potential (Figure 3-5), but Bam 10 in an area of lowest potential. As a result, mineral potential may not precisely coincide with ML-ARD potential.

For the two mineral showings near the southern portion of the road, BJ (Minfile 104G 070, Figures 3-1 to 3-5) and Bik (Minfile 104G 049), both contain the commodity elements of copper, silver, zinc, lead, and gold in/as sulphide minerals. The pyritic BJ showing is primarily hosted in metamorphic rock with some carbonate minerals present at least locally. Bik is hosted in limestone with some metamorphic and intrusive rock. The distance between these two showings along the proposed alignment includes Jan 1-2 and Bam 10. Thus, they extend the section of the road, with potential ML-ARD concerns in nearby rock, sediments, and drainages, from ~km 4 to ~km 17.

At Run and Run North copper-molybdenum showings (Minfile 104G 040 and 104G 041), pyrite is reported at 1-3% and as high as 10%, with some carbonate minerals present at least locally. This abundance of pyrite may explain the acidic aqueous pH values down to 4.5 reported to the north and east of Run North (Nahta Creek, Section 3.5), and thus these showings represent a significant ML-ARD potential. Consequently, the section of the proposed road encompassed by Run and Run North, and their ML-ARD significance, is from ~km 21 to ~km 24. However, acidic pH values to the north require an extension of the ML-ARD potential to the north, by roughly 2 km to ~km 26 (Section 3.5).

3.5 Regional Geochemical Surveys

The provincial government has conducted Regional Geochemical Surveys (RGS) across the province for decades (e.g., British Columbia Ministry of Energy, Mines and Petroleum Resources, 2006). The RGS program was designed primarily for exploration and geology, but can provide valuable information for environmental purposes. The RGS database contains mostly solid-phase analyses of fine-grained stream sediment, but some locations include aqueous parameters and solid-phase analyses of till, moss, and lake sediment.

The provincial Minfile and MapPlace website provided maps of the local RGS data near the proposed-access-road alignment. Water analyses focussed on pH (Figure 3-6). Aqueous pH was consistently near neutral around 6.9 to 8.1 near the road alignment and in tributaries to Mess Creek. The exception was the tributary (Nahta Creek) to the north and east of the Run North mineral showing (Section 3.5), at ~km 25.3, which produced pH values as low as 4.5. Thus, the rock and perhaps sediments in this section of the proposed road may have sufficient capacity to generate ARD, which was supported by a rock sample from the base of this valley (Chapter 4). This produces a zone of higher ML-ARD potential from close to the Run showing up to this tributary, approximately km 21 to km 26.

Elevated solid-phase levels of metals and other elements do not necessarily produce accelerated leaching rates into water. In fact, some solid-phase levels might be high due to slow leaching, but laboratory kinetic tests and detailed RGS water analyses are not available to resolve this (discussed further in Chapter 4). In any case, the RGS surveys provided solid-phase elements in alluvium sediments near the proposed road alignment and in tributaries to Mess Creek.

The RGS sediment analyses included elements like antimony, arsenic, copper, mercury, nickel, and zinc (Figures 3-7 to 3-12). In these figures, circle size was generally proportional to solid-phase concentration, but the MapPlace did not size all circles accurately. This information is used quantitatively, in more detail, in Section 4.3 of this report, combined with additional analyses from Rescan (2007). Thus, only a cursory review of the data is provided here.

The previous subsections showed that the sections of the proposed road with the highest indirect rating for ML-ARD potential were ~km 4-17 and ~km 21-26. Based on larger circles representing a greater risk for aqueous metal leaching in Figures 3-7 to 3-12, the larger circles were often found in these same sections of the proposed road. Copper (Figure 3-9), nickel (Figure 3-11), and zinc (Figure 3-12) generally showed less variability along the proposed road than the other three elements. Additionally, one sample with elevated copper and zinc was found on the north end of the road around ~km 34, but this sample was not elevated in the other elements.

Of note, the northern end of the road, running southwest towards the Schaft Creek site (km 35-39.5), did not have any samples. Therefore, although it lies in a zone of second-highest mineral potential (Figure 3-5), this could not be confirmed by solid-phase analyses.

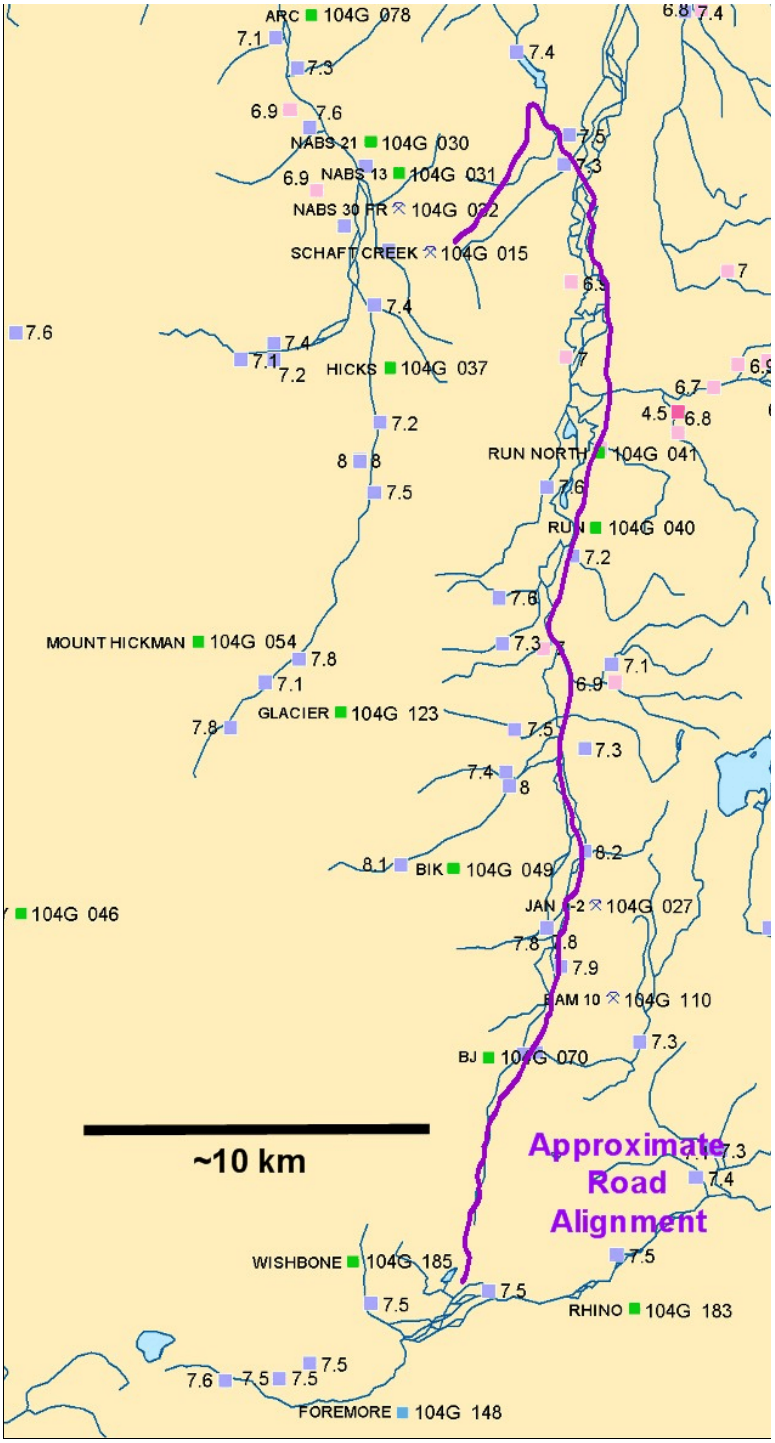


Figure 3-6. Aqueous pH from Provincial Regional Geochemical Surveys around the Proposed Road Alignment (taken from the British Columbia MapPlace website).

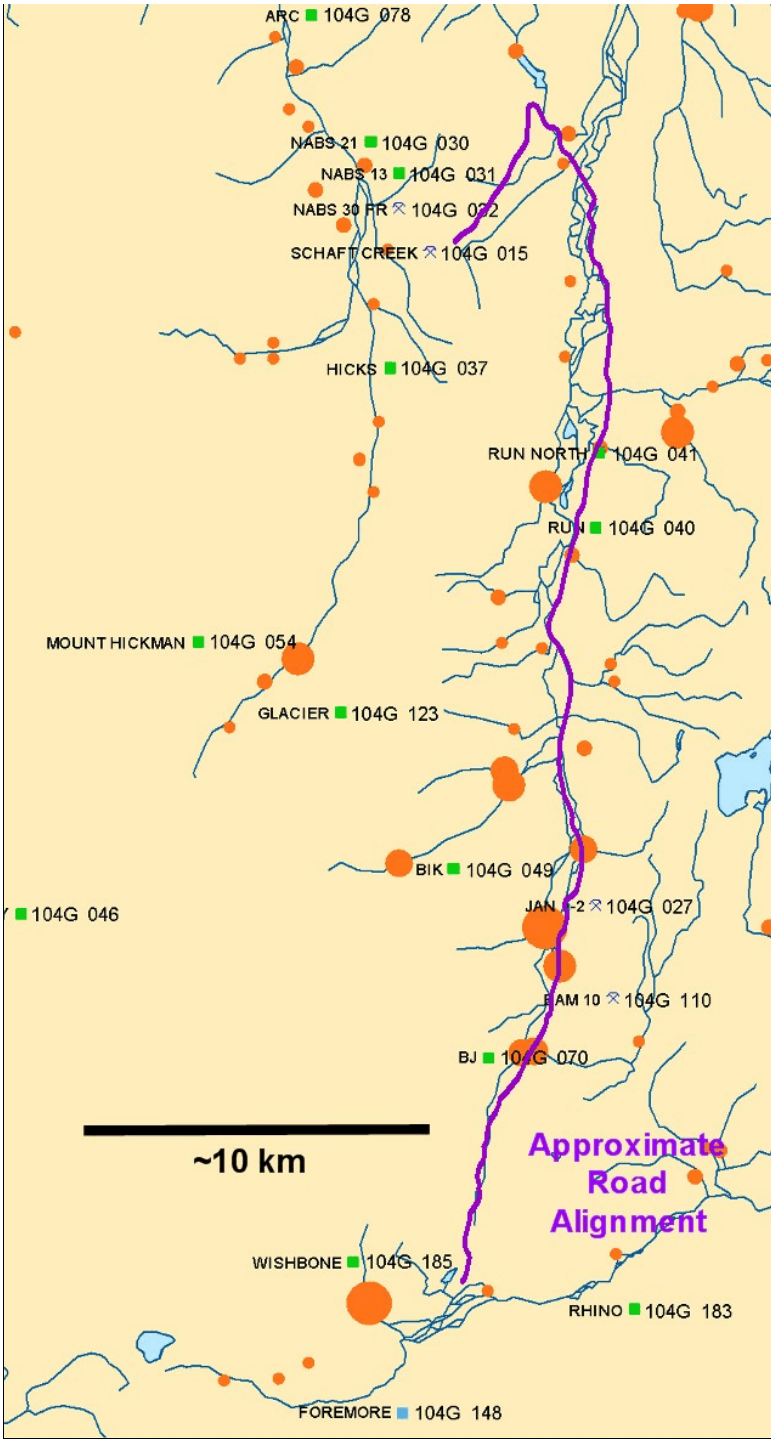


Figure 3-7. **Solid-Phase Antimony from Provincial Regional Geochemical Surveys around the Proposed Road Alignment (taken from the British Columbia MapPlace website).**

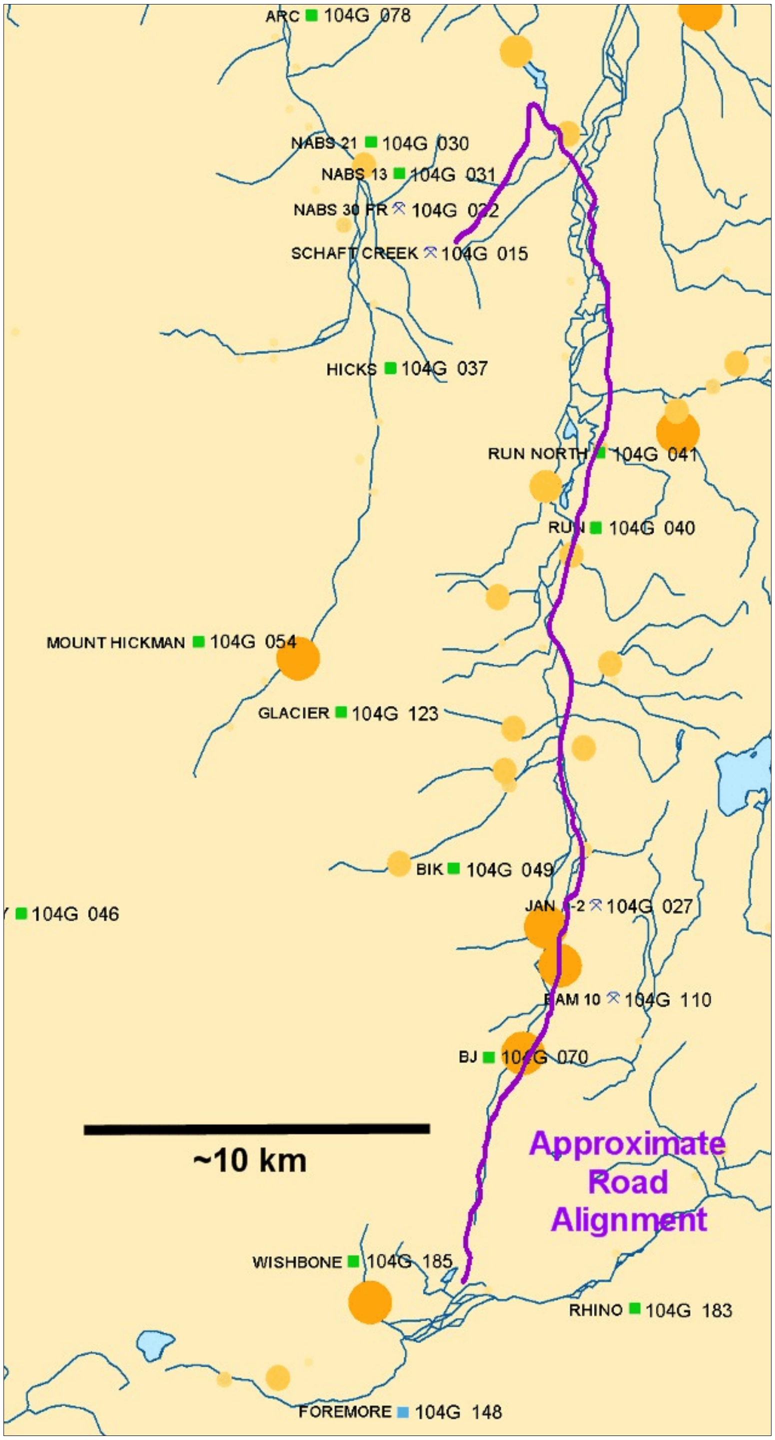


Figure 3-8. Solid-Phase Arsenic from Provincial Regional Geochemical Surveys around the Proposed Road Alignment (taken from the British Columbia MapPlace website).

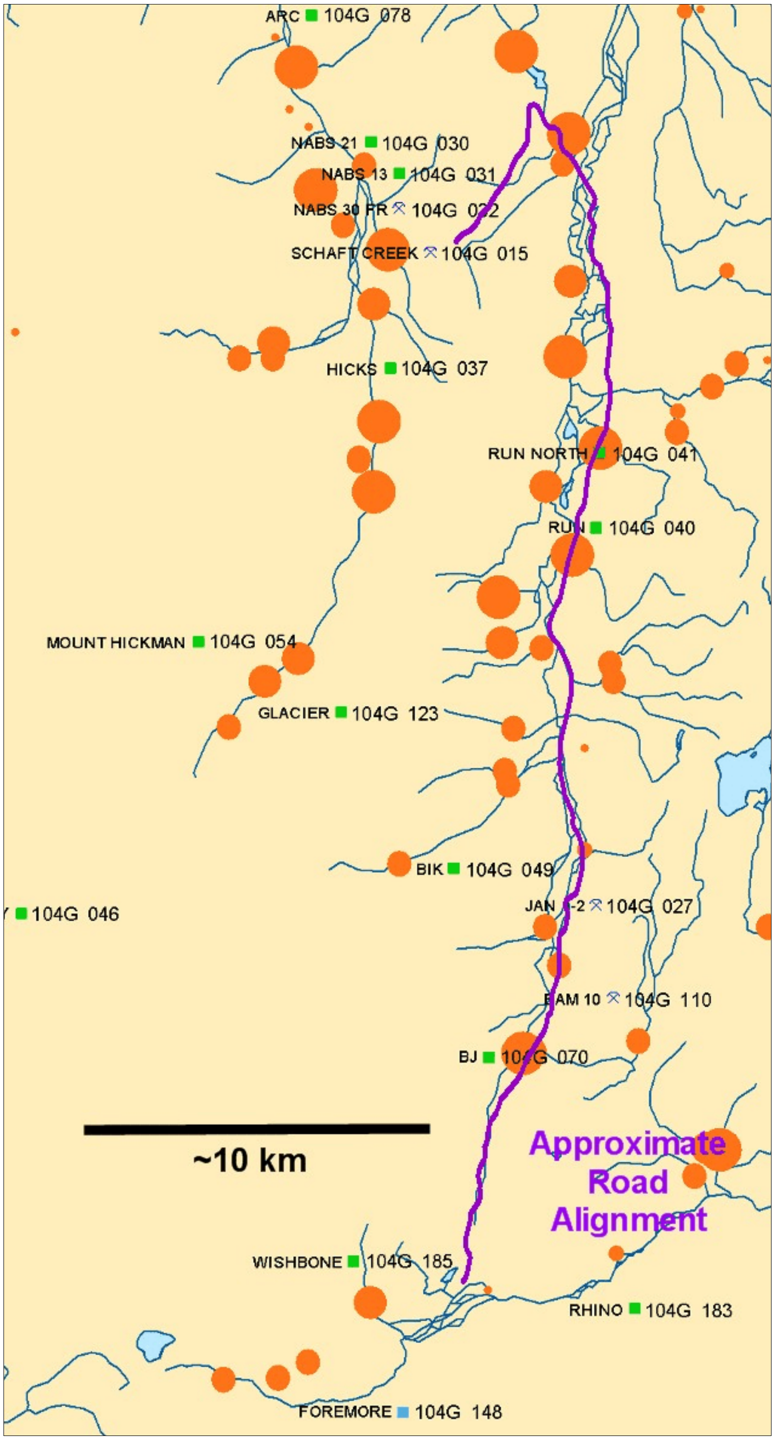


Figure 3-9. Solid-Phase Copper from Provincial Regional Geochemical Surveys around the Proposed Road Alignment (taken from the British Columbia MapPlace website).

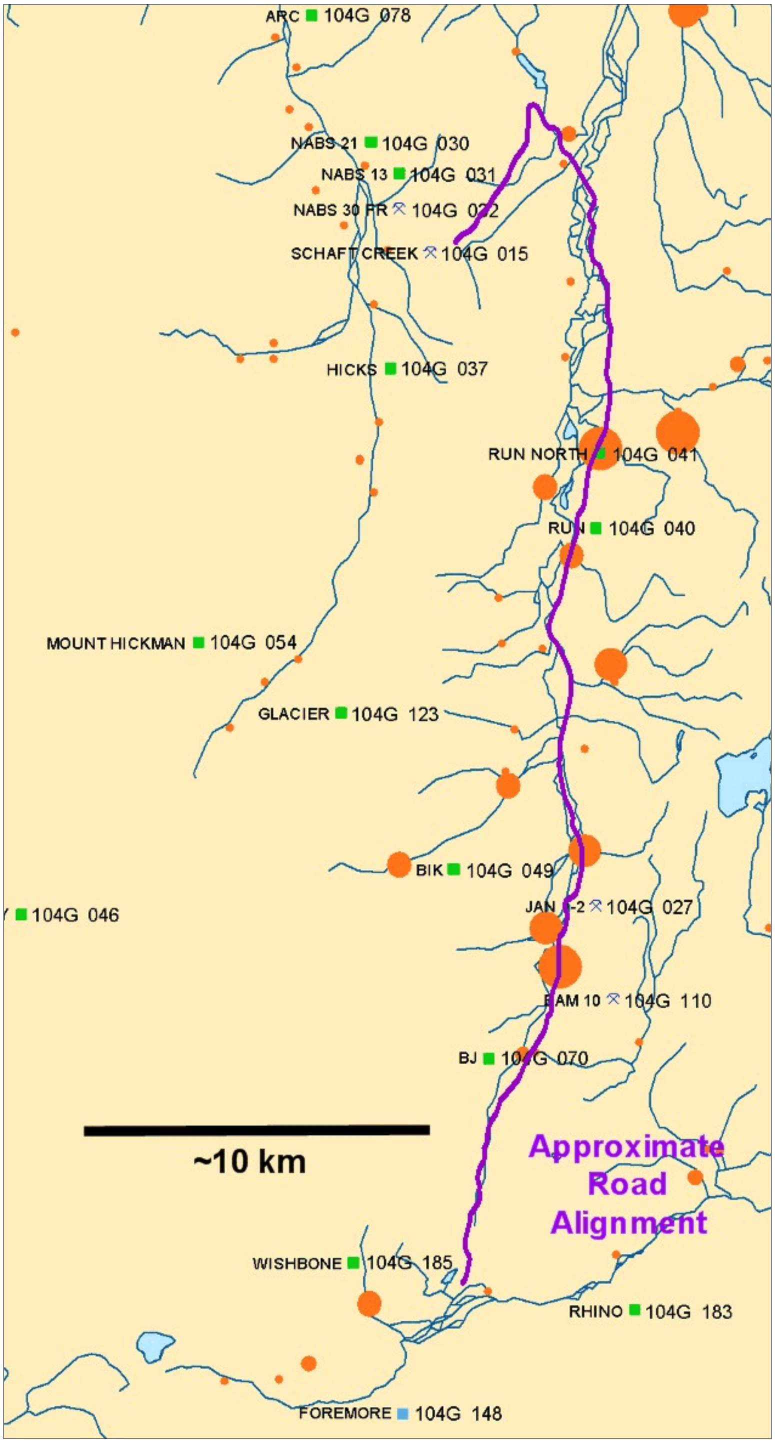


Figure 3-10. **Solid-Phase Mercury from Provincial Regional Geochemical Surveys around the Proposed Road Alignment (taken from the British Columbia MapPlace website).**

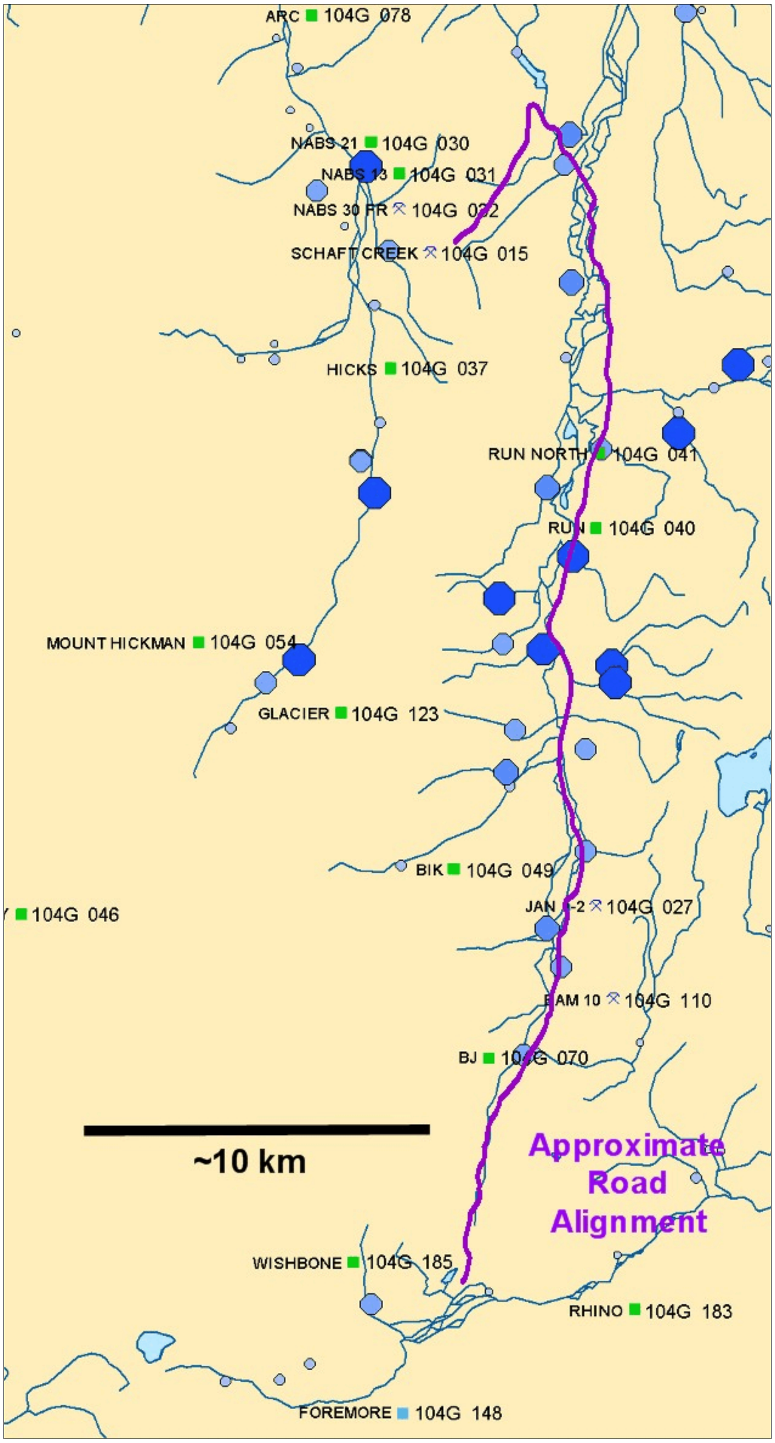


Figure 3-11. Solid-Phase Nickel from Provincial Regional Geochemical Surveys around the Proposed Road Alignment (taken from the British Columbia MapPlace website).

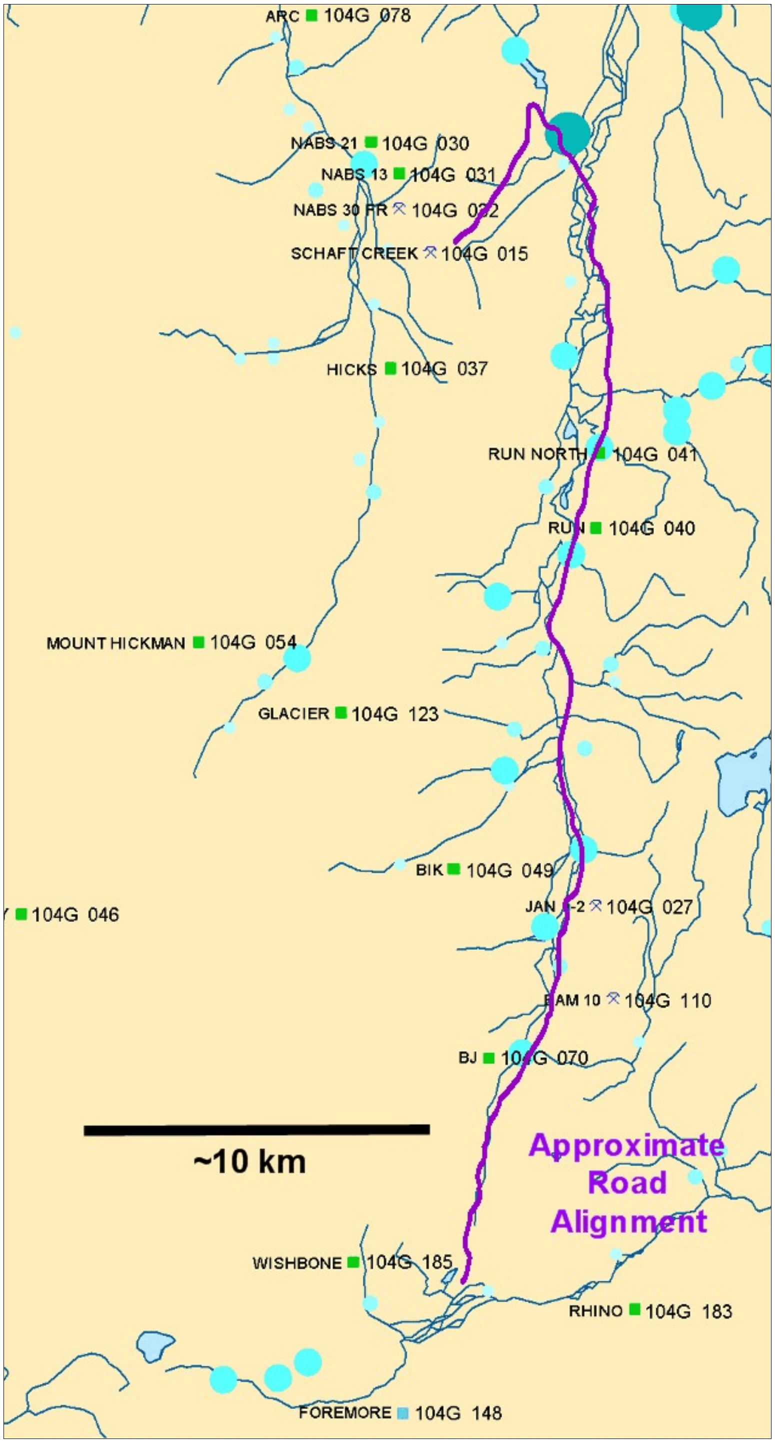


Figure 3-12. Solid-Phase Zinc from Provincial Regional Geochemical Surveys around the Proposed Road Alignment (taken from the British Columbia MapPlace website).

3.6 Air Photographs

The final indirect source of ML-ARD potential comes from air photographs. The air photographs showed that most of the proposed road alignment was covered by trees and other vegetation. Nevertheless, the air photographs also provided targets for "direct" ML-ARD examination (Chapter 4). In particular, surficial rusty-coloured iron staining can sometimes signal accelerated metal leaching and/or sulphide oxidation. Such staining was seen in the air photos around:

~km 0.0: possible iron staining in nearby wetlands

~km 10.5: orange-brown iron staining on west side of Mess Creek valley; possible minor staining on east side (between the Jan 1-2 and Bam 10 developed mineral prospects, Section 3.4)

~km 12.5: possible minor staining on east side of valley (near Jan 1-2 and the Bik mineral showing)

~km 13.0: possible minor staining in center of valley (near Jan 1-2 and the Bik mineral showing)

~km 14.8: possible minor staining on east and west sides

~km 18.5: possible minor staining on west side of valley and center

~km 19.5: possible minor staining on east, center, and west sides of valley

~km 22.0: iron-stained rock at top of mountain to the east (near the Run and Run North mineral showings)

~km 23.0: some iron staining in creek channel, and minor sporadic iron staining on the west slope (near the Run and Run North mineral showings)

~km 28-32: iron stained ponds in valley where the proposed road crosses Mess Creek (the site visit discussed in Chapter 4 identified some rock outcrops near the center of the valley in this area)

The apparent iron staining at ~km 0 in wetlands may be naturally organic in nature. However, the apparent iron staining at ~km 10.5 to 14.8 and at ~km 22.0 to 23.0 would be consistent with the elevated ML-ARD potential obtained from indirect information earlier in this chapter. Iron staining at ~km 18.5-19.5 would be consistent with the second-highest mineral potential in this section. Finally, apparent iron staining at ~km 28-32, in a zone of lowest mineral potential, is anomalous. These areas were inaccessible for direct monitoring (Chapter 4), but could be signs of ML-ARD.

3.7 Summary of Indirect ML-ARD Information for the Proposed Access Road

The proposed access road for the Schaft Creek Project covers a length of approximately 39.5 km, plus potential rock quarries and sand-gravel pits. Existing, external “indirect” sources of ML-ARD information have been used here. This started at the Ministry of Energy, Mines and Petroleum Resources’ Minfile and MapPlace website, which provided details of watersheds, surficial geology, bedrock geology, Regional Geochemical Studies (RGS), and nearby mineral deposits and showings. Another source of indirect ML-ARD for this study was air photographs of the road alignment and nearby areas.

The proposed access road passes through two primary watersheds. Most of the road alignment is in the Mess Creek watershed, which drains to the north. A small section, approximately 1.5 km long at the southern end, lies in the More Creek watershed that drains east and south to the Iskut River.

Maps and air photos showed that much of the proposed road alignment lies on the unconsolidated alluvium in the Mess Creek valley. Most of the alignment was covered by trees and other vegetation, and was thus not readily visible. If unconsolidated sediments were composed of locally weathered bedrock, their geochemistry may reflect weathered aspects of the bedrock. If the sediments were transported large distances by water and/or glaciers, then their geochemistry may bear little resemblance to the underlying bedrock. Thus, unconsolidated alluvium was not automatically assumed to have a similar ML-ARD potential as the underlying or nearby bedrock. However, if local rock had a high potential and the potential of local sediment could not be determined, then the sediments were assumed in this report to have the same potential as rock.

Bedrock geology, mostly hidden below the unconsolidated sediments in the Mess Creek valley, is complex. Zones of volcanic, intrusive, sedimentary, and metamorphic rock are mixed, sometimes on a relatively small scale. If ML-ARD potential is related to rock types, then the potential can be highly variable over short distances along the proposed road.

The potential for metals and other minerals can sometimes serve as a proxy for ML-ARD potential. Metallic-mineral potential along the proposed access-road alignment, from the provincial MapPlace website, showed that areas near the road ranged from the lowest mineral potential to the highest. The highest-potential zone coincided with a band of sedimentary rock from ~km 10 to ~km 15. Also, two zones of second-highest potential were at ~km 15-26 and ~km 36-39.5.

Another general indicator of ML-ARD potential can be mineral claims, prospects, and showings. The provincial Minfile site showed two developed mineral prospects and four mineral showings near the proposed road or in tributaries of Mess Creek. All six contained potentially acid-generating sulphide-borne metals like iron, copper, cadmium, arsenic, and/or molybdenum. All six also contained some carbonate minerals, but it was not clear if the carbonate was sufficient to prevent ARD. RGS water pH values (see below) showed that, just to the north and east of one mineral showing, values as low as 4.5 were measured. Even without ARD, near-neutral metal leaching would remain a concern in these areas. Therefore, along the nearby proposed road alignment, ~km 4-17 and ~km 21-26 were given high, indirect ML-ARD potentials.

The Regional Geochemical Survey (RGS) data from the provincial government provided aqueous pH measurements and solid-phase analyses of sediment near the proposed road alignment. Based on aqueous measurements, most pH values upstream of and near the road alignment were around 6.9 to 8.1. The lowest value of 4.5 was found in a tributary to the north and east of one mineral showing, suggesting ARD was actively produced in that tributary.

Solid-phase levels of metals and other elements do not necessarily produce accelerated leaching rates into water. In fact, some solid-phase levels might be high due to slow leaching, but laboratory kinetic tests and detailed RGS water analyses were not available to resolve this. In any case, the RGS surveys provided selected solid-phase elements in alluvium sediments near the proposed road alignment and in tributaries to Mess Creek. Based on solid-phase antimony, arsenic, copper, mercury, nickel, and zinc, the portions of the road alignment with relatively elevated levels included the aforementioned ~km 4-17 and ~km 21-26. Some elements like copper were less variable along the length of the alignment. Also, one sample, only with elevated copper and zinc, was found at the north end of the alignment, around km 34.

The final indirect source of ML-ARD potential came from air photographs, which provided targets for “direct” ML-ARD sampling and analyses in Chapter 4. Surficial rusty-coloured iron staining can sometimes signal accelerated metal leaching and/or sulphide oxidation. Such staining appeared to be present in the air photos around km 10.0-14.8 and km 22.0-23.0, which coincided with the aforementioned sections of high, indirect ML-ARD potential. Iron staining was also apparent around km 0.0, which may be from natural organic processes in the local wetlands; km 18.5-19.5 is in a zone of second-highest mineral potential; and km 28-32 anomalously is in a zone of lowest mineral potential. These areas of apparent iron staining could not be reached during the field visit (Chapter 4), but could be signs of ML-ARD.

4. "DIRECT" ML-ARD INFORMATION

The proposed access road for the Schaft Creek Project covers a length of approximately 39.5 km (Chapter 2 and Appendix A), plus potential rock quarries and sand-gravel pits that would be located some lateral distances from the road. As a result, detailed ML-ARD sampling of the entire potential disturbed area would be intensive, and still not provide all information like kinetic testing. Therefore, this ML-ARD assessment of surficial access-road samples is based on (a) existing, external "indirect" sources of ML-ARD information discussed in Chapter 3 and (b) "direct" information based on sampling and observations by the authors discussed in this chapter.

4.1 Visual Observations and Surficial Solid-Phase Samples Along the Road Alignment

In October 2007, the authors of this report flew by helicopter along the proposed road alignment (Appendix A), collecting photographs, notes, aqueous pH and electrical-conductivity measurements, and surficial solid-phase samples (Appendix B). For example, local water had a slightly acidic pH and an elevated electrical conductivity near ~km 11.8, so this probably represented local ML and perhaps neutralized ARD.

As explained in Chapter 3, most of the alignment of the proposed access road lies in areas of trees and other vegetation over unconsolidated sediment and alluvium. This ground cover was confirmed by direct observations and many areas were relatively inaccessible (Appendix B). Thus, most of the alignment was not directly sampled for ML-ARD potential. This was not a problem here, because this was expected as explained above and was offset by indirect information in Chapter 3.

An important indirect observation from Chapter 3 was apparently rusty-coloured iron staining near sections of the proposed road alignment (Section 3.6). This was considered a possible sign of surficial ML-ARD. The staining in a wetland around km 0.0 appeared related to natural wetland processes and not ML-ARD. Farther along the road alignment, several areas of iron staining visually appeared to be related to ML-ARD, but these areas could not be reached safely in October 2007. Therefore, the road sections listed in Section 3.6, except km 0.0, are taken as areas of elevated ML-ARD potential. All listed sections, except km 0.0 and km 28-32, coincided with elevated potential based on other indirect lines of evidence.

Based on indirect information (Chapter 3) and from visual observations from the air (above and Appendix B), the helicopter was landed, where safe and accessible. As a result, 12 small-scale "hand" samples of surficial rock and surficial unconsolidated sediments were collected (Appendices B and C). Eight of the 12 samples were of surficial rock, whereas the remaining four were of unconsolidated cobbles, gravel, sand, and/or finer material. As explained above, the extensive cover of trees and vegetation precluded the collection of surficial geological materials in most locations.

These solid samples were subjected to the ML-ARD analyses listed in Section 4.2, to estimate ML-ARD potentials of larger volumes that might be disturbed by road construction (Chapters 5 and 6). More reliable upscaling of small-scale ML-ARD predictions typically requires additional kinetic testing (Morin and Hutt, 2007c), which was not done as part of this study.

4.2 ML-ARD Analyses of the Rock and Unconsolidated Sediments

All 12 samples from Section 4.1 were sent to ALS Chemex in North Vancouver for:

1) Chemex Package ABA-PKG05A plus C-IR07, which is standard-Sobek (U.S. EPA 600 compliant, Sobek et al., 1978) expanded acid-base accounting (ABA) including:
    - paste pH in a mixture of deionized water and pulverized rock,
    - total sulphur,
    - leachable sulphate (both HCl and carbonate leach techniques),
    - measured sulphide,
    - calculated sulphide by subtracting sulphate from total sulphur,
    - barium-bound sulphate calculated from barium analyses,
    - calculation of acid potentials based on sulphide levels plus any unaccounted-for sulphur(Sulphide Acid Potential, SAP),
    - standard-Sobek neutralization potential (NP) by acid bath and base titration,
    - inorganic carbonate for mathematical conversion to Carbonate NP (Inorg CaNP),
    - total carbon for mathematical conversion to Carbonate-equivalent NP (Total CaNP),
    - CaNP calculated from calcium (Ca CaNP),
    - CaNP calculated from Ca + Mg (Ca+Mg CaNP),
    - various Net Neutralization Potential (NNP) balances of acid neutralizing capacities minus various acid generating capacities, and
    - various Net Potential Ratio (NPR) balances of acid neutralizing capacities divided by various acid generating capacities.
2) total-metal contents by:
    - Chemex Package ME-MS61m: 49-element analysis after strong 4-acid digestion, and
    - Chemex Package ME-XRF-06: XRF (x-ray-fluorescence) whole rock for 14 elements and parameters.

Analyses are compiled in Appendix C of this report and discussed in the following subsections. No kinetic testing for upscaling (Morin and Hutt, 2007c) or prediction of metal leaching (Section 4.3.2) was performed as part of this study.

4.3 Results of ML-ARD Analyses

4.3.1 Acid Base Accounting

As part of the ABA Package (Section 4.2), paste pH showed that none of the 12 samples was generating net acidity at that time (Figure 4-1 and Appendix C). All samples had pH 6.9 to 9.5, compared to pH 6.2 of the deionized water added to them.

Total sulphur ranged from <0.01%S in one rock sample to 0.39%S in another rock sample (<0.01%S is shown as one-half detection, or 0.005%S, in Figure 4-1). Analyses close to the detection limit typically have higher analytical inaccuracy, and this is an important issue for the proposed access road as explained below.

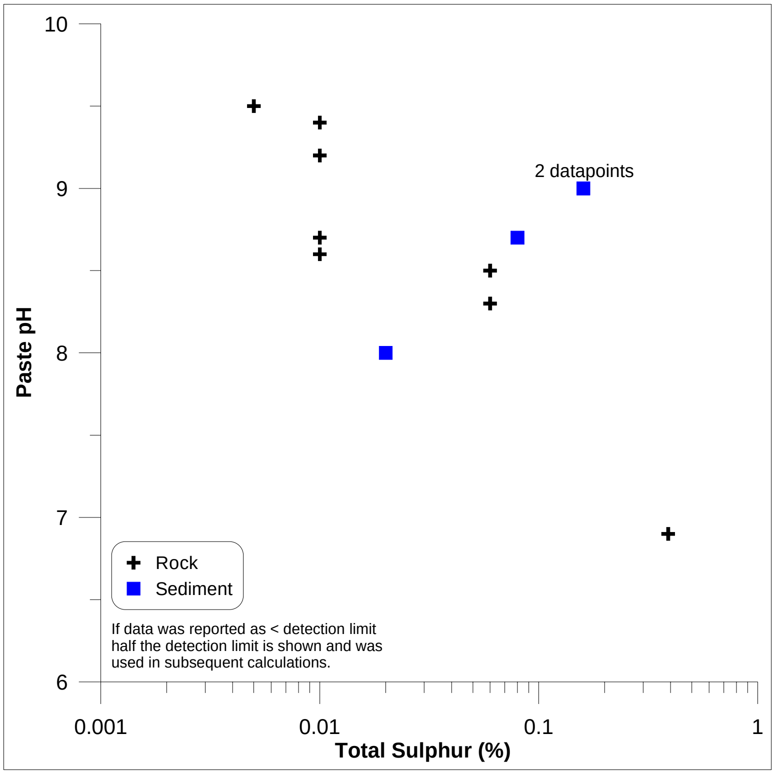


Figure 4-1. Paste pH vs. Total Sulphur in the 12 ML-ARD Proposed-Access-Road Samples.

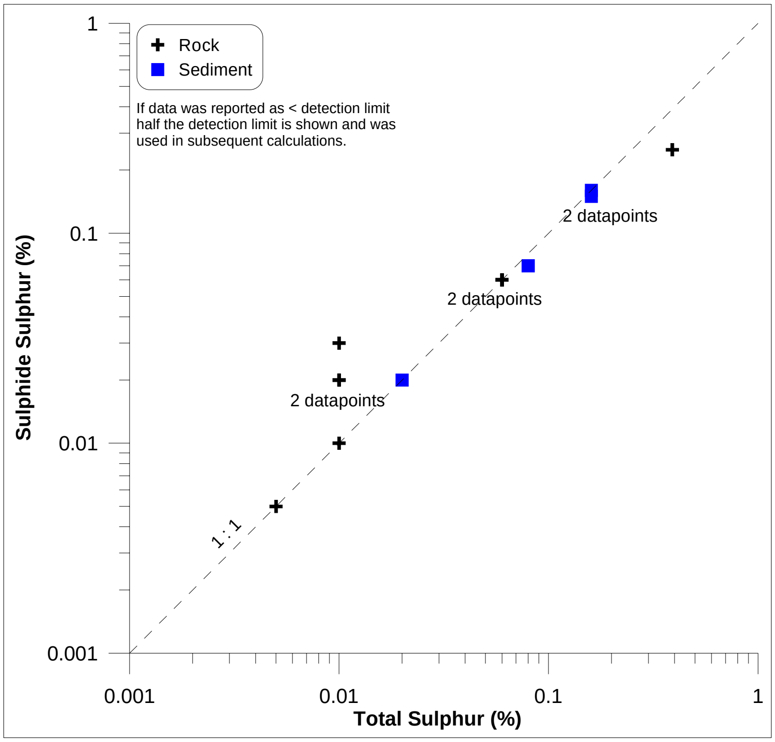


Figure 4-2. Sulphide vs. Total Sulphur in the 12 ML-ARD Proposed-Access-Road Samples.

It is important to understand that detection limits are technological limitations and not environmental criteria. In other words, a value close to, or below, detection does not automatically imply no environmental effects, or in this case no acid generation from sulphide oxidation. In fact, Morin and Hutt (2006) found that sulphur values at least as low as 0.02%S could still generate acidity, and no lower bound could be identified.

A scatterplot of total sulphur and potentially acid-generating sulphide showed that most sulphur was sulphide in most samples (Figure 4-2). Of note, three of the four highest sulphide values were found in the sediment samples, which are typically thought of as weathered and oxidized.

At sulphur levels generally around 0.05%S and below, analytical inaccuracy and numerical round-off can create major discrepancies. For example, in Figure 4-2, two rock samples contained twice as much sulphide (0.02%S) as total sulphur (0.01%S). Also, one rock sample had three times more sulphide (0.03%S) than total sulphur (0.01%S), which is theoretically not possible. Thus, analytical inaccuracy below 0.05%S is an important issue for interpreting the acid-generating potential of the low-sulphur proposed-road samples.

This raises a difficult issue: how to estimate acid potentials of the low-sulphur access-road samples when current analytical technology is not providing accurate information. Again, this technological limitation is not synonymous with environmental protection, since low levels of sulphide can still generate acidity. The safest and prudent way to proceed here is by considering measured total sulphur as 100% acid-generating sulphide, and calculating acid potentials accordingly. In the end, this makes little difference, because Neutralization Potential (NP, below) was the primary determination of ARD status, and using sulphide or total sulphur led to nearly the same predictions.

Sobek Neutralization Potential (NP) ranged from 9 to 387 kg $CaCO_3$ equivalent/tonne (Figure 4-3). Four of the five highest NP values were sediments, so the rock was often relatively depleted in NP.

NP typically reflects to some degree a sample's inorganic carbonate content. This can be seen for the 12 samples of rock and sediment (Figure 4-4, with inorganic carbonate mathematically converted to the same units as NP). However, there was a bias towards higher NP values compared with carbonate, possibly reflecting some non-carbonate neutralization. A better 1:1 correlation with NP was seen for total carbon (Figure 4-5) than inorganic carbonate alone. This suggested simpler total-carbon analyses or adjusted inorganic-carbonate analyses could be substituted for the more intensive NP analysis.

The correlation of NP with calcium was good (Figure 4-6, with calcium mathematically converted to the same units as NP), except for three rock samples. This implies the inorganic carbonate occurs primarily as calcite ($CaCO_3$). The three exceptions then contained additional calcium-bearing non-carbonate minerals.

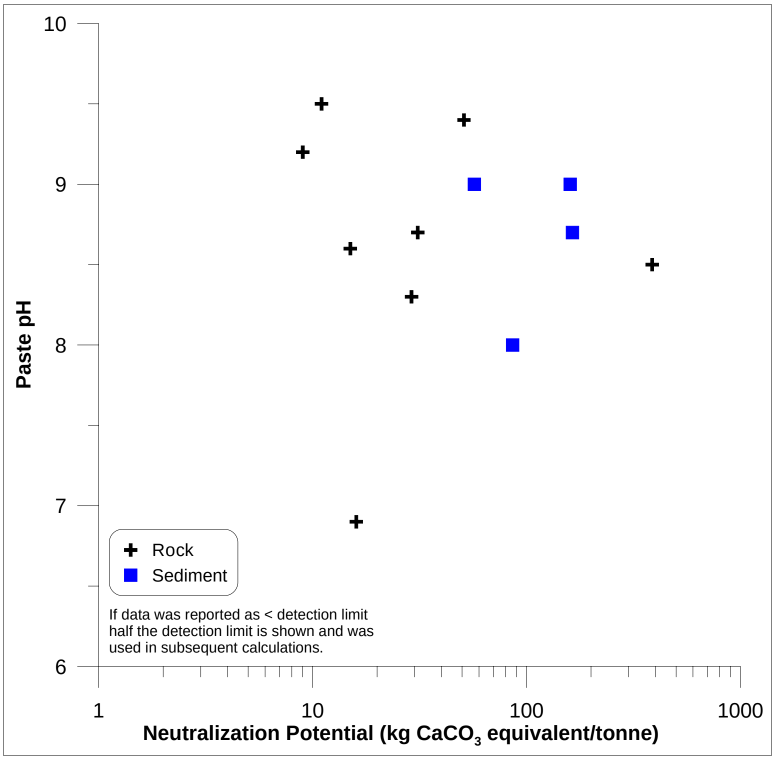


Figure 4-3. Paste pH vs. Sobek (U.S. EPA 600) Neutralization Potential in the 12 ML-ARD Proposed-Access-Road Samples.

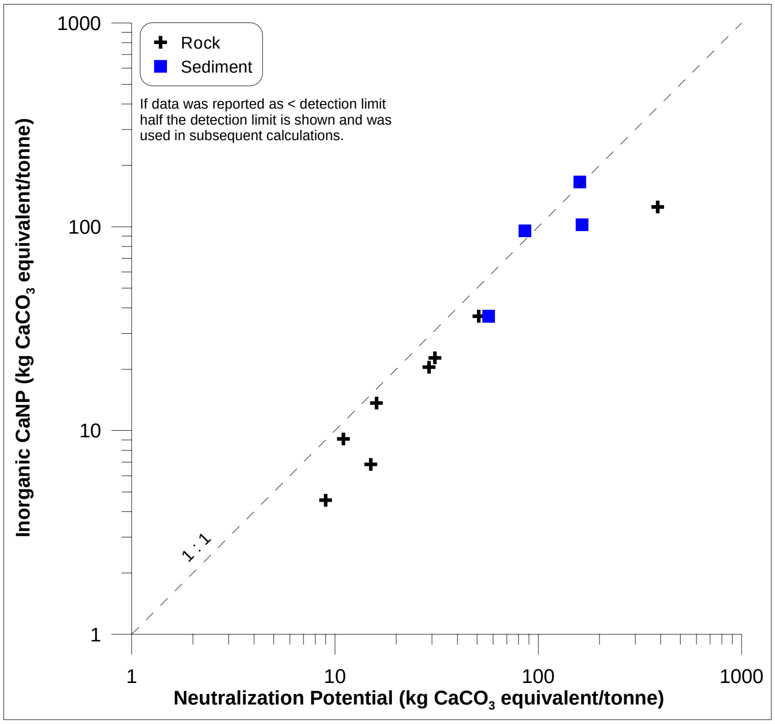


Figure 4-4. Inorganic-Carbonate-Based Neutralization Potential vs. Sobek Neutralization Potential in the 12 ML-ARD Proposed-Access-Road Samples.

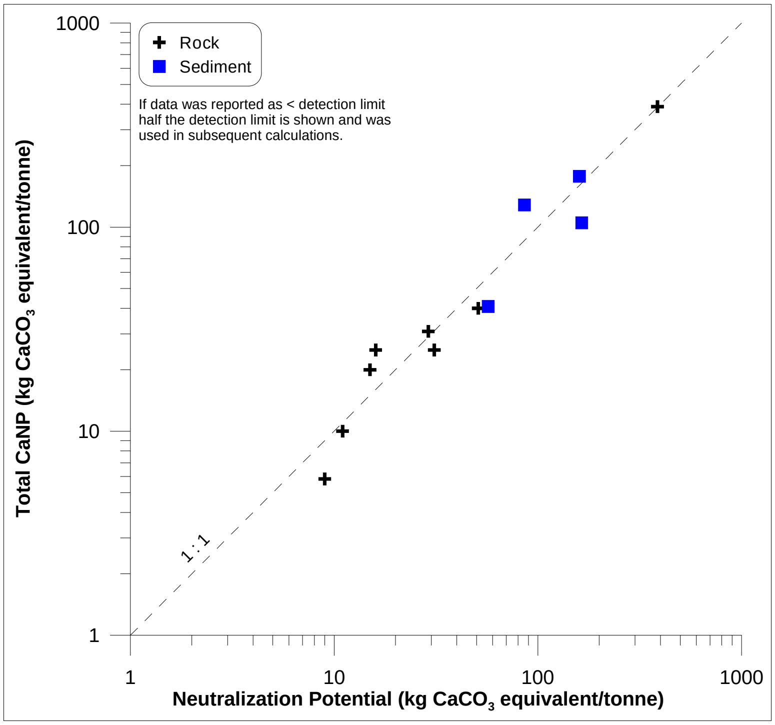


Figure 4-5. Total-Carbon-Based Neutralization Potential vs. Sobek Neutralization Potential in the 12 ML-ARD Proposed-Access-Road Samples.

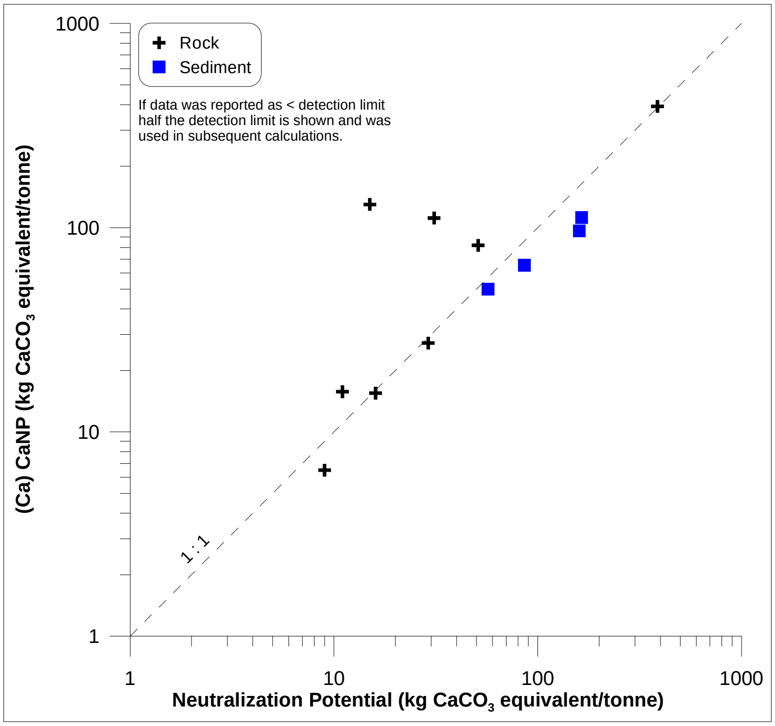


Figure 4-6. Calcium-Based Neutralization Potential vs. Sobek Neutralization Potential in the 12 ML-ARD Proposed-Access-Road Samples.

Interestingly, Sample SCR-05 with the highest NP had equivalent amounts of Total-Carbon-Based CaNP and Calcium-Based CaNP, but Inorganic-Carbonate-Based CaNP was about one-third. This suggests the inorganic-carbonate analyses may have been anonymously low, explaining the bias towards higher NP in Figure 4-4.

Typically, some amount of the measured NP is unavailable for neutralization, with paste pH falling to acidic values as NP decreases. Unavailable NP is typically between 5 and 15 kg/t, but values as low as zero and above 60 kg/t have been reported (Morin and Hutt, 1997 and 2001). Acidic paste pH was not detected in these proposed-access-road samples of rock and sediment (Figure 4-3), so Unavailable NP was not apparent. However, a value of 10 kg/t will be used here to illustrate the effect on net balances.

Net balances of acid-generating and acid-neutralizing capacities can be calculated from sulphur species and NP as discussed above. Based on its net balance, a sample could then be predicted to be net acid generating, perhaps after a long near-neutral “lag time”, “uncertain” without additional testing, or net acid neutralizing indefinitely.

Net balances can be calculated using division (Total-Sulphur-Based Net Potential Ratio, TNPR = NP /TAP) or subtraction (Total-Sulphur-Based Net Neutralization Potential, TNNP = NP - TAP). TNPR is used in this report, and is the preferred approach in British Columbia. Sulphide-based SNPR will also be discussed, to show that total sulphur provided the same predictions as sulphide.

“Adjusted” TNPR values were obtained by first subtracting the currently undefined unavailable NP, such as 10 kg/t, from measured NP:

$$\text{Adj TNPR} = [\text{NP} - 10] / [\%\text{S(total)} * 31.25]$$

Non-site-specific ABA screening criteria are: TNPR ≤ 1 is net acid generating, perhaps after some lag time, $1<\text{TNPR}<2$ is uncertain until further testing, and TNPR≥ 2 is net acid neutralizing. While site-specific criteria can be developed with additional testwork, like humidity cells, this years-long testing has not been conducted for the proposed access road. Furthermore, site-specific criteria might be too difficult considering the number and types of rock units near the alignment (Section 3.3).

Based on TNPR with no adjustment for Unavailable NP, only one (SCR-08A, rock) of the 12 access-road samples had a value below 2.0 (Figure 4-7 and Appendix C). Its TNPR value was 1.31, and it also had the highest level of total sulphur and sulphide (0.39%S and 0.25%S) and lowest paste pH (6.9). A value of 1.31 is considered “uncertain” without further testing. However, if sulphide were used in the calculation (SNPR), rather than total sulphur (TNPR), the SNPR value of 2.01 just extends into the net-neutralizing category. At this point, it is prudent to consider the ARD potential of SCR-08A as uncertain.

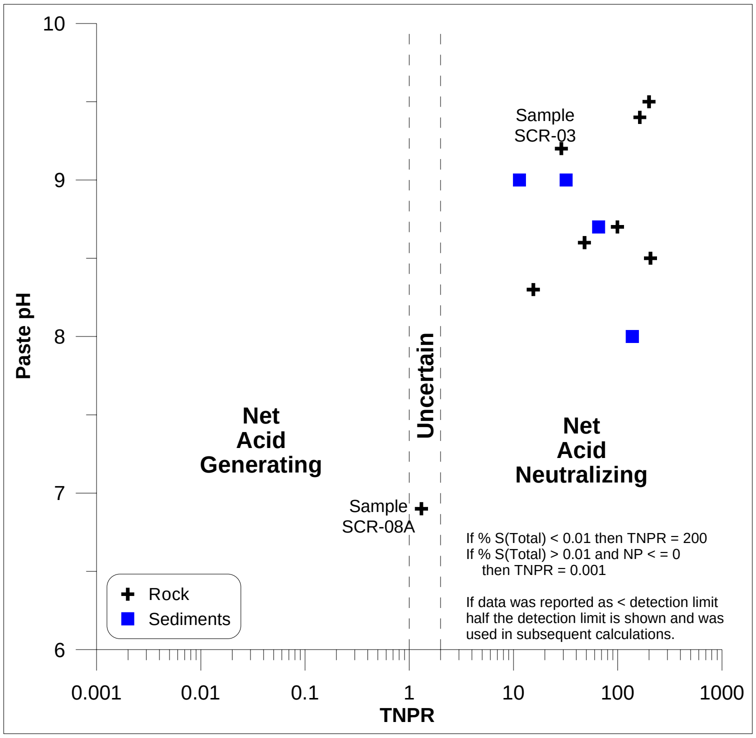


Figure 4-7. Paste pH vs. (Unadjusted) Total-Sulphur-Based Net Potential Ratio (TNPR) in the 12 ML-ARD Proposed-Access-Road Samples.

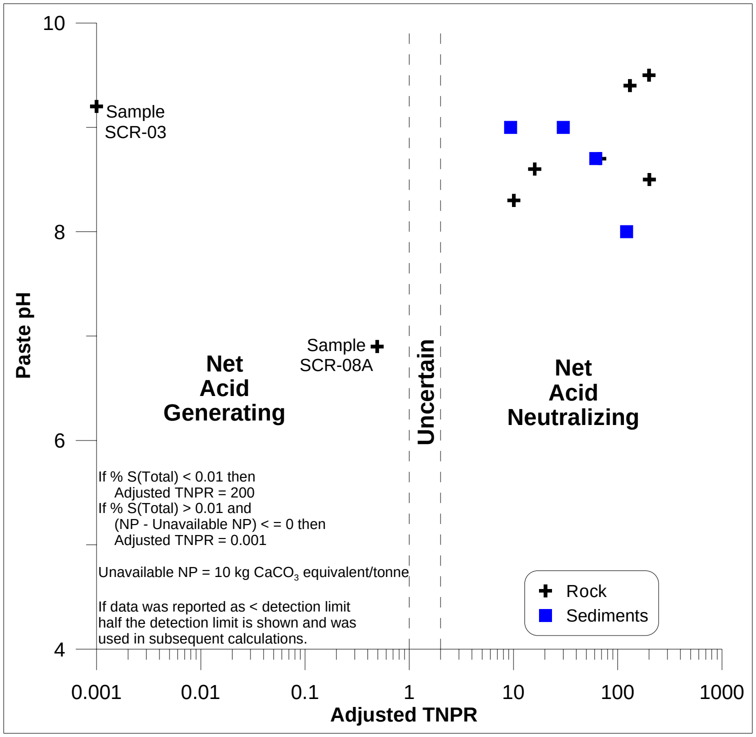


Figure 4-8. Paste pH vs. Adjusted Total-Sulphur-Based Net Potential Ratio (Adj TNPR) in the 12 ML-ARD Proposed-Access-Road Samples.

Based on TNPR with adjustments for Unavailable NP, two primary effects arise. First, preceding Sample SCR-08A, which was "uncertain" based on no unavailable NP, became net acid generating, (a) based on Adjusted TNPR < 1 with unavailable NP at 4 kg/t and higher, and (b) based on Adjusted SNPR < 1 with unavailable NP at 9 kg/t and higher (Figure 4-8). Again, at this point, it is prudent to consider the ARD potential of SCR-08A as uncertain, recognizing it could be net neutralizing or net acid generating.

Second, Sample SCR-03 (rock) with a high Unadjusted TNPR of 28.8 (Figure 4-7) became net acid generating, with a default Adjusted TNPR of 0.001 (Figure 4-8), at any level of unavailable NP at and above 9 kg/t. This is simply because its original, measured NP was 9 kg/t, so the simple declaration of all 9 kg/t as unavailable changed it to net acid generating. Even if unavailable NP were 8 kg/t instead of 9 kg/t, SCR-03 would still be predicted to be net neutralizing based on Adjusted TNPR. Interestingly, sulphide (0.02%S) in this sample was twice as high as total sulphur (0.01%S), which is not possible but reflected analytical inaccuracy as discussed above. Nevertheless, its Unadjusted SNPR was still high at 14.4, but its Adjusted SNPR became net acid generating at unavailable NP levels of 7 kg/t and higher. Therefore, due to major variations in its net balances depending on factors like unavailable NP, the ARD potential of SCR-03 as uncertain, recognizing it could be net neutralizing or net acid generating.

In summary, acid-base accounting (ABA) of the 12 samples of rock and sediments collected near the proposed access-road alignment showed that all had near-neutral paste pH at the time of analysis. Total sulphur ranged from <0.01%S in one rock sample to 0.39%S in another rock sample. Most of that total sulphur was potentially acid-generating sulphide, so the more easily measured total sulphur can be used for convenience. However, sulphur values below 0.05%S were relatively inaccurate. Three of the four highest sulphide values were found in the sediment samples, which are typically thought of as weathered and oxidized. Sobek (U.S. EPA 600) Neutralization Potential (NP) ranged from 9 to 387 kg $CaCO_3$ equivalent/tonne, with four of the five highest NP values in sediments. In many samples, the Sobek NP was apparently mostly comprised of calcite ($CaCO_3$), which could be measured by the simpler analytical techniques for total carbon or inorganic carbonate. Net balances of acid-generating and acid-neutralizing capacities were based on the Total-Sulphur-Based Net Potential Ratio (TNPR), with and without adjustments for unavailable NP. This showed eleven samples were net neutralizing indefinitely, plus one sample of rock that was "uncertain" without additional testing. When various amounts of unavailable NP were considered, a second sample of rock showed large changes in TNPR, suggesting the ARD status of this sample was also uncertain without additional testing.

4.3.2 Total Elements

Total-element contents of the 12 access-road samples of rock and sediments (Section 4.1) were measured by ICP-MS analysis after strong four-acid digestion, and by x-ray-fluorescence (XRF) whole-rock analysis (Section 4.2). The results are compiled in Appendix C.

XRF whole-rock data showed that most of the 12 access-road samples consisted predominantly of silica and alumina, with substantial and sometimes dominant amounts of iron, calcium, magnesium, sodium, potassium, and Loss on Ignition (LOI). LOI often reflects the weight loss from the samples of some or all sulphur, carbon, and tightly bound or crystalline water. Sample SCR-05 was apparently about 40% calcite ($CaCO_3$) and thus was mostly calcium and LOI.

ICP elemental analyses were compared to three times the maximum average crustal abundances from Price (1998), to highlight elements relatively enriched in the access-road samples (see element analyses surrounded by boxes in Appendix C). The 12 samples often contained elevated levels of bismuth and selenium, with fewer to rare elevated levels of silver (two samples of rock), cadmium (one sample of rock also with the highest silver), phosphorus (one sample of rock), lead (one sample of rock also with the highest silver and cadmium), antimony (two rock and one sediment sample), and zinc (one rock sample also with the highest silver, cadmium, lead, and antimony).

A comparison with XRF whole-rock chromium showed ICP-MS levels of chromium averaged 38% lower due to incomplete digestion, so total chromium levels were higher than the boxed levels in Appendix C. As a result, one sample of sediment (SCR-08B) contained elevated chromium.

Elevated solid-phase levels of elements do not necessarily mean they will leach at faster rates into water, because they may be elevated due to a low leaching rate. Only additional long-term kinetic tests or detailed on-site monitoring (Chapter 6) can better characterize leaching.

Solid-phase correlations of elements can sometimes reveal mineralogical associations. For example, elements correlating with sulphide (Section 4.3.1) may occur predominantly within the sulphide minerals. Correlations with Sobek Neutralization Potential may indicate those elements are concentrated in carbonate minerals, which can dissolve even without sulphide oxidation. The elements showing at least some minor correlation with sulphide included arsenic, copper, mercury, and nickel (e.g., Figure 4-9). The elements showing at least some minor correlation with NP included calcium (Figure 4-6) and manganese (Figure 4-10).

In summary, total-element contents of the 12 access-road samples of rock and sediments were measured by ICP-MS analysis after strong four-acid digestion, and by x-ray-fluorescence (XRF) whole-rock analysis. This showed that most of the 12 access-road samples consisted predominantly of silica and alumina, with substantial and sometimes dominant amounts of iron, calcium, magnesium, sodium, potassium, and Loss on Ignition (LOI). LOI often reflects the weight loss from the samples of some or all sulphur, carbon, and tightly bound or crystalline water. Also, the 12 samples often contained elevated levels of bismuth and selenium, with fewer to rare elevated levels of silver (two samples of rock), cadmium (one sample of rock), chromium (one sample of sediment), phosphorus (one sample of rock), lead (one sample of rock), antimony (two rock and one sediment sample), and zinc (one rock sample also with the highest silver, cadmium, lead, and antimony). Solid-phase correlations of elements can sometimes reveal mineralogical associations. For example, elements correlating with sulphide may occur predominantly within the sulphide minerals. The elements showing at least some minor correlation with sulphide included arsenic, copper, mercury, and nickel. The elements showing at least some minor correlation with Neutralization Potential, which can dissolve and release metals even without sulphide oxidation, included calcium and manganese.

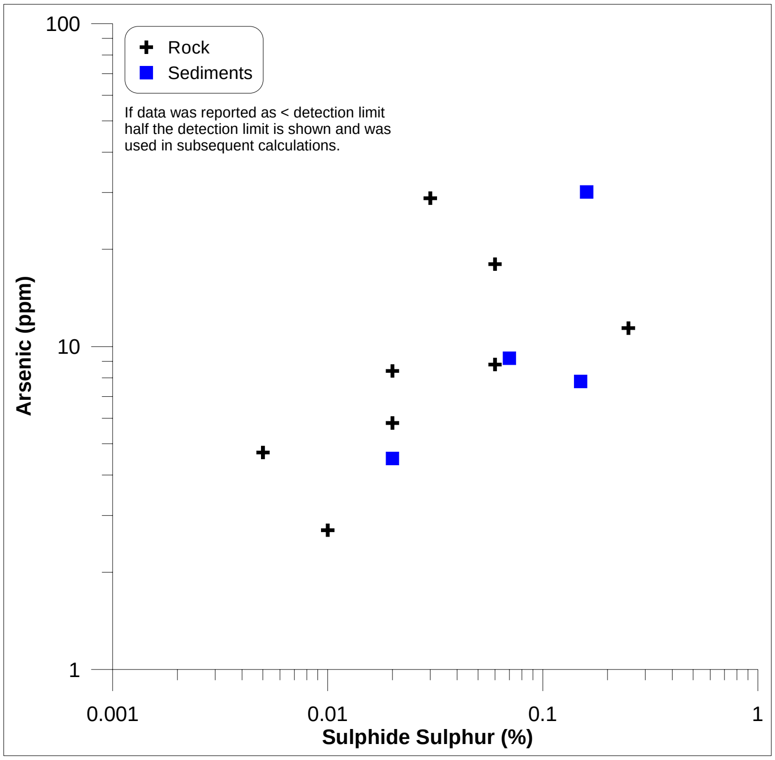


Figure 4-9. Solid-Phase Arsenic vs. Sulphide in the 12 ML-ARD Proposed-Access-Road Samples.

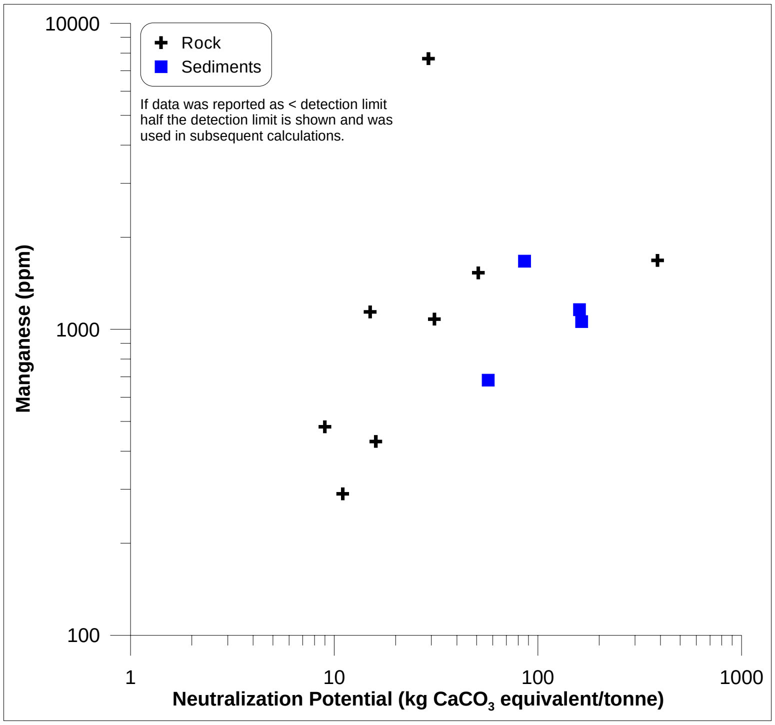


Figure 4-10. Solid-Phase Manganese vs. Sobek Neutralization Potential in the 12 ML-ARD Proposed-Access-Road Samples.

4.4 Spatial Trends in Acid Base Accounting and Total-Element Data

The preceding information on acid base accounting (Section 4.3.1) and total elements (Section 4.3.2) can be combined with "indirect" RGS data (Section 3.5) and Rescan (2007) data along the proposed road alignment (Figure 4-11 and Appendix D). This allows a spatial interpretation of the data, to highlight sections of the proposed roads with higher ML-ARD potential. It is important to note that these different sources of data (1) did not include all elements analyzed for Section 4.3.2, (2) did not use the same, aggressive four-acid digestion for the samples in this study, (3) had analytical methods with differing detection limits, and (4) did not include acid base accounting (Section 4.3.1).

RGS samples were partially digested by the weaker two-acid aqua regia. Rescan (2007) samples were digested with a weaker, non-aqua-regia two-acid digestion. Therefore, any higher solid-phase levels in the 12 ML-ARD samples of this study may be at least partially attributed to the more thorough digestion of the samples.

As shown in Figure 4-11, most sampling locations were of sediments (left side). Only this ML-ARD study provided rock samples (right side). All total-element maps are compiled in Appendix D, with selected ones discussed in this section.

As discussed in Section 4.3.1, total sulphur varied from <0.01%S (numerically set at 0.005%S) to 0.39%S. As seen in Figure 4-12, the highest and lowest values were in rock, between km 26 and 31. Nevertheless, some sediments carried significant levels of total sulphur, which were well distributed along the road alignment.

The map of net balances of acid-generating and acid-neutralizing (TNPR, Section 4.3.1) showed that the lowest, "uncertain" value of 1.31 was found near km 26 around Nahta Creek (Figure 4-13 and Appendix D). The remaining samples of rock and sediments were net neutralizing. Adjusted TNPR, allowing for an unavailable NP of 10 kg/t, showed that the lowest values were again around km 26 and also near the southern end around km 2 (Figure 4-14). This latter sample had low, relatively inaccurate sulphur analyses, so its ARD status was considered "uncertain".

For some solid-phase elements, only samples from this MDAG study were available, such as selenium (Figure 4-15 and Appendix D). As a result, spatial distributions for these elements, based on these relatively few samples, could not be estimated. Other elements included up to three data sets for sediments (MDAG, Rescan, and RGS), such as nickel (Figure 4-16 and Appendix D). Thus, spatial distributions for these elements in sediments were better defined.

For all analyzed elements, the spatial distributions in rock remain poorly defined, reflecting the eight available samples (Appendix C), which in turn reflects the dominant exposure of alluvium near most of the road alignment (Section 3.3). In areas where both rock and sediment analyses were available, sediments sometimes had notably higher levels of some elements, suggesting sediments were not necessarily genetically related to local rock.

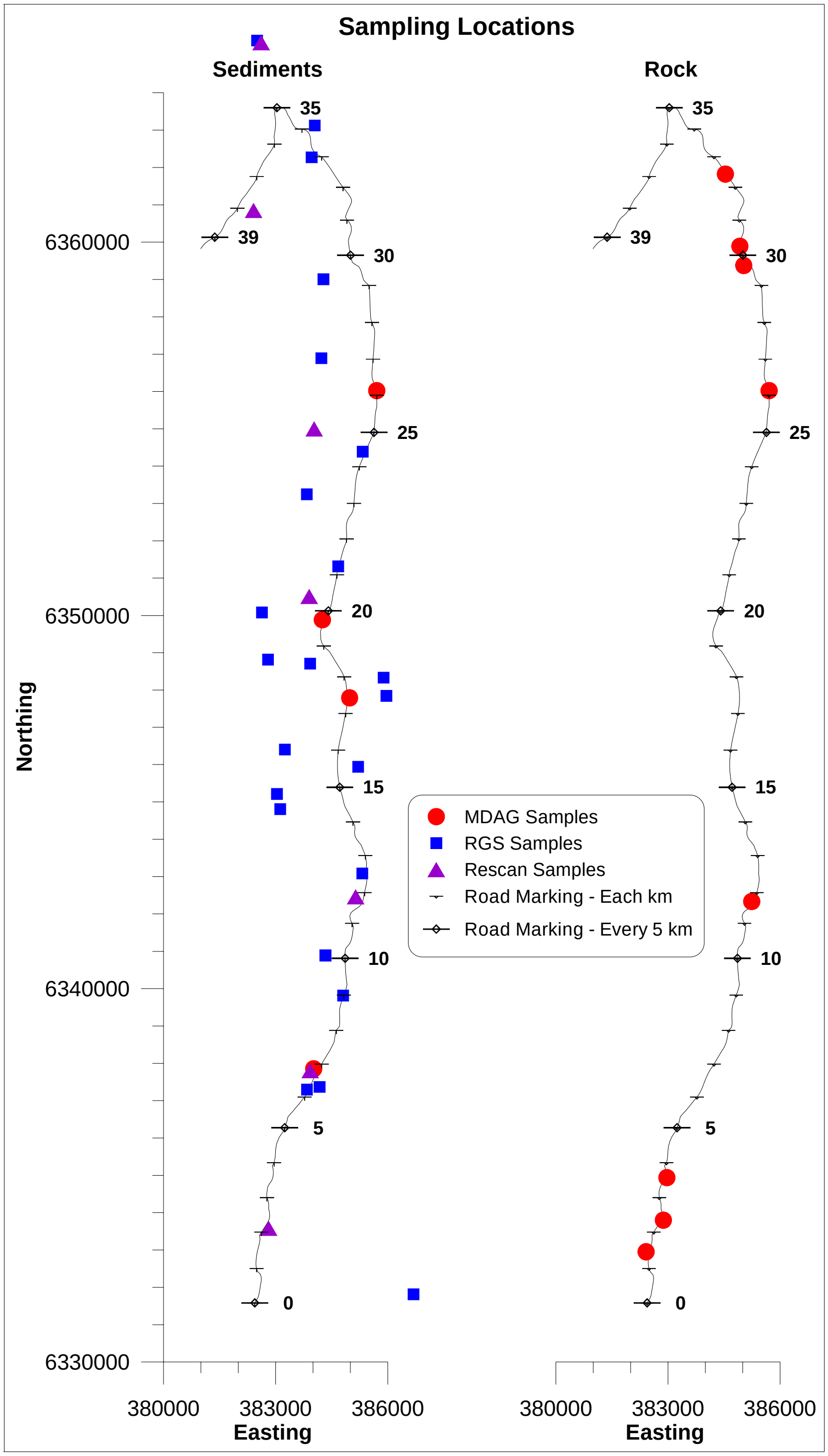


Figure 4-11. Map of Solid-Phase Sampling Locations near the Proposed Road Alignment and in Mess Creek Valley, (from three separate studies).

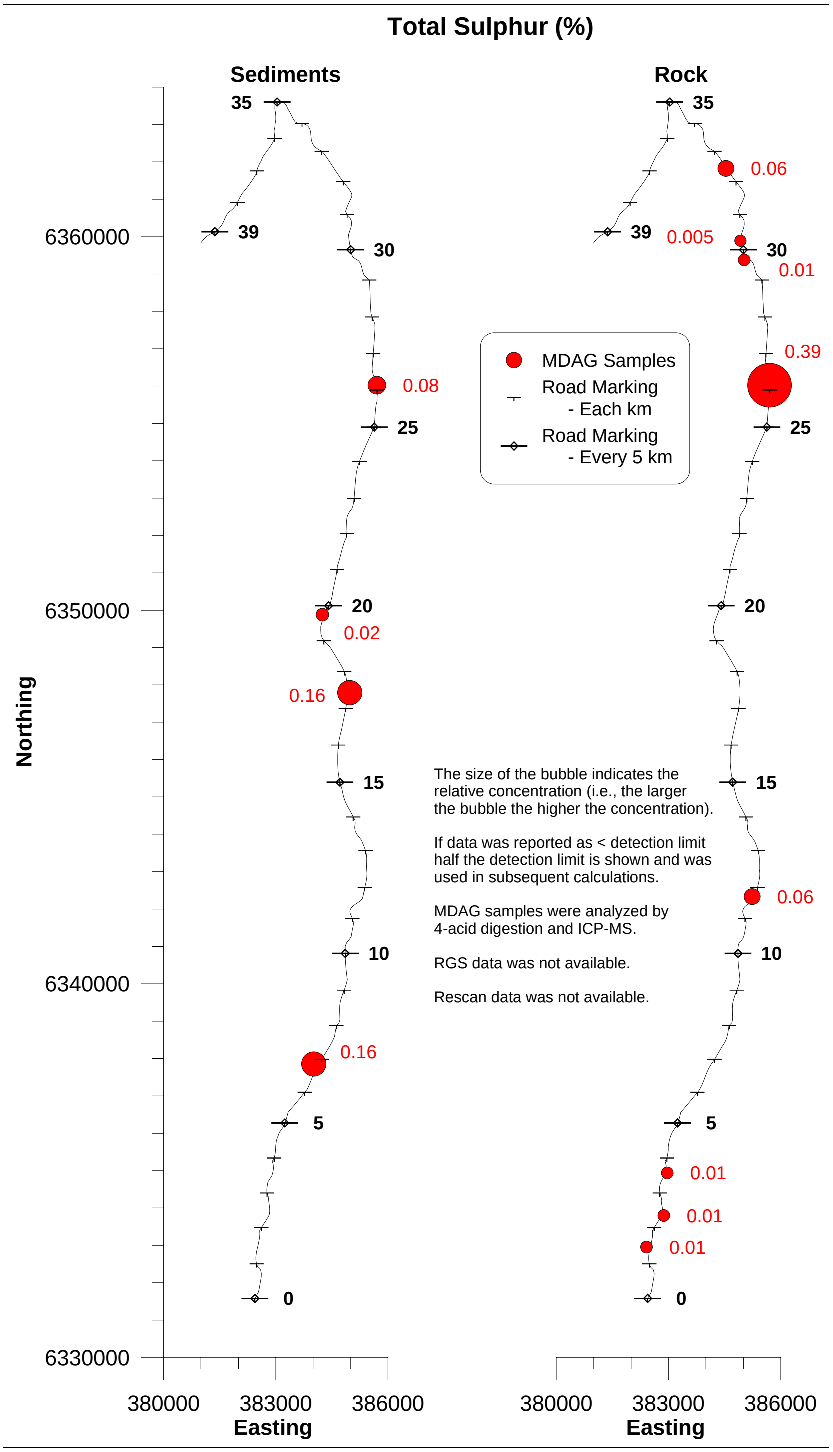
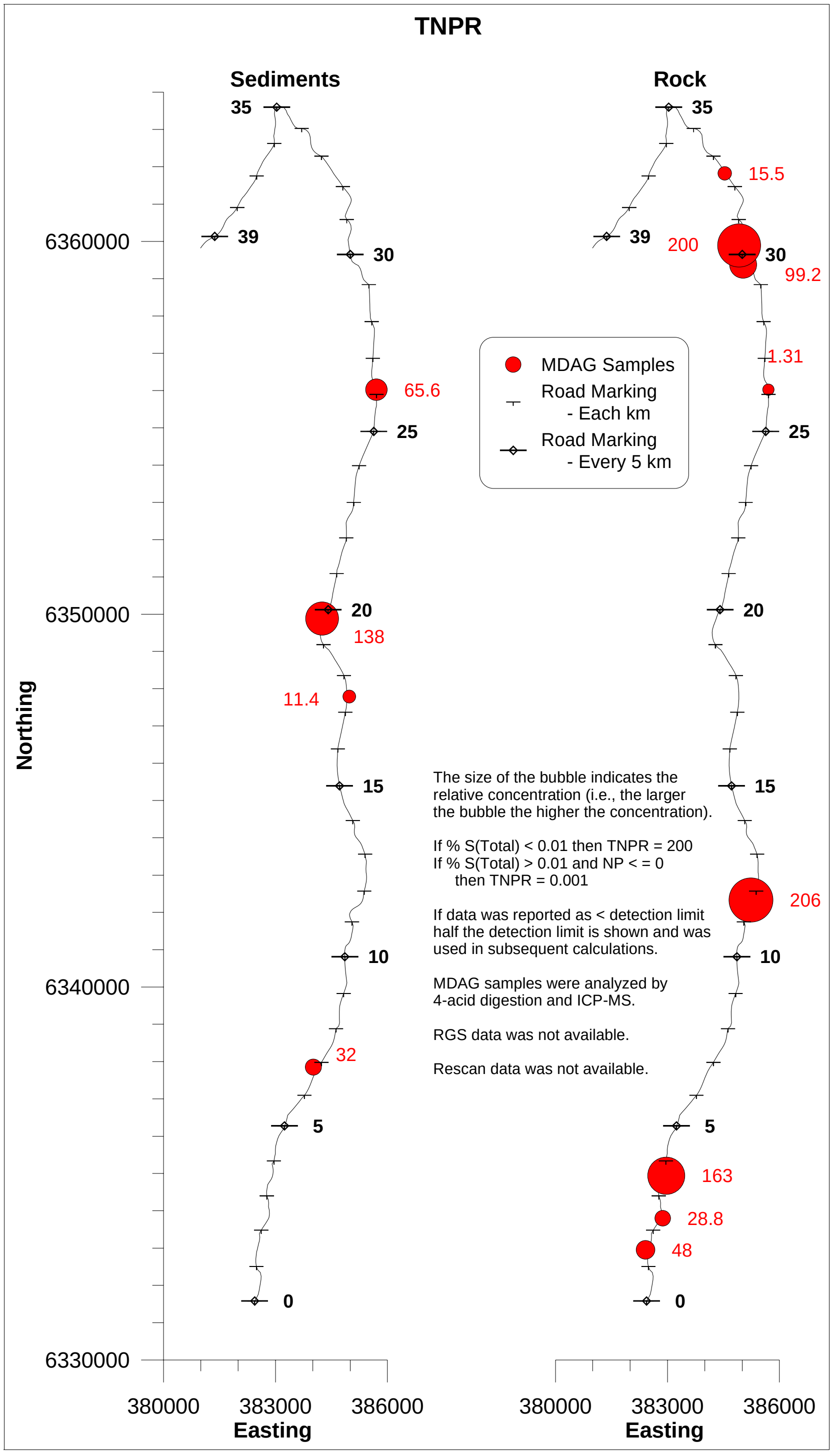


Figure 4-12. Map of Solid-Phase Total Sulphur near the Proposed Road Alignment and in Mess Creek Valley.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If % S(Total) < 0.01 then TNPR = 200
If % S(Total) > 0.01 and NP < = 0
then TNPR = 0.001

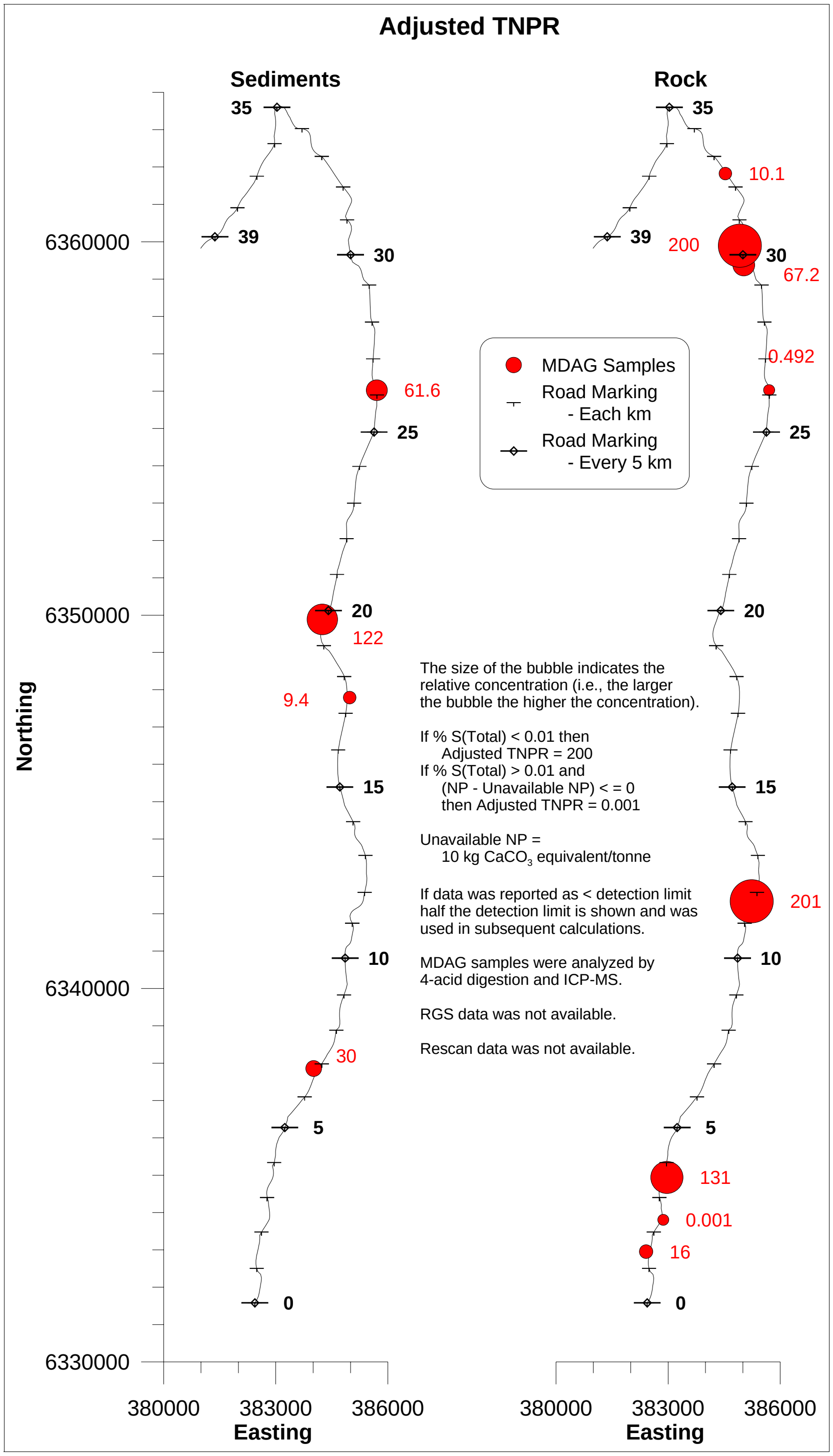
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

Figure 4-13. Map of (Unadjusted) Total-Sulphur-Based Net Potential Ratio (TNPR) near the Proposed Road Alignment and in Mess Creek Valley.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If % S(Total) < 0.01 then
Adjusted TNPR = 200
If % S(Total) > 0.01 and
(NP - Unavailable NP) < = 0
then Adjusted TNPR = 0.001

Unavailable NP =
10 kg $CaCO_3$ equivalent/tonne

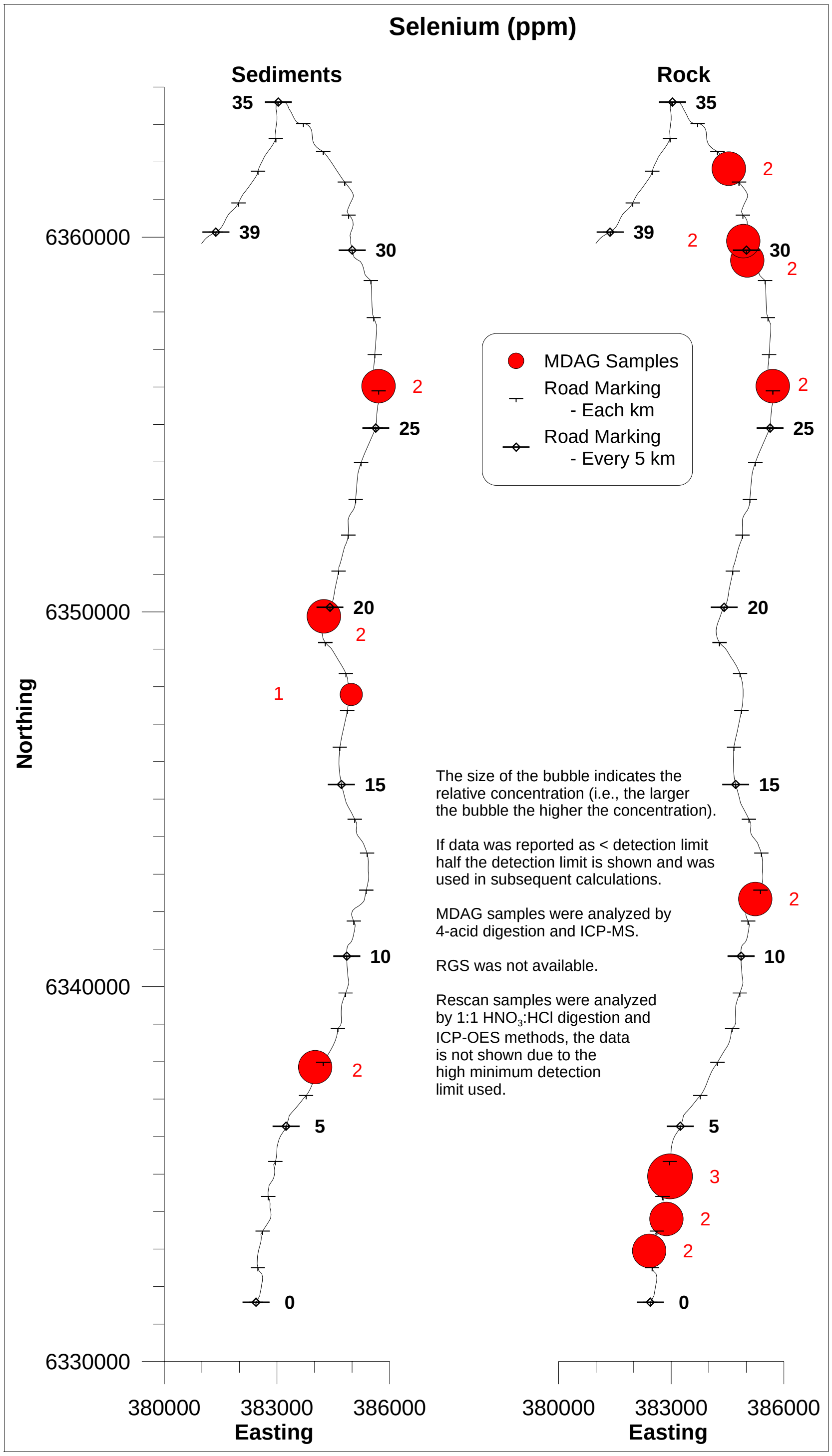
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

Figure 4-14. Map of Adjusted Total-Sulphur-Based Net Potential Ratio (Adj TNPR) near the Proposed Road Alignment and in Mess Creek Valley.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

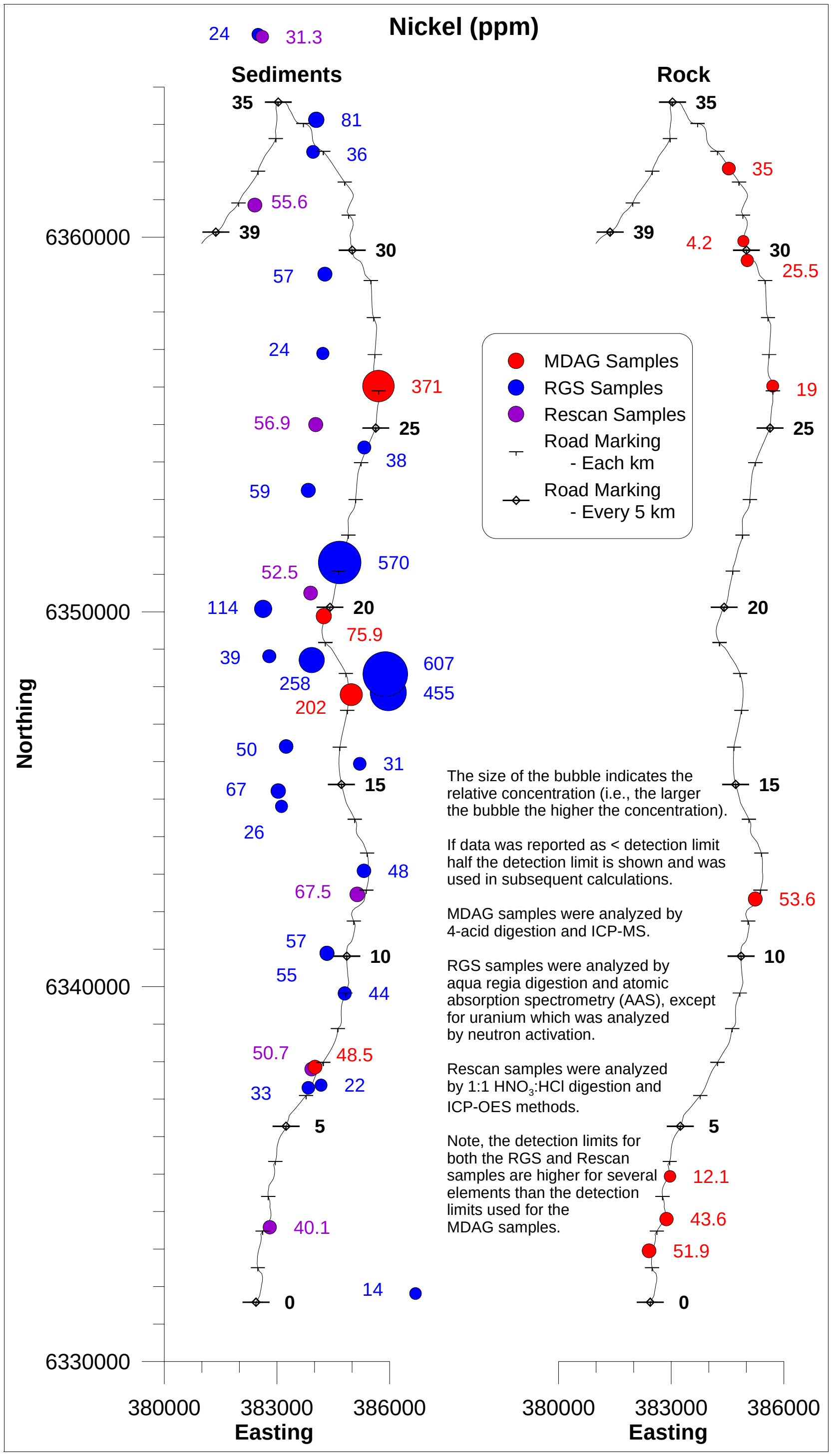
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS was not available.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods, the data is not shown due to the high minimum detection limit used.

Figure 4-15. Map of Solid-Phase Selenium near the Proposed Road Alignment and in Mess Creek Valley.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for both the RGS and Rescan samples are higher for several elements than the detection limits used for the MDAG samples.

Figure 4-16. Map of Solid-Phase Nickel near the Proposed Road Alignment and in Mess Creek Valley.

The solid-phase elements of greatest potential ML concern were based on three criteria. The first was their variability along the road alignment. In other words, if levels were consistently high or consistently low, there were no “hot spots” of potential concern for that element. Second, if the highest values were close to or above general crustal abundances (listed in Appendix C), then potential concern was high. Again, the solid-phase level of an element does not imply it will leach quickly into water (Section 4.3.2), but it could affect total (unfiltered) concentrations in water if suspended solids are high. Third, the element is commonly known as a water-quality concern, such as copper rather than potassium.

Based on these three criteria, the seven elements of greatest potential ML-ARD concern in sediments were antimony, arsenic, barium, cadmium, chromium, copper, and nickel. Sections of the proposed road alignment with elevated levels of concern are graphically depicted in Figure 4-17, as vertical lines along sections of proposed road. The total number of these elements, elevated along specific sections of the proposed road, showed that all seven were not elevated at the same location (Figure 4-18), but up to four were.

Similarly for rock, there were 12 elements of greatest potential concern based on the three preceding criteria, plus at least an “uncertain” potential for ARD (Figure 4-19). Notably, at km 32-34, eight of the 12 elements of greatest concern were elevated. The lack of rock samples from roughly km 5 to km 24, and from km 34 to km 39.5, precluded an assessment there. This incorrectly implied no ML-ARD concern, because zero elements were elevated in these sections (Figure 4-20). However, indirect information from Chapter 3 can be used to supplement the less abundant direct information for rock.

4.5 Summary of Direct ML-ARD Information for the Proposed Access Road

In summary, the authors of this report flew by helicopter along the proposed road alignment, collecting photographs, notes, and surficial solid-phase samples. As explained in Chapter 3, most of the alignment lies over sediments and alluvium. This field study confirmed most of the alignment was covered by trees and other vegetation, and thus was not readily accessible for sampling of geological materials.

Rusty-coloured iron staining, sometimes a sign of surficial ML-ARD, was seen along some portions of the alignment. These areas could not be safely reached without additional equipment, so their ML-ARD status is unknown. However, the colouring and staining appeared consistent with locally significant ML-ARD.

Acid base accounting (U.S. EPA 600 compliant Sobek ABA) of the eight samples of surficial rock and four samples of surficial sediments, collected near the proposed access-road alignment, showed that all had near-neutral paste pH at the time of analysis. Total sulphur ranged from <0.01%S in one rock sample to 0.39%S in another rock sample. Most of that total sulphur was potentially acid-generating sulphide, so the more easily measured total sulphur can be used for convenience. However, sulphur values below 0.05%S were relatively inaccurate. Three of the four highest sulphide values were found in the sediment samples, which are typically thought of as weathered and oxidized. Thus, the ARD potential of the sediments cannot be ignored.

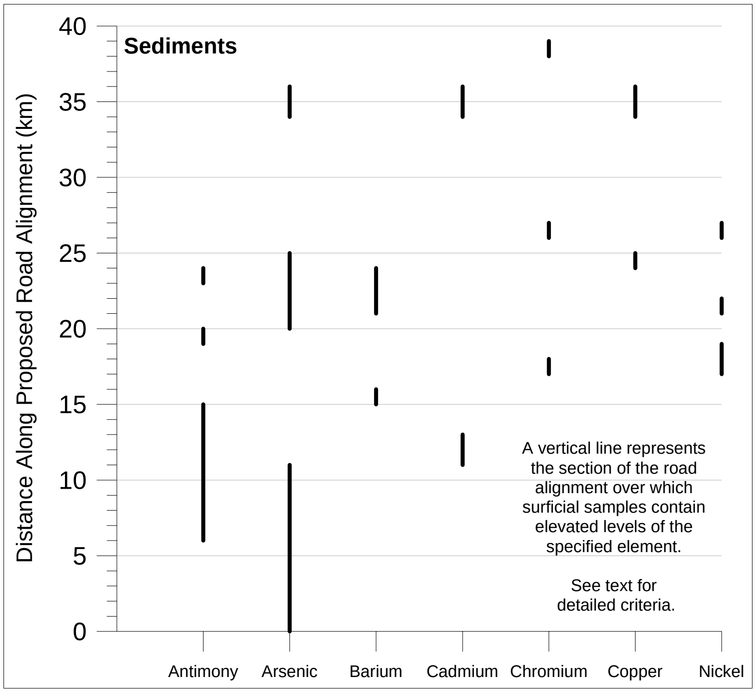


Figure 4-17. Sections of the Proposed Road with Elevated Solid-Phase Levels in Surficial Sediments for Seven Elements of Potential ML-ARD Concern.

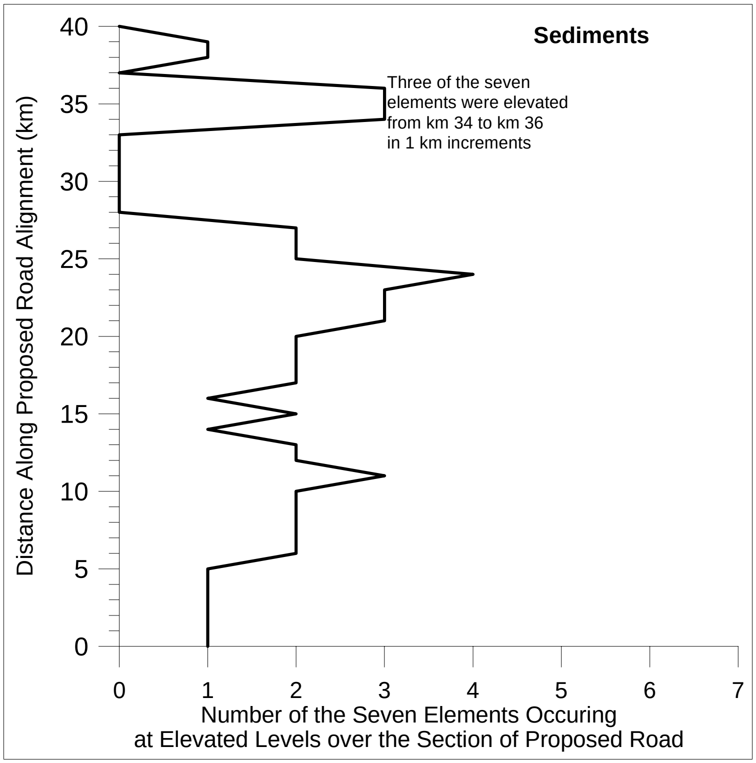


Figure 4-18. Sums of Elements in Surficial Sediments of Potential ML-ARD Concern along Sections of the Proposed Road.

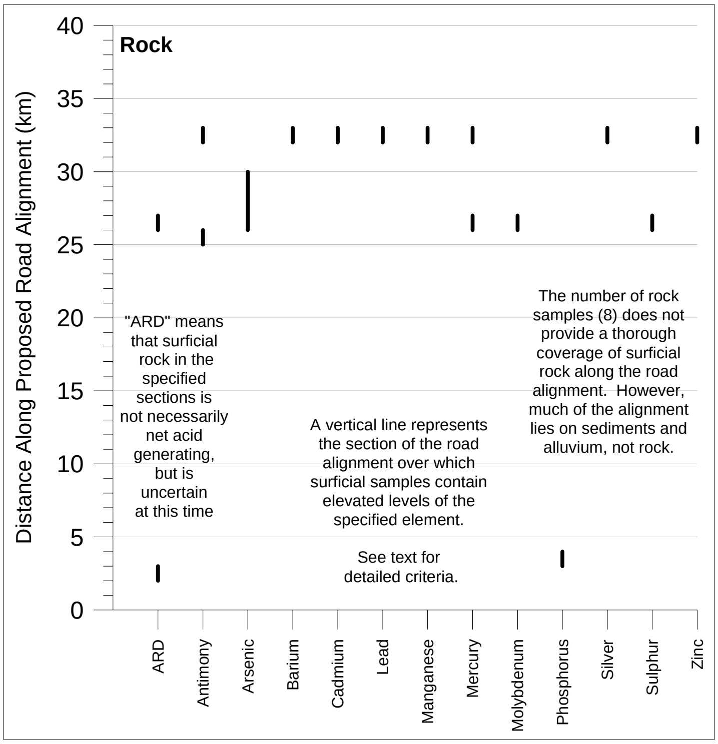


Figure 4-19. Sections of the Proposed Road with Elevated Solid-Phase Levels in Surficial Rock for Twelve Elements of Potential ML-ARD Concern.

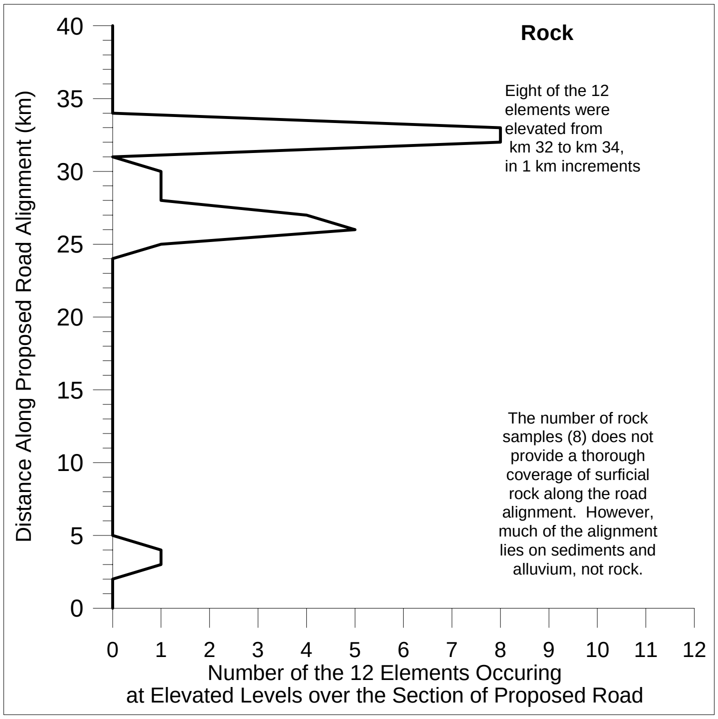


Figure 4-20. Sums of Elements in Surficial Rock of Potential ML-ARD Concern along Sections of the Proposed Road.

Neutralization Potential (NP) ranged from 9 to 387 kg $CaCO_3$ equivalent/tonne, with four of the five highest NP values in sediments. Thus, the sediments contained sufficient NP to offset any internal acid generation by sulphur. In many samples, the Sobek NP was apparently mostly comprised of calcite ($CaCO_3$), which could be measured by the simpler analytical techniques for total carbon or inorganic carbonate. Net balances of acid-generating and acid-neutralizing capacities were based on the Total-Sulphur-Based Net Potential Ratio (TNPR), with and without adjustments for unavailable NP. This showed eleven samples were net neutralizing indefinitely, plus one sample of rock that was “uncertain” without additional testing. When various amounts of unavailable NP were considered, a second sample of rock showed large changes in TNPR, suggesting the ARD status of this sample was also uncertain without additional testing.

Total-element contents of the 12 access-road samples of surficial rock and sediments were measured by ICP-MS analysis after strong four-acid digestion, and by x-ray-fluorescence (XRF) whole-rock analysis. This showed that most of the 12 access-road samples consisted predominantly of silica and alumina, with substantial and sometimes dominant amounts of iron, calcium, magnesium, sodium, potassium, and Loss on Ignition (LOI). LOI often reflects the weight loss from the samples of some or all sulphur, carbon, and tightly bound or crystalline water. Also, the 12 samples often contained elevated levels of bismuth and selenium, with fewer to rare elevated levels of silver (two samples of rock), cadmium (one sample of rock), chromium (one sample of sediment), phosphorus (one sample of rock), lead (one sample of rock), antimony (two rock and one sediment sample), and zinc (one rock sample also with the highest silver, cadmium, lead, and antimony).

Solid-phase correlations of total elements can sometimes reveal mineralogical associations. For example, elements correlating with sulphide may occur predominantly within the sulphide minerals. The elements showing at least some minor correlation with sulphide included arsenic, copper, mercury, and nickel. The elements showing at least some minor correlation with Neutralization Potential, which can dissolve and release metals even without sulphide oxidation, included calcium and manganese.

The preceding information on total elements was combined with “indirect” RGS data and Rescan data along the proposed road alignment. This allowed a spatial interpretation of the data, to highlight sections of the proposed roads with higher ML potential. However, these other sources did not include ABA, so ARD potential was available only for our MDAG samples. For total sulphur, the highest and lowest values were in surficial rock, between km 26 and 31. Nevertheless, some surficial sediments carried significant levels of total sulphur, which were well distributed along the road alignment. For ARD potential, the lowest, “uncertain” values were found near km 26 around Nahta Creek also near the southern end around km 2. The latter sample had low, relatively inaccurate sulphur analyses, so its ARD status was considered “uncertain”.

In areas where both surficial rock and sediment analyses were available, sediments sometimes had notably higher levels of some elements. This suggested sediments were not necessarily genetically related to local rock.

Based on selected solid-phase criteria that do not necessarily characterize ML-ARD potential accurately, the seven elements of greatest ML-ARD potential in surficial sediments were antimony, arsenic, barium, cadmium, chromium, copper, and nickel. However, these elements were only elevated along specific sections of the proposed road, and not all seven were elevated at the same location.

Similarly for surficial rock, there were 12 elements of greatest potential ML concern, plus at least an “uncertain” potential for ARD along specific sections of the proposed road. Notably, at km 32-34, eight of the 12 elements of greatest concern were elevated. The lack of rock samples from roughly km 5 to km 24, and from km 34 to km 39.5, precluded an assessment there. This incorrectly implied no ML-ARD concern, because zero elements were elevated in these sections. However, indirect information from Chapter 3 can be used to supplement the less abundant direct information for rock.

5. ML-ARD RANKINGS FOR THE PROPOSED ACCESS ROAD

Indirect information on ML-ARD potential for rock and unconsolidated sediments along the proposed access road was discussed in Chapter 3. Direct information of surficial rock and sediments was discussed in Chapter 4. These chapters showed that some surficial rock had an uncertain capacity to release ARD, and more extensive areas of surficial rock and sediments might leach metals at elevated levels even at neutral pH. This chapter brings together all the direct and indirect information to create ML-ARD rankings for sections of the proposed alignment.

There are two sets of Categories for ranking in this report.

ARD: acidic drainage due to sulphide-mineral oxidation and associated metal hydrolysis and/or precipitation

ML: metal leaching; ARD nearly always includes accelerated ML, but accelerated ML can also occur without ARD.

Not included here: water-quality parameters potentially created by construction activities, like suspended solids, nitrogen species from any blasting, organic compounds like from fuel, and any mined rock from the proposed minesite.

The Rankings used here are based on three levels.

1. Negligible to Minor (green)
2. Moderate, or Unknown, or Beyond Current Analytical Capability suggesting caution (yellow)
3. High to Severe (red)

It is important to note that Rankings should reflect the local receiving environment, but such environmental assessments are beyond the scope of this study. For example, pre-existing high background aqueous concentrations of dissolved copper might show no additional environmental effects in the future after road construction, despite a Ranking of 2 or 3 for a road section or quarry. Thus, the Rankings here assume a pristine environment. This is not consistently the case as shown in Chapters 3 and 4, by some elevated pre-existing metal levels and sulphide in sediments and rock.

The ML-ARD Rankings for each section of road were based on indirect information, like metallic-mineral potential and Regional Geochemical Surveys (Chapter 3), and direct information, like acid base accounts (ABA) and total-element contents (Chapter 4). Because surficial samples of sediments and rock were point-source samples, some judgment was needed in choosing the sections of road applying to them.

For ML Rankings of surficial sediments, the additional samples from the RGS and Rescan (2007) datasets assisted greatly for some elements (Section 4.4). Thus, the ML Rankings for surficial sediments, assuming a relationship with solid-phase levels, were relatively strong for many but not all elements. The ARD Rankings for surficial sediments were weak, due to only four samples over 39.5 km of proposed road.

For surficial rock, direct ML and ARD rankings were weak due to only eight samples. However, most of the proposed alignment is on sediment, so this is not a major issue. Nevertheless, for the road sections from ~km 5 to km 24, and from ~km 34 to km 39.5, no surficial rock was available. Thus, indirect information on metallic-mineral potential and local iron staining was used as surrogates to create ML and ARD Rankings in these sections.

The results produced Rankings for ARD and ML that spanned the range from 1 to 3 (Figure 5-1 and Table 5-1). There was no consistent spatial trend of increasing or decreasing Ranking with distance along the road. Overall, the ML Ranking along nearly the entire proposed alignment was high for surficial sediment, and was mostly moderate to high for surficial rock.

As a result, some accelerated metal leaching should be expected from the road during and after disturbance of surficial sediments and rock. However, the ML-ARD potentials of deeper sediments and rock remain unknown at this time. To clarify and improve the ML-ARD assessment of the proposed road alignment, both surficial and deeper, recommendations are offered in Chapter 6 before, during, and after road construction.

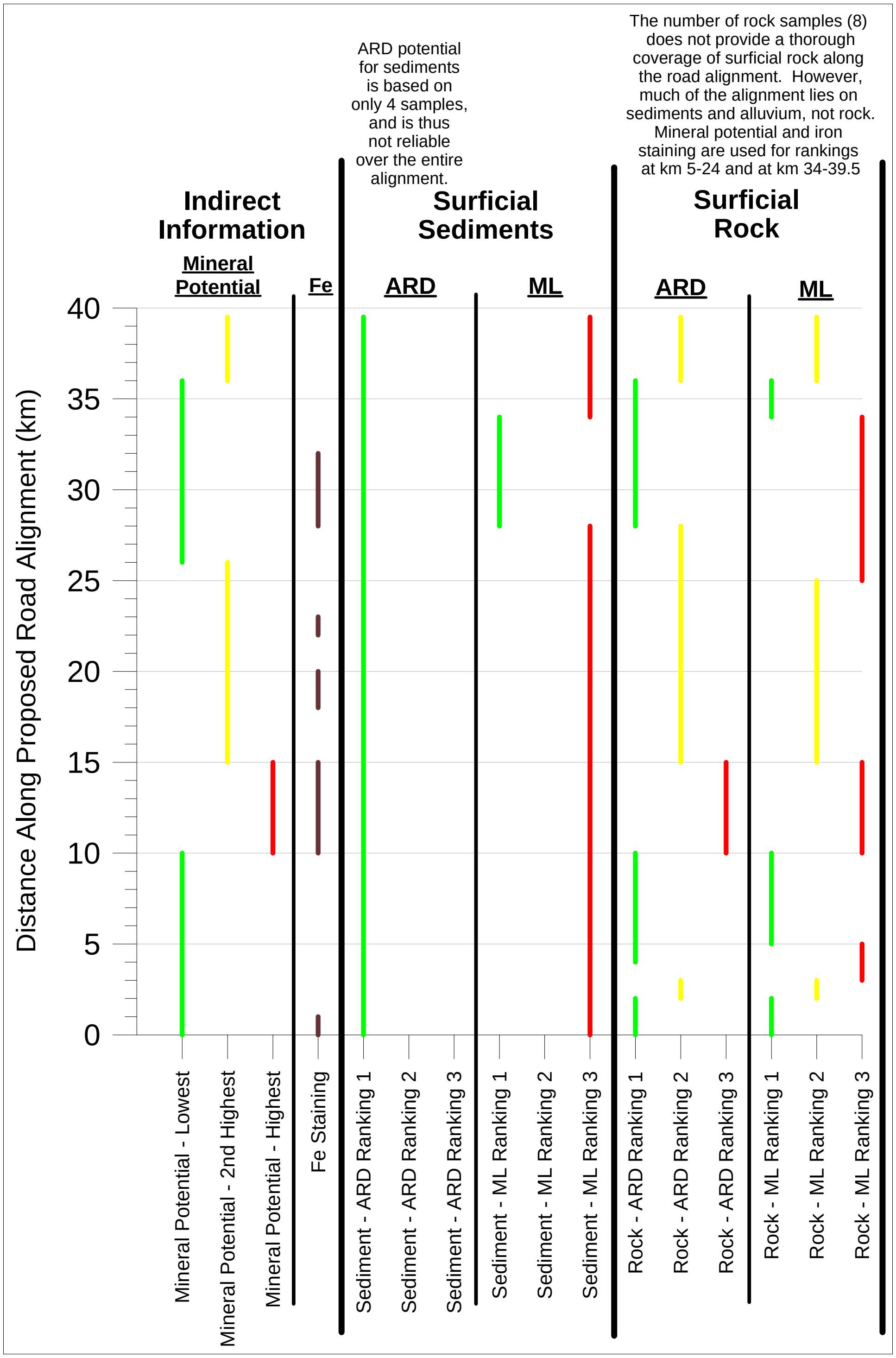


Figure 5-1. ARD and ML Rankings for Surficial Sediments and Surficial Rock along the Proposed Alignment for the Schaft Creek Access Road.

Table 5-1. ML-ARD Rankings for Surficial Sediments and Surficial Rock along the Proposed Alignment of the Schaft Creek Access Road

Road Section (km)	Surficial Sediment Ranking [1]		Surficial Rock Ranking [1,3]	
	ARD[2]	ML	ARD	ML
0-2	1	3	1	1
2-3	1	3	2	2
3-5	1	3	1	3
5-10	1	3	1	1
10-15	1	3	3	3
15-25	1	3	2	2
25-28	1	3	2	3
28-34	1	1	1	3
34-36	1	3	1	1
36-39.5	1	3	2	2

[1] Ranking 1 = Negligible to Minor (green); Ranking 2 = Moderate, or Unknown, or Beyond Current Analytical Capability suggesting caution (yellow); Ranking 3 = High to Severe (red); elevated solid-phase levels are used as surrogates for the ML rankings, although aqueous metal leaching is not necessarily dependent on solid-phase levels.

[2] ARD potential for surficial sediments is based on only 4 samples, and is thus not reliable over the entire alignment; ML potential was based on many more samples, from other studies.

[3] The number of surficial rock samples (8) does not provide thorough coverage of surficial rock along the road alignment. However, much of the alignment lies on sediments and alluvium, not rock. Mineral potential and iron staining are used for rankings at km 5-24 and at km 34-39.5.

6. ML-ARD RECOMMENDATIONS BEFORE, DURING, AND AFTER ROAD CONSTRUCTION

For this proposed access road, the pre-construction studies of Chapter 3 to 5 have shown some potential for ML-ARD, from surficial samples of both rock and unconsolidated sediments. Construction activities and any blasting may add suspended solids, other water-quality species (like nitrate, nitrite, and ammonia), and organic compounds (like fuel or oils) to drainage waters. However, only ML-ARD is addressed here.

Recent ML-ARD precedents established in Canada for roads include the following (e.g., Morin et al., 2003; Morin and Hutt, 2005 and 2007a).

1) Successful criminal prosecution under the *Fisheries Act* for ML-ARD from a road cut a few meters high and a few hundred meters long.

2) Visual examination of every horizontal meter of rock cut along dozens of kilometers of road alignment, with sampling and analysis as appropriate.

3) Major re-alignment of a highway to avoid disturbance of potentially acid-generating rock.

4) Special environmental controls and remediation for reactive rock removed from rock cuts and quarries and for broken rock used in the road bed.

5) Failure of geologic maps, preconstruction environmental and geologic surveys, and surficial sampling to identify all geochemically reactive rock reliably.

Therefore, the following recommendations are offered to reduce the risk of ML-ARD from the access road.

6.1 Preconstruction ML-ARD Testing of Rock and Unconsolidated Sediments

During construction, rock might be disturbed, such as in a road cut, road fill, or rock quarry. The ML-ARD potential of this deeper material may not match that of surficial material examined in this report. Before any substantial disturbance of rock, continuous core should be drilled to one meter vertically below the proposed bottom of the disturbance. Drill holes should be spaced 50 m apart along proposed rock disturbances that extend continuously more than 500 m; otherwise, drill holes should be spaced 20 m apart. Every one-meter-long interval from each hole should be analyzed.

During road construction, unconsolidated material like sand, gravel, alluvium, and soil may be disturbed, such as by road cuts, road fills, and granular borrow pits. Before any substantial disturbance of unconsolidated materials, auger holes or drill holes or hand-dug holes should be excavated to one meter vertically below the proposed bottom of the disturbance. Holes for unconsolidated materials should be spaced 100 m apart along proposed rock disturbances that extend continuously more than 500 m; otherwise, drill holes should be spaced 40 m apart. Every one-meter-long interval from each hole should be analyzed.

Every one-meter-long interval (one-meter composites) from each hole should be analyzed for the inorganic parameters in Table 6-1. Any analyses indicating a potential problem with future drainage chemistry should lead to:

(1) relocation of proposed construction to another location, or
(2) design of remediation procedures such as long-term water treatment, which should be started immediately upon disturbance unless a delay can be justified by the analyses.

Before construction, local waters should be analyzed for baseline water quality (Table 6-2). In this way, any pre-existing water-quality problems would not be attributed later to road construction, and any later construction impacts would be reliably defined.

6.2 Construction ML-ARD Testing of Rock and Unconsolidated Sediments

Past ML-ARD work in Canada has shown that the spacing of drill holes or auger holes during the preconstruction phase will not necessarily be sufficient to identify all reactive material in advance reliably. Therefore, additional work is required during construction.

As any substantial amounts of rock or unconsolidated material is disturbed, a geologist or engineer experienced in environmental drainage chemistry and ML-ARD should visually examine the disturbed material and the remaining walls. This visual examination should look for evidence of reactive material, such as that listed in Table 6-3.

Any rock showing significant evidence of past, current, or future geochemical reactivity or ML-ARD (e.g., Table 6-3) should be collected and submitted for the analyses in Table 6-1. Any analysis indicating a potential problem with future drainage chemistry requires immediate design of remediation procedures such as long-term water treatment. These procedures should be started immediately, unless a delay is justified by the analyses.

Before disturbance, local waters should be analyzed for baseline ML-ARD water quality (Table 6-2). Then, during construction, local water should be periodically analyzed for the following reasons.

1) Changes from baseline conditions might indicate some reactive material had not been detected, and
2) The success of any implemented remediation efforts would be characterized.

Frequent, inexpensive field measurements of pH and electrical conductivity in local waters, like puddles and seeps, would provide advance warning of any major changes of dominant ions in baseline water chemistry.

Table 6-1. Recommended Solid-Phase Analyses for Estimating Effects on Drainage Chemistry

Analytical Package	Included Measurements
U.S. EPA 600-compliant Acid-Base Accounting ("Sobek ABA")[1]	paste pH
	total sulphur
	sulphide
	leachable sulphate
	Sobek neutralization potential
	inorganic carbonate
	total carbon
ICP-based Total Elements	several dozens of metals and other elements
Whole-rock Total Elements	approximately a dozen elements often representing most of the sample's mass

[1] ABA includes many calculated parameters based on the results of all analytical packages.

Table 6-2. Parameters Included in Water-Quality Analyses[1]

Immediate field measurements of pH and electrical conductivity, plus immediate in-field filtering and/or preservation of laboratory samples
General parameters, including laboratory pH, electrical conductivity, alkalinity, acidity, suspended solids, and dissolved solids
Anions, including sulphate, chloride, and fluoride
Nutrients, including nitrate, nitrite, ammonia, and phosphorus
Dozens of cations, total metals, and dissolved metals, including but not limited to calcium, magnesium, sodium, potassium, aluminum, arsenic, antimony, manganese, molybdenum, selenium, zinc, etc.

[1] Detection limits should be at or below applicable water-quality objectives and guidelines

Table 6-3. Some Visible Evidence of Past, Current, or Future Reactive Material[1]
Sulphide minerals like pyrite that might react quickly when exposed to air and moisture
Rusty secondary iron staining that might signify already-reactive rock
Other secondary-mineral staining that might represent already-active metal leaching, such as green staining often reflecting copper leaching
Carbonate minerals like calcite that can dissolve quickly in rainwater and thus release any impurities such heavy metals and other elements into drainage waters
[1] Requires solid-phase analyses of Table 6-1, and experience and knowledge, for confirmation.

6.3 Post-Construction ML-ARD Monitoring

ML-ARD monitoring of local waters (Table 6-2) should continue periodically after construction. This will show:

1) any delayed effects from road construction,
2) any effects from road usage, and
3) the ongoing success of any implemented remediation efforts.

7. REFERENCES

British Columbia Ministry of Energy, Mines and Petroleum Resources. 2006. British Columbia Regional Geochemical Survey Database. Information Circular 2006-3. 2 p.

Morin, K.A., and N.M. Hutt. 2008. *DRAFT Schaft Creek Project - Prediction of Metal Leaching and Acid Rock Drainage, Phase 2*. Report for Rescan Environmental Services Ltd., dated January 31.

Morin, K.A., and N.M. Hutt. 2007a. Highway 97C Road-Cut Environmental Prosecution Near Pennask Creek. MDAG Internet Case Study #27, www.mdag.com/case_studies/cs27.html.

Morin, K.A., and N.M. Hutt. 2007b. *Schaft Creek Project - Prediction of Metal Leaching and Acid Rock Drainage, Phase 1*. Report for Rescan Environmental Services Ltd., dated August 10.

Morin, K.A., and N.M. Hutt. 2007c. Scaling and Equilibrium Concentrations in Minesite-Drainage Chemistry. MDAG.com Internet Case Study 26, at www.mdag.com/case_studies/cs26.html.

Morin, K.A., and N.M. Hutt. 2006. Is There a Solid-Phase Sulphide Level Below Which No ARD Is Possible? MDAG Internet Case Study #21, www.mdag.com/case_studies/cs21.html.

Morin, K.A., and N.M. Hutt. 2005. Case studies and guidelines for drainage-chemistry prediction. IN: Proceedings of the 12th Annual British Columbia MEND ML/ARD Workshop, Vancouver, Canada, November 30 and December 1, 2005.

Morin, K.A., and N.M. Hutt. 2001. *Environmental Geochemistry of Minesite Drainage: Practical Theory and Case Studies, Digital Edition*. MDAG Publishing (www.mdag.com), Surrey, British Columbia. ISBN: 0-9682039-1-4.

Morin, K.A., and N.M. Hutt. 1997. *Environmental Geochemistry of Minesite Drainage: Practical Theory and Case Studies*. MDAG Publishing (www.mdag.com), Surrey, British Columbia. ISBN: 0-9682039-0-6.

Morin, K.A., N.M. Hutt, T.S. Coulter, and W.M. Tekano. 2003. Case study of non-mining prediction and control of acid rock drainage - the Vancouver Island Highway Project. IN: T. Farrell and G. Taylor, eds., Proceedings from the Sixth International Conference on Acid Rock Drainage, July 14-17, Cairns, Australia, p. 495-501. The Australian Institute of Mining and Metallurgy.

Price, W.A., K.A. Morin, N.M. Hutt. 1997. Guidelines for the prediction of acid rock drainage and metal leaching for mines in British Columbia: Part II. Recommended procedures for static and kinetic testing. IN: Proceedings of the Fourth International Conference on Acid Rock Drainage, May 31-June 6, Vancouver, Canada, Volume I, p. 15-30.

Price, W.A., and J.C. Errington. 1998. Guidelines for Metal Leaching and Acid Rock Drainage at Minesites in British Columbia. Issued by the British Columbia Ministry of Energy and Mines.

Price, W.A. 1998. Draft Manual for the Prediction of Metal Leaching and Acid Rock Drainage. Issued by the British Columbia Ministry of Energy and Mines.

Rescan Tahltan Environmental Consultants. 2007. Schaft Creek Project 2006 Aquatics Baseline Report. Report dated March 2007.

Sobek, A.A., W.A. Schuller, J.R. Freeman, and R.M. Smith. 1978. Field and Laboratory Methods Applicable to Overburdens and Minesoils. Report EPA-600/2-78-054, U.S. National Technical Information Report PB-280 495. 403 p.

APPENDIX A. UTM Coordinates in NAD 83 Datum of the Proposed Access Road for the Schaft Creek Project

Schaft Creek Project

UTM Coordinates for the Proposed Access Road Every 100 m

Road km	Easting	Northing		Road km	Easting	Northing
0.0	382441	6331581		4.0	382958	6335339
0.1	382492	6331667		4.1	382975	6335437
0.2	382537	6331756		4.2	382993	6335535
0.3	382559	6331853		4.3	382994	6335635
0.4	382578	6331951		4.4	383005	6335735
0.5	382593	6332050		4.5	383026	6335832
0.6	382611	6332149		4.6	383059	6335927
0.7	382616	6332248		4.7	383094	6336020
0.8	382594	6332343		4.8	383151	6336102
0.9	382527	6332413		4.9	383207	6336184
1.0	382490	6332506		5.0	383242	6336277
1.1	382471	6332603		5.1	383280	6336370
1.2	382474	6332703		5.2	383305	6336466
1.3	382481	6332803		5.3	383327	6336563
1.4	382496	6332902		5.4	383391	6336638
1.5	382521	6332998		5.5	383458	6336712
1.6	382544	6333096		5.6	383523	6336788
1.7	382567	6333193		5.7	383586	6336866
1.8	382579	6333292		5.8	383650	6336942
1.9	382572	6333391		5.9	383710	6337022
2.0	382617	6333479		6.0	383774	6337099
2.1	382673	6333561		6.1	383838	6337176
2.2	382726	6333646		6.2	383882	6337265
2.3	382778	6333731		6.3	383919	6337358
2.4	382826	6333819		6.4	383956	6337451
2.5	382840	6333916		6.5	383993	6337544
2.6	382836	6334016		6.6	384030	6337637
2.7	382815	6334114		6.7	384070	6337728
2.8	382817	6334213		6.8	384123	6337813
2.9	382801	6334309		6.9	384177	6337897
3.0	382767	6334403		7.0	384231	6337981
3.1	382764	6334503		7.1	384283	6338066
3.2	382773	6334602		7.2	384333	6338153
3.3	382792	6334699		7.3	384384	6338239
3.4	382844	6334784		7.4	384437	6338324
3.5	382897	6334869		7.5	384490	6338409
3.6	382926	6334964		7.6	384532	6338499
3.7	382939	6335063		7.7	384570	6338592
3.8	382932	6335161		7.8	384588	6338690
3.9	382908	6335254		7.9	384601	6338789

Road km	Easting	Northing		Road km	Easting	Northing
8.0	384621	6338885		12.0	385378	6342575
8.1	384691	6338956		12.1	385400	6342672
8.2	384717	6339049		12.2	385422	6342770
8.3	384714	6339149		12.3	385435	6342869
8.4	384710	6339249		12.4	385438	6342969
8.5	384710	6339348		12.5	385428	6343068
8.6	384716	6339448		12.6	385425	6343168
8.7	384727	6339547		12.7	385429	6343268
8.8	384760	6339642		12.8	385432	6343368
8.9	384793	6339736		12.9	385415	6343466
9.0	384826	6339830		13.0	385400	6343565
9.1	384860	6339925		13.1	385365	6343659
9.2	384893	6340019		13.2	385329	6343752
9.3	384911	6340116		13.3	385291	6343845
9.4	384898	6340215		13.4	385232	6343924
9.5	384886	6340315		13.5	385169	6344000
9.6	384877	6340414		13.6	385123	6344089
9.7	384866	6340514		13.7	385110	6344187
9.8	384863	6340614		13.8	385123	6344286
9.9	384861	6340714		13.9	385116	6344379
10.0	384859	6340814		14.0	385070	6344468
10.1	384858	6340914		14.1	385026	6344557
10.2	384861	6341014		14.2	384981	6344647
10.3	384892	6341107		14.3	384933	6344734
10.4	384961	6341180		14.4	384884	6344822
10.5	385012	6341263		14.5	384843	6344913
10.6	385035	6341361		14.6	384818	6345009
10.7	385052	6341459		14.7	384795	6345107
10.8	385070	6341558		14.8	384770	6345203
10.9	385080	6341657		14.9	384743	6345300
11.0	385048	6341751		15.0	384716	6345396
11.1	385005	6341841		15.1	384694	6345494
11.2	384982	6341938		15.2	384678	6345592
11.3	385012	6342030		15.3	384666	6345691
11.4	385083	6342099		15.4	384659	6345791
11.5	385169	6342149		15.5	384658	6345891
11.6	385247	6342209		15.6	384657	6345991
11.7	385315	6342283		15.7	384657	6346091
11.8	385340	6342379		15.8	384659	6346191
11.9	385358	6342477		15.9	384665	6346291

Road km	Easting	Northing		Road km	Easting	Northing
16.0	384671	6346391		20.0	384410	6350122
16.1	384683	6346490		20.1	384463	6350207
16.2	384707	6346587		20.2	384489	6350303
16.3	384731	6346684		20.3	384510	6350401
16.4	384753	6346781		20.4	384528	6350499
16.5	384773	6346879		20.5	384546	6350598
16.6	384793	6346977		20.6	384565	6350696
16.7	384812	6347075		20.7	384585	6350794
16.8	384832	6347173		20.8	384606	6350892
16.9	384850	6347272		20.9	384627	6350989
17.0	384870	6347370		21.0	384640	6351089
17.1	384891	6347467		21.1	384648	6351188
17.2	384902	6347566		21.2	384681	6351282
17.3	384908	6347666		21.3	384709	6351378
17.4	384913	6347766		21.4	384733	6351475
17.5	384914	6347866		21.5	384758	6351572
17.6	384906	6347966		21.6	384783	6351669
17.7	384898	6348065		21.7	384815	6351764
17.8	384888	6348165		21.8	384847	6351859
17.9	384868	6348262		21.9	384886	6351951
18.0	384833	6348356		22.0	384898	6352048
18.1	384790	6348446		22.1	384899	6352148
18.2	384743	6348534		22.2	384898	6352248
18.3	384692	6348620		22.3	384895	6352348
18.4	384640	6348705		22.4	384893	6352448
18.5	384588	6348791		22.5	384920	6352542
18.6	384537	6348877		22.6	384970	6352629
18.7	384485	6348962		22.7	385025	6352712
18.8	384427	6349042		22.8	385067	6352802
18.9	384351	6349107		22.9	385084	6352900
19.0	384286	6349182		23.0	385095	6353000
19.1	384235	6349268		23.1	385102	6353099
19.2	384209	6349364		23.2	385109	6353199
19.3	384202	6349464		23.3	385118	6353299
19.4	384200	6349564		23.4	385127	6353398
19.5	384228	6349659		23.5	385136	6353498
19.6	384261	6349753		23.6	385144	6353598
19.7	384294	6349848		23.7	385156	6353697
19.8	384326	6349942		23.8	385178	6353794
19.9	384358	6350037		23.9	385205	6353890

Road km	Easting	Northing		Road km	Easting	Northing
24.0	385239	6353984		28.0	385577	6357848
24.1	385279	6354076		28.1	385543	6357942
24.2	385316	6354169		28.2	385537	6358042
24.3	385352	6354262		28.3	385533	6358141
24.4	385388	6354355		28.4	385529	6358241
24.5	385424	6354449		28.5	385526	6358341
24.6	385469	6354538		28.6	385522	6358441
24.7	385511	6354629		28.7	385518	6358541
24.8	385550	6354721		28.8	385515	6358641
24.9	385593	6354811		28.9	385511	6358741
25.0	385632	6354902		29.0	385500	6358840
25.1	385638	6355002		29.1	385427	6358905
25.2	385646	6355102		29.2	385358	6358977
25.3	385654	6355201		29.3	385326	6359071
25.4	385662	6355301		29.4	385300	6359168
25.5	385670	6355401		29.5	385273	6359264
25.6	385684	6355499		29.6	385220	6359348
25.7	385706	6355596		29.7	385134	6359398
25.8	385706	6355696		29.8	385056	6359458
25.9	385707	6355796		29.9	385023	6359552
26.0	385707	6355896		30.0	385003	6359649
26.1	385707	6355996		30.1	384983	6359748
26.2	385707	6356096		30.2	384961	6359845
26.3	385664	6356185		30.3	384963	6359944
26.4	385611	6356270		30.4	384944	6360042
26.5	385583	6356365		30.5	384971	6360137
26.6	385575	6356465		30.6	385008	6360230
26.7	385583	6356564		30.7	385029	6360327
26.8	385590	6356664		30.8	385021	6360426
26.9	385598	6356764		30.9	384977	6360515
27.0	385606	6356863		31.0	384908	6360587
27.1	385614	6356963		31.1	384865	6360674
27.2	385621	6357063		31.2	384896	6360768
27.3	385628	6357163		31.3	384934	6360861
27.4	385634	6357262		31.4	384978	6360951
27.5	385641	6357362		31.5	385021	6361041
27.6	385647	6357462		31.6	385026	6361139
27.7	385653	6357562		31.7	384988	6361231
27.8	385648	6357661		31.8	384926	6361309
27.9	385614	6357755		31.9	384862	6361386

Road km	Easting	Northing		Road km	Easting	Northing
32.0	384804	6361468		36.0	382969	6362626
32.1	384750	6361552		36.1	382928	6362535
32.2	384691	6361632		36.2	382878	6362449
32.3	384631	6361712		36.3	382822	6362366
32.4	384573	6361794		36.4	382766	6362283
32.5	384520	6361879		36.5	382699	6362209
32.6	384467	6361963		36.6	382652	6362121
32.7	384413	6362047		36.7	382609	6362031
32.8	384355	6362129		36.8	382564	6361942
32.9	384296	6362209		36.9	382522	6361851
33.0	384231	6362286		37.0	382494	6361755
33.1	384144	6362334		37.1	382465	6361660
33.2	384060	6362386		37.2	382414	6361574
33.3	383998	6362464		37.3	382358	6361492
33.4	383957	6362555		37.4	382301	6361409
33.5	383945	6362655		37.5	382242	6361329
33.6	383934	6362754		37.6	382183	6361248
33.7	383922	6362853		37.7	382117	6361172
33.8	383874	6362939		37.8	382065	6361088
33.9	383795	6363000		37.9	382015	6361001
34.0	383702	6363029		38.0	381975	6360909
34.1	383602	6363025		38.1	381923	6360824
34.2	383519	6363073		38.2	381857	6360750
34.3	383463	6363156		38.3	381783	6360682
34.4	383418	6363245		38.4	381712	6360612
34.5	383372	6363334		38.5	381656	6360530
34.6	383322	6363420		38.6	381622	6360436
34.7	383281	6363512		38.7	381576	6360347
34.8	383221	6363589		38.8	381520	6360264
34.9	383128	6363623		38.9	381452	6360191
35.0	383034	6363600		39.0	381372	6360132
35.1	382979	6363518		39.1	381284	6360084
35.2	382974	6363419		39.2	381197	6360034
35.3	382990	6363320		39.3	381118	6359974
35.4	383001	6363221		39.4	381052	6359899
35.5	382999	6363121		39.5	380989	6359821
35.6	382984	6363022				
35.7	382973	6362923				
35.8	382956	6362825				
35.9	382966	6362725				

APPENDIX B. MDAG Trip Report, October 17-21, 2007

This trip was to collect samples related to metal leaching and acid rock drainage (ML-ARD) at the Schaft Creek Project. This was done according to the British Columbia Policy, Guidelines, and Prediction Manual for ML-ARD.

There were two primary objectives for this trip:
1) the proposed road alignment, and
2) decades-old drill core that has been weathering in core boxes.

October 17, 2007

We (Nora Hutt and Kevin Morin) travelled from Vancouver to Smithers. We then joined Shane Uren flying to Bob Quinn airstrip and then on the Schaft Creek camp. The flight along Mess Creek to camp showed us that there would be relatively few sites with exposed rock or sand-gravel close to the road alignment. Most of the alignment was covered by trees, other vegetation, soil, and lichens.

No quarries or sand-gravel pits have yet been proposed along the road, and it is not yet clear if this is an issue. Also, deeper rock and other geological materials can have very different ML-ARD characteristics than the surficial samples collected during current ML-ARD road assessments. However, this can only be assessed with pre-construction drilling, or during construction with resulting delays for geochemical analyses and any necessary remediation or ongoing control.

Discussions with Nils on the geology of Schaft Creek and the road alignment were very helpful. We learned that there was old core at site dating back decades, although some had been lost. Because such old core can be an analogue for old mine rock, decades after mining, sample collection became an objective of this trip. We were particularly interested in obtaining old samples of the "high pyrite" zones, containing up to 10% pyrite, which were probably not caught in the Phase 1 or Phase 2 sampling.

October 18, 2007

We flew to the headwaters of Little Mess Creek, and began sampling rock and sand-gravel close to the road alignment (see sample list below). Samples were collected only when a safe landing area was nearby, and when the road alignment could be safely reached from the landing area without boats or hip-waders. Snow cover was a problem in a few areas for seeing rock.

We continued sampling until roughly noon. We then returned to camp. Due to helicopter schedules, shuttling to/from Burrage, and maintenance, we could not collect any more samples that day.

October 19, 2007

We had near-continuous helicopter support through the morning. This allowed us to collect samples quickly as the helicopter remained power up.

Around noon, we visually inspected the final part of the road (~km 33 to 37.5) and the airstrip. No rock outcrops or significant areas of sand-gravel were seen along this section, so no samples were taken.

In the afternoon, we reviewed drillhole maps for the old Hecla (H series) and Teck (T series) drillholes, relative to our existing ML-ARD samples. Also, Nils and Walter pointed out some old holes that might have elevated pyrite contents. We then visually inspected the old core, looking for intervals at least 0.3 m long with both elevated visual sulphides (see sample list below) and substantial ferric-iron staining (except T112 171-172'). This led to the collection of eight samples from the T series from 1980-1981.

October 20, 2007

In the morning, we flew from camp to Burrage airstrip. We then drove to Smithers, arriving in mid afternoon. This provided sufficient time to ship the samples of old core and from the road alignment to ALS Chemex in North Vancouver by Greyhound Courier. The samples should arrive at Chemex on Monday, October 22.

A chain-of-custody and analytical-request form was shipped with the samples. However, Shane needs to clarify the invoicing procedure.

October 21, 2007

We returned home to Surrey.

ML-ARD Samples Along the Proposed Road Alignment (SCR = Schaft Creek Road)

SCR-01 (~km 1.5)
09V 0382413 6332952
Near road alignment below talus slope and in broken-rock field. Snow cover precludes identification of broken rock as talus or in-situ subcrop. Visible rock is light grey silicified volcanics, but may be sedimentary.

SCR-02 (~km 6.9)
09V 0384018 6337854
Floodplain sediments (alluvium). Sediments are orange-brown to light grey gravelly silty sand. Sample SCR-02 contained mostly sand and finer material.

SCR-03 (~km 2.5)
09V 0382875 6333799
High rock outcrop along creek, with road alignment above in the outcrop. Sample SCR-03 was collected at the base of the outcrop, and contained mostly green to black mafic rock (gabbro and peridotite?) and some silicic volcanics.

SCR-04 (~km 3.7)
09V 0382970 6334938
In Little Mess Valley. Black to green-black basalt with thin quartz veining, ands some medium grey volcanics

SCR-05 (~km 11.8)
09V 0385240 6342335
Water in channel against east slope: pH = 6.56, conductivity = 830 µS/cm
Road alignment ~40 m up slope. Ground covered with vegetation and soil. One angular boulder ~1 m long near road alignment was matrix-supported conglomerate. Sample SCR-05 was small angular pieces of medium-grey volcanics near the conglomerate boulder.

SCR-06 (~km 17.4)
09V 0384980 6347790
Floodplain of Alexander Creek ~100 m wide; cobbles, gravel, and sand; Sample SCR-06 was brown to medium-grey to buff gravel. Alexander Creek pH = 8.00, conductivity = 260 µS/cm.

SCR-07 (~km 19.8)
09V 0384250 6349882
Brown sand exposure with some cobbles along east side of Mess Creek. Sample SCR-07 was half sand and half cobbles.

SCR-08 (~km 26.2)
09v 0385705 6356021
Road crossing at Nahta Creek. Nahta Creek pH = 7.89, conductivity = 140 µS/cm. Sample SCR-08A: rock outcrop on south side of creek: heavily weathered greywacke with heavy iron staining on rock surfaces. Sample SCR-08B: Nahta Creek alluvium: grey sand and gravel

SCR-09 (~km 29.8)
09V 0385028 6359373
Small outcrop ~10 m from easternmost channel; black small-block ("chunky") mudstone with some blue and green grains

SCR-10 (~km 30.3)
09V 0384923 6359889
Road alignment is ~half way up a high, steep outcrop. Sample SCR-10 was collected from boulders at the base of the outcrop; dark brown to medium grey, small-block ("chunky") silicified mudstone or volcanic.

SCR-11 (~km 32.5)
09V 0384536 6361822
Rock outcrop in the middle of Mess Creek floodplain, adjacent to road alignment. Sample SCRF-11 was dark brown to black small-block (“chunky”) silicified mudstone or volcanic.

APPENDIX C. ML-ARD Analyses of Surficial Proposed-Access-Road Samples

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: Sampled by MDAG Oct '07.

Sample	Top of Drillholes UTM NAD 27				Approx. km Along	Material		Adjacent Water	
Id.	Zone	Easting	Northing	Elevation (m)	Road	Type	Description	pH (pH units)	Conductivity (uS/cm)
Method									
MDL									
Crustal Abundance: From									
Crustal Abundance: To									
SCR-01	09V	382413	6332952	1133.3	1.5	Rock	Near road alignment below talus slope and in broken-rock field. Snow cover precludes identification of broken rock as talus or in-situ subcrop Visible rock is light grey silicified volcanics, but may be sedimentary.		
SCR-02	09V	384018	6337854	843.0	6.9	Sediment	Floodplain sediments (alluvium). Sediments are ornage-brown to light grey gravelly silty sand. Sample SCR-02 contained mostly sand and finer material.		
SCR-03	09V	382875	6333799	1035.9	2.5	Rock	High rock outcrop along creek, with road alignment above in the outcrop. Sample SCR-03 was collected at the base of the outcrop, and contained mostly green to black mafic rock (gabbro and peridotite?) and some silicic volcanics.		
SCR-04	09V	382970	6334938	1021.3	3.7	Rock	In Little Mess Valley. Black to green-black basalt with thin quartz veining, ands some medium grey volcanics		
SCR-05	09V	385240	6342335	812.7	11.8	Rock	Road alignment ~40 m up slope. Ground covered with vegetation and soil. One angular boulder ~1 m long near road alignment was matrix-supported conglomerate. Sample SCR-05 was small angular pieces of medium-grey volcanics near the conglomerate boulder. Collected water in channel against east slope.	6.56	830
SCR-06	09V	384980	6347790	793.7	17.4	Gravel	Floodplain of Alexander Creek ~100 m wide; cobbles, gravel, and sand; Sample SCR-06 was brown to medium-grey to buff gravel.	8	260
SCR-07	09V	384250	6349882	751.9	19.8	Sediment	Brown sand exposure with some cobbles along east side of Mess Creek. Sample SCR-07 was half sand and half cobbles.		
SCR-08A	09V	385705	6356021	756.0	26.2	Rock	Road crossing at Nahta Creek. Sample SCR-08A: rock outcrop on south side of creek: heavily weathered greywacke with heavy iron staining on rock surfaces.	7.89	140
SCR-08B	09V	385705	6356021	756.0	26.2	Sediment	Road crossing at Nahta Creek. Sample SCR-08B: Nahta Creek alluvium: grey sand and gravel		
SCR-09	09V	385028	6359373	718.5	29.8	Rock	Small outcrop ~10 m from easternmost channel; black small-block (“chunky”) mudstone with some blue and green grains		
SCR-10	09V	384923	6359889	721.6	30.3	Rock	Road alignment is ~half way up a high, steep outcrop. Sample SCR-10 was collected from boulders at the base of the outcrop; dark brown to medium grey, small-block (“chunky”) silicified mudstone or volcanic.		
SCR-11	09V	384536	6361822	724.5	32.5	Rock	Rock outcrop in the middle of Mess Creek floodplain, adjacent to road alignment. Sample SCRF-11 was dark brown to black small-block (“chunky”) silicified mudstone or volcanic.		

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: Sampled by MDAG Oct '07.
pH of DI water used for paste pH read 6.2

Sample Id.	Paste pH	S (Total)	S (Sulphide)	S (Sulphide)	Carbonate Leach S (Sulphate)	HCl Leachable S (Sulphate)	$S(BaSO_4)$	$S(del_{actual})$	S(del)	TAP	SAP	PAP	NP	Available NP	Total C	Inorganic C	Inorganic CO_2	Excess C
	Unity	(% Leco)	(% Leco)	(% Calc)	(%)	(%)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(% Leco)	(%)	(%)	(%)
Method	OA-ELE07	S-IR08	S-IR07	S-CAL06	S-GRA06	S-GRA06a	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	OA-VOL08	Calculated	C-IR07	C-GAS05	C-GAS05	Calculated
MDL	0.1	0.01	0.01	0.01	0.01	0.01							1		0.01	0.05	0.2	
SCR-01	8.6	0.01	0.02	-0.01	*0.005*	0.02	0.002	-0.032	0.000	0.3	0.6	0.2	15	5	0.24	0.07	0.3	0.17
SCR-02	9	0.16	0.16	0.15	0.01	0.01	0.015	-0.025	0.000	5.0	5.0	4.6	160	150	2.13	1.99	7.3	0.14
SCR-03	9.2	0.01	0.02	0	*0.005*	0.01	0.025	-0.045	0.000	0.3	0.6	0.3	9	-1	0.07	*0.025*	0.2	0.045
SCR-04	9.4	0.01	0.01	-0.01	*0.005*	0.02	0.019	-0.039	0.000	0.3	0.3	0.2	51	41	0.48	0.44	1.6	0.04
SCR-05	8.5	0.06	0.06	0.05	0.01	0.01	0.017	-0.027	0.000	1.9	1.9	1.6	387	377	4.67	1.5	5.5	3.17
SCR-06	9	0.16	0.15	0.14	0.01	0.02	0.036	-0.046	0.000	5.0	4.7	4.2	57	47	0.49	0.44	1.6	0.05
SCR-07	8	0.02	0.02	0.01	*0.005*	0.01	0.006	-0.016	0.000	0.6	0.6	0.3	86	76	1.54	1.14	4.2	0.4
SCR-08A	6.9	0.39	0.25	0.28	0.09	0.11	0.025	0.005	0.005	12.2	8.0	7.6	16	6	0.3	0.17	0.6	0.13
SCR-08B	8.7	0.08	0.07	0.07	0.01	0.01	0.013	-0.013	0.000	2.5	2.2	1.3	164	154	1.26	1.21	4.5	0.05
SCR-09	8.7	0.01	0.03	0	*0.005*	0.01	0.021	-0.051	0.000	0.3	0.9	0.6	31	21	0.3	0.27	1	0.03
SCR-10	9.5	*0.005*	*0.005*	-0.015	*0.005*	0.02	0.031	-0.051	0.000	0.2	0.2	0.2	11	1	0.12	0.11	0.4	0.01
SCR-11	8.3	0.06	0.06	0.055	0.04	*0.005*	0.088	-0.093	0.000	1.9	1.9	0.2	29	19	0.37	0.24	0.9	0.13
Maximum	9.5	0.39	0.25	0.28	0.09	0.11	0.088	0.0049	0.0049	12.2	7.97	7.58	387	377	4.67	1.99	7.3	3.17
Minimum	6.9	0.005	0.005	-0.015	0.005	0.005	0.0021	-0.093	0	0.16	0.16	0.16	9	-1	0.07	0.025	0.2	0.01
Mean	8.65	0.081	0.071	0.06	0.017	0.021	0.025	-0.036	0.00041	2.54	2.24	1.77	84.7	74.7	1	0.63	2.34	0.36
Standard Deviation	0.71	0.11	0.076	0.09	0.025	0.028	0.022	0.025	0.0014	3.51	2.42	2.41	110	110	1.32	0.65	2.4	0.89
10 Percentile	8.03	0.01	0.011	-0.01	0.005	0.01	0.0069	-0.051	0	0.31	0.34	0.16	11.4	1.4	0.13	0.074	0.31	0.031
25 Percentile	8.45	0.01	0.02	-0.0025	0.005	0.01	0.014	-0.047	0	0.31	0.62	0.2	15.8	5.75	0.28	0.16	0.55	0.044
Median	8.7	0.04	0.045	0.03	0.0075	0.01	0.02	-0.035	0	1.25	1.41	0.47	41	31	0.42	0.36	1.3	0.09
75 Percentile	9.05	0.1	0.09	0.088	0.01	0.02	0.027	-0.023	0	3.12	2.81	2.25	104	94.5	1.33	1.16	4.28	0.15
90 Percentile	9.38	0.16	0.16	0.15	0.037	0.02	0.035	-0.013	0	5	4.97	4.59	164	154	2.07	1.47	5.4	0.38
Interquartile Range (IQR) [1]	0.6	0.09	0.07	0.09	0.005	0.01	0.013	0.024	0	2.81	2.19	2.05	88.8	88.8	1.05	1	3.73	0.1
Variance	0.5	0.013	0.0058	0.008	0.00063	0.00081	0.00049	0.00061	0.000002	12.3	5.84	5.79	11998	11998	1.75	0.43	5.75	0.79
Skewness	-1.37	2.18	1.45	1.55	2.74	3.25	2.34	-0.73	3.46	2.18	1.49	1.64	2.21	2.21	2.27	1.05	1.05	3.38
Coefficient of Variation (CoV) [2]	0.082	1.38	1.07	1.49	1.5	1.34	0.89	-0.69	3.46	1.38	1.08	1.36	1.29	1.47	1.33	1.03	1.02	2.45
Count	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12

Total
NPR < 1.0 or NPR = 1.0
1.0 < NPR < 2.0
NPR > 2.0 or NPR =2.0

% NPR < 1.0 or NPR = 1.0 of Total
% 1.0 < NPR < 2.0 of Total
% NPR > 2.0 or NPR =2.0 of Total

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

% S (Sulphide) (calc) = % S (Total) - % S (Sulphate) Carbonate Leach
$\%S(BaSO_4)$ = Ba (ppm) * 0.0001 * 32.06 / 137.37
% S (del $_{actual}$) = %S(Total) - %S(Sulphide) Leco - %S(Sulphate) Carbonate Leach - $\%S(BaSO_4)$
% S (del) = % S (del $_{actual}$) unless < 0, then 0
TAP = % S (Total) * 31.25
SAP = % S (Sulphide + del) * 31.25

PAP = % Pyrite(Calculated) * 31.25
Note: If Calculated Pyrite is < 0.005 then calculated pyrite assumed to be 0.005
Unavailable NP (UNP) = 10
Available NP = NP - Unavailable NP

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: Sampled by MDAG Oct '07.

Sample Id.	Total CaNP (kg $CaCO_3$/t)	Inorganic CaNP (kg $CaCO_3$/t)	(Ca) CaNP (kg $CaCO_3$/t)	(Ca+Mg) CaNP (kg $CaCO_3$/t)	TNNP (kg $CaCO_3$/t)	Adjusted TNNP (kg $CaCO_3$/t)	SNNP (kg $CaCO_3$/t)	Adjusted SNNP (kg $CaCO_3$/t)	PNNP (kg $CaCO_3$/t)	Adjusted PNNP (kg $CaCO_3$/t)	TNPR	Adjusted TNPR	SNPR	Adjusted SNPR	PNPR	Adjusted PNPR	Fizz Rating Unity	Comparison of Fizz Rating & NP
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	OA-VOL08	
MDL																		
SCR-01	20.0	6.8	129.9	272.7	14.7	4.7	14.4	4.4	14.8	4.8	48	16	24	8	68.2	22.7	1	Agree
SCR-02	177.5	166.0	96.4	201.0	155.0	145.0	155.0	145.0	155.4	145.4	32	30	32	30	34.5	32.4	3	Agree
SCR-03	5.8	4.5	6.5	90.5	8.7	-1.3	8.4	-1.6	8.7	-1.3	28.8	0.001	14.4	0.001	26.3	0.001	1	Agree
SCR-04	40.0	36.4	81.9	160.1	50.7	40.7	50.7	40.7	50.8	40.8	163	131	163	131	200	200	2	Agree
SCR-05	389.2	125.1	392.1	454.7	385.1	375.1	385.1	375.1	385.4	375.4	206	201	206	201	240	234	3	Agree
SCR-06	40.8	36.4	49.9	173.5	52.0	42.0	52.3	42.3	52.8	42.8	11.4	9.4	12.2	10	13.7	11.3	2	Agree
SCR-07	128.3	95.5	65.4	123.9	85.4	75.4	85.4	75.4	85.7	75.7	138	122	138	122	258	228	2	Agree
SCR-08A	25.0	13.6	15.5	21.7	3.8	-6.2	8.0	-2.0	8.4	-1.6	1.31	0.492	2.01	0.753	2.11	0.791	2	Disagree
SCR-08B	105.0	102.3	112.1	365.3	161.5	151.5	161.8	151.8	162.7	152.7	65.6	61.6	75	70.4	128	120	3	Agree
SCR-09	25.0	22.7	111.4	165.3	30.7	20.7	30.1	20.1	30.4	20.4	99.2	67.2	33.1	22.4	51.5	34.9	2	Disagree
SCR-10	10.0	9.1	15.7	21.1	10.8	0.8	10.8	0.8	10.8	0.8	200	200	200	200	200	200	2	Disagree
SCR-11	30.8	20.5	27.2	65.9	27.1	17.1	27.1	17.1	28.8	18.8	15.5	10.1	15.5	10.1	200	200	2	Disagree
Maximum	389	166	392	455	385	375	385	375	385	375	206	201	206	201	258	234		
Minimum	5.83	4.55	6.49	21.1	3.81	-6.19	8.03	-1.97	8.42	-1.58	1.31	0.001	2.01	0.001	2.11	0.001		
Mean	83.1	53.3	92	176	82.1	72.1	82.4	72.4	82.9	72.9	84.1	70.7	76.3	67.1	119	107		
Standard Deviation	110	54.5	104	133	110	110	109	109	109	109	75	75.1	78.1	76.9	96	98.5		
10 Percentile	11	7.05	15.5	26.1	8.9	-1.1	8.62	-1.38	8.88	-1.12	11.8	1.38	12.4	1.48	15	1.84		
25 Percentile	23.8	12.5	24.3	84.3	13.7	3.73	13.5	3.49	13.8	3.8	25.5	9.93	15.2	9.5	32.4	19.8		
Median	35.4	29.6	73.7	163	40.7	30.7	40.4	30.4	40.6	30.6	56.8	45.8	32.6	26.2	98.1	77.4		
75 Percentile	111	97.2	112	219	103	92.8	103	92.8	103	93.1	144	124	144	124	200	200		
90 Percentile	173	123	128	356	161	151	161	151	162	152	196	193	196	193	236	225		
Interquartile Range (IQR) [1]	87.1	84.7	87.2	135	89.1	89.1	89.3	89.3	89.3	89.3	119	114	129	115	168	180		
Variance	12141	2972	10730	17619	12014	12014	11972	11972	11966	11966	5629	5642	6106	5907	9213	9695		
Skewness	2.27	1.05	2.47	0.92	2.22	2.22	2.23	2.23	2.22	2.22	0.62	0.86	0.81	0.93	0.2	0.18		
Coefficient of Variation (CoV) [2]	1.33	1.02	1.13	0.75	1.33	1.52	1.33	1.51	1.32	1.5	0.89	1.06	1.02	1.14	0.81	0.92		
Count	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12		
Total																		
NPR < 1.0 or NPR = 1.0											0	2	0	2	0	2		
1.0 < NPR < 2.0											1	0	0	0	0	0		
NPR > 2.0 or NPR =2.0											11	10	12	10	12	10		
% NPR < 1.0 or NPR = 1.0 of Total											0.00	16.67	0.00	16.67	0.00	16.67		
% 1.0 < NPR < 2.0 of Total											8.33	0.00	0.00	0.00	0.00	0.00		
% NPR > 2.0 or NPR =2.0 of Total											91.67	83.33	100.00	83.33	100.00	83.33		

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: Sampled by MDAG Oct '07.

Sample Id.	Total CaNP	Inorganic CaNP	(Ca) CaNP	(Ca+Mg) CaNP	TNNP	Adjusted TNNP	SNNP	Adjusted SNNP	PNNP	Adjusted PNNP	TNPR	Adjusted TNPR	SNPR	Adjusted SNPR	PNPR	Adjusted PNPR	Fizz Rating	Comparison of Fizz Rating & NP
	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)							Unity	
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	OA-VOL08	
MDL																		

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

Total CaNP = % C * 10 * 100.09 / 12.01
Inorganic CaNP = % CO_2 * 10 * 100.09 / 44.01
(Ca) CaNP = (Ca(ppm) * 100.09 / 40.08) / 1000
(Ca+Mg) CaNP = ((Ca(ppm) * 100.09 / 40.08) + (Mg(ppm) * 100.09 / 24.31)) / 1000
TNNP = NP - TAP
Adjusted TNNP = Available NP - TAP
SNNP = NP - SAP
Adjusted SNNP = Available NP - SAP
PNNP = NP - PAP
Adjusted PNNP = Available NP - PAP

- TNPR = NP / TAP
  - Note: If % S(Total) < 0.01 then TNPR = 200
  - Note: If % S(Total) > 0.01 and NP < = 0 then TNPR = 0.001
- Adjusted TNPR = UNP / TAP
  - Note: If % S(Total) < 0.01 then Adjusted TNPR = 200
  - Note: If % S(Total) > 0.01 and UNP < = 0 then Adjusted TNPR = 0.001
- SNPR = NP / SAP
  - Note: If % S(Sulphide + del) < 0.01 then SNPR = 200
  - Note: If % S(Sulphide + del) > 0.01 and NP < = 0 then SNPR = 0.001
- Adjusted SNPR = UNP / SAP
  - Note: If % S(Sulphide + del) < 0.01 then Adjusted SNPR = 200
  - Note: If % S(Sulphide + del) > 0.01 and UNP < = 0 then Adjusted SNPR = 0.001
- PNPR = NP / PAP
  - Note: If % S(Pyrite, calc) < 0.01 then PNPR = 200
  - Note: If % S(Pyrite, calc) > 0.01 and NP < = 0 then PNPR = 0.001
- Adjusted PNPR = UNP / TAP
  - Note: If % S(Pyrite, calc) < 0.005 then Adjusted PNPR = 200
  - Note: If % S(Pyrite, calc) > 0.005 and UNP < = 0 then Adjusted PNPR = 0.001

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Calculated Mineralogy**
Comments: Sampled by MDAG Oct '07.

Sample Id.	Calculated S (Pyrite) FeS_2 (%)	Calculated S (Chalcopyrite) $CuFeS_2 + CuS_2$ (%)	Calculated S (Arsenopyrite) FeAsS + AsS (%)	Calculated S (Galena) PbS (%)	Calculated S (Cinnibar) HgS (%)	Calculated S (Molybdenite) MoS_2 (%)	Calculated S (Pentlandite) ~NiS (%)	Calculated S (Sphalerite) ZnS (%)
SCR-01	0.007	0.006	0.00036	0.00005	0.00000008	0.0000	0.00288	0.0039
SCR-02	0.148	0.005	0.00129	0.00008	0.00000080	0.0000	0.00269	0.0030
SCR-03	0.011	0.002	0.00025	0.00012	0.00000008	0.0000	0.00242	0.0041
SCR-04	0.003	0.001	0.00012	0.00006	0.00000008	0.0001	0.00067	0.0051
SCR-05	0.052	0.002	0.00077	0.00007	0.00000016	0.0000	0.00298	0.0026
SCR-06	0.133	0.002	0.00033	0.00008	0.00000048	0.0000	0.01122	0.0026
SCR-07	0.011	0.002	0.00019	0.00009	0.00000064	0.0002	0.00422	0.0027
SCR-08A	0.243	0.007	0.00049	0.00018	0.00001216	0.0020	0.00106	0.0016
SCR-08B	0.041	0.004	0.00039	0.00009	0.00000048	0.0001	0.02061	0.0043
SCR-09	0.019	0.004	0.00124	0.00008	0.00000016	0.0001	0.00142	0.0038
SCR-10	0.000	0.000	0.00020	0.00014	0.00000008	0.0001	0.00023	0.0039
SCR-11	-0.012	0.013	0.00038	0.00433	0.00000720	0.0001	0.00194	0.0525
Maximum	0.24	0.013	0.0013	0.0043	0.000012	0.002	0.021	0.052
Minimum	-0.012	0.00044	0.00012	0.000053	0.00000008	0.000021	0.00023	0.0016
Mean	0.055	0.004	0.0005	0.00045	0.0000019	0.00023	0.0044	0.0075
Standard Deviation	0.079	0.0033	0.00039	0.0012	0.0000038	0.00056	0.0059	0.014
10 Percentile	0.00031	0.0012	0.00019	0.000062	0.00000008	0.000021	0.00071	0.0026
25 Percentile	0.006	0.002	0.00024	0.000076	0.00000008	0.000037	0.0013	0.0026
Median	0.015	0.003	0.00037	0.000084	0.00000032	0.000063	0.0026	0.0038
75 Percentile	0.072	0.0048	0.00056	0.00012	0.00000068	0.000089	0.0033	0.0041
90 Percentile	0.15	0.0069	0.0012	0.00017	0.0000066	0.00017	0.011	0.005
Interquartile Range (IQR) [1]	0.066	0.0028	0.00032	0.000049	0.0000006	0.000052	0.002	0.0015
Variance	0.0062	0.000011	0.00000016	0.0000015	1.4E-11	0.00000031	0.000034	0.0002
Skewness	1.58	1.71	1.37	3.46	2.37	3.43	2.38	3.44
Coefficient of Variation (CoV) [2]	1.44	0.84	0.79	2.74	2.04	2.46	1.34	1.9
Count	12	12	12	12	12	12	12	12

Calculated S (Pyrite) (%) =
% S (Sulphide) + S (del) - S (Chalcopyrite) - S (Arsenopyrite) - S (Galena) - S (Cinnibar) - S (Molybdenite) - S (Sphalerite)
Calculated S (Chalcopyrite) CuFeS2 + CuS2 (%) = (1 / 0.99) * Copper (ppm) / 10000
Calculated S (Arsenopyrite) FeAsS + AsS (%) = (1 / 2.33) * Iron (%) / 10000
Calculated S (Galena) PbS (%) = (1 / 6.45) * Iron (ppm) / 10000
Calculated S (Cinnibar) HgS (%) = (1 / 6.25) * Gallium (ppm) / 10000
Calculated S (Molybdenite) MoS2 (%) = (1 / 1.5) * Germanium (ppm) / 10000
Calculated S (Sphalerite) ZnS (%) = (1 / 2) * Hafnium (ppm) / 10000

1

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: Sampled by MDAG Oct '07.
Rare earth elements may not be totally soluble in MS61 method.
ME-MS61:Interference: Ca>10% on ICP-MS As ICP-AES results shown.

Sample	Silver	Aluminum	Arsenic	Barium	Beryllium	Bismuth	Calcium	Cadmium	Cerium	Cobalt	Chromium	Cesium	Copper	Iron	Gallium	Germanium
Id.	Ag	Al	As	Ba	Be	Bi	Ca	Cd	Ce	Co	Cr	Cs	Cu	Fe	Ga	Ge
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.01	100	0.2	10	0.05	0.01	100	0.02	0.01	0.1	1	0.05	0.2	100	0.05	0.05
Crustal Abundance: From	0.037	4200	1	0.4	1	0.007	5100	0.035	11.5	0.1	2	0.4	4	3800	4	0.2
Crustal Abundance: To	0.11	88000	13	2300	3	0.01	312400	0.42	345	74	170	6	250	86500	30	8
SCR-01	0.05	94000	8.4	10	1.75	0.02	52000	0.15	25.5	27	117	*0.025*	56.9	62200	21.4	0.17
SCR-02	0.16	55900	30.1	590	0.93	0.05	38600	0.17	24.8	21.9	62	1.22	44.7	51400	13.2	0.17
SCR-03	0.08	77100	5.8	1100	1.27	0.04	2600	0.26	29.1	18.5	59	0.59	21.6	27600	17.3	0.15
SCR-04	0.12	89300	2.7	770	3.06	0.01	32800	0.13	124.5	18.7	8	0.39	10.7	81600	25.6	0.3
SCR-05	0.09	68200	18	720	0.86	0.02	157000	0.18	24.4	12.4	60	0.7	18.9	24200	14.45	0.12
SCR-06	0.07	82800	7.8	1460	1.51	0.03	20000	0.04	26.5	19.4	208	1.69	22.8	32300	19.95	0.16
SCR-07	0.09	48900	4.5	290	1.17	0.06	26200	0.13	27.3	17	97	0.62	20.1	49300	11.55	0.15
SCR-08A	0.8	64200	11.4	1050	0.78	0.07	6200	0.12	19.1	8.8	9	1.1	69.2	32100	17	0.11
SCR-08B	0.11	63500	9.2	500	1.03	0.04	44900	0.17	23.8	38	436	1.29	36.5	51000	14.75	0.15
SCR-09	0.04	97100	28.8	790	1.74	0.04	44600	0.19	34.7	23.4	38	1.78	41.4	62000	20.8	0.18
SCR-10	0.04	75900	4.7	1320	2.88	0.03	6300	0.03	48.5	3.2	21	0.84	4.4	18600	18.05	0.14
SCR-11	1.7	87900	8.8	3590	1.96	0.02	10900	2.84	39	22.6	56	1.72	124.5	45100	19.9	0.16
Maximum	1.7	97100	30.1	3590	3.06	0.07	157000	2.84	124	38	436	1.78	124	81600	25.6	0.3
Minimum	0.04	48900	2.7	10	0.78	0.01	2600	0.03	19.1	3.2	8	0.025	4.4	18600	11.6	0.11
Mean	0.28	75400	11.7	1016	1.58	0.036	36842	0.37	37.3	19.2	97.6	1	39.3	44783	17.8	0.16
Standard Deviation	0.49	15450	9.19	910	0.75	0.018	41480	0.78	28.6	8.88	120	0.56	32.9	18536	3.97	0.048
10 Percentile	0.041	56660	4.52	311	0.87	0.02	6210	0.048	23.9	9.16	10.2	0.41	11.5	24540	13.3	0.12
25 Percentile	0.065	64025	5.52	568	1.01	0.02	9750	0.13	24.7	15.8	33.8	0.61	19.8	30975	14.7	0.15
Median	0.09	76500	8.6	780	1.39	0.035	29500	0.16	26.9	19	59.5	0.97	29.6	47200	17.7	0.16
75 Percentile	0.13	88250	13	1155	1.8	0.042	44675	0.18	35.8	22.8	102	1.39	47.8	54050	20.2	0.17
90 Percentile	0.74	93530	27.7	1446	2.79	0.059	51290	0.25	47.6	26.6	199	1.72	68	62180	21.3	0.18
Interquartile Range (IQR) [1]	0.065	24225	7.52	588	0.8	0.023	34925	0.055	11.1	6.95	68.2	0.78	28	23075	5.49	0.023
Variance	0.24	238690909	84.4	828117	0.57	0.00032	1720582652	0.61	818	78.8	14389	0.32	1083	343577879	15.8	0.0023
Skewness	2.66	-0.23	1.37	2.24	1.05	0.53	2.47	3.42	3.02	0.25	2.39	-0.04	1.71	0.43	0.25	2.34
Coefficient of Variation (CoV) [2]	1.77	0.2	0.79	0.9	0.48	0.5	1.13	2.13	0.77	0.46	1.23	0.57	0.84	0.41	0.22	0.29
Count	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12

$\boxed{1.7}$ NOTE: if data is boxed, then data is 3 times the maximum crustal abundance.

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

NOTE: If data was reported as > detection limit the detection limit is shown in bold and was used in subsequent calculations.

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: Sampled by MDAG Oct '07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.
Tailings: Detection limits on samples requiring dilutions for Hg-CV41 due to inteferences or high concentration levels have been increased according to the dilution factor.

Sample	Hafnium	Mercury	Indium	Potassium	Lanthanum	Lithium	Magnesium	Manganese	Molybdenum	Sodium	Niobium	Nickel	Phosphorus	Lead	Rubidium	Rhenium
Id.	Hf	Hg	In	K	La	Li	Mg	Mn	Mo	Na	Nb	Ni	P	Pb	Rb	Re
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	Hg-CV41	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.1	0.01	0.005	100	0.5	0.2	100	5	0.05	100	0.1	0.2	10	0.5	0.1	0.002
Crustal Abundance: From	0.3	0.03	0.01	40	10	5	1600	390	0.2	400	0.3	2	170	1	0.2	NA
Crustal Abundance: To	11	0.4	0.26	48000	115	66	47000	6700	27	40400	35	225	1500	80	170	NA
SCR-01	1.1	*0.005*	0.067	300	11	18.4	34700	1140	0.31	29300	7.5	51.9	1580	3.4	0.5	*0.001*
SCR-02	1	0.05	0.054	10400	11.6	27.2	25400	1160	0.7	13700	8.5	48.5	980	5.3	23	*0.001*
SCR-03	3.8	*0.005*	0.067	13600	12	23.5	20400	480	0.32	29100	6.8	43.6	610	7.8	30.1	*0.001*
SCR-04	3.5	*0.005*	0.088	19100	61.2	21.8	19000	1530	0.95	31000	80.6	12.1	5240	4	31.2	*0.001*
SCR-05	1.3	0.01	0.031	13900	13.8	24.6	15200	1680	0.34	19400	8.3	53.6	1120	4.2	36.4	*0.001*
SCR-06	2	0.03	0.026	20200	13.4	14.7	30000	682	0.63	36000	11.9	202	1260	5.2	57.5	*0.001*
SCR-07	1.4	0.04	0.048	10100	12.7	29.5	14200	1670	2.65	12000	13.2	75.9	690	5.5	29.2	*0.001*
SCR-08A	1.3	0.76	0.051	21400	9.9	28.5	1500	430	29.8	18100	4.6	19	840	11.5	54	0.021
SCR-08B	2.3	0.03	0.046	10500	11.2	17.5	61500	1060	0.95	16900	7.9	371	860	5.6	28.5	*0.001*
SCR-09	2.5	0.01	0.059	14100	15.7	20.2	13100	1080	1.14	28100	8	25.5	1830	5.1	34.2	*0.001*
SCR-10	6	*0.005*	0.026	32600	25.3	3.8	1300	290	1.67	30600	15.4	4.2	400	8.8	103	*0.001*
SCR-11	3.4	0.45	0.056	38700	19	12.5	9400	7670	1.22	5200	9	35	1460	279	91.5	*0.001*
Maximum	6	0.76	0.088	38700	61.2	29.5	61500	7670	29.8	36000	80.6	371	5240	279	103	0.021
Minimum	1	0.005	0.026	300	9.9	3.8	1300	290	0.31	5200	4.6	4.2	400	3.4	0.5	0.001
Mean	2.47	0.12	0.052	17075	18.1	20.2	20475	1573	3.39	22450	15.1	78.5	1406	28.8	43.3	0.0027
Standard Deviation	1.49	0.24	0.018	10401	14.2	7.42	16444	1977	8.34	9480	20.8	105	1278	78.8	29.1	0.0058
10 Percentile	1.12	0.005	0.026	10130	11	12.7	2290	435	0.32	12170	6.87	12.8	618	4.02	23.6	0.001
25 Percentile	1.3	0.005	0.042	10475	11.5	16.8	12175	632	0.56	16100	7.8	23.9	802	4.88	29	0.001
Median	2.15	0.02	0.052	14000	13	21	17100	1110	0.95	23750	8.4	46	1050	5.4	32.7	0.001
75 Percentile	3.42	0.042	0.061	20500	16.5	25.2	26550	1565	1.33	29625	12.2	59.2	1490	8.05	54.9	0.001
90 Percentile	3.77	0.41	0.067	31480	24.7	28.4	34230	1679	2.55	30960	15.2	189	1805	11.2	88.1	0.001
Interquartile Range (IQR) [1]	2.12	0.038	0.019	10025	5.02	8.45	14375	934	0.78	13525	4.42	35.3	688	3.18	25.8	0
Variance	2.21	0.057	0.00033	108189318	203	55.1	270412955	3909224	69.6	89868182	434	11130	1633990	6214	847	0.000033
Skewness	1.27	2.37	0.25	0.8	2.97	-0.85	1.4	3.11	3.43	-0.36	3.34	2.38	2.83	3.46	1.03	3.46
Coefficient of Variation (CoV) [2]	0.6	2.04	0.35	0.61	0.79	0.37	0.8	1.26	2.46	0.42	1.38	1.34	0.91	2.74	0.67	2.17
Count	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12

1.7 NOTE: if data is boxed, then data is 3 times the maximum crustal abundance.

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

NOTE: If data was reported as > detection limit the detection limit is shown in bold and was used in subsequent calculations.

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: Sampled by MDAG Oct '07.
Rare earth elements may not be totally soluble in MS61 method.

Sample	Sulphur	Antimony	Scandium	Selenium	Tin	Strontium	Tantalum	Tellurium	Thorium	Titanium	Thallium	Uranium	Vanadium	Tungsten	Yttrium	Zinc	Zirconium
Id.	S	Sb	Sc	Se	Sn	Sr	Ta	Te	Th	Ti	Tl	U	V	W	Y	Zn	Zr
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	100	0.05	1	1	0.2	0.2	0.05	0.05	0.2	50	0.02	0.1	1	0.1	0.1	2	0.5
Crustal Abundance: From	240	0.1	NA	0.05	0.5	1	0.8	NA	0.004	300	0.16	0.45	20	0.6	20	16	19
Crustal Abundance: To	2400	1.5	NA	0.6	6	2000	4.2	NA	17	13800	2.3	3.7	250	2.2	90	165	500
SCR-01	*50*	1.82	46.1	2	1.1	758	0.46	*0.025*	0.9	8020	*0.01*	0.4	278	0.3	26	78	30.6
SCR-02	2000	6.29	22.9	2	1	214	0.5	*0.025*	1.5	5320	0.12	0.6	154	2	13.2	60	36.9
SCR-03	100	0.23	20.6	2	1.7	56.4	0.39	*0.025*	3.1	2920	0.13	3.4	81	0.4	25	81	135
SCR-04	100	0.41	12.2	3	2.7	319	4.66	*0.025*	4.5	13100	0.08	1.6	128	0.6	27.7	102	150
SCR-05	600	0.3	11.5	2	0.8	1180	0.46	*0.025*	1.5	2650	0.12	1	103	0.3	15.2	52	44.2
SCR-06	1500	0.8	10.3	1	0.9	709	0.56	0.05	1.7	3410	0.33	0.8	93	1.8	9.5	51	70.7
SCR-07	200	3.84	9.1	2	1	102.5	0.73	0.1	1.5	2860	0.12	0.7	115	0.8	11.9	53	53.2
SCR-08A	4300	18.1	5.9	2	3	126.5	0.15	0.08	2.1	4700	0.66	3.2	181	1.9	6.2	31	40.9
SCR-08B	1200	0.99	20.1	2	1.2	295	0.48	*0.025*	1.4	4080	0.15	0.7	136	0.6	19	85	85.7
SCR-09	*50*	0.22	30	2	1.4	701	0.44	*0.025*	1.4	7270	0.17	0.8	287	0.2	25.4	75	91.6
SCR-10	*50*	1.07	5.4	2	2.6	197.5	1.1	*0.025*	8.4	2190	0.35	3.3	25	0.7	28.2	77	238
SCR-11	600	19.05	25.8	2	2	148.5	0.52	*0.025*	2.5	5220	1.22	1.1	179	1	22.8	1050	139
Maximum	4300	19	46.1	3	3	1180	4.66	0.1	8.4	13100	1.22	3.4	287	2	28.2	1050	238
Minimum	50	0.22	5.4	1	0.8	56.4	0.15	0.025	0.9	2190	0.01	0.4	25	0.2	6.2	31	30.6
Mean	896	4.43	18.3	2	1.62	401	0.87	0.038	2.54	5145	0.29	1.47	147	0.88	19.2	150	93
Standard Deviation	1255	6.85	11.9	0.43	0.78	352	1.21	0.026	2.09	3098	0.34	1.15	76.6	0.65	7.7	284	62.1
10 Percentile	50	0.24	6.22	2	0.91	105	0.4	0.025	1.4	2671	0.084	0.61	82.2	0.3	9.74	51.1	37.3
25 Percentile	87.5	0.38	10	2	1	143	0.46	0.025	1.48	2905	0.12	0.7	100	0.38	12.9	52.8	43.4
Median	400	1.03	16.2	2	1.3	254	0.49	0.025	1.6	4390	0.14	0.9	132	0.65	20.9	76	78.2
75 Percentile	1275	4.45	23.6	2	2.15	703	0.6	0.031	2.65	5808	0.34	2	180	1.2	25.5	82	136
90 Percentile	1950	16.9	29.6	2	2.69	753	1.06	0.077	4.36	7945	0.63	3.29	268	1.89	27.5	100	149
Interquartile Range (IQR) [1]	1188	4.07	13.6	0	1.15	560	0.15	0.0062	1.17	2902	0.22	1.3	79	0.82	12.7	29.2	92.6
Variance	1576117	46.9	141	0.18	0.6	123677	1.47	0.00066	4.36	9597355	0.12	1.31	5872	0.43	59.4	80773	3857
Skewness	2.09	1.79	1.15	0	0.77	1.14	3.26	1.9	2.37	1.71	2.23	1.1	0.66	0.91	-0.38	3.44	1.21
Coefficient of Variation (CoV) [2]	1.4	1.55	0.65	0.21	0.48	0.88	1.39	0.68	0.82	0.6	1.18	0.78	0.52	0.74	0.4	1.9	0.67
Count	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12

1.7 NOTE: if data is boxed, then data is 3 times the maximum crustal abundance.

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

NOTE: If data was reported as > detection limit the detection limit is shown in bold and was used in subsequent calculations.

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Whole Rock by XRF**
Comments: Sampled by MDAG Oct '07.

Sample Id.	Al_2O_3	BaO	CaO	Cr_2O_3	Fe_2O_3	K_2O	MgO	MnO	Na_2O	P_2O_5	SiO_2	SrO	TiO_2	LOI	Total
	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
Method	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06
MDL	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		
SCR-01	18.32	0.01	7.64	0.03	9.62	0.03	6.14	0.16	4.08	0.33	48.36	0.08	1.5	3.55	99.85
SCR-02	10.3	0.07	5.33	0.01	7.38	1.2	4.32	0.15	1.86	0.194	58.25	0.02	1.02	8.96	99.06
SCR-03	15.15	0.12	0.35	0.01	3.95	1.69	3.57	0.06	4.14	0.123	67.5	0.01	0.59	2.63	99.89
SCR-04	16.79	0.09	4.67	*0.005*	12.17	2.28	3.32	0.2	4.25	1.058	48.28	0.03	2.42	4.22	99.78
SCR-05	11.75	0.08	21.24	0.02	3.37	1.53	2.48	0.21	2.41	0.221	36.87	0.1	0.42	17.9	98.60
SCR-06	15.55	0.17	2.8	0.04	4.77	2.39	5.11	0.09	4.99	0.263	58.42	0.08	0.59	4.57	99.83
SCR-07	8.86	0.03	3.48	0.02	6.78	1.16	2.43	0.2	1.57	0.131	66.44	0.01	0.49	7.07	98.67
SCR-08A	12.37	0.12	0.84	*0.005*	4.56	2.63	0.31	0.05	2.62	0.174	72.18	0.02	0.8	3.13	99.81
SCR-08B	11.65	0.06	6.35	0.09	7.54	1.21	10.31	0.14	2.28	0.171	50.9	0.03	0.69	8.2	99.62
SCR-09	19.29	0.1	6.42	0.01	9.53	1.74	2.4	0.15	3.95	0.386	51.15	0.07	1.33	3.41	99.94
SCR-10	15.26	0.15	0.86	*0.005*	2.71	4.12	0.24	0.04	4.51	0.088	70.43	0.03	0.4	0.99	99.83
SCR-11	17.71	0.42	1.52	0.01	6.92	8.75	1.87	1.06	0.85	0.311	55.8	0.02	0.98	3.44	99.66
Maximum	19.3	0.42	21.2	0.09	12.2	8.75	10.3	1.06	4.99	1.06	72.2	0.1	2.42	17.9	
Minimum	8.86	0.01	0.35	0.005	2.71	0.03	0.24	0.04	0.85	0.088	36.9	0.01	0.4	0.99	
Mean	14.4	0.12	5.12	0.021	6.61	2.39	3.54	0.21	3.13	0.29	57	0.042	0.94	5.67	
Standard Deviation	3.37	0.11	5.64	0.024	2.87	2.24	2.75	0.27	1.35	0.26	10.6	0.032	0.58	4.52	
10 Percentile	10.4	0.033	0.84	0.005	3.43	1.16	0.47	0.051	1.6	0.12	48.3	0.011	0.43	2.68	
25 Percentile	11.7	0.068	1.36	0.0088	4.41	1.21	2.27	0.082	2.17	0.16	50.3	0.02	0.56	3.34	
Median	15.2	0.095	4.08	0.01	6.85	1.72	2.9	0.15	3.28	0.21	57	0.03	0.74	3.88	
75 Percentile	17	0.13	6.37	0.022	8.04	2.45	4.52	0.2	4.17	0.32	66.7	0.073	1.1	7.35	
90 Percentile	18.3	0.17	7.52	0.039	9.61	3.97	6.04	0.21	4.48	0.38	70.1	0.08	1.48	8.88	
Interquartile Range (IQR) [1]	5.3	0.06	5.01	0.014	3.63	1.24	2.25	0.12	1.99	0.15	16.4	0.053	0.53	4.01	
Variance	11.3	0.011	31.8	0.00059	8.22	5.01	7.59	0.075	1.81	0.067	113	0.001	0.34	20.4	
Skewness	-0.18	2.34	2.36	2.41	0.46	2.36	1.32	3.17	-0.25	2.75	-0.2	0.81	1.66	2.01	
Coefficient of Variation (CoV) [2]	0.23	0.89	1.1	1.14	0.43	0.93	0.78	1.31	0.43	0.9	0.19	0.76	0.62	0.8	
Count	12	12	12	12	12	12	12	12	12	12	12	12	12	12	

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: Sampled by MDAG Oct '07.

Sample Id.	Whole Rock Al * (ppm)	ICP Al (ppm)	Difference (%) [3]	Whole Rock Ba * (ppm)	ICP Ba (ppm)	Difference (%) [3]	Whole Rock Ca * (ppm)	ICP Ca (ppm)	Difference (%) [3]	Whole Rock Cr * (ppm)	ICP Cr (ppm)	Difference (%) [3]	Whole Rock Fe * (ppm)	ICP Fe (ppm)	Difference (%) [3]
SCR-01	96954	94000	-3.05	90	10	-88.84	54603	52000	-4.77	205	117	-43.00	67286	62200	-7.56
SCR-02	54510	55900	2.55	627	590	-5.90	38093	38600	1.33	68	62	-9.38	51618	51400	-0.42
SCR-03	80178	77100	-3.84	1075	1100	2.35	2501	2600	3.94	68	59	-13.77	27628	27600	-0.10
SCR-04	88857	89300	0.50	806	770	-4.48	33376	32800	-1.73	34	8	-76.62	85121	81600	-4.14
SCR-05	62184	68200	9.67	717	720	0.48	151801	157000	3.42	137	60	-56.15	23571	24200	2.67
SCR-06	82295	82800	0.61	1523	1460	-4.11	20011	20000	-0.06	274	208	-24.00	33363	32300	-3.19
SCR-07	46890	48900	4.29	269	290	7.93	24871	26200	5.34	137	97	-29.12	47422	49300	3.96
SCR-08A	65465	64200	-1.93	1075	1050	-2.31	6003	6200	3.27	34	9	-73.69	31894	32100	0.64
SCR-08B	61655	63500	2.99	537	500	-6.96	45383	44900	-1.06	616	436	-29.20	52738	51000	-3.29
SCR-09	102088	97100	-4.89	896	790	-11.80	45883	44600	-2.80	68	38	-44.46	66656	62000	-6.99
SCR-10	80760	75900	-6.02	1343	1320	-1.75	6146	6300	2.50	34	21	-38.62	18955	18600	-1.87
SCR-11	93726	87900	-6.22	3762	3590	-4.57	10863	10900	0.34	68	56	-18.15	48401	45100	-6.82
Maximum			9.67			7.93			5.34			-9.38			3.96
Minimum			-6.22			-88.8			-4.77			-76.6			-7.56
Mean			-0.44			-9.99			0.81			-38			-2.26
Standard Deviation			4.79			25.3			3.04			22			3.77
10 Percentile			-5.9			-11.3			-2.69			-71.9			-6.97
25 Percentile			-4.1			-6.16			-1.23			-47.4			-4.81
Median			-0.72			-4.29			0.83			-33.9			-2.53
75 Percentile			2.66			-1.19			3.31			-22.5			0.086
90 Percentile			4.16			2.16			3.89			-14.2			2.47
Interquartile Range (IQR) [1]			6.76			4.97			4.54			24.8			4.89
Variance			22.9			641			9.22			483			14.2
Skewness			0.69			-3.22			-0.32			-0.61			0.088
Coefficient of Variation (CoV) [2]			-10.8			-2.53			3.74			-0.58			-1.67
Count			12			12			12			12			12

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile
[2] Coefficient of Variation (CoV) = standard deviation divided by mean
[3] Difference (%) = (ICP - Whole Rock) * 100 / Whole Rock
* Element calculated from Whole Rock XRF analysis
Al (Whole Rock) = (Al_2O_3*2*10000*26.98)/(2*26.98+3*16)
Ba (Whole Rock) = (BaO*10000*137.34)/(137.34+16)
Ca (Whole Rock) = (CaO*10000*40.08)/(40.08+16)
Cr (Whole Rock) = (Cr_2O_3*2*10000*52.00)/(2*52.00+3*16)
Fe (Whole Rock) = (Fe_2O_3*2*10000*55.85)/(2*55.85+3*16)

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: Sampled by MDAG Oct '07.

Sample Id.	Whole Rock K * (ppm)	ICP K (ppm)	Difference (%) [3]	Whole Rock Mg * (ppm)	ICP Mg (ppm)	Difference (%) [3]	Whole Rock Mn * (ppm)	ICP Mn (ppm)	Difference (%) [3]	Whole Rock Na * (ppm)	ICP Na (ppm)	Difference (%) [3]	Whole Rock P * (ppm)	ICP P (ppm)	Difference (%) [3]
SCR-01	249	300	20.47	37029	34700	-6.29	1239	1140	-8.00	30268	29300	-3.20	1440	1580	9.72
SCR-02	9961	10400	4.40	26053	25400	-2.51	1162	1160	-0.15	13798	13700	-0.71	847	980	15.76
SCR-03	14029	13600	-3.06	21530	20400	-5.25	465	480	3.30	30713	29100	-5.25	537	610	13.65
SCR-04	18927	19100	0.92	20022	19000	-5.10	1549	1530	-1.22	31529	31000	-1.68	4617	5240	13.50
SCR-05	12701	13900	9.44	14956	15200	1.63	1626	1680	3.30	17879	19400	8.51	964	1120	16.13
SCR-06	19840	20200	1.82	30817	30000	-2.65	697	682	-2.15	37018	36000	-2.75	1148	1260	9.79
SCR-07	9629	10100	4.89	14655	14200	-3.10	1549	1670	7.82	11647	12000	3.03	572	690	20.70
SCR-08A	21832	21400	-1.98	1870	1500	-19.77	387	430	11.05	19437	18100	-6.88	759	840	10.63
SCR-08B	10044	10500	4.54	62177	61500	-1.09	1084	1060	-2.24	16914	16900	-0.08	746	860	15.25
SCR-09	14444	14100	-2.38	14474	13100	-9.49	1162	1080	-7.03	29303	28100	-4.11	1684	1830	8.64
SCR-10	34201	32600	-4.68	1447	1300	-10.18	310	290	-6.39	33458	30600	-8.54	384	400	4.16
SCR-11	72635	38700	-46.72	11278	9400	-16.65	8209	7670	-6.57	6306	5200	-17.54	1357	1460	7.58
Maximum			20.5			1.63			11			8.51			20.7
Minimum			-46.7			-19.8			-8			-17.5			4.16
Mean			-1.03			-6.7			-0.69			-3.27			12.1
Standard Deviation			15.9			6.34			6.09			6.37			4.54
10 Percentile			-4.52			-16			-6.99			-8.37			7.68
25 Percentile			-2.55			-9.66			-6.43			-5.66			9.45
Median			1.37			-5.18			-1.69			-2.97			12.1
75 Percentile			4.62			-2.62			3.3			-0.56			15.4
90 Percentile			8.99			-1.23			7.37			2.72			16.1
Interquartile Range (IQR) [1]			7.17			7.05			9.73			5.1			5.93
Variance			253			40.2			37.1			40.6			20.6
Skewness			-2.27			-1			0.64			-0.49			0.13
Coefficient of Variation (CoV) [2]			-15.5			-0.95			-8.82			-1.95			0.37
Count			12			12			12			12			12

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

[3] Difference (%) = (ICP - Whole Rock) * 100 / Whole Rock

* Element calculated from Whole Rock XRF analysis

K (Whole Rock) = (K_2O*2*10000*39.09)/(39.09*2+16)
Mg (Whole Rock) = (MgO*10000*24.31)/(24.31+16)
Mn (Whole Rock) = (MnO*10000*54.94)/(54.94+16)
Na (Whole Rock) = (Na_2O*2*10000*22.99)/(22.99*2+16)
P (Whole Rock) = (P_2O5*2*10000*30.97)/(2*30.97+5*16)

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: Sampled by MDAG Oct '07.

