2007 Assessment Report

A Technical Drilling Program on the

ReMac Zinc Project

64 Mineral Claims

located in the

Nelson Mining Division

British Columbia

NTS 82F3/W & 82F4/E

49°01' North Latitude, 117°24' West Longitude

BC Geological Survey
Assessment Report
30001

Owner and operator:

ReMac Zinc Development Corp.

Work Performed by:

Mineral Development Advisory Group Inc.

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Submitted:

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SUMMARY

The ReMac property consists of 64 contiguous mineral claims covering approximately 4262.66 hectares and comprises several properties owned or held under option by ReMac Zinc Development Corp. It is located in the heart of a prolific mining district with a long history of base metal sulphide production. The claims cover most of the old production areas of the Reeves MacDonald sulphide mine and adjoining Annex property, which produced a total of 7.25 million tons of zinc-lead sulphide ore from 1949 to 1977 with grades of 3.5% zinc, 1.39% lead and 8 g/t silver.

The property is located 25 kilometres southeast of Trail, BC. This area is gifted with an extensive infrastructure network including an extensive transportation hub, local heavy industry services, major electrical power dams located just outside the perimeter of the property and the Teck-Cominco zinc smelter located in Trail.

Zinc-lead mineralization on the ReMac property occurs in a series of deposits hosted within the Reeves Limestone over a distance of four kilometres, referred to as the Reeves-Redbird corridor. The zones, as demonstrated at the previously mined Reeves Zone, are elongated lenses measuring up to 1000 metres down plunge, 100-200 metres along strike and 5-25 metres in width. Historic mining records indicate extraordinary continuity and grade over these dimensions. There are four and possibly five known zones of mineralization, all striking easterly, dipping south at 50° to 60° and plunging to the west at 45° to 60°. The zones are offset by east-dipping normal faults which bring the faulted extensions closer to the surface and produce a series of distinct zinc deposits. The sulphide deposits consist of laminations and lenses of pyrite, sphalerite and galena and are structurally conformable and stratabound. They often contain a high grade central core which feathers out along strike. The upper portions of most of the zinc zones have been oxidized, and there is potential to develop an oxide zinc resource. To this end, early-stage metallurgical work was conducted at the Lakefield laboratory in 2007 on oxide zinc material which indicated that a potentially viable extraction process can be developed for the oxide.

The 2007 drilling program has been encouraging, with the main target, the Reeves Limestone, being intersected as predicted and proving an on-strike extension of the mineralization bearing limestone unit several kilometres to the west of the current known zones. This essentially doubles the previously known strike length of the Reeves Limestone on the property, and substantially increases the property's ore hosting potential. Along with increasing the length of the potential zone, the drilling program encountered mineralization similar to that found at the Reeves MacDonald mine. The widest intersection of the higher-grade material is 7% zinc over 2 metres, as noted in Hole 07-12 (459.9 to 461.9m). Importantly, this was found within a 58

metre wide zone of 0.6% zinc mineralization occurring in a zone of dolomite alteration within the Reeves Limestone, which was the ore host on the Reeves MacDonald property.

A baseline data collection program at the site has been started to support the permitting requirements for future mine development. Work to date has included fish and fish habitat assessment, hydrology and water quality studies.

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1.0 INTRODUCTION

The ReMac project is located approximately 25 kilometres southeast of Trail, BC, in the heart of a prolific mining district with a long history of base metal production. The property encompasses most of the area located between a loop in the Pend d'Oreille River and the Canada-USA border (Figure 1). The property is easily accessed by paved highway from Trail, with gravel logging roads providing good access within the claim group. The property is owned and operated by ReMac Zinc Development Corp. of Vancouver, BC.

The ReMac project includes the site of the past producing Reeves MacDonald zinc-lead-silver sulphide mine (7.25 million tons produced), which operated for 25 years before closing in 1975. Zinc mineralization at Reeves MacDonald occurs in a series of large, steeply plunging chimneys hosting zinc oxide and sulphide zones which are believed to be continuous. The Reeves MacDonald ore zones have been structurally repeated by faulting several times to the west. The purpose of the 2007 drilling program was to confirm this extension of mineralized and prospective Reeves limestone along the ReMac property and to provide target areas for further exploration. The drilling program succeeded in confirming this extension along strike.

The 2007 drilling program consisted of a total of 6189.6 metres of HQ and NQ drilling. Drilling was performed on 3 cell claims in total. Detailed air photographs were produced of the property, and a new topographic base map was produced. Baseline studies were undertaken to monitor water, and metallurgical work was completed on a bulk sample of the Redbird oxide to determine zinc recovery. A semi-permanent wooden-structure camp was constructed on the property during the 2007 exploration program.

2.0 PROPERTY LOCATION, OWNERSHIP AND DESCRIPTION

2.1 PROPERTY LOCATION

The ReMac property is located in the Nelson Mining Division of southeastern British Columbia (Figure 1), approximately 400 kilometres due east of Vancouver. It is situated 25 kilometres southeast of Teck Cominco's lead-zinc smelter complex in Trail, BC, and 15 kilometres north of Teck Cominco's Pend d'Oreille zinc mine and concentrator at Metalline Falls, in Washington, USA. The Canada-US border marks the southern property boundary of the claims.

2.2 PROPERTY OWNERSHIP HISTORY

After the Reeves-MacDonald mine shut down in 1975, Golden Eye Minerals Ltd. of Vancouver, BC, revisited the property, initially seeking to develop the oxide ores which remained. In 1985, the company staked several mineral claims, optioned the NOR claims and leased the Redbird Mineral Crown Grants. In 1991, Golden Eye Minerals Ltd. changed its name to Annex Exploration Corp. In 1993, Annex Exploration Corp. purchased the Redbird Mineral Crown Grants from Acadia Mineral Ventures Limited, a subsidiary of Hecla Mining Company.

Figure 1: Location Map

In 1994, the company changed its name to Redhawk Resources Inc. The Reeves Mineral Crown Grants were optioned in 1999. The option expired, and Redhawk initiated another option to purchase the property in 2000. On December 15, 2006, Redhawk sold (for shares) the ReMac Zinc project to its wholly owned subsidiary, ReMac Zinc Corp., a private company. OMC Capital Corp., a capital pool company, purchased ReMac Zinc Corp. from Redhawk through an exchange of shares on June 4, 2007. ReMac Zinc Corp. amalgamated with a BC numbered company, changed its name to ReMac Zinc Development Corp. and became a wholly owned subsidiary of OMC. OMC simultaneously changed its name to ReMac Zinc Corp. As a result, ReMac Zinc Development Corp., the owner of the ReMac Zinc project, became a wholly owned subsidiary of ReMac Zinc Corp.

ReMac Zinc Corp. became a Tier 2 Issuer, and started trading on the TSX on June 5, 2007 under the symbol RMZ.

2.3 Property Description

The ReMac property is an amalgamation of several types of claims with a various ownerships (Figure 2). ReMac Zinc Development Corp is the registered owner of 8 mineral cell claims and 32 Crown granted mineral claims covering a total of 3943.82 hectares. The company also holds an option to purchase 24 Crown granted mineral claims covering 318.84 Ha as well the surface rights of 35 Crown grants and fee simple surface lots consisting of 293.40 Ha covering essentially the same area (Table 2). This package, referred to as the Reeves Option, covers most of the old production areas of the Reeves MacDonald sulphide mine and adjoining Annex property, which produced a total of 7.25 million tons of zinc-lead sulphide ore from 1949 to 1977 with grades of 3.5% zinc, 1.39% lead and 8 g/t silver.

The Ministry of Energy, Mines and Petroleum Reserves defines a Crown granted mineral claim as a tenure administered under the Land Act which was originally a staked mineral claim that was subsequently surveyed and issued as a Crown granted tenure. The last Crown granted mineral claims were issued in 1957. The Crown grant is maintained by payment of an annual assessed mineral tax. It is important to note that Crown granted mineral claims are not within the jurisdiction of the Mineral Tenure Act.

The only method of acquiring new mineral rights in British Columbia today requires the registration of a cell claim over the land. A claim is the exploration and development tenure, and a recorded holder may convert a claim to a lease in order to carry out production.

The ReMac Zinc property is an amalgamation of three entities, which can be divided into 4 groups based on ownership and royalties. The 8 cell claims (converted in June 20, 2005) comprising the western portion of the property and the 32 historical Redbird Mineral Crown Grants, covering a total of 3943.82 hectares, are 100% owned by ReMac Zinc Development Corp. Some of these claims are subject to production royalties. The eastern historical Reeves Mineral Crown Grants are held under an Option to Purchase agreement with Reeves MacDonald Mines, and consist of approximately 318.84 hectares of Mineral Crown Grants. The

Option to Purchase agreement also provides 293.4 hectares of fee simple and crown granted surface rights for possible mill and tailings disposal areas, covering essentially the same area as that covered by the Reeves Mineral Crown Grants. Details of the various agreements are outlined below:

Group 1: Cell Claims

The 8 mineral cell claims in this group are all 100% owned by ReMac Zinc Development Corp. No further payments are due for any of the claims, nor are they subject to any royalties or other payments to third parties.

> Group 1a: The former TIC 1 & 3 legacy claims (1122.81Ha) were originally staked in 1985 by Golden Eye Minerals Ltd. They were converted to cell claims 514860 and 514862 in 2005.
>
> Group 1b: The former TIC 2 & 4 legacy claims (826.10 Ha) were staked by Redhawk Resources in 1998. They were converted to cell claims 361385 & 361386 in 2005.
>
> Group 1c: The RIV 1 & 2 claims (804.80 Ha) were staked in February, 2007 by ReMac Zinc Development Corp. and are owned outright.

Group 2: Cell Claims

The NOR 2 and NOR 3 modified grid claims were originally staked by G.H. Klein in July, 1981. Golden Eye Minerals Ltd. first optioned the claims from Klein in 1985 and Redhawk Resources Inc. purchased the claims from G.H. Klein in November, 1995. The claims were converted to internet cell claims (514866 and 514867) in 2005 (656.88 Ha). Production within the agreed original claim boundaries is subject to a 2% NSR production royalty payable to Klein. Under this agreement, 75% of this royalty (1.5% NSR) can be purchased at any time for Cdn$1.5 million and ReMac Zinc Development Corp. retains the right of first refusal to purchase the remaining 0.5% NSR.

Group 3: Redbird Group

Golden Eye Minerals Ltd. leased the Redbird group of 32 full and fractional Mineral Crown Grants (total 533.23 hectares) from Diem Mines Ltd., a Canadian subsidiary of the Hecla Mining Company of Wallace, Idaho, in May, 1985. Annex Exploration Corp. purchased the Redbird property outright from Acadia Mineral Ventures Limited, a successor to Diem Mines Ltd. on April 22, 1993. The claims are subject to a 2.5% NSR production royalty to a maximum of US$1 million. Taxes of $1.25 / hectare are due on July 2nd of each year.

Group 4: Reeves Option

In November, 1999, Redhawk Resources entered into an Option to Purchase the Reeves property from Reeves MacDonald Mines Limited, but it was not exercised and allowed to expire. In 2000, Redhawk Resources Inc. acquired a four year Option to Purchase a 100% interest in the Reeves property, consisting of 24 full and fractional Mineral Crown Grants and

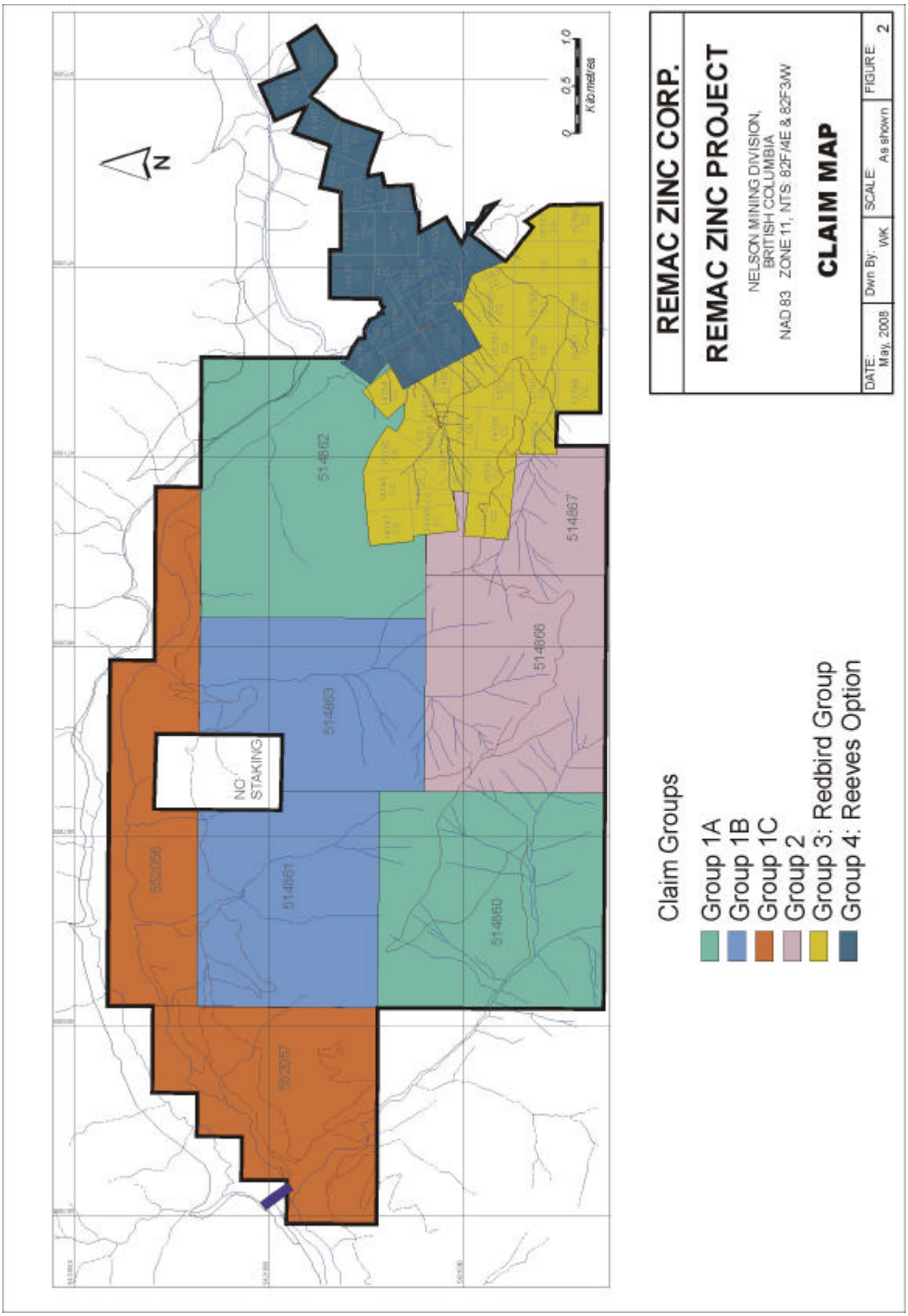


Figure 2: Claim Map

the BC Hydro Agreement Rights. Included in this deal are surface rights to approximately 293.4 hectares for possible mill and tailing disposal areas, covering essentially the same ground as the Mineral Crown Grants. The original agreement has been amended several times, pushing the Excise Date ahead by means of cash payments which total $565,000 to date. The outstanding terms of the Option to Purchase agreement are as follows:

1. The Excise Date has been extended to February 15, 2009.
2. No further payments are due on the property by ReMac Zinc Development Corp. until this date.
3. Applicable yearly taxes owing on the Mineral Crown Grants are to be paid by Reeves MacDonald Mines Ltd.
4. ReMac may purchase the Reeves property on or before this date for a payment of US$2,900,000

All claims and mineral crown grants owned or otherwise held by ReMac Zinc Development Corp. are currently in good standing.

TABLE 1a: Group 1 Modified Cell Claims

Group 1: Modified Cell Claim Tenures

Group	Tenure #	Name	Type	Date Staked	Converted From	Good To Date	Area (Ha)	Units
1a	514860		Cell	Jun-85	TIC 1	2013/may/24	529.728	21.189
1a	514862		Cell	Jun-85	TIC 3	2013/may/24	593.081	23.723
							1122.809	
1b	514861		Cell	Feb-98	TIC 2	2013/may/24	423.632	16.945
1b	514863		Cell	Feb-98	TIC 4	2013/may/24	402.466	16.099
							826.098	
1c	552056	RIV 1	Cell	07-Feb		2013/feb/15	402.354	16.094
1c	552057	RIV 2	Cell	07-Feb		2013/feb/15	402.449	16.098
							804.803	
2	514866		Cell	Jul-81	NOR 2	2013/may/24	423.796	16.952
2	514867		Cell	Jul-81	NOR 3	2013/may/24	233.088	9.324
							656.884	
						Total:	**3410.594**	**136.424**

TABLE 1b: Redbird Mineral Crown Grants

Group 3: Redbird

Claim Name	Hectares	District Lot #	Claim Name	Hectares	District Lot #
Lead Pot	15.11	13465	Caviar No. 1	20.03	15786
Lead Cup	12.84	13466	Caviar No. 2	19.73	15787
Royal	14.66	13469	Caviar No. 3	20.15	15788
Edna	11.13	13471	Caviar No. 4	20.72	15789
Annie	8.60	13472	Caviar No. 5	20.56	15790
McGee	20.78	13473	Caviar No. 6 Fr	17.85	15791
Gertrude Fr	6.60	14081	Caviar No. 7 Fr	8.23	15792
No. 1	16.07	14147	Val No. 1	19.89	15794
Red Top	18.97	14148	Val No. 2	19.73	15795
No. 2	13.20	14149	Val No. 3	19.76	15796
Red Mtn.	11.26	14150	Val No. 4 Fr	14.90	15797
Ruth	20.90	14153	Val No. 5	20.61	15798
Homestake No. 2	13.35	14154	Val No. 6 Fr	19.86	15799
Royal Fr	20.78	14155	Val No. 7 Fr	18.90	15800
Tough Going Fr	18.57	15030	Val No. 8 Fr	12.59	15801
Tough Nut Fr	20.90	15031	Larch No. 3 Fr	16.00	15804
			Total:	**533.23**	

TABLE 1c: Reeves Mineral Crown Grants and Surface Rights

Mineral Crown Grants (24)

Lot Name	Hectares	District Lot #	Lot Name	Hectares	District Lot #
Drumlumin	3.21	12076	RM	20.90	14435
Juliette	16.56	13463	RM1	16.47	14436
Gertrude	20.80	13464	RM2	10.13	14437
Dreadnaught	11.29	14034	RM3	20.90	14438
Tunnel Fraction	1.02	14035	Highland	14.01	12323
River	6.90	14036	Empire	2.41	13462
River No, 1	9.14	14061	Blue Bell	8.19	14032
River Fraction	15.12	14062	International Lead No. 1	17.27	12692
Annex No. 2 Fraction	10.76	14069	Salmon Fraction	13.93	14045
Annex No. 1	20.83	14070	Riverside	17.34	14049
Drumlumin Fraction	12.93	14074	V.B. Fraction	19.78	13995
A Fraction	17.16	14400	International Lead No. 2	11.79	12492
			Total:	**318.84**	

Surface Rights (35)

Lot Name	PID	District Lot #	Lot Name	PID	District Lot #
Gertrude MC	016-497-228	13464	Fee Simple Lot	016-520-530	Lot 19 Plan 971
Drumlumin Fraction	016-497-309	14074	Fee Simple Lot	016-520-548	Lot 20 Plan 971
Annex No. 1	016-497-261	14070	Fee Simple Lot	016-520-581	Lot 25 Plan 971

Lot Name	PID	District Lot #	Lot Name	PID	District Lot #
Annex No. 2	016-497-252	14069	Fee Simple Lot	016-520-556	Lot 21 Plan 971
River Fraction	016-497-350	14062	Fee Simple Lot	016-520-564	Lot 22 Plan 971
River No. 1	016-497-325	14061	Fee Simple Lot	016-520-572	Lot 23 Plan 971
River M.C.	016-497-244	14036	Fee Simple Lot	015-960-927	Lot A Plan 971
Juliette	016-497-295	13463	Fee Simple Lot	015-960-935	Lot B Plan 971
Fee Simple Lot	015-960-251	Parcel A, Lot 13 Plan 971	Fee Simple Lot	023-687-444	Lot 1 D.L. 8231 Plan NEP 23728
Fee Simple Lot	015-960-242	Lot 14 Plan 971	International Lead No. 1	016-497-571	12692
Fee Simple Lot	016-520-246	Lot 3 Plan 971	Salmon Fraction	016-497-546	14045
Fee Simple Lot	016-520-262	Lot 4 Plan 971	Riverside	016-497-848	14049
Fee Simple Lot	016-520-297	Lot 6 Plan 971	V.B. Fraction	016-497-945	13995
Fee Simple Lot	016-520-424	Lot 13, except parcel A Plan 971	International Lead No. 2	016-497-503	12492
Fee Simple Lot	016-520-441	Lot 14 Plan 971	Fee Simple Lot	016-520-181	Lot 1 Plan 971
Fee Simple Lot	016-520-475	Lot 15 Plan 971	Fee Simple Lot	016-520-220	Lot 2 Plan 971
Fee Simple Lot	016-520-483	Lot 16 Plan 971	Fee Simple Lot	016-520-271	Lot 5 Plan 971
Fee Simple Lot	016-520-505	Lot 17 Plan 971		**Total:**	**293.4 Ha**

3.0 ACCESSIBILITY, CLIMATE AND PHYSIOGRAPHY

3.1 ACCESS

The ReMac Zinc Project is easily accessible. From Trail, Highway 22A connects with the Pend d'Oreille River road, a 13 kilometre paved road to BC Hydro's Seven Mile Dam. The property essentially begins immediately east of the dam. Once across the dam, the exploration camp is gained via a 15 kilometre well maintained gravel logging road. Permission is now required by BC Hydro for access to travel across the dam. A criminal background check from the RCMP is first required, and then an electronic gate opener is provided upon application.

Access to the Reeves Mineral Crown Grants to the northeast of the Pend d'Oreille River is provided by a well maintained 11 km gravel road that runs along the north shore of the river continuing past the dam and connecting with the former Reeves MacDonald Mine road.

During the main production period at the mine, a bridge crossing was established across the Pend d'Oreille River immediately upstream from the mill, providing a connection between the

east and west parts of the property. The bridge span has since been removed but the substantial concrete pylons, which remain in excellent condition, are still in place. Under an agreement with BC Hydro, this bridge can be re-established if the piers are raised an additional 1.37 metres to mitigate any problems with high water events. Future major property development of the oxide zone would warrant re-establishment of this crossing.

3.2 CLIMATE

The climate of the region is typical of south-central British Columbia with hot, dry summers (June to August) and mild winters (November to April). Winter temperatures hover around the freezing level and rarely drop to -20°C for short periods, while summer temperatures approach highs of 40°C. Annual precipitation is light at 60-75 centimetres and is evenly distributed throughout the year. Snow accumulations at higher elevations typically range up to depths of one meter.

3.3 PHYSIOGRAPHY

The ReMac property is marked by rounded mountains with steep slopes and deeply incised drainage valleys. Elevations range from 545 metres to 1585 metres. The northern boundary of the property is roughly defined by the Pend d'Oreille River, and the southern limit of the property is defined by the Canada – US border.

Much of the property is covered by variably thick glacial deposits of till and kame terraces. Thick fluvial gravel deposits cover Pend d'Oreille River valley bottom. Outcrop exposures are mainly limited to local instances in drainages and along some steep hillsides. Most of the property is heavily forested although much of this is second growth semi-mature pine, fir, cedar, hemlock and larch. Parts of the property have been logged, especially in the vicinity of the former Reeves MacDonald Mine surface facilities. A large fire swept through the area during the 2007 work season, significantly opening up much of the western half of the property. Logging operations on the burned areas were conducted during the winter of 2007 - 2008. The clearing operations and road building for the logging has opened up a significant portion of the property to easy access.

4.0 INFRASTRUCTURE

The ReMac property is well located with respect to roads, electrical power and other infrastructure. Road access connects the property to the nearby communities of Trail, Castlegar, Salmo and Nelson where both general and major supplies and services can easily be obtained.

The Trail airport offers frequent scheduled prop-airline service from Vancouver. Jet aircraft service is available in Castlegar, approximately 30 kilometres north of Trail.

Adequate water supply for normal milling purposes is available from the Pend d'Oreille River, which transects the central portion of the property and roughly forms the northern and western perimeters of the property. The region is a major producer of hydro-electrical power, and three electrical power dams are located on the Pend d'Oreille River in close proximity to the property. Seattle City Light's Boundary Dam is located immediately across the border where the Pend d'Oreille enters the property. BC Hydro's Seven Mile Dam is located on the western boundary of the property, and Tech Cominco's Waneta Dam is located 8.5 kilometres southwest of the property just before the river re-enters the USA. Several high voltage power lines from the Boundary Dam pass over the eastern part of the property.

International markets are easily accessible for potential ore produced on the ReMac Zinc property. The network is well established as shipments of ore are regularly transported to the Trail smelter from ocean freighters via the Burlington Northern Railway.

In 1975, when the Reeves MacDonald Mine closed, a new tailing dam had just been completed on the property. This tailings dam is almost empty and may provide a ready option for tailings disposal in potential future production plans.

5.0 PROPERTY HISTORY

The earliest recorded instance of mining activity in the area goes back to 1865 when men of the Hudson's Bay Company attempted to recover gold from the Salmo River near its junction with the Pend d'Oreille River (Walker, 1934). Subsequent placer mining on the Pend d'Orielle River in 1886 attracted attention to the area. The 1890 discovery of copper-gold at Red Mountain (Rossland) led to the construction of a smelter in Trail in 1895. The first lead ore in the district was mined in 1906 at the Emerald mine, approximately 14 kilometres northeast of the property, and the purchase of the Sullivan mine in 1910 shifted the focus of the smelter to lead-zinc ores.

In 1955, J.T. Fyles and C.G. Hewitt of the Geological Survey of Canada mapped the geology and mineral deposits of the region, a work which today continues to be regarded as the best reference of the area.

Most of the Mineral Crown Grant claims which make up the eastern portion of the property were staked from 1910-1934. The Reeves MacDonald mine began production in 1949, and the Annex mine began operating in 1970. Mining operations ended in 1975, partially due to the introduction of a high royalty on mining by the provincial government.

Work on the property since the closure of the mine is described below. A complete chronological summary account of the history of the property history is found in Appendix III.

5.1 Reeves MacDonald-Annex Property History

This operation was the second largest producer of zinc-lead-silver along the productive Kootenay Arc belt. The original claims were staked between 1910 and 1912 and the initial development work was carried out in 1925. By 1929, the Point, Reeves, MacDonald, O'Donnell and Prospect ore bodies had been explored and the B.L. and Norcross showings had been discovered.

Major mine construction commenced in 1947 and a 500 tons per day flotation mill was constructed in 1949. Mill capacity was expanded to 900 tons per day in 1950. Operations were suspended in July 1953 but were re-opened in late 1955. By mid-1971, the known reserves on the east side of the river were largely depleted but production continued from the Annex Mine, which was developed in 1969 to exploit the newly discovered Annex zones across the river. On the east side of the river, the mineral deposits were developed underground by a series of adits, raises, and internal shafts through a vertical range of 1000 metres. On the west side, the Annex zones were accessed by an adit and internal shaft and mined over a vertical height of approximately 185 metres. A combination of low metal prices, property boundary constraints, and increasing provincial taxation forced final closure of the operation in March 1975.

Total production of the Reeves group is summarized in Table 2, below:

TABLE 2: Historic Production Figures, Recovered Grades

	Period	Tons	%Zn	%Pb	%Cd	opt Ag
Reeves MacDonald	1949-71	6,413,058	3.5	1.39	0.02	0.1
Annex	1970-75	841,410	5.59	0.93	0.06	1.3
Total:		7,254,468	3.74	1.33	0.03	0.24

In 2000, Redhawk Resources Inc. completed an option to purchase the Reeves MacDonald property. Redhawk also signed an option agreement with ZincOx Resources of London, England, in which ZincOx could earn up to a 50% interest in the oxides project contained within the Reeves MacDonald and the Redbird properties. A large drilling and trenching program was completed on the oxide zone in 2000 (discussed in detail below in *Redhawk Resources, 2000*).

No further work has been completed on the Reeves MacDonald property since this program.

5.2 Redhawk Property Group History

Early Property History, 1924 to 1975

The Redbird Group claims were staked prior to 1924 by S. Coulter and A.J. Campbell of Ymir to cover several surface exposed earthy gossan zones along strike with the Reeves MacDonald property immediately to the west. From 1924 to 1929, exploration was conducted by various owners including the Red Bird Mining Company and Boundary Basin Mines Ltd. Workings,

consisting of three adits, a shallow shaft and several open cuts were completed along with some diamond drill holes from 1927 to 1929. There is no record of work being done on the property between 1929 and 1944. Hecla Mining Company of Wallace, Idaho purchased the property in 1944. In 1947, geological mapping and a small amount of surface work was done on the claims by Diem Mines Ltd., a wholly owned Canadian subsidiary of Hecla. In 1955, Fyles and Hewett mapped the area, but the adits had caved in by this time. Hecla conducted further geological mapping, trenching, diamond drilling and sampling on the property up to 1960. In 1961, the property was leased to The Consolidated Mining and Smelting Company of Canada (Cominco). Cominco investigated the main Redbird showing from 1961 to 1962 by extending the 2650 level adit an additional 800 feet (244 metres) and by drilling an additional 12 diamond drill holes (1250 metres). Strong and apparently continuous oxidized zinc-lead mineralization was encountered, with one 600 foot (183 metre) length along the drift reportedly averaging 18.5% Zn and 6.5% Pb over an estimated 20 foot (6 metre) average width. No sulphides were encountered however, and the property was returned to Hecla Mining.

In 1973 and 1974, Reeves MacDonald Mines, under contract with Hecla, advanced the lowest level drift (the 800 level) from the Annex Mine westward some 700 feet (213 metres) on to the Redbird property. From this heading, 15 diamond drill holes totalling 6200 feet (1890 metres) were completed. The purpose of this program was to find the faulted offset sulphide zone. Four of these holes intersected four separate bands of zinc mineralization, each 6.5 metres wide, averaging 4.18% Zn, 0.12% Pb, 0.56 opt Ag and 0.04% Cd, grades comparable to ore being mined by Reeves MacDonald. The companies were unable to negotiate a suitable business arrangement and no further development was carried out prior to the Annex Mine closure in 1975.

Golden Eye Minerals Ltd., 1985 to 1989

In 1985, Golden Eye Minerals Ltd. staked the TIC claims and optioned the NOR claims from G.H Klein. Adding to this package, they acquired the adjoining Redbird property under a lease agreement with Diem Mines Ltd. (a Canadian subsidiary of Hecla Mining Company of Wallace, Idaho). Teck Corporation optioned the property from Golden Eye during 1985 to 1986 and completed six surface diamond drill holes (2691 metres) to test the down dip extension of the Redbird showing. Due to drilling difficulties, three of the drill holes were abandoned. Hole 86-3 encountered unexpected zinc mineralization in an overlying formation and Hole 86-5 encountered highly oxidized mineralization with very poor core recovery from the anticipated target at a vertical depth of 1,500 feet (457 metres) below surface (Betmanis, 1986).

Between 1986 and 1988, Golden Eye Mineral Ltd. drilled an additional eight surface diamond drill holes totalling 16,122 feet (4914 metres) to test the down plunge continuity of the Redbird zone. The faulted offsets of the Annex-Annex West zones from the adjacent Reeves property were also tested. Continuity of depth was confirmed by the occurrence of significant ore grade intercepts in several of the drill holes.

Golden Eye Minerals Ltd. changed its name to Annex Exploration Corp. in January, 1991.

Annex Exploration Corp., 1991 to 1994

Annex Exploration Corp. carried out a program of exploration in 1991 including reconnaissance soil and silt sampling, geological mapping, a bulk sampling program on the oxidized Redbird deposit, a mineralogical study of the oxidized material by J. Harris, Ph.D., and technical research by BC Research and by Fluor Daniel Wright, consulting Engineers, into the feasibility of leaching and solvent extraction of leachable zinc from the oxides material exposed at surface above the Redbird workings.

Analysis of the 100 kilogram bulk sample of limonite from the Beer Bottle showing identified the sample as 2% carbonate, 40% limonite, and 58% hemimorphite (a hydrated zinc silicate containing 67.5% Zn). A brief test program carried out at B.C. Research reported the material is easily reduced to a fine pulp and the zinc silicate was readily soluble in dilute sulphuric acid with recoveries of over 80% at pH 2 or over 97% at pH 3.

In 1991, Annex also commissioned a study by Fluor Daniel Wright of a "Cost Estimate to Re-Access the Annex Mine and Perform Underground Exploration on the Redbird Property" (Wortman, 1991). Annex also commissioned a review of previous exploration programs, their results and implications for further work on the Redbird property by D.S. Jennings, Ph.D. in 1991. This report discusses several exploration and development strategies for the Redbird property (Jennings, 1991).

In 1993 Annex Exploration Corp. purchased the Redbird property from Acadia Mines Ltd. (the successor to Diem Mines Ltd.).

Annex Exploration changed its name to Redhawk Resources in March, 1994.

Redhawk Resources Inc., 1994 to 1999

A limited program was conducted by Redhawk on the property in 1998 to test the surface oxide showings by trenching and also to attempt directional drilling methods to locate the core of the Annex mineralization. Results from the trenching of the Beer Bottle zone gave a footwall section grading 21.93% Zn, 3.11% Pb and 0.74 opt Ag over an estimated true thickness of 6.6 metres and overlying hanging wall intersection of 5.27% Zn, 1.82% Pb and 0.10 opt Ag over an estimated true thickness of 6.3 metres.

The 1998 drilling program completed 1,467 metres of HQ and NQ core drilling in one new hole (98-1), as well as two directional cuts: one from previously drilled hole 87-1 (87-1A), and one from the new hole (98-1A). Drillhole 87-1 was re-entered and then cut by directional drilling from a wedge at 743 metres down, with the target being the centre of the projected Annex zone. This drilling resulted in a mineralized intersection within the Reeves Limestone.

The new hole, 98-1 was subsequently drilled in an attempt to get an intersection at a lower elevation in the Annex ore body. This was done using the Annex plunge of 45° for placement of the target. The hole was completed to 1,140 m and intersected 12.93 m of Annex type mineralization in the Reeves Limestone. This intersection, located at approximately 415 metres below the 800 level, is the deepest intersection to date and appears to be in the same fault block as the mineralization on the 800 level exploration drift.

Hole 98-1A was conventionally wedged at 832 m and control drilled, taking advantage of the tendency of the hole to go perpendicular to the rock, hitting the target and intersecting 10.91 metres of 4.75% Zn. Neither 98-1A nor the intersection in 98-1 appeared to be in the main part of the Annex ore body, as extrapolated from mining at the Reeves Mine.

R.D. Westervelt completed a summary review of the project in 1999 concentrating mainly on the oxide zones, and recommended further drilling and exploration to define the extent of the oxide material.

Redhawk Resources Inc., 2000

In March 2000, ZincOx Resources BV entered into an option agreement with Redhawk Resources whereby ZincOx stood to earn a 50% interest in the ReMac Zinc property by spending $3,000,000 on expenditures over 4 years. ZincOx Resources of London, England, is a world leader in technologies for the beneficiation of zinc oxide ores such as that located on the Redbird property.

The 2000 trenching and drilling program was conducted on the oxide zone, which is located situated on both the Redbird and the Reeves groups of claims. The program proved the model of large coherent elongated lozenges of zinc mineralization repeated in a predictable manner by a series of normal faults and confirmed the potential for large zones of zinc oxide mineralization on the property (Gorzynski, 2000). Five oxide zones, referred to as Zones B, C, F, G and H, were selected for the 2000 field program and tested by 21 reverse circulation drill holes. In addition, Zones B and C were tested by trenching. Some exploratory trenching was also carried out on Zone A. After assaying, large samples of each oxide zone were sent to SGS Lakefield for metallurgical study under the direction of ZincOx Resources. A brief summary of each zone is as follows:

Zone A*:* A historically known zone of mineralization, this zone was tested with two trenches. Results suggested a zone of mineralization opening up to the west, perhaps just beyond the edge of the shale cap.

Zone B (Beer Bottle Zone): The Beer Bottle Zone was tested with five trenches and four RC drill holes. This zone trends about 230/45SE and is best exposed in the trench B-2000-01 (the Beer Bottle Cut). It was found that Zone B hosts zinc oxide mineralization of Redbird Zone affinity, being traced in trenches and drill holes over a strike length of 110 metres. The mineralization truncates to the east by the Beer Bottle Creek Fault and remains open to the west through

overburden-covered terrain. A steep east-west fault occurs nearby in the Redbird Creek gully, which may or may not interrupt Zone B to the west and/or at depth (Klein, 1999).

Zone C: This zone has historically been known as the main zone of mineralization on the property. Historic reports from 1927 and 1942 indicate Tunnel No.1 workings total about 470 metres of underground development including a zinc oxide section about 140 metres long with a high grade core about 75 metres long and 6.1 metres or more wide. Based on assays from 18 samples, the average grade is reported as 18.55% Zn, 5.97% Pb and 1.18 opt Ag. On average, the zone trends about 230/60SE. It was found that Zone C hosts zinc oxide mineralization of Redbird Zone affinity and is a down-faulted portion of Zone B offset by the Beer Bottle Creek Fault to the west. It has been traced in trenches and drill holes over a strike length of 70 metres (Hole R-2000-08 to the east end of Trench C-2000-02), being open to the east where the bulk of the zinc oxide mineralization is projected to occur. To the west, the pinching end of the mineralization has been found in Hole R-2000-01. At depth, Zone C remains strong to at least 85 metres below the highest trench (C-2000-01) where it was found in Redbird Tunnel No.1.

High Road Zone: This is a small historic zinc oxide zone located approximately 25 m into the structural footwall of Zone C. It has been tested in three places, returning trench results of 6.04% Zn over 3.5 metres and drill results of 5.62% Zn across 2.7 metres.

Zone F (Reeves): Also known as the Annex mine zone (mined between 1970-75), it was highest grade of the Reeves MacDonald operations. It lies in an area of deep overburden on the lower slopes of Redbird hill. It was found that Zone F hosts zinc oxide mineralization projected up from the high grade Annex Zone. The two drill intersections outline an initial strike length of 50 metres open to both the east and west. At depth, the oxide-sulphide interface is known to be 100-150 metres in elevation below these drill intersections. It was also confirmed that the wide high grade nature of the Annex Zone mineralization projects into the zone of oxidation.

Zone G (Reeves): A poorly understood faulted near-surface segment of the Annex West Zone, it was confirmed that the Zone G oxide mineralization is of Annex West Zone affinity. Annex West has historically been a lower grade zone and the results of the drill holes in the oxidized horizon are consistent with that history. The two drill intersections outline a strike length of 60 metres, remaining open to the west.

Zone H (Reeves): Another poorly understood mineralized section, Zone H also hosts zinc oxide mineralization thought to be of the Annex Zone affinity. This zone, somewhat constrained along strike, most likely continues as depth where grab samples of zinc oxides grading 20-25% Zn were collected from underground workings in the early 1970's.

Zone P (Reeves): This zone is a new zinc oxide discovery located between Zone H and Zone R. It was found in drill hole R-2000-11 and returned two intersections; one near the surface grading 6.68% Zn across 4.4 metres TW and another at depth of 13.25% Zn across 3.5 metres TW. The mineralization is open to the east and at depth. After assaying, large samples of each oxide

zone were sent to SGS Lakefield for metallurgical study under the direction of ZincOx Resources of London, England.

Upon completion of the exploration program in 2000, ZincOx opted to withdraw from the project and the Redbird zone did not undergo further exploration until 2004.

Redhawk Resources, 2004

The main objective of the 2004 program was to test extensions of the Zone A zinc mineralization beyond the main trench exposure on the western part of the ReMac property. A drill program was completed totalling 346.3 metres, consisting of eight BTW-size holes. The main objective of the program was to test the depth and strike extents of the Zone A mineralization. Drilling demonstrated however that Zone A becomes narrow and low grade at shallow depth, and does not have significant tonnage potential. Hole 2004-A4 was a surprise in that it intersected Reeves Formation Limestone at only 44.8 metres. Previous work has suggested that potential for zinc-lead deposits in this western portion of the property lay at great depth, discouraging exploration. The drill results from the 2004 drill program indicate the potential for zinc-lead deposits lies at relatively shallow depths in this area and the presence of mineralization in the fault may indicate a nearby deposit.

Redhawk Resources, 2005-2007

The 2005 program tied onto the Redbird property and stepped out to the west to evaluate the potential for Reeves Limestone to occur along strike and indicate possible new areas of mineralization. For years geologists had postulated the presence of ore-bearing Reeves Limestone to the north of the Redbird zone. The soil sampling and geological mapping program in 2005 was designed to map the stratigraphic and structural relationships along a southwesterly corridor from the previous drilling in Zone A to the headwaters of Harcourt Creek. The soil geochemistry proved successful in extending the possible extent of the ReMac-type mineralization associated with the No. 4 Adit area. Geological mapping also suggests the presence of the Reeves Limestone, the host to the ReMac-type mineralization in this area, with possible extensions to the northwest.

Two additional areas of anomalous soil geochemistry having the same signature as the pathfinder elements for the ReMac-type mineralization of the No.4 Adit area occur in the centre of the Redbird Grid at the headwaters of Harcourt Creek. Both areas appear to be underlain by the Emerald Member of the Laib Formation, the stratigraphic unit that immediately overlies the Reeves Limestone. The cause of these anomalies is interpreted to be hydromorphic leakage related to possible buried ReMac-type mineralization hosted by the Reeves Limestone, which would occur at depth in these regions. Both of these anomalous areas

are quite large measuring in the hundreds of meters with individual values that are significantly anomalous.

Redhawk Resources Inc. contracted Wardrop Engineering Inc. to conduct a comprehensive and independent review of the geology, exploration history and historic estimates based on reports prepared on the ReMac property since 1998 in accordance with the National Instrument 43-101 (NI 43-101).

ReMac Zinc Development Corp., 2000

After the completion of the41-101 report, the ReMac Zinc property was purchased by ReMac Zinc Development Corp. in June, 2007. The 2007 drilling program, discussed in this report, commenced immediately after this transaction.

5.3 Other Areas (Caviar Showing, TIC & NOR claims)

In 1959, four surface drill holes were completed on the Caviar showing, located 150 metres north of the U.S. border. Sulphide mineralization was intersected in two holes with the only significant intersection being 20 feet (6 metres) of 6.6% Zn. The Caviar claims were acquired by Hecla Mining Company circa 1984.

The Consolidated Mining and Smelting Company of Canada (Cominco) explored the BAR group of claims to the west of the Redbird, covering parts of the ground now covered by the TIC 1 and NOR claims. Soil geochemical prospecting and geological mapping were completed in 1950-51 and one deep vertical diamond drill hole was completed to a depth of 390 metres. Although this hole failed to encounter any significant mineralization, it did confirm a faulted segment of the favourable host Reeves limestone beneath the younger cap rocks at a vertical depth of approximately 335 metres. The claims lay dormant until 1981 when G.H. Klein recognized the potential for additional mineralized zones in the Reeves member along strike from the Redbird. The NOR claims were staked to cover this possible extension and repetition of the Reeves MacDonald-Annex type sulphide mineralization beneath the younger cap rocks to the west.

Northgane Minerals Ltd. of Calgary, explored the claims between 1981 to 1984, and completed airborne magnetometer and VLF-EM geophysical surveys over the property. The property was optioned by Annex Exploration Corp. in 1985 to consolidate the land package of the Reeves extension.

A reconnaissance soil and stream sediment sampling program was conducted in 1989 on the NOR claims, outlining a Zn-Ag-Cd anomaly near the head of Harcourt Creek. Subsequent geochemical surveys in 1991 were unsuccessful in defining any cohesive anomalies; however this is most probably due to the extensive and thick overburden cover and argillite cap rocks.

6.0 GEOLOGICAL SETTING

6.1 REGIONAL GEOLOGY

The stratigraphic definitions and relationships for the Salmo lead-zinc district, which includes the ReMac property, largely come from the work of Fyles and Hewitt (1959), from which much of the following information is summarized.

The ReMac Zinc project is located within the southern part of the Kootenay Arc, a north-south trending, curvilinear belt of complexly deformed sedimentary, volcanic, and metamorphic rocks extending some 400 kilometres from Colville, Washington to the vicinity of Revelstoke, B.C. (Figure 3). The Kootenay Arc lies between the Proterozoic Purcell Belt metasediments to the east, and the Shuswap Metamorphic Complex and the Nelson Batholith to the west. These rocks occur as a broadly conformable, thick succession of sediments and volcanics ranging in age from the earliest Cambrian in the east to late Mesozoic in the west.

The ReMac property is underlain by Lower Cambrian micaceous quartzites of the Reno Formation (Figure 4). Massive quartzites of the Quartzite Range Formation in turn represent the footwall to this stratigraphic succession. Overlaying this is the Laib Formation, containing the Truman, Reeves and Emerald members. The Truman Member of the Lower Laib consists of a thin sequence of interbedded phyllites and limestones. The principal zinc-lead deposits in the ReMac region all occur within the Reeves Member of the Lower Cambrian Laib Formation (Figure 4). The Reeves Member mainly consists of fine to medium grained limestone, which has been locally altered to dolostone. This limestone characteristically displays grey, black and white banding typically a few centimetres in width. The dolostone often weathers buff, is poorly banded or massive, and is normally finer grained than the limestone. Large masses of light grey dolostone are exposed in complex folds immediately south of the Salmo River Anticline near the Reves MacDonald mine. Black, vaguely banded dolostone is also exposed in the vicinity of the mine.

The Emerald member overlies the Reeves limestones, and is characterized by a black to grey foliated, carbonaceous, often-crenulated, schist/phyllite unit. Higher up in the Laib Formation is an undivided series of phyllites, with lesser intercalated micaceous quartzites and limestones, which have not been studied in detail and have been collectively lumped as the Upper Laib Formation. It is interesting to speculate as to whether the quartzites could represent the Reno Formation and the limestones the Reeves Member of the Laib Formation.

The Laib Formation is overlain by the Nelway Formation, a second unit of limestones and dolomites that also hosts lead-zinc deposits including TeckCominco's Pend Oreille Mine ore bodies in Washington State. At the Caviar area, to the south of the Reeves MacDonald mine, the Nelway Formation hosts similar Pb-Zn mineralization to the ReMac and Pend D'Oreille

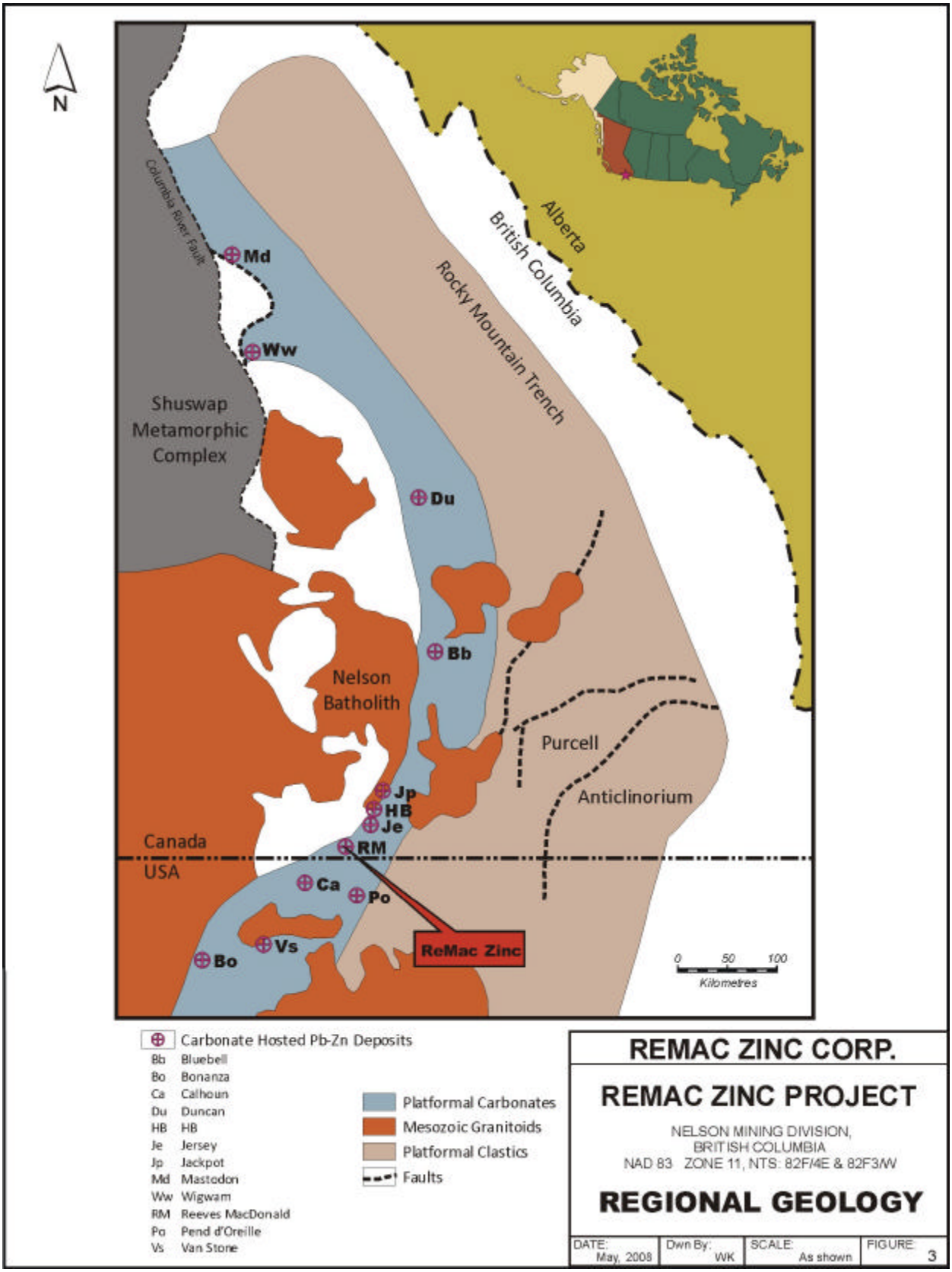


Figure 3: Regional Geology Map

AGE	FORMATION		MEMBER	LITHOLOGY	APPROXIMATE THICKNESS (m)
ORDOVICIAN	ACTIVE			Black shales	Thick
CAMBRIAN	NELWAY			Limestones, Dolostones	Varies
	LAIB	UPPER		Phyllites, Quartzites	Varies
		LOWER	EMERALD	Black Crenulated Phyllites	50-70
			REEVES	Banded Limestones, Dolostones	50-150
			TRUMAN	Green Phyllites, Limestones	20
	RENO			Quartzites	5-10

REMAC ZINC CORP.

REMAC ZINC PROJECT

NELSON MINING DIVISION,
BRITISH COLUMBIA
NAD 83 ZONE 11, NTS: 82F/4E & 82F3/W

STRATIGRAPHIC COLUMN

DATE:	Dwn By:	SCALE:	FIGURE:
May, 2008	WK	As shown	4

Figure 4: Stratigraphic Column

Districts. Due to the size and nature of this zone, it represents more of an interesting anomaly than a serious exploration target at this time.

Black argillite, slate and minor calcareous members of the Ordovician Active Formation overlie the Cambrian rocks. This formation is normally bounded by faults and consequently the stratigraphic relationships of the Active Formation to the younger stratigraphy of the Laib Formation can not be observed. Much confusion exists when the Active Formation occurs in close proximity to the black phyllites and schists of the Emerald Formation because of their similar appearance. This was encountered often during the core logging process during this past years work. In the Metaline Quadrangle in Washington State the Active Formation has been correlated with the Ledbetter slate, which disconformably overlies the Metaline Limestone, which in turn has been correlated with the Nelway. Although the commonest rock type is a relatively soft black argillite, Fyles and Hewlitt (1959) describe grey weathering black limestone is interbedded with black argillite on top of a ridge south of the head of Harcourt Creek, and near the head of the west fork of Harcourt Creek dark-grey limestone, dolomite and dolomite breccia have been found between elevations of 3,700 and 3,900 feet. Some of the dolomite is massive, but most is a sedimentary breccia made up of subparallel tabular fragments of dolomite about half an inch think and a few inches across in a matrix of dolomite.

To the north and west of the Remac District small plugs of intrusive rocks comprising of granites and leucocratic granites and syenties are present. These have traditionally been considered part of the Nelson Batholithic suite, which has been dated as Middle Jurassic.

Regional metamorphism to lower greenschist facies was synchronous with the first phase of deformation. The contact metamorphism postdates all phases of folding resulting in thermal aureoles up to 600 meters in width that surround the granitic plutons.

The rocks of the Kootenay Arc have a complex structural history involving at least three phases of folding, major regional low angle faults and multiple smaller faults (Jennings, 1991; Fyles and Hewitt, 1959).

Most of the area is covered with late Pleistocene deposits mainly related to the Fraser glaciation event which correlates with Late Wisconsian continental glaciation elsewhere in North America. The Fraser glaciation event in southern British Columbia occurred between 30,000 and 10,000 years B.P. and peaked in the ReMac area about 14,000 years ago. Kame terrace sediment deposits on the property as well as elsewhere in the district are evidence of retreating ice sheet stagnation.

6.2 Property Geology

Three regional-scale structural packages of rocks cross the ReMac Zinc property (Figures 3, 5): the Mine Belt on the north (containing the Reeves Limestone units), the Black Argillite Belt (Active Formation) on the south, and the Eastern Belt (Nelway Formation) along the southeastern edge of the property. Mine Belt rocks on the property typically strike WSW and dip steeply to moderately to the south. The Mine Belt and the Black Argillite Belt are separated by the major shallowly south-dipping Argillite Fault. Drilling in 2007 has demonstrated the continuation of the prolific Reeves-Redbird corridor of the Mine Belt (and potential for other zinc deposits) beneath the Active Formation within the property to the west of previously known occurrences. All significant zinc-lead mineralization within the Mine Belt occurs in the Reeves Member carbonates of the Lower Cambrian Laib Formation.

Three Reeves Member units cross the property. These were originally thought to be fold repetitions of the same Reeves horizon (Fyles and Hewitt, 1959, p.141) but the highly different character of the three units suggest they may represent three unique and different Reeves Member horizons (G. Klein, pers. communication with R.D. Westervelt, 2000). The northern Reeves horizon is an extensive unit of massive to bedded limestones that appears to be devoid of base metal mineralization. The central Reeves horizon (referred to as the Reeves-Redbird corridor) is host to all the past zinc-lead production from the mine and the majority of other known zinc-lead mineralization on the property. The southern Reeves horizon is named the Prospect Dolomite and is host to scattered zones of zinc-lead mineralization.

A variety of late lamprophyre dikes cut all formations on the property and commonly marks the location of faults. They are typically dark green to black with biotite phenocrysts. Rocks of the Reeves-Redbird corridor are deformed by two major west-southwesterly trending, isoclinal folds – the Salmo River Anticline and the Reeves Syncline. These folds have moderate to steep southerly-dipping axial planes. The corridor is also cut by a series of north-northeasterly trending normal faults. These faults dip 45° to 60° to the east, and have resulted in a down-faulted repetition of the stratigraphic and mineralized sequence eastward in a number of separate fault blocks. One of the better defined of these normal faults is the Beer Bottle Creek Fault which offsets Zone B mineralization down to the east to continue as Zone C. This fault was noted in the Redbird Tunnel No. 1 workings.

Cambrian quartzites of the Reno Formation are generally fine-grained and white. Although they do not outcrop, there existence has been determined by mapping the float within soil sample pits (Hall, 2005).

The Truman Member is the lowest unit of the Cambrian Laib Formation and consists of a narrow limestone unit that is defined by the presence of fine laminations of brownish biotite.

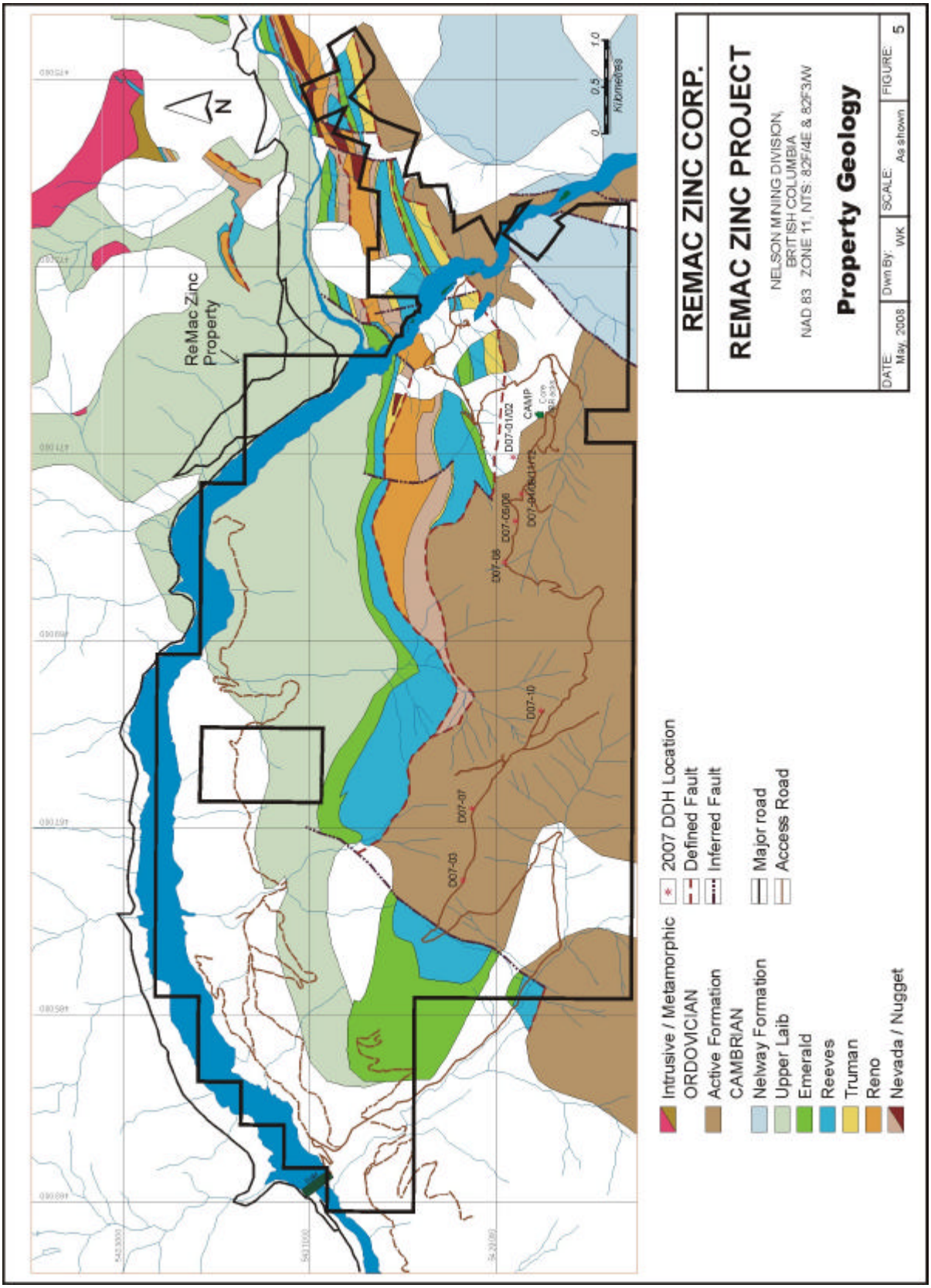


Figure 5: Property Geology

An arbitrary cut-off of 5% biotite laminations has been used to differentiate the Truman from the overlying Reeves Member.

The Reeves limestone is medium grained, weathers a blue-grey and is thinly banded between white, grey and sometimes black intervals. These laminations are generally on the scale of one to several centimetres. Where mineralization has been observed, the limestone has been converted to a buff coloured dolomite for a number of meters outboard.

Conformably overlying the ore-bearing limestones of the Reeves Member are black, carbonaceous phyllites and schists of the Emerald Member of the Upper Laib Formation. The characteristic rock type that comprises the Emerald Member is a black to grey, foliated, often-crenulated schist/phyllite unit. This rock type has been mapped south of the Reeves limestone in the eastern portion of the Redbird Grid and in the hinge of two interpreted anticlinal structures located in the central and eastern portion of the grid (Hall, 2005).

Disconformably overlying the Laib Formation is the Ordovician Active Formation. The Active Formation consists of black argillite, slate and minor calcareous members. On the property, the Active Formation is in thrust fault contact with the underlying carbonaceous schist of the Emerald Member. The most common rock type of the Active Formation seen in outcrop is a black to grey, carbonaceous phyllite, which is most prevalent in the eastern portion of the property. To the west, a series of carbonaceous dolomitic argillite predominate.

6.3 STRUCTURE

The 2005 Assessment Report (Hall, 2006) contains a detailed and extensive study of the structural aspects of the area and of the property, from which the following has been derived.

Regional Structure

Rocks exposed within the southern Kootenay Arc show a very complex structural history, involving at least three episodes of folding, major regional low angle faults and multiple smaller faults (Jennings, 1991; Macdonald, 1973, Fyles and Hewitt, 1959). The most in depth structural study of the Remac District is a doctorate dissertation by MacDonald (1973) from which much of the following is taken.

The Remac District occupies the south limb of an east-northeast trending anticline called the Salmo River Anticline. This ten kilometre long structure is cored by quartzites of the Cambrian Quartzite Range Formation with a variety of sedimentary rock types of the Cambrian Laib Formation occupying the flanks. Thrust over this anticline from the south are two panels of Ordovican carbonaceous rocks of the Active Formation. The Reeves Macdonald Mine occupies

the south limb of the Salmo River Anticline in a smaller, highly attenuated synclinal structure known as the Reeves Syncline.

According to MacDonald (1973) the first two phases of folding are regionally penetrative, coaxial planer and broadly associated with regional dynamothermal metamorphic events. The third phase of deformation consists of monoclinal folds and kink bands related the northward directed thrusting.

In more detail the first phase folds (F1) are near isoclinal, overturned toward the north and resulting in the development of the major structures, such as the Salmo River Anticline. Commonly the earliest recognized foliation (S1) is near coincident with bedding (SO), such that the two surfaces can only be distinguished with difficulty. Only where the bedding is cut at a high angle by the F1 foliation can the two be easily distinguished. The F1 foliation comprises a slightly micaceous, platy cleavage in the quartzites, and intense micaceouschloritic foliation or "schistosity" in the phyllites, and a cleavage in the carbonate rocks illustrated by sparse micas, and/or graphitic partings. The L 1 lineations are generally not very obvious and only noted where actual F1 folds were observed. The folds produced by this event are generally rare, tight to isoclinal structures, either with asymmetric single hinges or symmetric multiple hinges and long parasitically folded limbs. The L 1 linear structures have variable low to moderate plunges dominantly to the southwest, and less frequently to the northeast. The axial planes of these structures and S1 foliation strike roughly east west and dip moderately to the south (50-60°).

Phase 2 structures (F2) are distinguished as open to tight, asymmetric folds, which are generally upright to slightly overturned. Hinge profiles vary from rounded to subangular, tending towards the former in more massive rock types, such as the Reeves Limestone and the quartzite, and the latter in the finer grained rock types of the Laib and Active Formations. Axial plane cleavages (S2) are weakly developed in the massive rock types and represented by a pronounced crenulation cleavage in the phyllitic rocks. In general these folds are thought to have formed through "flexural slip", which have later been modified by flattening because of the difference in response between the competent and incompetent units and the generally slight attenuation of the fold limbs. The L2 linear structures plunge at low angles to the southwest, and less frequently to the northeast. The axial planes and foliation (S2) exhibit considerably less variation than the F1 folds and are usually steeply inclined east-southeast. Flattening of the F1 structures by the second phase of folding has presumably occurred and is reflected by the occurrence of intense shearing and transposition of the F1 fold closures. Some basin/dome interference structures are present, however these are relatively rare and recognized only the limestone units.

The Phase 3 structures (F3) are shallow to close asymmetric, monoclinal structures that plunge at moderate to steep angles. The larger folds in all lithologies tend to have gently rounded

hinges whereas the smaller examples have distinctly angular hinges, and in fact represent kink folds. Where deformation by this event is more intense, closely spaced kink bands and local crenulations are developed. However axial plane cleavage (S3) is generally absent, or only weakly developed. The F3 axial planes are generally vertical to subvertical striking to the northwest and southeast and can subdivided into a sinistral set that plunges to the east and northeast, and a dextral set the plunges to the east-southeast and southeast.

Two major bedding plane and/or thrust faults (the Emerald and Argillite Faults) cut across the stratigraphic section and juxtapose widely disparate units. The sense of movement appears to be from the south, and the age is viewed as problematic. Fyles and Hewitt (1959) believe these thrust faults were initiated during the first phase of folding and movement continued through the second phase of folding. The Argillite Fault in the vicinity of the H.B. Mine area has been refolded by the D3 event, and hence predates this the end of this event. At the Reeves MacDonald Mine area the Argillite Fault appears to be related to the kink folding and hence may be related to the 03 event.

Transverse faults include a variety of northeast to northwest trending faults that cut across all phases of the folds and thrust faults. Some of these may be strikeslip faults, others may be scallop faults having an east side down sense of displacement. The strike slip faults may be tear faults related to the thrusting of the Emerald and Argillite Faults, whereas the scallop faults appear to be a later event, possibly related to relaxation of the structural regime. These faults are most evident in the current structural scenario for the Reeves MacDonald Mine that involves scallop fault repetitions of a series of four ore horizons.

Property Structure

Structurally the property has undergone three phases of folding and four faulting events. This structural scenario is in general consistent with the work of MacDonald (1970, 1973) and other workers in the Salmo District. The first and second phases of folding are roughly co-axial planer, striking to the east northeast and in general dipping to the southeast. The dip of the axial planes and plunge of the fold axis tend to be shallower in the Redbird Grid area than the area of the Reeves MacDonald mine to the east. The first phase structures appear to be the larger of the two and have a relatively consistent plunge to the southwest, which is in keeping with observations from the Reeves MacDonald Mine. The third phase of folding involves compression from the northeast and southwest. This folding event postdates the Argillite Thrust Fault resulting in the curved surface pattern of this fault. Also associated with the Phase 3 folds are small faults that occupy occupying the noses of the folds. The other phases of faulting include a series of east northeasterly striking "normal" faults (note the precise dip is not known for these faults) located in the area of the No.4 Adit. Faults of this generation were likely responsible for the extensive development of fault gouge and broken rock conditions that

hampered the successful completion of the 2004 drilling program. Finally a northeasterly trending scallop fault located in the northeast portion of the Redbird Grid juxtaposes the Reeves Limestone against the Active Formation. This fault has 260 meters of apparent northeasterly displacement and represents the final deformation event on the property.

A generalized long section, adapted from Fyles and Walker, is presented in Appendix IV. This section has been updated through the years by G. Kleinand others, and represents the model ReMac Zinc Development Corp. was looking to substantiate through the 2007 drilling program.

7.0 DEPOSIT TYPES

There is no clear origin of the Salmo district base metal deposits, as they have undergone a number of phases of severe post emplacement deformation which consequently have obscured the primary textures.

The majority of the deposits in the Metalline, WA area are believed to be epigenetic cavity fillings of Mississippi Valley-type origin, which form in favourable dolomitized limestone horizons (Fyles and Hewitt, 1959). In the past, the mineralization in the Salmo district was considered hydrothermal replacements of the favourable carbonate host rocks. More recently, however, increasing evidence supports the origin of the Salmo area deposits as being Irish-type synsedimentary-exhalative (SEDEX) in nature (i.e. the mineralization was laid down as the sediments were deposited), with some local re-mobilization in response to late metamorphic events. These deposits are now highly deformed into elongated lozenges or “megamullions” in fold noses (Jennings, 1991). The lack of easy comparisons to deposits elsewhere prompted Sangster (1970) to coin the term ReMac-type deposits to describe them as a group.

8.0 MINERALIZATION

The following two sections have been extracted from a reports prepared for Redhawk by Jennings (1991), R.D. Westervelt (1999) and Hall (2005).

8.1 REGIONAL MINERALIZATION

Carbonate-hosted zinc-lead deposits occur along the entire length of the Kootenay Arc, from the Bonanza and Van Stone deposits in northeastern Washington to the Mastodon deposit in the vicinity of Revelstoke (Figure 3). The largest deposits occur in the vicinity of Salmo (including ReMac) and Metaline Falls on either side of the International border (Table 3).

Table 3: Production Statistics of Selected Kootenay Arc Carbonate-hosted Zinc-Lead Deposits

Deposit	Tonnage	Zn%	Pb%	Cd%	Ag opt
Salmo area Deposits					
Duncan (Reserves)	8,165,000	2.9	2.7	-	-
HB	7,283,000	4.45	0.93	0.013	0.12
Jersey	6,256,000	7.19	1.85	0.03	0.096
Reeves MacDonald*	7,254,000	3.5	1.39	0.02	0.238
Metaline Area Deposits*					
Pend d'Oreille***	5,451,000	2.58	1.33	0.002	0.047
Grandview	2,348,000	2.96	1.37	0.003	0.032
Metaline	431,500	4.28	1.2	0.0005	0.022
Monarch-Kicking Horse	744,000	8.85	5.63	-	-

*The Reeves MacDonald mining cut off was 3% Zn but with "adequate grade control procedures, the central core areas of the deposit could have been selectively mined at significantly higher grades" (G. Klein, pers. communication, 1996 quoted in Westervelt, 1998)
**Tonage to 1952
***Total production at the Pend d'Oreille Mine from 1935 to the mine closure in 1977 was 14,000,000 tons averaging 3.0% Zn and 1.3% Pb", (Westervelt, 1999). The Pend d'Oreille mine was reopened by TeckCominco in 2000 and continues to operate today.

The origin of the Kootenay Arc Pb-Zn deposits has been steeped in controversy with many different viewpoints being expressed over the years. The highly deformed nature of these deposits has contributed greatly to the various diverging viewpoints. The most succinct and balanced description has been provided by Jennings (1991), which is summarized below.

From north to south the major carbonate-hosted Pb-Zn deposits of the Kootenay Arc include the Duncan, HB, Jersey, Reeves MacDonald, Pend D'Oreille, Grandview and Metaline deposits. The Metaline District deposits (Pend D'Oreille, Grandview and Metaline) seem to be the least controversial and generally accepted to be "MVT" deposits (Ohle, 1970; Yakes, 1970; Addie, 1970; Sangster, 1970). The origin or metallogensis of the Salmo area deposits is less certain. Early studies suggested an epigenetic replacement model for their formation (Fyles and Hewlitt, 1957, 1959). On the basis of detailed structural studies of the Duncan deposit Muraro (1966) concluded that some of the deposits in northern Washington offer the closest approach to the "original" nature of all the deposits. Addie (1970) argues for the possibility of a syngenetic origin based upon the obvious stratigraphic control, along with the basis of their banded mineralization, interbanded chert (exhalite?) within an euxinic, graphitic carbonates and position within the central portion of a carbonate basin as opposed to being located in a "shale-out". Sangster coined the term "Remactype" for the Salmo area deposits, which he considered forming by synsedimentary processes in a deep water, shale-starved, carbonate, basinal environment. MacDonald (1973) suggested a variation on the model of Jackson and Beales

(1967) for the Salmo area. Hoy (1982) provided an excellent capsulization of the metallogenic arguments suggesting "these deposits may span the syngenetic-diagenetic interval and thereby accounting for the conflicting features of these ores that are characteristic of both stratiform and "Mississippi Valley type deposits." (Jennings, 1991).

Zinc-lead mineralization in the Kootenay Arc occurs in both the Reeves member of the Lower Cambrian Laib Formation and the Middle Cambrian Nelway Formation (Figure 6). At the Salmo District all the significant deposits are hosted by dolomitized limestone of the Reeves member of the Laib Formation. The deposits are often characterized by considerable lateral continuity (locally exceeding 1000m at the Reeves MacDonald and Jersey A Mines), stratabound to stratiform morphology and fine-scaled parallel sulphide layering. The sulphide mineralization mainly occurs as lenses and parallel layers of sphalerite, with pyrite and lessor galena.

Variable oxidation of sulphides to zinc-enriched gossans occurs most notably on the Remac Property (Gorzynski, 2000).

8.2 Property Mineralization

Mineralized Zones

The following information is compiled from a number of sources listed in the bibliography, various mine plans, and based on observations by Westervelt (1999). The main mineralization of interest on the ReMac property occurs in a series of carbonate-hosted base metal deposits and prospects (Zones 'A' to 'Z') exposed over a distance of some 4 kilometres referred to in this report as the Reeves-Redbird corridor (Figure x). The former Reeves- MacDonald Mine processed ore from several of these zones between 1949 and 1975. In total, 5.8 million tonnes of sulphide ore grading 3.50% Zn and 1.39% Pb was mined from the Reeves Mine (Zone R), the Annex Mine (Zones E & F), Zone K and some small ore blocks between Zones K and R. Other nearby base metal zones were tested by surface and underground exploration at various times since the 1920s.

Most significant mineralization on the property is hosted by dolomitized limestone of the Reeves Member of the Lower Cambrian Laib Formation. The base metal zones take the form of elongate lozenges typically 100-200 metres long, 5-25 metres wide and, where documented in the Reeves Mine (Zones R to K), over 1,000 metres down plunge (before faulting). Historical mining records from the Reeves Mine report extraordinary continuity of size and grade over these dimensions (G. Klein, pers. communication to Gorzynski, 2000). In total there are four, and possibly five, known zones of mineralization, typically striking east to ENE, dipping 50-60°S and plunging 45-60°W. These four zones are the Reeves, Annex, Annex West and Redbird. The average grades for the three principal zones are summarized in Table 4. Zone A at the west end of the corridor may or may not represent a new zone. Each of these zones is marked by typical

and distinct metal ratios. These four zones have been offset by a number of east-dipping normal faults, that repeat them several times to produce the series of distinct zinc deposits and prospects labelled Zones 'A' to 'H'.

Table 4: ReMac Principal Sulphide Zones (Source: Westervelt, 1999)

	Reeves MacDonald	Annex	Annex West
Zn	4.5-6.2%	8.0-12.9%	3.5-5.0%
Pb	1.60%	1.0-4.3%	3.5-5.0%
Cd	0.02%	0.09%	0.02%
Ag	0.3-0.5 opt	2.5-3.6 opt	1.0 opt
Zn/Pb	3.3	3.9	1.0

Primary sulphide mineralization at the Reeves-MacDonald Mine consists of laminations and lenses of massive and disseminated pyrite, honey-coloured sphalerite, galena and trace chalcopyrite. The sulphide bodies are structurally conformable and stratabound, often contain a high grade central core, and typically feather out along strike. Extensive 'barren' pyritic zones are not known to occur. The sulphide bodies are typically contained within dolomite envelopes, some of which extend for considerable distances along strike. The dolomites tend to be finer grained and more massive than nearby limestone. They commonly have a textured or tweedy pattern of irregular fine carbonaceous films thought to be the product of deformation (Fyles and Hewitt, 1959). Similar dolomites are also known to occur in areas of no known mineralization (G. Klein, pers. communication to Gorzynski, 2000).

The upper portions of most of the zinc zones have been oxidized to zinc-rich limonitic gossans or soils. Oxidation is known from underground workings and drill holes to extend to depths ranging from very shallow (Zones Q and R) to some 450 m below surface (Zone D). The transition from fresh sulphide to totally oxidized material is often abrupt, frequently occurring over only a few metres (e.g. Zone F (G. Klein, pers. Communication to Westervelt, 2000)). Higher grade sections tend to display coarse blue to grey radiating masses of hemimorphite ($Zn_4Si_2O_7(OH)_2 \cdot H_2O$) that are commonly several millimetres in diameter (e.g.- Zone B, Trench B-2000-01). Less common is dolomite mineralization which is visually innocuous but can attain very high grades derived from hemimorphite probably occurring in a finely disseminated form (e.g. Zone C, Trench C-2000- 02). There are also rare solution collapse breccias as described in (Zone B, Trench B-2000-05).

Other Zones

The following are descriptions of some of the other major zones of mineralization.

Reeves Zone (Zone R)

The Reeves Zone (Zone R) was the main historical zinc-lead ore body on the ReMac property. Between 1949-71 the Reeves MacDonald Mine processed 5,817,828 tonnes of sulphide ore at a recovered grade of 3.50% Zn, 0.99% Pb and 3.41 g/t Ag (MinFile, 2001), most of which came from the Reeves Zone (Zone R). The ore body had the form of an "attenuated syncline" with limbs striking eastward and dipping 50°- 60° to the south and axis plunging 215° azimuth at 55° (Fyles and Hewitt, 1959). The trough section of the Reeves ore body was about 100 metres long and up to 25 metres wide.

Dimensions and grades were extraordinarily continuous and consistent from surface to its final down plunge depth of about 800 metres where it was offset by a fault.

Annex Mine (Zones E & F)

The Annex Mine is located on the west side of the Pend d'Oreille River. It provided most of the production ore to the Reeves MacDonald mill during 1970-75 utilizing a bridge across the Pend d'Oreille River. Production from the Annex Mine totalled 763,314 tonnes of sulphide ore at a recovered grade of 5.59% Zn, 0.93% Pb and 44.61 g/t Ag, most of which came from Zones E and F (MinFile, 2001). Mined dimensions of the Zone F sulphide ore body were about 180 metres long, 6 metres wide and about 180 metres down. The sulphide-oxide boundary in Zone F was located and plotted during these operations (G. Klein, pers. communication to Gorzynski, 2000).

Zone K

Zone K is interpreted to be a fault offset portion of the Reeves Zone. Production from Zone K is included in the Annex Mine production statistics. At the closure of the mine in 1975 reported sulphide reserves in Zone K above the 240 level were 443,000 tons grading 5.35% Zn and 2.45% Pb (Westervelt, 1999). This resource estimate does not use categories that are consistent with those set out in Section 1.2 of NI 43-101; the estimate is relevant in that it is indicative of the possible exploration potential of the K Zone. The estimate should not be relied upon until verified by a Qualified Person. Zone K continues further down plunge for a distance of at least 150 metres.

The following are descriptions of some of the lesser known zones of mineralization from east to west.

O'Donnell Zone

The O'Donnell Zone is located about 900 metres northeast of the Reeves (Zone R) Glory Hole. It was developed from an adit on the 2350 level (MinFile, 2001) and from the 1900 Level workings below (Fyles and Hewitt, 1959). It is hosted by dolomite and "appears to have the same shape and plunge as the Reeves ore body, though the section of barren limestone between the dolomite halo and the Truman formation is thinner than it is to the west" (Fyles and Hewitt, 1959).

B.L. Prospect

The B.L. prospect is a poorly known zone located about 300 metres northeast of the Reeves Glory Hole (Zone R). Fyles and Hewitt (1959) report that at the time of their examination it was "exposed by surface strippings and partly explored by drilling. It is surrounded by dolomite and appears to have the same shape and plunge as the Reeves ore body." No size or assays are reported. MinFile (2001) reports the B.L. zone was developed from an opening at the 2350 level.

MacDonald Adit

The MacDonald adit was an old working located about 120 metres west of the 1900 level portal. It is now covered with rock waste and no longer visible. "The adit is reported to have been driven in earthy, calcareous, and limonitic materials containing secondary lead and zinc minerals", (Fyles and Hewitt, 1959). The adit probably cut Zone G.

Point Zone (Zone Z)

The Point Zone (Zone Z) is a small zinc sulphide prospect located 450 metres west of the 1900 Level portal and is now largely under water in the Pend d'Oreille River. Disseminated sphalerite, galena and pyrite were reported to occur in dolomitized Reeve limestone (Fyles and Hewitt, 1959). The zone comprised two mineralized lenses each about six metres wide separated by about 18 metres of barren dolomite. A small faulted portion of the Point Zone is visible today on a road cut beside the Reeves-MacDonald Mine road (G. Klein, pers. communication, 2000). A limited tonnage of sulphide ore was mined from the Point Zone reportedly averaging about 10% Zn (Westervelt, 1999).

Prospect Dolomite

The Prospect Dolomite is the southern unit of the Reeves Formation on the property. It does not have any history of production but is known for hosting zones of significant zinc-lead mineralization (Fyles and Hewitt, 1959; Klein, 1999a). Prospect Dolomite is typically light grey and massive and becomes siliceous in outcrops on the east side of the Pend d'Oreille River and near the Prospect adits. Mineralization in the Prospect Dolomite is known at several locations on the property. It consists of disseminated to layered pyrite, sphalerite and minor galena. The most significant mineralization is found in four drill holes south of Zone C where intersections in the Prospect Dolomite included 13.7% Zn across 0.9 metres (Hole 98-1), 8.24% Zn over 4.00 metres (Hole 87-3) and 2.02% Zn over 16.98 metres (Hole 87-1) (Klein, 1999a). Only minor zinc mineralization is known from the Prospect Dolomite on the Reeves Group claims (Klein, 1999a). Little is known of this mineralization in the old Prospect adits at the east end of the property (Fyles and Hewitt, 1959).

Caviar Prospect

The Caviar east and west zinc prospects are located west of the Pend d'Oreille River and some 200 metres north of the USA boundary line . They consist of lenses and stringers of sphalerite in dolomitic sections of limestone mapped as Nelway Formation by Fyles and Hewitt (1959) but noted to resemble Reeves Formation by Klein (1999c). Four core drill holes were completed in 1959 on the western Caviar showing with the best intersection returning 6.5% Zn over 6.1

metres, 60 metres below the surface. Surface oxidation of the mineralization is limited to a few metres (MinFile, 2001).

Metallurgical Studies

A metallurgical scoping review by Fluor Daniel Wright (1991) outlined a number of potential production options. In 1992, this review was followed up by preliminary mineralogical and metallurgical studies of the bulk sample collected from the Beer Bottle zone (Price, 1992). This work was conducted under the supervision of R.O. McElroy, Senior Metallurgist with Fluor Daniel Wright in Vancouver.

As observed by Westervelt (1999), the Beer Bottle oxides were found to consist of friable, earthy limonite which breaks up to a fine, reddish-brown, powder. No distinctive minerals are evident under hand lens examination. The mineralogical study identified the material as being 40% limonite, 58% hemimorphite and 2% carbonate. When pure, hemimphorite (a hydrated zinc silicate), contains 67.5% Zn, 25% SiO_2, and 7.5% H_20.

Although physical concentration tests provided poor results, sulphuric acid leaching was highly successful (97% recovery at pH2). On this basis, a solvent extraction/evaporative crystallization process was suggested which would produce zinc sulphate suitable as a feed for Teck Cominco's Trail smelter or for on-site metal production.

In 1995, Redhawk commissioned Fluor Daniel Wright to carry out a general metallurgical scoping review with regard to the ReMac oxide ores. As described in a report by R.O. McElroy, Senior Metallurgist, dated January 29, 1996:

1. Subject to confirmatory test work, zinc and cadmium from the ReMac oxide materials can be recovered using a process similar to the one used by the Paedeng Industry Co. Ltd., which is described in detail in Westervelt, 1999. Further testing would be required to determine whether sulphidizing flotation of the leach residue would recover the lead-silver values. The process would allow for either the production of a zinc sulphate material or for on-site production of metal.

2. Zinc silicate ore might be directly sold to smelters such as Cominco or Hudson Bay Mining and Smelting as preferential feed for their existing autoclave plants. Future test work should include magnetising roast/magnetic separation tests which may upgrade the zinc silicate ore to the 50% Zn content range for shipping purposes. In summation, the study did not indicate any particular problems in treating the oxides.

In 2000 ZincOx carried out a metallurgical study on the ReMac property. The aim of this study was to incorporate all available information on the ReMac property in order to carry out a preliminary economic appraisal on the processing of the ore by means of flotation at the mine

site. This low grade concentrate would then be transported to the Cominco smelter complex at Trail for the production of zinc metal. Beneficiation test work on a composite sample was carried out by CTP in Belgium. The final concentrate contained 21.0% zinc and recovered 86% of the contained zinc.

ReMac ore samples were subjected to Anaconda leach tests to determine zinc leaching efficiency, behavior of impurities and acid consumption data. Zinc leaching recoveries were generally excellent varying between 87-99% yield for the twelve composite samples tested.

The study concluded that several metallurgical challenges would need to be overcome to facilitate zinc recovery from the oxide ores.

9.0 2007 WORK PROGRAM

9.1 DIAMOND DRILLING

A 12 hole, 6189.6 metre diamond drill program was completed on the ReMac Zinc property during the 2007 exploration program (Figure 6, Table 5, and Appendix IV-VII). Midpoint Drilling Ltd., of Langley, BC, was contracted to conduct the drilling. The size of the drilling program was curtailed by a large forest fire which swept through the area mid-summer, effectively shutting down the entire project for a couple of months. A drill was caught up and consumed by fire in the middle of drilling hole D07-04, but luckily the camp was spared and no one was injured. It proved difficult to find a replacement drill in a busy drilling season, and a second company, Westcore Drilling Ltd. of Hope, BC, was brought onto the project in November to assist with the drilling.

Table 5: Diamond Drill Collar Summary

Hole No.	Easting	Northing	Elevation	Azimuth	Dip	Depth (m)	Claim Tenure
D07-01	470961	5428818	1125	330	-60	187.27	514867
D07-02	470961	5428818	1125	330	-70	434.64	514867
D07-03	466445	5429368	1346	330	-60	594.49	514860
D07-04	470556	5428738	1229	330	-60	528.22	514867
D07-05	470284	5428797	1287	358	-60	26.21	514867
D07-06	470284	5428797	1287	358	-55	555.65	514867
D07-07	467210	5429262	1469	360	-60	821.74	514860
D07-08	469,828	5428909	1350	360	-60	446.00	514867
D07-09	470572	5428736	1229	360	-54	338.69	514867
D07-10	469554	5428412	1477	360	-70	960.73	514866
D07-11	470568	5428731	1216	360	-58	609.50	514867
D07-12	470568	5428731	1216	360	-90	707.00	514867

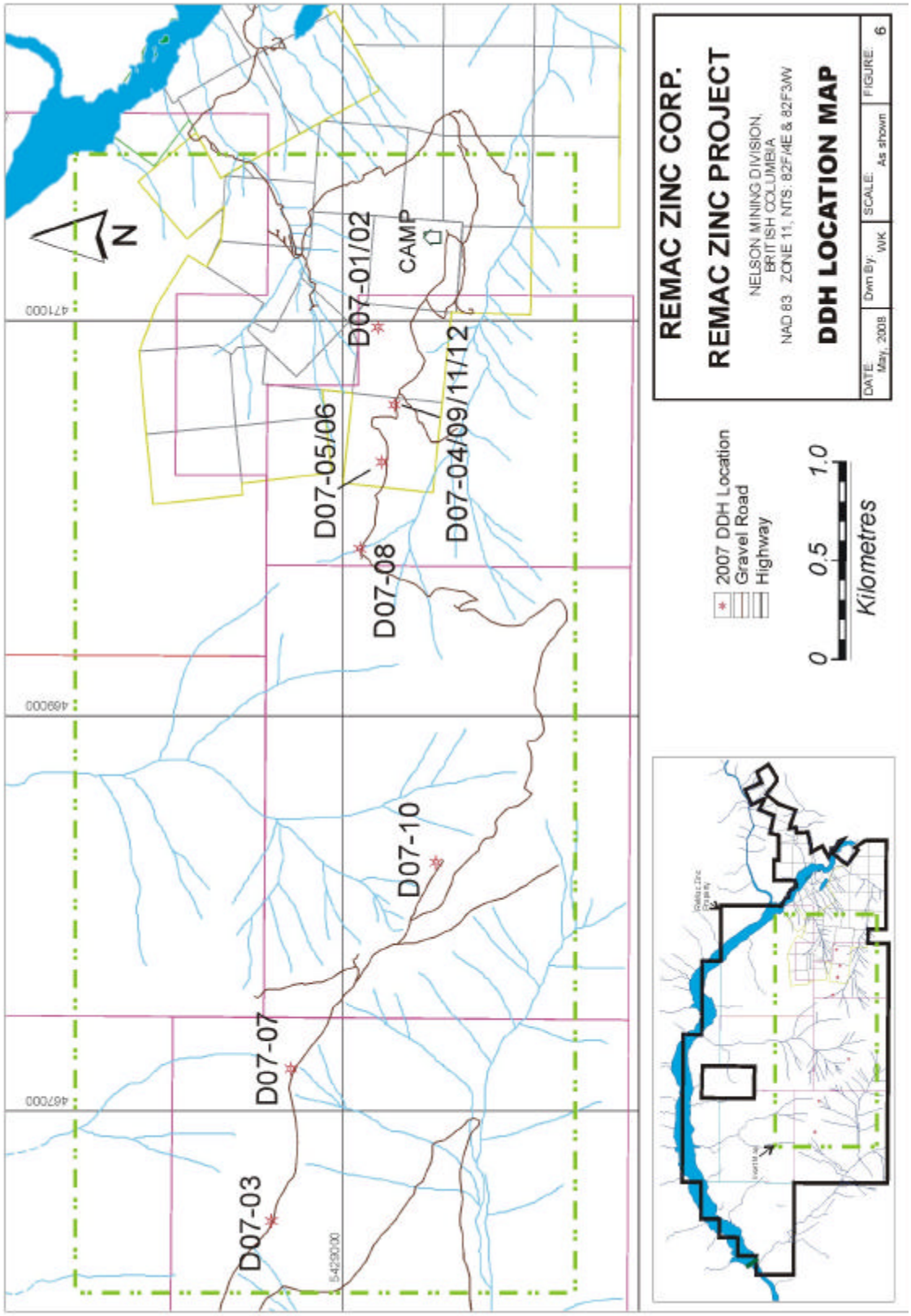


Figure 6: Drill Hole Locations

Difficulties were encountered in drilling through the fault zone at the base of the Active Argillite unit. This was mitigated by drilling with HQ size core until past the fault zone and then reducing to NQ for the remainder of the hole.

Water supply was a challenge throughout the program as well, as much of the drilling occurred topographically higher on the property than areas of significant water flow in drainages. A combination of pumping water from Russian Creek and trucking water from Church Creek kept the drills supplied with water. Both creeks maintained sufficient water flow through to the end of December.

Three of the twelve holes, totalling 531 metres, were abandoned in the course of the drilling program. Holes D07-01 and 09 encountered tight ground conditions and caving due to faulting and were unable to be continued. Hole D07-05 was mistakenly started in the wrong direction and had to be realigned.

The remaining nine holes were successfully completed to the target horizon.

9.2 METALLURGICAL

Although the 2007 drilling program concentrated locating an extension of Reeves type sulphide mineralization, work was conducted on furthering knowledge of the oxide zone mineralization through a continuation of the metallurgical work started earlier.

SGS Lakefield Research, in conjunction with Samadish Engineering Ltd., was contracted to determine the potential zinc concentrate grade and zinc recovery of the zinc oxide resources. In the fall of 2006 a metallurgical testing program was initiated by Redhawk Resources Inc. at SGS Lakefield using reverse circulation drill core from the oxide zones. The objective is to produce a marketable zinc oxide concentrate with a recovery of at least 80%. Heavy liquid separation testwork was performed on the ore, prior to grinding and desliming. The deslimed feed underwent floatation. Repeated testwork showed that a zinc concentrate grading 38.4% zinc could be achieved, at a recovery of 82.2% zinc (Appendix VIII), which compared to the earlier test results of 42.3% concentrate with a recovery of 83.6% zinc.

10.0 SAMPLING PROCEDURES AND ASSAY METHODS

10.1 DRILLING PROCEDURES AND CORE COLLECTION

Diamond drilling services were provided initially by Midpoint Drilling Ltd., of Langley, BC. Towards the end of the program, Westcore Drilling Ltd. of Hope, BC, was contracted to assist with the drilling program. Drilling methods were similar for both companies: HQ sized core was drilled for the length of the Active argillite. This was reduced to NQ size after encountering the

Emerald schist. It was found the larger size core produced fewer problems getting through the faulted zone at the base of the Active argillite. Core boxes were covered with lids and stored at the drill site. ReMac geologists picked up the core at the drill and transported it to the core logging shack in camp. The core was logged in a secure core shack used exclusively for that purpose. Following logging, the boxes of core were photographed, and taken to the core cutting shack for splitting with a rock saw. After samples were collected, the core was stacked in sturdy core racks located adjacent to historical core racks containing previously drilled core.

10.2 Core Logging and Sampling Methods

Sampling methodology varied throughout the program due to different phases of supervision resulting from the delays due to the fire. Initially, only areas of the Reeves limestone visually verified to contain abundant zinc mineralization were sampled by split core methods. Some of the early samples were sent directly for fire assay based on visual appraisal. The following description describes the methodology adopted for the latter portion of the drilling program.

Due to abundant previous sampling, it had been determined there was no other mineralization associated with pyrite and pyrrhotite rich sections of Active argillite (G. Klein, personal communication, 2007), and such zones encountered were not sampled for analysis.

Three-tag, pre-numbered sample books were employed for sampling purposes. Prior to sampling, tag books were marked for one certified standard sample to be included in the sequence every 15 samples. Certified samples were obtained from CDN Resource Laboratories Ltd. and consisted of three different concentrations (Table x). The inclusion of one of the three standards was randomly chosen each time so as not to have a noticeable pattern of standards. Sample blanks, consisting of non-mineralized rock collected by G.H. Klein for that purpose, were inserted into the sample stream immediately following any zones of intense zinc mineralization in the core to check for contamination following high grade areas.

Table 6: Reference Standards

	Std 1		Std 3		Std 7	
Element	**Value**	**Devience**	**Value**	**Devience**	**Value**	**Devience**
Au g/t	0.242	*0.018*	0.83	*0.12*	1.31	*0.16*
Ag g/t	354	*21*	65.1	*6.7*	101.2	*10.8*
Cu %	0.049	*0.003*	1.49	*0.06*	0.76	*0.03*
Pb %	0.957	*0.044*	0.29	*0.03*	0.815	*0.06*
Zn %	1.34	*0.11*	3.01	*0.17*	7.66	*0.36*

Mineralized zones within the Reeves limestone unit were identified visually and continuous split core sampling was conducted from 1-2 metres above the start of the zone through to 1 to 2 metres after the zone ended. Sampling was generally conducted across widths of 1 metre,

paying respect to lithological and mineralogical boundaries. Attempts were made to maintain a minimum sample length of 0.5 metres and a maximum of 1.5 metres. Mineralized zones were identified by the first appearance of sphalerite and/or galena in the core sample. In some areas, intensive concentrations of pyrrhotite were considered as mineralized zones as well, although no sphalerite of galena was noted. The core was first re-assembled and fit together in the boxes and then marked for sampling to ensure that the sampling was conducted on the same contiguous half section of core. Sample tags were stapled to the boxes at the start of each section sampled. A second tag was included in the bag with the sample, and the sample number was also written on the bag. The only feature on either of these two tags was the sample number. The third tag remained in a booklet, and was used to identify the specifics of the sample.

10.3 Sample Storage

The entire sequence of core boxes from the drilling program were marked with punched aluminium tags identifying hole number, box number and sample depth. All logged core and half core sampled sections is stored in heavy duty core racks on the property, near the site of the camp. Previous diamond drill core from other programs is also stored in the same area. The older core racks are beginning to disintegrate, and will eventually collapse; the old core boxes are in still fair condition. Management should consider building new racks and transfer the older core boxes to preserve them before they collapse. A smaller collection of older drill core in a similar condition is found along the road approximately 200 metres west of the main core storage area.

10.4 Sample Shipping

Since the standards used were previously prepared and the blanks consisted of broken rock samples, they were not blind to the receiving laboratory, but no recognition of their status or identity was included in the sample documentation to differentiate them from the rest of the core samples. The only key to the identity of the sample numbers was in the secure logs and records kept with ReMac geologists in the core shack.

The bags were sealed with nylon zip-lock ties, and from 5 to 7 samples were then put into rice bags which were again tied with zip lock ties. ReMac personnel then transported the samples to Trail for transport to the lab by Greyhound courier for early batches of samples. Later samples batches were packed into large plywood boxes constructed on pallets, securely sealed, and shipped directly to the lab via transport truck.

10.5 Laboratory Methods

The drill core samples were sent to the Teck Cominco Exploration Research Global Discovery Laboratory in Vancouver for analysis. Upon arrival at the lab, the core samples were subject to

standard preparation procedures which include digital log-in, weighing, drying and fine crushing of the entire sample. The samples were crushed to minus 150 mesh. They were then analyzed as described below.

Samples returning highly anomalous results for zinc, lead or silver were identified by ReMac geologists upon receipt of results, and were sent for fire assay.

ICP Digestion (Aqua Regia)

A 0.5 gram rock sample is digested in aqua regia on a sand bath at 95 ^{o}C for 3 hours, shaking every 20 to 30 minutes. The sample is diluted and mixed on a vortex. The sample is then analyzed on the I.C.P. to produce a 28 multi-element package which includes: Cu, Pb, Zn, Ag, As, Ba, Cd, Co, Ni, Fe, Mo, Cr. Bi, Sb, V, Sn, W, Sr, Y, La, Mn, Mg, Ti, Al, Ca, Na, K and P. Every 40 samples prepared includes 3 sample repeats, 1 in-house standard and/or commercial standard.

Mercury (Cold Vapour - AA)

A 0.5 gram sample is weighed. Nitric Acid and Hydrochloric Acid is added. The sample is digested on a hot plate, and then diluted with demineralized water. Stannous Chloride is added, and the sample is analyzed on A.A. Every 30 samples prepared includes 1 - 2 sample repeats and 1 in-house standard.

11.0 DISCUSSION

The 2007 drill program successfully proved through widely spaced drilling that the potential ore bearing Reeves Limestone underlies much of the ReMac Zinc property, and discovered encouraging new zones of sulphide mineralization within this unit (Table 7). Oxidation levels were also shown to be relatively shallow.

A new mineralized zone was discovered in the area of holes DDH 07-04, 11 and 12. In each of holes 11 and 12, mineralization consisted of two distinct bands within the limestone unit.

Another significant zone was discovered in DDH 07-02.

Table 7: Significant DDH Intersections

Hole	Sample	From	To	Interval	PB %	Zn %	Ag g/t	Cd %	Hg ppb
D07-02	A10032451	**368.05**	**369.03**	0.98	0.02	0.06	**13.2**	0.00	
D07-02	A10032452	369.03	369.71	0.68	**1.36**	0.05	0.0	0.00	
D07-02	A10032453	**369.71**	**370.67**	0.96	**2.98**	0.18	**26.8**	0.00	
D07-02	A10032454	370.67	371.76	1.09	**0.42**	0.11	**4.1**	0.00	

D07-02	A10032455	371.76	372.79	1.03	0.27	0.12	6.0	0.00	102
D07-02	A10032456	372.79	374.11	1.32	0.45	0.17	6.2	0.00	203
D07-02	A10032460	**393.05**	394.89	1.84	0.69	5.11	6.5	0.04	1381
D07-02	A10032461	394.89	396.02	1.13	0.64	2.48	5.9	0.01	677
D07-02	A10032462	396.02	396.91	0.89	0.03	0.75	0.0	0.00	213
D07-02	A10032463	396.91	**398.06**	1.15	0.22	1.50	2.1	0.01	426
D07-04	A10032472	369.12	369.85	0.73	0.10	0.56	1.0	0.005	70
D07-04	A10032473	369.85	370.16	0.31	0.10	4.69	1.9	0.037	1214
D07-04	A10032478	461.35	462.12	0.77	1.84	0.38	3.3	0.008	135
D07-04	A10032479	462.12	462.85	0.73	3.60	1.43	7.7	0.019	434
D07-04	A10032480	462.85	463.70	0.85	4.24	3.73	13.3	0.045	997
D07-04	A10032483	463.70	464.50	0.80	0.15	0.67	1.7	0.013	155
D07-04	A10032484	464.50	465.12	0.62	0.04	0.04	0.6	0.007	19
D07-04	A10032485	465.12	465.95	0.83	0.08	0.15	0.9	0.008	48
D07-04	A10032486	465.95	467.20	1.25	0.03	0.03	0.0	0.007	12
D07-04	A10032487	467.20	468.17	0.97	0.25	0.48	2.6	0.014	170
D07-04	A10032488	468.17	469.05	0.88	0.53	0.37	6.6	0.007	241
D07-04	A10032489	469.05	469.96	0.91	0.80	0.11	1.1	0.010	79
D07-04	A10032490	469.96	471.00	1.04	0.37	0.11	3.6	0.011	88
D07-04	A10032491	471.00	471.42	0.42	0.06	0.01	0.7	0.008	17
D07-04	A10032494	471.42	471.97	0.55	0.87	0.47	8.6	0.016	305
D07-04	A10032495	471.97	472.72	0.75	0.68	0.69	7.4	0.017	406
D07-04	A10032496	**472.72**	**473.77**	1.05	0.63	0.80	10.0	0.019	389
D07-04	A10032497	473.77	474.70	0.93	0.36	0.50	4.8	0.009	192
D07-04	A10032505	**507.37**	**507.86**	0.49	0.14	10.97	2.9	0.113	3581
D07-04	A10032506	507.86	508.82	0.96	0.01	0.64	0.0	0.016	237
D07-11	A10032564	334.00	335.00	1.00	0.00	0.51	0.0	0.004	124
D07-11	A10032565	335.00	336.00	1.00	0.00	0.07	0.0	0.001	15
D07-11	A10032566	336.00	337.00	1.00	0.01	0.56	0.0	0.006	139
D07-11	A10032620	462.00	463.00	1.00	0.02	0.41	0.0	0.002	72
D07-11	A10032621	463.00	464.00	1.00	0.01	0.32	0.0	0.002	50
D07-11	A10032622	464.00	465.07	1.07	0.01	0.48	0.0	0.003	93
D07-11	A10032623	465.07	466.43	1.36	0.04	0.66	0.0	0.006	208
D07-11	A10032661	504.50	505.00	0.50	0.26	4.64	0.061	3.9	175
D07-11	A10032679	**529.36**	530.00	0.64	0.00	1.96	0.016	1.2	106

D07-11	A10032680	530.00	530.71	0.71	0.00	**0.42**	0.0	0.004	17
D07-11	A10032681	530.71	531.64	0.93	0.00	**4.44**	0.046	**4.1**	**287**
D07-11	A10032706	531.64	**533.00**	1.36	0.00	**0.44**	0.0	0.005	10
D07-12	A10033711	426.71	427.69	0.98	0.18	**1.87**	**2.6**	**0.018**	**717**
D07-12	A10033715	**432.39**	**433.05**	0.66	**1.04**	**5.68**	**14.4**	**0.055**	**1603**
D07-12	A10033731	456.00	456.92	0.92	0.00	**3.42**	0.7	**0.039**	**888**
D07-12	A10033732	456.92	457.45	0.53	0.00	0.02	0.0	0.000	14
D07-12	A10033733	457.45	458.00	0.55	0.00	**1.92**	**1.3**	**0.019**	**488**
D07-12	A10033734	458.00	458.79	0.79	0.00	0.04	0.0	0.000	0
D07-12	A10033735	458.79	459.79	1.00	0.00	0.17	0.0	0.001	76
D07-12	A10033736	**459.88**	461.00	1.12	0.00	**8.90**	**1.4**	**0.097**	**2641**
D07-12	A10033737	461.00	**461.94**	0.94	0.00	**4.50**	**1.1**	**0.047**	**1496**
D07-12	A10033748	470.00	471.19	1.19	0.11	**1.85**	**2.7**	**0.013**	**597**
D07-12	A10033752	475.06	476.00	0.94	0.10	**0.52**	**1.1**	0.003	111
D07-12	A10033753	476.00	477.00	1.00	0.04	**0.70**	0.5	0.004	105
D07-12	A10033795	604.35	605.00	0.65	0.01	**0.75**	0.0	0.008	116
D07-12	A10033796	605.00	605.69	0.69	0.00	**4.87**	0.6	**0.041**	**424**
D07-12	A10033803	625.72	626.73	1.01	0.03	**0.52**	0.0	0.005	71
D07-12	A10033804	626.73	627.19	0.46	0.16	**6.06**	**1.1**	**0.027**	**285**

12.0 RECOMMENDATIONS

The main areas to focus the next phase of exploration upon are:

1. Downhole geophysical surveys should be completed in the areas of newly discovered mineralization to test if any methods of survey produce targets for further exploration. Geophysical targets produced should then be drill tested.

2. Follow-up drilling is recommended in the area of newly discovered mineralization. Step-outs from the holes should be in the order of 100 metres, as Reeves ore bodies are shown to be 180 metres or shorter in plan. A total of 2 to 4 holes up to 700 metres deep should be drilled between the areas of D07-02 and D07-04

3. The deeper sulphide target of the projected Redbird zone should be drilled. This was the next intended drill target of the 2007 program; time constraints did not allow the hole to be drilled. Drilling of this target would require 2 deep holes of 1000 metres each.

4. The Reeves Limestone should be drilled systematically to the west of Hole D07-08 towards the zinc anomaly at the head of Harcourt Creek to check structure, continuity and mineralization. Up to six holes, each approximately 1000 metres in depth, are recommended to be drilled in this area, depending on what is encountered as drilling progresses.

APPENDIX

I. STATEMENT OF QUALIFICATIONS

STATEMENT OF QUALIFICATIONS

I, Willie Kushner, B.Sc., do hereby certify that:

1. I graduated with a Bachelor of Science degree in Geology from the University of Alberta, Edmonton, Alberta, in 1987.
2. I have been practicing my profession as an Exploration Geologist continuously since my graduation for the past 20 years.
3. I am a consulting geologist.
4. I was contracted by Mineral Development for ReMac Zinc Development Corp. to conduct field work during the 2007 Exploration Program.
5. I was contracted by ReMac Zinc Development Corp. to write this assessment report on the drilling program.
6. I personally wrote this report and am responsible for all of the maps and content contained within. I personally believe this report accurately depicts the information available to date.
7. I hold no interest, directly or indirectly in the Minnie Lode Mining Claim property or any surrounding properties. I hold no securities in ReMac Zinc Development Corp. and have no agreements, arrangements or understandings with the issuer.

Dated this 12th day of May, 2008

Willie Kushner, B.Sc.

Louben Geological Ltd.

APPENDIX

II. 2007 EXPENDITURES

Categories	Cost	Totals
Camp Construction and Maintenance		**$ 903,556.59**
Labour - Construction, Maintenance, First Aid	$ 408,490.99	
Materials and Supplies	$ 187,745.01	
Equipment Contractors, Road Maintenance	$ 263,486.92	
Rentals (Generaotrs, Chainsaws, tools	$ 43,833.67	
Project Management		**$ 370,350.77**
Camp and Senior Project Management (DRD Consulting)	$ 198,407.53	
Overall Project Management (5%)	$ 171,943.24	
Mob / DeMob		**$ 132,769.96**
Room and Board	$ 56,893.52	
Travel	$ 38,834.04	
General	$ 37,042.40	
Vehicle Rentals		**$ 172,098.85**
DRD Consulting		
7 Trucks, 2 ATVs, 1 ATV trailer	$ 133,666.02	
2 skidoos	$ 9,669.68	
Misc Employee vehicle rentals	$ 9,083.15	
Contractor Truck rentals		
KDK	$ 9,700.00	
Daves Welding	$ 9,980.00	
Drilling ($282.50/m avg)		**$1,959,876.53**
Drill Contractors		
Midpoint - 3697.83 metres drilled	$1,090,896.73	
Westcore - 2021.50 metres drilled	$ 524,817.18	
Daves Welding		
Water Truck	$ 145,200.11	
Subcontractor	$ 36,465.96	
Expendibles		
Core Boxes	$ 29,108.20	
Fuel	$ 133,388.35	
Consultants		**$ 206,751.41**
Senior Project Consultant		
G Klein, 214 days @ $650/day	$ 139,100.00	
Vehicle Rental	$ 7,647.50	
Metallurgical Studies		
SGS Lakefield	$ 60,003.91	
Geology		**$ 205,143.96**
Geological Consultants		
Juan Calles, Calles Geological, 113.5 days @$650/day	$ 73,775.00	
Mike Miller, 59 days at $600/day	$ 35,400.00	
Willie Kushner, Louben Geological, 66.5 days @ $650/day	$ 43,225.00	
Tiia Mikkanen, Logging assistant, 71 days @ $275/day	$ 19,525.00	
Assaying, Global Discovery Labs	$ 6,888.01	
Drafting, Zenith Drafting	$ 15,630.68	
Equipment and Supplies	$ 10,700.27	
	TOTAL:	**$3,950,548.07**

APPENDIX

III. REMAC PROPERTY HISTORY

The following historical summary follows the traditional division of the property between the western Redbird claims and the eastern Reeves claims (adapted from Gorzynski, 2001).

GENERAL HISTORY

1865:	The first mineral discovery in the area is credited to men of the Hudson's Bay Company who attempted to recover gold from the Salmo River near its junction with the Pend d'Oreilie River (Walker, 1934). This is on the present-day Remac (Reeves) property.
1865-1890's:	Placer mining on the Pend D'Oreille River attracted attention to the area (Fyles and Hewitt, 1959).
1893:	Construction of the Nelson and Fort Sheppard Railway provided new access to the region.
1902:	Reconnaissance mapping by the R.A. Daly included the area of the property.
1906:	The first lead ore in the district was mined at the Emerald mine (Fyles and Hewitt, 1959) some 14 km northeast of the property.
1928-31:	The first comprehensive geological map of the region was prepared by the Geological Survey of Canada (Walker, 1934).
1947-49 & 1959:	H.W. Little carried out regional mapping for the Geological Survey of Canada.
1955:	J.T. Fyles and C.G. Hewitt of the Geological Survey of Canada mapped the area and reported on the mineral deposits (Fyles and Hewitt, 1959). This is still the best reference for work in the district.
1969-70:	Government airborne magnetics were flown over much of southern British Columbia including the Remac property area at a scale of 1 inch = 1 mile.

REEVES PROPERTY HISTORY

1910-1912:	James Quayle and J.H. ("Black Jack") MacDonald of Rossland' staked claims covering the Point (Zone Z) and MacDonald prospects (Zone G).
1918:	Prospector R.H. Reeves staked claims covering the Reeves main zone (Zone R) (Walker, 1934).
1925:	The Reeves and MacDonald properties were acquired by the Victoria Syndicate of London, England and active exploration and development

began. At this time the Reeves and MacDonald adits were driven, several thousand feet of exploratory drilling was done and exploratory work was carried out on the Prospect showing east of the Reeves Zone (Walker, 1934).

1928: Reeves-MacDonald Mines, Limited was incorporated (Federal Charter) with the Victoria Syndicate retaining a substantial interest (Walker, 1934).

1928-30: J.J. O'Neill of McGill University mapped the geology of the Reeves MacDonald mine area (Walker, 1934).

1929: Control of Reeves-MacDonald Mines, Limited passed to the Pend d'Oreille Mines and Metals Company. A "long, low-level adit" was driven into the Reeves zone at depth and development work was carried out on the O'Donnell showing east of the Reeves Zone (Walker, 1934).

Circa 1930: J.F. Walker visited the Reeves-MacDonald Mine and he reported on the geology and mineralization in the Reeves adit, the McDonald adit, the 1900 Level adit, the O'Donnell Adit, the Prospect adits and various surface showings east of the Reeves Zone (Walker, 1934).

1930: Work was suspended on the Reeves-MacDonald site (Walker, 1934).

1937-38: Some crosscutting and core drilling was done in the 1900 level workings.

1946: The "Reeves MacDonald Mine was prepared for production" (Fyles and Hewitt, 1959).

1949: The Reeves MacDonald Mine began commercial production in August 1949 with a 450 tonne-per-day concentrator which was increased to 900 tons-per-day in 1950.

1953-55: In June 1953 the Reeves MacDonald Mine was closed. In October 1955 the mine was reopened (Fyles and Hewitt, 1959).

1970-75: The Annex Mine (Zone F) was developed and became the main source of ore on the property (Westervelt, 1999).

1971: The Reeves Mine ore reserves were depleted although some scavenge mining continued through 1972-74.

1973: A.S. MacDonald completed a doctorate thesis on the deformation and metamorphism of the Salmo area zinc+lead deposits including the Reeves-MacDonald Mine.

1975: Reeves MacDonald Mines closed its mining operations "due in large part to the restrictive taxation then levied in British Columbia ... ". Subsequently most of the mine buildings and facilities were removed.

2000: Redhawk Resources signed an option to purchase agreement on the Reeves property with Reeves MacDonald Mines Limited.

2000: ZincOx Resources of London, England signed an option agreement with Redhawk Resources to earn a 50% interest in the ReMac zinc oxide project covering both the Redbird and Reeves properties. An extensive 21 hole reverse circulation drilling and trenching program is carried out to test the extent of the oxide zone.

THE REDBIRD AND ADJOINING PROPERTIES

pre-1924: The core Redbird property is staked by S. Coulter and AJ. Campbell of Ymir.

1913-34: The 17 claim (approximately 800 acre) Redbird property was staked and crown granted. The first claims are reported to have been staked by Jack MacDonald.

1925: Conrad Wolfe and associates of Spokane optioned the property (Walker, 1934).

1925: The Red Bird Mining Company of Spokane was incorporated.

1927: By this time about 1,000 feet of tunnelling had been completed on the property (Walker, 1934). Tunnels NO.1 (Zone C), 2 (Zone C near drillhole R-2000-08), 3 (Zone B in Beer Bottle Cut) and 4 (Zone A) as well as the Beer Bottle Cut (Zone B, re-exposed in Trench B-2000-01) were in place.

1928: A controlling interest in Red Bird Mining Company was acquired by a Vancouver syndicate and the NO.1 adit (Zone C) was advanced to 1,200 feet and some core drilling done (Walker, 1934).

1929: The Vancouver syndicate incorporated Boundary Basin Mines, Limited and carried out some drilling (Walker, 1934).

1929-43: Little work reported although a sample plan map of Tunnel No. 1 in Redbird Zone C dated 1942 exists.

1943: The property was purchased by Hecla Mining Company of Wallace, Idaho.

1947: Diem Mines Limited (subsidiary of Hecla Mining) carried out geological

mapping and surface work.

1950-51: Cominco Ltd. completed soil sampling and geological mapping on the Bar Claims (approximately the present day Tic 1 and NOR claims). Results are not known.

1951: Cominco Ltd. drilled a 390m (1,281 ft) deep vertical hole (DDH-B1) on the southeastern part of the present-day Tic 1 claim to target the Reeves Formation and potential zinc deposits at depth. Most of the hole was in Active Formation shales but it intersected 8m (26 ft) of Reeves limestone before entering Reno Formation quartzite at a depth of 343m (1126 ft).

1957-58: Hecla Mining Company completed an access bush road from Washington, USA to the Redbird prospects (Fyles and Hewitt, 1959, p.136), carried out bulldozer stripping on unspecified targets and drilled two core holes for a total of 130.2m (427 ft) (Betmanis, 1986).

1961-62: Consolidated Mining and Smelting Co. (Cominco) leased the property, advanced the No. 1 (Zone C) exploration drift about 250m (800 ft) and completed 1,247m (4,092 ft) of core drilling (651 m from underground and 596m from surface). While the drilling showed "strong and apparently continuous oxidized zinc-lead mineralization of ore grade ... at and below the 2650' elevation ... no sulphides were encountered, and the property was returned to Hecla" (Betmanis, 1986).

1969: Cominco (1969) drills a 454m (1,491 ft) hole (DDH-B2) on the eastern present-day Tic 1 claim. The hole was collared in Active Formation shales, passed through a fault and into Reno Formation quartzites at 400m (1,311 ft), missing the important Reeves Formation section.

1973-74: Under an agreement with Hecla, Reeves MacDonald Mines advanced the heading of their Annex Mine 800 level "about 700 feet in the Redbird property and fifteen hole totalling 6200 feet were diamond drilled; holes from the easterly part of the heading encountered oxide zinc-lead mineralization, some of ore grade, while four holes drilled from the face encountered four separate bands of zinc-lead sulphide mineralization, each about 20 feet in width, averaging 0.56 oz silver, 0.12% lead, 4.18% zinc and 0.04% cadmium. The grades are comparable to those of the ore mined by Reeves MacDonald (Klein, 1985b).

1975: The Reeves-MacDonald Mine closed and no further work was done on the 800 level working.

1981: Gerald Klein stakes the NOR 2 and NOR 3 claims.

1981-84: The NOR claims were explored by Northgane Minerals Ltd (Price, 1992). In 1982 airborne magnetic and VLF-electromagnetic surveys (130 line kilometers) were flown over the NOR claims (Pezzot & Vincent, 1982).

Circa 1984: Hecla Mining Company acquired Day Mines Inc. and the Caviar prospect claims (Klein, 1989).

1985: Golden Eye Minerals leased the Redbird, the Grouse and the Caviar properties from Diem Mines Ltd., a subsidiary of Hecla (Price, 1987).

1985: Golden Eye optioned the NOR claims from Gerald Klein (Price, 1987) and staked the adjoining TIC claims.

1985: Late in 1985, Golden Eye optioned the property to Teck Corporation.

1985-86: Golden Eye Minerals and Teck Exploration Limited built 6.5 km of new bush road to access the Redbird showings from the west. Six deep core holes were attempted (three completed) for a total of 2,691 m (8,829 ft) on western projections of the Reeves-Redbird corridor beneath the Active Formation cap. The best intersection was in hole GE-86-5 which was targeted on Zone D (Redbird Zone) and intersected 18.0m of limonitic material in a section of very poor recovery where values ranged from 0.03 - 8.95% Zn and 0.027.2% Pb. These results were not thought to be representative. At the base of this intersection, a section of good recovery in a dolostone breccia with sulphide mineralization returned 5.64% Zn and 0.38% Pb over 1.6m (5.2 ft) (Betmanis, 1986; Klein, 1986).

1986-88: Eight diamond drill holes were completed by Golden Eye Minerals, including three deep drill holes seeking sulphides on the western extension of the Reeves corridor beneath the Active Formation. Drill hole GE-87-1 intersected Zone M (Annex Zone) at depth and returned 16.3m (53.8 ft) grading 7.97% Zn, 0.88% Pb and 1.64 opt Ag in sulphide mineralization. Holes GE-87-3 and GE-88-1 also intersected the Zone M (Annex Zone) sulphide mineralization. The Beer Bottle showing (Zone B) was also sampled (Klein, 1987, 1988a).

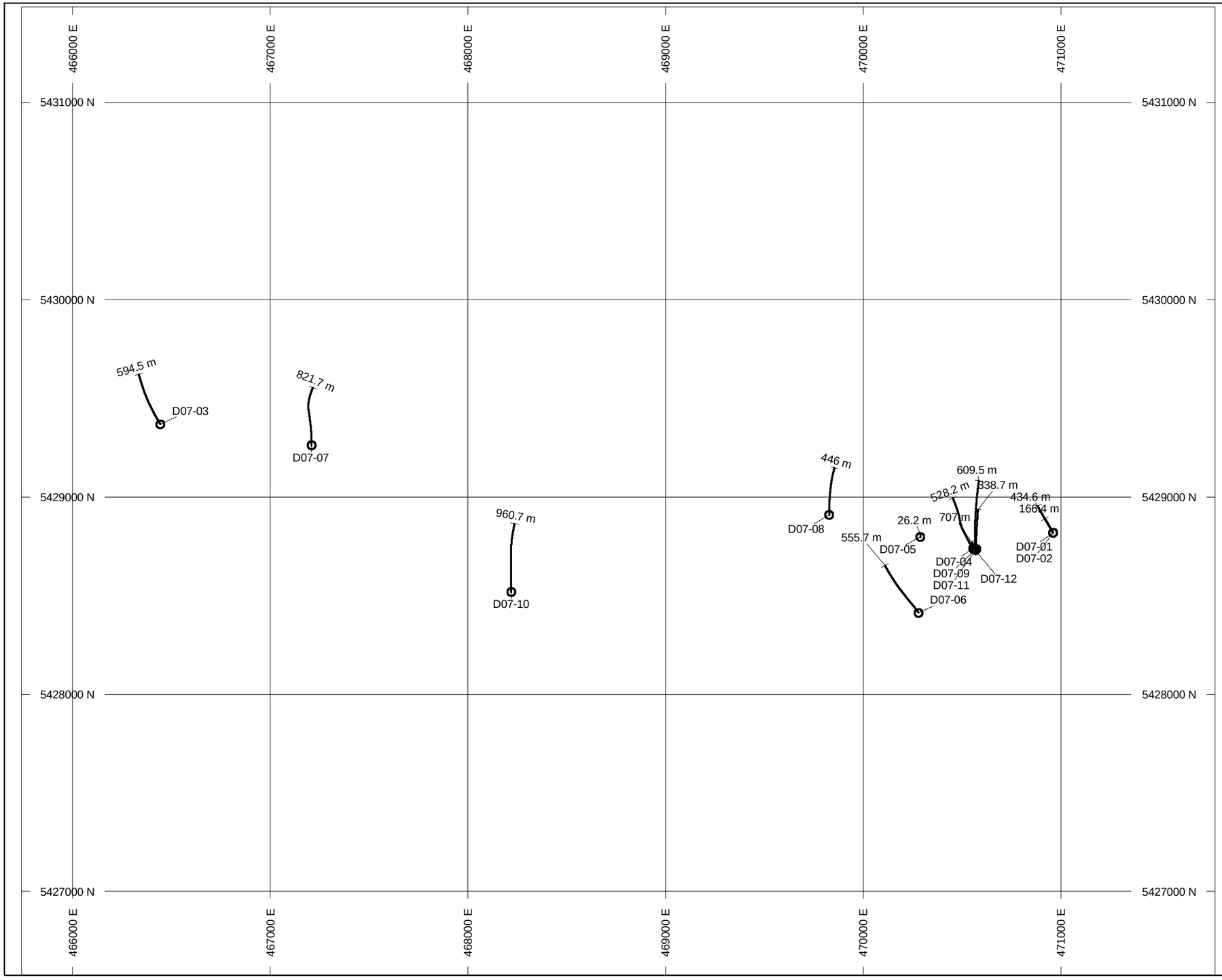
1989: Klein (1999b) carried out a small soil geochemical survey on the NOR claims near the headwaters of Harcourt Creek.

1991-92: Reconnaissance soil, stream silt and rock sampling work was carried out by Annex Exploration Corp. (the successor to Golden Eye) in the Church Creek, Harcourt Creek and Russian Creek areas with "inconclusive" results. The Caviar prospect was mapped and sampled. Metallurgical testing was done on a 100 kg bulk sample collected from the Zone B (Beer Bottle Zone) zinc oxides (Price, 1992).

1994-99:	Redhawk Resources, the successor to Annex Exploration, consolidated the various Redbird property claims through a number of agreements and acquired additional claims in the area.
1998:	Redhawk carried out 1,476m of deep core drilling on Zone M (Annex Zone). One new hole, 98-1, and a directional drilling cut (98-1 A) was drilled off it. The holes intersected 12.9m of 3.35% Zn and 10.9m of 4.75% Zn respectively. A directional cut off hole 87-1 (87-1A) intersected 10.3m of7.61% Zn. (Klein,1998 & 1999a).
2000:	ZincOx Resources of London, England signed an option agreement with Redhawk Resources to earn a 50% interest in the Remac zinc oxide project covering both the Redbird and Reeves properties. A 21 hole reverse circulation drilling and trenching program is conducted. ZincOx opts to withdraw from the option agreement.
2004:	Redhawk Resources conducted a small drill program to test the depth and extent of Zone A mineralization.
2005:	A geochemical soil sampling program is conducted by Redhawk to map the stratigraphic and structural relationships along a corridor from Zone A to the headwaters of Harcourt Creek. Based on this program, ReMac turns its attention from the oxide zone to locating a new sulphide zone along the trend from Reeves MacDonald.
2007:	The ReMac Zinc project is purchased by ReMac Zinc Development Corp. who in turn conducted the 12 hole, 6189.3 metre diamond drill program described in this report.

APPENDIX

IV. DRILL HOLE SECTIONS



HOLES PLOTTED

TOTAL 12

D07-01	D07-02	D07-03	D07-04	D07-05	D07-06
D07-07	D07-08	D07-09	D07-10	D07-11	D07-12

PLAN SPECS:

REF. PT. E, N	468800 m	5429000 m
EXTENTS	6035 m	4907 m

SCALE 1 : 20000

(m)

-200 0 200 400 600 800

*unknown

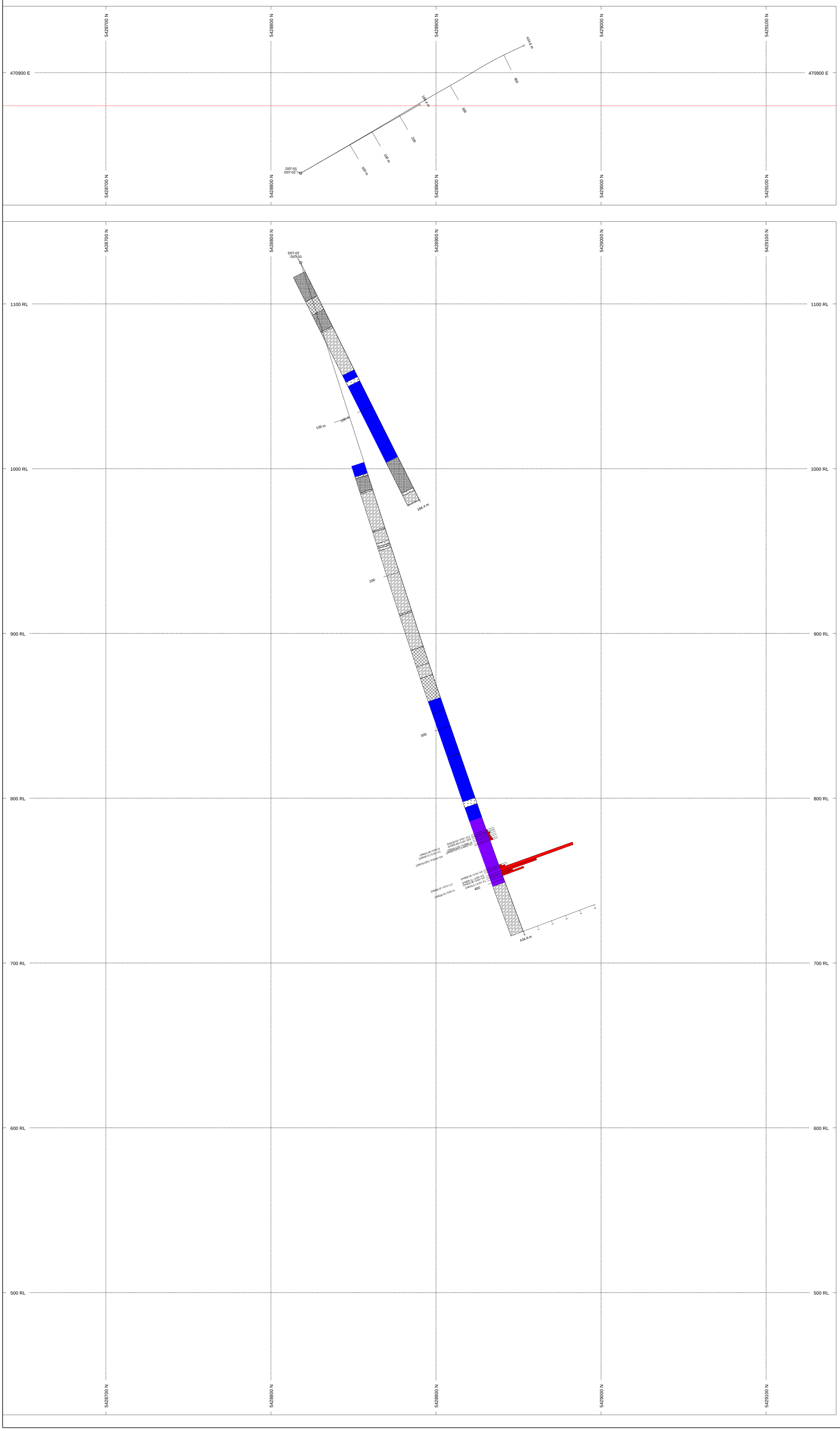
N
W E
S

ReMac Zinc Development Corp.

ReMac Zinc Project

Nelson Mining Division, BC

Figure A



HOLES PLOTTED

TOTAL 2

D07-01 D07-02

BAR GRAPHS	L/R	COL
Zn__	R	

ROCK CODES	L/R	PAT	LABEL	DESCRIPTION
Lithology	L		AC	Active
			DY	Dyke
			ES	Emerald Black Schist
			FL	Fault zone
			RD	Reeves Dolomite
			RL	Reeves Limestone
			TS	Truman Schist/Green Phyllites

POSTED TEXT	L/R	TEXT	ITEMS
Zn_Pb_Ag	L	------	All

SECTION SPECS:

REF. PT. E, N	470920 m	5428890 m
EXTENTS	505 m	724.3 m
SECTION TOP, BOT	1150 m	425.7 m
TOLERANCE +/-	72.5 m	

SCALE 1 : 1000

(m)

-10 0 10 20 30 40

*unknown

AZIMUTH = 0°

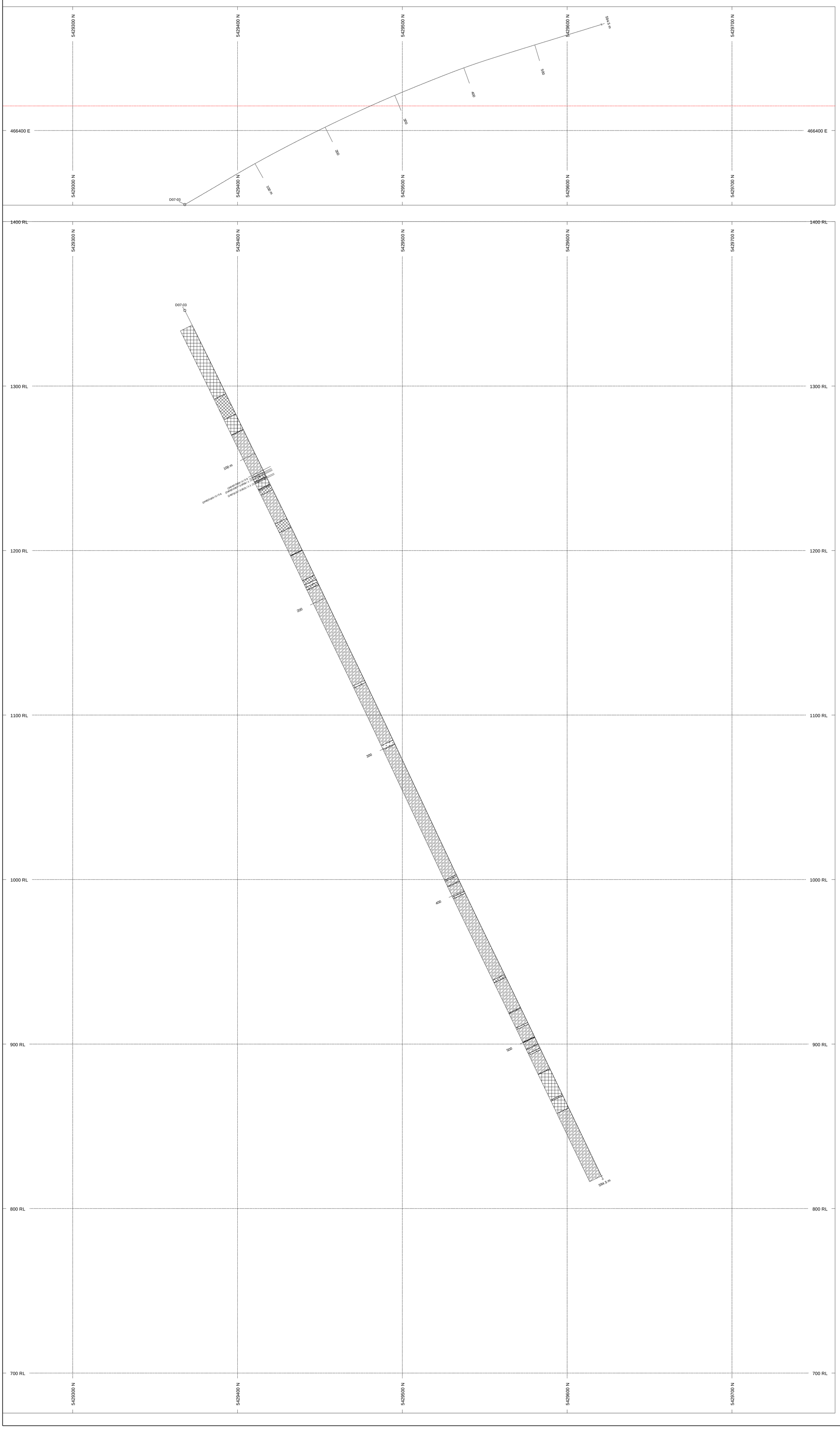
N W E S

ReMac Zinc Development Corp.

ReMac Zinc Project

Nelson Mining Division, BC

Figure B



HOLES PLOTTED

TOTAL 1

D07-03

BAR GRAPHS	L/R	COL
Zn__	R	

ROCK CODES	L/R	PAT	LABEL	DESCRIPTION
Lithology	L		AC	Active
			DY	Dyke
			ES	Emerald Black Schist
			FL	Fault zone

POSTED TEXT	L/R	TEXT	ITEMS
Zn_Pb_Ag	L	-------	All

SECTION SPECS:

REF. PT. E, N	466385 m	5429510 m
EXTENTS	505 m	724.3 m
SECTION TOP, BOT	1400 m	675.7 m
TOLERANCE +/-	139.5 m	

SCALE 1 : 1000

(m)

-10 0 10 20 30 40

*unknown

AZIMUTH = 0°

N W E S

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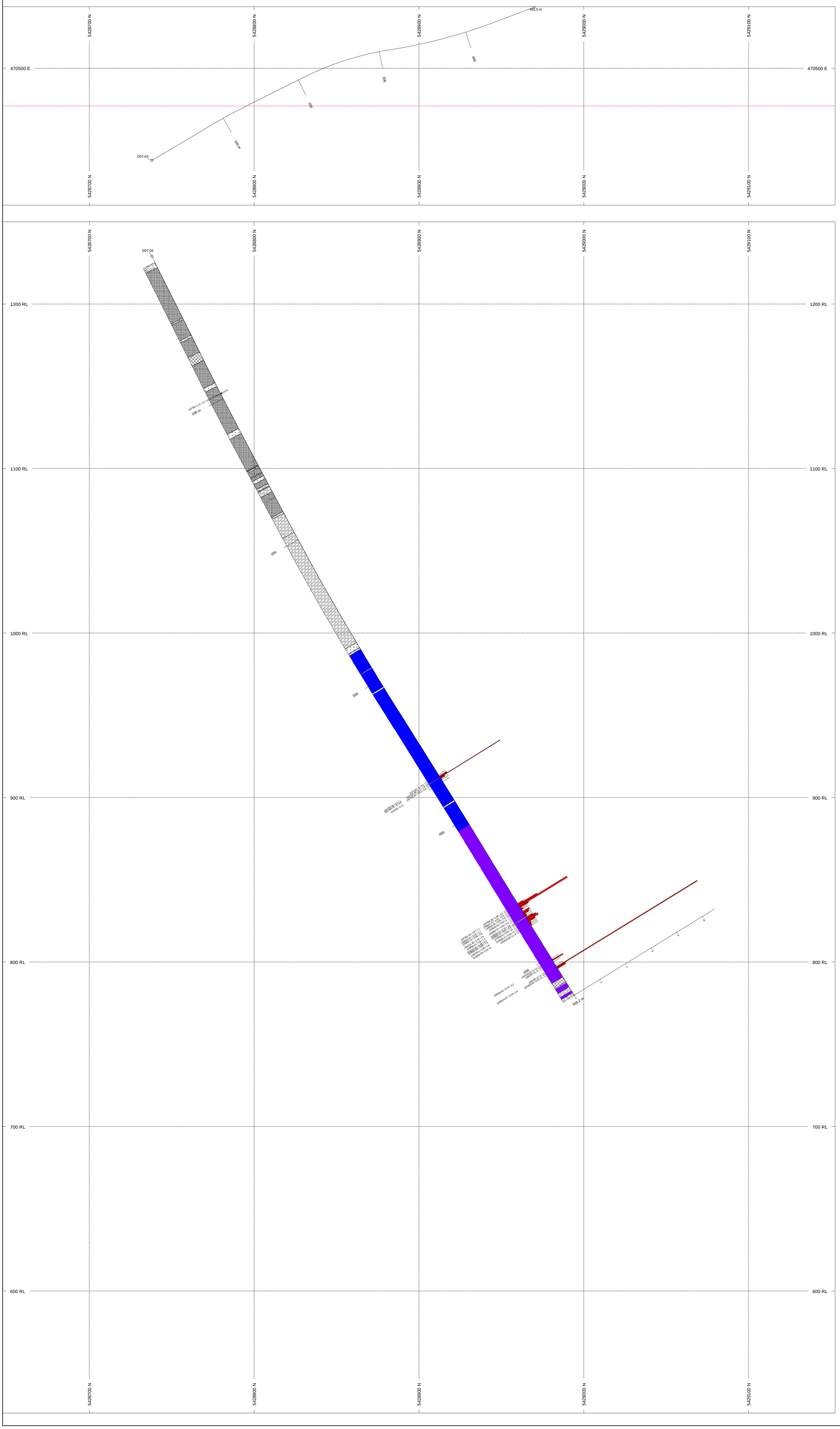
Nelson Mining Division, BC

Figure C



HOLES PLOTTED

TOTAL 1

D07-04

BAR GRAPHS	L/R	COL
Zn__	R	

ROCK CODES	L/R	PAT	LABEL	DESCRIPTION
Lithology	L		AC	Active
			DY	Dyke
			ES	Emerald Black Schist
			FL	Fault zone
			OV	Overburden
			RD	Reeves Dolomite
			RL	Reeves Limestone
			TS	Truman Schist/Green Phyllites

POSTED TEXT	L/R	TEXT	ITEMS
Zn_Pb_Ag	L	-------	All

SECTION SPECS:

REF. PT. E, N	470523 m	5428900 m
EXTENTS	505 m	724.3 m
SECTION TOP, BOT	1250 m	525.7 m
TOLERANCE +/-	164 m	

SCALE 1 : 1000

(m)

-10 0 10 20 30 40

*unknown

AZIMUTH = 0°

N W E S

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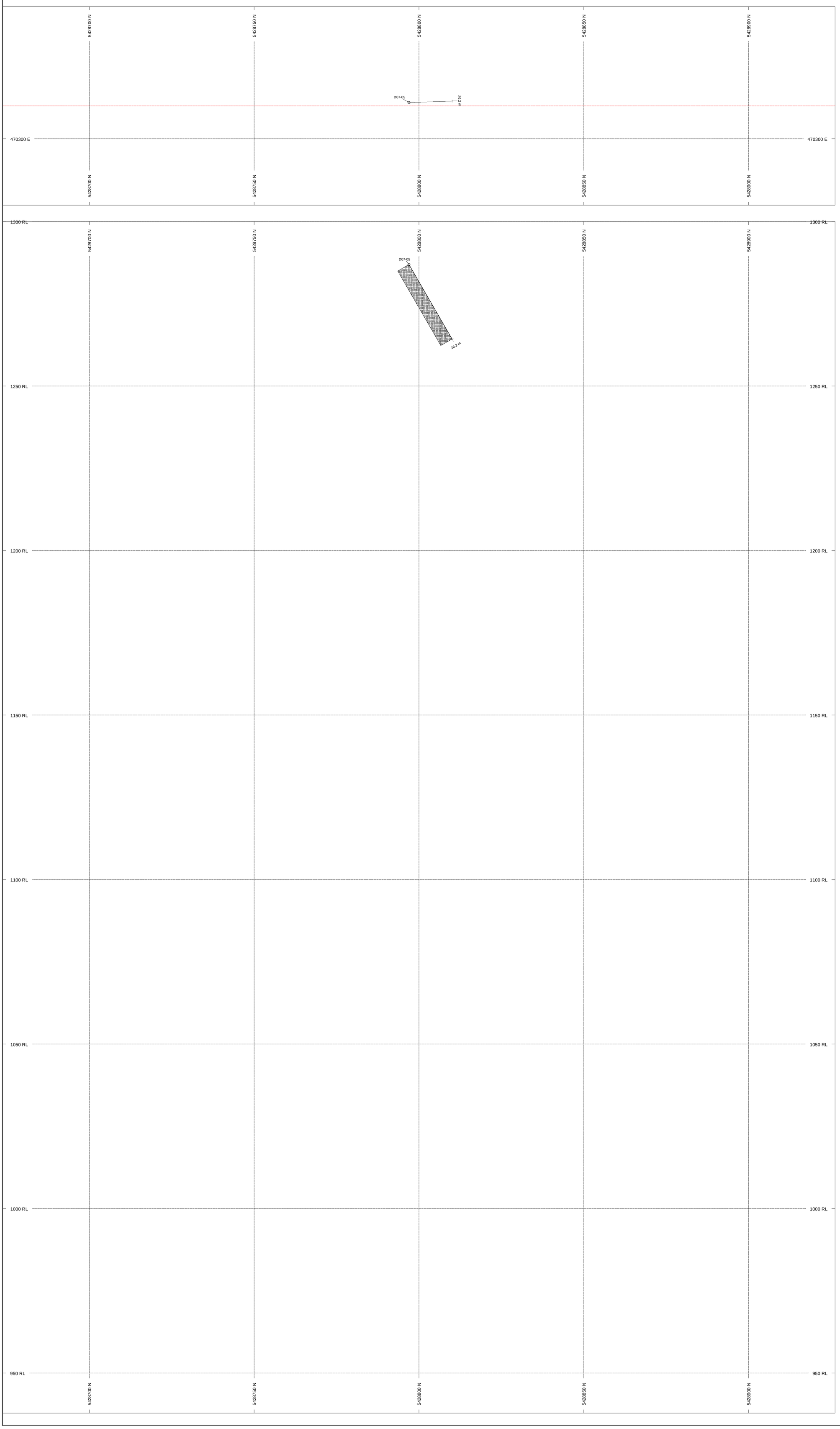
Figure D



HOLES PLOTTED

TOTAL 1

D07-05

BAR GRAPHS	L/R	COL
Zn__	R	

ROCK CODES	L/R	PAT	LABEL	DESCRIPTION
Lithology	L		AC	Active

POSTED TEXT	L/R	TEXT	ITEMS
Zn_Pb_Ag	L	-------	All

SECTION SPECS:

REF. PT. E, N	470290 m	5428800 m
EXTENTS	252.5 m	362.1 m
SECTION TOP, BOT	1300 m	937.9 m
TOLERANCE +/-	64 m	

SCALE 1 : 500

(m)

-5 0 5 10 15 20

*unknown

AZIMUTH = 0°

N W E S

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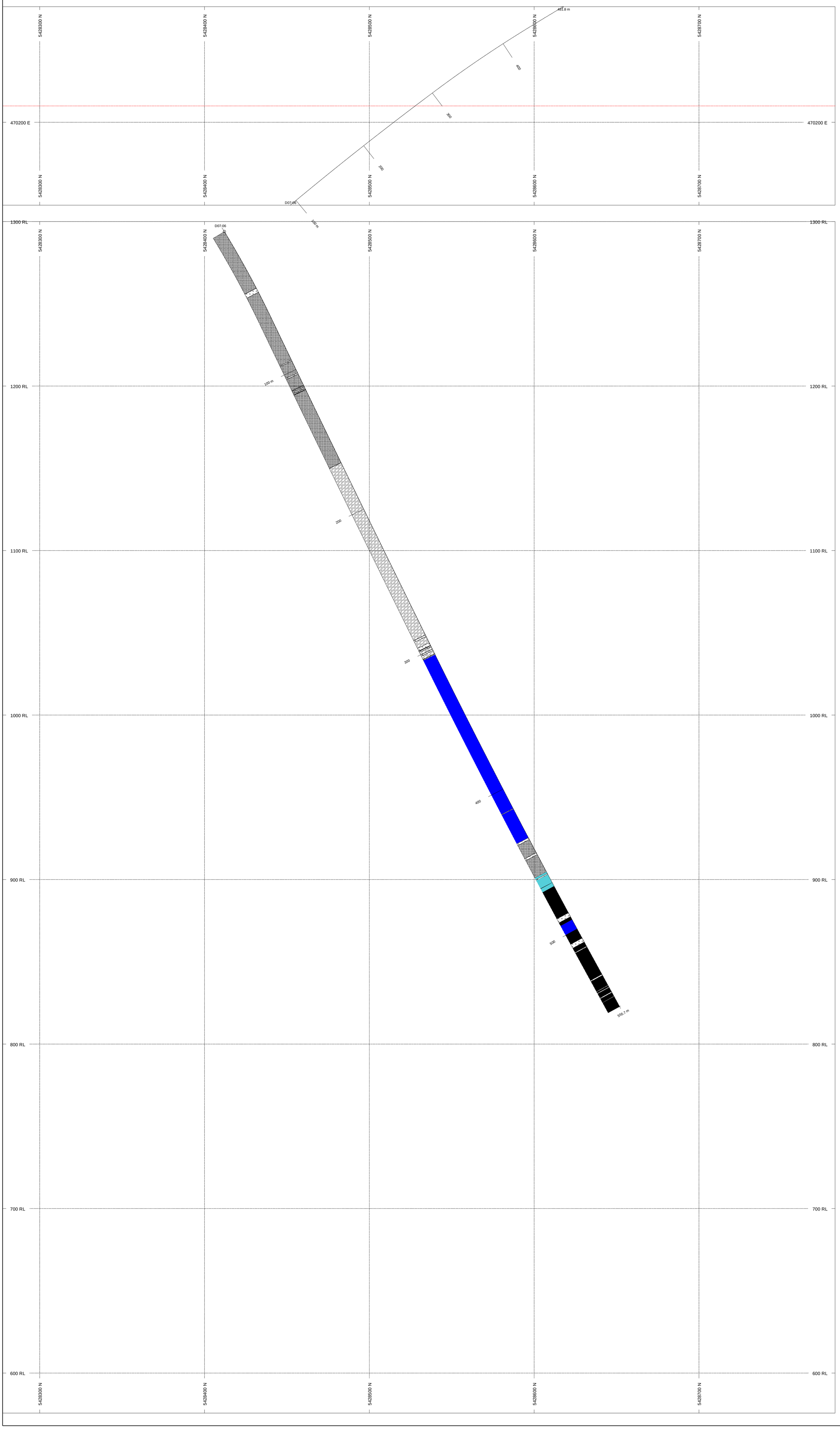
Figure E



HOLES PLOTTED

TOTAL 1

D07-06

BAR GRAPHS	L/R	COL
Zn__	R	

ROCK CODES	L/R	PAT	LABEL	DESCRIPTION
Lithology	L		AC	Active
			DY	Dyke
			ES	Emerald Black Schist
			KP	Klein Phyllite
			RL	Reeves Limestone
			TL	Truman Limestone

POSTED TEXT	L/R	TEXT	ITEMS
Zn_Pb_Ag	L	-------	All

SECTION SPECS:

REF. PT. E, N	470190 m	5428530 m
EXTENTS	505 m	724.3 m
SECTION TOP, BOT	1300 m	575.7 m
TOLERANCE +/-	175 m	

SCALE 1 : 1000

(m)

-10 0 10 20 30 40

*unknown

AZIMUTH = 0°

N W E S

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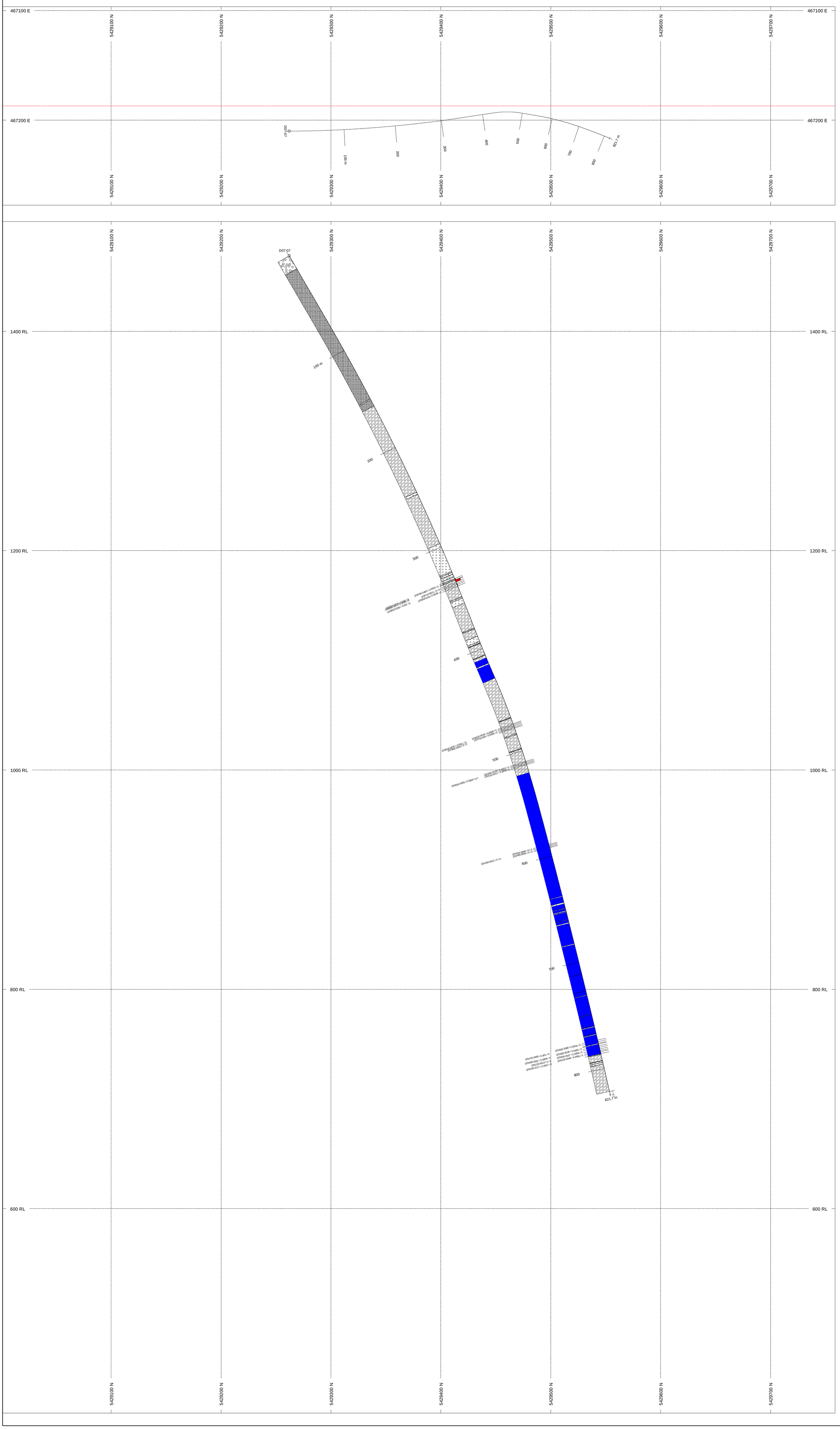
Figure F



HOLES PLOTTED

TOTAL 1

D07-07

BAR GRAPHS	L/R	COL
Zn__	R	

ROCK CODES	L/R	PAT	LABEL	DESCRIPTION
Lithology	L		AC	Active
			DY	Dyke
			EB	Emerald black schist
			ES	Emerald Black Schist
			FL	Fault zone
			OV	Overburden
			RL	Reeves Limestone
			TS	Truman Schist/Green Phyllites

POSTED TEXT	L/R	TEXT	ITEMS
Zn_Pb_Ag	L	-------	All

SECTION SPECS:

REF. PT. E, N	467187 m	5429380 m
EXTENTS	757.4 m	1086 m
SECTION TOP, BOT	1500 m	413.6 m
TOLERANCE +/-	195.5 m	

SCALE 1 : 1500

(m)

-20 0 20 40 60

*unknown

AZIMUTH = 0°

N W E S

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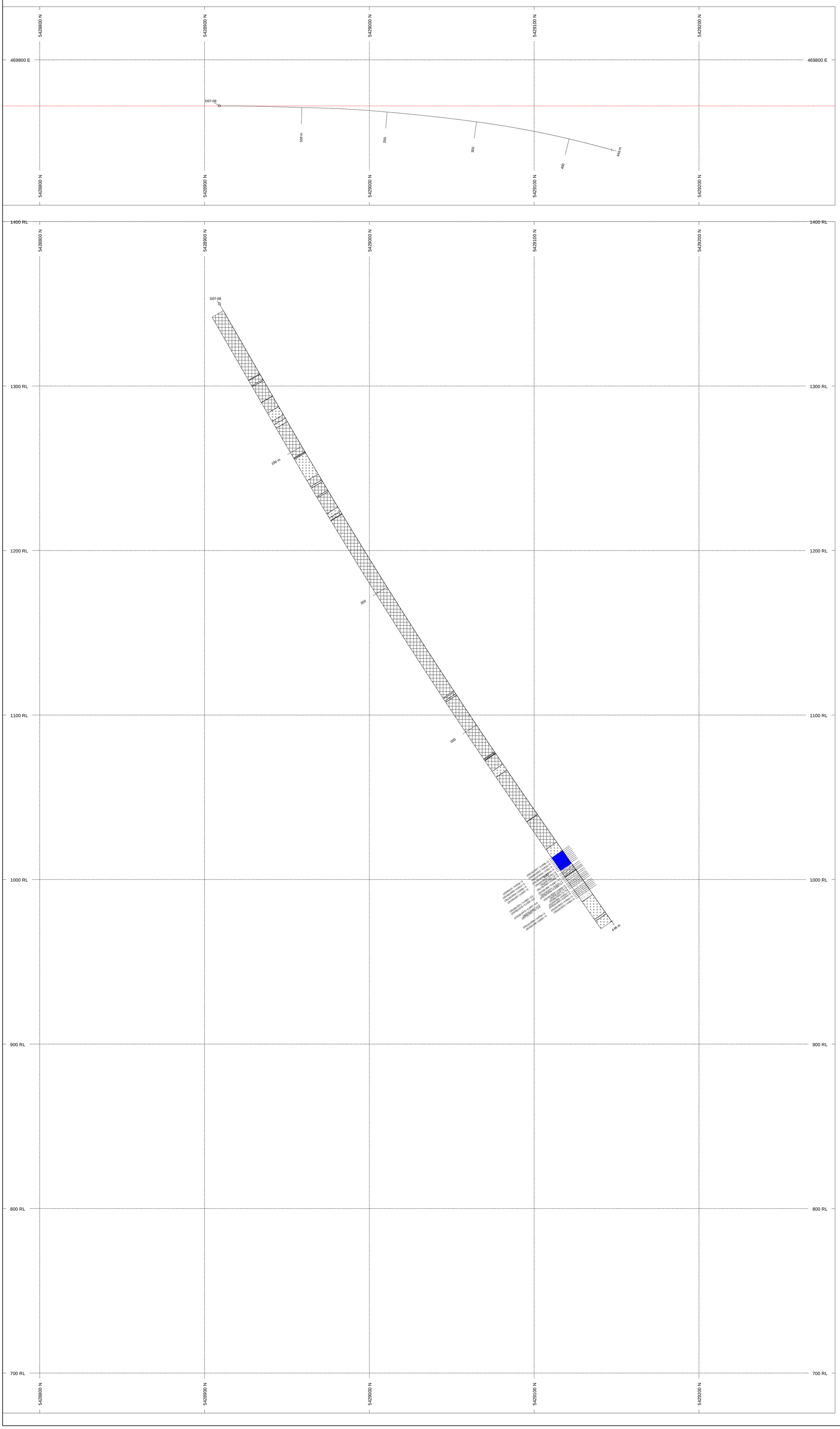
Nelson Mining Division, BC

Figure G



HOLES PLOTTED

TOTAL 1

D07-08

BAR GRAPHS	L/R	COL
Zn__	R	

ROCK CODES	L/R	PAT	LABEL	DESCRIPTION
Lithology	L		AC	Active
			DY	Dyke
			RL	Reeves Limestone
			RQ	Reno Quartzites
			TS	Truman Schist/Green Phyllites

POSTED TEXT	L/R	TEXT	ITEMS
Zn_Pb_Ag	L	-------	All

SECTION SPECS:

REF. PT. E, N	469828 m	5429030 m
EXTENTS	505 m	724.3 m
SECTION TOP, BOT	1400 m	675.7 m
TOLERANCE +/-	124.5 m	

SCALE 1 : 1000

(m)

-10 0 10 20 30 40

*unknown

AZIMUTH = 0°

N W E S

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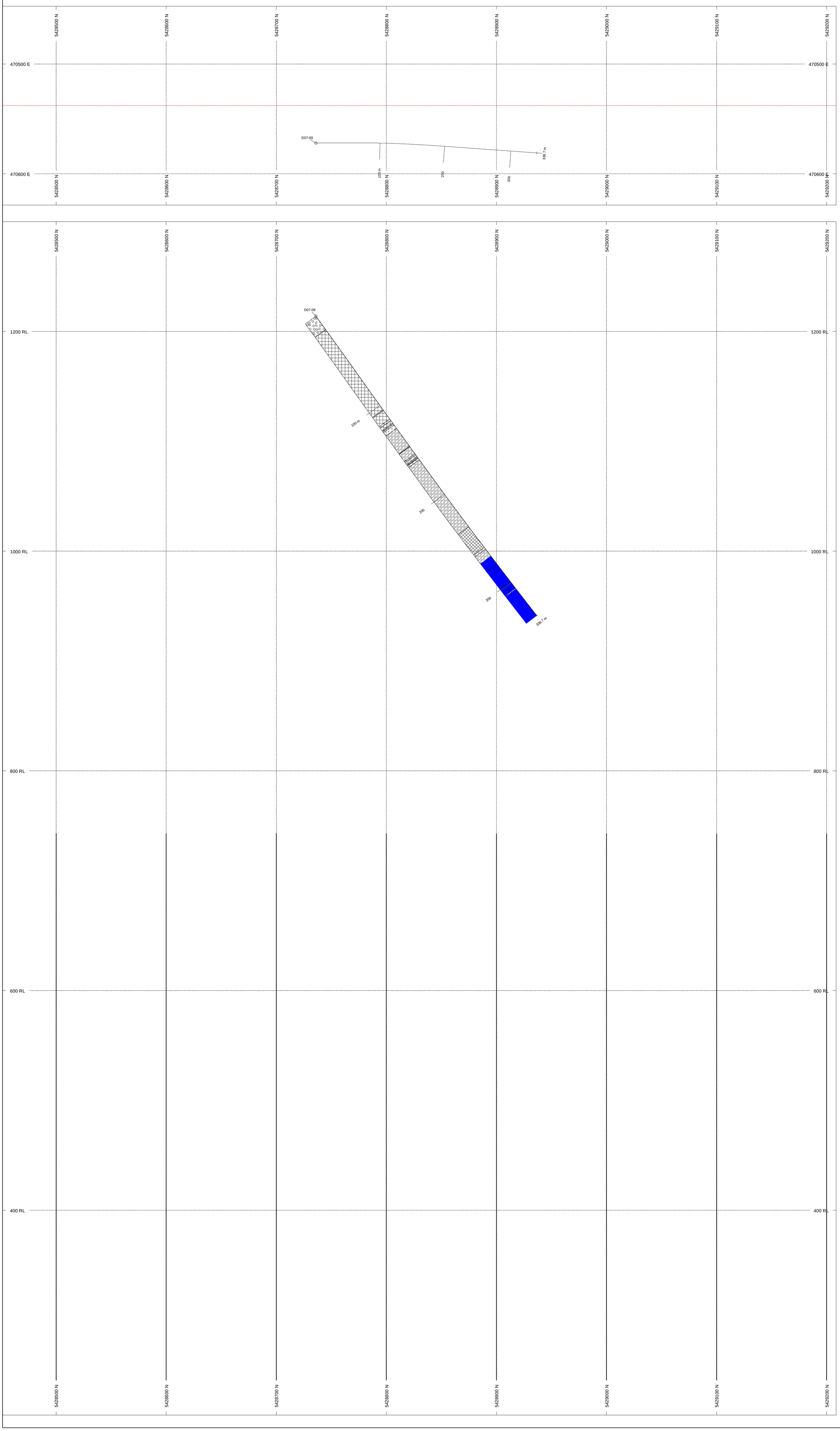
ReMac Zinc Project

Nelson Mining Division, BC

Figure H



HOLES PLOTTED

TOTAL 1

D07-09

BAR GRAPHS	L/R	COL
Zn__	R	

ROCK CODES	L/R	PAT	LABEL	DESCRIPTION
Lithology	L		AC	Active
			DY	Dyke
			ES	Emerald Black Schist
			FL	Fault zone
			OV	Overburden
			RL	Reeves Limestone
			TS	Truman Schist/Green Phyllites

POSTED TEXT	L/R	TEXT	ITEMS
Zn_Pb_Ag	L	-------	All

SECTION SPECS:

REF. PT. E, N	470538 m	5428830 m
EXTENTS	757.4 m	1086 m
SECTION TOP, BOT	1300 m	213.6 m
TOLERANCE +/-	121.5 m	

SCALE 1 : 1500

(m)

-20 0 20 40 60

*unknown

AZIMUTH = 0°

N W E S

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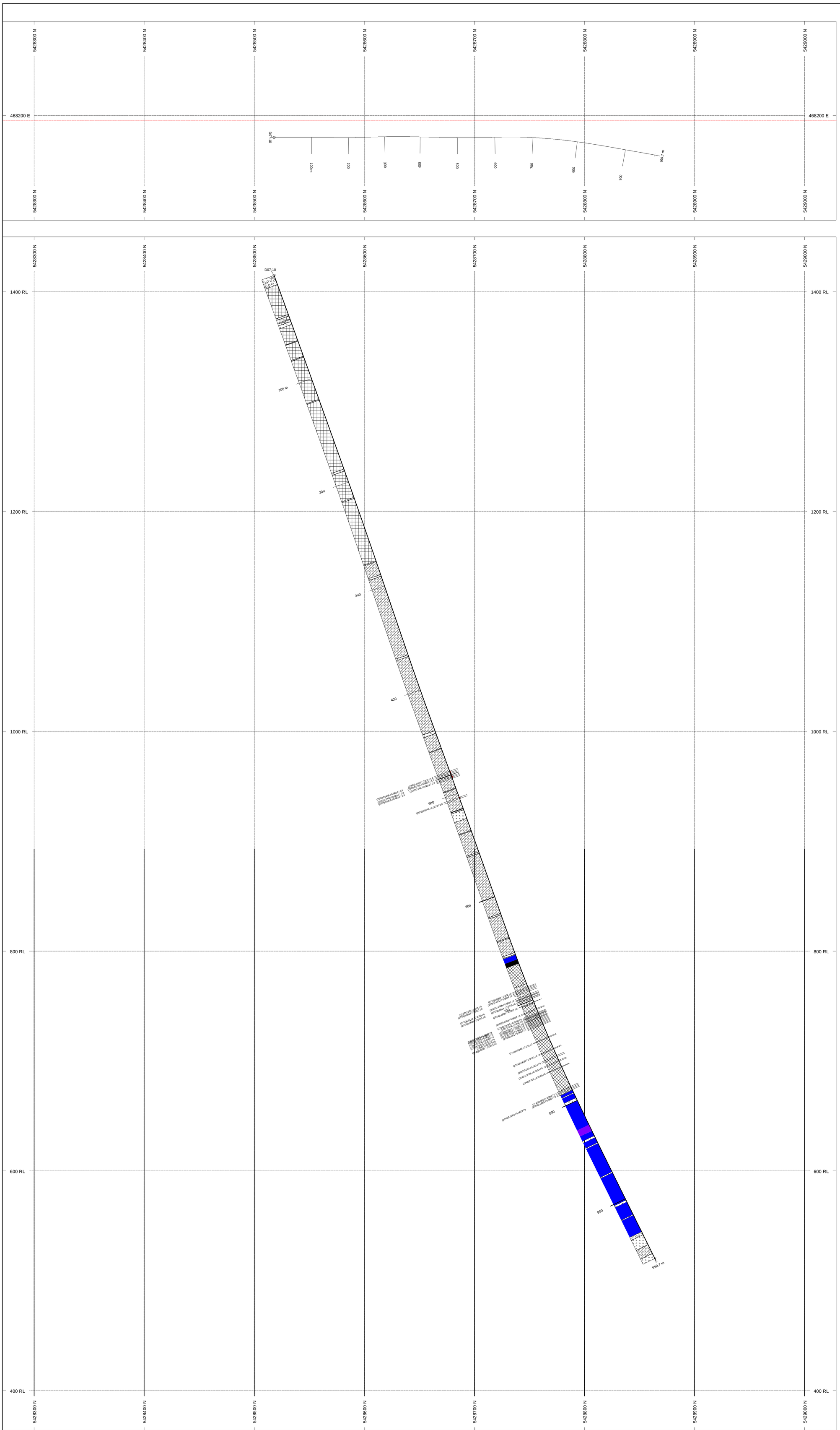
ReMac Zinc Project

Nelson Mining Division, BC

Figure I



HOLES PLOTTED

TOTAL 1

D07-10

BAR GRAPHS	L/R	COL
Zn__	R	

ROCK CODES Lithology	L/R	PAT	LABEL	DESCRIPTION
	L		AC	Active
			DY	Dyke
			EP	Eugene Pool
			ES	Emerald Black Schist
			KP	Klein Phyllite
			OV	Overburden
			RD	Reeves Dolomite
			RL	Reeves Limestone

POSTED TEXT	L/R	TEXT	ITEMS
Zn_Pb_Ag	L	------	All

SECTION SPECS:

REF. PT. E, N	468205 m	5428650 m
EXTENTS	757.4 m	1086 m
SECTION TOP, BOT	1450 m	363.6 m
TOLERANCE +/-	187 m	

SCALE 1 : 1500

(m)

-20 0 20 40 60

*unknown

AZIMUTH = 0°

N W E S

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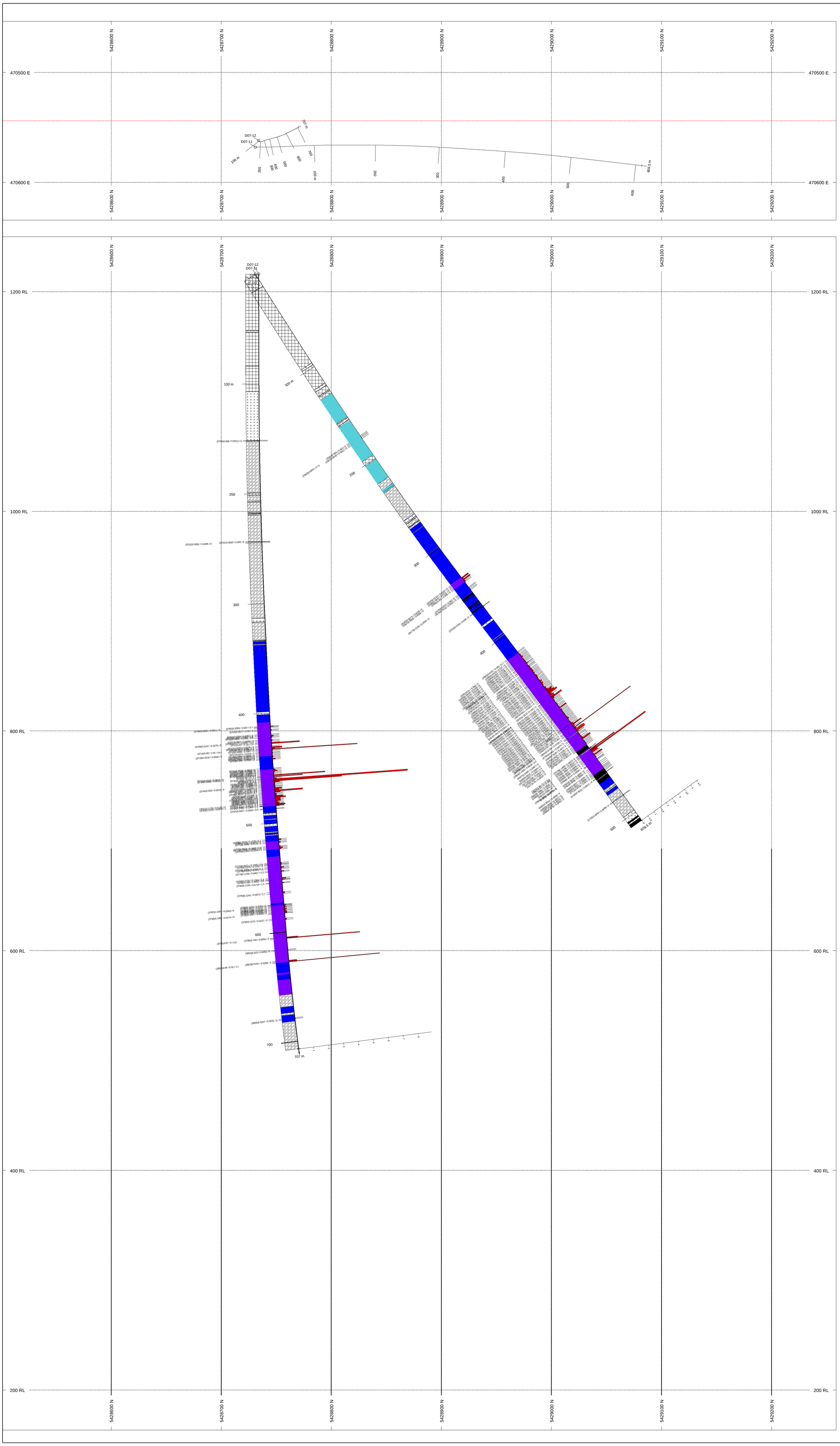
ReMac Zinc Project

Nelson Mining Division, BC

Figure J



HOLES PLOTTED

TOTAL 2

D07-11 D07-12

BAR GRAPHS	L/R	COL
Zn__	R	

ROCK CODES	L/R	PAT	LABEL	DESCRIPTION
Lithology	L		AC	Active
			DY	Dyke
			ES	Emerald Black Schist
			FL	Fault zone
			KP	Klein Phyllite
			KS	Klein Schist
			OV	Overburden
			RD	Reeves Dolomite
			RL	Reeves Limestone
			TL	Truman Limestone
			TS	Truman Schist/Green Phyllites

POSTED TEXT	L/R	TEXT	ITEMS
Zn_Pb_Ag	L	-------	All

SECTION SPECS:

REF. PT. E, N	470544 m	5428880 m
EXTENTS	757.4 m	1086 m
SECTION TOP, BOT	1250 m	163.6 m
TOLERANCE +/-	194 m	

SCALE 1 : 1500

(m)

-20 0 20 40 60

*unknown

AZIMUTH = 0°

N W E S

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ReMac Zinc Project

Nelson Mining Division, BC

Figure K

APPENDIX

V. 2007 DRILL LOGS AND LOGGING CODES

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-01	0.00	6.10	HQ	n/a	CASI																									
D07-01	6.10	23.10	HQ	AC	BLPH	bk	BN						BD	40						L	<<1%			L	1%					Active Fm. Qzt in thin laminations & occasional veins & veinlets. Py in conformable bands. Bedding measured perpedicular to core axis.
D07-01	23.10	32.54	HQ	FL	BLPH	bk	BN	FL					BD							A	1%			L	2%					Very broken with irreg & concordant qtz veins and veinlets. Some empty vugs partially filled with qtz. FAULT ZONE?
D07-01	32.54	44.40	HQ	AC	BLPH	bk	BN						BD	38										/	2%					
D07-01	44.40	45.24	NQ	DY	QZMO	gn gy	EQ																	S	<<1%					Qzt 30%, Feld 30%, Bio 3-5%; mafics (amphiboles?) 2-3%
D07-01	45.24	56.10	NQ	ES	BLPH	bl gy	BN						BD	34																Rusty iron carbonate (ankerite?) in laminations and banding, in places crenulated. Laminations semiparallel to bedding. Bedding measured perpendicular to core axis. 5% ankerite, crenulated / contorted laminations.
D07-01	56.10	66.90	NQ	ES	SCPH	bl gy	BN						BD	38																1% ankerite, crenulated / contorted laminations.
D07-01	66.90	71.24	NQ	ES	SCPH	bl gy	BN						BD																	3% ankerite, crenulated / contorted laminations.
D07-01	71.24	73.63	NQ	ES	SCPH	bl gy	BN						BD																	30% ankerite, crenulated / contorted laminations.
D07-01	73.63	74.98	NQ	ES	SCPH	bl gy	BN						BD	32																1% ankerite, crenulated / contorted laminations.
D07-01	74.98	79.76	NQ	RL	SCPH	bl gy	BN						BD																	Contorted ankerite bands and laminations. 20% ankerite
D07-01	79.76	82.61	NQ	DY	MONZ	bl tan	EQ																	S	<<1%					Fine grained, equigranular.
D07-01	82.61	84.88	NQ	RL	LMST	bl gy	BN																	S	<<1%			A	<<1%	
D07-01	84.88	89.11	NQ	RL	LMST	tan	BN																	S	<<1%	S	<<1%			Thinly laminated, tan colour (ankerite?), calcite and ankerite?
D07-01	89.11	94.77	NQ	RL	LMST	lt gy	BN						BD	45										S	<<1%			A	<<1%	Lt grey, dk gy and tan laminations
D07-01	94.77	96.48	NQ	RL	LMST	lt gy	BD	CN		CR			BD	43																Very contorted laminations.
D07-01	96.48	99.36	NQ	RL	LMST	lt gy	BN						BD	43										S	<<1%					Some 2-3cm bands and irregular blebs and blobs of calcite.
D07-01	99.36	105.51	NQ	RL	LMST	lt gy	BN																					A	<<1%	
D07-01	105.51	122.30	NQ	RL	LMST	tan	BD	CR					BD	40												S	<<1%	A	<<1%	Concordant bands of tan Ca with Fe? Vugs (<<1%) in veins & veinlets of leached sulphides?
D07-01	122.30	129.29	NQ	RL	LMST	bl tan	BN	CR																						
D07-01	129.29	135.86	NQ	RL	LMST	bl tan	BN	CR																						Concordant, crenulated and contorted bands of tan mixture of Ca and ankerite(?) (iron oxides).
D07-01	135.86	152.54	NQ	AC	BKSH	bk	BN	FL					BD	25										S	<<1%					Active Fm broken up; contact is fault zone.
D07-01	152.54	157.55	NQ	AC	BKSH	bk	BN						BD	15																Very brokien, fault zone that stops at next contact with dyke.
D07-01	157.55	159.27	NQ	DY	LMDK	bl gy	EQ																							
D07-01	159.27	165.89	NQ	ES	SCPH	bl gy	BN						BD	20																Concordant and minor crosscutgting veinlets of white and light brown calcite (with Fe?) about 7%.
D07-01	165.89	166.42	NQ	DY	LMDK	bl gy	EQ																							Concordant and minor crosscutting veinlets of white and brown calcite (with Fe?) about 7%. Summary. NQ rods got stuck at 166.32m and an attemp to ream down with HQ failed at …m (...ft). All the rods were lost except for 2 10-ft HQ rods. Geology, as
D07-02	0.00	128.91	HQ	TR	TRCO																									Triconing.
D07-02	128.91	134.37	HQ	RL	LMST	br gy	BN						BD	35																Grey and white, banded lmst with minor bands of concordant banded calcitge veins (Fe?). Core angle perpendicular to core axis.
D07-02	134.37	135.94	HQ	RL	LMST	lt gy	BN																							Abndt. Blebs, patches and semiconcordant white bands (lmst).
D07-02	135.94	137.19	HQ	FL	LMST	lt gy	BN		40	FL	5																			Fault contact?
D07-02	137.19	138.99	HQ	AC	BLPH	br bk	BN																							Concordant LMST and BLPH (or Truman?). The core angle flatten to almost 0 degrees (perpendicular to core axis).
D07-02	138.99	143.28	HQ	AC	BLPH	bk	BN	FL		BN			F/																	Very fractured fault zone.
D07-02	143.28	146.30	HQ	AC	BLPH	bk	BD						BD	30																
D07-02	146.30	147.06	HQ	DY	LMDK	gn tan	EQ						F/																	Fine grained, with wlongated spicules of magnetite (<=1%)
D07-02	147.06	148.13	HQ	ES	SCPH	br bk	BD						BD	40																Phyllite with schistose bands, some tan veins with iron oxides.
D07-02	148.13	148.46	HQ	ES	Clay	gn gy	MS																							
D07-02	148.46	154.50	HQ	ES	SCPH	br bk	BD																							
D07-02	154.50	157.89	HQ	ES	SCPH	bk	BD						BD	45																
D07-02	157.89	159.45	HQ	ES	SCPH	bk	BD															I	3%							Irregular & concordant quartz bands and veins.
D07-02	159.45	162.36	HQ	ES	PHYL	bk	BD																							
D07-02	162.36	171.08	HQ	ES	SCPH	br bk	BD																							Phyllite with schistose bands. Some concordant & contorted veins with iron oxides.
D07-02	171.08	171.83	HQ	DY	LMDK	dk gy	EQ																							Chilled fine to medium grained margins with porphyritic (Feld phenocrysts, up to 2mm and about 20% of rock.
D07-02	171.83	179.32	HQ	ES	PHLM	dk gy	BD						BD	45																Concordant and minor contorted bands of white limestonbe.