Sample Id.	Whole Rock Si * (ppm)	ICP Si (ppm)	Difference (%) [3]	Whole Rock Sr * (ppm)	ICP Sr (ppm)	Difference (%) [3]	Leco S (Total)** (ppm)	ICP S (ppm)	Difference (%) [3]	Whole Rock Ti * (ppm)	ICP Ti (ppm)	Difference (%) [3]
SCR-01	226066			676	758	12.05	100	50	-50.00	8992	8020	-10.81
SCR-02	272299			169	214	26.54	1600	2000	25.00	6115	5320	-13.00
SCR-03	315539			85	56	-33.30	100	100	0.00	3537	2920	-17.45
SCR-04	225692			254	319	25.75	100	100	0.00	14508	13100	-9.70
SCR-05	172355			846	1180	39.55	600	600	0.00	2518	2650	5.25
SCR-06	273093			676	709	4.81	1600	1500	-6.25	3537	3410	-3.59
SCR-07	310584			85	103	21.22	200	200	0.00	2938	2860	-2.64
SCR-08A	337417			169	127	-25.20	3900	4300	10.26	4796	4700	-2.00
SCR-08B	237940			254	295	16.29	800	1200	50.00	4137	4080	-1.37
SCR-09	239109			592	701	18.43	100	50	-50.00	7973	7270	-8.82
SCR-10	329236			254	198	-22.15	50	50	0.00	2398	2190	-8.67
SCR-11	260846			169	149	-12.19	600	600	0.00	5875	5220	-11.15
Maximum			NA			39.5			50			5.25
Minimum			NA			-33.3			-50			-17.4
Mean			NA			5.98			-1.75			-7
Standard Deviation			NA			23.6			27.4			6.23
10 Percentile			NA			-24.9			-45.6			-12.8
25 Percentile			NA			-14.7			-1.56			-10.9
Median			NA			14.2			0			-8.75
75 Percentile			NA			22.4			2.56			-2.48
90 Percentile			NA			26.5			23.5			-1.43
Interquartile Range (IQR) [1]			NA			37			4.13			8.42
Variance			NA			555			748			38.9
Skewness			NA			-0.49			-0.35			0.34
Coefficient of Variation (CoV) [2]			NA			3.94			-15.6			-0.89
Count			0			12			12			12

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

[3] Difference (%) = (ICP - Whole Rock) * 100 / Whole Rock

* Element calculated from Whole Rock XRF analysis

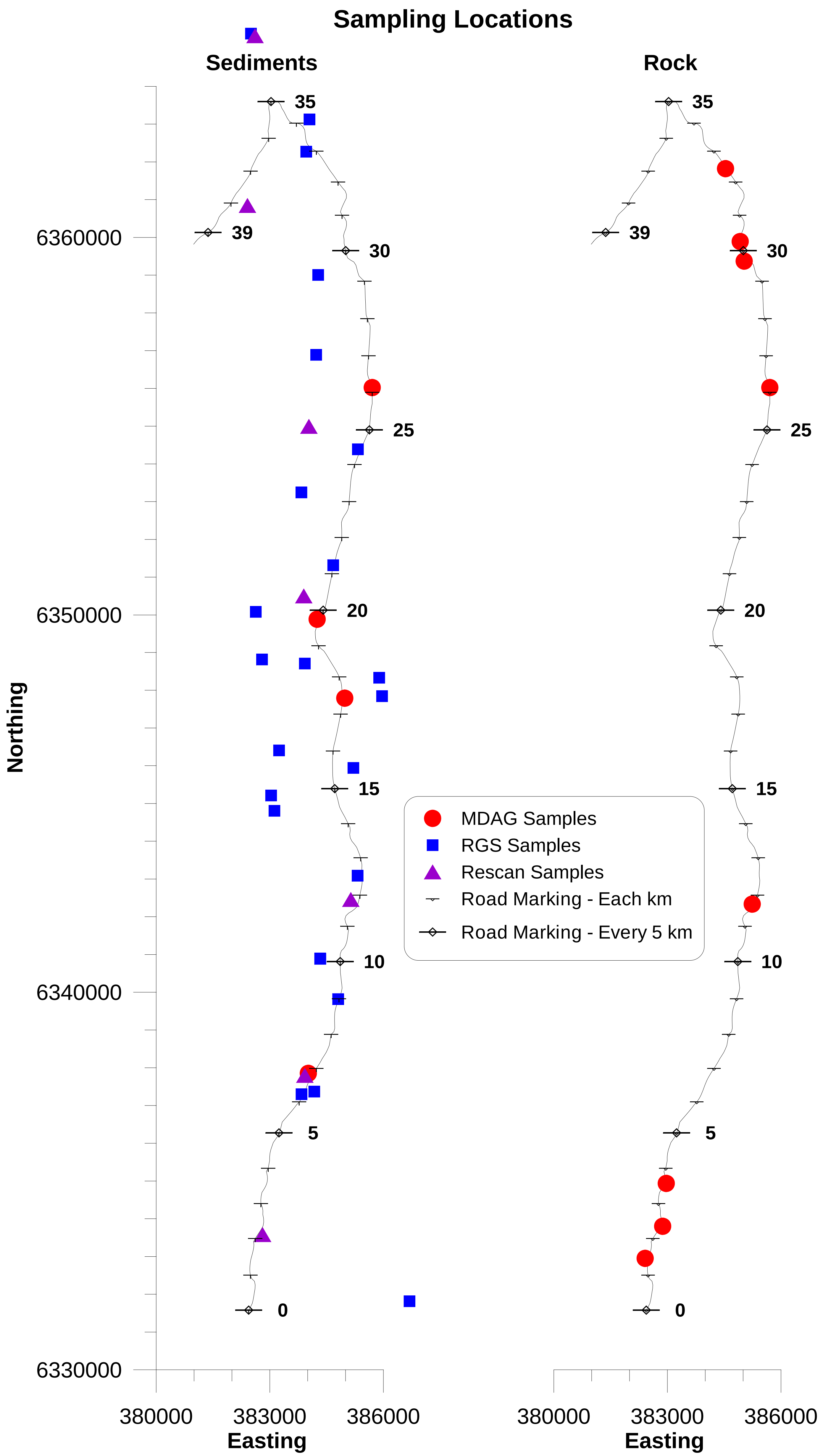
Si (Whole Rock) = (SiO_2*10000*28.09)/(28.09+2*16)

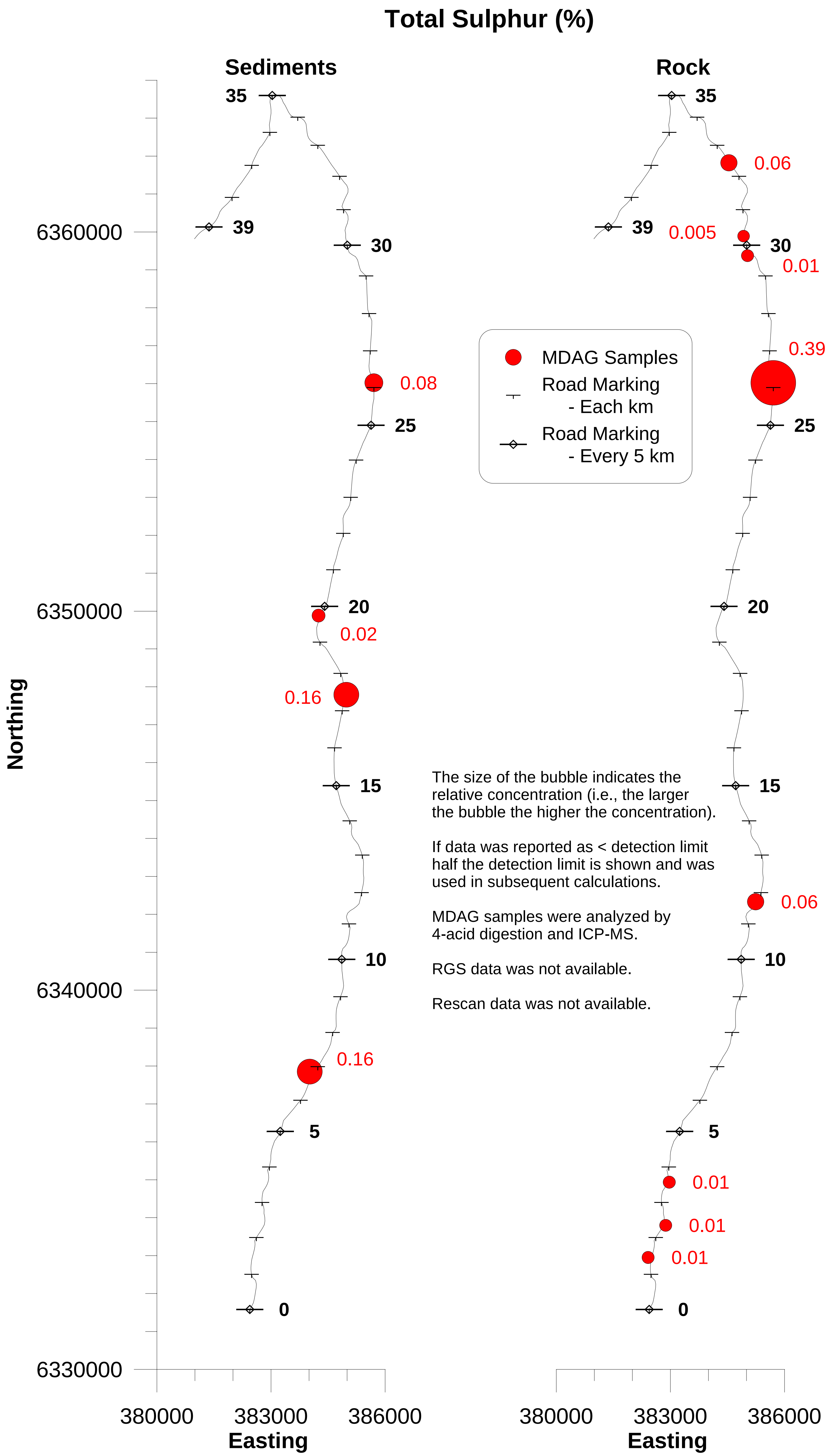
Sr (Whole Rock) = (SrO*10000*87.62)/(87.62+16)

Ti (Whole Rock) = (TiO_2*10000*47.9)/(47.9+2*16)

**S (Total) = S (Leco %) * 10000

APPENDIX D. Maps of Solid-Phase Element Levels Near the Proposed Road Alignment (from Appendix C of this study, from Rescan, 2007, and from provincial RGS Regional Geochemical Surveys)


Sampling Locations
Sediments
Rock
Northing
6360000
6350000
6340000
6330000
380000
383000
386000
Easting
380000
383000
386000
Easting
35
39
30
25
20
15
10
5
0
35
39
30
25
20
15
10
5
0
MDAG Samples
RGS Samples
Rescan Samples
Road Marking - Each km
Road Marking - Every 5 km



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

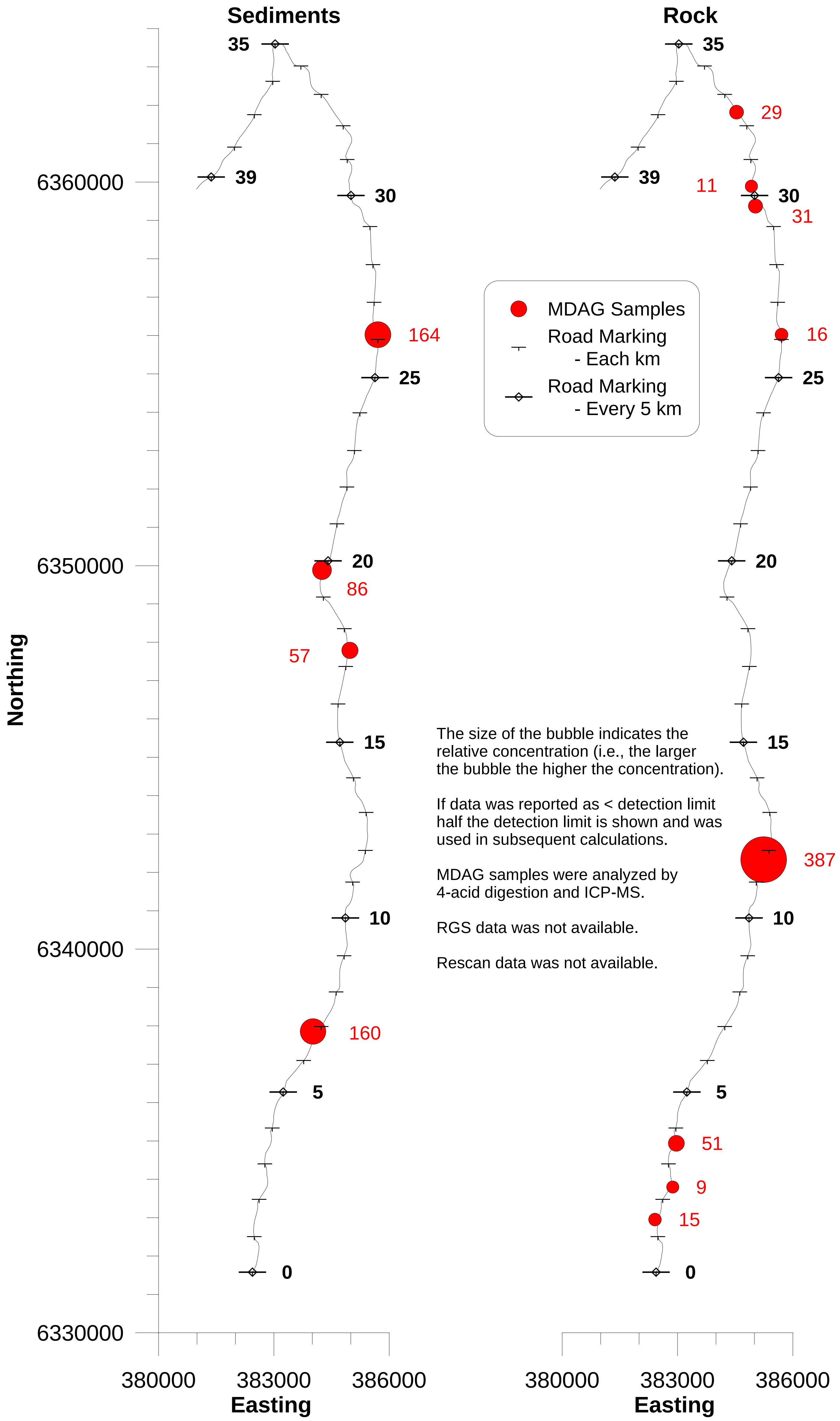
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

Neutralization Potential (kg $CaCO_3$ equivalent/tonne)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

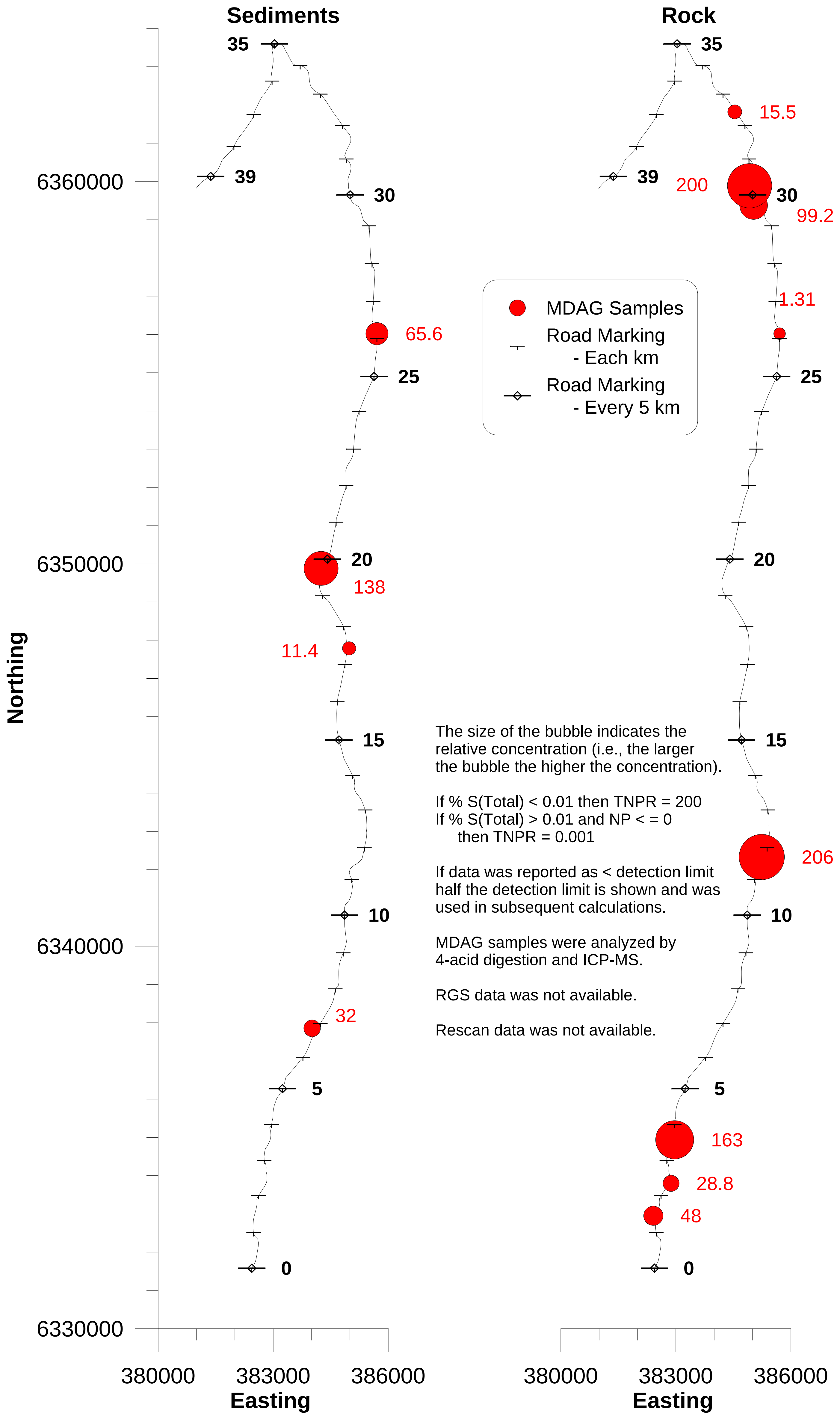
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

TNPR



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If % S(Total) < 0.01 then TNPR = 200
If % S(Total) > 0.01 and NP < = 0
then TNPR = 0.001

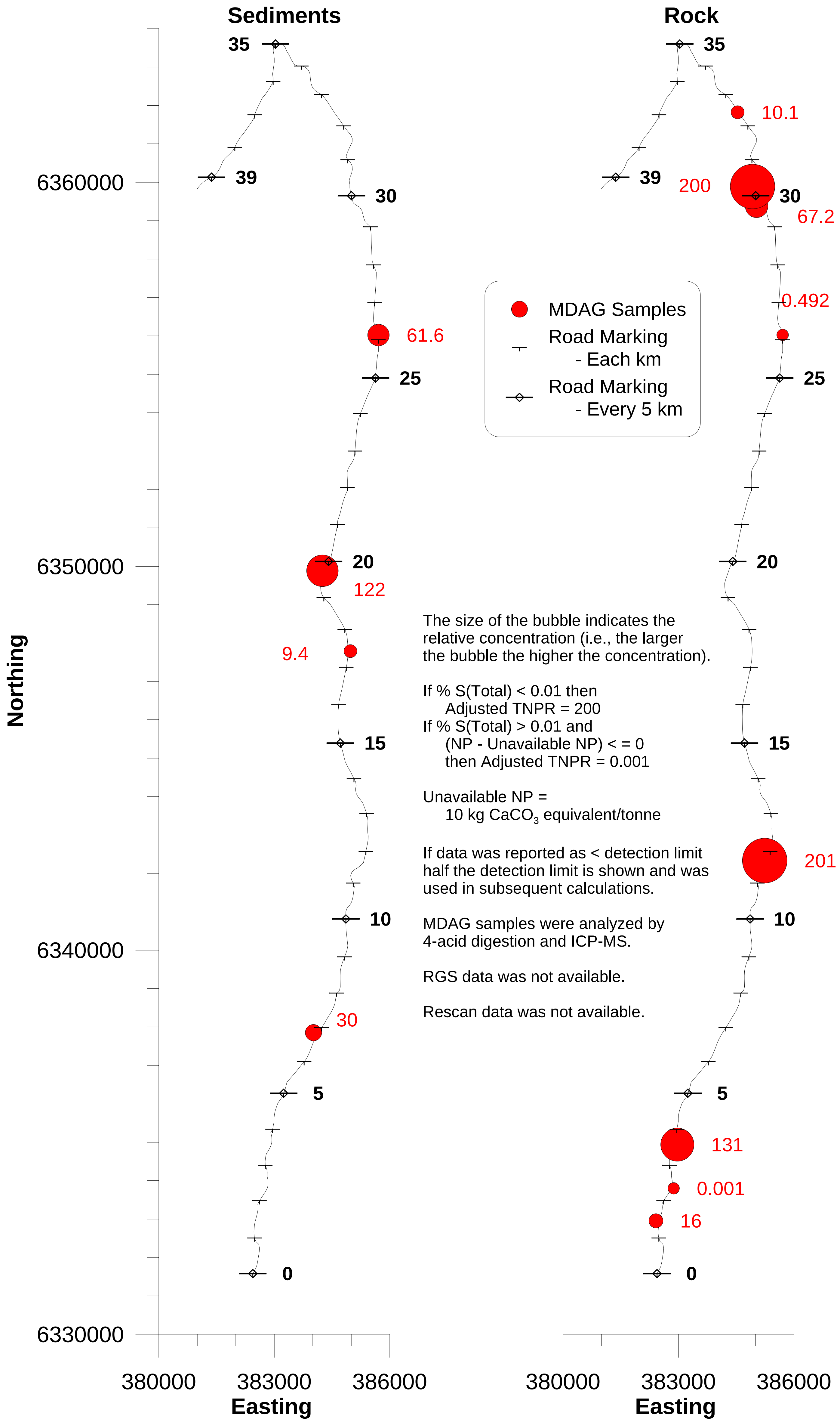
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

Adjusted TNPR



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If % S(Total) < 0.01 then
Adjusted TNPR = 200
If % S(Total) > 0.01 and
(NP - Unavailable NP) < = 0
then Adjusted TNPR = 0.001

Unavailable NP =
10 kg $CaCO_3$ equivalent/tonne

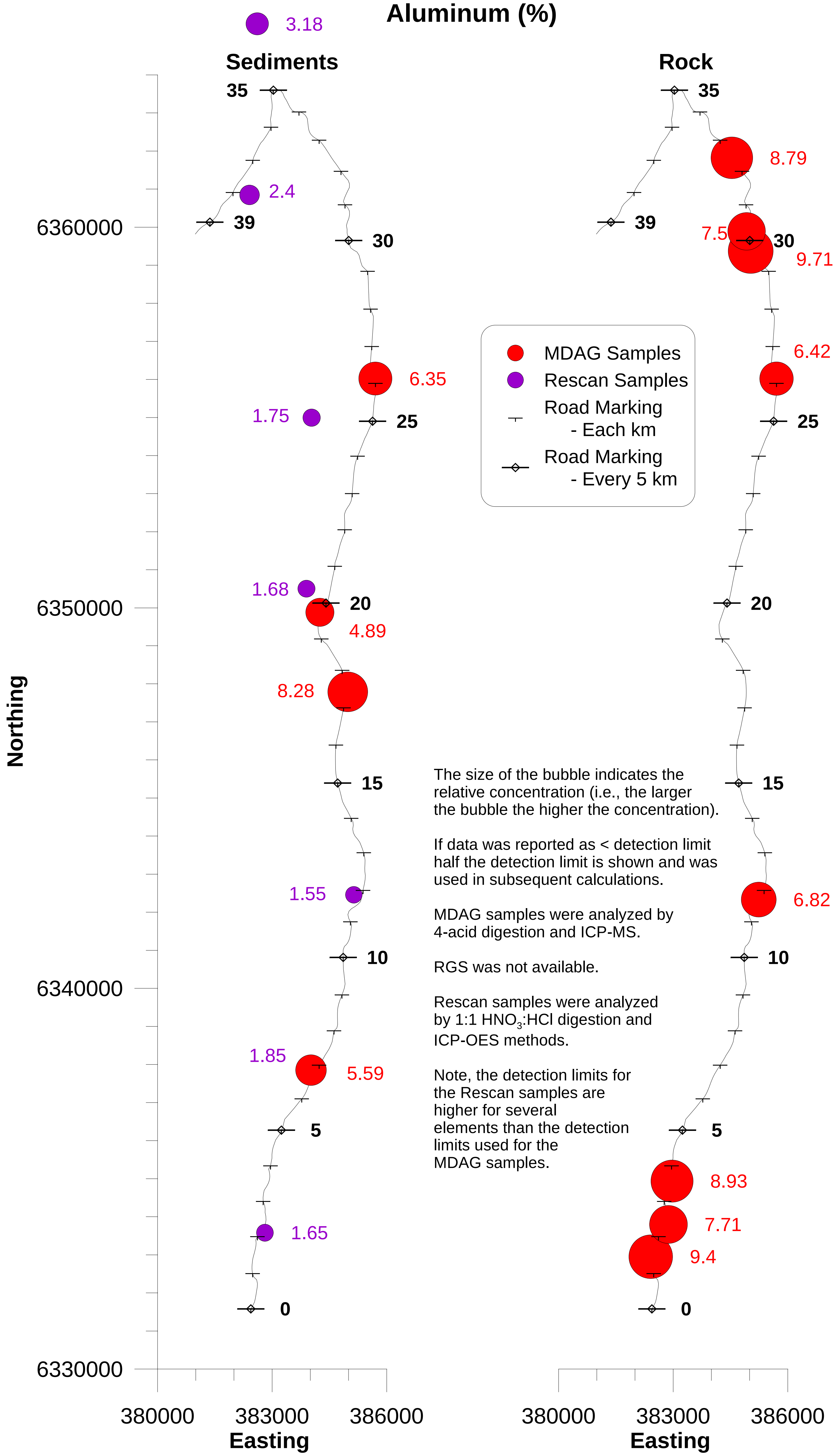
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

Aluminum (%)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

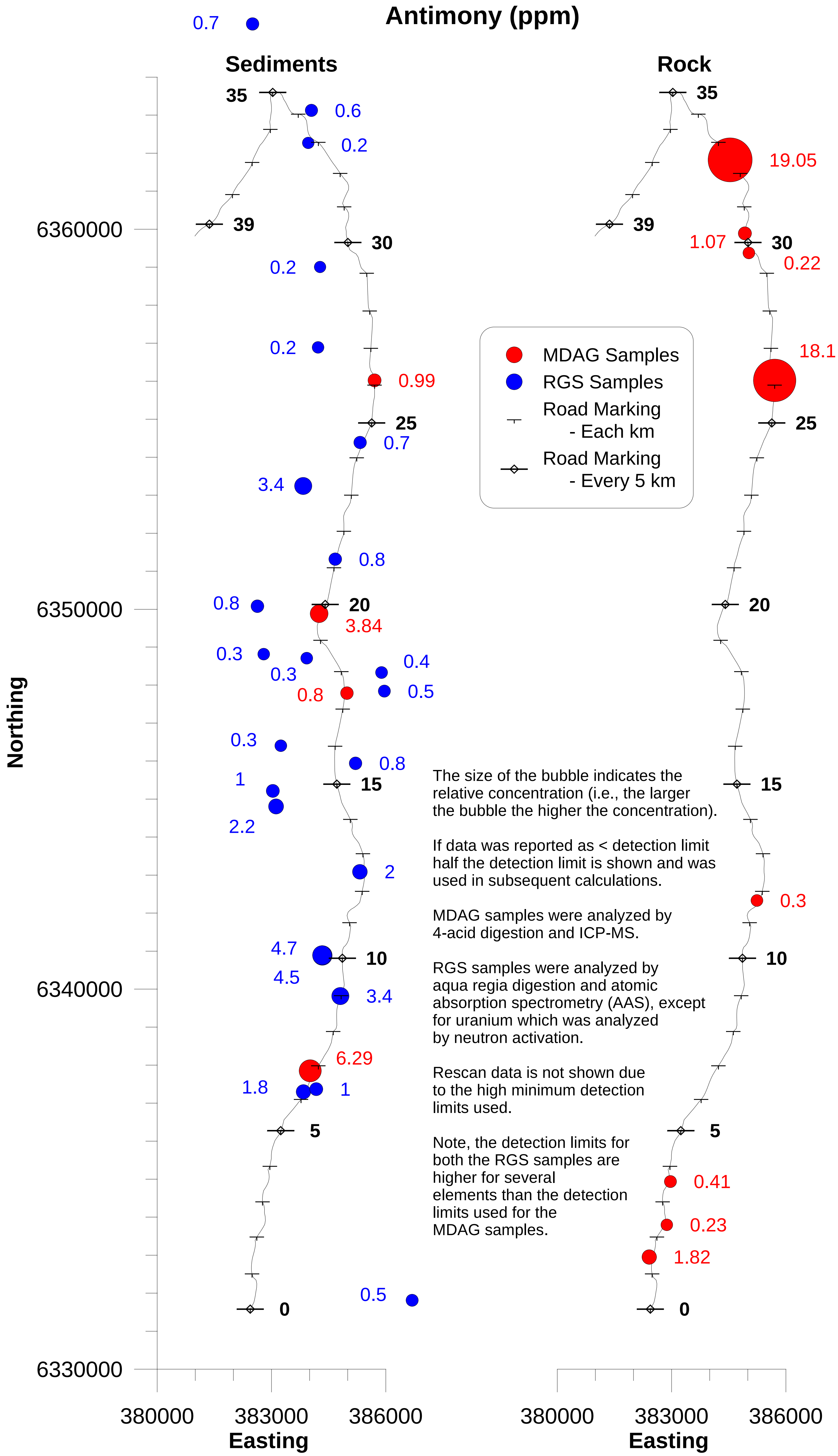
MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS was not available.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for the Rescan samples are higher for several elements than the detection limits used for the MDAG samples.

Antimony (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

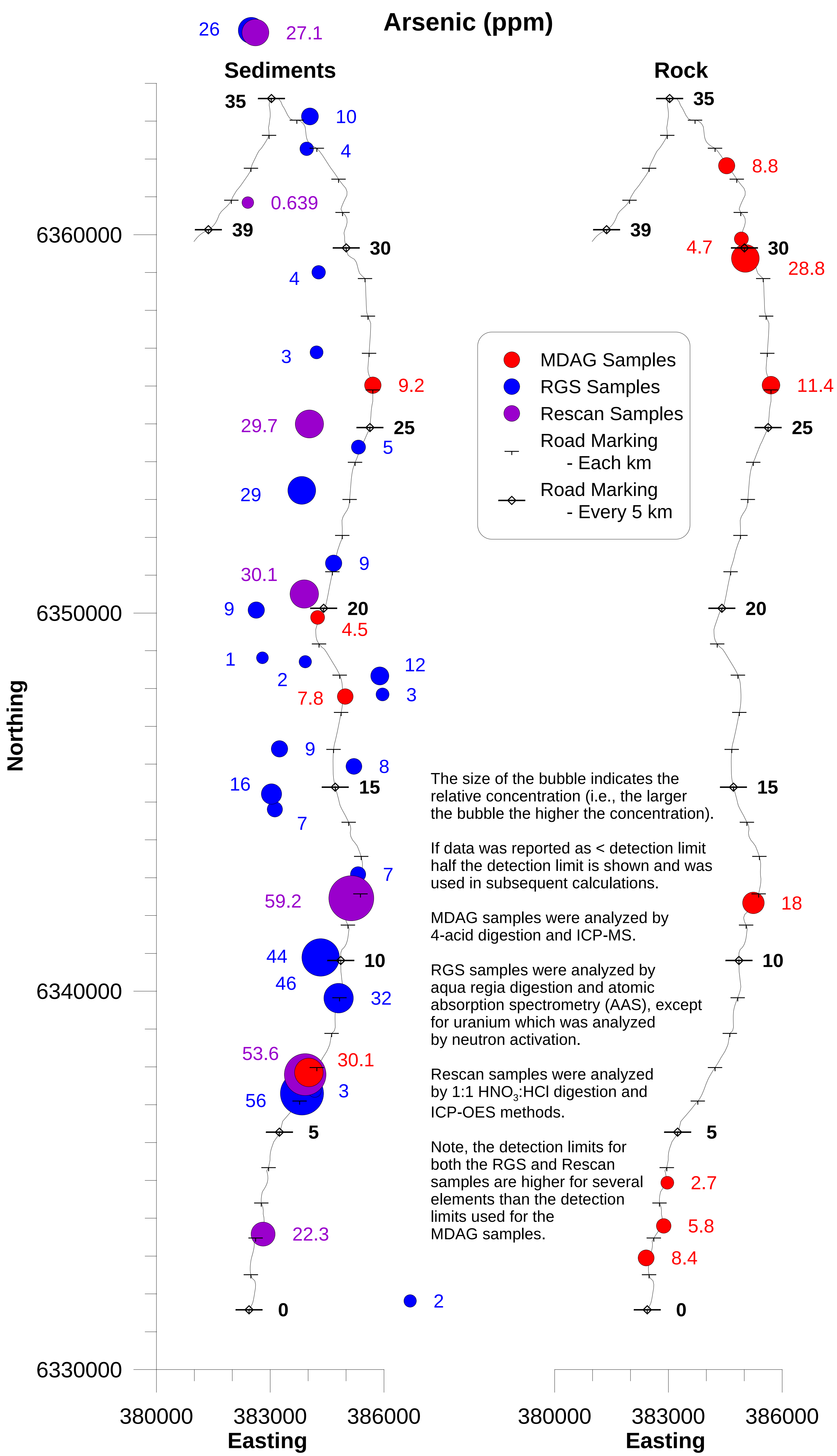
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan data is not shown due to the high minimum detection limits used.

Note, the detection limits for both the RGS samples are higher for several elements than the detection limits used for the MDAG samples.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

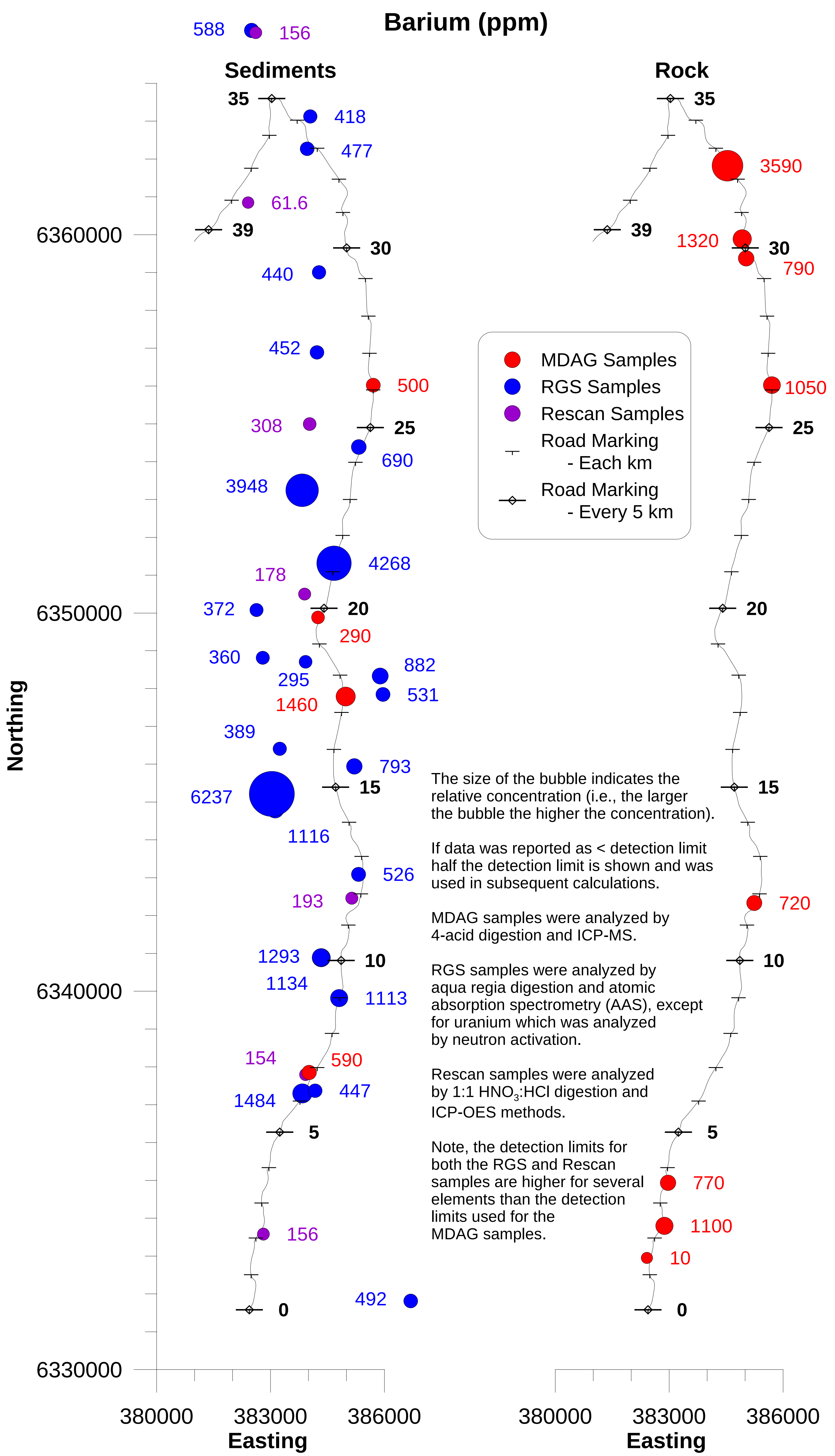
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for both the RGS and Rescan samples are higher for several elements than the detection limits used for the MDAG samples.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

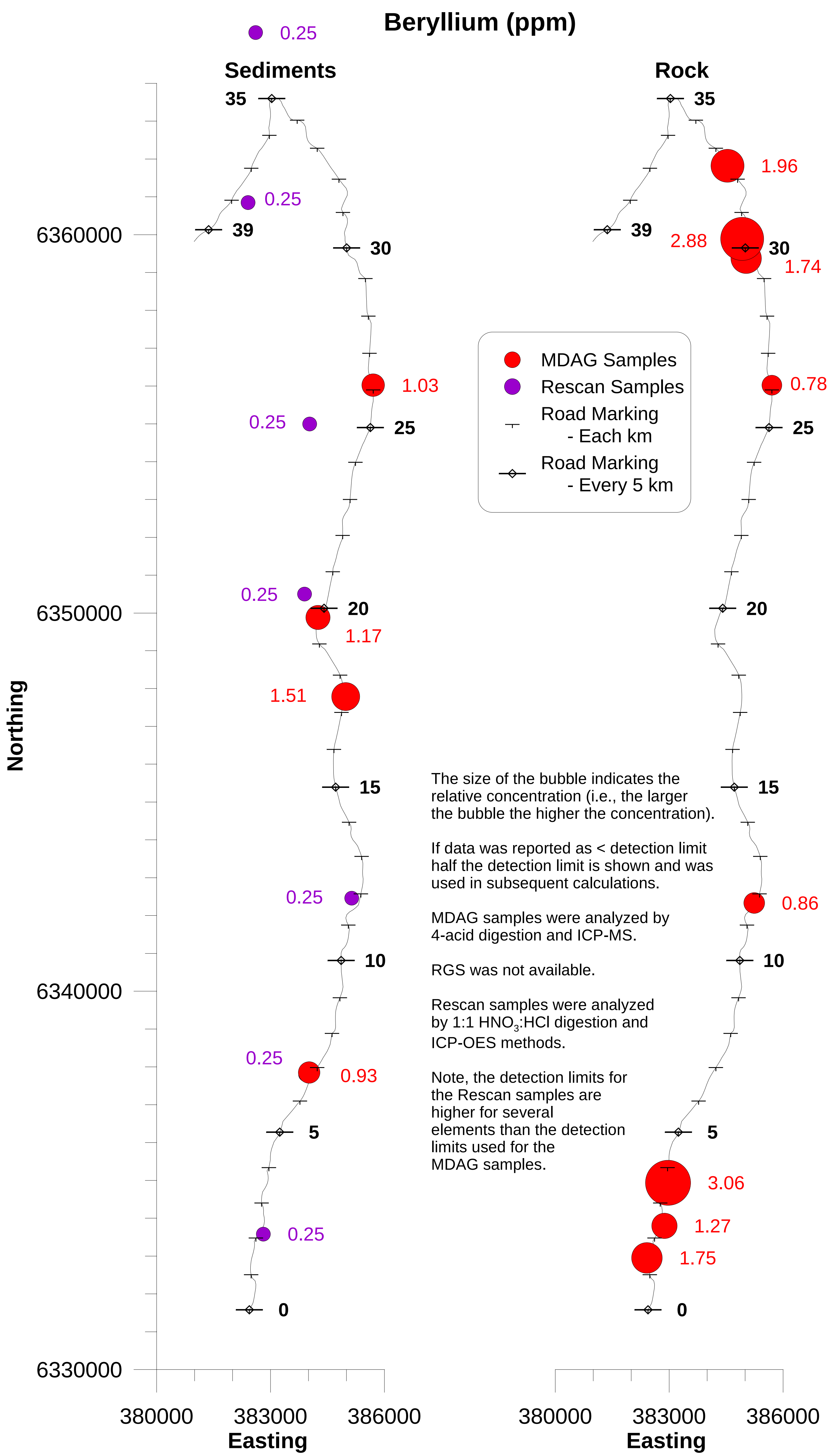
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for both the RGS and Rescan samples are higher for several elements than the detection limits used for the MDAG samples.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

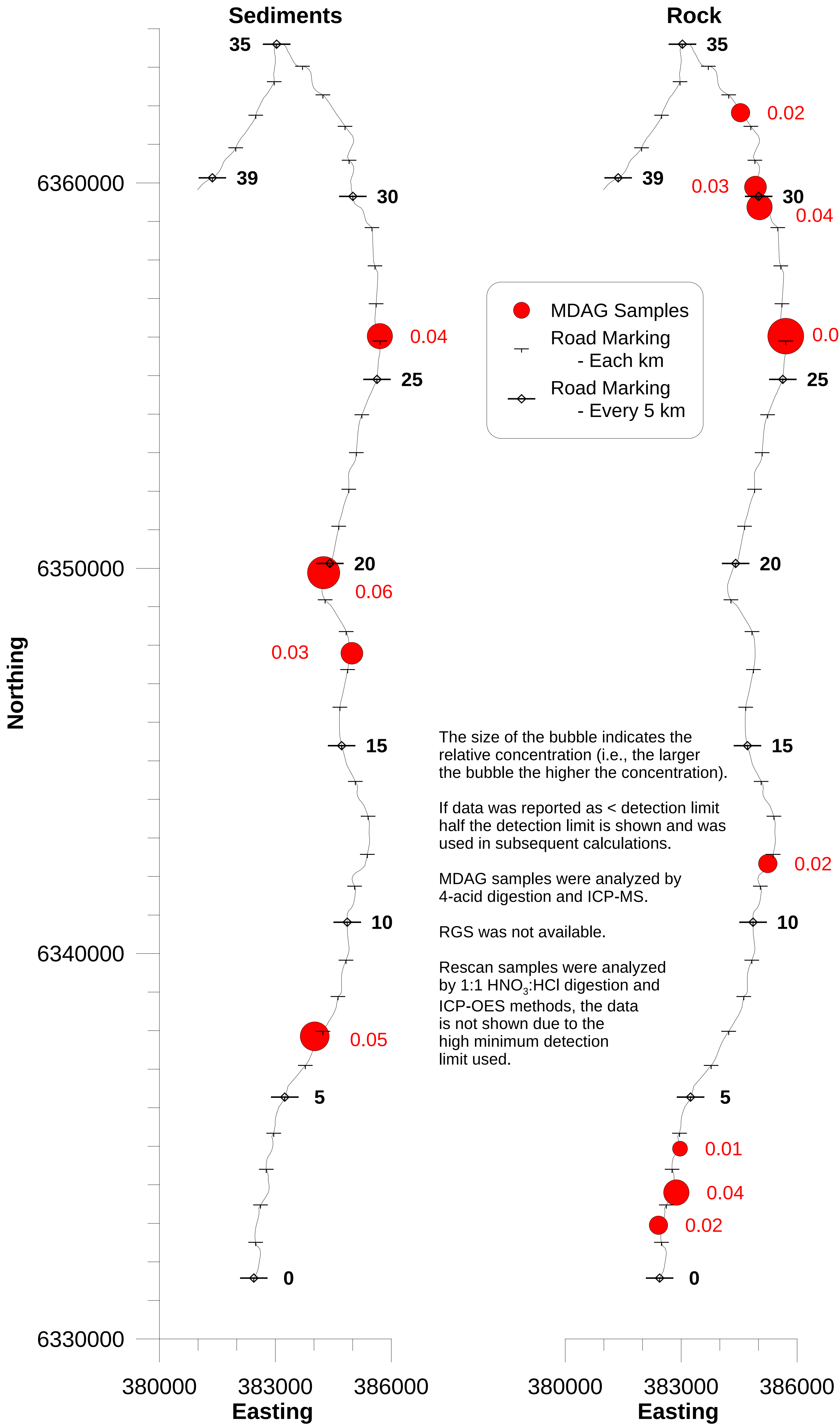
MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS was not available.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for the Rescan samples are higher for several elements than the detection limits used for the MDAG samples.

Bismuth (ppm)



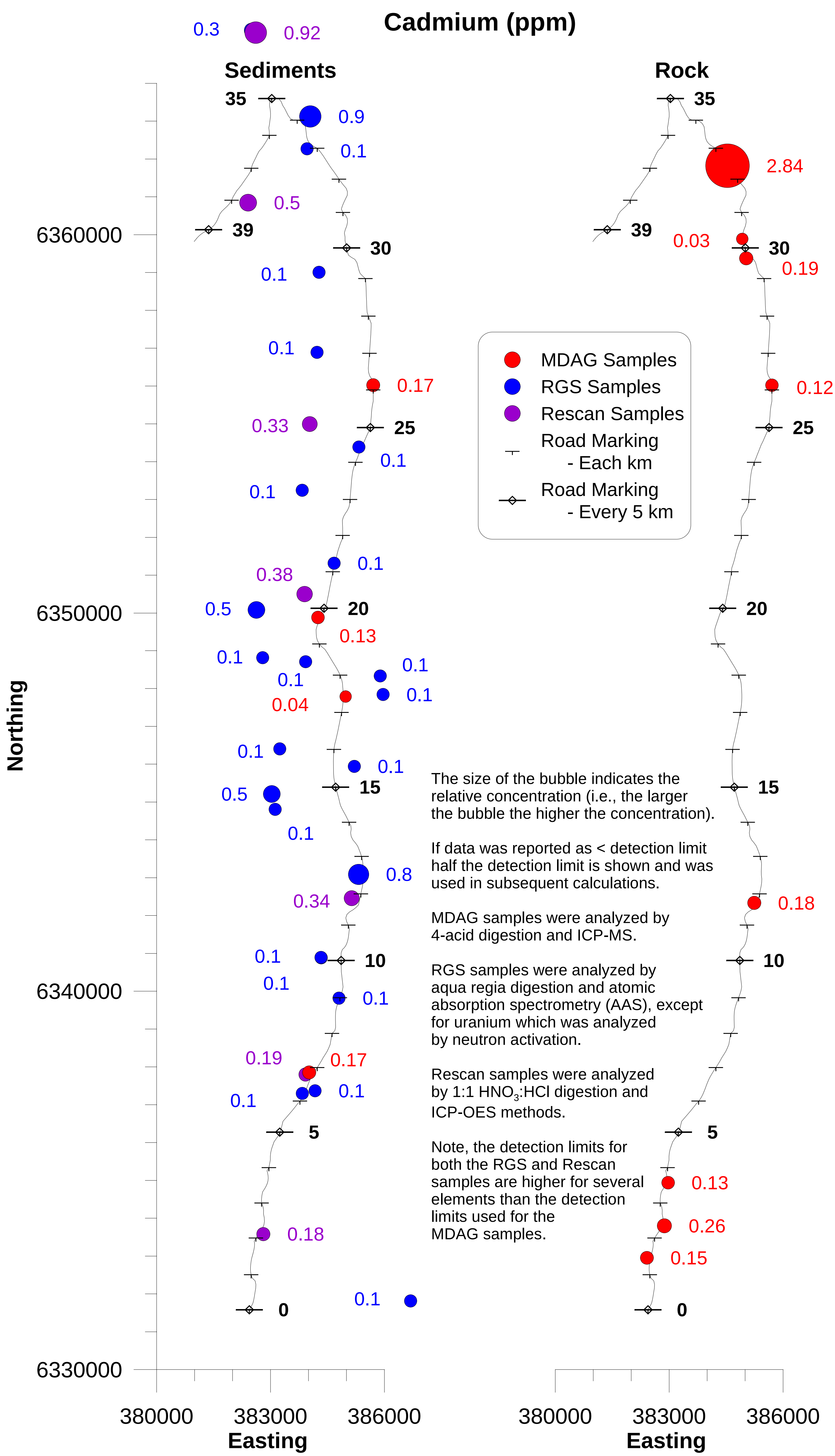
The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS was not available.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods, the data is not shown due to the high minimum detection limit used.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

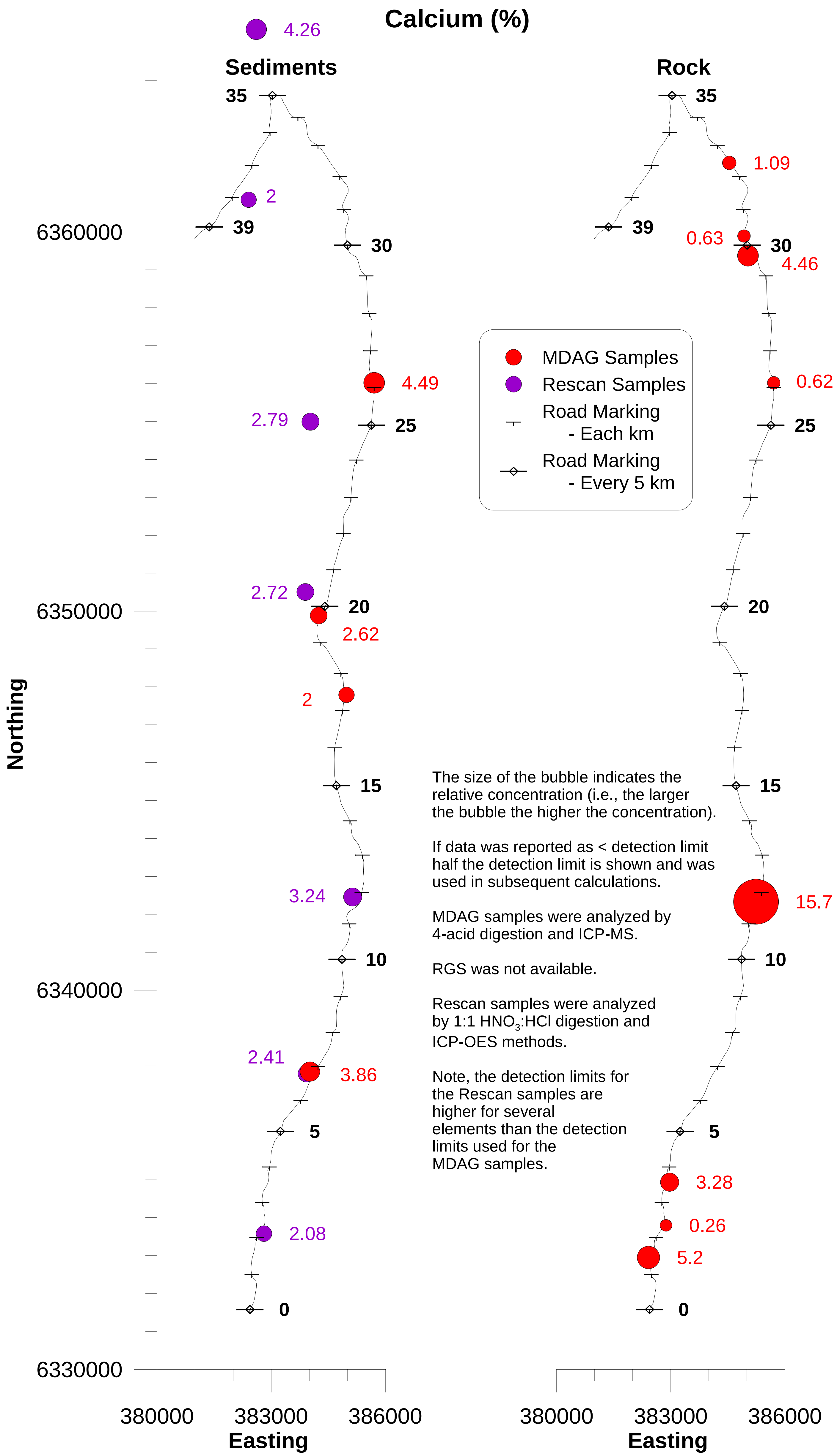
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for both the RGS and Rescan samples are higher for several elements than the detection limits used for the MDAG samples.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

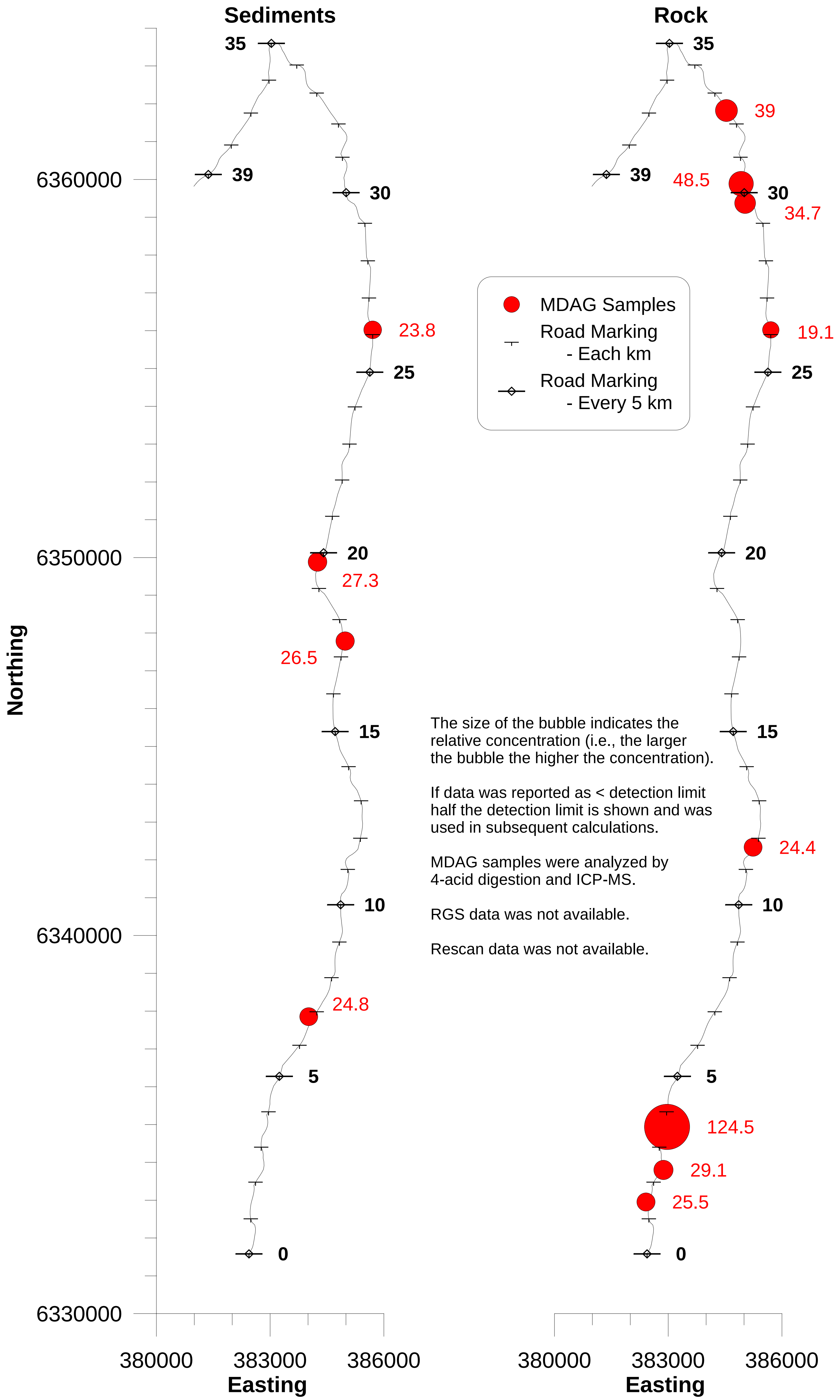
MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS was not available.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for the Rescan samples are higher for several elements than the detection limits used for the MDAG samples.

Cerium (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

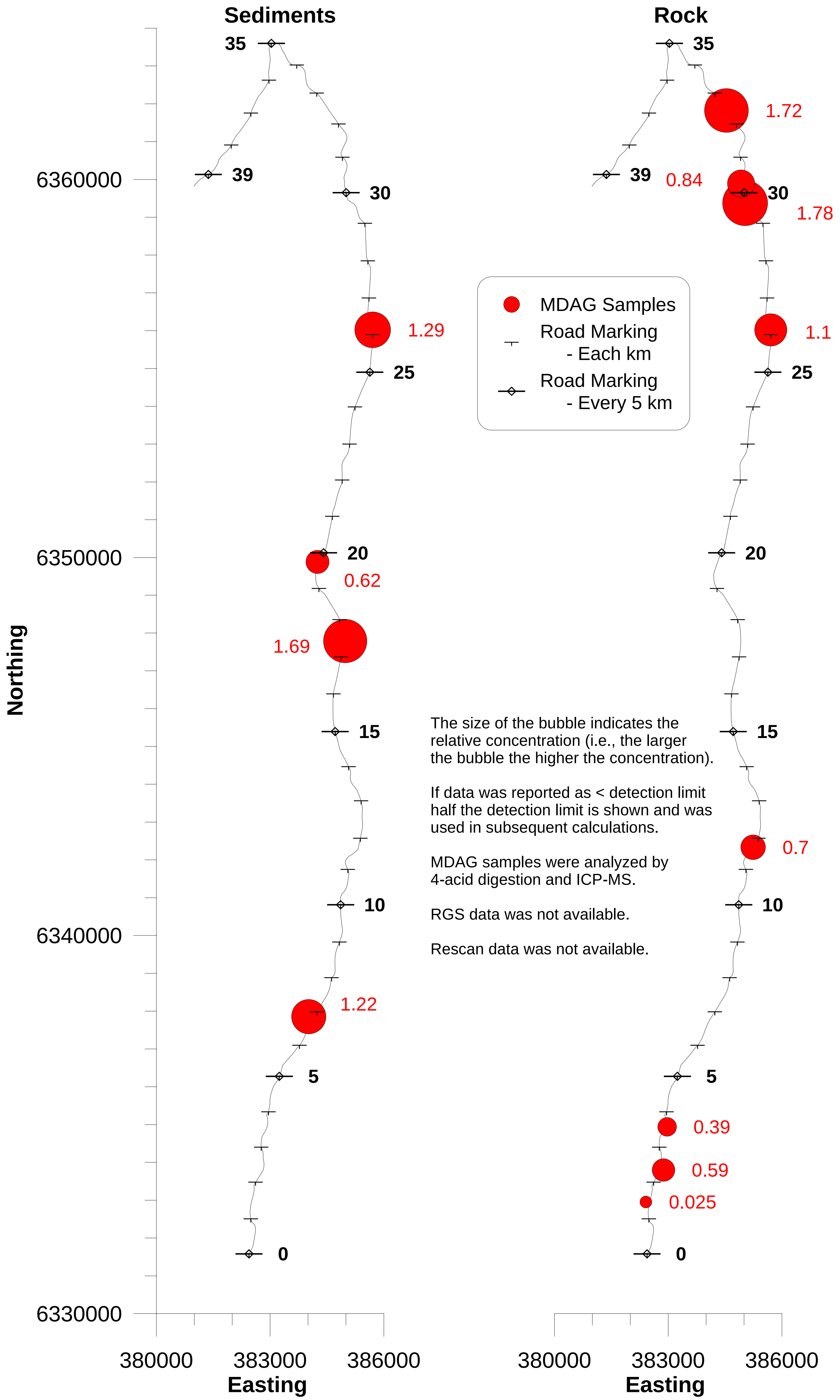
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

Cesium (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

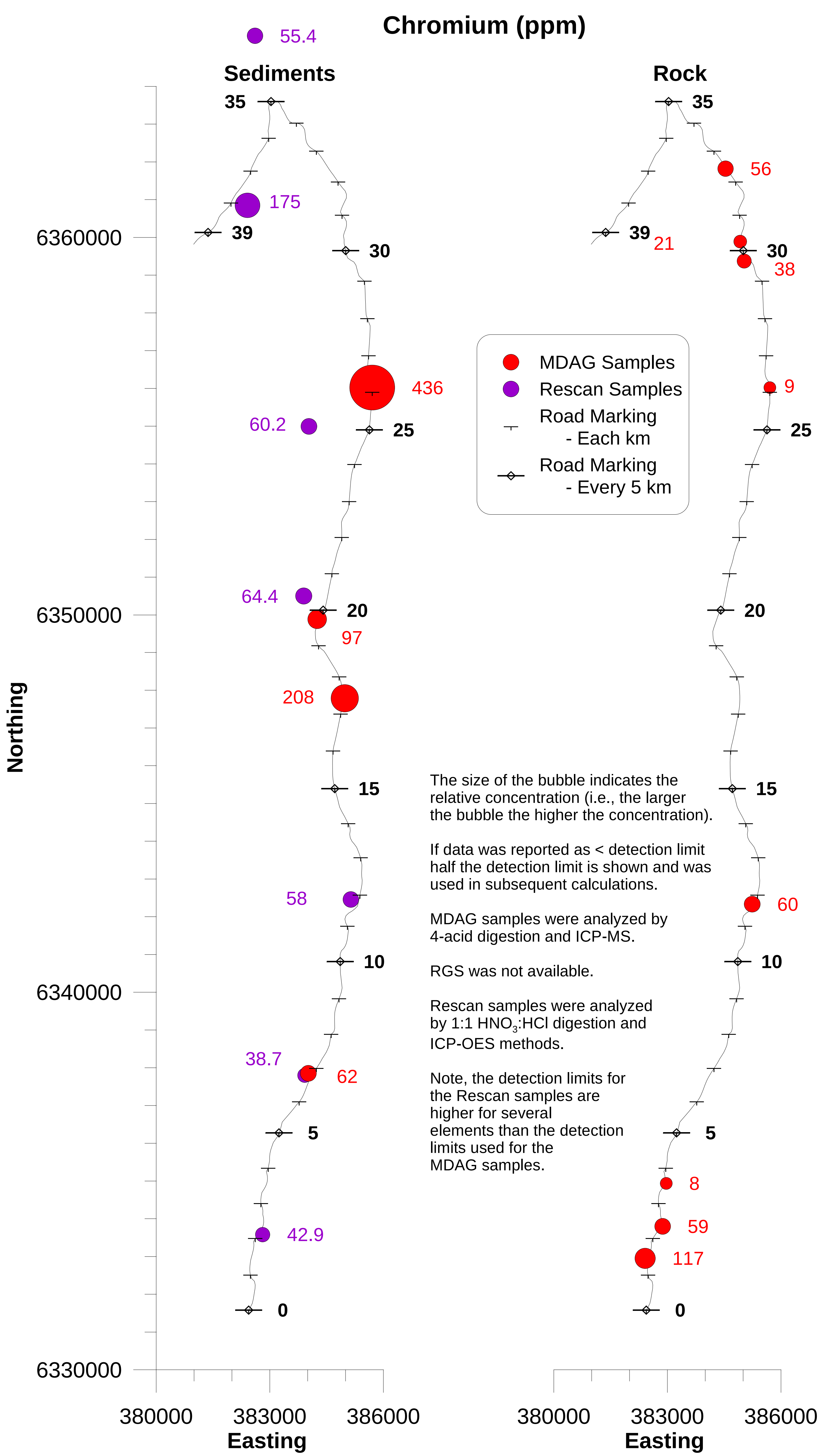
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

Chromium (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

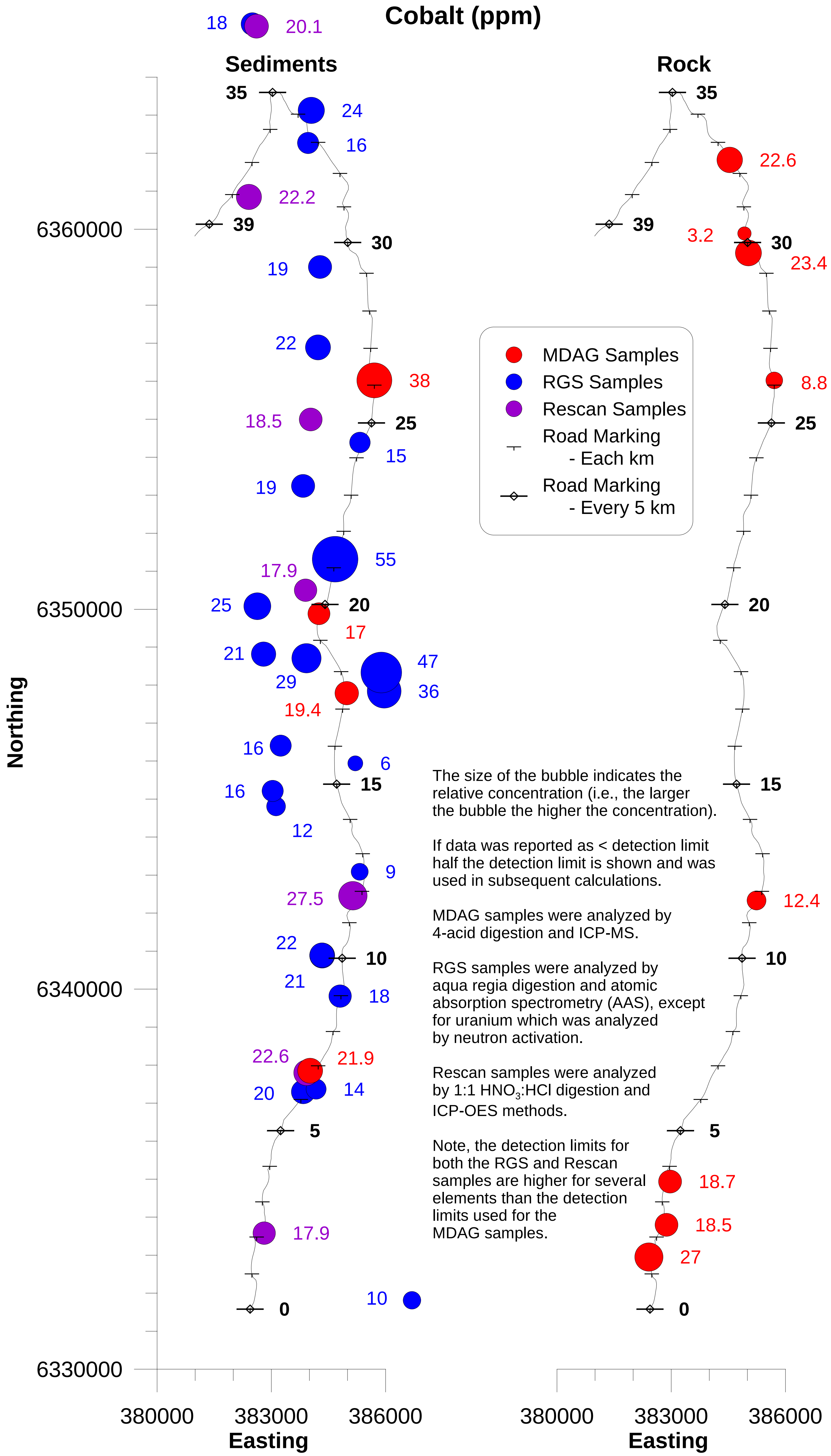
MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS was not available.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for the Rescan samples are higher for several elements than the detection limits used for the MDAG samples.

Cobalt (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

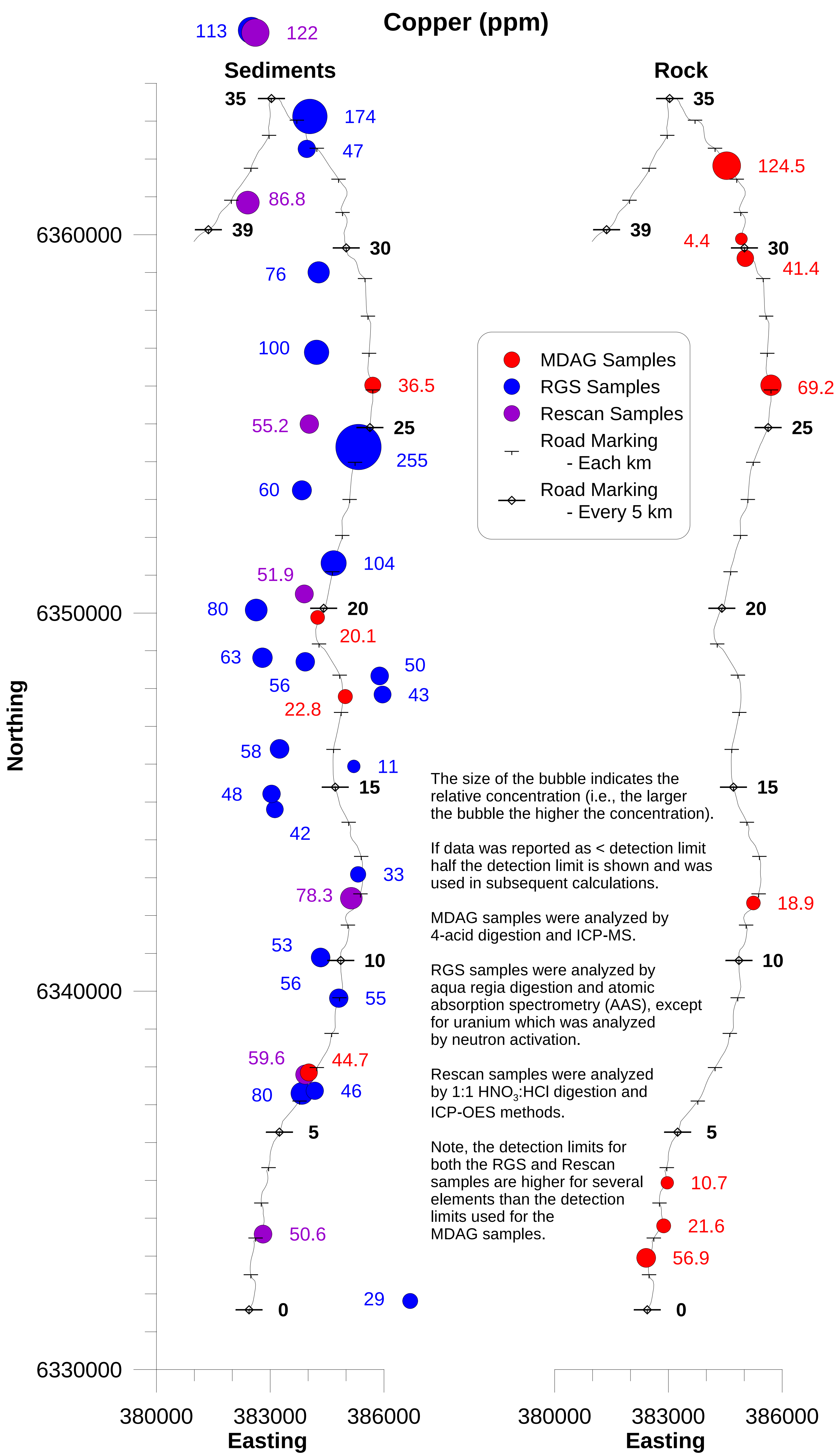
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for both the RGS and Rescan samples are higher for several elements than the detection limits used for the MDAG samples.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

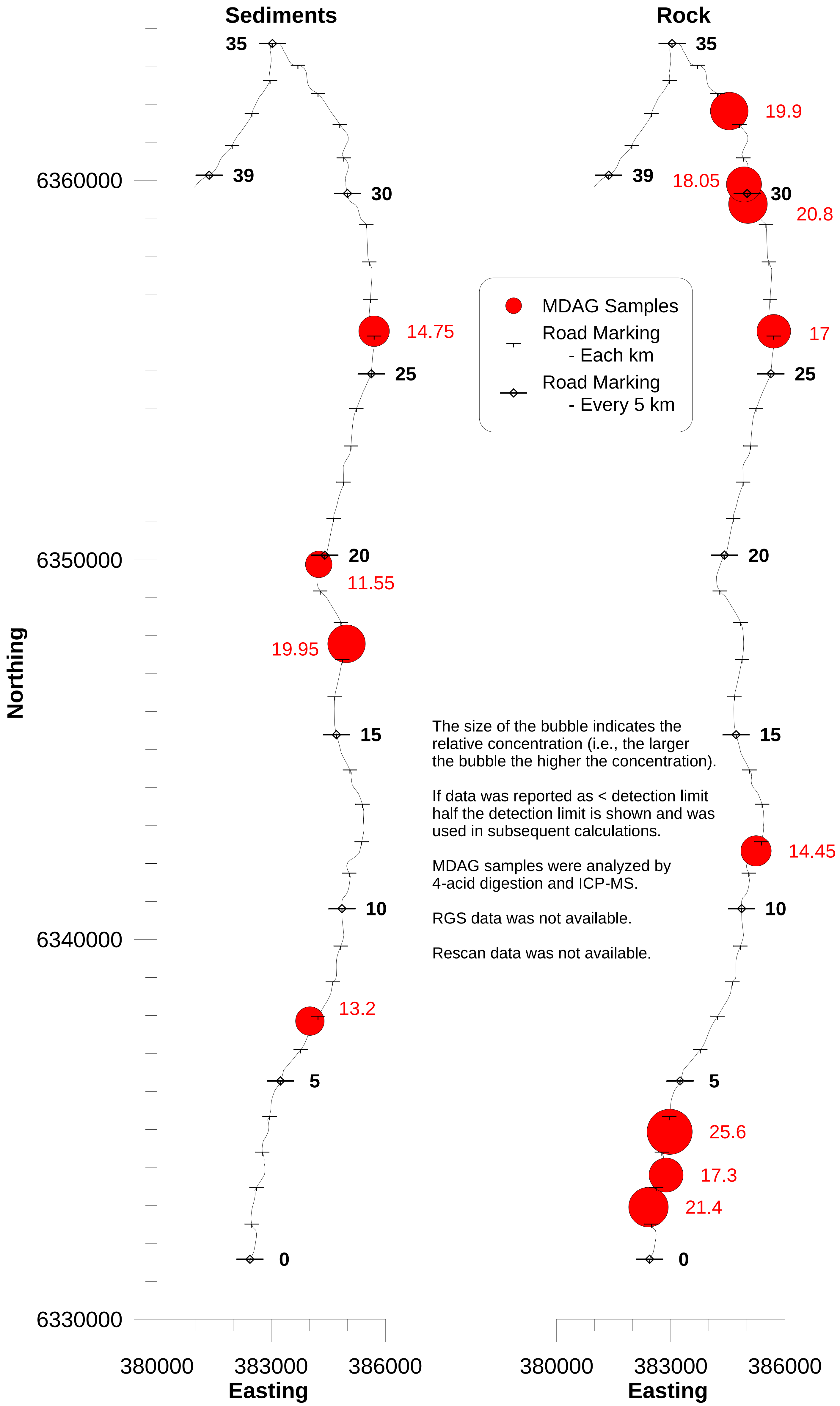
MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for both the RGS and Rescan samples are higher for several elements than the detection limits used for the MDAG samples.

Gallium (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

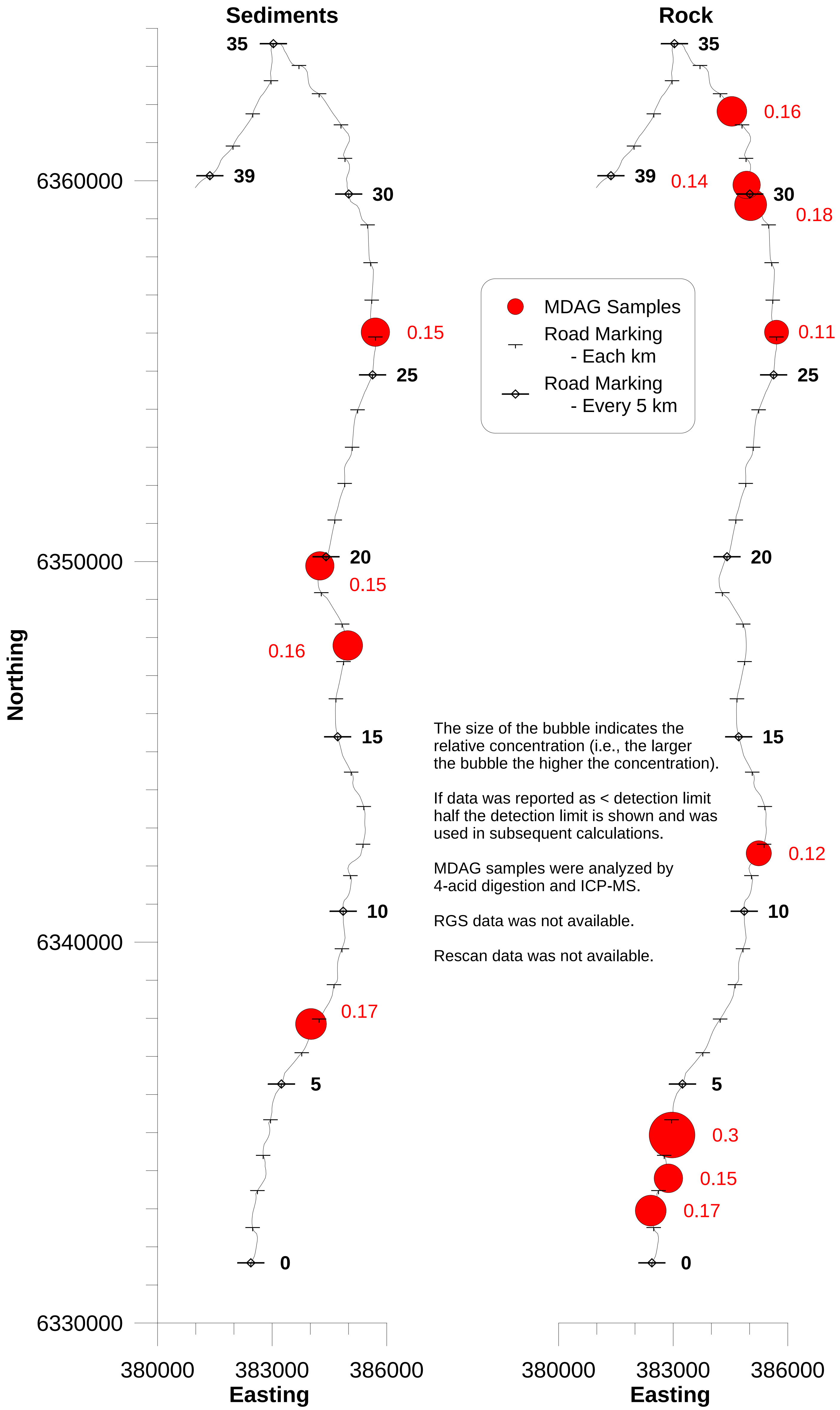
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

Germanium (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

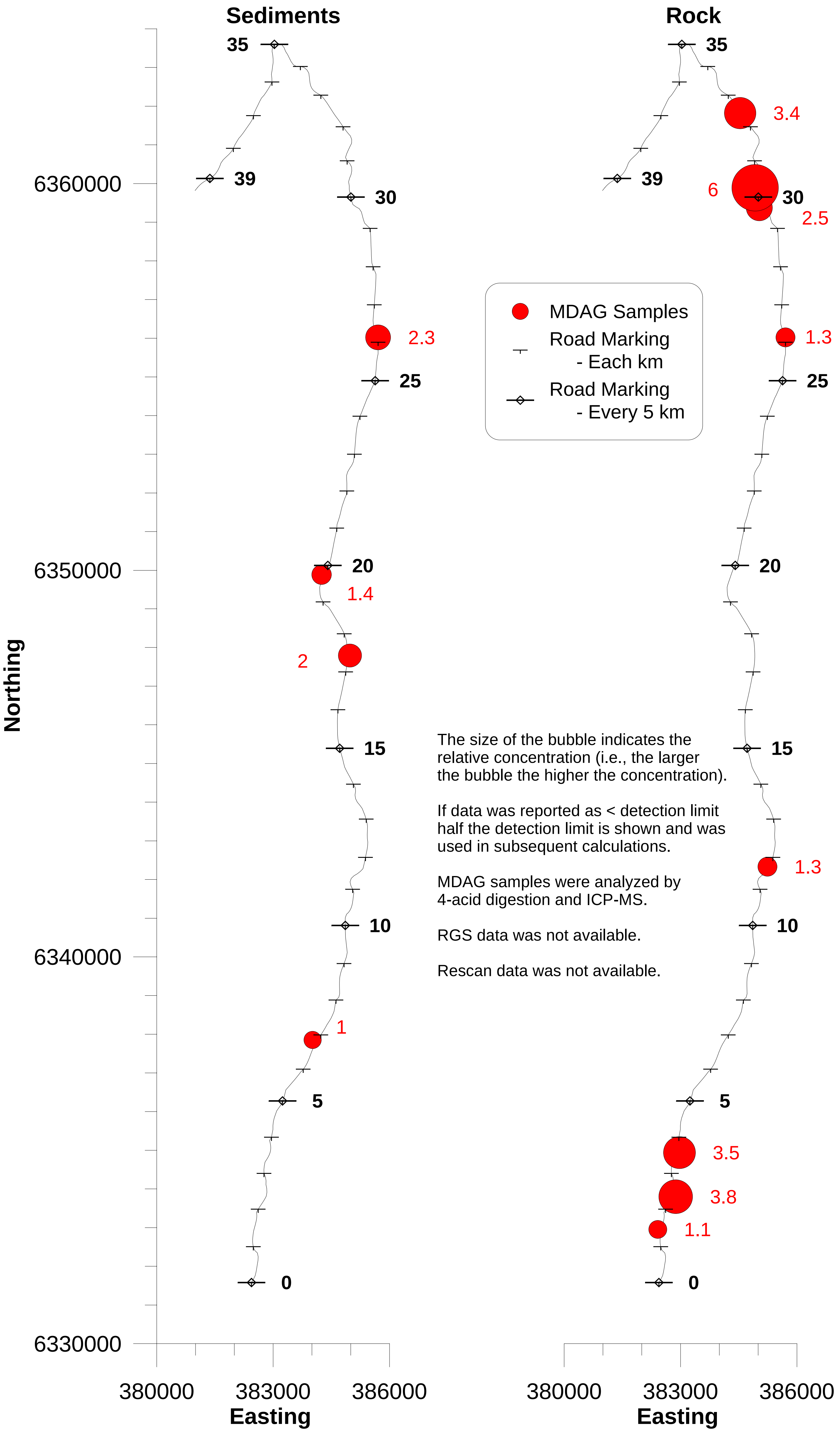
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

Hafnium (ppm)



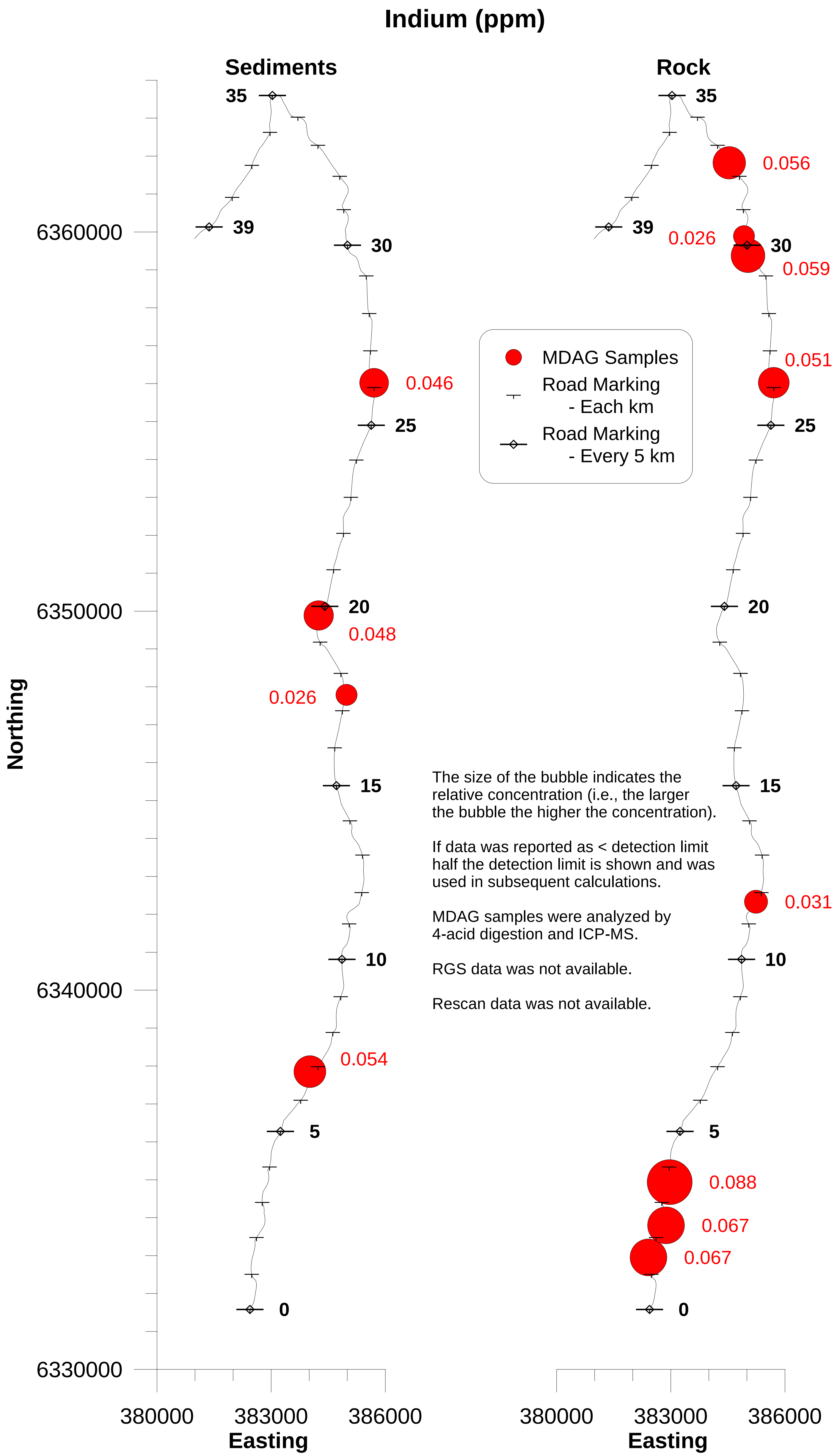
The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.



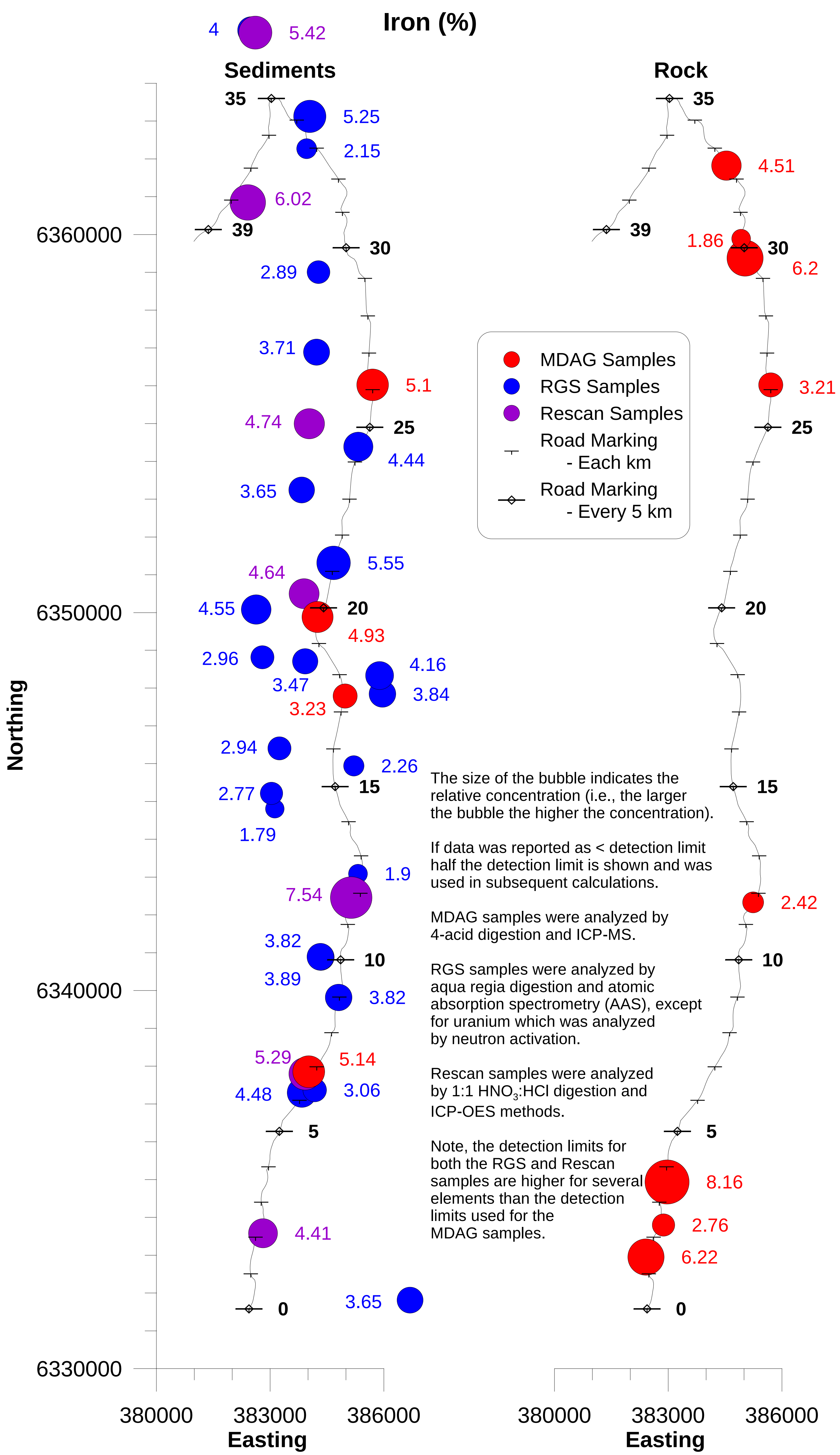
The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.



Iron (%)

The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

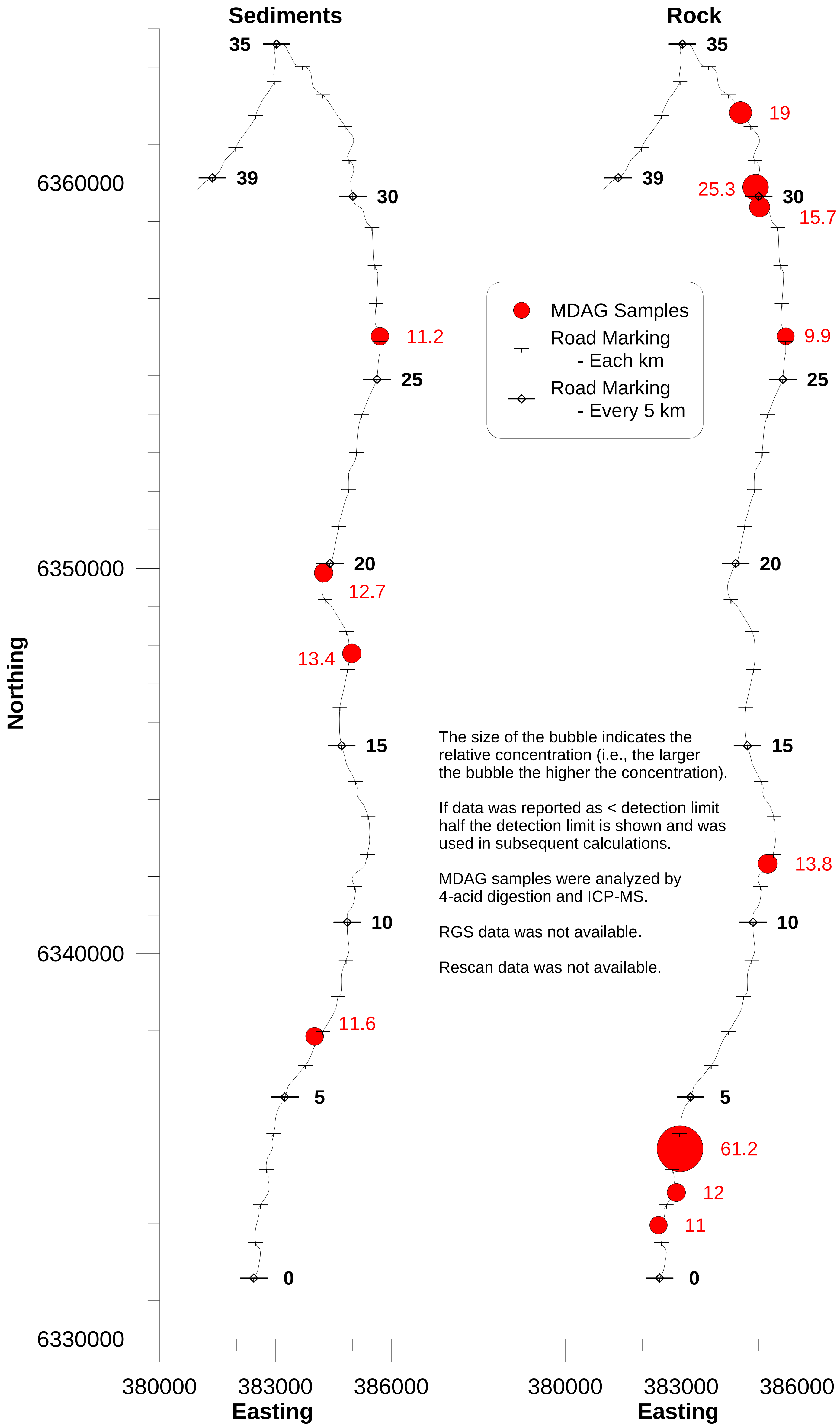
MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for both the RGS and Rescan samples are higher for several elements than the detection limits used for the MDAG samples.

Lanthanum (ppm)



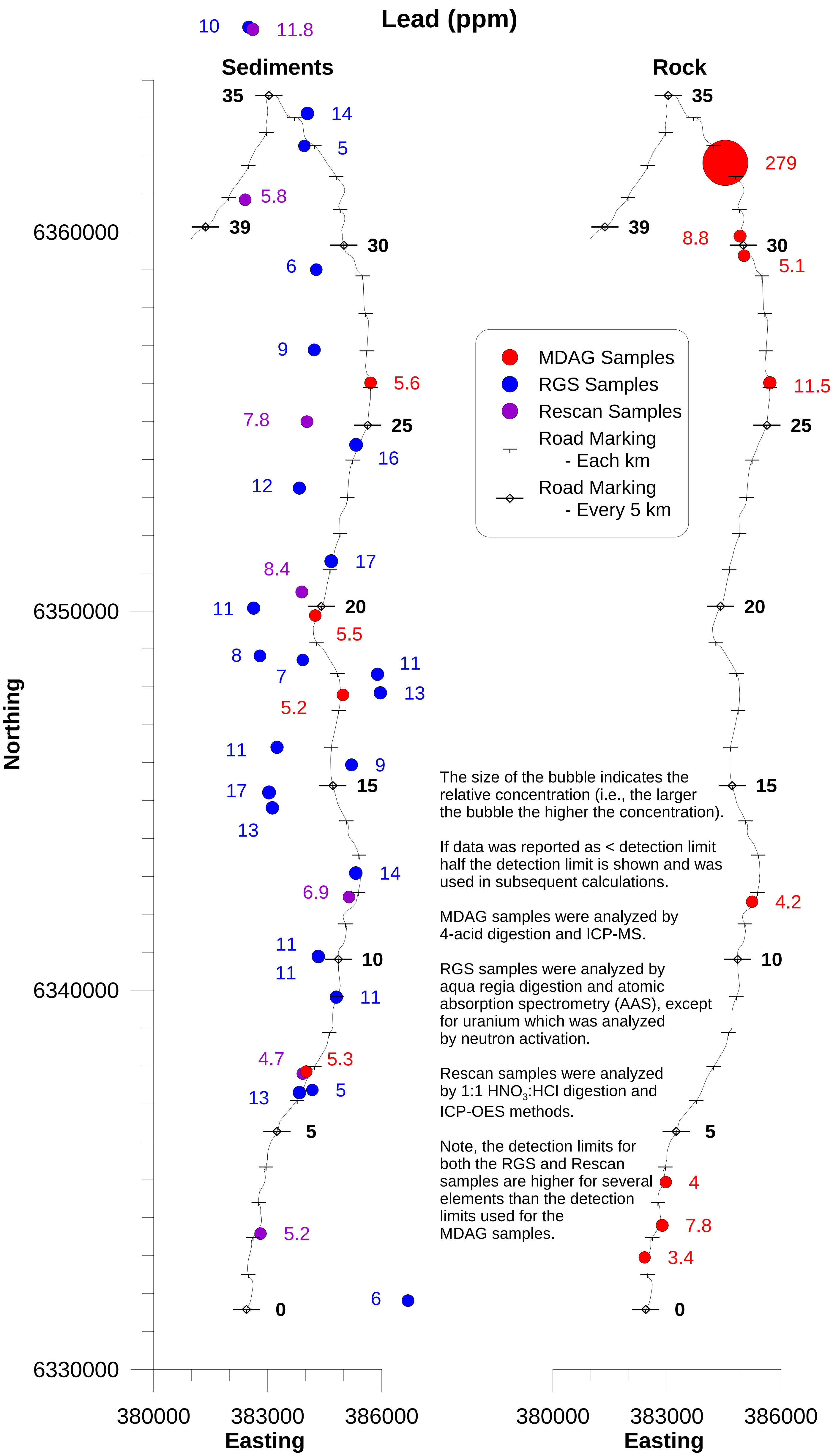
The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

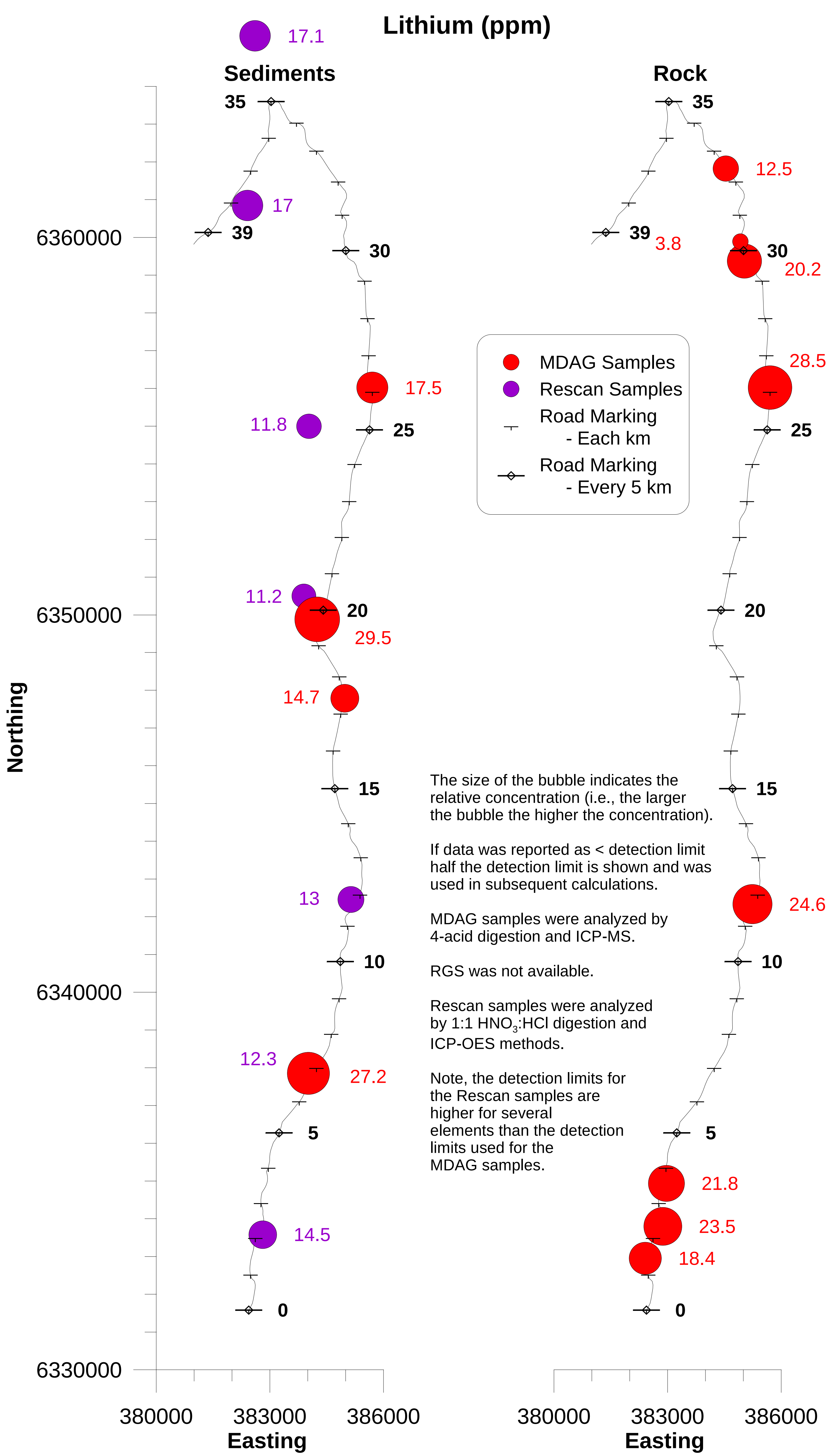
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for both the RGS and Rescan samples are higher for several elements than the detection limits used for the MDAG samples.



Lithium (ppm)

The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

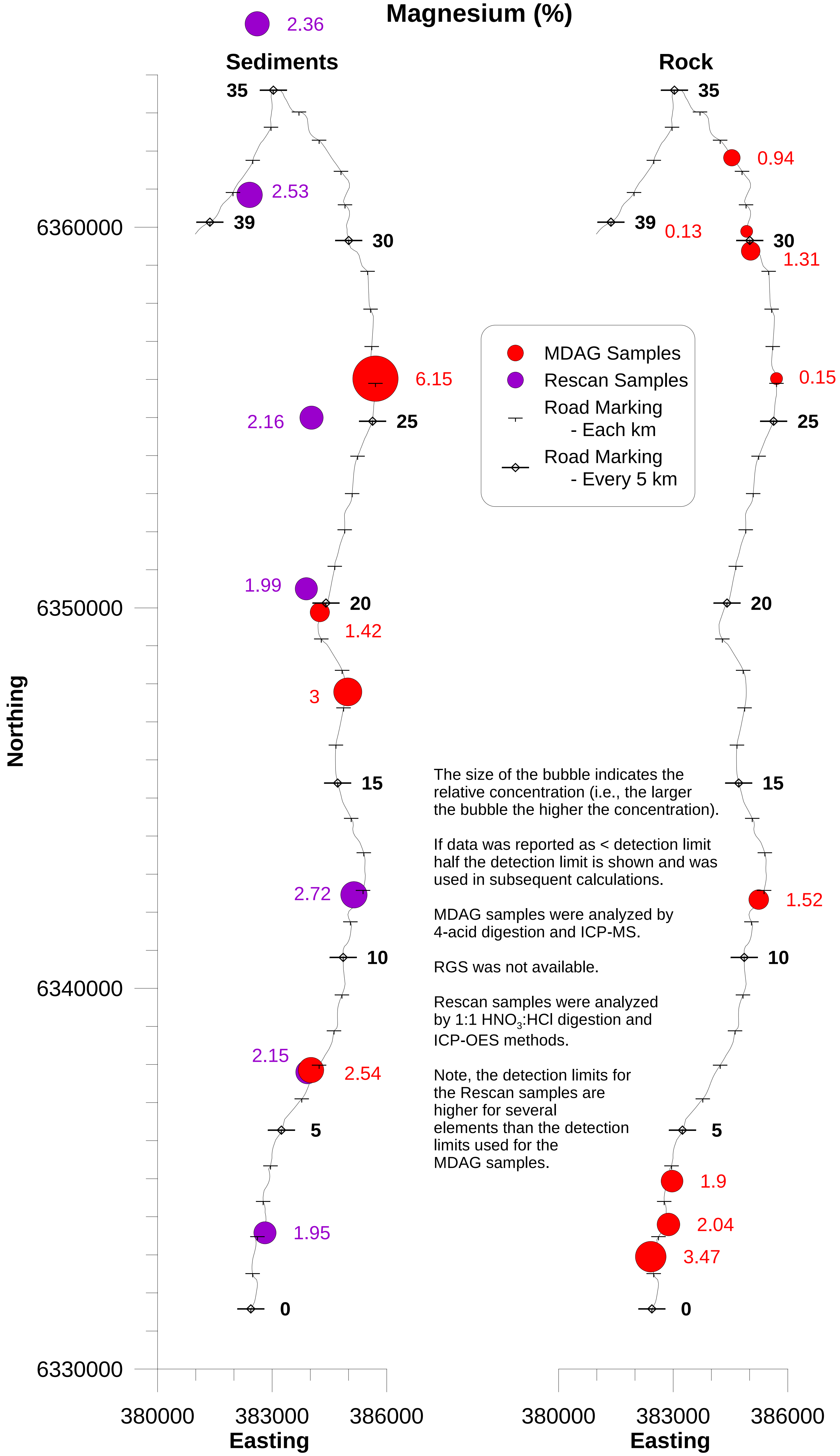
MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS was not available.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for the Rescan samples are higher for several elements than the detection limits used for the MDAG samples.

Magnesium (%)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

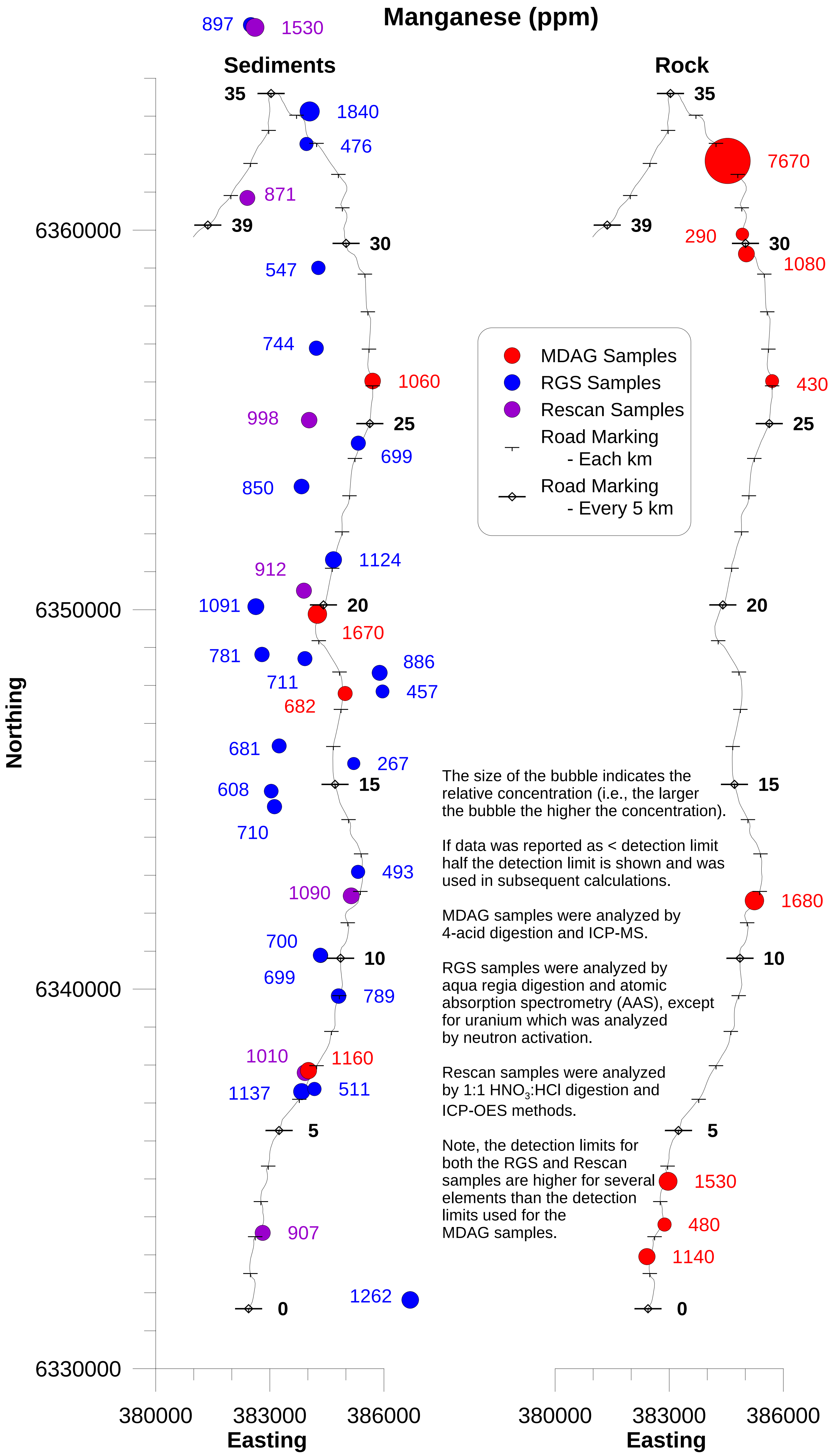
MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS was not available.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for the Rescan samples are higher for several elements than the detection limits used for the MDAG samples.

Manganese (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

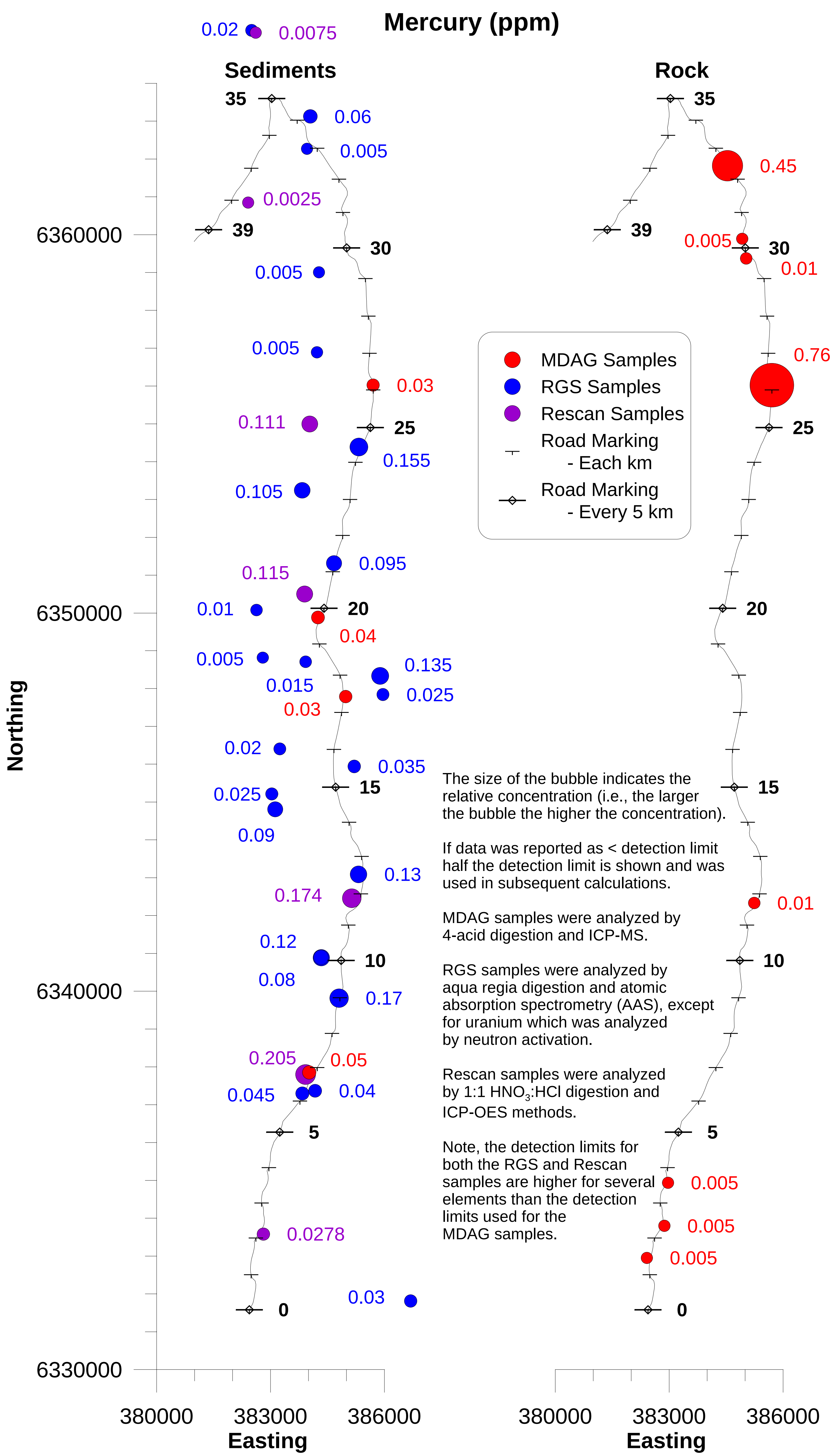
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for both the RGS and Rescan samples are higher for several elements than the detection limits used for the MDAG samples.



Mercury (ppm)

The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

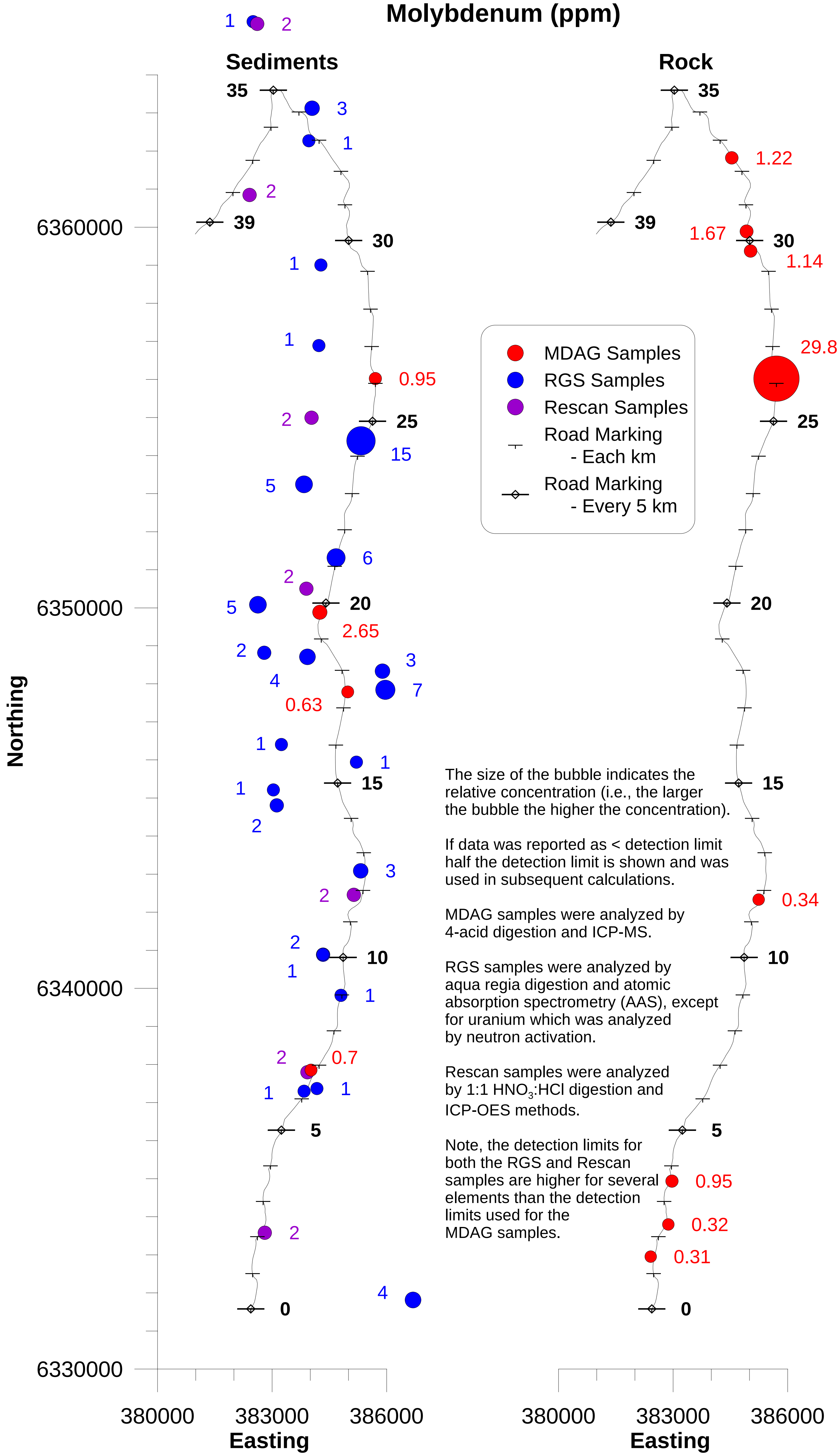
MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for both the RGS and Rescan samples are higher for several elements than the detection limits used for the MDAG samples.

Molybdenum (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

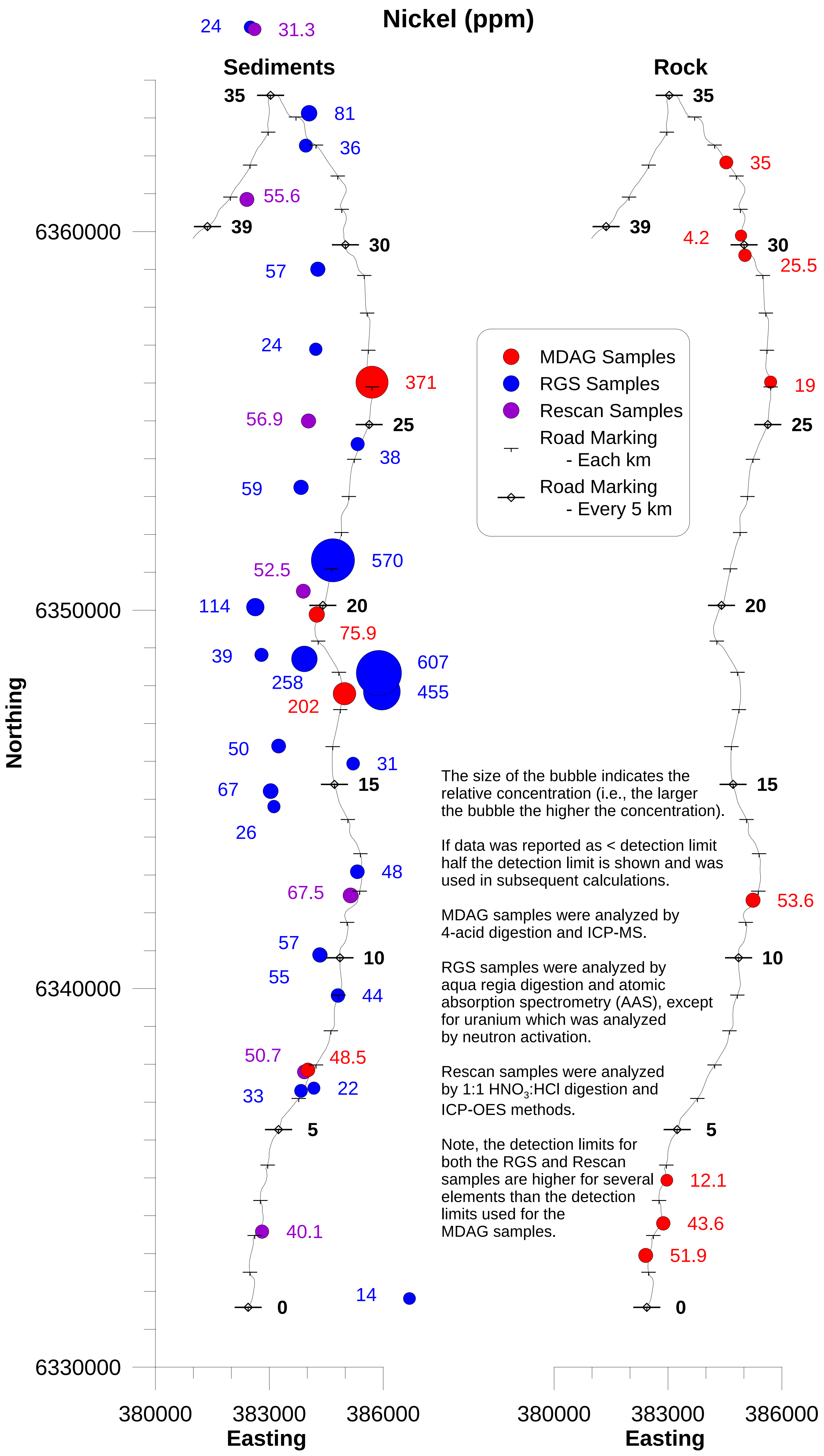
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for both the RGS and Rescan samples are higher for several elements than the detection limits used for the MDAG samples.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

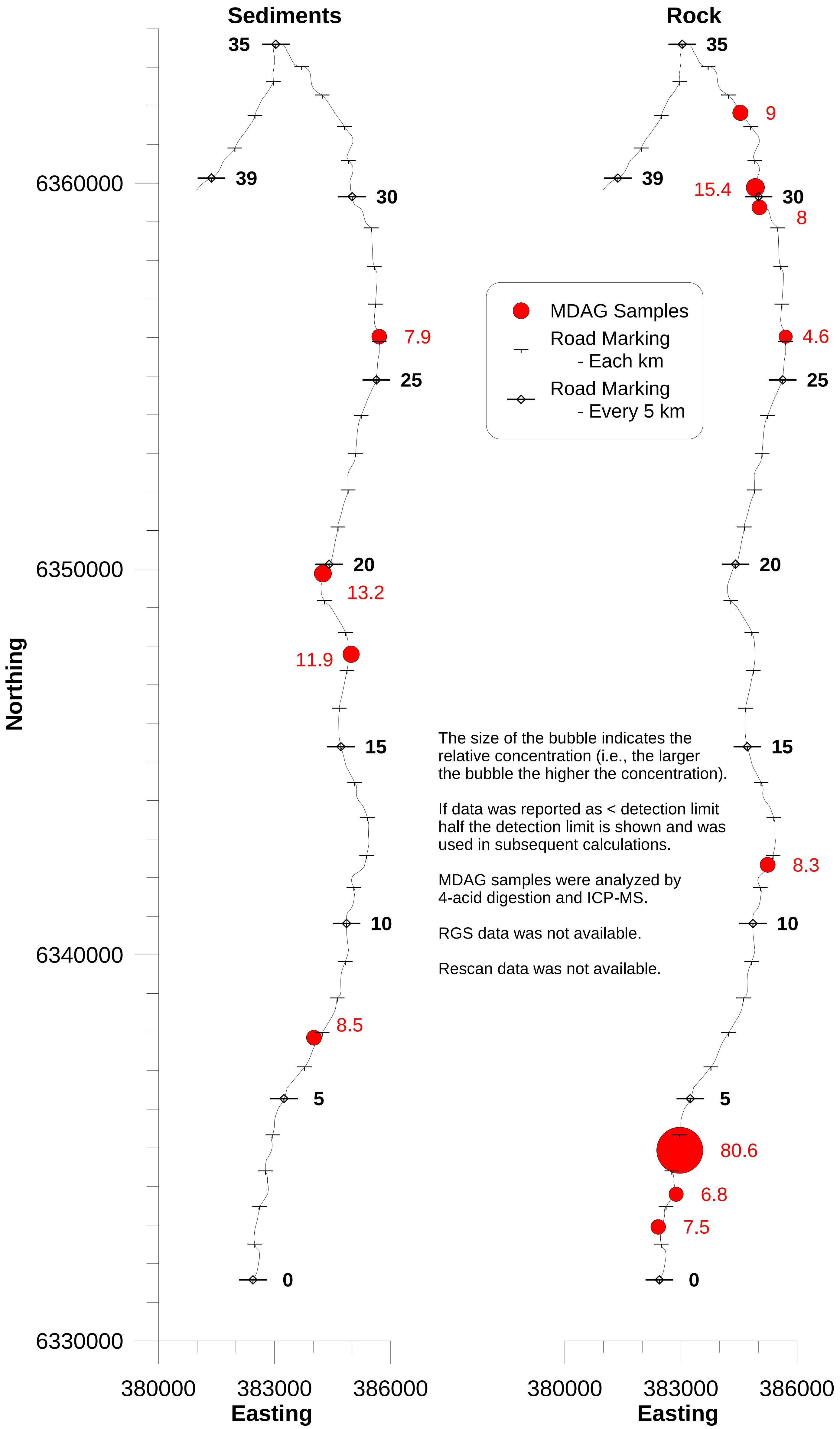
MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for both the RGS and Rescan samples are higher for several elements than the detection limits used for the MDAG samples.

Niobium (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

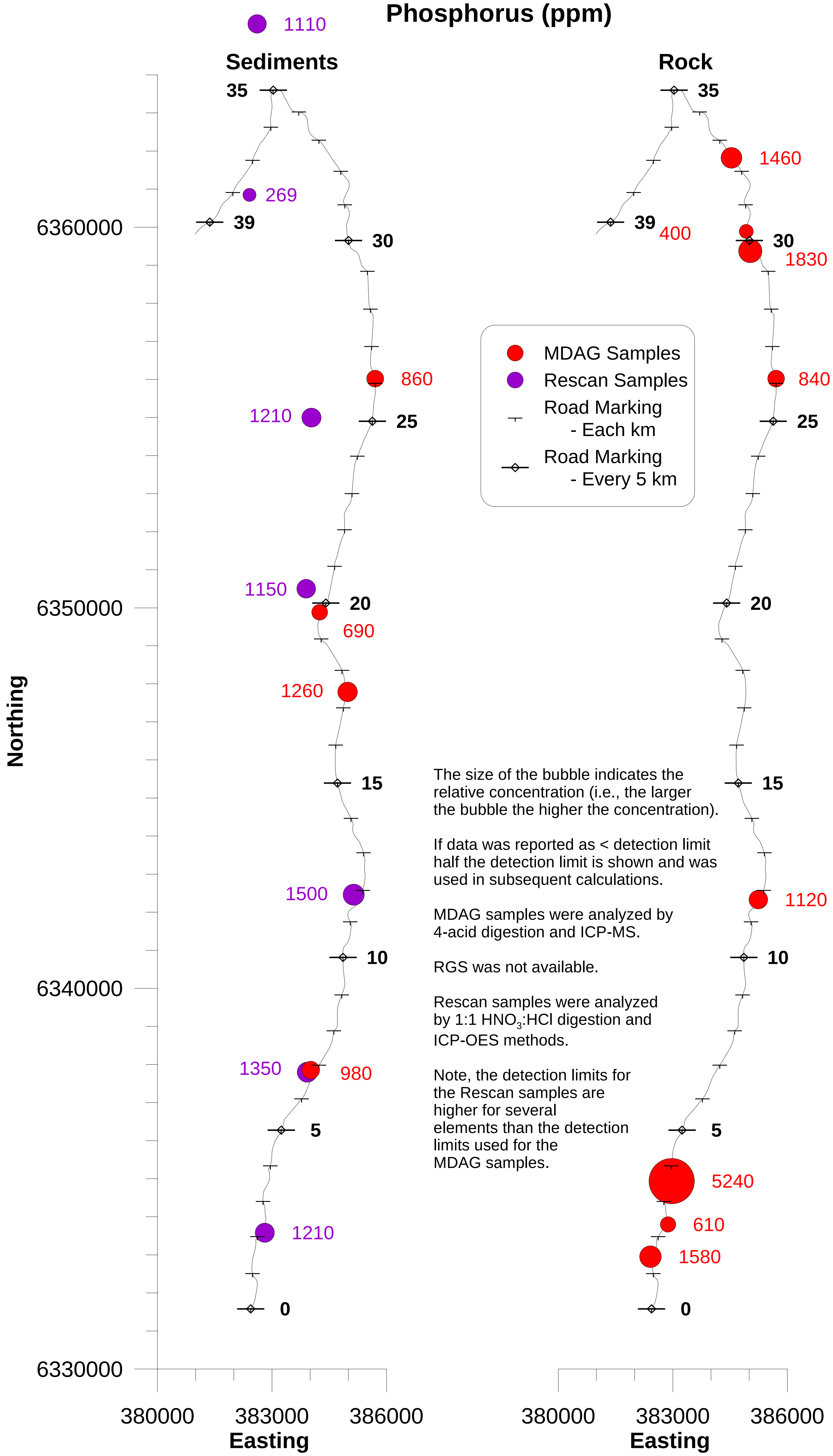
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

Phosphorus (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

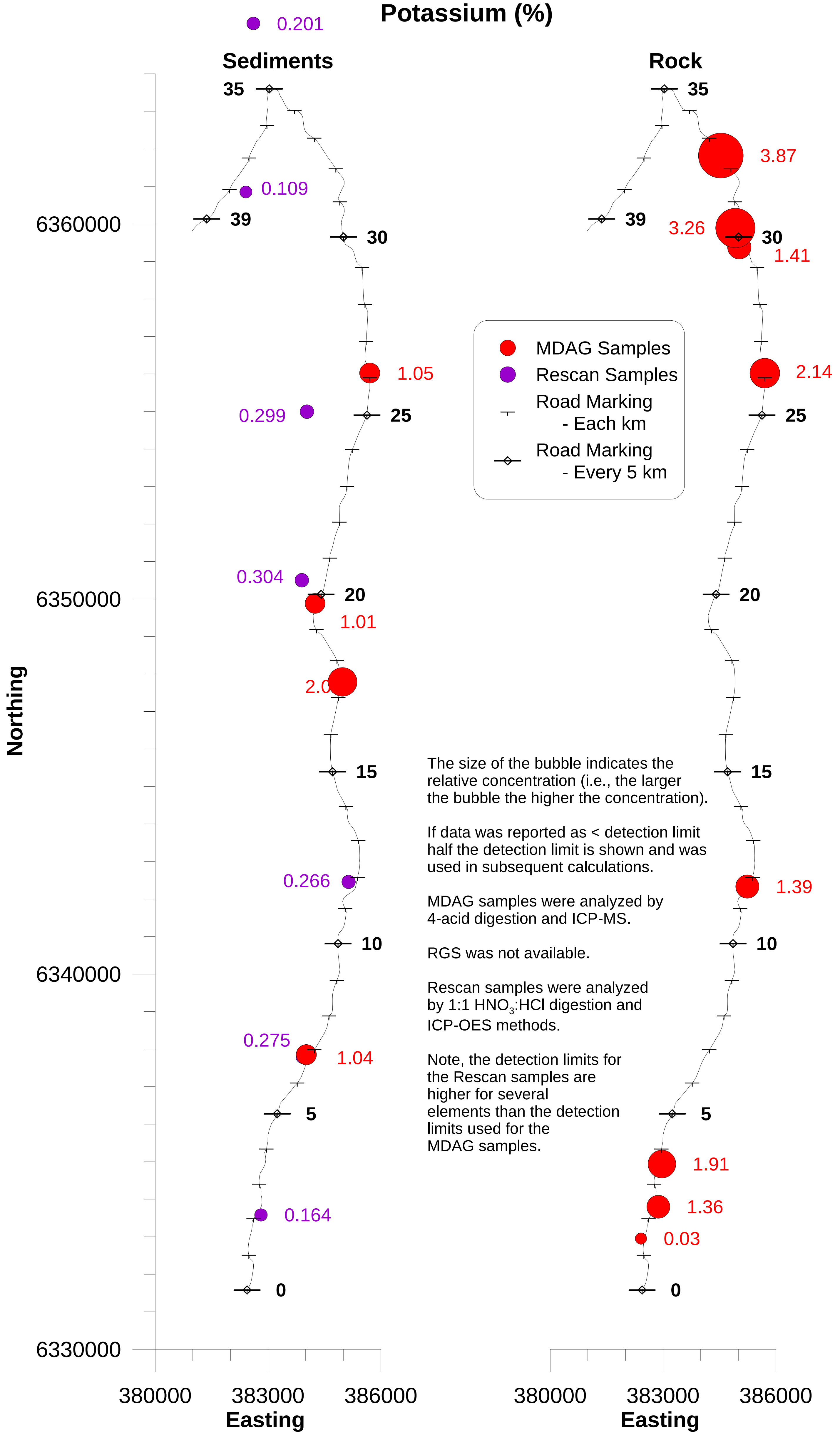
MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS was not available.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for the Rescan samples are higher for several elements than the detection limits used for the MDAG samples.

Potassium (%)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

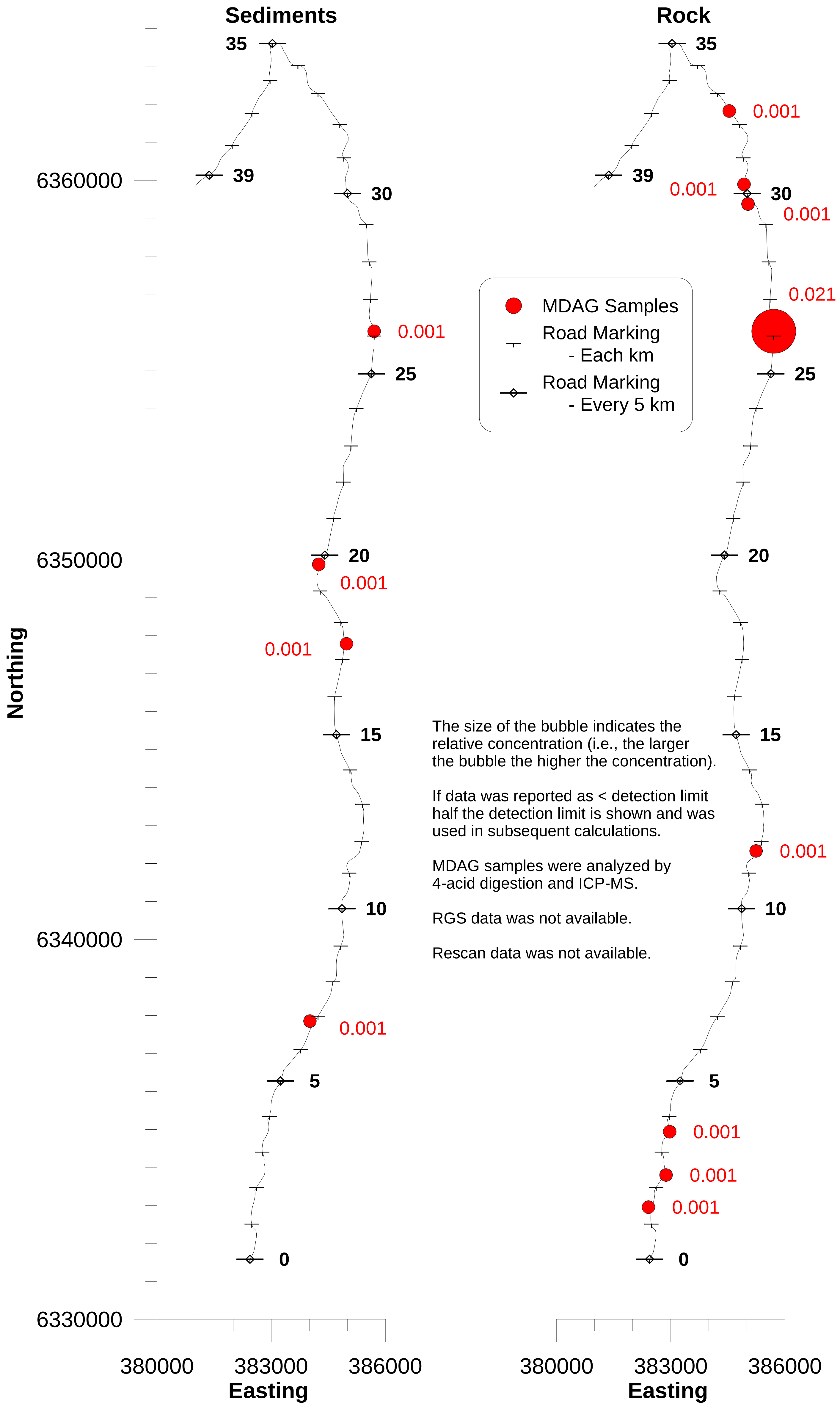
MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS was not available.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for the Rescan samples are higher for several elements than the detection limits used for the MDAG samples.

Rhenium (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

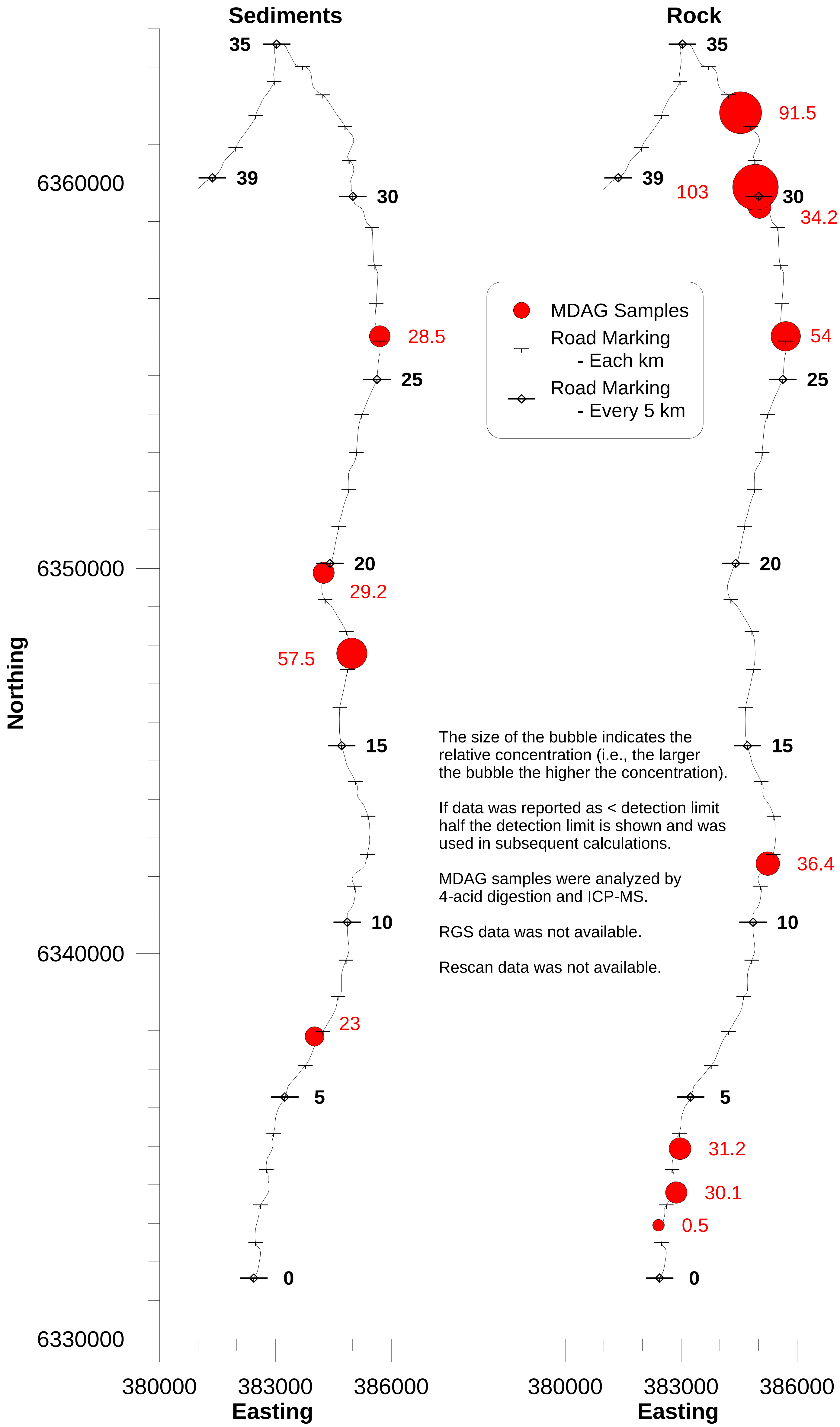
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

Rubidium (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

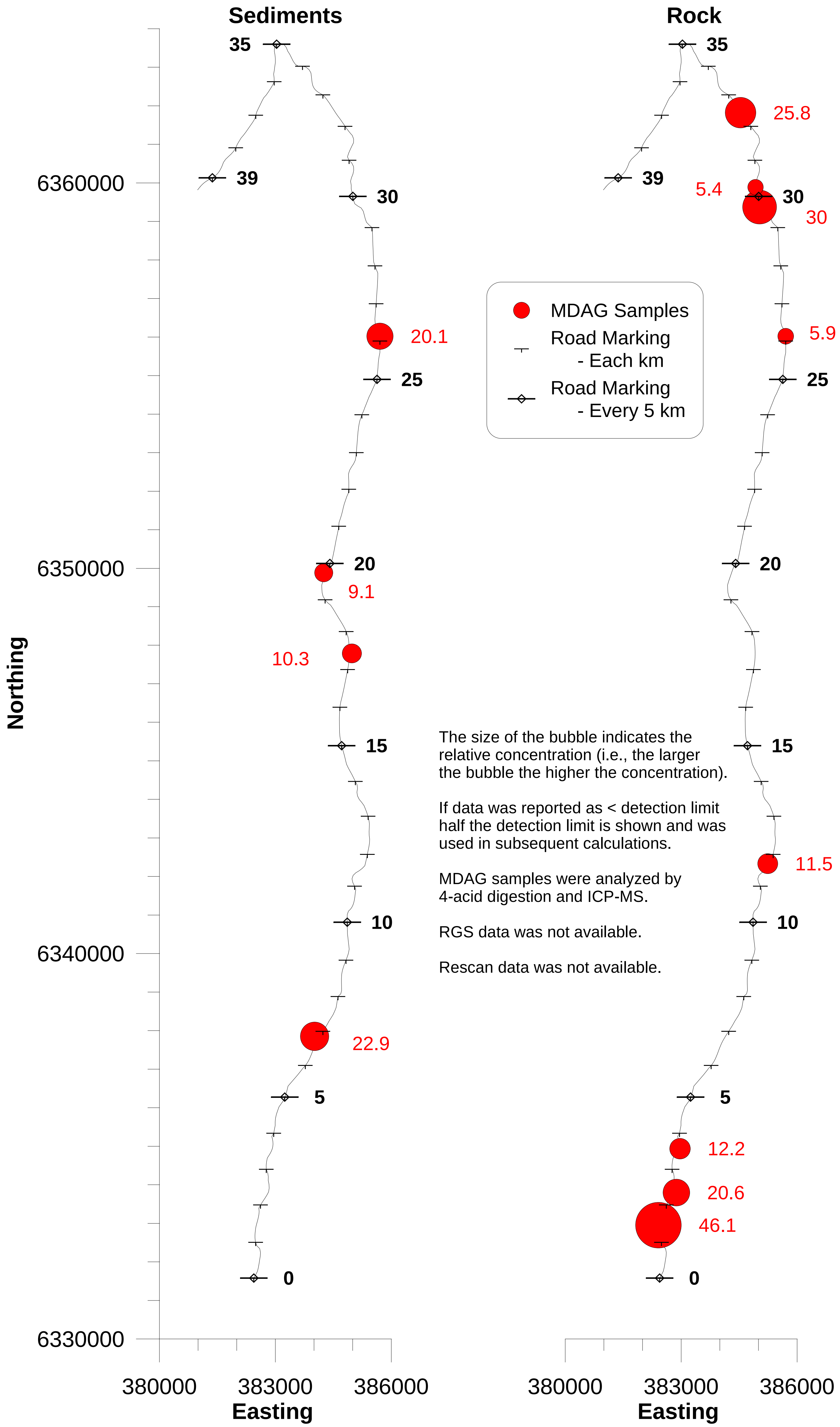
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

Scandium (ppm)



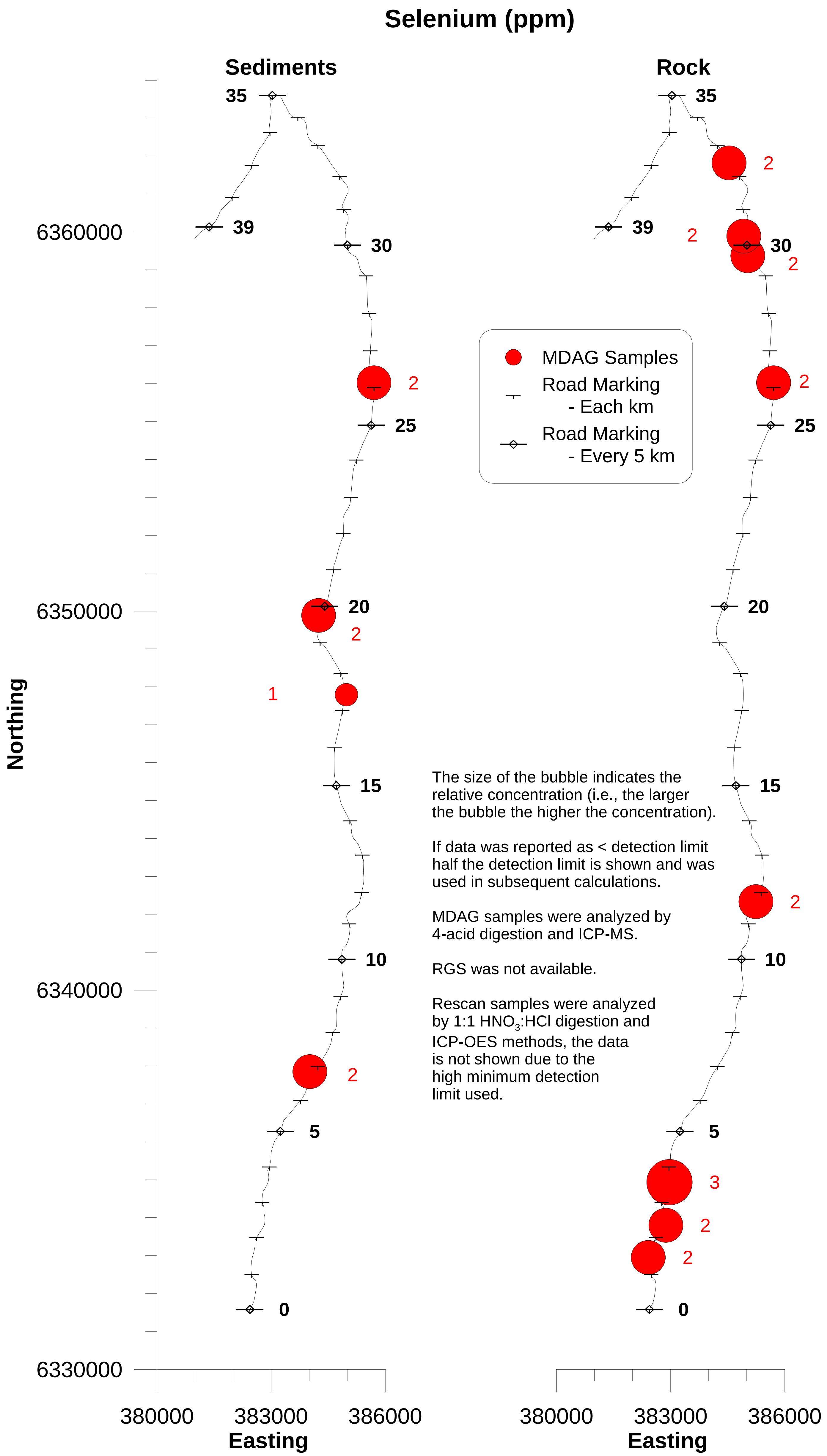
The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.



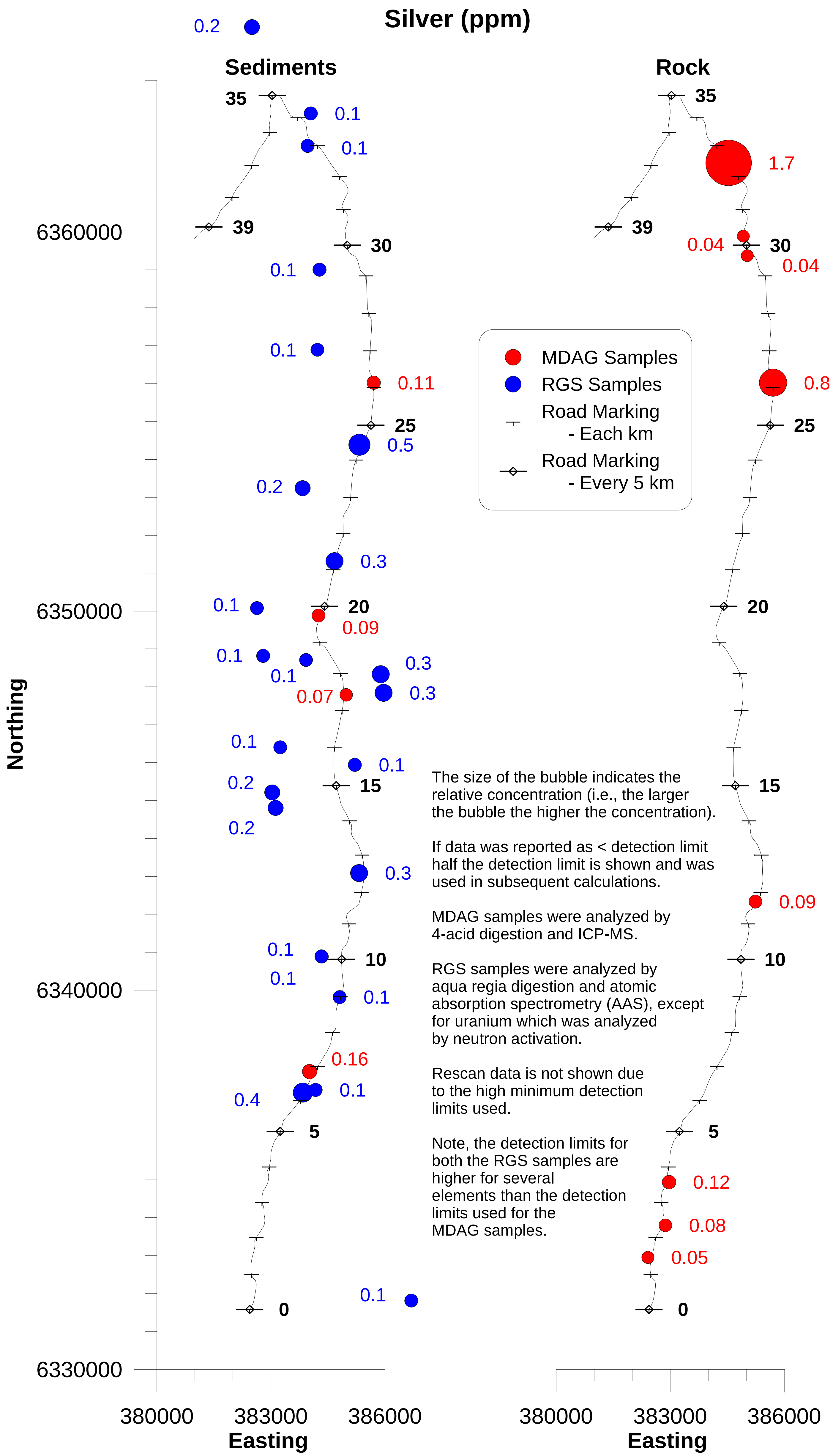
The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS was not available.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods, the data is not shown due to the high minimum detection limit used.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

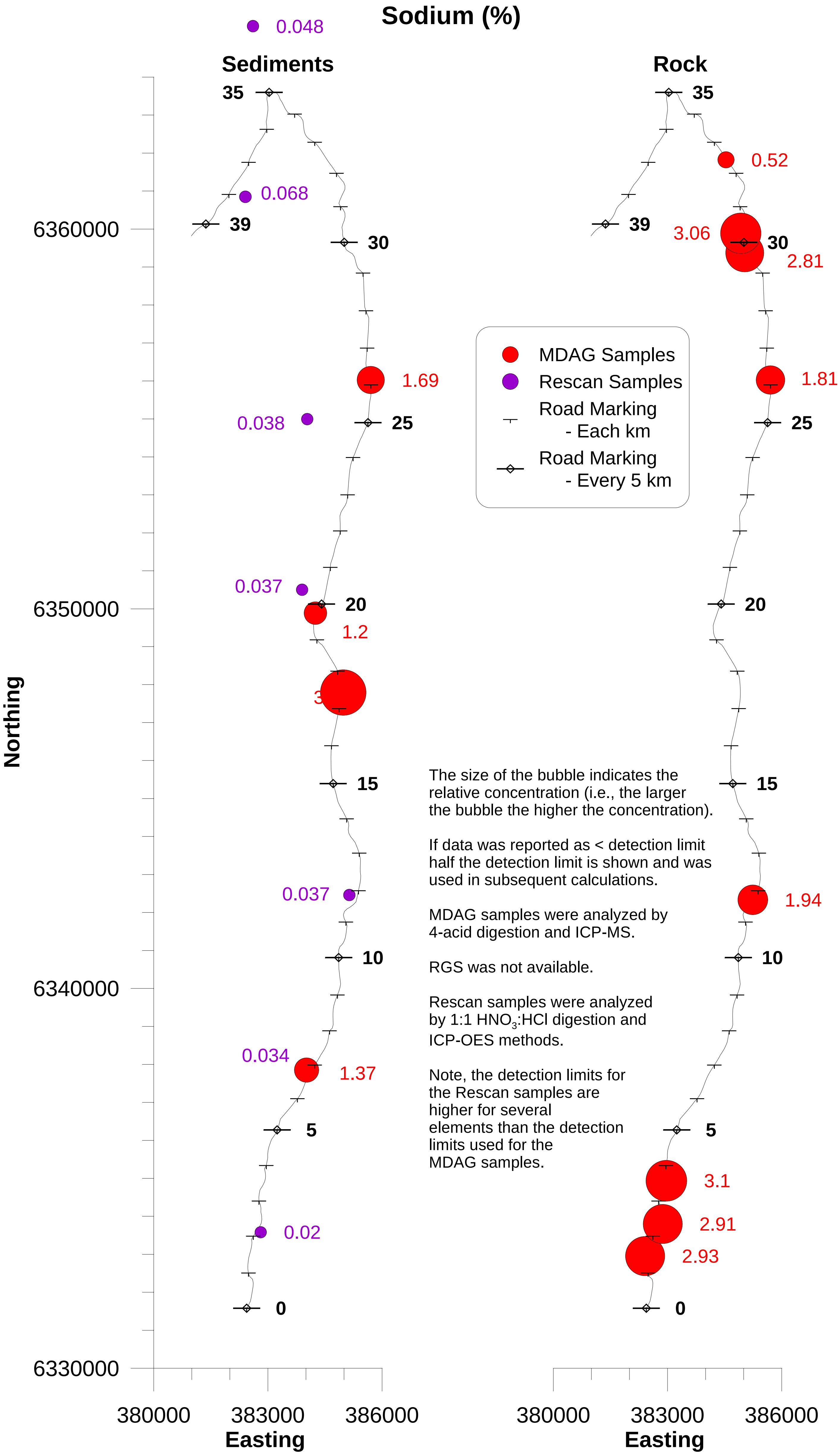
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan data is not shown due to the high minimum detection limits used.

Note, the detection limits for both the RGS samples are higher for several elements than the detection limits used for the MDAG samples.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

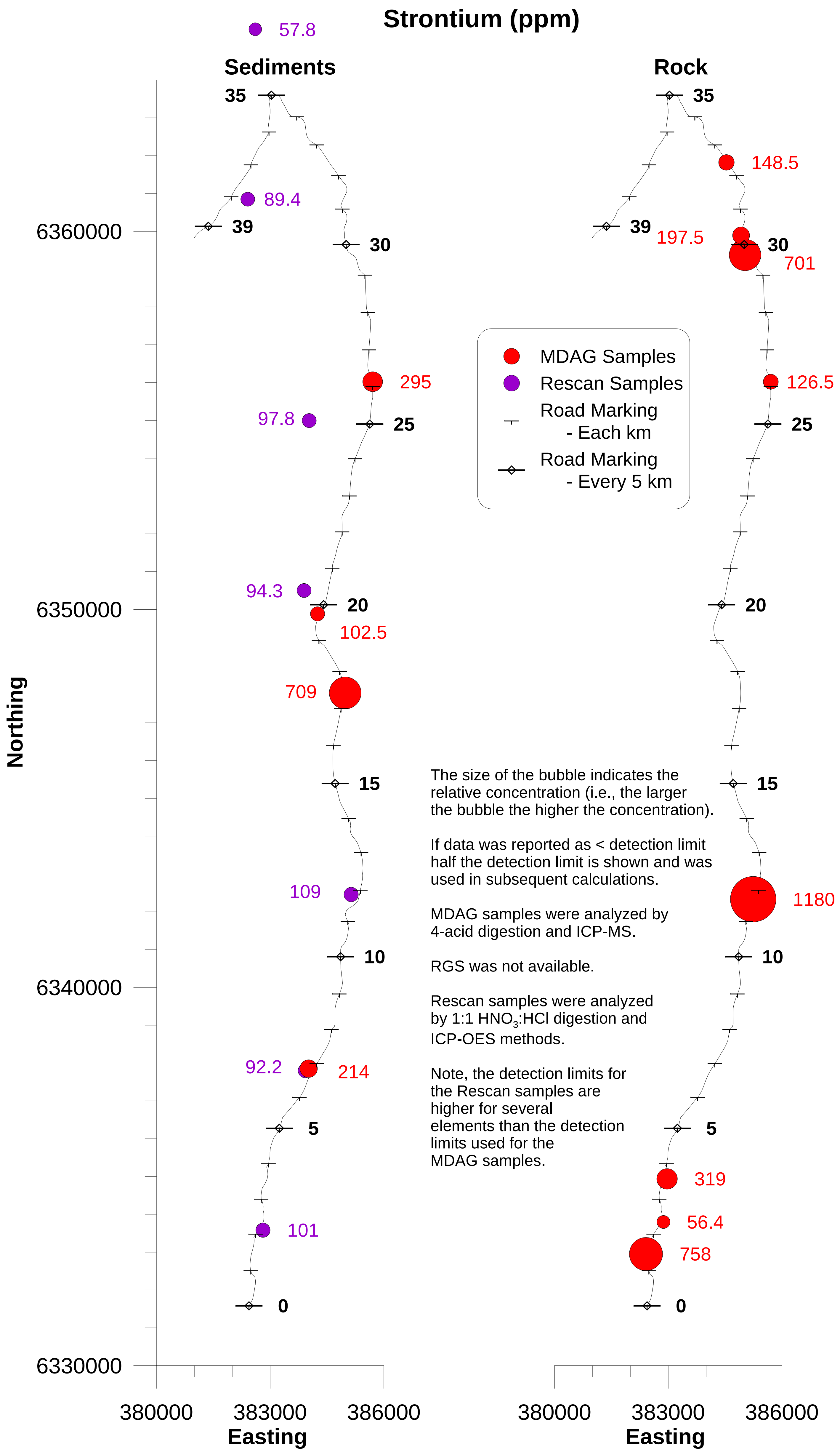
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS was not available.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for the Rescan samples are higher for several elements than the detection limits used for the MDAG samples.



Strontium (ppm)

The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

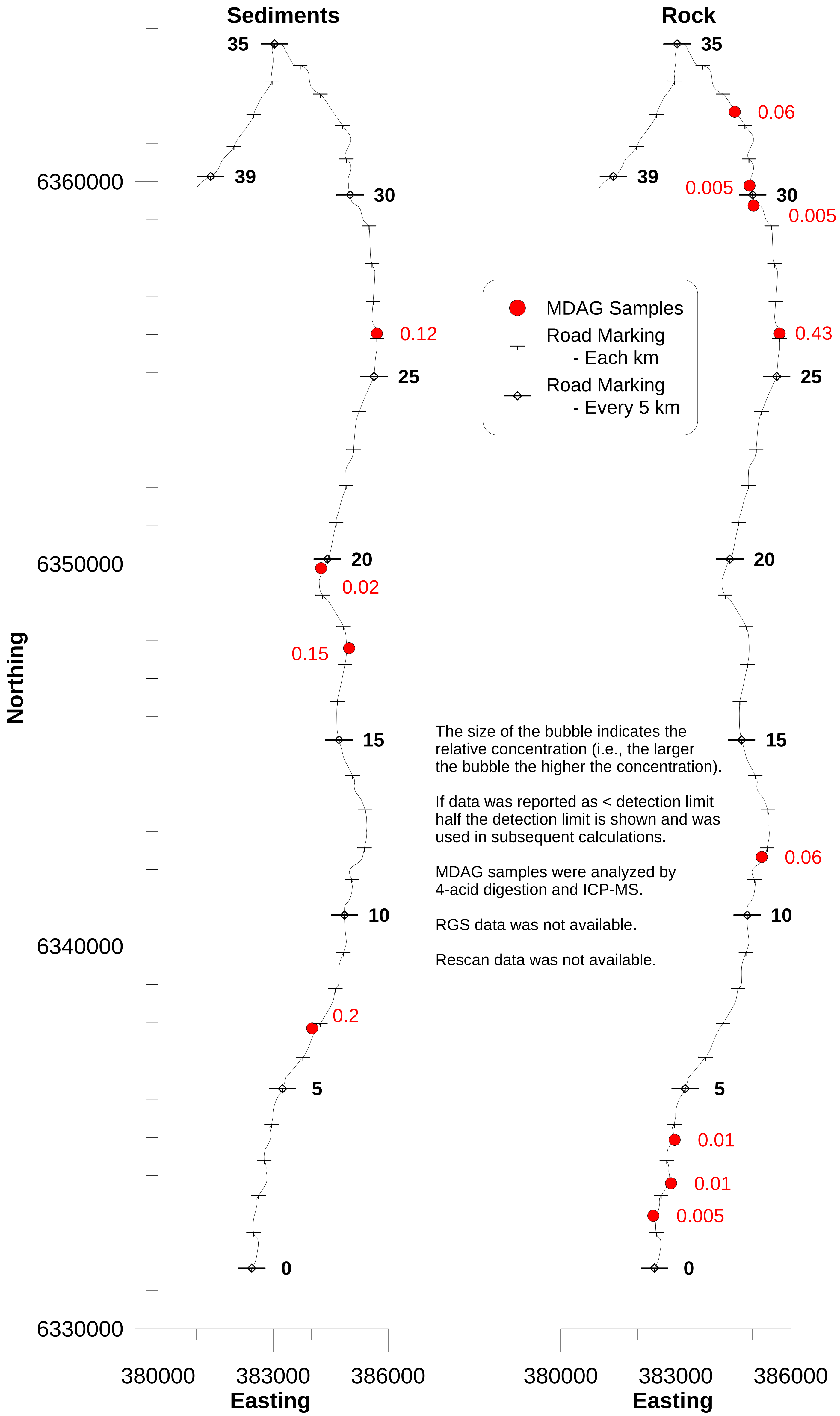
MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS was not available.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for the Rescan samples are higher for several elements than the detection limits used for the MDAG samples.

Sulphur (%)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

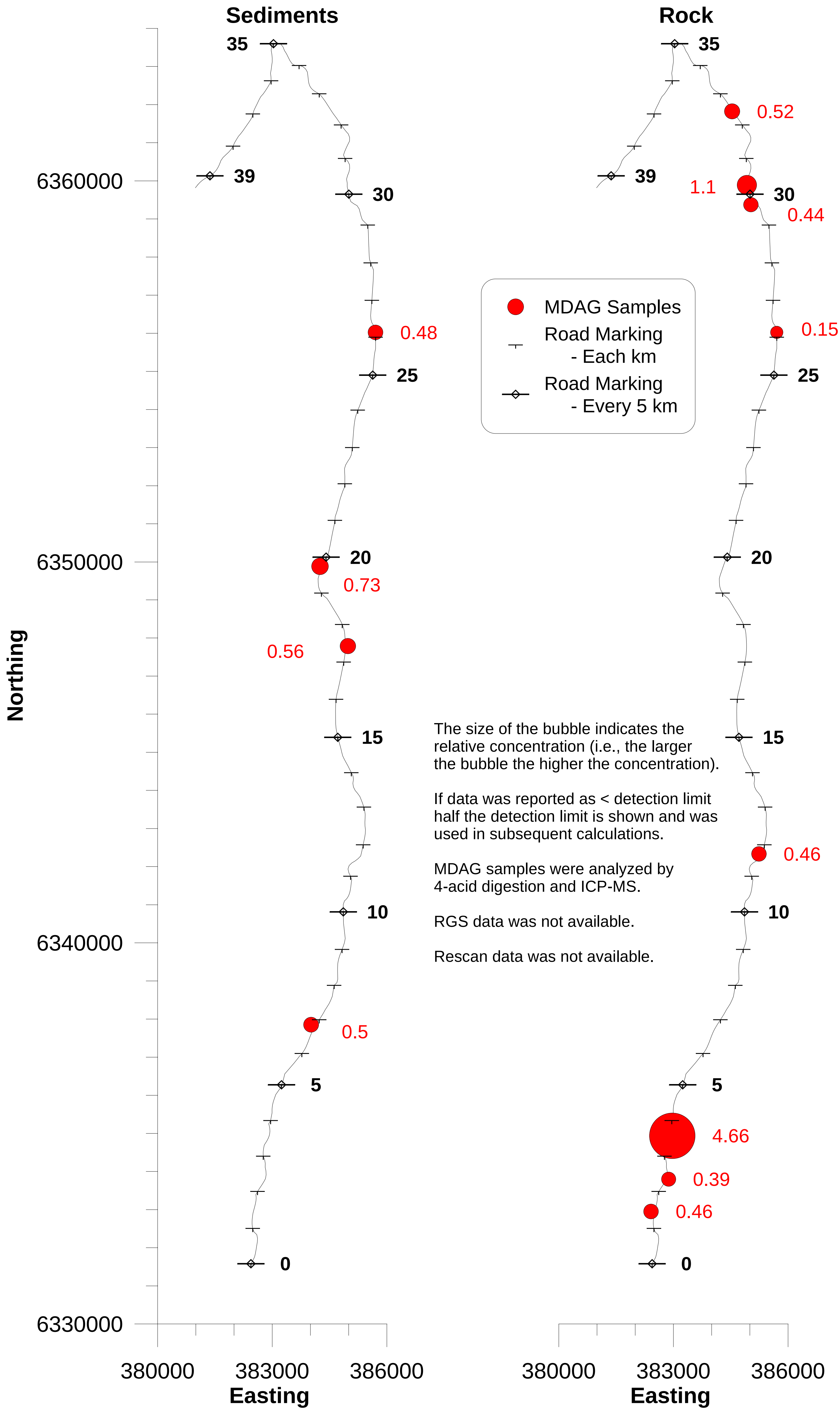
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

Tantalum (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

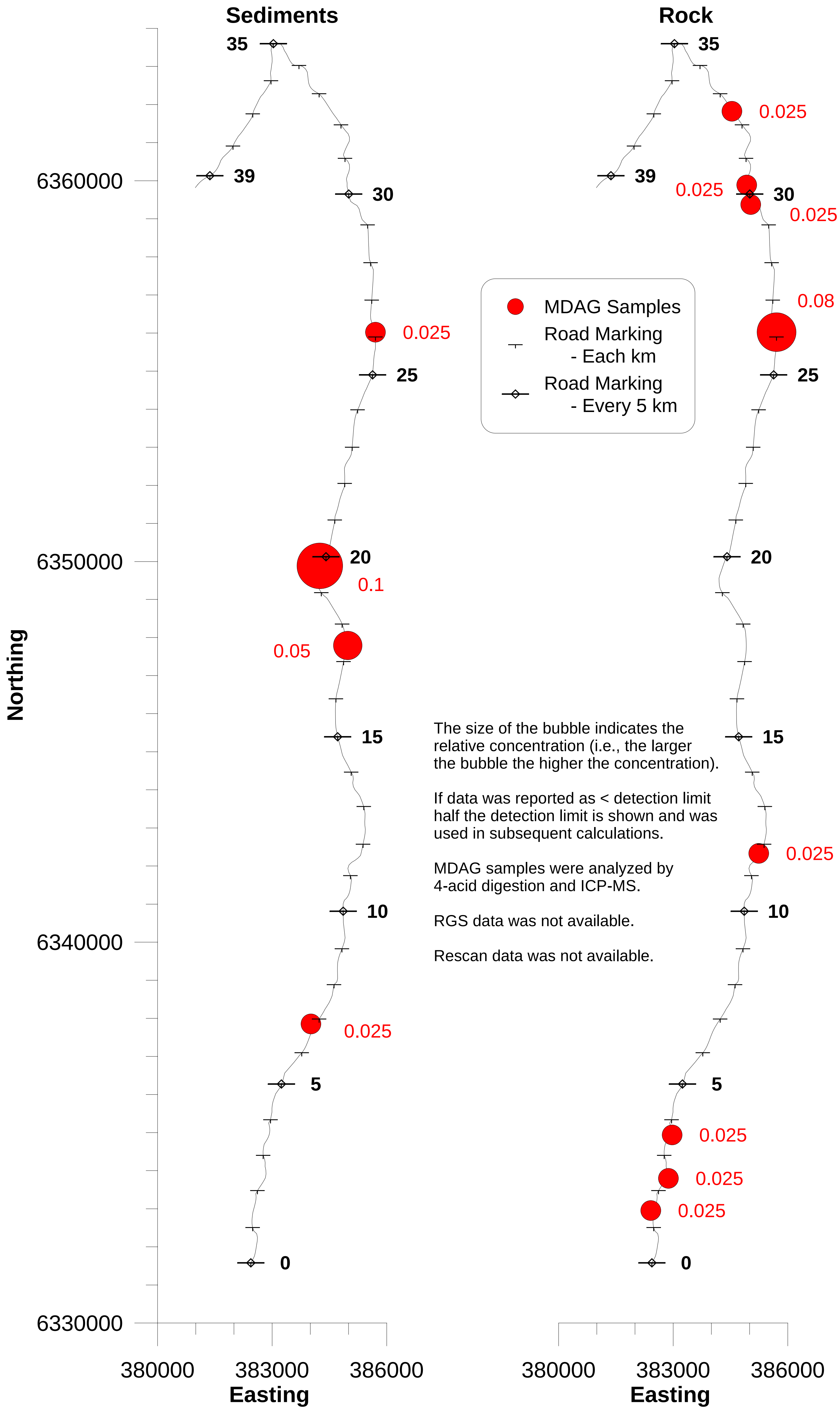
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

Tellurium (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

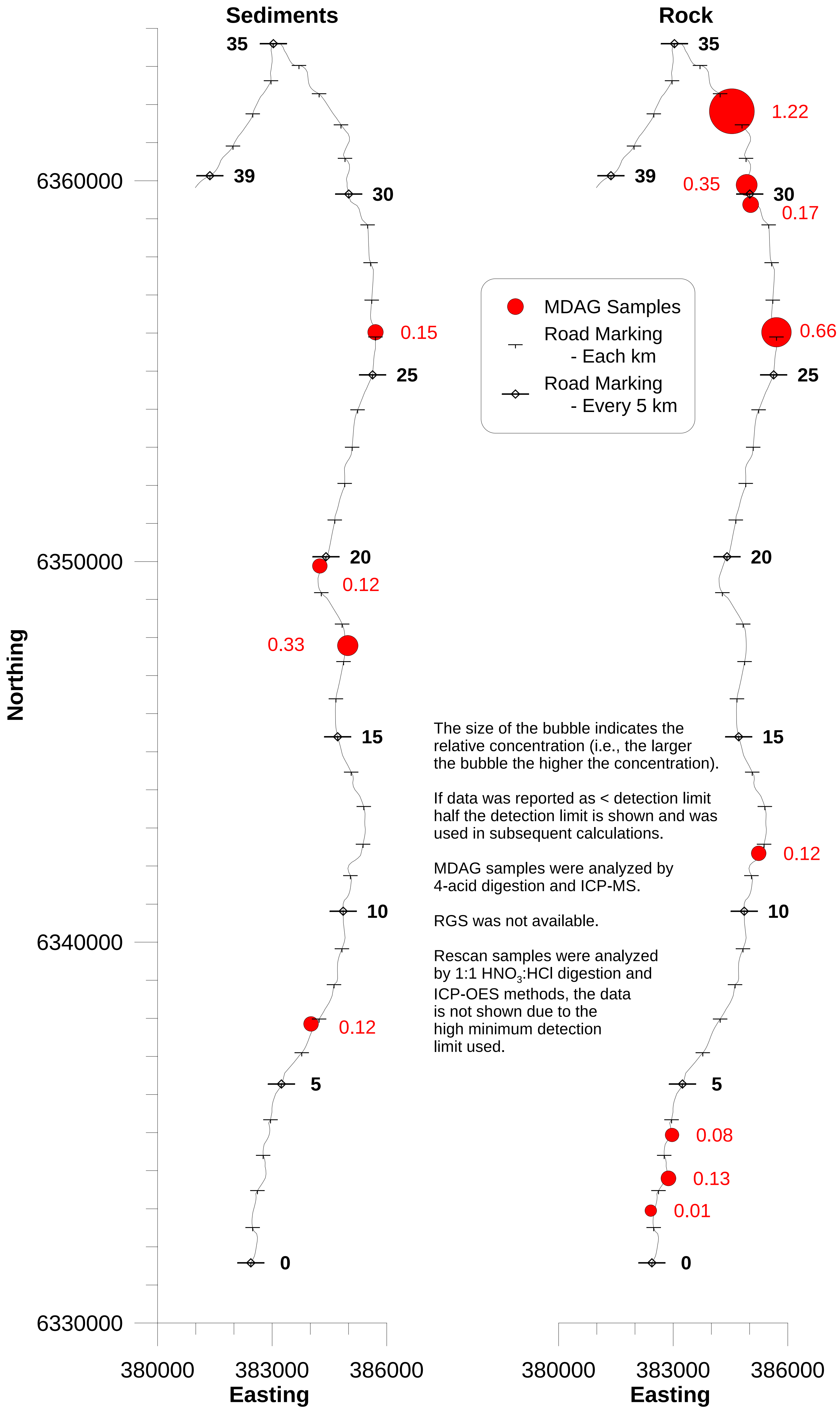
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

Thallium (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

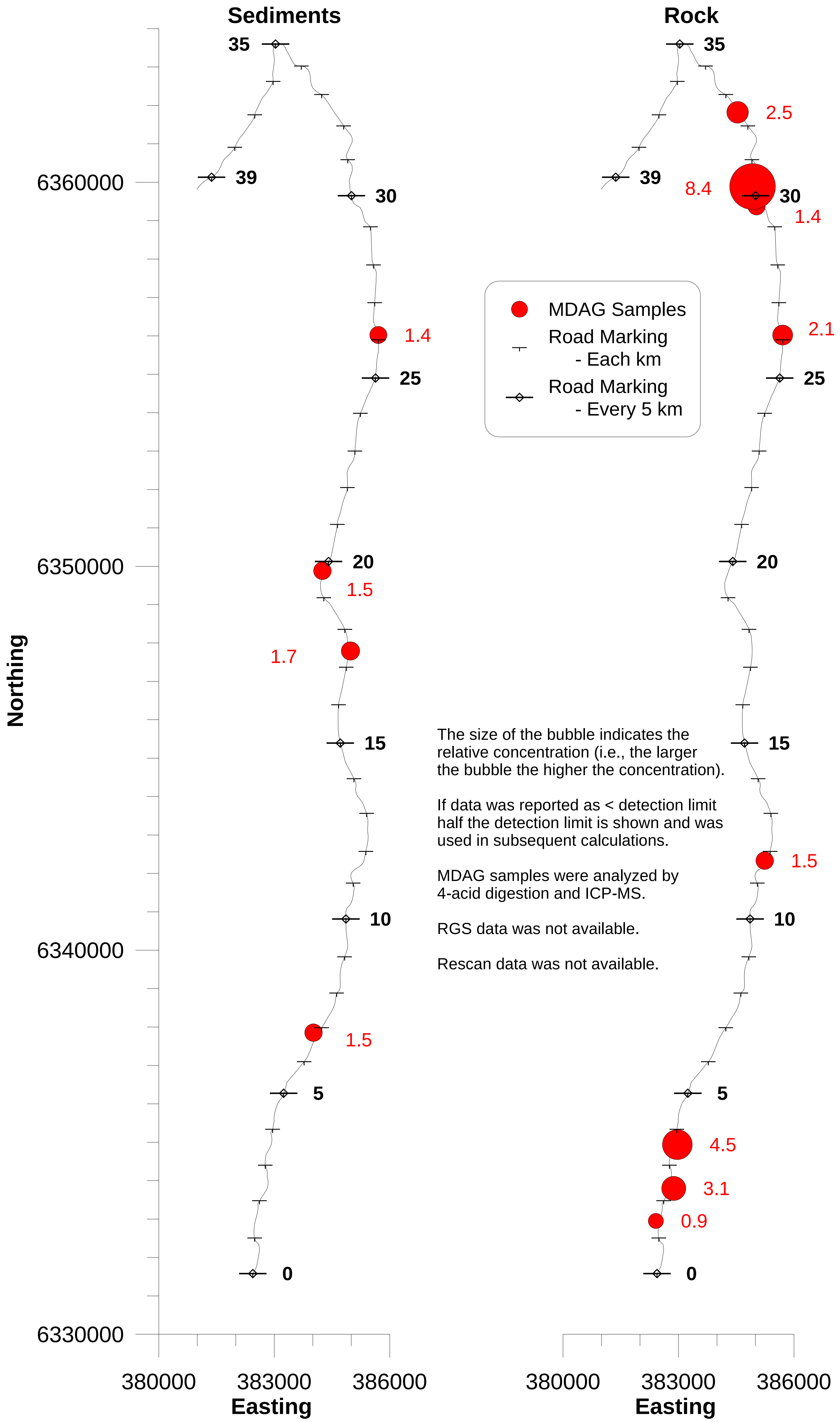
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS was not available.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods, the data is not shown due to the high minimum detection limit used.

Thorium (ppm)



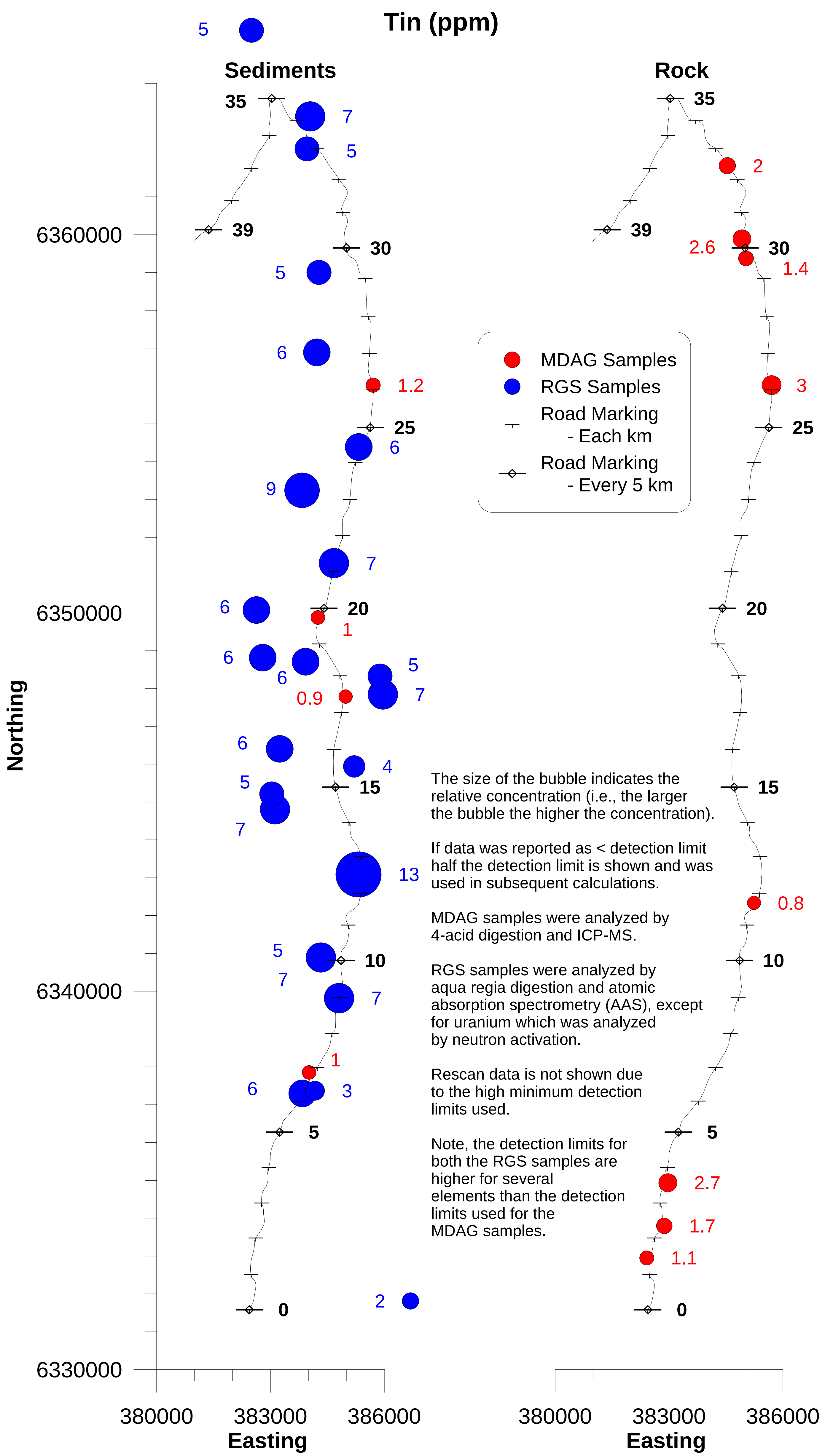
The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

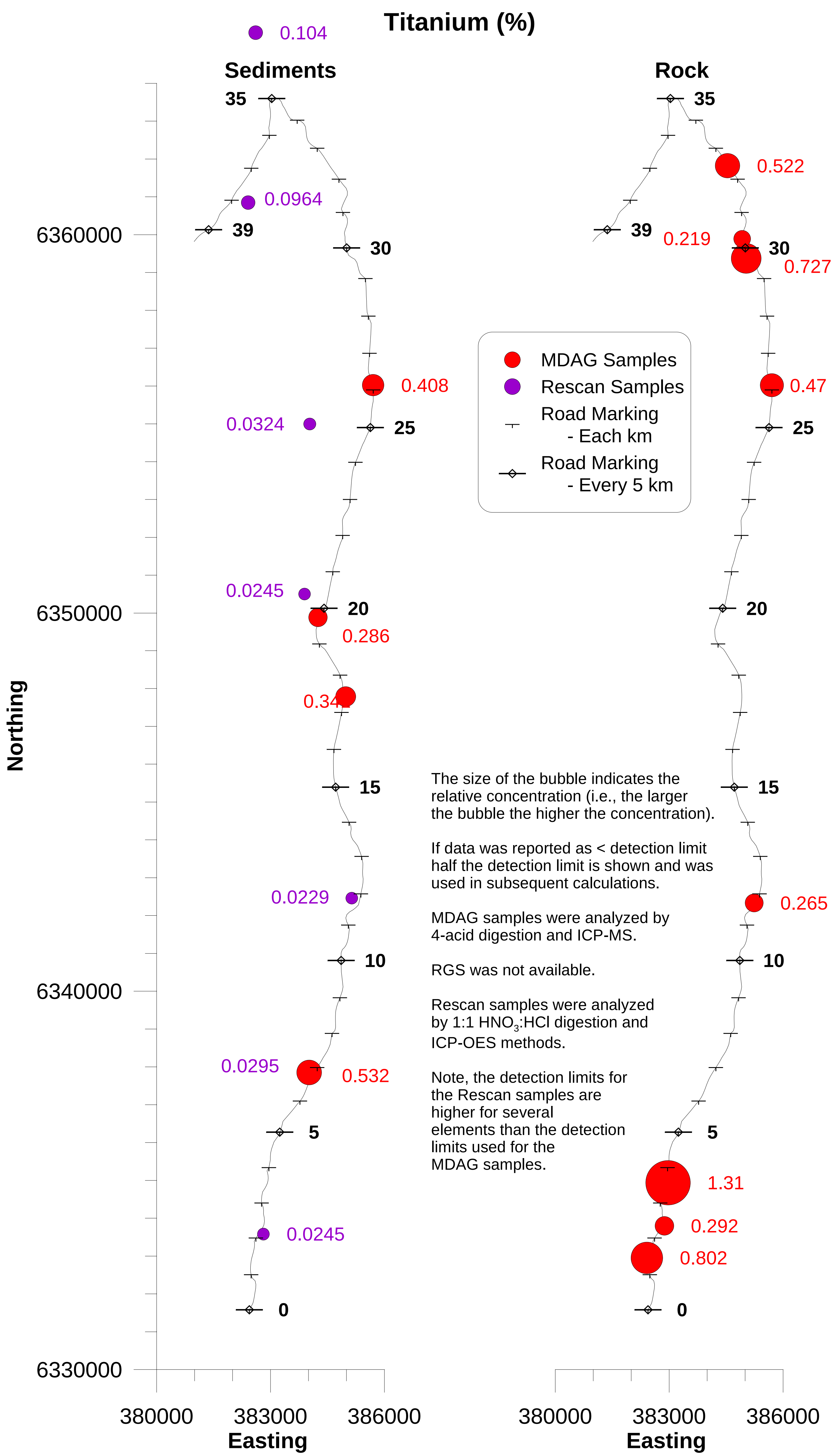
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan data is not shown due to the high minimum detection limits used.

Note, the detection limits for both the RGS samples are higher for several elements than the detection limits used for the MDAG samples.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

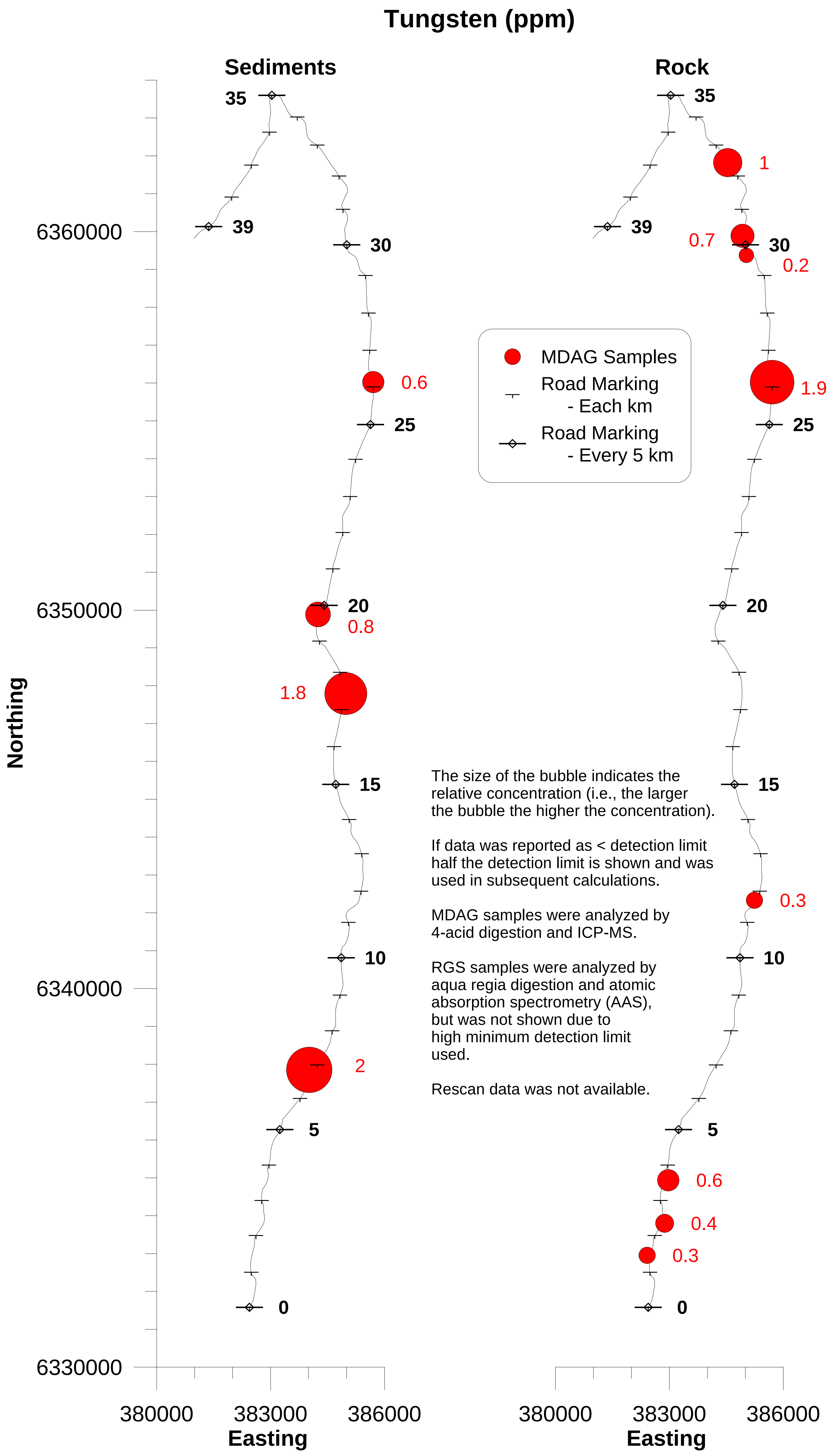
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS was not available.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for the Rescan samples are higher for several elements than the detection limits used for the MDAG samples.



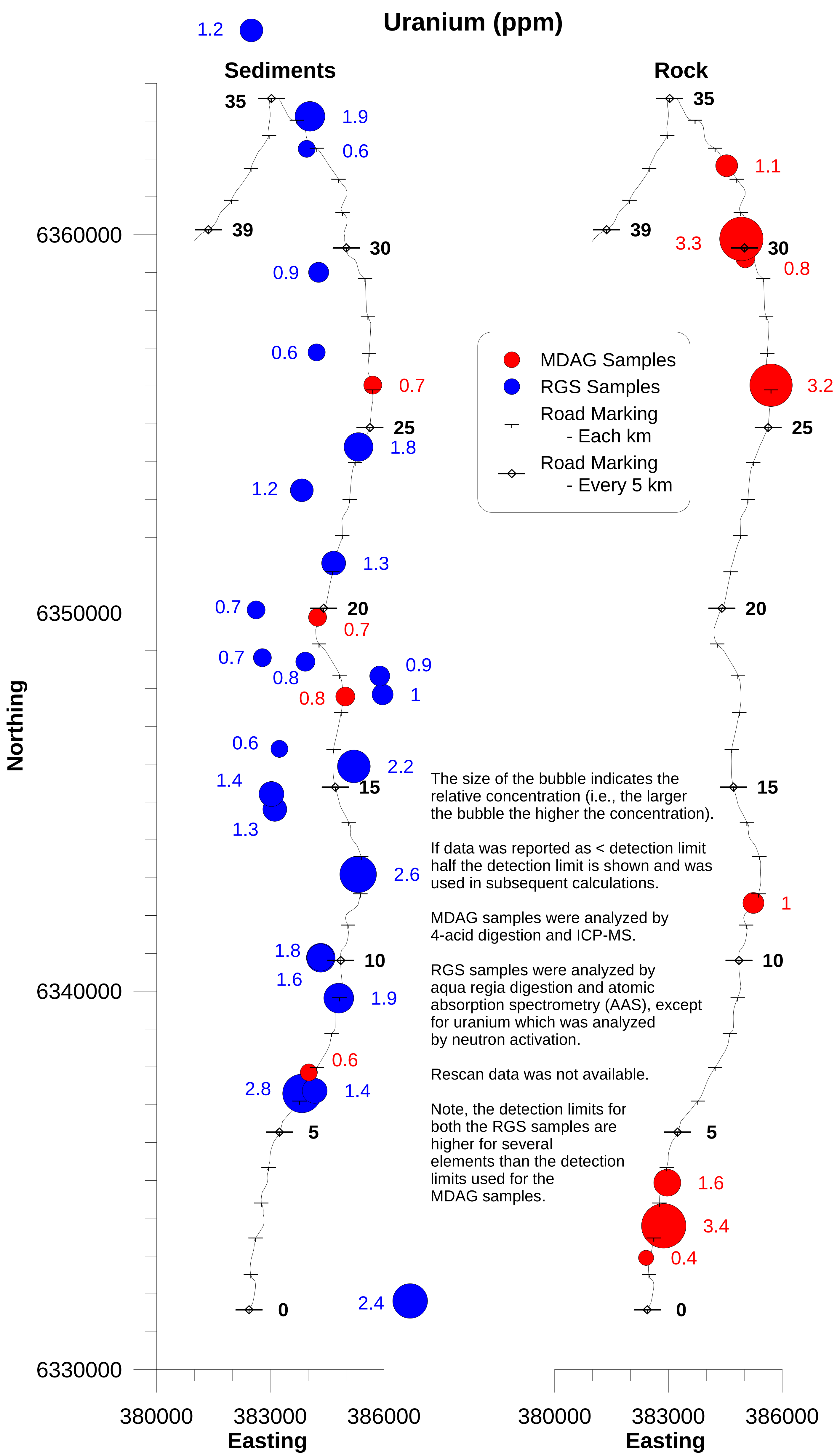
The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), but was not shown due to high minimum detection limit used.

Rescan data was not available.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

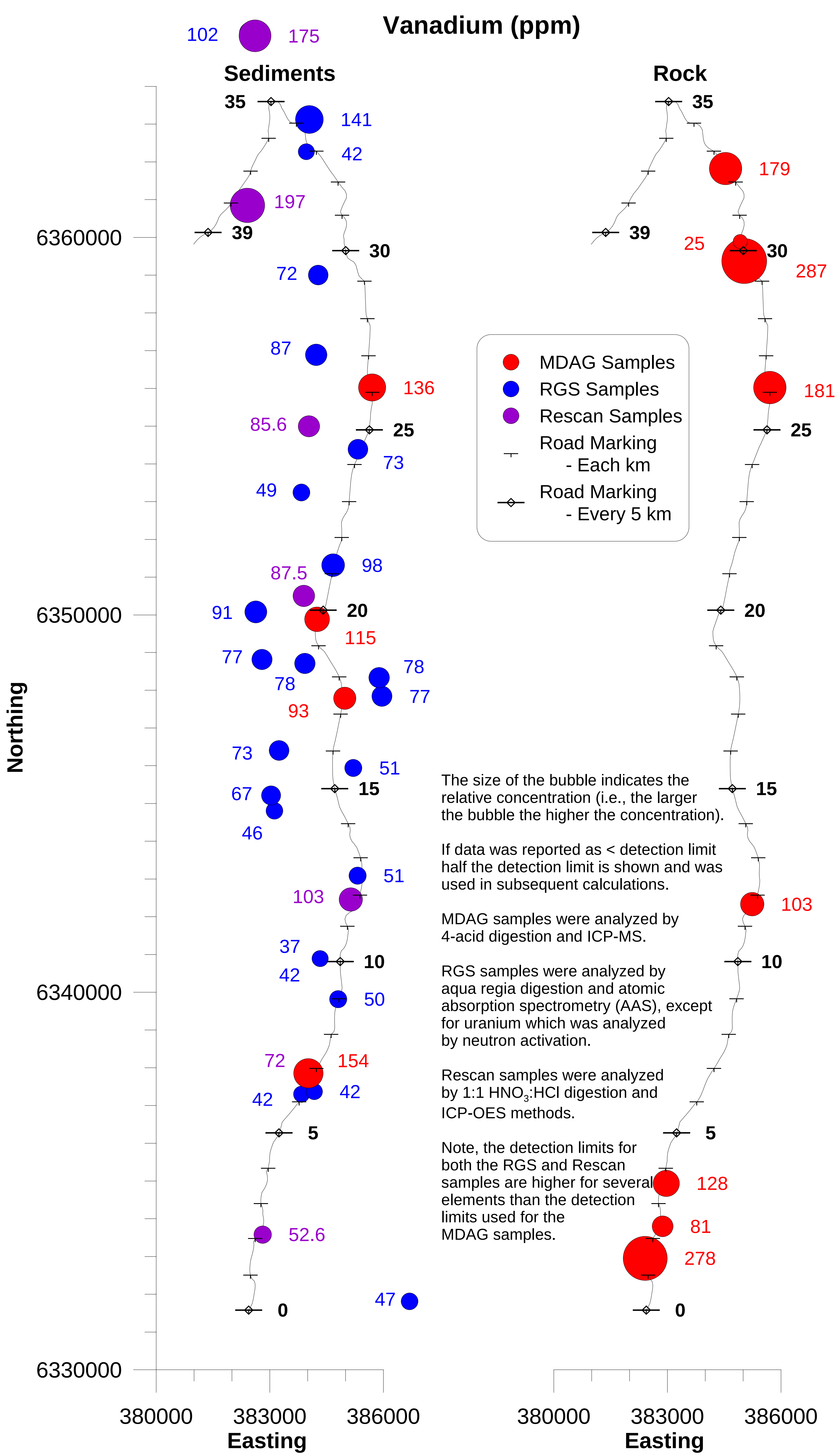
If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan data was not available.

Note, the detection limits for both the RGS samples are higher for several elements than the detection limits used for the MDAG samples.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

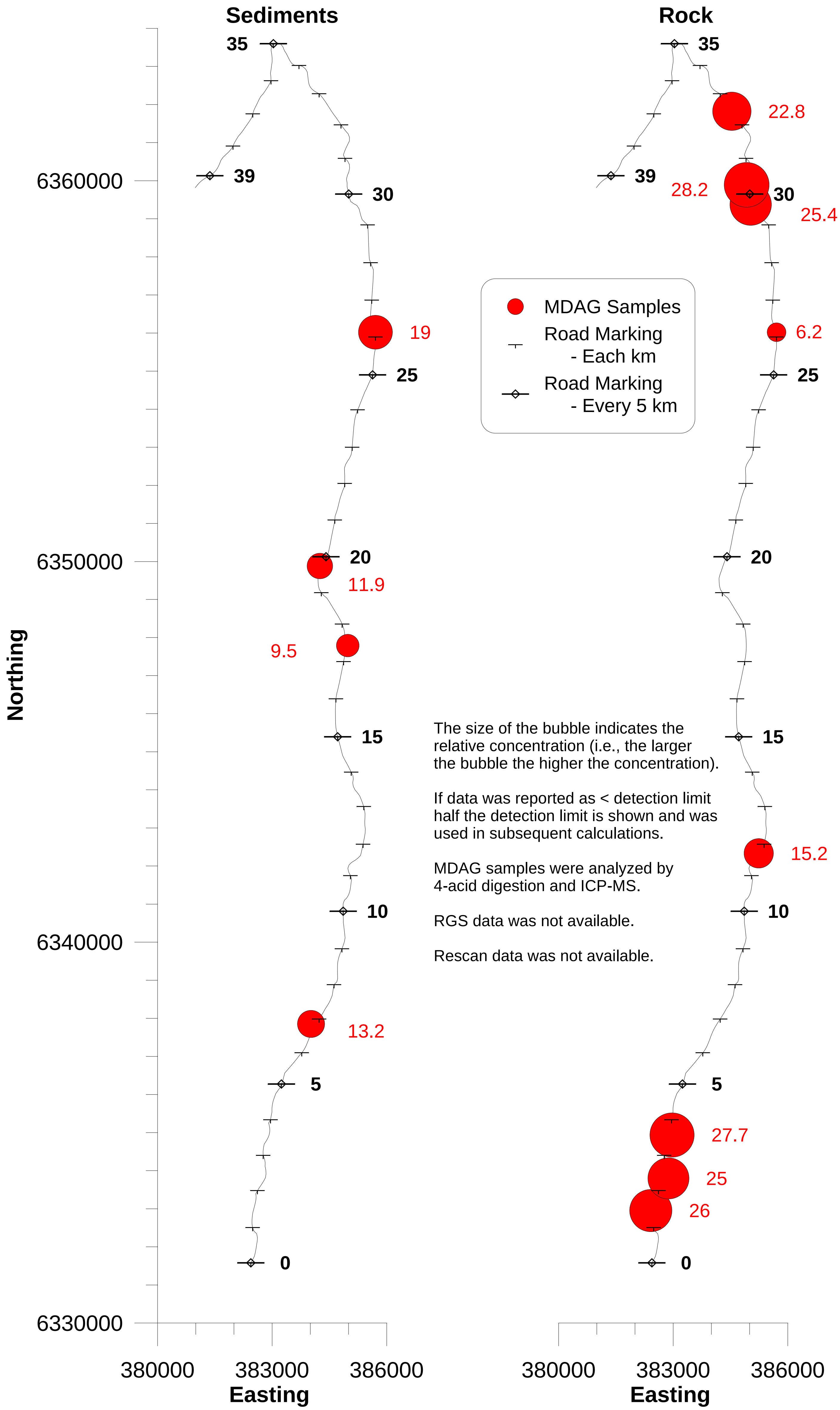
MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for both the RGS and Rescan samples are higher for several elements than the detection limits used for the MDAG samples.

Yttrium (ppm)



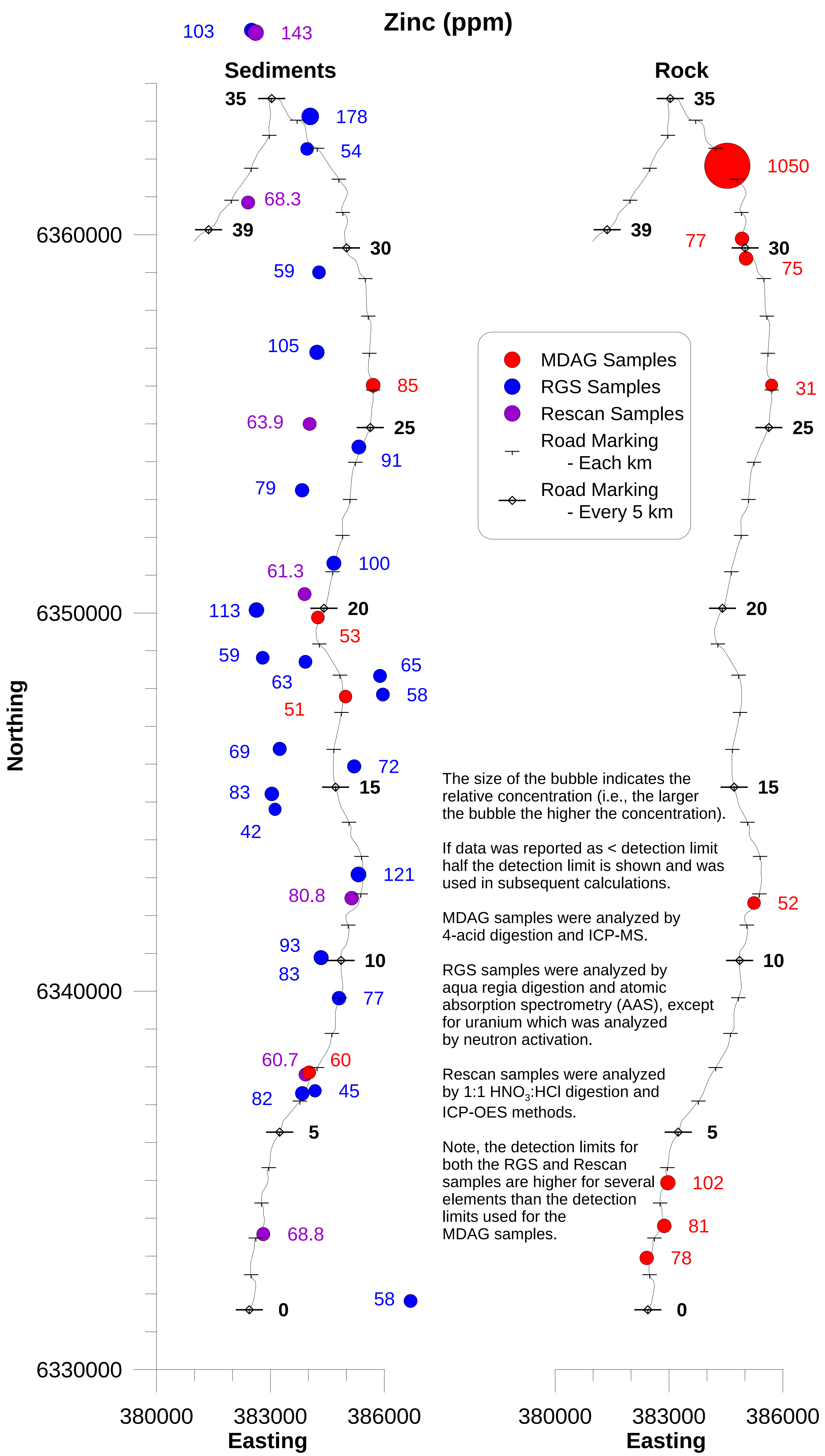
The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

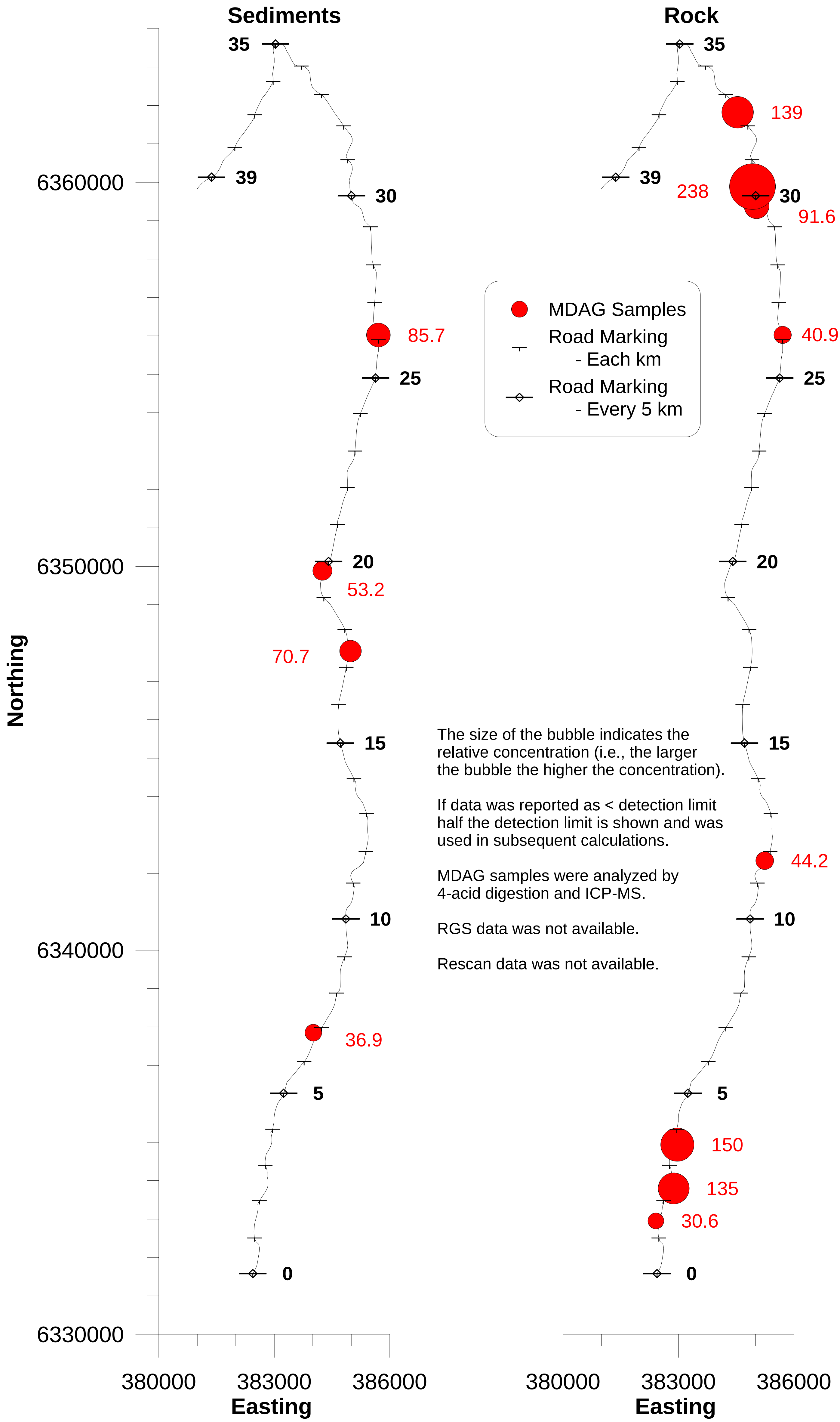
MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS samples were analyzed by aqua regia digestion and atomic absorption spectrometry (AAS), except for uranium which was analyzed by neutron activation.