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-02	179.32	181.20	HQ	DY	LMDK	dk gy	EQ																	S	tr					Fine grained lamprophyre.
D07-02	181.20	182.32	HQ	ES	PHLM	BR GY	BD																							Concordant and contorted veins of white limestone with monor bands of light bgrown iron oxides (Fe from ??).
D07-02	182.32	183.79	HQ	DY	LMDK	bl gr	EQ						F/																	Fine grained lamprophyre. FAULT ZONE.
D07-02	183.79	196.29	HQ	ES	PHLM	dk gy	BD	SC	40				BD	40																Concordant and contorted bands of argillite and limestone. Angles PCA.
D07-02	196.29	208.79	HQ	ES	PHLM	dk gy	BD						BD	35																Concordant and contorted bands of argillite and limestone. Angles PCA.
D07-02	208.79	211.83	HQ	ES	PHLM	dk gy	BD																							Alternating concordant and crenulated phyllite & limestone bands.
D07-02	211.83	215.50	NQ	ES	PHLM	dk gy	BD						BD	50																Alternating concordant and crenulated phyllite & limestone bands. CA perpendicular to CA.
D07-02	215.50	224.95	NQ	ES	SCHI	dk gy	BD	SC																E	<=1%					Graphitic schist (graphite in schistosity planes, about 2%). Veinlets & specks of Py (=<1%).
D07-02	224.95	225.88	NQ	FL	SCHI															V	<<1%			S	<<1%					In ES.
D07-02	225.88	234.00	NQ	ES	PHLM	lt gy	BD																	S	<<1%					
D07-02	234.00	236.08	NQ	ES	SCHI	bk		SC																						Abundant graphite on schistose planes.
D07-02	236.08	243.91	NQ	ES	PHLM	md gy	BD													A	1%									Thickly laminated argillite with laminae of limestone. Occasional concordant and crosscutting Qz veins.
D07-02	243.91	245.57	NQ	ES	SCHI	bk		SC																S	<<1%					Abundant graphite on schistose planes.
D07-02	245.57	248.24	NQ	ES	SCHI	dk gy	BD	SC					BD	35										S	<<1%					Core angle perpendicular to CA.
D07-02	248.24	259.08	NQ	FL	SCHI																									Very fractured and abndt graphite on bedding laminae planes.
D07-02	259.08	266.51	NQ	ES	SCHI	dk gy	BD	CN																S	<<1%					Core angle several reversals. Occ broken zone to 20 cm.
D07-02	266.51	276.79	NQ	FL	SCHI	dk gy	BD	CN																S	<<1%					Gaugh sections, shiny graphite partings, all angles
D07-02	276.79	281.54	NQ	FL	SCHI										LSH	(								S	<<1%					Shiny graphitic partings. Gouge seds, limy sections.
D07-02	281.54	281.65	NQ	RL	LMST	gy	BD	<<					BD	43					ST											Occ. Rusty partings, core angle perpendicular to CA.
D07-02	281.65	289.32	NQ	RL	LMST	gy	BD						BD	57	LSH	(		X						V	<<1%					Occ. Veinlet Py.
D07-02	289.32	289.39	NQ	DY	CLAY	vr												X												Sandy, dyke?
D07-02	289.39	296.31	NQ	RL	LMST	gy	BD						BD	45				X												Good RL
D07-02	296.31	296.51	NQ	RL	LMST	br	BD											X												
D07-02	296.51	310.06	NQ	RL	LMST	gy	BD						BD	40										V	<<1%					Occ. Py disseminations, veinlet partially limonitic. Bedding perpendicular to CA.
D07-02	310.06	315.53	NQ	RL	LMST	br gy	BD						BD	40				X												Thickly laminated RL with brown, oxidized limonitc laminae. No Zn-Zap reaction in limonites.
D07-02	315.53	317.90	NQ	RL	LMST	lt gy	BD											X	X											
D07-02	317.90	318.13	NQ	DY	MFDY	bk	EQ																	S	10%					Fine-grained mafic dyke (Mafics: about 50%-py, amph, Plag about 50%). DY contact 40 degrees, bgedding 52. degrees perpendicular to CA.
D07-02	318.13	322.01	NQ	RL	LMST	md gy	BD						BD	52				X	X											Occ. Laminae with limonites.
D07-02	322.01	323.62	NQ	RL	LMST	lt gy	BD																							Thickly laminated.
D07-02	323.62	328.52	NQ	RL	LMST	lt gy							BD	50																Thinly laminated
D07-02	328.52	333.20	NQ	RL	LMST	md gy	BD																							Thickly to thinly laminated LMST with intercalations of lt and dk gy laminae.
D07-02	333.20	336.38	NQ	RL	LMST	lt gy	BD																							Thicly laminated LMST with intercalations of lt and dk gy limestone laminae and bands.
D07-02	336.38	347.00	NQ	RL	LMST	lt gy	BD						BD	38																Thinly laminated LMST alternating with lt & dk gy laminae. Angle perpendicular to CA.
D07-02	347.00	350.84	NQ	DY	MFDY	dk gy	EQ																							Fine-grained lamprophyre. Sph??
D07-02	350.84	359.89	NQ	RL	LMST	lt gy	LM																							Interval mafic dyke at 352.97-357.27.
D07-02	359.89	361.33	NQ	RD	DOST	dk gy									CAR	/						B	2%	A	<<1%					Bird's eye LM within massive dolomite. Lower contact transitioned. Occsl. Showing tweedy texture.
D07-02	361.33	364.68	NQ	RD	DOST	dk gy						AU			CAR	/		X	X			B	<=1%			A	<<1%			Fractured laminations occur with remobilized calcite veinlets parallel to core angle. Large calcite crystals @ 364.9
D07-02	364.68	368.05	NQ	RD	DOST	lt gy		BR				AU						X	X											Chaotic orientation, recrystalisation of calcite
D07-02	368.05	369.03	NQ	RD	DOST	lt gy		BR				AU					MD	X	X					G	1%	S	<<1%			Assay:chaotic orientation of breccia
D07-02	369.03	369.71	NQ	RD	DOST	lt gy		BR				AU												G	5%	<	1%	D	tr	assayLarge irregular blocks of sulphide (py). Small 20 cm lamprophyre dyke @ 369.6
D07-02	369.71	370.67	NQ	RD	DOST	LT GY		BR				AU												G	5%	<	1%	D	tr	Assay: Large irreg blocks of sulphide (py) @ 370.67
D07-02	370.67	371.76	NQ	RD	DOST	lt gy		BR				AU												I	2%	D	<=1%	D	tr	assay. More Brecciated, small py. vein @371.60
D07-02	371.76	372.79	NQ	RD	DOST	lt gy		BR				AU												I	2%	D	<=1%	D	tr	Geochem: Sulphides more disseminated, veins and blebs, fracture fill
D07-02	372.79	374.11	NQ	RD	DOST	lt gy		BR				AU												I	2%	D	<=1%	D	tr	geochem:
D07-02	374.11	375.05	NQ	RD	DOST	lt gy		BR				AU												<	<=1%	S	<<1%			geochem: mineralization in small veinlets

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-02	375.05	391.04	NQ	RD	DOST	lt gy		BR				AU												B	<<1%			B	tr	Breccia becomes more massive, whiter, vugs 9<1mm) with calcite crystals @376.35-376-65
D07-02	391.04	391.97	NQ	RD	DOST	WT		BR				Au												G	<=1%	S	<<1%			Irreg. Py vein in mor bx zone.
D07-02	391.97	393.05	NQ	RD	DOST	wt		BR																G	<=1%	<	tr			geochem: More brecciated, sulphidesin veinlets
D07-02	393.05	394.89	NQ	RD	DOST	wt		BR				AU												I	5%	D	<<1%			GEOCHEM:
D07-02	394.89	396.02	NQ	RD	DOST	WT		BR				AU												I	2%	S	<<1%	D	tr	GEOCHEM
D07-02	396.02	396.91	NQ	RD	DOST	wt		BR				AU												G	<=1%	S	<<1%			Geochem
D07-02	396.91	398.06	NQ	RD	DOST	lt gy		BR				AU												G	<=1%	S	<<1%			Geochem: breccia becomes more massive
D07-02	398.06	402.29	NQ	RD	LMST	lt gy		BR																S	<<1%					
D07-02	402.29	418.60	NQ	TS	PHLM	dk gy	LM						BD	35										S	<<1%					
D07-02	418.60	434.64	NQ	TS	SCHI	lt gn	LM						BD	35										E	<=1%					EOH
D07-03	0.00	10.24	HW	n/a	CASI																									
D07-03	10.24	17.07	HQ	AC	BKSH	bk	BD						BD	45			WK													black rock
D07-03	17.07	23.16	HQ	AC	BLPH	bk						TB	BD	88			WK													Vuggy section (3%) @ 22m over 1m width. Low angle to core axis. Appear to be dissolution of calcium carbonate.
D07-03	23.16	39.31	HQ	AC	BLPH	bk	BD																							Core angle vatries from 30-60 Perp. TCA. Small folds of finer grained laminae . Variable carbonate content along laminae.
D07-03	39.31	50.59	HQ	AC	BKSH	bk	BD	FL	60	<<			BD	30			X	X												Laminae of oxidized limonite. One cross fault 5 TCA. Cross cutting oxidized laminae
D07-03	50.59	58.23	HQ	AC	BLPH	bk	LM						BD	37			X													Thinly laminated with limonite laminae of Fe-carbonate. Few contorted laminae. At 48.76 a 0.13m bed with oxidized zone at end (py, ankerite 20%)
D07-03	58.23	72.53	HQ	FL	BLPH	bk	LM																							Very broken argillite with small intervals of fault gouge @63.41. Some laminated competent sections with meso folds in darker banded (finer) material. Probably soft sediment deformation.
D07-03	72.53	77.41	HQ	AC	BLPH	bk	LM						BD	15			X													Some disturbed laminae. Wk fractures sub-parallel TCA filled with white qtz. Strong siderite along laminae
D07-03	77.41	82.24	HQ	AC	BLPH	br-rd	BD						F/	25	OXI	4	X	X												Oxidized section broken into blocky fragments. Distorted laminae either side.
D07-03	82.24	83.07	HQ	AC	BLPH	bk	LM																							
D07-03	83.07	83.38	HQ	DY	LMDK	br-rd	EQ						VOX	7			X	X												Dyke oxidized, porphyritic near top of dyke. Sharp contacts.
D07-03	83.38	111.92	HQ	ES	BLPH	bk	LM						BD	34			X	WK												Graphitic along laminae near top of section. Quartz infill along fractures increasing towards bottom of section
D07-03	111.92	112.80	HQ	ES	BLPH	wh		BR									X	WK		G	30%									Quartz stringers sub-parallel to core axis.
D07-03	112.80	113.53	HQ	AC	BLPH	dk gy		BR									X	WK		G	30%									Quartz stringers sub-parallel to core axis.
D07-03	113.53	114.24	HQ	AC	QZTE	wh-lt gy	BD	CN							SIL	6	X	X		R	70%									white quartz vein. Original distorted laminations present but silicified. Small cross-cutting open fractures present with limonitic staining.
D07-03	114.24	115.92	HQ	FL	BLPH	dk gy		XF	75								X	WK												
D07-03	115.92	116.33	HQ	AC	SCPH	DK GY	BD	CN									X	WK												Graphitic. Quartz infill along fractures increasing towards bottom of section. Lower contact gradational with increasing carbonate content
D07-03	116.33	117.03	HQ	FL	BLPH	dk gy		BR		FL	75						X	WK	X	G	30%			S	<=1%					Broken. Birds eye texture in competent layers. Quartz in fractures. <1% hematite.
D07-03	117.03	117.16	HQ	AC	BLPH	dk gy	LM																							Graphitic. Quartz infill along fractures increasing towards bottom of section. Lower contact gradational with increasing carbonate content.
D07-03	117.16	121.17	HQ	AC	BLPH	dk gy	VU										WK			U	10%			B	<<1%					Pyrite associated with quartzite. Remnant boxwork (vugs) in quartzite carbonate
D07-03	121.17	121.55	HQ	FL	SCPH	md gy	BD	CN												A	20%	/	10%							Distorted to abrupt lowercontact.
D07-03	121.55	122.12	HQ	DY	LMDK	gy	EQ	DC	30																					Megnetic with definite chilled margins.
D07-03	122.12	125.13	HQ	FL	SCPH			BR									MD	X	X					/	<<1%					Lower part of fault cut by dyke.
D07-03	125.13	145.02	HQ	ES	SCPH	md-gy	LM										MD							B	<=1%					@ 131.26m Qtzite veins over 33 cm as fracture fill.
D07-03	145.02	151.18	HQ	FL	SCHI												ST					I	30%							Calcite veins and disrupted laminations. Appears to be injection and disruption without horizontal displacement of fragments
D07-03	151.18	161.54	HQ	ES	SCPH	gy	LM						BD	80			MD													Some calcite veins . Limey phyllite. Graphitic laminations with crenulated trexture
D07-03	161.54	166.94	NQ	ES	SCPH	md gy	LM						BD	32			MD					A	20%	D	<<1%					Birds eye texture, Laminae weakly crenulated, graphitic
D07-03	166.94	167.33	NQ	FL	LMST	wh	MS						F/W	60			ST					V	x	F	<<1%					massive crystalline vein with very fine argillite layers containing pyrite

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-03	167.33	184.37	NQ	ES	SCPH	md gy	LM						BD	35			MD	WK				A	20%	D	<<1%					Occassional calcite veins . Disrupted and folded (m & S) laminae. Some weak brecciation throughout, increasing with depth
D07-03	184.37	185.62	NQ	FL	SCPH	md gy	BD	CN									ST	X												Rock broken, disrupted laminae
D07-03	185.62	186.54	NQ	FL	CLAY																									This is a void, no actual return
D07-03	186.54	187.34	NQ	FL	SCPH	md gy	BD	CN					F/W	35			ST													Laminae become parallel to core at lower contact
D07-03	187.34	188.95	NQ	DY	LMDK	gy	EQ						F/W	32			X													Chilled margins, magnetic
D07-03	188.95	190.87	NQ	FL	PHLM	wh gy	>>					AU	F/C	35	CAR	7	ST													Veins calcite/dolomite. Grades into normally laminated phyllitic schist
D07-03	190.87	256.73	NQ	ES	SCPH	md gy	LM						BD	40			MD							D	<<1%					Occassionally folded (M and S) sections. Small mostly concordant calcite/dolomite veins and blebs no >5cm occur. Pattern of folds and weak brecciation continues throughout section. Folds appear proximal and overlying brecciation
D07-03	256.73	258.11	NQ	DY	LMDK	BR	EQ																	S	<=1%					Three small dykes in laminated to contorted schist. 20% of section dyke, 80% scph. Dykes have irregular contacts, are magnetic and contain biotite flakes.
D07-03	258.11	297.62	NQ	ES	SCPH	gy	LM										MD							S	<<1%					Return to weakly schistose
D07-03	297.62	300.40	NQ	DY	LMDK	br gy	EQ																							
D07-03	300.40	307.30	NQ	ES	SCPH	md gy	LM						BD	20			WK			<	<=1%	<	3%							Contorted laminae. Some limey bands (10-15%) & concordant & minor discordant qtz veins and veinlets (<1)
D07-03	307.30	307.65	NQ	ES	SCPH	md gy	LM										WK			<	7%	<	3%							Concordant & irreg qtz veins (about 7%)
D07-03	307.65	340.16	NQ	ES	SCPH	md gy	LM						BD	20			WK					<	3%							315.00-315.13m Qtz vein (80%). 3007.41-307.60m qtz veining (20%). Bands (2-5 cm) with crenulated and contorted banding.
D07-03	340.16	352.35	NQ	ES	SCPH	md gy	LM	CR					BD	22			WK			<	<<1%	<	3%							Crenulated & concordant bands and laminae.
D07-03	352.35	367.27	NQ	ES	SCPH	md gy	LM	CR									WK					<	3%							
D07-03	367.27	367.59	NQ	ES	QTZ	wt	MS													V	30%									
D07-03	367.59	379.78	NQ	ES	QTZ	md gy	LM	CR					BD	20			WK			<	<<1%	<	3%							From 367.26 to 367.56
D07-03	379.78	385.88	NQ	ES	SCPH	md gy	LM	CR					BD	22			WK							S	<<1%					
D07-03	385.88	389.37	NQ	ES	SCPH	md gy	LM						BD	50			WK			L	<<1%	L	2%	S	tr					
D07-03	389.37	390.20	NQ	DY	LMDK	dk gy	EQ																	S	<<1%					Fine-grained, massive (amph 60%,pyx 10%, plag 30%.
D07-03	390.20	393.54	NQ	ES	SCPH	md gy											MD			L	tr	<	3%	S	<<1%					
D07-03	393.54	393.92	NQ	DY	LMDK	dk gy	PR																	S	<<1%					Fine-grained lamprophyre. Plag phenocrysts up to 1 to 2 mm.
D07-03	393.92	400.82	NQ	ES	SCPH	md gy	LM													L	<<1%	<	3%							
D07-03	400.82	401.94	NQ	DY	LMDK	dk gy	PR																							Lamprophyre dyke. Plag phenocrusts up to 1-2 mm in diameter.
D07-03	401.94	413.79	NQ	ES	SCPH	md gy	LM						F/				WK			L	2%	<	3%							At 403.07 los water return (fault?).
D07-03	413.79	418.50	NQ	ES	SCPH	md gy	LM						BD	43																Graphite covering fracture, bedding planes and along schistosity planes. Qtz with calcite in veins and veinlets. Abndt contorted lamianae.
D07-03	418.50	426.82	NQ	ES	SCPH	md gy	LM										wk			L	1%	<	3%	S	<<1%					0
D07-03	426.82	429.12	NQ	ES	SCPH	dk gy	LM						BD	45			WK			L	5%	<	3%	S	<<1%			S	tr	Concordant and subordinate crosscutting vein and blebs of qtz. Py and Sph? (<<1%) in some 3-5 mm veins.
D07-03	429.12	431.60	NQ	ES	SCPH	md gy	LM										WK			L	1%	L	2%	S	<<1%					
D07-03	431.60	433.63	NQ	ES	SCPH	dk gy	LM										MD			L	<=1%	L	3%	S	<<1%					Graphyte covering partings, bedding? Abd schistosity planes.
D07-03	433.63	435.21	NQ	ES	SCPH	md gy	LM										MD			L	2%	L	5%	<	<<1%					Irreg. & concordant qtz/calcite veins and veinlets.
D07-03	435.21	440.71	NQ	ES	SCPH	md gy	LM										MD			L	<=1%	L	5%	<	<<1%					Several intervals of contorted bedding (20-30 cm).
D07-03	440.71	442.63	NQ	ES	SCPH	md gy	LM						BD	20			MD			L	<<1%	L	5%	<	<<1%					Intervals (10-25 cm) with contorted bedding and microfolding.
D07-03	442.63	452.63	NQ	ES	SCPH	md gy	LM										WK			L	<<1%	L	3%							
D07-03	452.63	457.35	NQ	ES	SCPH	md gy	LM						BD	14			MD			L	<<1%	L	5%	<	<<1%					
D07-03	457.35	459.19	NQ	FL	SCPH	bk							F/	65						L	<<1%			L	<<1%					Very broken phyllite with graphyte & little qtz veining. Several slippage planes parallel to fault dip (65 degrees perpendicular to CA).
D07-03	459.19	460.37	NQ	ES	SCPH	md gy	LM						BD	50			WK			L	3%	L	2%	<	<<1%					
D07-03	460.37	463.59	NQ	ES	SCPH	bk							F/	50			WK													Graphitic schist. Fault bended bedding planes and produced slippage planes parallel to fault dip (lower angle perpendicular to CA.
D07-03	463.59	470.16	NQ	ES	SCPH	bk	LM						BD	37			WK			L	<<1%	L	2%	L	<=1%					Graphitic schist. At 456.18-456.68 brecciated interval with qtz veining (10-15%)
D07-03	470.16	471.49	NQ	ES	SCPH	bk	LM													L	1%	L	5%	L	<=1%					Some contorted intervals.
D07-03	471.49	474.27	NQ	ES	SCPH	GY	LM										WK			L	1%	L	<<1%	L	<=1%					
D07-03	474.27	476.60	NQ	ES	SCPH	DKGY	LM	CT									X			L	<=1%			L	<<1%					Very minor calc in areas.
D07-03	476.60	479.84	NQ	ES	BLPH	BK	LM	CN									X			L	<=1%			D	tr					Graphite rich thrt.
D07-03	479.84	480.36	NQ	DY	MFDY	Gngy	MO	DC	66								x													

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								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-03	480.36	480.82	NQ	ES	BLPH	BK	LM	SZ									X			U	&									Intenseyl graphitic in shear zone.
D07-03	480.82	483.29	NQ	ES	SCPH	DKGy	LM	CN									MD			U	<<1%	L	1%	D	tr					
D07-03	483.29	483.72	NQ	ES	SCPH	DKGY	LM	FR									MD			L	<=1%	L	1%	D	tr					Core double-drillerd-very broken zone.
D07-03	483.72	489.81	NQ	ES	SCPH	DKGY	LM	LC									MD			L	1%	L	2%	L	<=1%					Phyllite postions not calcareous.
D07-03	489.81	490.03	NQ	ES	SCPH	DKGY	LM	CT									WK			L	<=1%			L	tr					Graphtite rich, fractured and healed zone.
D07-03	490.03	491.15	NQ	DY	MFDY	GNGY	FG	DC	40																					
D07-03	491.15	496.69	NQ	ES	SCPH	DKGY	LM	CT									MD			L	2%			D	3%					Various angles.
D07-03	496.69	497.46	NQ	ES	SCPH	DKGY	MO	XF				FB					WK			L	5%									Graphitic small br. Sections & fracture filling- slickgnslides
D07-03	497.46	499.69	NQ	ES	SCPH	DKGY	LM	CT																						
D07-03	499.69	500.09	NQ	DY	MFDY	GNGY	PR		80																					Porphyrite magnetic.
D07-03	500.09	504.47	NQ	ES	MFDY	DKGY	LM	CT									MD							I	<<1%					Black near dyke contact.
D07-03	504.47	504.90	NQ	DY	MFDY	DKGY	PR																							Seg above- porphyrite at contacts.
D07-03	504.90	507.49	NQ	ES	SCPH	DKGY	LM										MD							I	<=1%					Fewer calcitic laminations.
D07-03	507.49	508.52	NQ	DY	MFDY	DKGY	CG																							
D07-03	508.52	521.27	NQ	ES	SCPH	DKGY	LM	CN		<<							WK													511.15 - 5cm DY. 10cm broken. Blocky core above minor + fracture in cacite infill.
D07-03	521.27	521.47	NQ	ES	SCPH	DKGY	LM	CN		FR																				
D07-03	521.47	521.73	NQ	DY	MFDY	GNGY	PR			FR																				Broken.
D07-03	521.73	522.83	NQ	AC	AR	MDGY	LM	CN									X			V	<<1%				3%					Broken.
D07-03	522.83	533.29	NQ	AC	AR	MDGY	LM	CR									X													
D07-03	533.29	534.21	NQ	AC	AR	MDGY	LM	CR									X													
D07-03	534.21	537.52	NQ	AC	LHAR	MDGY	LM	CR	40																					
D07-03	537.52	539.08	NQ	AC	ARLM	DKGY	LM	CN	40																					Graphitic towards lower contact in Dy con.
D07-03	539.08	539.81	NQ	DY	MFDY	GNGY	MS																							Sharp contact.
D07-03	539.81	548.12	NQ	AC	ARLM	DKGY	LM		40																					More competend. Becoming carbonacious/graphite.
D07-03	548.12	578.49	NQ	ES	GCHP	BK	LM	CN									X							E	2%					3-5% psilomelane. Beds brecciation silicious infilling. Increase convolution 559+in. Carbonacious.Arregular ankerite
D07-03	578.49	584.30	NQ	ES	GCHP	DKGY	LM	FL				TB	F/				X								tr					Broken. QTZ veins 578.52 no psilomglane still. Graphite.
D07-03	584.30	590.43	NQ	ES	GCHP	DKGY	LM	CT									X			A	<<1%				2%					Increase in pg. Psiloglane(?) noted. Laminations 11+CA to ++CA.
D07-03	590.43	593.83	NQ	ES	GCHP	BK	FL	FR				TB	F/				X			B	1%				3%					Biceciated in voids along fractures. Lwr contact with 2tz frags in breccia.
D07-03	593.83	594.49	NQ	ES	GCHP	BK	FL	XF				TB	F/				WK													Fault gauge. 6'6" washed out. Small pieces of graphite schst.
D07-04	0.00	4.26	HW	n/a	CASI																									
D07-04	4.26	7.92	NQ	OV	BLPH																									
D07-04	7.92	43.38	HQ	AC	BLPH	dk gy	BD	CN					BD	50			MD	X	WK					E	<=1%					Laminations are contorted (folds, crenulations) and faulted with calcite veinlets concordant to bedding. Veinlets are dolomite, quartzite/calcite. Pyrite appears associated with but marginal to veinlets . Graphitic in areas.
D07-04	43.38	44.33	HQ	DY	LMDK	br	EQ	DC	40				F/W	40																Chilled, distinct margins. Magnetic
D07-04	44.33	55.45	HQ	AC	BLPH	md gy	BD	CN					BD	45			WK	X	X					E	<=1%					Decreasing calcite content. Otherwise much as above sequence.
D07-04	55.45	56.72	HQ	DY	LMDK	br-gy	EQ						F/W	40																Magnetic
D07-04	56.72	67.24	HQ	AC	BLPH	bk-gy	BD	CN									X							E	<=1%					
D07-04	67.24	73.08	HQ	FL	GNPH	bk		BR				HY			SIC	4	X			G	20%			B	<<1%					Silicious veining with calcitic partings. Rock is very broken and brecciated. Graphite present along sheared surfaces
D07-04	73.08	88.88	HQ	AC	BLPH	md gy	LM						BD	40			X							E	<=1%					Appears finer grained. Less contorted bedding. Core angle varies from 70 near upper contact to as low as 20 @ 84m
D07-04	88.88	91.41	HQ	DY	LMDK	gy	EQ										wk													magnetic
D07-04	91.41	96.32	HQ	AC	BLPH	bk	LM						BD	40			X			E	<=1%			A	<=1%					Qtz filled, mayor concordant and minor crosscutting lamiane and veinlets.
D07-04	96.32	96.88	HQ	AC	BLPH	bk	LM										wk			E	2%									Qtz filled, mayor concordant and minor crosscutting lamiane and veinlets.
D07-04	96.88	102.41	HQ	AC	BLPH	bk	LM										WK			<	<=1%			E	2%					Qtz fillings in corcordant and monor crosscutting laminae and veinlets
D07-04	102.41	105.93	HQ	AC	BLPH	bk	LM	CT					BD	45			X			<	2%			E	2%					Qtz fillings in corcordant and monor crosscutting laminae and veinlets
D07-04	105.93	111.72	HQ	AC	BLPH	bk	LM	CT									X			<	2%			E	2%					Qtz fillings in corcordant and monor crosscutting laminae and veinlets. At 106.40m irregular qtz filling of fracture(10cm).
D07-04	111.72	114.18	HQ	AC	BLPH	bk	LM	CT									X			<	3%			E	2%					Qtz fillings in corcordant and monor crosscutting laminae and veinlets.

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-04	114.18	115.97	HQ	AC	BLPH	bk	LM						BD	28						<	1%			E						Qtz fillings in corcordant and monor crosscutting laminae and veinlets.
D07-04	115.97	117.37	HQ	AC	BLPH	bk	LM													<	1%			E	2%					Qtz filling in concordant and minor crosscutting laminae and veinlets.
D07-04	117.37	119.08	HQ	AC	BLPH	bk	LM													<	3%			E	2%					Qtz filling in concordant and minor crosscutting laminae and veinlets.
D07-04	119.08	120.70	HQ	AC	BLPH	bk		FL																E	1%					Very broken up AC (<=3cm)
D07-04	120.70	121.08	HQ	AC	BLPH	bk	LM						BD	35						<	2%			E	2%					
D07-04	121.08	123.71	HQ	DY	LMDK	dk gy	PR																	S	1%					Dyke contact at 17 degrees perpendicular to CA. Porphyritic lamprohyre (5mm porphyroclast in medium-grained matrix)
D07-04	123.71	124.58	HQ	DY	MONZ	bl gy	EQ																	S	<<1%					Fine-grained, massive monzonitic dyke (plag, amph, minor biotite, py?)
D07-04	124.58	125.45	HQ	AC	BLPH	bk	LM													C	<=1%			S	0					Quartz fillings in concordant laminae and veinlets.
D07-04	125.45	126.49	HQ	AC	BLPH	bk	MS																							Black, graphitic carbonaceous mud.
D07-04	126.49	130.49	HQ	AC	BLPH	bk	MS													E	<=1%			E	<=1%					Py as disseminated and fracture fillings.
D07-04	130.49	131.55	HQ	AC	BLPH	bk	MS													E	3%			E	<=1%					
D07-04	131.55	131.77	HQ	AC	QTZ	wt														I	80%			S	<<1%					Irregular qtz vein with scarce diss specks of Py.
D07-04	131.77	138.70	HQ	AC	BLPH	bk	LM													E	<<1%	C	<=1%	E	<=1%					Laminae with calcite fillings.
D07-04	138.70	141.33	HQ	AC	BLPH	bk		FL									wk			E	<<1%	C	2%							At 139.71 qtz vein 13cm thick.
D07-04	141.33	145.08	HQ	AC	BLPH	bk	LM										MD			E	<=1%	C	2%	S	<=1%					Disseminated calcite in veins and as fracture fillings. Diss. Specks of Py.
D07-04	145.08	146.97	HQ	AC	BLPH	bk	LM	FL									WK			E	<=1%	C	<=1%							Very broken. Last 10 cm totally crushed argillite. Graphite coatings along bedding and fracture surfaces.
D07-04	146.97	147.37	HQ	DY	MONZ	lt gy	EQ	FL									X													Fine-grain, equigranular, massive monzonitic dyke (plag, amph, bio).
D07-04	147.37	147.57	HQ	AC	BLPH	bk	LM	FL									WK			E	<=1%	C	<=1%							Abndt graphite as coatins of fractures and in concordant laminae (shearing planes?)
D07-04	147.57	148.35	HQ	DY	MONZ	lt gy	EQ	FL																						Fine-grain, equigranular, massive monzonitic dyke (plag, amph, bio).
D07-04	148.35	152.00	HQ	AC	BLPH	lt gy	BD	CN		FL										E	<<1%	/	2%							
D07-04	152.00	152.40	HQ	DY	MONZ	lt gy	EQ	FL																						
D07-04	152.40	154.43	HQ	AC	BLPH	lt gy		BR												G	7%	<	5%	S	<=1%					Brecciated argillite with laqrge qtz fillings (<=5cm). Abdnt graphite.
D07-04	154.43	156.51	HQ	DY	MONZ	lt gr	EQ																							Fine-grain, equigranular, massive monzonitic dyke (plag, amph, bio).
D07-04	156.51	160.04	HQ	AC	LMST	md gy	MB																							
D07-04	160.04	161.64	HQ	ES	SCHI	gn gy		SC																S	<<1%					Contorted laminae.
D07-04	161.64	162.04	HQ	DY	MONZ	lt gy	EQ																							Fine-grain, equigranular, massive monzonitic dyke (plag, amph, bio).
D07-04	162.04	165.74	HQ	ES	SCHI																									
D07-04	165.74	169.69	HQ	AC	BLPH	bk	LM						BD	25										E	<=1%					Thinly laminated
D07-04	169.69	179.88	HQ	AC	QTZ	wt	MS													<	90%									175.28-175.85: Strongly silicified remnant of phyllite (Schist?)
D07-04	179.88	181.02	HQ	DY	MONZ	lt gy	EQ																							Fine-grained, equigranular, massive monzonitic composition dyke.
D07-04	181.02	182.21	HQ	TS	SCPH	md gy	LM						BD	28			MD					<	3%	E	<=1%					Thickly laminated (0.3-1.0cm); some contorted laminae.
D07-04	182.21	186.09	HQ	TS	SCPH	lt gy	LM										md					L	5%	S	<<1%					Very thinly bedded (1.0 to 3.0cm) units with intercalated bands of limestone.
D07-04	186.09	194.56	HQ	TS	SCPH	bl gy	BD	CN									MD			<	5%			S	<<1%					Laminated, banded and contorted.
D07-04	194.56	199.33	HQ	ES	SCPH	bk	LM	CN					BD	43			MD							S	<<1%					196.90-197.27: contorted bands with abndt Py (7%)
D07-04	199.33	204.15	HQ	ES	SCPH	bk	LM	CN									X			<	5%									
D07-04	204.15	210.29	HQ	ES	SCPH	bk	LM						BD	30			X			<	2%			S	<<1%					Graphite coatings on schistosity planes.
D07-04	210.29	210.80	NQ	ES	SCPH	bk	LM	CR									X			G	20%									
D07-04	210.80	217.34	NQ	ES	SCPH	bk	LM										X			<	<<1%			E	<=1%					Graphite coatings on schistosity planes.
D07-04	217.34	217.90	NQ	ES	SCPH	bk	LM	CR									X			G	30%			S	<=1%					
D07-04	217.90	218.48	NQ	ES	GCHP	bk	MB						BD	33			MD			G	7%			S	<<1%	A				Abndt graphite on schistosity planes.
D07-04	218.48	220.98	NQ	ES	GCHP	bk		FR									WK			G	7%			S	<<1%					Broken
D07-04	220.98	224.66	NQ	ES	GCHP	bk	BD	CN									wk	WK		E	<=1%			D	<=1%					Abndt graphite on schitosity planes.
D07-04	224.66	228.43	NQ	ES	GCHP	bk	LM	CN									x													
D07-04	228.43	230.43	NQ	ES	GCHP	bk	LM										X			<	2%			E	<=1%					Broken. Abdnt graphite in fractures and schistosity planes.
D07-04	230.43	233.98	NQ	ES	GCHP	bk	BD	FL									X			G	7%			S	<<1%					Very broken, fault zone. Abdnt graphite schistosity planes.
D07-04	233.98	242.62	NQ	ES	GCHP	bk	LM	FL									X			<	<=1%			E	<=1%					Broken. Abdnt graphite schistosity planes.
D07-04	242.62	261.93	NQ	ES	SCPH	dk gy	LM	CN									MD			L	2%	L	<=1%	E	<=1%					Not broken. End of fault at start of interval.

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-04	261.93	269.04	NQ	ES	GCHP	bk	LM	CN									X			A	1%			<	1%					Some specks of pyrrhotite (<<1%). No core angle discernible bedding (schistosity?). Graphitic coatings on schistosity planes.
D07-04	269.04	272.32	NQ	ES	GCHP	dk gy	LM	CN									X			A	<=1%			L	1%					Less graphitic schist than previous interval.
D07-04	272.32	273.10	NQ	ES	GCHP	dk gy	LM	FL											X	A	<=1%			<	<=1%					Very broken. Abndt graphite coatings on schistosity planes and fractures.
D07-04	273.10	276.70	NQ	DY	LMDK	dk gy	EQ										X							S	<<1%					Phaneritic, equigranular dyke (plag, amph?, bio)
D07-04	276.70	277.90	NQ	ES	GCHP	bk	LM	CN					F/W	38			X			<	5%			<	5%					Contorted contact.
D07-04	277.90	285.37	NQ	RL	LMST	gy wt	LM	FR																						Dolomitic limestone. Dolomite replacing bands and laminae and filling fractures (=<10%).
D07-04	285.37	291.00	NQ	RL	LMST	gy wt	LM																							Intercalated argillaceous laminae (<10%) and carbonatic argillaceous laminae.
D07-04	291.00	291.39	NQ	DY	LMDK	md gy	EQ																							Irregular contacts. Phaneritic, equigranular lamprophyre dyke (plag, bio, amph?).
D07-04	291.39	296.88	NQ	RL	LMST	lt gy	LM	CN					BD	20										L	<<1%					Few laminae with Py (=<20%) on lamina up to 1.5cm.
D07-04	296.88	302.45	NQ	RL	LMST	lt gy	LM																	S	<<1%					
D07-04	302.45	303.96	NQ	RL	LMST	lt gy lc	LM						BD	3										S	<<1%					
D07-04	303.96	304.76	NQ	RL	LMST	md gy	LM	FL									ST							S	tr					
D07-04	304.76	305.58	NQ	DY	LMDK	gn	PR										X													Lamprophyre dyke.
D07-04	305.58	307.85	NQ	RL	PHYL	md gy	LM										ST							S	<<1%					
D07-04	307.85	318.63	NQ	RL	LMST	lt gy	LM						BD	25			ST							S	tr					
D07-04	318.63	335.29	NQ	RL	LMST	lt gy	LM										ST							S	tr					Abndt argillite laminae.
D07-04	335.29	353.52	NQ	RL	LMST	lt gy	LM						BD	10			ST													
D07-04	353.52	354.92	NQ	RL	SCHI	lt gy	LM										ST													
D07-04	354.92	368.20	NQ	RL	LMST	lt gy	LM						BD	3			ST													Core angle perpendicular to core axis = 3 degrees (very low, almost perpendicular to drill hole
D07-04	368.20	369.12	NQ	RL	LMST	lt gy	LM										ST													
D07-04	369.12	369.85	NQ	RL	LMST	md gy		BR									ST							G	1%	G	?	S	<=1%	Breccia fractures with Py, Sph and dolomite (dolomitization)
D07-04	369.85	370.16	HQ	FL	LMST	md gy		BR									MD							G	3%			G	2%	
D07-04	370.16	370.95	NQ	RL	LMAR	md gy		BR																						
D07-04	370.95	371.84	NQ	RL	LMAR	lt gy		BR									MD							G	\			G	\	Breccia fractures with pyrite and sphalerite and dolomitization. End of breccia.
D07-04	371.84	373.20	NQ	RL	LMAR	lt gy	LM										ST													Limestone laminae with intercalated argillaceous bands and dolomitization (bands and calcite replacement)
D07-04	373.20	386.50	NQ	RL	LMAR	lt gy	LM						BD	13			ST													Limestone laminae with intercalated argillaceous bands and dolomitization.
D07-04	386.50	387.38	NQ	DY	LMAR	gn gy	PR										X											S	<=1%	Both footwall and hanging wall margins are chilled into lighter-coloured, equigranular lamprophyre with =<1.0mm crystals (amp?, plag, bio).
D07-04	387.38	394.84	NQ	RL	LMAR	lt gy	LM										ST											S	<=1%	Limestone laminae with intercalated argillaceous bands and dolomitization.
D07-04	394.84	395.34	NQ	RL	LMAR	lt gy		BR																<	1%					Limestone laminae with intercalated phyllite bands and dolomitization. Phyllite bands have more pyrite (~2%) than limestone/dolomite bands.
D07-04	395.34	400.28	NQ	RL	LMAR	lt gy	LM						BD	15			ST							S	<<1%					Limestone laminae with intercalated argillaceous & dolomite bands.
D07-04	400.28	404.37	NQ	RL	LMAR	md gy	LM										ST							S	<<1%					Limestone laminae with intercalated argillaceous & dolomite bands. More Py specks in argillite than in limestone bands.
D07-04	404.37	412.50	NQ	RD	LMAR	dk gy	LM						BD	13			ST							S	<<1%					Limestone laminae with intercalated argillaceous & dolomite bands. More Py specks in argillite than in limestone bands.
D07-04	412.50	423.62	NQ	RD	LMAR	md gy											ST							S	<=1%					Some argillite bands (=< 2 cm) contain specks (=< 2mm) of Py (10-15%) but no Sph or Gn. Some argillite bands (=< 2 cm) contain specks (=< 2 mm) of Py but no Sph or Gn.
D07-04	423.62	426.80	NQ	RD	LMAR	dk gy											MD							S	<<1%					Some argillite bands (=< 2 cm) contain specks (=< 2mm) of Py (10-15%) but no Sph or Gn. More abndt argillite bands. The calcite/dolomite decreases (Ca/Do ~ 0.5).
D07-04	426.80	426.83	NQ	RD	DOTE	tan		BR					LX				WK	X						S	\					Vugs and cavities coated with iron oxides (jarosite?, lixiviation). No sulphides. Calcite in fracture coatings.
D07-04	426.83	430.32	NQ	RD	DOTE	lt gy	BN										WK	X												Crudely banded dolomite with limey bands.
D07-04	430.32	431.60	NQ	RD	DOTE	lt gy	BN						LX				WK	X						S	\					Vugs and cavities coated with iron oxides (jarosite?) indicating lixiviation.
D07-04	431.60	432.29	NQ	RD	AR	bk	FL	FL																						Very broken argillite.
D07-04	432.29	433.28	NQ	RD	DOTE	md gy	BN										MD							E	<<1%					Dolomite with arghillaceous and limey bands.

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-04	433.28	433.43	NQ	RD	AR	bk	FL	FL										MD												
D07-04	433.43	437.14	NQ	RD	DOTE	bk	BN										X							E	<<1%					Dolomite with argillaceous bands. Few of these bands (=< 2 cm) with specks (=<1.5 mm) of Py (=<15%).
D07-04	437.14	443.79	NQ	RD	DOTE	dk gy	TW										WK			A	<=1%			S	<<1%					Irregularly intercalated argillaceous bands.
D07-04	443.79	445.92	NQ	RD	DOTE	lt gy	TW	FL					LX				WK	WK						X						Lixiviation caused open fractures and empty vugs. Very week Zn-Zap reaction in few lixiviated fracture coatings.
D07-04	445.92	460.25	HQ	RD	DOTE	lt gy	TW						BD	3			X							E	<<1%					Few irregular argillaceous bands with dissemanated specks of fresh Py (3-5% Py in band).
D07-04	460.25	460.55	HQ	RD	DOTE	lt gy	TW	FL									X								\					Very broken, likely a fault.
D07-04	460.55	461.35	NQ	RD	DOTE	lt gy	TW	FL					LX				X			I	<=1%									
D07-04	461.35	462.12	NQ	RD	DOTE	md gy	TW										X							S	<<1%					Py specks in daqrk grey, aregillaceous bands.
D07-04	462.12	462.85	HQ	RD	DOTE	tw	TW	CT									X			I	<=1%			E	<=1%					
D07-04	462.85	463.70	HQ	RD	DOTE	dk gy	TW	CT									X							E	2%	S	<=1%	S	1%	
D07-04	463.70	464.50	HQ	RD	DOTE	md gy	TW										X			G				E	<=1%			S	<=1%	
D07-04	464.50	465.12	HQ	RD	DOTE	lt gy	TW										X							E	<<1%					
D07-04	465.12	465.95	HQ	RD	DOTE	lt gy	TW										X			G	3%			E	<=1%			E	<=1%	
D07-04	465.95	467.20	NQ	RD	DOTE	lt gy	TW																	S	<<1%					
D07-04	467.20	468.17	NQ	RD	DOTE	md gy	TW																	E	3%					
D07-04	468.17	469.05	NQ	RD	DOTE	md gy																		E	2%					
D07-04	469.05	469.96	NQ	RD	DOTE	lt gy	TW																	E	<<1%					
D07-04	469.96	471.00	NQ	RD	DOTE	lt gy																		E	<<1%					
D07-04	471.00	471.42	NQ	DY	LMDK	dk gy	EQ																							
D07-04	471.42	471.97	NQ	RD	DOTE	md gy tw	TW																	E	1%					
D07-04	471.97	472.72	NQ	RD	DOTE	md gy	TW																	E	3%					
D07-04	472.72	473.77	NQ	RD	DOTE	dk gy		CT																E	1%					
D07-04	473.77	474.70	NQ	RD	DOTE	dk gy											X							S	<<1%					Broken
D07-04	474.70	475.65	NQ	RD	DOTE	dk gy											X							S	tr					Broken
D07-04	475.65	476.50	NQ	RD	DOTE	dk gy											X							S	<<1%					Broken
D07-04	476.50	477.32	NQ	RD	DOTE	lt gy	TW										X							S	<<1%					
D07-04	477.32	483.33	NQ	RD	DOTE	lt gy	TW										X													
D07-04	483.33	497.38	NQ	RD	DOTE	md gy	TW										X							E	<<1%					
D07-04	497.38	498.41	NQ	RD	DOTE	md gy	TW										X			G	7%									
D07-04	498.41	501.53	NQ	RD	DOTE	md gy	TW										X			G	7%									
D07-04	501.53	502.38	NQ	RD	DOTE	md gy	TW										X													
D07-04	502.38	502.96	NQ	RD	DOTE	md gy	TW										X							E	5%			E	3%	
D07-04	502.96	503.81	NQ	RD	DOTE	md gy	TW										X							E	<=1%					
D07-04	503.81	506.47	NQ	RD	DOTE	dk gy	TW										X													
D07-04	506.47	507.37	NQ	RD	DOTE	dk gy	TW										X							S	<<1%					
D07-04	507.37	507.86	NQ	RD	DOTE	lt gy	TW										X							E	3%			E	7%	
D07-04	507.86	508.82	NQ	RD	LMST	lt gy	LM										MD							S	<<1%			E	<<1%	
D07-04	508.82	514.83	NQ	RD	LMST	md gy	LM										MD													From 508.22 to 511.77: Limey dolomite
D07-04	514.83	518.51	HQ	FL	DOTE	dk gy	TW						BD	20			X													
D07-04	518.51	519.04	HQ	DY	LMDK	gn gy	PR										X							S	1%					
D07-04	519.04	522.13	HQ	RD	DOTE	lt gy	TW										MD													Limey dolomite.
D07-04	522.13	524.86	HQ	TS	SCHI	gn gy	LM										X													Some bands of SCHI with Py specks (<<1%).
D07-04	524.86	526.38	NQ	RD	LMST	wt	MS										MD													At 525.55 Qtz vein 3.5 cm wide.
D07-04	526.38	528.22	NQ	TS	SCHI	md gy		SC					BD	22			X													EOH
D07-05	0.00	8.02	HQ	AC	PHLM	bk	LM	CN																<	1%					Very broken.
D07-05	8.02	12.48	HQ	AC	PHLM	bk	LM	CN												L	<<1%			<	3%					
D07-05	12.48	13.52	HQ	AC	PHLM	bk	LM	CN												L	5%			<	1%					Partially-filled fractures with Qz (open vugs).
D07-05	13.52	15.15	HQ	AC	PHLM	bk	LM	CN												L	<<1%			<	2%					
D07-05	15.15	16.24	HQ	AC	PHLM	bk	LM	CN												L	<<1%			<	2%					Some open vuggy areas.
D07-05	16.24	26.21	HQ	AC	PHLM	bk	LM	CN												L	2%			<	1%					EOH. Azimuth was off by 28 degrees. D07-06 collared at the same site at 330 degrees and -60-degree inclination.
D07-06	0.00	8.84	HQ	AC	ARLM	Bk	LM	CN												L	<<1%			L	<<1%					Highly broken
D07-06	8.84	11.89	HQ	AC	ARLM	GY	LM	CN												L	<=1%			L	<=1%					
D07-06	11.89	12.08	HQ	AC	ARLM	GY	LM	CN												L	1%			T	3%					
D07-06	12.08	15.19	HQ	AC	ARLM	dk gy	LM	CN												L	<=1%			L	2%					Some 3cm carbon rich bands
D07-06	15.19	15.43	HQ	AC	ARLM	dk gy	LM	CN												U	7%			L	<=1%					
D07-06	15.43	16.21	HQ	AC	ARLM	dk gy	LM	CN												L	<=1%			L	1%					Areas of 2mm pyrite blebs
D07-06	16.21	20.61	HQ	AC	ARLM	bk	LM	CN												L	<=1%			T	<=1%					Carbon rich, some limonite on fractures
D07-06	20.61	22.57	HQ	AC	ARLM	bk gy	LM	CN												L	<=1%			T	<=1%					Pyrite mostly along laminae, but some blebby bands 3cm thick, carbon rich blebs and laminae

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								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-06	22.57	23.53	HQ	AC	ARLM	bk	LM	SH		CN										E	<<1%			L	<=1%					Strongly carbon rich throughout
D07-06	23.53	26.25	HQ	AC	ARLM	gy	LM	CN												L	<=1%			L	<=1%					Carbon rich from 24.16 to 24.60, also py blebs in same zone
D07-06	26.25	26.43	HQ	AC	QTZ	gy		QV	40											V	50%			L	<<1%					Argillite bands in qzvn
D07-06	26.43	29.00	HQ	AC	ARLM	dkgy	LM	CN												L	2%			T	2%					
D07-06	29.00	30.14	HQ	AC	ARLM	bk	LM	CN												L	<<1%			L	<=1%					Limonite stains along some fractures, carbon rich throughout
D07-06	30.14	38.30	HQ	AC	ARLM	bk	LM	CN												L	<=1%			L	1%					
D07-06	38.30	41.58	HQ	AC	ARLM	bk	LM	CN												U	1%			L	<=1%					Mainly carbon rich, open qz-filled fractures 0.5 cms and 1-3 cm qz veinlets and silicified zones
D07-06	41.58	44.50	HQ	DY	LMDK	gy gn	PR						F/	35										S	1%					Contact at 35°
D07-06	44.50	48.19	HQ	AC	ARLM	bk	LM	CN									MD			<	<=1%			E	2%					Very contorted laminae
D07-06	48.19	49.30	HQ	AC	ARLM	MD GY	LM	CN									MD			V	30%			L	1%					
D07-06	49.30	50.60	HQ	AC	ARLM	MD GY	LM	CN									MD			<	<=1%			L	1%					
D07-06	50.60	51.89	HQ	AC	ARLM	WT														V	60%			E	<=1%					Py occurs only in argillite laminae and bands
D07-06	51.89	64.71	HQ	AC	ARLM	MD GY	LM	CN									MD			<	1%			S	1%					
D07-06	64.71	66.70	HQ	AC	ARLM	MD GY	LM	CN									MD			<	5%			E	<=1%					
D07-06	66.70	69.04	HQ	AC	ARLM	MD GY	LM	CN									WK			<	1%			E	2%					carbon rich
D07-06	69.04	75.93	HQ	AC	ARLM	MD GY	LM	CN									MD			<	1%			E	3%					very contorted
D07-06	75.93	77.57	HQ	AC	ARLM	MD GY	LM	CN									WK			<	3%			E	3%					very contorted
D07-06	77.57	87.17	HQ	AC	ARLM	DK GY	LM	CN									MD			<	2%			E	2%					very contorted intervals
D07-06	87.17	91.79	HQ	AC	ARLM	BK	LM	CN									MD							E	1%					very contorted
D07-06	91.79	92.20	HQ	AC	QTZ	WT	MS	CN																						few argillic band
D07-06	92.20	93.31	HQ	AC	ARLM	BK	LM	CN									MD							E	1%					
D07-06	93.31	93.92	HQ	DY	LMDK	GN	PR	DC	33																					fine, grained,equigranular
D07-06	93.92	99.39	HQ	AC	ARLM	BK	LM	CN					BD	32										<	2%					very contorted intervals with short (less than or equal to 10cm) laminated sections
D07-06	99.39	102.41	HQ	AC	ARLM	dk gy	LM	CN									X							<	1%					Very contorted.
D07-06	102.41	103.22	HQ	DY	LMDK	bl gn	EQ	DC	23								X													Fine-grained lamprophyre.
D07-06	103.22	111.14	HQ	AC	ARLM	bk	LM	CN					BD	20			WK							<	2%					Very contorted.
D07-06	111.14	111.56	HQ	DY	LMDK	gn	EQ										X													Fine-grained.
D07-06	111.56	112.58	HQ	AC	ARLM	bk	LM	CN									WK			>	<=1%			<	2%					
D07-06	112.58	113.27	HQ	DY	MFDY	bl gn	PR																							Fine-grained with amph? Phenocrysts (~5mm) partially replaced by mosaic of biotite.
D07-06	113.27	114.24	HQ	AC	ARLM	bk	LM	CN									WK			<	<=1%			<	2%					Very contorted.
D07-06	114.24	114.44	HQ	DY	MFDY	bl gn	PR																							Fine grained with amph/ phenocrysts (~5mm) replaced by mosaic of biotite.
D07-06	114.44	121.24	HQ	AC	ARLM	bk	LM						BD	39			WK			<	<<1%									Very weak acid reaction in thin laminae, carbon-rich
D07-06	121.24	126.80	HQ	AC	ARLM	BK	LM	CN									WK			<	<<1%			<	3%					Carbon rich. Acid reaction in thin, light grey limey laminae.
D07-06	126.80	130.71	HQ	AC	ARLM	DKGY	LM	CN									MD			<	<<1%			<	<=1%					Areas w/ 1-3mm fg py blebs.
D07-06	130.71	131.19	HQ	AC	ARLM	DKGY	LM										WK			<	<<1%			T	2%					
D07-06	131.19	133.14	HQ	AC	ARLM	DKGY	LM	CN									MD			<	<<1%			T	2%					
D07-06	133.14	133.38	HQ	AC	ARLM	DKGY	LM										WK			<	<=1%			<	1%					
D07-06	133.38	136.23	HQ	AC	ARLM	DKGY	LM	CT									MD			U	<=1%			<	<=1%					
D07-06	136.23	136.79	HQ	AC	ARLM	DKGY	LM	CT									MD			U	2%			<	<=1%					QzVn 5cm thick along bedding/ laminations.
D07-06	136.79	137.20	HQ	AC	ARLM	DKGY	LM	CT									MD			<	<=1%			<	<<1%					Mod Graph rich thrt.
D07-06	137.20	146.88	HQ	AC	ARLM	DKGY	LM	SZ									MD			<	<<1%			<	<<1%					Start of sz very broken- rest fract into 5-10cm chunks of core.
D07-06	146.88	147.12	HQ	AC	QTZ	WT	MS	QV	35								X													
D07-06	147.12	147.81	HQ	AC	AR	BK	LM	FR									X			<	<=1%			T	<=1%					Very broken and graphite rich.
D07-06	147.81	152.15	HQ	AC	ARLM	DKGY	LM	FR									WK			<	1%			T	<=1%					Fracture, but more competent rock- pieces 10-20cm across zone. Mod. Graph rich.
D07-06	152.15	156.38	HQ	AC	AR	DKGY	LM	FR									X			<	<=1%			T	<=1%					Some areas strongly graph rich.
D07-06	156.38	157.61	HQ	AC	AR	DKGY	LM	FR									X			<	<=1%			T	<=1%					Fault gauge at 157.28, other zones strongly fractured, strongly graphite rich thrt.
D07-06	157.61	161.10	HQ	AC	AR	MDGY	LM	FR																						Finishes in.
D07-06	161.10	161.42	HQ	AC	GCHP	BK		XF																						Very broken, graphite rich.
D07-06	161.42	166.42	HQ	AC	GCHP	DKGY	VA	XF																						
D07-06	166.42	166.78	HQ	AC	GCHP																									Clay.
D07-06	166.78	169.47	HQ	ES	SCPH	MDGY	LM	CT	10								WK							.						
D07-06	169.47	173.92	NQ	ES	SCPH	MDGY	LM	CT	10								WK							.						
D07-06	173.92	178.47	NQ	ES	SCPH	MDGY	LM	CN				TB	F/		PHI		ST													Broken front 178.01 to 178.47: clay seam 10cm, 147.10-147.20 - small gy 3cm. 70 degrees TCA.
D07-06	178.47	192.77	NQ	ES	QTZ	MDGY	LM	CT																						2cm gr. 191.72
D07-06	192.77	192.86	NQ	ES	QTZ	WT	MS	QV	15												50%		10%							1cm schist layers in qtz no apparent mineralization.
D07-06	192.86	198.40	NQ	ES	QTZ	WT	MS																							

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-06	198.40	198.51	NQ	ES	QTZ	WT	MS	QV	10												x									Barrer, sharp contacts, vitreons texture.
D07-06	198.51	202.16	NQ	ES	SCPH	MDGY	LM	CN									ST							E	<=1%					
D07-06	202.16	202.36	NQ	ES	SCPH	DKGY	FL	FR					F/				ST													Contorted laminag on either side.
D07-06	202.36	209.10	NQ	ES	SCPH	MDGY	LM	CN	35								ST													Laminae angle increases to lower contact.
D07-06	209.10	209.26	NQ	ES	SCPH	MDGY	FL	FR					F/C	50			ST													Open fracture surfaces.
D07-06	209.26	210.45	NQ	ES	SCPH	MDGY	LM	LC	70								ST													Very steep pipping laminae, pass drag fold.
D07-06	210.45	210.79	NQ	ES	SCPH	MDGY	FL	FR					F/C	35			ST													Only small chips remaining , upper contact fractures.
D07-06	210.79	215.05	NQ	ES	SCPH	MDGY	LM	CN		FR							ST													10% brittle fracture with carb ingill, random orientation.
D07-06	215.05	226.13	NQ	ES	SCPH	MDGY	LM	CN									ST													Orientation of lam sub parallel tca to 40 degrees TCA. Some fracturing in carb infill.
D07-06	226.13	226.89	NQ	ES	SCPH	MDGY	LM	FR	75			TB	F/				ST							T	<<1%					Fault zone. Blocky rock lam. Sub parallel tca either side some brecciation.
D07-06	226.89	245.10	NQ	ES	SCPH	MDGY	LM	CN									ST							T	<<1%					230.19 - 2cm wide gauge band. 75 degree TCA.
D07-06	245.10	245.45	NQ	ES	QTZ	WHT	BN	QV	65							x														Schist layer within Qtz vein qtzite breccia layer.
D07-06	245.45	248.30	NQ	ES	SCPH	MDGY	BN	LC																						
D07-06	248.30	249.03	NQ	ES	SCPH	MDGY	LM	FL		QV														E	<=1%					Irregular qv. 25cm
D07-06	249.03	254.87	NQ	ES	SCPH	MDGY	LM	LC																E	2%					Scm qv @ 254.76m in small fault /chips of rock.
D07-06	254.87	255.26	NQ	ES	SCPH	MDGY	LM	FL		QV														E	1%					Qtz veins interbedded with schist.
D07-06	255.26	283.00	NQ	ES	SCPH	MDGY	LM	LC	50								WK													Laminae vary from 40degrees-70degrees to parallel. Total sequence of fault, shearing.
D07-06	283.00	287.15	NQ	ES	SCPH	MDGY	LM	LC	22								X													Thinly lam slightly contorted 20-25.
D07-06	287.15	289.89	NQ	ES	SCPH	MDGY	LM	FL		FR							X													Lam in calcite. Infills in fracture. Wkly graphite.
D07-06	289.89	291.00	NQ	DY	LMDK	LTGY	MS						F/W	10			X			B	2%									Non mag. Lower contact 10 degrees perpendicular tca. 10cm sectiono contorted, fractured ES.
D07-06	291.00	295.40	NQ	ES	SCPH	MDGY	LM	LC									ST							E	<=1%					
D07-06	295.40	297.27	NQ	DY	LMDK	LTGY	MS																							Upper contact fault gauge. Slickers lie on ES surface. Lower contact 30degrees perpendicular tca.
D07-06	297.27	297.51	NQ	ES	LMDK	LTGY	MS																							Inner lam. LM STN/ARG with QTZ. Fracturess filled with calcite.
D07-06	297.51	298.26	NQ	DY	LMDK	MDGY	MS																							Fractures in calcite.
D07-06	298.26	300.00	NQ	ES	LMAR	Tan	LM																							Inter lam. LMSTN/ARG. Increase limestone towards middle. Interalaminar voids. Lower contact aburst.
D07-06	300.00	300.96	NQ	DY	LMDK	LTGY	AF																							Apnanite.
D07-06	300.96	301.45	NQ	ES	LMAR	BK											ST													See above. Lower contact gradational into lam.
D07-06	301.45	303.33	NQ	ES	AR	BK	LM										MD													Laminae become parallel TCA, then return to perpendicular TCA.
D07-06	303.33	303.57	NQ	DY	AR	GY	PR										X													Porphyriole DY contacts zone.
D07-06	303.57	304.01	NQ	ES	AR	BK	LM										ST													Lam thicker increasing disturbance towards btm gradationalined breccia/
D07-06	304.01	307.52	NQ	RL	LDAR	WO											ST													Breccia, 20cm gauge at top, grades into bedded limestone.
D07-06	307.52	410.07	NQ	RL	LMAR	IV	MB										ST													Angle changes from 15degreesto 5degrees. Alternating pure limestone and interbedded phyllite. Some small sections phyllite brecciation. Think mudstone beds towards bottom @ 408.75-408.80.
D07-06	410.07	413.65	NQ	RL	LDAR	WO	LM										MD							T	<=1%					Same as above. Some thin lamining with DY. Above dyke. Py assoc with phyllite zones.
D07-06	413.65	414.14	NQ	DY	LMDK	GN	MO	DC																						Epidote phenocrysts, magnetic.
D07-06	414.14	434.50	NQ	RL	LMAR	WO	LM						CA	10			ST							T	<<1%					Rang py concentrations. Assoc with phylite bands lower contact about 0 degrees.
D07-06	434.50	435.85	NQ	DY	LMDK	LTGR	MO																							Variable. Texture and graphs size. Magnetic.
D07-06	435.85	439.10	NQ	AC	PHLM	DKGY	BN	LC									WK			L	<<1%			T	<=1%					Three 30cm zones of banded LST/argillite in section.
D07-06	439.10	439.69	NQ	AC	AR	BK	BN	LC									WK			L	<<1%			T	<<1%					
D07-06	439.69	443.10	NQ	AC	AR	BK	LM										X							T	1%					Fractured, intense carbon rich along bddg, some gouge, zones with 5 cm clots of pyrobitumen.
D07-06	443.10	445.25	NQ	AC	AR	BK	LM										X							T	<=1%					Graphite/carbon rich areas, blebs of pyrobtm. Bddg @ 30 degrees.
D07-06	445.25	446.63	NQ	DY	LMDK	GY	FG										X													
D07-06	446.63	459.03	NQ	AC	AR	Bk	LM	CT									X							T	<=1%					Some carbon rich areas, 2-5cm blebs of PyBm thrt. Bddg @ 30 degrees.
D07-06	459.03	460.20	NQ	TL	LMAR	LTGY	BN										ST													Bddg between 20-60 degrees. Banded LST/arkose, bn arkose.
D07-06	460.20	460.91	NQ	DY	LMDK	GY	FG										X													
D07-06	460.91	466.63	NQ	TL	LMAR	LTGY											ST													Bddg between 20-60 degrees, some areas. More phyllic, less calcite.

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-06	466.63	466.77	NQ	DY	LMDK	GY	PR										X													
D07-06	466.77	469.26	NQ	TL	LMAR	LTGY	BN										ST													Bddg/banding approx 5 degrees. DY 467.19 to 467.27
D07-06	469.26	479.26	NQ	KP	PHYL	LTGY	BN										MD													TL and phyllite KP mixed bands. KP with calcite veins and along bddg only.
D07-06	479.26	480.90	NQ	KP	PHYL	GYBN	LM						BD				MD					T	3%	<	<<1%					Calcite in wavy/ whispy veins along bddg.
D07-06	480.90	481.99	NQ	KP	PHYL	BRGY	LM										X													
D07-06	481.99	486.89	NQ	KP	PHYL	DKGY	LM	FR									X			G	5%			T	<<1%					
D07-06	486.89	488.28	NQ	KP	PHYL	LTGY	LM						BD				X							T	3%					Very soft, finely lam, becoming crenluated towards bottom.
D07-06	488.28	491.11	NQ	DY	LMDK	DKGY	FG										X							D	<=1%					KP @ 488.76-488.96, 489.32-490.08
D07-06	491.11	493.29	NQ	KP	PHYL	BK	LM	CT									X			/	<=1%			D	<<1%					1% pyr in 20cm areas just above LST.
D07-06	493.29	499.83	NQ	RL	LMST	GYWT	LM										ST							D	<<1%					
D07-06	499.83	506.48	NQ	KP	PHYL	GNBN	LM										X													Up to 1% pyr just below 1st, and pyr areas thrt. Chl altn along some fractures.
D07-06	506.48	509.27	NQ	DY	LMDK	DKGY	MG										X							D	<=1%					KP from 507.09-507.64
D07-06	509.27	512.22	NQ	KP	PHYL	GY	LM										X													
D07-06	512.22	512.79	NQ	DY	LMDK	DKGY	MG										X							D	tr					
D07-06	512.79	520.14	NQ	KP	PHYL	BLBN	LM						BD				X													10cm DY centered @ 518.91 and @ 518.39 -> 45 degrees, pyr present along top 50cm of section.
D07-06	520.14	520.83	NQ	KP	PHYL	BLGY	LM						BD	5			X													Silicified areas in 2-3cm bands.
D07-06	520.83	532.45	NQ	KP	PHYL	BRGY	LM						BD				X													Sil bans 531.98-532.08, chloritized band from 525.73-525.93. Finely lam/banded.
D07-06	532.45	533.20	NQ	DY	LMDK	DKGY	MG	CN	40								ST							D	<<1%					Sl. Chloritized
D07-06	533.20	540.29	NQ	KP	PHYL	GY	LM						BD				MD													1-5cm bands of calcareous zones and also of silzones thrt sections.
D07-06	540.29	540.63	NQ	DY	LMDK	DKGY	MG	CN	25								ST							D	<<1%					
D07-06	540.63	541.45	NQ	KP	PHYL	GY	LM						BD				MD													Bands of sl calc and sil.
D07-06	541.45	542.00	NQ	DY	LMDK	DKGY	MG	CN	50																					10cm sil band of KP in middle.
D07-06	542.00	544.98	NQ	KP	PHYL	GY	LM						BD				X													Only 1 minor calc band and 1 minor sil band in section
D07-06	544.98	545.58	NQ	DY	LMDK	DKGY	MG	CN	5								ST							D	<<1%					
D07-06	545.58	548.13	NQ	KP	PHYL	GY	LM										X													Much of sections siliceous. No calcareous trace. Crenulations from 547.08-548.13
D07-06	548.13	548.42	NQ	DY	LMDK	DKGY	MG	CN	5								ST							D	<<1%					
D07-06	548.42	555.65	NQ	KP	PHYL	GY	LM	CT									X													Siliceous in most areas-almost a schist- strong bk/wht banded. EOH.
D07-07	0.00	13.85	HW	OV	BLPH																									
D07-07	13.85	38.40	HQ	AC	BLPH	BK	LM						BD	40			MD													Small contortions, weathered, possible ldrs. Oxidized dy in section.
D07-07	38.40	54.21	HQ	AC	BLPH	BK	LM					TB					MD													Very broken weathered. Some fracturfe filled eith calcite.
D07-07	54.21	59.74	HQ	AC	BLPH	BK	LM																							More broken with one section only chips.
D07-07	59.74	62.79	HQ	AC	BLPH	BK	LM																							More broken with one section only chips.
D07-07	62.79	68.88	HQ	AC	BLPH	BK	LM						BD				WK	X	X											Slightly vuggy. Very broken amd moderately broken sections but all broken.
D07-07	68.88	81.08	HQ	AC	BLPH	DKGY	LM						BD																	Mostly mod-very broken, lim ib most bractures, some areas carbon rich, qz fracture fills.
D07-07	81.08	87.17	HQ	AC	BLPH	BKGY	LM						BD	15			X	X	X											Lim no some fracture surfaces, occasional qz veins 1-4cm along bddg, vuggy (1-2mm) thrt, very broken.
D07-07	87.17	90.58	HQ	AC	BLPH	BKGY	LM	FL									X													Fault zone, very broken, low recovery.
D07-07	90.58	102.29	HQ	AC	BLPH	BKGY	LM						BD	2			X			.	<<1%									Competent core- all broken into 3-10cm pieces, some areas very ruggy along bddg planes.
D07-07	102.29	114.20	HQ	AC	BLPH	GY							BD	2			X													Broken, vuggy blebs along bddg, strong lim stns along fractures, strongly sil from 105.00 and on.
D07-07	114.20	115.60	HQ	AC	BLPH	LTGY	LM										X			P	<=1%									Broken silicified zone, strongly lim thrt.
D07-07	115.60	133.52	HQ	AC	BLPH	GYBK	LM						BD	5			X			.	1%									Strongly sil thrt, strongly lim stns in areas esp 121.31-121.96 and @ 123.81, broken thrt. Carbon rich.
D07-07	133.52	138.43	HQ	AC	BLPH	GYBK	LM						BD				X			.	1%			.	tr					Slightyl more competent rk-in 2-10cm pieces thrt.
D07-07	138.43	141.78	HQ	AC	BLPH	BK	LM						BD	5			X			/	<<1%				tr					Vuggy along bddg, extr. Carbon rich.
D07-07	141.78	145.08	HQ	AC	BLPH	BKGY	LM						BD	2			X			/	<<1%				tr					Fault zone-gouge @ 142.04m, very graphitic thrt.
D07-07	145.08	150.16	HQ	AC	BLPH	BKGY	LM										WK			/	<=1%			T	<=1%					1-2cm qz veins, carbon rich, some extr graphitic areas.
D07-07	150.16	151.09	HQ	DY	LMDK	GY		CN																						
D07-07	151.09	151.24	HQ	AC	BLPH	BK	LM	FL									MD													Broken carbon rich zone.
D07-07	151.24	157.28	HQ	AC	BLPH	BKGY	LM						BD	15			ST			/	<<1%			T	<<1%					Calcite bands along laminae, some headed and re-fractured zones. Transition between AC & ES.

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-07	157.28	187.76	HQ	ES	SCHI		LM						BD	15			ST			V	<=1%									QZ veins & valets, fine cal veins along bddg, shear zone from 165.94-166.69, band @161.8 -> fines up appears to be overturned bddg.
D07-07	187.76	192.62	HQ	ES	SCHI	GY	LM	FL									ST													Carbon rich fault zone, much of it gouge; very graphitic along fract planes.
D07-07	192.62	195.89	HQ	ES	SCHI	GY	LM						BD	10			ST			<	<=1%									
D07-07	195.89	196.85	HQ	ES	SCHI	BK	LM	FL									ST			<	<<1%									Carbon rich fractured zone.
D07-07	196.85	201.53	HQ	ES	SCHI	GY	LM	CN									ST			<	<=1%									
D07-07	201.53	205.38	HQ	ES	SCHI	TanGY	LM	CN	5						PRO		ST	X	X	<	<=1%									Lim staining thrt. And esp on fract surfaces.
D07-07	205.38	225.98	HQ	ES	SCHI	GY	LM	CN									ST	X	X	<	<<1%									Limstn areas @ 206.76-207.28, 209.04, 212.90, 218.54, 222.68, 222.88 (along fractures), 223.46-223.94, 225.15-225.30, 225.63-225.72
D07-07	225.98	226.89	HQ	ES	SCHI	GY	LM	FL									ST													Lim stnd, less than 1% recovery across fault void.
D07-07	226.89	233.48	HQ	ES	SCHI	BK	LM										ST			<	<=1%									End of HQ- reduced to NQ after 233.48
D07-07	233.48	243.91	NQ	ES	SCHI	BKGY	LM						BD	10			ST			<	<<1%									Slight Ct, carbon rich on some fractures.
D07-07	243.91	245.00	NQ	ES	SCHI	BKGY	LM	FL									ST													Extr. Carbon rich/ graphitic along much of fracture.
D07-07	245.00	247.22	NQ	DY	LMDK	GNGY	MG										ST			<	<<1%									
D07-07	247.22	256.65	NQ	ES	SCHI	BKGY	LM						BD	35			ST			<	<<1%									
D07-07	256.65	256.89	NQ	ES	SCHI	BKGY	LM	FL									ST													Small sheer.
D07-07	256.89	296.68	NQ	ES	SCHI	DKGY	LM						BD	5			ST			<	<<1%									Fine wt/bk laminae.
D07-07	296.68	296.88	NQ	DY	LMDK	GY	MG										ST													
D07-07	296.88	322.89	NQ	DY	SCHI	DKGY	LM										ST							<	<=1%					<<1%py from 299.50-311.00m <=1% for rest, some areas crenulated slightly.
D07-07	322.89	324.20	NQ	DY	LMDK	GY	MG										ST													
D07-07	324.20	325.26	NQ	ES	SCHI	DKGY	LM						BD	5			ST							<	<=1%					
D07-07	325.26	326.81	NQ	DY	LMDK	GNGY	CG								PRO		ST													Chl altn
D07-07	326.81	329.68	NQ	ES	SCHI	GY	LM										ST							<	<=1%					2-15cm wide qz veins.
D07-07	329.68	331.67	NQ	DY	LMDK	GNGY	MG								PRO		ST													Very slight chl altn.
D07-07	331.67	343.51	NQ	ES	SCHI	GY	LM	CT									ST							<	<=1%					Slightly contorted laminae.
D07-07	343.51	343.67	NQ	ES	SCHI	GY	LM	FL									ST													Graphitic along small sheer.
D07-07	343.67	344.84	NQ	ES	SCHI	GY	LM						BD	20			ST							<	<=1%					Silicified
D07-07	344.84	345.01	NQ	ES	SCHI	GYBK	LM	FL									ST													Very carbon rich along shear.
D07-07	345.01	349.12	NQ	ES	SCHI	DkGy	LM										st							<	<=1%					Contorted in areas
D07-07	349.12	350.55	NQ	EB	BSP	DKGY	LM	FL		CT							ST			<	30%									Broken, silicified fracture infills graphtic.
D07-07	350.55	355.40	NQ	DY	LMDK	GY	MG										ST													
D07-07	355.40	359.76	NQ	EB	BSP	BK		CT																						Carbon rich.
D07-07	359.76	360.67	NQ	EB	BSP	BK		FL																						Intensely carbon rich/graphitic along fractures.
D07-07	360.67	377.07	NQ	EB	BSP	BK	LM																							Variously laminated/crenulated/broken.
D07-07	377.07	379.83	NQ	EB	BSP																									
D07-07	379.83	380.67	NQ	DY	LMDK																									
D07-07	380.67	385.88	NQ	EB	BSP																									
D07-07	385.88	387.86	NQ	EB	BSP																									
D07-07	387.86	392.91	NQ	DY	LMDK																									
D07-07	392.91	394.44	NQ	EB	BSP			FL																						
D07-07	394.44	394.81	NQ	DY	LMDK																									
D07-07	394.81	406.00	NQ	TS	LHAR																									
D07-07	406.00	406.52	NQ	DY	LMDK																									
D07-07	406.52	409.18	NQ	TS	LHAR																									
D07-07	409.18	414.41	NQ	RL	LMST																									
D07-07	414.41	415.62	NQ	DY	LMDK																									
D07-07	415.62	418.52	NQ	RL	LMST																									Dy from 416.11 to 416.36
D07-07	418.52	429.26	NQ	RL	LMST																									
D07-07	429.26	447.10	NQ	TS	ARLM	IV											X													Bands of lst/limey phyllite. Angle A 5-10 degrees perpenicular tca ah.
D07-07	447.10	449.54	NQ	TS	LHAR	IV	PA										X			V	20%			E	<=1%					White qtz veins 20%- small sections appear bue dy cubic, intrudeded into massive to lam. Otzite.
D07-07	449.54	467.90	NQ	TS	LHAR	LTC	BD	LC	10	FR							X							I	tr					Lam to massive occasional x-cutting py veinlet. Ends in gravelly broken section.
D07-07	467.90	468.54	NQ	DY	MFDY	DKGY	MG	DC	45								X													Dy, magnetic.
D07-07	468.54	474.15	NQ	TS	LHAR	LTGY	LM	LC	25								X							E	1%					Increasing silic content down hole. Lower contact sunrd. Increase ylw alt downage to contact.
D07-07	474.15	475.15	NQ	TS	LHAR	GY	LM										X													
D07-07	475.15	476.20	NQ	TS	QZTE	BLYL	LM	>>	15				V/	45			X													GNYLW lam alt. Within bvug qtz in.

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-07	476.20	477.32	NQ	TS	QZTE	BLYL	LM	>>	45								X													Sml blue qtz veins concordant & x-cutting to laminae.
D07-07	477.32	478.30	NQ	TS	LHAR	MDGY	LM										X							B	<<1%					Small 2cm QV 45 degrees TCA with 1% py . Very silicious bleaching alteration from silicious infill of small cracks.
D07-07	478.30	483.55	NQ	TS	QZAR	MOGY	MB										X							T	1%					Cut by rare qv, and discordant pyrite veins up to 1cm thich. Colour varies from dark to light gy Alt along microfractures.
D07-07	483.55	484.42	NQ	DY	MFDY	LTBK	PR	DC	5																					
D07-07	484.42	497.77	NQ	TS	LHAR	MDGY	MB										X							T	1%					See 478-483 comments 496 open fractures.
D07-07	497.77	498.21	NQ	DY	MFDY	ltbk	PR	DC	20																					
D07-07	498.21	510.38	NQ	TS	LHAR	LTGY	MB										X													Tiger strip colour pattern to colour from LT-MD GY. Almost schistosen Lrgt stylolite parallel TCA.
D07-07	510.38	511.38	NQ	TS	LHAR	LTGY	MB										X								<=1%					As above.
D07-07	511.38	512.38	NQ	TS	QZAR	BL	MO										X			I	10%			B	5%					Blue qtz flooding. Msv dy @ 512.50-512.68. Assoc with x-serrentine veinlet & blue qtz.
D07-07	512.38	513.42	NQ	TS	LHAR	LTGY	LM	LC	30								X							T	1%					back to lam, sil. Trueman.
D07-07	513.42	517.74	NQ	TS	LHAR	LTGY	LM	LC	45															T	<<1%					As above. Incr sil & x-cutting py vgnlgts.
D07-07	517.74	521.00	NQ	TS	QZAR	BR	MO						CA	45			X							I	1%					Very silicious.
D07-07	521.00	521.58	NQ	RL	LMST	WT	MB	LC	20								ST	X	X											Crystalling limestone, msv to lam, minor arg. Lower contact gradational.
D07-07	521.58	525.34	NQ	RL	LMAR	GY	LM	LC	25								ST							/	50%					Incr arg. Lower contact disconformated.
D07-07	525.34	533.40	NQ	RL	LMST	WH	MB																	<	<=1%					Rare laminations.
D07-07	533.40	538.21	NQ	RL	LMAR	LTGY	LM	LC	20								ST													WH qtz vein 533.74-533.91 . Interbedded msv lmstn beds 2-10cm thick.
D07-07	538.21	541.00	NQ	RL	LMST	WH	MB										ST													H&L contacts gradational
D07-07	541.00	547.75	NQ	RL	LMAR	LTGY	LM	LC	15								ST													2 small qv with magnetic selvages (ylw, acid rxn) sml section of fractures 544.37-544.84
D07-07	547.75	548.09	NQ	RL	LMAR	OR	MS										ST	X	X											Oxidized section 40cm fractured rock either side.
D07-07	548.09	564.10	NQ	RL	LMAR	MDGY	LM	LC	15								ST													Incr arlgillite sown secton. Still very limey. Lower contatct. Gradational some contorted beds towards btm.
D07-07	564.10	565.62	NQ	RL	LMST	LTGYWH	MB										ST													
D07-07	565.62	589.10	NQ	RL	LMAR	MDGY	LM	LC	20								ST							D						Well am small sections of pure limestone.
D07-07	589.10	590.09	NQ	RL	LMAR	MDGY	LM	LC	20								ST													
D07-07	590.09	591.10	NQ	RL	LMAR	MDGY	LM	LC	20				SIG	20			ST							D	<<1%			C	<<1%	5cm section with weathered ;yrite & ylw-gld sphalerite in concordand laminae.
D07-07	591.10	592.12	NQ	RL	LMAR	MDGY	LM	LC	26				U/	30			ST													591.81-disconformith
D07-07	592.12	616.00	NQ	RL	LMAR	LTGY	LM	LC	25								ST													Mag. Small breccia 610.50 Lower contact gradational
D07-07	616.00	620.09	NQ	RL	LMAR	LTBL	LM	LC	25								ST													CG
D07-07	620.09	623.44	NQ	RL	LMST	WO	BD	LC	35								ST													Pure limestone gradine into laminated argillicaious beds.
D07-07	623.44	637.76	NQ	RL	LMAR	LTGY		LC	20								ST													
D07-07	637.76	638.21	NQ	DY	MFDY	DKGY	CG	DC	15																					
D07-07	638.21	643.61	NQ	RL	LMAR	WO	LM	LC	25								ST													
D07-07	643.61	645.06	NQ	DY	MFDY	DKGY	CG	DC	15																					Sharp contacts flat mag.
D07-07	645.06	649.04	NQ	RL	LMAR	WO	BD	LC	25	FR							ST													Occassional sections of fractured rock. Calcite infill in some fractures.
D07-07	649.04	649.47	NQ	DY	MFDY	DKGN	CG																							Contacts sharp, irregular mag.
D07-07	649.47	651.17	NQ	RL	LMAR	IV	BD			FR																				
D07-07	651.17	651.41	NQ	RL	LMAR	IV	FG	BR																						Brecciated section.
D07-07	651.41	652.10	NQ	DY	MFDY	LTGY	PR																							Upper contact sharp, intercalated. Lower sharp irregular . Non mag.
D07-07	652.10	652.39	NQ	RL	LMAR	WO	BD																							
D07-07	652.39	652.98	NQ	DY	MFDY	DKGY	PR																							Abrupt irregular contacts. Mag.
D07-07	652.98	659.80	NQ	RL	LMAR	WO	BD																							
D07-07	659.80	660.12	NQ	DY	MFDY	DKGY		DC	30																					Irregular sharp mag
D07-07	660.12	662.59	NQ	RL	LMAR	WO	BD	LC	20																					
D07-07	662.59	663.56	NQ	DY	MFDY	DKGY																								10cm sections of LMAR. Contacts sharply flat. Mag.
D07-07	663.56	669.48	NQ	RL	LMAR	WO	BD	LC	5																tr					Calcite filled fractures near bottom of section.
D07-07	669.48	675.27	NQ	RL	LMST	WO	BD	LC	15	GD																				Becomes more massive, contains some argillite, top of sequence 5cm calcie mudstone. Change of dip direction & angle below. Appears to be some graded bedding, tops up hole.
D07-07	675.27	682.59	NQ	RL	LMST	WO	LM	CN									ST													Some contorted sections, grades into LMAR towards bottom.
D07-07	682.59	683.36	NQ	DY	MFDY	DKGY	CG																							
D07-07	683.36	687.77	NQ	RL	LMAR	WO	LM	FL		FR							ST													Variable breccia section from total breccia to tension filled with calcite @ bottom of section.

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-07	687.77	711.23	NQ	RL	LMAR	WO	LM	LC	15																					Some graded bedding, stylolites, interbedded LMST/LMAR.
D07-07	711.23	711.42	NQ	DY	MFDY	LY																								
D07-07	711.42	727.13	NQ	RL	LMAR	WO	LM																							
D07-07	727.13	727.25	NQ	DY	MFDY																									
D07-07	727.25	730.97	NQ	RL	LMAR	WO	LM																							Thin non-mag dylelets. Upper and lower contacts brecciated.
D07-07	730.97	731.43	NQ	DY	MFDY	WO																								
D07-07	731.43	738.94	NQ	RL	LMAR	WO	LM																							Laminae interleaved. Graded bedding. Top-up. Some mudstone clasts.
D07-07	738.94	748.92	NQ	RL	LMST	WO	BD																							
D07-07	748.92	749.40	NQ	DY	LMST	WO																								as above mag sharp contacts.
D07-07	749.40	750.39	NQ	RL	LMST	WO	BD	BR																						Fragments of laminated LMST in coarse limestone matrix lower contact abrupt into laminated LMAR.
D07-07	750.39	754.84	NQ	RL	LMAR	WO	CG	LC	15								ST													Lam c.gr with
D07-07	754.84	759.88	NQ	RL	LMAR	WO	VA	BR		FR							ST													Fractures filled with calcite cut across breccia & laminations.
D07-07	759.88	760.07	NQ	DY	MFDY	DKGY	PR																							
D07-07	760.07	760.33	NQ	RL	LMAR	WO	LM	LC									ST													
D07-07	760.33	761.06	NQ	DY	MFDY	GY	PR																							
D07-07	761.06	767.11	NQ	RL	LMAR	LTGY	LM										ST													
D07-07	767.11	767.32	NQ	DY	MFDY	DKGY	PR	CN	30																					Upper and lower contacts 30 degrees
D07-07	767.32	767.71	NQ	RL	LMAR	LTGY	LM										ST													
D07-07	767.71	768.36	NQ	DY	MFDY	DKGY											ST													
D07-07	768.36	773.46	NQ	RL	LMAR	LTGY	LM	LC	25								ST													
D07-07	773.46	775.00	NQ	RL	LMAR	LTGY	LM	LC	25	FR							ST							/	<=1%					
D07-07	775.00	776.46	NQ	RL	LMAR	LTGY	LM	LC	20	FR							ST							/	1%					Contacts with dyke have concentrated py
D07-07	776.46	777.24	NQ	DY	MFDY	DKGY											ST													Contacts sharp, flat. Magnetic.
D07-07	777.24	778.75	NQ	RL	LMAR	WO	LM	LC	25								ST							/	tr					Upper contact concentrated py. Some contorted laminag, recrystallized calcite. Small breccia unit.
D07-07	778.75	780.19	NQ	RL	LMAR	LTGY	LM	LC									ST							/	tr					as above.
D07-07	780.19	781.81	NQ	RL	LMAR	LTGY	LM	LC	20								ST							T	tr					
D07-07	781.81	783.32	NQ	RL	LMST	LTGY	LM	LC	20								ST							T	tr					
D07-07	783.32	784.51	NQ	RL	LMAR	LTGY	VA	BR									ST							T	tr					Rare laminated section contorted. Breccia.
D07-07	784.51	786.15	NQ	RL	LMAR	MDGY	LM	CN									ST							T	tr					Scmqtz vein 784.54-784.59- minor folds laminae
D07-07	786.15	786.80	NQ	FL	MFDY	GY	MS										X													Fault gouge, very competent.
D07-07	786.80	792.56	NQ	ES	GCHP	BK	VA	FL									MD							E	<=1%					Graphitic schist breccia. Very broken.
D07-07	792.56	792.73	NQ	DY	GCHP	LTGY											X													Bleached lt gy.
D07-07	792.73	794.32	NQ	ES	GCHP	BK	VA	FL									WK							E	<=1%					
D07-07	794.32	795.87	NQ	DY	MFDY	DKGY	PR																							
D07-07	795.87	797.36	NQ	ES	BLPH	DKGY	LM	CN									X							E	<=1%					Contorted laminae.
D07-07	797.36	821.74	NQ	ES	BLPH	DKGY	LM	LC	20								WK							E	<=1%					Occassional qtz vein white.
D07-08	0.00	4.75	HQ	n/a	OVBN																									Oberburden/broken- no recovery
D07-08	4.75	26.00	HQ	AC	BLPH	GYBK	LM	CT					BD	5			MD			<	<<1%			T	<=1%					Some areas with larger (2-10mm) blebs of fg py.
D07-08	26.00	29.21	HQ	AC	BLPH	GYBK	LM	CT									MD			<	<<1%			T	<=1%					
D07-08	29.21	29.97	HQ	AC	BLPH	GYBK	LM	CT					BD	62			MD			<	<<1%			T	<=1%					
D07-08	29.97	49.01	HQ	AC	BLPH	GYBK	LM	CT					BD	5			MD			<	<<1%			T	<=1%					6cm DY @ 47.33, Py diss thrt, some 2-5mm clots of py along bddg. Pyr rich zones as well.
D07-08	49.01	49.39	HQ	DY	LMDK	GY		CN	23								MD							D	<<1%					
D07-08	49.39	52.93	HQ	AC	ARLM	GYBK	LM						BD	30			ST							T	<<1%					Sil bands and some 2cm qz veins moderately carbon rich if not silicified.
D07-08	52.93	53.64	HQ	DY	LMDK	GY											MD													Some chlorite altn of individ grains.
D07-08	53.64	64.60	HQ	AC	ARLM	DKGY	LM						BD	40			ST							T	<=1%					Carbon rich on fractures. Pyrn clots and diss in bands parallel to bddg, DY @ 54.32, 54.45-54.81, 55.00, 55.34-55.90, 59.20, 61.62-61.88, 63.27-63.42. DY parallel to bddg. Sil zones banded thrt, carbon rich esp on fractures.
D07-08	64.60	64.73	HQ	DY	LMDK	GY											MD													1.2mm bt books in dyke.
D07-08	64.73	72.10	HQ	AC	BLPH	BKGY	LM	CT	20								WK			<	2%			T	<=1%					Strongly sil thrt, bands and clots/blebs of pyr, Dy 65.57-65.67, 65.88-66.08, numerous dy from 66.93-69.93 aprrox 20-30cm.
D07-08	72.10	77.77	HQ	DY	LMDK	GYGN											MD													Mod to strong chl altn pervasive thrt.
D07-08	77.77	78.55	HQ	AC	BLPH	BKGY	LM	FL									MD							T	2%					Broken, faulted zone.
D07-08	78.55	80.21	HQ	AC	BLPH	BKGY	LM						BD	8			MD							T	2%					Some veins of py clots/blebs, mod carbon rich, calc bands thrt.
D07-08	80.21	82.66	HQ	DY	LMDK	BRGY	CG								PRO		MD													Slight chl altn, esp on fractures.
D07-08	82.66	94.76	HQ	AC	BLPH	BK	LM						BD	10			MD			P	<=1%			<	<=1%					Silicified thrt, calcite bands (thin), fine crenulations, bands of pyr as well.
D07-08	94.76	95.65	HQ	AC	BLPH	BK	LM	FL									MD													Broken acrbon rich with 24cm DY in middle of section.

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-08	95.65	99.04	HQ	AC	BLPH	BK	LM	CR									WK			P	<=1%			<	<=1%					Very silicified thrt.
D07-08	99.04	100.91	HQ	AC	BLPH	GYBK	LM						BD	10			WK			P	2%			<	<=1%					1-3cm calcite bands thrt, slightly cal along thing lam.
D07-08	100.91	103.62	HQ	AC	BLPH	GYBK	LM						BD	25			X			P	2%			<	<=1%					PY and Pyr in 1cm bands and clots and thrt.
D07-08	103.62	104.00	HQ	DY	LMDK		CG										WK													
D07-08	104.00	104.57	HQ	AC	BLPH	BK	LM	CR									X			P	<=1%			<	<=1%					Clots and bands of pyr in section.
D07-08	104.57	119.58	HQ	DY	LMDK	GYGN	CG	CN	30						PRO		WK													Chl alt'd thrt, esp along fractures fg section rfom 108.84-109.43, fractured from 110.14-112.77.
D07-08	119.58	123.44	HQ	AC	BLPH	BK	LM										X							<	2%					Minor contorted/crenulated in areas very sil thrt qz veins/bands 1cm thick, py/pyr together.
D07-08	123.44	123.81	HQ	AC	BLPH	BK	FL																							
D07-08	123.81	124.85	HQ	DY	LMDK	GYGN	CG								PRO															Chl alt'd thrt mainly broken/faulted.
D07-08	124.85	128.76	HQ	AC	LMDK	GYGN	CG										X							<	2%					Silicified, py and pyr thrt.
D07-08	128.76	130.96	HQ	AC	LMDK	GYGN	CG										X													Mixed with DY @ 128.76-128.96, 129.00-129.08,
D07-08	130.96	131.81	HQ	DY	LMDK	MG											X													Not chl altd.
D07-08	131.81	133.45	HQ	AC	BLPH	BK	LM	CR									X			P				<	<=1%					Strongly sil thrt, py & pyr along lam thrt.
D07-08	133.45	142.54	HQ	AC	BLPH	BK	LM	CN	20								X			P				<	<=1%					DY 133.45-133.48, 134.28-134.45, 136.10-136.36, 136.69-136.94, 137.46-137.53, 138.09-138.12, 139.69-139.81, 142.38-142.52 . Sil AC hrt, fg py/pyr, fg dy not chl alt 'd.
D07-08	142.54	142.93	HQ	AC	BLPH	BK	LM	CR									ST													Calcite banding.
D07-08	142.93	145.91	HQ	DY	LMDK	GNGY	CG								PRO															Mad-Int chl altn thrt, esp along fractures. Faulted at contact (145.91).
D07-08	145.91	147.67	HQ	AC	BLPH	BK	LM										X							<						2cm clot of pyr/py, py/pyr mnlzd bands thrt, DY 146.47-146.53
D07-08	147.67	147.87	HQ	DY	LMDK	GY	FG																							
D07-08	147.87	184.70	HQ	AC	BLPH	BK	LM										MD			P	<=1%			T	<=1%					Limey band and sil bands thrt, some large clots/ veins of py & pyr, pyr not as abundant except in veins. Qz calcite veins 1-2cm wide, fg py along bddg thrt, carbon rich thrt, only occasional crenulations.
D07-08	184.70	186.10	HQ	AC	BLPH	BK	LM	FL									MD			P	<=1%			T	<=1%					Carbon rich.
D07-08	186.10	187.28	HQ	AC	BLPH	BK	LM										MD			P	<=1%			T	<<1%					Carbon rich.
D07-08	187.28	207.84	HQ	AC	BLPH	BK	LM	CN									X			P	<=1%			T	<<1%					Calcite in some areas along bddg. Carbon rich.
D07-08	207.84	208.64	HQ	AC	BLPH	BK	LM						BD	25			ST			V	20%			T	<=1%					Fractured and healed zone. Carbon rich.
D07-08	208.64	209.40	HQ	AC	BLPH	BK	LM	FR									X													Variously fractured, some zones of gouge.
D07-08	209.40	213.05	HQ	AC	BLPH	BK	LM										X			P	<=1%			T	<=1%					
D07-08	213.05	213.90	HQ	AC	BLPH	BK	LM	FR																						
D07-08	213.90	221.00	HQ	AC	BLPH	BK	LM						BD	5			WK			P	<<1%			T	<<1%					Small fault @ 216.35 and another @ 217.50-217.80
D07-08	221.00	250.85	HQ	AC	BLPH	BK	LM										X			P	<<1%			T	2%					Carbon rich esp on fracture surfaces, minor crenulations in areas, vvfg py thrt, calcite laminae in some places, charge to NR 231.50
D07-08	250.85	255.02	NQ	AC	BLPH	BK	LM	FR									X							T	<=1%					Broken and some gouge, intensely carbon rich.
D07-08	255.02	275.14	NQ	AC	BLPH	BK	LM										X			P	<<1%			T	1%					Carbon rich along fractures, very hard, carbon rich on all fracture surfaces.
D07-08	275.14	275.77	NQ	DY	LMDK	GY		CN	30								X													
D07-08	275.77	277.26	NQ	AC	BLPH	BK	LM						BD	7			X			P	1%									Very hard, 3mm qz veins @ 12 degrees, x-cutting bddg, graphite rich on fractures.
D07-08	277.26	278.21	NQ	DY	LMDK	GYGN	CG	CN	30						PRO	t	X							T	tr					Slightly chl alt'd, 41cm wide dy intruded into center of main dyke.
D07-08	278.21	291.09	NQ	AC	BLPH	BK	LM						BD	20			X			P	1%			T	3%					Small DY @ 290.00-290.18, extra carbon rich along fracts.
D07-08	291.09	293.18	NQ	AC	BLPH	BK	LM	FR									X							T	3%					Strongly carbon rich thrt, calcareous from 292.45-293.18, fg py in areas. Faulted 291.09-292.15, also very carbon rich.
D07-08	293.18	294.96	NQ	AC	BLPH	BK	LM										X	X		I	2%									2cm qz veins with 10%-15% sphal in veins @ 294.72m, 5 other 2cm qz veins, no mineralization, trace oxide in qz veins
D07-08	294.96	319.71	NQ	AC	BLPH	GYBK	LM						BD	5			X			<	2%			T	tr					Graphite rich on fractures, very silicious, very fractured and qz rich 318.10-319.71, also <1% py in this zone.
D07-08	319.71	320.15	NQ	DY	LMDK	GY	FG										X													
D07-08	320.15	320.74	NQ	AC	BLPH	GYBK	LM	CN									X			<	2%									
D07-08	320.74	321.01	NQ	DY	LMDK	GY	FG										X													
D07-08	321.01	328.84	NQ	AC	BLPH	GYBK	LM	CT									X			<	2%			T	<=1%					Slightly crenulated and contorted.
D07-08	328.84	333.19	NQ	DY	LMDK	GY	FG										X													
D07-08	333.19	350.51	NQ	AC	BLPH	BK	LM	FR									X			<	10%			T	<=1%					Fractured and filled with qz veins, graphite on fract surfaces. Very siliceous- almost cherty appearance.
D07-08	350.51	366.06	NQ	AC	BLPH	BK	LM						BD	20			X			<	<=1%			T	1%					Qz fract fills @ 355.80-356.39 and 364.84-366.06, some slightly crenulated.
D07-08	366.06	366.22	NQ	DY	LMDK	dkgy	FG										X													

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-08	366.22	386.72	NQ	AC	BLPH	bk	LM	CT					BD	15			X			<	<=1%			T	2%					Almost cherty, graphitic on fractures, finely bedded or slightly crenualted
D07-08	386.72	389.67	NQ	DY	LMDK	DKGY											X			<	<=1%			T	<<1%					Mixed zone of 20-40cm either DY or broken, qz veined AC.
D07-08	389.67	392.97	NQ	DY	LMDK	GY	MG										X													
D07-08	392.97	394.17	NQ	RL	LMST	GY	LM						BD	15			ST							<	<<1%					
D07-08	394.17	396.03	NQ	RL	DOST	GY	LM						BD	5			MD							<	2%					Vfg py and pyr.
D07-08	396.03	402.55	NQ	RL	LMST	WTGY	LM						BD	5			ST													
D07-08	402.55	404.10	NQ	TS	SCHI	GNGY	LM						BD	5			X			<	<<1%									
D07-08	404.10	407.31	NQ	TS	SCHI	GNGY	LM										X			<	10%			<	1%					Mixed TS and RQ. Extremeyl siliceous rock.
D07-09	0.00	15.24	HW	OV	OVBN																									
D07-09	15.24	104.86	HQ	AC	AR	BK	LM	LC	45								WK							B	<=1%					19.45-20m white, irreg, qtz vein. Lam vary 20-45 degrees.
D07-09	104.86	105.60	HQ	DY	MFDY	GY	PR	DC	50				BD																	Mag. Upper contact=event.
D07-09	105.60	115.28	HQ	AC	AR	BK	LM	LC	10								WK													Mostly flat lam 50m, contorted.
D07-09	115.28	116.90	HQ	DY	MFDY	GY	PR	LC	20																					Mag
D07-09	116.90	117.98	HQ	AC	AR	GY-WH		CT		FR							WK													
D07-09	117.98	119.80	HQ	AC	AR	BK											MD													Graphite
D07-09	119.80	120.74	HQ	DY	AR	GY		CN																						Mag
D07-09	120.74	122.06	HQ	ES	BLPH	GY																		T	<=1%					
D07-09	122.06	125.78	HQ	DY	AR												X													Brk 124.90-125.10 Thin schist (15cm) @ 123.82 breccia @125.10 mag.
D07-09	125.78	145.80	HQ	ES	BLPH																									Small dyke 140.00 - 140.58
D07-09	145.80	146.31	NQ	DY	LMDK																									
D07-09	146.31	154.42	HQ	ES	SCPH	LTGY											WK							T	<<1%					Wk crenulations. Pyrohite becomes more prevalent.
D07-09	154.42	155.43	HQ	DY	MFDY	GY	FG																							Upper contact 10 degrees TCA. Lower contact 20 degrees.
D07-09	155.43	157.72	HQ	ES	SCPH	LTGY	MO										ST													Very contorted laminae. Py/pyhrotic.
D07-09	157.72	158.70	HQ	DY	MFDY	LTGY	FG										X													Mag
D07-09	158.70	159.29	HQ	ES	SCPH	MDGY	MO										MD													Mag
D07-09	159.29	161.05	HQ	DY	SCPH	LTGY	FG										X													Mag
D07-09	161.05	171.37	HQ	ES	SCPH	MDGY	MO										MD													Mag
D07-09	171.37	171.76	HQ	ES	PHLM	WO/BK	LM	VV	45								ST													Lam phyllite with qtz/calcite veins-
D07-09	171.76	189.93	HQ	ES	SCPH	LTGY	MO										MD													All of original bedding features destroyed. Thin clay seam 174.83-174.85
D07-09	189.93	192.30	HQ	ES	SCPH	LTGY	LM	LC	45								ST													Lam, as above. Non mag.
D07-09	192.30	201.08	NQ	ES	SCPH	LTGY		LC	45								ST													Massive with lam sections. Less sericite, serpentine.
D07-09	201.08	201.27	NQ	ES	BLPH	BK		LC	40								X							A	<=1%					LM, silica blebs.
D07-09	201.27	207.75	NQ	ES	BLPH	bk		LC	40								x							A	<=1%					
D07-09	207.75	223.44	NQ	ES	SCPH	LTGY											MD							T	tr					Upper contact abrupt, non calcic; strong acid 30cm below contact. 25cm qv @ 213.34
D07-09	223.44	223.68	NQ	ES	BLPH	Bk	LM	CT	40								X							/	<=1%					Graphitic phyllite with qtz irregular veinlets. Uppercontact sharp.
D07-09	223.68	224.00	NQ	ES	BLPH	BK	MO	FL									X				<=1%									Fault contorted laminae with qtz flooding. Two sections crumbly core.
D07-09	224.00	229.16	NQ	ES	BLPH			LC	30								X													225.2/5cm clay/crumble zone rare qv'let crumlated or poss slickerslide
D07-09	229.16	230.61	NQ	ES	BLPH	Bk		CN	3								X							T	tr					Much more contorted with qtz flooding graphitic.
D07-09	230.61	236.72	NQ	ES	BLPH	BK	LM	CN									X							E	2%					Finely contorted/laminated sil phyllite. Graphitic.
D07-09	236.72	260.22	NQ	FL	BLPH	Bk		CN									X													234.72-235.16 crumbly texture many blocky sections.
D07-09	260.22	262.23	NQ	DY	MFDY	DKGY	MO																							Upper contact sharp flat, lower sharp.
D07-09	262.23	270.31	NQ	ES	BLPH	BK	LM						H/W	30			WK													Fractures lined with calcite crystals. Lower contact disconformable, sharp dipping 30 degrees. 20cm oxidized zone 1m above lower contact.
D07-09	270.31	279.04	NQ	RL	LMAR	WO	LM	CN									ST	X	X											Foldin, oxidized layers prevalent with up to 50% material removed in 1-3cm widths, blocking in 3 places.
D07-09	279.04	279.30	NQ	DY	MFDY	DKGY	PR																	E	tr					Sharp contact mag.
D07-09	279.30	285.13	NQ	RL	LMAR	WO	LM	LC									ST	X	X					E	tr					Less contorted laminae rarer oxidized zones. Rare py lenses. Lwr laminae contacted before lower contact.
D07-09	285.13	285.19	NQ	DY	MFDY	DKGY	PR																							
D07-09	285.19	300.39	NQ	RL	LMAR	WO	LM	LC	20	FR							ST	X	X					E	<<1%					Upper contact contorted laminae. Laminae angle varies from 5-20 degrees. Oxidized 230.35-230.50, +293
D07-09	300.39	300.85	NQ	DY	MFDY	DKGY	PR										ST	X	X											
D07-09	300.85	304.11	NQ	RL	MFDY	WO	LM	LC		BR																				Fractures with crystal calcite on surfaces. Laminae disturbed. Rounded entrolithic clasts in places.
D07-09	304.11	304.28	NQ	DY	MFDY																									As above

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-09	304.28	307.16	NQ	RL	LMST	IV	BD										ST													Some argillacious bands.
D07-09	307.16	307.85	NQ	TS	LMST	LTBR											MD													Brecciated with brown.
D07-09	307.85	309.44	NQ	RL	LMAR	LTGY	LM										ST													
D07-09	309.44	310.56	NQ	RL	LMST	WO											ST													
D07-09	310.56	310.71	NQ	RL	LMDK	BK	CG										X	X	X											Bhyrelamprophyrg dyke non mag. Sharp, planar contacts.
D07-09	310.71	325.07	NQ	RL	LMAR	LTGY	LM	LC	20								ST													
D07-09	325.07	331.25	NQ	RL	LMST	IV	BD	LC	25								ST													
D07-09	331.25	332.51	NQ	RL	LDAR	GY-YL	MO	FL					CA				MD	X	X											Stylolites common near top. Rounded enterolitric fragments. Some oxidation small voids. Calcite filled fractures.
D07-09	332.51	332.84	NQ	RL	LMAR	LTGY	LM	LC	10								ST													
D07-09	332.84	334.66	NQ	RL	LDAR	GY-YL	MO						CA				WK	X	X											
D07-09	334.66	336.03	NQ	RL	LMAR	LTGY	LM	LC	20								ST	X	X											
D07-09	336.03	337.26	NQ	RL	LDAR	GY-YL	MO										WK	MD	X					D	tr					Rare laminated remnant of lmar.
D07-09	337.26	338.69	NQ	RL	LMAR	LTGY	LM	LC	25															D	tr					Oxidized void on lower 10cm. Lost hole at this point due to stuck rods. Retrieved string except core barrel. Tried to drill through but cave threathened to seize rods again. Hole abandoned.
D07-10	0.00	9.14	HW	OV	OVBN																									
D07-10	9.14	37.87	HQ	AC	AR	DKGY	LM	FR									WK													Small fracture zones. Qtzite infill. Acid reaction along limey laminae.
D07-10	37.87	39.32	HQ	DY	MFDY	GY	MS																							
D07-10	39.32	42.22	HQ	AC	AR	DKGY	LM	FR									WK													
D07-10	42.22	42.96	HQ	DY	MFDY	MDGY	MS																							
D07-10	42.96	43.91	HQ	AC	AR	DKGY	LM	FR					BD	15			WK													
D07-10	43.91	44.74	HQ	AC	AR	DKGY	MO	BR		CN		TB	BRS				WK													Graphitic sil. Contorted fractures filled with qtzite. Slickensides on some surfaces.
D07-10	44.74	47.55	HQ	DY	MFDY																									
D07-10	47.55	56.49	HQ	AC	AR	DKGY	MO	CK		CN			F/C				X													Crumbly
D07-10	56.49	63.13	HQ	AC	AR	DKGY	LM	LC	25								WK													Folding. Increasing to lower contact.
D07-10	63.13	63.66	HQ	DY	MFDY																									
D07-10	63.66	78.28	HQ	AC	AR	DKGY	LM	LC									X							D	<<1%					Laminae vary from 20 degrees to parallel tca. Folding.
D07-10	78.28	78.99	HQ	DY	MFDY	LTGY											WK													Bleached.
D07-10	78.99	87.00	HQ	AC	AR	DKGY	LM	LC									WK							E	<=1%					Same folds.
D07-10	87.00	111.56	HQ	AC	AR	DKGY		FL				TB	F/C		CAR		WK													Alternating sections of fractured, brecciated, laminated, blocky & crumbly material graphitic.
D07-10	111.56	117.92	HQ	AC	AR	DKGY	LM	CN																						Blocky fractures, but much more competent than section above.
D07-10	117.92	120.00	HQ	AC	AR	DKGY		FL																						Silicz flooding.
D07-10	120.00	120.80	HQ	DY	MFDY	LTGY	MG																							
D07-10	120.80	140.70	HQ	AC	AR	DKGY	LM	CN	45	FR							WK							T	<<1%					Fractures infilled with qtz, pyrite. Contorted to laminated. Small brecca @ 132.45
D07-10	140.70	142.52	HQ	AC	AR	WH	CG	QV																						Wh. Quartz vein. Broken with argillite.
D07-10	142.52	187.39	HQ	AC	AR												WK													As 120-140m. Small broken sections.
D07-10	187.39	189.19	HQ	DY	MFDY	LTGY											X													
D07-10	189.19	190.62	HQ	AC	AR	DKGY	LM	LC	20								WK													
D07-10	190.62	214.73	HQ	AC	AR	DKGY		CN									WK													Much more convoluted lamnac, folding, fractures filled with calcite/qtz common.
D07-10	214.73	215.73	HQ	DY	MFDY												X													
D07-10	215.73	225.86	HQ	AC	AR	DKGY		CN	25								WK													As 190-214
D07-10	225.86	271.75	NQ	AC	AR	DKGY	LM	LC									MD													Core angle triangles from 5-30n degrees. Some contorted sections.
D07-10	271.75	275.84	NQ	AC	AR	DKGY	LM	BR		CN							WK													Broken, fractured with calcite/qtz. Infill.
D07-10	275.84	276.57	NQ	DY	MFDY	LTGY	MS					CB																		Pale gray, bleached.
D07-10	276.57	279.75	NQ	ES	BLPH	DKGY	LM	BR				CB																		Broken, fract, with C2CO3/S1O2 infill.
D07-10	279.75	289.00	NQ	ES	BLPH	BK	LM																							
D07-10	289.00	290.72	NQ	DY	MFDY																									Lower contact 3cm breccia.
D07-10	290.72	351.46	NQ	ES	BLPH	BK	LM	LC	20															E	<=1%					Increase grain size. Some graded bedding, tops down, enterolothe folding.
D07-10	351.46	352.97	NQ	ES	BLPH	GN	LM	FR																						Healed and refractured, vuggy, carbon rich on fracture surfaces.
D07-10	352.97	363.25	NQ	ES	BLPH	Bk	LM																	T	<=1%					20cm Dy @ 328.73 @ 50 degrees
D07-10	363.25	366.22	NQ	ES	BLPH	Bk	LM	FR																						Extremely broken & carbon rich thrt, 25cm DY @ 365.21 @ 0 degrees. 365.75-366.22 fractured.
D07-10	366.22	367.77	NQ	DY	LMDK	GY	FG	CN	10								WK													

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								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-10	367.77	370.64	NQ	ES	BLPH	DK	LM	CT									ST							T	<=1%					Bands of limey schist thrt- limey areas fg, no qz.
D07-10	370.64	385.70	NQ	ES	BLPH	GYBK	LM	CT									X							T	<=1%					Small carbon rich fracture area @ 379.78
D07-10	385.70	387.48	NQ	ES	BLPH	GYBK	LM	FR									X													Carbon rich on fracture surfaces.
D07-10	387.48	434.20	NQ	ES	BLPH	GYBK	LM	CT									X							T	<=1%					Carbon rich on fracture surfaces.
D07-10	434.20	437.25	NQ	ES	BLPH	DKGY	LM						BD	60			X							T	<=1%					Bedding sharply changes to 60 degrees.
D07-10	437.25	439.36	NQ	ES	BLPH	DKGY	LM	FR									X			V	<=1%			T	<<1%					Brittle fractures, 1-10m qz crosscutying and along structures.
D07-10	439.36	441.97	NQ	DY	LMDK	GYGN	CG										X													Slight chlorite alteration thrt. DY contact @ 30 degrees.
D07-10	441.97	451.30	NQ	ES	BLPH	Bk	LM						BD	10			MD							T	<=1%					
D07-10	451.30	452.12	NQ	ES	BLPH	GYBK	LM	FR									MD			V	<=1%									Mostly brittle fractures, fault gauge in center area.
D07-10	452.12	456.30	NQ	ES	BLPH	GYBK	LM										MD							T	<=1%					Graphitic on fracture surfaces.
D07-10	456.30	456.74	NQ	DY	LMDK	GYGN	FG										X													Very slight chloritic alteration.
D07-10	456.74	482.00	NQ	ES	BLPH	BK	LM										MD							T	<=1%					Bands and stringers of calcite. Sphal in 7cm qz vn @ 480.00
D07-10	482.00	482.17	NQ	DY	LMDK	DKGY	FG										X													
D07-10	482.17	494.80	NQ	ES	BLPH	BK	LM										MD							T	<=1%					Sphal in 6cm qz vn @ 483.48
D07-10	494.80	495.46	NQ	DY	LMDK	LTGY											X													
D07-10	495.46	514.46	NQ	ES	BLPH	BK	LM										MD							T	<=1%					Small trace of sphal in 7cm qz vn at 505.0m, some chl on fractures in this area also.
D07-10	514.46	514.78	NQ	DY	LMDK	GNGY	FG	CN	50								MD													Slightly chloritized.
D07-10	514.78	515.85	NQ	ES	BLPH	BK	LM										MD							T	<=1%					
D07-10	515.85	524.18	NQ	DY	LMDK	GN	CG	CN	5								MD							D	<<1%					Varied thrt 'bands' of different textures.
D07-10	524.18	535.76	NQ	ES	BLPH	BK	LM										ST							T	<=1%					Core broken into 3-5cm pieces thrt, strong calcite to approxitmately 535.13m, weak after thrt.
D07-10	535.76	536.36	NQ	DY	LMDK	GY	MG										MD													2cm dyke within a dyke in center.
D07-10	536.36	543.99	NQ	ES	BLPH	BK	LM										WK							T	<=1%					Core broken into 3-5cm pieces thrt.
D07-10	543.99	556.68	NQ	ES	BLPH	BK	LM										MD							T	<=1%					Carbon rich on fracture surfaces- zones very limey.
D07-10	556.68	557.97	NQ	DY	LMDK	DKGY	CG	CN	5								WK													Clay/gouge at top contact.
D07-10	557.97	558.85	NQ	ES	BLPH	BK	LM	FR									WK							T	<<1%					Barbon rich thrt, 1-4cm pieces in fracture zone.
D07-10	558.85	571.90	NQ	ES	BLPH	BK	LM	CT									MD							T	<=1%					Minor crenulations and contortions.
D07-10	571.90	573.10	NQ	ES	BLPH	BK	LM	FR									MD			V	50%			T	<<1%					QzVns mostly along bedding graphitic along fractures, brittle fractures/
D07-10	573.10	578.64	NQ	ES	BLPH	BK	LM	FR									WK			<	<=1%			T	<=1%					
D07-10	578.64	581.00	NQ	ES	BLPH	BK	LM	FR									WK													Carbon rich on fracture surfaces.
D07-10	581.00	599.24	NQ	ES	BLPH	BKGY	LM	CT									WK			<	<<1%			T	<=1%					Minor contortions and crenulations, mumerous 3-10cm QzVns mostly parallel to bddg, graphite rich on fracture surfaces.
D07-10	599.24	599.92	NQ	ES	BLPH	BK	LM	CT									MD							T	1%					Some 2-5cm QzVns. Very hard rock-silicified thrt more phyllite than schist.
D07-10	599.92	601.09	NQ	ES	BLPH	bk		FR									md													Very carbon rich throughout fracture zone
D07-10	601.09	605.33	NQ	ES	BLPH	BK	LM	CT									MD							T	<<1%					
D07-10	605.33	610.37	NQ	ES	BLPH	BK	LM										ST							T	<=1%					Silicified, banded.
D07-10	610.37	610.98	NQ	ES	QTZ	WT											X													
D07-10	610.98	616.11	NQ	ES	BLPH	LM	LM										ST			V	1%			T	<=1%					Brittle qz filled fractures, QzVn 611.46-611.74
D07-10	616.11	617.28	NQ	DY	LMDK	GY	MG																							
D07-10	617.28	618.25	NQ	ES	BLPH	BK	LM	CT									ST			V	<=1%			T	<=1%					Brittle, Qz filled fractures.
D07-10	618.25	621.00	NQ	ES	BLPH	BKWT	LM										ST			V	5%			T	<=1%					Carbon rich thrt broken , qz and calcite filled fractures.
D07-10	621.00	624.72	NQ	ES	BLPH	BK	LM										ST							T	<<1%					
D07-10	624.72	626.67	NQ	ES	BLPH	WTGY	LM										ST													Mostly white calcite bands and fracture fills, some qz filling fractures.
D07-10	626.67	639.12	NQ	ES	BLPH	WTGY	LM						BD	20			ST			V	1%			T	<=1%					Pyrite in occasional 2-4cm bands, carbon rich on farcture surfaces.
D07-10	639.12	639.94	NQ	DY	LMDK	GYGN	FG										MD													Chlorite alteration thrt.
D07-10	639.94	641.42	NQ	ES	BLPH	WTBK	LM	FR									ST			G	3%			T	<<1%					Brittle fractures filled mostly with qz, also calcite filled.
D07-10	641.42	651.77	NQ	ES	BLPH	GYWT	BN										ST			V	2%			T	<=1%					Bands of very limey phyl and also silicious bands.
D07-10	651.77	652.94	NQ	ES	BLPH	GY		FL									MD							T	<=1%					Fault gouge, carbon rich with 30cm qz vn in center.
D07-10	652.94	653.78	NQ	ES	BLPH	GNGY		FR									MD													Chlorite altered, fracture zone.
D07-10	653.78	655.50	NQ	DY	LMDK	GNGY	FG										X													
D07-10	655.50	656.06	NQ	ES	BLPH	BK	LM										X							T	<<1%					
D07-10	656.06	660.47	NQ	RL	LMAR	GY	BN										ST													Argillite bands in lst.
D07-10	660.47	664.40	NQ	KP	PHYL	GYGN	LM										WK													Chlorite alt'd phyllite.
D07-10	664.40	670.63	NQ	EP	PHQZ	GYGN	LM						BD	20			X			P	10%			T	<=1%					Tweedy-like texture from 686.26-668.84. Carbon rich on some farctures.
D07-10	670.63	684.00	NQ	EP	PHQZ	GNGY	LM	FR									X			P	10%			T	1%					Fractured pieces approx 2cm thrt, chlorite altered at top, not towards bottom half.
D07-10	684.00	687.15	NQ	ES	PHQZ	GY	LM										X			P	10%									

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-10	687.15	688.08	NQ	ES	PHQZ	GY	LM										X			P	10%			M	20%			<	<=1%	Msv bands parallel to core.
D07-10	688.08	698.66	NQ	ES	PHQZ	GY	LM										X			P	10%			T	1%	<	tr	<	<=1%	Some banded sections sph in fractures etc thrt, gal in rare fractures, brittle fractured and healed, banded in areas.
D07-10	698.66	702.94	NQ	ES	PHQZ	DKGY	LM	FR									X			P	10%			T	<=1%	<	tr	<	<<1%	Slightly chlorite alt'd on fractures, 701.95-702.10: Fracture @ 77 degrees with Py, Pyr, Sph, dkfg mnl.
D07-10	702.94	712.15	NQ	EP	PHQZ	GY	LM						BD	20			X			P	10%			T	<<1%	<	tr	<	<<1%	Bk/Gy banding in areas.
D07-10	712.15	712.84	NQ	EP	PHQZ	GY	LM	FR									X			U	30%			<	1%	G	tr	G	<=1%	Qz filled brittle fractures with Py, Sphal, Gal in Qz.
D07-10	712.84	724.20	NQ	EP	PHQZ	GY	LM										X			P	10%			<	<=1%			<	<<1%	Some banding, areas quite fractured and slightly chlorite altered.
D07-10	724.20	724.61	NQ	EP	PHQZ	GY	LM	FR									X			P	10%			T	<=1%					Broken zone, chl altn on fracture surfaces.
D07-10	724.61	735.00	NQ	EP	PHQZ	GNGY	LM										X			P	10%									Slightly laminated-almost mottled in appearance, more chloritic, not as silicified.
D07-10	735.00	737.50	NQ	EP	GNPH	GNGY	LM										X							<	<<1%			<	<<1%	Pyr first appears at 735.00m, tension fractures with sphal.
D07-10	737.50	738.20	NQ	EP	GNPH	GY	LM	FR									X			V	60%			<	<<1%			<	<<1%	Clots of PY in fractures almost all qz vn here.
D07-10	738.20	760.72	NQ	EP	GNPH	GNGY	LM										X			V	2%			<	<=1%			<	<<1%	Sphal, py, amd pyr mnl only in qz filled fractures. Rk varies between 1-3m of Gy, then 1-3m GyGn, qz veins 1-6cm side with semi-msv pyr, pyr common thrt zone, enf of pyr zone @ 760.72m.
D07-10	760.72	786.00	NQ	EP	GNPH	GNGY	MB																	D	-					Rare sphal along tension fractures, chl altn thrt, varies between DkGy, fg py diss thrt.
D07-10	786.00	789.73	NQ	ES	PHQZ	GNGY	LM						BD	15			X			P	10%			T	<<1%			<	<<1%	Slightly schistose, brittle fractures.
D07-10	789.73	792.06	NQ	RL	LMST	DkGy	LM										ST							<	<<1%			<	tr	
D07-10	792.06	792.96	NQ	DY	LMDK	BkGn	MG																							
D07-10	792.96	797.33	NQ	RL	LMST	GyWt	BN										ST													Mostly white, mottled banding.
D07-10	797.33	800.21	NQ	DY	LMDK	GyGn	FG										X													
D07-10	800.21	808.93	NQ	RL	LMST	GyWt	BN										ST													DY 805.66-806.00. Mostly white, mottled banding.
D07-10	808.93	815.36	NQ	RL	LMST	BkWt	BN										ST													Sharply debined wt/bk banding, varies from 0-60 degrees, average 20 degrees.
D07-10	815.36	819.88	NQ	RL	LMST	GyWt	BN										ST													
D07-10	819.88	824.69	NQ	RL	LMAR	BkWt	BN										MD													Brittle fractured limey argillite, weak to strongly silicified in areas, more dolostone than 1st.
D07-10	824.69	830.88	NQ	RD	DOTE	GyWt	TW										WK													
D07-10	830.88	835.73	NQ	RL	LDAR	GyWt	BN										MD													Bands of lst/dol.
D07-10	835.73	837.70	NQ	DY	LMDK	DkGy	CG										X													
D07-10	837.70	842.62	NQ	RL	LMAR	BkWt	BN										ST													
D07-10	842.62	843.61	NQ	DY	LMDK	DkGy	MG										X													
D07-10	843.61	872.43	NQ	RL	LMAR	BkGy	BN						BD	30			ST											<	<=1%	DY from 863.20-863.70
D07-10	872.43	873.48	NQ	DY	LMDK	TnGy	FG										X													Chl alt'd, some bright green specs thrt?
D07-10	873.48	889.41	NQ	RL	LMAR	DkGy	BN						BD	25			ST							<	<=1%					dark gy/gy fire bands.
D07-10	889.41	901.22	NQ	RL	LMST	BkWt	BN						BD	25			ST													Sharp black/white banding, classic Reeves 1st.
D07-10	901.22	903.17	NQ	DY	LMDK	GyGn	MG										X													
D07-10	903.17	915.78	NQ	RL	LMST	BkWt	BN						BD	15			ST													Sharp bk/wt banding, classic reeves 1st. Dy from 915.03-915.23.
D07-10	915.78	916.68	NQ	DY	LMDK	Gy	FG										X													
D07-10	916.68	925.35	NQ	RL	LMST	GyWt	BN										ST													DY @ 918.40-919.28 and 922.22-922.91 and 925.07-925.29. 925.07-925.09 also fractured- Asenacous lst has a 'grainy sandy' appearance.
D07-10	925.35	933.34	NQ	RL	LMST	BkWt	BN	FR									ST													Fractured and re-healed, strong bands, chl DY and wt LMST from 928.50-929.29.
D07-10	933.34	936.55	NQ	ES	SCHI	Bk	LM	FR									WK													Graphite rich, esp on fractures.
D07-10	936.55	937.04	NQ	DY	LMDK	GyGn	FG										X													
D07-10	937.04	946.60	NQ	DY	SCHI	Bk		CN									WK													Graphitic, carbon rich thrt.
D07-10	946.60	955.54	NQ	ES	SCHI	DkGy		CN									WK													Most of section strongly silicified.
D07-10	955.54	960.73	NQ	DY	LMDK	Gn	CG										X													Chl altered, green phyllite caught up + contorted in areas of dyke. EOH.
D07-11	0.00	13.00	HW	OV	OVBN																									
D07-11	13.00	95.79	HQ	AC	AR	LTGY	LM	LC		QV							MD							T	<=1%					Weakly graphitic in places. QV 20-25m crumbly sections, also @ 42.1->55.60 blockly core angle varies from 5-25 degrees. Another QV 62.2-62.45m. 80.00-80.25 crumbly section.
D07-11	95.79	97.67	HQ	DY	MFDY			CN	55																					
D07-11	97.67	117.64	HQ	AC	AR	LTGY	LM	LC		BD							WK							T	1%					Some contorted laminae, massive (10cm) graphitic. Some qtz veins. Small dyke 106.31-106.92
D07-11	117.64	120.00	HQ	DY	MFDY					BD																				

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								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-11	120.00	124.63	HQ	AC	AR												WK													Broken graphitic. Contorted laminae.
D07-11	124.63	125.70	HQ	DY	MFDY	LTGY											WK													
D07-11	125.70	128.70	HQ	AC	AR	MDGY	LM										WK													Very broken.
D07-11	128.70	149.15	HQ	TL	SCPH												MD													Some bonding, m folds. Graded bedding with tops to bottom.
D07-11	149.15	154.25	HQ	TL	SCHI		BD										MD							S	<<1%					Becomes massive. Some minor lamination.
D07-11	154.25	155.12	HQ	DY	MFDY																									
D07-11	155.12	157.39	HQ	TS	SCHI	GY	BD										ST													Lower contact contains calvcite veining.
D07-11	157.39	158.52	HQ	DY	MFDY	DKGY	MS										X													
D07-11	158.52	175.29	HQ	TL	SCHI	GY	LM	CN									ST							S	<<1%					Crenulated, contorted. Foliation weakly developed, pyrrhotic.
D07-11	175.29	176.29	HQ	TL	SCHI	LTGY	MB										ST													Pyrrhotite
D07-11	176.29	177.21	HQ	TL	QTZ	BL	MS										ST													Almost pure qtz. Blue, tr py, phrrotite contacts graduation.
D07-11	177.21	178.36	HQ	TL	SCHI	LTGY	MB										ST													Pyrrhotite
D07-11	178.36	191.15	HQ	TL	SCHI	LTGY	MB										ST													Some laminated sections. Abrupt lower contact.
D07-11	191.15	191.49	HQ	TL	QTZ	BL	MS																							Contacts abrupt. Upper planar, lower irregular with altertion. Grain size graduation.
D07-11	191.49	196.01	HQ	TL	SCHI	BL-GY											ST													Both massive laminated sections.
D07-11	196.01	201.03	HQ	AC	AR	BK	BD	LC	25								WK							L	<=1%					Laminations calcarious.
D07-11	201.03	220.04	HQ	TL	SCPH	BL-GY	MB	LC									ST							S	<=1%					Laminations contorted in places. Pyrrhotiteal 1%.
D07-11	220.04	220.60	HQ	TL	SCPH	BL-GY	LM										ST													Interbedded schist-phyllite. Crenulated laminae. Lower contact abrupt.
D07-11	220.60	222.01	HQ	ES	BLPH	DKGY	LM										ST													
D07-11	222.01	224.26	HQ	ES	BLPH	DKGY	LM	CN		BR		TB					ST													Graphitic. Qtz flooding at upper and lower contacts. Contorted, fracture filled.
D07-11	224.26	227.58	HQ	ES	BLPH	DKGY	LM	LC									WK													Much more laminated. Crenulated. Angle to core varies from 30-5 degrees down section.
D07-11	227.58	229.31	HQ	TL	SCHI	BL-GY	BD	FR				TB					ST													Interlaminated schist/phyllite. Contorted bedding at lower contact.
D07-11	229.31	229.61	HQ	ES	QTZ	WH	MO	BR		FR							MD													Qtz flooded. Fractures qtz/calcite filled, open fractures. Sharp contacts.
D07-11	229.61	230.50	HQ	TL	SCHI	BL	LM																	E	<=1%					WK laminations. Lower contact. Clay seam.
D07-11	230.50	235.59	HQ	ES	BLPH	BK	LM	LC									WK							S	<=1%					Folded, contorted.
D07-11	235.59	246.62	HQ	ES	BLPH	BK	PA	BR									WK							E	<=1%					Graphitic, crumbly.
D07-11	246.62	261.66	HQ	ES	BLPH	BK	LM										X			U	5%									Qtz veins, crumbly sections @ 250.50, 256.50 graphitic. Lower contact faulted.
D07-11	261.66	264.20	HQ	DY	MFDY	GY	MS										WK													Upper contact abrupt/planar. Non-magnetic.
D07-11	264.20	265.35	HQ	FL	BLPH	bk											x													Totally broken, crumbly, graphitic
D07-11	265.35	268.73	HQ	ES	BLPH	BK	FL										X													
D07-11	268.73	269.36	HQ	DY	MFDY												X													Mag. Contacts 50 degrees.
D07-11	269.36	271.11	HQ	ES	BLPH																									
D07-11	271.11	272.96	HQ	RL	LMAR	WO	LM	BR		CN		TB					ST	X	X					B	<<1%					Oxidized laminae contorted to brecciates
D07-11	272.96	275.14	HQ	RL	LMAR	WO	LM	LC									ST	X	X					L	<<1%					Lam contorted, folded.
D07-11	275.14	275.72	HQ	DY	MFDY	GY		DC	35																					Contacst sharp. Irregular upper, planar lower, 35 degrees.
D07-11	275.72	294.54	HQ	RL	LMAR	WO	LM	LC									ST	X	X					L	<<1%					Some contorted, folded. Core angle varies from 15-50 degrees.
D07-11	294.54	294.91	HQ	RL	LMAR	RD-WO	LM										ST	X	X											Oxidized section. Purite replaced by siderite. Voids.
D07-11	294.91	298.63	HQ	RL	LMAR	WO	LM	LC									ST													Second oxidized section. 2cm @ 299.05
D07-11	298.63	299.07	HQ	DY	MFDY	DKGY	MS																							Sharp, planar contacts.
D07-11	299.07	302.07	HQ	RL	LMAR	LTGY	LM	LC		FR							ST													More laminated, darker colour due to higher mild content in laminations.
D07-11	302.07	302.26	HQ	DY	MFDY	DKGY	MS																							
D07-11	302.26	305.19	HQ	RL	LMAR	LTGY	LM																							Thin 10cm dyke @303m.
D07-11	305.19	305.32	HQ	DY	MFDY	LTGY	MS																							
D07-11	305.32	305.92	HQ	RL	LMAR	LTGY		FR		LC																				Micro faults-> disturbed bedding. Larger grain size, aoss. Recrystalization micrmg-> sparrite.
D07-11	305.92	312.19	HQ	RL	LMST	BLWO	BD	FR																						Larger beds, grain size increases. Slight blue tinge, transitional to LMAR.
D07-11	312.19	328.74	HQ	RL	LMAR	WOGY	LM	LC	10								ST													
D07-11	328.74	333.34	HQ	RL	LMST	WI	BD	LC	15								ST	X												
D07-11	333.34	333.61	HQ	RL	LMAR	LTGY	LM	CN									ST	MD	X											Thin contact.
D07-11	333.61	334.00	HQ	RD	LDAR	LTGY	MO	BR		FR		TB					WK	MD	X											Fractured, brecciated, small faults.
D07-11	334.00	335.00	HQ	RD	LDAR	MDGY	MO	BR		FR		TB					WK	WK												Scm oxidized seam open caly with zinc rxn.
D07-11	335.00	336.00	HQ	RD	LDAR	LTGY	LM	BR		FR		TB					MD	MD												
D07-11	336.00	337.00	HQ	RD	LDAR	DKGY	MO			FR		TB					WK	ST												10cm oxidized seam.
D07-11	337.00	338.00	HQ	RD	LDAR	MDGY	MO					TB					WK	X						S	<<1%					Broken towards bottom, lighter colour.

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-11	338.00	338.89	HQ	RD	LDAR	GY	MO	CN	35			TB					MD	X						S	<<1%					Very broken, 30cm Qz. A lower contact. Clay seam lower contact -> dipping limestone.
D07-11	338.89	342.00	HQ	RL	LMST	WO	CG						BD				ST	X												
D07-11	342.00	344.36	NQ	RL	LMST	WO	CG						BD																	
D07-11	344.36	345.63	HQ	RL	LMAR	gy	LM	LC	25								wk	wk	x											Lower contact brecciated
D07-11	345.63	347.84	NQ	RL	SCHI	GNGY	MS										WK	X						S	<<1%					Chloritic, greasy massive. Upper and lower cintact. Qtzite veins.
D07-11	347.84	350.25	NQ	RL	LMST	BL											ST	X	X					S	tr					Some oxidized secton ewith FR stain.
D07-11	350.25	352.58	NQ	KP	PHYL	RDBN	LM										X	X												Laminations at 20 degrees.
D07-11	352.58	353.32	NQ	RL	LMST	BL											ST													
D07-11	353.32	353.84	NQ	KP	PHYL	RDBN	LM	LC	15								X													Lower contact 3cm-chloritic schist.
D07-11	353.84	359.57	NQ	RL	LMST	BKGY	MS						BD																	Fairly massive.
D07-11	359.57	360.89	HQ	KP	PHYL																									Interbedded limestone sections 6-10 cm thick
D07-11	360.89	361.47	NQ	RL	LMAR	GY	LM						BD	5			ST													
D07-11	361.47	361.92	NQ	KP	PHYL	DKGY	LM						BD	5			X													Limonitic along fractures.
D07-11	361.92	363.11	NQ	RL	LMST	WTGY	LM										ST													Some slightly limey bands.
D07-11	363.11	363.30	NQ	KP	PHYL	DKGY	LM										WK													
D07-11	363.30	363.48	NQ	RL	LMST	GY	LM										ST													
D07-11	363.48	363.59	NQ	KP	PHYL	DKGY	LM										X													
D07-11	363.59	364.88	NQ	RL	LMST	WTGY	LM										ST													
D07-11	364.88	366.03	NQ	KP	PHYL	GY	LM										WK													Limonite along fractures and also in limm bands along bddg. Some qz filled tension fractures.
D07-11	366.03	366.28	NQ	RL	LMST	LTGY	LM										ST													
D07-11	366.28	366.42	NQ	KP	PHYL	RD	FL	FL									X													Intensely hematitic stained fault gouge.
D07-11	366.42	366.86	NQ	RL	LMAR	DKGY	LM	FR									MD			G	5%									Qz filled fractures lim stains thrt and bands of lim.
D07-11	366.86	380.19	NQ	RL	LMAR	WTGY	LM						BD	10			ST													Some areas very slightly tweedy.
D07-11	380.19	382.29	NQ	DY	LMDK	GNBN	FG	FL		CN							X													Rusty, limonite stained thrt, chloritic in areas, fractured steeply to CA, center is complete clay.
D07-11	382.29	396.30	NQ	RL	LMAR	GYWH	LM										ST													Fine wt/bk bands thrt.
D07-11	396.30	396.96	NQ	DY	LMDK	GY	FG										MD													
D07-11	396.96	398.20	NQ	RL	LMAR	WTGY	LM						BD	10			ST													
D07-11	398.20	398.77	NQ	DY	LMDK	GY	MG										ST													Uniform colour and grain size thrt.
D07-11	398.77	406.53	NQ	RL	LMAR	WTGY	TW										ST													Some areas tweedy-like.
D07-11	406.53	418.12	NQ	RL	LMAR	WTGY	TW										ST													Mostly slightly tweedy, some limestains in fractures and in zones.
D07-11	418.12	418.67	NQ	RL	LMAR	GY	LM										MD													Arkose rich section of lst.
D07-11	418.67	419.20	NQ	RL	LMAR	WTGY	LM										ST													
D07-11	419.20	419.71	NQ	RL	LMAR	NBGY	LM										ST													Limonite stained thrt and along bands, some vugs of sulphides rusted away.
D07-11	419.71	424.00	NQ	RD	DOTE	BRGY	LM	FR									WK													Brittle farctures thrt mod lim thrt, some voids due to lim alt'd suyhides.
D07-11	424.00	428.71	NQ	RD	DOTE	GY	TW	FR									WK													Some tweedy textures thrt, qz filled fractures, fault gouge @ 426.07, slightly lim stained thrt.
D07-11	428.71	431.43	NQ	RD	DOTE	TNGY	TW	FR									WK			V	<=1%									Brittle fractures, 5mm qz vns x-cutting bdd @ 90 degrees to CA, int lim staining in areas, vuggy zones, tweedy.
D07-11	431.43	432.00	NQ	RD	DOTE	RDBN	LM	FR									WK													Intense hem and lim stained fracture zone.
D07-11	432.00	442.15	NQ	RD	DOTE	GY	TW										WK							T	<=1%					Classic tweedy structure, some limestone on fracture, brittle fractures @ top.
D07-11	442.15	442.76	NQ	RD	DOTE	GY	LM										WK							X	7%					Not tweedy here, arkose-rich dolomite.
D07-11	442.76	445.36	NQ	RD	DOTE	GY	TW										WK							T	<=1%					Tweedy
D07-11	445.36	445.90	NQ	RD	DOTE		TW										WK							X	5%					Partially tweedy.
D07-11	445.90	455.00	NQ	RD	DOTE	GY	TW										WK							T	<=1%					Tweedy.
D07-11	455.00	461.00	NQ	RD	DOTE	GY	TW										WK							T	1%					Some tweedy areas, mostly not tweedy, 1cm py in 1cm qz vein.
D07-11	461.00	464.00	NQ	RD	DOTE	DKGY	LM										WK							T	<=1%					
D07-11	464.00	465.07	NQ	RD	DOTE	GY	LM										WK							T	<<1%			T	<<1%	
D07-11	465.07	466.43	NQ	RD	DOTE	GY	LM										WK			G	5%			T	<<1%			T	<=1%	Sph mainly in qz, Qz infills in tension gapsx-cutting bddg, small vugs assoc. with qz.
D07-11	466.43	470.50	NQ	RD	DOTE	GYWT	TW	FR									WK			G	1%			T	<=1%			T	<=1%	Healed vrittle fractures some lim on fract surfaces, fg sph in bands along bddg and diss thrt.
D07-11	470.50	472.10	NQ	RD	DOTE	GY	LM										WK			G	1%			T	3%			T	1%	Bands of fg py along bddg.
D07-11	472.10	474.10	NQ	RD	DOTE	LTGY	TW										WK			G	<=1%			T	<<1%			T	<<1%	

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-11	474.10	479.00	NQ	RD	DOTE	TNGY	MO	FR									WK			G	<=1%							T	7%	Limonitic/bleached thrt, porphyry-like textures, sph in qz vn and thrt, brittle fractures.
D07-11	479.00	482.00	NQ	RD	DOTE	TNGY	MO	FR									WK							T	<<1%			T	3%	Similar to section above, but less intense, possible vufg galena?
D07-11	482.00	492.06	NQ	RD	DOTE	DKGY	TW										WK							T	<=1%			T	<<1%	
D07-11	492.06	499.20	NQ	RD	DOTE	LTGY	TW										WK							T	<<1%			T	<<1%	
D07-11	499.20	504.50	NQ	RD	DOTE	GY	TW										WK							T	2%			T	<=1%	Bands of almost msv py in darker areas of dolomite, possible vfg galena?
D07-11	504.50	505.00	NQ	RD	DOTE	GY	TW										WK							T	40%			T	5%	20cm band of msv py with sphal.
D07-11	505.00	509.47	NQ	RD	DOTE	GY	TW										WK							T	<=1%			T	<<1%	Msv py + sph @ 507.36 and 3 other 2cm bands.
D07-11	509.47	510.08	NQ	DY	LMDK	DKGY	MG																							
D07-11	510.08	516.67	NQ	RD	DOTE	LTGY	LM										WK							<	tr					tweedy in areas-only slightly tweedy.
D07-11	516.67	518.00	NQ	RD	DOTE	DKGY	LM										WK							X	3%			T	1%	
D07-11	518.00	524.10	NQ	RD	DOTE	GY	TW										WK							<	<=1%			T	tr	A sort of mottled tweed.
D07-11	524.10	527.87	NQ	KP	PHYL	GYBN	LM										X							T	2%					Schistise-slightly chloritized, a klein schist(?).
D07-11	527.87	528.55	NQ	RD	DOTE	GY	LM										WK							T	<<1%			T	<=1%	
D07-11	528.55	529.36	NQ	DY	LMDK	DKGY	MG																							
D07-11	529.36	530.00	NQ	RD	DOTE	TNGY	BN																					T	5%	Calcite bands and sph bands.
D07-11	530.00	530.71	NQ	RD	DOTE	GY	TW																							
D07-11	530.71	531.64	NQ	RD	DOTE	TNGY	BN																					T	7%	Similar to 529.36-530.00 section above.
D07-11	531.64	548.89	NQ	RD	DOTE	DKGY	TW																	T	tr			T	tr	Fracture zone (brittle) around 542m and 546m also.
D07-11	548.89	550.65	NQ	RD	DOTE	LTGY	LM																	T	tr					Grades into phyllite over last 50cm. Possible bfg sph thrt?
D07-11	550.65	555.84	NQ	KP	PHYL	DKGY	LM																	T	<=1%			T	tr	Some sph in areas.
D07-11	555.84	556.43	NQ	DY	LMDK	GNGY	MG										MD													Slightly chloritic.
D07-11	556.43	560.11	NQ	KP	PHYL																									Intercalated limestone / KP
D07-11	560.11	560.30	NQ	DY	LMDK	GN	CG										WK													Chloritic.
D07-11	560.30	564.49	NQ	RL	LMST	GYWT	BN										ST													Slightly banded to 561.70, well banded below thrt.
D07-11	564.49	567.02	NQ	RL	LMAR	GNWT	LM										ST													Banded chlorite altered shistose argillaceous limestone- GnBn bands. 8cm and 15cm bands of TS @ 566.78m + 566.17m.
D07-11	567.02	569.11	NQ	TS	LHAR	GN	LM						BD	27			MD													Perrasive vhl altn thrt.
D07-11	569.11	570.16	NQ	DY	LMDK	GNGY	MG										WK													
D07-11	570.16	570.43	NQ	TS	LHAR	GN	LM										MD													Perrasive chl altn thrt.
D07-11	570.43	573.07	NQ	RL	LMST	GYWT	BN										ST													
D07-11	573.07	575.50	NQ	TS	LHAR	GNGY	LM										WK													Weak to moderate/chlorite alteration thougthout. End of limey zones.
D07-11	575.50	578.61	NQ	TS	LHAR	GYGN	LM										X			U	10%									Slightly chloritic-qz and calcite banding and veins from 2m-6cm. Thrt.
D07-11	578.61	583.14	NQ	TS	LHAR	GNBK	LM										X			P	1%								tr	Possible KP? Not very schistose, very hard.
D07-11	583.14	596.61	NQ	TS	LHAR	GYBK	LM						BD	25			X													Tan/bleached along fractures and thrt in areas, mottled in areas. Possible KP? Mostly not silicified.
D07-11	596.61	597.66	NQ	TS	LHAR	GYGN														P	1%									Slightly chlorite altered.
D07-11	597.66	603.71	NQ	DY	LMDK	GYGN	CG																							
D07-11	603.71	605.05	NQ	KP	LMAR	BRGY	LM													P										Top half intensely silicified, bottom half not slightly schistose.
D07-11	605.05	606.36	NQ	DY	LMDK		FG																							Cg core within a f=FG dyke- a CG dyke within a FG dyke.
D07-11	606.36	608.50	NQ	KP	LHAR	GY	LM																							Strongly silicified sections, others not. KP and RQ and TS all mixed?
D07-11	608.50	609.50	NQ	KP	LHAR	GY	LM													P	10%									Broken/fractured zone, intense silicification throughout. Unit member same as above.
D07-12	0.00	3.50	HQ	OV	OVBN								BD	25			ST							<	2%					
D07-12	3.50	7.80	HQ	AC	AR	Bk	LM	FR																						Broken zone.
D07-12	7.80	18.86	HQ	AC	AR	BK	LM										ST							<	2%					Carbon rich on fractures.
D07-12	18.86	22.20	HQ	AC	AR	BK	LM										ST							<	2%					Broken zone, extremely carbon rich thrt, graphite in some areas.
D07-12	22.20	25.57	HQ	AC	AR	BK	GG	FL									MD													
D07-12	25.57	26.24	HQ	AC	QTZ	Wt	MS										X													
D07-12	26.24	51.30	HQ	AC	AR	Bk	LM										WK							<	2%					Graphitic on fractures @ 43.75, some crenulations in areas.
D07-12	51.30	52.83	HQ	DY	LMDK	GY	FG	CN	60								WK													
D07-12	52.83	57.11	HQ	AC	AR	BK	LM						BD	70			WK							<	2%					
D07-12	57.11	59.82	HQ	AC	AR	BK	GG	FL									WK			<	30%									Portion of fault with qz filled fractures.
D07-12	59.82	68.50	HQ	AC	AR	BK							BD	10			WK							<	2%					
D07-12	68.50	69.33	HQ	AC	AR	BK	FL										WK													
D07-12	69.33	83.66	HQ	AC	AR	BK	LM						BD	10			WK							<	2%					
D07-12	83.66	83.75	HQ	DY	LMDK	GY	FG										WK													

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-12	83.75	85.40	HQ	AC	AR	BK	GG	FR									WK			<	1%			T	<=1%					
D07-12	85.40	103.26	HQ	AC	AR	BK	LM						BD	10			WK			<	<=1%			T	<=1%					
D07-12	103.26	107.00	HQ	AC	AR	BK	LM	FR									WK													Broken zone.
D07-12	107.00	107.50	HQ	DY	LMDK	GnGy	MG										X													Slight chl. Alt'n.
D07-12	107.50	115.83	HQ	DY	AR	BK	LM										WK			P										A few qz vns up to 3cm thick, vns and area around fractured, rk strongly silicified, carbon rich.
D07-12	115.83	119.90	HQ	DY	AR	BkWt	LM	FR									WK			<	3%			T	2%					Strongly silicified, brittle re-healed fractures, graphite on fracture surfaces.
D07-12	119.90	126.42	HQ	DY	AR	BK	LM										ST			P				T	1%					Strongly silicified, py in with qz in 1-5mm vns.
D07-12	126.42	137.07	HQ	DY	LMDK	GyGn	CG																							Mod-str chl. Altn.
D07-12	137.07	139.02	HQ	DY	AR	WtBk	LM	FR									ST			<	3%									Highly fractured, pervasively silicified and as fracture fills.
D07-12	139.02	144.00	HQ	DY	AR	BK	LM										WK			<	1%			T	<=1%			<	tr	Bottom couple m's strongly silicified 0.5-4cm qz vns thrt.
D07-12	144.00	144.65	HQ	DY	AR	BK	LM										ST			P										Strongly silicified.
D07-12	144.65	148.67	HQ	DY	AR	BK	LM	FR		GG							ST			<	1%									Fault gouge and higly fractured zone, carbon rich on fractures.
D07-12	148.67	151.88	HQ	DY	AR	BK	LM										ST							<	<=1%					Strongly silicified.
D07-12	151.88	164.30	HQ	ES	SCHI	BK	LM										X							<	<<1%			<	tr	Strongly sil, rare sph? In qz fractures, areas very siliceous, others not at all.
D07-12	164.30	169.80	HQ	ES	SCPH	BK	LM	BR									ST							<	<=1%					Bands of schist and argillite.
D07-12	169.80	174.23	HQ	ES	SCPH	DkGy	LM										ST			P				<	2%					Bands of argillite & schist.
D07-12	174.23	199.00	HQ	ES	SCHI	DkGy	LM	CR		BD							MD			<	<=1%									Some wk cal, some str cal thrt, mainly strongly sil, 179.50-182.50 not CR, brittle rehealed fractures.
D07-12	199.00	201.32	HQ	DY	LMDK	GyGn	FG										X													Chlorite altn thrt, strongly silicified.
D07-12	201.32	206.74	HQ	ES	SCHI	GY	LM	CR									ST													
D07-12	206.74	207.88	HQ	DY	LMDK	GnGy	FG										X													Slightly chloritic, strongly silicified.
D07-12	207.88	216.91	HQ	ES	GCHP	BK	LM	CR									X													Carbon rich on fractures.
D07-12	216.91	217.74	HQ	DY	LMDK	GyGn	MG										X													Slightly chloritic.
D07-12	217.74	218.23	HQ	ES	GCHP	BK	LM	CR									X													
D07-12	218.23	219.25	HQ	DY	LMDK	GnGy	MG										X													Very siliceous.
D07-12	219.25	222.41	HQ	ES	GCHP	BK	LM	CR									X													Carbon rich on fractures.
D07-12	222.41	227.38	HQ	ES	LMST	GY	BN										ST													
D07-12	227.38	240.99	HQ	ES	SCLM	GY		CN									ST													Very limey schist/limestone->shisty limestone?
D07-12	240.99	243.34	HQ	ES	LMST	GY	BN										MD													Fault gouge @ 242.00
D07-12	243.34	243.74	HQ	ES	GNPH	GnGy	LM	CR									WK							T	1%			<	tr	Limey phyllite, chloritic.
D07-12	243.74	244.68	HQ	ES	GCHP	Gy	LM	CR									WK							T	1%			<	tr	Chlorite alt'd.
D07-12	244.68	249.31	HQ	ES	GCHP	GY	LM						BD	45			X							<	2%					
D07-12	249.31	250.12	HQ	ES	GCHP	BK	GG										X													Carbon rich.
D07-12	250.12	265.06	HQ	ES	SCHI	BK	LM						BD	55			X							T	1%					Strongly grapihte rich in areas, DY from 260.45-260.86 (CG, chl altd).
D07-12	265.06	265.65	HQ	ES	LMDK	GnGy	FG																							
D07-12	265.65	281.00	HQ	ES	SCHI	DkGy		CN		BD							MD							<	1%					
D07-12	281.00	287.00	HQ	ES	GCHP	BK		CN		FR							WK			P				<	1%					Broken and carbon/graphite rich thrt, silicified and very hard.
D07-12	287.00	313.18	HQ	ES	GCHP	BK		CN		BD							X			<	5%			<	5%					Silicified, carbon/graphite rich thrt, chl altn on fractures, from 299.00-308.00, 10% vfg qz thrt.
D07-12	313.18	316.69	HQ	DY	LMDK	BkGy	MG										X													Chl alt'd, bleached at bottom.
D07-12	316.69	318.20	HQ	ES	GCHP	BK	LM	FR									X			<	\									Zones of fg qz along laminae up to 10%.
D07-12	318.20	326.30	HQ	ES	SCHI	BK	LM	CN									X			<	\									
D07-12	326.30	329.30	HQ	ES	SCHI	BK	LM	CN		GG							X													Zones of gouge in with fractured zone.
D07-12	329.30	331.06	HQ	ES	SCHI	BK	LM	CN									X			<	5%			<	5%					
D07-12	331.06	332.16	HQ	ES	SCHI	BK	GG										X													
D07-12	332.16	333.27	HQ	ES	SCHI	BK	LM										X			<	2%			<	2%					
D07-12	333.27	333.91	HQ	DY	LMDK	GnGy	FG																							
D07-12	333.91	334.48	HQ	ES	SCHI	BkGy											X			P										Strongly silicified transition zone between schist and limestone.
D07-12	334.48	336.79	HQ	RL	LMST	BkWt	BN						BD	37			ST							<	1%					Classic banded Reeves lst.
D07-12	336.79	337.61	HQ	DY	LMDK	GnGy	FG										X													Slightly chloritic.
D07-12	337.61	341.38	HQ	RL	LMST	BkWt	BN						BD	40			ST							<	1%					
D07-12	341.38	341.76	HQ	DY	LMDK	GnGy	CG										X													Chloritized.
D07-12	341.76	356.00	HQ	RL	LMST	BkWt	BN						BD	35			ST							<	2%					Mineralized bands of Fg pyrite 1-5cm thick thrt.
D07-12	356.00	375.69	HQ	RL	LMST	GyWt	BN						BD	40			ST							<	<<1%					Chl DY from 372.77-373.04, 373.56-373.83, and 375.42-375.69, lst uniform thrt.
D07-12	375.69	396.30	HQ	RL	LMST	BkGy	BN						BD	40			ST							<	<<1%					Lmst with darker bands, otherwise uniform thrt, entire lst unit very competant-core hardly broken.
D07-12	396.30	398.49	NQ	RL	LMST	BkGy	BN						BD	35			ST													
D07-12	398.49	401.07	NQ	DY	LMDK	GnGy	MG										X													Slightly chlorite.

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-12	401.07	408.26	NQ	RL	LDAR	GyWt	BN										ST													Mixed LST/Dolomite- bands of each, DY from 405.09-405.79. Mostly lst 405.79-408.26, wht mainly.
D07-12	408.26	413.00	NQ	RD	DOTE	DkGy	TW										WK							<	<<1%					Unknown vfg bk metalic mnl? Vp to 10% in areas -> Pb or Ag mnl.
D07-12	413.00	414.73	NQ	RD	DOTE	Gy	TW										wk							<	<<1%					
D07-12	414.73	422.00	NQ	RD	DOTE	DKGY	TW										WK							<	2%	<	<<1%	<	<<1%	420.00 - 421.00 very dark, 3% py thrt
D07-12	422.00	430.46	NQ	RD	DOTE	GY	TW										WK							<	?	>	tr	<	<=1%	Tweedy only in areas, not strong, almost mottled
D07-12	430.46	438.95	NQ	RD	DOTE	LTGY	BN										ST			U	1%			<	1%	<	tr	<	<=1%	Mixed zone of Limestone/dolostone
D07-12	438.95	451.00	NQ	RL	LMAR	dkgy	LM						BD	40			ST							<	<=1%			<	tr	Phyllitic limestone transition from 450-451 with tweedy DOTE and sphal in areas
D07-12	451.00	459.88	NQ	RD	DOTE	gy	TW										WK							<	<=1%	<	tr	<	<=1%	Dyke from 459.79-459.88, some very dark areas with vfg mineralization, some large blebs of sphal
D07-12	459.88	461.94	NQ	RD	DOTE	gy	TW										WK							<	1%	<	2%	<	10%	Strongly mineralized zone, mostly sphal, could be others in vfg bk mineral?
D07-12	461.94	470.00	NQ	RD	DOTE	gy	TW										WK							<	<=1%	<	tr	<	<<1%	
D07-12	470.00	471.19	NQ	RD	DOTE	gy	LM										WK							M	30%	<	tr	<	<=1%	Slighty tweedy in areas, bands of massive py
D07-12	471.19	484.51	NQ	RD	DOTE	gy	TW										WK							<	5%	<	tr	<	<=1%	Slightly tweedy, also banded/laminated in areas, 20-40 cm wide zones of semi-massive py + other mineralization, phyllitic bands
D07-12	484.51	490.04	NQ	RL	LMST	gywt	BN						BD	50			ST							<	<=1%			<	tr	Mineralized band between 486.62-487.12 with 8 cm band of semi massive py
D07-12	490.04	490.36	NQ	KS	PHSC	gngy	LM						BD	40			X													Chloritic schist
D07-12	490.36	490.81	NQ	RL	LMST	blgy	LM										ST													
D07-12	490.81	492.93	NQ	KS	PHSC	BR	LM						BD	43			X													Limey bands 20 cm wide in unit
D07-12	492.93	496.03	NQ	RL	LMST	wt	BN										ST													Last 50 cm banded, rest with lst only
D07-12	496.03	496.82	NQ	KS	PHSC	BR	LM										X													Some limey bands
D07-12	496.82	500.58	NQ	RL	LMST	blgy	BN						BD	45			ST													Siliceous bands, also phyllite bands, not entirely sure if Reeves - very phyllic rich limestone
D07-12	500.58	503.00	NQ	KS	PHSC	BRGY	LM										X													BlGy limestone from 501.52-501.95
D07-12	503.00	507.72	NQ	RL	LMST	blbn	LM										ST													Silicified bands and phyllic bands
D07-12	507.72	508.82	NQ	KS	PHSC	BRGY	LM										X													Limey band near bottom
D07-12	508.82	510.31	NQ	RL	LMST	blgy	LM						BD	60			ST													Blue-ish in colour
D07-12	510.31	511.31	NQ	KS	PHSC	bkbn	LM										X													Slightly chloritic, slightly blue-ish colour
D07-12	511.31	513.76	NQ	RL	LMST	wtgy	LM										ST													
D07-12	513.76	516.66	NQ	RL	LMST	gy	MO										ST													Transition zone between limestone / dolostone
D07-12	516.66	518.00	NQ	RD	DOTE	bkgy	TW	FR									WK							T	1%	T	tr	T	tr	Fractures filled with calcite, also vfg bk mineral?
D07-12	518.00	522.00	NQ	RD	DOTE	gy	TW	FR									WK							T	<=1%					Fractures are filled with calcite
D07-12	522.00	524.00	NQ	RD	DOTE	dkgy	TW										WK							T	5%	T	tr	T	tr	Highest mineralization from 522.00 - 523.69
D07-12	524.00	530.61	NQ	RL	LMST	gywt	BN						BD	30			ST													
D07-12	530.61	536.25	NQ	RD	DOTE	gy	TW										WK							T	<=1%					Py rich band @ 533.52 metres
D07-12	536.25	540.98	NQ	RD	DOTE	gy	TW										WK							T	10%	T	tr	T	tr	
D07-12	540.98	543.74	NQ	RD	DOTE	gy	TW										WK							T	<=1%			T	tr	
D07-12	543.74	544.50	NQ	RD	DOTE	gy	TW										WK							M	30%					
D07-12	544.50	554.38	NQ	RD	DOTE	ltgy	TW										WK							T	<<1%					
D07-12	554.38	554.88	NQ	RD	DOTE	gy	TW										WK							T	10%	T	tr	T	tr	Massive py zones from 550.00-550.71, 551.61-552.10, 554.13-554.82
D07-12	554.88	563.00	NQ	RD	DOTE	gy	TW										WK							T						
D07-12	563.00	564.36	NQ	RD	DOTE	dkgy	TW										WK							T	10%					Zones of msv py along length
D07-12	564.36	572.91	NQ	RD	DOTE	gy	TW										WK							T	<=1%					
D07-12	572.91	574.31	NQ	RL	LMST	dkgy	BN										ST							T	1%					
D07-12	574.31	574.85	NQ	RD	DOTE	gy	TW										MD							T	<=1%			T	tr	Slightly tweedy, limey bands towards bottom, grades into limestone
D07-12	574.85	575.29	NQ	RL	LMST	dkgy	BN										ST							T	1%					
D07-12	575.29	576.06	NQ	RD	DOTE	gy	TW										WK							T	2%			T	<=1%	
D07-12	576.06	582.55	NQ	RD	DOTE	dkgy	BN										WK			P				T	1%	T	tr	T	<=1%	Strongly silicified throughout, mottled bk/dkgy bands, vvfg dark mineral? Throughout
D07-12	582.55	598.10	NQ	RD	DOTE	dkgy	BN										WK			P				T	<=1%	T	tr	T	tr	Varies thrt: Banded, mottled, limey, silicified, brittle fracture zones with calcite infill
D07-12	598.10	601.26	NQ	RD	DOTE	ltgy	TW	FR									WK											T	tr	Fault zone, fractured, no gouge
D07-12	601.26	602.27	NQ	RD	DOTE	ltgy	BN										WK													
D07-12	602.27	602.78	NQ	RD	DOTE	ltgy	BN	FR									WK													
D07-12	602.78	603.27	NQ	RD	DOTE	ltgy	BN										WK													Mottled banding
D07-12	603.27	609.27	NQ	RD	DOTE	ltgy	TW										WK							T	2%	T	<=1%	T	2%	Mineralized from 604.35-605.69 and 608.70-609.22

*Key to codes and symbols used located at end of logs

								STRUCTURE					EVENT				TESTS			Quartz		Calcite		Pyrite		Galena		Sphalerite		
DDH	FROM	TO	CORE SIZE	MEMBER	ROCK	COLOUR	TEXTURE	Main	Angle	Second	Angle	BRECCIA TYPE	Type	Angle	Alteration	Amount	HCl	Zn Zap	Pb Zap	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Type	Amt	Description
D07-12	609.27	615.60	NQ	RD	DOTE	ltgy	MS										WK							T	<<1%					
D07-12	615.60	616.44	NQ	RD	DOTE	ltgy	MS										WK							T	<=1%	T	tr	T	<<1%	Mineralized section

*Key to codes and symbols used located at end of logs

MEMBER

CODE	MEMBER	FORMATION	AGE	LITHOLOGY
AC	Active	Active	Ordovician	Black shales
DY	Dyke	Igneous rock	Cretaceous?	Igneous rock
EB	Emerald black schist			
EP	Uncertain			Phyllites
ES	Uncertain			Black schist/phyllites
FL	Fault zone			
KP	Uncertain			Phyllites
KS	Uncertain			Mixed types - unsure of Mbr
OV	Overburden			
RD	Reeves Dolomite	Lower Laib	Lower Cambrian	Dolostones
RL	Reeves Limestone	Lower Laib	Lower Cambrian	Limestones/Dolostones
TL	Truman Limestone			
TS	Truman Schist/Green Phyllites	Lower Laib	Lower Cambrian	Green phyllites/Limestones

ROCKS

CODE	LITHOLOGY
AR	Argillite
ARLM	Limey argillite
BKSH	Black shale
BLPH	Black phyllite
BSP	Broken schist phyllite
CASI	Casing
CLAY	Clay
DOST	Dolostone
DOTE	Dolomite
GCHP	Graphitic schist with phyllite bands
GNPH	Green phyllite
LDAR	Limestone with dolomite & argillaceous bands
LHAR	Lithic arenite or wacke
LMAR	LMST with argillaceous & minor DOTE bands
LMDK	Lamprophyre dyke
LMST	Limestone
MFDY	Mafic dyke
MONZ	Monzonite
OVBN	Overburden
PHLM	Phyllite with limestone bands
PHQZ	Phyllite Quartz
PHSC	Schistose Phyllite
PHYL	Phyllite

ROCKS (cont'd)

CODE	LITHOLOGY
QTZ	Quartz vein
QZAR	Quartz arenite
QZMO	Quartz monzonite
QZTE	Quartzite
SCHI	Schist
SCLM	Shisty Limestone
SCPH	Schist with phyllite bands
TRCO	Triconing

COLOUR

Code	Colour
bk	black(ish)
bl	blue(bluish)
br	brown(ish)
dk	dark
gn	green(ish)
gy	grey(ish)
iv	ivory
lt	light
md	medium
rd	red(dish)
tan	tan
wo	off white/ivory
wt	white(ish)
yl	yellow(ish)

TEXTURE

CODE	TEXTURE NAME
>>	macroveined
BD	bedded
BN	banded
CG	coarse grained
EQ	equigranular
FG	fine-grained
FL	flour/powder
GG	Fault gauge
LM	laminated
MB	massive and banded
MG	medium grained
MO	mottled
MS	massive
PA	patchy
PR	porphyritic
TW	tweedy
VA	variegated
VU	vuggy

STRUCTURE

CODE	STRUCTURE NAME
<<	microveins
>>	macroveins
BR	breccia
CK	crackled breccia
CN	contorted
CR	crenulations
CT	contorted / crenulations
DC	Dyke
FL	fault
FR	fractured
LC	Laminated / contorted
QV	quartz vein(s)
SC	schistossity
SH	shear, shearing
SZ	sheared zone
VV	vein(s) & veinlet(s)
XF	fault breccia

BRECCIA

CODE	BRECCIA TYPE
AB	andesite breccia
AU	chaotic breccia
CB	crackled breccia
FB	flow breccia
HY	hydrothermal breccia
TB	tectonic breccia

EVENTS

CODE	DESCRIPTION
BD	bedding/core angle
BRS	bedrock surface
CA	core angle
F/	fault
F/C	fault contact
F/W	footwall
H/W	hangingwall
LX	lixiviation
SIG	significant zone
U/	unconformity
V/	vein
VOX	oxide vein

ALTERATION

CODE	Alteration
CAR	carbonatic
LSH	leaching
OXI	oxidased
PHI	phillic
PRO	propylitic
SIC	silifitn/carb
SIL	silicification

TESTS

HCL

Code	Intensity	Description
WK	Weak	Only seen with handlens
MD	Medium	Clearly visible with naked eye
ST	Strong	Boiling and bubles
X	No reaction	No visible reaction

ZINC ZAP

CODE	INTENSITY	DESCRIPTION
MD	Medium	Clearly colour visible in patches
ST	Strong	Widely spread out colour
WK	Weak	Only seen with handlens
X	No reaction	

LEAD ZAP

CODE	INTENSITY	DESCRIPTION
MD	Medium	Clearly colour visible in patches
ST	Strong	Widely spread out colour
WK	Weak	Only seen with handlens
X	No reaction	

MINERALIZATION

CODE	TYPE
.	laminations
/	crenulated/contorted laminations
<	microveins, fract. fills, interstitial in laminae
>	macroveins
A	irreg & concordant
B	blebs
C	concordant veins
E	veinlets and specks
G	fracture filling, breccia
I	irregular veins
L	laminations/bedded
M	massive
P	pervasive
R	replacement(s)
S	specks
T	Blebs, clots, laminae, microveins, fract. Fills
U	QZ veins & silicification
V	vein(s)
X	massive and/or banded

MINERALS

CODE	MINERAL
AK	ankerite
AS	arsenopyrite
BI	biotite
CA	calcite
CL	chlorite
CP	chalcopyrite
EP	epidote
GL	galena
HE	hematite
HM	hemimorphite
KF	k-spar, orthoclase
LI	limonite
MO	molybdenite
OX	oxides, general
PB	pyrobitumen
PR	pyrrhotite
PY	pyrite
QV	quartz vein, massive
QZ	quartz
SE	sericite
SL	sphalerite