Rescan samples were analyzed by 1:1 HNO_3:HCl digestion and ICP-OES methods.

Note, the detection limits for both the RGS and Rescan samples are higher for several elements than the detection limits used for the MDAG samples.

Zirconium (ppm)



The size of the bubble indicates the relative concentration (i.e., the larger the bubble the higher the concentration).

If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

MDAG samples were analyzed by 4-acid digestion and ICP-MS.

RGS data was not available.

Rescan data was not available.

Schaft Creek Project - Prediction of Metal Leaching and Acid Rock Drainage, Phase 1

prepared for:

Rescan Environmental Services Ltd.
Attn: Mr. Shane Uren
Sixth Floor,
1111 West Hastings Street.
Vancouver, British Columbia V6E 2J3

prepared by:

Kevin A. Morin, Ph.D., P.Geo., L.Hydrogeo.
Nora M. Hutt, A.Sc.T, c.C.T.
Minesite Drainage Assessment Group
A Division of Morwijk Enterprises Ltd.
8035 Redtail Court,
Surrey, British Columbia V3W 0N4

August 10, 2007

P.Geo. and A.Sc.T. Notice

This study is based on detailed technical information interpreted through standard and advanced chemical and geoscientific techniques available at this time. As with all geoscientific investigations, the findings are based on data collected at discrete points in time and location. In portions of this report, it has been necessary to infer information between and beyond the measured data points using established techniques and scientific judgement. In our opinion, this report contains the appropriate level of geoscientific information to reach the conclusions stated herein.

This study has been conducted in accordance with British Columbia provincial legislation as stated in the Engineers and Geoscientists Act and in the Applied Science Technologists and Technicians Act.

Kevin A. Morin, Ph.D., P.Geo.
Registration No. 18,721
Association of Professional
Engineers and Geoscientists

Nora M. Hutt, A.Sc.T., c.C.T.
Registration No. 10700
Association of Applied Science
Technologists and Technicians

TABLE OF CONTENTS

List of Tables

List of Figures

Executive Summary

This first-phase report predicts metal leaching (ML) and acid rock drainage (ARD) at Copper Fox Metal's Schaft Creek Project. As specified in the British Columbia Policy, Guidelines, and draft Prediction Manual, ML-ARD predictions are being developed in phases, with each phase focussing on resolving uncertainties identified in earlier phases. It is too early at this stage to reach any major or clear conclusions about ML-ARD potential.

In this first phase of ML-ARD testing, 59 samples of core rejects from the 2005 drilling program were submitted for expanded Sobek (EPA 600) acid-base accounting and for total-element analyses. Some major observations were:

- Previous observations of weathered core reported little evidence of oxidation and reaction.

- Schaft Creek rock contains abundant aluminosilicate minerals, which can provide some neutralization in addition to carbonate minerals.

- Based on the 59 core samples and generic criteria, only 0-2% of the samples were net acid generating and 5-14% were currently "uncertain", and thus most samples were net neutralizing. Additional testwork is needed to resolve the ARD status of the uncertain samples, and to examine other portions of the deposit.

- Although up to 2% of samples were net acid generating, none were acidic at the time of analysis, and years to decades may have to pass before they became acidic.

- Compared to general crustal abundances, the 59 samples were frequently elevated in silver, bismuth, copper, molybdenum, and selenium, and occasionally elevated in sulphur, antimony, and tungsten. However, solid-phase levels do not typically reflect leaching rates into water, so additional testwork is needed on metal leaching.

Recommendations were offered to improve the accuracy and to reduce the uncertainty in the current ML-ARD predictions for the Schaft Creek Project.

Report Summary

Whenever mined rock is exposed to air and moisture, the rates of weathering, oxidation, and leaching can accelerate. If sulphide minerals like pyrite are exposed, the oxidation will release acidity, some metals, sulphate, and heat. If the acidity is not neutralized by minerals like calcite or feldspar in the rock, the resulting acidic water is called "acid rock drainage" (ARD) in British Columbia. Whether sulphide minerals are present or not, weathering can still lead to accelerated metal leaching (ML). For example, the simple dissolution of carbonate minerals can release metals like manganese.

The provincial ML-ARD Policy, Guidelines, and draft Prediction Manual contain the recommendations and the expectations of the government for ML-ARD prediction and control. One recommendation is that ML-ARD studies are carried out in phases, with each phase focussing on the uncertainties identified in the previous ones.

This report contains the first phase of ML-ARD studies for the Schaft Creek Project. Previous relevant information was compiled. Also, 59 samples of core rejects, from 11 holes drilled in 2005, were collected from cold storage. This set included two duplicates for QA/QC checks. All 59 samples were analyzed for expanded Sobek (EPA 600) acid-base accounting, and for total-element contents using ICP-MS after four-acid digestion and using x-ray fluorescence whole rock.

Previous Information

The compilation of existing information relevant to ML-ARD led to the following important observations.

- The Schaft Creek copper-gold-molybdenum deposit is widely acknowledged as a porphyry copper deposit. It contains three mineral zones: the Liard, West Breccia, and Paramount Zones.

- During an examination of existing core, "It has been noted that the core from previous drilling programs, which is stored on site, exhibits a remarkable degree of preservation with limited visible weathering." Thus, the oxidation rate of Schaft Creek rock may be relatively slow.

- Based on 16 acid-base accounts from a previous, metallurgical study, all 16 samples were net acid neutralizing, with sulphide between 0.1 and 0.9%S, and Neutralization Potentials from 53 to 114 kg/t. Flotation recovery of sulphide reduced the sulphide levels in the synthetic tailings.

- Detailed mineralogy was examined in 18 thin sections, representing feldspar quartz porphyry (rock code PPFQ), tourmaline breccia, pneumatolytic breccia, and volcanics. Even one rock unit (PPFQ) was not entirely intrusive. Some PPFQ samples were porphyritic volcanics of felsic and intermediate composition (dacitic - andesitic), and one sample was a fine grained, feldspathic intrusive rock classified as either syenite or anorthosite, depending on the composition of feldspar. Groundmass in these samples was generally around one-half of the total, with the groundmass consisting of more than 90% feldspar, and accessory amounts of quartz, chlorite, sericite, carbonate, and opaques. Sulphide minerals were mostly disseminated and as veinlets and clusters, and mostly pyrite and chalcopyrite with less common molybdenite and bornite. Carbonate minerals, mostly reported as veins, patches, and groundmass, were not individually identified and were sometimes seen as feldspar replacement/alteration.

Results of Acid-Base Accounting (ABA)

As part of the ABA procedure, paste pH is measured in a mixture ("paste") of pulverized sample and deionized water. Paste pH in the 59 core samples for Schaft Creek ranged from 7.6 to 8.6. Thus, no samples were acidic at the time of analysis.

Total sulphur in the 59 Schaft Creek rock samples ranged from 0.02 to 1.91%S, with a mean of 0.45%S and a median of 0.26%S. In most samples, total sulphur and sulphide were similar, and thus the two parameters were typically interchangeable. Because a few samples did contain elevated leachable sulphate, sulphide is a better indicator of acid potential than total sulphur for Schaft Creek rock. However, in many samples, most sulphide was copper-bound sulphide (chalcopyrite) which may have less capacity to generate acidity. Therefore, each sample has a maximum "worst-case" Sulphide-Based Acid Potential (SAP) and a minimum "best-case" Pyrite-Calculated Acid Potential (PAP).

Sobek (EPA 600) Neutralization Potential (NP) ranged from 40 to 219 kg/t in the 59 Schaft Creek samples, with a mean of 97 and a median of 92 kg/t. These are relatively high values. They explain why no acidic paste pH values were detected, and suggest there could be a long lag time (years to decades) before these samples might become acidic. A certain amount of measured NP is typically "unavailable" for neutralization, and thus should be subtracted from measured values. The lack of acidic paste pH values precluded an initial estimate of Unavailable Neutralization Potential, so the common value of 10 kg/t is used here. NP was typically greater than inorganic carbonate in many samples, meaning NP also reflected the presence of non-carbonate aluminosilicate minerals. These minerals have been documented in Schaft Creek rock. Also, NP did not correlate well with solid-phase calcium plus magnesium levels, but some samples showed that calcium-bearing minerals could account for their NP levels.

Best-case and worst-case net balances of acid-generating and acid-neutralizing capacities were calculated for each of the 59 Schaft Creek samples. Overall, only 0-2% of the samples were net acid generating and 5-14% were "uncertain" based on generic criterion. Thus, most samples were net neutralizing. PPAU and PPFQ were the major rock units with uncertain samples, while net-acid-generating or uncertain samples were found in the minor rock units of ANDS, TOBR, BRIV, and DIOR.

To generally assess the spatial distribution of net balances, a general east-west cross-section showed the center area was net-neutralizing, while net-acid-generating and uncertain samples were found on the periphery. The general north-south cross-section showed uncertain samples were found in three adjacent holes. Based on this limited information, the net-acid-generating and uncertain samples may be spatially restricted in the Schaft Creek Deposit, but additional samples and geostatistical modelling are needed to confirm this.

Results of Total-Element Analyses

Total-element levels in the 59 Schaft Creek samples were measured by ICP-MS analysis after strong four-acid digestion and by x-ray-fluorescence whole-rock analysis. The 59 samples of Schaft Creek core were predominantly composed of silicon and aluminum, reflecting the abundant aluminosilicate minerals. Calcium, iron, potassium, magnesium, sodium, and Loss on Ignition (LOI) were also relatively abundant. Compared to general crustal abundances, the 59 samples were frequently elevated in silver, bismuth, copper, molybdenum, and selenium, and occasionally elevated in sulphur, antimony, and tungsten. However, solid-phase levels do not typically reflect leaching rates into water, so additional testwork is needed on metal leaching. Only copper showed some correlation with sulphide, reflecting the copper-bound sulphide discussed under Acid-Base Accounting. For Sobek Neutralization Potential, calcium showed some correlation. Samples of some rock units, particularly tourmaline breccia (TOBR), stood out as a distinct group for some elements like gallium, phosphorus, thallium, tungsten, and uranium.

Recommendations for Future ML-ARD Work

A phased approach, with each focussing on resolving uncertainties raised in previous ones, is recommended in the provincial ML-ARD Prediction Manual. Thus, based on the preceding initial information, we offer the following recommendations for the next phase of ML-ARD studies at the Schaft Creek Project.

- Overburden should be analyzed for ML-ARD potential. Up to several tens of meters of overburden have been reported in drillholes. This overburden in the pit area would be disturbed and oxidized during mining, and might be used for reclamation during and after operation.

- Unavailable Neutralization Potential (UNP) could not be reliably estimated from available data (Section 4.1.3), but affects net balances. Therefore, UNP should be determined better for Schaft Creek. This would likely require humidity cells (see below).

- Most samples with NPR < 2 were between 1.0 and 2.0, meaning their ARD potential is “uncertain” at this time (Section 4.1.5). This uncertain range should be resolved for proper planning of waste management and water management. Humidity cells would help with this (see next recommendation).

- Six laboratory-based kinetic tests, known as humidity cells, should be conducted for at least 40 weeks on 1-kg samples of Schaft Creek rock. These would provide bulk rates of acid generation, neutralization, and metal leaching, and would help in resolving UNP and “uncertain” samples (see above). Previous information on weathered core suggested reaction rates in Schaft Creek rock were low.

- Four on-site leach tests, each containing up to approximately one tonne of disturbed rock or broken core, should be set up at Schaft Creek and periodically sampled as part of routine on-site water-quality monitoring. These would provide on-site drainage-chemistry data and are important for upscaling the smaller-scale humidity cells.

- At this time, the net-acid-generating and "uncertain" samples may be clustered in portions of the deposit, which would focus waste management and any special handling onto specific zones. To examine this clustering further, additional core samples, including 2006 holes, should be collected from across the deposit and submitted for expanded acid-base accounting and total-element contents. The results would be used in geostatistical modelling (see next recommendation).

- Three-dimensional geostatistical modelling should be carried out to calculate total tonnages and year-by-year tonnages of net-acid-generating, currently "uncertain", and net-neutralizing rock. This is important for identifying the most cost-effective options for waste management and water management.

1. INTRODUCTION

Whenever mined rock is exposed to air and moisture, the rates of weathering, oxidation, and leaching can accelerate. If sulphide minerals like pyrite are exposed, the oxidation will release acidity, some metals, sulphate, and heat. If the acidity is not neutralized by minerals like calcite or feldspar in the rock, the resulting acidic water is called "acid rock drainage" (ARD) in British Columbia.

Whether sulphide minerals are present or not, weathering can still lead to accelerated metal leaching (ML). For example, the simple dissolution of carbonate minerals can release metals like manganese.

ML-ARD is often associated with minesites, where it is well documented (e.g., Morin and Hutt, 1997 and 2001). As a result, the accurate prediction and control of ML-ARD at minesites in British Columbia are high priorities of the provincial government, as explained in its formal Policy, Guidelines, and draft Prediction Manual (Price and Errington, 1998; Price, 1998; Price et al., 1997). This report follows the recommendations of those documents.

Because the provincial documents recommend a phased approach, this report compiles and interprets the currently existing information related to ML-ARD at the Schaft Creek Project. General background information is provided in Chapter 2. The ML-ARD samples, and the static analyses applied to them, are described in Chapter 3. The analytical results are discussed in Chapter 4. Chapter 5 concludes with recommendations for the next phase of ML-ARD work, including additional testwork as discussed in the provincial Prediction Manual. All relevant data are compiled in the appendices.

2. GENERAL INFORMATION AND PREVIOUS ML-ARD-RELATED STUDIES

The information presented below has been extracted mostly from the Project Description (Copper Fox Metals Ltd., 2006), a resource estimate by Giroux and Ostensoe (2003), and the 2005 drilling report (Fischer and Hanych, 2006).

2.1 Location and History

The Schaft Creek property is located in the mountainous terrain of northwestern British Columbia, approximately 1,000 km northwest of Vancouver. The area is located 80 kilometers southwest of Telegraph Creek and approximately 76 kilometers west of the Stewart-Cassiar paved highway (Highway 37). The mineral claims of interest are situated near the headwaters of Schaft Creek, a tributary of Mess Creek, which flows into the Stikine River downstream of the community of Telegraph Creek.

Schaft Creek is located in the coastal climate zone of British Columbia and is characterized by cool summers and cold humid winters. Elevations on the property range from 500 to 2,000 m above sea level. Average annual precipitation is estimated to be 640 mm or roughly 84% greater than that recorded at Telegraph Creek. Temperatures are strongly influenced by the Coast Mountains and may range from above +20°C in the summer to below -20°C in winter.

The Schaft Creek copper-gold-molybdenum-silver prospect was identified in 1957 by prospector Nick Bird while employed by the BIK Syndicate. Three diamond drill holes were drilled to moderate depths. Sample results from two of the holes returned sufficient copper values and resulted in further work. The prospecting syndicate was re-organized in 1966 into Liard Copper Mines Ltd. (“ Liard”) with Silver Standard Mines Limited, holding a 66% interest, acting as the manager. In 1966 ASARCO obtained an option to explore the Liard Copper Mines Ltd. ground and carried out geological and induced polarization surveys. The program included drilling 10,939 feet (3,335 metres) over 24 holes. The option was not maintained despite encouraging drill results and in 1968 Hecla Mining Company of Canada Ltd., a subsidiary of Hecla Mining Company of Wallace, Idaho, entered an option agreement to earn a 75% property interest and commenced drilling and other exploration work with Hecla operating company as its agent.

From 1968 through 1977, Hecla completed a total of 34,500 metres of diamond drilling, 6,500 metres of percussion drilling, induced polarization and resistivity surveys, geological mapping, air photography, and engineering studies related to the development of a large open pit copper-gold-molybdenum mine. In 1978 Wright Engineers Ltd. was contracted by Hecla to update a preliminary feasibility assessment initially completed in 1970. Exploration work at the property ceased in 1977 and in 1978 Hecla sold its interest to Teck Corporation (“Teck”) (now Teck Cominco Limited).

In 1980 Teck commenced a program of exploration and drilling designed to confirm and expand Hecla’s work. A total of 26,000 metres of diamond drilling was completed by 1981. Teck then undertook an engineering study to determine the feasibility of mine development. Further data reviews were completed by Western Copper Holdings in 1988 and Teck in 1993. A total of 230 core holes with a total length of 60,200 metres and percussion holes with total length 6,500 metres have been completed at the Schaft Creek property. Copper Fox Metals has completed 15 large diameter (PQWL) drill holes across the Main Liard and West Breccia zones for a total of 3,161 meters. A total of 50,000 pounds of core is presently undergoing geological assessment and reporting before metallurgical testing of this new core is initiated.

The feasibility work completed on the Schaft Creek site has been focussed on the development of an open pit within the Liard Zone. The present plan would see mining of up to 70,000 tonnes per day of ore using conventional drill and blast mining methods with a maximum estimated strip ratio of 1.13.

2.2 Geology

The Schaft Creek copper-gold-molybdenum property is located in the northern part of the Intermontane Belt of the Canadian Cordillera. It is part of the northwesterly trending suite of porphyry-style mineral deposits that extends in Canada from the Copper Mountain/Ingerbelle deposit near the southern International Boundary to Casino in west-central Yukon. Globally, such deposits typically exhibit a few characteristics in common and many variations.

The Schaft Creek copper-gold-molybdenum deposit is hosted principally by Upper Triassic age volcaniclastic rocks. They have been variously altered and disrupted by emplacement of feldspar porphyry dykes and, possibly, sills and by several northwest-trending faults. Augite porphyry basalt is present in proximity to the west of the deposit area and also in the Liard mineral zone but its relationship to mineralization has not been determined. The mineralized area is, arguably, in fault contact, or disconformably or unconformably overlain by unmineralized, comparatively unaltered and undisturbed purple weathering andesitic volcanic rocks. Geological mapping at surface, aided by diamond drill core information, has failed to reveal any strong overall pattern of stratigraphic or petrologic controls to mineralization.

The Schaft Creek copper-gold-molybdenum deposit is widely acknowledged as being a porphyry copper deposit. The deposit consists of three distinct but connected zones: (a) the Liard (Main) zone hosted mainly by andesite flows and epiclastic rocks; (b) the West Breccia zone, a faultbounded tourmaline-sulphide matrix breccia; and (c) the Paramount zone, an intrusive breccia in altered andesite, granodiorite and quartz monzonite.

> The broad, northerly plunging Liard, or Main, zone extends 1,000 metres in a northerly direction, 700 metres east-west, and has average thickness of 300 metres. It is a weakly altered stockwork system in volcanics (andesite flows and fragmentals) with minor felsic intrusive dykes carrying disseminated sulphide mineralization. A pyrite halo surrounds chalcopyrite, bornite and molybdenite mineralization in altered and faulted andesite. The zone has a low grade phyllic core and to the northwest is progressively down dropped on faults.

The West Breccia zone exhibits tourmaline, silicification and sericitization and is controlled by north-trending faults. Mineralization is contained within tourmaline and sulphide rich hydrothermal breccia. The Zone has a length of 500 metres, averages 100 metres in width and has been drilled to depths greater than 300 metres. Pyrite is the principal sulphide mineral, with lesser quantities of chalcopyrite and molybdenite. Copper and molybdenum contents are erratic but often high.

The Paramount zone of intrusive breccia occurs in granodiorite and quartz monzonite and has dimensions of 700 metres length, 200 metres width and +500 metres thickness. Exploration to the north has been constrained by practical considerations: rapidly increasing thicknesses of overlying apparently barren purple volcanic rocks challenge drilling methods and mitigate against practical conceptual open pit designs. The mineralization is contained in an intrusive breccia in altered andesite, granodiorite and quartz monzonite. Pyrite, bornite and chalcopyrite are present in equal proportions and molybdenite values exceed those found in the other two zones.

Additional information comes from the provincial Minfile website (http://minfile.gov.bc.ca/Summary.aspx?minfilno=104G++015):

“Mineralization occurs partly within a basin-like structure of fragmental and undivided green andesites, 900 metres in diameter. The basin is intruded by augite porphyry basalt and by vertical north striking quartz diorite dykes. A breccia cuts the western edge of the basin and trends north for at least 2700 metres. Post-mineralization mafic dykes are common. Later flat-lying fragmental purple andesites unconformably overlie the northeastern part of the deposit.

“In general, pyrite, chalcopyrite, bornite and molybdenite occur predominantly in fractured andesites. Less than 10 per cent of the mineralization occurs in felsic intrusives. Pyrite and bornite are mutually exclusive and most of the main deposit occurs within the bornite zone, with pyrite on the periphery. A barren zone, which contains no sulphides, conformably underlies the main deposit.

“Feldspathization and hydrothermal alteration are associated with mineralization. A quartz vein stockwork with biotite and some potassium feldspar coincides with the low-grade core of the main deposit. The biotite has a potassium/argon age of 182 Ma +/- 5 Ma. Epidote appears abruptly near the boundaries of the main deposit. Most mineralization occurs in an intermediate zone marked by chlorite- sericite alteration and the absence of epidote. Tourmaline and gypsum are locally abundant.

“The distribution of most sulphide minerals is fracture-controlled. They occur in dry fractures or combined with quartz or quartz-calcite veinlets within the andesitic volcanics. The sulphides within the felsic intrusives are usually disseminated and seem to have replaced the mafic minerals. Trace amounts of covellite, chalcocite, tetrahedrite and native copper have been identified. Minor amounts of galena and sphalerite occur in the breccia zone and in small calcite veins. Gold and silver are associated with the sulphides and average 0.34

grams per tonne and 1.71 grams per tonne, respectively."

2.3 Past ML-ARD-Related Work

During an examination of existing core, Associated Mining Consultants Ltd. (2004) observed, "It has been noted that the core from previous drilling programs, which is stored on site, exhibits a remarkable degree of preservation with limited visible weathering."

Also, after a visual assessment of the integrity of the core samples, Associated Mining Consultants Ltd. (2004) selected 16 samples for assay validation based on prior documentation of assays, lithology, and spatial distributions. These 16 samples selected were subjected to standard Acid-Base accounting procedures to assess any acid generation and environmental impact concerns (Table 2-1). Because only statistical summaries but no individual analyses were presented, these analyses were not added to the Phase 1 database in this study (Appendix B).

Table 2-1. Statistical Results of Previous Acid-Base Accounting for Sixteen Samples (from Associated Mining Consultants Ltd., 2004)

Parameter	Average	Range
Sulphide (%S)	0.43	0.1-0.9
Paste pH	8.8	7.5-9.3
Acid Potential (kg $CaCO_3$ eq/tonne)	13.4	3.4-28.6
Neutralization Potential (kg $CaCO_3$ eq/tonne)	75.5	53-114
Net Potential Ratio (NPR or NP/AP)	7.36	3.0-16.9
Net Neutralization Potential (NP-AP, kg $CaCO_3$ eq/tonne)	+62.2	+45 to +91

Then, five samples were selected from the suite of 16 for metallurgical validation using standard batch grinding and rougher flotation procedures for sulphides. The five samples selected for metallurgical validation were taken from drill holes H61, T182, T186, T172, and T176.

Based on all this work, Associated Mining Consultants Ltd. (2004) concluded,

> "The mineralogy is unlikely to pose acid generation concerns based on the analysis of the 16 selected core samples. Acid-Base accounting results indicated an excess neutralization potential of over twice the estimated acid potential in all cases and the paste pH ranged from neutral to alkaline. With the low head sulphide content in the samples to start and high flotation recoveries, the total sulphur in the tailings was reduced to below 0.03% to further reduce concerns on environmental impact."

As an addendum to Fischer and Hanych (2006), mineralogy was visually determined, using thin-section petrography, on 18 samples. This work focussed on feldspar quartz porphyry (rock code PPFQ, Table 3-1), with a few samples from tourmaline breccia, pneumatolytic breccia and volcanics. It was not meant to be representative of the Schaft Creek lithologic suite. Major observations from this work follow.

“- Not all samples logged as PPFQ are intrusives. Some are porphyritic volcanics of felsic and intermediate composition (dacitic - andesitic); one sample is a fine grained, feldspathic intrusive rock classified as either syenite or anorthosite, depending on the composition of feldspar.

- All rocks classified as FQP [PPFQ] are porphyritic, felsic, massive igneous rocks.
- All have plagioclase as the predominant phenocryst mineral. Quartz phenocrysts ('quartz eyes') are relatively rare, very subordinate to plagioclase phenocrysts.
- A few samples have no quartz phenocrysts (quartz eyes) and therefore are feldspar porphyry.
- Ferromagnesian ('Femag') phenocrysts are consistently completely replaced by secondary minerals, generally chlorite and accessory leucoxene, opaques, in places by sericite and skeletal fine grained opaques and highly refracting brown minerals.
- The groundmass makes up a variable portion of the rock, generally ½.
- The groundmass consists of >90% feldspar, and accessory amounts of quartz, chlorite, sericite, carbonate, opaques.
- The groundmass in all cases is fine grained to very fine grained, generally 100 to 200 microns (0.1 - 0.2 mm) grain size, in some samples extremely fine grained (20 - 50 microns). Differences in grain size of the groundmass feldspar is noticeable and attributed to varying cooling rates.
- The shape of groundmass feldspar and other minerals is generally anhedral, interlocking. Lathy and feathery feldspar are rare but were observed.
- Only accessory amounts of fresh potassic feldspar (microcline) and albite were observed in some feldspar-quartz-porphyries and are interpreted as very limited, secondary, potassic alteration.
- The common pink to orange colour of the samples is attributed to ubiquitous micron-size sericite grains within plagioclase phenocrysts and to a lesser degree in groundmass feldspar. It is pointed out that 'sericite' is a synonym for fine grained muscovite which is a potassic phyllosilicate. It appears justified to describe this partial alteration as 'potassic'.
- Fast cooling of the liquid that formed the groundmass is interpreted for all Liard Zone FQP samples. This is in contrast to the grains size of the interstitial minerals in the Hickman /Yeheniko samples which are medium grained (0.3 - 1 mm)
- This fast cooling of the inter-phenocryst liquid can be interpreted either as due to relatively small intrusive bodies or surface-near (subvolcanic) bodies.
- Alteration is weak to moderate. Mostly sericite, minor carbonate, chlorite, rare potassic, i.e., microcline.
- Sulphides in feldspar-quartz-porphyry and volcanics occur both in veins; and as disseminations, associated with hairline fractures and grain boundaries, and with minor quartz, carbonate, chlorite and sericite.

Other observations from the individual thin sections include:

- Undifferentiated plagioclase was typically the major mineral, with fine-grained sericite and quartz often significant.
- Sulphide minerals were mostly disseminated and as veinlets and clusters, and mostly pyrite and chalcopyrite with less common molybdenite and bornite
- Pyrite was typically 0.05-1.0 mm in size as subhedral to anhedral grains, but variable among samples.
- Carbonate minerals, mostly reported as veins, patches, and groundmass, were not individually identified and were sometimes seen as feldspar replacement/alteration.

2.4 Important ML-ARD Observations from Previous Studies

Based on the preceding subsections, important observations pertaining to ML-ARD were:

- The Schaft Creek copper-gold-molybdenum deposit is widely acknowledged as being a porphyry copper deposit. It contains three mineral zones: the Liard, West Breccia, and Paramount Zones.

- During an examination of existing core, “It has been noted that the core from previous drilling programs, which is stored on site, exhibits a remarkable degree of preservation with limited visible weathering.” Thus, the oxidation rate of Schaft Creek rock may be relatively slow.

- Based on 16 acid-base accounts from a previous, metallurgical study, all 16 samples were net acid neutralizing, with sulphide between 0.1 and 0.9%S, and Neutralization Potentials from 53 to 114 kg/t. Flotation recovery of sulphide reduced the sulphide levels in the synthetic tailings.

- Detailed mineralogy was examined in 18 thin sections, representing feldspar quartz porphyry (rock code PPFQ), tourmaline breccia, pneumatolytic breccia, and volcanics. Even one rock unit (PPFQ) was not entirely intrusive. Some PPFQ samples were porphyritic volcanics of felsic and intermediate composition (dacitic - andesitic), and one sample was a fine grained, feldspathic intrusive rock classified as either syenite or anorthosite, depending on the composition of feldspar. Groundmass in these samples was generally around one-half of the total, with the groundmass consisting of more than 90% feldspar, and accessory amounts of quartz, chlorite, sericite, carbonate, opaques. Sulphide minerals were mostly disseminated and as veinlets and clusters, and mostly pyrite and chalcopyrite with less common molybdenite and bornite. Carbonate minerals, mostly reported as veins, patches, and groundmass, were not individually identified, and were sometimes seen as feldspar replacement/alteration.

3. SAMPLING AND ANALYSIS

3.1 Sample Selection and Collection

Based on the 2005 diamond-drillhole Report (Fischer and Hanych, 2006), the important rock units and their total footages in the core are listed in Table 3-1. Results from the 2006 drilling program were not available for this Phase 1 study, and were thus not included here.

Table 3-1. Important Rock Units and Their Observed Abundances in 2005 Drill Core (based on Fischer and Hanych, 2006)

Rock-Unit Code	Description	Percentage of Footage in 2005 Core
PPAU	Plagioclase-Augite-phyric Andesite	32.1%
ANPL (and ANLP)	Andesitic Lapilli Tuff	19.6%
ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	14.4%
PPFQ	Quartz-Feldspar or Feldspar-Quartz Porphyry	6.6%
ANDS	Andesite	4.5%
BRVL	Volcanic Breccia	4.4%
TOBR	Tourmaline Breccia	4.2%
FAUL and SHER	Faults, and Shear Zone / Faults	3.7%
PPPL	Plagioclase or Feldspar Porphyry	3.0%
ANTF	Andesitic Tuff	2.1%
BRIV	Intrusive Breccia or Felsic Igneous Breccia	1.8%
D/BS	Diabase/Basic dyke	1.5%
DIOR	Diorite	1.1%
BRXX	Diorite Breccia	0.6%
PNBX	Pneumatolytic Breccia	0.5%
VN	Vein	NR
ANNX	Altered Andesite	NR

Phase 1 ML-ARD sampling of the 2005 core was based on two objectives. First, approximately 60 samples would be collected to generally match the percentage abundance in the 2005 core (Table 3-2 and Appendices A and B), although ANPL was under-represented. Second, these samples would be collected from several 2005 holes, from various depths, generally within the proposed mining area (eleven holes, from 05CF234 to 05CF248) to provide three-dimensional spatial coverage.

Table 3-2. Rock Units and Number of Phase 1 ML-ARD Samples from 2005 Drill Core

Rock-Unit Code	Description	Number of ML-ARD Samples (Percentage of Total)[1]
PPAU	Plagioclase-Augite-phyric Andesite	16 (27.1%)
ANPL (and ANLP)	Andesitic Lapilli Tuff	5 (8.5%)
ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	11 (18.6%)
PPFQ	Quartz-Feldspar or Feldspar-Quartz Porphyry	5 (8.5%)
ANDS	Andesite	4 (6.8%)
BRVL	Volcanic Breccia	2 (3.4%)
TOBR	Tourmaline Breccia	4 (6.8%)
FAUL and SHER	Faults, and Shear Zone / Faults	3 (5.1%)
PPPL	Plagioclase or Feldspar Porphyry	2 (3.4%)
ANTF	Andesitic Tuff	2 (3.4%)
BRIV	Intrusive Breccia or Felsic Igneous Breccia	1 (1.7%)
D/BS	Diabase/Basic dyke	1 (1.7%)
DIOR	Diorite	2 (3.4%)
BRXX	Diorite Breccia	0 (0%)
PNBX	Pneumatolytic Breccia	0 (0%)
VN	Vein	0 (0%)
ANNX	Altered Andesite	1 (1.7%)
	TOTAL	**59**

[1] Total includes two duplicates: 14578B from Hole 246 of PPAU, and 14685B from Hole 245 of DIOR.

The Paramount Zone was not sampled as part of this Phase 1 study.

Each sample was approximately a few hundred grams in weight. It was collected from the uppermost material (already ground to gravel and finer grain sizes) in a sealed plastic bucket that had been in unheated storage in Smithers. Each sample was collected with a fiberglass hand shovel, cleaned with soap and water between samples, and placed into a labelled ziploc bag. All samples were relatively dry, except three saturated and one moist (Appendix A).

Two duplicate samples were collected, with a “B” suffix in Appendices A and B. These duplicate samples were taken from the bottoms of the buckets, instead of the top. Therefore, differences between these duplicates can reflect analytical inaccuracy as well as any variability within theoretically homogenized buckets.

3.2 Sample Analysis

Based on the provincial ML-ARD Prediction Manual (Chapter 1), the Phase 1 samples (Section 3.1) were subjected to several geochemical “static” (one-time) analyses. The 59 samples were sent to ALS Chemex Labs in North Vancouver for:

1) Chemex Package ABA-PKG05A plus C-IR07, which is standard-Sobek (U.S. EPA 600) expanded acid-base accounting (ABA), providing measured and/or calculated values of:
   - paste pH in a mixture of pulverized rock and water,
   - total sulphur,
   - measured sulphide,
   - leachable sulphate (both HCl and carbonate leach techniques),
   - calculated sulphide by subtracting sulphate from total sulphur,
   - barium-bound sulphate calculated from barium analyses,
   - calculation of acid potentials based on sulphide levels plus any unaccounted-for sulphur (Sulphide Acid Potential, SAP),
   - standard-Sobek neutralization potential (NP) by acid bath and base titration,
   - inorganic carbonate for mathematical conversion to Carbonate NP (Inorg CaNP),
   - total carbon for mathematical conversion to Carbonate-equivalent NP (Total CaNP),
   - excess carbon calculated from the difference between total carbon and inorganic carbon,
   - CaNP calculated from calcium (Ca CaNP),
   - CaNP calculated from Ca + Mg (Ca+Mg CaNP),
   - various Net Neutralization Potential (NNP) balances of acid neutralizing capacities minus various acid generating capacities, and
   - various Net Potential Ratio (NPR) balances of acid neutralizing capacities divided by various acid generating capacities.

2) total-element contents by:
   - Chemex Package ME-MS41m: 48-element analysis after strong four-acid digestion, and
   - Chemex Package ME-XRF-06: XRF (x-ray-fluorescence) whole rock for 14 elements and parameters.

Mercury was determined separately by digesting a prepared sample with aqua regia for at least one hour in a graphite heating block. After cooling, the resulting solution was diluted with demineralized water and was treated with stannous chloride to reduce the mercury. The resulting mercury was volatilized by argon purging and measured by atomic absorption spectrometry.

ABA and total-element results are compiled in Appendix B and are discussed in Chapter 4.

4. RESULTS OF GEOCHEMICAL STATIC TESTS

As explained in Chapter 3, 57 samples plus two duplicates from Schaft Creek core, drilled in 2005, were subjected to various geochemical static (one-time) analyses. This chapter discusses the results of those analyses, and the analyses are compiled in Appendix B.

4.1 Acid-Base Accounting

As explained in Section 3.2, acid-base accounting (ABA) comprises several individual analyses and calculations. The major categories are paste pH (Section 4.1.1), sulphur species and acid potentials (Section 4.1.2), neutralization potentials (Section 4.1.3), and net balances of acid potentials and neutralization potentials (Section 4.1.4).

4.1.1 Paste pH

Paste pH is measured in a mixture ("paste") of pulverized sample and deionized water. If samples were well weathered and oxidized before analysis, then sometimes acidic pH values are measured, meaning the samples were already generating net acidity. QA/QC data showed the initial deionized water had a pH of 6.0-6.1, and values were reproducible to within ±0.2 pH units.

Paste pH in the 59 core samples for Schaft Creek ranged from 7.6 to 8.6 (Appendix B and Figure 4-1). Thus, no samples were acidic at the time of analysis.

4.1.2 Sulphur Species and Acid Potentials

Possible sulphur species that could be found in Schaft Creek rock are: sulphide including pyrite and chalcopyrite (Section 2.3), leachable sulphate like gypsum or anhydrite, and non-leachable sulphate like barite. The sum of these species theoretically equals total sulphur, although analytical inaccuracy and the existence of other sulphur species rarely yield an exact balance.

Total sulphur in the 59 rock samples ranged from 0.02 to 1.91%S, with a mean of 0.45%S and a median of 0.26%S (Figure 4-1 and Appendix B). In most samples, total sulphur and sulphide were similar (Figure 4-2), with sulphide representing 87% of total sulphur on average. Thus, the two parameters were typically interchangeable. Internal blanks, internal duplicates, and the two external duplicates showed acceptable QA/QC for total sulphur and sulphide, with RPD values less than 10%.

However, four samples contained more HCl-leachable sulphate than sulphide (Figure 4-3), with two from the major rock unit PPAU (Table 3-1). Carbonate-leachable sulphate, which is an alternative method, showed that only three samples contained more leachable sulphate than sulphide (Appendix B). In any case, a few percent of samples contained significant sulphate, so for better accuracy sulphide is used here instead of total sulphur to calculate acid potential.

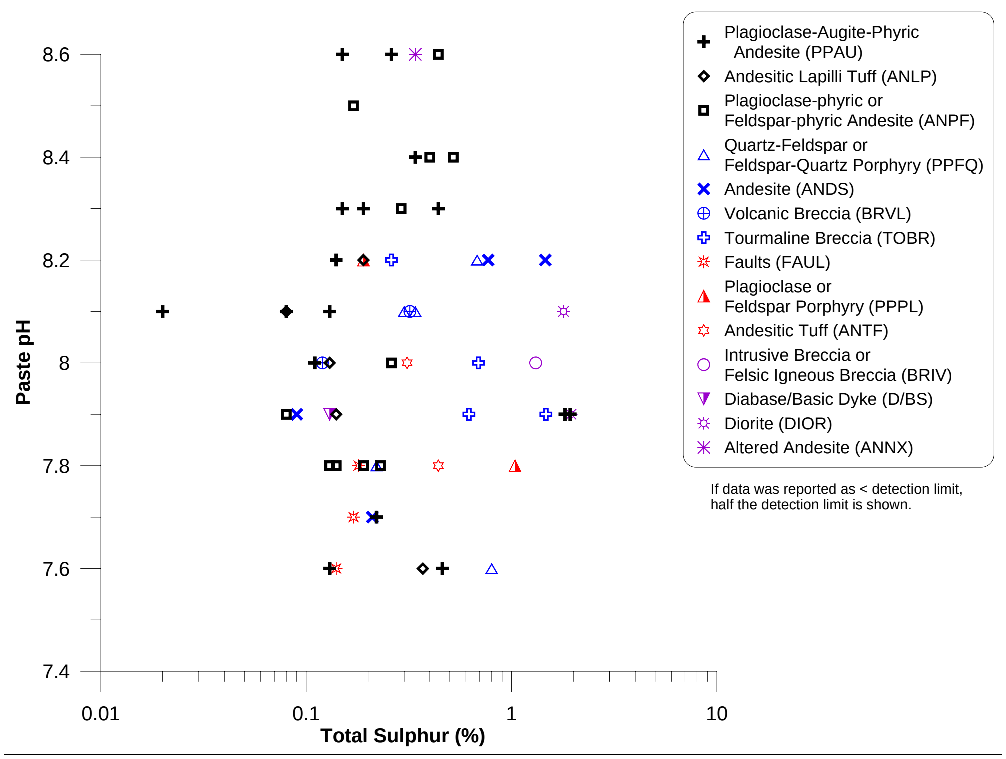


Figure 4-1. Paste pH vs. Total Sulphur in the 59 Schaft Creek Rock Samples.

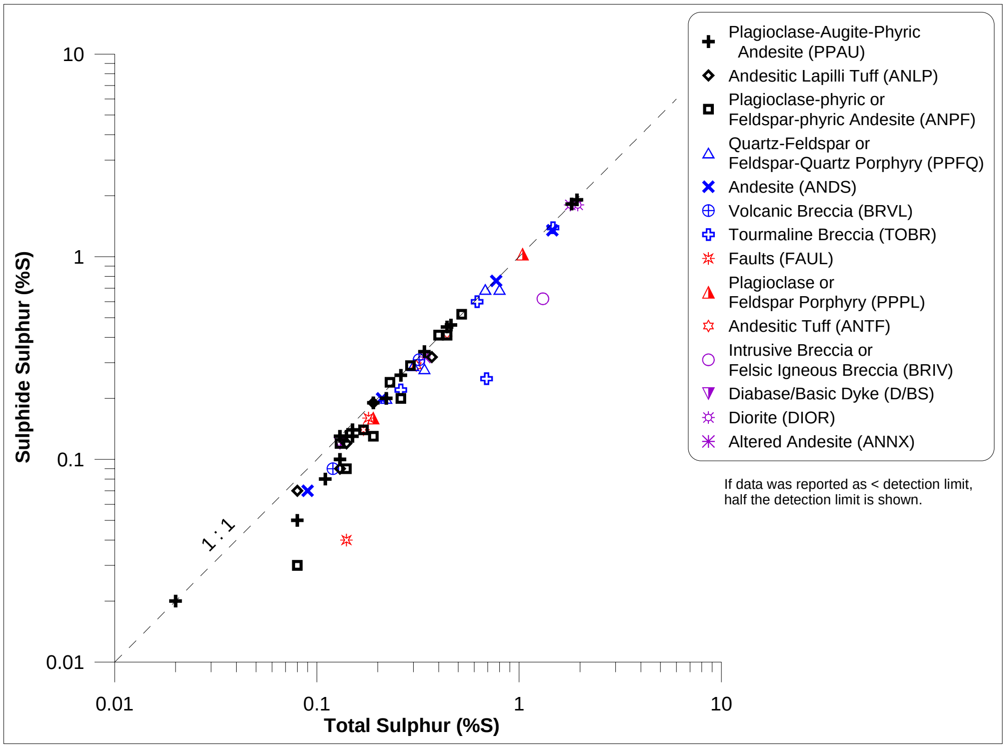


Figure 4-2. Sulphide vs. Total Sulphur in the 59 Schaft Creek Rock Samples.

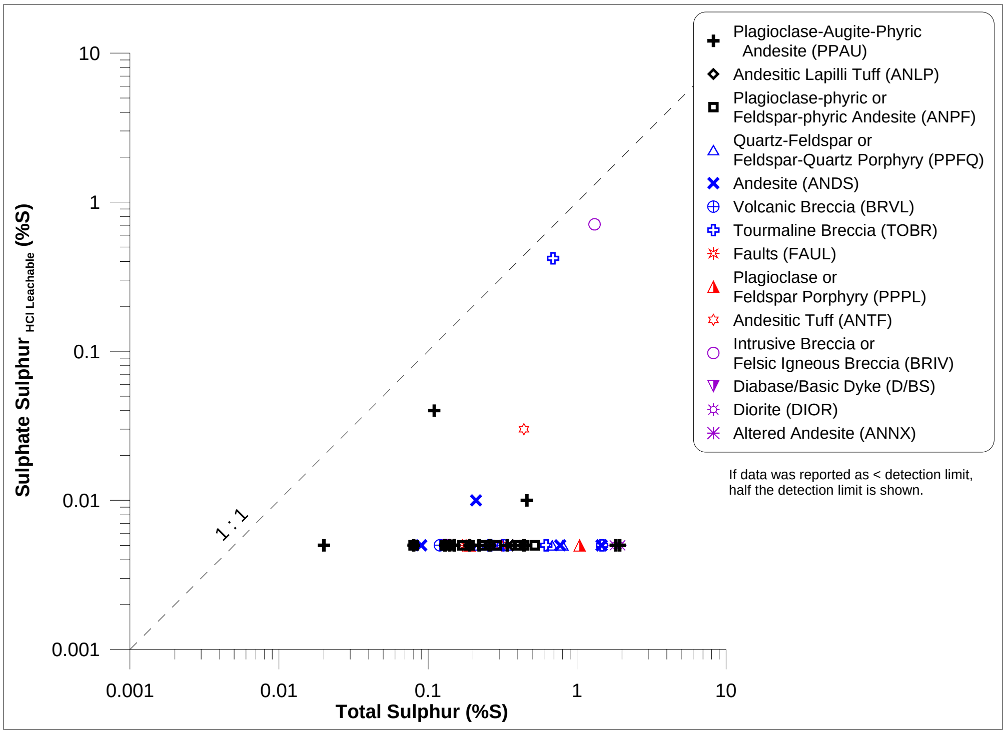


Figure 4-3. HCl-Leachable Sulphate vs. Total Sulphur in the 59 Schaft Creek Rock Samples.

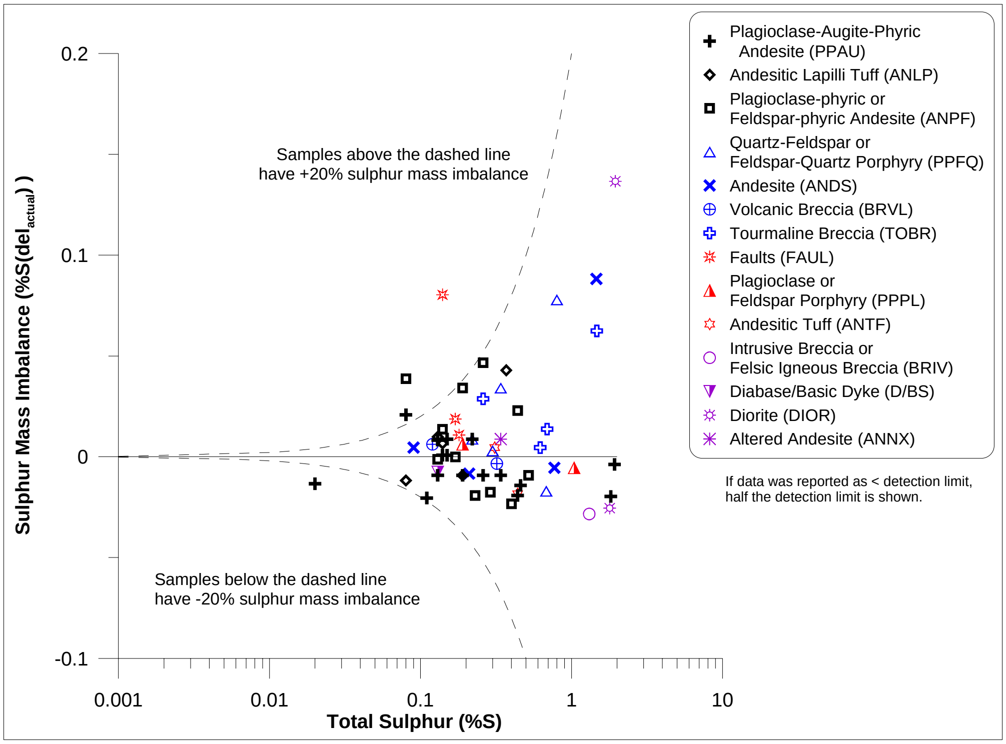


Figure 4-4. Sulphur Mass Imbalance vs. Total Sulphur in the 59 Schaft Creek Rock Samples.

Non-leachable sulphide as barite ($BaSO_4$) was calculated by assuming all barium from the ICP-MS analysis occurred as barite. This worst-case assumption showed that maximum non-leachable barium-bound sulphate would be 0.031%S with a mean of 0.01%S (Appendix B). On average, non-leachable sulphide as barite was 5.4% of total sulphur and thus not a major part of the sulphur mass balance.

A QA/QC mass-balance equation for sulphur species is:

$$\%S(del_{actual}) = \%S(Total) - \%S(Sulphide) - \%S(HCl\text{-}leachable\ sulphate) - \%S(BaSO_4)$$

Large negative values of $\%S(del_{actual})$ indicate the sum of sulphur species exceeds the measured total sulphur, sometimes due to analytical inaccuracy and detection limits. Large positive values indicate either (1) total sulphur was overestimated and/or (2) one or more sulphur species were underestimated. Positive values ("missing sulphur") can be added to acid-generating sulphide for safer calculations. This approach was used here for Schaft Creek rock, to calculate Sulphide-Based Acid Potentials (SAP, Section 4.1.4 and Appendix B).

Based on an allowable inaccuracy of 20% of total sulphur, 55 of 59 samples had acceptable balances (Figure 4-4). The four samples with significant imbalances had relatively low sulphur, including the sample with the lowest total sulphur. Low sulphur levels have higher probabilities of greater inaccuracies because they are closer to detection limits. In total, 32 of 59 samples had positive values of $\%S(del_{actual})$, so this "missing sulphur" was added to sulphide as a safety factor before calculating Sulphide-Based Acid Potential (SAP, Section 4.1.4 and Appendix B).

Because sulphide minerals in Schaft Creek rock are predominantly pyrite and chalcopyrite, and chalcopyrite does not necessarily generate as much acidity as pyrite upon oxidation, it is worthwhile to separate sulphide into individual sulphide minerals. To do this with ABA and total-element data (Section 3.2), the following steps were used.

1) Any "missing" sulphur due to mass imbalance (see %S(del) above) was added to measured/ calculated sulphide;
2) All measured zinc was assumed to occur as sphalerite; all measured molybdenum as molybdenite; all measured mercury as cinnabar; all measured arsenic as arsenopyrite or realgar; and all measured copper as chalcopyrite or proportionally as CuS_2; and
3) All the sulphide minerals from Step 2, converted to %S, were subtracted from Step 1, to obtain calculated pyrite in %S.

It is important to note that this approach can underestimate pyrite. It can even result in physically impossible negative pyrite concentrations due to analytical inaccuracy, detection limits, and the assumptions of the selected metals occurring only as the stated sulphides.

While several samples have more pyrite (as %S) than copper-bound sulphide as chalcopyrite and proportionally as CuS_2 (as %S), most contain more copper-bound sulphide (Figure 4-5). In fact, most have negative amounts of pyrite. Thus, this approach is not highly reliable. Nevertheless, two different sulphide values will be used in this study to calculate acid potential.

1) The aforementioned Sulphide-Based Acid Potential (SAP) which includes positive values of $\%S(del_{actual})$ and represents the maximum ("worst case") amount of acid potential.

2) The "Pyrite-Calculated Acid Potential" (PAP) which is based only on calculated pyrite-bound

sulphide, with any value less than one-half the typical detection limit, including negative values, set at one-half the limit (0.005%S); this represents the minimum ("best case") acid potential.

As a result, SAP represented the maximum ("worst case") acid potential, whereas PAP was the minimum ("best case") acid potential. Actual acid potential would be somewhere at or between these two endpoints, but additional testwork would be needed to determine this (Chapter 5).

A scatterplot of SAP and PAP showed that many samples had the low, default PAP value based on 0.005%S (Figure 4-6). A few samples had nearly equivalent values, meaning most of their sulphide was pyrite.

In summary, total sulphur in the 59 Schaft Creek rock samples ranged from 0.02 to 1.91%S, with a mean of 0.45%S and a median of 0.26%S. In most samples, total sulphur and sulphide were similar (Figure 4-2), and thus the two parameters were typically interchangeable. Because a few samples did contain elevated leachable sulphate, sulphide is a better indicator of acid potential than total sulphur for Schaft Creek rock. However, in many samples, most sulphide was copper-bound sulphide (chalcopyrite) which may have less capacity to generate acidity. Therefore, each sample has a maximum Sulphide-Based Acid Potential (SAP) and a minimum Pyrite-Calculated Acid Potential (PAP).

4.1.3 Neutralization Potentials

There are various types of neutralizing capacities in rock samples, all expressed in units of kg $CaCO_3$ equivalent/tonne (kg/t). These include:

(1) Sobek "bulk neutralization potential" (NP) based on an hours-long acid bath to determine how much acid was neutralized in the short term (EPA 600 technique),

(2) carbonate-equivalent neutralization potential (CaNP) calculated from measured solid-phase levels of inorganic carbonate (Inorg CaNP) or total carbon (Total CaNP), and

(3) calculated CaNP assuming all calcium occurs as calcite (Ca CaNP) or all calcium + magnesium occurs as calcite and dolomite (Ca+Mg CaNP).

Each can reveal important aspects of a sample's capacity to neutralize the acidity generated by sulphide oxidation. All values are compiled in Appendix B.

Short-term bulk Sobek NP ranged from 40 to 219 kg/t in the 59 Schaft Creek samples, with a mean of 97 and a median of 92 kg/t (Figure 4-7 and Appendix B). These are relatively high values. They explain why no acidic paste pH values were detected (Section 4.1.1), and suggest there could be a long lag time (years to decades) before these samples might become acidic. The two external duplicates and one internal duplicate showed good QA/QC for Sobek NP, with RPD values less than 10%.

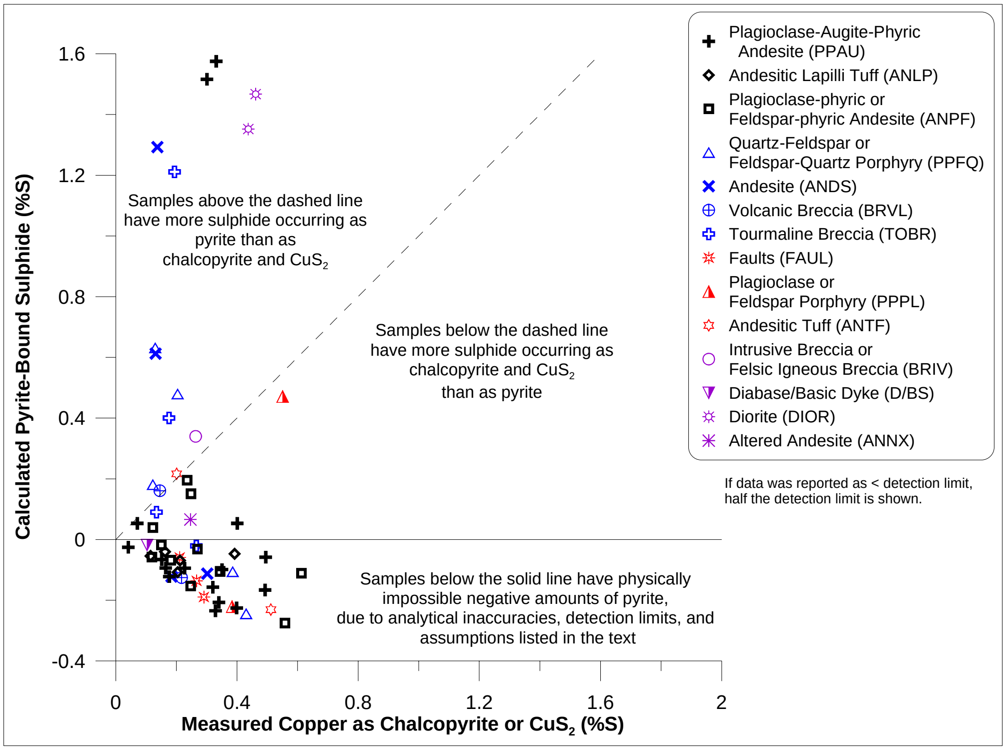


Figure 4-5. Calculated Pyrite-Bound Sulphide vs. Copper-Bound Sulphide as Chalcopyrite and CuS_2 in the 59 Schaft Creek Rock Samples.

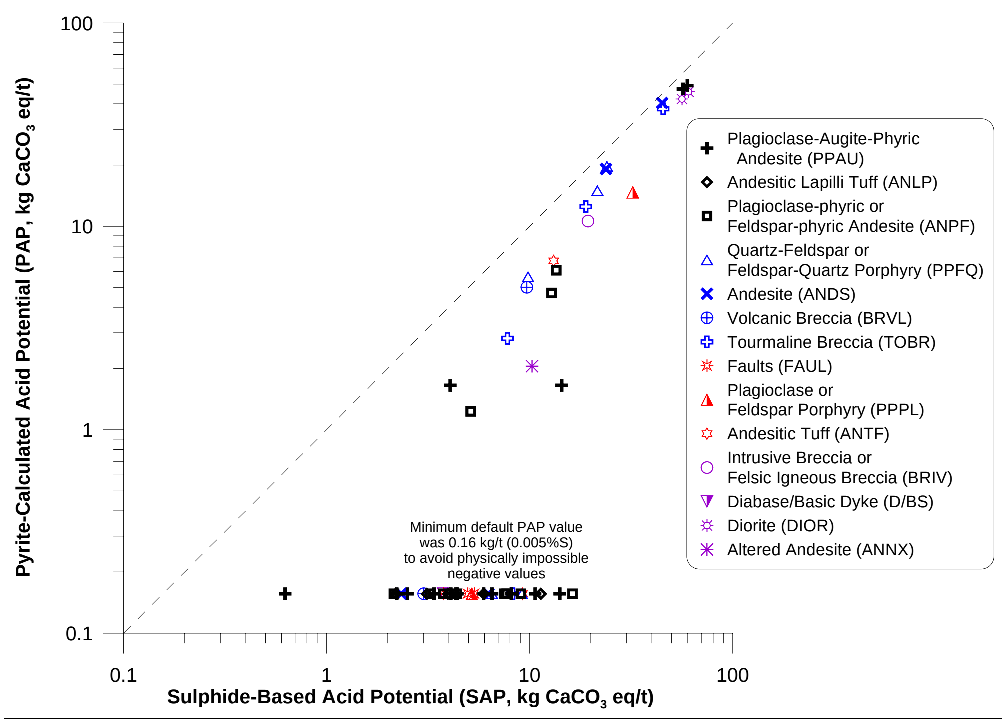


Figure 4-6. Pyrite-Calculated Acid Potential (PAP) vs. Sulphide-Based Acid Potential (SAP) in the 59 Schaft Creek Rock Samples.

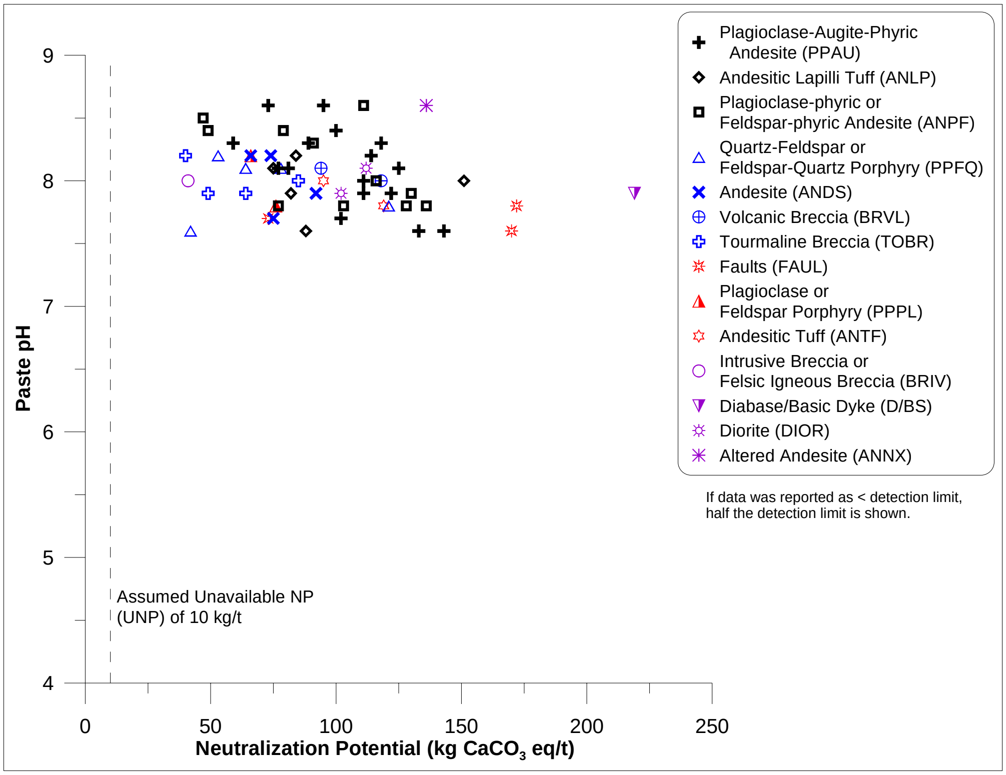


Figure 4-7. Paste pH vs. Sobek Neutralization Potential in the 59 Schaft Creek Rock Samples.

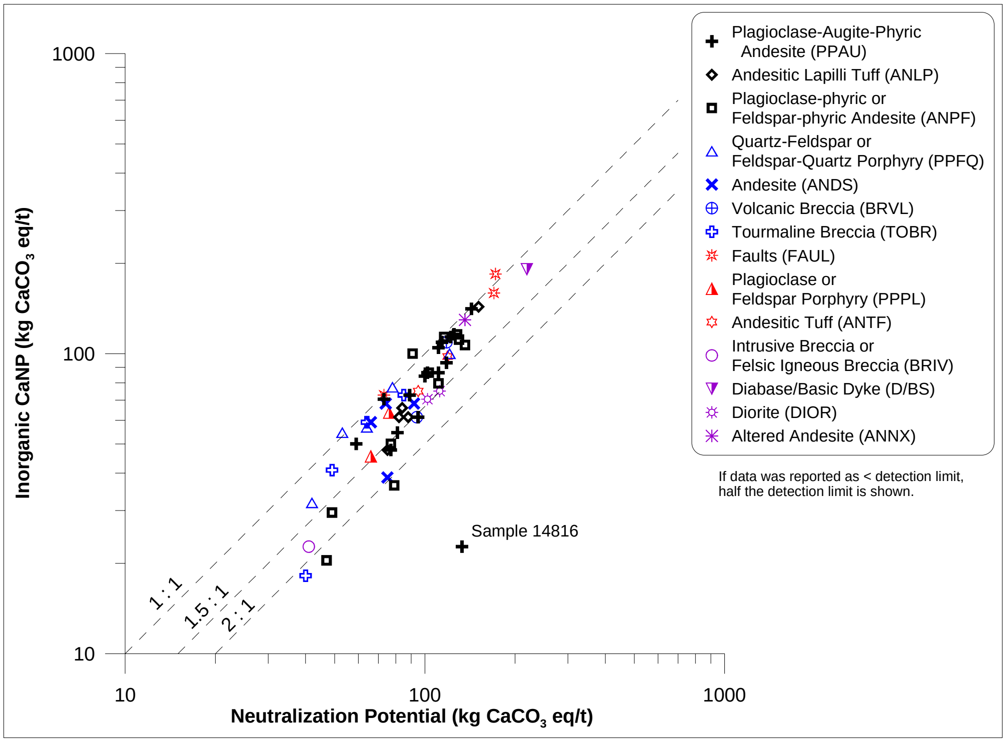


Figure 4-8. Inorganic-Carbon-Based Neutralization Potential vs. Sobek Neutralization Potential in the 59 Schaft Creek Rock Samples.

Some amount of measured NP is typically “unavailable” for neutralization, often between 5-15 kg/t although smaller and larger values have been documented (Morin and Hutt, 1997 and 2001). This can sometimes be seen in scatterplots of NP with paste pH after sufficient time has passed for net acidity to develop. The trends then typically show paste pH generally, but not consistently, decreasing as NP decreases, until acidic pH values are detected.

However, the lack of any acidic paste pH in the 59 samples means that Unavailable NP cannot be estimated at this time. Thus, the common default value of 10 kg/t will be used and will be subtracted from all measured values to obtain Available NP (Appendix B and Figure 4-7).

The comparison of total carbon with inorganic carbon showed that both were about the same in nearly all samples (Appendix B). Only four samples had noticeably higher total carbon, but inorganic carbon was still more than half of the total carbon in three of these four samples. In the remaining sample (14816, Appendix B), inorganic carbon was only around 17% of total carbon. This was probably an analytical error, with total carbon too high or inorganic carbon too low. As explained in the next paragraph, inorganic carbon was probably too low in this sample.

A scatterplot of Sobek NP with Inorganic Carbon, converted to the same units (Inorganic CaNP as kg/t), showed that Sobek NP was typically greater than Inorganic CaNP (Figure 4-8). NP was often greater by a factor of 1.5 or more, except above NP values above 100 kg/t when the two values converged. Such exceedances of NP above Inorganic CaNP are not common. Nevertheless, this appears valid for Schaft Creek rock based on (a) the consistency of the Schaft Creek results (Figure 4-8) and (b) the mineralogy showing abundant non-carbonate, aluminosilicate minerals (Chapter 2) that can provide neutralization. Based on the trend in Figure 4-8, Inorganic CaNP in anomalous Sample 14816 is likely too low.

Because the type of carbonate (calcite, dolomite, siderite, etc.) was not determined in previous studies (Chapter 2), scatterplots with Inorganic CaNP can sometimes reveal the carbonate composition, if elements like calcium and magnesium mostly occur only with carbonate. For the comparison, calcium was converted to “Ca CaNP” with similar units as Inorganic CaNP. This showed that some samples contained excess carbonate, many contained excess calcium, and some contained both in calcite-equivalent amounts (Figure 4-9). The excess calcium was consistent with calcium-bearing aluminosilicate minerals in Schaft Creek rock (Chapter 2).

A comparison of “Ca+Mg CaNP” to Inorganic CaNP showed that nearly every sample contained more Ca+Mg than carbonate (Figure 4-10). This meant that dolomite could not account for all the Ca+Mg, which was consistent with both calcium-bearing and magnesium-bearing aluminosilicate minerals in Schaft Creek rock (Chapter 2).

Sobek NP showed a better correlation with Ca CaNP (Figure 4-11) than with Inorganic CaNP (Figure 4-9), although the correlation was still poor for both. This suggests calcium-bearing minerals, both carbonate and aluminosilicate, can account for the Sobek NP in several samples, but not all samples. Ca+Mg CaNP displayed an even poorer correlation with Sobek NP (Figure 4-12). Thus, rapid assay-based analyses like calcium and magnesium cannot substitute for the more intensive Sobek NP in Schaft Creek rock.

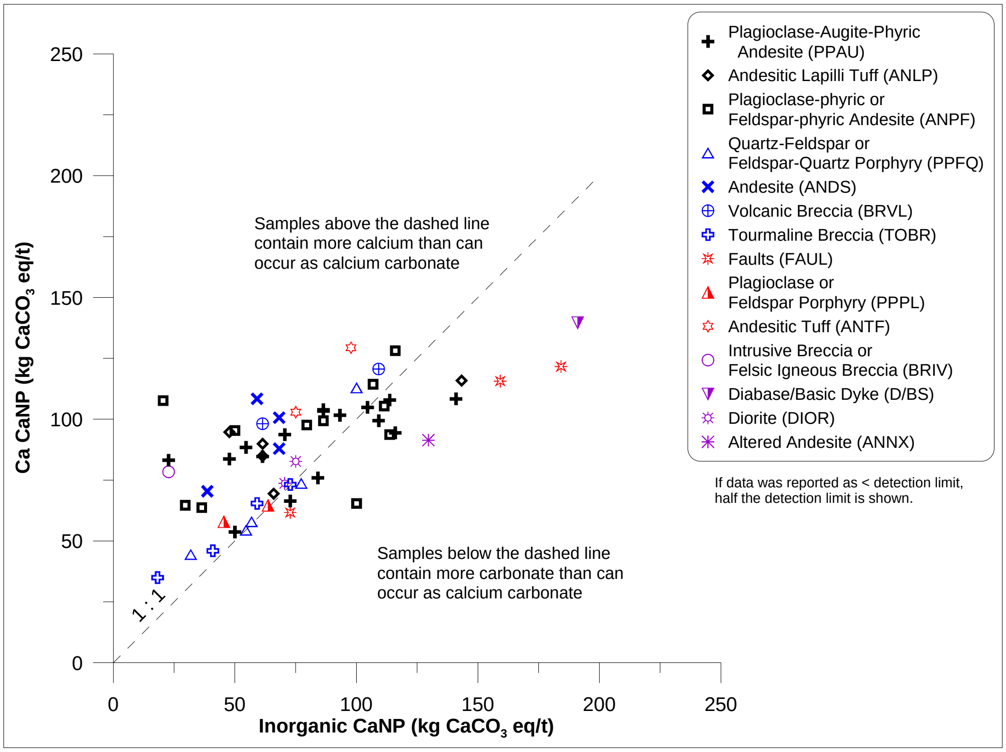


Figure 4-9. Calcium-Based Neutralization Potential vs. Inorganic-Carbon-Based Neutralization Potential in the 59 Schaft Creek Rock Samples.

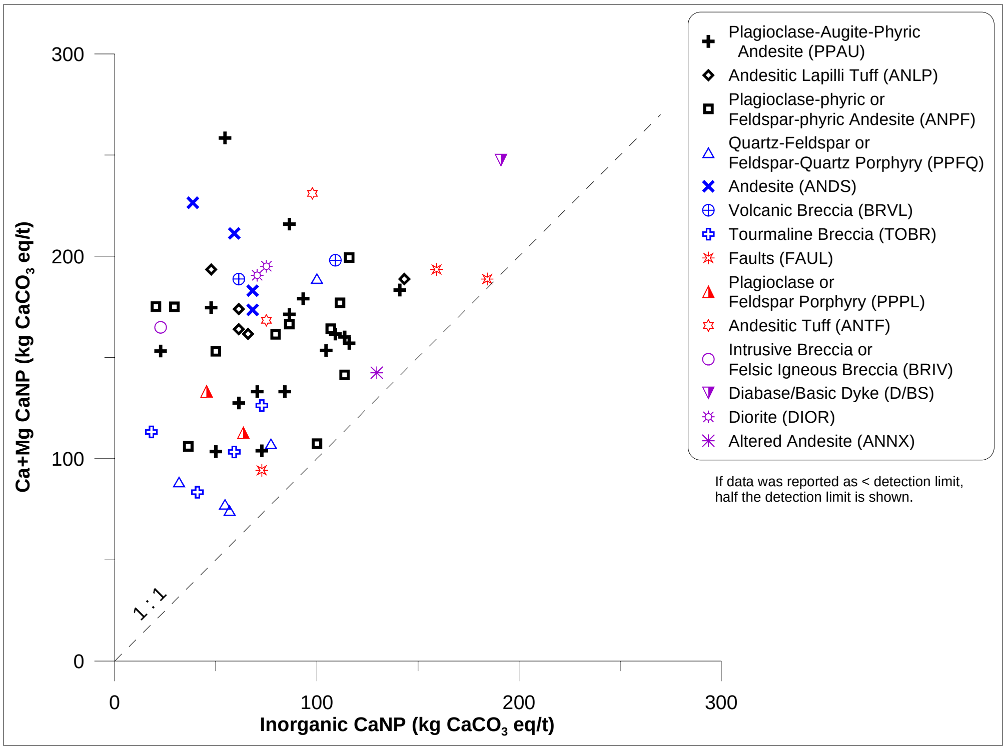


Figure 4-10. Calcium-Magnesium-Based Neutralization Potential vs. Inorganic-Carbon-Based Neutralization Potential in the 59 Schaft Creek Rock Samples.

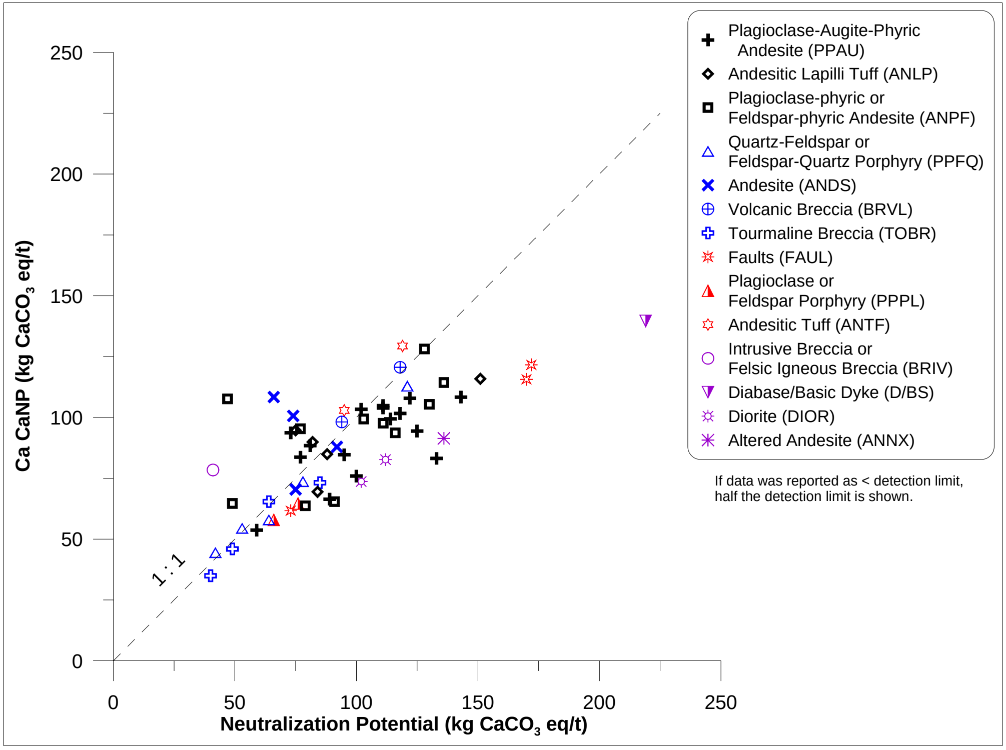


Figure 4-11. Calcium-Based Neutralization Potential vs. Sobek Neutralization Potential in the 59 Schaft Creek Rock Samples.

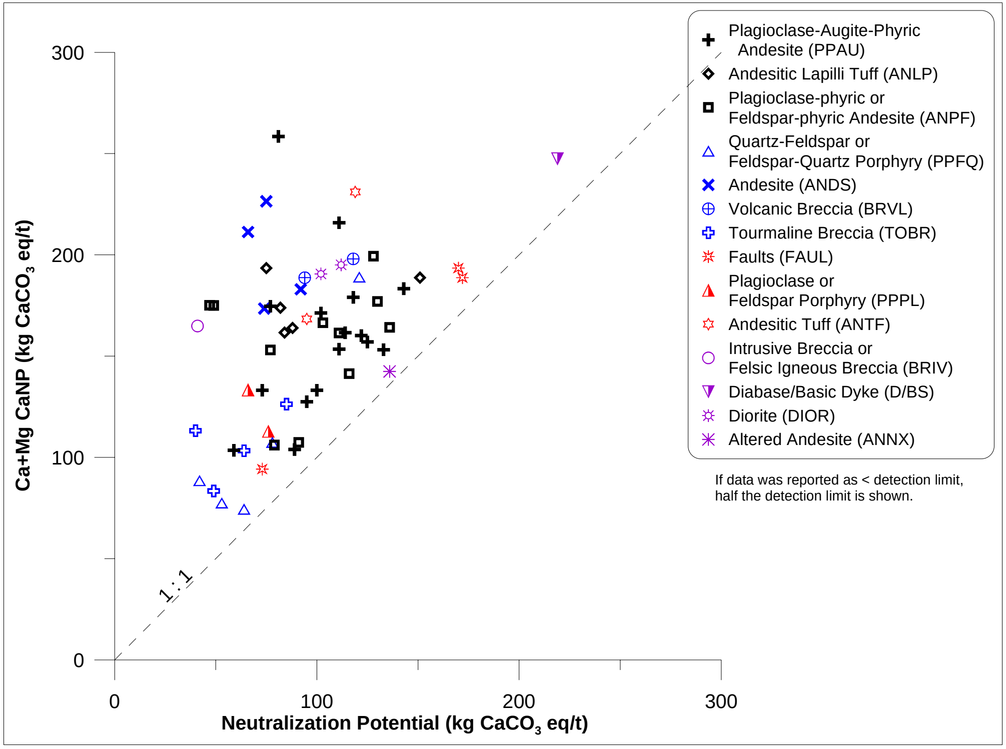


Figure 4-12. Calcium-Magnesium-Based Neutralization Potential vs. Sobek Neutralization Potential in the 59 Schaft Creek Rock Samples.

In summary, Sobek (EPA 600) Neutralization Potential (NP) ranged from 40 to 219 kg/t in the 59 Schaft Creek samples, with a mean of 97 and a median of 92 kg/t. These are relatively high values. They explain why no acidic paste pH values were detected, and suggest there could be a long lag time (years to decades) before these samples might become acidic. A certain amount of measured NP is typically "unavailable" for neutralization, and thus should be subtracted from measured values. The lack of acidic paste pH values precluded an initial estimate of Unavailable Neutralization Potential, so the common value of 10 kg/t is used here. NP was typically greater than inorganic carbonate in many samples, meaning NP also reflected the presence of non-carbonate aluminosilicate minerals. These minerals have been documented in Schaft Creek rock. Also, NP did not correlate well with solid-phase calcium or magnesium levels, but some samples showed that calcium-bearing minerals could account for their NP levels.

4.1.4 Net Balances of Acid-Generating and Acid-Neutralizing Capacities

As explained in Section 4.1.2, the acid-generating capacities of the Schaft Creek samples of rock could be calculated from total sulphur to obtain Total-Sulphur-Based Acid Potentials (TAP), or sulphide plus %S(del) to obtain Sulphide-Based Acid Potentials (SAP). Because total sulphur was mostly composed of sulphide, TAP and SAP were generally interchangeable. SAP is used here for net balances, because a few samples had significant amounts of leachable sulphate which was not acid generating. As explained in Section 4.1.2, SAP is considered the maximum "worst-case" acid potential for each sample, whereas the Pyrite-Calculated Acid Potential (PAP) is considered the "best-case" minimum.

Neutralization Potentials (NP) were discussed in Section 4.1.3. The current estimate of 10 kg/t was considered unavailable and was subtracted from measured values.

Net balances of these two potentials were calculated to predict whether a sample would be net acid generating, perhaps after a long near-neutral "lag time", or net acid neutralizing indefinitely. Net balances can be calculated using division (Net Potential Ratio, NPR = NP / AP) or subtraction (Net Neutralization Potential, NNP = NP - AP).

Provincially, NPR is preferred and used here. "Adjusted" Sulphide-Based NPR values were obtained by first subtracting 10 kg/t of unavailable NP from measured NP:

$$\text{Adj SNPR} = [\text{NP} - 10] / [\%\text{S(sulphide + positive delS values)} * 31.25] \qquad \text{(Eq. 4-1)}$$

Similarly, Adjusted Pyrite-Calculated NPR values were calculated by:

$$\text{Adj PNPR} = [\text{NP} - 10] / [\text{PAP}] \qquad \text{(Eq. 4-2)}$$

Provincial non-site-specific ABA screening criteria are: $\text{NPR} < 1$ is net acid generating, perhaps after some lag time; $1 \leq \text{NPR} \leq 2$ is uncertain until further testing; and $\text{NPR}>2$ is net acid neutralizing. The implications of using the alternative criterion of 1.0 are discussed below and in Chapter 5.

It is important to note that all discussions of net balances in this report are "unweighted". This means that they were not adjusted to tonnages in the Schaft Creek Deposit. Three-dimensional geostatistical modelling of geology and ML-ARD parameters should be conducted (Chapter 5; see also Section 4.1.5), to address issues such as (1) the total tonnages of net-acid-generating rock, (2) year-by-year production of net-acid-generating rock, and (3) portions of rock units that are net acid generating.

Worst-case Adjusted SNPR values ranged from 0.86 (net acid generating) to 114 (net neutralizing). Only one sample was less than 1.0 (tourmaline breccia, TOBR), and eight samples (several rock units) were between 1.0 and 2.0 (Figures 4-13 and 4-14, and Appendix B). Only samples with sulphide below 0.6%S or Sobek NP above 125 kg/t were consistently net neutralizing.

In contrast, best-case Adjusted PNPR values ranged from 1.03 (uncertain) to the default value of 200 which means that PAP was less than 0.01%S (Figures 4-15 and 4-16, and Appendix B). No values were less than 1.0, and only three samples from three rock units were less than 2.0. Many samples had the default value of 200. As with Adj SNPR, only samples with sulphide below 0.6%S or Sobek NP above 125 kg/t were consistently net neutralizing.

Overall, only 0-2% of the 59 samples were net acid generating and 5-14% were uncertain (Table 4-1). Therefore, most samples were net neutralizing. Although the numbers of samples from most rock units were limited, the major rock units (>5% of 2005 footage, Table 3-1) with some uncertain samples were PPAU and PPFQ. The minor units with uncertain or net-acid-generating percentages were ANDS, TOBR, BRIV, and DIOR.

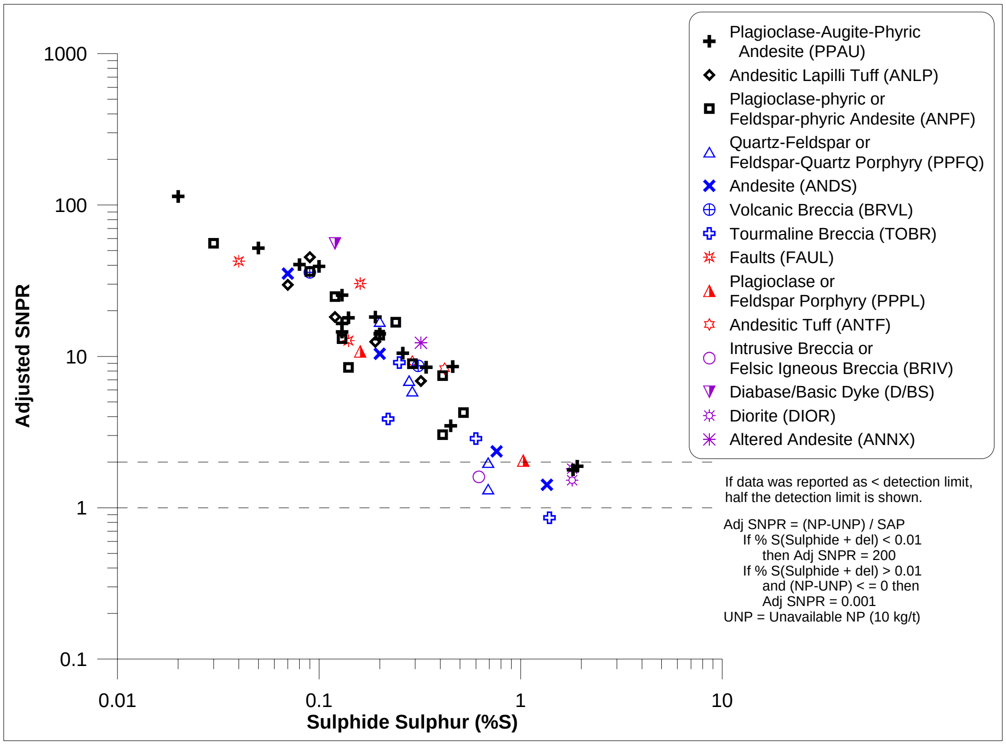
In summary, best-case and worst-case net balances of acid-generating and acid-neutralizing capacities were calculated for each of the 59 Schaft Creek samples. Overall, only 0-2% of the samples were net acid generating and 5-14% were uncertain based on generic criterion. Thus, most samples were net neutralizing. PPAU and PPFQ were the major rock units with uncertain samples, while net-acid-generating or uncertain samples were found in the minor rock units of ANDS, TOBR, BRIV, and DIOR.

4.1.5 Spatial Distribution of Net Balances

As explained in Section 4.1.4, net balances of acid-generating and acid-neutralizing capacities in the 59 samples of Schaft Creek core showed that most samples were net acid neutralizing. Only 0-2% of samples were net acid generating and 5-14% were uncertain.

An important aspect of these balances is whether there are any major spatial distributions through the Schaft Creek Deposit. For example, if all net-acid-generating and uncertain samples were located in one area, this area could be targetted for special mining and waste management.

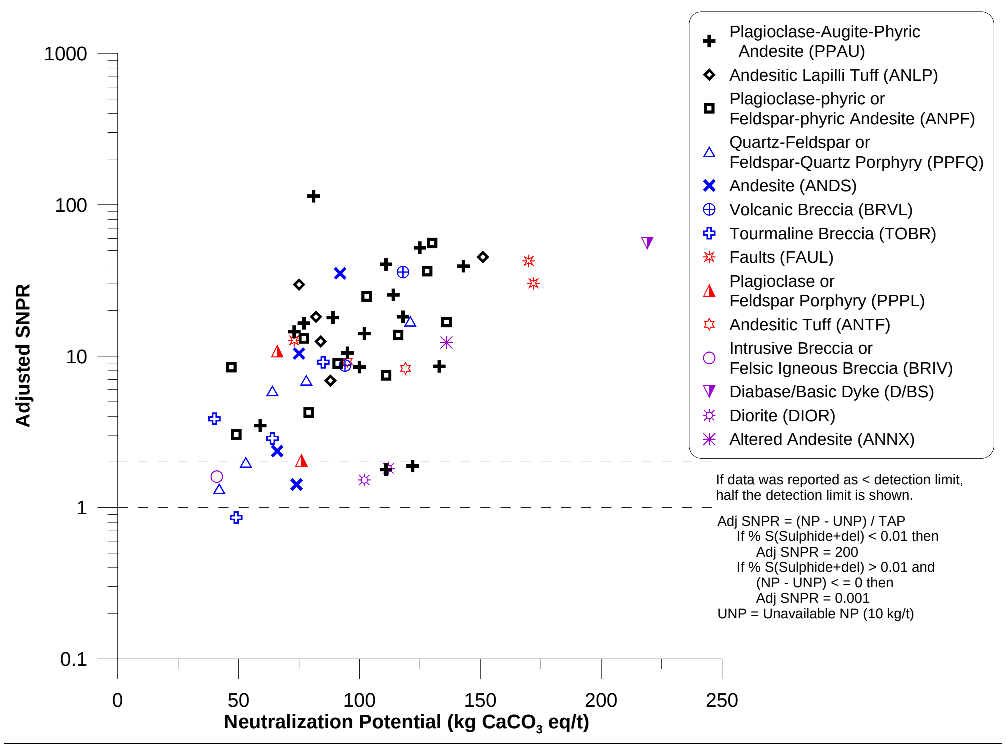
Spatial distributions are best determined by geostatistical modelling combined with the Schaft Creek geologic model (Chapter 5). However, as a general indication here, one general east-west and one general north-south vertical cross-section were plotted, with drillholes moved laterally onto the plane of the section.



If data was reported as < detection limit,
half the detection limit is shown.

Adj SNPR = (NP-UNP) / SAP
If % S(Sulphide + del) < 0.01
then Adj SNPR = 200
If % S(Sulphide + del) > 0.01
and (NP-UNP) < = 0 then
Adj SNPR = 0.001
UNP = Unavailable NP (10 kg/t)

Figure 4-13. Worst–Case Adjusted Sulphide-Based Net Potential Ratio vs. Sulphide in the 59 Schaft Creek Rock Samples.



If data was reported as < detection limit,
half the detection limit is shown.

Adj SNPR = (NP - UNP) / TAP
If % S(Sulphide+del) < 0.01 then
Adj SNPR = 200
If % S(Sulphide+del) > 0.01 and
(NP - UNP) < = 0 then
Adj SNPR = 0.001
UNP = Unavailable NP (10 kg/t)

Figure 4-14. Worst–Case Adjusted Sulphide-Based Net Potential Ratio vs. Sobek Neutralization Potential in the 59 Schaft Creek Rock Samples.

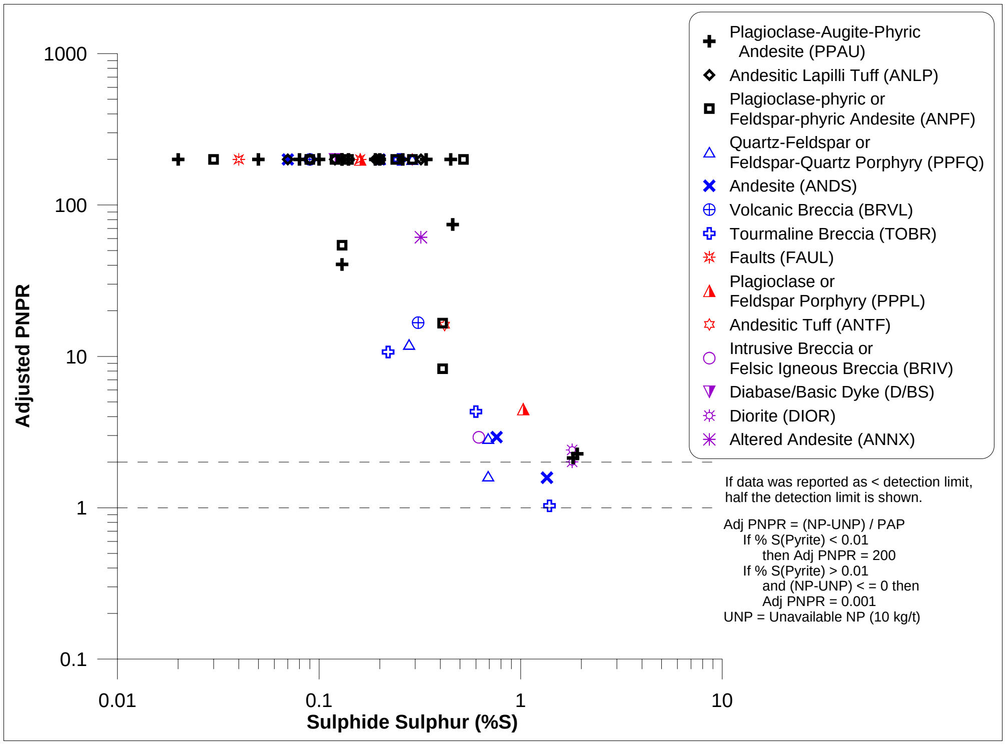


Figure 4-15. Best–Case Adjusted Pyrite-Calculated Net Potential Ratio vs. Sulphide in the 59 Schaft Creek Rock Samples.

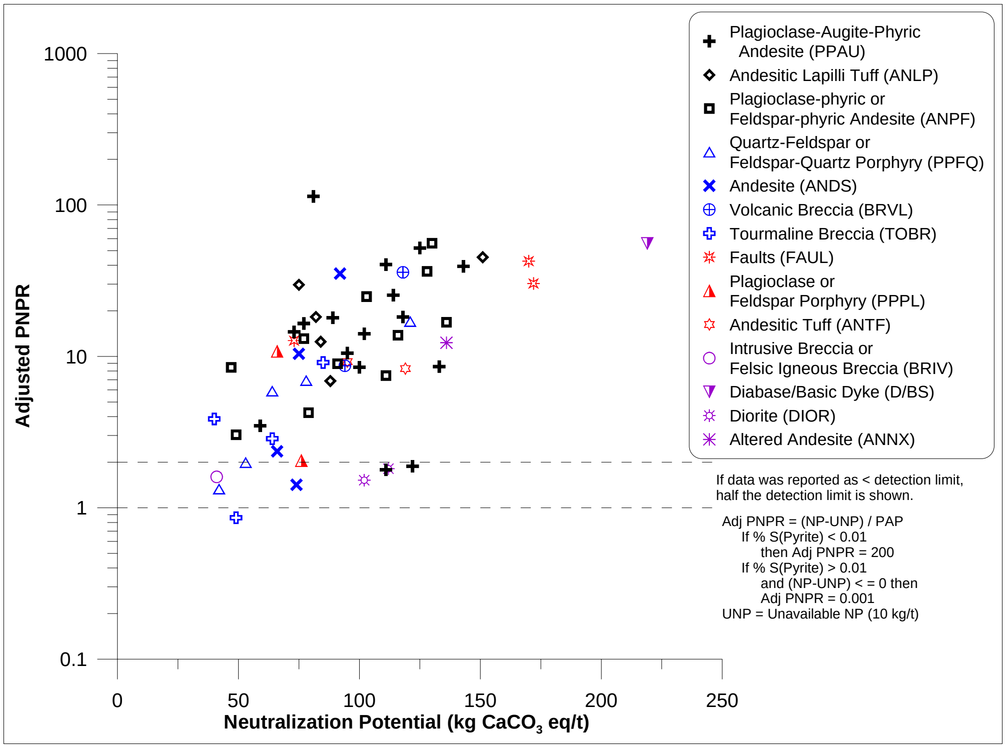


Figure 4-16. Best–Case Adjusted Pyrite-Calculated Net Potential Ratio vs. Sobek Neutralization Potential in the 59 Schaft Creek Rock Samples.

Table 4-1. Summary of Net-Acid-Generating, Uncertain, and Net-Neutralizing Percentages of Samples from 2005 Drill Core

Rock-Unit Code	Number of ML-ARD Samples[1]	Best-case and worst-case percentages[2] of . . .		
		Net acid generating	Uncertain	Net neutralizing
PPAU	16	0%	0-12.5%	87.5-100%
ANPL (and ANLP)	5	0%	0%	100%
ANPF	11	0%	0%	100%
PPFQ	5	0%	20-40%	60-80%
ANDS	4	0%	25-25%	75-75%
BRVL	2	0%	0%	100%
TOBR	4	0-25%	0-25%	75-75%
FAUL and SHER	3	0%	0%	100%
PPPL	2	0%	0%	100%
ANTF	2	0%	0%	100%
BRIV	1	0%	0-100%	0-100%
D/BS	1	0%	0%	100%
DIOR	2	0%	0-100%	0-100%
BRXX	0			
PNBX	0			
VN	0			
ANNX	1	0%	0%	100%
	59	**0-1.7%**	**5.1-13.6%**	**84.7-94.9%**

[1] Total includes two duplicates: 14578B from Hole 246 of PPAU, and 14685B from Hole 245 of DIOR.

[2] Net-acid-generating samples had NPR values less than 1.0, uncertain samples had 1.0 < NPR < 2.0, and net-neutralizing samples > 2.0; best case is defined by the Adjusted Pyrite-Calculated Net Potential Ratio (Adj PNPR) and the worst case is defined by the Adjusted Sulphide-Based Net Potential Ratio (Adj SNPR).

Based on the worst-case net balance (Adjusted SNPR, Section 4.1.4), the general east-west cross-section showed the center area was net-neutralizing (Figure 4-17), while net-acid-generating and uncertain samples were found on the periphery. The general north-south cross-section showed uncertain samples were found in three adjacent holes (Figure 4-18). Based on this limited information, the net-acid-generating and uncertain samples may be spatially restricted in the Schaft Creek Deposit, but additional samples and geostatistical modelling are needed to confirm this.

4.2 Total-Element Analyses

Total-element levels in the 59 Schaft Creek samples (Section 3.1) were measured by ICP-MS analysis after strong four-acid digestion and by x-ray-fluorescence whole-rock analysis (Section 3.2). The results are compiled in Appendix B. There was generally good agreement for elements detected by both methods (Appendix B), except chromium whose whole-rock levels were notably higher due to the higher detection limit.

Overall, the dominant elements in the Schaft Creek samples were silicon and aluminum (Appendix B), reflecting the dominance of aluminosilicate minerals (Chapter 2). Calcium, iron, potassium, magnesium, sodium, and Loss on Ignition (LOI) were relatively abundant. LOI typically reflects the loss from the samples of some or all sulphur, carbon, and tightly bound or crystalline water.

To identify the metals and other elements that occurred at relatively high levels in the rock, each element was compared with average crustal abundances, as recommended in provincial ML-ARD documents (Price, 1998). Any level at least three times greater than the average maximum crustal abundance was highlighted with a box in Appendix B.
This showed that the Schaft Creek samples were:
- frequently elevated in silver, bismuth, copper, molybdenum, and selenium; and,
- occasionally elevated in sulphur, antimony, and tungsten.

Elevated solid-phase levels of elements do not necessarily mean they will leach into water at high concentrations. In fact, they may be elevated because they did not leach. Additional testwork is needed to evaluate metal leaching in detail (Chapter 5).

Solid-phase correlations of elements can sometimes reveal mineralogical associations. For example, elements correlating with sulphide presumably occur within the sulphide minerals, which at the Schaft Creek Project are typically pyrite and chalcopyrite (Chapter 2). Correlations with Sobek Neutralization Potential (NP, Section 4.1.3) indicate those elements may be concentrated in certain carbonate and aluminosilicate minerals, which can dissolve even in the absence of sulphide oxidation.

The only element that showed some correlation with sulphide was copper. This was discussed in Section 4.1.2. NP showed some correlation with calcium, as discussed in Section 4.1.3, and perhaps minor negative correlations with arsenic and lead. The few samples of tourmaline breccia (TOBR), and a few samples of other units, sometimes stood out as distinct groupings of generally higher or lower levels of elements like gallium, phosphorus, thallium, tungsten, and uranium.

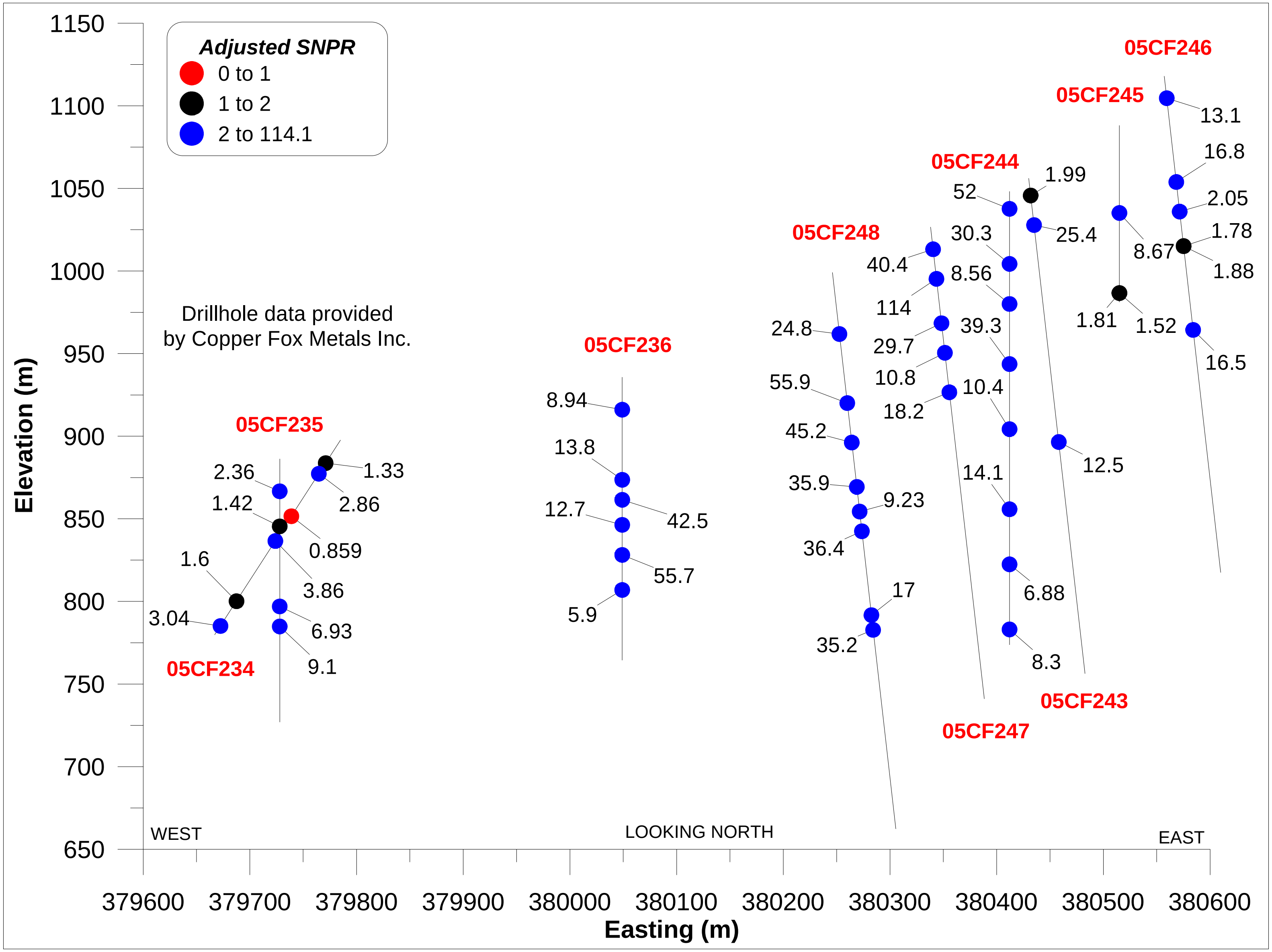


Figure 4-17. General East-West Vertical Cross-Section through the Schaft Creek Deposit, Showing Worst-Case Adjusted Sulphide-Based Net Potential Ratio (0-1 = net acid generating; 1-2 = uncertain; >2 = net acid neutralizing).

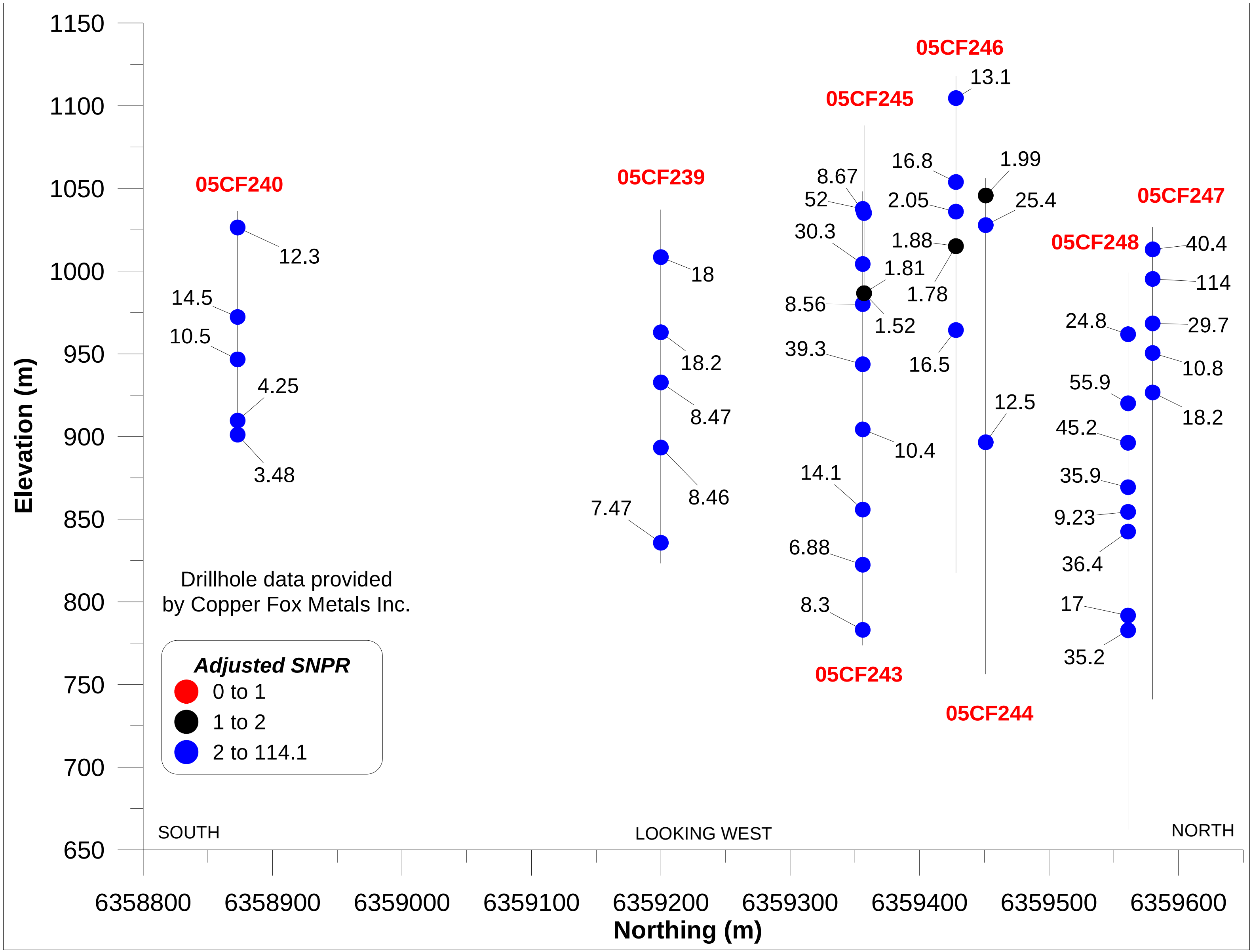


Figure 4-18. General North-South Vertical Cross-Section through the Schaft Creek Deposit, Showing Worst-Case Adjusted Sulphide-Based Net Potential Ratio (0-1 = net acid generating; 1-2 = uncertain; >2 = net acid neutralizing).

In summary, the 59 samples of Schaft Creek core were predominantly composed of silicon and aluminum, reflecting the abundant aluminosilicate minerals. Calcium, iron, potassium, magnesium, sodium, and Loss on Ignition (LOI) were also relatively abundant. Compared to general crustal abundances, the 59 samples were frequently elevated in silver, bismuth, copper, molybdenum, and selenium, and occasionally elevated in sulphur, antimony, and tungsten. However, solid-phase levels do not typically reflect leaching rates into water, so additional testwork is needed on metal leaching. Only copper showed some correlation with sulphide, reflecting the copper-bound sulphide discussed under Acid-Base Accounting. For Sobek Neutralization Potential, calcium showed some correlation, which was also discussed under Acid-Base Accounting. Samples of some rock units, particularly tourmaline breccia (TOBR), stood out as a distinct group for some elements like gallium, phosphorus, thallium, tungsten, and uranium.

5. CONCLUSION AND RECOMMENDATIONS

This report contains the first phase of ML-ARD studies for the Schaft Creek Project. Previous relevant information was compiled. Also, 59 samples of core rejects, from 11 holes drilled in 2005, were collected from cold storage. This set included two duplicates for QA/QC checks. All 59 samples were analyzed for expanded Sobek (EPA 600) acid-base accounting, and for total-element contents using ICP-MS after four-acid digestion and using x-ray fluorescence whole rock.

Previous Information

The compilation of existing information relevant to ML-ARD led to the following important observations.

- The Schaft Creek copper-gold-molybdenum deposit is widely acknowledged as being a porphyry copper deposit. It contains three mineral zones: the Liard, West Breccia, and Paramount Zones.

- During an examination of existing core, “It has been noted that the core from previous drilling programs, which is stored on site, exhibits a remarkable degree of preservation with limited visible weathering.” Thus, the oxidation rate of Schaft Creek rock may be relatively slow.

- Based on 16 acid-base accounts from a previous, metallurgical study, all 16 samples were net acid neutralizing, with sulphide between 0.1 and 0.9%S, and Neutralization Potentials from 53 to 114 kg/t. Flotation recovery of sulphide reduced the sulphide levels in the synthetic tailings.

- Detailed mineralogy was examined in 18 thin sections, representing feldspar quartz porphyry (rock code PPFQ), tourmaline breccia, pneumatolytic breccia, and volcanics. Even one rock unit (PPFQ) was not entirely intrusive. Some PPFQ samples were porphyritic volcanics of felsic and intermediate composition (dacitic - andesitic), and one sample was a fine grained, feldspathic intrusive rock classified as either syenite or anorthosite, depending on the composition of feldspar. Groundmass in these samples was generally around one-half of the total, with the groundmass consisting of more than 90% feldspar, and accessory amounts of quartz, chlorite, sericite, carbonate, opaques. Sulphide minerals were mostly disseminated and as veinlets and clusters, and mostly pyrite and chalcopyrite with less common molybdenite and bornite. Carbonate minerals, mostly reported as veins, patches, and groundmass, were not individually identified and were sometimes seen as feldspar replacement/alteration.

Results of Acid-Base Accounting (ABA)

Paste pH in the 59 core samples for Schaft Creek ranged from 7.6 to 8.6. Thus, no samples were acidic at the time of analysis.

Total sulphur in the 59 Schaft Creek rock samples ranged from 0.02 to 1.91%S, with a mean of 0.45%S and a median of 0.26%S. In most samples, total sulphur and sulphide were similar, and thus the two parameters were typically interchangeable. Because a few samples did contain elevated leachable sulphate, sulphide is a better indicator of acid potential than total sulphur for Schaft Creek rock. However, in many samples, most sulphide was copper-bound sulphide (chalcopyrite) which may have less capacity to generate acidity. Therefore, each sample has a maximum "worst-case" Sulphide-Based Acid Potential (SAP) and a minimum "best-case" Pyrite-Calculated Acid Potential (PAP).

Sobek (EPA 600) Neutralization Potential (NP) ranged from 40 to 219 kg/t in the 59 Schaft Creek samples, with a mean of 97 and a median of 92 kg/t. These relatively high values explain why no acidic paste pH values were detected, and suggest there could be a long lag time (years to decades) before these samples might become acidic. The lack of acidic paste pH values precluded an initial estimate of Unavailable Neutralization Potential, so the common value of 10 kg/t is used here.

NP was typically greater than inorganic carbonate in many samples, meaning NP also reflected the presence of non-carbonate aluminosilicate minerals. These minerals have been documented in Schaft Creek rock. Also, NP did not correlate well with solid-phase calcium or magnesium levels, but some samples showed that calcium-bearing minerals could account for their NP levels.

Best-case and worst-case net balances of acid-generating and acid-neutralizing capacities were calculated for each of the 59 Schaft Creek samples. Overall, only 0-2% of the samples were net acid generating and 5-14% were "uncertain" based on generic criterion. Thus, most samples were net neutralizing. PPAU and PPFQ were the major rock units with uncertain samples, while net-acid-generating or uncertain samples were found in the minor rock units of ANDS, TOBR, BRIV, and DIOR.

To generally assess the spatial distribution of net balances, a general east-west cross-section showed the center area was net-neutralizing, while net-acid-generating and uncertain samples were found on the periphery. The general north-south cross-section showed uncertain samples were found in three adjacent holes. Based on this limited information, the net-acid-generating and uncertain samples may be spatially restricted in the Schaft Creek Deposit, but additional samples and geostatistical modelling are needed to confirm this.

Results of Total-Element Analyses

The 59 samples of Schaft Creek core were predominantly composed of silicon and aluminum, reflecting the abundant aluminosilicate minerals. Calcium, iron, potassium, magnesium, sodium, and Loss on Ignition (LOI) were also relatively abundant.

Compared to general crustal abundances, the 59 samples were frequently elevated in silver, bismuth, copper, molybdenum, and selenium, and occasionally elevated in sulphur, antimony, and tungsten. However, solid-phase levels do not typically reflect leaching rates into water, so additional testwork is needed on metal leaching.

Only copper showed some correlation with sulphide, reflecting the copper-bound sulphide discussed under Acid-Base Accounting. For Sobek Neutralization Potential, calcium showed some correlation. Samples of some rock units, particularly tourmaline breccia (TOBR), stood out as a distinct group for some elements like gallium, phosphorus, thallium, tungsten, and uranium.

Recommendations for Future ML-ARD Work

A phased approach, with each focussing on resolving uncertainties raised in previous ones, is recommended in the provincial ML-ARD Prediction Manual. Thus, based on the preceding information, we offer the following recommendations for the next phase of ML-ARD studies at the Schaft Creek Project.

- Overburden should be analyzed for ML-ARD potential. Up to several tens of meters of overburden have been reported in drillholes. This overburden in the pit area would be disturbed and oxidized during mining, and might be used for construction or reclamation during and after operation.

- Unavailable Neutralization Potential (UNP) could not be reliably estimated from available data (Section 4.1.3), but affects net balances. Therefore, UNP should be determined better for Schaft Creek. This would likely require humidity cells (see below).

- Most samples with NPR < 2 were between 1.0 and 2.0, meaning their ARD potential is “uncertain” at this time (Section 4.1.5). This uncertain range should be resolved for proper planning of waste management and water management. Humidity cells would help with this (see next recommendation).

- Six laboratory-based kinetic tests, known as humidity cells, should be conducted for at least 40 weeks on 1-kg samples of Schaft Creek rock. These would provide bulk rates of acid generation, neutralization, and metal leaching, and would help in resolving UNP and “uncertain” samples (see above). Previous information on weathered core suggested reaction rates in Schaft Creek rock were low.

- Four on-site leach tests, each containing up to approximately one tonne of disturbed rock or broken core, should be set up at Schaft Creek and periodically sampled as part of routine on-site water-quality monitoring. These would provide on-site drainage-chemistry data and are important for upscaling the smaller-scale humidity cells.

- At this time, the net-acid-generating and “uncertain” samples may be clustered in portions of the deposit, which would focus waste management and any special handling onto specific zones. To examine this clustering further, additional core samples, including 2006 holes, should be collected from across the deposit and submitted for expanded acid-base accounting and total-element contents. The results would be used in geostatistical modelling (see next recommendation).

- Three-dimensional geostatistical modelling should be carried out to calculate total tonnages and year-by-year tonnages of net-acid-generating, currently “uncertain”, and net-neutralizing rock. This is important for identifying the most cost-effective options for waste management and water management.

6. REFERENCES

Associated Mining Consultants Ltd. 2004. Preliminary Assessment of the Schaft Creek Deposit, British Columbia Project Status Report No. 1. Prepared for 955528 (Alberta) Ltd., dated September 20.

Copper Fox Metals Inc. 2006. Schaft Creek Copper-Gold-Molybdenum-Silver Deposit Project Description. Dated July 2006.

Fischer, P., and W. Hanych. 2006. 2005 Diamond Drill Report Schaft Creek Property Northwestern British Columbia for Copper Fox Metals Inc. Dated March 27.

Giroux, G.H., and E.A. Ostensoe. 2003. Summary Report Status and Resources Estimate Schaft Creek Property Northwestern British Columbia. Prepared for 955528 Alberta Ltd., dated June 30.

Morin, K.A., and N.M. Hutt. 2001. *Environmental Geochemistry of Minesite Drainage: Practical Theory and Case Studies, Digital Edition*. MDAG Publishing (www.mdag.com), Surrey, British Columbia. ISBN: 0-9682039-1-4.

Morin, K.A., and N.M. Hutt. 1997. *Environmental Geochemistry of Minesite Drainage: Practical Theory and Case Studies*. MDAG Publishing (www.mdag.com), Surrey, British Columbia. ISBN: 0-9682039-0-6.

Price, W.A., K.A. Morin, N.M. Hutt. 1997. Guidelines for the prediction of acid rock drainage and metal leaching for mines in British Columbia: Part II. Recommended procedures for static and kinetic testing. IN: Proceedings of the Fourth International Conference on Acid Rock Drainage, May 31-June 6, Vancouver, Canada, Volume I, p. 15-30.

Price, W.A., and J.C. Errington. 1998. Guidelines for Metal Leaching and Acid Rock Drainage at Minesites in British Columbia. Issued by the British Columbia Ministry of Energy and Mines.

Price, W.A. 1998. Draft Manual for the Prediction of Metal Leaching and Acid Rock Drainage. Issued by the British Columbia Ministry of Energy and Mines.

APPENDIX A. Notes on the Collection of Phase 1 ML/ARD Samples by MDAG, February 2007

Schaft Creek Project
Trip Report for Static-Test Sampling

K. Morin, February 9, 2007

On February 3 (Saturday), staff at Bandstra Transportation Systems opened Copper Fox' unheated storage locker. They sorted up to 20 skids to find the 63 buckets containing the initial list of samples for static testing (acid-base accounting and total-element analyses). This saved several hours of Rescan/MDAG time. The selected buckets were consolidated onto two skids, and brought inside to warm up so that saturated samples could be sampled. Six of the 63 sample buckets could not be found and were thus deleted from the sampling list. This left 57 samples to be collected.

On February 7, Kevin Morin flew to Smithers on the early morning flight. At Bandstra, he collected the 57 samples, plus two additional backup samples (Table 1). This involved prying open each bucket, noting the general colour and the dryness of the rejects (gravel, sand, and silt), then removing a few hundred grams from the top of the rejects. To minimize cross-contamination of metals, each sample was removed with a fibreglass hand shovel, after cleaning with disposable soapy wipes and clean paper towels. The two backup samples were collected from the bottom, rather than the top, of the rejects, to check for any significant geochemical variability within each reject bucket.

The 59 samples were shipped in the late afternoon of February 7, by Greyhound Courier, to ALS Chemex Labs in North Vancouver.

Project: **Schaft Creek Project**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: Samples collected for ABA, trace metal, and whole rock analysis On Feb 7'07 by Kevin Morin, MDAG.

Sample No.	Hole Id	Lithology From (m)	To (m)	Rock Code	Mineralization Style	Alteration Minerals Ch Chlorite	Ep Epidote	Bt Biotite	Se Sericite	K K-spar	Si Silicic	Hm Hematite	Cb	Tm Tourmaline	% Mt Magnetite
14545	05CF246	12.1	15.2	ANPF	Py,Cp dis	W-M						W			
14565	05CF246	63.6	66.7	ANPF	Cp cb-qtz-ch stkwk	W				W		W			
14571	05CF246	81.8	84.8	PPPL	Py,Cp dis, Mb cb-qtz-ch vn	W				W		X			
14578	05CF246	103.0	106.1	PPAU	Py dis, Cp ch stckwk	W-M				W-M		X			
14578B	05CF246	103.0	106.1	PPAU											
14598	05CF246	154.5	157.6	PPAU	Cp,Py dis	M									5
14689	05CF244	9.1	12.1	PPFQ	Py,Cp, dis, cb-qtz vn, frct	W			W	S		X			
14695	05CF244	27.3	30.3	PPAU	Py,Cp, dis	M-S				W		W			T
14742	05CF244	160.6	163.6	ANLP	Cp dis, Cp,Bn qtz-cb vn, Mb frct	W				W			W		1
14998	05CF248	36.4	39.4	ANPF	STKWK	W									
15862	05CF248	78.8	81.8	ANPF	STKWK, MB-Frct	W	W			W					
15870	05CF248	103.0	106.1	ANLP	STKWK	W				M		W			
15879	05CF248	130.3	133.3	BRVL	STKWK	W	W			W		W			
15887	05CF248	145.5	148.5	ANTF	STKWK, Dis	W	W				W		W		
15891	05CF248	157.6	160.6	ANPF	STKWK	W				W		W			
15908	05CF248	209.1	212.1	PPFQ	STKWK, MB-Frct, Dis, Flt	W									
15911	05CF248	218.2	221.2	ANDS	STKWK, Dis	W				W					
14130	05CF236	18.2	21.2	ANPF	Cu diss & qtz veins					S	W				
14144	05CF236	60.6	63.6	ANPF	Cu diss & veins	M				M-S	W	M			
14148	05CF236	72.7	75.8	FAUL	Cu diss	S				S		W			
14156	05CF236	87.9	90.9	FAUL	Mb fracture					W					
14162	05CF236	106.1	109.1	D/BS											W
14169	05CF236	127.3	130.3	PPFQ	Cu, Mb qtz veins & diss					M-S					
14018	05CF234	18.2	21.2	PPFQ	Disseminated + Vein	W	W		W	W					
14021	05CF234	27.3	30.3	TOBR	Hydro Bx Matrix (vein) + diss	M	W		M	M	M			X	
14036	05CF234	63.6	66.7	TOBR	Stockwork + disseminated	M			S	M	M			X	
14043	05CF234	84.8	87.9	TOBR	Stockwork + disseminated	W	W		M	M	W			X	
14060	05CF234	136.4	139.4	BRIV	Disseminated in matrix	M	M		M	M?		M?			
14067	05CF234	157.6	160.6	ANPF	Disseminated, vein	S	W		S	W	W				
14076	05CF235	18.2	21.2	ANDS	STKWK, Dis	W									
14083	05CF235	39.4	42.4	ANDS	STKWK	W	W								
14099	05CF235	87.9	90.9	PPFQ	Dis	W									
14103	05CF235	100.0	103.0	TOBR	Dis	W	W			W				M	
14232	05CF239	27.3	30.3	PPAU	dis, stkwk, bx vns, Mb frct					W					
14250	05CF239	72.7	75.8	PPAU	stkwk	W				W		W			
14260	05CF239	103.0	106.1	PPAU	stkwk, Cp, Bn in vns	W				W		W			
14276	05CF239	142.4	145.5	ANPF	stkwk, dis, Cp,Mb vns, Mb frct	W	W								
14295	05CF239	200.0	203.0	ANPF	stkwk, Py vns	W	W			W		W			
14301	05CF240	9.1	12.1	ANNX	STKWK, Mb Frct					S					
14323	05CF240	66.7	69.7	PPAU	STKWK, Cp-V	W				W					
14332	05CF240	93.9	97.0	PPAU	STKWK, Mb-Frct	W				W		W			
14345	05CF240	133.3	136.4	ANPF	STKWK, Dis	W				W					
14348	05CF240	142.4	145.5	PPAU	STKWK, Dis, Mb-Frct	W				W				W	
14666	05CF245	51.5	54.5	BRVL	STKWK, Dis, MB-Frct	W	W			W					
14685	05CF245	100.0	103.0	DIOR	STKWK, Dis, MB-Frct	W				M					
14685B	05CF245	100.0	103.0	DIOR											
14797	05CF243	9.1	12.1	PPAU	STKWK, Dis, MB-Frct	W				W					
14808	05CF243	42.4	45.5	FAUL	STKWK, MB-Frct, SHEAR	W				S					
14816	05CF243	66.7	69.7	PPAU	STKWK, PY-Vns	W				M		W			
14828	05CF243	103.0	106.1	PPAU	STKWK, Dis, MB-Frct	W				W					
14844	05CF243	142.4	145.5	ANDS	STKWK, CP-Vn, Dis	W									
14860	05CF243	190.9	193.9	PPAU	STKWK, MB-Frct, CP-Frct	W				W					W
14871	05CF243	224.2	227.3	ANLP	STKWK, CP-Vn,Frct, Dis, SHR,	W	W			W		W			

Project: **Schaft Creek Project**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: Samples collected for ABA, trace metal, and whole rock analysis On Feb 7'07 by Kevin Morin, MDAG.

Sample No.	Hole Id	Lithology From (m)	To (m)	Rock Code	Mineralization Style	Alteration Minerals Ch Chlorite	Ep Epidote	Bt Biotite	Se Sericite	K K-spar	Si Silicic	Hm Hematite	Cb	Tm Tourmaline	% Mt Magnetite
14887	05CF243	263.6	266.7	ANTF	STKWK, CP-Vn, Dis	W	W					W			
14893	05CF247	12.1	15.2	PPAU	Mal frct-1%, Cp dis	W									5
14899	05CF247	30.3	33.3	PPAU		X						X			
14908	05CF247	57.6	60.6	ANLP	Cp,Bn qtz-cb stkwk, Cp dis	W				W					
14917	05CF247	75.8	78.8	PPPL	Bn dis, qtz-cb vn	X		X		W-M					
14925	05CF247	100.0	103.0	ANLP	Cp qtz-cb vn, dis	W	X			X		W			3

Rock Code Legend:

ANDS	Andesite
ANNX	Altered Andesite
ANPF	Plagioclase-phyric or Feldspar-phyric Andesite
ANPL/ANLP	Andesitic Lapilli Tuff
ANTF	Andesitic Tuff
BRIV	Intrusive Breccia or Felsic Igneous Breccia
BRVL	Volcanic Breccia
BRXX	Diorite Breccia
D/BS	Diabase/Basic dyke
DIOR	Diorite
FAUL	Faults
PNBX	Pneumatolytic Breccia
PPAU	Plagioclase-Augite-phyric Andesite
PPFQ	Quartz-Feldspar or Feldspar-Quartz Porphyry
PPPL	Plagioclase or Feldspar Porphyry
SHER	Shear Zone / Faults
TOBR	Tourmaline Breccia
VN	Vein

Mineral Legend:

Ch	Chlorite
Ep	Epidote
Bt	Biotite
Se	Sericite
K	K-spar
Si	Silicic
Hm	Hematite
Mt	Magnetite
Tm	Tourmaline
Cp	Chalcopyrite
Bn	Bornite
Py	Pyrite
Mb	Molybdenite
Oth	See description
X	mineral present

Legend:

T	Trace
W	weak
M	moderate
S	strong

Project: **Schaft Creek Project**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: Samples collected for ABA, trace metal, and whole rock analysis On Feb 7'07 by Kevin Morin, MDAG.

Sample No.	Sulphides % Cp Chalcopyrite	Bn Bornite	Py Pyrite	Mb Molybdenite	Other	Total	Sampling Notes	Assay Data Cu (%)	Mo (%)	Au (g/t)	Ag (g/t)
14545	T		T			T	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.113	0.001	0.02	0.4
14565	T					T	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.289	0.002	0.14	0.6
14571	2.0		1.0	0.5		3.5	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines	0.593	0.011	0.13	1.8
14578	T		1.0			1.0	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines (see 14578B)	0.293	0.002	0.04	0.7
14578B							Subsample collected from bottom of rejects stored in white plastic bucket; dry, light grey gravel and fines (see 14578)				
14598	T		T			T	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.075	0.005	0.02	0.3
14689	0.5		1.0	0.5		2.0	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines	0.213	0.008	0.07	0.4
14695	T		0.5			0.5	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines	0.182	0.059	0.13	0.7
14742	T			0.5		0.5	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines	0.223	0.071	0.17	1.0
14998	T	T	0.5	T		0.5	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.169	0.007	0.14	0.5
15862	T	T		0.5		0.5	Subsample collected from top of rejects stored in white plastic bucket; moist, dark grey gravel and fines	0.116	0.008	0.14	0.6
15870	0.5	T	T	0.5		1.0	Subsample collected from top of rejects stored in white plastic bucket; saturated, medium grey gravel and fines	0.157	0.002	0.09	0.8
15879	0.5	T		T		0.5	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.224	0.003	0.15	1.5
15887	1.0	T		0.5		1.5	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.285	0.008	0.28	1.8
15891	T	0.5		0.5		1.0	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.234	0.011	0.21	1.5
15908	0.5	0.5		0.5		1.5	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.421	0.032	0.38	2.4
15911	0.5	0.5		0.5		1.5	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.179	0.017	0.15	1.0
14130	T	~1				1.0	Subsample collected from top of rejects stored in white plastic bucket; dry, grey and pink (granite?) gravel and fines	0.555	0.008	0.39	3.3
14144	T	~1				1.0	Subsample collected from top of rejects stored in white plastic bucket; dry, grey and pink (granite?) gravel and fines	0.290	0.008	0.20	2.2
14148		T				T	Subsample collected from top of rejects stored in white plastic bucket; saturated, medium grey gravel and fines	0.275	0.020	0.17	1.2
14156		T		1.0		1.0	Subsample collected from top of rejects stored in white plastic bucket; dry, grey and pink (granite?) gravel and fines	0.204	0.005	0.07	1.0
14162							Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines	0.115	0.051	0.09	<0.5
14169	1.0	1.0		<1		<2	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines	0.386	0.016	0.18	3.0
14018			1.0			1.0	Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines	0.147	0.007	0.06	<0.5
14021	2.0		T			2.0	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.173	0.036	0.03	<0.5
14036	4.0					4.0	Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines	0.189	0.061	0.04	5.8
14043	0.0					2.0	Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines	0.153	0.034	0.15	2.0
14060	T-1					T-1	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.280	0.032	0.04	<0.5
14067	1.0					1.0	Subsample collected from top of rejects stored in white plastic bucket; saturated, dark grey gravel and fines	0.247	0.014	0.03	<0.5
14076	T		T			T	Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey-green gravel and fines	0.173	0.005	0.16	<0.5
14083	T		1.0			1.0	Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines	0.130	0.001	0.01	<0.5
14099	0.5		1.0			1.0	Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines	0.157	0.002	0.02	1.1
14103	1.0		T			1.0	Subsample collected from top of rejects stored in white plastic bucket; dry, grey and pink (granite?) gravel and fines	0.266	0.022	0.02	1.0
14232	0.5	1.0	0.5	0.5		2.5	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines; low weight remaining	0.325	0.011	0.21	1.8
14250	0.5	1.0	0.5	0.5		2.5	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.300	0.038	0.33	2.0
14260	1.0	0.5	0.5	T		2.0	Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines	0.505	0.016	0.9	3.1
14276	2.0	T	0.5	1.0		3.5	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines; low weight remaining	0.136	0.003	<0.01	1.0
14295	0.5	T	0.5	T		1.0	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.250	0.001	0.07	0.5
14301	T		T	0.5		0.5	Subsample collected from top of rejects stored in white plastic bucket; dry, grey and pink (granite?) gravel and fines	0.241	0.023	0.09	0.6
14323	0.5	0.5	T	T		1.0	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines	0.200	0.005	0.18	1.6
14332	0.5	0.5	T	1.0		2.0	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines	0.336	0.010	0.16	1.5
14345	2.0	0.5	0.5	0.5		3.5	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines	0.559	0.020	0.19	2.4
14348	1.0	0.5	0.5	0.5		2.5	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines	0.461	0.013	0.13	1.4
14666	0.5		1.0	T		1.5	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.163	0.002	0.07	0.3
14685	0.5		2.0	T		2.5	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines (see 14685B)	0.455	0.013	0.18	0.6
14685B							Subsample collected from bottom of rejects stored in white plastic bucket; dry, medium grey gravel and fines (see 14685)				
14797	0.5	0.5		0.5		1.5	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.184	0.034	0.10	1.0
14808	0.5	0.5		2.0		3.0	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.257	0.040	0.28	1.7
14816	T	0.5	1.0	T		1.5	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines	0.387	0.008	0.57	2.3
14828	0.5	2.0		0.5		3.0	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.317	0.019	0.74	2.3
14844	1.0	0.5	0.5	T		2.0	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.249	0.010	0.16	1.0
14860	1.0	0.5		0.5		2.0	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.373	0.035	0.25	2.5
14871	2.0	0.5		T		2.5	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.365	0.034	0.10	0.7

Project: **Schaft Creek Project**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: Samples collected for ABA, trace metal, and whole rock analysis On Feb 7'07 by Kevin Morin, MDAG.

	Sulphides %						**Sampling Notes**	**Assay Data**			
Sample No.	Cp Chalcopyrite	Bn Bornite	Py Pyrite	Mb Molybdenite	Other	Total		Cu (%)	Mo (%)	Au (g/t)	Ag (g/t)
14887	0.5		0.5			1.0	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.196	0.00	0.07	0.7
14893							Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.164	0.008	0.12	0.9
14899							Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.032	0.002	0.03	0.7
14908	1.5	T				0.5	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.113	0.005	0.08	0.7
14917		0.5				0.5	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.361	0.001	0.31	2.5
14925	T					T	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines	0.182	0.001	0.11	1.0

Mineral Legend:

Ch	Chlorite
Ep	Epidote
Bt	Biotite
Se	Sericite
K	K-spar
Si	Silicic
Hm	Hematite
Mt	Magnetite
Tm	Tourmaline
Cp	Chalcopyrite
Bn	Bornite
Py	Pyrite
Mb	Molybdenite
Oth	See description
X	mineral present

Legend:

T	Trace
W	weak
M	moderate
S	strong

APPENDIX B. Compiled Acid-Base Accounting and Total-Element Analyses for Rock at the Schaft Creek Project

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Hole Id	Lithology From (m)	To (m)	Interval (m)	Centre of Interval (m)	Zone	Rock Code	Rock Code Description	Mineralization Style
14018	05CF234	18.2	21.2	3.03	19.70	West Breccia	PPFQ	Quartz-Feldspar or Feldspar-Quartz Porphyry	Disseminated + Vein
14021	05CF234	27.3	30.3	3.03	28.79	West Breccia	TOBR	Tourmaline Breccia	Hydro Bx Matrix (vein) + diss
14036	05CF234	63.6	66.7	3.03	65.15	West Breccia	TOBR	Tourmaline Breccia	Stockwork + disseminated
14043	05CF234	84.8	87.9	3.03	86.36	West Breccia	TOBR	Tourmaline Breccia	Stockwork + disseminated
14060	05CF234	136.4	139.4	3.03	137.88	West Breccia	BRIV	Intrusive Breccia or Felsic Igneous Breccia	Disseminated in matrix
14067	05CF234	157.6	160.6	3.03	159.09	West Breccia	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	Disseminated, vein
14076	05CF235	18.2	21.2	3.03	19.70	West Breccia	ANDS	Andesite	STKWK, Dis
14083	05CF235	39.4	42.4	3.03	40.91	West Breccia	ANDS	Andesite	STKWK
14099	05CF235	87.9	90.9	3.03	89.39	West Breccia	PPFQ	Quartz-Feldspar or Feldspar-Quartz Porphyry	Dis
14103	05CF235	100.0	103.0	3.03	101.52	West Breccia	TOBR	Tourmaline Breccia	Dis
14130	05CF236	18.2	21.2	3.03	19.70	Liard Main	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	Cu diss & qtz veins
14144	05CF236	60.6	63.6	3.03	62.12	Liard Main	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	Cu diss & veins
14148	05CF236	72.7	75.8	3.03	74.24	Liard Main	FAUL	Faults	Cu diss
14156	05CF236	87.9	90.9	3.03	89.39	Liard Main	FAUL	Faults	Mb fracture
14162	05CF236	106.1	109.1	3.03	107.58	Liard Main	D/BS	Diabase/Basic dyke	
14169	05CF236	127.3	130.3	3.03	128.79	Liard Main	PPFQ	Quartz-Feldspar or Feldspar-Quartz Porphyry	Cu, Mb qtz veins & diss
14232	05CF239	27.3	30.3	3.03	28.79	Liard Main	PPAU	Plagioclase-Augite-phyric Andesite	dis, stkwk, bx vns, Mb frct
14250	05CF239	72.7	75.8	3.03	74.24	Liard Main	PPAU	Plagioclase-Augite-phyric Andesite	stkwk
14260	05CF239	103.0	106.1	3.03	104.55	Liard Main	PPAU	Plagioclase-Augite-phyric Andesite	stkwk, Cp, Bn in vns
14276	05CF239	142.4	145.5	3.03	143.94	Liard Main	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	stkwk, dis, Cp,Mb vns, Mb frct
14295	05CF239	200.0	203.0	3.03	201.52	Liard Main	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	stkwk, Py vns
14301	05CF240	9.1	12.1	3.03	10.61	Liard Main	ANNX	Altered Andesite	STKWK, Mb Frct
14323	05CF240	66.7	69.7	3.03	68.18	Liard Main	PPAU	Plagioclase-Augite-phyric Andesite	STKWK, Cp-V
14332	05CF240	93.9	97.0	3.03	95.45	Liard Main	PPAU	Plagioclase-Augite-phyric Andesite	STKWK, Mb-Frct
14345	05CF240	133.3	136.4	3.03	134.85	Liard Main	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	STKWK, Dis
14348	05CF240	142.4	145.5	3.03	143.94	Liard Main	PPAU	Plagioclase-Augite-phyric Andesite	STKWK, Dis, Mb-Frct
14797	05CF243	9.1	12.1	3.03	10.61	Liard Main	PPAU	Plagioclase-Augite-phyric Andesite	STKWK, Dis, MB-Frct
14808	05CF243	42.4	45.5	3.03	43.94	Liard Main	FAUL	Faults	STKWK, MB-Frct, SHEAR
14816	05CF243	66.7	69.7	3.03	68.18	Liard Main	PPAU	Plagioclase-Augite-phyric Andesite	STKWK, PY-Vns
14828	05CF243	103.0	106.1	3.03	104.55	Liard Main	PPAU	Plagioclase-Augite-phyric Andesite	STKWK, Dis, MB-Frct
14844	05CF243	142.4	145.5	3.03	143.94	Liard Main	ANDS	Andesite	STKWK, CP-Vn, Dis
14680	05CF243	190.9	193.9	3.03	192.42	Liard Main	PPAU	Plagioclase-Augite-phyric Andesite	STKWK, MB-Frct, CP-Frct
14871	05CF243	224.2	227.3	3.03	225.76	Liard Main	ANLP	Andesitic LapilliTuff	STKWK, CP-Vn,Frct, Dis, SHR,
14887	05CF243	263.6	266.7	3.03	265.15	Liard Main	ANTF	Andesitic Tuff	STKWK, CP-Vn, Dis
14689	05CF244	9.1	12.1	3.03	10.61	Liard Main	PPFQ	Quartz-Feldspar or Feldspar-Quartz Porphyry	Py,Cp, dis, cb-qtz vn, frct
14695	05CF244	27.3	30.3	3.03	28.79	Liard Main	PPAU	Plagioclase-Augite-phyric Andesite	Py,Cp, dis
14742	05CF244	160.6	163.6	3.03	162.12	Liard Main	ANLP	Andesitic LapilliTuff	Cp dis, Cp,Bn qtz-cb vn, Mb frct
14666	05CF245	51.5	54.5	3.03	53.03	Liard Main	BRVL	Volcanic Breccia	STKWK, Dis, MB-Frct
14685	05CF245	100.0	103.0	3.03	101.52	Liard Main	DIOR	Diorite	STKWK, Dis, MB-Frct
14685B	05CF245	100.0	103.0	3.03	101.52	Liard Main	DIOR	Diorite	
14545	05CF246	12.1	15.2	3.03	13.64	Liard Main	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	Py,Cp dis
14565	05CF246	63.6	66.7	3.03	65.15	Liard Main	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	Cp cb-qtz-ch stkwk
14571	05CF246	81.8	84.8	3.03	83.33	Liard Main	PPPL	Plagioclase or Feldspar Porphyry	Py,Cp dis, Mb cb-qtz-ch vn
14578	05CF246	103.0	106.1	3.03	104.55	Liard Main	PPAU	Plagioclase-Augite-phyric Andesite	Py dis, Cp ch stckwk
14578B	05CF246	103.0	106.1	3.03	104.55	Liard Main	PPAU	Plagioclase-Augite-phyric Andesite	
14598	05CF246	154.5	157.6	3.03	156.06	Liard Main	PPAU	Plagioclase-Augite-phyric Andesite	Cp,Py dis
14893	05CF247	12.1	15.2	3.03	13.64	Liard Main	PPAU	Plagioclase-Augite-phyric Andesite	Mal frct-1%, Cp dis
14899	05CF247	30.3	33.3	3.03	31.82	Liard Main	PPAU	Plagioclase-Augite-phyric Andesite	
14908	05CF247	57.6	60.6	3.03	59.09	Liard Main	ANLP	Andesitic LapilliTuff	Cp,Bn qtz-cb stkwk, Cp dis
14917	05CF247	75.8	78.8	3.03	77.27	Liard Main	PPPL	Plagioclase or Feldspar Porphyry	Bn dis, qtz-cb vn
14925	05CF247	100.0	103.0	3.03	101.52	Liard Main	ANLP	Andesitic LapilliTuff	Cp qtz-cb vn, dis
14998	05CF248	36.4	39.4	3.03	37.88	Liard Main	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	STKWK
15862	05CF248	78.8	81.8	3.03	80.30	Liard Main	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	STKWK, MB-Frct
15870	05CF248	103.0	106.1	3.03	104.55	Liard Main	ANLP	Andesitic LapilliTuff	STKWK
15879	05CF248	130.3	133.3	3.03	131.82	Liard Main	BRVL	Volcanic Breccia	STKWK
15887	05CF248	145.5	148.5	3.03	146.97	Liard Main	ANTF	Andesitic Tuff	STKWK, Dis
15891	05CF248	157.6	160.6	3.03	159.09	Liard Main	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	STKWK
15908	05CF248	209.1	212.1	3.03	210.61	Liard Main	PPFQ	Quartz-Feldspar or Feldspar-Quartz Porphyry	STKWK, MB-Frct, Dis, Flt

Project:	**Schaft Creek**
Client:	Copper Fox Metals Inc.
Data:	**Sample Information**
Comments:	Sampled by MDAG on Feb 7'07. For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Hole Id	**Lithology** From (m)	To (m)	Interval (m)	Centre of Interval (m)	Zone	Rock Code	Rock Code Description	Mineralization Style
15911	05CF248	218.2	221.2	3.03	219.70	Liard Main	ANDS	Andesite	STKWK, Dis

Rock Code Legend:

ANDS	Andesite
ANNX	Altered Andesite
ANPF	Plagioclase-phyric or Feldspar-phyric Andesite
ANPL/ANLP	Andesitic Lapilli Tuff
ANTF	Andesitic Tuff
BRIV	Intrusive Breccia or Felsic Igneous Breccia
BRVL	Volcanic Breccia
BRXX	Diorite Breccia
D/BS	Diabase/Basic dyke
DIOR	Diorite
FAUL	Faults
PNBX	Pneumatolytic Breccia
PPAU	Plagioclase-Augite-phyric Andesite
PPFQ	Quartz-Feldspar or Feldspar-Quartz Porphyry
PPPL	Plagioclase or Feldspar Porphyry
SHER	Shear Zone / Faults
TOBR	Tourmaline Breccia
VN	Vein

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample	Alteration Minerals									%	Sulphides %						Assay Data			
Id.	Ch	Ep	Bt	Se	K	Si	Hm	Cb	Tm	Mt	Cp	Bn	Py	Mb	Other	Total	Cu	Mo	Au	Ag
	Chlorite	Epidote	Biotite	Sericite	K-spar	Silicic	Hematite		Tourmaline	Magnetite	Chalcopyrite	Bornite	Pyrite	Molybdenite			(%)	(%)	(g/t)	(g/t)
14018	W	W		W	W								1.0			1.0	0.147	0.007	0.06	<0.5
14021	M	W		M	M	M			X		2.0		T			2.0	0.173	0.036	0.03	<0.5
14036	M			S	M	M			X		4.0					4.0	0.189	0.061	0.04	5.8
14043	W	W		M	M	W			X		0.0					2.0	0.153	0.034	0.15	2.0
14060	M	M		M	M?		M?				T-1					T-1	0.280	0.032	0.04	<0.5
14067	S	W		S	W	W					1.0					1.0	0.247	0.014	0.03	<0.5
14076	W										T		T			T	0.173	0.005	0.16	<0.5
14083	W	W									T		1.0			1.0	0.130	0.001	0.01	<0.5
14099	W										0.5		1.0			1.0	0.157	0.002	0.02	1.1
14103	W	W			W				M		1.0		T			1.0	0.266	0.022	0.02	1.0
14130					S	W					T	~1				1.0	0.555	0.008	0.39	3.3
14144	M				M-S	W	M				T	~1				1.0	0.290	0.008	0.20	2.2
14148	S				S		W					T				T	0.275	0.020	0.17	1.2
14156					W							T		1.0		1.0	0.204	0.005	0.07	1.0
14162										W							0.115	0.051	0.09	<0.5
14169					M-S						1.0	1.0		<1		<2	0.386	0.016	0.18	3.0
14232					W						0.5	1.0	0.5	0.5		2.5	0.325	0.011	0.21	1.8
14250	W				W		W				0.5	1.0	0.5	0.5		2.5	0.300	0.038	0.33	2.0
14260	W				W		W				1.0	0.5	0.5	T		2.0	0.505	0.016	0.9	3.1
14276	W	W									2.0	T	0.5	1.0		3.5	0.136	0.003	<0.01	1.0
14295	W	W			W		W				0.5	T	0.5	T		1.0	0.250	0.001	0.07	0.5
14301					S						T		T	0.5		0.5	0.241	0.023	0.09	0.6
14323	W				W						0.5	0.5	T	T		1.0	0.200	0.005	0.18	1.6
14332	W				W		W				0.5	0.5	T	1.0		2.0	0.336	0.010	0.16	1.5
14345	W				W						2.0	0.5	0.5	0.5		3.5	0.559	0.020	0.19	2.4
14348	W				W				W		1.0	0.5	0.5	0.5		2.5	0.461	0.013	0.13	1.4
14797	W				W						0.5	0.5		0.5		1.5	0.184	0.034	0.10	1.0
14808	W				S						0.5	0.5		2.0		3.0	0.257	0.040	0.28	1.7
14816	W				M		W				T	0.5	1.0	T		1.5	0.387	0.008	0.57	2.3
14828	W				W						0.5	2.0		0.5		3.0	0.317	0.019	0.74	2.3
14844	W										1.0	0.5	0.5	T		2.0	0.249	0.010	0.16	1.0
14680	W				W					W	1.0	0.5		0.5		2.0	0.373	0.035	0.25	2.5
14871	W	W			W		W				2.0	0.5		T		2.5	0.365	0.034	0.10	0.7
14887	W	W					W				0.5		0.5			1.0	0.196	0.00	0.07	0.7
14689	W			W	S		X				0.5		1.0	0.5		2.0	0.213	0.008	0.07	0.4
14695	M-S				W		W			T	T		0.5			0.5	0.182	0.059	0.13	0.7
14742	W				W			W		1	T			0.5		0.5	0.223	0.071	0.17	1.0
14666	W	W			W						0.5		1.0	T		1.5	0.163	0.002	0.07	0.3
14685	W				M						0.5		2.0	T		2.5	0.455	0.013	0.18	0.6
14685B																				
14545	W-M						W				T		T			T	0.113	0.001	0.02	0.4
14565	W				W		W				T					T	0.289	0.002	0.14	0.6
14571	W				W		X				2.0		1.0	0.5		3.5	0.593	0.011	0.13	1.8
14578	W-M				W-M		X				T		1.0			1.0	0.293	0.002	0.04	0.7
14578B																				
14598	M									5	T		T			T	0.075	0.005	0.02	0.3
14893	W									5							0.164	0.008	0.12	0.9
14899	X						X										0.032	0.002	0.03	0.7
14908	W				W						1.5	T				0.5	0.113	0.005	0.08	0.7
14917	X		X		W-M							0.5				0.5	0.361	0.001	0.31	2.5
14925	W	X			X		W			3	T					T	0.182	0.001	0.11	1.0
14998	W										T	T	0.5	T		0.5	0.169	0.007	0.14	0.5
15862	W	W			W						T	T		0.5		0.5	0.116	0.008	0.14	0.6
15870	W				M		W				0.5	T	T	0.5		1.0	0.157	0.002	0.09	0.8
15879	W	W			W		W				0.5	T		T		0.5	0.224	0.003	0.15	1.5
15887	W	W				W		W			1.0	T		0.5		1.5	0.285	0.008	0.28	1.8
15891	W				W		W				T	0.5		0.5		1.0	0.234	0.011	0.21	1.5
15908	W										0.5	0.5		0.5		1.5	0.421	0.032	0.38	2.4

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample	Alteration Minerals									%	Sulphides %						Assay Data			
Id.	Ch	Ep	Bt	Se	K	Si	Hm	Cb	Tm	Mt	Cp	Bn	Py	Mb	Other	Total	Cu	Mo	Au	Ag
	Chlorite	Epidote	Biotite	Sericite	K-spar	Silicic	Hematite		Tourmaline	Magnetite	Chalcopyrite	Bornite	Pyrite	Molybdenite			(%)	(%)	(g/t)	(g/t)
15911	W				W						0.5	0.5		0.5		1.5	0.179	0.017	0.15	1.0

Mineral Legend:

Ch	Chlorite
Ep	Epidote
Bt	Biotite
Se	Sericite
K	K-spar
Si	Silicic
Hm	Hematite
Mt	Magnetite
Tm	Tourmaline
Cp	Chalcopyrite
Bn	Bornite
Py	Pyrite
Mb	Molybdenite
Oth	See description
X	mineral present

Legend:

T	Trace
W	weak
M	moderate
S	strong

Mineral Legend:

Ch	Chlorite
Ep	Epidote
Bt	Biotite
Se	Sericite
K	K-spar
Si	Silicic
Hm	Hematite
Mt	Magnetite
Tm	Tourmaline
Cp	Chalcopyrite
Bn	Bornite
Py	Pyrite
Mb	Molybdenite
Oth	See description
X	mineral present

Legend:
T
W
M
S

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Description
14018	Quartz-feldspar porphyry of plag + k-spar + qtz + hbl. Hornblende is typically altered to chlorite. Light sericitic alteration of feldspars. Trace pyrite is disseminated and very-fine-grained. Locally some trace fine-grained epidote. Greater sulphide content is observed around fractures and fine quartz- carbonate veins, locally accounting for close to 1% by volume. These veins are randomly oriented, short (typically <2cm), and narrow (<3mm). Phenocrysts are medium- to coarse-grained. Compositionally the rock contains too much K-spar to be considered a quartz monzonite, but is rather more granodioritic in composition, however much of the k-spar could be secondary. Pyrite seems to occur preferentially with secondary chlorite replacement of hornblende. -From 18.6 - 19.8 m: fairly wide vein (~1cm) hosting notable pyrite and possible chalcopyrite.
14021	Tourmaline Breccia. Unit is primarily porphyritic quartz-feldspar with primarily medium-grained plagioclase phenocrysts. "Wall-rock" is identical to the unit described above, and this unit is really the same lithology having undergone intense hydrothermal fracturing and veining. Where altered, the unit appears coarser-grained due to the "meshing" of finer groundmass grains by k-spar, which is then later overprinted by sericite and light chloritic alteration, particularly of secondary biotite from potassic phase. The name of this unit is derived from the presence of hydrothermal "vein" material which locally brecciates the rock. A more appropriate name would be "Hydrothermally brecciated porphyritic granodiorite", although the system really more of a stockwork, as there is little evidence of clast movement. No heterolithic clasts, all in-situe, sharp, and angular to subangular clasts. The primary hydrothermal mineral is quartz with local feldspar and a pervasive dark blue-grey minera historically described as tourmaline. Locally, tourmaline is easily identifiable by it's acicular habit in the hydrothermal "vein" material, and may account for the rest of the blue-grey material. Ratio of wall-rock to vein material is roughly 70% wall rock
14036	As above, same texture. 62.8 - 69.8 m: Degree of brecciation decreases. Similar texturally to interval at 53.9 - 58.5 m. Mostly highly potassically altered porphyritic wall rock overprinted by sericite, silica, and chlorite. Locally zones of intense, but spatially restricted tourmaline veining/brecciation/stockwork. Sulphide content decreases to 1-2%. Photo of typical texture (Photo 12) at 65.1 - 65.5 m showing association of very intense potassic alteration with tourmaline veining. Chalcopyrite is restricted almost exclusively to the hydrothermal veins.
14043	As TOBR unit above. Locally trace molybdenite paint on fracture surfaces and down to ~88.4 m, after which no molybdenite is observed. Very light epidote is observed starting at 76.8 m, and is observed to increase downhole. Locally chalcopyrite approaches 10%, but averages to roughly 2%. Due to the very locally varying intensity of, and nature of, the hydrothermal stockwork veining, this unit could possibly be better described as a stockwork - a term which could possibly be applied to the entire hole reflecting the variable degree of fracturing as a result of a violent fluid event. Photo 14 taken of box 39 showing typical stockwork texture (82.0 - 84.1 m).
14060	Felsic intrusive breccia. Matrix is felsic, fine-grained, and roughly equigranular with either clasts, or zones, of variable alteration of locally intense epidote and potassic (possibly hematite?) alteration. More mafic clasts have sharp boundaries and are angular to subangular, and tend to be more fine-grained. Upper one meter (down to 122.5m) is more massive, and less fractured (brecciated) than further downhole. Photo 24 was taken at 136.8 - 137.5 m as a texturally representative photo of the igneous breccia unit. (sample 05-JES-228 was also collected from this interval).
14067	Pyroxene-phyric andesite (pyroxene phenocrysts). "Contact" with TOBR is not such, but this lithology passes up into the TOBR unit up to 152.4 m. "Contact" is more a gradual decrease in the volume of hydrothermal vein material relative to the host rock, with a corresponding decrease in sulphides. Sulphide % ~1-2%, primarily chalcopyrite with trace pyrite. Chlorite and sericite alteration (possibly overprinting weak potassic). Locally epidote, usually associated with tourmaline/quartz "Stringers" or veins distal to the stockwork zone. Chloritic alteration is variable and centered around hairline veins. Photo 27 is typical of the textures within this unit (Sample 05-JES-230). Minor randomly oriented quartz veins without tourmaline are barren and possibly were filling fractures. These minor veins are typically <2mm wide.
14076	Fine grained andesite. Weak brecciation and veining: epidote-carb-quartz, accessory pyrite, in part vuggy. Strong fracturing, low angle CA. Core rubbly. 1-2% pyrite, disseminated, associated with fractures.
14083	Andesite. Fine grained,similar to 15.8 m. Strongly fractured, moderately veined (epidote-carb-quartz). Locally developed as breccia.
14099	Ditto above 71.0 m. [Quartz-feldspar porphyry. Fine grained, colour light green grey. Partly brecciated by 5-10% cm portions of pneumatolytic breccia, low angle CA. greenish colour probably caused by sericite alteration.] Quartz-feldspar porphyry. Variously and erratically permeated by 5-30% cm-dm stringers of pneumatolytic breccia, both as 'dykes' with strong flow fabric and as stockwork. In places 0.3- 1.0 m portions of andesite. Orientation of breccia fabric 0-30CA. Sulphides generally trac to 1% each pyrite, chalcopyrite.
14103	Tourmaline Breccia. Clasts of felsic intrusives, generally pink colour. Matrix made up of tourmaline, epidote, chlorite with accessory sulphides. Strong variation in matrix abundance from 1 to 30%. Lithology of clasts variable, including andesite, porphyritic andesite, felsic porphyry. Sulphide minerals are chalcopyrite and pyrite, with trace molybdenite. Abundance of sulphides varies strongly, from trace to 10%. Sulphides are generally disseminated in matrix, to a minor degree disseminated in clasts.
14130	Moderate- Strongly Altered Plagioclase-Phyric Andesite. Variable colour from pink to grey, with pink overprinting resulting from K -alteration of andesite. Most intense flanking cm-scale low angle quartz veins, and forming meter-scale alteration envelopes, pervasive into host. Areas of high fracturing dominated by carbonate-chlorite filling. Randomly oriented, low-high angle mm-cm scale quartz veining, with erratic sulphide mineralization of chalcopyrite and bornite in trace to <1% over the section.
14144	Moderately-Strongly Altered Plagioclase-Phyric Andesite. Variably altered, similar to 6.4 - 36.6 m. Locally strong fault gouge and breccia developed. 57.9 - 61.0 m cm sections of fault gouge and broken core. 61.0 - 64.0 m medium to high angle fau gouge and breccia along 30cm length with a 20cm section at 61.9 m of a low angle hematized vein breccia.
14148	Fault Zone - Tectonic Deformation and Alteration Zone. 70.0 - 73.0 m cm-dm sections of intense deformation and ateration, similar to above. Strong chloritization and silicification. Disseminated bornite associatd with chloritization and quartz vein material. Chloritization over-printing K-alteration. 73.1 - 76.2 m intense chloritization and fault gouge anastomizing at low angle to core. Chloritization over-printing K-alteration. Cm sections of highly comminuted rock developing rock flour and soft clay rich zones.
14156	Fault Zone - Tectonic Deformation and Alteration Zone. 87.2 - 96.0 m relict protolith of possible feldspar porphyry displaying variable K-alteration.
14162	107.3-109.3 m: Mafic Dyke. Dark grey, fine grain, with 10% 0.5-3mm carbonate amygdules. Upper and lower contact at low angle with strong carbonatization and bleaching along 20cm , especially the lower contact. Section contains mm low angle carbonate veinlets. Upper contact displays weak chill margin. 106.1-107.3 m: Feldspar-Quartz Porphyry. Variable K-alteration diffuse through section with meter lengths of intense alteration. 103.6 - 107.3 m Very low angle sub-parallel mm-cm quartz veins with 10% bornite along 10cm length.
14169	Feldspar-Quartz Porphyry. Predominantly pink. Variable K-alteration ranging from moderate to strong. MM stockwork and quartz veinlets concentrated in zones. Bornite and chalcopyrite mineralization associated with with stockwork with bornite being greater than chlcopyrite, with total sulphide concentrations of up to 7% along 30cm. Minor molybdenite. Sulphides are also finely disseminated in wall rock with stringer-type concentrations associated with quartz veins. Late molybdenite is smeared or painted along fracture planes trace chalcopyrite. Typically the fractures are at a low-medium angle and average 1per meter.
14232	Plagioclase-augite porphyry andesite... pink-grey. Moderate potassic alteration. Core in part strongly fractured. Plagioclase phenocrysts light green, epidote alteration? Moderate stockwork of mm veins, medium-low angle, in part vuggy, mm to 2cm spacing: Quartz veins, carbonate veins, talc(?)-chlorite veins. Total sulphides 2%: 0.5% each, bornite, chalcopyrite, pyrite in veins and adjacent to veins. Very fine chalcopyrite commonly replacing augite crystals.
14250	Augite porphyry. Similar to above. Fine grained, porphyritic. Colour generally dark green-grey with minor pink grey, weak potassic alteration: 85.3 - 101.2 m higher abundance of quartz-stockwork with chalcopyrite, bornite. Quartz-carbonate stockwork strongly variable, generally low abundance.
14260	Augite porphyry. Similar to above. Fine grained, porphyritic. Colour generally dark green-grey with minor pink grey, weak potassic alteration: 85.3 - 101.2 m higher abundance of quartz-stockwork with chalcopyrite, bornite. Quartz-carbonate stockwork strongly variable, generally low abundance. 96.0 - 106.7 m Alternating weak chlorite alteration and weak potassic alteration. Weak quartz-carbonate stockwork, ~0.5% each chalcopyrite, bornite, pyrite, trace molybdenite.
14276	Plagioclase-phyric, porphyritic andesite. Fine grained, massive, generally competent. Fine grained groundmass with 10% 0.5-2mm plagioclase phenocrysts. Colour medium green-grey, locally beige. Alteration weak: Chlorite, epidote, hematite, loca potassic. Veining, stockwork generally weak-moderate: mm-1cm quartz veins, carbonate veins, cm-10cm spacing, random orientation. Locally strong stockwork and vein breccia, ft size. Sulphides predominantly in stockwork, minor disseminated. Moly commonly on slickensides, in fractures. Sulphide abundance 0.5% for each chalcopyrite, bornite, trace molybdenite. Locally high chalcopyrite abundance in mm to 10mm veins, essentially massive chalcopyrite veins. 139.0 - 150.9 m dark green chlorite alteration. Low vein density. Rare 1mm massive chalcopyrite veins and molybdenite coated slickensides, fractures.

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Description
14295	Plagioclase-phyric, porphyritic andesite. Fine grained, massive, generally competent. Fine grained groundmass with 10% 0.5-2mm plagioclase phenocrysts. Colour medium green-grey, locally beige. Alteration weak: Chlorite, epidote, hematite, loca potassic. Veining, stockwork generally weak-moderate: mm-1cm quartz veins, carbonate veins, cm-10cm spacing, random orientation. Locally strong stockwork and vein breccia, ft size. Sulphides predominantly in stockwork, minor disseminated. Moly commonly on slickensides, in fractures. Sulphide abundance 0.5% for each chalcopyrite, bornite, trace molybdenite. Locally high chalcopyrite abundance in mm to 10mm veins, essentially massive chalcopyrite veins. 199.0 - 212.7 m fine grained, dark green-grey, minor pink potassic alteration. Core competent. Weak stockwork of 1mm carbonate veins, quartz veins, in part with high abundance of sulphides (pyrite, chalcopyrite). Common 5-10mm pink potassic vein halos. Overall sulphides: 0.5-1% of each chalcopyrite, pyrite, in veins, halos.
14301	Altered Andesite - Moderate-Strong. Variable pink to grey. Variable dm-meter scale K-alteration ranging from moderate to strong, with dm-meter sections of weak incipient alteration. Light green alteration associated with mm carbonate veinlets appears to overprint the K-alteration, and may in part be epidote and serictic alteration. Areas of intense K-alteration completely obliterate protolith and are usually associated with stockwork arrray of mm-cm carbonate-quartz veins containing disseminated molybdenite and bornite. 10.8 - 12.8 m medium grey-green, fine grained with mm carbonate amygdules and mm low angle carbonate veinng. Possibly a late mafic dyke.
14323	Augite-Phyric Andesite. Medium grey, fine grain, with 3-5% 1-4mm anhedral augite phenocrysts displaying hematite rich rims and cores of chlorite-hematite. Some show distinct pseudomorphing of hexagonal crystal form. Overall this unit exhibits weak pervasive chloritization. Low to medium angle carbonate-chlorite fractures averaging 6/meter.
14332	Augite-Phyric Andesite. Medium grey, fine grain, with 3-5% 1-4mm anhedral augite phenocrysts displaying hematite rich rims and cores of chlorite-hematite. Some show distinct pseudomorphing of hexagonal crystal form. Overall this unit exhibits weak pervasive chloritization. Low to medium angle carbonate-chlorite fractures averaging 6/meter.
14345	Weakly-Moderately Altered Plagioclase-Phyric Andesite. Pale pink-grey. Weak to moderate pervasive K-alteration. Where alteration is quite strong the feldspar phenocryst component of the rock become highly accentuated. 2-5mm, medium-high angle carbonate-quartz-molybdenite veins spaced at 2-3/meter. 125.0 - 142.8 m moderate to strong K-alteration overprinted by a network of mm-cm fluid phase, dominated by carbonate and mineralized with fine grain disseminated chalcopyrite carrying up to 7%, and forming a stockwork array with diffuse boundaries and does not appear to be vein associated. More of a late mineralization phase which may also be contributing to painted molybdenite on fracture planes.
14348	Augite-Phyric Andesite. Fractured containing carbonate-chlorite filling and K-alteration envelopes on a mm-cm scale. Upper contact is fault controlled at high angle.
14797	Variably Altered Augite-Feldspar-Phyric Andesite. Intensely broken core resulting in high rubble content. Variable K-alteration from moderate to strong associated with mm-cm quartz-carbonate stockwork veining dominated by bornite mineralization. Moderate pervasive chloritization along meter lengths, accompanied by intense chlorite hairline chlorite veinlets forming a crackle breccia. Overall 5% magnetite.
14808	Fault Zone. 41.3 - 49.0 m; very strong chloritization and carbonatization resulting in veining and crackle brecciation of an earlier intense K-alteration phase. Heavy gouge and rubble developed along meter lengths. Late chlorite veinlets throughout. Dm section of low angle shearing and brittle deformation resulting in mylonite.
14816	Variably Altered Augite -Phyric Andesite. Moderate to intense pervasive K-alteration and chloritization completely obliterating protolith. Ghosty spotty hematization forming cm patches resulting from the overprinting by K-alteration. Highly fractured w cm sections of fault gouge. Mm-cm medium to high angle quartz-carbonate -chlorite veins some heavily mineralized with bornite.
14828	Marginal Alteration-Transition Zone -Augite-Phyric Andesite. Variable K-alteration ranging from weak to moderate with patchy mm-cm ghosty relic host inclusions, and associated with pervasive chloritization imparting a green hue to the host rock. 96.9 - 104.8 m; mm randomly oriented quartz-carbonate veins forming a weak stockwork array.
14844	Andesite. Grey, fine grain, masive, Incipient crackle brecciation developed by hairline to 3mm randomly oriented carbonate veinlets. Rare 5mm quartz-carbonate veins with bornite. Rare molybdenite painted fractures.
14680	Augite-Feldspar-Phyric Andesite. Grey-green, massive with weak patchy K-alteration, rare mm epidote and darker blotchy areas of high magnetite. Mm randomly oriented quartz-carbonate veins with molybdenite and bornite, about 2/meter.
14871	Andesitic Tuff-Lapilli Tuff. Medium grey, massive to interbeded tuff-lapilli tuff with dm sections of lithic tuff. Bedding at very low angle to core. Dominant mineralization is associated with mm quartz-carbonate veinlets carrying disseminated chalcopyrite and bornite and occasional chalcopyrite stringers. All veining in a random array sometimes concentrated sufficiently to form a weak stockworks. Minor molybdenum painted fracture surfaces. Dm sections of intercalated feldspar-phyric andesite with sharp high angle contacts.
14887	Andesitic Tuff. Massive fine grain rock displaying weak low angle bedding and intercalated lithic tuff horizons. Weak epidote forming cm patches.
14689	Feldspar-porphyry. Massive, competent. Pink colour, potassic alteration. Rock made up of very fine grained felsic groundmass and ~20% white feldspar phenocrysts and 1-2% yellowish, boxy, altered phenocrysts showing relict cleavage (pseudomorph after augite ?). Rare quartz eyes. 1% finely disseminated sulphides, chalcopyrite, pyrite. Comment: Rock considered as an altered variety of PPAU. Low vein density, dm spacing, ranndom orientation: hairline to 3mm quartz-carbona veins, chlorite veins, pink carbonate-hematite veins. Accessory chalcopyrite, molybdenite in veins.
14695	Plagioclase-phyric and augite phyric andesite. Colour medium green grey. 1mm greenish plagioclase phenocrysts , 1-3% altered augite phenocrysts. Common (5%) black-dark breccia portions grading into crackle breccia. Matrix carbonate-chlorite-red hematite. Moderate density hairline to 5mm veins with blackish halo (chlorite-carbonate), low angle to medium angle. Accessory chalcopyrite in veins and breccia. Sharp gradation. 28.3-29.9: Strongly altered, veined, rusty, in part rubble. Alterati hematite, chlorite. 29.1-29.4 m 3cm quartz-carbonate vein 45CA and 3cm strongly molybdenite-coated vein and fault 75CA (i.e. subhorizontal).
14742	Lapilli andesite and andesite, variously textured and altered. Unit divided into subdivisions 155.7 -164.3 m ANLP Colour medium grey. Weak chloritic and potassic alteration. Low vein density, medium angle.
14666	Volcanic Breccia. Variable grey-green colour, fine grain matrix. Varaible pervasive chloritization and weak carbonatization. Dm sections of cm size oxide inclusions. Randomly oriented hairline carbonate veinlets occasionally forming a weak stockwork array. Dm sections of weak K-alteration. Rare quartz-carbonate veinlet exhibiting biotite selvage. Locally disseminated and stringer chalcopyrite concentrations. Meter sections with mm-cm autobrecciated clasts as well as xenoliths ranging from fine grain mafic to intermediate in composition, with occasional porphyry clast. Alternating meter sections of interbedded andesite and voalcanic breccia. Rare molybdenite painted fractures. 51.8 - 57.9 m ; high in irregular shaped oxide void fillings and inclusions, up to 10% by volume.
14685	Diorite. Medium grey, massive. Variable chloritization, with sericite overprinting. Dm scale K-alteration associated with carbonate chlorite veins. 7% oxide and fine grain disseminated pyrite. Dm section of weak cumulate texture. 97.8 - 107.0 m; massive with a low vein density.
14685B	
14545	Porphyritic, plagioclase-phyric andesite. Very fine grained, igneous, felsic groundmass hosting abundant 0.3-2mm plagioclase phenocrysts and some augite phenocrysts, both altered. Core competent, moderate to strongly fractured. Colour 1/2 - 3/4 dark green grey; 1/4 to 1/2 medium pink green grey, i.e weak potassic alteration. Alteration generally weakly chloritic, 1/4 to 1/2 weak patchy, potassic alteration. Potassic alteration areas are spotty, with 20% dark green chloritic (with tourmaline?) spots. Accessory red hematite spots. Accessory disseminated pyrite, chalcopyrite, bornite. Rare epidote patches. Veining: Generally low vein density, quartz veins, carbonate veins, chlorite veins. Veins mm wide, low angle-medium angle, with mm wide pink halos. Sulphides: Trace to accessory pyrite, chalcopyrite, bornite in rare mm size patches, veins and disseminations. Rare 5-10mm size chalcopyrite patches or discontinuous veins.
14565	Slightly brecciated, in situ, jig-saw fit. Colour 70% pink, potassic alteration. Weak breccia: Distention breccia, randomly oriented mm fractures filled with chlorite, carbonate. Breccia matrix 2-5%, containing chlorite. 1/10 hematite alteration. Accessory chalcopyrite as a) disseminations, mm patches; b) in thin veins.
14571	Plagioclase porphyry. Massive, medium grained. Colour light pink grey, greenish grey. 40-60% 0.5-3mm size plagioclase phenocrysts, 5% interstitial chlorite grains, fine grained felsic matrix. Upper contact sharp, irregular, chilled, with andesite wall rock clasts in plagioclase porphyry. Chilled phase has 1% altered augite phenocrysts and rare quartz eyes. Common accessory (1%) chalcopyrite as disseminations and in veins. Trace molybdenite in veins. Two 5cm fault gouges 45CA at 85.0m and 85.3 m. Lower contact irregular: PPPL and ANPF are intertwined, fine grained andesite being broken up and intruded by medium grained plagioclase porphyry.

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Description
14578	Plagioclase-augite-phyric andesite; medium grained-coarse grained plagioclase- and augite phenocrysts; colour pale pink grey, i.e potassic alteration. Variable abundance of phenocrysts. Moderate vein density, variable, in places cm spacing, crackle breccia of dark veins, low angle, carbonate-chlorite-veins. 102.1 - 102.4 m Several 1mm high-molybdenite slickensides; at 108.5 m one 4cm quartz vein with 2% molybdenite. Overall accessory chalcopyrite, bornite, molybdenite.
14578B	
14598	Fine grained, plagioclase-phyric, augite-phyric andesite. Colour mostly medium green grey, rare (<1/10) pink potassic alteration, mostly as halos around veins. Moderate vein density, cm-10cm spacing, hairline to 5mm quartz veins, low angle to medium angle. Several 1-5cm carbonate-chlorite-veins and vein breccia with high sulphide abundance (several % of coarse grained chalcopyrite, pyrite, molybdenite)
14893	Plagioclase-phyric and augite-phyric andesite. Fine grained, massive, competent core. Fine grained, felsic, igneous grondmass hosting 20% 0.2-2mm plagioclase phenocrysts; and 1-5% dark, altered augite phenocrysts. Variable phenocryst abundance. Colour generally medium-dark green grey and medium brown grey, alternating at 1.5 - 3.0 m intervals. Weak chorititic and weak potassic alteration. Generally low vein density, 10cm spacing, random orientation, <1 to 10mm width. Rare 10-30mm veins. Scattered portions (0.3 - 1.5 m) of higher vein density/stockwork, cm spacing. Trace to ccessory sulphides in veins: chalcopyrite, bornite. Approximate subdivisions according to geological characteristics: 4.9 - 23.8 m PPAU Dark green grey with minor medium brown grey portions. Strongly fractured, rusty, limonitic, in part with malachite coating.
14899	Plagioclase-phyric and augite-phyric andesite. Fine grained, massive, competent core. Fine grained, felsic, igneous grondmass hosting 20% 0.2-2mm plagioclase phenocrysts; and 1-5% dark, altered augite phenocrysts. Variable phenocryst abundance. Colour generally medium-dark green grey and medium brown grey, alternating at 1.5 - 3.0 m intervals. Weak chorititic and weak potassic alteration. Generally low vein density, 10cm spacing, random orientation, <1 to 10mm width. Rare 10-30mm veins. Scattered portions (0.3 - 1.5 m) of higher vein density/stockwork, cm spacing. Trace to ccessory sulphides in veins: chalcopyrite, bornite. Approximate subdivisions according to geological characteristics: 23.8 - 40.5 m PPAU and ANDS, fine grained, low phenocrysts population.
14908	Lapilli andesite/agglomerate-andesite. Core competent, massive. Distinct fragmental texture, heterolithic clasts, andesitic. Clasts size < 1 to > 5 cm. Colour generally medium brown grey, minor dark green grey. Weak chlorite and potassic alteration. - Generally low vein density, but slightly higher than above: cm to dm spacing, medium angle.
14917	Plagioclase porphyry. Core competent, rock massive. Colour pale pink grey. Potassic alteration. 30-60% 1-3mm white and pink feldspar phenocrysts in fine grained felsic matrix. Contacts: Both upper and lower contact show ghost breccia over 0.6m. lower contact shows well preserved, sharp, chilled contact (50-60CA) of adjacent volcanic. This suggests that PPPL is probably older, i.e. pre-dated the andesite. Low vein density, dm spacing, 1-10mm quartz veins, with trace/accessory bornite, chalcopyrite. Quartz veins in part vuggy, open. Sharp contact 60CA
14925	Ditto above, to 74.4 m. Lapilli-andesite/agglomerate. Core competent, massive texture. Size of adesitic clasts mm to 5cm. Clasts shape angular and rounded. Both matrix and clasts andesitic. Colour medium green grey and brown grey. Low vein density, dm spacing, medium angle. Weak chloritic, potassic, hematite alteration. Rare cm wide, pink potassic selvages. Rare 0.3-1.0m size stockworks. 132.3 - 135.3m strongly fractured, core rubbly. Trace sulphides in veins, hairline to 1mm, chalcopyrite, bornite, molybdenite; and chalcopyrite fracture coating. Molybdenite commoly as fracture coating. Chalcopyrite forming 0.5-2mm veins with high chalcopyrite abundance, one per 1.5 - 3m. dm size portions with stockwork and higher sulphides abundanc: 84.7-85.0m; 87.8-88.4m; 91.1-91.4m; 99.4-100.0m; 100.6-101.8m; 110.9-112.8m; 114.3-114.9m; 117.3-118.0m; 120.7-121.9m; 127.7-128.3m; 134.1-137.1m.
14998	Feldspar-Phyric Andesite. Grey-green, 10-15% mm anhedral-euhedral feldspar phenocrysts in a very fine grain matrix. In part tuffaceous. 5% mm oxide inclusions. Weak pervasive chloritization and weak carbonatization. Randomly oriented mm-1/2cm quartz-carbonate-chlorite veins forming dm sections of stockworks, variably mineralized with chalcopyrite, bornite and molybdenite. Occasional molybdenite painted fracture surfaces. Late mm unmineralized arbonate veins.
15862	Feldspar-Phyric Andesite. Green-grey, 10-15% mm anhedral-euhedral feldspar phenocrysts. 5% oxide inclusions. Varaible dm-m sections of K-alteration and carbonate alteration associated with quartz-carbonate-chlorite and carbonate-quartz stockworks. 75.4 - 91.4 m; high fracture and fault density at variable angles from low to high associated with carbonate-chlorite veins. Occasional molybdenite painted fracture surfaces.
15870	Andesitic Lapilli Tuff-Agglomerate. Grey-green, lapilli fragments in fine grain andesitic matrix. Variable pervasive carbonatization from weak to strong, bleaching an earlier pervasive chloritization. High stockwork vein density of mm-cm quartz-chlorite-carbonate veins and chlorite-carbonate veins forming dm sections of crackle breccia. Rare mm pyrite stringers and strands. Chalcopyrite, bornite and molybdenite associated with the quartz-chlorite veins. Late cross-cutting unmineralized carbonate veins. Rare cm sections of highly comminuted rock forming bands at medium to high angle. Vuggy veins associated with carbonate phase. Cm sections of K-alteration, vein related.
15879	Andesite Breccia-Agglomerate. Angular mm-cm mafic-intermediate fragments amd mm oxide inclusions, auto-brecciated. Fine grain matrix. Moderate pervasive chloritization. Lower contact fault controlled with 3cm of gouge at high angle to core.
15887	Andesitic Tuffite. Pale olive green. Fine grain. Interbedded clastic and pyroclastic facies. Riddled with a high density stockwork array of mm carbonate-chlorite veinlets mineralized with fine grain bornite, and displaying mm-1/2cm silica alteration selvages manifest as grey tones overprinting an earlier pervasive alteration event of carbonate-sericite soaking the protolith. Fine mm scale bedding oriented at very low angle to core. Sharp high angle lower contact.
15891	Feldspar-Phyric Andesite. Green-grey. Variable chloritization overprinted by intermittent pervasive weak to strong carbonatization and dm sections of moderate to strong K-alteration associated with randomly oriented mm-cm quartz-carbonate-chlori veins. 158.8 m ; very low angle carbonate-quartz vein brecciating host rock, displaying moderate K-alteration. Fault associated vein walls.
15908	Feldspar-Quartz Porphyry. Andedral to subhedral feldspar phenocrysts and anhedral quartz compacted into a massive rock with disseminated chalcopyrite.
15911	Andesite. Green-grey. Pervasive carbonatization and chloritization, with cm sections of intense carbonatization. 10% angular to round oxide inclusions. Minor bornite and chalcopyrite associated with quartz-carbonate veins.

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: Sampled by MDAG on Feb 7'07.
pH of DI water used for paste pH read ???

Sample Id.	Paste pH	S (Total)	S (Sulphide)	S (Sulphide)	Carbonate Leach S (Sulphate)	HCl Leachable S (Sulphate)	S (Sulphate)	$S(BaSO_4)$	$S(del_{actual})$	S(del)	TAP	SAP	PAP
	Unity	(% Leco)	(% Leco)	(% Calc)	(%)	(%)	(% HCl/Carb)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)
Method	OA-ELE07	S-IR08	S-IR07	S-CAL06	S-GRA06	S-GRA06a		Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL	0.1	0.01	0.01	0.01	0.01	0.01							
14018	7.6	0.8	0.69	0.795	0.02	*0.005*	0.005	0.027	0.078	0.078	25.0	24.0	19.7
14021	7.9	0.62	0.6	0.615	0.03	*0.005*	0.005	0.010	0.005	0.005	19.4	18.9	12.5
14036	7.9	1.47	1.39	1.465	0.02	*0.005*	0.005	0.013	0.062	0.062	45.9	45.4	37.8
14043	8.2	0.26	0.22	0.255	0.02	*0.005*	0.005	0.006	0.029	0.029	8.1	7.8	2.8
14060	8	1.31	0.62	0.6	0.74	0.71	0.71	0.008	-0.028	0.000	40.9	19.4	10.6
14067	8.4	0.4	0.41	0.395	0.01	*0.005*	0.005	0.008	-0.023	0.000	12.5	12.8	4.7
14076	8.2	0.77	0.76	0.765	0.01	*0.005*	0.005	0.010	-0.005	0.000	24.1	23.8	19.1
14083	8.2	1.46	1.35	1.455	0.03	*0.005*	0.005	0.017	0.088	0.088	45.6	44.9	40.4
14099	8.1	0.34	0.28	0.335	0.03	*0.005*	0.005	0.021	0.034	0.034	10.6	9.8	5.6
14103	8	0.69	0.25	0.27	0.45	0.42	0.42	0.006	0.014	0.014	21.6	8.2	0.2
14130	8.3	0.29	0.29	0.285	0.03	*0.005*	0.005	0.013	-0.018	0.000	9.1	9.1	0.2
14144	8	0.26	0.2	0.255	0.02	*0.005*	0.005	0.008	0.047	0.047	8.1	7.7	0.2
14148	7.6	0.14	0.04	0.135	0.02	*0.005*	0.005	0.015	0.080	0.080	4.4	3.8	0.2
14156	7.7	0.17	0.14	0.165	0.04	*0.005*	0.005	0.006	0.019	0.019	5.3	5.0	0.2
14162	7.9	0.13	0.12	0.125	0.02	*0.005*	0.005	0.013	-0.008	0.000	4.1	3.8	0.2
14169	8.1	0.3	0.29	0.295	0.01	*0.005*	0.005	0.002	0.003	0.003	9.4	9.2	0.2
14232	8.3	0.15	0.14	0.145	*0.005*	*0.005*	0.005	0.004	0.001	0.001	4.7	4.4	0.2
14250	8.3	0.19	0.19	0.185	0.01	*0.005*	0.005	0.004	-0.009	0.000	5.9	5.9	0.2
14260	8.4	0.34	0.34	0.335	0.01	*0.005*	0.005	0.004	-0.009	0.000	10.6	10.6	0.2
14276	8.5	0.17	0.14	0.165	0.01	*0.005*	0.005	0.025	0.000	0.000	5.3	4.4	0.2
14295	8.6	0.44	0.41	0.435	*0.005*	*0.005*	0.005	0.002	0.023	0.023	13.8	13.5	6.1
14301	8.6	0.34	0.32	0.335	0.01	*0.005*	0.005	0.006	0.009	0.009	10.6	10.3	2.1
14323	8.6	0.15	0.13	0.145	*0.005*	*0.005*	0.005	0.006	0.009	0.009	4.7	4.3	0.2
14332	8.6	0.26	0.26	0.255	0.01	*0.005*	0.005	0.004	-0.009	0.000	8.1	8.1	0.2
14345	8.4	0.52	0.52	0.515	*0.005*	*0.005*	0.005	0.004	-0.009	0.000	16.3	16.3	0.2
14348	8.3	0.44	0.45	0.435	0.01	*0.005*	0.005	0.004	-0.019	0.000	13.8	14.1	0.2
14797	8.1	0.08	0.05	0.075	*0.005*	*0.005*	0.005	0.004	0.021	0.021	2.5	2.2	0.2
14808	7.8	0.18	0.16	0.175	*0.005*	*0.005*	0.005	0.004	0.011	0.011	5.6	5.3	0.2
14816	7.6	0.46	0.46	0.45	*0.005*	0.01	0.01	0.004	-0.014	0.000	14.4	14.4	1.7
14828	7.6	0.13	0.1	0.125	0.02	*0.005*	0.005	0.017	0.008	0.008	4.1	3.4	0.2
14844	7.7	0.21	0.2	0.2	*0.005*	0.01	0.01	0.008	-0.008	0.000	6.6	6.3	0.2
14680	7.7	0.22	0.2	0.215	0.01	*0.005*	0.005	0.006	0.009	0.009	6.9	6.5	0.2
14871	7.6	0.37	0.32	0.365	0.02	*0.005*	0.005	0.002	0.043	0.043	11.6	11.3	0.2
14887	7.8	0.44	0.42	0.41	0.01	0.03	0.03	0.008	-0.018	0.000	13.8	13.1	6.8
14689	8.2	0.68	0.69	0.675	0.01	*0.005*	0.005	0.002	-0.017	0.000	21.3	21.6	15.0
14695	8.2	0.14	0.13	0.135	*0.005*	*0.005*	0.005	0.004	0.001	0.001	4.4	4.1	0.2
14742	8.2	0.19	0.19	0.185	*0.005*	*0.005*	0.005	0.004	-0.009	0.000	5.9	5.9	0.2
14666	8.1	0.32	0.31	0.315	0.01	*0.005*	0.005	0.008	-0.003	0.000	10.0	9.7	5.0
14685	8.1	1.79	1.8	1.785	0.01	*0.005*	0.005	0.010	-0.025	0.000	55.9	56.3	42.3
14685B	7.9	1.95	1.8	1.945	0.01	*0.005*	0.005	0.008	0.137	0.137	60.9	60.5	45.9
14545	7.8	0.19	0.13	0.185	0.01	*0.005*	0.005	0.021	0.034	0.034	5.9	5.1	1.2
14565	7.8	0.23	0.24	0.225	*0.005*	*0.005*	0.005	0.004	-0.019	0.000	7.2	7.5	0.2
14571	7.8	1.04	1.03	1.035	0.02	*0.005*	0.005	0.010	-0.005	0.000	32.5	32.2	14.7
14578	7.9	1.82	1.82	1.815	0.02	*0.005*	0.005	0.015	-0.020	0.000	56.9	56.9	47.4
14578B	7.9	1.93	1.91	1.925	0.03	*0.005*	0.005	0.019	-0.004	0.000	60.3	59.7	49.2
14598	8.1	0.13	0.13	0.125	0.01	*0.005*	0.005	0.004	-0.009	0.000	4.1	4.1	1.7
14893	8	0.11	0.08	0.07	*0.005*	0.04	0.04	0.010	-0.020	0.000	3.4	2.5	0.2
14899	8.1	0.02	0.02	0.015	*0.005*	*0.005*	0.005	0.008	-0.013	0.000	0.6	0.6	0.2
14908	8.1	0.08	0.07	0.075	*0.005*	*0.005*	0.005	0.017	-0.012	0.000	2.5	2.2	0.2
14917	8.2	0.19	0.16	0.185	*0.005*	*0.005*	0.005	0.019	0.006	0.006	5.9	5.2	0.2
14925	7.9	0.14	0.12	0.135	*0.005*	*0.005*	0.005	0.008	0.007	0.007	4.4	4.0	0.2
14998	7.8	0.13	0.12	0.125	*0.005*	*0.005*	0.005	0.006	-0.001	0.000	4.1	3.8	0.2
15862	7.9	0.08	0.03	0.075	*0.005*	*0.005*	0.005	0.006	0.039	0.039	2.5	2.1	0.2
15870	8	0.13	0.09	0.125	0.02	*0.005*	0.005	0.025	0.010	0.010	4.1	3.1	0.2
15879	8	0.12	0.09	0.115	0.02	*0.005*	0.005	0.019	0.006	0.006	3.8	3.0	0.2
15887	8	0.31	0.29	0.305	0.01	*0.005*	0.005	0.010	0.005	0.005	9.7	9.2	0.2

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: Sampled by MDAG on Feb 7'07.
pH of DI water used for paste pH read ???

Sample Id.	Paste pH	S (Total)	S (Sulphide)	S (Sulphide)	Carbonate Leach S (Sulphate)	HCl Leachable S (Sulphate)	S (Sulphate)	S($BaSO_4$)	S(del_{actual})	S(del)	TAP	SAP	PAP
	Unity	(% Leco)	(% Leco)	(% Calc)	(%)	(%)	(% HCl/Carb)	(%) Calculated	(%) Calculated	(%) Calculated	(kg $CaCO_3$/t) Calculated	(kg $CaCO_3$/t) Calculated	(kg $CaCO_3$/t) Calculated
Method	OA-ELE07	S-IR08	S-IR07	S-CAL06	S-GRA06	S-GRA06a							
MDL	0.1	0.01	0.01	0.01	0.01	0.01							
15891	7.8	0.14	0.09	0.135	0.02	*0.005*	0.005	0.031	0.014	0.014	4.4	3.2	0.2
15908	7.8	0.22	0.2	0.215	0.02	*0.005*	0.005	0.006	0.009	0.009	6.9	6.5	0.2
15911	7.9	0.09	0.07	0.085	0.01	*0.005*	0.005	0.010	0.005	0.005	2.8	2.3	0.2
Maximum	8.6	1.95	1.91	1.94	0.74	0.71	0.71	0.031	0.14	0.14	60.9	60.5	49.2
Minimum	7.6	0.02	0.02	0.015	0.005	0.005	0.005	0.0021	-0.028	0	0.62	0.62	0.16
Mean	8.04	0.45	0.41	0.43	0.033	0.025	0.025	0.01	0.0089	0.015	14.1	13.2	6.75
Standard Deviation	0.27	0.5	0.48	0.49	0.11	0.11	0.11	0.0068	0.031	0.027	15.7	15.3	13.5
10 Percentile	7.7	0.12	0.078	0.11	0.005	0.005	0.005	0.0042	-0.019	0	3.69	2.9	0.16
25 Percentile	7.8	0.14	0.13	0.14	0.005	0.005	0.005	0.0042	-0.0092	0	4.38	4.08	0.16
Median	8	0.26	0.22	0.26	0.01	0.005	0.005	0.0084	0.0029	0.0029	8.12	7.71	0.16
75 Percentile	8.2	0.45	0.44	0.44	0.02	0.005	0.005	0.013	0.014	0.014	14.1	13.8	5.33
90 Percentile	8.4	1.34	1.09	1.12	0.03	0.006	0.006	0.019	0.044	0.044	41.9	34.7	23.4
Interquartile Range (IQR) [1]	0.4	0.31	0.3	0.3	0.015	0	0	0.0084	0.023	0.014	9.69	9.72	5.18
Variance	0.074	0.25	0.23	0.24	0.012	0.011	0.011	0.000047	0.00095	0.00071	246	234	182
Skewness	0.37	1.93	2.08	2.11	5.72	5.79	5.79	1.24	1.97	2.67	1.93	2.09	2.25
Coefficient of Variation (CoV) [2]	0.034	1.11	1.18	1.15	3.34	4.2	4.2	0.68	3.47	1.83	1.11	1.16	2
Count	59	59	59	59	59	59	59	59	59	59	59	59	59

Total
NPR < 1.0 or NPR = 1.0
1.0 < NPR < 2.0
NPR > 2.0 or NPR =2.0

% NPR < 1.0 or NPR = 1.0 of Total
% 1.0 < NPR < 2.0 of Total
% NPR > 2.0 or NPR =2.0 of Total

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile
[2] Coefficient of Variation (CoV) = standard deviation divided by mean
NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

% S (Sulphide) (calc) = % S (Total) - % S (Sulphate) Carbonate Leach
%S($BaSO_4$) = Ba (ppm) * 0.0001 * 32.06 / 137.37
% S (del_{actual}) = %S(Total) - %S(Sulphide) Leco - %S(Sulphate) Carbonate Leach - %S($BaSO_4$)
% S (del) = % S (del_{actual}) unless < 0, then 0
TAP = % S (Total) * 31.25
SAP = % S (Sulphide + del) * 31.25
PAP = % Pyrite(Calculated) * 31.25
Note: If Calculated Pyrite is < 0.005 then calculated pyrite assumed to be 0.005
Unavailable NP (UNP) = 10
Available NP = NP - Unavailable NP

Project:	**Schaft Creek**
Client:	Copper Fox Metals Inc.
Data:	**ABA Data**
Comments:	Sampled by MDAG on Feb 7'07.

Sample Id.	NP (kg $CaCO_3$/t)	Available NP (kg $CaCO_3$/t)	Total C (% Leco)	Inorganic C (%)	Inorganic CO_2 (%)	Excess C (%)	Total CaNP (kg $CaCO_3$/t)	Inorganic CaNP (kg $CaCO_3$/t)	(Ca) CaNP (kg $CaCO_3$/t)	(Ca+Mg) CaNP (kg $CaCO_3$/t)	TNNP (kg $CaCO_3$/t)	Adjusted TNNP (kg $CaCO_3$/t)	SNNP (kg $CaCO_3$/t)	Adjusted SNNP (kg $CaCO_3$/t)	PNNP (kg $CaCO_3$/t)	Adjusted PNNP (kg $CaCO_3$/t)
Method	OA-VOL08	Calculated	C-IR07	C-GAS05	C-GAS05	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL	1		0.01	0.05	0.2											
14018	42	32	0.4	0.38	1.4	0.02	33.3	31.8	44.5	88.5	17.0	7.0	18.0	8.0	22.3	12.3
14021	64	54	0.76	0.72	2.6	0.04	63.3	59.1	65.4	103.3	44.6	34.6	45.1	35.1	51.5	41.5
14036	49	39	0.52	0.48	1.8	0.04	43.3	40.9	45.9	83.4	3.1	-6.9	3.6	-6.4	11.2	1.2
14043	40	30	0.33	0.21	0.8	0.12	27.5	18.2	35.0	113.2	31.9	21.9	32.2	22.2	37.2	27.2
14060	41	31	0.29	0.28	1	0.01	24.2	22.7	78.4	164.9	0.1	-9.9	21.6	11.6	30.4	20.4
14067	49	39	0.41	0.35	1.3	0.06	34.2	29.6	64.7	175.0	36.5	26.5	36.2	26.2	44.3	34.3
14076	66	56	0.71	0.7	2.6	0.01	59.2	59.1	108.4	211.3	41.9	31.9	42.3	32.3	46.9	36.9
14083	74	64	0.85	0.83	3	0.02	70.8	68.2	100.6	173.5	28.4	18.4	29.1	19.1	33.6	23.6
14099	78	68	0.92	0.92	3.4	0	76.7	77.3	73.7	107.4	67.4	57.4	68.2	58.2	72.4	62.4
14103	85	75	0.9	0.87	3.2	0.03	75.0	72.8	73.2	126.3	63.4	53.4	76.8	66.8	84.8	74.8
14130	91	81	1.18	1.19	4.4	0	98.3	100.1	65.4	107.4	81.9	71.9	81.9	71.9	90.8	80.8
14144	116	106	1.43	1.37	5	0.06	119.2	113.7	93.6	141.4	107.9	97.9	108.3	98.3	115.8	105.8
14148	170	160	1.92	1.9	7	0.02	160.0	159.2	115.6	193.4	165.6	155.6	166.2	156.2	169.8	159.8
14156	73	63	0.88	0.86	3.2	0.02	73.3	72.8	61.7	94.2	67.7	57.7	68.0	58.0	72.8	62.8
14162	219	209	2.3	2.28	8.4	0.02	191.7	191.0	139.6	247.5	214.9	204.9	215.3	205.3	218.8	208.8
14169	64	54	0.7	0.69	2.5	0.01	58.3	56.9	57.9	74.4	54.6	44.6	54.8	44.8	63.8	53.8
14232	89	79	0.93	0.87	3.2	0.06	77.5	72.8	66.4	103.9	84.3	74.3	84.6	74.6	88.8	78.8
14250	118	108	1.14	1.12	4.1	0.02	95.0	93.2	101.6	179.0	112.1	102.1	112.1	102.1	117.8	107.8
14260	100	90	1.03	1.02	3.7	0.01	85.8	84.1	75.9	133.1	89.4	79.4	89.4	79.4	99.8	89.8
14276	47	37	0.43	0.25	0.9	0.18	35.8	20.5	107.6	175.2	41.7	31.7	42.6	32.6	46.8	36.8
14295	111	101	1.05	0.95	3.5	0.1	87.5	79.6	97.6	161.5	97.3	87.3	97.5	87.5	104.9	94.9
14301	136	126	1.56	1.54	5.7	0.02	130.0	129.6	91.4	142.5	125.4	115.4	125.7	115.7	133.9	123.9
14323	73	63	0.88	0.84	3.1	0.04	73.3	70.5	93.6	133.2	68.3	58.3	68.7	58.7	72.8	62.8
14332	95	85	0.84	0.74	2.7	0.1	70.0	61.4	84.7	127.5	86.9	76.9	86.9	76.9	94.8	84.8
14345	79	69	0.73	0.44	1.6	0.29	60.8	36.4	63.7	106.1	62.8	52.8	62.8	52.8	78.8	68.8
14348	59	49	0.61	0.6	2.2	0.01	50.8	50.0	53.7	103.5	45.3	35.3	44.9	34.9	58.8	48.8
14797	125	115	1.43	1.39	5.1	0.04	119.2	116.0	94.4	157.0	122.5	112.5	122.8	112.8	124.8	114.8
14808	172	162	2.23	2.21	8.1	0.02	185.8	184.2	121.6	188.7	166.4	156.4	166.7	156.7	171.8	161.8
14816	133	123	1.59	0.27	1	1.32	132.5	22.7	83.2	153.2	118.6	108.6	118.6	108.6	131.3	121.3
14828	143	133	1.7	1.69	6.2	0.01	141.7	141.0	108.4	183.3	138.9	128.9	139.6	129.6	142.8	132.8
14844	75	65	0.51	0.47	1.7	0.04	42.5	38.7	70.4	226.5	68.4	58.4	68.8	58.8	74.8	64.8
14680	102	92	1.06	1.05	3.8	0.01	88.3	86.4	103.4	171.3	95.1	85.1	95.5	85.5	101.8	91.8
14871	88	78	0.76	0.73	2.7	0.03	63.3	61.4	84.9	164.0	76.4	66.4	76.7	66.7	87.8	77.8
14887	119	109	1.2	1.18	4.3	0.02	100.0	97.8	129.4	231.1	105.3	95.3	105.9	95.9	112.2	102.2
14689	53	43	0.64	0.66	2.4	0	53.3	54.6	54.4	77.5	31.8	21.8	31.4	21.4	38.0	28.0
14695	114	104	1.35	1.3	4.8	0.05	112.5	109.2	99.4	161.6	109.6	99.6	109.9	99.9	113.8	103.8
14742	84	74	0.78	0.8	2.9	0	65.0	66.0	69.4	161.6	78.1	68.1	78.1	68.1	83.8	73.8
14666	94	84	0.77	0.74	2.7	0.03	64.2	61.4	98.1	188.7	84.0	74.0	84.3	74.3	89.0	79.0
14685	112	102	0.95	0.91	3.3	0.04	79.2	75.1	82.7	195.1	56.1	46.1	55.8	45.8	69.7	59.7
14685B	102	92	0.85	0.84	3.1	0.01	70.8	70.5	73.7	190.6	41.1	31.1	41.5	31.5	56.1	46.1
14545	77	67	0.63	0.59	2.2	0.04	52.5	50.0	95.4	153.0	71.1	61.1	71.9	61.9	75.8	65.8
14565	136	126	1.33	1.28	4.7	0.05	110.8	106.9	114.4	164.2	128.8	118.8	128.5	118.5	135.8	125.8
14571	76	66	0.76	0.75	2.8	0.01	63.3	63.7	64.7	112.9	43.5	33.5	43.8	33.8	61.3	51.3
14578	111	101	1.25	1.26	4.6	0	104.2	104.6	104.9	153.5	54.1	44.1	54.1	44.1	63.6	53.6
14578B	122	112	1.38	1.35	5	0.03	115.0	113.7	107.9	160.2	61.7	51.7	62.3	52.3	72.8	62.8
14598	77	67	0.59	0.57	2.1	0.02	49.2	47.8	83.7	174.6	72.9	62.9	72.9	62.9	75.3	65.3
14893	111	101	1.03	1.03	3.8	0	85.8	86.4	103.9	215.9	107.6	97.6	108.5	98.5	110.8	100.8
14899	81	71	0.68	0.65	2.4	0.03	56.7	54.6	88.4	258.4	80.4	70.4	80.4	70.4	80.8	70.8
14908	75	65	0.56	0.56	2.1	0	46.7	47.8	94.6	193.5	72.5	62.5	72.8	62.8	74.8	64.8
14917	66	56	0.55	0.54	2	0.01	45.8	45.5	57.9	133.3	60.1	50.1	60.8	50.8	65.8	55.8
14925	82	72	0.72	0.73	2.7	0	60.0	61.4	89.9	173.9	77.6	67.6	78.0	68.0	81.8	71.8
14998	103	93	1.05	1.04	3.8	0.01	87.5	86.4	99.4	166.5	98.9	88.9	99.3	89.3	102.8	92.8
15862	130	120	1.34	1.34	4.9	0	111.7	111.4	105.4	177.0	127.5	117.5	127.9	117.9	129.8	119.8
15870	151	141	1.72	1.72	6.3	0	143.3	143.3	115.9	188.7	146.9	136.9	147.9	137.9	150.8	140.8
15879	118	108	1.33	1.31	4.8	0.02	110.8	109.2	120.6	198.0	114.3	104.3	115.0	105.0	117.8	107.8
15887	95	85	0.94	0.91	3.3	0.03	78.3	75.1	102.9	168.4	85.3	75.3	85.8	75.8	94.8	84.8

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: Sampled by MDAG on Feb 7'07.