APPENDIX

VI. REFLEX REPORTS

Reflex Downhole Measurements Report

HOLE D07-01

HOLE	SDEPTH	REFLEX AZM	AZM DECLIN	DIP
D07-01	0		330	-60

HOLE D07-02

HOLE	SDEPTH	REFLEX AZM	AZM DECLIN	DIP
D07-02	0	313.5	330	-70
	227.38	312.5	329	-69.4
	288.34	314	330.5	-68.4
	349.31	312.1	328.6	-68
	410.27	318.2	334.7	-67.9
	434.65	318.1	334.6	-67.4

HOLE D07-03

HOLE	SDEPTH	REFLEX AZM	AZM DECLIN	DIP
D07-03	0	313.5	330	-60
	62.79	312.6	329.1	-60.6
	123.75	315.3	331.8	-60.8
	190.8	317.3	333.8	-62.1
	245.67	318.6	335.1	-62.1
	306.63	320.8	337.3	-63
	376.73	322.2	338.7	-63.3
	438	325.8	342.3	-62.9
	502.01	326.4	342.9	-63.4
	596.49	326.4	342.9	-63.4

HOLE D07-04

HOLE	SDEPTH	REFLEX AZM	AZM DECLIN	DIP
D07-04	0	313.5	330	-60
	71.93	312.2	328.7	-59.8
	129.85	316.6	333.1	-59.3
	209.1	317.2	333.7	-58.9
	312.73	334.4	350.9	-57.5
	416.36	351.6	8.1	-58
	434.65	322.9	339.4	-56.9
	489.51	322.6	339.1	-56.6

HOLE D07-05

HOLE	SDEPTH	REFLEX AZM	AZM DECLIN	DIP
D07-05	0		358	-60

HOLE D07-06

HOLE	SDEPTH	REFLEX AZM	AZM DECLIN	DIP
D07-06	0		330	-55
	62.79	303.2	319.7	-57.9
	306.63	306.8	323.3	-58.4
	422.45	311.5	328	-58.4
	519.99	313.8	330.3	-57.8

HOLE D07-07

HOLE	SDEPTH	REFLEX AZM	AZM DECLIN	DIP
D07-07	0		0	-60
	62.79	341.5	358	-59.7
	121.92	284.4	300.9	-60.4
	243.84	293.1	309.6	-60.6
	309.68	335	351.5	-66.7
	370.64	334.7	351.2	-68.6
	428.55	335.3	351.8	-66.5
	489.51	352.8	9.3	-71.2
	553.52	353.6	10.1	-74.7
	611.43	357.3	13.8	-75.1
	672.39	1.3	17.8	-75.3
	733.65	3.8	20.3	-75.5
	800	293.1	309.6	-60.6
	821.74	6.2	22.7	-76.4

HOLE D07-08

HOLE	SDEPTH	REFLEX AZM	AZM DECLIN	DIP
D07-08	0		0	-60
	62	345.2	1.7	-60.1
	120	345	1.5	-59.4
	182	348	4.5	-58.2
	251	349.7	6.2	-56.9
	302	351.3	7.8	-56
	362	354.5	11	-54.8
	422	358.1	14.6	-54.5
	446	358.5	15	-54

HOLE D07-09

HOLE	SDEPTH	REFLEX AZM	AZM DECLIN	DIP
D07-09	0		0	-54
	62	343.1	359.6	-54.7
	122	345.6	2.1	-54.1
	164	346.8	3.3	-53.9
	188	347.6	4.1	-53.9

D07-09	242	347.6	4.1	-52.9
	332	347.6	4.1	-52.1

HOLE D07-10

HOLE	SDEPTH	REFLEX AZM	AZM DECLIN	DIP
D07-10	0		0	-70
	184.71	343.9	0.4	-70.4
	245.67	341.5	358	-70.9
	306.63	342.2	358.7	-71.3
	370.64	344.8	1.3	-71
	428.55	344.8	1.3	-70.1
	489.51	344	0.5	-70
	617.52	342	358.5	-70.7
	678.48	345.5	1.9	-68.9
	736.4	348.2	4.7	-66.6
	797.36	351.2	7.7	-64.4
	861.36	353.6	10.1	-63.4

HOLE D07-11

HOLE	SDEPTH	REFLEX AZM	AZM DECLIN	DIP
D07-11	0		0	-58
	62	340.6	357.1	-57.4
	122	343	359.5	-56.8
	182	343.6	0.1	-55.8
	242	345.1	1.6	-54.8
	311	347.1	3.6	-53.3
	374	347.2	3.7	-52.8
	428	348.1	4.6	-53.1
	488	349.6	6.1	-53.2
	548	350.4	6.9	-53.9
	602	349.9	6.4	-53.9

HOLE D07-12

HOLE	SDEPTH	REFLEX AZM	AZM DECLIN	DIP
D07-12	0		0	-90
	62	53.9	70.4	-89.5
	122	25.2	41.7	-89.5
	182	356	12.5	-88.7
	245	323.1	339.6	-88
	302	327.1	343.6	-87.3
	362	327	343.5	-87.1
	396.3	331	347.5	-86.8
	434	325.2	341.7	-86
	482	329.2	345.7	-85.4
	602	317.2	333.7	-84.6

D07-12	707	316.9	333.4	-81.8

APPENDIX

VII. GEOCHEMICAL ANALYSIS

		Sampled Section				ICP ANALYSIS																					
Tag Number	Hole	From	To	Interval	Type	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm	Mn ppm	Mg %
A10032451	D07-02	368.05	369.03	0.98	Core																						
A10032452	D07-02	369.03	369.71	0.68	Core																						
A10032453	D07-02	369.71	370.67	0.96	Core																						
A10032454	D07-02	370.67	371.76	1.09	Core																						
A10032455	D07-02	371.76	372.79	1.03	Core	5	2696	1242	6.0	37	147	13	1	59	4.99	57	41	<5	<5	62	<2	<2	92	2	<2	251	8.93
A10032456	D07-02	372.79	374.11	1.32	Core	3	4463	1673	6.2	62	87	17	7	171	6.65	163	25	<5	<5	59	<2	<2	106	2	3	234	9.48
A10032457	D07-02	374.11	375.05	0.94	Core	1	184	2151	0.8	22	26	18	1	48	1.51	48	4	<5	<5	30	<2	<2	203	2	2	277	10.90
A10032458	D07-02	391.04	391.97	0.93	Core	1	1361	1599	5.8	28	33	14	2	65	1.93	17	4	11	<5	29	<2	<2	226	2	2	286	10.68
A10032459	D07-02	391.97	393.05	1.08	Core	<1	1222	3866	2.5	17	128	32	<1	26	1.15	7	7	<5	<5	34	<2	<2	266	4	3	314	10.18
A10032460	D07-02	393.05	394.89	1.84	Core	3	7358	52800	8.2	17	57	414	1	28	6.26	10	14	<5	<5	25	<2	<2	158	4	4	289	8.28
A10032461	D07-02	394.89	396.02	1.13	Core	3	7455	29910	7.3	18	72	249	1	34	3.88	13	14	<5	5	42	<2	<2	230	3	3	335	9.77
A10032462	D07-02	396.02	396.91	0.89	Core	<1	425	9509	0.7	8	33	77	<1	11	1.17	4	<4	<5	<5	24	<2	<2	173	<2	2	297	10.93
A10032463	D07-02	396.91	398.06	1.15	Core	1	2584	18300	3.3	26	47	149	2	57	5.96	22	12	<5	<5	33	<2	<2	244	3	2	294	8.19
A10032464	D07-03	111.52	112.80	1.28	Core	10	<4	6	0.8	21	581	<1	<1	8	0.86	14	121	<5	5	36	<2	<2	12	<2	12	7	0.01
A10032465	D07-03	112.80	113.53	0.73	Core	31	<4	60	0.6	36	60	<1	6	66	1.91	26	89	<5	<5	77	<2	<2	32	2	9	<5	0.02
A10032466	D07-03	113.53	114.24	0.71	Core	80	9	67	1.0	25	224	<1	2	46	1.05	20	86	<5	6	106	<2	<2	69	3	2	6	<.01
A10032467	D07-03	116.33	117.03	0.7	Core	105	21	100	1.1	32	96	<1	1	36	3.86	8	102	5	<5	66	<2	<2	245	5	13	6	0.02
A10032468	n/a	0.00	0.00	0	Grab	18	<4	34	<0.4	3	244	<1	6	15	1.49	<2	91	<5	<5	15	<2	<2	52	2	12	580	0.56
A10032469	n/a	0.00	0.00	0	Blank	16	4	39	<0.4	9	476	<1	12	28	2.95	<2	91	<5	<5	76	<2	<2	160	9	34	341	1.33
A10032470	D07-04	96.32	96.88	0.56	Core	158	14	978	2.4	22	76	13	6	82	1.74	22	70	<5	6	341	<2	2	149	12	7	76	0.67
A10032471	D07-04	368.20	369.12	0.92	Core	8	7	37	<0.4	4	213	<1	7	14	1.62	<2	10	<5	<5	<2	<2	<2	238	9	4	308	0.43
A10032472	D07-04	369.12	369.85	0.73	Core	11	878	2401	<0.4	10	94	18	1	13	1.85	2	6	<5	<5	15	<2	<2	382	4	3	408	9.75
A10032473	D07-04	369.85	370.16	0.31	Core	6	871	43980	0.9	27	30	338	1	28	4.41	9	11	<5	<5	18	<2	<2	465	4	4	399	8.90
A10032474	D07-04	370.16	370.95	0.79	Core	<1	53	3112	<0.4	4	48	23	<1	7	0.72	<2	5	<5	<5	16	<2	<2	416	2	2	383	10.51
A10032475	D07-04	370.95	371.84	0.89	Core	<1	37	281	<0.4	3	32	2	<1	7	0.83	<2	<4	<5	<5	14	<2	<2	244	<2	<2	496	12.11
A10032476	D07-04	371.84	373.20	1.36	Core	<1	18	72	<0.4	4	62	1	<1	4	0.20	<2	<4	<5	<5	8	<2	<2	258	<2	<2	250	2.70
A10032477	n/a	0.00	0.00	0	Grab	31	9	63	<0.4	12	498	<1	19	32	3.67	<2	86	<5	<5	87	<2	4	195	9	42	482	1.51
A10032478	D07-04	461.35	462.12	0.77	Core	23	18210	4087	2.3	12	44	39	<1	13	1.88	3	42	<5	<5	458	<2	2	92	4	5	444	9.13
A10032479	D07-04	462.12	462.85	0.73	Core	13	37350	16400	7.0	33	48	151	3	52	6.03	8	33	<5	5	141	<2	25	134	8	8	694	8.72
A10032480	D07-04	462.85	463.70	0.85	Core	25	44830	42220	13.0	23	41	447	5	33	3.05	10	14	<5	6	81	<2	<2	149	6	9	409	9.62
A10032481	n/a	0.00	0.00	0	Grab	24	113	116	<0.4	8	778	<1	19	28	4.37	<2	102	<5	<5	97	<2	5	176	13	65	529	1.55
A10032482	D07-04	0.00	0.00	0	STD 1	480	9847	15430	203.1	4460	29	184	11	29	7.92	8	27	<5	55	40	3	<2	74	5	2	1356	0.49
A10032483	D07-04	463.70	464.50	0.8	Core	13	1612	8344	1.0	35	43	86	<1	50	2.22	10	20	<5	<5	84	<2	<2	173	6	5	435	11.56
A10032484	D07-04	464.50	465.12	0.62	Core	2	451	562	<0.4	20	41	7	<1	41	1.11	5	11	<5	<5	27	<2	<2	127	3	2	320	12.43
A10032485	D07-04	465.12	465.95	0.83	Core	23	879	2047	0.9	34	52	21	<1	49	3.85	8	62	<5	<5	109	<2	<2	120	6	5	273	8.87
A10032486	D07-04	465.95	467.20	1.25	Core	5	273	524	<0.4	10	24	5	<1	13	1.39	<2	9	<5	<5	32	<2	<2	93	3	<2	429	12.14
A10032487	D07-04	467.20	468.17	0.97	Core	27	2922	6878	1.6	63	57	78	2	113	7.27	17	63	<5	<5	343	<2	3	119	7	3	370	9.71
A10032488	D07-04	468.17	469.05	0.88	Core	43	6540	6013	5.1	39	37	60	9	65	3.72	18	20	<5	8	105	<2	7	129	6	5	511	12.18
A10032489	D07-04	469.05	469.96	0.91	Core	14	793	1111	<0.4	17	20	14	1	18	1.58	<2	<4	<5	<5	17	<2	11	104	3	2	314	10.85
A10032490	D07-04	469.96	471.00	1.04	Core	8	3508	1177	2.4	28	23	19	4	37	2.46	3	6	<5	<5	23	<2	4	114	3	3	294	10.68
A10032491	D07-04	471.00	471.42	0.42	Core	41	668	194	<0.4	7	905	2	26	111	5.91	<2	285	<5	<5	127	<2	6	297	8	24	943	4.05
A10032492	D07-04	0.00	0.00	0	Grab	25	16	55	<0.4	11	383	<1	14	36	3.24	<2	91	<5	<5	66	<2	3	203	10	52	441	1.36
A10032493	D07-04	0.00	0.00	0	STD 3	13870	2302	26750	55.2	43	<5	79	130	18	33.91	9	29	52	<5	10	4	4	3	4	<2	589	1.07
A10032494	D07-04	471.42	471.97	0.55	Core	20	7738	4369	7.8	26	23	60	4	34	2.60	3	9	<5	5	46	<2	2	126	5	5	337	10.15
A10032495	D07-04	471.97	472.72	0.75	Core	17	7326	8552	6.7	42	95	99	9	63	5.71	6	24	<5	<5	42	<2	3	155	7	7	460	9.10
A10032496	D07-04	472.72	473.77	1.05	Core	21	6439	9390	9.7	33	35	101	10	64	3.81	13	17	<5	6	57	<2	3	185	10	8	430	8.57
A10032497	D07-04	473.77	474.70	0.93	Core	21	3752	5906	5.3	23	27	68	3	44	2.35	18	15	<5	<5	64	<2	2	187	7	6	365	10.80
A10032498	D07-04	474.70	475.65	0.95	Core	6	303	1204	<0.4	4	111	12	1	13	0.70	4	28	<5	<5	31	<2	<2	150	4	5	395	10.09
A10032499	D07-04	475.65	476.50	0.85	Core	13	239	978	<0.4	4	398	10	5	31	1.30	6	71	<5	<5	57	<2	<2	204	6	11	529	9.80
A10032500	D07-04	476.50	477.32	0.82	Core	2	84	937	<0.4	4	10	10	<1	7	0.40	3	6	<5	<5	19	<2	<2	136	3	3	276	11.42
A10032501	D07-04	501.53	502.38	0.85	Core	1	8	301	<0.4	5	17	3	<1	4	0.46	<2	<4	<5	<5	8	<2	<2	106	2	3	225	11.46

		Sampled Section				ICP ANALYSIS																					
Tag Number	Hole	From	To	Interval	Type	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm	Mn ppm	Mg %
A10032502	D07-04	502.38	502.96	0.58	Core	10	1205	8203	1.0	30	32	73	4	27	3.76	9	12	<5	<5	14	<2	<2	104	5	6	259	9.81
A10032503	D07-04	502.96	503.81	0.85	Core	7	22	96	<0.4	32	51	<1	8	26	1.78	<2	11	<5	<5	<2	<2	<2	99	8	4	231	7.57
A10032504	D07-04	506.47	507.37	0.9	Core	2	11	61	<0.4	4	17	<1	1	4	0.32	<2	5	<5	<5	<2	<2	<2	135	2	3	276	10.30
A10032505	D07-04	507.37	507.86	0.49	Core	19	1198	105500	1.0	13	13	1030	3	13	4.31	2	11	<5	<5	2	<2	<2	88	5	4	210	8.19
A10032506	D07-04	507.86	508.82	0.96	Core	1	102	8960	<0.4	6	14	52	<1	5	0.92	<2	7	<5	<5	3	<2	<2	125	4	5	286	12.36
A10032507	D07-08	392.97	393.97	1	Core	2	6	27	<0.4	13	41	<1	1	9	0.27	<2	<4	<5	<5	9	<2	5	312	3	3	252	3.04
A10032508	D07-08	393.97	395.00	1.03	Core	21	18	100	<0.4	7	64	<1	12	34	3.77	<2	38	<5	<5	18	<2	<2	160	6	12	411	1.26
A10032509	D07-08	395.00	396.03	1.03	Core	31	16	93	<0.4	9	80	<1	17	42	4.61	<2	37	<5	<5	17	<2	<2	113	9	24	727	1.12
A10032510	D07-08	396.03	396.96	0.93	Core	22	14	59	<0.4	10	48	<1	11	26	3.32	<2	22	<5	<5	11	<2	<2	299	11	19	1073	1.00
A10032511	D07-08	396.96	398.00	1.04	Core	11	10	33	<0.4	8	27	<1	6	13	2.40	<2	13	<5	<5	8	<2	<2	453	13	8	1326	1.04
A10032512	D07-08	398.00	399.02	1.02	Core	8	6	18	<0.4	9	20	<1	2	5	0.85	<2	4	<5	<5	<2	<2	<2	448	6	4	352	0.78
A10032513	D07-08	399.02	399.97	0.95	Core	5	4	8	<0.4	6	14	<1	1	3	0.47	<2	<4	<5	<5	<2	<2	2	454	4	4	169	1.29
A10032514	D07-08	399.97	401.00	1.03	Core	4	7	20	<0.4	7	15	<1	1	3	0.61	<2	<4	<5	<5	<2	<2	<2	475	7	4	573	1.50
A10032515	D07-08	401.00	401.99	0.99	Core	3	10	19	<0.4	4	17	<1	1	3	0.65	<2	<4	<5	<5	<2	<2	<2	382	8	4	986	0.91
A10032516	D07-08	401.99	404.00	2.01	Core	13	<4	51	<0.4	5	52	<1	10	27	2.68	<2	23	<5	<5	9	<2	<2	163	7	9	686	0.92
A10032517	D07-08	404.00	404.97	0.97	Core	19	6	44	<0.4	5	74	<1	15	33	3.04	<2	34	<5	<5	10	<2	<2	68	6	22	639	0.77
A10032518	D07-08	404.97	406.21	1.24	Core	8	22	71	0.5	11	42	<1	4	7	1.80	<2	41	<5	<5	5	<2	<2	327	14	11	1220	0.33
A10032519	D07-08	406.21	407.00	0.79	Core	15	7	80	0.7	7	63	<1	12	30	2.87	<2	27	<5	<5	9	<2	<2	73	6	22	594	0.71
A10032520	D07-08	407.00	407.63	0.63	Core	15	156	278	0.5	12	36	1	4	6	1.71	<2	72	<5	<5	3	<2	<2	180	10	9	530	0.28
A10032521	D07-08	407.63	408.98	1.35	Core	19	111	171	7.0	17	59	1	4	8	2.06	<2	84	7	<5	4	<2	<2	119	9	22	561	0.32
A10032522	D07-08	408.98	410.00	1.02	Core	21	36	44	0.7	22	67	<1	5	9	2.78	<2	94	<5	<5	5	<2	<2	132	11	20	480	0.34
A10032523	D07-08	410.00	411.23	1.23	Core	9	37	73	0.6	7	87	<1	9	22	2.33	<2	45	<5	<5	8	<2	<2	61	5	26	395	0.41
A10032524	D07-08	411.23	412.08	0.85	Core	15	5	39	<0.4	7	72	<1	13	26	2.73	<2	37	<5	<5	4	<2	<2	63	3	15	429	0.47
A10032525	D07-08	412.08	413.00	0.92	Core	16	<4	28	<0.4	8	60	<1	11	23	2.75	<2	34	<5	<5	5	<2	<2	64	4	13	467	0.49
A10032526	D07-08	413.00	413.07	0.07	Core	43	<4	23	<0.4	15	54	<1	10	38	3.56	<2	41	<5	<5	4	<2	<2	75	3	9	490	0.59
A10032527	D07-08	413.07	413.98	0.91	Core	42	<4	17	0.5	18	57	<1	21	35	3.76	<2	22	<5	<5	5	<2	<2	66	3	9	443	0.57
A10032528	D07-08	413.98	414.97	0.99	Core	35	<4	21	0.6	14	62	<1	10	35	2.86	<2	28	<5	<5	7	<2	<2	80	3	9	492	0.68
A10032529	D07-08	414.97	416.99	2.02	Core	15	12	60	<0.4	12	86	<1	11	25	2.52	<2	36	<5	<5	13	<2	<2	53	4	17	411	0.58
A10032530	D07-08	416.99	418.02	1.03	Core	13	14	93	<0.4	5	85	<1	12	27	2.89	<2	36	<5	<5	16	<2	<2	51	3	17	524	0.62
A10032531	D07-08	418.02	419.00	0.98	Core	15	18	84	<0.4	6	95	<1	15	29	3.07	<2	40	<5	<5	17	<2	<2	61	3	15	492	0.61
A10032532	D07-08	419.00	419.96	0.96	Core	13	15	33	<0.4	6	82	<1	12	25	2.87	<2	46	<5	<5	15	<2	<2	48	5	20	310	0.58
A10032533	D07-08	419.96	420.90	0.94	Core	17	57	60	<0.4	7	122	<1	13	34	3.19	<2	45	<5	<5	19	<2	<2	75	4	18	430	0.77
A10032534	D07-08	420.90	422.00	1.1	Core	13	40	72	<0.4	9	80	<1	14	26	2.82	<2	47	<5	<5	14	<2	<2	47	4	15	354	0.59
A10032535	D07-07	474.15	475.15	1	Core	1	8	18	<0.4	48	63	<1	9	14	1.80	<2	42	<5	<5	3	<2	<2	54	3	18	392	0.38
A10032536	D07-07	475.15	476.20	1.05	Core	2	11	16	<0.4	41	57	<1	8	13	2.45	<2	73	<5	<5	5	<2	<2	106	5	26	478	0.62
A10032537	D07-07	476.20	477.32	1.12	Core	16	5	30	<0.4	33	68	<1	9	17	3.67	<2	33	<5	<5	6	<2	<2	132	6	15	733	0.87
A10032538	D07-07	477.32	478.30	0.98	Core	23	<4	33	<0.4	234	14	<1	45	18	7.36	<2	60	<5	<5	9	<2	<2	124	6	2	824	0.52
A10032539	D07-07	510.38	511.38	1	Core	9	52	106	<0.4	20	81	<1	7	19	1.89	<2	35	<5	<5	4	<2	<2	62	5	18	503	0.41
A10032540	D07-07	511.38	512.38	1	Core	4	59	39	0.7	749	6	<1	115	28	10.30	<2	23	<5	<5	3	<2	<2	93	6	<2	696	0.56
A10032541	D07-07	512.38	513.42	1.04	Core	12	9	37	<0.4	115	64	<1	16	33	2.71	<2	30	<5	<5	4	<2	<2	61	4	9	411	0.44
A10032542	D07-07	589.00	590.09	1.09	Core	4	<4	8	<0.4	5	26	<1	<1	2	0.04	<2	<4	<5	<5	2	<2	<2	284	<2	<2	17	1.02
A10032543	D07-07	590.09	591.10	1.01	Core	2	<4	12	<0.4	7	19	<1	<1	5	0.16	<2	<4	<5	<5	3	<2	2	237	<2	<2	28	1.37
A10032544	D07-07	591.10	592.12	1.02	Core	<1	<4	5	<0.4	5	17	<1	<1	1	0.04	<2	<4	<5	<5	<2	<2	<2	273	<2	<2	14	0.97
A10032545	D07-07	0.00	0.00	0	STD 7	6790	7310	56630	93.2	45	<5	168	82	18	26.10	10	30	39	<5	10	4	<2	2	2	<2	546	0.70
A10032546	D07-07	773.46	775.00	1.54	Core	8	16	89	<0.4	40	95	<1	<1	21	1.34	9	5	<5	<5	17	<2	<2	278	6	5	72	5.18
A10032547	D07-07	775.00	776.47	1.47	Core	6	10	55	<0.4	51	159	<1	<1	31	1.23	9	<4	<5	<5	11	<2	<2	283	3	2	44	3.27
A10032548	D07-07	777.24	778.75	1.51	Core	4	6	35	<0.4	45	213	<1	<1	28	0.94	4	<4	<5	<5	4	<2	<2	250	2	2	46	2.70
A10032549	D07-07	778.75	780.19	1.44	Core	5	8	51	<0.4	49	111	<1	<1	25	1.15	12	<4	<5	<5	5	<2	<2	263	2	<2	36	2.32
A10032550	D07-07	780.19	781.81	1.62	Core	3	6	37	<0.4	60	185	<1	<1	32	0.87	13	<4	<5	<5	4	<2	<2	263	<2	<2	36	2.79
A10032551	D07-07	781.81	783.32	1.51	Core	1	<4	23	<0.4	49	253	<1	<1	31	0.29	7	<4	<5	<5	6	<2	<2	286	<2	<2	27	2.52
A10032552	D07-07	783.32	784.51	1.19	Core	1	9	48	<0.4	7	170	<1	<1	5	0.41	<2	9	<5	<5	12	<2	<2	355	4	4	103	7.46

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Tag Number	Hole	From	To	Interval	Type	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm	Mn ppm	Mg %
A10032553	D07-07	784.51	786.15	1.64	Core	15	17	117	<0.4	15	204	1	1	33	0.61	5	15	<5	<5	27	<2	<2	473	10	7	84	1.39
A10032554	D07-07	331.25	332.84	1.59	Core	1	53	483	<0.4	10	2126	3	<1	9	0.69	2	<4	<5	<5	17	<2	4	246	4	4	276	7.43
A10032555	D07-07	332.51	332.84	0.33	Core	<1	10	319	<0.4	13	677	2	<1	5	0.30	<2	<4	<5	<5	2	<2	4	307	3	2	182	0.65
A10032556	D07-07	332.84	334.66	1.82	Core	1	29	3441	<0.4	9	1053	39	<1	3	0.62	<2	<4	<5	<5	13	<2	<2	317	2	2	353	9.33
A10032557	D07-07	334.66	336.03	1.37	Core	4	<4	21	<0.4	11	22	<1	2	8	0.70	<2	<4	<5	<5	<2	<2	3	311	4	7	163	0.85
A10032558	D07-07	336.03	337.26	1.23	Core	<1	10	283	<0.4	7	806	2	<1	3	0.53	<2	5	<5	<5	22	<2	<2	353	2	3	338	9.98
A10032559	D07-07	337.26	338.69	1.43	Core	1	35	260	<0.4	9	1367	4	<1	2	0.11	<2	<4	<5	<5	13	<2	<2	290	<2	<2	48	2.25
A10032560	Hike	0.00	0.00	0	Float	719	10	18	1.5	21	22	<1	65	37	20.75	201	26	<5	<5	28	<2	<2	62	8	<2	148	0.19
A10032561	D07-11	175.29	176.29	1	Core	32	20	40	<0.4	5	43	<1	22	55	3.84	<2	14	<5	<5	6	<2	<2	298	5	20	371	1.19
A10032562	D07-11	176.29	177.21	0.92	Core	10	<4	2	<0.4	3	<5	<1	2	6	0.43	<2	71	<5	<5	<2	<2	<2	76	<2	11	80	0.07
A10032563	D07-11	177.21	178.36	1.15	Core	29	21	42	<0.4	4	46	<1	18	49	3.52	2	11	<5	<5	6	<2	<2	422	6	18	397	1.22
A10032564	D07-11	334.00	335.00	1	Core	1	25	5143	<0.4	3	54	36	<1	3	0.71	<2	<4	<5	<5	21	<2	5	157	<2	<2	318	12.02
A10032565	D07-11	335.00	336.00	1	Core	1	39	675	<0.4	2	1162	5	<1	4	0.81	<2	<4	<5	<5	16	<2	<2	186	2	<2	254	9.94
A10032566	D07-11	336.00	337.00	1	Core	<1	111	5647	<0.4	5	2001	62	<1	5	1.28	<2	<4	5	<5	18	<2	6	184	2	<2	237	8.93
A10032567	D07-11	337.00	338.00	1	Core	<1	28	806	<0.4	2	1155	5	<1	1	0.61	<2	<4	<5	<5	22	<2	5	351	<2	<2	282	11.81
A10032568	D07-11	338.00	338.89	0.89	Core	1	60	910	<0.4	<2	211	9	<1	2	0.67	<2	<4	<5	<5	12	<2	5	313	<2	<2	194	5.02
A10032569	D07-10	478.66	479.77	1.11	Core	87	20	475	1.4	19	218	5	3	46	0.75	15	53	<5	9	125	<2	<2	283	19	9	115	1.13
A10032570	D07-10	479.77	480.83	1.06	Core	75	21	499	1.8	13	217	6	3	47	0.68	17	101	<5	12	132	<2	<2	157	10	13	64	0.36
A10032571	D07-10	480.83	482.00	1.17	Core	79	23	501	1.3	12	268	6	7	57	1.26	16	79	<5	6	107	<2	<2	113	8	11	168	0.81
A10032572	D07-10	482.27	483.41	1.14	Core	58	13	402	0.8	16	114	5	4	41	0.72	16	50	<5	8	53	<2	<2	90	6	13	49	0.34
A10032573	D07-10	483.41	484.50	1.09	Core	39	12	640	0.7	14	172	8	4	35	0.77	12	92	<5	6	51	<2	<2	106	5	12	71	0.58
A10032574	D07-10	484.50	485.55	1.05	Core	44	11	403	0.6	14	112	5	4	35	0.74	13	61	<5	6	32	<2	<2	68	4	13	39	0.45
A10032575	D07-10	503.96	505.15	1.19	Core	112	19	648	2.8	19	156	9	6	67	1.25	15	93	<5	6	367	<2	<2	164	16	8	105	1.08
A10032576	D07-11	344.83	345.64	0.81	Core	5	20	23	<0.4	6	10	<1	3	5	1.06	<2	<4	<5	<5	4	<2	2	347	11	<2	1285	1.60
A10032577	D07-11	345.64	346.76	1.12	Core	17	31	105	<0.4	15	40	<1	21	45	4.18	<2	59	<5	<5	14	<2	<2	27	7	37	985	1.10
A10032578	D07-11	346.76	347.85	1.09	Core	26	22	116	<0.4	6	38	<1	22	50	4.28	<2	46	7	<5	16	<2	<2	8	6	35	579	1.01
A10032579	D07-11	366.38	366.86	0.48	Core	<1	60	319	<0.4	2	152	4	<1	1	0.71	<2	6	<5	<5	16	<2	4	178	<2	<2	441	5.88
A10032580	D07-11	418.67	419.71	1.04	Core	4	910	221	0.7	11	469	2	2	24	2.42	<2	<4	<5	<5	61	<2	<2	148	<2	<2	190	1.24
A10032581	D07-11	419.71	420.98	1.27	Core	3	480	100	<0.4	11	553	<1	<1	6	2.22	<2	<4	<5	<5	30	<2	2	139	<2	<2	218	3.22
A10032582	D07-11	420.98	422.00	1.02	Core	7	370	418	<0.4	10	1755	4	<1	7	2.03	<2	4	<5	<5	25	<2	<2	131	<2	<2	281	5.54
A10032583	D07-11	422.00	423.11	1.11	Core	4	165	434	<0.4	5	1843	3	<1	5	1.09	<2	7	<5	<5	28	<2	<2	151	<2	<2	248	6.28
A10032584	D07-11	423.11	424.00	0.89	Core	3	110	352	<0.4	13	194	2	<1	6	1.72	<2	18	<5	<5	57	<2	<2	95	<2	<2	224	6.62
A10032585	D07-11	424.00	425.00	1	Core	1	105	1018	<0.4	3	142	5	<1	2	0.72	<2	9	<5	<5	33	<2	2	130	2	<2	284	8.38
A10032586	D07-11	425.00	426.07	1.07	Core	<1	136	249	<0.4	3	136	2	<1	2	0.80	<2	5	<5	<5	41	<2	3	125	2	<2	314	9.42
A10032587	D07-11	426.07	427.11	1.04	Core	1	109	252	<0.4	2	331	2	<1	3	0.51	<2	5	<5	<5	40	<2	<2	116	<2	<2	265	9.89
A10032588	D07-11	427.11	428.00	0.89	Core	<1	152	453	<0.4	7	167	9	<1	6	0.58	<2	<4	<5	<5	72	<2	2	114	<2	<2	276	10.81
A10032589	D07-11	428.00	429.00	1	Core	2	75	465	<0.4	8	222	7	<1	4	0.97	<2	9	<5	<5	48	<2	<2	93	<2	<2	248	8.55
A10032590	D07-11	429.00	430.06	1.06	Core	3	98	528	<0.4	9	110	4	<1	7	1.32	<2	14	<5	<5	79	<2	3	101	<2	<2	274	8.35
A10032591	D07-11	430.06	431.43	1.37	Core	<1	175	542	0.4	12	307	1	<1	7	1.43	<2	5	<5	<5	62	<2	2	116	3	<2	283	9.91
A10032592	D07-11	0.00	0.00	0	STD 1	495	8539	9900	201.3	4023	18	141	12	25	6.98	6	25	<5	45	33	6	<2	73	4	5	1106	0.49
A10032593	D07-11	432.00	433.00	1	Core	29	40	78	<0.4	26	459	<1	16	30	2.88	<2	78	<5	<5	70	<2	<2	168	7	29	374	1.37
A10032594	D07-11	433.00	434.33	1.33	Core	2	138	177	<0.4	32	54	1	2	32	3.84	<2	<4	<5	<5	41	<2	<2	140	2	<2	314	10.43
A10032595	D07-11	434.33	435.00	0.67	Core	3	160	339	<0.4	12	46	3	<1	5	1.85	<2	<4	<5	<5	43	<2	3	125	<2	<2	261	9.60
A10032596	D07-11	435.00	436.00	1	Core	2	124	657	<0.4	11	34	6	<1	4	1.40	<2	<4	<5	<5	39	<2	<2	130	<2	<2	285	11.25
A10032597	D07-11	436.00	437.79	1.79	Core	2	112	614	<0.4	8	38	4	<1	4	1.15	<2	<4	<5	<5	46	<2	4	153	<2	<2	339	11.72
A10032598	D07-11	437.79	438.84	1.05	Core	5	178	610	<0.4	12	57	4	<1	5	1.60	2	<4	<5	<5	58	<2	<2	157	2	<2	350	10.43
A10032599	D07-11	438.84	440.00	1.16	Core	1	120	712	<0.4	13	35	6	<1	6	1.58	<2	<4	<5	<5	49	<2	6	157	<2	<2	341	10.98
A10032600	D07-11	440.00	440.95	0.95	Core	1	89	947	<0.4	15	40	8	<1	8	1.76	<2	<4	<5	<5	36	<2	2	151	<2	<2	319	9.87
A10032601	D07-11	440.95	442.00	1.05	Core	1	67	344	<0.4	3	29	2	<1	2	0.34	<2	<4	<5	<5	33	<2	4	149	<2	<2	306	9.95
A10032602	D07-11	442.00	443.00	1	Core	16	339	826	0.7	66	76	7	1	24	6.40	3	19	5	<5	151	<2	<2	108	2	<2	205	5.92
A10032603	D07-11	443.00	444.00	1	Core	4	68	342	<0.4	6	64	2	<1	5	0.84	<2	<4	<5	<5	62	<2	<2	141	2	<2	316	10.84

		Sampled Section				ICP ANALYSIS																					
Tag Number	Hole	From	To	Interval	Type	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm	Mn ppm	Mg %
A10032604	D07-11	444.00	445.10	1.1	Core	2	82	323	<0.4	3	33	2	<1	2	0.38	<2	<4	<5	<5	49	<2	3	132	<2	<2	308	10.97
A10032605	D07-11	445.10	446.21	1.11	Core	11	283	816	0.5	61	72	7	1	30	6.04	5	23	<5	<5	175	<2	3	114	3	<2	281	8.40
A10032606	D07-11	446.21	447.16	0.95	Core	5	208	940	<0.4	23	45	9	<1	12	1.91	2	5	<5	<5	79	<2	2	137	3	<2	274	10.06
A10032607	D07-11	447.16	448.34	1.18	Core	4	167	652	<0.4	17	43	6	<1	10	1.94	<2	<4	<5	<5	58	<2	2	163	3	<2	320	10.60
A10032608	D07-11	0.00	0.00	0	STD 3	11190	2248	22870	50.7	28	7	67	99	12	21.95	6	25	44	<5	<2	8	<2	3	<2	<2	491	1.00
A10032609	D07-11	449.52	450.71	1.19	Core	34	41	284	<0.4	6	29	1	<1	2	1.08	<2	<4	<5	<5	33	<2	4	110	<2	<2	316	9.87
A10032610	D07-11	450.71	451.76	1.05	Core	5	71	509	<0.4	10	27	2	<1	3	1.70	<2	<4	<5	<5	34	<2	3	125	<2	<2	299	9.58
A10032611	D07-11	451.76	452.87	1.11	Core	7	247	1531	<0.4	30	31	12	<1	14	3.33	3	<4	<5	<5	50	<2	2	159	<2	<2	284	8.58
A10032612	D07-11	452.87	453.87	1	Core	3	398	594	<0.4	15	41	5	3	26	1.51	4	<4	<5	<5	66	<2	3	150	2	<2	313	10.60
A10032613	D07-11	455.00	456.05	1.05	Core	1	38	698	<0.4	2	22	4	<1	2	0.51	<2	<4	<5	<5	35	<2	4	112	2	<2	360	10.90
A10032614	D07-11	456.05	457.00	0.95	Core	2	57	506	<0.4	2	21	3	<1	2	0.42	<2	<4	<5	<5	54	<2	<2	104	<2	<2	325	10.34
A10032615	D07-11	457.00	458.00	1	Core	2	39	187	<0.4	3	25	<1	<1	1	0.31	<2	6	<5	<5	35	<2	2	118	<2	<2	310	10.59
A10032616	D07-11	458.00	458.94	0.94	Core	9	57	352	<0.4	18	27	2	<1	3	1.00	<2	<4	<5	<5	40	<2	4	126	2	<2	306	10.47
A10032617	D07-11	458.94	459.89	0.95	Core	3	199	961	<0.4	4	31	10	<1	7	0.68	<2	<4	<5	<5	76	<2	3	169	2	<2	319	11.78
A10032618	D07-11	459.89	461.00	1.11	Core	3	250	703	<0.4	3	25	6	<1	7	0.65	<2	<4	<5	<5	70	<2	4	136	2	<2	322	11.67
A10032619	D07-11	461.00	462.00	1	Core	2	329	1233	<0.4	9	15	8	1	11	1.45	<2	<4	<5	<5	33	<2	3	120	<2	<2	360	11.10
A10032620	D07-11	462.00	463.00	1	Core	1	236	4073	<0.4	7	19	20	<1	7	1.37	<2	<4	<5	<5	22	<2	3	102	<2	<2	348	10.76
A10032621	D07-11	463.00	464.00	1	Core	2	139	3237	<0.4	3	21	15	<1	5	1.06	<2	<4	<5	<5	27	<2	4	105	<2	<2	377	10.35
A10032622	D07-11	464.00	465.07	1.07	Core	3	115	4844	<0.4	4	18	25	<1	4	1.02	<2	<4	<5	<5	27	<2	4	107	<2	<2	393	10.77
A10032623	D07-11	465.07	466.43	1.36	Core	3	433	6610	<0.4	4	25	56	<1	4	0.77	<2	<4	<5	<5	24	<2	3	111	<2	<2	367	10.26
A10032624	D07-11	466.43	467.82	1.39	Core	2	202	1513	<0.4	8	33	13	<1	9	1.39	<2	12	<5	<5	19	<2	2	104	<2	<2	326	7.76
A10032625	D07-11	467.82	469.86	2.04	Core	3	150	2613	<0.4	10	25	29	1	25	1.37	3	<4	<5	<5	26	<2	3	116	4	<2	405	8.76
A10032626	D07-11	469.86	471.00	1.14	Core	2	242	7987	0.4	6	34	95	<1	5	1.15	3	<4	<5	<5	29	<2	3	153	2	<2	405	10.53
A10032627	D07-11	471.00	472.10	1.1	Core	<1	125	1352	<0.4	8	40	10	<1	5	1.63	<2	<4	<5	<5	23	<2	2	157	2	<2	392	10.97
A10032628	D07-11	472.10	473.00	0.9	Core	2	58	305	<0.4	2	20	1	<1	3	0.71	<2	<4	<5	<5	15	<2	2	124	<2	<2	453	12.13
A10032629	D07-11	473.00	474.10	1.1	Core	1	37	469	<0.4	3	40	3	<1	2	0.76	<2	<4	<5	<5	18	<2	2	161	<2	<2	408	11.53
A10032630	D07-11	474.10	475.25	1.15	Core	1	34	243	<0.4	3	43	<1	<1	3	0.79	<2	<4	<5	<5	17	<2	2	179	<2	<2	425	12.07
A10032631	D07-11	475.25	476.29	1.04	Core	1	23	96	<0.4	<2	35	<1	<1	1	0.72	<2	<4	<5	<5	16	<2	4	170	<2	<2	384	11.72
A10032632	D07-11	476.29	477.34	1.05	Core	<1	43	291	<0.4	<2	147	5	<1	2	0.56	<2	<4	<5	<5	19	<2	4	155	<2	<2	343	11.23
A10032633	D07-11	477.34	478.83	1.49	Core	<1	61	559	<0.4	5	237	13	<1	4	0.53	<2	<4	<5	<5	14	<2	5	115	2	<2	381	10.67
A10032634	D07-11	0.00	0.00	0	Blank	24	16	119	<0.4	13	385	1	13	24	2.62	<2	71	<5	<5	76	2	2	141	7	22	387	1.26
A10032635	D07-11	479.80	480.80	1	Core	1	35	149	<0.4	4	37	<1	<1	3	0.78	<2	<4	<5	<5	16	<2	3	101	<2	<2	439	11.21
A10032636	D07-11	480.80	482.00	1.2	Core	2	75	549	<0.4	3	212	5	<1	7	0.66	<2	<4	<5	<5	14	<2	2	107	3	<2	344	10.51
A10032637	D07-11	482.00	483.00	1	Core	<1	48	5359	<0.4	4	20	45	<1	4	0.64	<2	<4	<5	<5	13	<2	5	96	2	<2	387	10.67
A10032638	D07-11	0.00	0.00	0	Blank	13	12	44	<0.4	15	310	<1	14	26	2.19	<2	72	<5	<5	57	<2	<2	110	7	34	292	1.12
A10032639	D07-11	0.00	0.00	0	STD 7	6506	5893	60660	71.3	43	<5	156	73	13	19.54	5	25	46	<5	4	8	<2	2	<2	<2	484	0.71
A10032640	D07-11	485.00	485.98	0.98	Core	26	63	530	<0.4	2	9	3	<1	3	0.65	<2	<4	<5	<5	18	<2	3	87	2	<2	338	11.19
A10032641	D07-11	485.98	487.10	1.12	Core	1	45	370	<0.4	2	13	3	<1	3	0.41	<2	<4	<5	<5	19	<2	<2	98	2	<2	280	11.60
A10032642	D07-11	487.10	488.00	0.9	Core	2	46	393	<0.4	4	13	3	<1	4	0.64	<2	<4	<5	<5	20	<2	<2	100	<2	<2	357	12.25
A10032643	D07-11	488.00	489.00	1	Core	3	47	393	<0.4	5	14	4	<1	5	0.45	<2	<4	<5	<5	17	<2	4	90	2	<2	224	11.97
A10032644	D07-11	489.00	490.00	1	Core	1	48	362	<0.4	2	16	3	<1	3	0.34	<2	<4	<5	<5	17	<2	3	88	2	<2	240	12.06
A10032645	D07-11	490.00	491.00	1	Core	2	34	327	<0.4	<2	19	3	<1	3	0.43	<2	<4	<5	<5	11	<2	2	87	2	<2	263	11.27
A10032646	D07-11	491.00	492.06	1.06	Core	1	34	349	<0.4	<2	20	3	<1	3	0.39	<2	<4	<5	<5	14	<2	4	91	2	<2	235	10.89
A10032647	D07-11	492.06	493.00	0.94	Core	1	45	411	<0.4	4	27	3	1	4	0.63	<2	<4	<5	<5	11	<2	2	91	2	<2	283	10.82
A10032648	D07-11	493.00	494.00	1	Core	3	63	643	<0.4	<2	6	6	<1	2	0.48	<2	<4	<5	<5	17	<2	2	82	<2	<2	262	11.09
A10032649	D07-11	0.00	0.00	0	STD 1	450	8187	9500	149.6	4046	15	141	13	24	6.61	6	24	<5	44	31	6	<2	66	4	6	1184	0.46
A10032650	D07-11	453.87	455.00	1.13	Core	5	582	1391	0.5	26	66	12	<1	11	1.72	3	4	<5	<5	68	<2	3	157	4	<2	317	10.00
A10032651	D07-11	494.00	494.99	0.99	Core	2	222	1035	1.1	20	14	13	1	18	2.94	34	<4	<5	<5	17	<2	<2	97	<2	<2	304	8.63
A10032652	D07-11	494.99	496.00	1.01	Core	2	53	225	<0.4	<2	8	1	<1	2	0.41	<2	<4	<5	<5	17	<2	2	86	<2	<2	214	11.28
A10032653	D07-11	496.00	497.00	1	Core	1	64	188	<0.4	2	26	1	<1	1	0.51	<2	<4	<5	<5	16	<2	<2	76	<2	<2	222	11.69
A10032654	D07-11	497.00	498.00	1	Core	1	38	191	<0.4	2	94	1	<1	1	0.36	<2	<4	<5	<5	12	<2	2	79	<2	<2	185	11.50

		Sampled Section				ICP ANALYSIS																					
Tag Number	Hole	From	To	Interval	Type	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm	Mn ppm	Mg %
A10032655	D07-11	498.00	499.20	1.2	Core	3	73	412	<0.4	2	11	4	<1	2	0.68	<2	<4	<5	<5	13	<2	3	89	<2	<2	209	11.64
A10032656	D07-11	499.20	500.15	0.95	Core	2	184	589	0.7	9	10	6	<1	6	2.54	<2	<4	<5	<5	13	<2	<2	84	<2	<2	193	10.84
A10032657	D07-11	500.15	501.15	1	Core	4	147	1414	<0.4	<2	12	15	<1	1	0.54	<2	<4	<5	<5	15	<2	4	98	<2	<2	241	12.22
A10032658	D07-11	501.15	502.03	0.88	Core	5	109	7406	0.6	10	12	105	1	9	3.10	2	<4	<5	<5	24	<2	6	101	<2	<2	260	10.90
A10032659	D07-11	502.03	503.50	1.47	Core	3	123	1297	<0.4	<2	44	14	<1	4	0.50	<2	<4	<5	<5	22	<2	6	98	<2	<2	219	11.44
A10032660	D07-11	0.00	0.00	0	STD 3	10880	2137	22220	57.2	34	6	69	105	12	21.28	6	23	44	<5	<2	7	<2	2	<2	<2	487	0.96
A10032661	D07-11	504.50	505.00	0.5	Core	46	2686	23030	2.6	28	12	654	6	21	11.85	2	14	7	<5	10	3	<2	67	<2	<2	209	6.55
A10032662	D07-11	0.00	0.00	0	Blank	27	58	675	<0.4	13	264	9	17	31	2.31	<2	101	<5	<5	72	2	4	97	9	35	373	1.18
A10032663	D07-11	506.10	506.73	0.63	Core	3	188	456	<0.4	<2	57	4	<1	1	0.40	<2	<4	<5	<5	16	<2	<2	108	<2	<2	216	11.85
A10032664	D07-11	506.73	508.59	1.86	Core	5	3739	6753	5.0	19	18	94	1	12	4.64	3	<4	<5	<5	16	2	4	96	<2	<2	213	10.06
A10032665	D07-11	508.59	509.47	0.88	Core	4	636	1026	0.6	4	37	11	<1	2	0.97	<2	<4	<5	<5	12	<2	3	102	<2	<2	172	10.85
A10032666	D07-11	0.00	0.00	0	Blank	20	21	57	<0.4	13	452	<1	17	28	2.95	<2	85	<5	<5	78	2	<2	205	9	40	404	1.42
A10032667	D07-11	511.67	512.75	1.08	Core	5	67	458	<0.4	4	20	5	<1	4	0.45	<2	<4	<5	<5	13	<2	4	121	<2	<2	194	11.06
A10032668	D07-11	512.75	514.39	1.64	Core	1	30	336	<0.4	<2	10	3	<1	1	0.29	<2	<4	<5	<5	10	<2	4	100	<2	<2	163	10.71
A10032669	D07-11	514.39	515.81	1.42	Core	3	45	532	<0.4	3	8	5	<1	2	0.39	<2	<4	<5	<5	13	<2	2	127	<2	<2	223	11.39
A10032670	D07-11	515.81	516.67	0.86	Core	3	236	929	<0.4	5	15	11	<1	4	0.59	<2	<4	<5	<5	13	<2	7	129	<2	<2	237	10.35
A10032671	D07-11	516.67	518.00	1.33	Core	6	1383	6385	1.4	15	21	92	2	13	4.84	3	9	<5	<5	11	2	<2	138	<2	<2	242	10.18
A10032672	D07-11	0.00	0.00	0	STD 7	5915	6583	61820	75.3	51	<5	184	103	14	21.96	5	27	51	<5	<2	8	<2	2	<2	<2	556	0.70
A10032673	D07-11	519.06	520.06	1	Core	12	19	258	<0.4	<2	7	2	<1	1	0.41	<2	<4	<5	<5	11	<2	4	105	<2	<2	251	10.86
A10032674	D07-11	520.06	521.00	0.94	Core	4	18	211	<0.4	<2	17	1	<1	2	0.51	<2	<4	<5	<5	9	<2	3	96	<2	<2	260	12.25
A10032675	D07-11	521.00	522.00	1	Core	1	10	282	<0.4	2	9	1	<1	1	0.55	<2	<4	<5	<5	10	<2	2	90	<2	<2	334	11.60
A10032676	D07-11	522.00	523.00	1	Core	4	20	335	<0.4	<2	14	3	1	2	0.54	<2	<4	<5	<5	8	<2	<2	106	2	<2	321	11.68
A10032677	D07-11	523.00	524.10	1.1	Core	4	16	100	<0.4	3	39	<1	2	7	0.66	<2	<4	<5	<5	7	<2	<2	198	3	<2	213	5.28
A10032678	D07-11	527.87	528.55	0.68	Core	3	23	1469	<0.4	2	23	8	3	8	0.96	<2	<4	<5	<5	6	<2	4	105	4	<2	238	9.07
A10032679	D07-11	529.36	530.00	0.64	Core	4	48	16990	0.7	3	41	153	2	4	0.78	2	<4	<5	<5	6	<2	5	112	2	<2	541	4.42
A10032680	D07-11	530.00	530.71	0.71	Core	3	12	4196	<0.4	2	13	40	1	2	0.44	<2	<4	<5	<5	10	<2	4	98	2	<2	336	9.30
A10032681	D07-11	530.71	531.64	0.93	Core	7	52	44880	4.7	2	38	485	2	3	0.61	3	<4	<5	<5	6	<2	7	123	3	<2	694	5.09
A10032682	D07-11	0.00	0.00	0	Blank	13	12	275	<0.4	13	415	2	16	29	2.41	<2	73	<5	<5	65	<2	<2	131	7	33	364	1.13
A10032683	D07-11	533.00	534.00	1	Core	2	6	65	<0.4	<2	7	<1	<1	<1	0.36	<2	<4	<5	<5	9	<2	3	68	<2	<2	242	10.47
A10032684	D07-11	534.00	535.09	1.09	Core	2	8	321	<0.4	<2	5	2	<1	1	0.45	<2	<4	<5	<5	6	<2	<2	78	<2	<2	266	12.90
A10032685	D07-11	535.09	536.00	0.91	Core	1	12	6449	<0.4	<2	7	66	<1	2	0.48	<2	<4	<5	<5	5	<2	7	73	<2	<2	244	11.39
A10032686	D07-11	536.00	537.03	1.03	Core	3	6	89	<0.4	<2	6	<1	<1	<1	0.32	<2	<4	<5	<5	7	<2	7	76	<2	<2	208	11.89
A10032687	D07-11	537.03	538.14	1.11	Core	<1	<4	306	<0.4	<2	5	1	<1	<1	0.30	<2	<4	<5	<5	6	<2	2	67	<2	<2	199	11.19
A10032688	D07-11	538.14	539.78	1.64	Core	1	6	13	<0.4	<2	5	<1	<1	1	0.30	<2	<4	<5	<5	6	<2	4	71	<2	<2	200	11.07
A10032689	D07-11	539.78	540.24	0.46	Core	3	5	12	<0.4	<2	5	<1	<1	1	0.31	<2	<4	<5	<5	8	<2	4	68	<2	<2	201	10.67
A10032690	D07-11	540.24	541.00	0.76	Core	4	<4	33	<0.4	<2	5	<1	1	1	0.29	<2	<4	<5	<5	8	<2	4	76	<2	<2	204	10.89
A10032691	D07-11	541.00	543.50	2.5	Core	3	6	19	<0.4	<2	5	<1	<1	1	0.32	<2	<4	<5	<5	6	<2	4	77	<2	<2	218	11.46
A10032692	D07-11	543.50	545.00	1.5	Core	4	9	6	<0.4	<2	5	<1	<1	1	0.32	<2	<4	<5	<5	4	<2	2	89	<2	<2	190	10.44
A10032693	D07-11	545.00	546.50	1.5	Core	4	6	14	<0.4	<2	<5	<1	<1	2	0.27	<2	<4	<5	<5	5	<2	4	92	<2	<2	213	10.96
A10032694	D07-11	546.50	548.00	1.5	Core	3	9	57	<0.4	<2	6	<1	1	3	0.30	<2	<4	<5	<5	4	<2	2	84	<2	<2	230	9.87
A10032695	D07-11	548.00	548.89	0.89	Core	4	7	5	<0.4	<2	5	<1	1	2	0.39	<2	<4	<5	<5	5	<2	4	77	<2	<2	259	10.77
A10032696	D07-11	548.89	549.74	0.85	Core	5	8	21	<0.4	3	11	<1	2	3	0.69	<2	<4	<5	<5	5	<2	3	110	3	<2	281	10.48
A10032697	D07-11	549.74	550.65	0.91	Core	3	18	30	<0.4	7	22	<1	4	8	1.58	<2	5	<5	<5	6	<2	<2	188	9	<2	626	5.40
A10032698	D07-11	0.00	0.00	0	STD 1	474	9152	10460	105.3	4420	15	159	14	27	7.07	8	28	<5	45	33	7	<2	76	5	7	1287	0.48
A10032699	D07-11	551.65	552.64	0.99	Core	9	42	78	<0.4	23	22	<1	4	10	1.83	<2	<4	<5	<5	3	<2	<2	281	13	<2	548	1.18
A10032700	D07-11	554.29	554.79	0.5	Core	9	11	32	<0.4	8	52	<1	11	26	1.48	<2	27	<5	<5	8	<2	<2	40	4	33	256	0.36
A10032701	D07-11	580.50	581.00	0.5	Core	4	96	264	<0.4	7	136	2	11	12	3.88	<2	48	<5	<5	15	3	<2	97	8	13	1184	0.68
A10032702	D07-11	478.83	479.80	0.97	Core	2	48	194	<0.4	3	46	1	<1	3	0.65	<2	<4	<5	<5	16	<2	6	88	<2	<2	482	10.68
A10032703	D07-11	483.00	484.00	1	Core	1	53	177	<0.4	<2	24	1	<1	3	0.44	<2	<4	<5	<5	7	<2	3	100	2	<2	284	10.59
A10032704	D07-11	505.00	506.10	1.1	Core	2	130	1209	<0.4	<2	17	14	<1	3	0.41	<2	<4	<5	<5	17	<2	3	112	<2	<2	216	11.36
A10032705	D07-11	510.08	511.67	1.59	Core	3	75	401	<0.4	<2	38	4	1	4	0.38	<2	<4	<5	<5	17	<2	4	124	<2	<2	192	10.39

		Sampled Section				ICP ANALYSIS																					
Tag Number	Hole	From	To	Interval	Type	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm	Mn ppm	Mg %
A10032706	D07-11	531.64	533.00	1.36	Core	3	15	4434	<0.4	<2	20	49	1	2	0.48	<2	<4	<5	<5	8	<2	5	86	3	<2	309	9.46
A10032707	D07-11	431.43	432.00	0.57	Core	3	273	1782	<0.4	25	145	11	1	19	3.52	4	4	<5	<5	95	2	2	113	3	<2	348	6.78
A10032708	D07-11	448.34	449.57	1.23	Core	1	127	311	<0.4	7	22	2	<1	4	0.80	<2	<4	<5	<5	29	<2	2	134	<2	<2	408	11.67
A10032709	D07-11	484.00	485.00	1	Core	2	85	709	<0.4	3	30	10	<1	6	0.45	<2	<4	<5	<5	17	<2	5	103	3	<2	328	11.26
A10032710	D07-11	470.00	471.00	1	Core	1	59	984	<0.4	4	34	5	<1	3	0.89	<2	<4	<5	<5	20	<2	3	183	<2	<2	561	11.60
A10032711	D07-11	503.50	504.50	1	Core	2	26	492	<0.4	<2	10	4	<1	2	0.38	<2	<4	<5	<5	14	<2	3	92	<2	<2	237	11.73
A10032712	D07-11	518.00	519.06	1.06	Core	3	7	129	<0.4	<2	7	<1	<1	<1	0.34	<2	<4	<5	<5	7	<2	4	110	<2	<2	210	11.06
A10032713	D07-11	550.65	551.65	1	Core	18	10	36	<0.4	12	46	<1	14	27	2.37	<2	7	<5	<5	3	<2	<2	135	13	<2	848	1.49
A10032714	D07-11	432.00	433.00	1	Core	2	134	392	<0.4	6	48	3	<1	4	0.91	<2	<4	<5	<5	49	<2	2	139	2	<2	302	10.55
A10032715	D07-10	0.00	0.00	0	STD 3	13490	2290	26000	47.5	34	6	62	112	12	26.79	8	25	48	<5	<2	9	<2	3	<2	<2	475	1.14
A10032716	D07-10	687.15	688.08	0.93	Core	51	40	99	<0.4	508	16	<1	18	15	7.70	<2	83	8	<5	2	2	<2	65	7	11	120	0.12
A10032717	D07-10	688.08	689.10	1.02	Core	20	10	20	<0.4	29	82	<1	10	13	2.67	<2	62	<5	<5	7	<2	<2	59	6	15	508	0.31
A10032718	D07-10	689.10	690.15	1.05	Core	7	14	12	<0.4	75	59	<1	8	14	2.74	<2	90	5	<5	7	<2	<2	78	7	18	511	0.35
A10032719	D07-10	690.15	691.29	1.14	Core	3	21	19	<0.4	119	51	<1	16	19	2.83	<2	92	6	<5	7	<2	<2	54	5	18	446	0.37
A10032720	D07-10	693.95	695.08	1.13	Core	9	11	9	<0.4	31	25	<1	5	8	1.14	<2	61	5	<5	4	<2	<2	35	4	15	242	0.12
A10032721	D07-10	695.56	696.06	0.5	Core	7	59	118	<0.4	36	65	<1	7	6	2.16	<2	61	<5	<5	5	<2	<2	44	4	18	418	0.22
A10032722	D07-10	697.19	697.67	0.48	Core	7	15	14	<0.4	41	29	<1	5	11	1.27	<2	109	<5	<5	3	<2	<2	26	3	17	230	0.15
A10032723	D07-10	697.67	698.66	0.99	Core	4	15	3	<0.4	389	31	<1	25	26	4.26	<2	102	<5	<5	4	<2	<2	26	3	13	197	0.16
A10032724	D07-10	701.95	702.10	0.15	Core	82	17	91	<0.4	10	98	<1	36	45	4.66	<2	39	<5	<5	26	2	<2	18	2	3	386	0.65
A10032725	D07-10	708.60	709.34	0.74	Core	35	18	69	<0.4	12	89	<1	20	33	4.05	<2	32	<5	<5	31	2	<2	25	3	8	294	0.78
A10032726	D07-10	712.15	712.84	0.69	Core	69	43	49	<0.4	41	95	<1	30	39	7.15	<2	43	5	<5	15	3	<2	29	3	18	1242	1.01
A10032727	D07-10	0.00	0.00	0	Blank	25	15	49	<0.4	14	555	<1	19	38	4.15	<2	109	<5	<5	93	<2	<2	239	10	40	463	1.85
A10032728	D07-10	712.84	713.51	0.67	Core	9	8	26	<0.4	12	103	<1	11	22	2.48	<2	37	<5	<5	19	<2	<2	53	5	35	598	0.65
A10032729	D07-10	713.51	714.01	0.5	Core	3	9	15	<0.4	77	54	<1	8	20	2.22	<2	23	6	<5	8	<2	<2	65	3	14	300	0.49
A10032730	D07-10	0.00	0.00	0	STD 1	540	8626	10200	150.4	4101	19	135	12	25	7.65	7	26	<5	44	35	6	<2	78	5	6	1045	0.51
A10032731	D07-10	714.29	715.06	0.77	Core	18	40	80	<0.4	37	87	<1	5	26	2.11	<2	55	<5	<5	15	<2	<2	94	4	26	540	0.81
A10032732	D07-10	715.06	716.07	1.01	Core	32	13	25	<0.4	28	95	<1	14	30	3.51	<2	39	6	<5	14	<2	<2	93	5	24	623	0.84
A10032733	D07-10	716.67	717.10	0.43	Core	9	7	11	<0.4	12	90	<1	8	11	1.38	<2	58	<5	<5	10	<2	<2	120	4	24	519	0.62
A10032734	D07-10	717.10	718.11	1.01	Core	6	6	6	<0.4	7	53	<1	2	8	0.68	<2	37	<5	<5	4	<2	<2	107	6	19	367	0.40
A10032735	D07-10	718.11	719.16	1.05	Core	5	4	13	<0.4	<2	77	<1	1	4	0.59	<2	99	<5	<5	9	<2	<2	91	6	30	316	0.30
A10032736	D07-10	719.16	720.20	1.04	Core	14	11	25	<0.4	19	70	<1	8	14	2.71	<2	51	5	<5	16	<2	<2	111	7	21	703	0.64
A10032737	D07-10	720.20	721.16	0.96	Core	16	6	15	<0.4	6	67	<1	4	9	2.06	<2	57	<5	<5	13	<2	<2	90	6	17	638	0.44
A10032738	D07-10	721.16	722.26	1.1	Core	13	<4	9	<0.4	10	71	<1	3	9	1.73	<2	53	5	<5	12	<2	<2	95	6	23	606	0.42
A10032739	D07-10	722.26	723.29	1.03	Core	26	7	10	<0.4	10	70	<1	10	24	2.72	<2	68	<5	<5	17	<2	<2	133	9	20	654	0.56
A10032740	D07-10	723.29	724.20	0.91	Core	49	13	21	<0.4	14	59	<1	30	21	4.65	<2	53	7	<5	12	2	<2	118	9	19	710	0.63
A10032741	D07-10	747.89	748.59	0.7	Core	88	13	39	<0.4	19	76	<1	22	32	5.38	<2	35	7	<5	13	2	<2	106	6	12	840	0.78
A10032742	D07-10	755.05	756.23	1.18	Core	36	14	30	<0.4	8	65	<1	15	19	3.62	<2	36	<5	<5	11	<2	<2	77	4	15	671	0.70
A10032743	D07-10	759.89	760.72	0.83	Core	35	34	36	<0.4	9	78	<1	21	31	3.92	<2	30	<5	<5	21	2	<2	43	4	16	601	0.73
A10032744	D07-10	766.01	766.47	0.46	Core	6	69	40	<0.4	6	60	<1	4	8	2.69	<2	57	<5	<5	8	<2	<2	103	6	36	988	0.61
A10032745	D07-10	0.00	0.00	0	STD 7	7825	7059	72890	86.4	51	<5	164	93	14	26.69	8	29	55	<5	<2	9	<2	2	<2	<2	494	0.85
A10032746	D07-10	736.50	737.07	0.57	Core	41	30	248	<0.4	8	69	<1	10	7	4.74	<2	54	6	<5	20	<2	<2	182	13	22	753	0.64
A10032747	D07-10	786.00	787.11	1.11	Core	26	20	52	<0.4	3	77	<1	13	20	4.11	<2	52	5	<5	11	<2	<2	41	5	23	910	0.58
A10032748	D07-10	787.11	788.21	1.1	Core	16	19	42	<0.4	5	62	<1	9	16	3.09	<2	69	<5	<5	13	<2	<2	39	6	28	481	0.43
A10032749	D07-10	788.21	789.31	1.1	Core	65	35	55	<0.4	11	82	<1	13	21	4.34	<2	66	5	<5	13	2	<2	134	13	24	1185	0.56
A10032750	D07-12	151.40	152.08	0.68	Core	51	13	80	<0.4	11	64	<1	20	64	4.72	49	18	<5	<5	5	2	<2	39	3	16	268	0.96
A10033701	D07-12	243.34	243.74	0.4	Core	58	20	33	<0.4	15	35	<1	18	61	3.96	3	12	<5	<5	4	<2	<2	363	6	<2	314	1.04
A10033702	D07-12	243.74	244.68	0.94	Core	35	36	92	<0.4	7	41	<1	15	43	3.23	2	11	<5	<5	7	<2	<2	246	6	<2	267	1.35
A10033703	D07-12	414.73	415.63	0.9	Core	3	200	577	<0.4	<2	179	4	<1	1	0.42	<2	5	<5	<5	20	<2	<2	144	<2	<2	307	12.32
A10033704	D07-12	419.00	420.00	1	Core	1	57	204	<0.4	3	383	1	<1	9	0.82	23	<4	<5	<5	32	<2	5	170	<2	<2	458	12.06
A10033705	D07-12	420.00	421.00	1	Core	19	530	1621	0.8	34	74	14	2	52	4.01	110	5	<5	<5	37	<2	3	166	<2	<2	495	9.09
A10033706	D07-12	421.00	422.00	1	Core	6	391	606	0.6	17	76	4	1	27	2.04	51	<4	<5	<5	24	<2	2	156	<2	<2	489	11.39

		Sampled Section				ICP ANALYSIS																					
Tag Number	Hole	From	To	Interval	Type	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm	Mn ppm	Mg %
A10033707	D07-12	424.00	425.00	1	Core	1	56	657	<0.4	<2	33	4	<1	4	0.76	2	<4	<5	<5	15	<2	3	148	<2	<2	212	12.38
A10033708	D07-12	425.00	426.18	1.18	Core	<1	457	172	0.5	<2	41	<1	<1	2	0.47	<2	11	<5	<5	19	<2	4	155	<2	<2	229	10.85
A10033709	D07-12	426.18	426.71	0.53	Core	<1	276	197	<0.4	<2	63	1	<1	1	0.31	2	<4	<5	<5	20	<2	<2	318	2	<2	305	9.44
A10033710	D07-12	0.00	0.00	0	STD 3	11750	2110	23800	45.0	24	5	58	103	11	24.04	7	22	48	<5	<2	7	<2	3	<2	<2	442	1.06
A10033711	D07-12	426.71	427.69	0.98	Core	44	1676	11770	1.7	<2	232	148	<1	1	0.41	<2	4	<5	<5	25	<2	8	257	2	<2	367	8.12
A10033712	D07-12	429.46	430.46	1	Core	3	26	203	<0.4	<2	99	<1	<1	1	0.41	<2	<4	<5	<5	18	<2	2	226	<2	<2	353	11.59
A10033713	D07-12	430.46	431.61	1.15	Core	1	1545	6749	2.2	24	250	70	1	17	4.25	5	<4	<5	<5	49	<2	<2	250	2	<2	304	8.84
A10033714	D07-12	431.61	432.39	0.78	Core	<1	63	1830	<0.4	2	69	15	<1	4	0.66	<2	<4	<5	<5	48	<2	3	293	<2	<2	276	12.22
A10033715	D07-12	432.39	433.05	0.66	Core	6	10690	57630	11.1	39	55	589	4	54	7.46	17	11	7	<5	34	2	8	139	2	<2	232	9.71
A10033716	D07-12	433.05	434.00	0.95	Core	<1	67	486	<0.4	<2	56	3	<1	2	0.40	<2	5	<5	<5	20	<2	<2	130	<2	<2	219	12.31
A10033717	D07-12	435.30	436.00	0.7	Core	<1	140	371	<0.4	<2	49	2	<1	4	0.49	<2	15	<5	<5	17	<2	3	107	<2	<2	197	11.03
A10033718	D07-12	436.00	437.00	1	Core	<1	46	216	<0.4	<2	64	1	<1	3	0.33	2	47	<5	<5	14	<2	2	113	2	<2	179	8.74
A10033719	D07-12	437.00	438.00	1	Core	1	55	64	<0.4	4	322	<1	<1	7	0.62	4	26	<5	<5	16	<2	<2	154	2	<2	212	5.71
A10033720	D07-12	438.00	439.00	1	Core	1	23	210	<0.4	6	1106	<1	<1	12	0.59	5	<4	<5	<5	20	<2	4	162	2	<2	250	8.86
A10033721	D07-12	439.00	440.00	1	Core	11	210	523	0.4	10	94	<1	1	10	3.11	2	<4	<5	<5	9	<2	<2	212	3	<2	243	6.56
A10033722	D07-12	440.00	441.08	1.08	Core	3	16	53	<0.4	3	190	<1	1	4	0.54	<2	<4	<5	<5	4	<2	<2	296	4	<2	57	1.10
A10033723	D07-12	441.08	442.00	0.92	Core	11	122	1840	<0.4	16	121	7	1	12	1.01	2	<4	<5	<5	3	<2	<2	255	4	<2	117	0.44
A10033724	D07-12	450.00	451.00	1	Core	2	23	528	<0.4	<2	425	3	<1	3	0.38	<2	<4	<5	<5	18	<2	3	127	2	<2	212	12.27
A10033725	D07-12	0.00	0.00	0	STD 1	511	8437	9856	113.5	4180	18	136	12	24	7.49	7	25	<5	44	32	5	<2	73	4	8	1091	0.52
A10033726	D07-12	451.00	452.00	1	Core	2	91	1388	<0.4	11	397	9	<1	1	0.29	<2	<4	<5	<5	16	<2	3	141	2	<2	168	12.02
A10033727	D07-12	452.00	453.00	1	Core	2	80	2547	<0.4	3	70	23	<1	2	0.56	<2	<4	<5	<5	14	<2	3	121	2	<2	165	11.71
A10033728	D07-12	453.00	454.00	1	Core	<1	64	796	<0.4	3	399	5	<1	4	0.59	<2	<4	<5	<5	13	<2	3	114	2	<2	181	12.05
A10033729	D07-12	454.00	455.00	1	Core	2	33	369	<0.4	<2	618	2	<1	1	0.25	<2	<4	<5	<5	13	<2	2	105	2	<2	190	11.53
A10033730	D07-12	455.00	456.00	1	Core	1	29	332	<0.4	2	806	1	<1	3	0.27	<2	6	<5	<5	16	<2	<2	111	4	<2	183	11.39
A10033731	D07-12	456.00	456.92	0.92	Core	<1	61	32520	<0.4	5	36	324	<1	7	0.67	4	<4	<5	<5	21	<2	5	138	4	<2	204	10.75
A10033732	D07-12	456.92	457.45	0.53	Core	1	15	242	<0.4	<2	79	1	<1	<1	0.36	<2	<4	<5	<5	28	<2	<2	210	2	<2	199	12.31
A10033733	D07-12	457.45	458.00	0.55	Core	7	215	12050	0.7	12	86	159	1	10	3.00	8	<4	<5	<5	27	<2	3	165	<2	<2	239	11.35
A10033734	D07-12	458.00	458.79	0.79	Core	2	43	356	<0.4	<2	58	2	<1	3	0.63	<2	<4	<5	<5	23	<2	2	155	<2	<2	226	12.85
A10033735	D07-12	458.79	459.79	1	Core	1	13	1694	<0.4	<2	347	14	<1	3	0.54	<2	<4	<5	<5	16	<2	4	121	<2	<2	221	11.88
A10033736	D07-12	459.88	461.00	1.12	Core	7	172	101000	0.8	6	26	1079	3	13	1.43	10	<4	<5	<5	28	<2	14	142	4	<2	275	11.46
A10033737	D07-12	461.00	461.94	0.94	Core	12	80	42900	0.6	5	36	361	1	9	1.31	6	<4	<5	<5	18	<2	6	149	3	<2	233	11.25
A10033738	D07-12	0.00	0.00	0	Blank	23	16	388	<0.4	10	363	2	12	23	2.66	<2	62	<5	<5	57	<2	<2	143	8	38	315	1.28
A10033739	D07-12	461.94	462.92	0.98	Core	1	47	3489	<0.4	<2	236	34	<1	4	0.43	<2	<4	<5	<5	15	<2	<2	146	2	<2	195	11.48
A10033740	D07-12	0.00	0.00	0	STD 7	6163	6275	61860	62.1	15	<5	147	52	13	17.26	6	26	47	<5	2	8	<2	2	<2	<2	483	0.79
A10033741	D07-12	462.92	464.00	1.08	Core	17	55	510	<0.4	<2	167	2	<1	1	0.30	<2	<4	<5	<5	12	<2	2	100	<2	<2	153	11.59
A10033742	D07-12	464.00	465.00	1	Core	<1	59	370	<0.4	<2	37	2	<1	1	0.39	<2	<4	<5	<5	15	<2	<2	124	<2	<2	166	12.47
A10033743	D07-12	465.00	466.05	1.05	Core	<1	22	461	<0.4	<2	41	2	<1	<1	0.35	<2	<4	<5	<5	10	<2	4	114	<2	<2	197	12.65
A10033744	D07-12	466.05	466.74	0.69	Core	2	16	280	<0.4	2	50	1	<1	2	0.46	<2	<4	<5	<5	15	<2	<2	145	<2	<2	259	11.56
A10033745	D07-12	466.74	467.74	1	Core	1	44	584	<0.4	<2	73	3	<1	2	0.59	<2	<4	<5	<5	12	<2	<2	122	<2	<2	214	11.85
A10033746	D07-12	467.74	469.00	1.26	Core	1	405	4765	0.8	5	96	37	<1	7	2.00	2	<4	<5	<5	14	<2	<2	116	<2	<2	228	11.48
A10033747	D07-12	469.00	470.00	1	Core	<1	135	2801	0.5	8	84	19	<1	6	2.29	<2	<4	<5	<5	16	<2	<2	121	<2	<2	241	11.64
A10033748	D07-12	470.00	471.19	1.19	Core	8	1797	23550	2.4	31	16	181	4	27	16.70	10	<4	15	<5	17	3	3	122	2	<2	253	7.73
A10033749	D07-12	471.19	472.19	1	Core	3	377	3574	0.7	8	50	23	<1	7	4.11	<2	<4	<5	<5	13	<2	3	113	2	<2	275	10.07
A10033750	D07-12	473.00	474.00	1	Core	1	80	1146	<0.4	8	165	10	1	16	1.49	2	<4	<5	<5	18	<2	2	139	<2	<2	224	11.02
A10033751	D07-12	474.00	475.06	1.06	Core	<1	187	864	<0.4	3	174	6	<1	8	0.79	<2	<4	<5	<5	13	<2	<2	114	<2	<2	197	11.46
A10033752	D07-12	475.06	476.00	0.94	Core	3	1029	5200	1.1	12	42	32	1	9	6.14	2	<4	5	<5	11	2	<2	102	<2	<2	189	9.77
A10033753	D07-12	476.00	477.00	1	Core	1	408	6973	0.5	3	42	35	<1	5	2.63	<2	<4	<5	<5	13	<2	3	105	2	<2	183	10.65
A10033754	D07-12	0.00	0.00	0	Blank	25	20	137	<0.4	12	414	<1	12	24	2.92	<2	63	<5	<5	63	<2	<2	137	7	35	303	1.34
A10033755	D07-12	0.00	0.00	0	STD 1	513	7947	9337	114.4	3848	17	124	11	23	7.23	6	23	<5	42	31	6	<2	72	4	6	980	0.49
A10033756	D07-12	477.00	478.00	1	Core	2	122	3249	<0.4	16	39	16	<1	5	0.91	<2	<4	<5	<5	15	<2	2	101	<2	<2	230	12.50
A10033757	D07-12	478.00	479.00	1	Core	1	172	3266	<0.4	7	61	17	<1	9	1.89	3	<4	<5	<5	15	<2	3	140	<2	<2	219	11.47

		Sampled Section				ICP ANALYSIS																					
Tag Number	Hole	From	To	Interval	Type	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm	Mn ppm	Mg %
A10033758	D07-12	479.00	480.00	1	Core	2	141	3376	<0.4	5	206	15	<1	8	1.21	4	<4	<5	<5	13	<2	3	156	<2	<2	218	11.25
A10033759	D07-12	480.00	481.00	1	Core	3	108	1353	<0.4	6	185	7	<1	14	0.84	4	<4	<5	<5	14	<2	2	123	2	<2	225	10.28
A10033760	D07-12	481.00	482.00	1	Core	5	376	2477	0.5	16	109	9	1	19	2.84	12	<4	<5	<5	11	<2	<2	111	3	<2	216	10.18
A10033761	D07-12	482.00	482.53	0.53	Core	4	136	1739	<0.4	11	101	7	<1	15	1.14	2	<4	<5	<5	14	<2	3	106	3	<2	229	10.96
A10033762	D07-12	482.53	483.45	0.92	Core	14	6425	6197	5.4	46	93	35	4	71	4.99	17	4	5	<5	20	<2	3	108	6	<2	288	8.85
A10033763	D07-12	483.45	483.80	0.35	Core	19	874	2219	1.0	79	81	12	6	86	5.16	19	<4	<5	<5	17	<2	<2	106	4	<2	322	8.89
A10033764	D07-12	484.04	484.51	0.47	Core	79	1384	2386	2.1	139	46	17	11	65	7.23	14	<4	<5	<5	30	2	<2	102	5	<2	297	5.88
A10033765	D07-12	411.72	412.22	0.5	Core	1	370	2093	0.7	8	45	18	<1	7	1.97	15	<4	<5	<5	16	<2	2	107	<2	<2	339	11.18
A10033766	D07-12	412.22	413.00	0.78	Core	1	911	52	<0.4	<2	443	<1	<1	1	0.56	<2	8	<5	<5	13	<2	2	95	<2	<2	247	10.55
A10033767	D07-12	486.62	487.12	0.5	Core	19	622	407	0.5	20	20	1	4	16	4.89	2	<4	<5	<5	5	2	<2	252	3	<2	111	1.04
A10033768	D07-12	514.66	515.68	1.02	Core	4	1279	1678	0.7	35	18	9	1	39	6.34	3	<4	<5	<5	50	<2	<2	166	<2	<2	258	10.31
A10033769	D07-12	515.68	517.00	1.32	Core	<1	72	101	<0.4	<2	301	<1	<1	1	0.50	<2	<4	<5	<5	47	<2	<2	147	<2	<2	230	12.76
A10033770	D07-12	0.00	0.00	0	STD 7	7146	5820	65690	66.6	40	<5	140	76	12	22.80	7	23	46	<5	<2	8	<2	2	<2	<2	429	0.85
A10033771	D07-12	517.00	518.00	1	Core	25	124	1098	<0.4	6	292	5	<1	5	1.05	<2	<4	<5	<5	54	<2	3	115	<2	<2	239	12.31
A10033772	D07-12	521.00	522.00	1	Core	1	1602	924	0.9	13	160	5	1	14	1.81	<2	<4	<5	<5	78	<2	2	159	2	<2	278	11.03
A10033773	D07-12	522.00	523.00	1	Core	<1	3432	2208	1.5	31	28	13	3	37	4.44	8	5	<5	<5	77	<2	4	153	5	<2	368	10.43
A10033774	D07-12	523.00	524.00	1	Core	15	3108	1153	1.0	28	22	5	2	37	5.99	5	18	<5	<5	254	2	<2	207	3	<2	416	7.73
A10033775	D07-12	536.25	537.25	1	Core	11	1565	671	0.8	65	27	<1	4	100	11.68	9	69	7	<5	973	2	6	149	2	<2	194	6.58
A10033776	D07-12	537.60	538.60	1	Core	3	1183	378	<0.4	28	40	<1	2	35	4.75	8	27	<5	<5	517	2	6	155	2	<2	223	11.26
A10033777	D07-12	539.95	540.98	1.03	Core	3	4104	1958	1.7	28	18	7	4	34	5.89	12	<4	<5	<5	66	<2	3	212	4	<2	308	10.25
A10033778	D07-12	540.98	542.00	1.02	Core	2	117	262	<0.4	5	135	1	<1	4	0.54	<2	<4	<5	<5	32	<2	3	142	<2	<2	319	12.97
A10033779	D07-12	543.74	544.50	0.76	Core	16	6467	1756	4.3	51	<5	12	7	51	21.10	14	8	<5	<5	21	3	17	88	<2	<2	181	5.97
A10033780	D07-12	550.00	551.00	1	Core	20	1344	2725	0.4	52	25	19	2	37	11.81	14	6	<5	<5	62	3	7	154	<2	<2	467	8.44
A10033781	D07-12	551.61	552.10	0.49	Core	15	4852	1880	0.8	26	26	15	5	24	13.68	18	8	<5	<5	51	3	17	128	2	<2	648	9.06
A10033782	D07-12	554.38	554.88	0.5	Core	50	5714	1194	1.5	95	9	10	11	73	21.59	31	11	<5	<5	50	<2	57	87	<2	<2	381	6.91
A10033783	D07-12	563.00	564.36	1.36	Core	24	5872	1241	3.7	96	28	12	14	129	15.21	29	16	<5	<5	48	3	44	95	2	<2	279	9.28
A10033784	D07-12	574.31	574.85	0.54	Core	7	152	1315	<0.4	4	36	14	1	14	1.18	<2	<4	<5	<5	17	<2	<2	150	3	<2	643	8.53
A10033785	D07-12	0.00	0.00	0	STD 3	13390	3824	31810	58.5	29	6	112	177	24	29.64	22	36	41	<5	2	8	70	3	<2	<2	704	1.35
A10033786	D07-12	575.29	576.06	0.77	Core	50	207	607	<0.4	5	30	4	1	8	1.15	<2	<4	<5	<5	22	<2	4	127	5	<2	370	12.43
A10033787	D07-12	576.06	576.77	0.71	Core	11	363	1481	<0.4	22	82	19	2	27	2.57	2	<4	<5	<5	19	<2	2	139	3	<2	379	10.81
A10033788	D07-12	576.77	577.83	1.06	Core	5	125	489	<0.4	<2	36	4	1	7	1.08	<2	<4	<5	<5	13	<2	<2	105	3	<2	325	11.72
A10033789	D07-12	577.83	579.00	1.17	Core	6	164	1483	<0.4	3	31	13	1	11	1.29	2	<4	<5	<5	17	<2	<2	123	2	<2	315	12.00
A10033790	D07-12	579.00	579.79	0.79	Core	4	157	576	<0.4	2	23	4	1	11	1.45	<2	<4	<5	<5	11	<2	<2	104	<2	<2	271	12.64
A10033791	D07-12	579.79	581.00	1.21	Core	3	68	1306	<0.4	<2	38	10	<1	5	0.72	<2	<4	<5	<5	15	<2	<2	115	2	<2	274	12.31
A10033792	D07-12	581.00	582.00	1	Core	3	63	1561	<0.4	2	41	12	1	6	0.86	<2	<4	<5	<5	12	<2	<2	116	2	<2	284	13.10
A10033793	D07-12	582.00	582.55	0.55	Core	5	174	1361	<0.4	2	28	11	<1	7	0.86	3	<4	<5	<5	14	<2	<2	112	2	<2	239	12.43
A10033794	D07-12	587.14	588.38	1.24	Core	4	227	1072	<0.4	<2	31	8	<1	3	0.35	<2	<4	<5	<5	21	<2	<2	115	2	<2	240	13.43
A10033795	D07-12	604.35	605.00	0.65	Core	4	56	7460	<0.4	<2	51	80	<1	2	0.59	2	<4	<5	<5	22	<2	<2	133	<2	<2	296	13.39
A10033796	D07-12	605.00	605.69	0.69	Core	13	38	23440	0.6	16	37	439	1	12	3.63	12	<4	<5	<5	34	2	2	133	2	<2	314	11.61
A10033801	D07-12	0.00	0.00	0	STD 3	13100	2899	29260	48.0	22	6	88	144	19	28.02	18	30	33	<5	<2	8	35	3	<2	<2	591	1.29
A10033802	D07-12	615.60	616.44	0.84	Core	42	55	230	<0.4	<2	55	<1	1	3	0.63	<2	<4	<5	<5	13	<2	4	121	<2	<2	409	13.14
A10033803	D07-12	625.72	626.73	1.01	Core	7	289	5191	<0.4	3	40	47	1	6	2.22	3	<4	<5	<5	14	<2	4	142	<2	<2	414	12.97
A10033804	D07-12	626.73	627.19	0.46	Core	11	2382	64020	0.9	7	37	378	5	16	7.91	17	<4	<5	<5	7	<2	14	115	2	<2	348	7.67
A10033805	D07-12	678.32	679.27	0.95	Core	7	22	257	<0.4	<2	17	<1	1	1	0.52	<2	<4	<5	<5	6	<2	<2	461	10	<2	1003	0.93

		Sampled Section				Ti	Al	Ca	Na	K	P	Ge	Hg	ASSAY					
Tag Number	Hole	From	To	Interval	Type	%	%	%	%	%	ppm	ppm	ppb	Pb(A) %	Zn(A) %	Ag(2) g/t	Cd(A) %	Fe(T) %	Ge(A) %
A10032451	D07-02	368.05	369.03	0.98	Core									0.02	0.06	13.2	<0.01	0.62	
A10032452	D07-02	369.03	369.71	0.68	Core									1.36	0.05	<0.4	<0.01	10.04	
A10032453	D07-02	369.71	370.67	0.96	Core									2.98	0.18	26.8	<0.01	25.12	
A10032454	D07-02	370.67	371.76	1.09	Core									0.42	0.11	4.1	<0.01	3.68	
A10032455	D07-02	371.76	372.79	1.03	Core	<.01	0.03	15.48	0.03	0.01	19	3	102						
A10032456	D07-02	372.79	374.11	1.32	Core	<.01	0.03	17.39	0.04	<.01	26	3	203						
A10032457	D07-02	374.11	375.05	0.94	Core	<.01	0.01	19.05	0.02	<.01	34	3	118						
A10032458	D07-02	391.04	391.97	0.93	Core	<.01	0.02	19.88	0.03	<.01	137	3	68	0.14	0.16	4.8	<0.01	2.02	
A10032459	D07-02	391.97	393.05	1.08	Core	<.01	0.03	20.68	0.03	<.01	83	3	97	0.12	0.37	1.2	<0.01	1.20	
A10032460	D07-02	393.05	394.89	1.84	Core	<.01	0.04	18.12	0.02	<.01	71	3	1381	0.69	5.11	6.5	0.04	6.51	0.002
A10032461	D07-02	394.89	396.02	1.13	Core	<.01	0.06	21.12	0.02	<.01	53	3	677	0.64	2.48	5.9	0.01	3.80	0.001
A10032462	D07-02	396.02	396.91	0.89	Core	<.01	0.02	22.70	0.02	<.01	25	3	213	0.03	0.75	<0.4	<0.01	1.20	
A10032463	D07-02	396.91	398.06	1.15	Core	<.01	0.02	20.63	0.02	<.01	71	3	426	0.22	1.50	2.1	0.01	6.55	
A10032464	D07-03	111.52	112.80	1.28	Core	<.01	0.23	0.02	0.04	0.23	121	N/A	64						
A10032465	D07-03	112.80	113.53	0.73	Core	<.01	0.36	0.02	0.03	0.15	476	N/A	53						
A10032466	D07-03	113.53	114.24	0.71	Core	0.02	0.89	0.06	0.04	0.09	1007	N/A	55						
A10032467	D07-03	116.33	117.03	0.7	Core	<.01	0.33	0.05	0.06	0.35	2675	N/A	56						
A10032468	n/a	0.00	0.00	0	Grab	<.01	0.33	1.32	0.11	0.01	140	N/A	<10						
A10032469	n/a	0.00	0.00	0	Blank	0.24	2.00	1.56	0.22	0.87	2925	N/A	<10						
A10032470	D07-04	96.32	96.88	0.56	Core	0.01	0.61	2.10	0.08	0.48	4818	N/A	145	<0.01	0.10	3.1	<0.005	1.65	
A10032471	D07-04	368.20	369.12	0.92	Core	<.01	0.17	20.81	0.06	0.12	406	N/A	<10	<0.01	<0.01	0.5	<0.005	1.49	
A10032472	D07-04	369.12	369.85	0.73	Core	<.01	0.04	18.73	0.06	0.03	42	N/A	70	0.10	0.56	1.0	0.005	1.75	
A10032473	D07-04	369.85	370.16	0.31	Core	<.01	0.02	19.37	0.05	0.01	46	N/A	1214	0.10	4.69	1.9	0.037	4.20	<0.001
A10032474	D07-04	370.16	370.95	0.79	Core	<.01	0.02	21.40	0.04	<.01	19	N/A	73	<0.01	0.31	0.5	0.007	0.70	
A10032475	D07-04	370.95	371.84	0.89	Core	<.01	0.01	24.07	0.05	<.01	18	N/A	14	0.01	0.02	0.6	<0.005	0.69	
A10032476	D07-04	371.84	373.20	1.36	Core	<.01	0.01	30.82	0.04	<.01	19	N/A	<10	<0.01	<0.01	<0.4	0.005	0.18	
A10032477	n/a	0.00	0.00	0	Grab	0.19	1.44	2.09	0.25	0.94	3036	N/A	<10	<0.01	<0.01	0.4	<0.005	3.65	
A10032478	D07-04	461.35	462.12	0.77	Core	<.01	0.03	16.51	0.06	0.01	1250	N/A	135	1.84	0.38	3.3	0.008	1.78	0.008
A10032479	D07-04	462.12	462.85	0.73	Core	<.01	0.05	17.10	0.06	0.02	2447	N/A	434	3.60	1.43	7.7	0.019	4.91	0.009
A10032480	D07-04	462.85	463.70	0.85	Core	<.01	0.04	19.17	0.05	0.03	656	N/A	997	4.24	3.73	13.3	0.045	2.59	0.005
A10032481	n/a	0.00	0.00	0	Grab	0.22	1.35	2.26	0.20	1.05	3127	N/A	<10	<0.01	<0.01	<0.4	0.005	3.45	
A10032482	D07-04	0.00	0.00	0	STD 1	0.05	0.70	1.61	0.10	0.16	489	N/A	457	0.96	1.26	369.9	0.020	7.09	
A10032483	D07-04	463.70	464.50	0.8	Core	<.01	0.04	24.52	0.05	0.02	739	N/A	155	0.15	0.67	1.7	0.013	1.86	
A10032484	D07-04	464.50	465.12	0.62	Core	<.01	0.05	24.45	0.05	0.03	141	N/A	19	0.04	0.04	0.6	0.007	0.93	
A10032485	D07-04	465.12	465.95	0.83	Core	<.01	0.06	20.50	0.05	0.02	3489	N/A	48	0.08	0.15	0.9	0.008	3.40	
A10032486	D07-04	465.95	467.20	1.25	Core	<.01	0.02	23.48	0.05	<.01	196	N/A	12	0.03	0.03	<0.4	0.007	1.20	
A10032487	D07-04	467.20	468.17	0.97	Core	<.01	0.08	21.37	0.05	0.04	1174	N/A	170	0.25	0.48	2.6	0.014	6.15	
A10032488	D07-04	468.17	469.05	0.88	Core	<.01	0.06	25.93	0.05	0.02	295	N/A	241	0.53	0.37	6.6	0.007	2.74	
A10032489	D07-04	469.05	469.96	0.91	Core	<.01	0.04	17.77	0.05	0.02	60	N/A	79	0.80	0.11	1.1	0.010	1.33	
A10032490	D07-04	469.96	471.00	1.04	Core	<.01	0.06	17.37	0.05	0.02	111	N/A	88	0.37	0.11	3.6	0.011	2.20	
A10032491	D07-04	471.00	471.42	0.42	Core	0.28	2.00	6.39	0.11	0.85	3242	N/A	17	0.06	0.01	0.7	0.008	4.82	
A10032492	D07-04	0.00	0.00	0	Grab	0.20	1.54	1.75	0.20	0.61	3645	N/A	<10	<0.01	<0.01	<0.4	0.008	3.29	
A10032493	D07-04	0.00	0.00	0	STD 3	0.01	0.64	0.78	0.06	0.06	82	N/A	581	0.28	2.86	61.2	0.018	32.35	0.016
A10032494	D07-04	471.42	471.97	0.55	Core	<.01	0.06	17.30	0.05	0.02	1046	N/A	305	0.87	0.47	8.6	0.016	2.50	
A10032495	D07-04	471.97	472.72	0.75	Core	0.03	0.29	20.51	0.06	0.10	1340	N/A	406	0.68	0.69	7.4	0.017	4.71	
A10032496	D07-04	472.72	473.77	1.05	Core	<.01	0.06	21.45	0.04	0.02	2836	N/A	389	0.63	0.80	10.0	0.019	3.70	
A10032497	D07-04	473.77	474.70	0.93	Core	<.01	0.04	21.22	0.05	0.01	654	N/A	192	0.36	0.50	4.8	0.009	2.03	
A10032498	D07-04	474.70	475.65	0.95	Core	0.01	0.15	20.46	0.04	0.06	352	N/A	32	0.03	0.11	<0.4	0.005	0.67	
A10032499	D07-04	475.65	476.50	0.85	Core	0.06	0.51	20.26	0.05	0.21	1059	N/A	30	0.02	0.08	<0.4	<0.005	1.18	
A10032500	D07-04	476.50	477.32	0.82	Core	<.01	0.02	21.68	0.04	<.01	224	N/A	21	<0.01	0.08	<0.4	0.005	0.36	
A10032501	D07-04	501.53	502.38	0.85	Core	<.01	0.02	19.70	0.04	0.01	97	N/A	16	<0.01	0.03	<0.4	0.009	0.53	

		Sampled Section				Ti	Al	Ca	Na	K	P	Ge	Hg	ASSAY					
Tag Number	Hole	From	To	Interval	Type	%	%	%	%	%	ppm	ppm	ppb	Pb(A) %	Zn(A) %	Ag(2) g/t	Cd(A) %	Fe(T) %	Ge(A) %
A10032502	D07-04	502.38	502.96	0.58	Core	<.01	0.08	17.97	0.04	0.03	300	N/A	110	0.14	0.81	2.2	0.017	4.13	
A10032503	D07-04	502.96	503.81	0.85	Core	<.01	0.18	15.32	0.05	0.09	156	N/A	13	<0.01	<0.01	<0.4	0.009	1.99	
A10032504	D07-04	506.47	507.37	0.9	Core	<.01	0.04	26.69	0.04	0.02	32	N/A	<10	<0.01	<0.01	<0.4	0.011	0.33	
A10032505	D07-04	507.37	507.86	0.49	Core	<.01	0.03	18.07	0.03	0.01	43	N/A	3581	0.14	10.97	2.9	0.113	4.98	0.003
A10032506	D07-04	507.86	508.82	0.96	Core	<.01	0.06	28.22	0.03	0.01	52	N/A	237	0.01	0.64	<0.4	0.016	0.95	
A10032507	D07-08	392.97	393.97	1	Core	<.01	0.08	22.07	0.04	0.03	524		<10						
A10032508	D07-08	393.97	395.00	1.03	Core	0.02	1.24	5.89	0.07	0.31	510		12						
A10032509	D07-08	395.00	396.03	1.03	Core	0.05	1.51	4.73	0.06	0.54	852		<10						
A10032510	D07-08	396.03	396.96	0.93	Core	0.02	1.17	12.32	0.06	0.38	1127		<10						
A10032511	D07-08	396.96	398.00	1.04	Core	<.01	0.75	19.92	0.05	0.12	1423		<10						
A10032512	D07-08	398.00	399.02	1.02	Core	<.01	0.12	22.17	0.05	0.06	351		<10						
A10032513	D07-08	399.02	399.97	0.95	Core	<.01	0.07	23.15	0.05	0.02	148		<10						
A10032514	D07-08	399.97	401.00	1.03	Core	<.01	0.07	22.32	0.02	0.02	379		<10						
A10032515	D07-08	401.00	401.99	0.99	Core	<.01	0.12	22.40	0.02	0.04	730		<10						
A10032516	D07-08	401.99	404.00	2.01	Core	0.03	1.02	8.55	0.03	0.37	578		<10						
A10032517	D07-08	404.00	404.97	0.97	Core	0.04	1.09	2.75	0.03	0.57	629		<10						
A10032518	D07-08	404.97	406.21	1.24	Core	<.01	0.38	10.10	0.03	0.16	1893		<10						
A10032519	D07-08	406.21	407.00	0.79	Core	0.04	1.05	2.56	0.03	0.55	629		<10						
A10032520	D07-08	407.00	407.63	0.63	Core	<.01	0.30	3.00	0.04	0.10	1449		11						
A10032521	D07-08	407.63	408.98	1.35	Core	<.01	0.41	1.90	0.03	0.19	1693		<10						
A10032522	D07-08	408.98	410.00	1.02	Core	<.01	0.50	1.36	0.04	0.22	2890		<10						
A10032523	D07-08	410.00	411.23	1.23	Core	0.02	0.82	0.61	0.03	0.49	1084		<10						
A10032524	D07-08	411.23	412.08	0.85	Core	0.01	0.66	0.85	0.03	0.41	772		<10						
A10032525	D07-08	412.08	413.00	0.92	Core	0.01	0.68	0.95	0.03	0.34	863		<10						
A10032526	D07-08	413.00	413.07	0.07	Core	<.01	0.55	1.21	0.04	0.35	522		<10						
A10032527	D07-08	413.07	413.98	0.91	Core	<.01	0.60	1.06	0.03	0.34	616		<10						
A10032528	D07-08	413.98	414.97	0.99	Core	0.01	0.61	1.22	0.03	0.37	603		<10						
A10032529	D07-08	414.97	416.99	2.02	Core	0.09	1.08	0.73	0.04	0.70	868		<10						
A10032530	D07-08	416.99	418.02	1.03	Core	0.13	1.11	0.63	0.03	0.79	656		<10						
A10032531	D07-08	418.02	419.00	0.98	Core	0.13	1.20	0.73	0.04	0.85	664		<10						
A10032532	D07-08	419.00	419.96	0.96	Core	0.08	1.08	0.49	0.04	0.66	1056		<10						
A10032533	D07-08	419.96	420.90	0.94	Core	0.09	1.17	0.66	0.04	0.80	1035		<10						
A10032534	D07-08	420.90	422.00	1.1	Core	0.06	1.03	0.56	0.04	0.64	762		<10						
A10032535	D07-07	474.15	475.15	1	Core	<.01	0.39	0.57	0.04	0.28	483		<10						
A10032536	D07-07	475.15	476.20	1.05	Core	<.01	0.49	1.17	0.04	0.27	827		<10						
A10032537	D07-07	476.20	477.32	1.12	Core	<.01	0.56	1.87	0.03	0.35	1288		<10						
A10032538	D07-07	477.32	478.30	0.98	Core	0.01	0.72	1.52	0.03	0.42	1435		<10						
A10032539	D07-07	510.38	511.38	1	Core	<.01	0.66	0.72	0.04	0.33	1111		<10						
A10032540	D07-07	511.38	512.38	1	Core	<.01	0.31	1.68	0.03	0.20	783		<10						
A10032541	D07-07	512.38	513.42	1.04	Core	<.01	0.55	0.88	0.04	0.38	762		<10						
A10032542	D07-07	589.00	590.09	1.09	Core	<.01	0.01	24.90	0.02	<.01	38		10						
A10032543	D07-07	590.09	591.10	1.01	Core	<.01	0.04	22.43	0.02	0.03	56		12						
A10032544	D07-07	591.10	592.12	1.02	Core	<.01	0.01	25.82	0.02	<.01	20		12						
A10032545	D07-07	0.00	0.00	0	STD 7	<.01	0.50	0.39	0.03	0.01	56		715						
A10032546	D07-07	773.46	775.00	1.54	Core	<.01	0.08	20.17	0.02	0.03	2193		39						
A10032547	D07-07	775.00	776.47	1.47	Core	<.01	0.04	21.47	0.02	0.01	1142		30						
A10032548	D07-07	777.24	778.75	1.51	Core	<.01	0.03	20.81	0.02	0.01	310		29						
A10032549	D07-07	778.75	780.19	1.44	Core	<.01	0.03	22.13	0.02	<.01	342		14						
A10032550	D07-07	780.19	781.81	1.62	Core	<.01	0.02	23.15	0.02	<.01	325		14						
A10032551	D07-07	781.81	783.32	1.51	Core	<.01	0.01	24.06	0.02	<.01	153		17						
A10032552	D07-07	783.32	784.51	1.19	Core	<.01	0.06	16.87	0.02	0.01	809		12						

		Sampled Section				Ti	Al	Ca	Na	K	P	Ge	Hg	ASSAY					
Tag Number	Hole	From	To	Interval	Type	%	%	%	%	%	ppm	ppm	ppb	Pb(A) %	Zn(A) %	Ag(2) g/t	Cd(A) %	Fe(T) %	Ge(A) %
A10032553	D07-07	784.51	786.15	1.64	Core	<.01	0.17	22.70	0.02	0.06	5634		14						
A10032554	D07-07	331.25	332.84	1.59	Core	<.01	0.14	23.70	0.02	<.01	324	N/A	29						
A10032555	D07-07	332.51	332.84	0.33	Core	<.01	0.06	30.59	0.02	<.01	126	N/A	13						
A10032556	D07-07	332.84	334.66	1.82	Core	<.01	0.07	22.75	0.02	<.01	41	N/A	106						
A10032557	D07-07	334.66	336.03	1.37	Core	<.01	0.10	29.48	0.02	0.01	77	N/A	<10						
A10032558	D07-07	336.03	337.26	1.23	Core	<.01	0.06	23.59	0.02	<.01	35	N/A	<10						
A10032559	D07-07	337.26	338.69	1.43	Core	<.01	0.02	31.30	0.02	<.01	88	N/A	10						
A10032560	Hike	0.00	0.00	0	Float	0.03	1.84	1.66	0.14	0.07	304	N/A	<10						
A10032561	D07-11	175.29	176.29	1	Core	<.01	0.37	8.14	0.03	0.18	372	N/A	<10						
A10032562	D07-11	176.29	177.21	0.92	Core	<.01	0.02	1.62	0.02	<.01	24	N/A	<10						
A10032563	D07-11	177.21	178.36	1.15	Core	<.01	0.32	9.86	0.02	0.19	347	N/A	<10						
A10032564	D07-11	334.00	335.00	1	Core	<.01	0.01	20.23	0.01	<.01	16	N/A	124						
A10032565	D07-11	335.00	336.00	1	Core	<.01	0.08	22.51	0.01	0.01	51	N/A	15						
A10032566	D07-11	336.00	337.00	1	Core	<.01	0.09	23.54	0.01	<.01	96	N/A	139						
A10032567	D07-11	337.00	338.00	1	Core	<.01	0.06	21.21	0.01	<.01	25	N/A	28						
A10032568	D07-11	338.00	338.89	0.89	Core	<.01	0.03	30.79	0.01	<.01	33	N/A	18						
A10032569	D07-10	478.66	479.77	1.11	Core	<.01	0.31	5.51	0.01	0.16	5904	N/A	113						
A10032570	D07-10	479.77	480.83	1.06	Core	<.01	0.23	2.90	0.01	0.11	3194	N/A	132						
A10032571	D07-10	480.83	482.00	1.17	Core	0.05	0.55	2.29	0.03	0.24	2758	N/A	129						
A10032572	D07-10	482.27	483.41	1.14	Core	<.01	0.14	1.70	0.01	0.07	2149	N/A	75						
A10032573	D07-10	483.41	484.50	1.09	Core	<.01	0.19	2.24	0.01	0.10	1587	N/A	169						
A10032574	D07-10	484.50	485.55	1.05	Core	<.01	0.13	1.40	0.01	0.07	1031	N/A	75						
A10032575	D07-10	503.96	505.15	1.19	Core	0.02	0.95	3.74	0.01	0.46	5265	N/A	132						
A10032576	D07-11	344.83	345.64	0.81	Core	<.01	0.15	28.46	0.01	0.01	356	N/A	<10						
A10032577	D07-11	345.64	346.76	1.12	Core	<.01	2.29	1.80	0.02	0.13	454	N/A	<10						
A10032578	D07-11	346.76	347.85	1.09	Core	<.01	2.21	0.30	0.02	0.12	379	N/A	<10						
A10032579	D07-11	366.38	366.86	0.48	Core	<.01	0.02	24.95	0.01	<.01	38	N/A	11						
A10032580	D07-11	418.67	419.71	1.04	Core	<.01	0.02	34.22	0.01	<.01	84	N/A	40						
A10032581	D07-11	419.71	420.98	1.27	Core	<.01	0.02	32.00	0.01	<.01	45	N/A	29						
A10032582	D07-11	420.98	422.00	1.02	Core	<.01	0.01	27.04	0.01	<.01	58	N/A	41						
A10032583	D07-11	422.00	423.11	1.11	Core	<.01	0.01	20.81	0.01	<.01	80	N/A	50						
A10032584	D07-11	423.11	424.00	0.89	Core	<.01	0.02	14.63	0.01	<.01	92	N/A	26						
A10032585	D07-11	424.00	425.00	1	Core	<.01	0.01	18.71	0.01	<.01	79	N/A	46						
A10032586	D07-11	425.00	426.07	1.07	Core	<.01	0.01	20.92	0.01	<.01	67	N/A	17						
A10032587	D07-11	426.07	427.11	1.04	Core	<.01	0.01	19.93	0.01	<.01	83	N/A	10						
A10032588	D07-11	427.11	428.00	0.89	Core	<.01	0.01	20.88	0.01	<.01	268	N/A	38						
A10032589	D07-11	428.00	429.00	1	Core	<.01	0.01	17.06	0.01	<.01	78	N/A	21						
A10032590	D07-11	429.00	430.06	1.06	Core	<.01	0.01	17.75	0.01	<.01	147	N/A	16						
A10032591	D07-11	430.06	431.43	1.37	Core	<.01	0.01	20.77	0.01	<.01	473	N/A	13						
A10032592	D07-11	0.00	0.00	0	STD 1	0.04	0.90	1.47	0.05	0.11	473	N/A	448						
A10032593	D07-11	432.00	433.00	1	Core	0.21	1.99	1.70	0.14	0.66	3482	N/A	<10						
A10032594	D07-11	433.00	434.33	1.33	Core	<.01	0.03	19.45	0.01	<.01	164	N/A	<10						
A10032595	D07-11	434.33	435.00	0.67	Core	<.01	0.02	18.87	0.03	<.01	248	N/A	16						
A10032596	D07-11	435.00	436.00	1	Core	<.01	0.01	20.68	0.03	<.01	211	N/A	19						
A10032597	D07-11	436.00	437.79	1.79	Core	<.01	0.01	21.72	0.04	<.01	110	N/A	20						
A10032598	D07-11	437.79	438.84	1.05	Core	<.01	0.03	20.94	0.03	0.01	450	N/A	15						
A10032599	D07-11	438.84	440.00	1.16	Core	<.01	0.02	22.11	0.03	<.01	126	N/A	14						
A10032600	D07-11	440.00	440.95	0.95	Core	<.01	0.02	21.77	0.03	0.01	55	N/A	24						
A10032601	D07-11	440.95	442.00	1.05	Core	<.01	0.01	21.35	0.02	<.01	37	N/A	<10						
A10032602	D07-11	442.00	443.00	1	Core	<.01	0.05	12.97	0.03	0.01	1500	N/A	31						
A10032603	D07-11	443.00	444.00	1	Core	<.01	0.03	19.70	0.03	0.01	81	N/A	<10						

		Sampled Section				Ti	Al	Ca	Na	K	P	Ge	Hg	ASSAY					
Tag Number	Hole	From	To	Interval	Type	%	%	%	%	%	ppm	ppm	ppb	Pb(A) %	Zn(A) %	Ag(2) g/t	Cd(A) %	Fe(T) %	Ge(A) %
A10032604	D07-11	444.00	445.10	1.1	Core	<.01	0.01	20.52	0.03	<.01	46	N/A	<10						
A10032605	D07-11	445.10	446.21	1.11	Core	<.01	0.04	16.42	0.03	0.01	1113	N/A	24						
A10032606	D07-11	446.21	447.16	0.95	Core	<.01	0.02	19.12	0.03	0.01	409	N/A	21						
A10032607	D07-11	447.16	448.34	1.18	Core	<.01	0.02	21.40	0.03	<.01	394	N/A	24						
A10032608	D07-11	0.00	0.00	0	STD 3	0.01	0.61	0.84	0.03	0.05	<10	N/A	611						
A10032609	D07-11	449.52	450.71	1.19	Core	<.01	0.01	18.63	0.04	<.01	111	N/A	12						
A10032610	D07-11	450.71	451.76	1.05	Core	<.01	0.01	19.82	0.03	<.01	231	N/A	<10						
A10032611	D07-11	451.76	452.87	1.11	Core	<.01	0.02	19.13	0.03	<.01	261	N/A	40						
A10032612	D07-11	452.87	453.87	1	Core	<.01	0.02	20.36	0.02	0.01	418	N/A	17						
A10032613	D07-11	455.00	456.05	1.05	Core	<.01	0.01	19.63	0.03	<.01	97	N/A	14						
A10032614	D07-11	456.05	457.00	0.95	Core	<.01	0.01	18.65	0.03	<.01	69	N/A	<10						
A10032615	D07-11	457.00	458.00	1	Core	<.01	0.01	19.36	0.03	<.01	67	N/A	<10						
A10032616	D07-11	458.00	458.94	0.94	Core	<.01	0.02	18.87	0.03	<.01	104	N/A	<10						
A10032617	D07-11	458.94	459.89	0.95	Core	<.01	0.02	21.15	0.03	<.01	607	N/A	14						
A10032618	D07-11	459.89	461.00	1.11	Core	<.01	0.02	20.84	0.03	<.01	191	N/A	14						
A10032619	D07-11	461.00	462.00	1	Core	<.01	0.01	19.98	0.03	<.01	86	N/A	19						
A10032620	D07-11	462.00	463.00	1	Core	<.01	0.01	18.90	0.03	<.01	38	N/A	72						
A10032621	D07-11	463.00	464.00	1	Core	<.01	0.01	19.38	0.03	<.01	64	N/A	50						
A10032622	D07-11	464.00	465.07	1.07	Core	<.01	0.02	19.65	0.03	<.01	82	N/A	93						
A10032623	D07-11	465.07	466.43	1.36	Core	<.01	0.02	19.70	0.03	<.01	113	N/A	208						
A10032624	D07-11	466.43	467.82	1.39	Core	<.01	0.01	14.89	0.03	<.01	189	N/A	88						
A10032625	D07-11	467.82	469.86	2.04	Core	<.01	0.03	18.70	0.03	0.01	826	N/A	76						
A10032626	D07-11	469.86	471.00	1.14	Core	<.01	0.01	19.52	0.03	<.01	389	N/A	283						
A10032627	D07-11	471.00	472.10	1.1	Core	<.01	0.01	19.97	0.03	<.01	363	N/A	30						
A10032628	D07-11	472.10	473.00	0.9	Core	<.01	0.01	21.04	0.03	<.01	239	N/A	<10						
A10032629	D07-11	473.00	474.10	1.1	Core	<.01	0.01	20.94	0.04	<.01	44	N/A	11						
A10032630	D07-11	474.10	475.25	1.15	Core	<.01	0.01	21.11	0.04	<.01	38	N/A	<10						
A10032631	D07-11	475.25	476.29	1.04	Core	<.01	0.01	19.87	0.03	<.01	31	N/A	<10						
A10032632	D07-11	476.29	477.34	1.05	Core	<.01	0.01	19.54	0.03	<.01	36	N/A	<10						
A10032633	D07-11	477.34	478.83	1.49	Core	<.01	0.02	20.03	0.03	<.01	130	N/A	13						
A10032634	D07-11	0.00	0.00	0	Blank	0.24	1.84	1.80	0.17	0.78	2899	N/A	<10						
A10032635	D07-11	479.80	480.80	1	Core	<.01	0.02	19.77	0.03	<.01	97	N/A	<10						
A10032636	D07-11	480.80	482.00	1.2	Core	<.01	0.04	20.01	0.04	0.01	132	N/A	15						
A10032637	D07-11	482.00	483.00	1	Core	<.01	0.02	19.89	0.04	<.01	59	N/A	152						
A10032638	D07-11	0.00	0.00	0	Blank	0.19	1.54	1.40	0.13	0.60	2782	N/A	11						
A10032639	D07-11	0.00	0.00	0	STD 7	0.01	0.48	0.38	0.04	0.01	<10	N/A	490						
A10032640	D07-11	485.00	485.98	0.98	Core	<.01	0.02	18.36	0.05	<.01	19	N/A	<10						
A10032641	D07-11	485.98	487.10	1.12	Core	<.01	0.02	19.15	0.04	<.01	12	N/A	<10						
A10032642	D07-11	487.10	488.00	0.9	Core	<.01	0.02	20.34	0.04	<.01	16	N/A	<10						
A10032643	D07-11	488.00	489.00	1	Core	<.01	0.03	20.02	0.04	0.01	20	N/A	<10						
A10032644	D07-11	489.00	490.00	1	Core	<.01	0.02	20.07	0.04	0.01	20	N/A	<10						
A10032645	D07-11	490.00	491.00	1	Core	<.01	0.03	19.86	0.04	0.01	25	N/A	<10						
A10032646	D07-11	491.00	492.06	1.06	Core	<.01	0.02	18.79	0.04	0.01	17	N/A	<10						
A10032647	D07-11	492.06	493.00	0.94	Core	<.01	0.02	19.62	0.04	0.01	19	N/A	<10						
A10032648	D07-11	493.00	494.00	1	Core	<.01	0.01	19.65	0.03	<.01	37	N/A	<10						
A10032649	D07-11	0.00	0.00	0	STD 1	0.04	0.93	1.38	0.08	0.11	471	N/A	490						
A10032650	D07-11	453.87	455.00	1.13	Core	<.01	0.04	18.56	0.03	0.01	1524	N/A	24						
A10032651	D07-11	494.00	494.99	0.99	Core	<.01	0.02	20.90	0.03	<.01	71	N/A	47						
A10032652	D07-11	494.99	496.00	1.01	Core	<.01	0.01	19.60	0.03	<.01	22	N/A	<10						
A10032653	D07-11	496.00	497.00	1	Core	<.01	0.01	18.93	0.04	<.01	<10	N/A	<10						
A10032654	D07-11	497.00	498.00	1	Core	<.01	0.01	18.98	0.03	<.01	17	N/A	<10						

		Sampled Section				Ti	Al	Ca	Na	K	P	Ge	Hg	ASSAY					
Tag Number	Hole	From	To	Interval	Type	%	%	%	%	%	ppm	ppm	ppb	Pb(A) %	Zn(A) %	Ag(2) g/t	Cd(A) %	Fe(T) %	Ge(A) %
A10032655	D07-11	498.00	499.20	1.2	Core	<.01	0.01	18.60	0.03	<.01	19	N/A	<10						
A10032656	D07-11	499.20	500.15	0.95	Core	<.01	0.01	18.79	0.03	<.01	23	N/A	<10						
A10032657	D07-11	500.15	501.15	1	Core	<.01	0.01	20.45	0.04	<.01	28	N/A	18						
A10032658	D07-11	501.15	502.03	0.88	Core	<.01	0.02	20.01	0.03	<.01	37	N/A	126						
A10032659	D07-11	502.03	503.50	1.47	Core	<.01	0.01	20.09	0.03	<.01	24	N/A	24						
A10032660	D07-11	0.00	0.00	0	STD 3	0.01	0.60	0.80	0.04	0.04	<10	N/A	613						
A10032661	D07-11	504.50	505.00	0.5	Core	<.01	0.05	15.07	0.02	<.01	22	N/A	175	0.26	4.64	0.061	3.9		0.003
A10032662	D07-11	0.00	0.00	0	Blank	0.23	1.49	2.07	0.11	0.54	3062	N/A	29						
A10032663	D07-11	506.10	506.73	0.63	Core	<.01	0.02	20.23	0.05	<.01	24	N/A	<10						
A10032664	D07-11	506.73	508.59	1.86	Core	<.01	0.02	19.15	0.03	<.01	48	N/A	143						
A10032665	D07-11	508.59	509.47	0.88	Core	<.01	0.02	19.45	0.03	<.01	46	N/A	16						
A10032666	D07-11	0.00	0.00	0	Blank	0.23	2.07	2.01	0.18	0.73	3473	N/A	<10						
A10032667	D07-11	511.67	512.75	1.08	Core	<.01	0.04	20.73	0.03	0.02	56	N/A	<10						
A10032668	D07-11	512.75	514.39	1.64	Core	<.01	0.02	20.04	0.03	0.01	29	N/A	<10						
A10032669	D07-11	514.39	515.81	1.42	Core	<.01	0.02	21.97	0.02	<.01	35	N/A	<10						
A10032670	D07-11	515.81	516.67	0.86	Core	<.01	0.03	21.52	0.03	0.01	63	N/A	<10						
A10032671	D07-11	516.67	518.00	1.33	Core	<.01	0.05	18.44	0.03	0.02	131	N/A	106						
A10032672	D07-11	0.00	0.00	0	STD 7	<.01	0.52	0.44	0.03	0.01	<10	N/A	335						
A10032673	D07-11	519.06	520.06	1	Core	<.01	0.02	19.75	0.03	0.01	20	N/A	<10						
A10032674	D07-11	520.06	521.00	0.94	Core	<.01	0.04	23.12	0.03	0.02	16	N/A	<10						
A10032675	D07-11	521.00	522.00	1	Core	<.01	0.03	22.17	0.03	0.01	10	N/A	<10						
A10032676	D07-11	522.00	523.00	1	Core	<.01	0.03	22.28	0.03	0.01	40	N/A	<10						
A10032677	D07-11	523.00	524.10	1.1	Core	<.01	0.07	26.12	0.03	0.03	51	N/A	<10						
A10032678	D07-11	527.87	528.55	0.68	Core	<.01	0.11	18.95	0.03	0.06	95	N/A	<10						
A10032679	D07-11	529.36	530.00	0.64	Core	<.01	0.06	28.88	0.03	0.03	50	N/A	106	<0.01	1.96	0.016	1.2		0.001
A10032680	D07-11	530.00	530.71	0.71	Core	<.01	0.04	22.75	0.03	0.02	38	N/A	17						
A10032681	D07-11	530.71	531.64	0.93	Core	<.01	0.04	31.35	0.03	0.02	49	N/A	287	<0.01	4.44	0.046	4.1		0.005
A10032682	D07-11	0.00	0.00	0	Blank	0.20	1.68	1.75	0.11	0.58	2882	N/A	15						
A10032683	D07-11	533.00	534.00	1	Core	<.01	0.03	20.25	0.03	0.01	28	N/A	<10						
A10032684	D07-11	534.00	535.09	1.09	Core	<.01	0.02	22.69	0.03	0.01	21	N/A	<10						
A10032685	D07-11	535.09	536.00	0.91	Core	<.01	0.03	21.27	0.03	0.01	29	N/A	43						
A10032686	D07-11	536.00	537.03	1.03	Core	<.01	0.02	21.97	0.03	0.01	19	N/A	<10						
A10032687	D07-11	537.03	538.14	1.11	Core	<.01	0.03	20.52	0.03	0.01	20	N/A	<10						
A10032688	D07-11	538.14	539.78	1.64	Core	<.01	0.03	20.39	0.03	0.01	26	N/A	<10						
A10032689	D07-11	539.78	540.24	0.46	Core	<.01	0.03	19.43	0.03	0.01	26	N/A	<10						
A10032690	D07-11	540.24	541.00	0.76	Core	<.01	0.03	19.95	0.03	0.01	33	N/A	<10						
A10032691	D07-11	541.00	543.50	2.5	Core	<.01	0.04	20.95	0.03	0.01	25	N/A	<10						
A10032692	D07-11	543.50	545.00	1.5	Core	<.01	0.03	19.89	0.03	0.01	27	N/A	<10						
A10032693	D07-11	545.00	546.50	1.5	Core	<.01	0.02	21.00	0.03	0.01	22	N/A	<10						
A10032694	D07-11	546.50	548.00	1.5	Core	<.01	0.04	20.85	0.02	0.02	22	N/A	<10						
A10032695	D07-11	548.00	548.89	0.89	Core	<.01	0.04	20.81	0.03	0.02	33	N/A	<10						
A10032696	D07-11	548.89	549.74	0.85	Core	<.01	0.05	21.19	0.03	0.02	54	N/A	<10						
A10032697	D07-11	549.74	550.65	0.91	Core	<.01	0.09	22.05	0.03	0.05	226	N/A	<10						
A10032698	D07-11	0.00	0.00	0	STD 1	0.05	1.02	1.60	0.07	0.11	516	N/A	319						
A10032699	D07-11	551.65	552.64	0.99	Core	<.01	0.23	29.62	0.03	0.12	560	N/A	<10						
A10032700	D07-11	554.29	554.79	0.5	Core	0.06	0.62	2.15	0.03	0.40	913	N/A	<10						
A10032701	D07-11	580.50	581.00	0.5	Core	0.22	1.65	1.76	0.03	1.04	1887	N/A	<10						
A10032702	D07-11	478.83	479.80	0.97	Core	<.01	0.02	20.23	0.03	<.01	151	N/A	<10						
A10032703	D07-11	483.00	484.00	1	Core	<.01	0.03	20.47	0.03	0.01	39	N/A	<10						
A10032704	D07-11	505.00	506.10	1.1	Core	<.01	0.01	21.25	0.03	<.01	13	N/A	18						
A10032705	D07-11	510.08	511.67	1.59	Core	<.01	0.05	19.92	0.03	0.02	77	N/A	<10						

		Sampled Section				Ti	Al	Ca	Na	K	P	Ge	Hg	ASSAY					
Tag Number	Hole	From	To	Interval	Type	%	%	%	%	%	ppm	ppm	ppb	Pb(A) %	Zn(A) %	Ag(2) g/t	Cd(A) %	Fe(T) %	Ge(A) %
A10032706	D07-11	531.64	533.00	1.36	Core	<.01	0.07	20.52	0.03	0.04	43	N/A	10						
A10032707	D07-11	431.43	432.00	0.57	Core	<.01	0.03	23.19	0.03	<.01	516	N/A	19						
A10032708	D07-11	448.34	449.57	1.23	Core	<.01	0.01	23.45	0.03	<.01	86	N/A	<10						
A10032709	D07-11	484.00	485.00	1	Core	<.01	0.03	21.75	0.03	<.01	39	N/A	<10						
A10032710	D07-11	470.00	471.00	1	Core	<.01	0.02	21.87	0.04	<.01	469	N/A	<10						
A10032711	D07-11	503.50	504.50	1	Core	<.01	0.01	21.40	0.03	<.01	24	N/A	<10						
A10032712	D07-11	518.00	519.06	1.06	Core	<.01	0.01	20.86	0.03	<.01	21	N/A	<10						
A10032713	D07-11	550.65	551.65	1	Core	0.01	0.35	15.03	0.03	0.20	435	N/A	<10						
A10032714	D07-11	432.00	433.00	1	Core	<.01	0.01	19.37	0.03	<.01	229	N/A	<10						
A10032715	D07-10	0.00	0.00	0	STD 3	0.01	0.68	0.80	0.05	0.06	<10	N/A	557						
A10032716	D07-10	687.15	688.08	0.93	Core	<.01	0.36	0.72	0.05	0.22	2877	N/A	11						
A10032717	D07-10	688.08	689.10	1.02	Core	0.02	0.58	0.63	0.05	0.43	2105	N/A	<10						
A10032718	D07-10	689.10	690.15	1.05	Core	<.01	0.49	0.89	0.05	0.33	3115	N/A	<10						
A10032719	D07-10	690.15	691.29	1.14	Core	<.01	0.48	0.60	0.06	0.33	2496	N/A	<10						
A10032720	D07-10	693.95	695.08	1.13	Core	<.01	0.21	0.36	0.04	0.15	1596	N/A	<10						
A10032721	D07-10	695.56	696.06	0.5	Core	<.01	0.54	0.55	0.04	0.39	1366	N/A	<10						
A10032722	D07-10	697.19	697.67	0.48	Core	<.01	0.25	0.34	0.04	0.17	850	N/A	<10						
A10032723	D07-10	697.67	698.66	0.99	Core	<.01	0.33	0.34	0.05	0.21	861	N/A	<10						
A10032724	D07-10	701.95	702.10	0.15	Core	0.12	1.36	0.16	0.04	0.96	721	N/A	<10						
A10032725	D07-10	708.60	709.34	0.74	Core	0.15	1.66	0.20	0.05	0.95	603	N/A	<10						
A10032726	D07-10	712.15	712.84	0.69	Core	0.01	1.02	0.32	0.06	0.58	743	N/A	<10						
A10032727	D07-10	0.00	0.00	0	Blank	0.28	2.84	2.08	0.28	1.01	4140	N/A	12						
A10032728	D07-10	712.84	713.51	0.67	Core	0.02	0.97	0.64	0.05	0.56	662	N/A	<10						
A10032729	D07-10	713.51	714.01	0.5	Core	<.01	0.40	0.83	0.05	0.31	747	N/A	<10						
A10032730	D07-10	0.00	0.00	0	STD 1	0.05	1.02	1.45	0.10	0.16	487	N/A	576						
A10032731	D07-10	714.29	715.06	0.77	Core	<.01	0.76	1.15	0.05	0.49	771	N/A	<10						
A10032732	D07-10	715.06	716.07	1.01	Core	<.01	0.80	1.02	0.05	0.52	1203	N/A	<10						
A10032733	D07-10	716.67	717.10	0.43	Core	<.01	0.58	1.20	0.05	0.42	926	N/A	<10						
A10032734	D07-10	717.10	718.11	1.01	Core	<.01	0.30	1.12	0.04	0.23	2035	N/A	<10						
A10032735	D07-10	718.11	719.16	1.05	Core	<.01	0.42	0.92	0.04	0.33	1749	N/A	<10						
A10032736	D07-10	719.16	720.20	1.04	Core	0.01	0.49	1.11	0.05	0.27	2174	N/A	<10						
A10032737	D07-10	720.20	721.16	0.96	Core	0.01	0.44	0.94	0.05	0.28	2132	N/A	<10						
A10032738	D07-10	721.16	722.26	1.1	Core	<.01	0.42	1.04	0.05	0.31	2211	N/A	<10						
A10032739	D07-10	722.26	723.29	1.03	Core	<.01	0.53	1.35	0.05	0.30	3621	N/A	<10						
A10032740	D07-10	723.29	724.20	0.91	Core	<.01	0.54	1.36	0.05	0.32	3267	N/A	<10						
A10032741	D07-10	747.89	748.59	0.7	Core	<.01	0.71	1.19	0.05	0.40	1268	N/A	<10						
A10032742	D07-10	755.05	756.23	1.18	Core	<.01	0.81	0.94	0.05	0.39	915	N/A	<10						
A10032743	D07-10	759.89	760.72	0.83	Core	0.06	1.21	0.48	0.06	0.67	766	N/A	<10						
A10032744	D07-10	766.01	766.47	0.46	Core	<.01	0.73	1.27	0.05	0.35	635	N/A	<10						
A10032745	D07-10	0.00	0.00	0	STD 7	0.01	0.57	0.42	0.04	0.02	<10	N/A	617						
A10032746	D07-10	736.50	737.07	0.57	Core	<.01	0.54	1.42	0.05	0.36	4136	N/A	<10						
A10032747	D07-10	786.00	787.11	1.11	Core	<.01	0.65	0.46	0.05	0.40	951	N/A	<10						
A10032748	D07-10	787.11	788.21	1.1	Core	<.01	0.79	0.46	0.05	0.34	1377	N/A	<10						
A10032749	D07-10	788.21	789.31	1.1	Core	<.01	0.78	1.89	0.05	0.38	4470	N/A	<10						
A10032750	D07-12	151.40	152.08	0.68	Core	<.01	0.65	1.92	0.05	0.26	336	N/A	<10						
A10033701	D07-12	243.34	243.74	0.4	Core	<.01	0.34	11.64	0.06	0.16	277	N/A	<10						
A10033702	D07-12	243.74	244.68	0.94	Core	<.01	0.31	9.78	0.05	0.25	329	N/A	<10						
A10033703	D07-12	414.73	415.63	0.9	Core	<.01	0.02	19.05	0.05	<.01	48	N/A	19						
A10033704	D07-12	419.00	420.00	1	Core	<.01	0.02	21.31	0.05	<.01	38	N/A	19						
A10033705	D07-12	420.00	421.00	1	Core	<.01	0.02	19.59	0.05	<.01	60	N/A	97						
A10033706	D07-12	421.00	422.00	1	Core	<.01	0.01	20.80	0.05	<.01	17	N/A	39						

Tag Number	Hole	Sampled Section From	To	Interval	Type	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb	ASSAY Pb(A) %	Zn(A) %	Ag(2) g/t	Cd(A) %	Fe(T) %	Ge(A) %
A10033707	D07-12	424.00	425.00	1	Core	<.01	0.01	18.29	0.05	<.01	25	N/A	19						
A10033708	D07-12	425.00	426.18	1.18	Core	<.01	0.01	17.54	0.05	<.01	40	N/A	<10						
A10033709	D07-12	426.18	426.71	0.53	Core	<.01	0.01	20.07	0.04	<.01	31	N/A	<10						
A10033710	D07-12	0.00	0.00	0	STD 3	0.01	0.61	0.81	0.04	0.06	<10	N/A	522						
A10033711	D07-12	426.71	427.69	0.98	Core	<.01	0.04	21.04	0.04	<.01	46	N/A	717	0.18	1.87	2.6	0.018		0.003
A10033712	D07-12	429.46	430.46	1	Core	<.01	0.01	21.22	0.04	<.01	14	N/A	17						
A10033713	D07-12	430.46	431.61	1.15	Core	<.01	0.13	22.85	0.05	0.06	60	N/A	237						
A10033714	D07-12	431.61	432.39	0.78	Core	<.01	0.01	20.12	0.05	<.01	24	N/A	50						
A10033715	D07-12	432.39	433.05	0.66	Core	<.01	0.03	18.71	0.04	<.01	40	N/A	1603	1.04	5.68	14.4	0.055		0.001
A10033716	D07-12	433.05	434.00	0.95	Core	<.01	0.02	19.97	0.05	<.01	10	N/A	26						
A10033717	D07-12	435.30	436.00	0.7	Core	<.01	0.02	19.67	0.05	<.01	28	N/A	21						
A10033718	D07-12	436.00	437.00	1	Core	<.01	0.01	16.47	0.05	<.01	74	N/A	<10						
A10033719	D07-12	437.00	438.00	1	Core	<.01	0.07	19.34	0.04	0.02	35	N/A	<10						
A10033720	D07-12	438.00	439.00	1	Core	<.01	0.10	23.27	0.05	0.02	48	N/A	<10						
A10033721	D07-12	439.00	440.00	1	Core	<.01	0.03	27.37	0.04	0.01	89	N/A	17						
A10033722	D07-12	440.00	441.08	1.08	Core	<.01	0.04	29.93	0.05	0.02	149	N/A	<10						
A10033723	D07-12	441.08	442.00	0.92	Core	<.01	0.03	33.27	0.04	0.02	339	N/A	23						
A10033724	D07-12	450.00	451.00	1	Core	<.01	0.03	19.82	0.05	<.01	59	N/A	24						
A10033725	D07-12	0.00	0.00	0	STD 1	0.05	1.00	1.44	0.09	0.14	485	N/A	525						
A10033726	D07-12	451.00	452.00	1	Core	<.01	0.03	19.15	0.05	0.01	37	N/A	37						
A10033727	D07-12	452.00	453.00	1	Core	<.01	0.02	18.76	0.05	0.01	36	N/A	62						
A10033728	D07-12	453.00	454.00	1	Core	<.01	0.04	19.62	0.05	0.01	45	N/A	20						
A10033729	D07-12	454.00	455.00	1	Core	<.01	0.04	19.10	0.05	0.01	25	N/A	<10						
A10033730	D07-12	455.00	456.00	1	Core	<.01	0.05	19.12	0.05	0.01	15	N/A	<10						
A10033731	D07-12	456.00	456.92	0.92	Core	<.01	0.08	19.79	0.05	0.02	72	N/A	888	<0.01	3.42	0.7	0.039		0.001
A10033732	D07-12	456.92	457.45	0.53	Core	<.01	0.01	21.14	0.05	<.01	47	N/A	14						
A10033733	D07-12	457.45	458.00	0.55	Core	<.01	0.02	19.53	0.05	<.01	57	N/A	488	<0.01	1.92	1.3	0.019		0.001
A10033734	D07-12	458.00	458.79	0.79	Core	<.01	0.01	21.03	0.05	<.01	64	N/A	<10						
A10033735	D07-12	458.79	459.79	1	Core	<.01	0.02	18.28	0.05	<.01	39	N/A	76						
A10033736	D07-12	459.88	461.00	1.12	Core	<.01	0.05	24.22	0.04	0.01	101	N/A	2641	<0.01	8.90	1.4	0.097		0.001
A10033737	D07-12	461.00	461.94	0.94	Core	<.01	0.04	18.85	0.05	<.01	72	N/A	1496	<0.01	4.50	1.1	0.047		<0.001
A10033738	D07-12	0.00	0.00	0	Blank	0.20	1.65	1.56	0.17	0.60	3196	N/A	52						
A10033739	D07-12	461.94	462.92	0.98	Core	<.01	0.02	19.69	0.05	<.01	46	N/A	139						
A10033740	D07-12	0.00	0.00	0	STD 7	0.01	0.49	0.44	0.04	0.01	<10	N/A	417						
A10033741	D07-12	462.92	464.00	1.08	Core	<.01	0.01	18.77	0.05	<.01	23	N/A	11						
A10033742	D07-12	464.00	465.00	1	Core	<.01	0.01	18.90	0.05	<.01	20	N/A	<10						
A10033743	D07-12	465.00	466.05	1.05	Core	<.01	0.01	19.70	0.06	<.01	15	N/A	<10						
A10033744	D07-12	466.05	466.74	0.69	Core	<.01	0.01	20.86	0.05	<.01	11	N/A	<10						
A10033745	D07-12	466.74	467.74	1	Core	<.01	0.02	19.78	0.06	0.01	14	N/A	10						
A10033746	D07-12	467.74	469.00	1.26	Core	<.01	0.01	18.98	0.05	<.01	38	N/A	149						
A10033747	D07-12	469.00	470.00	1	Core	<.01	0.02	18.95	0.05	<.01	34	N/A	53						
A10033748	D07-12	470.00	471.19	1.19	Core	<.01	0.07	22.51	0.05	<.01	49	N/A	597	0.11	1.85	2.7	0.013		
A10033749	D07-12	471.19	472.19	1	Core	<.01	0.03	19.70	0.05	0.01	27	N/A	118						
A10033750	D07-12	473.00	474.00	1	Core	<.01	0.04	18.69	0.05	0.02	25	N/A	45						
A10033751	D07-12	474.00	475.06	1.06	Core	<.01	0.07	18.53	0.05	0.01	21	N/A	28						
A10033752	D07-12	475.06	476.00	0.94	Core	<.01	0.03	18.07	0.05	0.01	41	N/A	111						
A10033753	D07-12	476.00	477.00	1	Core	<.01	0.02	16.67	0.06	0.01	56	N/A	105						
A10033754	D07-12	0.00	0.00	0	Blank	0.21	1.73	1.60	0.16	0.72	3328	N/A	14						
A10033755	D07-12	0.00	0.00	0	STD 1	0.05	0.95	1.30	0.10	0.15	464	N/A	514						
A10033756	D07-12	477.00	478.00	1	Core	<.01	0.02	20.26	0.05	0.01	39	N/A	59						
A10033757	D07-12	478.00	479.00	1	Core	<.01	0.02	18.78	0.05	0.01	28	N/A	63						

		Sampled Section				Ti	Al	Ca	Na	K	P	Ge	Hg	ASSAY					
Tag Number	Hole	From	To	Interval	Type	%	%	%	%	%	ppm	ppm	ppb	Pb(A) %	Zn(A) %	Ag(2) g/t	Cd(A) %	Fe(T) %	Ge(A) %
A10033758	D07-12	479.00	480.00	1	Core	<.01	0.04	19.15	0.05	0.02	59	N/A	71						
A10033759	D07-12	480.00	481.00	1	Core	<.01	0.05	19.04	0.05	0.02	110	N/A	33						
A10033760	D07-12	481.00	482.00	1	Core	<.01	0.04	18.75	0.05	0.02	180	N/A	64						
A10033761	D07-12	482.00	482.53	0.53	Core	<.01	0.05	18.70	0.05	0.03	217	N/A	46						
A10033762	D07-12	482.53	483.45	0.92	Core	<.01	0.08	18.97	0.05	0.04	662	N/A	195						
A10033763	D07-12	483.45	483.80	0.35	Core	<.01	0.06	21.87	0.05	0.03	723	N/A	70						
A10033764	D07-12	484.04	484.51	0.47	Core	<.01	0.08	22.47	0.04	0.04	1789	N/A	90						
A10033765	D07-12	411.72	412.22	0.5	Core	<.01	0.01	19.02	0.05	<.01	31	N/A	75						
A10033766	D07-12	412.22	413.00	0.78	Core	<.01	0.02	16.93	0.05	<.01	17	N/A	<10						
A10033767	D07-12	486.62	487.12	0.5	Core	<.01	0.03	33.08	0.04	0.01	245	N/A	14						
A10033768	D07-12	514.66	515.68	1.02	Core	<.01	0.06	20.35	0.05	0.01	239	N/A	55						
A10033769	D07-12	515.68	517.00	1.32	Core	<.01	0.02	19.79	0.06	0.01	36	N/A	<10						
A10033770	D07-12	0.00	0.00	0	STD 7	0.01	0.49	0.51	0.05	0.02	<10	N/A	493						
A10033771	D07-12	517.00	518.00	1	Core	<.01	0.02	19.34	0.06	<.01	120	N/A	32						
A10033772	D07-12	521.00	522.00	1	Core	<.01	0.02	20.23	0.05	<.01	135	N/A	23						
A10033773	D07-12	522.00	523.00	1	Core	<.01	0.04	23.65	0.05	<.01	158	N/A	66						
A10033774	D07-12	523.00	524.00	1	Core	<.01	0.13	22.98	0.04	0.02	531	N/A	94						
A10033775	D07-12	536.25	537.25	1	Core	<.01	0.11	19.89	0.04	0.04	870	N/A	105						
A10033776	D07-12	537.60	538.60	1	Core	<.01	0.05	22.65	0.05	0.02	221	N/A	51						
A10033777	D07-12	539.95	540.98	1.03	Core	<.01	0.06	25.52	0.04	<.01	94	N/A	128						
A10033778	D07-12	540.98	542.00	1.02	Core	<.01	0.02	23.44	0.05	<.01	32	N/A	<10						
A10033779	D07-12	543.74	544.50	0.76	Core	<.01	0.08	11.00	0.06	0.01	37	N/A	61						
A10033780	D07-12	550.00	551.00	1	Core	<.01	0.06	21.95	0.06	0.01	684	N/A	126						
A10033781	D07-12	551.61	552.10	0.49	Core	<.01	0.06	24.73	0.06	0.01	55	N/A	86						
A10033782	D07-12	554.38	554.88	0.5	Core	<.01	0.09	18.79	0.06	0.03	121	N/A	50						
A10033783	D07-12	563.00	564.36	1.36	Core	<.01	0.07	23.14	0.06	0.03	302	N/A	55						
A10033784	D07-12	574.31	574.85	0.54	Core	<.01	0.02	30.20	0.05	0.01	70	N/A	37						
A10033785	D07-12	0.00	0.00	0	STD 3	0.02	0.79	1.32	0.05	0.08	<10	N/A	764						
A10033786	D07-12	575.29	576.06	0.77	Core	<.01	0.03	27.93	0.06	0.01	198	N/A	17						
A10033787	D07-12	576.06	576.77	0.71	Core	<.01	0.06	26.10	0.06	0.03	229	N/A	42						
A10033788	D07-12	576.77	577.83	1.06	Core	<.01	0.04	21.65	0.05	0.02	71	N/A	16						
A10033789	D07-12	577.83	579.00	1.17	Core	<.01	0.04	22.34	0.05	0.02	50	N/A	22						
A10033790	D07-12	579.00	579.79	0.79	Core	<.01	0.04	19.61	0.06	0.01	50	N/A	12						
A10033791	D07-12	579.79	581.00	1.21	Core	<.01	0.04	18.93	0.06	0.02	88	N/A	23						
A10033792	D07-12	581.00	582.00	1	Core	<.01	0.04	19.73	0.06	0.02	177	N/A	26						
A10033793	D07-12	582.00	582.55	0.55	Core	<.01	0.04	19.86	0.06	0.02	244	N/A	32						
A10033794	D07-12	587.14	588.38	1.24	Core	<.01	0.02	20.37	0.06	0.01	25	N/A	21						
A10033795	D07-12	604.35	605.00	0.65	Core	<.01	0.01	19.71	0.07	0.01	40	N/A	116						
A10033796	D07-12	605.00	605.69	0.69	Core	<.01	0.03	20.75	0.06	0.01	54	N/A	424	<0.01	4.87	0.6	0.041		
A10033801	D07-12	0.00	0.00	0	STD 3	0.02	0.73	1.11	0.05	0.08	<10	N/A	665						
A10033802	D07-12	615.60	616.44	0.84	Core	<.01	0.01	30.30	0.06	0.01	22	N/A	<10						
A10033803	D07-12	625.72	626.73	1.01	Core	<.01	0.03	28.82	0.06	0.02	39	N/A	71						
A10033804	D07-12	626.73	627.19	0.46	Core	<.01	0.04	23.22	0.05	0.01	71	N/A	285	0.16	6.06	1.1	0.027		
A10033805	D07-12	678.32	679.27	0.95	Core	<.01	0.04	47.99	0.06	0.03	661	N/A	<10						

APPENDIX

VIII. GLOBAL DISCOVERY LABORATORY REPORTS

REMAC ZINC CORP.-X08

teckcominco
Global Discovery Labs

Ref/I.D.: A10032715-750 / 10033701-796 / 10033801-805
Report Date: 01 APR 2008
GDL Job No: V08-0016R

LAB NO	FIELD NUMBER	Pb(A) %	Zn(A) %	Cd(A) %	Ag(2) g/t	Ge(A) %
R0800922	A10033711A	0.18	1.87	0.018	2.6	0.003
R0800926	A10033715A	1.04	5.68	0.055	14.4	0.001
R0800942	A10033731A	<0.01	3.42	0.039	0.7	0.001
R0800944	A10033733A	<0.01	1.92	0.019	1.3	0.001
R0800947	A10033736A	<0.01	8.90	0.097	1.4	0.001
R0800948	A10033737A	<0.01	4.50	0.047	1.1	<0.001
R0800960	A10033748A	0.11	1.85	0.013	2.7	
R0801009	A10033796A	<0.01	4.87	0.041	0.6	
R0801013	A10033804A	0.16	6.06	0.027	1.1	
R0800944 rpt		<0.01	1.90	0.019	1.0	
STD: CZN-3		0.10	50.82	0.251	43.9	
STD: GG-1						0.128

I=insufficient sample
If requested analyses are not shown, results are to follow

ANALYTICAL METHODS

- Pb(A) Assay
- Zn(A) Assay
- Cd(A) Assay
- Ag(2) Acid decomposition / AAS
- Ge(A) Acid decomposition / solvent extraction / AAS

REMAC ZINC CORP.-X08

Ref/I.D.: A10032715-750 / 10033701-796 / 10033801-805
Report Date: 17 JAN 2008
GDL Job No: V08-0016R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm
R0800874	GDL PREP BLANK	5	6	57	<0.4	3	252	<1	5	4	2.26	<2	73	<5	<5	39	2	<2	63
R0800875	A10032715A	13490	2290	26000	47.5	34	6	62	112	12	26.79	8	25	48	<5	<2	9	<2	3
R0800876	A10032716A	51	40	99	<0.4	508	16	<1	18	15	7.70	<2	83	8	<5	2	2	<2	65
R0800877	A10032717A	20	10	20	<0.4	29	82	<1	10	13	2.67	<2	62	<5	<5	7	<2	<2	59
R0800878	A10032718A	7	14	12	<0.4	75	59	<1	8	14	2.74	<2	90	5	<5	7	<2	<2	78
R0800878 rpt		7	15	16	<0.4	70	57	<1	7	13	2.59	<2	82	<5	<5	6	<2	<2	73
R0800879	A10032719A	3	21	19	<0.4	119	51	<1	16	19	2.83	<2	92	6	<5	7	<2	<2	54
R0800880	A10032720A	9	11	9	<0.4	31	25	<1	5	8	1.14	<2	61	5	<5	4	<2	<2	35
R0800881	A10032721A	7	59	118	<0.4	36	65	<1	7	6	2.16	<2	61	<5	<5	5	<2	<2	44
R0800882	A10032722A	7	15	14	<0.4	41	29	<1	5	11	1.27	<2	109	<5	<5	3	<2	<2	26
R0800883	A10032723A	4	15	3	<0.4	389	31	<1	25	26	4.26	<2	102	<5	<5	4	<2	<2	26
R0800884	A10032724A	82	17	91	<0.4	10	98	<1	36	45	4.66	<2	39	<5	<5	26	2	<2	18
R0800884 rpt		83	17	97	<0.4	10	103	<1	39	47	4.97	<2	40	24	<5	27	2	<2	19
R0800885	A10032725A	35	18	69	<0.4	12	89	<1	20	33	4.05	<2	32	<5	<5	31	2	<2	25
R0800886	A10032726A	69	43	49	<0.4	41	95	<1	30	39	7.15	<2	43	5	<5	15	3	<2	29
R0800887	A10032727A	25	15	49	<0.4	14	555	<1	19	38	4.15	<2	109	<5	<5	93	<2	<2	239
R0800888	A10032728A	9	8	26	<0.4	12	103	<1	11	22	2.48	<2	37	<5	<5	19	<2	<2	53
R0800889	A10032729A	3	9	15	<0.4	77	54	<1	8	20	2.22	<2	23	6	<5	8	<2	<2	65
R0800890	A10032730A	540	8626	10200	150.4	4101	19	135	12	25	7.65	7	26	<5	44	35	6	<2	78
R0800891	A10032731A	18	40	80	<0.4	37	87	<1	5	26	2.11	<2	55	<5	<5	15	<2	<2	94
R0800892	A10032732A	32	13	25	<0.4	28	95	<1	14	30	3.51	<2	39	6	<5	14	<2	<2	93
R0800893	A10032733A	9	7	11	<0.4	12	90	<1	8	11	1.38	<2	58	<5	<5	10	<2	<2	120
R0800894	A10032734A	6	6	6	<0.4	7	53	<1	2	8	0.68	<2	37	<5	<5	4	<2	<2	107
R0800895	A10032735A	5	4	13	<0.4	<2	77	<1	1	4	0.59	<2	99	<5	<5	9	<2	<2	91
R0800896	A10032736A	14	11	25	<0.4	19	70	<1	8	14	2.71	<2	51	5	<5	16	<2	<2	111
R0800896 rpt		20	12	33	<0.4	26	79	<1	10	17	3.39	<2	60	11	<5	18	<2	<2	125
R0800897	A10032737A	16	6	15	<0.4	6	67	<1	4	9	2.06	<2	57	<5	<5	13	<2	<2	90
R0800898	A10032738A	13	<4	9	<0.4	10	71	<1	3	9	1.73	<2	53	5	<5	12	<2	<2	95
R0800899	A10032739A	26	7	10	<0.4	10	70	<1	10	24	2.72	<2	68	<5	<5	17	<2	<2	133
R0800900	A10032740A	49	13	21	<0.4	14	59	<1	30	21	4.65	<2	53	7	<5	12	2	<2	118
R0800901	A10032741A	88	13	39	<0.4	19	76	<1	22	32	5.38	<2	35	7	<5	13	2	<2	106

REMAC ZINC CORP.-X08

Ref/I.D.: A10032715-750 / 10033701-796 / 10033801-805
Report Date: 17 JAN 2008
GDL Job No: V08-0016R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm
R0800902	A10032742A	36	14	30	<0.4	8	65	<1	15	19	3.62	<2	36	<5	<5	11	<2	<2	77
R0800903	A10032743A	35	34	36	<0.4	9	78	<1	21	31	3.92	<2	30	<5	<5	21	2	<2	43
R0800904	A10032744A	6	69	40	<0.4	6	60	<1	4	8	2.69	<2	57	<5	<5	8	<2	<2	103
R0800905	A10032745A	7825	7059	72890	86.4	51	<5	164	93	14	26.69	8	29	55	<5	<2	9	<2	2
R0800906	A10032746A	41	30	248	<0.4	8	69	<1	10	7	4.74	<2	54	6	<5	20	<2	<2	182
R0800907	A10032747A	26	20	52	<0.4	3	77	<1	13	20	4.11	<2	52	5	<5	11	<2	<2	41
R0800908	A10032748A	16	19	42	<0.4	5	62	<1	9	16	3.09	<2	69	<5	<5	13	<2	<2	39
R0800909	A10032749A	65	35	55	<0.4	11	82	<1	13	21	4.34	<2	66	5	<5	13	2	<2	134
R0800910	A10032750A	51	13	80	<0.4	11	64	<1	20	64	4.72	49	18	<5	<5	5	2	<2	39
R0800911	A10033701A	58	20	33	<0.4	15	35	<1	18	61	3.96	3	12	<5	<5	4	<2	<2	363
R0800912	A10033702A	35	36	92	<0.4	7	41	<1	15	43	3.23	2	11	<5	<5	7	<2	<2	246
R0800913	10033702 GDL DUP	29	28	79	<0.4	8	41	<1	15	45	3.39	2	11	<5	<5	7	<2	<2	251
R0800914	A10033703A	3	200	577	<0.4	<2	179	4	<1	1	0.42	<2	5	<5	<5	20	<2	<2	144
R0800915	A10033704A	1	57	204	<0.4	3	383	1	<1	9	0.82	23	<4	<5	<5	32	<2	5	170
R0800916	A10033705A	19	530	1621	0.8	34	74	14	2	52	4.01	110	5	<5	<5	37	<2	3	166
R0800917	A10033706A	6	391	606	0.6	17	76	4	1	27	2.04	51	<4	<5	<5	24	<2	2	156
R0800917 rpt		6	420	642	0.5	23	76	4	1	28	2.15	55	<4	29	<5	22	<2	<2	151
R0800918	A10033707A	1	56	657	<0.4	<2	33	4	<1	4	0.76	2	<4	<5	<5	15	<2	3	148
R0800919	A10033708A	<1	457	172	0.5	<2	41	<1	<1	2	0.47	<2	11	<5	<5	19	<2	4	155
R0800920	A10033709A	<1	276	197	<0.4	<2	63	1	<1	1	0.31	2	<4	<5	<5	20	<2	<2	318
R0800921	A10033710A	11750	2110	23800	45.0	24	5	58	103	11	24.04	7	22	48	<5	<2	7	<2	3
R0800922	A10033711A	44	1676	11770	1.7	<2	232	148	<1	1	0.41	<2	4	<5	<5	25	<2	8	257
R0800923	A10033712A	3	26	203	<0.4	<2	99	<1	<1	1	0.41	<2	<4	<5	<5	18	<2	2	226
R0800924	A10033713A	1	1545	6749	2.2	24	250	70	1	17	4.25	5	<4	<5	<5	49	<2	<2	250
R0800925	A10033714A	<1	63	1830	<0.4	2	69	15	<1	4	0.66	<2	<4	<5	<5	48	<2	3	293
R0800925 rpt		<1	52	1712	<0.4	<2	68	14	<1	3	0.63	<2	<4	18	<5	43	<2	<2	289
R0800926	A10033715A	6	10690	57630	11.1	39	55	589	4	54	7.46	17	11	7	<5	34	2	8	139
R0800927	A10033716A	<1	67	486	<0.4	<2	56	3	<1	2	0.40	<2	5	<5	<5	20	<2	<2	130
R0800928	A10033717A	<1	140	371	<0.4	<2	49	2	<1	4	0.49	<2	15	<5	<5	17	<2	3	107
R0800929	A10033718A	<1	46	216	<0.4	<2	64	1	<1	3	0.33	2	47	<5	<5	14	<2	2	113
R0800930	A10033719A	1	55	64	<0.4	4	322	<1	<1	7	0.62	4	26	<5	<5	16	<2	<2	154
R0800931	A10033720A	1	23	210	<0.4	6	1106	<1	<1	12	0.59	5	<4	<5	<5	20	<2	4	162

REMAC ZINC CORP.-X08

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LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm
R0800932	A10033721A	11	210	523	0.4	10	94	<1	1	10	3.11	2	<4	<5	<5	9	<2	<2	212
R0800933	A10033722A	3	16	53	<0.4	3	190	<1	1	4	0.54	<2	<4	<5	<5	4	<2	<2	296
R0800934	A10033723A	11	122	1840	<0.4	16	121	7	1	12	1.01	2	<4	<5	<5	3	<2	<2	255
R0800935	A10033724A	2	23	528	<0.4	<2	425	3	<1	3	0.38	<2	<4	<5	<5	18	<2	3	127
R0800936	A10033725A	511	8437	9856	113.5	4180	18	136	12	24	7.49	7	25	<5	44	32	5	<2	73
R0800937	A10033726A	2	91	1388	<0.4	11	397	9	<1	1	0.29	<2	<4	<5	<5	16	<2	3	141
R0800938	A10033727A	2	80	2547	<0.4	3	70	23	<1	2	0.56	<2	<4	<5	<5	14	<2	3	121
R0800939	A10033728A	<1	64	796	<0.4	3	399	5	<1	4	0.59	<2	<4	<5	<5	13	<2	3	114
R0800940	A10033729A	2	33	369	<0.4	<2	618	2	<1	1	0.25	<2	<4	<5	<5	13	<2	2	105
R0800941	A10033730A	1	29	332	<0.4	2	806	1	<1	3	0.27	<2	6	<5	<5	16	<2	<2	111
R0800942	A10033731A	<1	61	32520	<0.4	5	36	324	<1	7	0.67	4	<4	<5	<5	21	<2	5	138
R0800942 rpt		<1	52	31290	<0.4	2	33	321	<1	7	0.66	3	<4	17	<5	24	<2	122	133
R0800943	A10033732A	1	15	242	<0.4	<2	79	1	<1	<1	0.36	<2	<4	<5	<5	28	<2	<2	210
R0800944	A10033733A	7	215	12050	0.7	12	86	159	1	10	3.00	8	<4	<5	<5	27	<2	3	165
R0800945	A10033734A	2	43	356	<0.4	<2	58	2	<1	3	0.63	<2	<4	<5	<5	23	<2	2	155
R0800946	A10033735A	1	13	1694	<0.4	<2	347	14	<1	3	0.54	<2	<4	<5	<5	16	<2	4	121
R0800947	A10033736A	7	172	101000	0.8	6	26	1079	3	13	1.43	10	<4	<5	<5	28	<2	14	142
R0800948	A10033737A	12	80	42900	0.6	5	36	361	1	9	1.31	6	<4	<5	<5	18	<2	6	149
R0800949	A10033738A	23	16	388	<0.4	10	363	2	12	23	2.66	<2	62	<5	<5	57	<2	<2	143
R0800950	A10033739A	1	47	3489	<0.4	<2	236	34	<1	4	0.43	<2	<4	<5	<5	15	<2	<2	146
R0800951	A10033740A	6163	6275	61860	62.1	15	<5	147	52	13	17.26	6	26	47	<5	2	8	<2	2
R0800952	A10033741A	17	55	510	<0.4	<2	167	2	<1	1	0.30	<2	<4	<5	<5	12	<2	2	100
R0800953	GDL PREP BLANK	<1	5	69	<0.4	3	225	<1	4	3	1.76	<2	27	<5	<5	36	<2	<2	46
R0800954	A10033742A	<1	59	370	<0.4	<2	37	2	<1	1	0.39	<2	<4	<5	<5	15	<2	<2	124
R0800955	A10033743A	<1	22	461	<0.4	<2	41	2	<1	<1	0.35	<2	<4	<5	<5	10	<2	4	114
R0800956	A10033744A	2	16	280	<0.4	2	50	1	<1	2	0.46	<2	<4	<5	<5	15	<2	<2	145
R0800956 rpt		<1	17	268	<0.4	<2	47	1	<1	1	0.44	<2	<4	25	<5	15	<2	<2	137
R0800957	A10033745A	1	44	584	<0.4	<2	73	3	<1	2	0.59	<2	<4	<5	<5	12	<2	<2	122
R0800958	A10033746A	1	405	4765	0.8	5	96	37	<1	7	2.00	2	<4	<5	<5	14	<2	<2	116
R0800959	A10033747A	<1	135	2801	0.5	8	84	19	<1	6	2.29	<2	<4	<5	<5	16	<2	<2	121
R0800960	A10033748A	8	1797	23550	2.4	31	16	181	4	27	16.70	10	<4	15	<5	17	3	3	122
R0800961	A10033749A	3	377	3574	0.7	8	50	23	<1	7	4.11	<2	<4	<5	<5	13	<2	3	113

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Ref/I.D.: A10032715-750 / 10033701-796 / 10033801-805
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LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm
R0800962	A10033750A	1	80	1146	<0.4	8	165	10	1	16	1.49	2	<4	<5	<5	18	<2	2	139
R0800963	A10033751A	<1	187	864	<0.4	3	174	6	<1	8	0.79	<2	<4	<5	<5	13	<2	<2	114
R0800964	A10033752A	3	1029	5200	1.1	12	42	32	1	9	6.14	2	<4	5	<5	11	2	<2	102
R0800965	A10033753A	1	408	6973	0.5	3	42	35	<1	5	2.63	<2	<4	<5	<5	13	<2	3	105
R0800966	A10033754A	25	20	137	<0.4	12	414	<1	12	24	2.92	<2	63	<5	<5	63	<2	<2	137
R0800967	A10033755A	513	7947	9337	114.4	3848	17	124	11	23	7.23	6	23	<5	42	31	6	<2	72
R0800968	A10033756A	2	122	3249	<0.4	16	39	16	<1	5	0.91	<2	<4	<5	<5	15	<2	2	101
R0800969	A10033757A	1	172	3266	<0.4	7	61	17	<1	9	1.89	3	<4	<5	<5	15	<2	3	140
R0800969 rpt		1	183	3448	<0.4	7	62	19	1	9	1.91	4	<4	23	<5	15	<2	7	148
R0800970	A10033758A	2	141	3376	<0.4	5	206	15	<1	8	1.21	4	<4	<5	<5	13	<2	3	156
R0800971	A10033759A	3	108	1353	<0.4	6	185	7	<1	14	0.84	4	<4	<5	<5	14	<2	2	123
R0800972	A10033760A	5	376	2477	0.5	16	109	9	1	19	2.84	12	<4	<5	<5	11	<2	<2	111
R0800973	A10033761A	4	136	1739	<0.4	11	101	7	<1	15	1.14	2	<4	<5	<5	14	<2	3	106
R0800973 rpt		6	142	1679	<0.4	10	90	8	1	16	1.00	2	<4	20	<5	14	<2	<2	106
R0800974	A10033762A	14	6425	6197	5.4	46	93	35	4	71	4.99	17	4	5	<5	20	<2	3	108
R0800975	A10033763A	19	874	2219	1.0	79	81	12	6	86	5.16	19	<4	<5	<5	17	<2	<2	106
R0800976	A10033764A	79	1384	2386	2.1	139	46	17	11	65	7.23	14	<4	<5	<5	30	2	<2	102
R0800977	A10033765A	1	370	2093	0.7	8	45	18	<1	7	1.97	15	<4	<5	<5	16	<2	2	107
R0800978	A10033766A	1	911	52	<0.4	<2	443	<1	<1	1	0.56	<2	8	<5	<5	13	<2	2	95
R0800979	A10033767A	19	622	407	0.5	20	20	1	4	16	4.89	2	<4	<5	<5	5	2	<2	252
R0800980	A10033768A	4	1279	1678	0.7	35	18	9	1	39	6.34	3	<4	<5	<5	50	<2	<2	166
R0800981	A10033769A	<1	72	101	<0.4	<2	301	<1	<1	1	0.50	<2	<4	<5	<5	47	<2	<2	147
R0800982	A10033770A	7146	5820	65690	66.6	40	<5	140	76	12	22.80	7	23	46	<5	<2	8	<2	2
R0800983	A10033771A	25	124	1098	<0.4	6	292	5	<1	5	1.05	<2	<4	<5	<5	54	<2	3	115
R0800984	A10033772A	1	1602	924	0.9	13	160	5	1	14	1.81	<2	<4	<5	<5	78	<2	2	159
R0800985	A10033773A	<1	3432	2208	1.5	31	28	13	3	37	4.44	8	5	<5	<5	77	<2	4	153
R0800986	A10033774A	15	3108	1153	1.0	28	22	5	2	37	5.99	5	18	<5	<5	254	2	<2	207
R0800987	A10033775A	11	1565	671	0.8	65	27	<1	4	100	11.68	9	69	7	<5	973	2	6	149
R0800988	A10033776A	3	1183	378	<0.4	28	40	<1	2	35	4.75	8	27	<5	<5	517	2	6	155
R0800989	A10033777A	3	4104	1958	1.7	28	18	7	4	34	5.89	12	<4	<5	<5	66	<2	3	212
R0800990	A10033778A	2	117	262	<0.4	5	135	1	<1	4	0.54	<2	<4	<5	<5	32	<2	3	142
R0800991	A10033779A	16	6467	1756	4.3	51	<5	12	7	51	21.10	14	8	<5	<5	21	3	17	88

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Ref/I.D.: A10032715-750 / 10033701-796 / 10033801-805
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GDL Job No: V08-0016R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm
R0800992	A10033780A	20	1344	2725	0.4	52	25	19	2	37	11.81	14	6	<5	<5	62	3	7	154
R0800993	10033780 GDL DUP	22	1592	2964	0.4	60	22	22	3	42	12.64	16	9	<5	<5	70	3	17	152
R0800994	A10033781A	15	4852	1880	0.8	26	26	15	5	24	13.68	18	8	<5	<5	51	3	17	128
R0800995	A10033782A	50	5714	1194	1.5	95	9	10	11	73	21.59	31	11	<5	<5	50	<2	57	87
R0800995 rpt		37	6160	1218	1.5	97	10	11	12	77	21.50	31	11	141	<5	47	<2	10	86
R0800996	A10033783A	24	5872	1241	3.7	96	28	12	14	129	15.21	29	16	<5	<5	48	3	44	95
R0800997	A10033784A	7	152	1315	<0.4	4	36	14	1	14	1.18	<2	<4	<5	<5	17	<2	<2	150
R0800998	A10033785A	13390	3824	31810	58.5	29	6	112	177	24	29.64	22	36	41	<5	2	8	70	3
R0800999	A10033786A	50	207	607	<0.4	5	30	4	1	8	1.15	<2	<4	<5	<5	22	<2	4	127
R0801000	A10033787A	11	363	1481	<0.4	22	82	19	2	27	2.57	2	<4	<5	<5	19	<2	2	139
R0801001	A10033788A	5	125	489	<0.4	<2	36	4	1	7	1.08	<2	<4	<5	<5	13	<2	<2	105
R0801002	A10033789A	6	164	1483	<0.4	3	31	13	1	11	1.29	2	<4	<5	<5	17	<2	<2	123
R0801003	A10033790A	4	157	576	<0.4	2	23	4	1	11	1.45	<2	<4	<5	<5	11	<2	<2	104
R0801004	A10033791A	3	68	1306	<0.4	<2	38	10	<1	5	0.72	<2	<4	<5	<5	15	<2	<2	115
R0801005	A10033792A	3	63	1561	<0.4	2	41	12	1	6	0.86	<2	<4	<5	<5	12	<2	<2	116
R0801006	A10033793A	5	174	1361	<0.4	2	28	11	<1	7	0.86	3	<4	<5	<5	14	<2	<2	112
R0801007	A10033794A	4	227	1072	<0.4	<2	31	8	<1	3	0.35	<2	<4	<5	<5	21	<2	<2	115
R0801007 rpt		5	237	1062	<0.4	<2	30	8	<1	3	0.41	<2	<4	21	<5	19	<2	5	112
R0801008	A10033795A	4	56	7460	<0.4	<2	51	80	<1	2	0.59	2	<4	<5	<5	22	<2	<2	133
R0801009	A10033796A	13	38	23440	0.6	16	37	439	1	12	3.63	12	<4	<5	<5	34	2	2	133
R0801010	A10033801A	13100	2899	29260	48.0	22	6	88	144	19	28.02	18	30	33	<5	<2	8	35	3
R0801011	A10033802A	42	55	230	<0.4	<2	55	<1	1	3	0.63	<2	<4	<5	<5	13	<2	4	121
R0801012	A10033803A	7	289	5191	<0.4	3	40	47	1	6	2.22	3	<4	<5	<5	14	<2	4	142
R0801013	A10033804A	11	2382	64020	0.9	7	37	378	5	16	7.91	17	<4	<5	<5	7	<2	14	115
R0801014	A10033805A	7	22	257	<0.4	<2	17	<1	1	1	0.52	<2	<4	<5	<5	6	<2	<2	461
STD: DA		140	229	685	5.9	55	483	3	13	42	3.86	3	44	14	<5	70	3	<2	40
STD: DA		135	213	639	6.7	53	480	3	12	40	3.58	2	41	14	<5	66	3	<2	40
STD: DA		122	198	595	6.5	46	388	3	11	37	3.30	2	38	14	<5	62	2	<2	36
STD: DA		118	210	613	6.5	43	466	4	12	39	3.03	3	37	18	<5	56	3	3	34
STD: MS2																			

REMAC ZINC CORP.-X08

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Report Date: 17 JAN 2008
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LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm

I=insufficient sample
If requested analyses are not shown, results are to follow

ANALYTICAL METHODS

ICP-OES PACKAGE : 0.5 gram sample digested in hot reverse aqua regia (soil,silt) or hot Aqua Regia(rocks).

ASSIGNED FOR ASSAYING

COMMENTS:

Ge analysis is not able to be provided.