Sample Id.	NP (kg CaCO$_3$/t)	Available NP (kg CaCO$_3$/t)	Total C (% Leco)	Inorganic C (%)	Inorganic CO$_2$ (%)	Excess C (%)	Total CaNP (kg CaCO$_3$/t)	Inorganic CaNP (kg CaCO$_3$/t)	(Ca) CaNP (kg CaCO$_3$/t)	(Ca+Mg) CaNP (kg CaCO$_3$/t)	TNNP (kg CaCO$_3$/t)	Adjusted TNNP (kg CaCO$_3$/t)	SNNP (kg CaCO$_3$/t)	Adjusted SNNP (kg CaCO$_3$/t)	PNNP (kg CaCO$_3$/t)	Adjusted PNNP (kg CaCO$_3$/t)
Method	OA-VOL08	Calculated	C-IR07	C-GAS05	C-GAS05	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL	1		0.01	0.05	0.2											
15891	128	118	1.44	1.4	5.1	0.04	120.0	116.0	128.1	199.3	123.6	113.6	124.8	114.8	127.8	117.8
15908	121	111	1.2	1.2	4.4	0	100.0	100.1	112.9	189.0	114.1	104.1	114.5	104.5	120.8	110.8
15911	92	82	0.85	0.82	3	0.03	70.8	68.2	87.9	183.0	89.2	79.2	89.7	79.7	91.8	81.8
Maximum	219	209	2.3	2.28	8.4	1.32	192	191	140	258	215	205	215	205	219	209
Minimum	40	30	0.29	0.21	0.8	0	24.2	18.2	35	74.4	0.062	-9.94	3.61	-6.39	11.2	1.16
Mean	96.5	86.5	1	0.94	3.46	0.055	83.2	78.8	88.3	159	82.4	72.4	83.3	73.3	89.8	79.8
Standard Deviation	35.2	35.2	0.44	0.46	1.67	0.17	36.9	38.1	23.1	42.2	41.1	41.1	40.4	40.4	39.3	39.3
10 Percentile	52.2	42.2	0.52	0.43	1.56	0	43.2	35.5	57.9	103	35.6	25.6	35.4	25.4	43	33
25 Percentile	74.5	64.5	0.7	0.66	2.4	0.01	58.8	54.6	69.9	130	55.3	45.3	55.3	45.3	64.8	54.8
Median	92	82	0.9	0.86	3.2	0.02	75	72.8	91.4	164	78.1	68.1	78.1	68.1	84.8	74.8
75 Percentile	118	108	1.29	1.23	4.5	0.04	108	102	104	189	109	98.8	109	99.2	115	105
90 Percentile	136	126	1.57	1.43	5.22	0.068	131	119	116	202	128	118	128	118	134	124
Interquartile Range (IQR) [1]	43.5	43.5	0.59	0.57	2.1	0.03	48.8	47.8	34.5	58.4	53.4	53.4	53.9	53.9	50	50
Variance	1237	1237	0.2	0.21	2.8	0.03	1363	1450	535	1781	1686	1686	1630	1630	1544	1544
Skewness	0.84	0.84	0.9	0.85	0.86	6.9	0.9	0.86	-0.14	-0.079	0.57	0.57	0.66	0.66	0.64	0.64
Coefficient of Variation (CoV) [2]	0.36	0.41	0.44	0.48	0.48	3.16	0.44	0.48	0.26	0.27	0.5	0.57	0.48	0.55	0.44	0.49
Count	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59

Total
NPR < 1.0 or NPR = 1.0
1.0 < NPR < 2.0
NPR > 2.0 or NPR =2.0

% NPR < 1.0 or NPR = 1.0 of Total
% 1.0 < NPR < 2.0 of Total
% NPR > 2.0 or NPR =2.0 of Total

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

Total CaNP = % C * 10 * 100.09 / 12.01
Inorganic CaNP = % CO_2 * 10 * 100.09 / 44.01
(Ca) CaNP = (Ca(ppm) * 100.09 / 40.08) / 1000
(Ca+Mg) CaNP = ((Ca(ppm) * 100.09 / 40.08) + (Mg(ppm) * 100.09 / 24.31)) / 1000
TNNP = NP - TAP
Adjusted TNNP = Available NP - TAP
SNNP = NP - SAP
Adjusted SNNP = Available NP - SAP
PNNP = NP - PAP
Adjusted PNNP = Available NP - PAP

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: Sampled by MDAG on Feb 7'07.

Sample Id.	TNPR	Adjusted TNPR	SNPR	Adjusted SNPR	PNPR	Adjusted PNPR	Fizz Rating	Comparison of Fizz Rating & NP
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Unity OA-VOL08	
MDL								
14018	1.68	1.28	1.75	1.33	2.13	1.62	2	Disagree
14021	3.3	2.79	3.39	2.86	5.12	4.32	2	Agree
14036	1.07	0.849	1.08	0.859	1.29	1.03	2	Disagree
14043	4.92	3.69	5.15	3.86	14.2	10.7	2	Disagree
14060	1	0.757	2.12	1.6	3.86	2.92	2	Disagree
14067	3.92	3.12	3.82	3.04	10.4	8.29	2	Disagree
14076	2.74	2.33	2.78	2.36	3.45	2.93	2	Agree
14083	1.62	1.4	1.65	1.42	1.83	1.58	2	Agree
14099	7.34	6.4	7.95	6.93	13.8	12	2	Agree
14103	3.94	3.48	10.3	9.1	200	200	3	Disagree
14130	10	8.94	10	8.94	200	200	3	Disagree
14144	14.3	13	15.1	13.8	200	200	3	Agree
14148	38.9	36.6	45.2	42.5	200	200	3	Agree
14156	13.7	11.9	14.7	12.7	200	200	3	Disagree
14162	53.9	51.4	58.4	55.7	200	200	3	Agree
14169	6.83	5.76	6.99	5.9	200	200	3	Disagree
14232	19	16.9	20.2	18	200	200	3	Disagree
14250	19.9	18.2	19.9	18.2	200	200	3	Agree
14260	9.41	8.47	9.41	8.47	200	200	3	Agree
14276	8.85	6.96	10.7	8.46	200	200	2	Disagree
14295	8.07	7.35	8.2	7.47	18.2	16.6	3	Agree
14301	12.8	11.9	13.2	12.3	66.1	61.3	3	Agree
14323	15.6	13.4	16.8	14.5	200	200	2	Agree
14332	11.7	10.5	11.7	10.5	200	200	3	Disagree
14345	4.86	4.25	4.86	4.25	200	200	3	Disagree
14348	4.29	3.56	4.2	3.48	200	200	2	Agree
14797	50	46	56.5	52	200	200	3	Agree
14808	30.6	28.8	32.2	30.3	200	200	3	Agree
14816	9.25	8.56	9.25	8.56	80.4	74.4	3	Agree
14828	35.2	32.7	42.3	39.3	200	200	3	Agree
14844	11.4	9.9	12	10.4	200	200	3	Disagree
14680	14.8	13.4	15.6	14.1	200	200	3	Agree
14871	7.61	6.75	7.76	6.88	200	200	3	Disagree
14887	8.65	7.93	9.07	8.3	17.6	16.1	3	Agree
14689	2.49	2.02	2.46	1.99	3.54	2.87	2	Agree
14695	26.1	23.8	27.9	25.4	200	200	3	Agree
14742	14.1	12.5	14.1	12.5	200	200	3	Disagree
14666	9.4	8.4	9.7	8.67	18.7	16.7	3	Disagree
14685	2	1.82	1.99	1.81	2.65	2.41	3	Agree
14685B	1.67	1.51	1.69	1.52	2.22	2.01	3	Agree
14545	13	11.3	15	13.1	62.5	54.3	3	Disagree
14565	18.9	17.5	18.1	16.8	200	200	3	Agree
14571	2.34	2.03	2.36	2.05	5.16	4.49	3	Disagree
14578	1.95	1.78	1.95	1.78	2.34	2.13	3	Agree
14578B	2.02	1.86	2.04	1.88	2.48	2.27	3	Agree
14598	19	16.5	19	16.5	46.5	40.5	3	Disagree
14893	32.3	29.4	44.4	40.4	200	200	3	Agree
14899	130	114	130	114	200	200	3	Disagree
14908	30	26	34.3	29.7	200	200	3	Disagree
14917	11.1	9.43	12.7	10.8	200	200	3	Disagree
14925	18.7	16.5	20.7	18.2	200	200	3	Disagree
14998	25.4	22.9	27.5	24.8	200	200	3	Agree
15862	52	48	60.5	55.9	200	200	3	Agree
15870	37.2	34.7	48.4	45.2	200	200	3	Agree
15879	31.5	28.8	39.3	35.9	200	200	3	Agree
15887	9.81	8.77	10.3	9.23	200	200	3	Disagree

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: Sampled by MDAG on Feb 7'07.

Sample Id.	TNPR	Adjusted TNPR	SNPR	Adjusted SNPR	PNPR	Adjusted PNPR	Fizz Rating	Comparison of Fizz Rating & NP
							Unity	
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	OA-VOL08	
MDL								
15891	29.3	27	39.5	36.4	200	200	3	Agree
15908	17.6	16.1	18.6	17	200	200	3	Agree
15911	32.7	29.2	39.5	35.2	200	200	3	Disagree
Maximum	130	114	130	114	200	200		
Minimum	1	0.76	1.08	0.86	1.29	1.03		
Mean	17.3	15.6	19.3	17.4	132	131		
Standard Deviation	20.1	18.1	21.7	19.6	90.2	90.9		
10 Percentile	1.99	1.81	2.03	1.8	2.62	2.38		
25 Percentile	4.58	3.62	5.01	4.06	15.9	14		
Median	11.4	9.9	12	10.5	200	200		
75 Percentile	22.6	20.5	24.1	21.5	200	200		
90 Percentile	35.6	33.1	44.6	40.8	200	200		
Interquartile Range (IQR) [1]	18.1	16.9	19.1	17.4	184	186		
Variance	405	328	470	385	8128	8265		
Skewness	3.36	3.14	2.72	2.53	-0.61	-0.6		
Coefficient of Variation (CoV) [2]	1.16	1.16	1.13	1.13	0.68	0.69		
Count	59	59	59	59	59	59		
Total								
NPR < 1.0 or NPR = 1.0	1	2	0	1	0	0		
1.0 < NPR < 2.0	5	6	6	8	2	3		
NPR > 2.0 or NPR =2.0	53	51	53	50	57	56		
% NPR < 1.0 or NPR = 1.0 of Total	1.694915	3.389831	0	1.694915	0	0		
% 1.0 < NPR < 2.0 of Total	8.474576	10.16949	10.16949	13.55932	3.389831	5.084746		
% NPR > 2.0 or NPR =2.0 of Total	89.83051	86.44068	89.83051	84.74576	96.61017	94.91525		

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile
[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and w

TNPR = NP / TAP
Note: If % S(Total) < 0.01 then TNPR = 200
Note: If % S(Total) > 0.01 and NP < = 0 then TNPR = 0.001
Adjusted TNPR = UNP / TAP
Note: If % S(Total) < 0.01 then Adjusted TNPR = 200
Note: If % S(Total) > 0.01 and UNP < = 0 then Adjusted TNPR = 0.001
SNPR = NP / SAP
Note: If % S(Sulphide + del) < 0.01 then SNPR = 200
'Note: If % S(Sulphide + del) > 0.01 and NP < = 0 then SNPR = 0.001
Adjusted SNPR = UNP / SAP
Note: If % S(Sulphide + del) < 0.01 then Adjusted SNPR = 200
Note: If % S(Sulphide + del) > 0.01 and UNP < = 0 then Adjusted SNPR = 0.001
PNPR = NP / PAP
Note: If % Pyrite(Calc) < 0.01 then PNPR = 200
Note: If % Pyrite(Calc) > 0.01 and NP < = 0 then PNPR = 0.001
Adjusted PNPR = UNP / TAP
Note: If % Pyrite(Calc) < 0.005 then Adjusted PNPR = 200
Note: If % Pyrite(Calc) > 0.005 and UNP < = 0 then Adjusted PNPR = 0.001

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: Sampled by MDAG on Feb 7'07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.

Sample Id.	Silver Ag (ppm)	Aluminum Al (ppm)	Arsenic As (ppm)	Barium Ba (ppm)	Beryllium Be (ppm)	Bismuth Bi (ppm)	Calcium Ca (ppm)	Cadmium Cd (ppm)	Cerium Ce (ppm)	Cobalt Co (ppm)	Chromium Cr (ppm)	Cesium Cs (ppm)	Copper Cu (ppm)	Iron Fe (ppm)	Gallium Ga (ppm)	Germanium Ge (ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.01	100	0.2	10	0.05	0.01	100	0.02	0.01	0.1	1	0.05	0.2	100	0.05	0.05
Crustal Abundance: From	0.037	4200	1	0.4	1	0.007	5100	0.035	11.5	0.1	2	0.4	4	3800	4	0.2
Crustal Abundance: To	0.11	88000	13	2300	3	0.01	312400	0.42	345	74	170	6	250	86500	30	8
14018	0.88	80300	15.5	1120	1.3	0.93	17800	0.02	26.5	12	24	5.11	1290	25800	17.8	0.09
14021	1.22	77000	24.5	460	1.03	0.86	26200	0.11	23.2	9.7	21	5.86	1740	18100	16.4	0.08
14036	1.43	74100	30.2	500	1	1.01	18400	*0.01*	23.8	16.6	20	8.17	1920	25600	16.2	0.18
14043	0.7	75600	10.9	230	1.03	0.4	14000	*0.01*	13.3	14.6	31	2.39	1330	28500	16.05	0.06
14060	0.87	79600	14.3	380	0.99	0.24	31400	*0.01*	23.7	15.4	26	4.87	2610	35900	16.25	0.09
14067	1.85	85100	17.3	370	0.95	0.18	25900	0.03	21.5	19.9	36	2.64	2460	42900	17.6	0.1
14076	1.32	90000	15.1	410	0.8	0.62	43400	0.61	22.6	23.3	33	5.75	1300	54600	18.05	0.12
14083	0.98	88500	13.9	700	0.78	0.86	40300	0.5	22.8	24	49	7.97	1360	57800	17.8	0.12
14099	1.36	72400	2.2	770	0.95	1.51	29500	1.16	21.3	6.4	16	9.67	1210	22300	15.1	0.07
14103	1.06	76000	5.6	250	1.06	1.02	29300	0.03	25.9	7.8	20	3.59	2630	21200	16.95	0.09
14130	3.33	85100	2.1	440	0.62	2	26200	*0.01*	15.5	5	15	3.56	5530	18000	18.25	0.08
14144	2.52	93900	5.1	380	0.84	2.32	37500	*0.01*	20.7	7.7	5	5.29	3410	36100	20	0.1
14148	1.75	81100	2.6	560	0.9	1.98	46300	*0.01*	22.7	11	4	4.68	2880	38300	18.75	0.1
14156	1.76	76900	1.1	280	1.56	1.47	24700	*0.01*	23.3	5.4	25	2.49	2090	17400	20.5	0.07
14162	0.53	79700	2.1	510	0.92	2.13	55900	*0.01*	25.2	20.8	71	2.12	1020	42500	14.85	0.1
14169	2.84	76400	1.9	100	1.09	6.51	23200	*0.01*	7.62	4.2	16	1.19	3820	11800	18.85	0.05
14232	1.73	94400	3.5	140	0.95	0.84	26600	*0.01*	22.2	4.7	14	6.81	3370	26400	19.75	0.08
14250	1.66	94400	3.4	170	0.75	1.14	40700	*0.01*	24.1	8.3	12	4.65	3170	45800	21	0.11
14260	2.92	89500	2.6	170	0.73	6.57	30400	*0.01*	21.6	7.8	3	4.9	4880	42300	20	0.1
14276	0.8	98400	7.5	1000	0.78	0.78	43100	0.13	21.2	8.8	17	2.68	1490	38900	20.3	0.08
14295	0.51	89700	3.7	110	0.7	0.2	39100	0.02	18.6	18.6	12	4.81	2330	47300	18.95	0.1
14301	0.39	87600	3.8	300	0.86	0.4	36600	*0.01*	20.1	10.4	15	3.85	2440	31300	18.05	0.09
14323	1.33	93600	3.3	280	0.92	0.74	37500	*0.01*	20.5	8.8	3	6.79	2250	38700	20.5	0.09
14332	1.36	96200	2.2	210	0.88	0.62	33900	*0.01*	23.9	7.7	3	5.41	3470	35500	20.8	0.09
14345	2.38	97300	2.1	190	0.9	2.05	25500	*0.01*	26.4	7.2	11	4.35	6070	22100	20.4	0.09
14348	1	94300	2.3	150	0.82	1.13	21500	*0.01*	24.6	8.4	11	4.61	4900	34700	20.1	0.09
14797	1.03	86900	2.5	150	0.92	0.43	37800	*0.01*	15.4	10.5	6	6.37	1750	42700	19.85	0.11
14808	2.27	81300	*0.1*	170	1.58	1.73	48700	*0.01*	21.5	9.2	6	5.38	2640	37600	18.75	0.33
14816	2.15	82900	1.8	140	0.84	2.94	33300	*0.01*	18.3	10.1	5	5.98	3970	41300	21.4	0.12
14828	2.42	89200	2.4	710	0.94	2.48	43400	*0.01*	23.8	10.3	4	5.11	3260	41200	20.9	0.13
14844	1.35	91800	3.7	300	0.67	1.02	28200	*0.01*	15.75	19	39	8.05	2990	51800	22	0.12
14680	3.36	90500	1.8	300	2.27	5.64	41400	*0.01*	27.1	11	5	10.45	3950	41400	21	0.28
14871	1.02	96200	2.3	120	0.74	1.28	34000	*0.01*	18.75	12.7	10	5.3	3880	46100	21.4	0.11
14887	0.41	96900	2.9	340	0.68	0.28	51800	*0.01*	22.1	16.2	20	3.33	1990	53100	20.4	0.12
14689	0.38	83800	1.4	120	1.01	0.44	21800	*0.01*	29.6	5.9	10	2.38	2020	14800	18.4	0.07
14695	0.71	97000	*0.1*	170	0.89	1.19	39800	*0.01*	26.4	9.6	6	7.95	1500	39900	21.4	0.24
14742	1.3	90600	0.5	120	1.35	4.71	27800	*0.01*	17.2	10.4	24	2.84	2100	33500	20.5	0.33
14666	0.37	92100	4.8	330	0.78	0.13	39300	*0.01*	19.3	21.9	21	4.19	1440	53900	21.9	0.1
14685	1.13	85900	6.6	380	1.04	0.51	33100	*0.01*	22.1	35.4	5	5.87	4330	63900	22.7	0.1
14685B	1	83100	5.9	310	1.1	0.48	29500	*0.01*	19.45	30.6	7	5.85	4570	59700	21.8	0.11
14545	0.26	94700	3.4	860	0.8	0.08	38200	*0.01*	24.1	10.3	16	4.7	1210	41700	21.2	0.1
14565	0.47	88300	3	220	0.7	0.39	45800	*0.01*	22.7	8.7	11	5.46	2670	37200	18.65	0.09
14571	1.92	82200	3.2	430	0.99	1.04	25900	*0.01*	20.9	12.9	7	5.37	5450	26900	18.05	0.08
14578	0.65	86800	5.2	640	1.16	0.33	42000	*0.01*	23.9	15.8	9	6.35	2980	41600	19.4	0.1
14578B	0.74	82400	4.5	760	1	0.31	43200	*0.01*	22.8	15.7	10	6.22	3280	39200	20.4	0.11
14598	0.39	92500	2.7	220	0.85	1.23	33500	*0.01*	16.15	15.9	3	4.8	703	46600	22.6	0.09
14893	0.67	92000	4.5	490	0.81	0.56	41600	*0.01*	18.75	18.3	44	5.23	1630	53400	22.6	0.11
14899	0.25	97000	8.1	330	0.78	0.18	35400	*0.01*	15.8	22.6	43	2.68	409	56900	24.2	0.12
14908	0.39	95800	6.2	690	0.69	0.29	37900	*0.01*	19.6	15	39	2.29	1140	53200	23.3	0.11
14917	2.53	85300	1.7	740	1.19	1.43	23200	*0.01*	25.1	9.4	16	2.27	3800	24200	23.5	0.1
14925	0.71	87800	3.5	390	0.71	0.58	36000	*0.01*	17.85	13.9	30	4.58	1610	46200	22.7	0.12
14998	0.72	90100	3.4	280	0.63	0.53	39800	*0.01*	20.1	12.8	6	5.88	1800	43600	21.6	0.12
15862	0.74	87200	2.2	290	0.66	0.49	42200	*0.01*	19.1	12.2	4	5.75	1180	41600	21	0.1
15870	1.17	81000	2.6	1030	0.46	0.54	46400	*0.01*	20.6	10.3	27	4.53	2020	39200	20.4	0.12

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: Sampled by MDAG on Feb 7'07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.

Sample	Silver	Aluminum	Arsenic	Barium	Beryllium	Bismuth	Calcium	Cadmium	Cerium	Cobalt	Chromium	Cesium	Copper	Iron	Gallium	Germanium
Id.	Ag	Al	As	Ba	Be	Bi	Ca	Cd	Ce	Co	Cr	Cs	Cu	Fe	Ga	Ge
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.01	100	0.2	10	0.05	0.01	100	0.02	0.01	0.1	1	0.05	0.2	100	0.05	0.05
Crustal Abundance: From	0.037	4200	1	0.4	1	0.007	5100	0.035	11.5	0.1	2	0.4	4	3800	4	0.2
Crustal Abundance: To	0.11	88000	13	2300	3	0.01	312400	0.42	345	74	170	6	250	86500	30	8
15879	1.4	90600	2.4	760	0.67	0.51	48300	*0.01*	19.85	13.6	29	4.83	2150	51500	21.7	0.12
15887	2.42	87200	2	440	0.75	1.14	41200	*0.01*	15.05	14	25	5.1	5070	34600	21.4	0.12
15891	2.15	89500	1.7	1250	0.66	0.98	51300	*0.01*	17.35	9.7	22	5.24	2450	38500	21.4	0.11
15908	2.82	87100	1.5	260	0.77	1.3	45200	*0.01*	17.95	12.7	24	5.96	4260	34500	20.8	0.1
15911	1.2	88600	2.1	410	0.7	0.56	35200	*0.01*	19.5	14.8	33	6.92	1820	46500	22.2	0.1
Maximum	3.36	98400	30.2	1250	2.27	6.57	55900	1.16	29.6	35.4	71	10.4	6070	63900	24.2	0.33
Minimum	0.25	72400	0.1	100	0.46	0.08	14000	0.01	7.62	4.2	3	1.19	409	11800	14.8	0.05
Mean	1.34	87481	5.08	412	0.91	1.26	35375	0.053	21	13	18.3	5.04	2661	38607	20	0.11
Standard Deviation	0.82	6660	5.75	273	0.28	1.42	9259	0.18	3.85	6.16	13.8	1.85	1333	11942	2.14	0.054
10 Percentile	0.39	76980	1.66	140	0.67	0.27	23200	0.01	15.8	7.04	4	2.47	1210	21920	16.8	0.08
25 Percentile	0.71	82650	2.1	215	0.74	0.46	28000	0.01	18.8	8.8	6.5	4.02	1620	32400	18.5	0.09
Median	1.17	88300	3	330	0.86	0.86	36600	0.01	21.3	11	16	5.11	2440	39200	20.4	0.1
75 Percentile	1.81	92300	5.15	505	1	1.36	41800	0.01	23.8	15.8	25	5.88	3440	46150	21.4	0.12
90 Percentile	2.52	96200	14	762	1.17	2.35	46320	0.03	25.3	21	36.6	7.13	4632	53500	22.6	0.12
Interquartile Range (IQR) [1]	1.1	9650	3.05	290	0.26	0.9	13800	0	5	6.95	18.5	1.85	1820	13750	2.88	0.03
Variance	0.68	44356026	33	74305	0.078	2.01	85737446	0.032	14.8	38	191	3.44	1775728	142622022	4.57	0.0029
Skewness	0.77	-0.38	2.61	1.23	2.42	2.57	-0.14	5.11	-0.65	1.37	1.33	0.42	0.68	-0.24	-0.49	2.96
Coefficient of Variation (CoV) [2]	0.61	0.076	1.13	0.66	0.31	1.13	0.26	3.38	0.18	0.47	0.76	0.37	0.5	0.31	0.11	0.47
Count	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59

3.36 NOTE: if data is boxed, then data is 3 times the maximum crustal abundance.

alerite

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

NOTE: If data was reported as > detection limit the detection limit is shown in bold and was used in subsequent calculations.

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: Sampled by MDAG on Feb 7'07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.

Sample Id.	Hafnium Hf (ppm)	Mercury Hg (ppm)	Indium In (ppm)	Potassium K (ppm)	Lanthanum La (ppm)	Lithium Li (ppm)	Magnesium Mg (ppm)	Manganese Mn (ppm)	Molybdenum Mo (ppm)	Sodium Na (ppm)	Niobium Nb (ppm)	Nickel Ni (ppm)	Phosphorus P (ppm)	Lead Pb (ppm)	Rubidium Rb (ppm)	Rhenium Re (ppm)
Method	ME-MS61	Hg-CV41	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.1	0.01	0.005	100	0.5	0.2	100	5	0.05	100	0.1	0.2	10	0.5	0.1	0.002
Crustal Abundance: From	0.3	0.03	0.01	40	10	5	1600	390	0.2	400	0.3	2	170	1	0.2	NA
Crustal Abundance: To	11	0.4	0.26	48000	115	66	47000	6700	27	40400	35	225	1500	80	170	NA
14018	1.9	0.01	0.065	24500	12.7	8.7	10700	476	36.3	31600	4.2	9.6	660	52	89.4	0.036
14021	1.7	*0.005*	0.082	22200	11.9	9.6	9200	629	348	23800	3.4	6.9	570	91.3	129.5	0.178
14036	1.7	*0.005*	0.087	21300	11.9	9.5	9100	475	658	24700	3	8.3	570	19.7	119.5	0.312
14043	1.4	*0.005*	0.041	10300	6.8	17.7	19000	446	324	32900	2.6	11.6	570	4.7	61.3	0.146
14060	2.2	*0.005*	0.053	12000	11.2	19.5	21000	422	220	30500	3.3	15.3	1290	5.8	67.9	0.133
14067	1.6	*0.005*	0.046	11200	10.1	26	26800	779	90.6	35100	2.7	16.2	1120	40.8	53.8	0.116
14076	1.9	0.01	0.06	14300	10.7	22.4	25000	1585	56.2	23000	2.6	15	1070	236	75.1	0.136
14083	1.4	0.01	0.076	30900	10.6	19.2	17700	1365	13.2	13600	2.5	17.2	1070	20	165	0.033
14099	1.4	0.02	0.04	32000	9.9	5.3	8200	1090	6.9	5400	3.2	6.5	470	23.4	177.5	0.002
14103	1.9	0.01	0.072	18100	12.3	7.8	12900	686	231	25100	2.9	10.2	620	8.2	93.2	0.185
14130	0.7	0.02	0.026	18100	6.3	3.5	10200	191	80.8	38300	3.8	4.1	1390	3.8	54.2	0.073
14144	0.7	0.01	0.05	15600	8.7	8.3	11600	451	72.5	34900	5.1	4.2	1830	4.7	47.1	0.049
14148	1	0.02	0.042	20600	10.6	13.3	18900	429	257	13800	4.2	5.5	1220	3.2	61.2	0.221
14156	1.6	*0.005*	0.027	12200	10.8	7	7900	339	77.8	37400	4.5	8.1	500	2.5	37.7	0.02
14162	1.9	*0.005*	0.062	16000	11.8	17.6	26200	853	479	19300	4.5	35	980	5.3	47.1	0.145
14169	1.4	0.02	0.036	9700	2.8	3.5	4000	278	176.5	47600	3.9	5.9	550	7.1	28.5	0.043
14232	0.9	0.01	0.05	16800	9.7	7.4	9100	189	97.4	42800	4.5	2.7	1430	2.5	55.2	0.09
14250	0.8	0.01	0.053	14600	11	15	18800	436	374	38300	4.3	2.5	1450	3.3	57.8	0.346
14260	0.8	0.01	0.09	15900	9.7	7.2	13900	275	173	38600	4	2.8	1390	3.8	61.3	0.145
14276	1.2	*0.005*	0.073	7600	9.1	11.6	16400	1085	22.8	40800	4.4	1.7	1440	6.7	20.9	0.008
14295	0.9	0.02	0.054	16000	8.3	12.1	15500	436	11.9	33600	4.1	4.5	1360	4.4	63.7	0.002
14301	1.4	0.01	0.058	19200	8.5	10.3	12400	517	215	27300	4.4	4.2	1380	3.6	56.5	0.137
14323	1	*0.005*	0.037	18200	8.9	7.5	9600	386	67.7	35000	4.6	2.2	1410	2.7	48.2	0.05
14332	1.1	0.01	0.055	20200	10.7	8.2	10400	281	102	32400	4.6	2.6	1470	2.8	64.7	0.072
14345	0.8	*0.005*	0.053	24000	12.1	6.9	10300	150	250	36900	3.9	3.1	1380	2.3	80.6	0.15
14348	0.9	0.01	0.053	18700	10.9	11.3	12100	191	170.5	38200	4.4	3	1520	2.3	65.9	0.135
14797	0.9	0.01	0.029	19500	6.4	16	15200	559	212	26700	4.6	4.2	1330	3.3	54.7	0.147
14808	1.2	0.06	0.037	20800	10.1	11.8	16300	493	580	20000	4	4.6	1080	7.6	83.3	0.936
14816	0.8	0.02	0.068	20900	7.8	9.4	17000	438	52.3	26700	4.9	5.2	1230	2.8	59.1	0.052
14828	0.8	0.03	0.032	17500	10.7	10.2	18200	507	182.5	32900	5	3.9	1280	5.9	65.3	0.119
14844	1.1	0.02	0.032	16900	6.9	26.3	37900	319	128	24600	5.9	23.4	1290	2.7	63.3	0.143
14680	1.8	0.02	0.035	16000	12.7	18.9	16500	493	500	34600	5.1	5.5	1300	5.4	84.9	0.326
14871	1	0.01	0.042	12300	8.7	12.3	19200	374	240	44300	5.9	7.3	1230	2.7	65.6	0.109
14887	1.1	0.01	0.042	11700	10.7	13	24700	613	8.29	35400	5.8	10.6	1200	2.8	51.1	0.003
14689	1.4	*0.005*	0.029	16400	14.4	3.3	5600	301	84.7	34300	2.7	6.4	540	1.6	42.9	0.065
14695	1.8	0.01	*0.0025*	22100	12.5	5.8	15100	611	641	30000	4.7	7.6	1400	3.4	83.4	0.499
14742	1.4	0.01	0.019	12800	8.2	11.2	22400	401	661	43600	5.4	16.2	1220	20.6	62	0.436
14666	1	*0.005*	0.048	12900	8.7	27.7	22000	543	28.4	35800	7	15.5	1250	2.2	42.3	0.04
14685	1	0.04	0.058	12100	9.5	25.9	27300	364	120	32000	4.5	9.1	1530	2.8	47.7	0.113
14685B	1.4	0.04	0.056	13200	8.7	24.9	28400	327	77.4	33900	4.3	7.9	1530	2.4	67.7	0.088
14545	1.5	*0.005*	0.055	11800	11	7.9	14000	273	14.05	35000	5.5	1.3	1330	2.4	52.5	0.004
14565	1.2	*0.005*	0.069	18600	10.1	9.9	12100	529	12.65	29900	5.1	1.6	1270	2.3	67.6	0.011
14571	1.4	0.01	0.058	14200	9.7	6.4	11700	230	101	32200	4.2	4.7	1030	3.6	53.4	0.062
14578	1.6	0.01	0.027	15800	10.1	7.6	11800	337	27	31500	5	6.7	1550	2.8	53.5	0.033
14578B	2.2	0.01	0.028	15800	9.4	8.2	12700	345	31.3	32900	4.9	5.8	1470	2.4	58.1	0.04
14598	0.7	*0.005*	0.022	12400	6.5	14.1	22100	631	53.3	31400	5.9	3.9	1540	2.3	26.5	0.071
14893	1.5	0.01	0.034	10200	9	16.7	27200	493	101	36600	6.5	19.8	1260	3.1	52.4	0.033
14899	0.9	0.01	0.024	7700	7	26.2	41300	546	19.2	34100	6.1	22.1	1260	3.3	18.9	0.014
14908	1.4	*0.005*	0.042	13700	9	17	24000	527	102.5	44700	7.1	18.7	1310	2.8	41.1	0.082
14917	2.3	0.01	0.023	16100	11	21.2	18300	379	17.15	47300	4.6	8.4	1100	3.8	50.4	0.01
14925	1.2	0.01	0.045	15400	7.8	16.2	20400	408	27.5	35600	6.8	16	1230	2.5	55	0.009
14998	0.9	0.01	0.036	12500	8.6	14.9	16300	452	65.2	41400	4.8	2.2	1440	2.5	42.7	0.035
15862	0.7	0.01	0.027	14800	8.2	12.4	17400	584	74	34400	5	4.4	1260	2.4	40.8	0.042
15870	1	*0.005*	0.035	18500	9.9	7.4	17700	539	17.9	26200	5.6	12.4	1120	3.2	70.5	0.01

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: Sampled by MDAG on Feb 7'07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.

Sample	Hafnium	Mercury	Indium	Potassium	Lanthanum	Lithium	Magnesium	Manganese	Molybdenum	Sodium	Niobium	Nickel	Phosphorus	Lead	Rubidium	Rhenium
Id.	Hf	Hg	In	K	La	Li	Mg	Mn	Mo	Na	Nb	Ni	P	Pb	Rb	Re
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	Hg-CV41	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.1	0.01	0.005	100	0.5	0.2	100	5	0.05	100	0.1	0.2	10	0.5	0.1	0.002
Crustal Abundance: From	0.3	0.03	0.01	40	10	5	1600	390	0.2	400	0.3	2	170	1	0.2	NA
Crustal Abundance: To	11	0.4	0.26	48000	115	66	47000	6700	27	40400	35	225	1500	80	170	NA
15879	1.2	0.01	0.035	14900	9.4	10.4	18800	554	20	32900	6.9	15.3	1280	3.8	56.7	0.018
15887	1	0.01	0.044	11900	6.7	11.3	15900	395	$\boxed{165.5}$	39300	6.5	11.6	1090	3.5	39.8	0.213
15891	0.9	0.01	0.021	17200	7.7	10.8	17300	558	$\boxed{104}$	34900	5.4	10.8	1120	3.6	60.8	0.08
15908	1	0.03	0.039	18000	8.4	10.9	18500	433	$\boxed{311}$	29000	6.1	12.6	1130	2.8	69.3	0.226
15911	1	0.02	0.027	13800	9.2	11.6	23100	402	$\boxed{154}$	32500	6.6	17.7	1250	2.5	69.5	0.135
Maximum	2.3	0.06	0.09	32000	14.4	27.7	41300	1585	661	47600	7.1	35	1830	236	178	0.94
Minimum	0.7	0.005	0.0025	7600	2.8	3.3	4000	150	6.9	5400	2.5	1.3	470	1.6	18.9	0.002
Mean	1.26	0.013	0.045	16247	9.54	12.8	17175	498	162	32500	4.71	9.02	1189	11.6	63.3	0.12
Standard Deviation	0.42	0.01	0.018	4772	1.99	6.3	7171	260	173	8004	1.19	6.66	309	32.9	28.3	0.15
10 Percentile	0.8	0.005	0.026	11600	6.88	6.8	9180	275	16.5	23640	2.98	2.58	570	2.38	40.6	0.0098
25 Percentile	0.9	0.005	0.032	12650	8.45	8.05	11950	354	33.8	29450	4.05	4.2	1095	2.6	49.3	0.034
Median	1.2	0.01	0.042	15900	9.7	11.3	16500	446	101	33600	4.6	6.9	1260	3.3	58.1	0.08
75 Percentile	1.5	0.01	0.056	18550	10.8	16.4	20700	550	218	36750	5.45	12.5	1390	5.35	67.8	0.14
90 Percentile	1.9	0.02	0.07	21460	11.9	22.9	26320	705	395	41680	6.5	17.3	1480	20.1	85.8	0.24
Interquartile Range (IQR) [1]	0.6	0.005	0.024	5900	2.3	8.4	8750	196	184	7300	1.4	8.3	295	2.75	18.5	0.11
Variance	0.17	0.0001	0.00033	22775295	3.98	39.7	51419515	67837	29834	64062759	1.41	44.3	95722	1086	802	0.023
Skewness	0.68	2.59	0.42	1.01	-0.45	0.84	0.98	2.21	1.63	-0.9	0.088	1.43	-1	5.92	2.14	3.26
Coefficient of Variation (CoV) [2]	0.33	0.81	0.4	0.29	0.21	0.49	0.42	0.52	1.07	0.25	0.25	0.74	0.26	2.84	0.45	1.24
Count	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59

$\boxed{3.36}$ NOTE: if data is boxed, then data is 3 times the maximum crustal abundance.

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

NOTE: If data was reported as > detection limit the detection limit is shown in bold and was used in subsequent calculations.

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: Sampled by MDAG on Feb 7'07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.

Sample	Sulphur	Antimony	Scandium	Selenium	Tin	Strontium	Tantalum	Tellurium	Thorium	Titanium	Thallium	Uranium	Vanadium	Tungsten	Yttrium	Zinc	Zirconium
Id.	S	Sb	Sc	Se	Sn	Sr	Ta	Te	Th	Ti	Tl	U	V	W	Y	Zn	Zr
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	100	0.05	1	1	0.2	0.2	0.05	0.05	0.2	50	0.02	0.1	1	0.1	0.1	2	0.5
Crustal Abundance: From	240	0.1	NA	0.05	0.5	1	0.8	NA	0.004	300	0.16	0.45	20	0.6	20	16	19
Crustal Abundance: To	2400	1.5	NA	0.6	6	2000	4.2	NA	17	13800	2.3	3.7	250	2.2	90	165	500
14018	8800	3.69	7.9	2	1.1	428	0.32	0.26	3.7	2400	0.6	2.3	70	12.8	10.8	41	50.3
14021	7000	6.36	7.7	2	1.2	173	0.28	0.09	3.3	2080	0.75	1.9	65	18.4	12.5	56	45.5
14036	16000	7.99	7.3	4	1.5	235	0.21	0.72	3.3	1970	0.71	1.9	67	25	10.2	41	41.3
14043	2800	4.34	10.2	2	1	276	0.22	0.07	2.3	2190	0.42	1.4	102	27	7.6	45	40.3
14060	14800	2.49	16.5	3	1	423	0.22	0.06	2.4	4100	0.44	1.6	155	30.1	17.1	27	66.3
14067	4300	3.8	21.1	4	1.1	410	0.17	0.06	1.5	4170	0.38	1.1	182	12.1	17.5	71	49.5
14076	9500	5.5	24.4	2	1.2	365	0.18	0.18	1.9	4540	0.47	1	197	6.5	19.9	163	55.8
14083	16000	5.68	24.7	2	1.6	232	0.16	0.27	1.7	4480	0.95	0.9	204	10.3	19.5	127	40.6
14099	3600	3.71	5	1	0.6	88	0.24	0.05	2.7	1670	1.04	1.9	47	17.4	8.2	205	33.7
14103	7700	4.72	10.2	3	1.1	197.5	0.24	0.05	3	2220	0.67	1.8	119	20.2	10.4	67	51.2
14130	3200	1.25	6.3	5	0.9	288	0.22	0.51	0.8	2800	0.28	0.3	73	5.6	12.7	26	19.7
14144	2800	2.5	6.8	4	0.9	343	0.29	0.54	0.9	3760	0.27	0.5	91	4	16.2	46	19.6
14148	1400	2.35	11.4	3	1.2	223	0.25	0.27	0.8	3780	0.31	0.9	146	4.9	15.6	40	28.9
14156	1700	1.66	5.6	3	1.1	259	0.33	0.09	3.1	1900	0.17	1.9	47	10.5	8.5	35	39.3
14162	1500	2.42	21.4	2	1.2	239	0.28	0.17	1.8	4270	0.22	1.1	159	5.2	15.7	67	59.6
14169	3200	1.63	5.9	3	1.9	207	0.3	0.46	2.8	1960	0.15	1.7	65	13	6.3	24	36.9
14232	1600	3.64	6.8	3	1.1	345	0.27	0.23	0.9	3290	0.3	0.5	87	3.5	14.5	21	23.6
14250	2000	3.46	12.1	3	1.4	424	0.25	0.29	0.8	4350	0.28	0.5	236	3.3	16.9	38	18.3
14260	3700	2.5	11.4	6	1.6	402	0.23	0.85	0.7	4050	0.31	0.5	144	4.5	14.3	36	17.6
14276	1700	10.95	7.2	2	1	798	0.28	0.07	1	4100	0.14	0.6	112	4.9	17.8	112	29.9
14295	4900	3.4	14.1	2	1.8	336	0.25	0.08	0.7	4240	0.38	0.7	154	15.6	14.8	34	23.5
14301	3500	2.57	11	3	1.6	209	0.26	0.13	1	3620	0.3	0.6	117	10.5	14.7	38	47.1
14323	1500	2.29	6.5	2	1.3	391	0.27	0.17	0.8	3310	0.31	0.4	94	3.3	15.5	29	29.3
14332	2700	1.94	6.9	2	1.4	355	0.27	0.19	0.9	3260	0.32	0.5	103	3.5	16.6	31	32.2
14345	5600	2.33	7.3	5	3.8	274	0.24	0.29	0.9	2970	0.41	0.6	101	14.5	14.8	27	20
14348	4800	2.53	6.8	3	1.7	276	0.27	0.19	0.9	3190	0.4	0.5	74	5.8	13.9	40	22.1
14797	700	4.83	11	3	1.2	234	0.28	0.15	0.6	4150	0.38	0.3	152	5.7	12	42	20.9
14808	1900	5.13	9.8	7	1.4	221	0.24	0.45	1	3260	0.43	0.7	117	4.5	14.5	34	34
14816	4700	3.45	10.9	5	1.7	285	0.28	0.77	0.7	3810	0.36	0.4	144	6.2	13.1	49	18.4
14828	1400	1.72	11.4	6	1.1	404	0.29	0.5	0.8	3940	0.29	0.4	141	3.3	17.5	32	20.7
14844	2200	5.28	17.9	4	1.4	265	0.33	0.23	1	5590	0.49	0.6	262	3.3	13	40	30.5
14680	2200	5.2	12.8	8	1.4	348	0.3	0.77	1.1	4040	0.43	0.7	151	4.8	17.8	38	64.4
14871	3800	4.15	12.7	4	1.7	405	0.31	0.19	1	4990	0.32	0.7	183	6	15.3	43	22.6
14887	5400	1.41	14	2	1.3	424	0.33	0.09	1.2	4960	0.28	0.7	188	5.2	15.1	39	22.8
14689	7900	1.27	5.3	3	0.9	141	0.21	0.15	3.1	1580	0.18	1.6	51	3	8.3	16	33.4
14695	1600	3.83	11.9	5	1.5	226	0.25	0.18	1	4310	0.23	0.9	161	6	14.9	49	48.5
14742	2100	2.37	15.2	7	1.9	302	0.34	0.23	1.6	4690	0.25	0.9	215	6.6	12	53	32.7
14666	3800	3.07	15.1	3	1.5	416	0.41	0.06	1.3	5070	0.27	1	209	8	15.4	38	27.7
14685	21000	3.51	25.5	6	2.2	393	0.26	0.15	1.3	7690	0.32	1	269	5.5	14.5	43	35
14685B	20400	3.19	23.4	5	1.9	374	0.25	0.14	1.4	7930	0.37	0.9	276	5.2	13.6	46	43.4
14545	1900	1.48	8.5	1	1.4	409	0.36	0.05	1.5	3980	0.26	0.8	90	4.2	16.3	26	44.7
14565	2600	4.4	8.3	2	1.4	259	0.32	0.14	1.3	3800	0.37	0.6	80	4.7	16.9	16	32.5
14571	11100	2.6	7.8	5	1.4	312	0.28	0.15	2.3	3170	0.26	1.3	86	4.8	11.2	34	42
14578	21300	2.42	11	4	1.4	324	0.33	0.11	1.8	4630	0.29	1.2	112	4.1	15.9	19	56
14578B	21100	2.47	11.3	4	1.4	330	0.3	0.09	2	4430	0.32	1.2	111	4.1	17.1	19	74.1
14598	1500	1.89	8.4	2	0.9	569	0.36	0.06	0.6	4330	0.28	0.4	131	2.7	13.2	47	22.7
14893	1100	6.95	20.1	3	1.7	379	0.36	0.12	1.3	6030	0.25	1.5	283	9.3	15.3	49	40.7
14899	200	3.09	19.4	2	1	366	0.34	0.06	1	5850	0.16	0.6	262	8.2	13.8	52	25.5
14908	900	4.87	19	2	1.6	479	0.39	0.1	1.6	5910	0.22	1.2	268	12.1	16.7	42	34.7
14917	1900	4.6	17.7	4	1.7	309	0.3	0.26	2.8	4580	0.22	1.7	178	8.9	16.1	44	74.3
14925	1500	6.54	15.5	3	1.7	353	0.38	0.11	1.4	5090	0.29	0.7	224	5.1	15	52	31
14998	1300	5.17	10.8	3	1.4	412	0.26	0.16	0.7	4460	0.3	0.6	152	13.5	16.6	41	22.5
15862	800	2.81	11.3	2	1.1	327	0.29	0.12	0.7	4050	0.29	0.3	146	2.9	14	49	17.8
15870	1400	6.6	14.3	3	1.4	234	0.31	0.15	1.3	4460	0.36	0.8	203	6.1	16.1	53	23.4

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: Sampled by MDAG on Feb 7'07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.

Sample	Sulphur	Antimony	Scandium	Selenium	Tin	Strontium	Tantalum	Tellurium	Thorium	Titanium	Thallium	Uranium	Vanadium	Tungsten	Yttrium	Zinc	Zirconium
Id.	S	Sb	Sc	Se	Sn	Sr	Ta	Te	Th	Ti	Tl	U	V	W	Y	Zn	Zr
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	100	0.05	1	1	0.2	0.2	0.05	0.05	0.2	50	0.02	0.1	1	0.1	0.1	2	0.5
Crustal Abundance: From	240	0.1	NA	0.05	0.5	1	0.8	NA	0.004	300	0.16	0.45	20	0.6	20	16	19
Crustal Abundance: To	2400	1.5	NA	0.6	6	2000	4.2	NA	17	13800	2.3	3.7	250	2.2	90	165	500
15879	1200	$\boxed{7.41}$	17.1	$\boxed{3}$	1.3	373	0.39	0.16	1.5	5450	0.28	0.9	246	3.3	16	63	27.3
15887	3300	$\boxed{5.99}$	15.3	$\boxed{5}$	1.7	402	0.34	0.37	1	5100	0.24	0.7	214	3.6	13.6	42	23.2
15891	1400	$\boxed{7.05}$	15	$\boxed{4}$	1.3	382	0.3	0.23	1.1	4920	0.31	0.6	213	5.3	15.1	51	19.4
15908	2200	$\boxed{6.21}$	14.2	$\boxed{5}$	1.5	288	0.32	0.29	1.2	4740	0.34	0.8	207	5.4	15.5	43	26.1
15911	900	$\boxed{4.97}$	17.9	$\boxed{3}$	1.3	335	0.37	0.13	1.5	5430	0.29	0.7	248	3	15.3	49	26.4
Maximum	21300	11	25.5	8	3.8	798	0.41	0.85	3.7	7930	1.04	2.3	283	30.1	19.9	205	74.3
Minimum	200	1.25	5	1	0.6	88	0.16	0.05	0.6	1580	0.14	0.3	47	2.7	6.3	16	17.6
Mean	4966	3.93	12.6	3.46	1.41	330	0.29	0.22	1.5	4086	0.35	0.93	152	8.08	14.4	48.1	34.9
Standard Deviation	5631	1.97	5.39	1.53	0.44	108	0.055	0.19	0.81	1307	0.17	0.5	66.7	6.18	2.86	32	14.5
10 Percentile	1180	1.71	6.74	2	1	219	0.22	0.06	0.7	2168	0.22	0.4	69.4	3.3	10.4	25.6	19.7
25 Percentile	1500	2.45	7.85	2	1.1	259	0.25	0.095	0.9	3275	0.27	0.6	97.5	4.15	13.2	34	23
Median	2700	3.51	11.4	3	1.4	335	0.28	0.16	1.3	4150	0.31	0.8	146	5.5	15	42	32.2
75 Percentile	5150	5.15	15.4	4	1.6	398	0.32	0.26	1.8	4715	0.38	1.2	206	10.4	16.2	49	42.7
90 Percentile	15040	6.55	20.3	5.2	1.72	423	0.36	0.5	2.84	5478	0.51	1.72	251	16	17.2	67	55.8
Interquartile Range (IQR)[1]	3650	2.7	7.55	2	0.5	138	0.075	0.17	0.9	1440	0.11	0.6	108	6.25	3	15	19.7
Variance	31711935	3.88	29.1	2.36	0.19	11719	0.0031	0.037	0.66	1709027	0.03	0.25	4454	38.2	8.16	1027	211
Skewness	1.91	1.03	0.69	0.9	2.75	1.22	0.037	1.81	1.15	0.35	2.21	0.95	0.29	1.9	-0.91	3.21	1
Coefficient of Variation (CoV)[2]	1.13	0.5	0.43	0.44	0.31	0.33	0.19	0.86	0.54	0.32	0.49	0.53	0.44	0.76	0.2	0.67	0.42
Count	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59

$\boxed{3.36}$ NOTE: if data is boxed, then data is 3 times the maximum crustal abundance.

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

NOTE: If data was reported as > detection limit the detection limit is shown in bold and was used in subsequent calculations.

Project:	**Schaft Creek**
Client:	Copper Fox Metals Inc.
Data:	**Whole Rock by XRF**
Comments:	Sampled by MDAG on Feb 7'07.

Sample Id.	Al_2O_3	BaO	CaO	Cr_2O_3	Fe_2O_3	K_2O	MgO	MnO	Na_2O	P_2O_5	SiO_2	SrO	TiO_2	LOI	Total
	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
Method	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06
MDL	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		
14018	16.2	0.13	2.53	*0.005*	3.77	2.92	1.74	0.05	4.01	0.14	62.92	0.05	0.42	3.69	98.58
14021	14.75	0.05	3.56	*0.005*	2.62	2.59	1.47	0.07	2.96	0.12	65.03	0.02	0.36	4.86	98.47
14036	14.93	0.06	2.56	*0.005*	3.72	2.51	1.51	0.05	3.13	0.12	64.89	0.03	0.38	4.53	98.43
14043	15.21	0.03	1.98	*0.005*	4.23	1.18	3.06	0.05	4.13	0.12	64.74	0.03	0.41	3.53	98.71
14060	15.16	0.04	4.27	*0.005*	5.14	1.42	3.28	0.05	3.71	0.26	58.18	0.05	0.73	6.18	98.48
14067	16.07	0.04	3.54	0.01	6.18	1.29	4.07	0.09	4.15	0.22	57.69	0.04	0.7	4.08	98.17
14076	16.09	0.05	5.61	*0.005*	7.43	1.58	3.72	0.19	2.64	0.21	55.56	0.04	0.72	5.1	98.95
14083	16.4	0.08	5.33	*0.005*	8.26	3.49	2.82	0.17	1.62	0.21	53.34	0.02	0.74	6.28	98.77
14099	15.15	0.1	4.16	*0.005*	3.38	3.94	1.47	0.14	0.73	0.11	63.71	0.01	0.31	5.67	98.89
14103	15	0.03	4.03	*0.005*	3.11	2.07	2.04	0.08	2.99	0.13	61.55	0.02	0.41	6.91	98.38
14130	17.11	0.06	3.59	*0.005*	2.6	2.11	1.61	0.02	4.61	0.28	60.15	0.03	0.53	5.91	98.62
14144	18.29	0.04	4.95	*0.005*	5.05	1.84	1.81	0.05	4.05	0.36	53.8	0.04	0.63	7.48	98.40
14148	16.83	0.07	6.26	*0.005*	5.63	2.49	3.13	0.05	1.72	0.26	52	0.03	0.64	9.85	98.97
14156	15.34	0.03	3.29	*0.005*	2.46	1.41	1.21	0.03	4.53	0.1	64.96	0.03	0.29	4.66	98.35
14162	14.36	0.06	7.5	0.01	5.92	1.79	3.97	0.1	2.27	0.2	50.21	0.02	0.69	11.1	98.20
14169	15.54	0.01	3.15	*0.005*	1.69	1.07	0.61	0.03	5.76	0.12	66.91	0.02	0.31	3.74	98.97
14232	19.47	0.02	3.67	*0.005*	3.86	2.01	1.48	0.02	5.31	0.3	56.55	0.04	0.61	5.19	98.54
14250	18.02	0.02	5.47	*0.005*	6.59	1.67	2.87	0.05	4.48	0.28	51.91	0.04	0.75	6.29	98.45
14260	17.85	0.02	4.18	*0.005*	6.23	1.9	2.21	0.03	4.77	0.28	54.62	0.04	0.72	5.77	98.63
14276	19.76	0.12	5.87	*0.005*	5.6	0.86	2.56	0.14	4.97	0.29	54.07	0.08	0.67	3.49	98.49
14295	17.5	0.01	5.22	*0.005*	6.81	1.83	2.43	0.05	4	0.27	53.53	0.03	0.73	6.48	98.90
14301	17.72	0.03	4.93	*0.005*	4.47	2.34	2	0.06	3.33	0.28	54.86	0.02	0.7	7.95	98.70
14323	19.07	0.03	5.02	*0.005*	5.54	2.1	1.55	0.04	4.17	0.28	54.65	0.04	0.56	5.5	98.56
14332	19.78	0.02	4.67	*0.005*	5.19	2.46	1.71	0.03	4.03	0.3	54.16	0.04	0.6	5.57	98.57
14345	19.52	0.02	3.44	*0.005*	3.18	2.73	1.64	0.01	4.47	0.28	57.5	0.03	0.58	5.16	98.57
14348	19.93	0.02	3.09	*0.005*	5.12	2.25	1.97	0.02	4.79	0.31	54.97	0.03	0.61	5.01	98.13
14797	18.18	0.02	5.12	*0.005*	6.2	2.28	2.46	0.06	3.22	0.27	51.74	0.03	0.7	8.21	98.50
14808	15.54	0.02	6.64	*0.005*	5.44	2.49	2.62	0.06	2.5	0.23	52.62	0.02	0.56	10.2	98.95
14816	17.11	0.02	4.56	*0.005*	6.06	2.5	2.78	0.05	3.25	0.26	53.34	0.03	0.65	7.62	98.24
14828	17.1	0.08	5.7	*0.005*	5.75	1.94	2.73	0.06	3.81	0.25	51.87	0.04	0.63	8.24	98.21
14844	17.61	0.04	3.8	*0.005*	7.4	1.98	5.94	0.03	2.92	0.26	52.79	0.03	0.93	5.17	98.91
14680	17.54	0.03	5.54	0.01	6.31	1.81	2.5	0.06	4.05	0.26	53.34	0.04	0.67	6.08	98.24
14871	18.56	0.01	4.62	*0.005*	6.55	1.36	2.87	0.04	5.16	0.24	53.53	0.04	0.82	4.77	98.58
14887	17.6	0.04	6.71	*0.005*	7.31	1.24	3.61	0.07	4.05	0.23	50.56	0.04	0.79	6.23	98.49
14689	15.75	0.01	2.71	*0.005*	1.96	1.91	0.91	0.03	4.34	0.11	66.25	0.02	0.33	3.81	98.15
14695	17.98	0.02	4.98	*0.005*	5.19	2.57	2.41	0.07	3.57	0.26	53.38	0.02	0.68	7.34	98.48
14742	18.48	0.02	3.84	*0.005*	4.8	1.49	3.39	0.04	5.21	0.25	54.87	0.03	0.86	4.97	98.26
14666	17.45	0.04	5.2	*0.005*	7.38	1.53	3.59	0.06	4.43	0.25	53.21	0.04	0.84	4.88	98.91
14685	16.54	0.05	4.49	*0.005*	8.92	1.47	4.51	0.04	4.03	0.31	49.87	0.04	1.38	7.01	98.67
14685B	16.58	0.04	4.16	*0.005*	9.45	1.54	4.37	0.04	3.98	0.3	50.4	0.04	1.38	5.99	98.28
14545	18.58	0.1	5.18	*0.005*	5.98	1.37	2.17	0.03	4.2	0.27	56.26	0.04	0.65	4.1	98.94
14565	17.23	0.02	6.05	*0.005*	5.25	2.14	1.89	0.06	3.57	0.26	53.85	0.03	0.63	7.44	98.43
14571	16.48	0.05	3.51	*0.005*	3.99	1.76	2.03	0.02	4.32	0.22	59.95	0.04	0.59	5.14	98.11
14578	16.78	0.07	5.57	*0.005*	5.71	1.89	1.99	0.04	4	0.31	54.01	0.03	0.86	7.27	98.54
14578B	16.4	0.09	5.75	*0.005*	5.95	1.84	1.97	0.04	3.91	0.3	54.47	0.03	0.82	6.61	98.19
14598	19.18	0.02	4.52	*0.005*	6.5	1.54	3.79	0.07	3.95	0.31	52.94	0.06	0.74	5.22	98.85
14893	17.39	0.05	5.57	*0.005*	7.59	1.11	4.07	0.06	4.23	0.25	50.42	0.04	1	6.37	98.16
14899	18.24	0.04	4.77	*0.005*	8.14	0.9	6.3	0.06	3.94	0.25	48.95	0.04	0.97	5.91	98.52
14908	17.57	0.08	4.99	*0.005*	7.49	1.51	3.56	0.06	5.09	0.26	52.92	0.05	0.97	3.87	98.43
14917	16.75	0.09	3.18	*0.005*	3.43	1.86	2.74	0.04	5.62	0.22	59.61	0.03	0.8	3.75	98.13
14925	17.48	0.04	4.83	*0.005*	6.57	1.8	3.11	0.05	4.16	0.25	54.26	0.04	0.88	4.77	98.25
14998	17.84	0.03	5.3	*0.005*	6.2	1.39	2.47	0.05	4.81	0.28	53.76	0.04	0.72	5.99	98.89
15862	17.45	0.03	5.66	*0.005*	6.02	1.73	2.74	0.07	4.12	0.26	52.87	0.03	0.68	7.2	98.87
15870	15.28	0.12	6.1	*0.005*	5.48	2.09	2.68	0.06	3.07	0.23	54.41	0.03	0.74	8.21	98.51
15879	17.04	0.09	6.38	*0.005*	7.37	1.69	2.84	0.06	3.81	0.25	50.72	0.04	0.9	7.09	98.29
15887	17.84	0.05	5.62	*0.005*	5.41	1.4	2.46	0.04	4.64	0.22	54.43	0.04	0.86	5.38	98.40

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Whole Rock by XRF**
Comments: Sampled by MDAG on Feb 7'07.

Sample Id.	Al_2O_3	BaO	CaO	Cr_2O_3	Fe_2O_3	K_2O	MgO	MnO	Na_2O	P_2O_5	SiO_2	SrO	TiO_2	LOI	Total
	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
Method	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06
MDL	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		
15891	17.63	0.15	6.76	*0.005*	5.43	1.99	2.66	0.06	4.12	0.23	51.38	0.04	0.86	7.61	98.93
15908	17.38	0.03	6.09	*0.005*	4.92	2.09	2.86	0.05	3.44	0.23	53.48	0.03	0.81	7.13	98.55
15911	17.39	0.05	4.88	*0.005*	6.78	1.62	3.54	0.05	3.89	0.25	52.8	0.04	0.91	5.87	98.08
Maximum	19.9	0.15	7.5	0.01	9.45	3.94	6.3	0.19	5.76	0.36	66.9	0.08	1.38	11.1	
Minimum	14.4	0.01	1.98	0.005	1.69	0.86	0.61	0.01	0.73	0.1	49	0.01	0.29	3.49	
Mean	17.2	0.048	4.76	0.0053	5.54	1.89	2.69	0.057	3.91	0.24	55.5	0.035	0.7	6.02	
Standard Deviation	1.37	0.033	1.19	0.0011	1.7	0.58	1.08	0.033	0.95	0.06	4.56	0.011	0.22	1.65	
10 Percentile	15.2	0.02	3.17	0.005	3.17	1.28	1.5	0.03	2.86	0.12	50.7	0.02	0.4	3.86	
25 Percentile	16.3	0.02	3.82	0.005	4.64	1.5	1.97	0.04	3.5	0.22	52.8	0.03	0.6	4.92	
Median	17.4	0.04	4.93	0.005	5.63	1.84	2.62	0.05	4.03	0.25	54	0.04	0.7	5.91	
75 Percentile	17.9	0.06	5.59	0.005	6.56	2.12	3.2	0.06	4.45	0.28	57	0.04	0.82	7.11	
90 Percentile	19.1	0.092	6.13	0.005	7.44	2.52	3.99	0.082	4.99	0.3	63.9	0.04	0.91	8	
Interquartile Range (IQR) [1]	1.62	0.04	1.77	0	1.93	0.62	1.24	0.02	0.94	0.06	4.19	0.01	0.21	2.18	
Variance	1.88	0.0011	1.43	1.2E-06	2.89	0.33	1.18	0.0011	0.9	0.0036	20.8	0.00012	0.047	2.72	
Skewness	-0.0061	1.24	-0.16	4.2	-0.21	1.03	1.01	2.22	-0.92	-0.99	1.15	1.02	0.6	0.79	
Coefficient of Variation (CoV) [2]	0.08	0.68	0.25	0.21	0.31	0.31	0.4	0.59	0.24	0.25	0.082	0.32	0.31	0.27	
Count	59	59	59	59	59	59	59	59	59	59	59	59	59	59	

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Calculated Mineralogy**
Comments: Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Calculated S (Pyrite) FeS_2 (%)	Calculated S (Chalcopyrite) $CuFeS_2 + CuS_2$ (%)	Calculated S (Arsenopyrite) FeAsS + AsS (%)	Calculated S (Galena) PbS (%)	Calculated S (Cinnibar) HgS (%)	Calculated S (Molybdenite) MoS_2 (%)	Calculated S (Sphalerite) ZnS (%)
14018	0.632	0.130	0.00067	0.00081	0.000000160	0.0024	0.0021
14021	0.400	0.176	0.00105	0.00142	0.000000080	0.0232	0.0028
14036	1.211	0.194	0.00130	0.00031	0.000000080	0.0439	0.0021
14043	0.090	0.134	0.00047	0.00007	0.000000080	0.0216	0.0023
14060	0.340	0.264	0.00061	0.00009	0.000000080	0.0147	0.0014
14067	0.151	0.248	0.00074	0.00063	0.000000080	0.0060	0.0036
14076	0.612	0.131	0.00065	0.00366	0.000000160	0.0037	0.0082
14083	1.293	0.137	0.00060	0.00031	0.000000160	0.0009	0.0064
14099	0.181	0.122	0.00009	0.00036	0.000000320	0.0005	0.0103
14103	-0.021	0.266	0.00024	0.00013	0.000000160	0.0154	0.0034
14130	-0.275	0.559	0.00009	0.00006	0.000000320	0.0054	0.0013
14144	-0.105	0.344	0.00022	0.00007	0.000000160	0.0048	0.0023
14148	-0.190	0.291	0.00011	0.00005	0.000000320	0.0171	0.0020
14156	-0.059	0.211	0.00005	0.00004	0.000000080	0.0052	0.0018
14162	-0.018	0.103	0.00009	0.00008	0.000000080	0.0319	0.0034
14169	-0.106	0.386	0.00008	0.00011	0.000000320	0.0118	0.0012
14232	-0.207	0.340	0.00015	0.00004	0.000000160	0.0065	0.0011
14250	-0.157	0.320	0.00015	0.00005	0.000000160	0.0249	0.0019
14260	-0.166	0.493	0.00011	0.00006	0.000000160	0.0115	0.0018
14276	-0.018	0.151	0.00032	0.00010	0.000000080	0.0015	0.0056
14295	0.195	0.235	0.00016	0.00007	0.000000320	0.0008	0.0017
14301	0.066	0.246	0.00016	0.00006	0.000000160	0.0143	0.0019
14323	-0.095	0.227	0.00014	0.00004	0.000000080	0.0045	0.0015
14332	-0.099	0.351	0.00009	0.00004	0.000000160	0.0068	0.0016
14345	-0.111	0.613	0.00009	0.00004	0.000000080	0.0167	0.0014
14348	-0.058	0.495	0.00010	0.00004	0.000000160	0.0114	0.0020
14797	-0.122	0.177	0.00011	0.00005	0.000000160	0.0141	0.0021
14808	-0.136	0.267	0.00000	0.00012	0.000000960	0.0387	0.0017
14816	0.053	0.401	0.00008	0.00004	0.000000320	0.0035	0.0025
14828	-0.235	0.329	0.00010	0.00009	0.000000480	0.0122	0.0016
14844	-0.113	0.302	0.00016	0.00004	0.000000320	0.0085	0.0020
14680	-0.226	0.399	0.00008	0.00008	0.000000320	0.0333	0.0019
14871	-0.047	0.392	0.00010	0.00004	0.000000160	0.0160	0.0022
14887	0.216	0.201	0.00012	0.00004	0.000000160	0.0006	0.0020
14689	0.479	0.204	0.00006	0.00002	0.000000080	0.0056	0.0008
14695	-0.066	0.152	0.00000	0.00005	0.000000160	0.0427	0.0025
14742	-0.069	0.212	0.00002	0.00032	0.000000160	0.0441	0.0027
14666	0.161	0.145	0.00021	0.00003	0.000000080	0.0019	0.0019
14685	1.352	0.437	0.00028	0.00004	0.000000640	0.0080	0.0022
14685B	1.467	0.462	0.00025	0.00004	0.000000640	0.0052	0.0023
14545	0.039	0.122	0.00015	0.00004	0.000000080	0.0009	0.0013
14565	-0.032	0.270	0.00013	0.00004	0.000000080	0.0008	0.0008
14571	0.471	0.551	0.00014	0.00006	0.000000160	0.0067	0.0017
14578	1.516	0.301	0.00022	0.00004	0.000000160	0.0018	0.0010
14578B	1.575	0.331	0.00019	0.00004	0.000000160	0.0021	0.0010
14598	0.053	0.071	0.00012	0.00004	0.000000080	0.0036	0.0024
14893	-0.094	0.165	0.00019	0.00005	0.000000160	0.0067	0.0025
14899	-0.026	0.041	0.00035	0.00005	0.000000160	0.0013	0.0026
14908	-0.054	0.115	0.00027	0.00004	0.000000080	0.0068	0.0021
14917	-0.221	0.384	0.00007	0.00006	0.000000160	0.0011	0.0022
14925	-0.041	0.163	0.00015	0.00004	0.000000160	0.0018	0.0026
14998	-0.068	0.182	0.00015	0.00004	0.000000160	0.0043	0.0021
15862	-0.058	0.119	0.00009	0.00004	0.000000160	0.0049	0.0025
15870	-0.108	0.204	0.00011	0.00005	0.000000080	0.0012	0.0027
15879	-0.126	0.217	0.00010	0.00006	0.000000160	0.0013	0.0032
15887	-0.231	0.512	0.00009	0.00005	0.000000160	0.0110	0.0021
15891	-0.153	0.247	0.00007	0.00006	0.000000160	0.0069	0.0026
15908	-0.245	0.430	0.00006	0.00004	0.000000480	0.0207	0.0022

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Calculated Mineralogy**
Comments: Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Calculated S (Pyrite) FeS_2 (%)	Calculated S (Chalcopyrite) $CuFeS_2 + CuS_2$ (%)	Calculated S (Arsenopyrite) FeAsS + AsS (%)	Calculated S (Galena) PbS (%)	Calculated S (Cinnibar) HgS (%)	Calculated S (Molybdenite) MoS_2 (%)	Calculated S (Sphalerite) ZnS (%)
15911	-0.122	0.184	0.00009	0.00004	0.000000320	0.0103	0.0025
Maximum	1.58	0.61	0.0013	0.0037	0.00000096	0.044	0.01
Minimum	-0.28	0.041	0.0000043	0.000025	0.00000008	0.00046	0.0008
Mean	0.14	0.27	0.00022	0.00018	0.0000002	0.011	0.0024
Standard Deviation	0.48	0.13	0.00025	0.00051	0.00000016	0.012	0.0016
10 Percentile	-0.21	0.12	0.000071	0.000037	0.00000008	0.0011	0.0013
25 Percentile	-0.12	0.16	0.00009	0.00004	0.00000008	0.0023	0.0017
Median	-0.054	0.25	0.00013	0.000051	0.00000016	0.0067	0.0021
75 Percentile	0.17	0.35	0.00022	0.000083	0.00000016	0.014	0.0024
90 Percentile	0.75	0.47	0.0006	0.00031	0.00000032	0.026	0.0034
Interquartile Range (IQR) [1]	0.29	0.18	0.00013	0.000043	0.00000008	0.012	0.00075
Variance	0.23	0.018	0.000000061	0.00000026	2.7E-14	0.00013	0.0000026
Skewness	1.99	0.68	2.61	5.92	2.59	1.63	3.21
Coefficient of Variation (CoV) [2]	3.39	0.5	1.13	2.84	0.81	1.07	0.67
Count	59	59	59	59	59	59	59

Calculated S (Pyrite) (%) =
% S (Sulphide) + S (del) - S (Chalcopyrite) - S (Arsenopyrite) - S (Galena) - S (Cinnibar) - S (Molybdenite) - S (Sph
Calculated S (Chalcopyrite) CuFeS2 + CuS2 (%) = (1 / 0.99) * Copper (ppm) / 10000
Calculated S (Arsenopyrite) FeAsS + AsS (%) = (1 / 2.33) * Iron (%) / 10000
Calculated S (Galena) PbS (%) = (1 / 6.45) * Iron (ppm) / 10000
Calculated S (Cinnibar) HgS (%) = (1 / 6.25) * Gallium (ppm) / 10000
Calculated S (Molybdenite) MoS2 (%) = (1 / 1.5) * Germanium (ppm) / 10000
Calculated S (Sphalerite) ZnS (%) = (1 / 2) * Hafnium (ppm) / 10000

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Whole Rock Al * (ppm)	ICP Al (ppm)	Difference (%) [3]	Whole Rock Ba * (ppm)	ICP Ba (ppm)	Difference (%) [3]	Whole Rock Ca * (ppm)	ICP Ca (ppm)	Difference (%) [3]	Whole Rock Cr * (ppm)	ICP Cr (ppm)	Difference (%) [3]	Whole Rock Fe * (ppm)	ICP Fe (ppm)	Difference (%) [3]
14018	85735	80300	-6.34	1164	1120	-3.81	18082	17800	-1.56	34	24	-29.85	26369	25800	-2.16
14021	78061	77000	-1.36	448	460	2.72	25443	26200	2.97	34	21	-38.62	18325	18100	-1.23
14036	79014	74100	-6.22	537	500	-6.96	18296	18400	0.57	34	20	-41.54	26019	25600	-1.61
14043	80495	75600	-6.08	269	230	-14.40	14151	14000	-1.07	34	31	-9.38	29586	28500	-3.67
14060	80231	79600	-0.79	358	380	6.07	30517	31400	2.89	34	26	-24.00	35951	35900	-0.14
14067	85047	85100	0.06	358	370	3.28	25300	25900	2.37	68	36	-47.38	43225	42900	-0.75
14076	85153	90000	5.69	448	410	-8.45	40094	43400	8.24	34	33	-3.54	51968	54600	5.06
14083	86793	88500	1.97	717	700	-2.31	38093	40300	5.79	34	49	43.23	57773	57800	0.05
14099	80178	72400	-9.70	896	770	-14.03	29731	29500	-0.78	34	16	-53.23	23641	22300	-5.67
14103	79384	76000	-4.26	269	250	-6.96	28802	29300	1.73	34	20	-41.54	21752	21200	-2.54
14130	90551	85100	-6.02	537	440	-18.12	25657	26200	2.11	34	15	-56.15	18185	18000	-1.02
14144	96796	93900	-2.99	358	380	6.07	35377	37500	6.00	34	5	-85.38	35322	36100	2.20
14148	89069	81100	-8.95	627	560	-10.68	44740	46300	3.49	34	4	-88.31	39378	38300	-2.74
14156	81183	76900	-5.28	269	280	4.21	23513	24700	5.05	34	25	-26.92	17206	17400	1.13
14162	75997	79700	4.87	537	510	-5.10	53602	55900	4.29	68	71	3.77	41407	42500	2.64
14169	82242	76400	-7.10	90	100	11.65	22513	23200	3.05	34	16	-53.23	11820	11800	-0.17
14232	103041	94400	-8.39	179	140	-21.85	26229	26600	1.41	34	14	-59.08	26998	26400	-2.22
14250	95367	94400	-1.01	179	170	-5.10	39094	40700	4.11	34	12	-64.92	46093	45800	-0.64
14260	94467	89500	-5.26	179	170	-5.10	29874	30400	1.76	34	3	-91.23	43575	42300	-2.93
14276	104575	98400	-5.91	1075	1000	-6.96	41952	43100	2.74	34	17	-50.31	39168	38900	-0.69
14295	92615	89700	-3.15	90	110	22.81	37307	39100	4.81	34	12	-64.92	47632	47300	-0.70
14301	93779	87600	-6.59	269	300	11.65	35234	36600	3.88	34	15	-56.15	31265	31300	0.11
14323	100924	93600	-7.26	269	280	4.21	35878	37500	4.52	34	3	-91.23	38749	38700	-0.13
14332	104681	96200	-8.10	179	210	17.23	33376	33900	1.57	34	3	-91.23	36301	35500	-2.21
14345	103305	97300	-5.81	179	190	6.07	24585	25500	3.72	34	11	-67.85	22242	22100	-0.64
14348	105475	94300	-10.59	179	150	-16.26	22084	21500	-2.64	34	11	-67.85	35811	34700	-3.10
14797	96213	86900	-9.68	179	150	-16.26	36592	37800	3.30	34	6	-82.46	43365	42700	-1.53
14808	82242	81300	-1.15	179	170	-5.10	47456	48700	2.62	34	6	-82.46	38049	37600	-1.18
14816	90551	82900	-8.45	179	140	-21.85	32590	33300	2.18	34	5	-85.38	42386	41300	-2.56
14828	90498	89200	-1.43	717	710	-0.91	40738	43400	6.54	34	4	-88.31	40218	41200	2.44
14844	93197	91800	-1.50	358	300	-16.26	27158	28200	3.84	34	39	14.00	51758	51800	0.08
14680	92826	90500	-2.51	269	300	11.65	39594	41400	4.56	68	5	-92.69	44134	41400	-6.20
14871	98225	96200	-2.06	90	120	33.98	33019	34000	2.97	34	10	-70.77	45813	46100	0.63
14887	93144	96900	4.03	358	340	-5.10	47956	51800	8.02	34	20	-41.54	51129	53100	3.86
14689	83353	83800	0.54	90	120	33.98	19368	21800	12.56	34	10	-70.77	13709	14800	7.96
14695	95155	97000	1.94	179	170	-5.10	35592	39800	11.82	34	6	-82.46	36301	39900	9.92
14742	97801	90600	-7.36	179	120	-33.01	27444	27800	1.30	34	24	-29.85	33573	33500	-0.22
14666	92350	92100	-0.27	358	330	-7.89	37164	39300	5.75	34	21	-38.62	51618	53900	4.42
14685	87534	85900	-1.87	448	380	-15.15	32090	33100	3.15	34	5	-85.38	62390	63900	2.42
14685B	87746	83100	-5.29	358	310	-13.47	29731	29500	-0.78	34	7	-79.54	66097	59700	-9.68
14545	98330	94700	-3.69	896	860	-3.98	37021	38200	3.18	34	16	-53.23	41826	41700	-0.30
14565	91186	88300	-3.16	179	220	22.81	43239	45800	5.92	34	11	-67.85	36720	37200	1.31
14571	87217	82200	-5.75	448	430	-3.98	25086	25900	3.25	34	7	-79.54	27908	26900	-3.61
14578	88804	86800	-2.26	627	640	2.08	39808	42000	5.51	34	9	-73.69	39938	41600	4.16
14578B	86793	82400	-5.06	806	760	-5.72	41095	43200	5.12	34	10	-70.77	41616	39200	-5.81
14598	101506	92500	-8.87	179	220	22.81	32304	33500	3.70	34	3	-91.23	45463	46600	2.50
14893	92033	92000	-0.04	448	490	9.42	39808	41600	4.50	34	44	28.62	53087	53400	0.59
14899	96531	97000	0.49	358	330	-7.89	34091	35400	3.84	34	43	25.69	56934	56900	-0.06
14908	92985	95800	3.03	717	690	-3.70	35663	37900	6.27	34	39	14.00	52388	53200	1.55
14917	88646	85300	-3.77	806	740	-8.20	22727	23200	2.08	34	16	-53.23	23991	24200	0.87
14925	92509	87800	-5.09	358	390	8.86	34520	36000	4.29	34	30	-12.31	45953	46200	0.54
14998	94414	90100	-4.57	269	280	4.21	37879	39800	5.07	34	6	-82.46	43365	43600	0.54
15862	92350	87200	-5.58	269	290	7.93	40452	42200	4.32	34	4	-88.31	42106	41600	-1.20
15870	80866	81000	0.17	1075	1030	-4.17	43596	46400	6.43	34	27	-21.08	38329	39200	2.27
15879	90180	90600	0.47	806	760	-5.72	45597	48300	5.93	34	29	-15.23	51548	51500	-0.09
15887	94414	87200	-7.64	448	440	-1.75	40166	41200	2.57	34	25	-26.92	37840	34600	-8.56
15891	93303	89500	-4.08	1343	1250	-6.96	48313	51300	6.18	34	22	-35.69	37979	38500	1.37
15908	91980	87100	-5.31	269	260	-3.24	43525	45200	3.85	34	24	-29.85	34412	34500	0.25

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Whole Rock Al * (ppm)	ICP Al (ppm)	Difference (%) [3]	Whole Rock Ba * (ppm)	ICP Ba (ppm)	Difference (%) [3]	Whole Rock Ca * (ppm)	ICP Ca (ppm)	Difference (%) [3]	Whole Rock Cr * (ppm)	ICP Cr (ppm)	Difference (%) [3]	Whole Rock Fe * (ppm)	ICP Fe (ppm)	Difference (%) [3]
15911	92033	88600	-3.73	448	410	-8.45	34877	35200	0.93	34	33	-3.54	47422	46500	-1.94
Maximum			5.69			34			12.6			43.2			9.92
Minimum			-10.6			-33			-2.64			-92.7			-9.68
Mean			-3.63			-1.63			3.76			-49.3			-0.32
Standard Deviation			3.81			13			2.74			35			3.33
10 Percentile			-8.4			-16.3			0.85			-88.3			-3.62
25 Percentile			-6.15			-8.04			2.27			-81			-2.05
Median			-4.08			-4.17			3.72			-53.2			-0.17
75 Percentile			-1.08			5.14			5.1			-28.4			1.22
90 Percentile			0.82			12.8			6.3			-2.08			2.88
Interquartile Range (IQR) [1]			5.07			13.2			2.82			52.6			3.27
Variance			14.5			169			7.52			1223			11.1
Skewness			0.41			0.66			0.57			0.76			0.066
Coefficient of Variation (CoV) [2]			-1.05			-7.96			0.73			-0.71			-10.3
Count			59			59			59			59			59

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

[3] Difference (%) = (ICP - Whole Rock) * 100 / Whole Rock

* Element calculated from Whole Rock XRF analysis

Al (Whole Rock) = $(Al_2O_3*2*10000*26.98)/(2*26.98+3*16)$
Ba (Whole Rock) = $(BaO*10000*137.34)/(137.34+16)$
Ca (Whole Rock) = $(CaO*10000*40.08)/(40.08+16)$
Cr (Whole Rock) = $(Cr_2O_3*2*10000*52.00)/(2*52.00+3*16)$
Fe (Whole Rock) = $(Fe_2O_3*2*10000*55.85)/(2*55.85+3*16)$

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Whole Rock K * (ppm)	ICP K (ppm)	Difference (%) ³	Whole Rock Mg * (ppm)	ICP Mg (ppm)	Difference (%) ³	Whole Rock Mn * (ppm)	ICP Mn (ppm)	Difference (%) ³	Whole Rock Na * (ppm)	ICP Na (ppm)	Difference (%) ³	Whole Rock P * (ppm)	ICP P (ppm)	Difference (%) ³
14018	24239	24500	1.08	10494	10700	1.97	387	476	22.92	29748	31600	6.22	611	660	8.03
14021	21500	22200	3.26	8865	9200	3.78	542	629	16.03	21959	23800	8.38	524	570	8.85
14036	20836	21300	2.23	9106	9100	-0.07	387	475	22.67	23220	24700	6.37	524	570	8.85
14043	9795	10300	5.15	18454	19000	2.96	387	446	15.18	30638	32900	7.38	524	570	8.85
14060	11788	12000	1.80	19781	21000	6.16	387	422	8.98	27523	30500	10.82	1135	1290	13.70
14067	10708	11200	4.59	24545	26800	9.19	697	779	11.76	30787	35100	14.01	960	1120	16.66
14076	13116	14300	9.03	22434	25000	11.44	1471	1585	7.72	19585	23000	17.44	916	1070	16.76
14083	28971	30900	6.66	17007	17700	4.08	1317	1365	3.68	12018	13600	13.16	916	1070	16.76
14099	32706	32000	-2.16	8865	8200	-7.50	1084	1090	0.53	5416	5400	-0.29	480	470	-2.09
14103	17183	18100	5.33	12303	12900	4.85	620	686	10.72	22181	25100	13.16	567	620	9.29
14130	17515	18100	3.34	9710	10200	5.05	155	191	23.31	34199	38300	11.99	1222	1390	13.76
14144	15274	15600	2.13	10916	11600	6.27	387	451	16.47	30045	34900	16.16	1571	1830	16.49
14148	20670	20600	-0.34	18876	18900	0.13	387	429	10.79	12760	13800	8.15	1135	1220	7.53
14156	11705	12200	4.23	7297	7900	8.26	232	339	45.91	33606	37400	11.29	436	500	14.58
14162	14859	16000	7.68	23942	26200	9.43	774	853	10.14	16840	19300	14.61	873	980	12.29
14169	8882	9700	9.21	3679	4000	8.73	232	278	19.65	42731	47600	11.40	524	550	5.03
14232	16685	16800	0.69	8926	9100	1.95	155	189	22.02	39392	42800	8.65	1309	1430	9.23
14250	13863	14600	5.32	17308	18800	8.62	387	436	12.59	33235	38300	15.24	1222	1450	18.67
14260	15772	15900	0.81	13328	13900	4.29	232	275	18.36	35386	38600	9.08	1222	1390	13.76
14276	7139	7600	6.46	15439	16400	6.23	1084	1085	0.07	36870	40800	10.66	1266	1440	13.79
14295	15191	16000	5.33	14655	15500	5.77	387	436	12.59	29674	33600	13.23	1178	1360	15.43
14301	19425	19200	-1.16	12062	12400	2.81	465	517	11.26	24704	27300	10.51	1222	1380	12.94
14323	17432	18200	4.40	9348	9600	2.70	310	386	24.60	30935	35000	13.14	1222	1410	15.40
14332	20421	20200	-1.08	10313	10400	0.85	232	281	20.94	29897	32400	8.37	1309	1470	12.29
14345	22662	24000	5.90	9890	10300	4.14	77	150	93.68	33161	36900	11.28	1222	1380	12.94
14348	18678	18700	0.12	11881	12100	1.85	155	191	23.31	35535	38200	7.50	1353	1520	12.36
14797	18927	19500	3.03	14836	15200	2.46	465	559	20.30	23888	26700	11.77	1178	1330	12.88
14808	20670	20800	0.63	15801	16300	3.16	465	493	6.10	18546	20000	7.84	1004	1080	7.60
14816	20753	20900	0.71	16766	17000	1.40	387	438	13.11	24110	26700	10.74	1135	1230	8.41
14828	16104	17500	8.67	16464	18200	10.54	465	507	9.11	28265	32900	16.40	1091	1280	17.33
14844	16436	16900	2.82	35823	37900	5.80	232	319	37.30	21662	24600	13.56	1135	1290	13.70
14680	15025	16000	6.49	15077	16500	9.44	465	493	6.10	30045	34600	15.16	1135	1300	14.58
14871	11290	12300	8.95	17308	19200	10.93	310	374	20.73	38280	44300	15.73	1047	1230	17.44
14887	10293	11700	13.67	21771	24700	13.45	542	613	13.07	30045	35400	17.82	1004	1200	19.56
14689	15855	16400	3.44	5488	5600	2.04	232	301	29.55	32196	34300	6.53	480	540	12.50
14695	21334	22100	3.59	14534	15100	3.89	542	611	12.71	26484	30000	13.28	1135	1400	23.39
14742	12369	12800	3.49	20444	22400	9.57	310	401	29.45	38651	43600	12.81	1091	1220	11.83
14666	12701	12900	1.57	21650	22000	1.61	465	543	16.86	32864	35800	8.93	1091	1250	14.58
14685	12203	12100	-0.84	27199	27300	0.37	310	364	17.50	29897	32000	7.04	1353	1530	13.10
14685B	12784	13200	3.26	26354	28400	7.76	310	327	5.56	29526	33900	14.82	1309	1530	16.87
14545	11373	11800	3.76	13087	14000	6.98	232	273	17.50	31158	35000	12.33	1178	1330	12.88
14565	17764	18600	4.70	11398	12100	6.16	465	529	13.84	26484	29900	12.90	1135	1270	11.93
14571	14610	14200	-2.81	12242	11700	-4.43	155	230	48.49	32048	32200	0.47	960	1030	7.29
14578	15689	15800	0.71	12001	11800	-1.68	310	337	8.79	29674	31500	6.15	1353	1550	14.58
14578B	15274	15800	3.44	11881	12700	6.90	310	345	11.37	29006	32900	13.42	1309	1470	12.29
14598	12784	12400	-3.00	22857	22100	-3.31	542	631	16.39	29303	31400	7.16	1353	1540	13.84
14893	9214	10200	10.70	24545	27200	10.82	465	493	6.10	31380	36600	16.63	1091	1260	15.50
14899	7471	7700	3.07	37994	41300	8.70	465	546	17.50	29229	34100	16.67	1091	1260	15.50
14908	12535	13700	9.30	21470	24000	11.79	465	527	13.41	37760	44700	18.38	1135	1310	15.46
14917	15440	16100	4.27	16524	18300	10.75	310	379	22.34	41692	47300	13.45	960	1100	14.58
14925	14942	15400	3.07	18756	20400	8.77	387	408	5.36	30861	35600	15.36	1091	1230	12.75
14998	11539	12500	8.33	14896	16300	9.43	387	452	16.73	35683	41400	16.02	1222	1440	17.85
15862	14361	14800	3.06	16524	17400	5.30	542	584	7.73	30564	34400	12.55	1135	1260	11.05
15870	17349	18500	6.63	16162	17700	9.51	465	539	16.00	22775	26200	15.04	1004	1120	11.59
15879	14029	14900	6.21	17127	18800	9.77	465	554	19.22	28265	32900	16.40	1091	1280	17.33
15887	11622	11900	2.40	14836	15900	7.17	310	395	27.51	34422	39300	14.17	960	1090	13.54
15891	16519	17200	4.12	16042	17300	7.84	465	558	20.08	30564	34900	14.19	1004	1120	11.59
15908	17349	18000	3.75	17248	18500	7.26	387	433	11.82	25520	29000	13.64	1004	1130	12.59

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Whole Rock K * (ppm)	ICP K (ppm)	Difference (%) [3]	Whole Rock Mg * (ppm)	ICP Mg (ppm)	Difference (%) [3]	Whole Rock Mn * (ppm)	ICP Mn (ppm)	Difference (%) [3]	Whole Rock Na * (ppm)	ICP Na (ppm)	Difference (%) [3]	Whole Rock P * (ppm)	ICP P (ppm)	Difference (%) [3]
15911	13448	13800	2.62	21349	23100	8.20	387	402	3.81	28858	32500	12.62	1091	1250	14.58
Maximum			13.7			13.5			93.7			18.4			23.4
Minimum			-3			-7.5			0.07			-0.29			-2.09
Mean			3.79			5.46			17.4			11.8			13.1
Standard Deviation			3.41			4.3			13.8			3.98			3.94
10 Percentile			-0.44			0.32			5.99			6.94			8.33
25 Percentile			1.69			2.58			10.4			8.79			11.7
Median			3.44			6.16			16			12.8			13.5
75 Percentile			5.62			8.75			20.8			14.7			15.4
90 Percentile			8.72			10.6			27.9			16.4			17.3
Interquartile Range (IQR) [1]			3.93			6.17			10.4			5.92			3.73
Variance			11.6			18.5			192			15.8			15.6
Skewness			0.37			-0.65			3.24			-0.85			-0.86
Coefficient of Variation (CoV) [2]			0.9			0.79			0.8			0.34			0.3
Count			59			59			59			59			59

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

[3] Difference (%) = (ICP - Whole Rock) * 100 / Whole Rock

* Element calculated from Whole Rock XRF analysis

$K_{\text{(Whole Rock)}} = (K_2O*2*10000*39.09)/(39.09*2+16)$

$Mg_{\text{(Whole Rock)}} = (MgO*10000*24.31)/(24.31+16)$

$Mn_{\text{(Whole Rock)}} = (MnO*10000*54.94)/(54.94+16)$

$Na_{\text{(Whole Rock)}} = (Na_2O*2*10000*22.99)/(22.99*2+16)$

$P_{\text{(Whole Rock)}} = (P_2O5*2*10000*30.97)/(2*30.97+5*16)$

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Whole Rock Si * (ppm)	ICP Si (ppm)	Difference (%) [3]	Whole Rock Sr * (ppm)	ICP Sr (ppm)	Difference (%) [3]	Leco S (Total)** (ppm)	ICP S (ppm)	Difference (%) [3]	Whole Rock Ti * (ppm)	ICP Ti (ppm)	Difference (%) [3]
14018	294129			423	428	1.23	8000	8800	10.00	2518	2400	-4.68
14021	303993			169	173	2.30	6200	7000	12.90	2158	2080	-3.62
14036	303338			254	235	-7.36	14700	16000	8.84	2278	1970	-13.52
14043	302637			254	276	8.80	2600	2800	7.69	2458	2190	-10.90
14060	271971			423	423	0.05	13100	14800	12.98	4376	4100	-6.31
14067	269681			338	410	21.22	4000	4300	7.50	4196	4170	-0.63
14076	259724			338	365	7.91	7700	9500	23.38	4316	4540	5.18
14083	249346			169	232	37.18	14600	16000	9.59	4436	4480	0.99
14099	297822			85	88	4.07	3400	3600	5.88	1858	1670	-10.14
14103	287725			169	198	16.78	6900	7700	11.59	2458	2220	-9.68
14130	281180			254	288	13.53	2900	3200	10.34	3177	2800	-11.88
14144	251496			338	343	1.41	2600	2800	7.69	3777	3760	-0.45
14148	243082			254	223	-12.09	1400	1400	0.00	3837	3780	-1.48
14156	303666			254	259	2.10	1700	1700	0.00	1739	1900	9.29
14162	234714			169	239	41.32	1300	1500	15.38	4137	4270	3.23
14169	312781			169	207	22.40	3000	3200	6.67	1858	1960	5.46
14232	264352			338	345	2.00	1500	1600	6.67	3657	3290	-10.03
14250	242661			338	424	25.36	1900	2000	5.26	4496	4350	-3.25
14260	255330			338	402	18.85	3400	3700	8.82	4316	4050	-6.17
14276	252759			676	798	17.97	1700	1700	0.00	4017	4100	2.08
14295	250234			254	336	32.45	4400	4900	11.36	4376	4240	-3.12
14301	256452			169	209	23.58	3400	3500	2.94	4196	3620	-13.74
14323	255470			338	391	15.60	1500	1500	0.00	3357	3310	-1.41
14332	253179			338	355	4.96	2600	2700	3.85	3597	3260	-9.37
14345	268793			254	274	8.01	5200	5600	7.69	3477	2970	-14.58
14348	256966			254	276	8.80	4400	4800	9.09	3657	3190	-12.77
14797	241867			254	234	-7.76	800	700	-12.50	4196	4150	-1.11
14808	245980			169	221	30.68	1800	1900	5.56	3357	3260	-2.90
14816	249346			254	285	12.35	4600	4700	2.17	3897	3810	-2.23
14828	242474			338	404	19.44	1300	1400	7.69	3777	3940	4.32
14844	246775			254	265	4.46	2100	2200	4.76	5575	5590	0.26
14680	249346			338	348	2.89	2200	2200	0.00	4017	4040	0.58
14871	250234			338	405	19.74	3700	3800	2.70	4916	4990	1.51
14887	236351			338	424	25.36	4400	5400	22.73	4736	4960	4.73
14689	309696			169	141	-16.63	6800	7900	16.18	1978	1580	-20.14
14695	249533			169	226	33.63	1400	1600	14.29	4077	4310	5.73
14742	256498			254	302	19.05	1900	2100	10.53	5156	4690	-9.03
14666	248738			338	416	22.99	3200	3800	18.75	5036	5070	0.68
14685	233125			338	393	16.19	17900	21000	17.32	8273	7690	-7.05
14685B	235603			338	374	10.57	19500	20400	4.62	8273	7930	-4.15
14545	262996			338	409	20.92	1900	1900	0.00	3897	3980	2.14
14565	251730			254	259	2.10	2300	2600	13.04	3777	3800	0.61
14571	280246			338	312	-7.76	10400	11100	6.73	3537	3170	-10.38
14578	252478			254	324	27.72	18200	21300	17.03	5156	4630	-10.20
14578B	254628			254	330	30.09	19300	21100	9.33	4916	4430	-9.88
14598	247476			507	569	12.15	1300	1500	15.38	4436	4330	-2.40
14893	235696			338	379	12.05	1100	1100	0.00	5995	6030	0.58
14899	228824			338	366	8.21	200	200	0.00	5815	5850	0.60
14908	247383			423	479	13.29	800	900	12.50	5815	5910	1.63
14917	278656			254	309	21.81	1900	1900	0.00	4796	4580	-4.50
14925	253647			338	353	4.37	1400	1500	7.14	5276	5090	-3.52
14998	251309			338	412	21.81	1300	1300	0.00	4316	4460	3.33
15862	247149			254	327	28.90	800	800	0.00	4077	4050	-0.65
15870	254348			254	234	-7.76	1300	1400	7.69	4436	4460	0.53
15879	237098			338	373	10.28	1200	1200	0.00	5395	5450	1.01
15887	254441			338	402	18.85	3100	3300	6.45	5156	5100	-1.08
15891	240184			338	382	12.94	1400	1400	0.00	5156	4920	-4.57
15908	250001			254	288	13.53	2200	2200	0.00	4856	4740	-2.39

Project:	**Schaft Creek**
Client:	Copper Fox Metals Inc.
Data:	**QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments:	Sampled by MDAG on Feb 7'07. For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Whole Rock Si * (ppm)	ICP Si (ppm)	Difference (%) [3]	Whole Rock Sr * (ppm)	ICP Sr (ppm)	Difference (%) [3]	Leco S (Total)** (ppm)	ICP S (ppm)	Difference (%) [3]	Whole Rock Ti * (ppm)	ICP Ti (ppm)	Difference (%) [3]
15911	246822			338	335	-0.96	900	900	0.00	5455	5430	-0.47
Maximum			NA			41.3			23.4			9.29
Minimum			NA			-16.6			-12.5			-20.1
Mean			NA			12.8			7.05			-3.22
Standard Deviation			NA			12.6			6.66			6.05
10 Percentile			NA			-2.24			0			-11.1
25 Percentile			NA			3.48			0			-8.04
Median			NA			12.9			7.14			-2.23
75 Percentile			NA			21.5			10.9			0.65
90 Percentile			NA			29.1			15.5			3.53
Interquartile Range (IQR) [1]			NA			18			10.9			8.69
Variance			NA			159			44.4			36.6
Skewness			NA			-0.061			0.13			-0.52
Coefficient of Variation (CoV) [2]			NA			0.99			0.94			-1.88
Count			0			59			59			59

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

[3] Difference (%) = (ICP - Whole Rock) * 100 / Whole Rock

* Element calculated from Whole Rock XRF analysis

Si (Whole Rock) = (SiO_2*10000*28.09)/(28.09+2*16)

Sr (Whole Rock) = (SrO*10000*87.62)/(87.62+16)

Ti (Whole Rock) = (TiO_2*10000*47.9)/(47.9+2*16)

**S (Total) = S (Leco %) * 10000

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Sulphur and NP Species**
Comments: Sampled by MDAG on Feb 7'07.

Sample Id.	Carbonate Leach S (Sulphate) (%)	HCl Leachable S (Sulphate) (%)	RPD (%)	S (Sulphide) (% Leco)	%S(Sulphide) Calculated from Carbonate Leach S (Sulphate) (%)	RPD (%)	S (Sulphide) (% Leco)	%S(Sulphide) Calculated from HCl Leachable S (Sulphate) (%)	RPD (%)	(% Leco/Calc)/ S (Sulphide)/ S (Total)*100 (%)	Carbonate Leach S (Sulphate)/ S (Total)*100 (%)	HCl Leachable S (Sulphate)/ S (Total)*100 (%)	S(BaSO4)/ S (Total)*100 (%)
14018	0.02	0.005	120.00	0.69	0.78	12.24	0.69	0.795	14.14	86.25	2.50	0.63	3.40
14021	0.03	0.005	142.86	0.6	0.59	1.68	0.6	0.615	2.47	96.77	4.84	0.81	1.69
14036	0.02	0.005	120.00	1.39	1.45	4.23	1.39	1.465	5.25	94.56	1.36	0.34	0.85
14043	0.02	0.005	120.00	0.22	0.24	8.70	0.22	0.255	14.74	84.62	7.69	1.92	2.41
14060	0.74	0.71	4.14	0.62	0.57	8.40	0.62	0.6	3.28	47.33	56.49	54.20	0.64
14067	0.01	0.005	66.67	0.41	0.39	5.00	0.41	0.395	3.73	102.50	2.50	1.25	2.09
14076	0.01	0.005	66.67	0.76	0.76	0.00	0.76	0.765	0.66	98.70	1.30	0.65	1.36
14083	0.03	0.005	142.86	1.35	1.43	5.76	1.35	1.455	7.49	92.47	2.05	0.34	1.15
14099	0.03	0.005	142.86	0.28	0.31	10.17	0.28	0.335	17.89	82.35	8.82	1.47	6.15
14103	0.45	0.42	6.90	0.25	0.24	4.08	0.25	0.27	7.69	36.23	65.22	60.87	0.91
14130	0.03	0.005	142.86	0.29	0.26	10.91	0.29	0.285	1.74	100.00	10.34	1.72	4.33
14144	0.02	0.005	120.00	0.2	0.24	18.18	0.2	0.255	24.18	76.92	7.69	1.92	3.22
14148	0.02	0.005	120.00	0.04	0.12	100.00	0.04	0.135	108.57	28.57	14.29	3.57	10.45
14156	0.04	0.005	155.56	0.14	0.13	7.41	0.14	0.165	16.39	82.35	23.53	2.94	3.69
14162	0.02	0.005	120.00	0.12	0.11	8.70	0.12	0.125	4.08	92.31	15.38	3.85	9.65
14169	0.01	0.005	66.67	0.29	0.29	0.00	0.29	0.295	1.71	96.67	3.33	1.67	0.70
14232	0.005	0.005	0.00	0.14	0.145	3.51	0.14	0.145	3.51	93.33	3.33	3.33	2.79
14250	0.01	0.005	66.67	0.19	0.18	5.41	0.19	0.185	2.67	100.00	5.26	2.63	2.20
14260	0.01	0.005	66.67	0.34	0.33	2.99	0.34	0.335	1.48	100.00	2.94	1.47	1.23
14276	0.01	0.005	66.67	0.14	0.16	13.33	0.14	0.165	16.39	82.35	5.88	2.94	14.76
14295	0.005	0.005	0.00	0.41	0.435	5.92	0.41	0.435	5.92	93.18	1.14	1.14	0.48
14301	0.01	0.005	66.67	0.32	0.33	3.08	0.32	0.335	4.58	94.12	2.94	1.47	1.84
14323	0.005	0.005	0.00	0.13	0.145	10.91	0.13	0.145	10.91	86.67	3.33	3.33	4.18
14332	0.01	0.005	66.67	0.26	0.25	3.92	0.26	0.255	1.94	100.00	3.85	1.92	1.61
14345	0.005	0.005	0.00	0.52	0.515	0.97	0.52	0.515	0.97	100.00	0.96	0.96	0.80
14348	0.01	0.005	66.67	0.45	0.43	4.55	0.45	0.435	3.39	102.27	2.27	1.14	0.95
14797	0.005	0.005	0.00	0.05	0.075	40.00	0.05	0.075	40.00	62.50	6.25	6.25	5.23
14808	0.005	0.005	0.00	0.16	0.175	8.96	0.16	0.175	8.96	88.89	2.78	2.78	2.32
14816	0.005	0.01	66.67	0.46	0.455	1.09	0.46	0.45	2.20	100.00	1.09	2.17	0.91
14828	0.02	0.005	120.00	0.1	0.11	9.52	0.1	0.125	22.22	76.92	15.38	3.85	12.87
14844	0.005	0.01	66.67	0.2	0.205	2.47	0.2	0.2	0.00	95.24	2.38	4.76	3.98
14680	0.01	0.005	66.67	0.2	0.21	4.88	0.2	0.215	7.23	90.91	4.55	2.27	2.85
14871	0.02	0.005	120.00	0.32	0.35	8.96	0.32	0.365	13.14	86.49	5.41	1.35	0.57
14887	0.01	0.03	100.00	0.42	0.43	2.35	0.42	0.41	2.41	95.45	2.27	6.82	1.90
14689	0.01	0.005	66.67	0.69	0.67	2.94	0.69	0.675	2.20	101.47	1.47	0.74	0.31
14695	0.005	0.005	0.00	0.13	0.135	3.77	0.13	0.135	3.77	92.86	3.57	3.57	2.99
14742	0.005	0.005	0.00	0.19	0.185	2.67	0.19	0.185	2.67	100.00	2.63	2.63	2.20
14666	0.01	0.005	66.67	0.31	0.31	0.00	0.31	0.315	1.60	96.88	3.13	1.56	2.61
14685	0.01	0.005	66.67	1.8	1.78	1.12	1.8	1.785	0.84	100.56	0.56	0.28	0.58
14685B	0.01	0.005	66.67	1.8	1.94	7.49	1.8	1.945	7.74	92.31	0.51	0.26	0.43
14545	0.01	0.005	66.67	0.13	0.18	32.26	0.13	0.185	34.92	68.42	5.26	2.63	11.00
14565	0.005	0.005	0.00	0.24	0.225	6.45	0.24	0.225	6.45	104.35	2.17	2.17	1.82
14571	0.02	0.005	120.00	1.03	1.02	0.98	1.03	1.035	0.48	99.04	1.92	0.48	1.01
14578	0.02	0.005	120.00	1.82	1.8	1.10	1.82	1.815	0.28	100.00	1.10	0.27	0.80
14578B	0.03	0.005	142.86	1.91	1.9	0.52	1.91	1.925	0.78	98.96	1.55	0.26	0.97
14598	0.01	0.005	66.67	0.13	0.12	8.00	0.13	0.125	3.92	100.00	7.69	3.85	3.22
14893	0.005	0.04	155.56	0.08	0.105	27.03	0.08	0.07	13.33	72.73	4.55	36.36	9.50
14899	0.005	0.005	0.00	0.02	0.015	28.57	0.02	0.015	28.57	100.00	25.00	25.00	41.82
14908	0.005	0.005	0.00	0.07	0.075	6.90	0.07	0.075	6.90	87.50	6.25	6.25	20.91
14917	0.005	0.005	0.00	0.16	0.185	14.49	0.16	0.185	14.49	84.21	2.63	2.63	9.90
14925	0.005	0.005	0.00	0.12	0.135	11.76	0.12	0.135	11.76	85.71	3.57	3.57	5.97
14998	0.005	0.005	0.00	0.12	0.125	4.08	0.12	0.125	4.08	92.31	3.85	3.85	4.82
15862	0.005	0.005	0.00	0.03	0.075	85.71	0.03	0.075	85.71	37.50	6.25	6.25	7.84
15870	0.02	0.005	120.00	0.09	0.11	20.00	0.09	0.125	32.56	69.23	15.38	3.85	19.30
15879	0.02	0.005	120.00	0.09	0.1	10.53	0.09	0.115	24.39	75.00	16.67	4.17	15.68
15887	0.01	0.005	66.67	0.29	0.3	3.39	0.29	0.305	5.04	93.55	3.23	1.61	3.37
15891	0.02	0.005	120.00	0.09	0.12	28.57	0.09	0.135	40.00	64.29	14.29	3.57	22.40
15908	0.02	0.005	120.00	0.2	0.2	0.00	0.2	0.215	7.23	90.91	9.09	2.27	2.85

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Sulphur and NP Species**
Comments: Sampled by MDAG on Feb 7'07.

Sample Id.	Carbonate Leach S (Sulphate) (%)	HCl Leachable S (Sulphate) (%)	RPD (%)	S (Sulphide) (% Leco)	%S(Sulphide) Calculated from Carbonate Leach S (Sulphate) (%)	RPD (%)	S (Sulphide) (% Leco)	%S(Sulphide) Calculated from HCl Leachable S (Sulphate) (%)	RPD (%)	(% Leco/Calc)/ S (Sulphide)/ S (Total)*100 (%)	Carbonate Leach S (Sulphate)/ S (Total)*100 (%)	HCl Leachable S (Sulphate)/ S (Total)*100 (%)	S(BaSO4)/ S (Total)*100 (%)
15911	0.01	0.005	66.67	0.07	0.08	13.33	0.07	0.085	19.35	77.78	11.11	5.56	11.62
Maximum			156			100			109	104.00	65.20	60.90	41.80
Minimum			0			0			1.4E-14	28.60	0.51	0.26	0.31
Mean			70.3			11.2			12.6	87	7.67	5.29	5.39
Standard Deviation			52.4			17.7			19	16.9	11.5	11.3	7.2
10 Percentile			0			0.97			0.94	67.6	1.27	0.45	0.69
25 Percentile			2.07			2.96			2.44	82.4	2.33	1.3	1.08
Median			66.7			5.92			5.92	92.5	3.57	2.27	2.79
75 Percentile			120			10.9			14.6	99.5	7.69	3.85	6.06
90 Percentile			143			27.3			29.4	100	15.4	6.25	13.2
Interquartile Range (IQR) [1]			118			7.95			12.2	17.2	5.37	2.55	4.99
Variance			2743			312			362	287	131	128	51.9
Skewness			-0.11			3.71			3.4	-1.87	3.72	3.99	2.89
Coefficient of Variation (CoV) [2]			0.74			1.58			1.51	0.19	1.49	2.14	1.34
Count			59			59			59	59	59	59	59

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Sulphur and NP Species**
Comments: Sampled by MDAG on Feb 7'07.

Sample Id.	Ratio NP / Inorganic CaNP	Ratio NP / (Ca) CaNP	Ratio NP / (Ca+Mg) CaNP	Ratio Inorganic CaNP / (Ca) CaNP	Ratio Inorganic CaNP / (Ca+Mg) CaNP
14018	1.32	0.94	0.47	0.72	0.36
14021	1.08	0.98	0.62	0.90	0.57
14036	1.20	1.07	0.59	0.89	0.49
14043	2.20	1.14	0.35	0.52	0.16
14060	1.80	0.52	0.25	0.29	0.14
14067	1.66	0.76	0.28	0.46	0.17
14076	1.12	0.61	0.31	0.55	0.28
14083	1.08	0.74	0.43	0.68	0.39
14099	1.01	1.06	0.73	1.05	0.72
14103	1.17	1.16	0.67	0.99	0.58
14130	0.91	1.39	0.85	1.53	0.93
14144	1.02	1.24	0.82	1.21	0.80
14148	1.07	1.47	0.88	1.38	0.82
14156	1.00	1.18	0.77	1.18	0.77
14162	1.15	1.57	0.88	1.37	0.77
14169	1.13	1.10	0.86	0.98	0.76
14232	1.22	1.34	0.86	1.10	0.70
14250	1.27	1.16	0.66	0.92	0.52
14260	1.19	1.32	0.75	1.11	0.63
14276	2.30	0.44	0.27	0.19	0.12
14295	1.39	1.14	0.69	0.82	0.49
14301	1.05	1.49	0.95	1.42	0.91
14323	1.04	0.78	0.55	0.75	0.53
14332	1.55	1.12	0.75	0.73	0.48
14345	2.17	1.24	0.74	0.57	0.34
14348	1.18	1.10	0.57	0.93	0.48
14797	1.08	1.32	0.80	1.23	0.74
14808	0.93	1.41	0.91	1.51	0.98
14816	5.85	1.60	0.87	0.27	0.15
14828	1.01	1.32	0.78	1.30	0.77
14844	1.94	1.06	0.33	0.55	0.17
14680	1.18	0.99	0.60	0.84	0.50
14871	1.43	1.04	0.54	0.72	0.37
14887	1.22	0.92	0.52	0.76	0.42
14689	0.97	0.97	0.68	1.00	0.70
14695	1.04	1.15	0.71	1.10	0.68
14742	1.27	1.21	0.52	0.95	0.41
14666	1.53	0.96	0.50	0.63	0.33
14685	1.49	1.35	0.57	0.91	0.38
14685B	1.45	1.38	0.54	0.96	0.37
14545	1.54	0.81	0.50	0.52	0.33
14565	1.27	1.19	0.83	0.93	0.65
14571	1.19	1.18	0.67	0.98	0.56
14578	1.06	1.06	0.72	1.00	0.68
14578B	1.07	1.13	0.76	1.05	0.71
14598	1.61	0.92	0.44	0.57	0.27
14893	1.28	1.07	0.51	0.83	0.40
14899	1.48	0.92	0.31	0.62	0.21
14908	1.57	0.79	0.39	0.50	0.25
14917	1.45	1.14	0.50	0.79	0.34
14925	1.34	0.91	0.47	0.68	0.35
14998	1.19	1.04	0.62	0.87	0.52
15862	1.17	1.23	0.73	1.06	0.63
15870	1.05	1.30	0.80	1.24	0.76
15879	1.08	0.98	0.60	0.91	0.55
15887	1.27	0.92	0.56	0.73	0.45
15891	1.10	1.00	0.64	0.91	0.58
15908	1.21	1.07	0.64	0.89	0.53

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Sulphur and NP Species**
Comments: Sampled by MDAG on Feb 7'07.

Sample Id.	Ratio NP / Inorganic CaNP	Ratio NP / (Ca) CaNP	Ratio NP / (Ca+Mg) CaNP	Ratio Inorganic CaNP / (Ca) CaNP	Ratio Inorganic CaNP / (Ca+Mg) CaNP
15911	1.35	1.05	0.50	0.78	0.37
Maximum	5.85	1.60	0.95	1.53	0.98
Minimum	0.91	0.44	0.25	0.19	0.12
Mean	1.37	1.09	0.62	0.88	0.51
Standard Deviation	0.67	0.24	0.18	0.3	0.22
10 Percentile	1.02	0.79	0.35	0.52	0.2
25 Percentile	1.08	0.97	0.5	0.7	0.36
Median	1.2	1.1	0.62	0.9	0.5
75 Percentile	1.45	1.24	0.76	1.05	0.69
90 Percentile	1.69	1.39	0.86	1.25	0.77
Interquartile Range (IQR)[1]	0.37	0.27	0.25	0.35	0.33
Variance	0.45	0.056	0.033	0.088	0.047
Skewness	5.47	-0.33	-0.24	0.039	0.089
Coefficient of Variation (CoV)[2]	0.49	0.22	0.29	0.34	0.43
Count	59	59	59	59	59

Schaft Creek Project -

Prediction of Metal Leaching and Acid Rock Drainage, Phase 2

prepared for:

Rescan Environmental Services Ltd.
Attn: Mr. Soren Jensen
Sixth Floor,
1111 West Hastings Street.
Vancouver, British Columbia V6E 2J3

prepared by:

Kevin A. Morin, Ph.D., P.Geo., L.Hydrogeo.
Nora M. Hutt, A.Sc.T, c.C.T.
Minesite Drainage Assessment Group
A Division of Morwijk Enterprises Ltd.
8035 Redtail Court,
Surrey, British Columbia V3W 0N4

February 21, 2008

P.Geo. and A.Sc.T. Notice

This study is based on detailed technical information interpreted through standard and advanced chemical and geoscientific techniques available at this time. As with all geoscientific investigations, the findings are based on data collected at discrete points in time and location. In portions of this report, it has been necessary to infer information between and beyond the measured data points using established techniques and scientific judgement. In our opinion, this report contains the appropriate level of geoscientific information to reach the conclusions stated herein.

This study has been conducted in accordance with British Columbia provincial legislation as stated in the Engineers and Geoscientists Act and in the Applied Science Technologists and Technicians Act.

Kevin A. Morin, Ph.D., P.Geo.
Registration No. 18,721
Association of Professional
Engineers and Geoscientists

Nora M. Hutt, A.Sc.T., c.C.T.
Registration No. 10700
Association of Applied Science
Technologists and Technicians

TABLE OF CONTENTS

List of Tables

List of Figures

Report Summary

Metal leaching (ML) and acid rock drainage (ARD) are often water-chemistry issues for many minesites. As a result, the accurate prediction and control of ML-ARD at minesites in British Columbia are high priorities of the provincial government. This is explained in British Columbia's formal Policy, Guidelines, and draft Prediction Manual.

This report contains the second phase of ML-ARD studies for the Schaft Creek Project in British Columbia. It follows the recommendations in the provincial ML-ARD Policy, Guidelines, and draft Prediction Manual.

Relevant Observations from Existing Information

A compilation of existing information relevant to ML-ARD produced the following important observations. First, the Schaft Creek copper-gold-molybdenum deposit is widely acknowledged as a porphyry copper deposit, containing three mineral zones: Main (or Liard), West Breccia, and Paramount Zones. Second, visual examinations of exposed core up to several decades old showed limited weathering, suggesting the oxidation rate of Schaft Creek rock may be relatively slow. Third, 16 acid-base accounts from a previous, metallurgical study showed all 16 samples were net acid neutralizing, with sulphide between 0.1 and 0.9%S, and Neutralization Potentials from 53 to 114 kg/t. Fourth, detailed mineralogy of 18 thin sections of selected rock units showed that the fine-grained groundmass was generally around one-half of the total, with the groundmass consisting of more than 90% feldspar, and accessory amounts of quartz, chlorite, sericite, carbonate, opaques. Sulphide minerals were mostly disseminated and as veinlets and clusters, and were mostly pyrite and chalcopyrite with less common molybdenite and bornite. Carbonate minerals, mostly reported as veins, patches, and groundmass, were not individually identified, and were sometimes seen as feldspar replacement/alteration.

Phase 2 Samples and Analyses

This Phase 2 ML-ARD study incorporated and integrated the samples and findings of the Phase 1 study. In total, 232 samples of rock from core were collected and analyzed, generally reflecting the abundances of the rock units. Also, three samples of tailings, with one each from the three ore zones, were collected and analyzed, for a total of 235 samples. All samples were analyzed for U.S. EPA-600-compliant Sobek expanded acid-base accounting (ABA) and total-element contents based on ICP-MS after four-acid digestion and on x-ray-fluorescence whole rock. Selected samples were analyzed for mineralogy by Rietveld x-ray diffraction and for bulk reaction rates by kinetic humidity cells.

Results of Acid-Base Accounting (ABA)

As part of the ABA procedure, paste pH, measured in a mixture of deionized water and pulverized sample, showed no samples were acidic at the time of analysis. Paste pH ranged from 7.4 to 9.2.

Total sulphur in the 235 Schaft Creek samples of rock and tailings ranged from 0.01 (detection limit) to 13.5%S, with a mean of 0.50%S and a median of 0.22%S. Although maximum total-sulphur values varied due to localized higher-sulphur rock in the three ore zones, the mean and minimum values were similar for all three. Statistically, sulphide represented 85% of total sulphur on average, with a median of 87%. Thus, the two parameters were typically interchangeable, but not identical. Approximately 5-10% of the samples had sulphur-species analyses within the relatively unreliable range below roughly 0.05%S. The MOE-recommended approach of using total sulphur and the associated Total-Sulphur-Based Acid Potential (TAP) was used here. This recognizes that TAP tends to overestimate sulphide acid potential, often by a small amount, and may be changed in Phase 3 studies based on additional work.

Sobek (EPA 600) Neutralization Potential (NP) ranged from 21 to 219 kg/t in the 235 Schaft Creek samples of rock and tailings, with a mean of 79 and a median of 75 kg/t. These relatively high values explained why no acidic paste pH values were detected. They also suggested there could be a long lag time (years to decades) before any sample might become acidic. Nearly all the measured total carbon was inorganic carbonate, which can neutralize acidity depending on the form of the carbonate. Correlations of inorganic carbonate with Sobek NP showed several trends, such as Sobek NP levels typically being significantly higher than inorganic carbonate implying non-carbonate minerals contributed to neutralization. Thus, Sobek NP was considered the better measure of neutralizing capacity than Inorganic CaNP. The lack of correlations with solid-phase calcium and calcium+magnesium meant that the form of the inorganic carbonate could not be inferred. Nevertheless, the minor correlation of Sobek NP and calcium probably reflected a calcium-bearing combination of carbonate and non-carbonate minerals.

Net balances of acid-generating and acid-neutralizing capacities for the 235 Phase 2 samples of rock and tailings were based on (1) total sulphur and the resulting Total Acid Potential (TAP) and (2) Sobek Neutralization Potential after Unavailable NP estimated at 10 kg/t was subtracted. This was called, “Adjusted TNPR”. These net balances for the samples showed that approximately 90% was net neutralizing indefinitely, 4% was net acid generating although not yet acidic, and 6% was uncertain until further testing. A sensitivity analysis showed these percentages did not change significantly when (1) total sulphur was replaced by sulphide plus unaccounted-for sulphur or (2) all measured NP was considered fully reactive and available (Unavailable NP = 0). By ore zone, the Main (Liard) Zone had the highest percentage of net-neutralizing samples (96%), and the West Breccia Zone the lowest (81%). The correlation of Adjusted TNPR with total sulphur showed that samples: with more than 2.1%S were consistently net acid generating, with less than 0.5%S were consistently net neutralizing, and between 0.5 and 2.1%S could fall into any ML-ARD category depending on NP.

Results of Total-Element Contents

The dominant solid-phase elements in the 235 Phase 2 samples were mostly silicon and aluminum, reflecting the dominance of aluminosilicate minerals in Schaft Creek rock. Compared with average crustal abundances, the samples were frequently elevated in silver, bismuth, copper, molybdenum, selenium, and tungsten; and occasionally to rarely elevated in cadmium, lead, sulphur, antimony, and zinc. These elevated levels do not automatically mean these elements will leach into water at high concentrations, but may instead indicate a general lack of leaching.

Minimum-to-maximum ranges of solid-phase elements were similar among the ore zones. However, some samples from the West Breccia Zone contained notably more antimony, lead, cadmium, and zinc.

The elements showing some correlation with sulphide, suggesting they were at least partly occurring in/as sulphide minerals, were copper, selenium, cobalt, and iron. Calcium showed some correlation with Sobek Neutralization Potential, reflecting the neutralizing, calcium-bearing, carbonate and non-carbonate minerals in Schaft Creek rock.

Additional Analyses of Tailings

Metallurgical testing of ore from the three ore zones at the Schaft Creek Project has produced one solid-phase tailings sample and supernatant (water) analyses for each ore zone, namely Main (Liard), West Breccia, and Paramount.

Overall, the supernatants were near-neutral calcium-sodium-potassium-sulphate waters. Alkalinity was relatively low, indicating relative low pH-buffering capacity, but greater than acidity. These supernatants represent the best available prediction of mill-effluent water chemistry that will enter the Schaft Creek tailings impoundment. If this effluent is the dominant inflow, then the tailings-pond chemistry can be predicted from the supernatant chemistry. If other inflows are significant, like background runoff or drainage from exposed tailings beaches, then the tailings-pond chemistry may not resemble the supernatant chemistry. Large-scale modelling for the environmental assessment will address this later.

Based on acid-base accounting (ABA), the paste pH of the tailings solids from all three zones was near neutral between 8.1 and 8.4. Total sulphur was relatively low, ranging from 0.08 to 0.20%S. Compared with the rock samples from the three ore zones, the three tailings samples contained relatively low sulphur and relatively high Sobek Neutralization Potential. Thus, like most of the rock samples, all three tailings samples were net neutralizing.

Based on total-element analyses, the three tailings samples were composed mostly of silicon and aluminum, reflecting the dominance of aluminosilicate minerals. Compared with average crustal abundances, the three tailings samples were consistently elevated in silver, bismuth, copper, and selenium. Additionally, West Breccia tailings were elevated in antimony and tungsten, and Paramount tailings were also elevated in tungsten. Removal of copper resulted in residual copper below the rock-core mean and median copper for the Main and Paramount tailings.

Quantitative mineralogy of the three tailings samples was determined by Rietveld x-ray diffraction. As expected, aluminosilicate minerals were dominant in these Schaft Creek tailings, with 43-50 weight-% plagioclase, 17-24 wt-% quartz, 12-17 wt-% muscovite, and 9-11 wt-%

clinochlore. The most abundant carbonate mineral was calcite, with dolomite second in abundance. No significant amounts of less-neutralizing, iron-bearing forms of carbonate were identified. Pyrite was the only identified sulphide mineral, and this was only seen in the West Breccia tailings sample because of the otherwise generally low sulphide levels.

To date, only 13 weeks of humidity-cell weekly humidity-cell analyses are available. These analyses showed the three tailings cells have remained near neutral to date, with the Main tailings showing the greatest variability to date. All three samples are expected to remain near neutral indefinitely based on their ABA. Sulphate production rate typically represents the rate of sulphide oxidation and total-acidity generation. The temporal trends in sulphate rates from the three cells showed two tailings cells (West Breccia and Paramount) have been generally steady around a definable range in recent weeks. In contrast, the sulphate rate in the Main tailings dropped to notably low levels, almost two orders of magnitude lower than the other two tailings cells, but then recovered on the last available week. Often months of testing are required to identify long-term geochemical stability, so these initial results should not be used as long-term predictions.

In humidity cells, the rate of sulphide oxidation can affect some rates of dissolution and leaching. At this early stage, the tailings rates showing some correlation with sulphate production included alkalinity (and thus Neutralization-Potential (NP) dissolution), antimony, barium, calcium, copper, magnesium, manganese, potassium, silicon, and strontium. Some of these elements, like copper, probably relate directly to sulphide oxidation, whereas others like calcium and potassium probably relate to NP dissolution driven by sulphide oxidation. However, at this early stage of testing, detailed interpretations are not yet warranted.

Recommendations

Based on the findings above and on the British Columbia ML-ARD documents, the following recommendations are offered.

First, the specific carbonate and sulphide minerals in Schaft Creek rock should be better identified. This has already been done on samples of Schaft Creek tailings, which showed carbonate was mostly calcite and dolomite, and sulphide was pyrite.

Second, three-dimensional modelling, possibly including geologic, alteration, and/or assay data, should be undertaken by Copper Fox Metals Inc. This should model total sulphur and available NP separately, then locally combine the two to calculate Adjusted TNPR. In this way, the spatial distribution of ARD categories, the year-by-year production of net-acid-generating and net-neutralizing rock, and the potential to segregate ARD rock during routine mining can be assessed. This may require additional ABA analyses, at the discretion of the modeller.

Third, laboratory-based humidity cells should be initiated on various types and ARD categories of Schaft Creek rock. These will provide bulk reaction rates under standardized conditions, to allow scaling of rates to full-scale conditions. Such cells have already been started for Schaft Creek tailings.

Fourth, on-site leach tests should be started after spring thaw in 2008. These tests, with hundreds of kilograms, will provide data for full-scale equilibrium conditions.

1. INTRODUCTION

Metal leaching (ML) and acid rock drainage (ARD) are often water-chemistry issues for many minesites (e.g., Morin and Hutt, 1997 and 2001). As a result, the accurate prediction and control of ML-ARD at minesites in British Columbia are high priorities of the provincial government. This is explained in British Columbia's formal Policy, Guidelines, and draft Prediction Manual (Price and Errington, 1998; Price, 1998; Price et al., 1997).

ARD results from oxidation of sulphide minerals, particularly iron-bearing sulphides like pyrite. Whether sulphide minerals are present or not, weathering can still lead to accelerated metal leaching (ML). For example, the simple dissolution of carbonate minerals can release metals like manganese.

Because the provincial documents recommend a phased approach, this report compiles and interprets the currently existing information related to ML-ARD at the Schaft Creek Project. This includes the earlier Phase 1 ML-ARD findings (Morin and Hutt, 2007a). General background information is provided in Chapter 2. The ML-ARD samples, and the analyses applied to them, are described in Chapter 3. The analytical results are discussed in Chapter 4 for rock and in Chapter 5 for tailings. All relevant data are compiled in the appendices.

2. GENERAL INFORMATION AND PREVIOUS ML-ARD-RELATED STUDIES

The information presented below has been extracted mostly from the Project Description (Copper Fox Metals Ltd., 2006), a resource estimate by Giroux and Ostensoe (2003), and the drilling reports for 2005 (Fischer and Hanych, 2006) and 2006 (Ewanchuk et al., 2007).

2.1 Location and History

The Schaft Creek property is located in the mountainous terrain of northwestern British Columbia, approximately 1,000 km northwest of Vancouver. The area is located 80 kilometers southwest of Telegraph Creek and approximately 76 kilometers west of the Stewart-Cassiar paved highway (Highway 37). The mineral claims of interest are situated near the headwaters of Schaft Creek, a tributary of Mess Creek, which flows into the Stikine River downstream of the community of Telegraph Creek.

Schaft Creek is located in the coastal climate zone of British Columbia and is characterized by cool summers and cold humid winters. Elevations on the property range from 500 to 2,000 m above sea level. Average annual precipitation is estimated to be 640 mm or roughly 84% greater than that recorded at Telegraph Creek. Temperatures are strongly influenced by the Coast Mountains and may range from above +20°C in the summer to below -20°C in winter.

The Schaft Creek copper-gold-molybdenum-silver prospect was identified in 1957 by prospector Nick Bird while employed by the BIK Syndicate. Three diamond drill holes were drilled to moderate depths. Sample results from two of the holes returned sufficient copper values and resulted in further work. The prospecting syndicate was re-organized in 1966 into Liard Copper Mines Ltd. ("Liard") with Silver Standard Mines Limited, holding a 66% interest, acting as the manager. In 1966 ASARCO obtained an option to explore the Liard Copper Mines Ltd. ground and carried out geological and induced polarization surveys. The program included drilling 10,939 feet (3,335 metres) over 24 holes. The option was not maintained despite encouraging drill results and in 1968 Hecla Mining Company of Canada Ltd., a subsidiary of Hecla Mining Company of Wallace, Idaho, entered an option agreement to earn a 75% property interest and commenced drilling and other exploration work with Hecla operating company as its agent.

From 1968 through 1977, Hecla completed a total of 34,500 metres of diamond drilling, 6,500 metres of percussion drilling, induced polarization and resistivity surveys, geological mapping, air photography, and engineering studies related to the development of a large open pit copper-gold-molybdenum mine. In 1978 Wright Engineers Ltd. was contracted by Hecla to update a preliminary feasibility assessment initially completed in 1970. Exploration work at the property ceased in 1977 and in 1978 Hecla sold its interest to Teck Corporation ("Teck") (now Teck Cominco Limited).

In 1980 Teck commenced a program of exploration and drilling designed to confirm and expand Hecla's work. A total of 26,000 metres of diamond drilling was completed by 1981. Teck then undertook an engineering study to determine the feasibility of mine development. Further data reviews were completed by Western Copper Holdings in 1988 and Teck in 1993. A total of 230 core holes with a total length of 60,200 metres and percussion holes with total length 6,500 metres have been completed at the Schaft Creek property.

In 2005, Copper Fox Metals completed 15 large diameter (PQWL) drill holes across the Main Liard and West Breccia zones for a total of 3,161 meters. A total of 50,000 pounds of core was undergoing geological assessment and reporting before metallurgical testing.

The 2006 diamond drill campaign ended with the completion of 42-holes, totaling 9,007-meters of drilling. Of this total, 5,300-meters included 25-PQ holes and 3,707-meters included 17-HQ holes. During the period from July 12th to October 23rd, a total of 2,107 samples were submitted for assaying, and 896 samples were collected for the metallurgical composite sample. The total of the metallurgical samples collected represented a combined weight of 44,800 pounds.

2.2 Geology

The Schaft Creek copper-gold-molybdenum property is located in the northern part of the Intermontane Belt of the Canadian Cordillera. It is part of the northwesterly trending suite of porphyry-style mineral deposits that extends in Canada from the Copper Mountain/Ingerbelle deposit near the southern International Boundary to Casino in west-central Yukon. Globally, such deposits typically exhibit a few characteristics in common and many variations.

The Schaft Creek copper-gold-molybdenum deposit is hosted principally by Upper Triassic age volcaniclastic rocks. They have been variously altered and disrupted by emplacement of feldspar porphyry dykes and, possibly, sills and by several northwest-trending faults. Augite porphyry basalt is present in proximity to the west of the deposit area and also in the Liard mineral zone but its relationship to mineralization has not been determined. The mineralized area is, arguably, in fault contact, or disconformably or unconformably overlain by unmineralized, comparatively unaltered and undisturbed purple weathering andesitic volcanic rocks. Geological mapping at surface, aided by diamond drill core information, has failed to reveal any strong overall pattern of stratigraphic or petrologic controls to mineralization.

The Schaft Creek copper-gold-molybdenum deposit is widely acknowledged as being a porphyry copper deposit. The deposit consists of three distinct but connected zones: (a) the Liard (Main) zone hosted mainly by andesite flows and epiclastic rocks; (b) the West Breccia zone, a fault-bounded tourmaline-sulphide matrix breccia; and (c) the Paramount zone, an intrusive breccia in altered andesite, granodiorite and quartz monzonite.

> The broad, northerly plunging Liard, or Main, zone extends 1,000 metres in a northerly direction, 700 metres east-west, and has average thickness of 300 metres. It is a weakly altered stockwork system in volcanics (andesite flows and fragmentals) with minor felsic intrusive dykes carrying disseminated sulphide mineralization. A pyrite halo surrounds chalcopyrite, bornite and molybdenite mineralization in altered and faulted andesite. The zone has a low grade phyllic core and to the northwest is progressively down dropped on

faults.

The West Breccia zone exhibits tourmaline, silicification and sericitization and is controlled by north-trending faults. Mineralization is contained within tourmaline and sulphide rich hydrothermal breccia. The Zone has a length of 500 metres, averages 100 metres in width and has been drilled to depths greater than 300 metres. Pyrite is the principal sulphide mineral, with lesser quantities of chalcopyrite and molybdenite. Copper and molybdenum contents are erratic but often high.

The Paramount zone of intrusive breccia occurs in granodiorite and quartz monzonite and has dimensions of 700 metres length, 200 metres width and +500 metres thickness. Exploration to the north has been constrained by practical considerations: rapidly increasing thicknesses of overlying apparently barren purple volcanic rocks challenge drilling methods and mitigate against practical conceptual open pit designs. The mineralization is contained in an intrusive breccia in altered andesite, granodiorite and quartz monzonite. Pyrite, bornite and chalcopyrite are present in equal proportions and molybdenite values exceed those found in the other two zones.

Additional information comes from the provincial Minfile website (http://minfile.gov.bc.ca/Summary.aspx?minfilno=104G++015):

“Mineralization occurs partly within a basin-like structure of fragmental and undivided green andesites, 900 metres in diameter. The basin is intruded by augite porphyry basalt and by vertical north striking quartz diorite dykes. A breccia cuts the western edge of the basin and trends north for at least 2700 metres. Post-mineralization mafic dykes are common. Later flat-lying fragmental purple andesites unconformably overlie the northeastern part of the deposit.

“In general, pyrite, chalcopyrite, bornite and molybdenite occur predominantly in fractured andesites. Less than 10 per cent of the mineralization occurs in felsic intrusives. Pyrite and bornite are mutually exclusive and most of the main deposit occurs within the bornite zone, with pyrite on the periphery. A barren zone, which contains no sulphides, conformably underlies the main deposit.

“Feldspathization and hydrothermal alteration are associated with mineralization. A quartz vein stockwork with biotite and some potassium feldspar coincides with the low-grade core of the main deposit. The biotite has a potassium/argon age of 182 Ma +/- 5 Ma. Epidote appears abruptly near the boundaries of the main deposit. Most mineralization occurs in an intermediate zone marked by chlorite-sericite alteration and the absence of epidote. Tourmaline and gypsum are locally abundant.

“The distribution of most sulphide minerals is fracture-controlled. They occur in dry fractures or combined with quartz or quartz-calcite veinlets within the andesitic volcanics. The sulphides within the felsic intrusives are usually disseminated and seem to have replaced the mafic minerals. Trace amounts of covellite, chalcocite, tetrahedrite and native copper

> have been identified. Minor amounts of galena and sphalerite occur in the breccia zone and in small calcite veins. Gold and silver are associated with the sulphides and average 0.34 grams per tonne and 1.71 grams per tonne, respectively."

2.3 Past ML-ARD-Related Work

During an examination of existing core, Associated Mining Consultants Ltd. (2004) observed, "It has been noted that the core from previous drilling programs, which is stored on site, exhibits a remarkable degree of preservation with limited visible weathering."

Also, after a visual assessment of the integrity of the core samples, Associated Mining Consultants Ltd. (2004) selected 16 samples for assay validation based on prior documentation of assays, lithology, and spatial distributions. These 16 samples selected were subjected to standard Acid-Base accounting procedures to assess any acid generation and environmental impact concerns (Table 2-1). Because only statistical summaries but no individual analyses were presented, these analyses were not added to the Phase 1 database in this study (Appendix A).

Table 2-1. Statistical Results of Previous Acid-Base Accounting for Sixteen Samples (from Associated Mining Consultants Ltd., 2004)

Parameter	Average	Range
Sulphide (%S)	0.43	0.1-0.9
Paste pH	8.8	7.5-9.3
Acid Potential (kg $CaCO_3$ eq/tonne)	13.4	3.4-28.6
Neutralization Potential (kg $CaCO_3$ eq/tonne)	75.5	53-114
Net Potential Ratio (NPR or NP/AP)	7.36	3.0-16.9
Net Neutralization Potential (NP-AP, kg $CaCO_3$ eq/tonne)	+62.2	+45 to +91

Then, five samples were selected from the suite of 16 for metallurgical validation using standard batch grinding and rougher flotation procedures for sulphides. The five samples selected for metallurgical validation were taken from drill holes H61, T182, T186, T172, and T176.

Based on all this work, Associated Mining Consultants Ltd. (2004) concluded,

> "The mineralogy is unlikely to pose acid generation concerns based on the analysis of the 16 selected core samples. Acid-Base accounting results indicated an excess neutralization potential of over twice the estimated acid potential in all cases and the paste pH ranged from neutral to alkaline. With the low head sulphide content in the samples to start and high flotation recoveries, the total sulphur in the tailings was reduced to below 0.03% to further reduce concerns on environmental impact."

As an addendum to Fischer and Hanych (2006), mineralogy was visually determined, using thin-section petrography, on 18 samples. This work focussed on feldspar quartz porphyry (rock code PPFQ, Table 3-1), with a few samples from tourmaline breccia, pneumatolytic breccia and volcanics. It was not meant to be representative of the Schaft Creek lithologic suite. Major observations from this work follow.

> “- Not all samples logged as PPFQ are intrusives. Some are porphyritic volcanics of felsic and intermediate composition (dacitic - andesitic); one sample is a fine grained, feldspathic intrusive rock classified as either syenite or anorthosite, depending on the composition of feldspar.
> - All rocks classified as FQP [PPFQ] are porphyritic, felsic, massive igneous rocks.
> - All have plagioclase as the predominant phenocryst mineral. Quartz phenocrysts ('quartz eyes') are relatively rare, very subordinate to plagioclase phenocrysts.
> - A few samples have no quartz phenocrysts (quartz eyes) and therefore are feldspar porphyry.
> - Ferromagnesian ('Femag') phenocrysts are consistently completely replaced by secondary minerals, generally chlorite and accessory leucoxene, opaques, in places by sericite and skeletal fine grained opaques and highly refracting brown minerals.
> - The groundmass makes up a variable portion of the rock, generally ½.
> - The groundmass consists of >90% feldspar, and accessory amounts of quartz, chlorite, sericite, carbonate, opaques.
> - The groundmass in all cases is fine grained to very fine grained, generally 100 to 200 microns (0.1 - 0.2 mm) grain size, in some samples extremely fine grained (20 - 50 microns). Differences in grain size of the groundmass feldspar is noticeable and attributed to varying cooling rates.
> - The shape of groundmass feldspar and other minerals is generally anhedral, interlocking. Lathy and feathery feldspar are rare but were observed.
> - Only accessory amounts of fresh potassic feldspar (microcline) and albite were observed in some feldspar-quartz-porphyries and are interpreted as very limited, secondary, potassic alteration.
> - The common pink to orange colour of the samples is attributed to ubiquitous micron-size sericite grains within plagioclase phenocrysts and to a lesser degree in groundmass feldspar. It is pointed out that 'sericite' is a synonym for fine grained muscovite which is a potassic phyllosilicate. It appears justified to describe this partial alteration as 'potassic'.
> - Fast cooling of the liquid that formed the groundmass is interpreted for all Liard Zone FQP samples. This is in contrast to the grains size of the interstitial minerals in the Hickman /Yeheniko samples which are medium grained (0.3 - 1 mm)
> - This fast cooling of the inter-phenocryst liquid can be interpreted either as due to relatively small intrusive bodies or surface-near (subvolcanic) bodies.
> - Alteration is weak to moderate. Mostly sericite, minor carbonate, chlorite, rare potassic, i.e., microcline.
> - Sulphides in feldspar-quartz-porphyry and volcanics occur both in veins; and as disseminations, associated with hairline fractures and grain boundaries, and with minor quartz, carbonate, chlorite and sericite.

Other observations from the individual thin sections include:

- Undifferentiated plagioclase was typically the major mineral, with fine-grained sericite and quartz often significant.
- Sulphide minerals were mostly disseminated and as veinlets and clusters, and mostly pyrite and chalcopyrite with less common molybdenite and bornite
- Pyrite was typically 0.05-1.0 mm in size as subhedral to anhedral grains, but variable among samples.
- Carbonate minerals, mostly reported as veins, patches, and groundmass, were not individually identified and were sometimes seen as feldspar replacement/alteration.

2.4 Important ML-ARD Observations from Previous Studies

Based on the preceding subsections, important observations pertaining to ML-ARD were:

- The Schaft Creek copper-gold-molybdenum deposit is widely acknowledged as being a porphyry copper deposit. It contains three mineral zones: the Liard, West Breccia, and Paramount Zones.

- During an examination of existing core, “It has been noted that the core from previous drilling programs, which is stored on site, exhibits a remarkable degree of preservation with limited visible weathering.” Thus, the oxidation rate of Schaft Creek rock may be relatively slow.

- Based on 16 acid-base accounts from a previous, metallurgical study, all 16 samples were net acid neutralizing, with sulphide between 0.1 and 0.9%S, and Neutralization Potentials from 53 to 114 kg/t. Flotation recovery of sulphide reduced the sulphide levels in the synthetic tailings.

- Detailed mineralogy was examined in 18 thin sections, representing feldspar quartz porphyry (rock code PPFQ), tourmaline breccia, pneumatolytic breccia, and volcanics. Even one rock unit (PPFQ) was not entirely intrusive. Some PPFQ samples were porphyritic volcanics of felsic and intermediate composition (dacitic - andesitic), and one sample was a fine grained, feldspathic intrusive rock classified as either syenite or anorthosite, depending on the composition of feldspar. Groundmass in these samples was generally around one-half of the total, with the groundmass consisting of more than 90% feldspar, and accessory amounts of quartz, chlorite, sericite, carbonate, opaques. Sulphide minerals were mostly disseminated and as veinlets and clusters, and mostly pyrite and chalcopyrite with less common molybdenite and bornite. Carbonate minerals, mostly reported as veins, patches, and groundmass, were not individually identified, and were sometimes seen as feldspar replacement/alteration.

3. SAMPLING AND ANALYSIS

3.1 Sample Selection and Collection

The authors of this report were asked by Copper Fox Metals Inc. to review the drilling reports and drill logs from the 2005 drilling program (Fischer and Hanych, 2006) and 2006 program (Ewanchuk et al., 2007). Based on these, we were instructed to select samples for ML-ARD analyses.

We set the objectives for sampling as follows:

- To collect samples of discrete rock units, generally reflecting the abundance of the rock units in the holes (Tables 3-1 and 3-2). This recognizes that many assay samples were based strictly on 3.05 m sections which crossed rock units in some places.

- To collect samples from three-dimensional distributions in all three zones: Main (Liard), West Breccia, and Paramount. The Paramount Zone was not drilled in 2005, so the 2006 samples were the first analyzed for ML-ARD potential from Paramount. This will contribute to the three-dimensional geostatistical modelling by Copper Fox Metals, which will determine if additional ML-ARD samples are needed for reliable estimates across the three zones.

- To collect samples with a range of assay levels, to ensure waste, low-grade ore, and ore were assessed for their ML-ARD characteristics.

- To collect a few samples that were purposely biased with elevated levels of visual sulphides, to ensure higher-sulphide rock at Schaft Creek was analyzed for its ML-ARD characteristics.

This resulted in 59 samples for the Phase 1 ML-ARD work (Morin and Hutt, 2007) and another subsequent 173 samples, which are all combined as 232 samples and re-interpreted here as one database (Appendix A). Table 3-2 shows that the abundances of many rock units were approximated, recognizing that numerical round-off precluded exact matches for some. Also, overburden represented up to 4% of core meterage, but was not sampled here because it is being assessed separately. This also precludes exact matches of percentages.

More important, drill-core meterage (Table 3-1) is only an approximation, so that some rock units with apparent zero abundance in some ore zones actually have samples analyzed in this ML-ARD study. For example, Rock Unit TOBR has generally zero abundance in all three ore zones (Table 3-1), despite being a recognized rock unit at Schaft Creek and having three samples of TOBR from the West Breccia Zone (Table 3-2). Therefore, exact matches were not attempted or achieved. Three-dimensional modelling by Copper Fox Metals will be used to decide if additional samples from an ore zone, a rock unit, or a lateral or vertical zone are needed.

Table 3-1. Rock Units and Abundances by Ore Zone at the Schaft Creek Deposit, Based on Drillhole Meterage
(abundances as percentages, from charts in Ewanchuk et al., 2007)

		Abundance, as Percentage of Drillhole Meterage			
Code	Name	Main-Liard	West Breccia	Paramount	Total
ANLP	Andesite, lapilli	20	9	5	16
ANAP	Augite-plagioclase phyric andesite	20	11	-	15
ANPF	Andesite, plagioclase-phyric	10	27	4	12
ANBX	Andesitic breccia	10	2	-	8
ANTF	Andesite, tuff	7	3	2	6
ANDS	Andesite, fine grained	6	19	2	7
FAUL/SHER	Fault/Shear	4	6	9	5
GRDR	Granodiorite	-	-	42	5
PPPL	Feldspar porphyry	5	1	6	5
OVER	Overburden[1]	3	4	4	4
ANAU	Augite-phyric andesite	3	2	-	3
BRVL	Volcanic breccia	4	-	3	3
D/BS	Diabase/mafic dyke	1	2	10	3
ANXX	Alteration zone	2	1	-	2
HVBX	Hydrothermal Breccia	1	5	4	2
OTHR	Other	2	3	-	2
PPFQ	Feldspar-quartz porphyry	2	3	-	2
BRIG	Breccia, intrusive	-	2	9	1
BRIV	Volcanic intrusive breccia	-	-	-	-
BRXX	Undifferentiated breccia	-	-	-	-
DIOR	Diorite	-	-	-	-
PNBX	Pneumatolytic breccia	-	-	-	-

		Abundance, as Percentage of Drillhole Meterage			
Code	Name	Main-Liard	West Breccia	Paramount	Total
TOBR	Tourmaline breccia	-	-	-	-
VEIN	Vein	-	-	-	-

[1] Overburden can contain up to 0.6% copper (Ewanchuk et al., 2007); overburden is not included in this ML-ARD study but is being assessed separately.

Table 3-2. ML-ARD Samples by Ore Zone and Rock Unit at the Schaft Creek Deposit (number of samples and as percentages of total, based on Appendix A)

		Samples are listed as: # of samples and then (% of total for ore zone / % of total from core meterage in Table 3-1)			
Code	Name	Main-Liard	West Breccia	Paramount	Total
ANLP	Andesite, lapilli	21 (14/20)	1 (2/9)	2 (6/5)	24 (10/16)
ANAP/ PPAU	Augite-plagioclase phyric andesite	29 (20/20)	0 (0/11)	0 (0/0)	29 (13/15)
ANPF	Andesite, plagioclase-phyric	26 (18/10)	13 (28/27)	0 (0/4)	39 (17/12)
ANBX	Andesitic breccia	8 (5/10)	1 (2/2)	0 (0/0)	9 (4/8)
ANTF	Andesite, tuff	13 (9/7)	3 (6/3)	1 (3/2)	17 (7/6)
ANDS	Andesite, fine grained	6 (4/6)	12 (26/19)	3 (10/2)	21 (9/7)
FAUL/ SHER	Fault/Shear	7 (5/4)	1 (2/6)	2 (6/9)	10 (4/5)
GRDR	Granodiorite	0 (0/0)	0 (0/0)	10 (32/42)	10 (4/5)
PPPL	Feldspar porphyry	2 (1/5)	0 (0/1)	0 (0/6)	2 (1/5)
OVER	Overburden[1]	0 (0/3)	0 (0/4)	0 (0/4)	0 (0/4)
ANAU	Augite-phyric andesite	6 (2/3)	1 (2/2)	0 (0/0)	7 (3/3)
BRVL	Volcanic breccia	5 (3/4)	0 (0/0)	0 (0/3)	5 (2/3)
D/BS	Diabase/mafic dyke	4 (3/1)	2 (4/2)	4 (13/10)	10 (4/3)

		Samples are listed as: # of samples and then (% of total for ore zone / % of total from core meterage in Table 3-1)			
Code	Name	Main-Liard	West Breccia	Paramount	Total
ANXX	Alteration zone	5 (3/2)	1 (2/1)	0 (0/0)	6 (3/2)
HVBX	Hydrothermal Breccia	2 (1/1)	2 (4/5)	4 (13/4)	8 (3/2)
OTHR	Other	1 (1/2)	0 (0/4)	2 (6/0)	11 (5/2)
PPFQ	Feldspar-quartz porphyry	11 (7/2)	3 (6/3)	3 (10/0)	17 (7/2)
BRIG	Breccia, intrusive	0 (0/0)	0 (0/2)	0 (0/9)	0 (0/1)
BRIV	Volcanic intrusive breccia	0 (0/0)	1 (2/0)	0 (0/0)	1 (1/0)
BRXX	Undifferentiated breccia	0 (0/0)	2 (4/0)	0 (0/0)	2 (1/0)
DIOR	Diorite	2 (1/0)	0 (0/0)	0 (0/0)	2 (1/0)
PNBX	Pneumatolytic breccia	0 (0/0)	0 (0/0)	0 (0/0)	0 (0/0)
TOBR	Tourmaline breccia	0 (0/0)	3 (6/0)	0 (0/0)	3 (1/0)
VEIN	Vein	0 (0/0)	0 (0/0)	0 (0/0)	0 (0/0)
TOTAL		**148**	**47**	**31**	**232**[2]

[1] Overburden can contain up to 0.6% copper (Ewanchuk et al., 2007); overburden is not included in this ML-ARD study but is being assessed separately.

[2] The total of 232 samples does not include three tailings samples, which produced a final total of 235 samples in Appendix A. The total of 232 does include 8 "Other" samples of biased high-sulphide core.

The original Phase 1 samples, from 2005 drilling, were collected from sealed plastic buckets containing coarsely ground core ("coarse rejects") that had been in unheated storage in Smithers. Each sample was collected with a fiberglass hand shovel, cleaned with soap and water between samples, and placed into a labelled ziploc bag. All samples were relatively dry, except three saturated and one moist.

The eight biased high-sulphide samples were collected by the authors at the Schaft Creek site from the long-term core-storage racks. The selection of these samples was based on visual inspection of thousands of meters of core, and identification of the few intervals from "T"-series core with elevated visual sulphide. The T series was drilled by Teck Corp in 1980-1981. The T-series holes, from which the eight biased high-sulphide samples were taken, are located in the Main, West Breccia, and Paramount ore zones.

The remaining 165 samples, from 2006 drilling, were collected by Rescan from storage. Details of this sampling will be provided by Rescan.

In addition to the 232 rock samples, three samples of tailings were collected and submitted by Rescan, one from each of the three ore zones (Appendix A). Details of the metallurgical testwork and sampling will be provided by Rescan.

3.2 Sample Analysis

Based on the provincial ML-ARD Prediction Manual (Chapter 1), the Phase 2 samples (Section 3.1) were subjected to several geochemical "static" (one-time) analyses as well as repetitive "kinetic" tests.

The 232 rock samples and three tailings samples (Section 3.1) were sent to ALS Chemex Labs in North Vancouver for static testing using:

1) Chemex Package ABA-PKG05A plus C-IR07, which is standard-Sobek (U.S. EPA 600 compliant; Sobek et al., 1978) expanded acid-base accounting (ABA), providing measured and/or calculated values of:
    - paste pH in a mixture of pulverized rock and water,
    - total sulphur,
    - measured sulphide,
    - leachable sulphate (both HCl and carbonate leach techniques),
    - calculated sulphide by subtracting sulphate from total sulphur,
    - barium-bound sulphate calculated from barium analyses,
    - calculation of acid potentials based on sulphide levels plus any unaccounted-for sulphur (Sulphide Acid Potential, SAP),
    - Sobek (U.S. EPA 600 compliant) neutralization potential (NP) by acid bath and base titration,
    - inorganic carbonate for mathematical conversion to Carbonate NP (Inorg CaNP),
    - total carbon for mathematical conversion to Carbonate-equivalent NP (Total CaNP),
    - excess carbon calculated from the difference between total carbon and inorganic carbon,

- CaNP calculated from calcium (Ca CaNP),
- CaNP calculated from Ca + Mg (Ca+Mg CaNP),
- various Net Neutralization Potential (NNP) balances of acid neutralizing capacities minus various acid generating capacities, and
- various Net Potential Ratio (NPR) balances of acid neutralizing capacities divided by various acid generating capacities.

2) total-element contents by:

- Chemex Package ME-MS61m: 49-element analysis after strong four-acid digestion, and
- Chemex Package ME-XRF-06: XRF (x-ray-fluorescence) whole rock for 14 elements and parameters.

ABA and total-element analyses for rock are compiled in Appendix A and are discussed in Chapter 4. Results for tailings are discussed in Chapter 5.

For laboratory-based repetitive kinetic testing, the "flood-leach", fine-grained, well-flushed, well-aerated humidity cell was used. This technique can be traced back to at least 1962, and is different from a leach column or trickle-leach cell which provide different geochemical information.

Samples were placed in well-flushed, well-aerated humidity cells at ALS Environmental in Vancouver. During a typical weekly cycle, approximately 0.5 L of deionized water was added to each cell, allowed to soak on and through the sample over a few hours after brief, gentle sample agitation, and then analyzed. Then three days of relatively dry air was pumped through/over the samples to de-saturate them, followed by three days of relatively moist air. Comparisons of water added and water recovered typically showed samples retained water each week and were thus not saturated during the weekly cycles. Leach waters from every cell cycle were analyzed so that maximum concentrations would not be missed. These aqueous analyses included pH, acidity, alkalinity, sulphate, conductivity, and dissolved metals.

4. ML-ARD RESULTS FOR ROCK

As explained in Chapter 3, 232 samples of rock from Schaft Creek core, most drilled in 2005 and 2006, were subjected to various geochemical static (one-time) analyses. This chapter discusses the results of those analyses, and the analyses are compiled in Appendix A. Samples for laboratory-kinetic testing are also recommended here. Tailings samples are discussed further in Chapter 5.

4.1 Acid-Base Accounting

As explained in Section 3.2, acid-base accounting (ABA) comprises several individual analyses and calculations. The major categories are paste pH (Section 4.1.1), sulphur species and acid potentials (Section 4.1.2), neutralization potentials (Section 4.1.3), and net balances of acid potentials and neutralization potentials (Section 4.1.4).

4.1.1 Paste pH

Paste pH is measured in a mixture ("paste") of pulverized sample and deionized water. If samples are well weathered and oxidized before analysis, then sometimes acidic pH values are measured, meaning the samples were already generating net acidity. QA/QC data showed the initial deionized water had a pH of 6.0-6.2, and values were reproducible to within ±0.1 pH units.

Paste pH in the 235 rock and tailings samples for Schaft Creek ranged from 7.4 to 9.2 (Appendix A and Figures 4-1a and b). Thus, no samples were acidic at the time of analysis. The sample with the lowest near-neutral paste pH also contained the highest amount of sulphur.

4.1.2 Sulphur Species and Acid Potentials

Possible sulphur species that could be found in Schaft Creek rock are: sulphide including pyrite and chalcopyrite (Section 2.3), leachable sulphate like gypsum or anhydrite, and non-leachable sulphate like barite. The sum of these species theoretically equals total sulphur, although analytical inaccuracy and the existence of other sulphur species rarely yield an exact balance.

Total sulphur in the 235 rock and tailings samples ranged from 0.01 (detection limit) to 13.5%S, with a mean of 0.50%S and a median of 0.22%S (Figure 4-1 and Appendix A). For the three ore zones (excluding the biased high-sulphide samples up to 13.5%S), all three had similar minimum total-sulphur values of 0.01 to 0.02%S; similar mean values from 0.36 to 0.41%S; and maximum values of 1.47 to 1.56%S except in the Main Zone with a maximum of 3.35%S. Therefore, while maximum total-sulphur values can vary due to localized higher-sulphur rock, the mean and minimum values were similar for all three ore zones.

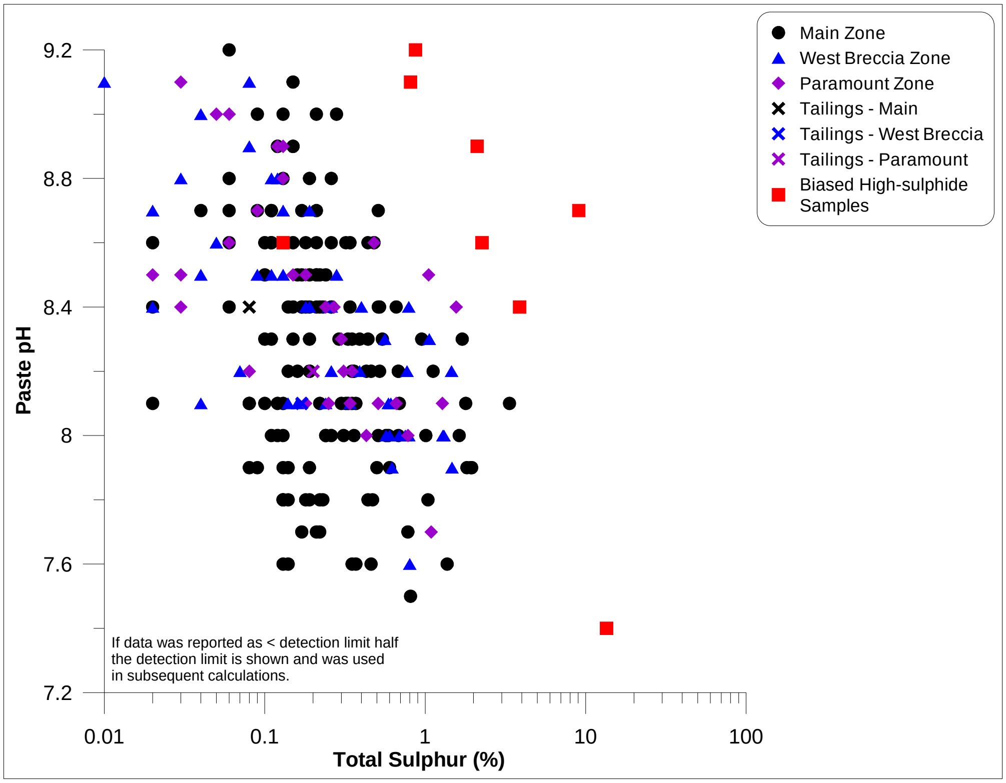


Figure 4-1a. Paste pH vs. Total Sulphur in the Phase 2 ML-ARD Samples, by Ore Zone.

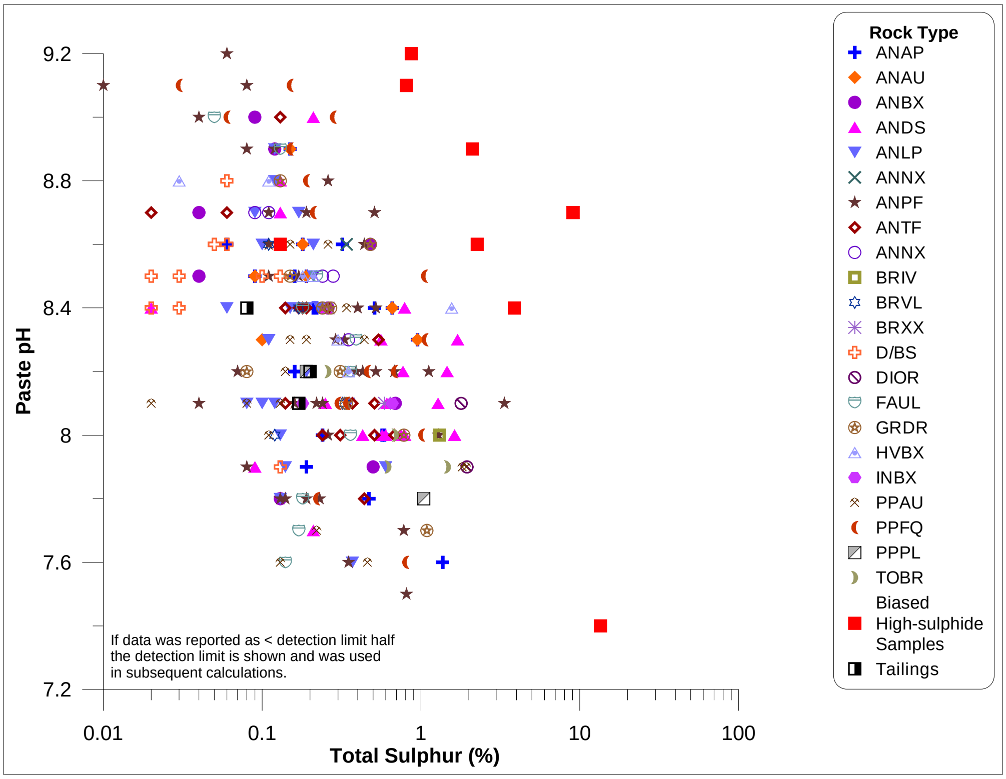


Figure 4-1b. Paste pH vs. Total Sulphur in the Phase 2 ML-ARD Samples, by Rock Unit.

Internal blanks, internal duplicates, and two external duplicates showed acceptable QA/QC for total sulphur and sulphide, with RPD values less than 10%. As an independent QA/QC check, ICP-MS total-element analyses (Sections 3.2 and 4.2) included a total-sulphur analysis that could be compared to the Leco-based ABA analysis. This showed good agreement across the range of values (Figures 4-2a and b), with the mean and median errors of +5.7% (ICP-MS total-sulphur was typically higher). Errors increased below 0.04%S due to numerical round-off, which included approximately 5% of the 235 samples, resulting in 30-100% errors at these levels.

In most samples, total sulphur and sulphide were similar (Figures 4-3a and b). Statistically, sulphide represented 85% of total sulphur on average, with a median of 87%. Thus, the two parameters were typically interchangeable, but not identical.

Several samples contained more HCl-leachable sulphate than sulphide, with some from the Main and West Breccia zones containing mostly sulphate (close to the 1:1 lines in Figures 4-4a and b). A comparison of HCl-leachable sulphate to Carbonate-leachable sulphate, which is an alternative sulphate method, was used to estimate a lower limit of good analytical accuracy. This comparison showed that sulphate analyses at and below 0.05%S were relatively inaccurate (Figures 4-5a and b), similar to total sulphur. About 90% of the 235 samples contained HCl-leachable sulphate in this inaccurate range at and below 0.05%S.

Non-leachable sulphide as barite ($BaSO_4$) was calculated by assuming all barium from the ICP-MS analysis (Sections 3.2 and 4.2) occurred as barite. This worst-case assumption showed that maximum non-leachable barium-bound sulphate would be 0.036%S with a mean of 0.01%S (Appendix A). This is within the analytical range (<0.05%S) with poor reliability and thus cannot be accurately compared with other sulphur species. In any case, on average, non-leachable sulphide as barite was 7.2% of total sulphur (median of 3.2%), and thus not a major part of the sulphur mass balance.

A QA/QC mass-balance equation for sulphur species is:

$$\%S(\mathrm{del}_{actual}) = \%S(\mathrm{Total}) - \%S(\mathrm{Sulphide}) - \%S(\mathrm{HCl\text{-}leachable\ sulphate}) - \%S(BaSO_4)$$

Large negative values of $\%S(\mathrm{del}_{actual})$ indicate the sum of sulphur species exceeds the measured total sulphur, sometimes due to analytical inaccuracy and detection limits. Large positive values indicate either (1) total sulphur was overestimated and/or (2) one or more sulphur species were underestimated. Positive values (“missing sulphur”) can be added to acid-generating sulphide for safer calculations. This approach was used here for Schaft Creek rock, to calculate Sulphide-Based Acid Potentials (SAP, Appendix A).

Based on an allowable inaccuracy of 20% of total sulphur, 212 of 235 samples (90%) had acceptable mass balances. Many of the 23 samples with significant imbalances had relatively low sulphur below 0.05%S, which as discussed above was close to detection limits. In total, 122 of 235 samples (52%) had positive values of $\%S(\mathrm{del}_{actual})$, so this “missing sulphur” was added to sulphide as a safety factor before calculating Sulphide-Based Acid Potential (SAP, Appendix A).

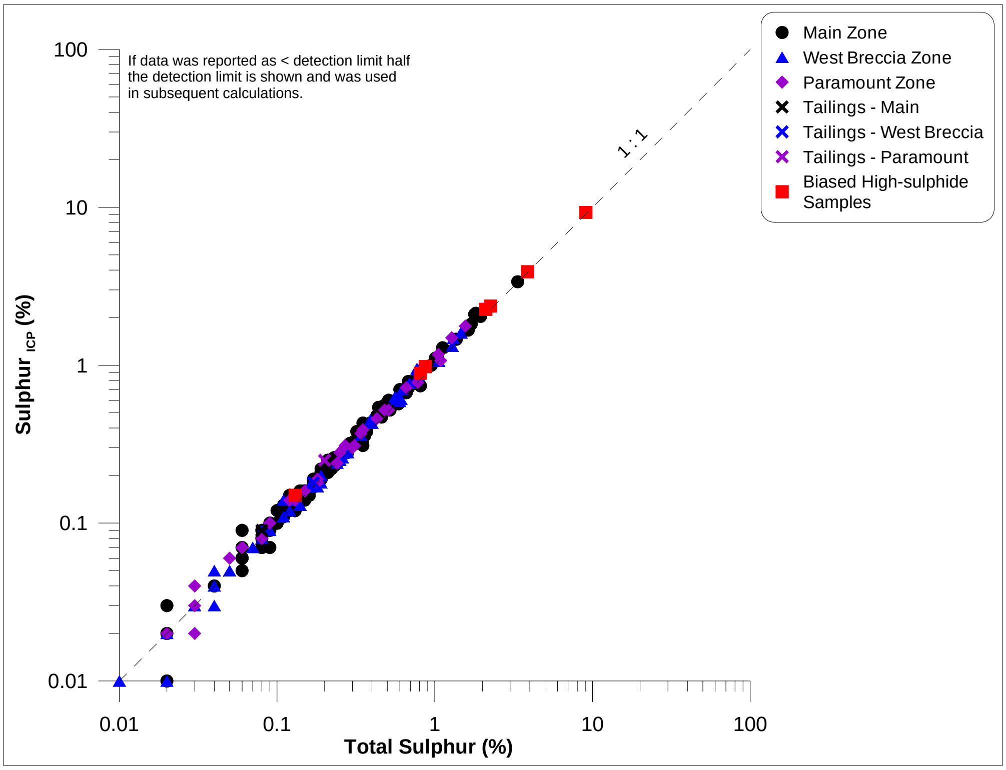


Figure 4-2a. ICP-MS Total Sulphur vs. Leco-ABA Total Sulphur in the Phase 2 ML-ARD Samples, by Ore Zone.

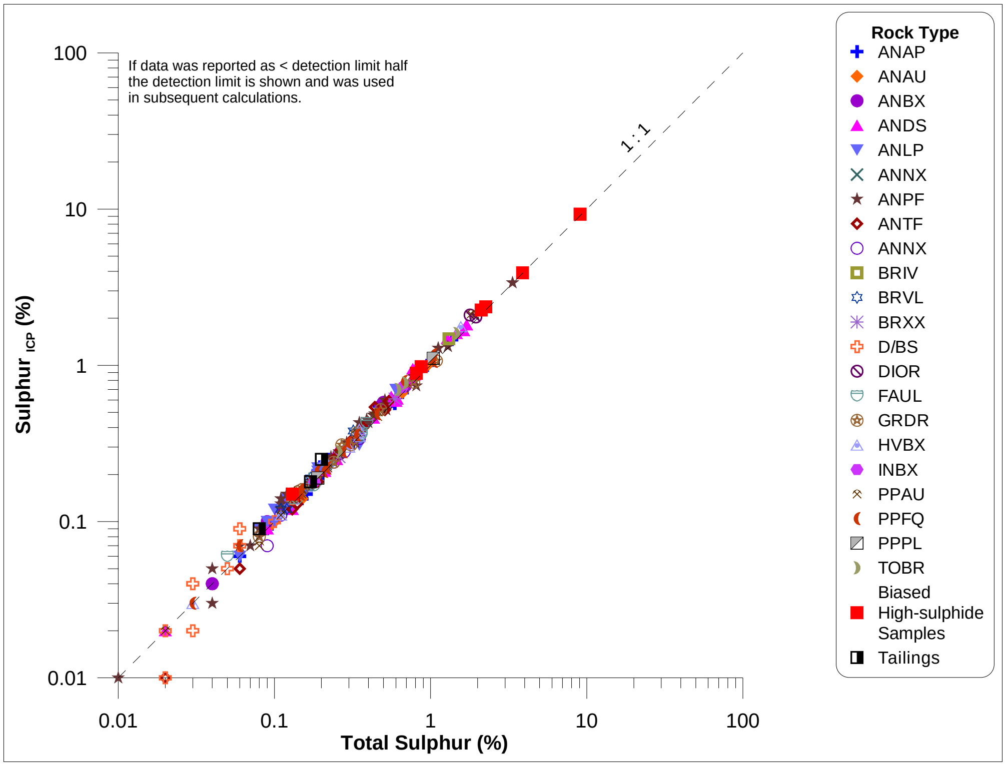


Figure 4-2b. ICP-MS Total Sulphur vs. Leco-ABA Total Sulphur in the Phase 2 ML-ARD Samples, by Rock Unit.

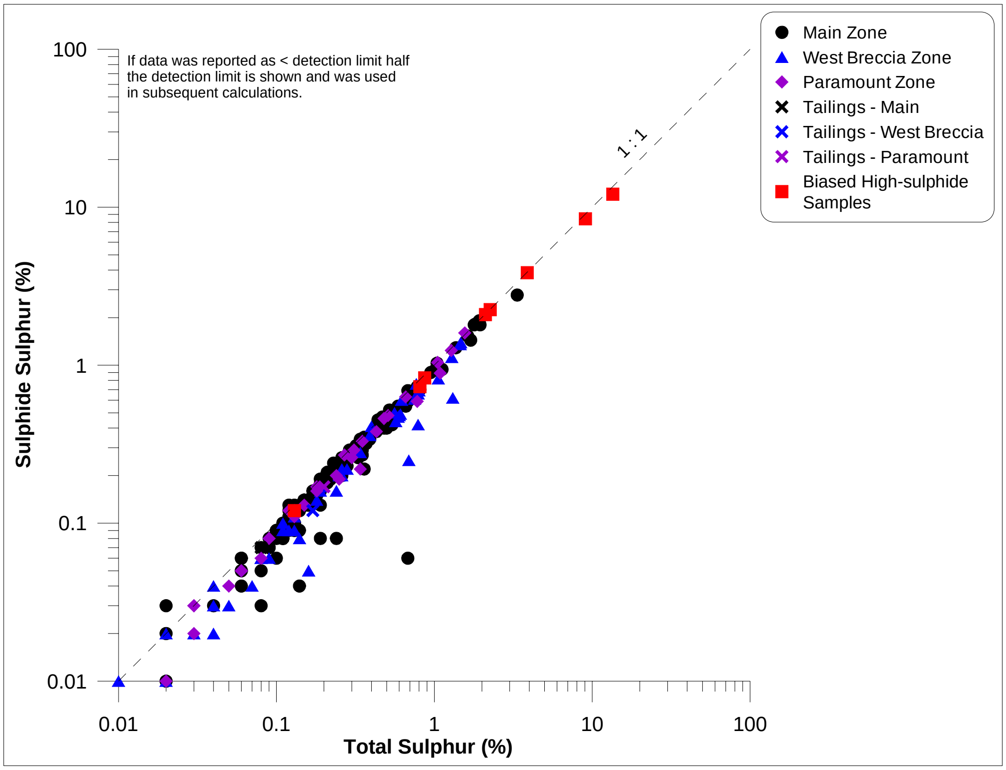


Figure 4-3a. Sulphide vs. Total Sulphur in the Phase 2 ML-ARD Samples, by Ore Zone.

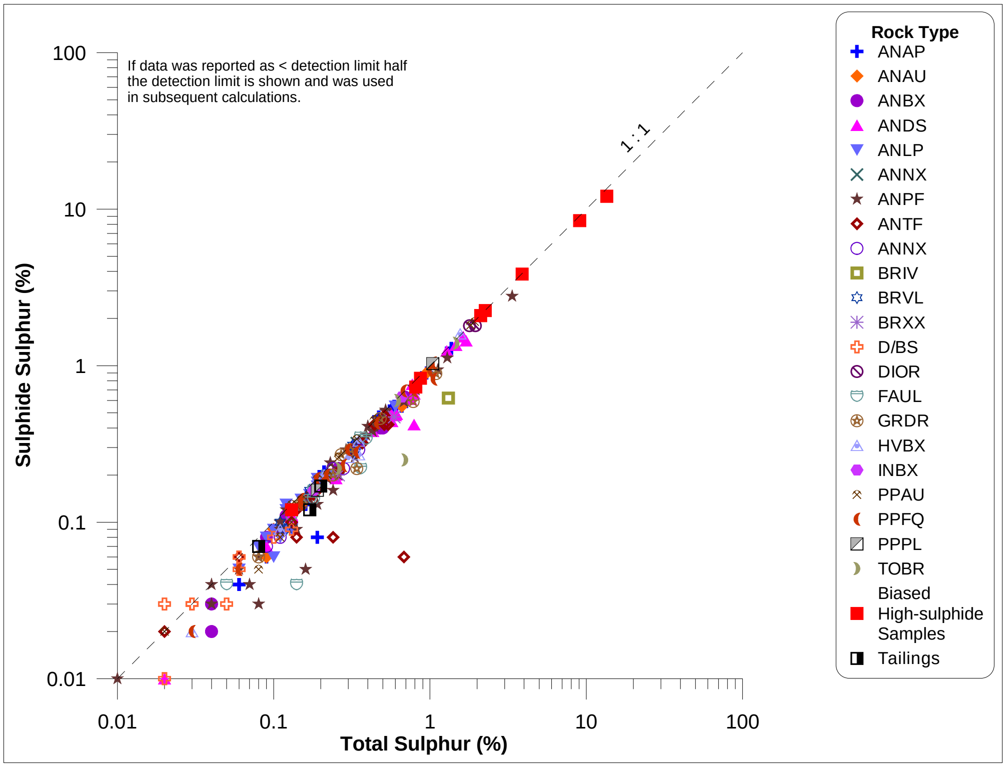


Figure 4-3b. Sulphide vs. Total Sulphur in the Phase 2 ML-ARD Samples, by Rock Unit.

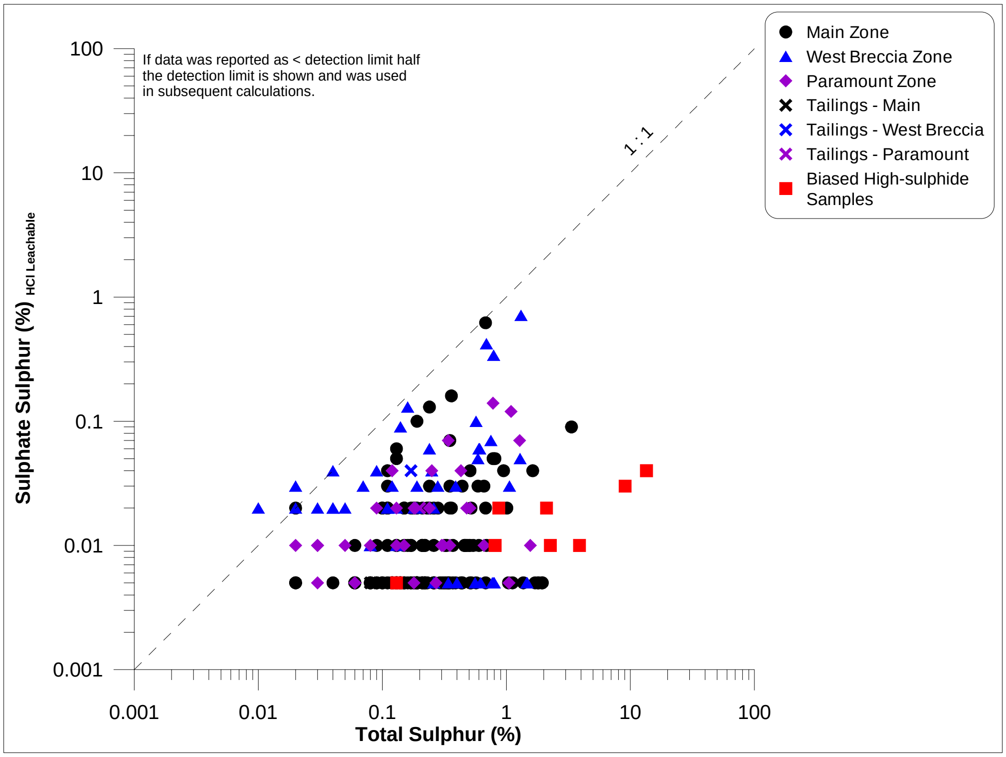


Figure 4-4a. HCl-Leachable sulphate vs. Total Sulphur in the Phase 2 ML-ARD Samples, by Ore Zone.

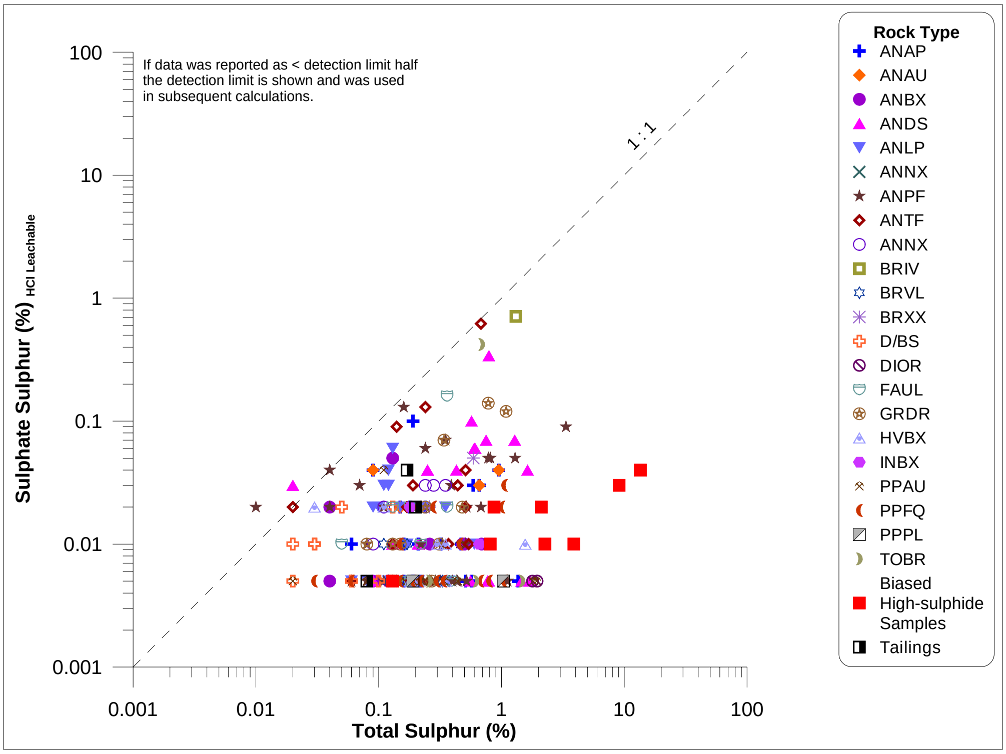
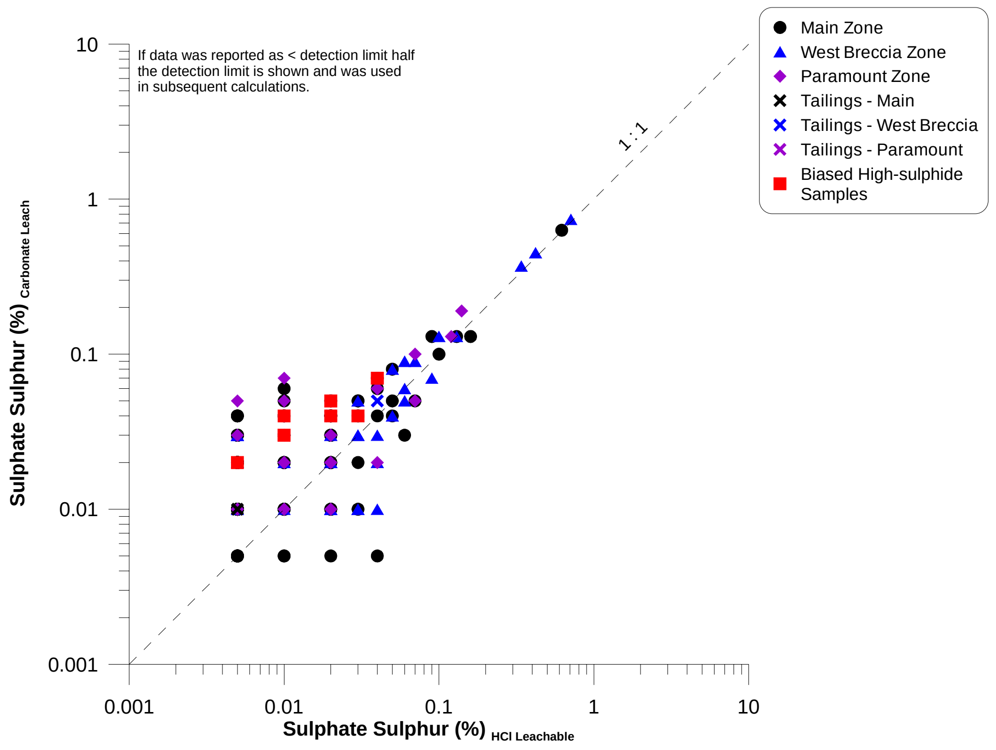
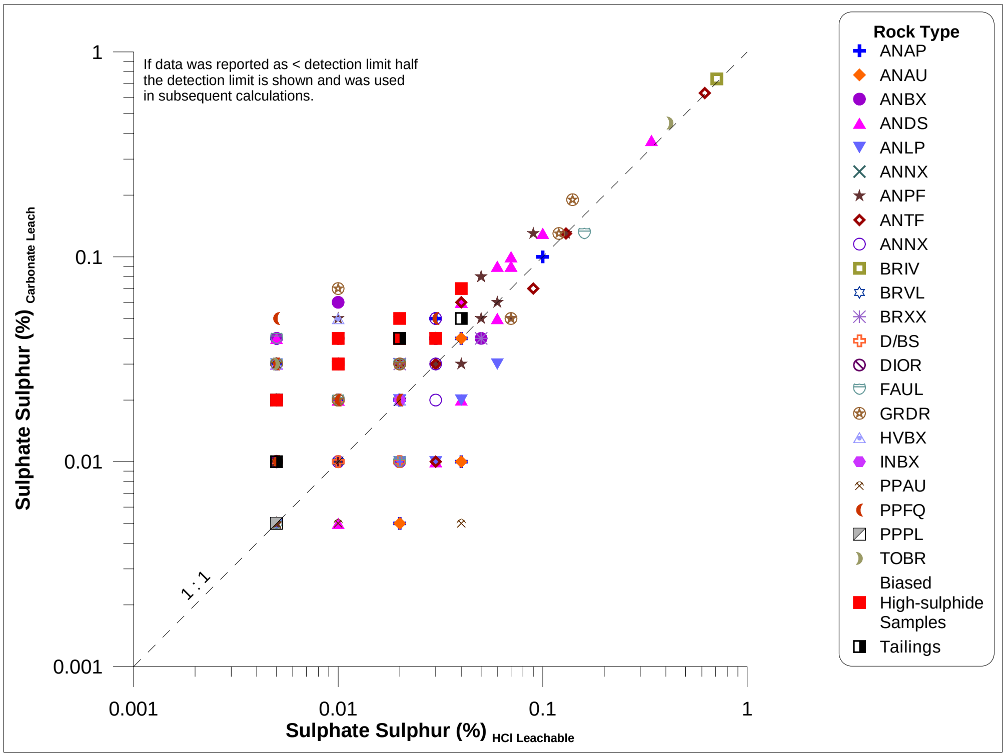


Figure 4-4b. HCl-Leachable sulphate vs. Total Sulphur in the Phase 2 ML-ARD Samples, by Rock Unit.



If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

Figure 4-5a. Carbonate-Leachable sulphate vs. HCl-Leachable sulphate in the Phase 2 ML-ARD Samples, by Ore Zone.



If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

Figure 4-5b. Carbonate-Leachable sulphate vs. HCl-Leachable sulphate in the Phase 2 ML-ARD Samples, by Rock Unit.

As explained in the Phase 1 ML-ARD report (Morin and Hutt, 2007), not all sulphide exists in an acid-generating form. In some rock, much of the sulphide occurs with copper (Chapter 2), which has less to no potential for acid generation, but not all copper occurs as sulphide. Calculations were made in the Phase 1 report to bracket the actual acid potential by assuming (1) all sulphide was acid generating and (2) only the sulphide not mathematically associated with copper, zinc, molybdenum, mercury, and arsenic was acid generating. The former could be used for "worst-case" (sulphide-based) acid potential, and the latter, "best-case" (pyrite-calculated) acid potential.

Recent comments from the British Columbia Ministry of Environment indicated the best-case, pyrite-calculated approach should no longer be used. Also, total sulphur rather than sulphide should be used to calculate acid potential, because total sulphur is easier to measure on a daily operational basis and because of inaccuracies in sulphur species. This Phase 2 report will use this MOE approach of Total-Sulphur-Based Acid Potential (TAP), recognizing it will definitely overestimate the acid potential of most samples and will be more "worst case" than the sulphide-based approach used in Phase 1. Phase 3 work may revise this approach based on kinetic testing and mineralogical studies.

In summary, total sulphur in the 235 Schaft Creek samples of rock and tailings ranged from 0.01 (detection limit) to 13.5%S, with a mean of 0.50%S and a median of 0.22%S. Although maximum total-sulphur values varied due to localized higher-sulphur rock in the three ore zones, the mean and minimum values were similar for all three. Statistically, sulphide represented 85% of total sulphur on average, with a median of 87%. Thus, the two parameters were typically interchangeable, but not identical. Approximately 5-10% of the samples had sulphur-species analyses within the relatively unreliable range below roughly 0.05%S. The MOE-recommended approach of using total sulphur and the associated Total-Sulphur-Based Acid Potential (TAP) will be used here. This recognizes that TAP tends to overestimate actual acid potential, often by a small amount, and may be changed in Phase 3 studies based on additional work.

4.1.3 Neutralization Potentials

There are various types of neutralizing capacities in rock samples, all expressed in units of kg $CaCO_3$ equivalent/tonne (kg/t). These include:

(1) Sobek "bulk neutralization potential" (NP) based on an hours-long acid bath to determine how much acid was neutralized in the short term (EPA 600 technique),

(2) carbonate-equivalent neutralization potential (CaNP) calculated from measured solid-phase levels of inorganic carbonate (Inorg CaNP) or total carbon (Total CaNP), and

(3) calculated CaNP assuming all calcium occurs as calcite (Ca CaNP) or all calcium + magnesium occurs as calcite and dolomite (Ca+Mg CaNP).

Each can reveal important aspects of a sample's capacity to neutralize the acidity generated by sulphide oxidation. All values are compiled in Appendix A.

Sobek NP ranged from 21 to 219 kg/t in the 235 Schaft Creek samples of rock and tailings, with a mean of 79 and a median of 75 kg/t (Figures 4-6a and b, and Appendix A). These are relatively high values. They explain why no acidic paste pH values were detected (Section 4.1.1), and suggest there could be a long lag time (years to decades) before any sample might become acidic. The two external duplicates and one internal duplicate showed good QA/QC for Sobek NP, with RPD values less than 10% based on internal and external duplicates.

Some amount of measured Sobek NP is typically "unavailable" for neutralization, often between 5-15 kg/t although smaller and larger values have been documented (Morin and Hutt, 1997 and 2001). This can sometimes be seen in scatterplots of Sobek NP with paste pH after sufficient time has passed for net acidity to develop. The trends then typically show that paste pH generally, but not consistently, decreases as NP decreases, until acidic pH values are detected.

However, the lack of any acidic paste pH in the 235 samples means that Unavailable NP cannot be estimated at this time. Thus, the common default value of 10 kg/t will be used and will be subtracted from all measured values to obtain Available NP (Appendix A and Figures 4-6a and b). As with the use of total sulphur for calculating acid potential (Section 4.1.2), this may overestimate the capacity for net acid generation (Section 4.1.4), but additional work is needed to assess this (Section 4.3).

The comparison of total carbon with inorganic carbon showed that both were about the same in nearly all samples (Appendix A), with inorganic carbon representing 97% of total carbon on average (median of 98%). Inorganic carbon was less than one-half of total carbon in only two samples. For Sample 125154 in the West Breccia Zone, inorganic carbon was only 5% of total carbon. For Sample 14816 in the Main Zone, inorganic carbon was only 17% of total carbon. These two samples probably had erroneous inorganic-carbon analyses, as explained below. Thus, total carbon and inorganic carbon were basically the same and interchangeable.

A scatterplot of Sobek NP with Inorganic Carbon, converted to the same units (Inorganic CaNP as kg/t), can reveal some geochemical relationships. For the 235 Phase 2 samples, this scatterplot showed that Sobek NP was greater than Inorganic CaNP in 78% of the samples (Figures 4-7a and b). Some distinct trends were apparent.

First, most samples (64%) fell within the range of NP = Inorganic CaNP to NP = 1.5 * Inorganic CaNP. This may reflect the mineralogy of abundant non-carbonate, aluminosilicate minerals (Chapter 2) that can provide neutralization.

Second, below an NP of 40-50 kg/t, NP frequently exceeded Inorganic CaNP by more than a factor of 1.5. This showed non-carbonate minerals represented a higher proportion of NP as NP decreased below 40-50 kg/t.

Third, around an NP of 60-90 kg/t, a distinct trend of increasing Inorganic CaNP greater than NP was seen, particularly for the Main Zone. This may reflect different carbonate minerals in different parts of the Main Zone, but three-dimensional modelling would be needed to assess this further (Section 4.3). In any case, Sobek NP is still considered the better measure of neutralizing capacity than Inorganic CaNP.

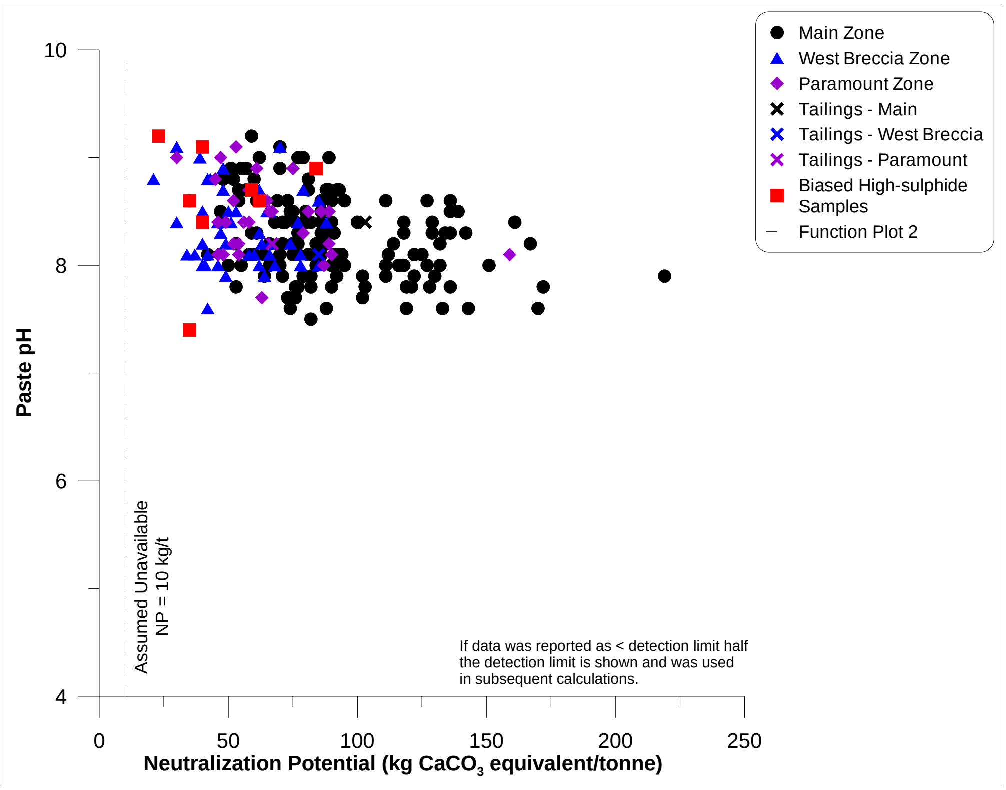


Figure 4-6a. Paste pH vs. Sobek Neutralization Potential in the Phase 2 ML-ARD Samples, by Ore Zone.

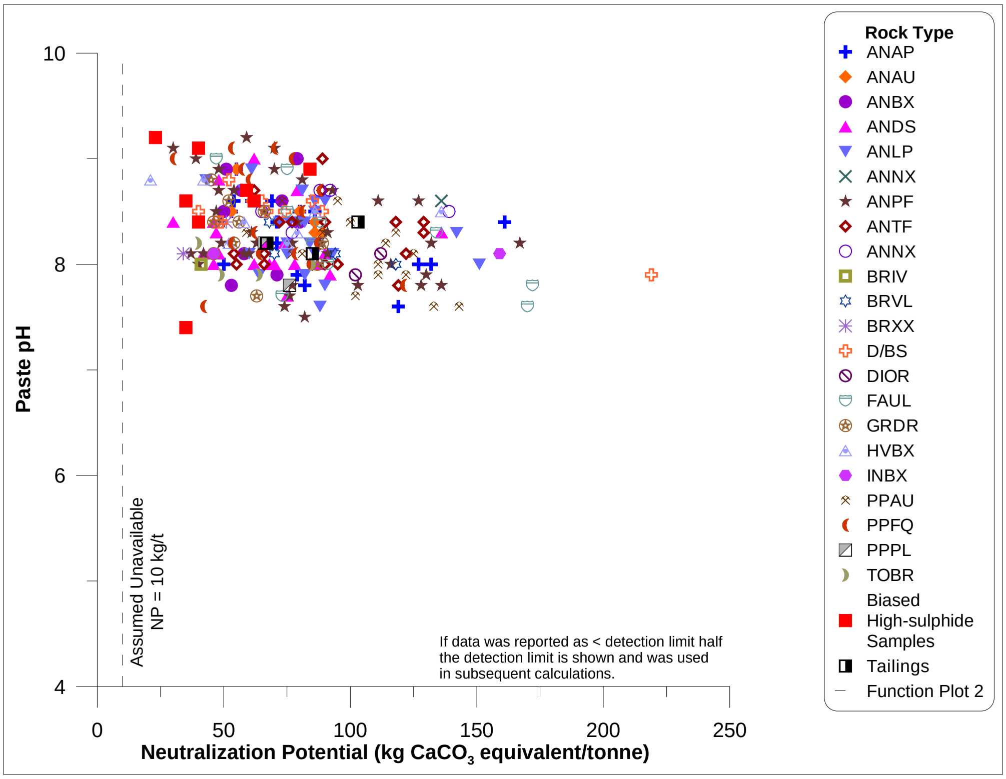


Figure 4-6b. Paste pH vs. Sobek Neutralization Potential in the Phase 2 ML-ARD Samples, by Rock Unit.

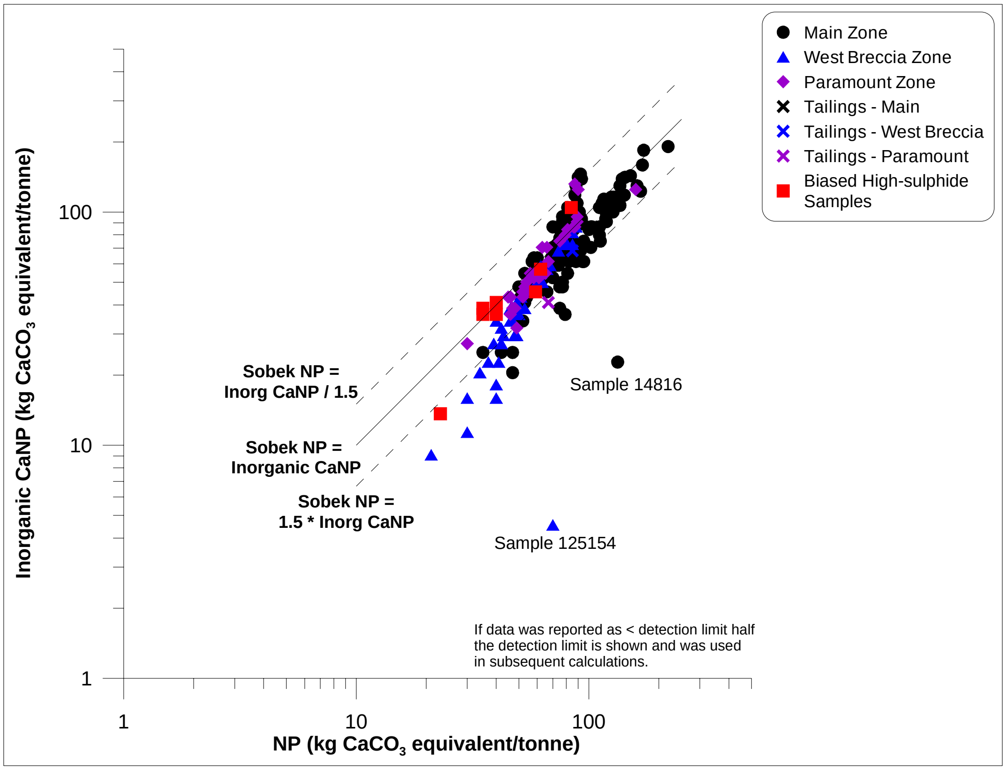


Figure 4-7a. Inorganic-Carbon-Based CaNP vs. Sobek Neutralization Potential in the Phase 2 ML-ARD Samples, by Ore Zone.

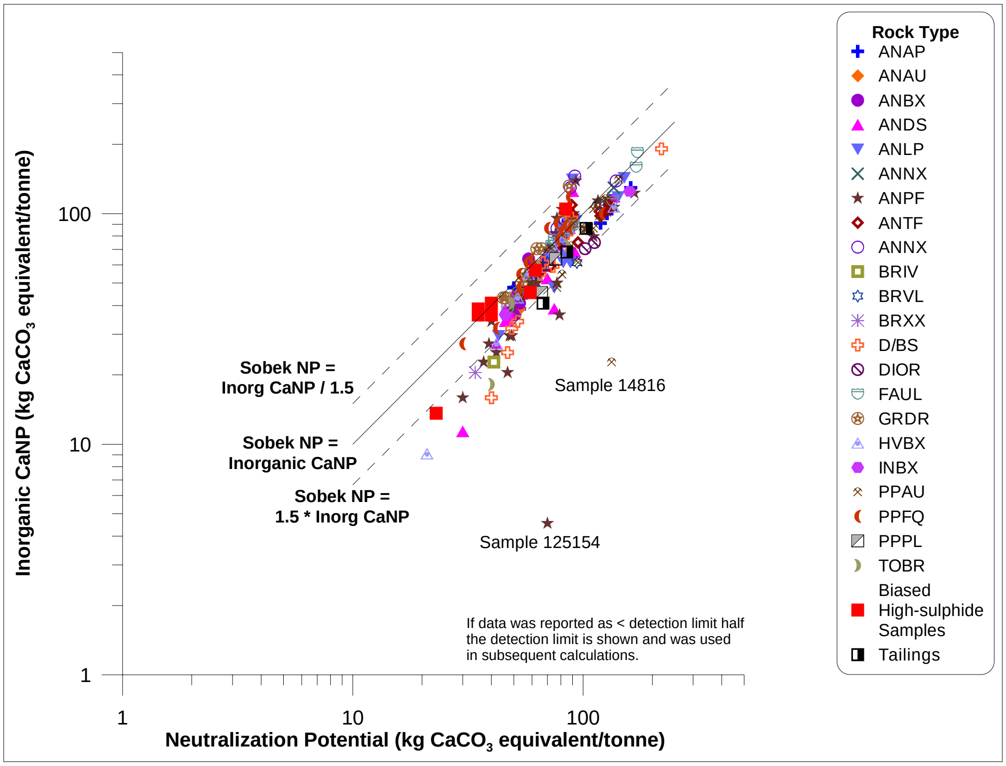


Figure 4-7b. Inorganic-Carbon-Based CaNP vs. Sobek Neutralization Potential in the Phase 2 ML-ARD Samples, by Rock Unit.

Fourth, Samples 125154 and 14816 (see previous paragraph) stood out as anomalous, but matched the general trend if total carbon replaced inorganic carbon. Thus, the inorganic-carbon analyses for these two samples appeared erroneous.

Because the type of carbonate (calcite, dolomite, siderite, etc.) was not determined in previous studies (Chapter 2), scatterplots with Inorganic CaNP can sometimes reveal the carbonate composition, if elements like calcium and magnesium mostly occur only with carbonate. For the comparison, calcium was converted to “Ca CaNP” with similar units as Inorganic CaNP. This showed that some samples contained excess carbonate, many contained excess calcium, and some contained both in calcite-equivalent amounts (Figures 4-8a and b). The common excess calcium was consistent with calcium-bearing aluminosilicate minerals in Schaft Creek rock (Chapter 2). Mineralogical work on the carbonate is recommended (Section 4.3). For the three tailings samples, x-ray-diffraction mineralogy showed most of the carbonate was calcite with lesser dolomite (Section 5.2).

Similarly, a comparison of “Ca+Mg CaNP” to Inorganic CaNP showed that nearly every sample contained more Ca+Mg than carbonate (Appendix A). This meant that dolomite could not account for all the Ca+Mg, which was consistent with both calcium-bearing and magnesium-bearing aluminosilicate minerals in Schaft Creek rock (Chapter 2).

Sobek NP showed some correlation with Ca CaNP (Figures 4-9a and b). This suggests calcium-bearing minerals, both carbonate and aluminosilicate, can account for Sobek NP in several samples, but not all samples. Ca+Mg CaNP displayed an even poorer correlation with Sobek NP. Thus, rapid assay-based analyses like calcium and magnesium cannot substitute for the more intensive Sobek NP in Schaft Creek rock.