REMAC ZINC CORP.-X08

Ref/I.D.: A10032715-750 / 10033
Report Date: 17 JAN 2008
GDL Job No: V08-0016R

LAB NO	FIELD NUMBER	Y ppm	La ppm	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0800874	GDL PREP BLANK	5	7	583	0.68	0.14	1.20	0.56	0.10	0.58	946	N/A	<10
R0800875	A10032715A	<2	<2	475	1.14	0.01	0.68	0.80	0.05	0.06	<10	N/A	557
R0800876	A10032716A	7	11	120	0.12	<.01	0.36	0.72	0.05	0.22	2877	N/A	11
R0800877	A10032717A	6	15	508	0.31	0.02	0.58	0.63	0.05	0.43	2105	N/A	<10
R0800878	A10032718A	7	18	511	0.35	<.01	0.49	0.89	0.05	0.33	3115	N/A	<10
R0800878 rpt		7	16	452	0.32	<.01	0.44	0.83	0.05	0.30	2833		<10
R0800879	A10032719A	5	18	446	0.37	<.01	0.48	0.60	0.06	0.33	2496	N/A	<10
R0800880	A10032720A	4	15	242	0.12	<.01	0.21	0.36	0.04	0.15	1596	N/A	<10
R0800881	A10032721A	4	18	418	0.22	<.01	0.54	0.55	0.04	0.39	1366	N/A	<10
R0800882	A10032722A	3	17	230	0.15	<.01	0.25	0.34	0.04	0.17	850	N/A	<10
R0800883	A10032723A	3	13	197	0.16	<.01	0.33	0.34	0.05	0.21	861	N/A	<10
R0800884	A10032724A	2	3	386	0.65	0.12	1.36	0.16	0.04	0.96	721	N/A	<10
R0800884 rpt		2	2	407	0.67	0.12	1.46	0.17	0.04	0.99	781		<10
R0800885	A10032725A	3	8	294	0.78	0.15	1.66	0.20	0.05	0.95	603	N/A	<10
R0800886	A10032726A	3	18	1242	1.01	0.01	1.02	0.32	0.06	0.58	743	N/A	<10
R0800887	A10032727A	10	40	463	1.85	0.28	2.84	2.08	0.28	1.01	4140	N/A	12
R0800888	A10032728A	5	35	598	0.65	0.02	0.97	0.64	0.05	0.56	662	N/A	<10
R0800889	A10032729A	3	14	300	0.49	<.01	0.40	0.83	0.05	0.31	747	N/A	<10
R0800890	A10032730A	5	6	1045	0.51	0.05	1.02	1.45	0.10	0.16	487	N/A	576
R0800891	A10032731A	4	26	540	0.81	<.01	0.76	1.15	0.05	0.49	771	N/A	<10
R0800892	A10032732A	5	24	623	0.84	<.01	0.80	1.02	0.05	0.52	1203	N/A	<10
R0800893	A10032733A	4	24	519	0.62	<.01	0.58	1.20	0.05	0.42	926	N/A	<10
R0800894	A10032734A	6	19	367	0.40	<.01	0.30	1.12	0.04	0.23	2035	N/A	<10
R0800895	A10032735A	6	30	316	0.30	<.01	0.42	0.92	0.04	0.33	1749	N/A	<10
R0800896	A10032736A	7	21	703	0.64	0.01	0.49	1.11	0.05	0.27	2174	N/A	<10
R0800896 rpt		8	19	834	0.74	0.01	0.59	1.25	0.06	0.31	2616		<10
R0800897	A10032737A	6	17	638	0.44	0.01	0.44	0.94	0.05	0.28	2132	N/A	<10
R0800898	A10032738A	6	23	606	0.42	<.01	0.42	1.04	0.05	0.31	2211	N/A	<10
R0800899	A10032739A	9	20	654	0.56	<.01	0.53	1.35	0.05	0.30	3621	N/A	<10
R0800900	A10032740A	9	19	710	0.63	<.01	0.54	1.36	0.05	0.32	3267	N/A	<10
R0800901	A10032741A	6	12	840	0.78	<.01	0.71	1.19	0.05	0.40	1268	N/A	<10

REMAC ZINC CORP.-X08

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LAB NO	FIELD NUMBER	Y ppm	La ppm	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0800902	A10032742A	4	15	671	0.70	<.01	0.81	0.94	0.05	0.39	915	N/A	<10
R0800903	A10032743A	4	16	601	0.73	0.06	1.21	0.48	0.06	0.67	766	N/A	<10
R0800904	A10032744A	6	36	988	0.61	<.01	0.73	1.27	0.05	0.35	635	N/A	<10
R0800905	A10032745A	<2	<2	494	0.85	0.01	0.57	0.42	0.04	0.02	<10	N/A	617
R0800906	A10032746A	13	22	753	0.64	<.01	0.54	1.42	0.05	0.36	4136	N/A	<10
R0800907	A10032747A	5	23	910	0.58	<.01	0.65	0.46	0.05	0.40	951	N/A	<10
R0800908	A10032748A	6	28	481	0.43	<.01	0.79	0.46	0.05	0.34	1377	N/A	<10
R0800909	A10032749A	13	24	1185	0.56	<.01	0.78	1.89	0.05	0.38	4470	N/A	<10
R0800910	A10032750A	3	16	268	0.96	<.01	0.65	1.92	0.05	0.26	336	N/A	<10
R0800911	A10033701A	6	<2	314	1.04	<.01	0.34	11.64	0.06	0.16	277	N/A	<10
R0800912	A10033702A	6	<2	267	1.35	<.01	0.31	9.78	0.05	0.25	329	N/A	<10
R0800913	10033702 GDL DUP	6	<2	287	1.43	<.01	0.32	10.05	0.05	0.27	334	N/A	<10
R0800914	A10033703A	<2	<2	307	12.32	<.01	0.02	19.05	0.05	<.01	48	N/A	19
R0800915	A10033704A	<2	<2	458	12.06	<.01	0.02	21.31	0.05	<.01	38	N/A	19
R0800916	A10033705A	<2	<2	495	9.09	<.01	0.02	19.59	0.05	<.01	60	N/A	97
R0800917	A10033706A	<2	<2	489	11.39	<.01	0.01	20.80	0.05	<.01	17	N/A	39
R0800917 rpt		<2	<2	515	10.90	<.01	0.02	21.09	0.04	<.01	21		40
R0800918	A10033707A	<2	<2	212	12.38	<.01	0.01	18.29	0.05	<.01	25	N/A	19
R0800919	A10033708A	<2	<2	229	10.85	<.01	0.01	17.54	0.05	<.01	40	N/A	<10
R0800920	A10033709A	2	<2	305	9.44	<.01	0.01	20.07	0.04	<.01	31	N/A	<10
R0800921	A10033710A	<2	<2	442	1.06	0.01	0.61	0.81	0.04	0.06	<10	N/A	522
R0800922	A10033711A	2	<2	367	8.12	<.01	0.04	21.04	0.04	<.01	46	N/A	717
R0800923	A10033712A	<2	<2	353	11.59	<.01	0.01	21.22	0.04	<.01	14	N/A	17
R0800924	A10033713A	2	<2	304	8.84	<.01	0.13	22.85	0.05	0.06	60	N/A	237
R0800925	A10033714A	<2	<2	276	12.22	<.01	0.01	20.12	0.05	<.01	24	N/A	50
R0800925 rpt		<2	<2	266	12.15	<.01	0.01	19.27	0.04	<.01	24		59
R0800926	A10033715A	2	<2	232	9.71	<.01	0.03	18.71	0.04	<.01	40	N/A	1603
R0800927	A10033716A	<2	<2	219	12.31	<.01	0.02	19.97	0.05	<.01	10	N/A	26
R0800928	A10033717A	<2	<2	197	11.03	<.01	0.02	19.67	0.05	<.01	28	N/A	21
R0800929	A10033718A	2	<2	179	8.74	<.01	0.01	16.47	0.05	<.01	74	N/A	<10
R0800930	A10033719A	2	<2	212	5.71	<.01	0.07	19.34	0.04	0.02	35	N/A	<10
R0800931	A10033720A	2	<2	250	8.86	<.01	0.10	23.27	0.05	0.02	48	N/A	<10

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LAB NO	FIELD NUMBER	Y ppm	La ppm	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0800932	A10033721A	3	<2	243	6.56	<.01	0.03	27.37	0.04	0.01	89	N/A	17
R0800933	A10033722A	4	<2	57	1.10	<.01	0.04	29.93	0.05	0.02	149	N/A	<10
R0800934	A10033723A	4	<2	117	0.44	<.01	0.03	33.27	0.04	0.02	339	N/A	23
R0800935	A10033724A	2	<2	212	12.27	<.01	0.03	19.82	0.05	<.01	59	N/A	24
R0800936	A10033725A	4	8	1091	0.52	0.05	1.00	1.44	0.09	0.14	485	N/A	525
R0800937	A10033726A	2	<2	168	12.02	<.01	0.03	19.15	0.05	0.01	37	N/A	37
R0800938	A10033727A	2	<2	165	11.71	<.01	0.02	18.76	0.05	0.01	36	N/A	62
R0800939	A10033728A	2	<2	181	12.05	<.01	0.04	19.62	0.05	0.01	45	N/A	20
R0800940	A10033729A	2	<2	190	11.53	<.01	0.04	19.10	0.05	0.01	25	N/A	<10
R0800941	A10033730A	4	<2	183	11.39	<.01	0.05	19.12	0.05	0.01	15	N/A	<10
R0800942	A10033731A	4	<2	204	10.75	<.01	0.08	19.79	0.05	0.02	72	N/A	888
R0800942 rpt		4	<2	209	10.47	<.01	0.08	18.84	0.05	0.02	70		933
R0800943	A10033732A	2	<2	199	12.31	<.01	0.01	21.14	0.05	<.01	47	N/A	14
R0800944	A10033733A	<2	<2	239	11.35	<.01	0.02	19.53	0.05	<.01	57	N/A	488
R0800945	A10033734A	<2	<2	226	12.85	<.01	0.01	21.03	0.05	<.01	64	N/A	<10
R0800946	A10033735A	<2	<2	221	11.88	<.01	0.02	18.28	0.05	<.01	39	N/A	76
R0800947	A10033736A	4	<2	275	11.46	<.01	0.05	24.22	0.04	0.01	101	N/A	2641
R0800948	A10033737A	3	<2	233	11.25	<.01	0.04	18.85	0.05	<.01	72	N/A	1496
R0800949	A10033738A	8	38	315	1.28	0.20	1.65	1.56	0.17	0.60	3196	N/A	52
R0800950	A10033739A	2	<2	195	11.48	<.01	0.02	19.69	0.05	<.01	46	N/A	139
R0800951	A10033740A	<2	<2	483	0.79	0.01	0.49	0.44	0.04	0.01	<10	N/A	417
R0800952	A10033741A	<2	<2	153	11.59	<.01	0.01	18.77	0.05	<.01	23	N/A	11
R0800953	GDL PREP BLANK	3	5	476	0.68	0.11	0.90	0.55	0.08	0.51	763	N/A	<10
R0800954	A10033742A	<2	<2	166	12.47	<.01	0.01	18.90	0.05	<.01	20	N/A	<10
R0800955	A10033743A	<2	<2	197	12.65	<.01	0.01	19.70	0.06	<.01	15	N/A	<10
R0800956	A10033744A	<2	<2	259	11.56	<.01	0.01	20.86	0.05	<.01	11	N/A	<10
R0800956 rpt		<2	<2	264	10.72	<.01	0.01	20.63	0.05	<.01	14		12
R0800957	A10033745A	<2	<2	214	11.85	<.01	0.02	19.78	0.06	0.01	14	N/A	10
R0800958	A10033746A	<2	<2	228	11.48	<.01	0.01	18.98	0.05	<.01	38	N/A	149
R0800959	A10033747A	<2	<2	241	11.64	<.01	0.02	18.95	0.05	<.01	34	N/A	53
R0800960	A10033748A	2	<2	253	7.73	<.01	0.07	22.51	0.05	<.01	49	N/A	597
R0800961	A10033749A	2	<2	275	10.07	<.01	0.03	19.70	0.05	0.01	27	N/A	118

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LAB NO	FIELD NUMBER	Y ppm	La ppm	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0800962	A10033750A	<2	<2	224	11.02	<.01	0.04	18.69	0.05	0.02	25	N/A	45
R0800963	A10033751A	<2	<2	197	11.46	<.01	0.07	18.53	0.05	0.01	21	N/A	28
R0800964	A10033752A	<2	<2	189	9.77	<.01	0.03	18.07	0.05	0.01	41	N/A	111
R0800965	A10033753A	2	<2	183	10.65	<.01	0.02	16.67	0.06	0.01	56	N/A	105
R0800966	A10033754A	7	35	303	1.34	0.21	1.73	1.60	0.16	0.72	3328	N/A	14
R0800967	A10033755A	4	6	980	0.49	0.05	0.95	1.30	0.10	0.15	464	N/A	514
R0800968	A10033756A	<2	<2	230	12.50	<.01	0.02	20.26	0.05	0.01	39	N/A	59
R0800969	A10033757A	<2	<2	219	11.47	<.01	0.02	18.78	0.05	0.01	28	N/A	63
R0800969 rpt		<2	<2	236	11.81	<.01	0.02	20.87	0.05	0.01	31		62
R0800970	A10033758A	<2	<2	218	11.25	<.01	0.04	19.15	0.05	0.02	59	N/A	71
R0800971	A10033759A	2	<2	225	10.28	<.01	0.05	19.04	0.05	0.02	110	N/A	33
R0800972	A10033760A	3	<2	216	10.18	<.01	0.04	18.75	0.05	0.02	180	N/A	64
R0800973	A10033761A	3	<2	229	10.96	<.01	0.05	18.70	0.05	0.03	217	N/A	46
R0800973 rpt		3	<2	232	10.55	<.01	0.04	20.07	0.05	0.02	220		60
R0800974	A10033762A	6	<2	288	8.85	<.01	0.08	18.97	0.05	0.04	662	N/A	195
R0800975	A10033763A	4	<2	322	8.89	<.01	0.06	21.87	0.05	0.03	723	N/A	70
R0800976	A10033764A	5	<2	297	5.88	<.01	0.08	22.47	0.04	0.04	1789	N/A	90
R0800977	A10033765A	<2	<2	339	11.18	<.01	0.01	19.02	0.05	<.01	31	N/A	75
R0800978	A10033766A	<2	<2	247	10.55	<.01	0.02	16.93	0.05	<.01	17	N/A	<10
R0800979	A10033767A	3	<2	111	1.04	<.01	0.03	33.08	0.04	0.01	245	N/A	14
R0800980	A10033768A	<2	<2	258	10.31	<.01	0.06	20.35	0.05	0.01	239	N/A	55
R0800981	A10033769A	<2	<2	230	12.76	<.01	0.02	19.79	0.06	0.01	36	N/A	<10
R0800982	A10033770A	<2	<2	429	0.85	0.01	0.49	0.51	0.05	0.02	<10	N/A	493
R0800983	A10033771A	<2	<2	239	12.31	<.01	0.02	19.34	0.06	<.01	120	N/A	32
R0800984	A10033772A	2	<2	278	11.03	<.01	0.02	20.23	0.05	<.01	135	N/A	23
R0800985	A10033773A	5	<2	368	10.43	<.01	0.04	23.65	0.05	<.01	158	N/A	66
R0800986	A10033774A	3	<2	416	7.73	<.01	0.13	22.98	0.04	0.02	531	N/A	94
R0800987	A10033775A	2	<2	194	6.58	<.01	0.11	19.89	0.04	0.04	870	N/A	105
R0800988	A10033776A	2	<2	223	11.26	<.01	0.05	22.65	0.05	0.02	221	N/A	51
R0800989	A10033777A	4	<2	308	10.25	<.01	0.06	25.52	0.04	<.01	94	N/A	128
R0800990	A10033778A	<2	<2	319	12.97	<.01	0.02	23.44	0.05	<.01	32	N/A	<10
R0800991	A10033779A	<2	<2	181	5.97	<.01	0.08	11.00	0.06	0.01	37	N/A	61

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R0800992	A10033780A	<2	<2	467	8.44	<.01	0.06	21.95	0.06	0.01	684	N/A	126
R0800993	10033780 GDL DUP	2	<2	519	8.21	<.01	0.06	25.90	0.06	0.01	739	N/A	123
R0800994	A10033781A	2	<2	648	9.06	<.01	0.06	24.73	0.06	0.01	55	N/A	86
R0800995	A10033782A	<2	<2	381	6.91	<.01	0.09	18.79	0.06	0.03	121	N/A	50
R0800995 rpt		<2	<2	393	6.74	<.01	0.09	18.89	0.05	0.03	134		54
R0800996	A10033783A	2	<2	279	9.28	<.01	0.07	23.14	0.06	0.03	302	N/A	55
R0800997	A10033784A	3	<2	643	8.53	<.01	0.02	30.20	0.05	0.01	70	N/A	37
R0800998	A10033785A	<2	<2	704	1.35	0.02	0.79	1.32	0.05	0.08	<10	N/A	764
R0800999	A10033786A	5	<2	370	12.43	<.01	0.03	27.93	0.06	0.01	198	N/A	17
R0801000	A10033787A	3	<2	379	10.81	<.01	0.06	26.10	0.06	0.03	229	N/A	42
R0801001	A10033788A	3	<2	325	11.72	<.01	0.04	21.65	0.05	0.02	71	N/A	16
R0801002	A10033789A	2	<2	315	12.00	<.01	0.04	22.34	0.05	0.02	50	N/A	22
R0801003	A10033790A	<2	<2	271	12.64	<.01	0.04	19.61	0.06	0.01	50	N/A	12
R0801004	A10033791A	2	<2	274	12.31	<.01	0.04	18.93	0.06	0.02	88	N/A	23
R0801005	A10033792A	2	<2	284	13.10	<.01	0.04	19.73	0.06	0.02	177	N/A	26
R0801006	A10033793A	2	<2	239	12.43	<.01	0.04	19.86	0.06	0.02	244	N/A	32
R0801007	A10033794A	2	<2	240	13.43	<.01	0.02	20.37	0.06	0.01	25	N/A	21
R0801007 rpt		<2	<2	242	13.13	<.01	0.02	19.93	0.07	0.01	24		30
R0801008	A10033795A	<2	<2	296	13.39	<.01	0.01	19.71	0.07	0.01	40	N/A	116
R0801009	A10033796A	2	<2	314	11.61	<.01	0.03	20.75	0.06	0.01	54	N/A	424
R0801010	A10033801A	<2	<2	591	1.29	0.02	0.73	1.11	0.05	0.08	<10	N/A	665
R0801011	A10033802A	<2	<2	409	13.14	<.01	0.01	30.30	0.06	0.01	22	N/A	<10
R0801012	A10033803A	<2	<2	414	12.97	<.01	0.03	28.82	0.06	0.02	39	N/A	71
R0801013	A10033804A	2	<2	348	7.67	<.01	0.04	23.22	0.05	0.01	71	N/A	285
R0801014	A10033805A	10	<2	1003	0.93	<.01	0.04	47.99	0.06	0.03	661	N/A	<10
STD: DA		9	16	661	0.62	0.09	2.22	0.53	0.06	0.14	1120		
STD: DA		8	17	618	0.61	0.08	2.03	0.55	0.06	0.14	1030		
STD: DA		8	14	570	0.55	0.08	1.88	0.49	0.05	0.12	944		
STD: DA		8	17	633	0.50	0.04	1.73	0.50	0.03	0.12	997		
STD: MS2													80

REMAC ZINC CORP.-X08

Ref/I.D.: A10032715-750 / 10033
Report Date: 17 JAN 2008
GDL Job No: V08-0016R

LAB NO	FIELD NUMBER	Y ppm	La ppm	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb

I=insufficient sample
If requested analyses are not shown, re

ANALYTICAL METHODS

ICP-OES PACKAGE : 0.5 gram sampl

ASSIGNED FOR ASSAYING

COMMENTS:

Ge analysis is not able to be provided

REMAC ZINC CORP.-X07

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Ref/I.D.: 2451A TO 2463A
Report Date: 01 APR 2008
GDL Job No: V07-0688R

LAB NO	FIELD NUMBER	Pb(A) %	Zn(A) %	Fe(T) %	Ag(2) g/t	Cd(A) %	Ge(A) %
R0747065	GDL PREP BLANK	<0.01	0.01	4.53	<0.4	<0.01	
R0747066	2451A	0.02	0.06	0.62	13.2	<0.01	
R0747066 rpt					13.2		
R0747067	2452	1.36	0.05	10.04	<0.4	<0.01	
R0747067 rpt		1.35	0.04	10.03		<0.01	
R0747068	2453	2.98	0.18	25.12	26.8	<0.01	
R0747069	2454A	0.42	0.11	3.68	4.1	<0.01	
R0747073	2458	0.14	0.16	2.02	4.8	<0.01	
R0747074	2459	0.12	0.37	1.20	1.2	<0.01	
R0747075	2460	0.69	5.11	6.51	6.5	0.04	0.002
R0747076	2461	0.64	2.48	3.80	5.9	0.01	0.001
R0747076 rpt		0.64	2.48	3.81	5.8	0.01	
R0747077	2462	0.03	0.75	1.20	<0.4	<0.01	
R0747078	2463A	0.22	1.50	6.55	2.1	0.01	
STD: CDN-FCM-1		0.51	1.91	33.06	80.0	<0.01	

I=insufficient sample
If requested analyses are not shown, results are to follow

ANALYTICAL METHODS

- Pb(A) Assay
- Zn(A) Assay
- Fe(T) Assay / Total Iron
- Ag(2) Acid decomposition / AAS
- Cd(A) Assay
- Ge(A) Acid decomposition / solvent extraction / AAS

REMAC ZINC CORP.-X07

Ref/I.D.: 2451A TO 2463A
Report Date: 14 FEB 2008
GDL Job No: V07-0688R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm
R0747070	2455A	5	2696	1242	6.0	37	147	13	1	59	4.99	57	41	<5	<5	62	<2	<2	92	2	<2
R0747071	2456	3	4463	1673	6.2	62	87	17	7	171	6.65	163	25	<5	<5	59	<2	<2	106	2	3
R0747072	2457	1	184	2151	0.8	22	26	18	1	48	1.51	48	4	<5	<5	30	<2	<2	203	2	2
R0747072 rpt																					
R0747073	2458	1	1361	1599	5.8	28	33	14	2	65	1.93	17	4	11	<5	29	<2	<2	226	2	2
R0747074	2459	<1	1222	3866	2.5	17	128	32	<1	26	1.15	7	7	<5	<5	34	<2	<2	266	4	3
R0747074 rpt																					
R0747075	2460	3	7358	52800	8.2	17	57	414	1	28	6.26	10	14	<5	<5	25	<2	<2	158	4	4
R0747075 rpt		3	8976	58980	7.9	20	53	494	2	33	6.19	12	18	<5	<5	27	<2	<2	156	5	4
R0747076	2461	3	7455	29910	7.3	18	72	249	1	34	3.88	13	14	<5	5	42	<2	<2	230	3	3
R0747077	2462	<1	425	9509	0.7	8	33	77	<1	11	1.17	4	<4	<5	<5	24	<2	<2	173	<2	2
R0747077 rpt																					
R0747078	2463A	1	2584	18300	3.3	26	47	149	2	57	5.96	22	12	<5	<5	33	<2	<2	244	3	2
STD: DA		130	240	732	5.7	52	593	6	13	44	3.76	3	47	<5	<5	74	3	<2	41	9	20
STD: RDC																					
STD: MS2																					

I=insufficient sample
If requested analyses are not shown, results are to follow

ANALYTICAL METHODS

ICP-OES PACKAGE : 0.5 gram sample digested in hot reverse aqua regia (soil,silt) or hot Aqua Regia(rocks).

REMAC ZINC CORP.-X07

Ref/I.D.: 2451A TO 2463A
Report Date: 14 FEB 2008
GDL Job No: V07-0688R

LAB NO	FIELD NUMBER	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0747070	2455A	251	8.93	<.01	0.03	15.48	0.03	0.01	19	3	102
R0747071	2456	234	9.48	<.01	0.03	17.39	0.04	<.01	26	3	203
R0747072	2457	277	10.90	<.01	0.01	19.05	0.02	<.01	34	3	118
R0747072 rpt										3	
R0747073	2458	286	10.68	<.01	0.02	19.88	0.03	<.01	137	3	68
R0747074	2459	314	10.18	<.01	0.03	20.68	0.03	<.01	83	3	97
R0747074 rpt											100
R0747075	2460	289	8.28	<.01	0.04	18.12	0.02	<.01	71	3	1381
R0747075 rpt		319	8.07	<.01	0.05	22.25	0.02	<.01	81		
R0747076	2461	335	9.77	<.01	0.06	21.12	0.02	<.01	53	3	677
R0747077	2462	297	10.93	<.01	0.02	22.70	0.02	<.01	25	3	213
R0747077 rpt										3	
R0747078	2463A	294	8.19	<.01	0.02	20.63	0.02	<.01	71	3	426
STD: DA		730	0.62	0.10	1.88	0.61	0.08	0.15	1019		
STD: RDC										74	
STD: MS2											74

I=insufficient sample
If requested analyses are not sl

ANALYTICAL METHODS
ICP-OES PACKAGE : 0.5 gran

REMAC ZINC CORP.-X07

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Global Discovery Labs

Ref/I.D.: #A10032464A-A10032469A
Report Date: 9 AUG 2007
GDL Job No: V07-0748R

LAB NO	FIELD NUMBER	Au ppb	Wt Au gram
R0751719	A10032464A	<10	5
R0751720	A10032465A	<10	5
R0751721	A10032466A	<10	5
R0751722	A10032467A	<10	5
R0751723	A10032468A	<10	5
R0751724	A10032469A	<10	5

I=insufficient sample
If requested analyses are not shown, results are to follow

ANALYTICAL METHODS
Au Aqua regia decomposition / solvent extraction / AAS
Wt Au The weight of sample taken to analyse for gold (geochem)

REMAC ZINC CORP.-X07

Ref/I.D.: #A10032464A-A10032469A
Report Date: 14 FEB 2008
GDL Job No: V07-0748R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm
R0751719	A10032464A	10	<4	6	0.8	21	581	<1	<1	8	0.86	14	121	<5	5	36	<2	<2	12	<2	12
R0751720	A10032465A	31	<4	60	0.6	36	60	<1	6	66	1.91	26	89	<5	<5	77	<2	<2	32	2	9
R0751721	A10032466A	80	9	67	1.0	25	224	<1	2	46	1.05	20	86	<5	6	106	<2	<2	69	3	2
R0751722	A10032467A	105	21	100	1.1	32	96	<1	1	36	3.86	8	102	5	<5	66	<2	<2	245	5	13
R0751722 rpt																					
R0751723	A10032468A	18	<4	34	<0.4	3	244	<1	6	15	1.49	<2	91	<5	<5	15	<2	<2	52	2	12
R0751724	A10032469A	16	4	39	<0.4	9	476	<1	12	28	2.95	<2	91	<5	<5	76	<2	<2	160	9	34
STD: DA		130	218	631	6.0	50	480	3	11	44	3.47	4	42	<5	<5	67	3	<2	39	8	17
STD: MS2																					

I=insufficient sample N/A=not available
If requested analyses are not shown, results are to follow

ANALYTICAL METHODS

ICP-OES PACKAGE : 0.5 gram sample digested in hot reverse aqua regia (soil,silt) or hot Aqua Regia(rocks).

COMMENTS:

Ge analysis is not able to be provided.

REMAC ZINC CORP.-X07

Ref/I.D.: #A10032464A-A1
Report Date: 14 FEB 2008
GDL Job No: V07-0748R

LAB NO	FIELD NUMBER	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0751719	A10032464A	7	0.01	<.01	0.23	0.02	0.04	0.23	121	N/A	64
R0751720	A10032465A	<5	0.02	<.01	0.36	0.02	0.03	0.15	476	N/A	53
R0751721	A10032466A	6	<.01	0.02	0.89	0.06	0.04	0.09	1007	N/A	55
R0751722	A10032467A	6	0.02	<.01	0.33	0.05	0.06	0.35	2675	N/A	56
R0751722 rpt											48
R0751723	A10032468A	580	0.56	<.01	0.33	1.32	0.11	0.01	140	N/A	<10
R0751724	A10032469A	341	1.33	0.24	2.00	1.56	0.22	0.87	2925	N/A	<10
STD: DA		653	0.58	0.09	1.97	0.52	0.05	0.13	1035		
STD: MS2											74

I=insufficient sample N/A=not
If requested analyses are not sl

ANALYTICAL METHODS
ICP-OES PACKAGE : 0.5 gran

COMMENTS:
Ge analysis is not able to be p

REMAC ZINC CORP.-X07

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Global Discovery Labs

Ref/I.D.: #A10032470 - A10032500
Report Date: 01 APR 2008
GDL Job No: V07-1024R

LAB NO	FIELD NUMBER	Pb(A) %	Zn(A) %	Ag(2) g/t	Cd(A) %	Fe(T) %	Ge(A) %
R0761261	GDL PREP BLANK	<0.01	0.01	<0.4	<0.005	1.82	
R0761262	A10032470	<0.01	0.10	3.1	<0.005	1.65	
R0761263	A10032471	<0.01	<0.01	0.5	<0.005	1.49	
R0761264	A10032472	0.10	0.56	1.0	0.005	1.75	
R0761265	A10032473	0.10	4.69	1.9	0.037	4.20	<0.001
R0761266	A10032474	<0.01	0.31	0.5	0.007	0.70	
R0761267	A10032475	0.01	0.02	0.6	<0.005	0.69	
R0761268	A10032476	<0.01	<0.01	<0.4	0.005	0.18	
R0761268 rpt				<0.4			
R0761269	A10032477	<0.01	<0.01	0.4	<0.005	3.65	
R0761270	A10032478	1.84	0.38	3.3	0.008	1.78	0.008
R0761270 rpt		1.89	0.38		0.007	1.76	
R0761271	A10032479	3.60	1.43	7.7	0.019	4.91	0.009
R0761271 rpt							0.009
R0761272	A10032480	4.24	3.73	13.3	0.045	2.59	0.005
R0761273	A10032481	<0.01	<0.01	<0.4	0.005	3.45	
R0761274	A10032482	0.96	1.26	369.9	0.020	7.09	
R0761275	A10032483	0.15	0.67	1.7	0.013	1.86	
R0761276	A10032484	0.04	0.04	0.6	0.007	0.93	
R0761277	A10032485	0.08	0.15	0.9	0.008	3.40	
R0761278	A10032486	0.03	0.03	<0.4	0.007	1.20	
R0761279	A10032487	0.25	0.48	2.6	0.014	6.15	
R0761280	A10032488	0.53	0.37	6.6	0.007	2.74	
R0761280 rpt		0.52	0.37		0.007	2.80	
R0761281	A10032489	0.80	0.11	1.1	0.010	1.33	
R0761282	A10032490	0.37	0.11	3.6	0.011	2.20	
R0761283	A10032491	0.06	0.01	0.7	0.008	4.82	
R0761284	A10032492	<0.01	<0.01	<0.4	0.008	3.29	
R0761285	A10032493	0.28	2.86	61.2	0.018	32.35	0.016
R0761286	A10032494	0.87	0.47	8.6	0.016	2.50	
R0761287	A10032495	0.68	0.69	7.4	0.017	4.71	
R0761288	A10032496	0.63	0.80	10.0	0.019	3.70	
R0761288 rpt				10.0			

REMAC ZINC CORP.-X07

teckcominco
Global Discovery Labs

Ref/I.D.: #A10032470 - A10032500
Report Date: 01 APR 2008
GDL Job No: V07-1024R

LAB NO	FIELD NUMBER	Pb(A) %	Zn(A) %	Ag(2) g/t	Cd(A) %	Fe(T) %	Ge(A) %
R0761289	A10032497	0.36	0.50	4.8	0.009	2.03	
R0761290	A10032498	0.03	0.11	<0.4	0.005	0.67	
R0761291	A10032499	0.02	0.08	<0.4	<0.005	1.18	
R0761292	A10032500	<0.01	0.08	<0.4	0.005	0.36	
STD: CDN-FCM-1				80.5			
STD: HLLC		0.25	2.89		0.010	32.40	

I=insufficient sample
If requested analyses are not shown, results are to follow

ANALYTICAL METHODS

- Pb(A) Assay
- Zn(A) Assay
- Ag(2) Acid decomposition / AAS
- Cd(A) Assay
- Fe(T) Assay / Total Iron
- Ge(A) Acid decomposition / solvent extraction / AAS

REMAC ZINC CORP.-X07

Ref/I.D.: #A10032470 - A10032500
Report Date: 14 FEB 2008
GDL Job No: V07-1024R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm
R0761261	GDL PREP BLANK	1	4	59	<0.4	<2	255	<1	4	9	2.00	<2	90	<5	<5	46	<2	<2	64	6	9
R0761262	A10032470	158	14	978	2.4	22	76	13	6	82	1.74	22	70	<5	6	341	<2	2	149	12	7
R0761263	A10032471	8	7	37	<0.4	4	213	<1	7	14	1.62	<2	10	<5	<5	<2	<2	<2	238	9	4
R0761264	A10032472	11	878	2401	<0.4	10	94	18	1	13	1.85	2	6	<5	<5	15	<2	<2	382	4	3
R0761265	A10032473	6	871	43980	0.9	27	30	338	1	28	4.41	9	11	<5	<5	18	<2	<2	465	4	4
R0761266	A10032474	<1	53	3112	<0.4	4	48	23	<1	7	0.72	<2	5	<5	<5	16	<2	<2	416	2	2
R0761267	A10032475	<1	37	281	<0.4	3	32	2	<1	7	0.83	<2	<4	<5	<5	14	<2	<2	244	<2	<2
R0761267 rpt																					
R0761268	A10032476	<1	18	72	<0.4	4	62	1	<1	4	0.20	<2	<4	<5	<5	8	<2	<2	258	<2	<2
R0761269	A10032477	31	9	63	<0.4	12	498	<1	19	32	3.67	<2	86	<5	<5	87	<2	4	195	9	42
R0761270	A10032478	23	18210	4087	2.3	12	44	39	<1	13	1.88	3	42	<5	<5	458	<2	2	92	4	5
R0761271	A10032479	13	37350	16400	7.0	33	48	151	3	52	6.03	8	33	<5	5	141	<2	25	134	8	8
R0761272	A10032480	25	44830	42220	13.0	23	41	447	5	33	3.05	10	14	<5	6	81	<2	<2	149	6	9
R0761273	A10032481	24	113	116	<0.4	8	778	<1	19	28	4.37	<2	102	<5	<5	97	<2	5	176	13	65
R0761274	A10032482	480	9847	15430	203.1	4460	29	184	11	29	7.92	8	27	<5	55	40	3	<2	74	5	2
R0761275	A10032483	13	1612	8344	1.0	35	43	86	<1	50	2.22	10	20	<5	<5	84	<2	<2	173	6	5
R0761275 rpt																					
R0761276	A10032484	2	451	562	<0.4	20	41	7	<1	41	1.11	5	11	<5	<5	27	<2	<2	127	3	2
R0761277	A10032485	23	879	2047	0.9	34	52	21	<1	49	3.85	8	62	<5	<5	109	<2	<2	120	6	5
R0761278	A10032486	5	273	524	<0.4	10	24	5	<1	13	1.39	<2	9	<5	<5	32	<2	<2	93	3	<2
R0761278 rpt		5	248	426	<0.4	8	21	5	<1	12	1.24	<2	11	<5	<5	27	<2	<2	89	3	2
R0761279	A10032487	27	2922	6878	1.6	63	57	78	2	113	7.27	17	63	<5	<5	343	<2	3	119	7	3
R0761280	A10032488	43	6540	6013	5.1	39	37	60	9	65	3.72	18	20	<5	8	105	<2	7	129	6	5
R0761281	A10032489	14	793	1111	<0.4	17	20	14	1	18	1.58	<2	<4	<5	<5	17	<2	11	104	3	2
R0761282	A10032490	8	3508	1177	2.4	28	23	19	4	37	2.46	3	6	<5	<5	23	<2	4	114	3	3
R0761283	A10032491	41	668	194	<0.4	7	905	2	26	111	5.91	<2	285	<5	<5	127	<2	6	297	8	24
R0761284	A10032492	25	16	55	<0.4	11	383	<1	14	36	3.24	<2	91	<5	<5	66	<2	3	203	10	52
R0761285	A10032493	13870	2302	26750	55.2	43	<5	79	130	18	33.91	9	29	52	<5	10	4	4	3	4	<2
R0761286	A10032494	20	7738	4369	7.8	26	23	60	4	34	2.60	3	9	<5	5	46	<2	2	126	5	5
R0761286 rpt		17	8769	5382	7.4	27	20	64	5	39	2.50	4	9	<5	5	48	<2	<2	129	6	5
R0761287	A10032495	17	7326	8552	6.7	42	95	99	9	63	5.71	6	24	<5	<5	42	<2	3	155	7	7
R0761288	A10032496	21	6439	9390	9.7	33	35	101	10	64	3.81	13	17	<5	6	57	<2	3	185	10	8
R0761288 rpt																					

REMAC ZINC CORP.-X07

Ref/I.D.: #A10032470 - A10032500
Report Date: 14 FEB 2008
GDL Job No: V07-1024R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm
R0761289	A10032497	21	3752	5906	5.3	23	27	68	3	44	2.35	18	15	<5	<5	64	<2	2	187	7	6
R0761290	A10032498	6	303	1204	<0.4	4	111	12	1	13	0.70	4	28	<5	<5	31	<2	<2	150	4	5
R0761291	A10032499	13	239	978	<0.4	4	398	10	5	31	1.30	6	71	<5	<5	57	<2	<2	204	6	11
R0761292	A10032500	2	84	937	<0.4	4	10	10	<1	7	0.40	3	6	<5	<5	19	<2	<2	136	3	3
STD: DA		135	237	679	5.3	51	519	4	12	43	3.80	3	41	<5	<5	66	<2	<2	38	8	18
STD: MS2																					

I=insufficient sample N/A=not available
If requested analyses are not shown, results are to follow

ANALYTICAL METHODS

ICP-OES PACKAGE : 0.5 gram sample digested in hot reverse aqua regia (soil,silt) or hot Aqua Regia(rocks).

COMMENTS:

Ge analysis is not able to be provided.

REMAC ZINC CORP.-X07

Ref/I.D.: #A10032470 - A1
Report Date: 14 FEB 2008
GDL Job No: V07-1024R

LAB NO	FIELD NUMBER	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0761261	GDL PREP BLANK	642	0.70	0.15	1.21	0.84	0.08	0.45	850	N/A	<10
R0761262	A10032470	76	0.67	0.01	0.61	2.10	0.08	0.48	4818	N/A	145
R0761263	A10032471	308	0.43	<.01	0.17	20.81	0.06	0.12	406	N/A	<10
R0761264	A10032472	408	9.75	<.01	0.04	18.73	0.06	0.03	42	N/A	70
R0761265	A10032473	399	8.90	<.01	0.02	19.37	0.05	0.01	46	N/A	1214
R0761266	A10032474	383	10.51	<.01	0.02	21.40	0.04	<.01	19	N/A	73
R0761267	A10032475	496	12.11	<.01	0.01	24.07	0.05	<.01	18	N/A	14
R0761267 rpt											11
R0761268	A10032476	250	2.70	<.01	0.01	30.82	0.04	<.01	19	N/A	<10
R0761269	A10032477	482	1.51	0.19	1.44	2.09	0.25	0.94	3036	N/A	<10
R0761270	A10032478	444	9.13	<.01	0.03	16.51	0.06	0.01	1250	N/A	135
R0761271	A10032479	694	8.72	<.01	0.05	17.10	0.06	0.02	2447	N/A	434
R0761272	A10032480	409	9.62	<.01	0.04	19.17	0.05	0.03	656	N/A	997
R0761273	A10032481	529	1.55	0.22	1.35	2.26	0.20	1.05	3127	N/A	<10
R0761274	A10032482	1356	0.49	0.05	0.70	1.61	0.10	0.16	489	N/A	457
R0761275	A10032483	435	11.56	<.01	0.04	24.52	0.05	0.02	739	N/A	155
R0761275 rpt											162
R0761276	A10032484	320	12.43	<.01	0.05	24.45	0.05	0.03	141	N/A	19
R0761277	A10032485	273	8.87	<.01	0.06	20.50	0.05	0.02	3489	N/A	48
R0761278	A10032486	429	12.14	<.01	0.02	23.48	0.05	<.01	196	N/A	12
R0761278 rpt		368	10.31	<.01	0.01	19.28	0.04	<.01	177		
R0761279	A10032487	370	9.71	<.01	0.08	21.37	0.05	0.04	1174	N/A	170
R0761280	A10032488	511	12.18	<.01	0.06	25.93	0.05	0.02	295	N/A	241
R0761281	A10032489	314	10.85	<.01	0.04	17.77	0.05	0.02	60	N/A	79
R0761282	A10032490	294	10.68	<.01	0.06	17.37	0.05	0.02	111	N/A	88
R0761283	A10032491	943	4.05	0.28	2.00	6.39	0.11	0.85	3242	N/A	17
R0761284	A10032492	441	1.36	0.20	1.54	1.75	0.20	0.61	3645	N/A	<10
R0761285	A10032493	589	1.07	0.01	0.64	0.78	0.06	0.06	82	N/A	581
R0761286	A10032494	337	10.15	<.01	0.06	17.30	0.05	0.02	1046	N/A	305
R0761286 rpt		379	9.52	<.01	0.06	21.63	0.04	0.02	1120		
R0761287	A10032495	460	9.10	0.03	0.29	20.51	0.06	0.10	1340	N/A	406
R0761288	A10032496	430	8.57	<.01	0.06	21.45	0.04	0.02	2836	N/A	389
R0761288 rpt											327

REMAC ZINC CORP.-X07

Ref/I.D.: #A10032470 - A1
Report Date: 14 FEB 2008
GDL Job No: V07-1024R

LAB NO	FIELD NUMBER	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0761289	A10032497	365	10.80	<.01	0.04	21.22	0.05	0.01	654	N/A	192
R0761290	A10032498	395	10.09	0.01	0.15	20.46	0.04	0.06	352	N/A	32
R0761291	A10032499	529	9.80	0.06	0.51	20.26	0.05	0.21	1059	N/A	30
R0761292	A10032500	276	11.42	<.01	0.02	21.68	0.04	<.01	224	N/A	21
STD: DA		706	0.61	0.08	1.14	0.52	0.09	0.17	955		
STD: MS2											74

I=insufficient sample N/A=not

If requested analyses are not sl

ANALYTICAL METHODS

ICP-OES PACKAGE : 0.5 gran

COMMENTS:

Ge analysis is not able to be p

REMAC ZINC CORP.-X07

teckcominco
Global Discovery Labs

Ref/I.D.: #A10032470 - A10032500
Report Date: 01 APR 2008
GDL Job No: V07-1073R

LAB NO	FIELD NUMBER	Pb(A) %	Zn(A) %	Ag(2) g/t	Cd(A) %	Fe(T) %	Ge(A) %
R0762129	A10032501	<0.01	0.03	<0.4	0.009	0.53	
R0762130	A10032502	0.14	0.81	2.2	0.017	4.13	
R0762131	A10032503	<0.01	<0.01	<0.4	0.009	1.99	
R0762132	A10032504	<0.01	<0.01	<0.4	0.011	0.33	
R0762132 rpt		<0.01	<0.01	<0.4	0.011	0.33	
R0762133	A10032505	0.14	10.97	2.9	0.113	4.98	0.003
R0762134	A10032506	0.01	0.64	<0.4	0.016	0.95	

I=insufficient sample
If requested analyses are not shown, results are to follow

ANALYTICAL METHODS

- Pb(A) Assay
- Zn(A) Assay
- Ag(2) Acid decomposition / AAS
- Cd(A) Assay
- Fe(T) Assay / Total Iron
- Ge(A) Acid decomposition / solvent extraction / AAS

REMAC ZINC CORP.-X07

Ref/I.D.: #A10032470 - A10032500
Report Date: 13 NOV 2007
GDL Job No: V07-1073R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm
R0762129	A10032501	1	8	301	<0.4	5	17	3	<1	4	0.46	<2	<4	<5	<5	8	<2	<2	106	2	3
R0762130	A10032502	10	1205	8203	1.0	30	32	73	4	27	3.76	9	12	<5	<5	14	<2	<2	104	5	6
R0762131	A10032503	7	22	96	<0.4	32	51	<1	8	26	1.78	<2	11	<5	<5	<2	<2	<2	99	8	4
R0762132	A10032504	2	11	61	<0.4	4	17	<1	1	4	0.32	<2	5	<5	<5	<2	<2	<2	135	2	3
R0762133	A10032505	19	1198	105500	1.0	13	13	1030	3	13	4.31	2	11	<5	<5	2	<2	<2	88	5	4
R0762134	A10032506	1	102	8960	<0.4	6	14	52	<1	5	0.92	<2	7	<5	<5	3	<2	<2	125	4	5
STD: DA		136	223	699	5.8	59	389	3	12	50	3.32	3	42	<5	<5	72	2	<2	31	9	17

I=insufficient sample N/A=not available
If requested analyses are not shown, results are to follow

ANALYTICAL METHODS

ICP-OES PACKAGE : 0.5 gram sample digested in hot reverse aqua regia (soil,silt) or hot Aqua Regia(rocks).

COMMENTS:

Ge analysis is not able to be provided.

REMAC ZINC CORP.-X07

Ref/I.D.: #A10032470 - A1
Report Date: 13 NOV 2007
GDL Job No: V07-1073R

LAB NO	FIELD NUMBER	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0762129	A10032501	225	11.46	<.01	0.02	19.70	0.04	0.01	97	N/A	16
R0762130	A10032502	259	9.81	<.01	0.08	17.97	0.04	0.03	300	N/A	110
R0762131	A10032503	231	7.57	<.01	0.18	15.32	0.05	0.09	156	N/A	13
R0762132	A10032504	276	10.30	<.01	0.04	26.69	0.04	0.02	32	N/A	<10
R0762133	A10032505	210	8.19	<.01	0.03	18.07	0.03	0.01	43	N/A	3581
R0762134	A10032506	286	12.36	<.01	0.06	28.22	0.03	0.01	52	N/A	237
STD: DA		697	0.60	0.08	1.64	0.56	0.08	0.12	1069		

I=insufficient sample N/A=not
If requested analyses are not sl

ANALYTICAL METHODS
ICP-OES PACKAGE : 0.5 gran

COMMENTS:
Ge analysis is not able to be p

REMAC ZINC CORP.-X07

Ref/I.D.: #2507-2541
Report Date: 18 DEC 2007
GDL Job No: V07-1295R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm
R0776883	GDL PREP BLANK	1	<4	55	0.5	6	241	<1	4	5	2.12	<2	76	<5	<5	41	<2	<2	66	6	9
R0776884	2507	2	6	27	<0.4	13	41	<1	1	9	0.27	<2	<4	<5	<5	9	<2	5	312	3	3
R0776885	2508	21	18	100	<0.4	7	64	<1	12	34	3.77	<2	38	<5	<5	18	<2	<2	160	6	12
R0776886	2509	31	16	93	<0.4	9	80	<1	17	42	4.61	<2	37	<5	<5	17	<2	<2	113	9	24
R0776887	2510	22	14	59	<0.4	10	48	<1	11	26	3.32	<2	22	<5	<5	11	<2	<2	299	11	19
R0776887 rpt		22	14	59	<0.4	9	47	<1	11	27	3.42	<2	20	<5	<5	10	<2	<2	324	12	19
R0776888	2511	11	10	33	<0.4	8	27	<1	6	13	2.40	<2	13	<5	<5	8	<2	<2	453	13	8
R0776889	2512	8	6	18	<0.4	9	20	<1	2	5	0.85	<2	4	<5	<5	<2	<2	<2	448	6	4
R0776890	2513	5	4	8	<0.4	6	14	<1	1	3	0.47	<2	<4	<5	<5	<2	<2	2	454	4	4
R0776891	2514	4	7	20	<0.4	7	15	<1	1	3	0.61	<2	<4	<5	<5	<2	<2	<2	475	7	4
R0776892	2515	3	10	19	<0.4	4	17	<1	1	3	0.65	<2	<4	<5	<5	<2	<2	<2	382	8	4
R0776893	2516	13	<4	51	<0.4	5	52	<1	10	27	2.68	<2	23	<5	<5	9	<2	<2	163	7	9
R0776894	2517	19	6	44	<0.4	5	74	<1	15	33	3.04	<2	34	<5	<5	10	<2	<2	68	6	22
R0776894 rpt		18	6	46	<0.4	6	71	<1	15	34	3.08	<2	34	<5	<5	10	<2	<2	68	6	21
R0776895	2518	8	22	71	0.5	11	42	<1	4	7	1.80	<2	41	<5	<5	5	<2	<2	327	14	11
R0776896	2519	15	7	80	0.7	7	63	<1	12	30	2.87	<2	27	<5	<5	9	<2	<2	73	6	22
R0776897	2520	15	156	278	0.5	12	36	1	4	6	1.71	<2	72	<5	<5	3	<2	<2	180	10	9
R0776898	2521	19	111	171	7.0	17	59	1	4	8	2.06	<2	84	7	<5	4	<2	<2	119	9	22
R0776899	2522	21	36	44	0.7	22	67	<1	5	9	2.78	<2	94	<5	<5	5	<2	<2	132	11	20
R0776900	2523	9	37	73	0.6	7	87	<1	9	22	2.33	<2	45	<5	<5	8	<2	<2	61	5	26
R0776901	2524	15	5	39	<0.4	7	72	<1	13	26	2.73	<2	37	<5	<5	4	<2	<2	63	3	15
R0776902	2525	16	<4	28	<0.4	8	60	<1	11	23	2.75	<2	34	<5	<5	5	<2	<2	64	4	13
R0776903	2526	43	<4	23	<0.4	15	54	<1	10	38	3.56	<2	41	<5	<5	4	<2	<2	75	3	9
R0776904	2527	42	<4	17	0.5	18	57	<1	21	35	3.76	<2	22	<5	<5	5	<2	<2	66	3	9
R0776905	2528	35	<4	21	0.6	14	62	<1	10	35	2.86	<2	28	<5	<5	7	<2	<2	80	3	9
R0776905 rpt		40	<4	24	0.4	18	66	<1	12	40	3.23	<2	28	<5	<5	7	<2	<2	88	4	10
R0776906	2529	15	12	60	<0.4	12	86	<1	11	25	2.52	<2	36	<5	<5	13	<2	<2	53	4	17
R0776907	2530	13	14	93	<0.4	5	85	<1	12	27	2.89	<2	36	<5	<5	16	<2	<2	51	3	17
R0776908	2531	15	18	84	<0.4	6	95	<1	15	29	3.07	<2	40	<5	<5	17	<2	<2	61	3	15
R0776909	2532	13	15	33	<0.4	6	82	<1	12	25	2.87	<2	46	<5	<5	15	<2	<2	48	5	20
R0776910	2533	17	57	60	<0.4	7	122	<1	13	34	3.19	<2	45	<5	<5	19	<2	<2	75	4	18
R0776911	2534	13	40	72	<0.4	9	80	<1	14	26	2.82	<2	47	<5	<5	14	<2	<2	47	4	15
R0776912	2535	1	8	18	<0.4	48	63	<1	9	14	1.80	<2	42	<5	<5	3	<2	<2	54	3	18

REMAC ZINC CORP.-X07

Ref/I.D.: #2507-2541
Report Date: 18 DEC 2007
GDL Job No: V07-1295R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm
R0776913	2536	2	11	16	<0.4	41	57	<1	8	13	2.45	<2	73	<5	<5	5	<2	<2	106	5	26
R0776914	2537	16	5	30	<0.4	33	68	<1	9	17	3.67	<2	33	<5	<5	6	<2	<2	132	6	15
R0776915	2538	23	<4	33	<0.4	234	14	<1	45	18	7.36	<2	60	<5	<5	9	<2	<2	124	6	2
R0776916	2539	9	52	106	<0.4	20	81	<1	7	19	1.89	<2	35	<5	<5	4	<2	<2	62	5	18
R0776917	2540	4	59	39	0.7	749	6	<1	115	28	10.30	<2	23	<5	<5	3	<2	<2	93	6	<2
R0776918	2541	12	9	37	<0.4	115	64	<1	16	33	2.71	<2	30	<5	<5	4	<2	<2	61	4	9
STD: MS2																					
STD: DA		139	218	678	6.5	57	417	4	12	44	3.81	3	45	<5	5	69	2	<2	44	10	18

I=insufficient sample N/A=not available
If requested analyses are not shown, results are to follow

ANALYTICAL METHODS

ICP-OES PACKAGE : 0.5 gram sample digested in hot reverse aqua regia (soil,silt) or hot Aqua Regia(rocks).

COMMENTS:

Ge analysis is not able to be provided.

REMAC ZINC CORP.-X07

Ref/I.D.: #2507-2541
Report Date: 18 DEC 2007
GDL Job No: V07-1295R

LAB NO	FIELD NUMBER	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0776883	GDL PREP BLANK	598	0.61	0.14	1.09	0.57	0.09	0.53	844	N/A	<10
R0776884	2507	252	3.04	<.01	0.08	22.07	0.04	0.03	524	N/A	<10
R0776885	2508	411	1.26	0.02	1.24	5.89	0.07	0.31	510	N/A	12
R0776886	2509	727	1.12	0.05	1.51	4.73	0.06	0.54	852	N/A	<10
R0776887	2510	1073	1.00	0.02	1.17	12.32	0.06	0.38	1127	N/A	<10
R0776887 rpt		1141	1.01	0.02	1.24	13.18	0.03	0.38	1194		12
R0776888	2511	1326	1.04	<.01	0.75	19.92	0.05	0.12	1423	N/A	<10
R0776889	2512	352	0.78	<.01	0.12	22.17	0.05	0.06	351	N/A	<10
R0776890	2513	169	1.29	<.01	0.07	23.15	0.05	0.02	148	N/A	<10
R0776891	2514	573	1.50	<.01	0.07	22.32	0.02	0.02	379	N/A	<10
R0776892	2515	986	0.91	<.01	0.12	22.40	0.02	0.04	730	N/A	<10
R0776893	2516	686	0.92	0.03	1.02	8.55	0.03	0.37	578	N/A	<10
R0776894	2517	639	0.77	0.04	1.09	2.75	0.03	0.57	629	N/A	<10
R0776894 rpt		640	0.76	0.04	1.10	2.79	0.04	0.55	644		<10
R0776895	2518	1220	0.33	<.01	0.38	10.10	0.03	0.16	1893	N/A	<10
R0776896	2519	594	0.71	0.04	1.05	2.56	0.03	0.55	629	N/A	<10
R0776897	2520	530	0.28	<.01	0.30	3.00	0.04	0.10	1449	N/A	11
R0776898	2521	561	0.32	<.01	0.41	1.90	0.03	0.19	1693	N/A	<10
R0776899	2522	480	0.34	<.01	0.50	1.36	0.04	0.22	2890	N/A	<10
R0776900	2523	395	0.41	0.02	0.82	0.61	0.03	0.49	1084	N/A	<10
R0776901	2524	429	0.47	0.01	0.66	0.85	0.03	0.41	772	N/A	<10
R0776902	2525	467	0.49	0.01	0.68	0.95	0.03	0.34	863	N/A	<10
R0776903	2526	490	0.59	<.01	0.55	1.21	0.04	0.35	522	N/A	<10
R0776904	2527	443	0.57	<.01	0.60	1.06	0.03	0.34	616	N/A	<10
R0776905	2528	492	0.68	0.01	0.61	1.22	0.03	0.37	603	N/A	<10
R0776905 rpt		555	0.75	0.02	0.71	1.39	0.04	0.39	694		<10
R0776906	2529	411	0.58	0.09	1.08	0.73	0.04	0.70	868	N/A	<10
R0776907	2530	524	0.62	0.13	1.11	0.63	0.03	0.79	656	N/A	<10
R0776908	2531	492	0.61	0.13	1.20	0.73	0.04	0.85	664	N/A	<10
R0776909	2532	310	0.58	0.08	1.08	0.49	0.04	0.66	1056	N/A	<10
R0776910	2533	430	0.77	0.09	1.17	0.66	0.04	0.80	1035	N/A	<10
R0776911	2534	354	0.59	0.06	1.03	0.56	0.04	0.64	762	N/A	<10
R0776912	2535	392	0.38	<.01	0.39	0.57	0.04	0.28	483	N/A	<10

REMAC ZINC CORP.-X07

Ref/I.D.: #2507-2541
Report Date: 18 DEC 2007
GDL Job No: V07-1295R

LAB NO	FIELD NUMBER	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0776913	2536	478	0.62	<.01	0.49	1.17	0.04	0.27	827	N/A	<10
R0776914	2537	733	0.87	<.01	0.56	1.87	0.03	0.35	1288	N/A	<10
R0776915	2538	824	0.52	0.01	0.72	1.52	0.03	0.42	1435	N/A	<10
R0776916	2539	503	0.41	<.01	0.66	0.72	0.04	0.33	1111	N/A	<10
R0776917	2540	696	0.56	<.01	0.31	1.68	0.03	0.20	783	N/A	<10
R0776918	2541	411	0.44	<.01	0.55	0.88	0.04	0.38	762	N/A	<10
STD: MS2											70
STD: DA		713	0.59	0.09	1.61	0.56	0.08	0.14	1045		

I=insufficient sample N/A=not
If requested analyses are not sl

ANALYTICAL METHODS
ICP-OES PACKAGE : 0.5 gran

COMMENTS:
Ge analysis is not able to be p

REMAC ZINC CORP.-X07

Ref/I.D.: #2542-2553
Report Date: 7 JAN 2008
GDL Job No: V07-1312R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm
R0778013	GDL PREP BLANK	10	<4	53	<0.4	7	252	<1	4	6	2.10	<2	63	<5	<5	42	<2	<2	58	5	7
R0778014	2542	4	<4	8	<0.4	5	26	<1	<1	2	0.04	<2	<4	<5	<5	2	<2	<2	284	<2	<2
R0778015	2543	2	<4	12	<0.4	7	19	<1	<1	5	0.16	<2	<4	<5	<5	3	<2	2	237	<2	<2
R0778016	2544	<1	<4	5	<0.4	5	17	<1	<1	1	0.04	<2	<4	<5	<5	<2	<2	<2	273	<2	<2
R0778016 rpt		1	<4	6	<0.4	5	15	<1	<1	1	0.03	<2	<4	<5	<5	<2	<2	<2	245	<2	<2
R0778017	2545	6790	7310	56630	93.2	45	<5	168	82	18	26.10	10	30	39	<5	10	4	<2	2	2	<2
R0778018	2546	8	16	89	<0.4	40	95	<1	<1	21	1.34	9	5	<5	<5	17	<2	<2	278	6	5
R0778019	2547	6	10	55	<0.4	51	159	<1	<1	31	1.23	9	<4	<5	<5	11	<2	<2	283	3	2
R0778020	2548	4	6	35	<0.4	45	213	<1	<1	28	0.94	4	<4	<5	<5	4	<2	<2	250	2	2
R0778021	2549	5	8	51	<0.4	49	111	<1	<1	25	1.15	12	<4	<5	<5	5	<2	<2	263	2	<2
R0778022	2550	3	6	37	<0.4	60	185	<1	<1	32	0.87	13	<4	<5	<5	4	<2	<2	263	<2	<2
R0778023	2551	1	<4	23	<0.4	49	253	<1	<1	31	0.29	7	<4	<5	<5	6	<2	<2	286	<2	<2
R0778024	2552	1	9	48	<0.4	7	170	<1	<1	5	0.41	<2	9	<5	<5	12	<2	<2	355	4	4
R0778025	2553	15	17	117	<0.4	15	204	1	1	33	0.61	5	15	<5	<5	27	<2	<2	473	10	7
STD: DA		132	226	702	5.6	58	480	4	12	43	3.67	4	43	<5	5	68	<2	<2	41	9	17

I=insufficient sample N/A=not available
If requested analyses are not shown, results are to follow

ANALYTICAL METHODS

ICP-OES PACKAGE : 0.5 gram sample digested in hot reverse aqua regia (soil,silt) or hot Aqua Regia(rocks).

COMMENTS:

Ge analysis is not able to be provided.

REMAC ZINC CORP.-X07

Ref/I.D.: #2542-2553
Report Date: 7 JAN 2008
GDL Job No: V07-1312R

LAB NO	FIELD NUMBER	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0778013	GDL PREP BLANK	602	0.62	0.14	1.05	0.52	0.08	0.55	828	N/A	10
R0778014	2542	17	1.02	<.01	0.01	24.90	0.02	<.01	38	N/A	10
R0778015	2543	28	1.37	<.01	0.04	22.43	0.02	0.03	56	N/A	12
R0778016	2544	14	0.97	<.01	0.01	25.82	0.02	<.01	20	N/A	12
R0778016 rpt		14	0.85	<.01	0.01	25.43	0.02	<.01	22		13
R0778017	2545	546	0.70	<.01	0.50	0.39	0.03	0.01	56	N/A	715
R0778018	2546	72	5.18	<.01	0.08	20.17	0.02	0.03	2193	N/A	39
R0778019	2547	44	3.27	<.01	0.04	21.47	0.02	0.01	1142	N/A	30
R0778020	2548	46	2.70	<.01	0.03	20.81	0.02	0.01	310	N/A	29
R0778021	2549	36	2.32	<.01	0.03	22.13	0.02	<.01	342	N/A	14
R0778022	2550	36	2.79	<.01	0.02	23.15	0.02	<.01	325	N/A	14
R0778023	2551	27	2.52	<.01	0.01	24.06	0.02	<.01	153	N/A	17
R0778024	2552	103	7.46	<.01	0.06	16.87	0.02	0.01	809	N/A	12
R0778025	2553	84	1.39	<.01	0.17	22.70	0.02	0.06	5634	N/A	14
STD: DA		697	0.56	0.09	1.65	0.53	0.05	0.13	1048		

I=insufficient sample N/A=not
If requested analyses are not sl

ANALYTICAL METHODS
ICP-OES PACKAGE : 0.5 gran

COMMENTS:
Ge analysis is not able to be p

REMAC ZINC CORP.-X07

Ref/I.D.: A10032554-A10032560
Report Date: 7 JAN 2008
GDL Job No: V07-1346R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm
R0780957	A10032554A	1	53	483	<0.4	10	2126	3	<1	9	0.69	2	<4	<5	<5	17	<2	4	246	4	4
R0780958	A10032555A	<1	10	319	<0.4	13	677	2	<1	5	0.30	<2	<4	<5	<5	2	<2	4	307	3	2
R0780959	A10032556A	1	29	3441	<0.4	9	1053	39	<1	3	0.62	<2	<4	<5	<5	13	<2	<2	317	2	2
R0780959 rpt		1	24	3127	<0.4	8	923	37	<1	3	0.53	<2	<4	<5	<5	10	<2	<2	291	<2	2
R0780960	A10032557A	4	<4	21	<0.4	11	22	<1	2	8	0.70	<2	<4	<5	<5	<2	<2	3	311	4	7
R0780961	A10032558A	<1	10	283	<0.4	7	806	2	<1	3	0.53	<2	5	<5	<5	22	<2	<2	353	2	3
R0780962	A10032559A	1	35	260	<0.4	9	1367	4	<1	2	0.11	<2	<4	<5	<5	13	<2	<2	290	<2	<2
R0780963	A10032560A	719	10	18	1.5	21	22	<1	65	37	20.75	201	26	<5	<5	28	<2	<2	62	8	<2
STD: DA		123	200	580	5.0	51	422	3	10	37	3.36	4	34	<5	<5	57	<2	<2	35	8	15

I=insufficient sample N/A=not available
If requested analyses are not shown, results are to follow

ANALYTICAL METHODS

ICP-OES PACKAGE : 0.5 gram sample digested in hot reverse aqua regia (soil,silt) or hot Aqua Regia(rocks).

COMMENTS:

Ge analysis is not able to be provided.

REMAC ZINC CORP.-X07

Ref/I.D.: A10032554-A10(
Report Date: 7 JAN 2008
GDL Job No: V07-1346R

LAB NO	FIELD NUMBER	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0780957	A10032554A	276	7.43	<.01	0.14	23.70	0.02	<.01	324	N/A	29
R0780958	A10032555A	182	0.65	<.01	0.06	30.59	0.02	<.01	126	N/A	13
R0780959	A10032556A	353	9.33	<.01	0.07	22.75	0.02	<.01	41	N/A	106
R0780959 rpt		322	8.62	<.01	0.07	22.20	0.02	<.01	35		
R0780960	A10032557A	163	0.85	<.01	0.10	29.48	0.02	0.01	77	N/A	<10
R0780961	A10032558A	338	9.98	<.01	0.06	23.59	0.02	<.01	35	N/A	<10
R0780962	A10032559A	48	2.25	<.01	0.02	31.30	0.02	<.01	88	N/A	10
R0780963	A10032560A	148	0.19	0.03	1.84	1.66	0.14	0.07	304	N/A	<10
STD: DA		641	0.53	0.08	1.49	0.46	0.05	0.13	908		320

I=insufficient sample N/A=not
If requested analyses are not sl

ANALYTICAL METHODS
ICP-OES PACKAGE : 0.5 gran

COMMENTS:
Ge analysis is not able to be p

REMAC ZINC CORP.-X07

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Global Discovery Labs

Ref/I.D.: A10032561-10032714
Report Date: 01 APR 2008
GDL Job No: V07-1405R

LAB NO	FIELD NUMBER	Pb(A) %	Zn(A) %	Cd(A) %	Ag(2) g/t	Ge(A) %
R0785439	A10032661A	0.26	4.64	0.061	3.9	0.003
R0785458	A10032679A	<0.01	1.96	0.016	1.2	0.001
R0785460	A10032681A	<0.01	4.44	0.046	4.1	0.005
STD: CZN-3		0.10	50.82	0.251	43.9	

I=insufficient sample
If requested analyses are not shown, results are to follow

ANALYTICAL METHODS
- Pb(A) Assay
- Zn(A) Assay
- Cd(A) Assay
- Ag(2) Acid decomposition / AAS
- Ge(A) Acid decomposition / solvent extraction / AAS

REMAC ZINC CORP.-X07

Ref/I.D.: A10032561-10032714
Report Date: 15 JAN 2008
GDL Job No: V07-1405R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm
R0785336	GDL PREP BLANK	2	7	46	<0.4	<2	235	<1	4	5	1.82	<2	70	<5	<5	38	<2	<2	51	4	<2
R0785337	A10032561A	32	20	40	<0.4	5	43	<1	22	55	3.84	<2	14	<5	<5	6	<2	<2	298	5	20
R0785338	A10032562A	10	<4	2	<0.4	3	<5	<1	2	6	0.43	<2	71	<5	<5	<2	<2	<2	76	<2	11
R0785339	A10032563A	29	21	42	<0.4	4	46	<1	18	49	3.52	2	11	<5	<5	6	<2	<2	422	6	18
R0785339 rpt		30	22	45	<0.4	4	51	<1	19	50	3.42	2	11	<5	<5	6	<2	<2	428	6	21
R0785340	A10032564A	1	25	5143	<0.4	3	54	36	<1	3	0.71	<2	<4	<5	<5	21	<2	5	157	<2	<2
R0785341	A10032565A	1	39	675	<0.4	2	1162	5	<1	4	0.81	<2	<4	<5	<5	16	<2	<2	186	2	<2
R0785342	A10032566A	<1	111	5647	<0.4	5	2001	62	<1	5	1.28	<2	<4	5	<5	18	<2	6	184	2	<2
R0785343	A10032567A	<1	28	806	<0.4	2	1155	5	<1	1	0.61	<2	<4	<5	<5	22	<2	5	351	<2	<2
R0785344	A10032568A	1	60	910	<0.4	<2	211	9	<1	2	0.67	<2	<4	<5	<5	12	<2	5	313	<2	<2
R0785345	A10032569A	87	20	475	1.4	19	218	5	3	46	0.75	15	53	<5	9	125	<2	<2	283	19	9
R0785346	A10032570A	75	21	499	1.8	13	217	6	3	47	0.68	17	101	<5	12	132	<2	<2	157	10	13
R0785346 rpt		70	19	492	1.2	13	220	6	3	47	0.67	16	100	<5	13	139	<2	<2	157	10	13
R0785347	A10032571A	79	23	501	1.3	12	268	6	7	57	1.26	16	79	<5	6	107	<2	<2	113	8	11
R0785348	A10032572A	58	13	402	0.8	16	114	5	4	41	0.72	16	50	<5	8	53	<2	<2	90	6	13
R0785349	A10032573A	39	12	640	0.7	14	172	8	4	35	0.77	12	92	<5	6	51	<2	<2	106	5	12
R0785350	A10032574A	44	11	403	0.6	14	112	5	4	35	0.74	13	61	<5	6	32	<2	<2	68	4	13
R0785351	A10032575A	112	19	648	2.8	19	156	9	6	67	1.25	15	93	<5	6	367	<2	<2	164	16	8
R0785352	A10032576A	5	20	23	<0.4	6	10	<1	3	5	1.06	<2	<4	<5	<5	4	<2	2	347	11	<2
R0785353	A10032577A	17	31	105	<0.4	15	40	<1	21	45	4.18	<2	59	<5	<5	14	<2	<2	27	7	37
R0785353 rpt		18	29	111	<0.4	10	42	<1	19	45	4.63	<2	59	7	<5	17	<2	<2	27	7	36
R0785354	A10032578A	26	22	116	<0.4	6	38	<1	22	50	4.28	<2	46	7	<5	16	<2	<2	8	6	35
R0785355	A10032579A	<1	60	319	<0.4	2	152	4	<1	1	0.71	<2	6	<5	<5	16	<2	4	178	<2	<2
R0785356	A10032580A	4	910	221	0.7	11	469	2	2	24	2.42	<2	<4	<5	<5	61	<2	<2	148	<2	<2
R0785357	A10032581A	3	480	100	<0.4	11	553	<1	<1	6	2.22	<2	<4	<5	<5	30	<2	2	139	<2	<2
R0785358	A10032582A	7	370	418	<0.4	10	1755	4	<1	7	2.03	<2	4	<5	<5	25	<2	<2	131	<2	<2
R0785359	A10032583A	4	165	434	<0.4	5	1843	3	<1	5	1.09	<2	7	<5	<5	28	<2	<2	151	<2	<2
R0785360	A10032584A	3	110	352	<0.4	13	194	2	<1	6	1.72	<2	18	<5	<5	57	<2	<2	95	<2	<2
R0785361	A10032585A	1	105	1018	<0.4	3	142	5	<1	2	0.72	<2	9	<5	<5	33	<2	2	130	2	<2
R0785362	A10032586A	<1	136	249	<0.4	3	136	2	<1	2	0.80	<2	5	<5	<5	41	<2	3	125	2	<2
R0785363	A10032587A	1	109	252	<0.4	2	331	2	<1	3	0.51	<2	5	<5	<5	40	<2	<2	116	<2	<2
R0785364	A10032588A	<1	152	453	<0.4	7	167	9	<1	6	0.58	<2	<4	<5	<5	72	<2	2	114	<2	<2
R0785365	A10032589A	2	75	465	<0.4	8	222	7	<1	4	0.97	<2	9	<5	<5	48	<2	<2	93	<2	<2

REMAC ZINC CORP.-X07

Ref/I.D.: A10032561-10032714
Report Date: 15 JAN 2008
GDL Job No: V07-1405R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm
R0785366	A10032590A	3	98	528	<0.4	9	110	4	<1	7	1.32	<2	14	<5	<5	79	<2	3	101	<2	<2
R0785367	A10032591A	<1	175	542	0.4	12	307	1	<1	7	1.43	<2	5	<5	<5	62	<2	2	116	3	<2
R0785368	A10032592A	495	8539	9900	201.3	4023	18	141	12	25	6.98	6	25	<5	45	33	6	<2	73	4	5
R0785369	A10032593A	29	40	78	<0.4	26	459	<1	16	30	2.88	<2	78	<5	<5	70	<2	<2	168	7	29
R0785370	A10032594A	2	138	177	<0.4	32	54	1	2	32	3.84	<2	<4	<5	<5	41	<2	<2	140	2	<2
R0785371	A10032595A	3	160	339	<0.4	12	46	3	<1	5	1.85	<2	<4	<5	<5	43	<2	3	125	<2	<2
R0785372	A10032596A	2	124	657	<0.4	11	34	6	<1	4	1.40	<2	<4	<5	<5	39	<2	<2	130	<2	<2
R0785373	A10032597A	2	112	614	<0.4	8	38	4	<1	4	1.15	<2	<4	<5	<5	46	<2	4	153	<2	<2
R0785374	A10032598A	5	178	610	<0.4	12	57	4	<1	5	1.60	2	<4	<5	<5	58	<2	<2	157	2	<2
R0785375	10032598 GDL DU	3	154	610	<0.4	11	51	4	<1	5	1.57	<2	<4	<5	<5	60	<2	5	157	2	<2
R0785375 rpt		2	160	654	<0.4	12	52	4	<1	6	1.82	2	<4	<5	<5	62	<2	4	158	2	<2
R0785376	A10032599A	1	120	712	<0.4	13	35	6	<1	6	1.58	<2	<4	<5	<5	49	<2	6	157	<2	<2
R0785377	A10032600A	1	89	947	<0.4	15	40	8	<1	8	1.76	<2	<4	<5	<5	36	<2	2	151	<2	<2
R0785378	A10032601A	1	67	344	<0.4	3	29	2	<1	2	0.34	<2	<4	<5	<5	33	<2	4	149	<2	<2
R0785379	A10032602A	16	339	826	0.7	66	76	7	1	24	6.40	3	19	5	<5	151	<2	<2	108	2	<2
R0785380	A10032603A	4	68	342	<0.4	6	64	2	<1	5	0.84	<2	<4	<5	<5	62	<2	<2	141	2	<2
R0785381	A10032604A	2	82	323	<0.4	3	33	2	<1	2	0.38	<2	<4	<5	<5	49	<2	3	132	<2	<2
R0785382	A10032605A	11	283	816	0.5	61	72	7	1	30	6.04	5	23	<5	<5	175	<2	3	114	3	<2
R0785383	A10032606A	5	208	940	<0.4	23	45	9	<1	12	1.91	2	5	<5	<5	79	<2	2	137	3	<2
R0785384	A10032607A	4	167	652	<0.4	17	43	6	<1	10	1.94	<2	<4	<5	<5	58	<2	2	163	3	<2
R0785385	A10032608A	11190	2248	22870	50.7	28	7	67	99	12	21.95	6	25	44	<5	<2	8	<2	3	<2	<2
R0785386	A10032609A	34	41	284	<0.4	6	29	1	<1	2	1.08	<2	<4	<5	<5	33	<2	4	110	<2	<2
R0785387	A10032610A	5	71	509	<0.4	10	27	2	<1	3	1.70	<2	<4	<5	<5	34	<2	3	125	<2	<2
R0785388	A10032611A	7	247	1531	<0.4	30	31	12	<1	14	3.33	3	<4	<5	<5	50	<2	2	159	<2	<2
R0785388 rpt		6	262	1621	<0.4	31	33	13	<1	18	3.43	3	<4	<5	<5	54	<2	<2	168	<2	<2
R0785389	A10032612A	3	398	594	<0.4	15	41	5	3	26	1.51	4	<4	<5	<5	66	<2	3	150	2	<2
R0785390	A10032613A	1	38	698	<0.4	2	22	4	<1	2	0.51	<2	<4	<5	<5	35	<2	4	112	2	<2
R0785391	A10032614A	2	57	506	<0.4	2	21	3	<1	2	0.42	<2	<4	<5	<5	54	<2	<2	104	<2	<2
R0785392	A10032615A	2	39	187	<0.4	3	25	<1	<1	1	0.31	<2	6	<5	<5	35	<2	2	118	<2	<2
R0785393	A10032616A	9	57	352	<0.4	18	27	2	<1	3	1.00	<2	<4	<5	<5	40	<2	4	126	2	<2
R0785394	A10032617A	3	199	961	<0.4	4	31	10	<1	7	0.68	<2	<4	<5	<5	76	<2	3	169	2	<2
R0785394 rpt		3	184	985	<0.4	6	29	10	<1	7	0.67	<2	<4	<5	<5	77	<2	2	164	2	<2
R0785395	A10032618A	3	250	703	<0.4	3	25	6	<1	7	0.65	<2	<4	<5	<5	70	<2	4	136	2	<2
R0785396	A10032619A	2	329	1233	<0.4	9	15	8	1	11	1.45	<2	<4	<5	<5	33	<2	3	120	<2	<2

REMAC ZINC CORP.-X07

Ref/I.D.: A10032561-10032714
Report Date: 15 JAN 2008
GDL Job No: V07-1405R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm
R0785397	A10032620A	1	236	4073	<0.4	7	19	20	<1	7	1.37	<2	<4	<5	<5	22	<2	3	102	<2	<2
R0785398	A10032621A	2	139	3237	<0.4	3	21	15	<1	5	1.06	<2	<4	<5	<5	27	<2	4	105	<2	<2
R0785399	A10032622A	3	115	4844	<0.4	4	18	25	<1	4	1.02	<2	<4	<5	<5	27	<2	4	107	<2	<2
R0785400	A10032623A	3	433	6610	<0.4	4	25	56	<1	4	0.77	<2	<4	<5	<5	24	<2	3	111	<2	<2
R0785401	A10032624A	2	202	1513	<0.4	8	33	13	<1	9	1.39	<2	12	<5	<5	19	<2	2	104	<2	<2
R0785402	A10032625A	3	150	2613	<0.4	10	25	29	1	25	1.37	3	<4	<5	<5	26	<2	3	116	4	<2
R0785403	A10032626A	2	242	7987	0.4	6	34	95	<1	5	1.15	3	<4	<5	<5	29	<2	3	153	2	<2
R0785404	A10032627A	<1	125	1352	<0.4	8	40	10	<1	5	1.63	<2	<4	<5	<5	23	<2	2	157	2	<2
R0785405	A10032628A	2	58	305	<0.4	2	20	1	<1	3	0.71	<2	<4	<5	<5	15	<2	2	124	<2	<2
R0785406	A10032629A	1	37	469	<0.4	3	40	3	<1	2	0.76	<2	<4	<5	<5	18	<2	2	161	<2	<2
R0785407	A10032630A	1	34	243	<0.4	3	43	<1	<1	3	0.79	<2	<4	<5	<5	17	<2	2	179	<2	<2
R0785408	A10032631A	1	23	96	<0.4	<2	35	<1	<1	1	0.72	<2	<4	<5	<5	16	<2	4	170	<2	<2
R0785409	A10032632A	<1	43	291	<0.4	<2	147	5	<1	2	0.56	<2	<4	<5	<5	19	<2	4	155	<2	<2
R0785410	A10032633A	<1	61	559	<0.4	5	237	13	<1	4	0.53	<2	<4	<5	<5	14	<2	5	115	2	<2
R0785411	A10032634A	24	16	119	<0.4	13	385	1	13	24	2.62	<2	71	<5	<5	76	2	2	141	7	22
R0785412	A10032635A	1	35	149	<0.4	4	37	<1	<1	3	0.78	<2	<4	<5	<5	16	<2	3	101	<2	<2
R0785413	A10032636A	2	75	549	<0.4	3	212	5	<1	7	0.66	<2	<4	<5	<5	14	<2	2	107	3	<2
R0785414	A10032637A	<1	48	5359	<0.4	4	20	45	<1	4	0.64	<2	<4	<5	<5	13	<2	5	96	2	<2
R0785415	GDL PREP BLANK	5	5	70	<0.4	3	215	<1	4	3	1.58	<2	28	<5	<5	36	<2	<2	46	3	3
R0785416	A10032638A	13	12	44	<0.4	15	310	<1	14	26	2.19	<2	72	<5	<5	57	<2	<2	110	7	34
R0785416 rpt		14	10	49	<0.4	12	324	<1	14	28	2.36	<2	76	<5	<5	53	2	<2	110	7	32
R0785417	A10032639A	6506	5893	60660	71.3	43	<5	156	73	13	19.54	5	25	46	<5	4	8	<2	2	<2	<2
R0785418	A10032640A	26	63	530	<0.4	2	9	3	<1	3	0.65	<2	<4	<5	<5	18	<2	3	87	2	<2
R0785419	A10032641A	1	45	370	<0.4	2	13	3	<1	3	0.41	<2	<4	<5	<5	19	<2	<2	98	2	<2
R0785420	A10032642A	2	46	393	<0.4	4	13	3	<1	4	0.64	<2	<4	<5	<5	20	<2	<2	100	<2	<2
R0785421	A10032643A	3	47	393	<0.4	5	14	4	<1	5	0.45	<2	<4	<5	<5	17	<2	4	90	2	<2
R0785422	A10032644A	1	48	362	<0.4	2	16	3	<1	3	0.34	<2	<4	<5	<5	17	<2	3	88	2	<2
R0785422 rpt		3	47	332	<0.4	2	16	3	<1	3	0.30	<2	<4	<5	<5	15	<2	<2	89	<2	<2
R0785423	A10032645A	2	34	327	<0.4	<2	19	3	<1	3	0.43	<2	<4	<5	<5	11	<2	2	87	2	<2
R0785424	A10032646A	1	34	349	<0.4	<2	20	3	<1	3	0.39	<2	<4	<5	<5	14	<2	4	91	2	<2
R0785425	A10032647A	1	45	411	<0.4	4	27	3	1	4	0.63	<2	<4	<5	<5	11	<2	2	91	2	<2
R0785426	A10032648A	3	63	643	<0.4	<2	6	6	<1	2	0.48	<2	<4	<5	<5	17	<2	2	82	<2	<2
R0785427	A10032649A	450	8187	9500	149.6	4046	15	141	13	24	6.61	6	24	<5	44	31	6	<2	66	4	6
R0785428	A10032650A	5	582	1391	0.5	26	66	12	<1	11	1.72	3	4	<5	<5	68	<2	3	157	4	<2

REMAC ZINC CORP.-X07

Ref/I.D.: A10032561-10032714
Report Date: 15 JAN 2008
GDL Job No: V07-1405R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm
R0785429	A10032651A	2	222	1035	1.1	20	14	13	1	18	2.94	34	<4	<5	<5	17	<2	<2	97	<2	<2
R0785430	A10032652A	2	53	225	<0.4	<2	8	1	<1	2	0.41	<2	<4	<5	<5	17	<2	2	86	<2	<2
R0785431	A10032653A	1	64	188	<0.4	2	26	1	<1	1	0.51	<2	<4	<5	<5	16	<2	<2	76	<2	<2
R0785432	A10032654A	1	38	191	<0.4	2	94	1	<1	1	0.36	<2	<4	<5	<5	12	<2	2	79	<2	<2
R0785433	A10032655A	3	73	412	<0.4	2	11	4	<1	2	0.68	<2	<4	<5	<5	13	<2	3	89	<2	<2
R0785434	A10032656A	2	184	589	0.7	9	10	6	<1	6	2.54	<2	<4	<5	<5	13	<2	<2	84	<2	<2
R0785435	A10032657A	4	147	1414	<0.4	<2	12	15	<1	1	0.54	<2	<4	<5	<5	15	<2	4	98	<2	<2
R0785436	A10032658A	5	109	7406	0.6	10	12	105	1	9	3.10	2	<4	<5	<5	24	<2	6	101	<2	<2
R0785437	A10032659A	3	123	1297	<0.4	<2	44	14	<1	4	0.50	<2	<4	<5	<5	22	<2	6	98	<2	<2
R0785438	A10032660A	10880	2137	22220	57.2	34	6	69	105	12	21.28	6	23	44	<5	<2	7	<2	2	<2	<2
R0785439	A10032661A	46	2686	23030	2.6	28	12	654	6	21	11.85	2	14	7	<5	10	3	<2	67	<2	<2
R0785440	A10032662A	27	58	675	<0.4	13	264	9	17	31	2.31	<2	101	<5	<5	72	2	4	97	9	35
R0785441	A10032663A	3	188	456	<0.4	<2	57	4	<1	1	0.40	<2	<4	<5	<5	16	<2	<2	108	<2	<2
R0785442	A10032664A	5	3739	6753	5.0	19	18	94	1	12	4.64	3	<4	<5	<5	16	2	4	96	<2	<2
R0785443	A10032665A	4	636	1026	0.6	4	37	11	<1	2	0.97	<2	<4	<5	<5	12	<2	3	102	<2	<2
R0785444	A10032666A	20	21	57	<0.4	13	452	<1	17	28	2.95	<2	85	<5	<5	78	2	<2	205	9	40
R0785445	A10032667A	5	67	458	<0.4	4	20	5	<1	4	0.45	<2	<4	<5	<5	13	<2	4	121	<2	<2
R0785446	A10032668A	1	30	336	<0.4	<2	10	3	<1	1	0.29	<2	<4	<5	<5	10	<2	4	100	<2	<2
R0785447	A10032669A	3	45	532	<0.4	3	8	5	<1	2	0.39	<2	<4	<5	<5	13	<2	2	127	<2	<2
R0785448	A10032670A	3	236	929	<0.4	5	15	11	<1	4	0.59	<2	<4	<5	<5	13	<2	7	129	<2	<2
R0785449	A10032671A	6	1383	6385	1.4	15	21	92	2	13	4.84	3	9	<5	<5	11	2	<2	138	<2	<2
R0785450	A10032672A	5915	6583	61820	75.3	51	<5	184	103	14	21.96	5	27	51	<5	<2	8	<2	2	<2	<2
R0785451	A10032673A	12	19	258	<0.4	<2	7	2	<1	1	0.41	<2	<4	<5	<5	11	<2	4	105	<2	<2
R0785452	A10032674A	4	18	211	<0.4	<2	17	1	<1	2	0.51	<2	<4	<5	<5	9	<2	3	96	<2	<2
R0785453	A10032675A	1	10	282	<0.4	2	9	1	<1	1	0.55	<2	<4	<5	<5	10	<2	2	90	<2	<2
R0785454	A10032676A	4	20	335	<0.4	<2	14	3	1	2	0.54	<2	<4	<5	<5	8	<2	<2	106	2	<2
R0785454 rpt		2	17	271	<0.4	<2	13	2	<1	1	0.45	<2	<4	<5	<5	8	<2	2	93	<2	<2
R0785455	10032676 GDL DU	5	21	315	<0.4	<2	12	2	<1	2	0.56	<2	<4	<5	<5	11	<2	3	110	<2	<2
R0785456	A10032677A	4	16	100	<0.4	3	39	<1	2	7	0.66	<2	<4	<5	<5	7	<2	<2	198	3	<2
R0785457	A10032678A	3	23	1469	<0.4	2	23	8	3	8	0.96	<2	<4	<5	<5	6	<2	4	105	4	<2
R0785458	A10032679A	4	48	16990	0.7	3	41	153	2	4	0.78	2	<4	<5	<5	6	<2	5	112	2	<2
R0785459	A10032680A	3	12	4196	<0.4	2	13	40	1	2	0.44	<2	<4	<5	<5	10	<2	4	98	2	<2
R0785460	A10032681A	7	52	44880	4.7	2	38	485	2	3	0.61	3	<4	<5	<5	6	<2	7	123	3	<2
R0785461	A10032682A	13	12	275	<0.4	13	415	2	16	29	2.41	<2	73	<5	<5	65	<2	<2	131	7	33

REMAC ZINC CORP.-X07

Ref/I.D.: A10032561-10032714
Report Date: 15 JAN 2008
GDL Job No: V07-1405R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm
R0785462	A10032683A	2	6	65	<0.4	<2	7	<1	<1	<1	0.36	<2	<4	<5	<5	9	<2	3	68	<2	<2
R0785463	A10032684A	2	8	321	<0.4	<2	5	2	<1	1	0.45	<2	<4	<5	<5	6	<2	<2	78	<2	<2
R0785464	A10032685A	1	12	6449	<0.4	<2	7	66	<1	2	0.48	<2	<4	<5	<5	5	<2	7	73	<2	<2
R0785465	A10032686A	3	6	89	<0.4	<2	6	<1	<1	<1	0.32	<2	<4	<5	<5	7	<2	7	76	<2	<2
R0785466	A10032687A	<1	<4	306	<0.4	<2	5	1	<1	<1	0.30	<2	<4	<5	<5	6	<2	2	67	<2	<2
R0785467	A10032688A	1	6	13	<0.4	<2	5	<1	<1	1	0.30	<2	<4	<5	<5	6	<2	4	71	<2	<2
R0785467 rpt		3	4	11	<0.4	<2	5	<1	<1	<1	0.27	<2	<4	<5	<5	9	<2	2	66	<2	<2
R0785468	A10032689A	3	5	12	<0.4	<2	5	<1	<1	1	0.31	<2	<4	<5	<5	8	<2	4	68	<2	<2
R0785469	A10032690A	4	<4	33	<0.4	<2	5	<1	1	1	0.29	<2	<4	<5	<5	8	<2	4	76	<2	<2
R0785470	A10032691A	3	6	19	<0.4	<2	5	<1	<1	1	0.32	<2	<4	<5	<5	6	<2	4	77	<2	<2
R0785471	A10032692A	4	9	6	<0.4	<2	5	<1	<1	1	0.32	<2	<4	<5	<5	4	<2	2	89	<2	<2
R0785472	A10032693A	4	6	14	<0.4	<2	<5	<1	<1	2	0.27	<2	<4	<5	<5	5	<2	4	92	<2	<2
R0785473	A10032694A	3	9	57	<0.4	<2	6	<1	1	3	0.30	<2	<4	<5	<5	4	<2	2	84	<2	<2
R0785473 rpt		2	8	57	<0.4	<2	6	<1	1	2	0.30	<2	<4	<5	<5	8	<2	4	89	<2	<2
R0785474	A10032695A	4	7	5	<0.4	<2	5	<1	1	2	0.39	<2	<4	<5	<5	5	<2	4	77	<2	<2
R0785475	A10032696A	5	8	21	<0.4	3	11	<1	2	3	0.69	<2	<4	<5	<5	5	<2	3	110	3	<2
R0785476	A10032697A	3	18	30	<0.4	7	22	<1	4	8	1.58	<2	5	<5	<5	6	<2	<2	188	9	<2
R0785477	A10032698A	474	9152	10460	105.3	4420	15	159	14	27	7.07	8	28	<5	45	33	7	<2	76	5	7
R0785478	A10032699A	9	42	78	<0.4	23	22	<1	4	10	1.83	<2	<4	<5	<5	3	<2	<2	281	13	<2
R0785479	A10032700A	9	11	32	<0.4	8	52	<1	11	26	1.48	<2	27	<5	<5	8	<2	<2	40	4	33
R0785480	A10032701A	4	96	264	<0.4	7	136	2	11	12	3.88	<2	48	<5	<5	15	3	<2	97	8	13
R0785481	A10032702A	2	48	194	<0.4	3	46	1	<1	3	0.65	<2	<4	<5	<5	16	<2	6	88	<2	<2
R0785482	A10032703A	1	53	177	<0.4	<2	24	1	<1	3	0.44	<2	<4	<5	<5	7	<2	3	100	2	<2
R0785483	A10032704A	2	130	1209	<0.4	<2	17	14	<1	3	0.41	<2	<4	<5	<5	17	<2	3	112	<2	<2
R0785484	A10032705A	3	75	401	<0.4	<2	38	4	1	4	0.38	<2	<4	<5	<5	17	<2	4	124	<2	<2
R0785485	A10032706A	3	15	4434	<0.4	<2	20	49	1	2	0.48	<2	<4	<5	<5	8	<2	5	86	3	<2
R0785486	A10032707A	3	273	1782	<0.4	25	145	11	1	19	3.52	4	4	<5	<5	95	2	2	113	3	<2
R0785487	A10032708A	1	127	311	<0.4	7	22	2	<1	4	0.80	<2	<4	<5	<5	29	<2	2	134	<2	<2
R0785488	A10032709A	2	85	709	<0.4	3	30	10	<1	6	0.45	<2	<4	<5	<5	17	<2	5	103	3	<2
R0785489	A10032710A	1	59	984	<0.4	4	34	5	<1	3	0.89	<2	<4	<5	<5	20	<2	3	183	<2	<2
R0785490	A10032711A	2	26	492	<0.4	<2	10	4	<1	2	0.38	<2	<4	<5	<5	14	<2	3	92	<2	<2
R0785491	A10032712A	3	7	129	<0.4	<2	7	<1	<1	<1	0.34	<2	<4	<5	<5	7	<2	4	110	<2	<2
R0785492	A10032713A	18	10	36	<0.4	12	46	<1	14	27	2.37	<2	7	<5	<5	3	<2	<2	135	13	<2
R0785493	A10032714A	2	134	392	<0.4	6	48	3	<1	4	0.91	<2	<4	<5	<5	49	<2	2	139	2	<2

REMAC ZINC CORP.-X07

Ref/I.D.: A10032561-10032714
Report Date: 15 JAN 2008
GDL Job No: V07-1405R

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm
STD: DA		134	221	650	4.9	54	482	3	13	40	3.34	2	41	<5	<5	68	2	<2	39	9	18
STD: DA		130	208	626	6.8	53	466	3	13	40	3.25	2	41	<5	<5	67	3	<2	39	8	17
STD: DA		135	208	639	5.8	54	307	3	13	39	3.57	2	41	<5	<5	63	3	<2	36	8	14
STD: DA		112	202	590	5.8	50	420	4	13	39	2.86	2	39	<5	<5	60	4	<2	35	8	17
STD: MS2																					

I=insufficient sample N/A=not available
If requested analyses are not shown, results are to follow

ANALYTICAL METHODS

ICP-OES PACKAGE : 0.5 gram sample digested in hot reverse aqua regia (soil,silt) or hot Aqua Regia(rocks).