In summary, Sobek (EPA 600) Neutralization Potential (NP) ranged from 21 to 219 kg/t in the 235 Schaft Creek samples of rock and tailings, with a mean of 79 and a median of 75 kg/t. These relatively high values explained why no acidic paste pH values were detected. They also suggested there could be a long lag time (years to decades) before any sample might become acidic. Nearly all the measured total carbon was inorganic carbonate, which can neutralize acidity depending on the form of the carbonate. Correlations of inorganic carbonate with Sobek NP showed several trends. First, Sobek NP was typically up to 1.5 times higher, meaning non-carbonate minerals apparently contributed to neutralization. Second, below a Sobek NP of 40-50 kg/t, NP frequently exceeded Inorganic CaNP by more than a factor of 1.5. This showed non-carbonate minerals represented a higher proportion of NP as NP decreased below 40-50 kg/t. Third, around an NP of 60-90 kg/t, a distinct trend of increasing Inorganic CaNP greater than NP was seen, particularly for the Main Zone. This may reflect different carbonate minerals in different parts of the Main Zone, but three-dimensional modelling would be needed to assess this further. In any case, Sobek NP is still considered the better measure of neutralizing capacity than Inorganic CaNP. The lack of correlations with solid-phase calcium and calcium+magnesium meant that the form of the inorganic carbonate could not be inferred, but some correlation of Sobek NP and calcium probably reflected a calcium-bearing combination of carbonate and non-carbonate minerals.

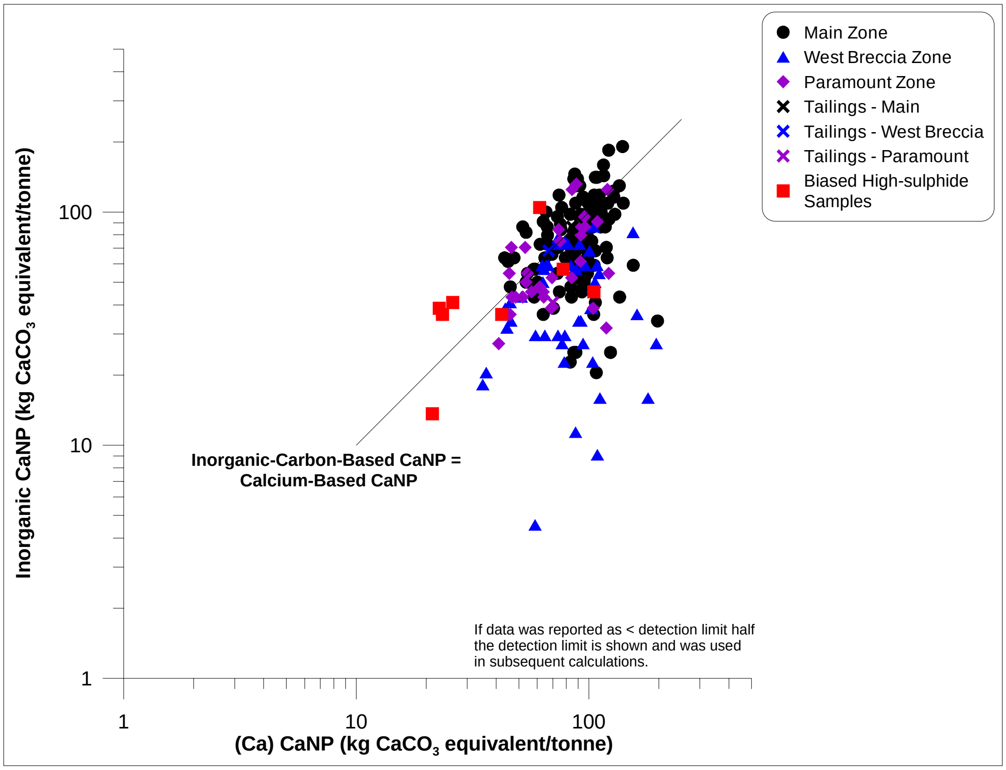


Figure 4-8a. Inorganic-Carbon-Based CaNP vs. Calcium-Based CaNP in the Phase 2 ML-ARD Samples, by Ore Zone.

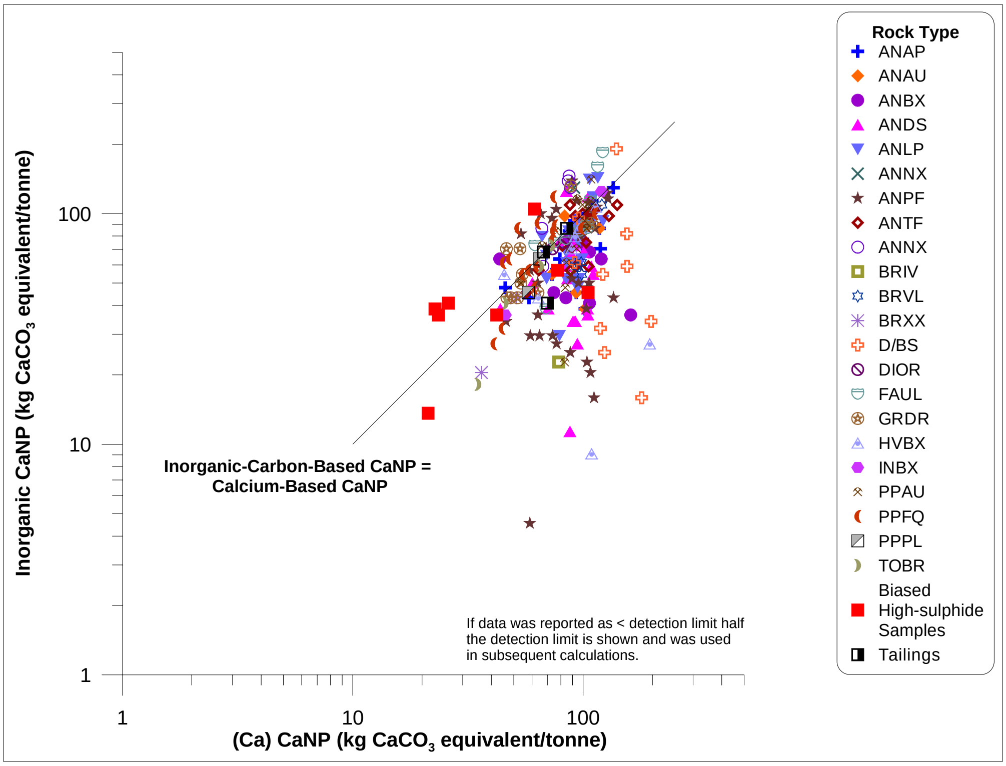


Figure 4-8b. Inorganic-Carbon-Based CaNP vs. Calcium-Based CaNP in the Phase 2 ML-ARD Samples, by Rock Unit.

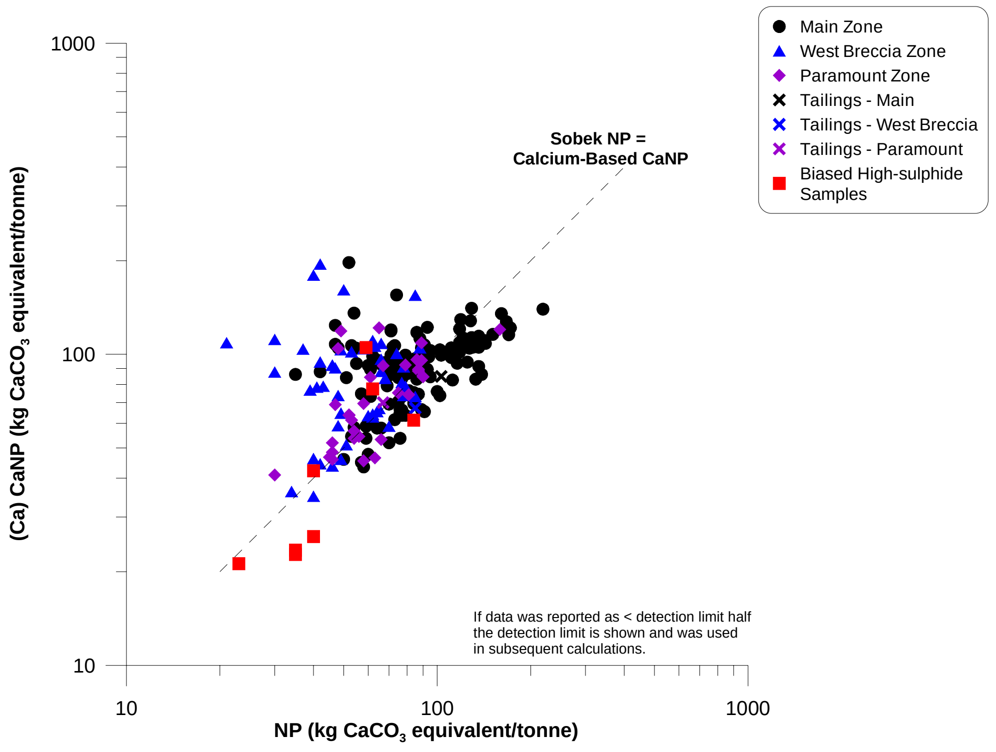


Figure 4-9a. Calcium-Based CaNP vs. Sobek Neutralization Potential in the Phase 2 ML-ARD Samples, by Ore Zone.

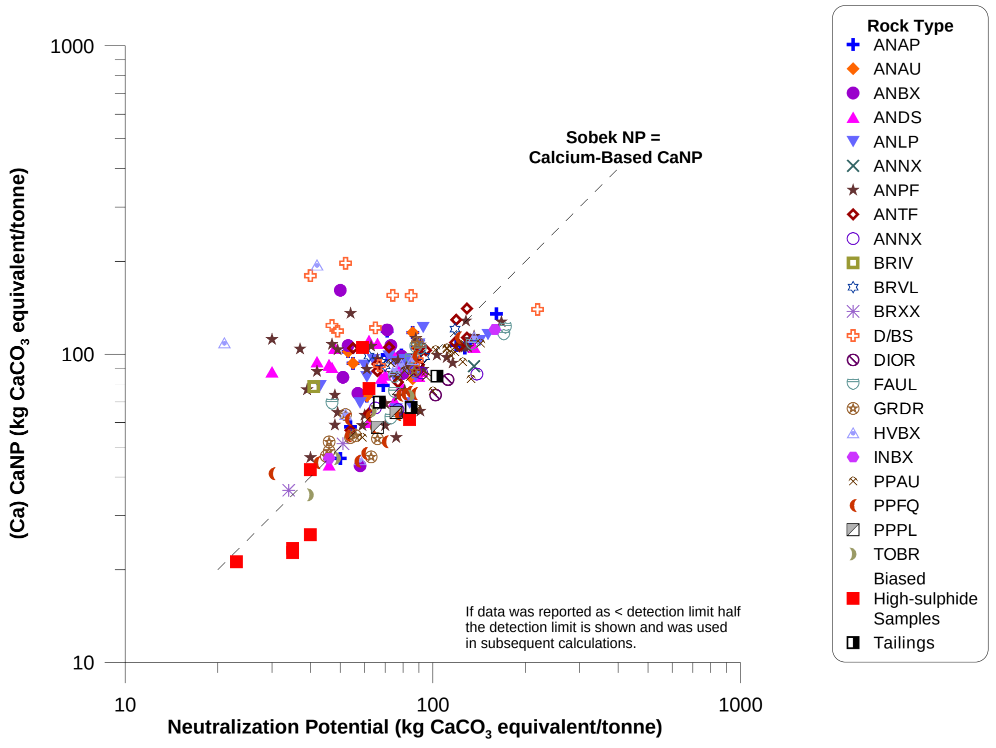


Figure 4-9b. Calcium-Based CaNP vs. Sobek Neutralization Potential in the Phase 2 ML-ARD Samples, by Rock Unit.

4.1.4 Net Balances of Acid-Generating and Acid-Neutralizing Capacities

As explained in Section 4.1.2, the acid-generating capacities of the Schaft Creek samples of rock could be calculated from total sulphur to obtain Total-Sulphur-Based Acid Potentials (TAP), or sulphide plus %S(del) to obtain Sulphide-Based Acid Potentials (SAP). Because total sulphur was mostly composed of sulphide, TAP and SAP were generally interchangeable. Due to the preference of the British Columbia Ministry of Environment, TAP is used here in this Phase 2 study, but may change in later phases.

Neutralization Potentials (NP) were discussed in Section 4.1.3. The current estimate of 10 kg/t was considered unavailable and can be subtracted from measured values to obtain Effective or Available NP.

Net balances of these two potentials were calculated to predict whether a sample would be net acid generating, perhaps after a long near-neutral "lag time", or net acid neutralizing indefinitely. Net balances can be calculated using division (Net Potential Ratio, NPR = NP / AP) or subtraction (Net Neutralization Potential, NNP = NP - AP).

Provincially, NPR is preferred and used here (Appendix A). Total-Sulphur-Based NPR values were obtained by:

$$\text{TNPR} = [\text{NP}] / [\text{TAP}] \qquad \text{(Eq. 4-1)}$$

with TAP obtained by:

$$\text{TAP} = \%\text{S(total)} * 31.25 \qquad \text{(Eq. 4-2)}$$

"Adjusted" Total-Sulphur-Based NPR values were obtained by first subtracting 10 kg/t of unavailable NP from measured NP:

$$\text{Adj TNPR} = [\text{NP} - 10] / [\text{TAP}] \qquad \text{(Eq. 4-3)}$$

Non-site-specific ABA screening criteria are: NPR $\leq$ 1 is net acid generating, perhaps after some lag time; 1<NPR<2 is uncertain until further testing; and NPR$\geq$2 is net acid neutralizing. The implications of using the alternative criterion of 1.0 are discussed below. These screening criteria differ from others with higher values, because they recognize and use Unavailable NP which is not included in other criteria. They also recognize the aqueous geochemistry of carbonate dissolution, which typically leads to values between 1.0 and 2.0.

It is important to note that all discussions of net balances in this report are "unweighted". This means that they were not adjusted to tonnages in the Schaft Creek Deposit. Three-dimensional geostatistical modelling of geology and ML-ARD parameters should be conducted (Section 4.3), to address issues such as (1) the total tonnages of net-acid-generating rock, (2) year-by-year production of net-acid-generating rock, and (3) portions of rock units that are net acid generating.

Adjusted TNPR values ranged from 0.059 (net acid generating) to 126.0 (net neutralizing), with a mean and median of 14.2 and 9.6, respectively (Figures 4-10a and b, Table 4-1, and Appendix A). Thus, most samples were net neutralizing. Only ten samples (4%) had Adj TNPR values at or below 1.0, and half were the biased high-sulphide samples. Another 15 samples (6%), from all three ore zones, were in the uncertain range.

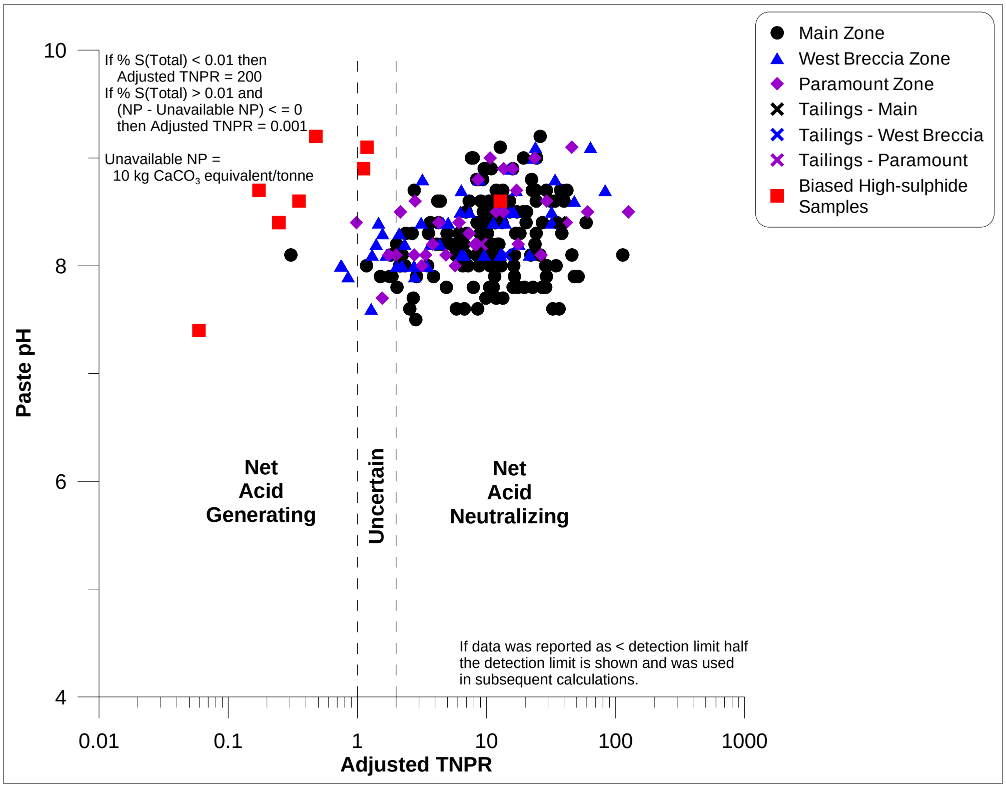


Figure 4-10a. Paste pH vs. Adjusted Total-Sulphur-Based Net Potential Ratio in the Phase 2 ML-ARD Samples, by Ore Zone.

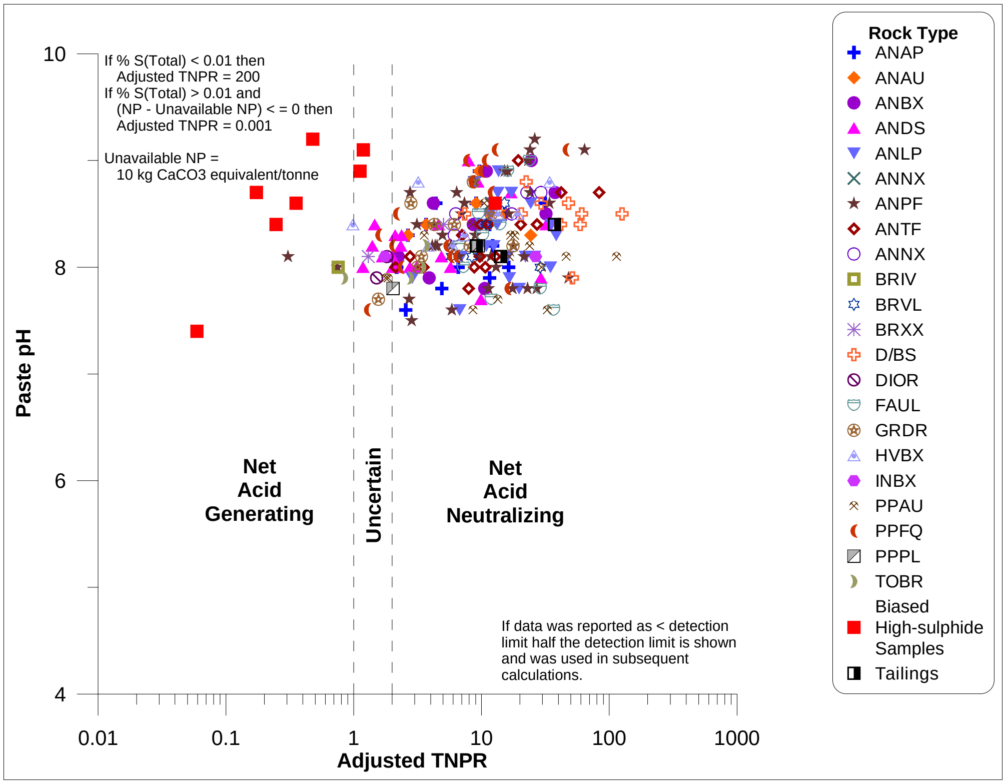


Figure 4-10b. Paste pH vs. Adjusted Total-Sulphur-Based Net Potential Ratio in the Phase 2 ML-ARD Samples, by Rock Unit.

Table 4-1. Percentages of Net-Acid-Generating, Uncertain, and Net-Acid-Neutralizing Samples by Ore Zone and by NPR Parameter (see also Appendix A)

		Percentage of Samples[1]		
NPR	Notes	Net Acid Generating	Uncertain	Net Acid Neutralizing
All Phase 2 Samples of Rock and Tailings				
Adjusted TNPR	uses total sulphur; unavailable NP = 10 kg/t	4.3	6.4	89.4
TNPR	uses total sulphur; all NP available	3.4	5.5	91.1
Adjusted SNPR	uses sulphide and any unaccounted-for sulphur; unavailable NP = 10 kg/t	3.8	7.2	88.9
SNPR	uses sulphide and any unaccounted-for sulphur; all NP available	2.6	5.5	91.9
Main (Liard) Zone				
Adjusted TNPR	uses total sulphur; unavailable NP = 10 kg/t	0.7	3.4	95.9
TNPR	uses total sulphur; all NP available	0.7	2.1	97.3
Adjusted SNPR	uses sulphide and any unaccounted-for sulphur; unavailable NP = 10 kg/t	0.7	4.1	95.2
SNPR	uses sulphide and any unaccounted-for sulphur; all NP available	0.7	2.7	96.6
West Breccia Zone				
Adjusted TNPR	uses total sulphur; unavailable NP = 10 kg/t	6.4	12.8	80.9
TNPR	uses total sulphur; all NP available	4.3	12.8	83.0
Adjusted SNPR	uses sulphide and any unaccounted-for sulphur; unavailable NP = 10 kg/t	4.3	14.9	80.9
SNPR	uses sulphide and any unaccounted-for sulphur; all NP available	0	12.8	87.2

		Percentage of Samples[1]		
NPR	Notes	Net Acid Generating	Uncertain	Net Acid Neutralizing
Paramount Zone				
Adjusted TNPR	uses total sulphur; unavailable NP = 10 kg/t	3.2	6.5	90.3
TNPR	uses total sulphur; all NP available	0	6.5	93.6
Adjusted SNPR	uses sulphide and any unaccounted-for sulphur; unavailable NP = 10 kg/t	3.2	6.5	90.3
SNPR	uses sulphide and any unaccounted-for sulphur; all NP available	0	3.2	96.8

[1] This does not include the biased high-sulphide samples, except in the first group of all samples; Net Acid Generating: $NPR \leq 1.0$; Uncertain: $1.0 < NPR < 2.0$; Net Acid Neutralizing: $NPR \geq 2.0$.

A sensitivity analysis was conducted, with total sulphur replaced by sulphide plus unaccounted-for (del) sulphur (Section 4.1.2) and with all measured NP considered reactive and available. For all Phase 2 samples, these various options had only minor effects on the percentages of samples in each ML-ARD category (top of Table 4-1), with roughly 90% of samples remaining net neutralizing. Thus, the ML-ARD status of Schaft Creek rock samples is not sensitive to these adjustments to sulphur and NP.

Net balances can be separated by ore zone. However, three-dimensional modelling is needed to determine if ore zone is the optimum category, rather than elevation, depth, or lateral location. In light of one sample representing up to 3% in an ore zone, the Main Zone generally had the lowest percentages of net-acid-generating and uncertain samples, and the highest percentage of net-neutralizing samples. In contrast, the West Breccia Zone had the lowest percentage of net-neutralizing samples. Again, in light of one sample representing up to 3% in an ore zone, the sensitivity analysis for each ore zone showed that various options had only minor effects on the percentages of samples in each ML-ARD category (Table 4-1).

Although net balances were based here on the combination of total sulphur and NP, a good correlation of Adjusted TNPR with one would allow a simpler approach, involving only one analysis. The correlation of Adjusted TNPR with total sulphur was noticeable (Figures 4-11a and b), but still left a region between 0.5 and 2.1%S where NP analyses would be required for proper prediction. The correlation of Adjusted TNPR with Sobek NP was poorer (Figures 4-12a and b), with only the few samples above an NP of 140 kg/t showing a consistently ML-ARD category.

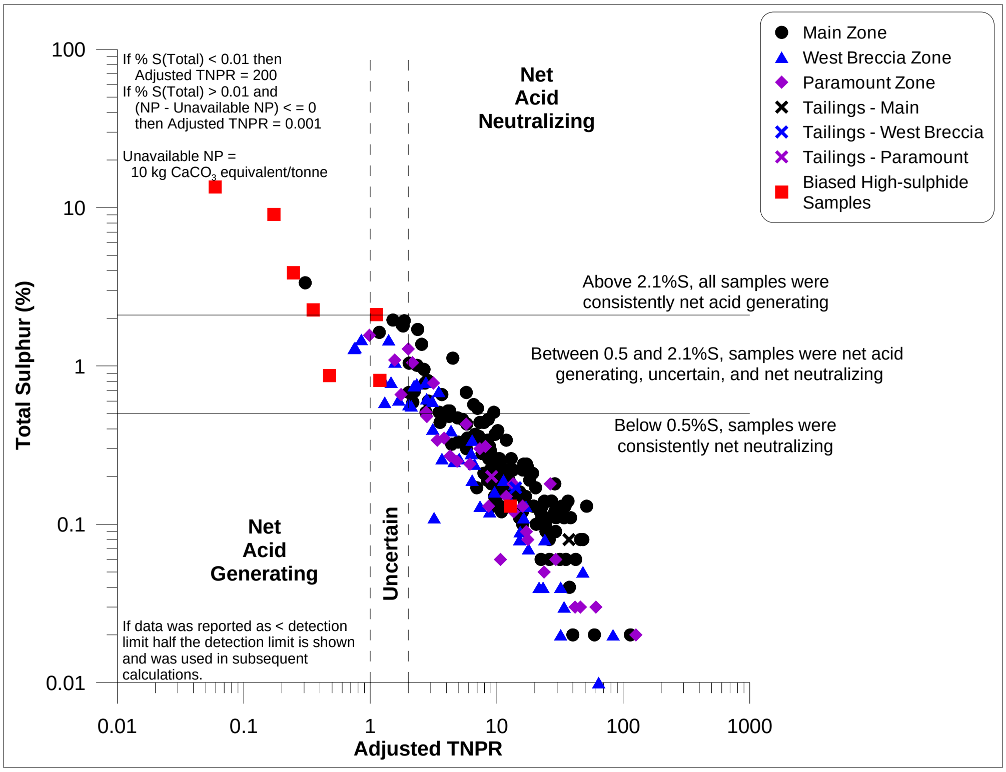


Figure 4-11a. Total Sulphur vs. Adjusted Total-Sulphur-Based Net Potential Ratio in the Phase 2 ML-ARD Samples, by Ore Zone.

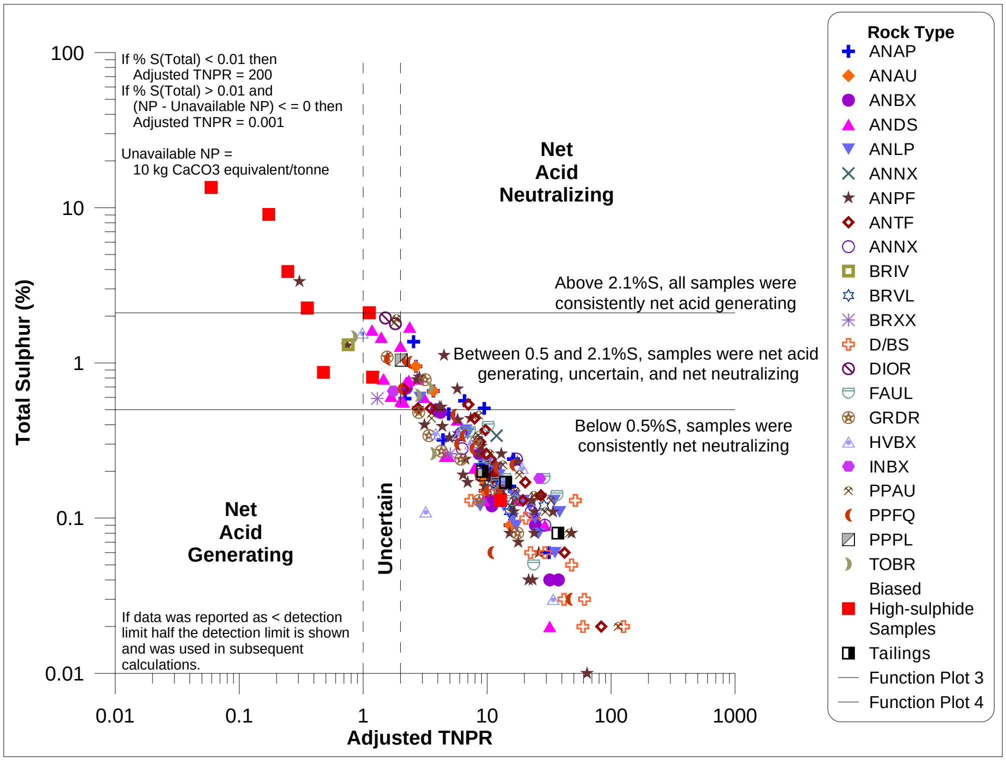


Figure 4-11b. Total Sulphur vs. Adjusted Total-Sulphur-Based Net Potential Ratio in the Phase 2 ML-ARD Samples, by Rock Unit.

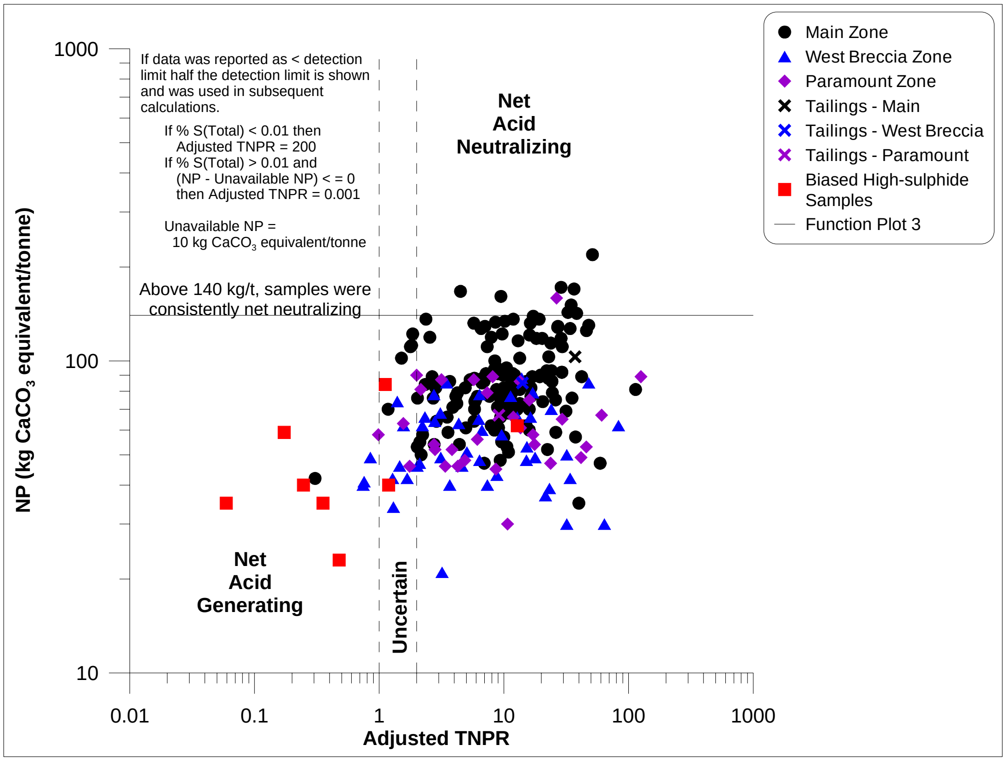


Figure 4-12a. Sobek Neutralization Potential vs. Adjusted Total-Sulphur-Based Net Potential Ratio in the Phase 2 ML-ARD Samples, by Ore Zone.

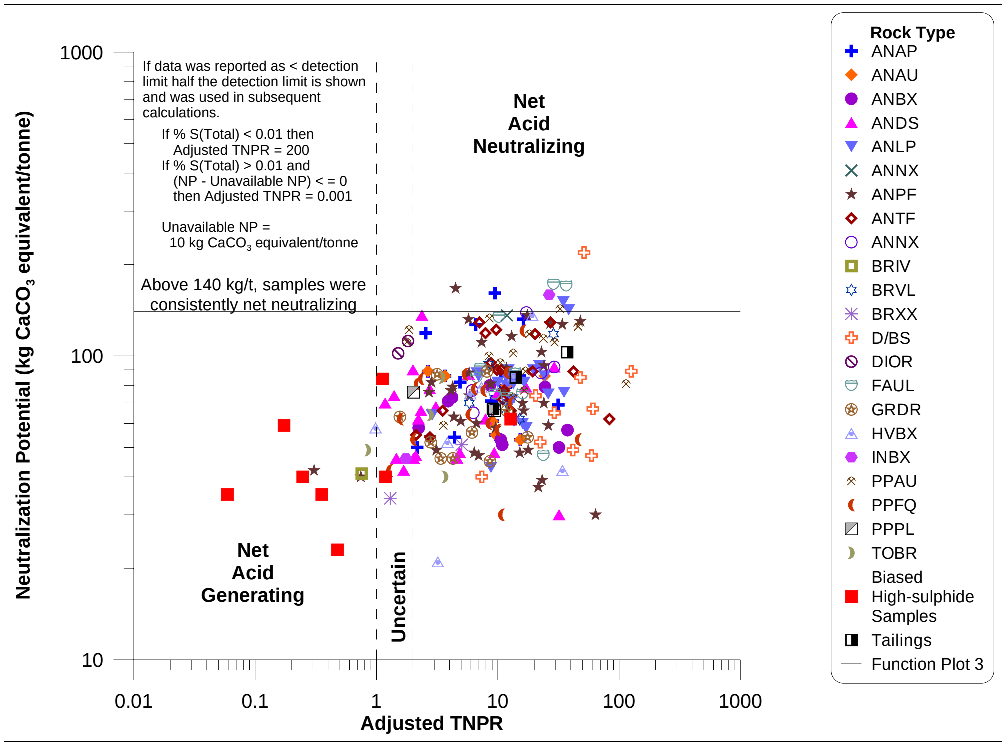


Figure 4-12b. Sobek Neutralization Potential vs. Adjusted Total-Sulphur-Based Net Potential Ratio in the Phase 2 ML-ARD Samples, by Rock Unit.

In summary, net balances of acid-generating and acid-neutralizing capacities for the 235 Phase 2 samples of rock and tailings were based on (1) total sulphur and the resulting Total Acid Potential (TAP) and (2) Sobek Neutralization Potential after Unavailable NP was subtracted. This was called, “Adjusted TNPR”. These net balances showed that approximately 90% was net neutralizing indefinitely, 4% was net acid generating although not yet acidic, and 6% was uncertain until further testing. A sensitivity analysis showed these percentages did not change significantly when (1) total sulphur was replaced by sulphide plus unaccounted-for sulphur or (2) all measured NP was considered fully reactive and available (Unavailable NP = 0). By ore zone, the Main (Liard) Zone had the highest percentage of net-neutralizing samples (96%), and the West Breccia Zone the lowest (81%). The correlation of Adjusted TNPR with total sulphur showed that samples: with more than 2.1%S were consistently net acid generating, with less than 0.5%S were consistently net neutralizing, and between 0.5 and 2.1%S could fall into any ML-ARD category depending on NP.

4.2 Total-Element Analyses

Total-element levels in the 235 Phase 2 samples (Section 3.1) were measured by ICP-MS analysis after strong four-acid digestion and by x-ray-fluorescence whole-rock analysis (Section 3.2). The results are compiled in Appendix A. There was generally good agreement for elements detected by both methods (Appendix A), except chromium whose whole-rock levels were often notably higher.

Overall, the dominant elements in the Schaft Creek samples were silicon and aluminum (Appendix A), reflecting the dominance of aluminosilicate minerals (Chapter 2). Calcium, iron, potassium, magnesium, sodium, and Loss on Ignition (LOI) were relatively abundant. LOI typically reflects the loss from the samples of some or all sulphur, carbon, and/or tightly bound or crystalline water.

To identify the metals and other elements that occurred at relatively high levels in the rock, each element was compared with average crustal abundances, as recommended in provincial ML-ARD documents (Price, 1998). Any level at least three times greater than the average maximum crustal abundance was highlighted with a box in Appendix A.
This showed that the Schaft Creek samples were:
- frequently elevated in silver, bismuth, copper, molybdenum, selenium, and tungsten; and,
- occasionally to rarely elevated in cadmium, lead, sulphur, antimony, and zinc.

Elevated solid-phase levels of elements do not necessarily mean they will leach into water at high concentrations. In fact, they may be elevated because they did not leach. Additional testwork is needed to evaluate metal leaching in detail (Section 4.3).

A comparison of minimum-to-maximum ranges of each solid-phase element in each ore zone showed generally similar ranges for a particular element (Figures 4-13a, b, and c). However, some notable differences were higher levels of antimony and lead in some samples from the West Breccia Zone (Figures 4-14 and 4-15) and typically lower levels of cadmium and zinc in the Main Zone (Figures 4-16 and 4-17).

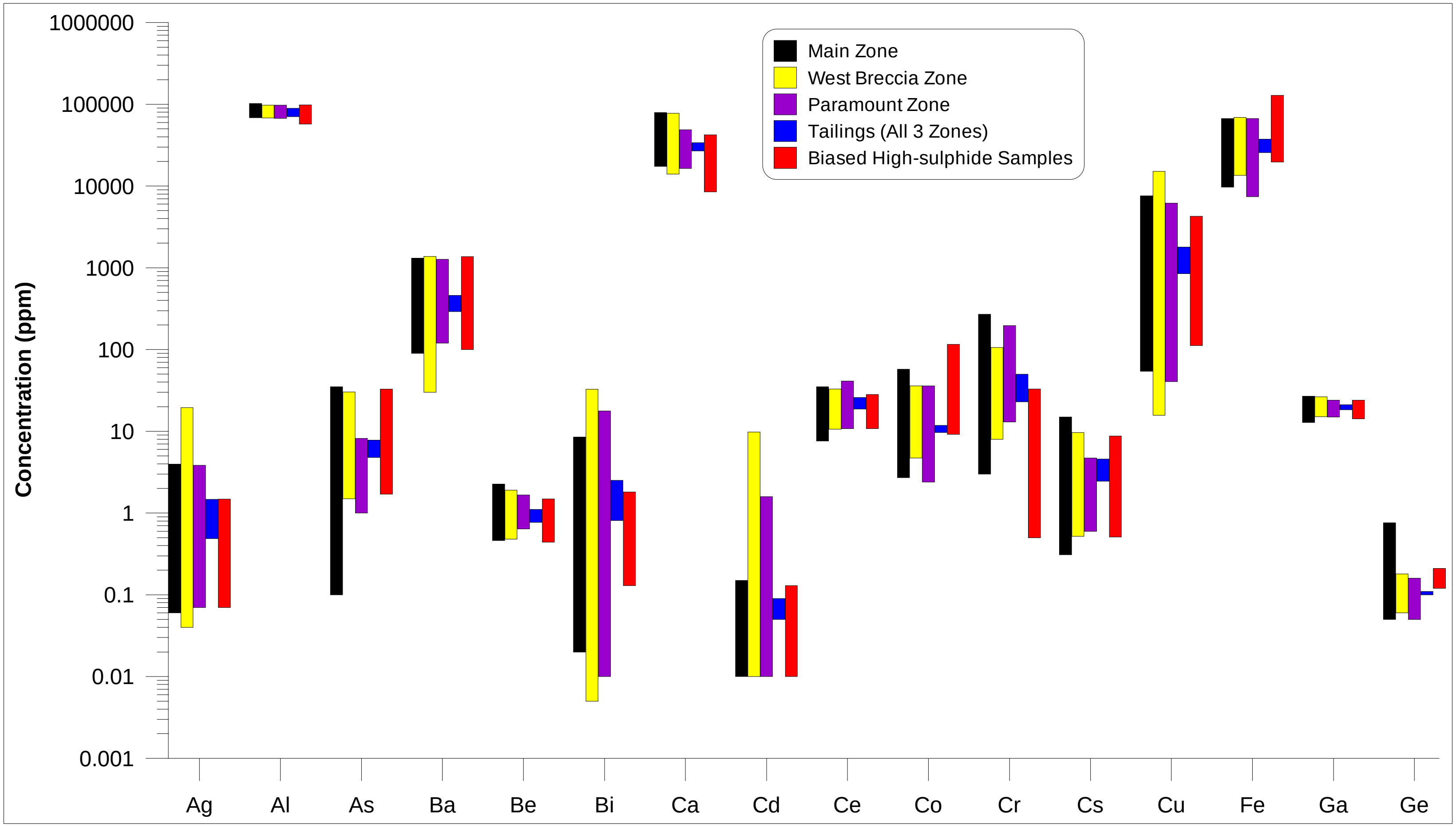


Figure 4-13a. Ranges of Minimum to Maximum Values for Solid-Phase Elements, by Ore Zone, Part 1.

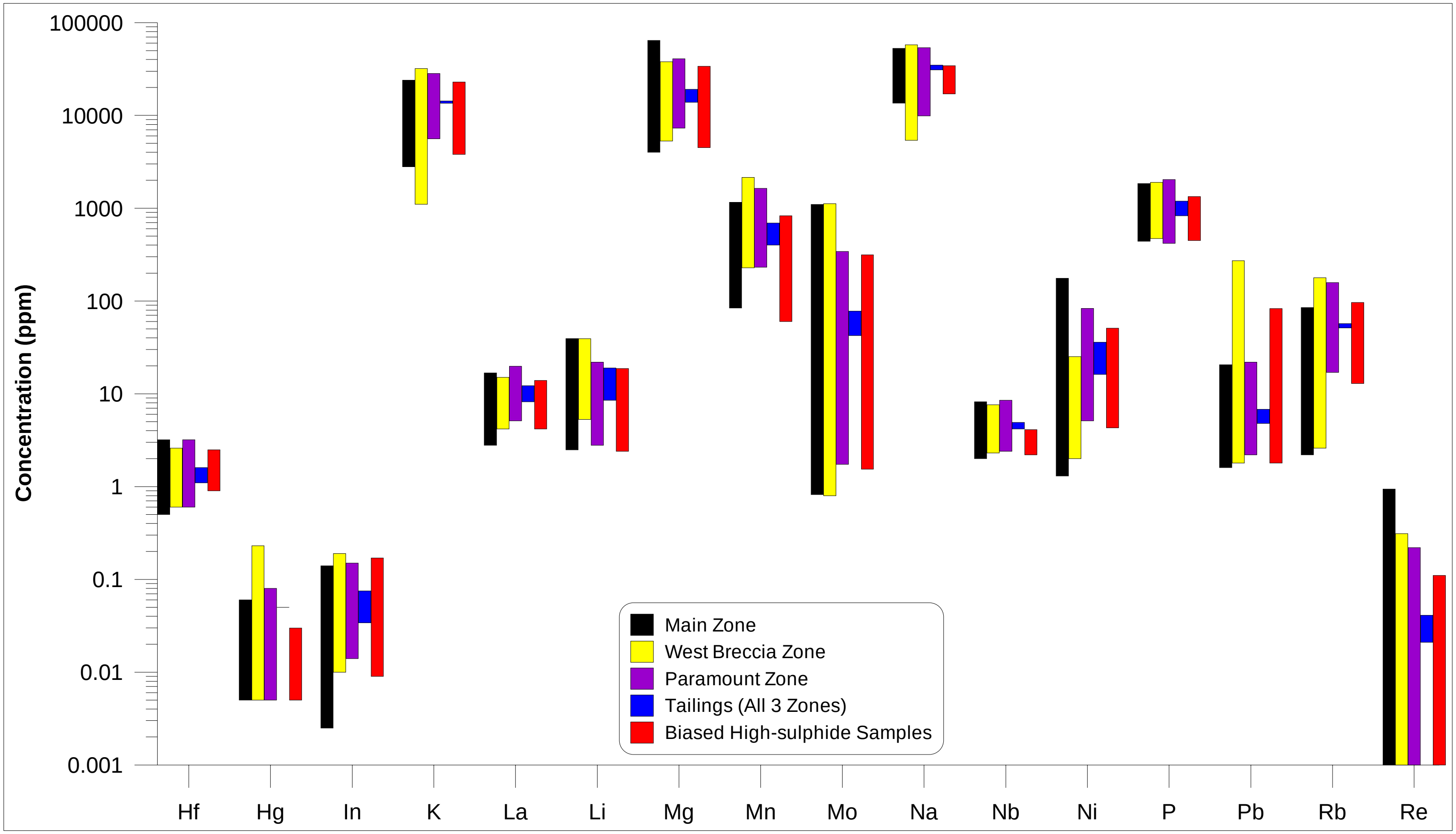


Figure 4-13a. Ranges of Minimum to Maximum Values for Solid-Phase Elements, by Ore Zone, Part 2.

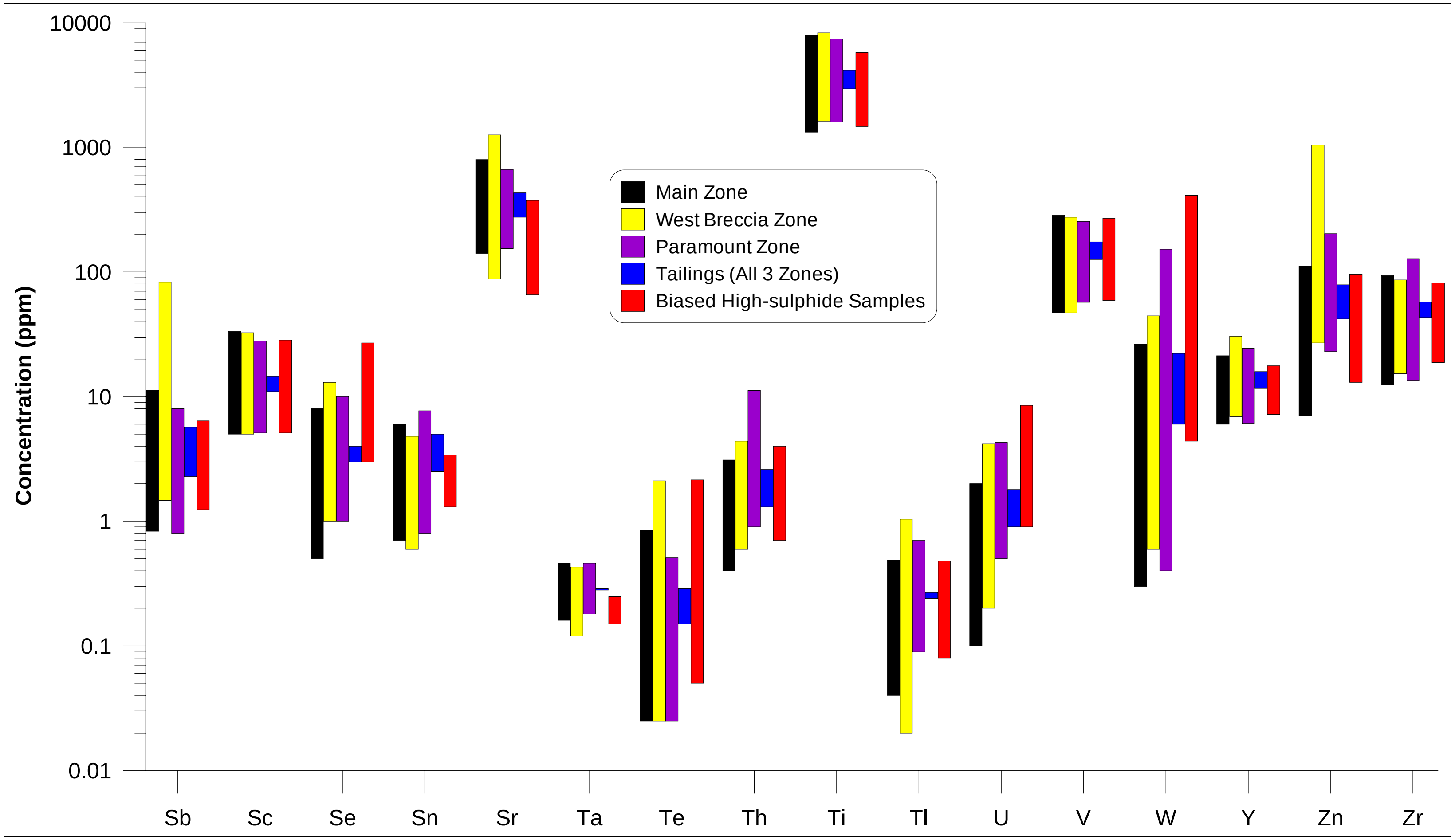
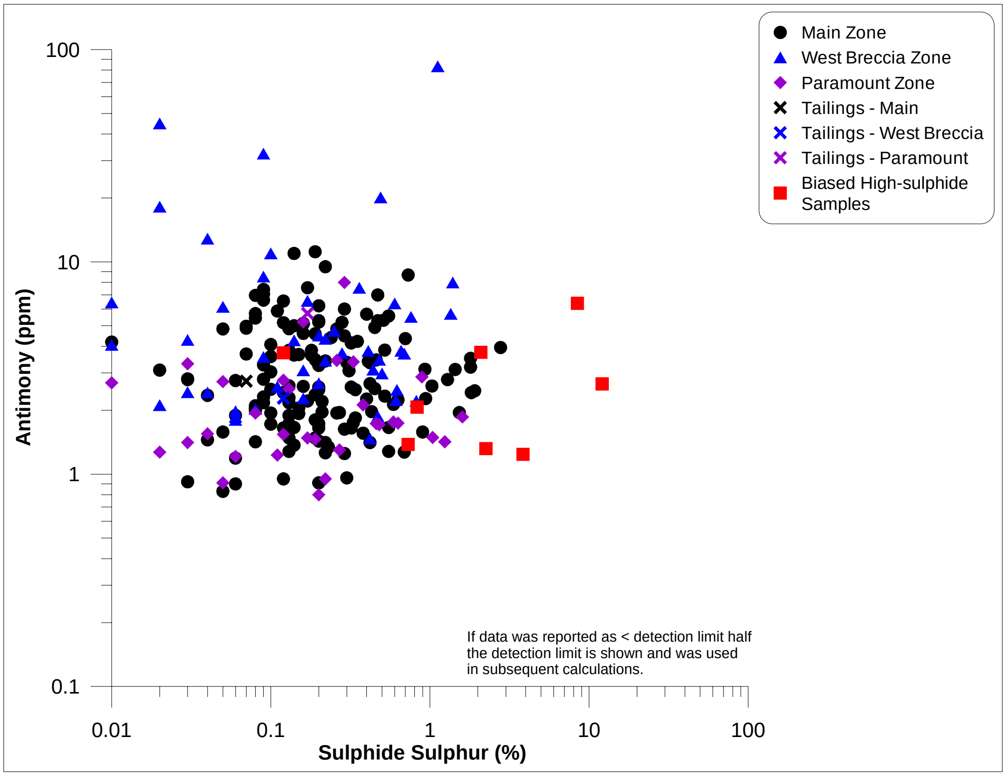
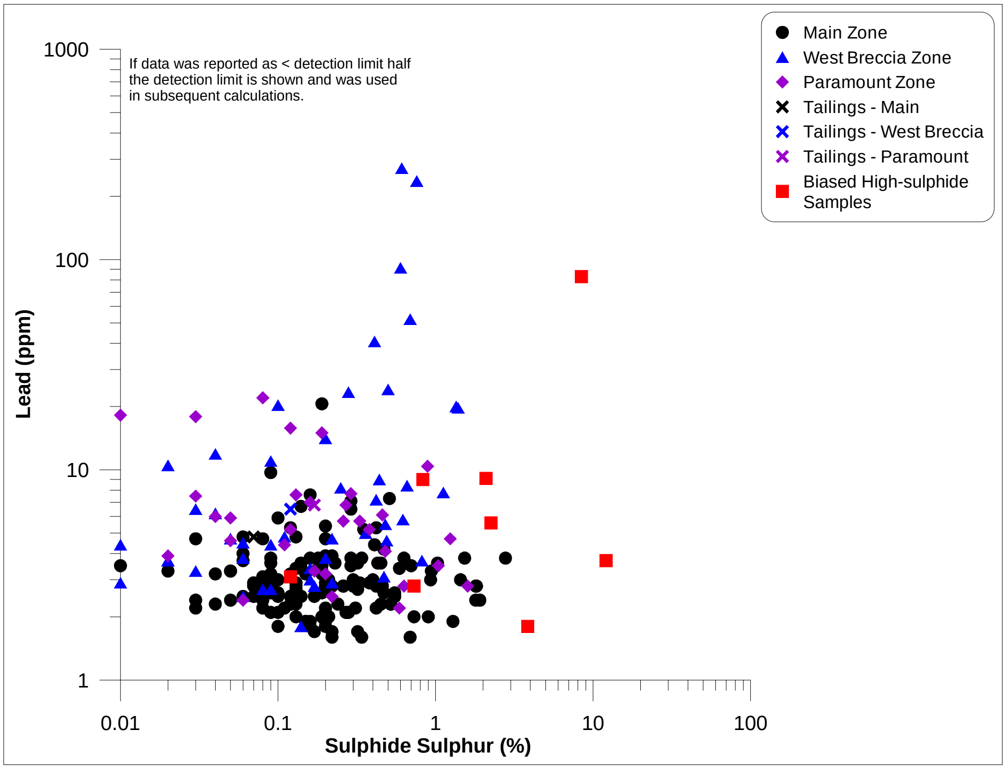


Figure 4-13a. Ranges of Minimum to Maximum Values for Solid-Phase Elements, by Ore Zone, Part 3.



If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

Figure 4-14. Solid-Phase Antimony vs. Sulphide in the Phase 2 ML-ARD Samples, by Ore Zone.



If data was reported as < detection limit half the detection limit is shown and was used in subsequent calculations.

Figure 4-15. Solid-Phase Lead vs. Sulphide in the Phase 2 ML-ARD Samples, by Ore Zone.

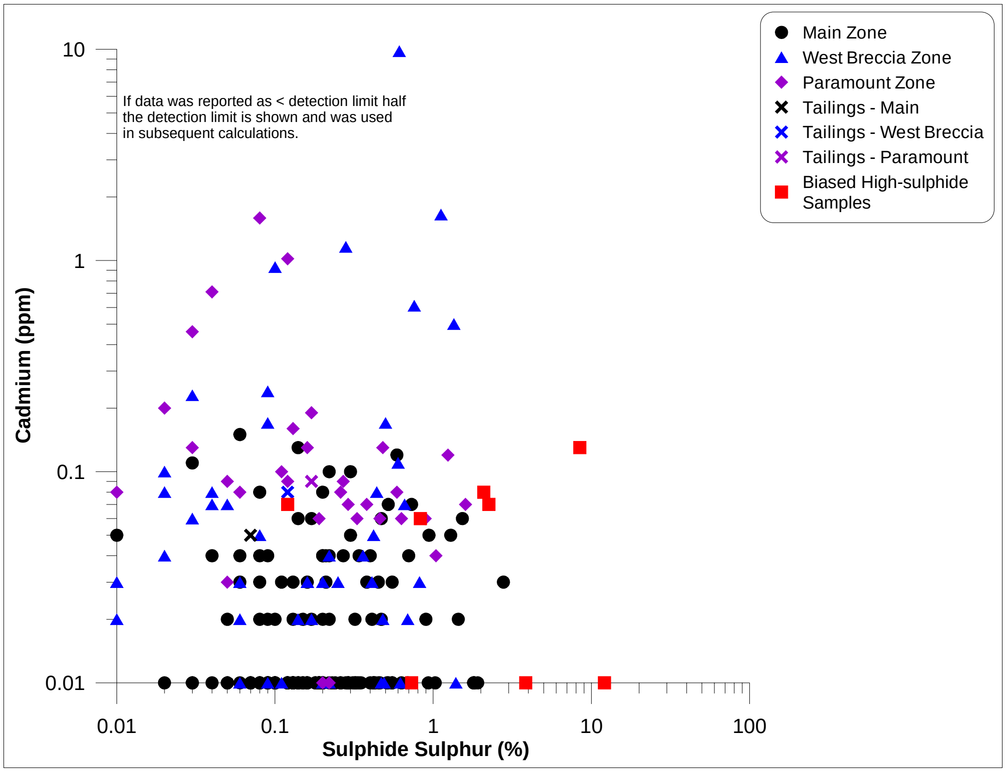


Figure 4-16. Solid-Phase Cadmium vs. Sulphide in the Phase 2 ML-ARD Samples, by Ore Zone.

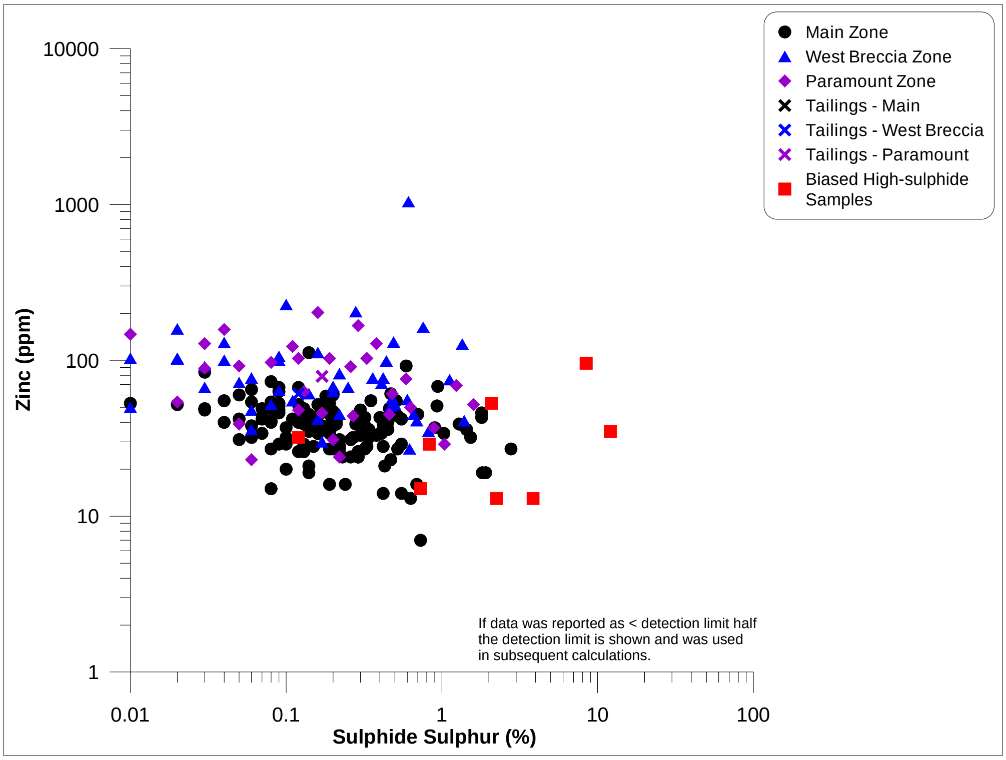


Figure 4-17. Solid-Phase Zinc vs. Sulphide in the Phase 2 ML-ARD Samples, by Ore Zone.

Solid-phase correlations of elements can sometimes reveal mineralogical associations. For example, elements correlating with sulphide presumably occur within the sulphide minerals, which at the Schaft Creek Project are typically pyrite and chalcopyrite (Chapter 2). Correlations with Sobek Neutralization Potential (NP, Section 4.1.3) indicate those elements may be concentrated in certain carbonate and aluminosilicate minerals, which can dissolve even in the absence of sulphide oxidation.

The elements showing some correlation with sulphide were copper and selenium (Figures 4-18 and 4-19), with the highest levels of cobalt and iron also showing some correlation (Figures 4-20 and 4-21). Thus, at least some significant percentage of these elements probably occur within sulphide minerals.

NP showed some correlation with calcium (Figure 4-22). However, as explained in Section 4.1.3, this was not sufficient to distinguish carbonate and non-carbonate calcium-bearing minerals.

In summary, the dominant solid-phase elements in the 235 Phase 2 samples were mostly silicon and aluminum, reflecting the dominance of aluminosilicate minerals in Schaft Creek rock. Compared with average crustal abundances, the samples were frequently elevated in silver, bismuth, copper, molybdenum, selenium, and tungsten; and occasionally to rarely elevated in cadmium, lead, sulphur, antimony, and zinc. These elevated levels do not automatically mean these elements will leach into water at high concentrations, but may instead indicate a general lack of leaching. Minimum-to-maximum ranges of solid-phase elements were similar among the ore zones. However, some samples from the West Breccia Zone contained notably more antimony, lead, cadmium, and zinc. The elements showing some correlation with sulphide, suggesting they were at least partly occurring in/as sulphide minerals, were copper, selenium, cobalt, and iron. Calcium showed some correlation with Sobek Neutralization Potential, reflecting the neutralizing, calcium-bearing, carbonate and non-carbonate minerals in Schaft Creek rock.

4.3 Recommendations for Additional ML-ARD Testwork on Rock

Based on the findings above (Section 4.1 and 4.2) and on the British Columbia ML-ARD documents, the following recommendations are offered.

First, the specific carbonate and sulphide minerals in Schaft Creek rock should be better identified. This has already been done on samples of Schaft Creek tailings (Section 5.2), which showed carbonate was mostly calcite and dolomite, and sulphide was pyrite.

Second, three-dimensional modelling, possibly including geologic, alteration, and/or assay data, should be undertaken by Copper Fox Metals Inc. This should model total sulphur and available NP separately, then locally combine the two to calculate Adjusted TNPR (Section 4.1.4). In this way, the spatial distribution of ARD categories, the year-by-year production of net-acid-generating and net-neutralizing rock, and the potential to segregate ARD rock during routine mining can be assessed. This may require additional ABA analyses, at the discretion of the modeller.

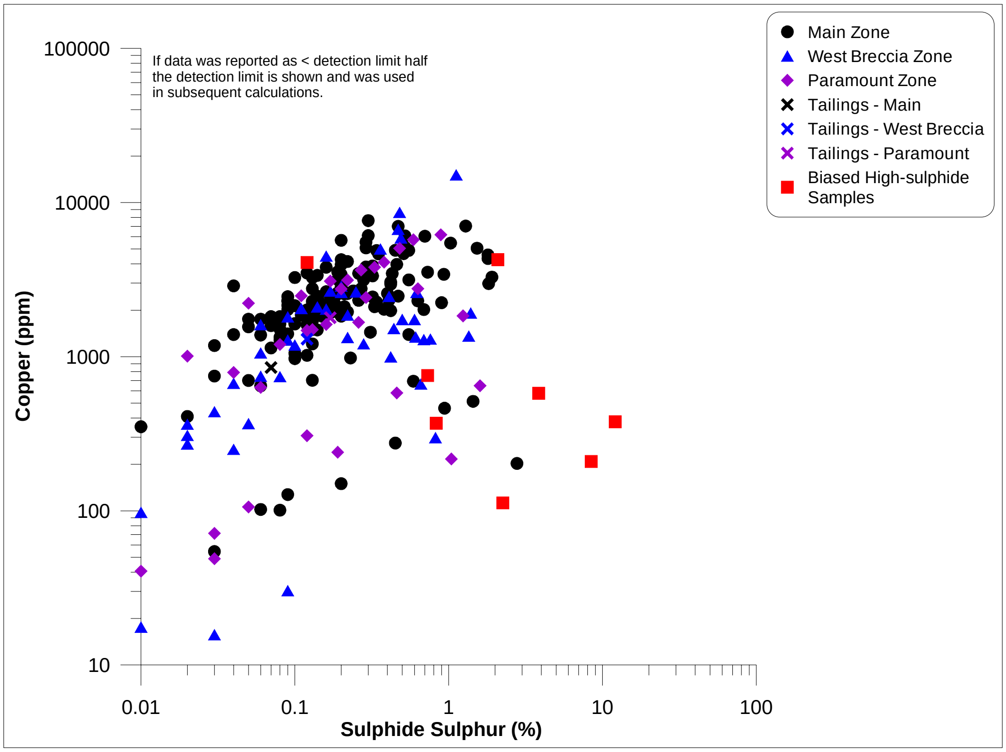


Figure 4-18. Solid-Phase Copper vs. Sulphide in the Phase 2 ML-ARD Samples, by Ore Zone.

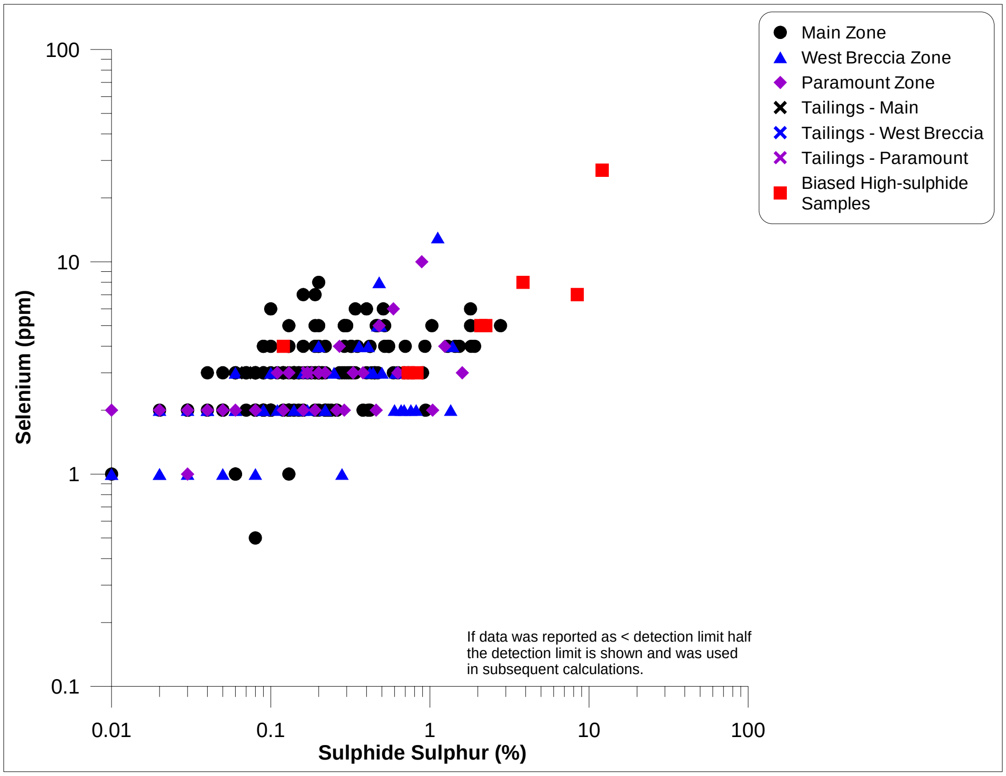


Figure 4-19. Solid-Phase Selenium vs. Sulphide in the Phase 2 ML-ARD Samples, by Ore Zone.

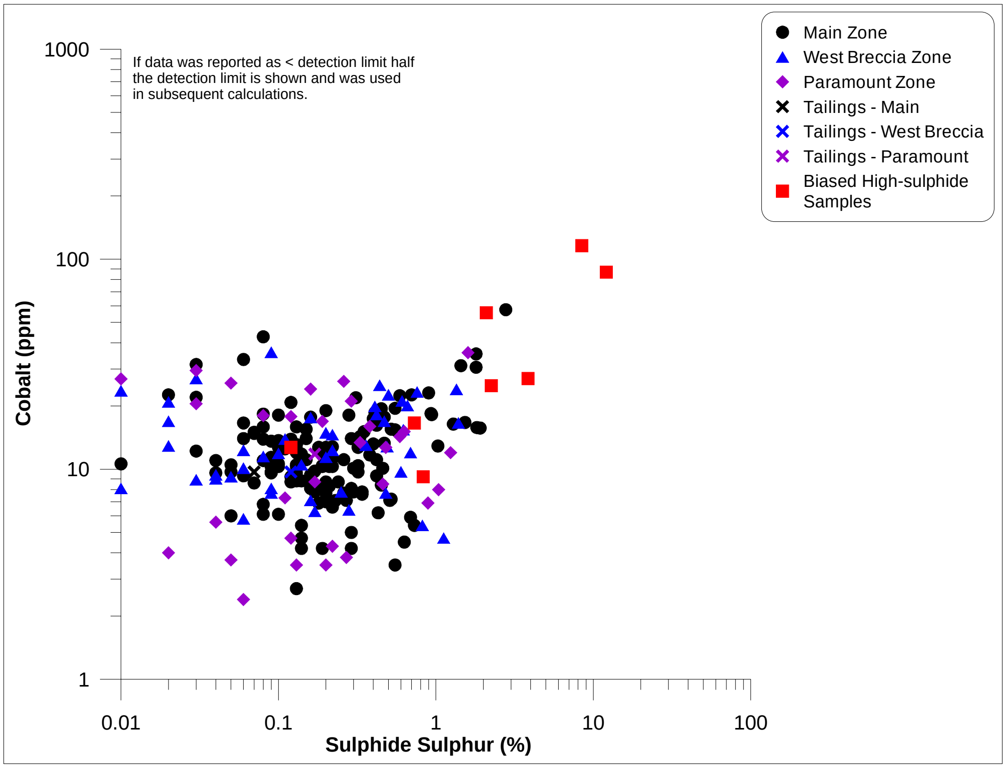


Figure 4-20. Solid-Phase Cobalt vs. Sulphide in the Phase 2 ML-ARD Samples, by Ore Zone.

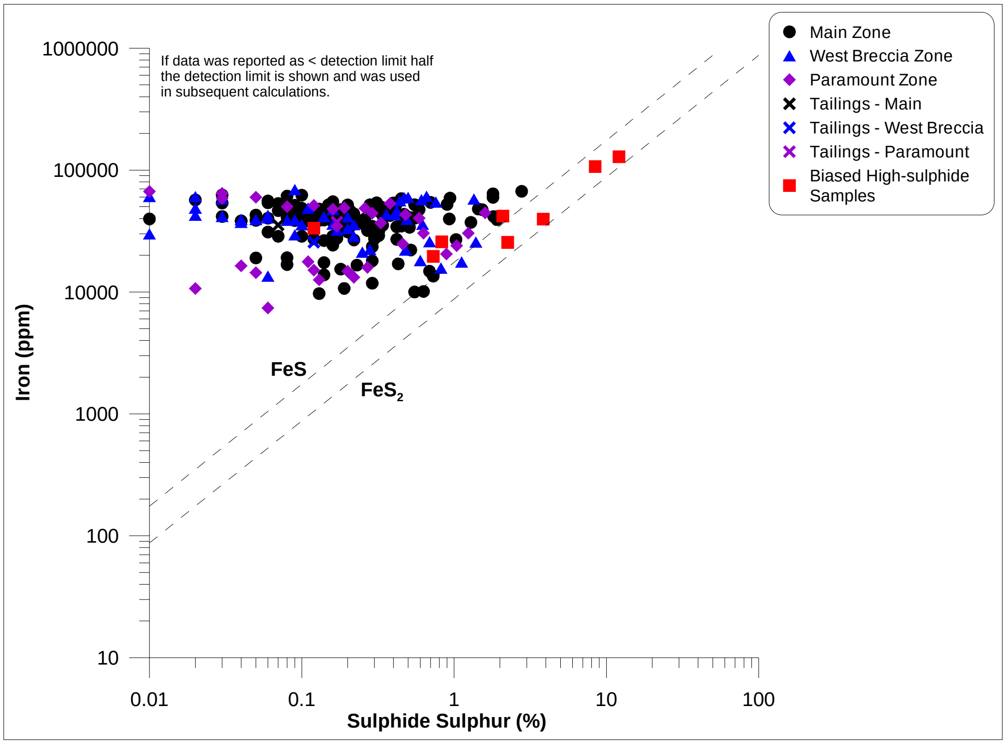


Figure 4-21. Solid-Phase Iron vs. Sulphide in the Phase 2 ML-ARD Samples, by Ore Zone.

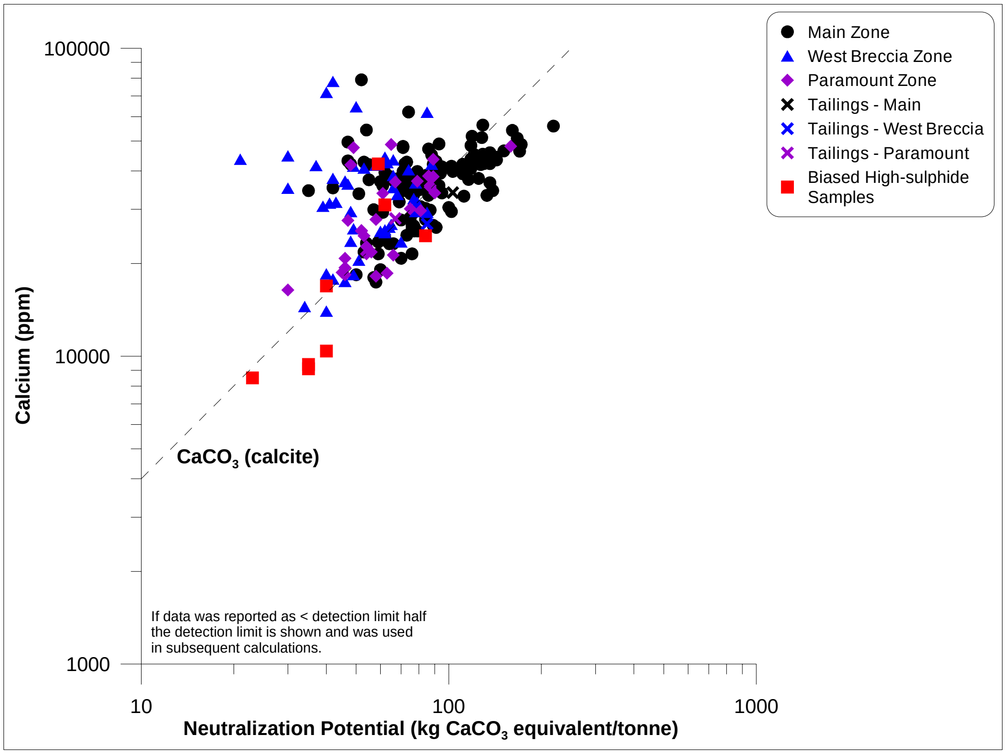


Figure 4-22. Solid-Phase Calcium vs. Sobek Neutralization Potential in the Phase 2 ML-ARD Samples, by Ore Zone.

Third, laboratory-based humidity cells should be initiated on various types and ARD categories of Schaft Creek rock. These will provide bulk reaction rates under standardized conditions, to allow scaling of rates to full-scale conditions. Such cells have already been started for Schaft Creek tailings (Section 5.2).

Fourth, on-site leach tests should be started after spring thaw in 2008. These tests, with hundreds of kilograms, will provide data for full-scale equilibrium conditions.

5. ML-ARD RESULTS FOR TAILINGS

As explained in Chapter 3, metallurgical testing of ore from the three ore zones at the Schaft Creek Project has produced one solid-phase tailings sample and supernatant (water) analyses for each ore zone, namely Main (Liard), West Breccia, and Paramount (Chapter 2). The tailings solid samples have been subjected to the ML-ARD testing described in Section 3.2, as well as laboratory-based kinetic testing. These are discussed in this chapter. The supernatant analyses are also discussed here.

5.1 Tailings Supernatant

As part of metallurgical testing for the Schaft Creek Project in 2007, the aqueous phase mixed with the tailings solids (the "supernatant") was separated from the solids, sampled periodically, and analyzed (Rescan Environmental Services, personal communication). For each ore zone, the supernatant was periodically sampled up to two hours for subsequent laboratory analysis (Appendix B), to reflect short-term aging. Sampling over longer-aging times has also been conducted, but those results are not yet available.

Overall, the supernatants were near-neutral calcium-sodium-potassium-sulphate waters (Appendix B). Alkalinity was relatively low, indicating relative low pH-buffering capacity, but greater than acidity.

These supernatants represent the best available prediction of mill-effluent water chemistry that will enter the Schaft Creek tailings impoundment. If this effluent is the dominant inflow, then the tailings-pond chemistry can be predicted from the supernatant chemistry. If other inflows are significant, like background runoff or drainage from exposed tailings beaches, then the tailings-pond chemistry may not resemble the supernatant chemistry. Large-scale modelling for the environmental assessment will address this later.

Furthermore, full-scale mill-effluent chemistry may differ from Appendix B for several reasons. For example, blasting residue on the ore may increase nitrogen-species concentrations above those in Appendix B. Also, long-term recirculation of tailings-pond water to the mill could result in rising levels of all species and elements, including sulphate and chloride. Again, large-scale modelling for the environmental assessment will address this later.

5.2 Tailings Solids

5.2.1 Tailings Acid-Base Accounting and Total Elements

The tailings solids were analyzed by the same methods as rock (Section 3.2). In fact, the results of the tailings solids were included in the interpretations of rock (Chapter 4), because the tailings solids did not produce any unusual results compared with the unprocessed rock.

Based on acid-base accounting (ABA, Section 4.1 and Appendix A), the paste pH of tailings from all three zones was near neutral between 8.1 and 8.4. Total sulphur was relatively low in the three tailings samples, and ranged from 0.08 to 0.20%S (Table 5-1). Compared with the rock samples from the three ore zones, the three tailings samples contained relatively low sulphur and relatively high Sobek Neutralization Potential. Thus, like most of the rock samples, all three tailings samples were net neutralizing.

Based on total-element analyses, the three tailings samples were composed mostly of silicon and aluminum (Appendix A), reflecting the dominance of aluminosilicate minerals. Compared with average crustal abundances, the three tailings samples were consistently elevated in silver, bismuth, copper, and selenium. Additionally, West Breccia tailings were elevated in antimony and tungsten, and Paramount tailings were also elevated in tungsten. Removal of copper resulted in residual copper below the rock-core mean and median copper for the Main and Paramount tailings (Table 5-1).

Quantitative mineralogy of the three tailings samples was determined by Rietveld x-ray diffraction (XRD, Appendix C). Visual petrographic examinations were not made, due to the fine-grained nature of the samples. The three tailings samples had particle-surface areas of 200-250 m^2/kg, were ~60% less than 0.3 µm in size, and were ~40% less than 0.04 µm.

As explained in Chapter 2 and inferred in Section 4.2, aluminosilicate minerals are dominant in Schaft Creek rock. This was confirmed quantitatively for these tailings samples, with 43-50 wt-% plagioclase, 17-24 wt-% quartz, 12-17 wt-% muscovite, and 9-11 wt-% clinochlore (Table 5-2). The most abundant carbonate mineral was calcite, with dolomite second in abundance. No significant amounts of less-neutralizing, iron-bearing forms of carbonate were identified. Pyrite was the only identified sulphide mineral, and this was only seen in the West Breccia tailings sample because of the generally low sulphide levels (Table 5-1).

Table 5-1. Summary of ML-ARD Characteristics for Phase 2 Tailings (data from Appendix A)

Sample	Total Sulphur (%S)	Sulphide (%S)	HCl-Leachable Sulphate (%S)	Sobek NP (kg/t)	Adjusted TNPR	Cu (ppm)
Main (Liard) Zone						
Tailings[1]	0.08	0.07	<0.01	103	37.2	850
Rock Mean[1]	0.37	0.33	0.02	90.4	14.8	2543
Rock Median[1]	0.21	0.19	<0.01	74.5	10.8	2245
West Breccia Zone						
Tailings[1]	0.20	0.17	0.02	67	9.12	1790
Rock Mean[1]	0.41	0.32	0.06	54.9	12.5	2077
Rock Median[1]	0.25	0.20	0.02	50	6.29	1340
Paramount Zone						
Tailings[1]	0.17	0.12	0.04	85	14.1	1300
Rock Mean[1]	0.36	0.33	0.03	65.7	16.9	1980
Rock Median[1]	0.24	0.19	0.01	58	8.15	1620

[1] Tailings sample was a single sample from the specified zone; Rock Mean and Median were based on all rock-core samples from the specified zone.

Table 5-2. X-Ray-Diffraction Mineralogy of the Three Tailings Samples (from Appendix C)

		Solid-Phase Levels in Weight-Percent		
Mineral	Ideal Formula	Main (Liard)	West Breccia	Paramount
Plagioclase	$NaAlSi_3O_8$ - $CaAl_2Si_2O_8$	42.7	49.5	44.7
Quartz	SiO_2	17.3	16.6	23.9
Muscovite	$KAl_2AlSi_3O_{10}(OH)_2$	16.9	12.2	14.1
Clinochlore	$(Mg,Fe^{2+})_5Al(Si_3Al)O_{10}(OH)_8$	11.1	10.7	9.0
Calcite	$CaCO_3$	6.4	4.5	5.5
Dolomite	$CaMg(CO_3)_2$	2.7	0.7	2.7
K-feldspar	$KAlSi_3O_8$	1.5	4.5	-
Hematite	α-Fe_2O_3	0.8	-	-
Magnetite	Fe_3O_4	0.5	0.8	-
Pyrite	FeS_2	-	0.4	-

5.2.2 Tailings Kinetic Testing

At this time, subsamples of the three tailings samples discussed in Section 5.2.1 have been operating in laboratory-based well-flushed, well-aerated humidity cells for 13 weeks. The procedure for these humidity cells was discussed in Section 3.2.

The three tailings cells have remained near neutral to date (Figure 5-1), with the Main tailings showing the greatest variability to date. All three samples are expected to remain near neutral indefinitely based on their ABA (Section 5.2.1).

Sulphate production rate typically represents the rate of sulphide oxidation and total-acidity generation. The temporal trends in sulphate rates from the three cells showed two tailings cells (West Breccia and Paramount) have been generally steady around a definable range in recent weeks (Figure 5-2). In contrast, the sulphate rate in the Main tailings dropped to notably low levels, almost two orders of magnitude lower than the other two tailings cells, but then recovered on the last available week. Often months of testing are required to identify long-term geochemical stability, so these initial results should not be used as long-term predictions.

The rate of sulphide oxidation can affect some rates of dissolution and leaching. At this early stage, the rates showing some correlation with sulphate production included alkalinity (and thus Neutralization-Potential (NP) dissolution), antimony, barium, calcium, copper, magnesium, manganese, potassium, silicon, and strontium. Some of these elements, like copper, probably relate directly to sulphide oxidation (Section 4.2), whereas other like calcium and potassium probably relate to NP dissolution driven by sulphide oxidation. However, at this early stage of testing, detailed interpretations are not yet warranted.

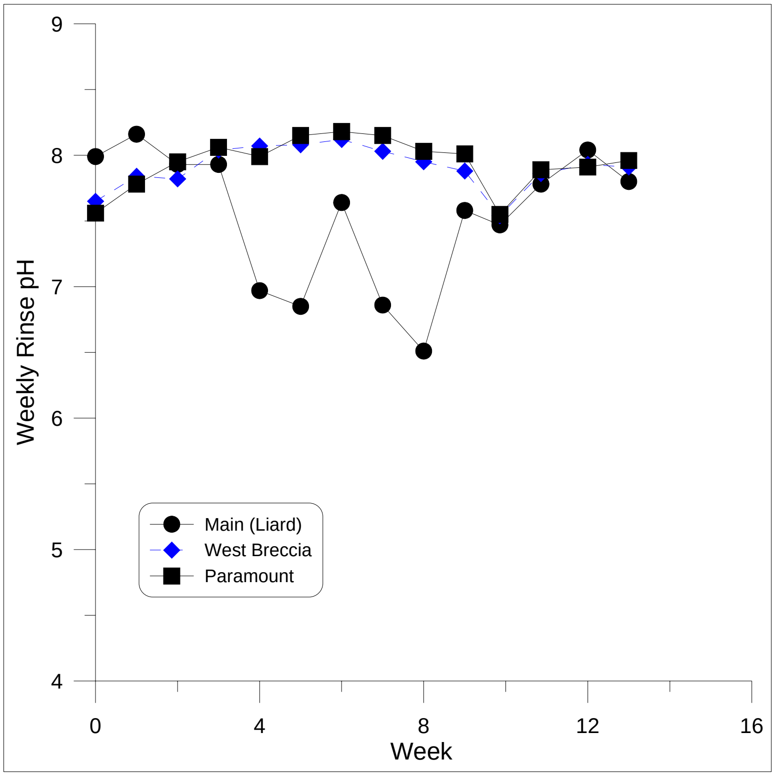


Figure 5-1. Temporal Trend of Rinse pH from the Three Tailings Humidity Cells.

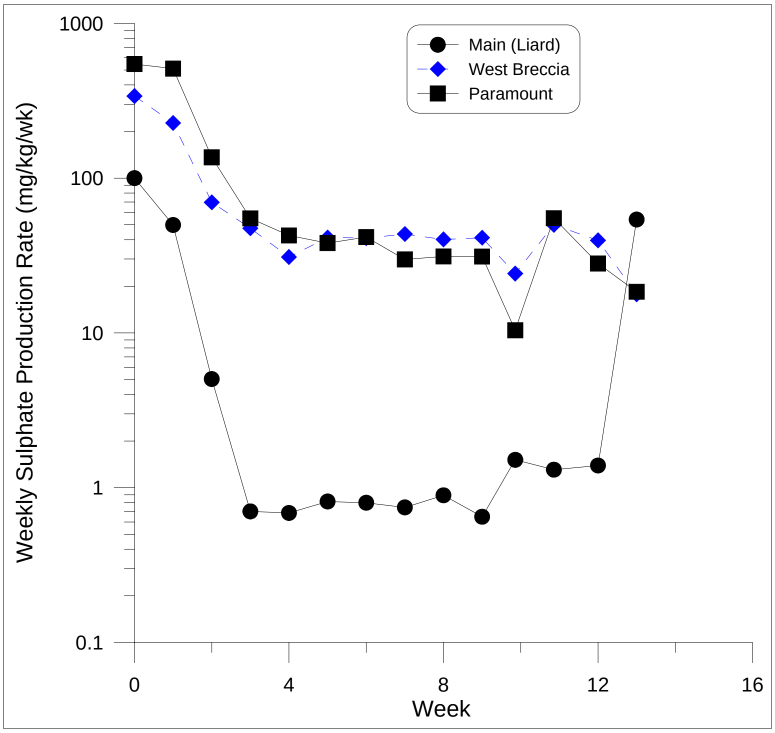


Figure 5-2. Temporal Trend of Sulphate Production Rate from the Three Tailings Humidity Cells.

6. CONCLUSION

For metal leaching (ML) and acid rock drainage (ARD), this Phase 2 report for the Schaft Creek Project has built on, and greatly expanded, the findings of the Phase 1 study. This work continues to follow the recommendations in the provincial ML-ARD Policy, Guidelines, and draft Prediction Manual.

Relevant Observations from Existing Information

The compilation of existing information relevant to ML-ARD produced the following important observations.

First, the Schaft Creek copper-gold-molybdenum deposit is widely acknowledged as being a porphyry copper deposit, containing three mineral zones: Main (or Liard), West Breccia, and Paramount Zones.

Second, visual examinations of exposed core up to several decades old showed limited weathering, suggesting the oxidation rate of Schaft Creek rock may be relatively slow.

Third, 16 acid-base accounts from a previous, metallurgical study showed all 16 samples were net acid neutralizing, with sulphide between 0.1 and 0.9%S, and Neutralization Potentials from 53 to 114 kg/t.

Fourth, detailed mineralogy of 18 thin sections of selected rock units showed that the fine-grained groundmass was generally around one-half of the total, with the groundmass consisting of more than 90% feldspar, and accessory amounts of quartz, chlorite, sericite, carbonate, opaques. Sulphide minerals were mostly disseminated and as veinlets and clusters, and were mostly pyrite and chalcopyrite with less common molybdenite and bornite. Carbonate minerals, mostly reported as veins, patches, and groundmass, were not individually identified, and were sometimes seen as feldspar replacement/alteration.

Phase 2 Samples and Analyses

In total, 232 samples of rock from core were collected and analyzed, generally reflecting the abundances of the rock units. Also, three samples of tailings, with one each from the three ore zones, were collected and analyzed, for a total of 235 samples. All samples were analyzed for U.S. EPA-600-compliant, Sobek expanded acid-base accounting (ABA) and total-element contents based on ICP-MS after four-acid digestion and on x-ray-fluorescence whole rock. Selected samples were analyzed for mineralogy by Rietveld x-ray diffraction and for bulk reaction rates by kinetic humidity cells.

Results of Acid-Base Accounting (ABA)

As part of the ABA procedure, paste pH showed no samples were acidic at the time of analysis, with values ranging from 7.4 to 9.2. Total sulphur in the 235 Schaft Creek samples of rock and tailings ranged from 0.01 (detection limit) to 13.5%S, with a mean of 0.50%S and a median of

0.22%S. Several total-sulphur statistics were similar for all three ore zones. Most of the total sulphur was composed of sulphide, and thus the two parameters were generally interchangeable. Approximately 5-10% of the samples had sulphur-species analyses within the relatively unreliable range below roughly 0.05%S. The MOE-recommended approach of using total sulphur and the associated Total-Sulphur-Based Acid Potential (TAP) was used here. This recognizes that TAP tends to overestimate actual acid potential, often by a small amount, and may be changed in Phase 3 studies based on additional work.

Sobek (EPA 600) Neutralization Potential (NP) ranged from 21 to 219 kg/t in the 235 Schaft Creek samples of rock and tailings, with a mean of 79 and a median of 75 kg/t. These relatively high values explained why no acidic paste pH values were detected. They also suggested there could be a long lag time (years to decades) before any sample might become acidic.

Most total carbon was composed of potentially acid-neutralizing inorganic carbonate. However, the comparison of NP to inorganic carbonate showed some important trends. First, Sobek NP was typically up to 1.5 times higher, meaning non-carbonate minerals apparently contributed to neutralization. Second, below a Sobek NP of 40-50 kg/t, NP frequently exceeded Inorganic CaNP by more than a factor of 1.5. This showed non-carbonate minerals represented a higher proportion of NP as NP decreased below 40-50 kg/t. Third, around an NP of 60-90 kg/t, a distinct trend of increasing Inorganic CaNP greater than NP was seen, particularly for the Main Zone. This may reflect different carbonate minerals in different parts of the Main Zone, but three-dimensional modelling would be needed to assess this further. In any case, Sobek NP was still considered the better measure of neutralizing capacity than Inorganic CaNP.

The lack of correlations with solid-phase calcium and calcium+magnesium meant that the form of the inorganic carbonate could not be inferred. However, some correlation of Sobek NP and calcium probably reflected a calcium-bearing combination of carbonate and non-carbonate minerals.

Net balances of acid-generating and acid-neutralizing capacities for the 235 Phase 2 samples of rock and tailings were based on (1) total sulphur and the resulting Total Acid Potential (TAP) and (2) Sobek Neutralization Potential after Unavailable NP estimated at 10 kg/t was subtracted. This was called, “Adjusted TNPR”. These net balances showed that approximately 90% was net neutralizing indefinitely, 4% was net acid generating although not yet acidic, and 6% was uncertain until further testing. A sensitivity analysis showed these percentages did not change significantly when (1) total sulphur was replaced by sulphide plus unaccounted-for sulphur or (2) all measured NP was considered fully reactive and available (Unavailable NP = 0). By ore zone, the Main (Liard) Zone had the highest percentage of net-neutralizing samples (96%), and the West Breccia Zone the lowest (81%). The correlation of Adjusted TNPR with total sulphur showed that samples: with more than 2.1%S were consistently net acid generating; with less than 0.5%S were consistently net neutralizing; and between 0.5 and 2.1%S could fall into any ML-ARD category depending on NP.

Results of Total-Element Contents

The dominant solid-phase elements in the 235 Phase 2 samples were mostly silicon and aluminum, reflecting the dominance of aluminosilicate minerals in Schaft Creek rock. Compared with average crustal abundances, the samples were frequently elevated in silver, bismuth, copper, molybdenum, selenium, and tungsten; and occasionally to rarely elevated in cadmium, lead, sulphur, antimony, and zinc. These elevated levels do not automatically mean these elements will leach into water at high concentrations, but may instead indicate a general lack of leaching.

Minimum-to-maximum ranges of solid-phase elements were similar among the ore zones. However, some samples from the West Breccia Zone contained notably more antimony, lead, cadmium, and zinc.

The elements showing some correlation with sulphide, suggesting they were at least partly occurring in/as sulphide minerals, were copper, selenium, cobalt, and iron. Calcium showed some correlation with Sobek Neutralization Potential, reflecting the neutralizing, calcium-bearing, carbonate and non-carbonate minerals in Schaft Creek rock.

Additional Analyses of Tailings

Metallurgical testing of ore from the three ore zones at the Schaft Creek Project has produced one solid-phase tailings sample and supernatant (water) analyses for each ore zone, namely Main (Liard), West Breccia, and Paramount.

Overall, the supernatants were near-neutral calcium-sodium-potassium-sulphate waters. Alkalinity was relatively low, indicating relative low pH-buffering capacity, but greater than acidity. These supernatants represent the best available prediction of mill-effluent water chemistry that will enter the Schaft Creek tailings impoundment. If this effluent is the dominant inflow, then the tailings-pond chemistry can be predicted from the supernatant chemistry. If other inflows are significant, like background runoff or drainage from exposed tailings beaches, then the tailings-pond chemistry may not resemble the supernatant chemistry. Large-scale modelling for the environmental assessment will address this later.

Based on acid-base accounting (ABA), the paste pH of the tailings solids from all three zones was near neutral between 8.1 and 8.4. Total sulphur was relatively low, ranging from 0.08 to 0.20%S. Compared with the rock samples from the three ore zones, the three tailings samples contained relatively low sulphur and relatively high Sobek Neutralization Potential. Thus, like most of the rock samples, all three tailings samples were net neutralizing.

Based on total-element analyses, the three tailings samples were composed mostly of silicon and aluminum, reflecting the dominance of aluminosilicate minerals. Compared with average crustal abundances, the three tailings samples were consistently elevated in silver, bismuth, copper, and selenium. Additionally, West Breccia tailings were elevated in antimony and tungsten, and Paramount tailings were also elevated in tungsten. Removal of copper resulted in residual copper below the rock-core mean and median copper for the Main and Paramount tailings.

Quantitative mineralogy of the three tailings samples was determined by Rietveld x-ray diffraction. As expected, aluminosilicate minerals were dominant in these Schaft Creek tailings, with 43-50 wt-% plagioclase, 17-24 wt-% quartz, 12-17 wt-% muscovite, and 9-11 wt-%

clinochlore. The most abundant carbonate mineral was calcite, with dolomite second in abundance. No significant amounts of less-neutralizing, iron-bearing forms of carbonate were identified. Pyrite was the only identified sulphide mineral, and this was only seen in the West Breccia tailings sample because of the generally low sulphide levels.

To date, only 13 weeks of humidity-cell weekly humidity-cell analyses are available. These analyses showed the three tailings cells have remained near neutral to date, with the Main tailings showing the greatest variability to date. All three samples are expected to remain near neutral indefinitely based on their ABA. Sulphate production rate typically represents the rate of sulphide oxidation and total-acidity generation. The temporal trends in sulphate rates from the three cells showed two tailings cells (West Breccia and Paramount) have been generally steady around a definable range in recent weeks. In contrast, the sulphate rate in the Main tailings dropped to notably low levels, almost two orders of magnitude lower than the other two tailings cells, but then recovered on the last available week. Often months of testing are required to identify long-term geochemical stability, so these initial results should not be used as long-term predictions.

In humidity cells, the rate of sulphide oxidation can affect some rates of dissolution and leaching. At this early stage, the tailings rates showing some correlation with sulphate production included alkalinity (and thus Neutralization-Potential (NP) dissolution), antimony, barium, calcium, copper, magnesium, manganese, potassium, silicon, and strontium. Some of these elements, like copper, probably relate directly to sulphide oxidation, whereas other like calcium and potassium probably relate to NP dissolution driven by sulphide oxidation. However, at this early stage of testing, detailed interpretations are not yet warranted.

Recommendations

Based on the findings above and on the British Columbia ML-ARD documents, the following recommendations are offered.

First, the specific carbonate and sulphide minerals in Schaft Creek rock should be better identified. This has already been done on samples of Schaft Creek tailings, which showed carbonate was mostly calcite and dolomite, and sulphide was pyrite.

Second, three-dimensional modelling, possibly including geologic, alteration, and/or assay data, should be undertaken by Copper Fox Metals Inc. This should model total sulphur and available NP separately, then locally combine the two to calculate Adjusted TNPR. In this way, the spatial distribution of ARD categories, the year-by-year production of net-acid-generating and net-neutralizing rock, and the potential to segregate ARD rock during routine mining can be assessed. This may require additional ABA analyses, at the discretion of the modeller.

Third, laboratory-based humidity cells should be initiated on various types and ARD categories of Schaft Creek rock. These will provide bulk reaction rates under standardized conditions, to allow scaling of rates to full-scale conditions. Such cells have already been started for Schaft Creek tailings.

Fourth, on-site leach tests should be started after spring thaw in 2008. These tests, with hundreds of kilograms, will provide data for full-scale equilibrium conditions.

7. REFERENCES

Associated Mining Consultants Ltd. 2004. Preliminary Assessment of the Schaft Creek Deposit, British Columbia Project Status Report No. 1. Prepared for 955528 (Alberta) Ltd., dated September 20.

Copper Fox Metals Inc. 2006. Schaft Creek Copper-Gold-Molybdenum-Silver Deposit Project Description. Dated July 2006.

Ewanchuk, S., P. Fischer, W. Hanych. 2007. 2006 Diamond Drill Report Schaft Creek Property Northwestern British Columbia For Copper Fox Metals Inc. Final Report. Report dated March 19, 2007.

Fischer, P., and W. Hanych. 2006. 2005 Diamond Drill Report Schaft Creek Property Northwestern British Columbia for Copper Fox Metals Inc. Dated March 27.

Giroux, G.H., and E.A. Ostensoe. 2003. Summary Report Status and Resources Estimate Schaft Creek Property Northwestern British Columbia. Prepared for 955528 Alberta Ltd., dated June 30.

Morin, K.A., and N.M. Hutt. 2007a. Schaft Creek Project - Prediction of Metal Leaching and Acid Rock Drainage, Phase 1. Report for Rescan Environmental Services Ltd., dated August 10.

Morin, K.A., and N.M. Hutt. 2007b. Scaling and Equilibrium Concentrations in Minesite-Drainage Chemistry. MDAG.com Internet Case Study 26, at www.mdag.com/case_studies/cs26.html.

Morin, K.A., and N.M. Hutt. 2006. Is There a Solid-Phase Sulphide Level Below Which No ARD Is Possible? MDAG Internet Case Study #21, www.mdag.com/case_studies/cs21.html.

Morin, K.A., and N.M. Hutt. 2001. *Environmental Geochemistry of Minesite Drainage: Practical Theory and Case Studies, Digital Edition*. MDAG Publishing (www.mdag.com), Surrey, British Columbia. ISBN: 0-9682039-1-4.

Morin, K.A., and N.M. Hutt. 1997. *Environmental Geochemistry of Minesite Drainage: Practical Theory and Case Studies*. MDAG Publishing (www.mdag.com), Surrey, British Columbia. ISBN: 0-9682039-0-6.

Price, W.A., K.A. Morin, N.M. Hutt. 1997. Guidelines for the prediction of acid rock drainage and metal leaching for mines in British Columbia: Part II. Recommended procedures for static and kinetic testing. IN: Proceedings of the Fourth International Conference on Acid Rock Drainage, May 31-June 6, Vancouver, Canada, Volume I, p. 15-30.

Price, W.A., and J.C. Errington. 1998. Guidelines for Metal Leaching and Acid Rock Drainage at Minesites in British Columbia. Issued by the British Columbia Ministry of Energy and Mines.

Price, W.A. 1998. Draft Manual for the Prediction of Metal Leaching and Acid Rock Drainage. Issued by the British Columbia Ministry of Energy and Mines.

Sobek, A.A., W.A. Schuller, J.R. Freeman, and R.M. Smith. 1978. Field and Laboratory Methods Applicable to Overburdens and Minesoils. Report EPA-600/2-78-054, U.S. National Technical Information Report PB-280 495. 403 p.

APPENDIX A. Compiled ML-ARD Analyses of Schaft Creek Rock and Tailings

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.
UTM NAD 27 was used for Northing and Easting data

									Top of Drillholes UTM NAD 27							For Easting Plots Centre of ABA Interval			For Northing Plots Centre of ABA Interval		
Sample Id.	Hole Id	From (m)	To (m)	Interval (m)	Centre of Interval (m)	Old Collar	Ore Zone	Zone	Easting	Northing	Elevation (m)	Azimuth	Inclination	Length (m)	Length (ft)	Easting	Northing	Elevation	Easting	Northing	Elevation
Main Zone																					
14130	05CF236	18.2	21.2	3.03	19.70	H83	Liard Main	9	380049	6359367	935.7	0	-90	171.3	562	380049	6359367	916.0	380049	6359367	916.0
14144	05CF236	60.6	63.6	3.03	62.12	H83	Liard Main	9	380049	6359367	935.7	0	-90	171.3	562	380049	6359367	873.6	380049	6359367	873.6
14148	05CF236	72.7	75.8	3.03	74.24	H83	Liard Main	9	380049	6359367	935.7	0	-90	171.3	562	380049	6359367	861.5	380049	6359367	861.5
14156	05CF236	87.9	90.9	3.03	89.39	H83	Liard Main	9	380049	6359367	935.7	0	-90	171.3	562	380049	6359367	846.4	380049	6359367	846.4
14162	05CF236	106.1	109.1	3.03	107.58	H83	Liard Main	9	380049	6359367	935.7	0	-90	171.3	562	380049	6359367	828.2	380049	6359367	828.2
14169	05CF236	127.3	130.3	3.03	128.79	H83	Liard Main	9	380049	6359367	935.7	0	-90	171.3	562	380049	6359367	807.0	380049	6359367	807.0
14232	05CF239	27.3	30.3	3.03	28.79	H76	Liard Main	9	380400	6359200	1037.2	0	-90	214	702	380400	6359200	1008.4	380400	6359200	1008.4
14250	05CF239	72.7	75.8	3.03	74.24	H76	Liard Main	9	380400	6359200	1037.2	0	-90	214	702	380400	6359200	963.0	380400	6359200	963.0
14260	05CF239	103.0	106.1	3.03	104.55	H76	Liard Main	9	380400	6359200	1037.2	0	-90	214	702	380400	6359200	932.7	380400	6359200	932.7
14276	05CF239	142.4	145.5	3.03	143.94	H76	Liard Main	9	380400	6359200	1037.2	0	-90	214	702	380400	6359200	893.3	380400	6359200	893.3
14295	05CF239	200.0	203.0	3.03	201.52	H76	Liard Main	9	380400	6359200	1037.2	0	-90	214	702	380400	6359200	835.7	380400	6359200	835.7
14301	05CF240	9.1	12.1	3.03	10.61	H85	Liard Main	9	380450	6358873	1036.3	90	-70	146.3	480	380454	6358873	1026.4	380450	6358873	1026.4
14323	05CF240	66.7	69.7	3.03	68.18	H85	Liard Main	9	380450	6358873	1036.3	90	-70	146.3	480	380473	6358873	972.3	380450	6358873	972.3
14332	05CF240	93.9	97.0	3.03	95.45	H85	Liard Main	9	380450	6358873	1036.3	90	-70	146.3	480	380483	6358873	946.6	380450	6358873	946.6
14345	05CF240	133.3	136.4	3.03	134.85	H85	Liard Main	9	380450	6358873	1036.3	90	-70	146.3	480	380496	6358873	909.6	380450	6358873	909.6
14348	05CF240	142.4	145.5	3.03	143.94	H85	Liard Main	9	380450	6358873	1036.3	90	-70	146.3	480	380499	6358873	901.1	380450	6358873	901.1
14797	05CF243	9.1	12.1	3.03	10.61	H85	Liard Main	9	380412	6359356	1048.2	0	-90	274.5	900.5	380412	6359356	1037.6	380412	6359356	1037.6
14808	05CF243	42.4	45.5	3.03	43.94	H72	Liard Main	9	380412	6359356	1048.2	0	-90	274.5	900.5	380412	6359356	1004.3	380412	6359356	1004.3
14816	05CF243	66.7	69.7	3.03	68.18	H72	Liard Main	9	380412	6359356	1048.2	0	-90	274.5	900.5	380412	6359356	980.0	380412	6359356	980.0
14828	05CF243	103.0	106.1	3.03	104.55	H72	Liard Main	9	380412	6359356	1048.2	0	-90	274.5	900.5	380412	6359356	943.7	380412	6359356	943.7
14844	05CF243	142.4	145.5	3.03	143.94	H72	Liard Main	9	380412	6359356	1048.2	0	-90	274.5	900.5	380412	6359356	904.3	380412	6359356	904.3
14680	05CF243	190.9	193.9	3.03	192.42	H72	Liard Main	9	380412	6359356	1048.2	0	-90	274.5	900.5	380412	6359356	855.8	380412	6359356	855.8
14871	05CF243	224.2	227.3	3.03	225.76	H72	Liard Main	9	380412	6359356	1048.2	0	-90	274.5	900.5	380412	6359356	822.5	380412	6359356	822.5
14887	05CF243	263.6	266.7	3.03	265.15	H72	Liard Main	9	380412	6359356	1048.2	0	-90	274.5	900.5	380412	6359356	783.1	380412	6359356	783.1
14689	05CF244	9.1	12.1	3.03	10.61	S2	Liard Main	9	380430	6359451	1056.1	90	-80	304.5	999	380432	6359451	1045.7	380430	6359451	1045.7
14695	05CF244	27.3	30.3	3.03	28.79	S2	Liard Main	9	380430	6359451	1056.1	90	-80	304.5	999	380435	6359451	1027.8	380430	6359451	1027.8
14742	05CF244	160.6	163.6	3.03	162.12	S2	Liard Main	9	380430	6359451	1056.1	90	-80	304.5	999	380458	6359451	896.5	380430	6359451	896.5
14666	05CF245	51.5	54.5	3.03	53.03	H84	Liard Main	9	380515	6359357	1088.1	0	-90	107	351	380515	6359357	1035.1	380515	6359357	1035.1
14685	05CF245	100.0	103.0	3.03	101.52	H84	Liard Main	9	380515	6359357	1088.1	0	-90	107	351	380515	6359357	986.6	380515	6359357	986.6
14685B	05CF245	100.0	103.0	3.03	101.52	H84	Liard Main	9	380515	6359357	1088.1	0	-90	107	351	380515	6359357	986.6	380515	6359357	986.6
14545	05CF246	12.1	15.2	3.03	13.64	H43	Liard Main	9	380557	6359428	1118.0	90	-80	305.1	1001	380559	6359428	1104.6	380557	6359428	1104.6
14565	05CF246	63.6	66.7	3.03	65.15	H43	Liard Main	9	380557	6359428	1118.0	90	-80	305.1	1001	380568	6359428	1053.9	380557	6359428	1053.9
14571	05CF246	81.8	84.8	3.03	83.33	H43	Liard Main	9	380557	6359428	1118.0	90	-80	305.1	1001	380571	6359428	1035.9	380557	6359428	1035.9
14578	05CF246	103.0	106.1	3.03	104.55	H43	Liard Main	9	380557	6359428	1118.0	90	-80	305.1	1001	380575	6359428	1015.1	380557	6359428	1015.1
14578B	05CF246	103.0	106.1	3.03	104.55	H43	Liard Main	9	380557	6359428	1118.0	90	-80	305.1	1001	380575	6359428	1015.1	380557	6359428	1015.1
14598	05CF246	154.5	157.6	3.03	156.06	H43	Liard Main	9	380557	6359428	1118.0	90	-80	305.1	1001	380584	6359428	964.3	380557	6359428	964.3
14893	05CF247	12.1	15.2	3.03	13.64	H57	Liard Main	9	380338	6359580	1026.6	90	-80	290	951.5	380340	6359580	1013.1	380338	6359580	1013.1
14899	05CF247	30.3	33.3	3.03	31.82	H57	Liard Main	9	380338	6359580	1026.6	90	-80	290	951.5	380344	6359580	995.2	380338	6359580	995.2
14908	05CF247	57.6	60.6	3.03	59.09	H57	Liard Main	9	380338	6359580	1026.6	90	-80	290	951.5	380348	6359580	968.4	380338	6359580	968.4
14917	05CF247	75.8	78.8	3.03	77.27	H57	Liard Main	9	380338	6359580	1026.6	90	-80	290	951.5	380351	6359580	950.5	380338	6359580	950.5
14925	05CF247	100.0	103.0	3.03	101.52	H57	Liard Main	9	380338	6359580	1026.6	90	-80	290	951.5	380356	6359580	926.6	380338	6359580	926.6
14998	05CF248	36.4	39.4	3.03	37.88	H49-50	Liard Main	9	380246	6359561	999.1	90	-80	342	1122	380253	6359561	961.8	380246	6359561	961.8
15862	05CF248	78.8	81.8	3.03	80.30	H49-50	Liard Main	9	380246	6359561	999.1	90	-80	342	1122	380260	6359561	920.1	380246	6359561	920.1
15870	05CF248	103.0	106.1	3.03	104.55	H49-50	Liard Main	9	380246	6359561	999.1	90	-80	342	1122	380264	6359561	896.2	380246	6359561	896.2
15879	05CF248	130.3	133.3	3.03	131.82	H49-50	Liard Main	9	380246	6359561	999.1	90	-80	342	1122	380269	6359561	869.3	380246	6359561	869.3

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.
UTM NAD 27 was used for Northing and Easting data

Sample Id.	Hole Id	From (m)	To (m)	Interval (m)	Centre of Interval (m)	Old Collar	Ore Zone	Zone	Top of Drillholes UTM NAD 27 Easting	Northing	Elevation (m)	Azimuth	Inclination	Length (m)	Length (ft)	For Easting Plots Centre of ABA Interval Easting	Northing	Elevation	For Northing Plots Centre of ABA Interval Easting	Northing	Elevation
15887	05CF248	145.5	148.5	3.03	146.97	H49-50	Liard Main	9	380246	6359561	999.1	90	-80	342	1122	380272	6359561	854.4	380246	6359561	854.4
15891	05CF248	157.6	160.6	3.03	159.09	H49-50	Liard Main	9	380246	6359561	999.1	90	-80	342	1122	380274	6359561	842.5	380246	6359561	842.5
15908	05CF248	209.1	212.1	3.03	210.61	H49-50	Liard Main	9	380246	6359561	999.1	90	-80	342	1122	380283	6359561	791.7	380246	6359561	791.7
15911	05CF248	218.2	221.2	3.03	219.70	H49-50	Liard Main	9	380246	6359561	999.1	90	-80	342	1122	380284	6359561	782.8	380246	6359561	782.8
125285	06CF251	24.40	27.45	3.05	25.93	T-98	Main	9	379930	6359792	951.6	N/A	-90	102.0		379930	6359792	925.6	379930	6359792	925.6
125288	06CF251	33.55	36.60	3.05	35.08	T-98	Main	9	379930	6359792	951.6	N/A	-90	102.0		379930	6359792	916.5	379930	6359792	916.5
125293	06CF251	48.80	51.85	3.05	50.33	T-98	Main	9	379930	6359792	951.6	N/A	-90	102.0		379930	6359792	901.2	379930	6359792	901.2
125305	06CF251	76.25	79.30	3.05	77.78	T-98	Main	9	379930	6359792	951.6	N/A	-90	102.0		379930	6359792	873.8	379930	6359792	873.8
125311	06CF251	94.55	97.60	3.05	96.08	T-98	Main	9	379930	6359792	951.6	N/A	-90	102.0		379930	6359792	855.5	379930	6359792	855.5
125703	06CF256	18.30	21.35	3.05	19.83	T169	Main	9	380264	6359700	1037.4	N/A	-90	303.0		380264	6359700	1017.5	380264	6359700	1017.5
125728	06CF256	94.55	97.60	3.05	96.08	T169	Main	9	380264	6359700	1037.4	N/A	-90	303.0		380264	6359700	941.3	380264	6359700	941.3
125755	06CF256	167.75	170.80	3.05	169.28	T169	Main	9	380264	6359700	1037.4	N/A	-90	303.0		380264	6359700	868.1	380264	6359700	868.1
125772	06CF256	219.60	222.65	3.05	221.13	T169	Main	9	380264	6359700	1037.4	N/A	-90	303.0		380264	6359700	816.2	380264	6359700	816.2
125795	06CF256	280.60	283.65	3.05	282.13	T169	Main	9	380264	6359700	1037.4	N/A	-90	303.0		380264	6359700	755.2	380264	6359700	755.2
125422	06CF258	30.50	33.55	3.05	32.03	H47	Main	9	380194	6359467	1001.5	90	-65	243.0		380208	6359467	972.5	380194	6359467	972.5
125435	06CF258	70.15	73.20	3.05	71.68	H47	Main	9	380194	6359467	1001.5	90	-65	243.0		380225	6359467	936.6	380194	6359467	936.6
125452	06CF258	122.00	125.05	3.05	123.53	H47	Main	9	380194	6359467	1001.5	90	-65	243.0		380247	6359467	889.6	380194	6359467	889.6
125476	06CF258	186.05	189.10	3.05	187.58	H47	Main	9	380194	6359467	1001.5	90	-65	243.0		380274	6359467	831.5	380194	6359467	831.5
125490	06CF258	228.75	231.80	3.05	230.28	H47	Main	9	380194	6359467	1001.5	90	-65	243.0		380292	6359467	792.8	380194	6359467	792.8
126192	06CF259	24.40	27.45	3.05	25.93	T183	Main	9	380420	6359860	1128.2	N/A	-90	312.0		380420	6359860	1102.3	380420	6359860	1102.3
126206	06CF259	67.10	70.15	3.05	68.63	T183	Main	9	380420	6359860	1128.2	N/A	-90	312.0		380420	6359860	1059.6	380420	6359860	1059.6
126225	06CF259	115.90	118.95	3.05	117.43	T183	Main	9	380420	6359860	1128.2	N/A	-90	312.0		380420	6359860	1010.8	380420	6359860	1010.8
126244	06CF259	173.85	176.90	3.05	175.38	T183	Main	9	380420	6359860	1128.2	N/A	-90	312.0		380420	6359860	952.8	380420	6359860	952.8
126266	06CF259	231.80	234.85	3.05	233.33	T183	Main	9	380420	6359860	1128.2	N/A	-90	312.0		380420	6359860	894.9	380420	6359860	894.9
126279	06CF259	271.45	274.50	3.05	272.98	T183	Main	9	380420	6359860	1128.2	N/A	-90	312.0		380420	6359860	855.2	380420	6359860	855.2
126288	06CF259	298.90	301.95	3.05	300.43	T183	Main	9	380420	6359860	1128.2	N/A	-90	312.0		380420	6359860	827.8	380420	6359860	827.8
126297	06CF260	18.30	21.35	3.05	19.83	T194	Main	9	380322	6360081	1137.4	N/A	-90	168.0		380322	6360081	1117.6	380322	6360081	1117.6
126314	06CF260	61.00	64.05	3.05	62.53	T194	Main	9	380322	6360081	1137.4	N/A	-90	168.0		380322	6360081	1074.9	380322	6360081	1074.9
126329	06CF260	106.75	109.80	3.05	108.28	T194	Main	9	380322	6360081	1137.4	N/A	-90	168.0		380322	6360081	1029.2	380322	6360081	1029.2
126337	06CF260	131.15	134.20	3.05	132.68	T194	Main	9	380322	6360081	1137.4	N/A	-90	168.0		380322	6360081	1004.8	380322	6360081	1004.8
126351	06CF260	164.70	168.00	3.30	166.35	T194	Main	9	380322	6360081	1137.4	N/A	-90	168.0		380322	6360081	971.1	380322	6360081	971.1
126427	06CF261	3.00	6.10	3.10	4.55	H32	Main	9	380604	6359635	1162.4	270	-65	210.0		380602	6359635	1158.3	380604	6359635	1158.3
126430	06CF261	12.20	15.25	3.05	13.73	H32	Main	9	380604	6359635	1162.4	270	-65	210.0		380598	6359635	1150.0	380604	6359635	1150.0
126434	06CF261	24.40	27.45	3.05	25.93	H32	Main	9	380604	6359635	1162.4	270	-65	210.0		380593	6359635	1139.0	380604	6359635	1139.0
126443	06CF261	51.85	54.90	3.05	53.38	H32	Main	9	380604	6359635	1162.4	270	-65	210.0		380581	6359635	1114.1	380604	6359635	1114.1
126449	06CF261	70.15	73.20	3.05	71.68	H32	Main	9	380604	6359635	1162.4	270	-65	210.0		380573	6359635	1097.5	380604	6359635	1097.5
126464	06CF261	106.75	109.80	3.05	108.28	H32	Main	9	380604	6359635	1162.4	270	-65	210.0		380558	6359635	1064.3	380604	6359635	1064.3
126492	06CF261	192.15	195.20	3.05	193.68	H32	Main	9	380604	6359635	1162.4	270	-65	210.0		380522	6359635	986.9	380604	6359635	986.9
145655	06CF262	27.45	30.50	3.05	28.98	H45	Main	9	380528	6359465	1124.3	270	-75	225.0		380521	6359465	1096.3	380528	6359465	1096.3
145669	06CF262	61.00	64.05	3.05	62.53	H45	Main	9	380528	6359465	1124.3	270	-75	225.0		380512	6359465	1063.9	380528	6359465	1063.9
145685	06CF262	109.80	112.85	3.05	111.33	H45	Main	9	380528	6359465	1124.3	270	-75	225.0		380500	6359465	1016.8	380528	6359465	1016.8
145694	06CF262	137.25	140.30	3.05	138.78	H45	Main	9	380528	6359465	1124.3	270	-75	225.0		380492	6359465	990.3	380528	6359465	990.3
145708	06CF262	170.80	173.85	3.05	172.33	H45	Main	9	380528	6359465	1124.3	270	-75	225.0		380484	6359465	957.9	380528	6359465	957.9
145723	06CF262	216.55	219.60	3.05	218.08	H45	Main	9	380528	6359465	1124.3	270	-75	225.0		380472	6359465	913.7	380528	6359465	913.7
146798	06CF263	15.25	18.30	3.05	16.78	H72	Main	9	380316	6359557	1051.8	90	-45	213.0		380328	6359557	1039.9	380316	6359557	1039.9
146824	06CF263	85.40	88.45	3.05	86.93	H72	Main	9	380316	6359557	1051.8	90	-45	213.0		380377	6359557	990.3	380316	6359557	990.3

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.
UTM NAD 27 was used for Northing and Easting data

Sample Id.	Hole Id	From (m)	To (m)	Interval (m)	Centre of Interval (m)	Old Collar	Ore Zone	Zone	Top of Drillholes UTM NAD 27 Easting	Northing	Elevation (m)	Azimuth	Inclination	Length (m)	Length (ft)	For Easting Plots Centre of ABA Interval Easting	Northing	Elevation	For Northing Plots Centre of ABA Interval Easting	Northing	Elevation
146831	06CF263	106.75	109.80	3.05	108.28	H72	Main	9	380316	6359557	1051.8	90	-45	213.0		380392	6359557	975.2	380316	6359557	975.2
146843	06CF263	143.35	146.40	3.05	144.88	H72	Main	9	380316	6359557	1051.8	90	-45	213.0		380418	6359557	949.3	380316	6359557	949.3
146861	06CF263	189.10	192.15	3.05	190.63	H72	Main	9	380316	6359557	1051.8	90	-45	213.0		380450	6359557	917.0	380316	6359557	917.0
146868	06CF263	210.45	213.00	2.55	211.73	H72	Main	9	380316	6359557	1051.8	90	-45	213.0		380465	6359557	902.1	380316	6359557	902.1
126352	06CF266	3.00	6.10	3.10	4.55	C245	Main	9	380406	6359554	1092.1	90	-60	123.0		380409	6359554	1088.2	380406	6359554	1088.2
126358	06CF266	21.35	24.40	3.05	22.88	C245	Main	9	380406	6359554	1092.1	90	-60	123.0		380418	6359554	1072.3	380406	6359554	1072.3
126374	06CF266	70.15	73.20	3.05	71.68	C245	Main	9	380406	6359554	1092.1	90	-60	123.0		380442	6359554	1030.0	380406	6359554	1030.0
126384	06CF266	91.50	94.55	3.05	93.03	C245	Main	9	380406	6359554	1092.1	90	-60	123.0		380453	6359554	1011.5	380406	6359554	1011.5
126391	06CF266	112.85	115.90	3.05	114.38	C245	Main	9	380406	6359554	1092.1	90	-60	123.0		380463	6359554	993.0	380406	6359554	993.0
146172	06CF269	6.10	9.15	3.05	7.63	H86	Main	9	380312	6359473	1036.8	90	-50	201.0		380317	6359473	1030.9	380312	6359473	1030.9
146182	06CF269	27.45	30.50	3.05	28.98	H86	Main	9	380312	6359473	1036.8	90	-50	201.0		380331	6359473	1014.6	380312	6359473	1014.6
146203	06CF269	91.50	94.55	3.05	93.03	H86	Main	9	380312	6359473	1036.8	90	-50	201.0		380372	6359473	965.5	380312	6359473	965.5
146214	06CF269	125.05	128.10	3.05	126.58	H86	Main	9	380312	6359473	1036.8	90	-50	201.0		380394	6359473	939.8	380312	6359473	939.8
146221	06CF269	137.25	140.30	3.05	138.78	H86	Main	9	380312	6359473	1036.8	90	-50	201.0		380402	6359473	930.5	380312	6359473	930.5
146238	06CF269	189.10	192.15	3.05	190.63	H86	Main	9	380312	6359473	1036.8	90	-50	201.0		380435	6359473	890.7	380312	6359473	890.7
147034	06CF271	21.35	24.40	3.05	22.88	T220	Main	9	380334	6359242	1038.2	90	-60	216.7		380346	6359242	1018.3	380334	6359242	1018.3
147038	06CF271	33.55	36.60	3.05	35.08	T220	Main	9	380334	6359242	1038.2	90	-60	216.7		380352	6359242	1007.8	380334	6359242	1007.8
147051	06CF271	73.20	76.25	3.05	74.73	T220	Main	9	380334	6359242	1038.2	90	-60	216.7		380372	6359242	973.4	380334	6359242	973.4
147070	06CF271	122.00	125.05	3.05	123.53	T220	Main	9	380334	6359242	1038.2	90	-60	216.7		380396	6359242	931.2	380334	6359242	931.2
147087	06CF271	173.85	176.90	3.05	175.38	T220	Main	9	380334	6359242	1038.2	90	-60	216.7		380422	6359242	886.3	380334	6359242	886.3
147097	06CF271	204.35	207.40	3.05	205.88	T220	Main	9	380334	6359242	1038.2	90	-60	216.7		380437	6359242	859.9	380334	6359242	859.9
145508	06CF273	24.40	27.45	3.05	25.93	C247	Main	9	380230	6359773	1028.6	45	-80	303.0		380225	6359773	1003.1	380230	6359773	1003.1
145527	06CF273	82.35	85.40	3.05	83.88	C247	Main	9	380230	6359773	1028.6	45	-80	303.0		380215	6359773	946.0	380230	6359773	946.0
145543	06CF273	122.00	125.05	3.05	123.53	C247	Main	9	380230	6359773	1028.6	45	-80	303.0		380208	6359773	907.0	380230	6359773	907.0
145562	06CF273	179.95	183.00	3.05	181.48	C247	Main	9	380230	6359773	1028.6	45	-80	303.0		380198	6359773	849.9	380230	6359773	849.9
145576	06CF273	222.65	225.70	3.05	224.18	C247	Main	9	380230	6359773	1028.6	45	-80	303.0		380191	6359773	807.9	380230	6359773	807.9
145601	06CF273	289.75	292.80	3.05	291.28	C247	Main	9	380230	6359773	1028.6	45	-80	303.0		380179	6359773	741.8	380230	6359773	741.8
146297	06CF275	27.40	30.50	3.10	28.95	T155	Main	9	380187	6359725	1007.7	270	-60	336.0		380172	6359725	982.6	380187	6359725	982.6
146314	06CF275	70.15	73.20	3.05	71.68	T155	Main	9	380187	6359725	1007.7	270	-60	336.0		380151	6359725	945.6	380187	6359725	945.6
146335	06CF275	134.20	137.25	3.05	135.73	T155	Main	9	380187	6359725	1007.7	270	-60	336.0		380119	6359725	890.1	380187	6359725	890.1
146352	06CF275	176.90	179.95	3.05	178.43	T155	Main	9	380187	6359725	1007.7	270	-60	336.0		380098	6359725	853.1	380187	6359725	853.1
146368	06CF275	225.70	228.75	3.05	227.23	T155	Main	9	380187	6359725	1007.7	270	-60	336.0		380073	6359725	810.9	380187	6359725	810.9
146390	06CF275	283.65	286.70	3.05	285.18	T155	Main	9	380187	6359725	1007.7	270	-60	336.0		380044	6359725	760.7	380187	6359725	760.7
146508	06CF276	18.30	21.35	3.05	19.83	H101	Main	9	380004	6359792	971.6	90	-60	351.0		380014	6359792	954.4	380004	6359792	954.4
146526	06CF276	73.20	76.25	3.05	74.73	H101	Main	9	380004	6359792	971.6	90	-60	351.0		380041	6359792	906.8	380004	6359792	906.8
146544	06CF276	118.95	122.00	3.05	120.48	H101	Main	9	380004	6359792	971.6	90	-60	351.0		380064	6359792	867.2	380004	6359792	867.2
146565	06CF276	183.00	186.05	3.05	184.53	H101	Main	9	380004	6359792	971.6	90	-60	351.0		380096	6359792	811.8	380004	6359792	811.8
146589	06CF276	247.05	250.10	3.05	248.58	H101	Main	9	380004	6359792	971.6	90	-60	351.0		380128	6359792	756.3	380004	6359792	756.3
146613	06CF276	320.25	323.30	3.05	321.78	H101	Main	9	380004	6359792	971.6	90	-60	351.0		380165	6359792	692.9	380004	6359792	692.9
146627	06CF278	9.15	12.20	3.05	10.68	H83-50S	Main	9	379957	6359515	921.9	N/A	-90	153.1		379957	6359515	911.2	379957	6359515	911.2
146637	06CF278	39.65	42.70	3.05	41.18	H83-50S	Main	9	379957	6359515	921.9	N/A	-90	153.1		379957	6359515	880.7	379957	6359515	880.7
146649	06CF278	76.25	79.30	3.05	77.78	H83-50S	Main	9	379957	6359515	921.9	N/A	-90	153.1		379957	6359515	844.1	379957	6359515	844.1
146657	06CF278	100.65	103.70	3.05	102.18	H83-50S	Main	9	379957	6359515	921.9	N/A	-90	153.1		379957	6359515	819.7	379957	6359515	819.7
146676	06CF278	149.45	153.05	3.60	151.25	H83-50S	Main	9	379957	6359515	921.9	N/A	-90	153.1		379957	6359515	770.6	379957	6359515	770.6
125188	06CF284	9.15	12.20	3.05	10.68	H12	Main	9	379949	6359567	945.4	90	-80	274.5		379951	6359567	934.9	379949	6359567	934.9
125198	06CF284	39.65	42.70	3.05	41.18	H12	Main	9	379949	6359567	945.4	90	-80	274.5		379956	6359567	904.9	379949	6359567	904.9

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.
UTM NAD 27 was used for Northing and Easting data

									Top of Drillholes							For Easting Plots			For Northing Plots		
Sample					Centre of	Old	Ore		UTM NAD 27							Centre of ABA Interval			Centre of ABA Interval		
Id.	Hole Id	From	To	Interval	Interval	Collar	Zone	Zone	Easting	Northing	Elevation	Azimuth	Inclination	Length	Length	Easting	Northing	Elevation	Easting	Northing	Elevation
		(m)	(m)	(m)	(m)						(m)			(m)	(ft)						
125207	06CF284	67.10	70.15	3.05	68.63	H12	Main	9	379949	6359567	945.4	90	-80	274.5		379961	6359567	877.8	379949	6359567	877.8
125228	06CF284	122.00	125.05	3.05	123.53	H12	Main	9	379949	6359567	945.4	90	-80	274.5		379970	6359567	823.8	379949	6359567	823.8
125244	06CF284	170.80	173.85	3.05	172.33	H12	Main	9	379949	6359567	945.4	90	-80	274.5		379979	6359567	775.7	379949	6359567	775.7
125257	06CF284	210.45	213.50	3.05	211.98	H12	Main	9	379949	6359567	945.4	90	-80	274.5		379986	6359567	736.7	379949	6359567	736.7
125278	06CF284	265.35	268.40	3.05	266.88	H12	Main	9	379949	6359567	945.4	90	-80	274.5		379995	6359567	682.6	379949	6359567	682.6
125596	06CF285	9.15	12.20	3.05	10.68	T133	Main	9	380250	635965	1028.6	90	-70	291.0		380254	635965	1018.6	380250	635965	1018.6
125610	06CF285	51.85	54.90	3.05	53.38	T133	Main	9	380250	635965	1028.6	90	-70	291.0		380268	635965	978.5	380250	635965	978.5
125626	06CF285	91.50	94.55	3.05	93.03	T133	Main	9	380250	635965	1028.6	90	-70	291.0		380282	635965	941.2	380250	635965	941.2
125641	06CF285	137.25	140.30	3.05	138.78	T133	Main	9	380250	635965	1028.6	90	-70	291.0		380297	635965	898.2	380250	635965	898.2
125669	06CF285	213.50	216.55	3.05	215.03	T133	Main	9	380250	635965	1028.6	90	-70	291.0		380323	635965	826.6	380250	635965	826.6
125690	06CF285	277.55	280.60	3.05	279.08	T133	Main	9	380250	635965	1028.6	90	-70	291.0		380345	635965	766.4	380250	635965	766.4
West Breccia Zone																					
14018	05CF234	18.2	21.2	3.03	19.70	H89	West Breccia	9	379785	6359307	897.6	270	45	166.7	550	379771	6359307	883.7	379785	6359307	883.7
14021	05CF234	27.3	30.3	3.03	28.79	H89	West Breccia	9	379785	6359307	897.6	270	45	166.7	550	379765	6359307	877.3	379785	6359307	877.3
14036	05CF234	63.6	66.7	3.03	65.15	H89	West Breccia	9	379785	6359307	897.6	270	45	166.7	550	379739	6359307	851.6	379785	6359307	851.6
14043	05CF234	84.8	87.9	3.03	86.36	H89	West Breccia	9	379785	6359307	897.6	270	45	166.7	550	379724	6359307	836.6	379785	6359307	836.6
14060	05CF234	136.4	139.4	3.03	137.88	H89	West Breccia	9	379785	6359307	897.6	270	45	166.7	550	379688	6359307	800.1	379785	6359307	800.1
14067	05CF234	157.6	160.6	3.03	159.09	H89	West Breccia	9	379785	6359307	897.6	270	45	166.7	550	379673	6359307	785.2	379785	6359307	785.2
14076	05CF235	18.2	21.2	3.03	19.70	H91	West Breccia	9	379728	6359382	886.4	0	-90	159.4	523	379728	6359382	866.7	379728	6359382	866.7
14083	05CF235	39.4	42.4	3.03	40.91	H91	West Breccia	9	379728	6359382	886.4	0	-90	159.4	523	379728	6359382	845.5	379728	6359382	845.5
14099	05CF235	87.9	90.9	3.03	89.39	H91	West Breccia	9	379728	6359382	886.4	0	-90	159.4	523	379728	6359382	797.0	379728	6359382	797.0
14103	05CF235	100.0	103.0	3.03	101.52	H91	West Breccia	9	379728	6359382	886.4	0	-90	159.4	523	379728	6359382	784.8	379728	6359382	784.8
125046	06CF249	18.30	21.35	3.05	19.83	H-20	West Breccia	9	379633	6359945	901.0	90	-55	153.0		379644	6359945	884.7	379633	6359945	884.7
125068	06CF249	76.25	79.30	3.05	77.78	H-20	West Breccia	9	379633	6359945	901.0	90	-55	153.0		379678	6359945	837.3	379633	6359945	837.3
125073	06CF249	91.50	94.55	3.05	93.03	H-20	West Breccia	9	379633	6359945	901.0	90	-55	153.0		379686	6359945	824.8	379633	6359945	824.8
125079	06CF249	109.80	112.85	3.05	111.33	H-20	West Breccia	9	379633	6359945	901.0	90	-55	153.0		379697	6359945	809.8	379633	6359945	809.8
125084	06CF249	125.05	128.10	3.05	126.58	H-20	West Breccia	9	379633	6359945	901.0	90	-55	153.0		379706	6359945	797.3	379633	6359945	797.3
125127	06CF252	18.30	21.35	3.05	19.83	T179	West Breccia	9	379745	6359873	907.5	N/A	-90	78.0		379745	6359873	887.7	379745	6359873	887.7
125129	06CF252	24.40	27.45	3.05	25.93	T179	West Breccia	9	379745	6359873	907.5	N/A	-90	78.0		379745	6359873	881.6	379745	6359873	881.6
125134	06CF252	39.65	42.70	3.05	41.18	T179	West Breccia	9	379745	6359873	907.5	N/A	-90	78.0		379745	6359873	866.4	379745	6359873	866.4
125142	06CF252	54.90	57.95	3.05	56.43	T179	West Breccia	9	379745	6359873	907.5	N/A	-90	78.0		379745	6359873	851.1	379745	6359873	851.1
125149	06CF252	76.25	78.00	1.75	77.13	T179	West Breccia	9	379745	6359873	907.5	N/A	-90	78.0		379745	6359873	830.4	379745	6359873	830.4
125154	06CF254	15.25	18.30	3.05	16.78	T135	West Breccia	9	379793	6359649	916.4	N/A	-90	107.0		379793	6359649	899.6	379793	6359649	899.6
125165	06CF254	48.80	51.85	3.05	50.33	T135	West Breccia	9	379793	6359649	916.4	N/A	-90	107.0		379793	6359649	866.1	379793	6359649	866.1
125176	06CF254	82.35	85.40	3.05	83.88	T135	West Breccia	9	379793	6359649	916.4	N/A	-90	107.0		379793	6359649	832.5	379793	6359649	832.5
146112	06CF280	15.25	18.30	3.05	16.78	T160-50S	West Breccia	9	379811	6359508	918.9	N/A	-90	184.5		379811	6359508	902.1	379811	6359508	902.1
146115	06CF280	24.40	27.45	3.05	25.93	T160-50S	West Breccia	9	379811	6359508	918.9	N/A	-90	184.5		379811	6359508	893.0	379811	6359508	893.0
146124	06CF280	51.85	54.90	3.05	53.38	T160-50S	West Breccia	9	379811	6359508	918.9	N/A	-90	184.5		379811	6359508	865.5	379811	6359508	865.5
146127	06CF280	61.00	64.05	3.05	62.53	T160-50S	West Breccia	9	379811	6359508	918.9	N/A	-90	184.5		379811	6359508	856.4	379811	6359508	856.4
146135	06CF280	85.40	88.45	3.05	86.93	T160-50S	West Breccia	9	379811	6359508	918.9	N/A	-90	184.5		379811	6359508	832.0	379811	6359508	832.0
146149	06CF280	118.95	122.00	3.05	120.48	T160-50S	West Breccia	9	379811	6359508	918.9	N/A	-90	184.5		379811	6359508	798.4	379811	6359508	798.4
146161	06CF280	155.55	158.60	3.05	157.08	T160-50S	West Breccia	9	379811	6359508	918.9	N/A	-90	184.5		379811	6359508	761.8	379811	6359508	761.8
146164	06CF280	164.70	167.75	3.05	166.23	T160-50S	West Breccia	9	379811	6359508	918.9	N/A	-90	184.5		379811	6359508	752.7	379811	6359508	752.7
145951	06CF281	12.20	15.25	3.05	13.73	H97	West Breccia	9	379748	6359417	910.2	N/A	-90	168.0		379748	6359417	896.5	379748	6359417	896.5
145956	06CF281	27.45	30.50	3.05	28.98	H97	West Breccia	9	379748	6359417	910.2	N/A	-90	168.0		379748	6359417	881.3	379748	6359417	881.3
145974	06CF281	82.35	85.40	3.05	83.88	H97	West Breccia	9	379748	6359417	910.2	N/A	-90	168.0		379748	6359417	826.4	379748	6359417	826.4

Project:	**Schaft Creek**
Client:	Copper Fox Metals Inc.
Data:	**Sample Information**
Comments:	2005 core samples were collected by MDAG on Feb 7'07. 2006 core samples were collected by Copper Fox personnel in Sep '07. For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps. UTM NAD 27 was used for Northing and Easting data

Sample Id.	Hole Id	From (m)	To (m)	Interval (m)	Centre of Interval (m)	Old Collar	Ore Zone	Zone	Top of Drillholes UTM NAD 27 Easting	Northing	Elevation (m)	Azimuth	Inclination	Length (m)	Length (ft)	For Easting Plots Centre of ABA Interval Easting	Northing	Elevation	For Northing Plots Centre of ABA Interval Easting	Northing	Elevation
145982	06CF281	97.60	100.65	3.05	99.13	H97	West Breccia	9	379748	6359417	910.2	N/A	-90	168.0		379748	6359417	811.1	379748	6359417	811.1
145992	06CF281	128.10	131.15	3.05	129.63	H97	West Breccia	9	379748	6359417	910.2	N/A	-90	168.0		379748	6359417	780.6	379748	6359417	780.6
145999	06CF281	149.45	152.50	3.05	150.98	H97	West Breccia	9	379748	6359417	910.2	N/A	-90	168.0		379748	6359417	759.3	379748	6359417	759.3
145834	06CF282	6.10	9.15	3.05	7.63	T157-50W	West Breccia	9	379695	6359652	899.6	N/A	-90	121.0		379695	6359652	892.0	379695	6359652	892.0
145842	06CF282	30.50	33.55	3.05	32.03	T157-50W	West Breccia	9	379695	6359652	899.6	N/A	-90	121.0		379695	6359652	867.6	379695	6359652	867.6
145852	06CF282	61.00	64.05	3.05	62.53	T157-50W	West Breccia	9	379695	6359652	899.6	N/A	-90	121.0		379695	6359652	837.1	379695	6359652	837.1
145857	06CF282	76.25	79.30	3.05	77.78	T157-50W	West Breccia	9	379695	6359652	899.6	N/A	-90	121.0		379695	6359652	821.9	379695	6359652	821.9
145871	06CF282	109.80	112.85	3.05	111.33	T157-50W	West Breccia	9	379695	6359652	899.6	N/A	-90	121.0		379695	6359652	788.3	379695	6359652	788.3
145608	06CF283	9.15	12.20	3.05	10.68	A18+50N	West Breccia	9	379570	6359671	881.7	N/A	-90	120.0		379570	6359671	871.1	379570	6359671	871.1
145614	06CF283	27.45	30.50	3.05	28.98	A18+50N	West Breccia	9	379570	6359671	881.7	N/A	-90	120.0		379570	6359671	852.8	379570	6359671	852.8
145628	06CF283	61.00	64.05	3.05	62.53	A18+50N	West Breccia	9	379570	6359671	881.7	N/A	-90	120.0		379570	6359671	819.2	379570	6359671	819.2
145640	06CF283	97.60	100.65	3.05	99.13	A18+50N	West Breccia	9	379570	6359671	881.7	N/A	-90	120.0		379570	6359671	782.6	379570	6359671	782.6
145646	06CF283	115.90	118.95	3.05	117.43	A18+50N	West Breccia	9	379570	6359671	881.7	N/A	-90	120.0		379570	6359671	764.3	379570	6359671	764.3
Paramount Zone																					
125965	06CF286	15.25	18.30	3.05	16.78	T203	Paramount	9	379450	6360878	960.3	N/A	-90	213.0		379450	6360878	943.6	379450	6360878	943.6
125974	06CF286	42.70	45.75	3.05	44.23	T203	Paramount	9	379450	6360878	960.3	N/A	-90	213.0		379450	6360878	916.1	379450	6360878	916.1
125983	06CF286	61.00	64.05	3.05	62.53	T203	Paramount	9	379450	6360878	960.3	N/A	-90	213.0		379450	6360878	897.8	379450	6360878	897.8
125988	06CF286	76.25	79.30	3.05	77.78	T203	Paramount	9	379450	6360878	960.3	N/A	-90	213.0		379450	6360878	882.6	379450	6360878	882.6
126007	06CF286	134.20	137.25	3.05	135.73	T203	Paramount	9	379450	6360878	960.3	N/A	-90	213.0		379450	6360878	824.6	379450	6360878	824.6
126031	06CF286	198.25	201.30	3.05	199.78	T203	Paramount	9	379450	6360878	960.3	N/A	-90	213.0		379450	6360878	760.6	379450	6360878	760.6
126040	06CF287	21.35	24.40	3.05	22.88	T203	Paramount	9	379450	6360878	960.3	90	-60	243.0		379462	6360878	940.5	379450	6360878	940.5
126054	06CF287	64.05	67.10	3.05	65.58	T203	Paramount	9	379450	6360878	960.3	90	-60	243.0		379483	6360878	903.6	379450	6360878	903.6
126067	06CF287	94.55	97.60	3.05	96.08	T203	Paramount	9	379450	6360878	960.3	90	-60	243.0		379498	6360878	877.1	379450	6360878	877.1
126081	06CF287	137.25	140.30	3.05	138.78	T203	Paramount	9	379450	6360878	960.3	90	-60	243.0		379519	6360878	840.2	379450	6360878	840.2
126110	06CF287	216.55	219.60	3.05	218.08	T203	Paramount	9	379450	6360878	960.3	90	-60	243.0		379559	6360878	771.5	379450	6360878	771.5
126118	06CF287	240.95	243.00	2.05	241.98	T203	Paramount	9	379450	6360878	960.3	90	-60	243.0		379571	6360878	750.8	379450	6360878	750.8
125904	06CF288	9.15	12.20	3.05	10.68	T204	Paramount	9	379308	6360888	929.6	N/A	-90	183.0		379308	6360888	919.0	379308	6360888	919.0
125919	06CF288	54.90	57.95	3.05	56.43	T204	Paramount	9	379308	6360888	929.6	N/A	-90	183.0		379308	6360888	873.2	379308	6360888	873.2
125928	06CF288	82.35	85.40	3.05	83.88	T204	Paramount	9	379308	6360888	929.6	N/A	-90	183.0		379308	6360888	845.8	379308	6360888	845.8
125933	06CF288	97.60	100.65	3.05	99.13	T204	Paramount	9	379308	6360888	929.6	N/A	-90	183.0		379308	6360888	830.5	379308	6360888	830.5
125944	06CF288	122.00	125.05	3.05	123.53	T204	Paramount	9	379308	6360888	929.6	N/A	-90	183.0		379308	6360888	806.1	379308	6360888	806.1
125952	06CF288	146.40	149.45	3.05	147.93	T204	Paramount	9	379308	6360888	929.6	N/A	-90	183.0		379308	6360888	781.7	379308	6360888	781.7
125963	06CF288	179.95	183.00	3.05	181.48	T204	Paramount	9	379308	6360888	929.6	N/A	-90	183.0		379308	6360888	748.2	379308	6360888	748.2
126120	06CF289	6.10	9.15	3.05	7.63	T206	Paramount	9	379320	6361049	958.4	N/A	-90	183.0		379320	6361049	950.8	379320	6361049	950.8
126131	06CF289	39.65	42.70	3.05	41.18	T206	Paramount	9	379320	6361049	958.4	N/A	-90	183.0		379320	6361049	917.2	379320	6361049	917.2
126142	06CF289	64.05	67.10	3.05	65.58	T206	Paramount	9	379320	6361049	958.4	N/A	-90	183.0		379320	6361049	892.8	379320	6361049	892.8
126154	06CF289	100.65	103.70	3.05	102.18	T206	Paramount	9	379320	6361049	958.4	N/A	-90	183.0		379320	6361049	856.2	379320	6361049	856.2
126171	06CF289	152.50	155.55	3.05	154.03	T206	Paramount	9	379320	6361049	958.4	N/A	-90	183.0		379320	6361049	804.4	379320	6361049	804.4
126181	06CF289	173.85	176.90	3.05	175.38	T206	Paramount	9	379320	6361049	958.4	N/A	-90	183.0		379320	6361049	783.0	379320	6361049	783.0
125806	06CF290	27.45	30.50	3.05	28.98	T124	Paramount	9	379539	6361181	1052.4	90	-70	291.0		379549	6361181	1025.1	379539	6361181	1025.1
125816	06CF290	57.95	61.00	3.05	59.48	T124	Paramount	9	379539	6361181	1052.4	90	-70	291.0		379559	6361181	996.5	379539	6361181	996.5
125833	06CF290	100.65	103.70	3.05	102.18	T124	Paramount	9	379539	6361181	1052.4	90	-70	291.0		379574	6361181	956.3	379539	6361181	956.3
125861	06CF290	176.90	179.95	3.05	178.43	T124	Paramount	9	379539	6361181	1052.4	90	-70	291.0		379600	6361181	884.7	379539	6361181	884.7
125875	06CF290	219.60	222.65	3.05	221.13	T124	Paramount	9	379539	6361181	1052.4	90	-70	291.0		379615	6361181	844.6	379539	6361181	844.6
125897	06CF290	286.70	289.75	3.05	288.23	T124	Paramount	9	379539	6361181	1052.4	90	-70	291.0		379637	6361181	781.5	379539	6361181	781.5

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.
UTM NAD 27 was used for Northing and Easting data

									Top of Drillholes UTM NAD 27							For Easting Plots Centre of ABA Interval			For Northing Plots Centre of ABA Interval		
Sample Id.	Hole Id	From	To	Interval	Centre of Interval	Old Collar	Ore Zone	Zone	Easting	Northing	Elevation	Azimuth	Inclination	Length	Length	Easting	Northing	Elevation	Easting	Northing	Elevation
		(m)	(m)	(m)	(m)						(m)			(m)	(ft)						
Tailings																					
LIARD ZONE							Liard														
PARAMOUNT							Paramount														
WEST BRECCIA							West Breccia														
High-Sulphide Historic Core																					
T112 (171' - 172')	T112	52.1	52.4	0.30	52.27	T112	West Breccia														
T113 (81' - 82')	T113	24.7	25.0	0.30	24.84	T113	West Breccia														
T113 (983' - 985')	T113	299.6	300.2	0.61	299.92	T113	West Breccia														
T140 (30' - 31')	T140	9.1	9.4	0.30	9.30	T140	Main														
T166 (389' - 390')	T166	118.6	118.9	0.30	118.72	T166	Main														
T185 (116' - 117')	T185	35.4	35.7	0.30	35.51	T185	West Breccia														
T207 (261.5' - 262')	T207	79.7	79.9	0.15	79.78	T207	Paramount														
T207 (269' - 271')	T207	82.0	82.6	0.61	82.30	T207	Paramount														

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.
Sample 126352: drilling mineral log (ANLP) and litho log are different (BRVL)
Samples 147051, 147070, 147087, and 147097: drilling mineral log (ANPF) and litho log are different (ANAP)

Legend:

T	Trace
W	weak
M	moderate
S	strong

Sample	Rock	Rock Code						Alteration Minerals					%
Id.	Code	Description	Mineralization Style	Ch	Ep	Bt	Se	K	Si	Hm	Cb	Tm	Mt
				Chlorite	Epidote	Biotite	Sericite	K-spar	Silicic	Hematite		Tourmaline	Magnetite
Main Zone													
14130	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	Cu diss & qtz veins					S	W				
14144	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	Cu diss & veins	M				M-S	W	M			
14148	FAUL	Faults	Cu diss	S				S		W			
14156	FAUL	Faults	Mb fracture					W					
14162	D/BS	Diabase/Basic dyke											W
14169	PPFQ	Quartz-Feldspar or Feldspar-Quartz Porphyry	Cu, Mb qtz veins & diss					M-S					
14232	PPAU	Plagioclase-Augite-phyric Andesite	dis, stkwk, bx vns, Mb frct					W					
14250	PPAU	Plagioclase-Augite-phyric Andesite	stkwk	W				W		W			
14260	PPAU	Plagioclase-Augite-phyric Andesite	stkwk, Cp, Bn in vns	W				W		W			
14276	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	stkwk, dis, Cp,Mb vns, Mb frct	W	W								
14295	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	stkwk, Py vns	W	W			W		W			
14301	ANNX	Altered Andesite	STKWK, Mb Frct					S					
14323	PPAU	Plagioclase-Augite-phyric Andesite	STKWK, Cp-V	W				W					
14332	PPAU	Plagioclase-Augite-phyric Andesite	STKWK, Mb-Frct	W				W		W			
14345	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	STKWK, Dis	W				W					
14348	PPAU	Plagioclase-Augite-phyric Andesite	STKWK, Dis, Mb-Frct	W				W				W	
14797	PPAU	Plagioclase-Augite-phyric Andesite	STKWK, Dis, MB-Frct	W				W					
14808	FAUL	Faults	STKWK, MB-Frct, SHEAR	W				S					
14816	PPAU	Plagioclase-Augite-phyric Andesite	STKWK, PY-Vns	W				M		W			
14828	PPAU	Plagioclase-Augite-phyric Andesite	STKWK, Dis, MB-Frct	W				W					
14844	ANDS	Andesite	STKWK, CP-Vn, Dis	W									
14680	PPAU	Plagioclase-Augite-phyric Andesite	STKWK, MB-Frct, CP-Frct	W				W					W
14871	ANLP	Andesitic LapilliTuff	STKWK, CP-Vn,Frct, Dis, SHR,	W	W			W		W			
14887	ANTF	Andesitic Tuff	STKWK, CP-Vn, Dis	W	W					W			
14689	PPFQ	Quartz-Feldspar or Feldspar-Quartz Porphyry	Py,Cp, dis, cb-qtz vn, frct	W			W	S		X			
14695	PPAU	Plagioclase-Augite-phyric Andesite	Py,Cp, dis	M-S				W		W			T
14742	ANLP	Andesitic LapilliTuff	Cp dis, Cp,Bn qtz-cb vn, Mb frct	W				W			W		1
14666	BRVL	Volcanic Breccia	STKWK, Dis, MB-Frct	W	W			W					
14685	DIOR	Diorite	STKWK, Dis, MB-Frct	W				M					
14685B	DIOR	Diorite											
14545	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	Py,Cp dis	W-M						W			
14565	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	Cp cb-qtz-ch stkwk	W				W		W			
14571	PPPL	Plagioclase or Feldspar Porphyry	Py,Cp dis, Mb cb-qtz-ch vn	W				W		X			
14578	PPAU	Plagioclase-Augite-phyric Andesite	Py dis, Cp ch stckwk	W-M				W-M		X			
14578B	PPAU	Plagioclase-Augite-phyric Andesite											
14598	PPAU	Plagioclase-Augite-phyric Andesite	Cp,Py dis	M									5
14893	PPAU	Plagioclase-Augite-phyric Andesite	Mal frct-1%, Cp dis	W									5
14899	PPAU	Plagioclase-Augite-phyric Andesite		X						X			
14908	ANLP	Andesitic LapilliTuff	Cp,Bn qtz-cb stkwk, Cp dis	W				W					
14917	PPPL	Plagioclase or Feldspar Porphyry	Bn dis, qtz-cb vn	X		X		W-M					
14925	ANLP	Andesitic LapilliTuff	Cp qtz-cb vn, dis	W	X			X		W			3
14998	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	STKWK	W									
15862	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	STKWK, MB-Frct	W	W			W					
15870	ANLP	Andesitic LapilliTuff	STKWK	W				M		W			
15879	BRVL	Volcanic Breccia	STKWK	W	W			W		W			

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.
Sample 126352: drilling mineral log (ANLP) and litho log are different (BRVL)
Samples 147051, 147070, 147087, and 147097: drilling mineral log (ANPF) and litho log are different (ANAP)

Legend:

T	Trace
W	weak
M	moderate
S	strong

Sample Id.	Rock Code	Rock Code Description	Mineralization Style	Alteration Minerals Ch Chlorite	Ep Epidote	Bt Biotite	Se Sericite	K K-spar	Si Silicic	Hm Hematite	Cb	Tm Tourmaline	% Mt Magnetite
15887	ANTF	Andesitic Tuff	STKWK, Dis	W	W				W		W		
15891	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	STKWK	W				W		W			
15908	PPFQ	Quartz-Feldspar or Feldspar-Quartz Porphyry	STKWK, MB-Frct, Dis, Flt	W									
15911	ANDS	Andesite	STKWK, Dis	W				W					
125285	ANAP	Feldspar Augite Phyric Andesite	quartz stwrk, dis	W			M	W					
125288	D/BS	Late Mafic Dyke	dis	W			W						
125293	ANDS	Andesite	stwk, dis, Mo-slick	W			M	W					
125305	ANPF	Andesite, feldspar-phyric	stwk	M			W						
125311	ANPF	Andesite, feldspar-phyric	stwk	M			W	W		W	W		
125703	ANAU/ANAP	Augite-phyric to augite-plagioclase-phyric andesite	fract coatg	W			W	W					0.5
125728	ANLP	Lapilli Tuff	q-cb-stkwk, diss, strgs, frct	W			W	W		W			0.5
125755	ANAP	Plagioclase-augite-phyric andesite	q-cb-v, diss, fract coatg				M	S					
125772	ANLP/ANBX	Andesitic lapilli tuff to breccia	q-cb-v, diss, Mo-slicks	M			W						
125795	ANLP/ANBX	Andesitic lapilli tuff to breccia	q-cb-v, strgs	M			M			W			0.5
125422	ANAP	Andesite, feldspar- and pyroxene phyric	Vn, vnlt	M			W-M	T		T			T
125435	ANAP	Andesite, feldspar- and pyroxene phyric	Dis, vnlt, moly fracture	M			M	M		W			5
125452	ANAP	Andesite, feldspar- and pyroxene phyric	Vnlt, hlv, dis, moly fracture	W			M	T		W		T	
125476	ANPF	Andesite, feldspar phyric	Vn, dis	M-S			W	S					
125490	ANPF	Andesite, feldspar phyric	Stringers, hlv	M	M		M			M-S			
126192	ANAU	Augite Feldspar Phyric Andesite	Cp, Py dis, str	W/M			M	M	M		W		X
126206	ANAP	Feldspar Augite Phyric Andesite	Cp, Py dis, qcv, Mo/Sp, Cp frac	W			W/M	W	M/S	X	W		0.5
126225	HVBX	Hydrothermal Magnetite Pseudobreccia	Cp dis, Cp, Mo/Sp qz cb vn, frac	W			S	W/M	M		W		2.5
126244	ANTF/ANLP	Andesite Tuff- Lapilli Tuff	Cp dis, str, qz cb vn, Mo/Sp frac	W			S	W	W/M	W	W		X
126266	ANLP/ANBX	Andesite Lapilli Tuff-Breccia	Cp dis, Mo/Sp frac	W/M			S	W	W	X	W		0.5
126279	FAUL	Fault	Cp dis, Mo/Sp frac	W			M/S	W	M/S		W		X
126288	ANTF/ANBX	Andesite Tuff-Breccia	Cp dis, qcv, Mo, Cp frac	W/M			S	W	S	W	W		X
126297	ANAP	Andesite, augit- and feldspar phyric	Cp, Py dis, qcv	W/M			M		W/M	W	W		0.0
126314	ANAP	Andesite, augit- and feldspar phyric	Cp, Py dis, qcv, frac	W/M			M/S	X	M/S	X	W		0.0
126329	ANAP	Andesite, augit- and feldspar phyric	Cp, Mo, Bn dis, str, qcv, frac	W			S	W/M	M/S	W	W		0.0
126337	ANAP	Andesite, augit- and feldspar phyric	Cp, Py, Bn dis, str, Cp, Mo qcv, frac	W/M			M	X	W/M	X	W		X
126351	ANTF	Andesite Tuff	Bn, Mo qcv, Cp, Bn dis, str	W			W/M	W	W/M		W		0.0
126427	ANPF	Andesite	Dis, hlv	M-S			W			X-W			
126430	HVBX	Hydrothermal Breccia	Dis	W-M			M	W		X			
126434	ANPF	Andesite		M			M			X-W	W		
126443	ANDS	Andesite	Dis, stringers	W-M			S			X	W		4.0
126449	D/BS	Baisc Dyke		X									
126464	ANPF	Andesite	Stringer, dis	M	W		S			X			T
126492	ANPF	Andesite	Stringer, dis	W			S	W		X			2.0
145655	ANAU	Augite phyric Andesite	Py dis, str, qcv, Cp dis, str	W	M		M/S	W	M	W/M	W		3.0
145669	ANAU	Augite phyric Andesite	Py, Cp dis, str, frac	W			M/S	W	W/M	M	W		2.5
145685	ANLP	Andesite Lapilli Tuff	Cp, Py cqv, dis	W			W/M	W	W/M		W		0.5
145694	ANTF/ANLP	Andesite Tuff-Lapilli Tuff	Cp dis, str, qcv, Py dis	W	X		M		W	X	W		3.0
145708	ANBX/ANLP	Andesite Breccia/Lapilli Tuff	Cp, Py str, dis	W			M	X	W		W		3.0
145723	ANDS	Andesite	Cp dis, str, qcv, Py qcv	W			M	X	W	W	X		1.5
146798	ANLP/ANTF	Andesitic Lapilli Tuff	Bn, Cp str, cqv, Mo cqv	X			M	X	W		W		X
146824	ANLP/ANTF	Andestic Tuff-Lapilli Tuff	Cp, Bn cqv	W			M		W	X	W		0.5

Project:	**Schaft Creek**
Client:	Copper Fox Metals Inc.
Data:	**Sample Information**
Comments:	2005 core samples were collected by MDAG on Feb 7'07.
	2006 core samples were collected by Copper Fox personnel in Sep '07.
	For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.
	Sample 126352: drilling mineral log (ANLP) and litho log are different (BRVL)
	Samples 147051, 147070, 147087, and 147097: drilling mineral log (ANPF) and litho log are different (ANAP)

Legend:

T	Trace
W	weak
M	moderate
S	strong

Sample Id.	Rock Code	Rock Code Description	Mineralization Style	Alteration Minerals Ch Chlorite	Ep Epidote	Bt Biotite	Se Sericite	K K-spar	Si Silicic	Hm Hematite	Cb	Tm Tourmaline	% Mt Magnetite
146831	FAUL	Fault Zone	Cp dis, mas, cqv, Mo frac	W			M	M	W/M	X	W		1.0
146843	ANLP/ANTF	Andesitic Lapilli Tuff	Cp str, Cp, Bn hlv, Mo/Sp frac	X			M		W	X	W		1.5
146861	ANDS	Andesite	Cp str, cqv, frac	X			W		X	X	X		1.5
146868	ANTF	Andesitic Tuff	Cp dis, str, hlv, frac, Mo frac	X			X	X	X		W		0.5
126352	ANLP (BRVL)	Andesitic Lapilli Tuff (Volcanic Breccia)	Cp str, dis	W			W	X			X		T
126358	BRVL	Lapilli Volcanoclastic Breccia	cp dis	W/M			W	X			M		T
126374	BRVL	Lapilli Volcanoclastic Breccia	Cp dis, str	M			M			X	W		10.0
126384	BRVL/ANTF	Lapilli Volcanoclastic Breccia	Cp, Bn qz cb vn	W			W/M	X			W		5.0
126391	ANTF/ANLP	Intermediate Tuff - Lapilli Tuff	Cp, Bn str, Mo frac	W			W			X	M		3.0
146172	ANXX	Very strongly altered andesite	Veinlet	W			W	M		W			0.5
146182	ANAU	Phyllically-altered augite-phyric andesite	Veinlet, stringer, quartz vein	W			W						0.5
146203	ANAU	Phyllically-altered augite-phyric andesite	Quartz vein, stringer, hairline vein		W		W	M					
146214	FAUL	Fault	Diss, hairlien vein, fracture coating	W	W		W			W			
146221	ANPF	Phyllically-altered plagioclase-phyric andesite	Diss, slickensides	W			W	W					0.5
146238	ANBX	Phyllically-altered andesitic breccia	Diss, hairline veins, slickensides	M			W						1.0
147034	ANPF	Feldspar-phyric Andesite	Cp dis, Cp, Mo cqv, Mo frac	W			W/M	M	W		W		X
147038	ANXX	Alteration Zone	Cp, Mo, Bn qcv, hlv, Cp dis, Mo/Sp frac	X			W	M/S	X		W		X
147051	ANPF (ANAP)	Plagioclase-phyric or Feldspar-phyric Andesite (Andesite)	Cp, Bn hlv, Cp, Py dis, str, mas	X	W		X	W	X		W		2.0
147070	ANPF (ANAP)	Plagioclase-phyric or Feldspar-phyric Andesite (Andesite)	Py dis, str, qcv, frac, mas	W	W/M				X	X	X		5.0
147087	ANPF (ANAP)	Plagioclase-phyric or Feldspar-phyric Andesite (Andesite)	Py str, dis, mas, frac	W	W			W	W		X		2.0
147097	ANPF (ANAP)	Plagioclase-phyric or Feldspar-phyric Andesite (Andesite)	Py str, dis, frac, Cp dis, str	M/S			W	W/M	W	W	W	X	1.5
145508	ANBX	Phyllically-altered andesitic pyroclastic breccia	Veinlets, stringers	W			W						
145527	ANBX	Phyllically-altered andesitic pyroclastic breccia	Quartz veins, stringers	W			W						T
145543	ANBX	Phyllically-altered andesitic pyroclastic breccia	Quartz veins, stringers				W	W					T
145562	ANBX	Phyllically-altered andesitic pyroclastic breccia	Veinlets, stringers	W			W						T
145576	ANBX	Potassically altered andesitic pyroclastic breccia	Disseminations, quartz veins				W	M					
145601	ANBX	Propylitically-altered andesitic pyroclastic breccia	Veinlets, stringers, disseminations	W	M		W						
146297	ANLP	Andesite, lapilli tuff	Dis, vnlt, hlv, stringer, vein	M			M	W					
146314	ANLP	Andesite, lapilli tuff	Vn, vnlt	M			M-S						T
146335	ANLP	Andesite, lapilli tuff	Vn, vnlt, hlv	M-S			M-S						T
146352	ANAP	Andesite	Vnlt	M-S			M-S						T
146368	ANAP	Andesite	Vn, vnlt, hlv	M			M-S			X			T
146390	ANAP	Andesite	Vnlt, hlv, vn	M-S			M	X					T
146508	ANTF/ANLP	Andesitic Tuff-Lapilli Tuff	Bn qcv, Mo frac	X			M/S	W	M/S	X	M		X
146526	ANTF/ANLP	Andesitic Tuff-Lapilli Tuff	Bn, Mo qcv, hlv				W/M	W	W	X	W/M		1.0
146544	ANTF/ANLP	Andesitic Tuff-Lapilli Tuff	Bn, Cp qcv, dis	W			W/M	W/M	M		M		0.0
146565	ANXX	Alteration Zone	Bn, Mo, Cp qcv, Bn dis, str	W			M/S	S	M		M		0.0
146589	ANTF/ANLP/ANBX	Andesitic Tuff-Lapilli Tuff-Breccia	Mo, Bn, Cp qcv, Bn, Cp str, dis	W			M		W		W/M		1.0
146613	ANTF/ANLP/ANBX	Andesitic Tuff-Lapilli Tuff-Breccia	Cp dis, cqv, str, mas	W			S	W	M		M		X
146627	ANXX	Alteration Zone	bn strg	X			S	S			S		0.0
146637	PPFQ	Highly Altered Feldspar Porphyry	py, cp dis				M	S			M		0.0
146649	PPFQ	Feldspar Porphry	py dis, cp, mb qz-cb vn	W			W	S			W		0.0
146657	PPFQ	Feldspar Porphry	py dis, bn strg, qz-cb vn				W	S			W		0.0
146676	PPFQ	Highly Altered Feldspar Porphyry	bn strg, cp dis	M			S	M			S		0.0
125188	ANPF	Plagioclase-phyric andesite	Bn dis & quartz vn, Cp quartz vn	W			M	S			W		
125198	FAUL	Fault	Mb, Cp qz vn	S			W	W			S		

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.
Sample 126352: drilling mineral log (ANLP) and litho log are different (BRVL)
Samples 147051, 147070, 147087, and 147097: drilling mineral log (ANPF) and litho log are different (ANAP)

Legend:

T	Trace
W	weak
M	moderate
S	strong

Sample Id.	Rock Code	Rock Code Description	Mineralization Style	Alteration Minerals Ch Chlorite	Ep Epidote	Bt Biotite	Se Sericite	K K-spar	Si Silicic	Hm Hematite	Cb	Tm Tourmaline	% Mt Magnetite
125207	ANPF	Plagioclase-phyric andesite	Mb stkw	W			S	S		W/M	S		
125228	PPFQ	Quartz-feldspar porphyry	Bn, Cp, Mb qz vn, dis, Mb fract	W			M	S		W	M		
125244	PPFQ	Quartz-feldspar porphyry	Cp dis, Bn qz vn, strg	W			W	S	M		W		
125257	D/BS	Late mafic dyke	Py, dis	W							W		
125278	PVPF	Hematized plagioclase-augite-phyric andesite	None	M	W/M			W	M	W			3.0
125596	ANLP	Lapilli Tuff	Cp,Bn dis, cb-qz vn, Py dis	W			M			X	W		7.0
125610	ANLP	Lapilli Tuff	Bn, Cp str, qz vn, Mo cb-qz vn bx	W			M	M			M		
125626	PPFQ	Feldspar Porphyry	Cp, Py dis, Cp, Mo stwk	W			M	S		X	M		
125641	ANLP/ANBX	Lapilli/Breccia Crystal Tuff	Cp, Mo cb-qz vn stwk, Mo frac	M			W/M	X		X	M		X
125669	PPFQ	Feldspar Porphyry	Cp, Mo qz-cb vn, Py dis	W			W	M		X	W		1.0
125690	ANLP	Lapilli Tuff	Cp str	W	W			X		W	W		
West Breccia Zone													
14018	PPFQ	Quartz-Feldspar or Feldspar-Quartz Porphyry	Disseminated + Vein	W	W		W	W					
14021	TOBR	Tourmaline Breccia	Hydro Bx Matrix (vein) + diss	M	W		M	M	M			X	
14036	TOBR	Tourmaline Breccia	Stockwork + disseminated	M			S	M	M			X	
14043	TOBR	Tourmaline Breccia	Stockwork + disseminated	W	W		M	M	W			X	
14060	BRIV	Intrusive Breccia or Felsic Igneous Breccia	Disseminated in matrix	M	M		M	M?		M?			
14067	ANPF	Plagioclase-phyric or Feldspar-phyric Andesite	Disseminated, vein	S	W		S	W	W				
14076	ANDS	Andesite	STKWK, Dis	W									
14083	ANDS	Andesite	STKWK	W	W								
14099	PPFQ	Quartz-Feldspar or Feldspar-Quartz Porphyry	Dis	W									
14103	TOBR	Tourmaline Breccia	Dis	W	W			W				M	
125046	ANPF	Andesite, feldspar-phyric	Vein	M	W		W	W	W	W	W		
125068	ANPF	Andesite, feldspar-phyric	Vnlt, Mo/Specularite in fractures	M	M		W	W			W		
125073	ANDS	Andesite	Bx, vnlt, vein	M	X		W	W/M	W		W		
125079	ANPF	Andesite, feldspar-phyric	Bx, vein, vnlts				M	S	M		W		
125084	ANDS	Andesite	Vein, vnlt, dis	M	M		M	W	W	X	X		1
125127	ANPF	Andesite, feldspar-phyric	vnlt, dis, Bn in fract	M	X		M	W	W	X	W		5.0
125129	ANDS	Andesite	vein, dis	M	X		M	W	W/M	W	W		1.0
125134	BRXX	Intrusive Breccia	Vein, vnlt, dis, fract, bx	W			W	M	W/M	X	W		7.0
125142	BRXX	Intrusive Breccia	Dis, fract, vein, bx, vnlt	M	X		W	W	W/M		W/M		X
125149	ANDS	Andesite	None	M/S			W	X	W		M		X
125154	ANPF	Andesite, feldspar-phyric	Vnlt, veins, dis	W/M			W	M	W		W/M		
125165	ANPF	Andesite, feldspar-phyric	Dis, vnlt	M	M		W	T/W	W	X	X		X
125176	ANPF	Andesite, feldspar-phyric	Stringers	S			W	W	W	X			X
146112	ANLP/ANTF	Andesitic Lapilli Tuff	Cp dis, Cp, Bn frac	W	W		X	W	W	W			0.5
146115	D/BS	Mafic Dyke	Py dis, concretions	W	X						W		2.0
146124	ANAU	Augite-phyric Andesite	Cp hlv, str, dis, qz vn	W					W	X	X		X
146127	PPFQ	Feldspar Porphyry	Py dis	W			S	W	S	X	X		0.0
146135	ANPF	Feldspar-phyric Andesite	None	W	W		W		W		W		1.5
146149	ANPF	Feldspar-phyric Andesite	Cp dis	M	X		X		W		X		2.0
146161	ANBX	Andesite Breccia	None	W	M		X		W		X		2.5
146164	ANDS	Andesite	None	X	W				W	W	W		1.5
145951	FAUL	Fault Zone	Cp dis, str	W/M			M	X	W	W	X		0.0
145956	ANTF/ANBX	Andesitic Tuff-Breccia	Cp dis, Cp, Bn str, Cp cqv, frac	W			W		W/M	M	W		1.5
145974	ANTF/ANBX	Andesitic Tuff-Breccia	Bn dis	W			W		W		X		X

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.
Sample 126352: drilling mineral log (ANLP) and litho log are different (BRVL)
Samples 147051, 147070, 147087, and 147097: drilling mineral log (ANPF) and litho log are different (ANAP)

Legend:

T	Trace
W	weak
M	moderate
S	strong

Sample	Rock	Rock Code		Alteration Minerals									%
Id.	Code	Description	Mineralization Style	Ch	Ep	Bt	Se	K	Si	Hm	Cb	Tm	Mt
				Chlorite	Epidote	Biotite	Sericite	K-spar	Silicic	Hematite		Tourmaline	Magnetite
145982	D/BS	Mafic Dyke	None	W					W		W		1.0
145992	ANXX	Alteration Zone	Cp, Mo qcv, Py dis	W/M	X		M/S	W	W/M	X	W		X
145999	ANTF/ANBX	Andesitic Lapilli Tuff-Breccia	None	W	X		W/M		W	W	X		1.0
145834	ANPF/PPFQ	Plagioclase feldspar-phyric Andesite/ Quartz Feldspar Porphyry		W	X		W	W					
145842	HVBX/PPFQ	Quartz Feldspar Porphyry/Hydrothermal Breccia	Cp dis	M	M		S	M	W		S		
145852	HVBX/PPFQ	Quartz Feldspar Porphyry/Hydrothermal Breccia	Cp, Bn dis, frac, quartz vein (qv)	M/S	S		S	S	M		S		
145857	ANPF	Plagioclase feldspar-phyric Andesite		M	W		W	M			W		3.0
145871	ANPF	Plagioclase feldspar-phyric Andesite	Py str	M	W		W			X	W		3.0
145608	ANDS/FAUL	Fault Zone/Andesite	Py dis, frac	W	W						W		T
145614	ANDS	Andesite	Py cev	W	W						W		T
145628	ANDS	Andesite	Py carbonate vein	M							S		T
145640	ANDS	Andesite	Py dis, str, Mt dis	W	X						W/M		5.0
145646	ANDS	Andesite	Mt str, Py dis	W	M						M		1.0
Paramount Zone													
125965	HVBX	Intrusive-Hydrothermal Breccia	Cp, Py, Mo, Bn dis, str, frac, qz vn	W	W		W/M	W	M/S	W	W		X
125974	HVBX	Intrusive-Hydrothermal Breccia	Py qz cb vn, str, dis, frac, Cp dis	W			W/M	X	W/M		W		0.0
125983	HVBX	Intrusive-Hydrothermal Breccia	Cp, Py dis, frac	W	W		M	W	W/M	W	W		1.0
125988	D/BS	Mafic Dyke	Py dis	M	W		X		W	X	M		1.0
126007	GRDR	Granodiorite	Cp, Mo/Sp frac, str, qz cb vn, dis	W			M	S	S		W		0.0
126031	GRDR	Granodiorite	Cp dis, qz cb vn, Mo/Sp rac	W			M	M/S	S		W		0.0
126040	INBX	Intrusive Breccia	Primary magmatic	W			W	W					
126054	INBX	Intrusive Breccia	Primary magmatic, veinlet	W			W	W		X			T
126067	GRDR	Granodiorite	Disseminations, stringers	M	W		W	W		W			
126081	GRDR	Granodiorite	Disseminations, veins, veinlets	X		X		M					
126110	D/BS	Mafic Dyke	None	X									
126118	GRDR	Granodiorite	Veins, veinlets	M-S			M	M					
125904	HVBX/BRIG	Breccia, intrusive and hydrothermal	Bn, Cp, Mo bx, qzcb vn, dis, frac	W			W	X	W/M	X	W	X	1.0
125919	ANTF	Andedsite crystal tuff	Cp, Mo, Bn, frac, qz vn, dis, str	W			W	X	W	X	X		1.0
125928	ANLP	Andesite Lapilli Tuff	Cp, Mo, Bn dis, str	W			W/M	X	M/S	X	W		2.0
125933	D/BS	Mafic Dyke	None				W		W	W	W		0.5
125944	ANLP/ANTF	Lapilli Andesite	Py dis, str	X			W	X	W/M	W	W		1.5
125952	PPFQ	Feldspar Porphyry	Py dis, qz cb vn, frac	M			M/S	W	S	X	W		0.0
125963	ANDS	Andesite	Py dis, str, frac, Cp qz vn, dis	W			W	W	M/S	X	W		0.5
126120	PPFQ	Feldspar Porphyry	Bn, Cp dis, Mo frac	W			M	W	S		X		0.0
126131	PPFQ/BRXX	Feldspar Porphyry Breccia	None	W			M	W	S		W		0.0
126142	FAUL	Fault	None	W			M	X	S		X		X
126154	FAUL	Fault	Cp cqv, str, Mo, Cp frac	W			M	X	M		W		0.0
126171	ANDS/ANPF	Andesite / Feldspar-phyric Andesite	Cp, Py dis, Mo/Sp, cqv, frac	W			S	M	S		W/M		0.0
126181	ANDS/ANPF	Feldspar-phyric Andesite / Andesite	Py dis, str, mas	W/M				X	X	X	W		2.0
125806	GRDR	Granodiorite	dis, vnlt	X			W	W	S		X		0
125816	D/BS	Mafic Dyke	None						M/S		X		1.0
125833	GRDR	Granodiorite	Mo, Cp, Bn frac	W			W/M	M/S	S		X		0.0
125861	GRDR	Granodiorite	Cp, Py dis,str,qz vn,frac, Mo/Sp frac	W			M	W	S		W	W	0.0
125875	GRDR	Granodiorite	Mo/Sp, Cp frac, Cp, Bn qz vn, dis, str	W			M	W/M	S		W		0.0
125897	GRDR	Granodiorite	Cp, Bn dis, qz vn, str, Mo/Sp str, frac	W			M	W	S		W	W	0.0

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.
Sample 126352: drilling mineral log (ANLP) and litho log are different (BRVL)
Samples 147051, 147070, 147087, and 147097: drilling mineral log (ANPF) and litho log are different (ANAP)

Legend:

T	Trace
W	weak
M	moderate
S	strong

Sample Id.	Rock Code	Rock Code Description	Mineralization Style	Alteration Minerals									%
				Ch Chlorite	Ep Epidote	Bt Biotite	Se Sericite	K K-spar	Si Silicic	Hm Hematite	Cb	Tm Tourmaline	Mt Magnetite
Tailings													
LIARD ZONE		Tailings sample											
PARAMOUNT		Tailings sample											
WEST BRECCIA		Tailings sample											
High-Sulphide Histor													
T112 (171' - 172')													
T113 (81' - 82')	GRDR	Granodiorite											
T113 (983' - 985')	TOIV												
T140 (30' - 31')													
T166 (389' - 390')													
T185 (116' - 117')	GRDR	Granodiorite											
T207 (261.5' - 262')	GRDR	Granodiorite											
T207 (269' - 271')	GRDR	Granodiorite											

Project:	**Schaft Creek**
Client:	Copper Fox Metals Inc.
Data:	**Sample Information**
Comments:	2005 core samples were collected by MDAG on Feb 7'07.
	2006 core samples were collected by Copper Fox personnel in Sep '07.
	For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample	Sulphides %						Assay Data				
Id.	Cp	Bn	Py	Mb	Other	Total	Cu	Mo	Au	Ag	MoS2
	Chalcopyrite	Bornite	Pyrite	Molybdenite			(%)	(%)	(g/t)	(g/t)	(%)
Main Zone											
14130	T	~1				1.0	0.555	0.008	0.39	3.3	
14144	T	~1				1.0	0.290	0.008	0.20	2.2	
14148		T				T	0.275	0.020	0.17	1.2	
14156		T		1.0		1.0	0.204	0.005	0.07	1.0	
14162							0.115	0.051	0.09	<0.5	
14169	1.0	1.0		<1		<2	0.386	0.016	0.18	3.0	
14232	0.5	1.0	0.5	0.5		2.5	0.325	0.011	0.21	1.8	
14250	0.5	1.0	0.5	0.5		2.5	0.300	0.038	0.33	2.0	
14260	1.0	0.5	0.5	T		2.0	0.505	0.016	0.9	3.1	
14276	2.0	T	0.5	1.0		3.5	0.136	0.003	<0.01	1.0	
14295	0.5	T	0.5	T		1.0	0.250	0.001	0.07	0.5	
14301	T		T	0.5		0.5	0.241	0.023	0.09	0.6	
14323	0.5	0.5	T	T		1.0	0.200	0.005	0.18	1.6	
14332	0.5	0.5	T	1.0		2.0	0.336	0.010	0.16	1.5	
14345	2.0	0.5	0.5	0.5		3.5	0.559	0.020	0.19	2.4	
14348	1.0	0.5	0.5	0.5		2.5	0.461	0.013	0.13	1.4	
14797	0.5	0.5		0.5		1.5	0.184	0.034	0.10	1.0	
14808	0.5	0.5		2.0		3.0	0.257	0.040	0.28	1.7	
14816	T	0.5	1.0	T		1.5	0.387	0.008	0.57	2.3	
14828	0.5	2.0		0.5		3.0	0.317	0.019	0.74	2.3	
14844	1.0	0.5	0.5	T		2.0	0.249	0.010	0.16	1.0	
14680	1.0	0.5		0.5		2.0	0.373	0.035	0.25	2.5	
14871	2.0	0.5		T		2.5	0.365	0.034	0.10	0.7	
14887	0.5		0.5			1.0	0.196	0.00	0.07	0.7	
14689	0.5		1.0	0.5		2.0	0.213	0.008	0.07	0.4	
14695	T		0.5			0.5	0.182	0.059	0.13	0.7	
14742	T			0.5		0.5	0.223	0.071	0.17	1.0	
14666	0.5		1.0	T		1.5	0.163	0.002	0.07	0.3	
14685	0.5		2.0	T		2.5	0.455	0.013	0.18	0.6	
14685B											
14545	T		T			T	0.113	0.001	0.02	0.4	
14565	T					T	0.289	0.002	0.14	0.6	
14571	2.0		1.0	0.5		3.5	0.593	0.011	0.13	1.8	
14578	T		1.0			1.0	0.293	0.002	0.04	0.7	
14578B											
14598	T		T			T	0.075	0.005	0.02	0.3	
14893							0.164	0.008	0.12	0.9	
14899							0.032	0.002	0.03	0.7	
14908	1.5	T				0.5	0.113	0.005	0.08	0.7	
14917		0.5				0.5	0.361	0.001	0.31	2.5	
14925	T					T	0.182	0.001	0.11	1.0	
14998	T	T	0.5	T		0.5	0.169	0.007	0.14	0.5	
15862	T	T		0.5		0.5	0.116	0.008	0.14	0.6	
15870	0.5	T	T	0.5		1.0	0.157	0.002	0.09	0.8	
15879	0.5	T		T		0.5	0.224	0.003	0.15	1.5	

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample			Sulphides %					Assay Data			
Id.	Cp	Bn	Py	Mb	Other	Total	Cu	Mo	Au	Ag	MoS2
	Chalcopyrite	Bornite	Pyrite	Molybdenite			(%)	(%)	(g/t)	(g/t)	(%)
15887	1.0	T		0.5		1.5	0.285	0.008	0.28	1.8	
15891	T	0.5		0.5		1.0	0.234	0.011	0.21	1.5	
15908	0.5	0.5		0.5		1.5	0.421	0.032	0.38	2.4	
15911	0.5	0.5		0.5		1.5	0.179	0.017	0.15	1.0	
125285	0.5	0.5				1.0					
125288						T					
125293	T	1.0		T		1.0					
125305		T				T					
125311		T				T					
125703	T					T	0.156	0.028	0.10	<0.5	
125728	0.5	T		0.2		0.7	0.252	0.013	0.28	1.0	
125755	1.0		1.0	0.3		2.3	0.360	0.055	0.52	<0.5	
125772	0.5	0.5		0.5		1.5	0.269	0.045	0.44	1.3	
125795	T	1.5				1.5	0.142	0.002	0.07	0.6	
125422	T	T				T	0.210	0.002	0.19	1.9	
125435	0.5			T		0.5	0.200	0.021	0.16	<0.5	
125452	3.0	0.5		T		3.5	0.741	0.029	0.31	2.3	
125476	1.5			0.5		2.0	0.400	0.011	0.20	1.1	
125490	0.5		T			0.5	0.210	0.000	0.03	<0.5	
126192	T		T		Ma/Gp	T	0.205	0.004	0.13	<0.5	
126206	0.5		T	0.5	Gp/Sp	1.0	0.159	0.011	0.10	<0.5	
126225	0.5			1.0	Gp/Sp	1.5	0.268	0.027	0.23	<0.5	
126244	T			0.5	Gp/Sp	0.5	0.222	0.027	0.15	0.9	
126266	T			T	Gp/Sp	T	0.173	0.012	0.08	<0.5	
126279	T			T	Gp/Sp	T	0.215	0.020	0.11	<0.5	
126288	0.5			T	Gp	0.5	0.306	0.026	0.19	<0.5	
126297	0.5		T		Ma/Gp	0.5	0.222	0.010	0.11	<0.5	
126314	0.5		0.5		Gp	1.0	0.600	0.010	0.17	<0.5	
126329	0.5	T		T	Gp	0.5	0.272	0.006	0.26	0.6	
126337	0.5	T	0.5	0.5	Ma/Gp	1.5	0.466	0.025	0.35	1.0	
126351	T	0.5		0.5	Gp	1.0	0.204	0.008	0.18	1.2	
126427			3.0			3.0	0.044	0.001	0.01	<0.5	
126430	T		T			T	0.015	0.001	0.01	<0.5	
126434					Gp		0.014	0.001	0.01	<0.5	
126443			1.5			1.5	0.050	0.001	0.02	<0.5	
126449							0.006	0.001	<0.01	<0.5	
126464			1.0	T		1.0	0.203	0.001	0.04	<0.5	
126492	0.5		1.0			1.5	0.186	0.004	0.09	<0.5	
145655	T		1.0		Gp	1.0	0.132	0.001	0.09	<0.5	
145669	0.5		0.5		Gp	1.0	0.214	0.001	0.05	<0.5	
145685	2.0		T		Gp	2.0	0.180	0.001	0.02	<0.5	
145694	0.5				Gp	0.5	0.173	0.002	0.06	<0.5	
145708	0.5		0.5			1.0	0.195	0.002	0.08	<0.5	
145723	2.5		T			2.5	0.477	0.010	0.07	0.9	
146798	0.5	0.5		T		1.0	0.335	0.017	0.22	1.3	
146824	T	T				T	0.208	0.004	0.14	0.6	

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample			Sulphides %				Assay Data				
Id.	Cp	Bn	Py	Mb	Other	Total	Cu	Mo	Au	Ag	MoS2
	Chalcopyrite	Bornite	Pyrite	Molybdenite			(%)	(%)	(g/t)	(g/t)	(%)
146831	0.5			T		0.5	0.460	0.021	0.15	1.6	
146843	T	T		T	Gp/Sp	T	0.211	0.012	0.08	1.2	
146861	0.5				Gp	0.5	0.094	0.014	0.11	<0.5	
146868	0.5			T		0.5	0.321	0.007	0.10	0.7	
126352	0.5					0.5	0.460	0.023	0.16	<0.5	
126358	T					T	0.297	0.007	0.08	<0.5	
126374	T					T	0.205	0.003	0.08	<0.5	
126384	T	1.0				1.0	0.166	0.003	0.25	0.6	
126391	T	T			Gp	T	0.217	0.014	1.18	<0.5	
146172	T	T		T		T	0.254	0.027	0.21	0.6	
146182	T	0.5				0.5	0.312	0.008	0.34	1.2	
146203	0.5			T		0.5	0.191	0.007	0.58	0.7	
146214	T			T		T	0.260	0.003	0.06	<0.5	
146221	0.5		T	T		0.5	0.583	0.003	0.19	0.8	
146238	0.5		0.5	T		0.5	0.080	0.002	0.02	<0.5	
147034	T			0.5	Gp	0.5	0.471	0.060	0.24	1.9	
147038	0.5	T		0.5	Sp	1.0	0.346	0.016	0.17	0.7	
147051	0.5	T	T			0.5	0.231	0.009	0.03	<0.5	
147070			2.5			2.5	0.024	0.002	0.01	<0.5	
147087			7.0			7.0	0.019	0.002	0.02	<0.5	
147097	T		1.0			1.0	0.063	0.002	0.09	<0.5	
145508	0.5	T				0.5	0.063	0.002	0.05	<0.5	
145527	T		1.0			1.0	0.195	0.002	0.21	<0.5	
145543	0.5	T		T		0.5	0.198	0.010	0.26	0.5	
145562	0.5	T		T		0.5	0.187	0.013	0.21	<0.5	
145576	0.5		2.0	T		2.5	0.246	0.116	0.21	<0.5	
145601	0.5					0.5	0.241	0.008	0.30	0.9	
146297	T	0.5		T		0.5	0.710	0.013	0.59	3.5	
146314	T	T	T	T		T	0.245	0.009	0.21	0.9	
146335	T	T		T		T	0.217	0.004	0.11	1.0	
146352	T					T	0.136	0.003	0.13	0.7	
146368	T		T			T	0.170	0.003	0.23	<0.5	
146390	T	0.5			Gp	0.5	0.262	0.005	0.26	0.90	
146508		1.0		T	Gp	1.0	0.127	0.003	0.17	0.5	
146526		T		T		T	0.178	0.001	0.22	0.8	
146544	T	T				T	0.131	0.001	0.15	<0.5	
146565	T	1.0		T	Gp	1.0	0.150	0.009	0.19	0.8	
146589	T	0.5		T		0.5	0.209	0.032	0.22	25.1	
146613	T					T	0.274	0.038	0.12	0.5	
146627		T				T	0.152	0.005	0.23	1.0	
146637	1.0					1.0	0.345	0.023	0.05	<0.5	
146649	T		1.0	T	Gp	1.0	0.086	0.009	0.03	<0.5	
146657		3.0	T			3.0	0.249	0.011	0.09	1.9	
146676	T	0.5				0.5	0.223	0.009	0.06	1.3	
125188	0.5	1.0				1.5	0.413	0.007	0.39	1.8	
125198	T			T		T	0.285	0.019	0.21	1.4	

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample	Sulphides %						Assay Data				
Id.	Cp Chalcopyrite	Bn Bornite	Py Pyrite	Mb Molybdenite	Other	Total	Cu (%)	Mo (%)	Au (g/t)	Ag (g/t)	MoS2 (%)
125207				T		T	0.168	0.002	0.16	<0.5	
125228	0.5	3.0		1.0		3.5	0.220	0.027	0.06	1.20	
125244	T	1.0				1.0	0.176	0.002	0.16	1.10	
125257			T			T	0.011	0.002	0.01	0.60	
125278						0	0.030	0.001	0.01	0.60	
125596	1.0	T	0.5			1.5	0.215	0.007	0.16	<0.5	
125610	T	T		T		T	0.068	0.003	0.17	<0.5	
125626	3.0		3.0	T		3.0	0.247	0.004	0.23	<0.5	
125641	T			T		T	0.230	0.038	0.43	1.1	
125669	0.5		5.0	T	Gp	5.5	0.366	0.012	0.09	<0.5	
125690	0.5					0.5	0.062	0.001	0.02	<0.5	
West Breccia Zone											
14018			1.0			1.0	0.147	0.007	0.06	<0.5	
14021	2.0		T			2.0	0.173	0.036	0.03	<0.5	
14036	4.0					4.0	0.189	0.061	0.04	5.8	
14043	0.0					2.0	0.153	0.034	0.15	2.0	
14060	T-1					T-1	0.280	0.032	0.04	<0.5	
14067	1.0					1.0	0.247	0.014	0.03	<0.5	
14076	T		T			T	0.173	0.005	0.16	<0.5	
14083	T		1.0			1.0	0.130	0.001	0.01	<0.5	
14099	0.5		1.0			1.0	0.157	0.002	0.02	1.1	
14103	1.0		T			1.0	0.266	0.022	0.02	1.0	
125046				T		T	0.124	0.005	0.090	0.7	
125068	T	T		0.5	Sp	0.5	0.466	0.009	0.200	3.3	
125073	2.0	2.0		0.5		5.5	0.883	0.037	0.370	9.5	
125079	4.0	T		1.0		5.0	1.522	0.108	3.080	18.8	
125084	3.0			T		3.0	0.600	0.015	0.270	3.7	
125127	0.5	0.5		T		1.0	0.166	0.006	0.13	<0.5	
125129	0.5	0.5		0.5		1.5	0.293	0.010	0.22	1.2	
125134	2.5	T		0.5		3.0	0.681	0.016	0.18	1.0	
125142	1.0			0.5		1.5	0.269	0.015	0.05	0.6	
125149						0.0	0.206	0.004	0.12	0.6	
125154	0.5	0.5		T		1.0	0.100	0.010	0.05	0.9	
125165	0.5	T				0.5	0.271	0.002	0.22	1.1	
125176	0.5	1.0				1.5	0.467	0.001	0.18	4.1	
146112	T	T				T	0.162	0.001	0.36	<0.5	
146115			T			T	0.004	0.001	<0.01	<0.5	
146124	0.5				Gp	0.5	0.063	0.003	0.01	<0.5	
146127			1.0			1.0	0.026	0.001	0.01	<0.5	
146135						0.0	0.035	0.001	0.06	<0.5	
146149	T					T	0.021	0.001	<0.01	<0.5	
146161							0.030	0.001	0.01	<0.5	
146164							0.003	0.001	0.01	<0.5	
145951	0.5				Gp	0.5	0.191	0.002	0.03	<0.5	
145956	1.0	T			Gp	1.0	0.207	0.005	0.03	<0.5	
145974		T				T	0.025	0.001	0.01	<0.5	

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample	Sulphides %						Assay Data				
Id.	Cp Chalcopyrite	Bn Bornite	Py Pyrite	Mb Molybdenite	Other	Total	Cu (%)	Mo (%)	Au (g/t)	Ag (g/t)	MoS2 (%)
145982						0.0	0.002	0.001	<0.01	<0.5	
145992	T		T	T	Gp	T	0.179	0.006	0.04	<0.5	
145999					Gp	0.0	0.068	0.001	0.01	<0.5	
145834							0.056	0.001	0.01	<0.5	
145842	T					T	0.024	0.001	0.01	<0.5	
145852	0.5	T				0.5	0.123	0.001	0.01	<0.5	
145857							0.009	0.001	0.01	<0.5	
145871		T				T	0.030	0.001	0.02	<0.5	
145608			5.0			5.0	0.058	0.002	0.03	<0.5	
145614			3.0			3.0	0.170	0.002	0.08	<0.5	
145628			T		Gp	T	0.086	0.002	0.03	<0.5	
145640			3.0			3.0	0.126	0.001	0.05	<0.5	
145646			T			T	0.142	0.002	0.07	<0.5	
Paramount Zone											
125965	2.0	T	0.5	T		2.5	0.325	0.009	0.03	<0.5	
125974	0.5		2.5		Gp	3.0	0.053	0.005	<0.01	<0.5	
125983	0.5		0.5		Gp	1.0	0.154	0.018	0.02	<0.5	
125988			T		Gp/Az	T	0.006	0.001	<0.01	<0.5	
126007	0.5			0.5	Gp/Sp	1.0	0.130	0.020	0.17	<0.5	
126031	0.5			0.5	Gp/Sp	1.0	0.139	0.006	0.14	0.8	
126040	1.0		1.0		Ma	2.0	0.262	0.033	0.02	<0.5	
126054	0.5		T	T		0.5	0.148	0.008	0.01	<0.5	
126067	0.5		T			0.5	0.217	0.009	0.02	<0.5	
126081	1.5		0.5	0.5		2.5	0.620	0.009	0.05	3.1	
126110							0.210	0.038	0.06	1.0	
126118	1.0		0.5			1.5	0.548	0.017	0.10	<0.5	
125904	0.5	0.5		T	Ma	1.0	0.290	0.032	0.18	0.6	
125919	2.5	T		0.5	Gp	3.0	0.430	0.032	0.12	0.6	
125928	0.5	T		T	Gp	0.5	0.100	0.011	0.07	1.1	
125933					Gp		0.005	0.001	<0.01	<0.5	
125944			0.5		Gp	0.5	0.025	0.002	0.01	<0.5	
125952			2.5		Gp	2.5	0.020	0.001	0.01	<0.5	
125963	0.5		0.5		Gp	1.0	0.350	0.006	0.07	<0.5	
126120	T	0.5		T	Ma	0.5	0.198	0.005	0.20	2.1	
126131					Ma	0.0	0.085	0.001	0.05	<0.5	
126142					Ma	0.0	0.069	0.002	0.28	<0.5	
126154	0.5			0.5		1.0	0.230	0.008	0.21	1.5	
126171	0.5		1.5	0.5	Sp	2.5	0.163	0.009	0.03	<0.5	
126181			1.0			1.0	0.019	0.001	0.01	<0.5	
125806			T			T	0.054	0.001	0.02	<0.5	
125816						0.0	0.007	0.001	<0.01	<0.5	
125833	0.5	T		0.5	Gp	1.0	0.384	0.011	0.22	2.6	
125861	1.0	T		0.5	Sp/Gp	1.5	0.318	0.019	0.23	0.9	
125875	0.5	0.5		0.5	Sp/Gp	1.5	0.303	0.014	0.26	1.6	
125897	0.5	T		0.5	Sp/Gp	1.00	0.054	0.015	0.15	<0.5	

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample	Sulphides %						Assay Data				
Id.	Cp	Bn	Py	Mb	Other	Total	Cu	Mo	Au	Ag	MoS2
	Chalcopyrite	Bornite	Pyrite	Molybdenite			(%)	(%)	(g/t)	(g/t)	(%)
Tailings											
LIARD ZONE											
PARAMOUNT											
WEST BRECCIA											
High-Sulphide Histor											
T112 (171' - 172')							0.036	0.002	0.01	0.9	0.003
T113 (81' - 82')							0.075	0.003	0.03	1.1	0.005
T113 (983' - 985')							0.219	0.007	0.08	1.0	0.012
T140 (30' - 31')							0.739	0.029			0.049
T166 (389' - 390')											
T185 (116' - 117')							0.010	0.002			0.003
T207 (261.5' - 262')							0.095	0.017	0.06	0.7	0.028
T207 (269' - 271')							0.095	0.017	0.06	0.7	0.028

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Description	Sampling Notes
Main Zone		
14130	Moderate- Strongly Altered Plagioclase-Phyric Andesite. Variable colour from pink to grey, with pink overprinting resulting from K -alteration of andesite. Most intense flanking cm-scale low angle quartz veins, and forming meter-scale alteration envelopes, pervasive into host. Areas of high fracturing dominated by carbonate-chlorite filling. Randoml oriented, low-high angle mm-cm scale quartz veining, with erratic sulphide mineralization of chalcopyrite and bornite in trace to <1% over the section.	Subsample collected from top of rejects stored in white plastic bucket; dry, grey and pink (granite?) gravel and fines
14144	Moderately-Strongly Altered Plagioclase-Phyric Andesite. Variably altered, similar to 6.4 - 36.6 m. Locally strong fault gouge and breccia developed. 57.9 - 61.0 m cm sections of fault gouge and broken core. 61.0 - 64.0 m medium to high angle fault gouge and breccia along 30cm length with a 20cm section at 61.9 m of a low angle hematized vein breccia.	Subsample collected from top of rejects stored in white plastic bucket; dry, grey and pink (granite?) gravel and fines
14148	Fault Zone - Tectonic Deformation and Alteration Zone. 70.0 - 73.0 m cm-dm sections of intense deformation and ateration, similar to above. Strong chloritization and silicification. Disseminated bornite associatd with chloritization and quartz vein material. Chloritization over-printing K-alteration. 73.1 - 76.2 m intense chloritization and fault gouge anastomizing at low angle to core. Chloritization over-printing K-alteration. Cm sections of highly comminuted rock developing rock flour and soft clay rich zones.	Subsample collected from top of rejects stored in white plastic bucket; saturated, medium grey gravel and fines
14156	Fault Zone - Tectonic Deformation and Alteration Zone. 87.2 - 96.0 m relict protolith of possible feldspar porphyry displaying variable K-alteration.	Subsample collected from top of rejects stored in white plastic bucket; dry, grey and pink (granite?) gravel and fines
14162	107.3-109.3 m: Mafic Dyke. Dark grey, fine grain, with 10% 0.5-3mm carbonate amygdules. Upper and lower contact at low angle with strong carbonatization and bleaching along 20cm , especially the lower contact. Section contains mm low angle carbonate veinlets. Upper contact displays weak chill margin. 106.1-107.3 m: Feldspar-Quartz Porphyry. Variable K-alteration diffuse through section with meter lengths of intense alteration. 103.6 - 107.3 m Very low angle sub-parallel mm-cm quartz veins with 10% bornite along 10cm length.	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines
14169	Feldspar-Quartz Porphyry. Predominantly pink. Variable K-alteration ranging from moderate to strong. MM stockwork and quartz veinlets concentrated in zones. Bornite and chalcopyrite mineralization associated with with stockwork with bornite being greater than chlcopyrite, with total sulphide concentrations of up to 7% along 30cm. Minor molybdenite. Sulphides are also finely disseminated in wall rock with stringer-type concentrations associated with quartz veins. Late molybdenite is smeared or painted along fracture planes trace chalcopyrite. Typically the fractures are at a low-medium angle and average 1per meter.	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines
14232	Plagioclase-augite porphyry andesite... pink-grey. Moderate potassic alteration. Core in part strongly fractured. Plagioclase phenocrysts light green, epidote alteration? Moderate stockwork of mm veins, medium-low angle, in part vuggy, mm to 2cm spacing: Quartz veins, carbonate veins, talc(?)-chlorite veins. Total sulphides 2%: 0.5% each, bornite, chalcopyrite, pyrite in veins and adjacent to veins. Very fine chalcopyrite commonly replacing augite crystals.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines; low weight remaining
14250	Augite porphyry. Similar to above. Fine grained, porphyritic. Colour generally dark green-grey with minor pink grey, weak potassic alteration: 85.3 - 101.2 m higher abundance of quartz-stockwork with chalcopyrite, bornite. Quartz-carbonate stockwork strongly variable, generally low abundance.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14260	Augite porphyry. Similar to above. Fine grained, porphyritic. Colour generally dark green-grey with minor pink grey, weak potassic alteration: 85.3 - 101.2 m higher abundance of quartz-stockwork with chalcopyrite, bornite. Quartz-carbonate stockwork strongly variable, generally low abundance. 96.0 - 106.7 m Alternating weak chlorite alteration and weak potassic alteration. Weak quartz-carbonate stockwork, ~0.5% each chalcopyrite, bornite, pyrite, trace molybdenite.	Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines
14276	Plagioclase-phyric, porphyritic andesite. Fine grained, massive, generally competent. Fine grained groundmass with 10% 0.5-2mm plagioclase phenocrysts. Colour medium green-grey, locally beige. Alteration weak: Chlorite, epidote, hematite, locally potassic. Veining, stockwork generally weak-moderate: mm-1cm quartz veins, carbonate veins, cm-10cm spacing, random orientation. Locally strong stockwork and vein breccia, ft size. Sulphides predominantly in stockwork, minor disseminated. Moly commonly on slickensides, in fractures. Sulphide abundance 0.5% for each chalcopyrite, bornite, trace molybdenite. Locally high chalcopyrite abundance in mm to 10mm veins, essentially massive chalcopyrite veins. 139.0 - 150.9 m dark green chlorite alteration. Low vein density. Rare 1mm massive chalcopyrite veins and molybdenite coated slickensides, fractures.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines; low weight remaining
14295	Plagioclase-phyric, porphyritic andesite. Fine grained, massive, generally competent. Fine grained groundmass with 10% 0.5-2mm plagioclase phenocrysts. Colour medium green-grey, locally beige. Alteration weak: Chlorite, epidote, hematite, locally potassic. Veining, stockwork generally weak-moderate: mm-1cm quartz veins, carbonate veins, cm-10cm spacing, random orientation. Locally strong stockwork and vein breccia, ft size. Sulphides predominantly in stockwork, minor disseminated. Moly commonly on slickensides, in fractures. Sulphide abundance 0.5% for each chalcopyrite, bornite, trace molybdenite. Locally high chalcopyrite abundance in mm to 10mm veins, essentially massive chalcopyrite veins. 199.0 - 212.7 m fine grained, dark green-grey, minor pink potassic alteration. Core competent. Weak stockwork of 1mm carbonate veins, quartz veins, in part with high abundance of sulphides (pyrite, chalcopyrite). Common 5-10mm pink potassic vein halos. Overall sulphides: 0.5-1% of each chalcopyrite, pyrite, in veins, halos.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14301	Altered Andesite - Moderate-Strong. Variable pink to grey. Variable dm-meter scale K-alteration ranging from moderate to strong, with dm-meter sections of weak incipient alteration. Light green alteration associated with mm carbonate veinlets appears to overprint the K-alteration, and may in part be epidote and serictic alteration. Areas of intense K-alteration completely obliterate protolith and are usually associated with stockwork arrray of mm-cm carbonate-quartz veins containing disseminated molybdenite ar bornite. 10.8 - 12.8 m medium grey-green, fine grained with mm carbonate amygdules and mm low angle carbonate veinng. Possibly a late mafic dyke.	Subsample collected from top of rejects stored in white plastic bucket; dry, grey and pink (granite?) gravel and fines
14323	Augite-Phyric Andesite. Medium grey, fine grain, with 3-5% 1-4mm anhedral augite phenocrysts displaying hematite rich rims and cores of chlorite-hematite. Some show distinct pseudomorphing of hexagonal crystal form. Overall this unit exhibits weak pervasive chloritization. Low to medium angle carbonate-chlorite fractures averaging 6/meter.	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines
14332	Augite-Phyric Andesite. Medium grey, fine grain, with 3-5% 1-4mm anhedral augite phenocrysts displaying hematite rich rims and cores of chlorite-hematite. Some show distinct pseudomorphing of hexagonal crystal form. Overall this unit exhibits weak pervasive chloritization. Low to medium angle carbonate-chlorite fractures averaging 6/meter.	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Description	Sampling Notes
14345	Weakly-Moderately Altered Plagioclase-Phyric Andesite. Pale pink-grey. Weak to moderate pervasive K-alteration. Where alteration is quite strong the feldspar phenocryst component of the rock become highly accentuated. 2-5mm, medium-high angle carbonate-quartz-molybdenite veins spaced at 2-3/meter. 125.0 - 142.8 m moderate to strong K-alteration overprinted by a network of mm-cm fluid phase, dominated by carbonate and mineralized with fine grain disseminated chalcopyrite carrying up to 7%, and forming a stockwork array with diffuse boundaries and does not appear to be vein associated. More of a late mineralization phase which may also be contributing to painted molybdenite on fracture planes.	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines
14348	Augite-Phyric Andesite. Fractured containing carbonate-chlorite filling and K-alteration envelopes on a mm-cm scale. Upper contact is fault controlled at high angle.	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines
14797	Variably Altered Augite-Feldspar-Phyric Andesite. Intensely broken core resulting in high rubble content. Variable K-alteration from moderate to strong associated with mm-cm quartz-carbonate stockwork veining dominated by bornite mineralization. Moderate pervasive chloritization along meter lengths, accompanied by intense chlorite hairline chlorite veinlets forming a crackle breccia. Overall 5% magnetite.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14808	Fault Zone. 41.3 - 49.0 m; very strong chloritization and carbonatization resulting in veining and crackle brecciation of an earlier intense K-alteration phase. Heavy gouge and rubble developed along meter lengths. Late chlorite veinlets throughout. Dm section of low angle shearing and brittle deformation resulting in mylonite.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14816	Variably Altered Augite -Phyric Andesite. Moderate to intense pervasive K-alteration and chloritization completely obliterating protolith. Ghosty spotty hematization forming cm patches resulting from the overprinting by K-alteration. Highly fractured with cm sections of fault gouge. Mm-cm medium to high angle quartz-carbonate -chlorite veins some heavily mineralized with bornite.	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines
14828	Marginal Alteration-Transition Zone -Augite-Phyric Andesite. Variable K-alteration ranging from weak to moderate with patchy mm-cm ghosty relic host inclusions, and associated with pervasive chloritization imparting a green hue to the host rock. 96.9 - 104.8 m; mm randomly oriented quartz-carbonate veins forming a weak stockwork array.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14844	Andesite. Grey, fine grain, masive, Incipient crackle brecciation developed by hairline to 3mm randomly oriented carbonate veinlets. Rare 5mm quartz-carbonate veins with bornite. Rare molybdenite painted fractures.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14680	Augite-Feldspar-Phyric Andesite. Grey-green, massive with weak patchy K-alteration, rare mm epidote and darker blotchy areas of high magnetite. Mm randomly oriented quartz-carbonate veins with molybdenite and bornite, about 2/meter.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14871	Andesitic Tuff-Lapilli Tuff. Medium grey, massive to interbeded tuff-lapilli tuff with dm sections of lithic tuff. Bedding at very low angle to core. Dominant mineralization is associated with mm quartz-carbonate veinlets carrying disseminated chalcopyrite and bornite and occasional chalcopyrite stringers. All veining in a random array sometimes concentrated sufficiently to form a weak stockworks. Minor molybdenum painted fracture surfaces. Dm sections of intercalated feldspar-phyric andesite with sharp high angle contacts.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14887	Andesitic Tuff. Massive fine grain rock displaying weak low angle bedding and intercalated lithic tuff horizons. Weak epidote forming cm patches.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14689	Feldspar-porphyry. Massive, competent. Pink colour, potassic alteration. Rock made up of very fine grained felsic groundmass and ~20% white feldspar phenocrysts and 1-2 yellowish, boxy, altered phenocrysts showing relict cleavage (pseudomorph after augite ?). Rare quartz eyes. 1% finely disseminated sulphides, chalcopyrite, pyrite. Comment: Rock considered as an altered variety of PPAU. Low vein density, dm spacing, ranndom orientation: hairline to 3mm quartz-carbonate-veins, chlorite veins, pink carbonate-hematite veins. Accessory chalcopyrite, molybdenite in veins.	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines
14695	Plagioclase-phyric and augite phyric andesite. Colour medium green grey. 1mm greenish plagioclase phenocrysts , 1-3% altered augite phenocrysts. Common (5%) black-dar breccia portions grading into crackle breccia. Matrix carbonate-chlorite-red hematite. Moderate density hairline to 5mm veins with blackish halo (chlorite-carbonate), low angle to medium angle. Accessory chalcopyrite in veins and breccia. Sharp gradation. 28.3-29.9: Strongly altered, veined, rusty, in part rubble. Alteration hematite, chlorite. 29.1-29.4 m 3cm quartz-carbonate vein 45CA and 3cm strongly molybdenite-coated vein and fault 75CA (i.e. subhorizontal).	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines
14742	Lapilli andesite and andesite, variously textured and altered. Unit divided into subdivisions 155.7 -164.3 m ANLP Colour medium grey. Weak chloritic and potassic alteration. Low vein density, medium angle.	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines
14666	Volcanic Breccia. Variable grey-green colour, fine grain matrix. Varaible pervasive chloritization and weak carbonatization. Dm sections of cm size oxide inclusions. Randomly oriented hairline carbonate veinlets occasionally forming a weak stockwork array. Dm sections of weak K-alteration. Rare quartz-carbonate veinlet exhibiting biotite selvage. Locally disseminated and stringer chalcopyrite concentrations. Meter sections with mm-cm autobrecciated clasts as well as xenoliths ranging from fine grain mafic to intermediate in composition, with occasional porphyry clast. Alternating meter sections of interbedded andesite and voalcanic breccia. Rare molybdenite painted fractures. 51.8 - 57.9 m ; high in irregular shaped oxide void fillings and inclusions, up to 10% by volume.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14685	Diorite. Medium grey, massive. Variable chloritization, with sericite overprinting. Dm scale K-alteration associated with carbonate chlorite veins. 7% oxide and fine grain disseminated pyrite. Dm section of weak cumulate texture. 97.8 - 107.0 m; massive with a low vein density.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines (see 14685B)
14685B		Subsample collected from bottom of rejects stored in white plastic bucket; dry, medium grey gravel and fines (see 14685)

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Description	Sampling Notes
14545	Porphyritic, plagioclase-phyric andesite. Very fine grained, igneous, felsic groundmass hosting abundant 0.3-2mm plagioclase phenocrysts and some augite phenocrysts, bot altered. Core competent, moderate to strongly fractured. Colour 1/2 - 3/4 dark green grey; 1/4 to 1/2 medium pink green grey, i.e weak potassic alteration. Alteration generally weakly chloritic, 1/4 to 1/2 weak patchy, potassic alteration. Potassic alteration areas are spotty, with 20% dark green chloritic (with tourmaline?) spots. Accessory red hematite spots. Accessory disseminated pyrite, chalcopyrite, bornite. Rare epidote patches. Veining: Generally low vein density, quartz veins, carbonate veins, chlorite veins. Veins mm wide, low angle-medium angle, with mm wide pink halos. Sulphides: Trace to accessory pyrite, chalcopyrite, bornite in rare mm size patches, veins and disseminations. Rare 5-10mm size chalcopyrite patches or discontinuous veins.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14565	Slightly brecciated, in situ, jig-saw fit. Colour 70% pink, potassic alteration. Weak breccia: Distention breccia, randomly oriented mm fractures filled with chlorite, carbonate. Breccia matrix 2-5%, containing chlorite. 1/10 hematite alteration. Accessory chalcopyrite as a) disseminations, mm patches; b) in thin veins.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14571	Plagioclase porphyry. Massive, medium grained. Colour light pink grey, greenish grey. 40-60% 0.5-3mm size plagioclase phenocrysts, 5% interstitial chlorite grains, fine grained felsic matrix. Upper contact sharp, irregular, chilled, with andesite wall rock clasts in plagioclase porphyry. Chilled phase has 1% altered augite phenocrysts and rare quartz eyes. Common accessory (1%) chalcopyrite as disseminations and in veins. Trace molybdenite in veins. Two 5cm fault gouges 45CA at 85.0m and 85.3 m. Lower contact irregular: PPPL and ANPF are intertwined, fine grained andesite being broken up and intruded by medium grained plagioclase porphyry.	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines
14578	Plagioclase-augite-phyric andesite; medium grained-coarse grained plagioclase- and augite phenocrysts; colour pale pink grey, i.e potassic alteration. Variable abundance of phenocrysts. Moderate vein density, variable, in places cm spacing, crackle breccia of dark veins, low angle, carbonate-chlorite-veins. 102.1 - 102.4 m Several 1mm high-molybdenite slickensides; at 108.5 m one 4cm quartz vein with 2% molybdenite. Overall accessory chalcopyrite, bornite, molybdenite.	Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines (see 14578B)
14578B		Subsample collected from bottom of rejects stored in white plastic bucket; dry, light grey gravel and fines (see 14578)
14598	Fine grained, plagioclase-phyric, augite-phyric andesite. Colour mostly medium green grey, rare (<1/10) pink potassic alteration, mostly as halos around veins. Moderate vein density, cm-10cm spacing, hairline to 5mm quartz veins, low angle to medium angle. Several 1-5cm carbonate-chlorite-veins and vein breccia with high sulphide abundance (several % of coarse grained chalcopyrite, pyrite, molybdenite)	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14893	Plagioclase-phyric and augite-phyric andesite. Fine grained, massive, competent core. Fine grained, felsic, igneous grondmass hosting 20% 0.2-2mm plagioclase phenocrysts and 1-5% dark, altered augite phenocrysts. Variable phenocryst abundance. Colour generally medium-dark green grey and medium brown grey, alternating at 1.5 - 3.0 m intervals. Weak chorititic and weak potassic alteration. Generally low vein density, 10cm spacing, random orientation, <1 to 10mm width. Rare 10-30mm veins. Scattered portions (0.3 - 1.5 m) of higher vein density/stockwork, cm spacing. Trace to ccessory sulphides in veins: chalcopyrite, bornite. Approximate subdivisions according to geological characteristics: 4.9 - 23.8 m PPAU Dark green grey with minor medium brown grey portions. Strongly fractured, rusty, limonitic, in part with malachite coating.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14899	Plagioclase-phyric and augite-phyric andesite. Fine grained, massive, competent core. Fine grained, felsic, igneous grondmass hosting 20% 0.2-2mm plagioclase phenocrysts and 1-5% dark, altered augite phenocrysts. Variable phenocryst abundance. Colour generally medium-dark green grey and medium brown grey, alternating at 1.5 - 3.0 m intervals. Weak chorititic and weak potassic alteration. Generally low vein density, 10cm spacing, random orientation, <1 to 10mm width. Rare 10-30mm veins. Scattered portions (0.3 - 1.5 m) of higher vein density/stockwork, cm spacing. Trace to ccessory sulphides in veins: chalcopyrite, bornite. Approximate subdivisions according to geological characteristics: 23.8 - 40.5 m PPAU and ANDS, fine grained, low phenocrysts population.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14908	Lapilli andesite/agglomerate-andesite. Core competent, massive. Distinct fragmental texture, heterolithic clasts, andesitic. Clasts size < 1 to > 5 cm. Colour generally medium brown grey, minor dark green grey. Weak chlorite and potassic alteration. - Generally low vein density, but slightly higher than above: cm to dm spacing, medium angle.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14917	Plagioclase porphyry. Core competent, rock massive. Colour pale pink grey. Potassic alteration. 30-60% 1-3mm white and pink feldspar phenocrysts in fine grained felsic matrix. Contacts: Both upper and lower contact show ghost breccia over 0.6m. lower contact shows well preserved, sharp, chilled contact (50-60CA) of adjacent volcanic. Thi suggests that PPPL is probably older, i.e. pre-dated the andesite. Low vein density, dm spacing, 1-10mm quartz veins, with trace/accessory bornite, chalcopyrite. Quartz veins in part vuggy, open. Sharp contact 60CA	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14925	Ditto above, to 74.4 m. Lapilli-andesite/agglomerate. Core competent, massive texture. Size of adesitic clasts mm to 5cm. Clasts shape angular and rounded. Both matrix anc clasts andesitic. Colour medium green grey and brown grey. Low vein density, dm spacing, medium angle. Weak chloritic, potassic, hematite alteration. Rare cm wide, pink potassic selvages. Rare 0.3-1.0m size stockworks. 132.3 - 135.3m strongly fractured, core rubbly. Trace sulphides in veins, hairline to 1mm, chalcopyrite, bornite, molybdenite; and chalcopyrite fracture coating. Molybdenite commoly as fracture coating. Chalcopyrite forming 0.5-2mm veins with high chalcopyrite abundance, one per 1.5 - 3m. dm size portions with stockwork and higher sulphides abundanc: 84.7-85.0m; 87.8-88.4m; 91.1-91.4m; 99.4-100.0m; 100.6-101.8m; 110.9-112.8m; 114.3-114.9m; 117.3 118.0m; 120.7-121.9m; 127.7-128.3m; 134.1-137.1m.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14998	Feldspar-Phyric Andesite. Grey-green, 10-15% mm anhedral-euhedral feldspar phenocrysts in a very fine grain matrix. In part tuffaceous. 5% mm oxide inclusions. Weak pervasive chloritization and weak carbonatization. Randomly oriented mm-1/2cm quartz-carbonate-chlorite veins forming dm sections of stockworks, variably mineralized with chalcopyrite, bornite and molybdenite. Occasional molybdenite painted fracture surfaces. Late mm unmineralized arbonate veins.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
15862	Feldspar-Phyric Andesite. Green-grey, 10-15% mm anhedral-euhedral feldspar phenocrysts. 5% oxide inclusions. Varaible dm-m sections of K-alteration and carbonate alteration associated with quartz-carbonate-chlorite and carbonate-quartz stockworks. 75.4 - 91.4 m; high fracture and fault density at variable angles from low to high associated with carbonate-chlorite veins. Occasional molybdenite painted fracture surfaces.	Subsample collected from top of rejects stored in white plastic bucket; moist, dark grey gravel and fines

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Description	Sampling Notes
15870	Andesitic Lapilli Tuff-Agglomerate. Grey-green, lapilli fragments in fine grain andesitic matrix. Variable pervasive carbonatization from weak to strong, bleaching an earlier pervasive chloritization. High stockwork vein density of mm-cm quartz-chlorite-carbonate veins and chlorite-carbonate veins forming dm sections of crackle breccia. Rare mm pyrite stringers and strands. Chalcopyrite, bornite and molybdenite associated with the quartz-chlorite veins. Late cross-cutting unmineralized carbonate veins. Rare cm sections of highly comminuted rock forming bands at medium to high angle. Vuggy veins associated with carbonate phase. Cm sections of K-alteration, vein related.	Subsample collected from top of rejects stored in white plastic bucket; saturated, medium grey gravel and fines
15879	Andesite Breccia-Agglomerate. Angular mm-cm mafic-intermediate fragments amd mm oxide inclusions, auto-brecciated. Fine grain matrix. Moderate pervasive chloritization Lower contact fault controlled with 3cm of gouge at high angle to core.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
15887	Andesitic Tuffite. Pale olive green. Fine grain. Interbedded clastic and pyroclastic facies. Riddled with a high density stockwork array of mm carbonate-chlorite veinlets mineralized with fine grain bornite, and displaying mm-1/2cm silica alteration selvages manifest as grey tones overprinting an earlier pervasive alteration event of carbonate-sericite soaking the protolith. Fine mm scale bedding oriented at very low angle to core. Sharp high angle lower contact.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
15891	Feldspar-Phyric Andesite. Green-grey. Variable chloritization overprinted by intermittent pervasive weak to strong carbonatization and dm sections of moderate to strong K-alteration associated with randomly oriented mm-cm quartz-carbonate-chlorite veins. 158.8 m ; very low angle carbonate-quartz vein brecciating host rock, displaying moderate K-alteration. Fault associated vein walls.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
15908	Feldspar-Quartz Porphyry. Andedral to subhedral feldspar phenocrysts and anhedral quartz compacted into a massive rock with disseminated chalcopyrite.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
15911	Andesite. Green-grey. Pervasive carbonatization and chloritization, with cm sections of intense carbonatization. 10% angular to round oxide inclusions. Minor bornite and chalcopyrite associated with quartz-carbonate veins.	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
125285		
125288		
125293		
125305		
125311		
125703		
125728		
125755		
125772		
125795		
125422		
125435		
125452		
125476		
125490		
126192		
126206		
126225		
126244		
126266		
126279		
126288		
126297		
126314		
126329		
126337		
126351		
126427		
126430		
126434		
126443		
126449		
126464		
126492		

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Description	Sampling Notes
145655		
145669		
145685		
145694		
145708		
145723		
146798		
146824		
146831		
146843		
146861		
146868		
126352		
126358		
126374		
126384		
126391		
146172		
146182		
146203		
146214		
146221		
146238		
147034		
147038		
147051		
147070		
147087		
147097		
145508		
145527		
145543		
145562		
145576		
145601		
146297		
146314		
146335		
146352		
146368		
146390		
146508		
146526		
146544		
146565		
146589		
146613		
146627		
146637		
146649		

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Description	Sampling Notes
146657		
146676		
125188		
125198		
125207		
125228		
125244		
125257		
125278		
125596		
125610		
125626		
125641		
125669		
125690		
West Breccia Zone		
14018	Quartz-feldspar porphyry of plag + k-spar + qtz + hbl. Hornblende is typically altered to chlorite. Light sericitic alteration of feldspars. Trace pyrite is disseminated and very-fine-grained. Locally some trace fine-grained epidote. Greater sulphide content is observed around fractures and fine quartz- carbonate veins, locally accounting for close to 1% by volume. These veins are randomly oriented, short (typically <2cm), and narrow (<3mm). Phenocrysts are medium- to coarse-grained. Compositionally the rock contains too much K-spar to be considered a quartz monzonite, but is rather more granodioritic in composition, however much of the k-spar could be secondary. Pyrite seems to occur preferentially with secondary chlorite replacement of hornblende. -From 18.6 - 19.8 m: fairly wide vein (~1cm) hosting notable pyrite and possible chalcopyrite.	Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines
14021	Tourmaline Breccia. Unit is primarily porphyritic quartz-feldspar with primarily medium-grained plagioclase phenocrysts. "Wall-rock" is identical to the unit described above, and this unit is really the same lithology having undergone intense hydrothermal fracturing and veining. Where altered, the unit appears coarser-grained due to the "meshing" of finer groundmass grains by k-spar, which is then later overprinted by sericite and light chloritic alteration, particularly of secondary biotite from potassic phase. The name of this unit is derived from the presence of hydrothermal "vein" material which locally brecciates the rock. A more appropriate name would be "Hydrothermally brecciated porphyritic granodiorite", although the system is really more of a stockwork, as there is little evidence of clast movement. No heterolithic clasts, all in-situe, sharp, and angular to subangular clasts. The primary hydrothermal mineral is quartz with local feldspar and a pervasive dark blue-grey mineral, historically described as tourmaline. Locally, tourmaline is easily identifiable by it's acicular habit in the hydrothermal "vein" material, and may account for the rest of the blue-grey material. Ratio of wall-rock to vein materi	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14036	As above, same texture. 62.8 - 69.8 m: Degree of brecciation decreases. Similar texturally to interval at 53.9 - 58.5 m. Mostly highly potassically altered porphyritic wall rock overprinted by sericite, silica, and chlorite. Locally zones of intense, but spatially restricted tourmaline veining/brecciation/stockwork. Sulphide content decreases to 1-2%. Photo of typical texture (Photo 12) at 65.1 - 65.5 m showing association of very intense potassic alteration with tourmaline veining. Chalcopyrite is restricted almost exclusively to the hydrothermal veins.	Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines
14043	As TOBR unit above. Locally trace molybdenite paint on fracture surfaces and down to ~88.4 m, after which no molybdenite is observed. Very light epidote is observed starting at 76.8 m, and is observed to increase downhole. Locally chalcopyrite approaches 10%, but averages to roughly 2%. Due to the very locally varying intensity of, and nature of, the hydrothermal stockwork veining, this unit could possibly be better described as a stockwork - a term which could possibly be applied to the entire hole reflecting the variable degree of fracturing as a result of a violent fluid event. Photo 14 taken of box 39 showing typical stockwork texture (82.0 - 84.1 m).	Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines
14060	Felsic intrusive breccia. Matrix is felsic, fine-grained, and roughly equigranular with either clasts, or zones, of variable alteration of locally intense epidote and potassic (possibly hematite?) alteration. More mafic clasts have sharp boundaries and are angular to subangular, and tend to be more fine-grained. Upper one meter (down to 122.5m) is more massive, and less fractured (brecciated) than further downhole. Photo 24 was taken at 136.8 - 137.5 m as a texturally representative photo of the igneous breccia unit. (sample 05-JES-228 was also collected from this interval).	Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines
14067	Pyroxene-phyric andesite (pyroxene phenocrysts). "Contact" with TOBR is not such, but this lithology passes up into the TOBR unit up to 152.4 m. "Contact" is more a gradual decrease in the volume of hydrothermal vein material relative to the host rock, with a corresponding decrease in sulphides. Sulphide % ~1-2%, primarily chalcopyrite with trace pyrite. Chlorite and sericite alteration (possibly overprinting weak potassic). Locally epidote, usually associated with tourmaline/quartz "Stringers" or veins distal to the stockwork zone. Chloritic alteration is variable and centered around hairline veins. Photo 27 is typical of the textures within this unit (Sample 05-JES-230). Minor random oriented quartz veins without tourmaline are barren and possibly were filling fractures. These minor veins are typically <2mm wide.	Subsample collected from top of rejects stored in white plastic bucket; saturated, dark grey gravel and fines
14076	Fine grained andesite. Weak brecciation and veining: epidote-carb-quartz, accessory pyrite, in part vuggy. Strong fracturing, low angle CA. Core rubbly. 1-2% pyrite, disseminated, associated with fractures.	Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey-green gravel and fines
14083	Andesite. Fine grained,similar to 15.8 m. Strongly fractured, moderately veined (epidote-carb-quartz). Locally developed as breccia.	Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Description	Sampling Notes
14099	Ditto above 71.0 m. [Quartz-feldspar porphyry. Fine grained, colour light green grey. Partly brecciated by 5-10% cm portions of pneumatolytic breccia, low angle CA. greenish colour probably caused by sericite alteration.] Quartz-feldspar porphyry. Variously and erratically permeated by 5-30% cm-dm stringers of pneumatolytic breccia, both as 'dykes' with strong flow fabric and as stockwork. In places 0.3- 1.0 m portions of andesite. Orientation of breccia fabric 0-30CA. Sulphides generally trace to 1% each pyrite, chalcopyrite.	Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines
14103	Tourmaline Breccia. Clasts of felsic intrusives, generally pink colour. Matrix made up of tourmaline, epidote, chlorite with accessory sulphides. Strong variation in matrix abundance from 1 to 30%. Lithology of clasts variable, including andesite, porphyritic andesite, felsic porphyry. Sulphide minerals are chalcopyrite and pyrite, with trace molybdenite. Abundance of sulphides varies strongly, from trace to 10%. Sulphides are generally disseminated in matrix, to a minor degree disseminated in clasts.	Subsample collected from top of rejects stored in white plastic bucket; dry, grey and pink (granite?) gravel and fines
125046		
125068		
125073		
125079		
125084		
125127		
125129		
125134		
125142		
125149		
125154		
125165		
125176		
146112		
146115		
146124		
146127		
146135		
146149		
146161		
146164		
145951		
145956		
145974		
145982		
145992		
145999		
145834		
145842		
145852		
145857		
145871		
145608		
145614		
145628		
145640		
145646		
Paramount Zone		
125965		
125974		
125983		
125988		

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Sample Information**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Description	Sampling Notes
126007		
126031		
126040		
126054		
126067		
126081		
126110		
126118		
125904		
125919		
125928		
125933		
125944		
125952		
125963		
126120		
126131		
126142		
126154		
126171		
126181		
125806		
125816		
125833		
125861		
125875		
125897		
Tailings		
LIARD ZONE		
PARAMOUNT		
WEST BRECCIA		
High-Sulphide Histor		
T112 (171' - 172')		51.816 - 54.864 m (170 - 180 ft)
T113 (81' - 82')		24.384 - 27.432 m (80 - 90 ft)
T113 (983' - 985')		298.704 - 301.752 m (980 - 990 ft)
T140 (30' - 31')		9.144 - 12.192 m (30 - 40 ft)
T166 (389' - 390')		
T185 (116' - 117')		33.528 - 36.576 m (110 - 120 ft)
T207 (261.5' - 262')		79.248 - 82.296 m (260 - 270 ft)
T207 (269' - 271')		79.248 - 82.296 m (260 - 270 ft)

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
pH of DI water used for paste pH read 6.2

Sample Id.	Weight Received	Dry Weight	Rinse pH	Paste pH	S (Total)	S (Sulphide)	S (Sulphide)	Carbonate Leach S (Sulphate)	HCl Leachable S (Sulphate)	S ($BaSO_4$)	S (del_{actual})	S (del)	TAP	SAP	PAP
	(kg)	(kg)	Unity	Unity	(% Leco)	(% Leco)	(% Calc)	(%)	(%)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)
Method	WEI-21	WEI-22	OA-ELE08	OA-ELE07	S-IR08	S-IR07	S-CAL06	S-GRA06	S-GRA06a	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL				0.1	0.01	0.01	0.01	0.01	0.01						
Main Zone															
14130				8.3	0.29	0.29	0.285	0.03	0.005	0.013	-0.018	0.000	9.1	9.1	0.2
14144				8	0.26	0.2	0.255	0.02	0.005	0.008	0.047	0.047	8.1	7.7	0.2
14148				7.6	0.14	0.04	0.135	0.02	0.005	0.015	0.080	0.080	4.4	3.8	0.2
14156				7.7	0.17	0.14	0.165	0.04	0.005	0.006	0.019	0.019	5.3	5.0	0.2
14162				7.9	0.13	0.12	0.125	0.02	0.005	0.013	-0.008	0.000	4.1	3.8	0.2
14169				8.1	0.3	0.29	0.295	0.01	0.005	0.002	0.003	0.003	9.4	9.2	0.2
14232				8.3	0.15	0.14	0.145	0.005	0.005	0.004	0.001	0.001	4.7	4.4	0.2
14250				8.3	0.19	0.19	0.185	0.01	0.005	0.004	-0.009	0.000	5.9	5.9	0.2
14260				8.4	0.34	0.34	0.335	0.01	0.005	0.004	-0.009	0.000	10.6	10.6	0.2
14276				8.5	0.17	0.14	0.165	0.01	0.005	0.025	0.000	0.000	5.3	4.4	0.2
14295				8.6	0.44	0.41	0.435	0.005	0.005	0.002	0.023	0.023	13.8	13.5	6.1
14301				8.6	0.34	0.32	0.335	0.01	0.005	0.006	0.009	0.009	10.6	10.3	2.0
14323				8.6	0.15	0.13	0.145	0.005	0.005	0.006	0.009	0.009	4.7	4.3	0.2
14332				8.6	0.26	0.26	0.255	0.01	0.005	0.004	-0.009	0.000	8.1	8.1	0.2
14345				8.4	0.52	0.52	0.515	0.005	0.005	0.004	-0.009	0.000	16.3	16.3	0.2
14348				8.3	0.44	0.45	0.435	0.01	0.005	0.004	-0.019	0.000	13.8	14.1	0.2
14797				8.1	0.08	0.05	0.075	0.005	0.005	0.004	0.021	0.021	2.5	2.2	0.2
14808				7.8	0.18	0.16	0.175	0.005	0.005	0.004	0.011	0.011	5.6	5.3	0.2
14816				7.6	0.46	0.46	0.45	0.005	0.01	0.004	-0.014	0.000	14.4	14.4	1.6
14828				7.6	0.13	0.1	0.125	0.02	0.005	0.017	0.008	0.008	4.1	3.4	0.2
14844				7.7	0.21	0.2	0.2	0.005	0.01	0.008	-0.008	0.000	6.6	6.3	0.2
14680				7.7	0.22	0.2	0.215	0.01	0.005	0.006	0.009	0.009	6.9	6.5	0.2
14871				7.6	0.37	0.32	0.365	0.02	0.005	0.002	0.043	0.043	11.6	11.3	0.2
14887				7.8	0.44	0.42	0.41	0.01	0.03	0.008	-0.018	0.000	13.8	13.1	6.7
14689				8.2	0.68	0.69	0.675	0.01	0.005	0.002	-0.017	0.000	21.3	21.6	15.0
14695				8.2	0.14	0.13	0.135	0.005	0.005	0.004	0.001	0.001	4.4	4.1	0.2
14742				8.2	0.19	0.19	0.185	0.005	0.005	0.004	-0.009	0.000	5.9	5.9	0.2
14666				8.1	0.32	0.31	0.315	0.01	0.005	0.008	-0.003	0.000	10.0	9.7	5.0
14685				8.1	1.79	1.8	1.785	0.01	0.005	0.010	-0.025	0.000	55.9	56.3	42.2
14685B				7.9	1.95	1.8	1.945	0.01	0.005	0.008	0.137	0.137	60.9	60.5	45.8
14545				7.8	0.19	0.13	0.185	0.01	0.005	0.021	0.034	0.034	5.9	5.1	1.2
14565				7.8	0.23	0.24	0.225	0.005	0.005	0.004	-0.019	0.000	7.2	7.5	0.2
14571				7.8	1.04	1.03	1.035	0.02	0.005	0.010	-0.005	0.000	32.5	32.2	14.7
14578				7.9	1.82	1.82	1.815	0.02	0.005	0.015	-0.020	0.000	56.9	56.9	47.4
14578B				7.9	1.93	1.91	1.925	0.03	0.005	0.019	-0.004	0.000	60.3	59.7	49.2
14598				8.1	0.13	0.13	0.125	0.01	0.005	0.004	-0.009	0.000	4.1	4.1	1.6
14893				8	0.11	0.08	0.07	0.005	0.04	0.010	-0.020	0.000	3.4	2.5	0.2
14899				8.1	0.02	0.02	0.015	0.005	0.005	0.008	-0.013	0.000	0.6	0.6	0.2
14908				8.1	0.08	0.07	0.075	0.005	0.005	0.017	-0.012	0.000	2.5	2.2	0.2
14917				8.2	0.19	0.16	0.185	0.005	0.005	0.019	0.006	0.006	5.9	5.2	0.2
14925				7.9	0.14	0.12	0.135	0.005	0.005	0.008	0.007	0.007	4.4	4.0	0.2
14998				7.8	0.13	0.12	0.125	0.005	0.005	0.006	-0.001	0.000	4.1	3.8	0.2
15862				7.9	0.08	0.03	0.075	0.005	0.005	0.006	0.039	0.039	2.5	2.1	0.2
15870				8	0.13	0.09	0.125	0.02	0.005	0.025	0.010	0.010	4.1	3.1	0.2
15879				8	0.12	0.09	0.115	0.02	0.005	0.019	0.006	0.006	3.8	3.0	0.2

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
pH of DI water used for paste pH read 6.2

Sample Id.	Weight Received (kg)	Dry Weight (kg)	Rinse pH Unity	Paste pH Unity	S (Total) (% Leco)	S (Sulphide) (% Leco)	S (Sulphide) (% Calc)	Carbonate Leach S (Sulphate) (%)	HCl Leachable S (Sulphate) (%)	S (BaSO$_4$) (%)	S (del$_{actual}$) (%)	S (del) (%)	TAP (kg CaCO$_3$/t)	SAP (kg CaCO$_3$/t)	PAP (kg CaCO$_3$/t)
Method	WEI-21	WEI-22	OA-ELE08	OA-ELE07	S-IR08	S-IR07	S-CAL06	S-GRA06	S-GRA06a	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL				0.1	0.01	0.01	0.01	0.01	0.01						
15887				8	0.31	0.29	0.305	0.01	0.005	0.010	0.005	0.005	9.7	9.2	0.2
15891				7.8	0.14	0.09	0.135	0.02	0.005	0.031	0.014	0.014	4.4	3.2	0.2
15908				7.8	0.22	0.2	0.215	0.02	0.005	0.006	0.009	0.009	6.9	6.5	0.2
15911				7.9	0.09	0.07	0.085	0.01	0.005	0.010	0.005	0.005	2.8	2.3	0.2
125285				8.6	0.32	0.3	0.31	0.03	0.01	0.010	0.000	0.000	10.0	9.4	0.2
125288				8.5	0.1	0.08	0.095	0.01	0.005	0.008	0.007	0.007	3.1	2.7	2.0
125293				9	0.21	0.2	0.2	0.02	0.01	0.004	-0.004	0.000	6.6	6.3	0.2
125305				8.9	0.12	0.12	0.115	0.01	0.005	0.008	-0.013	0.000	3.8	3.8	0.2
125311				9.2	0.06	0.05	0.055	0.02	0.005	0.013	-0.008	0.000	1.9	1.6	0.2
125703				8.3	0.1	0.09	0.095	0.01	0.005	0.004	0.001	0.001	3.1	2.8	0.2
125728				8.2	0.19	0.18	0.17	0.03	0.02	0.013	-0.023	0.000	5.9	5.6	0.2
125755				8	0.59	0.55	0.56	0.05	0.03	0.010	0.000	0.000	18.4	17.2	6.1
125772				8.5	0.21	0.19	0.205	0.03	0.005	0.008	0.007	0.007	6.6	6.1	0.2
125795				8.3	0.11	0.08	0.08	0.04	0.03	0.015	-0.015	0.000	3.4	2.5	0.2
125422				8.4	0.21	0.21	0.2	0.02	0.01	0.004	-0.014	0.000	6.6	6.6	0.2
125435				8.5	0.16	0.13	0.15	0.02	0.01	0.004	0.016	0.016	5.0	4.6	0.2
125452				7.8	0.47	0.47	0.46	0.02	0.01	0.004	-0.014	0.000	14.7	14.7	0.2
125476				7.7	0.78	0.73	0.73	0.08	0.05	0.033	-0.033	0.000	24.4	22.8	11.4
125490				7.6	0.35	0.33	0.28	0.05	0.07	0.002	-0.052	0.000	10.9	10.3	3.6
126192				8.5	0.19	0.17	0.185	0.01	0.005	0.004	0.011	0.011	5.9	5.7	0.2
126206				8.4	0.22	0.2	0.215	0.02	0.005	0.010	0.005	0.005	6.9	6.4	0.3
126225				8.2	0.35	0.27	0.345	0.03	0.005	0.015	0.060	0.060	10.9	10.3	1.0
126244				8.4	0.26	0.21	0.255	0.02	0.005	0.004	0.041	0.041	8.1	7.8	0.2
126266				8.4	0.19	0.17	0.185	0.02	0.005	0.004	0.011	0.011	5.9	5.7	0.2
126279				8.3	0.39	0.34	0.385	0.03	0.005	0.004	0.041	0.041	12.2	11.9	4.3
126288				8.1	0.37	0.32	0.36	0.01	0.01	0.004	0.036	0.036	11.6	11.1	0.2
126297				8.4	0.51	0.47	0.505	0.01	0.005	0.004	0.031	0.031	15.9	15.7	7.5
126314				7.6	1.37	1.29	1.365	0.04	0.005	0.004	0.071	0.071	42.8	42.5	20.0
126329				8	0.24	0.2	0.22	0.02	0.02	0.015	0.005	0.005	7.5	6.4	0.2
126337				8	0.57	0.52	0.565	0.03	0.005	0.008	0.037	0.037	17.8	17.4	0.6
126351				8.4	0.14	0.12	0.135	0.01	0.005	0.008	0.007	0.007	4.4	4.0	0.2
126427				8.2	1.12	0.94	1.115	0.03	0.005	0.004	0.171	0.171	35.0	34.7	33.1
126430				8.5	0.21	0.2	0.205	0.02	0.005	0.004	0.001	0.001	6.6	6.3	5.7
126434				8.6	0.11	0.09	0.105	0.02	0.005	0.004	0.011	0.011	3.4	3.2	2.7
126443				8.3	1.7	1.44	1.695	0.04	0.005	0.002	0.253	0.253	53.1	52.9	51.2
126449				8.4	0.02	0.03	0.015	0.01	0.005	0.010	-0.025	0.000	0.6	0.9	0.6
126464				8.2	0.43	0.38	0.425	0.03	0.005	0.006	0.039	0.039	13.4	13.1	6.6
126492				8.1	0.22	0.19	0.21	0.03	0.01	0.006	0.014	0.014	6.9	6.4	0.2
145655				8.4	0.66	0.55	0.63	0.04	0.03	0.017	0.063	0.063	20.6	19.2	14.7
145669				8.3	0.95	0.9	0.91	0.04	0.04	0.004	0.006	0.006	29.7	28.3	21.2
145685				8.4	0.23	0.2	0.21	0.03	0.02	0.004	0.006	0.006	7.2	6.4	0.2
145694				8.4	0.17	0.15	0.15	0.03	0.02	0.004	-0.004	0.000	5.3	4.7	0.2
145708				8.4	0.26	0.22	0.25	0.03	0.01	0.002	0.028	0.028	8.1	7.7	1.5
145723				8	1.63	1.53	1.59	0.07	0.04	0.004	0.056	0.056	50.9	49.6	33.3
146798				8.6	0.21	0.19	0.205	0.02	0.005	0.008	0.007	0.007	6.6	6.1	0.2
146824				8.7	0.17	0.15	0.16	0.03	0.01	0.006	0.004	0.004	5.3	4.8	0.2

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
pH of DI water used for paste pH read 6.2

Sample Id.	Weight Received	Dry Weight	Rinse pH	Paste pH	S (Total)	S (Sulphide)	S (Sulphide)	Carbonate Leach S (Sulphate)	HCl Leachable S (Sulphate)	S ($BaSO_4$)	S (del_{actual})	S (del)	TAP	SAP	PAP
	(kg)	(kg)	Unity	Unity	(% Leco)	(% Leco)	(% Calc)	(%)	(%)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)
Method	WEI-21	WEI-22	OA-ELE08	OA-ELE07	S-IR08	S-IR07	S-CAL06	S-GRA06	S-GRA06a	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL				0.1	0.01	0.01	0.01	0.01	0.01						
146831				8.2	0.36	0.35	0.34	0.04	0.02	0.004	-0.014	0.000	11.3	10.9	0.2
146843															
146861				8.8	0.13	0.1	0.12	0.02	0.01	0.010	0.010	0.010	4.1	3.4	0.2
146868				8	0.51	0.42	0.47	0.06	0.04	0.006	0.044	0.044	15.9	14.5	4.7
126352				7.9	0.6	0.55	0.59	0.04	0.01	0.008	0.032	0.032	18.8	18.2	2.1
126358				8.1	0.33	0.28	0.325	0.02	*0.005*	0.006	0.039	0.039	10.3	10.0	0.2
126374				8.4	0.17	0.16	0.16	0.03	0.01	0.006	-0.006	0.000	5.3	5.0	0.2
126384				8.6	0.11	0.1	0.1	0.01	0.01	0.006	-0.006	0.000	3.4	3.1	0.2
126391				8.4	0.18	0.15	0.175	0.02	*0.005*	0.008	0.017	0.017	5.6	5.2	0.2
146172				8.5	0.24	0.22	0.21	0.02	0.03	0.006	-0.016	0.000	7.5	6.9	0.2
146182				8.9	0.15	0.13	0.13	0.01	0.02	0.004	-0.004	0.000	4.7	4.1	0.2
146203				8.6	0.18	0.16	0.16	*0.005*	0.02	0.004	-0.004	0.000	5.6	5.0	0.2
146214				8	0.36	0.22	0.2	0.13	0.16	0.006	-0.026	0.000	11.3	6.9	0.2
146221				7.5	0.81	0.7	0.76	0.05	0.05	0.006	0.054	0.054	25.3	23.6	4.3
146238				7.8	0.13	0.1	0.08	0.04	0.05	0.006	-0.026	0.000	4.1	3.1	0.2
147034				8.2	0.52	0.51	0.5	0.04	0.02	0.004	-0.014	0.000	16.3	15.9	0.2
147038				8.3	0.35	0.29	0.32	0.05	0.03	0.027	0.003	0.003	10.9	9.2	0.2
147051				8.3	0.33	0.26	0.32	0.05	0.01	0.021	0.039	0.039	10.3	9.3	1.8
147070				8.7	0.51	0.45	0.5	0.03	0.01	0.004	0.046	0.046	15.9	15.5	14.5
147087				8.1	3.35	2.78	3.26	0.13	0.09	0.004	0.476	0.476	104.7	101.7	101.0
147097				8.2	0.68	0.59	0.66	0.05	0.02	0.025	0.045	0.045	21.3	19.8	17.5
145508				8.7	0.04	0.03	0.035	0.01	*0.005*	0.008	-0.003	0.000	1.3	0.9	0.2
145527				8.6	0.48	0.4	0.47	0.03	0.01	0.010	0.060	0.060	15.0	14.4	7.7
145543				8.9	0.12	0.11	0.115	0.02	*0.005*	0.008	-0.003	0.000	3.8	3.4	0.2
145562				9	0.09	0.08	0.085	0.04	*0.005*	0.008	-0.003	0.000	2.8	2.5	0.2
145576				8.1	0.69	0.63	0.68	0.04	0.01	0.019	0.031	0.031	21.6	20.7	11.1
145601				7.9	0.5	0.4	0.49	0.06	0.01	0.013	0.077	0.077	15.6	14.9	6.5
146297				8.1	0.35	0.3	0.33	0.01	0.02	0.006	0.024	0.024	10.9	10.1	0.2
146314				8.4	0.15	0.14	0.13	0.02	0.02	0.006	-0.016	0.000	4.7	4.4	0.2
146335				7.8	0.13	0.09	0.07	0.03	0.06	0.006	-0.026	0.000	4.1	2.8	0.2
146352				8.6	0.06	0.04	0.05	0.01	0.01	0.006	0.004	0.004	1.9	1.4	0.2
146368				7.9	0.19	0.08	0.09	0.1	0.1	0.004	0.006	0.006	5.9	2.7	0.2
146390				8.2	0.16	0.13	0.155	0.02	*0.005*	0.004	0.021	0.021	5.0	4.7	0.2
146508				8.7	0.06	0.06	0.055	0.01	*0.005*	0.006	-0.011	0.000	1.9	1.9	0.2
146526				8	0.68	0.06	0.06	0.63	0.62	0.013	-0.013	0.000	21.3	1.9	0.2
146544				8	0.24	0.08	0.11	0.13	0.13	0.010	0.020	0.020	7.5	3.1	0.2
146565				8.7	0.11	0.08	0.09	0.04	0.02	0.031	-0.021	0.000	3.4	2.5	0.2
146589				9	0.13	0.1	0.12	0.01	0.01	0.008	0.012	0.012	4.1	3.5	0.2
146613				8.3	0.54	0.42	0.53	0.03	0.01	0.004	0.106	0.106	16.9	16.4	6.1
146627				8.7	0.09	0.07	0.08	0.01	0.01	0.008	0.002	0.002	2.8	2.2	0.2
146637				8.2	0.46	0.43	0.45	0.04	0.01	0.025	-0.005	0.000	14.4	13.4	2.0
146649				9	0.28	0.23	0.26	0.04	0.02	0.023	0.007	0.007	8.8	7.4	4.1
146657				8.8	0.19	0.19	0.185	0.02	*0.005*	0.010	-0.015	0.000	5.9	5.9	0.2
146676				8.7	0.21	0.18	0.19	0.02	0.02	0.004	0.006	0.006	6.6	5.8	0.2
125188				8.8	0.26	0.22	0.24	0.03	0.02	0.017	0.003	0.003	8.1	7.0	0.2
125198				8.5	0.22	0.2	0.21	0.03	0.01	0.006	0.004	0.004	6.9	6.4	0.2

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
pH of DI water used for paste pH read 6.2

Sample Id.	Weight Received (kg)	Dry Weight (kg)	Rinse pH Unity	Paste pH Unity	S (Total) (% Leco)	S (Sulphide) (% Leco)	S (Sulphide) (% Calc)	Carbonate Leach S (Sulphate) (%)	HCl Leachable S (Sulphate) (%)	S ($BaSO_4$) (%) Calculated	S (del_{actual}) (%) Calculated	S (del) (%) Calculated	TAP (kg $CaCO_3$/t) Calculated	SAP (kg $CaCO_3$/t) Calculated	PAP (kg $CaCO_3$/t) Calculated
Method	WEI-21	WEI-22	OA-ELE08	OA-ELE07	S-IR08	S-IR07	S-CAL06	S-GRA06	S-GRA06a						
MDL				0.1	0.01	0.01	0.01	0.01	0.01						
125207				8.7	0.11	0.1	0.09	0.02	0.02	0.008	-0.018	0.000	3.4	3.1	0.2
125228				9.1	0.15	0.14	0.145	0.02	*0.005*	0.010	-0.005	0.000	4.7	4.4	0.2
125244				8.9	0.15	0.13	0.14	0.02	0.01	0.004	0.006	0.006	4.7	4.2	0.2
125257				8.8	0.06	0.06	0.055	0.01	*0.005*	0.006	-0.011	0.000	1.9	1.9	1.3
125278				8.6	0.02	0.01	0	0.01	0.02	0.008	-0.018	0.000	0.6	0.3	0.2
125596				8.1	0.12	0.13	0.115	0.02	*0.005*	0.006	-0.021	0.000	3.8	4.1	0.2
125610				8.4	0.06	0.05	0.055	0.01	*0.005*	0.002	0.003	0.003	1.9	1.7	0.2
125626															
125641				8.6	0.1	0.09	0.08	0.02	0.02	0.004	-0.014	0.000	3.1	2.8	0.2
125669				8	1.01	0.93	0.99	0.04	0.02	0.004	0.056	0.056	31.6	30.8	19.6
125690				8.1	0.1	0.06	0.08	0.03	0.02	0.006	0.014	0.014	3.1	2.3	0.2
West Breccia Zone															
14018				7.6	0.8	0.69	0.795	0.02	*0.005*	0.027	0.078	0.078	25.0	24.0	19.7
14021				7.9	0.62	0.6	0.615	0.03	*0.005*	0.010	0.005	0.005	19.4	18.9	12.5
14036				7.9	1.47	1.39	1.465	0.02	*0.005*	0.013	0.062	0.062	45.9	45.4	37.8
14043				8.2	0.26	0.22	0.255	0.02	*0.005*	0.006	0.029	0.029	8.1	7.8	2.8
14060				8	1.31	0.62	0.6	0.74	0.71	0.008	-0.028	0.000	40.9	19.4	10.6
14067				8.4	0.4	0.41	0.395	0.01	*0.005*	0.008	-0.023	0.000	12.5	12.8	4.7
14076				8.2	0.77	0.76	0.765	0.01	*0.005*	0.010	-0.005	0.000	24.1	23.8	19.1
14083				8.2	1.46	1.35	1.455	0.03	*0.005*	0.017	0.088	0.088	45.6	44.9	40.4
14099				8.1	0.34	0.28	0.335	0.03	*0.005*	0.021	0.034	0.034	10.6	9.8	5.6
14103				8	0.69	0.25	0.27	0.45	0.42	0.006	0.014	0.014	21.6	8.2	0.2
125046				8.5	0.11	0.1	0.09	0.02	0.02	0.004	-0.014	0.000	3.4	3.1	0.2
125068				8.2	0.39	0.36	0.36	0.04	0.03	0.010	-0.010	0.000	12.2	11.3	0.2
125073				8	0.6	0.48	0.54	0.05	0.06	0.015	0.045	0.045	18.8	16.4	0.2
125079				8	1.29	1.12	1.24	0.08	0.05	0.036	0.084	0.084	40.3	37.6	0.2
125084				8.1	0.61	0.49	0.55	0.09	0.06	0.021	0.039	0.039	19.1	16.5	0.2
125127				8.9	0.08	0.06	0.07	0.01	0.01	0.013	-0.003	0.000	2.5	1.9	0.2
125129				8.4	0.25	0.2	0.21	0.02	0.04	0.006	0.004	0.004	7.8	6.4	0.2
125134				8.1	0.59	0.47	0.54	0.04	0.05	0.013	0.057	0.057	18.4	16.5	0.2
125142				8.4	0.26	0.2	0.24	0.03	0.02	0.008	0.032	0.032	8.1	7.2	0.2
125149				8.7	0.13	0.11	0.12	0.02	0.01	0.013	-0.003	0.000	4.1	3.4	0.2
125154				9.1	0.08	0.06	0.07	0.02	0.01	0.004	0.006	0.006	2.5	2.1	0.2
125165				8.7	0.19	0.17	0.17	0.02	0.02	0.004	-0.004	0.000	5.9	5.3	0.2
125176				8.1	0.24	0.16	0.18	0.06	0.06	0.006	0.014	0.014	7.5	5.4	0.2
146112				8.8	0.12	0.09	0.09	0.01	0.03	0.006	-0.006	0.000	3.8	2.8	0.2
146115				8.5	0.13	0.09	0.11	0.01	0.02	0.015	0.005	0.005	4.1	3.0	2.7
146124				8.5	0.09	0.06	0.05	0.01	0.04	0.015	-0.025	0.000	2.8	1.9	0.2
146127				8.3	1.06	0.82	1.03	0.05	0.03	0.013	0.197	0.197	33.1	31.8	30.8
146135				8.1	0.04	0.03	0	0.03	0.04	0.013	-0.043	0.000	1.3	0.9	0.2
146149				8.2	0.07	0.04	0.04	0.03	0.03	0.013	-0.013	0.000	2.2	1.3	0.3
146161				8.5	0.04	0.02	0.02	0.01	0.02	0.017	-0.017	0.000	1.3	0.6	0.2
146164				8.4	0.02	0.01	-0.01	0.01	0.03	0.013	-0.033	0.000	0.6	0.3	0.2
145951				8.4	0.18	0.14	0.16	0.03	0.02	0.006	0.014	0.014	5.6	4.8	0.2
145956				8.4	0.19	0.16	0.16	0.03	0.03	0.004	-0.004	0.000	5.9	5.0	0.2
145974				8.7	0.02	0.02	0	0.02	0.02	0.006	-0.026	0.000	0.6	0.6	0.2

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
pH of DI water used for paste pH read 6.2

Sample Id.	Weight Received (kg)	Dry Weight (kg)	Rinse pH Unity	Paste pH Unity	S (Total) (% Leco)	S (Sulphide) (% Leco)	S (Sulphide) (% Calc)	Carbonate Leach S (Sulphate) (%)	HCl Leachable S (Sulphate) (%)	S ($BaSO_4$) (%)	S (del_{actual}) (%)	S (del) (%)	TAP (kg $CaCO_3$/t)	SAP (kg $CaCO_3$/t)	PAP (kg $CaCO_3$/t)
Method	WEI-21	WEI-22	OA-ELE08	OA-ELE07	S-IR08	S-IR07	S-CAL06	S-GRA06	S-GRA06a	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL				0.1	0.01	0.01	0.01	0.01	0.01						
145982				8.6	0.05	0.03	0.03	0.01	0.02	0.006	-0.006	0.000	1.6	0.9	0.7
145992				8.5	0.28	0.22	0.25	0.03	0.03	0.006	0.024	0.024	8.8	7.6	1.5
145999				8.1	0.14	0.08	0.05	0.07	0.09	0.004	-0.034	0.000	4.4	2.5	0.2
145834				9	0.04	0.04	0.02	0.02	0.02	0.004	-0.024	0.000	1.3	1.3	0.2
145842				8.8	0.03	0.02	0.01	0.02	0.02	0.002	-0.012	0.000	0.9	0.6	0.2
145852				8.8	0.11	0.09	0.09	0.02	0.02	0.001	-0.001	0.000	3.4	2.8	0.2
145857				9.1	0.01	0.01	-0.01	0.02	0.02	0.006	-0.026	0.000	0.3	0.3	0.2
145871				8.1	0.16	0.05	0.03	0.13	0.13	0.006	-0.026	0.000	5.0	1.6	0.3
145608				8.4	0.79	0.66	0.785	0.03	*0.005*	0.008	0.117	0.117	24.7	24.3	22.0
145614				8.3	0.56	0.5	0.555	0.03	*0.005*	0.013	0.042	0.042	17.5	17.0	11.3
145628				8	0.79	0.42	0.45	0.37	0.34	0.002	0.028	0.028	24.7	14.0	10.7
145640				8	0.75	0.61	0.68	0.09	0.07	0.010	0.060	0.060	23.4	20.9	14.9
145646				8	0.57	0.44	0.47	0.13	0.1	0.008	0.022	0.022	17.8	14.4	9.4
Paramount Zone															
125965				8.2	0.35	0.33	0.34	0.04	0.01	0.006	0.004	0.004	10.9	10.4	0.2
125974				8.4	1.56	1.6	1.55	0.05	0.01	0.008	-0.058	0.000	48.8	50.0	47.7
125983				8.3	0.3	0.26	0.29	0.03	0.01	0.013	0.017	0.017	9.4	8.7	2.8
125988				8.4	0.03	0.03	0.02	0.01	0.01	0.017	-0.027	0.000	0.9	0.9	0.6
126007				8.5	0.15	0.13	0.14	0.04	0.01	0.010	0.000	0.000	4.7	4.1	0.2
126031				8.8	0.13	0.12	0.12	0.02	0.01	0.021	-0.021	0.000	4.1	3.8	0.2
126040				8.1	0.66	0.63	0.65	0.03	0.01	0.006	0.014	0.014	20.6	20.1	10.6
126054				8.1	0.18	0.16	0.16	0.02	0.02	0.008	-0.008	0.000	5.6	5.0	0.2
126067				8.2	0.31	0.29	0.3	0.07	0.01	0.004	0.006	0.006	9.7	9.2	1.1
126081				7.7	1.09	0.89	0.97	0.13	0.12	0.031	0.049	0.049	34.1	29.3	9.6
126110				8.6	0.06	0.05	0.055	0.01	*0.005*	0.021	-0.016	0.000	1.9	1.6	1.0
126118				8	0.78	0.59	0.64	0.19	0.14	0.008	0.042	0.042	24.4	19.7	1.1
125904				8.5	0.18	0.17	0.175	0.02	*0.005*	0.006	-0.001	0.000	5.6	5.3	0.2
125919				8.1	0.51	0.48	0.49	0.04	0.02	0.006	0.004	0.004	15.9	15.1	0.2
125928				8.7	0.09	0.08	0.07	0.02	0.02	0.017	-0.027	0.000	2.8	2.5	0.2
125933				8.5	0.02	0.01	0.01	0.02	0.01	0.013	-0.013	0.000	0.6	0.3	0.2
125944				8.9	0.12	0.12	0.08	0.02	0.04	0.015	-0.055	0.000	3.8	3.8	2.6
125952				8.5	1.05	1.04	1.045	0.05	*0.005*	0.008	-0.003	0.000	32.8	32.5	31.7
125963				8	0.43	0.38	0.39	0.06	0.04	0.010	0.000	0.000	13.4	11.9	0.2
126120				9	0.06	0.05	0.055	0.01	*0.005*	0.013	-0.008	0.000	1.9	1.6	0.2
126131				9.1	0.03	0.02	0.025	0.01	*0.005*	0.010	-0.005	0.000	0.9	0.6	0.2
126142				9	0.05	0.04	0.04	0.02	0.01	0.006	-0.006	0.000	1.6	1.3	0.2
126154				8.9	0.13	0.11	0.11	0.01	0.02	0.002	-0.002	0.000	4.1	3.4	0.2
126171				8.1	1.28	1.24	1.21	0.1	0.07	0.023	-0.053	0.000	40.0	38.8	32.6
126181				8.1	0.25	0.19	0.21	0.06	0.04	0.008	0.012	0.012	7.8	6.3	5.3
125806				8.6	0.48	0.46	0.46	0.03	0.02	0.025	-0.025	0.000	15.0	14.4	12.4
125816				8.5	0.03	0.03	0.02	0.01	0.01	0.029	-0.039	0.000	0.9	0.9	0.5
125833				8.4	0.27	0.27	0.265	0.03	*0.005*	0.017	-0.022	0.000	8.4	8.4	0.2
125861				8.1	0.34	0.22	0.27	0.05	0.07	0.017	0.033	0.033	10.6	7.9	0.2
125875				8.4	0.24	0.2	0.22	0.03	0.02	0.021	-0.001	0.000	7.5	6.3	0.2
125897				8.2	0.08	0.06	0.07	0.03	0.01	0.006	0.004	0.004	2.5	2.0	0.2

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
pH of DI water used for paste pH read 6.2

Sample Id.	Weight Received	Dry Weight	Rinse pH	Paste pH	S (Total)	S (Sulphide)	S (Sulphide)	Carbonate Leach S (Sulphate)	HCl Leachable S (Sulphate)	S ($BaSO_4$)	S (del_{actual})	S (del)	TAP	SAP	PAP
	(kg)	(kg)	Unity	Unity	(% Leco)	(% Leco)	(% Calc)	(%)	(%)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)
Method	WEI-21	WEI-22	OA-ELE08	OA-ELE07	S-IR08	S-IR07	S-CAL06	S-GRA06	S-GRA06a	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL				0.1	0.01	0.01	0.01	0.01	0.01						
Tailings															
LIARD ZONE	5.98	4.12	8.3	8.4	0.08	0.07	0.075	0.01	*0.005*	0.008	-0.003	0.000	2.5	2.2	0.2
PARAMOUNT	5.48	2.98	7.8	8.1	0.17	0.12	0.13	0.05	0.04	0.013	-0.003	0.000	5.3	3.8	0.2
WEST BRECCIA	5.8	3.84	7.9	8.2	0.2	0.17	0.18	0.04	0.02	0.013	-0.003	0.000	6.3	5.3	0.2
High-Sulphide Histor															
T112 (171' - 172')				8.7	9.06	8.45	9.03	0.04	0.03	0.004	0.576	0.576	283.1	282.1	281.1
T113 (81' - 82')				9.2	0.87	0.83	0.85	0.04	0.02	0.031	-0.011	0.000	27.2	25.9	24.7
T113 (983' - 985')				8.9	2.11	2.09	2.09	0.05	0.02	0.004	-0.004	0.000	65.9	65.3	51.6
T140 (30' - 31')				8.6	0.13	0.12	0.125	0.02	*0.005*	0.008	-0.003	0.000	4.1	3.8	0.2
T166 (389' - 390')				9.1	0.81	0.73	0.8	0.03	0.01	0.013	0.057	0.057	25.3	24.6	22.2
T185 (116' - 117')				8.6	2.26	2.25	2.25	0.03	0.01	0.017	-0.017	0.000	70.6	70.3	69.9
T207 (261.5' - 262')				8.4	3.88	3.85	3.87	0.04	0.01	0.008	0.012	0.012	121.3	120.7	118.5
T207 (269' - 271')				7.4	13.5	12.1	13.46	0.07	0.04	0.008	1.352	1.352	421.9	420.4	418.4

Project:	**Schaft Creek**
Client:	Copper Fox Metals Inc.
Data:	**ABA Data**
Comments:	2005 core samples were collected by MDAG on Feb 7'07. 2006 core samples were collected by Copper Fox personnel in Sep '07. pH of DI water used for paste pH read 6.2

Sample Id.	Weight Received	Dry Weight	Rinse pH	Paste pH	S (Total)	S (Sulphide)	S (Sulphide)	Carbonate Leach S (Sulphate)	HCl Leachable S (Sulphate)	S ($BaSO_4$)	S (del_{actual})	S (del)	TAP	SAP	PAP
	(kg)	(kg)	Unity	Unity	(% Leco)	(% Leco)	(% Calc)	(%)	(%)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)
Method	WEI-21	WEI-22	OA-ELE08	OA-ELE07	S-IR08	S-IR07	S-CAL06	S-GRA06	S-GRA06a	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL				0.1	0.01	0.01	0.01	0.01	0.01						
All Data															
Maximum			8.3	9.2	13.5	12.1	13.5	0.74	0.71	0.036	1.35	1.35	422	420	418
Minimum			7.8	7.4	0.01	0.01	-0.01	0.005	0.005	0.001	-0.058	0	0.31	0.31	0.16
Mean			8	8.31	0.5	0.44	0.47	0.038	0.028	0.0098	0.019	0.026	15.6	14.6	8.92
Standard Deviation			0.26	0.37	1.14	1.05	1.14	0.075	0.072	0.0068	0.11	0.1	35.7	35.6	35.6
10 Percentile			7.82	7.8	0.064	0.05	0.055	0.01	0.005	0.0042	-0.023	0	2	1.74	0.16
25 Percentile			7.85	8	0.13	0.1	0.11	0.01	0.005	0.0042	-0.012	0	4.06	3.14	0.16
Median			7.9	8.3	0.22	0.2	0.2	0.02	0.01	0.0084	0.0016	0.0016	6.88	6.25	0.16
75 Percentile			8.1	8.6	0.5	0.42	0.46	0.04	0.02	0.013	0.02	0.02	15.8	14.4	4.19
90 Percentile			8.22	8.8	1.03	0.87	0.95	0.06	0.05	0.019	0.055	0.055	32.1	28.9	19.9
Interquartile Range (IC			0.25	0.6	0.38	0.32	0.35	0.03	0.015	0.0084	0.032	0.02	11.7	11.2	4.04
Variance			0.07	0.14	1.31	1.1	1.3	0.0056	0.0052	0.000046	0.011	0.011	1277	1267	1264
Skewness			1.46	0.17	8.39	8.17	8.45	6.9	7.06	1.55	9.56	10	8.39	8.46	8.79
Coefficient of Variatior			0.033	0.045	2.29	2.37	2.42	1.96	2.59	0.69	5.55	3.98	2.29	2.43	3.98
Count			3	235	235	235	235	235	235	235	235	235	235	235	235
NPR < 1.0 or NPR = 1															
1.0 < NPR < 2.0															
NPR > 2.0 or NPR =2.															
% NPR < 1.0 or NPR =															
% 1.0 < NPR < 2.0 of															
% NPR > 2.0 or NPR =															
Main Zone															
Maximum			NA	9.2	3.35	2.78	3.26	0.63	0.62	0.033	0.48	0.48	105	102	101
Minimum			NA	7.5	0.02	0.01	0	0.005	0.005	0.0021	-0.052	0	0.62	0.31	0.16
Mean			NA	8.26	0.37	0.33	0.35	0.029	0.019	0.0088	0.014	0.02	11.5	10.8	4.7
Standard Deviation			NA	0.37	0.45	0.42	0.45	0.055	0.055	0.0064	0.053	0.05	14.2	14.1	12.8
10 Percentile			NA	7.8	0.095	0.07	0.078	0.005	0.005	0.0042	-0.018	0	2.97	2.32	0.16
25 Percentile			NA	8	0.13	0.1	0.12	0.01	0.005	0.0042	-0.0092	0	4.06	3.55	0.16
Median			NA	8.2	0.21	0.19	0.2	0.02	0.005	0.0063	0.0037	0.0037	6.56	6.2	0.16
75 Percentile			NA	8.5	0.42	0.35	0.38	0.03	0.02	0.01	0.019	0.019	13.1	11.8	1.97
90 Percentile			NA	8.7	0.68	0.66	0.68	0.045	0.03	0.018	0.046	0.046	21.4	21.1	14.6
Interquartile Range (IC			NA	0.5	0.29	0.24	0.26	0.02	0.015	0.0063	0.029	0.019	9.06	8.21	1.81
Variance			NA	0.14	0.21	0.17	0.2	0.003	0.003	0.000041	0.0028	0.0025	201	198	163
Skewness			NA	0.2	3.45	3.17	3.42	9.4	9.54	1.81	5.57	6.33	3.45	3.43	4.51
Coefficient of Variatior			NA	0.045	1.23	1.28	1.29	1.9	2.86	0.73	3.79	2.56	1.23	1.3	2.71
Count			0	146	146	146	146	146	146	146	146	146	146	146	146
NPR < 1.0 or NPR = 1															
1.0 < NPR < 2.0															
NPR > 2.0 or NPR =2.															
% NPR < 1.0 or NPR =															
% 1.0 < NPR < 2.0 of															
% NPR > 2.0 or NPR =															

Project:	**Schaft Creek**
Client:	Copper Fox Metals Inc.
Data:	**ABA Data**
Comments:	2005 core samples were collected by MDAG on Feb 7'07. 2006 core samples were collected by Copper Fox personnel in Sep '07. pH of DI water used for paste pH read 6.2

Sample Id.	Weight Received (kg)	Dry Weight (kg)	Rinse pH Unity	Paste pH Unity	S (Total) (% Leco)	S (Sulphide) (% Leco)	S (Sulphide) (% Calc)	Carbonate Leach S (Sulphate) (%)	HCl Leachable S (Sulphate) (%)	S ($BaSO_4$) (%)	S (del_{actual}) (%)	S (del) (%)	TAP (kg $CaCO_3$/t)	SAP (kg $CaCO_3$/t)	PAP (kg $CaCO_3$/t)
Method	WEI-21	WEI-22	OA-ELE08	OA-ELE07	S-IR08	S-IR07	S-CAL06	S-GRA06	S-GRA06a	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL				0.1	0.01	0.01	0.01	0.01	0.01						
West Breccia Zone															
Maximum			NA	9.1	1.47	1.39	1.46	0.74	0.71	0.036	0.2	0.2	45.9	45.4	40.4
Minimum			NA	7.6	0.01	0.01	-0.01	0.01	0.005	0.001	-0.043	0	0.31	0.31	0.16
Mean			NA	8.34	0.41	0.32	0.35	0.065	0.059	0.01	0.015	0.023	12.8	10.8	5.57
Standard Deviation			NA	0.34	0.41	0.34	0.38	0.13	0.12	0.0065	0.045	0.039	12.7	11.6	10.1
10 Percentile			NA	8	0.04	0.026	0.016	0.01	0.005	0.0042	-0.026	0	1.25	0.81	0.16
25 Percentile			NA	8.1	0.1	0.06	0.06	0.02	0.01	0.0063	-0.013	0	3.12	1.97	0.16
Median			NA	8.3	0.25	0.2	0.21	0.03	0.02	0.0084	0.0037	0.0037	7.81	6.37	0.16
75 Percentile			NA	8.5	0.62	0.48	0.55	0.045	0.045	0.013	0.033	0.033	19.2	16.5	7.52
90 Percentile			NA	8.8	0.9	0.72	0.79	0.11	0.094	0.017	0.069	0.069	28.2	24.1	19.4
Interquartile Range (IC			NA	0.4	0.52	0.42	0.49	0.025	0.035	0.0063	0.046	0.033	16.1	14.5	7.36
Variance			NA	0.12	0.17	0.12	0.15	0.017	0.015	0.000043	0.002	0.0015	162	136	102
Skewness			NA	0.44	1.22	1.53	1.45	4.04	4.11	1.69	1.8	2.55	1.22	1.48	2.18
Coefficient of Variatior			NA	0.041	1	1.07	1.09	1.99	2.08	0.64	2.98	1.66	1	1.07	1.81
Count			0	47	47	47	47	47	47	47	47	47	47	47	47
NPR < 1.0 or NPR = 1															
1.0 < NPR < 2.0															
NPR > 2.0 or NPR =2.															
% NPR < 1.0 or NPR =															
% 1.0 < NPR < 2.0 of															
% NPR > 2.0 or NPR =															
Paramount Zone															
Maximum			NA	9.1	1.56	1.6	1.55	0.19	0.14	0.031	0.049	0.049	48.8	50	47.7
Minimum			NA	7.7	0.02	0.01	0.01	0.01	0.005	0.0021	-0.058	0	0.62	0.31	0.16
Mean			NA	8.42	0.36	0.33	0.34	0.041	0.025	0.013	-0.0067	0.0059	11.3	10.5	5.23
Standard Deviation			NA	0.34	0.4	0.39	0.39	0.039	0.033	0.0075	0.025	0.013	12.5	12.2	11.4
10 Percentile			NA	8.1	0.03	0.03	0.025	0.01	0.005	0.0063	-0.039	0	0.94	0.94	0.16
25 Percentile			NA	8.1	0.085	0.07	0.07	0.02	0.01	0.0073	-0.021	0	2.66	2.25	0.16
Median			NA	8.4	0.24	0.19	0.21	0.03	0.01	0.01	-0.0034	0	7.5	6.25	0.16
75 Percentile			NA	8.6	0.45	0.42	0.42	0.05	0.02	0.017	0.0037	0.0037	14.2	13.1	2.67
90 Percentile			NA	8.9	1.05	0.89	0.97	0.07	0.07	0.023	0.017	0.017	32.8	29.3	12.4
Interquartile Range (IC			NA	0.5	0.37	0.35	0.36	0.03	0.01	0.0094	0.025	0.0037	11.6	10.9	2.51
Variance			NA	0.12	0.16	0.15	0.15	0.0015	0.0011	0.000056	0.00063	0.00016	156	149	130
Skewness			NA	0.27	1.65	1.9	1.75	2.49	2.46	0.83	-0.068	2.48	1.65	1.85	2.73
Coefficient of Variatior			NA	0.041	1.1	1.17	1.14	0.95	1.29	0.57	-3.74	2.14	1.1	1.16	2.18
Count			0	31	31	31	31	31	31	31	31	31	31	31	31
NPR < 1.0 or NPR = 1															
1.0 < NPR < 2.0															
NPR > 2.0 or NPR =2.															
% NPR < 1.0 or NPR =															
% 1.0 < NPR < 2.0 of															
% NPR > 2.0 or NPR =															

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
pH of DI water used for paste pH read 6.2

Sample Id.	Weight Received (kg)	Dry Weight (kg)	Rinse pH Unity	Paste pH Unity	S (Total) (% Leco)	S (Sulphide) (% Leco)	S (Sulphide) (% Calc)	Carbonate Leach S (Sulphate) (%)	HCl Leachable S (Sulphate) (%)	S ($BaSO_4$) (%)	S (del_{actual}) (%)	S (del) (%)	TAP (kg $CaCO_3$/t)	SAP (kg $CaCO_3$/t)	PAP (kg $CaCO_3$/t)
Method	WEI-21	WEI-22	OA-ELE08	OA-ELE07	S-IR08	S-IR07	S-CAL06	S-GRA06	S-GRA06a	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL				0.1	0.01	0.01	0.01	0.01	0.01						
Tailings															
Maximum			8.3	8.4	0.2	0.17	0.18	0.05	0.04	0.013	-0.0025	0	6.25	5.31	0.16
Minimum			7.8	8.1	0.08	0.07	0.075	0.01	0.005	0.0084	-0.0034	0	2.5	2.19	0.16
Mean			8	8.23	0.15	0.12	0.13	0.033	0.022	0.011	-0.0028	0	4.69	3.75	0.16
Standard Deviation			0.26	0.15	0.062	0.05	0.053	0.021	0.018	0.0024	0.00047	0	1.95	1.56	0
10 Percentile			7.82	8.12	0.098	0.08	0.086	0.016	0.008	0.0092	-0.0032	0	3.06	2.5	0.16
25 Percentile			7.85	8.15	0.12	0.095	0.1	0.025	0.012	0.01	-0.003	0	3.91	2.97	0.16
Median			7.9	8.2	0.17	0.12	0.13	0.04	0.02	0.013	-0.0025	0	5.31	3.75	0.16
75 Percentile			8.1	8.3	0.18	0.15	0.16	0.045	0.03	0.013	-0.0025	0	5.78	4.53	0.16
90 Percentile			8.22	8.36	0.19	0.16	0.17	0.048	0.036	0.013	-0.0025	0	6.06	5	0.16
Interquartile Range (IC			0.25	0.15	0.06	0.05	0.053	0.02	0.017	0.0021	0.00041	0	1.88	1.56	0
Variance			0.07	0.023	0.0039	0.0025	0.0028	0.00043	0.00031	0.0000058	0.00000022	0	3.81	2.44	0
Skewness			1.46	0.94	-1.29	2E-15	-0.14	-1.29	0.42	-1.73	-1.73	NA	-1.29	0	NA
Coefficient of Variatior			0.033	0.019	0.42	0.42	0.41	0.62	0.81	0.22	-0.17	NA	0.42	0.42	0
Count			3	3	3	3	3	3	3	3	3	3	3	3	3
NPR < 1.0 or NPR = 1															
1.0 < NPR < 2.0															
NPR > 2.0 or NPR =2.															
% NPR < 1.0 or NPR =															
% 1.0 < NPR < 2.0 of															
% NPR > 2.0 or NPR =															
High-Sulphide Histor															
Maximum			NA	9.2	13.5	12.1	13.5	0.07	0.04	0.031	1.35	1.35	422	420	418
Minimum			NA	7.4	0.13	0.12	0.12	0.02	0.005	0.0042	-0.017	0	4.06	3.75	0.16
Mean			NA	8.61	4.08	3.8	4.06	0.04	0.018	0.012	0.25	0.25	127	127	123
Standard Deviation			NA	0.56	4.74	4.27	4.73	0.015	0.012	0.0089	0.49	0.49	148	148	149
10 Percentile			NA	8.1	0.61	0.55	0.6	0.027	0.0085	0.0042	-0.013	0	18.9	18.4	15.6
25 Percentile			NA	8.55	0.86	0.8	0.84	0.03	0.01	0.0073	-0.006	0	26.7	25.6	24
Median			NA	8.65	2.18	2.17	2.17	0.04	0.015	0.0084	0.0041	0.0058	68.3	67.8	60.7
75 Percentile			NA	8.95	5.18	5	5.16	0.042	0.022	0.014	0.19	0.19	162	161	159
90 Percentile			NA	9.13	10.4	9.54	10.4	0.056	0.033	0.021	0.81	0.81	325	324	322
Interquartile Range (IC			NA	0.4	4.32	4.2	4.32	0.013	0.012	0.0063	0.19	0.19	135	135	135
Variance			NA	0.31	22.5	18.2	22.4	0.00023	0.00014	0.00008	0.24	0.24	21954	21864	22160
Skewness			NA	-1.58	1.46	1.36	1.46	0.99	0.93	1.78	2.11	2.12	1.46	1.46	1.46
Coefficient of Variatior			NA	0.065	1.16	1.12	1.17	0.38	0.66	0.76	2	1.95	1.16	1.17	1.21
Count			0	8	8	8	8	8	8	8	8	8	8	8	8
NPR < 1.0 or NPR = 1															
1.0 < NPR < 2.0															
NPR > 2.0 or NPR =2.															
% NPR < 1.0 or NPR =															
% 1.0 < NPR < 2.0 of															
% NPR > 2.0 or NPR =															

Project:	**Schaft Creek**
Client:	Copper Fox Metals Inc.
Data:	**ABA Data**
Comments:	2005 core samples were collected by MDAG on Feb 7'07. 2006 core samples were collected by Copper Fox personnel in Sep '07. pH of DI water used for paste pH read 6.2

Sample Id.	Weight Received	Dry Weight	Rinse pH	Paste pH	S (Total)	S (Sulphide)	S (Sulphide)	Carbonate Leach S (Sulphate)	HCl Leachable S (Sulphate)	S $(BaSO_4)$	S (del_{actual})	S (del)	TAP	SAP	PAP
	(kg)	(kg)	Unity	Unity	(% Leco)	(% Leco)	(% Calc)	(%)	(%)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)
Method	WEI-21	WEI-22	OA-ELE08	OA-ELE07	S-IR08	S-IR07	S-CAL06	S-GRA06	S-GRA06a	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL				0.1	0.01	0.01	0.01	0.01	0.01						

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

Data in blue indicates a calculated parameter.

% S (Sulphide) (calc) = % S (Total) - % S (Sulphate) Carbonate Leach

%S$(BaSO_4)$ = Ba (ppm) * 0.0001 * 32.06 / 137.37

% S (del $_{actual}$) = %S(Total) - %S(Sulphide) Leco - %S(Sulphate) Carbonate Leach - %S$(BaSO_4)$

% S (del) = % S (del $_{actual}$) unless < 0, then 0

TAP = % S (Total) * 31.25

SAP = % S (Sulphide + del) * 31.25

PAP = % Pyrite(Calculated) * 31.25

Note: If Calculated Pyrite is < 0.005 then calculated pyrite assumed to be 0.005

Unavailable NP (UNP) = 10

Available NP = NP - Unavailable NP

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	NP	Available NP	Total C	Inorganic C	Inorganic CO_2	Excess C	Total CaNP	Inorganic CaNP	(Ca) CaNP	(Ca+Mg) CaNP	TNNP	Adjusted TNNP	SNNP	Adjusted SNNP	PNNP	Adjusted PNNP
	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(% Leco)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)
Method	OA-VOL08	Calculated	C-IR07	C-GAS05	C-GAS05	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL	1		0.01	0.05	0.2											
Main Zone																
14130	91	81	1.18	1.19	4.4	0	98.3	100.1	65.4	107.4	81.9	71.9	81.9	71.9	90.8	80.8
14144	116	106	1.43	1.37	5	0.06	119.2	113.7	93.6	141.4	107.9	97.9	108.3	98.3	115.8	105.8
14148	170	160	1.92	1.9	7	0.02	160.0	159.2	115.6	193.4	165.6	155.6	166.2	156.2	169.8	159.8
14156	73	63	0.88	0.86	3.2	0.02	73.3	72.8	61.7	94.2	67.7	57.7	68.0	58.0	72.8	62.8
14162	219	209	2.3	2.28	8.4	0.02	191.7	191.0	139.6	247.5	214.9	204.9	215.3	205.3	218.8	208.8
14169	64	54	0.7	0.69	2.5	0.01	58.3	56.9	57.9	74.4	54.6	44.6	54.8	44.8	63.8	53.8
14232	89	79	0.93	0.87	3.2	0.06	77.5	72.8	66.4	103.9	84.3	74.3	84.6	74.6	88.8	78.8
14250	118	108	1.14	1.12	4.1	0.02	95.0	93.2	101.6	179.0	112.1	102.1	112.1	102.1	117.8	107.8
14260	100	90	1.03	1.02	3.7	0.01	85.8	84.1	75.9	133.1	89.4	79.4	89.4	79.4	99.8	89.8
14276	47	37	0.43	0.25	0.9	0.18	35.8	20.5	107.6	175.2	41.7	31.7	42.6	32.6	46.8	36.8
14295	111	101	1.05	0.95	3.5	0.1	87.5	79.6	97.6	161.5	97.3	87.3	97.5	87.5	104.9	94.9
14301	136	126	1.56	1.54	5.7	0.02	130.0	129.6	91.4	142.5	125.4	115.4	125.7	115.7	134.0	124.0
14323	73	63	0.88	0.84	3.1	0.04	73.3	70.5	93.6	133.2	68.3	58.3	68.7	58.7	72.8	62.8
14332	95	85	0.84	0.74	2.7	0.1	70.0	61.4	84.7	127.5	86.9	76.9	86.9	76.9	94.8	84.8
14345	79	69	0.73	0.44	1.6	0.29	60.8	36.4	63.7	106.1	62.8	52.8	62.8	52.8	78.8	68.8
14348	59	49	0.61	0.6	2.2	0.01	50.8	50.0	53.7	103.5	45.3	35.3	44.9	34.9	58.8	48.8
14797	125	115	1.43	1.39	5.1	0.04	119.2	116.0	94.4	157.0	122.5	112.5	122.8	112.8	124.8	114.8
14808	172	162	2.23	2.21	8.1	0.02	185.8	184.2	121.6	188.7	166.4	156.4	166.7	156.7	171.8	161.8
14816	133	123	1.59	0.27	1	1.32	132.5	22.7	83.2	153.2	118.6	108.6	118.6	108.6	131.4	121.4
14828	143	133	1.7	1.69	6.2	0.01	141.7	141.0	108.4	183.3	138.9	128.9	139.6	129.6	142.8	132.8
14844	75	65	0.51	0.47	1.7	0.04	42.5	38.7	70.4	226.5	68.4	58.4	68.8	58.8	74.8	64.8
14680	102	92	1.06	1.05	3.8	0.01	88.3	86.4	103.4	171.3	95.1	85.1	95.5	85.5	101.8	91.8
14871	88	78	0.76	0.73	2.7	0.03	63.3	61.4	84.9	164.0	76.4	66.4	76.7	66.7	87.8	77.8
14887	119	109	1.2	1.18	4.3	0.02	100.0	97.8	129.4	231.1	105.3	95.3	105.9	95.9	112.3	102.3
14689	53	43	0.64	0.66	2.4	0	53.3	54.6	54.4	77.5	31.8	21.8	31.4	21.4	38.0	28.0
14695	114	104	1.35	1.3	4.8	0.05	112.5	109.2	99.4	161.6	109.6	99.6	109.9	99.9	113.8	103.8
14742	84	74	0.78	0.8	2.9	0	65.0	66.0	69.4	161.6	78.1	68.1	78.1	68.1	83.8	73.8
14666	94	84	0.77	0.74	2.7	0.03	64.2	61.4	98.1	188.7	84.0	74.0	84.3	74.3	89.0	79.0
14685	112	102	0.95	0.91	3.3	0.04	79.2	75.1	82.7	195.1	56.1	46.1	55.8	45.8	69.8	59.8
14685B	102	92	0.85	0.84	3.1	0.01	70.8	70.5	73.7	190.6	41.1	31.1	41.5	31.5	56.2	46.2
14545	77	67	0.63	0.59	2.2	0.04	52.5	50.0	95.4	153.0	71.1	61.1	71.9	61.9	75.8	65.8
14565	136	126	1.33	1.28	4.7	0.05	110.8	106.9	114.4	164.2	128.8	118.8	128.5	118.5	135.8	125.8
14571	76	66	0.76	0.75	2.8	0.01	63.3	63.7	64.7	112.9	43.5	33.5	43.8	33.8	61.3	51.3
14578	111	101	1.25	1.26	4.6	0	104.2	104.6	104.9	153.5	54.1	44.1	54.1	44.1	63.6	53.6
14578B	122	112	1.38	1.35	5	0.03	115.0	113.7	107.9	160.2	61.7	51.7	62.3	52.3	72.8	62.8
14598	77	67	0.59	0.57	2.1	0.02	49.2	47.8	83.7	174.6	72.9	62.9	72.9	62.9	75.4	65.4
14893	111	101	1.03	1.03	3.8	0	85.8	86.4	103.9	215.9	107.6	97.6	108.5	98.5	110.8	100.8
14899	81	71	0.68	0.65	2.4	0.03	56.7	54.6	88.4	258.4	80.4	70.4	80.4	70.4	80.8	70.8
14908	75	65	0.56	0.56	2.1	0	46.7	47.8	94.6	193.5	72.5	62.5	72.8	62.8	74.8	64.8
14917	66	56	0.55	0.54	2	0.01	45.8	45.5	57.9	133.3	60.1	50.1	60.8	50.8	65.8	55.8
14925	82	72	0.72	0.73	2.7	0	60.0	61.4	89.9	173.9	77.6	67.6	78.0	68.0	81.8	71.8
14998	103	93	1.05	1.04	3.8	0.01	87.5	86.4	99.4	166.5	98.9	88.9	99.3	89.3	102.8	92.8
15862	130	120	1.34	1.34	4.9	0	111.7	111.4	105.4	177.0	127.5	117.5	127.9	117.9	129.8	119.8
15870	151	141	1.72	1.72	6.3	0	143.3	143.3	115.9	188.7	146.9	136.9	147.9	137.9	150.8	140.8
15879	118	108	1.33	1.31	4.8	0.02	110.8	109.2	120.6	198.0	114.3	104.3	115.0	105.0	117.8	107.8

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	NP	Available NP	Total C	Inorganic C	Inorganic CO_2	Excess C	Total CaNP	Inorganic CaNP	(Ca) CaNP	(Ca+Mg) CaNP	TNNP	Adjusted TNNP	SNNP	Adjusted SNNP	PNNP	Adjusted PNNP
	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(% Leco)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)
Method	OA-VOL08	Calculated	C-IR07	C-GAS05	C-GAS05	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL	1		0.01	0.05	0.2											
15887	95	85	0.94	0.91	3.3	0.03	78.3	75.1	102.9	168.4	85.3	75.3	85.8	75.8	94.8	84.8
15891	128	118	1.44	1.4	5.1	0.04	120.0	116.0	128.1	199.3	123.6	113.6	124.8	114.8	127.8	117.8
15908	121	111	1.2	1.2	4.4	0	100.0	100.1	112.9	189.0	114.1	104.1	114.5	104.5	120.8	110.8
15911	92	82	0.85	0.82	3	0.03	70.8	68.2	87.9	183.0	89.2	79.2	89.7	79.7	91.8	81.8
125285	54	44	0.51	0.52	1.9	0	42.5	43.2	58.2	138.1	44.0	34.0	44.6	34.6	53.8	43.8
125288	74	64	0.78	0.71	2.6	0.07	65.0	59.1	155.1	419.8	70.9	60.9	71.3	61.3	72.0	62.0
125293	62	52	0.63	0.61	2.2	0.02	52.5	50.0	60.2	169.3	55.4	45.4	55.8	45.8	61.8	51.8
125305	70	60	0.85	0.86	3.1	0	70.8	70.5	69.2	152.3	66.3	56.3	66.3	56.3	69.8	59.8
125311	59	49	0.7	0.68	2.5	0.02	58.3	56.9	58.7	115.5	57.1	47.1	57.4	47.4	58.8	48.8
125703	86	76	1.16	1.17	4.3	0	96.7	97.8	83.2	137.1	82.9	72.9	83.2	73.2	85.8	75.8
125728	75	65	0.81	0.81	3	0	67.5	68.2	84.4	167.2	69.1	59.1	69.4	59.4	74.8	64.8
125755	50	40	0.6	0.57	2.1	0.03	50.0	47.8	45.9	67.8	31.6	21.6	32.8	22.8	43.9	33.9
125772	86	76	1	1.01	3.7	0	83.3	84.1	86.7	169.8	79.4	69.4	79.9	69.9	85.8	75.8
125795	142	132	1.47	1.43	5.2	0.04	122.5	118.3	110.6	192.1	138.6	128.6	139.5	129.5	141.8	131.8
125422	86	76	1.19	1.11	4.1	0.08	99.2	93.2	91.9	159.0	79.4	69.4	79.4	69.4	85.8	75.8
125435	86	76	1.05	1.01	3.7	0.04	87.5	84.1	86.9	141.7	81.0	71.0	81.4	71.4	85.8	75.8
125452	82	72	0.97	0.96	3.5	0.01	80.8	79.6	96.1	158.7	67.3	57.3	67.3	57.3	81.8	71.8
125476	76	66	1	0.99	3.6	0.01	83.3	81.9	53.7	85.0	51.6	41.6	53.2	43.2	64.6	54.6
125490	74	64	0.87	0.83	3.1	0.04	72.5	70.5	86.7	168.2	63.1	53.1	63.7	53.7	70.4	60.4
126192	80	70	1.01	0.98	3.6	0.03	84.2	81.9	92.4	133.2	74.1	64.1	74.3	64.3	79.8	69.8
126206	71	61	0.84	0.79	2.9	0.05	70.0	66.0	99.4	146.7	64.1	54.1	64.6	54.6	70.7	60.7
126225	75	65	0.88	0.86	3.1	0.02	73.3	70.5	89.2	119.2	64.1	54.1	64.7	54.7	74.0	64.0
126244	90	80	1.13	1.11	4.1	0.02	94.2	93.2	104.4	155.0	81.9	71.9	82.2	72.2	89.8	79.8
126266	80	70	0.99	0.97	3.6	0.02	82.5	81.9	90.7	143.8	74.1	64.1	74.3	64.3	79.8	69.8
126279	134	124	1.36	1.35	5	0.01	113.3	113.7	107.6	150.9	121.8	111.8	122.1	112.1	129.7	119.7
126288	122	112	1.22	1.21	4.4	0.01	101.7	100.1	106.1	149.4	110.4	100.4	110.9	100.9	121.8	111.8
126297	161	151	1.61	1.56	5.7	0.05	134.2	129.6	135.1	206.7	145.1	135.1	145.3	135.3	153.5	143.5
126314	119	109	1.13	1.09	4	0.04	94.2	91.0	106.6	168.4	76.2	66.2	76.5	66.5	99.0	89.0
126329	132	122	1.39	1.37	5	0.02	115.8	113.7	109.4	162.5	124.5	114.5	125.6	115.6	131.8	121.8
126337	127	117	1.25	1.19	4.4	0.06	104.2	100.1	104.6	174.6	109.2	99.2	109.6	99.6	126.4	116.4
126351	129	119	1.3	1.24	4.6	0.06	108.3	104.6	113.1	176.5	124.6	114.6	125.0	115.0	128.8	118.8
126427	167	157	1.59	1.48	5.4	0.11	132.5	122.8	127.4	224.9	132.0	122.0	132.3	122.3	133.9	123.9
126430	136	126	1.28	1.28	4.7	0	106.7	106.9	113.6	184.9	129.4	119.4	129.7	119.7	130.3	120.3
126434	127	117	1.28	1.22	4.5	0.06	106.7	102.3	105.4	150.7	123.6	113.6	123.8	113.8	124.3	114.3
126443	136	126	1.49	1.41	5.2	0.08	124.2	118.3	105.4	165.9	82.9	72.9	83.1	73.1	84.8	74.8
126449	47	37	0.31	0.3	1.1	0.01	25.8	25.0	123.9	282.0	46.4	36.4	46.1	36.1	46.4	36.4
126464	88	78	1.07	1.04	3.8	0.03	89.2	86.4	112.4	170.8	74.6	64.6	74.9	64.9	81.4	71.4
126492	91	81	1.2	1.16	4.3	0.04	100.0	97.8	107.1	167.7	84.1	74.1	84.6	74.6	90.8	80.8
145655	86	76	1.04	1.02	3.8	0.02	86.7	86.4	117.6	177.7	65.4	55.4	66.8	56.8	71.3	61.3
145669	89	79	1.07	1.07	3.9	0	89.2	88.7	104.9	164.2	59.3	49.3	60.7	50.7	67.8	57.8
145685	82	72	1.01	1.03	3.8	0	84.2	86.4	92.9	162.9	74.8	64.8	75.6	65.6	81.8	71.8
145694	118	108	1.24	1.23	4.5	0.01	103.3	102.3	109.1	180.4	112.7	102.7	113.3	103.3	117.8	107.8
145708	80	70	0.89	0.92	3.4	0	74.2	77.3	86.7	133.6	71.9	61.9	72.3	62.3	78.5	68.5
145723	70	60	0.75	0.61	2.3	0.14	62.5	52.3	85.7	133.4	19.1	9.1	20.4	10.4	36.7	26.7
146798	90	80	1.71	1.68	6.2	0.03	142.5	141.0	106.6	162.2	83.4	73.4	83.9	73.9	89.8	79.8
146824	81	71	0.94	0.9	3.3	0.04	78.3	75.1	96.1	194.5	75.7	65.7	76.2	66.2	80.8	70.8

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	NP	Available NP	Total C	Inorganic C	Inorganic CO_2	Excess C	Total CaNP	Inorganic CaNP	(Ca) CaNP	(Ca+Mg) CaNP	TNNP	Adjusted TNNP	SNNP	Adjusted SNNP	PNNP	Adjusted PNNP
	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(% Leco)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)
Method	OA-VOL08	Calculated	C-IR07	C-GAS05	C-GAS05	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL	1		0.01	0.05	0.2											
146831	85	75	1.02	1	3.7	0.02	85.0	84.1	96.9	208.5	73.8	63.8	74.1	64.1	84.8	74.8
146843																
146861	48	38	0.46	0.43	1.6	0.03	38.3	36.4	104.9	173.2	43.9	33.9	44.6	34.6	47.8	37.8
146868	66	56	0.76	0.72	2.6	0.04	63.3	59.1	92.9	152.2	50.1	40.1	51.5	41.5	61.3	51.3
126352	64	54	0.63	0.63	2.3	0	52.5	52.3	95.9	192.2	45.3	35.3	45.8	35.8	61.9	51.9
126358	70	60	0.76	0.73	2.7	0.03	63.3	61.4	91.6	175.6	59.7	49.7	60.0	50.0	69.8	59.8
126374	68	58	0.74	0.7	2.6	0.04	61.7	59.1	94.1	186.8	62.7	52.7	63.0	53.0	67.8	57.8
126384	62	52	0.67	0.66	2.4	0.01	55.8	54.6	98.6	162.9	58.6	48.6	58.9	48.9	61.8	51.8
126391	72	62	0.82	0.71	2.6	0.11	68.3	59.1	105.4	178.3	66.4	56.4	66.8	56.8	71.8	61.8
146172	139	129	1.65	1.65	6.1	0	137.5	138.7	86.2	143.0	131.5	121.5	132.1	122.1	138.8	128.8
146182	55	45	0.51	0.54	2	0	42.5	45.5	93.4	171.2	50.3	40.3	50.9	40.9	54.8	44.8
146203	61	51	0.63	0.65	2.4	0	52.5	54.6	73.2	137.8	55.4	45.4	56.0	46.0	60.8	50.8
146214	91	81	1.06	1.07	3.9	0	88.3	88.7	103.6	161.3	79.8	69.8	84.1	74.1	90.8	80.8
146221	82	72	0.98	0.99	3.6	0	81.7	81.9	90.9	190.9	56.7	46.7	58.4	48.4	77.7	67.7
146238	53	43	0.49	0.49	1.8	0	40.8	40.9	106.6	195.2	48.9	38.9	49.9	39.9	52.8	42.8
147034	77	67	1.21	1.15	4.2	0.06	100.8	95.5	73.2	113.5	60.8	50.8	61.1	51.1	76.8	66.8
147038	77	67	1.07	1.04	3.8	0.03	89.2	86.4	66.2	110.6	66.1	56.1	67.8	57.8	76.8	66.8
147051	61	51	0.66	0.64	2.3	0.02	55.0	52.3	89.4	154.5	50.7	40.7	51.7	41.7	59.2	49.2
147070	54	44	0.54	0.51	1.9	0.03	45.0	43.2	135.6	214.2	38.1	28.1	38.5	28.5	39.5	29.5
147087	42	32	0.39	0.3	1.1	0.09	32.5	25.0	87.9	161.6	-62.7	-72.7	-59.7	-69.7	-59.0	-69.0
147097	132	122	1.32	1.28	4.7	0.04	110.0	106.9	111.6	176.3	110.8	100.8	112.2	102.2	114.5	104.5
145508	57	47	0.58	0.55	2	0.03	48.3	45.5	74.7	238.9	55.8	45.8	56.1	46.1	56.8	46.8
145527	73	63	0.85	0.81	3	0.04	70.8	68.2	106.6	170.4	58.0	48.0	58.6	48.6	65.3	55.3
145543	51	41	0.54	0.53	1.9	0.01	45.0	43.2	84.2	154.6	47.3	37.3	47.6	37.6	50.8	40.8
145562	79	69	0.97	0.9	3.3	0.07	80.8	75.1	98.6	168.6	76.2	66.2	76.5	66.5	78.8	68.8
145576	58	48	0.78	0.76	2.8	0.02	65.0	63.7	43.5	67.7	36.4	26.4	37.3	27.3	46.9	36.9
145601	71	61	0.82	0.76	2.8	0.06	68.3	63.7	119.9	200.2	55.4	45.4	56.1	46.1	64.5	54.5
146297	86	76	1.2	1.09	4	0.11	100.0	91.0	94.6	175.8	75.1	65.1	75.9	65.9	85.8	75.8
146314	72	62	0.74	0.75	2.8	0	61.7	63.7	98.6	167.4	67.3	57.3	67.6	57.6	71.8	61.8
146335	90	80	1.09	1.1	4	0	90.8	91.0	107.9	164.3	85.9	75.9	87.2	77.2	89.8	79.8
146352	69	59	0.76	0.77	2.8	0	63.3	63.7	79.2	143.0	67.1	57.1	67.6	57.6	68.8	58.8
146368	79	69	0.91	0.94	3.4	0	75.8	77.3	99.4	157.9	73.1	63.1	76.3	66.3	78.8	68.8
146390	71	61	0.89	0.85	3.1	0.04	74.2	70.5	118.9	182.3	66.0	56.0	66.3	56.3	70.8	60.8
146508	89	79	1.35	1.3	4.8	0.05	112.5	109.2	87.7	188.5	87.1	77.1	87.1	77.1	88.8	78.8
146526	55	45	0.56	0.53	2	0.03	46.7	45.5	104.6	168.9	33.8	23.8	53.1	43.1	54.8	44.8
146544	90	80	1.22	1.16	4.3	0.06	101.7	97.8	92.4	139.3	82.5	72.5	86.9	76.9	89.8	79.8
146565	88	78	1.63	1.56	5.7	0.07	135.8	129.6	88.2	135.9	84.6	74.6	85.5	75.5	87.8	77.8
146589	89	79	1.26	1.2	4.4	0.06	105.0	100.1	99.6	169.6	84.9	74.9	85.5	75.5	88.8	78.8
146613	129	119	1.33	1.3	4.8	0.03	110.8	109.2	140.6	204.0	112.1	102.1	112.6	102.6	122.9	112.9
146627	92	82	1.8	1.74	6.4	0.06	150.0	145.6	86.9	152.4	89.2	79.2	89.8	79.8	91.8	81.8
146637	87	77	1.45	1.42	5.2	0.03	120.8	118.3	74.4	119.7	72.6	62.6	73.6	63.6	85.0	75.0
146649	77	67	1.14	1.09	4	0.05	95.0	91.0	63.7	103.6	68.3	58.3	69.6	59.6	72.9	62.9
146657	60	50	0.79	0.76	2.8	0.03	65.8	63.7	47.7	80.2	54.1	44.1	54.1	44.1	59.8	49.8
146676	88	78	1.08	1.05	3.8	0.03	90.0	86.4	98.4	135.0	81.4	71.4	82.2	72.2	87.8	77.8
125188	81	71	1.23	1.24	4.6	0	102.5	104.6	76.4	126.2	72.9	62.9	74.0	64.0	80.8	70.8
125198	75	65	0.92	0.92	3.4	0	76.7	77.3	84.2	141.4	68.1	58.1	68.6	58.6	74.8	64.8

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	NP	Available NP	Total C	Inorganic C	Inorganic CO_2	Excess C	Total CaNP	Inorganic CaNP	(Ca) CaNP	(Ca+Mg) CaNP	TNNP	Adjusted TNNP	SNNP	Adjusted SNNP	PNNP	Adjusted PNNP
	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(% Leco)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)
Method	OA-VOL08	Calculated	C-IR07	C-GAS05	C-GAS05	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL	1		0.01	0.05	0.2											
125207	93	83	1.66	1.67	6.1	0	138.3	138.7	89.4	142.1	89.6	79.6	89.9	79.9	92.8	82.8
125228	70	60	1.02	1.04	3.8	0	85.0	86.4	51.9	84.9	65.3	55.3	65.6	55.6	69.8	59.8
125244	57	47	0.74	0.73	2.7	0.01	61.7	61.4	45.0	81.2	52.3	42.3	52.8	42.8	56.8	46.8
125257	52	42	0.42	0.42	1.5	0	35.0	34.1	197.3	377.6	50.1	40.1	50.1	40.1	50.7	40.7
125278	35	25	0.29	0.3	1.1	0	24.2	25.0	86.2	145.9	34.4	24.4	34.7	24.7	34.8	24.8
125596	93	83	1.16	1.12	4.1	0.04	96.7	93.2	122.1	189.6	89.3	79.3	88.9	78.9	92.8	82.8
125610	76	66	0.99	0.96	3.5	0.03	82.5	79.6	66.4	140.1	74.1	64.1	74.3	64.3	75.8	65.8
125626																
125641	86	76	1.05	1.03	3.8	0.02	87.5	86.4	89.4	193.2	82.9	72.9	83.2	73.2	85.8	75.8
125669	84	74	1.13	1.06	3.9	0.07	94.2	88.7	75.4	150.4	52.4	42.4	53.2	43.2	64.4	54.4
125690	60	50	0.63	0.62	2.3	0.01	52.5	52.3	92.1	180.7	56.9	46.9	57.7	47.7	59.8	49.8
West Breccia Zone																
14018	42	32	0.4	0.38	1.4	0.02	33.3	31.8	44.5	88.5	17.0	7.0	18.0	8.0	22.3	12.3
14021	64	54	0.76	0.72	2.6	0.04	63.3	59.1	65.4	103.3	44.6	34.6	45.1	35.1	51.5	41.5
14036	49	39	0.52	0.48	1.8	0.04	43.3	40.9	45.9	83.4	3.1	-6.9	3.6	-6.4	11.2	1.2
14043	40	30	0.33	0.21	0.8	0.12	27.5	18.2	35.0	113.2	31.9	21.9	32.2	22.2	37.2	27.2
14060	41	31	0.29	0.28	1	0.01	24.2	22.7	78.4	164.9	0.1	-9.9	21.6	11.6	30.4	20.4
14067	49	39	0.41	0.35	1.3	0.06	34.2	29.6	64.7	175.0	36.5	26.5	36.2	26.2	44.3	34.3
14076	66	56	0.71	0.7	2.6	0.01	59.2	59.1	108.4	211.3	41.9	31.9	42.3	32.3	46.9	36.9
14083	74	64	0.85	0.83	3	0.02	70.8	68.2	100.6	173.5	28.4	18.4	29.1	19.1	33.6	23.6
14099	78	68	0.92	0.92	3.4	0	76.7	77.3	73.7	107.4	67.4	57.4	68.2	58.2	72.4	62.4
14103	85	75	0.9	0.87	3.2	0.03	75.0	72.8	73.2	126.3	63.4	53.4	76.8	66.8	84.8	74.8
125046	66	56	0.73	0.72	2.6	0.01	60.8	59.1	96.4	181.6	62.6	52.6	62.9	52.9	65.8	55.8
125068	63	53	0.61	0.59	2.2	0.02	50.8	50.0	106.1	196.7	50.8	40.8	51.8	41.8	62.8	52.8
125073	68	58	0.77	0.71	2.6	0.06	64.2	59.1	83.7	144.2	49.3	39.3	51.6	41.6	67.8	57.8
125079	40	30	0.42	0.4	1.5	0.02	35.0	34.1	46.2	83.3	-0.3	-10.3	2.4	-7.6	39.8	29.8
125084	42	32	0.41	0.32	1.2	0.09	34.2	27.3	94.4	176.3	22.9	12.9	25.5	15.5	41.8	31.8
125127	48	38	0.38	0.36	1.3	0.02	31.7	29.6	58.9	152.4	45.5	35.5	46.1	36.1	47.8	37.8
125129	46	36	0.54	0.47	1.7	0.07	45.0	38.7	43.7	118.2	38.2	28.2	39.6	29.6	45.8	35.8
125134	34	24	0.25	0.25	0.9	0	20.8	20.5	36.2	118.1	15.6	5.6	17.5	7.5	33.8	23.8
125142	51	41	0.49	0.51	1.9	0	40.8	43.2	51.2	135.2	42.9	32.9	43.8	33.8	50.8	40.8
125149	79	69	0.91	0.89	3.3	0.02	75.8	75.1	78.9	159.2	74.9	64.9	75.6	65.6	78.8	68.8
125154	70	60	1.09	0.06	0.2	1.03	90.8	4.5	58.7	99.9	67.5	57.5	67.9	57.9	69.8	59.8
125165	48	38	0.41	0.36	1.3	0.05	34.2	29.6	73.7	137.9	42.1	32.1	42.7	32.7	47.8	37.8
125176	60	50	0.62	0.61	2.2	0.01	51.7	50.0	63.4	133.0	52.5	42.5	54.6	44.6	59.8	49.8
146112	43	33	0.34	0.35	1.3	0	28.3	29.6	78.9	132.4	39.3	29.3	40.2	30.2	42.8	32.8
146115	40	30	0.18	0.2	0.7	0	15.0	15.9	179.6	335.6	35.9	25.9	37.0	27.0	37.3	27.3
146124	53	43	0.48	0.46	1.7	0.02	40.0	38.7	101.9	173.9	50.2	40.2	51.1	41.1	52.8	42.8
146127	62	52	0.69	0.71	2.6	0	57.5	59.1	62.9	84.8	28.9	18.9	30.2	20.2	31.2	21.2
146135	37	27	0.26	0.26	1	0	21.7	22.7	103.9	155.4	35.8	25.8	36.1	26.1	36.8	26.8
146149	49	39	0.45	0.47	1.7	0	37.5	38.7	103.4	144.6	46.8	36.8	47.8	37.8	48.7	38.7
146161	50	40	0.42	0.42	1.6	0	35.0	36.4	161.1	295.7	48.8	38.8	49.4	39.4	49.8	39.8
146164	30	20	0.13	0.14	0.5	0	10.8	11.4	87.7	232.2	29.4	19.4	29.7	19.7	29.8	19.8
145951	88	78	1.01	1.03	3.8	0	84.2	86.4	104.9	162.1	82.4	72.4	83.2	73.2	87.8	77.8
145956	77	67	0.86	0.87	3.2	0	71.7	72.8	81.2	172.6	71.1	61.1	72.0	62.0	76.8	66.8
145974	62	52	0.63	0.68	2.5	0	52.5	56.9	64.2	161.3	61.4	51.4	61.4	51.4	61.8	51.8

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	NP	Available NP	Total C	Inorganic C	Inorganic CO_2	Excess C	Total CaNP	Inorganic CaNP	(Ca) CaNP	(Ca+Mg) CaNP	TNNP	Adjusted TNNP	SNNP	Adjusted SNNP	PNNP	Adjusted PNNP
	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(% Leco)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)
Method	OA-VOL08	Calculated	C-IR07	C-GAS05	C-GAS05	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL	1		0.01	0.05	0.2											
145982	85	75	0.97	0.97	3.6	0	80.8	81.9	154.8	284.1	83.4	73.4	84.1	74.1	84.3	74.3
145992	65	55	0.7	0.71	2.6	0	58.3	59.1	66.9	133.2	56.3	46.3	57.4	47.4	63.5	53.5
145999	66	56	0.68	0.69	2.5	0	56.7	56.9	88.2	153.6	61.6	51.6	63.5	53.5	65.8	55.8
145834	39	29	0.31	0.33	1.2	0	25.8	27.3	76.7	144.2	37.8	27.8	37.8	27.8	38.8	28.8
145842	42	32	0.3	0.34	1.2	0	25.0	27.3	194.8	296.5	41.1	31.1	41.4	31.4	41.8	31.8
145852	21	11	0.09	0.12	0.4	0	7.5	9.1	108.9	151.7	17.6	7.6	18.2	8.2	20.8	10.8
145857	30	20	0.18	0.19	0.7	0	15.0	15.9	111.6	176.3	29.7	19.7	29.7	19.7	29.8	19.8
145871	58	48	0.54	0.57	2.1	0	45.0	47.8	104.1	163.4	53.0	43.0	56.4	46.4	57.7	47.7
145608	46	36	0.43	0.42	1.5	0.01	35.8	34.1	92.1	222.3	21.3	11.3	21.7	11.7	24.0	14.0
145614	47	37	0.42	0.41	1.5	0.01	35.0	34.1	90.4	199.9	29.5	19.5	30.0	20.0	35.7	25.7
145628	78	68	0.89	0.86	3.2	0.03	74.2	72.8	91.1	181.3	53.3	43.3	64.0	54.0	67.3	57.3
145640	62	52	0.71	0.64	2.4	0.07	59.2	54.6	110.6	214.8	38.6	28.6	41.1	31.1	47.1	37.1
145646	46	36	0.45	0.42	1.5	0.03	37.5	34.1	92.4	204.4	28.2	18.2	31.6	21.6	36.6	26.6
Paramount Zone																
125965	52	42	0.52	0.51	1.9	0.01	43.3	43.2	63.9	148.7	41.1	31.1	41.6	31.6	51.8	41.8
125974	58	48	0.65	0.65	2.4	0	54.2	54.6	45.5	128.2	9.3	-0.8	8.0	-2.0	10.3	0.3
125983	79	69	0.95	0.95	3.5	0	79.2	79.6	92.4	232.4	69.6	59.6	70.3	60.3	76.2	66.2
125988	49	39	0.35	0.37	1.4	0	29.2	31.8	118.9	252.3	48.1	38.1	48.1	38.1	48.4	38.4
126007	66	56	0.82	0.86	3.1	0	68.3	70.5	53.2	88.6	61.3	51.3	61.9	51.9	65.8	55.8
126031	45	35	0.46	0.51	1.9	0	38.3	43.2	46.7	80.5	40.9	30.9	41.3	31.3	44.8	34.8
126040	46	36	0.43	0.44	1.6	0	35.8	36.4	45.9	126.6	25.4	15.4	25.9	15.9	35.4	25.4
126054	159	149	1.51	1.51	5.5	0	125.8	125.1	120.1	288.1	153.4	143.4	154.0	144.0	158.8	148.8
126067	89	79	1.08	1.1	4	0	90.0	91.0	108.9	238.2	79.3	69.3	79.8	69.8	87.9	77.9
126081	63	53	0.83	0.84	3.1	0	69.2	70.5	46.4	84.3	28.9	18.9	33.7	23.7	53.4	43.4
126110	65	55	0.68	0.67	2.4	0.01	56.7	54.6	121.6	239.0	63.1	53.1	63.4	53.4	64.0	54.0
126118	87	77	1.56	1.58	5.8	0	130.0	131.9	88.4	190.9	62.6	52.6	67.3	57.3	85.9	75.9
125904	86	76	1.07	1.04	3.8	0.03	89.2	86.4	96.1	146.8	80.4	70.4	80.7	70.7	85.8	75.8
125919	54	44	0.53	0.54	2	0	44.2	45.5	56.7	131.6	38.1	28.1	38.9	28.9	53.8	43.8
125928	58	48	0.62	0.62	2.3	0	51.7	52.3	69.4	155.9	55.2	45.2	55.5	45.5	57.8	47.8
125933	89	79	1.19	1.15	4.2	0.04	99.2	95.5	95.6	219.6	88.4	78.4	88.7	78.7	88.8	78.8
125944	61	51	0.63	0.63	2.3	0	52.5	52.3	84.4	179.9	57.3	47.3	57.3	47.3	58.4	48.4
125952	81	71	1.01	1.02	3.7	0	84.2	84.1	74.2	116.6	48.2	38.2	48.5	38.5	49.3	39.3
125963	87	77	1.04	1.05	3.8	0	86.7	86.4	89.4	176.7	73.6	63.6	75.1	65.1	86.8	76.8
126120	30	20	0.3	0.31	1.2	0	25.0	27.3	41.0	76.4	28.1	18.1	28.4	18.4	29.8	19.8
126131	53	43	0.55	0.56	2.1	0	45.8	47.8	61.4	112.1	52.1	42.1	52.4	42.4	52.8	42.8
126142	47	37	0.45	0.45	1.7	0	37.5	38.7	68.9	132.3	45.4	35.4	45.8	35.8	46.8	36.8
126154	75	65	0.86	0.89	3.3	0	71.7	75.1	75.2	177.7	70.9	60.9	71.6	61.6	74.8	64.8
126171	90	80	1.53	1.5	5.5	0.03	127.5	125.1	84.7	155.9	50.0	40.0	51.3	41.3	57.4	47.4
126181	48	38	0.48	0.46	1.7	0.02	40.0	38.7	104.4	200.3	40.2	30.2	41.7	31.7	42.7	32.7
125806	52	42	0.61	0.55	2	0.06	50.8	45.5	63.7	111.9	37.0	27.0	37.6	27.6	39.6	29.6
125816	67	57	0.74	0.72	2.7	0.02	61.7	61.4	91.9	186.6	66.1	56.1	66.1	56.1	66.5	56.5
125833	46	36	0.52	0.51	1.9	0.01	43.3	43.2	51.9	84.9	37.6	27.6	37.6	27.6	45.8	35.8
125861	46	36	0.5	0.51	1.9	0	41.7	43.2	48.4	83.0	35.4	25.4	38.1	28.1	45.8	35.8
125875	56	46	0.72	0.64	2.4	0.08	60.0	54.6	54.4	84.5	48.5	38.5	49.8	39.8	55.8	45.8
125897	54	44	0.59	0.6	2.2	0	49.2	50.0	53.7	87.0	51.5	41.5	52.0	42.0	53.8	43.8

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	NP	Available NP	Total C	Inorganic C	Inorganic CO_2	Excess C	Total CaNP	Inorganic CaNP	(Ca) CaNP	(Ca+Mg) CaNP	TNNP	Adjusted TNNP	SNNP	Adjusted SNNP	PNNP	Adjusted PNNP
	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(% Leco)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)
Method	OA-VOL08	Calculated	C-IR07	C-GAS05	C-GAS05	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL	1		0.01	0.05	0.2											
Tailings																
LIARD ZONE	103	93	1.07	1.03	3.8	0.04	89.2	86.4	84.9	142.1	100.5	90.5	100.8	90.8	102.8	92.8
PARAMOUNT	85	75	0.83	0.82	3	0.01	69.2	68.2	67.2	124.4	79.7	69.7	81.3	71.3	84.8	74.8
WEST BRECCIA	67	57	0.54	0.5	1.8	0.04	45.0	40.9	69.9	148.6	60.8	50.8	61.7	51.7	66.8	56.8
High-Sulphide Histor																
T112 (171' - 172')	59	49	0.55	0.53	2	0.02	45.8	45.5	105.1	244.3	-224.1	-234.1	-223.1	-233.1	-222.1	-232.1
T113 (81' - 82')	23	13	0.16	0.17	0.6	0	13.3	13.6	21.2	77.2	-4.2	-14.2	-2.9	-12.9	-1.7	-11.7
T113 (983' - 985')	84	74	1.29	1.25	4.6	0.04	107.5	104.6	61.4	135.5	18.1	8.1	18.7	8.7	32.4	22.4
T140 (30' - 31')	62	52	0.73	0.69	2.5	0.04	60.8	56.9	77.4	138.4	57.9	47.9	58.3	48.3	61.8	51.8
T166 (389' - 390')	40	30	0.48	0.43	1.6	0.05	40.0	36.4	42.2	69.0	14.7	4.7	15.4	5.4	17.8	7.8
T185 (116' - 117')	35	25	0.46	0.42	1.6	0.04	38.3	36.4	23.5	49.4	-35.6	-45.6	-35.3	-45.3	-34.9	-44.9
T207 (261.5' - 262')	40	30	0.53	0.5	1.8	0.03	44.2	40.9	26.0	44.5	-81.3	-91.3	-80.7	-90.7	-78.5	-88.5
T207 (269' - 271')	35	25	0.52	0.46	1.7	0.06	43.3	38.7	22.7	47.8	-386.9	-396.9	-385.4	-395.4	-383.4	-393.4

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	NP	Available NP	Total C	Inorganic C	Inorganic CO_2	Excess C	Total CaNP	Inorganic CaNP	(Ca) CaNP	(Ca+Mg) CaNP	TNNP	Adjusted TNNP	SNNP	Adjusted SNNP	PNNP	Adjusted PNNP
	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(% Leco)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)
Method	OA-VOL08	Calculated	C-IR07	C-GAS05	C-GAS05	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL	1		0.01	0.05	0.2											
All Data																
Maximum	219	209	2.3	2.28	8.4	1.32	192	191	197	420	215	205	215	205	219	209
Minimum	21	11	0.09	0.06	0.2	0	7.5	4.55	21.2	44.5	-387	-397	-385	-395	-383	-393
Mean	78.5	68.5	0.87	0.84	3.09	0.036	72.9	70.4	88.1	160	62.9	52.9	63.9	53.9	69.6	59.6
Standard Deviation	31.1	31.1	0.39	0.39	1.44	0.11	32.8	32.7	27.5	51.8	49.8	49.8	49.6	49.6	49.8	49.8
10 Percentile	46	36	0.42	0.37	1.4	0	35	31.8	52.4	88.5	29.1	19.1	30.1	20.1	36.6	26.6
25 Percentile	56.5	46.5	0.56	0.54	2	0	46.7	45.5	69.3	133	45.2	35.2	45.8	35.8	51.2	41.2
Median	75	65	0.84	0.81	3	0.02	70	68.2	89.9	161	63.1	53.1	64.6	54.6	70.4	60.4
75 Percentile	89.5	79.5	1.11	1.08	3.95	0.04	92.5	89.8	105	182	82.2	72.2	83.1	73.1	87.8	77.8
90 Percentile	126	116	1.39	1.35	5	0.06	116	114	116	215	112	102	113	103	121	111
Interquartile Range (I	33	33	0.55	0.54	1.95	0.04	45.8	44.3	35.6	48.8	36.9	36.9	37.3	37.3	36.7	36.7
Variance	969	969	0.15	0.15	2.07	0.012	1076	1070	756	2684	2484	2484	2458	2458	2480	2480
Skewness	1.09	1.09	0.63	0.64	0.64	9.63	0.63	0.64	0.46	1.05	-3.83	-3.83	-3.87	-3.87	-3.98	-3.98
Coefficient of Variatio	0.4	0.45	0.45	0.47	0.46	3.12	0.45	0.46	0.31	0.32	0.79	0.94	0.78	0.92	0.72	0.84
Count	235	235	235	235	235	235	235	235	235	235	235	235	235	235	235	235
NPR < 1.0 or NPR = 1																
1.0 < NPR < 2.0																
NPR > 2.0 or NPR =2.																
% NPR < 1.0 or NPR =																
% 1.0 < NPR < 2.0 of																
% NPR > 2.0 or NPR =																
Main Zone																
Maximum	219	209	2.3	2.28	8.4	1.32	192	191	197	420	215	205	215	205	219	209
Minimum	35	25	0.29	0.25	0.9	0	24.2	20.5	43.5	67.7	-62.7	-72.7	-59.7	-69.7	-59	-69
Mean	90.4	80.4	1.02	0.98	3.6	0.04	84.9	81.9	93.7	164	78.9	68.9	79.6	69.6	85.7	75.7
Standard Deviation	30.4	30.4	0.37	0.37	1.37	0.11	30.9	31.1	22.6	46	33	33	32.7	32.7	32.3	32.3
10 Percentile	57	47	0.57	0.54	2	0	47.5	45.5	63.7	112	45.8	35.8	46.8	36.8	54.8	44.8
25 Percentile	71	61	0.76	0.72	2.62	0.01	63.3	59.7	83.8	141	58.1	48.1	58.7	48.7	66.3	56.3
Median	84.5	74.5	1	0.98	3.6	0.02	83.3	81.9	93.9	164	74.1	64.1	74.3	64.3	80.8	70.8
75 Percentile	111	101	1.24	1.2	4.4	0.04	103	100	107	183	89.3	79.3	89.7	79.7	98	88
90 Percentile	132	122	1.48	1.42	5.2	0.07	123	118	118	200	124	114	125	115	130	120
Interquartile Range (I	40	40	0.48	0.48	1.78	0.03	39.8	40.4	22.7	41.4	31.2	31.2	31	31	31.6	31.6
Variance	926	926	0.14	0.14	1.87	0.013	954	969	511	2116	1088	1088	1072	1072	1044	1044
Skewness	1.08	1.08	0.65	0.62	0.63	10.3	0.65	0.63	0.5	1.73	0.44	0.44	0.48	0.48	0.38	0.38
Coefficient of Variatio	0.34	0.38	0.36	0.38	0.38	2.83	0.36	0.38	0.24	0.28	0.42	0.48	0.41	0.47	0.38	0.43
Count	146	146	146	146	146	146	146	146	146	146	146	146	146	146	146	146
NPR < 1.0 or NPR = 1																
1.0 < NPR < 2.0																
NPR > 2.0 or NPR =2.																
% NPR < 1.0 or NPR =																
% 1.0 < NPR < 2.0 of																
% NPR > 2.0 or NPR =																

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	NP	Available NP	Total C	Inorganic C	Inorganic CO_2	Excess C	Total CaNP	Inorganic CaNP	(Ca) CaNP	(Ca+Mg) CaNP	TNNP	Adjusted TNNP	SNNP	Adjusted SNNP	PNNP	Adjusted PNNP
	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(% Leco)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)
Method	OA-VOL08	Calculated	C-IR07	C-GAS05	C-GAS05	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL	1		0.01	0.05	0.2											
West Breccia Zone																
Maximum	88	78	1.09	1.03	3.8	1.03	90.8	86.4	195	336	83.4	73.4	84.1	74.1	87.8	77.8
Minimum	21	11	0.09	0.06	0.2	0	7.5	4.55	35	83.3	-0.31	-10.3	2.36	-7.64	11.2	1.17
Mean	54.9	44.9	0.55	0.52	1.89	0.041	45.8	43.1	87.1	165	42.1	32.1	44	34	49.3	39.3
Standard Deviation	16.2	16.2	0.25	0.25	0.92	0.15	21.1	20.9	34.2	56.6	19.8	19.8	19.5	19.5	18.2	18.2
10 Percentile	38.2	28.2	0.26	0.21	0.76	0	21.3	17.3	46.1	102	17.3	7.34	20.2	10.3	29.8	19.8
25 Percentile	42	32	0.39	0.34	1.25	0	32.5	28.4	64.4	133	29.4	19.4	30.1	20.1	36.7	26.7
Median	50	40	0.49	0.47	1.7	0.01	40.8	38.7	83.7	159	41.9	31.9	42.2	32.2	47.1	37.1
75 Percentile	66	56	0.72	0.71	2.6	0.03	60	59.1	104	181	53.2	43.2	56.9	46.9	63.2	53.2
90 Percentile	78	68	0.9	0.87	3.2	0.064	75.3	72.8	111	226	67.4	57.4	69.7	59.7	74.2	64.2
Interquartile Range (I	24	24	0.33	0.36	1.35	0.03	27.5	30.7	39.2	48.7	23.7	23.7	26.8	26.8	26.5	26.5
Variance	262	262	0.064	0.062	0.85	0.022	444	438	1167	3199	394	394	382	382	332	332
Skewness	0.26	0.26	0.27	0.25	0.25	6.52	0.27	0.25	1.19	1.09	-0.064	-0.064	0.1	0.1	0.3	0.3
Coefficient of Variatio	0.3	0.36	0.46	0.48	0.49	3.67	0.46	0.49	0.39	0.34	0.47	0.62	0.44	0.57	0.37	0.46
Count	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47
NPR < 1.0 or NPR = 1																
1.0 < NPR < 2.0																
NPR > 2.0 or NPR =2.																
% NPR < 1.0 or NPR =																
% 1.0 < NPR < 2.0 of																
% NPR > 2.0 or NPR =																
Paramount Zone																
Maximum	159	149	1.56	1.58	5.8	0.08	130	132	122	288	153	143	154	144	159	149
Minimum	30	20	0.3	0.31	1.2	0	25	27.3	41	76.4	9.25	-0.75	8	-2	10.3	0.25
Mean	65.7	55.7	0.77	0.77	2.82	0.01	63.9	64	74.8	152	54.4	44.4	55.2	45.2	60.5	50.5
Standard Deviation	23.8	23.8	0.34	0.34	1.23	0.019	28.5	28	24.6	59.4	25.6	25.6	25.6	25.6	25.8	25.8
10 Percentile	46	36	0.45	0.45	1.7	0	37.5	38.7	46.4	84.3	28.9	18.9	33.7	23.7	39.6	29.6
25 Percentile	50.5	40.5	0.52	0.51	1.9	0	43.3	43.2	53.4	100	39.1	29.1	40.1	30.1	46.3	36.3
Median	58	48	0.65	0.64	2.4	0	54.2	54.6	69.4	147	50	40	51.2	41.2	53.8	43.8
75 Percentile	80	70	0.98	0.98	3.6	0.01	81.7	81.9	92.1	189	64.6	54.6	66.7	56.7	70.7	60.7
90 Percentile	89	79	1.19	1.15	4.2	0.03	99.2	95.5	109	238	79.3	69.3	79.8	69.8	86.8	76.8
Interquartile Range (I	29.5	29.5	0.46	0.48	1.7	0.01	38.3	38.7	38.7	88.5	25.5	25.5	26.6	26.6	24.3	24.3
Variance	569	569	0.12	0.12	1.51	0.00038	814	783	603	3523	656	656	656	656	668	668
Skewness	2.04	2.04	1.01	1.04	1.06	2.37	1.01	1.06	0.44	0.52	1.86	1.86	1.83	1.83	1.75	1.75
Coefficient of Variatio	0.36	0.43	0.45	0.44	0.44	1.95	0.45	0.44	0.33	0.39	0.47	0.58	0.46	0.57	0.43	0.51
Count	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31
NPR < 1.0 or NPR = 1																
1.0 < NPR < 2.0																
NPR > 2.0 or NPR =2.																
% NPR < 1.0 or NPR =																
% 1.0 < NPR < 2.0 of																
% NPR > 2.0 or NPR =																

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	NP	Available NP	Total C	Inorganic C	Inorganic CO_2	Excess C	Total CaNP	Inorganic CaNP	(Ca) CaNP	(Ca+Mg) CaNP	TNNP	Adjusted TNNP	SNNP	Adjusted SNNP	PNNP	Adjusted PNNP
	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(% Leco)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)
Method	OA-VOL08	Calculated	C-IR07	C-GAS05	C-GAS05	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL	1		0.01	0.05	0.2											
Tailings																
Maximum	103	93	1.07	1.03	3.8	0.04	89.2	86.4	84.9	149	100	90.5	101	90.8	103	92.8
Minimum	67	57	0.54	0.5	1.8	0.01	45	40.9	67.2	124	60.8	50.8	61.7	51.7	66.8	56.8
Mean	85	75	0.81	0.78	2.87	0.03	67.8	65.2	74	138	80.3	70.3	81.2	71.2	84.8	74.8
Standard Deviation	18	18	0.27	0.27	1.01	0.017	22.1	22.9	9.54	12.5	19.9	19.9	19.6	19.6	18	18
10 Percentile	70.6	60.6	0.6	0.56	2.04	0.016	49.8	46.4	67.7	128	64.5	54.5	65.6	55.6	70.4	60.4
25 Percentile	76	66	0.68	0.66	2.4	0.025	57.1	54.6	68.5	133	70.2	60.2	71.5	61.5	75.8	65.8
Median	85	75	0.83	0.82	3	0.04	69.2	68.2	69.9	142	79.7	69.7	81.2	71.2	84.8	74.8
75 Percentile	94	84	0.95	0.92	3.4	0.04	79.2	77.3	77.4	145	90.1	80.1	91	81	93.8	83.8
90 Percentile	99.4	89.4	1.02	0.99	3.64	0.04	85.2	82.8	81.9	147	96.3	86.3	96.9	86.9	99.2	89.2
Interquartile Range (IC	18	18	0.26	0.27	1	0.015	22.1	22.7	8.87	12.1	19.9	19.9	19.6	19.6	18	18
Variance	324	324	0.07	0.071	1.01	0.0003	489	524	91.1	157	395	395	383	383	324	324
Skewness	0	0	-0.28	-0.61	-0.59	-1.73	-0.28	-0.59	1.57	-1.23	0.14	0.14	0	0	0	0
Coefficient of Variatior	0.21	0.24	0.33	0.34	0.35	0.58	0.33	0.35	0.13	0.09	0.25	0.28	0.24	0.27	0.21	0.24
Count	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
NPR < 1.0 or NPR = 1																
1.0 < NPR < 2.0																
NPR > 2.0 or NPR =2.																
% NPR < 1.0 or NPR =																
% 1.0 < NPR < 2.0 of T																
% NPR > 2.0 or NPR =																
High-Sulphide Histor																
Maximum	84	74	1.29	1.25	4.6	0.06	108	105	105	244	57.9	47.9	58.2	48.2	61.8	51.8
Minimum	23	13	0.16	0.17	0.6	0	13.3	13.6	21.2	44.5	-387	-397	-385	-395	-383	-393
Mean	47.2	37.2	0.59	0.56	2.05	0.035	49.2	46.6	47.4	101	-80.2	-90.2	-79.4	-89.4	-76.1	-86.1
Standard Deviation	19.6	19.6	0.32	0.32	1.16	0.019	27	26.4	31.1	69.1	151	151	151	151	152	152
10 Percentile	31.4	21.4	0.37	0.34	1.3	0.014	30.8	29.6	22.3	46.8	-273	-283	-272	-282	-270	-280
25 Percentile	35	25	0.48	0.43	1.6	0.028	39.6	36.4	23.3	49	-117	-127	-116	-126	-114	-124
Median	40	30	0.52	0.48	1.75	0.04	43.8	39.8	34.1	73.1	-19.9	-29.9	-19.1	-29.1	-18.3	-28.3
75 Percentile	59.8	49.8	0.6	0.57	2.12	0.043	49.6	48.3	65.4	136	15.5	5.53	16.2	6.22	21.5	11.5
90 Percentile	68.6	58.6	0.9	0.86	3.13	0.053	74.8	71.2	85.7	170	30	20	30.6	20.6	41.2	31.2
Interquartile Range (IC	24.8	24.8	0.12	0.14	0.52	0.015	10	11.9	42.1	87.2	132	132	132	132	136	136
Variance	386	386	0.1	0.099	1.34	0.00034	728	695	969	4770	22896	22896	22800	22800	23231	23231
Skewness	0.9	0.9	1.47	1.66	1.64	-0.81	1.47	1.64	1.04	1.47	-1.48	-1.48	-1.48	-1.48	-1.45	-1.45
Coefficient of Variatior	0.42	0.53	0.55	0.57	0.57	0.53	0.55	0.57	0.66	0.69	-1.89	-1.68	-1.9	-1.69	-2	-1.77
Count	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
NPR < 1.0 or NPR = 1																
1.0 < NPR < 2.0																
NPR > 2.0 or NPR =2.																
% NPR < 1.0 or NPR =																
% 1.0 < NPR < 2.0 of T																
% NPR > 2.0 or NPR =																

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	NP	Available NP	Total C	Inorganic C	Inorganic CO_2	Excess C	Total CaNP	Inorganic CaNP	(Ca) CaNP	(Ca+Mg) CaNP	TNNP	Adjusted TNNP	SNNP	Adjusted SNNP	PNNP	Adjusted PNNP
	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(% Leco)	(%)	(%)	(%)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)	(kg $CaCO_3$/t)
Method	OA-VOL08	Calculated	C-IR07	C-GAS05	C-GAS05	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL	1		0.01	0.05	0.2											

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

Data in blue indicates a calculated parameter.

Total CaNP = % C * 10 * 100.09 / 12.01
Inorganic CaNP = % CO_2 * 10 * 100.09 / 44.01
(Ca) CaNP = (Ca(ppm) * 100.09 / 40.08) / 1000
(Ca+Mg) CaNP = ((Ca(ppm) * 100.09 / 40.08) + (Mg(ppm) * 100.09 / 24.31)) / 1000
TNNP = NP - TAP
Adjusted TNNP = Available NP - TAP
SNNP = NP - SAP
Adjusted SNNP = Available NP - SAP
PNNP = NP - PAP
Adjusted PNNP = Available NP - PAP

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	TNPR	Adjusted TNPR	SNPR	Adjusted SNPR	PNPR	Adjusted PNPR	Fizz Rating	Comparison of Fizz Rating & NP
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Unity OA-VOL08	Calculated
MDL								
Main Zone								
14130	10	8.94	10	8.94	200	200	3	Disagree
14144	14.3	13	15.1	13.8	200	200	3	Agree
14148	38.9	36.6	45.2	42.5	200	200	3	Agree
14156	13.7	11.9	14.7	12.7	200	200	3	Disagree
14162	53.9	51.4	58.4	55.7	200	200	3	Agree
14169	6.83	5.76	6.99	5.9	200	200	3	Disagree
14232	19	16.9	20.2	18	200	200	3	Disagree
14250	19.9	18.2	19.9	18.2	200	200	3	Agree
14260	9.41	8.47	9.41	8.47	200	200	3	Agree
14276	8.85	6.96	10.7	8.46	200	200	2	Disagree
14295	8.07	7.35	8.2	7.47	18.3	16.6	3	Agree
14301	12.8	11.9	13.2	12.3	66.4	61.5	3	Agree
14323	15.6	13.4	16.8	14.5	200	200	2	Agree
14332	11.7	10.5	11.7	10.5	200	200	3	Disagree
14345	4.86	4.25	4.86	4.25	200	200	3	Disagree
14348	4.29	3.56	4.2	3.48	200	200	2	Agree
14797	50	46	56.5	52	200	200	3	Agree
14808	30.6	28.8	32.2	30.3	200	200	3	Agree
14816	9.25	8.56	9.25	8.56	80.8	74.8	3	Agree
14828	35.2	32.7	42.3	39.3	200	200	3	Agree
14844	11.4	9.9	12	10.4	200	200	3	Disagree
14680	14.8	13.4	15.6	14.1	200	200	3	Agree
14871	7.61	6.75	7.76	6.88	200	200	3	Disagree
14887	8.65	7.93	9.07	8.3	17.7	16.2	3	Agree
14689	2.49	2.02	2.46	1.99	3.54	2.87	2	Agree
14695	26.1	23.8	27.9	25.4	200	200	3	Agree
14742	14.1	12.5	14.1	12.5	200	200	3	Disagree
14666	9.4	8.4	9.7	8.67	18.8	16.8	3	Disagree
14685	2	1.82	1.99	1.81	2.65	2.41	3	Agree
14685B	1.67	1.51	1.69	1.52	2.23	2.01	3	Agree
14545	13	11.3	15	13.1	62.6	54.4	3	Disagree
14565	18.9	17.5	18.1	16.8	200	200	3	Agree
14571	2.34	2.03	2.36	2.05	5.17	4.49	3	Disagree
14578	1.95	1.78	1.95	1.78	2.34	2.13	3	Agree
14578B	2.02	1.86	2.04	1.88	2.48	2.28	3	Agree
14598	19	16.5	19	16.5	46.7	40.7	3	Disagree
14893	32.3	29.4	44.4	40.4	200	200	3	Agree
14899	130	114	130	114	200	200	3	Disagree
14908	30	26	34.3	29.7	200	200	3	Disagree
14917	11.1	9.43	12.7	10.8	200	200	3	Disagree
14925	18.7	16.5	20.7	18.2	200	200	3	Disagree
14998	25.4	22.9	27.5	24.8	200	200	3	Agree
15862	52	48	60.5	55.9	200	200	3	Agree
15870	37.2	34.7	48.4	45.2	200	200	3	Agree
15879	31.5	28.8	39.3	35.9	200	200	3	Agree

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	TNPR	Adjusted TNPR	SNPR	Adjusted SNPR	PNPR	Adjusted PNPR	Fizz Rating	Comparison of Fizz Rating & NP
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Unity OA-VOL08	Calculated
MDL								
15887	9.81	8.77	10.3	9.23	200	200	3	Disagree
15891	29.3	27	39.5	36.4	200	200	3	Agree
15908	17.6	16.1	18.6	17	200	200	3	Agree
15911	32.7	29.2	39.5	35.2	200	200	3	Disagree
125285	5.4	4.4	5.76	4.69	200	200	2	Agree
125288	23.7	20.5	27.3	23.6	37.8	32.7	2	Agree
125293	9.45	7.92	9.92	8.32	200	200	2	Agree
125305	18.7	16	18.7	16	200	200	2	Agree
125311	31.5	26.1	37.8	31.4	200	200	2	Agree
125703	27.5	24.3	30.3	26.8	200	200	2	Agree
125728	12.6	10.9	13.3	11.6	200	200	2	Agree
125755	2.71	2.17	2.91	2.33	8.2	6.56	2	Agree
125772	13.1	11.6	14	12.4	200	200	2	Agree
125795	41.3	38.4	56.8	52.8	200	200	3	Agree
125422	13.1	11.6	13.1	11.6	200	200	2	Agree
125435	17.2	15.2	18.9	16.7	200	200	2	Agree
125452	5.58	4.9	5.58	4.9	200	200	2	Agree
125476	3.12	2.71	3.33	2.89	6.66	5.79	2	Agree
125490	6.77	5.85	7.18	6.21	20.7	17.9	2	Agree
126192	13.5	11.8	14.2	12.4	200	200	2	Agree
126206	10.3	8.87	11.1	9.54	236	202	2	Agree
126225	6.86	5.94	7.26	6.3	77.7	67.3	2	Agree
126244	11.1	9.85	11.5	10.2	200	200	2	Agree
126266	13.5	11.8	14.2	12.4	200	200	2	Agree
126279	11	10.2	11.3	10.4	31.1	28.8	3	Agree
126288	10.6	9.69	11	10.1	200	200	3	Agree
126297	10.1	9.47	10.3	9.65	21.5	20.1	3	Agree
126314	2.78	2.55	2.8	2.56	5.95	5.45	3	Agree
126329	17.6	16.3	20.6	19	200	200	3	Agree
126337	7.13	6.57	7.3	6.73	195	180	3	Agree
126351	29.5	27.2	32.6	30.1	200	200	3	Agree
126427	4.77	4.49	4.81	4.52	5.05	4.74	3	Agree
126430	20.7	19.2	21.7	20.1	23.9	22.2	3	Agree
126434	36.9	34	40.3	37.1	47.2	43.5	3	Agree
126443	2.56	2.37	2.57	2.38	2.66	2.46	3	Agree
126449	75.2	59.2	50.1	39.5	84.9	66.8	2	Disagree
126464	6.55	5.8	6.73	5.96	13.4	11.8	2	Agree
126492	13.2	11.8	14.3	12.7	200	200	2	Agree
145655	4.17	3.68	4.49	3.97	5.84	5.16	2	Agree
145669	3	2.66	3.14	2.79	4.21	3.73	2	Agree
145685	11.4	10	12.7	11.2	200	200	2	Agree
145694	22.2	20.3	25.2	23	200	200	3	Agree
145708	9.85	8.62	10.3	9.04	53.1	46.5	2	Agree
145723	1.37	1.18	1.41	1.21	2.1	1.8	2	Agree
146798	13.7	12.2	14.6	13	200	200	2	Agree
146824	15.2	13.4	16.9	14.8	200	200	2	Agree

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	TNPR	Adjusted TNPR	SNPR	Adjusted SNPR	PNPR	Adjusted PNPR	Fizz Rating	Comparison of Fizz Rating & NP
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Unity OA-VOL08	Calculated
MDL								
146831	7.56	6.67	7.77	6.86	200	200	2	Agree
146843								
146861	11.8	9.35	14	11.1	200	200	2	Disagree
146868	4.14	3.51	4.55	3.86	14.1	11.9	2	Agree
126352	3.41	2.88	3.52	2.97	30.2	25.5	2	Agree
126358	6.79	5.82	7.03	6.02	200	200	2	Agree
126374	12.8	10.9	13.6	11.6	200	200	2	Agree
126384	18	15.1	19.8	16.6	200	200	2	Agree
126391	12.8	11	13.8	11.9	200	200	2	Agree
146172	18.5	17.2	20.2	18.8	200	200	3	Agree
146182	11.7	9.6	13.5	11.1	200	200	2	Agree
146203	10.8	9.07	12.2	10.2	200	200	2	Agree
146214	8.09	7.2	13.2	11.8	200	200	2	Agree
146221	3.24	2.84	3.48	3.06	18.9	16.6	2	Agree
146238	13	10.6	17	13.8	200	200	2	Agree
147034	4.74	4.12	4.83	4.2	200	200	2	Agree
147038	7.04	6.13	8.41	7.32	200	200	2	Agree
147051	5.92	4.95	6.53	5.46	33.8	28.3	2	Agree
147070	3.39	2.76	3.49	2.84	3.71	3.02	2	Agree
147087	0.401	0.306	0.413	0.315	0.416	0.317	2	Disagree
147097	6.21	5.74	6.65	6.15	7.55	6.97	3	Agree
145508	45.6	37.6	60.8	50.1	200	200	2	Agree
145527	4.87	4.2	5.08	4.39	9.44	8.15	2	Agree
145543	13.6	10.9	14.8	11.9	200	200	2	Agree
145562	28.1	24.5	31.6	27.6	200	200	2	Agree
145576	2.69	2.23	2.81	2.32	5.23	4.33	2	Agree
145601	4.54	3.9	4.76	4.09	10.9	9.35	2	Agree
146297	7.86	6.95	8.5	7.51	200	200	2	Agree
146314	15.4	13.2	16.5	14.2	200	200	2	Agree
146335	22.2	19.7	32	28.4	200	200	2	Agree
146352	36.8	31.5	50.5	43.2	200	200	2	Agree
146368	13.3	11.6	29.5	25.7	200	200	2	Agree
146390	14.2	12.2	15.1	12.9	200	200	2	Agree
146508	47.5	42.1	47.5	42.1	200	200	2	Agree
146526	2.59	2.12	29.3	24	200	200	2	Agree
146544	12	10.7	28.9	25.7	200	200	2	Agree
146565	25.6	22.7	35.2	31.2	200	200	2	Agree
146589	21.9	19.4	25.5	22.6	200	200	2	Agree
146613	7.64	7.05	7.85	7.24	21.1	19.4	3	Agree
146627	32.7	29.2	41.1	36.6	200	200	2	Agree
146637	6.05	5.36	6.47	5.73	44.2	39.1	2	Agree
146649	8.8	7.66	10.4	9.05	18.9	16.4	2	Agree
146657	10.1	8.42	10.1	8.42	200	200	2	Agree
146676	13.4	11.9	15.2	13.4	200	200	2	Agree
125188	9.97	8.74	11.6	10.2	200	200	2	Agree
125198	10.9	9.45	11.8	10.2	200	200	2	Agree

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	TNPR	Adjusted TNPR	SNPR	Adjusted SNPR	PNPR	Adjusted PNPR	Fizz Rating	Comparison of Fizz Rating & NP
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Unity OA-VOL08	Calculated
MDL								
125207	27.1	24.1	29.8	26.6	200	200	2	Agree
125228	14.9	12.8	16	13.7	200	200	2	Agree
125244	12.2	10	13.4	11.1	200	200	2	Agree
125257	27.7	22.4	27.7	22.4	40.8	32.9	2	Agree
125278	56	40	112	80	200	200	2	Disagree
125596	24.8	22.1	22.9	20.4	200	200	2	Agree
125610	40.5	35.2	46	39.9	200	200	2	Agree
125626								
125641	27.5	24.3	30.6	27	200	200	2	Agree
125669	2.66	2.34	2.73	2.4	4.28	3.77	2	Agree
125690	19.2	16	26	21.7	368	306	2	Agree
West Breccia Zone								
14018	1.68	1.28	1.75	1.33	2.13	1.62	2	Disagree
14021	3.3	2.79	3.39	2.86	5.12	4.32	2	Agree
14036	1.07	0.849	1.08	0.859	1.3	1.03	2	Disagree
14043	4.92	3.69	5.15	3.86	14.3	10.7	2	Disagree
14060	1	0.757	2.12	1.6	3.87	2.93	2	Disagree
14067	3.92	3.12	3.82	3.04	10.5	8.34	2	Disagree
14076	2.74	2.33	2.78	2.36	3.45	2.93	2	Agree
14083	1.62	1.4	1.65	1.42	1.83	1.59	2	Agree
14099	7.34	6.4	7.95	6.93	13.8	12.1	2	Agree
14103	3.94	3.48	10.3	9.1	200	200	3	Disagree
125046	19.2	16.3	21.1	17.9	200	200	2	Agree
125068	5.17	4.35	5.6	4.71	200	200	2	Agree
125073	3.63	3.09	4.14	3.53	200	200	2	Agree
125079	0.992	0.744	1.06	0.797	200	200	2	Disagree
125084	2.2	1.68	2.54	1.94	200	200	2	Disagree
125127	19.2	15.2	25.6	20.3	200	200	2	Disagree
125129	5.89	4.61	7.23	5.65	200	200	2	Disagree
125134	1.84	1.3	2.06	1.46	200	200	2	Disagree
125142	6.28	5.05	7.05	5.66	200	200	2	Agree
125149	19.4	17	23	20.1	200	200	2	Agree
125154	28	24	34	29.2	200	200	2	Agree
125165	8.08	6.4	9.04	7.15	200	200	2	Disagree
125176	8	6.67	11.1	9.21	200	200	2	Agree
146112	11.5	8.8	15.3	11.7	200	200	2	Disagree
146115	9.85	7.38	13.4	10.1	14.9	11.2	2	Disagree
146124	18.8	15.3	28.3	22.9	200	200	2	Agree
146127	1.87	1.57	1.95	1.64	2.02	1.69	2	Agree
146135	29.6	21.6	39.5	28.8	200	200	2	Disagree
146149	22.4	17.8	39.2	31.2	174	138	2	Disagree
146161	40	32	80	64	200	200	2	Agree
146164	48	32	96	64	200	200	2	Disagree
145951	15.6	13.9	18.3	16.2	200	200	2	Agree
145956	13	11.3	15.4	13.4	200	200	2	Agree
145974	99.2	83.2	99.2	83.2	200	200	2	Agree

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	TNPR	Adjusted TNPR	SNPR	Adjusted SNPR	PNPR	Adjusted PNPR	Fizz Rating	Comparison of Fizz Rating & NP
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Unity OA-VOL08	Calculated
MDL								
145982	54.4	48	90.7	80	117	104	2	Agree
145992	7.43	6.29	8.53	7.22	44.6	37.8	2	Agree
145999	15.1	12.8	26.4	22.4	200	200	2	Agree
145834	31.2	23.2	31.2	23.2	200	200	2	Disagree
145842	44.8	34.1	67.2	51.2	200	200	2	Disagree
145852	6.11	3.2	7.47	3.91	200	200	2	Disagree
145857	96	64	96	64	200	200	2	Disagree
145871	11.6	9.6	37.1	30.7	215	178	2	Agree
145608	1.86	1.46	1.9	1.48	2.09	1.63	2	Disagree
145614	2.69	2.11	2.77	2.18	4.16	3.27	2	Disagree
145628	3.16	2.75	5.57	4.86	7.31	6.37	2	Agree
145640	2.65	2.22	2.96	2.49	4.17	3.49	2	Agree
145646	2.58	2.02	3.19	2.5	4.89	3.83	2	Disagree
Paramount Zone								
125965	4.75	3.84	4.99	4.03	200	200	2	Agree
125974	1.19	0.985	1.16	0.96	1.21	1.01	2	Agree
125983	8.43	7.36	9.11	7.96	28.4	24.8	2	Agree
125988	52.3	41.6	52.3	41.6	86.7	69	2	Disagree
126007	14.1	11.9	16.2	13.8	200	200	2	Agree
126031	11.1	8.62	12	9.33	200	200	2	Disagree
126040	2.23	1.75	2.29	1.79	4.35	3.41	2	Disagree
126054	28.3	26.5	31.8	29.8	200	200	3	Agree
126067	9.19	8.15	9.63	8.55	84.4	74.9	2	Agree
126081	1.85	1.56	2.15	1.81	6.59	5.54	2	Agree
126110	34.7	29.3	41.6	35.2	64	54.1	2	Agree
126118	3.57	3.16	4.41	3.9	78.9	69.8	2	Agree
125904	15.3	13.5	16.2	14.3	200	200	2	Agree
125919	3.39	2.76	3.57	2.91	200	200	2	Agree
125928	20.6	17.1	23.2	19.2	200	200	2	Agree
125933	142	126	285	253	200	200	2	Agree
125944	16.3	13.6	16.3	13.6	23.9	20	2	Agree
125952	2.47	2.16	2.49	2.18	2.55	2.24	2	Agree
125963	6.47	5.73	7.33	6.48	200	200	2	Agree
126120	16	10.7	19.2	12.8	200	200	2	Disagree
126131	56.5	45.9	84.8	68.8	200	200	2	Agree
126142	30.1	23.7	37.6	29.6	200	200	2	Disagree
126154	18.5	16	21.8	18.9	200	200	2	Agree
126171	2.25	2	2.32	2.06	2.76	2.45	2	Agree
126181	6.14	4.86	7.62	6.03	8.97	7.1	2	Disagree
125806	3.47	2.8	3.62	2.92	4.18	3.38	2	Agree
125816	71.5	60.8	71.5	60.8	141	120	2	Agree
125833	5.45	4.27	5.45	4.27	200	200	2	Disagree
125861	4.33	3.39	5.81	4.55	200	200	2	Disagree
125875	7.47	6.13	8.96	7.36	200	200	2	Agree
125897	21.6	17.6	27.1	22.1	200	200	2	Agree

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	TNPR	Adjusted TNPR	SNPR	Adjusted SNPR	PNPR	Adjusted PNPR	Fizz Rating	Comparison of Fizz Rating & NP
							Unity	
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	OA-VOL08	Calculated
MDL								
Tailings								
LIARD ZONE	41.2	37.2	47.1	42.5	200	200	3	Agree
PARAMOUNT	16	14.1	22.7	20	200	200	3	Disagree
WEST BRECCIA	10.7	9.12	12.6	10.7	200	200	3	Disagree
High-Sulphide Histor								
T112 (171' - 172')	0.208	0.173	0.209	0.174	0.21	0.174	2	Agree
T113 (81' - 82')	0.846	0.478	0.887	0.501	0.933	0.527	2	Disagree
T113 (983' - 985')	1.27	1.12	1.29	1.13	1.63	1.43	2	Agree
T140 (30' - 31')	15.3	12.8	16.5	13.9	200	200	2	Agree
T166 (389' - 390')	1.58	1.19	1.63	1.22	1.8	1.35	2	Disagree
T185 (116' - 117')	0.496	0.354	0.498	0.356	0.501	0.358	2	Disagree
T207 (261.5' - 262')	0.33	0.247	0.331	0.249	0.337	0.253	2	Disagree
T207 (269' - 271')	0.083	0.0593	0.0833	0.0595	0.0836	0.0597	2	Disagree

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	TNPR	Adjusted TNPR	SNPR	Adjusted SNPR	PNPR	Adjusted PNPR	Fizz Rating	Comparison of Fizz Rating & NP
							Unity	
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	OA-VOL08	Calculated
MDL								
All Data								
Maximum	142	126	285	253	368	306		
Minimum	0.083	0.059	0.083	0.06	0.084	0.06		
Mean	16.6	14.2	20.3	17.4	136	134		
Standard Deviation	19.3	16.4	27.3	23.3	88.9	88.9		
10 Percentile	2.21	1.84	2.3	1.9	3.61	2.93		
25 Percentile	4.76	3.87	5.3	4.33	20.9	18.6		
Median	11.1	9.6	12.7	10.8	200	200		
75 Percentile	19.6	17.4	26.2	22.4	200	200		
90 Percentile	36.9	32	44.9	39.7	200	200		
Interquartile Range (IC	14.9	13.5	20.9	18.1	179	181		
Variance	372	268	745	541	7906	7912		
Skewness	3.16	3.23	4.92	5.3	-0.59	-0.62		
Coefficient of Variatior	1.16	1.15	1.34	1.34	0.65	0.66		
Count	235	235	235	235	235	235		
NPR < 1.0 or NPR = 1	8	10	6	9	6	6		
1.0 < NPR < 2.0	13	15	13	17	5	9		
NPR > 2.0 or NPR =2.	214	210	216	209	224	220		
% NPR < 1.0 or NPR =	3.40	4.26	2.55	3.83	2.55	2.55		
% 1.0 < NPR < 2.0 of	5.53	6.38	5.53	7.23	2.13	3.83		
% NPR > 2.0 or NPR =	91.06	89.36	91.91	88.94	95.32	93.62		
Main Zone								
Maximum	130	114	130	114	368	306		
Minimum	0.4	0.31	0.41	0.32	0.42	0.32		
Mean	16.8	14.8	19.3	16.9	146	144		
Standard Deviation	16.1	14.1	18.8	16.1	85.7	85.6		
10 Percentile	3.06	2.68	3.4	2.86	5.9	5.3		
25 Percentile	6.9	5.99	7.42	6.76	41.6	34.4		
Median	12.7	10.8	13.7	11.9	200	200		
75 Percentile	21.6	19.3	27	22.9	200	200		
90 Percentile	34	30.4	41.7	38.2	200	200		
Interquartile Range (IC	14.7	13.4	19.6	16.1	158	166		
Variance	260	199	352	260	7351	7322		
Skewness	3.18	3.11	2.7	2.46	-0.73	-0.81		
Coefficient of Variatior	0.96	0.96	0.97	0.95	0.59	0.59		
Count	146	146	146	146	146	146		
NPR < 1.0 or NPR = 1	1	1	1	1	1	1		
1.0 < NPR < 2.0	3	5	4	6	0	1		
NPR > 2.0 or NPR =2.	142	140	141	139	145	144		
% NPR < 1.0 or NPR =	0.68	0.68	0.68	0.68	0.68	0.68		
% 1.0 < NPR < 2.0 of	2.05	3.42	2.74	4.11	0.00	0.68		
% NPR > 2.0 or NPR =	97.26	95.89	96.58	95.21	99.32	98.63		

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	TNPR	Adjusted TNPR	SNPR	Adjusted SNPR	PNPR	Adjusted PNPR	Fizz Rating	Comparison of Fizz Rating & NP
							Unity	
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	OA-VOL08	Calculated
MDL								
West Breccia Zone								
Maximum	99.2	83.2	99.2	83.2	215	200		
Minimum	0.99	0.74	1.06	0.8	1.3	1.03		
Mean	15.9	12.5	21.7	17.1	129	126		
Standard Deviation	21.9	16.9	28.3	21.9	92.7	92.6		
10 Percentile	1.78	1.36	1.93	1.47	2.92	2.43		
25 Percentile	2.72	2.28	3.08	2.5	8.9	7.36		
Median	7.34	6.29	8.53	7.15	200	200		
75 Percentile	19.2	15.8	27.4	22.6	200	200		
90 Percentile	41.9	32	72.3	56.3	200	200		
Interquartile Range (I	16.5	13.5	24.3	20.2	191	193		
Variance	481	285	799	478	8592	8568		
Skewness	2.53	2.53	1.78	1.79	-0.56	-0.53		
Coefficient of Variatio	1.38	1.35	1.3	1.28	0.72	0.73		
Count	47	47	47	47	47	47		
NPR < 1.0 or NPR = 1	2	3	0	2	0	0		
1.0 < NPR < 2.0	6	6	6	7	2	5		
NPR > 2.0 or NPR =2.	39	38	41	38	45	42		
% NPR < 1.0 or NPR =	4.26	6.38	0.00	4.26	0.00	0.00		
% 1.0 < NPR < 2.0 of	12.77	12.77	12.77	14.89	4.26	10.64		
% NPR > 2.0 or NPR =	82.98	80.85	87.23	80.85	95.74	89.36		
Paramount Zone								
Maximum	142	126	285	253	200	200		
Minimum	1.19	0.98	1.16	0.96	1.21	1.01		
Mean	20.1	16.9	27	22.9	127	124		
Standard Deviation	28.5	24.9	52.1	45.9	86.8	88.2		
10 Percentile	2.25	2	2.32	2.06	4.18	3.38		
25 Percentile	3.95	3.28	4.7	3.96	26.2	22.4		
Median	9.19	8.15	9.63	8.55	200	200		
75 Percentile	21.1	17.4	25.2	20.6	200	200		
90 Percentile	52.3	41.6	52.3	41.6	200	200		
Interquartile Range (I	17.2	14.1	20.4	16.7	174	178		
Variance	813	618	2712	2110	7539	7788		
Skewness	3.03	3.22	4.36	4.49	-0.48	-0.41		
Coefficient of Variatio	1.42	1.47	1.93	2	0.68	0.71		
Count	31	31	31	31	31	31		
NPR < 1.0 or NPR = 1	0	1	0	1	0	0		
1.0 < NPR < 2.0	2	2	1	2	1	1		
NPR > 2.0 or NPR =2.	29	28	30	28	30	30		
% NPR < 1.0 or NPR =	0.00	3.23	0.00	3.23	0.00	0.00		
% 1.0 < NPR < 2.0 of	6.45	6.45	3.23	6.45	3.23	3.23		
% NPR > 2.0 or NPR =	93.55	90.32	96.77	90.32	96.77	96.77		

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	TNPR	Adjusted TNPR	SNPR	Adjusted SNPR	PNPR	Adjusted PNPR	Fizz Rating	Comparison of Fizz Rating & NP
							Unity	
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	OA-VOL08	Calculated
MDL								
Tailings								
Maximum	41.2	37.2	47.1	42.5	200	200		
Minimum	10.7	9.12	12.6	10.7	200	200		
Mean	22.6	20.1	27.5	24.4	200	200		
Standard Deviation	16.3	15	17.7	16.4	0	0		
10 Percentile	11.8	10.1	14.6	12.6	200	200		
25 Percentile	13.4	11.6	17.6	15.4	200	200		
Median	16	14.1	22.7	20	200	200		
75 Percentile	28.6	25.6	34.9	31.2	200	200		
90 Percentile	36.2	32.6	42.2	38	200	200		
Interquartile Range (I	15.3	14	17.2	15.9	0	0		
Variance	266	224	315	267	0	0		
Skewness	1.53	1.52	1.12	1.12	NA	NA		
Coefficient of Variatio	0.72	0.74	0.65	0.67	0	0		
Count	3	3	3	3	3	3		
NPR < 1.0 or NPR = 1	0	0	0	0	0	0		
1.0 < NPR < 2.0	0	0	0	0	0	0		
NPR > 2.0 or NPR =2.	3	3	3	3	3	3		
% NPR < 1.0 or NPR =	0.00	0.00	0.00	0.00	0.00	0.00		
% 1.0 < NPR < 2.0 of	0.00	0.00	0.00	0.00	0.00	0.00		
% NPR > 2.0 or NPR =	100.00	100.00	100.00	100.00	100.00	100.00		
High-Sulphide Histor								
Maximum	15.3	12.8	16.5	13.9	200	200		
Minimum	0.083	0.059	0.083	0.06	0.084	0.06		
Mean	2.51	2.05	2.68	2.2	25.7	25.5		
Standard Deviation	5.19	4.36	5.61	4.75	70.4	70.5		
10 Percentile	0.17	0.14	0.17	0.14	0.17	0.14		
25 Percentile	0.3	0.23	0.3	0.23	0.31	0.23		
Median	0.67	0.42	0.69	0.43	0.72	0.44		
75 Percentile	1.35	1.14	1.38	1.15	1.67	1.37		
90 Percentile	5.7	4.67	6.09	5.02	61.3	61		
Interquartile Range (I	1.05	0.91	1.07	0.92	1.37	1.14		
Variance	27	19	31.5	22.5	4961	4971		
Skewness	2.77	2.78	2.78	2.78	2.83	2.83		
Coefficient of Variatio	2.07	2.13	2.09	2.16	2.74	2.76		
Count	8	8	8	8	8	8		
NPR < 1.0 or NPR = 1	5	5	5	5	5	5		
1.0 < NPR < 2.0	2	2	2	2	2	2		
NPR > 2.0 or NPR =2.	1	1	1	1	1	1		
% NPR < 1.0 or NPR =	62.50	62.50	62.50	62.50	62.50	62.50		
% 1.0 < NPR < 2.0 of	25.00	25.00	25.00	25.00	25.00	25.00		
% NPR > 2.0 or NPR =	12.50	12.50	12.50	12.50	12.50	12.50		

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ABA Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	TNPR	Adjusted TNPR	SNPR	Adjusted SNPR	PNPR	Adjusted PNPR	Fizz Rating	Comparison of Fizz Rating & NP
							Unity	
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	OA-VOL08	Calculated
MDL								

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and w

Data in blue indicates a calculated parameter.

TNPR = NP / TAP
Note: If % S(Total) < 0.01 then TNPR = 200
Note: If % S(Total) > 0.01 and NP < = 0 then TNPR = 0.001
Adjusted TNPR = UNP / TAP
Note: If % S(Total) < 0.01 then Adjusted TNPR = 200
Note: If % S(Total) > 0.01 and Available NP < = 0 then Adjusted TNPR = 0.001
SNPR = NP / SAP
Note: If % S(Sulphide + del) < 0.01 then SNPR = 200
'Note: If % S(Sulphide + del) > 0.01 and NP < = 0 then SNPR = 0.001
Adjusted SNPR = UNP / SAP
Note: If % S(Sulphide + del) < 0.01 then Adjusted SNPR = 200
Note: If % S(Sulphide + del) > 0.01 and Available NP < = 0 then Adjusted SNPR = 0
PNPR = NP / PAP
Note: If % S(Pyrite, Calc) < 0.01 then PNPR = 200
Note: If % S(Pyrite, Calc) > 0.01 and NP < = 0 then PNPR = 0.001
Adjusted PNPR = UNP / TAP
Note: If % S(Pyrite, Calc) < 0.005 then Adjusted PNPR = 200
Note: If % S(Pyrite, Calc) > 0.005 and Available NP < = 0 then Adjusted PNPR = 0.

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Calculated Mineralogy**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Calculated S (Pyrite) FeS_2 (%)	Calculated S (Chalcopyrite) $CuFeS_2 + CuS_2$ (%)	Calculated S (Arsenopyrite) FeAsS + AsS (%)	Calculated S (Galena) PbS (%)	Calculated S (Cinnibar) HgS (%)	Calculated S (Molybdenite) MoS_2 (%)	Calculated S (Pentlandite) ~NiS (%)	Calculated S (Sphalerite) ZnS (%)
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL								
Main Zone								
14130	-0.276	0.559	0.00009	0.00006	0.00000032	0.0054	0.00023	0.0013
14144	-0.105	0.344	0.00022	0.00007	0.00000016	0.0048	0.00023	0.0023
14148	-0.190	0.291	0.00011	0.00005	0.00000032	0.0171	0.00031	0.0020
14156	-0.060	0.211	0.00005	0.00004	0.00000008	0.0052	0.00045	0.0018
14162	-0.020	0.103	0.00009	0.00008	0.00000008	0.0319	0.00194	0.0034
14169	-0.106	0.386	0.00008	0.00011	0.00000032	0.0118	0.00033	0.0012
14232	-0.207	0.340	0.00015	0.00004	0.00000016	0.0065	0.00015	0.0011
14250	-0.157	0.320	0.00015	0.00005	0.00000016	0.0249	0.00014	0.0019
14260	-0.167	0.493	0.00011	0.00006	0.00000016	0.0115	0.00016	0.0018
14276	-0.018	0.151	0.00032	0.00010	0.00000008	0.0015	0.00009	0.0056
14295	0.195	0.235	0.00016	0.00007	0.00000032	0.0008	0.00025	0.0017
14301	0.066	0.246	0.00016	0.00006	0.00000016	0.0143	0.00023	0.0019
14323	-0.095	0.227	0.00014	0.00004	0.00000008	0.0045	0.00012	0.0015
14332	-0.099	0.351	0.00009	0.00004	0.00000016	0.0068	0.00014	0.0016
14345	-0.111	0.613	0.00009	0.00004	0.00000008	0.0167	0.00017	0.0014
14348	-0.059	0.495	0.00010	0.00004	0.00000016	0.0114	0.00017	0.0020
14797	-0.123	0.177	0.00011	0.00005	0.00000016	0.0141	0.00023	0.0021
14808	-0.137	0.267	0.00000	0.00012	0.00000096	0.0387	0.00026	0.0017
14816	0.053	0.401	0.00008	0.00004	0.00000032	0.0035	0.00029	0.0025
14828	-0.235	0.329	0.00010	0.00009	0.00000048	0.0122	0.00022	0.0016
14844	-0.114	0.302	0.00016	0.00004	0.00000032	0.0085	0.00130	0.0020
14680	-0.226	0.399	0.00008	0.00008	0.00000032	0.0333	0.00031	0.0019
14871	-0.048	0.392	0.00010	0.00004	0.00000016	0.0160	0.00041	0.0022
14887	0.216	0.201	0.00012	0.00004	0.00000016	0.0006	0.00059	0.0020
14689	0.479	0.204	0.00006	0.00002	0.00000008	0.0056	0.00036	0.0008
14695	-0.066	0.152	0.00000	0.00005	0.00000016	0.0427	0.00042	0.0025
14742	-0.070	0.212	0.00002	0.00032	0.00000016	0.0441	0.00090	0.0027
14666	0.160	0.145	0.00021	0.00003	0.00000008	0.0019	0.00086	0.0019
14685	1.352	0.437	0.00028	0.00004	0.00000064	0.0080	0.00051	0.0022
14685B	1.467	0.462	0.00025	0.00004	0.00000064	0.0052	0.00044	0.0023
14545	0.039	0.122	0.00015	0.00004	0.00000008	0.0009	0.00007	0.0013
14565	-0.032	0.270	0.00013	0.00004	0.00000008	0.0008	0.00009	0.0008
14571	0.471	0.551	0.00014	0.00006	0.00000016	0.0067	0.00026	0.0017
14578	1.516	0.301	0.00022	0.00004	0.00000016	0.0018	0.00037	0.0010
14578B	1.575	0.331	0.00019	0.00004	0.00000016	0.0021	0.00032	0.0010
14598	0.053	0.071	0.00012	0.00004	0.00000008	0.0036	0.00022	0.0024
14893	-0.095	0.165	0.00019	0.00005	0.00000016	0.0067	0.00110	0.0025
14899	-0.027	0.041	0.00035	0.00005	0.00000016	0.0013	0.00123	0.0026
14908	-0.055	0.115	0.00027	0.00004	0.00000008	0.0068	0.00104	0.0021
14917	-0.222	0.384	0.00007	0.00006	0.00000016	0.0011	0.00047	0.0022
14925	-0.042	0.163	0.00015	0.00004	0.00000016	0.0018	0.00089	0.0026
14998	-0.069	0.182	0.00015	0.00004	0.00000016	0.0043	0.00012	0.0021
15862	-0.058	0.119	0.00009	0.00004	0.00000016	0.0049	0.00024	0.0025
15870	-0.109	0.204	0.00011	0.00005	0.00000008	0.0012	0.00069	0.0027
15879	-0.126	0.217	0.00010	0.00006	0.00000016	0.0013	0.00085	0.0032

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Calculated Mineralogy**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Calculated S (Pyrite) FeS_2	Calculated S (Chalcopyrite) $CuFeS_2$ + CuS_2	Calculated S (Arsenopyrite) FeAsS + AsS	Calculated S (Galena) PbS	Calculated S (Cinnibar) HgS	Calculated S (Molybdenite) MoS_2	Calculated S (Pentlandite) ~NiS	Calculated S (Sphalerite) ZnS
	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL								
15887	-0.231	0.512	0.00009	0.00005	0.00000016	0.0110	0.00064	0.0021
15891	-0.154	0.247	0.00007	0.00006	0.00000016	0.0069	0.00060	0.0026
15908	-0.245	0.430	0.00006	0.00004	0.00000048	0.0207	0.00070	0.0022
15911	-0.123	0.184	0.00009	0.00004	0.00000032	0.0103	0.00098	0.0025
125285	-0.320	0.616	0.00009	0.00005	0.00000032	0.0011	0.00046	0.0024
125288	0.063	0.010	0.00020	0.00007	0.00000016	0.0001	0.00975	0.0037
125293	-0.393	0.574	0.00010	0.00004	0.00000032	0.0147	0.00129	0.0030
125305	-0.239	0.353	0.00011	0.00005	0.00000032	0.0038	0.00046	0.0020
125311	-0.111	0.158	0.00010	0.00005	0.00000016	0.0015	0.00026	0.0016
125703	-0.070	0.142	0.00009	0.00004	0.00000016	0.0166	0.00023	0.0023
125728	-0.079	0.245	0.00015	0.00006	0.00000016	0.0093	0.00097	0.0030
125755	0.195	0.318	0.00003	0.00004	0.00000016	0.0355	0.00032	0.0007
125772	-0.094	0.258	0.00012	0.00005	0.00000016	0.0299	0.00078	0.0023
125795	-0.059	0.135	0.00014	0.00004	0.00000016	0.0012	0.00075	0.0020
125422	-0.006	0.213	0.00011	0.00005	0.00000016	0.0010	0.00013	0.0021
125435	-0.060	0.189	0.00013	0.00004	0.00000016	0.0135	0.00017	0.0021
125452	-0.260	0.707	0.00011	0.00007	0.00000048	0.0210	0.00022	0.0012
125476	0.365	0.357	0.00020	0.00003	0.00000016	0.0075	0.00035	0.0004
125490	0.115	0.213	0.00014	0.00004	0.00000016	0.0004	0.00027	0.0014
126192	-0.057	0.232	0.00020	0.00004	0.00000016	0.0033	0.00012	0.0019
126206	0.010	0.185	0.00017	0.00003	0.00000016	0.0083	0.00017	0.0014
126225	0.031	0.279	0.00012	0.00003	0.00000016	0.0188	0.00014	0.0016
126244	-0.030	0.259	0.00012	0.00003	0.00000016	0.0197	0.00010	0.0020
126266	-0.025	0.195	0.00011	0.00003	0.00000008	0.0083	0.00011	0.0018
126279	0.138	0.228	0.00017	0.00002	0.00000016	0.0127	0.00016	0.0016
126288	0.000	0.337	0.00008	0.00003	0.00000016	0.0169	0.00010	0.0014
126297	0.240	0.249	0.00019	0.00004	0.00000016	0.0077	0.00049	0.0031
126314	0.640	0.711	0.00015	0.00003	0.00000016	0.0070	0.00025	0.0020
126329	-0.113	0.312	0.00007	0.00003	0.00000016	0.0039	0.00023	0.0020
126337	0.021	0.517	0.00014	0.00004	0.00000016	0.0160	0.00030	0.0022
126351	-0.083	0.203	0.00019	0.00004	0.00000016	0.0047	0.00026	0.0013
126427	1.059	0.047	0.00059	0.00005	0.00000016	0.0002	0.00084	0.0034
126430	0.182	0.015	0.00040	0.00003	0.00000008	0.0001	0.00012	0.0031
126434	0.086	0.013	0.00020	0.00004	0.00000008	0.0001	0.00012	0.0015
126443	1.638	0.052	0.00056	0.00005	0.00000032	0.0001	0.00024	0.0018
126449	0.018	0.005	0.00011	0.00007	0.00000008	0.0001	0.00232	0.0042
126464	0.211	0.205	0.00016	0.00004	0.00000016	0.0007	0.00016	0.0017
126492	0.003	0.196	0.00011	0.00003	0.00000008	0.0031	0.00013	0.0014
145655	0.471	0.140	0.00008	0.00004	0.00000008	0.0002	0.00013	0.0015
145669	0.677	0.226	0.00021	0.00003	0.00000016	0.0002	0.00031	0.0019
145685	0.001	0.202	0.00020	0.00003	0.00000008	0.0003	0.00038	0.0024
145694	-0.039	0.185	0.00021	0.00003	0.00000016	0.0016	0.00057	0.0019
145708	0.048	0.197	0.00010	0.00003	0.00000008	0.0011	0.00017	0.0014
145723	1.067	0.510	0.00022	0.00006	0.00000016	0.0071	0.00015	0.0016
146798	-0.176	0.359	0.00020	0.00005	0.00000032	0.0119	0.00022	0.0017
146824	-0.075	0.222	0.00020	0.00005	0.00000016	0.0029	0.00118	0.0020

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Calculated Mineralogy**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Calculated S (Pyrite) FeS_2	Calculated S (Chalcopyrite) $CuFeS_2 + CuS_2$	Calculated S (Arsenopyrite) $FeAsS + AsS$	Calculated S (Galena) PbS	Calculated S (Cinnibar) HgS	Calculated S (Molybdenite) MoS_2	Calculated S (Pentlandite) ~NiS	Calculated S (Sphalerite) ZnS
	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL								
146831	-0.137	0.469	0.00013	0.00008	0.00000064	0.0144	0.00084	0.0028
146843								
146861	-0.007	0.106	0.00017	0.00004	0.00000008	0.0092	0.00009	0.0010
146868	0.150	0.308	0.00013	0.00003	0.00000016	0.0045	0.00010	0.0007
126352	0.068	0.494	0.00028	0.00004	0.00000016	0.0165	0.00097	0.0021
126358	-0.007	0.318	0.00019	0.00003	0.00000016	0.0047	0.00091	0.0020
126374	-0.058	0.213	0.00014	0.00003	0.00000008	0.0018	0.00097	0.0017
126384	-0.070	0.166	0.00008	0.00003	0.00000008	0.0022	0.00027	0.0015
126391	-0.051	0.207	0.00009	0.00003	0.00000016	0.0093	0.00016	0.0014
146172	-0.059	0.260	0.00018	0.00004	0.00000016	0.0178	0.00022	0.0016
146182	-0.207	0.329	0.00012	0.00003	0.00000032	0.0053	0.00022	0.0021
146203	-0.054	0.206	0.00014	0.00003	0.00000016	0.0050	0.00022	0.0026
146214	-0.044	0.261	0.00012	0.00002	0.00000016	0.0020	0.00022	0.0014
146221	0.139	0.610	0.00013	0.00005	0.00000032	0.0017	0.00039	0.0023
146238	-0.001	0.098	0.00024	0.00003	0.00000016	0.0007	0.00086	0.0015
147034	-0.002	0.471	0.00027	0.00011	0.00000032	0.0379	0.00017	0.0028
147038	-0.069	0.351	0.00015	0.00010	0.00000016	0.0091	0.00037	0.0012
147051	0.058	0.234	0.00015	0.00004	0.00000016	0.0054	0.00030	0.0012
147070	0.466	0.028	0.00033	0.00006	0.00000016	0.0001	0.00013	0.0018
147087	3.233	0.021	0.00037	0.00006	0.00000016	0.0002	0.00038	0.0014
147097	0.560	0.070	0.00017	0.00005	0.00000016	0.0002	0.00012	0.0046
145508	-0.051	0.076	0.00027	0.00003	0.00000016	0.0012	0.00117	0.0024
145527	0.247	0.208	0.00013	0.00005	0.00000016	0.0010	0.00078	0.0022
145543	-0.089	0.188	0.00012	0.00003	0.00000032	0.0080	0.00085	0.0021
145562	-0.116	0.184	0.00013	0.00003	0.00000016	0.0094	0.00083	0.0021
145576	0.355	0.232	0.00000	0.00006	0.00000016	0.0730	0.00032	0.0007
145601	0.209	0.260	0.00028	0.00004	0.00000048	0.0063	0.00071	0.0017
146297	-0.459	0.771	0.00012	0.00004	0.00000032	0.0096	0.00027	0.0017
146314	-0.118	0.249	0.00010	0.00006	0.00000016	0.0060	0.00020	0.0023
146335	-0.148	0.233	0.00015	0.00015	0.00000064	0.0022	0.00017	0.0024
146352	-0.102	0.140	0.00012	0.00004	0.00000008	0.0018	0.00016	0.0028
146368	-0.100	0.181	0.00007	0.00004	0.00000008	0.0018	0.00018	0.0027
146390	-0.133	0.279	0.00018	0.00007	0.00000016	0.0024	0.00017	0.0020
146508	-0.085	0.139	0.00017	0.00007	0.00000016	0.0016	0.00113	0.0027
146526	-0.119	0.177	0.00011	0.00006	0.00000048	0.0003	0.00028	0.0016
146544	-0.032	0.129	0.00009	0.00004	0.00000016	0.0007	0.00035	0.0014
146565	-0.079	0.153	0.00012	0.00004	0.00000016	0.0055	0.00023	0.0008
146589	-0.131	0.216	0.00017	0.00004	0.00000016	0.0235	0.00090	0.0015
146613	0.196	0.298	0.00151	0.00008	0.00000064	0.0286	0.00044	0.0014
146627	-0.094	0.161	0.00020	0.00004	0.00000048	0.0028	0.00025	0.0017
146637	0.063	0.349	0.00009	0.00006	0.00000016	0.0159	0.00043	0.0011
146649	0.130	0.099	0.00005	0.00006	0.00000008	0.0059	0.00046	0.0012
146657	-0.080	0.262	0.00008	0.00004	0.00000016	0.0069	0.00029	0.0008
146676	-0.050	0.226	0.00032	0.00005	0.00000016	0.0060	0.00026	0.0026
125188	-0.202	0.418	0.00010	0.00006	0.00000016	0.0054	0.00025	0.0014
125198	-0.098	0.286	0.00012	0.00006	0.00000032	0.0135	0.00027	0.0021

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Calculated Mineralogy**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Calculated S (Pyrite) FeS_2	Calculated S (Chalcopyrite) $CuFeS_2$ + CuS_2	Calculated S (Arsenopyrite) FeAsS + AsS	Calculated S (Galena) PbS	Calculated S (Cinnibar) HgS	Calculated S (Molybdenite) MoS_2	Calculated S (Pentlandite) ~NiS	Calculated S (Sphalerite) ZnS
	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL								
125207	-0.068	0.165	0.00017	0.00005	0.00000032	0.0015	0.00024	0.0019
125228	-0.095	0.214	0.00006	0.00005	0.00000016	0.0189	0.00039	0.0010
125244	-0.039	0.172	0.00007	0.00004	0.00000016	0.0016	0.00022	0.0013
125257	0.041	0.010	0.00040	0.00006	0.00000016	0.0011	0.00408	0.0033
125278	-0.029	0.035	0.00048	0.00005	0.00000016	0.0001	0.00007	0.0027
125596	-0.109	0.231	0.00014	0.00004	0.00000008	0.0051	0.00023	0.0023
125610	-0.023	0.071	0.00015	0.00004	0.00000016	0.0022	0.00027	0.0030
125626								
125641	-0.175	0.231	0.00012	0.00003	0.00000048	0.0291	0.00099	0.0034
125669	0.628	0.345	0.00018	0.00005	0.00000016	0.0088	0.00053	0.0026
125690	0.005	0.065	0.00018	0.00004	0.00000016	0.0002	0.00079	0.0019
West Breccia Zone								
14018	0.631	0.130	0.00067	0.00081	0.00000016	0.0024	0.00053	0.0021
14021	0.400	0.176	0.00105	0.00142	0.00000008	0.0232	0.00038	0.0028
14036	1.211	0.194	0.00130	0.00031	0.00000008	0.0439	0.00046	0.0021
14043	0.089	0.134	0.00047	0.00007	0.00000008	0.0216	0.00064	0.0023
14060	0.339	0.264	0.00061	0.00009	0.00000008	0.0147	0.00085	0.0014
14067	0.150	0.248	0.00074	0.00063	0.00000008	0.0060	0.00090	0.0036
14076	0.612	0.131	0.00065	0.00366	0.00000016	0.0037	0.00083	0.0082
14083	1.292	0.137	0.00060	0.00031	0.00000016	0.0009	0.00096	0.0064
14099	0.180	0.122	0.00009	0.00036	0.00000032	0.0005	0.00036	0.0103
14103	-0.022	0.266	0.00024	0.00013	0.00000016	0.0154	0.00057	0.0034
125046	-0.036	0.120	0.00031	0.00031	0.00000064	0.0031	0.00067	0.0114
125068	-0.156	0.504	0.00034	0.00008	0.00000064	0.0072	0.00095	0.0039
125073	-0.373	0.871	0.00010	0.00009	0.00000048	0.0248	0.00028	0.0029
125079	-0.401	1.525	0.00083	0.00012	0.00000368	0.0747	0.00041	0.0038
125084	-0.084	0.595	0.00044	0.00007	0.00000032	0.0103	0.00096	0.0066
125127	-0.110	0.163	0.00017	0.00004	0.00000016	0.0043	0.00091	0.0018
125129	-0.097	0.289	0.00014	0.00022	0.00000032	0.0074	0.00086	0.0032
125134	-0.164	0.677	0.00012	0.00005	0.00000016	0.0110	0.00112	0.0026
125142	-0.047	0.264	0.00009	0.00006	0.00000032	0.0101	0.00139	0.0034
125149	-0.103	0.207	0.00012	0.00007	0.00000032	0.0025	0.00083	0.0028
125154	-0.050	0.107	0.00024	0.00006	0.00000016	0.0062	0.00039	0.0024
125165	-0.102	0.269	0.00027	0.00004	0.00000016	0.0011	0.00024	0.0015
125176	-0.283	0.454	0.00022	0.00005	0.00000048	0.0006	0.00038	0.0021
146112	-0.097	0.183	0.00028	0.00007	0.00000008	0.0002	0.00012	0.0032
146115	0.086	0.003	0.00014	0.00004	0.00000016	0.0001	0.00139	0.0050
146124	-0.022	0.075	0.00012	0.00007	0.00000008	0.0020	0.00012	0.0039
146127	0.985	0.030	0.00010	0.00006	0.00000016	0.0006	0.00033	0.0018
146135	-0.018	0.044	0.00033	0.00005	0.00000016	0.0001	0.00011	0.0034
146149	0.009	0.025	0.00019	0.00018	0.00000008	0.0001	0.00019	0.0050
146161	-0.024	0.037	0.00104	0.00006	0.00000008	0.0001	0.00066	0.0051
146164	0.002	0.002	0.00036	0.00007	0.00000008	0.0001	0.00047	0.0052
145951	-0.063	0.212	0.00028	0.00003	0.00000016	0.0013	0.00026	0.0031
145956	-0.055	0.205	0.00021	0.00005	0.00000016	0.0034	0.00088	0.0056
145974	-0.017	0.031	0.00011	0.00006	0.00000008	0.0002	0.00016	0.0052

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Calculated Mineralogy**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Calculated S (Pyrite) FeS_2 (%)	Calculated S (Chalcopyrite) $CuFeS_2 + CuS_2$ (%)	Calculated S (Arsenopyrite) FeAsS + AsS (%)	Calculated S (Galena) PbS (%)	Calculated S (Cinnibar) HgS (%)	Calculated S (Molybdenite) MoS_2 (%)	Calculated S (Pentlandite) ~NiS (%)	Calculated S (Sphalerite) ZnS (%)
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL								
145982	0.023	0.002	0.00006	0.00010	0.00000008	0.0001	0.00044	0.0046
145992	0.047	0.188	0.00017	0.00004	0.00000016	0.0042	0.00070	0.0041
145999	0.002	0.075	0.00019	0.00004	0.00000016	0.0003	0.00027	0.0026
145834	-0.035	0.068	0.00042	0.00010	0.00000008	0.0001	0.00031	0.0065
145842	-0.018	0.027	0.00103	0.00016	0.00000008	0.0006	0.00099	0.0080
145852	-0.047	0.129	0.00073	0.00017	0.00000008	0.0007	0.00030	0.0053
145857	-0.003	0.010	0.00038	0.00004	0.00000008	0.0001	0.00043	0.0025
145871	0.009	0.037	0.00019	0.00007	0.00000008	0.0002	0.00028	0.0036
145608	0.705	0.067	0.00047	0.00013	0.00000008	0.0006	0.00063	0.0023
145614	0.362	0.176	0.00037	0.00037	0.00000008	0.0009	0.00089	0.0026
145628	0.341	0.101	0.00050	0.00011	0.00000008	0.0010	0.00053	0.0039
145640	0.476	0.135	0.00035	0.00422	0.00000112	0.0006	0.00086	0.0520
145646	0.301	0.154	0.00043	0.00014	0.00000016	0.0011	0.00051	0.0050
Paramount Zone								
125965	-0.063	0.384	0.00027	0.00009	0.00000008	0.0071	0.00069	0.0052
125974	1.528	0.065	0.00028	0.00004	0.00000008	0.0031	0.00059	0.0026
125983	0.089	0.169	0.00035	0.00009	0.00000016	0.0125	0.00232	0.0046
125988	0.018	0.005	0.00018	0.00012	0.00000008	0.0001	0.00211	0.0045
126007	-0.039	0.152	0.00006	0.00012	0.00000016	0.0133	0.00054	0.0032
126031	-0.036	0.149	0.00005	0.00008	0.00000016	0.0038	0.00061	0.0024
126040	0.338	0.279	0.00033	0.00004	0.00000016	0.0217	0.00231	0.0025
126054	-0.024	0.164	0.00009	0.00011	0.00000008	0.0056	0.00462	0.0102
126067	0.034	0.244	0.00019	0.00012	0.00000008	0.0070	0.00194	0.0084
126081	0.306	0.624	0.00012	0.00016	0.00000016	0.0060	0.00028	0.0019
126110	0.033	0.011	0.00025	0.00009	0.00000008	0.0002	0.00161	0.0046
126118	0.035	0.580	0.00020	0.00003	0.00000008	0.0113	0.00118	0.0038
125904	-0.168	0.312	0.00013	0.00005	0.00000016	0.0228	0.00059	0.0023
125919	-0.052	0.509	0.00014	0.00006	0.00000016	0.0226	0.00032	0.0031
125928	-0.056	0.121	0.00020	0.00034	0.00000016	0.0085	0.00079	0.0049
125933	-0.003	0.004	0.00014	0.00028	0.00000008	0.0001	0.00077	0.0074
125944	0.082	0.031	0.00021	0.00024	0.00000008	0.0008	0.00081	0.0052
125952	1.015	0.022	0.00010	0.00005	0.00000016	0.0006	0.00046	0.0015
125963	-0.046	0.414	0.00018	0.00008	0.00000016	0.0045	0.00037	0.0064
126120	-0.180	0.224	0.00004	0.00007	0.00000032	0.0037	0.00051	0.0020
126131	-0.086	0.102	0.00013	0.00006	0.00000080	0.0003	0.00060	0.0027
126142	-0.049	0.080	0.00012	0.00009	0.00000080	0.0006	0.00066	0.0079
126154	-0.153	0.251	0.00015	0.00007	0.00000128	0.0055	0.00108	0.0062
126171	1.044	0.186	0.00010	0.00007	0.00000016	0.0063	0.00058	0.0035
126181	0.171	0.024	0.00011	0.00023	0.00000016	0.0001	0.00061	0.0052
125806	0.398	0.059	0.00028	0.00009	0.00000008	0.0001	0.00079	0.0023
125816	0.015	0.007	0.00035	0.00028	0.00000008	0.0001	0.00038	0.0064
125833	-0.110	0.369	0.00006	0.00011	0.00000016	0.0082	0.00049	0.0022
125861	-0.080	0.317	0.00005	0.00004	0.00000016	0.0142	0.00044	0.0012
125875	-0.090	0.278	0.00004	0.00005	0.00000016	0.0099	0.00029	0.0016
125897	-0.012	0.064	0.00018	0.00004	0.00000008	0.0099	0.00043	0.0012

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Calculated Mineralogy**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Calculated S (Pyrite) FeS_2 (%)	Calculated S (Chalcopyrite) $CuFeS_2$ + CuS_2 (%)	Calculated S (Arsenopyrite) FeAsS + AsS (%)	Calculated S (Galena) PbS (%)	Calculated S (Cinnibar) HgS (%)	Calculated S (Molybdenite) MoS_2 (%)	Calculated S (Pentlandite) ~NiS (%)	Calculated S (Sphalerite) ZnS (%)
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL								
Tailings								
LIARD ZONE	-0.023	0.086	0.00021	0.00007	0.00000080	0.0037	0.00090	0.0021
PARAMOUNT	-0.021	0.131	0.00022	0.00010	0.00000080	0.0052	0.00156	0.0031
WEST BRECCIA	-0.020	0.181	0.00033	0.00011	0.00000080	0.0028	0.00199	0.0040
High-Sulphide Histor								
T112 (171' - 172')	8.994	0.021	0.00140	0.00129	0.00000016	0.0006	0.00284	0.0048
T113 (81' - 82')	0.789	0.037	0.00048	0.00014	0.00000048	0.0008	0.00053	0.0015
T113 (983' - 985')	1.651	0.430	0.00070	0.00014	0.00000016	0.0040	0.00079	0.0027
T140 (30' - 31')	-0.298	0.412	0.00015	0.00005	0.00000016	0.0042	0.00024	0.0016
T166 (389' - 390')	0.710	0.076	0.00007	0.00004	0.00000008	0.0001	0.00044	0.0008
T185 (116' - 117')	2.236	0.011	0.00027	0.00009	0.00000016	0.0008	0.00036	0.0007
T207 (261.5' - 262')	3.793	0.058	0.00012	0.00003	0.00000016	0.0092	0.00044	0.0007
T207 (269' - 271')	13.390	0.038	0.00036	0.00006	0.00000016	0.0209	0.00064	0.0018
All Data								
Maximum	13.4	1.53	0.0015	0.0042	0.0000037	0.075	0.0098	0.052
Minimum	-0.46	0.0016	0.0000043	0.000025	0.00000008	0.000053	0.000072	0.00035
Mean	0.22	0.23	0.00022	0.00012	0.00000023	0.0079	0.00061	0.0029
Standard Deviation	1.16	0.18	0.00022	0.00038	0.00000029	0.011	0.00083	0.0037
10 Percentile	-0.17	0.033	0.000077	0.000033	0.00000008	0.00017	0.00014	0.0012
25 Percentile	-0.095	0.12	0.00011	0.00004	0.00000008	0.00099	0.00023	0.0016
Median	-0.027	0.21	0.00015	0.000051	0.00000016	0.0045	0.00039	0.0022
75 Percentile	0.13	0.31	0.00024	0.000079	0.00000016	0.01	0.00079	0.0031
90 Percentile	0.64	0.47	0.00041	0.00014	0.00000048	0.02	0.0011	0.0051
Interquartile Range (IC	0.23	0.19	0.00014	0.00004	0.00000008	0.009	0.00056	0.0015
Variance	1.34	0.034	0.000000047	0.00000015	8.5E-14	0.00012	0.00000069	0.000013
Skewness	8.52	2.15	3.21	8.93	7.79	2.97	6.81	10.6
Coefficient of Variatior	5.21	0.79	0.99	3.18	1.29	1.37	1.35	1.27
Count	235	235	235	235	235	235	235	235
Main Zone								
Maximum	3.23	0.77	0.0015	0.00032	0.00000096	0.073	0.0098	0.0056
Minimum	-0.46	0.0055	0.0000043	0.000025	0.00000008	0.000055	0.000072	0.00035
Mean	0.077	0.26	0.00016	0.00005	0.0000002	0.0087	0.00052	0.002
Standard Deviation	0.44	0.15	0.00015	0.00003	0.00000014	0.011	0.0009	0.00076
10 Percentile	-0.18	0.073	0.000075	0.000031	0.00000008	0.00036	0.00012	0.0012
25 Percentile	-0.11	0.16	0.000099	0.000036	0.00000016	0.0015	0.00018	0.0014
Median	-0.051	0.23	0.00013	0.000043	0.00000016	0.0053	0.00028	0.002
75 Percentile	0.063	0.33	0.00019	0.000056	0.00000016	0.012	0.0006	0.0024
90 Percentile	0.47	0.48	0.00027	0.000073	0.00000032	0.02	0.00097	0.0028
Interquartile Range (IC	0.17	0.17	0.00009	0.00002	0	0.01	0.00042	0.0009
Variance	0.2	0.023	0.000000021	8.8E-10	2E-14	0.00012	0.00000082	0.00000058
Skewness	3.91	0.94	5.94	5.71	2.37	2.57	7.93	1.19
Coefficient of Variatior	5.7	0.59	0.89	0.59	0.69	1.24	1.74	0.38
Count	146	146	146	146	146	146	146	146

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Calculated Mineralogy**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Calculated S (Pyrite) FeS_2 (%)	Calculated S (Chalcopyrite) $CuFeS_2 + CuS_2$ (%)	Calculated S (Arsenopyrite) $FeAsS + AsS$ (%)	Calculated S (Galena) PbS (%)	Calculated S (Cinnibar) HgS (%)	Calculated S (Molybdenite) MoS_2 (%)	Calculated S (Pentlandite) ~NiS (%)	Calculated S (Sphalerite) ZnS (%)
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL								
West Breccia Zone								
Maximum	1.29	1.53	0.0013	0.0042	0.0000037	0.075	0.0014	0.052
Minimum	-0.4	0.0016	0.000064	0.000028	0.00000008	0.000053	0.00011	0.0014
Mean	0.12	0.21	0.00039	0.00033	0.00000027	0.0067	0.00059	0.0051
Standard Deviation	0.36	0.27	0.0003	0.00081	0.00000054	0.013	0.00033	0.0073
10 Percentile	-0.13	0.027	0.00011	0.000044	0.00000008	0.00012	0.00022	0.002
25 Percentile	-0.059	0.067	0.00017	0.000057	0.00000008	0.00037	0.00032	0.0026
Median	-0.017	0.14	0.00031	0.000078	0.00000016	0.0011	0.00053	0.0036
75 Percentile	0.24	0.23	0.00048	0.00018	0.00000016	0.0067	0.00086	0.0051
90 Percentile	0.62	0.47	0.00078	0.00048	0.00000048	0.018	0.00096	0.0071
Interquartile Range (IC	0.3	0.16	0.00032	0.00012	0.00000008	0.0063	0.00054	0.0026
Variance	0.13	0.071	0.000000088	0.00000065	3E-13	0.00018	0.00000011	0.000054
Skewness	1.68	3.24	1.31	4.16	5.64	3.65	0.54	5.98
Coefficient of Variatior	2.93	1.27	0.76	2.45	2	1.98	0.56	1.44
Count	47	47	47	47	47	47	47	47
Paramount Zone								
Maximum	1.53	0.62	0.00035	0.00034	0.0000013	0.023	0.0046	0.01
Minimum	-0.18	0.0041	0.000043	0.000034	0.00000008	0.00012	0.00028	0.0012
Mean	0.12	0.2	0.00016	0.00011	0.00000021	0.0068	0.00096	0.0041
Standard Deviation	0.39	0.17	0.000091	0.000081	0.00000026	0.0067	0.0009	0.0023
10 Percentile	-0.11	0.011	0.000052	0.000043	0.00000008	0.00014	0.00037	0.0016
25 Percentile	-0.06	0.061	0.0001	0.000057	0.00000008	0.00059	0.00048	0.0023
Median	-0.012	0.16	0.00014	0.000088	0.00000016	0.0056	0.00061	0.0034
75 Percentile	0.085	0.3	0.00021	0.00012	0.00000016	0.0099	0.00095	0.0052
90 Percentile	0.4	0.41	0.00028	0.00024	0.00000032	0.014	0.0021	0.0074
Interquartile Range (IC	0.15	0.23	0.0001	0.00006	0.00000008	0.0093	0.00047	0.0029
Variance	0.15	0.03	8.4E-09	6.5E-09	7E-14	0.000045	0.00000081	0.0000054
Skewness	2.51	0.88	0.57	1.61	3.09	1.11	2.65	0.84
Coefficient of Variatior	3.12	0.87	0.55	0.73	1.25	0.99	0.94	0.57
Count	31	31	31	31	31	31	31	31

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Calculated Mineralogy**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

Sample Id.	Calculated S (Pyrite) FeS_2 (%)	Calculated S (Chalcopyrite) $CuFeS_2$ + CuS_2 (%)	Calculated S (Arsenopyrite) FeAsS + AsS (%)	Calculated S (Galena) PbS (%)	Calculated S (Cinnibar) HgS (%)	Calculated S (Molybdenite) MoS_2 (%)	Calculated S (Pentlandite) ~NiS (%)	Calculated S (Sphalerite) ZnS (%)
Method	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated	Calculated
MDL								
Tailings								
Maximum	-0.02	0.18	0.00033	0.00011	0.0000008	0.0052	0.002	0.004
Minimum	-0.023	0.086	0.00021	0.000074	0.0000008	0.0028	0.0009	0.0021
Mean	-0.021	0.13	0.00025	0.000094	0.0000008	0.0039	0.0015	0.003
Standard Deviation	0.0014	0.047	0.00007	0.000017	0	0.0012	0.00055	0.00093
10 Percentile	-0.023	0.095	0.00021	0.00008	0.0000008	0.003	0.001	0.0023
25 Percentile	-0.022	0.11	0.00021	0.000088	0.0000008	0.0033	0.0012	0.0026
Median	-0.021	0.13	0.00022	0.0001	0.0000008	0.0037	0.0016	0.0031
75 Percentile	-0.021	0.16	0.00028	0.0001	0.0000008	0.0044	0.0018	0.0035
90 Percentile	-0.02	0.17	0.00031	0.0001	0.0000008	0.0049	0.0019	0.0038
Interquartile Range (IC	0.0014	0.047	0.000064	0.000016	0	0.0012	0.00055	0.00093
Variance	0.000002	0.0023	4.9E-09	2.8E-10	0	0.0000014	0.0000003	0.00000086
Skewness	0.012	0.13	1.62	-1.58	NA	0.8	-0.61	-0.081
Coefficient of Variatior	-0.065	0.36	0.27	0.18	0	0.3	0.37	0.3
Count	3	3	3	3	3	3	3	3
High-Sulphide Histor								
Maximum	13.4	0.43	0.0014	0.0013	0.00000048	0.021	0.0028	0.0048
Minimum	-0.3	0.011	0.000073	0.000028	0.00000008	0.0001	0.00024	0.00065
Mean	3.91	0.14	0.00045	0.00023	0.00000019	0.0051	0.00079	0.0018
Standard Deviation	4.8	0.18	0.00044	0.00043	0.00000012	0.0071	0.00085	0.0014
10 Percentile	0.41	0.018	0.00011	0.000039	0.00000014	0.00046	0.00032	0.00065
25 Percentile	0.77	0.033	0.00014	0.000047	0.00000016	0.00077	0.00042	0.00072
Median	1.94	0.048	0.00032	0.000072	0.00000016	0.0024	0.00049	0.0015
75 Percentile	5.09	0.16	0.00054	0.00014	0.00000016	0.0054	0.00068	0.002
90 Percentile	10.3	0.42	0.00091	0.00048	0.00000026	0.013	0.0014	0.0033
Interquartile Range (IC	4.32	0.13	0.00039	0.000093	0	0.0046	0.00026	0.0013
Variance	23	0.031	0.00000019	0.00000018	1.5E-14	0.00005	0.00000072	0.0000019
Skewness	1.43	1.39	1.75	2.77	2.49	1.98	2.61	1.67
Coefficient of Variatior	1.23	1.31	0.98	1.88	0.63	1.39	1.08	0.78
Count	8	8	8	8	8	8	8	8

Data in blue indicates a calculated parameter.

Calculated S (Pyrite) (%) =
% S (Sulphide) + S (del) - S (Chalcopyrite) - S (Arsenopyrite) - S (Galena) - S (Cinnibar) - S (Molybdenite) - S (Sphalerite)
Calculated S (Chalcopyrite) CuFeS2 + CuS2 (%) = (1 / 0.99) * Copper (ppm) / 10000
Calculated S (Arsenopyrite) FeAsS + AsS (%) = (1 / 2.33) * Iron (%) / 10000
Calculated S (Galena) PbS (%) = (1 / 6.45) * Iron (ppm) / 10000
Calculated S (Cinnibar) HgS (%) = (1 / 6.25) * Gallium (ppm) / 10000
Calculated S (Molybdenite) MoS2 (%) = (1 / 1.5) * Germanium (ppm) / 10000
Calculated S (Sphalerite) ZnS (%) = (1 / 2) * Hafnium (ppm) / 10000

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.
ME-MS61:Interference: Ca>10% on ICP-MS As ICP-AES results shown.