ASSIGNED FOR ASSAYING

COMMENTS:

Ge analysis is not able to be provided.

REMAC ZINC CORP.-X07

Ref/I.D.: A10032561-1003
Report Date: 15 JAN 2008
GDL Job No: V07-1405R

LAB NO	FIELD NUMBER	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0785336	GDL PREP BLANK	557	0.60	0.12	0.99	0.45	0.06	0.49	785	N/A	<10
R0785337	A10032561A	371	1.19	<.01	0.37	8.14	0.03	0.18	372	N/A	<10
R0785338	A10032562A	80	0.07	<.01	0.02	1.62	0.02	<.01	24	N/A	<10
R0785339	A10032563A	397	1.22	<.01	0.32	9.86	0.02	0.19	347	N/A	<10
R0785339 rpt		422	1.23	<.01	0.36	10.15	0.02	0.21	357		11
R0785340	A10032564A	318	12.02	<.01	0.01	20.23	0.01	<.01	16	N/A	124
R0785341	A10032565A	254	9.94	<.01	0.08	22.51	0.01	0.01	51	N/A	15
R0785342	A10032566A	237	8.93	<.01	0.09	23.54	0.01	<.01	96	N/A	139
R0785343	A10032567A	282	11.81	<.01	0.06	21.21	0.01	<.01	25	N/A	28
R0785344	A10032568A	194	5.02	<.01	0.03	30.79	0.01	<.01	33	N/A	18
R0785345	A10032569A	115	1.13	<.01	0.31	5.51	0.01	0.16	5904	N/A	113
R0785346	A10032570A	64	0.36	<.01	0.23	2.90	0.01	0.11	3194	N/A	132
R0785346 rpt		65	0.36	<.01	0.24	2.95	0.01	0.11	3151		91
R0785347	A10032571A	168	0.81	0.05	0.55	2.29	0.03	0.24	2758	N/A	129
R0785348	A10032572A	49	0.34	<.01	0.14	1.70	0.01	0.07	2149	N/A	75
R0785349	A10032573A	71	0.58	<.01	0.19	2.24	0.01	0.10	1587	N/A	169
R0785350	A10032574A	39	0.45	<.01	0.13	1.40	0.01	0.07	1031	N/A	75
R0785351	A10032575A	105	1.08	0.02	0.95	3.74	0.01	0.46	5265	N/A	132
R0785352	A10032576A	1285	1.60	<.01	0.15	28.46	0.01	0.01	356	N/A	<10
R0785353	A10032577A	985	1.10	<.01	2.29	1.80	0.02	0.13	454	N/A	<10
R0785353 rpt		963	1.16	<.01	2.39	1.74	0.02	0.13	467		<10
R0785354	A10032578A	579	1.01	<.01	2.21	0.30	0.02	0.12	379	N/A	<10
R0785355	A10032579A	441	5.88	<.01	0.02	24.95	0.01	<.01	38	N/A	11
R0785356	A10032580A	190	1.24	<.01	0.02	34.22	0.01	<.01	84	N/A	40
R0785357	A10032581A	218	3.22	<.01	0.02	32.00	0.01	<.01	45	N/A	29
R0785358	A10032582A	281	5.54	<.01	0.01	27.04	0.01	<.01	58	N/A	41
R0785359	A10032583A	248	6.28	<.01	0.01	20.81	0.01	<.01	80	N/A	50
R0785360	A10032584A	224	6.62	<.01	0.02	14.63	0.01	<.01	92	N/A	26
R0785361	A10032585A	284	8.38	<.01	0.01	18.71	0.01	<.01	79	N/A	46
R0785362	A10032586A	314	9.42	<.01	0.01	20.92	0.01	<.01	67	N/A	17
R0785363	A10032587A	265	9.89	<.01	0.01	19.93	0.01	<.01	83	N/A	10
R0785364	A10032588A	276	10.81	<.01	0.01	20.88	0.01	<.01	268	N/A	38
R0785365	A10032589A	248	8.55	<.01	0.01	17.06	0.01	<.01	78	N/A	21

REMAC ZINC CORP.-X07

Ref/I.D.: A10032561-1003
Report Date: 15 JAN 2008
GDL Job No: V07-1405R

LAB NO	FIELD NUMBER	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0785366	A10032590A	274	8.35	<.01	0.01	17.75	0.01	<.01	147	N/A	16
R0785367	A10032591A	283	9.91	<.01	0.01	20.77	0.01	<.01	473	N/A	13
R0785368	A10032592A	1106	0.49	0.04	0.90	1.47	0.05	0.11	473	N/A	448
R0785369	A10032593A	374	1.37	0.21	1.99	1.70	0.14	0.66	3482	N/A	<10
R0785370	A10032594A	314	10.43	<.01	0.03	19.45	0.01	<.01	164	N/A	<10
R0785371	A10032595A	261	9.60	<.01	0.02	18.87	0.03	<.01	248	N/A	16
R0785372	A10032596A	285	11.25	<.01	0.01	20.68	0.03	<.01	211	N/A	19
R0785373	A10032597A	339	11.72	<.01	0.01	21.72	0.04	<.01	110	N/A	20
R0785374	A10032598A	350	10.43	<.01	0.03	20.94	0.03	0.01	450	N/A	15
R0785375	10032598 GDL DU	342	10.01	<.01	0.01	21.46	0.03	<.01	442	N/A	20
R0785375 rpt		365	10.22	<.01	0.02	21.29	0.03	<.01	459		19
R0785376	A10032599A	341	10.98	<.01	0.02	22.11	0.03	<.01	126	N/A	14
R0785377	A10032600A	319	9.87	<.01	0.02	21.77	0.03	0.01	55	N/A	24
R0785378	A10032601A	306	9.95	<.01	0.01	21.35	0.02	<.01	37	N/A	<10
R0785379	A10032602A	205	5.92	<.01	0.05	12.97	0.03	0.01	1500	N/A	31
R0785380	A10032603A	316	10.84	<.01	0.03	19.70	0.03	0.01	81	N/A	<10
R0785381	A10032604A	308	10.97	<.01	0.01	20.52	0.03	<.01	46	N/A	<10
R0785382	A10032605A	281	8.40	<.01	0.04	16.42	0.03	0.01	1113	N/A	24
R0785383	A10032606A	274	10.06	<.01	0.02	19.12	0.03	0.01	409	N/A	21
R0785384	A10032607A	320	10.60	<.01	0.02	21.40	0.03	<.01	394	N/A	24
R0785385	A10032608A	491	1.00	0.01	0.61	0.84	0.03	0.05	<10	N/A	611
R0785386	A10032609A	316	9.87	<.01	0.01	18.63	0.04	<.01	111	N/A	12
R0785387	A10032610A	299	9.58	<.01	0.01	19.82	0.03	<.01	231	N/A	<10
R0785388	A10032611A	284	8.58	<.01	0.02	19.13	0.03	<.01	261	N/A	40
R0785388 rpt		309	8.96	<.01	0.02	20.03	0.03	<.01	274		44
R0785389	A10032612A	313	10.60	<.01	0.02	20.36	0.02	0.01	418	N/A	17
R0785390	A10032613A	360	10.90	<.01	0.01	19.63	0.03	<.01	97	N/A	14
R0785391	A10032614A	325	10.34	<.01	0.01	18.65	0.03	<.01	69	N/A	<10
R0785392	A10032615A	310	10.59	<.01	0.01	19.36	0.03	<.01	67	N/A	<10
R0785393	A10032616A	306	10.47	<.01	0.02	18.87	0.03	<.01	104	N/A	<10
R0785394	A10032617A	319	11.78	<.01	0.02	21.15	0.03	<.01	607	N/A	14
R0785394 rpt		326	11.40	<.01	0.02	20.94	0.03	<.01	589		24
R0785395	A10032618A	322	11.67	<.01	0.02	20.84	0.03	<.01	191	N/A	14
R0785396	A10032619A	360	11.10	<.01	0.01	19.98	0.03	<.01	86	N/A	19

REMAC ZINC CORP.-X07

Ref/I.D.: A10032561-1003
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GDL Job No: V07-1405R

LAB NO	FIELD NUMBER	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0785397	A10032620A	348	10.76	<.01	0.01	18.90	0.03	<.01	38	N/A	72
R0785398	A10032621A	377	10.35	<.01	0.01	19.38	0.03	<.01	64	N/A	50
R0785399	A10032622A	393	10.77	<.01	0.02	19.65	0.03	<.01	82	N/A	93
R0785400	A10032623A	367	10.26	<.01	0.02	19.70	0.03	<.01	113	N/A	208
R0785401	A10032624A	326	7.76	<.01	0.01	14.89	0.03	<.01	189	N/A	88
R0785402	A10032625A	405	8.76	<.01	0.03	18.70	0.03	0.01	826	N/A	76
R0785403	A10032626A	405	10.53	<.01	0.01	19.52	0.03	<.01	389	N/A	283
R0785404	A10032627A	392	10.97	<.01	0.01	19.97	0.03	<.01	363	N/A	30
R0785405	A10032628A	453	12.13	<.01	0.01	21.04	0.03	<.01	239	N/A	<10
R0785406	A10032629A	408	11.53	<.01	0.01	20.94	0.04	<.01	44	N/A	11
R0785407	A10032630A	425	12.07	<.01	0.01	21.11	0.04	<.01	38	N/A	<10
R0785408	A10032631A	384	11.72	<.01	0.01	19.87	0.03	<.01	31	N/A	<10
R0785409	A10032632A	343	11.23	<.01	0.01	19.54	0.03	<.01	36	N/A	<10
R0785410	A10032633A	381	10.67	<.01	0.02	20.03	0.03	<.01	130	N/A	13
R0785411	A10032634A	387	1.26	0.24	1.84	1.80	0.17	0.78	2899	N/A	<10
R0785412	A10032635A	439	11.21	<.01	0.02	19.77	0.03	<.01	97	N/A	<10
R0785413	A10032636A	344	10.51	<.01	0.04	20.01	0.04	0.01	132	N/A	15
R0785414	A10032637A	387	10.67	<.01	0.02	19.89	0.04	<.01	59	N/A	152
R0785415	GDL PREP BLANK	525	0.62	0.11	0.89	0.55	0.07	0.43	722	N/A	<10
R0785416	A10032638A	292	1.12	0.19	1.54	1.40	0.13	0.60	2782	N/A	11
R0785416 rpt		305	1.16	0.20	1.66	1.43	0.14	0.67	3068		18
R0785417	A10032639A	484	0.71	0.01	0.48	0.38	0.04	0.01	<10	N/A	490
R0785418	A10032640A	338	11.19	<.01	0.02	18.36	0.05	<.01	19	N/A	<10
R0785419	A10032641A	280	11.60	<.01	0.02	19.15	0.04	<.01	12	N/A	<10
R0785420	A10032642A	357	12.25	<.01	0.02	20.34	0.04	<.01	16	N/A	<10
R0785421	A10032643A	224	11.97	<.01	0.03	20.02	0.04	0.01	20	N/A	<10
R0785422	A10032644A	240	12.06	<.01	0.02	20.07	0.04	0.01	20	N/A	<10
R0785422 rpt		225	11.55	<.01	0.02	21.32	0.04	<.01	27		<10
R0785423	A10032645A	263	11.27	<.01	0.03	19.86	0.04	0.01	25	N/A	<10
R0785424	A10032646A	235	10.89	<.01	0.02	18.79	0.04	0.01	17	N/A	<10
R0785425	A10032647A	283	10.82	<.01	0.02	19.62	0.04	0.01	19	N/A	<10
R0785426	A10032648A	262	11.09	<.01	0.01	19.65	0.03	<.01	37	N/A	<10
R0785427	A10032649A	1184	0.46	0.04	0.93	1.38	0.08	0.11	471	N/A	490
R0785428	A10032650A	317	10.00	<.01	0.04	18.56	0.03	0.01	1524	N/A	24

REMAC ZINC CORP.-X07

Ref/I.D.: A10032561-1003
Report Date: 15 JAN 2008
GDL Job No: V07-1405R

LAB NO	FIELD NUMBER	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0785429	A10032651A	304	8.63	<.01	0.02	20.90	0.03	<.01	71	N/A	47
R0785430	A10032652A	214	11.28	<.01	0.01	19.60	0.03	<.01	22	N/A	<10
R0785431	A10032653A	222	11.69	<.01	0.01	18.93	0.04	<.01	<10	N/A	<10
R0785432	A10032654A	185	11.50	<.01	0.01	18.98	0.03	<.01	17	N/A	<10
R0785433	A10032655A	209	11.64	<.01	0.01	18.60	0.03	<.01	19	N/A	<10
R0785434	A10032656A	193	10.84	<.01	0.01	18.79	0.03	<.01	23	N/A	<10
R0785435	A10032657A	241	12.22	<.01	0.01	20.45	0.04	<.01	28	N/A	18
R0785436	A10032658A	260	10.90	<.01	0.02	20.01	0.03	<.01	37	N/A	126
R0785437	A10032659A	219	11.44	<.01	0.01	20.09	0.03	<.01	24	N/A	24
R0785438	A10032660A	487	0.96	0.01	0.60	0.80	0.04	0.04	<10	N/A	613
R0785439	A10032661A	209	6.55	<.01	0.05	15.07	0.02	<.01	22	N/A	175
R0785440	A10032662A	373	1.18	0.23	1.49	2.07	0.11	0.54	3062	N/A	29
R0785441	A10032663A	216	11.85	<.01	0.02	20.23	0.05	<.01	24	N/A	<10
R0785442	A10032664A	213	10.06	<.01	0.02	19.15	0.03	<.01	48	N/A	143
R0785443	A10032665A	172	10.85	<.01	0.02	19.45	0.03	<.01	46	N/A	16
R0785444	A10032666A	404	1.42	0.23	2.07	2.01	0.18	0.73	3473	N/A	<10
R0785445	A10032667A	194	11.06	<.01	0.04	20.73	0.03	0.02	56	N/A	<10
R0785446	A10032668A	163	10.71	<.01	0.02	20.04	0.03	0.01	29	N/A	<10
R0785447	A10032669A	223	11.39	<.01	0.02	21.97	0.02	<.01	35	N/A	<10
R0785448	A10032670A	237	10.35	<.01	0.03	21.52	0.03	0.01	63	N/A	<10
R0785449	A10032671A	242	10.18	<.01	0.05	18.44	0.03	0.02	131	N/A	106
R0785450	A10032672A	556	0.70	<.01	0.52	0.44	0.03	0.01	<10	N/A	335
R0785451	A10032673A	251	10.86	<.01	0.02	19.75	0.03	0.01	20	N/A	<10
R0785452	A10032674A	260	12.25	<.01	0.04	23.12	0.03	0.02	16	N/A	<10
R0785453	A10032675A	334	11.60	<.01	0.03	22.17	0.03	0.01	10	N/A	<10
R0785454	A10032676A	321	11.68	<.01	0.03	22.28	0.03	0.01	40	N/A	<10
R0785454 rpt		286	10.02	<.01	0.03	19.46	0.03	<.01	33		<10
R0785455	10032676 GDL DU	335	12.07	<.01	0.03	23.45	0.03	<.01	43	N/A	<10
R0785456	A10032677A	213	5.28	<.01	0.07	26.12	0.03	0.03	51	N/A	<10
R0785457	A10032678A	238	9.07	<.01	0.11	18.95	0.03	0.06	95	N/A	<10
R0785458	A10032679A	541	4.42	<.01	0.06	28.88	0.03	0.03	50	N/A	106
R0785459	A10032680A	336	9.30	<.01	0.04	22.75	0.03	0.02	38	N/A	17
R0785460	A10032681A	694	5.09	<.01	0.04	31.35	0.03	0.02	49	N/A	287
R0785461	A10032682A	364	1.13	0.20	1.68	1.75	0.11	0.58	2882	N/A	15

REMAC ZINC CORP.-X07

Ref/I.D.: A10032561-1003
Report Date: 15 JAN 2008
GDL Job No: V07-1405R

LAB NO	FIELD NUMBER	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
R0785462	A10032683A	242	10.47	<.01	0.03	20.25	0.03	0.01	28	N/A	<10
R0785463	A10032684A	266	12.90	<.01	0.02	22.69	0.03	0.01	21	N/A	<10
R0785464	A10032685A	244	11.39	<.01	0.03	21.27	0.03	0.01	29	N/A	43
R0785465	A10032686A	208	11.89	<.01	0.02	21.97	0.03	0.01	19	N/A	<10
R0785466	A10032687A	199	11.19	<.01	0.03	20.52	0.03	0.01	20	N/A	<10
R0785467	A10032688A	200	11.07	<.01	0.03	20.39	0.03	0.01	26	N/A	<10
R0785467 rpt		186	10.42	<.01	0.02	19.04	0.03	0.01	26		<10
R0785468	A10032689A	201	10.67	<.01	0.03	19.43	0.03	0.01	26	N/A	<10
R0785469	A10032690A	204	10.89	<.01	0.03	19.95	0.03	0.01	33	N/A	<10
R0785470	A10032691A	218	11.46	<.01	0.04	20.95	0.03	0.01	25	N/A	<10
R0785471	A10032692A	190	10.44	<.01	0.03	19.89	0.03	0.01	27	N/A	<10
R0785472	A10032693A	213	10.96	<.01	0.02	21.00	0.03	0.01	22	N/A	<10
R0785473	A10032694A	230	9.87	<.01	0.04	20.85	0.02	0.02	22	N/A	<10
R0785473 rpt		226	10.31	<.01	0.03	21.56	0.03	0.01	21		<10
R0785474	A10032695A	259	10.77	<.01	0.04	20.81	0.03	0.02	33	N/A	<10
R0785475	A10032696A	281	10.48	<.01	0.05	21.19	0.03	0.02	54	N/A	<10
R0785476	A10032697A	626	5.40	<.01	0.09	22.05	0.03	0.05	226	N/A	<10
R0785477	A10032698A	1287	0.48	0.05	1.02	1.60	0.07	0.11	516	N/A	319
R0785478	A10032699A	548	1.18	<.01	0.23	29.62	0.03	0.12	560	N/A	<10
R0785479	A10032700A	256	0.36	0.06	0.62	2.15	0.03	0.40	913	N/A	<10
R0785480	A10032701A	1184	0.68	0.22	1.65	1.76	0.03	1.04	1887	N/A	<10
R0785481	A10032702A	482	10.68	<.01	0.02	20.23	0.03	<.01	151	N/A	<10
R0785482	A10032703A	284	10.59	<.01	0.03	20.47	0.03	0.01	39	N/A	<10
R0785483	A10032704A	216	11.36	<.01	0.01	21.25	0.03	<.01	13	N/A	18
R0785484	A10032705A	192	10.39	<.01	0.05	19.92	0.03	0.02	77	N/A	<10
R0785485	A10032706A	309	9.46	<.01	0.07	20.52	0.03	0.04	43	N/A	10
R0785486	A10032707A	348	6.78	<.01	0.03	23.19	0.03	<.01	516	N/A	19
R0785487	A10032708A	408	11.67	<.01	0.01	23.45	0.03	<.01	86	N/A	<10
R0785488	A10032709A	328	11.26	<.01	0.03	21.75	0.03	<.01	39	N/A	<10
R0785489	A10032710A	561	11.60	<.01	0.02	21.87	0.04	<.01	469	N/A	<10
R0785490	A10032711A	237	11.73	<.01	0.01	21.40	0.03	<.01	24	N/A	<10
R0785491	A10032712A	210	11.06	<.01	0.01	20.86	0.03	<.01	21	N/A	<10
R0785492	A10032713A	848	1.49	0.01	0.35	15.03	0.03	0.20	435	N/A	<10
R0785493	A10032714A	302	10.55	<.01	0.01	19.37	0.03	<.01	229	N/A	<10

REMAC ZINC CORP.-X07

Ref/I.D.: A10032561-1003
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GDL Job No: V07-1405R

LAB NO	FIELD NUMBER	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	P ppm	Ge ppm	Hg ppb
STD: DA		632	0.60	0.09	1.91	0.55	0.03	0.12	1017		
STD: DA		636	0.57	0.09	1.87	0.54	0.06	0.12	1009		
STD: DA		645	0.59	0.09	2.01	0.52	0.07	0.12	1053		
STD: DA		673	0.52	0.08	1.79	0.55	0.05	0.10	973		
STD: MS2											83

I=insufficient sample N/A=not

If requested analyses are not sl

ANALYTICAL METHODS

ICP-OES PACKAGE : 0.5 gran

ASSIGNED FOR ASSAYING

COMMENTS:

Ge analysis is not able to be p

APPENDIX

IX. METALLURGICAL REPORT

An Investigation into

THE RECOVERY OF ZINC FROM A ZINC OXIDE SAMPLE

prepared for

REMAC ZINC DEVELOPMENT CORP.

Project 11419-003 – Final Report
April 18, 2008

NOTE:
This report refers to the samples as received.

The practice of this Company in issuing reports of this nature is to require the recipient not to publish the report or any part thereof without the written consent of SGS Minerals Services.

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Details of Tests 12

Executive Summary

The objective of this study was to further examine the metallurgical response of the Remac zinc oxide ore to a combined heavy liquid separation/flotation flowsheet. For the study, Redhawk Resources Inc. provided samples of Remac zinc oxide ore, which had been on-site since 2001 (under project number 10182-001).

Heavy liquid separation (HLS) testwork was performed on the ore, prior to grinding and desliming to a K_{80} of 70 µm. The deslimed feed underwent flotation. It was demonstrated through repeat testwork that a zinc concentrate grading 38.4% Zn could be achieved, at a recovery of 82.2% Zn of the deslimed flotation feed in a locked cycle test.

The previous phase of the program recovered 83.6% of the Zn in the deslimed flotation feed in batch flotation testwork, generating a zinc concentrate grading 42.3% Zn. The current composite, despite a higher proportion of Ca gangue, produced comparable results to previous testwork.

Introduction

A previous testing program, undertaken on Remac zinc oxide ore, had outlined a promising process route that incorporated both heavy liquid separation and flotation of a deslimed feed. The purpose of the current test program was to further examine the metallurgical response of the Zn oxide composite, specifically exploring the effect of grind size and reagent dosage. This report presents the metallurgical testwork results of the program.

All test results and conditions are presented in the accompanying appendix. The results refer to samples as received. Results were sent to Byard Maclean of Samadish Engineering Ltd. as they were available throughout the program.

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Testwork Summary

1. Sample Receipt and Description

In July of 2007, 5 drums of partially crushed ore samples were removed from storage at the SGS Lakefield site, having been there since 2001. A previous test program had also used some of these samples for testwork, under the project number 11419-001. The samples were in various stages of wetness and sizes, and were set aside to dry before sample preparation. Samples were chosen to be combined into an overall composite, and this material was crushed to minus $^{3}/_{8}$ inch. Table 1 displays the blend of samples making up the Remac zinc oxide ore composite for this test program.

Table 1: Samples Included in Second Composite

Sample #	Weight (kg) currently in drum	Sample weight to be used in composite (kg)	Sample #	Weight (kg) currently in drum	Sample weight to be used in composite (kg)
117104	4.06	4	183291	0.82	0.82
117113	5.8	2	183292	1.90	1.90
117114	26.2	2	183293	0.66	0.66
117115	18.56	2	183647	1.32	1.32
117116	25.82	2	183648	0.98	0.98
117117	20.38	2	183649	0.52	0.52
117195	3.24	2	183650	1.60	1.60
182829	5.24	2	183652	0.62	0.62
182856	8.98	2	183653	0.68	0.68
182859	5.08	2	183654	0.86	0.86
182884	0.96	1	183655	0.44	0.44
182981	4.08	2	183656	0.10	0.10
183015	4.36	2	183819	2.52	2.52
183062	4.26	2	183836	0.48	0.48
183063	3.38	2	183837	0.82	0.82
183072	7.84	2	183838	1.38	1.38
183074	4.94	2	183839	1.66	1.66
183075	4.86	2	183840	1.58	1.58
183154	6.54	2	183841	0.96	0.96
183232	3.10	3.10	183842	1.08	1.08
183233	1.52	1.52	183843	0.36	0.36
183234	3.12	3.12	183850	1.36	1.36
183235	0.48	0.48	183852	1.54	1.54
183245	0.82	0.82	183853	0.86	0.86
183246	2.40	2.40	183909	0.52	0.52
183248	0.62	0.62	183910	2.52	2.52
183249	0.30	0.30	183911	0.62	0.62
183250	0.28	0.28	183912	1.98	1.98
183252	1.26	1.26	183913	0.76	0.76
183253	2.48	2.48	183914	0.44	0.44
183278	2.98	2.98	183920	0.24	0.24
183280	0.68	0.68	183921	0.62	0.62
183281	1.16	1.16	183925	0.72	0.72
183282	2.36	2.36	183927	0.60	0.60
183290	1.44	1.44			

The testwork on this phase of the program was conducted as an extension of the testwork performed in 11419-001.

The composite generated was blended before being sub-sampled for assay. Much of the material was already finer than $^{3}/_{8}$ inch, and did not require crushing – this material was screened out prior to crushing. The sub-sample (5 kg) was crushed to -10 mesh, and a 150 g sample removed for chemical characterisation. Table 2 displays the complete head assays for the -003 composite, and Table 3 compares the main assays of the -001 and -003 composites.

Table 2: Remac Composite Head Assays

	-10M Heads		-10M Heads		-10M Heads
Zn %	7.04	Cu g/t	51.0	SiO_2 %	10.8
Ca %	17.5	Li g/t	< 5	Al_2O_3 %	1.93
Fe %	11.2	Mo g/t	< 10	Fe_2O_3 %	15.6
CO_3 %	32.4	Ni g/t	100	MgO %	7.33
Ag g/t	12.0	Pb g/t	1.48	CaO %	22.3
As g/t	50.0	Sb g/t	< 20	Na_2O %	2.15
Ba g/t	390	Se g/t	< 30	K_2O %	0.28
Be g/t	0.87	Sn g/t	< 20	TiO_2 %	0.13
Bi g/t	< 20	Sr g/t	63.0	P_2O_5 %	0.64
Cd g/t	570	Tl g/t	< 30	MnO %	0.09
Co g/t	15.0	U g/t	< 30	Cr_2O_3 %	< 0.01
Cr g/t	26.0	Y g/t	6.90	V_2O_5 %	0.02

Table 3: Comparison with -001 Phase Head Assays

Sample ID	Zn %	CaO %	Fe %	CO_3 %
003 -10M Heads	7.04	22.3	11.2	32.4
001 -10M Heads	7.13	28.1	7.02	42.7

While the Zn head grade was similar to the previous composite, the Ca and Fe assays indicated there were some differences between the first and second composites. It was not readily apparent at first how significant these differences would be to the metallurgy.

The -$^{3}/_{8}$ inch composite material was screened at 20 mesh, and the minus fraction was sub-sampled for assay. The +20 mesh fraction advanced to heavy liquid separation (HLS).

As in the previous test program, the feed samples were fairly fine (RC drilling chips), resulting in a substantial amount of the weight (73.8%) being finer than 20 mesh. This material was not subjected to HLS, resulting in a decreased impact of HLS on calcium rejection prior to flotation.

2. Heavy Liquid Separation, Stage Grinding and Desliming

2.1. Heavy Liquid Separation

Heavy liquid separation was performed on the +20 mesh fraction of the composite, at a density of 2.8 g/cc. This density was chosen based on testwork conducted on the -001 composite, as that had been the optimum density of separation.

The sink and float fractions were sub-sampled for assay. The results are displayed in Table 4, including the results of the bulk HLS performed in the first phase of the program.

Table 4: HLS Balance

+20 M Only	**Wt**		**Assays (%)**			**Distribution (%)**		
Product	**kg**	**%**	**Zn**	**Ca**	**Fe**	**Zn**	**Ca**	**Fe**
2.8 Sink	14.7	66.2	17.2	9.69	17.4	93.8	37.6	95.4
2.8 Float	7.52	33.8	2.21	31.5	1.64	6.2	62.4	4.6
Head (calc)	22.2	100	12.1	17.1	12.1	100.0	100.0	100.0
Full balance:								
Product	**Wt**		**Assays (%)**			**Distribution (%)**		
	kg	**%**	**Zn**	**Ca**	**Fe**	**Zn**	**Ca**	**Fe**
2.8 Sink	14.7	17.3	17.2	9.69	17.4	36.1	10.6	24.3
2.8 Float	7.52	8.85	2.21	31.5	1.64	2.4	17.5	1.2
-20M	62.7	73.8	6.87	15.5	12.5	61.5	71.9	74.5
Head (calc)	84.9	100	8.25	15.9	12.4	100.0	100.0	100.0
Head (dir)			7.04	17.5	11.2			
Combined		**Wt**	**Assays (%)**			**Distribution (%)**		
Products		**%**	**Zn**	**Ca**	**Fe**	**Zn**	**Ca**	**Fe**
2.8 Sink		17.3	17.2	9.69	17.4	36.1	10.6	24.3
2.8 + -20M		91.1	8.83	14.4	13.4	97.6	82.5	98.8
Combined		***Wt***	***Assays (%)***			***Distribution (%)***		
Products (11419-001)		***%***	***Zn***	***Ca***	***Fe***	***Zn***	***Ca***	***Fe***
2.8 Sink		*9.29*	*21.2*	*5.26*	*23.9*	*29.4*	*2.27*	*34.2*
2.8 + -20M		*80.6*	*8.00*	*19.3*	*7.74*	*96.3*	*72.2*	*96.0*

Heavy liquid separation on the +20 mesh material at 2.8 g/cc (not considering the -20 mesh fraction) eliminated 33.8% of the weight, rejecting 62.4% of the Ca in that mass at only 6.2% Zn losses. The sink fraction was crushed to -10 mesh and recombined with the -20 mesh material, and this blend was split into 10 kg charges.

In comparison to the HLS performed in the first phase of the program, the current testwork recovered 10.5% more mass at 91.1%, causing an increase of 1.3% in Zn recovery. Ca and Fe recoveries increased by 10.3% and 2.8%, respectively.

2.2. Stage Grinding and Desliming

The 10 kg blended charges were subjected to stage grinding to several different sizes. The slurry was then deslimed using a hydrocyclone, with the undersize becoming the flotation feed and the oversize being stored.

Several target grind sizes were tested during this phase of the program, in an effort to optimize the metallurgy and flotation results. A second stage grind to 150 mesh was conducted in February of 2008, in order to produce charges for further flotation testwork. The mass balances for each of the stage grinds are presented in Table 5.

Table 5: Summary of Stage Grinding/Desliming Results

Product	Wt		Assays (%)			Distribution (%)		
	g	%	Zn	Fe	Ca	Zn	Fe	Ca
100M UF	7626	88.9	7.6	11.9	16.8	88.4	82.9	93.2
100M OF	948	11.1	8.06	19.8	9.87	11.6	17.1	6.8
Head (calc)	8574	100.0	7.65	12.8	16.0	100.0	100.0	100.0
Head (dir)			7.72	12.7	19.3			
Product	**Wt**		**Assays (%)**			**Distribution (%)**		
	g	**%**	**Zn**	**Fe**	**Ca**	**Zn**	**Fe**	**Ca**
200M UF	6662	84.2	7.82	12.3	16.1	83.2	76.8	89.1
200M OF	1255	15.8	8.39	19.7	10.5	16.8	23.2	10.9
Head (calc)	7917	100.0	7.91	13.5	15.2	100.0	100.0	100.0
Head (dir)			7.72	12.7	19.3			
Product	**Wt**		**Assays (%)**			**Distribution (%)**		
	g	**%**	**Zn**	**Fe**	**Ca**	**Zn**	**Fe**	**Ca**
150M UF	15515	82.5	7.89	11.3	17	82.2	74.4	88.5
150M OF	3292	17.5	8.07	18.3	10.4	17.8	25.6	11.5
Head (calc)	18807	100.0	7.92	12.5	15.8	100.0	100.0	100.0
Head (dir)			7.72	12.7	19.3			

Mass and Zn recovery were nearly proportional in all of the stage grinds. Fe and Ca recovery also tracked mass recovery, but at slightly lower (Fe) and higher (Ca) recoveries comparatively.

The underflow from each desliming stage was dried, blended, and sub-sampled for assay. The remaining material was rotary split into 1 kg charges and became the flotation feed.

3. Flotation Testwork

Flotation testwork examined the effects of several variables. The first two tests looked at whether improvements could be made on previous testwork results, using a different target grind size. In LR project number 11419-001, the target grind of 150 mesh was used, while the current tests F1 and F2 used grinds of 100 mesh and 200 mesh respectively. Tests F1 and F2 were conducted as cleaner tests.

Tests F3 and F4 were conducted using charges from the previous program, that had been ground to 150 mesh and deslimed. These charges were used as the new composite was not ready at time of testwork. These tests, and Tests F5-F8, explored the effect of changes to the depressant dosage, and were conducted as rougher kinetics tests only.

Tests F9-F11 explored the effects of sulphidizer and collector dosage. Test F11 reverted to the conditions of F6 for depressants, and also was conducted through cleaning stages.

Table 6 presents the summary of the flotation test conditions. Full test details are available in the Appendix. Table 7 displays the results of the cleaner tests focussing on the effects of grind, including the values of the best test of the previous program (FF1-7).

Table 6: Summary of Flotation Test Conditions

Test #	UF Feed	Rougher Reagents (g/t)					Cleaner Reagents (g/t)			
	Size (mesh)	Na_2CO_3	Silicate N	P-40	Na_2S	Armac C	Silicate N	P-40	Na_2S	Armac C
F1	100	300	750	750	3000	150	250	750	450	50
F2	200	300	750	750	3000	150	250	750	450	50
F3	150 (-001)	300	500	500	3000	150				
F4	150 (-001)	300	500+500	500+500	3300	150				
F5	150 (-003)	300	500	1000	3000	150				
F6	150 (-003)	300	250	1000	3000	150				
F7	150 (-003)	300	0	1000	3000	150				
F8	150 (-003)	300	1000	500	3000	150				
F9	150 (-003)	300	750	750	3000	150				
F10	150 (-003)	300	750	750	4300	215				
F11	150 (-003)	300	250	1000	5000	300	100	400	550	60

The two tests conducted at different target grinds did not yield as promising results as had Test FF1-7. While the final recovery to the third cleaner concentrate was higher in Test F1, the earlier testwork had indicated that two stage of cleaning only were necessary to reach grades of 40% and higher. Thus, the second cleaner concentrate was the product being compared across the three tests, and a target grind of 150 mesh was set for the remainder of the program.

Table 7: Summary of Effect of Grind Cleaner Tests (F1-F2)

Test #	Product	Weight	Assays, %, g/t			% Distribution		
		%	Zn	Fe	Ca	Zn	Fe	Ca
FF1-7	*ZnO 3rd Clnr Con*	*7.89*	*49.5*	*0.90*	*2.18*	*46.1*	*1.0*	*0.8*
	ZnO 2nd Clnr Con	*16.7*	*42.3*	*1.25*	*5.54*	*83.6*	*3.0*	*4.6*
	Rougher Tail	*71.5*	*1.10*	*8.90*	*22.9*	*9.28*	*90.5*	*80.8*
	Head (calc.)	*100.0*	*8.47*	*7.03*	*20.3*			
F1	ZnO 3rd Clnr Con	11.2	42.8	1.55	2.23	65.5	1.5	1.5
(100M)	ZnO 2nd Clnr Con	13.0	40.9	2.10	2.84	72.8	2.3	2.3
	Rougher Tail	78.0	1.89	12.8	18.6	20.2	84.7	89.9
	Head (calc.)	*100.0*	*7.30*	*11.8*	*16.1*			
F2	ZnO 3rd Clnr Con	8.01	40.7	1.78	3.34	43.1	1.2	1.7
(200M)	ZnO 2nd Clnr Con	8.99	38.5	2.29	4.09	45.8	1.8	2.3
	Rougher Tail	85.5	4.49	12.5	17.1	50.7	91.0	91.9
	Head (calc.)	*100.0*	*7.56*	*11.7*	*15.9*			

Tests F3 through F10 examined changes in depressant dosage. Test F4 also used an increased amount of sulphidizer (an increase of 300 g/t). Test F10 was conducted as a repeat of Test F6, with increased amounts of both sulphidizer and collector.

Table 8 displays the results of these tests, with full test details available in the Appendix.

It was noted that tests F3 and F4 showed a significantly higher Zn recovery than all other rougher kinetics tests. The recoveries of Fe and Ca were also significantly increased alongside the Zn. During the course of testwork, depressant dosages were adjusted in order to help increase Zn recovery while still suppressing gangue; this was not successful in that the Zn recoveries in FF1-7, F3, and F4 were not matched.

The tests using higher or similar dosages of Silicate N depressant (F8, F9) had decreased Zn recovery, compared to the recoveries of FF1-7, F3, and F4. Tests with decreased dosages of Silicate N had improved recovery (83.6-84.6% Zn). However, cutting out the reagent entirely in Test F7 showed a decrease in Zn recovery (81.5%) and generated products which were observed to filter very slowly.

Table 8: Summary of Depressant Rougher Kinetics Tests (F3-F10)

Test #	Product	Weight	Assays, %, g/t			% Distribution		
		%	Zn	Fe	Ca	Zn	Fe	Ca
FF1-7	*Ro Conc*	*28.5*	*27.0*	*2.34*	*13.7*	*90.7*	*9.49*	*19.2*
(750/750)	*Rougher Tail*	*71.5*	*1.10*	*8.90*	*22.9*	*9.3*	*90.5*	*80.8*
	Head (calc.)	*100.0*	*8.47*	*7.03*	*20.3*			
F3	Ro Conc	28.5	27.2	4.19	10.2	93.4	16.8	15.8
(500/500)	Rougher Tail	71.5	0.77	8.30	21.6	6.6	83.2	84.2
	Head (calc.)	*100.0*	*8.32*	*7.13*	*18.3*			
F4	Ro Conc	26.2	29.2	3.68	9.23	93.2	13.9	12.7
(1000/1000)	Rougher Tail	73.8	0.76	8.09	22.5	6.8	86.1	87.3
	Head (calc.)	*100.0*	*8.20*	*6.94*	*19.0*			
F5	Ro Conc	23.1	28.9	7.42	6.72	83.6	14.8	9.9
(500/1000)	Rougher Tail	76.9	1.70	12.8	18.4	16.4	85.2	90.1
	Head (calc.)	*100.0*	*7.98*	*11.6*	*15.7*			
F6	Ro Conc	22.8	29.7	6.90	6.57	84.6	14.0	9.1
(250/1000)	Rougher Tail	77.2	1.59	12.5	19.5	15.4	86.0	90.9
	Head (calc.)	*100.0*	*7.99*	*11.2*	*16.6*			
F7	Ro Conc	20.4	31.6	6.20	7.00	81.5	11.1	8.7
(0/1000)	Rougher Tail	79.6	1.83	12.7	18.8	18.5	88.9	91.3
	Head (calc.)	*100.0*	*7.89*	*11.4*	*16.4*			
F8	Ro Conc	23.8	26.1	11.6	6.63	79.1	25.0	9.4
(1000/500)	Rougher Tail	76.2	2.15	10.8	19.9	20.9	75.0	90.6
	Head (calc.)	*100.0*	*7.85*	*11.0*	*16.7*			
F9	Ro Conc 1-3	15.5	27.1	8.52	6.11	54.4	11.8	5.7
(750/750)	Rougher Tail	84.5	4.18	11.7	18.7	45.6	88.2	94.3
	Head (calc.)	*100.0*	*7.74*	*11.2*	*16.7*			
F10	Ro Conc 1-3	21.6	31.1	7.66	5.61	83.7	14.2	8.4
(+Na2S,	Rougher Tail	78.4	1.67	12.8	17.0	16.3	85.8	91.6
Armac C)	*Head (calc.)*	*100.0*	*8.03*	*11.7*	*14.5*			

Test F10 returned to the conditions of F6, seen as the best of the rougher kinetics tests thus far. Increases were made to both sulphidizer and collector dosage, in an attempt to activate and float more Zn. This produced a Zn recovery similar to that in Tests F5 and F6, at a slightly lower mass and with slightly less Ca recovery. However, the Zn recovery of tests FF1-7, F3, and F4 was not matched.

Figure 1 shows the Zn recovery curves for the rougher tests.

Tests F5 through F10 (the new composite charges) show greater weight rejection in the rougher circuit than did charges from tests F3, F4 and FF1-7 from the previous program. They also show a decrease in Ca recovery to the rougher concentrate, as can be seen in Figure 2.

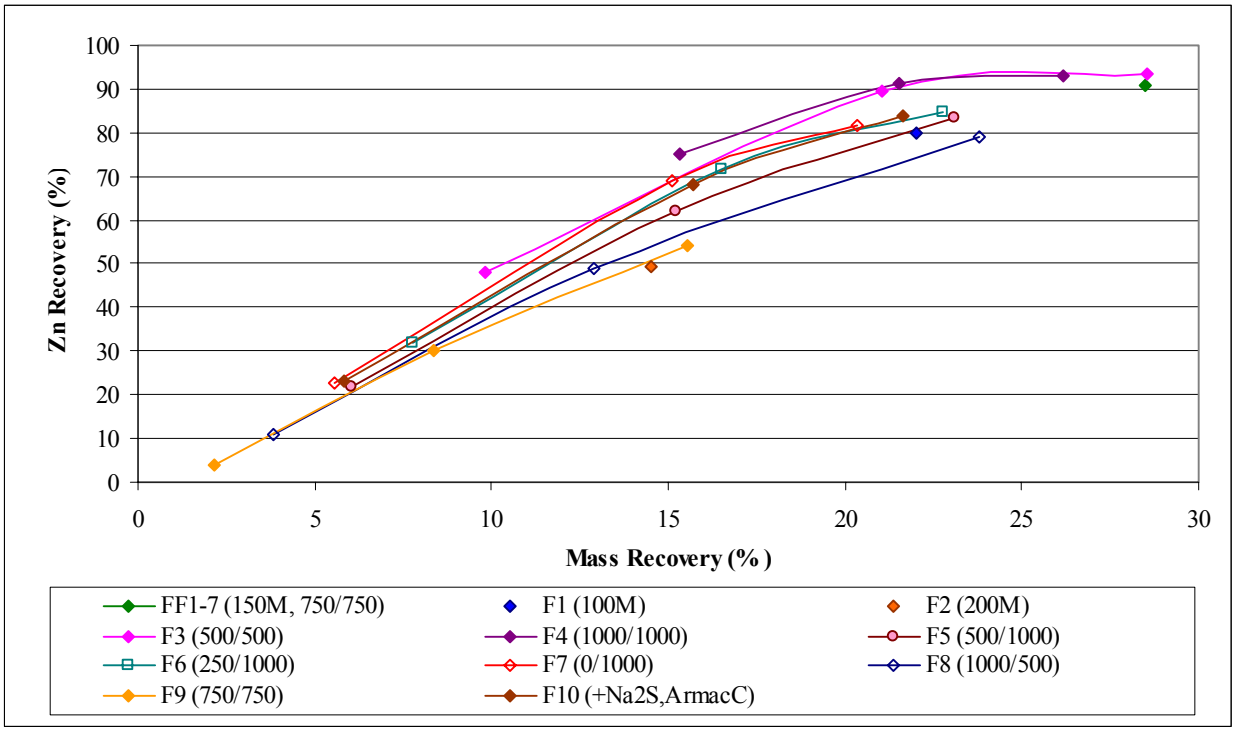


Figure 1: Zn Recovery Curves in Rougher Kinetics Tests (F3-F10)

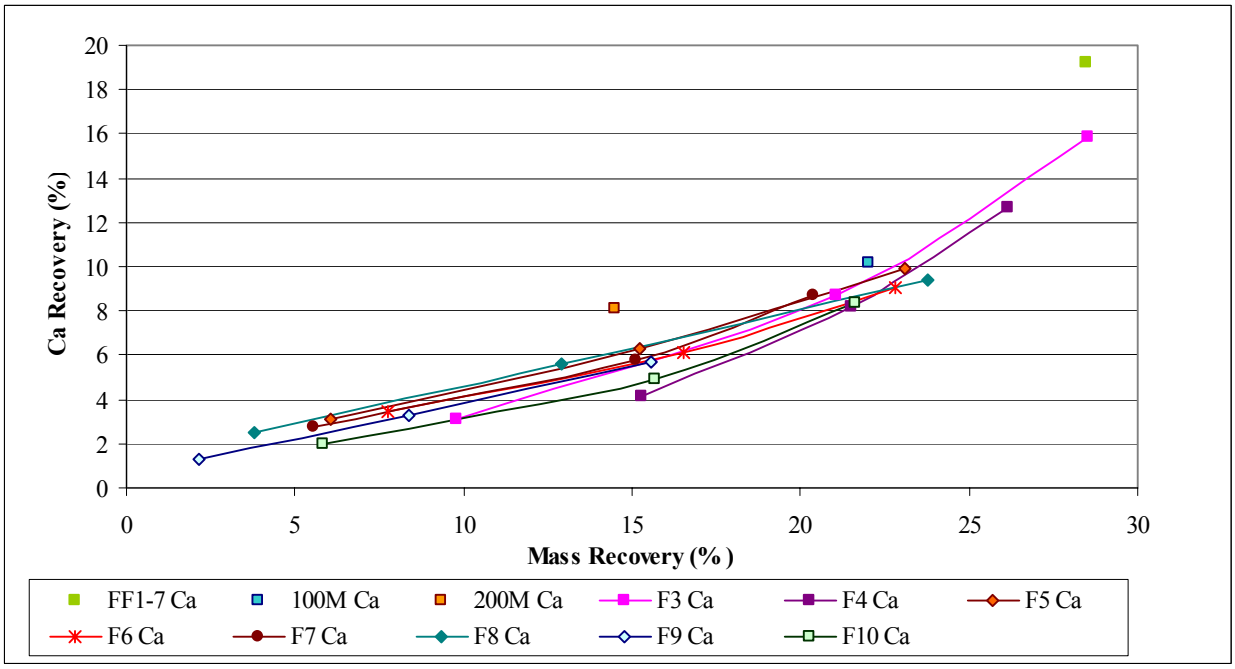


Figure 2: Ca Recovery Curves in Rougher Kinetics Tests (F3-F10)

Returning to a comparison of the feeds, the difference in head grades from a metallurgical perspective began to become apparent. HLS had recovered 10.5% more mass and 10.3% more Ca in this phase of the program, using the same specific gravity of separation. Stage grinding and desliming had produced similar weight recoveries. A significantly higher fraction of Ca gangue was likely recovered to the flotation feed, negatively impacting flotation by inhibiting Zn recovery. Table 3 shows the difference in Ca, Fe, and CO_3 assays. Unfortunately, no mineralogy was available to confirm the mineralogical difference between the two feed samples.

Table 3: Comparison with -001 Phase Head Assays

Sample ID	Zn %	CaO %	Fe %	CO_3 %
003 -10M Heads	7.04	22.3	11.2	32.4
001 -10M Heads	7.13	28.1	7.02	42.7

Another cleaner test was performed, to see how the higher gangue content would affect cleaning to a final Zn concentrate. Increases were made to both sulphidizer and collector, in an attempt to boost Zn recovery. Table 9 shows the results of this test, compared to FF1-7 and Tests F1-2. Full test details are available in the Appendix.

Table 9: Summary of Cleaner Test Results (F1-F2, F11, LCT)

Test #	Product	Weight	Assays, %, g/t			% Distribution		
		%	Zn	Fe	Ca	Zn	Fe	Ca
FF1-7	*ZnO 3rd Clnr Con*	*7.89*	*49.5*	*0.90*	*2.18*	*46.1*	*1.0*	*0.8*
	ZnO 2nd Clnr Con	*16.7*	*42.3*	*1.25*	*5.54*	*83.6*	*3.0*	*4.6*
	Rougher Tail	*71.5*	*1.10*	*8.90*	*22.9*	*9.28*	*90.5*	*80.8*
	Head (calc.)	*100.0*	*8.47*	*7.03*	*20.3*			
F1	ZnO 3rd Clnr Con	11.2	42.8	1.55	2.23	65.5	1.5	1.5
	ZnO 2nd Clnr Con	13.0	40.9	2.10	2.84	72.8	2.3	2.3
	Rougher Tail	78.0	1.89	12.8	18.6	20.2	84.7	89.9
	Head (calc.)	*100.0*	*7.30*	*11.8*	*16.1*			
F2	ZnO 3rd Clnr Con	8.01	40.7	1.78	3.34	43.1	1.2	1.7
	ZnO 2nd Clnr Con	8.99	38.5	2.29	4.09	45.8	1.8	2.3
	Rougher Tail	85.5	4.49	12.5	17.1	50.7	91.0	91.9
	Head (calc.)	*100.0*	*7.56*	*11.7*	*15.9*			
F11	ZnO 2nd Clnr Con	17.9	37.5	5.20	2.92	82.5	8.3	3.3
	Ro Conc	24.4	28.7	7.47	6.45	86.1	16.2	10.0
	Rougher Tail	75.6	1.50	12.5	18.8	13.9	83.8	90.0
	Head (calc.)	*100.0*	*8.14*	*11.3*	*15.8*			

Test F11, despite the lower recovery to the rougher concentrate, produced a 2nd cleaner concentrate with a recovery almost equal to that achieved in the first phase of testwork, in FF1-7. The gangue recovery (both Fe- and Ca-gangue) was higher in F11 by a substantial amount.

However, the final Zn grade was 37.5% Zn, which, while shy of the 40% Zn target grade, would be able to be upgraded using a third cleaning stage and/or calcining.

A locked cycle test was conducted, in order to examine the effects of recycle water on flotation performance. Table 10 shows the metallurgical projection from the LCT results. Full test details are available in the Appendix.

Table 10: Metallurgical Projections on Cycles C-F from Remac LCT

Product	Weight	Assays, %			% Distribution		
	%	Zn	Fe	Ca	Zn	Fe	Ca
2nd Cl Concentrate	17.3	38.4	3.93	3.61	82.2	6.08	4.28
1st Cl Scav Tail	10.3	3.14	13.7	18.0	4.01	12.6	12.8
Ro Tail	72.0	1.54	12.6	16.8	13.7	81.3	83.0
Head	100.0	8.08	11.2	14.6	100.0	100.0	100.0

The Zn grade of the 2nd cleaner concentrate projected to be 38.4% Zn, which is still below the target grade but is reasonably close. Final Zn recovery to the Zn concentrate fell slightly, to 82.2% of the flotation feed (compared to 82.5% in the best cleaner test, and 83.6% in FF1-7).

When considering the entire cycle of production, from HLS through stage grinding, desliming, and flotation, the final recovery from the Remac composite was 66.0% Zn. This compares to an overall recovery of 66.9% from the previous program, under LR project number 11419-001.

4. Conclusions and Recommendations

Heavy liquid separation, grinding, desliming and flotation tests were performed on the Remac zinc oxide ore, testing the use of a mixed HLS/flotation flowsheet for processing. This composite was generated from RC drilling reject material, producing a fairly fine composite even before grinding was conducted.

The test results showed heavy liquid separation, done on +20M material at 2.8 g/cc, rejected 8.9% of the weight while recovering 97.6% of the Zn. Mass recovery to this stage was 10.5% higher than in the previous program, and a higher proportion of gangue was recovered to the combined 2.8 sinks and -20 mesh material. Calcium-based gangue in particular showed increased recovery (10.3% more than in previous HLS testwork). HLS sinks and the -20 mesh material were recombined for stage grinding and desliming.

Stage grinding and desliming showed that a target grind of 150 mesh would produce the most beneficial flotation results.

Flotation tests on ground and deslimed material were conducted. Locked cycle testwork showed that a concentrate grading 38.4% Zn at a recovery of 82.2% Zn (of the deslimed flotation feed) could be achieved. This compared reasonably well with previous testwork, though both recoveries and grades were slightly below that achieved with previous testwork. There was a notable difference in Zn recovery in rougher flotation with this material, indicating an appreciable effect of feed variability.

Further testwork should examine:

1) The effect of feed variability on responses to HLS and flotation, to evaluate the overall zinc recovery that can be expected from the different ore zones in the deposit;
2) The effect of a coarser feed sample, to fully evaluate the impact of Ca rejection via HLS on the subsequent flotation results and the overall project economics;
3) The feasibility of blending flotation slimes (hydrocyclone overflow) with the final Zn concentrate, or the feasibility of flotation on a non-deslimed feed, to evaluate the potential for maximising Zn recovery.

Details of Tests

Flotation Test

Test No.: F1 **Project No.: 11419-002** **Operator: RU** **Date: Sept. 26, 07**

Purpose: To conduct a repeat of 11419-001's FF1-7 to explore response of the 100M material.

Procedure: As outlined below.

Feed: 1 kg of 100M cyclone UF material.

Grind:

Conditions:

	Reagents added, g/t						Time				Eh
	Na_2CO_3	Silicate N	Armac C	Na_2S	MIBC	P-40	Grind	Cond.	Froth	pH	mV
										7.8	80
ZnO Circuit											
Condition	300	750			10	750		5		8.8	50
ZnO Ro 1			90	1800				1			
					5				2	10.0	-140
ZnO Ro 2			30	600				1			
									2.5	10.2	-120
ZnO Ro 3			30	600				1	4	10.4	-130
Condition		150				400		3		9.8	-50
ZnO 1st Cln			25	250				1	3	9.8	-110
ZnO 1st Cln Scav			10	100	5			1	1	9.8	-120
Condition		50				200		3		9.8	-40
ZnO 2nd Cln 1			10	50				1	1		
ZnO 2nd Cln 2					5				2.5	9.4	-80
ZnO 3rd Clnr		50				150		3		8.4	-20
			5	50				1	2	9.3	-100

Stage	Rougher, 1st Clnr	2nd-3rd Clnrs		
Flotation Cell	500g-D1	250g-D1		
Speed: r.p.m.	1500	1200		

Metallurgical Balance

Product	**Weight**		**Assays, %, g/t**			**% Distribution**		
	g	**%**	**Zn**	**Fe**	**Ca**	**Zn**	**Fe**	**Ca**
ZnO 3rd Cln Con	113	11.2	**42.8**	**1.55**	**2.23**	**65.5**	**1.47**	**1.54**
ZnO 3rd Cln Tls	18.5	1.83	29.2	5.44	6.57	7.32	0.85	0.75
ZnO 2nd Cln Tls	13.6	1.35	11.10	13.5	12.6	2.05	1.54	1.05
ZnO 1st Cl Sc Tls	77.5	7.67	4.72	17.6	14.3	4.96	11.5	6.80
Rougher Tail	788	78.0	1.89	12.8	18.6	20.2	84.7	89.9
Head (calc.)	1011	100.0	7.30	11.8	16.1	100.0	100.0	100.0
(actual)			7.60	11.9	16.8			

Combined Products

ZnO 3rd Clnr Con		11.2	42.8	1.55	2.23	65.5	1.47	1.54
ZnO 2nd Clnr Con		13.0	**40.9**	2.10	2.84	**72.8**	2.31	2.29
ZnO 1st Cl Con		14.3	38.1	3.17	3.76	74.9	3.86	3.34
Ro Conc		22.0	26.5	8.19	7.43	79.8	15.3	10.1

Flotation Test

Test No.: F2 **Project No.: 11419-002** **Operator: RU** **Date: Sept. 26, 07**

Purpose: To conduct a repeat of 11419-001's FF1-7 to explore response of the 100M material.

Procedure: As outlined below.

Feed: 1 kg of 200M cyclone UF material.

Grind:

Conditions:

	Reagents added, g/t						Time				Eh
	Na_2CO_3	Silicate N	Armac C	Na_2S	MIBC	P-40	Grind	Cond.	Froth	pH	mV
										7.8	60
ZnO Circuit											
Condition	300	750				750		5		9.0	50
ZnO Ro 1			90	1800	5			1			
									2	10.0	-180
ZnO Ro 2			30	600	5			1			
									2.5	10.3	-160
ZnO Ro 3			30	600	5			1	4	10.4	-150
Condition		150				400		3		9.8	-40
ZnO 1st Cln			25	250	5			1	3	9.9	-140
ZnO 1st Cln Scav			10	100	10			1	2	9.8	-140
Condition		50				200		3		9.6	-60
ZnO 2nd Cln 1			10	50				1	1		
ZnO 2nd Cln 2					5				2.5	9.4	-90
ZnO 3rd Clnr		50				150		3		9.3	-20
			5	50	5			1	2	9.3	-100

Stage	Rougher, 1st Clnr	2nd-3rd Clnrs		
Flotation Cell	500g-D1	250g-D1		
Speed: r.p.m.	1500	1200		

Metallurgical Balance

Product	**Weight**		**Assays, %, g/t**			**% Distribution**		
	g	**%**	**Zn**	**Fe**	**Ca**	**Zn**	**Fe**	**Ca**
ZnO 3rd Cln Con	80.9	8.01	**40.7**	**1.78**	**3.34**	**43.1**	**1.22**	**1.68**
ZnO 3rd Cln Tls	9.9	0.98	20.7	6.43	10.2	2.68	0.54	0.63
ZnO 2nd Cln Tls	12.6	1.25	8.74	12.3	14.5	1.44	1.31	1.14
ZnO 1st Cl Sc Tls	43.1	4.27	3.62	16.2	17.2	2.04	5.89	4.62
Rougher Tail	863	85.5	4.49	12.5	17.1	50.7	91.0	91.9
Head (calc.)	1010	100.0	7.56	11.7	15.9	100.0	100.0	100.0
(actual)			7.82	12.3	16.2			

Combined Products

ZnO 3rd Clnr Con		8.01	40.7	1.78	3.34	43.1	1.22	1.68
ZnO 2nd Clnr Con		8.99	**38.5**	2.29	4.09	**45.8**	1.75	2.31
ZnO 1st Cl Con		10.2	34.9	3.51	5.36	47.3	3.06	3.45
Ro Conc		14.5	25.7	7.24	8.84	49.3	8.95	8.07

Flotation Test

Test No.: F3 **Project No.: 11419-002** **Operator: RU** **Date: 15-Oct-07**

Purpose: To conduct a rougher cleaner test on the FF2 UF material using a decreased amount of depressant.

Procedure: As outlined below.

Feed: 1 kg of FF2 cyclone UF material.

Grind:

Conditions: K_{80} (µm): 73

	Reagents added, g/t						Time				Eh
	Na_2CO_3	Silicate N	Armac C	Na_2S	MIBC	P-40	Grind	Cond.	Froth	pH	mV
										7.9	200
ZnO Circuit											
Condition	300	500				500		5		9.4	100
ZnO Ro 1			90	1800				1			
									2		
ZnO Ro 2			30	600	5			1			
									2.5	10.8	-240
ZnO Ro 3			30	600	10			1	4	10.8	-300

Stage	Rougher, 1st Clnr			
Flotation Cell	500g-D1			
Speed: r.p.m.	1500			

Metallurgical Balance

Product	**Weight**		**Assays, %, g/t**			**% Distribution**		
	g	**%**	**Zn**	**Fe**	**Ca**	**Zn**	**Fe**	**Ca**
Ro Conc 1	99.7	9.80	40.6	2.22	5.77	47.8	3.05	3.09
Ro Conc 2	114	11.2	31.0	3.85	9.11	41.9	6.07	5.58
Ro Conc 3	76.2	7.49	4.11	7.27	17.5	3.70	7.64	7.15
Rougher Tail	727	71.5	0.77	8.30	21.6	6.61	83.2	84.2
Head (calc.)	1017	100.0	8.32	7.13	18.3	100.0	100.0	100.0
(actual)			8.40	7.49	18.3			

Combined Products

Ro Conc 1		9.80	40.6	2.22	5.77	47.8	3.05	3.09
Ro Conc 1-2		21.0	35.5	3.09	7.55	89.7	9.13	8.67
Ro Conc		28.5	27.2	4.19	10.2	93.4	16.8	15.8

Flotation Test

Test No.: F4 **Project No.: 11419-002** **Operator: RU** **Date: 15-Oct-07**

Purpose: To conduct a rougher cleaner test on the FF2 UF material using an increased amount of depressant.

Procedure: As outlined below.

Feed: 1 kg of FF2 cyclone UF material.

Grind:

Conditions: K_{80} (µm): 73

	Reagents added, g/t						Time				Eh
	Na_2CO_3	Silicate N	Armac C	Na_2S	MIBC	P-40	Grind	Cond.	Froth	pH	mV
										7.9	200
ZnO Circuit											
Condition	300	500				500		5		9.4	80
				1800				1			
Condition		500				500		3			
ZnO Ro 1			90	300				1			
									2	10.6	-270
ZnO Ro 2			30	600	5			1			
									2.5	10.7	-270
ZnO Ro 3			30	600	10			1	4	10.7	-300

Stage	Rougher, 1st Clnr			
Flotation Cell	500g-D1			
Speed: r.p.m.	1500			

Metallurgical Balance

Product	**Weight**		**Assays, %, g/t**			**% Distribution**		
	g	**%**	**Zn**	**Fe**	**Ca**	**Zn**	**Fe**	**Ca**
Ro Conc 1	155	15.3	40.2	2.50	5.10	75.0	5.52	4.10
Ro Conc 2	63.0	6.20	21.4	4.59	12.6	16.2	4.11	4.11
Ro Conc 3	47.3	4.66	3.39	6.33	18.3	1.93	4.25	4.48
Rougher Tail	750	73.8	0.76	8.09	22.5	6.84	86.1	87.3
Head (calc.)	1016	100.0	8.20	6.94	19.0	100.0	100.0	100.0
(actual)			8.40	7.49	18.3			

Combined Products

Ro Conc 1		15.3	40.2	2.50	5.10	75.0	5.52	4.10
Ro Conc 1-2		21.5	34.8	3.10	7.26	91.2	9.62	8.21
Ro Conc		26.2	29.2	3.68	9.23	93.2	13.9	12.7

Flotation Test

Test No.: F5 **Project No.: 11419-002** **Operator: RU** **Date: 29-Oct-07**

Purpose: To conduct a rougher cleaner test on the new 150M UF material using in a series of tests altering the amount of depressant.

Procedure: As outlined below.

Feed: 1 kg of new 150M cyclone UF material.

Grind:

Conditions: K_{80} (µm): 70

	Reagents added, g/t						Time				Eh
	Na_2CO_3	Silicate N	Armac C	Na_2S	MIBC	P-40	Grind	Cond.	Froth	pH	mV
ZnO Circuit											
Condition	300	500				1000		5		9.3	80
ZnO Ro 1			90	1800	5			1			
									2	10.5	-190
ZnO Ro 2			30	600	5			1			
									2.5	10.6	-200
ZnO Ro 3			30	600	10			1	4	10.6	-180

Stage	Rougher, 1st Clnr			
Flotation Cell	500g-D1			
Speed: r.p.m.	1500			

Metallurgical Balance

Product	**Weight**		**Assays, %, g/t**			**% Distribution**		
	g	**%**	**Zn**	**Fe**	**Ca**	**Zn**	**Fe**	**Ca**
Ro Conc 1	57.8	6.05	29.0	5.42	8.10	22.0	2.84	3.12
Ro Conc 2	87.7	9.18	34.8	6.11	5.48	40.0	4.85	3.20
Ro Conc 3	75.1	7.86	21.9	10.5	7.10	21.6	7.14	3.56
Rougher Tail	735	76.9	1.70	12.8	18.4	16.4	85.2	90.1
Head (calc.)	955	100.0	7.98	11.6	15.7	100.0	100.0	100.0
(actual)			7.89	11.3	17.0			

Combined Products

Ro Conc 1		6.05	29.0	5.42	8.10	22.0	2.84	3.12
Ro Conc 1-2		15.2	32.5	5.84	6.52	62.0	7.69	6.33
Ro Conc		23.1	28.9	7.42	6.72	83.6	14.8	9.88

Flotation Test

Test No.: F6 **Project No.: 11419-002** **Operator: RU** **Date: 29-Oct-07**

Purpose: To conduct a rougher cleaner test on the new 150M UF material using in a series of tests altering the amount of depressant.

Procedure: As outlined below.

Feed: 1 kg of new 150M cyclone UF material.

Grind:

Conditions: K_{80} (µm): 70

	Reagents added, g/t						Time				Eh
	Na_2CO_3	Silicate N	Armac C	Na_2S	MIBC	P-40	Grind	Cond.	Froth	pH	mV
ZnO Circuit											
Condition	300	250				1000		5		9.3	60
ZnO Ro 1			90	1800	5			1			
									2	10.6	-160
ZnO Ro 2			30	600	5			1			
									2.5	10.7	-180
ZnO Ro 3			30	600	10			1	4	10.6	-180

Stage	Rougher, 1st Clnr			
Flotation Cell	500g-D1			
Speed: r.p.m.	1500			

Metallurgical Balance

Product	**Weight**		**Assays, %, g/t**			**% Distribution**		
	g	**%**	**Zn**	**Fe**	**Ca**	**Zn**	**Fe**	**Ca**
Ro Conc 1	73.8	7.76	32.8	4.73	7.36	31.9	3.27	3.45
Ro Conc 2	83.1	8.74	36.3	5.72	5.05	39.7	4.45	2.67
Ro Conc 3	59.8	6.29	16.6	11.2	7.72	13.1	6.28	2.93
Rougher Tail	734	77.2	1.59	12.5	19.5	15.4	86.0	90.9
Head (calc.)	951	100.0	7.99	11.2	16.6	100.0	100.0	100.0
(actual)			7.89	11.3	17.0			

Combined Products

Ro Conc 1		7.76	32.8	4.73	7.36	31.9	3.27	3.45
Ro Conc 1-2		16.5	34.7	5.25	6.14	71.6	7.73	6.12
Ro Conc		22.8	29.7	6.90	6.57	84.6	14.0	9.05

Flotation Test

Test No.: F7 **Project No.: 11419-002** **Operator: RU** **Date: 29-Oct-07**

Purpose: To conduct a rougher cleaner test on the new 150M UF material using in a series of tests altering the amount of depressant.

Procedure: As outlined below.

Feed: 1 kg of new 150M cyclone UF material.

Grind:

Conditions: K_{80} (µm): 70

	Reagents added, g/t						Time				Eh
	Na_2CO_3	Silicate N	Armac C	Na_2S	MIBC	P-40	Grind	Cond.	Froth	pH	mV
ZnO Circuit											
Condition	300	0				1000		5		9.0	50
ZnO Ro 1			90	1800	5			1			
									2	10.6	-150
ZnO Ro 2			30	600	5			1			
									2.5	10.8	-180
ZnO Ro 3			30	600	5			1	4	10.7	-150

Stage	Rougher, 1st Clnr			
Flotation Cell	500g-D1			
Speed: r.p.m.	1500			

Metallurgical Balance

Product	**Weight**		**Assays, %, g/t**			**% Distribution**		
	g	**%**	**Zn**	**Fe**	**Ca**	**Zn**	**Fe**	**Ca**
Ro Conc 1	53.4	5.56	32.1	4.63	8.06	22.6	2.26	2.73
Ro Conc 2	91.9	9.57	38.1	4.76	5.26	46.2	4.01	3.07
Ro Conc 3	50.1	5.22	19.2	10.5	9.05	12.7	4.82	2.88
Rougher Tail	765	79.6	1.83	12.7	18.8	18.5	88.9	91.3
Head (calc.)	960	100.0	7.89	11.4	16.4	100.0	100.0	100.0
(actual)			7.89	11.3	17.0			

Combined Products

Ro Conc 1		5.56	32.1	4.63	8.06	22.6	2.26	2.73
Ro Conc 1-2		15.1	35.9	4.71	6.29	68.8	6.27	5.80
Ro Conc		20.4	31.6	6.20	7.00	81.5	11.1	8.68

Flotation Test

Test No.: F8 **Project No.: 11419-002** **Operator: RU** **Date: 29-Oct-07**

Purpose: To conduct a rougher cleaner test on the new 150M UF material using in a series of tests altering the amount of depressant.

Procedure: As outlined below.

Feed: 1 kg of new 150M cyclone UF material.

Grind:

Conditions: K_{80} (µm): 70

	Reagents added, g/t						Time				Eh
	Na_2CO_3	Silicate N	Armac C	Na_2S	MIBC	P-40	Grind	Cond.	Froth	pH	mV
ZnO Circuit											
Condition	300	1000				500		5		9.6	40
ZnO Ro 1			90	1800	5			1			
									2	10.5	-240
ZnO Ro 2			30	600	5			1			
									2.5	10.6	-240
ZnO Ro 3			30	600	10			1	4	10.6	-240

Stage	Rougher, 1st Clnr			
Flotation Cell	500g-D1			
Speed: r.p.m.	1500			

Metallurgical Balance

Product	**Weight**		**Assays, %, g/t**			**% Distribution**		
	g	**%**	**Zn**	**Fe**	**Ca**	**Zn**	**Fe**	**Ca**
Ro Conc 1	36.7	3.82	22.8	6.34	10.9	11.1	2.21	2.49
Ro Conc 2	87.2	9.07	32.6	8.42	5.81	37.7	6.96	3.15
Ro Conc 3	105	10.9	21.9	16.0	5.81	30.3	15.8	3.77
Rougher Tail	733	76.2	2.15	10.8	19.9	20.9	75.0	90.6
Head (calc.)	961	100.0	7.85	11.0	16.7	100.0	100.0	100.0
(actual)			7.89	11.3	17.0			

Combined Products

Ro Conc 1		3.82	22.8	6.34	10.9	11.1	2.21	2.49
Ro Conc 1-2		12.9	29.7	7.80	7.32	48.8	9.17	5.63
Ro Conc		23.8	26.1	11.6	6.63	79.1	25.0	9.41

Flotation Test

Test No.: F9 **Project No.: 11419-001** **Operator: RU** **Date: 11/30/2007**

Purpose: To conduct a repeat of FF1-7 to confirm metallurgical results.

Procedure: As outlined below.

Feed: 1 kg of new 150M cyclone UF material.

Grind:

Conditions: K_{80} (µm): 70

	Reagents added, g/t						Time				Eh
	Na_2CO_3	Silicate N	Armac C	Na_2S	MIBC	P-40	Grind	Cond.	Froth	pH	mV
										8.3	240
ZnO Circuit											
Condition	300	750				750		5		9.5	180
ZnO Ro 1			90	1800				1			
									2	10.3	-120
ZnO Ro 2			30	600				1			
									2.5	10.4	-120
ZnO Ro 3			30	600	10			1	4	10.5	-140

Stage	Rougher, 1st Clnr			
Flotation Cell	500g-D1			
Speed: r.p.m.	1500			

Metallurgical Balance

Product	**Weight**		**Assays, %, g/t**			**% Distribution**		
	g	**%**	**Zn**	**Fe**	**Ca**	**Zn**	**Fe**	**Ca**
Ro Conc 1	20.9	2.15	14.1	7.90	10.3	3.93	1.52	1.33
Ro Conc 2	60.4	6.23	32.4	6.33	5.29	26.1	3.52	1.97
Ro Conc 3	69.5	7.16	26.3	10.6	5.57	24.4	6.78	2.39
Rougher Tail	819	84.5	4.18	11.70	18.7	45.6	88.2	94.3
Head (calc.)	970	100.0	7.74	11.2	16.7	100.0	100.0	100.0
(actual)			7.89	11.3	17.0			

Combined Products

Ro Conc 1		2.15	14.1	7.90	10.3	3.93	1.52	1.33
Ro Conc 1-2		8.38	27.7	6.73	6.58	30.0	5.04	3.30
Ro Conc 1-3		15.5	27.1	8.52	6.11	54.4	11.8	5.69

Flotation Test

Test No.: F10 **Project No.: 11419-003** **Operator: RU** **Date: 01/09/2008**

Purpose: To conduct a repeat of F6 with increased amounts of collector and sulphidizer.

Procedure: As outlined below.

Feed: 1 kg of new 150M cyclone UF material.

Grind:

Conditions: K_{80} (µm): 70

	Reagents added, g/t						Time				Eh
	Na_2CO_3	Silicate N	Armac C	Na_2S	MIBC	P-40	Grind	Cond.	Froth	pH	mV
ZnO Circuit											
Condition	300	750				750		5		9.5	100
ZnO Ro 1			125	2500	5			1			
									2	10.8	-280
ZnO Ro 2			45	900	5			1			
									2.5	11.0	-300
ZnO Ro 3			45	900	10			1	4	11.2	-310

Stage	Rougher, 1st Clnr			
Flotation Cell	500g-D1			
Speed: r.p.m.	1500			

Metallurgical Balance

Product	**Weight**		**Assays, %, g/t**			**% Distribution**		
	g	**%**	**Zn**	**Fe**	**Ca**	**Zn**	**Fe**	**Ca**
Ro Conc 1	56.9	5.80	32.0	5.53	4.99	23.1	2.75	1.99
Ro Conc 2	96.8	9.88	36.7	6.36	4.25	45.1	5.37	2.89
Ro Conc 3	58.5	5.97	20.8	11.9	8.47	15.5	6.08	3.48
Rougher Tail	768	78.4	1.67	12.8	17.0	16.3	85.8	91.6
Head (calc.)	980	100.0	8.03	11.7	14.5	100.0	100.0	100.0
(actual)			7.89	11.3	17.0			

Combined Products

Ro Conc 1		5.80	32.0	5.53	4.99	23.1	2.75	1.99
Ro Conc 1-2		15.7	35.0	6.05	4.52	68.3	8.12	4.88
Ro Conc 1-3		21.6	31.1	7.66	5.61	83.7	14.2	8.36

Flotation Test

Test No.: F11 **Project No.: 11419-003** **Operator: RU** **Date: 01/31/2008**

Purpose: To conduct a rougher cleaner test with increased collector and decreased silicate.

Procedure: As outlined below.

Feed: 1 kg of new 150M cyclone UF material.

Grind:

Conditions: K_{80} (µm): 70

	Reagents added, g/t						Time				Eh
	Na_2CO_3	Silicate N	Armac C	Na_2S	MIBC	P-40	Grind	Cond.	Froth	pH	mV
ZnO Circuit											
Condition	300	250				1000		5		9.2	60
ZnO Ro 1			150	3000				1			
									2	11.0	-280
ZnO Ro 2			50	1000	5			1			
									2.5	11.4	-300
ZnO Ro 3			100	1000	30			1	5.5	11.5	-270
Condition		75				300		3		11.1	-250
ZnO 1st Cln			40	400	20			1	3	11.1	-270
ZnO 1st Cln Scav			10	100	10			1	2	11.0	-270
Condition		25				100		3		10.8	-220
ZnO 2nd Cln 1			10	50				1	1		
ZnO 2nd Cln 2					5				2.5		

Stage	Rougher, 1st Clnr	2nd-3rd Clnrs		
Flotation Cell	500g-D1	250g-D1		
Speed: r.p.m.	1500	1200		

Metallurgical Balance

Product	**Weight**		**Assays, %, g/t**			**% Distribution**		
	g	**%**	**Zn**	**Fe**	**Ca**	**Zn**	**Fe**	**Ca**
ZnO 2nd Cln Con	174	17.9	**37.5**	**5.20**	**2.92**	**82.5**	**8.26**	**3.31**
ZnO 2nd Cln Tls	13.3	1.37	5.75	14.3	15.3	0.97	1.74	1.33
ZnO 1st Cl Sc Con	5.20	0.54	9.19	15.1	10.5	0.60	0.72	0.36
ZnO 1st Cl Sc Tls	44.6	4.59	3.53	13.4	17.1	1.99	5.46	4.97
Rougher Tail	734	75.6	1.50	12.5	18.8	13.9	83.8	90.0
Head (calc.)	971	100.0	8.14	11.3	15.8	100.0	100.0	100.0
(actual)			7.89	11.3	17.0			

Combined Products

ZnO 2nd Clnr Con		17.9	37.5	5.20	2.92	82.5	8.26	3.31
ZnO 1st Cl Con		19.3	35.2	5.85	3.80	83.5	10.0	4.64
Ro Conc		24.4	28.7	7.47	6.45	86.1	16.2	10.0

Flotation Test

Test No.: LCT **Project No.: 11419-003** **Operator: RU** **Date: 02/13/2008**

Purpose: To conduct a locked cycle test with increased collector and decreased silicate.

Procedure: As outlined below.

Feed: 6 x 1 kg of new 150M cyclone UF material.

Grind:

Conditions: K_{80} (µm): 70

	Reagents added, g/t						Time				Eh
	Na_2CO_3	Silicate N	Armac C	Na_2S	MIBC	P-40	Grind	Cond.	Froth	pH	mV
ZnO Circuit											
Condition	300	250				1000		5		9.2	60
ZnO Ro 1			175	3000				1			
									2	11.0	-280
ZnO Ro 2			75	1500	5			1			
									2.5	11.4	-300
ZnO Ro 3			125	1500	30			1	6	11.5	-270
Condition		75				300		3		11.1	-250
ZnO 1st Cln			40	400	20			1	3	11.1	-270
ZnO 1st Cln Scav			10	100	10			1	2	11.0	-270
Condition		25				200		3		10.8	-220
ZnO 2nd Cln 1			10	50				1	1		
ZnO 2nd Cln 2					5				2		

Stage	Rougher, 1st Clnr	2nd-3rd Clnrs
Flotation Cell	500g-D1	250g-D1
Speed: r.p.m.	1500	1200

Test No.: LCT **Project No.: 11419-003** **Operator: RU** **Date: 02/13/2008**
Test No.: LCT **Project No.: 11419-003** **Operator: RU** **Date: 02/13/2008**

Metallurgical Projection (C-F)

Product	Weight	Assays, %			% Distribution		
	%	Zn	Fe	Ca	Zn	Fe	Ca
2nd Cl Concentrate	17.3	38.4	3.93	3.61	82.2	6.08	4.28
1st Cl Scav Tail	10.3	3.14	13.7	18.0	4.01	12.6	12.8
Ro Tail	72.0	1.54	12.6	16.8	13.7	81.3	83.0
Head	100.0	8.08	11.2	14.6	100.0	100.0	100.0

Metallurgical Balance

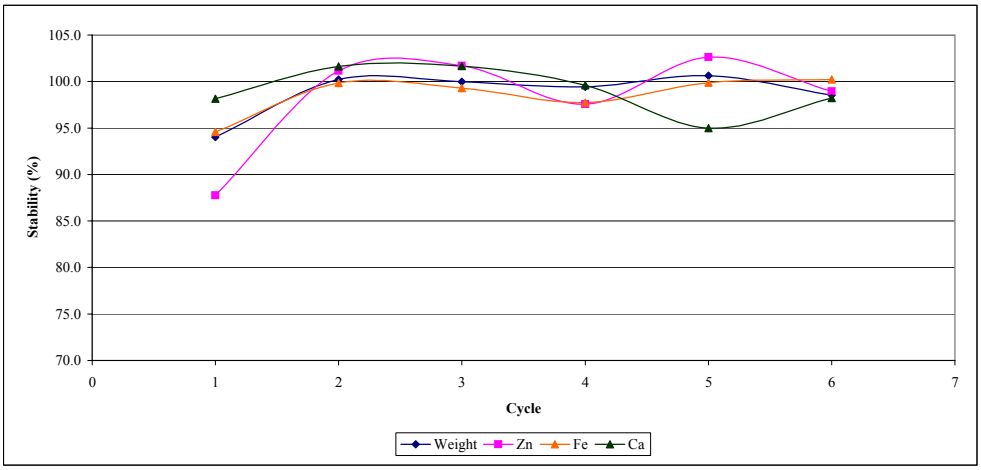
Product	Weight		Assays, %			% Distribution		
	g	%	Zn	Fe	Ca	Zn	Fe	Ca
2nd Clnr Conc A	142.9	2.41	39.5	3.22	3.06	11.8	0.69	0.50
2nd Clnr Conc B	172.2	2.91	38.4	3.54	3.16	13.8	0.91	0.62
2nd Clnr Conc C	171.5	2.90	38.8	3.92	3.53	13.9	1.01	0.69
2nd Clnr Conc D	163.9	2.77	38.7	3.65	3.38	13.3	0.90	0.63
2nd Clnr Conc E	175.9	2.97	38.3	4.03	3.83	14.1	1.06	0.77
2nd Clnr Conc F	171.1	2.89	38.0	4.12	3.67	13.6	1.06	0.72
2nd Cln Tls F	43.6	0.74	11.9	13.3	11.6	1.09	0.87	0.58
1st Cl Sc Con F	27.8	0.47	10.5	13.0	12.2	0.61	0.54	0.39
1st Cl Sc Tls A	95.7	1.62	2.98	13.6	17.6	0.60	1.95	1.92
1st Cl Sc Tls B	117	1.97	3.08	14.3	17.4	0.75	2.50	2.32
1st Cl Sc Tls C	109	1.84	3.16	13.5	17.8	0.72	2.21	2.22
1st Cl Sc Tls D	104	1.76	3.18	13.7	17.8	0.69	2.14	2.12
1st Cl Sc Tls E	97.1	1.64	3.02	13.6	18.6	0.61	1.98	2.06
1st Cl Sc Tls F	97.5	1.65	3.18	13.9	17.8	0.65	2.03	1.98
Ro Tls A	689	11.6	1.53	12.7	17.7	2.21	13.1	13.9
Ro Tls B	700	11.8	1.54	12.6	17.5	2.26	13.2	14.0
Ro Tls C	706	11.9	1.55	12.6	17.4	2.29	13.3	14.0
Ro Tls D	713	12.0	1.53	12.4	17.0	2.29	13.3	13.8
Ro Tls E	720	12.2	1.58	12.6	15.8	2.38	13.6	13.0
Ro Tls F	704	11.9	1.51	12.9	17.0	2.23	13.6	13.7
Head (calc)	5921.3	100.0	8.06	11.3	14.8	100.0	100.0	100.0
Head (direct)			7.89	11.3	17.0			

Combined Products

2nd Cl Conc A-F	998	16.8	38.6	3.76	3.45	80.6	5.63	3.93
Cl Tails	71.4	1.21	11.4	13.2	11.8	1.70	1.41	0.97
Cl Scav Tail A-F	620	10.5	3.10	13.8	17.8	4.03	12.8	12.6
Ro Tail A-F	4232	71.5	1.54	12.6	17.1	13.7	80.1	82.5

Stability Check

Cycle	Wt%	Zn	Fe	Ca
A	94.0	87.8	94.6	98.2
B	100.2	101.2	99.8	101.6
C	100.0	101.7	99.3	101.6
D	99.4	97.6	97.7	99.6
E	100.6	102.6	99.9	95.0
F	98.5	99.0	100.2	98.2
Avg C-F	99.6	100.2	99.3	98.6



APPENDIX

X. SOFTWARE PROGRAMS USED

SOFTWARE PROGRAMS

The following software programs were used during the drilling and exploration program, and in the preparation of this report:

1. Microsoft Office (Word and Excel)
2. Microsoft Access
3. Garmin GPS software
4. Corel Draw
5. AutoCAD
6. Micromine
7. Adobe Photoshop

APPENDIX

XI. REFERENCES

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