Sample	Silver	Aluminum	Arsenic	Barium	Beryllium	Bismuth	Calcium	Cadmium	Cerium	Cobalt	Chromium	Cesium	Copper	Iron	Gallium	Germanium
Id.	Ag	Al	As	Ba	Be	Bi	Ca	Cd	Ce	Co	Cr	Cs	Cu	Fe	Ga	Ge
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.01	100	0.2	10	0.05	0.01	100	0.02	0.01	0.1	1	0.05	0.2	100	0.05	0.05
Crustal Abundance: Fron	0.037	4200	1	0.4	1	0.007	5100	0.035	11.5	0.1	2	0.4	4	3800	4	0.2
Crustal Abundance: To	0.11	88000	13	2300	3	0.01	312400	0.42	345	74	170	6	250	86500	30	8
Main Zone																
14130	3.33	85100	2.1	440	0.62	2	26200	*0.01*	15.5	5	15	3.56	5530	18000	18.25	0.08
14144	2.52	93900	5.1	380	0.84	2.32	37500	*0.01*	20.7	7.7	5	5.29	3410	36100	20	0.1
14148	1.75	81100	2.6	560	0.9	1.98	46300	*0.01*	22.7	11	4	4.68	2880	38300	18.75	0.1
14156	1.76	76900	1.1	280	1.56	1.47	24700	*0.01*	23.3	5.4	25	2.49	2090	17400	20.5	0.07
14162	0.53	79700	2.1	510	0.92	2.13	55900	*0.01*	25.2	20.8	71	2.12	1020	42500	14.85	0.1
14169	2.84	76400	1.9	100	1.09	6.51	23200	*0.01*	7.62	4.2	16	1.19	3820	11800	18.85	0.05
14232	1.73	94400	3.5	140	0.95	0.84	26600	*0.01*	22.2	4.7	14	6.81	3370	26400	19.75	0.08
14250	1.66	94400	3.4	170	0.75	1.14	40700	*0.01*	24.1	8.3	12	4.65	3170	45800	21	0.11
14260	2.92	89500	2.6	170	0.73	6.57	30400	*0.01*	21.6	7.8	3	4.9	4880	42300	20	0.1
14276	0.8	98400	7.5	1000	0.78	0.78	43100	0.13	21.2	8.8	17	2.68	1490	38900	20.3	0.08
14295	0.51	89700	3.7	110	0.7	0.2	39100	0.02	18.6	18.6	12	4.81	2330	47300	18.95	0.1
14301	0.39	87600	3.8	300	0.86	0.4	36600	*0.01*	20.1	10.4	15	3.85	2440	31300	18.05	0.09
14323	1.33	93600	3.3	280	0.92	0.74	37500	*0.01*	20.5	8.8	3	6.79	2250	38700	20.5	0.09
14332	1.36	96200	2.2	210	0.88	0.62	33900	*0.01*	23.9	7.7	3	5.41	3470	35500	20.8	0.09
14345	2.38	97300	2.1	190	0.9	2.05	25500	*0.01*	26.4	7.2	11	4.35	6070	22100	20.4	0.09
14348	1	94300	2.3	150	0.82	1.13	21500	*0.01*	24.6	8.4	11	4.61	4900	34700	20.1	0.09
14797	1.03	86900	2.5	150	0.92	0.43	37800	*0.01*	15.4	10.5	6	6.37	1750	42700	19.85	0.11
14808	2.27	81300	*0.1*	170	1.58	1.73	48700	*0.01*	21.5	9.2	6	5.38	2640	37600	18.75	0.33
14816	2.15	82900	1.8	140	0.84	2.94	33300	*0.01*	18.3	10.1	5	5.98	3970	41300	21.4	0.12
14828	2.42	89200	2.4	710	0.94	2.48	43400	*0.01*	23.8	10.3	4	5.11	3260	41200	20.9	0.13
14844	1.35	91800	3.7	300	0.67	1.02	28200	*0.01*	15.75	19	39	8.05	2990	51800	22	0.12
14680	3.36	90500	1.8	300	2.27	5.64	41400	*0.01*	27.1	11	5	10.45	3950	41400	21	0.28
14871	1.02	96200	2.3	120	0.74	1.28	34000	*0.01*	18.75	12.7	10	5.3	3880	46100	21.4	0.11
14887	0.41	96900	2.9	340	0.68	0.28	51800	*0.01*	22.1	16.2	20	3.33	1990	53100	20.4	0.12
14689	0.38	83800	1.4	120	1.01	0.44	21800	*0.01*	29.6	5.9	10	2.38	2020	14800	18.4	0.07
14695	0.71	97000	*0.1*	170	0.89	1.19	39800	*0.01*	26.4	9.6	6	7.95	1500	39900	21.4	0.24
14742	1.3	90600	0.5	120	1.35	4.71	27800	*0.01*	17.2	10.4	24	2.84	2100	33500	20.5	0.33
14666	0.37	92100	4.8	330	0.78	0.13	39300	*0.01*	19.3	21.9	21	4.19	1440	53900	21.9	0.1
14685	1.13	85900	6.6	380	1.04	0.51	33100	*0.01*	22.1	35.4	5	5.87	4330	63900	22.7	0.1
14685B	1	83100	5.9	310	1.1	0.48	29500	*0.01*	19.45	30.6	7	5.85	4570	59700	21.8	0.11
14545	0.26	94700	3.4	860	0.8	0.08	38200	*0.01*	24.1	10.3	16	4.7	1210	41700	21.2	0.1
14565	0.47	88300	3	220	0.7	0.39	45800	*0.01*	22.7	8.7	11	5.46	2670	37200	18.65	0.09
14571	1.92	82200	3.2	430	0.99	1.04	25900	*0.01*	20.9	12.9	7	5.37	5450	26900	18.05	0.08
14578	0.65	86800	5.2	640	1.16	0.33	42000	*0.01*	23.9	15.8	9	6.35	2980	41600	19.4	0.1
14578B	0.74	82400	4.5	760	1	0.31	43200	*0.01*	22.8	15.7	10	6.22	3280	39200	20.4	0.11
14598	0.39	92500	2.7	220	0.85	1.23	33500	*0.01*	16.15	15.9	3	4.8	703	46600	22.6	0.09
14893	0.67	92000	4.5	490	0.81	0.56	41600	*0.01*	18.75	18.3	44	5.23	1630	53400	22.6	0.11
14899	0.25	97000	8.1	330	0.78	0.18	35400	*0.01*	15.8	22.6	43	2.68	409	56900	24.2	0.12
14908	0.39	95800	6.2	690	0.69	0.29	37900	*0.01*	19.6	15	39	2.29	1140	53200	23.3	0.11
14917	2.53	85300	1.7	740	1.19	1.43	23200	*0.01*	25.1	9.4	16	2.27	3800	24200	23.5	0.1
14925	0.71	87800	3.5	390	0.71	0.58	36000	*0.01*	17.85	13.9	30	4.58	1610	46200	22.7	0.12
14998	0.72	90100	3.4	280	0.63	0.53	39800	*0.01*	20.1	12.8	6	5.88	1800	43600	21.6	0.12
15862	0.74	87200	2.2	290	0.66	0.49	42200	*0.01*	19.1	12.2	4	5.75	1180	41600	21	0.1
15870	1.17	81000	2.6	1030	0.46	0.54	46400	*0.01*	20.6	10.3	27	4.53	2020	39200	20.4	0.12
15879	1.4	90600	2.4	760	0.67	0.51	48300	*0.01*	19.85	13.6	29	4.83	2150	51500	21.7	0.12

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.
ME-MS61:Interference: Ca>10% on ICP-MS As ICP-AES results shown.

Sample	Silver	Aluminum	Arsenic	Barium	Beryllium	Bismuth	Calcium	Cadmium	Cerium	Cobalt	Chromium	Cesium	Copper	Iron	Gallium	Germanium
Id.	Ag	Al	As	Ba	Be	Bi	Ca	Cd	Ce	Co	Cr	Cs	Cu	Fe	Ga	Ge
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.01	100	0.2	10	0.05	0.01	100	0.02	0.01	0.1	1	0.05	0.2	100	0.05	0.05
Crustal Abundance: Fron	0.037	4200	1	0.4	1	0.007	5100	0.035	11.5	0.1	2	0.4	4	3800	4	0.2
Crustal Abundance: To	0.11	88000	13	2300	3	0.01	312400	0.42	345	74	170	6	250	86500	30	8
15887	2.42	87200	2	440	0.75	1.14	41200	*0.01*	15.05	14	25	5.1	5070	34600	21.4	0.12
15891	2.15	89500	1.7	1250	0.66	0.98	51300	*0.01*	17.35	9.7	22	5.24	2450	38500	21.4	0.11
15908	2.82	87100	1.5	260	0.77	1.3	45200	*0.01*	17.95	12.7	24	5.96	4260	34500	20.8	0.1
15911	1.2	88600	2.1	410	0.7	0.56	35200	*0.01*	19.5	14.8	33	6.92	1820	46500	22.2	0.1
125285	3.53	86700	2	420	0.73	2.05	23300	0.05	12.45	7.8	50	2.18	6100	27400	21.9	0.11
125288	0.15	78400	4.7	320	0.66	0.08	62100	0.08	29.1	42.7	269	0.48	101	61200	13.35	0.13
125293	3.52	82700	2.4	170	0.89	2.21	24100	*0.01*	15.25	12.3	67	2.75	5680	37200	20.9	0.12
125305	2.56	92600	2.6	390	0.87	1.41	27700	*0.01*	19.85	8.7	40	3.75	3490	33100	20.6	0.1
125311	1.14	90300	2.3	490	0.78	0.48	23500	0.02	14.85	6	32	4.53	1560	19000	18.5	0.09
125703	0.73	87600	2.1	150	1.15	0.45	33300	*0.01*	16.75	9.6	29	5.86	1405	39600	19.9	0.1
125728	1.36	85700	3.6	460	0.81	1.48	33800	*0.01*	18.9	12.7	43	3.71	2430	47400	20.1	0.08
125755	0.8	69000	0.7	400	1.07	1.56	18400	*0.01*	14.75	3.5	53	2.51	3150	10000	14.55	0.06
125772	1.63	85800	2.9	320	0.93	3.27	34700	*0.01*	19.5	11.9	37	4.96	2550	42100	18.9	0.1
125795	1.16	83900	3.2	520	0.6	2.29	44300	0.02	18.5	15.9	30	5.05	1335	50000	18.3	0.09
125422	0.97	94800	2.6	180	1.15	0.53	36800	0.03	23.4	10.3	14	5.68	2110	45600	22.1	0.13
125435	0.86	84700	3.1	120	0.87	0.78	34800	*0.01*	21.1	10.5	14	5.1	1875	46200	21.2	0.12
125452	3.2	89000	2.6	120	1.11	2.33	38500	0.02	19.8	13.3	8	8.73	7000	43400	22.8	0.12
125476	1.16	68500	4.7	1310	1.01	2.16	21500	0.07	15.5	5.4	58	3.14	3530	13500	12.85	0.07
125490	0.39	92900	3.2	90	0.68	0.11	34700	*0.01*	22.8	14.3	16	4.06	2110	49900	21	0.11
126192	0.59	93200	4.6	200	0.87	0.29	37000	0.06	21.6	7.8	22	4.27	2300	27600	21.4	0.08
126206	0.62	102500	3.9	430	0.89	1.14	39800	0.04	23.9	7.9	19	4.96	1830	36400	21.9	0.1
126225	0.89	86100	2.7	660	0.68	1.06	35700	0.04	18.7	7.1	18	5.1	2760	31900	20.2	0.09
126244	1.67	93600	2.9	180	0.71	3.23	41800	0.04	17.85	8.3	9	5.03	2560	34800	21	0.09
126266	0.71	97100	2.6	170	0.76	1.23	36300	0.02	19.6	9.8	13	5.34	1930	39500	21.5	0.08
126279	0.32	79700	4	160	0.61	2.01	43100	0.04	13.6	7.6	20	3.24	2260	35300	17.9	0.08
126288	1.04	90500	1.9	190	0.77	2.27	42500	0.02	16.7	9.7	13	7.68	3340	29000	20.4	0.08
126297	0.6	88400	4.5	170	0.99	0.58	54100	0.06	29.5	17.7	24	6.75	2470	42300	20.9	0.09
126314	1	93700	3.6	220	0.88	0.42	42700	0.05	18.75	16.4	20	8.18	7040	37200	20.8	0.08
126329	1.31	83200	1.7	660	0.82	0.46	43800	0.08	23.2	7.2	24	3.74	3090	31100	21.3	0.08
126337	1.97	88600	3.2	370	0.81	0.97	41900	0.07	19.15	15.5	23	5.24	5120	40800	19.6	0.1
126351	1.29	88100	4.4	330	0.73	1.13	45300	*0.01*	20.8	9.2	20	4.93	2010	27300	21.3	0.14
126427	0.54	90800	13.8	200	0.81	0.61	51000	0.05	18.45	18.2	24	3.45	463	58900	20.9	0.13
126430	0.13	95100	9.3	180	0.52	0.13	45500	0.04	25.5	8.7	12	5.07	150	50400	20.2	0.13
126434	0.1	82200	4.7	160	0.73	0.11	42200	0.02	19.7	10.8	11	8.02	127.5	41400	22	0.14
126443	0.26	88300	13.1	120	0.74	0.84	42200	0.02	22.2	31.1	11	8.25	513	48000	20.2	0.16
126449	0.06	94900	2.6	450	1.02	0.02	49600	0.11	35.1	31.5	49	0.35	54.4	62500	20.1	0.16
126464	0.72	93400	3.8	200	0.62	0.46	45000	0.03	24.7	11.7	23	4.33	2030	42400	19.35	0.11
126492	0.36	90400	2.6	210	0.68	0.16	42900	*0.01*	21.3	10.3	15	6.25	1940	40400	21.3	0.12
145655	0.34	91100	1.9	700	0.67	0.14	47100	0.03	25.3	15.4	13	3.58	1390	40300	21.1	0.16
145669	0.53	92300	5	190	0.7	0.36	42000	0.02	22.2	23.1	11	4.83	2240	52300	19.7	0.09
145685	0.3	86900	4.7	130	0.57	0.07	37200	0.02	16.4	12	19	5.03	2000	46000	19.3	0.1
145694	0.55	85100	5	130	0.58	0.22	43700	0.02	15.65	14	23	4.97	1830	48500	19.05	0.09
145708	0.46	83200	2.4	100	0.67	0.24	34700	0.02	18.85	12.8	20	4.53	1950	36800	18.75	0.09
145723	1.72	80900	5.1	160	0.66	8.5	34300	0.06	17.15	16.7	23	8.9	5050	47300	18.45	0.1
146798	2.08	86300	4.7	340	0.81	1.1	42700	*0.01*	20.1	11.7	16	10.6	3550	41600	21.7	0.22
146824	1.16	90200	4.6	230	0.71	1.57	38500	*0.01*	19.5	15.5	43	3.6	2200	51900	22.5	0.21

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.
ME-MS61:Interference: Ca>10% on ICP-MS As ICP-AES results shown.

Sample Id.	Silver Ag (ppm)	Aluminum Al (ppm)	Arsenic As (ppm)	Barium Ba (ppm)	Beryllium Be (ppm)	Bismuth Bi (ppm)	Calcium Ca (ppm)	Cadmium Cd (ppm)	Cerium Ce (ppm)	Cobalt Co (ppm)	Chromium Cr (ppm)	Cesium Cs (ppm)	Copper Cu (ppm)	Iron Fe (ppm)	Gallium Ga (ppm)	Germanium Ge (ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.01	100	0.2	10	0.05	0.01	100	0.02	0.01	0.1	1	0.05	0.2	100	0.05	0.05
Crustal Abundance: Fron	0.037	4200	1	0.4	1	0.007	5100	0.035	11.5	0.1	2	0.4	4	3800	4	0.2
Crustal Abundance: To	0.11	88000	13	2300	3	0.01	312400	0.42	345	74	170	6	250	86500	30	8
146831	2.22	87200	3	170	0.79	2.49	38800	*0.01*	18.95	15.1	44	2.93	4640	45100	20.6	0.22
146843																
146861	0.45	94200	4	430	0.8	1.75	42000	*0.01*	24.2	10.6	21	4.16	1050	42100	22	0.23
146868	1	89100	3.1	270	0.87	1.5	37200	*0.01*	23.3	11.1	15	6.3	3050	34300	21.1	0.2
126352	1.13	96100	6.6	320	0.61	0.81	38400	*0.01*	21.7	19.5	44	3.82	4890	52000	24.8	0.15
126358	0.54	92500	4.4	260	0.63	1.96	36700	*0.01*	18.45	18.1	41	3.99	3150	51900	21.6	0.12
126374	0.49	90700	3.2	270	0.51	0.35	37700	*0.01*	21	17.7	45	3.74	2110	55100	21.2	0.14
126384	1.07	91000	1.9	280	0.69	1.92	39500	*0.01*	21.2	12.7	33	4.57	1640	48700	22	0.13
126391	1.19	89100	2	320	0.63	4.01	42200	*0.01*	17	11.1	11	4.15	2050	45300	22.3	0.13
146172	0.95	72200	4.2	210	0.68	0.61	34500	0.1	15.5	11.3	27	6.93	2570	43700	17.7	0.09
146182	1.94	85800	2.8	210	0.67	0.98	37400	0.03	19.3	12	27	3.01	3260	46400	20.9	0.1
146203	0.64	85400	3.2	130	0.74	0.71	29300	0.03	14.8	8.1	27	4.39	2040	28700	19.35	0.07
146214	0.7	81900	2.7	180	0.66	0.37	41500	0.04	20.7	10.3	17	3.89	2580	38400	19.25	0.08
146221	1.31	86400	3.1	290	0.96	1.49	36400	0.04	26.5	22.6	14	5.25	6040	54300	20.3	0.1
146238	0.24	94800	5.7	300	0.66	0.1	42700	0.02	21.3	18.1	41	2.9	971	62300	22.1	0.11
147034	2.42	88900	6.3	200	1.1	1.43	29300	*0.01*	22.3	7.1	19	7.97	4660	33900	20.7	0.76
147038	1.21	76000	3.4	1130	1.03	0.73	26500	*0.01*	20.5	8.1	48	3.81	3470	23500	18.7	0.19
147051	0.65	88300	3.6	880	1.22	0.1	35800	*0.01*	26.6	11.1	23	5.74	2320	39800	20.7	0.2
147070	0.21	101500	7.6	180	0.96	0.16	54300	0.03	29.9	19.4	26	3.23	275	58300	24.1	0.23
147087	0.22	86600	8.7	120	0.71	0.4	35200	0.03	21.3	57.5	25	2.37	203	66900	19.65	0.23
147097	0.23	94700	3.9	1010	0.86	0.23	44700	0.12	26.1	22.4	8	4.55	693	47400	21.2	0.22
145508	0.46	91400	6.4	360	0.67	0.3	29900	*0.01*	13.05	22	43	2.07	748	53700	23.7	0.13
145527	1.06	95400	3.1	490	0.75	0.79	42700	0.04	23	13.2	42	5.31	2060	51900	23.4	0.13
145543	1.29	87700	2.7	370	0.72	0.76	33700	0.03	19.8	12.5	46	3.62	1860	38200	22.4	0.14
145562	1.07	89100	3	290	0.73	1.63	39500	*0.01*	20.3	13.9	42	7.14	1820	45300	21.7	0.12
145576	0.61	73700	*0.1*	750	0.73	2	17400	*0.01*	18.05	4.5	62	2.17	2300	10100	14.55	0.08
145601	1.88	96800	6.6	560	0.58	4.15	48000	*0.01*	22.2	17.4	30	4.97	2570	53800	22.7	0.15
146297	3.96	82600	2.8	250	0.66	1.85	37900	0.1	20.5	10.1	17	4.98	7630	32100	22	0.09
146314	1.65	83900	2.4	220	0.79	0.77	39500	0.06	18.1	11.8	21	5.91	2470	43200	20.6	0.09
146335	1.57	87000	3.6	220	0.83	0.47	43200	0.04	23.1	11.3	16	7.51	2310	44100	21.3	0.1
146352	0.92	77000	2.7	220	0.7	0.24	31700	0.04	18.3	9.6	35	4.12	1390	38100	18.5	0.07
146368	1.15	81100	1.7	170	0.72	0.72	39800	0.04	16.4	11	19	4.31	1790	40900	20.3	0.08
146390	1.68	93800	4.3	230	0.83	0.98	47600	*0.01*	25.9	13.1	5	5.11	2760	43500	22.1	0.22
146508	1.04	90400	3.9	250	1.03	0.53	35100	*0.01*	19.5	14	48	5.27	1380	40300	26.9	0.22
146526	1.32	88500	2.6	470	0.91	0.65	41900	0.04	22.7	9.3	30	5.35	1750	31000	21.5	0.2
146544	0.69	83200	2.2	460	0.97	0.48	37000	0.03	15.9	6.8	47	4.84	1280	19100	20.3	0.2
146565	1.22	79900	2.7	1230	1.01	0.64	35300	*0.01*	20	6.1	29	15.05	1510	16800	20.4	0.22
146589	1.49	83600	3.9	370	0.91	1.1	39900	*0.01*	18.25	13.7	46	7.02	2140	40900	20.9	0.21
146613	1.12	91400	35.1	130	0.93	2.25	56300	*0.01*	17.25	9.3	23	4.61	2950	27000	20.9	0.22
146627	1.02	71100	4.6	340	0.73	1.07	34800	*0.01*	17.9	8.6	49	3.19	1590	28600	16	0.2
146637	1.17	77600	2.1	1060	1.09	2	29800	*0.01*	16.5	6.2	71	3.93	3460	17000	20.8	0.21
146649	0.23	79900	1.2	980	1.39	0.18	25500	*0.01*	22	7.1	53	2.74	980	16600	19.25	0.18
146657	1.81	79400	1.9	410	1.26	4.43	19100	*0.01*	13.15	4.2	66	2.11	2590	10700	21.4	0.17
146676	1.98	92300	7.5	230	1.6	4.04	39400	*0.01*	13	6.9	11	4.96	2240	15400	25.8	0.22
125188	2.13	93100	2.3	650	0.98	1.5	30600	*0.01*	16.45	6.6	19	4.07	4140	26700	20.1	0.08
125198	1.65	91000	2.9	290	0.9	1.92	33700	*0.01*	20	7	25	4.26	2830	33800	21.3	0.09

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.
ME-MS61:Interference: Ca>10% on ICP-MS As ICP-AES results shown.

Sample	Silver	Aluminum	Arsenic	Barium	Beryllium	Bismuth	Calcium	Cadmium	Cerium	Cobalt	Chromium	Cesium	Copper	Iron	Gallium	Germanium
Id.	Ag	Al	As	Ba	Be	Bi	Ca	Cd	Ce	Co	Cr	Cs	Cu	Fe	Ga	Ge
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.01	100	0.2	10	0.05	0.01	100	0.02	0.01	0.1	1	0.05	0.2	100	0.05	0.05
Crustal Abundance: Fron	0.037	4200	1	0.4	1	0.007	5100	0.035	11.5	0.1	2	0.4	4	3800	4	0.2
Crustal Abundance: To	0.11	88000	13	2300	3	0.01	312400	0.42	345	74	170	6	250	86500	30	8
125207	0.87	78300	3.9	370	0.82	1.33	35800	*0.01*	17.95	6.1	31	5.85	1630	28600	17.4	0.08
125228	1.9	80000	1.5	430	1.78	4.17	20800	*0.01*	17.1	4.2	56	2.23	2120	13800	18	0.08
125244	1.53	74600	1.6	170	1.54	4.68	18000	*0.01*	12.5	2.7	51	1.8	1700	9700	17.55	0.06
125257	0.09	86900	9.3	210	0.61	0.18	79000	0.15	12.8	33.3	126	0.31	102	55800	14.3	0.09
125278	0.42	97700	11.3	310	0.96	0.15	34500	0.05	18.75	10.6	17	1.65	351	39700	20	0.14
125596	1.21	88100	3.3	220	0.88	0.59	48900	0.02	20.4	12.5	12	9.66	2290	48000	20.3	0.1
125610	0.5	85700	3.5	130	0.82	0.74	26600	*0.01*	18.3	9.7	18	2.45	700	38700	19.5	0.08
125626																
125641	1.53	89200	2.7	140	0.83	2.05	35800	*0.01*	16.25	11.4	42	5.11	2290	47100	19.8	0.08
125669	0.42	84700	4.1	110	0.79	1.38	30200	*0.01*	19.05	18.4	37	3.4	3420	39700	18.6	0.08
125690	0.24	88100	4.3	270	0.78	0.11	36900	0.03	18	16.6	33	1.93	647	53900	18.35	0.07
West Breccia Zone																
14018	0.88	80300	15.5	1120	1.3	0.93	17800	0.02	26.5	12	24	5.11	1290	25800	17.8	0.09
14021	1.22	77000	24.5	460	1.03	0.86	26200	0.11	23.2	9.7	21	5.86	1740	18100	16.4	0.08
14036	1.43	74100	30.2	500	1	1.01	18400	*0.01*	23.8	16.6	20	8.17	1920	25600	16.2	0.18
14043	0.7	75600	10.9	230	1.03	0.4	14000	*0.01*	13.3	14.6	31	2.39	1330	28500	16.05	0.06
14060	0.87	79600	14.3	380	0.99	0.24	31400	*0.01*	23.7	15.4	26	4.87	2610	35900	16.25	0.09
14067	1.85	85100	17.3	370	0.95	0.18	25900	0.03	21.5	19.9	36	2.64	2460	42900	17.6	0.1
14076	1.32	90000	15.1	410	0.8	0.62	43400	0.61	22.6	23.3	33	5.75	1300	54600	18.05	0.12
14083	0.98	88500	13.9	700	0.78	0.86	40300	0.5	22.8	24	49	7.97	1360	57800	17.8	0.12
14099	1.36	72400	2.2	770	0.95	1.51	29500	1.16	21.3	6.4	16	9.67	1210	22300	15.1	0.07
14103	1.06	76000	5.6	250	1.06	1.02	29300	0.03	25.9	7.8	20	3.59	2630	21200	16.95	0.09
125046	0.64	82200	7.3	210	0.89	1.45	38600	0.93	15.95	11.9	35	3.67	1190	35500	21.8	0.14
125068	3.78	91500	7.9	440	0.85	5.55	42500	0.04	17.45	13	45	3.63	4990	43200	24	0.14
125073	9.94	82500	2.4	590	0.93	11.9	33500	0.02	22.5	7.7	27	6.32	8620	22000	22.1	0.13
125079	19.5	78800	19.4	1380	0.85	32.6	18500	1.65	31.4	4.7	37	3.23	15100	17600	19.05	0.14
125084	3.55	84900	10.2	800	0.99	12.35	37800	*0.01*	20.7	12.8	47	3.52	5890	39400	24	0.13
125127	1.14	87600	3.9	500	0.94	1.69	23600	*0.01*	16.95	12.3	35	2.84	1610	42400	22.9	0.13
125129	1.43	76500	3.3	270	0.68	2.86	17500	0.03	12.7	11.4	69	2.33	2860	33100	18.55	0.13
125134	1.24	79900	2.8	470	0.87	6.22	14500	*0.01*	19.2	16.9	58	1.62	6700	59100	22.2	0.17
125142	0.89	78500	2.2	310	0.96	3.9	20500	*0.01*	22.4	14.9	92	2.57	2610	41100	19.75	0.15
125149	0.98	85500	2.7	470	0.79	2.14	31600	*0.01*	19.85	13.9	32	2.43	2050	48600	18.75	0.1
125154	0.97	85800	5.7	150	1.91	0.96	23500	0.02	10.6	5.8	23	1.49	1055	13500	26.4	0.09
125165	1.88	97300	6.3	160	1.22	15.75	29500	0.02	25	6.3	14	3.34	2660	32100	20.8	0.08
125176	3.93	86000	5.1	240	0.88	9.31	25400	0.03	19.15	7.1	15	3.11	4490	36000	18.6	0.06
146112	0.92	92900	6.5	260	0.8	4.9	31600	*0.01*	27.3	7.7	30	3.16	1810	39000	20.7	0.08
146115	0.04	89100	3.3	550	0.75	0.02	71900	0.17	26	36	41	0.52	30.3	69100	17.1	0.12
146124	0.18	96300	2.8	570	0.72	0.11	40800	0.03	19.35	10.1	12	4.11	746	40500	20.8	0.08
146127	0.25	68000	2.3	510	1.08	0.18	25200	0.03	18.3	5.4	63	3.19	298	15700	16.55	0.06
146135	0.2	95600	7.7	490	0.68	0.51	41600	0.06	19.4	8.9	18	3.82	439	41600	21.1	0.08
146149	0.1	87600	4.4	470	0.66	0.04	41400	0.08	18.95	9	25	5.59	250	37200	20.2	0.08
146161	0.14	88900	24.3	690	0.48	0.33	64500	0.08	17.6	20.9	21	3.14	364	60400	20.2	0.1
146164	0.04	83700	8.3	510	0.53	*0.005*	35100	0.02	13.15	23.6	15	1.4	17.6	60600	19.65	0.08
145951	0.51	90200	6.5	290	0.66	1	42000	0.02	18.05	10.5	18	3.34	2100	41500	19.8	0.09
145956	0.22	83800	4.8	150	0.73	0.33	32500	0.03	16.4	17.6	27	3.87	2030	47400	20.9	0.09
145974	0.14	86700	2.6	230	0.72	0.21	25700	0.04	20.1	16.9	8	3.09	308	48700	21.7	0.09

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.
ME-MS61:Interference: Ca>10% on ICP-MS As ICP-AES results shown.

Sample	Silver	Aluminum	Arsenic	Barium	Beryllium	Bismuth	Calcium	Cadmium	Cerium	Cobalt	Chromium	Cesium	Copper	Iron	Gallium	Germanium
Id.	Ag	Al	As	Ba	Be	Bi	Ca	Cd	Ce	Co	Cr	Cs	Cu	Fe	Ga	Ge
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.01	100	0.2	10	0.05	0.01	100	0.02	0.01	0.1	1	0.05	0.2	100	0.05	0.05
Crustal Abundance: Fron	0.037	4200	1	0.4	1	0.007	5100	0.035	11.5	0.1	2	0.4	4	3800	4	0.2
Crustal Abundance: To	0.11	88000	13	2300	3	0.01	312400	0.42	345	74	170	6	250	86500	30	8
145982	0.08	90400	1.5	230	0.88	*0.005*	62000	0.23	32.8	27	23	0.77	15.7	57900	16.65	0.11
145992	0.74	77100	4	180	0.74	0.92	26800	0.04	14.8	12.3	31	2.17	1860	35600	20.3	0.07
145999	0.13	82700	4.5	160	0.66	0.12	35300	0.05	16.85	11.5	15	3.27	741	38600	19.75	0.08
145834	0.52	87500	9.8	150	0.82	0.39	30700	0.07	18.9	9.4	24	2.28	672	39200	21.2	0.08
145842	0.28	88400	24.1	30	1.08	7.68	78000	0.1	22.8	12.9	106	0.82	271	42600	25.1	0.08
145852	0.41	84100	17.1	40	1.1	3.5	43600	0.24	20.5	8.1	56	0.63	1280	29400	19.9	0.07
145857	0.08	94000	8.9	240	0.76	0.32	44700	0.03	18.8	8.1	31	2.8	97.6	29900	21.5	0.06
145871	0.15	88200	4.5	290	0.82	0.58	41700	0.07	20.6	9.2	30	4.06	367	39300	20.6	0.08
145608	0.4	91900	10.9	390	0.66	0.54	36900	0.07	16.1	20.1	28	2.31	664	60800	19.4	0.14
145614	1.58	90000	8.6	520	0.78	2.64	36200	0.17	19.6	22.6	33	2.43	1740	59600	19.4	0.12
145628	0.19	78900	11.7	80	0.48	0.19	36500	0.05	16.3	18.2	25	0.92	995	46100	16.9	0.11
145640	0.85	92100	8.2	420	0.76	0.51	44300	9.8	19.3	21.1	43	2.87	1340	57100	20.3	0.14
145646	0.87	89600	10.1	330	0.71	0.29	37000	0.08	19.15	25.1	31	1.97	1520	55900	18	0.13
Paramount Zone																
125965	1.01	88900	6.3	260	1.15	0.66	25600	0.06	22.7	13.4	68	1.16	3800	36800	20.8	0.09
125974	0.15	78700	6.6	300	1.08	0.49	18200	0.07	20.4	35.9	38	1.39	648	44700	19.75	0.09
125983	0.81	74200	8.1	520	1	0.17	37000	0.08	20.2	26.2	141	1.36	1670	48600	17.6	0.1
125988	0.08	93800	4.3	660	0.99	0.02	47600	0.13	36.5	29.5	46	0.6	48.9	58700	18.05	0.12
126007	1.11	79000	1.3	470	1.17	2.38	21300	0.16	16.8	3.5	81	3.37	1500	12600	19.1	0.06
126031	1.12	80000	1.2	850	1.22	1.38	18700	0.09	19.95	4.7	71	2.24	1480	15100	17.75	0.06
126040	0.44	86100	7.7	280	1.22	0.19	18400	0.06	23.7	15.1	101	1.2	2760	30400	20.2	0.07
126054	0.19	67400	2.2	410	1.06	0.47	48100	0.13	25.1	24.1	196	1.52	1620	47900	15	0.09
126067	0.92	75400	4.5	200	1.08	1.26	43600	0.07	21.4	21.1	123	2.16	2420	44300	18.5	0.09
126081	3.83	67400	2.9	1270	0.96	17.7	18600	0.06	10.75	6.9	108	3.49	6180	20500	16.4	0.16
126110	0.12	95700	5.8	840	1.06	0.1	48700	0.09	37.1	25.7	54	0.84	106	59900	18.85	0.1
126118	1.1	79000	4.7	330	0.95	1.83	35400	0.08	24.6	14.3	76	3.48	5740	40300	19.3	0.1
125904	1.51	91400	3.1	270	1.22	3.24	38500	0.19	24	8.7	17	2.4	3090	34700	23.1	0.11
125919	1.3	95400	3.3	240	0.9	1.67	22700	0.13	26.4	12.7	13	4.72	5040	43100	22.5	0.11
125928	1.36	82800	4.7	610	0.76	1.59	27800	1.59	18.15	18	38	2.92	1200	50100	21.1	0.09
125933	0.07	94200	3.2	510	1.18	0.03	38300	0.08	41.2	26.9	27	1.28	40.6	66800	19.35	0.13
125944	0.28	95900	4.9	610	0.64	0.14	33800	1.02	21.3	17.8	36	2.54	307	51300	19.75	0.09
125952	0.08	74900	2.4	390	1.15	0.18	29700	0.04	18.65	8	76	1.91	217	24000	17.7	0.09
125963	0.46	90800	4.3	400	0.9	0.17	35800	0.07	26.2	16	26	2.63	4100	53300	22	0.11
126120	2.37	85400	1	510	1.65	2.68	16400	0.03	14.1	3.7	85	3.04	2220	14400	20.7	0.05
126131	0.87	82400	3	450	1.6	1.11	24600	0.2	25.1	4	53	1.35	1010	10700	20.5	0.05
126142	0.64	82000	2.7	280	1.41	0.88	27600	0.71	22.9	5.6	50	1.64	791	16400	20.2	0.07
126154	1.98	83800	3.5	120	1.35	1.61	30100	0.1	27.3	7.3	37	1.69	2480	17700	24	0.08
126171	0.22	80000	2.4	990	1.09	0.18	33900	0.12	21.3	12	52	2.94	1840	30400	18.35	0.08
126181	0.34	97400	2.5	310	0.65	0.01	41800	0.06	18.65	16.9	44	1.69	240	49000	20.7	0.09
125806	0.29	79600	6.6	1060	1.44	0.22	25500	0.06	21.6	8.5	66	2.19	582	24800	16.65	0.07
125816	0.27	91800	8.2	1180	1.54	0.23	36800	0.46	40.6	20.5	27	0.94	71.4	64500	18.3	0.12
125833	2.55	77700	1.4	670	1.5	3.39	20800	0.09	14.1	3.8	94	3	3650	15900	18.65	0.08
125861	1.74	81900	1.2	750	1.66	2.98	19400	*0.01*	14.8	4.3	76	3.11	3140	13200	18.1	0.06
125875	2.09	73900	1	800	1.43	2.78	21800	*0.01*	18.35	3.5	71	2.29	2750	14800	16.65	0.07
125897	0.91	73800	4.1	250	1.43	0.62	21500	0.08	20.1	2.4	65	1.86	632	7400	19.3	0.07

Project:	**Schaft Creek**
Client:	Copper Fox Metals Inc.
Data:	**ICP Metals Data**
Comments:	2005 core samples were collected by MDAG on Feb 7'07. 2006 core samples were collected by Copper Fox personnel in Sep '07. Rare earth elements may not be totally soluble in MS61 method. ME-MS61:Interference: Ca>10% on ICP-MS As ICP-AES results shown.

Sample	Silver	Aluminum	Arsenic	Barium	Beryllium	Bismuth	Calcium	Cadmium	Cerium	Cobalt	Chromium	Cesium	Copper	Iron	Gallium	Germanium
Id.	Ag	Al	As	Ba	Be	Bi	Ca	Cd	Ce	Co	Cr	Cs	Cu	Fe	Ga	Ge
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.01	100	0.2	10	0.05	0.01	100	0.02	0.01	0.1	1	0.05	0.2	100	0.05	0.05
Crustal Abundance: Fron	0.037	4200	1	0.4	1	0.007	5100	0.035	11.5	0.1	2	0.4	4	3800	4	0.2
Crustal Abundance: To	0.11	88000	13	2300	3	0.01	312400	0.42	345	74	170	6	250	86500	30	8
Tailings																
LIARD ZONE	0.49	79200	4.8	290	0.77	0.81	34000	0.05	18.8	9.7	23	4.59	850	35400	18.45	0.11
PARAMOUNT	0.85	70400	5.2	430	1.11	1.85	26900	0.08	19.55	9.7	45	2.46	1300	25600	18.85	0.11
WEST BRECCIA	1.47	89400	7.8	460	0.98	2.51	28000	0.09	25.9	11.8	50	3.49	1790	37500	21.1	0.1
High-Sulphide Histor																
T112 (171' - 172')	0.68	71700	32.7	100	0.44	1.61	42100	0.13	10.85	116	16	0.51	209	107000	17.7	0.19
T113 (81' - 82')	0.19	86100	11.3	1370	1.4	0.13	8500	0.06	27.5	9.2	15	2.13	370	25800	20	0.12
T113 (983' - 985')	1.29	81100	16.2	200	1.17	1.19	24600	0.08	28.1	55.6	33	1.78	4260	42000	20	0.17
T140 (30' - 31')	1.48	98200	3.5	330	0.98	1.31	31000	0.07	16.7	12.7	*0.5*	8.75	4080	33400	24	0.16
T166 (389' - 390')	0.27	85800	1.7	490	1.49	0.23	16900	*0.01*	16.4	16.6	28	3.33	754	19600	21.4	0.12
T185 (116' - 117')	0.07	84800	6.4	430	1.36	0.22	9400	0.07	20.6	25	9	2.36	112.5	25500	18.2	0.13
T207 (261.5' - 262')	0.19	72400	2.9	220	1.1	1.14	10400	*0.01*	11.55	27	28	1.37	579	39600	18.45	0.16
T207 (269' - 271')	0.34	57200	8.4	190	0.79	1.81	9100	*0.01*	15	86.8	10	1.31	378	128500	14.25	0.21
All Data																
Maximum	19.5	102500	35.1	1380	2.27	32.6	79000	9.8	41.2	116	269	15	15100	128500	26.9	0.76
Minimum	0.04	57200	0.1	30	0.44	0.005	8500	0.01	7.62	2.4	0.5	0.31	15.7	7400	12.8	0.05
Mean	1.2	86247	5.12	394	0.91	1.67	35272	0.12	20.5	14.2	33.4	4.06	2319	39220	20.1	0.12
Standard Deviation	1.58	7345	5.06	275	0.28	3.05	11010	0.67	4.83	11.4	30.1	2.16	1829	15347	2.23	0.063
10 Percentile	0.19	76440	1.8	140	0.66	0.14	21000	0.01	15.1	6.04	9	1.56	325	17480	17.6	0.07
25 Percentile	0.42	81900	2.5	200	0.72	0.34	27750	0.01	17.8	8.45	15.5	2.44	1195	30150	18.7	0.08
Median	0.95	87200	3.5	310	0.85	0.86	36000	0.02	19.8	11.8	26	3.82	2030	39900	20.3	0.1
75 Percentile	1.48	91400	5.7	490	1.03	1.84	42000	0.06	22.8	16.6	43	5.17	3070	47400	21.4	0.13
90 Percentile	2.33	95020	9.6	760	1.24	3.34	46360	0.12	26.1	23.2	65.6	6.77	4652	56500	22.5	0.2
Interquartile Range (IC	1.06	9500	3.2	290	0.31	1.5	14250	0.05	4.95	8.15	27.5	2.73	1875	17250	2.67	0.05
Variance	2.49	53951819	25.6	75802	0.076	9.32	121218762	0.44	23.3	130	903	4.65	3346571	235534000	4.96	0.004
Skewness	7.6	-0.63	3.21	1.55	1.46	6.07	0.46	13.4	1.02	4.8	3.46	1.04	2.15	0.94	-0.31	5.09
Coefficient of Variatior	1.32	0.085	0.99	0.7	0.3	1.83	0.31	5.77	0.24	0.8	0.9	0.53	0.79	0.39	0.11	0.54
Count	235	235	235	235	235	235	235	235	235	235	235	235	235	235	235	235
Main Zone																
Maximum	3.96	102500	35.1	1310	2.27	8.5	79000	0.15	35.1	57.5	269	15	7630	66900	26.9	0.76
Minimum	0.06	68500	0.1	90	0.46	0.02	17400	0.01	7.62	2.7	3	0.31	54.4	9700	12.8	0.05
Mean	1.19	87793	3.82	359	0.86	1.3	37540	0.023	20.1	12.8	27.2	4.77	2543	39346	20.4	0.13
Standard Deviation	0.82	6427	3.39	261	0.25	1.39	9054	0.026	3.99	7.35	27	2.06	1508	12385	2.1	0.075
10 Percentile	0.31	79700	1.75	130	0.64	0.17	25500	0.01	15.5	6.4	6	2.33	726	19050	18.3	0.08
25 Percentile	0.54	83825	2.3	180	0.7	0.43	33550	0.01	17.9	8.62	12.2	3.58	1630	33575	19.4	0.09
Median	1.04	88300	3.1	280	0.81	0.82	37600	0.01	19.8	11.1	21.5	4.8	2245	40850	20.7	0.11
75 Percentile	1.65	92450	4.4	430	0.94	1.74	42650	0.03	22.3	15.3	37	5.62	3275	47250	21.5	0.14
90 Percentile	2.4	95250	6.35	725	1.1	2.49	47350	0.05	25.2	19.4	48.5	7.08	4770	53750	22.6	0.22
Interquartile Range (IC	1.11	8625	2.1	250	0.24	1.31	9100	0.02	4.41	6.7	24.8	2.04	1645	13675	2.08	0.048
Variance	0.68	41308091	11.5	67895	0.063	1.93	81980494	0.00066	16	54	732	4.24	2273457	153384569	4.41	0.0056
Skewness	1.07	-0.55	5.94	1.73	2.26	2.38	0.5	2.63	0.38	2.64	5.41	1.12	0.94	-0.48	-0.79	4.71
Coefficient of Variatior	0.69	0.073	0.89	0.73	0.29	1.07	0.24	1.09	0.2	0.57	0.99	0.43	0.59	0.31	0.1	0.58
Count	146	146	146	146	146	146	146	146	146	146	146	146	146	146	146	146

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.
ME-MS61:Interference: Ca>10% on ICP-MS As ICP-AES results shown.

Sample	Silver	Aluminum	Arsenic	Barium	Beryllium	Bismuth	Calcium	Cadmium	Cerium	Cobalt	Chromium	Cesium	Copper	Iron	Gallium	Germanium
Id.	Ag	Al	As	Ba	Be	Bi	Ca	Cd	Ce	Co	Cr	Cs	Cu	Fe	Ga	Ge
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.01	100	0.2	10	0.05	0.01	100	0.02	0.01	0.1	1	0.05	0.2	100	0.05	0.05
Crustal Abundance: Fron	0.037	4200	1	0.4	1	0.007	5100	0.035	11.5	0.1	2	0.4	4	3800	4	0.2
Crustal Abundance: To	0.11	88000	13	2300	3	0.01	312400	0.42	345	74	170	6	250	86500	30	8
West Breccia Zone																
Maximum	19.5	97300	30.2	1380	1.91	32.6	78000	9.8	32.8	36	106	9.67	15100	69100	26.4	0.18
Minimum	0.04	68000	1.5	30	0.48	0.005	14000	0.01	10.6	4.7	8	0.52	15.7	13500	15.1	0.06
Mean	1.5	84964	9.07	403	0.87	2.97	34877	0.36	20.2	14.1	33.2	3.38	2077	40213	19.7	0.1
Standard Deviation	3.12	6669	6.91	260	0.24	5.7	13677	1.44	4.49	6.77	19.4	1.94	2630	13797	2.5	0.03
10 Percentile	0.12	76300	2.52	150	0.66	0.12	18460	0.01	15.5	6.82	15	1.21	263	21680	16.5	0.07
25 Percentile	0.21	79750	3.95	230	0.72	0.3	25800	0.02	17.5	8.95	21	2.32	668	31000	17.8	0.08
Median	0.87	85800	7.3	380	0.82	0.86	33500	0.04	19.4	12.3	30	3.14	1340	39400	19.8	0.09
75 Percentile	1.28	89800	11.3	505	0.98	2.75	41500	0.09	22.7	17.9	36.5	3.84	2280	48650	21	0.13
90 Percentile	2.55	92420	18.1	694	1.08	8.33	44460	0.54	25.9	23.4	56.8	5.79	4690	59300	22.5	0.14
Interquartile Range (IC	1.07	10050	7.35	275	0.25	2.44	15700	0.07	5.18	8.95	15.5	1.52	1612	17650	3.2	0.05
Variance	9.74	44478881	47.8	67727	0.055	32.5	187058353	2.08	20.1	45.8	378	3.77	6919367	190362877	6.27	0.00091
Skewness	4.79	-0.36	1.31	1.57	1.92	3.63	1.19	6.37	0.54	0.98	1.92	1.26	3.24	0.016	0.45	0.61
Coefficient of Variatior	2.08	0.078	0.76	0.65	0.27	1.92	0.39	4.03	0.22	0.48	0.59	0.58	1.27	0.34	0.13	0.3
Count	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47
Paramount Zone																
Maximum	3.83	97400	8.2	1270	1.66	17.7	48700	1.59	41.2	35.9	196	4.72	6180	66800	24	0.16
Minimum	0.07	67400	1	120	0.64	0.01	16400	0.01	10.8	2.4	13	0.6	40.6	7400	15	0.05
Mean	0.97	83248	3.84	542	1.18	1.62	29935	0.2	23	13.6	66.3	2.16	1980	34268	19.3	0.089
Standard Deviation	0.89	8474	2.13	302	0.28	3.17	9834	0.33	7.34	9.16	38.9	0.95	1721	18024	2.02	0.024
10 Percentile	0.12	73900	1.2	250	0.9	0.1	18600	0.04	14.8	3.7	27	1.16	106	13200	16.6	0.06
25 Percentile	0.28	78200	2.4	290	1	0.18	21400	0.06	18.6	5.15	38	1.38	607	16150	18.1	0.07
Median	0.87	82000	3.3	470	1.15	0.66	27800	0.08	21.4	12.7	65	2.16	1620	34700	19.3	0.09
75 Percentile	1.33	91100	4.8	710	1.42	1.75	36900	0.13	25.1	19.2	78.5	2.93	2925	48800	20.6	0.1
90 Percentile	2.09	95400	6.6	990	1.54	2.98	43600	0.46	36.5	26.2	108	3.37	4100	58700	22	0.12
Interquartile Range (IC	1.06	12900	2.4	420	0.42	1.57	15500	0.07	6.45	14.1	40.5	1.55	2318	32650	2.52	0.03
Variance	0.79	71812581	4.54	91187	0.076	10	96710366	0.11	53.8	83.9	1510	0.9	2961043	324848925	4.06	0.0006
Skewness	1.39	0.054	0.57	0.87	-0.0022	4.62	0.44	3.22	1.1	0.66	1.42	0.57	0.88	0.16	0.27	0.74
Coefficient of Variatior	0.91	0.1	0.55	0.56	0.23	1.95	0.33	1.69	0.32	0.67	0.59	0.44	0.87	0.53	0.1	0.28
Count	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.
ME-MS61:Interference: Ca>10% on ICP-MS As ICP-AES results shown.

Sample	Silver	Aluminum	Arsenic	Barium	Beryllium	Bismuth	Calcium	Cadmium	Cerium	Cobalt	Chromium	Cesium	Copper	Iron	Gallium	Germanium
Id.	Ag	Al	As	Ba	Be	Bi	Ca	Cd	Ce	Co	Cr	Cs	Cu	Fe	Ga	Ge
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.01	100	0.2	10	0.05	0.01	100	0.02	0.01	0.1	1	0.05	0.2	100	0.05	0.05
Crustal Abundance: Fron	0.037	4200	1	0.4	1	0.007	5100	0.035	11.5	0.1	2	0.4	4	3800	4	0.2
Crustal Abundance: To	0.11	88000	13	2300	3	0.01	312400	0.42	345	74	170	6	250	86500	30	8
Tailings																
Maximum	1.47	89400	7.8	460	1.11	2.51	34000	0.09	25.9	11.8	50	4.59	1790	37500	21.1	0.11
Minimum	0.49	70400	4.8	290	0.77	0.81	26900	0.05	18.8	9.7	23	2.46	850	25600	18.4	0.1
Mean	0.94	79667	5.93	393	0.95	1.72	29633	0.073	21.4	10.4	39.3	3.51	1313	32833	19.5	0.11
Standard Deviation	0.5	9509	1.63	90.7	0.17	0.86	3821	0.021	3.9	1.21	14.4	1.07	470	6352	1.43	0.0058
10 Percentile	0.56	72160	4.88	318	0.81	1.02	27120	0.056	19	9.7	27.4	2.67	940	27560	18.5	0.1
25 Percentile	0.67	74800	5	360	0.88	1.33	27450	0.065	19.2	9.7	34	2.98	1075	30500	18.6	0.11
Median	0.85	79200	5.2	430	0.98	1.85	28000	0.08	19.6	9.7	45	3.49	1300	35400	18.8	0.11
75 Percentile	1.16	84300	6.5	445	1.04	2.18	31000	0.085	22.7	10.8	47.5	4.04	1545	36450	20	0.11
90 Percentile	1.35	87360	7.28	454	1.08	2.38	32800	0.088	24.6	11.4	49	4.37	1692	37080	20.7	0.11
Interquartile Range (IC	0.49	9500	1.5	85	0.17	0.85	3550	0.02	3.55	1.05	13.5	1.06	470	5950	1.33	0.005
Variance	0.25	90413333	2.65	8233	0.029	0.73	14603333	0.00043	15.2	1.47	206	1.13	221033	40343333	2.04	0.000033
Skewness	0.76	0.22	1.62	-1.52	-0.68	-0.65	1.57	-1.29	1.66	1.73	-1.5	0.099	0.13	-1.52	1.58	-1.73
Coefficient of Variatior	0.53	0.12	0.27	0.23	0.18	0.5	0.13	0.28	0.18	0.12	0.37	0.3	0.36	0.19	0.073	0.054
Count	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
High-Sulphide Histor																
Maximum	1.48	98200	32.7	1370	1.49	1.81	42100	0.13	28.1	116	33	8.75	4260	128500	24	0.21
Minimum	0.07	57200	1.7	100	0.44	0.13	8500	0.01	10.8	9.2	0.5	0.51	112	19600	14.2	0.12
Mean	0.56	79662	10.4	416	1.09	0.96	19000	0.055	18.3	43.6	17.4	2.69	1343	52675	19.2	0.16
Standard Deviation	0.54	12375	10.2	407	0.35	0.67	12466	0.043	6.59	39.2	11.3	2.59	1757	41251	2.86	0.033
10 Percentile	0.15	67350	2.54	163	0.68	0.19	8920	0.01	11.3	11.6	6.45	1.07	180	23730	16.7	0.12
25 Percentile	0.19	72225	3.35	198	0.93	0.23	9325	0.01	14.1	15.6	9.75	1.36	330	25725	18.1	0.13
Median	0.31	82950	7.4	275	1.14	1.16	13650	0.065	16.5	26	15.5	1.96	478	36500	19.2	0.16
75 Percentile	0.83	85875	12.5	445	1.37	1.38	26200	0.073	22.3	63.4	28	2.6	1586	58250	20.4	0.18
90 Percentile	1.35	89730	21.2	754	1.43	1.67	34330	0.095	27.7	95.6	29.5	4.96	4134	113450	22.2	0.2
Interquartile Range (IC	0.64	13650	9.18	248	0.44	1.16	16875	0.063	8.19	47.8	18.2	1.25	1256	32525	2.28	0.048
Variance	0.29	153131250	104	165598	0.12	0.45	155394286	0.0018	43.4	1534	127	6.68	3086959	1701682143	8.21	0.0011
Skewness	1.08	-0.52	1.75	2.28	-0.85	-0.24	1.04	0.42	0.62	1.14	0.032	2.27	1.39	1.38	-0.1	0.29
Coefficient of Variatior	0.96	0.16	0.98	0.98	0.32	0.7	0.66	0.78	0.36	0.9	0.65	0.96	1.31	0.78	0.15	0.21
Count	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8

$\boxed{19.5}$ NOTE: if data is boxed, then data is 3 times the maximum crustal abundance.

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile
[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

NOTE: If data was reported as > detection limit the detection limit is shown in bold and was used in subsequent calculations.

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07. 2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.
Tailings: Detection limits on samples requiring dilutions for Hg-CV41 due to inteferences or high concentration levels have been increased according to the dilution factor.

Sample	Hafnium	Mercury	Indium	Potassium	Lanthanum	Lithium	Magnesium	Manganese	Molybdenum	Sodium	Niobium	Nickel	Phosphorus	Lead	Rubidium	Rhenium
Id.	Hf	Hg	In	K	La	Li	Mg	Mn	Mo	Na	Nb	Ni	P	Pb	Rb	Re
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	Hg-CV41	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.1	0.01	0.005	100	0.5	0.2	100	5	0.05	100	0.1	0.2	10	0.5	0.1	0.002
Crustal Abundance: Fron	0.3	0.03	0.01	40	10	5	1600	390	0.2	400	0.3	2	170	1	0.2	NA
Crustal Abundance: To	11	0.4	0.26	48000	115	66	47000	6700	27	40400	35	225	1500	80	170	NA
Main Zone																
14130	0.7	0.02	0.026	18100	6.3	3.5	10200	191	80.8	38300	3.8	4.1	1390	3.8	54.2	0.073
14144	0.7	0.01	0.05	15600	8.7	8.3	11600	451	72.5	34900	5.1	4.2	1830	4.7	47.1	0.049
14148	1	0.02	0.042	20600	10.6	13.3	18900	429	257	13800	4.2	5.5	1220	3.2	61.2	0.221
14156	1.6	*0.005*	0.027	12200	10.8	7	7900	339	77.8	37400	4.5	8.1	500	2.5	37.7	0.02
14162	1.9	*0.005*	0.062	16000	11.8	17.6	26200	853	479	19300	4.5	35	980	5.3	47.1	0.145
14169	1.4	0.02	0.036	9700	2.8	3.5	4000	278	176.5	47600	3.9	5.9	550	7.1	28.5	0.043
14232	0.9	0.01	0.05	16800	9.7	7.4	9100	189	97.4	42800	4.5	2.7	1430	2.5	55.2	0.09
14250	0.8	0.01	0.053	14600	11	15	18800	436	374	38300	4.3	2.5	1450	3.3	57.8	0.346
14260	0.8	0.01	0.09	15900	9.7	7.2	13900	275	173	38600	4	2.8	1390	3.8	61.3	0.145
14276	1.2	*0.005*	0.073	7600	9.1	11.6	16400	1085	22.8	40800	4.4	1.7	1440	6.7	20.9	0.008
14295	0.9	0.02	0.054	16000	8.3	12.1	15500	436	11.9	33600	4.1	4.5	1360	4.4	63.7	0.002
14301	1.4	0.01	0.058	19200	8.5	10.3	12400	517	215	27300	4.4	4.2	1380	3.6	56.5	0.137
14323	1	*0.005*	0.037	18200	8.9	7.5	9600	386	67.7	35000	4.6	2.2	1410	2.7	48.2	0.05
14332	1.1	0.01	0.055	20200	10.7	8.2	10400	281	102	32400	4.6	2.6	1470	2.8	64.7	0.072
14345	0.8	*0.005*	0.053	24000	12.1	6.9	10300	150	250	36900	3.9	3.1	1380	2.3	80.6	0.15
14348	0.9	0.01	0.053	18700	10.9	11.3	12100	191	170.5	38200	4.4	3	1520	2.3	65.9	0.135
14797	0.9	0.01	0.029	19500	6.4	16	15200	559	212	26700	4.6	4.2	1330	3.3	54.7	0.147
14808	1.2	0.06	0.037	20800	10.1	11.8	16300	493	580	20000	4	4.6	1080	7.6	83.3	0.936
14816	0.8	0.02	0.068	20900	7.8	9.4	17000	438	52.3	26700	4.9	5.2	1230	2.8	59.1	0.052
14828	0.8	0.03	0.032	17500	10.7	10.2	18200	507	182.5	32900	5	3.9	1280	5.9	65.3	0.119
14844	1.1	0.02	0.032	16900	6.9	26.3	37900	319	128	24600	5.9	23.4	1290	2.7	63.3	0.143
14680	1.8	0.02	0.035	16000	12.7	18.9	16500	493	500	34600	5.1	5.5	1300	5.4	84.9	0.326
14871	1	0.01	0.042	12300	8.7	12.3	19200	374	240	44300	5.9	7.3	1230	2.7	65.6	0.109
14887	1.1	0.01	0.042	11700	10.7	13	24700	613	8.29	35400	5.8	10.6	1200	2.8	51.1	0.003
14689	1.4	*0.005*	0.029	16400	14.4	3.3	5600	301	84.7	34300	2.7	6.4	540	1.6	42.9	0.065
14695	1.8	0.01	*0.0025*	22100	12.5	5.8	15100	611	641	30000	4.7	7.6	1400	3.4	83.4	0.499
14742	1.4	0.01	0.019	12800	8.2	11.2	22400	401	661	43600	5.4	16.2	1220	20.6	62	0.436
14666	1	*0.005*	0.048	12900	8.7	27.7	22000	543	28.4	35800	7	15.5	1250	2.2	42.3	0.04
14685	1	0.04	0.058	12100	9.5	25.9	27300	364	120	32000	4.5	9.1	1530	2.8	47.7	0.113
14685B	1.4	0.04	0.056	13200	8.7	24.9	28400	327	77.4	33900	4.3	7.9	1530	2.4	67.7	0.088
14545	1.5	*0.005*	0.055	11800	11	7.9	14000	273	14.05	35000	5.5	1.3	1330	2.4	52.5	0.004
14565	1.2	*0.005*	0.069	18600	10.1	9.9	12100	529	12.65	29900	5.1	1.6	1270	2.3	67.6	0.011
14571	1.4	0.01	0.058	14200	9.7	6.4	11700	230	101	32200	4.2	4.7	1030	3.6	53.4	0.062
14578	1.6	0.01	0.027	15800	10.1	7.6	11800	337	27	31500	5	6.7	1550	2.8	53.5	0.033
14578B	2.2	0.01	0.028	15800	9.4	8.2	12700	345	31.3	32900	4.9	5.8	1470	2.4	58.1	0.04
14598	0.7	*0.005*	0.022	12400	6.5	14.1	22100	631	53.3	31400	5.9	3.9	1540	2.3	26.5	0.071
14893	1.5	0.01	0.034	10200	9	16.7	27200	493	101	36600	6.5	19.8	1260	3.1	52.4	0.033
14899	0.9	0.01	0.024	7700	7	26.2	41300	546	19.2	34100	6.1	22.1	1260	3.3	18.9	0.014
14908	1.4	*0.005*	0.042	13700	9	17	24000	527	102.5	44700	7.1	18.7	1310	2.8	41.1	0.082
14917	2.3	0.01	0.023	16100	11	21.2	18300	379	17.15	47300	4.6	8.4	1100	3.8	50.4	0.01
14925	1.2	0.01	0.045	15400	7.8	16.2	20400	408	27.5	35600	6.8	16	1230	2.5	55	0.009
14998	0.9	0.01	0.036	12500	8.6	14.9	16300	452	65.2	41400	4.8	2.2	1440	2.5	42.7	0.035
15862	0.7	0.01	0.027	14800	8.2	12.4	17400	584	74	34400	5	4.4	1260	2.4	40.8	0.042
15870	1	*0.005*	0.035	18500	9.9	7.4	17700	539	17.9	26200	5.6	12.4	1120	3.2	70.5	0.01
15879	1.2	0.01	0.035	14900	9.4	10.4	18800	554	20	32900	6.9	15.3	1280	3.8	56.7	0.018

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07. 2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.
Tailings: Detection limits on samples requiring dilutions for Hg-CV41 due to inteferences or high concentration levels have been increased according to the dilution factor.

Sample	Hafnium	Mercury	Indium	Potassium	Lanthanum	Lithium	Magnesium	Manganese	Molybdenum	Sodium	Niobium	Nickel	Phosphorus	Lead	Rubidium	Rhenium
Id.	Hf	Hg	In	K	La	Li	Mg	Mn	Mo	Na	Nb	Ni	P	Pb	Rb	Re
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	Hg-CV41	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.1	0.01	0.005	100	0.5	0.2	100	5	0.05	100	0.1	0.2	10	0.5	0.1	0.002
Crustal Abundance: Fron	0.3	0.03	0.01	40	10	5	1600	390	0.2	400	0.3	2	170	1	0.2	NA
Crustal Abundance: To	11	0.4	0.26	48000	115	66	47000	6700	27	40400	35	225	1500	80	170	NA
15887	1	0.01	0.044	11900	6.7	11.3	15900	395	165.5	39300	6.5	11.6	1090	3.5	39.8	0.213
15891	0.9	0.01	0.021	17200	7.7	10.8	17300	558	104	34900	5.4	10.8	1120	3.6	60.8	0.08
15908	1	0.03	0.039	18000	8.4	10.9	18500	433	311	29000	6.1	12.6	1130	2.8	69.3	0.226
15911	1	0.02	0.027	13800	9.2	11.6	23100	402	154	32500	6.6	17.7	1250	2.5	69.5	0.135
125285	0.7	0.02	0.033	18600	5.1	11.6	19400	256	16.3	33500	3.8	8.2	1230	3	37.1	0.01
125288	2	0.01	0.051	8500	12.5	30.2	64300	1070	0.82	13600	4.8	175.5	860	4.7	18.8	0.002
125293	1	0.02	0.031	11100	6.1	15.1	26500	341	221	34600	3.5	23.2	1250	2.9	26.8	0.117
125305	0.7	0.02	0.018	18300	9.3	8	20200	279	56.5	35400	4	8.3	1270	3.2	55.8	0.029
125311	0.6	0.01	0.007	20200	6.4	6.1	13800	192	22.1	35400	3.7	4.6	1260	3.3	51.1	0.013
125703	0.8	0.01	0.04	22500	7.2	6.9	13100	456	249	23100	4.4	4.2	1300	2.8	59.5	0.2
125728	0.9	0.01	0.043	12500	9.3	12.9	20100	363	139	33700	5.7	17.5	1190	3.8	51.3	0.099
125755	1.5	0.01	0.02	19600	7.1	2.9	5300	89	533	27300	2	5.8	440	2.6	52.4	0.361
125772	1	0.01	0.03	13700	9.2	13	20200	422	448	30800	5.5	14.1	1110	3.2	65	0.388
125795	0.9	0.01	0.046	15500	9.1	10.1	19800	712	17.8	25400	5.6	13.5	1150	2.6	60.7	0.009
125422	0.8	0.01	0.048	14900	10.7	11.9	16300	391	14.4	34200	4.3	2.4	1360	3	56.7	0.011
125435	0.7	0.01	0.07	15100	9.5	12.9	13300	359	203	33000	4.1	3	1260	2.8	58.2	0.169
125452	0.9	0.03	0.07	13400	9.1	15.9	15200	306	315	36000	3.8	3.9	1380	4.2	62.4	0.194
125476	1.7	0.01	0.021	17800	7	3.5	7600	183	112	23500	2.4	6.3	470	2	59	0.022
125490	0.9	0.01	0.07	16200	10.7	15.2	19800	415	5.87	30000	3.9	4.9	1300	2.9	67.3	0.002
126192	1	0.01	0.044	11200	9	11.1	9900	389	49.9	45100	5.4	2.2	1540	2.5	33.4	0.027
126206	0.6	0.01	0.029	12700	10.3	9.9	11500	331	125	39400	5.8	3	1840	2.2	44.1	0.078
126225	0.8	0.01	0.043	14900	7.5	5.9	7300	369	282	41000	5.6	2.6	1670	2.1	42.7	0.193
126244	0.9	0.01	0.052	19800	7.6	6.4	12300	492	296	35400	5.5	1.8	1380	2	47.2	0.092
126266	1	*0.005*	0.047	20800	8.4	7	12900	493	125	33000	5.8	1.9	1490	1.7	59	0.057
126279	0.9	0.01	0.055	16300	5.5	7.8	10500	554	190	35300	5.1	2.8	1320	1.6	35.2	0.061
126288	1	0.01	0.043	21000	7.1	5.4	10500	358	254	31000	5.4	1.8	1310	1.7	63	0.132
126297	1.6	0.01	0.053	17400	13.1	7	17400	514	115	26800	4.4	8.8	1420	2.6	64.1	0.095
126314	0.7	0.01	0.092	22100	8.4	7.9	15000	410	104.5	24200	3.8	4.5	1300	1.9	64.9	0.065
126329	0.9	0.01	0.044	17400	10	8.7	12900	438	58.5	24600	5.5	4.2	1270	1.8	42.7	0.041
126337	1	0.01	0.077	16500	8.9	6.3	17000	366	240	28700	4.7	5.4	1320	2.3	50.7	0.195
126351	0.9	0.01	0.026	16400	8.9	5.5	15400	395	70.7	30500	4.7	4.6	1330	2.3	58.1	0.06
126427	1.7	0.01	0.144	15900	8.7	13.3	23700	1150	3.29	19700	2.8	15.1	1080	3.3	52.7	0.002
126430	1	*0.005*	0.048	14400	11.8	11.9	17300	733	1.58	32800	5.4	2.2	1580	2.1	52.6	0.002
126434	1	*0.005*	0.064	13500	8.1	12.4	11000	520	1	34100	5.9	2.1	1440	2.6	47.9	*0.001*
126443	1.5	0.02	0.05	16100	10	11.9	14700	624	1.82	28400	4.9	4.4	1480	3	65.6	0.003
126449	3.2	*0.005*	0.061	5100	16.8	39.5	38400	1155	1.38	22800	6.8	41.7	1240	4.7	10.1	0.002
126464	1.2	0.01	0.05	14700	11.8	14.1	14200	602	11.2	28100	5.5	2.8	1400	2.9	58.6	0.009
126492	1.2	*0.005*	0.069	16400	9.6	12.7	14700	420	46.9	28600	5.6	2.4	1430	2	69.2	0.03
145655	1.6	*0.005*	0.083	13200	12	9.1	14600	506	2.48	31900	5.4	2.3	1400	2.5	57.2	0.002
145669	1.3	0.01	0.083	13800	10.4	7.4	14400	537	3.66	32500	6.2	5.5	1440	2	60.4	*0.001*
145685	0.8	*0.005*	0.076	15400	7.3	10.2	17000	660	4.96	29900	5.3	6.9	1180	1.9	43.2	0.002
145694	0.8	0.01	0.078	12900	6.8	10	17300	561	23.7	34900	5.6	10.3	1210	1.9	37.4	0.014
145708	1.4	*0.005*	0.081	13000	9.2	10.4	11400	448	16.2	37100	8.2	3.1	950	1.7	57	0.008
145723	1.1	0.01	0.063	15000	7.3	8.3	11600	305	106	27800	5.5	2.7	1210	3.8	51.6	0.093
146798	0.7	0.02	0.058	15600	8.4	11.3	13500	535	179	32500	4.7	3.9	1250	3.5	43.2	0.233
146824	1.1	0.01	0.071	10100	9.6	18.5	23900	432	43	40700	6.7	21.3	1300	3.2	47.3	0.044

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07. 2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.
Tailings: Detection limits on samples requiring dilutions for Hg-CV41 due to inteferences or high concentration levels have been increased according to the dilution factor.

Sample	Hafnium	Mercury	Indium	Potassium	Lanthanum	Lithium	Magnesium	Manganese	Molybdenum	Sodium	Niobium	Nickel	Phosphorus	Lead	Rubidium	Rhenium
Id.	Hf	Hg	In	K	La	Li	Mg	Mn	Mo	Na	Nb	Ni	P	Pb	Rb	Re
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	Hg-CV41	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.1	0.01	0.005	100	0.5	0.2	100	5	0.05	100	0.1	0.2	10	0.5	0.1	0.002
Crustal Abundance: Fron	0.3	0.03	0.01	40	10	5	1600	390	0.2	400	0.3	2	170	1	0.2	NA
Crustal Abundance: To	11	0.4	0.26	48000	115	66	47000	6700	27	40400	35	225	1500	80	170	NA
146831	1.1	0.04	0.058	11000	9.2	27.6	27100	467	216	31900	5.3	15.1	1190	5.2	54	0.146
146843																
146861	1	*0.005*	0.054	11900	11	15.7	16600	312	138.5	34400	5.7	1.6	1310	2.5	49	0.138
146868	1.2	0.01	0.048	15200	10.7	12.2	14400	189	67.2	30500	5.4	1.8	1270	2.2	77.4	0.035
126352	1.6	0.01	0.075	12600	10.6	24	23400	390	248	39700	7.3	17.5	1290	2.5	58	0.303
126358	1.6	0.01	0.074	13500	8.7	19.7	20400	384	70.1	39800	7.4	16.4	1290	2.1	63.7	0.034
126374	1.5	*0.005*	0.051	9200	10.1	15.3	22500	483	26.4	35500	7.2	17.5	1350	1.8	45.2	0.041
126384	1.6	*0.005*	0.046	9900	10.5	9.8	15600	433	33.5	32100	8	4.9	930	1.8	49.5	0.04
126391	1.3	0.01	0.057	9500	8.1	11.9	17700	402	139.5	31100	5.7	2.8	1080	1.9	44.3	0.106
146172	0.9	0.01	0.053	14400	6.6	9.6	13800	411	267	31100	3.9	4	1140	2.8	35.9	0.368
146182	0.7	0.02	0.043	11700	8.4	26.5	18900	392	79.8	29500	4	3.9	1300	2	35.6	0.116
146203	0.8	0.01	0.045	13600	6.3	17.5	15700	427	74.3	36500	4	4	1270	1.9	51	0.072
146214	0.9	0.01	0.075	12900	9	15.6	14000	464	29.8	34200	4.8	4	1260	1.6	43.6	0.011
146221	1.5	0.02	0.086	11700	12.1	19.4	24300	424	25	32400	4.4	7	1490	3.5	62.7	0.011
146238	1.1	0.01	0.065	12300	10.2	17.9	21500	545	11.2	33400	7.1	15.4	1280	2.1	47.7	0.003
147034	0.9	0.02	*0.0025*	20500	9.9	7.6	9800	230	568	30600	4.1	3.1	1350	7.3	68.7	0.376
147038	1.7	0.01	0.05	15900	9.3	6.8	10800	172	137	29500	3.3	6.6	800	6.5	48	0.09
147051	1.5	0.01	0.077	14800	12.1	14.5	15800	250	80.4	29100	5	5.4	1390	2.8	67.9	0.02
147070	0.8	0.01	0.108	8500	14.1	24.7	19100	702	2.05	32500	5	2.3	1550	3.6	35.2	*0.001*
147087	0.7	0.01	0.068	6100	9.9	18.7	17900	485	3.14	38000	4.6	6.9	1240	3.8	27.9	*0.001*
147097	0.7	0.01	0.087	21400	12.5	11.7	15700	549	2.96	27500	4.2	2.2	1320	3.4	78	*0.001*
145508	1.4	0.01	0.022	7700	5.7	28.7	39900	557	17.75	34600	6	21.1	1150	2.2	20.4	0.009
145527	1.5	0.01	0.056	16400	11.3	11.4	15500	409	15.2	34400	7.6	14	1240	3	71.6	0.007
145543	1.3	0.02	0.042	14600	9.2	17.7	17100	352	120	35000	6.9	15.3	1210	2.2	60.3	0.075
145562	1.1	0.01	0.031	15200	9.7	15.2	17000	418	141.5	32900	6.5	14.9	1200	2.2	76.7	0.095
145576	1.7	0.01	0.035	20800	8.6	3	5900	84	1095	31600	2.6	5.8	460	3.8	60.5	0.766
145601	1.4	0.03	0.057	13500	11.1	15.7	19500	703	93.8	36800	7.2	12.8	1310	2.9	64.1	0.065
146297	1	0.02	0.039	15300	9.2	17	19700	341	144	28600	3.4	4.8	1240	2.8	59	0.095
146314	0.8	0.01	0.037	12100	7.8	16.9	16700	444	90.7	29800	4.2	3.6	1340	3.6	41.6	0.058
146335	0.7	0.04	0.05	17600	10.3	6.5	13700	459	33	27900	4.9	3	1300	9.7	55.5	0.027
146352	0.7	*0.005*	0.04	8600	8	13.4	15500	423	26.6	32200	4.2	2.8	1220	2.3	18.5	0.018
146368	0.6	*0.005*	0.039	13500	6.6	9.6	14200	532	27.5	28600	4.5	3.3	1350	2.4	23.4	0.023
146390	0.6	0.01	0.038	11500	11.6	8	15400	468	36.1	32300	4.6	3	1440	4.8	37.8	0.028
146508	0.9	0.01	0.029	23000	8.8	16.9	24500	355	24.2	29000	6.7	20.4	1190	4.8	78.9	0.009
146526	0.5	0.03	0.024	14900	10.5	21.5	15600	287	5.01	33400	4.7	5.1	1260	4	44.7	0.004
146544	1	0.01	0.02	16400	6.9	6.9	11400	362	10.25	31900	3.6	6.3	870	2.9	46.9	0.003
146565	1	0.01	0.014	23100	8.5	4.6	11600	275	82.9	26900	3.9	4.1	1630	2.8	65.2	0.058
146589	1.1	0.01	0.022	15900	8.6	10.9	17000	319	352	26600	6.3	16.2	1130	2.6	60	0.306
146613	1.2	0.04	0.067	8100	7.7	13.3	15400	497	429	49400	6.5	8	1180	5.3	32.2	0.164
146627	0.7	0.03	0.027	12100	8.4	7.7	15900	389	42.5	24100	3.2	4.5	930	2.9	37.7	0.055
146637	1.6	0.01	0.084	23100	7.6	2.5	11000	301	238	20800	3.7	7.8	640	3.6	64.6	0.079
146649	1.6	*0.005*	0.03	15400	10.7	3.8	9700	247	88.5	34100	4.6	8.2	560	3.6	36.5	0.06
146657	1.4	0.01	0.034	12200	4.9	5.3	7900	258	104	39700	4.5	5.2	550	2.6	35.9	0.024
146676	1.4	0.01	0.057	14200	4.7	7.9	8900	456	90.3	47900	4.5	4.6	1500	3.4	35.2	0.02
125188	1	0.01	0.025	18100	6.8	4.5	12100	206	81.4	37200	3.9	4.5	1500	3.9	48.8	0.06
125198	0.8	0.02	0.038	16900	8.3	11.1	13900	325	203	31800	4.6	4.8	1740	3.9	53.6	0.146

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07. 2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.
Tailings: Detection limits on samples requiring dilutions for Hg-CV41 due to inteferences or high concentration levels have been increased according to the dilution factor.

Sample Id.	Hafnium Hf	Mercury Hg	Indium In	Potassium K	Lanthanum La	Lithium Li	Magnesium Mg	Manganese Mn	Molybdenum Mo	Sodium Na	Niobium Nb	Nickel Ni	Phosphorus P	Lead Pb	Rubidium Rb	Rhenium Re
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	Hg-CV41	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.1	0.01	0.005	100	0.5	0.2	100	5	0.05	100	0.1	0.2	10	0.5	0.1	0.002
Crustal Abundance: Fron	0.3	0.03	0.01	40	10	5	1600	390	0.2	400	0.3	2	170	1	0.2	NA
Crustal Abundance: To	11	0.4	0.26	48000	115	66	47000	6700	27	40400	35	225	1500	80	170	NA
125207	0.6	0.02	0.063	17300	7.3	7.5	12800	436	22.2	25800	4.3	4.4	1580	3	50.2	0.022
125228	1.5	0.01	0.023	11700	7.3	3.1	8000	207	284	42100	4	7.1	520	3.4	31.1	0.078
125244	1.5	0.01	0.026	6100	4.2	4.4	8800	277	23.8	45400	4.1	4	500	2.9	17.2	0.004
125257	1.7	0.01	0.049	2800	5.4	25.1	43800	989	16.3	16400	2.7	73.4	630	3.7	2.2	0.005
125278	1.4	0.01	0.061	5700	6.8	8.5	14500	780	2.1	52600	5.3	1.3	1190	3.5	13.5	*0.001*
125596	0.8	*0.005*	0.054	11600	9.4	9.5	16400	626	76.9	30600	3.5	4.2	1260	2.9	42	0.046
125610	0.7	0.01	0.033	12200	7.8	8.6	17900	565	32.9	36700	4.1	4.8	1190	2.4	36.3	0.031
125626																
125641	0.9	0.03	0.034	11200	7.5	10.7	25200	585	437	36600	5.1	17.8	1240	2.1	46.6	0.369
125669	1.9	0.01	0.059	15400	9	6.5	18200	530	132	28800	3.9	9.6	1410	3	64.8	0.049
125690	1.1	0.01	0.045	9500	8.4	12.2	21500	718	3.49	34500	6.2	14.3	1160	2.5	34.1	0.002
West Breccia Zone																
14018	1.9	0.01	0.065	24500	12.7	8.7	10700	476	36.3	31600	4.2	9.6	660	52	89.4	0.036
14021	1.7	*0.005*	0.082	22200	11.9	9.6	9200	629	348	23800	3.4	6.9	570	91.3	129.5	0.178
14036	1.7	*0.005*	0.087	21300	11.9	9.5	9100	475	658	24700	3	8.3	570	19.7	119.5	0.312
14043	1.4	*0.005*	0.041	10300	6.8	17.7	19000	446	324	32900	2.6	11.6	570	4.7	61.3	0.146
14060	2.2	*0.005*	0.053	12000	11.2	19.5	21000	422	220	30500	3.3	15.3	1290	5.8	67.9	0.133
14067	1.6	*0.005*	0.046	11200	10.1	26	26800	779	90.6	35100	2.7	16.2	1120	40.8	53.8	0.116
14076	1.9	0.01	0.06	14300	10.7	22.4	25000	1585	56.2	23000	2.6	15	1070	236	75.1	0.136
14083	1.4	0.01	0.076	30900	10.6	19.2	17700	1365	13.2	13600	2.5	17.2	1070	20	165	0.033
14099	1.4	0.02	0.04	32000	9.9	5.3	8200	1090	6.9	5400	3.2	6.5	470	23.4	177.5	0.002
14103	1.9	0.01	0.072	18100	12.3	7.8	12900	686	231	25100	2.9	10.2	620	8.2	93.2	0.185
125046	1.3	0.04	0.062	7900	6.6	27	20700	1100	46.2	35300	6.7	12	1160	20.3	17.2	0.016
125068	1.2	0.04	0.073	9500	7.6	30	22000	837	107.5	37200	6.8	17.1	1280	5	21.6	0.034
125073	1.3	0.03	0.051	15300	10.1	17.3	14700	479	372	32500	4.8	5.1	1180	5.5	45.2	0.103
125079	1	0.23	0.02	29300	15.1	11.5	9000	340	1120	29800	3.2	7.4	1080	7.8	78.7	0.184
125084	1	0.02	0.067	12100	8.6	23.3	19900	1425	155	29900	5.9	17.2	1230	4.6	26	0.037
125127	0.8	0.01	0.031	15000	7.2	31.7	22700	444	64.2	38000	6.5	16.3	1220	2.5	40.4	0.037
125129	0.7	0.02	0.024	13500	5.2	21.3	18100	409	111	32500	4.8	15.4	1080	14.1	58.6	0.089
125134	0.9	0.01	0.04	15300	9	21	19900	475	165.5	34900	5.3	20.1	1130	3.1	58.4	0.115
125142	1	0.02	0.053	11000	9.9	18.1	20400	798	152	32400	4.6	25.1	1000	3.8	42.3	0.147
125149	0.9	0.02	0.042	12100	10.1	17.9	19500	639	37.5	39000	6	15	1120	4.8	47.2	0.031
125154	1.7	0.01	0.038	5100	4.2	7	10000	323	92.9	57700	4.1	7.1	1620	3.8	13.6	0.029
125165	0.8	0.01	0.061	5100	10.8	18.5	15600	403	17.15	51300	5.4	4.3	1680	2.8	15	0.003
125176	0.8	0.03	0.076	7600	8.7	17.1	16900	474	9.04	46100	4.4	6.8	1440	3.4	17	0.002
146112	0.9	*0.005*	0.093	9000	13.8	8.8	13000	618	2.32	39400	5.4	2.1	1210	4.4	20.5	*0.001*
146115	2.6	0.01	0.07	6200	10.7	17.7	37900	1290	1.29	23200	5.7	25	1260	2.7	6.2	*0.001*
146124	0.7	*0.005*	0.029	13500	8.2	18.8	17500	702	30.2	30600	4.5	2.1	1480	4.5	32.9	0.002
146127	2.2	0.01	0.01	16300	8.4	8.7	5300	228	8.38	25600	3.6	6	480	3.7	36.8	*0.001*
146135	1.1	0.01	0.051	9100	8	13.1	12500	906	1.56	40500	4.7	2	1460	3.3	17.2	*0.001*
146149	1.1	*0.005*	0.048	9500	7.9	13.3	10000	831	2.17	38300	4.8	3.5	1370	11.9	21.5	*0.001*
146161	0.9	*0.005*	0.079	6800	8	21.6	32700	2140	1.96	17200	4.5	11.9	1250	3.7	16.8	*0.001*
146164	0.6	*0.005*	0.048	7500	5.2	39.2	35100	1720	0.8	24500	5	8.4	1470	4.4	6.2	*0.001*
145951	1.1	0.01	0.087	16800	7.9	6.1	13900	611	19.6	32400	6.4	4.7	1420	1.8	36	0.009
145956	0.9	0.01	0.087	11900	7.2	7.9	22200	784	51.5	31700	6.4	15.9	1210	3	32.1	0.008
145974	1	*0.005*	0.065	14500	8.6	11.6	23600	829	2.51	30400	7.1	2.8	1240	3.7	22.6	*0.001*

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07. 2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.
Tailings: Detection limits on samples requiring dilutions for Hg-CV41 due to inteferences or high concentration levels have been increased according to the dilution factor.

Sample	Hafnium	Mercury	Indium	Potassium	Lanthanum	Lithium	Magnesium	Manganese	Molybdenum	Sodium	Niobium	Nickel	Phosphorus	Lead	Rubidium	Rhenium
Id.	Hf	Hg	In	K	La	Li	Mg	Mn	Mo	Na	Nb	Ni	P	Pb	Rb	Re
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	Hg-CV41	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.1	0.01	0.005	100	0.5	0.2	100	5	0.05	100	0.1	0.2	10	0.5	0.1	0.002
Crustal Abundance: Fron	0.3	0.03	0.01	40	10	5	1600	390	0.2	400	0.3	2	170	1	0.2	NA
Crustal Abundance: To	11	0.4	0.26	48000	115	66	47000	6700	27	40400	35	225	1500	80	170	NA
145982	2.5	*0.005*	0.062	3500	15	20.4	31400	1110	1.25	18900	7.6	7.9	1370	6.5	5.8	*0.001*
145992	1.1	0.01	0.051	11800	6.4	7.9	16100	724	63.5	37300	6.7	12.6	1240	2.9	31.8	*0.001*
145999	0.9	0.01	0.073	8600	7.2	11.8	15900	644	4.17	33800	7	4.8	1180	2.7	21.6	*0.001*
145834	1	*0.005*	0.059	6500	8.3	22.3	16400	1020	1.79	42400	6.1	5.5	1230	6.2	14.5	*0.001*
145842	2	*0.005*	0.191	1100	8.3	24.2	24700	1880	8.9	18700	4	17.9	1900	10.5	3.2	0.002
145852	0.9	*0.005*	0.065	1400	8.7	14.9	10400	1190	10.7	35200	5.9	5.4	970	11	2.6	*0.001*
145857	1.1	*0.005*	0.057	5700	7.7	12.1	15700	808	1.7	44900	6.8	7.7	1440	2.9	7.7	*0.001*
145871	0.8	*0.005*	0.053	9900	9	20.3	14400	983	2.43	33800	6.9	5.1	1180	4.7	22.4	*0.001*
145608	1.1	*0.005*	0.043	11400	7.5	23.2	31600	740	9.37	29500	2.5	11.4	1000	8.4	43.9	0.027
145614	1.2	*0.005*	0.09	12800	9	20.5	26600	816	13	30700	2.5	16.1	990	24.1	52.2	0.038
145628	1.4	*0.005*	0.047	3300	7.3	15.4	21900	804	15.6	46400	2.4	9.6	890	7.2	9.3	0.048
145640	1.2	0.07	0.059	13300	8.8	18.4	25300	1165	8.56	30000	2.4	15.4	990	272	58.8	0.013
145646	1	0.01	0.058	8200	8.8	19.3	27200	1010	16.95	33900	2.3	9.2	1010	9	29.2	0.017
Paramount Zone																
125965	1.2	*0.005*	0.093	8300	10.1	10.3	20600	870	106	44400	3.2	12.5	980	5.7	33.2	0.046
125974	1.2	*0.005*	0.041	15900	8.7	7.6	20100	496	46.2	29100	2.8	10.6	890	2.8	48.2	0.022
125983	1.2	0.01	0.094	11000	9.1	8	34000	741	187	26600	2.9	41.8	910	5.7	33.1	0.106
125988	2.9	*0.005*	0.056	13200	17.7	16.2	32400	1160	1.74	26100	6.3	38	1260	7.5	30.1	*0.001*
126007	1.1	0.01	0.018	19400	7.5	4	8600	544	199	32100	3.1	9.7	520	7.6	66.4	0.08
126031	1.4	0.01	0.016	13100	9.5	4.5	8200	265	57.7	41500	3.9	10.9	560	5.2	41.4	0.029
126040	1.3	0.01	0.085	9000	11.7	6.7	19600	372	326	42500	3.2	41.5	840	2.8	29.4	0.114
126054	1.3	*0.005*	0.08	7700	11	22	40800	1510	83.4	17300	2.9	83.1	1040	7	27	0.055
126067	1.1	*0.005*	0.148	10000	10	11.3	31400	1640	105.5	21300	2.9	35	960	7.7	39.4	0.059
126081	1.4	0.01	0.062	28300	5.1	2.8	9200	679	89.3	9900	3.5	5.1	420	10.4	157.5	0.052
126110	2.4	*0.005*	0.065	18600	17.3	12.1	28500	1200	3.31	28300	5.8	29	1330	5.9	44.4	0.003
126118	1	*0.005*	0.087	16500	11.1	9.8	24900	965	170	23400	6.4	21.2	1730	2.2	53.6	0.225
125904	0.7	0.01	0.079	12300	9.7	5.2	12300	581	342	44700	4.8	10.7	1410	3.3	35.4	0.199
125919	0.6	0.01	0.085	10800	11.9	7.2	18200	524	339	49300	5.1	5.7	1360	4.1	38.6	0.161
125928	0.8	0.01	0.066	11500	7.9	7.6	21000	1130	128	39600	6.7	14.3	1220	22	23.6	0.062
125933	2.7	*0.005*	0.078	10000	18.1	11.7	30100	1340	1.9	36600	8.5	13.9	2040	18.2	18	*0.001*
125944	0.6	*0.005*	0.056	10000	10.4	9.3	23200	1400	12.55	43100	6.5	14.6	1170	15.8	29.6	0.01
125952	1.5	0.01	0.033	17500	8.1	4.2	10300	423	9.19	29000	4	8.3	560	3.5	40.5	0.003
125963	0.8	0.01	0.101	11700	12.1	7.4	21200	774	67.4	41200	5	6.6	1320	5.2	32.1	0.011
126120	1.6	0.02	0.014	10100	7	5.6	8600	247	54.9	44800	4	9.1	540	4.6	32.8	0.036
126131	1.4	0.05	0.032	9600	9.6	11.9	12300	231	5.04	48200	4.6	10.8	890	3.9	27.8	0.002
126142	1.2	0.05	0.032	9400	8.8	15.5	15400	339	8.62	42500	5.1	11.8	920	6	31.2	0.003
126154	1.2	0.08	0.061	5600	8.4	20	24900	430	82.6	53600	6.2	19.5	1490	4.4	17	0.028
126171	1.9	0.01	0.023	16300	9.9	10.4	17300	407	94.6	31900	3.1	10.5	900	4.7	49.1	0.046
126181	0.6	0.01	0.035	8400	8.6	9.4	23300	984	2.17	31900	6.6	10.9	1080	15	19.3	0.004
125806	1.6	*0.005*	0.034	18400	9.8	6.6	11700	380	1.97	36100	4	14.2	700	6.1	38.7	0.002
125816	3.2	*0.005*	0.072	16600	19.8	14	23000	1140	2.09	32100	7.2	6.9	1490	17.9	42.1	0.002
125833	1.2	0.01	0.032	18600	6.6	5.8	8000	317	122.5	35200	3	8.8	530	6.8	52.8	0.058
125861	1.1	0.01	0.038	14200	7.2	2.9	8400	243	213	38100	2.4	8	540	2.5	39.5	0.068
125875	1.7	0.01	0.033	19000	8.3	3.1	7300	282	148	32800	3.4	5.3	540	3.2	46.2	0.077
125897	2.3	*0.005*	0.019	16100	9	6.3	8100	237	149	32100	4	7.8	730	2.4	42.6	0.093

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07. 2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.
Tailings: Detection limits on samples requiring dilutions for Hg-CV41 due to inteferences or high concentration levels have been increased according to the dilution factor.

Sample Id.	Hafnium Hf (ppm)	Mercury Hg (ppm)	Indium In (ppm)	Potassium K (ppm)	Lanthanum La (ppm)	Lithium Li (ppm)	Magnesium Mg (ppm)	Manganese Mn (ppm)	Molybdenum Mo (ppm)	Sodium Na (ppm)	Niobium Nb (ppm)	Nickel Ni (ppm)	Phosphorus P (ppm)	Lead Pb (ppm)	Rubidium Rb (ppm)	Rhenium Re (ppm)
Method	ME-MS61	Hg-CV41	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.1	0.01	0.005	100	0.5	0.2	100	5	0.05	100	0.1	0.2	10	0.5	0.1	0.002
Crustal Abundance: Fron	0.3	0.03	0.01	40	10	5	1600	390	0.2	400	0.3	2	170	1	0.2	NA
Crustal Abundance: To	11	0.4	0.26	48000	115	66	47000	6700	27	40400	35	225	1500	80	170	NA
Tailings																
LIARD ZONE	1.1	*0.05*	0.034	14300	8.5	9.6	13900	402	55.2	31000	4.9	16.2	1160	4.8	57.2	0.03
PARAMOUNT	1.6	*0.05*	0.043	13700	8.2	8.5	13900	547	77.7	32500	4.6	28.1	830	6.5	51.5	0.041
WEST BRECCIA	1.4	*0.05*	0.075	13500	12.2	19	19100	691	42.5	34900	4.2	35.9	1190	6.8	51.3	0.021
High-Sulphide Histor																
T112 (171' - 172')	1.1	0.01	0.17	3800	4.2	18.7	33800	828	9.16	29900	3.1	51.1	1110	83	12.9	0.016
T113 (81' - 82')	1.7	0.03	0.019	18300	13.9	9.2	13600	211	12.35	34400	3.3	9.6	630	9	49.6	0.031
T113 (983' - 985')	1.9	0.01	0.08	15900	13.8	8.2	18000	631	59.3	24600	2.2	14.3	810	9.1	79.4	0.106
T140 (30' - 31')	1	0.01	0.036	21000	7.4	11.4	14800	224	62.3	25200	4.1	4.3	1330	3.1	96.3	0.047
T166 (389' - 390')	1.2	*0.005*	0.009	17700	8.1	4	6500	121	1.54	31000	2.9	8	510	2.8	55.5	*0.001*
T185 (116' - 117')	2.5	0.01	0.017	22900	10.6	4.2	6300	60	12.65	22800	2.7	6.4	690	5.6	78.4	0.04
T207 (261.5' - 262')	1	0.01	0.018	16500	5.7	2.4	4500	189	137.5	26400	2.8	7.9	570	1.8	52.7	0.029
T207 (269' - 271')	0.9	0.01	0.017	15100	6.9	7.5	6100	207	313	17100	2.7	11.5	450	3.7	45.3	0.087
All Data																
Maximum	3.2	0.23	0.19	32000	19.8	39.5	64300	2140	1120	57700	8.5	176	2040	272	178	0.94
Minimum	0.5	0.005	0.0025	1100	2.8	2.4	4000	60	0.8	5400	2	1.3	420	1.6	2.2	0.001
Mean	1.21	0.014	0.051	14109	9.22	12.6	17488	555	118	32813	4.8	11	1167	7.78	48.6	0.078
Standard Deviation	0.48	0.018	0.026	4975	2.43	6.84	7969	334	161	7688	1.36	14.9	318	24.8	24.1	0.12
10 Percentile	0.7	0.005	0.022	7980	6.6	5.34	8940	245	2.49	23920	2.9	2.6	570	2.1	19.1	0.0014
25 Percentile	0.9	0.005	0.034	11200	7.75	7.6	12300	354	14.8	29000	3.9	4.2	1035	2.55	35.2	0.009
Median	1.1	0.01	0.049	14200	9	11.3	16300	456	67.4	32500	4.7	7.1	1240	3.3	48.2	0.04
75 Percentile	1.4	0.01	0.065	16700	10.5	16.9	20650	642	150	36600	5.7	14.3	1360	5.1	60.2	0.097
90 Percentile	1.76	0.03	0.082	20380	12.1	21.8	26720	1050	305	42500	6.7	19.7	1490	9.06	69.3	0.19
Interquartile Range (IC	0.5	0.005	0.032	5500	2.75	9.3	8350	288	136	7600	1.8	10.1	325	2.55	24.9	0.088
Variance	0.23	0.00033	0.00067	24752014	5.92	46.8	63510199	111416	26064	59099355	1.86	223	101029	613	581	0.013
Skewness	1.45	7.79	1.49	0.31	0.97	1.06	1.62	1.75	2.97	-0.072	0.2	6.81	-0.64	8.93	1.58	3.62
Coefficient of Variatior	0.39	1.29	0.5	0.35	0.26	0.54	0.46	0.6	1.37	0.23	0.28	1.35	0.27	3.18	0.5	1.48
Count	235	235	235	235	235	235	235	235	235	235	235	235	235	235	235	235
Main Zone																
Maximum	3.2	0.06	0.14	24000	16.8	39.5	64300	1155	1095	52600	8.2	176	1840	20.6	84.9	0.94
Minimum	0.5	0.005	0.0025	2800	2.8	2.5	4000	84	0.82	13600	2	1.3	440	1.6	2.2	0.001
Mean	1.13	0.013	0.048	14737	9.04	12.2	17027	444	131	32907	4.99	9.37	1238	3.25	51.1	0.095
Standard Deviation	0.4	0.0088	0.021	4015	2.07	6.46	7727	185	162	6491	1.18	16.3	270	1.92	15.6	0.14
10 Percentile	0.7	0.005	0.024	9600	6.6	5.65	9850	248	5.44	25600	3.8	2.25	900	2	31.6	0.0025
25 Percentile	0.82	0.01	0.032	12200	7.72	7.6	12475	338	23	29200	4.2	3.15	1190	2.32	42.4	0.011
Median	1	0.01	0.046	14900	9	11.1	15750	424	80.1	32900	4.8	5	1270	2.8	52.6	0.051
75 Percentile	1.4	0.01	0.058	17125	10.3	15.2	19350	530	176	35750	5.68	10.8	1390	3.6	61.8	0.12
90 Percentile	1.6	0.02	0.075	20350	11.7	20.4	24400	625	304	40750	6.7	17.5	1500	4.7	67.8	0.22
Interquartile Range (IC	0.57	0	0.026	4925	2.58	7.6	6875	192	153	6550	1.47	7.6	200	1.28	19.4	0.11
Variance	0.16	0.000078	0.00045	16121519	4.29	41.7	59708486	34203	26368	42137884	1.38	265	72992	3.68	243	0.018
Skewness	1.4	2.37	0.87	-0.13	0.24	1.26	2.45	1.4	2.57	-0.0028	0.32	7.93	-1.23	5.71	-0.48	3.22
Coefficient of Variatior	0.36	0.69	0.44	0.27	0.23	0.53	0.45	0.42	1.24	0.2	0.24	1.74	0.22	0.59	0.31	1.43
Count	146	146	146	146	146	146	146	146	146	146	146	146	146	146	146	146

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07. 2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.
Tailings: Detection limits on samples requiring dilutions for Hg-CV41 due to inteferences or high concentration levels have been increased according to the dilution factor.

Sample	Hafnium	Mercury	Indium	Potassium	Lanthanum	Lithium	Magnesium	Manganese	Molybdenum	Sodium	Niobium	Nickel	Phosphorus	Lead	Rubidium	Rhenium
Id.	Hf	Hg	In	K	La	Li	Mg	Mn	Mo	Na	Nb	Ni	P	Pb	Rb	Re
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	Hg-CV41	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.1	0.01	0.005	100	0.5	0.2	100	5	0.05	100	0.1	0.2	10	0.5	0.1	0.002
Crustal Abundance: Fron	0.3	0.03	0.01	40	10	5	1600	390	0.2	400	0.3	2	170	1	0.2	NA
Crustal Abundance: To	11	0.4	0.26	48000	115	66	47000	6700	27	40400	35	225	1500	80	170	NA
West Breccia Zone																
Maximum	2.6	0.23	0.19	32000	15.1	39.2	37900	2140	1120	57700	7.6	25.1	1900	272	178	0.31
Minimum	0.6	0.005	0.01	1100	4.2	5.3	5300	228	0.8	5400	2.3	2	470	1.8	2.6	0.001
Mean	1.27	0.017	0.06	12217	9.09	17.1	18943	844	100	32162	4.68	10.6	1138	21.2	43.9	0.049
Standard Deviation	0.49	0.034	0.027	7002	2.35	7.27	7553	421	199	9482	1.61	5.9	312	52.1	40	0.07
10 Percentile	0.8	0.005	0.035	5100	6.72	7.9	9680	417	1.75	21360	2.5	3.98	600	2.86	7.1	0.001
25 Percentile	0.9	0.005	0.046	7750	7.65	11.6	13450	478	5.54	27550	3.2	5.75	1000	3.7	17.1	0.001
Median	1.1	0.01	0.059	11400	8.7	17.9	18100	784	17.2	32400	4.7	9.6	1180	5	32.1	0.016
75 Percentile	1.5	0.01	0.072	14750	10.4	21.2	23150	1055	100	37250	6.05	15.4	1285	11.4	58.5	0.068
90 Percentile	1.94	0.03	0.087	21660	12.1	24.9	28880	1389	268	43400	6.8	17.2	1464	30.8	90.9	0.15
Interquartile Range (IC	0.6	0.005	0.026	7000	2.7	9.6	9700	578	94.7	9700	2.85	9.65	285	7.75	41.4	0.068
Variance	0.24	0.0012	0.00074	49034921	5.52	52.8	57053367	177381	39518	89909806	2.6	34.8	97544	2715	1601	0.0049
Skewness	1.08	5.64	2.3	1.14	0.63	0.55	0.51	1.14	3.65	-0.075	0.035	0.54	-0.35	4.16	1.74	1.81
Coefficient of Variatior	0.38	2	0.45	0.57	0.26	0.42	0.4	0.5	1.98	0.29	0.34	0.56	0.27	2.45	0.91	1.44
Count	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47
Paramount Zone																
Maximum	3.2	0.08	0.15	28300	19.8	22	40800	1640	342	53600	8.5	83.1	2040	22	158	0.22
Minimum	0.6	0.005	0.014	5600	5.1	2.8	7300	231	1.74	9900	2.4	5.1	420	2.2	17	0.001
Mean	1.43	0.013	0.057	13455	10.3	9.01	18803	705	102	35010	4.55	17.3	996	7.1	40.7	0.053
Standard Deviation	0.66	0.017	0.031	4788	3.48	4.79	9190	429	101	9793	1.6	16.2	400	5.2	24.3	0.058
10 Percentile	0.7	0.005	0.019	8400	7.2	4	8200	247	2.09	23400	2.9	6.6	540	2.8	23.6	0.002
25 Percentile	1.1	0.005	0.032	10000	8.35	5.7	9750	356	8.9	29050	3.15	8.55	630	3.7	29.8	0.0035
Median	1.2	0.01	0.056	12300	9.6	7.6	19600	544	83.4	35200	4	10.9	920	5.7	38.6	0.046
75 Percentile	1.6	0.01	0.08	16550	11	11.5	24100	1057	148	42500	6	17	1290	7.55	43.5	0.073
90 Percentile	2.4	0.02	0.093	18600	17.3	15.5	31400	1340	213	44800	6.6	38	1490	15.8	52.8	0.11
Interquartile Range (IC	0.5	0.005	0.047	6550	2.7	5.8	14350	702	140	13450	2.85	8.5	660	3.85	13.6	0.069
Variance	0.44	0.00027	0.00098	22922559	12.1	22.9	84461656	183731	10230	95895570	2.57	262	160165	27.1	591	0.0034
Skewness	1.19	3.09	0.73	0.93	1.46	1.03	0.5	0.69	1.11	-0.43	0.67	2.65	0.61	1.61	3.89	1.52
Coefficient of Variatior	0.47	1.25	0.55	0.36	0.34	0.53	0.49	0.61	0.99	0.28	0.35	0.94	0.4	0.73	0.6	1.09
Count	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07. 2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.
Tailings: Detection limits on samples requiring dilutions for Hg-CV41 due to inteferences or high concentration levels have been increased according to the dilution factor.

Sample	Hafnium	Mercury	Indium	Potassium	Lanthanum	Lithium	Magnesium	Manganese	Molybdenum	Sodium	Niobium	Nickel	Phosphorus	Lead	Rubidium	Rhenium
Id.	Hf	Hg	In	K	La	Li	Mg	Mn	Mo	Na	Nb	Ni	P	Pb	Rb	Re
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	Hg-CV41	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.1	0.01	0.005	100	0.5	0.2	100	5	0.05	100	0.1	0.2	10	0.5	0.1	0.002
Crustal Abundance: Fron	0.3	0.03	0.01	40	10	5	1600	390	0.2	400	0.3	2	170	1	0.2	NA
Crustal Abundance: To	11	0.4	0.26	48000	115	66	47000	6700	27	40400	35	225	1500	80	170	NA
Tailings																
Maximum	1.6	0.05	0.075	14300	12.2	19	19100	691	77.7	34900	4.9	35.9	1190	6.8	57.2	0.041
Minimum	1.1	0.05	0.034	13500	8.2	8.5	13900	402	42.5	31000	4.2	16.2	830	4.8	51.3	0.021
Mean	1.37	0.05	0.051	13833	9.63	12.4	15633	547	58.5	32800	4.57	26.7	1060	6.03	53.3	0.031
Standard Deviation	0.25	8.5E-18	0.022	416	2.23	5.77	3002	145	17.8	1967	0.35	9.92	200	1.08	3.35	0.01
10 Percentile	1.16	0.05	0.036	13540	8.26	8.72	13900	431	45	31300	4.28	18.6	896	5.14	51.3	0.023
25 Percentile	1.25	0.05	0.038	13600	8.35	9.05	13900	474	48.8	31750	4.4	22.2	995	5.65	51.4	0.026
Median	1.4	0.05	0.043	13700	8.5	9.6	13900	547	55.2	32500	4.6	28.1	1160	6.5	51.5	0.03
75 Percentile	1.5	0.05	0.059	14000	10.4	14.3	16500	619	66.4	33700	4.75	32	1175	6.65	54.4	0.036
90 Percentile	1.56	0.05	0.069	14180	11.5	17.1	18060	662	73.2	34420	4.84	34.3	1184	6.74	56.1	0.039
Interquartile Range (IC	0.25	0	0.02	400	2	5.25	2600	144	17.6	1950	0.35	9.85	180	1	2.95	0.01
Variance	0.063	NA	0.00046	173333	4.96	33.3	9013333	20880	318	3870000	0.12	98.4	39900	1.16	11.2	0.0001
Skewness	-0.59	-2.45	1.4	1.29	1.7	1.66	1.73	-0.01	0.8	0.67	-0.42	-0.61	-1.69	-1.58	1.73	0.3
Coefficient of Variatior	0.18	1.7E-16	0.43	0.03	0.23	0.47	0.19	0.26	0.3	0.06	0.077	0.37	0.19	0.18	0.063	0.33
Count	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
High-Sulphide Histor																
Maximum	2.5	0.03	0.17	22900	13.9	18.7	33800	828	313	34400	4.1	51.1	1330	83	96.3	0.11
Minimum	0.9	0.005	0.009	3800	4.2	2.4	4500	60	1.54	17100	2.2	4.3	450	1.8	12.9	0.001
Mean	1.41	0.012	0.046	16400	8.83	8.2	12950	309	76	26425	2.98	14.1	762	14.8	58.8	0.045
Standard Deviation	0.57	0.0075	0.055	5725	3.61	5.2	9770	270	106	5366	0.56	15.2	309	27.7	25.7	0.035
10 Percentile	0.97	0.0085	0.015	11710	5.25	3.52	5620	103	6.87	21090	2.55	5.77	492	2.5	35.6	0.012
25 Percentile	1	0.01	0.017	15700	6.6	4.15	6250	172	11.6	24150	2.7	7.52	555	3.02	48.5	0.026
Median	1.15	0.01	0.018	17100	7.75	7.85	10050	209	36	25800	2.85	8.8	660	4.65	54.1	0.036
75 Percentile	1.75	0.01	0.047	18975	11.4	9.75	15600	326	81.1	30175	3.15	12.2	885	9.02	78.6	0.057
90 Percentile	2.08	0.016	0.11	21570	13.8	13.6	22740	690	190	32020	3.54	25.3	1176	31.3	84.5	0.093
Interquartile Range (IC	0.75	0	0.03	3275	4.8	5.6	9350	154	69.5	6025	0.45	4.67	330	6	30.1	0.031
Variance	0.32	0.000057	0.003	32774286	13	27	95460000	73146	11213	28790714	0.31	232	95193	768	662	0.0012
Skewness	1.16	2.49	2.08	-1.65	0.49	1.16	1.58	1.41	1.98	-0.27	1.04	2.61	1.09	2.77	-0.34	0.84
Coefficient of Variatior	0.4	0.63	1.2	0.35	0.41	0.63	0.75	0.88	1.39	0.2	0.19	1.08	0.4	1.88	0.44	0.79
Count	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8

$\boxed{19.5}$ NOTE: if data is boxed, then data is 3 times the maximum crustal abundance.

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

NOTE: If data was reported as > detection limit the detection limit is shown in bold and was used in subsequent calculations.

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07. 2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.
Tailings: Detection limits on samples requiring dilutions for Hg-CV41 due to inteferences or high concentration levels have been increased according to the dilution factor.

Sample	Hafnium	Mercury	Indium	Potassium	Lanthanum	Lithium	Magnesium	Manganese	Molybdenum	Sodium	Niobium	Nickel	Phosphorus	Lead	Rubidium	Rhenium
Id.	Hf	Hg	In	K	La	Li	Mg	Mn	Mo	Na	Nb	Ni	P	Pb	Rb	Re
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	Hg-CV41	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	0.1	0.01	0.005	100	0.5	0.2	100	5	0.05	100	0.1	0.2	10	0.5	0.1	0.002
Crustal Abundance: Fron	0.3	0.03	0.01	40	10	5	1600	390	0.2	400	0.3	2	170	1	0.2	NA
Crustal Abundance: To	11	0.4	0.26	48000	115	66	47000	6700	27	40400	35	225	1500	80	170	NA

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.

Sample Id.	Sulphur S	Antimony Sb	Scandium Sc	Selenium Se	Tin Sn	Strontium Sr	Tantalum Ta	Tellurium Te	Thorium Th	Titanium Ti	Thallium Tl	Uranium U	Vanadium V	Tungsten W	Yttrium Y	Zinc Zn	Zirconium Zr
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	100	0.05	1	1	0.2	0.2	0.05	0.05	0.2	50	0.02	0.1	1	0.1	0.1	2	0.5
Crustal Abundance: Fron	240	0.1	NA	0.05	0.5	1	0.8	NA	0.004	300	0.16	0.45	20	0.6	20	16	19
Crustal Abundance: To	2400	1.5	NA	0.6	6	2000	4.2	NA	17	13800	2.3	3.7	250	2.2	90	165	500
Main Zone																	
14130	3200	1.25	6.3	5	0.9	288	0.22	0.51	0.8	2800	0.28	0.3	73	5.6	12.7	26	19.7
14144	2800	2.5	6.8	4	0.9	343	0.29	0.54	0.9	3760	0.27	0.5	91	4	16.2	46	19.6
14148	1400	2.35	11.4	3	1.2	223	0.25	0.27	0.8	3780	0.31	0.9	146	4.9	15.6	40	28.9
14156	1700	1.66	5.6	3	1.1	259	0.33	0.09	3.1	1900	0.17	1.9	47	10.5	8.5	35	39.3
14162	1500	2.42	21.4	2	1.2	239	0.28	0.17	1.8	4270	0.22	1.1	159	5.2	15.7	67	59.6
14169	3200	1.63	5.9	3	1.9	207	0.3	0.46	2.8	1960	0.15	1.7	65	13	6.3	24	36.9
14232	1600	3.64	6.8	3	1.1	345	0.27	0.23	0.9	3290	0.3	0.5	87	3.5	14.5	21	23.6
14250	2000	3.46	12.1	3	1.4	424	0.25	0.29	0.8	4350	0.28	0.5	236	3.3	16.9	38	18.3
14260	3700	2.5	11.4	6	1.6	402	0.23	0.85	0.7	4050	0.31	0.5	144	4.5	14.3	36	17.6
14276	1700	10.95	7.2	2	1	798	0.28	0.07	1	4100	0.14	0.6	112	4.9	17.8	112	29.9
14295	4900	3.4	14.1	2	1.8	336	0.25	0.08	0.7	4240	0.38	0.7	154	15.6	14.8	34	23.5
14301	3500	2.57	11	3	1.6	209	0.26	0.13	1	3620	0.3	0.6	117	10.5	14.7	38	47.1
14323	1500	2.29	6.5	2	1.3	391	0.27	0.17	0.8	3310	0.31	0.4	94	3.3	15.5	29	29.3
14332	2700	1.94	6.9	2	1.4	355	0.27	0.19	0.9	3260	0.32	0.5	103	3.5	16.6	31	32.2
14345	5600	2.33	7.3	5	3.8	274	0.24	0.29	0.9	2970	0.41	0.6	101	14.5	14.8	27	20
14348	4800	2.53	6.8	3	1.7	276	0.27	0.19	0.9	3190	0.4	0.5	74	5.8	13.9	40	22.1
14797	700	4.83	11	3	1.2	234	0.28	0.15	0.6	4150	0.38	0.3	152	5.7	12	42	20.9
14808	1900	5.13	9.8	7	1.4	221	0.24	0.45	1	3260	0.43	0.7	117	4.5	14.5	34	34
14816	4700	3.45	10.9	5	1.7	285	0.28	0.77	0.7	3810	0.36	0.4	144	6.2	13.1	49	18.4
14828	1400	1.72	11.4	6	1.1	404	0.29	0.5	0.8	3940	0.29	0.4	141	3.3	17.5	32	20.7
14844	2200	5.28	17.9	4	1.4	265	0.33	0.23	1	5590	0.49	0.6	262	3.3	13	40	30.5
14680	2200	5.2	12.8	8	1.4	348	0.3	0.77	1.1	4040	0.43	0.7	151	4.8	17.8	38	64.4
14871	3800	4.15	12.7	4	1.7	405	0.31	0.19	1	4990	0.32	0.7	183	6	15.3	43	22.6
14887	5400	1.41	14	2	1.3	424	0.33	0.09	1.2	4960	0.28	0.7	188	5.2	15.1	39	22.8
14689	7900	1.27	5.3	3	0.9	141	0.21	0.15	3.1	1580	0.18	1.6	51	3	8.3	16	33.4
14695	1600	3.83	11.9	5	1.5	226	0.25	0.18	1	4310	0.23	0.9	161	6	14.9	49	48.5
14742	2100	2.37	15.2	7	1.9	302	0.34	0.23	1.6	4690	0.25	0.9	215	6.6	12	53	32.7
14666	3800	3.07	15.1	3	1.5	416	0.41	0.06	1.3	5070	0.27	1	209	8	15.4	38	27.7
14685	21000	3.51	25.5	6	2.2	393	0.26	0.15	1.3	7690	0.32	1	269	5.5	14.5	43	35
14685B	20400	3.19	23.4	5	1.9	374	0.25	0.14	1.4	7930	0.37	0.9	276	5.2	13.6	46	43.4
14545	1900	1.48	8.5	1	1.4	409	0.36	0.05	1.5	3980	0.26	0.8	90	4.2	16.3	26	44.7
14565	2600	4.4	8.3	2	1.4	259	0.32	0.14	1.3	3800	0.37	0.6	80	4.7	16.9	16	32.5
14571	11100	2.6	7.8	5	1.4	312	0.28	0.15	2.3	3170	0.26	1.3	86	4.8	11.2	34	42
14578	21300	2.42	11	4	1.4	324	0.33	0.11	1.8	4630	0.29	1.2	112	4.1	15.9	19	56
14578B	21100	2.47	11.3	4	1.4	330	0.3	0.09	2	4430	0.32	1.2	111	4.1	17.1	19	74.1
14598	1500	1.89	8.4	2	0.9	569	0.36	0.06	0.6	4330	0.28	0.4	131	2.7	13.2	47	22.7
14893	1100	6.95	20.1	3	1.7	379	0.36	0.12	1.3	6030	0.25	1.5	283	9.3	15.3	49	40.7
14899	200	3.09	19.4	2	1	366	0.34	0.06	1	5850	0.16	0.6	262	8.2	13.8	52	25.5
14908	900	4.87	19	2	1.6	479	0.39	0.1	1.6	5910	0.22	1.2	268	12.1	16.7	42	34.7
14917	1900	4.6	17.7	4	1.7	309	0.3	0.26	2.8	4580	0.22	1.7	178	8.9	16.1	44	74.3
14925	1500	6.54	15.5	3	1.7	353	0.38	0.11	1.4	5090	0.29	0.7	224	5.1	15	52	31
14998	1300	5.17	10.8	3	1.4	412	0.26	0.16	0.7	4460	0.3	0.6	152	13.5	16.6	41	22.5
15862	800	2.81	11.3	2	1.1	327	0.29	0.12	0.7	4050	0.29	0.3	146	2.9	14	49	17.8
15870	1400	6.6	14.3	3	1.4	234	0.31	0.15	1.3	4460	0.36	0.8	203	6.1	16.1	53	23.4
15879	1200	7.41	17.1	3	1.3	373	0.39	0.16	1.5	5450	0.28	0.9	246	3.3	16	63	27.3

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.

Sample	Sulphur	Antimony	Scandium	Selenium	Tin	Strontium	Tantalum	Tellurium	Thorium	Titanium	Thallium	Uranium	Vanadium	Tungsten	Yttrium	Zinc	Zirconium
Id.	S	Sb	Sc	Se	Sn	Sr	Ta	Te	Th	Ti	Tl	U	V	W	Y	Zn	Zr
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	100	0.05	1	1	0.2	0.2	0.05	0.05	0.2	50	0.02	0.1	1	0.1	0.1	2	0.5
Crustal Abundance: Fron	240	0.1	NA	0.05	0.5	1	0.8	NA	0.004	300	0.16	0.45	20	0.6	20	16	19
Crustal Abundance: To	2400	1.5	NA	0.6	6	2000	4.2	NA	17	13800	2.3	3.7	250	2.2	90	165	500
15887	3300	5.99	15.3	5	1.7	402	0.34	0.37	1	5100	0.24	0.7	214	3.6	13.6	42	23.2
15891	1400	7.05	15	4	1.3	382	0.3	0.23	1.1	4920	0.31	0.6	213	5.3	15.1	51	19.4
15908	2200	6.21	14.2	5	1.5	288	0.32	0.29	1.2	4740	0.34	0.8	207	5.4	15.5	43	26.1
15911	900	4.97	17.9	3	1.3	335	0.37	0.13	1.5	5430	0.29	0.7	248	3	15.3	49	26.4
125285	3200	0.96	13.2	3	1.2	276	0.21	0.64	0.7	3860	0.17	0.5	186	4.2	10.2	48	17.1
125288	1000	1.99	33.3	*0.5*	0.7	368	0.26	*0.025*	0.9	5620	0.13	0.3	202	0.5	18	73	76
125293	2100	0.91	22.1	3	1.4	220	0.2	0.61	1.2	4330	0.12	0.7	224	4.2	12	60	28.1
125305	1500	0.95	12	3	1.3	312	0.26	0.38	0.8	3700	0.2	0.4	143	2.2	12.9	40	22.5
125311	700	0.83	9.8	2	0.9	328	0.25	0.19	0.7	3510	0.21	0.3	114	3.4	11.3	31	20.7
125703	1000	3.27	10.3	2	1	168	0.29	0.09	0.6	3960	0.4	0.4	129	10.5	11.3	46	24.4
125728	2000	3.83	16.9	3	1.5	353	0.36	0.32	1.3	5100	0.24	0.7	223	4.4	12.7	59	25.2
125755	5700	1.66	5	4	0.8	228	0.18	0.28	2.5	1320	0.22	1.2	49	2.8	6	14	43.9
125772	2200	4.58	15.7	5	1.3	311	0.36	0.42	1.3	4680	0.29	0.8	205	3.6	13.7	45	29.9
125795	1100	2.04	14.3	2	1	269	0.35	0.14	1.2	4560	0.31	0.6	186	2.9	13.2	40	25.1
125422	2400	2.2	11.4	3	1.4	333	0.28	0.19	0.7	3930	0.26	0.5	126	8.6	16	41	22.3
125435	1600	4.84	12.8	3	1.4	245	0.26	0.21	0.7	4080	0.3	0.4	137	6.9	15.2	41	18.4
125452	5500	5.28	12.5	5	2.1	341	0.26	0.41	0.7	4100	0.37	0.7	129	9.4	16.3	23	25.1
125476	8500	8.67	6	3	2	248	0.2	0.4	2.5	1420	0.31	1.3	63	9.9	7.2	7	53.9
125490	4300	1.75	14.9	3	1.8	250	0.26	0.08	0.7	4210	0.38	0.5	157	4.2	14.5	28	25
126192	2100	7.55	7.1	3	1.5	336	0.34	0.12	0.9	3920	0.24	0.6	89	2.8	13.4	38	27.2
126206	2500	2.57	9	3	0.9	419	0.34	0.17	0.7	4410	0.25	0.5	127	3.3	15.4	27	12.8
126225	3500	1.95	7.9	3	1.3	439	0.32	0.22	0.5	4150	0.26	0.4	155	3.1	12.4	32	17.7
126244	2800	1.96	7.7	3	1.4	315	0.33	0.34	0.9	4130	0.28	0.6	138	6	13.6	39	19.4
126266	2200	2.21	8.3	3	1.4	284	0.35	0.2	1	4370	0.29	0.6	136	7.6	13.4	36	22.7
126279	4300	1.84	7	3	1.3	417	0.31	0.19	0.8	3890	0.23	0.6	155	5.2	10.7	32	21.7
126288	4000	1.65	7.6	4	1.5	270	0.33	0.22	1	3830	0.33	0.6	149	9.1	12.6	27	26.8
126297	5700	6.98	21.6	3	2.7	223	0.28	0.11	2.1	6580	0.26	1.4	238	4.2	17	61	51.6
126314	14600	2.79	9.4	4	1.5	263	0.23	0.17	0.7	4470	0.32	0.5	149	3.5	14.3	39	19.1
126329	2500	3.25	7	3	1.2	200	0.35	0.18	0.8	3510	0.24	0.5	92	1.9	14.9	39	24.4
126337	5900	3.84	15.3	4	1.9	320	0.27	0.24	1.1	5630	0.23	0.7	205	2.7	14.6	44	28.4
126351	1500	1.65	12.4	3	1.5	369	0.26	0.15	1.9	4250	0.25	0.6	140	2.7	14.8	26	19.6
126427	12900	2.27	26.6	2	1.7	289	0.16	0.1	1.6	5430	0.27	0.7	243	2.3	15.3	68	38.6
126430	2500	1.65	8.7	2	0.7	183	0.31	*0.025*	0.9	4220	0.3	0.4	100	1.3	14.4	61	18.7
126434	1300	2.31	8.6	2	1.2	297	0.39	*0.025*	1.2	3980	0.31	0.5	90	1.9	14.1	29	16.9
126443	18200	3.11	10.6	4	1.6	218	0.28	0.1	1.1	4420	0.34	0.8	118	2.9	14.3	36	35.8
126449	100	0.92	27.4	2	1.1	511	0.38	*0.025*	2.2	5830	0.07	0.8	228	0.3	21.3	84	93.6
126464	4800	1.56	8.4	2	0.9	369	0.32	0.06	1.2	3980	0.29	0.5	112	3	15.4	33	26.2
126492	2300	1.48	9.1	2	1.1	295	0.31	0.05	1	4020	0.34	0.7	198	2.4	14.6	27	27
145655	6700	1.28	8.9	4	1.4	320	0.32	0.05	1.2	4000	0.3	0.7	144	2.1	16.6	29	40.6
145669	10000	1.58	10.3	3	1.6	285	0.34	0.09	1.1	4110	0.32	0.7	172	3.5	15.4	37	36.1
145685	2300	1.73	13	3	1	263	0.26	0.05	0.6	4220	0.28	0.3	159	2	11.4	47	18.4
145694	1800	1.93	12.4	2	1.7	359	0.3	0.13	0.7	4580	0.29	0.4	192	3.4	12.1	37	16.9
145708	2700	1.41	7	2	1.3	316	0.45	0.15	1.5	3190	0.31	0.8	104	6.9	12.2	27	37.4
145723	16700	1.95	7.5	4	1.6	284	0.3	0.47	0.9	3710	0.38	0.5	132	3.3	12.4	32	29.3
146798	2100	11.15	10.9	4	1.1	307	0.28	0.4	0.6	3950	0.35	0.3	144	4.5	14.7	34	17.9
146824	1700	3.66	20.5	3	1.8	355	0.4	0.18	1.5	5880	0.2	1.1	278	4.5	16.2	39	29.2

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.

Sample Id.	Sulphur S (ppm)	Antimony Sb (ppm)	Scandium Sc (ppm)	Selenium Se (ppm)	Tin Sn (ppm)	Strontium Sr (ppm)	Tantalum Ta (ppm)	Tellurium Te (ppm)	Thorium Th (ppm)	Titanium Ti (ppm)	Thallium Tl (ppm)	Uranium U (ppm)	Vanadium V (ppm)	Tungsten W (ppm)	Yttrium Y (ppm)	Zinc Zn (ppm)	Zirconium Zr (ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	100	0.05	1	1	0.2	0.2	0.05	0.05	0.2	50	0.02	0.1	1	0.1	0.1	2	0.5
Crustal Abundance: Fron	240	0.1	NA	0.05	0.5	1	0.8	NA	0.004	300	0.16	0.45	20	0.6	20	16	19
Crustal Abundance: To	2400	1.5	NA	0.6	6	2000	4.2	NA	17	13800	2.3	3.7	250	2.2	90	165	500
146831	3600	4.22	17.3	4	1.7	307	0.31	0.26	1.2	5190	0.23	1.2	237	7.2	15.8	55	30.5
146843																	
146861	1200	1.94	9.3	2	1	388	0.34	0.15	1.4	4140	0.29	0.6	71	1.9	18	20	31.1
146868	5200	2.67	9	4	1.4	305	0.33	0.14	1.4	3870	0.39	0.8	99	3.7	16.6	14	39.3
126352	7000	5.56	18.5	4	1.8	390	0.39	0.13	2.2	5540	0.28	1	238	3.1	16.8	42	31.9
126358	3700	5.19	17	3	1.5	335	0.41	0.16	2	5420	0.3	0.9	226	3.3	14.9	39	32.4
126374	1900	2.59	15.9	3	1.5	386	0.4	0.09	2	5440	0.21	0.9	217	6.7	16.2	34	31.6
126384	1200	3.03	11.3	2	1.4	434	0.46	0.11	2.1	4250	0.24	0.9	153	4.3	14	30	35.8
126391	1900	2.05	11	3	1.1	457	0.32	0.22	1.4	4300	0.21	0.6	151	1.8	14	28	24.7
146172	2400	9.48	11.2	3	1.5	268	0.21	0.25	0.5	3940	0.32	0.4	148	5.5	12.1	31	23.3
146182	1400	2.17	13.8	4	1.4	446	0.2	0.38	0.6	4430	0.2	0.3	184	3.6	15.2	41	17.6
146203	1800	5.1	11.7	2	1.6	294	0.22	0.11	0.6	3620	0.32	0.4	147	5.4	11.6	52	20.4
146214	3700	3.41	10.3	2	1.4	378	0.25	0.1	0.6	3540	0.3	0.4	152	3.5	13.8	28	21.6
146221	7400	4.35	23.2	4	2.9	420	0.26	0.2	1.4	7100	0.27	1.1	257	7.5	16.8	45	46.8
146238	1500	3.58	16.9	2	1.7	490	0.39	0.05	1.2	5460	0.28	0.7	235	8.9	16.2	30	25
147034	5200	5.3	8.2	6	2.3	251	0.21	0.46	0.7	3200	0.05	0.3	96	4.9	14.6	55	24.6
147038	3400	4.48	8	4	1.6	261	0.24	0.15	2.9	2650	0.28	1.4	86	2.8	10.7	24	52.4
147051	3200	4.83	9.6	2	2	390	0.31	*0.025*	1.7	4220	0.44	1.1	101	5.9	15.9	24	49.1
147070	6000	4.91	13.6	3	1.3	546	0.28	*0.025*	0.8	4770	0.27	0.4	165	4.7	20.1	36	20.4
147087	33800	3.95	14.3	5	1.1	411	0.25	0.45	0.8	4200	0.2	0.6	153	17.6	16.7	27	15
147097	7200	2.13	13	3	1.3	258	0.24	0.1	0.7	4400	0.49	0.4	147	4.4	17.7	92	19.3
145508	400	2.79	18.9	2	1.1	326	0.32	0.05	1	5700	0.17	0.7	286	11.8	12.6	48	35.1
145527	5500	5.67	17.6	3	1.6	382	0.41	0.19	2	5190	0.29	0.9	232	5.9	16.7	43	32.6
145543	1300	5.87	16.9	3	1.3	396	0.38	0.21	1.8	4950	0.26	0.8	214	4.4	15.1	42	29.5
145562	1000	5.44	16.8	3	1.3	325	0.36	0.18	1.7	5190	0.29	0.8	231	3	15.5	41	22.7
145576	7400	2.24	5.4	3	1.1	214	0.19	0.24	2.7	1340	0.28	1.4	49	3.9	7	13	38.6
145601	5800	2.26	16.9	6	1.4	472	0.41	0.29	2	5170	0.25	0.9	214	5.4	16.8	34	27.3
146297	3100	3.36	14	5	1.7	294	0.18	0.5	0.6	4200	0.31	0.6	197	11.4	15	33	24.8
146314	1500	5	12.6	3	1.3	377	0.21	0.28	0.6	4370	0.26	0.4	171	6	14.1	45	19.3
146335	1300	2.8	11.9	2	1.3	361	0.25	0.21	0.7	4180	0.32	0.3	151	5.9	16.3	48	15.3
146352	600	1.45	9.4	2	1	366	0.22	0.1	0.5	3590	0.15	0.3	142	5.2	11.4	55	14.1
146368	1900	1.42	10.3	2	1.1	335	0.23	0.2	0.5	4160	0.2	0.2	156	3.7	12.4	54	12.4
146390	1500	1.73	13.5	4	1.2	476	0.27	0.17	0.8	4660	0.2	0.4	162	5.4	17.9	39	14.3
146508	500	1.89	20.6	3	1.4	286	0.39	0.19	1.5	5510	0.31	0.7	281	8.5	14.3	54	24
146526	7400	0.9	11.3	3	0.9	512	0.28	0.22	0.9	3780	0.22	0.3	150	2.4	15.9	32	13.1
146544	2500	2.1	8.9	3	1	338	0.25	0.11	1.6	2810	0.23	0.6	108	2.9	11.5	27	27.3
146565	1100	5.71	6.3	3	0.8	295	0.23	0.16	0.7	3290	0.44	0.5	112	6.2	15.4	15	28
146589	1200	4.08	16.7	4	1.2	331	0.37	0.2	1.4	5080	0.31	0.9	242	2.5	14.8	29	29.5
146613	5900	3.35	15.1	4	3.2	394	0.37	0.21	1.4	4860	0.19	1.2	234	7.8	17.2	28	32.4
146627	700	3.68	9.6	3	0.9	201	0.19	0.24	1.2	3210	0.18	0.6	109	2.2	12.8	34	17.9
146637	4900	1.97	6.8	3	1.4	204	0.26	0.13	2.2	2260	0.37	1.5	74	5.2	9.1	21	44.9
146649	2800	1.34	6.3	2	1.4	336	0.34	*0.025*	3.1	2130	0.18	1.8	56	3	8.7	24	43.5
146657	2100	1.8	6.9	3	1.7	211	0.32	0.24	3.1	2140	0.16	1.8	67	9.8	7.1	16	40.3
146676	2100	3.63	9.7	3	5.3	348	0.28	0.22	0.8	4250	0.21	1.4	107	26.4	13.3	51	40.9
125188	2700	1.26	6.9	4	1	346	0.26	0.4	0.8	3080	0.26	0.5	72	3.8	13.5	28	34
125198	2300	1.43	6.7	3	1	310	0.29	0.51	0.8	3520	0.32	0.4	103	5.6	14.3	42	25.3

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.

Sample	Sulphur	Antimony	Scandium	Selenium	Tin	Strontium	Tantalum	Tellurium	Thorium	Titanium	Thallium	Uranium	Vanadium	Tungsten	Yttrium	Zinc	Zirconium
Id.	S	Sb	Sc	Se	Sn	Sr	Ta	Te	Th	Ti	Tl	U	V	W	Y	Zn	Zr
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	100	0.05	1	1	0.2	0.2	0.05	0.05	0.2	50	0.02	0.1	1	0.1	0.1	2	0.5
Crustal Abundance: Fron	240	0.1	NA	0.05	0.5	1	0.8	NA	0.004	300	0.16	0.45	20	0.6	20	16	19
Crustal Abundance: To	2400	1.5	NA	0.6	6	2000	4.2	NA	17	13800	2.3	3.7	250	2.2	90	165	500
125207	1200	2.51	5.7	3	0.9	252	0.28	0.29	0.7	3190	0.32	0.3	88	2.7	13.4	37	17.3
125228	1600	1.37	5.3	3	1.4	296	0.33	0.23	2.9	1980	0.15	2	49	5.8	7.4	19	42.2
125244	1500	1.28	5.6	2	1.6	335	0.35	0.17	2.4	1980	0.1	1.5	57	23.9	7	26	43.9
125257	900	2.76	30.9	1	0.7	321	0.2	*0.025*	0.4	4900	0.04	0.1	175	0.5	15.5	65	67
125278	300	4.19	10.7	1	6	504	0.3	0.05	1.2	4680	0.09	1.3	176	7.5	16.6	53	40.5
125596	1400	2.61	13.2	2	1.3	386	0.25	0.15	0.6	4260	0.26	0.5	156	7.5	15.9	45	23.3
125610	600	1.58	11.5	2	1.1	217	0.28	0.16	0.6	3690	0.19	0.5	143	4.8	10.7	60	20.3
125626																	
125641	1200	2.17	16.6	4	1.4	250	0.34	0.35	1.2	5280	0.21	0.6	256	4.5	12.1	67	24.9
125669	11100	3.12	13.1	4	1.6	192.5	0.29	0.33	2.3	3930	0.29	1.6	157	7.3	12.9	51	67.3
125690	1000	1.19	14.1	1	1	358	0.42	0.07	1.4	4630	0.19	0.7	194	2.3	13.7	38	31.3
West Breccia Zone																	
14018	8800	3.69	7.9	2	1.1	428	0.32	0.26	3.7	2400	0.6	2.3	70	12.8	10.8	41	50.3
14021	7000	6.36	7.7	2	1.2	173	0.28	0.09	3.3	2080	0.75	1.9	65	18.4	12.5	56	45.5
14036	16000	7.99	7.3	4	1.5	235	0.21	0.72	3.3	1970	0.71	1.9	67	25	10.2	41	41.3
14043	2800	4.34	10.2	2	1	276	0.22	0.07	2.3	2190	0.42	1.4	102	27	7.6	45	40.3
14060	14800	2.49	16.5	3	1	423	0.22	0.06	2.4	4100	0.44	1.6	155	30.1	17.1	27	66.3
14067	4300	3.8	21.1	4	1.1	410	0.17	0.06	1.5	4170	0.38	1.1	182	12.1	17.5	71	49.5
14076	9500	5.5	24.4	2	1.2	365	0.18	0.18	1.9	4540	0.47	1	197	6.5	19.9	163	55.8
14083	16000	5.68	24.7	2	1.6	232	0.16	0.27	1.7	4480	0.95	0.9	204	10.3	19.5	127	40.6
14099	3600	3.71	5	1	0.6	88	0.24	0.05	2.7	1670	1.04	1.9	47	17.4	8.2	205	33.7
14103	7700	4.72	10.2	3	1.1	197.5	0.24	0.05	3	2220	0.67	1.8	119	20.2	10.4	67	51.2
125046	1400	10.95	14.8	3	2.3	482	0.43	0.07	1.1	4830	0.18	1.3	198	44.5	14.8	228	32.9
125068	4500	7.54	17.5	4	2.2	558	0.43	0.45	1.4	5270	0.19	1.2	223	39.3	15.7	77	30
125073	5900	3.46	8.4	8	1.7	386	0.33	1.01	1.3	3640	0.26	1	126	26.1	15.4	57	39.2
125079	13200	83.3	6.6	13	1.9	270	0.23	2.11	1	2940	0.38	0.7	119	19.9	14.2	75	29.5
125084	6100	20.1	15.7	5	2.8	601	0.37	0.85	1.2	5010	0.19	1.2	235	6.3	15.5	131	23.9
125127	900	1.86	16.6	3	1.4	382	0.41	0.18	1.3	5080	0.22	1	213	20.4	15.5	36	18.2
125129	2500	4.49	16	4	1.4	221	0.3	0.33	1.2	4340	0.22	0.7	202	35.8	14	63	20
125134	6100	1.87	15.9	5	1.3	281	0.34	0.2	1.7	4360	0.25	0.9	245	26.5	14.9	51	22.3
125142	2600	2.68	16.1	4	1.2	272	0.3	0.65	1.8	4110	0.21	1.1	164	13.3	13.5	68	22.1
125149	1400	2.58	15.3	2	1.1	301	0.41	0.16	1.5	4290	0.21	1	201	17.2	14.9	55	21.5
125154	800	1.98	6.5	2	3.4	252	0.29	0.18	0.9	3190	0.08	4.2	124	8.1	12.8	48	61.4
125165	2000	6.54	8.8	2	2.3	676	0.36	0.23	0.7	4360	0.09	1.3	100	15.9	17.4	30	21.2
125176	2400	3.08	6.9	2	1.7	399	0.3	0.17	0.6	3530	0.11	1	81	24.1	12	42	21.9
146112	1200	8.52	7.4	2	1.6	541	0.31	0.08	1	4060	0.14	0.6	101	3.1	15.8	64	20.1
146115	1400	3.56	32.3	2	1.2	513	0.29	*0.025*	0.8	8300	0.09	0.3	275	0.6	23.9	100	84.3
146124	900	1.8	7	2	0.7	484	0.26	*0.025*	0.6	3970	0.27	0.2	92	5.4	14.8	77	16.2
146127	10600	2.21	5.4	2	0.7	162	0.29	0.14	4.4	1620	0.22	1.9	53	2.9	6.9	35	60.2
146135	500	4.28	6.8	2	1.4	678	0.27	0.05	0.7	4010	0.14	0.6	106	5.8	15.6	67	28.4
146149	700	2.42	6.4	2	1	565	0.27	*0.025*	0.7	3810	0.17	0.4	93	11.6	15.2	100	25.2
146161	400	18.15	17.5	1	0.9	656	0.25	*0.025*	0.8	5250	0.12	0.4	172	17.9	14.5	102	18.8
146164	200	4.06	14	1	0.8	440	0.27	*0.025*	0.6	5940	0.14	0.3	250	1.5	12.7	103	15.3
145951	1700	4.26	9.2	2	1.5	253	0.34	0.05	1.1	4600	0.22	0.7	107	6.6	14.6	61	30.1
145956	1800	2.27	15.6	3	1.9	286	0.34	0.08	1.1	4660	0.18	0.8	211	14.4	13.6	112	21.2
145974	100	2.11	9.2	1	1.2	240	0.39	0.1	0.9	4220	0.21	0.5	152	10.5	13.5	103	23.7

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.

Sample	Sulphur	Antimony	Scandium	Selenium	Tin	Strontium	Tantalum	Tellurium	Thorium	Titanium	Thallium	Uranium	Vanadium	Tungsten	Yttrium	Zinc	Zirconium
Id.	S	Sb	Sc	Se	Sn	Sr	Ta	Te	Th	Ti	Tl	U	V	W	Y	Zn	Zr
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	100	0.05	1	1	0.2	0.2	0.05	0.05	0.2	50	0.02	0.1	1	0.1	0.1	2	0.5
Crustal Abundance: Fron	240	0.1	NA	0.05	0.5	1	0.8	NA	0.004	300	0.16	0.45	20	0.6	20	16	19
Crustal Abundance: To	2400	1.5	NA	0.6	6	2000	4.2	NA	17	13800	2.3	3.7	250	2.2	90	165	500
145982	500	2.43	26.1	1	0.9	450	0.39	*0.025*	1.5	6560	0.05	0.6	235	0.9	22.3	91	86.3
145992	2800	3.42	9.6	2	3	224	0.35	0.27	1.1	4170	0.2	1.2	137	13.9	13	82	30.1
145999	1300	2.03	9.9	1	1.6	379	0.38	0.06	1.2	4130	0.13	0.6	121	6	14.1	52	22.5
145834	300	12.85	9.4	2	1.2	662	0.33	*0.025*	1	4050	0.1	0.6	137	1.6	16.6	130	25.1
145842	300	44.9	32.6	2	4.8	1260	0.22	0.07	1.7	6610	0.02	1.9	272	1.4	30.5	159	46.7
145852	1100	32.3	9.4	2	1.9	941	0.31	*0.025*	0.9	3690	0.02	0.7	145	1.8	14.6	106	24.8
145857	100	6.43	9.8	1	1.4	904	0.37	*0.025*	1.2	4450	0.08	0.7	137	1.2	15.1	50	26.8
145871	1700	6.14	7.4	1	0.9	578	0.37	*0.025*	0.7	3650	0.12	0.4	116	11	13.2	72	21.3
145608	9300	3.81	26	2	1.2	462	0.13	0.2	1.3	4540	0.29	0.5	153	2.4	17.2	45	23.1
145614	6300	2.98	26.7	3	2.1	447	0.13	1.37	1.4	4410	0.34	0.5	173	2.2	19	52	29.8
145628	8700	1.47	22	3	1	230	0.13	0.1	1.2	3860	0.08	0.4	174	4.8	16.2	77	32.7
145640	8000	2.23	27.5	3	1.2	375	0.13	0.2	1.3	4550	0.33	0.5	207	3.8	19	1040	24.7
145646	6100	3.1	26.7	3	1.1	437	0.12	0.16	1.2	4460	0.17	0.4	189	2.6	19.2	99	19.9
Paramount Zone																	
125965	3900	3.38	17.1	3	2.4	286	0.21	0.16	1.8	3520	0.18	1.6	172	152	13.2	103	32.5
125974	17700	1.86	13.6	3	2.1	154	0.22	0.14	1.8	3370	0.19	1.8	143	14.5	10	52	30.9
125983	3000	3.43	20.9	2	1.9	308	0.22	0.11	1.9	2870	0.14	1.4	167	10.3	11.3	91	29.7
125988	400	1.41	25.3	2	0.9	597	0.35	*0.025*	1.9	5410	0.15	0.7	214	0.4	20.7	89	103
126007	1600	2.52	5.1	3	1.1	250	0.22	0.21	2.7	1680	0.33	1.3	63	7.1	6.5	63	26.4
126031	1500	1.54	6.1	2	0.8	326	0.28	0.17	3	1890	0.19	1.6	57	9	7.7	48	35.1
126040	7200	1.74	15.1	3	2.1	254	0.22	0.18	2.4	2980	0.13	1.9	157	71.1	9.6	50	32.7
126054	1800	5.21	22.7	2	1.8	227	0.18	0.07	1.6	3400	0.12	1.4	194	48.1	12.4	203	37.5
126067	3100	8	22	2	2.4	312	0.18	0.07	1.5	3340	0.19	1.6	180	80.7	12.5	167	26.5
126081	10700	2.87	5.3	10	1.4	194	0.27	0.51	4.5	1600	0.7	1.7	59	15.1	6.1	37	42.5
126110	700	2.73	28	2	1.1	663	0.31	*0.025*	2	5620	0.24	0.7	254	1.6	21.2	92	81.3
126118	7800	1.76	21.8	6	2.4	192.5	0.39	0.4	1.6	5690	0.26	1	230	19.6	14.3	76	24.1
125904	1900	1.48	10.8	3	3.4	340	0.3	0.41	0.9	3600	0.19	1.1	155	20.2	13.4	46	17
125919	5200	1.71	13	5	2.1	502	0.3	0.24	0.9	3980	0.18	0.9	168	27.2	13.8	61	14.2
125928	1000	1.94	14.9	2	1.4	490	0.39	0.13	1.2	4850	0.17	0.8	211	16.5	13.4	97	17.6
125933	200	2.69	26.4	2	1.3	408	0.46	*0.025*	1	7390	0.11	0.5	243	11.2	24.4	147	81.4
125944	1400	2.77	16.1	2	1	582	0.37	0.08	1.2	5020	0.15	0.7	201	13.9	14.7	103	13.5
125952	11700	1.49	6.2	2	1.1	211	0.3	0.07	3	2020	0.2	1.7	58	8.1	7.5	29	34.9
125963	4600	2.12	16.1	3	1.6	333	0.29	0.1	0.9	4450	0.16	1.1	175	24.9	13.8	128	17.2
126120	700	0.91	5.3	2	1.2	394	0.28	0.48	3	1860	0.15	1.6	63	6.9	6.8	39	38.5
126131	300	1.27	8.9	2	3.6	350	0.33	0.12	3.8	2760	0.12	1.5	115	15.5	12.5	54	33.6
126142	600	1.55	10.3	2	3.6	312	0.35	0.12	2.9	3400	0.17	1.4	143	12.5	13	158	28.1
126154	1400	1.23	13.9	3	7.7	310	0.36	0.27	1.6	4580	0.09	2.2	226	12.9	14.6	123	30.8
126171	14900	1.42	13	4	1.2	373	0.22	0.06	2.7	3250	0.23	1.9	116	10.3	12	69	53.4
126181	2800	1.46	13.2	2	1	469	0.35	*0.025*	1.1	4780	0.12	0.5	203	2	14.1	103	16.3
125806	5200	1.73	9.4	2	1	421	0.33	0.06	3.1	2580	0.27	1.6	75	5.7	10.6	45	45.9
125816	200	3.31	27.2	1	1.2	612	0.45	*0.025*	2.6	6350	0.26	1.1	251	6	23.9	128	127.5
125833	3100	1.3	6	4	2	292	0.26	0.38	3	1770	0.3	1.8	61	9.4	7.1	44	32.1
125861	3700	0.95	5.6	3	1	293	0.23	0.21	2.9	1650	0.18	2.2	59	6.6	7.1	24	26.9
125875	2400	0.8	6	3	1.1	297	0.34	0.24	4.1	1940	0.22	2.8	60	11.9	7.3	31	51.2
125897	800	1.21	5.9	2	1.1	186.5	0.39	0.12	11.2	1800	0.19	4.3	59	5.3	9.7	23	58.2

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.

Sample	Sulphur	Antimony	Scandium	Selenium	Tin	Strontium	Tantalum	Tellurium	Thorium	Titanium	Thallium	Uranium	Vanadium	Tungsten	Yttrium	Zinc	Zirconium
Id.	S	Sb	Sc	Se	Sn	Sr	Ta	Te	Th	Ti	Tl	U	V	W	Y	Zn	Zr
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	100	0.05	1	1	0.2	0.2	0.05	0.05	0.2	50	0.02	0.1	1	0.1	0.1	2	0.5
Crustal Abundance: Fron	240	0.1	NA	0.05	0.5	1	0.8	NA	0.004	300	0.16	0.45	20	0.6	20	16	19
Crustal Abundance: To	2400	1.5	NA	0.6	6	2000	4.2	NA	17	13800	2.3	3.7	250	2.2	90	165	500
Tailings																	
LIARD ZONE	900	2.74	11	3	2.5	280	0.29	0.15	1.3	3640	0.25	0.9	150	6	13.5	42	43.2
PARAMOUNT	1800	2.28	11.7	4	4	275	0.29	0.26	2.6	2950	0.24	1.8	126	22.2	11.7	61	57.7
WEST BRECCIA	2500	5.72	14.6	3	5	432	0.28	0.29	1.4	4180	0.27	1.4	174	21.2	15.9	79	49.1
High-Sulphide Histor																	
T112 (171' - 172')	92700	6.38	28.4	7	1.9	361	0.17	1.49	0.7	5750	0.08	0.9	269	7	16.4	96	30
T113 (81' - 82')	9800	2.07	8.5	3	1.4	375	0.24	0.1	4	1950	0.33	2.1	72	5.2	7.8	29	49.4
T113 (983' - 985')	22600	3.75	17.4	5	3.4	174	0.15	0.23	3	2330	0.48	2.7	125	412	12.5	53	58.6
T140 (30' - 31')	1500	3.73	12.5	4	1.4	249	0.25	0.21	1	4410	0.43	0.9	166	25.7	17.7	32	34.5
T166 (389' - 390')	8900	1.38	6.1	3	1.5	318	0.2	0.05	2.6	1680	0.23	1.1	59	4.4	7.3	15	32.5
T185 (116' - 117')	23700	1.32	9	5	2.6	165.5	0.21	0.17	4	1470	0.47	2.3	72	13.2	9.6	13	82.1
T207 (261.5' - 262')	39100	1.24	6.5	8	1.3	94.7	0.21	0.46	3.7	1500	0.2	8.5	62	11.1	7.2	13	22.7
T207 (269' - 271')	**100000**	2.66	5.1	27	1.5	65.6	0.22	2.15	3.2	1550	0.2	2.1	67	7.7	7.8	35	18.8
All Data																	
Maximum	100000	83.3	33.3	27	7.7	1260	0.46	2.15	11.2	8300	1.04	8.5	286	412	30.5	1040	128
Minimum	100	0.8	5	0.5	0.6	65.6	0.12	0.025	0.4	1320	0.02	0.1	47	0.3	6	7	12.4
Mean	5129	4.08	13	3.23	1.58	350	0.29	0.23	1.52	4044	0.26	0.97	153	11.1	14	57.6	33.2
Standard Deviation	10078	6.64	6.24	2.19	0.86	139	0.069	0.27	1.07	1267	0.13	0.78	62.1	29.6	3.51	73.1	17.2
10 Percentile	700	1.39	6.3	2	0.94	215	0.21	0.05	0.7	1996	0.12	0.4	67	2.3	8.58	24.8	17.9
25 Percentile	1400	1.85	8.25	2	1.1	264	0.25	0.09	0.8	3385	0.19	0.5	104	3.4	12.4	32	22.1
Median	2300	2.68	11.4	3	1.4	330	0.29	0.16	1.2	4140	0.26	0.7	151	5.6	14.4	43	28.4
75 Percentile	5450	4.38	16.1	4	1.7	402	0.34	0.26	1.85	4680	0.31	1.2	202	10.5	15.9	61	39.3
90 Percentile	10660	6.41	22	5	2.3	497	0.39	0.46	2.9	5490	0.38	1.8	238	20.1	17.3	101	53.7
Interquartile Range (IC	4050	2.52	7.85	2	0.6	138	0.09	0.16	1.05	1295	0.12	0.7	99	7.1	3.5	29	17.2
Variance	101560698	44.1	38.9	4.81	0.73	19426	0.0048	0.072	1.15	1605212	0.017	0.61	3859	874	12.3	5347	295
Skewness	6.83	8.76	1.06	6.17	3.46	2.14	-0.0096	4.21	3.78	0.08	2.09	4.7	0.18	11.3	0.25	10.6	2.02
Coefficient of Variatior	1.96	1.63	0.48	0.68	0.54	0.4	0.24	1.18	0.7	0.31	0.5	0.81	0.41	2.67	0.25	1.27	0.52
Count	235	235	235	235	235	235	235	235	235	235	235	235	235	235	235	235	235
Main Zone																	
Maximum	33800	11.2	33.3	8	6	798	0.46	0.85	3.1	7930	0.49	2	286	26.4	21.3	112	93.6
Minimum	100	0.83	5	0.5	0.7	141	0.16	0.025	0.4	1320	0.04	0.1	47	0.3	6	7	12.4
Mean	3932	3.29	12.4	3.22	1.47	331	0.3	0.21	1.25	4213	0.27	0.74	157	5.5	14.1	39.4	30.7
Standard Deviation	4860	1.97	5.31	1.25	0.66	89.5	0.061	0.16	0.65	1112	0.08	0.39	61.1	3.78	2.69	15.2	13.9
10 Percentile	1000	1.41	6.8	2	0.95	222	0.22	0.055	0.6	3025	0.17	0.35	77	2.4	11	23.5	17.8
25 Percentile	1425	1.89	8.4	2	1.1	269	0.26	0.11	0.8	3722	0.22	0.5	110	3.3	12.8	29	21.1
Median	2200	2.6	11.4	3	1.4	328	0.29	0.17	1.05	4205	0.28	0.6	151	4.5	14.6	39	27.1
75 Percentile	4600	4.39	15.2	4	1.6	382	0.34	0.26	1.5	4838	0.31	0.9	205	6.18	15.9	47	35.8
90 Percentile	7400	5.69	19	5	1.85	424	0.38	0.44	2.2	5485	0.37	1.35	240	9.6	16.8	55	47
Interquartile Range (IC	3175	2.5	6.77	2	0.5	113	0.08	0.15	0.7	1115	0.09	0.4	95.5	2.88	3.07	18	14.7
Variance	23619966	3.89	28.2	1.57	0.43	8016	0.0037	0.024	0.42	1237107	0.0065	0.15	3729	14.3	7.25	230	193
Skewness	3.25	1.46	1.19	0.97	4.13	1.16	0.22	1.63	1.23	0.038	-0.14	1.18	0.23	2.58	-0.88	1.19	1.73
Coefficient of Variatior	1.24	0.6	0.43	0.39	0.45	0.27	0.2	0.74	0.52	0.26	0.3	0.52	0.39	0.69	0.19	0.38	0.45
Count	146	146	146	146	146	146	146	146	146	146	146	146	146	146	146	146	146

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.

Sample Id.	Sulphur S (ppm)	Antimony Sb (ppm)	Scandium Sc (ppm)	Selenium Se (ppm)	Tin Sn (ppm)	Strontium Sr (ppm)	Tantalum Ta (ppm)	Tellurium Te (ppm)	Thorium Th (ppm)	Titanium Ti (ppm)	Thallium Tl (ppm)	Uranium U (ppm)	Vanadium V (ppm)	Tungsten W (ppm)	Yttrium Y (ppm)	Zinc Zn (ppm)	Zirconium Zr (ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	100	0.05	1	1	0.2	0.2	0.05	0.05	0.2	50	0.02	0.1	1	0.1	0.1	2	0.5
Crustal Abundance: Fron	240	0.1	NA	0.05	0.5	1	0.8	NA	0.004	300	0.16	0.45	20	0.6	20	16	19
Crustal Abundance: To	2400	1.5	NA	0.6	6	2000	4.2	NA	17	13800	2.3	3.7	250	2.2	90	165	500

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.

Sample	Sulphur	Antimony	Scandium	Selenium	Tin	Strontium	Tantalum	Tellurium	Thorium	Titanium	Thallium	Uranium	Vanadium	Tungsten	Yttrium	Zinc	Zirconium
Id.	S	Sb	Sc	Se	Sn	Sr	Ta	Te	Th	Ti	Tl	U	V	W	Y	Zn	Zr
	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	100	0.05	1	1	0.2	0.2	0.05	0.05	0.2	50	0.02	0.1	1	0.1	0.1	2	0.5
Crustal Abundance: Fron	240	0.1	NA	0.05	0.5	1	0.8	NA	0.004	300	0.16	0.45	20	0.6	20	16	19
Crustal Abundance: To	2400	1.5	NA	0.6	6	2000	4.2	NA	17	13800	2.3	3.7	250	2.2	90	165	500
West Breccia Zone																	
Maximum	16000	83.3	32.6	13	4.8	1260	0.43	2.11	4.4	8300	1.04	4.2	275	44.5	30.5	1040	86.3
Minimum	100	1.47	5	1	0.6	88	0.12	0.025	0.6	1620	0.02	0.2	47	0.6	6.9	27	15.3
Mean	4389	8.01	14.3	2.72	1.52	427	0.28	0.25	1.49	4135	0.27	1.02	154	13	15.2	102	34
Standard Deviation	4456	13.8	7.77	2.02	0.77	222	0.086	0.39	0.86	1270	0.23	0.71	59.9	11	4.07	146	17
10 Percentile	360	2.01	6.72	1	0.9	223	0.15	0.025	0.7	2208	0.08	0.4	76.6	1.56	10.6	41	20
25 Percentile	1000	2.46	7.8	2	1.1	262	0.22	0.05	0.95	3670	0.12	0.55	106	3.45	13.4	51.5	22
Median	2500	3.8	10.2	2	1.2	399	0.29	0.1	1.2	4170	0.21	0.9	152	11	14.9	71	28.4
75 Percentile	6650	6.4	17.5	3	1.7	527	0.34	0.22	1.7	4545	0.34	1.25	202	19.2	16.8	102	41
90 Percentile	9940	15	26.3	4	2.3	668	0.39	0.68	2.82	5258	0.63	1.9	235	26.7	19.3	142	57.6
Interquartile Range (IC	5650	3.93	9.7	1	0.6	266	0.12	0.17	0.75	875	0.21	0.7	95	15.7	3.5	51	19
Variance	19857493	190	60.4	4.07	0.6	49443	0.0075	0.16	0.75	1613686	0.054	0.5	3590	121	16.6	21428	288
Skewness	1.21	4.26	0.82	3.36	2.22	1.51	-0.31	3.17	1.69	0.45	1.75	2.2	0.16	0.99	1.06	5.98	1.5
Coefficient of Variatior	1.02	1.72	0.54	0.74	0.51	0.52	0.3	1.6	0.58	0.31	0.85	0.69	0.39	0.84	0.27	1.44	0.5
Count	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47
Paramount Zone																	
Maximum	17700	8	28	10	7.7	663	0.46	0.51	11.2	7390	0.7	4.3	254	152	24.4	203	128
Minimum	200	0.8	5.1	1	0.8	154	0.18	0.025	0.9	1600	0.09	0.5	57	0.4	6.1	23	13.5
Mean	3919	2.19	13.9	2.87	1.87	353	0.3	0.17	2.51	3529	0.2	1.5	146	21.2	12.4	81.4	40
Standard Deviation	4427	1.43	7.33	1.67	1.34	134	0.075	0.14	1.88	1555	0.11	0.75	68.4	30.4	4.85	46.4	26.3
10 Percentile	400	1.21	5.6	2	1	194	0.22	0.025	1	1770	0.12	0.7	59	5.3	7.1	31	17
25 Percentile	900	1.42	6.15	2	1.1	270	0.22	0.07	1.55	1980	0.15	1.05	63	7	8.65	45.5	26.4
Median	2400	1.73	13.2	2	1.4	312	0.3	0.12	2	3370	0.18	1.5	157	11.9	12.5	69	32.5
75 Percentile	4900	2.71	19	3	2.1	414	0.35	0.22	3	4680	0.22	1.75	202	18	14	103	44.2
90 Percentile	10700	3.38	25.3	4	3.4	582	0.39	0.4	3.8	5620	0.27	2.2	230	48.1	20.7	147	81.3
Interquartile Range (IC	4000	1.3	12.8	1	1	144	0.12	0.15	1.45	2700	0.075	0.7	139	11	5.3	57.5	17.8
Variance	19600280	2.06	53.7	2.78	1.79	17921	0.0056	0.019	3.55	2418929	0.012	0.56	4682	922	23.5	2155	689
Skewness	1.8	2.62	0.49	2.98	3.04	0.79	0.23	1.15	3.43	0.63	3.41	1.78	-0.074	3.23	0.98	0.84	1.91
Coefficient of Variatior	1.13	0.66	0.53	0.58	0.71	0.38	0.25	0.82	0.75	0.44	0.53	0.5	0.47	1.43	0.39	0.57	0.66
Count	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31	31

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **ICP Metals Data**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.
Rare earth elements may not be totally soluble in MS61 method.

Sample Id.	Sulphur S (ppm)	Antimony Sb (ppm)	Scandium Sc (ppm)	Selenium Se (ppm)	Tin Sn (ppm)	Strontium Sr (ppm)	Tantalum Ta (ppm)	Tellurium Te (ppm)	Thorium Th (ppm)	Titanium Ti (ppm)	Thallium Tl (ppm)	Uranium U (ppm)	Vanadium V (ppm)	Tungsten W (ppm)	Yttrium Y (ppm)	Zinc Zn (ppm)	Zirconium Zr (ppm)
Method	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61	ME-MS61
MDL	100	0.05	1	1	0.2	0.2	0.05	0.05	0.2	50	0.02	0.1	1	0.1	0.1	2	0.5
Crustal Abundance: Fron	240	0.1	NA	0.05	0.5	1	0.8	NA	0.004	300	0.16	0.45	20	0.6	20	16	19
Crustal Abundance: To	2400	1.5	NA	0.6	6	2000	4.2	NA	17	13800	2.3	3.7	250	2.2	90	165	500
Tailings																	
Maximum	2500	5.72	14.6	4	5	432	0.29	0.29	2.6	4180	0.27	1.8	174	22.2	15.9	79	57.7
Minimum	900	2.28	11	3	2.5	275	0.28	0.15	1.3	2950	0.24	0.9	126	6	11.7	42	43.2
Mean	1733	3.58	12.4	3.33	3.83	329	0.29	0.23	1.77	3590	0.25	1.37	150	16.5	13.7	60.7	50
Standard Deviation	802	1.87	1.91	0.58	1.26	89.2	0.0058	0.074	0.72	617	0.015	0.45	24	9.08	2.11	18.5	7.29
10 Percentile	1080	2.37	11.1	3	2.8	276	0.28	0.17	1.32	3088	0.24	1	131	9.04	12.1	45.8	44.4
25 Percentile	1350	2.51	11.4	3	3.25	278	0.29	0.2	1.35	3295	0.24	1.15	138	13.6	12.6	51.5	46.2
Median	1800	2.74	11.7	3	4	280	0.29	0.26	1.4	3640	0.25	1.4	150	21.2	13.5	61	49.1
75 Percentile	2150	4.23	13.2	3.5	4.5	356	0.29	0.28	2	3910	0.26	1.6	162	21.7	14.7	70	53.4
90 Percentile	2360	5.12	14	3.8	4.8	402	0.29	0.28	2.36	4072	0.27	1.72	169	22	15.4	75.4	56
Interquartile Range (IC	800	1.72	1.8	0.5	1.25	78.5	0.005	0.07	0.65	615	0.015	0.45	24	8.1	2.1	18.5	7.25
Variance	643333	3.49	3.64	0.33	1.58	7963	0.000033	0.0054	0.52	380100	0.00023	0.2	576	82.4	4.44	342	53.2
Skewness	-0.37	1.61	1.47	1.73	-0.59	1.73	-1.73	-1.41	1.69	-0.36	0.94	-0.33	0	-1.71	0.42	-0.081	0.55
Coefficient of Variatior	0.46	0.52	0.15	0.17	0.33	0.27	0.02	0.32	0.41	0.17	0.06	0.33	0.16	0.55	0.15	0.3	0.15
Count	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
High-Sulphide Histor																	
Maximum	100000	6.38	28.4	27	3.4	375	0.25	2.15	4	5750	0.48	8.5	269	412	17.7	96	82.1
Minimum	1500	1.24	5.1	3	1.3	65.6	0.15	0.05	0.7	1470	0.08	0.9	59	4.4	7.2	13	18.8
Mean	37288	2.82	11.7	7.75	1.88	225	0.21	0.61	2.78	2580	0.3	2.58	112	60.8	10.8	35.8	41.1
Standard Deviation	38264	1.76	7.85	7.98	0.75	119	0.033	0.78	1.29	1609	0.15	2.49	73.9	142	4.25	27.9	21.2
10 Percentile	6680	1.3	5.8	3	1.37	86	0.16	0.085	0.91	1491	0.16	0.9	61.1	4.96	7.27	13	21.5
25 Percentile	9575	1.36	6.4	3.75	1.4	148	0.19	0.15	2.2	1538	0.2	1.05	65.8	6.55	7.68	14.5	28.2
Median	23150	2.37	8.75	5	1.5	212	0.21	0.22	3.1	1815	0.28	2.1	72	9.4	8.7	30.5	33.5
75 Percentile	52500	3.74	13.7	7.25	2.08	329	0.22	0.72	3.78	2850	0.44	2.4	135	16.3	13.5	39.5	51.7
90 Percentile	94890	4.54	20.7	13.7	2.84	365	0.24	1.69	4	4812	0.47	4.44	197	142	16.8	65.9	65.6
Interquartile Range (IC	42925	2.37	7.32	3.5	0.68	181	0.032	0.56	1.58	1312	0.24	1.35	69.5	9.77	5.8	25	23.5
Variance	1.464E+09	3.11	61.6	63.6	0.56	14107	0.0011	0.61	1.65	2589514	0.022	6.2	5467	20185	18.1	779	448
Skewness	1.09	1.26	1.65	2.56	1.56	-0.000078	-0.52	1.56	-0.89	1.52	-0.069	2.41	1.69	2.82	0.91	1.67	1.12
Coefficient of Variatior	1.03	0.63	0.67	1.03	0.4	0.53	0.16	1.28	0.46	0.62	0.49	0.97	0.66	2.34	0.39	0.78	0.52
Count	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8

19.5 NOTE: if data is boxed, then data is 3 times the maximum crustal abundance.

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

NOTE: If data was reported as > detection limit the detection limit is shown in bold and was used in subsequent calculations.

Project:	**Schaft Creek**
Client:	Copper Fox Metals Inc.
Data:	**Whole Rock by XRF**
Comments:	2005 core samples were collected by MDAG on Feb 7'07. 2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Al_2O_3	BaO	CaO	Cr_2O_3	Fe_2O_3	K_2O	MgO	MnO	Na_2O	P_2O_5	SiO_2	SrO	TiO_2	LOI	Total
	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
Method	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06
MDL	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		
Main Zone															
14130	17.11	0.06	3.59	*0.005*	2.6	2.11	1.61	0.02	4.61	0.28	60.15	0.03	0.53	5.91	98.62
14144	18.29	0.04	4.95	*0.005*	5.05	1.84	1.81	0.05	4.05	0.36	53.8	0.04	0.63	7.48	98.40
14148	16.83	0.07	6.26	*0.005*	5.63	2.49	3.13	0.05	1.72	0.26	52	0.03	0.64	9.85	98.97
14156	15.34	0.03	3.29	*0.005*	2.46	1.41	1.21	0.03	4.53	0.1	64.96	0.03	0.29	4.66	98.35
14162	14.36	0.06	7.5	0.01	5.92	1.79	3.97	0.1	2.27	0.2	50.21	0.02	0.69	11.1	98.20
14169	15.54	0.01	3.15	*0.005*	1.69	1.07	0.61	0.03	5.76	0.12	66.91	0.02	0.31	3.74	98.97
14232	19.47	0.02	3.67	*0.005*	3.86	2.01	1.48	0.02	5.31	0.3	56.55	0.04	0.61	5.19	98.54
14250	18.02	0.02	5.47	*0.005*	6.59	1.67	2.87	0.05	4.48	0.28	51.91	0.04	0.75	6.29	98.45
14260	17.85	0.02	4.18	*0.005*	6.23	1.9	2.21	0.03	4.77	0.28	54.62	0.04	0.72	5.77	98.63
14276	19.76	0.12	5.87	*0.005*	5.6	0.86	2.56	0.14	4.97	0.29	54.07	0.08	0.67	3.49	98.49
14295	17.5	0.01	5.22	*0.005*	6.81	1.83	2.43	0.05	4	0.27	53.53	0.03	0.73	6.48	98.90
14301	17.72	0.03	4.93	*0.005*	4.47	2.34	2	0.06	3.33	0.28	54.86	0.02	0.7	7.95	98.70
14323	19.07	0.03	5.02	*0.005*	5.54	2.1	1.55	0.04	4.17	0.28	54.65	0.04	0.56	5.5	98.56
14332	19.78	0.02	4.67	*0.005*	5.19	2.46	1.71	0.03	4.03	0.3	54.16	0.04	0.6	5.57	98.57
14345	19.52	0.02	3.44	*0.005*	3.18	2.73	1.64	0.01	4.47	0.28	57.5	0.03	0.58	5.16	98.57
14348	19.93	0.02	3.09	*0.005*	5.12	2.25	1.97	0.02	4.79	0.31	54.97	0.03	0.61	5.01	98.13
14797	18.18	0.02	5.12	*0.005*	6.2	2.28	2.46	0.06	3.22	0.27	51.74	0.03	0.7	8.21	98.50
14808	15.54	0.02	6.64	*0.005*	5.44	2.49	2.62	0.06	2.5	0.23	52.62	0.02	0.56	10.2	98.95
14816	17.11	0.02	4.56	*0.005*	6.06	2.5	2.78	0.05	3.25	0.26	53.34	0.03	0.65	7.62	98.24
14828	17.1	0.08	5.7	*0.005*	5.75	1.94	2.73	0.06	3.81	0.25	51.87	0.04	0.63	8.24	98.21
14844	17.61	0.04	3.8	*0.005*	7.4	1.98	5.94	0.03	2.92	0.26	52.79	0.03	0.93	5.17	98.91
14680	17.54	0.03	5.54	0.01	6.31	1.81	2.5	0.06	4.05	0.26	53.34	0.04	0.67	6.08	98.24
14871	18.56	0.01	4.62	*0.005*	6.55	1.36	2.87	0.04	5.16	0.24	53.53	0.04	0.82	4.77	98.58
14887	17.6	0.04	6.71	*0.005*	7.31	1.24	3.61	0.07	4.05	0.23	50.56	0.04	0.79	6.23	98.49
14689	15.75	0.01	2.71	*0.005*	1.96	1.91	0.91	0.03	4.34	0.11	66.25	0.02	0.33	3.81	98.15
14695	17.98	0.02	4.98	*0.005*	5.19	2.57	2.41	0.07	3.57	0.26	53.38	0.02	0.68	7.34	98.48
14742	18.48	0.02	3.84	*0.005*	4.8	1.49	3.39	0.04	5.21	0.25	54.87	0.03	0.86	4.97	98.26
14666	17.45	0.04	5.2	*0.005*	7.38	1.53	3.59	0.06	4.43	0.25	53.21	0.04	0.84	4.88	98.91
14685	16.54	0.05	4.49	*0.005*	8.92	1.47	4.51	0.04	4.03	0.31	49.87	0.04	1.38	7.01	98.67
14685B	16.58	0.04	4.16	*0.005*	9.45	1.54	4.37	0.04	3.98	0.3	50.4	0.04	1.38	5.99	98.28
14545	18.58	0.1	5.18	*0.005*	5.98	1.37	2.17	0.03	4.2	0.27	56.26	0.04	0.65	4.1	98.94
14565	17.23	0.02	6.05	*0.005*	5.25	2.14	1.89	0.06	3.57	0.26	53.85	0.03	0.63	7.44	98.43
14571	16.48	0.05	3.51	*0.005*	3.99	1.76	2.03	0.02	4.32	0.22	59.95	0.04	0.59	5.14	98.11
14578	16.78	0.07	5.57	*0.005*	5.71	1.89	1.99	0.04	4	0.31	54.01	0.03	0.86	7.27	98.54
14578B	16.4	0.09	5.75	*0.005*	5.95	1.84	1.97	0.04	3.91	0.3	54.47	0.03	0.82	6.61	98.19
14598	19.18	0.02	4.52	*0.005*	6.5	1.54	3.79	0.07	3.95	0.31	52.94	0.06	0.74	5.22	98.85
14893	17.39	0.05	5.57	*0.005*	7.59	1.11	4.07	0.06	4.23	0.25	50.42	0.04	1	6.37	98.16
14899	18.24	0.04	4.77	*0.005*	8.14	0.9	6.3	0.06	3.94	0.25	48.95	0.04	0.97	5.91	98.52
14908	17.57	0.08	4.99	*0.005*	7.49	1.51	3.56	0.06	5.09	0.26	52.92	0.05	0.97	3.87	98.43
14917	16.75	0.09	3.18	*0.005*	3.43	1.86	2.74	0.04	5.62	0.22	59.61	0.03	0.8	3.75	98.13
14925	17.48	0.04	4.83	*0.005*	6.57	1.8	3.11	0.05	4.16	0.25	54.26	0.04	0.88	4.77	98.25
14998	17.84	0.03	5.3	*0.005*	6.2	1.39	2.47	0.05	4.81	0.28	53.76	0.04	0.72	5.99	98.89
15862	17.45	0.03	5.66	*0.005*	6.02	1.73	2.74	0.07	4.12	0.26	52.87	0.03	0.68	7.2	98.87
15870	15.28	0.12	6.1	*0.005*	5.48	2.09	2.68	0.06	3.07	0.23	54.41	0.03	0.74	8.21	98.51
15879	17.04	0.09	6.38	*0.005*	7.37	1.69	2.84	0.06	3.81	0.25	50.72	0.04	0.9	7.09	98.29

Project:	**Schaft Creek**
Client:	Copper Fox Metals Inc.
Data:	**Whole Rock by XRF**
Comments:	2005 core samples were collected by MDAG on Feb 7'07. 2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Al_2O_3	BaO	CaO	Cr_2O_3	Fe_2O_3	K_2O	MgO	MnO	Na_2O	P_2O_5	SiO_2	SrO	TiO_2	LOI	Total
	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
Method	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06
MDL	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		
15887	17.84	0.05	5.62	*0.005*	5.41	1.4	2.46	0.04	4.64	0.22	54.43	0.04	0.86	5.38	98.40
15891	17.63	0.15	6.76	*0.005*	5.43	1.99	2.66	0.06	4.12	0.23	51.38	0.04	0.86	7.61	98.93
15908	17.38	0.03	6.09	*0.005*	4.92	2.09	2.86	0.05	3.44	0.23	53.48	0.03	0.81	7.13	98.55
15911	17.39	0.05	4.88	*0.005*	6.78	1.62	3.54	0.05	3.89	0.25	52.8	0.04	0.91	5.87	98.08
125285	17.11	0.05	3.14	0.01	3.89	2.28	3.2	0.03	4.63	0.257	60.57	0.03	0.68	3.95	99.83
125288	15.19	0.04	9.2	0.07	9.18	1.08	10.81	0.15	1.83	0.187	44.45	0.04	1.04	6.5	99.77
125293	15.91	0.02	3.25	0.01	5.27	1.42	4.28	0.04	4.68	0.262	57.87	0.03	0.79	4.8	98.63
125305	18.08	0.04	3.76	0.01	4.55	2.28	3.23	0.03	4.58	0.261	57.01	0.03	0.66	5.3	99.82
125311	18.18	0.06	3.16	*0.005*	2.65	2.53	2.28	0.02	4.7	0.263	61	0.04	0.64	4.45	99.98
125703	19.76	0.02	4.82	0.01	5.81	2.91	2.37	0.06	3.2	0.284	52.31	0.02	0.71	7.58	99.86
125728	18.27	0.06	4.93	0.01	6.95	1.62	3.45	0.05	4.65	0.259	52.85	0.04	0.97	5.74	99.85
125755	15.83	0.05	2.7	0.01	1.53	2.72	1	0.01	4.03	0.108	67.27	0.03	0.33	3.71	99.33
125772	17.93	0.04	5.14	0.01	6.29	1.78	3.52	0.06	4.31	0.255	53.21	0.04	0.88	6.42	99.89
125795	17.31	0.07	6.36	0.01	7.28	1.98	3.37	0.1	3.44	0.248	50.53	0.03	0.83	8.09	99.65
125422	18.78	0.02	4.99	*0.005*	6.25	1.81	2.65	0.05	4.4	0.28	52.55	0.04	0.68	6.63	99.14
125435	18.53	0.02	5.08	*0.005*	6.84	1.95	2.36	0.05	4.58	0.281	53.19	0.03	0.75	6.26	99.93
125452	19.02	0.02	5.57	*0.005*	6.34	1.69	2.59	0.04	4.87	0.298	52.23	0.04	0.76	5.91	99.38
125476	14.96	0.16	3.1	0.01	2	2.42	1.4	0.02	3.41	0.112	65.89	0.03	0.34	4.43	98.28
125490	18.6	0.01	4.86	*0.005*	7.1	2.04	3.29	0.06	4.06	0.28	53.01	0.03	0.78	5.84	99.97
126192	18.97	0.02	4.9	*0.005*	4.03	1.31	1.61	0.05	5.78	0.31	56.47	0.04	0.67	5.67	99.84
126206	19.37	0.05	5.21	*0.005*	5.06	1.46	1.81	0.04	4.94	0.352	55.5	0.04	0.79	4.98	99.61
126225	18.89	0.07	5.04	*0.005*	4.81	1.83	1.27	0.05	5.41	0.342	55.66	0.05	0.76	5.29	99.48
126244	19.25	0.02	5.46	*0.005*	4.95	2.27	2.07	0.06	4.51	0.27	53.34	0.03	0.69	6.51	99.44
126266	19.41	0.02	4.82	*0.005*	5.65	2.36	2.11	0.06	4.16	0.296	53.49	0.03	0.74	6.27	99.42
126279	17.81	0.02	5.92	0.01	5.25	1.98	1.89	0.07	4.62	0.277	53.71	0.04	0.67	7.12	99.39
126288	18.68	0.02	5.78	*0.005*	4.27	2.48	1.8	0.04	3.97	0.266	54.53	0.03	0.66	6.72	99.25
126297	16.34	0.02	7.18	*0.005*	5.96	1.94	2.73	0.06	3.35	0.274	51.51	0.02	1.22	8.27	98.88
126314	18.69	0.02	5.7	*0.005*	5.38	2.45	2.48	0.05	3.2	0.263	52.73	0.03	0.75	6.53	98.28
126329	17.56	0.07	5.94	*0.005*	4.57	1.98	2.19	0.05	3.29	0.26	55.63	0.02	0.58	7.53	99.68
126337	17.64	0.04	5.76	*0.005*	6.09	1.96	2.81	0.05	3.87	0.271	52.72	0.03	1.02	7.36	99.63
126351	18.01	0.04	6.29	*0.005*	3.93	2.01	2.63	0.05	4.01	0.28	54.55	0.04	0.75	7.25	99.85
126427	17.33	0.02	6.99	*0.005*	8.38	1.86	3.9	0.15	2.54	0.226	48.37	0.03	0.91	7.98	98.69
126430	17.79	0.02	5.93	*0.005*	6.78	1.63	2.73	0.09	4.02	0.312	52.08	0.02	0.67	7.55	99.63
126434	18.63	0.02	6.11	*0.005*	6.27	1.69	2.04	0.07	4.59	0.326	52.32	0.03	0.68	7.09	99.87
126443	17.52	0.01	5.9	*0.005*	6.96	2	2.55	0.08	3.77	0.318	51.65	0.02	0.78	6.88	98.44
126449	17.98	0.05	6.86	0.01	8.87	0.59	6.21	0.15	2.91	0.258	50.13	0.05	0.97	4.89	99.93
126464	18.56	0.03	6.15	*0.005*	6.04	1.78	2.4	0.08	3.63	0.294	53.51	0.04	0.67	6.31	99.50
126492	18.48	0.03	5.97	0.01	5.85	1.97	2.52	0.05	3.73	0.302	52.72	0.03	0.71	6.9	99.27
145655	18.24	0.08	6.47	*0.005*	5.81	1.54	2.41	0.06	4.08	0.293	53.61	0.04	0.67	6.53	99.84
145669	18.32	0.02	5.84	*0.005*	7.7	1.71	2.38	0.07	4.41	0.297	50.96	0.03	0.73	6.61	99.08
145685	18.1	0.02	5.25	*0.005*	6.9	1.8	2.88	0.09	4.06	0.251	53	0.03	0.73	6.28	99.40
145694	17.85	0.02	6.17	*0.005*	7.23	1.59	2.95	0.07	4.64	0.255	50.08	0.04	0.87	7.02	98.79
145708	16.4	0.01	4.49	*0.005*	5.15	1.54	1.8	0.05	4.72	0.191	52.71	0.03	0.55	11.25	98.90
145723	18.09	0.02	4.96	*0.005*	7.29	1.85	2.14	0.04	3.93	0.266	54.22	0.03	0.68	5.41	98.93
146798	18.35	0.04	5.69	*0.005*	5.93	1.89	2.25	0.07	4.14	0.264	51.63	0.03	0.67	8.34	99.30
146824	17.77	0.03	5.25	0.04	7.6	1.18	3.73	0.06	5.18	0.267	51.2	0.04	0.98	5.71	99.04

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Whole Rock by XRF**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Al_2O_3	BaO	CaO	Cr_2O_3	Fe_2O_3	K_2O	MgO	MnO	Na_2O	P_2O_5	SiO_2	SrO	TiO_2	LOI	Total
	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
Method	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06
MDL	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		
146831	17.08	0.02	5.33	0.01	6.53	1.31	4.27	0.06	4.18	0.254	52.04	0.03	0.86	6.6	98.57
146843															0.00
146861	18.8	0.05	5.71	*0.005*	6.18	1.39	2.67	0.04	4.43	0.267	56.25	0.04	0.66	3.27	99.76
146868	19	0.03	5.37	*0.005*	5.27	1.98	2.44	0.02	4.22	0.275	55.31	0.04	0.67	4.98	99.61
126352	18.17	0.04	5.03	0.01	7.04	1.41	3.62	0.05	4.8	0.261	53.09	0.04	0.93	4.98	99.47
126358	17.79	0.03	4.77	0.01	7.11	1.53	3.21	0.05	4.9	0.258	53.46	0.04	0.9	5	99.06
126374	17.87	0.03	5.11	0.01	7.91	1.08	3.68	0.06	4.65	0.281	52.99	0.04	0.92	5.2	99.83
126384	17.76	0.03	5.25	*0.005*	6.84	1.2	2.56	0.05	4.07	0.193	55.59	0.05	0.74	4.5	98.84
126391	19.38	0.04	6.21	*0.005*	7.04	1.22	3.18	0.06	4.34	0.248	51.99	0.05	0.77	5.48	100.01
146172	17.2	0.03	5.07	*0.005*	6.86	1.87	2.52	0.05	4.49	0.255	52.49	0.03	0.74	8.03	99.64
146182	19.06	0.02	5.47	*0.005*	7.23	1.43	3.27	0.05	4.16	0.276	53.37	0.05	0.82	4	99.21
146203	17.93	0.02	3.93	*0.005*	4.25	1.62	2.65	0.05	4.96	0.259	58.05	0.03	0.73	4.56	99.04
146214	17.8	0.03	5.86	*0.005*	5.8	1.65	2.4	0.06	4.66	0.266	53.61	0.04	0.67	6.31	99.16
146221	17.42	0.03	5.3	*0.005*	8.35	1.45	4.1	0.06	4.46	0.317	49.78	0.04	1.4	5.88	98.59
146238	18.69	0.03	5.88	0.01	9.13	1.4	3.53	0.07	4.43	0.262	51.29	0.05	0.94	4.16	99.87
147034	19.08	0.02	4.05	*0.005*	5.03	2.54	1.71	0.03	4.22	0.293	54.91	0.03	0.59	6.57	99.08
147038	16.02	0.13	3.63	0.01	3.49	1.97	1.84	0.02	3.98	0.176	61.64	0.03	0.51	5.69	99.14
147051	18.86	0.1	5.08	0.01	5.96	1.8	2.62	0.03	3.96	0.294	55.43	0.05	0.77	4.96	99.92
147070	19.08	0.02	7.09	0.01	8.11	0.93	2.93	0.09	4.02	0.303	52.15	0.05	0.75	4.29	99.82
147087	17.66	0.02	5	*0.005*	9.89	0.74	2.92	0.07	5.13	0.262	51.79	0.04	0.73	5.6	99.86
147097	18.87	0.12	6.09	*0.005*	6.91	2.57	2.58	0.07	3.69	0.277	50.07	0.03	0.75	7.19	99.22
145508	18.69	0.04	4.1	0.01	7.63	0.93	6.4	0.07	4.34	0.242	50.39	0.03	0.98	5.73	99.58
145527	17.69	0.05	5.53	0.01	7.07	1.86	2.44	0.05	4.2	0.249	54.64	0.04	0.86	4.86	99.55
145543	18.62	0.04	4.77	0.01	5.77	1.84	2.97	0.05	4.71	0.267	56	0.04	0.91	3.99	99.99
145562	18.21	0.04	5.57	0.01	6.77	1.83	2.94	0.06	4.41	0.264	53	0.04	0.9	5.9	99.94
145576	15.57	0.09	2.43	0.01	1.49	2.68	1.05	0.01	4.4	0.106	67.14	0.03	0.31	3.65	98.97
145601	18.22	0.06	6.35	*0.005*	7.44	1.53	3.07	0.09	4.5	0.264	52.25	0.05	0.83	4.7	99.36
146297	18.1	0.03	5.37	*0.005*	4.82	1.8	3.2	0.04	3.85	0.255	53.53	0.03	0.8	6.61	98.44
146314	19.08	0.03	5.72	*0.005*	6.66	1.49	2.83	0.06	4.08	0.284	53	0.04	0.78	5.33	99.39
146335	18.73	0.03	6.24	0.02	6.82	2.09	2.39	0.06	3.86	0.282	51.36	0.04	0.74	6.79	99.45
146352	17.12	0.03	4.51	0.01	5.94	1.07	2.75	0.06	4.54	0.268	57.44	0.04	0.69	5.4	99.87
146368	18.87	0.02	5.82	0.01	6.46	1.7	2.65	0.07	4.05	0.293	52.75	0.04	0.75	6.42	99.90
146390	19.33	0.02	6.64	*0.005*	6.34	1.35	2.51	0.06	4.17	0.301	53.08	0.05	0.78	4.94	99.58
146508	17.84	0.03	4.69	0.01	5.61	2.7	3.78	0.04	3.65	0.242	52.12	0.03	0.95	7.58	99.27
146526	18.21	0.06	5.85	*0.005*	4.56	1.8	2.57	0.04	4.46	0.262	55.41	0.06	0.68	5.97	99.94
146544	16.19	0.05	4.93	0.01	2.7	1.94	1.84	0.04	4.12	0.176	60.33	0.04	0.48	6.44	99.29
146565	18.4	0.15	4.93	*0.005*	2.51	2.86	2.06	0.03	3.66	0.354	56.06	0.04	0.63	8.26	99.95
146589	17.55	0.04	5.55	0.01	6.05	1.96	2.84	0.04	3.55	0.237	54.04	0.04	0.88	7.01	99.80
146613	17.75	0.02	7.42	*0.005*	3.83	0.92	2.36	0.06	6.13	0.237	53.34	0.04	0.8	6.25	99.16
146627	14.05	0.04	4.73	0.01	4.05	1.42	2.53	0.05	3.15	0.194	60.55	0.02	0.56	8.49	99.84
146637	16.12	0.12	4.01	0.01	2.46	2.83	1.87	0.04	2.79	0.135	61.18	0.02	0.39	6.83	98.81
146649	16.12	0.11	3.41	0.01	2.36	1.87	1.58	0.03	4.54	0.117	64.02	0.04	0.35	5.35	99.91
146657	16.41	0.05	2.6	0.01	1.57	1.45	1.29	0.03	5.4	0.118	66.34	0.03	0.35	4.18	99.83
146676	20.29	0.02	5.38	*0.005*	2.24	1.69	1.52	0.06	6.28	0.319	54.87	0.04	0.72	5.96	99.39
125188	19.14	0.08	4.14	*0.005*	3.69	2.22	1.99	0.02	4.76	0.307	55.53	0.04	0.58	6.13	98.63
125198	19.16	0.03	4.65	*0.005*	4.81	2.04	2.35	0.04	4.18	0.364	55.56	0.03	0.64	5.84	99.70

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Whole Rock by XRF**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Al_2O_3	BaO	CaO	Cr_2O_3	Fe_2O_3	K_2O	MgO	MnO	Na_2O	P_2O_5	SiO_2	SrO	TiO_2	LOI	Total
	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
Method	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06
MDL	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		
125207	17.14	0.04	5.13	*0.005*	4.17	2.22	2.28	0.06	3.47	0.34	56.18	0.03	0.58	8.18	99.83
125228	16.46	0.05	2.84	0.01	1.96	1.43	1.34	0.02	5.56	0.114	65.02	0.04	0.33	4.65	99.82
125244	16.42	0.02	2.63	0.01	1.46	0.79	1.51	0.04	6.38	0.117	66.38	0.04	0.34	3.59	99.73
125257	18.42	0.03	11.26	0.03	8.09	0.39	7.12	0.14	2.12	0.136	47.27	0.03	0.88	3.92	99.84
125278	19.41	0.04	4.74	*0.005*	5.63	0.72	2.37	0.1	7.12	0.249	56.09	0.06	0.81	2.54	99.88
125596	18.85	0.03	6.96	*0.005*	6.94	1.44	2.8	0.09	4.06	0.273	50.81	0.04	0.75	6.76	99.81
125610	17.85	0.01	3.69	*0.005*	5.37	1.53	2.97	0.07	4.87	0.258	56.13	0.03	0.71	6.01	99.50
125626															0.00
125641	17.86	0.02	4.92	0.01	6.49	1.33	4.02	0.08	4.71	0.256	52.03	0.03	0.93	6.7	99.39
125669	16.53	0.02	4.19	0.01	5.63	1.89	2.99	0.07	3.86	0.299	56.64	0.02	0.82	5.58	98.55
125690	17.88	0.03	5.16	0.01	7.57	1.17	3.51	0.1	4.5	0.243	53.54	0.04	0.83	4.81	99.39
West Breccia Zone															
14018	16.2	0.13	2.53	*0.005*	3.77	2.92	1.74	0.05	4.01	0.14	62.92	0.05	0.42	3.69	98.58
14021	14.75	0.05	3.56	*0.005*	2.62	2.59	1.47	0.07	2.96	0.12	65.03	0.02	0.36	4.86	98.47
14036	14.93	0.06	2.56	*0.005*	3.72	2.51	1.51	0.05	3.13	0.12	64.89	0.03	0.38	4.53	98.43
14043	15.21	0.03	1.98	*0.005*	4.23	1.18	3.06	0.05	4.13	0.12	64.74	0.03	0.41	3.53	98.71
14060	15.16	0.04	4.27	*0.005*	5.14	1.42	3.28	0.05	3.71	0.26	58.18	0.05	0.73	6.18	98.48
14067	16.07	0.04	3.54	0.01	6.18	1.29	4.07	0.09	4.15	0.22	57.69	0.04	0.7	4.08	98.17
14076	16.09	0.05	5.61	*0.005*	7.43	1.58	3.72	0.19	2.64	0.21	55.56	0.04	0.72	5.1	98.95
14083	16.4	0.08	5.33	*0.005*	8.26	3.49	2.82	0.17	1.62	0.21	53.34	0.02	0.74	6.28	98.77
14099	15.15	0.1	4.16	*0.005*	3.38	3.94	1.47	0.14	0.73	0.11	63.71	0.01	0.31	5.67	98.89
14103	15	0.03	4.03	*0.005*	3.11	2.07	2.04	0.08	2.99	0.13	61.55	0.02	0.41	6.91	98.38
125046	17.86	0.02	5.49	0.01	5.19	0.99	3.66	0.15	4.79	0.244	55.16	0.05	0.83	5.17	99.61
125068	18.33	0.05	5.76	0.02	6.04	1.13	3.68	0.11	4.79	0.26	54.03	0.06	0.88	4.78	99.92
125073	18	0.07	4.77	0.02	3.28	1.94	2.65	0.07	4.52	0.258	58.16	0.05	0.64	5.29	99.72
125079	17.66	0.17	2.67	*0.005*	2.68	3.83	1.73	0.05	4.37	0.236	62.22	0.03	0.61	3.72	99.98
125084	18.5	0.1	5.46	0.01	5.87	1.55	3.55	0.2	4.16	0.267	55.29	0.07	0.9	3.95	99.88
125127	18.78	0.06	3.33	0.01	6.22	1.92	4.01	0.06	5.28	0.268	55.01	0.04	0.92	3.93	99.84
125129	15.88	0.03	2.46	0.01	4.86	1.7	3.21	0.05	4.61	0.232	62.02	0.03	0.78	3.95	99.82
125134	16.42	0.06	1.98	0.01	8.55	1.95	3.44	0.06	4.74	0.238	58.02	0.03	0.79	3.31	99.60
125142	16.47	0.04	2.88	0.02	6	1.38	3.6	0.11	4.51	0.221	59.53	0.03	0.73	4.34	99.86
125149	17.48	0.06	4.68	*0.005*	7.19	1.6	3.36	0.09	5.43	0.251	53.05	0.03	0.85	5.78	99.86
125154	19.05	0.02	3.49	*0.005*	2.07	0.65	1.69	0.04	7.96	0.352	59.48	0.03	0.63	4.39	99.86
125165	19.83	0.02	4.16	*0.005*	4.57	0.65	2.53	0.05	6.87	0.358	56.69	0.08	0.8	3.2	99.81
125176	18.59	0.03	3.67	*0.005*	5.24	1	2.84	0.06	6.19	0.309	56.01	0.05	0.65	4.5	99.14
146112	18.98	0.03	4.23	*0.005*	5.73	1.03	2.17	0.08	5.36	0.252	58	0.06	0.74	3.3	99.97
146115	16.96	0.07	10.19	0.01	10.35	0.68	6.28	0.18	3.05	0.266	47	0.05	1.49	3.39	99.97
146124	21.15	0.07	5.94	*0.005*	6.28	1.68	3.04	0.09	4.21	0.313	52.08	0.06	0.72	4.2	99.84
146127	15.87	0.06	3.57	0.01	2.49	1.97	1.02	0.03	3.8	0.115	66.01	0.02	0.36	4.15	99.48
146135	20.22	0.06	5.9	*0.005*	6.31	1.06	2.13	0.12	5.46	0.309	55.03	0.07	0.71	2.59	99.97
146149	20.29	0.06	6.09	*0.005*	5.9	1.16	1.81	0.11	5.36	0.298	54.75	0.07	0.69	3.35	99.94
146161	17.6	0.08	9.29	*0.005*	9.2	0.81	5.6	0.29	2.32	0.266	49.04	0.07	0.98	4.26	99.81
146164	19.16	0.06	5.15	*0.005*	9.53	0.97	6.36	0.24	3.44	0.317	49.46	0.05	1.05	3.95	99.74
145951	18.25	0.03	5.6	*0.005*	5.98	1.92	2.32	0.08	4.27	0.288	53.89	0.03	0.77	6.46	99.89
145956	18.33	0.02	4.77	*0.005*	7.26	1.52	3.76	0.1	4.36	0.258	52.29	0.03	0.87	6.16	99.73
145974	19.29	0.03	3.6	*0.005*	7.34	1.81	4.15	0.11	4.15	0.263	52.11	0.03	0.78	5.97	99.64

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Whole Rock by XRF**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Al_2O_3	BaO	CaO	Cr_2O_3	Fe_2O_3	K_2O	MgO	MnO	Na_2O	P_2O_5	SiO_2	SrO	TiO_2	LOI	Total
	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
Method	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06
MDL	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		
145982	17.96	0.03	9.08	0.01	8.93	0.42	5.44	0.15	2.6	0.294	47	0.05	1.25	6.75	99.96
145992	18.64	0.03	4.06	*0.005*	5.71	1.48	2.83	0.1	5.41	0.272	55.12	0.03	0.77	4.98	99.44
145999	19.15	0.02	5.47	*0.005*	6.28	1.07	2.84	0.09	4.92	0.261	53.82	0.05	0.78	5.1	99.86
145834	19.33	0.02	4.42	*0.005*	6.1	0.78	2.85	0.14	5.99	0.267	55.46	0.08	0.76	3.53	99.73
145842	16.68	0.01	11.09	0.03	6.42	0.13	4.05	0.26	2.48	0.389	53.18	0.13	1.28	3.65	99.78
145852	17.8	*0.005*	6.27	0.01	4.54	0.17	1.81	0.16	5.03	0.211	61.07	0.11	0.67	1.99	99.85
145857	19.84	0.03	6.15	*0.005*	4.45	0.68	2.65	0.1	6	0.295	56.57	0.1	0.79	2.07	99.73
145871	18.98	0.03	5.98	*0.005*	5.98	1.16	2.46	0.13	4.56	0.248	55.05	0.07	0.67	4.53	99.85
145608	17.29	0.04	4.82	*0.005*	8.41	1.32	5	0.09	3.66	0.209	53.35	0.05	0.74	4.19	99.17
145614	17.2	0.06	4.82	*0.005*	8.45	1.51	4.31	0.11	3.89	0.209	54.56	0.05	0.74	3.89	99.80
145628	16.34	0.01	5.14	*0.005*	6.7	0.42	3.61	0.1	5.92	0.192	54	0.03	0.69	6.68	99.84
145640	16.97	0.05	5.91	0.01	7.9	1.5	4.03	0.15	3.76	0.205	53.09	0.04	0.73	4.68	99.03
145646	17.36	0.04	4.98	*0.005*	7.95	0.96	4.39	0.13	4.32	0.21	54.39	0.05	0.75	4.31	99.85
Paramount Zone															
125965	16.39	0.03	3.15	0.01	4.89	0.88	3	0.1	5.47	0.18	60.25	0.03	0.64	4.04	99.06
125974	16.48	0.04	2.58	*0.005*	6.61	1.81	3.36	0.06	4.01	0.19	58.07	0.02	0.62	5.19	99.05
125983	14.04	0.06	5.11	0.03	7.12	1.29	5.53	0.09	3.49	0.19	56.18	0.03	0.5	5.93	99.59
125988	17.59	0.08	6.55	0.01	8.55	1.55	5.29	0.15	3.38	0.254	50.3	0.06	0.96	4.3	99.02
126007	15.62	0.05	2.77	0.02	1.78	2.12	1.4	0.06	4.21	0.108	66.74	0.03	0.31	4.55	99.77
126031	15.92	0.1	2.54	0.01	2.19	1.57	1.33	0.03	5.57	0.117	66.83	0.04	0.36	3.24	99.85
126040	16.79	0.03	2.52	0.01	4.43	1.03	3.17	0.05	5.77	0.172	60.7	0.03	0.55	4.06	99.31
126054	12.76	0.04	6.75	0.04	6.97	0.86	6.65	0.2	2.3	0.217	52.9	0.02	0.6	8.96	99.27
126067	14.74	0.02	6.21	0.03	6.67	1.16	5.3	0.22	2.9	0.207	53.99	0.03	0.58	6.86	98.92
126081	13.3	0.15	2.51	0.02	2.88	3.43	1.61	0.09	1.32	0.098	68.17	0.02	0.31	4.33	98.24
126110	17.97	0.1	6.58	0.01	8.54	2.13	4.51	0.15	3.6	0.268	49.11	0.06	0.97	5.33	99.33
126118	15.95	0.04	5.02	0.01	5.99	1.98	4.09	0.12	3.14	0.356	52.58	0.02	1.1	7.77	98.17
125904	18.73	0.03	5.31	*0.005*	5.12	1.49	2.01	0.07	5.77	0.282	53.74	0.04	0.66	5.82	99.08
125919	19.58	0.03	3.2	*0.005*	6.47	1.22	2.92	0.07	6.42	0.276	54.34	0.05	0.73	4.42	99.73
125928	18.4	0.08	3.98	0.01	7.74	1.39	3.54	0.15	5.18	0.256	53.53	0.05	0.9	4.53	99.74
125933	17.68	0.06	5.09	*0.005*	9.24	1.08	4.74	0.17	4.53	0.395	47.48	0.04	1.25	7.71	99.47
125944	18.26	0.07	4.51	0.01	7.41	1.1	3.67	0.18	5.51	0.233	53.28	0.06	0.87	4.71	99.87
125952	15.36	0.04	3.91	0.01	3.44	2.07	1.71	0.05	3.88	0.117	62.17	0.02	0.34	6.01	99.13
125963	17.56	0.05	4.82	*0.005*	7.56	1.29	3.27	0.09	5.1	0.256	51.99	0.03	0.74	6.43	99.19
126120	16.75	0.06	2.15	0.02	2.02	1.1	1.35	0.03	5.92	0.11	67.38	0.05	0.32	2.6	99.86
126131	15.96	0.05	3.15	0.01	1.48	1.04	1.86	0.02	6.13	0.174	65.61	0.04	0.5	3.48	99.50
126142	17.22	0.03	3.78	0.01	2.46	1.09	2.52	0.04	5.76	0.191	62.62	0.04	0.6	3.42	99.78
126154	17.93	0.01	4.12	0.01	2.59	0.64	3.82	0.05	6.72	0.29	57.5	0.04	0.84	5.24	99.80
126171	15.23	0.11	4.3	0.01	4.27	1.83	2.69	0.05	4.03	0.176	58.64	0.04	0.6	6.92	98.90
126181	19.38	0.04	5.76	0.01	7.19	0.92	3.78	0.13	4.17	0.22	53.08	0.05	0.81	4.27	99.81
125806	16.38	0.12	3.53	0.01	3.54	2.34	1.96	0.05	4.86	0.155	62.5	0.05	0.49	3.84	99.83
125816	17.21	0.14	4.99	*0.005*	8.84	2	3.65	0.15	4.14	0.304	51.75	0.06	1.11	5.56	99.91
125833	16.07	0.08	2.8	0.01	2.24	2.34	1.36	0.04	4.68	0.111	66.32	0.04	0.35	3.4	99.84
125861	16.09	0.08	2.52	0.01	1.76	1.69	1.34	0.03	4.91	0.109	66.67	0.03	0.37	3.56	99.17
125875	15.55	0.1	2.98	0.01	2.12	2.49	1.27	0.04	4.44	0.116	66.4	0.04	0.4	3.84	99.80
125897	15.34	0.03	2.97	0.01	1.1	1.94	1.38	0.03	4.35	0.152	68.1	0.02	0.36	4.06	99.84

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Whole Rock by XRF**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Al_2O_3	BaO	CaO	Cr_2O_3	Fe_2O_3	K_2O	MgO	MnO	Na_2O	P_2O_5	SiO_2	SrO	TiO_2	LOI	Total
	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
Method	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06
MDL	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		
Tailings															
LIARD ZONE	17.71	0.04	5.02	0.01	5.54	1.86	2.67	0.06	4.46	0.257	55.2	0.03	0.77	6.05	99.68
PARAMOUNT	16.01	0.06	4.01	0.01	4.1	1.74	2.67	0.08	4.61	0.189	60.01	0.03	0.6	4.92	99.04
WEST BRECCIA	17.54	0.06	4.07	0.01	5.51	1.69	3.35	0.09	4.9	0.261	57.14	0.05	0.77	4.08	99.52
High-Sulphide Histor															
T112 (171' - 172')	13.2	0.02	6	0.01	15.67	0.46	5.72	0.11	3.99	0.229	43.68	0.03	1.03	7.95	98.10
T113 (81' - 82')	16.21	0.15	1.17	*0.005*	3.65	2.17	2.35	0.02	4.75	0.135	65.58	0.04	0.46	2.54	99.23
T113 (983' - 985')	14.91	0.02	3.35	*0.005*	5.93	1.91	3.09	0.08	3.36	0.153	60.06	0.02	0.56	5.01	98.46
T140 (30' - 31')	18.88	0.04	4.23	*0.005*	4.84	2.59	2.61	0.03	3.48	0.27	56.51	0.03	0.82	5.58	99.92
T166 (389' - 390')	16.31	0.06	2.32	*0.005*	2.85	2.07	1.16	0.01	4.34	0.105	67.15	0.04	0.3	2.91	99.63
T185 (116' - 117')	16.46	0.08	1.32	0.03	3.7	2.81	1.16	0.01	3.27	0.145	66.34	0.02	0.46	4.09	99.90
T207 (261.5' - 262')	14.43	0.04	1.5	*0.005*	5.87	2.12	0.85	0.02	3.89	0.127	65.44	0.01	0.38	4.87	99.55
T207 (269' - 271')	11.49	0.04	1.33	*0.005*	17.65	1.78	1.12	0.03	2.4	0.102	51.1	0.01	0.31	11.6	98.97
All Data															
Maximum	21.2	0.17	11.3	0.07	17.6	3.94	10.8	0.29	7.96	0.4	68.2	0.13	1.49	11.6	
Minimum	11.5	0.005	1.17	0.005	1.1	0.13	0.61	0.01	0.73	0.098	43.7	0.01	0.29	1.99	
Mean	17.5	0.047	4.86	0.0081	5.7	1.69	2.88	0.07	4.27	0.24	55.7	0.038	0.72	5.57	
Standard Deviation	1.49	0.032	1.53	0.0068	2.2	0.61	1.28	0.046	1	0.064	5	0.015	0.21	1.63	
10 Percentile	15.5	0.02	2.82	0.005	2.54	0.93	1.49	0.03	3.13	0.12	50.8	0.02	0.38	3.67	
25 Percentile	16.5	0.02	3.88	0.005	4.44	1.32	2.04	0.04	3.83	0.21	52.7	0.03	0.62	4.32	
Median	17.7	0.04	4.99	0.005	5.92	1.7	2.67	0.06	4.21	0.26	54.2	0.04	0.73	5.41	
75 Percentile	18.6	0.06	5.76	0.01	6.96	1.98	3.48	0.09	4.74	0.28	57.8	0.04	0.83	6.58	
90 Percentile	19.2	0.09	6.33	0.01	8.1	2.49	4.22	0.14	5.47	0.31	64.9	0.05	0.96	7.58	
Interquartile Range (IC	2.11	0.04	1.88	0.005	2.52	0.67	1.44	0.05	0.92	0.066	5.06	0.01	0.21	2.26	
Variance	2.22	0.001	2.36	0.000047	4.86	0.37	1.65	0.0021	1	0.0041	25	0.00023	0.046	2.64	
Skewness	-0.72	1.55	0.62	4.88	0.79	0.38	1.77	1.81	-0.014	-0.68	0.87	2.07	0.36	0.65	
Coefficient of Variatior	0.085	0.69	0.32	0.84	0.39	0.36	0.45	0.65	0.23	0.26	0.09	0.39	0.3	0.29	
Count	235	235	235	235	235	235	235	235	235	235	235	235	235	235	
Main Zone															
Maximum	20.3	0.16	11.3	0.07	9.89	2.91	10.8	0.15	7.12	0.36	67.3	0.08	1.4	11.2	
Minimum	14	0.01	2.43	0.005	1.46	0.39	0.61	0.01	1.72	0.1	44.4	0.02	0.29	2.54	
Mean	17.8	0.042	5.15	0.0074	5.69	1.77	2.77	0.055	4.22	0.26	54.6	0.036	0.74	6.05	
Standard Deviation	1.18	0.031	1.25	0.0067	1.79	0.49	1.23	0.026	0.81	0.053	4.12	0.0092	0.19	1.49	
10 Percentile	16.2	0.02	3.42	0.005	2.68	1.14	1.61	0.03	3.27	0.19	50.6	0.03	0.56	4.13	
25 Percentile	17.2	0.02	4.57	0.005	4.81	1.44	2.08	0.04	3.88	0.25	52.2	0.03	0.66	4.98	
Median	17.8	0.03	5.15	0.005	5.94	1.8	2.58	0.05	4.18	0.26	53.5	0.04	0.74	5.96	
75 Percentile	18.6	0.05	5.85	0.01	6.89	2.01	3.17	0.06	4.64	0.28	55.6	0.04	0.84	6.98	
90 Percentile	19.2	0.085	6.37	0.01	7.6	2.47	3.84	0.08	5.11	0.31	60.4	0.045	0.94	7.96	
Interquartile Range (IC	1.47	0.03	1.27	0.005	2.08	0.56	1.09	0.02	0.76	0.033	3.35	0.01	0.18	2	
Variance	1.38	0.00094	1.56	0.000045	3.22	0.24	1.51	0.00066	0.65	0.0029	17	0.000085	0.036	2.22	
Skewness	-0.63	1.81	0.69	6.82	-0.47	-0.047	2.74	1.48	0.0069	-1.25	1.41	0.88	0.34	0.59	
Coefficient of Variatior	0.066	0.73	0.24	0.91	0.32	0.28	0.44	0.47	0.19	0.21	0.076	0.26	0.26	0.25	
Count	146	146	146	146	146	146	146	146	146	146	146	146	146	146	

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Whole Rock by XRF**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Al_2O_3	BaO	CaO	Cr_2O_3	Fe_2O_3	K_2O	MgO	MnO	Na_2O	P_2O_5	SiO_2	SrO	TiO_2	LOI	Total
	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
Method	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06
MDL	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		
West Breccia Zone															
Maximum	21.2	0.17	11.1	0.03	10.4	3.94	6.36	0.29	7.96	0.39	66	0.13	1.49	6.91	
Minimum	14.8	0.005	1.98	0.005	2.07	0.13	1.02	0.03	0.73	0.11	47	0.01	0.31	1.99	
Mean	17.6	0.049	4.91	0.0077	5.95	1.48	3.19	0.11	4.31	0.24	56.4	0.048	0.74	4.5	
Standard Deviation	1.61	0.031	1.95	0.0052	2.01	0.85	1.25	0.058	1.34	0.065	4.62	0.024	0.23	1.19	
10 Percentile	15.2	0.02	2.63	0.005	3.21	0.65	1.71	0.05	2.62	0.13	52.1	0.026	0.41	3.31	
25 Percentile	16.4	0.03	3.58	0.005	4.56	0.98	2.24	0.065	3.68	0.21	53.6	0.03	0.67	3.7	
Median	17.7	0.04	4.77	0.005	6	1.38	3.06	0.1	4.32	0.25	55.2	0.05	0.74	4.31	
75 Percentile	18.9	0.06	5.68	0.01	7.3	1.86	3.88	0.14	5.16	0.27	58.8	0.06	0.8	5.14	
90 Percentile	19.5	0.08	6.2	0.01	8.49	2.54	4.63	0.18	5.95	0.31	63.2	0.074	0.94	6.22	
Interquartile Range (IC	2.51	0.03	2.1	0.005	2.74	0.88	1.64	0.075	1.47	0.06	5.24	0.03	0.12	1.43	
Variance	2.59	0.00098	3.81	0.000027	4.02	0.72	1.57	0.0034	1.79	0.0043	21.3	0.00059	0.052	1.41	
Skewness	0.017	1.69	1.28	2.64	0.023	1.18	0.62	1.19	-0.047	-0.33	0.31	1.27	0.76	0.24	
Coefficient of Variatior	0.091	0.64	0.4	0.68	0.34	0.57	0.39	0.53	0.31	0.27	0.082	0.5	0.31	0.26	
Count	47	47	47	47	47	47	47	47	47	47	47	47	47	47	
Paramount Zone															
Maximum	19.6	0.15	6.75	0.04	9.24	3.43	6.65	0.22	6.72	0.4	68.2	0.06	1.25	8.96	
Minimum	12.8	0.01	2.15	0.005	1.1	0.64	1.27	0.02	1.32	0.098	47.5	0.02	0.31	2.6	
Mean	16.5	0.063	4.07	0.012	4.94	1.58	3.03	0.089	4.57	0.2	58.7	0.038	0.64	4.98	
Standard Deviation	1.62	0.036	1.38	0.0081	2.6	0.61	1.48	0.057	1.24	0.078	6.52	0.013	0.26	1.52	
10 Percentile	14.7	0.03	2.52	0.005	1.78	0.92	1.35	0.03	3.14	0.11	51.8	0.02	0.34	3.42	
25 Percentile	15.6	0.035	2.88	0.01	2.35	1.1	1.66	0.045	3.94	0.13	53.2	0.03	0.38	3.94	
Median	16.4	0.05	3.91	0.01	4.89	1.49	3	0.07	4.53	0.19	58.1	0.04	0.6	4.53	
75 Percentile	17.6	0.08	5.06	0.01	7.16	1.99	3.8	0.14	5.54	0.26	66	0.05	0.82	5.88	
90 Percentile	18.4	0.11	6.21	0.02	8.54	2.34	5.29	0.17	5.92	0.29	66.8	0.06	0.97	6.92	
Interquartile Range (IC	2.05	0.045	2.17	0	4.8	0.89	2.14	0.095	1.6	0.12	12.8	0.02	0.44	1.94	
Variance	2.64	0.0013	1.91	0.000066	6.76	0.37	2.19	0.0033	1.53	0.006	42.5	0.00017	0.069	2.3	
Skewness	-0.26	0.83	0.5	2.07	0.077	0.92	0.59	0.77	-0.52	0.57	0.082	0.19	0.62	0.87	
Coefficient of Variatior	0.098	0.57	0.34	0.66	0.53	0.39	0.49	0.64	0.27	0.38	0.11	0.34	0.41	0.3	
Count	31	31	31	31	31	31	31	31	31	31	31	31	31	31	

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **Whole Rock by XRF**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Al_2O_3	BaO	CaO	Cr_2O_3	Fe_2O_3	K_2O	MgO	MnO	Na_2O	P_2O_5	SiO_2	SrO	TiO_2	LOI	Total
	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
Method	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06	ME-XRF06
MDL	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		
Tailings															
Maximum	17.7	0.06	5.02	0.01	5.54	1.86	3.35	0.09	4.9	0.26	60	0.05	0.77	6.05	
Minimum	16	0.04	4.01	0.01	4.1	1.69	2.67	0.06	4.46	0.19	55.2	0.03	0.6	4.08	
Mean	17.1	0.053	4.37	0.01	5.05	1.76	2.9	0.077	4.66	0.24	57.5	0.037	0.71	5.02	
Standard Deviation	0.94	0.012	0.57	0	0.82	0.087	0.39	0.015	0.22	0.04	2.42	0.012	0.098	0.99	
10 Percentile	16.3	0.044	4.02	0.01	4.38	1.7	2.67	0.064	4.49	0.2	55.6	0.03	0.63	4.25	
25 Percentile	16.8	0.05	4.04	0.01	4.8	1.72	2.67	0.07	4.54	0.22	56.2	0.03	0.68	4.5	
Median	17.5	0.06	4.07	0.01	5.51	1.74	2.67	0.08	4.61	0.26	57.1	0.03	0.77	4.92	
75 Percentile	17.6	0.06	4.54	0.01	5.52	1.8	3.01	0.085	4.76	0.26	58.6	0.04	0.77	5.48	
90 Percentile	17.7	0.06	4.83	0.01	5.53	1.84	3.21	0.088	4.84	0.26	59.4	0.046	0.77	5.82	
Interquartile Range (IC	0.85	0.01	0.5	0	0.72	0.085	0.34	0.015	0.22	0.036	2.41	0.01	0.085	0.98	
Variance	0.88	0.00013	0.32	0	0.68	0.0076	0.15	0.00023	0.05	0.0016	5.86	0.00013	0.0096	0.98	
Skewness	-1.67	-1.73	1.71	NA	-1.73	1.12	1.73	-0.94	0.9	-1.71	0.57	1.73	-1.73	0.44	
Coefficient of Variatior	0.055	0.22	0.13	0	0.16	0.05	0.14	0.2	0.048	0.17	0.042	0.31	0.14	0.2	
Count	3	3	3	3	3	3	3	3	3	3	3	3	3	3	
High-Sulphide Histor															
Maximum	18.9	0.15	6	0.03	17.6	2.81	5.72	0.11	4.75	0.27	67.2	0.04	1.03	11.6	
Minimum	11.5	0.02	1.17	0.005	2.85	0.46	0.85	0.01	2.4	0.1	43.7	0.01	0.3	2.54	
Mean	15.2	0.056	2.65	0.0088	7.52	1.99	2.26	0.039	3.68	0.16	59.5	0.025	0.54	5.57	
Standard Deviation	2.26	0.043	1.75	0.0088	5.77	0.71	1.63	0.036	0.72	0.06	8.52	0.012	0.26	2.96	
10 Percentile	12.7	0.02	1.28	0.005	3.41	1.38	1.04	0.01	3.01	0.1	48.9	0.01	0.31	2.8	
25 Percentile	14.1	0.035	1.33	0.005	3.69	1.88	1.15	0.018	3.34	0.12	55.2	0.018	0.36	3.8	
Median	15.6	0.04	1.91	0.005	5.36	2.09	1.76	0.025	3.68	0.14	62.8	0.025	0.46	4.94	
75 Percentile	16.3	0.065	3.57	0.0062	8.36	2.28	2.73	0.042	4.08	0.17	65.8	0.032	0.62	6.17	
90 Percentile	17.2	0.1	4.76	0.016	16.3	2.66	3.88	0.089	4.46	0.24	66.6	0.04	0.88	9.04	
Interquartile Range (IC	2.23	0.03	2.24	0.0013	4.68	0.4	1.58	0.025	0.74	0.05	10.6	0.015	0.26	2.38	
Variance	5.12	0.0018	3.05	0.000077	33.3	0.5	2.64	0.0013	0.52	0.0036	72.5	0.00014	0.067	8.75	
Skewness	-0.15	1.78	1.15	2.63	1.33	-1.52	1.56	1.46	-0.36	1.21	-1.03	0	1.2	1.34	
Coefficient of Variatior	0.15	0.76	0.66	1	0.77	0.35	0.72	0.94	0.2	0.38	0.14	0.48	0.48	0.53	
Count	8	8	8	8	8	8	8	8	8	8	8	8	8	8	

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

Data in blue indicates a calculated parameter.

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock Al * (ppm)	ICP Al (ppm)	Difference (%)[3]	Whole Rock Ba * (ppm)	ICP Ba (ppm)	Difference (%)[3]	Whole Rock Ca * (ppm)	ICP Ca (ppm)	Difference (%)[3]	Whole Rock Cr * (ppm)	ICP Cr (ppm)	Difference (%)[3]	Whole Rock Fe * (ppm)	ICP Fe (ppm)	Difference (%)[3]
Main Zone															
14130	90551	85100	-6.02	537	440	-18.12	25657	26200	2.11	34	15	-56.15	18185	18000	-1.02
14144	96796	93900	-2.99	358	380	6.07	35377	37500	6.00	34	5	-85.38	35322	36100	2.20
14148	89069	81100	-8.95	627	560	-10.68	44740	46300	3.49	34	4	-88.31	39378	38300	-2.74
14156	81183	76900	-5.28	269	280	4.21	23513	24700	5.05	34	25	-26.92	17206	17400	1.13
14162	75997	79700	4.87	537	510	-5.10	53602	55900	4.29	68	71	3.77	41407	42500	2.64
14169	82242	76400	-7.10	90	100	11.65	22513	23200	3.05	34	16	-53.23	11820	11800	-0.17
14232	103041	94400	-8.39	179	140	-21.85	26229	26600	1.41	34	14	-59.08	26998	26400	-2.22
14250	95367	94400	-1.01	179	170	-5.10	39094	40700	4.11	34	12	-64.92	46093	45800	-0.64
14260	94467	89500	-5.26	179	170	-5.10	29874	30400	1.76	34	3	-91.23	43575	42300	-2.93
14276	104575	98400	-5.91	1075	1000	-6.96	41952	43100	2.74	34	17	-50.31	39168	38900	-0.69
14295	92615	89700	-3.15	90	110	22.81	37307	39100	4.81	34	12	-64.92	47632	47300	-0.70
14301	93779	87600	-6.59	269	300	11.65	35234	36600	3.88	34	15	-56.15	31265	31300	0.11
14323	100924	93600	-7.26	269	280	4.21	35878	37500	4.52	34	3	-91.23	38749	38700	-0.13
14332	104681	96200	-8.10	179	210	17.23	33376	33900	1.57	34	3	-91.23	36301	35500	-2.21
14345	103305	97300	-5.81	179	190	6.07	24585	25500	3.72	34	11	-67.85	22242	22100	-0.64
14348	105475	94300	-10.59	179	150	-16.26	22084	21500	-2.64	34	11	-67.85	35811	34700	-3.10
14797	96213	86900	-9.68	179	150	-16.26	36592	37800	3.30	34	6	-82.46	43365	42700	-1.53
14808	82242	81300	-1.15	179	170	-5.10	47456	48700	2.62	34	6	-82.46	38049	37600	-1.18
14816	90551	82900	-8.45	179	140	-21.85	32590	33300	2.18	34	5	-85.38	42386	41300	-2.56
14828	90498	89200	-1.43	717	710	-0.91	40738	43400	6.54	34	4	-88.31	40218	41200	2.44
14844	93197	91800	-1.50	358	300	-16.26	27158	28200	3.84	34	39	14.00	51758	51800	0.08
14680	92826	90500	-2.51	269	300	11.65	39594	41400	4.56	68	5	-92.69	44134	41400	-6.20
14871	98225	96200	-2.06	90	120	33.98	33019	34000	2.97	34	10	-70.77	45813	46100	0.63
14887	93144	96900	4.03	358	340	-5.10	47956	51800	8.02	34	20	-41.54	51129	53100	3.86
14689	83353	83800	0.54	90	120	33.98	19368	21800	12.56	34	10	-70.77	13709	14800	7.96
14695	95155	97000	1.94	179	170	-5.10	35592	39800	11.82	34	6	-82.46	36301	39900	9.92
14742	97801	90600	-7.36	179	120	-33.01	27444	27800	1.30	34	24	-29.85	33573	33500	-0.22
14666	92350	92100	-0.27	358	330	-7.89	37164	39300	5.75	34	21	-38.62	51618	53900	4.42
14685	87534	85900	-1.87	448	380	-15.15	32090	33100	3.15	34	5	-85.38	62390	63900	2.42
14685B	87746	83100	-5.29	358	310	-13.47	29731	29500	-0.78	34	7	-79.54	66097	59700	-9.68
14545	98330	94700	-3.69	896	860	-3.98	37021	38200	3.18	34	16	-53.23	41826	41700	-0.30
14565	91186	88300	-3.16	179	220	22.81	43239	45800	5.92	34	11	-67.85	36720	37200	1.31
14571	87217	82200	-5.75	448	430	-3.98	25086	25900	3.25	34	7	-79.54	27908	26900	-3.61
14578	88804	86800	-2.26	627	640	2.08	39808	42000	5.51	34	9	-73.69	39938	41600	4.16
14578B	86793	82400	-5.06	806	760	-5.72	41095	43200	5.12	34	10	-70.77	41616	39200	-5.81
14598	101506	92500	-8.87	179	220	22.81	32304	33500	3.70	34	3	-91.23	45463	46600	2.50
14893	92033	92000	-0.04	448	490	9.42	39808	41600	4.50	34	44	28.62	53087	53400	0.59
14899	96531	97000	0.49	358	330	-7.89	34091	35400	3.84	34	43	25.69	56934	56900	-0.06
14908	92985	95800	3.03	717	690	-3.70	35663	37900	6.27	34	39	14.00	52388	53200	1.55
14917	88646	85300	-3.77	806	740	-8.20	22727	23200	2.08	34	16	-53.23	23991	24200	0.87
14925	92509	87800	-5.09	358	390	8.86	34520	36000	4.29	34	30	-12.31	45953	46200	0.54
14998	94414	90100	-4.57	269	280	4.21	37879	39800	5.07	34	6	-82.46	43365	43600	0.54
15862	92350	87200	-5.58	269	290	7.93	40452	42200	4.32	34	4	-88.31	42106	41600	-1.20
15870	80866	81000	0.17	1075	1030	-4.17	43596	46400	6.43	34	27	-21.08	38329	39200	2.27
15879	90180	90600	0.47	806	760	-5.72	45597	48300	5.93	34	29	-15.23	51548	51500	-0.09

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock Al * (ppm)	ICP Al (ppm)	Difference (%)[3]	Whole Rock Ba * (ppm)	ICP Ba (ppm)	Difference (%)[3]	Whole Rock Ca * (ppm)	ICP Ca (ppm)	Difference (%)[3]	Whole Rock Cr * (ppm)	ICP Cr (ppm)	Difference (%)[3]	Whole Rock Fe * (ppm)	ICP Fe (ppm)	Difference (%)[3]
15887	94414	87200	-7.64	448	440	-1.75	40166	41200	2.57	34	25	-26.92	37840	34600	-8.56
15891	93303	89500	-4.08	1343	1250	-6.96	48313	51300	6.18	34	22	-35.69	37979	38500	1.37
15908	91980	87100	-5.31	269	260	-3.24	43525	45200	3.85	34	24	-29.85	34412	34500	0.25
15911	92033	88600	-3.73	448	410	-8.45	34877	35200	0.93	34	33	-3.54	47422	46500	-1.94
125285	90551	86700	-4.25	448	420	-6.21	22441	23300	3.83	68	50	-26.92	27208	27400	0.71
125288	80390	78400	-2.47	358	320	-10.68	65752	62100	-5.55	479	269	-43.84	64208	61200	-4.69
125293	84200	82700	-1.78	179	170	-5.10	23228	24100	3.76	68	67	-2.08	36860	37200	0.92
125305	95684	92600	-3.22	358	390	8.86	26872	27700	3.08	68	40	-41.54	31824	33100	4.01
125311	96213	90300	-6.15	537	490	-8.82	22584	23500	4.05	34	32	-6.46	18535	19000	2.51
125703	104575	87600	-16.23	179	150	-16.26	34448	33300	-3.33	68	29	-57.62	40637	39600	-2.55
125728	96690	85700	-11.37	537	460	-14.40	35234	33800	-4.07	68	43	-37.15	48611	47400	-2.49
125755	83777	69000	-17.64	448	400	-10.68	19297	18400	-4.65	68	53	-22.54	10701	10000	-6.55
125772	94890	85800	-9.58	358	320	-10.68	36735	34700	-5.54	68	37	-45.92	43995	42100	-4.31
125795	91609	83900	-8.42	627	520	-17.06	45454	44300	-2.54	68	30	-56.15	50919	50000	-1.80
125422	99389	94800	-4.62	179	180	0.48	35663	36800	3.19	34	14	-59.08	43715	45600	4.31
125435	98066	84700	-13.63	179	120	-33.01	36306	34800	-4.15	34	14	-59.08	47841	46200	-3.43
125452	100659	89000	-11.58	179	120	-33.01	39808	38500	-3.29	34	8	-76.62	44344	43400	-2.13
125476	79172	68500	-13.48	1433	1310	-8.59	22155	21500	-2.96	68	58	-15.23	13989	13500	-3.49
125490	98436	92900	-5.62	90	90	0.48	34734	34700	-0.10	34	16	-53.23	49660	49900	0.48
126192	100394	93200	-7.17	179	200	11.65	35020	37000	5.65	34	22	-35.69	28187	27600	-2.08
126206	102511	102500	-0.01	448	430	-3.98	37236	39800	6.89	34	19	-44.46	35391	36400	2.85
126225	99971	86100	-13.88	627	660	5.27	36021	35700	-0.89	34	18	-47.38	33643	31900	-5.18
126244	101876	93600	-8.12	179	180	0.48	39022	41800	7.12	34	9	-73.69	34622	34800	0.51
126266	102723	97100	-5.47	179	170	-5.10	34448	36300	5.38	34	13	-62.00	39518	39500	-0.05
126279	94255	79700	-15.44	179	160	-10.68	42310	43100	1.87	68	20	-70.77	36720	35300	-3.87
126288	98860	90500	-8.46	179	190	6.07	41309	42500	2.88	34	13	-62.00	29866	29000	-2.90
126297	86476	88400	2.23	179	170	-5.10	51315	54100	5.43	34	24	-29.85	41686	42300	1.47
126314	98913	93700	-5.27	179	220	22.81	40738	42700	4.82	34	20	-41.54	37630	37200	-1.14
126329	92932	83200	-10.47	627	660	5.27	42453	43800	3.17	34	24	-29.85	31964	31100	-2.70
126337	93356	88600	-5.09	358	370	3.28	41166	41900	1.78	34	23	-32.77	42596	40800	-4.22
126351	95314	88100	-7.57	358	330	-7.89	44954	45300	0.77	34	20	-41.54	27488	27300	-0.68
126427	91715	90800	-1.00	179	200	11.65	49957	51000	2.09	34	24	-29.85	58613	58900	0.49
126430	94150	95100	1.01	179	180	0.48	42381	45500	7.36	34	12	-64.92	47422	50400	6.28
126434	98595	82200	-16.63	179	160	-10.68	43668	42200	-3.36	34	11	-67.85	43855	41400	-5.60
126443	92721	88300	-4.77	90	120	33.98	42167	42200	0.08	34	11	-67.85	48681	48000	-1.40
126449	95155	94900	-0.27	448	450	0.48	49028	49600	1.17	68	49	-28.38	62040	62500	0.74
126464	98225	93400	-4.91	269	200	-25.57	43954	45000	2.38	34	23	-32.77	42246	42400	0.36
126492	97801	90400	-7.57	269	210	-21.85	42667	42900	0.55	68	15	-78.08	40917	40400	-1.26
145655	96531	91100	-5.63	717	700	-2.31	46241	47100	1.86	34	13	-62.00	40637	40300	-0.83
145669	96954	92300	-4.80	179	190	6.07	41738	42000	0.63	34	11	-67.85	53857	52300	-2.89
145685	95790	86900	-9.28	179	130	-27.43	37521	37200	-0.86	34	19	-44.46	48261	46000	-4.69
145694	94467	85100	-9.92	179	130	-27.43	44097	43700	-0.90	34	23	-32.77	50569	48500	-4.09
145708	86793	83200	-4.14	90	100	11.65	32090	34700	8.13	34	20	-41.54	36021	36800	2.16
145723	95737	80900	-15.50	179	160	-10.68	35449	34300	-3.24	34	23	-32.77	50989	47300	-7.23
146798	97113	86300	-11.13	358	340	-5.10	40666	42700	5.00	34	16	-53.23	41477	41600	0.30
146824	94044	90200	-4.09	269	230	-14.40	37521	38500	2.61	274	43	-84.29	53157	51900	-2.37

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock Al * (ppm)	ICP Al (ppm)	Difference (%) [3]	Whole Rock Ba * (ppm)	ICP Ba (ppm)	Difference (%) [3]	Whole Rock Ca * (ppm)	ICP Ca (ppm)	Difference (%) [3]	Whole Rock Cr * (ppm)	ICP Cr (ppm)	Difference (%) [3]	Whole Rock Fe * (ppm)	ICP Fe (ppm)	Difference (%) [3]
146831	90392	87200	-3.53	179	170	-5.10	38093	38800	1.86	68	44	-35.69	45673	45100	-1.26
146843															
146861	99495	94200	-5.32	448	430	-3.98	40809	42000	2.92	34	21	-38.62	43225	42100	-2.60
146868	100553	89100	-11.39	269	270	0.48	38379	37200	-3.07	34	15	-56.15	36860	34300	-6.95
126352	96161	96100	-0.06	358	320	-10.68	35949	38400	6.82	68	44	-35.69	49240	52000	5.60
126358	94150	92500	-1.75	269	260	-3.24	34091	36700	7.65	68	41	-40.08	49730	51900	4.36
126374	94573	90700	-4.10	269	270	0.48	36521	37700	3.23	68	45	-34.23	55325	55100	-0.41
126384	93991	91000	-3.18	269	280	4.21	37521	39500	5.27	34	33	-3.54	47841	48700	1.79
126391	102564	89100	-13.13	358	320	-10.68	44382	42200	-4.92	34	11	-67.85	49240	45300	-8.00
146172	91027	72200	-20.68	269	210	-21.85	36235	34500	-4.79	34	27	-21.08	47981	43700	-8.92
146182	100871	85800	-14.94	179	210	17.23	39094	37400	-4.33	34	27	-21.08	50569	46400	-8.24
146203	94890	85400	-10.00	179	130	-27.43	28087	29300	4.32	34	27	-21.08	29726	28700	-3.45
146214	94202	81900	-13.06	269	180	-33.01	41881	41500	-0.91	34	17	-50.31	40567	38400	-5.34
146221	92191	86400	-6.28	269	290	7.93	37879	36400	-3.90	34	14	-59.08	58403	54300	-7.03
146238	98913	94800	-4.16	269	300	11.65	42024	42700	1.61	68	41	-40.08	63859	62300	-2.44
147034	100977	88900	-11.96	179	200	11.65	28945	29300	1.23	34	19	-44.46	35182	33900	-3.64
147038	84782	76000	-10.36	1164	1130	-2.95	25943	26500	2.15	68	48	-29.85	24410	23500	-3.73
147051	99812	88300	-11.53	896	880	-1.75	36306	35800	-1.39	68	23	-66.38	41686	39800	-4.53
147070	100977	101500	0.52	179	180	0.48	50672	54300	7.16	68	26	-62.00	56724	58300	2.78
147087	93462	86600	-7.34	179	120	-33.01	35735	35200	-1.50	34	25	-26.92	69174	66900	-3.29
147097	99865	94700	-5.17	1075	1010	-6.03	43525	44700	2.70	34	8	-76.62	48331	47400	-1.93
145508	98913	91400	-7.60	358	360	0.48	29302	29900	2.04	68	43	-37.15	53367	53700	0.62
145527	93620	95400	1.90	448	490	9.42	39523	42700	8.04	68	42	-38.62	49450	51900	4.95
145543	98542	87700	-11.00	358	370	3.28	34091	33700	-1.15	68	46	-32.77	40357	38200	-5.35
145562	96372	89100	-7.55	358	290	-19.05	39808	39500	-0.77	68	42	-38.62	47352	45300	-4.33
145576	82401	73700	-10.56	806	750	-6.96	17367	17400	0.19	68	62	-9.38	10422	10100	-3.09
145601	96425	96800	0.39	537	560	4.21	45383	48000	5.77	34	30	-12.31	52038	53800	3.39
146297	95790	82600	-13.77	269	250	-6.96	38379	37900	-1.25	34	17	-50.31	33713	32100	-4.78
146314	100977	83900	-16.91	269	220	-18.12	40880	39500	-3.38	34	21	-38.62	46582	43200	-7.26
146335	99124	87000	-12.23	269	220	-18.12	44597	43200	-3.13	137	16	-88.31	47702	44100	-7.55
146352	90604	77000	-15.01	269	220	-18.12	32233	31700	-1.65	68	35	-48.85	41547	38100	-8.30
146368	99865	81100	-18.79	179	170	-5.10	41595	39800	-4.32	68	19	-72.23	45184	40900	-9.48
146390	102300	93800	-8.31	179	230	28.40	47456	47600	0.30	34	5	-85.38	44344	43500	-1.90
146508	94414	90400	-4.25	269	250	-6.96	33519	35100	4.72	68	48	-29.85	39238	40300	2.71
146526	96372	88500	-8.17	537	470	-12.54	41810	41900	0.22	34	30	-12.31	31894	31000	-2.80
146544	85682	83200	-2.90	448	460	2.72	35234	37000	5.01	68	47	-31.31	18885	19100	1.14
146565	97378	79900	-17.95	1343	1230	-8.45	35234	35300	0.19	34	29	-15.23	17556	16800	-4.31
146589	92879	83600	-9.99	358	370	3.28	39665	39900	0.59	68	46	-32.77	42316	40900	-3.35
146613	93938	91400	-2.70	179	130	-27.43	53030	56300	6.17	34	23	-32.77	26788	27000	0.79
146627	74356	71100	-4.38	358	340	-5.10	33805	34800	2.94	68	49	-28.38	28327	28600	0.96
146637	85311	77600	-9.04	1075	1060	-1.38	28659	29800	3.98	68	71	3.77	17206	17000	-1.20
146649	85311	79900	-6.34	985	980	-0.53	24371	25500	4.63	68	53	-22.54	16507	16600	0.57
146657	86846	79400	-8.57	448	410	-8.45	18582	19100	2.79	68	66	-3.54	10981	10700	-2.56
146676	107380	92300	-14.04	179	230	28.40	38450	39400	2.47	34	11	-67.85	15667	15400	-1.71
125188	101294	93100	-8.09	717	650	-9.28	29588	30600	3.42	34	19	-44.46	25809	26700	3.45
125198	101400	91000	-10.26	269	290	7.93	33233	33700	1.40	34	25	-26.92	33643	33800	0.47

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock Al * (ppm)	ICP Al (ppm)	Difference (%) [3]	Whole Rock Ba * (ppm)	ICP Ba (ppm)	Difference (%) [3]	Whole Rock Ca * (ppm)	ICP Ca (ppm)	Difference (%) [3]	Whole Rock Cr * (ppm)	ICP Cr (ppm)	Difference (%) [3]	Whole Rock Fe * (ppm)	ICP Fe (ppm)	Difference (%) [3]
125207	90710	78300	-13.68	358	370	3.28	36664	35800	-2.36	34	31	-9.38	29166	28600	-1.94
125228	87111	80000	-8.16	448	430	-3.98	20297	20800	2.48	68	56	-18.15	13709	13800	0.66
125244	86899	74600	-14.15	179	170	-5.10	18796	18000	-4.24	68	51	-25.46	10212	9700	-5.01
125257	97484	86900	-10.86	269	210	-21.85	80474	79000	-1.83	205	126	-38.62	56584	55800	-1.39
125278	102723	97700	-4.89	358	310	-13.47	33876	34500	1.84	34	17	-50.31	39378	39700	0.82
125596	99759	88100	-11.69	269	220	-18.12	49743	48900	-1.69	34	12	-64.92	48541	48000	-1.11
125610	94467	85700	-9.28	90	130	45.14	26372	26600	0.86	34	18	-47.38	37560	38700	3.04
125626															
125641	94520	89200	-5.63	179	140	-21.85	35163	35800	1.81	68	42	-38.62	45393	47100	3.76
125669	87481	84700	-3.18	179	110	-38.59	29946	30200	0.85	68	37	-45.92	39378	39700	0.82
125690	94626	88100	-6.90	269	270	0.48	36878	36900	0.06	68	33	-51.77	52947	53900	1.80
West Breccia Zone															
14018	85735	80300	-6.34	1164	1120	-3.81	18082	17800	-1.56	34	24	-29.85	26369	25800	-2.16
14021	78061	77000	-1.36	448	460	2.72	25443	26200	2.97	34	21	-38.62	18325	18100	-1.23
14036	79014	74100	-6.22	537	500	-6.96	18296	18400	0.57	34	20	-41.54	26019	25600	-1.61
14043	80495	75600	-6.08	269	230	-14.40	14151	14000	-1.07	34	31	-9.38	29586	28500	-3.67
14060	80231	79600	-0.79	358	380	6.07	30517	31400	2.89	34	26	-24.00	35951	35900	-0.14
14067	85047	85100	0.06	358	370	3.28	25300	25900	2.37	68	36	-47.38	43225	42900	-0.75
14076	85153	90000	5.69	448	410	-8.45	40094	43400	8.24	34	33	-3.54	51968	54600	5.06
14083	86793	88500	1.97	717	700	-2.31	38093	40300	5.79	34	49	43.23	57773	57800	0.05
14099	80178	72400	-9.70	896	770	-14.03	29731	29500	-0.78	34	16	-53.23	23641	22300	-5.67
14103	79384	76000	-4.26	269	250	-6.96	28802	29300	1.73	34	20	-41.54	21752	21200	-2.54
125046	94520	82200	-13.03	179	210	17.23	39237	38600	-1.62	68	35	-48.85	36301	35500	-2.21
125068	97007	91500	-5.68	448	440	-1.75	41166	42500	3.24	137	45	-67.12	42246	43200	2.26
125073	95261	82500	-13.40	627	590	-5.90	34091	33500	-1.73	137	27	-80.27	22942	22000	-4.10
125079	93462	78800	-15.69	1523	1380	-9.37	19082	18500	-3.05	34	37	8.15	18745	17600	-6.11
125084	97907	84900	-13.29	896	800	-10.68	39022	37800	-3.13	68	47	-31.31	41057	39400	-4.04
125127	99389	87600	-11.86	537	500	-6.96	23799	23600	-0.84	68	35	-48.85	43505	42400	-2.54
125129	84041	76500	-8.97	269	270	0.48	17581	17500	-0.46	68	69	0.85	33993	33100	-2.63
125134	86899	79900	-8.05	537	470	-12.54	14151	14500	2.47	68	58	-15.23	59802	59100	-1.17
125142	87164	78500	-9.94	358	310	-13.47	20583	20500	-0.40	137	92	-32.77	41966	41100	-2.06
125149	92509	85500	-7.58	537	470	-12.54	33448	31600	-5.52	34	32	-6.46	50289	48600	-3.36
125154	100818	85800	-14.90	179	150	-16.26	24943	23500	-5.78	34	23	-32.77	14478	13500	-6.76
125165	104946	97300	-7.29	179	160	-10.68	29731	29500	-0.78	34	14	-59.08	31964	32100	0.42
125176	98383	86000	-12.59	269	240	-10.68	26229	25400	-3.16	34	15	-56.15	36650	36000	-1.77
146112	100447	92900	-7.51	269	260	-3.24	30232	31600	4.53	34	30	-12.31	40078	39000	-2.69
146115	89757	89100	-0.73	627	550	-12.28	72827	71900	-1.27	68	41	-40.08	72392	69100	-4.55
146124	111932	96300	-13.97	627	570	-9.09	42453	40800	-3.89	34	12	-64.92	43925	40500	-7.80
146127	83988	68000	-19.04	537	510	-5.10	25515	25200	-1.23	68	63	-7.92	17416	15700	-9.85
146135	107010	95600	-10.66	537	490	-8.82	42167	41600	-1.34	34	18	-47.38	44134	41600	-5.74
146149	107380	87600	-18.42	537	470	-12.54	43525	41400	-4.88	34	25	-26.92	41267	37200	-9.85
146161	93144	88900	-4.56	717	690	-3.70	66395	64500	-2.85	34	21	-38.62	64348	60400	-6.14
146164	101400	83700	-17.46	537	510	-5.10	36807	35100	-4.64	34	15	-56.15	66656	60600	-9.09
145951	96584	90200	-6.61	269	290	7.93	40023	42000	4.94	34	18	-47.38	41826	41500	-0.78
145956	97007	83800	-13.61	179	150	-16.26	34091	32500	-4.67	34	27	-21.08	50779	47400	-6.65
145974	102088	86700	-15.07	269	230	-14.40	25729	25700	-0.11	34	8	-76.62	51339	48700	-5.14

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock Al * (ppm)	ICP Al (ppm)	Difference (%) [3]	Whole Rock Ba * (ppm)	ICP Ba (ppm)	Difference (%) [3]	Whole Rock Ca * (ppm)	ICP Ca (ppm)	Difference (%) [3]	Whole Rock Cr * (ppm)	ICP Cr (ppm)	Difference (%) [3]	Whole Rock Fe * (ppm)	ICP Fe (ppm)	Difference (%) [3]
145982	95049	90400	-4.89	269	230	-14.40	64894	62000	-4.46	68	23	-66.38	62460	57900	-7.30
145992	98648	77100	-21.84	269	180	-33.01	29017	26800	-7.64	34	31	-9.38	39938	35600	-10.86
145999	101347	82700	-18.40	179	160	-10.68	39094	35300	-9.70	34	15	-56.15	43925	38600	-12.12
145834	102300	87500	-14.47	179	150	-16.26	31589	30700	-2.82	34	24	-29.85	42666	39200	-8.12
145842	88275	88400	0.14	90	30	-66.51	79259	78000	-1.59	205	106	-48.36	44904	42600	-5.13
145852	94202	84100	-10.72	45	40	-10.68	44811	43600	-2.70	68	56	-18.15	31754	29400	-7.41
145857	104999	94000	-10.48	269	240	-10.68	43954	44700	1.70	34	31	-9.38	31125	29900	-3.94
145871	100447	88200	-12.19	269	290	7.93	42739	41700	-2.43	34	30	-12.31	41826	39300	-6.04
145608	91503	91900	0.43	358	390	8.86	34448	36900	7.12	34	28	-18.15	58823	60800	3.36
145614	91027	90000	-1.13	537	520	-3.24	34448	36200	5.09	34	33	-3.54	59102	59600	0.84
145628	86476	78900	-8.76	90	80	-10.68	36735	36500	-0.64	34	25	-26.92	46862	46100	-1.63
145640	89810	92100	2.55	448	420	-6.21	42238	44300	4.88	68	43	-37.15	55255	57100	3.34
145646	91874	89600	-2.47	358	330	-7.89	35592	37000	3.96	34	31	-9.38	55605	55900	0.53
Paramount Zone															
125965	86740	88900	2.49	269	260	-3.24	22513	25600	13.71	68	68	-0.62	34202	36800	7.59
125974	87217	78700	-9.76	358	300	-16.26	18439	18200	-1.30	34	38	11.08	46233	44700	-3.32
125983	74303	74200	-0.14	537	520	-3.24	36521	37000	1.31	205	141	-31.31	49800	48600	-2.41
125988	93091	93800	0.76	717	660	-7.89	46812	47600	1.68	68	46	-32.77	59802	58700	-1.84
126007	82665	79000	-4.43	448	470	4.95	19797	21300	7.59	137	81	-40.81	12450	12600	1.21
126031	84253	80000	-5.05	896	850	-5.10	18153	18700	3.01	68	71	3.77	15318	15100	-1.42
126040	88857	86100	-3.10	269	280	4.21	18010	18400	2.16	68	101	47.62	30985	30400	-1.89
126054	67529	67400	-0.19	358	410	14.44	48242	48100	-0.29	274	196	-28.38	48751	47900	-1.75
126067	78008	75400	-3.34	179	200	11.65	44382	43600	-1.76	205	123	-40.08	46652	44300	-5.04
126081	70387	67400	-4.24	1343	1270	-5.47	17939	18600	3.69	137	108	-21.08	20144	20500	1.77
126110	95102	95700	0.63	896	840	-6.21	47027	48700	3.56	68	54	-21.08	59732	59900	0.28
126118	84412	79000	-6.41	358	330	-7.89	35878	35400	-1.33	68	76	11.08	41896	40300	-3.81
125904	99124	91400	-7.79	269	270	0.48	37950	38500	1.45	34	17	-50.31	35811	34700	-3.10
125919	103623	95400	-7.94	269	240	-10.68	22870	22700	-0.74	34	13	-62.00	45254	43100	-4.76
125928	97378	82800	-14.97	717	610	-14.87	28445	27800	-2.27	68	38	-44.46	54136	50100	-7.46
125933	93567	94200	0.68	537	510	-5.10	36378	38300	5.28	34	27	-21.08	64628	66800	3.36
125944	96637	95900	-0.76	627	610	-2.71	32233	33800	4.86	68	36	-47.38	51828	51300	-1.02
125952	81289	74900	-7.86	358	390	8.86	27945	29700	6.28	68	76	11.08	24061	24000	-0.25
125963	92932	90800	-2.29	448	400	-10.68	34448	35800	3.92	34	26	-24.00	52877	53300	0.80
126120	88646	85400	-3.66	537	510	-5.10	15366	16400	6.73	137	85	-37.88	14129	14400	1.92
126131	84465	82400	-2.44	448	450	0.48	22513	24600	9.27	68	53	-22.54	10352	10700	3.37
126142	91133	82000	-10.02	269	280	4.21	27015	27600	2.16	68	50	-26.92	17206	16400	-4.69
126154	94890	83800	-11.69	90	120	33.98	29445	30100	2.22	68	37	-45.92	18115	17700	-2.29
126171	80601	80000	-0.75	985	990	0.48	30732	33900	10.31	68	52	-24.00	29866	30400	1.79
126181	102564	97400	-5.04	358	310	-13.47	41166	41800	1.54	68	44	-35.69	50289	49000	-2.56
125806	86687	79600	-8.18	1075	1060	-1.38	25229	25500	1.08	68	66	-3.54	24760	24800	0.16
125816	91080	91800	0.79	1254	1180	-5.90	35663	36800	3.19	34	27	-21.08	61830	64500	4.32
125833	85047	77700	-8.64	717	670	-6.49	20011	20800	3.94	68	94	37.38	15667	15900	1.48
125861	85153	81900	-3.82	717	750	4.67	18010	19400	7.72	68	76	11.08	12310	13200	7.23
125875	82295	73900	-10.20	896	800	-10.68	21298	21800	2.36	68	71	3.77	14828	14800	-0.19
125897	81183	73800	-9.09	269	250	-6.96	21226	21500	1.29	68	65	-5.00	7694	7400	-3.82

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock Al * (ppm)	ICP Al (ppm)	Difference (%) [3]	Whole Rock Ba * (ppm)	ICP Ba (ppm)	Difference (%) [3]	Whole Rock Ca * (ppm)	ICP Ca (ppm)	Difference (%) [3]	Whole Rock Cr * (ppm)	ICP Cr (ppm)	Difference (%) [3]	Whole Rock Fe * (ppm)	ICP Fe (ppm)	Difference (%) [3]
Tailings															
LIARD ZONE	93726	79200	-15.50	358	290	-19.05	35878	34000	-5.23	68	23	-66.38	38749	35400	-8.64
PARAMOUNT	84729	70400	-16.91	537	430	-19.98	28659	26900	-6.14	68	45	-34.23	28677	25600	-10.73
WEST BRECCIA	92826	89400	-3.69	537	460	-14.40	29088	28000	-3.74	68	50	-26.92	38539	37500	-2.70
High-Sulphide Histor															
T112 (171' - 172')	69858	71700	2.64	179	100	-44.18	42882	42100	-1.82	68	16	-76.62	109602	107000	-2.37
T113 (81' - 82')	85788	86100	0.36	1343	1370	1.97	8362	8500	1.65	34	15	-56.15	25529	25800	1.06
T113 (983' - 985')	78908	81100	2.78	179	200	11.65	23942	24600	2.75	34	33	-3.54	41477	42000	1.26
T140 (30' - 31')	99918	98200	-1.72	358	330	-7.89	30232	31000	2.54	34	1	-98.54	33853	33400	-1.34
T166 (389' - 390')	86317	85800	-0.60	537	490	-8.82	16581	16900	1.92	34	28	-18.15	19934	19600	-1.68
T185 (116' - 117')	87111	84800	-2.65	717	430	-39.99	9434	9400	-0.36	205	9	-95.62	25879	25500	-1.47
T207 (261.5' - 262')	76367	72400	-5.20	358	220	-38.59	10720	10400	-2.99	34	28	-18.15	41057	39600	-3.55
T207 (269' - 271')	60808	57200	-5.93	358	190	-46.97	9505	9100	-4.27	34	10	-70.77	123451	128500	4.09
All Data															
Maximum			5.69			45.1			13.7			47.6			9.92
Minimum			-21.8			-66.5			-9.7			-98.5			-12.1
Mean			-6.66			-5.19			1.58			-39.8			-1.61
Standard Deviation			5.46			14.3			3.85			28.1			3.77
10 Percentile			-14.1			-19.6			-3.59			-77.5			-6.87
25 Percentile			-10.2			-10.7			-1.26			-59.1			-3.81
Median			-6.02			-5.1			1.92			-38.6			-1.53
75 Percentile			-2.8			2.4			4.08			-21.8			0.77
90 Percentile			0.28			11.6			6.18			-3.54			2.96
Interquartile Range (IC			7.43			13.1			5.34			37.3			4.58
Variance			29.9			203			14.8			791			14.2
Skewness			-0.31			-0.091			0.0043			0.25			-0.11
Coefficient of Variatior			-0.82			-2.75			2.43			-0.71			-2.33
Count			235			235			235			235			235
Main Zone															
Maximum			4.87			45.1			12.6			28.6			9.92
Minimum			-20.7			-38.6			-5.55			-92.7			-9.68
Mean			-6.66			-3.69			2.12			-46.2			-1.15
Standard Deviation			5.06			14.5			3.54			26.4			3.55
10 Percentile			-13.7			-21.8			-3.26			-82.5			-5.7
25 Percentile			-9.97			-10.7			0.064			-67.8			-3.33
Median			-5.86			-5.1			2.59			-44.5			-1.07
75 Percentile			-3.19			4.21			4.52			-29.8			0.86
90 Percentile			-0.049			11.6			6.17			-12.3			2.94
Interquartile Range (IC			6.78			14.9			4.45			38			4.19
Variance			25.6			209			12.5			697			12.6
Skewness			-0.31			0.41			-0.13			0.27			-0.052
Coefficient of Variatior			-0.76			-3.92			1.67			-0.57			-3.09
Count			146			146			146			146			146

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock Al * (ppm)	ICP Al (ppm)	Difference (%) [3]	Whole Rock Ba * (ppm)	ICP Ba (ppm)	Difference (%) [3]	Whole Rock Ca * (ppm)	ICP Ca (ppm)	Difference (%) [3]	Whole Rock Cr * (ppm)	ICP Cr (ppm)	Difference (%) [3]	Whole Rock Fe * (ppm)	ICP Fe (ppm)	Difference (%) [3]
West Breccia Zone															
Maximum			5.69			17.2			8.24			43.2			5.06
Minimum			-21.8			-66.5			-9.7			-80.3			-12.1
Mean			-8.49			-8.38			-0.52			-31.9			-3.61
Standard Deviation			6.46			12.1			3.88			24.5			3.86
10 Percentile			-16.4			-15.1			-4.75			-61.4			-8.51
25 Percentile			-13.3			-12.5			-2.95			-48.6			-6.12
Median			-8.76			-8.82			-1.07			-32.8			-3.36
75 Percentile			-4.41			-3.47			2.42			-12.3			-1.2
90 Percentile			0.094			4.39			4.9			-5.29			0.65
Interquartile Range (IC			8.93			9.07			5.37			36.3			4.92
Variance			41.7			145			15			600			14.9
Skewness			0.11			-2.27			0.18			0.39			-0.042
Coefficient of Variatior			-0.76			-1.44			-7.51			-0.77			-1.07
Count			47			47			47			47			47
Paramount Zone															
Maximum			2.49			34			13.7			47.6			7.59
Minimum			-15			-16.3			-2.27			-62			-7.46
Mean			-4.72			-1.96			3.31			-17.8			-0.53
Standard Deviation			4.39			9.96			3.72			25.9			3.48
10 Percentile			-10			-10.7			-1.3			-45.9			-4.69
25 Percentile			-8.06			-7.42			1.3			-36.8			-2.83
Median			-4.24			-5.1			2.36			-22.5			-1.02
75 Percentile			-0.75			2.35			5.07			1.58			1.63
90 Percentile			0.68			8.86			7.72			11.1			3.37
Interquartile Range (IC			7.3			9.77			3.77			38.4			4.46
Variance			19.2			99.2			13.8			671			12.1
Skewness			-0.32			1.67			0.87			0.7			0.49
Coefficient of Variatior			-0.93			-5.07			1.12			-1.46			-6.6
Count			31			31			31			31			31

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock Al * (ppm)	ICP Al (ppm)	Difference (%)[3]	Whole Rock Ba * (ppm)	ICP Ba (ppm)	Difference (%)[3]	Whole Rock Ca * (ppm)	ICP Ca (ppm)	Difference (%)[3]	Whole Rock Cr * (ppm)	ICP Cr (ppm)	Difference (%)[3]	Whole Rock Fe * (ppm)	ICP Fe (ppm)	Difference (%)[3]
Tailings															
Maximum			-3.69			-14.4			-3.74			-26.9			-2.7
Minimum			-16.9			-20			-6.14			-66.4			-10.7
Mean			-12			-17.8			-5.04			-42.5			-7.36
Standard Deviation			7.26			2.99			1.21			21			4.17
10 Percentile			-16.6			-19.8			-5.96			-60			-10.3
25 Percentile			-16.2			-19.5			-5.69			-50.3			-9.69
Median			-15.5			-19.1			-5.23			-34.2			-8.64
75 Percentile			-9.59			-16.7			-4.49			-30.6			-5.67
90 Percentile			-6.05			-15.3			-4.04			-28.4			-3.89
Interquartile Range (IC			6.61			2.79			1.2			19.7			4.02
Variance			52.7			8.95			1.47			441			17.4
Skewness			1.66			1.55			0.71			-1.5			1.26
Coefficient of Variatior			-0.6			-0.17			-0.24			-0.49			-0.57
Count			3			3			3			3			3
High-Sulphide Histor															
Maximum			2.78			11.6			2.75			-3.54			4.09
Minimum			-5.93			-47			-4.27			-98.5			-3.55
Mean			-1.29			-21.6			-0.071			-54.7			-0.5
Standard Deviation			3.25			23.3			2.7			37.1			2.46
10 Percentile			-5.42			-45			-3.37			-96.5			-2.73
25 Percentile			-3.29			-41			-2.11			-81.4			-1.85
Median			-1.16			-23.7			0.65			-63.5			-1.4
75 Percentile			0.93			-5.42			2.08			-18.2			1.11
90 Percentile			2.68			4.88			2.6			-13.8			2.11
Interquartile Range (IC			4.22			35.6			4.19			63.2			2.96
Variance			10.6			542			7.28			1375			6.06
Skewness			-0.16			0.24			-0.49			0.24			0.87
Coefficient of Variatior			-2.52			-1.08			-37.8			-0.68			-4.94
Count			8			8			8			8			8

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile

[2] Coefficient of Variation (CoV) = standard deviation divided by mean

[3] Difference (%) = (ICP - Whole Rock) * 100 / Whole Rock

* Element calculated from Whole Rock XRF analysis

Al (Whole Rock) = $(Al_2O_3*2*10000*26.98)/(2*26.98+3*16)$
Ba (Whole Rock) = $(BaO*10000*137.34)/(137.34+16)$
Ca (Whole Rock) = $(CaO*10000*40.08)/(40.08+16)$
Cr (Whole Rock) = $(Cr_2O_3*2*10000*52.00)/(2*52.00+3*16)$
Fe (Whole Rock) = $(Fe_2O_3*2*10000*55.85)/(2*55.85+3*16)$

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock K * (ppm)	ICP K (ppm)	Difference (%) [3]	Whole Rock Mg * (ppm)	ICP Mg (ppm)	Difference (%) [3]	Whole Rock Mn * (ppm)	ICP Mn (ppm)	Difference (%) [3]	Whole Rock Na * (ppm)	ICP Na (ppm)	Difference (%) [3]	Whole Rock P * (ppm)	ICP P (ppm)	Difference (%) [3]
Main Zone															
14130	17515	18100	3.34	9710	10200	5.05	155	191	23.31	34199	38300	11.99	1222	1390	13.76
14144	15274	15600	2.13	10916	11600	6.27	387	451	16.47	30045	34900	16.16	1571	1830	16.49
14148	20670	20600	-0.34	18876	18900	0.13	387	429	10.79	12760	13800	8.15	1135	1220	7.53
14156	11705	12200	4.23	7297	7900	8.26	232	339	45.91	33606	37400	11.29	436	500	14.58
14162	14859	16000	7.68	23942	26200	9.43	774	853	10.14	16840	19300	14.61	873	980	12.29
14169	8882	9700	9.21	3679	4000	8.73	232	278	19.65	42731	47600	11.40	524	550	5.03
14232	16685	16800	0.69	8926	9100	1.95	155	189	22.02	39392	42800	8.65	1309	1430	9.23
14250	13863	14600	5.32	17308	18800	8.62	387	436	12.59	33235	38300	15.24	1222	1450	18.67
14260	15772	15900	0.81	13328	13900	4.29	232	275	18.36	35386	38600	9.08	1222	1390	13.76
14276	7139	7600	6.46	15439	16400	6.23	1084	1085	0.07	36870	40800	10.66	1266	1440	13.79
14295	15191	16000	5.33	14655	15500	5.77	387	436	12.59	29674	33600	13.23	1178	1360	15.43
14301	19425	19200	-1.16	12062	12400	2.81	465	517	11.26	24704	27300	10.51	1222	1380	12.94
14323	17432	18200	4.40	9348	9600	2.70	310	386	24.60	30935	35000	13.14	1222	1410	15.40
14332	20421	20200	-1.08	10313	10400	0.85	232	281	20.94	29897	32400	8.37	1309	1470	12.29
14345	22662	24000	5.90	9890	10300	4.14	77	150	93.68	33161	36900	11.28	1222	1380	12.94
14348	18678	18700	0.12	11881	12100	1.85	155	191	23.31	35535	38200	7.50	1353	1520	12.36
14797	18927	19500	3.03	14836	15200	2.46	465	559	20.30	23888	26700	11.77	1178	1330	12.88
14808	20670	20800	0.63	15801	16300	3.16	465	493	6.10	18546	20000	7.84	1004	1080	7.60
14816	20753	20900	0.71	16766	17000	1.40	387	438	13.11	24110	26700	10.74	1135	1230	8.41
14828	16104	17500	8.67	16464	18200	10.54	465	507	9.11	28265	32900	16.40	1091	1280	17.33
14844	16436	16900	2.82	35823	37900	5.80	232	319	37.30	21662	24600	13.56	1135	1290	13.70
14680	15025	16000	6.49	15077	16500	9.44	465	493	6.10	30045	34600	15.16	1135	1300	14.58
14871	11290	12300	8.95	17308	19200	10.93	310	374	20.73	38280	44300	15.73	1047	1230	17.44
14887	10293	11700	13.67	21771	24700	13.45	542	613	13.07	30045	35400	17.82	1004	1200	19.56
14689	15855	16400	3.44	5488	5600	2.04	232	301	29.55	32196	34300	6.53	480	540	12.50
14695	21334	22100	3.59	14534	15100	3.89	542	611	12.71	26484	30000	13.28	1135	1400	23.39
14742	12369	12800	3.49	20444	22400	9.57	310	401	29.45	38651	43600	12.81	1091	1220	11.83
14666	12701	12900	1.57	21650	22000	1.61	465	543	16.86	32864	35800	8.93	1091	1250	14.58
14685	12203	12100	-0.84	27199	27300	0.37	310	364	17.50	29897	32000	7.04	1353	1530	13.10
14685B	12784	13200	3.26	26354	28400	7.76	310	327	5.56	29526	33900	14.82	1309	1530	16.87
14545	11373	11800	3.76	13087	14000	6.98	232	273	17.50	31158	35000	12.33	1178	1330	12.88
14565	17764	18600	4.70	11398	12100	6.16	465	529	13.84	26484	29900	12.90	1135	1270	11.93
14571	14610	14200	-2.81	12242	11700	-4.43	155	230	48.49	32048	32200	0.47	960	1030	7.29
14578	15689	15800	0.71	12001	11800	-1.68	310	337	8.79	29674	31500	6.15	1353	1550	14.58
14578B	15274	15800	3.44	11881	12700	6.90	310	345	11.37	29006	32900	13.42	1309	1470	12.29
14598	12784	12400	-3.00	22857	22100	-3.31	542	631	16.39	29303	31400	7.16	1353	1540	13.84
14893	9214	10200	10.70	24545	27200	10.82	465	493	6.10	31380	36600	16.63	1091	1260	15.50
14899	7471	7700	3.07	37994	41300	8.70	465	546	17.50	29229	34100	16.67	1091	1260	15.50
14908	12535	13700	9.30	21470	24000	11.79	465	527	13.41	37760	44700	18.38	1135	1310	15.46
14917	15440	16100	4.27	16524	18300	10.75	310	379	22.34	41692	47300	13.45	960	1100	14.58
14925	14942	15400	3.07	18756	20400	8.77	387	408	5.36	30861	35600	15.36	1091	1230	12.75
14998	11539	12500	8.33	14896	16300	9.43	387	452	16.73	35683	41400	16.02	1222	1440	17.85
15862	14361	14800	3.06	16524	17400	5.30	542	584	7.73	30564	34400	12.55	1135	1260	11.05
15870	17349	18500	6.63	16162	17700	9.51	465	539	16.00	22775	26200	15.04	1004	1120	11.59
15879	14029	14900	6.21	17127	18800	9.77	465	554	19.22	28265	32900	16.40	1091	1280	17.33

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock K * (ppm)	ICP K (ppm)	Difference (%)[3]	Whole Rock Mg * (ppm)	ICP Mg (ppm)	Difference (%)[3]	Whole Rock Mn * (ppm)	ICP Mn (ppm)	Difference (%)[3]	Whole Rock Na * (ppm)	ICP Na (ppm)	Difference (%)[3]	Whole Rock P * (ppm)	ICP P (ppm)	Difference (%)[3]
15887	11622	11900	2.40	14836	15900	7.17	310	395	27.51	34422	39300	14.17	960	1090	13.54
15891	16519	17200	4.12	16042	17300	7.84	465	558	20.08	30564	34900	14.19	1004	1120	11.59
15908	17349	18000	3.75	17248	18500	7.26	387	433	11.82	25520	29000	13.64	1004	1130	12.59
15911	13448	13800	2.62	21349	23100	8.20	387	402	3.81	28858	32500	12.62	1091	1250	14.58
125285	18927	18600	-1.73	19298	19400	0.53	232	256	10.18	34348	33500	-2.47	1122	1230	9.67
125288	8965	8500	-5.19	65193	64300	-1.37	1162	1070	-7.89	13576	13600	0.18	816	860	5.39
125293	11788	11100	-5.83	25812	26500	2.67	310	341	10.08	34719	34600	-0.34	1143	1250	9.33
125305	18927	18300	-3.31	19479	20200	3.70	232	279	20.08	33977	35400	4.19	1139	1270	11.51
125311	21002	20200	-3.82	13750	13800	0.36	155	192	23.96	34867	35400	1.53	1148	1260	9.79
125703	24156	22500	-6.86	14293	13100	-8.35	465	456	-1.87	23739	23100	-2.69	1239	1300	4.90
125728	13448	12500	-7.05	20806	20100	-3.39	387	363	-6.26	34496	33700	-2.31	1130	1190	5.29
125755	22579	19600	-13.19	6031	5300	-12.12	77	89	14.92	29897	27300	-8.69	471	440	-6.64
125772	14776	13700	-7.28	21228	20200	-4.84	465	422	-9.18	31974	30800	-3.67	1113	1110	-0.25
125795	16436	15500	-5.70	20324	19800	-2.58	774	712	-8.06	25520	25400	-0.47	1082	1150	6.26
125422	15025	14900	-0.83	15982	16300	1.99	387	391	0.97	32641	34200	4.77	1222	1360	11.30
125435	16187	15100	-6.72	14233	13300	-6.55	387	359	-7.29	33977	33000	-2.87	1226	1260	2.75
125452	14029	13400	-4.48	15620	15200	-2.69	310	306	-1.22	36128	36000	-0.35	1300	1380	6.12
125476	20089	17800	-11.39	8443	7600	-9.99	155	183	18.15	25297	23500	-7.10	489	470	-3.84
125490	16934	16200	-4.34	19841	19800	-0.21	465	415	-10.69	30119	30000	-0.40	1222	1300	6.39
126192	10874	11200	2.99	9710	9900	1.96	387	389	0.46	42879	45100	5.18	1353	1540	13.84
126206	12120	12700	4.79	10916	11500	5.35	310	331	6.85	36647	39400	7.51	1536	1840	19.79
126225	15191	14900	-1.92	7659	7300	-4.69	387	369	-4.71	40134	41000	2.16	1492	1670	11.90
126244	18844	19800	5.08	12484	12300	-1.47	465	492	5.88	33458	35400	5.81	1178	1380	17.12
126266	19591	20800	6.17	12725	12900	1.38	465	493	6.10	30861	33000	6.93	1292	1490	15.35
126279	16436	16300	-0.83	11398	10500	-7.88	542	554	2.19	34274	35300	2.99	1209	1320	9.20
126288	20587	21000	2.01	10855	10500	-3.27	310	358	15.56	29452	31000	5.26	1161	1310	12.86
126297	16104	17400	8.05	16464	17400	5.69	465	514	10.62	24852	26800	7.84	1196	1420	18.76
126314	20338	22100	8.66	14956	15000	0.29	387	410	5.88	23739	24200	1.94	1148	1300	13.27
126329	16436	17400	5.86	13207	12900	-2.33	387	438	13.11	24407	24600	0.79	1135	1270	11.93
126337	16270	16500	1.41	16946	17000	0.32	387	366	-5.48	28710	28700	-0.03	1183	1320	11.62
126351	16685	16400	-1.71	15861	15400	-2.91	387	395	2.01	29748	30500	2.53	1222	1330	8.85
126427	15440	15900	2.98	23520	23700	0.77	1162	1150	-1.01	18843	19700	4.55	986	1080	9.51
126430	13531	14400	6.42	16464	17300	5.08	697	733	5.16	29822	32800	9.98	1362	1580	16.05
126434	14029	13500	-3.77	12303	11000	-10.59	542	520	-4.08	34051	34100	0.14	1423	1440	1.22
126443	16602	16100	-3.03	15378	14700	-4.41	620	624	0.72	27968	28400	1.55	1388	1480	6.65
126449	4898	5100	4.13	37451	38400	2.53	1162	1155	-0.58	21588	22800	5.61	1126	1240	10.14
126464	14776	14700	-0.51	14474	14200	-1.89	620	602	-2.84	26929	28100	4.35	1283	1400	9.12
126492	16353	16400	0.29	15198	14700	-3.27	387	420	8.46	27671	28600	3.36	1318	1430	8.51
145655	12784	13200	3.26	14534	14600	0.45	465	506	8.89	30268	31900	5.39	1279	1400	9.49
145669	14195	13800	-2.78	14353	14400	0.33	542	537	-0.94	32716	32500	-0.66	1296	1440	11.11
145685	14942	15400	3.07	17369	17000	-2.12	697	660	-5.31	30119	29900	-0.73	1095	1180	7.73
145694	13199	12900	-2.26	17791	17300	-2.76	542	561	3.48	34422	34900	1.39	1113	1210	8.74
145708	12784	13000	1.69	10855	11400	5.02	387	448	15.69	35015	37100	5.95	833	950	13.98
145723	15357	15000	-2.33	12906	11600	-10.12	310	305	-1.54	29155	27800	-4.65	1161	1210	4.24
146798	15689	15600	-0.57	13569	13500	-0.51	542	535	-1.31	30713	32500	5.82	1152	1250	8.50
146824	9795	10100	3.11	22495	23900	6.25	465	432	-7.03	38428	40700	5.91	1165	1300	11.57

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock K * (ppm)	ICP K (ppm)	Difference (%) [3]	Whole Rock Mg * (ppm)	ICP Mg (ppm)	Difference (%) [3]	Whole Rock Mn * (ppm)	ICP Mn (ppm)	Difference (%) [3]	Whole Rock Na * (ppm)	ICP Na (ppm)	Difference (%) [3]	Whole Rock P * (ppm)	ICP P (ppm)	Difference (%) [3]
146831	10874	11000	1.15	25751	27100	5.24	465	467	0.50	31009	31900	2.87	1108	1190	7.36
146843															
146861	11539	11900	3.13	16102	16600	3.09	310	312	0.72	32864	34400	4.67	1165	1310	12.43
146868	16436	15200	-7.52	14715	14400	-2.14	155	189	22.02	31306	30500	-2.58	1200	1270	5.83
126352	11705	12600	7.65	21831	23400	7.19	387	390	0.72	35609	39700	11.49	1139	1290	13.26
126358	12701	13500	6.29	19359	20400	5.38	387	384	-0.83	36351	39800	9.49	1126	1290	14.58
126374	8965	9200	2.62	22193	22500	1.38	465	483	3.94	34496	35500	2.91	1226	1350	10.09
126384	9961	9900	-0.62	15439	15600	1.04	387	433	11.82	30193	32100	6.31	842	930	10.42
126391	10127	9500	-6.19	19178	17700	-7.71	465	402	-13.49	32196	31100	-3.41	1082	1080	-0.21
146172	15523	14400	-7.24	15198	13800	-9.20	387	411	6.14	33309	31100	-6.63	1113	1140	2.45
146182	11871	11700	-1.44	19721	18900	-4.16	387	392	1.23	30861	29500	-4.41	1204	1300	7.94
146203	13448	13600	1.13	15982	15700	-1.76	387	427	10.27	36796	36500	-0.80	1130	1270	12.37
146214	13697	12900	-5.82	14474	14000	-3.27	465	464	-0.15	34570	34200	-1.07	1161	1260	8.55
146221	12037	11700	-2.80	24726	24300	-1.72	465	424	-8.75	33087	32400	-2.08	1383	1490	7.71
146238	11622	12300	5.84	21289	21500	0.99	542	545	0.53	32864	33400	1.63	1143	1280	11.95
147034	21085	20500	-2.77	10313	9800	-4.97	232	230	-1.01	31306	30600	-2.26	1279	1350	5.58
147038	16353	15900	-2.77	11097	10800	-2.67	155	172	11.05	29526	29500	-0.09	768	800	4.16
147051	14942	14800	-0.95	15801	15800	0.00	232	250	7.60	29377	29100	-0.94	1283	1390	8.34
147070	7720	8500	10.10	17670	19100	8.09	697	702	0.72	29822	32500	8.98	1322	1550	17.23
147087	6143	6100	-0.70	17610	17900	1.65	542	485	-10.54	38057	38000	-0.15	1143	1240	8.46
147097	21334	21400	0.31	15559	15700	0.90	542	549	1.27	27374	27500	0.46	1209	1320	9.20
145508	7720	7700	-0.26	38597	39900	3.38	542	557	2.74	32196	34600	7.47	1056	1150	8.90
145527	15440	16400	6.22	14715	15500	5.33	387	409	5.62	31158	34400	10.41	1087	1240	14.12
145543	15274	14600	-4.41	17911	17100	-4.53	387	352	-9.10	34941	35000	0.17	1165	1210	3.85
145562	15191	15200	0.06	17730	17000	-4.12	465	418	-10.04	32716	32900	0.56	1152	1200	4.16
145576	22247	20800	-6.50	6332	5900	-6.83	77	84	8.46	32641	31600	-3.19	463	460	-0.55
145601	12701	13500	6.29	18514	19500	5.32	697	703	0.86	33383	36800	10.23	1152	1310	13.71
146297	14942	15300	2.40	19298	19700	2.08	310	341	10.08	28561	28600	0.14	1113	1240	11.43
146314	12369	12100	-2.17	17067	16700	-2.15	465	444	-4.45	30268	29800	-1.54	1239	1340	8.12
146335	17349	17600	1.44	14414	13700	-4.95	465	459	-1.22	28635	27900	-2.57	1231	1300	5.64
146352	8882	8600	-3.18	16585	15500	-6.54	465	423	-8.97	33680	32200	-4.39	1170	1220	4.32
146368	14112	13500	-4.34	15982	14200	-11.15	542	532	-1.87	30045	28600	-4.81	1279	1350	5.58
146390	11207	11500	2.62	15137	15400	1.74	465	468	0.72	30935	32300	4.41	1314	1440	9.63
146508	22413	23000	2.62	22796	24500	7.47	310	355	14.60	27078	29000	7.10	1056	1190	12.68
146526	14942	14900	-0.28	15499	15600	0.65	310	287	-7.35	33087	33400	0.95	1143	1260	10.21
146544	16104	16400	1.84	11097	11400	2.73	310	362	16.86	30564	31900	4.37	768	870	13.28
146565	23741	23100	-2.70	12423	11600	-6.63	232	275	18.36	27152	26900	-0.93	1545	1630	5.52
146589	16270	15900	-2.28	17127	17000	-0.74	310	319	2.98	26336	26600	1.00	1034	1130	9.26
146613	7637	8100	6.06	14233	15400	8.20	465	497	6.96	45476	49400	8.63	1034	1180	14.10
146627	11788	12100	2.65	15258	15900	4.21	387	389	0.46	23368	24100	3.13	847	930	9.85
146637	23492	23100	-1.67	11278	11000	-2.46	310	301	-2.84	20698	20800	0.49	589	640	8.64
146649	15523	15400	-0.79	9529	9700	1.80	232	247	6.31	33680	34100	1.25	511	560	9.68
146657	12037	12200	1.36	7780	7900	1.55	232	258	11.05	40060	39700	-0.90	515	550	6.81
146676	14029	14200	1.22	9167	8900	-2.91	465	456	-1.87	46588	47900	2.82	1392	1500	7.75
125188	18428	18100	-1.78	12001	12100	0.82	155	206	33.00	35312	37200	5.35	1340	1500	11.97
125198	16934	16900	-0.20	14172	13900	-1.92	310	325	4.91	31009	31800	2.55	1588	1740	9.54

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock K * (ppm)	ICP K (ppm)	Difference (%) [3]	Whole Rock Mg * (ppm)	ICP Mg (ppm)	Difference (%) [3]	Whole Rock Mn * (ppm)	ICP Mn (ppm)	Difference (%) [3]	Whole Rock Na * (ppm)	ICP Na (ppm)	Difference (%) [3]	Whole Rock P * (ppm)	ICP P (ppm)	Difference (%) [3]
125207	18428	17300	-6.12	13750	12800	-6.91	465	436	-6.17	25742	25800	0.22	1484	1580	6.49
125228	11871	11700	-1.44	8081	8000	-1.01	155	207	33.64	41247	42100	2.07	497	520	4.53
125244	6558	6100	-6.98	9106	8800	-3.37	310	277	-10.58	47330	45400	-4.08	511	500	-2.07
125257	3237	2800	-13.51	42939	43800	2.01	1084	989	-8.78	15727	16400	4.28	593	630	6.15
125278	5977	5700	-4.63	14293	14500	1.45	774	780	0.72	52820	52600	-0.42	1087	1190	9.52
125596	11954	11600	-2.96	16886	16400	-2.88	697	626	-10.19	30119	30600	1.60	1191	1260	5.76
125610	12701	12200	-3.94	17911	17900	-0.06	542	565	4.22	36128	36700	1.58	1126	1190	5.70
125626															
125641	11040	11200	1.44	24244	25200	3.94	620	585	-5.58	34941	36600	4.75	1117	1240	11.00
125669	15689	15400	-1.84	18032	18200	0.93	542	530	-2.24	28635	28800	0.57	1305	1410	8.06
125690	9712	9500	-2.19	21168	21500	1.57	774	718	-7.29	33383	34500	3.34	1060	1160	9.39
West Breccia Zone															
14018	24239	24500	1.08	10494	10700	1.97	387	476	22.92	29748	31600	6.22	611	660	8.03
14021	21500	22200	3.26	8865	9200	3.78	542	629	16.03	21959	23800	8.38	524	570	8.85
14036	20836	21300	2.23	9106	9100	-0.07	387	475	22.67	23220	24700	6.37	524	570	8.85
14043	9795	10300	5.15	18454	19000	2.96	387	446	15.18	30638	32900	7.38	524	570	8.85
14060	11788	12000	1.80	19781	21000	6.16	387	422	8.98	27523	30500	10.82	1135	1290	13.70
14067	10708	11200	4.59	24545	26800	9.19	697	779	11.76	30787	35100	14.01	960	1120	16.66
14076	13116	14300	9.03	22434	25000	11.44	1471	1585	7.72	19585	23000	17.44	916	1070	16.76
14083	28971	30900	6.66	17007	17700	4.08	1317	1365	3.68	12018	13600	13.16	916	1070	16.76
14099	32706	32000	-2.16	8865	8200	-7.50	1084	1090	0.53	5416	5400	-0.29	480	470	-2.09
14103	17183	18100	5.33	12303	12900	4.85	620	686	10.72	22181	25100	13.16	567	620	9.29
125046	8218	7900	-3.87	22073	20700	-6.22	1162	1100	-5.31	35535	35300	-0.66	1065	1160	8.94
125068	9380	9500	1.28	22193	22000	-0.87	852	837	-1.75	35535	37200	4.69	1135	1280	12.82
125073	16104	15300	-4.99	15982	14700	-8.02	542	479	-11.64	33532	32500	-3.08	1126	1180	4.81
125079	31793	29300	-7.84	10433	9000	-13.74	387	340	-12.20	32419	29800	-8.08	1030	1080	4.87
125084	12867	12100	-5.96	21409	19900	-7.05	1549	1425	-8.00	30861	29900	-3.11	1165	1230	5.57
125127	15938	15000	-5.89	24183	22700	-6.13	465	444	-4.45	39170	38000	-2.99	1170	1220	4.32
125129	14112	13500	-4.34	19359	18100	-6.50	387	409	5.62	34199	32500	-4.97	1012	1080	6.68
125134	16187	15300	-5.48	20746	19900	-4.08	465	475	2.22	35164	34900	-0.75	1039	1130	8.80
125142	11456	11000	-3.98	21711	20400	-6.04	852	798	-6.33	33458	32400	-3.16	964	1000	3.69
125149	13282	12100	-8.90	20263	19500	-3.77	697	639	-8.32	40283	39000	-3.18	1095	1120	2.25
125154	5396	5100	-5.48	10192	10000	-1.88	310	323	4.27	59051	57700	-2.29	1536	1620	5.46
125165	5396	5100	-5.48	15258	15600	2.24	387	403	4.07	50965	51300	0.66	1562	1680	7.54
125176	8301	7600	-8.45	17127	16900	-1.33	465	474	2.01	45921	46100	0.39	1348	1440	6.79
146112	8550	9000	5.26	13087	13000	-0.66	620	618	-0.25	39763	39400	-0.91	1100	1210	10.03
146115	5645	6200	9.84	37873	37900	0.07	1394	1290	-7.46	22626	23200	2.53	1161	1260	8.55
146124	13946	13500	-3.20	18334	17500	-4.55	697	702	0.72	31232	30600	-2.02	1366	1480	8.36
146127	16353	16300	-0.33	6151	5300	-13.84	232	228	-1.87	28190	25600	-9.19	502	480	-4.35
146135	8799	9100	3.42	12846	12500	-2.69	929	906	-2.51	40505	40500	-0.01	1348	1460	8.27
146149	9629	9500	-1.34	10916	10000	-8.39	852	831	-2.45	39763	38300	-3.68	1300	1370	5.35
146161	6724	6800	1.13	33772	32700	-3.17	2246	2140	-4.72	17211	17200	-0.06	1161	1250	7.69
146164	8052	7500	-6.86	38356	35100	-8.49	1859	1720	-7.46	25520	24500	-4.00	1383	1470	6.27
145951	15938	16800	5.41	13991	13900	-0.65	620	611	-1.38	31677	32400	2.28	1257	1420	12.99
145956	12618	11900	-5.69	22676	22200	-2.10	774	784	1.23	32345	31700	-1.99	1126	1210	7.47
145974	15025	14500	-3.49	25028	23600	-5.70	852	829	-2.69	30787	30400	-1.26	1148	1240	8.04

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock K * (ppm)	ICP K (ppm)	Difference (%) [3]	Whole Rock Mg * (ppm)	ICP Mg (ppm)	Difference (%) [3]	Whole Rock Mn * (ppm)	ICP Mn (ppm)	Difference (%) [3]	Whole Rock Na * (ppm)	ICP Na (ppm)	Difference (%) [3]	Whole Rock P * (ppm)	ICP P (ppm)	Difference (%) [3]
145982	3486	3500	0.39	32807	31400	-4.29	1162	1110	-4.45	19288	18900	-2.01	1283	1370	6.78
145992	12286	11800	-3.95	17067	16100	-5.67	774	724	-6.52	40134	37300	-7.06	1187	1240	4.47
145999	8882	8600	-3.18	17127	15900	-7.17	697	644	-7.61	36499	33800	-7.40	1139	1180	3.60
145834	6475	6500	0.39	17188	16400	-4.58	1084	1020	-5.92	44437	42400	-4.58	1165	1230	5.57
145842	1079	1100	1.93	24425	24700	1.13	2014	1880	-6.63	18398	18700	1.64	1698	1900	11.93
145852	1411	1400	-0.79	10916	10400	-4.72	1239	1190	-3.97	37315	35200	-5.67	921	970	5.35
145857	5645	5700	0.98	15982	15700	-1.76	774	808	4.33	44511	44900	0.87	1287	1440	11.86
145871	9629	9900	2.81	14836	14400	-2.94	1007	983	-2.36	33828	33800	-0.08	1082	1180	9.03
145608	10957	11400	4.04	30154	31600	4.80	697	740	6.17	27152	29500	8.65	912	1000	9.64
145614	12535	12800	2.12	25993	26600	2.34	852	816	-4.21	28858	30700	6.38	912	990	8.55
145628	3486	3300	-5.35	21771	21900	0.59	774	804	3.81	43918	46400	5.65	838	890	6.22
145640	12452	13300	6.81	24304	25300	4.10	1162	1165	0.29	27894	30000	7.55	895	990	10.67
145646	7969	8200	2.90	26475	27200	2.74	1007	1010	0.32	32048	33900	5.78	916	1010	10.21
Paramount Zone															
125965	7305	8300	13.62	18092	20600	13.86	774	870	12.34	40579	44400	9.42	785	980	24.76
125974	15025	15900	5.82	20263	20100	-0.81	465	496	6.74	29748	29100	-2.18	829	890	7.34
125983	10708	11000	2.72	33350	34000	1.95	697	741	6.31	25891	26600	2.74	829	910	9.75
125988	12867	13200	2.59	31903	32400	1.56	1162	1160	-0.15	25075	26100	4.09	1108	1260	13.68
126007	17598	19400	10.24	8443	8600	1.86	465	544	17.07	31232	32100	2.78	471	520	10.33
126031	13033	13100	0.52	8021	8200	2.23	232	265	14.06	41321	41500	0.43	511	560	9.68
126040	8550	9000	5.26	19118	19600	2.52	387	372	-3.93	42805	42500	-0.71	751	840	11.91
126054	7139	7700	7.86	40105	40800	1.73	1549	1510	-2.51	17063	17300	1.39	947	1040	9.83
126067	9629	10000	3.85	31963	31400	-1.76	1704	1640	-3.74	21514	21300	-0.99	903	960	6.28
126081	28473	28300	-0.61	9710	9200	-5.25	697	679	-2.58	9792	9900	1.10	428	420	-1.79
126110	17681	18600	5.20	27199	28500	4.78	1162	1200	3.30	26707	28300	5.97	1170	1330	13.72
126118	16436	16500	0.39	24666	24900	0.95	929	965	3.84	23294	23400	0.45	1554	1730	11.36
125904	12369	12300	-0.56	12122	12300	1.47	542	581	7.17	42805	44700	4.43	1231	1410	14.58
125919	10127	10800	6.64	17610	18200	3.35	542	524	-3.34	47627	49300	3.51	1204	1360	12.92
125928	11539	11500	-0.33	21349	21000	-1.63	1162	1130	-2.73	38428	39600	3.05	1117	1220	9.21
125933	8965	10000	11.54	28586	30100	5.30	1317	1340	1.78	33606	36600	8.91	1724	2040	18.35
125944	9131	10000	9.51	22133	23200	4.82	1394	1400	0.43	40876	43100	5.44	1017	1170	15.07
125952	17183	17500	1.84	10313	10300	-0.12	387	423	9.24	28784	29000	0.75	511	560	9.68
125963	10708	11700	9.26	19721	21200	7.50	697	774	11.05	37834	41200	8.90	1117	1320	18.16
126120	9131	10100	10.61	8142	8600	5.63	232	247	6.31	43918	44800	2.01	480	540	12.50
126131	8633	9600	11.20	11217	12300	9.65	155	231	49.14	45476	48200	5.99	759	890	17.21
126142	9048	9400	3.89	15198	15400	1.33	310	339	9.43	42731	42500	-0.54	833	920	10.38
126154	5313	5600	5.41	23038	24900	8.08	387	430	11.05	49852	53600	7.52	1266	1490	17.74
126171	15191	16300	7.30	16223	17300	6.64	387	407	5.11	29897	31900	6.70	768	900	17.18
126181	7637	8400	9.99	22796	23300	2.21	1007	984	-2.26	30935	31900	3.12	960	1080	12.50
125806	19425	18400	-5.27	11820	11700	-1.02	387	380	-1.87	36054	36100	0.13	676	700	3.49
125816	16602	16600	-0.01	22012	23000	4.49	1162	1140	-1.87	30713	32100	4.52	1327	1490	12.32
125833	19425	18600	-4.25	8202	8000	-2.46	310	317	2.33	34719	35200	1.39	484	530	9.42
125861	14029	14200	1.22	8081	8400	3.94	232	243	4.59	36425	38100	4.60	476	540	13.53
125875	20670	19000	-8.08	7659	7300	-4.69	310	282	-8.97	32938	32800	-0.42	506	540	6.68
125897	16104	16100	-0.03	8322	8100	-2.67	232	237	2.01	32271	32100	-0.53	663	730	10.06

Project:	**Schaft Creek**
Client:	Copper Fox Metals Inc.
Data:	**QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments:	2005 core samples were collected by MDAG on Feb 7'07.
	2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock K * (ppm)	ICP K (ppm)	Difference (%) ^{3}	Whole Rock Mg * (ppm)	ICP Mg (ppm)	Difference (%) ^{3}	Whole Rock Mn * (ppm)	ICP Mn (ppm)	Difference (%) ^{3}	Whole Rock Na * (ppm)	ICP Na (ppm)	Difference (%) ^{3}	Whole Rock P * (ppm)	ICP P (ppm)	Difference (%) ^{3}
Tailings															
LIARD ZONE	15440	14300	-7.38	16102	13900	-13.68	465	402	-13.49	33087	31000	-6.31	1122	1160	3.43
PARAMOUNT	14444	13700	-5.15	16102	13900	-13.68	620	547	-11.71	34199	32500	-4.97	825	830	0.64
WEST BRECCIA	14029	13500	-3.77	20203	19100	-5.46	697	691	-0.86	36351	34900	-3.99	1139	1190	4.48
High-Sulphide Histor															
T112 (171' - 172')	3819	3800	-0.48	34496	33800	-2.02	852	828	-2.81	29600	29900	1.01	999	1110	11.08
T113 (81' - 82')	18013	18300	1.59	14172	13600	-4.04	155	211	36.22	35238	34400	-2.38	589	630	6.94
T113 (983' - 985')	15855	15900	0.28	18635	18000	-3.41	620	631	1.85	24926	24600	-1.31	668	810	21.32
T140 (30' - 31')	21500	21000	-2.33	15740	14800	-5.97	232	224	-3.59	25816	25200	-2.39	1178	1330	12.88
T166 (389' - 390')	17183	17700	3.01	6996	6500	-7.09	77	121	56.24	32196	31000	-3.72	458	510	11.30
T185 (116' - 117')	23326	22900	-1.83	6996	6300	-9.94	77	60	-22.53	24259	22800	-6.01	633	690	9.05
T207 (261.5' - 262')	17598	16500	-6.24	5126	4500	-12.21	155	189	22.02	28858	26400	-8.52	554	570	2.85
T207 (269' - 271')	14776	15100	2.19	6754	6100	-9.69	232	207	-10.91	17804	17100	-3.96	445	450	1.10
All Data															
Maximum			13.7			13.9			93.7			18.4			24.8
Minimum			-13.5			-13.8			-22.5			-9.19			-6.64
Mean			0.85			0.42			5.88			3.75			9.92
Standard Deviation			5.02			5.67			13.2			6.32			4.91
10 Percentile			-5.77			-6.88			-7.46			-3.68			4.27
25 Percentile			-2.78			-3.27			-2.48			-0.72			6.79
Median			1.08			0.82			3.68			2.74			9.68
75 Percentile			4.08			4.39			11.8			7.99			13
90 Percentile			7.11			8.09			20.6			13.3			15.8
Interquartile Range (IC			6.86			7.66			14.3			8.71			6.18
Variance			25.2			32.2			175			39.9			24.1
Skewness			-0.026			-0.16			2.04			0.37			-0.24
Coefficient of Variatior			5.93			13.4			2.25			1.68			0.5
Count			235			235			235			235			235
Main Zone															
Maximum			13.7			13.5			93.7			18.4			23.4
Minimum			-13.5			-12.1			-13.5			-8.69			-6.64
Mean			0.76			1.39			7.92			5.26			10.3
Standard Deviation			4.81			5.39			13.6			6.38			4.8
10 Percentile			-5.76			-4.96			-7.29			-2.52			4.71
25 Percentile			-2.31			-2.43			-0.99			0.15			7.63
Median			0.97			1.42			6.1			4.61			10.7
75 Percentile			3.71			5.35			15.4			10.6			13.7
90 Percentile			6.44			8.66			22			14.4			15.5
Interquartile Range (IC			6.02			7.78			16.4			10.5			6.03
Variance			23.1			29.1			186			40.7			23.1
Skewness			-0.22			-0.17			2.1			0.2			-0.52
Coefficient of Variatior			6.33			3.88			1.72			1.21			0.47
Count			146			146			146			146			146

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock K * (ppm)	ICP K (ppm)	Difference (%) [3]	Whole Rock Mg * (ppm)	ICP Mg (ppm)	Difference (%) [3]	Whole Rock Mn * (ppm)	ICP Mn (ppm)	Difference (%) [3]	Whole Rock Na * (ppm)	ICP Na (ppm)	Difference (%) [3]	Whole Rock P * (ppm)	ICP P (ppm)	Difference (%) [3]
West Breccia Zone															
Maximum			9.84			11.4			22.9			17.4			16.8
Minimum			-8.9			-13.8			-12.2			-9.19			-4.35
Mean			-0.41			-1.96			0.53			1.31			7.89
Standard Deviation			4.85			5.35			8.04			6.24			4.12
10 Percentile			-5.92			-7.71			-7.52			-5.25			4.07
25 Percentile			-4.66			-5.87			-5.01			-3.1			5.52
Median			0.39			-2.1			-1.38			-0.084			8.04
75 Percentile			3.08			2.11			4.17			6			9.47
90 Percentile			5.36			4.38			11.1			9.52			12.9
Interquartile Range (IC			7.74			7.98			9.18			9.1			3.95
Variance			23.5			28.6			64.7			39			17
Skewness			0.13			0.16			1.05			0.68			-0.22
Coefficient of Variatior			-11.9			-2.73			15.3			4.77			0.52
Count			47			47			47			47			47
Paramount Zone															
Maximum			13.6			13.9			49.1			9.42			24.8
Minimum			-8.08			-5.25			-8.97			-2.18			-1.79
Mean			4.11			2.43			4.82			3.03			11.9
Standard Deviation			5.33			4.18			10.3			3.2			4.98
10 Percentile			-0.61			-2.46			-3.34			-0.54			6.68
25 Percentile			0.19			-0.46			-2.07			0.44			9.68
Median			3.89			1.95			3.3			2.78			11.9
75 Percentile			8.56			4.8			8.2			5.02			14.2
90 Percentile			10.6			7.5			12.3			7.52			17.7
Interquartile Range (IC			8.37			5.27			10.3			4.58			4.47
Variance			28.4			17.5			106			10.2			24.8
Skewness			-0.25			0.51			2.75			0.44			-0.11
Coefficient of Variatior			1.3			1.72			2.13			1.05			0.42
Count			31			31			31			31			31

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock K * (ppm)	ICP K (ppm)	Difference (%) [3]	Whole Rock Mg * (ppm)	ICP Mg (ppm)	Difference (%) [3]	Whole Rock Mn * (ppm)	ICP Mn (ppm)	Difference (%) [3]	Whole Rock Na * (ppm)	ICP Na (ppm)	Difference (%) [3]	Whole Rock P * (ppm)	ICP P (ppm)	Difference (%) [3]
Tailings															
Maximum			-3.77			-5.46			-0.86			-3.99			4.48
Minimum			-7.38			-13.7			-13.5			-6.31			0.64
Mean			-5.43			-10.9			-8.69			-5.09			2.85
Standard Deviation			1.82			4.74			6.83			1.16			1.99
10 Percentile			-6.94			-13.7			-13.1			-6.04			1.19
25 Percentile			-6.27			-13.7			-12.6			-5.64			2.03
Median			-5.15			-13.7			-11.7			-4.97			3.43
75 Percentile			-4.46			-9.57			-6.29			-4.48			3.96
90 Percentile			-4.05			-7.1			-3.03			-4.19			4.27
Interquartile Range (IC			1.81			4.11			6.31			1.16			1.92
Variance			3.33			22.5			46.7			1.35			3.95
Skewness			-0.68			1.73			1.6			-0.46			-1.21
Coefficient of Variatior			-0.34			-0.43			-0.79			-0.23			0.7
Count			3			3			3			3			3
High-Sulphide Histor															
Maximum			3.01			-2.02			56.2			1.01			21.3
Minimum			-6.24			-12.2			-22.5			-8.52			1.1
Mean			-0.48			-6.8			9.56			-3.41			9.56
Standard Deviation			2.99			3.59			26.4			2.91			6.31
10 Percentile			-3.5			-10.6			-14.4			-6.76			2.32
25 Percentile			-1.95			-9.75			-5.42			-4.47			5.92
Median			-0.1			-6.53			-0.48			-3.05			10.1
75 Percentile			1.74			-3.88			25.6			-2.11			11.7
90 Percentile			2.44			-2.99			42.2			-0.61			15.4
Interquartile Range (IC			3.69			5.87			31			2.36			5.78
Variance			8.94			12.9			697			8.48			39.8
Skewness			-0.93			-0.18			0.79			-0.41			0.56
Coefficient of Variatior			-6.29			-0.53			2.76			-0.85			0.66
Count			8			8			8			8			8

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile
[2] Coefficient of Variation (CoV) = standard deviation divided by mean
[3] Difference (%) = (ICP - Whole Rock) * 100 / Whole Rock
* Element calculated from Whole Rock XRF analysis
K (Whole Rock) = (K_2O*2*10000*39.09)/(39.09*2+16)
Mg (Whole Rock) = (MgO*10000*24.31)/(24.31+16)
Mn (Whole Rock) = (MnO*10000*54.94)/(54.94+16)
Na (Whole Rock) = (Na_2O*2*10000*22.99)/(22.99*2+16)
P (Whole Rock) = (P_2O5*2*10000*30.97)/(2*30.97+5*16)

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock Si * (ppm)	ICP Si (ppm)	Difference (%)[3]	Whole Rock Sr * (ppm)	ICP Sr (ppm)	Difference (%)[3]	Leco S (Total)** (ppm)	ICP S (ppm)	Difference (%)[3]	Whole Rock Ti * (ppm)	ICP Ti (ppm)	Difference (%)[3]
Main Zone												
14130	281180			254	288	13.53	2900	3200	10.34	3177	2800	-11.88
14144	251496			338	343	1.41	2600	2800	7.69	3777	3760	-0.45
14148	243082			254	223	-12.09	1400	1400	0.00	3837	3780	-1.48
14156	303666			254	259	2.10	1700	1700	0.00	1739	1900	9.29
14162	234714			169	239	41.32	1300	1500	15.38	4137	4270	3.23
14169	312781			169	207	22.40	3000	3200	6.67	1858	1960	5.46
14232	264352			338	345	2.00	1500	1600	6.67	3657	3290	-10.03
14250	242661			338	424	25.36	1900	2000	5.26	4496	4350	-3.25
14260	255330			338	402	18.85	3400	3700	8.82	4316	4050	-6.17
14276	252759			676	798	17.97	1700	1700	0.00	4017	4100	2.08
14295	250234			254	336	32.45	4400	4900	11.36	4376	4240	-3.12
14301	256452			169	209	23.58	3400	3500	2.94	4196	3620	-13.74
14323	255470			338	391	15.60	1500	1500	0.00	3357	3310	-1.41
14332	253179			338	355	4.96	2600	2700	3.85	3597	3260	-9.37
14345	268793			254	274	8.01	5200	5600	7.69	3477	2970	-14.58
14348	256966			254	276	8.80	4400	4800	9.09	3657	3190	-12.77
14797	241867			254	234	-7.76	800	700	-12.50	4196	4150	-1.11
14808	245980			169	221	30.68	1800	1900	5.56	3357	3260	-2.90
14816	249346			254	285	12.35	4600	4700	2.17	3897	3810	-2.23
14828	242474			338	404	19.44	1300	1400	7.69	3777	3940	4.32
14844	246775			254	265	4.46	2100	2200	4.76	5575	5590	0.26
14680	249346			338	348	2.89	2200	2200	0.00	4017	4040	0.58
14871	250234			338	405	19.74	3700	3800	2.70	4916	4990	1.51
14887	236351			338	424	25.36	4400	5400	22.73	4736	4960	4.73
14689	309696			169	141	-16.63	6800	7900	16.18	1978	1580	-20.14
14695	249533			169	226	33.63	1400	1600	14.29	4077	4310	5.73
14742	256498			254	302	19.05	1900	2100	10.53	5156	4690	-9.03
14666	248738			338	416	22.99	3200	3800	18.75	5036	5070	0.68
14685	233125			338	393	16.19	17900	21000	17.32	8273	7690	-7.05
14685B	235603			338	374	10.57	19500	20400	4.62	8273	7930	-4.15
14545	262996			338	409	20.92	1900	1900	0.00	3897	3980	2.14
14565	251730			254	259	2.10	2300	2600	13.04	3777	3800	0.61
14571	280246			338	312	-7.76	10400	11100	6.73	3537	3170	-10.38
14578	252478			254	324	27.72	18200	21300	17.03	5156	4630	-10.20
14578B	254628			254	330	30.09	19300	21100	9.33	4916	4430	-9.88
14598	247476			507	569	12.15	1300	1500	15.38	4436	4330	-2.40
14893	235696			338	379	12.05	1100	1100	0.00	5995	6030	0.58
14899	228824			338	366	8.21	200	200	0.00	5815	5850	0.60
14908	247383			423	479	13.29	800	900	12.50	5815	5910	1.63
14917	278656			254	309	21.81	1900	1900	0.00	4796	4580	-4.50
14925	253647			338	353	4.37	1400	1500	7.14	5276	5090	-3.52
14998	251309			338	412	21.81	1300	1300	0.00	4316	4460	3.33
15862	247149			254	327	28.90	800	800	0.00	4077	4050	-0.65
15870	254348			254	234	-7.76	1300	1400	7.69	4436	4460	0.53
15879	237098			338	373	10.28	1200	1200	0.00	5395	5450	1.01

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock Si * (ppm)	ICP Si (ppm)	Difference (%) [3]	Whole Rock Sr * (ppm)	ICP Sr (ppm)	Difference (%) [3]	Leco S (Total)** (ppm)	ICP S (ppm)	Difference (%) [3]	Whole Rock Ti * (ppm)	ICP Ti (ppm)	Difference (%) [3]
15887	254441			338	402	18.85	3100	3300	6.45	5156	5100	-1.08
15891	240184			338	382	12.94	1400	1400	0.00	5156	4920	-4.57
15908	250001			254	288	13.53	2200	2200	0.00	4856	4740	-2.39
15911	246822			338	335	-0.96	900	900	0.00	5455	5430	-0.47
125285	283144			254	276	8.80	3200	3200	0.00	4077	3860	-5.31
125288	207788			338	368	8.80	1000	1000	0.00	6235	5620	-9.86
125293	270522			254	220	-13.28	2100	2100	0.00	4736	4330	-8.57
125305	266502			254	312	22.99	1200	1500	25.00	3957	3700	-6.49
125311	285154			338	328	-3.03	600	700	16.67	3837	3510	-8.52
125703	244531			169	168	-0.66	1000	1000	0.00	4256	3960	-6.96
125728	247056			338	353	4.37	1900	2000	5.26	5815	5100	-12.30
125755	314464			254	228	-10.12	5900	5700	-3.39	1978	1320	-33.28
125772	248738			338	311	-8.05	2100	2200	4.76	5276	4680	-11.29
125795	236210			254	269	6.04	1100	1100	0.00	4976	4560	-8.36
125422	245653			338	333	-1.55	2100	2400	14.29	4077	3930	-3.60
125435	248645			254	245	-3.42	1600	1600	0.00	4496	4080	-9.26
125452	244157			338	341	0.82	4700	5500	17.02	4556	4100	-10.01
125476	308013			254	248	-2.24	7800	8500	8.97	2038	1420	-30.33
125490	247803			254	250	-1.45	3500	4300	22.86	4676	4210	-9.97
126192	263978			338	336	-0.66	1900	2100	10.53	4017	3920	-2.41
126206	259443			338	419	23.88	2200	2500	13.64	4736	4410	-6.88
126225	260191			423	439	3.83	3500	3500	0.00	4556	4150	-8.92
126244	249346			254	315	24.17	2600	2800	7.69	4137	4130	-0.16
126266	250047			254	284	11.95	1900	2200	15.79	4436	4370	-1.49
126279	251076			338	417	23.29	3900	4300	10.26	4017	3890	-3.15
126288	254909			254	270	6.43	3700	4000	8.11	3957	3830	-3.20
126297	240791			169	223	31.86	5100	5700	11.76	7314	6580	-10.03
126314	246495			254	263	3.68	13700	14600	6.57	4496	4470	-0.58
126329	260051			169	200	18.26	2400	2500	4.17	3477	3510	0.95
126337	246448			254	320	26.14	5700	5900	3.51	6115	5630	-7.93
126351	255002			338	369	9.10	1400	1500	7.14	4496	4250	-5.48
126427	226113			254	289	13.92	11200	12900	15.18	5455	5430	-0.47
126430	243456			169	183	8.21	2100	2500	19.05	4017	4220	5.06
126434	244578			254	297	17.08	1100	1300	18.18	4077	3980	-2.37
126443	241446			169	218	28.90	17000	18200	7.06	4676	4420	-5.48
126449	234340			423	511	20.86	200	100	-50.00	5815	5830	0.26
126464	250141			338	369	9.10	4300	4800	11.63	4017	3980	-0.91
126492	246448			254	295	16.29	2200	2300	4.55	4256	4020	-5.56
145655	250608			338	320	-5.39	6600	6700	1.52	4017	4000	-0.41
145669	238220			254	285	12.35	9500	10000	5.26	4376	4110	-6.09
145685	247757			254	263	3.68	2300	2300	0.00	4376	4220	-3.57
145694	234107			338	359	6.14	1700	1800	5.88	5216	4580	-12.19
145708	246401			254	316	24.57	2600	2700	3.85	3297	3190	-3.25
145723	253460			254	284	11.95	16300	16700	2.45	4077	3710	-8.99
146798	241352			254	307	21.02	2100	2100	0.00	4017	3950	-1.66
146824	239342			338	355	4.96	1700	1700	0.00	5875	5880	0.08

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock Si * (ppm)	ICP Si (ppm)	Difference (%) ^{3}	Whole Rock Sr * (ppm)	ICP Sr (ppm)	Difference (%) ^{3}	Leco S (Total)** (ppm)	ICP S (ppm)	Difference (%) ^{3}	Whole Rock Ti * (ppm)	ICP Ti (ppm)	Difference (%) ^{3}
146831	243269			254	307	21.02	3600	3600	0.00	5156	5190	0.67
146843												
146861	262949			338	388	14.71	1300	1200	-7.69	3957	4140	4.63
146868	258555			338	305	-9.83	5100	5200	1.96	4017	3870	-3.65
126352	248177			338	390	15.30	6000	7000	16.67	5575	5540	-0.63
126358	249907			338	335	-0.96	3300	3700	12.12	5395	5420	0.45
126374	247710			338	386	14.12	1700	1900	11.76	5515	5440	-1.37
126384	259864			423	434	2.65	1100	1200	9.09	4436	4250	-4.20
126391	243035			423	457	8.09	1800	1900	5.56	4616	4300	-6.85
146172	245373			254	268	5.65	2400	2400	0.00	4436	3940	-11.19
146182	249486			423	446	5.49	1500	1400	-6.67	4916	4430	-9.88
146203	271364			254	294	15.90	1800	1800	0.00	4376	3620	-17.28
146214	250608			338	378	11.76	3600	3700	2.78	4017	3540	-11.87
146221	232704			338	420	24.17	8100	7400	-8.64	8393	7100	-15.41
146238	239763			423	490	15.90	1300	1500	15.38	5635	5460	-3.11
147034	256685			254	251	-1.06	5200	5200	0.00	3537	3200	-9.53
147038	288146			254	261	2.89	3500	3400	-2.86	3057	2650	-13.33
147051	259116			423	390	-7.76	3300	3200	-3.03	4616	4220	-8.58
147070	243783			423	546	29.14	5100	6000	17.65	4496	4770	6.09
147087	242100			338	411	21.51	33500	33800	0.90	4376	4200	-4.03
147097	234060			254	258	1.70	6800	7200	5.88	4496	4400	-2.14
145508	235556			254	326	28.51	400	400	0.00	5875	5700	-2.98
145527	255423			338	382	12.94	4800	5500	14.58	5156	5190	0.67
145543	261781			338	396	17.08	1200	1300	8.33	5455	4950	-9.26
145562	247757			338	325	-3.91	900	1000	11.11	5395	5190	-3.81
145576	313856			254	214	-15.64	6900	7400	7.25	1858	1340	-27.90
145601	244251			423	472	11.64	5000	5800	16.00	4976	5170	3.90
146297	250234			254	294	15.90	3500	3100	-11.43	4796	4200	-12.43
146314	247757			338	377	11.46	1500	1500	0.00	4676	4370	-6.55
146335	240090			338	361	6.73	1300	1300	0.00	4436	4180	-5.78
146352	268512			338	366	8.21	600	600	0.00	4137	3590	-13.21
146368	246588			338	335	-0.96	1900	1900	0.00	4496	4160	-7.48
146390	248131			423	476	12.58	1600	1500	-6.25	4676	4660	-0.34
146508	243643			254	286	12.74	600	500	-16.67	5695	5510	-3.25
146526	259023			507	512	0.92	6800	7400	8.82	4077	3780	-7.28
146544	282022			338	338	-0.07	2400	2500	4.17	2878	2810	-2.35
146565	262061			338	295	-12.78	1100	1100	0.00	3777	3290	-12.89
146589	252618			338	331	-2.14	1300	1200	-7.69	5276	5080	-3.71
146613	249346			338	394	16.49	5400	5900	9.26	4796	4860	1.33
146627	283050			169	201	18.85	900	700	-22.22	3357	3210	-4.38
146637	285995			169	204	20.63	4600	4900	6.52	2338	2260	-3.34
146649	299271			338	336	-0.66	2800	2800	0.00	2098	2130	1.51
146657	310117			254	211	-16.82	1900	2100	10.53	2098	2140	1.99
146676	256498			338	348	2.89	2100	2100	0.00	4316	4250	-1.54
125188	259584			338	346	2.30	2600	2700	3.85	3477	3080	-11.42
125198	259724			254	310	22.20	2200	2300	4.55	3837	3520	-8.26

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock Si * (ppm)	ICP Si (ppm)	Difference (%) [3]	Whole Rock Sr * (ppm)	ICP Sr (ppm)	Difference (%) [3]	Leco S (Total)** (ppm)	ICP S (ppm)	Difference (%) [3]	Whole Rock Ti * (ppm)	ICP Ti (ppm)	Difference (%) [3]
125207	262622			254	252	-0.66	1100	1200	9.09	3477	3190	-8.26
125228	303946			338	296	-12.49	1500	1600	6.67	1978	1980	0.08
125244	310304			338	335	-0.96	1500	1500	0.00	2038	1980	-2.86
125257	220971			254	321	26.54	600	900	50.00	5276	4900	-7.12
125278	262201			507	504	-0.66	200	300	50.00	4856	4680	-3.62
125596	237519			338	386	14.12	1200	1400	16.67	4496	4260	-5.25
125610	262388			254	217	-14.46	600	600	0.00	4256	3690	-13.31
125626												
125641	243222			254	250	-1.45	1000	1200	20.00	5575	5280	-5.30
125669	264772			169	193	13.83	10100	11100	9.90	4916	3930	-20.06
125690	250281			338	358	5.84	1000	1000	0.00	4976	4630	-6.95
West Breccia Zone												
14018	294129			423	428	1.23	8000	8800	10.00	2518	2400	-4.68
14021	303993			169	173	2.30	6200	7000	12.90	2158	2080	-3.62
14036	303338			254	235	-7.36	14700	16000	8.84	2278	1970	-13.52
14043	302637			254	276	8.80	2600	2800	7.69	2458	2190	-10.90
14060	271971			423	423	0.05	13100	14800	12.98	4376	4100	-6.31
14067	269681			338	410	21.22	4000	4300	7.50	4196	4170	-0.63
14076	259724			338	365	7.91	7700	9500	23.38	4316	4540	5.18
14083	249346			169	232	37.18	14600	16000	9.59	4436	4480	0.99
14099	297822			85	88	4.07	3400	3600	5.88	1858	1670	-10.14
14103	287725			169	198	16.78	6900	7700	11.59	2458	2220	-9.68
125046	257854			423	482	14.00	1100	1400	27.27	4976	4830	-2.93
125068	252572			507	558	9.98	3900	4500	15.38	5276	5270	-0.11
125073	271878			423	386	-8.70	6000	5900	-1.67	3837	3640	-5.13
125079	290857			254	270	6.43	12900	13200	2.33	3657	2940	-19.61
125084	258462			592	601	1.54	6100	6100	0.00	5395	5010	-7.14
125127	257153			338	382	12.94	800	900	12.50	5515	5080	-7.89
125129	289922			254	221	-12.88	2500	2500	0.00	4676	4340	-7.19
125134	271223			254	281	10.77	5900	6100	3.39	4736	4360	-7.94
125142	278282			254	272	7.22	2600	2600	0.00	4376	4110	-6.09
125149	247990			254	301	18.65	1300	1400	7.69	5096	4290	-15.81
125154	278048			254	252	-0.66	800	800	0.00	3777	3190	-15.54
125165	265006			676	676	-0.07	1900	2000	5.26	4796	4360	-9.09
125176	261827			423	399	-5.63	2400	2400	0.00	3897	3530	-9.41
146112	271130			507	541	6.63	1200	1200	0.00	4436	4060	-8.48
146115	219709			423	513	21.34	1300	1400	7.69	8933	8300	-7.08
146124	243456			507	484	-4.60	900	900	0.00	4316	3970	-8.03
146127	308574			169	162	-4.21	10600	10600	0.00	2158	1620	-24.94
146135	257246			592	678	14.54	400	500	25.00	4256	4010	-5.79
146149	255937			592	565	-4.55	700	700	0.00	4137	3810	-7.89
146161	229245			592	656	10.83	400	400	0.00	5875	5250	-10.64
146164	231208			423	440	4.07	200	200	0.00	6295	5940	-5.64
145951	251917			254	253	-0.27	1800	1700	-5.56	4616	4600	-0.35
145956	244438			254	286	12.74	1900	1800	-5.26	5216	4660	-10.65
145974	243596			254	240	-5.39	200	100	-50.00	4676	4220	-9.75

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock Si * (ppm)	ICP Si (ppm)	Difference (%)[3]	Whole Rock Sr * (ppm)	ICP Sr (ppm)	Difference (%)[3]	Leco S (Total)** (ppm)	ICP S (ppm)	Difference (%)[3]	Whole Rock Ti * (ppm)	ICP Ti (ppm)	Difference (%)[3]
145982	219709			423	450	6.43	500	500	0.00	7494	6560	-12.46
145992	257667			254	224	-11.70	2800	2800	0.00	4616	4170	-9.66
145999	251590			423	379	-10.36	1400	1300	-7.14	4676	4130	-11.68
145834	259256			676	662	-2.14	400	300	-25.00	4556	4050	-11.11
145842	248598			1099	1260	14.62	300	300	0.00	7674	6610	-13.86
145852	285481			930	941	1.17	1100	1100	0.00	4017	3690	-8.13
145857	264445			846	904	6.91	100	100	0.00	4736	4450	-6.04
145871	257340			592	578	-2.35	1600	1700	6.25	4017	3650	-9.13
145608	249393			423	462	9.27	7900	9300	17.72	4436	4540	2.34
145614	255049			423	447	5.73	5600	6300	12.50	4436	4410	-0.59
145628	252431			254	230	-9.33	7900	8700	10.13	4137	3860	-6.69
145640	248177			338	375	10.87	7500	8000	6.67	4376	4550	3.97
145646	254254			423	437	3.36	5700	6100	7.02	4496	4460	-0.81
Paramount Zone												
125965	281648			254	286	12.74	3500	3900	11.43	3837	3520	-8.26
125974	271457			169	154	-8.94	15600	17700	13.46	3717	3370	-9.33
125983	262622			254	308	21.41	3000	3000	0.00	2997	2870	-4.25
125988	235135			507	597	17.67	300	400	33.33	5755	5410	-6.00
126007	311986			254	250	-1.45	1500	1600	6.67	1858	1680	-9.60
126031	312407			338	326	-3.62	1300	1500	15.38	2158	1890	-12.43
126040	283752			254	254	0.13	6600	7200	9.09	3297	2980	-9.62
126054	247289			169	227	34.23	1800	1800	0.00	3597	3400	-5.48
126067	252385			254	312	22.99	3100	3100	0.00	3477	3340	-3.94
126081	318671			169	194	14.71	10900	10700	-1.83	1858	1600	-13.91
126110	229572			507	663	30.68	600	700	16.67	5815	5620	-3.36
126118	245793			169	193	13.83	7800	7800	0.00	6594	5690	-13.72
125904	251216			338	340	0.52	1800	1900	5.56	3957	3600	-9.01
125919	254021			423	502	18.73	5100	5200	1.96	4376	3980	-9.06
125928	250234			423	490	15.90	900	1000	11.11	5395	4850	-10.11
125933	221953			338	408	20.63	200	200	0.00	7494	7390	-1.38
125944	249066			507	582	14.71	1200	1400	16.67	5216	5020	-3.75
125952	290623			169	211	24.77	10500	11700	11.43	2038	2020	-0.90
125963	243035			254	333	31.27	4300	4600	6.98	4436	4450	0.31
126120	314978			423	394	-6.81	600	700	16.67	1918	1860	-3.04
126131	306704			338	350	3.48	300	300	0.00	2997	2760	-7.92
126142	292727			338	312	-7.76	500	600	20.00	3597	3400	-5.48
126154	268793			338	310	-8.35	1300	1400	7.69	5036	4580	-9.05
126171	274122			338	373	10.28	12800	14900	16.41	3597	3250	-9.65
126181	248131			423	469	10.93	2500	2800	12.00	4856	4780	-1.56
125806	292166			423	421	-0.42	4800	5200	8.33	2938	2580	-12.17
125816	241913			507	612	20.63	300	200	-33.33	6654	6350	-4.58
125833	310023			338	292	-13.67	2700	3100	14.81	2098	1770	-15.64
125861	311659			254	293	15.50	3400	3700	8.82	2218	1650	-25.61
125875	310397			338	297	-12.19	2400	2400	0.00	2398	1940	-19.10
125897	318344			169	187	10.28	800	800	0.00	2158	1800	-16.60

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock Si * (ppm)	ICP Si (ppm)	Difference (%) [3]	Whole Rock Sr * (ppm)	ICP Sr (ppm)	Difference (%) [3]	Leco S (Total)** (ppm)	ICP S (ppm)	Difference (%) [3]	Whole Rock Ti * (ppm)	ICP Ti (ppm)	Difference (%) [3]
Tailings												
LIARD ZONE	258041			254	280	10.38	800	900	12.50	4616	3640	-21.15
PARAMOUNT	280526			254	275	8.41	1700	1800	5.88	3597	2950	-17.99
WEST BRECCIA	267110			423	432	2.18	2000	2500	25.00	4616	4180	-9.45
High-Sulphide Histor												
T112 (171' - 172')	204189			254	361	42.31	90600	92700	2.32	6175	5750	-6.88
T113 (81' - 82')	306564			338	375	10.87	8700	9800	12.64	2758	1950	-29.29
T113 (983' - 985')	280760			169	174	2.89	21100	22600	7.11	3357	2330	-30.60
T140 (30' - 31')	264165			254	249	-1.84	1300	1500	15.38	4916	4410	-10.29
T166 (389' - 390')	313903			338	318	-5.98	8100	8900	9.88	1798	1680	-6.59
T185 (116' - 117')	310117			169	166	-2.14	22600	23700	4.87	2758	1470	-46.69
T207 (261.5' - 262')	305909			85	95	11.99	38800	39100	0.77	2278	1500	-34.16
T207 (269' - 271')	238875			85	66	-22.42	135000	100000	-25.93	1858	1550	-16.60
All Data												
Maximum			NA			42.3			50			9.29
Minimum			NA			-22.4			-50			-46.7
Mean			NA			8.57			5.61			-6.69
Standard Deviation			NA			12.2			10.9			7.56
10 Percentile			NA			-7.76			0			-13.9
25 Percentile			NA			-0.66			0			-9.88
Median			NA			8.8			5.56			-6.04
75 Percentile			NA			16.6			11.4			-1.44
90 Percentile			NA			24.1			16.7			0.84
Interquartile Range (IC			NA			17.3			11.4			8.44
Variance			NA			149			118			57.1
Skewness			NA			0.12			-0.81			-1.5
Coefficient of Variatior			NA			1.42			1.94			-1.13
Count			0			235			235			235
Main Zone												
Maximum			NA			41.3			50			9.29
Minimum			NA			-16.8			-50			-33.3
Mean			NA			9.83			5.72			-4.99
Standard Deviation			NA			12.1			10.4			6.62
10 Percentile			NA			-6.57			0			-12.4
25 Percentile			NA			1.04			0			-8.97
Median			NA			10.4			5.26			-3.64
75 Percentile			NA			18.9			10.5			-0.45
90 Percentile			NA			25			16.7			1.57
Interquartile Range (IC			NA			17.8			10.5			8.52
Variance			NA			146			107			43.9
Skewness			NA			-0.059			-0.1			-1.24
Coefficient of Variatior			NA			1.23			1.81			-1.33
Count			0			146			146			146

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock Si * (ppm)	ICP Si (ppm)	Difference (%) ^{3}	Whole Rock Sr * (ppm)	ICP Sr (ppm)	Difference (%) ^{3}	Leco S (Total)** (ppm)	ICP S (ppm)	Difference (%) ^{3}	Whole Rock Ti * (ppm)	ICP Ti (ppm)	Difference (%) ^{3}
West Breccia Zone												
Maximum			NA			37.2			27.3			5.18
Minimum			NA			-12.9			-50			-24.9
Mean			NA			4.67			3.88			-7.45
Standard Deviation			NA			9.99			12			5.8
10 Percentile			NA			-7.9			-3.11			-13.7
25 Percentile			NA			-2.24			0			-10.4
Median			NA			4.07			3.39			-7.89
75 Percentile			NA			10.8			9.79			-4.91
90 Percentile			NA			15.5			13.9			-0.25
Interquartile Range (IC			NA			13			9.79			5.48
Variance			NA			99.9			143			33.7
Skewness			NA			0.62			-1.94			-0.26
Coefficient of Variatior			NA			2.14			3.08			-0.78
Count			0			47			47			47
Paramount Zone												
Maximum			NA			34.2			33.3			0.31
Minimum			NA			-13.7			-33.3			-25.6
Mean			NA			9.77			7.4			-8.52
Standard Deviation			NA			13.5			11			5.79
10 Percentile			NA			-8.35			0			-15.6
25 Percentile			NA			-0.94			0			-11.1
Median			NA			12.7			8.33			-9.01
75 Percentile			NA			19.7			14.1			-4.1
90 Percentile			NA			24.8			16.7			-1.56
Interquartile Range (IC			NA			20.6			14.1			7.04
Variance			NA			183			121			33.6
Skewness			NA			-0.1			-1.29			-0.9
Coefficient of Variatior			NA			1.38			1.48			-0.68
Count			0			31			31			31

Project: **Schaft Creek**
Client: Copper Fox Metals Inc.
Data: **QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses**
Comments: 2005 core samples were collected by MDAG on Feb 7'07.
2006 core samples were collected by Copper Fox personnel in Sep '07.

Sample Id.	Whole Rock Si * (ppm)	ICP Si (ppm)	Difference (%)[3]	Whole Rock Sr * (ppm)	ICP Sr (ppm)	Difference (%)[3]	Leco S (Total)** (ppm)	ICP S (ppm)	Difference (%)[3]	Whole Rock Ti * (ppm)	ICP Ti (ppm)	Difference (%)[3]
Tailings												
Maximum			NA			10.4			25			-9.45
Minimum			NA			2.18			5.88			-21.1
Mean			NA			6.99			14.5			-16.2
Standard Deviation			NA			4.28			9.71			6.05
10 Percentile			NA			3.42			7.21			-20.5
25 Percentile			NA			5.29			9.19			-19.6
Median			NA			8.41			12.5			-18
75 Percentile			NA			9.39			18.8			-13.7
90 Percentile			NA			9.98			22.5			-11.2
Interquartile Range (IC			NA			4.1			9.56			5.85
Variance			NA			18.3			94.3			36.6
Skewness			NA			-1.33			0.87			1.22
Coefficient of Variatior			NA			0.61			0.67			-0.37
Count			0			3			3			3
High-Sulphide Histor												
Maximum			NA			42.3			15.4			-6.59
Minimum			NA			-22.4			-25.9			-46.7
Mean			NA			4.46			3.38			-22.6
Standard Deviation			NA			18.7			12.8			14.7
10 Percentile			NA			-10.9			-7.24			-37.9
25 Percentile			NA			-3.1			1.93			-31.5
Median			NA			0.52			5.99			-22.9
75 Percentile			NA			11.2			10.6			-9.44
90 Percentile			NA			21.1			13.5			-6.79
Interquartile Range (IC			NA			14.3			8.64			22
Variance			NA			350			165			216
Skewness			NA			0.98			-2.01			-0.37
Coefficient of Variatior			NA			4.19			3.8			-0.65
Count			0			8			8			8

[1] Interquartile Range (IQR) = 75th percentile minus 25th percentile
[2] Coefficient of Variation (CoV) = standard deviation divided by mean
[3] Difference (%) = (ICP - Whole Rock) * 100 / Whole Rock
* Element calculated from Whole Rock XRF analysis

Si (Whole Rock) = (SiO_2*10000*28.09)/(28.09+2*16)
Sr (Whole Rock) = (SrO*10000*87.62)/(87.62+16)
Ti (Whole Rock) = (TiO_2*10000*47.9)/(47.9+2*16)

**S (Total) = S (Leco %) * 10000

APPENDIX B. Compiled Chemical Analyses of Tailings Supernatants from Metallurgical Testing of the Main (Liard), West Breccia, and Paramount Ore

Project 830-7 SCHAFT CREEK
Report To JONATHAN OLSEN, RESCAN ENVIRONMENTAL SERVICES

RESULTS OF ANALYSIS

Sample ID	Units	Detection Limits	LIARD ZONE REP 1	LIARD ZONE REP 2	LIARD ZONE REP 3	PARAMOUNT REP 1	PARAMOUNT REP 2	PARAMOUNT REP 3	WEST BRECCIA REP 1	WEST BRECCIA REP 2	WEST BRECCIA REP 3	FIELD BLANK	TRAVEL BLANK
Date Sampled			27-AUG-07	27-AUG-07	27-AUG-07	28-AUG-07	28-AUG-07	28-AUG-07	05-SEP-07	05-SEP-07	05-SEP-07	05-SEP-07	05-SEP-07
Time Sampled			12:00	12:00	12:00	10:30	11:30	12:15	10:00	11:00	11:45	11:15	00:00
ALS Sample ID			L547761-1	L547761-2	L547761-3	L547756-1	L547756-2	L547756-3	L550220-1	L550220-2	L550220-3	L550220-4	L550220-5
Matrix			Water	Water	Water	Water	Water	Water	Water	Water	Water	Water	Water
ALS File No.			L547761	L547761	L547761	L547756	L547756	L547756	L550220	L550220	L550220	L550220	L550220
Date Received			29-Aug-07	29-Aug-07	29-Aug-07	29-Aug-07	29-Aug-07	29-Aug-07	05-Sep-07	05-Sep-07	05-Sep-07	05-Sep-07	05-Sep-07
Date Finalized			03-Oct-07	03-Oct-07	03-Oct-07	22-Sep-07	22-Sep-07	22-Sep-07	02-Oct-07	02-Oct-07	02-Oct-07	02-Oct-07	02-Oct-07
Physical Tests													
Hardness (as CaCO3)	mg/L	0.5	65.5	67.6	68.9	828	959	1050	366	347	339	<0.50	<0.50
Colour, True	CU	5	5.9	6.6	6.5	<5.0	<5.0	<5.0	5.2	5.8	6.2	<5.0	<5.0
Conductivity	uS/cm	2	523	511	508	1630	1790	1830	897	867	854	<2.0	<2.0
pH	pH	0.01	8.35	8.37	8.44	7.78	7.91	7.93	6.83	7.50	7.61	5.57	5.57
Total Dissolved Solids	mg/L	10	334	334	333	1360	1500	1620	653	627	622	<10	<10
Total Suspended Solids	mg/L	3	88.0	89.5	92.0	32.0	41.0	201	114	62.9	35.4	<3	<3.0
Turbidity	NTU	0.1	133	120	139	26.1	21.9	137	25.8	28.7	20.0	<0.10	<0.10
Anions and Nutrients													
Ammonia as N	mg/L	0.005	0.0209	0.0260	0.0217	0.0589	0.0613	0.0702	0.0145	0.0066	0.0065	<0.0050	<0.0050
Acidity (as CaCO3)	mg/L	1	<1.0	<1.0	<1.0	6.9	6.1	6.0	4.3	2.6	2.2	1.7	1.5
Alkalinity, Bicarbonate (as CaCO3)	mg/L	1	36.8	36.9	33.6	18.6	16.7	16.8	20.7	19.8	19.3	<2.0	<2.0
Alkalinity, Carbonate (as CaCO3)	mg/L	1	<1.0	<1.0	<1.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0
Alkalinity, Hydroxide (as CaCO3)	mg/L	1	<1.0	<1.0	<1.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0
Alkalinity, Total (as CaCO3)	mg/L	1	36.8	36.9	33.6	18.6	16.7	16.8	20.7	19.8	19.3	<2.0	<2.0
Bromide (Br)	mg/L	0.05	<0.050	<0.050	<0.050	<0.050	<0.050	<0.050	<0.050	<0.050	<0.050	<0.050	<0.050
Chloride (Cl)	mg/L	0.5	6.62	6.59	6.63	9.97	10.6	10.6	7.04	6.86	6.83	<0.50	<0.50
Fluoride (F)	mg/L	0.02	0.734	0.749	0.746	0.419	0.460	0.458	0.644	0.623	0.621	<0.020	<0.020
Sulfate (SO4)	mg/L	0.5	191	185	184	856	980	1010	397	376	373	<0.50	<0.50
Nitrate (as N)	mg/L	0.005	0.0242	0.0250	0.0337	0.0292	0.0272	0.0264	0.0066	0.0159	0.0164	<0.0050	<0.0050
Nitrite (as N)	mg/L	0.001	0.0058	0.0042	0.0049	0.0033	0.0025	0.0030	0.0038	0.0045	0.0042	<0.0010	<0.0010
Total Kjeldahl Nitrogen	mg/L	0.05	2.67	2.75	2.78	2.69	2.73	2.75	1.25	1.02	0.829	<0.050	<0.050
Total Nitrogen	mg/L	0.05	2.70	2.78	2.82	2.72	2.76	2.78	1.26	1.04	0.85	<0.05	<0.05
Total Phosphate as P	mg/L	0.002	0.0208	0.0304	0.0344	0.0190	0.0347	0.144	0.0656	0.0503	0.0306	<0.0020	<0.0020
Cyanides													
Cyanide, Total	mg/L	0.001	0.0028	0.0028	0.0027	0.0020	0.0025	0.0026	0.0024	0.0021	0.0020	<0.0010	<0.0010
Total Metals													
Aluminum (Al)-Total	mg/L	0.001	1.39	1.45	4.05	0.547	2.22	0.614	0.729	0.690	0.982	<0.0010	<0.0010
Antimony (Sb)-Total	mg/L	0.0001	0.00183	0.00184	0.00207	0.00086	0.00098	0.00084	<0.0010	<0.0010	<0.0010	<0.00010	<0.00010
Arsenic (As)-Total	mg/L	0.0001	0.00104	0.00115	0.00133	0.00074	0.00071	0.00054	0.00129	0.00106	0.00096	<0.00010	<0.00010
Barium (Ba)-Total	mg/L	0.00005	0.0437	0.0500	0.0537	0.0537	0.0683	0.0462	0.0325	0.0316	0.0341	<0.000050	<0.000050
Beryllium (Be)-Total	mg/L	0.0005	<0.00050	<0.00050	<0.00050	<0.0025	<0.0025	<0.0025	<0.0010	<0.0010	<0.0010	<0.00050	<0.00050
Bismuth (Bi)-Total	mg/L	0.0005	<0.00050	<0.00050	<0.00050	<0.0025	<0.0025	<0.0025	<0.0010	<0.0010	<0.0010	<0.00050	<0.00050
Boron (B)-Total	mg/L	0.01	0.041	0.045	0.042	<0.050	<0.050	<0.050	0.047	0.045	0.049	<0.010	<0.010
Cadmium (Cd)-Total	mg/L	0.00002	0.000109	<0.0010	0.000337	0.00013	0.00014	<0.00010	0.000075	0.000126	0.000199	<0.000020	<0.000020
Calcium (Ca)-Total	mg/L	0.02	26.5	30.8	29.4	321	372	343	139	135	135	<0.020	<0.020
Chromium (Cr)-Total	mg/L	0.0005	0.00146	0.00198	0.00270	<0.0025	0.0043	<0.0025	0.0029	0.0029	0.0031	<0.00050	<0.00050
Cobalt (Co)-Total	mg/L	0.0001	0.00046	0.00054	0.00111	<0.00050	0.00079	<0.00050	0.00020	0.00020	0.00032	<0.00010	<0.00010
Copper (Cu)-Total	mg/L	0.0001	0.0202	0.0224	0.0676	0.0112	0.302	0.0200	0.0164	0.0137	0.00830	<0.00010	<0.00010
Iron (Fe)-Total	mg/L	0.03	1.58	2.01	3.02	0.609	2.01	0.263	0.821	0.748	0.992	<0.030	<0.030
Lead (Pb)-Total	mg/L	0.00005	0.000230	0.000324	0.000330	0.00032	0.00076	0.00026	0.00036	0.00028	0.00023	<0.000050	<0.000050
Lithium (Li)-Total	mg/L	0.005	<0.0050	<0.0050	<0.0050	<0.025	<0.025	<0.025	<0.010	<0.010	<0.010	<0.0050	<0.0050
Magnesium (Mg)-Total	mg/L	0.005	1.64	1.88	2.65	8.49	10.7	9.16	2.79	2.95	3.43	<0.0050	<0.0050
Manganese (Mn)-Total	mg/L	0.00005	0.0364	0.0522	0.0491	0.0259	0.0635	0.0154	0.0298	0.0280	0.0339	<0.000050	<0.000050
Mercury (Hg)-Total	mg/L	0.00001	<0.000010	<0.000010	<0.000010	<0.000010	<0.000010	<0.000010	<0.000010	<0.000010	<0.000010	<0.000010	<0.000010
Molybdenum (Mo)-Total	mg/L	0.00005	0.581	0.598	0.655	0.512	0.536	0.504	0.276	0.255	0.248	<0.00011	<0.000050
Nickel (Ni)-Total	mg/L	0.0005	0.00177	0.00214	0.00235	0.0028	0.0045	0.0029	0.0012	0.0013	0.0014	<0.00050	<0.00050
Phosphorus (P)-Total	mg/L	0.3	<0.30	<0.30	<0.30	<0.30	<0.30	<0.30	<0.30	<0.30	<0.30	<0.30	<0.30
Potassium (K)-Total	mg/L	0.05	20.0	21.0	21.3	41.3	42.7	40.9	27.2	27.8	28.3	<0.050	<0.050
Selenium (Se)-Total	mg/L	0.0005	0.00358	0.00373	0.00516	0.00718	0.00849	0.00827	0.00456	0.00413	0.00367	<0.00050	<0.00050

Project 830-7 SCHAFT CREEK
Report To JONATHAN OLSEN, RESCAN ENVIRONMENTAL SERVICES

RESULTS OF ANALYSIS

Sample ID	Units	Detection Limits	LIARD ZONE REP 1	LIARD ZONE REP 2	LIARD ZONE REP 3	PARAMOUNT REP 1	PARAMOUNT REP 2	PARAMOUNT REP 3	WEST BRECCIA REP 1	WEST BRECCIA REP 2	WEST BRECCIA REP 3	FIELD BLANK	TRAVEL BLANK
Date Sampled			27-AUG-07	27-AUG-07	27-AUG-07	28-AUG-07	28-AUG-07	28-AUG-07	05-SEP-07	05-SEP-07	05-SEP-07	05-SEP-07	05-SEP-07
Time Sampled			12:00	12:00	12:00	10:30	11:30	12:15	10:00	11:00	11:45	11:15	00:00
ALS Sample ID			L547761-1	L547761-2	L547761-3	L547756-1	L547756-2	L547756-3	L550220-1	L550220-2	L550220-3	L550220-4	L550220-5
Matrix			Water	Water	Water	Water	Water	Water	Water	Water	Water	Water	Water
ALS File No.			L547761	L547761	L547761	L547756	L547756	L547756	L550220	L550220	L550220	L550220	L550220
Date Received			29-Aug-07	29-Aug-07	29-Aug-07	29-Aug-07	29-Aug-07	29-Aug-07	05-Sep-07	05-Sep-07	05-Sep-07	05-Sep-07	05-Sep-07
Date Finalized			03-Oct-07	03-Oct-07	03-Oct-07	22-Sep-07	22-Sep-07	22-Sep-07	02-Oct-07	02-Oct-07	02-Oct-07	02-Oct-07	02-Oct-07
Silicon (Si)-Total	mg/L	0.05	4.47	4.61	9.00	1.97	4.61	1.82	2.28	2.04	2.40	<0.050	<0.050
Silver (Ag)-Total	mg/L	0.00001	0.000021	0.000022	0.000049	<0.000050	0.000255	<0.000050	0.000023	0.000033	<0.000020	<0.000010	<0.000010
Sodium (Na)-Total	mg/L	2	63.4	66.8	59.6	54.7	53.0	52.8	50.6	50.5	49.8	<2.0	<2.0
Strontium (Sr)-Total	mg/L	0.0001	0.682	0.747	0.798	2.28	2.24	2.16	1.47	1.47	1.47	<0.00010	<0.00010
Thallium (Tl)-Total	mg/L	0.0001	<0.00010	<0.00010	<0.00010	<0.00050	<0.00050	<0.00050	<0.00020	<0.00020	<0.00020	<0.00010	<0.00010
Tin (Sn)-Total	mg/L	0.0001	0.00576	0.00638	0.00641	0.00440	0.00215	0.00226	0.0119	0.0107	0.00993	<0.00010	<0.00010
Titanium (Ti)-Total	mg/L	0.01	<0.010	<0.010	0.053	<0.010	0.042	<0.010	<0.010	<0.010	0.011	<0.010	<0.010
Uranium (U)-Total	mg/L	0.00001	0.000032	0.000035	0.000044	0.000056	0.000139	<0.000050	0.000034	0.000028	0.000028	<0.000010	<0.000010
Vanadium (V)-Total	mg/L	0.001	0.0070	0.0076	0.0132	<0.0050	0.0070	<0.0050	0.0028	0.0025	0.0037	<0.0010	<0.0010
Zinc (Zn)-Total	mg/L	0.001	0.0036	0.0045	<0.0090	0.0053	0.0107	0.0055	0.0060	0.0040	0.0044	<0.0010	<0.0010
Dissolved Metals													
Aluminum (Al)-Dissolved	mg/L	0.001	0.378	0.335	0.366	0.0709	0.0717	0.0729	0.154	0.104	0.113	-	-
Antimony (Sb)-Dissolved	mg/L	0.0001	0.00298	0.00309	0.00293	0.00110	0.00088	0.00089	0.0013	0.0011	0.0010	-	-
Arsenic (As)-Dissolved	mg/L	0.0001	0.00114	0.00115	0.00117	0.00064	0.00054	0.00054	0.00120	0.00083	0.00074	-	-
Barium (Ba)-Dissolved	mg/L	0.00005	0.0205	0.0208	0.0210	0.0517	0.0454	0.0440	0.0254	0.0259	0.0268	-	-
Beryllium (Be)-Dissolved	mg/L	0.0005	<0.00050	<0.00050	<0.00050	<0.0025	<0.0025	<0.0025	<0.0010	<0.0010	<0.0010	-	-
Bismuth (Bi)-Dissolved	mg/L	0.0005	<0.00050	<0.00050	<0.00050	<0.0025	<0.0025	<0.0025	<0.0010	<0.0010	<0.0010	-	-
Boron (B)-Dissolved	mg/L	0.01	0.043	0.047	0.047	<0.050	<0.050	<0.050	0.047	0.046	0.048	-	-
Cadmium (Cd)-Dissolved	mg/L	0.00002	0.000123	<0.0010	0.000071	0.00019	0.00024	0.00037	0.000086	0.000104	0.000071	-	-
Calcium (Ca)-Dissolved	mg/L	0.02	24.3	25.1	25.8	318	368	404	142	134	131	-	-
Chromium (Cr)-Dissolved	mg/L	0.0005	0.00096	0.00161	0.00100	<0.0025	<0.0025	<0.0025	0.0016	0.0014	0.0013	-	-
Cobalt (Co)-Dissolved	mg/L	0.0001	<0.00010	<0.00010	<0.00010	<0.00050	<0.00050	<0.00050	<0.00020	<0.00020	<0.00020	-	-
Copper (Cu)-Dissolved	mg/L	0.0001	0.00022	0.00021	0.00025	0.00186	0.00214	0.00135	0.00049	0.00062	0.00073	-	-
Iron (Fe)-Dissolved	mg/L	0.03	<0.030	<0.030	<0.030	0.058	<0.030	<0.030	<0.030	<0.030	<0.030	-	-
Lead (Pb)-Dissolved	mg/L	0.00005	<0.000050	<0.000050	<0.000050	<0.00025	<0.00025	<0.00025	<0.00010	<0.00010	<0.00010	-	-
Lithium (Li)-Dissolved	mg/L	0.005	<0.0050	<0.0050	<0.0050	<0.025	<0.025	<0.025	<0.010	<0.010	<0.010	-	-
Magnesium (Mg)-Dissolved	mg/L	0.005	1.15	1.17	1.11	8.05	9.67	10.2	2.55	2.71	2.81	-	-
Manganese (Mn)-Dissolved	mg/L	0.00005	0.00117	0.00307	0.000443	0.0113	0.0101	0.0158	0.0133	0.0132	0.0124	-	-
Mercury (Hg)-Dissolved	mg/L	0.00001	<0.000010	<0.000010	<0.000010	<0.000010	<0.000010	<0.000010	<0.000010	<0.000010	<0.000010	-	-
Molybdenum (Mo)-Dissolved	mg/L	0.00005	0.607	0.617	0.623	0.515	0.537	0.598	0.282	0.264	0.254	-	-
Nickel (Ni)-Dissolved	mg/L	0.0005	<0.00050	<0.00050	<0.00050	<0.0025	<0.0025	0.0036	<0.0010	<0.0010	<0.0010	-	-
Phosphorus (P)-Dissolved	mg/L	0.3	<0.30	<0.30	<0.30	<0.30	<0.30	<0.30	<0.30	<0.30	<0.30	-	-
Potassium (K)-Dissolved	mg/L	0.05	22.0	22.0	21.4	41.0	44.0	48.5	27.7	28.0	27.4	-	-
Selenium (Se)-Dissolved	mg/L	0.0005	0.00408	0.00375	0.00403	0.00714	0.00798	0.00839	0.00465	0.00449	0.00413	-	-
Silicon (Si)-Dissolved	mg/L	0.05	3.36	3.40	3.46	1.56	1.40	1.40	1.79	1.57	1.52	-	-
Silver (Ag)-Dissolved	mg/L	0.00001	<0.000010	<0.000010	<0.000010	<0.000050	<0.000050	<0.000050	<0.000020	<0.000020	<0.000020	-	-
Sodium (Na)-Dissolved	mg/L	2	70.1	70.9	70.8	55.5	53.5	53.8	52.0	50.9	51.9	-	-
Strontium (Sr)-Dissolved	mg/L	0.0001	0.686	0.679	0.716	2.27	2.29	2.65	1.50	1.44	1.43	-	-
Thallium (Tl)-Dissolved	mg/L	0.0001	<0.00010	<0.00010	<0.00010	<0.00050	<0.00050	<0.00050	<0.00020	<0.00020	<0.00020	-	-
Tin (Sn)-Dissolved	mg/L	0.0001	0.00567	0.00596	0.00617	0.00435	0.00233	0.00227	0.0122	0.0104	0.00982	-	-
Titanium (Ti)-Dissolved	mg/L	0.01	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010	<0.010	-	-
Uranium (U)-Dissolved	mg/L	0.00001	0.000013	0.000011	0.000011	<0.000050	<0.000050	<0.000050	<0.000020	<0.000020	<0.000020	-	-
Vanadium (V)-Dissolved	mg/L	0.001	0.0045	0.0046	0.0048	<0.0050	<0.0050	<0.0050	<0.0020	<0.0020	<0.0020	-	-
Zinc (Zn)-Dissolved	mg/L	0.001	<0.0010	<0.0010	<0.0010	<0.0050	<0.0050	<0.0050	<0.0020	<0.0020	<0.0020	-	-
Organic Parameters													
COD	mg/L	20	460	490	490	470	480	510	470	520	550	<20	<20
Total Organic Carbon	mg/L	0.5	104	116	116	113	115	115	115	125	133	<0.50	<0.50

APPENDIX C. Rietveld X-Ray-Diffraction Mineralogy of the Three Tailings Samples (by the University of British Columbia)

QUANTITATIVE PHASE ANALYSIS OF THREE POWDER SAMPLES USING THE RIETVELD METHOD AND X-RAY POWDER DIFFRACTION DATA.

(Project : Schaft Creek Tailings)

Uren Shane
Rescan Environmental Services
6th Floor – 1111 West Hastings Street
Vancouver, B.C. V6E 2J3

Mati Raudsepp, Ph.D.
Elisabetta Pani, Ph.D.
Dept. of Earth & Ocean Sciences
6339 Stores Road
The University of British Columbia
Vancouver, BC V6T 1Z4

October 22, 2007

EXPERIMENTAL METHOD

The three samples “Liard Zone”, “Paramount” and “West Breccia” were reduced into fine powder to the optimum grain-size range for X-ray analysis (<10μm) grinding under ethanol in a vibratory McCrone Micronising Mill for 7 minutes. Step-scan X-ray powder-diffraction data were collected over a range 3-80°2θ with CoKα radiation on a standard Siemens (Bruker) D5000 Bragg-Brentano diffractometer equipped with an Fe monochromator foil, 0.6 mm (0.3°) divergence slit, incident- and diffracted-beam Soller slits and a Vantec-1 strip detector. The long fine-focus Co X-ray tube was operated at 35 kV and 40 mA, using a take-off angle of 6°.

RESULTS AND DISCUSSION

The X-ray diffractograms were analyzed using the International Centre for Diffraction Database PDF-4 using Search-Match software by Siemens (Bruker). X-ray powder-diffraction data were refined with Rietveld program Topas 3 (Bruker AXS). The results of quantitative phase analysis by Rietveld refinement are given in Table 1. These amounts represent the relative amounts of crystalline phases normalized to 100%. The Rietveld refinement plots for the samples are shown in Figures 1 – 3.

Table 1. Results of quantitative phase analysis (wt. %) – Proj. Schaft Creek Tailings

Mineral	Ideal formula	Liard Zone	Paramount	West Breccia
Quartz	SiO_2	17.3	23.9	16.6
Muscovite	$KAl_2AlSi_3O_{10}(OH)_2$	16.9	14.1	12.2
Clinochlore	$(Mg,Fe^{2+})_5Al(Si_3Al)O_{10}(OH)_8$	11.1	9.0	10.7
K-feldspar	$KAlSi_3O_8$	1.5		4.5
Plagioclase	$NaAlSi_3O_8$ – $CaAl_2Si_2O_8$	42.7	44.7	49.5
Calcite	$CaCO_3$	6.4	5.5	4.5
Dolomite	$CaMg(CO_3)_2$	2.7	2.7	0.7
Pyrite	FeS_2			0.4
Hematite	α-Fe_2O_3	0.8		
Magnetite	Fe_3O_4	0.5		0.8
Total		100.0	100.0	100.0

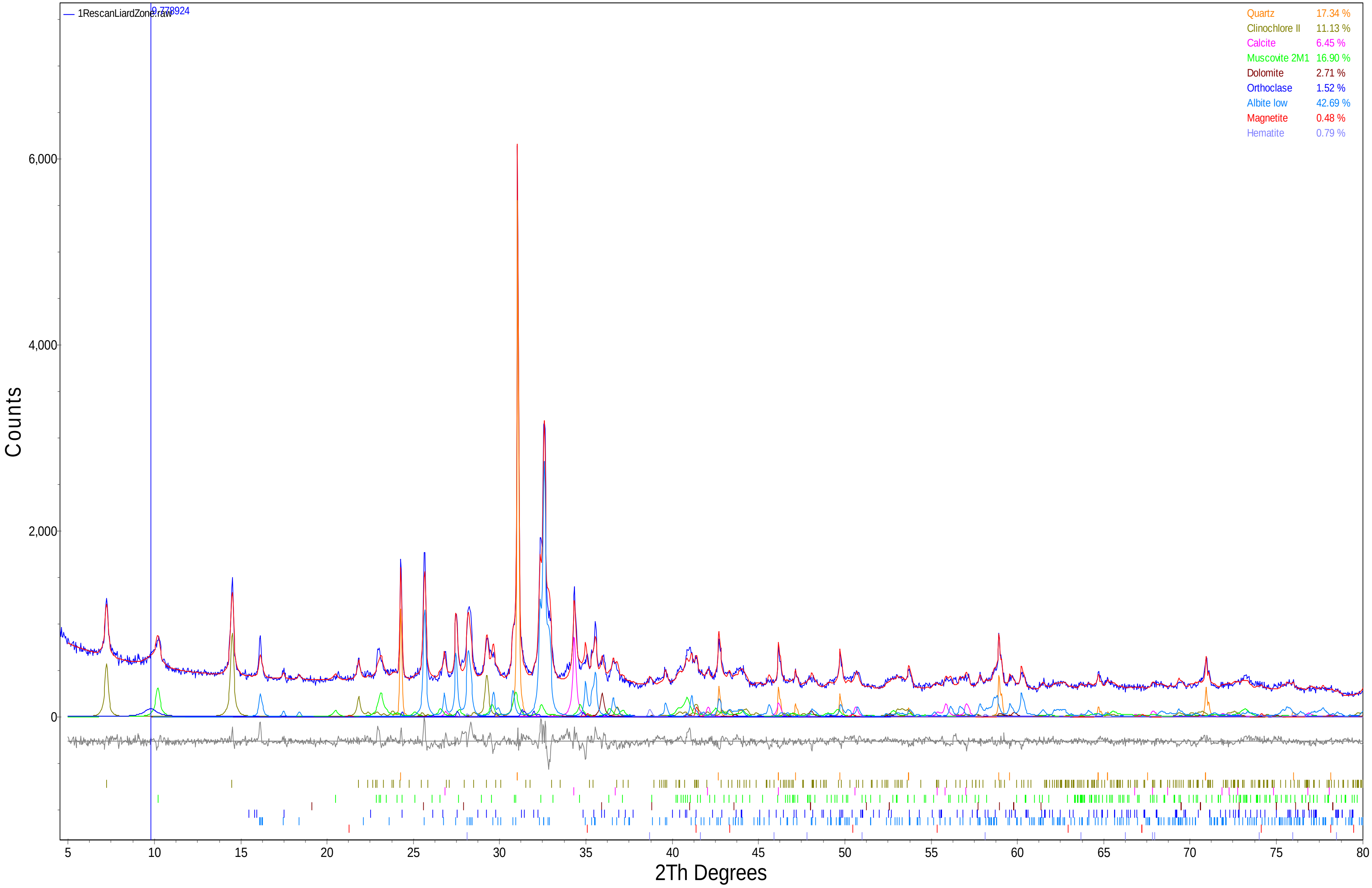


Figure 1. Rietveld refinement plot of sample **Rescan Liard Zone** (blue line - observed intensity at each step; red line - calculated pattern; solid grey line below – difference between observed and calculated intensities; vertical bars, positions of all Bragg reflections). Coloured lines are individual diffraction patterns of all phases.

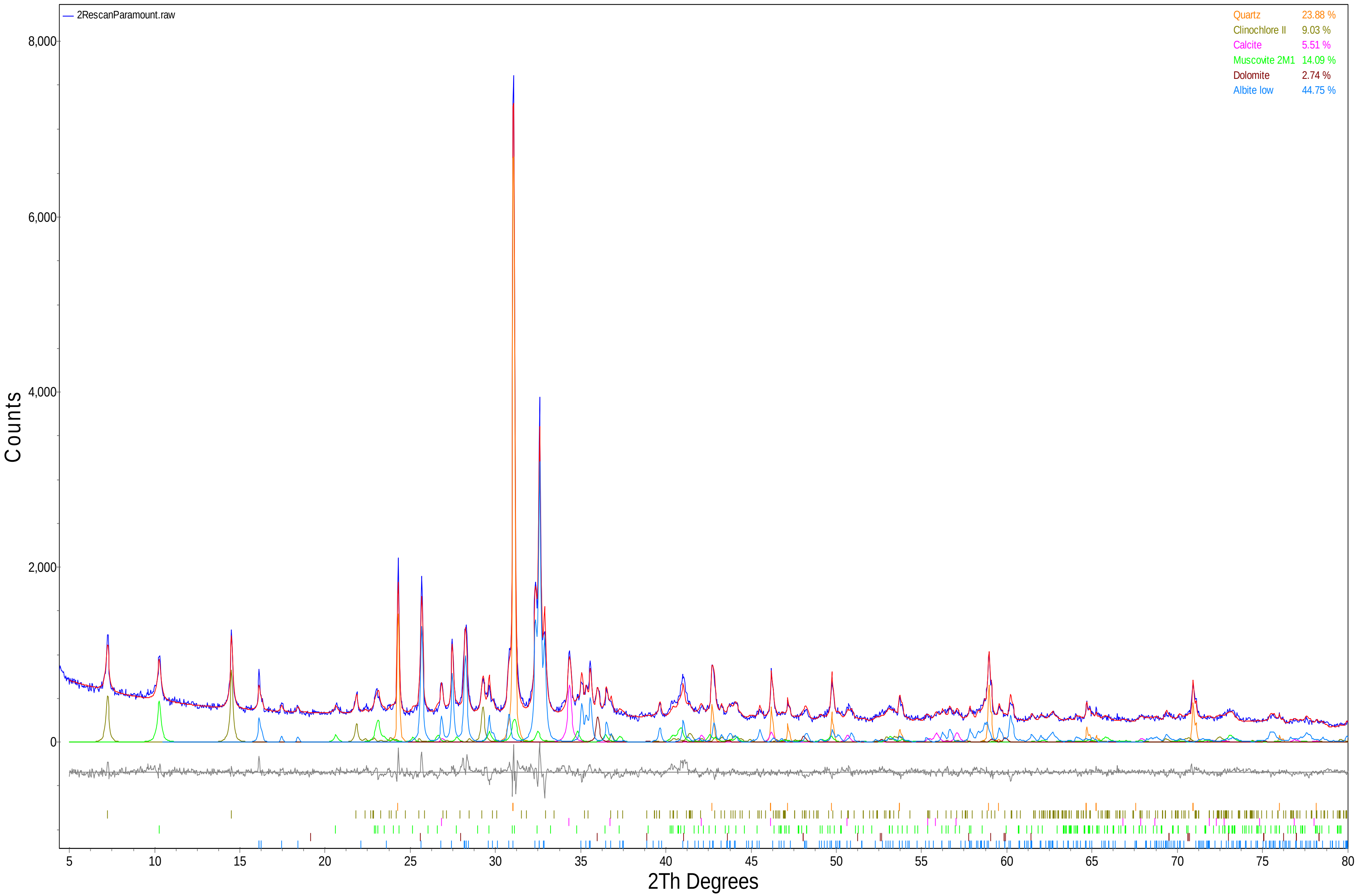


Figure 2. Rietveld refinement plot of sample **Rescan Paramount** (blue line - observed intensity at each step; red line - calculated pattern; solid grey line below – difference between observed and calculated intensities; vertical bars, positions of all Bragg reflections). Coloured lines are individual diffraction patterns of all phases.

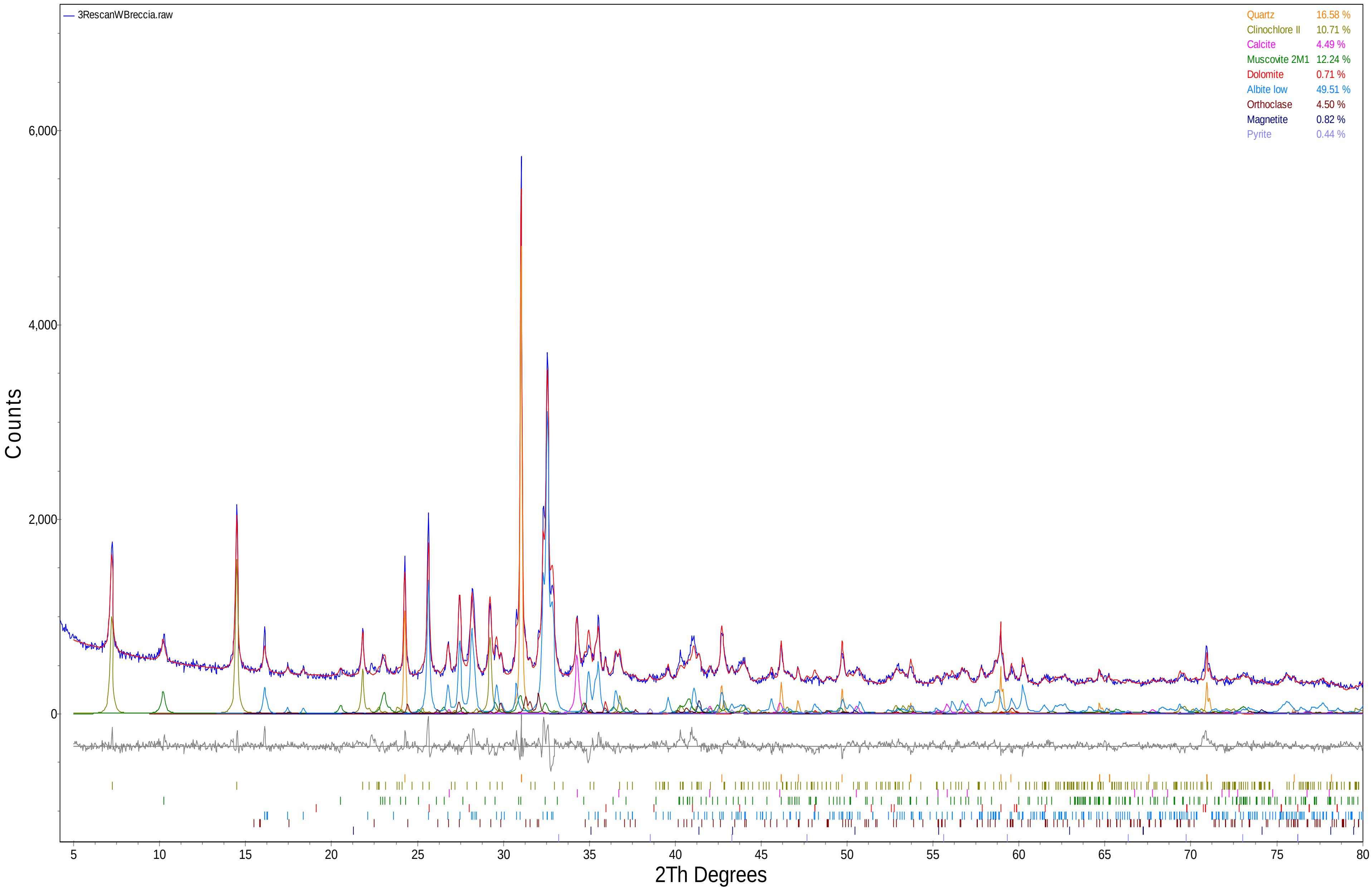


Figure 3. Rietveld refinement plot of sample **Rescan West Breccia** (blue line - observed intensity at each step; red line - calculated pattern; solid grey line below – difference between observed and calculated intensities; vertical bars, positions of all Bragg reflections). Coloured lines are individual diffraction patterns of all phases.

CopperFox Metals Inc.
Schaft Creek Project
British Columbia, Canada

Schaft Creek Project
Noise Baseline Report



Prepared by:

Rescan Tahltan Environmental Consultants
Vancouver, British Columbia

February 2008

EXECUTIVE SUMMARY

Executive Summary

The Schaft Creek Project is located on the eastern edge of the Coastal Mountains in north central British Columbia, 80 kilometers southwest of Telegraph Creek and 76 kilometers west of Highway 37. The property is within the Tahltan Nation's traditional territory, and is comprised of 40 mineral claims, covering 21,016 hectares.

The construction and operation of the Schaft Creek copper deposit proposed by Copper Fox Metals Inc. (Copper Fox) will create noise. Noise is defined as unwanted sound. During the construction phase, the primary sources of noise will be excavation equipment, vehicles, blasting and air traffic. Throughout operation of the mine, noise will be generated by rock blasting and ore crushing, along with vehicles and air traffic.

The objective of this study is to describe the baseline noise levels measured in the Schaft Creek Project area. In 2007, baseline noise was measured at four locations within or near the Project area. Two locations in the Mess Creek valley (FD-7 and FD-8) were monitored between 3:00 pm on June 26th, 2007 and 3:00 pm on June 30th, 2007. Two additional locations 9.7 km and 12.8 km north of the Schaft Creek Camp area (FD-4 and FD-5, respectively) in the Schaft Creek valley were monitored between 11:00 am on July 14th, 2007 and 11:00 am on July 18th, 2007. The meters recorded average and peak sound levels in "A" weighted decibels (dBA) every minute. The observed 4 day equivalent noise level (L_{eq}) values were 48.2 dBA and 45.2 dBA at stations FD-7 and FD-8, respectively and 45.6 dBA and 40.0 dBA at stations FD-4 and FD-5.

Elevated noise levels at all four study locations correlated with elevated wind speeds at the Saddle meteorological station at Schaft Creek. Noise effects of precipitation were at most noticeable but generally negligible. Thus, baseline noise fluctuations can generally be attributed to wind effects the area.

TABLE OF CONTENTS

Schaft Creek Project: Noise Baseline Report

TABLE OF CONTENTS

LIST OF FIGURES

Figure **Page**

LIST OF TABLES

Table **Page**

LIST OF PLATES

Plate **Page**

1. INTRODUCTION

1. Introduction

The construction and operation of the proposed Schaft Creek Project will create noise. Noise is defined as unwanted sound. During the construction and operation phase of the mine, drilling, blasting, excavating and haul equipment as well as ore crushing and air traffic will be the primary sources of noise. An assessment of potential effects of noise associated with the construction and operation of the Schaft Creek Project will be completed as part of the Environmental Assessment (EA) process, which will be completed in early 2009.

The objective of this study is to describe the baseline noise levels at the Schaft Creek property.

1.1 Schaft Creek Project Summary

Copper Fox Metals Inc. (Copper Fox) is a Canadian mineral exploration and development company focused on developing the Schaft Creek deposit located in north-western British Columbia, approximately 60 km south of the village of Telegraph Creek (Figure 1.1-1). The Schaft Creek deposit is a polymetallic (copper-gold-silver-molybdenum) deposit located in the Liard District of north-western British Columbia (Latitude 57^{o} 22’ 4.2’’; Longitude 130^{o}, 58’ 48.9”). The property is comprised of 40 mineral claims covering an area totalling approximately 20,932 ha within the Cassiar Iskut-Stikine Land and Resource Management Plan (Figure 1.1-2).

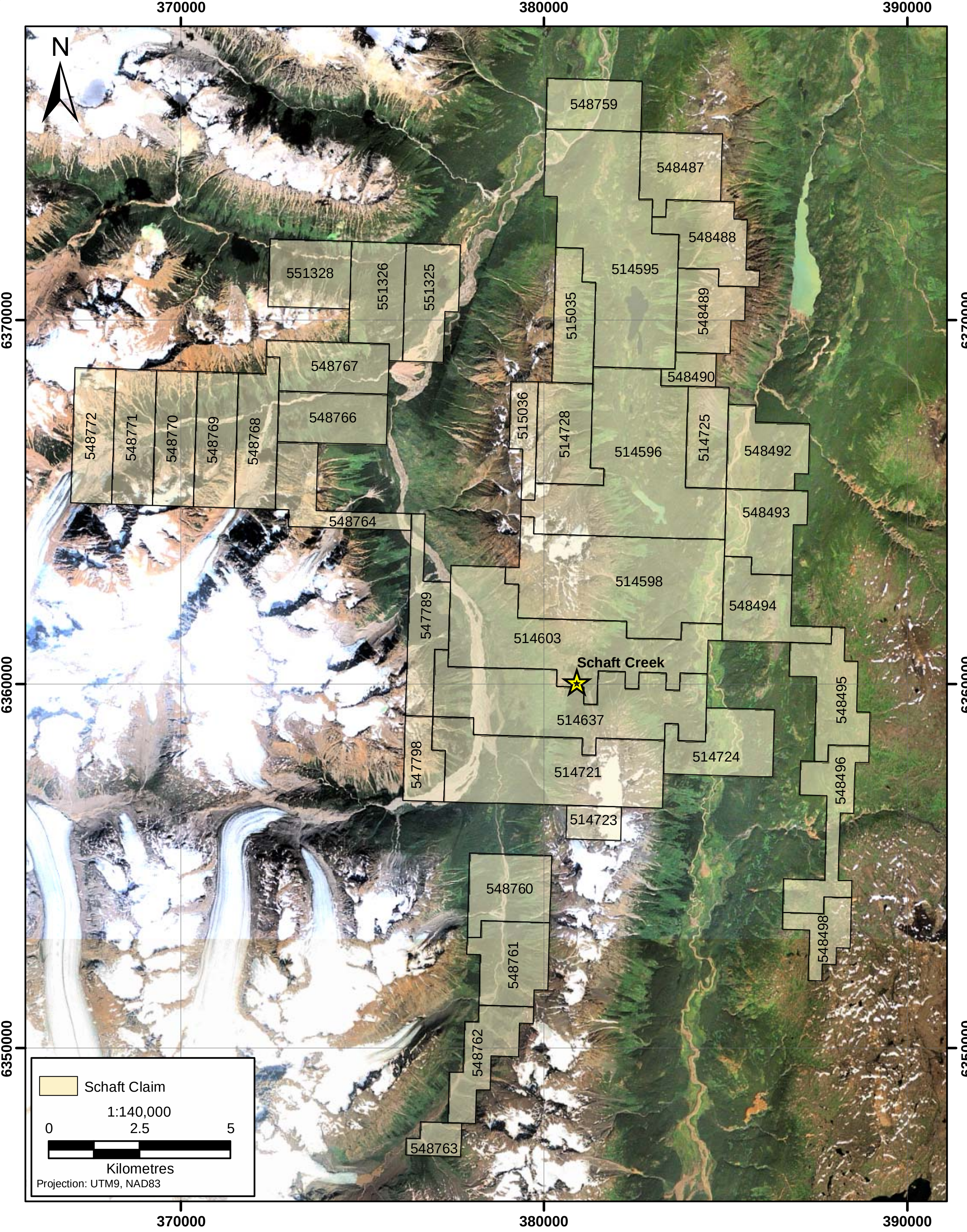
The Schaft Creek Project is located within the traditional territory of the Tahltan Nation. Copper Fox has been in discussions with the Tahltan Central Council (TCC) and the Tahltan Heritage Resources Environmental Assessment Team (THREAT) since initiating exploration activities in 2005. Copper Fox has engaged in numerous agreements with the TCC including a Communications Agreement, Traditional Knowledge Agreement, Letter of Understanding with the Tahltan Nation Development Corporation (TNDC) and a THREAT Agreement. Copper Fox will continue to work together with the Tahltan Nation as work on the Schaft Creek Project continues.

The Schaft Creek deposit was discovered in 1957 and has since been investigated by prospecting, geological mapping, geophysical surveys as well as diamond and percussion drilling. Over 65,000 meters of drilling has been completed on the property as of end of 2007. Additional drilling is planned for 2008 to support future economic assessments of the property and an environmental assessment application.

The Schaft Creek Project entered the British Columbia environmental assessment process in August 2006. Although a formal federal decision has not yet been made, the Project will likely require federal approval as per the Canadian Environmental Assessment Act. Copper Fox has targeted the end of 2008 for submission of their Schaft Creek Environmental Assessment Application.

Location Map for Schaft Creek Project

FIGURE 1.1-1



copper FOX metals inc.

Schaft Creek Project Mineral Claims

FIGURE 1.1-2

RTEC Rescan™

Copper Fox has recently released a scoping level engineering and economic report for Schaft Creek. The mine and associated infrastructure are presented in Figure 1.1-3. The current mine plan has ore milled from an open pit at a rate of 65,000 tonnes/day. The Schaft deposit will be mined with large truck/shovel operations and typical drill and blast techniques. An explosives manufacturing facility will be constructed on-site to support blasting activities. The mine plan includes 719 million tonnes of minable ore over a 31 year mine life. The Project is estimated to generate up to 1,200 jobs during the construction phase of the project and approximately 500 permanent jobs during the life of the mine.

Ore will be crushed, milled and filtered on-site to produce copper and molybdenum concentrates. The mill will include a typical comminution circuit (Semi-Autogenous Mill, Ball Mill and Pebble Crusher) followed by a flotation circuit and a copper circuit with thickener, filtration and concentrate loadout and shipping. The mill includes a designated molybdenum circuit with thickener, filtration circuit, drying and bagging. The filter plant will be located at the plant site. A tailings thickener and water reclaim system will be used to recycle process water. The circuit will have a design capacity of 70,652 tonnes per day and a nominal capacity of 65,000 tonnes per day (23,400,000 tonnes per year). The copper and molybdenum concentrates will be shipped via truck from the mill to the port of Stewart, BC.

Copper Fox will construct an access road from Highway 37 to the Schaft Creek property. Access to the property from Highway 37 will require approximately 105 km of new road. The first 65 km of the access road to the Schaft Creek property corresponds to the Galore Creek access road. NovaGold and Teck Cominco have currently put a hold on future construction efforts along their access road and the overall Galore Creek Project. Copper Fox will seek approval from the provincial government and NovaGold/Teck Cominco to construct the first 65 km of the Galore Creek access road should the status of the project not change.

The route of the final 40 km of access road has not been finalized. Copper Fox has completed initial investigations of a route along Mess Creek. An alternative route is also being considered that utilizes the plateau to the east of Mess Creek. Copper Fox is currently investigating the feasibility, as it relates to geohazards, of the two alignments. Both alignments include a 30 m bridge on Mess Creek. Mess Creek is considered navigable as per Transportation Canada criteria. Figure 1.1-4 presents the access road alignment that follows the Galore Creek road (65 km from Highway 37) and the Mess Creek alignment (40 km) to the Schaft Creek property.

Over the life of the mine, the Schaft Creek Project will generate over 700 million tonnes of tailings. There are three tailings facilities being considered (Figure 1.1-3). The three options will undergo an alternatives assessment that will include engineering, construction and operating costs, geotechnical, geohazards, environmental and social considerations.

The Project will generate over a billion tonnes of waste rock. Waste rock dumps are proposed around the perimeter of the pit (Figure 1.1-3). This includes the flat area between the proposed pit and Schaft Creek.

gis no. 832-4-11 Job No. 832-4 February 25, 2008

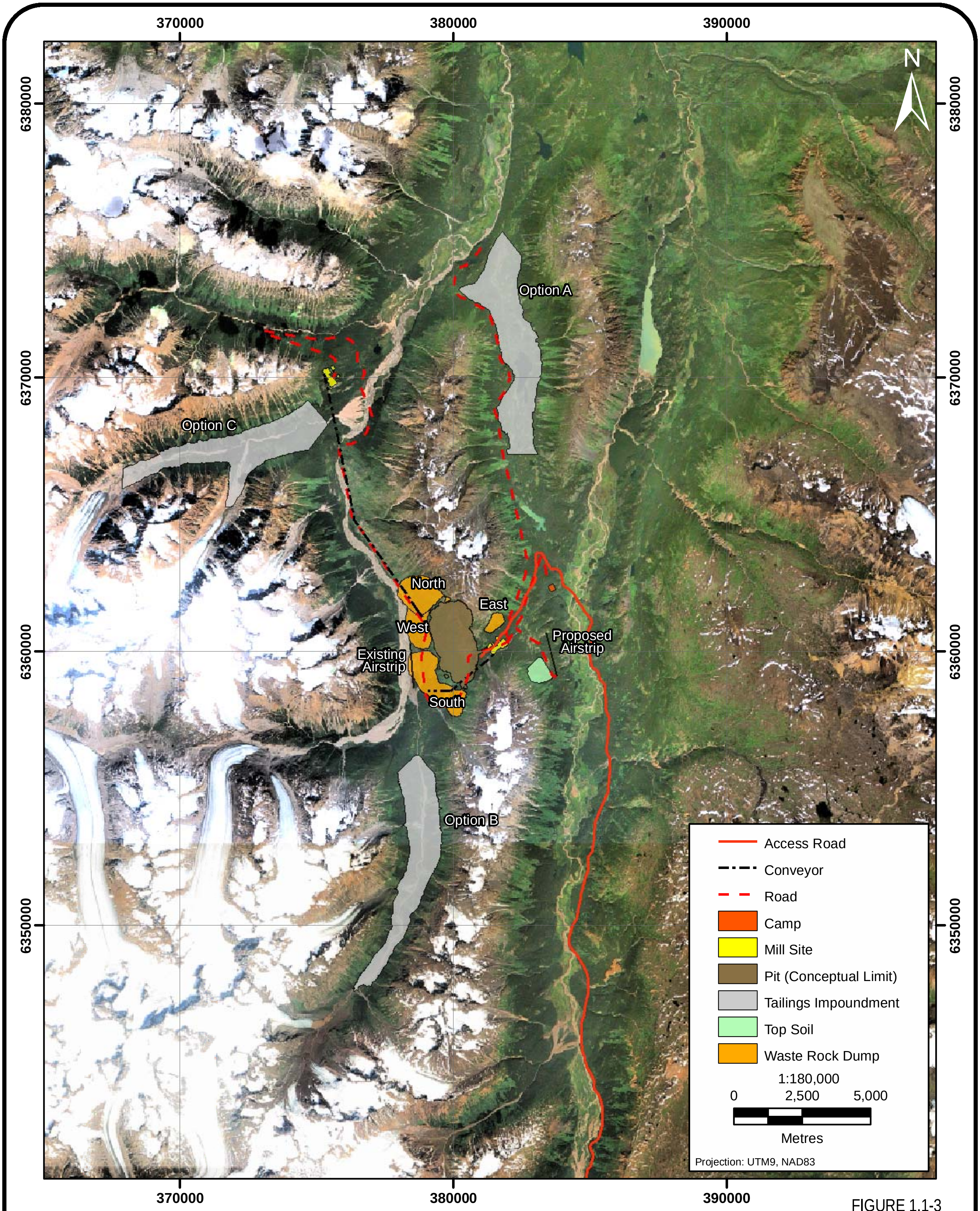


FIGURE 1.1-3

Schaft Creek Project Mine and Associated Infrastructure

copper FOX metals inc.

RTEC

Rescan™

gis no. 832-4-08 Job No. 832-4 February 18, 2008

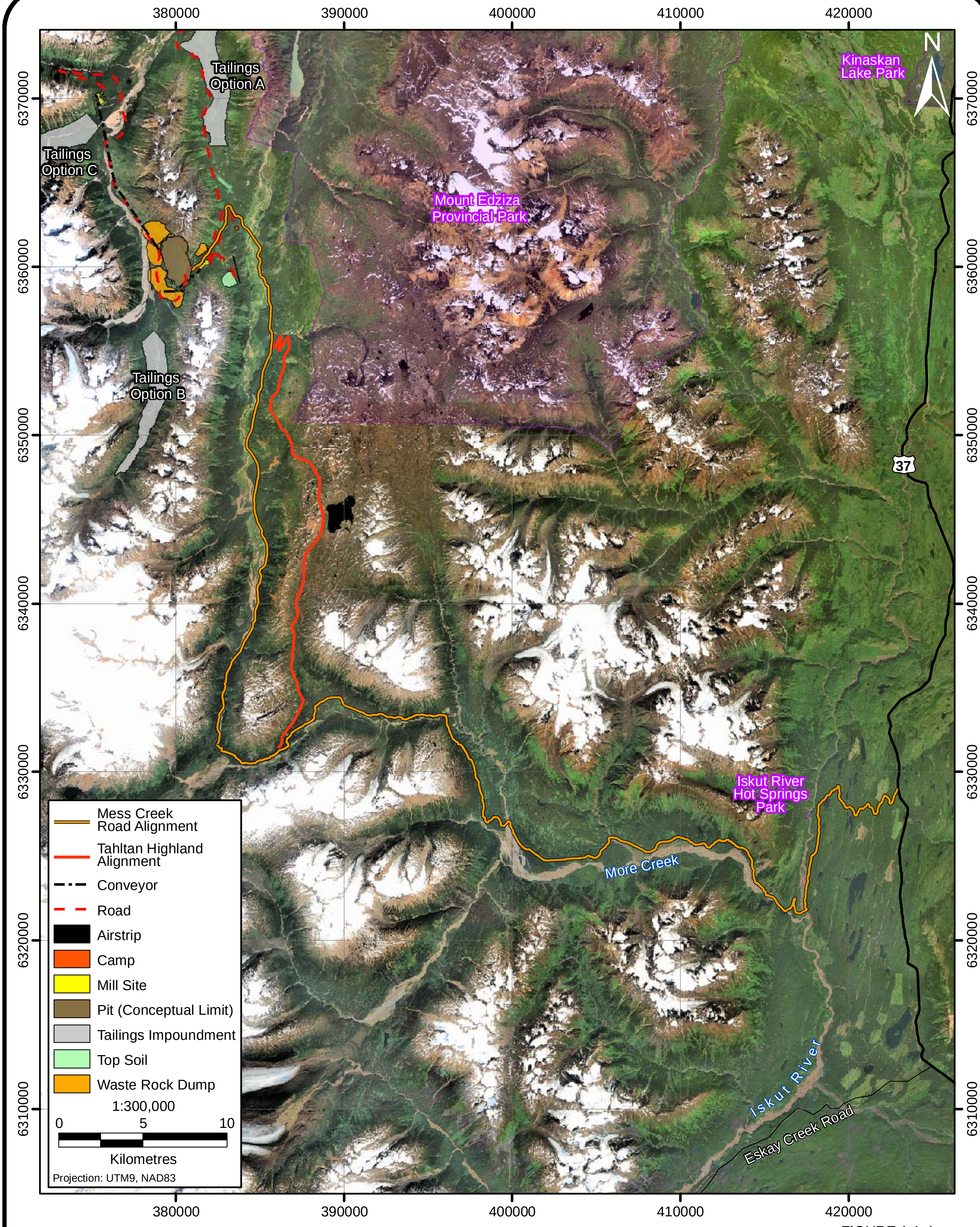


FIGURE 1.1-4

Proposed Access Road Alignment for the Schaft Creek Project

A detailed water management plan has yet to be developed for the Project. A water management plan will be included in the next level of economic assessment (pre-feasibility) and the next project description update. A waste water discharge is expected from the tailings facility, waste rock dumps and domestic waste water treatment plant. The management plan will detail the plans to minimize natural drainage into the tailings facility, the pit and the waste rock dumps. Pit water will be pumped to the tailings facility.

A new airfield will be constructed to the east of the pit (Figure 1.1-3). The Project will be a fly-in, fly-out operation. The new landing strip will be capable of handling a Boeing 737. Other facilities include a terminal building, fuelling, maintenance and control facilities.

A permanent camp will be constructed to support a staff of approximately 500 employees. Other facilities include truck shop, warehouse, administration, maintenance laboratory, explosives storage, water treatment facilities and potable water storage.

Copper Fox has targeted the end of 2008 for submission of their Environmental Assessment Application and full Feasibility Report. Screening of the EA Application plus the 180 day review period will result in project approval as early as July 2009. Copper Fox will likely seek concurrent permitting for strategic permits to facilitate the timely construction of key project components. Construction is estimated to take two and half years. Thus, production could begin by early 2012.

1.2 Overview of Noise Measurement

Noise is defined as unwanted sound, and is characterized by the pressure of sound waves. Because the sound perception of humans is non-linear, a ten-fold increase in sound pressure is perceived as a doubling of the sound level. The decibel (dB) is a logarithmic measure of noise level which takes this non-linearity into consideration. It is defined as the logarithm of the ratio of the root mean square (rms) sound pressure with respect to the standard rms sound pressure. The standard rms sound pressure is the hearing threshold below which the human ear cannot detect sound, and is usually 20 µPa. For humans, a change in sound level is only perceived if the change is greater than 3 dB.

The detection of sound by humans is frequency dependent, and therefore the sound pressure is weighted by its frequency. Most common is the “A” weighting, which represents human hearing, given units of “dBA.” Described below are some typical noise levels in terms of dBA.

- **0 dBA:** human hearing threshold (flying mosquito, 3 m away)
- **10 dBA:** the rustling of leaves
- **20 - 40 dBA:** quiet room
- **40 – 60 dBA**: typical conversation
- **60 – 80 dBA**: passenger car, 10 m away

- **80 – 90 dBA**: busy road, 10 m away
- **100 dBA**: jackhammer, 1 m away
- **110 – 130 dBA**: takeoff of a jet, 100 m away
- **130 dBA**: human pain threshold

Due to the non-linear nature of the decibel scale, sounds are not easily added together. Alternatively, the logarithm must be inverted before addition (Alberta EUB, 2007),

$$L_{total} = 10\log_{10}(10^{\frac{L_1}{10}} + 10^{\frac{L_2}{10}})$$

where L_1 and L_2 are the noise levels to be added (in dB). As an example, a typical conversation (50 dBA) in a quiet room (35 dBA) does not result in a total noise of 85 dBA, comparable to a busy road, 10 m away. Instead, the background noise of the quiet room will not be audible over the conversation. Following the formula for the addition of dB, the noise levels will only increase to 50.1 dBA. Figure 1.2-1 displays the change to overall noise upon addition to a background noise of 35 dBA. In order for the additional noise to be audible, it must be of equal or greater magnitude to the background noise.

Noise levels are dynamic, and are characterized by the equivalent continuous sound level (L_{eq}). This is the dBA level of a constant rms sound pressure containing the same energy as the varying noise. The L_{eq} is usually given for a specific time interval, such as 1 day.

This baseline study uses the L_{eq} and additional measurements to evaluate the noise levels of the study area. The maximum and minimum sound levels observed over the study time period are reported (L_{min} and L_{max}). In addition, the sound level exceeded x % of the time is presented in this report (L_x). The L_x is given for 5, 10, 50 and 90% exceedance.

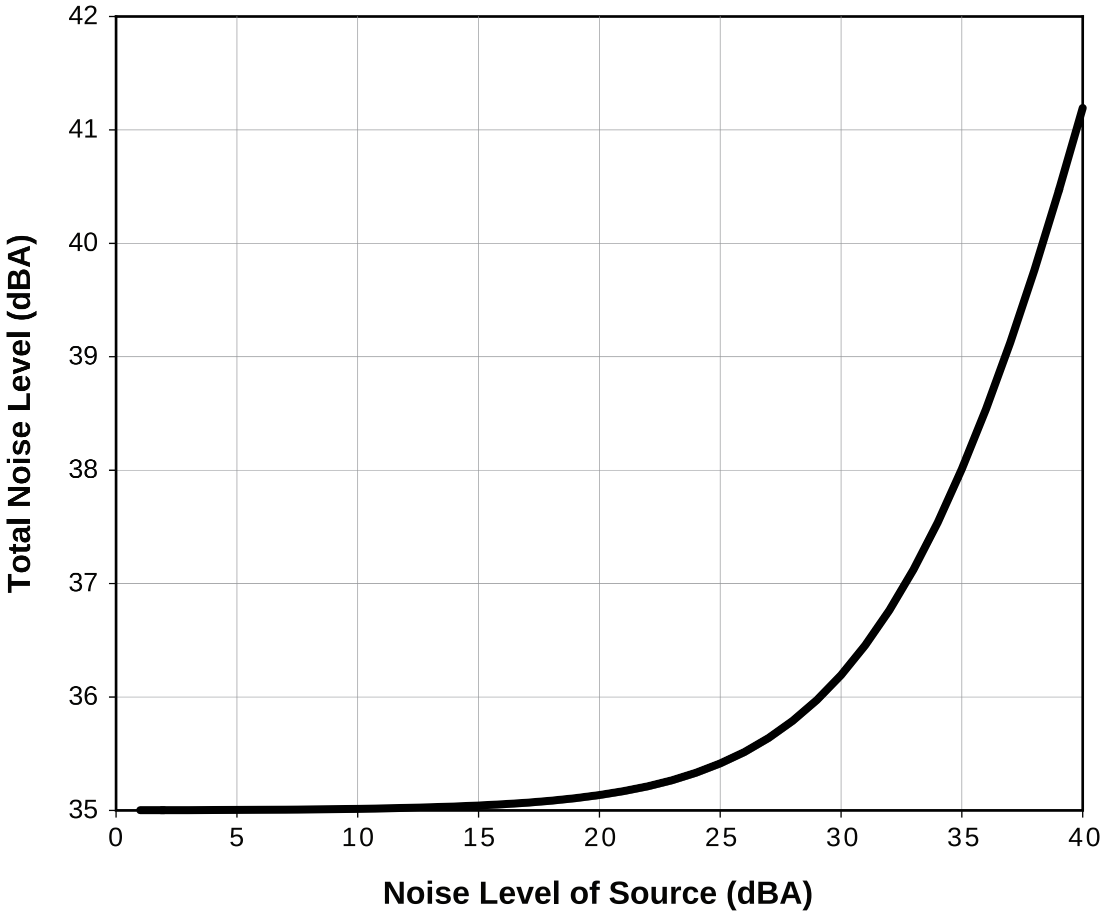


FIGURE 1.2-1

Adding Background Noise (35 dBA) and Source Noise

2. METHODS

2. Methods

Two Quest Model 2900 sound level meters were used for measuring baseline noise. The sound level meter recorded the average sound level and peak sound levels in dBA. Calibration of the sound level was performed using a Quest QC10 Calibrator beforehand. The noise measurements were recorded every minute and the sound meter was located approximately 1.5 m above ground level. The Quest Model 2900 sound level meter has an accuracy of ±2 dB, a noise floor of 30 dBA and a maximum noise range of 90 dBA (Plate 2-1).

Plate 2-1. Photograph of a Quest Model 2900 sound level meter (centre) at Schaft Creek station FD-7 surrounded by two dustfall collectors

Sound level meters were placed at two sampling locations in the Mess Creek Valley alongside two dust collector stands (FD-7 and FD-8) between 3:00 pm on June 26th, 2007 and 3:00 pm on June 30th, 2007 (Table 2-1). The meters were moved to locations FD-4 and FD-5 where noise data was collected starting at 11:00 am on July 14th, 2007, and ending at 11:00 am on July 18th, 2007 (Figure 2-1).

Table 2-1
Location of Noise Baseline Measurements

Location	Easting	Northing	Elevation (masl)	Duration of Noise Measurement
FD-4	376,249	6,368,709	765	14 July 11:00 to 18 July 11:00
FD-5	379,757	6,374,512	719	14 July 11:00 to 18 July 11:00
FD-7	384,926	6,355,244	732	26 June 15:00 to 30 June 15:00
FD-8	383,850	6,345,472	795	26 June 15:00 to 30 June 15:00

gis no. 830-2-03 Job No. 830-2 February 04, 2008

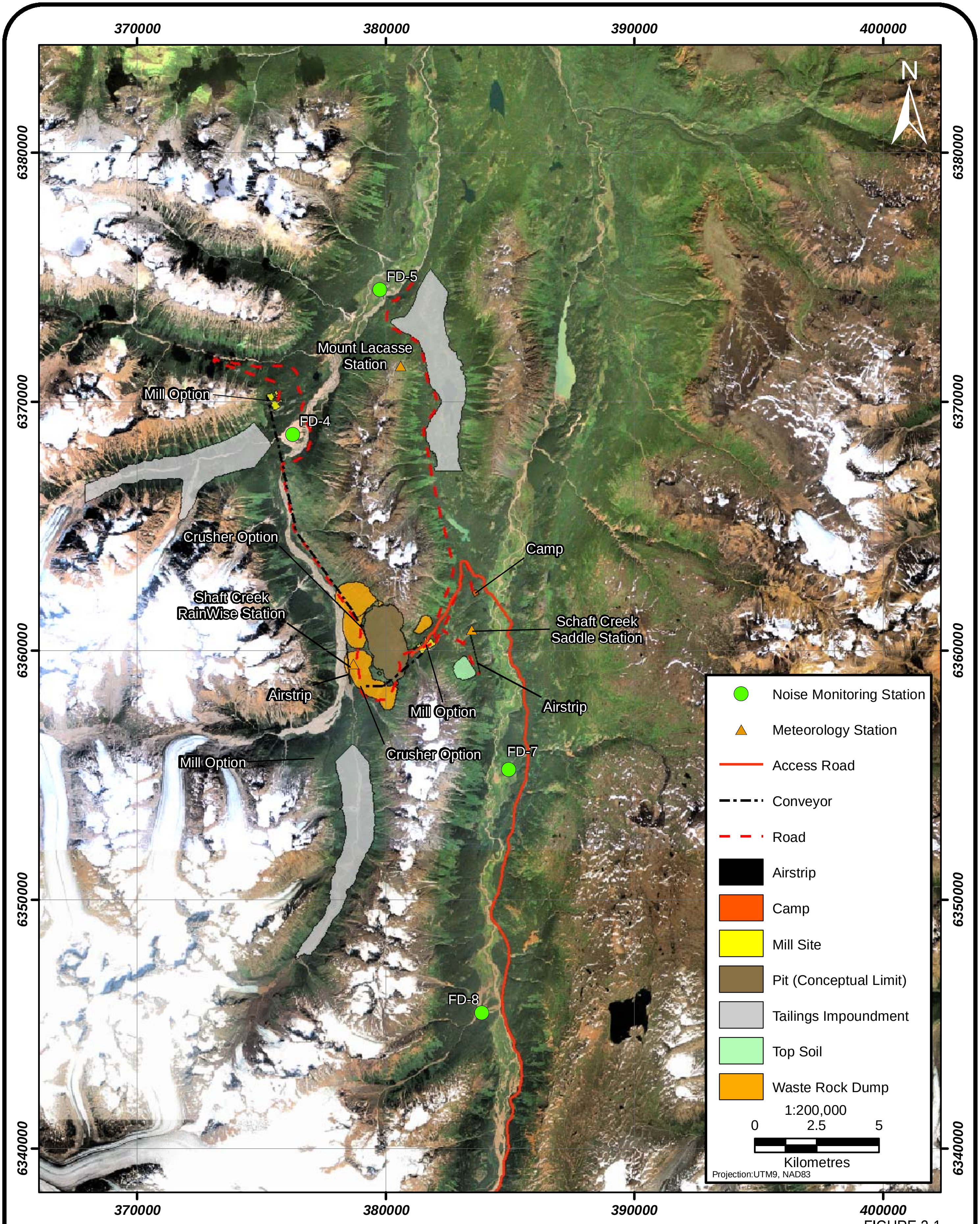


FIGURE 2-1

Schaft Creek Project
Noise Station Locations

3. RESULTS

3. Results

The 4-day L_{eq} values measured at stations FD-7 and FD-8 were 48.2 dBA and 45.2 dBA, respectively. For stations FD-4 and FD-5, the 4-day L_{eq} values were 45.6 dBA and 40.0 dBA, respectively (Table 3-1). These L_{eq} values coincide with noise baseline conditions reported for the Environmental Assessment application for the Galore Creek Project in 2005 by NovaGold Canada Inc. (Rescan, 2005). At Galore Creek, the L_{eq} values reported ranged from 38.5 dBA to 50.5 dBA, conducted in study periods of 7 to 20 hours during July. However, helicopter activity was reported at the majority of the noise sample stations during these study periods.

Table 3-1
Sound Levels (dBA) of the Study Locations

Location	4-day L_{eq}	L_{max}	L_5	L_{10}	L_{50}	L_{90}	L_{min}
FD-4	45.6	75.0	50.2	48.9	43.5	36.1	32.0
FD-5	40.0	78.4	42.1	40.6	36.5	30.6	26.5
FD-7	48.2	89.5	48.8	48.2	42.8	38.6	35.2
FD-8	45.2	61.5	48.7	48.1	44.4	38.4	34.6

Figure 3-1 shows the one minute L_{eq} values recorded at stations FD-7 and FD-8 over the 4 day study period (June 26th to June 30th), along with hourly wind speeds recorded at the Saddle Meteorological Station, located approximately 5.8 km to the north of FD-7 and 15.4 km to the north of FD-8. The Saddle Station wind speeds were assumed to be representative of wind speeds in the Mess Creek valley during the study period.

Figure 3-2 shows the one minute L_{eq} values recorded at stations FD-4 and FD-5 over the 4 day study period (July 14th to July 18th), together with the hourly wind speeds recorded at the Saddle Station. The FD-4 and FD-5 stations were located approximately 9.7 km and 12.8 km north of the Schaft Creek Camp, respectively. Comparison to changes in wind speeds recorded at the Mount LaCasse Station was not possible due to a power surge at the station during the study period caused by a lightning strike. The noise levels were compared to wind speed variations recorded at the Saddle Station, located 10.8 km southeast of FD-4 and 14.2 km southeast of FD-5. Wind speed patterns at the two meteorological stations are generally well correlated.

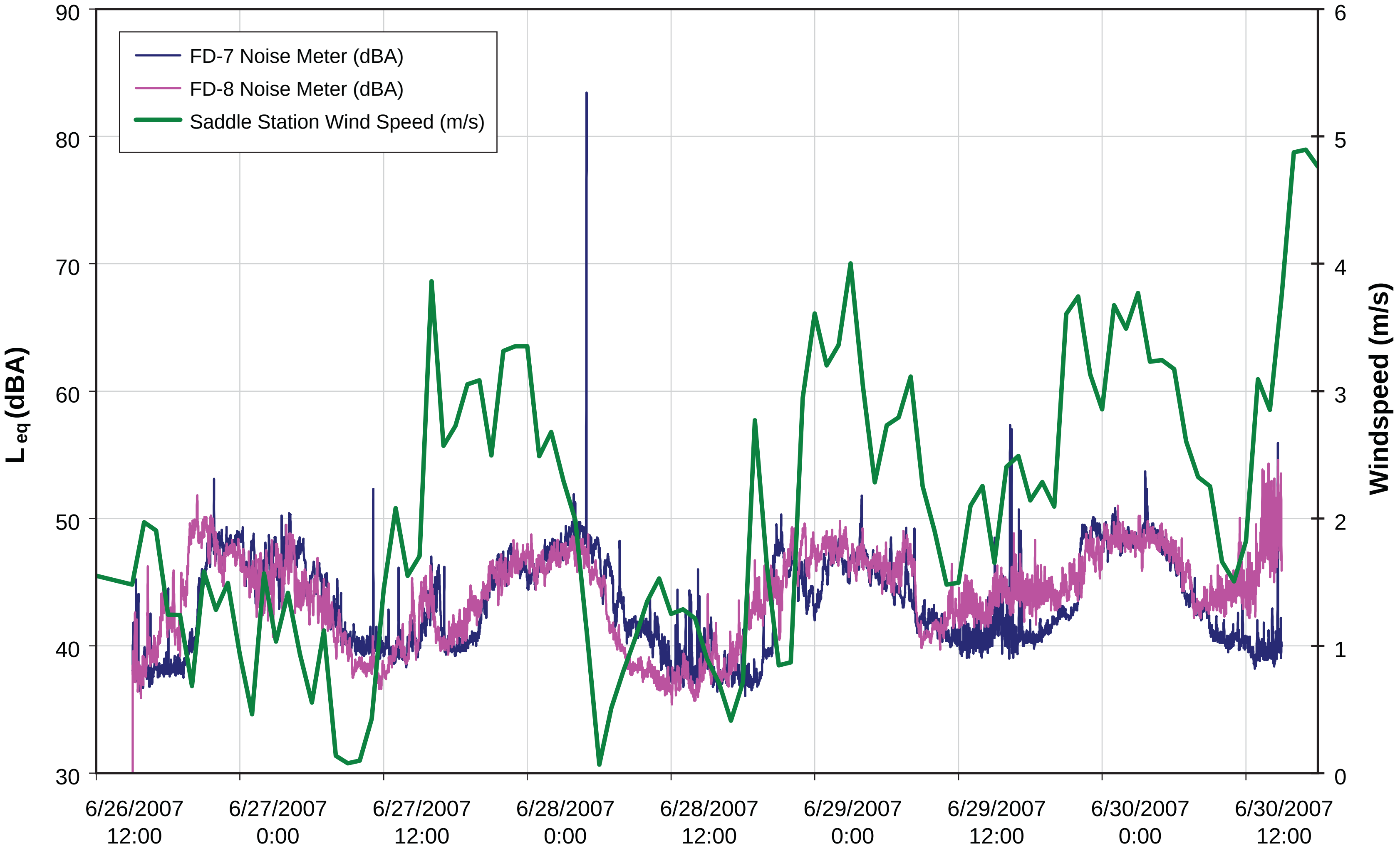
The wind speeds observed at the Saddle Station increased during the nights throughout the study periods, which is consistent with the trend of increasing night-time noise. Noise fluctuations, with lows throughout the day and elevated noise levels at night, can therefore be attributed to effects associated with increased wind speeds in the area. The average hourly observed wind speeds of the Saddle Station during these study periods were 2.0 m/s and 2.3 m/s (June 26th to June 30th and July 14th to July 18th, respectively) and are representative of the average annual wind speed of 2.4 m/s observed at the Saddle Station in 2007.

Figure 3-2 shows that the noise level at station FD-4 was consistently higher than noise levels at FD-5. Station FD-4 was located approximately 3 km closer to the camp than station FD-5 (9.7

km vs. 12.8 km). However, given the distance and the presence of topographical sound barriers between the noise monitoring stations (mountain ridges and hills) it is very unlikely that noise from the exploration camp (drilling and other activities) would have influenced the noise measurements at either of the stations. The differences in noise levels were more likely associated with differences in wind exposure. FD-4 is situated on a rocky, relatively barren fluvial fan while FD-5 is situated in a heavily vegetated wetland area. These ground cover difference would likely affect the local noise levels.

Although it is likely that helicopters were audible at the sample stations during the monitoring period the duration of helicopter noise would have been short and restricted to day-light hours. Figures 3-1 and 3-2 show that night-time noise levels were generally higher than day-time noise levels. Therefore, helicopter noise is unlikely to have significantly influenced the baseline noise measurements.

Effects of precipitation on the noise levels during the study periods were examined. During a rain event on June 29, 2007 the noise levels at FD-7 and FD-8 were elevated slightly. However, a general correlation between noise levels and precipitation was not noted during the study periods.



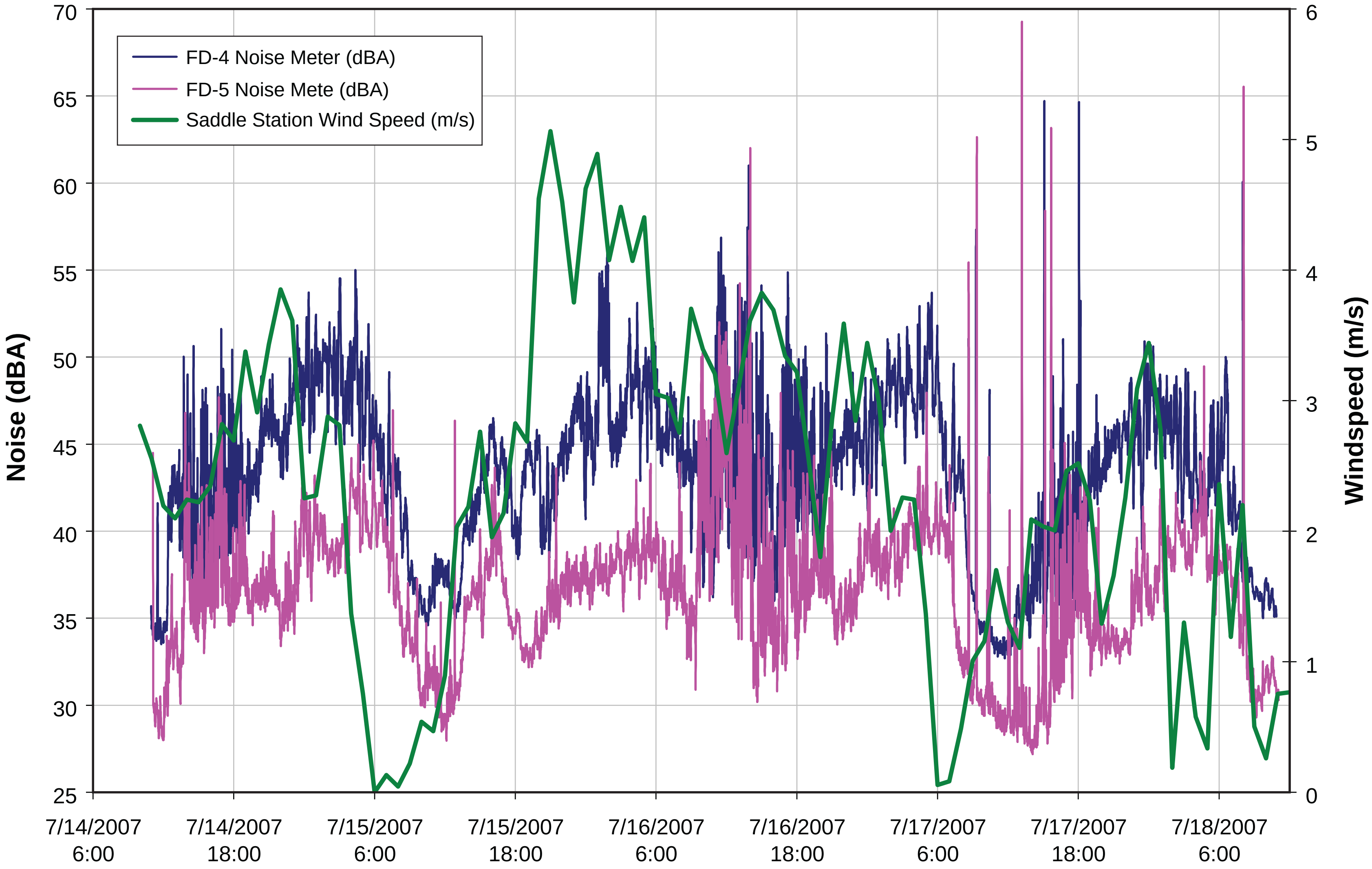
copper FOX metals inc.

Noise Levels Of Stations FD-7 And FD-8

FIGURE 3-1

RTEC Keepers of the Land

Rescan™



copper FOX metals inc.

FIGURE 3-2

Noise Levels Of Stations FD-4 And FD-5

RTEC Keepers of the Land

Rescan™

4. SUMMARY

4. Summary

Noise baseline measurements were completed at 4 sampling locations in June and July of 2007, using two Quest Technologies 2900 Type 2 sound level meters. Sampling was carried out during two study periods from June 26th to June 30th at two locations in the Mess Creek Valley (FD-7 and FD-8), and from July 14th to July 18th at two locations north of the Schaft Creek Camp in the Schaft Creek Valley (FD-4 and FD-5). The observed 4 day L_{eq} values were 48.2 and 45.2 dBA at stations FD-7 and FD-8, respectively. The 4 day L_{eq} values at stations FD-4 and FD-5 were 45.6 and 40.0 dBA, respectively.

Wind speed was deemed to have the greatest effect on baseline noise levels at the noise monitoring stations during the study periods. Helicopter noise and exploration camp activities did not likely influence the baseline noise measurements.

REFERENCES

References

Alberta EUB. 2007. *Directive 038 – Noise Control.* Calgary, AB: Revised edition. February 16, 2007.

Copper Fox Metals Inc. (Copper Fox). 2008. *Schaft Creek Project Description.* Prepared by Copper Fox Metals Inc. January 2008. www.copperfoxmetals.com

Rescan. 2006. *Appendix 6-A Galore Creek Meteorology, Air Quality and Noise Baseline Studies Report.* Prepared for NovaGold Canada Inc. by Rescan Environmental Services Ltd.